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PRZEDMOWA

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PRÉFACE

„L'annuaire météorologique 1957" a été élaboré par l'Établissement des Annuaires et Monographies Météorologiques de l'Institut Hydrologique et Météorologique d'État, sous la direction et rédaction de mag. Feliks Janiszewski; y ont collaboré: ing. Krystyna Brzostek, Wanda Gawałko et Wanda Plak.

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OBJAŚNIENIA

Użyte w niniejszym roczniku symbole mają następujące znaczenie:

φ — szerokość geograficzna.

λ — długość geograficzna.

H_s — wysokość terenu ogródka meteorologicznego nad średnim poziomem morza.

H_b — wysokość barometru nad średnim poziomem morza.

Dla stacji posiadających barometry H_s i H_b zostały wyznaczone za pomocą niwelacji, dla pozostałych stacji H_s wyznaczono z mapy topograficznej.

h_w — wysokość wiatromierza nad powierzchnią gruntu.

m — w połączeniu z literowym symbolem elementu oznacza wartość średnią miesięczną (np. U_m oznacza średnią miesięczną wilgotność względną).

P — ciśnienie atmosferyczne w milibarach, zredukowane do 0° i do ciężkości normalnej.

$P_{o,m}$ — wartość średnia miesięczna ciśnienia atmosferycznego, sprowadzona do średniego poziomu morza.

T — temperatura w °C.

Temperaturę wyznaczano za pomocą termometrów umieszczonych w klatce meteorologicznej typu angielskiego na wysokości 2 m nad powierzchnią gruntu. Skrajne dobowe wartości temperatur odnoszą się do okresu od III obserwacji dnia poprzedniego do III obserwacji danego dnia.

$\overline{Max}$ — średnia miesięczna z wartości temperatur maksymalnych dobowych.

$\overline{Min}$ — średnia miesięczna z wartości temperatur minimalnych dobowych.

U — wilgotność względna w procentach.

Δ — niedosyt wilgotności w milibarach.

N — zachmurzenie w skali 11-stopniowej (przy tym 0 oznacza niebo bezchmurne, zaś 10 — niebo całkowicie pokryte chmurami).

W tablicy I rocznika obok wartości zachmurzenia podane są za pomocą symboli również dane o zjawiskach zaobserwowanych podczas obserwacji terminowych.

D — kierunek wiatru.

v — prędkość wiatru w m/sek.

n_D — częstotliwość występowania poszczególnych kierunków wiatru.

v_{mD} — średnia prędkość wiatru wg kierunków.

Obserwacje nad wiatrem były dokonywane (z nielicznymi wyjątkami) przy użyciu wiatromierzy Wilda.

R — wysokość opadu w milimetrach.

Wysokość opadu odnosi się do okresu od I (porannej) obserwacji jednego dnia do I obserwacji dnia następnego i jest podawana pod datą dnia poprzedniego. Obserwacje te były dokonywane za pomocą deszczomierzy Hellmanna o powierzchni otworu 200 cm^2, umieszczonych na wysokości 1 m nad powierzchnią gruntu, z wyjątkiem części stacji górskich, położonych powyżej 500 m nad poziomem morza, gdzie używa się deszczomierzy typu górskiego, mających powierzchnię otworu 500 cm^2 i umieszczonych na wysokości 1,5 m nad powierzchnią gruntu.

V — widzialność z II terminu obserwacji, wyrażona w następującej skali międzynarodowej:

0 — przedmioty są niewidoczne już z odległości mniejszej od 50 m;

1 — przedmioty są widoczne z odległości 50 m, lecz niewidoczne z odległości 200 m;

2 — przedmioty są widoczne z odległości 200 m, lecz niewidoczne z odległości 500 m;

3 — przedmioty są widoczne z odległości 500 m, lecz niewidoczne z odległości 1 km;

4 — przedmioty są widoczne z odległości 1 km, lecz niewidoczne z odległości 2 km;

5 — przedmioty są widoczne z odległości 2 km, lecz niewidoczne z odległości 4 km;

6 — przedmioty są widoczne z odległości 4 km, lecz niewidoczne z odległości 10 km;

7 — przedmioty są widoczne z odległości 10 km, lecz niewidoczne z odległości 20 km;

8 — przedmioty są widoczne z odległości 20 km, lecz niewidoczne z odległości 50 km;

9 — przedmioty są widoczne z odległości 50 km i więcej.

h — grubość pokrywy śnieżnej w centymetrach wg obserwacji dokonywanych w I terminie.

pł. — śnieg w płatach.

Usłonecznienie — w godzinach. Obserwacji dokonywano za pomocą heliografów Campbell—Stokes'a.

n — liczba dni z poszczególnymi zjawiskami.

Za dzień z mgłą przyjęto w niniejszym roczniku dzień, w którym to zjawisko powodowało zmniejszenie się widzialności poniżej 1 km.

Za dni pogodne uważa się takie, w których średnia wartość zachmurzenia wyznaczona z trzech terminów jest mniejsza od 2.0, zaś za dni pochmurne — w których wartość ta jest większa od 8.0.

I, II, III — terminy obserwacji (7^h, 13^h i 21^h średniego miejscowego czasu słonecznego).

Dies — średnia dobowa, obliczona dla temperatury wg wzoru:

śr. = 1/4 (I + II + 2 × III), a dla pozostałych elementów

śr. = 1/3 (I + II + III).

Natężenie zjawisk oznaczono za pomocą małych cyferek: ^{0}, ^{1} albo ^{2} umieszczonych z prawej strony u góry odpowiedniego symbolu („^{0}" oznacza zjawisko o natężeniu słabym, „^{1}" o natężeniu umiarkowanym, a „^{2}" o natężeniu silnym; w przypadku mgły cyferki te oznaczają odpowiednio: mgłę umiarkowaną, mgłę gęstą i mgłę bardzo gęstą).

Do oznaczania czasu obok godzin i minut użyto następujących symboli:

n — czas od III obserwacji dnia poprzedniego do I obserwacji dnia danego,

na — czas od północy do I obserwacji dnia danego,

a — czas między I a II terminem obserwacji,

p — czas między II a III terminem obserwacji,

np — czas od III obserwacji do północy.

Przerwy w czasie trwania zjawiska oznaczono wielokropkiem (...) lub skrótem „z prz.".

Kropka (.) postawiona na miejscu wartości liczbowej oznacza brak zjawiska, kreska (—) zaś brak danych, wartości wątpliwe podano ze znakiem zapytania (?), wartości oszacowane podano w nawiasach.

NOTE EXPLICATIVE

Les symboles employés dans le présent annuaire signifient ce qui suit:

φ — latitude géographique.

λ — longitude géographique.

H_s — hauteur du terrain du jardin météorologique, au-dessus du niveau moyen de la mer.

H_b — hauteur du baromètre au-dessus du niveau de la mer.

Pour les stations disposant d'un baromètre H_b et H_s, ces données ont été déterminées à l'aide de nivellement, pour les autres stations H_s elles l'ont été d'après la carte topographique.

h_w — hauteur d'une girouette au-dessus du sol.

m — joint à une lettre-symbole de l'élément, indique la valeur mensuelle moyenne (p.e. U_m — indique la valeur mensuelle moyenne de l'humidité relative).

P — pression atmosphérique en millibars, réduite à 0° et à la gravité normale.

$P_{o,m}$ — moyenne d'une valeur mensuelle de la pression atmosphérique, réduite au niveau moyen de la mer.

T — température en C°.

La température a été mesurée à l'aide de thermomètres installés dans un abri météorologique du type anglais à une hauteur de 2 mètres au-dessus du sol. Les températures diurnes extrêmes se rapportent à une période partant de la III-ème observation du jour précédent à la III-ème observation du jour donné.

$\overline{Max}$ — valeur mensuelle moyenne des maxima des températures diurnes.

$\overline{Min}$ — valeur mensuelle moyenne des valeurs minima des températures diurnes.

U — humidité relative en %.

Δ — déficit de l'humidité en millibars.

N — nébulosité en échelle 11° (0 signifie ciel serein, 10 — ciel entièrement couvert par les nuages). Dans la table I de l'annuaire, à côté des valeurs de la nébulosité, figurent aussi les données se rapportant aux phénomènes remarqués au cours des observations normales, et consignées à l'aide de symboles.

D — direction du vent.

v — vitesse du vent en m/sec.

n_D — fréquence de l'apparition des directions du vent.

v_{mD} — vitesse moyenne du vent selon la direction. Les observations sur le vent ont été faites (avec quelques exceptions) à l'aide d'une girouette, modèle Wild.

R — hauteur de la précipitation en mm. L'hauteur dè la précipitation se rapporte à la période comprise entre la première observation (matinale) d'un jour et l'observation du jour suivant. Elle se trouve inscrite à la date du jour précédent. Ces observations ont été faites à l'aide de pluviomètres, modèle Hellmann, dont la superficie de l'ouverture mesure 200 cm², placés à 1 m au-dessus du sol, à l'exception, toutefois, de certaines stations de montagne, situées à une hauteur qui dépasse 500 m au-dessus du niveau de la mer, où l'on emploie des pluviomètres, de type montagnard, à orifice mesurant 500 cm² et placés à une hauter de 1,5 m au-dessus du sol.

V — visibilité à l'heure de la II-ème observation, exprimée d'après l'échelle internationale:

0 — les objets sont invisibles déjà à une distance inférieure à 50 m;

1 — les objets sont visibles à 50 m, mais invisibles à 200 m de distance;

2 — les objets sont visibles à 200 m, mais invisibles à 500 m de distance;

3 — les objets sont visibles à 500 m, mais invisibles à 1000 m de distance;

4 — les objets sont visibles à 1 km, mais invisibles à 2 km;

5 — les objets sont visibles à 2 km, mais invisibles à 4 km;

6 — les objets sont visibles à 4 km, mais invisibles à 10 km;

7 — les objets sont visibles à 10 km, mais invisibles à 20 km;

8 — les objets sont visibles à 20 km, mais invisiblès à 50 km;

9 — les objets sont visibles à partir de 50 km de distance.

h — épaisseur de la couche de neige en centimètres selon l'observation enregistrée dans le premier délai.

pl. — neige éparse.

Insolation — en heures. Les observations effectuées à l'aide d'héliographes Campbell-Stokes.

n — nombre des jours avec phénomènes particuliers.

Dans le présent annuaire, on entend par jour avec brouillard le jour où ce phénomène entraine une diminution de visibilité au-dessous de 1 km.

Dans le présent annuaire, on entend par jours sereins les jours dont la valeur moyenne de nébulosité, résultant de trois délais, est inférieure à 2.0 et par jours couverts les jours où cette valeur est supérieure à 8.0.

I, II, III — les délais d'observations (7^h, 13^h, et 21^h du temps moyen solaire local).

Dies — moyenne diurne, calculée pour la température d'après la formule:

$m = 1/4\ (I + II + 2 \times III)$, et pour les autres éléments $m = 1/3\ (I + II + III)$.

L'intensité du phenomène est marquée en petits chiffres: $^{0,\ 1}$ ou ^{2} placés du coté droit en haut du symbole respectif: („^{0}" indique le phénomène dont l'intensité est faible, „^{1}" modérée et „^{2}" forte; en cas de brouillard modéré, brouillard épais et brouillard très épais).

Pour indiquer le temps (à part les heures et les minutes), on a utilisé les symboles suivants:

n — le temps écoulé depuis la III-ème observation du jour précédent jusqu'à la I-ère observation du jour donné,

na — le temps écoulé depuis minuit jusqu'à l'observation du jour donné,

a — intervalle de temps entre la I-ère et la II-ème observation,

p — intervalle de temps entre la II-ème et la III-ème observation,

np — intervalle de temps entre la III-ème observation et minuit.

Les intervalles de temps, dans la durée d'un phénomène sont indiqués par des points de suspension (...) ou par une abréviation „z prz.".

Un point (.) mis à la place d'une valeur numérique marque l'absence d'un phénomène; un trait d'union (—) indique le défaut de données; un point d'interrogation (?) signale les valeurs douteuses; les parenthèses enferment les valeurs éstimées.

Wykaz użytych w roczniku symboli meteorologicznych

Les symboles météorologiques employés dans l'annuaire

deszcz	— pluie
mżawka	— bruine
śnieg	— neige
deszcz ze śniegiem	— pluie et neige
śnieg ziarnisty	— neige en grains
krupy miękkie	— neige roulée
krupy twarde	— grésil
deszcz lodowy	— grains de glace
grad	— grêle
igły lodowe	— aiguilles de glace
(pod symbolem opadu) opad przelotny	— (sous symbole de précipitation) averses
rosa	— rosée
szron	— gelée blanche
szadź miękka	— givre mou
szadź twarda	— givre dur
gołoledź	— verglas
mgła	— brouillard
mgła przyziemna	— brouillard épais au sol
zamglenie	— brume
mgła (niebo widoczne)	— brouillard (ciel visible)
mgła z kryształków lodu	— brouillard glacé
wiatr 10 – 15 m/sek	— vent 10 – 15 m/sec
wiatr > 15 m/sek	— vent > 15 m/sec
burza	— orage
burza odległa	— orage lointain
błyskawica	— éclair
zorza polarna	— aurore boréale
tęcza	— arc-en-ciel
halo naokoło słońca	— halo solaire
halo naokoło księżyca	— halo lunaire
wieniec naokoło słońca	— couronne autour du soleil
wieniec naokoło księżyca	— couronne autour de la lune
zamieć niska	— chasse neige au sol
zamieć wysoka	— chasse neige élevée
zawieja	— tempête de neige
pokrywa śnieżna	— couche de neige
zmętnienie	— brume sèche
słońce w czasie obserwacji	— insolation
gloria	— glorie
iryzacja	— irisation
ognie św Elma	— feux de St. Elme
mgła w ławicach	— brouillard en bancs
morze mgieł	— mer de brouillard
przejrzyste powietrze	— air pur
dni pogodne	— jours sereins
dni pochmurne	— jours couverts

1957

ALFABETYCZNY SPIS STACJI METEOROLOGICZNYCH
LISTE ALPHABÉTIQUE DES STATIONS MÉTÉOROLOGIQUES

Nr	Stacja — Station	Miesiące — Mois	Strona — Page			φ N	λ E Gr.	H_s	H_b	Dorzecze — Bassin
			Tabl. I	Tabl. II	Tabl. III					
1	Aleksandrowice	I—XII	—	434	480	49°48′	19°00′	398	403.4	Wisła
2	Aleksandrówka	I—XII	—	448	480	49°38′	20°42′	280	—	Dunajec
3	Antałówka[1])	I—XII	—	472	480	49°18′	19°59′	918	—	Dunajec
4	Antopol	I—XII	—	370	480	51°17′	22°15′	203	—	Wisła
5	Babia Góra[1])	I—XII	—	452	480	49°35′	19°31′	1180	—	Skawa
6	Baligród	I—XII	—	470	480	49°20′	22°17′	450	—	San
7	Bartoszyce	I—XII	—	282	480	54°15′	20°48′	60	—	Łyna
8	Barwinek	I—XII	—	466	480	49°26′	21°41′	420	—	Wisłoka
9	Biała Podlaska	I—XII	—	350	480	52°01′	23°08′	146	146.7	Bug
10	Białowieża	I—XII	—	322	480	52°42′	23°51′	163	163.7	Narew
11	Białystok	I—XII	100	316	480	53°07′	23°11′	139	140.8	Narew
12	Biecz	I—XII	—	440	480	49°44′	21°15′	260	—	Wisłoka
13	Bielsk Podlaski	I—XII	—	322	480	52°47′	23°11′	145	—	Narew
14	Bieruń Stary	I—XII	—	422	480	50°05′	19°05′	236	239.0	Wisła
15	Bircza	I—XII	—	444	—	49°41′	22°29′	300	—	San
16	Biskupiec	I—XII	—	296	480	53°52′	20°57′	160	—	Łyna
17	Błonie—Topola	I—XII	—	348	480	52°05′	19°11′	109	—	Ner
18	Bobrowniki Śląskie	I—XII	—	400	—	50°26′	18°52′	300	—	Kłodnica
19	Bochnia—Chodenice	I—XII	—	430	480	49°59′	20°24′	200	—	Raba
20	Bodzentyn	I—XII	—	382	480	50°57′	20°57′	288	—	Kamienna
21	Borowo	I—XII	—	344	480	52°07′	16°47′	80	—	Obra
22	Borusowa	I—XII	—	412	480	50°17′	20°47′	170	—	Wisła
23	Brwinów	I—XII	—	344	480	52°08′	20°42′	96	111.4	Bzura
24	Brzegi Dolne	I—XII	—	462	480	49°27′	22°38′	420	—	Strwiąż
25	Brzezna	I—XII	—	452	480	49°36′	20°37′	320	—	Dunajec
26	Bukowina Tatrzańska	I—XII	—	468	480	49°21′	20°07′	880	—	Dunajec
27	Busko—Zdrój	I—XII	—	398	480	50°27′	20°43′	225	—	Nida
28	Bydgoszcz	I—XII	88	314	480	53°07′	17°58′	70	70.5	Brda
29	Bydgoszcz, IMiUZ	I—XII	—	314	480	53°08′	18°01′	47	—	Brda
30	Bystrzyca Kłodzka	V—XII	—	408	480	50°18′	16°39′	370	—	Nysa Kłodzka
31	Bytom, park	I—XII	—	404	480	50°21′	18°55′	300	—	Przemsza
32	Chełm k. Krakowa	I—XII	—	426	480	50°04′	19°51′	225	—	Rudawa
33	Chełm Lubelski	I—XII	—	376	480	51°08′	23°30′	209	209.6	Bug
34	Chmielnik	I—XII	—	394	480	50°37′	20°46′	255	—	Wisła
35	Chojnice	I—XII	—	300	480	53°42′	17°33′	173	177.1	Brda
36	Chorzelów	I—XII	—	406	480	50°21′	21°27′	170	—	Wisła
37	Chorzów, park	VII—XII	—	412	—	50°17′	19°00′	316	—	Przemsza
38	Chrząstowo	I—XII	—	312	480	53°10′	17°35′	105	—	Noteć
39	Chylice	I—XII	—	346	480	52°06′	20°34′	98	—	Bzura
40	Ciechocinek	I—XII	—	318	480	52°53′	18°48′	43	—	Wisła
41	Cieplice Śl.—Zdrój	I—XII	—	384	480	50°52′	15°41′	345	—	Bóbr
42	Cieszyn	I—XII	—	438	480	49°45′	18°38′	300	—	Olza
43	Cieszyn—Borek	I—XII	—	438	480	49°45′	18°39′	300	—	Olza
44	Ciężkowice	I—XII	—	433	480	49°47′	20°58′	280	—	Dunajec
45	Ciołkowo	V—XII	—	356	480	51°45′	16°59′	110	—	Baryczka
46	Czarna Dąbrówka	I—XII	—	278	480	54°21′	17°34′	120	—	Łupawa
47	Czarny Dunajec	I—XII	—	462	480	49°27′	19°51′	680	—	Dunajec
48	Czernichów	I—XII	—	428	480	50°00′	19°41′	218	—	Wisła
49	Częstochowa	I—XII	—	388	480	50°49′	19°06′	261	262.2	Warta
50	Czorsztyn, leśnictwo	I—XII	—	462	480	49°26′	20°19′	496	—	Dunajec
51	Czorsztyn—Nadzamcze[1])	I—XII	—	464	480	49°26′	20°20′	650	—	Dunajec
52	Darłowo	I—XII	—	274	480	54°27′	16°23′	3	—	Wieprza
53	Dąbrowa Górnicza	I—XII	—	406	480	50°19′	19°11′	290	—	Przemsza

[1]) Podane w roczniku wysokości opadów otrzymano za pomocą deszczomierza o powierzchni otworu 500 cm².

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54	Dąbrowa Tarnowska	I—XII	—	418	480	50°10′	20°59′	210	—	Wisła
55	Dęba—Rozalin	IV—IX	—	398	480	50°27′	21°45′	166	—	Wisła
56	Dębica	I—XII	—	426	480	50°03′	21°24′	205	—	Wisłoka
57	Dobrogostów	I—XII	—	388	480	50°46′	17°01′	170	—	Oława
58	Dobryszyce	I—XII	—	374	480	51°09′	19°24′	210	—	Warta
59	Dolina Chochołowska[1])	I—XII	—	474	480	49°15′	19°49′	1028	—	Dunajec
60	Dolina Pięciu Stawów	I—XII	—	476	480	49°13′	20°03′	1668	—	Dunajec
61	Duszniki—Zdrój	I—XII	—	400	480	50°24′	16°24′	540	—	Nysa Kłodzka
62	Dynów	I—XII	—	436	480	49°48′	22°14′	270	—	San
63	Dziwnów	I—XII	—	290	480	54°01′	14°44′	7	4.0	Przymorze
64	Elbląg	I—XII	—	284	480	54°10′	19°25′	38	42.8	Elblążka
65	Felin	I—XII	—	372	480	51°14′	22°38′	209	—	Wieprz
66	Frombork	I—XII	—	278	480	54°22′	19°41′	2	—	Zalew Wiślany
67	Garlica Murowana	I—XII	—	418	480	50°09′	19°56′	270	—	Prądnik
68	Gdańsk—Nowy Port	I—XII	—	276	480	54°25′	18°40′	8	—	Wisła
69	Gdańsk—Siedlice	I—XII	—	276	480	54°21′	18°36′	72	—	Wisła
70	Gdańsk—Wrzeszcz	I—XII	28	276	480	54°23′	18°36′	13	12.4	Wisła
71	Gdynia	I—XII	—	272	480	54°31′	18°33′	2	—	Przymorze
72	Gliwice, park	I—XII	—	410	480	50°18′	18°40′	220	—	Kłodnica
73	Głębokie	I—XII	—	324	480	52°39′	18°26′	85	—	Noteć
74	Głodówka	III—VIII, XI, XII	—	472	480	49°18′	20°07′	1149	—	Dunajec
75	Głogów	I—XII	—	358	480	51°40′	16°04′	77	—	Odra
76	Głowno	I—XII	—	350	—	51°58′	19°42′	133	—	Bzura
77	Głubczyce	I—XII	—	416	480	50°12′	17°49′	290	—	Odra
78	Głuchołazy—Zdrój	I—XII	—	408	480	50°18′	17°23′	344	—	Nysa Kłodzka
79	Gniezno	I—XII	—	328	480	52°33′	17°36′	110	—	Wełna
80	Goczałkowice	II—XII	—	432	—	49°57′	18°55′	260	—	Wisła
81	Gołdap	I—XII	—	282	480	54°19′	22°19′	150	—	Węgorapa
82	Gorzów Wlkp.	I—XII	—	322	480	52°44′	15°15′	65	—	Warta
83	Goszyce	I—XII	—	416	480	50°11′	20°08′	260	—	Wisła
84	Grądy—Woniecko	I—XII	—	314	480	53°09′	22°24′	110	—	Narew
85	Grodkowice	I—XII	—	430	480	49°59′	20°16′	280	—	Rabka
86	Grodków	I—XII	—	392	480	50°41′	17°23′	176	—	Nysa Kłodzka
87	Grudziądz	I—XII	—	304	480	53°30′	18°46′	40	—	Wisła
88	Gryfice	I—XII	—	294	480	53°55′	15°13′	40	—	Rega
89	Gubałówka[1])	I—XII	—	470	480	49°18′	19°56′	1000	—	Dunajec
90	Hala Gąsienicowa[1])	I—XII	—	474	480	49°15′	20°00′	1520	1522	Dunajec
91	Hala Ornak[1])	I—XII	—	476	480	49°14′	19°51′	1110	—	Dunajec
92	Hel	I—XII	—	272	480	54°36′	18°49′	1	2.6	Przymorze
93	Hopowo	I—XII	—	282	480	54°16′	18°14′	220	—	Wisła
94	Horyniec	I—XII	—	416	480	50°11′	23°21′	240	—	San
95	Igołomia	I—XII	—	420	480	50°06′	20°16′	202	—	Wisła
96	Iłowa	I—XII	—	364	480	51°30′	15°12′	125	—	Bóbr
97	Inowrocław	I—XII	—	320	480	52°48′	18°14′	90	—	Noteć
98	Istebna—Kubalonka[1])	I—XII	—	450	—	49°36′	18°54′	800	—	Olza
99	Istebna—Stecówka[1])	I—XII	—	450	480	49°35′	18°57′	750	—	Wisła
100	Istebna—Zaolzie[1])	I—XII	—	450	480	49°34′	18°56′	580	—	Olza
101	Iwonicz	I—XII	—	454	480	49°34′	21°48′	410	403.4	Wisłok
102	Izbica Kujawska	I—XII	—	332	480	52°25′	18°46′	120	—	Noteć
103	Jabłonka[1])	I—XII	—	460	480	49°28′	19°42′	620	—	Czarna Orawa
104	Jarosław	I—XII	—	428	480	50°01′	22°42′	204	—	San
105	Jasło	I—XII	—	442	—	49°44′	21°28′	240	—	Wisłoka
106	Jastrzębie—Zdrój	I—XII	—	430	—	49°57′	18°34′	227	—	Olza
107	Jaworzyna Krynicka[1])	I—XII	—	466	480	49°25′	20°54′	995	—	Poprad
108	Jelenia Góra	I—XII	172	382	480	50°54′	15°48′	342	343.0	Bóbr
109	Jeziory	I—XII	—	338	480	52°16′	16°48′	84	—	Obra
110	Jordanów	I—XII	—	446	480	49°39′	19°50′	500	—	Skawa
111	Kalisz	I—XII	—	356	480	51°44′	18°05′	140	143.1	Prosna
112	Kamienica	I—XII	—	452	480	49°35′	20°21′	460	—	Dunajec
113	Kamienica Królewska	I, III—XII	—	276	480	54°23′	17°54′	160	—	Łupawa
144	Kamień Krajeński	I—XII	—	304	480	53°32′	17°31′	124	—	Brda
115	Karpacz[1])	I—XII	—	388	480	50°46′	15°46′	700	707.9	Bóbr

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116	Kartuzy	I—XII	—	280	480	54°20′	18°12′	220	—	Wisła
117	Kasprowy Wierch[1])	I—XII	256	476	480	49°14′	19°59′	1991	1988.8	Dunajec
118	Katowice	I—XII	—	414	480	50°14′	19°02′	285	285.4	Przemsza
119	Kętrzyn	I—XII	—	288	480	54°06′	21°21′	110	107.4	Łyna
120	Kielce	I—XII	—	386	480	50°51′	20°37′	268	270.0	Nida
121	Kisielnica	I—XI	—	310	480	53°15′	22°07′	140	—	Narew
122	Klimczok	I—XII	—	440	480	49°44′	19°00′	1010	—	Wisła
123	Kluczbork	I—XII	—	378	480	50°59′	18°13′	180	—	Stobrawa
124	Kluczewo	I—XII	—	310	480	53°18′	15°01′	30	—	Ina
125	Kłodzko	I—XII	—	400	480	50°26′	16°39′	318	320.1	Nysa Kłodzka
126	Kobylec	I—XII	—	320	480	52°51′	17°12′	90	—	Wełna
127	Kochcice	I—XII	—	390	480	50°43′	18°41′	280	—	Warta
128	Kolbuszowa	I—XII	—	414	480	50°14′	21°47′	208	—	Wisła
129	Kolno	I—XII	—	306	480	53°25′	21°56′	125	—	Pisa
130	Koło	I—XII	—	340	480	52°12′	18°38′	95	101.7	Warta
131	Kołobrzeg	I—XII	—	284	480	54°11′	15°35′	3	5.4	Parsęta
132	Komańcza	I—XII	—	470	480	49°20′	22°04′	470	—	San
133	Koniaków[1])	I—XII	—	454	480	49°33′	18°57′	740	—	Olza
134	Kończewice	I—XII	—	312	480	53°11′	18°33′	94	—	Wisła
135	Koszalin	I—XII	—	284	480	54°12′	16°10′	30	37.7	Przymorze
136	Kościerzyna	I—XII	—	286	481	54°06′	17°58′	180	—	Wierzyca
137	Kowale Oleckie	I, III—XII	—	286	481	54°10′	22°25′	210	—	Węgorapa
138	Kórnik	I—XII	—	338	481	52°15′	17°06′	77	—	Warta
139	Kraków—Czyżyny	IX—XII	—	424	481	50°05′	20°01′	213	213.4	Wisła
140	Kraków, Inst. Geogr. UJ	I—XII	—	424	481	50°03′	19°57′	202	—	Rudawa
141	Kraków, Obserw. Astr. UJ	I—XII	220	424	481	50°04′	19°57′	221	219.8	Wisła
142	Kraków—Rakowice	I—VIII	—	422	481	50°05′	19°59′	210	216.0	Prądnik
143	Krasnystaw	I—XII	—	380	481	50°59′	23°10′	182	—	Wieprz
144	Krosno	I—XII	—	442	481	49°42′	21°45′	270	—	Wisłok
145	Krynica	I—XII	—	466	481	49°26′	20°58′	604	609.6	Poprad
146	Krynica—Góra Parkowa[1])	I—XII	—	466	481	49°25′	20°58′	740	—	Poprad
147	Krynica Morska	I—XII	—	278	481	54°23′	19°27′	4	—	Zalew Wiślany
148	Krzesławice	I—VII, IX	—	424	481	50°05′	20°03′	200	—	Wisła
149	Kudowa—Zdrój	I—XII	—	398	481	50°27′	16°16′	385	383.3	Łaba
150	Kuźnice[1])	I—XII	—	472	481	49°16′	19°59′	1023	—	Dunajec
151	Kwidzyń	I—XII	—	298	481	53°44′	18°55′	15	—	Wisła
152	Laskowice Oławskie	I—XII	—	378	481	51°03′	17°21′	135	—	Widawa
153	Lądek—Zdrój[1])	I—XII	—	404	481	50°21′	16°53′	495	—	Nysa Kłodzka
154	Legionowo	I—XII	—	332	481	52°24′	20°58′	93	103.7	Wisła
155	Legnica	I—XII	—	372	481	51°13′	16°10′	121	126.3	Kaczawa
156	Lesko	I—XII	—	462	481	49°28′	22°20′	386	375.2	San
157	Leskowiec[1])	I—XII	—	436	481	49°48′	19°27′	870	—	Skawa
158	Leszkowice	I—XII	—	360	481	51°37′	16°19′	81	—	Odra
159	Leszno—Antoniny	I—XII	—	352	481	51°51′	16°35′	93	—	Barycz
160	Leszno—Strzyżewice	IX—XII	—	352	481	51°50′	16°32′	91	—	Barycz
161	Leżajsk	I—XII	—	414	481	50°15′	22°25′	190	—	San
162	Lębork	I—XII	—	272	481	54°33′	17°45′	18	21.8	Łeba
163	Lidzbark	I—XII	—	310	481	53°16′	19°49′	150	—	Drwęca
164	Lidzbark Warmiński	I—XII	—	286	481	54°08′	20°36′	90	—	Łyna
165	Limanowa	I—XII	—	442	481	49°42′	20°25′	440	—	Dunajec
166	Lipiny	I—XII	—	406	—	50°19′	18°54′	250	—	Przemsza
167	Lipowa	I—XII	—	386	481	50°50′	21°27′	245	—	Wisła
168	Lubaczów	I—XII	—	420	—	50°09′	23°08′	214	—	San
169	Lublin	I—XII	—	372	481	51°14′	22°34′	171	176.7	Wieprz
170	Luboń Wielki[1])	I—XII	—	446	481	49°39′	19°59′	1024	—	Raba
171	Lućmierz	I—XII	—	352	481	51°54′	19°23′	160	—	Bzura
172	Łagiewniki	I—XII	—	324	—	52°40′	18°19′	80	—	Noteć
173	Łapanów	I—XII	—	432	481	49°52′	20°18′	240	—	Raba
174	Ławica, IUNiG	I—XII	—	396	481	50°28′	16°40′	286	—	Nysa Kłodzka
175	Łącko	I—XII	—	456	481	49°33′	20°26′	369	—	Dunajec
176	Łeba	I—XII	—	270	481	54°46′	17°34′	2	—	Łeba
177	Łosice	I—XII	—	342	481	52°12′	22°43′	153	—	Bug
178	Łowicz—Blich	I—XII	—	346	481	52°06′	19°56′	95	—	Bzura
179	Łódź—Lublinek	I—XII	148	358	481	51°44′	19°24′	184	186.8	Ner
180	Łódź—Ruda Pabianicka	I—XII	—	358	481	51°42′	19°27′	181	—	Ner
181	Łysa Polana[1])	I—XII	—	474	481	49°16′	20°07′	988	—	Dunajec

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182	Maków Podhalański	I—XII	—	440	481	49°44′	19°40′	350	—	Skawa
183	Malbork	I—XII	—	290	481	54°02′	19°02′	20	—	Wisła
184	Maniowy[1])	I—XII	—	460	481	49°28′	20°15′	520	—	Dunajec
185	Miastko	I—XII	—	292	481	54°00′	16°58′	145	—	Wieprza
186	Michorzewo	I—XII	—	334	481	52°22′	16°21′	85	—	Obra
187	Miechów	I—XII	—	404	481	50°22′	20°02′	290	—	Wisła
188	Mielec, WSK	I—XII	—	410	481	50°18′	21°27′	168	170.1	Wisłoka
189	Międzybrodzie	I—XII	—	436	481	49°47′	19°12′	320	—	Soła
190	Międzychód	I—XII	—	326	481	52°36′	15°53′	40	—	Warta
191	Międzyzdroje	I—XII	—	294	481	53°56′	14°27′	10	—	Przymorze
192	Mikołajki I	I—XII	—	296	481	53°47′	21°35′	127	132.1	Pisa
193	Mikołajki II	VIII—XII	—	298	—	53°47′	21°35′	127	—	Pisa
194	Minikowo	I—XII	—	312	481	53°10′	17°45′	92	—	Noteć
195	Mława	I—XII	—	314	481	53°07′	20°22′	142	146.0	Wkra
196	Młochów	I—XII	—	348	481	52°03′	20°47′	141	—	Bzura
197	Modzurów	I—XII	—	418	481	50°10′	18°08′	271	—	Odra
198	Morskie Oko[1])	I—XII	—	476	481	49°12′	20°04′	1400	—	Dunajec
199	Motycz	I—XII	—	370	481	51°16′	22°25′	213	—	Wieprz
200	Mszana Dolna I	I—XII	—	444	—	49°41′	20°04′	380	—	Raba
201	Mszana Dolna II	IX—XII	—	444	—	49°40′	20°05′	410	—	Raba
202	Murcki	I—XII	—	416	481	50°12′	19°03′	321	—	Wisła
203	Muszyna	I—XII	—	468	481	49°21′	20°53′	445	447.5	Poprad
204	Myszyniec—Zawodzie	I—XII	—	308	481	53°23′	21°24′	122	—	Narew
205	Myślenice	I—XII	—	434	481	49°49′	19°56′	295	—	Raba
206	Myślenickie Turnie[1])	I—XII	—	474	481	49°15′	19°59′	1360	—	Dunajec
207	Namysłów	I—XII	—	376	481	51°05′	17°43′	151	—	Widawa
208	Nidzica	I—XII	—	308	481	53°22′	20°25′	170	—	Wkra
209	Niepokalanów	I—XII	—	342	481	52°12′	20°25′	91	—	Bzura
210	Nikutowo	I—XII	—	296	481	53°50′	21°18′	140	—	Łyna
211	Nisko	I—XII	—	396	481	50°31′	22°10′	164	—	San
212	Nowa Wieś	I—XII	—	366	481	51°27′	22°45′	179	—	Wieprz
213	Nowe Miasto n.P.	I—XII	—	362	—	51°37′	20°35′	162	—	Pilica
214	Nowy Dwór Gdański	I—XII	—	282	481	54°13′	19°08′	0	—	Wisła
215	Nowy Dwór Mazowiecki	I—XII	—	332	481	52°26′	20°43′	70	—	Wisła
216	Nowy Sącz	I—XII	—	448	481	49°37′	20°42′	285	300.6	Dunajec
217	Nowy Targ	I—XII	—	460	481	49°29′	20°02′	600	—	Dunajec
218	Nur	I—XII	—	324	481	52°40′	22°19′	108	—	Bug
219	Oborniki Śląskie	I—XII	—	370	481	51°18′	16°55′	169	174.8	Odra
220	Ochaby	I—XII	—	434	481	49°51′	18°46′	270	—	Wisła
221	Olesno	I—XII	—	384	481	50°53′	18°25′	238	—	Stobrawa
222	Olsztyn—Dajtki	I—XII	52	298	481	53°46′	20°25′	133	135.6	Łyna
223	Oława	I—XII	—	380	481	50°57′	17°18′	137	—	Odra
224	Opole	I—XII	—	394	481	50°40′	17°58′	176	180.7	Odra
225	Opolnica	I—XII	—	396	481	50°31′	16°44′	282	—	Nysa Kłodzka
226	Orzysz	I—XII	—	296	481	53°48′	21°57′	120	—	Pisa
227	Osiny	I—XII	—	364	481	51°28′	22°48′	153	—	Wisła
228	Osowiec	I—XII	—	304	481	53°29′	22°39′	110	—	Biebrza
229	Ostojów	I—XII	—	278	481	54°23′	22°55′	240	—	Niemen
230	Ostrołęka	I—XII	—	316	481	53°05′	21°34′	97	98.2	Narew
231	Ostrowy	I—XII	—	336	481	52°18′	19°12′	120	—	Bzura
232	Ostróda	I—XII	—	302	481	53°42′	19°58′	106	—	Drwęca
233	Ostrów Wlkp.	I—XII	—	360	—	51°39′	17°49′	126	—	Prosna
234	Ostrzeszów	I—XII	—	366	481	51°26′	17°56′	198	—	Prosna
235	Otmuchów	I—XII	—	396	481	50°28′	17°10′	211	—	Nysa Kłodzka
236	Paproć	VI—XII	—	334	481	52°19′	16°09′	70	—	Obra
237	Pawłowice	I—XII	—	354	481	51°50′	16°45′	101	—	Barycz
238	Pętkowo	I—XII	—	340	481	52°12′	17°15′	86	—	Warta
239	Pieńczykówek	I—XII	—	302	481	53°39′	22°36′	117	—	Biebrza
240	Pilsko	I—IX	—	458	481	49°32′	19°19′	1270	—	Soła
241	Piotrków Trybunalski	I—XII	—	368	481	51°24′	19°42′	200	—	Pilica
242	Piwniczna	I—XII	—	464	481	49°26′	20°42′	380	—	Poprad
243	Plewiska	I—XII	—	334	481	52°22′	16°48′	80	—	Warta
244	Płock—Radziwie	I—XII	—	328	481	52°32′	19°40′	62	63.1	Wisła
245	Płocko	I—XII	—	286	481	54°09′	16°50′	125	—	Wieprza

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246	Polanica—Zdrój	I—XII	—	402	481	50°24′	16°30′	400	—	Nysa Kłodzka
247	Poraj	I—XII	—	270	481	54°39′	17°36′	5	—	Łeba
248	Porąbka	I—XII	—	434	481	49°49′	19°13′	315	—	Soła
249	Poronin[1])	I—XII	—	470	481	49°20′	20°02′	800	—	Dunajec
250	Poświętne	I—XII	—	326	481	52°38′	20°23′	100	—	Wkra
251	Poznań—Ławica	I—XII	112	330	481	52°25′	16°50′	86	92.1	Warta
252	Poznań—Sołacz	I—XII	—	330	481	52°26′	16°54′	74	76.8	Warta
253	Pożóg	I—XII	—	368	481	51°23′	22°04′	180	—	Wisła
254	Prabuty	I—XII	—	300	481	53°44′	19°13′	104	—	Wisła
255	Prudnik	I—XII	—	406	—	50°19′	17°34′	265	—	Odra
256	Przasnysz	I—XII	—	318	481	53°01′	20°53′	120	—	Narew
257	Przebędowo	I—XII	—	326	481	52°35′	17°01′	82	—	Warta
258	Przedbórz	I—XII	—	378	481	51°05′	19°52′	235	—	Pilica
259	Przelewice	I—XII	—	316	481	53°06′	15°05′	60	—	Odra
260	Przemyśl	I—XII	232	436	481	49°48′	22°46′	238	238.9	San
261	Przewodziszowice	I—XII	—	394	—	50°39′	19°23′	380	—	Warta
262	Przybroda	I—XII	—	328	481	52°31′	16°40′	88	—	Warta
263	Pszczela Wola	I—VI	—	376	481	51°07′	22°31′	198	—	Wieprz
264	Pszczyna	I—XII	—	428	—	50°00′	18°55′	270	—	Wisła
265	Ptaszkowa[1])	I—XII	—	452	481	49°36′	20°53′	522	—	Dunajec
266	Puck	I—XII	—	270	481	54°43′	18°25′	1	—	Przymorze
267	Puczniew	I—XII	—	356	481	51°47′	19°05′	135	—	Ner
268	Puławy, IUNiG	I—XII	—	368	481	51°25′	21°58′	142	—	Wisła
269	Puławy—Kępa	I—XII	—	368	481	51°25′	21°57′	119	—	Wisła
270	Pułtusk	I—XII	—	322	481	52°43′	21°06′	80	—	Narew
271	Raba Wyżna	I—XII	—	454	481	49°34′	19°53′	600	—	Raba
272	Rabka	I—XII	—	450	481	49°36′	19°58′	510	552.4	Raba
273	Racibórz	I—XII	208	422	481	50°05′	18°13′	189	196.1	Odra
274	Radom—Wacyn	I—XII	—	366	481	51°25′	21°07′	180	181.7	Wisła
275	Radostowo	I—XII	—	292	481	53°59′	18°45′	40	—	Wisła
276	Radzików	I—XII	—	340	481	52°13′	20°39′	90	—	Bzura
277	Radzyń Podlaski	I—XII	—	354	482	51°48′	22°39′	151	—	Wieprz
278	Ramlewo Dolne	I—IX	—	292	482	53°59′	15°43′	45	—	Parsęta
279	Rdzawka na Obidowej[1])	I—XII	—	456	482	49°33′	19°58′	800	—	Raba
280	Reguły	I—XII	—	342	482	52°10′	20°51′	98	—	Bzura
281	Resko	I—XII	—	298	482	53°46′	15°25′	50	56.2	Rega
282	Rębiska	I—XII	—	274	482	54°27′	18°20′	150	—	Przymorze
283	Rokitnica	I—XII	—	402	482	50°22′	18°48′	300	—	Kłodnica
284	Rosnowo	I—XII	—	290	482	54°04′	16°18′	62	—	Parsęta
285	Rozewie	I—XII	—	270	482	54°50′	18°20′	54	—	Przymorze
286	Rożnów	I—XII	—	438	482	49°46′	20°41′	300	—	Dunajec
287	Rudka	I—XII	—	344	482	52°09′	21°50′	169	—	Liwiec
288	Rybnik	I—XII	—	420	482	50°06′	18°33′	243	—	Odra
289	Rymanów—Zdrój	I—XII	—	458	482	49°33′	21°51′	360	—	Wisłok
290	Rzeszów—Jasionka	I—XII	—	422	482	50°06′	22°03′	198	197.5	Wisłok
291	Sandomierz	I—XII	196	392	482	50°41′	21°45′	202	200.3	Wisła
292	Sanok	I—XII	—	454	482	49°34′	22°12′	314	—	San
293	Sejny	I—XII	—	288	482	54°06′	23°21′	130	—	Niemen
294	Sękocin	II—XII	—	346	482	52°07′	20°53′	110	—	Wisła
295	Siedlce	I—XII	—	342	482	52°11′	22°16′	147	148.8	Liwiec
296	Siejnik	I—XII	—	292	482	54°01′	22°29′	170	—	Biebrza
297	Sielec Pińczowski	I—XII	—	408	482	50°19′	20°25′	202	—	Wisła
298	Sielec Stary	I—XII	—	360	482	51°39′	17°09′	110	—	Barycz
299	Siemianice	I—XII	—	374	482	51°11′	18°09′	182	—	Prosna
300	Siemiatycze	I—XII	—	332	482	52°26′	22°51′	145	—	Bug
301	Sieniawa	I—XII	—	458	482	49°32′	19°55′	578	—	Raba
302	Sieradz	I—XII	—	362	482	51°36′	18°44′	137	—	Warta
303	Sinołęka	I—XII	—	340	482	52°13′	21°54′	153	—	Liwiec
304	Skawina	I—XII	—	430	482	49°59′	19°48′	210	—	Wisła
305	Skierniewice	I—XII	—	350	482	51°58′	20°09′	129	129.0	Bzura
306	Skroniów	I—XII	—	394	482	50°38′	20°16′	256	—	Nida
307	Słubice	I—XII	—	334	482	52°21′	14°36′	20	—	Odra
308	Słupia Nowa	I—XII	—	384	482	50°52′	21°05′	307	—	Kamienna
309	Słupsk	I—XII	—	274	482	54°28′	17°02′	23	—	Słupia
310	Smolice	I—XII	—	358	482	51°42′	17°11′	107	—	Barycz
311	Sobieszyn	I—XII	—	362	482	51°36′	22°10′	159	—	Wieprz

Nr	Stacja — Station	Miesiące — Mois	Strona — Page			φ N	λ E Gr.	H_s	H_b	Dorzecze — Bassin
			Tabl. I	Tabl. II	Tabl. III					
312	Sokołowsko[1])	I—XII	—	392	482	50°41′	16°14′	570	—	Nysa Kłodzka
313	Sokółka	I—XII	—	308	482	53°24′	23°30′	180	—	Narew
314	Sopot	I—XII	—	274	482	54°27′	18°34′	2	—	Przymorze
315	Sosnowiec	I—XII	—	412	482	50°17′	19°06′	250	—	Przemsza
316	Spalona	I—XII	—	410	482	50°17′	16°32′	810	—	Nysa Kłodzka
317	Stańcowa[1])	I—XII	—	456	482	49°33′	19°32′	850	—	Czarna Orawa
318	Stare Olesno	I—XII	—	382	—	50°54′	18°21′	230	—	Stobrawa
319	Stare Pole	I—XII	—	290	482	54°03′	19°13′	3	—	Wisła
320	Stary Sącz	I—XII	—	458	482	49°33′	20°39′	320	—	Dunajec
321	Sternalice	I—XII	—	380	—	50°58′	18°34′	239	—	Prosna
322	Strzelna	I—XII	—	354	482	51°49′	19°54′	194	—	Bzura
323	Strzyżów	I—XII	—	386	482	50°51′	24°02′	185	—	Bug
324	Suchedniów	I—XII	—	378	482	51°03′	20°50′	272	—	Kamienna
325	Sulęcin	I—XII	—	330	—	52°27′	15°07′	70	—	Odra
326	Suwałki	I—XII	40	288	482	54°06′	22°57′	165	169.5	Niemen
327	Szczawnica—Zdrój	I—XII	—	464	482	49°26′	20°29′	500	—	Dunajec
328	Szczawno—Zdrój	I—XII	—	388	482	50°48′	16°15′	415	—	Bystrzyca
329	Szczecin—Dąbie	I—XII	64	306	482	53°24′	14°37′	1	6.9	Odra
330	Szczecin—Łabędzia	I—XII	—	306	482	53°27′	14°33′	69	—	Odra
331	Szczecinek	I—XII	—	300	482	53°43′	16°41′	137	142.6	Gwda
332	Szczerców	I—XII	—	370	—	51°20′	19°07′	160	—	Warta
333	Szczuczyn	I—XII	—	304	482	53°34′	22°17′	130	—	Biebrza
334	Szczytno	I—XII	—	302	482	53°34′	21°02′	144	—	Narew
335	Szepietowo	I—XII	—	320	482	52°51′	22°32′	150	—	Bug
336	Szklarska Poręba[1])	I—XII	—	384	482	50°51′	15°32′	640	—	Bóbr
337	Szprotawa	I—XII	—	362	482	51°34′	15°32′	122	—	Bóbr
338	Ślęża	I—XII	—	382	482	50°53′	16°43′	718	—	Bystrzyca
339	Śliwice	I—XII	—	300	482	53°43′	18°11′	115	—	Czarna Woda
340	Śnieżka[1])	I—XII	184	390	482	50°44′	15°44′	1603	1610	Bóbr
341	Śnieżnik Kłodzki	I—XII	—	414	482	50°12′	16°49′	1218	—	Nysa Kłodzka
342	Śrem	I—XII	—	348	482	52°05′	17°01′	78	—	Warta
343	Świbno	I—XII	—	280	482	54°20′	18°56′	8	—	Wisła
344	Świbno—Ujście Wisły	III—XII	—	280	482	54°21′	18°56′	5	—	Wisła
345	Świder	I—XII	—	346	482	52°07′	21°15′	100	—	Świder
346	Świdnica	I—XII	—	386	482	50°51′	16°30′	230	—	Bystrzyca
347	Świebodzin	I—XII	—	338	482	52°15′	15°32′	78	84.1	Odra
348	Świecie	I—XII	—	308	482	53°24′	18°27′	25	—	Czarna Woda
349	Świerklaniec	I—XII	—	400	482	50°26′	18°57′	284	—	Przemsza
350	Świętochłowice	I—XI	—	410	—	50°17′	18°56′	300	—	Przemsza
351	Świniarsko	I—XII	—	448	482	49°37′	20°39′	295	—	Dunajec
352	Świnoujście	I—XII	—	294	482	53°55′	14°16′	2	4.6	Przymorze
353	Tarnogród	I—XII	—	404	—	50°22′	22°45′	217	—	San
354	Tarnów	I—XII	—	426	482	50°02′	20°59′	209	209.1	Dunajec
355	Tczew	I—XII	—	288	482	54°05′	18°48′	10	—	Wisła
356	Terespol n.B.	I—XII	—	348	482	52°05′	23°37′	143	—	Bug
357	Tęgoborze	I—XII	—	440	482	49°44′	20°38′	300	—	Dunajec
358	Tolkmicko	I—XII	—	280	482	54°19′	19°32′	1	—	Zalew Wiślany
359	Tomaszów Lubelski	I—XII	—	398	482	50°27′	23°25′	273	—	Bug
360	Toruń—Podgórz	I—XII	—	318	482	53°03′	18°35′	53	—	Wisła
361	Toruń—Wrzosy	I—XII	—	316	482	53°03′	18°35′	69	70.1	Wisła
362	Trzcińsko—Zdrój	I—XII	—	318	—	52°58′	14°36′	57	—	Odra
363	Trzebież	I—XII	—	302	482	53°40′	14°31′	1	6.6	Zalew Szczec.
364	Trzebinia	I—XII	—	418	482	50°10′	19°28′	320	—	Wisła
365	Trzemeszno	I—XII	—	328	482	52°34′	17°49′	105	—	Wełna
366	Turbacz[1])	I—XII	—	456	482	49°33′	20°07′	1308	—	Raba
367	Tychy	I—XII	—	420	482	50°08′	18°59′	280	—	Wisła
368	Tyniec	I—XII	—	426	482	50°01′	19°48′	210	—	Wisła
369	Urbanowice	I—XII	—	408	—	50°18′	18°02′	200	—	Odra
370	Ustka	I—XII	16	272	482	54°35′	16°52′	6	8.1	Słupia
371	Wadowice	I—XII	—	432	482	49°53′	19°31′	260	—	Skawa
372	Wałcz	I—XII	76	310	482	53°17′	16°28′	111	113.8	Gwda
373	Warka n.P.	I—XII	—	354	482	51°48′	21°11′	120	—	Pilica
374	Warszawa—Bielany	I—XII	124	336	482	52°17′	20°58′	101	104.7	Wisła
375	Warszawa, Obserw. Astr. UW	I—XII	—	336	482	52°13′	21°02′	110	114.8	Wisła

Nr	Stacja — Station	Miesiące — Mois	Strona — Page			φ N	λ E Gr.	H_s	H_b	Dorzecze — Bassin
			Tabl. I	Tabl. II	Tabl. III					
376	Warszawa—Okęcie	I—XII	—	336	482	52°11′	20°58′	106	106.9	Wisła
377	Werbkowice	I—XII	—	390	482	50°45′	23°46′	207	—	Bug
378	Wielichowo	I—XII	—	344	482	52°07′	16°21′	65	—	Obra
379	Wieliczka	I—XII	—	428	482	50°00′	20°03′	225	—	Wisła
380	Wieliszew	I—XII	—	330	482	52°28′	20°58′	78	—	Bug
381	Wieluń	I—XII	—	372	482	51°13′	18°35′	195	198.4	Warta
382	Wieniec—Zdrój	I—XII	—	324	482	52°40′	18°59′	82	—	Wisła
383	Wierzchowo	I—XII	—	306	—	53°27′	16°06′	140	—	Drawa
384	Więcławice	I—XII	—	320	—	52°51′	18°19′	90	—	Noteć
385	Wińsko	I—XII	—	364	482	51°28′	16°37′	180	—	Barycz
386	Wirty	I—XII	—	294	482	53°54′	18°23′	121	—	Wierzyca
387	Wisła	I—XII	—	446	482	49°39′	18°52′	430	—	Wisła
388	Wisznice	I—XII	—	356	482	51°47′	23°12′	152	—	Bug
389	Witów[1])	I—XII	—	468	482	49°20′	19°50′	835	—	Dunajec
390	Włodawa	I—XII	—	364	482	51°33′	23°33′	174	175.5	Bug
391	Wojcieszów Górny	I—XII	—	380	482	50°57′	15°55′	358	362.1	Kaczawa
392	Wolbrom	I—XII	—	402	482	50°23′	19°45′	260	—	Przemsza
393	Wrocław—Mały Gądów	I—XII	160	374	482	51°08′	16°59′	116	118.6	Odra
394	Wrocław, WSR	I—XII	—	376	482	51°07′	17°05′	117	—	Odra
395	Wyrzysk	I—XII	—	312	482	53°09′	17°16′	90	—	Noteć
396	Wysokie[1])	I—XII	—	446	482	49°39′	20°34′	645	—	Dunajec
397	Wysowa[1])	I—XII	—	464	482	49°26′	21°11′	525	—	Wisłoka
398	Wyszków	I—XII	—	326	482	52°35′	21°27′	96	—	Bug
399	Zakopane[1])	I—XII	244	472	482	49°18′	19°57′	844	838.2	Dunajec
400	Zakrzów	I—XII	—	412	482	50°15′	18°10′	217	—	Odra
401	Zamość	I—XII	—	390	482	50°44′	23°15′	217	218.6	Wieprz
402	Zawoja[1])	I—XII	—	448	482	49°37′	19°31′	670	—	Skawa
403	Ząbkowice	I—XII	—	402	482	50°22′	19°18′	314	—	Przemsza
404	Zbąszyń	I—XII	—	338	482	52°15′	15°56′	57	—	Obra
405	Zbyszyce	VII—XII	—	442	—	49°43′	20°40′	315	—	Dunajec
406	Zdanów	I—XII	—	392	482	50°43′	21°33′	236	—	Wisła
407	Zgorzelec	I—XII	—	374	482	51°10′	15°00′	219	217.9	Nysa Łużycka
408	Zielona Góra I	I—XII	136	350	482	51°56′	15°30′	176	174.0	Odra
409	Zielona Góra II	VIII—XII	—	352	482	51°56′	15°30′	182	—	Odra
410	Złoczew	I—IV, VI—XII	—	366	—	51°25′	18°36′	174	—	Warta
411	Zwardoń[1])	I—XII	—	460	482	49°30′	18°59′	690	—	Soła
412	Żarnowa	I—XII	—	432	482	49°52′	21°49′	240	—	Wisłok
413	Żary	I—XII	—	360	482	51°38′	15°08′	157	—	Bóbr
414	Żegiestów—Zdrój	I—XII	—	468	482	49°22′	20°49′	440	—	Poprad
415	Żelisławki	I—XII	—	284	482	54°10′	18°39′	68	—	Wisła
416	Żywiec—Sporysz	I—XII	—	444	482	49°41′	19°13′	360	—	Soła

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1957

TABLICA I

SPOSTRZEŻENIA CODZIENNE STACJI METEOROLOGICZNYCH:

OBSERVATIONS DIURNES DE STATIONS MÉTÉOROLOGIQUES:

1. Ustka
2. Gdańsk – Wrzeszcz
3. Suwałki
4. Olsztyn – Dajtki
5. Szczecin – Dąbie
6. Wałcz
7. Bydgoszcz
8. Białystok
9. Poznań — Ławica
10. Warszawa—Bielany
11. Zielona Góra
12. Łódź — Lublinek
13. Wrocław — Mały Gądów
14. Jelenia Góra
15. Śnieżka, Obserwatorium Wysokogórskie
16. Sandomierz
17. Racibórz
18. Kraków, Obserwatorium Astronomiczne UJ
19. Przemyśl
20. Zakopane
21. Kasprowy Wierch, Obserwatorium Wysokogórskie

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ Styczeń – Janvier 1957

DNI	CIŚNIENIE P− +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	116.6	116.8	116.7	116.7	-5.4	-5.2	-7.2	-6.2	-4.7	-7.3	95	90	93	93	0.2	0.4	0.2	0.3	10	10	10	SE 2	S 1	SE 4
2	114.1	112.1	112.7	113.0	-6.9	-1.6	-1.1	-2.7	-0.9	-8.5	94	92	95	94	0.2	0.4	0.3	0.3	10	10	10	SE 2	S 1	SE 3
3	117.6	119.0	118.6	118.4	0.2	0.8	1.0	0.8	1.8	-1.9	94	94	94	94	0.4	0.4	0.4	0.4	10	10	9	SW 5	S 3	S 3
4	119.9	119.6	119.2	119.6	0.5	1.5	2.1	1.6	2.5	0.4	96	89	95	93	0.2	0.8	0.4	0.5	10	10	10	S 4	S 4	SSW 3
5	114.8	109.0	109.4	111.1	3.1	6.3	5.4	5.0	8.5	2.0	98	98	100	99	0.1	0.1	0.0	0.1	10	10 ●	10	SSW 5	SSW 7	W 10
6	102.8	103.9	104.9	103.9	9.5	6.2	4.5	6.2	10.4	4.5	96	85	84	88	0.5	1.5	1.3	1.1	10 ●	4 ⊙	7	W 12	W 12	W 14
7	113.5	119.2	123.4	118.7	4.2	4.2	3.6	3.9	4.7	3.5	85	92	93	90	1.2	0.6	0.5	0.8	0	1 ⊙	0	W 17	NW 14	W 12
8	121.5	119.5	118.5	119.8	4.4	4.8	6.1	5.4	6.3	3.4	98	98	90	98	0.2	0.1	0.1	0.1	10	10 ◔	10 ◔	W 10	W 12	W 12
9	115.3	113.1	110.0	112.8	8.0	8.2	6.9	7.5	8.5	5.7	89	81	96	89	1.2	2.1	0.4	1.2	10	10	10 ●	W 14	SW 14	SW 10
10	107.5	106.1	108.2	107.3	3.8	3.3	2.8	3.2	6.9	2.4	92	85	89	89	0.7	1.2	0.8	0.9	3	9 ●	2	SW 8	W 12	W 9
11	113.4	116.6	117.2	115.7	2.3	3.1	2.6	2.6	4.2	2.1	82	76	68	75	1.3	1.8	2.4	1.8	5	0	0	N 8	NW 6	NW 6
12	108.5	101.8	98.2	102.8	0.5	1.8	1.8	1.5	2.6	0.1	98	98	96	97	0.1	0.2	0.3	0.2	10 ✱	10 ●	10	SW 7	SW 5	SW 2
13	101.1	106.4	116.0	107.8	0.5	1.2	-2.6	-0.9	1.8	-2.6	100	96	93	96	0.0	0.3	0.3	0.2	10	10 ✱	10	C 0	E 5	E 7
14	124.0	127.7	131.7	127.8	-3.8	-3.6	-5.5	-4.6	-2.3	-5.6	69	58	75	67	1.4	2.0	1.0	1.5	7	0 ⊙	1	NE 6	E 7	E 4
15	131.6	130.0	129.0	130.2	-6.6	-4.1	-7.0	-6.2	-3.6	-7.8	75	66	82	74	0.9	1.5	0.6	1.0	4	0 ⊙	9	E 3	SE 2	SE 3
16	130.0	130.3	130.9	130.4	-5.0	0.6	1.2	-0.5	1.3	-7.3	85	83	77	82	0.6	1.1	1.5	1.1	10 ✱	6 ⊙	9	S 1	N 4	WNW 5
17	130.2	130.9	130.4	130.5	1.4	2.4	-0.3	0.8	3.4	-2.5	94	86	100	93	0.4	1.1	0.0	0.5	8	7 ⊙	10 ≡	W 3	W 2	SW 4
18	128.1	126.9	125.0	126.7	0.6	-0.7	1.8	0.9	1.8	-1.3	100	100	78	93	0.0	0.0	1.6	0.5	10	10	10	W 5	W 4	W 8
19	126.7	127.6	127.4	127.2	0.6	0.7	1.0	0.8	1.9	-0.1	96	98	100	98	0.3	0.1	0.0	0.1	10	10	10 ◔	W 3	W 6	SW 5
20	125.1	122.5	119.0	122.2	1.2	1.8	1.8	1.6	2.8	1.0	98	93	89	93	0.2	0.6	0.8	0.5	10	9	10	WSW 5	SW 8	SW 8
21	115.1	116.5	118.0	116.5	-0.4	-0.4	0.3	0.0	1.8	-0.7	88	88	100	92	0.7	0.7	0.0	0.5	10	10	10 ◔	SW 10	SW 8	SW 8
22	117.4	115.8	114.9	116.0	0.0	1.4	-2.8	-1.0	1.9	-2.8	100	76	80	85	0.0	1.7	1.0	0.9	10 ◔	0 ⊙	10	SW 7	SW 8	SW 5
23	113.8	115.2	116.7	115.2	0.0	2.6	0.8	1.0	3.6	-2.9	92	77	83	84	0.5	1.7	1.2	1.1	9	4 ⊙	0	SW 4	SW 4	SW 5
24	114.4	112.1	109.5	112.0	-3.6	0.8	-1.4	-1.4	1.9	-3.8	87	75	82	81	0.6	1.7	1.0	1.1	8	9	10	S 2	SE 5	SE 3
25	106.6	107.0	110.3	108.0	-2.6	-1.0	-1.8	-1.8	-0.3	-2.7	89	95	96	93	0.6	0.3	0.2	0.4	10	10	10	SE 2	SE 1	SW 3
26	115.4	114.9	110.2	113.5	0.4	4.0	2.5	2.4	4.3	-1.8	96	83	73	84	0.3	1.3	1.9	1.2	10	4	10	WSW 3	SW 3	S 6
27	106.8	108.4	112.2	109.1	3.4	4.6	3.4	3.7	5.6	1.6	100	84	85	90	0.0	1.4	1.2	0.9	10	7	0	SW 7	W 8	SW 10
28	114.6	121.0	126.5	120.7	1.2	2.5	2.2	2.0	3.4	0.8	98	91	98	96	0.2	0.6	0.2	0.3	10 ●	9	0	SW 5	W 5	W 5
29	126.0	124.9	123.5	124.8	0.7	2.2	3.0	2.2	3.0	-0.4	94	96	100	97	0.4	0.3	0.0	0.2	6	10 ●	10 ●	SW 5	SW 3	SW 6
30	120.7	119.0	119.1	119.6	0.8	2.2	1.2	1.4	4.1	0.4	92	87	100	93	0.5	1.0	0.0	0.5	6	10	10 ◔	SW 4	SW 2	SW 2
31	118.9	119.5	120.0	119.5	1.0	1.0	0.4	0.7	1.7	0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10 ✱	10	E 1	SSE 2	C 0
M	117.2	117.2	117.7	117.4	0.5	1.7	0.9	1.0	2.9	-1.0	93	87	90	90	0.4	0.9	0.6	0.6	8.6	7.4	7.6	5.5	5.9	6.0

Luty – Février

1	114.1	110.9	108.6	111.2	1.2	3.9	7.2	4.9	7.5	0.1	100	97	100	99	0.0	0.3	0.0	0.1	10	10	10 ●	SSE 4	S 7	SSW 7
2	114.1	119.6	123.6	119.1	6.0	5.9	2.2	4.1	11.0	2.0	73	77	95	82	2.6	2.1	0.4	1.7	0	9 ⊙	0	W 12	W 12	SW 6
3	123.3	124.3	126.8	124.8	1.5	6.4	0.9	2.4	6.7	0.9	98	79	100	92	0.1	2.0	0.0	0.7	10	0 ⊙	10 ≡	SW 3	W 4	W 3
4	122.5	119.0	118.9	120.1	0.7	3.4	5.2	3.6	5.3	-1.1	98	100	100	99	0.1	0.0	0.0	0.0	7	10 ●	10 ≡	S 3	SW 5	SW 3
5	117.4	115.6	114.3	115.8	4.6	7.7	5.4	5.8	9.8	3.4	98	84	94	92	0.2	1.6	0.6	0.8	6	10	4	SSW 3	SSW 6	SW 5
6	111.0	107.3	107.0	108.4	2.6	9.1	7.2	6.5	10.3	2.6	96	71	91	86	0.3	3.4	0.9	1.5	7	10	10	SW 4	SW 6	WSW 5
7	110.0	109.0	111.4	110.1	3.6	5.2	4.3	4.4	8.6	3.6	97	84	93	91	0.3	1.4	0.5	0.7	5	9	4	SW 7	SW 12	W 10
8	108.7	103.5	97.3	103.2	2.8	5.0	7.1	5.5	7.3	2.6	96	94	99	96	0.3	0.5	0.2	0.3	10	10	10 ●	SW 5	SSW 5	SW 5
9	94.8	94.3	97.2	95.4	7.6	7.0	5.0	6.2	8.5	5.0	93	96	94	94	0.7	0.4	0.5	0.5	10	9	10 ●	SW 7	SW 10	W 10
10	101.9	103.7	105.0	103.5	3.2	4.5	0.6	2.2	5.4	0.5	97	92	100	96	0.3	0.7	0.0	0.3	10	3 ⊙	10	W 14	W 6	W 3
11	105.2	107.4	109.8	107.5	3.0	2.3	2.5	2.6	3.7	0.0	96	98	86	93	0.3	0.1	1.0	0.5	10 ●	10 ●	9	W 4	W 5	NW 6
12	109.5	104.9	99.9	104.8	-0.8	2.9	4.2	2.6	4.7	-1.5	98	88	98	95	0.2	0.9	0.1	0.4	9	10	10 ●	W 3	SSE 3	S 6
13	96.7	92.9	85.2	91.6	2.6	5.8	5.1	4.6	6.9	2.6	100	85	92	92	0.0	1.4	0.7	0.7	10	9	10 ●	S 3	SSW 4	SE 4
14	80.2	82.0	83.4	81.9	6.0	7.8	5.4	6.2	8.2	5.0	98	86	97	94	0.2	1.5	0.3	0.7	10	9	9	SSW 4	SSW 4	SSW 2
15	83.5	84.8	83.6	84.0	2.5	6.3	4.6	4.5	7.4	2.3	98	85	87	90	0.1	1.4	1.1	0.9	10 ●	8	10	S 2	SW 6	SSW 2
16	87.2	91.1	95.1	91.1	3.4	4.6	2.4	3.2	5.7	2.4	98	74	95	89	0.1	2.2	0.4	0.9	10	9 ⊙	5	SW 3	W 4	SW 5
17	99.9	102.1	103.1	101.7	0.4	5.4	0.5	1.7	5.7	0.3	92	77	92	87	0.5	2.1	0.5	1.0	0	6 ⊙	0	SW 5	SW 5	SW 3
18	104.3	103.7	101.2	103.1	-0.4	5.1	2.2	2.3	5.8	-0.6	100	75	96	90	0.0	2.2	0.3	0.8	4	8 ⊙	10	SW 2	S 4	S 1
19	100.3	104.2	107.8	104.1	2.6	2.3	1.6	2.0	3.0	1.4	98	89	94	94	0.2	0.8	0.4	0.5	10	10	10	N 3	NW 8	W 7
20	108.9	109.0	107.4	108.4	0.5	3.8	1.6	1.9	4.9	-0.1	98	85	96	93	0.1	1.2	0.3	0.5	10	6 ⊙	10 ●	SW 4	SSW 3	SSE 1
21	104.7	105.8	110.1	106.9	1.2	5.2	2.2	2.7	5.5	0.7	100	87	95	94	0.0	1.1	0.4	0.5	10	10	10	SSE 2	SSW 2	NW 5
22	113.7	114.0	112.9	113.5	0.7	2.8	0.4	1.1	3.6	0.3	98	91	98	96	0.1	0.7	0.1	0.3	10	5	10	WSW 3	W 5	W 3
23	112.1	112.0	112.7	112.3	-0.8	0.3	-0.8	-0.5	1.3	-1.3	99	98	79	92	0.0	0.1	1.2	0.4	9	10 ✱	10	SW 3	N 4	NNW 5
24	107.9	104.8	105.6	106.1	-1.9	0.6	-1.6	-1.1	0.9	-1.9	82	71	90	81	0.9	1.9	0.5	1.1	8	8	0	N 2	NE 3	NE 3
25	108.4	108.5	109.8	108.9	-3.2	2.5	-1.2	-0.8	2.9	-3.2	97	61	89	82	0.1	2.8	0.6	1.2	1	4 ⊙	0	N 1	E 2	E 3
26	115.0	117.4	119.9	117.4	-1.6	2.0	-1.0	-0.4	2.9	-3.3	96	76	92	88	0.2	1.7	0.5	0.8	10	10	0	E 1	E 1	E 1
27	122.0	123.2	125.5	123.6	-3.6	3.1	1.1	0.4	4.9	-3.9	92	68	85	82	0.4	2.5	1.0	1.3	0	8	10	E 1	S 1	S 1
28	131.0	133.6	136.7	133.8	0.2	1.4	1.1	1.0	2.5	-0.7	92	89	83	88	0.5	0.8	1.1	0.8	9	9	0	NE 3	NE 6	NE 7
29																								
30																								
31																								
M	107.4	107.4	107.8	107.5	1.6	4.4	2.7	2.8	5.7	0.6	96	84	93	91	0.3	1.4	0.5	0.7	7.7	8.2	7.2	4.0	5.1	4.4

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	1	.	
2	6	0.0	1	.	●⁰ 18³⁵–21¹⁰ ; = 1²⁰–11³⁰, 14³⁰–24
3	5	0.0	1	.	●⁰ 6³⁵–8¹⁰ ; = 0⁰⁰–24
4	5	.	1	.	= 0⁰⁰–24
5	5	5.5	pł.	.	●¹ 7⁴⁵–9⁰⁵ ●⁰–18³⁶ ; = 0⁰⁰–18⁴⁰ ≡⁰–20²⁰ = –22⁴⁰ ≡⁰–24
6	7	0.4	.	1.2	●⁰ 2¹⁵–3⁰⁵ ●¹–6¹⁰ ●⁰–7²⁰ ; ≡⁰ 0⁰⁰–1⁴⁰ = –n
7	7	.	.	4.2	
8	4	0.3	.	.	●⁰ 12³⁵–17⁰⁵ ●²–21²⁰ ●⁰–22¹⁵ ; ≡⁰ 3⁴⁰–5³⁵ = –24
9	7	1.4	.	.	●⁰ n–3³⁰ ●⁰ 18⁴⁰–21⁴⁰ ●¹–23¹⁰ ; = 0⁰⁰–10³⁰
10	7	0.4	.	1.0	♉ 11³⁰–46, 12⁴⁵–13⁰⁵
11	8	1.4	.	5.4	
12	5	6.4	.	.	⚹ 4⁴⁵–5³⁰ ✳⁰–8²⁰ ✱⁰–12⁰⁵ ●⁰–18⁴⁰ ; = 20³⁰–24
13	5	1.4	.	.	●⁰ 7¹⁰–6³⁰ ●⁰ 9⁴⁰–10²⁰ ●⁰–12¹⁰ ✱⁰–15¹⁵ ✳⁰–19³⁰ ; = 0⁰⁰–21⁴⁵ ; ⌴⁰ 7²⁰–a
14	8	.	1	6.1	
15	7	0.2	1	6.2	
16	7	0.9	1	2.2	♉ 0¹⁰–30 ✳⁰ 3¹⁰–4⁴⁰ 6¹⁰–7¹⁵ 9¹⁰–10²⁰ △¹–10³³ △⁰–10⁴³
17	7	.	2	4.7	= 14⁴⁰–15²⁵ ≡⁰–15⁴⁰ ≡¹–16³⁰ ≡²–18³⁵ = –19³⁰ ≡⁰–24
18	5	.	1	.	≡⁰ 0⁰⁰–6²⁰ = –13⁵⁰ ≡⁰–15³⁵ = –20²⁰
19	6	0.0	1	.	●⁰ 15⁵⁰–17¹⁵ ●¹–19⁴⁵ ●⁰–21²⁵ ; ≡⁰ 16⁴⁵–17⁰⁰ = –23¹⁰ ≡⁰–24
20	7	.	pł.	.	≡⁰ 0⁰⁰–3⁵⁰ = –5³⁰
21	6	0.2	.	.	●⁰ 13⁵⁵–14¹⁰ 15¹¹–40 ●⁰ 17⁵⁰–23²⁰
22	7	0.0	.	3.0	●¹ 0⁰⁰–1¹⁵ ●⁰–3³⁰ ●¹ 6¹⁰–7⁰⁵ ●⁰–9¹⁵
23	6	.	.	1.6	
24	6	.	.	0.1	⊕ 13⁴⁰–14⁰⁰
25	5	0.8	.	.	✳⁰ 7⁵⁰–8²⁰ ✳¹–11⁴⁵ ; = 8⁰⁰–21⁴⁵ ≡–24
26	5	2.9	1	1.7	●⁰ 1⁴⁰–2⁰⁵ ●⁰–2³⁰ 22⁴⁰–24 ; ≡⁰ 0⁰⁰–2⁵⁰ = –24
27	7	0.9	.	0.6	●⁰ 0⁰⁰–1¹⁰ ●¹–2²⁰ ●⁰ 2³⁰–6³⁰ ●⁰ 7³⁰–10²⁷ ●⁰⁻¹–11⁰⁰ ; = 0⁰⁰–9⁴⁰ ≡⁰–10⁵⁵ = –11⁰⁰
28	7	0.0	.	1.2	●⁰ 6¹⁰–8¹⁰ ; = 8¹⁰–10¹⁵ ; ⌴⁰ 20⁴⁰–24
29	6	0.3	.	.	●⁰ 12⁵⁴–13⁵⁰ 14¹⁰–16⁰⁰ 20¹⁰–22¹⁵ ; = 16⁰⁰–22⁴⁰ ; ⌴² 0⁰⁰–9³⁰
30	6	1.6	.	.	●⁰ 20⁴⁰–23⁴⁰ ; = 0⁰⁰–20⁴⁵ ≡⁰–20⁵⁰ ≡¹–24
31	5	0.7	.	.	●⁰ 1¹⁵–8⁴⁰ ✳⁰–13¹⁵ ; ≡¹ 0⁰⁰–1²⁵ ≡⁰–1⁴⁰ = –8⁴⁰ ≡⁰–12¹⁰ = –13⁴⁰ ≡⁰–15⁴⁰ = –15⁵⁵
Σ	–	25.7	–	39.2	UWAGI.

Luty – Février

1	5	3.6	.	.	●¹ 14²⁵–16³⁵ ●⁰–20¹⁰ ●¹–21³⁰ ●⁰–23³⁰ ; = 6⁵⁰–15⁰⁵ ≡⁰–15⁴⁰ = –24
2	7	.	.	5.2	
3	7	.	.	2.8	= 15⁴⁰–50 ≡⁰–21⁴⁵ ≡¹–24 ; ⌴⁰ 0⁵⁰–9⁰⁰
4	6	2.2	.	.	●⁰ 10⁴⁰–11³⁰ ●¹–13¹⁰ ●⁰–14⁰⁰, 15⁴⁰–16¹⁰ ●¹–20³⁰ ; ≡¹ 0⁰⁰–3⁴⁵ ≡⁰–4³⁰ = –6³⁰, 15³⁰–16⁰² ≡⁰–24 ;
5	6	.	.	0.4	≡⁰ 0⁰⁰–5⁴⁰ = –24 [4.II: ⌴⁰ 3⁵⁰–9⁰⁰
6	7	0.0	.	2.9	●⁰ 16²⁰–17¹⁵, 19¹³–20¹⁰ ; = 0⁰⁰–24
7	7	.	.	2.5	= 0⁰⁰–6⁴⁰
8	6	5.7	.	.	●⁰ 8³⁰–10²⁰, 13²⁵–15⁰⁰–21²⁰ ; = 1⁰⁰–24
9	7	6.4	.	.	●⁰ 5¹⁰–40 9³⁵–10⁵⁰, 12³⁵–50, 16⁵⁰–17¹⁰, 20⁴⁰–21¹⁵ ●¹–24 ; = 0⁰⁰–3⁴⁰
10	7	0.2	.	3.4	●⁰ 0⁰⁰–3⁴⁰, 5⁵⁰–6¹⁵ ⌓ 19³⁰–21⁴⁰, 22⁴⁰–24 = 18³⁰–24
11	6	1.4	.	0.1	●⁰ 5³⁰–7⁰⁵ ●¹–7⁴⁰ ●⁰–8²⁰, 10⁴⁰–11³⁰, 12²⁵–14¹⁵, 15⁵⁰ 16¹³ ✱⁰–16¹⁸ ●⁰ 17³⁵⁻⁵⁰ = 0⁰⁰–14²⁰, 19⁴⁰–21¹⁰ ⌓ 0⁰⁰–4⁰
12	6	3.2	.	.	●⁰ 15⁰³⁻³⁰ ●¹–16²⁰ ●⁰–21⁵⁰ ●¹–22⁴⁰ ●⁰–24 ⌴¹ n–9²⁰ ⌓ 12³⁵–32⁰ ; = 6¹⁰–8⁴⁰ 9³⁰–24
13	7	5.0	.	1.3	●⁰ 0⁰⁰–45 8⁰⁵–10¹⁷ ●¹ 20³⁰–23³⁰ ●⁰–24 ; ⌓ 1⁴⁵–2³⁰ ⌓ ⁰ 17⁴⁵–18⁵⁰ ; = 0⁰⁰–17³⁰, 20³⁰–24
14	7	4.5	.	.	●⁰ 0⁰⁰–7²⁵ ♉ 18¹⁰–45 ; = 0⁰⁰–7³⁰ 21⁴⁰–24
15	7	1.0	.	2.4	●⁰ 2⁴⁰–3⁴⁵ ●¹–4³⁰ ●⁰–7¹⁵, 8⁴⁵–11²⁰, 17¹⁰–35, 22³⁰–23⁴⁰ ; = 0⁰⁰–12⁴⁰, 16²⁰–n
16	7	.	.	0.4	●⁰ 2⁴⁰–5⁴⁰ ; = 0⁰⁰–9²⁰
17	7	.	.	5.2	= 7³⁰–9³⁰ ; ⌴⁰ n
18	7	.	.	4.5	= 18³⁰–24 ; ⌴¹ n–8³⁰
19	6	0.0	.	0.2	= 0⁰⁰–14³⁰ 19⁴⁰–24
20	7	0.7	.	3.2	✳⁰ 6²⁵–30 ✳¹ 7²⁰–8³⁵ ✳⁰ 9⁴⁰–10¹⁵ ●⁰ 19⁴⁰–21⁴⁰ ●¹–23²⁰ ; = 0⁰⁰–12²⁰
21	6	0.2	.	.	●⁰ 8⁰⁵–10²⁰ 18⁴⁰–19³⁵ 20⁴⁵–21²⁵ ; por. wiatru do 12 m/sek 23²⁰–24 ; = 4⁴⁰–10³⁰
22	7	1.6	.	3.5	⚹ 7²⁵–45 ⚹ 11⁴⁰–12¹⁰ ⚹ 13¹²⁻¹⁵ ♉ 13³⁰–38 ✳⁰ 23⁴⁰–24 ; por. wiatru do 14 m/sek 0⁰⁰–3³⁰
23	4	1.4	2	0.7	✳⁰ 0⁰⁰–2¹⁰ △–3³⁰ ✳⁰–4⁴⁰, 5²⁵–6¹⁵ ✳¹–9¹⁵ ♉ 10⁵⁰–11³⁵, 11⁴⁵–13¹² virga 14²⁰–16³⁰ ; por. wiatru do 14 m/sek 14³⁰–15²⁰
24	7	0.0	pł.	2.9	⚹ 7⁵⁰–9¹⁰
25	8	.	pł.	7.1	△ 3⁵⁰–4⁰⁰ ; = 3⁵⁰–6⁴⁰ 19⁴⁰–24
26	7	.	pł.	0.6	= 0⁰⁰–a, 22⁴⁰–24 ; ⌴⁰ n–10²⁰
27	7	0.3	pł.	4.7	= 0⁰⁰–9²⁰ ; ⌴⁰ n–10⁴⁰
28	7	0.7	1	2.0	✳⁰ 0⁴⁰–5²⁵ △ 7²⁰–8¹⁰ ♉ 8⁵²–10⁰⁴, 11⁵⁵–12²⁵, 13⁰²–15, 15¹¹–20, 16⁰⁸–15
29					
30					
31					
Σ	–	38.1	–	56.0	UWAGI.

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ Marzec – Mars 1957

DNI	CIŚNIENIE P − 700				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	137.5	137.1	135.3	136.6	0.8	2.6	1.0	1.4	3.7	-0.1	77	82	87	82	1.5	1.3	0.9	1.2	9	4	7	N 5	N 1	NW 3
2	132.7	131.5	128.4	130.9	1.0	2.2	0.8	1.2	3.1	-1.0	81	86	90	86	1.3	1.1	0.7	1.0	9	4	2	N 3	N 1	NW 2
3	125.0	122.4	117.4	121.6	-2.2	3.6	1.1	0.9	3.8	-2.5	100	73	83	85	0.0	2.1	1.1	1.1	9	7 ⊙	0	C 0	S 2	S 2
4	110.0	107.7	107.5	108.4	0.2	1.6	2.6	1.8	3.4	-0.7	76	98	89	88	1.5	0.2	0.8	0.8	10	10 ●	0	S 4	SW 4	NW 6
5	111.5	112.9	113.8	112.7	1.8	2.8	0.1	1.2	3.4	0.1	85	82	94	87	1.1	1.3	0.4	0.9	6 ⊙	0 ⊙	0	NW 5	W 8	WNW 3
6	114.0	114.5	114.4	114.3	-3.3	-0.5	-1.5	-1.7	0.9	-3.3	99	100	92	97	0.0	0.0	0.4	0.1	10 ≡	10 ≡	0	WNW 1	W 2	E 3
7	114.7	115.2	115.8	115.2	-0.8	0.3	-1.4	-0.8	2.8	-3.6	79	83	86	83	1.2	1.0	0.8	1.0	9	2	0	E 1	SE 3	SE 3
8	117.9	118.8	122.8	119.8	-4.4	2.5	-1.9	-1.4	3.0	-4.4	89	60	75	75	0.5	2.9	1.3	1.6	0 ⊙	0 ⊙	4	SE 3	SSE 4	SE 2
9	127.2	128.7	131.2	129.0	-5.8	3.9	-1.0	-1.0	5.1	-5.8	92	62	85	80	0.3	3.1	0.9	1.4	0 ⊙	0 ⊙	0	SE 3	S 3	SE 2
10	133.3	133.0	133.3	133.2	-4.8	7.0	-0.6	0.2	9.0	-4.8	95	39	75	70	0.2	6.1	1.4	2.6	0 ⊙	0 ⊙	0	S 1	S 3	C 0
11	132.1	131.5	126.6	130.1	-2.6	3.8	3.4	2.0	11.6	-2.6	87	83	60	77	0.7	1.3	3.1	1.7	0 ⊙	0 ⊙	5	C 0	E 1	S 4
12	122.5	120.4	118.4	120.4	2.9	5.4	1.2	2.7	7.9	0.9	69	69	96	78	2.3	2.8	0.3	1.8	9	8	0	SSW 3	W 3	W 2
13	116.8	116.4	111.4	114.9	0.9	9.1	7.1	6.0	12.2	-0.2	92	62	69	74	0.5	4.4	3.2	2.7	0	8 ⊙	0	W 2	W 4	SW 3
14	103.9	102.3	101.8	102.7	7.6	9.6	5.9	7.2	10.2	5.9	87	75	86	83	1.3	3.0	1.3	1.9	2	10	10	SW 5	SW 14	SW 17
15	106.6	104.9	100.0	103.8	3.2	3.8	2.0	2.8	6.0	0.3	91	87	96	91	0.7	1.1	0.3	0.7	10	10 ●	10	WNW 10	W 8	NW 7
16	106.3	112.5	116.8	111.9	-3.8	-3.4	-2.6	-3.1	2.6	-4.9	71	70	77	73	1.3	1.4	1.2	1.3	5	7	8	N 10	N 7	NE 8
17	114.9	109.5	97.7	107.4	-5.3	-2.0	-0.8	-2.2	-0.5	-5.6	93	77	95	88	0.3	1.3	0.3	0.6	10	10 ✳	10 ●	NE 1	S 5	S 6
18	87.8	89.6	98.0	91.8	6.2	4.7	1.8	3.6	6.2	-1.1	98	100	83	94	0.2	0.0	1.2	0.5	10	10 ●	10	WSW 7	W 10	NNW 7
19	106.2	107.6	109.6	107.8	0.1	2.2	-0.1	0.5	2.6	-0.2	80	70	98	83	1.3	2.2	0.2	1.2	8	10	10	N 3	NE 2	E 5
20	109.6	104.9	100.3	104.9	0.6	2.6	7.5	4.6	7.5	-0.7	88	98	99	95	0.8	0.2	0.2	0.4	10	10 ●	10	E 4	SSE 4	S 5
21	102.5	106.0	107.6	105.4	6.2	8.4	6.4	6.8	9.8	4.5	91	71	85	82	0.9	3.1	1.4	1.8	7 ⊙	10	10 ●	SW 8	SW 8	SW 6
22	110.6	113.1	115.5	113.1	4.1	5.4	4.4	4.6	6.9	3.8	92	86	84	87	0.7	1.3	1.4	1.1	7	2 ⊙	0	W 6	W 8	W 7
23	118.3	121.3	126.5	122.0	0.4	4.5	-1.2	0.6	5.7	-1.2	100	87	82	90	0.0	1.1	1.0	0.7	3 ⊙	6 ⊙	0	W 2	N 4	E 8
24	129.1	128.3	127.4	128.3	-2.8	4.0	1.3	1.0	5.4	-3.3	60	36	51	49	2.0	5.2	3.3	3.5	8 ⊙	3 ⊙	0	SE 8	SE 10	SE 8
25	123.6	122.5	121.9	122.7	0.6	4.4	2.6	2.6	5.4	0.2	70	57	65	64	1.9	3.6	2.6	2.7	10 ●	8	0	S 7	SE 7	S 8
26	120.3	118.4	117.9	118.9	2.8	10.6	9.0	7.8	13.8	2.3	72	68	71	70	2.1	4.1	3.4	3.2	10 ●	9	0	S 7	S 4	S 5
27	117.8	116.9	116.2	117.0	5.2	14.1	11.8	10.7	16.9	4.6	80	38	53	57	1.8	9.9	6.4	6.0	2 ⊙	4 ⊙	0	S 5	SSW 6	S 3
28	112.2	113.4	113.9	113.2	5.6	4.3	4.3	4.6	11.9	3.9	78	98	98	91	2.0	0.1	0.1	0.7	10 ●	10 ●	9	S 3	W 3	SW 2
29	114.4	115.5	117.7	115.9	3.3	3.2	3.2	3.2	4.8	2.7	98	100	100	99	0.1	0.0	0.0	0.0	10	10 ● ≡	10 ≡	N 2	N 4	NE 4
30	121.3	122.3	124.2	122.6	3.2	5.0	2.0	3.0	5.6	2.0	100	90	100	97	0.0	0.8	0.0	0.3	3 ⊙	0 ⊙	10 ≡	NE 3	NE 6	NE 5
31	123.4	123.5	123.3	123.4	2.2	2.9	5.8	4.2	6.5	1.9	100	100	85	95	0.0	0.0	1.4	0.5	10 ≡	10 ≡	0	NE 3	NE 5	NE 2
M	116.9	116.9	116.5	116.8	0.7	4.1	2.4	2.4	6.4	-0.4	86	77	84	82	0.9	2.1	1.3	1.4	6.6	6.2	4.0	4.0	5.0	4.8

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1	124.2	123.4	122.7	123.4	2.1	17.5	9.2	9.5	17.9	0.1	93	36	62	64	0.5	12.9	4.4	5.9	0 ⊙	0	0	NE 1	E 3	E 2
2	122.0	120.9	122.9	121.9	5.6	11.4	9.3	8.9	17.3	2.6	75	60	60	65	2.2	5.5	4.7	4.1	0 ⊙	3 ⊙	0	E 1	NE 5	E 5
3	125.5	126.9	128.2	126.9	5.8	7.7	5.6	6.2	9.7	3.9	82	82	91	85	1.7	1.9	0.9	1.5	0 ⊙	1 ⊙	0	E 1	NE 5	ENE 2
4	130.2	130.6	128.9	129.9	2.9	8.2	4.8	5.2	12.5	0.4	88	70	76	78	0.9	3.3	2.0	2.1	5 ⊙	0 ⊙	0	ENE 2	ENE 1	C 0
5	126.6	123.0	117.3	122.3	6.0	15.1	9.1	9.8	19.1	1.6	70	42	70	67	2.9	9.9	3.6	5.5	0 ⊙	3 ⊙	0	S 2	W 2	C 0
6	111.1	110.8	110.1	110.7	10.8	5.8	3.9	6.1	11.4	3.9	54	97	98	83	6.0	0.3	0.2	2.2	9	10	1	SW 5	NW 4	W 3
7	111.8	116.2	121.9	116.6	3.7	4.8	2.4	3.3	5.4	1.6	100	87	68	85	0.0	1.1	2.4	1.2	10 ●	3 ⊙	1	NE 6	NE 6	NE 8
8	121.9	118.4	114.6	118.3	2.6	4.8	4.6	4.2	5.3	1.4	72	78	98	83	2.1	1.9	0.2	1.4	8 ⊙	6 ⊙	9	N 5	WNW 7	NW 8
9	114.1	114.8	112.0	113.6	2.6	3.0	-1.4	0.7	4.6	-1.4	89	62	70	74	0.8	2.9	1.6	1.8	10	8	7	NW 2	NNE 4	NE 2
10	104.0	98.9	93.2	98.7	1.6	6.2	5.9	4.9	8.1	-1.9	64	75	89	76	2.5	2.4	1.0	2.0	10	10	10	SSW 5	W 8	WSW 8
11	90.0	95.8	102.9	96.2	1.3	1.6	0.8	1.1	6.3	0.1	98	85	81	88	0.1	1.1	1.3	0.8	10 ⛈	10	10 ⛈	SW 8	N 7	N 8
12	107.4	107.9	110.4	108.6	0.2	1.4	-0.4	0.2	3.6	-1.7	90	85	100	92	0.6	1.0	0.0	0.5	9	10	10	N 3	W 2	W 8
13	113.0	114.6	116.0	114.5	-1.4	1.8	-0.6	-0.2	2.3	-2.2	99	71	83	84	0.1	2.1	1.0	1.1	10 △	5	3	N 5	N 2	W 3
14	116.1	117.5	119.8	117.8	-1.4	2.9	-0.5	0.1	3.5	-2.8	99	71	82	84	0.1	2.2	1.1	1.1	9 ✳	8 ⊙	6	SW 3	NW 4	N 1
15	120.5	120.8	122.5	121.3	-1.4	3.4	-0.6	0.2	3.4	-2.9	99	70	88	86	0.1	2.4	0.7	1.1	7	8 ⊙	1	N 1	NW 5	NW 1
16	119.2	115.9	116.0	117.0	0.3	3.9	5.4	3.8	7.2	-2.0	81	100	100	94	1.1	0.0	0.0	0.4	10	10 ●	10	SSW 4	SW 5	W 5
17	117.8	120.7	122.6	120.4	4.4	4.5	2.7	3.6	5.8	2.5	100	92	86	93	0.0	0.7	1.0	0.6	10 ●	10	10	W 5	N 2	NE 2
18	121.6	120.4	117.7	119.9	3.1	4.5	2.2	3.0	4.9	2.1	97	98	96	97	0.2	0.1	0.3	0.2	10	10	8	N 4	NE 4	NE 2
19	114.4	112.2	113.1	113.2	2.0	6.2	4.3	4.2	7.8	-1.0	93	86	98	92	0.6	1.3	0.1	0.7	6	10 ⊙	10 ●	ESE 3	NE 4	NE 4
20	117.1	121.3	125.7	121.4	4.1	4.8	3.4	3.9	5.5	3.4	98	92	90	93	0.2	0.7	0.8	0.6	10 ●	10	10	NW 3	NW 3	N 1
21	128.3	129.1	129.9	129.1	3.8	5.6	3.8	4.2	6.6	3.1	90	94	100	95	0.8	0.6	0.0	0.5	10	10	10 ●	N 3	NNE 2	NE 4
22	130.2	131.2	131.5	131.0	4.0	5.8	4.6	4.8	7.3	3.4	100	92	100	97	0.0	0.7	0.0	0.2	10	9	6	N 2	W 3	N 1
23	131.2	131.3	131.7	131.4	3.9	4.9	2.3	3.4	5.5	2.3	97	92	100	96	0.3	0.7	0.0	0.3	10	10	2	NW 3	NW 3	NNW 2
24	131.1	131.2	130.1	130.8	2.4	4.8	2.6	3.1	5.5	1.6	98	90	100	96	0.2	0.8	0.0	0.3	10	10	10 ≡ ●	NW 2	NNW 2	NE 5
25	128.7	128.2	126.6	127.8	3.1	4.2	3.4	3.5	4.8	2.4	100	90	100	97	0.0	0.8	0.0	0.3	10	10	10	NE 6	NE 6	NE 7
26	125.2	124.7	122.3	124.1	3.1	5.6	4.8	4.6	6.6	2.7	100	91	100	97	0.0	0.9	0.0	0.3	10 ≡	10	7	NE 5	NE 5	NNE 4
27	120.0	118.6	115.4	118.0	5.2	7.1	5.4	5.8	7.5	4.5	97	90	98	95	0.2	1.0	0.2	0.5	9	4	10	NNW 3	! 3	NE 5
28	111.9	110.0	108.6	110.2	6.1	7.8	6.3	6.6	9.0	4.8	98	90	98	95	0.1	1.1	0.1	0.4	4 ⊙	3 ⊙	7	ENE 3	NE 3	NE 3
29	108.8	110.2	111.5	110.2	5.9	6.0	5.6	5.8	8.8	4.6	100	98	100	99	0.0	0.2	0.0	0.1	5 (K)	2 ⊙	10 ● ≡	W 1	W 5	W 3
30	110.8	109.8	110.1	110.2	7.1	6.3	6.0	6.4	9.0	5.4	100	94	83	92	0.0	0.5	1.6	0.7	10 ≡	10	2	SW 2	W 5	WNW 7
31																								
M	118.5	118.5	118.5	118.5	3.3	5.9	3.8	4.2	7.7	1.4	91	82	89	87	0.8	2.0	1.0	1.3	7.7	7.1	6.0	3.3	4.0	3.8

Ustka $H_s = 6\ m$ $H_k = 8{,}1\ m$ $h_w = 18\ m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	pż.	7.1	
2	7	.	.	5.6	= 130–630 2330–24
3	7	.	.	2.8	= 000–820, 1740–24
4	5	1.0	.	.	•0 1040–1110 •1–1230 •0–1415; = 000–1630
5	8	.	.	9.6	
6	3	.	.	0.5	= 030–445 ≡0–630 ≡1–1020 ≡0–1025 =–1110, 1135–40 ≡0–1350 ≡1–1440 =–1605 ≡0–1715 ≡1–1810
7	6	.	.	4.3	⌴1 000–1000; = 730–1330, 1720–24 [6.II:] =..2200; V 540–1030 ⌴0 2040–24
8	8	.	.	9.0	⌴1 100–830; = 000–750, 1940–21
9	8	.	.	9.1	= 000–940
10	7	.	.	9.3	= 640–730, 1840–2145; ⌴0 000–n
11	6	.	.	9.6	⌴0 250–630 ⌴1–1030; ⌔ 2105–24; = 240–930, 1230–1615
12	7	.	.	3.1	= 1920–24, ⌔ 000–220
13	6	.	.	7.3	= 000–24; ⌴2 n–900
14	6	0.0	.	2.4	•0 2120–2310, 24; ⩒ 1020–1320 ⩓–24 W; SW; = 000–332, 930–1645, 2145–24
15	6	8.6	.	.	•0 000–10, 1240–1330 ⁂1–1410 ✳1–1610 ✳2–1715 ✳1–1915 ⁂1–2040 ⩓ 000–830 W, SW, WNW ⩒–1020 por. wiatru ponad 10 m/sek
16	8	8.3	1	5.9	⁂ 1707–24, 1744–55, 1805–20, 1853–1905, 2120–2325 por. wiatru ponad 10 m/sek 000–628 ⩒–845 (por. do 16 m/sek) por. wiatru ponad 10 m/sek – 1435 N
17	7	1.1	1	.	✳0 1140, 1365 ✳1 1440 ✳2–1450 ✳1–1513 ✳2–1530 ✳1–1550 ✳0–2032 •0 24, ⌔ 2302, 3340 [15.III:] 2240, 24 = 000–530, 1240–24 W, NW
18	6	0.3	.	0.1	•0 000–632 810–915 1235–1315, 1420–1530 [16.III:] = 000–30
19	7	0.3	.	0.6	⁂ 1510–1605 ✳0–1815 •0–1935; = 1630–24
20	6	6.9	.	.	•0 923–1732; = 000–a
21	7	0.9	.	4.4	•0 100–50 •0–155 •1–220 •0–245 ⁂ 2046–2232 ⩒ 250–1932
22	7	.	.	6.5	⁂ 546–607 por. wiatru ponad 10 m/sek 020–626; = 2230–24
23	7	.	.	7.2	= 000–820
24	7	0.0	.	8.7	
25	7	0.0	.	0.9	•0 610–16 640 715
26	7	0.4	.	0.8	•0 645–830; ⊕ 1520–1610
27	8	0.3	.	7.6	•0 1730...41, 1845–1905
28	4	4.9	.	0.1	•0 618–820 •1–935 •0–1025 •0 1210–1415; = 1210–1550 2110–2240 ≡0–24; ⌒ 610–14 SW
29	3	1.7	.	.	•0 820–1240 •0–1340 1445–1505 •0–1540, 1725–50; ≡1 000–320 ≡0–425 =–815 ≡0–1545 =–2045 ≡0–2210 =–24
30	6	0.0	.	7.6	= 000–250 ≡0 1540–2040 ≡1–2315 ≡2–24
31	2	.	.	1.8	≡2 000–815 ≡1–1520 ≡0–1530 =–24
Σ	–	26.7	–	131.9	UWAGI.

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1	8	.	.	11.0	= 000–915; ⌴1 n
2	7	.	.	10.9	⌒1 n
3	7	.	.	10.7	= 1825–24; ⌒0 n
4	8	.	.	11.3	= 000–840 1940–24; ⌴1 n
5	7	.	.	11.0	= 000–24
6	5	1.5	.	1.6	•0 1305–1420; = 000–400 1240–1430 2020–24; ⊕ 640–840
7	7	1.5	.	5.8	•0 340–610 •1–705 •0–920; = 000–550
8	8	0.0	.	7.4	•0 1948–2020
9	7	0.0	.	6.8	•0 735–825 ⚹ 914–1025 ✳ 1102–36; = 100–540
10	7	2.9	.	0.7	•0 1610–2202 •1–2340 •0–24
11	7	0.5	.	3.6	•0 000–30 •1620–33 △0 647–700, 1203–20, 1328–45, 1355–1510 △0–1640, 1710–1805 ⚹ 1847–1930 ⚹0 2040–2215
12	7	3.6	.	7.8	✳ 325–415 ⚹ 615–728 ⚹ 732–845 ⚹0 850–907, 940–1030 △ 1100–30 ⚹ 1205–40, 1638–1838 ✳0 1930–2020 = 000–4[illegible]
13	7	2.2	3	7.2	✳0 150–530 △1 630–700 ⚹–738 ⚹ 1833–40 [11.IV:] = 2215–24
14	7	0.0	1	9.3	⚹0 255–303 △0 409–15 ⚹ 605–736, 930–1002, 1412–25
15	7	.	pż.	.	△ 345–55; = 2130–24
16	5	6.9	pż.	.	✳0 710–35 ✳1–920 △ 940–1030 •0–1530 •1–1540 •0–1935; = 000–24
17	6	0.0	.	.	•0 640–715 = 000–340, 650–715, 845–900
18	5	.	.	0.1	= 1230–1530 ≡0–1715 =–1735
19	7	1.9	.	4.4	•0 1620–24
20	6	0.0	.	.	•0 000–235, 640–725; = 235–1810, 2040–24
21	7	0.8	.	1.0	•0 1450–56 •0 1502–1658 •0–1735 1930–24; = 000–350
22	6	.	.	0.5	•0 000–620; = 620–1130, 1240–24
23	7	.	.	0.3	= 1530–40 ≡0–1650 =–1730
24	6	0.0	.	.	≡0 444–540 =–802, 1630–50 ≡0–1710 ≡1–1715 ≡0–1720 =–1740, 1845–1945 ≡0–24
25	6	.	.	.	•0 648–43; ≡0 000–340 =–630, 2030–24
26	6	.	.	2.7	= 000–635 ≡0–820 =–905 ≡0–1020 =–24
27	6	0.4	.	8.7	•0 1935–45, 2133–2320; = 000–830, 1130–p
28	6	0.2	.	8.8	•0 010–220, ⚹ 1747–58 (K) 1722–40 S–SE; = 000–620
29	5	0.4	.	6.1	⚹ 815–55, •0 2005–2110, 2240–24 (K) 535–a W; = 1240–1745 ≡0–1940 ≡1–24
30	5	0.0	.	2.1	•0 000–410, 805–940; ≡1 000–1010 ≡0–1030 =–1130 ≡0–1225 =–1310
31					
Σ	–	22.8	–	139.8	UWAGI.

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ **Maj – Mai 1957**

DNI	CIŚNIENIE P− +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	116.2	118.8	119.1	118.0	6.2	7.4	4.7	5.8	8.4	4.5	88	86	98	91	1.2	1.5	0.1	0.9	0 ⊙	4 ⊙	0	NW 2	WNW 3	NW 2
2	116.9	115.2	113.2	115.1	5.2	8.1	8.0	7.3	9.6	0.6	67	78	67	71	2.8	2.4	3.5	2.9	9 ⊙	6 ⊙	10	SSW 4	WNW 2	WNW 1
3	111.3	109.2	104.9	108.5	7.1	8.0	9.5	8.5	10.0	7.1	93	99	71	88	0.8	0.1	3.4	1.4	9	9 ≡	9	W 3	W 8	SW 3
4	102.5	104.6	105.0	104.0	5.0	6.6	4.2	5.0	10.0	4.1	64	65	71	67	3.1	3.4	2.4	3.0	9	5	2	W 10	W 17	W 14
5	104.6	105.8	107.2	105.9	4.2	6.2	3.2	4.2	6.7	3.1	82	80	84	82	1.4	1.9	1.2	1.5	9	8 ⊙	1	WNW 14	W 7	SW 2
6	108.5	109.2	109.0	108.9	4.0	7.1	3.8	4.7	7.5	−0.4	85	83	93	87	1.2	1.8	0.5	1.2	0 ⊙	9 ●	9	SW 3	N 2	ENE 3
7	108.3	109.7	110.2	109.4	4.0	4.2	3.8	4.0	5.8	3.2	97	93	77	89	0.2	0.5	1.9	0.9	10 ●	10 ●	8	ENE 3	NE 4	NE 7
8	108.9	108.7	109.1	108.9	3.3	4.2	3.9	3.8	5.2	3.0	98	93	90	94	0.1	0.5	0.8	0.5	10	10	10	N 8	N 8	NW 3
9	111.2	113.8	114.9	113.3	5.6	8.1	6.1	6.5	8.7	2.7	83	86	80	83	1.6	1.5	1.8	1.6	5 ⊙	10	10 ●	SW 4	W 3	NNE 3
10	111.3	111.2	111.7	111.4	5.0	5.2	5.0	5.0	6.8	3.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10	10 ≡	N 5	NW 3	W 5
11	111.4	113.4	113.3	112.7	5.8	6.0	5.8	5.8	8.7	5.0	100	97	95	97	0.0	0.3	0.4	0.2	10 ●	10	0	WNW 3	W 3	S 4
12	113.3	113.2	113.6	113.4	10.0	15.5	15.7	14.2	19.9	5.0	74	66	64	68	3.2	6.0	6.4	5.2	1 ⊙	3 ⊙	6	S 4	C 0	SSE 3
13	115.2	115.7	115.4	115.4	12.4	13.9	13.4	13.3	16.7	11.2	87	84	90	87	1.9	2.5	1.6	2.0	7	2	8 (K)	S 3	W 2	S 1
14	116.5	118.3	119.3	118.0	12.2	11.4	10.6	11.2	14.0	10.2	94	88	95	92	0.9	1.7	0.7	1.1	2 ⊙	2 ⊙	0	W 3	WNW 3	W 1
15	121.6	122.1	120.1	121.3	11.3	13.8	13.3	12.9	15.9	7.1	83	71	65	73	2.3	4.6	5.3	4.1	5 ⊙	0 ⊙	0	W 4	W 3	ENE 1
16	118.5	115.4	113.7	115.9	15.0	23.7	18.2	18.8	24.5	11.1	59	28	48	45	6.9	21.2	10.8	13.0	1 ⊙	1 ⊙	2	SSE 5	S 8	S 3
17	116.6	118.8	118.5	118.0	10.3	10.2	11.0	10.6	18.2	8.8	92	93	94	93	0.9	0.8	0.8	0.8	6 ⊙	10	9	W 3	WNW 3	W 2
18	118.6	118.0	115.7	117.4	13.3	15.4	14.1	14.2	16.7	9.0	77	74	67	73	3.5	4.6	5.3	4.5	0 ⊙	1 ⊙	4	W 1	N 2	ENE 2
19	113.4	110.7	107.8	110.6	13.6	13.8	14.7	14.2	16.6	8.6	73	79	93	82	4.2	3.4	1.1	2.9	0 ⊙	4 ⊙	6	SE 2	NE 6	NE 1
20	108.0	111.5	114.5	111.3	13.0	11.2	9.6	10.8	15.2	9.6	94	92	87	91	0.9	1.0	1.6	1.2	9 (K)	6 ⊙	9	C 0	WNW 5	W 8
21	116.4	117.6	117.3	117.1	8.8	9.5	9.0	9.1	10.6	7.9	76	86	93	85	2.7	1.7	0.8	1.7	4 ⊙	1 ⊙	1	NW 6	W 8	WNW 5
22	116.9	117.9	118.2	117.7	8.6	10.2	8.0	8.7	11.3	3.8	96	88	100	95	0.5	1.4	0.0	0.6	8	6 ⊙	10 ≡	C 0	NW 2	NE 5
23	116.0	115.5	115.3	115.6	8.4	11.6	8.6	9.3	11.6	7.9	100	74	92	89	0.0	3.6	1.0	1.5	10	6	10	NE 3	NE 6	NE 8
24	117.8	122.1	126.9	122.3	9.6	9.0	6.7	8.0	10.3	6.6	83	77	81	80	2.1	2.6	1.9	2.2	8 ⊙	2 ⊙	0	ENE 8	NE 8	NE 14
25	128.9	130.6	131.1	130.2	6.8	8.2	5.9	5.7	9.1	5.9	88	86	77	84	1.2	1.5	2.1	1.6	7	4	4	NE 8	NE 7	NE 7
26	131.0	130.9	129.6	130.5	6.2	8.4	6.1	6.7	8.8	5.0	82	78	89	83	1.7	2.4	1.0	1.7	7 ⊙	5 ⊙	0	NE 5	NE 4	NE 2
27	128.6	128.3	126.9	127.9	7.6	9.4	6.3	7.4	9.8	0.6	77	65	88	77	2.3	4.1	1.1	2.5	4 ⊙	7 ⊙	4	NE 4	NE 6	ENE 4
28	125.3	124.4	122.6	124.1	7.0	8.8	5.4	6.6	9.7	2.5	82	71	84	79	1.7	3.3	1.4	2.1	6 ⊙	2 ⊙	8	NE 3	NE 3	C 0
29	121.0	121.0	120.3	120.8	7.6	9.4	8.7	8.6	9.8	2.3	90	91	86	89	1.0	1.1	1.5	1.2	9	10	8	SW 3	W 5	W 4
30	121.1	121.9	120.0	121.0	9.4	10.7	10.0	10.0	13.0	6.7	87	86	77	83	1.6	1.8	2.9	2.1	8 ⊙	2 ⊙	0	N 4	W 6	C 0
31	117.8	116.0	114.6	116.1	12.8	14.8	10.2	12.0	20.0	5.1	66	59	88	71	5.1	6.9	1.4	4.5	1 ⊙	1 ⊙	2	WSW 2	W 5	W 3
M	115.9	116.4	116.1	116.1	8.4	10.0	8.5	8.8	11.9	5.5	84	81	83	83	1.8	2.9	2.1	2.3	5.9	5.4	5.2	4.2	4.9	3.9

Czerwiec – Juin

1	113.8	114.8	113.9	114.2	10.9	12.3	11.0	11.3	13.3	6.6	86	73	80	80	1.8	3.9	2.6	2.8	9 ⊙	7 ⊙	5	W 5	W 8	SW 4
2	115.0	117.9	118.2	117.0	10.6	11.0	11.1	11.0	13.2	10.3	94	92	89	92	0.8	1.0	1.5	1.1	9	10	0	W 5	W 6	SW 3
3	118.6	118.0	114.6	117.1	15.8	13.9	15.9	15.4	17.5	9.3	82	84	85	84	3.2	2.5	2.7	2.8	5 ⊙	5 ⊙	8	SW 1	W 4	W 1
4	112.3	111.9	108.8	111.0	16.1	15.3	13.6	14.6	17.7	11.5	85	83	84	84	2.7	3.0	2.5	2.7	3 ⊙	6 ⊙	8	WNW 2	W 5	W 1
5	104.5	103.7	102.1	103.4	12.2	13.4	11.0	11.9	14.9	11.0	98	85	87	90	0.3	2.3	1.6	1.4	10 ●	7 ⊙	5	W 4	W 7	SW 4
6	103.0	105.3	105.7	104.7	10.4	12.8	10.3	11.0	15.7	9.3	85	67	87	80	1.9	4.9	1.6	2.8	8	2 ⊙	8	W 5	W 8	SW 4
7	106.7	107.6	108.9	107.7	11.8	13.1	10.8	11.6	15.7	9.5	77	70	75	74	3.1	4.5	3.3	3.6	9	9	0	SW 3	W 8	W 2
8	111.5	112.5	110.9	111.6	12.2	14.6	14.0	13.7	16.7	6.3	80	71	79	77	2.9	4.8	3.4	3.7	6	7	3	SW 2	N 3	NE 2
9	108.0	106.6	108.9	107.8	19.1	26.0	13.2	17.9	26.6	13.1	70	51	99	73	6.6	16.5	0.2	7.8	7 ⊙	7	6	SE 6	SW 3	W 1
10	112.1	112.9	112.2	112.4	13.1	13.9	13.4	13.4	15.3	11.5	96	91	98	95	0.6	1.5	0.4	0.8	2 ⊙	7 ⊙	4	W 2	NW 3	NE 3
11	110.0	107.0	105.7	107.6	16.3	27.6	23.0	22.5	28.3	11.7	98	50	79	76	0.4	18.4	6.0	8.3	5 ⊙	8 ⊙	7	SE 3	SE 5	SE 2
12	118.7	124.9	129.1	124.2	12.3	13.0	12.0	12.3	23.1	11.6	93	80	80	84	1.0	3.0	2.8	2.3	10	5 ⊙	0	W 8	W 8	W 8
13	130.5	131.0	129.4	130.3	11.4	12.4	11.4	11.6	13.9	10.9	76	85	94	85	3.3	2.2	0.9	2.1	1 ⊙	2 ⊙	0	W 10	W 8	W 3
14	130.0	131.3	130.3	130.5	14.7	17.1	13.8	14.8	17.9	8.3	83	71	70	75	2.9	5.6	4.7	4.4	0 ⊙	0 ⊙	4	C 0	NE 2	NE 2
15	131.3	129.7	126.4	129.1	13.1	15.1	13.2	13.6	15.8	7.0	77	70	88	78	3.5	5.1	1.8	3.5	2 ⊙	1 ⊙	0	NE 1	NE 4	NE 1
16	124.9	124.4	122.0	123.8	17.2	16.7	14.5	15.7	18.6	8.6	62	75	97	78	7.4	4.8	0.6	4.3	0 ⊙	0 ⊙	1	C 0	W 3	N 1
17	121.7	120.6	118.0	120.1	17.3	18.6	16.3	17.1	22.3	10.3	54	72	77	68	9.0	6.1	4.2	6.4	2 ⊙	0 ⊙	0	SE 3	NE 2	C 0
18	116.7	114.7	111.7	114.4	18.2	20.0	18.9	19.0	23.2	12.0	59	57	68	61	8.6	10.1	6.9	8.5	1 ⊙	0 ⊙	0	SW 1	W 2	C 0
19	112.1	113.3	113.6	113.0	13.8	13.9	12.4	13.1	18.9	12.2	92	80	86	86	1.3	3.2	2.0	2.2	8	1 ⊙	8	ENE 5	NE 8	NE 4
20	115.9	116.9	118.2	117.0	13.6	14.7	11.8	13.0	16.5	10.1	76	79	82	79	3.7	3.4	2.5	3.2	6 ⊙	8 ⊙	1	E 1	NE 3	NE 1
21	117.6	114.8	110.2	114.2	13.6	16.6	15.1	15.1	19.6	8.0	61	63	74	66	6.2	7.0	4.4	5.9	4 ⊙	4 ⊙	0	S 3	NW 3	N 1
22	105.5	104.5	103.6	104.5	14.3	13.2	13.4	13.6	16.5	9.8	78	92	98	89	3.6	1.3	0.4	1.8	8 ⊙	10 ●	10	NW 1	NE 3	NE 1
23	106.8	108.2	109.8	108.3	13.1	16.2	12.1	13.4	17.1	11.5	79	80	98	86	3.1	3.6	0.3	2.3	7	8 ⊙	10 ●	W 2	WNW 5	W 5
24	110.8	110.0	107.5	109.4	13.0	15.8	12.6	13.5	16.6	8.5	88	66	77	77	1.8	6.0	3.4	3.7	8 ⊙	2 ⊙	2	SW 4	NW 3	NE 1
25	106.4	109.8	112.8	109.7	11.8	12.5	12.0	12.1	14.5	9.4	80	71	84	78	2.8	4.2	2.2	3.1	10 ●	10 ●	7	N 1	NNE 3	W 2
26	115.9	118.2	119.2	117.8	11.4	13.1	11.6	11.9	14.7	8.5	93	70	83	82	1.0	4.5	2.3	2.6	8 ●	4	2	SW 3	W 10	W 5
27	120.3	122.3	121.6	121.4	12.7	13.9	12.8	13.0	15.5	9.8	75	65	77	72	3.7	5.6	3.4	4.2	9	5	10	NW 7	W 8	SW 5
28	117.1	116.7	118.3	117.4	14.1	20.8	18.2	17.8	21.4	12.5	100	69	85	85	0.0	7.6	3.1	3.6	10 ●	10	9	SW 7	W 12	W 8
29	120.3	121.1	117.6	119.7	15.3	16.4	22.2	19.0	25.2	14.6	91	89	73	84	1.5	2.1	7.4	3.7	10	5	1	W 5	W 5	W 1
30	119.2	120.5	120.9	120.2	16.5	19.2	15.3	16.6	22.7	15.3	90	80	98	89	2.0	4.4	0.4	2.3	4 ⊙	1 ⊙	0	WNW 3	W 2	NNE 2
31																								
M	115.2	115.7	115.0	115.3	13.9	15.8	13.9	14.4	18.3	10.3	82	74	86	80	3.0	5.1	2.6	3.6	6.0	5.0	4.0	3.4	5.1	2.6

Ustka $H_s = 6\ m$ $H_b = 8{,}1\ m$ $h_w = 18\ m$ **Maj – Mai 1957**

DNI	WI. DZIAŁ. NOŚĆ V	OPAD R	GRUB. ŚNIE. GU h	USŁO. NIECZ. NIENIE	P O G O D A
1	8	.	.	12.9	⌓ ⁰ n
2	7	.	.	4.8	⌓ ² 0⁰⁰–3⁴⁵ ⌴ ² – 5³⁰
3	3	0.1	.	4.4	● ⁰ 22⁴⁰–23⁰² ● ¹–24. = 12³⁰–40 ≡ ⁰ – 13¹⁰ = – 14⁴⁰
4	8	0.0	.	8.0	● ¹ 7²⁰–35 3⁰⁵–15 5⁰²–07 ▽ 22⁴¹–47 ≫ 4³⁰ – 8³⁰ ⩫ –24
5	7	0.0	.	8.3	▽ 3³⁷–41 4⁵¹–5⁰⁴ ⟺ 8²³–9⁰² ● ⁰ 11²²–30 ⩫ 0⁰⁰–9²⁰
6	7	4.6	.	6.4	▽ 12⁵⁵–13⁰⁵ 14¹⁰–15⁰⁷ 16²⁵–17²⁰ ● ⁰ 23⁴⁵–24. ⌴ ² 3⁵⁰–5²⁰
7	6	0.7	.	.	● ⁰ 0⁰⁰–5¹⁰ 6⁰⁷–7⁰² ● ⁰ 7²⁵–13³⁵ 14³⁰ 16³⁰
8	7	0.5	.	.	● ⁰ 6¹⁸ 7³⁵ = 1⁰⁰–3⁵⁰ 23³⁰–24
9	7	15.0	.	6.0	● ⁰ 19⁵⁰–24. = 0⁰⁰–3³⁰
10	6	5.6	.	.	● ⁰ 0⁰⁰–1⁴⁵ ● ¹–2⁴⁰ ● ⁰ 6⁰² ● ²–6¹⁵ ● ⁰–12⁴⁰ 17⁰⁵–18⁴⁰ ● ⁰ 21³⁰–23⁰⁰ ● ⁰ 23⁴⁰–24. = 10⁴⁰–11³⁰ ≡ ⁰ 20³⁵–45 ≡ ¹–21⁵⁰
11	6	2.5	.	2.9	● ⁰ 0⁰⁰–6⁴⁰ ● ¹–10⁴⁰ ● ⁰–12⁴⁰. = 0⁰⁰–n. 20⁴⁵–24 **[10.V:** ≡ ⁰–22⁴⁰ = –24
12	7	0.0	.	10.0	= 0⁰⁰–8¹⁵
13	6	13.9	.	7.9	● ⁰ 5²⁰–6⁰² ▽ 15⁴⁰–16¹⁵ 21¹⁵–⁴² 22³⁰–23¹⁶ (ℝ) 14⁴⁰–15⁴⁰ ℝ –16¹⁵ (ℝ) 20⁴⁰–21³⁰ SW–W–NW ℝ ⁰–21³⁶ (ℝ) –22⁴⁰ ℝ ⁰–23⁰⁵
14	6	.	.	10.6	= 0⁰⁰–3⁵⁰ 4⁵⁵–5⁰⁰ ≡ ⁰–5⁴⁰ = –6⁰⁰. ⌴ ¹ 21⁴⁰–24 **[13.V:** (ℝ) –23²⁵. = 7³⁰–8³⁰. 9⁴⁰–24
15	7	.	.	13.4	⌴ ¹ 0⁰⁰–6⁵⁰
16	8	.	.	13.7	
17	7	0.0	.	2.8	● ⁰ 17²⁰–18⁰⁸. 18⁴³–19⁰⁵. ⌓ ⁰ 3⁴⁵–a. = 21⁰⁰–24
18	7	.	.	13.7	= n
19	7	2.4	.	9.4	▽ 16³⁸–17¹⁰ 17⁴⁶–18¹². (ℝ) 15³⁰–16²⁵ SE–SW ℝ ⁰–17⁴² (ℝ) –18⁵². ⌓ ⁰ 5²⁰–a
20	7	.	.	4.1	▽ 2⁵⁰–4⁰³. 4¹⁹–²⁵. (ℝ) 21³–3¹⁵ ℝ ⁰–4¹⁰ (ℝ) –8⁴⁵ SE–W. ⌒ 4¹⁰–5³³
21	7	.	.	13.2	= 1³⁰–3³⁰
22	7	0.0	.	7.1	≡ ⁰ 19⁴⁵–21¹⁵ = –24. ⌓ ⁰ 2⁰⁰–11⁰⁰
23	7	0.5	.	2.7	● ⁰ 0¹⁵–3¹⁰ ● ⁰ 19⁰⁹–24. = 0⁰⁰–3¹⁰
24	7	.	.	0.7	● ¹ 1⁰⁰–2²⁰. ≫ 14⁰⁰–24 NE
25	7	.	.	10.8	≫ 1⁰⁰–3³⁰ NE
26	7	.	.	9.9	
27	8	.	.	13.0	
28	8	.	.	12.0	
29	6	0.0	.	0.5	● ⁰ 8¹⁰–11¹³. = 0⁰⁰–13⁴⁵. 20⁵⁰–24
30	7	.	.	11.6	= 0⁰⁰–6¹⁰
31	8	.	.	13.0	= 22²⁰–24
Σ	–	45.8	–	235.8	UWAGI:

Czerwiec – Juin

1	7	.	.	9.1	= 0⁰⁰–7²⁰
2	6	0.0	.	0.6	● ⁰ 10²⁰–11⁵⁰. = 6³⁰–8³⁰. 11⁵⁰–19¹⁰
3	8	0.4	.	9.3	● ⁰ 18¹⁰–19¹⁵
4	6	1.2	.	10.3	= 0²⁰–8³⁰ ∞ –11²⁰ = –24
5	7	3.0	.	4.2	● ⁰ 5⁴⁵–7³⁰ ● ¹–8³⁰ ● ⁰–9¹⁵. = 0⁰⁰–n,a
6	8	0.0	.	8.4	▽ 5⁴²–47. 6⁴⁰–7¹⁰. 19³⁵–21¹⁰
7	7	.	.	6.0	
8	6	0.0	.	8.2	● ⁰ 9⁴²–10⁰⁰. = 0⁴⁰–a, n. 20³⁰–24
9	7	24.4	.	5.7	● ⁰ 16⁴⁰–17⁰³ ● ¹ 17³⁵–18³⁵ ● ²–18⁵⁰ ▽ –20⁵⁷. (ℝ) 14¹⁵–⁴⁰ ℝ ⁰–20⁴⁵ SW–E. = 0⁰⁰–4²⁰. 19⁰⁰–24
10	6	.	.	9.4	= 0⁰⁰–9³⁰. 13³⁰–24. ⊕ ¹ 15¹⁰–17³⁰
11	7	0.0	.	9.5	= 0⁰⁰–4⁴⁵ ≡ ¹–7⁴⁵ = –8²⁰ ⊕ 16⁴⁰–18²⁰ ⌓ na
12	8	.	.	9.4	● ⁰ 4⁵⁰–55 ● ¹–5⁴⁰ ● ⁰–7¹⁰. = 0³⁰–4³⁵ ≡ ⁰–4⁴⁵ ≡ ¹–5¹⁰ ≡ ⁰–5⁴⁰ = –7²⁰
13	7	.	.	13.3	
14	7	.	.	13.4	= 4⁴⁵–7⁰⁰. ⌓ ⁰ n
15	8	.	.	15.1	= 22⁵⁰–24. ⌓ ⁰ 22⁵⁰–24
16	8	.	.	14.8	= 0⁰⁰–5⁵⁰. ⌓ ¹ 0⁰⁰–4⁵⁰ ⌓ ² –5⁵⁰
17	8	.	.	14.9	
18	8	.	.	15.0	⌓ ⁰ n
19	7	.	.	10.2	= 4⁴⁰–5¹⁵
20	8	.	.	12.7	
21	7	.	.	12.1	
22	6	2.4	.	3.2	● ⁰ 11³⁰–12⁰⁰ ● ¹–12⁴⁰ ● ⁰–14³⁵ 22²⁰–23¹⁵ ● ¹–23²⁰ ● ⁰–23⁴⁰. = 2⁰⁰–4³⁰. 14³⁵–24. ⊕ 7⁴⁰–8³⁵
23	7	0.1	.	7.7	● ⁰ 3⁵⁰–5⁴⁰ ▽ ⁰ 17³⁵–18⁰⁵ ● ⁰–22¹⁵. = 0⁰⁰–n. 22¹⁵–24
24	8	0.7	.	9.8	= 0⁰⁰–4¹⁰ 22⁵⁰–24. ⊕ 8¹⁰–12³⁰
25	7	1.3	.	0.9	● ⁰ 6⁵⁰–7¹⁵ ● ¹–7⁴⁰ ● ⁰–9¹⁵. 13¹⁰–15⁰⁷. 17²⁰–18³⁰. = 0⁰⁰–n
26	8	1.6	.	11.9	● ⁰ 20⁷–40. 7³⁵–8⁰⁰ ▽ 14¹⁵–²⁰
27	7	2.1	.	5.3	▽ 1¹⁵–50. 4²⁰–40. 6⁴⁵–7⁰⁰. 8³⁵–50. = 21³⁰–24
28	7	0.0	.	2.2	● ⁰ 3²⁰–9⁴⁰ 22³⁵–23⁰⁰. ≫ 13²⁰–22⁰⁰. = 0⁰⁰–5³⁰ ≡ ⁰–7⁵⁰ = –13³⁰. 21¹⁰–24
29	6	.	.	13.0	= 0⁰⁰–22⁴⁵
30	7	.	.	7.4	= 3⁴⁰–8²⁰. 20¹⁰–24
31					
Σ	–	37.2	–	273.0	UWAGI:

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ **Lipiec – Juillet 1957**

DNI	CIŚNIENIE p − 700				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	121.2	118.5	115.3	118.3	14.5	25.7	22.4	21.2	28.5	11.2	88	37	56	60	2.0	21.0	11.8	11.6	7	3 ⊙	3	SE 5	SE 4	SE 4
2	112.2	115.7	117.5	115.1	18.9	15.5	15.3	16.2	24.4	15.3	84	95	93	91	3.5	0.9	1.2	1.9	9	10	0	SE 4	WNW 8	W 5
3	119.2	119.(	117.6	118.7	15.0	16.3	14.4	15.0	18.1	14.3	80	84	71	78	3.4	2.9	4.8	3.7	2 ⊙	8 ⊙	2	NW 8	NW 8	C 0
4	114.8	112.3	109.3	112.1	15.3	22.4	21.4	20.1	25.4	10.5	83	66	80	76	3.0	9.3	5.2	5.8	10 ●	2 ⊙	10	SSW 3	WNW 2	NW 2
5	111.7	114.7	116.4	114.3	17.3	16.9	16.7	16.9	21.4	16.2	98	98	84	93	0.4	0.4	3.1	1.3	5	9	0	NW 4	WNW 6	W 8
6	119.4	120.2	119.4	119.7	15.1	17.2	15.7	15.9	17.8	14.9	79	75	84	79	3.7	4.9	2.8	3.8	6 ⊙	1 ⊙	0	NW 7	W 8	W 4
7	120.4	120.5	118.0	119.6	16.3	19.5	19.4	18.6	20.3	10.1	83	76	70	76	3.1	5.5	6.8	5.1	5	1	7	W 1	N 4	E 4
8	114.3	115.9	114.8	115.0	20.6	20.3	20.1	20.3	24.4	18.3	62	82	69	71	9.1	4.2	7.2	6.8	7	4 ⊙	4	S 2	W 5	W 1
9	114.4	115.0	113.3	114.2	18.2	18.5	17.3	17.8	20.1	17.2	81	79	82	81	3.9	4.5	3.5	4.0	7	1 ⊙	0	W 4	W 6	W 3
10	111.8	111.0	110.3	111.0	17.0	20.2	18.2	18.4	22.1	11.9	81	69	69	73	3.8	7.3	6.4	5.8	3 ⊙	5 ⊙	1	SW 3	WNW 2	NNE 1
11	109.7	111.3	112.2	111.1	17.2	17.7	17.3	17.4	20.0	15.4	78	91	84	84	4.3	1.8	3.1	3.1	10	10 ●	10	NNE 1	NE 1	NNE 3
12	112.0	112.4	112.2	112.2	17.3	18.3	17.6	17.7	20.7	16.2	91	88	93	91	1.8	2.4	1.4	1.9	8	10	10	NE 5	NE 6	NE 5
13	111.6	114.8	116.5	114.3	16.9	19.0	17.3	17.6	20.1	16.7	100	85	92	92	0.0	3.4	1.6	1.7	10	7	1	W 4	W 3	WNW 1
14	116.7	115.4	114.0	115.4	18.7	21.5	18.7	19.4	21.9	11.0	86	76	76	79	3.2	6.1	5.2	4.8	7 ⊙	7 ⊙	10	C 0	NE 2	C 0
15	111.5	111.1	111.1	111.2	16.9	20.5	16.7	17.7	20.6	16.5	98	76	98	91	0.4	5.9	0.4	2.2	9	10	5	E 1	SSE 2	C 0
16	111.0	111.2	110.2	110.8	15.7	19.6	17.0	17.3	20.4	12.3	98	76	88	87	0.4	5.5	2.4	2.8	8 ⊙	7 ⊙	10 ●	W 2	NW 2	NNW 2
17	105.9	105.7	106.5	106.0	15.7	15.5	16.1	15.8	17.3	15.1	96	100	94	97	0.7	0.0	1.2	0.6	10 ●	10 ●	10	NW 6	NW 8	NW 10
18	107.6	108.9	107.9	108.1	16.1	17.2	15.8	16.2	17.4	15.6	89	96	96	94	1.9	0.8	0.7	1.1	10	10	2	NW 10	W 8	W 2
19	106.4	106.5	105.9	106.3	16.9	18.8	17.4	17.6	20.4	12.2	93	90	89	91	1.4	2.1	2.3	1.9	2 ⊙	0 ⊙	0	WSW 3	W 3	N 2
20	103.9	103.3	103.9	103.7	19.8	28.0	20.1	22.0	28.7	14.9	91	40	94	75	2.2	22.6	1.3	8.8	8 ⊙	8	8	SE 4	SE 6	SE 1
21	102.5	100.4	102.6	101.8	17.9	27.0	17.6	20.0	27.1	15.3	100	40	99	80	0.0	21.3	0.2	7.2	5	6 (≡)	9	C 0	SE 5	SE 3
22	102.0	102.6	103.5	102.7	18.7	19.5	17.7	18.4	23.2	17.5	94	96	99	96	1.3	0.9	0.2	0.8	9 ⊙	10	3	E 3	NE 6	NNE 2
23	103.5	104.0	103.4	103.6	17.7	19.2	18.7	18.6	20.5	17.3	99	92	98	96	0.2	1.7	0.5	0.8	10 ●	7 ⊙	8	N 3	N 2	W 3
24	104.4	106.0	106.2	105.5	17.2	17.1	17.2	17.2	19.0	16.5	97	68	71	79	0.6	6.2	5.6	4.1	10 ●	8	7	NW 8	NW 10	W 10
25	105.9	106.6	105.3	105.9	13.8	16.7	13.8	14.5	17.6	13.6	99	94	97	97	0.2	1.2	0.6	0.7	10 ●	9	6	W 6	W 5	NW 1
26	102.6	104.6	103.7	103.6	14.1	17.5	14.7	15.2	17.9	12.0	99	86	100	95	0.2	2.8	0.0	1.0	9	7	10 ●	S 1	WNW 8	SW 3
27	100.2	100.8	100.9	100.6	15.1	15.1	14.7	14.9	18.8	14.0	100	100	98	99	0.0	0.0	0.4	0.1	10 ●	10 ●	9	SW 3	W 4	SW 3
28	101.4	103.2	104.5	103.0	14.1	15.5	13.7	14.2	17.3	11.3	98	98	92	96	0.4	0.4	1.3	0.7	9	8	6	SW 6	SW 2	W 3
29	105.1	107.5	109.1	107.2	14.4	18.3	16.1	16.2	19.5	11.6	91	76	92	86	1.4	5.0	1.6	2.7	4 ⊙	7 ⊙	7	SSW 4	W 7	WSW 3
30	108.5	111.3	115.5	111.8	16.0	18.9	17.9	17.7	19.7	13.9	95	96	98	96	1.0	0.8	0.4	0.7	8	7 ⊙	1	S 2	NW 4	WNW 4
31	118.3	121.2	121.4	120.3	17.4	17.4	16.7	17.0	18.1	16.6	96	95	90	94	0.9	1.1	2.0	1.3	10	5 ⊙	9	NW 10	NW 14	W 7
M	110.0	110.7	110.6	110.4	16.6	19.1	17.2	17.5	20.9	14.4	91	81	87	86	1.9	4.9	2.7	3.2	7.6	6.7	5.4	4.0	5.2	3.2

Sierpień – Août

1	120.8	121.6	120.2	120.9	17.6	18.1	17.7	17.8	18.8	13.4	80	75	77	77	4.0	5.3	4.5	4.6	1 ⊙	3 ⊙	0	WNW 8	W 8-	WNW 8
2	118.7	119.7	119.9	119.4	16.3	17.1	17.2	17.0	18.3	16.0	72	86	71	76	5.1	2.8	5.6	4.5	4	5 ⊙	8	NW 8	WNW 14	NW 8
3	118.5	118.3	117.6	118.1	16.5	17.2	18.1	17.5	18.6	15.6	80	77	80	79	3.9	4.5	4.1	4.2	6 ⊙	7	1	NW 8	WNW 10	NW 8
4	118.4	120.3	121.6	120.1	18.2	20.4	16.6	18.0	20.7	12.7	79	75	90	81	4.5	6.1	2.0	4.2	2 ⊙	1 ⊙	1	NW 3	NNW 2	C 0
5	122.5	123.4	122.8	122.9	14.4	20.8	16.4	17.0	21.2	11.6	100	68	91	86	0.0	7.8	1.7	3.2	1 ⊙	6 ⊙	1	N 1	NW 3	N 1
6	122.6	121.4	118.8	120.9	16.0	21.6	16.6	17.7	21.9	11.5	87	71	84	81	2.3	7.4	3.1	4.3	2 ⊙	2 ⊙	2	SW 3	NW 3	N 1
7	114.5	111.4	109.3	111.7	17.9	23.5	16.4	18.6	24.0	14.6	75	56	94	75	5.2	12.6	1.1	6.3	7	10	9 ●	SE 3	S 3	SE 1
8	109.0	111.1	112.0	110.7	18.7	20.5	14.4	17.0	20.5	14.2	85	75	79	80	3.4	6.1	3.4	4.3	4 ⊙	5 ⊙	2	N 4	NE 6	E 2
9	110.2	107.2	102.9	106.8	15.1	21.6	18.8	18.6	22.8	10.1	76	55	74	68	4.1	11.7	5.5	7.1	4 ⊙	6 ⊙	10	W 2	SE 4	SE 7
10	98.2	98.5	101.1	99.3	16.3	18.0	18.0	17.6	22.6	15.5	94	97	90	94	1.1	0.6	2.0	1.2	10 ●	10	4	S 3	S 3	W 3
11	106.1	106.6	107.0	106.6	17.2	25.6	20.8	21.1	26.5	14.4	88	56	76	73	2.4	14.6	6.0	7.7	0 ⊙	6 ⊙	3	W 5	SW 6	SW 2
12	107.7	109.2	109.1	108.7	17.5	19.7	18.5	18.6	23.0	17.4	89	74	79	81	2.2	5.9	4.5	4.2	9	8	4	SSW 4	WNW 4	W 2
13	110.7	112.2	112.8	111.9	15.8	20.2	17.3	17.6	21.6	14.2	87	69	88	81	2.2	7.5	2.4	4.0	3 ⊙	1 ⊙	3	SW 3	W 7	W 1
14	111.9	111.6	110.7	111.4	15.2	21.6	18.1	18.2	22.6	13.9	92	71	92	85	1.3	7.4	1.7	3.5	9	7	10	W 1	W 2	S 2
15	107.5	107.9	108.5	108.0	16.7	18.9	16.9	17.4	20.9	15.5	92	86	90	89	1.6	2.9	1.9	2.1	8	9	10	NW 1	N 1	NE 2
16	109.4	109.3	109.1	109.3	16.5	20.3	15.1	16.8	22.3	15.1	97	85	100	94	0.6	3.5	0.0	1.4	9	10	10 ●	S 2	S 2	WSW 1
17	107.3	107.3	105.9	106.8	14.9	17.9	15.7	16.0	18.4	14.9	100	71	85	85	0.0	5.9	2.6	2.8	10	9	9	WSW 1	W 5	W 4
18	102.7	102.5	104.2	103.1	17.1	16.3	17.7	17.2	17.7	13.2	81	100	82	88	3.7	0.0	3.6	2.4	10	10 ●	8	W 7	W 10	W 12
19	107.5	110.5	113.0	110.3	17.6	19.0	16.2	17.2	19.7	16.2	91	86	94	90	1.8	3.2	1.2	2.1	10	5 ⊙	5	W 5	WSW 6	SW 4
20	112.7	112.4	111.6	112.2	15.3	16.4	16.5	16.2	17.8	14.1	89	84	94	89	1.9	2.8	1.2	2.0	7	10 ●	10	SW 5	SW 6	SW 6
21	111.6	111.0	110.1	110.9	17.3	17.7	13.7	15.6	18.3	13.7	72	80	94	82	5.4	4.0	0.9	3.4	8 ⊙	9	10 ●	WNW 6	W 8	W 2
22	109.1	110.0	109.5	109.5	15.6	15.7	15.7	15.7	16.5	12.2	74	73	64	70	4.6	4.8	6.4	5.3	8	7	7	WNW 4	NW 6	WNW 10
23	109.9	110.4	110.0	110.1	11.0	16.0	12.2	12.8	17.3	9.6	91	63	87	80	1.1	6.8	1.9	3.3	6	4 ⊙	0	SW 4	W 5	WNW 1
24	105.5	100.7	101.2	102.5	12.5	16.1	15.5	14.9	18.3	10.3	78	81	80	80	3.2	3.4	3.5	3.4	8	10 ●	8	S 2	S 5	W 74
25	107.1	106.0	105.8	106.3	11.2	17.7	12.7	13.6	18.5	9.9	88	51	98	79	1.7	9.8	0.4	4.0	8 ⊙	9	10 ●	SW 7	SW 8	W 1
26	104.6	103.3	103.7	103.9	11.6	15.8	12.1	12.9	16.7	9.9	87	73	93	84	1.8	4.8	1.0	2.5	0 ⊙	10	10	S 5	SW 8	SW 6
27	106.0	108.8	110.4	108.4	14.9	15.5	11.0	13.1	15.7	10.6	83	73	96	84	2.9	4.8	0.5	2.7	9 ●	8 ⊙	10	W 8	W 6	SW 2
28	110.4	111.3	112.6	111.4	11.0	15.3	12.0	12.6	17.4	9.2	96	59	94	83	0.5	7.2	0.8	2.8	10 ●	10 (≡)	4	SSW 3	WSW 3	WNW 1
29	113.5	114.6	115.2	114.4	11.0	15.5	11.8	12.5	16.7	10.2	99	73	95	89	0.1	4.8	0.6	1.8	10	4 ⊙	3	SW 2	SW 3	SW 2
30	115.6	116.3	115.6	115.8	11.6	14.6	11.6	12.4	15.5	9.6	99	76	87	87	0.1	4.0	1.8	2.0	7 ⊙	10 ●	0	SW 3	W 8	W 7
31	111.8	111.8	111.0	111.5	11.7	15.3	9.9	11.7	15.7	9.9	88	85	93	89	1.6	2.6	0.8	1.7	8	4	1	SW 4	SW 5	C 0
M	111.0	111.2	111.1	111.1	15.2	18.4	15.5	16.2	19.6	12.9	87	74	87	83	2.4	5.7	2.5	3.5	6.4	6.9	5.6	4.0	5.5	3.9

Ustka $H_s = 6\ m$ $H_b = 8.1\ m$ $h_w = 18\ m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	2.1	.	-	= $0^{00}-5^{20}$ $20^{40}-n$
2	7	.	.	8.3	(K) $1^{45}-2^{40}$ ▽K -4^{40} (K) $6^{40}-7^{20}$ ▽K -7^{30} ; = n
3	8	0.3	.	13.5	
4	7	9.3	.	9.1	• $^{0}5^{20-40}$ $6^{25}-8^{40}$ • $^{1}-8^{51}$ • $^{0}-8^{56}$ (K) $21^{45}-22^{03}$ ▽K -23^{45} ; = $19^{40}-24$
5	6	.	.	8.1	= $0^{00}-6^{15}$ ≡ $^{1}-7^{10}$ ≡ $^{0}-7^{30}$ = -9^{10} ≡ $^{1}-10^{45}$ = $-n$
6	8	.	.	14.2	
7	7	.	.	12.4	⊕ $9^{40}-10^{20}$
8	7	.	.	9.3	⊕ $7^{20}-9^{45}$
9	7	.	.	8.8	= $10^{20}-13^{30}$, $19^{40}-24$
10	6	.	.	9.4	= $0^{00}-24$
11	6	0.4	.	0.3	• $^{0}11^{10}-14^{15}$; = $0^{00}-15^{20}$
12	6	1.1	.	0.8	▽ $20^{15}-21^{10}$; = $9^{20}-18^{10}$, $21^{10}-24$
13	6	1.1	.	5.7	• $^{0}0^{30}-3^{10}$; = $0^{00}-15^{10}$, $21^{20}-24$
14	7	4.0	.	8.3	• $^{0}16^{40}-19^{15}$; = $0^{00}-4^{15}$ ≡ $^{0}-5^{35}$ = -11^{30}, $16^{05}-24$ ⌒ $^{0}5^{30}-9^{00}$
15	6	5.2	.	0.9	• $^{0}0^{20-40}$, $3^{45}-7^{10}$ ▽ $14^{10}-15^{15}$, $15^{50}-16^{05}$ • $^{0}16^{30-45}$; = $0^{00}-18^{30}$, $20^{40}-24$
16	6	24.0	.	6.9	• $^{0}21^{30}-24$; = $0^{00}-24$
17	6	29.0	.	0.1	• $^{0}0^{00}-6^{10}$ • $^{1}-9^{50}$ • $^{0}-13^{02}$ • $^{1}-14^{05}$ • $^{0}-15^{35}$; = n
18	7	.	.	1.2	• $^{0}2^{55}-3^{10}$ 6^{33-50}, 7^{15-35} ; = $22^{40}-24$
19	7	.	.	12.9	= $0^{00}-10^{20}$, $20^{20}-n$
20	6	0.0	.	10.5	(K) $17^{51}-18^{59}$ SW – W – NNW ▽K 20^{17-40}
21	6	10.2	.	5.3	▽ 2^{35-45} (K) 13^{55} SW, 14^{55} W ▽K $16^{50}-17^{55}$ ▽ 18^{20-42} ; = $6^{20}-a$
22	6	4.0	.	4.1	• $^{0}14^{35-50}$
23	7	0.0	.	4.9	▽ $3^{40}-5^{40}$ • $^{0}7^{10-55}$, = $n-7^{40}$, $20^{10}-24$
24	7	2.8	.	4.5	• $^{0}7^{40-55}$; = $0^{00}-a$
25	7	18.0	.	1.8	▽ $6^{56}-7^{05}$, $7^{17}-8^{12}$, $10^{30}-11^{10}$, $11^{25}-12^{05}$, 22^{10-50} ; = $7^{20}-9^{30}$; ≫ $0^{00}-5^{20}$
26	7	18.2	.	3.6	▽ $3^{20}-6^{40}$, $9^{53}-10^{05}$ • $^{0}18^{20}-24$; = $22^{40}-24$
27	6	9.6	.	3.6	• $^{0}0^{00}-2^{30}$, $3^{00}-5^{40}$ • $^{1}7^{00-30}$ • $^{0}-8^{10}$ ▽ 8^{40-50} $12^{10}-14^{55}$; = $0^{00}-n$, $8^{00}-10^{40}$
28	7	5.1	.	4.3	▽ 0^{15-45}, $3^{47}-4^{20}$, $8^{45}-9^{10}$, $10^{30}-12^{21}$, $12^{45}-13^{17}$, 15^{26-40} (K) $4^{40}-5^{40}$; = $2^{00}-7^{40}$
29	7	5.1	.	7.4	▽ 7^{10-20}, 21^{50-53}, $21^{57}-22^{20}$
30	7	.	.	8.5	▽ $3^{40}-5^{25}$; = $2^{00}-10^{20}$ $22^{15}-24$
31	7	.	.	3.8	≫ $11^{20}-21^{00}$; = $0^{00}-12^{30}$
Σ	–	149.5	–	-	UWAGI.

Sierpień – Août

1	7	.	.	11.7	= $0^{00}-4^{40}$
2	7	.	.	12.7	
3	8	.	.	12.8	
4	8	.	.	13.4	
5	7	.	.	12.7	= $2^{40}-9^{15}$, $21^{30}-24$, ⌒ $^{0}4^{00}-9^{00}$
6	8	.	.	12.8	= $0^{00}-7^{20}$
7	7	1.1	.	1.7	▽ 14^{25-45} $15^{30}-18^{20}$ • $^{0}21^{12}-22^{20}$; = $19^{20}-24$
8	7	.	.	12.4	= $0^{00}-4^{30}$
9	7	1.2	.	7.1	⊕ $10^{45}-14^{20}$
10	6	20.7	.	1.6	• $^{0}5^{20-35}$ • $^{1}-12^{12}$ • $^{0}-13^{18}$ ▽ 18^{40-45} ; (K) $^{0}18^{36}-19^{20}$ ≤ $21^{40}-22^{22}$; = $14^{23}-24$
11	8	0.2	.	11.4	= $0^{00}-6^{12}$
12	7	.	.	5.0	• $^{0}4^{25}-5^{40}$ 7^{20-45}
13	7	.	.	11.2	= $20^{20}-24$
14	6	4.2	.	2.2	= $0^{00}-24$
15	7	0.0	.	4.2	▽ $0^{31}-3^{12}$ • $^{0}-7^{12}$, $23^{15}-24$; = $0^{00}-9^{20}$, $17^{20}-24$
16	6	20.3	.	2.2	• $^{0}0^{00}-1^{00}$ ▽ 13^{20-35} $17^{30}-18^{40}$ • $^{0}-22^{10}$; = $0^{00}-n$
17	7	1.1	.	0.3	• $^{0}0^{30}-1^{00}$ $2^{00}-7^{10}$, $8^{30}-10^{40}$ • $^{1}-11^{20}$ • $^{0}-14^{25}$; = $n-13^{40}$ $22^{20}-24$
18	6	16.4	.	.	▽ $9^{40}-10^{00}$ • $^{0}10^{20-30}$ • $^{1}-11^{50}$ • $^{2}-13^{00}$ • $^{1}-17^{20}$ • $^{0}-19^{30}$ ▽ $22^{50}-23^{30}$.
19	7	.	.	5.2	• $^{0}0^{40}-3^{30}$
20	6	3.4	.	0.7	• $^{0}13^{15}-15^{30}$ $16^{45}-20^{30}$; = $15^{20}-24$
21	7	0.7	.	1.6	• $^{0}0^{25}-3^{00}$, ▽ $17^{47}-19^{10}$ • $^{0}19^{40}-22^{30}$; = $0^{00}-4^{40}$, $22^{30}-24$
22	8	0.0	.	8.7	▽ $3^{30}-4^{25}$; ≫ $22^{00}-24$
23	8	.	.	11.2	▽ 2^{30-42} ; ≫ $0^{00}-na$
24	7	9.0	.	0.9	• $^{0}12^{50}-16^{02}$ • $^{1}-17^{40}$ • $^{0}-20^{40}$; (K) $20^{30}-21^{10}$; ≫ $20^{40}-24$
25	7	0.2	.	3.2	▽ $18^{50}-19^{35}$ • $^{0}20^{40}-22^{25}$
26	7	30.1	.	7.8	▽ $15^{30}-16^{05}$ 17^{30-55} $18^{40}-19^{48}$ $20^{50}-22^{15}$ $22^{45}-24$
27	7	21.6	.	5.3	▽ 0^{00-10} $0^{50}-3^{25}$ $3^{50}-4^{15}$ $7^{49}-9^{47}$ 10^{32-43} 11^{00-35} $12^{52}-13^{02}$ 19^{12-35} ; = $20^{30}-n$
28	6	0.0	.	1.2	• $^{0}7^{40}-8^{40}$ $10^{35}-11^{14}$ ▽ $15^{07}-16^{25}$, $17^{50}-18^{20}$, (K) $13^{40}-14^{10}$ NW – N ; = $0^{00}-n$
29	7	0.5	.	6.6	▽ $17^{45}-18^{28}$, 23^{10-35} ; = $0^{00}-9^{20}$
30	7	0.0	.	6.8	▽ $13^{55}-14^{15}$; = $0^{20}-5^{20}$ $6^{40}-8^{30}$ $21^{40}-24$
31	7	0.5	.	3.4	• $^{0}4^{35}-5^{15}$, 9^{30-48} • $^{1}-10^{00}$ ▽ 11^{35-45}, $18^{50}-19^{40}$; = $0^{00}-a$, $20^{20}-24$
Σ	–	131.2	–	198.2	UWAGI.

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	110.5	111.7	113.2	111.8	9.6	14.8	13.9	13.0	14.9	9.4	99	72	82	84	0.2	4.7	2.9	2.6	8 ⊙	7 ⊙	9	SW 1	NW 5	NW 2
2	112.6	111.9	111.1	111.9	12.0	17.0	14.0	14.2	19.3	10.2	82	71	99	84	2.5	5.6	0.2	2.8	8	7	10	SW 3	SW 4	SW 2
3	110.5	113.0	115.2	112.9	13.9	15.1	11.1	12.8	15.2	11.1	76	78	94	83	3.6	3.9	0.8	2.8	10 ●	8	2	W 6	WNW 6	W 3
4	117.4	119.7	120.9	119.3	10.1	15.1	10.5	11.6	16.1	8.4	99	67	91	86	0.2	5.6	1.1	2.3	4 ⊙	4 ⊙	4	SW 4	W 8	WSW 7
5	119.6	116.4	113.3	116.4	10.4	16.6	13.5	13.5	18.1	7.8	90	57	98	82	1.3	8.2	0.4	3.3	8	10	10 ●	SSW 2	SW 4	SW 4
6	114.1	115.2	117.1	115.5	10.9	17.8	12.1	13.2	18.2	10.4	97	65	93	85	0.3	7.1	1.0	2.8	9	6	2	SW 5	W 6	W 7
7	118.0	117.5	116.0	117.2	10.8	21.4	16.3	16.2	21.5	8.6	90	49	81	73	1.4	13.0	3.4	5.9	7	7 ⊙	1	SW 2	SSW 3	S 7
8	114.7	116.2	118.9	116.6	16.5	19.1	14.9	16.4	25.5	14.3	84	81	97	87	3.1	4.2	0.5	2.6	4 ⊙	6 ⊙	7	S 3	W 5	C 0
9	116.9	117.3	122.1	118.8	16.1	17.7	13.9	15.4	20.4	13.4	88	90	83	87	2.1	2.0	2.7	2.3	7 ⊙	9	9	NNE 1	NW 4	NW 5
10	122.1	119.8	116.1	119.3	11.8	18.9	12.6	14.0	18.9	11.0	97	55	87	80	0.3	9.9	1.9	4.0	7 ⊙	3 ⊙	0	SW 3	SSW 2	NW 1
11	109.9	104.1	93.9	102.6	12.0	20.5	15.9	16.1	20.9	10.5	91	54	82	76	1.2	11.0	3.3	5.2	3 ⊙	4 ⊙	10 ●	S 2	SSW 8	S 8
12	89.9	88.4	93.4	90.6	13.9	13.4	11.0	12.3	17.7	10.1	93	87	91	90	1.1	2.0	1.1	1.4	8	8	9	SSW 3	SW 6	SW 5
13	98.1	98.1	96.2	97.5	9.9	13.8	10.7	11.3	14.3	9.4	87	66	84	79	1.6	5.4	2.1	3.0	9	8 ⊙	8	SW 6	SW 5	S 5
14	96.4	97.5	100.5	98.1	9.0	13.6	12.1	11.7	14.7	8.8	95	71	79	82	0.7	4.5	3.0	2.7	10 ●	10	10 ●	SW 8	SW 8	SW 7
15	101.7	102.3	104.6	102.9	9.8	13.7	12.3	12.0	14.0	9.8	95	74	94	88	0.6	4.1	0.9	1.9	10 ●	9 ⊙	3	SW 4	W 8	W 8
16	107.2	111.0	114.1	110.8	9.2	11.9	7.2	8.9	12.9	7.2	100	83	97	93	0.0	2.3	0.3	0.9	10 ●	8	0	SW 8	SW 6	WSW 3
17	114.4	114.3	114.4	114.4	4.2	11.6	11.2	9.6	12.4	3.8	100	83	83	89	0.0	2.3	2.3	1.5	10 ≡	4	0	SW 3	S 2	E 3
18	110.7	110.6	108.8	110.0	11.9	12.7	12.9	12.5	13.5	11.2	88	84	72	81	1.7	2.4	4.1	2.7	9	8	8	NW 8	NW 8	NW 10
19	106.4	105.3	105.3	105.7	11.0	11.2	10.6	10.8	12.9	10.4	69	77	79	75	4.0	3.1	2.8	3.3	9	10	10	NW 6	W 4	N 3
20	107.2	110.6	113.9	110.6	9.4	10.2	11.2	10.5	12.1	9.1	89	95	85	90	1.3	0.6	2.0	1.3	9 ●	10 ●	10	NW 5	WNW 4	NE 3
21	115.5	116.3	114.9	115.6	9.2	10.0	8.2	8.9	11.2	8.1	100	92	100	97	0.0	1.0	0.0	0.3	10	10 ●	5	C 0	W 2	WNW 1
22	110.4	108.1	106.0	108.2	8.3	10.4	10.5	9.9	10.9	8.0	99	97	100	99	0.2	0.3	0.0	0.2	10	10 ●	10	S 3	SSE 2	SE 1
23	98.0	95.9	96.9	96.9	14.6	15.8	12.3	13.8	16.3	10.5	100	95	88	94	0.0	0.9	1.7	0.9	9	10 ●	10	SW 3	SW 3	NW 5
24	100.5	101.2	101.8	101.2	11.6	10.8	8.2	9.7	12.3	7.9	69	47	75	64	4.2	6.9	2.7	4.6	9	2 ⊙	9 ●	NW 10	WNW 8	NW 17
25	108.8	113.7	116.3	112.9	8.6	9.6	8.6	8.8	10.2	7.7	89	73	72	78	1.3	3.3	3.2	2.6	4 ⊙	4 ⊙	7	NW 14	NW 12	NW 2
26	114.9	115.7	117.0	115.9	9.0	9.5	8.9	9.1	10.4	8.1	52	57	57	55	5.5	5.2	4.9	5.2	8	7 ⊙	0	NNW 5	NNW 5	NW 7
27	112.9	107.6	96.7	105.7	10.4	7.8	12.2	10.6	12.4	4.1	77	100	78	85	2.9	0.0	3.2	2.0	10 ●	10 ●	10	NW 14	SW 17	W 25
28	99.0	100.3	101.1	100.1	11.1	11.7	10.6	11.0	12.4	10.4	84	83	77	81	2.1	2.3	2.9	2.4	7	6 ⊙	2	NW 20	WNW 17	WNW 17
29	98.3	96.3	96.1	96.9	7.4	10.0	6.7	7.7	11.1	6.1	94	78	100	91	0.6	2.7	0.0	1.1	7	7	8	SW 3	SW 5	SW 2
30	99.6	106.2	112.0	105.9	8.1	9.1	6.8	7.7	10.1	5.4	83	77	94	85	1.8	2.7	0.6	1.7	10	9	10	NNW 4	NNE 8	NW 6
31																								
M	108.5	108.7	108.9	108.7	10.7	13.7	11.4	11.8	15.0	9.0	89	75	86	83	1.5	4.2	1.9	2.5	8.1	7.4	6.4	5.3	6.2	5.3

Październik – Octobre

1	112.5	115.0	118.7	115.4	5.3	7.6	7.4	6.9	8.6	4.7	86	71	63	73	1.3	3.0	3.8	2.7	10 ●	8	9	NE 6	W 2	N 3
2	121.3	121.8	118.3	120.5	3.2	9.4	6.8	6.6	10.2	3.2	100	58	84	81	0.0	5.0	1.6	2.2	8	4 ⊙	8	SW 3	W 4	SW 5
3	110.7	104.2	100.7	105.2	6.3	6.6	10.0	8.2	10.3	5.8	86	100	69	85	1.2	0.0	3.8	1.7	10 ●	10	6	SW 7	SW 10	W 10
4	105.0	110.4	115.6	110.3	7.8	8.2	9.4	8.7	10.3	7.3	61	61	66	63	4.1	4.3	4.0	4.1	5	6 ⊙	9	WNW 12	NW 14	NW 12
5	116.3	115.2	110.4	114.0	9.2	9.6	7.6	8.5	10.4	7.6	62	69	100	77	4.4	3.8	0.0	2.7	10	10	10 ●	WNW 14	SW 8	SW 8
6	113.2	117.9	119.1	116.7	10.3	10.2	11.2	10.7	11.6	7.6	100	93	89	94	0.0	0.8	1.5	0.8	9	10	9	NW 8	W 8	W 8
7	118.9	121.0	123.9	121.3	10.7	11.3	11.2	11.1	12.3	10.5	97	91	99	96	0.4	1.2	0.2	0.6	10	10	10	WNW 12	W 12	W 2
8	126.3	128.2	127.5	127.3	11.2	12.0	11.7	11.6	12.2	10.8	99	96	99	98	0.2	0.5	0.1	0.3	10	10	10	W 1	W 1	WSW 1
9	125.3	123.9	122.1	123.8	10.7	12.9	8.7	10.2	13.7	8.7	95	86	100	94	0.7	2.1	0.0	0.9	10	1 ⊙	0	W 1	N 2	C 0
10	119.6	117.9	117.5	118.3	7.1	18.1	11.8	12.2	18.6	6.5	100	63	90	84	0.0	7.7	1.3	3.0	0 ⊙	0 ⊙	0	C 0	SSW 3	SW 5
11	118.3	118.9	118.3	118.5	9.8	12.0	9.2	10.0	12.6	9.2	100	84	97	94	0.0	2.2	0.3	0.8	10	8 ⊙	8	W 1	SW 5	W 1
12	115.7	119.4	124.7	119.9	9.0	11.1	10.7	10.4	11.7	8.5	100	88	89	92	0.0	1.6	1.5	1.0	10 ●	0 ⊙	2	SW 2	NW 8	W 8
13	125.3	123.3	121.0	123.2	6.9	13.0	10.0	10.0	14.2	6.8	100	66	93	86	0.0	5.1	0.8	2.0	9	9	9	SW 3	SW 6	SW 3
14	119.9	122.5	124.8	122.4	10.2	10.2	9.8	10.0	11.1	8.8	100	73	84	86	0.0	3.3	1.9	1.7	10	7 ⊙	1	N 6	NW 6	W 8
15	126.4	127.3	127.1	126.9	9.8	9.5	7.8	8.7	10.2	7.8	65	71	82	73	4.2	3.4	2.0	3.2	9	10	10	NW 7	WNW 8	C 0
16	124.4	121.7	117.7	121.3	7.6	11.2	7.8	8.6	12.1	7.0	86	68	87	80	1.4	4.2	1.4	2.3	10	8 ⊙	0	SW 2	S 5	S 5
17	110.9	112.0	114.9	112.6	6.4	11.8	8.2	8.6	12.3	6.2	97	88	96	94	0.3	1.6	0.5	0.8	8	10	0	S 6	WSW 8	SW 6
18	107.6	103.4	103.9	105.0	8.6	14.5	11.4	11.5	15.4	6.8	89	84	98	90	1.3	2.7	0.4	1.5	10	10	10 ●	S 6	SW 5	W 7
19	101.6	102.9	105.1	103.2	13.6	16.1	10.4	12.6	16.7	10.3	86	72	92	83	2.2	5.1	1.0	2.8	7	9	10 ●	SW 5	SW 7	SW 5
20	108.3	111.1	113.4	110.9	9.7	10.6	6.5	8.3	11.5	6.2	93	88	97	93	0.8	1.5	0.3	0.9	9	8	0	W 4	SW 7	SW 4
21	112.4	109.4	106.4	109.4	4.6	9.4	9.6	8.3	10.7	4.2	95	74	87	85	0.4	3.1	1.6	1.7	0 ⊙	9	10	SW 6	SW 7	SW 6
22	101.7	100.1	101.1	101.0	7.2	11.3	8.6	8.9	11.4	7.1	91	70	94	85	0.9	4.1	0.6	1.9	10	9	10 ●	S 8	S 5	SSW 1
23	104.3	107.3	107.5	106.4	8.4	9.7	7.5	8.3	10.5	6.9	100	83	89	91	0.0	2.0	1.2	1.1	10 ● ≡	8	10	SSW 2	SW 8	SW 7
24	103.5	109.3	116.8	109.9	9.1	10.9	9.9	10.0	11.3	7.2	100	79	74	84	0.0	2.7	3.1	1.9	10 ●	0 ⊙	0	SW 10	W 10	W 17
25	120.9	123.2	121.7	121.9	8.9	9.4	7.7	8.4	9.9	7.7	79	80	90	83	2.4	2.4	1.0	1.9	2 ⊙	4 ⊙	10	W 8	W 8	SW 3
26	118.8	118.8	117.2	118.3	10.7	12.9	11.8	11.8	13.1	7.7	96	87	87	90	0.5	1.9	1.8	1.4	10	10	10	SW 5	SW 3	SW 5
27	114.9	114.4	114.3	114.5	8.6	11.7	10.4	10.3	12.0	8.6	93	78	83	85	0.8	2.9	2.1	1.9	10	10	10	SW 6	SW 8	WSW 4
28	113.8	113.4	113.1	113.4	7.6	12.2	10.7	10.3	12.2	7.2	97	80	89	89	0.3	2.9	1.5	1.6	8	9	8	SW 3	SW 5	SW 4
29	111.1	111.7	111.7	111.5	10.6	12.8	12.4	12.0	13.8	9.7	87	76	79	81	1.6	3.6	3.0	2.7	10	9	10	SW 8	SW 6	SW 8
30	108.7	109.1	110.8	109.5	9.3	11.6	11.8	11.1	12.6	9.3	91	94	100	95	1.1	0.8	0.0	0.6	8	10 ●	10 ●	SW 7	SW 6	SW 4
31	108.6	106.6	104.6	106.6	11.4	11.6	11.3	11.4	12.3	10.7	95	99	99	98	0.7	0.1	0.2	0.3	9	10 ●	10	SW 5	SW 7	SW 5
M	114.4	114.9	115.2	114.8	8.7	11.3	9.7	9.8	12.1	7.6	91	80	89	87	1.0	2.8	1.4	1.7	8.4	7.6	7.1	5.6	6.5	5.3

Ustka $H_s = 6\ m$ $H_b = 8{,}1\ m$ $h_w = 18\ m$ **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIE GU h	USŁONECZNIENIE	POGODA
1	8	0.0	.	-	•° 19²⁰–40 . = 0⁰⁰–9²⁰
2	7	8.2	.	-	•¹ 17¹⁵–42 , 19¹⁰–21²³ . (R)° 20¹⁹–40 WSW . = 18¹⁰–24
3	7	2.7	.	-	▽ 0⁵⁰–1³⁰ •¹ 2⁴⁰–3¹⁵ •° 6³⁵–12²⁵ . = 0⁰⁰–13²⁰ , 21³⁰–24
4	8	0.0	.	-	▽ 5³⁰–6²⁰ , 7⁰⁵–10 , 9⁴⁸–10³⁰ . = 0⁰⁰–7²⁰
5	7	0.0	.	-	•° 16¹⁵–40 , 17⁰⁶ , 19⁰⁵ , 21⁰⁰–22⁴⁰ . = 19⁰⁵–n
6	8	.	.	8.6	= n – 10³⁰ , 20⁰⁰–24 . ⊕ 5³⁰–9³⁰
7	7	.	.	7.6	= 0⁰⁰–13¹⁰ , 19³⁰–24
8	7	.	.	6.9	= 0⁰⁰–10⁰⁰ , 16⁴⁰–24
9	7	0.0	.	6.3	•° 15²⁰–16³⁵ . = 0⁰⁰–7²⁰ . ⌓° n–9⁰⁰ . ▽ 22⁰⁵–24
10	8	.	.	9.3	▽ 4³⁰–5⁰⁰ . ▽ 0⁰⁰–20
11	7	1.1	.	7.3	•° 19⁴⁰–24 . por. wiatru ponad 10 m/sek 21³⁰–24
12	7	15.5	.	-	•° 2²⁰–3³⁰ . ▽ 11⁵⁷–n , 15⁴⁰–16³⁵ , 17⁴⁵–19¹⁰ , 20⁴⁰–21²⁰ , por. wiatru ponad 10 m/sek 0⁰⁰–4³⁰ . = 0⁰⁰–a
13	7	4.4	.	5.9	▽ 15¹⁵–35
14	7	0.4	.	0.8	•° 0⁴⁰–3²⁰ , 7²⁰–9²⁰ , 18³⁰–19⁰⁰ , 21⁵³–23¹⁰ . = 0³⁵–10⁴⁰
15	7	13.3	.	1.5	•° 6⁵⁵–8¹⁵ •¹ 10⁴⁵–11⁰⁵ ▽ 11⁴⁵–12¹⁰ , 13⁰⁰–05 , 18⁴⁰–19⁰⁸ , 19⁴³–20⁰⁰ , 20⁵²–21³⁰ , 22²⁰–45 . = 0⁰⁰–10²⁰
16	7	19.1	.	0.8	▽ 1³⁵–55 , 2⁰⁵–3¹⁰ , 3⁴⁵–4²⁵ , 4³⁵–5³⁰ •¹ 5⁴⁰–6³⁰ •°–7⁴⁰ •¹–12³⁰ ▽ 15⁵²–16¹⁶ . = 18⁴⁰–24
17	6	0.5	.	4.8	= 0⁰⁰–7⁵⁰ = °–11³⁰ = –14³⁰ . ⌓² n – 10⁰⁰
18	7	.	.	2.1	▽ 5⁰³–⁰⁵ , 6⁵⁵–7⁰⁷ , 7²⁷–³¹ , ≫ 8³⁰… 24 . = 20⁴⁰–24
19	7	0.6	.	0.2	= 0⁰⁰–4³⁰
20	7	5.8	.	.	•° 1³⁰–4⁴⁰ ▽ 6⁵⁵–8²⁰ , 13³⁰–14⁰⁵ , 19¹⁵–21⁰⁷
21	6	1.0	.	.	•° 10³⁰–12³⁵ •¹–13¹⁰ •°–15⁰⁰ . = 0⁵⁰–a
22	6	12.9	.	.	•° 12⁰⁰–14⁴⁰ •¹–15⁴⁵ •°–17¹⁵ . = na – 22³⁰ ≡° – 23⁰⁰ = –24
23	6	0.3	.	.	•° 1²⁰–4⁰ •¹–3³⁰ •°–4⁴⁰ •¹ 5²⁰–6³⁰ •°–7⁴⁵ , 8⁴⁵–9¹⁰ , 13⁰⁶–16²⁰ . = 0⁰⁰–24
24	8	3.8	.	5.1	▽ 9⁵⁰ , 10²⁵ , 15⁴⁵–16⁰⁵ , 19³⁰ , 23³⁰ . ≫ 15⁴⁵–16⁰⁰ ≋ –24 . = 0⁰⁰–3⁴⁰
25	7	.	.	8.4	▽ 0¹⁰ , 2⁰⁰–3⁵⁰ . ≋ 0⁰⁰–14³⁰ ≫ – 15⁴⁵
26	8	0.4	.	6.0	
27	6	19.5	.	.	▽ 5⁴⁵–6²⁵ , 6³⁵–7⁰⁵ , 7³⁰–8¹⁰ , 8⁴⁵–9⁰⁵ , 10⁰⁰–20 •° 10⁴⁰ , 13⁴⁰ •¹–17²⁵ •²–17⁵⁰ •¹–21⁴⁰ •° 22⁴⁰–23¹⁵ . ≫ 4³⁰–8⁴⁰
28	7	0.0	.	4.7	▽ 19¹⁰–20 ≋ 0⁰⁰–8³⁰ . ≫ – 11³⁰ ≋ –24 . = 0⁰⁰–n **27.IX:** ≋ –9³⁰ ≫ 21²⁰ ≋ –24 . = 0⁰⁰–4³⁰ , 21⁴⁰–24
29	7	20.3	.	1.5	▽ 8⁰¹–45 , 9⁴⁰–11¹⁰ , 17³⁰–57 , 22²⁵–40 , 23²⁴–24 . ≋ 0⁰⁰–3⁴⁰ ≫ – 5⁴⁵
30	7	11.2	.	3.7	▽ 0⁰⁰–1⁰⁰ •¹ 1¹⁰–40 ▽ 3³⁰–4¹⁰ , 6²⁵–40 , 9³⁵–10²⁰ , 20⁴⁰–21¹⁵ , 21⁴⁰–22³⁸
31					
Σ	–	141.0	–	-	UWAGI

Październik – Octobre

1	8	4.1	.	2.5	▽ 1⁰⁰–3⁰⁰ •°–5⁰⁰ •¹–8¹⁰ ▽ 9⁴⁰–10¹⁰ , 15⁰⁵–15
2	7	0.0	.	6.5	▽ 1⁴⁵–2³⁰ , 3³⁰–4²⁵ , 5³³–46
3	6	1.4	.	.	•° 2⁴⁰ , 11³⁰ , 12⁰⁵–50 , 14³⁰–15⁰⁵ , 15³⁵–17¹⁵ , 18⁴⁵–19¹⁰ , 23¹⁰–30 , ≫ 13³⁰–24
4	8	0.2	.	5.8	≫ 0⁰⁰–24 , ▽ 20¹⁰–22³⁰
5	7	3.9	.	0.2	▽ 2⁵⁰–3³⁰ , 4²⁵–5⁴⁰ , 8¹⁰–40 •° 13³⁰ , 14⁰⁵ , 15⁰⁷ , 22⁴⁰ •¹–24 . ≫ 0⁰⁰–10³⁰
6	6	0.2	.	.	•¹ 0⁰⁰–2³⁰ , •°–6⁴⁵ , 13¹⁰–15²⁰ . ≫ n
7	6	.	.	1.1	•° 3⁰⁵–5¹⁵ ≫ 1³⁰–13³⁰ (por. do 18 m/sek) . = 1⁰⁰–8²⁰ , 12⁴⁰–24
8	5	0.0	.	.	•° 9³⁵–15²⁰ , 17²⁵–18²⁰ . = 0⁰⁰–24
9	6	0.0	.	6.3	= 0⁰⁰–24
10	6	0.0	.	7.7	= 0⁰⁰–24 . ⌓² n
11	5	0.5	.	1.0	•° 3⁵⁵–4⁴⁰ •¹–5¹⁵ . = 0⁰⁰–2⁵⁰ ≡° – 3⁵⁵ ≡¹ – 6³⁰ = –24
12	6	2.1	.	3.6	•° 6¹⁵–7³⁰ •¹–8⁰⁵ •° 9⁴⁰–10²⁰ •°–11¹⁰ . = 6⁰⁰–8¹⁵ ≡° – 11²⁰ = –13³⁰
13	7	.	.	4.3	= 1⁰⁰–7⁴⁰ , 18²⁰–24
14	7	.	.	4.5	= 0⁰⁰–12³⁰
15	7	.	.	.	
16	7	.	.	2.4	= 6¹⁰–9³⁰ , 13³⁵–24
17	6	0.5	.	.	•° 9⁰⁵–27 •¹–10²⁰ •°–12⁰⁵ . = 0⁰⁰–a , 21⁴⁰–24
18	6	1.0	.	.	•° 18²⁵–40 , 20⁴⁵–24 . = 0⁰⁰–24
19	7	0.1	.	0.1	•° 0⁰⁰–10 , 8¹⁰–9⁰⁰ , 18⁰⁵–21³⁵ . = 0⁰⁰–13²⁰ , 16⁴⁰–24
20	7	.	.	1.8	= 0⁰⁰–7⁴⁰ , 18¹⁵–24
21	6	0.1	.	1.6	•° 14¹⁰–15⁰⁷ , 21⁴⁵–22³⁰ , 23⁴⁰–24 . = 0⁰⁰–n/p
22	6	1.4	.	.	•° 0⁰⁰–2³⁰ , 16¹⁰–21¹⁵ , 22⁴⁰–24 . = 0⁰⁰–24
23	7	4.1	.	4.2	•° 0⁰⁰–05 , 5²⁰–6¹⁰ , 7⁰⁰ = 3¹⁰–6⁴⁰ ≡° – 7²⁰ = –10²⁰ , 17¹⁵–n
24	8	1.4	.	4.8	▽ 1¹⁰–2²⁰ •° 3⁰⁵–5²⁰ •¹–6²⁵ •°–8³⁰ •¹–8³⁷ . ≫ 8⁰⁰–20³⁰ (por. do 20 m/sek) ≋ –24 (por. do 22 m/sek) . = 0⁰⁰–9³⁰
25	8	0.8	.	3.5	•° 21⁴⁰–24 . ≋ 0⁰⁰–6³⁰ (por. do 22 m/sek) ≫ – 7³⁰ (por. do 16 m/sek) . = 19²⁰–24 . ⊕ 14²⁵–15³⁰
26	6	.	.	.	•° 0⁰⁰–1²⁰ . = 0⁰⁰–24
27	6	.	.	.	= 0⁰⁰–24
28	6	0.1	.	0.3	= 0⁰⁰–24
29	7	.	.	1.7	•° 2²⁰–4³⁰ . = 0⁰⁰–9⁴⁰ , 12⁴⁰– n
30	6	4.0	.	0.2	•° 11⁴⁰–13²⁰ , 15³⁰–17¹⁰ , 18³⁰–24 . = 0⁰⁰–24 . ⌒ 6⁴⁵–7⁰⁰
31	5	4.2	.	.	•° 0⁰⁰–3⁰⁵ , 4⁴⁰–6¹⁰ , 7⁴⁰–10⁴⁰ , 11²⁰–20⁴⁰ , 22⁴⁰–24 . = 0⁰⁰–22⁴⁰
Σ	–	29.1	–	64.1	UWAGI

Ustka $\varphi = 54°35'$ $\lambda = 16°52'$ **Listopad – Novembre 1957**

DNI	CIŚNIENIE P=900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	98.8	98.6	103.1	100.2	10.4	11.2	8.7	9.8	12.5	8.7	91	89	88	89	1.1	1.5	1.3	1.3	9	10	7	SW 5	SW 6	SW 6
2	106.2	107.6	110.6	108.1	5.5	11.4	6.3	7.4	11.6	5.2	89	66	88	81	1.0	4.6	1.1	2.2	1	4 ⊙	0	SW 5	SW 5	SW 5
3	113.1	113.4	111.9	112.8	2.8	11.6	6.2	6.7	11.9	2.8	96	67	85	83	0.3	4.5	1.5	2.1	0	3 ⊙	0	S 4	SSW 3	SSW 6
4	108.9	107.9	108.8	108.5	8.6	13.6	11.3	11.2	14.2	5.2	97	77	89	86	0.3	4.5	1.5	2.1	9	8	6	S 5	S 7	S 4
5	107.4	103.8	104.0	105.1	6.8	13.5	10.6	10.4	14.8	6.6	97	71	94	87	0.3	4.5	0.8	1.9	3	8	6	S 4	SSE 5	S 4
6	105.2	106.3	107.0	106.2	8.9	11.9	8.7	9.6	11.9	8.6	93	82	99	91	0.8	2.5	0.1	1.1	6	9	10	S 5	SE 4	S 1
7	102.9	102.2	105.4	103.5	7.5	12.0	9.1	9.4	12.3	5.9	100	82	96	93	0.0	2.5	0.5	1.0	10	10	10	SE 1	S 4	SW 5
8	107.7	108.4	109.2	108.4	8.1	9.3	9.7	9.2	10.1	8.1	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	SW 1	SW 3	N 4
9	107.9	107.9	109.0	108.3	8.6	10.0	9.9	9.6	10.1	8.5	100	89	96	95	0.0	1.3	0.5	0.6	10	10	10	E 4	E 5	E 3
10	110.5	112.0	116.1	112.9	9.7	11.6	10.2	10.4	12.5	9.7	96	83	93	91	0.4	2.3	0.8	1.2	10	9	10	SE 6	ESE 7	E 3
11	119.4	122.0	125.5	122.3	8.3	9.2	7.0	7.9	10.3	7.0	93	92	91	92	0.8	0.9	0.9	0.9	10	9	10	E 7	E 6	E 6
12	128.3	129.9	131.4	129.9	5.1	5.2	2.4	3.8	7.1	2.4	92	83	89	88	0.7	1.5	0.8	1.0	10	9	4	E 8	E 4	E 1
13	131.4	131.2	131.3	131.3	1.1	3.9	2.6	2.6	4.4	0.2	94	82	86	87	0.4	1.5	1.1	1.0	9	10	10	SSW 2	SW 2	SW 2
14	130.4	131.2	131.9	131.2	1.5	4.4	3.0	3.0	4.6	1.4	91	87	90	89	0.6	1.1	0.8	0.8	9	9	10	SSW 3	W 3	SW 2
15	131.7	131.0	130.8	131.2	0.4	0.3	-1.2	-0.4	3.0	-1.2	84	86	91	87	1.0	0.8	0.5	0.8	10	10	10	SSW 5	S 4	C 0
16	130.4	131.5	132.8	131.6	0.2	2.6	2.2	1.8	3.0	-1.7	96	93	96	95	0.3	0.6	0.3	0.4	10	10	10 ●	SSW 3	SW 3	S 2
17	133.5	133.8	134.7	134.0	2.0	4.7	0.6	2.0	5.1	0.5	93	87	90	90	0.6	1.1	0.6	0.8	10	10	0	S 1	S 1	SE 1
18	133.8	132.9	132.6	133.1	2.1	2.7	1.7	2.0	3.0	0.5	73	72	81	75	1.9	2.1	1.3	1.8	10	10	10	SE 3	S 2	SE 1
19	133.7	135.7	138.5	136.0	1.1	3.1	-0.8	0.6	3.4	-0.9	85	76	96	86	1.0	1.8	0.3	1.0	10	10	0	C 0	S 2	S 2
20	139.5	139.1	138.9	139.2	-2.8	4.6	-0.6	0.2	5.2	-2.8	97	62	91	83	0.1	3.3	0.5	1.3	0	5	5	S 1	SSE 2	S 1
21	137.1	134.7	129.0	133.6	-3.2	3.6	-1.0	-0.4	3.7	-3.2	99	70	87	85	0.0	2.4	0.8	1.1	2	0 ⊙	0	S 2	S 4	S 1
22	118.8	115.9	113.3	116.0	-2.1	0.8	0.8	0.1	1.1	-2.4	94	96	83	91	0.3	0.3	1.2	0.6	0	10	10	S 3	SW 5	SSW 6
23	111.2	111.1	116.8	113.0	0.6	1.4	5.1	3.0	6.0	0.0	96	98	76	90	0.3	0.2	2.1	0.9	10	10 ●	10	S 7	SW 6	WNW 8
24	116.0	115.2	114.3	115.2	5.2	6.8	7.5	6.8	7.7	4.1	98	97	94	96	0.1	0.3	0.6	0.3	10 ●	10 ●	10	W 7	WNW 10	W 14
25	112.6	113.8	116.5	114.3	7.6	8.0	7.8	7.8	8.2	7.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ●	10 ●	W 10	W 8	W 7
26	117.8	117.5	113.3	116.2	7.4	7.8	7.8	7.7	8.0	7.3	100	100	87	96	0.0	0.0	1.4	0.5	10 ●	10 ●	10	W 6	W 8	W 10
27	109.6	112.3	113.9	111.9	8.2	7.4	7.2	7.5	8.6	7.1	92	91	91	91	0.9	0.9	0.9	0.9	10 ●	8	10	W 12	WNW 10	W 6
28	107.6	105.3	103.1	105.3	7.6	7.6	7.7	7.6	8.5	6.8	100	97	89	95	0.0	0.3	1.2	0.5	10 ●	10 ●	9	W 9	W 14	NW 14
29	112.2	119.1	130.1	120.5	1.2	2.3	-1.1	0.3	8.0	-1.6	70	70	63	68	2.0	2.2	2.1	2.1	10	8	6	N 14	NE 14	E 8
30	133.1	133.3	132.6	133.0	0.5	-0.2	-2.6	-1.2	2.1	-2.8	76	96	100	91	1.5	0.2	0.0	0.6	7 ✱	7	8	N 10	E 2	ESE 2
31																								
M	118.6	118.8	119.9	119.1	4.3	6.7	4.9	5.2	7.8	3.2	93	84	90	89	0.6	1.7	0.8	1.0	7.8	8.5	7.4	5.1	5.3	4.5

Grudzień – Décembre

1	128.1	123.6	124.5	125.4	0.6	-0.1	4.8	2.5	5.3	-3.8	88	98	89	92	0.8	0.2	1.0	0.7	10 ✱	10 ✱	10	W 8	SW 6	NE 5
2	126.1	126.7	126.4	126.4	4.8	6.0	4.6	5.0	6.3	3.6	94	94	100	96	0.6	0.6	0.0	0.4	10 ●	6 ⊙	9	C 0	N 2	NW 2
3	122.9	123.1	123.8	123.3	5.1	4.4	4.8	4.8	5.7	3.9	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	N 4	NE 1	N 3
4	121.2	119.0	115.9	118.7	3.6	5.4	6.4	5.4	6.5	3.5	100	89	100	96	0.0	1.0	0.0	0.3	10 ●	10	10	W 5	W 4	W 8
5	115.5	117.6	123.1	118.7	6.4	7.0	5.8	6.2	7.3	5.3	91	82	79	84	0.9	1.7	2.0	1.5	1	1 ⊙	8	NW 10	NW 8	N 4
6	125.7	124.4	119.6	123.2	0.4	5.0	0.7	1.7	6.1	-0.3	92	73	98	88	0.5	2.3	0.1	1.0	6	1 ⊙	10	NE 4	SW 1	SW 5
7	110.2	107.3	99.9	105.8	1.2	2.5	1.5	1.7	2.6	0.7	85	95	92	91	1.1	0.4	0.5	0.7	10	10	10	SW 7	SW 8	S 8
8	84.1	73.7	67.3	75.0	1.2	3.2	7.0	4.6	7.8	0.7	90	100	80	90	0.7	0.0	2.0	0.9	10 ●	10 ●	8	SSW 8	SW 7	SW 10
9	73.0	83.3	91.2	82.5	2.2	0.6	-1.0	0.2	7.1	-1.0	89	82	99	90	0.8	1.1	0.1	0.7	10 ●	9	8	N 14	N 10	WNW 14
10	93.4	96.1	101.3	96.9	-1.4	-0.6	2.2	0.6	3.3	-2.6	88	64	61	71	0.6	2.1	2.8	1.8	10 ✱	10	4	NW 10	NW 10	WNW 10
11	104.8	106.1	104.3	105.1	-3.9	-2.2	-1.2	-2.1	2.5	-5.6	78	66	47	64	1.0	1.8	3.0	1.9	2	10	10	SW 8	SW 3	SE 5
12	100.4	98.9	98.1	99.1	0.3	0.2	-0.6	-0.2	0.5	-1.8	55	66	87	69	2.8	2.1	0.7	1.9	10	10	10	E 8	SE 7	E 5
13	95.4	92.5	88.4	92.1	-0.4	0.8	2.4	1.3	2.7	-1.1	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ≡	10	SE 4	E 3	E 8
14	89.4	96.3	107.5	97.7	2.2	2.3	1.5	1.9	2.7	1.1	89	79	61	76	0.8	1.5	2.6	1.6	10	10	9	NE 14	NE 14	NE 12
15	118.9	124.0	128.0	123.6	-2.1	1.0	-2.2	-1.4	1.9	-2.2	96	73	76	82	0.1	1.8	1.2	1.0	4	0 ⊙	0	ENE 5	SE 3	SE 3
16	129.1	129.7	128.8	129.2	-7.2	-3.2	-6.9	-6.0	-2.2	-7.6	88	66	80	78	0.4	1.6	0.7	0.9	0	4 ⊙	0	SE 2	S 3	S 1
17	124.7	122.7	122.3	123.2	-9.5	-3.1	-6.5	-6.4	-3.1	-9.5	82	53	78	71	0.5	2.3	0.8	1.2	0	5	4	S 4	S 4	S 1
18	123.2	123.2	122.9	123.1	-9.4	-6.2	-5.4	-6.6	-5.1	-10.6	88	94	85	89	0.4	0.2	0.6	0.4	0	6	10	S 1	SW 4	S 4
19	123.6	125.4	127.9	125.6	-3.4	-3.2	-2.5	-2.9	-2.2	-5.4	88	83	89	87	0.6	0.8	0.6	0.7	10	10	10	S 3	S 4	S 4
20	127.5	126.3	123.1	125.6	-0.5	2.4	1.8	1.4	2.9	-2.5	98	86	83	89	0.2	1.1	1.2	0.8	8	5 ⊙	0	SW 7	SW 7	SW 8
21	118.6	118.2	122.8	119.9	3.8	5.8	4.3	4.6	6.1	1.6	87	82	95	88	1.1	1.7	0.4	1.1	8	10	10	SW 8	SW 8	SW 5
22	122.1	121.9	121.7	121.9	2.8	3.6	3.2	3.2	4.6	2.5	93	100	100	98	0.6	0.0	0.0	0.2	10	10	10 ● ≡	SW 4	SW 5	SW 5
23	116.9	115.7	113.3	116.0	2.4	1.4	-1.4	0.2	3.7	-1.4	100	85	88	91	0.0	1.0	0.6	0.5	10	7	0	SW 2	S 4	S 6
24	112.4	113.8	115.8	114.0	0.1	1.0	0.5	0.5	1.7	-1.5	83	85	90	86	1.1	1.0	0.6	0.9	10	10	8	S 6	SSW 5	S 2
25	113.9	113.4	116.0	114.4	1.2	2.4	1.5	1.6	2.7	-1.6	77	66	94	79	1.5	2.5	0.4	1.5	10	10	10	S 7	SW 4	SW 2
26	117.4	119.6	121.5	119.5	2.6	4.4	3.9	3.7	4.9	1.3	95	100	98	98	0.4	0.0	0.2	0.2	10	10	10	WSW 6	W 7	SW 6
27	120.6	119.1	117.5	119.1	3.2	3.2	4.0	3.6	4.4	2.7	97	98	100	98	0.3	0.2	0.0	0.2	10	10	10 ● ≡	SW 8	SW 8	SW 8
28	110.8	107.0	104.3	107.4	5.4	5.2	4.2	4.8	6.0	3.7	84	90	95	90	1.4	0.8	0.4	0.9	10	10 ●	8	SW 10	SW 9	WSW 8
29	100.9	100.1	90.9	97.3	2.6	3.0	3.2	3.0	4.7	1.9	100	100	98	99	0.0	0.0	0.2	0.1	6	9	10 ●	W 10	W 6	SW 4
30	90.2	89.8	90.8	90.3	3.8	0.6	2.8	2.5	4.7	0.0	77	98	79	85	1.9	0.1	1.6	1.2	4	10	6	W 17	W 8	W 8
31	93.6	94.2	95.1	94.3	1.2	1.3	2.6	1.9	3.4	-0.1	96	98	77	90	0.3	0.1	1.7	0.7	9 ●	8	5	NW 10	W 8	WNW 8
M	111.5	111.4	111.4	111.4	0.6	1.7	1.5	1.3	3.4	-0.8	89	85	87	87	0.7	1.0	0.8	0.8	7.7	8.1	7.6	6.9	5.8	5.9

Ustka

$H_s = 6\ m$ $H_b = 8{,}1\ m$ $h_w = 18\ m$

Listopad – Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.2	.	.	•⁰0⁰⁰–7⁴⁰ 10⁵⁰ 14²⁰ ▽ 18¹¹–⁴⁴ . = 0⁰⁰–24
2	6		.	6.3	= 0⁰⁰–24
3	6	0.0	.	5.6	= 0⁰⁰–24
4	7	.	.	2.7	•⁰4⁴⁰–5²⁰ . = 0⁰⁰–12³⁰ 16³⁰–24
5	6	.	.	0.9	= 8⁰⁰–24 . ⌔ 1⁰⁰–3⁴⁰
6	6	.	.	.	= 0⁰⁰–24 . ⌔ 21³⁰–24
7	6	.	.	.	= 0⁰⁰–24
8	5	1.0	.	.	•⁰7¹²⁵–³⁰ 14⁴⁰–19⁴⁰ = 0⁰⁰–24
9	6	0.1	.	.	•⁰14⁴⁰–15⁰⁰ 17⁴²–18³⁰ = 0⁰⁰–24
10	6	.	.	.	•⁰0⁰⁰–3³⁰ = 0⁰⁰–15¹⁰ 18⁵⁰–24
11	7	.	.	0.6	= 0⁰⁰–12⁰⁰ 16³⁰–24
12	7	.	.	0.5	= 0⁰⁰–7²⁰ ⌐ –24
13	6	.	.	.	= 0⁰⁰–13²⁰ ⌐ –24
14	7	.	.	.	= 0⁰⁰–7⁴⁰ 15³⁵–24
15	6	.	.	.	= 0⁰⁰–24
16	6	0.0	.	.	•⁰15³⁰–⁵⁰ •¹–19⁴⁰ •⁰–21³⁰ . = 0⁰⁰–24
17	6	.	.	0.1	= 0⁰⁰–24
18	6	.	.	.	= 0⁰⁰–24
19	6	.	.	.	= 0⁰⁰–24
20	8	.	.	5.0	= 0⁰⁰–11²⁵ 15⁴⁰–24 . ⌴¹ 2⁴⁵–10³⁰
21	6	.	.	5.9	= 0⁰⁰–24 . ⌴¹ 3⁰⁰–10³⁰
22	5	0.0	.	1.1	= 0⁰⁰–24 . ⌴² ⌐
23	3	1.4	.	.	△ 3¹⁰–5¹⁵ •⁰9⁴⁵–10¹⁵ ✶⁰11⁴⁸–12²⁰ •⁰12⁴⁰–19³⁰ ▽⁰22¹⁵–²¹ . = 0⁰⁰–8¹⁰ ≡⁰–14²⁰ = – ⌐
24	6	0.6	.	.	•⁰6¹⁰–16⁴⁰ = 6³⁰–24 . ≫ 11⁰⁰–24 (por. do 18 m/sek)
25	6	1.4	.	.	•⁰1¹⁰–4²⁰ 12⁴⁰–24 . ≫ 0⁰⁰–7²⁰ (por. do 18 m/sek) . = 0⁰⁰–24
26	5	0.8	.	.	•¹0⁰⁰–5⁴⁰ •⁰ 15⁴⁵ ≫ 21³⁰–24 . = 0⁰⁰–24
27	7	8.2	.	.	•⁰5²⁰–7⁰⁵ 21⁴⁰–24 . ≫ 0⁰⁰–13⁰⁰ . = 0⁰⁰–7⁵⁰
28	6	2.0	.	.	•¹0⁰⁰–3⁰⁰ •⁰–3⁴⁰ •¹4⁴⁰–6¹⁰ •⁰–10⁴⁵ •¹12³⁰–13³⁰ •⁰16¹⁰–17¹⁰ 21⁰⁵–22²⁰ ≫ 3⁰⁰ 8¹⁰–24
29	7	3.4	.	0.1	▽ 7⁰⁵–³⁰ ✶⁰–8²⁵ ▽ 8⁴⁷–9¹⁸ 10¹⁴–11⁰⁵ 11⁴⁶–12¹⁵ 13²²–15²⁰ ▽ 15⁴⁸–16⁴⁰ ▽ 17¹⁰–⁴⁵ 18⁴²–19⁵⁷ ≫ 8⁰⁰–9³⁰ ≫ – ≡ –17³⁰
30	7	1.0	2	0.8	▽ 0¹⁵–⁵⁰ △ 1⁰⁵–2³⁰ ▽ 3⁵⁰–4¹⁵ 6²⁵–7⁰⁰ 13⁰⁵ 14³⁰ 15⁴⁰–16⁰⁷ 16⁵⁷–17⁰³ 18⁵⁰–19¹⁵ ≫ 22⁰–11⁰⁰ (por. do 16 m/sek) = 0⁰⁰–4²⁰ 20³⁰–24
31					29.XI: ≫ – 10⁵⁷
Σ	–	20.1	–	29.6	UWAGI

Grudzień – Décembre

1	4	5.5	2	.	▽ 6⁴⁰–7³⁰ ✶¹–9⁵⁰ ✶²–10³⁰ ✶¹–12⁴⁵ ✶⁰–13⁴⁰ •⁰14⁴⁵–20²⁰ . = 0⁰⁰–4³⁰ ⌐ –24
2	7	0.2	.	0.6	•⁰1⁴⁰ 2¹⁰ 6⁴⁰–7⁴⁵ •⁰9³⁰–10²⁵ . = 0⁰⁰–11³⁰ 18⁵⁰–24
3	5	0.2	.	.	•⁰8⁰²–12²⁵ . = 0⁰⁰–24
4	6	0.4	.	.	•⁰3⁴⁰–7³⁰ •⁰13³⁰–16⁴⁰ 18⁴⁰–19⁰⁵ •⁰22³⁰–24 . = 0⁰⁰– ⌐
5	8	.	.	5.0	•⁰0⁰⁰–25 . = 0⁰⁰–25
6	7	0.0	.	5.5	•⁰23²⁵–24 . = 6⁴⁰–12¹⁵ 15⁴⁰–24
7	5	0.1	.	.	•⁰0⁰⁰–¹⁰ 9⁰⁵–12³⁰ 15¹⁰–18⁰⁰ = 0⁰⁰–14⁴⁵ ≡¹–18¹⁰ = –24
8	6	10.3	.	.	•⁰0³⁵–2⁰⁰ 3⁴⁰–13⁵⁰ •¹–14⁰⁰ . •⁰–18¹⁰ . = 0⁰⁰– ⌐ . ≫ 18³⁰–24 (por. do 16 m/sek)
9	7	0.2	.	0.4	▽⁰0³⁰–4⁴⁰ 5⁴⁰–6⁰⁵ •⁰6²⁰–⁴⁰ •¹–6⁵⁰ •⁰–7²⁰ ✶⁰–10⁴⁰ ✶²21⁰⁵–²⁰ . ≫ 0⁰⁰–24 (por. do 20 m/sek)
10	7	0.8	1	0.3	✶13¹⁵–⁴⁵ ✶⁰6²⁰–⁴⁰ 7¹⁰–8²⁵ 11⁵⁰–12²⁰ ▽⁰13⁴⁰–14¹⁰ 14³⁵–⁴⁷ 15⁰⁵–²⁰ 16⁵⁰–17¹² ≫ 0⁰⁰–7³⁰ 12³⁰–24
11	7	.	1	0.5	≫ 0⁰⁰ 5²⁰ ⊕ 10²⁰–14¹⁰
12	7	.	1	.	= 17²⁰–24
13	3	0.0	1	.	≫ 2⁴⁵–24 . = 0⁰⁰–7³⁰ ≡⁰–15²⁰ = –24
14	7	1.3	.	.	•⁰0³⁰–5⁴⁰ •⁰7³⁰–8²⁰ ✶⁰–9⁵⁰ △ –10¹⁰ △ –12²⁰ . ≫ – ≡ 7³⁰–21³⁰ (por. do 22 m/sek) ≫ –24 . = 0⁰⁰–12³⁰
15	7	0.5	1	3.2	▽ 4⁴⁵–5¹⁰ ▽ 5³⁰–6²⁵ 8²⁰–⁴⁰ ▽ –9⁴⁰
16	7	.	1	6.0	= 10⁰–8²⁰ ⌣ 3⁴⁰–7⁴⁰
17	6	.	1	5.5	= 0⁰⁰–24
18	6	.	1	.	= 0⁰⁰–24
19	5	.	1	.	= 0⁰⁰–24
20	6	0.0	1	1.8	= 0⁰⁰–24
21	6	0.0	.	.	•⁰1²⁰–3⁰⁵ 14³⁰–15²⁰ ≫ 1⁰⁰–12³⁰ = 0⁰⁰–24
22	5	0.0	.	.	•⁰9⁴⁰–10³⁰ 13⁴⁰–15¹⁰ •¹ 24 = 0⁰⁰–9⁴⁵ ≡⁰–10²⁵ = – 15³⁰ ≡⁰–24
23	6	.	.	.	•⁰0⁰⁰–4⁰⁰ 5³⁰ 6²⁰ . ≡⁰0⁰⁰–10⁰ ≡¹–5¹⁵ ≡⁰–6⁴⁰ = –24 . ⊕ 9³⁰–12⁴⁰
24	6	.	.	.	= 0⁰⁰–24
25	6	0.0	.	.	•⁰14¹⁰–⁵⁰ = 0⁰⁰–24
26	6	0.0	.	.	•⁰8¹⁵–9⁰⁵ •¹–12³⁰ •⁰14⁴⁰–16¹⁰ . = 0⁰⁰–9³⁰ ≡⁰–12⁴⁵ = –24
27	6	0.0	.	.	•⁰8³⁰–9¹⁵ 15⁰⁵–18²⁰ •²–21³⁰ •⁰–24 = 0⁰⁰–20⁴⁰ ≡⁰–24 ≫ 22⁰⁰–24
28	6	0.4	.	.	•⁰0⁰⁰–1¹⁰ 9³⁶–10²⁰ 12³⁵–14⁵⁵ 17²⁰–24 . ≫ 0⁰⁰–9³⁰ 12⁰⁰–16³⁰ ≡⁰0⁰⁰–2⁴⁰ = –24
29	6	8.0	.	.	▽ 5²⁰–³⁵ 6²⁰–⁵⁵ 10¹⁰–⁴⁰ 12¹⁰–⁴⁵ •⁰19¹⁰–24 . ≫ 1⁰⁰–8⁰⁰ (por. do 20 m/sek) 23⁰⁰–24 = 0⁰⁰–5²⁰ 14²⁰–24
30	6	16.4	.	.	•⁰0⁰⁰ 3³⁰ ▽ 9²⁵–⁴⁰ ▽ 9⁵⁰–10⁰⁵ ▽ –10¹⁵ ▽ –13⁰² •△ 14⁴⁰–15²⁰ ▽ 16³⁰–⁵⁰ ▽ 17⁰⁵–³⁰ ▽ 18⁰⁵–³⁵ ▽ 23⁴³–⁵¹ ▽ –24
31	7	6.7	1	0.4	▽ 0⁰⁰ 2⁵ ▽ 6¹⁰–¹³ ▽ 7⁴³–8⁰⁵ 9³⁰–11⁰ 11¹⁴–²⁰ ▽ –12⁴⁰ 13⁴⁵–14²⁵ 15⁴⁸–16²⁰ 17³⁰–⁴⁰ ▽ 18¹⁰–⁴⁵ 19⁴²–20¹⁵ 21²⁹–⁴⁰ . ≫ 11⁵ –20³⁰
Σ	–	51.0	–	29.2	UWAGI 30.XII: ≫ 1⁰⁰–3³⁰ ≡ –7²⁰ ≫ –13⁰⁰ . = 0⁰⁰–3³⁰

Gdańsk-Wrzeszcz — φ = 54°23' — λ = 18°36' — Styczeń – Janvier 1957

Dni	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	116.8	116.9	116.9	116.9	-6.4	-5.6	-5.4	-5.7	-3.5	-7.2	89	92	92	91	0.4	0.3	0.3	0.3	10	10	10	C 0	C 0	C 0
2	114.7	113.0	112.6	113.4	-4.4	-1.8	-1.4	-2.2	-1.1	-6.0	91	90	94	92	0.4	0.5	0.3	0.4	10	10	10	SSW 1	C 0	C 0
3	117.7	119.5	120.3	119.2	0.3	1.0	0.6	0.6	1.5	-1.6	94	87	96	92	0.3	0.9	0.3	0.5	10	10	10	SW 2	C 0	S 1
4	121.1	121.1	121.0	121.1	-0.1	0.0	0.2	0.1	1.0	-1.3	100	96	92	96	0.0	0.2	0.5	0.2	10 ≡	10	9	S 3	S 2	S 4
5	117.0	109.8	107.9	111.6	1.0	3.7	7.2	4.8	8.3	-0.5	96	93	87	92	0.3	0.6	1.4	0.8	10	10 ●	10	SSW 4	S 7	W 2
6	101.6	101.5	102.3	101.8	9.7	7.6	5.8	7.3	10.8	5.4	95	71	64	77	0.6	3.1	3.3	2.3	10 ●	5	9	WSW 8	WNW 17	WNW 17
7	110.3	116.2	121.4	116.0	3.5	5.0	4.2	4.2	7.9	2.9	78	72	84	78	1.7	2.4	1.3	1.8	0	1	7	NW 14	NW 10	NW 8
8	120.2	117.8	115.6	117.9	5.0	6.8	8.0	7.0	8.2	3.5	92	88	90	90	0.7	1.2	1.0	1.0	10 ●	10 ●	9	W 6	W 8	WNW 17
9	114.0	112.6	109.7	112.1	9.2	8.9	8.3	8.7	9.8	7.4	80	76	83	80	2.3	2.8	1.9	2.3	9	10	10 ●	W 9	W 12	WSW 8
10	106.3	104.7	103.8	105.6	4.8	4.8	2.8	3.8	8.7	1.9	75	71	82	76	2.2	2.5	1.3	2.0	7	8	6	W 8	WNW 10	WNW 8
11	110.6	114.4	115.0	113.3	1.4	3.0	1.2	1.7	3.8	0.2	78	69	81	76	1.6	2.4	1.3	1.8	9	6	5	NNW 6	NW 6	NW 6
12	110.6	101.6	98.7	103.6	0.2	2.2	2.1	1.6	2.6	-0.5	96	89	93	93	0.3	0.8	0.5	0.5	10 ✳	10 ●	10	W 8	SW 7	WSW 5
13	101.3	107.7	116.3	108.4	0.4	0.0	-3.6	-1.7	2.6	-4.2	98	94	92	95	0.1	0.4	0.4	0.3	10	10 ✳	10	C 0	NE 6	NE 7
14	123.4	128.1	131.6	127.7	-5.4	-4.9	-6.4	-5.6	-2.3	-7.2	80	73	83	79	0.8	1.1	0.6	0.8	7	3	1	ENE 6	E 8	SE 4
15	131.2	129.8	128.8	129.9	-8.0	-6.1	-8.0	-7.5	-5.0	-9.3	90	73	81	81	0.3	1.0	0.6	0.6	10	10	10	SSE 1	ENE 2	S 2
16	129.0	129.4	129.9	129.4	-6.7	-3.2	-2.2	-3.6	-1.8	-10.8	88	88	89	88	0.4	0.6	0.6	0.5	10 ✳	9 ✳	10	C 0	SW 3	W 2
17	128.3	129.1	128.3	128.6	1.0	2.3	-0.1	0.8	2.6	-2.6	92	84	90	89	0.5	1.2	0.7	0.8	9	3	3	N 4	NW 4	W 6
18	126.3	125.1	123.7	125.0	-1.2	0.2	0.8	0.2	1.2	-1.7	94	82	86	87	0.4	1.1	0.9	0.8	3	0	10	WNW 8	NW 4	NW 5
19	125.0	126.6	126.7	126.1	0.3	0.3	0.3	0.3	1.7	-1.7	82	92	92	89	1.1	0.5	0.5	0.7	9	10	10	NNW 5	NNW 4	W 5
20	124.2	122.4	117.8	121.5	1.9	1.8	1.2	1.5	2.8	-0.1	80	85	81	82	1.4	1.1	1.3	1.3	9	10	8	WNW 6	W 7	W 10
21	114.3	115.3	117.1	115.6	-1.3	0.9	0.8	0.3	2.0	-1.8	86	87	92	88	0.8	0.9	0.5	0.7	7	9	10	SW 3	SW 2	SW 1
22	117.4	116.4	114.6	116.1	1.6	1.2	-2.0	-0.3	2.4	-2.8	91	61	75	76	0.7	2.6	1.4	1.6	10	0	0	SW 8	SW 5	C 0
23	113.9	114.5	116.6	115.0	-3.2	2.6	1.0	0.4	4.1	-4.7	83	72	92	82	0.8	2.1	0.5	1.1	0	6	7	SW 1	WSW 7	C 0
24	115.6	113.7	110.2	113.2	-5.2	-2.0	-2.4	-3.0	1.5	-5.9	90	89	87	89	0.4	0.6	0.7	0.6	3	9	10	S 4	C 0	SE 3
25	106.7	108.6	109.8	107.7	-2.7	-1.1	-2.4	-2.2	-0.4	-3.4	95	93	93	94	0.2	0.4	0.3	0.3	10 ✳	10 ✳	10	S 2	C 0	C 0
26	114.6	116.1	112.1	114.3	1.8	2.7	0.2	1.2	3.8	-3.2	91	86	88	88	0.7	1.0	0.7	0.8	10	9	9	W 5	SW 3	S 5
27	106.0	107.5	111.6	108.4	2.6	5.4	3.9	4.0	5.7	0.2	93	81	72	82	0.6	1.7	2.3	1.5	10	7	3	W 8	W 8	W 10
28	114.3	119.2	125.3	119.6	1.4	4.0	2.5	2.6	4.6	0.6	87	80	88	85	0.9	1.6	0.9	1.1	5	9	6	WSW 4	NW 6	W 5
29	125.8	124.9	123.1	124.6	1.6	3.7	3.3	3.0	4.0	0.7	85	82	88	85	1.1	1.5	0.9	1.2	10	9	10	SW 3	SSW 3	WSW 6
30	120.5	118.6	118.3	119.1	1.6	4.3	0.9	1.9	4.7	-0.3	87	74	96	86	0.9	2.2	0.2	1.1	3	10	10	WSW 2	C 0	C 0
31	118.9	120.0	120.5	119.8	-1.2	0.0	1.4	0.4	2.2	-1.6	100	96	96	97	0.0	0.2	0.3	0.2	0	10 ≡	6	C 0	S 1	C 0
M	116.7	116.8	117.1	116.9	0.1	1.5	0.7	0.8	3.0	-1.8	89	83	87	86	0.7	1.3	0.9	1.0	7.8	7.8	8.0	4.5	4.9	4.7

Luty – Février

Dni	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	115.5	112.9	110.5	113.0	1.2	2.2	4.7	3.2	5.2	0.1	98	100	95	98	0.2	0.0	0.4	0.2	10	10	10 ●	SSE 2	S 6	S 5
2	112.9	118.5	122.1	117.8	7.8	7.2	4.4	6.0	10.6	3.8	64	65	80	70	3.8	3.6	1.7	3.0	6	4	0	WNW 9	WNW 9	W 9
3	122.8	123.7	125.8	124.1	3.4	5.3	1.0	2.7	7.3	-1.7	85	75	94	84	1.3	2.2	0.4	1.3	10	5	9	C 0	SSW 4	C 0
4	124.4	119.9	118.4	120.9	-0.9	2.2	3.6	2.1	3.8	-1.9	100	93	97	97	0.0	0.6	0.3	0.3	10 ≡	10 ●	10	S 2	S 4	C 0
5	117.7	116.6	114.9	116.4	4.4	7.0	6.8	6.2	8.6	3.1	93	80	82	85	0.6	2.0	1.8	1.5	5	9	8	SW 3	SW 3	S 2
6	111.6	108.7	106.7	109.1	3.2	7.7	6.6	6.0	9.6	1.0	93	75	82	83	0.5	2.6	1.7	1.6	5	4	10	SSW 3	S 5	SW 2
7	109.1	107.6	108.9	108.5	5.0	8.2	3.4	6.0	8.7	4.5	81	57	75	71	1.6	4.7	2.3	2.9	10	7	4	W 8	W 10	WNW 10
8	109.3	104.6	97.7	103.9	4.2	5.9	6.0	5.5	8.4	3.0	84	82	91	86	1.3	1.7	0.9	1.3	10	10	10 ●	W 3	S 4	S 3
9	94.9	94.3	96.3	95.2	7.6	8.0	5.9	6.8	9.1	5.4	87	89	80	85	1.3	1.2	1.9	1.5	10	10 ●	7	SW 5	WSW 6	WSW 9
10	100.1	102.8	104.7	102.5	3.2	5.3	2.8	3.5	6.6	2.2	93	83	82	86	0.5	1.5	1.3	1.1	10 ●	8	10	NW 6	WNW 7	W 3
11	104.1	106.2	108.5	106.3	1.8	3.1	2.3	2.4	4.1	0.3	96	86	87	90	0.3	1.0	0.9	0.7	10	9	10	C 0	WNW 6	WNW 5
12	110.0	107.4	102.0	106.5	0.6	3.0	3.8	2.8	4.3	-0.3	88	76	90	85	0.8	1.9	0.8	1.2	9	9	10	WSW 3	SSE 3	S 5
13	98.1	94.7	88.1	93.6	4.2	5.8	3.7	4.4	8.8	3.2	88	82	88	86	0.9	1.7	1.0	1.2	9	9	10	SSW 5	S 5	S 3
14	81.3	83.6	84.4	83.2	5.3	8.2	6.4	6.6	9.4	3.2	97	81	87	88	0.3	2.1	1.3	1.2	10 ●	9	9	S 4	SW 4	S 2
15	84.4	85.8	84.7	85.0	3.2	6.5	3.9	4.4	8.1	2.6	91	71	88	83	0.7	2.9	1.0	1.5	10	6	10 ●	S 2	SW 5	S 2
16	84.9	90.5	95.1	90.2	3.6	4.4	3.6	3.8	5.9	2.9	93	82	76	84	0.5	1.5	1.9	1.3	8 ●	9	9	NW 5	WNW 7	SW 5
17	100.0	102.6	103.6	102.1	1.2	5.0	1.1	2.1	5.9	0.5	87	67	89	81	0.9	2.8	0.7	1.5	7	5	10	SW 5	SW 5	SW 1
18	103.0	104.5	100.9	103.5	0.0	2.8	3.4	2.4	4.9	-0.3	100	79	86	88	0.0	1.6	1.1	0.9	10	9	10	C 0	S 4	C 0
19	96.5	101.4	106.6	101.5	2.1	3.2	1.6	2.1	3.9	1.4	96	76	81	84	0.3	1.9	1.3	1.2	10 ●	9	10	N 8	NW 10	NW 4
20	109.0	109.6	108.3	109.0	0.8	2.9	1.2	1.5	3.8	0.5	86	83	96	88	0.9	1.3	0.3	0.8	7	9	10 ✳	SW 4	SSW 3	SSE 2
21	105.9	106.0	108.3	106.7	0.4	5.0	4.4	3.6	7.1	0.1	100	83	82	88	0.0	1.5	1.5	1.0	10	10	9	C 0	SSW 2	W 3
22	112.7	113.3	112.8	112.9	0.6	0.8	0.8	0.8	4.7	-0.1	84	96	94	91	1.0	0.3	0.4	0.6	6	9 ✳	8	NW 4	NW 2	C 0
23	111.8	111.4	110.7	111.3	-1.2	1.7	0.4	0.3	2.4	-2.1	96	80	92	89	0.2	1.4	0.5	0.7	7	9	10 ✳	C 0	W 3	W 2
24	107.0	104.9	105.0	105.6	-1.4	0.0	-1.5	-1.1	1.8	-2.5	97	86	86	90	0.2	0.9	0.8	0.6	10 ✳	10	9	C 0	C 0	C 0
25	107.8	108.4	109.1	108.4	-4.9	0.8	-0.2	-1.1	1.8	-6.6	81	77	80	79	0.8	1.5	1.2	1.2	1	4	10	C 0	C 0	ENE 3
26	113.7	116.7	120.0	116.8	0.4	1.6	0.6	0.8	3.2	-1.0	87	80	92	86	0.8	1.4	0.5	0.9	10	10	10	NE 1	C 0	C 0
27	122.0	123.9	125.9	123.9	-0.3	1.0	-0.3	0.0	1.7	-0.6	88	59	74	74	0.8	2.8	1.6	1.7	10	9	10	C 0	S 3	C 0
28	129.5	131.9	134.5	132.0	-1.6	0.4	0.8	0.1	1.2	-2.6	94	81	85	87	0.3	1.2	1.0	0.8	10 ✳	10	9	C 0	NNE 4	NE 7
29																								
30																								
31																								
M	107.2	107.6	107.7	107.5	1.9	4.1	3.0	3.0	5.7	0.6	90	79	86	85	0.7	1.8	1.1	1.2	8.6	8.2	9.0	2.9	4.4	3.2

Gdańsk – Wrzeszcz $H_s = 13$ m $H_b = 12{,}4$ m $h_w = 11$ m **Styczeń – Janvier 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	3	–	= 0⁰⁰–24
2	5	0.0	2	–	•° 18³⁵–20⁰⁰ . = 0⁰⁰–24
3	5	.	1	–	= 0⁰⁰–30 7¹⁵–24
4	4	.	1	–	= 0⁰⁰–3³⁰ ≡° –4¹⁰ ≡¹–6³⁵ ≡° –7⁰⁵ = –24
5	6	0.5	1	–	•° 10¹⁵ .. 18⁵⁰ . = 0⁰⁰–19¹⁰
6	7	2.2	.	–	•° 3²⁵–6⁴⁰ •° –9³⁵ ⩓ 8⁴⁰–11⁵⁰ (por. 15 m/sek) ⩓ –24 (por. 23 m/sek)
7	7	0.0	.	–	•° 1¹⁵–2³⁰ ⩓ 0⁰⁰–8²⁰ (por. 25 m/sek) ⩓ –13³⁰ (por. 15 m/sek)
8	6	0.0	.	–	•° 6³⁰–8¹⁰ 9²⁰–18³⁰ ⩓ 14³⁰–17⁴⁵ (por. 18 m/sek) ⩓ –21⁴⁰ (por. 26 m/sek) ⩓ –22⁴⁰ (por. 18 m/sek); = 7¹⁰–18³⁰
9	7	0.7	.	–	•¹ 2³⁰–3⁴⁰ •° 20¹⁰–24 ⩓ 8²⁵–15⁴⁰ (por. 17 m/sek); = 14³⁰–17²⁰
10	8	0.6	.	–	•° 0⁰⁰–20 ▽° 12¹⁵–35 ▽¹ 13¹⁰–35 ▽° 14⁴⁵–15⁰⁵, 16⁴⁰–17⁰⁵ ▽¹ 17¹⁵–40; ⩓ 11³⁰–18³⁰ (por. 15 m/sek)
11	8	0.0	.	–	
12	7	0.7	.	–	*° 6³⁵–10²⁰ •° 12¹⁰–15⁴⁰ •° –20³⁰
13	6	0.4	.	–	*° 5³⁵–6⁵⁰, 8²⁰–18²⁵; = 3³⁰–5²⁰, 7¹⁵–8¹²
14	7	.	1	–	
15	8	0.0	1	–	= 7³⁰–10²⁰
16	6	0.3	1	–	*° 5³⁵–10³⁵, 11⁴⁰–13⁰⁷ ⁂ 14⁴⁰–15¹⁰; = 10³⁵–13²⁰
17	7	.	2	–	⊠° 23²⁰–24
18	7	.	1	–	= 14²⁰–20³⁵; ⊠° 0⁰⁰–3¹⁰
19	7	0.0	.	–	= 15³⁵–24
20	7	.	.	–	•° 0²⁵–3²⁵ ⩓ 18³⁰–20⁰⁰; = 0⁰⁰–3⁴⁰
21	6	.	.	–	= 2³⁵–24
22	6	.	.	–	= 0⁰⁰–18²⁵
23	6	.	.	–	= 6¹⁰–24
24	5	0.5	.	–	= 0⁰⁰–24 ⌴¹ n – 6³⁰
25	4	1.5	1	–	*° 4⁴⁵–8⁵⁰ *¹–11³⁰ *° –15³⁰, = 0⁰⁰–4⁴⁵, 15³⁰–24
26	6	1.0	4	–	= 0⁰⁰–7⁴⁰ 10²⁰–24
27	7	0.0	pł.	–	•° 0³⁵–1¹⁵ •° .. 4²⁵ •¹–5⁴⁰ •° 12⁰⁵–40; = 0⁰⁰–2³⁰, 7²⁰–12⁰⁵
28	7	.	.	–	= 7³⁰–12³⁰
29	6	.	.	–	= 7³⁰–22⁴⁰; ⌴¹ n – 10⁰⁰
30	6	.	.	–	= 6²⁰–24
31	3	0.0	.	–	*° 15³⁰–16²⁰ •° –18²⁰; = 0⁰⁰–7²⁵ ≡° –7⁵⁰ = –10³⁰ ≡¹–11⁴⁰ ≡° –14⁵⁰ ≡¹–18⁴⁰ = –24
Σ	–	8.4	–		UWAGI.

Luty – Février

1	4	3.6	.	–	•° 2⁴⁰–4²⁰ •° 15⁴⁰ 17¹⁰–22²⁰, 23²⁰–24; = 0⁰⁰–22³⁰ ⌴° n – a
2	6	.	.	–	•° 0⁰⁰ .. 12⁵ = 0⁰⁰–3³⁰
3	7	.	.	–	= 8³⁰–11¹⁰ 22¹⁵–24 ⌴° n – 9⁰⁰
4	6	1.8	.	–	•° 11⁴⁵–16³⁵ 17²⁰–20³⁰ . = 0⁰⁰–2¹⁵ ≡¹–5⁴⁵ ≡° –7²⁵ ≡¹–8⁰⁵ = –24
5	6	.	.	–	= 0⁰⁰–24
6	6	.	.	–	= 0⁰⁰–7³⁰ ≡° –8³⁵ = –24
7	7	.	.	–	⩓ 11⁴⁰–22⁴⁰ (por. 19 m/sek); = 0⁰⁰–2⁴⁰
8	6	3.0	.	–	•° 11³⁰–12³⁰ 16¹⁵–24 = 8¹⁵–21²⁰
9	7	4.5	.	–	•° 0⁰⁰–1⁴⁰ 3²⁵–5¹⁰ 8³⁵ 9⁴⁰ ▽° 12¹⁵–50 •° 13¹⁰ 15²⁰ ▽¹ 17⁵⁰–18¹⁵, 18⁴⁵–19¹⁰, 19³⁵–20⁴⁰ ▽¹ 22³⁰–24; ⩓ 22⁴⁰–24
10	7	1.4	.	–	▽¹ 0⁰⁰–10 0³⁵–1¹⁰ •° –9⁰⁵ ⩓ 10⁰⁰–13⁰ ⊠° 19³⁰–23²⁰ 9.II: = 6²⁰–11³⁰
11	7	2.3	.	–	•° 8⁴⁰–45 *° –11³⁰ •° 16²⁵–17¹⁰ ▽° 18⁴⁰–19¹⁵; = 5²⁵–7⁴⁵ ≡° –8⁴⁰
12	7	1.4	.	–	•° 16²⁰–20⁴⁰, 23³⁰–24; = 13⁴⁰–15³⁰
13	6	2.7	.	–	•° 0⁰⁰–4³⁰ 22³⁰–24; = 6³⁰–24 ⌣ n – n
14	7	0.7	.	–	•° 0⁰⁰–8¹⁵ ▽° 14²⁵–45; = 0⁰⁰–8¹⁵ 17¹⁵–19³⁰
15	7	2.0	.	–	▽° 0²⁰–12⁵ •° 19²⁰–24; = 5³⁰–11³⁰ 16²⁰–24
16	7	2.7	.	–	•° 0⁰⁰–9¹⁰ 10²⁵ 11⁵⁰; = 0⁰⁰–7³⁰, 17⁵⁰–21²⁵
17	7	0.0	.	–	*° 23²⁵–24; = 16³⁵–19²⁰
18	7	4.3	.	–	*° 0⁰⁰ .. 15 •° 22¹⁰–24; = 3²⁰–11⁴⁰ 16³⁵–24
19	7	1.6	.	–	•° 0⁰⁰–3³⁰ •¹–9³⁰ •° –11³⁰ ⩓ 12¹⁰–14¹² (por. 15 m/sek); = 0⁰⁰–12²⁰, 18²⁵–24
20	6	1.1	.	–	▽° 20¹⁵–22³⁰ *° –24; = 0⁰⁰–1³⁰ 5²⁰–24
21	6	0.0	.	–	*° 0⁰⁰–1¹⁰ = 0⁰⁰–14³⁰ 16⁴⁰–21³⁰ ⊕° 8³⁰–9²⁵
22	6	0.0	.	–	*° 1⁴⁵–3¹⁵ ▽° 5⁴⁰–6⁰⁸ 9²⁰–12¹⁰ ▽° 12²⁰–13⁴⁰ ▽° 15¹⁰–30 = 17¹⁰–21²⁰
23	6	6.8	.	–	*° 7²⁰–8³⁵ *¹–9⁴⁰ *° –11⁴⁵ 19⁰⁵–23¹⁰ *² –24; = 6¹⁰–13²⁰ 17²⁰–24
24	6	0.0	6	–	*² 0⁰⁰–40 *¹–1²⁰ *° –7³⁰; = 0⁰⁰–6³⁰, 8¹⁵–15²⁰, 18⁴⁰–24
25	6	.	3	–	= 0⁰⁰–3³⁰ 6¹⁰–13³⁰ 14³⁵–19³⁰
26	7	⌴ .	3	–	= 8²⁵–9²⁰ 20³²–22²⁰
27	7	0.4	2	–	* 23²⁵–24; = 5²⁰–11⁴⁵ ∞ –12³⁰ 17²⁰–18⁴⁰ = –22³⁰
28	7	1.0	2	–	*° 0⁰⁰–1³⁰, 3⁴⁰–7¹⁵ *¹–9³⁵ ▽° 21³⁵–22¹⁰; = 16³⁰–19³⁰
29					
30					
31					
Σ	–	41.3	–	–	UWAGI.

Gdańsk – Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ Marzec – Mars 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	135.4	135.7	134.4	135.2	-0.2	1.0	-2.2	-0.9	2.0	-2.7	74	92	85	84	1.5	0.5	0.8	0.9	9	9	0	NNE 5	N 6	N 3
2	131.6	130.0	127.7	129.8	0.0	1.9	0.1	0.5	2.4	-2.7	68	64	76	76	0.7	2.5	1.5	1.6	10	10	10	NNW 3	NNW 4	N 1
3	124.7	122.8	118.6	122.0	-1.3	1.0	-1.2	-0.7	1.9	-3.0	82	66	69	79	1.0	2.3	0.6	1.3	10	4	0	C 0	C 0	S 1
4	110.8	107.0	105.9	107.9	-1.2	2.3	2.2	1.4	3.2	-1.9	89	71	82	81	0.6	2.0	1.3	1.3	9	10	3	S 3	S 3	W 3
5	109.6	111.1	112.5	111.1	-0.4	5.2	0.3	1.4	5.6	-1.2	80	36	76	64	1.2	5.6	1.4	2.7	2	1	0	WNW 4	WNW 9	WNW 5
6	112.7	113.2	113.8	113.2	-1.3	3.0	0.5	0.7	4.1	-2.1	86	71	75	77	0.8	2.2	1.7	1.6	0	1	10	WNW 3	NNE 7	NE 4
7	114.6	115.9	117.0	115.9	-1.7	0.1	-2.0	-1.4	1.2	-2.5	74	62	85	74	1.4	2.4	0.8	1.5	10	7	0	ESE 5	SE 5	SE 2
8	118.9	120.2	123.6	120.9	-3.4	-0.7	-2.4	-2.2	0.3	-4.3	85	66	80	77	0.7	2.0	1.0	1.2	1	8	10	SE 1	S 2	SSE 4
9	127.8	129.5	131.3	129.5	-5.0	1.8	-0.2	-0.9	3.2	-5.5	80	60	84	75	0.8	2.8	0.9	1.5	0	0	0	C 0	ENE 3	E 1
10	133.3	133.4	133.3	133.3	-5.2	4.6	-0.4	-0.4	6.6	-5.7	95	50	86	77	0.2	4.3	0.8	1.8	0	0	0	C 0	C 0	C 0
11	132.6	131.6	126.8	130.3	-1.6	10.0	3.4	3.8	11.0	-3.3	78	36	60	58	1.2	7.8	3.1	4.0	0	2	2	C 0	S 1	S 2
12	122.1	119.6	117.4	119.7	4.6	10.2	4.2	5.8	11.4	2.3	50	41	77	56	4.3	7.2	1.8	4.4	10	10	2	W 2	W 3	C 0
13	115.3	114.9	111.0	113.7	4.4	14.0	10.5	9.8	15.6	0.5	68	27	47	47	2.7	11.7	6.8	7.1	2	3	0	W 2	NW 5	SW 3
14	104.0	101.2	98.1	101.1	6.6	10.6	7.7	8.2	13.0	5.9	69	74	77	73	2.9	3.4	2.4	2.9	3	8	8	W 7	WSW 9	WNW 17
15	103.9	104.6	97.6	102.0	3.6	3.8	1.2	2.4	9.6	0.2	90	87	94	90	0.8	1.1	0.4	0.8	10	10	10	WNW 7	W 6	W 3
16	103.1	108.7	114.6	108.8	-5.2	-4.2	-3.0	-3.8	2.2	-5.6	68	61	75	68	1.3	1.8	1.2	1.4	4	8	10	N 14	N 14	NNE 9
17	115.4	112.3	101.2	109.6	-6.0	-3.6	-3.0	-3.9	-2.5	-6.8	94	71	95	87	0.2	1.4	0.3	0.6	10	10	10	SSE 4	SSE 5	SSE 5
18	87.3	87.9	95.4	90.2	4.6	6.4	1.6	3.6	7.4	-3.7	95	88	76	86	0.4	1.1	1.7	1.1	10	10	9	W 6	W 7	N 7
19	105.2	107.9	109.7	107.6	-0.6	0.0	-0.1	-0.2	2.2	-1.1	72	77	78	76	1.7	1.4	1.3	1.5	9	9	10	N 4	NE 3	E 3
20	111.3	108.0	101.4	106.9	-0.4	0.7	4.2	2.2	4.5	-0.7	76	96	97	90	1.4	0.2	0.2	0.6	10	10	10	C 0	SSE 3	SSW 1
21	101.8	104.6	107.0	104.5	5.7	9.8	6.4	7.1	11.0	3.9	80	59	79	73	1.9	4.9	2.0	2.9	0	9	0	W 6	W 12	SW 3
22	109.2	111.6	114.6	111.8	5.0	8.4	4.4	5.6	9.8	4.0	76	51	77	68	2.0	5.4	1.9	3.1	9	4	0	W 7	W 8	W 8
23	117.6	120.4	126.7	121.6	2.2	4.6	-0.5	1.4	7.9	-0.8	89	84	69	81	0.8	1.4	1.8	1.3	0	10	9	C 0	NE 5	NE 9
24	131.4	130.7	129.9	130.7	-3.6	3.3	0.3	0.1	4.9	-4.4	60	35	59	51	1.9	5.0	2.5	3.1	8	2	0	SE 4	SE 7	SE 5
25	126.8	125.6	124.6	125.7	-1.2	3.8	2.4	1.8	4.3	-2.1	66	48	61	59	1.8	4.2	2.9	3.0	9	10	0	SE 6	SSE 6	S 6
26	122.4	120.9	120.0	121.1	2.0	8.2	6.8	6.0	11.6	1.4	68	57	68	64	2.3	4.7	3.2	3.4	9	10	0	S 5	S 7	S 4
27	119.5	118.5	117.6	118.5	2.4	14.0	9.5	8.8	15.9	1.9	89	38	57	61	0.8	9.9	5.2	5.3	4	7	0	S 4	S 7	S 3
28	113.4	113.3	113.4	113.4	4.6	10.4	6.6	7.2	11.4	3.6	63	52	93	69	3.1	6.0	0.8	3.3	8	10	10	S 5	SSW 4	C 0
29	113.0	113.7	116.7	114.5	3.6	4.2	5.0	4.4	7.4	3.1	100	97	95	97	0.0	0.2	0.4	0.2	10	10	10	NE 2	NE 6	NE 2
30	121.3	121.7	122.4	121.8	2.7	5.8	3.4	3.8	6.5	1.5	95	65	93	91	0.4	1.4	0.5	0.8	7	2	0	N 2	NE 6	NNE 1
31	122.6	123.3	123.5	123.1	3.0	8.2	7.0	6.3	11.4	0.3	98	70	71	80	0.2	3.3	2.9	2.1	10	8	0	N 5	NE 2	C 0
M	116.7	116.8	116.4	116.6	0.5	4.6	2.4	2.5	6.7	-1.0	80	64	78	74	1.3	3.6	1.7	2.2	6.2	6.6	4.5	3.8	5.4	3.7

Kwiecień – Avril

1	124.6	124.2	122.9	123.9	2.8	11.8	6.8	7.0	12.7	1.1	84	47	71	68	1.2	7.3	2.6	3.7	0	0	0	C 0	NE 2	C 0
2	122.4	122.2	123.1	122.6	4.4	14.0	8.0	8.6	15.0	2.9	67	49	72	69	1.1	8.2	2.9	4.1	0	0	0	C 0	NE 4	C 0
3	126.4	127.0	128.4	126.9	5.2	10.3	5.4	6.6	12.2	3.2	83	65	74	73	1.5	4.7	2.4	2.9	0	1	0	C 0	NNE 3	C 0
4	129.6	130.1	128.8	129.5	2.6	12.7	6.2	6.9	13.9	-0.3	86	35	70	64	1.1	9.5	2.8	4.5	5	1	0	C 0	NE 3	C 0
5	126.1	122.9	119.3	121.4	9.8	19.4	10.8	12.7	21.1	4.1	49	30	60	46	6.2	15.7	5.3	9.1	0	0	0	C 0	SW 4	C 0
6	110.9	108.5	108.7	109.4	12.8	13.0	6.5	9.7	19.1	6.0	41	56	76	58	8.8	6.6	2.3	5.9	7	9	8	WSW 5	NNE 6	NW 6
7	110.5	114.2	119.7	114.8	4.8	5.7	1.8	3.5	6.9	1.2	78	70	67	72	1.9	2.8	2.3	2.3	8	4	9	NE 8	NE 9	NE 10
8	120.1	116.4	113.9	116.8	1.1	7.0	4.2	4.1	8.7	0.7	61	39	74	58	2.6	6.1	2.1	3.6	8	4	9	N 6	NW 7	WNW 4
9	113.2	114.2	111.8	113.1	1.8	1.8	-1.6	0.1	4.8	-1.9	91	85	75	84	0.7	1.1	1.3	1.0	10	4	0	NE 7	NE 7	C 0
10	105.7	98.6	93.9	99.4	1.0	9.0	6.9	6.0	10.3	-3.3	87	42	68	66	0.9	6.7	3.1	3.6	10	9	9	SW 4	SW 8	WSW 4
11	90.5	92.9	99.7	94.4	3.4	3.7	0.6	2.1	7.6	0.0	70	55	88	74	2.4	2.8	0.8	2.0	4	9	10	WSW 6	NW 8	NNW 8
12	106.3	108.5	110.3	108.4	0.0	1.8	-0.8	0.0	3.8	-1.8	70	69	85	75	1.8	2.2	0.9	1.6	5	9	3	NNW 3	NE 3	WNW 2
13	111.6	113.3	115.2	113.4	-1.2	0.6	-1.2	-0.8	2.1	-3.8	86	81	91	86	0.8	1.3	0.5	0.9	6	8	2	W 2	NE 4	C 0
14	115.7	116.3	118.6	116.9	-0.8	0.7	-1.4	-0.7	4.1	-2.7	83	90	86	86	1.0	0.6	0.8	0.8	2	9	2	W 4	NE 3	C 0
15	120.1	119.8	121.3	120.4	-0.6	2.7	-1.3	-0.1	3.6	-3.5	81	69	87	79	1.1	2.3	0.8	1.4	3	10	0	C 0	NE 2	C 0
16	120.3	116.8	114.5	117.2	-0.4	2.4	6.3	3.6	7.4	-2.8	80	93	91	88	1.2	0.6	0.8	0.9	10	10	10	S 1	S 5	W 4
17	115.9	118.6	120.9	118.5	6.0	4.4	3.0	4.1	8.6	2.1	88	95	86	90	1.2	0.5	1.1	0.9	10	10	10	WNW 5	NNE 7	N 4
18	120.0	119.1	117.6	118.9	3.3	4.9	3.0	3.6	5.8	2.3	93	92	90	92	0.5	0.7	0.8	0.7	10	10	10	NNE 4	NE 5	NE 5
19	113.9	112.7	113.4	113.3	3.0	4.1	4.5	4.0	5.7	1.4	90	80	79	83	0.8	1.6	1.8	1.4	9	10	10	N 2	NE 2	SE 1
20	116.2	119.7	124.0	120.0	4.1	7.0	5.2	5.4	8.0	3.0	93	88	94	92	0.6	1.2	0.5	0.8	10	10	10	C 0	C 0	NNE 3
21	125.9	126.9	127.4	126.7	4.6	5.1	4.0	4.4	5.7	3.3	92	94	98	95	0.7	0.6	0.1	0.5	10	10	10	NNE 6	N 5	N 5
22	129.7	131.0	131.3	130.7	4.6	8.4	4.6	5.6	10.0	3.3	92	79	93	88	0.7	2.2	0.6	1.2	10	9	10	SW 2	E 3	NE 3
23	129.4	129.9	130.4	129.9	4.6	5.4	3.6	4.3	9.0	3.1	97	94	95	95	0.3	0.6	0.4	0.4	10	10	8	NE 4	NE 5	NW 2
24	129.6	129.4	128.5	129.2	3.2	8.3	3.4	4.6	9.8	1.7	98	86	98	94	0.2	1.6	0.1	0.6	10	8	9	NNW 2	NE 7	N 8
25	126.6	126.5	125.3	126.1	3.0	4.3	3.4	3.5	5.6	2.5	98	88	95	94	0.2	1.0	0.4	0.5	10	10	10	NNE 8	NE 9	NNE 8
26	123.9	121.9	120.9	122.2	3.3	8.6	7.4	6.7	9.8	2.6	100	81	83	88	0.0	2.2	1.8	1.3	10	10	2	NNE 5	NNE 9	N 3
27	118.1	117.4	115.1	116.9	9.8	10.0	6.8	8.4	13.1	5.3	84	81	94	86	1.9	2.4	0.6	1.6	3	7	5	N 2	NE 4	NE 3
28	111.3	109.3	109.0	109.9	10.9	16.8	11.0	12.4	23.0	5.9	83	68	89	80	2.2	6.1	1.5	3.3	8	7	9	C 0	C 0	NE 1
29	107.1	108.2	110.3	108.5	14.4	16.6	10.2	12.8	19.2	9.7	75	67	88	77	4.1	6.3	1.4	3.9	8	4	0	C 0	NE 4	C 0
30	110.7	108.0	108.7	109.1	8.6	12.8	6.6	8.6	15.1	5.6	92	80	71	81	1.0	2.9	2.8	2.2	10	9	0	C 0	NE 2	W 9
31																								
M	117.7	117.5	117.6	117.6	4.3	7.8	4.5	5.3	10.1	1.7	83	72	83	79	1.6	3.6	1.5	2.2	6.9	7.0	5.5	2.9	4.7	3.2

Gdańsk – Wrzeszcz

$H_s = 13\ m$ $H_b = 12{,}4\ m$ $h_w = 11\ m$

Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	3	–	= 8²⁵ – 30
2	7	.	2	–	= 7²⁵ – 11³⁰
3	7	.	pł.	–	= 8³⁰ – 11²⁰ 17³⁰ – 21¹⁵
4	6	0.3	pł.	–	●° 13¹⁰ – 14³⁰ 17¹⁵, = 5⁴⁰ – 18²⁰
5	8	.	pł.	–	⌴ ° 3¹⁰ – 7³⁰
6	8	.	.	–	⌴ n
7	7	.	.	–	= 17³⁰ – 21³⁰, ⌴ ¹ 22¹⁰ – 24
8	7	.	.	–	= 5³⁰ – 6³⁵, ⌴ ¹ 0⁰⁰ – 7³⁰
9	7	.	.	–	= 5²⁰ – 9⁴⁵ ∞ – 11¹⁰ = 21⁴⁰ – 24
10	7	.	.	–	= 0⁰⁰ – 4¹⁰ 5³⁰ – 12³⁰ 17³⁰ – 24, ⌴ n – 10⁰⁰
11	7	.	.	–	= 0⁰⁰ – 3³⁰ 6²⁰ – 10³⁵, ⌴ n – 7¹⁰
12	7	.	.	–	= 16³⁰ – 21⁴⁵
13	7	.	.	–	∞ 16¹⁰ – 22³⁰
14	7	0.0	.	–	●▽° 20⁴⁵ – 21⁰⁵ 22²⁵ – 24, ⩢ 13³⁰ – 15²⁰ (por. 18 m/sek) ⩢ – 24 (por. 26 m/sek), ∞ 5³⁰ – 9⁴⁰ = 11³⁰ – 12⁴⁰
15	7	4.4	.	–	●▽° 0⁰⁰ – 20 ●¹ 4³⁵ – 6⁴⁰ ●° – 7⁴⁰ ✳° 16¹⁰ – 21³⁰ ⩢ 0⁰⁰ – 4⁴⁰ (por. 25 m/sek) ⩢ – 5²⁰
16	7	1.3	.	–	✳▽¹ 9¹⁵ – 13³⁵ 14⁰⁵ – 18¹⁰ ✳▽° 18²⁰ – 23⁴⁰ ⩢ 4¹⁰ – 25 (por. 18 m/sek) ⩢ – 15³⁰ (por. 22 m/sek)
17	7	2.5	2	–	✳° 2²⁰ – 9³⁵, 13¹⁰ – 40 ✳¹ – 14²⁰ ✳° – 15³⁵ ✳¹ – 17⁴⁰ ✳° – 23⁴⁰
18	6	0.2	2	–	✳° 0³⁵ – 4³⁰, ● ° – 5³⁵ ●° – 11³⁵, 13⁴⁵ – 14⁴⁰, 15²⁰ – 16³⁵, = 11³⁵ – 15²⁰
19	7	.	.	–	
20	6	4.0	.	–	✳¹ 10³⁴ – 11³⁰ ●¹ – 12¹⁰ ●¹ – 13³⁵ ●° – 19¹⁰, 21³⁵ – 22¹⁵, = 19¹⁰ – 24
21	7	.	.	–	⩢ 10³⁰ – 17³⁰ (por. 17 m/sek), = 0⁴⁰ – 4²⁰
22	8	.	.	–	
23	7	.	.	–	⩢ 14³⁰ – 15³⁰ (por. 15 m/sek)
24	8	.	.	–	
25	7	.	.	–	⩢ 16¹⁰ – 17⁴⁰ (por. 15 m/sek)
26	7	.	.	–	
27	7	.	.	–	
28	7	0.4	.	–	●° 13¹⁰ – 14³⁰ ●° 18¹⁰ – ³⁰ ●¹ – 20³⁰ ●° 23²⁰ – 24, = 20³⁰ – 24
29	5	0.7	.	–	●° 0⁰⁰ – ³⁰ ●¹ – ¹³⁰ ●° – 2³⁰ ●° 5¹⁰ – 6⁴⁰, 7²⁰ – 9³⁰, 13²⁵ – 14¹⁵ ●° – 14⁴⁰ ●° – 15⁴⁰ ●° 16²⁰ 17⁵⁰, 18²⁵ – 19¹⁵ = 0⁰⁰ – 8¹⁰ = ¹ – 10⁴⁵ = – 16²⁰
30	6	.	.	–	= 0⁰⁰ – ²⁰ 4¹⁰ – 24 [29.III: = ¹ – 18²⁰ = – 21³⁰, 23¹⁰ – 24
31	7	.	.	–	= 0⁰⁰ – ²⁰, 4¹⁰ – 24
Σ	–	13.8	–	–	UWAGI

Kwiecień – Avril

1	7	.	.	–	= 0⁰⁰ – 8³⁰ ∞ – 11¹⁵
2	7	.	.	–	= 4³⁰ – 8²⁰
3	7	.	.	–	= 5²⁰ – 8³⁵
4	7	.	.	–	= 6⁴⁰ – 8⁴⁰ 19³⁵ – 22⁴⁰
5	8	.	.	–	⌴ ° 4⁵⁰ – 6³⁰
6	7	0.0	.	–	●° 17⁵⁰ – 18⁴⁰ ⌒ 18³⁰ – ³⁷
7	8	0.0	.	–	●° 8²⁰ – 10³⁵, ⩢ 15³⁰ – 24 (por. 16 m/sek)
8	8	0.8	.	–	⩢ 0⁰⁰ – ³⁰ (por. 16 m/sek)
9	8	0.0	.	–	●° 4³⁰ – 5¹⁰ ✳° – 7³⁰ ✳° – 9⁴⁰
10	7	0.0	.	–	
11	8	0.0	.	–	●° ¹³⁵ ⁴⁴⁵ ●▽° 11⁴⁰ – 12⁰⁵ 13³⁰ – 14¹⁵, 14⁴⁰ – 15¹⁰ ✳▽° 15²⁰ – ³⁵ 16¹⁰ – ³⁰ ✳▽° 16⁵⁰ – 17¹⁰ ✳▽° 20⁴⁰ – 21⁰⁵, 21²⁰ – 22⁴⁰, ⩢ 8⁴⁰ 10⁴⁵
12	7	0.8	.	–	✳▽° 8³⁰ – 11⁴⁰ 12²⁵ – 13⁴⁰, 15⁵⁰ – 16³⁰ ✳▽¹ – 17²⁰ ✳▽° – 18⁰⁵ ✳▽¹ 18²⁰ – 19³⁵, = 19³⁵ – 21⁴⁰
13	6	2.9	1	–	✳▽¹ 8⁴⁰ – 11⁴⁰ ✳▽° 12⁴⁵ – 18⁰⁷ 23¹⁵ – ⁴⁰
14	6	0.5	.	–	✳▽° 0³⁵ – 1²⁵ 10⁰⁵ – ³⁵ 11³⁵ – 12¹⁰, 12⁴⁰ – 13²⁵, 13⁵⁰ – 15¹⁰, 15³⁵ – 16³⁰, 16⁵⁰ – 18²⁰
15	6	1.3	.	–	✳▽° 10⁵³ – 14²⁵ ✳▽¹ – 15³⁵ ✳▽° 16¹⁵ – ²⁸ ⌴ na – 8³⁰
16	6	0.8	.	–	✳° 9⁴⁰ – 11²⁰ ✳° – 13²⁰ ●° 16⁰⁰, 16²⁰ 23³⁵
17	5	0.0	.	–	●° 12³⁵ 14⁴⁰
18	6	0.0	.	–	●° 9¹⁵ – 11¹⁰ 19²⁰ – 20¹⁵ = 5³⁰ – 11¹⁰ = ¹ – 12¹⁰ = – 15¹⁰
19	7	1.0	.	–	●° 21²⁵ – 24, = 19¹⁵ – 21²⁵
20	6	0.3	.	–	●° 0⁰⁰ – 4¹⁵, ●° 7³⁵ – 11¹⁰, = 4¹⁵ – 24
21	6	3.0	.	–	●° 7⁴⁰ 15²⁵ ●¹ – 18³⁰ ●° – 19¹⁵ 20³⁵ – 21¹⁰ = 0⁰⁰ – 7⁴⁰, 19¹⁵ – 24
22	7	4.5	.	–	●° 14³⁵ – 19³⁵ ●¹ – 21³⁰ ●° – 24, = 0⁰⁰ – 7⁴⁰
23	6	0.0	.	–	●° 0⁰⁰ – 6¹⁵, 7⁴⁵ – 8²⁵, = 6¹⁵ – 10¹⁵, 12³⁵ – 13³⁰, 20³⁰ – 23²⁰, ⌓ ° 22²⁰ – 24
24	7	.	.	–	= 2²⁰ – 12³⁰, 18²⁰ – 24, ⌓ ² 0⁰⁰ – 6⁰⁰
25	7	.	.	–	= 0⁰⁰ – 10³⁵, 18³⁰ – 24
26	7	1.3	.	–	= 0⁰⁰ – 3⁵⁰ = ° – 4²⁵ = ¹ – 6³⁵ = ° – 7⁰⁵ = – 10³⁰
27	7	0.3	.	–	●▽° 0³⁰ – 1²⁰ ●▽° – 1⁴⁰ = 4²⁵ – 9⁴⁰, 16²⁵ – 24
28	7	.	.	–	●▽° 0¹⁵ – 1⁵⁰ (◹)° 18²⁵ – 20⁴⁰ SW – N, 22⁴⁰ – 23³⁵ NE – SSE, = 0⁰⁰ – ¹⁵ 4¹⁵ – 8⁴⁰, 15²⁵ – 24
29	7	.	.	–	= 0⁰⁰ – 4¹⁵ 7³⁰ – 9³⁰
30	6	0.0	.	–	●° 9³⁵ – 10¹⁰ ●▽° 14³⁵ – 15³⁵ ●° 16²⁰ 18⁰⁵, = 0²⁰ – 16¹⁰
31					
Σ	–	17.5	–	–	UWAGI

Gdańsk – Wrzeszcz

$\varphi = 54°23'$ $\lambda = 18°36'$

Maj – Mai 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	114.8	118.0	119.4	117.4	5.7	7.6	3.8	5.2	8.9	2.8	64	52	77	64	3.4	5.0	1.9	3.4	1	7	1	NNW 7	ENE 6	C 0
2	118.4	116.0	113.2	115.9	4.6	12.4	10.8	9.6	13.7	1.8	67	38	55	53	2.9	9.0	5.9	5.9	9	8	10	SSE 3	SW 3	C 0
3	110.9	109.1	105.7	108.6	9.4	13.6	9.4	10.4	15.0	7.5	51	50	73	58	5.7	7.8	3.2	5.6	10	9	7	SW 5	W 6	W 3
4	101.8	103.7	104.8	103.4	5.8	6.2	4.7	5.4	9.9	3.9	71	62	64	66	2.6	3.7	3.1	3.1	4	8	1	W 9	W 2	WSW 8
5	103.8	103.4	107.3	105.5	4.0	6.0	3.5	4.2	9.3	1.7	77	80	83	80	1.9	1.9	1.3	1.7	6	7 ●	1	W 9	WNW 9	SW 3
6	108.6	108.6	108.6	108.6	3.2	8.0	4.8	5.2	10.0	0.8	78	63	92	78	1.7	3.9	0.7	2.1	0	8	10	S 2	E 5	ENE 4
7	107.0	108.3	108.4	107.9	3.6	4.2	3.8	3.8	5.4	2.9	93	90	93	92	0.5	0.8	0.5	0.6	10 ●	10	10 ●	NNE 5	NE 4	WNW 5
8	106.5	106.4	107.8	106.9	3.4	4.0	3.6	3.6	4.9	2.5	90	87	90	89	0.8	1.1	0.8	0.9	10	10 ●	10	N 6	N 7	N 3
9	111.1	113.2	113.2	112.5	4.6	6.4	5.0	5.2	7.7	3.1	84	79	92	85	1.4	2.0	0.7	1.4	9	9	10 ●	NW 1	NE 2	N 6
10	109.4	108.7	109.8	109.3	5.4	9.6	6.2	6.8	11.1	3.9	95	88	91	91	0.5	1.5	0.9	1.0	10	10	10	NNW 4	NE 5	NW 2
11	110.3	113.0	114.7	112.7	5.8	7.9	7.3	7.1	9.5	4.9	98	90	93	94	0.1	1.0	0.7	0.6	10 ●	10 ●	0	C 0	W 4	C 0
12	114.7	114.7	113.5	113.0	9.4	20.1	14.8	14.8	20.1	2.0	79	43	59	60	2.5	13.5	6.9	7.6	0	4	1	S 1	SSW 6	S 2
13	113.4	113.2	113.8	113.5	13.7	22.6	12.4	15.3	23.8	7.6	65	44	80	63	5.5	15.2	2.9	7.9	4	6	9	C 0	SSW 1	C 0
14	116.0	116.6	118.8	117.1	13.2	16.7	12.4	13.7	17.0	11.3	86	68	78	77	2.1	6.1	3.2	3.8	5	7●	3	C 0	NE 2	WNW 3
15	120.9	122.1	121.4	121.5	12.8	15.7	10.6	12.4	17.4	9.1	64	55	74	64	5.4	8.1	3.4	5.6	0	0	0	W 5	E 3	C 0
16	120.1	117.4	115.0	117.5	14.0	21.6	17.2	17.5	25.2	7.6	54	36	58	49	7.4	16.4	8.2	10.7	0	1	0	C 0	S 5	C 0
17	115.0	116.3	117.7	116.3	15.2	15.3	11.7	13.5	21.7	9.3	63	76	68	69	6.3	4.3	4.4	5.0	4	9	9	S 4	NE 7	NNW 2
18	118.3	118.4	116.4	117.7	14.2	14.7	10.2	12.3	16.0	9.7	64	60	81	68	5.8	6.7	2.4	5.0	4	4	3	NW 4	NE 4	C 0
19	113.6	111.5	107.6	110.9	11.1	15.8	15.4	14.4	18.6	6.9	83	71	79	78	2.3	5.1	3.7	3.7	6	3	7(R)	N 4	NE 2	C 0
20	107.5	109.1	111.9	109.5	15.8	18.5	11.9	14.5	20.9	11.3	87	76	70	78	2.2	5.1	4.1	3.8	9	7(R)	6	S 3	W 8	NW 6
21	114.4	115.5	116.3	115.4	9.0	13.2	9.3	10.2	15.0	7.5	75	48	76	66	2.9	7.8	2.8	4.5	9	7	3	NW 7	NW 3	NNW 3
22	115.6	116.1	116.9	116.2	9.8	11.8	7.4	9.1	13.6	6.4	81	73	100	85	2.3	3.8	0.0	2.0	10	8	10 ≡	NW 4	NE 8	N 6
23	114.4	114.0	113.5	114.0	11.2	10.4	9.1	10.0	11.7	6.7	91	85	97	91	1.2	1.9	0.4	1.2	8	10	10 ●	N 5	N 8	NNE 8
24	116.0	120.4	124.5	120.3	9.9	10.2	7.2	8.6	11.2	6.8	81	66	74	74	2.4	4.2	2.7	3.1	9	6	1	NE 9	NE 9	NE 10
25	126.9	128.6	129.0	128.2	7.9	8.4	6.3	7.2	8.4	5.7	72	68	78	73	2.9	3.6	2.1	2.9	3	4	7	NE 8	NE 9	NE 9
26	129.2	129.2	128.5	129.0	7.0	8.0	6.4	7.0	10.0	5.2	71	67	65	68	2.9	3.5	3.4	3.3	9	7	4	NE 8	NE 8	NE 5
27	127.2	127.4	125.9	126.8	8.1	8.4	6.6	7.4	10.0	4.7	66	56	76	66	3.7	4.8	2.3	3.6	9	5	2	ENE 5	NE 7	NE 3
28	124.1	123.1	121.7	123.0	5.0	9.6	5.9	6.6	10.7	2.5	89	64	82	78	1.0	4.3	1.7	2.3	8 ●	4	0	W 3	NE 6	NNE 1
29	119.9	119.5	119.3	119.6	7.3	9.9	8.8	8.7	12.7	3.5	61	64	82	69	4.0	4.3	2.0	3.4	10	10	6	W 4	NW 6	C 0
30	120.3	121.0	119.6	120.3	8.5	12.0	10.2	10.2	13.1	5.1	74	64	70	69	2.9	5.1	3.7	3.9	6	5	1	NNE 6	NE 4	C 0
31	118.4	115.6	113.5	115.8	14.5	21.8	13.1	15.6	22.7	6.9	54	31	65	50	7.6	17.9	5.3	10.3	1	5	2	W 2	SW 5	C 0
M	115.2	115.6	115.5	115.4	8.8	12.0	8.7	9.6	13.7	5.5	75	64	78	72	3.1	5.8	2.8	3.9	6.2	6.7	5.0	4.3	5.7	3.0

Czerwiec – Juin

1	112.6	113.3	112.7	112.9	12.6	16.1	12.9	13.6	17.9	9.0	65	51	65	60	5.2	9.1	5.3	6.5	7	9	10	WNW 7	WNW 8	WNW 6
2	113.9	116.9	118.2	116.3	12.6	14.3	13.2	13.3	15.7	11.4	79	75	74	76	3.1	4.1	4.0	3.7	10	9	10	WNW 5	NW 5	NW 3
3	118.1	117.7	115.3	117.0	16.2	21.8	13.2	16.1	23.0	9.4	71	48	85	68	5.2	13.7	2.3	7.1	1	7	4	W 6	WSW 5	C 0
4	112.0	110.6	108.6	110.4	17.6	19.5	15.8	17.2	21.0	9.4	68	62	84	71	6.4	8.7	2.8	6.0	1	10	9	C 0	E 3	C 0
5	104.1	103.0	101.9	103.0	13.4	13.0	12.1	12.6	17.7	11.0	91	88	83	87	1.4	1.8	2.3	1.8	10 ●	10	8	S 2	W 5	W 4
6	101.9	105.0	106.6	104.5	11.5	15.1	12.1	12.7	17.0	9.3	81	40	68	63	2.7	10.3	4.5	5.8	9	5	10	W 4	WNW 7	WSW 4
7	107.2	106.6	109.0	107.6	13.0	17.8	12.8	14.1	19.3	10.4	66	39	75	60	5.1	12.5	3.8	7.1	8	9	5	SW 4	SW 8	C 0
8	111.5	112.7	112.0	112.1	14.6	18.6	15.2	15.9	20.6	6.3	67	46	82	65	5.5	11.6	3.2	6.8	4	8	0	C 0	SW 1	C 0
9	110.6	108.3	108.1	109.0	17.4	26.3	17.2	19.5	27.7	10.5	79	47	90	72	4.2	18.0	2.0	8.1	0	7	9	SE 2	SE 6	C 0
10	111.2	112.7	113.0	112.3	16.3	17.0	15.4	15.0	20.9	13.0	76	77	95	83	4.3	4.5	0.7	3.2	3	10	10	C 0	NE 3	C 0
11	111.7	109.1	106.9	109.2	13.8	20.8	24.1	20.7	29.5	10.6	99	74	74	82	0.2	6.4	7.8	4.8	10 ≡	6	3	C 0	NE 3	C 0
12	115.7	122.5	127.5	121.9	16.1	18.8	12.8	15.1	24.1	12.4	80	54	64	66	3.6	10.1	5.4	6.4	9	4	2	WNW 6	W 7	W 5
13	127.9	129.2	127.7	128.3	12.8	15.4	14.6	14.4	18.7	9.4	56	64	74	65	6.5	6.4	4.3	5.7	0	9	0	WNW 9	WNW 8	C 0
14	129.1	130.7	130.2	130.0	16.1	16.3	11.3	13.8	17.7	10.1	57	43	64	55	7.9	10.6	4.8	7.8	0	0	4	N 5	NNE 6	NNW 3
15	130.1	129.4	126.3	128.6	11.9	15.8	12.6	13.2	17.5	7.5	78	35	65	59	3.0	11.7	5.2	6.6	4	2	1	NNE 6	NE 5	C 0
16	124.1	123.0	122.1	123.1	18.6	18.4	13.5	16.0	25.2	8.9	45	57	63	55	11.8	9.1	5.7	8.9	1	5	1	SSW 2	NNE 4	NNW 1
17	121.5	121.1	118.4	120.3	15.6	18.8	15.2	16.2	20.0	9.7	52	41	60	51	0.6	12.9	7.0	9.5	0	0	2	NNE 3	ENE 2	C 0
18	116.3	113.3	111.3	113.6	20.0	27.8	18.3	21.1	29.3	10.3	46	33	64	48	12.6	25.1	7.5	15.1	0	1	0	NNE 5	NNE 2	C 0
19	111.4	112.9	113.3	112.5	13.5	14.0	12.8	13.3	18.5	12.0	90	72	71	78	1.6	4.4	4.3	3.4	10	1	3	N 5	N 8	NE 6
20	114.9	116.2	117.7	116.3	14.8	17.2	12.0	14.0	17.8	11.7	53	43	76	57	7.9	11.1	3.3	7.4	2	9	1	ENE 3	NE 3	C 0
21	118.6	114.6	110.6	114.6	13.3	21.2	16.7	17.0	24.1	6.6	56	34	64	51	6.8	16.8	6.8	10.1	3	4	4	SSE 1	SSE 3	C 0
22	105.9	104.1	102.2	104.1	16.0	17.1	14.7	15.6	21.6	10.8	62	90	93	82	7.0	2.0	1.1	3.4	9	10 ●	10	C 0	SE 1	C 0
23	105.2	108.0	108.4	107.2	13.2	17.0	13.8	14.4	19.6	12.7	84	67	82	78	2.5	6.3	2.9	3.9	10	10	10 ●	WNW 3	SW 1	NW 5
24	110.6	109.9	107.3	109.3	14.1	16.1	12.6	13.8	16.8	9.4	74	66	87	76	4.3	6.3	1.9	4.2	6	9	2	WNW 4	SE 2	C 0
25	105.0	108.7	112.4	108.7	11.8	13.6	12.0	12.4	15.5	7.6	94	57	76	76	0.8	6.7	3.3	3.6	10 ●	10	9 ●	C 0	NW 3	WSW 1
26	115.6	117.4	118.9	117.3	13.0	16.1	12.1	13.3	18.0	8.9	68	46	64	59	4.8	9.9	3.1	6.6	2	6	0	WSW 5	W 7	W 3
27	119.2	121.3	122.1	120.9	12.0	15.0	12.4	13.0	17.4	9.3	77	51	54	61	3.2	8.2	6.6	6.0	8	9	2	W 4	WNW 7	W 2
28	117.6	115.5	117.1	116.7	14.7	23.2	19.8	19.4	24.6	11.4	76	61	77	71	4.0	11.1	3.3	6.8	10	9	10	SW 7	W 12	WNW 5
29	119.0	120.0	117.4	118.8	17.6	22.6	18.4	19.2	24.3	16.7	85	59	84	76	3.0	11.3	3.3	5.9	9	6	0	W 5	NW 6	C 0
30	117.4	119.2	120.8	119.1	20.9	20.2	13.3	16.9	25.1	12.7	66	70	99	78	8.4	7.1	0.2	5.2	6	2	10 ≡	NW 7	NW 5	NE 1
31																								
M	114.7	115.1	114.8	114.9	14.8	18.2	14.4	15.4	20.9	10.3	71	56	75	67	5.1	9.6	4.1	6.3	5.5	6.6	5.0	3.7	4.9	1

Gdańsk – Wrzeszcz $H_s = 13\ m$ $H_b = 12{,}4\ m$ $h_w = 11\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	.	.	–	
3	8	0.0	.	–	▽° 16¹⁵–17¹⁰
4	8	0.2	.	–	●° 0³²–1³⁰ ▽° 14²⁰–23³⁰ 7²⁰–35 8⁴²–9⁰⁵ 12⁰³–08 12³⁴–40 13⁰⁹–20 ▽° 13⁴³–50. ≫ 7¹⁰–19³⁰ (por. 18 m/sek) 22¹⁵–24
5	7	0.7	.	–	▽° 1⁰⁰–4²⁵ 5¹⁵–6⁰⁵ 8²⁷–40 9³⁰–38 ▽° 10⁵⁰–11⁰³ ▽° 11²³ 12²⁰–13³⁵ 13⁴⁵–14⁴⁰ 15⁵⁰–16³⁵. ≫ 0⁰⁰–4²⁰ 7²⁰–16³⁰ (por. 16 m/sek)
6	8	3.8	.	–	▽° 11²⁰–35 13¹⁰–20 13⁵⁰–14²⁰, 14⁵⁰–15⁰⁵ ●° 16¹⁰–17⁴⁰, 18¹⁰–20³⁵, 22⁴⁰–24; = 6³⁵–7⁵⁰ 5.V. ⌒ 8²¹–27
7	7	1.1	.	–	●° 0²⁰ 9¹⁰ ● ° 19²⁰ 24
8	7	2.0	.	–	●° 0⁰⁰–35 7⁴⁰ 9³⁰ 11³⁵–13⁴⁰ ●°–19⁴⁰ ●° 22⁴⁰–24; = 20²⁰–22¹⁰
9	8	3.8	.	–	● ° 1⁰⁰–30 ' ● ° 14²⁵–24
10	6	8.5	.	–	●° 0⁰⁰–2⁵⁰ = 4³⁰–14³⁰
11	6	1.9	.	–	●° 1²⁵–3⁴⁰ ●°–4³⁰ ●¹–6²⁵ ●°–11¹⁰ 12²⁵–14⁴⁰; = 16³⁰–24
12	7	.	.	–	= 0⁰⁰–3²⁵ 4¹⁰–8⁴⁰, 22²⁰–24
13	7	0.0	.	–	= 0⁰⁰–3⁴⁰ ∞ 7²⁰–10⁴⁰ = 20³⁰–24
14	7	2.3	.	–	▽° 3³⁵–5²⁰ ● ◹ ° 12³⁰–15¹⁰ W–SE (◹)° 16¹⁰–50 S; = 0⁰⁰–1³⁰, 6¹⁵–7³⁵
15	8	.	.	–	
16	8	.	.	–	
17	7	.	.	–	
18	7	.	.	–	
19	7	3.0	.	–	▽° 21⁵²–24; (◹)° 20⁴⁰–21³⁵ SE; = 0³⁰–4²⁰
20	7	0.4	.	–	▽° 0⁰⁰–2⁰⁵, 5³⁵–6²⁰ ● ° 13²⁰–14¹⁰ W–SE; ◹° 0⁰⁰–2¹⁰ SE–N (◹)° 12¹⁵–13²⁰ N ◹°–14¹⁰ W–SE < 22²⁰–23³⁰
21	8	.	.	–	
22	8	.	.	–	= 19³⁰–20¹⁰ ≡°–24
23	7	3.2	.	–	●° 19³⁵–20¹⁰ ●¹–21³⁰ ●°–22²⁵; ≡° 0⁰⁰–1²⁰ = 2³⁰–5²⁰ ≡°–6⁴⁰ = –8⁴⁰
24	8	.	.	–	≫ 13³⁰–24 (por. 17 m/sek)
25	8	.	.	–	≫ 0⁰⁰–1²⁵ (por. 17 m/sek)
26	8	.	.	–	
27	8	0.9	.	–	
28	8	1.6	.	–	▽° 4³⁰–55 ▽° 6³⁹–45 ▽°–7²⁰ ▽° 8³⁰–9⁴⁵
29	8	0.0	.	–	● ° 7⁰³–20, 8¹⁰–12³⁵
30	8	.	.	–	= 2³⁰–4⁵⁰
31	8	.	.	–	
Σ	–	33.2	–	–	UWAGI.

Czerwiec – Juin

1	8	.	.	–	
2	7	0.0	.	–	▽° 11⁴⁵–12⁰⁰
3	8	.	.	–	
4	7	2.3	.	–	▽° 15⁰⁵–25; = 3²⁰–5³⁵ 18²⁰–24
5	7	4.2	.	–	● ° 5²⁰–12⁴⁰ ▽° 10⁴⁵–20⁰⁰; = 0⁰⁰–11⁴⁵
6	8	0.0	.	–	▽° 15³⁴–45
7	8	.	.	–	
8	7	.	.	–	= 0³⁰–7²⁰ 21²⁰–24
9	7	0.0	.	–	▽° 18⁴⁵–19¹⁵ 20²⁵–40; = 0⁰⁰–8²⁰
10	6	0.0	.	–	● ° 15⁴⁰–16⁰⁰; = 3¹⁵–6²⁰ 13³⁰–22⁴⁵ ≡¹–23⁴³ = –24
11	7	.	.	–	= 0⁰⁰–4⁴⁵ ≡²–8¹⁰ = –10⁴⁰ 22¹⁵–24
12	8	.	.	–	= 0⁰⁰–2³⁸ ≫ 4²⁰–5⁴⁰ (por. 15 m/sek)
13	7	.	.	–	≫ 9²⁰–10⁴⁰ (por. 15 m/sek)
14	8	.	.	–	
15	8	.	.	–	
16	8	.	.	–	
17	8	.	.	–	
18	8	.	.	–	
19	8	.	.	–	= 4²⁵–8¹⁰
20	8	.	.	–	
21	8	.	.	.	
22	6	5.2	.	–	●° 11⁴⁷–12²⁰ ●¹–16³⁵; = 18¹⁵–24
23	7	0.0	.	–	●° 8³⁰–33 21³⁵–24; = 0³⁰–4³⁰
24	8	1.6	.	–	●° 0⁰⁰–10⁰
25	8	2.6	.	–	●° 5²⁵–10²⁵ ▽° 20²⁰–23⁴⁰
26	8	0.0	.	–	▽° 13⁰⁵–15 ▽¹ 14¹⁵–30
27	8	0.0	.	–	▽ 6³⁵–45 6⁵⁵–7¹⁰
28	7	0.2	.	–	●° 2²⁰–6³⁰; ≫ 12²⁰–17³⁵ (por. 15 m/sek)
29	7	.	.	–	●° 0³⁵–1¹⁵, 2⁰⁵–45
30	8	.	.	–	= 18³⁵–20⁴⁵ ≡°–24
31					
Σ	–	16.1	–	–	UWAGI.

Gdańsk – Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	121.5	120.5	117.5	119.8	15.2	19.1	17.8	17.5	20.6	10.5	78	61	79	73	3.9	8.7	4.2	5.6	2	7	1	C 0	ENE 3	C 0
2	113.8	112.6	115.8	114.1	16.0	20.7	16.4	17.4	22.5	15.3	89	79	73	80	2.0	5.1	5.1	4.1	10 ● R	10 ●	0	SSE 3	S 2	W 5
3	117.4	118.1	117.6	117.7	16.7	21.4	15.6	17.3	22.6	12.9	68	47	87	67	6.1	13.5	2.3	7.3	1	8	0	NW 9	WNW 5	C 0
4	115.4	112.6	110.6	112.9	15.0	23.4	18.6	18.9	23.8	11.5	84	57	83	75	2.7	12.5	3.7	6.3	10 ●	3	9	SSE 1	E 4	C 0
5	110.4	112.5	114.6	112.5	21.4	23.6	17.8	20.2	24.3	16.0	79	61	66	69	5.5	11.2	6.9	7.9	4	5	0	NNW 5	NW 7	WNW 6
6	117.3	118.3	119.0	118.2	15.9	21.7	16.6	17.7	22.8	12.8	74	55	67	59	4.7	16.9	6.3	9.3	5	2	1	W 8	WNW 8	WNW 3
7	120.3	120.5	119.1	120.0	18.4	22.2	18.0	19.2	23.8	12.5	65	57	80	67	7.4	11.6	4.0	7.7	0	1	7	C 0	E 6	C 0
8	114.8	114.6	114.4	114.6	18.7	25.8	19.4	20.8	29.2	16.4	65	54	83	67	7.7	15.5	3.8	8.9	10	5	6	SSE 2	ENE 4	C 0
9	113.3	113.5	112.8	113.2	19.0	21.3	17.7	18.9	23.5	17.4	75	59	68	67	5.4	10.3	6.4	7.4	9	9	0	WNW 2	N 6	C 0
10	111.7	110.9	110.4	111.0	17.2	20.8	17.2	18.1	23.0	13.4	69	61	75	68	6.0	9.6	4.9	6.8	0	9	9	W 1	ESE 1	C 0
11	110.2	110.5	110.9	110.5	18.5	21.2	17.4	18.6	22.3	14.2	80	65	73	73	4.3	8.8	5.3	6.1	7	7	7	C 0	ENE 3	NE 3
12	110.4	112.0	110.9	111.1	18.4	18.0	17.7	18.0	19.3	14.9	83	96	97	92	3.7	0.8	0.6	1.7	9	10 ●	10 ●	NNE 3	ENE 3	ENE 4
13	110.7	113.9	116.0	113.5	19.5	21.5	17.4	19.0	25.1	17.2	91	77	94	87	2.0	5.8	1.5	3.0	9	8	5	SW 2	W 5	C 0
14	116.5	115.6	113.9	115.3	17.7	20.4	17.6	18.5	21.9	14.2	93	84	86	88	1.4	3.8	2.8	2.7	9	2	10	C 0	NE 4	C 0
15	111.9	111.4	110.8	111.4	17.2	17.8	17.4	17.4	20.6	15.6	93	89	93	92	1.4	2.2	1.5	1.7	10 ●	10	10	C 0	C 0	C 0
16	110.0	110.3	108.0	109.4	17.7	19.2	16.4	17.4	20.0	14.9	89	81	94	88	2.2	4.2	1.1	2.5	7	8	10 ●	C 0	NNE 5	N 7
17	103.6	103.2	105.1	104.0	15.8	20.0	16.6	17.2	20.2	11.6	96	81	88	88	0.7	4.4	2.4	2.5	10 ●	9	10	NW 6	NW 3	WNW 6
18	105.8	107.2	106.9	106.6	16.4	17.4	16.0	16.4	19.8	15.3	84	79	84	82	2.8	4.2	2.9	3.3	9	10	6	WNW 7	NW 8	NW 3
19	105.9	105.7	106.5	105.9	16.3	23.8	17.7	18.9	24.9	13.7	61	41	61	68	3.4	17.5	3.8	8.2	8	4	0	NW 3	NW 7	C 0
20	105.1	104.5	104.3	104.6	18.6	28.6	19.7	21.6	29.2	13.5	82	46	88	72	3.9	21.0	2.8	9.2	0	6	7	C 0	SSE 7	C 0
21	102.6	101.7	101.4	101.9	20.3	24.0	21.4	21.8	28.6	16.2	72	69	72	71	6.6	9.2	7.1	7.6	0	5	9	C 0	NE 3	E 2
22	101.3	101.9	101.7	101.6	19.2	21.4	19.4	19.8	22.3	17.4	91	79	92	87	1.9	5.5	1.7	3.0	9	8	9	ENE 2	NE 5	NNE 5
23	101.6	102.2	102.4	102.1	19.9	21.8	19.0	19.9	22.6	18.4	89	81	83	84	2.6	5.1	3.8	3.8	9	7	7	NNE 5	NE 7	NW 2
24	101.9	103.6	105.4	103.6	18.2	18.0	15.4	16.8	20.1	14.9	89	74	72	78	2.3	5.4	5.0	4.2	10	10	1	WNW 7	NW 8	W 3
25	106.0	106.4	106.0	106.1	15.3	16.6	14.0	15.0	19.5	13.3	77	70	90	79	4.1	5.7	1.6	3.8	9	9 ●	9 ●	WSW 6	WSW 6	C 0
26	104.1	104.0	103.8	104.0	14.4	17.4	15.1	15.5	19.8	10.6	87	76	90	84	2.2	4.8	1.7	2.9	9	9 ●	10 ●	SW 2	W 4	C 0
27	100.0	100.1	100.5	100.2	16.0	16.8	14.4	15.4	19.6	13.9	92	82	91	88	1.6	3.5	1.4	2.2	10	9	2	SW 2	C 0	C 0
28	101.4	103.0	104.6	103.0	14.7	18.2	14.8	15.6	20.5	11.9	81	61	82	75	3.1	8.3	3.1	4.8	1	6	6	SW 3	WSW 5	SW 4
29	105.5	106.9	109.6	107.3	14.8	20.6	14.7	16.2	22.8	12.3	75	52	89	72	4.1	11.6	1.8	5.8	6	7	9	SW 6	SW 6	C 0
30	109.3	110.1	114.3	111.2	15.4	16.6	15.5	15.8	18.5	14.0	90	84	89	88	1.7	3.1	1.9	2.2	10	9	1	S 3	NE 2	C 0
31	116.5	118.9	119.6	118.3	18.0	20.2	15.8	17.4	20.9	13.8	87	64	78	76	2.6	8.5	3.9	5.0	5	5	3	NW 5	NW 8	W 10
M	109.5	109.9	110.1	109.8	17.3	20.6	17.0	18.0	22.4	14.3	82	68	83	78	3.5	8.3	3.4	5.1	6.7	7.0	5.6	3.0	4.7	2.0

Sierpień – Août

1	119.3	119.6	119.1	119.3	16.7	22.9	17.3	18.6	23.8	14.7	86	47	75	69	2.7	14.8	4.9	7.5	2	0	6	WNW 2	W 4	WNW 5
2	117.6	117.0	116.4	117.7	16.4	18.7	14.3	15.9	19.4	13.3	72	49	78	66	5.2	11.0	3.6	6.6	2	4	1	W 7	NW 9	WNW 5
3	116.9	116.2	116.8	116.6	16.3	20.6	17.4	17.9	21.4	12.9	70	47	78	65	5.6	12.9	4.4	7.6	1	5	9	W 7	NW 9	WNW 7
4	117.2	118.6	120.2	118.7	18.3	19.2	15.3	17.0	20.1	14.2	64	69	82	72	7.5	6.8	3.2	5.8	5	7	3	WNW 5	NE 7	NNW 3
5	121.1	121.9	122.1	121.7	17.6	19.2	15.8	17.1	19.9	13.5	80	72	82	78	4.0	6.2	3.2	4.5	4	2	1	N 6	NE 8	C 0
6	121.9	121.0	119.1	120.7	18.1	21.1	15.9	17.8	22.5	12.4	63	66	88	72	7.7	8.5	2.1	6.1	6	3	0	WNW 1	ENE 5	C 0
7	115.2	112.1	108.9	112.1	17.9	24.0	16.3	18.6	24.6	12.7	76	49	95	73	5.0	15.2	1.0	7.1	8	9	10 ●	S 2	S 4	C 0
8	107.8	110.3	111.0	109.7	17.7	18.2	16.3	17.1	19.6	14.6	89	80	72	80	2.2	4.3	5.3	3.9	2	9	4	N 6	ENE 8	NE 6
9	109.8	108.4	105.0	107.7	15.4	21.0	18.0	18.1	22.7	11.2	85	55	76	72	2.6	11.3	4.8	6.2	2	6	3	C 0	C 0	C 0
10	99.6	99.0	100.8	99.8	16.2	16.8	18.2	17.4	20.3	14.5	82	96	96	91	3.2	0.8	0.9	1.6	9	10 ●	7	SSE 5	S 3	C 0
11	106.2	107.7	107.9	107.3	17.8	25.2	20.9	21.2	26.2	15.0	82	52	77	70	5.6	15.4	5.7	8.2	0	6	2	SW 2	SW 7	S 2
12	107.9	108.6	109.8	108.8	19.8	24.1	17.5	19.7	24.8	17.1	74	58	92	75	5.9	12.7	1.6	6.7	9	9	7	W 1	SW 3	C 0
13	110.4	111.5	112.2	111.4	17.6	24.1	18.3	19.6	25.0	15.6	79	42	85	69	4.2	17.3	3.0	8.2	7	3	9	SW 2	W 7	C 0
14	111.0	111.7	109.8	110.8	17.2	20.1	17.2	17.9	20.7	14.2	84	74	92	83	3.2	6.2	1.6	3.7	9	10	10 ●	C 0	C 0	C 0
15	106.0	107.3	109.1	107.5	17.8	19.6	15.4	17.0	19.7	14.9	96	82	90	89	0.8	4.1	1.7	2.2	10 ●	9	7	NNE 4	NNE 6	C 0
16	109.9	110.1	108.7	109.6	16.4	18.6	16.2	16.8	20.2	14.6	90	92	98	93	1.9	1.7	0.4	1.3	9	10 ●	10 ●	C 0	C 0	C 0
17	106.8	106.3	104.7	106.0	15.0	16.7	15.5	15.7	16.8	14.2	97	91	87	92	0.5	1.8	2.3	1.5	10 ●	10 ●	10 ●	C 0	C 0	W 4
18	101.1	101.2	102.6	101.6	14.6	16.7	16.3	16.0	16.8	13.7	90	79	90	86	1.6	4.1	1.9	2.5	10 ●	10 ●	10	W 8	W 8	WNW 6
19	106.0	108.7	111.9	108.9	16.7	21.6	17.1	18.1	23.3	13.7	91	65	82	79	1.8	9.1	3.5	4.8	9	7	0	W 5	WNW 8	W 7
20	112.3	112.2	111.6	112.0	16.2	19.6	17.2	17.6	21.2	14.1	87	62	82	77	2.3	8.6	3.5	4.8	7	10	4	WSW 4	W 8	WSW 7
21	110.8	110.7	110.6	110.7	17.4	19.8	15.3	17.0	20.3	15.2	82	66	90	79	3.6	7.9	1.7	4.4	3	10	10 ●	W 4	W 2	C 0
22	108.0	108.7	108.7	108.5	13.8	14.3	12.1	13.1	17.2	11.7	90	84	80	85	1.6	2.5	2.8	2.3	9	9 ●	5	WNW 5	N 3	W 3
23	108.7	109.6	110.3	109.5	12.1	16.7	12.6	13.5	18.3	9.7	74	58	85	72	3.7	8.0	2.2	4.6	3	7	4	W 5	NNE 6	C 0
24	107.7	103.3	101.2	104.1	11.6	18.3	14.1	14.5	18.7	8.4	82	60	88	77	2.4	8.4	2.0	4.3	3	10 ●	9	S 2	SSE 5	WSW 7
25	108.4	107.5	105.6	107.2	12.1	19.5	15.0	15.4	20.5	10.5	76	46	71	64	3.3	12.4	4.8	6.8	1	9	4	SW 6	SW 10	S 4
26	106.2	104.9	104.4	105.2	12.5	18.7	13.3	14.4	19.2	12.0	81	54	79	71	2.7	9.9	3.2	5.3	5	7	1	SSW 3	SW 7	SW 7
27	105.7	108.8	110.3	108.3	13.9	17.6	13.6	14.7	18.6	12.5	80	54	83	72	3.2	9.1	2.7	5.0	5	8	10	WSW 9	WSW 6	W 1
28	110.6	110.9	112.0	111.2	11.4	18.5	12.7	13.8	19.2	9.5	90	63	94	82	1.4	8.0	0.9	3.4	9	9	10	C 0	SSE 1	C 0
29	113.3	114.1	115.4	114.3	12.1	18.7	13.1	14.2	19.0	10.5	87	55	82	75	1.8	9.7	2.8	4.8	4	5	9	C 0	WNW 5	C 0
30	115.2	115.1	115.5	115.3	12.4	16.1	11.9	13.1	17.0	9.7	88	67	83	79	1.7	6.0	2.3	3.3	3	9	9	W 5	NW 5	WSW 3
31	112.9	113.1	111.9	112.6	11.2	14.4	10.6	11.7	15.6	9.9	86	75	94	85	1.8	4.1	0.8	2.2	10 ●	8	4	SSW 2	S 6	SW 1
M	110.7	110.8	110.8	110.8	15.3	19.4	15.5	16.5	20.4	13.0	82	65	85	77	3.2	8.3	2.7	4.7	5.7	7.5	6.1	3.5	5.2	2.5

Gdańsk - Wrzeszcz

$H_s = 13\,m$ $H_b = 12{,}4\,m$ $h_w = 11\,m$

Lipiec - Juillet 1957

DNI	WI. DZIAŁ. NOŚCI Y	OPAD R	GRUB ŚNIE. GU +	USŁO. NECZ. NIENIE	P O G O D A
1	8	2.6	.	-	= 0⁰⁰–2³⁵ = –3²⁰
2	7	15.1	.	-	(K) 5²⁰–6³⁰ ●K⁰–9¹⁰ NW-SW △K–9³⁰ ●K⁰–11⁴⁰ (K)–13¹⁵ ▽⁰ 13³⁵–14⁰⁵, 14¹⁵–25
3	8	0.0	.	-	
4	7	8.5	.	-	●⁰ 7³³ 8²⁵. K⁰ 23¹⁵–⁴⁰ N–W ●K⁰–24. = 5¹⁵–11³²
5	7	.	.	-	●K⁰ 0⁰⁰–⁴⁰ N–W ▽⁰–2³⁵. = 2³⁵–5³⁰
6	8	.	.	-	
7	8	.	.	-	
8	8	.	.	-	
9	7	0.0	.	-	▽⁰ 8⁰⁵–¹⁰
10	7	.	.	-	
11	7	.	.	-	= 4²⁵–8²⁰
12	6	19.6	.	-	●⁰ 11⁴⁰–12⁴⁵ ●¹–15⁵⁰ ●⁰–24
13	7	.	.	-	●⁰ 0⁰⁰–2³⁰ 3²⁰ ●¹–5¹⁵ = 5¹⁵–7⁴⁰, 22⁴⁰–24. ⌒⁰ 21³⁰–24
14	7	0.0	.	-	= 0⁰⁰–5³⁰, 7¹⁰–12³⁰ =⁰ 14¹⁰–15¹⁵, 22³⁰–24. ⌒¹ 0⁰⁰–8¹⁵
15	6	0.0	.	-	●⁰ 7²⁰ 9¹⁰, 10³⁵ 12²⁵ ▽⁰ 20¹²–²⁵. = 0⁰⁰–14⁴⁵, 21²⁰–24. (K)⁰ 19⁵⁰–20⁵⁵ S
16	7	18.6	.	-	●⁰ 18¹⁵ 21²⁰ ▽¹–23¹⁰ ●K⁰–24. = 0⁰⁰–9²⁵
17	6	0.0	.	-	●K⁰ 0⁰⁰–135 ●¹–4³⁰ ●⁰–6⁴⁰ ●¹ 7³⁰–9⁴⁰, = –15³⁰
18	7	.	.	-	
19	8	.	.	-	
20	6	0.0	.	-	(K)⁰ 17⁴⁰–18¹⁵ ●K⁰ 18¹⁵–19³⁰ S–N ▽⁰ 19⁵⁰–20¹⁰. = 7²⁰–9²⁰ ∞–14¹⁰ = 22³⁰–24
21	6	0.0	.	-	= 0⁰⁰–8⁴⁵ ∞–10⁴⁵ = –14⁴⁰
22	7	.	.	-	▽⁰ 7²⁰–³⁰. = 4²⁵–11⁴⁰, 21³⁰–24
23	8	.	.	-	= 0⁰⁰–8²⁰
24	7	0.0	.	-	●⁰ 8⁰⁵–¹⁵ ●⁰–9³⁵. ≫ 14³⁰–15⁴⁵ 17¹⁰–⁴⁰ (nor. 17 m/sek): = 2²⁰–6³⁰
25	8	1.2	.	-	▽⁰ 6⁰⁵–¹⁵ 13⁴⁵–14¹⁰ ▽¹ 14²⁵–⁴⁰ ▽⁰ 18¹⁰–²⁵ ▽¹ 18³⁰–⁴⁰ ▽⁰ 20²⁵–⁴⁰ 20⁵⁵–21¹⁵, 21³⁰–22¹⁰
26	8	5.2	.	-	▽⁰ 9⁰⁵–¹⁰ 9²⁵–⁴⁰ 10⁵⁵–11⁰⁵ 13⁴⁰–14⁰⁵ 16⁰²–²⁰ ●⁰ 21²⁰–23¹⁰ ●¹–24
27	7	14.8	.	-	●¹ 0⁰⁰–2¹⁰ ●⁰–3³⁰ ●⁰–5¹⁵ ▽⁰ 11¹⁰–³⁰ ●K⁰ 12⁴⁰–13³⁵ NW–E ▽ 14²⁵–15¹⁰ ●⁰–17⁴⁰
28	8	0.0	.	-	▽⁰ 13⁴⁰–15⁵⁰ 16³⁰–⁴⁵ 18⁴⁰–⁴⁵ 19⁴⁰–⁵⁰
29	8	0.9	.	-	▽⁰ 12⁰⁶–¹⁷ 18³⁵–19⁰⁵ ●K⁰ 19²⁰–20²⁵ SW–E
30	7	1.6	.	-	●⁰ 9³⁵–12³⁵, = 8¹⁵–12³⁵
31	8	.	.	-	≫ 17²⁰–19³⁰, 21¹⁰–24. = 4²⁰–6³⁰
Σ	–	88.1	–	–	UWAGI.

Sierpień - Août

1	8	.	.	-	≫ 0⁰⁰–3³⁰ (nor. 18 m/sek)
2	8	1.4	.	-	▽⁰ 12¹⁵–²⁷ ▽¹ 14²⁰–⁴³, 15²⁰–³⁵
3	8	.	.	-	= 23²⁵–24
4	8	.	.	-	= 0⁰⁰–1⁴⁰
5	8	.	.	-	
6	8	.	.	-	
7	8	11.6	.	-	▽⁰ 17²⁵–⁴⁵ ▽²– 18⁰⁵ ▽⁰–21¹⁰ ●⁰ 22⁴⁰. K⁰ 17⁴⁵–19¹⁰ SW–SE
8	8	.	.	-	
9	7	.	.	-	
10	6	10.3	.	-	●⁰ 11³⁵–12¹⁵ ●¹–13¹⁰ ●⁰–15⁴⁵ ▽⁰ 20⁴⁵–21⁰⁵ ▽¹–21¹⁵, < 21⁴⁰–22¹⁵ NE. = 22³⁰–24
11	8	.	.	-	= 0⁰⁰–1³⁰
12	8	.	.	-	
13	8	.	.	-	= 22²⁰–24
14	6	1.8	.	-	●⁰ 19⁴⁰–22²⁰. = 0⁰⁰–4²⁰ 8³⁰–16¹⁵
15	7	0.0	.	-	●⁰ 4²⁰–11²⁵. = 0⁰⁰–12²⁵ 20¹⁵–24
16	6	19.3	.	-	●⁰ 11⁴⁰ 15¹⁰ (K) 18⁵⁰–19¹⁰ S ●K⁰–20³⁰ SW–NE ●⁰–24. = 0⁰⁰–3³⁰, 6¹⁰–16³⁵
17	6	5.4	.	-	●⁰ 0⁰⁰–2¹⁵ ●¹–5⁴⁰ ●⁰ 11³⁵ ▽⁰ 13²⁰–16³⁸, 17⁴⁰–24
18	7	1.6	.	-	▽⁰ 0⁰⁰–3²⁵ ●⁰–11⁴⁰, 13³⁷–16²⁰, 18¹⁰–35 ▽⁰ 20⁰⁵–21¹⁵
19	8	.	.	-	▽⁰ 2⁰⁸–⁴⁰ 4²⁰–35
20	8	0.0	.	-	= 4²⁰–6⁴⁰, 19¹⁵–24
21	7	0.6	.	-	▽⁰ 3³⁵–4²⁰, 6⁰⁷–¹⁵ ●⁰ 16¹⁰–17⁴⁰ 21³⁰–23³⁵. = 0⁰⁰–5³⁰, 20²⁰–24
22	7	0.9	.	-	●⁰ 12⁵⁰–13⁰⁵ ▽¹ 13³⁰–⁴⁵ ▽⁰–14⁰⁵. = 0⁰⁰–1²⁰
23	8	0.0	.	-	▽⁰ 5¹⁸–³⁵ 12⁴⁵–13⁴⁰ 14⁴⁰–15³⁵ 16³⁰–⁴⁰
24	7	2.3	.	-	●⁰ 13³⁸ 14⁰⁵–14⁴⁵–20³², ⌒ n–9⁰⁰
25	8	.	.	-	≫ 12¹⁵–17²⁰
26	8	0.0	.	-	▽⁰ 17³⁵–⁴⁷
27	8	0.0	.	-	▽⁰ 3⁰⁷–²⁰ 14⁴⁰–15¹⁰
28	7	11.9	.	-	▽⁰ 14⁰⁴–²⁵ ▽¹ 15³⁶–16²⁰. (K)⁰ 15³⁰–⁴² SW K¹–16³⁵ SW–NE, = 6³⁰–13³⁵, 18¹⁵–24
29	7	.	.	-	= 0⁰⁰–4⁴⁰
30	8	0.5	.	-	▽⁰ 12⁵⁰–13¹⁰ 14⁵⁰–15¹⁰ 15²⁰–⁴⁵ 16¹⁰–⁴⁰
31	7	7.3	.	-	●⁰ 5⁴⁰ 6²⁵, 7³⁰ 8²⁰, 11²⁰ 12²⁵ ●K⁰ 18²⁰–⁴⁰, = 21⁴⁰–24
Σ	–	74.9	–	–	UWAGI.

Gdańsk – Wrzeszcz φ = 54°23' λ = 18°36' Wrzesień – Septembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	110.3	111.0	113.0	111.4	10.2	14.1	12.2	12.2	16.4	8.1	92	71	85	83	0.9	4.6	2.2	2.6	9	9	3	SW 3	W 4	W 4
2	113.4	112.8	112.4	112.9	12.8	19.2	15.2	15.6	19.7	10.5	77	56	76	70	3.4	9.8	4.3	5.8	5	6	10	SW 6	SW 5	S 2
3	110.4	112.0	113.0	112.5	13.6	13.7	11.4	12.9	16.8	10.9	92	84	86	87	1.3	2.5	1.8	1.9	10	10 ●	3	C 0	NW 4	W 3
4	117.6	118.6	119.0	119.1	11.4	17.8	11.4	13.0	18.6	8.6	88	50	83	74	1.7	10.1	2.3	4.7	6	6	0	WSW 2	WSW 5	C 0
5	120.2	117.6	114.2	117.3	11.8	18.2	13.3	14.2	18.3	8.5	76	50	87	71	3.3	10.4	2.0	5.2	2	10	10 ●	WSW 5	SW 6	S 2
6	114.5	115.4	117.2	115.7	12.6	18.5	12.8	14.2	19.5	11.1	88	49	74	70	1.7	10.9	3.9	5.5	9	5	1	WSW 3	WSW 6	W 2
7	118.5	118.6	117.2	118.1	12.8	21.0	16.6	16.8	21.8	8.2	77	46	75	66	3.4	13.6	4.8	7.3	7	7	7	WSW 2	S 2	S 2
8	116.0	116.0	118.4	116.8	15.5	27.0	16.8	19.0	27.5	12.7	84	50	92	75	2.8	17.6	1.6	7.4	6	4	0	S 2	SW 5	C 0
9	116.6	114.9	121.2	117.6	15.0	27.1	14.3	17.7	27.7	13.4	98	52	82	77	0.3	17.2	2.9	6.8	7	5	10	C 0	SW 5	NNW 4
10	121.9	119.9	116.9	119.6	12.2	15.6	11.6	12.8	17.2	11.1	90	80	93	88	1.4	3.5	1.0	2.0	9	7	1	C 0	ENE 3	C 0
11	111.4	106.1	97.4	105.0	10.7	20.1	16.5	16.0	20.5	8.4	92	58	77	76	1.0	9.9	4.4	5.1	7	7	10 ●	C 0	S 7	S 6
12	91.3	90.2	94.3	91.9	15.7	14.4	12.6	13.8	17.4	11.6	89	81	70	80	1.9	3.1	4.4	3.1	9	10 ●	9	S 3	WSW 9	WSW 9
13	99.5	99.4	98.5	99.1	11.0	16.1	9.8	11.7	16.1	9.3	77	54	91	74	3.1	8.4	1.1	4.2	9	6	4	SW 7	SW 8	S 3
14	97.7	98.9	101.5	99.4	9.9	14.6	12.3	12.3	15.2	8.5	86	61	72	73	1.8	6.5	4.0	4.1	9	8	0	SW 7	SW 9	SSW 5
15	102.3	101.4	103.4	102.7	8.0	12.1	11.3	10.7	12.7	6.9	90	81	80	84	1.0	2.7	2.6	2.1	10	10 ●	9	S 3	W 2	WSW 6
16	107.5	111.3	114.0	110.9	10.1	12.2	8.9	10.0	13.0	8.4	82	70	85	79	2.3	4.3	1.7	2.8	7	10	2	WSW 8	SW 9	SSW 1
17	114.7	113.7	112.8	113.7	5.1	13.3	8.1	8.6	14.2	3.9	97	66	89	84	0.3	5.2	1.2	2.2	6	8	5	C 0	SSE 3	NNE 1
18	107.1	106.7	106.2	106.7	10.2	12.1	10.4	10.8	12.6	7.2	91	77	81	83	1.1	3.2	2.4	2.2	9 ●	10	9 ●	NW 6	NNW 9	NNW 9
19	104.7	104.8	104.0	104.5	10.0	11.2	9.2	9.9	11.3	8.8	78	73	88	80	2.7	3.6	1.4	2.6	10	10	10	WNW 6	W 5	NW 5
20	104.6	108.5	112.3	108.5	9.5	11.7	9.2	9.9	13.4	7.9	84	90	92	89	1.9	1.3	0.9	1.4	9	9	0	WNW 5	NW 7	NW 3
21	114.4	115.3	114.6	114.8	8.3	12.3	9.4	9.8	13.0	6.8	84	66	91	80	1.7	4.8	1.1	2.5	9	9	10	WNW 4	NW 5	C 0
22	111.0	108.8	106.8	108.9	8.3	11.9	10.4	10.2	12.3	7.1	94	83	95	91	0.7	2.3	0.5	1.2	10	10 ●	10	C 0	C 0	C 0
23	98.9	96.5	93.8	96.4	14.8	15.5	13.7	14.4	17.6	10.0	93	90	97	93	1.1	1.7	0.6	1.1	9	10 ●	10	SW 3	SW 4	N 6
24	99.9	99.9	98.9	99.5	9.7	10.4	5.4	7.7	13.8	5.1	87	67	84	79	1.6	4.1	1.4	2.4	8	9	9 ●	W 4	NW 6	WNW 12
25	105.0	111.0	114.0	110.1	7.0	8.4	5.4	6.6	8.6	5.0	81	73	87	80	1.9	3.0	1.2	2.0	9	9	1	NW 10	N 8	W 5
26	113.9	113.9	115.9	114.4	5.0	9.4	4.0	5.6	10.1	3.4	79	45	70	65	1.8	6.4	2.4	3.5	7	7	1	WNW 7	N 8	W 5
27	111.9	107.7	99.3	105.0	6.6	8.6	9.6	8.6	9.8	3.5	88	70	93	84	1.1	3.3	0.8	1.7	9	10 ●	9	SW 6	WSW 10	WSW 8
28	95.6	93.3	93.5	97.9	10.1	12.6	9.0	10.2	13.7	8.4	79	67	90	79	2.6	4.9	1.1	2.9	5	7	5	NW 10	NW 10	NW 7
29	98.8	96.7	95.6	97.0	7.4	9.8	7.3	8.0	11.7	5.9	86	70	88	81	1.5	3.6	1.2	2.1	5	9	10	WSW 5	WSW 3	C 0
30	97.9	103.2	109.9	103.7	5.5	7.2	5.0	5.7	10.6	4.2	88	94	81	88	1.1	0.6	1.6	1.1	6	9 ●	3	WNW 5	N 6	WNW 5
31																								
M	108.2	108.3	108.6	108.4	10.4	14.5	10.8	11.6	15.7	8.1	86	67	84	79	1.7	6.1	2.1	3.3	7.7	8.2	5.7	4.1	5.7	3.8

Październik – Octobre

1	111.5	113.1	116.8	113.8	4.6	7.4	4.1	5.0	9.2	3.2	95	72	90	86	0.4	2.9	0.8	1.4	10 ●	5	2	WNW 4	N 7	NW 5
2	120.3	121.0	118.7	120.0	3.0	8.7	6.0	5.9	10.1	2.3	93	55	73	74	0.6	5.0	2.6	2.7	4	8	4	W 3	W 6	SW 6
3	112.1	106.1	100.8	106.3	6.3	7.5	8.7	7.8	9.5	5.3	75	70	80	75	2.4	3.1	2.2	2.6	10	10 ●	10 ●	S 6	SW 9	WSW 9
4	102.9	107.7	113.6	108.1	6.0	7.2	5.9	6.2	8.8	5.3	89	73	73	78	1.1	2.8	2.5	2.1	1	9	3	W 10	NW 9	W 5
5	115.8	115.4	110.8	114.0	6.7	9.9	8.1	8.2	11.5	4.7	81	58	86	75	1.9	5.1	1.5	2.8	9	10	10	W 4	WSW 9	SW 10
6	112.0	116.0	117.5	115.2	10.4	12.2	10.4	10.8	13.5	8.0	91	85	81	86	1.1	2.2	2.4	1.9	10	9	7	W 5	NW 7	WNW 6
7	116.8	118.9	123.1	119.6	12.0	13.2	10.1	11.4	14.4	9.6	87	77	95	86	1.8	3.5	0.7	2.0	10	8	3	W 8	NW 10	C 0
8	127.0	128.2	127.6	127.6	10.3	13.8	12.3	12.2	14.3	8.6	94	73	78	82	0.8	4.2	3.2	2.7	10	9	10	C 0	SW 4	C 0
9	125.4	123.6	122.1	123.7	10.1	16.0	9.7	11.4	16.8	9.2	92	65	95	84	1.0	6.3	0.6	2.6	10	0	0	C 0	S 1	C 0
10	120.4	118.7	117.7	118.9	4.6	19.0	12.4	12.1	20.5	4.2	100	58	87	82	0.0	9.3	1.9	3.7	0 ≡	0	0	C 0	S 3	C 0
11	117.5	118.4	118.6	118.2	10.6	13.5	9.8	10.9	14.0	7.1	95	67	90	84	0.7	5.2	1.3	2.4	10	9	9	W 5	W 3	C 0
12	115.5	117.1	123.6	118.7	8.0	12.2	8.6	9.4	13.3	7.0	97	87	90	91	0.3	1.9	1.1	1.1	9	10 ●	2	WSW 3	W 7	W 4
13	125.2	123.5	120.9	123.2	8.0	13.4	8.8	9.8	14.3	7.2	93	59	92	81	0.7	6.3	0.9	2.6	7	5	5	WSW 3	SW 5	SSW 2
14	119.3	120.7	123.7	121.2	8.3	12.9	6.4	8.5	13.3	5.0	94	65	85	81	0.7	5.3	1.4	2.5	10	6	0	SW 3	W 7	WNW 5
15	125.5	126.3	126.8	126.2	6.0	10.3	8.1	8.1	10.7	4.6	88	58	72	73	1.2	5.3	3.0	3.2	1	9	10	W 5	NW 6	WNW 2
16	125.0	123.5	119.8	122.8	7.4	9.8	6.3	7.4	10.1	5.8	72	65	86	74	2.9	4.2	1.2	2.8	9	9	0	SW 3	S 3	SSE 2
17	112.9	111.6	115.0	113.2	3.8	12.4	8.8	8.4	13.5	2.6	97	80	82	86	0.3	2.9	2.0	1.7	10	9	0	S 5	WSW 5	W 3
18	109.8	104.8	104.0	106.2	7.6	13.3	14.6	12.5	15.3	6.3	90	82	85	86	1.0	2.8	2.5	2.1	9	10	10	SW 2	SW 6	SSW 2
19	102.9	102.9	104.4	103.4	13.8	18.4	13.3	14.7	18.9	12.8	81	66	61	69	3.0	7.2	6.0	5.4	3	8	10	SW 8	SW 8	NW 6
20	108.3	110.9	113.1	110.8	9.4	11.4	7.5	9.0	13.3	7.1	91	72	84	82	1.1	3.8	1.7	2.2	10	10	0	W 2	WSW 4	WSW 2
21	113.6	111.6	108.1	111.1	4.8	9.0	8.0	7.4	10.0	4.4	87	80	85	84	1.1	2.3	1.5	1.6	0	9	10	SW 5	SSW 5	SSW 7
22	103.6	101.7	102.3	102.5	6.2	11.5	7.8	8.3	12.2	5.7	88	67	93	83	1.2	4.6	0.8	2.2	8	8	6	S 7	S 5	S 2
23	103.9	106.3	108.2	106.1	7.1	11.5	6.7	8.0	12.2	6.3	97	70	84	84	0.3	4.1	1.6	2.0	10	7	0	C 0	NW 5	SW 3
24	103.6	107.7	115.6	109.0	7.8	11.7	8.2	9.0	12.4	6.3	89	60	73	74	1.2	5.5	3.0	3.2	10 ●	5	0	SW 9	WNW 9	W 8
25	119.8	122.2	121.9	121.3	5.4	11.2	7.3	7.8	11.6	4.6	86	62	76	75	1.3	5.1	2.5	3.0	2	8	9	W 1	W 6	C 0
26	118.9	119.1	117.7	118.6	10.5	14.0	12.5	12.4	14.5	7.2	88	72	78	79	1.5	4.4	3.2	3.0	10	10	9	WSW 5	WSW 5	W 5
27	114.9	114.7	114.9	114.8	8.2	14.1	10.2	10.7	14.4	7.7	87	65	76	75	1.4	5.9	3.0	3.4	6	5	10	WSW 6	SW 5	WSW 7
28	114.4	113.7	114.1	114.1	8.2	13.0	9.3	10.0	13.3	7.5	90	66	89	82	1.1	5.1	1.3	2.5	3	8	0	SW 5	WSW 6	SSW 3
29	111.9	112.5	113.0	112.5	9.2	13.8	11.8	11.6	14.2	7.4	83	67	80	77	2.0	5.2	2.8	3.3	10	9	10	SW 8	SW 7	SSW 3
30	110.5	109.2	110.3	110.1	8.0	14.2	12.4	11.8	14.7	7.6	89	68	89	82	1.2	5.1	1.6	2.6	3	9	10 ●	SSW 2	SW 8	C 0
31	109.2	106.8	105.3	107.2	12.2	13.3	12.3	12.6	13.6	11.6	92	82	86	87	1.2	2.8	2.0	2.0	10 ●	10	10	WSW 4	WSW 8	SW 6
M	114.9	114.6	115.2	114.8	7.9	12.3	9.2	9.6	13.2	6.5	89	69	83	80	1.2	4.9	2.0	2.6	7.3	7.8	5.5	4.2	6.1	3.6

Gdańsk–Wrzeszcz

$H_s = 13\ m$ $H_b = 12{,}4\ m$ $h_w = 11\ m$

Wrzesień–Septembre 1957

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	●¹14²⁰–5¹⁵ · = 2⁰⁰–6¹⁵ , ⌒¹12⁰⁰–4²⁰
2	7	0.0	.	–	●⁰23³⁵–24
3	8	0.0	.	–	●⁰0⁰⁰–1³⁵ 12⁰⁵–14¹⁰ , = 5³⁰–12⁰⁰
4	8	.	.	–	⌒⁰ n – 7³⁰
5	8	0.9	.	–	●⁰19³⁷–22⁴⁰ , ⌒ n – 9³⁰
6	7	.	.	–	= 5¹⁵–8¹⁵
7	8	.	.	–	= 5²⁰–6³⁰
8	7	.	.	–	= 2¹⁰–10³⁰ , 18²⁰–24
9	7	1.2	.	–	= 0⁰⁰–10⁴⁰ , ⌒ n – 9¹⁰
10	8	0.0	.	–	●⁰5¹⁰ 6⁵⁰ 9³⁰ 10¹⁰
11	7	0.2	.	–	●⁰21³⁵–23⁴⁰ · = 7³⁰–10³⁰ · ⌒ n – 9³⁰
12	7	2.6	.	–	●⁰10⁴⁰ 13²⁰ ●⁰13⁴⁰–50 ●¹–14³⁵ , 17²⁵–35 , ≫ 16²⁵–17²⁵ ≫–17³⁵ (por. 20 m/sek) ≫–21⁴⁰ (por. 17 m/sek)
13	8	1.7	.	–	●⁰15⁰⁵–40 , 23¹⁰–24
14	7	.	.	–	●⁰0⁰⁰–10 , 6⁵⁰–7⁰⁵
15	7	0.2	.	–	●⁰13³⁵ , 16³⁰ , 20¹⁰–21⁴⁰
16	8	.	.	–	
17	7	1.2	.	–	= 5⁴⁰–12²⁰ 19¹⁵–21³⁰ ⌒ n – 9³⁰
18	8	0.2	.	–	●⁰4²⁵–5¹⁰ 6⁴⁰–7⁰⁵ 7⁴²–8¹⁰ , 10³⁵–40 ●¹10⁵⁰–11⁰⁰ , 11⁴⁵–12⁰⁵ ●⁰19⁴⁰–20⁰⁰ , 21⁴⁰–22⁰⁵ , ≫ 14²⁰–20³⁰ (por. 18 m/sek)
19	8	0.0	.	–	●⁰12⁰–40 ●⁰18⁵⁰ 19¹⁵
20	8	5.7	.	–	●⁰9²⁰ 10³⁰ ●⁰11²⁵–40 ●¹13¹⁷–40 ●⁰14¹⁰–15³⁵ , 17²⁰–35 ●¹19¹⁵–37
21	8	.	.	–	= 19¹⁰–24
22	6	6.9	.	–	●⁰13⁴⁰–15³⁵ ●¹16²⁰–17¹⁰ ●⁰–18⁴⁰ , = 0⁰⁰–24
23	6	21.6	.	–	●¹4⁴⁰–5²⁰ ●⁰–6¹⁵ ●¹7⁰⁵–14 ●¹13⁰³–15¹⁵ ●⁰–18²⁰ ●¹–21³⁵ = 0⁰⁰–3⁴⁵ = ¹–4⁴⁰ = 6¹⁵–40
24	8	2.8	.	–	●⁰12⁰⁵–35 17³⁰–40 ●⁰18⁰⁵–25 20¹⁰–30 20³⁵–45 ●⁰21⁰⁵–20 21²⁵–40 ●¹21⁵⁰–22¹⁰ ●⁰22³⁰–45 22⁵⁰–23⁰⁵ , 23¹⁰–15 , 23⁴⁵–24 ,
25	8	.	.	–	●⁰0⁰⁰–05 ●¹0²⁰–10⁵ ●⁰14⁰–21⁰ , 23⁵–3¹⁵ , 3⁴⁰–4¹⁰ 4⁵⁰–5¹⁰ 5⁴⁰–6¹⁵ · ≫ 6⁰⁰–13³⁰ (por. 17 m/sek)
26	8	0.0	.	–	24.IX: ≫ 20¹⁰–24 (por. 17 m/sek)
27	8	11.6	.	–	●⁰6³⁵–7⁰⁶ 7²⁵–37 8⁴⁰–9²⁵ ●⁰13⁰⁵–18⁰⁵ ●¹–21³⁵ · ≫ 12²⁰–14⁴⁰ (por. 16 m/sek) , 23¹⁰–24 (por. 18 m/sek)
28	8	5.7	.	–	●⁰0⁰⁰–2⁵⁰ 4⁵⁰–5⁰⁵ 13¹⁵–20 ●²15⁰⁵–10 ●⁰15³⁰–35 , 16¹⁰–17³⁰ , 19²⁰–40 , 22¹⁰–45 · ≫ 0⁰⁰–17³⁰ (por. 13 m/sek) ; ⌒ 8¹⁵–23
29	8	0.0	.	–	●⁰0⁴⁰–12⁰ , 19³⁵–20⁰⁵
30	8	4.6	.	–	●¹10⁴⁵–11⁰⁰ ●⁰–11⁰⁵ ●¹–11¹⁰ ●⁰11⁵⁰–12⁰⁵ ●¹12¹⁵–13⁰⁰ ●⁰13⁵⁰–14¹⁵ , 18⁴⁵–19²⁰
31					
Σ	–	67.1	–	–	UWAGI

Październik–Octobre

1	8	0.9	.	–	●¹4⁴⁵–5¹⁰ ●⁰6¹⁵–9³⁰ ●⁰18⁴⁵–19²⁰ , 23²⁵–35
2	8	.	.	–	
3	7	0.9	.	–	●⁰11²⁵ 13¹⁰ , 18¹⁵ 21²⁰ = 18¹⁰–21²⁰
4	8	0.0	.	–	●¹0⁴⁰–1¹⁵ ●¹2³⁰–3⁰⁵ 9²⁰–35 , 10³⁵–11²⁰ , 12¹⁶–25 , 13¹⁴–35 , 15⁰²–15 , ≫ 1¹⁵–12³⁵ , 14¹⁰–16²⁰
5	8	0.0	.	–	●⁰7¹⁰–15 ≫ 19¹⁰–24
6	8	0.0	.	–	●⁰0²⁰ 6³⁰ ●⁰8¹⁵–30 , 9¹⁵–25 , 12¹⁵–40 , 15⁴⁵–16⁴⁰ , ≫ 0⁰⁰–2⁴⁰
7	7	.	.	–	≫ 8³⁰–15²⁰ , = 20³⁰–24
8	8	.	.	–	= 0⁰⁰–8²⁰
9	7	.	.	–	= 6¹⁰–10⁴⁰ , 15¹⁵–24
10	7	.	.	–	= 0⁰⁰–3³⁰ , = ¹–7¹⁵ , = – 12³⁰ , 21³⁰–24 · ⌒⁰ n – 9⁰⁰
11	6	0.0	.	–	= 0⁰⁰–24 · ⌒⁰ n – 8⁴⁰ , 23³⁰–24
12	5	0.0	.	–	●⁰5³⁵–6¹⁰ , 8⁰⁴ 13⁰⁵ , = 0⁰⁰–13³⁰ , ⌒¹ 0⁰⁰–5³⁵
13	8	.	.	–	= 22³⁰–24 , ⌒¹ 6²⁰–9²⁰
14	7	.	.	–	= 0⁰⁰–11⁴⁰
15	8	.	.	–	
16	7	.	.	–	= 16²⁵–20²⁰
17	5	0.0	.	–	●⁰11²⁵–30 · = 4¹⁵–7⁴⁵ = ⁰–8⁴⁵ = – 13⁴⁰
18	6	0.3	.	–	●⁰19¹⁵–40 , 21¹⁰–22²⁵ , = 5²⁰–17⁴⁰
19	7	1.4	.	–	●⁰22³⁵–24
20	7	.	.	–	●⁰0⁰⁰–3⁴⁰
21	6	.	.	–	= 8¹⁵–24
22	7	.	.	–	= 0⁰⁰–11²⁵ 16²⁰–20³⁰
23	7	0.2	.	–	= 2³⁰–10²⁰
24	8	0.0	.	–	●⁰4¹⁰ 9²⁵ · ≫ 16²⁰–19⁴⁰
25	7	0.1	.	–	●⁰22⁴⁰–24
26	6	.	.	–	●⁰0⁰⁰–3³⁰ , = 3³⁰–14³⁰ , 16⁴⁰–24
27	6	.	.	–	= 0⁰⁰–10³⁰ ∞ – 15⁴⁵ = – 24
28	7	.	.	–	= 0⁰⁰–10³⁰ ∞ – 11⁴⁰ = 13⁴⁰–17³⁰
29	7	.	.	–	= 1¹⁰–9⁴⁰ 16²⁰–18²⁰
30	6	0.0	.	–	●⁰16³⁰–38 , 20²⁰ 22³⁰ · = 6¹⁰–17²⁰ , 18²⁰–24
31	6	0.8	.	–	●⁰6⁴⁰–7¹⁰ , 13⁴⁰ 15³⁵ , 16⁵⁰ 18⁰⁵ , = 0⁰⁰–19²⁰
Σ	–	4.6	–	–	UWAGI

Gdańsk – Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ Listopad – Novembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	100.3	99.5	103.3	101.0	10.7	12.8	10.0	10.9	13.1	9.5	84	71	86	80	2.1	4.3	1.8	2.7	10	10	0	SSW 5	SW 7	SW 5
2	107.4	108.6	111.4	109.1	6.6	11.8	7.4	8.3	12.0	5.9	82	61	80	74	1.7	5.3	2.1	3.0	1	3	0	SW 5	S 6	SW 4
3	113.4	114.1	113.4	113.6	2.4	10.8	5.4	6.0	11.1	2.0	95	70	91	85	0.4	3.9	0.9	1.7	0	1	3	C 0	S 3	C 0
4	110.5	110.4	110.6	110.5	8.4	10.1	9.5	9.4	11.3	4.4	97	92	96	95	0.3	1.0	0.5	0.6	10	10	9	SW 3	S 5	S 3
5	109.3	106.4	106.3	107.4	7.6	14.2	10.2	10.6	14.7	6.8	99	71	93	88	0.1	4.8	0.8	1.9	10	6	7	S 4	S 5	C 0
6	107.4	107.0	107.9	107.4	8.1	12.9	8.3	9.4	13.4	7.4	91	76	96	88	0.9	3.6	0.5	1.7	6	10	9	S 3	S 4	C 0
7	104.9	103.7	105.3	104.6	9.9	12.5	10.1	10.6	12.6	5.9	91	79	88	86	1.1	3.1	1.5	1.9	10	9	10	S 1	S 5	SW 2
8	107.6	108.5	108.9	108.3	9.0	10.3	9.9	9.8	10.7	8.4	95	86	92	91	0.7	1.7	1.0	1.1	10	8	9	C 0	C 0	SSE 3
9	108.3	108.3	109.8	108.8	8.7	10.2	10.4	9.9	10.4	7.8	92	88	91	90	0.9	1.4	1.1	1.1	10	10	10	C 0	ESE 4	SE 4
10	111.3	112.8	115.9	113.3	9.7	10.2	9.7	9.8	10.6	8.9	95	95	95	94	0.6	0.6	0.8	0.7	10	10 ●	10	SE 3	E 2	ESE 3
11	119.3	121.6	124.8	122.0	8.1	7.9	6.0	7.0	9.9	5.6	95	91	82	89	0.8	0.9	1.8	1.2	10 ●	10	10	E 3	E 7	ESE 7
12	127.6	129.4	130.5	129.2	4.2	2.7	2.1	2.8	6.2	1.8	90	91	87	89	0.8	0.6	0.9	0.8	10	10	10	E 4	E 5	C 0
13	130.5	130.3	130.1	130.2	1.8	4.6	3.7	3.4	4.9	1.3	82	75	80	78	1.3	2.3	1.6	1.7	10	9	9	C 0	C 0	C 0
14	129.6	130.4	131.3	130.4	3.5	4.6	4.2	4.1	4.8	2.3	78	71	80	76	1.7	2.5	1.6	1.9	9	10	10	WNW 2	NW 4	W 2
15	131.9	130.9	130.2	130.9	1.6	1.2	−0.8	0.3	4.4	−1.2	76	77	85	79	1.7	1.5	0.9	1.4	10	9	9	SSW 3	SW 1	WSW 3
16	129.4	130.6	132.0	130.7	0.4	2.4	3.0	2.2	3.2	−1.0	90	79	83	84	0.6	1.6	1.3	1.2	10 ●	10	10	WSW 2	WSW 3	C 0
17	133.0	132.8	134.4	133.4	3.0	5.7	3.0	3.7	5.9	2.5	88	74	81	81	0.9	2.4	1.5	1.6	10 ●	10	10	C 0	C 0	C 0
18	133.8	133.1	132.5	133.1	1.9	3.4	2.5	2.6	3.7	1.3	80	60	67	69	1.4	3.1	2.4	2.3	10	10	10	C 0	S 5	C 0
19	135.5	135.7	138.5	135.9	2.3	4.0	2.0	2.6	4.0	−1.9	70	66	82	73	2.2	2.8	1.3	2.1	10	9	10	C 0	SSE 2	C 0
20	139.8	139.6	138.8	139.4	1.6	3.7	0.0	1.3	3.8	−0.4	85	60	86	77	1.1	3.2	0.9	1.7	10	10	0	C 0	S 3	C 0
21	136.7	134.8	129.7	133.7	−0.6	4.0	0.4	1.0	4.4	−3.5	87	61	84	77	0.7	3.2	1.0	1.6	7	1	0	C 0	SW 3	C 0
22	120.3	116.5	114.3	117.0	−3.0	2.2	1.2	0.4	2.9	−4.3	93	78	90	87	0.4	1.6	0.7	0.9	0	0	10 ●	SSW 3	SW 4	SW 5
23	111.4	110.6	112.9	111.6	0.8	2.0	3.3	2.4	3.5	0.4	85	89	91	88	1.0	0.8	0.6	0.8	10	10	3	SW 3	SW 2	NNW 7
24	115.8	112.9	112.4	113.7	2.4	6.2	6.6	5.4	6.8	1.3	84	85	93	87	1.2	1.5	0.7	1.1	10	10	10 ●	W 5	W 9	NNW 6
25	110.7	112.3	115.0	112.7	7.7	8.9	7.8	8.0	9.3	6.4	94	93	99	95	0.6	0.8	0.2	0.5	10 ●	10	10 ●	NW 6	NW 5	WNW 2
26	116.7	115.9	112.2	114.9	7.6	8.3	7.4	7.7	9.0	6.9	96	96	86	93	0.4	0.5	1.5	0.8	10 ●	10 ●	10 ●	NW 1	W 2	W 9
27	106.5	109.7	112.7	109.6	8.6	8.1	6.7	7.5	8.7	6.2	81	78	91	83	2.2	2.4	0.9	1.8	10	10	9	WNW 12	NW 9	C 0
28	106.4	102.7	98.6	102.6	8.3	8.4	7.2	7.8	9.0	5.7	92	89	84	88	1.0	1.2	1.7	1.3	10 ●	10 ●	10 ●	W 6	NW 8	NW 12
29	107.2	116.1	127.7	117.0	0.2	−1.1	−2.2	−1.3	7.4	−2.5	86	79	62	76	0.9	1.2	2.0	1.4	10 ✳	9 ⁂	9 ✳	N 14	NE 17	NE 12
30	130.7	131.5	131.2	131.1	−0.6	−0.4	−0.1	−0.3	0.3	−3.5	60	64	67	64	2.3	2.1	2.0	2.1	8 ✳	8	9	NE 7	ENE 9	NE 6
31																								
M	118.4	118.6	119.4	118.8	4.7	6.8	5.2	5.5	7.7	3.0	87	78	86	84	1.1	2.2	1.2	1.5	8.7	8.4	7.8	3.2	4.6	3.2

Grudzień – Décembre

1	127.1	122.8	123.2	124.4	−1.6	0.4	1.6	0.5	1.9	−3.1	71	88	96	85	1.5	0.8	0.3	0.9	10	10 ✳	10	W 4	WSW 7	C 0
2	125.0	125.7	125.8	125.5	2.7	4.2	4.0	3.7	4.8	1.6	98	100	97	98	0.1	0.0	0.2	0.1	10 ●	10 ●	10	C 0	C 0	C 0
3	122.0	121.3	122.4	121.9	4.2	6.0	5.8	5.4	7.1	3.1	93	91	91	92	0.5	0.9	0.8	0.7	10	9	10	W 5	NW 7	ENE 2
4	120.9	118.5	113.9	117.8	4.2	3.8	5.8	4.9	6.2	2.9	98	88	91	92	0.1	0.9	0.8	0.6	10	10	10 ●	C 0	SW 4	WNW 7
5	112.6	114.7	120.3	115.9	6.3	7.2	4.6	5.8	8.1	4.3	84	71	81	79	1.5	2.9	1.7	2.0	3	2	9 ●	WNW 7	NW 9	N 9
6	124.7	124.2	119.6	122.8	3.4	4.8	0.8	2.4	5.8	0.0	88	75	88	84	0.9	2.2	0.8	1.3	9	8	4	C 0	C 0	SSW 3
7	110.7	107.4	101.2	106.4	1.2	2.4	1.7	1.8	2.8	−0.3	85	87	89	87	1.1	1.0	0.8	1.0	10	10	10	SW 7	SW 2	SW 5
8	86.4	76.0	67.3	76.6	0.7	2.4	7.4	4.5	8.3	0.3	88	93	83	88	0.7	0.6	1.8	1.0	10 ✳	10 ●	1	S 5	SSW 7	W 10
9	66.9	80.3	89.7	79.0	3.6	0.1	−2.3	−0.2	7.6	−3.1	90	81	64	78	0.8	1.2	1.9	1.3	10 ●	9 ⁂	0	N 10	NNW 9	W 6
10	91.8	94.0	99.2	95.0	−1.7	−3.0	−2.7	−2.5	−0.6	−4.6	90	60	69	75	0.6	2.0	1.5	1.4	10 ✳	9	2	NW 7	WNW 5	W 7
11	104.0	106.2	105.9	105.4	−2.0	−1.2	−3.2	−2.4	−0.5	−3.9	64	47	81	64	1.9	3.0	0.9	1.9	7	8	9	W 8	WSW 5	C 0
12	101.9	100.7	99.2	100.6	−0.6	−0.8	−0.4	−0.6	0.0	−6.5	62	67	86	72	2.2	1.9	0.8	1.6	10	10	10	SE 5	ESE 4	ESE 2
13	96.0	92.5	86.9	91.8	−1.2	2.1	2.4	1.4	2.8	−1.9	99	93	96	96	0.1	0.5	0.3	0.3	10 ≡	10	10	SE 2	E 1	E 4
14	87.1	93.7	105.5	95.4	0.1	0.8	−0.2	0.1	2.8	−0.5	90	92	72	85	0.7	0.5	1.7	1.0	10 ✳	10 ⁂	2	NE 9	NE 17	NE 14
15	117.3	123.3	127.3	122.6	−0.8	−4.8	−5.5	−4.2	1.1	−7.3	56	78	70	68	2.6	0.9	1.2	1.6	9	6	4	ENE 9	S 2	S 2
16	127.9	129.1	128.5	128.5	−5.1	−3.4	−7.0	−5.6	−1.7	−7.6	51	50	72	58	2.0	2.4	1.0	1.8	0	3	0	SW 5	SW 2	SW 1
17	125.0	122.3	121.4	122.9	−10.3	−4.0	−7.0	−7.1	−3.5	−11.2	84	80	74	79	0.4	0.9	0.9	0.7	0	2	6	S 1	S 3	S 3
18	122.0	122.4	123.1	122.5	−7.5	−4.8	−8.4	−7.3	−2.5	−9.7	79	91	92	87	0.7	0.4	0.3	0.5	0	0	0	SW 3	C 0	SW 1
19	124.6	126.2	127.8	126.2	−5.0	−4.1	−3.6	−4.1	−3.4	−9.6	90	87	85	87	0.4	0.6	0.7	0.6	9	10	10	SW 2	SSE 1	SW 3
20	127.6	126.8	124.0	126.1	−1.1	1.8	1.4	0.9	2.2	−4.0	85	85	85	85	0.9	1.1	1.0	1.0	10	4	0	S 1	SW 6	SW 3
21	118.2	117.8	122.0	119.3	2.7	4.6	4.4	4.0	5.2	1.0	86	79	84	83	1.0	1.8	1.4	1.4	10	9	0	S 7	WSW 10	W 3
22	121.7	121.9	121.6	121.7	2.7	4.0	3.6	3.5	4.5	2.1	84	87	93	88	1.2	1.1	0.5	0.9	5	9	10	SW 1	WSW 1	SW 2
23	120.3	116.8	115.0	117.4	1.6	2.0	−1.1	0.4	4.4	−1.5	100	85	81	89	0.0	1.1	1.1	0.7	10	9	0	S 2	S 8	SW 5
24	113.2	113.8	115.6	114.2	−1.8	1.2	0.8	0.2	2.3	−2.9	79	89	75	81	1.1	0.8	1.6	1.2	9	10	10	SSW 3	C 0	SSW 3
25	115.1	113.6	115.1	114.6	−1.4	2.3	1.1	0.8	3.2	−2.7	84	79	77	80	0.9	1.5	1.5	1.3	8	10 ●	5	S 4	S 3	C 0
26	116.9	119.0	120.7	118.9	2.9	3.6	4.2	3.7	4.4	0.6	85	90	88	87	1.3	0.8	0.9	1.0	10	10	10	WSW 4	W 7	W 7
27	120.0	118.7	116.6	118.4	3.6	3.7	3.9	3.8	4.5	2.9	90	88	92	90	0.8	1.0	0.7	0.8	10	10	8	W 7	SW 5	WSW 8
28	111.0	107.-	103.6	107.3	4.7	5.2	4.6	4.8	5.5	3.2	82	83	87	84	1.5	1.5	1.1	1.4	10	9	10	SW 5	WSW 8	WSW 5
29	100.0	100.2	92.3	97.5	3.0	3.4	2.7	3.0	4.8	2.4	84	76	89	83	1.2	1.9	0.8	1.3	9	7	10 ●	WSW 9	W 8	SW 8
30	88.6	89.3	89.4	89.1	3.1	1.9	0.8	1.6	5.0	0.2	74	91	92	86	1.9	0.6	0.5	1.0	3	10 ⁂	10 ✳	WSW 14	W 7	C 0
31	92.5	94.1	94.2	93.6	0.7	1.1	0.1	0.5	1.8	−0.5	83	85	98	89	1.1	1.0	0.2	0.8	3	9 ✳	9 ✳	W 6	WSW 7	W 7
M	110.9	111.0	110.9	110.9	0.4	1.4	0.7	0.8	3.1	−1.9	85	82	84	83	1.0	1.2	1.0	1.1	7.9	8.1	6.4	4.9	4.9	4.3

Gdańsk – Wrzeszcz

$H_s = 13$ m $H_b = 12{,}4$ m $h_w = 11$ m

Listopad – Novembre 1957

DNI	WIELKOŚĆ OPADU	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	.	–	= 6^20 – 18^10
2	7	.	.	–	= 5^20 – 8^20
3	6	.	.	–	= 6^20 – 7^40, 8^25 – 24; ⌴ 5^40 – 7^30
4	5	.	.	–	= 0^00 – 24
5	6	.	.	–	= 0^00 – 24
6	6	.	.	–	= 0^00 – 24
7	6	0.5	.	–	= 0^00 – 24
8	5	0.0	.	–	•^0 1^10 – 2^35, 3^20 – 5^40, 18^40 – 20^40; = 0^00 – 8^30 ≡^0 – 9^40 = – 24
9	6	.	.	–	= 0^00 – 20^30
10	6	0.1	.	–	•^0 11^10 – 16^20; = 6^20 – 19^30
11	7	0.0	.	–	•^0 4^10 – 7^25; = 7^25 – 8^45
12	7	.	.	–	= 20^20 – 24
13	7	.	.	–	= 0^00 – 1^30, 6^10 – 9^30
14	7	.	.	–	
15	7	0.0	.	–	= 15^30 – 24
16	6	0.0	.	–	•^0 5^30 – 8^10 = 0^00 – 24
17	6	0.0	.	–	•^0 2^20 – 3^15 •^0 6^10 – 9^20; = 0^00 – 24
18	7	.	.	–	= 0^00 – 8^40
19	7	.	.	–	= 7^10 – 8^30 ∞ – 12^20 = 15^25 – 24
20	7	.	.	–	= 0^00 – 10^40, ⌴ 21^20 – 24
21	6	.	.	–	= 6^20 – 10^40, ∞ – 15^30 ≡ – 24; ⌴ 0^00 – 8^45
22	6	0.0	.	–	•^0 20^20 – 22^30; = 0^00 – 24; ⌴ n – 9^40
23	6	0.2	.	–	*^0 7^25 – 10^40 •^0 15^10 – 17^10 ▽^0 17^35 – 18^10, 18^45 – 19^05, 21^10-20, 21^50 – 22^10; = 0^00 – 17^10
24	7	0.7	.	–	•^0 8^40 – 11^35, 13^38 – 14^10, 15^35 – 17^40 •^0 – 24; ≫ 11^30 – 13^40
25	7	0.3	.	–	•^0 0^00 – 8^20 •^0 8^50, 10^20, 15^40 – 16^10, 18^45 – 23^20 •^2 – 24
26	6	0.0	.	–	•^2 0^00 – 1^40 •^0 – 2^35, 6^20 – 11^30, 12^40 – 24; ≫ 23^15 – 24
27	7	2.4	.	–	•^0 0^00-25 •^0 7^20 – 8^25, 23^35 – 24; ≫ 0^00 – 12^35 (por. 17 m/sek)
28	6	3.9	.	–	•^0 0^00 – 9^25, 11^32 – 18^35 •^1 – 19^20 •^0 24; ≫ 19^30 – 24 (por. 18 m/sek); = 9^25 – 11^20
29	7	1.1	.	–	•^0 0^00 3^35 *^0 5^28, 6^05 *^0 6^10, 8^30 ▽^0 8^50, 9^10 △^0 9^45, 10^10, 11^35, 12^10, 12^20, 13^20, 13^40 – 14^10 *^0 14^40 – 16^30, 19^10-40, 20^20 – 21^20, 21^30 – 45
30	8	0.0	2	–	*^0 0^15-40, 1^10 – 3^25, 6^30 – 7^05, 7^30-50, 8^05-35, 12^02-40, 13^05-50, 14^40 – 15^45; ≫ 0^00 – 1^30 (por. 16 m/sek)
31					29.XI: ≫ 0^00 – 9^20 (por. 18 m/sek) ⩓ – 18^30 (por. 25 m/sek) ≫ – 24
Σ	–	9.2	–	–	UWAGI

Grudzień – Décembre

1	5	0.0	2	–	*^0 9^15 – 10^35 *^1 – 11^20 *^0 – 14^50 •^0 17^40 – 18^15
2	5	1.7	.	–	•^0 5^10 – 8^15 •^1 9^20 – 11^15, 12^20 – 15^20; = 8^15 – 18^45
3	7	0.0	.	–	= 7^10 – 11^20, 15^20 – 19^30, 22^30 – 24
4	6	0.0	.	–	•^0 5^25 – 6^20, 15^40 – 16^10 •^0 – 17^50 •^0 19^15, 22^45, 23^50 – 24; ≫ 21^40 – 24; = 0^00 – 9^35, 12^30 – 23^30
5	8	0.0	.	–	•^0 0^00 – 1^50 ▽^0 20^42 – 21^15, 23^35 – 24; ≫ 0^00 – 3^30, 7^20 – 11^35
6	7	.	.	–	▽^0 0^00 – 1^40; = 15^20 – 24
7	6	0.0	.	–	= 0^00 – 24
8	6	2.3	.	–	*^0 6^35 – 7^15 •^0 11^15 – 16^45 •^0 – 17^30 •^0 – 19^25; ≫ 20^15 – 24; = 0^00 – 18^45
9	7	3.0	.	–	•^0 2^25-40, 3^35 5^30, 6^40, 9^05 •^1 – 11^15 ▽^0 12^40 – 13^10, 13^25-50 ▽^0 14^05-15, 14^40 – 15^10, 15^35 – 16^40 *^0 21^10-50 *^0 22^20 – 23^20, 23^40 – 24
10	8	0.0	6	–	▽^0 0^00 – 7^10 *^1 – 7^25 ▽^0 8^45 – 9^05, 13^45 – 14^05 — 9.XII: ≫ 0^00 – 2^15, 5^35 – 16^30
11	8	.	5	–	⊣ 0^15 – 6^20; ≫ 0^15 – 6^20; = 14^30 – 21^40
12	7	.	4	–	
13	6	3.8	3	–	= 2^30 – 5^40 ≡^0 – 7^30 ≡ – 24
14	7	3.0	3	–	•^0 1^35 – 5^05 •^1 – 5^35 *^1 – 9^20 *^0 10^25 – 12^45 •^0 – 13^30; ≫ 6^50 – 9^35 ⩓ – 20^10 ≫ – 23^00 ⩓ – 24; = 0^00 – 1^25
15	7	.	3	–	⩓ 0^00 – 1^45 (por. 22 m/sek) ≫ – 5^30; = 9^10 – 12^20
16	8	.	2	–	
17	6	.	2	–	= 7^30 – 24
18	4	.	2	–	= 0^00 – 1^20, 6^40 – 24
19	5	.	2	–	= 0^00 – 1^40, 4^30 – 24
20	6	.	2	–	= 0^00 – 24
21	7	0.0	2	–	•^0 14^25 – 16^40 •^0 17^20 – 18^35; ≫ 12^45 – 15^30 (por. 16 m/sek); = 0^00 – 10^40
22	6	.	pł.	–	= 7^30 – 24
23	6	.	.	–	= 0^00 – 7^20 ≡^1 – 7^50 ≡^2 – 8^20 ≡^1 – 10^40 = – 19^30
24	6	.	.	–	= 7^35 – 20^40
25	6	0.0	.	–	•^0 12^25 – 14^10; = 8^15 – 18^30
26	6	0.0	.	–	•^0 10^30 – 11^25; = 0^10 – 18^45, 20^30 – 24
27	6	.		–	≫ 17^50 – 19^30; = 0^00 – 24
28	6	0.1		.	•^0 14^20-45 15^00, 19^40; = 0^00 – 23^30
29	8	2.3	.	–	•^0 3^33 – 4^47 ▽^0 8^25-55, 9^05 – 10^25 •^0 20^20 – 24
30	6	9.2	.	–	•^0 0^00, 1^20 ▽^0 3^15, 4^38 – 5^05 ▽^1 8^15-40 ▽^0 11^46 – 12^06, 12^20 – 13^05 ▽^0 – 13^46 *^0 14^15 •^0 – 15^05 ▽^0 17^30-41 *^0 20^25 – 21^40, ≫ 0^10 – 1^40
31	6	3.2	2	–	▽^0 1^51 – 2^10 ▽^1 3^35, 4^07, 7^44 – 8^06 ▽^1 8^15-28, 9^16, 14^10, 18^23 – 21^15 (por. 19 m/sek)
Σ	–	28.6	–	–	UWAGI

Suwałki — φ = 54°06' — λ = 22°57' — Styczeń – Janvier 1957

DNI	CIŚNIENIE p − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	100.7	99.6	99.0	99.8	-10.8	-10.0	-7.8	-9.1	-7.8	-12.3	76	87	93	85	0.6	0.4	0.2	0.4	10	10 ✳	10 ✳	SE 12	SE 8	SE 5
2	98.2	96.9	95.5	96.9	-6.0	-5.0	-2.6	-4.0	-2.3	-7.8	94	93	93	93	0.2	0.3	0.3	0.3	10	10	10	SE 4	SE 7	SE 6
3	97.9	101.2	102.5	100.5	0.1	-1.1	-1.6	-1.0	0.6	-2.6	96	95	98	96	0.3	0.3	0.1	0.2	10	10	10 ✳	WSW 4	W 2	E 2
4	102.8	104.2	104.7	103.9	-0.8	0.1	0.3	0.0	0.7	-1.8	100	98	96	98	0.0	0.2	0.2	0.1	10 ≡	10	10	C 0	SSW 1	SSE 3
5	102.4	97.4	88.9	96.2	-0.2	-1.4	1.1	0.2	1.4	-1.8	94	98	96	96	0.4	0.1	0.2	0.2	10	10	10 ●	SSW 3	SSW 10	SW 9
6	84.9	80.5	79.6	81.7	2.5	5.4	3.1	3.5	6.6	1.1	100	98	73	90	0.0	0.2	2.1	0.8	10 ≡●	10	10	SW 6	WSW 5	W 12
7	82.3	88.2	95.9	88.8	1.1	1.7	1.3	1.4	3.2	0.3	92	85	83	87	0.5	1.0	1.1	0.9	10 ●	10 ✳	8	WNW 8	WNW 9	NW 10
8	99.9	97.1	95.0	97.3	1.7	2.6	4.0	3.1	4.3	0.1	92	98	98	96	0.5	0.2	0.1	0.3	10	10	10 ●	WSW 5	WSW 6	W 6
9	93.2	92.2	90.2	91.9	6.0	6.5	5.9	6.1	7.0	3.9	98	82	85	88	0.2	1.7	1.4	1.1	10 ●	10	10	W 6	W 6	W 8
10	86.2	83.9	84.3	84.8	4.1	3.5	0.7	2.8	6.1	0.5	77	73	88	79	1.9	3.1	0.7	1.6	6	10	9 ✳	WNW 7	W 10	W 8
11	87.0	90.4	91.2	89.5	-0.4	0.2	-0.1	-0.1	1.0	-1.4	94	82	88	88	0.3	1.1	0.8	0.7	6	2 ⊙	9	W 4	NW 4	WNW 6
12	88.2	85.5	81.1	84.9	-0.8	-0.9	-1.6	-1.2	0.2	-2.3	87	87	96	90	0.7	0.7	0.2	0.5	10	10 ⊙	10 ✳	WNW 6	W 6	SSE 1
13	89.8	88.2	95.9	89.3	-2.4	-4.9	-8.8	-6.2	-1.0	-9.0	98	90	83	90	0.1	0.4	0.5	0.3	10 ✳	10 ✳	10	ENE 4	ENE 9	ENE 12
14	102.8	107.1	111.0	107.0	-11.7	-8.4	-11.0	-10.5	-8.1	-12.5	78	66	90	78	0.5	1.1	0.3	0.6	2	0 ⊙	0	ENE 9	ENE 8	NE 4
15	110.9	109.3	107.2	109.1	-7.8	-9.8	-14.0	-11.4	-7.8	-14.6	81	81	92	85	0.6	0.5	0.2	0.4	10 ✳	2 ⊙	0	ESE 4	ESE 3	E 1
16	108.3	108.5	108.3	108.4	-17.8	-10.4	-10.0	-12.0	-9.2	-18.4	90	80	91	87	0.2	0.5	0.3	0.3	0	5 ⊙	8	C 0	SW 1	W 4
17	105.9	105.4	105.5	105.6	-5.8	0.1	0.1	-1.4	0.7	-10.1	95	94	92	94	0.2	0.4	0.5	0.4	10 ✳	10	10	W 5	W 5	NW 5
18	101.9	101.1	101.2	101.4	0.3	0.9	0.1	0.4	1.2	-1.6	94	88	88	90	0.3	0.7	0.8	0.6	10	9	10	WNW 8	NW 8	WNW 7
19	101.7	103.4	105.7	103.6	-1.2	0.1	-0.8	-0.7	0.4	-1.5	91	88	93	91	0.5	0.8	0.4	0.6	10	6 ⊙	10	NW 5	WNW 9	W 5
20	103.5	101.5	98.0	101.0	-2.9	-0.3	-0.8	-1.2	0.0	-3.4	95	94	93	94	0.2	0.4	0.4	0.3	10	10	10	SW 7	WSW 7	WSW 9
21	93.7	94.5	97.9	95.4	-4.2	-2.2	-1.8	-2.5	-0.4	-4.8	91	83	98	91	0.4	0.9	0.1	0.5	9	10	10	WNW 8	WSW 10	W 8
22	98.6	98.4	96.5	97.8	-1.9	-1.8	-7.0	-4.4	-1.1	-7.4	100	98	80	93	0.0	0.1	0.7	0.3	10●≡	9	0	SW 6	SW 5	SW 5
23	94.6	95.6	98.1	96.4	-10.0	-5.6	-3.4	-5.6	-3.1	-10.4	91	95	90	92	0.3	0.2	0.5	0.3	0	10	10	WSW 5	SW 4	SW 3
24	97.9	97.0	93.8	96.2	-6.8	-3.0	-2.2	-3.6	-1.7	-9.1	94	95	91	93	0.2	0.3	0.5	0.3	4	10 ✳	10	C 0	ESE 3	ESE 5
25	90.3	89.0	90.4	89.9	-4.0	-3.2	-2.3	-3.0	-1.9	-4.2	91	90	96	92	0.4	0.5	0.3	0.4	10 ✳	10 ✳	10	SE 6	SE 4	SW 3
26	94.5	97.0	98.0	96.5	-3.4	-1.3	-1.6	-2.0	0.6	-3.6	94	97	96	96	0.3	0.2	0.2	0.2	10	10 ✳	10	SW 4	SW 3	SW 3
27	90.8	88.6	91.4	90.3	-1.4	0.7	1.3	0.5	2.2	-2.7	92	98	87	92	0.4	0.1	0.9	0.5	10 ✳	10 ✳	0	S 5	W 4	W 6
28	94.4	97.9	103.6	98.6	-2.0	0.5	0.7	0.0	1.7	-2.7	94	88	75	86	0.4	0.7	1.6	0.9	4	8 ⊙	10	WSW 5	WSW 4	WNW 6
29	107.0	107.2	105.9	106.7	0.7	0.3	-0.2	0.2	1.2	-0.5	85	84	96	88	1.0	0.9	0.2	0.7	10	10	10 ✳	W 3	SW 4	SW 3
30	102.5	101.4	100.7	101.5	0.2	0.8	-0.2	0.2	1.0	-0.7	98	98	100	99	0.1	0.2	0.0	0.1	10 ●	10	10 ≡	WSW 1	SW 3	SSW 2
31	101.7	103.6	104.8	103.4	-2.2	0.1	-0.2	-0.6	0.8	-3.4	98	94	98	97	0.1	0.4	0.1	0.2	4	9	10	SSE 2	SE 3	SE 3
M	97.0	97.2	97.5	97.2	-2.8	-1.5	-1.9	-2.0	-0.1	-4.7	92	90	91	91	0.4	0.6	0.5	0.5	8.2	8.7	8.5	4.9	5.6	5.5

Luty – Février

1	101.9	100.5	98.7	100.4	-0.6	0.1	0.3	0.0	0.5	-1.5	95	88	84	89	0.3	0.8	0.9	0.7	10	10	10	SE 7	SE 8	SSE 10
2	94.6	97.2	101.4	97.7	1.3	5.8	2.5	3.0	6.0	0.0	96	73	82	84	0.2	2.5	1.3	1.3	10 ●	5 ⊙	6	SW 10	WSW 7	W 4
3	103.1	103.1	105.0	103.7	-0.7	1.9	0.6	0.6	2.6	-1.1	96	93	94	94	0.2	0.5	0.4	0.4	6	9 ⊙	8	W 2	W 3	W 4
4	106.8	106.2	100.9	104.6	-1.4	-1.2	-0.2	-0.8	1.0	-1.7	93	96	98	96	0.3	0.2	0.1	0.2	10	10	10 ●	SSW 3	SSW 5	SSW 5
5	98.2	99.0	97.4	98.4	1.0	2.5	1.1	1.4	2.7	-0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 4	SW 2	SW 4
6	95.3	93.3	89.6	92.7	0.1	0.9	2.1	1.0	2.7	-0.4	100	100	95	98	0.0	0.0	0.4	0.1	10 ≡	10 ≡	0	SW 3	SW 3	SW 5
7	88.2	89.1	86.7	88.0	2.2	4.2	4.1	3.6	4.8	1.3	100	86	71	86	0.0	0.9	2.4	1.1	10	9 ⊙	10 ●	WSW 5	WSW 5	W 10
8	89.7	88.3	83.0	87.0	2.1	3.2	2.7	2.7	4.6	1.6	82	84	95	87	1.3	1.2	0.4	1.0	10	10	10 ●	W 6	WSW 7	SSW 4
9	76.8	76.2	76.7	76.6	4.1	5.9	4.9	5.0	6.5	2.5	98	94	87	93	0.2	0.6	1.1	0.6	10 ●	10	9	WSW 5	WSW 6	W 7
10	76.7	81.1	85.0	80.9	2.1	0.9	1.0	1.2	5.0	0.3	93	85	96	91	0.5	1.0	0.3	0.6	10	10	10 ●	W 8	WNW 8	NW 2
11	86.7	86.6	87.7	87.0	0.1	3.5	0.5	1.2	4.1	-0.7	100	86	92	93	0.0	1.0	0.5	0.5	10 ≡	9 ⊙	10 ●	W 1	SSE 3	WNW 5
12	89.5	91.3	89.9	90.2	0.1	0.9	0.1	0.3	1.8	-0.2	88	70	84	81	0.8	2.0	1.0	1.3	10	10	10	WNW 3	WNW 1	SE 3
13	93.7	81.0	77.0	80.6	0.7	1.3	2.3	1.6	2.9	-0.3	88	94	96	93	0.7	0.4	0.3	0.5	8	10 ●	9	SSE 6	SSE 5	SSE 6
14	71.1	70.1	70.6	70.6	1.1	4.0	3.9	3.2	5.2	0.4	92	92	95	93	0.5	0.6	0.4	0.5	10 ●	10	10 ●	SE 5	SE 8	SE 6
15	69.5	71.3	70.1	70.3	3.3	4.1	1.7	2.7	5.2	0.5	95	87	92	91	0.4	1.1	0.5	0.7	10	9 ⊙	10	SW 3	SSW 4	SE 3
16	66.6	69.2	76.4	70.7	4.3	4.7	2.5	3.5	5.4	1.6	97	90	93	93	0.3	0.8	0.5	0.5	10 ●	10 ●	10	SSW 4	WSW 5	WSW 4
17	82.2	84.6	87.3	84.7	0.1	1.7	1.1	1.0	2.8	-0.3	96	87	89	91	0.3	0.9	0.7	0.6	10	9	10	WSW 3	SW 6	SW 2
18	86.7	88.9	85.3	87.0	0.7	1.3	1.7	1.4	3.7	-1.4	96	89	90	92	0.2	0.8	0.6	0.5	10	10	10	SW 3	SSW 4	E 3
19	74.5	73.5	83.1	77.0	3.5	5.1	0.7	2.5	5.2	0.1	93	94	83	90	0.5	0.6	1.1	0.7	10	10 ●	10	ESE 8	SSW 3	W 10
20	90.3	92.0	92.2	91.5	-0.4	0.4	0.3	0.2	1.7	-0.6	84	94	96	91	0.9	0.4	0.2	0.5	4	10	10 ✳	W 6	S 4	SE 2
21	89.9	89.3	90.0	89.7	-0.4	4.9	1.3	1.8	6.0	-0.7	98	81	89	89	0.1	1.7	0.8	0.9	10	2 ⊙	0	SE 1	SE 3	SE 1
22	90.8	91.3	91.5	91.2	1.2	1.6	-0.3	0.6	1.9	-0.5	98	81	84	88	0.2	1.3	1.0	0.8	10 ●	10	10	SW 2	NW 5	NW 6
23	91.5	91.6	91.1	91.4	-1.6	-0.2	-1.2	-1.0	1.6	-1.9	86	76	91	84	0.7	1.4	0.5	0.9	8	6 ⊙	4	NW 3	NW 3	NW 1
24	89.3	87.2	86.9	87.8	-3.0	-0.4	-3.2	-2.4	1.2	-4.9	97	72	95	88	0.1	1.6	0.2	0.6	10 ✳	8 ⊙	10	S 1	SE 3	E 2
25	87.6	88.5	89.0	88.4	-4.4	-1.3	-1.6	-2.2	-0.8	-4.7	96	99	96	97	0.2	0.1	0.2	0.2	10 ✳	10 ✳	10 ✳	E 2	E 3	ENE 2
26	91.9	95.5	99.9	95.8	-3.4	-2.8	-3.2	-3.2	-1.1	-3.6	97	91	86	91	0.2	0.5	0.7	0.5	10 ✳	10	10	NE 2	NE 5	NE 1
27	103.0	104.7	105.9	104.5	-6.6	-4.0	-7.7	-6.5	-3.1	-7.9	86	77	81	81	0.5	1.0	0.6	0.7	10	10	0	NE 2	ESE 1	N 2
28	107.8	109.4	111.2	109.5	-7.6	-3.3	-5.0	-5.2	-2.4	-9.2	90	68	78	79	0.3	1.6	0.9	0.9	6 ⊙	8 ⊙	0	NNE 2	N 4	N 3
29																								
30																								
31																								
M	88.7	89.3	89.6	89.2	-0.1	1.6	0.5	0.6	2.8	-1.2	94	87	90	90	0.4	0.9	0.6	0.6	9.4	9.1	8.1	3.9	4.4	4.2

Suwałki $H_s = 165\ m$ $H_b = 169{,}2\ m$ $h_w = 12\ m$ **Styczeń – Janvier 1957**

DNI	WYDZIAŁ NOŚCI V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	F O G O D A
1	6	1.9	9	.	⚹ 4 15–35 ✳ 0 945–24
2	7	0.2	9	.	✳ 0 000–610 1820–2010 · = 1950–2120
3	6	3.0	15	.	● 0 315–510 ✳ 0–620 ✳ 1 1705–2110 ✳ 0–24 · = 230–24
4	4	.	17	.	✳ 0 000–715 · = 000–330 ≡ 1–1035 = –1115 ≡ 0–1210 = –24
5	5	4.6	16	.	● 0 1605–24 · = 000–230 ≡ 1–445 = –24
6	7	10.0	8	.	● 0 000–25 635–1210 2220–24 · = 000–615 ≡ 1–740 = –1210
7	6	0.6	pż.	.	● 0 000–210 ✱ 0–315 ● 0–720 ⚹ 815–50 ⚹ 1010–45 1125–1305 △ 0 1320–1510
8	5	0.9	pż.	.	● 0 720–1210 1420–1915 ● 0–24 · = 1015–1325 ≡ 1–1640 = –24
9	7	0.0	pż.	.	● 0 000–240 404–740 · = 000–830
10	7	0.3	pż.	0.1	⚹ 1625–35 ⚹ 2006–2115 2120–2235 2315–40
11	8	0.2	pż.	2.5	⚹ 505–10 1825–40 2320–32
12	7	4.6	1	.	✳ 1 1305–1710 ✳ 0–2030 ✳ 1–24
13	7	0.2	8	.	✳ 1 000–830 ✳ 0–1310
14	8	0.0	10	6.7	
15	8	0.0	10	3.4	✳ 0 055–150 230–1135
16	7	0.2	10	2.9	✳ 0 1120–1215 ⚹ 1320–1420 · = 715–1225
17	5	0.0	12	.	✳ 0 350 735, 820 1150 · = 110–1345
18	7	0.2	11	0.1	
19	7	0.1	10	3.6	✳ 0 010–240
20	7	.	11	.	✳ 0 315–620
21	6	0.0	11	0.1	= 620–24
22	5	0.0	10	1.7	● 0 030–340 615–1220 (marznąca) · = 000–435 ≡ 1–930 = –1025 ≡ 0–a = –1920, 2230–24
23	6	.	8	.	= 000–24
24	5	0.0	8	0.1	✳ 0 1215–50 · = 000–1320
25	6	0.1	6	.	✳ 0 605–40, 1040–1525 · = 730–24
26	4	0.0	6	.	✳ 0 945–1240 · = 000–1430 ≡ 1–1745 = –24
27	5	2.1	6	.	✳ 0 625–735 ✳ 1–1245 ● 0 1340–1615 ● 0–1745 · = 600–2115
28	6	.	4	1.0	
29	7	0.6	4	.	✳ 0 2025–2310 ● 0–24 · = 2330–24
30	5	1.6	3	.	● 0 000–40 ● 0 110–235, 310–615 ● 1–725 ● 0–1145 · = 000–1730 ≡ 1–2045 = –24
31	6	0.2	3	.	✳ 0 2110–2340 · = 000–24
Σ	–	31.8	–	22.2	UWAGI.

Luty – Février

1	6	6.9	4	.	✳ 0 100–35 840–1145 ● 0 2315–24 · = 000–1315
2	7	(0.0)	2	4.1	● 0 000–720 · = 000–940 ≡ 1–1050 = –1220
3	7	.	pż.	0.8	⌴ 0 n–950 · ⊕ 1 815–955
4	7	0.9	pż.	.	● 0 1830–2140 (marznący) · = 1630–2245 ≡ 1–24
5	2	0.0	pż.	.	● 0 910–1140 · ≡ 1 000–1630 ≡ 2–24
6	1	1.7	pż.	.	≡ 2 000–1540 = –24
7	7	0.2	pż.	0.8	● 0 330–610 ⚹ 1815–30, 1935–2240 · = 000–645 ≡ 1–840
8	7	4.0	pż.	0.7	● 0 1910–24
9	6	0.3	.	.	● 0 000–635 940–1010 1715–2030 ⚹ 2220–30, 2340–24 · = 600–730 ≡ 1–935 = –2130
10	7	1.6	.	.	● 0 100–45 515–625 ✳ 0 740–1015 ⚹ 0–1110 ✳ 0–1245, 1530–1635 ✱ 0–1650 ● 0 1815–24 · = 1650–24
11	7	0.4	.	0.9	● 0 000–35 1340 1550 1720–2045 · = 000–na ≡ 1–1030 = –1215
12	7	.	pż.	.	✳ 0 310–545 · ⏀ 0 2020–24
13	6	1.1	.	.	⚹ 0 930–1040 ● 0–1345 1415–1530 · = 1345–24
14	7	7.1	.	.	● 0 620–1145 2010–24 · = 000–1145 · ⏀ 2 035–230
15	6	1.3	.	5.3	● 0 000–340 ● 0–620 ● 0 2340–24 · = 430–1520
16	6	2.0	.	.	● 0 000–445 ● 0 610–1235 ● 0–1935 · = 1935–24
17	7	1.4	.	.	= 000–830
18	6	3.7	2	1.4	✳ 0 000–335 ● 0 2040–2105 2210–24 · = 410–1305
19	6	3.4	.	.	● 0 000–100 ● 1–220 ● 0–540 820–940 1035–1440 ✳ 1–1840
20	6	0.4	1	0.3	⚹ 415–535 ● 0 1620–1710 ✳ 0–2140 · = 720–2140
21	7	0.2	1	3.5	✳ 0 420–535 · = 430–1030
22	7	0.1	.	.	● 0 315–740 ✳ 0–1220 · = 530–815
23	7	1.6	.	4.8	⚹ 1115–50 1345–1435 1535–1605 2010–25
24	6	1.2	3	3.8	✳ 0 015–610 830–1035 ⚹ 2120–2225 · = 1035–24
25	6	0.8	5	.	✳ 0 015–240 610–2240 · = 000–24
26	7	0.0	6	.	✳ 0 215–1015 · = 000–1015
27	7	.	6	.	
28	7	.	4	3.3	= 610–930
29					
30					
31					
Σ	–	40.5	–	29.7	UWAGI.

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ **Marzec – Mars 1957**

DNI	CIŚNIENIE P – 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	111.4	111.7	110.7	111.3	-4.2	-3.6	-5.6	-4.8	-2.9	-6.1	84	85	77	82	0.7	0.7	0.9	0.8	10	10 ✳	0	N 4	N 6	N 4
2	109.4	108.1	107.0	108.2	-7.3	-7.2	-8.4	-7.8	-5.4	-8.5	88	85	83	85	0.4	0.5	0.5	0.5	10	9	10 ✳	NNW 5	N 9	NE 6
3	104.6	102.8	100.9	102.8	-9.4	-6.4	-11.2	-9.6	-5.3	-11.3	88	75	86	83	0.4	0.9	0.4	0.6	10 ✳	5 ⊙	0	NNE 2	NE 2	NE 1
4	95.5	92.6	87.1	92.1	-14.0	-3.2	-3.6	-6.1	-1.9	-14.5	96	63	94	84	0.1	1.7	0.1	0.7	2 ⊙	8	10 ✳	C 0	SSW 9	SSW 7
5	86.1	87.5	90.2	87.9	-0.8	-0.4	-0.9	-0.8	1.0	-3.9	95	78	85	86	0.3	1.3	0.8	0.8	10	7 ⊙	10	W 4	WNW 5	WNW 5
6	89.7	90.8	92.8	91.1	-3.0	-1.6	-4.2	-3.2	-0.4	-4.4	88	86	84	86	0.6	0.7	0.7	0.7	9	10 ✳	10	NW 4	NW 5	N 3
7	94.6	96.3	98.0	96.3	-4.6	-2.9	-4.6	-4.2	-2.0	-5.1	93	79	74	82	0.3	1.0	1.1	0.8	10 ✳	10 ✳	10	NNE 2	NE 2	ENE 3
8	99.8	101.7	104.0	101.8	-5.7	-2.8	-5.4	-4.8	-1.7	-5.9	77	62	77	72	0.9	1.3	0.9	1.2	10	9	0	ENE 2	ENE 1	NNE 3
9	106.9	108.0	110.3	108.4	-7.6	-4.6	-3.8	-4.2	0.0	-8.5	84	63	78	75	0.5	2.0	1.0	1.2	6 ⊙	3 ⊙	0	NNE 2	NE 9	NNE 3
10	113.0	113.5	113.8	113.4	-9.6	1.1	-4.0	-4.1	2.0	-10.6	88	53	89	77	0.4	3.1	0.5	1.3	0 ⊙	0 ⊙	0	NNW 1	NE 2	C 0
11	112.5	111.2	108.4	110.7	-5.2	5.1	1.2	0.6	6.3	-6.4	83	45	64	64	0.7	4.9	2.4	2.7	4 ⊙	3 ⊙	3	W 3	WNW 2	WNW 3
12	102.5	98.7	95.6	98.9	-0.4	4.9	2.3	2.3	7.2	-1.0	78	62	79	73	1.3	3.3	1.5	2.0	10	9 ⊙	2	WSW 4	WSW 4	NW 3
13	94.8	95.1	91.9	93.9	-0.1	3.2	4.9	3.2	8.0	-1.4	98	79	73	83	0.2	1.6	2.4	1.4	9	9	10	WNW 1	WSW 3	WSW 2
14	85.5	81.1	77.0	81.2	2.1	10.0	7.1	6.6	11.2	1.8	78	66	74	73	1.5	4.2	2.6	2.8	3 ⊙	9 ⊙	10	W 3	WSW 6	W 17
15	80.0	83.7	75.7	79.8	0.7	1.9	0.1	0.7	7.2	0.1	86	57	98	80	0.9	3.0	0.2	1.4	10	6 ⊙	10 ✳	WNW12	WNW10	C 0
16	73.7	79.9	90.4	81.3	-2.6	-6.4	-9.8	-7.2	0.4	-10.3	87	60	68	72	0.7	1.5	0.9	1.0	9 ✳	3 ⊙	8	WNW 9	NW 14	N 8
17	96.6	96.3	90.7	94.5	-13.4	-8.8	-8.6	-9.8	-6.5	-14.0	76	65	71	71	0.5	1.1	0.9	0.8	4 ⊙	8 ⊙	10 ✳	NNE 2	ENE 4	SE 8
18	74.1	68.8	70.0	71.0	-6.3	1.1	2.1	-0.2	4.4	-9.2	91	100	84	92	0.3	0.0	1.2	0.5	10	10 ≡	10 ●	SE 10	SW 3	W 9
19	80.8	86.9	90.6	86.1	-3.0	-2.3	-3.9	-3.3	2.4	-4.0	73	55	64	64	1.3	2.4	1.7	1.8	10 ✳	8 ⊙	5	NW 9	NNW 8	ENE 3
20	94.9	94.5	87.8	92.4	-6.7	-0.9	-2.2	-3.0	-0.3	-7.1	80	55	96	77	0.7	2.5	0.2	1.1	3 ⊙	9 ⊙	10 ●	E 3	SE 4	SE 10
21	80.9	85.2	88.2	84.8	1.5	8.5	5.7	5.4	9.3	-2.3	100	68	83	84	0.0	3.6	1.6	1.7	10 ≡	6 ⊙	3	SW 2	WSW 6	W 5
22	88.5	91.2	93.2	91.0	2.4	5.3	3.3	3.6	5.9	2.0	91	69	83	81	0.7	2.8	1.3	1.6	10	10	10	WSW 4	W 8	WSW 6
23	96.8	99.5	105.8	100.7	0.7	2.9	-3.8	-1.0	3.4	-4.0	96	76	85	86	0.2	1.8	0.7	0.9	10	9	10	WNW 3	ENE 3	NE 10
24	113.4	114.7	115.7	114.6	-5.6	0.5	-2.4	-2.5	1.7	-6.5	62	43	57	54	1.5	3.6	2.2	2.4	0 ⊙	0 ⊙	0	ENE 7	E 12	ESE 9
25	115.1	113.6	111.9	113.5	-4.8	2.9	-0.2	-0.6	3.4	-5.8	59	41	56	52	1.7	4.4	2.6	2.9	3 ⊙	3 ⊙	0	SE 10	SE 14	SE 12
26	109.6	108.0	107.7	108.4	-1.5	6.4	1.7	2.1	7.2	-2.8	70	36	60	55	1.7	6.2	2.8	3.6	4 ⊙	3 ⊙	0	SE 10	SSE12	SE 6
27	106.2	105.2	103.1	104.8	-0.6	9.4	5.5	5.0	11.5	-2.3	71	47	62	60	1.6	6.3	3.4	3.8	5 ⊙	3 ⊙	0	SE 4	SSE 6	SSE 6
28	100.1	97.9	96.1	98.0	2.4	13.4	4.7	6.3	14.3	1.2	77	39	78	61	1.7	10.9	1.9	4.8	4 ⊙	4 ⊙	0	SSW 4	SSW 9	C 0
29	95.1	95.6	97.0	95.9	1.9	11.3	6.5	6.6	12.4	0.5	91	63	85	80	0.6	5.0	1.5	2.4	9	6 ⊙	0	C 0	NW 1	NW 2
30	99.7	101.2	102.5	101.1	1.4	13.2	7.7	7.5	15.2	0.8	91	44	61	65	0.7	8.4	4.1	4.4	4 ⊙	2 ⊙	0	NE 2	E 3	NE 1
31	104.3	105.0	105.2	104.8	3.1	15.4	6.7	8.0	16.2	1.4	83	34	68	62	1.3	11.6	3.1	5.3	0 ⊙	0 ⊙	0	NE 1	SE 6	C 0
M	97.3	97.6	97.4	97.4	-3.2	2.2	-0.7	-0.6	4.0	-4.8	84	62	77	74	0.8	3.3	1.5	1.9	6.7	6.2	4.9	4.2	6.1	5.0

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1	106.2	106.0	104.7	105.6	2.3	16.1	7.1	8.2	17.1	-0.3	89	36	74	66	0.8	11.7	2.6	5.0	0 ⊙	1 ⊙	4	C 0	SE 3	C 0
2	104.1	103.6	103.4	103.7	3.3	16.4	7.7	8.8	17.3	1.9	93	33	75	67	0.5	12.5	2.6	5.2	3 ⊙	2 ⊙	0	C 0	C 0	C 0
3	105.4	106.4	108.1	106.6	3.6	15.6	6.3	8.0	16.4	0.8	91	41	76	69	0.7	10.4	2.2	4.4	0 ⊙	4 ⊙	0	C 0	NNE 1	NNE 1
4	109.0	108.8	108.2	108.7	3.3	14.5	7.7	8.3	16.6	0.2	88	36	61	62	0.9	10.5	4.1	5.2	1 ⊙	2 ⊙	0	NNW 1	WNW 3	WNW 3
5	106.5	104.1	99.1	103.2	2.8	16.2	8.9	9.2	17.6	0.1	82	36	68	62	1.3	11.8	3.6	5.6	5 ⊙	5 ⊙	0	W 1	W 5	C 0
6	93.8	89.6	87.3	90.2	5.3	17.8	9.2	10.4	18.5	3.7	71	29	74	58	2.6	14.5	3.0	6.7	0 ⊙	3 ⊙	6	WSW 2	WSW 7	N 2
7	87.2	89.9	94.0	90.4	5.0	8.7	3.5	5.2	9.3	3.2	86	48	68	67	1.2	5.8	2.5	3.2	10	9 ⊙	9	NNE 6	NNE 8	NE 5
8	96.9	94.6	89.8	93.8	-1.4	2.1	0.9	0.6	4.8	-2.5	87	50	96	78	0.7	3.5	0.2	1.5	10	9 ⊙	10 ✳	N 4	W 3	WNW 7
9	88.6	89.9	89.2	89.2	-0.8	-0.2	-3.7	-2.1	1.7	-3.9	85	35	73	64	0.9	3.9	1.2	2.0	8 ⊙	8 ⊙	1	NNW 9	NW 12	NW 5
10	87.6	84.3	77.5	83.1	-3.0	3.1	5.6	2.8	5.9	-5.2	77	40	52	56	1.1	4.6	4.4	3.4	4 ⊙	9	10	WSW 3	SSW 8	S 10
11	71.9	72.0	76.5	73.5	5.7	8.5	1.1	4.1	10.5	0.8	76	52	70	66	2.3	5.3	2.0	3.2	9	9	10	SSW 8	WSW 5	W 6
12	83.2	87.5	90.8	87.2	-1.0	2.3	0.2	0.4	3.5	-1.5	75	71	63	70	1.5	2.0	2.3	1.9	7	9	6	NW 6	NNW 5	C 0
13	91.8	92.1	94.0	92.6	-1.3	5.3	-0.2	0.9	6.8	-6.7	76	25	98	66	1.3	6.6	0.1	2.7	6 ⊙	4 ⊙	10	SE 2	WSW 6	WNW 2
14	95.8	97.3	97.6	96.9	-4.4	-0.2	-1.2	-1.8	3.7	-5.5	91	80	84	85	0.4	1.2	0.9	0.8	1 ⊙	8 ✳	6	WNW 2	C 0	C 0
15	98.6	98.5	99.6	98.9	-1.6	2.1	-2.4	-1.1	2.8	-2.7	86	55	91	77	0.7	3.2	0.4	1.4	9	9	1	N 3	NW 3	NW 1
16	100.5	99.7	97.8	99.3	-2.3	3.7	3.7	2.2	6.8	-4.8	89	46	52	62	0.6	4.3	3.8	2.9	4 ⊙ ✳	8 ⊙	10	WNW 3	W 3	S 3
17	95.9	97.6	99.8	97.8	5.4	8.7	5.8	6.4	10.4	1.9	95	63	89	82	0.5	4.1	1.0	1.9	10 ●	10	10	SW 3	WNW 1	ESE 4
18	99.6	97.1	94.6	97.1	1.7	2.3	0.9	1.4	6.0	0.6	96	89	96	94	0.3	0.8	0.2	0.4	10	10 ●	10 ●	N 3	NNE 8	NNE 3
19	92.3	91.9	94.6	92.9	1.2	3.7	2.8	2.6	4.2	0.6	98	82	91	90	0.2	1.5	0.7	0.8	10 ☔	10	10	N 1	W 2	SSW 1
20	98.4	100.3	103.2	100.6	2.6	9.4	6.4	6.2	10.9	1.7	95	54	78	76	0.4	5.4	2.1	2.6	10	6	10 ●	S 2	E 2	ENE 5
21	104.7	106.1	108.1	106.4	4.9	10.3	6.9	7.2	12.2	4.3	92	72	94	86	0.7	3.5	0.5	1.6	10	10	10	E 4	E 2	C 0
22	110.5	110.8	111.0	110.8	5.1	14.7	9.6	9.8	15.8	2.8	89	50	68	69	1.0	8.3	3.9	4.4	1 ⊙	4 ⊙	1	E 1	ENE 5	E 5
23	110.1	109.1	108.9	109.4	7.1	11.0	9.1	9.1	12.0	5.0	88	75	88	84	1.2	3.2	1.4	1.9	10	9	6	ENE 2	NE 3	N 3
24	107.0	106.5	104.6	106.0	7.1	16.3	13.7	12.7	17.6	6.4	99	51	54	68	0.2	9.1	7.2	5.5	10 ⊙	8 ⊙	6	NE 2	ENE 2	N 3
25	103.0	102.7	101.7	102.5	5.9	14.5	12.0	11.1	16.9	5.5	97	62	76	78	0.3	6.3	3.3	3.3	10	4 ⊙	4	NNE 5	NE 4	N 5
26	101.1	100.1	99.5	100.2	8.3	20.2	15.5	14.9	23.2	5.9	83	45	59	62	1.9	13.0	7.2	7.4	4 ⊙	6 ⊙	2	NE 3	ENE 6	ENE 2
27	99.9	98.3	97.2	98.2	13.0	21.7	14.3	15.8	23.7	10.1	76	37	68	60	3.6	16.5	5.3	8.5	7 ⊙	9	4	ENE 1	ENE 3	ESE 5
28	95.9	92.9	92.6	93.6	13.3	23.3	12.3	15.3	24.0	8.5	77	31	95	68	3.5	19.8	0.7	8.0	3 ⊙	7 ⊙	6 ●	ESE 2	S 6	C 0
29	91.7	90.4	90.9	90.8	12.9	23.5	15.7	17.0	24.1	8.1	86	39	73	66	2.1	17.5	4.8	8.1	8 ⊙	5 ⊙	10(R)	S 2	S 7	W 5
30	91.8	89.5	84.9	88.7	12.5	21.6	13.1	15.1	24.1	8.5	90	48	91	76	1.4	13.4	1.4	5.4	0 ⊙	3 ⊙	10 ●	C 0	SSE 8	NW 4
31																								
M	97.6	97.3	97.0	97.3	3.9	11.1	6.4	7.0	12.8	1.6	87	50	76	71	1.1	7.8	2.5	3.8	6.0	6.7	6.1	2.7	4.4	3.0

Suwałki $H_s = 165\ m$ $H_b = 169.2\ m$ $h_w = 12\ m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.0	4	.	$*^0\ 8^{10}\ 9^{10}\ 10^{30}\ 13^{20}\ 17^{20}-18^{30}$
2	7	0.0	4	.	$*^0\ 11^{20}-12^{20},\ 20^{20}-22^{35}$
3	7	0.0	4	6.8	$*^0\ 6^{15}-9^{30},\ =5^{30}-9^{30}$
4	7	1.6	4	5.3	$*^1\ 20^{05}-23^{20},\ =0^{40}-10^{00}$
5	7	0.2	7	3.1	$*^0\ 6^{55}-7^{35}\ *^1-8^{45}\ \overset{*}{\triangledown}\ 13^{05-09},\ 13^{45}-16^{33},\ =5^{30}-9^{15}$
6	6	0.0	7	0.7	$\overset{*}{\triangledown}\ 2^{20}-3^{50}\ *^0-4^{25},\ 7^{20}-10^{15},\ 10^{25}-13^{40}\ *^0-20^{10}$
7	7	0.0	7	1.4	$*^0\ 0^{10}-7^{06},\ 9^{05}-12^{45},\ =2^{20}-12^{45}$
8	7	0.0	5	3.1	$*^0\ 7^{30}-12^{05},\ =18^{15}-20^{00}$
9	6	.	4	9.4	$=9^{30}-24$
10	7	.	3	10.6	$=0^{00}-10^{30}$
11	7	.	3	10.4	
12	7	.	pż.	0.4	
13	7	0.0	.	1.8	$\bullet^0\ 10^{04}-11^{20},\ =0^{35}-12^{15}$
14	6	3.3	.	3.8	$\overset{\bullet}{\triangledown}\ 14^{40-43},\ 15^{05-27},\ 18^{35}-19^{45}\ 20^{40}-21^{20},\ 22^{25}-24,\ \diagdown\!\!\diagup\ 20^{15}-24,\ =6^{10}-18^{10}$
15	8	3.8	.	5.8	$\overset{\bullet}{\triangledown}\ 0^{00}-1^{10}\ \bullet^1-6^{10}\ *^0\ 17^{35}-19^{15}\ *^1-24$
16	8	0.0	4	2.9	$*^0\ 0^{00-05}\ \overset{*}{\triangledown}\ 6^{05-20}\ \Sigma-6^{25}\ \overset{*}{\triangledown}\ 6^{30}-8^{03},\ 14^{40}-15^{35},\ \ast\!\!\rightarrow\!\!\uparrow^1\ 7^{15}-8^{03}\ \uparrow^1-11^{45}$
17	8	0.4	4	8.3	$*^0\ 20^{15}-24$
18	3	3.9	6	.	$*^1\ 0^{00}-3^{30}\ *^0-6^{10}\ \bullet^0\ 8^{45}-11^{40}$ (marznący), $13^{45}-21^{40},\ \equiv^1\ 11^{40}-13^{45}=-21,\ \simeq^0\ 8^{45}-12^{00}$
19	8	0.0	pż.	4.6	$*^0\ 6^{05}-10^{35},\ =0^{00-15}$
20	8	4.0	pż.	5.8	$*^0\ 16^{20}-17^{35}\ *^1-19^{35}\ \bullet^0-24$ (marznący); $\simeq^0\ 22^{30}-24$
21	8	0.2	2	7.0	$\bullet^0\ 0^{00}-3^{10}$ (marznący), $7^{35}-9^{15},\ \equiv^1\ 3^{30}-7^{40}=-9^{15},\ \simeq^0\ 0^{00}-4^{15}$
22	7	0.1	pż.	3.0	$\overset{\bullet}{\triangledown}\ 4^{25-35}\ 5^{50}-6^{02},\ 16^{08-18},\ 16^{25}-17^{05},\ 18^{25-35},\ =6^{10}-8^{20}$
23	7	0.0	.	0.8	$\overset{*}{\triangledown}\ 17^{15}-18^{10},\ 18^{25}-19^{07},\ =6^{02}-9^{10}$
24	8	.	.	11.4	
25	8	.	.	10.7	
26	8	.	.	10.4	
27	7	.	.	11.0	
28	7	.	.	11.0	
29	7	.	.	5.7	
30	7	.	.	11.2	$\llcorner^0 n-7^{00}$
31	8	.	.	11.6	$\llcorner^0 n-7^{00}$
Σ	—	17.5	—	178.0	UWAGI

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1	7	.	.	11.6	$\llcorner^0 n-6^{40}$
2	8	.	.	11.6	
3	7	.	.	11.3	$=4^{30}-8^{00}\ \llcorner^0\ 3^{20}-6^{50}$
4	7	.	.	11.9	$\llcorner^1 n-7^{15}$
5	8	.	.	11.5	$\llcorner^0 n-7^{00}$
6	8	0.6	.	11.2	
7	8	.	.	7.5	$\bullet^0\ 2^{10-45},\ 3^{15}-4^{40},\ =1^{00}-4^{40}$
8	8	0.0	.	1.9	$*^0\ 18^{50}-20^{50},\ =20^{10}-21^{30}$
9	8	0.0	.	7.5	$\overset{*}{\triangledown}\ 5^{35}-6^{10},\ 16^{10}-45$
10	8	.	.	3.7	
11	8	0.0	.	2.7	$\bullet^0\ 7^{35}-8^{20}$
12	8	0.0	.	1.2	$\overset{\bullet}{\triangledown}\ 1^{03}-07\ 5^{50}-6^{02}\ \overset{*}{\triangledown}-6^{20}\ 12^{45}-13^{05}$
13	8	2.2	.	9.6	$\overset{*}{\triangledown}\ 19^{08}-20^{20}\ 21^{30}-24,\ \llcorner^1 n-8^{00}$
14	6	0.2	5	7.8	$\overset{*}{\triangledown}\ 0^{00-50}\ 1^{20}-12^{35}\ 13^{45}-14^{10},\ 14^{40-50},\ \equiv^1\ 4^{00}-45\ =-7^{30}$
15	8	0.0	1	1.3	$\overset{*}{\triangledown}\ 3^{30-35}\ 4^{15}-6^{23}$
16	8	1.8	.	8.2	$\overset{*}{\triangledown}\ 6^{25}-7^{10},\ \llcorner^1 n-7^{15}$
17	8	1.3	.	0.2	$\bullet^0\ 0^{15}-4^{05},\ 5^{05}.45\ 6^{10}-8^{08},\ =4^{05}-8^{10}$
18	6	3.8	.	.	$\bullet^0\ 2^{35}-5^{05}\ \bullet^1-5^{30}\ \bullet^0-6^{40}\ 8^{50}-9^{10}\ \overset{\bullet}{*}^0-11^{40}\ \bullet^0-13^{05}\ \overset{\bullet}{*}^0-16^{35}\ \bullet^0-21^{35}\ \times^0-22^{10}\ \circ^0-24$
19	7	0.5	.	.	$\bullet^0\ 0^{00}-5^{10}\ \overset{\bullet}{*}^0-8^{35}\ \bullet^0-12^{20}\ 13^{45}-15^{30}\ 16^{36},\ =4^{30}-12^{25}$
20	7	2.0	.	2.9	$\bullet^0\ 4^{40}\ 5^{15}\ 18^{20}-19^{25}\ 20^{25}\ 21^{05}-22^{40},\ =3^{30}-7^{30}$
21	7	7.8	.	0.2	$\bullet^0\ 3^{40}-5^{03}\ \bullet^1-5^{35}\ \bullet^0-6^{10}\ \overset{\bullet}{\triangledown}\ 13^{15}-15^{15},\ 15^{45}-17^{50},\ \swarrow^1\ 13^{45}-14^{00}\ 14^{13}\ SE-NW$
22	7	.	.	10.7	
23	7	.	.	1.2	
24	7	.	.	5.2	$=5^{20}-7^{45}\ 12^{35}-15^{25}$
25	7	.	.	8.5	$=5^{45}-11^{25}$
26	7	.	.	5.7	$=6^{40}-10^{20}$
27	7	2.9	.	3.9	$\overset{\bullet}{\triangledown}\ 11^{10-35}\ \blacktriangle^0\ 11^{15-18},\ 12^{45}-13^{50}\ 14^{10}-15^{20}$ (↙)$^0\ 11^{05-10}$ ↙$^0\ 11^{10-120}-13^{30}$ SE-NW, $12^{45}-13^{20}-14^{35}$ SE-NW
28	7	1.	.	7.8	$\overset{\bullet}{\triangledown}\ 13^{35-43}\ 14^{05-20},\ 16^{20}-17^{10}\ 17^{15}-20^{35}$ ↙$^0\ 12^{25}\ 12^{55}\ 13^{25}$ SE-NW (↙)$^0\ 14^{05-45}$ ↙$\ 20^{35}-22^{15},\ \frown\ n-8^{20}$
29	8	2.2	.	7.2	$\overset{\bullet}{\triangledown}\ 7^{40-45}\ 14^{45-50}\ 15^{18-28}\ 17^{07-20}\ 18^{55}-19^{30}\ 20^{15-30}$ ↙$^0\ 16^{35}\ 16^{50}-17^{35}$ SW-NE ↙$^2\ 18^{45}\ 18^{59}\ 19^{35}$ SW-NE (↙)-21^{25}
30	7	8.9	.	8.1	$\overset{\bullet}{\triangledown}\ 9^{45}-10^{15},\ 16^{35}-17^{40},\ 18^{10}-19^{50},\ 20^{10}-24,$ ↙$^0\ 18^{05}\ 19^{10}\ 19^{35}$ SW-NE, $=5^{05}-8^{00},\ \frown^2\ n-8^{00}$
31					28.IV $\frown^1\ 16^{50-55}$
Σ	—	35.9	—	182.1	UWAGI.

Suwałki — φ = 54°06' — λ = 22°57' — Maj – Mai 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.8	95.8	98.8	95.5	4.1	7.5	2.7	4.2	13.1	2.5	72	53	72	66	2.3	4.9	2.1	3.1	7	5 ⊙	0	W 10	WNW 9	NW 2
2	100.0	97.7	95.2	97.6	3.5	9.7	5.7	6.2	11.9	-1.4	66	39	67	57	2.6	7.3	3.1	4.3	0 ⊙	4 ⊙	1	E 3	ESE 3	SW 1
3	92.8	90.9	87.4	90.4	7.5	12.9	7.7	9.0	14.7	-0.4	56	29	64	50	4.6	10.6	3.8	6.3	5 ⊙	5 ⊙	2	C 0	WSW 3	C 0
4	83.6	84.3	86.2	84.7	8.5	8.5	3.9	6.2	11.2	3.4	70	65	54	63	3.3	3.9	3.7	3.6	8 ⊙	9	0	WSW 6	W 8	SW 5
5	86.1	87.4	88.9	87.5	2.7	7.4	3.1	4.1	9.0	0.4	72	44	90	69	2.1	5.8	0.8	2.9	8 ⊙	7 ⊙	2	SW 10	WSW 9	WSW 6
6	91.3	90.7	88.7	90.2	1.7	7.8	3.5	4.1	8.1	-1.6	89	48	93	77	0.8	5.5	0.5	2.3	6 ⊙	10 ⊙	10 ●	C 0	ENE 2	ENE 6
7	87.5	88.3	86.4	87.4	5.0	5.7	5.7	5.5	7.2	3.2	89	80	91	87	1.0	1.9	0.9	1.3	10	10	10 ●	SW 3	C 0	N 3
8	82.4	82.4	85.5	83.4	5.7	9.9	5.3	6.6	11.4	4.6	98	84	97	93	0.2	1.9	0.3	0.8	10 ≡	9	10	WNW 3	WSW 3	WNW 2
9	89.4	90.1	88.8	89.4	5.1	9.4	12.1	9.7	12.5	4.3	97	83	88	89	0.3	2.0	1.7	1.3	10 ●	9	8	N 2	NE 6	NNE 6
10	87.8	88.2	92.0	89.3	11.8	14.3	10.9	12.0	16.8	9.5	82	87	87	85	2.5	2.2	1.6	2.1	9 ⊙	6 ⊙	9	NNE 4	SSE 3	ESE 5
11	92.0	95.5	97.6	95.0	8.5	9.2	9.3	9.1	10.9	8.0	97	93	91	94	0.3	0.8	1.1	0.7	10 ●	10	10	SE 8	S 5	SSW 1
12	97.6	98.4	98.6	98.2	10.6	16.1	11.4	12.4	17.1	5.3	85	56	85	75	2.0	8.1	2.0	4.0	1	9	4	S 3	SW 5	C 0
13	99.1	98.3	97.2	98.2	11.1	21.8	15.4	15.9	22.7	6.5	85	31	65	60	2.0	17.9	6.2	8.7	0 ⊙	5 ⊙	2	SE 1	S 3	C 0
14	96.2	95.8	97.0	96.3	15.9	21.0	12.7	15.6	22.3	7.4	73	47	77	66	4.9	13.2	3.4	7.2	2 ⊙	4 ⊙	4	C 0	WNW 7	NW 4
15	99.7	101.2	101.9	100.9	10.8	16.9	9.7	11.8	18.0	7.1	82	40	69	64	2.3	11.6	3.7	5.9	3 ⊙	5 ⊙	0	WNW 6	W 8	NW 1
16	102.6	100.9	98.6	100.7	11.9	19.1	13.5	14.5	21.3	2.9	69	38	69	59	4.3	13.7	4.9	7.6	0 ⊙	0 ⊙	0	ESE 4	E 4	C 0
17	99.3	97.4	96.8	97.8	14.9	22.2	15.0	16.8	22.8	7.8	63	35	84	61	6.2	17.5	2.7	8.8	0 ⊙	5 ⊙	9	ESE 3	ENE 4	C 0
18	96.9	97.3	96.2	96.8	12.9	21.0	16.4	16.7	22.3	9.7	83	47	65	65	2.7	13.2	6.5	7.5	9	4 ⊙	7	NNW 3	NNE 3	N 3
19	94.9	92.8	91.2	93.0	16.3	24.8	15.3	17.9	26.6	12.1	77	47	87	70	4.2	16.7	2.3	7.7	7 ⊙	8 ⊙	10	NE 6	E 8	NE 4
20	91.3	90.9	90.7	91.0	16.4	23.6	17.2	18.6	26.4	11.3	82	44	75	67	3.2	16.4	4.9	8.2	2 ⊙	5 ⊙	6	ESE 2	SE 8	C 0
21	91.7	92.8	94.2	92.9	15.8	18.0	10.7	13.8	19.2	10.4	81	71	82	78	3.3	5.9	2.3	3.8	6 ⊙	9	10	NNE 4	N 4	NW 6
22	93.2	93.7	93.3	93.4	11.3	18.2	15.6	15.2	20.0	8.3	85	63	72	73	2.0	7.7	5.0	4.9	10	8	8	N 3	N 6	NW 6
23	91.3	90.7	90.9	91.0	14.1	19.2	14.5	15.6	20.2	11.7	94	71	91	85	0.9	5.4	1.5	2.9	10 ●	8 ●	10	N 5	N 1	N 3
24	93.2	96.3	100.4	96.6	10.0	12.9	8.0	9.7	14.6	7.6	76	53	63	64	3.0	7.0	3.9	4.6	10	8	0	NE 8	NE 9	NNE 4
25	103.6	105.0	105.7	104.8	6.5	7.2	6.1	6.5	9.4	3.4	68	56	67	64	3.1	4.5	3.1	3.6	4 ⊙	10	10	NNE 8	NNE 7	N 4
26	106.5	106.9	106.7	106.7	5.3	7.7	5.3	5.9	8.7	3.7	78	52	72	67	1.9	5.0	2.5	3.1	9	9	9	N 3	NE 4	N 2
27	105.9	105.7	104.5	105.4	5.7	8.1	6.1	6.5	10.7	1.9	80	51	85	72	1.9	5.2	1.4	2.8	4 ⊙	9	10	NNE 3	SE 1	NNE 3
28	103.0	101.8	100.4	101.7	5.9	11.3	6.5	7.6	11.4	4.6	79	53	82	71	2.0	6.4	1.7	3.4	9	8	4	ESE 3	ENE 5	C 0
29	99.1	98.2	98.2	98.5	8.5	11.3	7.9	8.9	12.6	0.8	59	39	79	59	4.6	8.1	2.2	5.0	2 ⊙	8 ⊙	10	N 3	N 2	NW 3
30	99.3	100.4	99.9	99.9	6.4	10.8	8.3	8.4	11.4	4.9	92	57	82	77	0.7	5.6	2.0	2.8	10 ●	9	8	WSW 3	WSW 4	WNW 3
31	99.7	98.4	95.5	97.9	9.3	17.5	11.7	12.8	19.0	1.9	71	41	78	63	3.4	11.9	2.9	6.1	2 ⊙	6 ⊙	0	W 2	W 5	W 2
M	95.1	95.3	95.3	95.2	9.2	13.9	9.6	10.6	15.6	5.2	79	55	78	71	2.9	8.0	2.7	4.4	5.9	7.1	5.9	3.9	4.8	2.7

Czerwiec – Juin

1	93.3	92.1	92.5	92.6	12.1	20.0	12.2	14.1	20.7	8.8	68	41	64	58	4.5	13.8	5.1	7.8	9	8 ⊙	10	SW 3	WSW 7	W 6
2	93.2	95.3	97.5	95.3	11.3	17.0	13.1	13.6	19.0	10.1	80	51	86	72	2.6	9.5	2.1	4.7	10	9 ⊙	2	W 6	WNW 6	WNW 2
3	100.1	99.3	97.1	98.8	12.0	19.6	16.4	16.1	22.3	8.2	84	48	76	69	2.2	11.8	4.4	6.1	9	4 ⊙	3	SW 3	WSW 5	C 0
4	94.0	91.3	89.5	91.6	18.4	24.4	17.6	19.5	24.9	10.1	69	42	81	64	6.7	17.7	3.8	9.4	2 ⊙	9 ⊙	10	C 0	SW 3	C 0
5	85.5	82.5	83.5	83.8	14.1	14.0	12.0	13.0	17.8	10.2	84	79	96	86	2.5	3.4	0.5	2.1	10	10 ●	10	NW 1	NNW 2	W 2
6	83.5	85.0	89.1	85.9	12.1	14.1	10.9	12.0	17.1	8.5	90	74	85	83	1.4	4.3	1.9	2.5	9	6 ⊙	8	W 4	C 0	SW 3
7	90.8	90.5	90.2	90.5	10.1	18.6	13.1	13.7	20.0	7.1	82	55	93	77	2.3	9.6	1.1	4.3	10	8 ⊙	10 ●	SW 6	SW 9	C 0
8	93.8	94.9	95.7	94.8	10.9	19.8	15.3	15.3	21.4	7.7	99	47	75	74	0.1	12.3	4.4	5.6	8 ⊙	4 ⊙	1	ENE 2	NW 3	ENE 2
9	96.3	94.1	92.3	94.2	16.2	24.4	20.2	20.2	25.9	10.4	84	53	67	68	2.9	14.4	7.9	8.4	2 ⊙	6 ⊙	6	ESE 4	SE 9	SE 3
10	93.5	93.6	93.9	93.7	19.2	25.2	18.8	20.5	25.5	14.0	78	58	78	71	4.8	13.4	4.7	7.6	5 ⊙	9 ⊙	5	S 5	SE 5	SSE 3
11	95.0	93.9	93.5	94.1	19.4	26.4	22.2	22.6	28.1	13.8	78	51	76	68	4.8	16.8	6.5	9.4	2 ⊙	8 ⊙	3	SE 3	SE 8	SE 2
12	95.5	99.9	105.4	100.3	23.0	21.8	14.2	18.3	26.9	13.8	76	78	71	75	6.9	5.7	4.8	5.8	10 ⊙	10	8	S 2	NW 8	NW 4
13	105.9	106.7	105.9	106.5	11.3	13.3	11.6	12.0	14.2	9.3	67	69	79	72	4.4	4.8	2.8	4.0	7 ⊙	10	6	WSW 7	WNW 6	NW 4
14	105.7	106.2	107.0	106.3	12.1	19.9	14.1	15.0	21.0	7.4	72	35	47	51	4.0	15.1	8.5	9.2	0 ⊙	0 ⊙	1	NW 7	NW 10	N 3
15	108.9	107.9	105.2	107.3	12.7	19.4	15.4	15.7	20.6	7.7	70	43	70	61	4.4	12.8	5.3	7.5	2 ⊙	1 ⊙	1	NNE 1	NNW 3	NW 3
16	103.7	102.7	100.6	102.3	15.8	19.4	16.6	17.1	22.7	10.9	64	51	61	59	6.4	11.0	7.3	8.2	5 ⊙	9	2 ⊙	NW 3	NW 5	N 4
17	101.1	100.3	98.6	100.0	14.8	19.8	16.2	16.8	21.5	8.5	51	39	61	50	8.2	14.1	7.2	9.8	0 ⊙	1 ⊙	0	NNE 4	NNE 4	C 0
18	98.2	96.5	93.0	95.9	18.2	25.0	20.0	20.8	26.5	7.5	54	29	50	44	9.5	22.4	11.6	14.5	4 ⊙	4 ⊙	1	WSW 3	SW 7	C 0
19	91.0	91.1	91.5	91.2	19.6	23.0	14.0	17.6	23.6	9.7	62	56	63	60	8.6	12.5	5.9	9.0	2 ⊙	2 ⊙	3	N 4	NE 7	NNE 4
20	94.2	95.2	95.7	95.0	11.9	17.3	12.0	13.3	18.5	8.7	55	33	59	49	6.3	13.2	5.7	8.4	5 ⊙	5 ⊙	4	NE 6	NE 3	NW 2
21	99.1	98.2	94.7	97.3	10.3	16.4	11.9	12.6	18.8	3.4	60	39	60	53	5.0	11.2	5.5	7.2	1 ⊙	2 ⊙	1	N 2	NE 3	SSW 1
22	90.6	87.8	82.4	86.9	17.4	22.8	16.4	18.2	24.2	8.0	41	51	98	63	11.7	13.5	0.4	8.5	1 ⊙	7 ⊙	10(R)	SSE 9	SSE 9	SE 2
23	84.7	89.7	90.2	88.2	15.1	20.0	17.2	17.4	21.0	14.5	85	62	78	75	2.6	8.8	4.3	5.2	10	6 ⊙	10	WNW 4	WNW 3	NW 1
24	90.2	90.0	87.9	89.4	15.1	18.0	9.7	13.1	19.8	9.7	94	79	97	90	1.0	4.2	0.3	1.8	10	10	10 ●	C 0	NW 3	NNE 4
25	82.8	86.1	92.3	87.1	11.9	11.7	10.5	11.2	12.7	9.3	97	95	94	95	0.3	0.6	0.8	0.6	10 ●	10 ●	10	NE 4	W 4	W 2
26	96.0	97.1	99.3	97.5	11.1	16.3	11.7	12.7	17.1	7.0	90	49	81	73	1.3	9.4	2.6	4.4	8 ⊙	9	2	WSW 4	WNW 4	NW 1
27	100.3	100.6	102.8	101.2	12.1	16.2	11.4	12.8	17.6	6.7	74	50	79	68	3.7	9.2	2.8	5.2	1 ⊙	8 ⊙	2	WSW 3	W 4	W 4
28	101.6	98.2	96.5	98.8	12.5	14.9	15.3	14.5	17.1	7.3	70	74	97	80	4.4	4.3	0.6	3.1	9 ⊙	10	10	SW 4	SW 10	WSW 4
29	98.9	99.9	99.2	99.3	15.2	21.8	16.6	17.6	23.0	13.0	89	57	83	76	1.9	11.1	3.3	5.4	10	8 ⊙	1	NW 4	WNW 2	WNW 1
30	96.2	97.2	99.3	97.6	19.7	23.5	16.2	18.9	24.2	12.0	81	61	82	75	4.3	11.2	3.2	6.2	4 ⊙	8 ⊙	2	WNW 4	WNW 7	NW 4
31																								
M	95.5	95.5	95.4	95.5	14.5	19.5	14.8	15.9	21.1	9.4	75	55	76	69	4.3	10.7	4.2	6.4	5.8	6.7	5.1	3.7	5.3	2.4

Suwałki $H_s = 155\ m$ $H_b = 169{,}2\ m$ $h_w = 12\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	10.0	∴ 000–30
2	8	.	.	12.2	⌴¹ n – 600
3	8	.	.	13.0	⌴¹ n – 610
4	7	0.0	.	2.9	∴ 1040 – 1208
5	8	1.9	.	9.7	∴ 1105–10 1825 – 1925
6	8	1.4	.	2.3	•⁰ 1625 – 2315 •⁰–24 ⌴¹ n – 630
7	7	6.4	.	.	•⁰ 000 – 140 •¹ 810–35 •⁰–1125 1435 1525 1710 – 1835 2015–24 = 315–730 1835–2000
8	6	0.0	.	3.0	•¹ 000 – 240 315–605 •⁰ 2135 – 2240 2315–24 ≡¹ 605–930 = –1430 2010–24
9	7	0.0	.	2.2	•⁰ 000 – 105 340–620 •⁰–710 ∴ 1905–10 = 000–800
10	7	4.7	.	4.1	∴ 1025–35 1107–10 1340 – 1420 2345 – 24
11	6	0.4	.	.	∴ 000–05 110–205 210–315 320–425 •⁰–1110 = 1110–1425
12	7	.	.	6.8	= 230–345 ≡¹–445 = –925
13	7	.	.	13.3	= 215–840 ⌓² n – 830
14	7	0.0	.	10.3	∴ 1120–30 1855–1905 ⌓ n – 800
15	8	.	.	13.6	= 440–930 ⌓⁰ n – 720
16	8	.	.	14.7	⌓⁰ n – 650
17	8	1.4	.	9.3	•⁰ 1605 – 1850 2010–2335 ⌓¹ n – 710
18	8	.	.	9.9	•⁰ 045 – 140
19	8	5.3	.	8.6	∴ 1550 – 1605 1715–50 1805–45 (K)⁰ 1530 – 1600 1640 E-W (K)¹ 1715 – 1805 1820 E-W
20	8	.	.	13.3	
21	7	0.3	.	4.3	•⁰ 2115–24 (K)⁰ 1040 – 1130 N = 420–630
22	7	6.2	.	4.0	•⁰ 000 – 125
23	6	13.2	.	2.4	•⁰ 140 – 220 •⁰–745 ∴ 1235 – 1305 1345 – 1510 1520 – 1650 1715 – 1840
24	8	.	.	7.7	⋙ 950 – 1210
25	8	.	.	5.5	
26	8	.	.	1.2	
27	8	0.1	.	2.8	∴ 1205–15 1410–45 1710 – 1825 1850 – 1905
28	8	0.0	.	3.9	∴ 635 – 701 1120–35 1602–20 1645 – 1705 1730–45
29	8	0.0	.	6.6	⌴⁰ n – 500 •⁰ 2325–24
30	8	0.0	.	1.5	•⁰ 000–10 625 715
31	8	.	.	13.4	= 105–410 ≡¹–445 =–520 ⌓² n – 705
Σ	–	41.3	–	212.5	UWAGI

Czerwiec – Juin

1	7	.	.	8.5	
2	7	.	.	7.3	
3	8	.	.	9.7	= 320–530 ⌓¹ n – 700
4	7	0.0	.	5.5	∴ 1519–28 (K) 1504 – 1625 W–E ⌓¹ n – 600
5	6	3.6	.	.	•⁰ 810 – 1135 1315 – 1625 1945 – 2108 = 2108–24
6	7	12.5	.	7.5	•⁰ 410–40 ∴ 1225 – 1302 1311–13 1606–35 ▲ 1627–28 ∴ 1630–35 = 000–135 ≡¹–435 =–800
7	7	1.7	.	3.8	∴ 1938 – 2210
8	7	.	.	11.3	= 305–635 ≡² –715 =–920
9	7	0.8	.	10.8	= 315–725 ⌓¹ n – 715
10	7	.	.	8.4	∴ 115–25 202–315 (K)¹ 1435 – 1530
11	8	.	.	12.8	⌓⁰ n – 600
12	7	.	.	2.4	⌓⁰ n – 640
13	8	0.0	.	6.1	•⁰ 1720 – 1835
14	8	.	.	15.8	
15	8	.	.	15.7	
16	8	.	.	13.3	
17	8	.	.	15.8	
18	8	.	.	15.3	
19	8	.	.	15.1	
20	9	.	.	10.8	
21	8	.	.	15.8	
22	8	8.6	.	6.4	∴ 1630 – 1930 1950–2015 2204–2310 (K)⁰ 1640 – 1805–1820 NW–SE (K)⁰ n–2240 W–E = 1930–24
23	7	2.9	.	4.4	= 000–740
24	7	6.0	.	2.1	∴ 2115–20 315–620 1540 – 1820 1845–2010 •⁰ 2110–2350
25	6	11.7	.	.	•⁰ 720 – 855 •¹–1105 •⁰–1320 •¹–1520 •⁰ 1625 – 1825
26	7	0.0	.	5.3	∴ 1940–50 ⌒ 1945–50
27	8	.	.	11.1	⌓¹ n – 740
28	7	1.2	.	0.3	•⁰ 1450 – 1930 2002–15 ⋙ 1130 – 1410
29	8	.	.	8.8	
30	7	.	.	13.3	⌓⁰ n – 750
31					
Σ	–	49.0	–	263.4	UWAGI

Suwałki — φ = 54°06' — λ = 22°57' — Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.7	102.0	101.1	101.6	15.6	20.6	15.0	16.6	22.2	11.6	64	38	71	58	6.4	15.1	4.8	8.8	4 ⊙	1 ⊙	1	NE 3	ENE 3	ENE 3
2	99.0	96.4	94.2	96.5	15.9	24.3	17.7	18.9	25.0	10.9	65	48	92	68	6.3	15.8	1.6	7.9	8 ⊙	10	10 ●	SSE 4	SSE 6	WSW 3
3	96.1	97.3	99.0	97.5	14.6	20.4	14.9	16.2	22.1	11.3	79	55	71	68	3.4	10.9	4.8	6.4	4 ⊙	5 ⊙	6	WNW 4	WNW 6	NW 2
4	99.6	97.7	94.1	97.1	15.6	21.3	18.0	18.2	22.6	8.0	76	53	72	67	4.3	11.9	5.7	7.3	8 ⊙	10 ⊙	7	SW 3	SW 4	SE 2
5	90.4	91.2	93.7	91.8	18.9	23.8	16.2	18.8	24.2	15.6	94	66	85	82	1.3	10.0	2.7	4.7	9 ⊙	7 ⊙	0	W 4	WNW 7	NW 3
6	95.8	97.4	99.0	97.4	15.3	20.4	14.7	16.3	21.2	11.2	82	43	60	62	3.2	13.6	6.7	7.8	3 ⊙	7	0	W 6	WNW 7	WNW 1
7	101.9	102.2	101.8	102.0	12.7	20.2	16.5	16.5	22.8	9.2	91	34	64	63	1.4	15.7	6.8	8.0	6 ⊙	2 ⊙	0	NE 1	E 2	C 0
8	101.7	97.9	94.8	98.1	17.3	25.5	22.2	21.8	27.7	9.3	53	37	61	50	9.2	20.6	10.6	13.5	10 ⊙	2 ⊙	8	S 5	SSW 9	SW 1
9	92.9	92.1	92.9	92.6	19.4	21.4	15.8	18.1	23.5	15.4	76	74	82	77	5.4	6.7	3.2	5.1	6 ⊙	10	2	NNW 1	WNW 6	WNW 2
10	92.4	92.8	91.7	92.3	15.6	20.8	17.6	17.9	22.7	11.0	86	54	75	72	2.4	11.4	4.9	6.2	3 ⊙	6 ⊙	2	NW 3	NNW 2	C 0
11	92.4	91.3	91.0	91.6	14.8	24.9	18.4	19.1	25.5	11.9	76	42	91	70	4.0	18.4	1.9	8.1	10 ⊙	8 ⊙	6	ENE 3	NNE 5	NE 4
12	92.3	93.4	93.7	93.1	19.0	25.2	20.9	21.5	26.3	16.2	89	55	70	71	2.4	14.5	7.4	8.1	7 ⊙	10 ⊙	9	E 4	SE 6	E 3
13	96.6	96.1	96.1	96.3	20.0	25.2	19.7	21.2	26.1	16.7	78	54	90	74	5.2	14.8	2.1	7.4	9 ⊙	9 ⊙	10	SE 7	SE 5	WNW 2
14	96.9	96.9	94.7	96.2	17.2	20.0	19.4	19.0	22.7	17.0	99	84	91	91	0.2	3.7	1.9	1.9	10	10	10	NNW 2	NNE 3	NNE 1
15	92.8	91.5	91.5	91.9	18.8	22.4	18.4	19.5	23.1	16.9	89	69	91	83	2.3	8.5	1.9	4.2	10 ●	9 ⊙	9	SSW 2	ESE 1	W 2
16	90.4	88.2	86.3	88.3	19.0	24.8	18.6	20.2	25.5	15.7	86	58	87	77	3.2	13.3	2.7	6.4	8 ⊙	9 ⊙	10	NNE 3	NE 3	NNE 4
17	85.4	85.0	86.2	85.5	17.4	20.2	16.0	17.4	23.0	16.0	97	86	88	90	0.7	3.3	2.1	2.0	10	8 ⊙	5	ESE 3	ESE 4	S 2
18	86.1	86.3	84.6	85.7	16.1	15.9	16.0	16.0	18.3	13.3	92	88	95	92	1.6	2.1	1.0	1.6	10	10	10 ●	SE 1	WNW 5	WNW 6
19	84.2	86.9	88.8	86.6	14.7	15.0	16.5	15.7	18.9	14.3	96	97	93	95	0.7	0.5	1.4	0.9	10 ●	10 ●	4	WSW 5	WSW 4	SW 1
20	90.2	89.9	88.3	89.5	15.8	25.0	18.7	19.6	26.5	10.5	86	42	77	68	2.4	18.5	5.0	8.6	0 ⊙	5 ⊙	0	SSW 1	SE 6	SE 2
21	86.6	86.2	84.5	85.8	18.0	26.4	19.4	20.8	26.6	15.0	77	46	78	67	4.6	18.5	4.8	9.3	4 ⊙	5 ⊙	8	E 3	E 7	ESE 2
22	83.8	82.9	83.2	83.3	18.2	23.7	16.6	18.8	24.2	15.3	85	60	93	79	3.1	11.7	1.4	5.4	9	9 ⊙	8	ENE 2	ENE 4	SSW 2
23	83.3	82.9	81.2	82.5	14.4	22.1	17.2	17.7	24.0	12.3	100	65	87	84	0.0	9.4	2.6	4.0	10 ≡	7 ⊙	1	SW 1	WSW 2	NW 1
24	80.6	81.0	84.6	82.1	17.9	17.3	14.7	16.2	21.0	13.7	91	98	91	93	1.8	0.4	1.5	1.2	10	10 ⊙ ●	10	WNW 4	WNW 7	W 3
25	87.0	88.5	88.7	88.1	14.1	17.8	15.0	15.5	20.4	11.8	89	59	83	77	1.8	8.4	2.9	4.4	10	9 ⊙	6	WSW 4	WSW 4	C 0
26	87.3	86.8	86.2	86.8	13.0	18.6	15.1	15.4	19.8	9.7	91	57	83	77	1.4	9.3	3.0	4.6	10	7 ⊙	8	C 0	W 5	SW 3
27	83.4	83.4	82.6	83.1	14.0	18.0	13.9	15.0	19.4	10.9	90	70	93	84	1.6	6.1	1.1	2.9	10	10	10	SW 4	SW 5	SW 2
28	84.0	84.8	86.6	85.1	13.5	19.3	13.3	14.8	20.6	12.1	93	50	83	75	1.1	11.2	2.7	5.0	10	7 ⊙	10 ●	SW 3	SW 6	S 4
29	89.4	90.5	92.7	90.9	13.4	20.2	12.4	14.6	21.3	9.4	88	49	96	78	1.8	12.1	0.5	4.8	1 ⊙	6 ⊙	6	SW 4	SSW 5	S 2
30	93.6	93.2	94.0	93.6	12.9	19.8	14.9	15.6	20.6	9.7	95	61	93	83	0.7	8.9	1.1	3.6	9	9	9	S 2	SW 5	SW 1
31	95.2	95.4	99.0	96.9	15.1	17.8	15.6	16.0	20.7	12.9	89	81	92	87	1.9	3.8	1.3	2.3	9	8	10	WNW 4	NW 6	WNW 4
M	91.4	91.3	91.2	91.3	16.1	21.2	16.8	17.7	22.9	12.7	85	60	83	76	2.8	10.6	3.3	5.6	7.6	7.6	6.3	3.1	4.8	2.2

Sierpień – Août

1	99.4	99.6	98.5	99.2	15.8	19.0	15.4	16.4	23.3	14.1	89	78	80	82	1.9	4.8	3.5	3.4	9	8 ⊙	1	W 3	W 5	WNW 3
2	97.3	95.8	96.0	96.4	15.1	18.2	13.3	15.0	19.8	12.4	83	54	79	72	3.0	9.5	3.2	5.2	5 ⊙	8 ⊙	6	W 7	WNW 8	NW 6
3	95.1	94.6	94.9	94.9	14.2	16.9	13.3	14.4	18.4	10.0	90	62	70	74	1.6	7.3	4.7	4.5	8 ⊙	8 ⊙	8	SW 4	W 7	WNW 5
4	94.8	95.5	97.1	95.8	14.1	18.6	15.1	15.7	20.1	12.0	85	69	85	80	2.4	6.6	2.6	3.9	8	8 ⊙	10	NW 4	NW 7	NW 6
5	98.7	99.2	99.6	99.2	14.1	19.9	15.6	16.3	22.5	11.8	91	71	90	84	1.5	6.7	1.7	3.3	10	6 ⊙	3	NW 6	NW 5	WNW 4
6	100.5	99.9	98.8	99.7	14.3	20.0	16.0	16.6	22.0	11.2	86	55	84	75	2.4	10.5	2.9	5.3	3 ⊙	5 ⊙	0	NW 4	NW 3	NW 3
7	98.0	95.1	91.1	94.7	16.1	22.2	18.0	18.6	23.6	9.4	84	52	78	71	2.9	13.0	4.4	6.8	8 ⊙	8 ⊙	10	C 0	SW 1	C 0
8	86.1	86.8	89.9	87.6	15.4	19.1	13.1	15.2	20.5	12.7	88	68	86	81	2.1	7.0	2.1	3.7	10 ●	8	3	N 3	N 5	N 1
9	91.8	91.7	89.7	91.1	13.5	19.1	13.0	14.6	19.9	8.2	76	44	78	66	3.7	12.3	3.3	6.4	1 ⊙	4 ⊙	1	E 3	C 0	SSE 1
10	87.8	84.2	80.9	84.3	15.4	22.5	15.4	17.2	23.4	9.1	66	34	97	72	6.0	12.4	0.6	6.3	10 ⊙	10 ⊙	10 ●	SE 5	SE 10	W 3
11	87.9	91.3	92.9	90.7	16.7	23.2	18.0	19.0	24.4	15.4	91	57	83	77	1.8	12.1	3.4	5.8	4 ⊙	7 ⊙	0	WSW 5	WSW 7	SW 2
12	92.9	91.7	89.4	91.3	20.0	28.5	17.8	21.0	28.7	14.0	77	46	98	74	5.4	21.2	0.4	9.0	2 ⊙	1 ⊙	8	S 3	S 5	C 0
13	92.0	93.5	94.2	93.2	16.6	22.1	16.6	18.0	23.6	16.0	97	60	89	82	0.6	10.7	2.2	4.5	4 ⊙	6 ⊙	5	WNW 3	SW 3	C 0
14	94.2	93.9	91.2	93.1	15.9	20.0	16.6	17.3	22.0	11.0	94	74	97	88	1.2	6.2	0.6	2.7	6 ⊙	10	10	C 0	SE 4	NE 4
15	84.3	83.2	87.7	85.1	16.0	17.3	15.3	16.0	18.5	15.0	98	85	89	91	0.4	2.9	1.9	1.7	10	10	8	SE 1	W 10	W 4
16	90.4	91.1	90.6	90.7	13.2	20.7	15.4	16.2	21.8	10.1	93	65	86	81	1.1	8.6	2.4	4.0	2 ⊙	8 ⊙	4	W 3	WNW 5	W 1
17	88.7	86.9	83.7	86.4	15.1	15.4	13.3	14.3	19.2	10.2	96	96	93	95	0.8	0.8	1.1	0.9	8	10 ●	10	WNW 1	SW 1	SW 6
18	79.9	81.9	82.1	81.3	12.9	13.3	14.1	13.6	15.2	11.8	91	93	90	91	1.4	1.1	1.6	1.4	10 ●	10 ●	10 ●	WSW 13	SW 9	SW 9
19	85.3	88.3	92.0	88.5	14.5	17.6	14.9	15.5	19.2	13.4	96	83	90	90	0.7	3.4	1.6	1.9	10 ●	10	2	WSW 7	WSW 9	WSW 4
20	94.7	94.6	94.0	94.4	13.7	19.2	16.5	16.5	21.5	12.6	98	69	80	82	0.4	6.8	3.9	3.7	10 ●	9	8	WSW 4	SW 2	SW 3
21	93.0	93.0	91.8	92.6	16.0	17.3	14.6	15.6	18.0	14.4	86	85	98	90	2.5	2.9	0.4	1.9	9	10	5	SW 5	SSW 4	C 0
22	87.0	87.5	87.2	87.2	14.7	14.5	13.3	14.0	15.4	12.8	99	99	94	97	0.2	0.2	0.9	0.4	10	10 ●	10	SW 3	SW 3	W 4
23	87.9	88.7	90.9	89.2	11.1	16.4	10.3	12.0	17.3	10.3	95	52	85	77	0.7	8.9	1.9	3.8	8	8 ⊙	0	W 4	WNW 6	W 1
24	92.3	90.5	85.4	89.4	9.3	18.2	14.6	14.2	19.0	5.7	92	48	86	75	0.9	10.9	2.4	4.7	0 ⊙	7 ⊙	10 ●	W 1	S 8	SSE 7
25	91.4	94.4	93.8	93.2	11.9	18.0	11.3	13.1	18.8	9.7	85	46	83	71	2.0	11.2	2.3	5.2	2 ⊙	5 ⊙	2	SW 7	SW 10	S 3
26	91.3	89.1	89.2	89.9	11.5	20.4	13.0	14.5	21.1	8.6	85	57	81	74	2.0	10.3	2.8	5.0	6	7 ⊙	3	SSE 3	SSE 6	SSW 4
27	89.7	91.8	93.2	91.6	10.5	14.1	12.5	12.4	16.7	8.5	92	74	85	84	1.0	4.3	2.2	2.5	8	10	7	SW 5	SW 7	SW 3
28	94.5	93.7	94.0	94.1	9.4	18.4	13.3	13.6	19.2	5.9	96	56	95	82	0.5	9.3	0.7	3.5	3 ⊙ ≡	9	10 ●	C 0	SSE 3	SE 4
29	94.8	96.2	96.5	95.8	12.1	14.6	12.2	12.8	15.1	11.5	96	88	96	93	0.5	2.0	0.5	1.0	10	10 ●	10 ●	SSW 1	S 1	SW 1
30	94.4	94.4	94.4	94.4	11.9	15.3	12.1	12.8	17.6	11.3	97	73	89	86	0.3	4.8	1.5	2.2	9	10	3	W 1	NW 4	W 3
31	95.7	96.5	96.4	96.2	10.4	17.1	10.3	12.0	17.5	9.0	95	54	88	79	0.6	9.0	1.4	3.7	4 ⊙	7 ⊙	4	SW 3	SW 6	S 2
M	92.0	92.1	91.8	92.0	13.9	18.6	14.3	15.3	20.1	11.2	90	67	87	81	1.7	7.7	2.1	3.8	6.7	8.0	5.8	3.6	5.3	3.2

Suwałki $H_s = 135$ m $H_b = 189{,}2$ m $h_w = 12$ m **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	8	.	.	13.4	⌒⁰ n – 715
2	7	5.4	.	0.6	▽ 1440 – 1501, 1525-35, 1607 – 1830, 2115-35 (K)⁰ 1610 – 1735 SW – NE; = 2105 – 24
3	8	.	.	15.1	= 000-10 · ⌒¹ n – 730
4	8	9.8	.	4.0	⌒² n – 810
5	7	.	.	11.8	▽ 230 – 435; (K)⁰ 245 – 310 – 345; = 430 – 815
6	8	.	.	13.1	
7	8	.	.	13.2	= 235 – 820 · ⌒¹ n – 800
8	8	15.3	.	11.2	≺ 2128 – 2210
9	7	0.3	.	5.0	▽ 015 – 145, 202 – 310, 1520 – 1610; (K)⁰ 030 – 110 – 140 SW – NE
10	7	.	.	9.5	= 420 – 740 · ⌒² n – 800
11	8	3.6	.	10.2	▽ 1750 – 1910
12	7	0.0	.	5.8	▽ 125 – 245
13	7	10.5	.	1.1	▽ 204 – 35, 1650 – 55, ●⁰ 2125 – 2245
14	7	0.0	.	1.1	▽ 040 – 325, ▽ 530 – 615; = 405 – 810
15	7	0.4	.	0.5	●⁰ 720 – 815, ▽ 925 – 1010, 1045 – 1130, 1625 – 1735; (K)² 1418 – 1545 W – E; = 430 – 1015, 1050 – 1135, 1625 – 1735, 2115 – 24
16	7	7.8	.	7.4	(K)⁰ 130 – 215 W – E, ▽ 145 – 240, 1410-15, 1455 – 1500, ▽K 1705 – 1810 – 1900, ●⁰ 1910 – 2000, ▽ 2040-50, 2135-55, ▽K – 2225; = 0029 15
17	6	2.6	.	5.2	▽ 150 – 325, 830 – 930
18	7	21.1	.	0.1	●⁰ 903 – 1210, 1305-35, ●¹ 1715 – 1830, ●⁰ – 24
19	6	33.8	.	0.1	●⁰ 000-40, ●ᵇ 140 – 205, ●¹ – 1200, ●⁰ – 1255, ●¹ – 1435, ●⁰ – 1515
20	7	.	.	12.7	≡¹ 200 – 300, ≡² – 600 = – 930, 1635 – 24; ⌒² 2115 – 24
21	7	.	.	10.0	= 000 – 1145; ⌒² 000 – 800
22	7	.	.	6.4	⌒⁰ n – 800
23	7	1.0	.	6.4	≡¹ 110 – 800 = – 930; ≺ 2340 – 24
24	6	26.6	.	1.3	▽ 110 – 250, 1135 – 1425, 1536 – 2020; ≺ 000-45 (K)⁰ 1304-15-40 NW – SE; = 415 – 720, 2040 – 24
25	8	0.3	.	6.4	▽ 1525-40; = 000 – 330; ⌒¹ 1845 – 1900 E
26	7	0.0	.	8.3	▽ 540 – 605; ⌒¹ 2000-20
27	7	0.0	.	1.9	▽ 415-25, ●ᵇ 850 – 940, ▽ 1012-20, 1910-13, 2010-45, 2137 – 2225; ⌒² n – 415
28	7	0.9	.	6.2	▽ 1530-45, 1705-25, ▽K⁰ n – 2342 – 24 S – N; = 435 – 1200; ⌒¹ n – 840
29	8	0.5	.	9.7	▽ 1920 – 2015 (K)⁰ 1755 – 1920 W; = 340 – 815; ⌒¹ 1940 – 2010
30	7	1.6	.	2.9	▽ 1440 – 1515, 1618 – 1827 (K)¹ 1440 – 1622 – 1645 S – N; = 330 – 735; ⌒² n – 825; ⌒⁰ 1648 – 52
31	7	0.0	.	4.2	▽ 1730-45, 1800-03, ●¹ 2240 – 2330; = 250 – 700; ⌒² n – 845; ⌒² 1803 – 15
Σ	–	143.5	–	206.4	UWAGI:

Sierpień – Août

1	7	0.0	.	6.3	●⁰ 200-40, 925, 1010, 1215...35; = 430 – 830
2	8	0.3	.	10.0	▽ 1402-30; ⌒⁰ 1945-51
3	7	1.6	.	8.3	▽ 1120-35, 1234-47, 1250-54, 1328-40; ⌒² n – 815
4	7	0.0	.	4.5	● 335 – 415, ▽ 2040 – 2110; = 415 – 550
5	7	0.0	.	5.2	▽ 1820-40
6	8	.	.	13.0	▽ 1630-35; ⌒² n – 800
7	8	0.1	.	9.1	= 440 – 810; ⌒² n – 800
8	8	0.0	.	9.9	▽ 235 – 340, 715 – 835, 1332 – 52
9	8	.	.	12.6	⌒² n – 815
10	8	10.9	.	6.5	●¹ 1640 – 1910, ●⁰ – 2335; ≫ 830 – 1730
11	7	.	.	12.5	⌒⁰ 2030 – 24
12	7	8.5	.	9.9	●¹ 1820 – 2105; (K) 1445 – 2200; ⌒¹ 000 – 730
13	8	.	.	10.0	= 500 – 800, ≡ 2100 – 24; ⌒¹ 2100 – 24
14	7	2.3	.	2.7	▽ 1325-30, 1720-35, ●⁰ 1835 – 2035; = 320 – 820, 2035 – 24; ⌒² 000 – 700
15	6	5.7	.	0.3	▽ 225 – 330, ●⁰ 435 – 540, ▽ 715 – 805, 1045 – 1105; (K) 230 – 345; = 000 – 1200, 1430 – 24
16	7	.	.	13.0	
17	6	28.4	.	0.3	▽ 1310 – 1420, 1445 – 1505, ●⁰ – 1650, ▽ 1748 – 1910, ●¹ – 2125; = 525 – 1135, 2125 – 24; ⌒⁰ n – 1200
18	5	46.9	.	.	▽ 115 – 230, 325 – 405, ●¹ – 930, ● – 1015, ●¹ – 1545, 1730 – 1850, 1913 – 2005, 2120 – 24; ≫ 310 – 900; = 000-40
19	7	0.3	.	2.4	●¹ 000 – 535, 605 – 910, ▽ 1640 – 1710
20	7	0.0	.	5.2	●⁰ 725 – 845, ▽ 1335-38; = 430 – 640, ≡¹ – 725 = – 1045
21	5	1.2	.	0.3	● 1415-20, ▽ – 1430, ●⁰ 1502-35, 1645 – 1825; = 415 – 24
22	6	6.6	.	.	●⁰ 000-40, 105 – 315, 525-40, 610 – 1458, ●⁰ – 1605, ▽ 1845 – 1910, ●⁰ 2330 – 24
23	7	0.0	.	9.6	●⁰ 000 – 415, ▽ 1810-17; = 620 – 815; ⌒² 1810-28
24	8	0.7	.	8.2	▽ 2101-45
25	8	.	.	11.6	
26	7	0.0	.	3.5	▽ 1628-45
27	6	.	.	5.5	= 620 – 900; ⌒² n – 800
28	7	5.3	.	6.1	▽ 1415 – 1505, ●⁰ 1630 – 1700, ●⁰ 1710 – 1802, ▽ 2120-45; (K)¹ 1410 – 1425 – 1505 SE – NW; ≫ 1415-45; ≡¹ 520 – na = – 800
29	6	12.8	.	.	●⁰ 1330 – 1710, ●¹ – 1750, ●⁰ – 24; = 320 – 1330
30	6	.	.	2.4	●⁰ 000-45, ●⁰ – 130, ●⁰ – 635; = 635 – 1740
31	8	1.9	.	7.9	▽⁰ 1450 – 1635
Σ	–	135.1	–	192.2	UWAGI

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	93.5	92.5	93.1	93.0	10.3	10.7	9.6	10.0	12.5	8.2	97	95	97	96	0.3	0.7	0.4	0.5	10 ●	9	10 ●	SSE 4	WSW 5	SW 2
2	97.0	97.4	97.1	97.2	10.1	17.1	10.2	11.9	17.7	9.2	95	67	95	86	0.7	6.3	0.6	2.5	9	8 ⊙	3	SW 6	SW 5	S 2
3	94.5	94.4	95.0	94.6	11.7	17.6	12.1	13.4	18.2	8.3	91	75	96	87	1.1	4.9	0.5	2.2	9	9	6	SE 3	S 3	C 0
4	97.5	99.4	100.9	99.3	10.7	16.6	12.2	12.9	17.6	10.0	99	69	86	85	0.2	5.9	2.0	2.7	9	9	5	NW 2	NW 1	NW 2
5	101.2	100.5	99.0	100.2	11.0	17.5	10.6	12.4	18.4	6.5	90	56	91	79	1.3	8.8	1.2	3.8	0 ⊙	8 ⊙	8	C 0	SW 2	C 0
6	96.6	96.7	98.4	97.2	12.1	17.3	9.4	12.0	17.6	9.3	83	70	92	82	2.3	6.0	1.0	3.1	10	9	4	SW 3	SW 5	C 0
7	100.4	101.0	101.1	100.8	9.0	18.8	12.5	13.2	20.0	4.7	92	47	86	75	1.0	11.5	2.1	4.9	1 ⊙	6 ⊙	3	C 0	W 4	C 0
8	102.0	102.3	101.6	102.0	13.3	22.1	14.8	16.8	22.6	8.9	77	51	83	70	3.5	13.1	2.9	6.5	0 ⊙	4 ⊙	3	SSW 4	S 4	S 1
9	101.1	100.2	98.6	100.0	14.5	25.2	18.1	19.0	25.7	12.1	93	50	80	74	1.1	16.0	4.1	7.1	4 ⊙	1 ⊙	1	S 2	S 4	S 2
10	101.2	99.7	98.0	99.6	12.7	14.8	12.1	12.9	18.1	11.7	80	71	93	81	2.9	4.8	1.0	2.9	10	10	10	NNE 6	NNE 2	N 2
11	94.8	91.5	85.8	90.7	9.5	15.7	11.9	12.2	17.2	7.0	96	66	87	83	0.5	6.0	1.8	2.8	4 ⊙	9	1	W 1	SW 4	SSE 5
12	78.6	75.4	78.9	77.6	13.3	17.4	13.3	14.3	19.7	10.3	95	83	63	80	0.7	3.4	5.6	3.2	10 ●	10 ●	10	SSE 8	S 7	WSW 8
13	83.4	85.0	84.6	84.3	9.8	13.5	10.4	11.0	15.4	7.8	75	58	74	69	3.0	6.5	3.3	4.3	2 ⊙	9	2	WSW 7	SW 7	S 4
14	82.5	84.5	86.6	84.5	9.8	12.6	10.9	11.0	13.9	7.5	82	65	73	73	2.2	5.2	3.5	3.6	10 ●	9	2	S 5	WSW 7	S 4
15	85.3	78.2	84.3	82.6	6.9	11.0	8.3	8.6	11.8	4.9	94	97	96	96	0.5	0.3	0.5	0.4	10 ●	10 ●	10 ●	S 2	SE 3	SW 7
16	90.1	93.7	96.1	93.3	7.7	11.7	6.0	7.8	12.4	5.6	94	69	92	85	0.6	4.2	0.8	1.9	10	9	0	SW 8	SW 10	SW 3
17	96.0	93.8	90.9	93.6	1.9	12.3	8.1	7.6	13.4	1.0	100	58	89	82	0.0	6.1	1.2	2.4	4 ≡	10	0	C 0	WNW 2	NW 3
18	81.4	76.3	77.1	78.3	7.4	9.3	8.5	8.4	10.0	5.3	99	85	92	92	0.2	1.7	0.9	0.9	10 ●	10 ●	10 ●	W 7	NW 10	NW 6
19	79.7	81.9	83.2	81.6	8.7	10.5	8.3	9.0	11.2	7.8	89	80	93	87	1.2	2.6	0.8	1.5	10	10	6	W 6	W 10	WSW 5
20	82.8	85.5	89.3	85.9	8.4	11.3	8.9	9.4	13.1	7.2	97	90	92	93	0.3	1.3	0.9	0.8	10 ●	9	0	W 4	W 2	W 3
21	92.1	93.5	94.8	93.5	9.1	11.3	8.5	9.4	12.9	7.3	97	85	94	92	0.4	2.0	0.6	1.0	10	9 ●	6	W 4	NW 3	W 2
22	94.3	91.9	88.5	91.6	2.9	12.3	9.2	8.4	12.5	1.7	100	76	99	92	0.0	3.4	0.1	1.2	9 ≡	10	10 ●	C 0	SSE 6	SE 5
23	83.8	81.2	73.5	79.5	13.3	17.2	14.2	14.7	17.8	9.0	99	83	97	93	0.2	3.4	0.6	1.4	10 ●	10	10 ●	S 5	SSW 7	SSE 2
24	75.8	79.7	77.7	77.7	12.0	11.2	5.7	8.6	14.2	5.3	87	71	94	84	1.8	3.9	0.6	2.1	10	10	0	WNW 6	WSW 8	SW 5
25	76.7	82.7	90.1	83.2	6.3	8.3	5.5	6.4	8.9	4.3	91	89	84	88	0.8	1.3	1.4	1.2	9	10 ●	0	W 6	W 14	W 5
26	90.6	91.2	93.0	91.6	4.1	7.9	2.9	4.4	8.2	2.7	97	67	84	83	0.3	3.5	1.2	1.7	10 ●	8	1	W 3	W 7	W 5
27	92.4	89.2	79.9	87.2	3.1	7.7	5.3	5.4	7.8	2.6	84	77	97	86	1.2	2.4	0.3	1.3	4 ⊙	10	10 ●	WSW 6	WSW 7	SW 10
28	70.0	74.4	77.2	73.9	7.5	9.1	6.9	7.6	9.7	5.3	91	66	92	83	0.9	4.0	0.7	1.9	10 ●	10	10 ●	WSW 6	WNW 10	W 6
29	79.2	79.2	77.1	78.5	6.3	9.0	6.1	6.9	10.9	5.6	97	73	97	89	0.2	3.1	0.3	1.2	9	9	10	W 2	WSW 6	S 2
30	76.5	79.1	86.2	80.6	6.4	7.3	5.3	6.1	8.5	5.3	89	86	95	90	1.0	1.5	0.4	1.0	10	10 ●	5	W 3	NW 6	W 5
31																								
M	89.0	89.1	89.3	89.1	9.0	13.5	9.5	10.4	14.6	6.7	92	72	89	84	1.0	4.8	1.4	2.4	7.8	8.8	5.2	4.0	5.7	3.5

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1	89.8	92.2	94.2	92.1	4.3	7.4	4.7	5.3	8.2	4.2	93	70	90	84	0.5	3.1	0.8	1.5	10	9	9	WSW 6	W 8	W 2
2	98.0	100.0	100.0	99.3	2.7	7.4	3.7	4.4	9.8	2.6	95	77	88	87	0.4	2.3	1.0	1.2	9	8	6	WNW 4	NW 4	SW 3
3	96.9	92.2	85.8	91.6	1.1	8.4	6.7	5.7	8.8	0.6	92	62	88	81	0.5	4.1	1.2	1.9	2	9	10 ●	SSW 5	SW 10	SW 8
4	82.8	84.7	90.5	86.0	6.2	8.7	3.7	5.6	9.0	3.5	78	56	87	74	2.2	4.9	1.1	2.7	10	6 ⊙	9	SW 8	WSW 12	WNW 7
5	94.8	95.5	94.6	95.0	2.9	7.3	5.7	5.4	8.4	2.2	93	80	79	84	0.5	2.0	2.0	1.5	3 ⊙	10 ●	10	WSW 5	WSW 7	SW 7
6	90.9	93.8	97.1	93.9	6.9	9.3	7.6	7.8	11.2	5.3	97	97	94	96	0.3	0.3	0.6	0.4	10 ●	10 ●	10	WSW 7	W 4	WSW 4
7	92.9	94.8	100.8	96.2	10.3	11.2	7.8	9.3	11.7	7.4	94	89	90	91	0.8	1.5	1.1	1.1	10	10 ●	2	W 9	W 12	NW 5
8	108.5	110.5	110.0	109.7	4.7	10.3	6.9	7.2	10.9	3.8	94	51	91	79	0.5	6.1	0.8	2.5	7	4 ⊙	9	C 0	SE 2	WSW 2
9	107.7	106.7	104.3	106.2	6.1	14.3	6.2	8.2	15.1	5.2	88	61	94	81	1.1	6.3	0.6	2.7	9	3 ⊙	0	SW 3	SW 3	C 0
10	102.9	102.9	102.0	102.6	3.9	16.5	8.1	9.2	17.2	3.1	98	51	91	80	0.2	9.2	0.9	3.4	2 ⊙	1 ⊙	0	SSW 2	SSW 5	SSW 2
11	99.8	99.3	99.3	99.5	6.3	15.8	12.0	11.5	16.6	5.9	97	64	93	85	0.2	6.4	1.0	2.5	1 ⊙	5 ⊙	10	S 2	SSW 6	C 0
12	96.5	96.1	101.3	98.0	10.1	11.0	8.3	9.4	12.7	8.2	100	99	92	97	0.0	0.1	1.0	0.4	10 ≡	10 ●	0	SSW 5	WSW 5	WNW 3
13	106.0	105.5	102.9	104.8	6.4	9.5	6.1	7.0	10.8	5.8	100	87	94	94	0.0	1.6	0.6	0.7	10 ≡	9	6	SW 4	SW 7	SW 4
14	99.9	99.5	102.1	100.5	7.7	11.9	5.7	7.8	12.2	5.3	97	74	88	86	0.3	3.6	1.2	1.7	10	10	1	SW 3	W 6	W 4
15	104.2	105.8	106.1	105.4	3.9	9.4	4.1	5.4	10.5	2.1	100	71	97	89	0.0	3.4	0.3	1.2	10 ≡	6 ⊙	2	W 3	WNW 4	W 2
16	106.6	105.8	104.0	105.5	4.5	7.8	5.9	6.0	8.4	2.0	97	68	76	80	0.3	3.4	2.3	2.0	9	10	10	C 0	SSW 3	S 2
17	99.0	95.0	95.1	96.4	4.3	12.0	10.1	9.1	12.7	4.1	84	70	90	81	1.4	4.1	1.3	2.3	5	3 ⊙	2	SE 3	S 6	SW 6
18	93.6	90.2	87.2	90.3	6.7	10.9	12.3	10.6	12.6	6.3	97	90	93	93	0.3	1.3	1.0	0.9	10	10	10	SW 5	SW 6	SW 6
19	86.4	87.1	86.7	86.7	11.3	16.1	13.4	13.6	16.5	10.8	93	74	84	84	1.0	4.7	2.5	2.7	8 ⊙	9	0	SSW 5	SW 9	SSW 4
20	86.7	90.6	93.3	90.2	8.9	9.0	7.6	8.3	13.5	7.3	94	85	97	92	0.6	1.7	0.3	0.9	10	10 ●	10	C 0	W 4	WSW 3
21	94.9	95.5	93.7	94.7	5.5	5.9	3.3	4.5	8.0	3.1	97	94	97	96	0.3	0.6	0.2	0.4	9	10	0	WSW 3	SW 6	S 3
22	90.5	88.1	86.8	88.5	3.1	6.9	6.5	5.8	7.2	2.3	97	84	91	91	0.2	1.6	0.9	0.9	8	10	5	SSE 3	SSE 8	SSE 5
23	86.1	87.3	89.7	87.7	6.5	7.9	7.7	7.4	9.4	5.9	96	96	98	97	0.5	0.4	0.1	0.3	10	10	10	SE 4	SSW 3	SW 4
24	88.8	87.9	93.0	89.9	3.8	5.8	7.1	6.0	9.0	3.7	95	97	83	92	0.4	0.3	1.8	0.8	10	10 ●	0	SW 7	SW 8	WSW 7
25	98.2	101.1	103.0	100.8	4.0	8.9	5.5	6.0	9.1	3.1	93	66	89	83	0.5	3.9	1.0	1.8	8	6 ⊙	0	WSW 6	W 8	WSW 4
26	100.8	100.8	99.8	100.5	4.5	9.2	9.9	8.4	11.2	4.3	97	89	84	90	0.3	1.2	1.9	1.1	10 ●	10	10	SW 3	WSW 5	SW 6
27	97.0	96.4	97.1	96.8	4.3	7.5	5.0	5.4	9.9	3.9	100	96	100	99	0.0	0.5	0.0	0.2	10 ≡	10	0 ≡	SW 3	WSW 5	SW 2
28	97.0	97.1	97.4	97.2	6.4	9.3	8.1	8.0	9.6	3.5	97	91	86	91	0.3	1.1	1.5	1.0	10	10	10	SSW 4	SW 3	SW 6
29	95.7	95.6	96.6	96.0	7.7	10.1	7.1	8.0	11.6	6.9	83	77	93	84	1.8	2.9	0.8	1.8	10	10	0	SSW 7	SW 6	SSW 4
30	94.8	92.8	92.1	93.2	4.5	12.0	10.1	9.2	13.1	4.1	98	74	81	84	0.1	3.6	2.4	2.0	3	3	10	SSW 3	SSW 7	SW 4
31	90.8	89.8	88.6	89.7	9.1	10.8	10.9	10.4	11.8	8.7	100	92	81	91	0.0	1.0	2.4	1.1	10 ≡ 9	10	10	SW 3	WSW 5	SW 5
M	96.1	96.1	96.6	96.3	5.8	10.0	7.3	7.6	11.2	4.7	95	78	90	88	0.5	2.8	1.1	1.5	8.2	8.1	5.5	4.0	6.0	4.0

Suwałki $H_s = 165$ m $H_b = 169{,}2$ m $h_w = 12$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	P O G O D A
1	7	29.8	.	1.0	●⁰6³⁰–8³⁰ ●¹–9²⁰ ●²–9³⁰ ●¹–10⁴⁵ ●⁰–12³⁵, 12⁵⁰ 13¹⁵ ▽ 13²⁵–⁵⁰ 14³⁷–15⁴⁰ 19³⁰–20¹⁰ ●¹–22⁴⁵, 23⁰⁵–24, = 22⁴⁵–23⁰⁵
2	7	.	.	9.1	●⁰0⁰⁰–1¹⁵, = 6²⁰–12⁴⁵
3	7	0.0	.	1.4	●⁰14²⁰–³⁵ = 5⁴⁵–10³⁰
4	7	.	.	1.1	= 2⁰⁰–6⁰⁰ ≡¹–7⁴⁰ = –19⁴⁰
5	7	0.0	.	10.2	= 0¹⁵–3¹⁵, 7²⁵–10¹⁵
6	7	.	.	2.5	▽ 6³⁰–40 ⌒¹ n
7	7	.	.	11.5	= 5⁴⁵–8³⁰, ⌒² n–8³⁰
8	7	.	.	10.6	⌒² n–9⁰⁰
9	7	.	.	10.8	= 5²⁰–8³⁰, ⌒² n–9⁰⁰
10	8	1.1	.	0.1	●⁰15⁰⁵–19⁴⁵
11	7	0.1	.	6.1	= 5³⁰–9³⁰ ⌒² n–9⁰⁰
12	7	5.5	.	0.7	●⁰4⁴⁰–8³⁵, 11³⁰–12⁴⁰, 13²⁵ 15²⁰ ▽–16¹⁰, 17¹⁰–³⁰, ⊽¹ 15⁴⁰–16⁰⁰–16¹⁵ S–N
13	8	0.0	.	6.5	
14	7	0.0	.	3.7	●⁰7¹⁰. ⁴⁰ ▽ 15⁴⁰–16¹⁰, 16³⁵–⁵⁰
15	6	31.9	.	.	●⁰8¹⁰–³⁵, 9⁴⁰–15⁴⁰ ▽–19¹⁰ ●⁰–22³⁵
16	7	.	.	3.7	⊽⁰ 4⁴⁵–5¹⁰
17	7	1.4	.	3.7	= 2⁰⁰–⁴⁵ ≡¹–9²⁰ = –12⁴⁵, 16³⁰–21¹⁵
18	6	26.6	.	.	●⁰6¹⁰–12⁴⁵ ●¹ 13²⁰–24
19	7	1.1	.	.	●¹0⁰⁰–7²⁰
20	7	0.8	.	1.8	●¹6⁰⁰–10¹⁵ ▽⁰ 10³³–⁴⁰, 12⁰⁵–²⁰, 13³⁰–⁴⁵, 15¹⁰–¹⁵
21	7	0.8	.	0.5	▽ 12¹⁰–⁴⁰, 13⁰⁵–14⁰⁵, 15⁴⁰–16²⁰, = 2⁰⁰–8³⁰
22	7	3.6	.	.	●⁰1⁷⁴⁵–24, ≡¹ 2⁴⁵–9⁰⁰
23	6	11.9	.	0.2	●⁰0⁰⁰–3⁰⁰, 7¹⁵–8³⁵ ▽ 14³⁰–⁴⁴, 16²⁵–⁴⁵ ●⁰17³⁷–22³⁰, 23¹⁵–24, ≡¹ 3⁰⁰–7¹⁵ = –24
24	7	3.0	.	2.2	●⁰0⁰⁰–2⁰⁰, ●¹–4⁰⁵ ●⁰–6¹⁰, 16¹⁰–19⁴⁰
25	6	23.0	.	0.9	●⁰0⁴⁵–6²⁰ ▽ 7²⁵–⁴⁵, 8⁰⁷–10²⁵ ●⁰–13³⁰ ▽–15³⁵, 16²⁰–17⁴⁰
26	8	1.5	.	4.5	▽ 1²⁰–³⁵, 3³⁵–⁵⁰, 4¹⁰–²⁰, 6⁰⁵–⁴⁵, 7¹⁰–8¹⁵, 9³⁵–11⁰⁵, 14⁰³–16, 16⁴⁵–17¹⁰
27	7	12.2	.	1.8	▽ 11³³–12⁰⁵ ●⁰14⁰⁵–24, = 12⁰⁵–15
28	7	7.2	.	1.5	●⁰0⁰⁰–2⁴⁰, 3¹⁵–5³⁵, 6²⁰–10¹⁵, 15⁰⁵–16¹⁰, 18⁴⁵–22⁴⁰, 23¹⁰–24
29	8	1.1	.	3.6	●⁰0⁰⁰–³⁵ ▽ 9¹⁰–⁵⁵ ●⁰21⁰⁵–24
30	6	3.4	.	0.2	●⁰0⁰⁰–1⁴⁵ ▽ 9²⁵–10²⁰, 11⁴⁵–13⁵⁰, 15⁵⁵–16¹⁰
31					
Σ	–	176.0	–	99.9	UWAGI

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1	7	0.0	.	5.7	●⁰0²⁰–²⁰⁵ ▽⁰ 3³⁰–4³⁰, 5⁵⁰–6¹⁰, 14³⁰–³⁵
2	7	0.0	.	6.3	▽ 12⁴⁰–⁴²
3	7	0.5	.	5.3	●⁰18⁴⁵–21¹⁰ ⌴⁰ 2⁰⁰–7⁰⁰
4	8	1.1	.	4.5	●⁰1⁰⁰ 3⁴⁵ ▲⁰ 13⁰⁵–¹⁰ ▽ 13⁰⁵–⁴⁰, 14²⁰–16⁰⁰ ●⁰–18⁴⁵, ≫ 10⁰⁰–13⁴⁰
5	7	0.9	.	3.1	▽ 12²³–⁵⁰ 13⁰²–¹⁰ ●⁰16³⁰ 17¹⁰ ⌒² n–8⁰⁰
6	5	1.4	.	.	●⁰0³⁰–3¹⁵ ●⁰–5²⁰ ●⁰–7¹⁵ ●⁰–7³⁰, 8²⁵–⁴², 9¹⁰–⁴⁰, 10¹⁵–12⁴⁵ ▽ 22⁴⁰–⁴⁵
7	6	0.0	.	0.9	●⁰5⁰⁵–³⁵, 12²⁵–14³⁵
8	8	.	.	5.7	
9	8	.	.	7.6	
10	7	.	.	5.6	⌒² n–8⁰⁰
11	7	.	.	6.9	= 5¹⁵–8⁰⁰, ⌒² n–8⁰⁰
12	5	2.6	.	.	●⁰8³⁰–10⁴⁰, 11¹⁵–17³⁰ ●⁰–18²⁰, = 10⁰⁰–¹⁵ ≡¹–8³⁰ = –19²⁰
13	6	.	.	0.9	≡¹ 5³⁰–7⁴⁰ = –13¹⁵
14	5	.	.	1.0	= 10⁰⁰–18²⁰
15	7	.	.	4.3	= 4¹⁰–³⁵ ≡¹–8⁴⁰, ⌒² n–9⁰⁰, ⊽¹ 14⁰–3²⁵
16	7	.	.	.	
17	7	0.8	.	6.1	▽ 15³⁰–16¹⁰, = 14²⁰–24
18	6	0.0	.	.	●⁰14⁰⁵–⁴⁰ ●⁰16⁰⁵–17²⁰, = 0⁰⁰–24
19	6	.	.	1.1	= 0⁰⁰–14¹⁵
20	7	2.7	.	.	●⁰ 8¹⁰–9¹⁰, 11¹⁰–²⁵, 12²⁵ 14³⁰–15⁴⁰ ●¹–17⁴⁵
21	6	.	.	0.1	= 0⁰⁰–24
22	7	0.0	.	.	⌒² n–8⁰⁰
23	6	0.2	.	.	●⁰3⁴⁰–4³⁵, 7⁰⁵–11⁴⁰, = 6²⁰–18⁴⁰ ≡¹–19⁴⁵
24	6	2.6	.	.	●⁰8¹⁰–15²⁰, ≫ 8³⁰–12¹⁰, = 5³⁰–20³⁰
25	7	0.3	.	6.1	
26	6	(0.0)	.	0.4	●⁰4²⁵–7³⁵, = 10³⁰–24
27	5	.	.	.	= 0⁰⁰–6¹⁵ ≡¹–10²⁵ = 12⁴⁵–p ≡¹–24
28	6	.	.	.	≡² 0⁰⁰–3⁴⁵ = –18³⁰
29	6	.	.	0.2	= 8³⁰–13⁴⁰
30	6	3.3	.	6.4	= 6¹⁰–19¹⁵
31	6	0.0	.	0.2	●⁰0¹⁵–1⁰⁵ ●¹–1³⁰ ●⁰–3³⁵ ●⁰6¹⁰–9³⁰, 10⁵⁰–11³⁵, = 3³⁵–6¹⁵ ≡¹–7⁵⁰ = –20⁴⁵
Σ	–	16.4	–	82.4	UWAGI.

Suwałki — φ = 54°06' — λ = 22°57' — Listopad – Novembre 1957

DNI	CIŚNIENIE p − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	85.7	88.8	85.7	85.1	9.3	10.7	10.1	10.0	11.2	8.2	91	81	85	86	1.1	2.5	2.0	1.9	9	8	9	S 6	SW 9	SW 5
2	89.4	91.8	93.7	91.6	6.8	10.6	7.5	8.1	11.0	6.5	96	86	96	93	0.5	1.8	0.5	0.9	6	10	6	SW 4	SW 4	SW 1
3	95.9	96.5	96.2	96.2	6.3	9.1	8.3	8.0	9.4	5.4	100	97	96	98	0.0	0.4	0.5	0.3	10	10	10	C 0	SW 1	SSE 3
4	95.6	95.5	96.5	95.9	8.2	9.9	9.9	9.5	10.5	7.5	96	93	99	96	0.5	0.8	0.2	0.5	10 🌧	9	10 🌧	SE 5	SE 4	S 3
5	95.7	94.9	94.6	95.1	9.5	10.3	10.0	10.0	11.4	7.7	96	94	87	92	0.5	0.8	1.6	1.0	10	10	9	SSE 5	SE 8	SE 10
6	94.0	94.2	94.8	94.3	7.3	13.4	9.5	9.9	13.6	7.0	93	71	79	81	0.7	4.5	2.5	2.6	6	3 ⊙	3	SE 7	SE 7	SE 8
7	92.7	91.9	91.1	91.9	6.4	9.7	8.0	8.0	10.5	6.1	91	79	85	85	0.9	2.5	1.5	1.6	10	9	10	SE 9	SE 12	SE 10
8	91.7	92.4	93.3	92.5	6.4	7.7	7.9	7.5	8.7	6.0	94	93	91	93	0.6	0.7	0.9	0.7	10	10	10	SSE 6	SSE 6	SE 7
9	92.0	91.8	92.8	92.2	7.5	9.3	8.3	8.4	9.8	7.1	91	87	96	91	0.9	1.6	0.5	1.0	10	10	10 🌧	SE 4	SE 6	SE 6
10	93.8	95.1	97.8	95.6	7.3	7.4	6.9	7.1	8.3	6.5	100	99	96	98	0.0	0.2	0.4	0.2	10	10	10	E 6	E 7	ENE 6
11	100.0	102.0	104.8	102.3	6.5	6.3	3.8	5.1	7.2	3.6	96	91	90	92	0.5	0.8	0.8	0.7	10	10	10	E 7	ENE 7	E 9
12	107.5	109.1	109.6	108.7	−0.5	−0.3	−2.4	−1.4	4.3	−2.5	98	92	86	92	0.1	0.5	0.7	0.4	10	10	10	NE 7	NNE 5	NNE 1
13	109.2	109.7	108.9	109.3	−3.7	−2.1	1.1	−0.9	1.4	−4.2	92	83	79	85	0.3	0.9	1.4	0.9	10	10	10	C 0	C 0	NW 2
14	106.7	107.7	109.8	108.1	1.3	3.3	3.3	2.8	3.7	0.6	87	85	91	88	0.9	1.2	0.6	0.9	10	10	10	W 3	NW 4	WNW 1
15	110.8	110.6	109.6	110.3	2.9	2.4	0.2	1.4	3.4	0.1	96	89	84	90	0.2	0.8	1.0	0.7	10	10 ●	10	W 2	WSW 2	WSW 3
16	108.6	109.6	111.3	109.8	−0.9	0.1	0.7	0.2	1.1	−1.5	85	90	94	90	0.8	0.7	0.4	0.6	10	10 ✳	10	W 3	W 4	W 1
17	112.3	113.2	114.4	113.3	1.3	4.1	2.3	2.5	4.3	0.6	94	87	91	91	0.4	1.1	0.6	0.7	10	10	10	W 1	W 2	WNW 1
18	114.4	113.8	113.3	113.8	1.9	2.8	1.1	1.7	3.1	1.1	91	67	89	82	0.6	2.5	0.7	1.3	10	10	10	WNW 1	W 2	C 0
19	113.7	115.3	119.0	116.0	0.7	2.5	−0.3	0.6	3.2	−1.5	90	84	96	90	0.6	1.2	0.3	0.7	10	10	9	C 0	WNW 2	NE 2
20	120.7	120.9	119.7	120.4	−0.2	2.3	−0.2	0.4	3.4	−0.6	96	70	84	83	0.2	2.2	1.0	1.1	10	9	10	SE 1	SW 4	SW 2
21	117.2	115.2	110.7	114.4	−1.5	0.9	−1.5	−0.9	2.2	−2.5	89	79	88	85	0.6	1.4	0.7	0.9	8	6	0	SW 2	WSW 2	WSW 2
22	103.9	100.0	96.8	100.2	−4.4	2.4	−1.6	−1.3	2.7	−5.9	93	65	86	81	0.3	2.6	0.7	1.2	2	0 ⊙	0	C 0	SSW 6	SSW 3
23	93.7	92.2	90.2	92.0	−0.1	0.1	0.2	0.1	0.6	−1.9	96	86	96	93	0.3	0.9	0.3	0.5	10	10	10 ✳	SW 4	SW 4	WSW 4
24	92.7	92.1	90.4	91.7	0.1	1.7	3.1	2.0	3.3	0.0	90	78	97	88	0.7	1.5	0.2	0.8	4	10 ✳	10	W 3	W 4	WSW 6
25	87.9	90.5	93.7	90.7	5.1	5.9	3.6	4.8	6.4	3.1	95	95	98	96	0.4	0.5	0.1	0.3	10	10 ●	0	W 6	NW 5	C 0
26	96.2	96.9	91.3	94.8	3.6	5.1	6.2	5.3	6.5	2.9	97	90	97	95	0.3	0.9	0.3	0.5	10	10	10 ●	WNW 1	WNW 1	SW 7
27	83.5	83.2	92.4	86.4	6.2	7.1	−2.8	1.9	7.4	−3.0	95	81	93	90	0.5	1.9	0.4	0.9	9	9	10	W 8	NW 10	N 4
28	89.4	82.4	74.8	82.2	−1.5	2.7	5.4	3.0	6.7	−3.2	92	98	98	96	0.4	0.1	0.2	0.2	10	10 ●	10 ●	SE 4	SSW 4	W 7
29	79.1	87.6	100.3	89.0	−6.8	−9.3	−9.5	−8.8	5.4	−9.9	85	82	69	79	0.5	0.5	0.9	0.6	10 ✳	10 ✳	0	N 10	NNE 12	N 10
30	104.7	105.4	105.7	105.3	−8.7	−7.2	−8.4	−8.2	−7.1	−10.0	77	82	77	79	0.7	0.6	0.7	0.7	10	4 ⊙	0	N 10	N 10	N 9
31																								
M	99.3	99.5	100.1	99.6	2.5	4.3	3.0	3.2	5.8	1.1	93	85	90	89	0.5	1.3	0.8	0.9	9.1	8.9	7.9	4.2	5.1	4.4

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1	104.3	103.3	103.5	103.7	−8.8	−2.7	−4.7	−5.2	−2.6	−9.5	83	75	93	84	0.5	1.2	0.3	0.7	0	9	4	NNW 3	W 1	C 0
2	104.2	105.2	105.1	104.8	−2.9	−1.7	−2.3	−2.3	−1.4	−8.4	97	88	89	91	0.1	0.7	0.6	0.5	10	10	8	C 0	W 1	W 1
3	99.6	99.2	100.6	99.8	−0.5	0.6	0.1	0.1	0.9	−2.5	98	100	98	99	0.2	0.0	0.2	0.1	10	10 〓	10	C 0	N 2	NE 2
4	101.1	99.5	96.6	99.1	−0.5	−0.3	−0.2	−0.3	0.6	−1.5	98	94	98	97	0.2	0.4	0.1	0.2	10 ✳	10	10 ●	C 0	SW 3	SSW 7
5	89.0	89.0	93.8	90.6	1.7	4.5	2.9	3.0	4.7	−0.4	98	85	95	93	0.1	1.2	0.4	0.6	10 🌧	9	10 ●	SW 4	NW 7	NNW 6
6	102.1	104.7	102.6	103.1	−1.1	−1.1	−4.0	−2.6	3.1	−4.4	85	73	89	82	0.9	1.6	0.5	1.0	9	4 ⊙	0	NE 5	NE 1	NE 2
7	94.2	89.5	85.1	89.6	−3.3	−1.3	−1.3	−1.8	−0.9	−4.8	90	90	95	92	0.5	0.5	0.3	0.4	8	8	10	SSW 7	SW 9	SW 7
8	73.5	65.1	53.0	63.9	−1.9	−1.5	−0.1	−0.9	0.2	−2.2	90	94	98	94	0.5	0.3	0.2	0.3	10	10	10 ✳	S 6	S 8	S 10
9	46.7	52.4	66.8	55.3	2.3	1.9	−3.1	−0.5	3.2	−3.4	93	94	70	86	0.5	0.4	1.4	0.8	10 ●	10 ●	4	SSW 8	WNW 7	W 10
10	69.9	71.6	74.5	72.0	−2.3	−1.1	−3.8	−2.8	−0.8	−5.3	91	73	76	80	0.5	1.6	1.1	1.1	10 ✳	9 ✳	10	WSW 9	WNW 7	WSW 7
11	80.3	86.6	89.2	85.4	−2.9	−1.9	−6.1	−4.2	−1.6	−6.4	56	60	84	67	2.2	2.1	0.6	1.6	9	6	2	W 10	WSW 4	C 0
12	87.1	84.8	81.9	84.6	−6.5	−4.6	−4.3	−4.9	−3.9	−8.0	83	93	89	88	0.6	0.3	0.5	0.5	4	10 ✳	10	E 6	E 8	E 4
13	79.9	77.4	70.7	76.0	−3.4	−2.1	0.7	−1.9	1.0	−4.9	92	96	98	95	0.4	0.2	0.1	0.2	10	10	10 ●	ESE 5	E 3	E 3
14	63.1	67.8	80.9	70.6	0.5	−5.5	−8.4	−5.4	1.9	−8.6	100	90	83	91	0.0	0.4	0.5	0.3	10	10 ●	10	NNE 6	N 10	NNE 8
15	94.9	101.0	106.0	100.6	−11.3	−8.0	−10.3	−10.0	−7.8	−11.6	86	81	81	83	0.4	0.6	0.5	0.5	3	9	0	NNE 5	NE 4	C 0
16	108.3	108.6	109.4	108.8	−10.5	−6.3	−9.1	−8.8	−5.4	−12.8	87	76	82	82	0.4	0.9	0.5	0.6	1	9	0	SSW 1	SSW 7	SW 2
17	106.8	103.7	102.4	104.3	−12.4	−5.7	−10.9	−10.0	−4.6	−13.2	81	67	87	78	0.4	1.3	0.4	0.7	1	1 ⊙	0	C 0	SSW 2	C 0
18	101.3	102.0	103.7	102.3	−12.9	−6.3	−10.9	−10.2	−4.4	−14.2	88	65	94	82	0.3	1.3	0.2	0.6	1	0 ⊙	0	C 0	C 0	C 0
19	105.4	107.8	109.4	107.5	−13.5	−9.6	−6.5	−9.0	−6.2	−14.4	92	85	91	89	0.2	0.4	0.3	0.3	2	9	10	C 0	C 0	S 1
20	108.3	108.1	106.4	107.6	−3.9	−2.1	−0.6	−1.8	−0.3	−6.6	94	96	95	95	0.3	0.2	0.3	0.3	10	10	10	SSW 4	WSW 3	WSW 7
21	101.8	99.4	101.8	101.0	−1.8	0.9	1.7	0.6	2.0	−2.4	94	85	94	91	0.3	1.0	0.4	0.6	3	10	10	SW 7	WSW 10	WSW 5
22	103.4	103.2	103.2	103.2	1.1	1.3	1.1	1.2	2.2	0.6	90	94	96	93	0.6	0.4	0.2	0.4	10	10 🌧	10	SW 6	WSW 6	SW 5
23	102.4	101.9	99.2	101.2	0.5	1.0	−1.7	−0.5	1.3	−2.0	100	100	88	96	0.0	0.0	0.7	0.2	10 〓 🌧	10	0	SW 4	S 4	SSE 4
24	97.2	97.4	98.3	97.6	−4.5	−2.9	−5.4	−4.6	−1.4	−6.0	93	82	90	88	0.3	0.9	0.4	0.5	10	5 ⊙	0	SW 4	S 1	SW 1
25	98.7	97.5	95.6	97.3	−5.1	−3.3	−2.3	−3.2	−2.2	−6.7	90	83	91	88	0.4	0.8	0.5	0.6	10	5 ⊙	10	SSW 3	S 2	SSW 4
26	96.6	98.4	100.7	98.6	−2.5	−0.3	0.9	−0.2	1.3	−3.2	98	96	96	97	0.1	0.3	0.2	0.2	10	10	10	SW 4	SW 5	WSW 4
27	100.1	99.0	97.5	98.9	0.9	0.9	0.8	0.9	1.6	0.5	98	98	98	98	0.1	0.1	0.2	0.1	10	10 🌧	10 🌧	SW 5	SW 5	SW 6
28	93.5	89.6	84.7	89.3	1.4	1.5	1.7	1.6	2.4	0.6	100	98	92	97	0.0	0.1	0.5	0.2	10	10 ●	10 ●	SW 7	SW 8	SW 6
29	81.1	80.7	78.5	80.1	1.1	1.3	0.3	0.8	1.8	0.1	94	92	96	94	0.4	0.5	0.2	0.4	10	9	10 ✳	SW 6	WSW 5	SW 6
30	69.0	70.9	70.9	70.3	1.5	2.1	0.5	1.0	2.5	−0.1	92	71	90	84	0.5	2.0	0.6	1.0	10	9	9	SW 10	SW 10	W 5
31	72.4	74.3	75.5	74.1	−0.3	0.3	−0.5	−0.2	0.9	−0.8	86	86	86	86	0.9	0.8	0.9	0.9	9	9	10	WSW 7	WSW 7	SW 8
M	91.5	91.6	91.9	91.7	−3.3	−1.7	−2.8	−2.6	−0.4	−5.2	91	86	90	89	0.4	0.7	0.4	0.5	7.7	8.4	7.0	4.6	4.9	4.2

Suwałki $H_s = 165\ m$ $H_b = 169{,}2\ m$ $h_w = 12\ m$ **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	7	.	.	0.4	= 645 – 1030
2	7	0.3	.	1.4	= 610 – 1030, 2115 – 24 · ⌒1 n – 800
3	6	0.3	.	.	●0 404 – 645, 740 – 930, 1025 – 1235 · = 000 – 645 ≡1 – 730 = – 24
4	6	0.0	.	.	●0 100 – 45, 620 – 810, 2005 – 2130 · = 000 – 24
5	6	.	.	.	= 000 – 835 ≡1 – 940 = – 1430 · ≫ 1535 – 1645, 1910 – 50
6	7	.	.	6.3	= 845 – 1145
7	7	0.7	.	2.3	●0 2130 – 24 · ≫ 715 – 2030
8	7	0.0	.	.	●0 000 – 340, ●0 945 – 1010 · = 1130 – 1840
9	7	0.1	.	.	●0 1345 – 24
10	5	0.0	.	.	●0 000 – 145, 340 – 450 ●0 730 – 815 ●0 1125 – 1215 · = 100 – 645 ≡1 – 730 = – 1730
11	7	0.0	.	0.1	●0 240 – 350, 425 – 545 ●0 1045 – 1120 · = 015 – 610
12	7	.	.	.	● 345 – 615 · = 345 – 745
13	7	.	.	.	
14	7	.	.	.	
15	7	0.0	.	.	▽ 920 – 1010, 1215 – 1315 · = 610 – 1010
16	6	0.0	.	.	✳0 830 – 1325 · = 1325 – 1815
17	6	0.0	.	.	●0 315 – 40, 420 – 535, 1610 – 1715 · = 535 – 1300
18	7	.	.	.	
19	7	0.0	.	.	✳0 730 – 945
20	7	.	.	0.3	⌴1 n – 910
21	7	.	.	2.7	⌴1 n – 1005
22	7	.	.	6.6	= 605 – 1215 · ⌴2 n – 24
23	6	3.6	.	.	✳0 935 – 1015, 1305 – 2340 · = 730 – 24
24	6	1.7	3	0.7	●0 745 – 515 ✳1 1240 – 1335 ✱0 – 1505 ●0 – 1540 · = 000 – 515, 1540 – 24
25	6	0.1	.	.	●0 100 – 620, 725 – 1500, 1810-30 · = 020 – 1319, 2010 – 24
26	7	5.7	.	.	●0 1415 – 1530 ●0 – 2330 · = 000 – 1015 1415 – 24
27	7	2.9	.	.	●0 015 – 610, 745 – 810, ▽ – 1035, 1115 – 1210, 1345 – 1405 · = 000 – 610
28	5	19.1	.	.	✳0 310 – 615 ●0 720 – 915 (marznąca), 915 – 1210 ●0 – 1335 ●0 – 1540 ●0 – 1730 ●1 1815 – 24 · = 615 – 24
29	5	0.2	3	.	●1 000 – 145 ✳1 – 310 ✳0 – 1640 · ≫ 100 – 24
30	8	0.0	3	3.2	✳0 715 – 815 · ≫ 000 – 830
31					
Σ	—	34.7	—	24.0	UWAGI.

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1	8	.	1	2.3	
2	6	0.2	1	.	= 605 – 1430
3	2	0.3	2	.	✳0 110 320 – 515 ●0 1400-15 ✳0 1420 – 1825 ✱0 – 1835 ●0 1920 – 2035, 2220 – 23·0 · = 515 – 615 ✱0 – 1345 = – 2220 = 0 – 24
4	7	1.4	1	.	✳0 635 – 720 1915 – 2030 ●– 2110 ●– 2205 · ≡0 000 – 430 = – 1130
5	7	1.1	.	0.3	●0 310 – 730 ▽ 2015 – 2110
6	8	.	.	4.7	⌴1 1900 – 24
7	7	.	.	0.6	= 2020 – 24 · ⌴1 000 – 912
8	6	9.8	.	.	✳0 745 – 1110 ✳1 1435 – 1715 ✳0 – 2230 ●0 – 24 · ≡0 025 – 240 = – 24
9	7	2.9	pż.	.	●0 000-20 615 – 1315 ✱0 – 1430 ✳1 – 1515 ✱ 2110-15
10	6	0.2	5	2.2	✱ 020 – 110, 215 – 420, 605 – 946, ⌓ – 1320, 1440 – 1615, 1825 – 1910
11	8	.	3	3.8	✱ 215 – 50, 310 – 45
12	5	1.6	3	.	✳0 1115 – 2030
13	5	7.4	5	.	●0 1845 – 24 · = 000 – 730 ≡1 – 1145 = – 1550 ≡1 – 1845 = – 24 · ▼0 730 – 1930
14	6	0.4	3	.	●0 000 – 335 ●0 835 – 1010 △0 1135 – 1215 ○0 – 1310 (marznący) ✳1 – 1340, 1615 – 1725 · = 000 – 630 ≡1 – 1040 = – 1915 ·
15	7	0.0	2	.	✳0 100 · 402 850 · 1025 [14.XII: ≫ 1140 – 2000 · ○0 1615 – 1725
16	7	.	2	0.5	V0 115 – 1100
17	7	.	2	5.4	
18	7	.	2	6.3	= 940 – 1220
19	7	.	2	.	≡1 745 – 1045 = – 1545 ≡1 – 1945 = – 24 · V0 815 – 24
20	5	.	2	.	= 000 – 24 · V0 000 – 830
21	7	0.0	2	.	●0 1840 – 1945 · = 000 – 830 · ≫ 1015 – 1420
22	5	1.3	pż.	.	●0 1120 – 1445, 1825 – 1910 · = 935 – 1340 ≡1 – 1940 = – 24
23	5	0.0	pż.	.	●0 010 – 740 · ≡1 100 – 1230 · = – 24
24	6	.	pż.	2.2	= 000 – 24
25	6	.	pż.	2.8	= 000 – 24
26	5	0.0	pż.	.	● 1035 – 1110 ✳0 1310 – 40 · = 000 – 745 ≡1 – 1130 = – 1445 ≡0 – 1930 = – 24
27	5	0.1	pż.	.	●0 1215 – 1825, 1920 – 2130 · = 000 – 24
28	5	1.6	pż.	.	●0 1240 – 1345, 1620 – 1750, 2005 – 24 · = 000 – 24
29	6	1.6	pż.	.	●0 000 – 105 ✱0 900-20 ●0 1020 – 1110 ✱ – 1145, 1335 – 1415 ✱ 1530 – 1610, 2005 – 2140 · = 000 – 1330
30	8	1.3	1	0.7	✳0 015 – 135 ✳1 – 240 ✱ 725 – 40 815 – 935 ▲1 925 – 30 ✱ 1640 – 1725 · ≫ 230 – 1430
31	7	0.5	1	.	✳0 020 – 35, 840 – 1215, 1525 – 1615, 2315 – 24
Σ	—	31.7	—	31.8	UWAGI.

Olsztyn – Dajtki

$\varphi = 53°46'$ $\lambda = 20°25'$

Styczeń – Janvier 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			SIEROKIEK i PREDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.3	100.9	100.6	100.9	-8.5	-7.7	-6.6	-7.4	-6.5	-9.5	83	84	94	87	0.5	0.5	0.2	0.4	10 ✳	10	10	SE 4	SE 2	SE 1
2	98.8	97.8	97.5	98.0	-4.1	-2.7	-0.8	-2.1	-0.7	-7.0	89	89	89	89	0.5	0.6	0.6	0.6	10	10	10	ESE 2	E 3	E 3
3	102.4	104.3	105.5	104.1	-1.4	-0.7	-1.3	-1.2	0.3	-1.5	92	89	93	91	0.4	0.6	0.4	0.5	10	10	10 △	SW 1	C 0	C 0
4	106.0	106.5	107.2	106.6	-1.4	0.9	-1.9	-1.1	2.1	-2.2	100	88	96	95	0.0	0.7	0.2	0.3	10 ≡	10	10	C 0	S 3	S 3
5	104.3	99.1	93.5	99.0	-2.8	0.6	3.8	1.4	4.1	-3.6	91	98	98	96	0.5	0.1	0.1	0.2	10	10 ≡	10	S 6	S 6	SSW 6
6	89.4	86.4	86.6	87.5	6.9	8.6	3.7	5.7	8.9	3.4	99	90	68	86	0.1	1.1	2.6	1.3	10 ●	10	0	SW 4	WSW 9	W 10
7	91.5	97.7	104.6	97.9	3.0	3.6	1.8	2.6	4.7	1.6	79	78	91	83	1.6	1.7	0.7	1.3	10	9	5	WNW12	W 8	WNW 4
8	105.6	103.0	101.3	103.3	2.7	3.8	5.9	4.6	6.1	1.6	93	98	94	95	0.5	0.1	0.6	0.4	10	10 ● ≡	10	W 3	WSW 5	WSW 5
9	100.2	98.2	95.8	98.1	6.4	6.5	6.9	6.7	7.1	5.7	97	88	81	89	0.3	1.2	1.8	1.1	10 ●	10	10	WSW 6	WSW 6	WSW 9
10	92.0	90.0	90.8	90.9	4.2	4.2	1.7	3.0	7.0	1.6	75	69	80	75	2.0	2.5	1.4	2.0	4	9	10	W 8	W 7	WSW 6
11	92.9	97.0	98.2	96.0	0.8	1.8	-0.2	0.6	2.1	-0.5	88	80	90	86	0.8	1.5	0.6	1.0	9	8 ⊙	2	W 4	WNW 4	W 4
12	94.8	88.5	84.2	89.2	-1.3	-0.6	0.4	-0.3	0.7	-1.5	86	96	96	93	0.8	0.2	0.3	0.4	4	10 ✳	10 ✳	W 6	SW 3	SW 3
13	86.4	89.6	97.7	91.2	0.1	-0.1	-5.8	-2.9	0.6	-5.8	96	98	82	92	0.3	0.2	0.7	0.4	10 ✳	10 ✳	10 ✳	C 0	ENE 3	NE 6
14	105.2	109.9	113.4	109.5	-9.5	-8.8	-11.2	-10.2	-5.8	-11.6	75	65	79	73	0.7	1.1	0.5	0.8	9	2	0	NE 5	NE 5	NE 2
15	113.8	112.3	111.2	112.4	-10.1	-10.0	-16.5	-13.3	-9.6	-16.8	84	78	85	82	0.4	0.6	0.2	0.4	8	6 ✳	0	ENE 5	ENE 5	C 0
16	112.9	113.4	113.5	113.3	-19.1	-9.1	-7.8	-10.9	-7.4	-20.6	89	79	84	84	0.1	0.6	0.5	0.4	0	5 ⊙	9 ✳	C 0	SSW 11	SSW 1
17	112.0	111.9	112.0	112.0	-4.4	-1.1	0.5	-1.1	0.9	-8.6	89	94	92	92	0.5	0.3	0.5	0.4	10	10	10	SW 3	W 1	W 2
18	109.4	108.7	107.9	108.7	-1.8	0.4	-2.9	-1.8	0.7	-4.5	92	76	91	86	0.4	1.5	0.4	0.8	8	0	10	W 5	W 5	W 2
19	108.2	110.2	111.2	109.9	-0.4	-0.9	-2.4	-1.5	0.1	-3.1	88	96	95	93	0.7	0.2	0.2	0.4	10	10	10	W 3	W 3	W 3
20	108.7	107.3	103.4	106.5	-1.6	-0.8	-0.8	-1.0	0.0	-3.3	94	93	90	92	0.3	0.4	0.6	0.4	10 ✳	10	10	SW 4	SW 5	SW 12
21	99.1	100.6	102.8	100.8	-4.3	-2.6	-1.8	-2.6	-0.8	-4.6	85	84	88	86	0.6	0.8	0.7	0.7	4	10	10	SW 7	SW 6	SW 5
22	103.3	103.0	100.4	102.2	-2.6	-2.4	-4.1	-3.3	-1.5	-4.3	98	65	66	76	0.1	1.8	1.5	1.1	10 ●	0	0	SW 4	SSW 3	SSW 2
23	99.2	100.6	101.8	100.5	-6.8	-0.9	-3.0	-3.4	-0.5	-10.0	85	73	79	79	0.5	1.5	1.0	1.0	10	6 ⊙	4	SW 2	SSW 3	SSW 2
24	100.3	98.6	94.9	97.9	-10.5	-3.1	-3.6	-5.2	-2.7	-11.8	90	86	85	87	0.3	0.7	0.7	0.6	3	10	10	SSW 1	E 3	E 2
25	91.8	91.3	94.0	92.4	-3.4	-2.2	-2.6	-2.7	-0.8	-4.0	93	94	91	93	0.4	0.3	0.5	0.4	10 ✳	10 ✳	6	E 1	SE 1	SW 2
26	99.1	101.7	100.2	100.3	-1.0	1.2	-0.6	-0.2	2.0	-4.9	99	85	94	93	0.1	1.1	0.3	0.5	10 ≡	4	10	SW 2	WSW 2	S 2
27	92.8	93.5	96.8	94.4	0.4	2.2	1.7	1.5	3.2	-1.1	96	96	80	91	0.3	0.3	1.4	0.7	10 ✳	10 ≡	0	S 5	SW 4	SW 6
28	99.0	102.6	109.4	103.7	-0.6	0.6	1.0	0.5	1.7	-1.0	91	94	85	90	0.5	0.4	1.0	0.6	7	10 ✳	10	SSW 3	SW 1	W 2
29	112.0	111.0	109.1	110.7	-0.3	1.6	1.0	0.8	1.6	-0.6	92	81	90	88	0.5	1.3	0.7	0.8	10	10	10	SW 4	SSW 4	SW 3
30	106.5	104.3	102.9	104.6	1.3	4.2	-0.3	1.2	4.4	-0.4	98	72	94	88	0.1	2.2	0.4	0.9	10	5	0	S 1	S 2	C 0
31	104.1	105.7	105.9	105.2	0.4	1.7	1.2	1.1	1.9	-1.0	96	89	98	94	0.3	0.8	0.2	0.4	10	10	10	SSE 1	SE 1	SE 1
M	101.4	101.5	101.8	101.6	-2.2	-0.4	-1.4	-1.4	0.8	-4.2	90	85	88	88	0.5	0.9	0.7	0.7	8.6	8.2	7.3	3.6	3.7	3.5

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1	101.9	100.9	99.1	100.6	1.0	1.4	1.8	1.5	2.3	0.7	94	96	96	95	0.4	0.3	0.3	0.3	10 ✳	10	10 ●	SE 3	S 4	S 5
2	98.4	103.3	106.7	102.8	2.4	7.6	3.6	4.3	8.5	1.4	89	64	80	78	0.8	3.7	1.6	2.0	10	7	5	SW 4	WSW 5	SW 3
3	107.7	108.1	109.8	108.5	1.3	4.3	0.0	1.4	5.5	0.0	92	82	92	89	0.5	1.5	0.5	0.8	8	9	0	SW 2	WSW 2	C 0
4	110.2	107.5	103.5	107.1	-2.4	1.4	1.1	0.3	1.8	-3.0	98	87	98	94	0.1	0.9	0.1	0.4	10 ≡	8	10	C 0	SSE 2	S 2
5	103.7	102.9	100.8	102.5	2.4	4.6	3.3	3.4	4.8	0.9	100	100	95	98	0.0	0.0	0.4	0.1	10 ≡	10 ≡	5	SSW 1	SW 3	SSW 2
6	98.2	95.9	93.1	95.7	0.8	5.6	3.8	3.5	6.0	0.0	100	77	88	88	0.0	2.1	0.9	1.0	10 ≡	0	5	ESE 3	S 5	S 2
7	93.8	93.9	93.9	93.9	4.6	6.1	4.4	4.9	6.6	2.8	93	77	74	81	0.6	2.1	2.2	1.6	10	2	9	SW 4	WSW 4	WSW 7
8	94.8	91.5	85.1	90.5	2.2	5.0	3.8	3.7	5.3	1.5	87	83	95	88	1.0	1.5	0.4	1.0	8	10	10 ●	WSW 4	SW 3	SSW 2
9	81.3	80.8	82.2	81.4	5.6	7.3	4.4	5.4	7.6	3.3	98	88	84	90	0.2	1.2	1.4	0.9	10	10	5	SW 3	SW 5	SW 8
10	83.7	86.7	89.8	86.7	2.6	3.9	2.2	2.7	5.0	2.0	95	93	91	93	0.4	0.6	0.7	0.6	10 ●	10	9	NW 10	WSW 3	WSW 2
11	89.5	89.7	92.5	90.6	0.4	2.9	1.5	1.6	3.2	-1.0	94	96	87	92	0.4	0.2	0.9	0.5	9	10 ●	10	C 0	SW 2	SW 1
12	94.7	93.8	89.7	92.7	0.2	2.8	2.7	2.1	3.4	-0.4	88	65	82	78	0.7	2.6	1.3	1.5	9	9	10	SW 3	SE 2	SE 3
13	85.0	82.3	76.5	81.3	2.7	5.6	3.0	3.6	6.9	2.4	86	78	90	85	1.0	2.0	0.8	1.3	10 ●	5	4	SSE 2	SSE 2	SSE 4
14	70.2	71.1	71.4	70.9	4.1	7.4	6.2	6.0	7.9	2.9	92	87	86	88	0.7	1.3	1.3	1.1	10 ●	10	10	SSW 6	S 3	SE 3
15	71.7	72.9	70.3	71.6	1.4	6.1	4.2	4.0	6.7	1.3	91	72	82	85	0.7	2.7	0.6	1.3	6	4	10 ●	S 3	SSW 6	SE 3
16	69.3	75.2	81.2	75.2	3.8	3.6	1.0	2.4	4.7	0.8	97	93	92	94	0.3	0.5	0.5	0.4	10	10 ●	3	S 3	WSW 4	SW 2
17	86.1	88.5	89.4	88.0	0.7	2.0	0.3	0.8	2.4	-0.1	94	89	88	90	0.4	0.8	0.7	0.6	10	10	0	SSW 4	SSW 4	S 1
18	90.0	90.1	85.5	88.5	1.3	4.4	3.0	2.9	6.0	-0.5	94	74	96	88	0.4	2.2	0.3	1.0	10	3	10 ●	SW 2	S 2	SSE 1
19	77.4	81.7	90.8	83.3	3.4	0.5	0.9	1.4	3.7	-0.1	98	100	83	94	0.1	0.0	1.1	0.4	10 ●	10 ✳	10	E 1	WNW 6	W 6
20	94.4	95.2	93.4	94.3	-0.4	1.7	0.5	0.6	2.2	-0.8	92	87	96	92	0.5	0.9	0.2	0.5	10	10 ●	8	SSW 3	S 2	ESE 1
21	91.3	91.8	93.3	92.1	0.1	6.3	3.5	3.4	6.6	-0.4	96	70	88	85	0.3	2.8	0.9	1.3	5	4	10	C 0	S 2	S 1
22	96.2	97.3	96.7	96.7	0.6	2.3	-1.9	-0.2	3.7	-2.3	84	66	96	82	1.0	2.4	0.2	1.2	10	9	0	W 3	WNW 5	C 0
23	96.5	95.8	95.1	95.8	-2.0	-0.4	-1.2	-1.2	0.0	-3.4	94	92	91	92	0.4	0.5	0.5	0.5	10	10 ✳	8	C 0	C 0	SW 1
24	92.2	89.5	88.9	90.2	-2.6	0.8	-1.6	-1.2	0.9	-2.7	93	69	86	83	0.3	2.0	0.7	1.0	10	4	10	C 0	SE 3	ESE 2
25	90.9	91.6	92.0	91.5	-2.1	-0.4	-0.7	-1.0	0.2	-3.0	96	90	89	92	0.2	0.6	0.6	0.5	10 ✳	10	10	NE 1	NNE 3	NE 2
26	96.1	99.9	103.7	99.9	-1.3	0.4	-0.7	-0.6	0.7	-1.9	90	78	79	82	0.5	1.4	1.2	1.0	10	9	10	NNE 3	NNE 3	NNE 2
27	106.4	108.2	109.9	108.2	-1.9	-0.9	-1.4	-1.4	-0.4	-2.1	89	77	74	80	0.6	1.3	1.4	1.1	10	10	10	C 0	E 1	C 0
28	112.3	114.2	116.6	114.4	-2.6	-0.7	-3.8	-2.7	-0.1	-4.1	87	69	87	81	0.7	1.8	0.6	1.0	8	9	0	C 0	NNE 3	NNW 1
29																								
30																								
31																								
M	92.3	92.9	92.9	92.7	0.9	3.3	1.6	1.8	4.0	-0.2	93	82	88	88	0.5	1.4	0.8	0.9	9.4	7.9	7.2	2.4	3.2	2.4

Olsztyn – Dajtki

H_s = 133 m H_b = 138,7 m h_w = 12 m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.2	6	–	✳° 0⁰⁰–⁴⁵ , 1³⁵–11²⁵ ; = 8²⁰–24
2	6	.	6	–	= 0⁰⁰–24
3	5	0.5	6	–	△ 18³⁵–24 , = 2⁰⁰–24
4	6	.	7	–	△ 0⁰⁰–1³⁵ , = 0⁰⁰–6⁴⁰ ≡° –7⁵⁰ = –24
5	3	9.9	5	–	•° 13²²–20²⁰ ; = 0⁰⁰–9¹⁵ ≡° –14⁴⁵ = –24
6	6	7.3	pł.	–	•° 3²⁵–17²⁰ , = 0⁰⁰–13²⁵
7	7	0.1	.	–	•° 0²⁰–2⁴⁰ , •¹–5²⁰ •°–6¹⁰
8	1	0.5	.	–	•° 4²⁵–7³⁰ •°–10²⁵ , 11²⁵–13²⁵ , 15⁴⁰–17⁵⁰ •°–18⁴⁰ •°–20⁰⁵ , 21³²–24 , ≡ 11¹⁵–15⁴⁰ = –24
9	6	0.0	.	–	•° 0⁰⁰–³⁰ , 6⁰⁶–8²⁵ , = 0⁰⁰–24
10	7	0.5	.	–	•° 3³⁰–5²⁰ △° 21⁴⁵–22¹⁵ = 0⁰⁰–5⁴⁰
11	8	0.0	1	–	△¹ 4⁴⁰–5²² ✳ 9⁴⁰–⁵¹ , 13²⁰–⁴⁰ , 17⁰⁷–³⁰ , 17⁴⁰–18¹⁰
12	6	3.4	1	–	✳° 9⁴⁰–13³⁵ , 15²⁰–24
13	3	0.8	6	–	✳° 0⁰⁰–22²⁰ , = 7⁴⁰–8²⁰ ≡ – 13²⁵ = – 19³⁰
14	7	.	9	–	⊹ 12¹⁰–15¹⁰
15	7	0.0	9	–	✳° 9¹⁵–13¹³
16	7	0.0	9	–	✳ 18³⁰–19³⁰ , 20⁵⁰–21⁰⁵
17	5	.	10	–	✳ 3²⁰–6¹⁰ = 7²⁰–24
18	7	0.0	10	–	•° 23⁴⁰–24 , = 0⁰⁰–8²⁰
19	7	0.0	8	–	•° 0⁰⁰–5²⁰ , = 21¹⁰–24
20	7	0.2	8	–	•° 3⁰⁶–5⁵⁰ ✳°–9³⁵ , = 0⁰⁰–9²⁰
21	7	0.0	8	–	•° 15⁴⁰–18³⁰ , = 7²⁰–24
22	6	0.0	7	–	•° 6²⁰–8⁴⁰ , = 0⁰⁰–24 , ∞ 6⁴⁰–7⁰⁰
23	6	.	7	–	= 0⁰⁰–24
24	6	0.0	7	–	= 0⁰⁰–24
25	5	0.6	8	–	✳° 3¹⁰–7²⁰ ✳¹ 9⁰⁵–12¹⁰ ✳°–14²⁰ , = 0⁰⁰–24
26	6	1.4	9	–	= 0⁰⁰–3⁴⁰ ≡° –10⁵⁵ ▼ 7¹⁰–8⁴⁰
27	3	1.8	9	–	✳° 3⁵⁰–4³⁰ ✳¹–8²⁵ ✳°–8⁵⁰ •°–9¹⁰ , = 0⁰⁰–11³⁵ ≡° –14²⁰ = –20¹⁵
28	5	1.0	6	–	△ 7¹⁰–¹⁴ ✳° 10³⁵–13²⁰ , = 13²⁰–24
29	7	0.1	4	–	= 0⁰⁰–6¹⁰ , 14²⁵–24
30	6	.	3	–	•° 3¹⁰–6¹⁵ , = 0⁰⁰–24
31	6	2.6	2	–	✳° 14³⁷–⁴⁵ •°–14⁵⁰ , 17¹⁰–⁴⁰ , = 0⁰⁰–24
Σ	–	30.9	–	–	UWAGI

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1	6	7.3	pł.	–	•° 1²⁰–2⁴⁵ , 3⁴⁰–6²⁵ ✳°–7¹⁰ •° 17³⁰–18⁵⁰ , 19²⁰–24 , = 0⁰⁰–24
2	7	.	pł.	–	•° 0⁰⁰–2⁴⁰ •° 4¹⁰–6²⁰ , = 0⁰⁰–10¹⁰
3	7	.	.	–	= 21⁴⁰–24
4	7	3.2	.	–	•° 13⁴⁰–18²² , = 0⁰⁰–1⁴⁰ ≡° –8⁵⁰ = –11³⁰ , 18²²–24 , ⌴° 1³⁰–10¹⁵ ▼ 7⁰⁵–10¹⁵
5	3	.	.	–	= 0⁰⁰–¹⁵ ≡° –14⁵⁰ = –24
6	6	2.0	.	–	= 0⁰⁰–6⁴⁸ ≡° –7⁴⁰ ≡¹ –10⁴⁵ = –24 ; ⌔ 20¹⁰– n
7	7	.	.	–	•° 0²⁵–5²⁰ , = 0⁰⁰–12²⁰
8	6	5.0	.	–	•° 12⁵⁵–13³⁵ 15⁴⁰–16¹⁵ , 17⁰⁵–24 , = 7⁵⁰–17⁰⁵
9	6	8.1	.	–	•° 0⁰⁰–5³⁰ 9²⁰–10¹⁵ 15¹⁰–17¹⁰ , 18¹⁰–⁵⁰ , = 5³⁰–17⁵⁰
10	7	0.6	.	–	▽ 3³⁵–5⁵⁰ , 6²⁰–8¹⁵ •°–12²⁵
11	6	1.3	.	–	•° 7⁵⁰–8³⁰ •°–9⁴⁰ •° 11⁴⁰–14³⁵ ✳°–16³⁰ •°–19²⁰ , = 3⁴⁰–24
12	7	0.0	.	–	✳° 0⁰⁰–4¹⁰ , = 0⁰⁰–8¹⁰
13	6	3.2	.	–	✳° 4³⁰–57 •° 5²⁰–10²⁰
14	7	1.4	.	–	•° 0²⁰–10³⁵ , = 10³⁵–12¹⁰
15	7	3.0	.	–	•° 0²⁰ 2²⁰ , 17⁴⁰–24
16	6	1.1	.	–	•° 0⁰⁰–6²⁵ , 7²⁵–13³⁰ , = 6²⁵–13⁰⁰
17	6	2.5	.	–	✳° 11¹⁵–³⁵ , = 2⁴⁰–21²⁰ , ⌴° 1³⁰–α
18	7	14.8	2	–	✳¹ 0⁴⁰–1⁴⁸ •° 4¹⁰–5⁴⁰ , 17¹²–18¹⁵ •¹–24 , = 4¹⁰–11³⁰
19	5	3.5	.	–	•¹ 0⁰⁰–8²⁹ ✳°–9³⁰ ✳¹–13⁴⁰ •°–14¹⁰
20	6	1.7	pł.	–	•° 12¹⁰–13⁰⁰ ✳°–14⁰⁰ ✳¹–16¹⁰ , = 6¹⁵–24
21	6	0.9	.	–	•° 2¹⁰–24 , = 0⁰⁰–24
22	8	0.0	.	–	•° 0⁰⁰–5⁴⁰ △ 7¹⁸–6²⁵ , 8²¹–²⁶ 8⁴⁹–⁵⁵ , 9¹⁰–¹⁶ ✳ 9³⁰–⁴⁶ , – 0⁰⁰–8¹⁰ , 20⁰⁵–24
23	6	0.4	.	–	✳° 12¹²–15¹⁰ , = 0⁰⁰–24 ; ⌴° 5¹⁰–α
24	7	0.3	.	–	= 0⁰⁰–12²⁰
25	6	0.1	2	–	✳° 1³⁰–6²⁵ ✳¹–7⁵⁰ ✳°–9⁴⁵ , 10⁴⁰–11²⁵ , 18²⁰–20²² ; = 9⁴⁵–24
26	6	.	pł.	–	= 0⁰⁰–20¹⁰
27	7	.	.	–	= 6³⁰–12¹⁰
28	7	.	.	–	
29					
30					
31					
Σ	–	60.4	–	–	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Marzec – Mars 1957

Dni	CIŚNIENIE p = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I.	II	III	I	II	III
1	117.4	117.2	116.2	116.9	−2.5	−0.5	−1.3	−1.4	0.0	−4.1	84	66	78	76	0.8	2.0	1.2	1.3	10	9	9	NNW 3	N 6	NW 5
2	114.4	112.9	110.9	112.7	−3.6	0.3	−2.8	−2.2	1.1	−4.2	85	67	88	80	0.7	2.0	0.6	1.1	6	6	3	NNW 1	NNW 4	NNW 3
3	108.5	106.8	103.9	106.4	−7.0	−2.7	−5.8	−5.3	−1.0	−7.5	88	60	79	76	0.4	2.0	0.8	1.1	10	2	0	NE 2	SE 1	C 0
4	98.9	94.3	89.8	94.3	−4.5	0.6	−0.2	−1.1	1.2	−7.1	88	63	92	81	0.5	2.4	0.5	1.1	8	8	10 ✳	S 2	S 5	S 4
5	92.5	94.3	96.3	94.4	−1.3	1.4	−2.6	−1.3	2.2	−2.7	90	74	75	80	0.5	1.8	1.3	1.2	9	4	0	SW 3	W 6	NW 2
6	96.1	96.1	96.9	96.4	−4.0	2.4	−0.9	−0.8	3.8	−4.3	91	66	87	81	0.4	2.5	0.7	1.2	3	4	10	W 5	NW 4	N 1
7	98.6	100.3	101.4	100.1	−3.8	−1.9	−4.0	−3.4	−0.5	−4.1	78	63	82	74	1.0	2.0	0.8	1.3	8	3	0	ENE 1	ENE 3	E 1
8	102.8	104.8	107.4	105.0	−3.6	−3.0	−5.4	−4.4	−2.5	−5.4	83	60	82	75	0.8	2.0	0.7	1.2	10	10	0	ENE 3	ESE 3	E 1
9	111.3	112.8	114.3	112.8	−9.1	1.8	−3.0	−3.3	2.4	−9.3	92	52	81	75	0.3	3.4	0.9	1.5	0	0	0	C 0	ENE 3	NE 1
10	116.9	117.6	117.5	117.3	−8.5	3.3	−3.1	−2.8	5.3	−9.2	95	53	77	75	0.2	3.6	1.1	1.6	0	0	0	C 0	ENE 2	C 0
11	117.3	116.4	112.9	115.5	−7.2	7.1	0.4	0.2	9.1	−7.9	96	40	76	71	0.1	6.0	1.5	2.5	0	1	4	S 1	S 2	C 0
12	107.8	104.1	101.5	104.5	1.7	10.1	2.7	4.3	10.4	−1.8	70	37	75	61	2.0	7.9	1.8	3.9	10	8 ⊙	8	SSW 2	SW 4	W 1
13	99.9	99.4	96.6	98.6	0.4	12.9	6.4	6.5	14.0	−0.8	88	27	65	60	0.8	10.9	3.4	5.0	4	2	0	C 0	SW 3	C 0
14	90.2	86.3	84.2	86.9	4.5	10.9	9.2	8.4	11.7	4.0	71	66	62	66	2.4	4.4	4.4	3.7	0	10	10 •	SW 4	SW 6	W 10
15	87.5	89.5	80.5	85.8	3.4	3.2	0.2	1.8	9.3	0.1	97	86	100	94	0.3	1.1	0.0	0.5	10 •	10 ✳	10 ✳	W 9	W 3	NW 3
16	83.0	89.6	96.7	89.8	−2.4	−6.6	−6.5	−5.5	0.4	−7.9	89	86	81	85	0.5	0.5	0.7	0.6	9	9 ✳	8	NW 8	NW 14	NW 3
17	100.4	98.3	88.3	95.7	−11.8	−5.6	−5.5	−7.1	−4.7	−13.4	82	74	87	81	0.4	1.0	0.5	0.6	8	4	10	C 0	E 1	E 6
18	74.5	73.5	78.1	75.4	0.4	6.1	2.1	2.7	7.0	−5.5	98	92	82	91	0.1	0.7	1.3	0.7	10 •	10	10 •	S 2	SW 3	W 5
19	88.2	91.5	93.3	91.0	−1.2	0.7	−0.3	−0.3	2.3	−1.9	76	67	76	73	1.3	2.1	1.5	1.6	10	7	10	NW 5	NNW 2	NE 2
20	96.4	94.8	88.2	93.1	−1.2	1.9	1.3	0.8	2.1	−1.4	74	71	96	80	1.4	2.0	0.2	1.2	10	10 ✳	10 •	E 2	ESE 5	SE 4
21	86.4	90.8	93.4	90.2	7.1	9.7	5.2	6.8	10.9	1.1	93	57	78	76	0.8	5.2	1.9	2.6	9	8	0	W 7	W 9	S 1
22	94.2	96.4	98.8	96.5	3.2	7.4	3.6	4.4	9.1	2.9	91	58	63	71	0.7	4.3	2.9	2.6	0	8	0	SW 5	W 6	W 3
23	101.7	102.8	109.8	104.8	0.1	8.1	−1.8	+1.2	9.0	−2.0	96	53	83	77	0.3	5.1	0.9	2.1	0	4 ⊙	10	W 1	NW 1	NE 9
24	114.5	115.7	115.1	115.1	−4.4	1.8	−0.6	−1.0	2.7	−5.1	67	36	60	54	1.4	4.5	2.3	2.7	3 ⊙	3 ⊙	0	ENE 10	E 10	E 10
25	113.2	112.3	111.3	112.3	−2.6	3.4	1.5	1.0	4.4	−2.9	63	49	51	54	1.9	4.0	3.4	3.1	10	10	3	E 10	SE 8	SE 10
26	109.1	108.2	107.4	108.2	0.8	8.3	5.1	4.8	9.3	−0.1	53	43	52	49	3.1	6.3	4.2	4.5	10	10	0	SE 8	SE 6	SE 6
27	106.8	106.0	105.0	105.9	1.0	13.4	8.4	7.8	14.4	0.0	73	30	66	56	1.8	10.8	3.7	5.4	0	4 ⊙	2	SSE 3	S 9	SSE 3
28	101.9	100.2	99.0	100.4	3.6	12.1	7.4	7.6	12.8	2.8	72	36	79	62	2.2	9.0	2.2	4.5	7	8 ⊙	10 •	S 6	SSE 8	C 0
29	97.3	98.5	101.3	99.0	5.2	5.6	6.0	5.7	7.6	5.1	97	91	88	92	0.2	0.9	1.2	0.8	10	10 •	3	SSE 1	SSE 2	E 1
30	103.0	104.7	105.4	104.4	0.2	10.3	7.6	6.4	13.4	−0.4	98	75	80	84	0.1	3.1	2.0	1.7	4	2	2	C 0	NE 1	NE 1
31	106.5	107.3	108.2	107.3	3.2	16.1	7.7	8.7	17.0	0.9	81	24	63	56	1.5	13.9	3.9	6.4	0	0 ⊙	0	C 0	E 3	E 1
M	101.2	101.4	101.0	101.2	−1.4	4.5	1.0	1.3	5.9	−3.0	84	59	77	73	0.9	4.1	1.7	2.2	6.1	5.9	4.6	3.4	4.6	3.1

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1	109.3	108.7	107.5	108.5	3.2	15.4	8.2	8.8	16.6	−0.5	78	29	66	58	1.7	12.3	3.7	5.9	0 ⊙	0	0	E 1	E 3	C 0
2	106.9	105.9	106.7	106.5	4.8	15.7	7.4	8.8	16.6	1.8	86	34	72	64	1.2	11.8	2.9	5.3	0	4	0	E 1	E 3	C 0
3	108.9	110.2	111.5	110.2	2.5	16.6	8.9	9.2	18.6	0.1	96	30	61	62	0.3	13.1	4.5	6.0	0	0 ⊙	0	C 0	ENE 1	NE 1
4	113.3	113.3	112.5	113.0	2.1	15.7	5.0	7.0	17.2	−1.1	96	31	70	66	0.3	12.3	2.6	5.1	2 ⊙	1 ⊙	0	C 0	NNW 3	C 0
5	111.3	108.7	103.1	107.7	1.6	17.6	8.9	9.2	18.9	−1.5	94	25	52	57	0.4	15.0	5.5	7.0	3	2	0	C 0	S 2	SW 1
6	97.3	93.5	92.1	94.3	8.3	17.9	6.2	9.6	19.1	5.0	52	22	91	55	5.3	15.9	0.9	7.4	0	3 ⊙	4	SW 2	SSW 5	NW 3
7	92.5	94.9	100.7	96.0	4.2	8.1	−0.6	2.8	9.6	−0.8	92	48	75	72	0.6	5.7	1.4	2.6	9	8	1	NNW 3	N 6	N 6
8	102.5	100.1	96.9	99.8	−0.4	4.4	3.2	2.6	6.9	−2.5	88	42	79	70	0.7	4.9	1.6	2.4	6	6	10 🌫	N 3	NW 6	NW 5
9	95.4	95.9	95.3	95.5	1.3	2.2	−3.9	−1.1	3.5	−4.2	79	40	64	61	1.4	4.3	1.7	2.5	10	6 ⊙	1	NW 3	NNW 6	NW 2
10	91.8	86.5	79.4	85.9	−2.4	6.8	9.0	5.6	9.7	−5.8	68	45	51	55	1.6	5.5	5.7	4.3	8	10	10	S 3	SSW 6	S 6
11	75.8	76.0	82.8	78.2	5.2	7.7	0.6	3.5	9.4	0.6	75	35	79	63	2.2	6.8	1.4	3.5	8	3 ⊙	10	SW 1	W 6	NW 7
12	89.8	92.4	94.7	92.3	−0.9	3.1	−0.8	0.2	3.8	−1.4	96	48	67	70	0.2	4.0	2.0	2.1	10 ✳	9	2	W 4	NW 5	C 0
13	96.3	96.6	98.8	97.2	−2.1	2.5	−2.3	−1.0	5.0	−4.4	92	75	83	83	0.4	1.8	0.9	1.0	3	9	1	SW 1	WNW 4	NW 1
14	100.6	100.6	101.6	100.9	−2.5	3.5	0.4	0.4	5.8	−6.9	87	44	94	75	0.7	4.4	0.4	1.8	5 ✳	9	9 ✳	SW 1	SW 3	NNW 1
15	103.3	103.6	104.1	103.7	−1.4	3.2	−1.1	−0.1	4.6	−4.1	88	48	97	78	0.6	4.0	0.2	1.6	6	7	10 ✳	N 2	NNW 3	N 3
16	105.6	103.2	99.7	102.8	−2.7	5.0	5.6	3.4	5.9	−5.0	93	40	97	77	0.3	5.2	0.3	1.9	4 ⊙	10	10 •	SW 1	SW 6	SW 2
17	100.5	101.7	104.0	102.1	6.1	6.8	3.1	4.8	8.4	2.9	89	87	86	87	1.0	1.3	1.0	1.1	9	9 •	10	W 1	W 2	NW 3
18	102.9	102.0	100.0	101.6	2.6	4.2	1.9	2.6	4.7	1.3	100	74	93	89	0.0	2.1	0.5	0.9	10 ≡	10 •	10	N 2	NE 2	N 2
19	97.7	96.6	98.3	97.5	1.3	3.6	2.9	2.7	4.0	0.6	94	76	88	86	0.4	1.9	0.9	1.1	10 ✳	10	10	NW 2	NW 2	C 0
20	101.3	103.7	106.9	104.0	2.6	8.2	3.8	5.6	9.6	1.0	95	67	95	86	0.4	3.6	0.4	1.5	10 •	10	10 •	SE 1	SSE 3	NW 2
21	108.1	109.8	111.5	109.8	4.9	7.5	5.0	5.6	9.6	4.2	97	86	94	92	0.3	1.5	0.5	0.8	10	10	3	NW 1	SW 1	S 1
22	114.3	114.3	112.9	113.8	4.4	12.2	10.5	9.4	13.8	2.6	90	60	85	78	0.9	5.7	1.9	2.8	9	5 ⊙	10	SSW 1	E 2	NW 1
23	112.7	112.5	113.4	112.9	7.9	15.6	5.3	8.5	16.0	5.2	83	51	98	77	1.7	8.7	0.1	3.5	9	5 ⊙	3	ENE 2	NE 3	NE 2
24	112.2	110.9	110.0	111.0	4.1	14.8	8.6	9.0	17.0	2.8	100	62	64	75	0.0	6.4	4.1	3.5	10 ≡	8	6	NW 3	N 3	NNW 3
25	107.9	107.3	106.6	107.3	4.8	12.1	7.8	8.1	15.9	3.8	97	68	86	84	0.3	4.5	1.5	2.1	10	10	2	N 4	N 6	N 2
26	105.6	104.5	103.7	104.6	5.1	16.1	10.5	10.6	19.4	2.9	100	61	84	82	0.0	7.2	2.1	3.1	10 ≡	10	5	N 3	N 3	NW 1
27	102.5	100.2	99.6	100.8	8.6	23.2	14.3	15.1	24.8	4.2	86	33	75	65	1.6	19.0	4.1	8.2	0	7 •	4	C 0	ESE 1	NNW 1
28	97.8	95.1	94.9	95.7	14.1	22.3	13.6	15.9	24.0	9.2	73	42	86	67	4.4	15.7	2.2	7.4	2	8	10 🌂	SE 1	S 2	E 2
29	93.8	93.0	94.7	93.8	13.0	23.4	13.4	15.8	24.5	9.8	84	35	81	67	2.3	18.8	3.0	8.1	4	3 ⊙	5 (🌂)	SE 1	S 3	NNW 2
30	95.0	91.7	93.1	93.3	11.5	18.8	5.7	10.4	21.7	5.5	89	74	88	84	1.3	5.7	1.2	2.8	9	8 (🌂)	10 •	C 0	SE 2	NW 6
31																								
M	101.7	101.1	101.2	101.3	3.7	11.1	5.4	6.4	12.8	0.8	88	50	80	73	1.1	7.6	2.0	3.6	6.2	6.7	5.5	1.6	3.4	2.2

Olsztyn – Dajtki

$H_s = 133$ m $H_b = 138{,}7$ m $h_w = 12$ m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	
2	7	.	.	–	
3	6	.	.	–	= 7⁵⁰–24
4	7	1.9	.	–	*⁰ 6²⁰–⁴⁵ *¹–21¹⁰ *⁰–23⁰¹ . = 0⁰⁰–6²⁰ . 23⁰¹–24
5	7	.	4	–	= 0⁰⁰–7²⁰
6	7	.	pż.	–	
7	7	.	.	–	
8	7	0.0	.	–	*⁰ 7²⁰–9⁵⁰ 10¹⁵–12¹⁰
9	7	.	.	–	= 5³⁰–7⁴⁰ ; ⌴⁰ 5¹⁰–6⁰⁰
10	6	.	.	–	= 3¹⁰–24
11	7	.	.	–	= 0⁰⁰–12³⁰ ; ⌴² n–7²⁰
12	6	.	.	–	∞ 7²⁰–13⁴⁰ = 18¹⁰–24 ; ⌴⁰ n–6⁰⁵
13	6	.	.	–	= 0⁰⁰–14¹⁰
14	6	0.5	.	–	•⁰ 20²⁰–21³⁵ 22¹⁰–24 ; ⩺ 18⁴⁰–24 . = 6¹⁰–20¹⁰
15	7	7.9	.	–	•⁰ 0⁰⁰–11⁴⁰ 13⁰⁶–17³⁰ *¹–24 . ⩺ 0⁰⁰–5²⁰
16	5	1.6	4	–	*¹ 0⁰⁰–12 ⛆ 6⁵⁸–7²⁵ . 7⁵⁰ 15¹⁵–17⁴⁰ ; ⛆ 7²⁵–8¹⁰ ⛆ 15¹⁵ ⛆ 17⁴⁰
17	7	2.7	4	–	*⁰ 17⁰⁷–24
18	6	2.0	6	–	*⁰ 0⁰⁰–2³⁰ •⁰ 3³⁰–6¹⁰ •⁰–10⁵⁰ . 16¹⁵–17¹⁰ . 18²⁰–21⁴⁰ . = 8²⁰–21²⁰
19	8	.	.	–	
20	7	3.9	.	–	*⁰ 11⁵⁸–14¹⁰ •⁰ 14²⁵–22²⁰ . = 22²⁰–24
21	7	.	.	–	= 0⁰⁰–6¹⁰
22	8	.	.	–	
23	8	.	.	–	⌴¹ n–7⁴⁰
24	8	.	.	–	⩺ 6⁴⁰–24
25	8	.	.	–	⩺ 0⁰⁰–12²⁰ . 14⁴⁰–15⁵⁰ . 18³⁰–24
26	7	.	.	–	⩺ 0⁰⁰–4³⁰
27	8	.	.	–	
28	7	1.5	.	–	•⁰ 19³⁰–24 . ⊕ 9³⁵–12¹⁰
29	6	1.1	.	–	•⁰ 0⁰⁰–5⁵⁰ . 12²⁰–15¹⁰ . = 4⁴⁰–21¹⁰
30	6	.	.	–	≍ 3³⁰–5⁰⁵ ≡⁰–6⁰⁰ = –7²⁰ ≡¹–10⁵⁵ = –16³⁰ . 18⁴⁵–24
31	7	.	.	–	= 0⁰⁰–6¹⁰
Σ	–	20.1	–	–	UWAGI

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1	8	.	.	–	⌴⁰ 4¹⁰–6⁴⁰
2	7	.	.	–	= 6³⁰–8³⁰
3	7	.	.	–	= 6²⁰–9⁰⁵
4	8	.	.	–	= 3¹⁰–10²⁰
5	8	.	.	–	= 6¹⁰–9¹⁰ ; ⌴¹ n–a
6	8	0.5	.	–	•⁰ 23¹⁵–24
7	8	.	.	–	•⁰ 0⁰⁰–2¹⁰ . = 2¹⁰–7⁵⁰
8	8	0.0	.	–	*⁰ 14³⁰–16¹⁰ *⁰–22²⁵
9	8	0.0	.	–	⛆ 7¹²–25 . 9⁰²–¹⁰
10	8	.	.	–	
11	8	0.2	.	–	
12	8	0.0	.	–	⛆ 5³⁰–7⁵⁰
13	8	0.0	.	–	⛆ 13⁴²–14²⁸ . = 4¹⁵–5³⁰ . ⌴⁰ 5³⁰–6³⁰
14	8	0.0	.	–	⛆ 6²⁰–7²⁵ . 9⁵⁰–10⁴⁰ 15⁵⁵–16³⁵ 18²⁵–21¹⁵ ; ⌴² n–8¹⁰
15	8	2.1	.	–	⛆ 5⁵⁰–6²⁰ . 17⁵⁵–23³⁵ ; ⌴² n–8¹⁰
16	7	1.9	4	–	•⁰ 15⁴⁵–24
17	6	1.0	.	–	•⁰ 0⁰⁰–3⁴⁵ ⛆ 10¹⁰–²⁵ 11⁴⁰–12⁵⁰ . 13¹⁰–⁴⁰ . 16⁰⁵–²⁵ . = 3⁴⁰–7³⁰ . 19⁴⁰–24
18	7	2.1	.	–	•⁰ 8⁰⁵–11¹⁰ 12³⁵–18⁴⁵ . = 0⁰⁰–5⁴⁰ ≡⁰–8¹² = –11³⁰ . 19³⁰–24
19	7	0.5	.	–	•⁰ 3²⁵–4²⁰ *⁰ 5³⁵–10²⁰ •⁰ 14³⁰–16²⁵ = 4¹⁰–10²⁰
20	7	1.4	.	–	•⁰ 5²⁰–8³⁵ 9⁴⁰ 11²⁵ 15³⁰ 18³⁷ 20²⁵–24 . = 5¹⁰–11³⁰ . 18²⁰–24
21	6	.	.	–	•⁰ 0⁰⁰ 5²⁵ . = 0⁰⁰–15¹⁰ . 22⁰⁵–24
22	7	0.0	.	–	⛆ 17³⁰–⁴⁵ . = 0⁰⁰–3⁴⁰ ≡¹–5⁵⁰ = –10³⁰ . 21⁴⁰–24
23	7	.	.	–	= 0⁰⁰–6¹⁰ 20²⁰–21⁵⁰ ≡⁰–24
24	7	.	.	–	≡⁰ 0⁰⁰–7³⁰ = –9²⁰
25	7	.	.	–	= 3¹⁵–6³⁸ ≡⁰–8⁴⁰ = –12¹⁰
26	7	.	.	–	= 2²⁰–3³⁵ ≡⁰–7⁵⁰ = –12³⁰ ∞ 16³⁰–20³⁰ = –24
27	7	1.4	.	–	⛆ 12³⁸–³⁹ 12⁴⁹–⁵² 12⁵⁹–13⁰⁰ 13²⁰–²² ⛆ R 13⁵⁰–15⁴⁰ ⛆ 18¹⁰–¹³ 18⁵⁰–⁵³ 19⁰⁴–⁰⁷ 19⁴⁰–20⁰⁶ . = 0⁰⁰ 10¹⁰ ∞–12²⁰ ⌓! n–8²⁰
28	7	2.9	.	–	⛆ 14⁰⁵–²⁰ R⁰ 18⁴⁰–21⁵⁰ < 22⁴⁰–24
29	7	.	.	–	(R) 13⁵⁵–14²⁰ 20³⁵–21⁴⁰ < –22³⁰
30	7	11.2	.	–	⛆ 7⁴⁵–8¹⁵ ⛆ (R) 11²⁵–³⁶ (R) 12¹⁰–²⁵ 12⁴⁰ ⛆ 12⁵⁰ •R 14²⁰–19²⁰ ⛆ 20²⁵–22¹⁰ . = 3²⁸–8¹⁵
31					
Σ	–	25.2	–	–	UWAGI.

Olsztyn – Dajtki

$\varphi = 53°46'$ $\lambda = 20°25'$

Maj – Mai 1957

DNI	CIŚNIENIE p − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	98.7	101.8	103.0	101.2	4.4	8.9	3.7	5.2	9.7	2.5	76	49	70	65	2.1	5.8	2.4	3.4	8	4	0	WNW 6	WNW 7	C 0
2	103.3	101.3	98.6	101.1	4.1	10.4	6.8	7.0	12.3	−1.7	74	40	54	56	2.2	7.6	4.5	4.8	2	2	2	E 1	SE 2	C 0
3	96.5	94.2	91.0	93.9	7.0	13.7	11.1	10.7	15.2	−1.3	63	34	53	50	3.7	10.4	6.2	6.8	3	5 ⊙	10	SE 1	NNW 2	SSW 1
4	87.5	89.6	90.8	89.3	6.7	6.9	4.7	5.8	11.3	4.6	97	51	54	67	0.3	4.9	3.9	3.0	10	10	1	SW 3	W 6	WSW 5
5	90.4	91.0	92.6	91.3	3.0	7.9	2.2	3.8	9.3	1.0	69	46	86	67	2.4	5.7	1.1	3.1	4	5 ⊙	1	SW 7	SW 6	SW 2
6	94.0	93.2	92.3	93.2	3.1	8.6	3.6	4.7	9.3	−1.5	81	41	97	73	1.4	6.5	0.3	2.7	0	10	10 •	SE 1	E 3	NE 2
7	90.3	91.4	91.4	91.0	4.7	7.8	4.1	5.2	8.5	3.3	90	64	97	84	0.8	3.8	0.3	1.6	10	10	10 •	NNE 1	NW 1	NW 1
8	88.9	88.9	91.2	89.7	3.6	4.2	3.2	3.6	4.6	3.2	93	92	98	94	0.5	0.6	0.2	0.4	10 •	10 •	10 •	NW 3	NW 4	NNW 3
9	94.5	95.4	94.1	94.7	3.8	5.3	5.6	5.1	6.6	2.7	97	92	91	93	0.3	0.7	0.9	0.6	10 •	10 •	10	NW 3	NNW 4	N 5
10	92.5	91.2	94.5	92.7	6.8	15.2	7.4	9.2	16.4	4.9	100	82	97	93	0.0	3.2	0.3	1.2	10 ≡	8	10 •	NW 1	NW 3	NNW 2
11	94.3	98.0	100.2	97.5	6.7	8.0	7.9	7.6	8.8	5.9	99	90	93	94	0.1	1.0	0.7	0.6	10 •	10 •	8	NW 1	SW 3	C 0
12	100.7	100.9	101.0	100.9	5.8	16.3	10.9	11.0	19.2	4.5	100	41	78	73	0.0	10.9	2.9	4.6	10 ≡	8	9	SE 1	SSE 2	C 0
13	101.2	101.0	100.4	100.9	12.4	21.8	14.1	15.6	22.6	8.2	79	43	79	67	3.0	14.8	3.4	7.1	0	3 ⊙	1	E 1	S 3	C 0
14	100.1	101.5	103.2	101.6	13.3	18.0	11.7	13.7	18.9	7.4	78	66	91	78	3.3	6.9	1.1	3.8	9 • ₹	9	9	NW 1	NW 1	W 3
15	105.0	105.4	105.9	105.8	10.9	16.6	11.0	12.4	17.6	6.9	89	38	67	65	1.4	11.7	4.3	5.8	0	1 ⊙	0	W 3	W 4	C 0
16	106.0	103.6	101.0	103.5	11.6	19.5	15.4	15.5	21.0	5.0	69	46	48	53	4.2	12.2	9.2	8.5	0 ⊙	0	0	E 1	E 3	C 0
17	101.4	100.5	101.1	101.0	12.6	21.7	11.7	14.4	23.0	4.7	82	37	85	68	2.6	16.3	2.0	7.0	4	6 ⊙	8	SE 1	E 1	NW 3
18	102.3	102.3	100.3	101.6	10.4	18.1	12.3	13.3	20.1	5.5	81	54	83	73	2.4	9.5	2.4	4.8	0	0 ⊙	0	NW 3	NNW 3	NNW 3
19	97.3	95.3	92.7	95.1	14.4	22.9	18.7	18.7	25.0	9.7	73	58	59	63	4.4	11.8	8.8	8.3	8	8	5	NNE 1	NE 3	NE 2
20	93.3	93.1	94.4	93.6	16.7	23.6	12.5	16.3	24.1	12.1	80	50	90	73	3.9	14.6	1.4	6.6	3	4 ⊙	9 (₹)	SSE 1	E 3	NW 6
21	98.0	99.5	100.1	99.2	9.6	9.6	7.6	8.6	12.8	7.4	88	83	82	84	1.5	2.1	1.9	1.8	10	10	9	WNW 3	NW 4	NNW 4
22	99.0	99.3	99.1	99.1	8.6	13.1	11.4	11.1	15.1	7.4	88	67	71	75	1.4	5.0	3.9	3.4	10	10	7	NNW 3	NW 3	NW 3
23	97.5	96.5	95.7	96.6	9.1	14.1	14.6	13.1	15.9	5.7	100	92	92	95	0.0	1.3	1.3	0.9	10 ≡	10	10	NNW 2	NW 2	NNE 2
24	97.9	101.1	105.6	101.5	11.4	14.7	9.4	11.2	15.7	9.2	79	47	59	62	2.8	8.8	4.9	5.5	10	6	0	NNE 5	NNW 7	NNW 4
25	108.7	109.7	111.0	109.8	6.4	9.2	5.9	6.8	10.3	2.4	62	36	71	56	3.6	7.5	2.7	4.6	0	9	9	NNE 3	NNE 6	NNE 4
26	111.5	111.5	111.2	111.4	5.6	7.4	6.1	6.3	9.3	4.1	75	75	80	77	2.2	2.6	1.8	2.2	9	10	9	NNE 3	NNE 3	NNE 3
27	110.5	109.7	108.9	109.7	6.2	10.3	5.4	6.8	10.7	3.7	73	47	84	68	2.6	6.6	1.4	3.5	6	9	8	NNE 2	N 3	NW 2
28	107.2	105.8	105.0	106.0	4.9	11.2	6.9	7.5	13.2	−0.5	94	50	78	74	0.6	6.6	2.2	3.1	9	8 ⊙	4	N 1	N 2	NNE 2
29	104.4	104.1	103.3	103.9	5.1	8.8	7.3	7.1	9.7	0.4	83	68	93	81	1.5	3.6	0.7	1.9	9	10 •	10	N 2	W 2	W 2
30	104.0	104.8	104.3	104.4	8.2	11.1	7.8	8.7	13.4	6.0	83	66	73	74	1.8	4.5	2.8	3.0	8	5 ⊙	0	W 2	NW 6	NW 1
31	103.9	102.1	98.6	101.5	11.3	18.9	13.8	14.4	20.7	3.7	66	32	58	52	4.5	14.8	6.7	8.7	0	5 ⊙	1	S 1	SSW 3	SW 1
M	99.4	99.5	99.4	99.4	8.0	13.0	8.9	9.7	14.5	4.4	83	57	78	73	2.0	7.2	2.8	4.0	6.2	6.9	5.5	2.2	3.4	2.1

Czerwiec – Juin

1	97.7	96.9	97.8	97.5	13.7	19.7	11.7	14.2	20.9	9.2	62	45	76	61	6.0	12.5	3.3	7.3	6	10	10	SW 1	SW 4	NW 1
2	98.4	100.7	102.8	100.6	12.0	15.1	11.8	12.7	16.5	9.6	79	71	95	82	3.0	5.0	0.6	2.9	5	10	10	W 3	NW 3	C 0
3	103.6	103.2	100.1	102.3	14.2	19.7	16.7	16.8	21.7	8.2	76	56	78	70	3.9	10.0	4.2	6.0	1	8 ⊙	3	SW 3	SW 2	C 0
4	96.8	94.9	93.6	95.1	14.3	24.8	15.0	17.3	25.6	10.4	86	40	77	68	2.4	18.7	3.8	8.3	10	10	10	E 1	SW 3	N 1
5	88.9	88.2	87.3	88.1	12.2	13.5	12.4	12.6	16.5	9.5	96	91	94	94	0.5	1.5	0.9	1.0	10 •	10 •	7	N 1	W 2	SW 1
6	87.6	90.1	93.0	90.2	12.0	12.0	10.9	11.4	15.2	8.4	87	90	74	84	1.8	1.3	3.4	2.2	5	9	3	S 3	SW 3	SW 2
7	93.8	92.3	94.7	93.6	12.1	19.3	12.3	14.0	20.6	8.9	76	46	81	68	3.3	12.1	2.7	6.0	9	8	8	S 3	S 5	N 1
8	97.1	98.2	98.0	97.8	13.4	21.1	16.1	16.7	22.5	7.3	73	44	72	63	4.2	13.9	5.1	7.7	2	4	3	SSE 1	SE 2	E 1
9	96.9	94.8	94.3	95.3	18.0	26.1	17.0	19.5	26.9	12.7	76	48	79	68	4.8	17.9	4.1	8.8	2	8 ⊙	10 •	E 3	SE 6	SSE 2
10	96.6	96.1	97.5	96.7	14.9	16.8	15.3	15.6	21.4	12.3	100	96	93	96	0.0	0.8	1.2	0.7	10 ≡	10 ₹	4	W 1	SW 6	C 0
11	97.1	95.0	94.0	95.4	15.5	26.8	23.5	22.3	28.9	11.9	98	53	69	73	0.4	16.6	9.0	8.7	4	3	8	E 2	SE 3	E 2
12	98.8	106.3	111.0	105.4	21.7	18.3	13.0	16.5	24.1	12.8	83	80	83	82	4.4	4.2	2.6	3.7	10	10	4	W 4	NW 5	NNW 2
13	112.4	112.7	112.3	112.5	10.9	14.3	10.2	11.4	15.6	8.3	68	68	92	76	4.1	5.3	0.9	3.4	3 ⊙	10	0	WNW 6	NW 5	NW 1
14	112.3	112.3	112.9	112.5	11.5	19.1	12.1	13.7	19.9	7.6	97	38	59	65	0.4	13.7	5.7	6.6	4	0	2	NE 4	NNW 5	NNW 4
15	113.3	112.5	110.2	112.0	12.1	19.0	12.2	13.9	20.4	5.0	77	40	65	61	3.2	13.2	5.0	7.1	6	2	1	NW 1	NNW 2	NNW 1
16	108.9	107.7	105.4	107.3	14.5	22.2	17.5	17.9	23.5	5.6	64	41	64	56	6.0	15.8	7.2	9.7	1 ⊙	1 ⊙	0	NNW 1	N 3	C 0
17	105.3	104.7	102.6	104.2	13.3	20.3	14.6	15.7	21.7	8.4	71	33	60	55	4.5	16.0	6.7	9.1	2	0	0	NE 1	NE 2	C 0
18	101.8	99.8	96.7	99.4	17.1	25.5	20.6	21.0	27.2	9.7	56	32	50	46	8.5	22.2	12.0	14.2	1	2 ⊙	0	C 0	SSW 2	C 0
19	94.7	94.8	95.6	95.0	18.3	24.2	15.7	18.5	25.1	9.4	62	34	68	61	7.9	13.9	5.7	9.2	2 ⊙	2 ⊙	3	C 0	NNE 4	NNE 4
20	98.5	99.4	101.2	99.7	10.9	18.2	11.7	13.1	19.6	8.5	73	31	58	54	3.5	14.5	5.8	7.9	4	6 ⊙	3	NE 2	NNE 3	NNW 3
21	103.8	101.2	96.4	100.5	11.1	18.7	16.3	15.6	21.2	4.1	65	38	70	58	4.6	13.4	5.6	7.9	1 ⊙	3 ⊙	2	C 0	E 1	SE 2
22	92.2	88.7	85.9	88.9	15.7	23.0	16.3	17.8	24.0	11.7	59	60	100	73	7.2	11.2	0.0	6.1	3	10	10	SE 4	SE 3	W 1
23	89.6	93.2	93.2	92.0	14.3	15.5	16.1	15.5	18.7	13.8	94	84	84	87	0.9	2.8	2.9	2.2	10	10	9	WSW 1	W 4	W 1
24	95.1	94.8	91.9	93.9	12.6	13.0	10.9	12.4	16.8	9.5	88	66	92	82	1.7	5.7	1.0	2.8	9	10 •	5	NW 3	NNW 3	NNE 3
25	88.4	92.2	97.4	92.7	9.1	10.7	11.3	10.6	12.5	8.9	96	86	85	89	0.5	1.8	2.0	1.4	10 •	10	10	N 3	NE 1	SW 1
26	100.6	101.7	103.8	102.0	11.7	15.9	10.2	12.0	18.0	9.3	77	47	86	70	3.1	9.5	1.7	4.8	4	8	5	SW 4	SW 4	SSW 1
27	104.5	105.6	107.2	105.8	10.5	14.7	12.6	12.6	16.5	6.9	86	65	72	74	1.8	5.8	4.1	3.9	4 ⊙	8 ⊙	6	SW 1	NNW 4	C 0
28	105.2	102.4	102.4	103.3	12.4	16.2	16.7	15.5	21.6	8.2	70	82	90	81	4.4	3.2	2.0	3.2	10	10	6	S 4	SW 6	NW 4
29	103.6	104.9	103.3	103.9	16.9	22.1	18.7	19.1	24.7	15.7	95	58	86	80	1.0	11.3	3.0	5.1	10	6	2	W 2	W 3	C 0
30	101.6	103.2	104.2	103.0	20.5	23.1	16.7	19.2	24.6	15.8	78	56	83	72	5.3	12.5	3.3	7.0	2	6 ⊙	2	W 3	W 9	NW 2
31																								
M	99.5	99.6	99.6	99.6	13.9	19.0	14.3	15.5	21.1	9.6	79	58	78	72	3.4	10.2	3.8	5.8	5.3	6.8	4.9	2.2	3.6	1.4

Olsztyn – Dajtki

H_s = 133 m H_b = 138,7 m h_w = 12 m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	.	.	–	$\sqcup^2$ n – 6^{10}
3	8	0.0	.	–	$\frown^2$ n – 9^{00}
4	7	0.0	.	–	▽ 6^{03} – 06 • ^{0} 6^{45} – 7^{09} ✳ 21^{50} – 22^{15}
5	8	0.2	.	–	✳ 14^{32} – 15^{10} ✳ 15^{20} – 35 ▽ 16^{25} – 45
6	8	3.7	.	–	• ^{0} 15^{54} – 24 ; ≡ 3^{45} – 5^{20} ; $\sqcup^2$ n – a
7	7	14,3	.	–	• ^{0} 0^{00} – 2^{45} 4^{42} – 55 ▽ 7^{25} – 9^{20} 13^{55} – 20^{10} • ^{1} – 22^{30} • ^{0} – 24 ; = 2^{45} – 7^{25}
8	6	3.4	.	–	• ^{0} 0^{00} – 11^{30} • ^{1} – 12^{20} • ^{0} – 16^{45} • ^{0} 20^{10} – 24
9	6	0.5	.	–	• ^{0} 0^{00} – 8^{10} • ^{0} 9^{45} – 13^{10} ... 50 – 15^{40} 19^{50} – 20^{10}
10	6	10.9	.	–	▽ 15^{15} – 16^{30} • ^{1} 17^{35} – 21^{20} ; ↯ ^{0} 15^{15} – 35 ; = 0^{05} – 3^{10} ≡ ^{1} – 7^{00} ≡ ^{0} – 9^{05} = – 22^{45}
11	7	1.4	.	–	• ^{1} 4^{05} – 10^{40} • ^{0} 11^{05} 15^{30} ; ≡ ^{1} 0^{00} – 4^{10} ≡ ^{0} – 5^{40} = – 10^{40} , 19^{25} – 24
12	8	.	.	–	= 0^{00} – 1^{10} ≡ ^{0} – 3^{50} ≡ ^{1} – 7^{50} = – 8^{20} , 23^{25} – 24
13	7	0.0	.	–	= 0^{00} – 9^{40} 20^{20} – 24
14	7	5.1	.	–	▽ 6^{23} – 75 12^{05} – 20 , 13^{10} – 25 , 15^{55} – 16^{35} ; (↯) 5^{25} – 6^{20} ↯ ^{0} 6^{20} – 6^{30} – 7^{40} SW-NE (↯) 12^{55} – 13^{05} ; = 0^{00} – 10^{05}
15	8	.	.	–	= 0^{40} – 9^{05}
16	8	.	.	–	
17	8	.	.	–	$\frown^1$ n – 7^{20}
18	8	.	.	–	
19	7	0.0	.	–	• ^{0} 10^{15} – 25 ; (↯) 15^{50} – 16^{10}
20	8	0.8	.	–	▽ 22^{20} – 24 ; (↯) 18^{20} – 19^{00} , 20^{20} – 23^{10}
21	7	0.0	.	–	▽ 0^{00} – 2^{35} , 20^{04} – 05 ; = 2^{50} – 7^{40}
22	7	0.0	.	–	
23	6	0.0	.	–	• ^{0} 6^{30} – 7^{30} • ^{0} 14^{02} – 09 ; = 1^{00} – 25 ≡ ^{1} 1^{25} – 7^{45} = – 15^{20}
24	7	.	.	–	• ^{0} 1^{10} – 3^{30} ; = 0^{30} – 3^{30}
25	8	.	.	–	
26	7	0.0	.	–	▽ 11^{45} – 12^{20}
27	8	0.8	.	–	▽ 13^{10} – 14^{10} 16^{25} – 18^{20}
28	8	0.0	.	–	▽ 10^{11} – 14 ▽▲ 10^{33} ▽ – 10^{45} , 16^{01} – 05 17^{05} – 18^{05} 18^{30} – 19^{10} ; ≡ ^{0} 0^{50} – 6^{35} = – 7^{45} ; $\sqcup^0$ n – 6^{00}
29	7	0.9	.	–	• ^{0} 8^{10} – 9^{35} ▽ 11^{50} – 13^{10} • ^{0} – 20^{20} ; = 20^{20} – 24 ; $\sqcup^0$ n – 5^{30}
30	8	.	.	–	• ^{0} 0^{35} – 3^{25} ; = 0^{00} – 7^{10}
31	8	.	.	–	
Σ	–	42.0	–	–	UWAGI.

Czerwiec – Juin

1	7	.	.	–	
2	7	0.0	.	–	• ^{0} 16^{45} – 18^{35} ; = 14^{25} – 24
3	8	.	.	–	= 0^{00} – 3^{20}
4	7	0.0	.	–	
5	6	11.5	.	–	• ^{0} 6^{20} – 9^{20} • ^{1} – 12^{40} • ^{0} 13^{30} – 16^{35} ; = 4^{20} – 24
6	7	2.6	.	–	▽ 10^{30} – 33 12^{32} – 13^{16} , 13^{40} – 50 , 14^{25} – 27 16^{30} – 17^{02} , 17^{50} – 18^{08} , 18^{20} – 32 ; = 0^{00} – 9^{20}
7	7	0.0	.	–	▽ 16^{15} – 50 ; = 22^{20} – 24
8	7	.	.	–	= 0^{00} – 10^{30}
9	7	1.2	.	–	▽ 18^{56} – 19^{20} 19^{35} – 20^{20} III n ; (↯) 18^{55}
10	6	34.6	.	–	▽ 11^{30} – 45 , 13^{07} – 15^{15} ; ↯ 13^{13} – 13^{50} – 15^{10} SW-SE ; ≡ ^{0} 7^{05} – 9^{45} = – 11^{40} ≡ 21^{10} – 24
11	7	.	.	–	≡ 0^{00} – 05 ≡ 0^{35} – 7^{30} = – 10^{20}
12	7	.	.	–	
13	7	.	.	–	
14	8	.	.	–	= 4^{30} – 5^{20} ≡ – 6^{35} = – 8^{10}
15	8	.	.	–	
16	8	.	.	–	
17	8	.	.	–	
18	8	.	.	–	
19	8	.	.	–	
20	8	.	.	–	
21	8	.	.	–	
22	8	13.5	.	–	(↯) 13^{42} ▽↯ 14^{47} – 17^{10} ▽(↯) 17^{45} – 19^{35} • ^{0} 20^{40} ... 21^{20} ; = 17^{10} – 24
23	6	2.4	.	–	= 0^{00} – 21^{20}
24	7	7.9	.	–	• ^{1} 2^{10} – 3^{10} • ^{0} 12^{50} – 17^{32} ; = 3^{10} – 11^{10}
25	7	0.6	.	–	• ^{0} 6^{40} – 10^{40} • ^{0} – 12^{15} ; = 12^{15} – 13^{30}
26	8	0.2	.	–	▽ 18^{10} – 15 19^{25} – 36 , 20^{05} – 21^{10}
27	7	0.0	.	–	▽ 15^{40} – 50
28	7	0.1	.	–	• ^{0} 10^{25} – 15^{15} ▽ 16^{25} – 12^{10} ; = 22^{40} – 24
29	7	.	.	–	• ^{0} 2^{35} – 43 , 7^{10} – 28 ; = 0^{00} – 12^{10} , 21^{40} – 24
30	8	.	.	–	
31					
Σ	–	94.6	–	–	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	105.9	105.6	103.5	105.0	14.2	21.5	18.3	18.1	23.4	10.5	81	55	78	71	3.1	11.4	4.6	6.4	2 ⊙	4 ⊙	4	N 1	E 2	C 0
2	100.6	97.6	100.0	99.4	17.8	26.6	14.4	18.3	27.3	13.0	69	50	88	69	6.3	17.6	2.0	8.6	9	8	1	SE 3	SE 4	N 2
3	102.0	102.6	102.5	102.4	14.8	20.0	15.2	16.3	21.1	11.2	82	51	85	73	3.1	11.4	2.6	5.7	2	4	0	W 3	NW 4	C 0
4	101.9	99.8	96.3	99.3	15.1	21.2	22.5	20.3	26.2	9.6	81	68	63	71	3.4	8.2	10.2	7.3	10	10	8	SE 2	ESE 2	ESE 1
5	99.0	96.6	99.1	96.9	21.1	24.3	15.3	19.0	25.5	15.3	83	67	94	81	4.3	10.0	1.0	5.1	4 ⊙	6 ⊙	0	SW 4	NW 6	C 0
6	101.8	102.7	103.5	102.7	14.5	19.9	13.0	15.1	21.8	12.1	79	55	78	71	3.4	10.4	3.3	5.7	4	5 ⊙	0	NW 4	W 4	C 0
7	103.3	105.6	104.4	105.1	16.1	21.7	17.9	18.4	23.2	8.2	75	47	65	62	4.5	13.9	7.3	8.6	1	2	2	NW 1	NW 1	NE 1
8	103.1	100.5	98.6	100.7	17.7	27.5	22.1	22.4	29.5	12.7	62	42	75	60	7.7	21.3	6.7	11.9	10	3 ⊙	6	S 2	SE 2	WNW 1
9	97.5	98.2	97.9	97.9	18.8	17.9	15.0	16.7	22.4	15.0	73	92	87	84	5.9	1.6	2.2	3.2	10	10 ●	2	W 2	W 3	C 0
10	96.8	96.5	95.2	96.2	16.3	21.2	18.3	18.5	23.4	9.7	82	47	73	67	3.2	13.3	5.6	7.4	0	8 ⊙	6	W 1	NW 2	N 1
11	94.8	94.3	94.1	94.4	16.8	24.3	20.0	20.3	25.5	14.9	79	34	67	60	4.1	20.0	7.8	10.6	8	1	4	ENE 2	NE 4	NE 3
12	94.9	95.4	95.4	95.2	17.7	21.3	17.7	18.6	22.3	16.0	98	90	98	95	0.4	2.5	0.4	1.1	10 ●	10	10 ●	NE 2	NE 1	C 0
13	96.4	98.6	100.5	98.5	18.8	22.8	17.5	19.2	23.5	17.1	96	77	93	89	0.9	6.3	1.4	2.9	10	9	2	SSE 2	WSW 3	C 0
14	101.5	100.4	98.6	100.2	15.1	22.0	17.9	18.2	24.1	13.8	100	77	93	90	0.0	6.2	1.4	2.5	10 ≡	6	9	NNW 1	NW 1	C 0
15	96.1	95.3	95.4	95.6	16.6	20.3	16.6	17.5	21.3	13.5	100	82	96	93	0.0	4.2	0.8	1.7	10 ≡	10	4	C 0	W 3	C 0
16	94.7	93.3	89.9	92.6	16.6	18.8	15.1	16.4	19.6	14.6	99	84	97	93	0.2	3.5	0.6	1.4	10 ≡	10	10 ●	N 2	N 4	N 3
17	87.8	87.8	89.1	88.2	17.2	21.6	16.4	17.9	22.0	14.5	94	77	97	89	1.2	5.9	0.6	2.6	10	10	4	C 0	NE 1	C 0
18	90.6	91.6	91.2	91.1	15.1	15.6	14.6	15.0	17.1	14.2	99	99	92	97	0.2	0.2	1.3	0.6	10 ●	10 ●	7	W 3	W 3	W 3
19	90.7	91.2	91.6	91.2	14.8	22.0	18.4	18.4	24.5	11.9	88	53	77	73	2.0	12.4	4.9	6.4	5	5 ⊙	2	W 3	W 3	C 0
20	91.8	91.4	89.9	91.0	17.6	27.0	20.8	21.6	27.3	13.1	81	46	76	68	3.8	19.1	6.0	9.6	5	2 ⊙	2	E 2	SE 3	C 0
21	88.1	87.3	86.4	87.3	18.9	25.9	19.8	21.1	26.6	15.1	79	41	68	63	4.5	19.7	7.3	10.5	2	4 ⊙	6	E 3	ESE 5	E 2
22	86.1	86.1	86.3	86.2	18.4	22.8	16.6	18.6	23.6	15.7	83	65	100	83	3.7	9.6	0.0	4.4	4	8	9	E 4	E 4	C 0
23	86.7	86.8	86.8	86.8	15.7	22.8	18.3	18.8	23.8	13.4	100	58	95	84	0.0	11.5	1.0	4.2	9	5 ⊙	10	C 0	SW 3	NW 3
24	86.3	87.7	90.5	88.2	17.5	17.9	15.6	16.6	20.3	15.6	96	83	79	86	0.8	3.4	3.7	2.6	10	10	4	W 3	W 6	W 3
25	91.7	92.1	91.6	91.8	13.7	17.8	14.0	14.9	19.6	11.8	87	55	84	75	2.0	9.2	2.5	4.6	9	7 ⊙	4	SW 4	SW 4	C 0
26	90.6	91.3	89.9	90.6	12.4	16.3	13.6	14.0	17.0	10.8	98	80	95	91	0.4	3.6	0.7	1.6	10	8	8	WSW 2	S 6	SW 2
27	86.9	85.9	86.4	86.4	13.7	19.0	12.6	14.5	19.5	12.6	100	76	100	92	0.0	5.2	0.0	1.7	10 ●	10	2	SSW 2	SSE 3	C 0
28	87.3	88.7	90.8	88.9	13.2	19.2	12.0	14.1	19.8	10.9	92	58	98	83	1.3	9.2	0.3	3.6	2	8	6	SSW 2	SW 4	WSW 2
29	92.1	93.4	95.6	93.7	13.1	18.5	14.3	15.2	21.0	10.1	93	57	88	79	1.1	9.3	2.0	4.1	3 ⊙	9	3	S 2	S 4	S 3
30	96.1	95.6	98.0	96.6	14.9	15.7	14.9	15.1	18.5	9.9	89	94	97	93	1.8	1.1	0.5	1.1	8	10 ●	8	SSE 2	S 3	W 2
31	101.0	102.0	104.5	102.5	14.8	21.3	16.9	17.5	21.8	14.0	96	85	82	88	0.7	3.9	3.5	2.7	9	9	9	W 4	NW 4	W 3
M	94.9	94.9	95.0	94.9	16.1	21.1	16.6	17.6	22.7	12.9	88	66	86	80	2.4	9.2	3.0	4.9	7.0	7.1	5.0	2.2	3.3	1.1

Sierpień – Août

1	104.6	104.5	103.6	104.2	13.8	21.8	16.8	17.3	23.3	11.2	91	61	81	78	1.5	10.1	3.7	5.1	3 ⊙	4 ⊙	6	W 3	W 4	W 2
2	103.1	101.7	102.5	102.4	15.5	16.6	12.9	14.5	19.1	12.4	80	82	92	85	3.5	3.5	1.3	2.8	0	7 ⊙	5 ●	W 3	W 3	W 3
3	101.3	100.6	100.9	100.9	12.4	18.1	14.3	14.8	20.2	10.3	95	55	92	81	0.7	9.4	1.3	3.8	6	8	7	W 5	W 5	WNW 1
4	101.1	102.1	103.7	102.3	14.6	20.1	14.9	16.1	21.4	12.5	92	62	92	82	1.3	9.0	1.3	3.9	8	6	7	W 2	NW 5	NW 3
5	104.7	105.2	105.3	105.1	15.3	20.3	14.2	16.0	21.6	13.9	89	69	98	85	1.9	7.4	0.4	3.2	10	4	0	NW 3	NW 3	NW 3
6	106.0	105.4	103.8	105.1	15.4	20.6	15.0	16.5	21.9	11.1	96	61	89	82	0.8	9.3	1.8	4.0	3	3	0	NW 3	NW 2	C 0
7	101.6	98.4	93.6	97.9	14.9	22.8	17.9	18.4	23.4	9.4	88	49	84	74	2.0	14.1	3.2	6.4	4	9	10 ●	C 0	SSE 2	SSW 1
8	91.2	93.1	94.8	93.0	15.2	17.6	13.8	15.1	21.2	13.2	96	98	95	96	0.8	0.4	0.7	0.6	9	9 ●	0	NNW 2	N 5	C 0
9	95.1	94.4	91.4	93.6	12.9	20.9	16.0	16.4	21.5	8.2	94	47	80	74	0.9	13.1	3.6	5.9	0	7	2	C 0	SE 2	SE 1
10	87.1	84.8	86.8	86.2	15.8	18.9	16.0	16.7	21.2	12.9	77	76	98	84	4.1	5.1	0.4	3.2	10	10 ●	9	ESE 3	SE 2	SSW 3
11	92.6	95.1	95.5	94.4	16.9	23.2	19.7	19.9	24.7	14.7	87	62	80	76	2.5	10.8	4.5	5.9	0	4	2	SSW 5	SW 5	S 1
12	94.7	93.7	94.3	94.2	18.8	25.8	17.7	20.0	27.6	16.5	78	65	98	80	4.7	11.7	0.4	5.6	3	9	3	SE 2	S 4	C 0
13	96.4	97.2	97.9	97.2	16.2	23.4	17.2	18.5	24.2	13.4	89	51	76	72	1.9	14.1	4.7	6.9	3	4	3	SW 1	SW 4	C 0
14	96.9	96.4	94.0	95.8	17.5	20.1	18.2	18.5	21.5	13.0	79	74	92	82	4.2	6.2	1.7	4.0	8	10	7	SE 1	E 1	NE 2
15	88.9	90.8	93.5	91.1	15.8	19.4	14.6	16.1	20.9	14.2	98	78	98	91	0.3	4.8	0.4	1.8	10 ●	9	6	N 3	NW 3	NW 1
16	95.1	95.2	93.9	94.7	15.1	22.1	18.6	18.6	23.0	10.9	93	59	81	78	1.2	10.9	4.1	5.4	8	8	10 ●	SSE 1	SE 1	E 1
17	92.0	91.7	90.4	91.4	14.0	14.9	13.1	13.8	18.9	13.0	98	87	99	95	0.4	2.2	0.2	0.9	10 ●	10	10 ●	SW 1	NW 3	S 2
18	86.9	87.3	88.3	87.5	12.6	16.7	14.3	14.5	18.4	12.5	95	73	93	87	0.7	5.2	1.1	2.3	10 ●	9	10 ●	SW 6	SW 10	W 8
19	91.4	94.6	97.5	94.5	14.0	17.6	14.8	15.3	20.5	13.8	94	84	96	91	0.9	3.2	0.7	1.6	10 ●	9	8 ●	SW 6	SW 6	SW 3
20	98.8	98.7	98.4	98.6	14.7	18.9	17.0	16.9	21.1	13.6	96	73	76	82	0.7	5.9	4.7	3.8	9	4	10	SSW 3	SW 6	SW 3
21	96.6	96.5	94.3	95.8	15.8	19.0	16.1	16.8	20.4	15.2	89	75	97	87	1.9	5.4	0.6	2.6	10	6	10 ●	SW 3	S 3	SW 1
22	92.3	92.5	93.1	92.6	12.3	15.7	12.2	13.1	16.5	11.9	99	78	93	90	0.2	3.9	1.0	1.7	10	10	9	NW 2	WNW 3	NW 1
23	93.6	94.6	95.6	94.6	10.3	14.1	10.2	11.2	17.1	8.4	86	64	90	80	1.7	5.8	1.2	2.9	3 ⊙	7	2	W 4	SSW 6	C 0
24	95.0	90.7	87.6	91.1	10.0	17.7	13.0	13.4	20.2	7.5	89	57	94	80	1.3	8.6	0.9	3.6	0	8	10 ●	C 0	S 5	SSW 5
25	96.0	96.2	94.7	95.6	10.9	19.2	15.3	15.2	20.0	9.7	86	44	66	65	1.8	12.3	6.0	6.7	1	4 ⊙	3	SW 5	SSW 8	SSE 3
26	92.7	92.6	92.3	92.5	12.9	16.9	11.9	13.4	18.8	11.5	85	54	87	75	2.3	8.7	1.8	4.3	9	8	3	S 3	SSW 3	S 2
27	93.3	95.7	97.0	95.3	11.0	15.2	11.7	12.4	16.9	9.9	92	70	84	82	1.0	5.1	2.1	2.7	10	8	0	SSW 5	SW 5	S 2
28	97.0	96.9	97.5	97.1	10.3	16.0	12.5	12.8	16.4	8.8	94	74	98	89	0.8	4.7	0.4	2.0	10 ●	9	10	SSE 1	SE 2	SE 1
29	98.3	99.7	100.2	99.5	10.3	16.3	13.7	13.5	17.3	8.5	99	69	79	82	0.1	5.8	3.4	3.1	10 ≡	10	10	C 0	SW 1	W 2
30	99.6	99.9	100.1	99.9	9.4	15.1	11.5	11.9	16.8	7.1	97	71	97	88	0.3	5.0	0.4	1.9	3	6	6	C 0	W 3	● 2
31	99.8	99.7	98.3	99.3	10.1	14.3	11.6	11.9	15.8	7.8	92	71	85	83	1.0	4.8	1.9	2.6	2	9	9	SW 3	SSW 3	S 3
M	96.3	96.3	96.2	96.3	13.7	18.7	14.7	15.4	20.4	11.5	91	68	89	83	1.5	7.3	1.9	3.6	6.2	7.4	6.0	2.5	3.8	1.9

Olsztyn – Dajtki $H_s = 133\ m$ $H_b = 138{,}7\ m$ $h_w = 12\ m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ LODU	USŁONECZNIENIE	POGODA
1	7	.	.	–	
2	7	16.4	.	–	☃ $12^{15}-17^{10}$; R^{2} $12^{10}-12^{35}-17^{30}$ SW–NE
3	8	.	.	–	
4	8	16.8	.	–	(R) $22^{45}-24$
5	7	.	.	–	(R) $0^{00}-1^{30}$ ☃R-3^{35} SW ☃-3^{58}; = $3^{58}-7^{25}$
6	8	.	.	–	⌒ $0^{30}-a$
7	8	.	.	–	
8	8	.	.	–	(R) $15^{25}-50$
9	6	0.5	.	–	● $^{0}11^{07}-16^{35}$; (R) $2^{20}-45$
10	7	.	.	–	= $0^{00}-7^{30}$; ⌒^{2} $n-a$
11	7	3.0	.	–	= $0^{00}-4^{10}$
12	6	18.3	.	–	☃ $3^{35}-40$ $5^{40}-7^{20}$ ●$^{1}-13^{20}$, $14^{20}-15^{40}$ ☃ $18^{45}-23^{30}$; R^{0} $20^{05}-30$ SE
13	7	0.0	.	–	☃ $1^{30}-11^{40}$; = $4^{40}-10^{10}$ ≡ $22^{15}-24$
14	7	.	.	–	≡ $0^{00}-3^{40}$ ≡$^{0}-8^{40}$ = -9^{10}, $21^{25}-24$
15	6	0.1	.	–	R^{0} $15^{50}-17^{28}$ E; = $0^{00}-4^{50}$ ≡$^{0}-8^{40}$ = -17^{25}, $19^{30}-24$
16	6	16.6	.	–	☃ $14^{05}-17^{40}$, $17^{55}-22^{40}$; R^{0} $18^{35}-18^{45}-21^{30}$; = $0^{00}-2^{00}$ ≡$^{0}-7^{50}$ = -24
17	7	13.6	.	–	☃ $18^{45}-19^{40}$; = $0^{00}-11^{40}$, $20^{50}-24$
18	6	3.6	.	–	☃ $0^{35}-4^{20}$ ●$^{6}-7^{30}$ ●$^{7}-9^{25}$, 20^{30}; = $0^{00}-24$
19	8	.	.	–	= $0^{00}-2^{30}$, $21^{15}-24$; ⌒^{1} $22^{00}-24$
20	6	.	.	–	= $0^{00}-15^{30}$, $20^{25}-24$; ⌒^{1} $0^{00}-8^{10}$
21	7	.	.	–	= $0^{00}-10^{40}$
22	8	7.3	.	–	☃R $17^{45}-20^{25}$ N–NE–NW–S; = $20^{25}-24$
23	7	1.2	.	–	☃ $15^{30}-50$ $16^{50}-18^{20}$, $18^{40}-19^{25}$ ●^{0} $22^{15}-24$; = $0^{00}-2^{00}$ ≡$^{1}-7^{30}$ = -8^{25}, $20^{30}-24$
24	6	.	.	–	● $^{0}0^{00}-3^{25}$; = $0^{00}-22^{25}$
25	8	10.2	.	–	☃ $10^{40}-11^{10}$, $23^{35}-50$ ●$^{1}-24$; ≤ 23^{05}; ⌒^{0} $19^{15}-23^{35}$
26	7	2.4	.	–	● $^{1}0^{00}-3^{30}$ ●$^{0}-4^{15}$ ☃ $12^{20}-45$ $15^{20}-17^{40}$; = $4^{15}-10^{25}$
27	7	3.0	.	–	☃ $0^{00}-4^{40}$ ●$^{0}7^{15}-8^{50}$ ☃ $15^{30}-16^{50}$ $18^{20}-45$; = $9^{50}-24$
28	8	3.6	.	–	☃ $12^{56}-58$, $13^{32}-37$ $19^{10}-20^{03}$; R^{0} $18^{57}-19^{00}-19^{55}$ NE; = $0^{00}-2^{00}$ ≡$^{0}-3^{50}$ = -10^{38}, $21^{10}-24$; ⌒^{1} $19^{45}-51$
29	7	0.2	.	–	☃ $14^{10}-35$, $18^{50}-19^{25}$
30	6	16.2	.	–	☃ $9^{50}-11^{55}$ $12^{55}-16^{30}$, $18^{58}-20^{20}$; = $3^{40}-17^{20}$
31	8	0.0	.	–	☃ $0^{00}-4^{25}$, $14^{20}-25$; = $0^{00}-9^{20}$
Σ	–	133.3	–	–	UWAGI.

Sierpień – Août

1	7	.	.	–	
2	8	2.5	.	–	☃ $10^{55}-11^{38}$, 12^{35-50}, $17^{50}-18^{30}$, $21^{30}-23^{25}$
3	8	0.2	.	–	☃ $22^{35}-24$
4	7	0.0	.	–	☃ $0^{00}-7^{36}$, 15^{05-12}
5	7	0.0	.	–	☃ 8^{10-30}
6	8	.	.	–	⌒^{2} $n-8^{20}$
7	8	5.4	.	–	● $^{2}1^{15}-23^{40}$ ☃R^{0} $23^{40}-23^{50}-24$ S–NE; = $3^{40}-4^{10}$ ≡$^{0}-5^{40}$ = -8^{30}
8	7	0.3	.	–	☃R^{0} 0^{00} 133 ☃ $2^{31}-4^{40}$, $13^{40}-14^{05}$, 15^{05-25}; = $4^{40}-7^{40}$
9	8	.	.	–	= $2^{20}-5^{30}$ ≡-6^{40} = -7^{30}
10	6	15.1	.	–	● $^{0}13^{05}-15^{05}$ ●^{1} $15^{25}-17^{36}$; ⊕ $7^{28}-10^{20}$
11	7	.	.	–	= $4^{12}-8^{40}$
12	7	1.6	.	–	☃ $13^{30}-16^{25}$; R^{0} $14^{30}-15^{40}$; = $21^{20}-22^{20}$
13	8	.	.	–	
14	7	9.0	.	–	● $^{0}12^{15-30}$
15	7	14.5	.	–	● $^{1}1^{30}-10^{40}$ ● $^{0}-12^{25}$ ☃ $14^{50}-15^{15}$; = $21^{30}-24$
16	8	22.4	.	–	● $^{2}1^{37}-24$; = $0^{00}-8^{30}$
17	6	20.5	.	–	● $^{0}0^{00-10}$ $2^{10}-10^{55}$, $11^{10}-13^{35}$, $18^{55}-24$; = $13^{35}-18^{55}$
18	7	2.4	.	–	● $^{0}0^{00}-11^{20}$ ☃ $16^{50}-18^{20}$, $19^{50}-24$
19	8	7.9	.	–	☃ $0^{00}-1^{50}$ $6^{35}-9^{25}$, $10^{25}-12^{20}$, $17^{55}-20^{42}$, $21^{40}-22^{02}$; R 18^{25}, $19^{35}-20^{42}$ SW–NE; = $4^{40}-12^{20}$, $22^{02}-24$
20	7	0.0	.	–	= $0^{00}-10^{10}$
21	7	19.6	.	–	● $^{6}6^{40}-7^{10}$ 8^{30} 10^{15} ☃ 15^{10-22}, $19^{25}-22^{20}$; = $7^{10}-12^{30}$, $21^{20}-24$
22	7	0.7	.	–	☃ $0^{00}-6^{25}$ ● $^{9}9^{40}-10^{15}$ ☃ 14^{24-44}, 15^{28-46}, $16^{46}-17^{40}$; = $0^{00}-8^{11}$
23	7	0.0	.	–	☃ $1^{45}-3^{39}$ 14^{35-38}
24	8	6.7	.	–	● $^{1}17^{20}-24$; ⌒^{8} $n-a$
25	8	.	.	–	● $^{0}0^{00}-2^{10}$
26	7	0.2	.	–	☃ 18^{07-20}
27	7	0.1	.	–	☃ 13^{13-25} 18^{03-10}
28	7	1.9	.	–	● $^{7}7^{20}-11^{25}$ ☃ $19^{44}-21^{26}$; = $4^{30}-13^{30}$, $22^{36}-24$
29	6	.	.	–	= $0^{00}-1^{30}$ ≡$^{0}-3^{10}$ ≡$^{4}-9^{20}$ = -24
30	7	1.2	.	–	● $^{0}10^{40}-12^{20}$ ☃ 17^{01-45} $20^{40}-21^{15}$; = $0^{00}-8^{05}$ ≡$^{0}-10^{45}$ = -12^{30}; ⌒^{1} $n-8^{10}$
31	7	2.1	.	–	☃ $12^{55}-13^{15}$, $13^{55}-14^{11}$; R^{8} 20^{00-54} SW–E; = $20^{54}-24$; ⌒^{2} $n-9^{10}$
Σ	–	134.3	–	–	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Wrzesień – Septembre 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.9	96.1	98.3	96.8	9.5	10.3	10.5	10.2	12.8	9.4	91	88	94	91	1.1	1.4	0.8	1.1	8	10 ●	2	SSW 4	SW 3	SW 2
2	100.5	100.1	98.9	99.8	10.3	17.2	13.4	13.6	18.4	8.7	92	50	85	76	0.9	9.7	2.3	4.3	3	4	5	SSW 3	SW 5	SE 1
3	96.7	97.3	99.8	97.9	13.0	15.4	10.8	12.5	16.8	10.8	98	86	100	95	0.4	2.4	0.0	0.9	10	9	5	S 2	SSW 4	C 0
4	102.1	103.8	105.0	103.6	9.9	15.9	10.9	11.9	17.7	7.4	97	60	91	83	0.3	7.2	1.1	2.9	4 ⊙	7	2	W 1	NW 1	C 0
5	105.7	104.2	101.7	103.9	6.8	16.8	13.4	12.6	17.7	5.1	97	45	71	71	0.3	10.6	4.5	5.1	0	4	8	C 0	W 3	S 3
6	100.3	101.5	102.0	101.3	13.0	16.3	12.6	13.6	18.1	12.5	89	58	92	80	1.6	7.7	1.2	3.5	4	9	2	SW 3	SW 4	SSW 1
7	104.1	104.4	103.6	104.0	7.5	20.5	14.6	14.3	21.6	4.5	100	47	87	78	0.0	12.7	2.2	5.0	3 ≡	2	4	C 0	SE 2	C 0
8	103.5	103.8	104.0	103.8	13.7	24.5	17.9	18.5	25.5	13.4	85	52	84	74	2.3	14.6	3.2	6.7	3	2	1	SE 2	SE 6	SE 1
9	103.3	102.4	104.5	103.4	16.1	25.0	15.7	18.1	26.2	13.0	82	49	88	73	3.1	16.2	2.1	7.1	3	0 ⊙	10	SSE 1	S 5	NNW 7
10	105.4	104.8	102.2	104.1	13.3	14.9	12.5	13.3	16.1	12.5	74	74	92	80	4.0	4.3	1.2	3.2	10	9	8	NNE 2	N 1	C 0
11	98.3	93.9	86.4	92.9	10.0	18.6	14.8	14.6	19.4	7.1	96	53	71	73	0.5	10.0	4.8	5.1	2	4	10	C 0	S 4	SE 4
12	79.4	76.1	82.2	79.2	15.2	17.7	11.1	13.8	17.9	10.5	91	84	73	83	1.5	3.2	3.6	2.8	10	9	2	S 3	S 4	SW 8
13	86.6	87.8	86.3	86.9	9.7	13.8	11.4	11.6	15.6	8.6	80	59	73	71	2.3	6.5	3.5	4.1	7	8	6	SW 5	SSW 9	S 4
14	85.9	87.4	89.1	87.5	8.8	12.2	11.5	11.0	14.0	8.5	86	67	68	74	1.5	4.6	4.4	3.5	6	8	1	S 5	SSW 8	SSW 4
15	88.7	87.1	90.3	88.7	3.4	8.1	9.9	9.1	11.6	6.9	92	91	92	92	0.9	0.9	1.0	0.9	10 ●	10 ●	8	SSE 1	WNW 1	SW 5
16	94.3	97.5	99.7	97.2	8.3	11.5	7.9	8.9	12.8	7.5	86	70	87	81	1.6	4.1	1.3	2.3	9	8	10	SSW 7	SW 6	C 0
17	99.9	98.6	96.6	98.4	3.5	11.4	5.8	6.6	12.1	1.7	98	66	95	86	0.1	4.6	0.4	1.7	0 ≡	4	0	C 0	NW 2	NW 1
18	89.9	87.2	88.4	88.5	7.8	11.1	9.8	9.6	11.4	5.5	97	84	87	89	0.3	2.1	1.6	1.3	10 ●	10 ●	10	W 4	WNW 9	WNW12
19	88.1	89.1	88.6	88.6	8.7	10.9	8.8	9.3	12.4	8.1	85	71	88	81	1.6	3.7	1.4	2.2	10	9	10	WSW 6	WSW 7	C 0
20	89.0	92.3	96.1	92.5	8.2	10.6	9.1	9.2	12.1	7.7	92	90	95	92	0.9	1.3	0.7	1.0	10	10 ●	4	SW 4	W 4	W 4
21	98.7	99.5	99.7	99.3	7.3	11.1	7.9	8.6	12.3	6.8	97	75	93	88	0.3	3.2	0.7	1.4	6	9	9	W 2	W 4	C 0
22	96.5	94.2	91.7	94.1	8.0	12.2	11.9	11.0	12.8	5.4	90	82	94	89	1.0	2.5	0.8	1.4	9	10	10	E 1	SE 2	C 0
23	86.4	83.7	76.7	82.3	14.9	17.7	14.2	15.2	18.0	10.6	97	79	99	92	0.5	4.2	0.2	1.6	10 ●	10	10 ●	SSE 3	SSW 4	C 0
24	84.2	84.9	83.9	84.3	9.8	11.4	6.0	8.3	14.4	5.7	86	75	79	80	1.7	3.5	2.0	2.4	7	10	3	W 8	WSW 6	WSW 6
25	86.6	93.3	98.2	92.7	5.9	7.9	5.3	6.1	8.9	4.2	89	78	84	84	1.0	2.3	1.4	1.6	10 ●	9	8	W 12	W 14	W 5
26	97.4	98.2	99.9	98.5	3.2	6.9	2.3	3.7	8.5	1.9	91	70	80	80	0.7	3.0	1.4	1.7	9	9	3	W 2	WNW 4	WSW 2
27	98.2	95.2	83.7	92.4	3.4	7.6	7.2	6.4	8.2	1.8	76	68	93	79	1.9	3.3	0.8	2.0	9	10 ●	10 ●	SW 3	SW 6	SW 6
28	79.1	82.4	84.4	82.0	9.0	9.4	6.9	8.0	12.4	6.7	85	85	94	88	1.7	1.7	0.5	1.3	9 ●	9 ●	10 ●	WSW 9	W 9	WNW 3
29	84.6	82.9	80.7	82.7	5.7	8.3	6.5	6.8	10.2	5.2	92	84	96	91	0.8	1.7	0.5	1.0	8	8	7	SW 3	S 2	SSW 1
30	82.1	85.4	92.6	86.7	5.5	6.2	4.9	5.4	8.2	4.8	92	89	89	90	0.7	1.0	1.0	0.9	10 ●	9 ●	5	W 4	WSW 6	WSW 3
31																								
M	93.7	93.8	93.8	93.8	9.1	13.4	10.2	10.7	14.8	7.4	90	71	87	83	1.2	5.1	1.7	2.7	7.0	7.6	6.1	3.3	4.8	2.8

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1	96.2	97.3	100.4	98.0	3.5	6.2	3.4	4.1	7.1	1.8	90	83	91	88	0.8	1.6	0.7	1.0	6	10	5	SW 5	SW 2	W 2
2	104.2	105.9	104.7	104.9	1.3	8.4	3.8	4.3	9.2	0.7	94	93	85	77	0.4	5.1	1.2	2.2	0	5	0	WNW 2	WSW 3	SW 3
3	99.8	95.2	89.3	94.8	3.1	8.6	7.7	6.8	8.8	1.5	83	63	80	75	1.3	4.2	2.1	2.5	6	10	10 ●	SSW 4	S 6	SSW 6
4	88.6	91.3	98.2	92.7	5.5	8.1	4.7	5.8	9.1	4.2	83	61	78	74	1.5	4.3	1.9	2.6	9	9	9 ●	SW 6	W 9	W 6
5	101.0	101.4	99.1	100.5	4.6	8.8	7.3	7.0	9.1	1.8	92	67	69	76	0.7	3.7	3.2	2.5	8	9	10	W 4	SW 6	SSW 6
6	97.1	100.2	103.6	100.3	8.1	11.1	8.8	9.2	11.5	6.0	97	92	86	92	0.3	1.0	1.5	0.9	10 ●	10	10	SW 6	SW 6	W 3
7	101.5	102.8	107.2	103.8	10.9	12.3	10.7	11.2	12.8	8.7	91	80	89	87	1.1	2.9	1.5	1.8	8	10	10	W 8	W 8	NW 3
8	111.8	113.4	113.4	112.9	5.4	13.7	6.0	7.8	14.4	5.1	97	66	95	86	0.3	5.4	0.5	2.1	3	4 ⊙	2	C 0	S 1	C 0
9	111.2	109.5	107.6	109.4	2.5	16.1	7.4	8.4	17.0	2.2	96	55	97	83	0.3	8.2	0.3	2.9	0	0	0	C 0	S 2	C 0
10	106.5	105.2	104.5	105.4	3.8	18.9	11.7	11.5	19.3	3.2	97	67	85	83	0.3	7.1	2.0	3.1	0	0 ⊙	0	C 0	SSE 3	S 3
11	102.9	103.4	103.6	103.3	8.4	15.6	11.0	11.5	16.6	7.6	93	74	95	87	0.7	4.6	0.6	2.0	4	8	10	S 3	SW 2	C 0
12	101.1	101.8	108.0	103.6	9.3	10.4	7.2	8.5	11.7	7.2	99	97	94	97	0.1	0.3	0.6	0.3	10 ≡	10 ●	2	S 2	WSW 2	W 2
13	110.4	109.9	107.3	109.2	5.9	10.2	6.2	7.1	11.2	4.8	100	85	97	94	0.0	1.9	0.3	0.7	10 ≡	9	2	SSW 1	SSW 2	SSW 2
14	104.4	105.5	108.3	106.1	8.8	10.8	5.6	7.7	11.8	5.4	95	82	91	89	0.6	2.3	0.9	1.3	10	10	3	WSW 3	SW 4	W 2
15	110.1	110.6	111.1	110.6	4.2	9.4	7.4	7.1	9.7	2.7	93	66	77	79	0.5	4.0	2.3	2.3	9	8	10	SW 2	W 3	C 0
16	110.6	109.4	106.5	108.8	5.8	8.0	5.1	6.0	8.8	4.9	82	62	80	75	1.7	4.1	1.8	2.5	10	10	8	SSW 1	SSW 2	SE 1
17	100.3	98.1	100.0	99.5	3.2	12.2	10.9	9.3	13.3	3.0	93	76	86	85	0.5	3.4	1.8	1.9	0	10	10	SE 3	SW 6	SW 5
18	96.8	92.5	91.3	93.5	8.2	12.7	13.5	12.0	14.0	6.7	99	84	91	91	0.2	2.4	1.5	1.4	10	10	10 ●	S 1	S 2	S 4
19	90.3	90.8	89.8	90.3	12.5	17.4	14.1	14.5	17.7	12.5	87	70	85	81	1.9	6.1	2.4	3.5	9	9	9	SW 4	SW 3	SSW 2
20	93.1	95.9	98.3	95.8	7.7	9.4	8.6	8.6	14.4	7.5	96	87	93	92	0.5	1.6	0.8	1.0	10 ●	10	9	W 1	SW 1	SW 1
21	99.8	98.9	95.9	98.2	5.8	7.5	5.9	6.3	9.1	4.9	95	83	88	89	0.4	1.8	1.2	1.1	10	9	0	SW 2	SSW 3	SE 4
22	91.9	89.1	88.5	89.8	5.4	9.3	8.0	7.7	10.1	5.0	89	74	87	83	1.0	3.1	1.3	1.8	5	6	10	SSE 3	SE 4	ESE 2
23	89.4	91.5	95.0	92.0	7.8	11.0	7.2	8.3	12.1	7.0	94	78	87	86	0.6	2.9	1.4	1.6	10	4	3	SSE 1	SW 1	SW 3
24	91.9	93.2	100.1	95.1	5.3	7.9	6.2	6.4	9.6	3.9	92	94	83	90	0.7	0.6	1.6	1.0	10 ●	10	0	S 4	SW 6	W 2
25	104.7	107.0	107.6	106.4	3.5	9.0	4.6	5.4	9.3	3.3	95	71	89	85	0.4	3.4	1.0	1.6	0	7 ⊙	4	SW 3	W 3	WSW 1
26	105.0	105.1	104.1	104.7	7.4	12.3	10.4	10.1	12.8	3.9	87	81	74	81	1.3	2.7	3.3	2.4	10	10	3	SSW 2	SW 2	SSW 2
27	101.2	100.7	101.1	101.0	4.5	8.7	6.1	6.4	10.6	4.1	97	90	95	94	0.3	1.0	0.4	0.6	3 ≡	10	10	SSW 2	SSW 2	SSW 1
28	100.7	100.6	101.3	100.9	7.6	9.4	8.2	8.4	9.7	5.6	93	75	83	84	0.7	2.9	1.8	1.8	9	10	10	S 1	SSW 2	SSW 3
29	99.1	99.3	99.9	99.4	7.8	11.5	8.2	8.9	12.2	6.6	84	72	87	81	1.7	3.8	1.4	2.3	9	8	4	S 3	SW 4	S 3
30	97.7	96.3	96.3	96.8	5.8	13.7	11.5	10.6	14.3	5.5	94	62	79	78	0.6	6.0	2.8	3.1	2	6	10	S 2	S 5	SSW 4
31	95.2	93.9	92.0	93.7	10.3	12.5	11.3	11.4	13.5	9.9	96	80	83	86	0.5	2.9	2.3	1.9	10	9	10	SSW 2	SSW 3	SW 3
M	100.5	100.5	101.1	100.7	6.3	11.0	8.0	8.3	12.0	5.1	93	75	86	85	0.7	3.4	1.5	1.9	6.8	8.1	6.2	2.6	3.5	2.5

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$H_s = 133$ m $H_b = 138{,}7$ m $h_w = 12$ m

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DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.9	.	–	▽ 2^56 – 3^56, 10^55 – 12^05, 12^20-40, 13^15 – 14^06, 16^35-50, 19^08-10, ≤ 21^10-50 S, = 0^00 – 7^05
2	7	1.0	.	–	• 12^40 – 24, = 5^10 – 8^20, ⌒ n – 9^00
3	7	2.8	.	–	•^0 0^00 – 7^10, 7^40 – 12^40, ▽^1 16^20 – 17^26, = 7^10 – 13^10, 20^40 – 24
4	7	.	.	–	= 0^00 – 8^10
5	8	0.3	.	–	•^0 23^35 – 24, = 2^20 – 8^30
6	7	.	.	–	•^0 0^00 – 4^30, = 4^30 – 8^10, ⌒^0 21^06 – 24
7	7	.	.	–	≡^0 1^50 – 4^20, ≡^1 – 7^15 ≡^0 – 7^45 = – 11^10, 19^30 – 24, ⌒ 0^00 – 1^50
8	7	.	.	–	= 0^00 – 1^20, 5^10 – 9^20
9	7	.	.	–	= 2^25 – 8^50, 21^20 – 24, ⌒^2 n – a
10	7	0.0	.	–	•^0 10^45, 11^10 – 12^10, = 0^00 – 1^30
11	7	0.0	.	–	≡ 6^50 – 7^45, ⌒^1 n – a
12	7	9.9	.	–	•^0 4^45 – 7^15, 10^50 – 11^16, ▽ 12^10 – 13^26, 19^15-36, ▽ 14^08 – 16^20, = 7^15 – 13^25
13	7	1.0	.	–	▽ 17^10 – 40
14	7	0.0	.	–	▽ 4^10 – 45
15	6	27.0	.	–	•^0 7^10 – 11^35, •^1 – 17^44, •^0 – 19^05, 20^41 – 21^10, = 19^05 – 24
16	7	0.5	.	–	•^0 6^04 – 8^15, ▽ 16^57 17^50, = 0^00 – 10
17	7	3.0	.	–	= 7^05 – 50 ≡^0 – 9^40 = – 11^20, 19^35 – 24
18	6	13.7	.	–	▽ 2^10-35, 3^15 – 8^10, •^0 – 10^06, ▽ – 11^10, 11^30 – 13^20, •^0 – 21^22, ≫ 21^16 – 24
19	7	0.0	.	–	•^0 0^05 – 5^41, ≫ 0^00 – 05
20	6	0.4	.	–	•^0 7^50 – 8^30, ▽ 10^50 – 11^15, 13^13 – 14^20
21	7	0.0	.	–	▽ 12^48-51, 14^29-33, = 2^30 – 10^10, 20^20 – 24, ⌒^2 n – a, ⌒^0 22^15 – 24
22	6	6.5	.	–	•^0 16^50 – 21^10, 22^04 – 24, = 0^00 – 24, ⌒ 0^00 – a
23	6	27.1	.	–	•^0 0^00 – 57, ▽ 3^30 – 5^15, •^0 6^04 – 8^15, 14^10 – 21^30, •^1 – 24, ≡ 1^50 – 3^30 = 9^20 – 22^20
24	7	5.1	.	–	•^1 0^00 – 2^20, •^0 – 6^30, ▽ 14^25 – 17^28
25	7	2.0	.	–	▽ 0^26 – 1^15, 11^40 – 12^22, 14^30 – 15^10, ≫ 0^05 – 19^15
26	8	0.5	.	–	▽ 6^15-30, 9^05-20, 12^30-50, 15^15-25
27	7	11.5	.	–	•^0 9^55 – 11^44, 13^34 – 24
28	7	21.4	.	–	•^0 0^00 – 4^28, ▽ 7^11 – 10^10, 13^13-50, 14^54 – 15^04, 15^31-36, 16^38-53, 17^58 – 18^03, 18^24-26, 18^52 – 20^51, 21^34 – 24
29	7	5.5	.	–	▽ 0^00 – 3^20, 11^55 – 12^20, 12^50, 13^12, 13^45 – 15^25, 16^20 – 17^35, 19^20 – 20^10, ⌓ 20^40 – 21^25
30	6	3.1	.	–	▽ 6^20 – 9^16, 11^27 – 12^43, 13^29 – 14^22, 15^24-56, 17^01 – 11, 17^49 – 18^13, 19^44 – 20^06
31					
Σ	–	143.2	–	–	UWAGI.

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1	7	0.3	.	–	▽ 2^06 – 3^14, 7^54 – 8^16, 13^15 – 14^25, 17^50 – 18^10
2	8	0.0	.	–	▽ 14^35 – 15^08
3	7	1.2	.	–	•^0 14^25 – 24, = 15^10 – 20^40
4	7	1.9	.	–	•^0 0^00 – 1^40, ▽ 3^55 – 4^15, 11^45-55, 16^45 – 17^15, 19^20 – 21^15, 22^45 – 23^20
5	7	1.8	.	–	▽ 10^50 – 11^05, •^0 22^15 – 24
6	6	0.5	.	–	•^0 0^00 – 7^40, 11^55 – 12^25, 13^15 – 40, 18^30 – 19^10, = 3^10 – 19^20
7	7	0.6	.	–	•^0 3^15 – 6^10, 8^30 – 10^10, = 6^10 – 10^30
8	8	.	.	–	≡ 6^06 – 54 = 19^15 – 24
9	7	.	.	–	= 0^00 – 5^12 ≡ – 7^30 = – 10^40, 20^20 – 24
10	7	.	.	–	= 0^00 – 2^40 ≡ – 7^45, ⌣^0 n – a
11	6	.	.	–	= 1^10 – 24
12	5	0.8	.	–	•^0 8^50 – 9^30, 11^25 – 13^10 = 0^00 – 6^10 ≡ – 8^50 = – 24, ⌣ 20^30 – 23^10
13	7	.	.	–	= 0^00 – 4^30 ≡^0 – 9^25 = – 11^30, 20^20 – 24
14	5	.	.	–	= 0^00 – 24
15	7	.	.	–	= 0^00 – 11^30
16	7	.	.	–	= 6^20 – 7^44
17	6	0.0	.	–	•^0 13^10-35 = 5^10 – 24
18	6	0.0	.	–	•^0 11^23 – 12^40, 19^40, 21^10, = 0^00 – 6^20 ≡^0 – 7^40 = – 24
19	6	0.7	.	–	= 0^00 – 10^30 ∞ 12^30 – 17^45 = – 24
20	6	0.6	.	–	•^0 3^50 – 11^20, = 0^00 – 1^40, 11^20 – 24
21	6	.	.	–	= 0^00 – 24
22	7	0.2	.	–	•^0 22^45 – 24, = 0^00 – 10^30
23	6	0.3	.	–	•^0 0^00 – 40, = 0^40 – 24
24	6	4.3	.	–	•^0 6^04 – 12^20, = 0^00 – 18^20
25	8	0.3	.	–	= 20^54 – 24
26	6	0.0	.	–	•^0 1^35 – 3^22, 6^54 – 7^40, = 6^10 – 24
27	4	.	.	–	= 0^00 – 6^10 ≡^0 – 12^34 = – 24
28	5	.	.	–	= 0^00 – 24
29	6	.	.	–	= 0^00 – 24
30	6	5.3	.	–	•^0 21^20 – 24, = 0^00 – 21^20
31	6	.	.	–	•^0 0^00 – 2^20, •^0 3^20 – 6^05, = 2^20 – 3^20, 6^05 – 24
Σ	–	18.2	–	–	UWAGI.

Olsztyn – Dajtki

$\varphi = 53°46'$ $\lambda = 20°25'$

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DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	88.3	86.9	89.5	88.2	8.0	10.3	10.0	9.6	11.6	7.6	85	75	84	81	1.3	3.1	1.9	2.2	5	10	9	SSW 3	SSW 3	S 2
2	93.6	95.2	97.7	95.5	6.0	11.1	7.0	7.8	11.4	5.8	97	73	82	84	0.3	3.6	1.7	1.9	3	5	9	S 1	S 2	S 1
3	99.1	99.8	99.4	99.4	6.7	9.3	6.9	7.4	9.7	5.5	88	76	96	87	1.2	2.8	0.4	1.5	9	8	10	SSE 1	E 1	E 2
4	97.3	97.7	97.9	97.6	8.0	9.5	10.9	9.8	11.2	6.6	94	97	99	97	0.6	0.3	0.1	0.3	9	10	10 =	SE 2	SE 2	SE 2
5	96.6	94.6	94.3	95.2	8.6	11.4	11.8	10.9	14.0	8.3	97	88	87	91	0.3	1.7	1.8	1.3	10 =	9	7	CB 3	SE 6	SE 6
6	94.7	94.2	94.7	94.5	8.2	14.3	11.7	11.5	14.7	7.8	93	71	82	82	0.8	4.8	2.5	2.7	9	8	9	SE 3	SE 4	SE 3
7	91.9	91.2	91.5	91.5	9.2	10.5	11.3	10.6	12.4	8.7	87	79	83	83	1.5	2.7	2.3	2.2	10	9	10 •	SE 6	SE 6	SE 6
8	93.1	93.9	94.3	93.8	9.0	10.7	8.6	9.2	11.6	7.7	89	82	92	88	1.3	2.3	1.0	1.5	10	9	10	SE 2	ESE 2	SE 3
9	93.1	93.1	94.8	93.7	8.6	10.3	9.2	9.3	11.7	8.2	90	82	88	87	1.1	2.2	1.4	1.6	10	10	9	SE 4	ESE 3	E 2
10	95.6	97.4	100.1	97.7	8.9	9.2	7.9	8.5	9.5	7.7	97	93	97	96	0.3	0.8	0.2	0.4	10	10	10 •	E 3	E 4	E 3
11	102.6	106.6	107.5	104.9	7.7	7.6	5.6	6.6	8.6	5.4	94	91	85	90	0.6	0.9	1.4	1.0	10	10	10	ENE 3	ENE 6	ENE 7
12	110.3	112.3	113.8	112.1	3.2	2.1	0.6	1.6	3.4	0.5	88	91	92	90	0.9	0.6	0.5	0.7	10	10	10	NE 5	NE 3	NE 2
13	114.2	114.6	114.6	114.5	−2.1	−1.5	−2.8	−2.3	1.3	−4.4	84	85	94	87	0.8	0.9	0.5	0.7	10	10	0	NE 2	ENE 2	C 0
14	113.2	114.0	115.3	114.2	−0.3	1.6	1.9	1.3	2.1	−4.1	86	81	84	84	0.9	1.3	1.2	1.1	10	10	10 .	SSW 1	SW 2	SW 1
15	115.8	114.9	114.1	114.9	1.1	1.4	−0.8	0.2	2.1	−0.8	90	76	77	81	0.6	1.7	1.4	1.2	10	10	10	WSW 1	SSW 2	SSW 2
16	113.0	114.7	116.1	114.6	−2.6	0.3	0.4	−0.4	0.8	−2.8	94	84	96	90	0.4	0.9	0.3	0.5	6	10	10 *	WSW 1	E 1	SE 1
17	117.0	117.9	119.2	118.0	0.6	2.6	1.4	1.5	3.0	0.2	96	75	85	85	0.3	1.9	1.0	1.1	10	9	10	C 0	S 1	C 0
18	118.5	117.6	117.1	117.7	1.5	2.9	1.4	1.8	3.0	0.8	80	71	70	74	1.4	2.2	2.1	1.9	10	10	10	C 0	SE 1	C 0
19	117.5	119.7	122.7	120.0	0.9	2.9	1.7	1.8	3.0	0.7	83	67	87	79	1.1	2.4	0.9	1.5	10	10	10	C 0	E 2	E 1
20	124.1	124.4	123.2	123.9	1.4	2.7	−2.3	−0.1	2.7	−2.4	81	60	89	77	1.3	2.9	0.6	1.6	10	10	0	SE 1	SE 2	SE 1
21	121.1	119.4	115.1	118.5	−3.2	3.3	−2.1	−1.0	3.7	−5.5	90	60	89	80	0.9	3.1	0.6	1.4	3	2	0	S 1	SSW 1	SSW 1
22	106.7	103.1	99.9	103.2	−3.5	2.4	1.3	0.4	2.5	−4.4	93	68	79	80	0.3	2.4	1.4	1.4	0	0	10	SSE 2	SSE 4	S 3
23	97.5	96.0	96.1	96.5	0.4	0.4	0.6	0.5	1.4	0.1	84	92	96	91	1.0	0.5	0.3	0.6	10	10 *	10 *	SSW 4	SW 5	W 3
24	100.4	98.2	97.0	98.5	0.1	1.5	4.8	2.8	5.1	−0.1	92	87	92	90	0.5	0.9	0.7	0.7	3	10 *	10 •	SW 3	WSW 4	WSW 3
25	94.8	96.4	99.1	96.8	5.6	7.0	7.2	6.8	7.3	4.2	95	97	97	96	0.4	0.3	0.3	0.3	10 •	10 •	10 •	W 6	W 3	WNW 2
26	100.7	101.1	97.7	99.8	7.1	7.5	7.4	7.4	7.8	6.7	97	96	93	95	0.3	0.5	0.8	0.5	10 •	10 •	10 •	W 2	W 2	W 4
27	91.1	92.4	97.0	93.5	6.8	7.1	5.0	6.0	7.5	4.9	90	84	92	89	1.0	1.6	0.7	1.1	10 •	10 •	10 •	W 9	W 9	NW 3
28	92.2	87.5	81.6	87.1	5.2	7.8	5.9	6.2	8.1	4.4	95	94	89	93	0.4	0.6	1.0	0.7	10 •	10 •	10 •	SW 2	WSW 3	W 8
29	86.8	95.7	108.5	97.0	0.4	−6.9	−7.8	−5.5	6.1	−8.3	94	80	67	80	0.4	0.7	1.1	0.7	9 *	10 *	0	NNW 8	N 10	N 10
30	112.5	113.1	113.5	113.0	−6.8	−4.3	−6.8	−6.2	−3.9	−8.1	80	70	77	76	0.7	1.3	0.8	0.9	0	3	0	N 6	N 8	N 4
31																								
M	103.1	103.4	104.1	103.5	3.5	5.2	3.9	4.1	6.4	2.0	90	81	87	86	0.8	1.7	1.0	1.2	8.2	8.7	8.1	2.8	3.5	2.9

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1	110.9	108.7	108.3	109.3	−6.8	−0.9	−1.7	−2.8	−0.9	−9.4	75	75	90	80	0.9	1.4	0.6	1.0	5	6	10 △	W 1	WSW 2	SSW 2
2	108.8	109.4	109.7	109.3	−1.7	0.0	−0.3	−0.6	0.1	−2.0	92	94	98	95	0.4	0.4	0.2	0.3	10	10 △	10 *	SW 1	C 0	SW 1
3	104.8	104.0	105.9	104.9	1.1	2.8	1.7	1.8	3.0	−0.4	100	98	98	99	0.0	0.2	0.1	0.1	10 ≡ •	10 ≡ •	10 •	W 1	N 2	NE 3
4	105.6	103.9	100.8	103.4	0.9	1.6	1.9	1.6	3.0	0.6	98	96	98	97	0.1	0.3	0.1	0.2	10 =	10 •	10 ≡ •	C 0	S 2	SW 3
5	96.1	97.2	101.8	98.4	5.5	5.4	3.8	4.6	6.0	1.8	95	84	90	90	0.4	1.4	0.8	0.9	10	9	10	W 4	NW 6	NW 6
6	108.0	109.2	106.5	107.9	−3.5	0.2	−3.3	−2.5	4.0	−4.0	93	86	92	90	0.3	0.9	0.4	0.5	0	4	0	C 0	NW 1	SE 1
7	98.0	94.0	88.4	93.5	−1.5	−1.0	0.0	−0.6	0.1	−3.9	82	87	94	88	1.0	0.8	0.4	0.7	9	10	10	SSW 5	SSW 5	SSW 5
8	75.1	65.5	55.5	65.4	−1.2	1.0	5.2	2.6	5.5	−2.2	89	88	94	90	0.6	0.8	0.5	0.6	10 *	10 •	10 •	S 7	S 8	SW 6
9	50.4	62.5	74.6	62.5	3.0	0.4	−2.7	−0.5	5.7	−3.0	91	92	60	81	0.7	0.5	2.0	1.1	10 •	10 ⁂	3	SW 10	WSW 8	WSW 10
10	76.8	78.0	82.7	79.2	−1.9	−3.4	−4.4	−3.5	−1.5	−5.3	79	83	84	82	1.1	0.8	0.7	0.9	9	10 *	2	SW 9	WSW 5	WSW 5
11	88.8	91.5	91.2	90.5	−5.4	−2.1	−6.3	−5.0	−1.6	−6.4	62	42	70	58	1.5	3.0	1.1	1.9	5	8	2	SW 7	SW 1	E 1
12	86.7	85.7	83.8	85.4	−3.5	−1.6	−1.5	−2.0	−1.5	−7.1	65	76	89	77	1.6	1.3	0.6	1.2	8	10	10	NNE 7	E 3	E 2
13	80.5	77.8	72.2	76.8	−0.4	1.7	1.9	1.3	2.4	−1.9	94	90	94	93	0.3	0.6	0.4	0.4	10	10	10	E 3	E 3	E 1
14	67.9	74.0	86.6	76.2	−0.6	−4.6	−4.3	−3.4	2.8	−5.2	94	91	79	88	0.3	0.4	0.9	0.5	10	10 •	10	NNE 5	NNE 8	NNE 10
15	99.9	106.0	111.2	105.7	−8.7	−6.4	−11.0	−9.3	−4.3	−12.5	71	68	90	76	0.9	1.2	0.3	0.8	4	7	0	NNE 5	NE 2	C 0
16	112.9	114.5	113.8	113.7	−10.8	−5.5	−10.3	−9.2	−4.8	−13.0	87	70	84	80	0.4	1.2	0.4	0.7	0	3	0	SE 1	SW 1	C 0
17	110.0	107.2	105.9	107.7	−13.3	−4.4	−11.4	−10.1	−4.2	−14.1	84	56	86	75	0.4	2.0	0.4	0.9	2	2 ⊙	0	C 0	SE 1	C 0
18	106.2	106.6	108.0	106.9	−13.8	−4.3	−12.9	−11.0	−2.6	−15.3	83	65	92	80	0.3	1.5	0.2	0.7	2	0	0	C 0	S 1	C 0
19	109.6	111.0	113.1	111.2	−11.7	−6.1	−8.5	−6.7	−4.3	−15.5	89	94	88	90	0.3	0.2	0.5	0.3	9	10	10	C 0	SE 1	SSW 2
20	112.9	113.1	111.5	112.5	−1.8	0.3	−0.5	−0.6	0.6	−4.6	90	86	92	89	0.5	0.8	0.5	0.6	10	8	9	SW 2	SW 3	SSW 4
21	106.4	104.6	107.6	106.2	−0.7	1.8	2.3	1.4	2.5	−4.4	83	78	91	84	1.0	1.6	0.6	1.1	6	10	10	SW 5	SW 5	SW 3
22	107.6	107.3	107.6	107.5	1.4	1.8	1.7	1.6	2.3	1.0	96	96	98	97	0.3	0.3	0.1	0.2	10	10 =	10 ≡	SSW 4	SW 4	SW 2
23	106.0	104.0	101.7	103.9	1.4	1.2	−1.6	−0.2	1.9	−1.8	100	89	82	90	0.0	0.8	1.0	0.6	10 =	9	0	S 2	SE 2	SE 2
24	99.8	100.2	101.8	100.6	−4.7	−1.7	−2.2	−2.7	−1.4	−4.9	88	78	84	83	0.5	1.2	0.8	0.8	2	4	10	SE 1	SE 2	S 1
25	101.7	100.8	100.4	101.0	−4.6	−0.7	−1.7	−2.2	−0.4	−5.3	90	75	82	82	0.4	1.4	1.0	0.9	0	7	6	C 0	S 1	S 4
26	101.9	103.6	106.2	103.9	−1.0	0.4	1.6	0.6	1.6	−2.8	95	96	96	96	0.3	0.3	0.3	0.3	10 =	10 =	10 •	SSW 2	SW 4	SW 3
27	105.4	104.6	103.2	104.4	1.3	1.0	1.7	1.4	1.8	0.4	96	94	96	95	0.2	0.4	0.3	0.3	10	10 •	10 =	SW 4	SW 3	SW 5
28	98.1	94.2	89.9	94.1	1.6	2.5	2.4	2.2	2.8	1.4	96	91	91	93	0.3	0.6	0.7	0.5	10 =	10	10 •	SW 4	SW 5	SW 7
29	86.1	86.0	82.0	84.7	2.3	2.1	2.1	2.2	2.7	0.5	86	89	84	86	1.0	0.8	1.2	1.0	10	9	9	SW 5	SW 5	SW 6
30	75.1	76.3	74.9	75.4	2.7	2.8	0.4	1.6	3.6	0.0	79	79	94	84	1.5	1.6	0.4	1.2	4	9	9	WSW 7	SW 6	SW 2
31	77.8	80.1	80.3	79.4	−0.3	0.2	0.1	0.0	0.4	−1.2	90	86	80	85	0.6	0.9	1.3	0.9	8	8	7	SW 8	SW 4	SW 4
M	96.0	96.2	96.4	96.2	−2.3	−0.5	−1.7	−1.6	0.8	−4.3	87	83	88	86	0.6	1.0	0.6	0.7	7.2	8.2	7.0	3.5	3.4	3.3

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$H_s = 133$ m $H_b = 138{,}7$ m $h_w = 12$ m

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DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ LODU	USŁONECZNIENIE	POGODA
1	6	0.0	.	-	• 17⁴⁰–20²⁰, = 0⁰⁰–24
2	6	.	.	-	= 0⁰⁰–24
3	7	.	.	-	= 0⁰⁰–7³⁰, 20¹⁵–24
4	4	.	.	-	= 0⁰⁰–10, ≡¹–6²⁵ = –17⁴⁰ ≡⁰–24
5	5	.	.	-	≡⁰ 0⁰⁰–3³⁸ = –6⁴⁰ ≡⁰–8⁵⁰ = –24
6	7	.	.	-	= 0⁰⁰–10³⁰
7	6	0.3	.	-	• 19³⁰–24, = 6¹⁰–24
8	6	.	.	-	• 0⁰⁰–2⁴⁰, = 0⁰⁰–24
9	6	0.0	.	-	= 0⁰⁰–24
10	6	0.1	.	-	• ¹5¹⁰–6²⁵ • ⁰8¹⁰–9²⁵, 15¹⁰–17⁵⁰, 18³³–24, = 0⁰⁰–5¹⁰, 6²⁵–24
11	6	0.0	.	-	• 0⁰⁰–3⁴⁴, 7¹⁰–11³⁰, = 0⁰⁰–18³⁰
12	7	.	.	-	
13	7	.	.	-	
14	7	0.0	.	-	
15	6	(0.0)	.	-	• ⁰2⁵⁵–4⁵⁵, 7⁰⁵–11, = 0³⁰–19²⁰
16	6	0.3	.	-	* ⁰13⁴⁰–15⁴⁰, 20¹⁰–23²⁰, = 6²⁰–24
17	6	.	.	-	• 0⁰⁰–2³⁰, = 0⁰⁰–13⁴⁰
18	7	.	.	-	
19	7	.	.	-	
20	7	.	.	-	
21	7	.	.	-	= 6²⁰–10¹⁰, ⌴ 3⁵⁰–7²⁰
22	6	.	.	-	= 0⁰⁰–24, ⌴ 1⁵⁰–24
23	5	3.3	.	-	• ⁰9³⁵ 10⁴⁰ * ⁰ 17²⁰–21⁴⁰ • ⁰–24, = 0⁰⁰–24, ⌴ ⁰ 0⁰⁰–8¹⁰
24	6	2.2	.	-	• ⁰0⁰⁰–2³⁵ * ⁰ 10⁴⁵–11⁰⁵ * ¹–12¹⁵ * ⁰– 14⁵⁵ • ⁰ 16⁵⁰–18²⁵, 20²⁰–24, = 0⁰⁰–3¹⁰, 14⁰⁰–24
25	6	1.4	.	-	• ⁰0⁰⁰–1²⁰ • ⁰–7¹⁵ • ⁰–18³⁰, 19³³–24, = 0⁰⁰–24
26	6	3.3	.	-	• ⁰0⁰⁰–10²⁰ 18⁴⁰ • ¹ 20²⁰–24, = 0⁰⁰–24
27	6	4.5	.	-	• ¹0⁰⁰–2⁴⁰ • ⁰–6²⁰ • ⁰ 20¹⁰ • ⁰–24, = 0⁰⁰–24
28	6	10.7	.	-	• ⁰0⁰⁰ 2⁴⁰–4²⁰ • ⁰–9⁴⁰ • ¹–11⁵⁰ • ⁰–13³⁰ • ⁰–18³⁵, 19¹⁰–24, = 0⁰⁰–24
29	7	0.3	pł.	-	• ⁰0⁰⁰–4¹⁵ * –5⁴⁰ * ¹–6²⁰ * –7¹⁶, 11¹⁰–16³⁰, » 3¹⁰–6³⁰
30	8	.	ł	-	
31					
Σ	–	26.4	–	-	UWAGI

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1	7	0.0	ł	-	* ⁰14²⁰–15²⁰ △⁰–21²⁵
2	6	0.2	ł	-	△ 3⁴⁵–6¹⁰, 11⁴⁰–13²⁶ * ⁰ 16²⁰–21¹⁰, = 5²⁰–21⁴⁵ ≡⁰–24
3	3	0.1	ł	-	• ⁰4⁴⁵–7¹⁵, 9³⁰–13³⁰ 18¹⁵–24 ≡⁰ 0⁰⁰–20³⁰
4	6	1.0	.	-	• ⁰0⁰⁰–3¹⁵, 10³⁰–12⁴⁰ 16³⁵–18²⁵, 20⁴⁵ 23²⁰–24, ≡⁰ 3¹⁵–9³⁰ = –15⁴⁰ ≡⁰–24
5	7	0.2	.	-	• ⁰0⁰⁰–3⁴⁰ ▽ 17⁰⁵–18⁴⁵, 20²⁰–50, 21³⁰–55, ≡⁰ 0⁰⁰–6²⁰ = –12³⁰
6	8	:	.	-	= 15³⁰–24, ⌴¹ 18²⁰–24
7	6	0.0	.	-	= 0⁰⁰–11¹⁰ ∞–12³⁰ = –24, ⌴² 0⁰⁰–a
8	5	8.4	.	-	* ⁰3²⁵–7⁸⁰ △ 10⁵⁰–11²⁰ • ¹–13¹⁰ * –18²⁰ • ⁰–20⁰⁵, = 0⁰⁰–22¹⁰
9	6	0.1	.	-	• ⁰3¹⁵–11²⁰ * –13⁵⁰ * ⁰–14³⁵ » 15⁴⁰–24
10	6	0.3	.	-	▽ 0³⁰–2⁴⁵, 3¹⁰–5⁵⁰, 11⁰²–14²⁰, 19¹⁵–20²⁵, » 0⁰⁰–6³⁰
11	7	.	ł	-	⊍ 21²⁰–24
12	7	.	ł	-	⊍ 0⁰⁰–3²⁰
13	5	2.1	.	-	• ⁰21⁴⁰–24, = 0¹⁵–45 ≡⁰–6¹⁵ = –24
14	6	0.4	.	-	• ⁰0⁰⁰–6³⁰, 6⁵⁰–9²⁵, 10²⁰–11¹⁰ • * ⁰–14¹⁰ * ⁰–18³⁰, = 0⁰⁰–19²⁶
15	8	.	pł.	-	
16	8	.	pł.	-	V n– 10³⁰
17	7	.	pł.	-	= 18³⁰–24
18	6	.	pł.	-	= 0⁰⁰–3³⁰, 9³⁰–12¹⁰ ∞–15²⁰ = –24
19	6	.	pł.	-	= 0⁰⁰–24
20	6	.	pł.	-	= 0⁰⁰–19¹⁰
21	7	0.0	pł.	-	• ⁰15²⁰–40, 17³⁰–40, 21¹⁰ 22⁵⁰, = 15⁴⁰–24
22	2	0.0	.	-	• ⁰4²⁵–45 • ⁰9²⁰–12²⁰ 22²⁰–24, = 0⁰⁰–7¹⁵ ≡⁰–12²⁰ ≡¹–20¹⁰ ≡⁰–24
23	5	.	.	-	• ⁰0⁰⁰–2³⁰, ≡⁰ 0⁰⁰–10²⁰ = –24
24	6	.	.	-	= 0⁰⁰–24
25	6	.	.	-	= 0⁰⁰–24
26	3	0.1	.	-	• ⁰18¹⁰–24, = 0⁰⁰–3³⁵ ≡¹–9³⁰ ≡⁰–15²⁰ ≡¹–18⁴⁰ = –24
27	5	0.2	.	-	• ⁰0⁰⁰–5²⁰ 10¹⁰–15³⁰, = 0⁰⁰–7³⁰ ≡⁰–10⁴⁰ = –18³⁰ ≡⁰–24
28	5	1.6	.	-	• ¹0³⁰–2⁵⁰ • ⁰–4³⁰ • ⁰ 16²⁰ 21³⁰ • ¹–22⁵⁰, ≡⁰ 0⁰⁰–12²⁰ = –24
29	7	3.9	.	-	• ⁰0¹⁵–3¹⁵ 7⁴⁵–8⁵⁰ 9⁴⁵ ▽–10²⁰ ▽–11⁴⁰, 12⁴⁰–13⁰⁶ ▽ 18⁵¹ 19⁰⁵ ▽ 21⁴⁰ 22⁴⁵ ▽–24, = 0⁰⁰–10²⁰
30	8	2.3	.	-	▽ 0⁰⁰–30 0³⁵–50 0⁵⁵–15⁵ ▽ 12⁵⁰–15³⁵ 16³⁰–17⁴⁰ 19¹⁰–20²⁰ ▽ 21²⁰–22³⁰ *¹–24, » 3³⁰–5³⁰
31	7	0.0	ł	-	* ¹0⁰⁰–1³⁰ * ⁰–3⁴⁰ ▽ 8³⁰–50, 10⁴⁵–11³⁰, 18⁴⁰–19³⁰, 20⁵⁵–21³⁰, 23⁴⁵–24
Σ	–	22.9	–	-	UWAGI.

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$

Styczeń–Janvier 1957

DNI	CIŚNIENIE P=				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	116.5	115.5	114.8	115.6	-6.5	-6.2	-6.2	-6.3	-5.7	-9.8	94	97	94	95	0.2	0.1	0.2	0.2	10	10	10	SE 1	E 1	E 1
2	111.1	110.5	114.0	111.9	-3.2	-1.3	-0.6	-1.4	-0.5	-6.9	97	95	93	95	0.1	0.3	0.4	0.3	10	10	10	SE 2	ESE 2	SW 4
3	118.?	117.4	116.8	117.4	0.5	0.4	1.6	1.0	1.9	-1.0	90	92	89	90	0.6	0.5	0.8	0.6	10	10	10	SW 3	SSW 3	S 2
4	119.0	118.9	118.3	118.7	1.9	2.6	3.2	2.7	3.7	1.1	91	93	90	91	0.6	0.6	0.8	0.7	10	10	10	SSW 3	SW 5	SW 5
5	115.3	111.9	112.5	113.2	4.7	6.8	8.8	7.3	9.4	2.3	95	97	97	96	0.4	0.3	0.3	0.3	10 ●	10 ●	10	SW 7	SW 6	SW 4
6	106.6	108.6	111.9	109.0	10.7	8.8	4.7	7.2	11.0	3.8	91	76	82	83	1.2	2.7	1.5	1.8	10	9	6	SW 8	WNW 8	W 8
7	120.1	124.8	127.7	124.2	6.4	6.7	5.1	5.8	7.0	3.9	75	72	84	77	2.4	2.7	1.4	2.2	9	8	9	WNW 9	NW 8	W 5
8	125.3	124.3	122.2	123.9	5.8	7.3	7.6	7.1	8.4	4.0	86	87	94	89	1.3	1.3	0.6	1.1	10	10	10	WSW 4	WSW 7	W 7
9	119.3	117.2	115.5	116.7	8.0	8.8	8.1	8.2	9.0	7.2	87	81	82	83	1.3	2.1	2.0	1.8	9	9	10	SW 7	SW 5	SW 5
10	111.5	110.8	112.6	111.6	4.9	5.3	3.6	4.4	8.3	3.1	82	71	76	76	1.6	2.6	1.9	2.0	7	9	9	SW 4	W 8	WNW 6
11	118.8	119.7	121.1	118.9	1.3	4.1	0.0	1.4	4.4	-0.4	83	71	88	81	1.1	2.4	0.7	1.4	0	1	0	W 5	NNW 5	W 5
12	111.1	104.0	99.0	104.7	1.2	3.2	2.7	2.4	3.5	-1.4	96	91	95	94	0.3	0.7	0.4	0.5	10 ✱	10 ●	9	SW 6	WSW 7	W 5
13	100.7	103.2	110.7	104.9	2.2	3.3	0.7	1.7	3.4	0.3	95	97	90	94	0.4	0.2	0.6	0.4	9	10 ●	10	W 1	SW 1	NNE 6
14	120.3	124.6	128.4	124.4	-2.5	-2.8	-4.9	-3.8	1.0	-5.4	80	73	73	73	1.0	1.3	1.1	1.1	10	9	10	NE 7	NE 9	E 7
15	129.8	129.1	129.5	129.5	-8.9	-5.2	-8.2	-7.6	-4.1	-9.4	86	75	89	83	0.4	1.0	0.3	0.6	6	2	1	NE 5	NNE 4	C 0
16	130.4	131.3	132.7	131.5	-3.4	0.2	-2.6	-2.1	1.0	-10.2	90	74	93	86	0.3	1.6	0.3	0.8	10 ✱	5	9	W 2	NNE 4	NW 2
17	131.6	132.2	131.6	131.8	-1.1	-0.8	-0.8	-0.9	0.2	-3.2	95	97	99	97	0.3	0.2	0.0	0.2	10	10 ≡	10 ≡	SW 1	SW 1	SW 1
18	130.1	129.5	127.0	128.9	-2.8	-2.3	-0.2	-1.4	-0.2	-3.8	95	98	94	96	0.2	0.1	0.4	0.2	10 ≡	10	10	W 3	SW 4	SW 4
19	128.1	129.2	129.4	128.9	0.2	0.8	0.8	0.6	1.1	-0.6	94	92	98	95	0.4	0.5	0.2	0.4	10	10	10 ●	NW 2	WNW 2	SW 2
20	127.4	125.6	122.3	125.1	0.9	1.6	0.6	0.9	2.4	0.1	92	87	84	88	0.5	0.9	1.0	0.8	10 ●	10	10	W 4	WSW 6	SW 8
21	118.4	119.7	120.1	119.4	-2.2	0.1	0.0	-0.5	0.7	-2.8	85	73	78	79	0.8	1.7	1.3	1.3	0	9	10	SW 7	W 6	SW 7
22	119.6	117.6	116.0	117.7	-4.8	-0.5	-2.5	-2.6	0.8	-5.9	78	66	74	73	0.9	2.0	1.4	1.4	2	0	0	SW 6	SW 6	SW 4
23	115.5	116.2	115.0	115.6	-0.5	2.1	-3.8	-1.5	3.8	-4.3	76	60	80	72	1.4	2.8	0.9	1.7	9	0	0	SW 6	SW 4	SE 3
24	110.5	108.6	107.6	108.9	-0.6	0.5	-1.2	-0.6	0.7	-4.7	66	57	74	66	2.0	2.7	1.4	2.0	10	10	10	SE 5	SE 6	SE 2
25	106.2	107.5	111.8	108.5	-2.0	0.7	1.6	0.5	1.9	-4.1	87	85	93	88	0.7	1.0	0.6	0.8	9	10	10	SW 1	SW 3	SW 2
26	115.2	114.8	109.5	113.2	1.7	3.4	3.9	3.2	4.2	-0.2	83	73	65	74	1.1	2.1	2.8	2.0	10	0	10	SW 4	SW 6	SSW 9
27	109.4	112.9	115.6	112.6	4.4	5.9	2.3	3.7	6.4	1.6	97	70	79	82	0.3	2.8	1.5	1.5	10	9	0	SW 5	W 8	SW 5
28	117.2	124.6	128.7	123.5	2.1	4.3	0.6	1.9	5.7	-0.2	84	80	90	85	1.2	1.6	0.6	1.1	10	6	0	W 5	NW 6	SW 4
29	126.5	125.7	123.7	125.3	1.9	2.6	2.9	2.6	3.6	-0.2	87	93	88	89	0.9	0.6	0.9	0.8	10	10	0	SW 6	SW 7	SW 6
30	120.7	119.3	119.7	119.9	0.3	2.9	1.7	1.6	4.0	-0.1	84	77	98	86	0.9	1.7	0.1	0.9	8	7	10 ≡	SW 4	W 4	SW 1
31	119.8	120.3	118.1	119.4	1.7	2.3	1.6	1.8	2.6	0.1	98	89	96	94	0.1	0.8	0.3	0.4	10 ●	10	10	NW 1	W 2	SE 4
M	118.3	118.6	118.8	118.6	0.7	2.1	1.0	1.2	3.2	-1.5	88	82	87	86	0.8	1.4	0.9	1.0	8.6	7.8	7.5	4.4	5.0	4.4

Luty – Février

1	111.6	110.7	110.1	110.8	4.0	7.2	9.3	7.4	9.5	1.1	95	94	93	94	0.4	0.6	0.8	0.6	10 ●	10 ●	10	SW 3	SW 6	SW 7
2	118.1	121.4	123.6	121.0	7.7	8.6	5.9	7.0	10.6	5.5	72	76	92	80	2.9	2.8	0.7	2.1	8	7	6	SW 3	SW 4	SW 1
3	123.8	125.1	125.0	124.6	4.5	6.2	0.1	2.7	7.7	-0.4	98	89	98	95	0.1	1.0	0.2	0.4	10 ●	7	4	SW 1	SE 3	SE 1
4	120.3	119.2	119.3	119.6	2.6	6.5	6.9	5.7	8.2	-0.9	99	93	92	93	0.4	0.7	0.7	0.6	10 ●	10	0	SE 4	SSW 4	SW 3
5	117.7	116.5	114.6	116.3	4.6	9.0	6.8	6.8	10.4	2.8	92	76	86	85	0.7	2.8	1.5	1.7	0	8	7	SW 4	SW 7	SW 4
6	110.3	108.4	108.7	109.1	3.5	7.3	7.3	6.4	8.2	2.3	81	73	87	80	1.4	2.7	1.3	1.8	6	9	10	SW 7	SW 7	SW 7
7	112.9	113.1	114.5	113.5	4.3	7.5	3.8	4.8	8.5	3.1	92	72	88	84	0.7	3.0	0.9	1.5	7	5	1	SW 6	W 9	W 4
8	108.1	102.5	99.4	103.3	4.2	6.4	7.1	6.2	7.6	2.5	90	94	97	94	0.8	0.6	0.3	0.6	10 ●	10 ●	10 ●	SW 6	SW 7	SW 4
9	97.6	97.9	102.3	99.3	6.6	9.3	4.9	6.4	10.0	4.6	91	83	76	83	0.8	2.0	2.1	1.6	10	8	3	SW 6	W 8	W 7
10	104.4	104.5	105.6	104.2	0.2	6.5	4.7	4.0	7.0	-0.3	96	69	97	87	0.3	3.0	0.2	1.2	1	9	9	W 3	SW 1	S 2
11	107.5	110.3	112.0	109.9	3.5	4.8	2.1	3.1	6.0	1.5	93	71	85	83	0.5	2.5	1.0	1.3	10 ●	9	8	NW 5	W 6	WNW 2
12	106.3	102.4	99.4	102.7	2.8	6.0	5.1	4.8	7.0	-0.1	89	85	90	88	0.8	1.5	0.9	1.1	10	10 ●	10	S 5	S 6	SW 7
13	95.1	90.9	80.8	88.9	4.1	8.1	5.8	6.0	8.4	2.8	85	66	92	81	1.2	3.7	0.7	1.9	10	7	10 ●	SW 8	S 9	S 9
14	80.4	81.5	83.1	81.7	6.2	7.5	5.0	5.9	8.1	4.1	88	87	86	87	1.2	1.4	1.2	1.3	7	9	9 ●	SW 7	SW 7	SW 5
15	83.5	82.7	83.1	83.1	3.9	5.9	3.9	4.4	6.5	2.6	85	77	97	86	1.2	2.1	0.3	1.2	10	9	10 ●	SW 4	S 4	C 0
16	89.5	92.2	96.6	92.8	2.8	4.9	2.7	3.5	5.7	0.8	91	67	82	80	0.7	2.9	1.3	1.6	9	6	5	W 4	SW 4	SW 6
17	101.3	102.2	102.9	102.1	0.3	5.1	1.2	2.0	5.8	-0.4	94	66	98	86	0.3	3.0	0.2	1.2	8	8	10 ●	SW 6	SW 5	SW 1
18	102.9	101.7	99.2	101.3	-0.7	6.3	2.9	2.8	6.5	-1.4	94	67	88	83	0.4	3.1	0.9	1.5	3	3	10	SE 4	SE 6	NE 3
19	103.3	107.2	108.8	106.4	0.6	2.2	1.0	1.2	4.5	-0.1	94	82	90	89	0.4	1.3	0.7	0.8	10	9	0	W 4	W 5	SW 3
20	107.6	107.4	104.5	106.5	1.3	3.3	2.4	2.4	3.6	0.3	87	85	95	89	0.9	1.2	0.4	0.8	10	10	10	SW 3	S 2	SE 3
21	104.1	107.3	114.1	108.5	3.5	4.7	1.7	2.9	5.0	1.1	81	85	87	84	1.4	1.2	0.9	1.2	10	10	7	SW 4	SW 4	W 4
22	115.5	114.9	113.1	114.5	-0.3	2.9	0.7	1.0	4.3	-1.3	92	79	90	87	0.5	1.6	0.6	0.9	6	7	10 ✱	SW 3	SW 3	C 0
23	113.6	113.6	112.5	113.2	-0.6	2.9	-0.9	0.1	3.9	-2.3	93	64	93	83	0.4	2.7	0.4	1.2	10	9	0	W 1	WNW 4	E 1
24	105.4	102.2	104.3	104.0	-3.6	2.4	-1.0	-0.8	3.3	-4.9	97	72	85	85	0.2	2.1	0.9	1.1	8	9	0	E 4	E 5	ENE 2
25	107.6	106.9	108.2	107.6	-4.8	2.3	-0.6	-0.9	3.4	-7.1	98	59	83	80	0.1	2.9	1.0	1.3	2	5	4	E 2	SE 6	E 1
26	114.6	116.4	118.3	116.4	-7.4	3.1	-2.3	-2.2	3.6	-7.9	90	51	89	77	0.3	3.7	0.6	1.5	0	1	0	E 1	SE 5	SE 2
27	119.8	121.8	125.1	122.2	-0.9	1.7	0.6	0.5	1.8	-3.7	83	69	96	83	1.0	2.1	0.3	1.1	10	10	10 ✱	SE 3	SE 2	W 2
28	130.0	133.8	137.2	133.7	0.9	1.3	0.1	0.6	3.4	-0.9	88	92	85	88	0.7	0.5	1.0	0.7	10	9	9	ENE 3	N 4	N 2
29																								
30																								
31																								
M	107.6	107.7	108.0	107.8	1.9	5.4	3.1	3.4	6.4	0.1	90	77	90	86	0.7	2.1	0.8	1.2	7.7	8.0	6.5	4.1	5.1	3.4

Szczecin – Dąbie

H_s – 1 m H_b = 6.9 m h_w = 21.5 m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	8	–	= 13⁰⁰–24
2	5	.	8	–	= 0⁰⁰–24
3	5	.	7	–	= 0⁰⁰–24
4	6	0.9	4	–	•⁰ 18¹⁰ 19⁴⁵, = 0⁰⁰–24
5	6	7.0	pz.	–	•⁰ 1⁴⁰–2¹⁵ •⁰ 5³⁵–10³⁰ 13⁴⁰ 18¹⁰–20, 21³⁰–24, por. wiatru do 12 m/sek 7³⁰–8⁴⁰, = 0⁰⁰–24
6	8	0.3	.	–	•⁰ 0⁰⁰–1⁴⁰ ▽⁰ 7³⁰–40 •⁰ 22¹⁵ 23³⁰
7	8	.	.	–	por. wiatru do 15 m/sek 0⁰⁰–15²⁰
8	6	0.0	.	.	•⁰ 9⁴⁵–11¹⁵ 17³⁰–19³⁰ •⁰–20³⁰ •⁰ 21⁴⁰–23¹⁵, = 7³⁵–14³⁰
9	7	0.4	.	–	•⁰ 4³⁰–5²⁰, = 3⁰⁰–11³⁰
10	7	0.6	.	–	•⁰ 0¹⁰–40 ▽⁰ 13²⁰–35
11	8	0.6	.	–	
12	6	2.1	.	–	*⁰ 2⁴⁵–5²⁵ ✱⁰–7³⁵ •⁰–9¹⁰ 10³⁵–11¹⁵ 13¹⁵ 14⁴⁵ 17³⁰ ✱⁰–19²⁵, por. wiatru 12 m/sek 12³⁰–17³⁰, = 9¹⁰–24
13	6	5.7	.	–	•⁰ 8¹⁰ 17³⁰ ✱⁰–20²⁰, 22⁴⁰–23³⁰ *⁰ 24, = 0⁰⁰–21³⁰
14	8	.	1	–	*⁰ 0⁰⁰–3²⁰
15	7	0.0	.	–	
16	8	0.0	.	–	*⁰ 3⁴⁰ 5⁰⁰ 6²⁰ 8²⁰, = 0³⁰–5⁰⁰ 8²⁰–10³⁵, 19³⁰–21³⁰
17	2	.	.	–	= 7²⁰–10¹⁰ ≡¹– 15²⁰ =– 19²⁰ ≡⁰–24
18	6	.	.	–	≡⁰ 0⁰⁰–9³⁰ ≡–24
19	6	0.4	.	–	•⁰ 7⁴⁰–9⁰⁰ 10¹⁵ 17²³–24, = 0⁰⁰–2⁰⁰, 6³⁰–24
20	7	0.0	.	–	•⁰ 0⁰⁰–3³⁵ 6⁰⁵ 7³⁰ 9³⁰ 12³⁰ por. wiatru 14 m/sek 20³⁰–23³⁰ ≫–24 (por. 17 m/sek), = 0⁰⁰–12³⁰
21	7	.	.	–	≫ 0⁰⁰–30 (por. 17 m/sek), por. wiatru 12 m/sek –3¹⁵ ≫–3⁴⁵ (por. 17 m/sek), por. wiatru do 14 m/sek –18²⁰, = 6³⁰ 9³⁰ 13³⁰ 24
22	6	.	.	–	= 0⁰⁰–24
23	6	.	.	–	= 0⁰⁰–13³⁰ ∞–16⁴⁰ =–24
24	7	0.4	.	–	= 0⁰⁰–2³⁰, 14³⁰–24
25	4	.	1	–	*⁰ 0³⁰ 2¹⁵–5³⁰, = 0⁰⁰–24
26	6	4.0	.	–	•⁰ 21⁴⁰–24, = 0⁰⁰–14³⁰
27	8	0.6	.	–	•⁰ 0⁰⁰–3¹⁰ •⁰–5³⁰, = 5³⁰–9⁴⁰ ⊕ 11¹⁵–30
28	6	0.2	.	–	•⁰ 1⁴⁰–4⁰⁰ 5²⁰ ▽⁰ 7⁴²–51 •⁰ 8¹³ 9²⁰, = 9²⁰–13²⁵
29	5	.	.	–	= 7³⁰–21³⁰
30	6	0.7	.	–	•⁰ 18¹⁰–20⁴⁰, = 7¹⁵–20⁵⁰ ≡⁰–24
31	7	3.4	.	–	✱⁰ 0⁵⁰–2⁴⁰ •⁰ 5⁴⁵–7³⁰, 9¹⁵–35, 10⁰⁸–40 11¹⁰ •⁰ 22⁰⁵ 24, ≡⁰ 0⁰⁰–50 =–4⁴⁵ ≡⁰–5⁴⁵ =–7³⁰ ≡⁰–8²⁵
Σ	–	27.5	–	–	UWAGI. [31.I: =–12¹⁵, 20³⁰–24

Luty – Février

1	6	2.3	.	–	•⁰ 0⁰⁰–30–1⁴⁰, 5⁰⁵–19³⁰, = 0⁰⁰–24
2	8	0.1	.	–	= 0⁰⁰–2³⁰
3	7	1.6	.	–	•⁰ 3⁴⁰–11¹⁰, = 4⁵⁰–12³⁰
4	6	0.7	.	–	•⁰ 5⁵⁰–9¹⁰, = 9¹⁰–24
5	6	.	.	–	= 0⁰⁰–24
6	7	0.0	.	–	•⁰ 17⁴⁰–18³⁰, = 0⁰⁰–5³⁰, 19³⁰–24
7	7	0.0	.	–	= 0⁰⁰–4³⁰
8	6	5.2	.	–	•⁰ 6⁴⁰–9³⁰ 10³⁰–18¹⁵ 20³⁰–21¹⁵, = 18¹⁵–24
9	7	.	.	–	por. wiatru 17 m/sek 12⁴⁵–16¹⁵, = 0⁰⁰–6¹⁵, ▽ 18⁴⁵–19²⁰
10	7	0.6	.	–	▽⁰ 16³⁵–40 •⁰ 22¹⁰–24, = 8²⁰–10²⁰, 16⁴⁰–24, ⌴ 5⁰⁰–8⁰⁰
11	8	0.1	.	–	•⁰ 0⁰⁰ 3²⁰ 6³⁰ 7⁴⁰, = 0⁰⁰–8³⁰
12	6	0.3	.	–	•⁰ 8⁴⁰ 9²⁵ 10³⁷ 13¹⁰ 14⁴² 15³⁰–16⁵², 17²⁵ 18⁴⁰–20⁴⁵, = 8³⁰–10¹⁵, ▽ 22⁰⁰–24
13	7	5.4	.	–	•⁰ 6³⁵ 7³⁵, 16⁴⁵–24, ▽ 0⁰⁰–3⁰⁰
14	7	1.9	.	–	•⁰ 0⁰⁰–30, 1³⁰–2³⁰ ▽⁰ 10³⁵–40 •⁰ 13²⁰ 14⁴⁰ ▽⁰ 15⁵⁰–16¹⁰, 20⁵⁵–21⁰⁴
15	7	0.3	.	–	•⁰ 2²⁵–4³⁰ 5⁴⁵ ▽⁰ 14²⁰–40 •⁰ 17⁴⁵–21⁴⁰
16	7	.	.	–	= 1³⁰–8³⁰
17	7	2.4	.	–	•⁰ 16⁰⁴–21¹⁵, = 3³⁰–12³⁰
18	7	.	.	–	= 1³⁰–9²⁰
19	6	.	.	–	= 4³⁰–13³⁰ 17²⁰–24
20	7	0.7	.	–	•⁰ 13¹⁵–18³⁵, = 7¹⁵–12⁴⁰, 18³⁵–24
21	7	0.0	.	–	•⁰ 9⁴⁰ 10¹⁵, 16⁰³ 18¹⁰, = 0⁰⁰–3³⁰ 7³⁵–9³⁰, 16²⁰–20³⁰
22	6	0.0	.	–	*⁰ 20⁴⁰–21³⁰, = 2³⁰–24, ⌴ 3⁰⁰–9³⁰
23	7	0.2	.	–	✱⛹⁰ 11⁵³–12⁰⁸ ▽ 14⁴⁰–46 ⛹⁰ 16⁰³–12 ✱⛹⁰ 16³³–17⁰⁵, = 0⁰⁰–12⁰⁸, ⌴ 21³⁰–24
24	7	.	.	–	= 6³⁰–8³⁰, ⌴ 0⁰⁰–6³⁰, ⊕ 8³⁰–9¹⁵, 13⁴⁵–16³⁵
25	7	.	.	–	= 6¹⁵–11²⁰, ⌴ 3⁰⁰–6¹⁵
26	8	.	.	–	= 1⁰⁰–10³⁰
27	7	1.0	.	–	▽⁰ 18⁴⁰–19³⁰ *¹–20¹⁵ *⁰–22¹⁰, = 15³⁰–24
28	6	0.0	.	–	•⁰ 2³⁵–3⁴⁵, 8³⁰–9⁴⁵ △–10²⁰ *⁰ 12¹¹–47 ⛹ 16¹²–18, = 0⁰⁰–3⁴⁵, 6³⁰–12⁵⁰
29					
30					
31					
Σ	–	23.0	–	–	UWAGI.

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$

Marzec – Mars 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	137.7	137.4	135.7	136.9	−3.3	2.7	−3.0	−1.6	4.0	−5.9	97	58	90	82	0.1	3.1	0.5	1.2	0	4	0	C 0	NE 2	C 0
2	133.2	131.5	128.3	131.0	−8.2	4.1	−2.4	−2.2	5.2	−6.7	95	55	87	79	0.2	3.7	0.7	1.5	0	0	0	SW 2	W 3	W 1
3	124.6	122.1	117.3	121.3	−3.5	5.5	1.4	1.2	7.5	−6.4	97	43	63	68	0.1	5.1	2.5	2.6	7	9	0	W 1	SW 1	SW 1
4	111.3	109.5	110.6	110.5	1.2	5.5	2.2	2.8	5.6	−0.7	77	71	78	75	1.5	2.6	1.6	1.9	10	10	0	SW 4	W 5	NW 5
5	113.2	114.2	114.7	114.0	−2.0	6.3	−2.0	0.1	6.8	−2.5	96	55	89	80	0.2	4.3	0.6	1.7	1	3	0	W 2	W 1	C 0
6	113.7	112.7	111.4	112.6	−6.2	6.4	−0.2	0.0	7.5	−7.4	97	48	76	74	0.1	5.0	1.4	2.2	1	0	0	E 1	SE 4	E 1
7	111.3	111.3	112.3	111.6	−2.4	5.6	−0.1	0.8	6.2	−3.0	85	52	76	71	0.8	4.4	1.5	2.2	3	7	5	E 4	SE 12	SE 7
8	113.6	115.1	119.0	115.9	−2.3	4.1	−0.4	0.2	5.7	−4.0	80	44	72	65	1.0	4.6	1.7	2.4	7	2	0	SE 7	SE 9	SE 6
9	123.7	126.4	128.9	126.3	−3.8	3.7	−0.4	−0.2	5.0	−4.3	85	52	70	69	0.7	3.8	1.8	2.1	0	0	0	ESE 5	SE 9	SE 3
10	130.8	131.4	131.1	131.1	−3.0	6.8	1.3	1.6	8.2	−3.5	90	45	68	68	0.5	5.5	2.1	2.7	0	0	0	E 4	SE 5	E 2
11	130.4	129.6	126.3	128.8	−1.0	11.3	7.1	6.1	12.5	−4.5	77	28	45	50	1.3	9.7	5.5	5.5	0	6	4	SE 3	SE 7	SSE 6
12	122.8	120.5	118.6	120.7	−0.5	11.9	2.7	4.2	15.1	−2.1	92	38	74	68	0.5	8.7	1.9	3.7	9	1	0	C 0	SW 2	W 1
13	118.1	117.1	112.9	116.0	−2.2	15.1	9.9	8.2	17.1	−2.9	91	39	54	61	0.5	10.6	5.7	5.6	4	6	0	C 0	W 4	W 4
14	107.6	107.1	107.7	107.5	6.7	13.3	9.2	9.6	13.6	5.3	78	54	63	65	2.2	7.1	4.2	4.5	4	7	10	SW 5	W 12	W 10
15	110.0	105.8	102.5	106.1	6.9	8.3	5.7	6.6	10.0	5.2	78	96	94	89	2.2	0.5	0.6	1.1	7	10 ●	10 ●	W 5	W 8	NNW 7
16	106.9	112.4	116.5	111.9	1.7	1.1	−2.8	−0.7	5.9	−3.1	92	62	73	76	0.5	2.5	1.3	1.4	9	8	10	NW 4	NE 4	E 4
17	111.4	106.8	97.3	105.2	−3.4	−1.7	4.3	0.9	4.4	−4.4	92	96	98	95	0.4	0.2	0.1	0.2	10 ✳	10 ●	10 ●	SE 7	SE 12	SW 4
18	91.5	93.4	100.2	95.0	8.3	9.7	6.5	7.8	10.5	4.3	93	78	78	83	0.8	2.6	2.2	1.9	9	10 ●	9	W 6	W 9	WNW 8
19	105.5	105.9	106.7	106.0	5.4	7.3	6.1	6.2	8.5	5.0	91	83	100	91	0.9	1.7	0.0	0.9	9	10 ●	10	W 4	SW 4	C 0
20	106.6	103.5	100.6	103.6	6.6	12.1	10.2	9.8	12.7	5.3	100	89	80	90	0.0	1.5	2.5	1.3	10	10	3	SE 4	SW 7	SW 6
21	106.0	108.3	109.4	107.9	6.5	10.0	7.7	8.0	11.0	5.4	90	69	76	78	1.0	3.8	2.5	2.4	2	9	9	WSW 6	SW 9	SW 3
22	113.2	115.6	117.2	115.3	2.6	10.3	2.6	4.5	11.2	2.1	96	51	89	79	0.3	6.1	0.8	2.4	2	6	0	SW 4	W 5	C 0
23	118.0	118.3	121.0	119.1	−1.0	11.9	3.3	4.4	12.0	−3.4	91	46	88	75	0.5	7.5	0.9	3.0	3	3	6	C 0	E 5	E 8
24	122.9	121.9	120.9	121.9	−0.9	5.1	3.0	2.6	6.0	−1.7	77	52	69	66	1.3	4.2	2.4	2.6	6	10	10	E 9	ESE12	SE 12
25	119.4	119.1	119.6	119.4	2.2	7.3	5.4	5.1	9.0	0.7	77	70	86	78	1.7	3.0	1.3	2.0	9	5	4	SE 12	SE 10	SE 5
26	118.2	116.0	115.9	116.7	3.9	14.3	6.5	7.8	16.0	3.4	97	57	90	81	0.3	7.0	1.0	2.8	8	6	0	SE 5	SE 6	S 4
27	116.3	116.4	114.5	115.7	6.7	14.7	12.4	11.6	17.3	5.1	60	53	54	56	4.0	7.8	6.6	6.1	3	9	6	S 5	S 6	S 9
28	111.3	112.4	112.7	112.1	7.4	11.9	7.9	8.8	14.3	5.9	94	68	83	82	0.6	4.4	1.7	2.2	10	5	10	SW 8	SW 3	NW 3
29	113.4	115.1	116.5	115.0	5.3	7.6	4.1	5.3	8.3	3.5	98	82	98	93	0.1	1.9	0.2	0.7	10 ●	10	10 ●	C 0	NNE 6	N 6
30	118.7	119.6	121.8	120.0	5.3	11.9	4.1	6.4	12.7	3.1	96	75	98	90	0.1	3.5	0.2	1.3	10	8	10	NNE 6	NE 6	NNE 5
31	121.4	120.9	122.9	121.7	2.6	10.8	4.9	5.8	14.7	2.2	100	78	100	93	0.0	3.0	0.0	1.0	10	1	10	NNE 5	N 4	WNW 2
M	116.2	116.0	115.8	116.0	1.1	8.2	3.8	4.2	9.8	−0.4	89	61	79	76	0.8	4.5	1.8	2.4	5.6	6.0	4.7	4.1	6.2	4.3

Kwiecień – Avril

1	123.0	120.5	119.3	120.9	2.4	15.7	8.9	9.0	18.4	1.9	100	55	75	77	0.0	8.1	2.9	3.7	10 ≡	1	0	NNE 3	E 2	NE 4
2	118.7	117.9	120.0	118.9	4.7	18.1	12.1	11.8	18.7	0.6	95	38	77	70	0.4	13.0	3.2	5.5	8	2	10 ●	E 3	E 8	S 3
3	123.2	125.4	127.0	125.2	7.5	16.9	9.0	10.6	19.3	6.7	91	51	66	76	0.9	9.4	1.6	4.0	9	8	4	E 1	C 0	NE 1
4	129.1	129.0	128.4	128.8	4.7	19.5	9.9	11.0	20.9	1.5	98	49	77	75	0.1	11.5	2.8	4.8	0	1	0	C 0	NE 2	NE 1
5	126.2	123.0	117.1	122.1	4.7	20.9	15.1	14.0	21.8	1.4	89	33	49	57	0.9	16.5	8.8	8.7	0	1	3	C 0	SW 4	SW 3
6	111.7	111.1	111.6	111.5	7.3	10.3	6.2	7.5	15.3	4.3	79	81	88	83	2.2	2.4	1.2	1.9	9	10	3	W 1	N 7	N 1
7	112.1	115.2	121.8	116.4	5.5	6.3	2.6	4.2	9.8	2.1	86	67	79	77	1.2	3.1	1.6	2.0	2	9	0	N 4	NE 8	NNE 7
8	122.7	119.7	117.0	119.8	2.7	7.9	4.4	4.6	10.0	0.8	67	45	69	60	2.4	5.8	2.6	3.6	0	6	3	N 6	N 4	NNW 2
9	114.1	112.7	112.2	113.0	2.5	10.3	1.7	4.0	11.6	0.4	91	57	80	76	0.6	5.4	1.4	2.5	10	8	4	W 1	NE 5	SE 2
10	105.6	100.3	95.6	100.5	2.5	11.3	7.1	7.0	12.3	−3.1	72	54	73	66	2.1	6.2	2.8	3.7	9	2	9	SW 5	NW 8	W 4
11	94.2	97.4	103.7	98.4	2.6	3.6	1.3	2.2	7.3	0.5	79	81	89	83	1.6	1.5	0.8	1.3	10 ●	10	10 ⁂	W 5	NNW 5	N 1
12	107.9	109.9	111.3	109.7	0.7	3.3	−0.5	0.8	4.8	−1.5	86	64	73	74	0.9	2.7	1.6	1.7	6	7	9	WNW 2	NW 4	E 1
13	113.1	114.9	117.0	115.0	0.0	3.1	0.0	0.8	6.4	−1.7	86	61	86	78	0.9	3.0	0.9	1.6	6	8	0	E 1	N 4	N 1
14	117.2	117.7	119.5	118.1	−0.6	3.9	0.9	1.3	6.3	−2.4	85	87	75	82	0.9	1.1	1.6	1.2	8	7	0	SW 4	W 2	N 5
15	121.5	121.2	122.4	121.7	−1.4	7.5	3.1	3.1	9.7	−6.6	90	37	76	68	0.5	6.5	1.8	2.9	0	9	4	W 3	W 6	NE 2
16	119.2	117.7	118.1	118.3	3.5	12.1	8.3	8.0	12.5	−0.1	91	62	94	82	0.6	5.4	0.7	2.2	10 ●	10	10 ●	W 4	W 8	W 2
17	119.8	121.5	122.1	121.1	6.3	7.1	5.7	6.2	8.5	5.2	86	83	80	83	1.2	1.8	1.9	1.6	10	10	10	WNW 5	N 5	N 3
18	121.4	119.6	117.5	119.5	2.6	8.2	2.9	4.2	9.8	2.1	86	59	84	76	1.1	4.4	1.2	2.2	10	4	0	E 3	NNE 5	E 1
19	112.5	111.0	113.6	112.4	3.7	6.0	7.3	6.1	7.5	−2.6	88	92	96	92	1.0	0.8	0.4	0.7	10	10 ●	10 ●	SE 3	SE 2	NW 4
20	119.3	122.0	125.3	122.2	4.1	10.0	4.1	5.6	10.3	2.1	92	68	87	82	0.7	3.9	1.1	1.9	10	9	0	WNW 4	NNW 4	NE 2
21	128.3	128.7	129.8	128.9	3.4	8.6	4.0	5.0	9.0	−1.6	83	60	87	77	1.3	4.5	1.1	2.3	9	9	0	E 4	N 3	N 5
22	131.0	131.2	130.9	131.0	3.9	8.1	3.7	4.8	9.0	2.1	92	76	98	89	0.7	2.5	0.2	1.1	10	9	1	W 1	N 3	N 3
23	130.6	129.9	130.1	130.2	3.2	10.2	5.9	6.3	12.0	1.7	98	72	92	87	0.2	3.4	0.7	1.4	10	3	0	SE 2	NE 2	N 4
24	130.7	129.9	129.2	129.9	1.1	11.4	4.4	5.3	11.9	−0.2	100	60	84	81	0.0	5.5	1.4	2.3	10 ≡	3	4	NE 3	N 5	N 5
25	127.0	126.4	125.2	126.2	5.3	6.7	4.2	5.1	7.5	3.2	86	81	93	87	1.3	1.9	0.5	1.2	10	10 ●	10	NE 7	NNE 6	NNE 7
26	123.6	122.6	121.7	122.6	4.7	10.5	7.2	7.4	12.0	3.6	97	80	87	88	0.2	2.6	1.4	1.4	10	9	6	NE 4	NNE 4	NNE 4
27	119.0	116.0	113.6	116.2	5.9	18.9	10.4	11.4	19.6	3.5	94	58	93	82	0.6	9.2	0.8	3.5	9	7	6	NNE 3	N 4	N 4
28	111.2	108.6	107.8	109.2	8.8	17.9	10.3	11.8	20.5	7.4	100	74	92	89	0.0	5.4	0.9	2.1	10	1	0	E 2	NE 3	N 2
29	109.2	109.6	111.6	110.1	9.4	19.4	10.1	12.2	20.9	6.3	100	84	91	85	0.0	8.2	1.2	3.1	10	3	3	W 2	W 5	N 2
30	110.7	110.3	113.7	111.6	7.7	11.6	8.2	8.9	12.9	3.0	100	75	56	77	0.0	3.4	4.9	2.8	10 ≡	9	0	E 1	NE 4	NW 6
31																								
M	118.5	118.0	118.5	118.3	4.0	10.8	6.0	6.7	12.6	1.4	90	64	82	79	0.8	5.3	1.8	2.6	7.8	6.6	4.0	2.9	4.4	3.1

Szczecin – Dąbie

$H_s = 1\ m$ $H_b = 6{,}9\ m$ $h_w = 21{,}5\ m$

Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 6³⁰–9³⁰, ⌴ 20⁰⁰–6³⁰
2	7	.	.	–	
3	7	.	.	–	= 6³⁰–12³⁰
4	6	0.0	.	–	△° 7⁰⁵–12 ●° 9⁴² 10²⁰, 16⁴⁰ 17¹⁰; = 5³⁰–20¹⁵
5	7	.	.	–	⌴ 2⁰⁰–9²⁰
6	8	.	.	–	= 5¹⁰–6³⁰ ⌴ 1⁰⁰–5¹⁰
7	8	.	.	–	⩻ 10³⁰–16³⁰, 22³⁰–24; ⊖ 19³⁰–21³⁰
8	7	.	.	–	⩻ 0⁰⁰–3⁰
9	8	.	.	–	
10	7	.	.	–	
11	7	.	.	–	
12	7	.	.	–	= 5¹⁵–9³⁰, 19³⁰–24
13	6	.	.	–	= 0⁰⁰–10³⁰ ∞–24
14	7	.	.	–	por. wiatru do 15 m/sek 12⁰⁰–5⁰ ⩻–22³⁰ ∞ 0⁰⁰–2³⁰ = –6³⁰ ∞–10⁰⁰ = –11³⁰
15	6	9.1	.	–	●° 9⁴⁵ 10³⁰–13¹⁵, 16¹⁵ 18¹⁵–23¹⁵
16	8	0.2	.	–	
17	6	9.1	1	–	✳° 0²⁵–7¹³ ✳¹–7³⁷ ✳°–8⁴⁶ ✳¹–9⁵⁰ ●°–14⁴⁰ ●°–15⁴⁰ 16⁵⁰–17²⁰ ●°–24; ⩻ 7³⁰–8³⁵, 10³⁰–13²⁰
18	8	2.7	.	–	●° 0⁰⁰–4⁰ 4¹⁰–5²⁰ ▽ 12⁴⁰–13⁰⁵ 13⁴⁰–14⁰² 15⁰⁶–25 16¹⁰–23 16³⁵–5⁰ ●° 21²⁰ 22⁴⁵, = 0⁴⁰–4¹⁰
19	7	3.1	.	–	▽ 7⁰⁵–20 ●° 12⁴⁵–19²⁰ ●° 22⁴⁵–23³⁰ ●°–24 = 19²⁰–24
20	6	1.8	.	–	●° 0⁰⁰–3⁰ 8¹⁰–30, 10³⁵ 11²⁰ ▽ 22⁴⁵–23²³; ◹° 22⁴⁵–23¹⁸ W–E; = 0⁰⁰–17¹⁰
21	7	0.0	.	–	▽ 21²⁰–24
22	8	.	.	–	
23	7	.	.	–	⌴ 0⁰⁰–7³⁰
24	7	1.1	.	–	●° 16⁰⁴–19¹⁵, 19²⁵ 20²⁰, 22⁴⁰–23¹⁵, por. wiatru do 14 m/sek 3³⁰–7³⁰ ⩻–24 (por. wiatru 17 m/sek)
25	7	1.2	.	–	⩻ 0⁰⁰–1⁴⁵ (por. 17 m/sek) por. wiatru do 14 m/sek –3²⁰ ⩻–13²⁰ (por. do 17 m/sek), 15¹⁰–17¹⁰ (por. do 16 m/sek)
26	7	.	.	–	●¹ 1⁵⁰–6²⁰; = 6²⁰–10³⁰
27	7	2.9	.	–	
28	8	0.3	.	–	●° 3³⁰–4⁰⁰ ●¹–5¹⁰ ●°–6⁴⁰
29	7	6.1	.	–	●° 5⁴⁸–7⁴⁰, 13²⁰ 17³⁰–22⁵⁰ 23¹⁰; = 5³⁰–10²⁰
30	7	0.0	.	–	●° 7¹⁵–9¹⁰ = 0⁰⁰–10³⁰, 18⁰⁰–24
31	7	.	.	–	= 0⁰⁰–5⁵⁵ ≡°–8¹⁵ =–11³⁰, 18³⁰–20⁴⁰ ≡°–21³⁰ ≡¹–24
Σ	–	37.6	–	–	UWAGI

Kwiecień – Avril

1	8	.	.	–	≡¹ 0⁰⁰–8⁵⁰ ≡°–9⁴⁰ =–10³⁰
2	8	0.0	.	–	●° 19¹⁰ 22¹⁵; ⌴ 5⁰⁰–6³⁰
3	7	.	.	–	⌓ 20⁰⁰–24
4	6	.	.	–	= 1³⁰–10³⁰ ∞–13²⁰; ⌓ 0⁰⁰–1³⁰
5	8	.	.	–	⌓ 1⁰⁰–7³⁰
6	7	0.0	.	–	●° 16¹⁰–5⁰ ⌓ 3³⁰–7³⁰ ⊕ 9⁰⁰–14¹⁵
7	8	0.3	.	–	▽ 8⁴³–54 12⁴⁹–57, 13⁰⁸–12 ▲° ▽ 14²⁶–34, 14⁵⁹–15⁰⁰, por. wiatru do 14 m/sek 14⁵⁰–19³⁰
8	8	.	.	–	⌴ 4⁰⁰–6³⁰
9	8	.	.	–	= 7²⁰–10³⁰ ⌓ 20⁰⁰–22⁰⁰ ⌴ –24
10	7	0.0	.	–	⌴ 0⁰⁰–2⁰⁰
11	7	0.7	.	–	●° 6⁴⁵ 8⁰⁰ ▽ 12²⁷–35, 13⁰²–15 ⧖° 18⁵⁵–19¹² 20⁴⁵–21³⁰
12	8	0.0	.	–	✳° 0¹⁵–2⁴⁵ 3³⁰ 6³⁰ ✳ 10¹⁵–32 11²²–40 ⧖° 13³⁵–47, 14¹⁰–25 21³⁵–22¹⁰, = 4⁰⁰–6⁴⁵
13	8	0.0	.	–	✳ ▽ 9³²–44, 11⁰⁶–12 11⁵⁷–12⁰⁰, 12⁵⁴–13⁰¹
14	8	1.5	.	–	✳ 10¹⁰–18, 11³⁵–45, 12²⁰–40, 13³⁷–14³⁵, ⌴ 1⁰⁰–7³⁰
15	8	2.0	.	–	⌴ 0⁰⁰–7³⁰
16	7	2.5	.	–	●° 2³⁵–3³⁰ ✳°–4³⁰ ●°–7⁴⁰, 13⁰⁶ 14²⁵, 16⁴⁴–23³⁵; = 7⁴⁰–10⁴⁰
17	7	.	.	–	
18	8	.	.	–	= 23³⁰–24 ⌓ 20⁰⁰–23³⁰
19	6	3.0	.	–	●° 7⁴⁵–14⁴⁵ 17³⁶–21¹⁰; = 0⁰⁰–5³⁰, 15³⁰–21¹⁰
20	7	.	.	–	⌓ 20³⁰–23⁰⁰ ⌴ –24
21	8	.	.	–	= 3³⁰–5³⁰ ⌴ 0⁰⁰–3³⁰ ⌓ 22⁰⁰–24
22	7	0.0	.	–	●° 8¹⁵–9⁴⁰ = 5¹⁰–9⁵⁰ 21³⁰–24; ⌓ 0⁰⁰–5³⁰, 19³⁰–21³⁰
23	8	.	.	–	= 0⁰⁰–3⁵ ≡°–5⁴⁵ =–9³⁰; ⌓ 20⁰⁰–24
24	7	.	.	–	= 3³⁰–4⁴⁵ ≡¹–7⁴⁰ ≡°–8¹⁰ =–8⁴⁵; ⌓ 0⁰⁰–3³⁰
25	7	2.5	.	–	●° 8⁴⁵–11¹⁴, 12⁰⁷ 13⁵⁰, 17²⁵–20⁴⁰; 23¹⁰–24
26	7	.	.	–	●° 0⁰⁰–3⁰ 3³⁵–5⁴⁵ = 5⁴⁵–9³⁰; ⌓ 20⁰⁰–24
27	8	0.0	.	–	▽ 16³⁰–40 (K) 16²⁵–45 NNE; ⌓ 0⁰⁰–8⁰⁰
28	7	0.2	.	–	= 0³⁰–6²⁰ ≡°–6⁵⁰ =–9⁰⁵ ≡°–10⁰⁷ =–11³⁰, 18²⁵–24
29	7	.	.	–	●° 2⁴²–3¹⁰ ▽ 3¹⁸–40 3⁵⁵–4⁰⁷ ◹° 3¹⁸–30–48 SW–NE; = 0⁰⁰–8²⁰, 19³⁰–24
30	7	.	.	–	por. wiatru do 14 m/sek 16³⁰–19³⁰; = 0⁰⁰–10⁰ ≡°–4³⁰ ≡¹–7³⁵ =–11³⁰
31					
Σ	–	12.7	–	–	UWAGI.

Szczecin – Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ Maj – Mai 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	118.0	118.6	118.4	118.3	5.9	10.7	6.9	8.6	12.5	3.2	77	53	62	64	2.1	6.1	4.4	4.2	1	7	10	WNW 3	NE 2	N 4
2	116.5	114.2	112.4	114.4	6.8	13.8	9.7	10.0	14.1	5.4	82	45	80	69	1.8	8.8	2.3	4.3	10	9	6	E 2	SW 5	C 0
3	111.5	110.1	107.0	109.5	9.3	13.7	10.3	10.9	13.8	7.6	87	63	71	74	1.6	5.9	3.6	3.7	9	8	9	NW 2	W 6	SW 5
4	107.1	108.7	110.5	108.8	6.2	9.3	4.2	6.0	10.8	3.8	60	37	72	56	3.8	7.4	2.2	4.5	9	9	2	WNW 8	W 9	W 6
5	108.9	108.3	107.9	108.4	4.5	7.6	4.4	5.2	10.5	2.0	71	57	71	66	2.4	4.4	2.5	3.1	8	7	4	W 7	W 7	SW 2
6	108.7	108.4	108.6	108.6	2.7	6.5	4.7	4.6	9.0	−0.3	93	76	85	85	0.5	2.3	1.2	1.3	6	6	9 ●	W 3	C 0	NNW 4
7	107.8	108.4	109.6	108.6	4.3	6.5	5.1	5.2	10.2	2.1	97	75	83	85	0.3	2.5	1.5	1.4	4	9 ●	10	NE 1	NNE 1	NE 5
8	110.0	109.8	109.9	109.9	3.9	6.5	2.4	3.8	7.6	2.0	82	71	77	77	1.5	2.9	1.7	2.0	10	10	3	NNE 5	N 5	C 0
9	111.8	112.6	113.7	112.7	3.2	11.1	7.7	7.4	13.0	−3.8	84	51	69	68	1.2	6.4	3.2	3.6	4	7	9	C 0	E 1	NE 3
10	113.5	112.8	113.0	113.1	4.9	7.9	6.9	6.6	8.6	4.0	86	74	80	80	1.3	2.8	2.0	2.0	10	10	10	NE 5	N 5	NNW 2
11	113.0	112.1	111.3	112.1	5.6	14.3	9.8	9.9	17.6	4.6	86	48	70	68	1.3	8.4	3.6	4.4	10	2	0	W 2	W 4	SE 4
12	111.9	110.9	112.9	111.9	9.7	23.1	15.1	15.8	23.9	4.7	80	32	75	62	2.3	19.3	4.6	8.7	0	5	9	SE 2	SW 4	SW 1
13	114.7	115.8	115.5	115.3	13.7	17.5	11.3	13.4	21.7	5.3	80	67	96	81	3.2	6.6	0.5	3.4	3	10 ●	9	C 0	SW 4	SE 2
14	117.5	118.2	120.5	118.7	10.7	18.3	11.5	13.0	19.1	8.0	96	61	84	80	0.5	8.1	2.2	3.6	2	7	1	WSW 3	W 4	NW 1
15	121.6	120.4	117.5	119.8	13.1	21.3	13.9	15.6	22.3	3.5	85	44	68	66	2.3	14.2	5.1	7.2	2	1	0	C 0	SSE 5	SE 4
16	115.1	112.4	115.4	114.3	15.1	24.5	13.2	16.5	26.0	10.8	70	43	91	68	5.1	17.5	1.4	8.0	0	8	10 ●R	SE 7	SE 9	WNW 5
17	117.5	119.3	119.0	118.6	11.1	13.5	10.9	11.6	15.9	10.3	92	82	89	88	1.0	2.8	1.4	1.7	10	10	0	NW 3	SW 2	SE 2
18	118.1	116.6	112.9	115.9	13.9	19.5	14.5	15.6	21.6	7.8	82	45	78	68	2.9	12.5	3.6	6.3	0	8	10	SW 1	SE 4	SE 1
19	110.8	108.3	105.8	108.3	13.9	23.5	17.6	18.2	25.2	9.9	72	48	84	68	4.4	15.1	3.2	7.6	0	6	8	SE 6	SE 5	E 1
20	110.4	114.1	117.2	113.9	13.1	13.0	10.1	11.6	18.3	9.7	96	84	75	85	0.6	2.5	3.2	2.1	10 ●	10	4	NNW 3	NNW 4	NW 4
21	118.5	117.5	116.7	117.6	8.6	14.1	11.3	11.3	15.9	4.7	86	54	70	70	1.6	7.4	4.1	4.4	3	4	4	W 2	SE 2	E 2
22	116.4	115.6	116.2	116.1	9.1	15.5	11.8	12.0	16.9	4.0	83	62	78	74	2.0	6.7	3.0	3.9	9	8	8	SE 4	NE 4	NNE 6
23	114.3	112.5	112.0	112.9	10.3	17.5	10.7	12.3	20.3	7.7	90	69	92	84	1.3	6.2	1.0	2.8	9	9	9	NE 2	NNE 5	NNE 7
24	115.0	118.6	124.8	119.5	10.9	14.3	7.7	10.2	15.3	7.2	92	80	77	83	1.0	3.2	2.4	2.2	10	10	4	NE 4	N 7	NE 9
25	127.8	128.2	129.4	128.5	7.8	12.5	6.7	8.4	13.4	4.3	78	55	67	67	2.4	6.6	3.3	4.1	2	4	0	NNE 7	NE 6	NE 9
26	130.4	129.1	128.7	129.4	6.1	11.1	7.1	7.8	12.3	−0.3	77	57	66	67	2.1	5.7	3.5	3.8	2	6	0	NE 4	N 4	NE 4
27	128.3	126.4	125.3	126.7	6.4	11.9	8.1	8.6	12.8	0.0	85	46	67	66	1.4	7.5	3.6	4.2	2	6	6	NE 1	NNE 6	NE 5
28	124.5	123.2	122.4	123.4	6.2	12.3	7.8	8.5	13.4	2.3	88	43	67	66	1.2	8.2	3.5	4.3	7	8	1	NE 3	NE 3	NE 5
29	122.3	121.6	120.8	121.6	6.3	14.5	9.7	10.0	16.1	−0.5	82	50	68	67	1.7	8.3	3.8	4.6	9	4	2	E 1	E 3	NE 1
30	121.5	120.5	118.8	120.3	10.7	17.7	12.1	13.2	19.5	2.0	71	43	72	62	3.7	11.4	4.0	6.4	4	4	0	E 1	C 0	SE 3
31	117.5	115.5	114.7	116.0	12.6	21.6	13.1	15.1	22.7	4.8	74	36	86	65	3.7	16.6	2.1	7.5	0	5	2	C 0	SW 3	NE 3
M	116.2	115.8	115.8	115.9	8.6	14.4	9.6	10.6	16.1	4.4	83	56	76	72	2.0	7.9	2.8	4.2	5.3	7.0	5.1	3.0	4.1	3.5

Czerwiec – Juin

1	115.7	115.9	115.1	115.6	11.1	17.2	13.5	13.8	19.4	6.8	80	54	80	71	2.6	9.0	3.2	4.9	6	8	0	NW 2	W 6	WNW 1
2	117.2	119.2	119.0	118.5	11.5	16.5	14.1	14.0	18.7	7.8	85	70	88	81	2.0	5.7	2.0	3.2	8	10	1	NW 3	WNW 4	W 1
3	119.5	118.1	114.3	117.3	15.1	19.2	14.9	16.0	22.3	10.1	84	74	91	83	2.8	5.8	1.5	3.4	8	10 ●	8	W 2	SW 1	C 0
4	112.5	111.5	108.6	110.9	15.4	22.5	18.1	18.5	23.6	8.2	96	46	76	73	0.8	14.8	5.1	6.9	7	7	10	C 0	NE 4	SW 4
5	106.3	104.3	103.3	104.6	13.3	15.8	12.9	13.7	18.5	10.3	91	79	79	83	1.4	3.7	3.1	2.7	9	9 ▲●	9	W 6	SW 8	W 2
6	105.8	106.9	107.3	106.7	11.0	14.3	13.1	12.9	16.1	9.4	80	69	67	72	2.6	5.1	5.0	4.2	8	4	9	WNW 7	WSW 8	SW 5
7	107.6	107.0	109.1	107.9	13.1	16.6	11.3	13.1	17.0	10.8	72	61	90	74	4.3	7.3	1.3	4.3	6	9	0	WSW 5	W 4	W 1
8	110.8	109.4	108.5	109.6	11.1	21.4	17.4	16.8	24.1	7.6	99	54	74	76	0.2	11.6	5.1	5.6	10 ●	5	7	W 1	SE 6	SE 4
9	106.0	107.8	110.0	107.9	18.4	19.4	16.8	17.8	22.4	13.2	84	81	93	86	3.3	4.2	1.4	3.0	9	10	6	SE 3	WNW 4	E 1
10	111.3	110.2	109.8	110.4	16.1	23.1	18.6	19.1	24.8	8.9	93	52	72	72	1.3	13.5	6.1	7.0	3	6	7	SE 1	E 2	E 2
11	105.3	103.7	109.1	105.4	19.9	28.8	18.6	21.5	30.7	14.1	79	46	89	71	4.9	21.4	2.3	9.5	2	8	10	SE 7	SE 9	W 4
12	121.0	126.0	130.5	125.8	13.4	17.9	13.9	14.8	20.3	12.7	78	58	72	69	3.3	8.7	4.4	5.5	10	6	0	NW 5	NNW 5	NW 3
13	132.6	131.7	130.3	131.5	11.3	16.9	13.7	13.9	18.8	6.8	76	69	83	76	3.3	5.9	2.7	4.0	8	2	1	NW 6	NE 5	NNE 2
14	129.7	129.1	128.5	129.1	14.9	23.8	18.5	18.9	25.3	9.6	84	45	68	66	2.7	16.1	6.8	8.5	2	1	2	C 0	C 0	NE 4
15	129.9	127.2	125.2	127.4	15.4	24.1	17.0	18.4	24.9	7.8	65	36	67	56	6.2	19.2	6.3	10.6	0	0	0	C 0	NE 3	NE 4
16	124.4	122.1	120.0	122.2	16.3	25.7	19.2	20.1	27.3	6.4	59	27	67	51	7.6	24.1	7.4	13.0	0	0	0	E 2	E 4	NE 2
17	119.6	118.3	116.5	118.2	18.0	27.0	20.8	21.6	28.3	11.3	75	43	73	64	5.2	20.4	6.6	10.7	1	2	0	E 2	NE 4	NE 2
18	115.7	113.1	110.9	113.2	20.1	28.7	21.7	23.0	30.0	13.4	61	24	55	47	9.2	30.1	11.8	17.0	0	0	0	E 1	SE 2	NE 1
19	110.6	110.2	110.6	110.5	19.3	26.3	18.1	20.5	26.8	11.7	71	59	82	71	6.4	14.1	3.7	8.1	0	2	0	NE 2	N 5	NE 4
20	114.3	114.9	117.3	115.5	15.0	23.6	16.7	18.0	24.5	11.4	66	43	61	57	5.7	16.6	7.3	9.9	9	5	0	E 4	NE 4	NE 2
21	116.8	113.5	109.1	113.1	16.7	24.6	18.8	19.6	26.0	5.9	60	38	69	54	7.7	19.3	7.7	11.6	1	4	4	SE 2	W 3	C 0
22	104.6	104.0	104.3	104.3	15.5	18.0	13.7	15.2	18.9	9.8	86	94	94	91	2.4	1.2	0.9	1.5	10	10	10	NE 1	NW 4	NW 5
23	108.0	107.3	110.6	108.6	13.2	20.3	12.9	14.8	20.7	10.1	86	54	88	76	2.1	11.0	1.8	5.0	2	9	5	SW 4	W 5	WNW 1
24	111.0	109.2	105.7	108.6	11.8	16.7	15.1	14.7	18.7	5.9	95	58	71	75	0.6	8.0	5.0	4.5	10	9	10	C 0	S 5	NE 5
25	106.2	111.6	114.6	110.8	10.3	12.4	11.0	11.2	15.3	9.8	100	90	97	96	0.0	1.4	0.3	0.6	10 ●	10	1	N 5	W 3	W 2
26	118.0	119.5	121.2	119.6	11.9	15.9	12.5	13.2	17.3	7.3	82	59	87	76	2.5	7.5	1.9	4.0	0	6	4	W 6	W 6	W 3
27	122.6	124.1	122.3	123.0	11.0	16.5	17.0	15.4	19.3	8.3	89	61	72	74	1.5	7.3	5.4	4.7	6	3	10	W 5	NW 4	SW 4
28	120.0	119.4	120.1	119.8	17.0	26.9	22.5	22.2	28.2	15.3	96	53	63	71	0.8	16.6	10.2	9.2	9	4	2	SW 5	W 8	WNW 1
29	121.6	120.5	118.7	120.3	19.3	29.1	24.6	24.4	30.9	15.2	72	46	68	62	6.2	21.7	9.8	12.6	2	4	1	W 4	W 4	WNW 2
30	119.9	120.1	119.5	119.8	20.9	25.3	22.1	22.6	28.5	17.3	83	67	77	76	4.3	10.8	6.2	7.1	6	9	7(R)	W 1	C 0	N 3
31																								
M	115.5	115.2	115.0	115.2	14.9	21.2	16.6	17.3	22.9	10.1	81	57	77	72	3.5	12.1	4.7	6.8	5.4	5.8	4.1	3.1	4.3	2.5

Szczecin – Dąbie

$H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 21{,}5\,m$

Maj – Mai 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	0.0	.	–	● 16 35 17 15
3	8	0.0	.	–	● 22 10–40 · = 3 30 – 6 30
4	8	0.0	.	–	▽ 7 40–50 15 21–24 17 15–25 · por. wiatru 14 m/sek 8 30–10 15 ≫ 12 30 (por. do 19 m/sek) por. wiatru 14 m/sek – 17 40 ≫ – 18 30 (por. 17 m/sek)
5	8	0.0	.	–	▽ 11 15–18 12 40–43 · por. wiatru 12 m/sek 0 00–4 30 6 30–7 30 por. wiatru 14 m/sek – 10 30 [4.V:] por. wiatru do 14 m/sek – 20 30 por. wiatru 12 m/sek 22 30–24
6	8	3.8	.	–	▽ 10 44–55 11 07–16 12 03–22 20 56–21 05 21 35–22 10
7	8	3.4	.	–	▽ 8 26–52 9 35–10 03 12 18–13 10 16 37–18 40 · = 3 15–7 30
8	8	.	.	–	⌒ 20 30–22 00 ⌴ –24
9	8	.	.	–	≡ 2 45–3 15 = –4 45 ≡ 2–5 15 ≡ 1–5 30 ≡ 0–5 35 = –6 30 · ⌴ 0 00–2 45 · ⊕ 7 40–16 30
10	8	.	.	–	
11	8	.	.	–	⌒ 22 00–24
12	7	.	.	–	⌒ 0 00–8 00
13	7	2.6	.	–	▽ 12 02–05 ● 0 12 39–13 09 ▽ 18 41–19 20 · (K) 0 11 33–12 15 SE-E-NE K 0 18 40–19 00 19 25 SW–NE ≤ 20 30–21 15 · por. wiatru 17 m/sek 18 41–45 ·
14	7	.	.	–	≡ 0 15–2 30 = 6 15–7 25 ≡ 22 20–24 [13.V:] ≡ 2 10–45 = 0–5 20 = –5 45 · ⊕ 13 25–45
15	8	.	.	–	≡ 0 00–2 50 = 0–5 40 = –6 20
16	7	10.4	.	–	▽ 19 35–40 20 38–23 15 ● 0–24 · (K) 19 20–21 30 S-NE (K) 19 30–21 15 K 0–22 05 (K) –22 45 SW–NE; por. wiatru do 14 m/sek 10 30–15 30
17	7	0.0	.	–	● 0 00–35 9 45 10 15 11 40 12 25 · ≡ 23 30–24
18	8	.	.	–	≡ 0 00–2 20 · ⌒ 20 30–24 · ⊕ 16 30–17 35
19	8	12.8	.	–	▽ 23 10–24 · (K) 22 40–23 10 K 1–24 · ⌒ 0 00–8 00
20	7	0.0	.	–	▽ 0 00–35 · 0 55–2 30 · 2 55–4 15 ● 0 4 30–7 10 · K 1 0 00–3 00 (K) –3 50 SW–NE; por. wiatru do 14 m/sek 8 30–9 30
21	8	.	.	–	
22	8	.	.	–	⊕ 17 15–18 20
23	8	3.8	.	–	● 0 17 40 18 00–19 30 · 19 50 · 20 35 · = 4 20–5 45
24	7	0.0	.	–	● 0 9 45–10 15 · por. wiatru do 14 m/sek 13 30–24
25	8	.	.	–	por. wiatru do 12 m/sek 0 00–30
26	8	.	.	–	
27	8	.	.	–	⌒ 2 00–8 00
28	8	.	.	–	⌒ 0 00–8 00
29	8	.	.	–	
30	8	.	.	–	⌒ 20 30–24
31	8	.	.	–	⌒ 0 00–7 30
Σ	–	96.6	–	–	UWAGI:

Czerwiec – Juin

1	8	.	.	–	= 7 10–4 30 · ⌒ 20 30–24
2	7	.	.	–	= 2 15–6 30 · ≡ 22 20–23 30
3	6	0.6	.	–	● 13 40–14 45
4	7	0.3	.	–	= 1 30–2 50 ≡ 1–3 30 ≡ 0–3 45 = –5 15 ≡ 1–6 10 ≡ 0–6 45 = –11 30
5	7	21.7	.	–	● 0 2 35–4 45 · 6 45–7 20 · ▽ 13 50–14 35 ▲ 0 (φ 0,5 mm) 13 58–14 02 ▽ 23 10–20 · K 2 13 55–14 10 14 50 NE; por. wiatru do 15 m/sek [5.V:] 13 55–14 10 · = 4 45–8 30
6	8	0.0	.	–	▽ 3 45–4 10 · 16 41–53
7	8	1.0	.	–	⌒ 21 30–24
8	7	0.0	.	–	● 0 5 50 6 20–7 20 · 9 15 · ⌒ 0 00–5 50
9	7	0.1	.	–	▽ 10 30–35 ● 0 12 10–20 · 12 40–55 · = 22 30–24 · ⌒ 0 00–8 30
10	8	.	.	–	= 0 00–50 ≡ 0–2 45 ≡ 1–6 30 ≡ 0–6 40 = –7 30
11	7	1.4	.	–	▽ 19 20–20 15 · K 1 19 10–20 15–20 25 · = 3 30–6 45 · ⌒ 1 00–3 30
12	8	.	.	–	
13	8	.	.	–	⌒ 0 00–8 30
14	8	.	.	–	≡ 0 15–2 30
15	8	.	.	–	⌒ 2 00–7 30 · 22 00–24
16	9	.	.	–	⌒ 0 00–6 00
17	8	.	.	–	⌒ 0 00–7 30 · 22 00–24
18	8	.	.	–	⌒ 0 00–8 30 · 23 00–24
19	8	.	.	–	⌒ 0 00–6 30
20	9	.	.	–	
21	8	.	.	–	⌒ 0 00–7 30
22	7	0.0	.	–	● 0 9 50 10 15 · 13 05–14 45 · 15 15…35 ▽ 23 10–20
23	8	0.0	.	–	▽ 15 10–30 · ● 18 10–20 · ≡ 22 30–24
24	8	13.9	.	–	≡ 0 00–2 30 = 4 30–10 30
25	7	3.6	.	–	● 0 1 45–2 15 · 1–8 20 · 0–13 50 ▽ 14 10–25 · 15 55–16 07 · 16 50–17 10
26	8	0.0	.	–	▽ 14 20–25 · 19 15–18
27	8	0.0	.	–	
28	7	.	.	–	● 0 2 20–3 15 · 6 45–7 10 · = 7 10–9 30
29	8	.	.	–	
30	8	0.1	.	–	▽ 12 50–13 08 · (K) 21 50–22 45 NW–SE
31					
Σ	–	42.7	–	–	UWAGI:

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$

Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	118.5	115.4	112.7	115.5	20.5	30.2	26.9	26.1	32.4	16.9	79	44	46	56	5.0	23.9	19.3	16.1	2	0	3	SE 6	SE 6	S 9
2	112.4	117.2	119.6	116.4	21.5	23.9	16.6	19.6	26.9	16.3	81	63	83	76	4.8	10.9	3.3	6.3	4	8	0	N 2	N 5	N 2
3	120.3	118.5	115.6	118.1	16.4	24.3	19.9	20.1	26.0	11.7	84	53	63	67	2.8	14.4	8.5	8.6	2	3	9	C >	N 2	E 2
4	112.5	111.4	109.2	111.0	20.7	30.2	26.8	26.1	32.2	16.7	71	50	63	61	7.2	21.3	13.1	13.9	4	2	9	SW 5	SW 4	W 5
5	112.7	113.3	118.2	115.4	23.2	23.9	17.7	20.6	27.7	17.4	80	76	68	75	5.8	7.0	6.4	6.4	9	8	0	NNW 3	NNE 4	NNW 2
6	121.3	120.2	118.9	120.1	15.5	23.7	19.2	19.6	25.0	11.7	76	46	69	65	4.3	15.3	7.0	8.9	0	1	1	W 2	NE 2	NE 4
7	120.0	117.3	113.6	117.0	15.5	26.3	25.6	23.8	31.4	10.8	75	38	58	57	4.4	23.6	13.9	14.0	6	6	10	E 1	E 4	SE 1
8	114.4	113.0	114.1	114.5	21.3	26.0	22.9	23.8	28.9	18.6	86	63	77	75	3.4	13.9	6.4	7.9	2	8	6	W 2	NE 2	NNE 1
9	114.8	114.9	113.9	114.5	16.3	23.4	17.9	19.4	25.0	17.7	92	57	63	77	1.6	12.5	3.4	5.8	9	7	7	C 0	NW 4	NW 1
10	111.6	109.6	108.9	110.0	17.8	23.3	19.8	20.2	24.6	14.6	84	56	78	73	3.2	12.6	5.1	7.0	9	8	10	C 0	NE 1	E 2
11	108.8	110.3	112.6	110.6	15.4	16.5	17.1	17.0	19.8	14.8	100	100	97	99	0.0	0.0	0.6	0.2	10 ●	10 ●	10 ●	NNE 4	N 4	NNE 5
12	112.1	111.7	111.4	111.7	17.2	24.1	19.2	19.9	25.6	16.2	93	65	93	84	1.4	10.6	1.5	4.5	10	7	1	N 2	NNW 2	NW 2
13	112.8	114.0	115.7	114.2	15.4	24.3	20.7	20.3	26.2	14.4	100	64	81	82	0.0	10.9	4.6	5.2	10 ≡	7	4	SE 2	W 2	NE 1
14	114.9	114.6	113.7	114.4	18.7	22.0	16.4	18.4	23.8	15.5	89	81	97	89	2.3	5.1	0.6	2.7	5	9	10	E 1	N 2	C 0
15	111.6	111.3	111.3	111.4	16.3	19.7	16.4	17.2	23.1	15.6	100	80	86	89	0.0	4.5	2.7	2.4	10 ≡	9	2	W 2	W 3	C 0
16	111.2	110.7	110.1	110.7	14.9	22.3	19.1	18.8	23.1	10.3	97	58	77	77	0.5	11.3	5.0	5.6	7	7	10	WSW 12	NE 1	NNW 2
17	108.8	108.8	110.0	109.2	15.8	20.1	17.7	17.8	22.3	13.9	90	67	75	77	1.7	7.8	4.9	4.8	9	10	6	WNW 5	WNW 6	NW 4
18	110.5	109.5	108.2	109.4	15.2	23.0	18.1	18.6	24.4	12.5	91	49	83	74	1.5	13.3	3.5	6.1	5	6	0	W 2	W 4	E 1
19	106.0	104.7	103.6	104.8	17.1	27.1	22.1	22.1	27.7	11.3	84	40	72	65	3.2	21.6	7.5	10.8	0	1	9	C 0	S 4	SE 1
20	101.7	102.0	103.9	102.5	18.6	23.7	17.1	19.1	24.5	14.8	80	71	89	80	4.3	8.4	2.2	5.0	4	9	7	E 1	SW 5	W 1
21	103.1	102.9	103.2	103.1	16.0	16.5	16.3	16.3	18.1	15.1	95	96	95	95	1.0	0.8	1.0	0.9	10	10 ●	10	C 0	W 1	C 0
22	102.8	101.6	103.5	102.6	16.5	21.7	19.8	19.4	23.7	15.2	97	83	90	90	0.6	4.4	2.4	2.5	10 ●	9	10	NW 4	N 5	N 5
23	104.7	105.1	106.8	105.5	18.1	23.9	19.4	20.2	25.2	16.8	92	70	83	82	1.7	8.9	3.8	4.8	9	7	10	NW 1	NNW 6	W 4
24	108.0	108.6	108.6	108.4	15.8	18.2	15.1	16.0	19.5	14.7	81	65	86	77	3.3	7.3	2.5	4.4	10	9	6	NW 5	W 4	W 2
25	108.6	107.9	106.4	107.6	13.0	17.7	14.6	15.0	19.8	11.1	86	55	92	78	2.1	9.2	1.3	4.2	9	9	9	SW 6	W 7	SW 3
26	106.8	106.2	103.8	105.6	12.8	15.1	15.3	14.6	17.9	11.9	88	94	99	94	1.8	1.0	0.2	1.0	10	10	10 ●	W 5	SW 1	SW 5
27	101.5	100.8	101.7	101.3	15.7	17.2	14.5	15.5	19.7	13.8	95	77	94	89	0.9	4.5	0.9	2.1	10 ●	8	6	W 3	W 4	SW 3
28	103.6	104.5	105.9	104.7	12.1	16.6	14.9	15.1	20.3	10.4	93	61	78	78	0.7	8.3	3.6	4.2	2	7	8	SW 3	W 6	W 5
29	106.6	107.7	109.5	107.9	13.8	19.7	16.1	16.4	20.5	11.1	91	62	86	80	1.5	8.6	2.5	4.2	1	7	7	W 4	SW 6	SW 4
30	110.3	113.3	117.8	113.8	15.8	17.9	16.7	16.8	19.9	14.5	96	86	89	92	0.3	2.4	2.2	1.6	10 ●	9	10	W 4	WNW 6	W 3
31	120.9	122.6	122.9	122.1	15.0	16.9	14.9	15.4	18.4	14.5	89	71	92	84	1.8	5.5	1.3	2.9	10	10	1	W 2	W 4	WNW 1
M	110.8	110.8	110.8	110.8	16.8	22.2	18.5	19.0	24.0	14.2	88	66	81	78	2.4	10.0	4.6	5.7	6.7	7.1	6.5	2.5	3.6	2.6

Sierpień – Août

1	123.0	122.7	122.2	122.6	15.1	21.1	16.6	17.4	23.6	11.0	91	64	85	80	1.5	9.1	2.9	4.5	0	4	2	W 3	W 3	WNW 2
2	122.2	122.4	122.8	122.5	14.9	20.2	13.9	15.7	21.1	11.7	67	44	79	70	2.2	13.4	3.4	6.3	2	5	0	WNW 5	NW 7	WNW 3
3	121.3	120.3	120.3	120.6	14.1	20.6	17.3	17.3	22.5	10.6	91	54	71	72	1.5	11.2	5.6	6.1	9	5	2	W 3	NW 3	WNW 3
4	120.3	121.1	121.9	121.1	16.0	20.9	15.8	17.1	22.7	12.7	89	71	94	85	2.0	7.2	1.1	3.4	10	7	2	NW 3	NNW 5	C 0
5	122.8	123.1	122.0	122.6	14.5	23.1	16.8	17.8	24.1	10.3	92	49	82	74	1.3	14.5	3.5	6.4	0	7	1	W 1	C 0	E 2
6	121.8	119.9	116.8	119.5	15.3	24.0	18.9	19.3	25.5	9.3	88	50	80	73	2.1	14.8	4.3	7.1	0	4	10	SE 1	SE 1	SE 2
7	112.5	110.6	109.1	110.7	17.1	18.9	17.4	17.7	20.8	16.0	85	86	89	87	3.0	3.1	2.3	2.8	9	10	4	E 3	SW 1	NNW 2
8	110.0	109.9	109.8	109.9	16.0	22.8	17.4	18.4	24.5	13.8	96	66	86	83	0.8	9.4	2.8	4.3	3	5	6	NW 1	NE 4	NE 4
9	106.7	103.7	99.0	103.1	14.0	20.5	20.2	18.7	22.7	12.6	93	76	75	81	1.1	5.7	5.9	4.2	6	10	10	SE 6	SE 7	SE 6
10	97.7	98.1	101.8	99.2	17.9	21.9	18.8	19.4	23.8	17.3	93	65	74	77	1.4	9.2	5.5	5.4	10	9	4	SW 4	SW 5	SW 3
11	106.1	105.8	106.6	106.2	18.0	26.1	20.2	21.1	26.6	15.5	90	53	65	66	4.0	15.7	8.3	9.3	1	5	4	SW 6	SW 8	S 3
12	108.1	109.0	109.4	108.8	16.7	23.3	16.9	19.4	24.1	15.3	69	57	71	72	2.2	12.2	6.3	6.9	7	9	8	SW 5	SSW 4	SW 3
13	111.8	111.7	111.4	111.6	16.2	24.2	18.7	19.4	24.9	13.9	82	51	66	66	3.2	14.9	7.3	8.5	1	5	9	SW 5	SW 7	SW 3
14	110.9	110.5	109.8	110.4	15.4	22.9	16.5	17.8	23.5	11.9	86	56	97	81	2.1	11.6	0.6	4.8	9	9	10	C 0	W 4	SE 2
15	107.5	105.9	107.4	106.9	15.8	23.6	17.1	18.4	25.0	14.3	98	51	97	82	0.3	14.4	0.6	5.1	8	9	9	C 0	S 6	SE 3
16	108.3	109.6	109.0	109.0	16.8	19.9	16.1	17.2	20.4	15.1	95	67	85	82	1.0	7.7	2.7	3.8	9	10	9	SE 1	W 3	SW 1
17	108.6	107.8	107.3	107.9	13.3	18.3	14.3	15.0	21.1	11.5	91	69	89	83	1.4	6.6	1.8	3.3	9	8	2	W 5	SW 4	SW 2
18	105.2	105.6	108.0	106.3	15.3	20.5	15.3	16.6	21.7	13.2	91	57	89	79	1.5	10.3	1.9	4.6	10	8	0	W 4	W 7	W 1
19	110.7	113.1	114.6	112.8	14.1	16.0	16.5	15.6	20.9	11.6	99	96	83	93	0.2	0.8	3.3	1.4	10	10 ●	2	W 3	W 3	W 2
20	114.5	114.0	113.5	114.0	13.7	16.2	17.5	16.2	18.5	12.2	93	88	85	89	1.1	2.1	3.0	2.1	10	10	10	SW 6	SW 6	WSW 5
21	113.0	111.7	111.6	112.1	15.7	18.1	12.4	14.6	19.3	11.9	97	81	99	92	0.6	3.9	0.2	1.6	9	10	6	WSW 5	W 1	SW 3
22	111.4	111.5	111.5	111.5	11.6	17.7	11.1	12.9	18.4	9.6	94	54	88	79	0.8	9.3	1.6	3.9	5	6	3	W 3	NW 5	W 2
23	111.0	110.5	108.6	110.0	9.9	16.3	12.1	12.6	18.1	7.5	92	66	90	83	1.0	6.0	1.4	2.8	2	5	0	SW 5	SW 5	S 2
24	102.3	99.9	105.9	102.7	14.1	14.1	12.1	13.1	15.7	11.1	70	97	88	85	4.8	0.6	1.7	2.4	9	10 ●	0	SE 7	SW 4	WSW 5
25	107.6	104.9	105.5	106.0	11.7	18.7	11.3	13.2	20.4	9.4	78	51	90	73	2.9	10.6	1.3	4.9	9	7	9	SSW 8	SW 10	SW 5
26	103.3	102.7	106.2	104.1	11.6	15.1	13.4	13.4	16.4	9.3	85	75	83	81	1.9	4.3	2.7	3.0	9	6	3	SSW 7	SW 9	SW 5
27	109.0	109.6	110.1	109.6	12.3	16.9	12.3	13.5	17.7	11.2	89	63	89	80	1.3	7.2	1.3	3.4	10	9	9	SW 6	W 6	SW 3
28	110.0	111.0	113.0	111.3	10.9	16.7	12.1	13.0	18.4	9.7	97	69	94	87	0.3	5.9	0.8	2.3	7	8	7	SW 2	SW 3	W 1
29	114.5	113.4	117.1	115.7	10.2	15.5	12.3	12.6	17.4	8.9	97	77	94	89	0.3	4.1	0.9	1.8	10	7	6	WSW 5	W 4	W 2
30	118.0	118.3	116.0	117.4	12.3	15.9	13.3	13.7	17.1	10.7	89	64	82	78	1.3	6.5	2.8	3.6	9	9	10	W 3	WNW 5	SW 3
31	112.6	111.8	111.7	112.0	11.7	16.4	10.4	12.2	17.2	10.1	98	56	95	83	0.3	8.1	0.5	3.0	9	7	9	SW 6	W 6	W 5
M	111.7	111.4	111.6	111.6	14.3	19.6	15.4	16.2	21.1	11.9	90	65	83	80	1.6	8.4	2.9	4.3	6.8	7.6	5.4	3.9	4.6	2.8

Szczecin – Dąbie

$H_s = 1\ m$ $H_b = 6{,}9\ m$ $h_w = 21{,}5\ m$

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DNI	WIATR	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.0	.	–	▽ 4³⁰–³⁷
2	7	0.0	.	–	▽ 5⁰⁵–⁰⁸, 11³¹–³⁷; (K) 4¹⁵–5⁰⁰ SW–NE
3	8	.	.	–	
4	7	0.0	.	–	▽ 21⁴⁰–⁵⁰
5	7	.	.	–	▽ 2⁰⁵–¹⁵, 2²⁵–⁴⁵, 3²⁰–²⁵; (K) 0⁵⁰–5⁵⁰ SW–NE; = 6³⁰–9³⁰
6	8	.	.	–	
7	8	1.0	.	–	▽ 23³⁰–24; (K) 22⁵⁰–23³⁰ K–24
8	7	0.0	.	–	▽ 0⁰⁰–1³⁰, 2¹³–⁴⁵ K 0⁰⁰–⁴⁰ (K)–3⁵⁰ SW–NE
9	7	0.0	.	–	▽ 4¹⁰–²⁵, 11¹⁰–²⁰; (K) 2¹⁵–3⁴⁵ SW–E, NW–NE
10	7	11.1	.	–	
11	6	9.7	.	–	▽ 1⁴⁵–2⁴⁵ 3¹⁰–5⁰⁵ ●⁰5²⁰–7⁴⁰ ●¹–8²⁵ ●⁰–14³⁰ 16⁴⁰–20²⁰ 23¹⁵; (K) 2⁵⁰–4⁴⁵ NE–SW
12	7	.	.	–	●⁰ 0⁴⁵ 4¹⁵ = 20³⁰–23⁴⁵ ≡⁰–24
13	7	.	.	–	≡⁰ 0⁰⁰–4³⁰ ≡¹–7⁴⁰ ≡⁰–8³⁰ =–11¹⁰
14	7	35.4	.	–	▽ 12¹⁰–13¹⁵, 20¹⁵–21⁴⁰; (K) 11⁰⁰–13⁰⁰ SW–NE, 20¹⁰–³⁰ K–20⁴⁵ K–21³⁰ SW–NE; = 3³⁰–6³⁰
15	7	1.7	.	–	▽ 12¹⁰–⁵⁰ 18⁴⁵–⁴⁷; (K) 11⁵⁰–12¹⁰ K–12³⁵ (K)–12⁴⁵ SW–NE; = 0³⁰–4⁰⁰ ≡⁰–6¹⁵ ≡¹–7³⁰ ≡⁰–8²⁰ =–13²⁰, 23²⁰–²⁴
16	7	.	.	–	= 0⁰⁰–2⁰⁰ ≡⁰–3⁵⁰ =–7²⁰
17	7	.	.	–	= 3⁵⁰–6³⁰
18	8	.	.	–	
19	7	.	.	–	= 5²⁵–7¹⁵, ⌓ 10⁰⁰–5²⁵
20	7	0.4	.	–	▽ 23⁰⁵–²⁰ = 5³⁰–7³⁰
21	5	22.7	.	–	●⁰ 1⁴⁰ 3³⁰ 4¹⁵ 5⁰⁵ 8²⁵–10¹¹ ●¹–11²⁰ ●⁰–12¹⁹ ●¹–15⁰⁷ ●⁰–15⁵⁵ 17⁵⁰ 18²⁰ 22⁴⁵ 24; = 4³⁰–17²⁰ 21¹⁰–24
22	7	0.6	.	–	●⁰ 0⁰⁰–1³⁰ ●¹–4⁴⁰ ●⁰–6²⁵ 7³⁹ 8²⁵ 9⁴⁰ 11³⁵ 12¹⁰ 13¹⁵ ▽ 15²⁵–16⁰⁵; (K) 14³⁰–16²⁰ NE–SW, 18⁵⁰–21⁴⁵ NE–SW; = 0⁰⁰ 11³⁵ 23³⁰–²⁴
23	6	.	.	–	= 0⁰⁰–1⁵⁰ 4³⁰–13³⁰ ∞–14⁴⁰ 17²⁰–21¹⁰
24	8	0.0	.	–	▽ 14²¹–³⁸ 16⁰³–⁰⁶, ⌒ 20³³–⁴⁵
25	8	2.4	.	–	●⁰ 19⁰⁵–⁴⁵
26	7	5.1	.	–	●⁰ 2¹⁰ 5⁵⁰ 12⁴⁰–⁵⁰ ▽ 14⁵⁰–15⁰⁴ 15¹³–²⁰ 16¹⁰–²⁰ ●⁰ 16⁴⁰–22⁴⁰, = 22⁴⁰–24
27	7	6.4	.	–	●⁰ 2⁰⁵–3⁴⁰ ●⁰ 7³⁵–9¹⁵ ▽ 12²⁶–³⁷ 15⁰⁸–¹² 17¹⁸–³⁵ 19³¹–³⁵ 19⁴⁸–20¹², 20²⁰–³⁹; K⁰ 19²⁷–20⁰⁹ SW–NE; = 0⁰⁰–9³⁰
28	8	2.0	.	–	▽ 12¹³–²⁵ 14⁵²–15⁰², 16²⁰–³⁰ 16⁵⁰–17⁰⁵, 22⁰³–⁴⁵; ↙ 2²⁵–3¹⁰ SW
29	8	6.4	.	–	▽ 12⁰³–⁰⁵ 14²⁵–²⁸ ●⁰ 22⁵⁰–24
30	7	0.4	.	–	●⁰ 0⁰⁰–7²⁰, 8¹⁰ ●⁰ 9⁴⁸–10²⁵ ●⁰ … 13²⁰ ▽ 16⁵¹–⁵⁶
31	8	.	.	–	⌓ 22⁰⁰–24
Σ	–	105.3	–	–	UWAGI

Sierpień – Août

1	7	.	.	–	⌓ 0⁰⁰–7⁰⁰
2	8	0.0	.	–	= 4⁵⁰–6¹⁰
3	8	.	.	–	▽ 5⁵⁵–6⁰⁴
4	8	.	.	–	= 23²⁰–24, ⌓ 1⁰⁰–8³⁰
5	8	..	.	–	= 0⁰⁰–1⁵⁰ ≡⁰–6¹⁰ =–6⁵⁰, ⌓ 22³⁰–24
6	8	.	.	–	= 3²⁰–4⁴⁰ ≡–6³⁰ =–7⁴⁰, ⌓ 0⁰⁰–3²⁰, ⊕ 15³⁵–18⁰⁰
7	7	0.0	.	–	●⁰ 9¹⁵–⁵⁰ 12⁴⁰–13²⁰; (K) 19⁵⁰–20⁴⁵ W–E
8	7	.	.	–	= 5³⁰–6⁵⁵ ≡⁰–7⁴⁵ =–10²⁰
9	7	1.2	.	–	●⁰ 12¹⁵–13²⁰, 14⁰⁷–¹² por. wiatru 12 m/sek 17³⁰–20³⁰
10	7	0.9	.	–	●⁰ 1¹⁵–4¹⁵ ▽ 13⁵⁰–⁵⁵, 14¹²–²⁷, 17⁴⁸–18⁰⁵
11	8	3.0	.	–	
12	8	.	.	–	●⁰ 1⁴⁰–3³⁰
13	8	.	.	–	
14	8	1.1	.	–	●⁰ 15⁴⁵–17¹⁰ = 4³⁰–7³⁰, 19⁴⁰–24
15	7	1.0	.	–	●⁰ 17³²–19⁴⁵; = 0⁰⁰–10¹⁵
16	7	.	.	–	= 2³⁰–11³⁰, ⌓ 21⁰⁰–24
17	7	.	.	–	⌓ 0⁰⁰–8³⁰, ⊕ 11³⁵–13¹⁵
18	7	1.8	.	–	▽ 16¹⁰–⁴⁵, = 4³⁰–8⁴⁰
19	6	0.8	.	–	▽ 9²³–³², ●⁰ 11¹⁵–14³⁰ 15³⁵ = 4¹⁵–9²³
20	7	0.3	.	–	●⁰ 11⁴⁵ 12³⁰–13¹⁵ 23¹⁵–24 = 17²⁰–24
21	7	8.5	.	–	●⁰ 0⁰⁰–1²⁰ ▽ 11³⁰–⁴⁰ ●⁰ 14⁰⁶–15¹⁵ ▽ 16⁵⁰–19¹⁰ 19⁴⁵–20⁰⁸, = 0⁰⁰–6³⁰, ⌒ 19⁴⁷–20¹⁹
22	8	0.6	.	–	▽ 14²⁵–⁴⁸, 17⁴⁵–18¹², ≡⁰ 0⁵⁰–1⁵⁰ =–5³⁰
23	8	.	.	–	⌓ 21⁰⁰–24
24	6	11.6	.	–	●⁰ 8⁵⁵–9¹⁰ 10⁰⁹–²⁰ 11¹² 12⁰⁵–16⁵⁵ ▽–17⁰⁸ por. wiatru 18 m/sek 16⁵⁷–17⁰³, ⌓ 0⁰⁰–8³⁰
25	8	1.9	.	–	▽ 17²⁰–²⁵ 17³³–⁴⁵ ●⁰ 17⁵⁵–21³⁵ por. wiatru do 12 m/sek 8³⁰–9³⁰ ≫–16³⁰
26	8	5.0	.	–	●⁰ 10⁰³ 11⁰⁰ ▽ 11⁵⁷–12⁴⁶ 14¹²–¹⁶ 14⁴⁹–15⁰³ por. wiatru do 13 m/sek 10⁴⁰–12³⁰ por. wiatru do 14 m/sek 13³⁵–18²⁶
27	8	0.2	.	–	▽ 14²⁵–²⁹ ●⁰ 15⁰⁵ 16¹⁰, ▽ 20⁰³–⁰⁷ (K) 19⁵⁰–20⁴⁰ NW–NE
28	7	1.7	.	–	▽ 16⁴⁵–17¹⁰ 17⁴⁵–18²⁰, (K) 17³⁰–⁴⁵ K–18¹⁵ (K)–18⁴⁵ W–E; = 6³⁰–9³⁰
29	8	0.0	.	–	▽ 17⁴²–⁵³
30	8	1.1	.	–	▽ 17⁵⁷–15⁰⁰ 15⁵⁴–16⁰⁷
31	8	1.8	.	–	●⁰ 5²⁰–6³⁰ ▽ 14⁴⁰–⁴⁷, 15⁵³–16¹⁵ ●⁰ 17³⁰–19¹⁵, = 7³⁰–8³⁰
Σ	–	42.3	–	–	UWAGI

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$

Wrzesień – Septembre 1957

DNI	CIŚNIENIE P+900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	112.6	114.0	114.7	113.8	11.4	15.7	12.5	13.0	17.6	8.8	98	76	92	89	0.4	4.3	1.2	2.0	10	7	4	W 6	W 7	SW 3
2	112.6	111.7	110.4	111.6	11.9	16.8	14.7	14.5	19.6	10.1	89	82	94	88	1.5	3.5	0.9	2.0	10	10 ●	10	SW 4	S 4	SW 4
3	112.8	114.3	116.3	114.5	12.1	16.6	11.5	12.9	18.0	10.9	95	67	96	86	0.7	6.3	0.5	2.5	2	8	4	WNW 4	NW 4	C 0
4	119.3	120.5	121.6	120.5	8.7	17.5	8.1	10.6	18.5	7.3	99	55	96	83	0.1	9.0	0.5	3.2	1	5	2 ≡	W 3	W 4	C 0
5	118.9	114.2	114.9	116.0	11.5	17.9	13.3	14.0	18.3	4.8	79	57	96	77	2.8	8.9	0.6	4.1	9	9	0	SW 4	S 7	SW 2
6	115.4	116.0	117.3	116.2	12.7	18.5	9.4	12.5	20.4	9.0	99	51	93	81	0.2	10.3	0.8	3.8	10	6	0	SW 2	W 4	W 1
7	116.9	116.0	114.6	115.8	10.7	22.9	15.2	16.0	23.5	5.1	99	63	88	83	0.2	10.3	2.1	4.2	5	5	2	C 0	S 6	SSE 4
8	114.2	116.2	117.1	115.8	16.9	24.7	17.4	19.1	25.9	14.7	84	63	94	80	3.1	11.5	1.3	5.3	5	6	0	SW 4	W 3	NNE 3
9	116.6	120.7	123.0	120.1	14.6	15.3	11.4	13.2	17.5	11.0	95	88	98	94	0.7	2.1	0.4	1.1	9	10 ●	8	NNE 3	NW 4	C 0
10	121.6	119.0	115.5	118.7	12.5	18.6	15.3	15.4	20.1	9.0	99	65	74	79	0.2	7.4	4.6	4.1	4	6	6	S 2	S 4	SW 2
11	109.0	101.6	93.1	101.2	13.1	20.1	16.3	16.4	21.5	11.1	83	60	91	78	2.6	9.4	1.7	4.6	7	9	8	SW 6	S 9	SSW 8
12	88.6	89.7	96.9	91.7	13.9	13.5	10.3	12.0	17.3	9.8	85	65	86	79	2.3	5.5	1.7	3.2	9	10 ●	6	S 7	SW 10	SW 7
13	99.2	98.6	96.1	98.0	9.0	13.9	10.1	10.8	15.2	7.6	85	62	96	81	1.7	6.1	0.5	2.8	6	7	10 ●	SW 7	WSW 8	SW 2
14	97.7	99.3	101.6	99.5	10.3	13.8	11.9	12.0	14.6	8.4	86	71	77	78	1.7	4.6	3.1	3.1	10	10	4	SW 7	SW 7	SW 3
15	102.7	104.4	106.1	105.1	10.5	14.4	10.2	11.3	15.3	9.8	95	66	83	81	0.7	5.6	2.0	2.8	10	9	9	SW 4	W 6	W 6
16	109.6	111.6	113.4	111.5	9.6	9.3	8.9	9.2	12.9	8.5	86	85	86	86	1.8	1.7	1.5	1.7	9	9	7	W 6	W 3	SW 5
17	112.9	113.2	114.6	113.6	10.7	11.9	10.7	11.0	16.0	8.4	99	91	94	95	0.2	1.2	0.9	0.8	10	9 ●	10	W 3	NW 3	N 2
18	114.6	113.9	112.2	113.6	6.7	15.4	9.2	10.4	16.4	4.6	100	63	89	84	0.0	6.5	1.2	2.6	10 ≡	9	0	W 2	NW 5	W 2
19	107.5	104.2	106.1	105.9	7.8	10.3	9.9	9.5	12.5	5.7	94	99	99	97	0.6	0.1	0.2	0.3	7	10 ●	10 ●	W 2	SE 3	NE 2
20	109.4	112.5	114.8	112.2	8.7	12.2	9.5	10.0	12.8	7.8	97	82	93	91	0.3	2.5	0.8	1.2	9	9	10	WNW 4	N 3	N 1
21	115.8	115.6	113.5	115.0	4.9	13.0	9.8	9.4	14.5	3.2	100	70	95	88	0.0	4.5	0.6	1.7	5 ≡	10	9	W 1	C 0	C 0
22	108.7	107.5	105.3	107.2	9.7	12.9	15.6	13.4	15.8	8.7	95	99	96	97	0.6	0.2	0.7	0.5	10	10	10	SE 1	SW 3	SW 2
23	99.0	95.6	99.9	98.2	15.1	16.2	12.3	14.0	17.0	11.8	99	94	96	96	0.2	1.2	0.5	0.6	10 ●	10 ●	10 ●	SW 5	SW 3	N 4
24	103.7	104.2	109.8	105.9	9.7	12.0	7.8	9.3	13.6	7.4	91	51	75	72	1.1	6.9	2.7	3.6	9	7	0	W 2	NW 5	NW 6
25	114.2	116.7	118.0	116.3	5.3	12.3	5.5	7.2	13.4	3.6	84	53	91	76	1.4	6.7	0.8	3.0	1	5	2	W 4	NNW 6	NW 2
26	116.3	116.9	118.9	117.4	3.9	12.0	5.2	6.6	12.4	3.3	95	61	92	83	0.4	5.4	0.7	2.2	9	3	0	NW 1	N 5	NW 2
27	116.4	111.8	103.5	110.6	4.8	9.8	10.9	9.1	11.2	2.9	86	83	94	88	1.2	2.0	0.8	1.3	9	10 ●	10 ●	SW 4	WSW 7	W 9
28	104.8	104.9	105.4	105.0	9.2	12.7	9.3	10.1	14.4	8.6	87	73	92	84	1.5	3.9	0.9	2.1	6 ●	7	4	NW 6	NW 8	W 5
29	100.7	97.4	98.6	98.9	8.5	11.7	5.8	8.0	13.0	5.4	96	76	94	89	0.5	3.3	0.6	1.5	9	9	0	SW 5	SW 6	W 1
30	103.7	109.2	113.8	108.9	5.5	9.0	6.3	6.8	10.5	4.5	95	89	89	91	0.4	1.3	1.0	0.9	5	9	6	WNW 3	NNW 5	NNW 1
31																								
M	109.8	109.7	110.3	109.9	10.0	14.7	10.8	11.6	16.3	7.7	92	72	91	85	1.0	5.1	1.2	2.4	7.5	8.1	5.4	3.7	5.1	3.0

Październik – Octobre

1	114.7	116.5	120.0	117.1	4.4	7.1	3.3	4.5	9.9	2.7	93	81	95	90	0.6	1.9	0.4	1.0	9	9 ●	1	WNW 3	NNW 4	N 2
2	122.7	123.0	120.8	122.2	1.3	10.0	7.3	6.5	11.4	-0.7	98	56	81	78	0.1	5.4	1.9	2.5	2	6	9	W 4	W 3	SW 4
3	112.6	107.7	106.9	109.1	6.3	7.6	8.2	7.6	10.0	5.3	76	94	82	84	2.2	0.6	2.0	1.6	10	10 ●	1	S 7	SW 7	W 7
4	110.4	115.1	119.2	114.9	5.3	11.4	6.6	7.5	12.2	4.7	86	47	85	73	1.3	7.1	1.4	3.3	3	6	6	W 6	WNW 9	W 3
5	119.9	117.8	113.8	117.2	6.9	10.7	8.7	8.8	10.9	6.1	87	56	93	79	1.3	5.7	0.7	2.6	10	10	10 ●	W 6	WSW 7	WSW 7
6	116.7	120.2	122.5	119.8	10.1	13.1	11.9	11.8	13.4	8.3	96	77	91	88	0.3	3.5	1.2	1.7	9	10	9	W 4	W 5	W 4
7	122.7	123.0	124.8	123.5	12.0	16.0	9.3	11.6	17.3	8.4	88	69	93	83	1.7	5.6	0.8	2.7	10	2	0	WNW 3	W 4	WNW 1
8	126.2	127.3	126.4	126.6	7.9	13.5	11.5	11.1	14.4	4.3	99	88	91	93	0.1	1.8	1.2	1.0	9	10	9	C 0	C 0	SE 1
9	123.5	122.4	120.3	122.1	7.5	14.5	6.7	8.8	17.8	5.7	100	80	100	93	0.0	3.2	0.0	1.1	10 ≡	1	10 ≡	SE 3	E 4	C 0
10	118.2	117.2	117.5	117.6	5.6	18.2	12.7	12.3	19.1	2.9	100	64	91	85	0.0	7.5	1.4	3.0	0 ≡	0	0	C 0	S 3	SW 2
11	119.2	119.2	118.1	118.8	8.4	12.2	7.1	8.7	14.3	6.6	99	82	94	92	0.1	2.5	0.6	1.1	10 ≡	9	6	W 3	SW 2	SW 1
12	117.6	121.9	126.3	121.9	9.2	13.0	6.9	9.0	14.6	5.1	100	86	92	93	0.0	2.1	0.7	0.9	10 ● ≡	2	1	SW 1	NNW 3	NW 2
13	125.8	123.8	122.4	124.0	4.3	12.1	9.3	8.8	14.7	3.1	98	89	99	95	0.1	1.5	0.1	0.6	6	6	0 ≡	C 0	SW 3	SW 3
14	122.4	123.6	126.3	124.2	8.3	12.3	8.7	9.5	12.3	7.7	97	87	93	92	0.4	1.9	0.7	1.0	10	10	9	W 4	WNW 2	N 1
15	127.5	127.4	126.4	127.1	6.9	11.4	9.8	9.5	12.2	4.4	96	70	79	82	0.4	4.1	2.5	2.3	10	9	9	W 2	C 0	S 3
16	122.8	120.0	116.1	119.6	7.3	13.3	10.1	10.2	14.8	6.7	97	74	91	87	0.3	4.0	1.2	1.8	9	4	0	SE 4	SW 5	S 3
17	112.4	114.9	116.4	114.6	9.5	14.5	8.9	10.4	16.0	7.5	95	71	89	85	0.7	4.8	1.2	2.2	10 ●	8	0	SW 5	WNW 7	W 2
18	107.2	105.5	104.6	105.8	11.2	15.7	15.5	14.5	16.9	7.9	88	82	78	83	1.7	3.2	3.9	2.9	10	10	4	SW 7	SW 6	SW 7
19	103.2	104.3	106.7	104.7	14.9	15.4	10.5	12.8	16.3	9.7	77	66	96	80	3.8	6.0	0.5	3.4	9	10	10 ●	SW 6	SW 5	SW 4
20	110.3	112.6	114.7	112.5	9.4	11.4	6.7	8.6	12.8	6.3	97	75	87	86	0.3	3.5	1.3	1.7	10	8	0	WSW 2	W 4	W 2
21	112.7	109.4	106.0	109.4	6.3	10.5	10.9	9.6	11.8	5.1	84	76	71	77	1.5	3.0	3.7	2.7	2	9	10	SW 7	SSW 7	SSW 7
22	101.0	99.4	100.9	100.4	8.1	9.7	9.3	9.1	11.1	7.5	82	79	93	85	2.0	2.5	0.8	1.8	9	10	10 ●	SSW 6	SW 6	C 0
23	106.4	108.7	108.9	108.0	6.7	9.6	9.2	8.7	10.2	5.5	97	78	71	82	0.3	2.7	3.3	2.1	10	9	10	W 6	SW 6	SW 7
24	107.7	112.6	120.1	113.5	8.5	13.1	7.7	9.2	13.5	7.1	99	75	87	87	0.2	3.8	1.3	1.8	10 ●	7	2	SW 7	W 4	W 2
25	122.9	123.2	121.8	122.6	3.5	11.1	11.1	9.2	12.1	2.9	97	72	91	87	0.2	3.7	1.1	1.7	2	9	9	SW 3	SW 3	SW 4
26	120.2	119.9	118.1	119.4	9.5	13.7	9.9	10.8	16.0	8.6	96	81	88	88	0.5	3.0	1.4	1.6	10	9	0	SW 4	SW 4	W 3
27	116.1	115.9	115.2	115.7	5.9	11.3	9.9	9.2	12.2	5.5	98	82	89	90	0.2	2.5	1.3	1.3	10	9	6	SW 5	SW 5	SW 3
28	114.6	114.5	114.1	114.4	9.3	13.4	11.5	11.4	13.8	8.0	85	76	77	79	1.7	3.7	3.2	2.9	10	9	10	SW 5	SW 6	SW 5
29	113.2	113.1	112.7	113.0	9.7	13.6	10.7	11.2	13.6	9.0	83	70	85	79	2.0	4.7	2.0	2.9	7	9	1	SW 7	SW 7	SW 4
30	110.4	110.3	112.0	110.9	9.1	14.3	12.7	12.2	14.4	8.3	85	75	89	83	1.8	4.1	1.6	2.5	6	10 ●	10	SW 6	SW 5	SW 3
31	110.2	108.7	105.4	108.1	11.1	13.2	12.5	12.3	13.7	10.1	86	82	80	83	1.8	2.8	2.9	2.5	10 ●	10	10	SW 5	SW 6	SW 7
M	115.9	116.1	116.3	116.1	7.9	12.5	9.5	9.8	13.7	6.1	92	75	88	85	0.9	3.6	1.5	2.0	8.1	7.7	5.3	4.2	4.6	3.4

Szczecin – Dąbie

$H_s = 1\ m$ $H_b = 6{,}9\ m$ $h_w = 21{,}5\ m$

Wrzesień – Septembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	4.0	.	–	•⁰6¹⁰–45 ⛆ 17⁵⁵–18²⁷ 19¹⁰–25 ⌒ 18¹⁵–19
2	6	4.3	.	–	•⁰10²⁶ 11¹⁵ 13⁴⁰ 14⁰⁵ 16⁵⁰ 17⁴⁵ ⛆ 18³⁴–43 18⁵¹–19⁰⁶ 22⁰⁸–14 ☇⁰22⁰⁹ = 9¹⁵–14³⁰ 18¹⁰–24
3	8	1.4	.	–	•⁰1⁵⁵–4⁴⁵ ⛆ 13⁵⁵–14⁴⁰ 14⁵³–15¹⁰ 16⁴⁵–17⁰⁵ 19⁵⁵–20²⁵ = 0⁰⁰–4³⁰ ⌒ 16⁵³–17⁰⁰
4	8	.	.	–	≡ 20²⁰–21⁵⁰ ≡⁰–22⁴⁵ =–24
5	7	1.0	.	–	•⁰14²⁶–45 16²⁵–19¹⁵ = 0⁰⁰–5³⁰ 18³⁰–24 ⊕ 9⁴⁰–10⁴⁵
6	7	.	.	–	= 0⁰⁰–2¹⁵ ≡⁰–4²⁰ ≡¹–4⁵⁰ =–11³⁰ ≡ 21¹⁵–24
7	7	.	.	–	≡ 0⁰⁰–1⁰⁰ ≡⁰–1⁵⁰ =–5³⁰ ≡–6³⁰ =–8⁴⁰
8	7	.	.	–	= 20³⁰–22⁴⁰ ⌒ 0⁰⁰–7³⁰ 23⁰⁰–24
9	9	0.0	.	–	•⁰13⁴⁵–14⁴⁰ ≡ 21³⁰–23³⁰ ⌒ 0⁰⁰–9⁰⁰
10	8	.	.	–	•⁰2⁰⁵…12 23⁴⁰…50
11	7	1.7	.	–	•⁰15⁴⁵ 18⁰⁰–19⁰⁵ •¹–19²⁸ •⁰–20²⁵ 23⁴⁰ 24 par. wiatru do 14 m/sek 13²⁰–16⁴⁵ par. wiatru do 16 m/sek – 17²⁵
12	8	4.3	.	–	•⁰0⁰⁰ 1²⁰ ⛆ 9⁰⁵–12 9²⁰–42 9⁵²–10¹² 13⁵⁰–15¹⁰ •⁰–16⁴⁰ par. wiatru do 17 m/sek 9²⁰–25 par. wiatru do 14 m/sek – 9³⁵ 11³⁰–13¹⁰
13	8	1.6	.	–	⛆ 10¹¹–11⁰⁴ 12³⁰–3⁵ 19⁵⁰–22²⁰ 23¹⁰–12 par. do 14 m/sek 7³⁰–10⁴⁰, 11⁴⁵–15²⁰ [12.IX: ≫–16³⁰ (par. do 18 m/sek), par. wiatru do
14	7	0.0	.	–	⛆ 16⁰³–06 par. wiatru do 12 m/sek 9³⁰–16²⁰ 15 m/sek – 23³⁰
15	8	1.6	.	–	⛆ 15²³–28 16⁰⁶–17 18⁵⁰–19⁰⁵ par. wiatru 12 m/sek 15⁴⁵–16²⁰ par. wiatru 14 m/sek 18⁵⁵–19⁰⁵
16	7	3.1	.	–	•⁰2⁰⁵–3¹⁵ 4³⁰ ⛆ 13³⁰–40
17	8	8.0	.	–	•⁰2⁰³–3¹⁰ 5³⁵ 9⁰⁸–10¹⁵ ⛆ 13¹⁹–14⁰³ 14¹²–28 14³⁴–47
18	7	.	.	–	≡ 1⁴⁰–2²⁵ =–4⁴⁰ ≡⁰–6²⁵ ≡¹–7⁵⁵ ≡⁰–8⁴⁰ =–9³⁰
19	5	4.9	.	–	•⁰8⁵⁰–14¹⁰ •⁰–15⁴⁰ 18⁴⁵–22³⁰ 23¹⁰ •⁰ 24 = 15⁴⁰–18⁴⁵
20	8	.	.	–	•⁰0⁰⁰–12⁰ = 13⁰–6³⁰
21	7	0.1	.	–	= 0⁴⁰–1⁴⁵ ≡⁰–4³⁰ ≡¹–7³⁵ ≡⁰–8¹⁵ =–9¹⁵ ⊕ 13³⁰–14¹⁵
22	6	30.0	.	–	•⁰5³⁰–6³⁰ ⛆ 12⁴⁷–13³⁵ •⁰15⁵⁰–16⁴⁰ ⛆ 23⁴⁵–24 (☇) 23⁵⁰–24 W = 7³⁰–23⁴⁵
23	6	5.3	.	–	⛆ 0⁰⁰–1³⁰ •⁰6⁵⁰ 9⁰⁰–11¹⁰ 12⁵⁰ 15²⁰ 16⁰³–18⁰⁸ 19²⁰–20³⁰ 21⁴² 22⁴⁰ ☇⁰0⁰⁰–20 W-E (☇)–0⁴⁵ = 12¹⁵–17³⁰
24	8	.	.	–	par. wiatru do 14 m/sek 15³⁰–20³⁰
25	8	.	.	–	
26	8	.	.	–	
27	7	2.9	.	–	•⁰12⁴⁵ 14¹⁵ 16⁰⁷ 19²⁰ 20⁴⁰…22⁴⁵ par. wiatru do 14 m/sek 13³⁰–24 ⌒ 0³⁰–8³⁰
28	8	3.3	.	–	⛆ 7⁵⁰–8⁰⁵ 8²⁰–40 11⁵⁰–12²⁰ 12⁵⁵–13⁰⁴ 14¹⁰–14 16²⁰–22 20¹⁰–22 par. wiatru do 12 m/sek 0⁰⁰–7³⁰ par. wiatru do
29	7	2.9	.	–	⛆ 2¹⁰–14 13⁰⁷–18 13²⁴–44 15⁴³–16¹⁵ 16²⁹–36 16⁵³–17⁰⁴ 17³⁰–18²⁵ ⌓ 20⁴⁰–24 [28.IX: 14 m/sek 12³⁰–16³⁰
30	8	2.4	.	–	•⁰3⁰⁵–4²⁰ ⛆ 8³⁴–10⁴⁵ 11²⁵–12¹⁰ 12³⁰–45 ⌓ 0⁰⁰–1⁵
31					
Σ	–	82.8	–	–	UWAGI.

Październik – Octobre

1	8	0.5	.	–	⛆ 6⁴⁰–47 8⁵⁰–9¹⁰ 12³⁵–13²⁷ 15⁵⁰–52 = 20³⁰–22³⁰ ⌴ 22³⁰–24
2	8	0.0	.	–	⛆ 18²³–27 20⁴²–55 ⌴ 0⁰⁰–7²⁰
3	6	1.6	.	–	•⁰7²⁰–8¹⁵ 8³⁵–9²⁰ 11⁴⁰ 13¹⁰ 16³⁵ 17¹⁰ ⛆ 17⁵⁰–18⁰⁵ par. wiatru do 12 m/sek 9³⁰–19³⁰ 21²⁰–24 = 6¹⁵–8²⁵ 9²⁰–17⁴⁰
4	8	.	.	–	⛆ 0²⁸–31 par. wiatru do 12 m/sek 0⁰⁰–6¹⁵ par. wiatru do 14 m/sek 10⁰⁰–13¹⁵
5	8	3.0	.	–	•⁰14⁰⁵–17³⁰ 21¹⁰
6	8	.	.	–	
7	7	.	.	–	≡ 20¹⁵–24
8	7	.	.	–	≡ 0⁰⁰–1⁵ =–3⁴⁰ ≡⁰–4⁴⁵ =–12³⁰
9	6	.	.	–	= 0³⁰–5⁰⁰ ≡⁰–6³⁰ ≡¹–8¹⁵ ≡⁰–9¹⁵ =–19⁰⁵ ≡⁰–20⁴⁵ ≡²–24
10	6	.	.	–	≡² 0⁰⁰–4³⁰ ≡¹–7³⁰ =–11³⁰ ∞–16⁴⁵ =–22⁴⁵ ≡¹–23¹⁰ ≡²–24
11	6	0.6	.	–	≡² 0⁰⁰–3⁴⁰ ≡⁰–8⁴⁵ =–22⁵⁰ ≡²–24
12	7	0.0	.	–	•⁰5²⁰⁻³⁵ 6⁰⁵⁻¹⁵ 6⁵⁰ 7⁰⁵ •⁰9¹⁰–11⁴⁰ ≡⁰ 0⁰⁰–1³⁰ ≡¹–8³⁰ ≡⁰–11⁵⁰ =–12²⁰ ≡ 20³⁰–21³⁰
13	6	.	.	–	≡ 6¹⁵–8³⁰ =–13³⁰ ∞–16³⁰ =–18³⁰ ≡⁰–21⁴⁰ =–24
14	5	0.0	.	–	•⁰13⁰⁴–50 = 0⁰⁰–20¹⁵ ≡ 22²⁵–24
15	7	.	.	–	≡ 0⁰⁰–45 ≡⁰–1⁵⁵ =–5³⁰
16	6	0.0	.	–	= 6¹⁵–11³⁰ ∞–16³⁰ =–21⁴⁵
17	7	0.0	.	–	•⁰6⁵⁵–7²⁰ = 10⁰⁰–10²⁵
18	7	.	.	–	= 6²⁰–11³⁰
19	7	3.6	.	–	•⁰15¹⁰…²⁵ 16⁰⁵–22¹⁵ 23⁴⁰ 24 = 22¹⁵–24
20	7	.	.	–	•⁰0⁰⁰ 2¹⁵ = 0⁰⁰–9³⁰
21	7	0.0	.	–	•⁰14⁴⁰ 15¹⁰
22	7	0.4	.	–	•⁰5⁵⁰–6⁰⁵ 8²⁰–9³⁷ 15⁴²–17¹⁰ 19⁴⁰ 21⁰⁰–23³⁵ = 17⁰⁰–24
23	7	3.8	.	–	•⁰21⁵⁰–24 = 0⁰⁰–2³⁰ 6²⁰–10⁴⁰ par. wiatru do 12 m/sek 20¹⁵–24
24	8	0.4	.	–	•⁰0⁰⁰–3⁴⁰ 5¹⁰–8³⁰ 10⁴⁰ •⁰ 11²⁰ par. wiatru do 12 m/sek 0⁰⁰–6¹⁵ ⌒ 21⁵⁰–24
25	7	.	.	–	≡ 16⁵⁰–19³⁰ ⌒ 0⁰⁰–4⁵⁰ ⌴–7³⁰
26	6	.	.	–	= 1⁰⁰–13³⁰ ∞ 14⁴⁰–16³⁰ =–24
27	6	.	.	–	= 0⁰⁰–24
28	6	0.0	.	–	= 0⁰⁰–13³⁰
29	7	.	.	–	•⁰1⁰⁵ 2²⁰ = 6³⁰–9³⁰
30	6	0.0	.	–	•⁰12⁰⁸…13²⁰ 17¹⁰–18²⁵ = 7³⁰–8⁴⁵ ∞–14³⁰ =–24
31	7	0.0	.	–	•⁰6⁴⁸–7⁴⁰ = 0⁰⁰–11³⁰ 13³⁰–22³⁰
Σ	–	13.9	–	–	UWAGI.

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$

Listopad – Novembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.6	100.3	104.4	101.4	11.2	13.5	8.5	10.4	14.0	8.2	76	71	77	75	2.9	4.5	2.6	3.3	7	10	0	SW 6	SW 7	SW 4
2	106.9	107.9	110.3	108.4	5.6	11.4	7.4	8.0	11.5	5.1	85	62	79	75	1.4	5.2	2.2	2.9	1	2	0	SW 6	SW 7	SW 4
3	112.3	111.4	109.4	111.0	3.0	11.4	7.5	7.4	12.1	2.1	93	60	83	79	0.6	5.5	1.7	2.6	1	7	0	C 0	S 5	ESE 5
4	107.4	106.7	107.1	107.1	5.9	14.1	11.1	10.6	14.8	4.9	92	62	79	78	0.7	6.1	2.8	3.2	7	9	10	E 3	S 5	SW 7
5	105.4	102.0	102.2	103.2	5.9	12.4	10.9	10.0	13.0	4.9	95	75	79	83	0.5	3.5	2.7	2.2	8	9	9	E 2	SE 7	SE 4
6	104.4	106.1	106.2	105.6	6.9	11.1	7.3	8.2	12.0	6.4	96	81	99	92	0.4	2.4	0.1	1.0	8	9	10	C 0	C 0	NE 2
7	101.3	102.3	105.9	103.2	6.6	8.6	9.0	8.3	9.5	5.7	98	96	89	94	0.1	0.5	1.3	0.6	10	10	10	SE 3	SW 4	SW 3
8	107.1	107.4	107.2	107.2	7.9	8.2	8.3	8.2	9.1	7.2	99	97	99	98	0.1	0.3	0.2	0.2	10 ●	10	10	NNE 1	NNE 5	N 5
9	104.7	103.2	106.1	105.3	9.2	9.1	9.4	9.3	9.5	7.6	100	96	99	98	0.0	0.5	0.2	0.2	10	10 ●	10	E 5	E 4	SE 7
10	108.4	109.2	112.1	109.9	9.2	11.2	10.7	10.4	12.1	8.6	100	92	91	94	0.0	1.0	1.2	0.7	10	9	10	SE 2	SE 4	E 6
11	115.3	118.5	122.3	118.7	9.7	10.1	8.3	9.1	11.5	7.0	93	81	96	90	0.8	2.4	0.5	1.2	10	10	10	E 7	E 5	NE 5
12	126.0	128.1	129.7	127.9	6.1	6.5	4.9	5.6	9.6	4.4	86	75	81	81	1.3	2.5	1.7	1.8	10	9	10	NE 6	NE 6	E 2
13	130.9	131.1	131.2	131.1	1.5	2.0	0.3	1.0	5.0	-1.2	80	69	86	78	1.4	2.2	0.8	1.5	10	8	10	E 2	SE 2	E 1
14	131.1	131.6	131.9	131.5	-0.7	0.3	-0.4	-0.3	0.9	-2.7	89	84	86	86	0.6	0.9	0.6	0.8	10	10	10	SE 3	E 4	SE 6
15	131.0	130.0	129.6	130.2	-2.0	-0.4	0.3	-0.4	0.4	-2.3	92	90	92	91	0.5	0.6	0.5	0.5	10	10	10	SE 4	SE 3	SE 2
16	129.8	130.8	131.4	130.7	0.1	1.2	1.2	0.9	1.4	-0.2	96	89	90	92	0.3	0.8	0.7	0.6	10 ●	10	10	SE 2	E 3	SE 3
17	131.2	131.2	132.2	131.5	1.3	3.9	-0.5	1.0	3.9	-0.9	87	70	92	83	0.9	2.4	0.5	1.3	10	9	0	E 3	SE 8	E 2
18	131.4	130.8	131.0	131.1	-4.0	3.5	2.1	0.9	3.8	-4.7	99	78	84	87	0.1	1.7	1.2	1.0	6	10	10	C 0	SE 3	E 1
19	131.5	133.4	135.4	133.4	1.5	3.1	2.1	2.2	3.2	1.1	80	73	69	74	1.4	2.1	2.2	1.9	10	10	10	SE 2	E 4	SE 6
20	136.7	136.7	137.4	136.9	1.9	3.6	-3.3	-0.2	4.0	-4.1	67	57	93	72	2.3	3.4	0.4	2.0	7	0	0	SE 6	SE 6	SE 3
21	136.1	133.9	128.1	132.7	-4.6	3.8	2.7	1.2	4.2	-6.0	96	72	65	78	0.2	2.2	2.6	1.7	0	0	0	SE 1	SE 4	S 6
22	119.4	116.1	114.2	116.6	-1.5	1.1	1.1	0.4	2.8	-2.0	89	85	77	84	0.6	1.0	1.5	1.0	0	10	10	SW 5	SW 5	SSW 5
23	111.7	114.5	120.5	115.6	1.4	4.5	3.5	3.2	4.9	0.2	92	90	81	88	0.6	0.8	1.4	0.9	10 ●	10	9	SW 6	NW 6	WNW 4
24	121.0	120.6	119.6	120.4	1.1	6.0	6.7	5.1	6.8	-0.9	90	86	85	86	0.6	1.2	1.4	1.1	10	10	10	SW 5	W 7	W 5
25	116.8	118.3	119.7	118.3	6.5	8.7	8.9	8.4	9.1	5.9	99	99	96	98	0.1	0.1	0.5	0.2	10 ●	10 ●●	10	W 7	W 6	W 6
26	120.8	121.0	118.7	120.2	7.9	8.6	7.3	7.8	9.1	6.7	99	93	87	93	0.1	0.6	1.3	0.7	10	10	10	SW 6	W 6	W 5
27	114.8	116.5	116.6	116.0	8.4	8.4	8.7	8.6	9.6	6.6	90	71	94	85	1.0	3.1	0.6	1.6	10	10	10	WSW 7	NW 5	W 4
28	112.8	111.1	109.1	111.0	8.5	10.0	8.6	8.9	10.0	7.8	96	82	78	85	0.5	2.2	2.4	1.7	10	10	10	W 6	W 7	NW 7
29	113.8	120.6	130.6	121.7	4.1	2.1	-1.0	1.0	9.6	-1.4	72	85	77	78	2.3	1.0	1.3	1.5	7	8	2	N 9	NNE 9	NE 6
30	134.8	134.4	133.7	134.3	-1.4	1.4	-1.9	-1.0	1.6	-2.7	84	74	77	78	0.9	1.8	1.2	1.3	9	7	9	NW 5	N 4	N 1
31																								
M	118.5	118.9	119.8	119.1	3.9	6.7	5.0	5.2	7.6	2.4	90	80	85	85	0.8	2.1	1.3	1.4	8.0	8.5	7.6	4.0	5.0	4.2

Grudzień – Décembre

1	130.9	127.5	125.6	128.0	-1.7	-0.7	2.9	0.8	3.0	-3.6	75	97	98	90	1.3	0.2	0.1	0.5	9	10 ✳	10 ●	WNW 1	SW 6	NW 4
2	126.8	127.6	127.8	127.4	3.5	4.7	3.1	3.6	5.0	2.5	98	97	95	97	0.1	0.2	0.4	0.2	10 ●	10	10	NW 2	N 2	W 3
3	123.9	123.2	124.4	123.8	4.1	5.5	3.9	4.4	5.7	2.6	100	97	98	96	0.0	0.3	0.2	0.2	10 ●	10 ●	10 ●	W 2	N 4	N 1
4	123.5	121.8	120.1	121.8	3.2	5.1	5.2	4.7	5.6	2.9	97	90	94	94	0.3	0.9	0.5	0.6	10	10	10 ●	W 1	W 4	W 5
5	120.3	121.3	124.3	122.0	6.3	7.2	3.7	5.2	7.8	3.2	86	80	95	87	1.2	2.1	0.4	1.2	9	6	0	NW 5	WNW 4	NW 3
6	126.1	125.2	119.5	123.6	0.5	1.5	2.7	1.8	3.9	-0.5	100	100	88	96	0.0	0.0	0.9	0.3	10 ≡	10 ≡	9	SW 1	SW 5	S 6
7	112.2	108.8	100.7	107.2	0.7	2.1	0.5	1.0	2.8	0.2	90	89	96	92	0.6	0.8	0.2	0.5	10	10	10 ✳	SW 6	SW 8	SW 7
8	84.1	74.6	72.1	76.9	2.5	5.0	6.9	5.3	9.7	0.1	95	95	75	88	0.4	0.4	2.4	1.1	10 ●	10 ●	0	SSW 7	SW 9	WSW 9
9	77.3	88.6	95.5	87.1	3.9	1.4	-1.4	0.6	7.9	-2.3	82	81	84	82	1.5	1.3	0.9	1.2	10	6	1	WNW 7	WNW 6	WSW 4
10	94.1	100.1	105.1	99.8	-1.0	-1.2	-6.0	-3.6	-0.6	-6.5	85	74	87	82	0.9	1.4	0.5	0.9	9	2	0	SW 3	NW 3	SW 3
11	104.3	101.3	98.7	101.4	-11.8	-4.4	-2.8	-5.4	-2.6	-12.6	93	84	77	85	0.2	0.7	1.1	0.7	1	9	9	SE 3	SE 6	ESE 5
12	95.3	94.7	95.1	95.0	-2.3	0.3	-4.3	-2.6	0.3	-5.6	85	79	96	87	0.8	1.3	0.2	0.8	10	1	3	E 5	E 5	NE 3
13	92.5	90.6	86.6	89.9	-0.6	0.6	0.7	0.4	0.8	-7.4	99	98	98	98	0.0	0.1	0.1	0.1	10	10	10 ≡	NE 2	NE 3	NE 4
14	87.9	94.5	106.2	96.2	1.7	2.4	1.4	1.7	2.7	0.2	90	82	65	79	0.6	1.3	2.4	1.4	10	10	10	NNE 9	NNE 9	NE 10
15	117.2	123.2	127.8	122.7	-1.4	0.0	-9.1	-4.9	1.8	-9.4	80	71	88	80	1.1	1.8	0.4	1.1	3	6	0	NE 5	E 5	E 1
16	129.0	128.5	127.4	128.3	-9.7	-4.1	-7.4	-7.2	-3.7	-11.6	91	75	82	83	0.3	1.1	0.6	0.7	1	2	0	SE 1	SE 4	SE 2
17	124.2	121.9	122.2	122.8	-11.0	-5.5	-7.2	-7.7	-5.2	-13.3	90	75	85	83	0.3	1.0	0.5	0.6	1	2	10	E 3	S 4	C 0
18	122.6	122.6	121.7	122.3	-5.7	-5.3	-3.9	-4.7	-3.8	-7.6	90	85	89	88	0.4	0.6	0.5	0.5	10	10 ⛬	10	SW 1	SW 3	SE 5
19	121.3	123.8	127.8	124.3	-2.5	-0.6	0.1	-0.7	0.2	-4.4	91	83	88	87	0.5	1.0	0.8	0.8	10	10	10	SE 5	S 1	SW 2
20	130.2	128.7	125.8	128.2	0.9	3.5	1.6	1.9	3.7	-0.5	88	76	81	82	0.7	1.8	1.3	1.3	10	4	4	SW 7	SW 8	SW 7
21	121.1	121.6	124.3	122.3	3.0	4.4	3.5	3.6	4.8	0.7	77	80	91	83	1.7	1.7	0.6	1.3	10	10	7	SW 9	SW 8	WSW 5
22	122.8	122.3	121.8	122.3	3.1	4.3	3.1	3.4	4.4	2.3	97	92	95	95	0.2	0.7	0.4	0.4	10	10	10	WSW 5	SW 5	SW 2
23	117.2	114.8	112.0	114.7	1.3	0.0	0.0	0.3	3.4	-1.3	91	68	74	78	0.6	1.9	1.6	1.4	10	10	0	S 5	S 7	SW 6
24	112.4	114.1	115.1	113.9	1.1	2.3	0.4	1.0	3.0	-1.2	75	59	71	68	1.6	2.9	1.9	2.1	9	6	0	SW 3	SW 2	SW 2
25	114.9	114.9	117.8	115.9	-0.2	0.4	0.5	0.3	1.2	-2.0	84	80	84	83	0.9	1.3	1.0	1.1	10	9	4	SW 2	SW 5	SW 4
26	120.3	122.6	124.0	122.3	1.7	2.6	1.9	2.0	2.9	-0.5	94	93	96	95	0.4	0.6	0.4	0.4	10	10	10	WSW 5	SW 4	SW 3
27	123.5	122.4	120.6	122.2	1.3	2.6	3.3	2.6	3.6	0.7	98	98	95	97	0.1	0.2	0.4	0.2	10 ●	10 ●	10	WSW 2	SW 5	SW 5
28	114.2	110.5	107.5	110.7	4.0	5.1	4.5	4.5	5.1	2.8	90	83	97	90	0.8	1.5	0.3	0.9	10	10	6	SW 7	SW 5	W 4
29	104.6	103.1	94.5	100.7	3.4	4.4	4.4	4.2	4.7	1.6	90	84	90	88	0.8	1.4	0.9	1.0	10	9	10 ●	SW 7	W 8	WSW 9
30	94.6	93.1	94.8	94.2	3.4	4.6	1.6	2.8	5.2	1.2	90	77	87	85	0.8	1.9	0.9	1.2	9	9	2	W 9	W 7	W 4
31	98.0	98.1	98.6	98.2	1.5	2.1	0.7	1.2	2.6	0.0	83	78	88	83	1.1	1.5	0.7	1.1	9	9	4	W 6	WSW 6	WSW 4
M	112.5	112.5	112.4	112.5	0.1	1.6	0.5	0.7	2.8	-2.2	89	84	88	87	0.7	1.1	0.7	0.8	8.7	8.1	6.1	4.4	5.2	4.3

Szczecin – Dąbie

H_s = 1 m H_b = 6,9 m h_w = 21,5 m

Listopad – Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	
2	7	.	.	–	
3	7	.	.	–	
4	7	.	.	–	por. wiatru do 13 m/sek 19^{35}–20^{25}; = 6^{30}–10^{20} ∞–12^{30}
5	6	.	.	–	= 5^{30}–18^{30}, 21^{30}–22^{30}
6	6	.	.	–	= 3^{30}–24
7	5	0.6	.	–	= 0^{00}–24
8	7	3.6	.	–	●^{0}3^{40} 4^{30}–7^{20} 8^{15}–9^{40} 11$^{10-30}$ 12$^{20-45}$ 14^{35} 15^{05} 18^{40} 19^{10}, = 0^{00}–9^{00}, 23^{30}–24
9	5	2.8	.	–	●^{10}3^{0}–2^{10} 4^{40}, 9^{10} 10^{10}–12^{15}, 17^{15}–20^{15}; = 0^{00}–24
10	6	.	.	–	= 0^{00}–7^{50} ≡^{0}–9^{30} =–19^{30}
11	8	0.0	.	–	●^{0}7^{10}–9^{40}, 14^{45}–15^{05}
12	8	.	.	–	
13	8	.	.	–	
14	7	.	.	–	
15	6	0.0	.	–	= 6^{20}–24
16	5	0.0	.	–	●^{0}5^{30}–7^{40}; = 0^{00}–24
17	7	.	.	–	= 0^{00}–11^{30}
18	7	.	.	–	= 4^{30}–12^{30}
19	7	.	.	–	= 16^{30}–20^{30}
20	8	.	.	–	⌴ 20^{00}–24
21	6	.	.	–	= 6^{30}–19^{30}, 22^{30}–23^{30}, ⌴ 0^{00}–6^{30}
22	6	0.0	.	–	= 6^{15}–24
23	6	1.0	.	–	✱▽3^{20}–25 ●^{0}6^{35}–7^{20} ✱^{0}7^{40}–9^{35} ●^{0}11^{22} 12^{10}; = 0^{00}–13^{20}
24	7	1.4	.	–	
25	6	2.3	.	–	●^{0}4^{05}–6^{10} ●^{0}–9^{40} 10^{45} 12^{10} ●●^{0}–14^{20} ●^{0}–19^{30}, 20^{35}, 21^{45} 24; por. wiatru do 12 m/sek 1^{30}–2^{30}, = 20^{35}–21^{45}
26	6	1.7	.	–	●^{0}0^{00} 6^{30} ●●^{0}–9^{15} ●^{0}–10^{35}; = 7^{30}–24
27	7	3.4	.	–	●^{0}0^{35} 2^{25} ●^{0}3^{15}–4^{40} 7^{20}–8^{35}, 20^{40}–23^{15}; = 0^{00}–5^{30}, 8^{35}–9^{20}
28	7	1.0	.	–	●^{0}0^{15}–2^{10} 6^{10} 8^{30} ●^{0} 9^{20} ●^{0}14^{50}–16^{40} 19^{05}–20^{10}, por. wiatru do 14 m/sek 17^{30}–21^{20}, = 2^{10}–5^{15}
29	8	0.2	.	–	●▽4$^{20-30}$ ✱▽9^{49}–10^{04} 10$^{44-48}$ 11$^{07-12}$, 11^{40}–12^{22} 17$^{48-52}$, 19$^{03-09}$, por. wiatru do 14 m/sek 6^{30} 10^{30}, por. do 16 m/sek 14^{30} 19^{25}
30	8	0.0	.	▲	✱▽7$^{22-29}$, 11^{45}–12^{05}, 20^{50}–21^{10}; = 9^{30}–10^{30}
31					
Σ	–	18.0	–	–	UWAGI.

Grudzień – Décembre

1	5	3.7	.	–	✱^{0}7^{45}–9^{20} ✱^{1}–13^{40} ✱^{0}–14^{30} ●^{0}–15^{30} ●●^{0}–18^{10} ●^{0}–18^{45}, 20^{40}–24; = 18^{45}–24
2	6	0.1	.	–	●^{0}0^{00}–4^{30} 5^{20} 9^{20} = 0^{00}–24
3	5	0.6	.	–	●^{0}5^{40}–11^{25}, 12^{40}–22^{20}, 23^{40}–24; = 0^{00}–24
4	7	0.0	.	–	●^{0}0^{00}–2^{15}, ●^{0}20^{50}–21^{45}, ●^{0}–24; = 0^{00}–7^{30}
5	7	.	.	–	●^{0}0^{00}–2^{40}; = 2^{40}–6^{30} 19^{20}–22^{40} ≡^{0}–23^{30} ≡^{1}–24
6	3	.	.	–	≡^{1}0^{00}–6^{15} ≡^{2}–7^{25} ≡^{1}–9^{15} ≡^{0}–9^{30} =–10^{15} ≡^{0}–14^{30} =–19^{30}
7	5	1.6	.	–	✱●^{0}18^{50}–24; por. wiatru do 12 m/sek 21^{30}–24; = 4^{30}–24
8	6	11.1	.	–	✱●^{0}0^{00}–2^{40}, ●^{0}4^{50}–17^{20}; por. wiatru 12 m/sek 0^{00}–9^{30} ≫ 17^{30}–18^{30} (por. 16 m/sek) por. wiatru 14 m/sek 22^{30}–24; = 0^{00} 17^{20}
9	8	2.3	.	–	●^{0}0^{30} 1^{50} 7^{10}–9^{20} ✱^{0}–11^{12} ✱^{0} 11^{32}–12^{00}; ≫ 0^{00}–4^{30} (por. do 20 m/sek) por. wiatru 14 m/sek – 5^{00}
10	8	1.6	.	–	✱^{0}7^{35}–8^{28} ✱^{1}–10^{35}; ⌴ 10^{00}–7^{35}
11	7	.	3	–	⌴ 5^{30}–7^{30}
12	7	.	4	–	= 16^{25}–24
13	4	0.0	3	–	= 0^{00}–5^{0} ≡^{0}–6^{45} =–11^{30} ≡^{0}–12^{45} =–13^{05} ≡^{0}–21^{40} =–24
14	8	2.1	pł.	–	●^{0}3^{30} 5^{30} ●^{0} 6^{20}, 7^{30}–10^{10}; por. wiatru do 15 m/sek 6^{50}–14^{00} ≫–24 (por. do 18 m/sek); = 0^{00}–6^{20}
15	8	.	.	–	
16	8	.	.	–	⌴ 1^{00}–9^{30}
17	7	.	.	–	⌴ 13^{0}–9^{00}
18	6	0.0	.	–	▲^{0}10^{40}–13^{50}, 23^{35}–24, = 7^{30}–24
19	6	.	.	–	▲ 0^{00}–2^{10} = 0^{00}–24
20	6	0.0	.	–	por. wiatru do 12 m/sek 17^{30}–23^{50} = 0^{00}–20^{30}
21	6	.	.	–	●^{0}0^{05}–3^{40}; = 3^{40}–8^{30}, 11^{30}–24
22	5	.	.	–	= 0^{00}–24
23	7	.	.	–	= 0^{00}–12^{30}, 15^{30}–19^{30}
24	7	.	.	–	
25	7	.	.	–	= 14^{30}–24
26	5	0.0	.	–	= 0^{00}–24
27	4	0.0	.	–	●^{0}5^{35}–15^{20}; = 0^{00}–24
28	7	1.0	.	–	●^{0}13^{50}–14^{40} ●●^{0}–20^{35}; = 0^{00}–12^{10}, 13^{10}–24
29	7	2.5	.	–	●▽10$^{15-20}$ 11$^{07-15}$ ●^{0}16$^{05-45}$ 17^{10}–21^{30}; por. wiatru 14 m/sek 20^{00}–24; = 0^{00}–5^{15}
30	8	3.0	.	–	●^{0}0^{20} 1^{00}–2^{45} 5^{30} 6^{50}, 8$^{15-40}$, 10^{36} 11^{25}, 13^{40}–16^{10}; por. wiatru 14 m/sek 0^{00}–5^{00}
31	8	.	.	–	◡ 22^{35}–23^{15}
Σ	–	29.6	–	–	UWAGI.

Wałcz $\varphi = 53°17'$ $\lambda = 16°28'$ **Styczeń – Janvier 1957**

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	103.0	102.8	102.4	102.7	−6.8	−6.2	−5.4	−6.0	−5.3	−7.1	75	86	87	83	0.9	0.5	0.5	0.6	10	10	10	E 2	N 1	N 1
2	98.8	98.4	100.9	99.4	−3.8	−2.0	−1.1	−2.0	−0.6	−5.5	87	89	93	90	0.6	0.6	0.4	0.5	10	10	10	NE 1	NE 1	C 0
3	105.6	106.2	106.5	106.1	−0.4	0.6	0.0	0.0	1.1	−1.4	92	96	96	95	0.5	0.3	0.2	0.3	10 ≡	10	10	C 0	SE 1	E 1
4	106.9	107.8	108.0	107.6	−0.8	0.9	0.6	0.3	1.5	−2.2	94	83	94	90	0.4	1.1	0.4	0.6	10	10	10	C 0	SE 1	SE 2
5	104.7	100.4	99.9	101.7	1.8	4.4	8.5	5.8	8.6	0.5	98	97	97	97	0.2	0.3	0.3	0.3	10	10 ●	10	S 1	SW 2	WSW 4
6	95.1	94.3	97.1	95.5	9.6	9.0	3.4	6.4	10.0	3.4	93	79	78	83	0.8	2.5	1.7	1.7	10	7	0	SW 8	SW 6	W 6
7	104.2	109.1	113.1	108.8	4.7	5.1	4.9	4.9	5.3	2.9	87	86	81	85	1.1	1.3	1.7	1.4	10 ●	10	10	W 6	W 8	W 6
8	112.2	110.7	109.3	110.7	4.5	5.2	6.8	5.8	6.8	4.0	90	95	97	94	0.8	0.4	0.3	0.5	10	10 ●	10 ●	W 8	WNW 6	W 3
9	106.8	104.3	101.1	104.1	6.8	7.7	7.0	7.1	8.0	6.3	96	84	84	88	0.5	1.6	1.6	1.2	10	10	10	W 3	W 4	W 3
10	98.5	97.1	96.1	97.9	4.4	4.6	2.8	3.6	7.6	2.7	85	73	77	78	1.3	2.3	1.7	1.8	10	10	10	WSW 3	W 6	W 4
11	100.8	105.0	106.3	104.0	1.4	2.8	0.6	1.4	3.2	0.5	89	76	86	84	0.8	1.9	0.8	1.2	7	6	7	W 3	WNW 3	WNW 3
12	99.3	91.9	86.5	92.6	−0.2	1.0	0.4	0.4	1.5	−1.2	88	96	96	93	0.7	0.3	0.3	0.4	10 ✳	10 ✳	10 ✳	W 2	SW 2	SW 2
13	86.8	91.1	98.0	92.0	1.4	0.4	−2.0	−0.6	1.4	−2.0	96	98	89	94	0.3	0.1	0.6	0.3	10 ✳	10 ✳	10 ✳	W 2	N 1	NNE 4
14	106.8	111.2	115.1	111.0	−6.5	−6.9	−9.8	−8.2	−2.0	−9.9	78	74	68	73	0.8	0.9	0.9	0.9	10	9	0	NE 5	NE 3	NE 3
15	115.8	115.2	115.2	115.4	−11.7	−8.2	−11.7	−10.8	−7.9	−12.6	82	75	82	80	0.4	0.8	0.4	0.5	8	8	2	NW 2	N 1	N 1
16	116.7	117.8	118.9	117.8	−12.1	−4.8	−9.6	−9.0	−3.9	−14.8	82	74	82	79	0.4	1.1	0.5	0.7	8	6	1	NW 1	SSW 1	NW 1
17	117.7	118.1	118.0	117.9	−4.4	−1.7	−3.4	−3.2	−1.1	−10.3	86	92	94	91	0.6	0.4	0.3	0.4	10	10	10	WSW 1	WNW 1	NW 1
18	116.5	115.7	113.8	115.3	−2.8	−3.0	−2.7	−2.8	−2.3	−4.1	95	93	91	93	0.2	0.4	0.5	0.4	10	10	10	WNW 1	W 2	SW 1
19	114.4	115.5	116.4	115.4	−1.4	−1.4	−1.5	−1.4	−0.8	−2.9	90	90	94	91	0.5	0.5	0.3	0.4	10	10	10 ●	C 0	NW 1	W 1
20	114.3	112.8	109.8	112.3	−0.5	0.2	−0.4	−0.3	0.4	−1.7	94	92	90	92	0.4	0.5	0.6	0.5	10	10	10	WSW 2	WSW 4	WSW 1
21	106.0	106.6	107.9	106.8	−4.8	−0.6	−1.7	−2.2	0.0	−4.9	86	74	79	80	0.6	1.5	1.1	1.1	0	6	10	SW 2	W 5	SW 1
22	107.4	106.1	103.7	105.7	−7.6	−1.8	−4.9	−4.8	−0.8	−7.6	79	69	71	73	0.7	1.7	1.2	1.2	0	4	0	SW 1	SW 1	S 1
23	103.6	104.5	104.0	104.0	−4.2	−0.3	−6.4	−4.3	0.3	−6.8	82	61	81	75	0.8	2.4	0.7	1.3	10	0	0	SW 2	SSW 2	C 0
24	100.1	97.4	95.2	97.6	−5.2	−1.7	−2.6	−3.0	−1.3	−8.3	80	75	85	79	0.8	1.5	0.8	1.0	9	10	5	SE 1	NE 1	E 1
25	93.4	94.8	98.4	95.5	−4.0	−1.0	0.8	−0.8	0.8	−4.1	89	81	94	88	0.5	1.1	0.4	0.7	10	10	10	NE 1	S 1	SW 1
26	103.1	103.9	99.7	102.2	0.5	2.4	1.5	1.5	2.7	0.2	96	80	70	82	0.2	1.5	2.0	1.2	10	1	10	S 1	SSE 2	S 4
27	97.0	99.3	103.1	99.8	3.0	5.0	2.2	3.1	5.6	1.3	95	81	82	86	0.4	1.6	1.3	1.1	10 ●	5	1	W 2	WSW 4	WSW 2
28	102.9	109.2	115.0	109.0	0.6	1.4	0.3	0.6	2.2	0.3	94	94	92	93	0.4	0.4	0.5	0.4	10 ●	10	0	SW 3	SW 3	W 1
29	115.3	114.1	112.7	114.0	−0.2	0.9	1.6	1.0	1.7	−2.0	92	92	94	93	0.5	0.5	0.4	0.5	8	10	10	NW 1	SW 2	SW 1
30	108.9	107.2	106.7	107.6	−0.8	1.4	1.2	0.8	1.6	−1.1	89	87	89	88	0.6	0.9	0.8	0.8	7	10	10	C 0	SW 2	C 0
31	106.3	107.5	106.6	106.8	0.7	1.3	0.8	0.9	1.7	0.5	96	96	96	96	0.2	0.2	0.3	0.2	10 ≡	10	10	C 0	SW 1	C 0
M	105.4	105.7	106.0	105.7	−1.2	0.5	−0.6	−0.5	1.5	−2.8	89	84	87	87	0.6	1.0	0.8	0.8	8.9	8.5	7.3	2.1	2.5	1.9

Luty – Février

1	101.1	100.0	99.9	100.3	1.4	3.8	6.7	4.6	6.7	0.7	98	98	100	99	0.2	0.1	0.0	0.1	10 ≡	10	10 ●	C 0	E 1	SE 2
2	104.8	108.7	111.1	108.2	7.9	8.0	4.4	6.2	9.5	4.4	93	67	90	83	0.7	3.5	0.9	1.7	8	8	10	SW 4	SW 3	WSW 1
3	111.3	112.9	113.0	112.4	2.4	3.5	−1.2	0.9	6.5	−1.2	98	95	94	96	0.2	0.4	0.4	0.3	10	9	0	C 0	NW 1	S 1
4	109.9	107.4	107.5	108.3	0.6	2.8	3.0	2.4	5.0	−1.9	96	96	98	97	0.3	0.3	0.2	0.3	10	10	10 ≡	E 2	SE 1	C 0
5	106.8	105.1	103.3	105.1	1.2	9.2	5.2	5.2	10.2	−0.4	98	81	94	91	0.2	2.1	0.5	0.9	10 ≡	9	4	SW 1	S 1	C 0
6	100.2	97.3	96.8	98.1	0.4	7.7	6.6	5.3	8.8	0.3	94	73	87	85	0.4	2.8	1.3	1.5	3	7	10	C 0	SSE 3	C 0
7	100.0	99.9	101.4	100.4	4.2	7.5	4.5	5.2	8.0	4.0	87	72	82	80	1.0	3.0	1.5	1.8	5	3	0	W 1	SW 6	W 2
8	97.1	91.9	87.3	92.1	1.4	4.9	6.6	4.9	6.6	1.1	94	94	96	95	0.4	0.6	0.4	0.5	10	10 ●	10 ●	S 1	S 2	WSW 2
9	85.3	85.0	88.4	86.2	6.6	7.4	6.5	6.8	8.4	6.0	91	88	64	81	0.8	1.2	3.6	1.9	10	10	6	SSW 1	W 3	SW 8
10	91.5	92.5	92.0	92.0	1.4	6.0	4.3	4.0	7.0	1.1	91	70	88	83	0.7	2.9	1.0	1.5	10	7	10	W 2	WSW 2	SE 1
11	92.7	96.7	98.9	96.1	3.9	3.5	0.5	2.1	4.3	0.5	93	85	80	86	0.6	1.2	1.2	1.0	10	10	4	W 3	W 4	WSW 2
12	96.3	92.4	88.8	92.6	0.5	3.3	4.3	3.1	6.0	−0.4	92	88	87	89	0.5	0.9	1.1	0.8	10	10 ●	C 0	SE 2	S 3	
13	85.4	80.8	71.7	79.3	1.8	6.7	5.4	4.8	7.7	1.7	83	72	97	84	1.2	2.7	0.3	1.4	10	6	10 ●	S 2	S 3	E 4
14	69.7	70.7	72.0	70.8	5.2	7.1	4.8	5.5	7.4	4.8	84	85	95	88	1.4	1.5	0.4	1.1	7	10	6	S 2	SW 3	SW 2
15	72.4	71.6	69.3	71.2	3.4	5.2	3.8	4.0	6.5	3.0	93	77	95	88	0.5	2.0	0.4	1.0	10	8	10	SSW 2	E 2	N 2
16	76.1	80.0	84.5	80.2	2.8	3.6	1.4	2.3	4.6	1.4	95	75	91	87	0.4	2.0	0.7	1.0	10	9	0	W 1	WSW 1	S 1
17	89.4	91.0	89.4	89.9	0.9	3.0	1.2	1.6	4.3	−0.2	90	79	94	88	0.6	1.6	0.4	0.9	10	9	10	SW 1	S 2	E 1
18	91.8	90.0	85.5	89.1	0.6	6.4	3.9	3.7	6.7	0.5	94	60	90	81	0.4	3.8	0.6	1.7	10	6	10	C 0	E 1	NE 2
19	87.6	92.9	96.5	92.3	2.2	2.8	0.1	1.3	3.9	0.1	86	74	88	83	1.1	2.0	0.8	1.3	10	10	10	W 2	W 4	W 1
20	96.6	96.0	93.3	95.3	−0.1	1.5	1.9	1.3	2.0	−0.7	96	96	89	94	0.3	0.3	0.8	0.5	10	10	10	S 1	SSE 2	NE 1
21	92.1	94.0	99.0	95.0	1.8	6.4	1.7	2.9	7.0	1.3	93	88	85	89	0.6	1.1	1.0	0.9	10	9	10	E 1	SW 2	W 3
22	102.2	102.1	100.2	101.5	−0.5	2.9	0.8	1.0	4.5	−0.7	92	79	83	85	0.5	1.6	1.2	1.1	10	5	10	SW 1	SW 2	W 1
23	100.0	100.1	99.4	99.8	−2.4	1.1	−1.5	−1.1	2.1	−2.6	91	74	86	84	0.4	1.7	0.8	1.0	10	8	0	W 1	W 3	NW 1
24	93.2	90.4	91.1	91.6	−4.7	1.4	−1.7	−1.7	2.4	−5.4	81	69	82	77	0.8	2.2	1.0	1.3	2	8	0	C 0	NE 2	N 1
25	95.1	94.4	94.6	94.7	−6.4	−0.4	−1.8	−2.6	1.0	−6.3	81	74	86	80	0.7	1.5	0.8	1.0	0	10	0	C 0	ENE 2	E 1
26	101.5	104.0	106.1	103.9	−6.2	1.9	−1.9	−2.0	3.0	−6.5	86	57	83	75	0.5	3.0	0.9	1.5	1	3	0	C 0	E 2	C 0
27	108.1	109.8	112.0	110.0	−4.1	3.5	0.2	0.0	4.0	−4.6	87	57	78	74	0.6	3.4	1.4	1.8	1	1	10	C 0	SE 2	E 1
28	116.4	119.5	122.4	119.4	−1.6	1.0	−1.9	−1.1	1.6	−1.9	88	79	87	85	0.6	1.4	0.7	0.9	10	8	0	E 1	WNW 1	NW 1
29																								
30																								
31																								
M	95.5	95.6	95.6	95.6	0.9	4.3	2.4	2.5	5.6	−0.1	91	79	88	86	0.6	1.8	0.9	1.1	8.1	8.0	6.4	1.1	2.2	1.6

DNI	WIATR DZIAŁALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	5	–	= 10^{20} – 13^{40}
2	6	.	5	–	= 10^{10} – n
3	5	.	4	–	≡^{0} n – 8^{30} = – n
4	7	.	4	–	= n – 12^{30} 15^{20} – n
5	6	12.3	3	–	•^{0} 9^{10} – 12^{25} •^{0} 12^{35} – 15^{17} •^{0} 15^{40} … 17^{30} •^{0} – 18^{28} ; = n – n
6	7	6.7	.	–	•^{0} 8^{30} – 10^{28}
7	7	0.2	.	–	•^{0} n – 7^{42}
8	6	0.9	.	–	•^{0} 11^{22} 12^{40} – 19^{15} •^{0} 19^{40} – n
9	7	.	.	–	• n
10	7	0.0	.	–	⛆ 15^{11} – 40
11	7	0.4	.	–	
12	6	7.3	.	–	*^{0} 6^{18} – 12^{10} ⁂^{0} – 14^{05} *^{0} – 14^{43} 18^{35} – 19^{40} ⁂^{0} – n ; = n – n
13	5	10.8	.	–	•^{0} n – 5^{20} ⁂^{0} – 7^{30} •^{0} – 8^{15} ⁂^{0} – 9^{40} ⁂ – 10^{45} *^{1} – 11^{18} *^{0} – 16^{05} ⁂^{0} – 17^{32} •^{0} – 18^{15} △ 18^{20} – 19^{04} *^{0} – n
14	7	0.2	3	–	*^{0} 9^{17} – 11^{07}
15	7	.	3	–	
16	7	0.1	3	–	*^{0} 9^{13} … 12^{35}
17	5	.	3	–	= 7^{20} – n
18	6	.	3	–	= n – n
19	6	0.2	3	–	•^{0} 19^{12} – n ; = 7^{10} – n
20	6	.	2	–	•^{0} n ; = n – 14^{40}
21	7	.	2	–	= 15^{30} – n
22	7	.	2	–	
23	7	.	1	–	
24	7	.	1	–	
25	7	0.1	1	–	*^{0} 8^{10} – 9^{22} ; = 6^{15} – 10^{30} , 14^{10} – n
26	7	2.4	1	–	= n – 12^{40}
27	7	3.2	.	–	• n •^{0} 5^{11} – 6^{15} •^{0} – 7^{22} ; = n – 11^{40}
28	7	0.6	.	–	* n •^{0} 6^{15} – 7^{10} ⁂^{0} – 8^{22} , 9^{52} – 10^{30} ; = 5^{20} – a
29	6	.	.	–	= 9^{15} – n
30	7	.	.	–	= 14^{15} – 20^{00}
31	7	.	.	–	= n – 5^{50} ≡^{0} – 10^{40} = – n
Σ	–	45.4	–	–	UWAGI.

Luty – Février

1	5	6.9	.	–	•^{0} 14^{15} – 15^{05} •^{0} – 16^{25} •^{0} – n ; ≡^{1} n – 9^{40} = – n
2	7	.	.	–	• n
3	6	0.6	.	–	•^{0} 10^{18} – 11^{40} 11^{50} … 12^{42} ; = n – 7^{59} ≡^{0} – 9^{48} = – 12^{20}
4	4	4.6	.	–	•^{0} 7^{24} … 8^{16} – 11^{18} ; = a – 16^{55} ≡^{0} – 17^{35} ≡^{1} – n
5	7	.	.	–	≡^{1} n – 6^{45} ≡^{0} – 7^{20} ≡^{1} – 9^{18} ≡^{0} – 9^{37} = – 12^{15}
6	7	.	.	–	= n – 8^{20}
7	8	.	.	–	
8	6	6.1	.	–	•^{0} 9^{10} … 10^{30} •^{0} 11^{12} , 12^{40} … 14^{15} , 14^{35} – n
9	7	.	.	–	• n
10	7	7.0	.	–	
11	7	.	.	–	• n •^{0} 5^{10} – 6^{25} ; = n – 10^{00}
12	6	1.0	.	–	•^{0} 13^{35} – 15^{10} , 18^{30} – n ; = 9^{30} – n
13	7	7.8	.	–	• n •^{0} 19^{08} – n ; = n – 6^{15}
14	7	3.1	.	–	•^{0} 11^{19} – 12^{35} ▽^{0} 13^{50} – 14^{05} ▽^{1} 14^{38} – 15^{11}
15	7	1.4	.	–	• n •^{0} 16^{22} – 20^{35}
16	7	0.2	.	–	• n •^{0} 19^{15} – 10^{22}
17	7	1.0	.	–	⁂^{0} 19^{11} – 20^{32} ; = 5^{30} – 9^{20}
18	7	1.3	.	–	= n – 8^{30} ≡^{0} – 9^{50} = – 10^{25}
19	7	.	.	–	• n
20	6	1.8	.	–	*^{0} 7^{28} – 11^{40} ; = 6^{15} – 20^{30}
21	7	0.0	.	–	•^{0} 16^{13} … 42
22	7	1.1	.	–	
23	7	.	1	–	* n ; = 6^{15} – 8^{40}
24	7	.	.	–	⌴^{1} n – 9^{30}
25	7	.	.	–	⌴^{2} n – 9^{00}
26	8	.	.	–	⌴^{2} n – 10^{00}
27	7	2.0	.	–	⌴^{1} n – 8^{00}
28	7	0.8	2	–	* n *^{0} 10^{22} – 12^{40}
29					
30					
31					
Σ	–	46.7	–	–	UWAGI.

Wałcz $\varphi = 53°17'$ $\lambda = 16°28'$ **Marzec – Mars 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	123.9	123.3	122.3	123.2	-6.3	2.0	-2.2	-2.2	3.6	-6.5	83	54	83	73	0.6	3.3	0.9	1.6	0	3	0	NW 1	NW 2	C 0
2	120.6	116.3	115.2	116.0	-6.7	2.7	-2.7	-2.4	4.0	-7.0	80	69	82	77	0.7	2.3	0.9	1.3	1	4	0	C 0	NW 1	WNW 1
3	112.2	108.7	105.8	108.9	-7.0	2.8	0.0	-1.0	4.0	-7.2	80	54	86	74	0.7	3.5	0.7	1.6	1	1	0	NW 1	NE 2	SE 2
4	99.3	96.6	96.4	97.4	-2.2	1.4	1.0	0.3	2.4	-2.2	89	83	90	87	0.6	1.1	0.7	0.8	10	10	3	SSW 1	W 1	W 2
5	99.4	100.8	101.7	100.6	-1.5	3.7	-1.8	-0.4	5.5	-2.4	92	67	73	77	0.4	2.7	1.4	1.5	10	1	0	C 0	W 2	C 0
6	101.3	100.5	99.6	100.5	-5.6	6.4	-1.8	-0.7	7.6	-5.9	82	38	75	65	0.7	5.9	1.3	2.6	0	1	0	C 0	E 1	C 0
7	100.0	100.4	101.4	100.6	-4.1	1.6	-2.0	-1.6	2.8	-4.2	75	58	71	68	1.1	2.9	1.6	1.9	0	8	0	C 0	NE 2	NE 4
8	102.8	104.1	107.6	104.8	-4.6	2.4	-2.6	-1.8	2.7	-4.9	84	58	77	73	0.7	3.1	1.2	1.7	0	0	0	E 3	ENE 6	NE 4
9	112.4	114.7	116.7	114.6	-5.4	3.0	-0.8	-1.0	4.2	-5.8	77	66	77	73	0.9	2.6	1.3	1.6	0	0	0	NE 2	NE 4	NE 1
10	119.0	119.5	119.6	119.4	-5.4	6.0	0.2	0.2	7.0	-6.0	77	43	65	62	0.9	5.4	2.2	2.8	0	0	0	ENE 1	NE 2	C 0
11	119.2	118.8	115.3	117.8	-3.4	8.6	1.7	2.2	10.2	-3.5	79	34	74	62	1.0	7.4	1.8	3.4	0	1	0	C 0	E 2	E 1
12	111.0	108.2	106.1	108.4	1.0	12.8	2.2	4.6	14.6	-1.2	79	37	77	64	1.4	9.4	1.7	4.2	8	3	0	S 1	W 2	C 0
13	105.3	104.4	100.7	103.5	-1.0	15.4	8.4	7.8	17.0	-1.1	89	31	55	58	0.7	12.0	5.0	5.9	0	0	0	C 0	W 2	SW 1
14	95.2	93.9	93.4	94.2	5.2	9.9	8.2	7.9	12.4	0.5	78	78	63	73	1.9	2.7	4.0	2.9	0	9	10	N 2	WNW 7	WNW 8
15	95.7	94.9	87.7	92.8	5.1	5.6	5.1	5.2	8.7	4.7	64	94	94	84	3.2	0.6	0.6	1.5	6	10 ●	10 ●	WNW 6	W 3	W 6
16	91.6	97.6	103.2	97.5	0.4	-0.4	-4.4	-2.2	5.1	-4.5	88	53	70	70	0.8	2.8	1.3	1.6	9	7	8	WNW 3	WNW 3	NNE 2
17	100.4	96.4	86.0	94.3	-4.0	-3.1	0.2	-1.7	0.2	-4.9	70	81	92	81	1.3	0.9	0.5	0.9	10	10	10	NE 2	E 4	E 2
18	78.2	79.6	85.3	81.0	6.8	8.9	5.2	6.5	10.0	-0.3	97	77	84	86	0.3	2.6	1.4	1.4	10 ●	10 ●	8	W 3	W 8	W 7
19	92.5	93.6	94.4	93.5	1.4	6.1	4.4	4.1	7.0	1.3	96	94	100	97	0.3	0.6	0.0	0.3	10 ❟	10	10	NW 1	N 1	NE 1
20	95.8	93.2	89.6	92.9	2.4	7.1	6.7	6.7	10.7	2.2	98	99	88	95	0.2	0.2	1.3	0.6	10 ❟	10 ≡	9	E 2	E 1	SSE 1
21	93.2	96.0	97.0	95.4	6.6	9.8	5.4	6.8	10.2	5.4	88	59	77	75	1.1	4.9	2.1	2.7	8	8	0	W 4	SW 6	SW 1
22	100.0	101.9	104.2	102.0	3.6	9.1	3.1	4.7	10.4	2.8	88	48	61	72	0.9	6.0	1.4	2.8	9	8	0	WNW 2	WNW 5	WNW 1
23	105.9	106.0	109.3	107.1	-1.2	11.4	0.4	2.8	12.4	-2.2	89	47	78	71	0.6	7.1	1.4	3.0	1	0	0	C 0	E 2	NE 8
24	112.0	111.7	111.0	111.6	-2.6	3.8	1.6	1.1	4.0	-3.0	67	39	81	62	1.7	4.9	1.3	2.6	8	9	10	ENE 7	ENE 8	ENE 8
25	110.1	109.5	109.3	109.6	-0.1	2.1	2.6	1.8	4.4	-0.3	88	78	79	82	0.8	1.5	1.6	1.3	10	10	0	ENE 8	ENE 5	E 4
26	107.7	105.7	104.9	106.1	1.8	11.3	8.7	7.6	14.0	1.3	82	64	72	73	1.3	4.8	3.1	3.1	10	9	0	E 2	E 2	E 1
27	105.8	103.7	104.7	105.4	3.5	14.8	8.9	9.0	15.5	2.7	80	43	61	61	1.5	9.6	4.5	5.2	2	2	0	ESE 2	SE 3	C 0
28	101.0	101.2	100.7	101.0	4.9	6.2	4.9	5.2	8.5	4.2	81	83	94	86	1.7	1.6	0.6	1.3	9	10	10	SE 2	SSE 2	S 1
29	100.4	101.2	102.6	101.4	3.9	5.1	4.4	4.4	5.6	3.4	97	97	100	98	0.3	0.3	0.0	0.2	10	10 ●	10	C 0	NW 1	NW 1
30	105.4	106.5	107.8	106.6	5.1	12.7	7.1	8.0	14.8	2.6	94	60	84	79	0.6	5.9	1.6	2.7	10	9	0	NNE 1	ENE 2	NE 1
31	108.1	108.2	109.9	108.7	3.2	14.4	7.6	8.2	15.2	0.7	91	53	66	77	0.7	7.8	1.4	3.3	1	0	0	NE 1	E 1	C 0
M	104.0	103.9	103.5	103.8	-0.2	6.6	2.6	2.9	8.2	-1.3	84	63	80	76	1.0	4.1	1.6	2.2	5.3	5.6	3.2	1.9	3.0	2.2

Kwiecień – Avril

1	109.9	108.8	107.9	108.9	2.4	17.1	9.4	9.6	17.4	-0.1	91	27	59	59	0.7	14.2	4.9	6.6	0	0	0	N 1	ENE 3	NE 1
2	107.0	106.1	107.9	107.0	4.4	16.3	12.3	11.3	17.9	3.2	80	43	67	63	1.7	10.6	4.7	5.7	8	3	10	NE 2	NE 3	E 1
3	110.5	112.4	114.3	112.4	7.5	18.6	10.1	11.6	19.7	5.7	73	37	77	62	2.8	13.5	2.9	6.4	3	3	8	NNE 2	ESE 2	C 0
4	116.7	116.3	116.0	116.3	3.8	20.2	9.4	10.7	21.4	2.4	92	36	74	67	0.7	15.2	3.1	6.3	1	1	0	NE 1	C 0	C 0
5	114.5	111.3	105.8	110.5	3.2	20.1	12.1	11.9	21.1	1.2	86	33	61	60	1.1	15.7	5.6	7.5	0	3	0	C 0	E 1	C 0
6	99.8	96.4	97.5	97.9	6.0	19.0	6.2	9.4	19.6	3.0	79	35	83	66	2.0	14.4	1.6	6.0	1	8	10	W 1	W 2	NW 2
7	97.5	101.2	107.2	102.0	3.0	3.0	0.6	1.8	6.7	0.5	95	90	69	85	0.4	0.8	2.0	1.1	10	10 ●	0	NW 2	NW 6	NW 4
8	108.7	106.0	103.4	106.0	-1.8	7.1	4.6	3.6	8.1	-3.9	79	43	59	60	1.1	5.8	3.5	3.5	0	6	8	NW 1	NW 3	WNW 1
9	100.3	100.1	99.3	99.9	2.3	6.8	1.3	2.9	7.6	1.3	86	56	68	70	1.0	4.4	2.1	2.5	10	10	7	NW 1	NNE 1	N 1
10	93.6	87.4	82.8	87.9	-0.4	11.2	5.3	5.4	13.2	-2.4	70	46	77	64	1.8	7.2	2.1	3.7	7	8	8	SE 1	SW 4	SW 1
11	80.6	82.3	90.0	84.3	1.7	4.3	0.4	1.7	6.0	0.4	76	68	84	76	1.6	2.7	1.0	1.8	0	10	10	W 2	W 5	NW 2
12	94.8	95.8	98.3	96.3	0.3	3.4	-1.4	0.2	4.3	-1.9	82	63	81	75	1.1	2.9	1.1	1.7	8	8	0	C 0	W 3	C 0
13	99.4	101.1	103.2	101.2	-2.2	3.3	-1.4	-0.4	5.0	-3.9	80	65	88	78	1.1	2.7	0.6	1.5	3	6	10	C 0	N 2	W 1
14	104.5	103.9	105.8	104.7	-1.6	6.4	-0.8	0.8	7.0	-3.9	86	42	79	69	0.7	5.5	1.2	2.5	8	9	1	SW 1	W 4	NW 1
15	108.1	108.1	109.1	108.4	-2.2	4.9	1.6	1.5	6.5	-3.5	85	43	81	70	0.8	5.0	1.3	2.4	0	8	7	NW 1	W 2	C 0
16	108.1	105.3	104.8	106.1	0.3	8.7	7.6	6.0	9.9	-2.4	90	81	93	88	0.6	2.1	0.7	1.1	10	10	10	SE 1	WSW 2	W 1
17	106.3	107.7	108.7	107.6	5.4	5.7	4.3	4.9	7.7	4.2	91	91	85	89	0.9	0.9	1.2	1.0	9	10 ❟	10	WNW 2	W 3	N 1
18	107.8	106.4	104.4	106.2	1.4	5.1	4.4	3.6	6.8	0.7	87	75	84	82	0.9	2.2	1.4	1.5	8	10	8	NW 2	N 2	WNW 1
19	101.0	99.0	100.0	100.0	3.6	8.8	5.8	6.0	9.7	3.0	91	60	94	82	0.7	4.5	0.6	1.9	10	10	10 ●	NE 2	SE 2	W 2
20	105.0	108.8	111.6	108.5	4.9	7.3	3.4	4.8	7.8	3.2	81	72	88	80	1.7	2.9	0.9	1.8	10	10	4	W 4	WNW 3	NNW 1
21	114.3	115.4	116.0	115.2	3.1	6.0	3.8	4.2	9.0	1.3	84	77	90	84	1.2	2.2	0.8	1.4	10	10	0	NNW 1	NW 2	NW 1
22	117.8	117.8	117.6	117.7	4.2	10.3	5.6	6.5	11.8	0.7	85	44	78	69	1.2	7.1	2.0	3.4	0	8	8	WNW 1	ESE 1	NE 1
23	117.8	116.9	117.3	117.3	-0.7	12.6	6.7	6.3	13.5	-1.6	98	44	84	75	0.1	8.1	1.6	3.3	10 ≡	2	0	C 0	WNW 2	NE 1
24	116.8	116.2	115.1	116.0	1.8	13.4	8.2	7.9	13.7	-0.7	85	46	83	71	1.1	8.4	1.8	3.8	0	8	7	NNW 1	N 2	N 1
25	112.7	111.8	111.1	111.9	4.9	10.1	6.3	6.9	12.3	3.8	81	67	79	76	1.7	4.1	2.0	2.6	10	9	9	NW 2	N 4	NNE 2
26	109.9	108.6	108.0	108.8	4.9	16.7	11.8	11.3	19.4	3.7	95	57	75	76	0.5	8.2	3.4	4.0	10	8	9	NNE 1	NNE 1	N 1
27	105.8	103.8	100.6	103.4	8.3	19.6	13.5	13.7	20.8	6.7	82	55	82	73	2.0	10.4	2.8	5.1	10	10	8	C 0	E 1	WNW 1
28	98.4	96.3	95.1	96.6	10.1	22.6	13.2	14.8	22.7	7.5	91	51	82	75	1.2	13.3	2.8	5.8	3	5	1	NE 1	E 1	E 1
29	96.2	97.3	98.1	97.2	11.2	20.9	14.1	15.1	22.7	7.6	90	53	80	74	1.3	11.6	3.2	5.4	10	5	0	NW 1	NW 2	C 0
30	97.6	96.5	99.7	97.9	7.1	12.2	6.0	7.8	14.1	6.0	96	79	82	86	0.5	3.0	1.8	1.8	10	10	0	C 0	NW 2	WNW 3
31																								
M	103.4	104.8	105.2	103.1	3.2	11.4	6.1	6.7	12.8	1.3	86	56	79	74	1.1	7.0	2.1	3.4	6.0	7.3	5.4	1.2	2.4	1.1

Wałcz $H_s = 111\,m$ $H_b = 113{,}8\,m$ $h_w = 10\,m$ **Marzec – Mars 1957**

DNI	WILGOTNOŚĆ WZGLĘDNA V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	1	–	
2	8	.	.	–	
3	7	.	.	–	
4	6	1.1	.	–	$\bullet^{0}\,17^{11}-12^{42}$, $\bullet^{0}\,15^{30}-17^{40}$ $\ast^{0}-18^{22}$ $\bullet^{0}-20^{10}$, $= a-p$
5	8	.	.	–	$= n-10^{20}$
6	8	.	.	–	
7	8	.	.	–	
8	8	.	.	–	
9	8	.	.	–	
10	8	.	.	–	
11	8	.	.	–	
12	8	.	.	–	
13	8	.	.	–	
14	7	.	.	–	$\gg n-n$
15	6	13.1	.	–	$\bullet^{0}\,11^{41}-n$, $\gg 5^{18}-6^{40}$, $p-20^{30}$
16	7	.	.	–	
17	6	7.8	.	–	$\ast^{0}\,8^{35}$ $10^{10}-12^{35}$ $\bullet^{0}\,15^{20}-19^{35}$ $\bullet^{0}\,19^{40}-n$, $\backsim\ 15^{20}-n$
18	6	8.7	.	–	$\bullet^{0}\,n-7^{36}$ $\triangledown\ 12^{38}-13^{34}$ $14^{06}-35$ $15^{15}-37$ $16^{43}-17^{10}$ $17^{50}-18^{33}$
19	6	3.4	.	–	$\bullet^{0}\,n-5^{20}$ $\bullet^{0}\,6^{15}-8^{35}$, $10^{40}-12^{10}$ $\bullet^{0}\,15^{25}-18^{30}$ $\bullet^{0}\,18^{45}-n$, $= n-n$
20	2	0.7	.	–	$\bullet^{0}\,n-10^{30}$, $= n-11^{50}$ $\equiv^{1}-13^{50}$ $\equiv^{2}-14^{50}$ $=-17^{20}$
21	7	.	.	–	
22	7	.	.	–	
23	8	.	.	–	$= 7^{20}-8^{40}$, $\llcorner^{0}\,n-7^{30}$
24	7	0.6	.	–	$\gg 5^{30}-n$
25	7	.	.	–	$\bullet\ n$
26	7	.	.	–	
27	7	.	.	–	
28	6	1.2	.	–	$\bullet^{0}\,7^{35}$ $8^{50}-10^{20}$, $= 12^{20}-n$
29	6	8.5	.	–	$\bullet^{0}\,9^{32}-17^{18}$, $17^{40}-20^{10}$, $= n-n$
30	7	.	.	–	$= n-10^{50}$
31	7	.	.	–	
Σ	–	47.1	–	–	UWAGI

Kwiecień – Avril

1	7	.	.	–	
2	7	.	.	–	
3	7	.	.	–	
4	8	.	.	–	$\frown^{0}\,7^{40}$
5	7	.	.	–	$\frown^{0}\,n-7^{50}$
6	8	.	.	–	
7	6	0.4	.	–	$\bullet^{0}\,12^{05}-13^{30}$ $\triangledown\ 14^{10}-13$, $14^{22}-40$, $\frown^{0}\,n-8^{20}$
8	7	.	.	–	
9	7	.	.	–	$\supset^{1}\,20^{30}-23^{22}$
10	7	.	.	–	$\llcorner^{2}\,n-7^{50}$
11	7	0.0	.	–	$\ast\ 13^{15}-27$ $15^{10}-15$
12	7	0.3	.	–	$\ast\ 11^{06}-36$ $16^{11}-23$
13	7	0.0	.	–	$\ast^{0}\,3^{50}$ 5^{20} $\ast\ 17^{25}-31$
14	7	0.0	.	–	$\ast\ 13^{13}-20$ $13^{37}-42$, $15^{04}-15$
15	7	.	.	–	$\llcorner\ n-7^{25}$
16	7	4.8	.	–	$\ast^{0}\,7^{38}-9^{10}$ $\bullet^{0}-9^{45}$ $13^{40}-15^{10}$ 16^{15} , 17^{40} 24
17	6	0.0	.	–	$\bullet^{0}\,0^{00}$ 1^{18} $\bullet^{0}\,12^{15}-13^{40}$
18	7	.	.	–	
19	7	2.5	.	–	$\bullet^{0}\,16^{16}$ 24 $= 6^{10}-7^{40}$
20	7	.	.	–	$\bullet^{0}\,0^{00}$ $15^{0}-3^{20}$
21	7	.	.	–	
22	7	.	.	–	
23	8	.	.	–	$= 3^{50}-4^{50}$ $\equiv^{1}-8^{40}$ $=-9^{30}$
24	7	.	.	–	$\llcorner^{0}\,n$
25	7	5.1	.	–	$\bullet^{0}\,8^{17}-10^{15}$
26	7	.	.	–	$\bullet^{0}\,0^{12}-6^{35}$, $= n-8^{30}$
27	8	3.4	.	–	$\bullet^{2}\,\mathrm{K}\ 15^{17}-15^{27}$ 16^{04} NE – NW $\bullet^{0}\,\mathrm{K}\ 22^{06}-10-18$ NW – NNE
28	7	0.1	.	–	$\triangledown\ 14^{57}-15^{17}$ · $(\mathrm{K})^{0}\ 13^{45}-13^{59}-14^{40}$ E – W , $= 3^{50}-6^{40}$
29	7	.	.	–	$\frown^{2}\,n-7^{30}$
30	7	0.4	.	–	$\bullet^{0}\,7^{05}-35$, $15^{23}-16^{18}$, $= 0^{50}-4^{40}$ $\equiv^{1}-6^{25}$ $=-7^{50}$
31					
Σ	–	17.0	–	–	UWAGI

Wałcz — φ = 53°17' — λ = 16°28' — Maj – Mai 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	104.3	103.7	103.3	103.1	5.2	10.1	5.6	6.6	12.8	1.9	81	48	75	68	1.6	6.5	2.2	3.4	2	7	0	W 1	NW 3	NW 1
2	104.4	102.8	100.7	102.6	5.9	11.9	9.6	9.2	12.6	2.7	73	45	74	64	2.5	7.6	3.2	4.4	10	9	10	ESE 1	SE 1	C 0
3	99.0	97.0	94.9	97.0	8.2	13.4	7.8	9.3	14.0	7.5	62	61	73	65	4.2	6.0	2.8	4.3	10	9	2	S 1	SW 1	WSW 2
4	93.3	95.1	96.8	95.1	5.1	8.0	3.8	5.2	9.5	3.7	73	71	60	68	2.4	3.1	3.2	2.9	10	9	4	W 8	W 10	W 8
5	95.7	94.7	93.8	95.4	2.8	9.4	2.8	4.4	9.9	1.9	74	40	81	65	2.0	7.1	1.5	3.5	10	6	4	WSW 8	W 7	W 1
6	96.1	95.7	95.6	95.9	1.5	5.7	3.4	3.5	6.8	−0.6	91	59	91	80	0.6	3.8	0.7	1.7	7	10	10 ●	C 0	E 2	NE 1
7	94.9	95.0	96.3	95.4	3.4	8.5	3.7	4.8	9.7	2.4	91	61	85	79	0.7	4.3	1.2	2.1	10	8	10	C 0	N 1	NNW 1
8	95.9	95.3	96.4	95.9	2.8	5.6	4.0	4.1	6.3	0.3	81	77	77	78	1.5	2.1	1.9	1.8	10	10	10	WNW 2	NW 3	NW 2
9	98.6	99.6	100.5	99.6	4.0	9.7	6.5	6.7	10.8	1.8	79	54	90	74	1.7	5.5	1.0	2.7	10	8	10 ●	WNW 1	N 2	NNE 1
10	98.9	98.9	99.2	99.0	4.3	6.6	5.8	5.6	7.6	2.6	87	82	86	85	1.1	1.7	1.3	1.4	10	10	10	N 2	WNW 3	WNW 1
11	99.4	100.8	100.7	100.3	5.9	11.2	8.8	8.7	15.6	4.8	86	55	80	74	1.3	6.0	2.3	3.2	10	5	1	WNW 1	SW 1	NE 1
12	100.8	100.4	101.6	100.9	8.2	21.4	15.3	15.0	22.7	3.6	83	34	48	55	1.8	16.9	9.0	9.2	0	6	4	ENE 1	E 4	ESE 1
13	103.1	103.1	103.2	103.1	14.4	22.2	14.1	16.2	23.7	8.6	74	36	77	62	4.3	17.2	3.7	8.4	2	8	9	C 0	SSW 2	ESE 1
14	104.5	105.6	107.5	105.9	13.1	19.4	11.9	14.1	20.7	8.9	79	43	87	70	3.1	12.8	1.8	5.9	1	7	0	W 1	SSW 4	C 0
15	109.4	108.9	107.1	108.5	11.6	20.6	15.1	15.6	22.2	5.3	90	41	62	64	1.3	14.2	6.5	7.3	0	2	0	WNW 1	E 1	E 1
16	105.4	102.6	101.1	103.0	14.2	22.9	18.0	18.3	24.1	9.2	61	35	54	50	6.3	18.1	9.4	11.3	1	5	4	ENE 2	E 7	ENE 2
17	103.5	105.8	106.3	105.2	11.6	14.2	10.9	11.9	18.0	9.8	84	75	79	79	2.1	4.1	2.7	3.0	9	10	10	W 3	NW 4	C 0
18	106.1	105.2	102.1	104.5	12.3	20.8	13.8	15.2	21.7	9.4	81	41	69	64	2.7	14.6	4.9	7.4	6	5	2	C 0	ESE 1	C 0
19	99.1	96.5	94.1	96.6	14.5	24.8	18.5	19.1	26.4	8.0	66	47	68	60	5.7	16.5	6.8	9.7	0	5	9	WNW 1	E 4	NE 1
20	95.5	98.9	102.6	99.0	16.3	16.4	9.7	13.0	19.8	9.4	77	75	77	76	4.2	4.5	2.8	3.8	5	9	9	WNW 3	NW 5	WNW 4
21	104.6	104.5	104.7	104.6	8.7	15.0	9.4	10.6	16.6	4.7	81	43	63	62	2.1	9.7	4.4	5.4	8	10	0	WNW 2	W 2	NNW 1
22	104.1	103.0	103.3	103.5	8.6	17.3	12.8	12.9	18.5	3.7	72	36	63	57	3.2	12.6	5.6	7.1	5	8	7	NNE 1	NNW 2	NNW 2
23	101.6	99.3	99.4	100.1	10.4	22.7	13.4	15.0	23.7	8.6	78	34	81	64	2.7	18.4	3.0	8.0	10	2	1	N 2	NE 4	NNE 1
24	102.1	104.8	110.6	105.8	12.0	19.1	8.6	12.1	19.8	8.5	89	46	50	62	1.5	12.0	5.6	6.4	10	7	2	NNE 2	NNE 3	NNE 6
25	113.4	114.0	115.9	114.4	7.6	14.7	7.1	9.8	15.4	2.4	66	33	49	49	3.5	11.1	5.1	6.6	0	5	8	NNE 3	NE 6	NNE 6
26	116.7	115.9	115.6	116.1	6.0	8.9	5.8	6.6	11.6	0.8	70	57	59	65	2.9	4.9	3.7	3.8	2	9	5	NW 4	NNE 6	NNE 2
27	114.4	113.5	112.1	113.3	5.8	10.1	6.8	7.6	12.8	−1.3	65	47	74	62	3.2	6.6	2.6	4.1	3	8	7	N 1	NE 3	NNE 2
28	111.3	109.9	109.0	110.1	6.8	11.8	7.2	8.2	14.0	−0.6	75	43	69	62	2.5	7.9	3.2	4.5	7	8	2	NNE 1	NW 1	NNW 1
29	109.0	107.8	108.3	108.4	7.0	15.7	8.6	10.0	16.5	−0.5	69	33	70	57	3.1	12.0	3.3	6.1	3	8	1	NNW 1	NW 2	NNW 1
30	109.0	108.6	107.1	108.2	8.8	16.4	11.2	11.9	18.5	1.3	71	42	66	60	3.3	10.8	4.5	6.2	1	9	0	NW 1	WNW 1	NNE 1
31	106.1	103.9	101.9	104.0	12.7	20.9	13.9	15.4	22.9	2.7	64	32	60	52	5.4	16.9	6.4	9.6	0	8	2	C 0	SW 2	SW 1
M	103.2	103.0	103.1	103.1	8.4	14.7	9.5	10.8	16.3	4.2	77	49	71	66	2.7	9.5	3.8	5.3	5.5	7.4	4.9	1.8	3.2	1.7

Czerwiec – Juin

1	102.3	102.6	102.1	102.3	11.4	17.1	12.4	13.3	19.0	7.7	73	45	70	63	3.6	10.7	4.4	6.2	3	9	0	WNW 2	W 3	W 1
2	103.4	105.8	106.8	105.3	11.9	18.0	11.0	13.0	19.0	7.9	83	57	95	78	2.3	8.7	0.6	3.9	8	5	0	W 1	WNW 5	WNW 1
3	107.3	105.3	102.0	104.9	14.9	22.4	17.2	17.9	25.8	8.8	79	45	69	64	3.4	15.0	6.0	8.1	8	8	8	SW 1	C 0	C 0
4	100.3	98.6	96.5	98.5	15.7	23.4	17.6	18.6	25.1	10.8	82	46	63	64	3.2	15.5	7.5	8.7	10	10	10	C 0	W 3	C 0
5	93.5	92.3	91.3	92.4	12.7	17.0	12.1	13.0	18.0	11.8	91	62	76	76	1.4	7.4	3.3	4.0	10	8	5	W 2	SW 3	SW 2
6	92.2	94.9	95.6	94.2	9.8	14.1	12.4	12.2	15.4	9.5	87	56	69	71	1.6	7.1	4.5	4.4	10	8	9	W 3	WSW 5	SW 3
7	95.8	95.9	97.3	96.3	11.6	17.8	11.6	13.2	18.3	9.7	79	46	81	69	2.8	11.0	2.6	5.5	10	10	1	SW 1	SW 3	C 0
8	99.3	98.8	98.1	98.7	13.2	23.0	16.3	17.2	23.6	6.8	74	36	63	58	4.0	18.0	6.9	9.6	8	4	3	NE 1	E 3	ENE 1
9	95.5	93.6	97.6	95.6	18.1	25.2	14.1	17.9	26.5	13.3	77	51	97	75	4.9	15.6	0.6	7.0	7	10	10	E 4	SE 1	W 1
10	99.8	99.2	98.8	99.3	14.4	22.8	17.7	18.2	23.7	10.6	91	55	82	76	1.4	12.3	3.6	5.8	4	9	9	C 0	N 1	NE 1
11	96.3	93.5	93.3	94.4	18.6	27.7	22.8	23.0	29.9	14.1	85	53	74	71	3.1	17.3	7.2	9.2	3	8	10	NE 2	NE 4	C 0
12	106.6	112.2	117.4	112.1	14.1	17.8	12.6	14.5	22.8	12.4	87	59	66	71	2.2	8.4	5.0	5.2	10	5	0	W 3	W 4	NW 1
13	118.5	118.0	117.3	117.9	11.6	19.7	13.8	14.7	20.7	6.7	70	52	68	63	4.0	10.9	5.1	6.7	6	1	0	NW 3	W 3	NW 1
14	117.3	116.5	115.9	116.9	14.2	24.7	17.1	18.5	25.9	7.6	79	35	54	56	3.4	20.2	9.0	10.9	0	1	7	NW 1	N 3	NNE 1
15	117.5	115.2	112.6	115.1	13.5	24.1	17.4	18.1	25.3	6.1	58	30	51	46	6.5	21.1	9.8	12.5	0	1	0	NNE 2	NE 2	C 0
16	112.2	110.1	107.8	110.0	14.4	26.4	20.1	20.2	27.1	7.0	63	31	37	50	6.1	23.7	10.1	13.3	0	0	1	NE 1	NE 2	N 1
17	108.2	106.8	105.4	106.8	17.0	27.1	18.2	20.1	28.0	11.6	56	35	48	46	8.3	23.2	10.9	14.2	1	0	0	NE 2	NE 2	NE 1
18	104.2	101.9	98.8	101.6	17.6	28.3	21.4	22.2	29.7	9.0	60	27	51	46	8.1	28.0	12.6	16.2	0	0	0	NE 1	NE 1	C 0
19	98.0	97.0	98.9	98.0	18.3	29.7	19.0	21.5	30.6	10.9	64	31	65	53	7.5	28.7	7.8	14.7	0	3	1	N 1	NNW 1	NNE 3
20	102.0	102.5	104.5	103.0	14.8	23.4	16.7	17.9	25.3	9.3	65	34	49	49	5.9	19.0	9.7	11.5	8	8	5	NNE 2	NNE 3	N 1
21	105.2	101.7	97.2	101.4	15.1	23.4	19.4	19.3	25.5	8.1	57	41	56	51	7.3	17.1	9.9	11.4	1	5	7	NE 1	ENE 1	N 1
22	92.4	91.6	90.4	91.5	17.2	18.5	16.7	17.3	19.4	11.9	72	82	86	80	5.4	3.9	2.7	4.0	10	10	10	NE 1	WNW 1	W 1
23	95.0	95.2	97.8	96.0	13.4	20.3	12.8	14.8	22.6	11.1	61	45	94	73	3.0	13.2	0.9	5.7	6	8	10	NE 1	SW 2	NW 1
24	99.0	97.8	94.0	96.9	11.7	14.5	13.3	13.2	16.8	8.3	81	72	79	76	2.6	4.6	3.8	3.7	10	8	8	C 0	NE 1	NE 1
25	92.5	98.3	102.2	97.7	9.0	12.5	10.0	10.4	14.1	8.6	93	80	91	89	0.7	2.9	1.1	1.6	10 ●	10	2	NE 2	W 2	SW 2
26	105.7	106.7	108.7	107.0	11.2	16.4	11.7	12.8	16.8	7.6	79	46	77	67	2.8	9.9	3.1	5.3	1	6	5	SW 2	WSW 5	SW 1
27	109.1	111.3	110.9	110.4	12.0	15.1	13.6	13.6	17.0	8.4	84	53	69	69	2.2	8.2	4.9	5.1	8	8	10	W 1	W 3	SSE 2
28	108.4	107.1	107.6	107.7	14.2	24.6	20.0	19.7	27.2	12.5	93	57	78	77	0.7	13.2	5.2	6.4	10	6	2	S 3	WSW 4	NW 2
29	108.6	109.0	106.6	108.1	18.7	27.1	22.4	22.6	29.5	15.6	73	51	75	66	6.0	17.4	6.7	10.0	6	2	1	W 1	SW 3	C 0
30	107.4	107.5	107.5	107.5	20.8	27.1	21.7	22.8	29.1	16.5	78	49	70	66	5.4	18.3	7.9	10.5	1	7	7	C 0	W 2	NW 1
31																								
M	103.1	102.9	102.7	102.9	14.4	21.6	16.1	17.0	23.3	10.0	77	49	71	66	4.0	14.4	5.8	8.1	5.6	5.9	4.7	1.5	2.5	1.0

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	$\cap^1$ n – a
2	7	.	.	–	
3	7	0.2	.	–	
4	7	0.0	.	–	$\bullet^0$ 23^{39} – 35^{0} 43^{5} 94^{8} 102^{5} $\triangledown$ 171^{3}–25
5	7	0.1	.	–	$\triangledown$ 94^{6}–50 95^{3}–59 100^{3}–06 150^{5}–09 163^{0}–42
6	7	1.9	.	–	$\bullet^0$ 2020 2250 – 24
7	7	0.0	.	–	$\bullet^0$ 000 – 115 4^{10} $\triangledown$ 113^{1}–42 $\bullet^0$ 1015 2015
8	7	0.0	.	–	$\bullet^0$ 713 .. 24 $\triangledown$ 1156 – 58 1200 – 05
9	7	1.1	.	–	$\bullet^0$ 1930 2010 – 24 $\cap^0$ n – 750
10	6	0.7	.	–	$\bullet^0$ 000 – 10 1242 1612
11	7	.	.	–	$\bullet^0$ 415 620
12	7	.	.	–	$\cap^0$ n – 740
13	7	0.4	.	–	(K) 1325 – 1406 1722 – 31 $\bullet^0$K 1731 – 1750 – 1820 SE – NW < 2010 – 2310
14	8	.	.	–	$\cap^1$ n – 840
15	7	.	.	–	= 440 – 630 $\cap^0$ n – 830
16	7	0.0	.	–	$\bullet^0$ 2328 – 24 $\cap^0$ n – 750
17	7	.	.	–	$\bullet^0$ 000 – 20
18	7	.	.	–	
19	7	.	.	–	
20	7	.	.	–	$\cap^2$ n – 715
21	8	.	.	–	
22	8	.	.	–	
23	7	.	.	–	
24	7	.	.	–	
25	8	.	.	–	
26	7	.	.	–	$\sqcup^0$ n
27	7	0.0	.	–	$\triangledown$ 1404 – 32 $\sqcup^2$ n
28	7	.	.	–	$\sqcup^1$ n – 550
29	7	.	.	–	$\sqcup^1$ n – 600
30	7	.	.	–	$\sqcup^0$ n
31	8	.	.	–	$\cap^2$ n – 720
Σ	–	4.4	–	–	UWAGI

1	8	.	.	–	
2	7	.	.	–	$\cap^1$ n – 750
3	7	.	.	–	
4	7	2.3	.	–	$\triangledown$ 2305 – 39
5	7	3.2	.	–	$\triangledown$ 113 – 440 $\bullet^0$ 447 – 705 $\triangledown$ 1625 – 1704
6	7	0.0	.	–	$\bullet^0$ 632 704 $\triangledown$ 2012 – 19
7	7	.	.	–	
8	7	.	.	–	
9	7	15.2	.	–	(K) 1418 – 31 NE – SW K^1 – 1444 NE – SW $\bullet^1$K 1444 – 1530 – 1616 W – E (K) – 1620 W – E $\bullet^0$ 1922 – 47 $\bullet^1$ – 2012
10	7	.	.	–	= 315 – 640 [9.VI: $\bullet^0$ – 2019
11	7	.	.	–	$\cap^1$ n – 840
12	7	.	.	–	
13	7	.	.	–	$\cap^2$ n – 740
14	7	.	.	–	$\cap^0$ n – 820
15	8	.	.	–	
16	8	.	.	–	
17	7	.	.	–	$\cap^1$ n – 750
18	8	.	.	–	$\cap^1$ n – 800
19	8	.	.	–	
20	7	.	.	–	
21	8	.	.	–	
22	7	0.1	.	–	$\bullet^0$ 1042 1245
23	7	3.6	.	–	$\triangledown$ 1708 – 2017
24	7	8.3	.	–	$\bullet^0$ 940 1136 , = 200 – 1120
25	7	1.3	.	–	$\bullet^0$ 214 – 405 $\bullet^1$ – 540 $\bullet^0$ – 941 $\triangledown$ 1907 – 33
26	7	6.4	.	–	$\triangledown$ 1606 – 1703 , 1801 – 09
27	7	0.0	.	–	
28	7	0.0	.	–	$\bullet^0$ 708 910
29	8	.	.	–	$\cap^1$ n – 816
30	7	1.2	.	–	< 2240 – 2335
31					
Σ	–	41.6	–	–	UWAGI

Wałcz $\varphi = 53°17'$ $\lambda = 16°28'$ **Lipiec – Juillet 1957**

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	108.7	106.2	103.6	106.2	15.6	25.5	23.3	21.9	28.4	15.4	95	59	66	73	0.9	13.4	9.6	8.0	9	6	6	NNE 1	NE 2	ENE 2
2	100.1	102.8	106.7	103.2	21.2	23.6	15.4	18.9	24.2	15.4	75	71	71	72	6.3	8.4	5.1	6.6	7	9	0	ENE 1	WSW 4	NW 1
3	107.6	106.6	104.9	106.4	16.6	25.3	18.4	19.2	25.7	10.8	78	39	62	60	4.3	17.4	8.2	10.0	0	5	9	W 1	WNW 3	N 1
4	102.0	100.3	97.7	100.0	19.5	29.6	26.8	25.7	32.1	10.7	64	46	59	56	8.3	22.2	14.2	14.9	5	2	8	NNE 1	SW 2	C 0
5	99.7	101.9	105.3	102.3	24.4	27.4	17.8	21.8	27.8	17.8	73	57	54	65	8.2	15.8	7.4	10.5	9	5	0	WNW 2	WSW 4	WNW 2
6	108.2	107.8	107.2	107.7	16.7	23.9	18.0	19.2	25.3	11.6	77	38	64	60	4.4	18.3	7.4	10.0	0	0	1	WNW 1	WNW 6	NW 1
7	108.0	106.9	103.9	106.3	16.4	28.7	24.1	23.3	30.6	10.3	72	42	50	55	5.2	22.7	15.1	14.3	3	2	4	ENE 1	NE 1	ENE 1
8	102.8	102.5	102.2	102.5	20.8	28.6	21.4	23.0	29.5	15.9	76	57	62	65	6.0	16.9	9.6	10.8	2	7	7	SW 2	W 2	C 0
9	102.9	102.5	101.8	102.4	17.4	22.4	18.2	19.0	22.7	17.2	84	73	89	82	3.2	7.4	2.3	4.3	10 ●	8	8	NW 2	SE 1	C 0
10	99.8	98.4	96.9	98.4	17.8	21.7	18.7	19.2	22.4	16.2	91	73	86	83	1.8	7.0	3.0	3.9	4	9	8	ENE 1	NE 1	NE 1
11	96.0	96.7	98.3	97.0	16.1	22.7	17.7	18.6	23.1	15.6	97	67	86	83	0.6	9.0	2.8	4.1	10 ●	10	10	N 2	NW 2	NW 3
12	98.4	98.9	98.7	98.7	16.7	20.4	18.7	18.6	21.4	13.8	86	82	92	87	2.7	4.4	1.7	2.9	10	10	8	NW 1	N 3	NW 1
13	100.7	102.1	103.8	102.2	16.8	26.0	20.2	20.8	27.6	14.7	96	58	80	78	0.8	14.1	4.8	6.6	10	4	8	NW 1	WSW 1	N 1
14	103.3	103.2	101.9	102.8	19.7	18.8	17.2	18.2	23.0	14.3	81	94	96	90	4.3	1.3	0.8	2.1	7	9	10 ●	N 1	E 2	E 1
15	99.3	99.3	99.2	99.3	17.3	19.2	17.6	17.9	22.4	16.6	96	78	91	88	0.8	4.8	1.8	2.5	10	10	9	E 1	SW 1	SE 1
16	99.0	98.1	97.1	98.1	15.1	21.3	17.2	17.7	22.5	12.4	90	59	76	75	1.7	10.3	4.7	5.6	8	10	10	WNW 2	NW 2	NW 2
17	94.4	95.0	96.6	95.3	15.4	17.6	15.4	16.0	18.7	13.9	97	81	93	91	0.6	3.8	1.0	1.8	10 ●	10	10	WNW 2	W 4	NW 2
18	97.3	96.9	96.2	96.8	16.3	21.7	15.9	17.4	23.4	13.0	91	53	81	75	1.7	12.2	3.5	5.8	8	7	0	W 3	WSW 5	NW 1
19	94.9	93.7	92.6	93.7	15.3	26.3	19.6	20.2	26.9	11.1	88	43	70	67	2.1	19.3	6.9	9.4	0	3	7	C 0	ENE 2	NE 1
20	90.8	91.0	91.8	91.2	19.3	24.9	20.6	21.4	26.8	14.3	77	58	72	69	5.0	13.3	6.7	8.3	9	9	9	NE 1	ESE 6	SE 4
21	90.2	90.1	90.3	90.2	16.9	16.9	16.6	16.8	20.6	15.8	96	96	95	96	0.8	0.8	1.0	0.9	10	10	10	WNW 1	WSW 2	W 1
22	88.6	88.0	89.7	88.7	17.4	23.7	19.3	19.9	25.3	16.0	93	63	81	79	1.5	10.9	4.2	5.5	10	7	7	NW 2	NE 6	NNW 1
23	90.4	92.1	92.4	91.6	17.4	20.5	19.3	19.1	23.6	16.7	90	76	88	85	2.1	5.5	2.8	3.6	10	9	10	NW 1	WNW 3	NW 3
24	93.9	95.0	96.0	95.0	16.4	17.2	14.5	15.6	19.3	14.4	87	72	81	80	2.5	5.4	3.1	3.7	10	9	5	WSW 6	W 6	WSW 2
25	96.4	96.0	94.5	95.6	13.7	17.4	13.3	14.4	18.7	12.7	82	59	92	78	2.9	8.3	1.3	4.2	4	8	10 ● ⚿	SW 5	SW 6	SSW 1
26	94.0	94.5	93.2	93.9	12.1	17.3	14.0	14.4	18.3	11.7	95	70	97	87	0.7	6.0	0.6	2.4	10 ●	7	10	SW 4	WSW 4	W 2
27	89.1	89.2	89.8	89.4	15.5	16.6	13.2	14.6	18.4	13.0	97	82	94	91	0.6	3.9	0.9	1.7	10	9	6	SW 2	WSW 2	ESE 2
28	91.3	92.5	93.6	92.5	11.6	17.7	12.8	13.7	19.2	10.4	95	63	86	81	0.6	7.5	2.1	3.4	10	7	2	SW 4	W 4	S 1
29	94.2	95.9	97.8	96.0	13.1	18.6	15.3	15.6	20.8	10.1	89	66	87	81	1.6	7.2	2.3	3.7	0	7	9	S 1	SW 2	S 2
30	97.5	99.4	104.0	100.3	14.9	17.2	15.3	15.7	19.7	14.4	98	93	90	94	0.3	1.4	1.7	1.1	10 ●	9	1	SW 3	SW 5	W 1
31	107.1	109.4	110.5	109.0	16.4	17.8	14.9	16.0	19.2	14.3	92	73	85	83	1.5	5.6	2.5	3.2	9	10	9	W 3	W 4	W 1
M	98.3	98.5	98.7	98.5	16.8	21.8	17.8	18.5	23.5	13.9	87	66	80	78	2.7	9.8	4.5	5.7	7.2	7.3	6.8	1.9	3.2	1.4

Sierpień – Août

1	110.1	109.6	109.0	109.6	13.7	22.0	16.6	17.2	23.9	11.6	94	62	85	80	0.9	10.0	2.9	4.6	10	4	4	W 2	W 4	W 2
2	108.5	108.3	109.3	108.7	13.4	17.4	13.2	14.3	19.9	12.2	95	54	77	75	0.7	9.1	3.5	4.4	10	8	0	W 4	W 7	W 2
3	107.8	107.1	107.1	107.3	13.2	19.0	14.1	15.1	21.4	10.0	90	53	78	74	1.6	10.4	3.6	5.2	2	5 ⊙	0	WSW 3	W 2	W 1
4	107.0	107.5	109.1	107.9	15.1	20.2	15.4	16.5	22.9	11.0	91	59	82	77	1.5	9.7	3.2	4.8	10	8	0	W 2	WNW 3	C 0
5	110.3	110.2	109.8	110.1	13.0	21.6	17.9	17.6	24.0	9.7	100	59	78	79	0.0	10.5	4.4	5.0	10	8	6	C 0	WNW 2	NW 1
6	110.2	108.5	106.1	108.3	15.4	24.0	16.9	18.3	25.4	9.6	88	47	79	71	2.1	15.8	4.0	7.3	0	3	6	NE 1	ENE 1	NE 1
7	101.9	99.0	96.2	99.0	16.4	21.4	17.5	18.2	21.9	12.1	79	67	97	81	3.8	8.4	0.6	4.3	9	10	10	C 0	E 2	W 1
8	96.6	97.4	97.8	97.3	15.4	22.2	16.4	17.6	23.6	14.5	97	64	87	83	0.6	9.7	2.5	4.3	10	7	6	NW 1	N 3	NE 1
9	96.2	93.5	89.5	93.1	14.2	22.3	20.0	19.1	22.6	10.9	89	63	75	76	1.8	9.9	5.8	5.8	8	10	10	NE 2	NE 6	NE 4
10	86.9	87.3	90.4	88.2	16.6	21.3	17.2	18.1	22.7	16.5	98	74	89	87	0.4	6.5	2.2	3.0	10 ●	8	3	E 1	S 2	C 0
11	95.5	95.8	96.0	95.8	16.8	25.2	20.9	21.0	27.0	14.4	87	57	68	71	2.5	13.9	7.8	8.1	0	5	1	SW 3	SE 5	S 1
12	96.5	97.6	98.3	97.5	17.6	20.9	18.4	18.6	24.1	16.3	90	71	77	79	2.0	7.2	4.9	4.7	10	9	5	SW 1	SE 2	SSE 1
13	99.9	100.5	100.3	100.2	15.1	24.3	18.5	19.1	25.1	13.2	89	46	72	69	1.9	16.4	5.9	8.1	1	8	7	SW 1	SW 3	SW 1
14	99.5	99.3	97.6	98.8	14.6	17.9	16.0	16.1	19.4	12.3	95	84	88	89	0.7	3.2	2.1	2.0	10	10	10	C 0	C 0	NW 1
15	95.9	95.1	96.2	95.7	14.8	22.7	17.8	18.3	23.8	14.2	96	58	81	78	0.7	11.7	3.8	5.4	8	8	10	W 1	SW 1	NW 1
16	96.4	97.0	97.4	96.9	16.7	18.7	15.3	16.5	20.7	15.3	96	86	93	92	0.8	3.2	1.2	1.7	10	10 ●	10	C 0	SSW 4	S 1
17	96.6	96.3	95.2	96.0	12.3	16.2	13.9	14.6	19.0	11.5	94	74	88	85	0.9	5.5	2.0	2.8	6	10	5	SW 1	WSW 3	SW 2
18	93.2	93.3	95.0	93.8	13.7	15.1	14.4	14.4	18.0	12.3	87	94	90	90	2.0	1.0	1.6	1.5	10	10 ●	0	SW 3	W 3	SW 3
19	97.7	100.0	102.4	100.0	13.0	15.7	14.2	14.3	16.4	11.5	95	96	94	95	0.7	0.7	0.9	0.8	10	10 ●	2	SW 3	SW 3	C 0
20	102.8	102.4	101.7	102.3	13.8	18.0	16.9	16.4	19.1	12.4	92	72	85	83	1.3	5.7	2.9	3.3	2	10	10	SW 2	SW 3	SW 1
21	100.6	99.5	98.3	99.5	16.3	19.2	12.4	15.1	20.7	12.3	93	71	96	87	1.3	6.4	0.5	2.7	9	9	10	WSW 2	SW 2	W 2
22	98.1	98.1	98.6	98.3	11.9	16.7	11.7	13.0	17.7	10.2	97	61	84	81	0.3	7.3	2.1	3.2	10	8	6	W 2	WNW 4	SW 2
23	96.9	98.7	97.8	98.5	8.8	16.7	12.9	12.8	18.0	7.0	96	64	84	81	0.4	6.8	2.4	3.2	0	7	0	SW 2	SW 2	SE 1
24	93.0	88.9	93.1	91.7	11.2	15.0	10.7	11.9	16.4	9.2	86	93	94	91	1.8	1.1	0.3	1.3	10	10	0	E 4	C 0	NW 5
25	97.8	95.8	94.9	96.2	10.1	16.4	12.5	13.4	19.7	8.1	90	57	87	78	1.3	9.1	1.9	4.1	1	8	10	SW 3	S 6	WNW 3
26	93.3	93.0	94.3	93.5	11.3	15.7	11.3	12.4	17.4	9.5	86	72	90	83	1.8	5.0	1.3	2.7	6	8	2	SE 3	SW 4	SW 2
27	96.8	98.3	98.9	98.0	12.3	15.4	11.4	12.6	18.2	10.4	92	70	96	86	1.2	5.3	0.5	2.3	10	8	10	SW 4	WSW 3	C 0
28	98.3	99.2	101.2	99.6	10.6	14.1	11.0	11.7	15.8	9.7	99	83	92	91	0.2	2.7	1.0	1.3	10	9	6	C 0	SE 1	C 0
29	102.6	103.9	104.1	103.5	9.4	13.8	12.0	11.8	15.4	8.8	99	79	90	89	0.2	3.4	1.3	1.6	10	10	1	SW 2	SW 3	W 1
30	104.8	105.3	104.7	104.9	10.9	13.9	11.0	11.7	16.1	8.8	96	73	91	87	0.5	4.2	1.1	1.9	10	9	10	W 2	SW 3	SW 1
31	101.2	100.6	99.4	100.4	10.1	15.4	10.9	11.8	16.3	9.8	96	65	92	84	0.5	6.2	1.0	2.6	10 ●	8	9 ●	S 2	S 4	SW 2
M	99.8	99.6	99.7	99.7	13.5	18.8	14.8	15.5	20.4	11.5	93	69	86	83	1.2	7.3	2.6	3.7	7.5	8.2	5.5	1.8	3.0	1.5

Wałcz $H_s = 111\ m$ $H_b = 113{,}8\ m$ $h_w = 10\ m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	–	▽ 6^{17-39} $7^{18}-8^{07}$
2	7	1.4	.	–	↘ $1^{20}-3^{25}$ (K) $8^{50}-9^{38}$ S–N ●^{0}K $9^{38}-10^{28}-11^{02}$ S–N (K) -11^{06}
3	7	0.0	.	–	
4	7	.	.	–	●^{0} $5^{54}-6^{06}$ ↘ $22^{30}-24$
5	7	.	.	–	↘ $0^{00}-40$ (K) $2^{15}-40$ W–E K^{0} $2^{40}-3^{20}-4^{45}$ W–E (K) -5^{10} W–E
6	7	.	.	–	⌒^{0} $n-7^{30}$
7	7	5.4	.	–	↘ $23^{10}-24$
8	7	0.1	.	–	↘ $0^{00}-2^{30}$ (K) 2^{30-47} SW–NE ●^{0}K^{0} $2^{47}-3^{50}-5^{40}$ SW–NE (K) -6^{10} S–N
9	7	8.4	.	–	▽^{0} 6^{18-40} ▽^{1} $7^{54}-9^{40}$ ▽ -10^{37}, 14^{40-44}, $15^{47}-16^{26}$
10	7	4.4	.	–	
11	7	0.4	.	–	●^{0} $4^{25}-6^{15}$ ●^{1} 6^{43} ●^{0} $6^{55}-8^{12}$ ▽ 8^{28-39}
12	7	0.7	.	–	●^{0} $10^{17}-13^{21}$
13	7	.	.	–	= $3^{40}-6^{14}$ ≡^{0} -6^{16} ≡^{1} -6^{48} ≡^{0} -7^{22} = -8^{26}
14	7	8.8	.	–	●^{0} $13^{28}-14^{28}$ ▽ $20^{21}-21^{05}$ ●^{0} $21^{16}-24$; (K) $12^{55}-13^{18}$ SE–NW K^{0} $13^{18}-13^{42}-14^{28}$ SE–NW
15	7	.	.	–	●^{0} $0^{00}-1^{15}$; = $n-10^{50}$ [14.VII: (K) -14^{46}; ⌒^{2} $n-8^{18}$
16	7	2.3	.	–	●^{0} $23^{37}-24$; ⌒^{1} $n-8^{30}$; ⊕ $9^{15}-11^{20}$
17	7	6.0	.	–	●^{0} $0^{00}-9^{18}$ ●^{1} -10^{24} ●^{0} -12^{26}, 18^{32-48} ●^{1} 22^{41} 23^{22}, $23^{30}-24$
18	7	.	.	–	●^{0} $0^{00}-1^{20}$
19	7	.	.	–	⌒^{1} $n-8^{16}$
20	7	6.6	.	–	▽ 22^{20-46} 23^{24-29} $23^{51}-24$; ↘ $21^{48}-22^{10}$; ⌒^{2} $n-8^{40}$
21	6	8.6	.	–	▽ 0^{00-06} ●^{0} 5^{15-20} ●^{1} -5^{48} ●^{0} -7^{13}, $10^{20}-12^{03}$ ●^{1} -13^{40} ●^{0} -15^{05}, $16^{39}-17^{35}$, $21^{38}-23^{42}$ ●^{1} -24;
22	7	0.8	.	–	●^{1} $0^{00}-1^{08}$ ●^{0} -1^{15} [21.VII: = $n-17^{30}$
23	7	0.9	.	–	●^{0} $5^{39}-7^{16}$, 9^{36} $10^{22}-10^{44}$ $11^{09}-12^{46}$; ↘ $0^{10}-2^{30}$
24	7	0.1	.	–	●^{0} 9^{17-36}
25	7	8.0	.	–	●^{1}K^{0} $21^{25}-22^{10}-22^{30}$ SW – NE ▽ 23^{09-35}
26	7	5.6	.	–	●^{0} $6^{37}-8^{28}$ ●^{1} 11^{18-38} ●^{0} $18^{20}-24$
27	7	10.9	.	–	●^{0} $0^{00}-1^{32}$ ▽ 9^{05-25} 10^{03}; 11^{25} $12^{30}-13^{17}$ 15^{01-16} ●^{0}K^{0} $16^{35}-17^{07}$ K^{0} -17^{25} SW–NE ▽ $18^{30}-19^{05}$; = $n-11^{30}$
28	7	2.9	.	–	▽ 15^{00-14} 17^{13-20} ▽^{0} 18^{00-03} ▽^{1} -18^{12} ▽^{0} -18^{52}; (K) $16^{51}-17^{25}$ S–W
29	7	9.2	.	–	▽ 12^{20-29} 17^{24-37} 23^{43-49} ⌒^{2} $n-9^{50}$
30	7	11.2	.	–	▽ $2^{12}-3^{02}$ ●^{0} 3^{08-45} ●^{1} -3^{55} ●^{0} -4^{08} ●^{1} -4^{15} ●^{0} -5^{24}, $6^{12}-7^{10}$ ●^{0} -8^{25} ●^{0} -9^{05} ▽ 11^{35-41} 12^{04-36} 13^{07-22}
31	7	.	.	–	[30.VII: 16^{07-35}
Σ	–	102.7	–	–	UWAGI.

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1	7	.	.	–	= $4^{50}-8^{20}$
2	7	.	.	–	= $n-8^{30}$; ⌒^{2} $n-8^{50}$
3	8	0.0	.	–	▽ $9^{49}-11^{05}$; ⌒^{1} $n-8^{20}$
4	7	.	.	–	= $4^{10}-8^{15}$
5	7	.	.	–	= $3^{40}-5^{22}$ ≡^{1} -8^{20} = -9^{10}
6	7	.	.	–	= $4^{40}-6^{30}$ ⌒^{0} $n-7^{50}$
7	7	.	.	–	⌒^{2} $n-8^{20}$
8	7	.	.	–	⌒^{2} $n-8^{30}$
9	7	2.4	.	–	●^{0} 17^{20-42}; ⌒^{1} $n-8^{45}$
10	7	5.1	.	–	●^{0} 3^{18} $5^{35}-10^{30}$ ▽ 17^{32-44}; 20^{01-13}; = $n-13^{30}$
11	7	1.1	.	–	= $3^{10}-8^{20}$; ⌒^{2} $n-8^{40}$
12	7	.	.	–	▽ $4^{25}-5^{10}$
13	8	0.0	.	–	⌒^{1} $n-8^{10}$
14	7	0.9	.	–	●^{0} 7^{12-35} $8^{22}-11^{14}$; = $4^{10}-$na.; ⌒^{2} $n-7^{12}$
15	7	1.9	.	–	⌒^{2} $n-10^{00}$
16	7	5.1	.	–	●^{0} $1^{32}-2^{42}$ ●^{1} 3^{12-48} ●^{0} -4^{10} ▽ 8^{08-29} $13^{40}-17^{17}$ ●^{0} $19^{35}-22^{18}$; = $n-8^{20}$
17	7	1.3	.	–	▽ 14^{02-16} 16^{09-15}; = $0^{00}-6^{20}$ $22^{10}-24$
18	6	2.1	.	–	▽ 12^{19-32} $13^{24}-14^{08}$; = $0^{00}-8^{15}$
19	6	0.8	.	–	●^{0} 11^{25} 12^{45} $13^{10}-14^{07}$ 14^{14}, 16^{27}; ●^{0} 16^{33} 17^{17}; = $4^{30}-10^{40}$
20	7	0.2	.	–	= $4^{20}-7^{40}$; ⌒^{1} $n-8^{30}$
21	7	7.1	.	–	●^{0} 2^{10} 4^{16} ▽ $16^{16}-17^{36}$ ●^{0} -18^{12} ▽ -20^{38}; = $n-8^{20}$; $n-24$
22	7	0.8	.	–	▽ 16^{12-31} 22^{09-23}; = $0^{00}-8^{50}$
23	8	.	.	–	= $n-8^{30}$
24	7	10.7	.	–	●^{1} $12^{32}-13^{06}$ ●^{0} -13^{37}, 14^{41-54} ●^{1} $15^{31}-16^{17}$ ●^{0} -17^{16}, $17^{47}-18^{24}$
25	7	.	.	–	= $4^{30}-7^{40}$
26	7	2.8	.	–	●^{0} 12^{25-30} ▽ $14^{20}-15^{06}$ 15^{32-36} 17^{01-42}; = $22^{10}-24$; ⌒^{0} $n-9^{15}$
27	7	1.4	.	–	▽ 12^{21-25} $13^{56}-14^{01}$, $17^{48}-18^{02}$ 18^{10-50}; = $0^{00}-10^{20}$, $19^{20}-24$
28	7	0.9	.	–	●^{0} 8^{45} $10^{05}-12^{10}$; = $0^{00}-12^{30}$
29	7	0.1	.	–	▽ 19^{32-37}; = $n-8^{40}$ $22^{50}-24$
30	7	0.9	.	–	▽ 17^{28-41}; = $0^{00}-8^{40}$
31	7	16.3	.	–	●^{0} 2^{00}..17, 6^{05}..32; $7^{15}-8^{16}$ ▽ 18^{08-33}, $21^{41}-24$
Σ	–	62.1	–	–	UWAGI.

Wałcz $\varphi = 53°17'$ $\lambda = 16°28'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE : POGODA N,w			KIERUNEK : PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.9	101.2	102.8	101.3	9.6	11.8	10.5	10.6	14.4	8.0	97	95	96	96	0.4	0.6	0.5	0.5	10	10	7	SW 3	WSW 2	SW 1
2	101.7	100.8	99.4	100.6	9.4	17.2	13.9	13.6	18.1	7.4	92	72	94	86	1.0	5.4	0.9	2.4	2	8	10 ●	SE 2	S 3	SSW 1
3	99.4	101.2	103.9	101.5	12.2	16.4	11.2	12.8	17.7	11.1	98	71	95	88	0.3	5.4	0.7	2.1	10 ●	7	1	WSW 1	W 4	C 0
4	106.3	107.8	109.2	107.8	7.6	17.6	9.2	10.9	18.2	6.0	99	58	93	83	0.1	8.4	0.8	3.1	4	5	0	SW 1	W 2	C 0
5	108.2	105.1	103.0	105.4	9.4	17.3	14.6	14.0	19.0	5.8	92	54	86	77	1.0	9.0	2.4	4.1	6	9	10 ●	S 1	SE 4	SSW 2
6	103.6	104.1	105.5	104.4	12.6	17.4	10.4	12.7	16.7	10.2	99	78	93	90	0.2	4.4	0.8	1.8	10	8	0	WSW 1	S 3	C 0
7	105.9	105.4	103.9	105.1	6.8	21.5	15.3	14.7	22.5	4.9	99	55	90	83	0.2	10.4	1.7	4.1	5	1 ⊙	0	C 0	S 2	E 1
8	103.7	104.6	105.1	104.5	15.4	26.8	17.3	19.2	27.3	14.1	89	56	95	80	1.9	15.6	1.0	6.2	7	6	3	SE 2	SE 2	C 0
9	104.3	106.3	110.3	107.0	16.4	16.9	13.6	15.1	23.6	12.2	91	88	91	90	1.7	2.3	1.5	1.8	3	10	10	SE 1	SW 6	SW 1
10	110.1	107.8	104.5	107.5	11.6	15.8	13.1	13.4	17.4	11.2	99	82	94	92	0.1	3.2	0.9	1.4	7	8	9	NE 1	NE 1	E 1
11	98.7	93.1	84.1	92.0	10.8	20.0	15.2	15.3	20.4	10.0	97	58	93	83	0.4	9.8	1.2	3.8	3	7	10 ●	SE 2	SE 4	E 8
12	78.7	79.4	85.1	81.1	14.6	13.4	10.6	12.3	17.0	10.5	97	76	84	86	0.5	3.7	2.1	2.1	10	8	6	SE 4	S 5	SW 6
13	88.9	87.9	84.8	87.2	8.4	12.7	11.5	11.0	14.8	7.4	90	81	82	84	1.0	2.8	2.3	2.1	8	9	9	S 5	SW 5	SE 4
14	86.9	88.7	90.7	88.8	8.7	12.5	9.9	10.2	13.8	8.0	94	76	83	84	0.6	3.6	2.1	2.1	10	9	1	S 5	SSW 6	SSE 3
15	90.6	91.3	95.7	92.5	8.0	12.5	10.2	10.2	13.3	7.0	93	85	86	88	0.7	2.2	1.7	1.5	10 ●	9 ●	10	SW 2	SW 3	SW 4
16	97.4	99.5	101.7	99.5	8.6	10.8	7.5	8.6	11.7	7.5	88	73	96	86	1.4	3.6	0.5	1.8	10	9	0	S 6	W 4	S 2
17	101.3	100.8	101.5	101.2	6.6	10.8	5.8	7.2	11.6	5.1	100	91	98	96	0.0	1.2	0.1	0.4	10 ●	10	0	E 1	SW 1	C 0
18	99.7	99.2	98.4	99.1	7.0	13.4	9.2	9.7	14.4	3.3	98	75	93	89	0.1	3.8	0.8	1.6	8	8	0	W 2	W 5	W 4
19	95.7	93.1	92.0	93.6	7.1	10.7	8.9	8.9	11.7	7.1	100	94	97	97	0.0	0.9	0.3	0.4	10 ≡	10 ●	10	SW 1	S 1	NW 1
20	95.3	99.0	101.7	98.7	7.4	10.8	5.6	7.4	12.4	5.6	97	74	95	89	0.3	3.4	0.4	1.4	8	10	0	W 1	W 3	C 0
21	103.1	103.2	101.5	102.6	7.4	13.1	9.2	9.7	13.6	4.3	91	68	93	84	0.9	4.8	0.8	2.2	10	9	6	W 1	SW 2	SW 1
22	97.2	95.5	94.3	95.7	8.9	11.8	14.6	12.5	14.8	8.2	93	94	99	95	0.8	0.8	0.2	0.6	10	10	10	NE 1	NE 1	S 2
23	88.2	83.5	84.7	85.5	15.1	15.1	13.5	14.3	15.4	13.4	96	98	97	97	0.8	0.4	0.6	0.6	10	10 ●	10	SW 3	S 2	W 4
24	90.2	90.6	93.9	91.6	9.4	10.0	6.2	8.0	13.5	6.2	93	77	91	87	0.8	2.9	0.9	1.5	10	9	10	W 3	W 5	WSW 8
25	99.2	102.4	104.4	102.0	5.6	11.6	4.4	6.5	12.0	3.6	92	49	89	77	0.7	7.0	1.0	2.9	2	4	1	W 5	W 5	SW 1
26	103.4	103.1	105.6	104.0	3.8	11.3	2.4	5.0	12.1	1.8	97	64	95	85	0.3	4.8	0.4	1.8	10 ●	5 ⊙	0	SW 2	W 2	C 0
27	104.0	99.6	89.0	97.5	4.6	8.7	9.3	8.0	9.6	0.8	84	81	99	88	1.4	2.1	0.1	1.2	10	10 ●	10 ●	SW 4	SW 5	W 8
28	90.0	90.6	91.7	90.8	9.3	11.3	7.5	8.9	12.7	7.5	88	85	93	89	1.4	2.0	0.8	1.4	9	6	0	W 8	W 7	SW 6
29	88.6	85.2	84.6	86.1	8.0	9.9	6.8	7.9	11.1	6.1	96	84	97	92	0.4	1.9	0.3	0.9	9	9	10	SW 4	SW 3	SW 4
30	88.7	94.3	100.7	94.6	4.8	7.4	3.1	4.6	8.8	3.0	97	94	95	95	0.3	0.6	0.4	0.4	8	10 ●	0	SW 4	W 5	C 0
31																								
M	97.6	97.5	97.8	97.6	9.2	13.9	10.0	10.8	15.4	7.3	93	76	93	88	0.7	4.2	0.9	1.9	8.0	8.1	5.1	2.6	3.4	2.4

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1	101.0	102.5	105.3	102.9	3.6	6.2	1.2	3.0	8.0	1.2	96	88	100	95	0.1	1.2	0.0	0.4	9	8	0	W 2	W 3	W 1
2	109.7	110.2	108.6	109.5	0.5	9.3	4.4	4.6	10.2	-0.6	100	64	79	81	0.0	4.3	1.8	2.0	0	8	4	W 1	W 2	SSW 1
3	101.6	96.4	93.3	97.1	4.0	6.0	7.6	6.3	8.3	3.0	85	82	84	84	1.2	1.8	1.6	1.5	10	10	3	S 4	SSW 6	W 8
4	95.8	100.0	105.2	100.3	3.6	8.8	4.6	5.4	9.7	3.3	97	65	77	80	0.3	3.9	1.9	2.0	8	8	1	W 6	SW 6	W 3
5	107.1	105.7	101.8	104.9	6.4	9.8	6.8	7.4	10.5	4.1	81	57	91	76	1.9	5.2	0.9	2.7	8	10	10 ●	SW 3	SW 5	SSW 6
6	102.9	107.0	109.2	106.4	9.6	10.8	10.4	10.3	11.5	6.7	96	81	85	87	0.5	2.5	1.9	1.6	10	10	9	W 4	W 4	W 1
7	108.8	109.8	111.7	110.1	11.4	16.2	10.8	12.3	16.7	10.2	88	64	95	82	1.7	6.7	0.7	3.0	10	5	10	WSW 4	W 4	W 1
8	114.1	115.5	114.8	114.8	11.0	12.8	11.6	11.8	13.1	10.5	95	87	87	90	0.5	1.9	1.8	1.4	10	10	9	C 0	SSE 1	ENE 1
9	112.3	110.8	109.1	110.7	5.6	17.2	8.8	10.1	18.3	5.3	100	70	99	90	0.0	5.8	0.1	2.0	10 ≡	0	0	C 0	NE 1	C 0
10	107.1	106.6	105.5	106.4	3.8	17.6	7.9	9.3	18.2	2.8	98	62	96	85	0.1	7.7	0.4	2.7	0	0	0	C 0	SE 1	C 0
11	106.2	106.9	106.3	106.5	9.1	14.3	8.8	10.2	15.2	7.6	100	71	100	90	0.0	4.6	0.0	1.6	10 ≡	8	10 ≡	C 0	C 0	C 0
12	104.4	108.1	113.5	108.7	8.5	11.2	6.1	8.0	12.6	5.7	97	96	95	96	0.3	0.5	0.4	0.4	10 ≡	10	0	C 0	WSW 4	C 0
13	113.6	112.0	109.6	111.7	5.2	13.4	9.3	9.3	14.2	4.0	95	74	99	89	0.4	4.0	0.1	1.5	8	9	10 ≡	C 0	SW 2	SSE 2
14	109.4	110.8	113.1	111.1	7.8	9.7	7.6	8.2	10.4	7.1	97	91	99	96	0.3	1.1	0.1	0.5	10	10	3	SW 1	WSW 3	WSW 1
15	114.7	115.3	114.6	114.9	5.1	9.0	7.9	7.5	9.4	2.4	98	80	76	85	0.2	2.3	2.3	1.7	10	9	10	SW 1	W 1	S 1
16	111.8	109.2	105.3	108.8	6.9	12.6	8.0	8.9	13.4	6.4	80	72	92	81	2.0	4.1	0.9	2.3	10	6	0	E 2	SE 3	ESE 3
17	100.8	102.5	104.1	102.5	5.9	13.0	8.2	8.8	13.4	5.3	95	80	94	90	0.5	3.0	0.6	1.4	8	10	0	SE 2	SW 4	SW 1
18	97.2	94.3	93.6	95.0	8.4	14.4	15.1	13.2	15.6	6.9	96	86	80	87	0.4	2.4	3.5	2.1	10	9	10	SSE 4	SSW 5	SW 4
19	92.4	92.8	94.3	93.2	12.4	16.9	8.9	11.8	17.6	8.7	88	69	96	84	1.7	5.9	0.5	2.7	8	10	10 ●	S 2	SSW 4	WNW 2
20	97.2	100.1	102.3	99.9	8.8	10.8	5.8	7.8	11.0	5.8	97	81	95	91	0.3	2.5	0.4	1.1	10	9	0	W 1	W 2	SW 1
21	102.0	99.4	95.9	99.1	2.4	7.6	7.6	6.3	10.1	1.2	98	89	86	91	0.2	1.2	1.4	0.9	10 ≡	10	10	S 2	SE 6	SE 3
22	90.7	88.1	89.0	89.3	4.8	11.1	8.4	8.2	11.4	4.7	90	65	92	82	0.8	4.6	0.9	2.1	8	8	10	SE 1	SE 2	SW 1
23	93.0	96.4	98.0	95.8	7.9	7.9	5.8	6.8	9.8	5.8	96	79	89	88	0.4	2.2	1.0	1.2	10	8	0	WSW 2	WSW 4	S 2
24	95.4	99.4	106.5	100.4	7.5	10.1	5.4	7.1	11.0	5.4	96	95	91	94	0.5	0.7	0.9	0.7	10	8	0	WSW 6	WSW 1	SW 1
25	110.2	111.2	110.4	110.6	2.7	9.9	8.9	7.6	11.0	2.5	96	64	92	84	0.2	4.3	0.9	1.8	0	9	10	SSW 1	SW 3	S 1
26	108.9	108.1	106.0	107.7	7.2	13.1	7.9	9.0	14.4	6.7	99	77	93	90	0.2	3.5	0.7	1.5	10	7	0	SSW 1	SSW 2	S 1
27	104.1	104.1	103.8	104.0	5.9	8.5	8.8	8.0	9.2	5.7	98	92	92	94	0.2	0.9	0.9	0.7	10	10	10	SW 2	SW 2	S 1
28	103.2	103.0	103.0	103.1	7.4	12.2	8.2	9.0	12.6	5.0	93	78	89	87	0.8	3.2	1.2	1.7	10	7	0	SSW 3	S 3	S 1
29	101.8	102.2	101.4	101.8	8.0	12.4	8.8	9.5	13.4	6.4	89	77	88	85	1.2	3.4	1.4	2.0	10	10	0	S 2	SW 2	S 1
30	99.1	98.9	99.9	99.3	6.4	13.2	11.6	10.7	13.7	6.0	92	73	87	84	0.7	4.2	1.8	2.2	7	8	10	S 4	SW 2	SW 1
31	99.0	97.2	94.7	97.0	9.6	12.4	11.2	11.1	12.7	9.3	92	80	85	86	1.0	2.9	2.0	2.0	10	10	10	SW 1	SW 2	SW 2
M	103.7	104.0	104.2	104.0	6.7	11.6	8.1	8.6	12.5	5.4	94	77	90	87	0.6	3.3	1.1	1.7	8.5	8.2	5.1	2.0	2.9	1.7

Wałcz $H_s = 111$ m $H_b = 113{,}8$ m $h_w = 10$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	6	15.8	•	–	▽ 0^{00}–1^{16} • 2^{15}–3^{35} • 14^{04}–30 • 11^{15}–13^{42} ▽ 15^{18}–16^{20}, 17^{41}–18^{08}. = n – 24
2	7	2.2	•	–	• 17^{05}–17 20^{51}–24. = 0^{00}–8^{40} 17^{40}–n, ⌒² n – 9^{20}
3	7	1.9	•	–	• 0^{00}–18 6^{35}–8^{35} ▽ 12^{10}–25. = n – 10^{30}
4	8	•	•	–	= 0^{30}–7^{25} ≡ ^{0}–7^{50} = –24
5	7	2.1	•	–	• 21^{52}–22^{49}. = 0^{00}–8^{45}, 23^{30}–24, ⌒² n – 9^{50}
6	7	•	•	–	= 0^{00}–11^{40}, 23^{30}–24
7	8	•	•	–	= 0^{00}–8^{20}, 23^{10}–24. ⌒² n – 10^{30}
8	8	•	•	–	= 0^{00}–9^{30}, 22^{20}–24. ⌒² n – 9^{40}
9	7	4.9	•	–	= 0^{00}–9^{20}
10	7	•	•	–	• 0^{42}–1^{06} • ^{1}–2^{07} • ^{0}–3^{24}. = 4^{20}–9^{15} 19^{40}–24
11	7	0.3	•	–	• ^{0} 19^{32}, 20^{15}–21^{05} 21^{30}, 22^{10}. = 0^{00}–9^{20}. ⌒² n – 9^{40}
12	7	2.4	•	–	• ^{0} 2^{30}–3^{18} 8^{48}–9^{25} ▽ 11^{06}–38, 16^{10}–17^{34}. ≫ 14^{10}–18^{20}. = n – 9^{30}
13	7	2.3	•	–	▽ 12^{59}–13^{28}, 19^{27}–31 23^{10}–24
14	7	0.0	•	–	▽ 0^{00}–41. = 1^{20}–9^{40}
15	7	5.6	•	–	• ^{0} 7^{36} 9^{15}–11^{08} • ^{1}–11^{17} ▽ 13^{55}–14^{25}, 14^{33}–15^{20}, 18^{26}–38
16	7	0.9	•	–	• ^{0} 8^{10}–36 ▽ 16^{03}–16 17^{08}–30. = 19^{20}–24
17	7	1.3	•	–	• ^{0} 6^{15}–8^{20}, 8^{26}–9^{44}, 10^{07}–11^{36}, 11^{41}–12^{21}. = 0^{00}–12^{20}, 21^{35}–24
18	7	•	•	–	= 0^{00}–9^{30}. ⌒² n – 10^{10}
19	6	1.1	•	–	c ^{0} 13^{10}–30 14^{28}–15^{10} 16^{20}. = 1^{30}–7^{32} ≡ ^{0}–8^{45} = –24
20	7	•	•	–	= 0^{00}–9^{30}. ⌒² n – 9^{20}
21	7	•	•	–	= n – 8^{40}, ⌒² n – 9^{30}
22	6	7.2	•	–	• ^{0} 8^{07}–36 ▽ 14^{30}–15^{25} • ^{0} 20^{06}–24, 23^{23}–24. = 7^{20}–15^{50} 16^{40}–24; ⌒⁰ n – 9^{50}
23	6	17.0	•	–	• ^{0} 0^{00}–2^{34} • ^{1} 4^{10}–20 • ^{0} 10^{19}–19^{43} 20^{30}–21^{35}. = 0^{00}–24
24	7	2.0	•	–	▽ 17^{38}–49, 19^{29}–41, 20^{15}–22, 20^{48}–21^{15}, 21^{49}–22^{15}, 22^{35}–23^{20}, ≫ 20^{35}–21^{10}. = 0^{00}–8^{30}; ⌒² n – a
25	7	0.2	•	–	
26	7	0.4	•	–	• ^{0} 7^{38}–8^{42}. = n – 8^{42} 21^{30}–24
27	6	11.4	•	–	• ^{0} 13^{53} 17^{20}, 17^{38}–22^{15} • ^{1}–22^{45} • ^{0}–23^{30} ≫ 22^{20}–24. = 0^{00}–7^{20}
28	7	0.9	•	–	▽ 12^{04}–15, 12^{42}–47 14^{28}–39 14^{52}–57 15^{46}–54. ≫ 0^{00}–1^{30}, 2^{30}–7^{20}
29	7	6.3	•	–	▽ 8^{25}–46, 8^{55}–9^{35}, 16^{04}–11 16^{33}–17^{07} 17^{15}–21 21^{12}–26. = 18^{20}–24
30	6	5.4	•	–	▽ 3^{06}–18, 3^{43}–4^{12}, 9^{47}–10^{25}, 10^{38}–11^{03} 11^{15}–59 12^{08}–13^{21}. = 0^{00}–7^{40}, 21^{10}–24
31					
Σ	–	91.6	–	–	UWAGI.

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1	7	2.7	•	–	• ^{0} 9^{04}–12^{36} ▽ 14^{33}–15^{14}. = 0^{00}–8^{40}, 18^{30}–24, ⌒² n – a. ⌴ ^{1} 20^{30}–24
2	7	•	•	–	⌴ ^{1} 0^{00}–8^{30}. = 0^{00}–7^{30}
3	6	2.3	•	–	• ^{0} 10^{15}–11^{30}, 13^{40}–14^{05}, 14^{30} 15^{35}. = a – 21^{30}
4	7	4.2	•	–	▽ 4^{37}–6^{30}, 7^{37}–9^{12}, 9^{36}–10^{12}
5	7	3.0	•	–	• ^{0} 17^{23}–18^{38}, 19^{25}–23^{48}. = 19^{10}–24. ⌒¹ n – 9^{20}
6	7	0.0	•	–	• ^{0} 8^{20}–46. = 0^{00}–7^{30}
7	7	•	•	–	
8	7	•	•	–	= 6^{15}–9^{40}
9	7	•	•	–	= 5^{10}–6^{15} ≡ ^{0}–9^{30} = –24. ⌒² n – 10^{50}
10	7	•	•	–	= 0^{00}–10^{15}, 18^{30}–24. ⌴ ^{1} n – a ⌒² 18^{00}–24
11	7	•	•	–	= 0^{00}–5^{30} ≡ ^{1}–8^{15} ≡ ^{0}–9^{30} = –12^{10}, 18^{15}–19^{50} ≡ ^{0}–24; ⌒² 0^{00}–9^{30}
12	5	1.6	•	–	• ^{0} 8^{18}–10^{44} ≡ ^{0} 0^{00}–10^{20} = –14^{40}, 20^{10}–24
13	7	•	•	–	= 0^{00}–9^{30}, 16^{40}–20^{30} ≡ ^{0}–24. ⌒² n – 11^{15}
14	6	•	•	–	≡ ^{0} 0^{00}–5^{40} = –24
15	7	•	•	–	= 0^{00}–12^{15}, 17^{30}–21^{10}
16	7	•	•	–	
17	7	•	•	–	= 2^{20}–10^{15}, 23^{20}–24. ⌒² n – 10^{00}
18	7	•	•	–	= 0^{00}–3^{40}, 6^{20}–12^{20}
19	7	5.3	•	–	• ^{0} 20^{12}–21^{10} • ^{1}–21^{40} • ^{0}–24. ⌒² n – 11^{12}
20	7	•	•	–	• ^{0} 1^{24}–6^{35}. = n – 10^{30}
21	7	•	•	–	= 2^{30}–6^{19} ≡ ^{0}–9^{45} = –12^{40}, ⌒⁰ n – 9^{30}
22	7	•	•	–	= 18^{20}–24. ⌒² n – a
23	7	3.0	•	–	= 0^{00}–9^{40}. ⌒² n – 10^{20}
24	6	0.8	•	–	• ^{0} 2^{30}–7^{45}, 9^{40}, 11^{20} • 11^{35}–12^{08}
25	7	•	•	–	= n – 9^{50}, 20^{20}–24. ⌴ ^{1} n – 7^{40}
26	7	•	•	–	= 0^{00}–9^{40}, 21^{20}–24
27	5	•	•	–	= 0^{00}–7^{30} ≡ ^{1}–9^{10} ≡ ^{0}–11^{18} = –24; ⌒² n – 10^{20}
28	7	•	•	–	= 0^{00}–9^{40}
29	7	•	•	–	
30	7	0.0	•	–	• ^{0} 22^{15}–23^{10}. = 3^{30}–8^{20}
31	7	•	•	–	= n – 8^{20}
Σ	–	23.4	–	–	UWAGI.

Wałcz $\varphi = 53°17'$ $\lambda = 16°28'$ **Listopad – Novembre 1957**

DNI	CIŚNIENIE P=900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	89.2	88.6	92.1	90.0	9.6	12.5	8.8	9.9	12.6	8.8	84	74	95	84	1.9	3.7	0.6	2.1	10	10	1	S 2	SW 6	SSE 1
2	95.6	96.9	99.3	97.3	4.4	10.4	5.2	6.3	11.7	4.2	93	65	87	82	0.6	4.4	1.1	2.0	2	4	4	S 2	S 3	SSE 2
3	100.7	100.9	99.1	100.2	1.4	9.8	5.8	5.7	10.9	1.1	94	68	95	86	0.4	3.9	0.4	1.6	1	0	0	SSE 1	b 1	E 1
4	97.6	97.2	97.1	97.3	6.3	8.5	9.2	8.3	10.2	4.8	100	97	93	97	0.0	0.3	0.8	0.4	10 ≡	9	7	E 2	E 2	SE 1
5	95.2	91.3	91.9	92.8	4.2	13.1	6.7	8.7	14.4	3.9	98	75	92	88	0.1	3.8	0.9	1.6	10	9	10	SE 1	ENE 3	E 1
6	92.9	93.9	93.7	93.5	6.0	10.9	6.4	7.4	11.0	5.9	97	87	95	93	0.3	1.6	0.4	0.8	9	9	9	E 1	SE 2	ENE 1
7	89.7	90.8	94.3	91.6	6.8	10.2	8.6	8.6	10.6	4.4	97	90	94	94	0.3	1.2	0.6	0.7	10	10	10	NE 1	E 1	S 1
8	94.4	94.2	94.5	94.4	7.2	9.6	9.6	9.0	10.1	7.0	99	95	99	98	0.2	0.7	0.2	0.4	10	10	10	WNW 1	NNE 1	NE 1
9	93.3	93.4	94.8	93.8	7.8	8.8	6.7	8.5	9.6	7.5	97	92	94	94	0.3	0.9	0.6	0.6	10	10	10	NE 1	NE 2	ENE 2
10	96.8	97.9	100.8	98.5	8.2	9.2	9.8	9.2	10.1	8.0	97	93	82	91	0.3	0.8	2.2	1.1	10	10	10	NE 2	NE 4	NE 4
11	103.7	106.0	109.5	106.4	8.2	9.4	7.3	8.0	9.9	7.3	90	79	84	84	1.1	2.5	1.6	1.7	10	10	10	NE 4	NE 3	NNE 4
12	112.9	114.8	117.3	115.0	4.2	4.8	1.5	3.0	7.6	1.5	85	76	92	84	1.2	2.0	0.5	1.2	10	10	10	NNE 6	NE 4	NE 2
13	118.1	118.0	118.4	118.2	0.0	1.3	0.1	0.4	2.1	-0.9	86	76	80	81	0.9	1.6	1.3	1.3	10	9	10	NE 2	NE 2	NE 1
14	118.1	118.9	119.1	118.7	-0.5	0.0	-0.2	-0.2	0.2	-0.8	81	78	82	80	1.1	1.3	1.1	1.2	10	10	10	SE 1	NE 1	E 3
15	118.9	117.8	117.2	118.0	-3.1	-2.3	-2.4	-2.6	0.2	-3.1	88	87	98	91	0.6	0.7	0.1	0.5	10	10	10	E 3	E 2	E 1
16	116.9	117.9	119.0	117.9	-1.4	0.1	-0.2	-0.4	0.6	-2.4	97	92	94	94	0.2	0.5	0.4	0.4	10	10	10	NNE 1	NE 1	C 0
17	119.4	119.6	120.5	119.8	0.6	2.3	1.0	1.2	2.5	-0.5	88	71	87	82	0.8	2.0	0.9	1.2	10	10	10	E 1	ENE 4	NE 2
18	119.6	118.8	118.5	119.0	0.9	2.4	1.4	1.5	2.6	0.7	88	79	79	82	0.7	1.6	1.4	1.2	10	10	10	ENE 2	E 2	ENE 2
19	119.1	121.2	123.9	121.4	0.6	1.8	1.4	1.3	2.0	0.4	79	74	76	76	1.4	1.8	1.7	1.6	10	10	10	NE 2	NE 3	E 3
20	124.7	125.1	125.1	125.0	-1.6	3.4	-1.5	-0.3	3.9	-2.4	76	60	89	75	1.3	3.1	0.6	1.7	4	0	0	NNE 2	ESE 3	ESE 1
21	124.0	122.4	116.7	121.0	-5.3	3.6	-1.2	-1.0	3.9	-6.2	95	63	91	83	0.2	2.9	0.5	1.2	0	0	0	C 0	NE 1	E 1
22	107.8	104.5	102.6	105.0	-2.9	0.8	0.4	-0.3	1.1	-3.1	95	85	78	86	0.2	1.0	1.4	0.9	0	10	10	SE 2	SW 3	SSW 3
23	100.3	99.8	103.2	101.8	0.1	1.4	2.1	1.4	2.5	-0.2	90	96	95	94	0.7	0.3	0.4	0.5	10	10	8	S 3	S 3	W 4
24	107.2	105.8	105.1	106.0	0.7	3.3	5.0	3.5	5.2	0.0	94	97	94	95	0.4	0.2	0.5	0.4	10	10 ●	10	WSW 3	SW 4	SW 6
25	102.7	103.5	105.5	103.9	6.1	8.2	8.6	7.9	8.8	4.7	100	94	94	96	0.0	0.6	0.6	0.4	10 ●	10 ●	10	W 8	SW 6	W 4
26	106.5	106.9	105.0	106.1	7.7	8.1	6.6	7.2	8.6	6.5	98	97	88	94	0.1	0.3	1.1	0.5	10 ●	10 ●	10 ●	W 4	W 4	W 8
27	100.6	101.9	103.4	102.0	7.0	7.1	5.4	6.2	8.2	5.3	93	74	91	86	0.7	2.6	0.9	1.4	10	10	8	WSW 10	W 8	WSW 3
28	98.9	96.4	93.0	96.1	7.8	8.8	7.1	7.7	9.0	5.4	94	82	83	86	0.6	2.0	1.8	1.5	10 ●	10 ◞	10	W 10	W 8	W 9
29	98.1	104.4	115.7	106.1	1.0	1.2	-3.4	-1.2	7.1	-3.5	94	75	70	80	0.4	1.7	1.4	1.2	10 ✱	8	1	NW 8	NW 6	NW 3
30	119.7	119.6	119.7	119.7	-4.3	-0.9	-5.9	-4.2	-0.7	-7.1	89	83	94	89	0.5	1.0	0.2	0.6	3	8	1	NW 1	NW 3	NW 1
31																								
M	106.1	106.3	107.3	106.6	2.9	5.6	3.8	4.0	6.6	1.9	92	82	89	88	0.6	1.7	0.9	1.1	8.3	8.5	7.6	2.9	3.2	2.5

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1	116.7	113.4	111.6	113.9	-3.4	-1.7	0.6	-1.0	0.9	-7.4	92	88	98	93	0.4	0.7	0.1	0.4	9	10 ✱	10	W 3	W 2	W 1
2	112.8	114.0	114.2	113.7	1.0	3.4	2.2	2.2	4.3	0.4	98	91	98	96	0.2	0.7	0.2	0.4	10	8	10	NW 1	NW 2	W 2
3	110.6	109.3	110.7	110.2	2.9	4.3	2.6	3.1	4.7	2.2	100	97	96	98	0.0	0.3	0.3	0.2	10 ●	10	10	W 1	W 1	NW 1
4	109.8	108.5	106.4	108.2	1.7	3.3	3.8	3.2	4.1	1.6	96	91	95	94	0.3	0.6	0.4	0.4	10	10	10	WNW 1	W 1	W 3
5	105.0	106.3	110.2	107.2	5.6	6.3	2.2	4.1	6.5	2.2	85	81	95	87	1.4	1.8	0.4	1.2	10	8	1	W 5	W 5	W 2
6	113.3	112.8	108.2	111.4	-2.3	-1.1	0.8	-0.4	2.2	-2.5	98	97	94	96	0.2	0.2	0.4	0.3	4	10 ≡	10	W 1	SSW 1	SSE 2
7	100.2	96.6	89.7	95.5	-0.2	1.1	-0.4	0.0	1.4	-1.1	92	90	92	91	0.5	0.6	0.5	0.5	10	10	10	SW 4	SW 1	SSW 2
8	73.9	64.3	60.0	66.1	0.6	3.2	6.2	4.0	8.5	-0.5	92	97	82	90	0.5	0.3	1.7	0.8	10	10 ●	1	SSE 4	SSW 4	W 8
9	62.0	72.5	82.1	72.2	2.5	0.2	-2.0	-0.5	6.4	-2.0	91	92	75	86	0.6	0.5	1.4	0.8	10	10	0	SW 8	W 3	WSW 4
10	81.5	84.6	92.3	86.1	-2.0	-3.4	-6.0	-4.4	-2.0	-6.1	85	79	76	80	0.8	1.0	0.9	0.9	8	9	0	SW 2	NW 2	SW 3
11	95.2	91.2	87.6	90.7	-10.0	-5.3	-4.0	-5.9	-3.9	-10.2	94	77	66	79	0.2	0.9	1.5	0.9	0	9	10	SSW 1	NE 1	NE 2
12	84.6	83.4	83.0	83.7	-3.1	-0.8	-3.4	-2.7	-0.4	-4.5	79	83	94	85	1.0	1.0	0.3	0.8	9	9	7	NE 3	NE 3	NE 1
13	80.2	77.6	72.8	76.9	-1.3	1.0	0.8	0.3	1.3	-3.5	95	98	98	97	0.3	0.2	0.2	0.2	10	10 ≡	10 ≡	NE 2	NE 2	NNE 2
14	72.8	79.6	91.4	81.3	0.6	0.6	-0.1	0.2	1.4	-0.1	96	86	68	83	0.3	0.9	2.0	1.1	10 ●	10	10	NNW 2	N 5	W 8
15	103.9	109.6	113.1	109.5	-2.9	-2.7	-8.6	-5.7	-0.1	-8.8	77	63	83	74	1.1	1.9	0.5	1.2	10	7	0	NE 3	NE 7	NE 1
16	116.3	116.5	114.8	115.9	-9.9	-6.5	-9.6	-8.9	-6.1	-11.2	91	67	75	78	0.3	1.2	0.7	0.7	0	1	0	E 1	NE 1	ESE 1
17	111.9	109.1	109.0	109.9	-12.7	-7.6	-7.3	-8.7	-7.1	-12.7	83	67	79	77	0.4	1.1	0.7	0.7	0	0	10	NE 1	E 1	N 1
18	109.9	110.3	110.1	110.1	-6.8	-5.8	-5.1	-5.7	-5.1	-7.5	83	82	85	83	0.6	0.7	0.6	0.6	10	10	10	SW 1	SW 1	SE 1
19	110.0	112.3	115.5	112.6	-4.8	-4.3	-2.4	-3.5	-2.2	-5.4	86	84	93	88	0.6	0.7	0.3	0.5	10	10	10	ESE 3	E 2	SSE 2
20	117.1	117.2	114.4	116.2	-0.6	1.5	-0.1	0.2	1.7	-2.5	97	91	90	93	0.2	0.6	0.7	0.5	10	5	0	SW 1	SW 2	SW 4
21	109.7	109.4	112.1	110.4	1.0	3.6	2.4	2.4	3.8	-1.1	81	75	96	84	1.3	2.0	0.3	1.2	10	10	10	SW 4	SW 3	SW 1
22	110.9	110.8	110.3	110.7	1.8	2.4	2.1	2.1	2.6	1.6	98	98	98	98	0.2	0.2	0.1	0.2	10	10 ≡	10 ≡	S 2	S 2	SSW 1
23	106.2	103.7	101.8	103.9	0.0	-1.5	-2.4	-1.6	2.1	-2.4	98	90	85	91	0.1	0.5	0.8	0.5	10	8	0	ESE 2	SE 3	E 1
24	101.5	102.1	103.7	102.4	-2.8	-0.4	-3.2	-2.4	0.4	-3.2	82	76	88	82	0.9	1.4	0.6	1.0	6	8	0	SE 2	S 2	E 1
25	103.5	102.8	103.2	103.9	-3.8	-1.8	-1.2	-2.0	-0.7	-5.0	87	83	84	85	0.6	0.9	0.9	0.8	7	7	0	E 1	SE 1	WSW 2
26	107.2	109.4	110.9	109.2	-0.4	1.4	1.6	1.0	1.6	-2.2	94	96	98	96	0.3	0.3	0.2	0.3	10	10 ≡	10 ≡	SW 2	SW 1	SW 1
27	110.7	109.7	108.1	109.5	1.2	1.6	1.5	1.4	2.3	0.8	96	96	98	97	0.3	0.3	0.1	0.2	10	10	10	SW 2	SW 2	WSW 2
28	102.9	98.1	94.2	98.4	2.4	3.0	2.9	2.8	3.2	1.4	98	88	96	94	0.2	0.9	0.2	0.4	10	9	10 ●	SW 1	SW 2	SW 2
29	91.4	90.3	82.9	88.2	2.4	2.6	3.0	2.8	3.3	2.4	82	93	90	88	1.3	0.6	0.8	0.9	10	10 ●	10 ●	WSW 6	SW 4	SW 8
30	81.9	80.0	81.0	81.0	2.8	1.8	0.8	1.6	3.0	0.8	84	93	94	90	1.2	0.6	0.4	0.7	8	10 ●	10 ✱	SW 8	SSW 4	SW 3
31	84.3	85.1	85.3	85.0	0.7	1.3	1.0	1.0	1.4	0.6	85	76	87	83	1.0	1.6	0.9	1.2	10	8	7	WSW 3	SW 3	SW 4
M	99.9	99.7	99.8	99.8	-1.3	0.0	-0.7	-0.7	1.3	-2.8	90	86	89	88	0.6	0.8	0.5	0.7	8.4	8.6	6.6	2.6	2.2	2.3

Wartcz $H_s = 111{,}m$ $H_b = 113{,}8\,m$ $h_w = 10\,m$ **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	
2	7	.	.	–	= $3^{20}-7^{30}$
3	7	.	.	–	= $3^{20}-9^{30}$ $21^{10}-24$; ⌴^{0} n – 9^{00}
4	4	.	.	–	= $0^{00}-4^{50}$ ≡$^{0}-6^{30}$ ≡$^{1}-7^{40}$ ≡$^{0}-10^{45}$ =–24
5	7	.	.	–	= $0^{00}-2^{45}$ ≡$^{0}-4^{30}$ =– 12^{10}
6	7	.	.	–	= $1^{20}-7^{50}$ $17^{30}-22^{50}$ ≡^{0}–24
7	6	.	.	–	≡^{0} $0^{00}-4^{50}$ =–24
8	6	1.1	.	–	•^{0} 15^{17} 18^{10} 21^{20} 22^{18} = $0^{00}-24$; ⌒^{1} n – p.
9	6	0.8	.	–	•^{0} 14^{28} 15^{10} = $0^{00}-24$
10	6	.	.	–	= $0^{00}-14^{15}$
11	7	.	.	–	= $2^{35}-6^{10}$
12	7	.	.	–	
13	7	.	.	–	
14	7	.	.	–	
15	7	.	.	–	= $14^{10}-24$
16	6	.	.	–	= $0^{00}-24$
17	7	.	.	–	= $0^{00}-9^{10}$
18	7	.	.	–	
19	7	.	.	–	
20	7	.	.	–	
21	7	.	.	–	= $3^{10}-9^{20}$ ⌴^{2} n – 10^{40}
22	7	0.2	.	–	•^{0} $16^{20}-18^{10}$ ⌴ n – 11^{10}
23	6	0.3	.	–	*^{0} $9^{22}..50$ •*^{0} $10^{02}-11^{06}$ •^{0} 15^{30} 17^{15} $17^{24}-18^{25}$, 19^{20} 20^{20} = $7^{20}-24$
24	6	0.8	.	–	• $12^{10}-14^{28}$ •^{0} $15^{38}-19^{25}$ $21^{25}-23^{30}$ •^{0}–24; = $0^{00}-19^{30}$, $21^{20}-24$
25	6	1.0	.	–	•^{0} $0^{00}-4^{45}$, 7^{20} 13^{30} $13^{50}-19^{10}$, = $0^{00}-24$
26	6	1.1	.	–	•^{0} 0^{10} $2^{20}-21^{15}$, 23^{25} 24; = $0^{00}-24$
27	7	1.2	.	–	•^{0} $0^{00}..20$, $0^{30}-6^{35}$ $22^{25}-24$; = $0^{00}-9^{30}$
28	7	2.8	.	–	•^{0} $0^{00}-15$, •^{0} $0^{40}-2^{25}$, $3^{35}-7^{15}$ $8^{05}-10^{42}$
29	7	1.9	.	–	•^{0} $0^{10}-2^{17}$ $4^{30}-6^{10}$ ⁑$^{0}-7^{15}$ *^{0} $9^{04}-42$, $11^{22}-12^{07}$, $13^{02}-14^{25}$, $14^{50}-15^{15}$
30	7	0.0	.	–	*^{0} $10^{05}-40$
31					
Σ	–	11.2	–	–	UWAGI

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1	6	2.3	.	–	*^{0} $10^{26}-15^{42}$ •^{0} 21^{25} 23^{35} = $18^{20}-24$
2	7	0.3	2	–	•^{0} $15^{40}-17^{25}$ = $0^{00}-10^{20}$, $14^{10}-24$
3	5	0.4	.	–	•^{0} $6^{25}-12^{38}$ = $0^{00}-24$
4	6	1.2	.	–	•^{0} $7^{20}-9^{35}$ •^{0} $16^{50}-17^{45}$ = $0^{00}-24$
5	7	.	.	–	= $0^{20}-7^{30}$
6	2	.	.	–	= $5^{15}-11^{28}$ ≡$^{0}-15^{15}$ =–24; ⌴^{2} n – 10^{30}
7	6	0.2	.	–	*^{0} 17^{40} $18^{20}-19^{30}$ = $8^{20}-$ n
8	6	15.4	.	–	*^{0} $2^{34}-4^{19}$ $7^{42}-8^{32}$ •^{0} $9^{19}-19^{36}$ = n – 19^{40}
9	7	2.9	.	–	•^{0} $6^{05}-7^{38}$ *^{0} 8^{15-34} •$^{0}-9^{09}$ *$^{0}-9^{46}$ •^{0} $10^{28}-11^{16}$ *$^{1}-12^{16}$ *$^{0}-12^{33}$
10	7	3.0	.	–	*^{0} $9^{46}-10^{05}$ *$^{1}-10^{52}$ *$^{0}-12^{29}$
11	7	.	4	–	
12	7	.	4	–	
13	3	2.3	3	–	= $3^{10}-8^{30}$ ≡$^{0}-24$
14	7	1.6	.	–	•^{0} $2^{34}-5^{38}$ $6^{41}-8^{18}$ △ $9^{25}-10^{07}$ ⁑$^{0}-11^{10}$ *^{0} $11^{38}-12^{05}$, 14^{40}..15^{15}; ≡^{0} 0^{00-20} =–12^{30}
15	7	.	pł.	–	
16	7	.	pł.	–	
17	7	.	pł.	–	
18	7	.	pł.	–	
19	7	.	.	–	= $13^{30}-24$
20	6	.	.	–	= $0^{00}-18^{00}$ ≡$^{0}-9^{15}$ =–13^{30}
21	7	.	.	–	= $7^{20}-8^{30}$, $18^{20}-24$
22	3	.	.	–	= $0^{00}-7^{50}$ ≡$^{0}-8^{30}$ ≡$^{1}-12^{15}$ ≡$^{0}-13^{45}$ =–17^{55} ≡^{0}–24
23	7	.	.	–	≡^{0} $0^{00}-6^{10}$ =–9^{10}
24	7	.	.	–	
25	7	.	.	–	
26	3	.	.	–	= $4^{20}-7^{48}$ ≡^{0}–24
27	6	0.3	.	–	•^{0} $7^{19}-10^{31}$ $13^{24}-15^{16}$ 16^{37}, ≡^{0} $0^{00}-2^{45}$ =–24
28	7	3.4	.	–	•^{0} $17^{10}-21^{27}$ = $0^{00}-12^{20}$
29	6	3.2	.	–	•^{0} 9^{22-45} 12^{38} 13^{06} 17^{28} 18^{10}, $18^{20}-24$
30	6	6.4	.	–	•^{0} $0^{00}-1^{10}$, $9^{21}-11^{04}$, ⁑$^{0}-12^{21}$ •$^{0}-13^{18}$, $15^{24}-16^{16}$ ⁑$^{0}-17^{19}$ •$^{0}-18^{26}$ *^{0} $19^{14}-21^{04}$
31	7	.	.	–	
Σ	–	43.1	–	–	UWAGI.

Bydgoszcz $\varphi = 53°07'$ $\lambda = 17°58'$ **Styczeń – Janvier 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	107.9	108.3	108.4	108.2	−5.6	−4.5	−5.5	−5.3	−4.2	−6.5	-	-	-	-	-	-	-	-	10	10	10	C 0	C 0	ENE 3
2	104.8	104.0	106.3	105.0	−2.8	−1.0	−0.8	−1.4	0.0	−6.1	-	-	-	-	-	-	-	-	10	10	10 ≡	E 5	E 1	SSW 2
3	111.4	113.0	113.1	112.5	−0.4	0.6	0.4	0.2	0.9	−2.3	-	-	-	-	-	-	-	-	10	10	10	C 0	W 2	S 2
4	113.7	114.8	114.5	114.3	−3.0	−1.4	0.6	−0.8	0.9	−5.3	-	-	-	-	-	-	-	-	10 ≡	9	9	SE 3	SE 2	SSE 4
5	111.7	107.0	105.0	107.9	1.4	3.0	4.9	3.6	5.4	−2.2	-	-	-	-	-	-	-	-	10	10	10 ≡	SSW 5	SSW 7	WSW 4
6	99.8	98.1	101.1	99.7	7.4	9.8	4.8	6.7	10.0	4.2	-	-	-	-	-	-	-	-	10 ●	9	0	WSW 6	W 6	W 8
7	106.8	112.6	117.2	112.2	4.6	5.2	4.6	4.8	5.5	2.6	-	-	-	-	-	-	-	-	10	9	10	NW 8	NW 6	NW 5
8	116.8	115.4	113.2	115.1	4.8	5.4	6.9	6.0	7.1	3.4	-	-	-	-	-	-	-	-	10 ●	10	10 ●	W 7	W 7	W 8
9	111.5	109.9	107.1	109.5	7.1	8.0	7.3	7.4	8.2	6.0	-	-	-	-	-	-	-	-	10	10	10	W 7	W 8	WSW 5
10	103.5	101.7	102.5	102.6	5.3	5.5	3.2	4.3	7.6	(2.5)	-	-	-	-	-	-	-	-	8	10	9	W 5	W 7	WNW 6
11	105.0	109.1	110.6	108.2	1.8	2.1	−0.4	0.8	3.2	−1.0	-	-	-	-	-	-	-	-	9	9	2	W 4	WNW 6	W 5
12	105.3	98.6	92.6	98.8	−1.2	0.2	1.2	0.4	1.2	−2.0	-	-	-	-	-	-	-	-	10	10 ✳	10	WSW 5	SW 7	SW 3
13	92.6	96.6	103.4	97.5	0.2	0.6	−1.4	−0.5	1.3	−1.6	-	-	-	-	-	-	-	-	10 ✳	10 ✳	10 ✳	C 0	ENE 3	NE 5
14	112.0	117.0	120.6	116.5	−6.6	−6.9	−8.7	−7.7	−0.9	−8.9	-	-	-	-	-	-	-	-	10 ✳	10	9	NE 7	ENE 5	NE 5
15	121.0	120.3	120.1	120.5	−8.8	−7.8	−8.1	−8.2	−7.1	−10.0	-	-	-	-	-	-	-	-	10	9 ✳	10	NE 4	ENE 5	NNE 3
16	122.5	123.4	123.8	123.2	−15.3	−8.2	−8.8	−10.3	−6.7	−18.6	-	-	-	-	-	-	-	-	0	4	10	C 0	C 0	C 0
17	122.8	122.9	123.2	123.0	−5.0	−2.2	−1.4	−2.5	−0.9	−9.5	-	-	-	-	-	-	-	-	10	10	10	WNW 2	W 3	NW 4
18	121.5	120.6	118.8	120.3	−3.2	−2.5	−2.8	−2.8	−0.8	−4.6	-	-	-	-	-	-	-	-	10	9	10	W 3	WNW 4	WSW 3
19	119.4	120.9	121.8	120.7	−1.9	−1.1	−2.2	−1.8	−0.7	−4.3	-	-	-	-	-	-	-	-	10	10	10 ✳	WSW 2	W 2	W 4
20	119.8	118.1	115.4	117.8	−1.3	0.2	−0.1	−0.3	0.7	−2.4	-	-	-	-	-	-	-	-	10	10 ●	10	SW 6	WSW 5	W 6
21	111.2	112.4	113.8	112.5	−5.2	−1.4	−2.3	−2.8	−0.9	−5.8	-	-	-	-	-	-	-	-	3	8	10	WSW 6	WSW 7	WSW 6
22	113.8	112.6	109.6	112.0	−8.0	−1.5	−5.0	−4.9	−0.3	−9.0	-	-	-	-	-	-	-	-	0	1	0	WSW 5	SW 4	SW 3
23	109.5	110.6	110.8	110.3	−6.0	−1.8	−7.1	−5.5	−0.4	−9.1	-	-	-	-	-	-	-	-	9	5	0	SW 4	SW 5	SW 1
24	107.0	103.9	101.5	104.1	−7.2	−1.0	−3.2	−3.6	−0.8	−10.6	-	-	-	-	-	-	-	-	9	10	10	ESE 3	E 5	E 1
25	99.1	100.2	104.1	101.1	−3.0	−0.9	0.4	−0.8	0.5	−3.9	-	-	-	-	-	-	-	-	10 ✳	10	10	C 0	SSW 3	WSW 4
26	109.7	110.9	107.4	109.3	0.6	1.0	0.0	0.4	2.3	−1.0	-	-	-	-	-	-	-	-	10	5	0	W 2	SSW 3	S 6
27	102.1	104.2	108.7	105.0	1.8	4.3	2.4	2.7	5.8	−0.2	-	-	-	-	-	-	-	-	10	8	0	SW 4	WSW 5	WSW 6
28	107.8	113.3	120.2	113.8	1.0	1.3	1.0	1.1	2.7	−1.2	-	-	-	-	-	-	-	-	10	10 ●	9	SW 4	WNW 4	NW 1
29	121.5	120.8	118.7	120.3	−1.4	1.2	1.2	0.6	2.4	−2.5	-	-	-	-	-	-	-	-	5	10	10	SW 2	SW 4	SSW 3
30	115.4	112.5	112.1	113.3	−0.8	2.7	1.4	1.2	3.8	−1.2	-	-	-	-	-	-	-	-	3	8	10	SSW 3	SW 4	SW 1
31	112.1	113.4	112.9	112.8	1.0	2.4	1.7	1.7	2.7	−0.5	-	-	-	-	-	-	-	-	10	10	10 ● ≡	SW 2	SSW 4	WSW 3
M	110.9	111.2	111.6	111.2	−1.6	0.4	−0.5	−0.6	1.6	−3.6	-	-	-	-	-	-	-	-	8.6	8.8	8.0	3.7	4.3	3.9

Luty – Février

1	107.9	107.1	106.4	107.1	1.4	3.8	5.6	4.1	5.8	0.1	-	-	-	-	-	-	-	-	10 ●	10 ●	10 ●	SE 3	S 6	SSW 6
2	109.7	114.4	116.8	113.6	7.4	8.9	4.1	6.1	9.0	3.6	-	-	-	-	-	-	-	-	8	9 ⊙	10	WSW 5	W 6	W 1
3	116.5	118.2	119.5	118.1	2.1	4.1	−2.0	0.6	6.7	−2.4	-	-	-	-	-	-	-	-	10 ≡	10 ●	0 ≡	C 0	C 0	C 0
4	117.4	114.2	113.1	114.9	−2.0	1.6	4.0	1.9	5.0	−3.9	-	-	-	-	-	-	-	-	9	10 ●	10 ≡	ESE 1	SSE 5	WNW 2
5	113.2	111.7	109.6	111.5	1.2	8.2	4.3	4.5	10.4	0.1	-	-	-	-	-	-	-	-	10 ≡	8	0	WSW 3	SW 5	SSW 2
6	106.9	103.5	102.7	104.4	−0.4	7.1	4.7	4.0	7.8	−1.2	-	-	-	-	-	-	-	-	0	2	9	SSW 2	SSW 5	SW 5
7	105.1	105.1	106.2	105.5	5.0	7.9	5.8	6.1	9.0	3.6	-	-	-	-	-	-	-	-	10	7	9	WNW 4	WSW 8	W 5
8	103.6	99.1	93.1	98.6	1.0	4.9	6.2	4.6	6.6	0.0	-	-	-	-	-	-	-	-	10	10 ●	10 ●	WSW 3	SW 4	WSW 6
9	91.0	90.4	93.5	91.6	6.6	7.8	6.4	6.8	8.4	3.1	-	-	-	-	-	-	-	-	10	10 ●	10	WSW 4	WSW 6	W 7
10	96.2	98.0	97.8	97.3	2.6	5.0	1.8	2.8	6.8	1.4	-	-	-	-	-	-	-	-	5	3	9	W 6	WNW 3	C 0
11	97.8	101.0	103.9	100.9	4.2	4.8	2.9	3.7	5.7	−0.4	-	-	-	-	-	-	-	-	10	10	10	W 2	WNW 6	W 4
12	102.9	99.8	96.0	99.6	−0.2	5.1	4.8	3.6	5.5	−2.6	-	-	-	-	-	-	-	-	8	10	10	W 3	S 7	S 4
13	92.2	88.5	79.9	86.9	2.8	7.8	6.9	6.1	7.9	1.3	-	-	-	-	-	-	-	-	10	9	10 ●	SSW 3	SSW 6	SSE 9
14	76.7	77.4	78.8	77.6	6.0	9.2	5.4	6.5	9.3	4.2	-	-	-	-	-	-	-	-	10	9	10 ●	SW 8	SW 6	SW 6
15	78.9	79.0	73.1	77.7	3.4	7.1	4.6	4.9	8.0	2.1	-	-	-	-	-	-	-	-	6	6 ⊙	10 ●	SSW 5	S 7	E 3
16	80.9	85.5	90.7	85.7	3.7	4.2	2.6	3.3	5.3	2.5	-	-	-	-	-	-	-	-	10 ●	6	5	W 6	W 5	SW 5
17	95.1	97.0	96.3	96.1	0.6	2.0	1.2	1.2	2.9	−1.0	-	-	-	-	-	-	-	-	10	10	10 ●	WSW 4	SSW 5	SSW 3
18	98.2	96.5	91.0	95.2	0.6	7.6	4.1	4.1	7.7	−1.2	-	-	-	-	-	-	-	-	10	7	10 ●	C 0	SE 5	ENE 2
19	89.5	96.7	102.5	96.2	2.6	4.6	0.2	1.9	4.8	−0.3	-	-	-	-	-	-	-	-	10 ●	8	3	NW 5	WNW 6	WSW 4
20	102.9	102.3	100.3	101.8	0.1	0.7	1.8	1.1	2.4	−1.6	-	-	-	-	-	-	-	-	10	10 ✳	9	SW 1	S 1	E 1
21	98.0	99.9	103.4	100.4	0.2	6.8	3.0	3.2	7.9	−0.8	-	-	-	-	-	-	-	-	9	8	10	SE 1	SW 5	WNW 4
22	107.3	107.7	105.6	106.9	−0.6	1.9	−1.5	−0.4	4.2	−2.3	-	-	-	-	-	-	-	-	8	9	3	WNW 2	WNW 3	NNW 2
23	104.9	105.8	104.0	104.9	−1.3	0.6	−0.2	−0.3	1.7	−2.4	-	-	-	-	-	-	-	-	7	10	6 ✳	C 0	WNW 3	W 2
24	99.7	95.7	96.7	97.4	−6.0	1.9	−0.2	−1.1	2.5	−6.9	-	-	-	-	-	-	-	-	4	5	10	C 0	E 4	E 2
25	100.1	100.1	99.8	100.0	−3.4	1.4	−0.2	−0.6	1.9	−4.1	-	-	-	-	-	-	-	-	6	7	10	NE 1	E 4	NE 3
26	105.7	109.5	112.0	109.1	−1.0	3.2	0.3	0.7	3.5	−4.3	-	-	-	-	-	-	-	-	10	6	9	NNE 1	NNE 2	C 0
27	114.4	116.5	118.4	116.4	−2.5	3.0	−1.8	−0.8	3.3	−5.5	-	-	-	-	-	-	-	-	8	7	6	NNE 1	SE 1	C 0
28	121.7	124.0	127.0	124.2	−1.6	0.5	−1.5	−1.0	1.0	−2.6	-	-	-	-	-	-	-	-	9 ✳	10 ✳	7	SSE 2	NNW 3	C 0
29																								
30																								
31																								
M	101.2	101.6	101.4	101.4	1.2	4.7	2.6	2.8	5.8	−0.8	-	-	-	-	-	-	-	-	8.5	8.1	8.0	2.7	4.5	3.1

Bydgoszcz $H_s = 70\ m$ $H_b = 70{,}5\ m$ $h_w = 70\ m$ **Styczeń – Janvier 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	11	-	= 0⁰⁰ – 24
2	6	.	10	-	= 0⁰⁰ – 16²⁰ ≡⁰ – 21³² = – 24
3	5	0.3	10	-	*⁰ 13³⁰ – 15²⁵ = 0⁰⁰ – 24
4	6	.	9	-	= 0⁰⁰ – 5⁴⁸ ≡⁰ – 9⁵⁰ = – 24
5	5	9.1	8	-	•⁰ 10⁴⁶ – 18¹⁵ •⁰ – 20²⁰ = 0⁰⁰ – 2³⁰, 5³⁰ – 20⁴⁵ ≡⁰ – 24
6	7	0.3	1	-	•⁰ 2⁴⁵ – 4³⁰ •⁰ – 7²⁰ •⁰ – 10⁰⁵ ≡⁰ 0⁰⁰ – 2⁴⁵
7	8	0.0	.	-	
8	6	1.3	.	-	•⁰ 5⁴⁵ – 12⁴⁰ •⁰ 15²⁰ – 21³⁰ = 12⁴⁰ – 15²⁰
9	6	0.0	.	-	= 6³⁰ – 23²⁰
10	7	0.0	.	-	•⁰ 3³⁵ – 5⁰⁵, 15⁵⁰ – 16⁰⁵, 16⁴⁵ – 5.3
11	8	.	.	-	
12	6	4.9	.	-	*⁰ 5⁴⁶ – 9¹⁵, 11³⁵ – 17⁴⁰, 22⁴⁰ – 24, = 20³⁰ – 24
13	3	4.0	3	-	*⁰ 0⁰⁰ – 24
14	7	0.0	6	-	*⁰ 0⁰⁰ – 7³⁰ 9⁵⁰ – 11²⁵ = 7³⁰ – 8³⁰
15	6	0.3	7	-	*⁰ 9²⁵ – 20⁵⁰, = 23³⁵ – 24
16	6	0.0	6	-	= 0⁰⁰ – 23⁴⁰ ≡⁰ – 24
17	5	.	6	-	*⁰ 3³⁰ – 4⁴⁵, ≡⁰ 0⁰⁰ – 1⁴⁰ = – 14⁴⁰ ≡⁰ – 18⁵³ = – 24
18	6	.	6	-	= 0⁰⁰ – 24
19	7	0.0	6	-	*⁰ 20²² – 24 = 0⁰⁰ – 10³⁰, 14⁴⁰ – 24
20	5	0.0	7	-	*⁰ 0⁰⁰ – 17 •⁰ 10³⁵ – 13³⁵, = 0⁰⁰ – 21³⁰
21	6	.	5	-	= 3³⁰ – 21²⁵
22	6	.	5	-	= 4³⁰ – 13⁴⁰, 16³⁰ – 24
23	7	.	5	-	= 0⁰⁰ – 24
24	6	0.1	5	-	= 0⁰⁰ – 24
25	5	0.0	5	-	*⁰ 4³⁰ – 8³⁸, = 0⁰⁰ – 24
26	5	1.2	5	-	= 0⁰⁰ – 7⁴⁰ ≡⁰ – 12³⁵ = – 24
27	6	0.3	.	-	•⁰ 4⁰⁵ – 8⁰⁵, = 0⁰⁰ – 8⁴⁰ ≡⁰ – 11⁴⁵ = – 13³⁰
28	6	0.7	.	-	*⁰ 7¹¹ – 8³⁵ *⁰ 11³⁰ – 14¹⁵
29	6	.	pż.	-	= 2³⁰ – 24
30	7	0.0	pż.	-	*⁰ 17⁴² – 45, = 0⁰⁰ – 4³⁰, 7¹⁰ – 12⁴⁰, 15³⁰ – 24
31	4	1.9	pż.	-	•⁰ 16¹⁰ – 24, = 0⁰⁰ – 7²⁵ ≡¹ – 12⁵⁰ = – 17⁵⁰ ≡¹ – 24
Σ	–	24.4	–	-	UWAGI

Luty – Février

1	5	3.0	.	-	•⁰ 0⁰⁰ – 40 •⁰ – 9⁴⁰ •⁰ 11¹⁸ – 38 •⁰ – 24 ≡¹ 0⁰⁰ – 1⁴⁰ = 9⁴⁰ – 11¹⁸
2	7	.	.	-	•⁰ 0⁰⁰ – 1³⁰ = 1³⁰ – 6³⁰, 21³⁰ – 24
3	5	0.0	.	-	•⁰ 10²⁰ – 11⁴⁰ •⁰ – 13³⁰ = 0⁰⁰ – 5⁴⁰ ≡⁰ – 8³⁵ ≡¹ – 11⁴⁰ = 13³⁰ – 16¹⁰ ≡¹ – 24
4	4	2.5	.	-	•⁰ 9⁴⁰ – 13⁴⁹ •⁰ 19¹⁰ – 20⁵¹ ≡⁰ 0⁰⁰ – 6⁴⁵ = – 7³⁰, 13⁴⁹ – 16²⁰ ≡¹ – 24
5	6	.	.	-	≡¹ 0⁰⁰ – 9³⁹ = – 24
6	7	0.0	.	-	•⁰ 22⁰⁵ – 15, = 0⁰⁰ – 11³⁰, ⌴ 5⁰⁰ – 9³⁵
7	7	.	.	-	
8	6	4.1	.	-	•⁰ 11⁴⁵ – 24, = 5²⁰ – 11⁴⁵
9	6	0.0	.	-	•⁰ 0⁰⁰ – 4¹⁵, 12⁴⁵ – 14³⁸, = 4¹⁵ – 11⁴⁰, 14³⁸ – 17³⁰
10	7	1.3	.	-	•⁰ 21³⁵ – 24
11	7	0.4	.	-	•⁰ 0⁰⁰ – 2¹⁰ 7⁴⁰ – 9²⁵ = 2¹⁰ – 7⁴⁰, 9²⁵ – 11¹²
12	7	1.1	.	-	•⁰ 19⁴⁰ – 20²⁰, 21⁴⁰ – 24, = 14³⁰ – 24
13	7	4.1	.	-	•⁰ 0⁰⁰ – 1⁴⁰, 20²⁰ – 24, = 7²⁰ – 8³⁰
14	7	2.6	.	-	•⁰ 0⁰⁰ – 40, 1⁵⁰ – 6³⁰ •⁰ 14⁴⁹ – 15¹¹, 17¹⁸ – 41, 20³⁹ – 21⁰⁶
15	7	4.7	.	-	•⁰ 15⁵⁰ – 21³⁵
16	6	0.0	.	-	•⁰ 2²⁵ – 7⁴⁰, = 10⁴⁰ – 13³⁵
17	6	3.0	.	-	•⁰ 18³² – 23⁴⁰, = 3⁴⁰ – 14⁴⁵, 15¹⁵ – 18³², 23⁴⁰ – 24
18	6	14.1	.	-	•⁰ 16⁴⁰ – 24, = 0⁰⁰ – 9⁴⁰ ∞ – 16⁴⁰
19	7	0.0	.	-	•⁰ 0⁰⁰ – 8⁴⁵
20	5	3.4	.	-	*⁰ 8²⁵ – 9⁴⁰ *¹ – 10³⁰ *⁰ – 13⁴⁵, = 13⁵ – 24
21	7	0.2	.	-	•⁰ 17⁰⁸ – 18⁴⁵, = 0⁰⁰ – 9⁴⁰
22	7	1.3	.	-	= 8²⁰ – 11⁴⁰, 17³⁰ – 24
23	6	0.0	2	-	*⁰ 1⁴⁰ – 2²⁰, 3⁴⁵ – 6¹⁰, 8⁴⁰ – 11¹⁵, 20³⁶ – 21⁵¹, = 0⁰⁰ – 7⁰⁵ ≡⁰ – 7⁵⁰ = – 8⁴⁰, 11¹⁵ – 14²⁰
24	7	.	.	-	≡⁰ 8²⁰ – 45 ≡¹ – 9⁵⁰ = – 12³⁰, 17³⁰ – 22⁴⁰
25	6	.	.	-	= 3³⁰ – 19⁴⁰
26	6	.	.	-	= 6⁴⁰ – 11⁴⁵ ∞ – 14²⁰
27	7	0.0	.	-	
28	6	0.3	.	-	*⁰ 6²⁵ – 14³⁵, = 5¹⁰ – 6²⁵
29					
30					
31					
Σ	–	46.7	–	-	UWAGI

Bydgoszcz $\varphi = 53°07'$ $\lambda = 17°58'$ **Marzec – Mars 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	128.0	128.1	127.0	127.7	-1.5	2.2	-2.4	-1.0	2.9	-2.7	-	-	-	-	-	-	-	-	9	6	0	N 3	N 4	N 1
2	125.2	123.7	120.6	123.2	-3.8	1.6	0.1	-0.5	2.1	-4.6	-	-	-	-	-	-	-	-	7	9	8	N 1	NNW 5	C 0
3	117.5	115.2	112.1	114.9	-1.0	1.6	-2.4	-1.0	3.2	-3.4	-	-	-	-	-	-	-	-	9	1	1	NE 1	NE 1	C 0
4	106.4	102.6	101.1	103.4	-2.7	3.1	0.9	0.6	3.3	-4.4	-	-	-	-	-	-	-	-	9	10	10 ⛆	S 4	SW 6	W 2
5	103.8	105.6	106.8	105.4	-1.8	4.6	-0.4	0.5	5.8	-2.4	-	-	-	-	-	-	-	-	3 ⊙	3	0	WSW 4	W 5	NW 1
6	106.9	106.0	106.0	106.3	-6.5	5.1	0.4	-0.2	6.4	-7.2	-	-	-	-	-	-	-	-	0 ⊙	0 ⊙	0	C 0	NW 2	ENE 4
7	106.0	107.1	108.7	107.3	-3.2	0.4	-3.0	-2.2	1.3	-4.3	-	-	-	-	-	-	-	-	0	4	0	C 0	E 5	ESE 3
8	110.0	110.9	114.3	111.7	-5.3	1.4	-3.5	-2.7	2.1	-5.9	-	-	-	-	-	-	-	-	0	3	0	E 4	E 5	E 6
9	119.3	120.8	122.9	121.0	-5.0	2.7	-0.4	-0.8	3.3	-5.8	-	-	-	-	-	-	-	-	0	0 ⊙	0	E 3	E 5	E 2
10	125.4	125.6	126.0	125.7	-7.7	4.0	-1.9	-1.9	6.1	-8.2	-	-	-	-	-	-	-	-	0	0 ⊙	0	C 0	E 4	C 0
11	125.8	124.6	121.6	124.0	-7.6	8.3	-1.0	-0.3	10.7	-8.7	-	-	-	-	-	-	-	-	0	0	1	E 1	ESE 4	C 0
12	117.0	113.8	110.8	113.9	-3.5	12.1	1.8	3.0	12.5	-6.0	-	-	-	-	-	-	-	-	9	6	0	C 0	SW 3	C 0
13	110.0	109.7	106.6	108.8	-0.6	14.0	5.8	6.2	16.5	-3.3	-	-	-	-	-	-	-	-	7	2	1	SW 2	WNW 5	NW 2
14	100.6	98.8	97.6	99.0	4.2	10.6	9.8	8.6	13.1	2.1	-	-	-	-	-	-	-	-	0	10	9	WSW 4	W 9	W 10
15	100.1	99.3	91.5	97.0	5.8	8.2	6.0	6.5	9.9	5.0	-	-	-	-	-	-	-	-	5	10	10 ●	W 7	W 5	NW 9
16	95.9	102.5	108.6	102.3	0.4	-3.0	-4.6	-3.0	6.0	-5.3	-	-	-	-	-	-	-	-	9	6	8	WNW 4	N 8	N 3
17	108.0	104.0	93.0	101.7	-4.6	-1.4	-0.1	-1.6	0.3	-6.6	-	-	-	-	-	-	-	-	10	10	10 ●	C 0	SE 8	SE 4
18	94.0	84.4	90.0	89.5	5.8	10.7	6.0	7.1	11.2	-1.3	-	-	-	-	-	-	-	-	10 ●	9	10 ●	WSW 3	W 8	WNW 5
19	98.4	100.4	100.6	99.8	0.4	1.8	2.6	1.8	3.2	-0.2	-	-	-	-	-	-	-	-	10 ● *	10 ●	10 ●	C 0	NW 2	E 3
20	102.9	100.4	95.3	99.5	1.6	4.2	7.7	5.3	8.1	1.1	-	-	-	-	-	-	-	-	10	10 ●	10	ESE 5	SE 6	SSW 1
21	98.1	101.1	103.1	100.8	6.6	11.2	4.6	6.8	12.7	4.4	-	-	-	-	-	-	-	-	0 ⊙	5 ⊙	0	W 5	W 7	WNW 2
22	105.2	107.0	109.4	107.2	4.4	8.8	3.6	5.1	10.5	2.6	-	-	-	-	-	-	-	-	4 ⊙	5	0	W 3	W 7	NW 2
23	111.2	112.0	116.0	113.1	-2.0	10.2	1.4	2.8	11.9	-3.8	-	-	-	-	-	-	-	-	1	1	2	C 0	NW 2	NE 3
24	120.1	120.0	119.2	119.8	-2.8	3.7	1.5	1.0	5.0	-3.9	-	-	-	-	-	-	-	-	4	9	9	E 6	E 12	E 10
25	117.9	117.8	116.7	117.5	-0.6	3.4	2.3	1.8	4.3	-1.2	-	-	-	-	-	-	-	-	10	10	0	ESE 6	ESE 9	SE 9
26	114.5	113.6	112.8	113.6	1.6	11.3	8.6	7.5	13.7	0.5	-	-	-	-	-	-	-	-	9	4	0	SE 5	SSE 7	SE 7
27	113.2	113.1	111.7	112.7	4.3	14.1	9.2	9.2	15.3	2.8	-	-	-	-	-	-	-	-	8	3	2	SSE 7	S 9	S 6
28	108.7	107.9	106.6	107.7	4.4	8.6	6.2	6.4	10.4	2.5	-	-	-	-	-	-	-	-	9	10 ●	10	S 5	SW 6	SW 2
29	104.5	105.8	108.6	106.3	5.7	5.2	2.8	4.1	6.4	2.5	-	-	-	-	-	-	-	-	10 ●	10 ●	5	SW 2	ENE 2	C 0
30	111.2	112.0	113.1	112.1	5.1	12.9	7.1	8.0	13.4	1.6	-	-	-	-	-	-	-	-	9	7	0	NE 4	ENE 5	NNE 5
31	113.8	114.6	115.6	114.7	4.6	15.2	6.0	8.0	16.9	2.6	-	-	-	-	-	-	-	-	0	0 ⊙	0	ENE 3	E 2	C 0
M	110.3	109.9	109.5	109.9	-0.2	6.3	2.4	2.7	8.0	-2.0	-	-	-	-	-	-	-	-	5.5	5.6	3.7	3.0	5.4	3.3

Kwiecień – Avril

1	116.0	114.7	113.9	114.9	4.8	16.3	10.2	10.4	17.5	1.1	-	-	-	-	-	-	-	-	0	0	0	E 3	E 5	E 3
2	112.6	112.4	113.2	112.7	6.4	16.9	12.2	11.9	18.9	4.5	-	-	-	-	-	-	-	-	3 ⊙	0	0	E 6	E 5	ENE 3
3	116.0	117.8	119.8	117.9	7.6	19.0	12.1	12.7	19.9	5.3	-	-	-	-	-	-	-	-	3 ⊙	3	0	ENE 3	ENE 5	NE 2
4	122.1	121.9	121.2	121.7	5.2	17.7	6.2	8.8	19.4	1.0	-	-	-	-	-	-	-	-	0 ⊙	0	0	NE 2	NNE 3	C 0
5	120.1	116.9	111.4	116.1	7.1	19.7	9.4	9.9	20.4	-1.6	-	-	-	-	-	-	-	-	0	0	0	C 0	SW 3	SW 2
6	105.7	101.4	101.6	102.9	3.6	19.3	8.8	10.1	20.5	0.3	-	-	-	-	-	-	-	-	0 ⊙	5	8	C 0	SW 6	NNW 5
7	102.0	104.5	111.3	105.9	2.8	6.4	1.0	2.8	8.8	0.7	-	-	-	-	-	-	-	-	10	7	3	NNW 2	NNE 8	NNE 10
8	112.8	110.2	107.9	110.3	0.0	6.8	4.1	3.8	8.7	-3.2	-	-	-	-	-	-	-	-	6	8 ⊙	8	NNE 4	NNW 5	NW 3
9	105.8	105.5	104.9	105.4	1.8	4.3	0.1	1.6	5.3	-1.2	-	-	-	-	-	-	-	-	10	10 ●	5	C 0	NNE 4	E 4
10	100.3	94.0	98.4	97.6	-2.0	11.7	8.8	6.8	13.9	-5.7	-	-	-	-	-	-	-	-	8	7	9	E 3	SW 7	SW 2
11	86.0	87.1	94.5	89.2	3.8	5.8	1.0	2.9	8.8	-2.0	-	-	-	-	-	-	-	-	6	10	10	W 5	W 6	N 5
12	100.5	101.1	104.0	101.9	0.6	5.0	-1.6	0.6	6.3	-2.3	-	-	-	-	-	-	-	-	1	7	0	N 1	W 1	W 1
13	105.1	106.0	108.3	106.5	-2.7	2.2	0.2	0.0	5.4	-8.0	-	-	-	-	-	-	-	-	10 ≡	9	2	C 0	N 1	C 0
14	110.5	109.8	111.1	110.5	-2.0	5.8	-1.2	0.4	7.3	-8.5	-	-	-	-	-	-	-	-	0	8	3	C 0	W 5	C 0
15	113.1	113.1	114.6	113.6	-0.6	5.2	0.6	1.4	6.4	-3.3	-	-	-	-	-	-	-	-	0	5	7	NNE 2	NW 6	N 1
16	114.7	111.4	109.5	111.9	-0.2	6.3	7.4	5.2	9.5	-5.4	-	-	-	-	-	-	-	-	10	10	10 ●	SW 4	SW 5	WSW 2
17	111.1	112.2	113.5	112.3	5.8	6.6	5.0	5.6	8.6	4.5	-	-	-	-	-	-	-	-	9	10	10	WNW 3	WNW 5	WNW 3
18	112.2	110.8	109.5	110.8	2.4	6.4	4.6	4.5	6.8	1.6	-	-	-	-	-	-	-	-	10 ●	10	10	NNW 3	NNW 3	ENE 1
19	106.7	105.4	106.0	106.0	3.4	7.6	5.6	5.6	8.9	1.9	-	-	-	-	-	-	-	-	9	10	10 ●	NE 2	C 0	E 4
20	109.4	113.7	116.7	113.3	5.6	7.8	5.8	6.2	8.6	4.3	-	-	-	-	-	-	-	-	10 ●	10	10	NW 5	NW 7	C 0
21	119.0	119.4	121.0	119.8	4.2	7.6	6.0	6.0	8.8	2.8	-	-	-	-	-	-	-	-	10	10	9	NNW 2	NNW 2	C 0
22	123.3	123.5	123.1	123.3	4.3	8.6	4.8	5.6	8.8	-0.7	-	-	-	-	-	-	-	-	9	10 ●	10 ●	C 0	N 3	NE 4
23	122.2	122.2	122.2	122.2	4.8	8.8	8.2	7.5	10.1	1.9	-	-	-	-	-	-	-	-	10	10	10	N 3	N 2	N 3
24	121.7	120.8	119.7	120.7	2.4	11.5	8.2	7.6	13.9	1.5	-	-	-	-	-	-	-	-	10 ≡	9	10 ●	N 4	N 4	N 6
25	117.1	115.7	115.4	116.1	4.6	9.6	5.4	6.2	10.9	3.9	-	-	-	-	-	-	-	-	10	9	7	N 6	NNE 8	NE 5
26	114.8	113.7	113.0	113.8	5.0	13.6	10.0	9.6	16.2	3.5	-	-	-	-	-	-	-	-	10	10	4	E 4	ENE 3	N 1
27	111.0	108.4	106.8	108.7	8.2	21.1	15.7	15.2	23.6	5.5	-	-	-	-	-	-	-	-	6	6	10 ● ⛈	NNE 3	NNE 2	SSE 2
28	103.9	102.0	100.8	102.2	12.0	22.5	15.1	16.2	23.6	8.5	-	-	-	-	-	-	-	-	0	4	2	ENE 1	S 5	S 1
29	101.0	102.1	102.5	101.9	12.7	22.9	15.1	16.4	24.0	6.6	-	-	-	-	-	-	-	-	0	1	0	S 2	W 6	WSW 1
30	102.2	99.9	104.5	102.2	11.7	19.0	7.0	11.2	19.9	6.2	-	-	-	-	-	-	-	-	4	10	0	NE 3	N 4	NE 3
31																								
M	110.6	109.9	110.7	110.4	3.9	11.4	6.5	7.1	13.0	0.8	-	-	-	-	-	-	-	-	5.8	6.9	5.6	2.5	4.3	2.6

Bydgoszcz $H_s = 70\ m$ $H_b = 70{,}5\ m$ $h_w = 10\ m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	$*^0\ 3^{35}-5^{40}$; = $17^{20}-24$
2	7	.	.	-	= $0^{00}-8^{40}$
3	7	.	.	-	
4	7	1.9	.	-	$*^0\ 13^{20}-14^{10}$ $\bullet^0-15^{45}$ $*^0-16^{05}$ $\bullet^0-16^{40}$ $*^0-17^{40}$ $*^1-18^{30}$ $*^0-19^{30}$ $*^0-21^{40}$; = $21^{40}-24$
5	8	.	.	-	= $0^{00}-6^{30}$
6	8	.	.	-	
7	7	.	.	-	= $5^{20}-9^{30}$; ⌴ $9^{30}-24$
8	7	.	.	-	⌴ $0^{00}-11^{45}$; $19^{30}-24$
9	7	.	.	-	= $19^{30}-24$; ⌴ $0^{00}-8^{00}$ $20^{34}-24$
10	7	.	.	-	= $0^{00}-9^{30}$; ⌴ $0^{00}-8^{00}$; $20^{40}-24$
11	7	.	.	-	= $5^{00}-8^{50}$; ⌴ $0^{00}-10^{00}$; $20^{30}-24$
12	6	.	.	-	= $1^{40}-16^{40}$; $20^{20}-24$; ⌴ $0^{00}-9^{00}$; $23^{30}-24$
13	7	.	.	-	= $0^{00}-8^{30}$; $23^{40}-24$; ⌴ $0^{00}-8^{00}$
14	6	.	.	-	= $0^{00}-8^{35}$; ∞ -13^{40}
15	8	2.2	.	-	$\bullet^0\ 13^{40}-24$
16	8	.	.	-	$\bullet^0\ 0^{00}-1^{35}$
17	7	6.4	.	-	$*^0\ 15^{40}-17^{10}$ $\bullet^0-24$; ∞ $17^{10}-24$
18	8	4.0	.	-	$\bullet^0\ 0^{00}-8^{30}$; $13^{45}-14^{05}$; 17^{35-50}; $20^{30}-24$; ∞ $0^{00}-4^{20}$
19	6	1.8	1	-	$\bullet^0\ 0^{00}-5^{30}$ $*^0-8^{30}$ $\bullet^0-14^{35}$; $17^{40}-22^{38}$; = $14^{35}-17^{40}$; $22^{38}-24$
20	4	0.5	.	-	$\bullet^0\ 10^{15}-16^{10}$ $\bullet^0\ 17^{35}-18^{30}$; = $0^{00}-24$
21	7	.	.	-	= $0^{00}-2^{30}$
22	8	.	.	-	= $1^{40}-4^{10}$
23	8	.	.	-	⌴^{0} n -8^{00}
24	8	0.1	.	-	
25	7	0.0	.	-	$\bullet^0\ 4^{15}-10^{35}$; ∞ $4^{15}-10^{35}$
26	7	.	.	-	
27	8	.	.	-	
28	7	4.9	.	-	$\bullet^0\ 12^{15}-18^{25}$; = $18^{25}-24$
29	6	10.6	.	-	$\bullet^0\ 1^{20}-2^{30}$ $\bullet\bullet^0\ 4^{35}$ $\bullet^0-13^{35}$; = $0^{00}-1^{20}$; $20^{30}-21^{45}$ $\equiv^0-23^{35}$ $\equiv^2-24$
30	6	.	.	-	$\equiv^2 0^{00}-1^{30}$ = -13^{40}; $18^{30}-21^{35}$
31	7	.	.	-	
Σ	–	32.4	–	-	UWAGI.

Kwiecień – Avril

1	8	.	.	-	= $0^{00}-7^{30}$
2	7	.	.	-	
3	8	.	.	-	
4	8	.	.	-	= $7^{30}-11^{40}$
5	8	.	.	-	= $5^{30}-8^{40}$; ⌴ $5^{20}-7^{30}$
6	8	.	.	-	
7	7	.	.	-	= $5^{15}-10^{10}$
8	8	.	.	-	
9	7	0.0	.	-	$\bullet^0\ 11^{50}-13^{25}$
10	8	.	.	-	
11	8	.	.	-	
12	8	1.5	.	-	$*^1\ 16^{10-45}$ $*^0-17^{40}$; = $19^{40}-21^{50}$ $\equiv^1-24$
13	7	2.0	2	-	$*^0\ 9^{40}-10^{05}$ $*^2-10^{25}$ $*^0-10^{50}$; $\equiv^1 0^{00}-2^{40}$ = -3^{55} $\equiv^1-5^{35}$ = -6^{50} $\equiv^0-7^{25}$ = -8^{30}; $10^{50}-11^{15}$
14	8	0.0	.	-	$\bullet^0\ 17^{46-50}$; = $21^{20}-24$; ⌴ $21^{40}-24$
15	8	0.0	.	-	$*^0\ 16^{30-40}$ 17^{42-45}; = $0^{00}-9^{40}$; ⌴ $0^{00}-9^{10}$
16	7	2.9	.	-	$\bullet^0\ 9^{23}-11^{15}$; $15^{11}-24$; ⌴ n -9^{10}
17	8	0.0	.	-	$\bullet^0\ 0^{00}-4^{35}$
18	7	0.0	.	-	$\bullet^0\ 5^{50}-7^{35}$ $\bullet^0\ 22^{30}-23^{30}$; = $17^{40}-24$
19	7	3.3	.	-	$\bullet^0\ 0^{10}-2^{10}$ $\bullet^0\ 18^{35}-24$; = $0^{00}-4^{30}$
20	8	0.0	.	-	$\bullet^0\ 0^{00}-7^{40}$; $16^{35}-17^{04}$
21	7	.	.	-	= $10^{40}-24$
22	6	7.0	.	-	$\bullet^0\ 12^{40}-24$; = $0^{00}-7^{30}$; ⌓ n -8^{30}
23	7	.	.	-	$\bullet^0\ 0^{00}-4^{40}$; = $4^{40}-9^{15}$; $19^{15}-24$
24	7	0.0	.	-	$\bullet^0\ 19^{18}-22^{35}$; = $0^{00}-4^{40}$ $\equiv^1-7^{55}$ $\equiv^0-8^{25}$ = -12^{35}
25	7	0.0	.	-	$\bullet^0\ 1^{05}-2^{30}$ $9^{54}-10^{07}$; = $6^{25}-10^{07}$
26	7	.	.	-	= $2^{40}-10^{35}$ ∞ -11^{25} = $23^{45}-24$
27	7	6.4	.	-	(K)$^0\ 19^{55}-20^{20}$ $\bullet$K$^0-21^{15}$ $\bullet^0-22^{15}$ $\bullet$K$^2-22^{40}$ $\bullet$K$^0-23^{10}$ $\bullet^0-23^{35}$; = $0^{00}-12^{40}$
28	7	.	.	-	= $4^{25}-6^{30}$
29	8	0.0	.	-	= $4^{40}-8^{20}$
30	8	0.0	.	-	$\bullet^0\ 5^{15-18}$; $16^{45}-17^{30}$; = $4^{30}-5^{40}$
31					
Σ	–	23.1	–	-	UWAGI.

Bydgoszcz $\varphi = 53°07'$ $\lambda = 17°58'$ **Maj - Mai 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	109.1	110.4	110.7	110.1	5.4	11.7	7.3	7.9	13.0	1.1	75	40	63	59	2.3	8.2	3.7	4.7	0	6	5	WNW 4	NW 3	NNE 2
2	110.6	108.3	106.6	108.5	6.6	12.3	7.0	8.2	14.0	-0.1	62	48	69	60	3.6	7.4	3.1	4.7	6	8	6	ESE 3	SSW 3	S 1
3	105.2	103.3	100.1	102.9	7.8	13.7	11.1	10.9	16.0	-0.4	65	44	75	61	3.7	8.7	3.2	5.2	9	10	8	S 1	SW 4	W 1
4	97.6	100.2	101.7	99.8	7.2	8.0	4.8	6.2	11.5	4.4	71	47	50	59	2.9	5.6	3.5	4.0	9	9	1	W 7	W 7	W 5
5	101.4	100.4	101.6	101.1	3.4	9.4	0.6	3.5	9.8	0.1	75	47	92	71	2.0	6.3	0.5	2.9	9	5	0	SW 8	WSW 8	C 0
6	101.8	100.1	100.4	100.8	0.4	6.2	2.8	3.0	7.2	-2.9	88	70	89	82	0.8	2.8	0.8	1.5	10	10	10 ●	C 0	NNE 3	NNE 3
7	99.8	100.0	100.6	100.1	2.8	7.2	4.3	4.6	8.6	-1.4	96	66	92	85	0.3	3.5	0.7	1.5	10	10	4	NW 3	NNW 4	NNE 3
8	99.9	99.4	101.3	100.2	3.3	6.2	4.3	4.5	7.8	0.2	83	70	88	80	1.3	2.8	1.0	1.7	9	10	10 ●	NNW 5	NW 5	NNW 3
9	103.9	104.6	105.3	104.6	3.5	9.0	4.4	5.3	9.5	-0.1	90	59	89	79	0.8	4.7	1.0	2.2	9	9	10 ●	C 0	N 3	N 4
10	103.0	102.4	103.3	102.9	4.2	8.6	6.8	6.6	9.4	3.0	92	81	87	87	0.6	2.2	1.3	1.4	10	10	10	NNW 5	NW 7	NW 4
11	104.6	107.2	107.2	106.3	5.7	8.2	6.6	6.8	11.4	4.5	95	85	90	90	0.5	1.7	1.0	1.1	10 ●	10	0	WNW 3	WNW 2	SW 2
12	107.3	107.2	107.5	107.3	7.8	20.9	13.5	13.9	22.0	1.1	90	39	76	68	1.1	15.1	3.7	6.6	0	0	6	SSE 2	SSE 7	SSE 1
13	108.6	108.8	108.5	108.6	10.1	20.9	13.1	14.3	24.0	6.0	92	40	67	66	1.0	14.9	5.0	7.0	6	4	4	C 0	NW 2	C 0
14	110.1	110.6	112.7	111.1	11.9	18.5	13.7	14.4	21.0	8.4	95	53	75	74	0.7	10.0	3.9	4.9	9	7	1	WNW 3	W 5	N 2
15	114.8	114.5	113.3	114.2	11.7	19.7	13.7	14.7	22.3	4.1	90	41	69	67	1.3	13.4	4.9	6.5	1	1	0	NNW 2	WNW 1	E 1
16	112.2	109.3	107.1	109.5	15.0	22.7	16.7	17.8	23.6	7.5	55	40	51	49	7.6	16.5	9.2	11.1	0	1	0	E 4	SE 7	C 0
17	108.3	108.4	110.5	109.1	13.7	22.2	12.9	15.4	24.0	9.4	75	41	68	61	3.9	15.8	4.8	8.2	9	7	3	ESE 2	S 4	N 3
18	111.4	110.6	107.7	109.9	12.1	19.2	15.5	15.6	20.8	7.9	72	44	57	58	4.0	12.3	7.6	8.0	9	4	0	N 2	NE 2	ENE 3
19	104.2	101.7	99.1	101.7	15.4	25.5	20.0	20.2	26.0	9.9	63	46	62	57	6.5	17.7	9.0	11.1	2	4	6	NE 4	ENE 6	ENE 2
20	100.5	100.7	106.1	102.4	17.0	22.4	11.9	15.8	24.0	11.9	79	56	78	71	4.1	11.8	3.0	6.3	2	8	10	ENE 3	NW 2	NW 7
21	108.9	108.9	109.1	109.0	8.0	14.7	11.4	11.4	16.3	7.0	87	51	64	67	1.3	8.2	4.9	4.8	10	9	8	NW 3	W 4	NNW 2
22	109.1	108.6	108.7	108.8	9.1	15.9	12.1	12.3	16.6	7.6	81	52	63	65	2.2	8.7	5.2	5.4	10	7	10	N 1	ENE 6	N 5
23	106.5	105.2	105.0	105.5	10.9	17.0	13.5	13.7	18.4	7.4	80	69	84	78	2.6	6.0	2.5	3.7	3	3	10	NE 3	NE 3	N 4
24	106.8	109.7	115.6	110.7	12.3	16.1	8.2	11.2	17.5	8.2	86	60	69	72	2.0	7.4	3.4	4.3	10	8	1	NNE 3	NE 6	NNE 8
25	117.8	119.2	120.4	119.1	8.2	10.9	6.2	7.9	12.3	4.0	63	39	67	56	4.0	8.0	3.1	5.0	0	6	1	NNE 8	NE 6	NNE 5
26	120.6	120.4	120.6	120.5	6.0	9.5	6.0	6.9	11.0	1.1	82	61	63	69	1.8	4.6	3.5	3.3	8	9	4	NNE 6	NE 8	NE 3
27	119.0	118.5	117.6	118.4	6.6	10.7	7.0	7.8	11.9	1.4	81	49	75	68	1.8	6.6	2.4	3.6	9	8	4	NE 3	NNE 4	NNE 2
28	116.2	114.6	114.0	114.9	6.4	12.3	9.0	9.2	13.9	0.7	79	51	70	67	2.0	7.0	3.5	4.2	1	8	3	NE 4	NE 3	NE 2
29	114.1	113.2	113.0	113.4	7.0	14.5	9.9	10.3	15.9	0.1	75	42	73	63	2.4	9.5	3.3	5.1	1	9	3	NNE 1	NW 3	N 2
30	113.8	113.8	112.7	113.4	10.8	16.2	10.9	12.2	18.0	4.6	64	49	78	64	4.6	9.4	2.9	5.6	1	8	0	NNW 2	W 4	C 0
31	111.8	109.8	106.8	109.5	12.5	21.7	12.9	15.0	23.0	3.9	71	34	70	58	4.2	17.0	4.4	8.5	1 ⊙	4	2	WNW 2	SW 4	SW 2
M	108.4	108.7	108.2	108.2	8.5	14.6	9.6	10.6	16.2	3.9	79	52	73	68	2.5	8.8	3.5	4.9	5.9	6.8	4.5	3.1	4.4	2.6

Czerwiec - Juin

1	107.0	106.1	107.4	106.8	12.1	20.5	13.1	14.7	22.0	9.4	74	49	66	63	3.7	12.2	5.1	7.0	6	5	4	W 2	W 6	NW 1
2	108.6	110.6	111.9	110.4	12.7	18.5	12.2	13.9	19.4	6.0	75	59	76	70	3.7	8.7	3.4	5.3	8	5	0	WNW 3	NNW 6	NNW 1
3	113.1	110.8	107.1	110.3	14.9	23.3	19.5	19.3	25.6	5.6	73	48	67	63	4.5	14.8	7.5	8.9	7	6	1	NNW 1	SW 5	C 0
4	104.8	103.5	101.2	103.2	18.2	24.7	19.8	20.6	25.6	12.1	73	42	68	61	5.6	18.1	7.3	10.3	6	6	10	W 1	NW 4	NNE 2
5	98.2	97.4	96.8	97.5	12.5	16.2	12.1	13.2	19.9	11.8	99	75	96	90	0.2	4.5	0.5	1.7	10 ●	8	6	C 0	W 4	W 1
6	97.0	99.9	101.3	99.4	10.9	14.9	11.4	12.2	16.4	8.0	91	52	84	76	1.1	8.0	2.2	3.8	10 ●	7	8	WSW 4	WSW 7	SW 2
7	101.5	100.6	102.6	101.6	12.6	20.6	13.1	14.8	21.5	9.5	84	50	77	70	2.4	12.0	3.5	6.0	8	9	1	SW 3	W 5	C 0
8	105.1	105.1	104.5	104.9	13.7	20.9	17.5	17.4	22.8	5.0	80	48	66	65	3.2	12.7	6.8	7.6	6	6	5	WNW 1	S 3	ESE 2
9	102.0	100.0	102.2	101.4	19.5	26.3	17.1	20.0	27.7	13.5	73	53	94	73	6.1	16.1	1.2	7.8	7 ⊙	6	7	SE 5	S 6	WSW 1
10	104.9	104.9	104.3	104.7	16.1	18.5	18.1	17.7	21.5	11.8	79	79	86	81	3.8	4.5	2.9	3.7	6	10	2	W 1	ENE 2	ENE 3
11	102.6	99.8	99.3	100.6	18.1	28.7	23.9	23.6	30.0	14.1	88	50	81	73	2.5	19.7	5.6	9.3	1	4	4	E 2	SSE 7	SE 3
12	110.5	116.8	122.0	116.4	17.9	18.2	15.0	16.5	24.3	14.0	80	66	63	70	4.0	7.1	6.2	5.8	10	8	0	NW 4	NW 4	NNW 5
13	123.3	122.1	121.4	122.3	11.6	19.5	15.8	15.7	21.5	7.7	72	52	62	62	3.7	10.9	6.7	7.1	3	1	0	NW 5	WNW 5	NNW 3
14	121.6	122.1	122.1	121.9	14.2	22.0	15.5	16.8	23.0	5.3	76	38	51	55	3.9	16.4	8.6	9.6	0	1	4	NNW 1	NE 5	NNE 3
15	122.2	120.8	118.2	120.4	12.7	21.9	16.7	17.0	23.4	4.6	79	44	53	59	3.1	14.7	8.9	8.9	1	2	0	NE 3	E 3	NE 3
16	117.4	115.4	113.4	115.4	14.9	24.8	21.3	20.6	26.5	4.4	64	36	57	52	6.0	19.9	10.7	12.2	0	0	1	NE 1	ESE 3	E 2
17	113.7	112.4	110.3	112.1	17.3	24.7	19.7	20.4	25.9	9.9	61	39	51	50	7.6	19.1	11.3	12.7	1	1	0	E 3	NE 3	NE 3
18	109.7	107.3	104.3	107.1	18.8	27.7	19.5	21.4	29.0	7.5	62	30	61	51	8.2	26.0	8.9	14.4	0	0	0	C 0	SSW 2	C 0
19	103.2	101.9	104.3	103.1	21.1	28.1	16.5	20.6	29.0	10.5	56	43	74	58	11.7	21.7	5.0	12.6	0	2	6	C 0	NNE 3	N 6
20	107.3	107.9	109.6	108.3	13.9	21.4	15.3	16.5	23.0	9.9	71	39	65	58	4.6	15.6	6.2	8.8	7	8	6	ENE 5	NE 4	ENE 5
21	111.4	107.7	102.6	107.2	14.7	23.9	18.5	18.9	25.5	9.1	66	41	60	56	5.7	17.5	8.5	10.6	2	2	1	E 3	SW 3	SSE 2
22	98.4	96.6	95.2	96.7	15.8	18.9	17.1	17.2	21.4	13.0	79	88	98	88	3.7	2.5	0.4	2.2	8	10	9	SSE 2	SW 4	WNW 2
23	99.9	101.4	101.9	101.1	14.3	19.7	16.0	16.5	23.5	12.5	76	56	77	70	3.9	10.1	4.2	6.1	6	8	10	WNW 4	C 0	NNW 5
24	104.2	103.5	99.7	102.5	13.2	10.7	12.7	12.3	16.4	9.5	84	91	86	87	2.5	1.2	2.1	1.9	10	10 ●	3	C 0	NE 2	ENE 1
25	97.7	102.2	107.4	102.4	10.3	10.4	11.7	11.0	14.2	9.3	96	95	88	93	0.5	0.6	1.6	0.9	10 ●	10 ●	9	C 0	NNW 5	W 2
26	110.5	111.4	114.1	112.0	10.0	16.7	11.1	12.2	18.3	7.0	91	51	85	76	1.1	9.2	2.0	4.1	6	6	5	W 3	W 4	W 3
27	114.3	115.8	116.8	115.6	12.6	15.5	9.8	11.9	17.9	6.4	81	65	86	77	2.7	6.2	1.7	3.5	4	7	4	W 1	WNW 5	WNW 2
28	113.7	112.2	112.4	112.8	14.7	23.7	20.9	20.0	27.5	6.1	68	61	73	67	5.3	11.5	6.6	7.8	10	6	3	WSW 6	WSW 6	NW 4
29	113.7	113.3	111.8	112.9	19.0	26.9	22.1	22.5	29.3	14.5	75	50	79	68	5.6	17.7	5.6	9.6	6	1	1	NW 4	WNW 5	C 0
30	111.8	111.7	112.0	111.8	21.7	28.3	21.7	23.4	29.3	15.2	76	46	72	65	6.4	20.7	7.2	11.4	1	7	3	WNW 2	NW 6	ENE 4
31																								
M	108.3	108.0	107.9	108.1	15.0	21.2	16.5	17.3	23.4	9.4	77	55	73	68	4.2	12.7	5.3	7.4	5.3	5.4	3.8	2.3	4.2	2.4

Bydgoszcz $H_s = 70\ m$ $H_b = 70{,}5\ m$ $h_w = 10\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	.	.	–	
3	8	0.0	.	–	
4	8	.	.	–	$\bullet^0$ 330–50 $\ast^0$ 510–22
5	8	3.4	.	–	⛈ 1345–59 △ 1505–10, 1535–52 $\ast^0$ 1610–30 $\bullet^0$ 1645–1700 ; ⌴ n
6	7	20.4	.	–	$\bullet^0$ 710–920 1332–57 1509–24 ; ⌴ n
7	6	0.0	.	–	$\bullet^0$ 000–335, 440–540, 1430–35 ; = 335–440, 540–830
8	8	0.0	.	–	$\bullet^0$ 2026–2120
9	8	3.2	.	–	$\bullet^0$ 1350–1420, 1435–1510, 1530–24
10	7	4.5	.	–	$\bullet^0$ 000–415, 725–1026, 2110–24
11	7	0.0	.	–	$\bullet^0$ 000–1035 ; = 2135–24
12	6	0.1	.	–	= 000–840
13	7	3.4	.	–	$\bullet^0$ 530–46, 2320–24 ; = 220–720
14	7	0.3	.	–	$\bullet^0$ 000–10, R_x^0 0–045 $\bullet^0$ 0–205, 1346–1413 ; = 205–730
15	8	.	.	–	= 340–640
16	8	.	.	–	
17	8	.	.	–	
18	8	.	.	–	
19	8	.	.	–	
20	8	17.3	.	–	$\bullet^0$ 1320–30 $\bullet^2$ 1435–50 $\bullet^0$ – 1540 ; R_x^0 1330–1445–1530 SW-SE
21	8	.	.	–	$\bullet^0$ 640–735
22	7	0.0	.	–	$\bullet^0$ 2150–2218
23	8	.	.	–	
24	7	.	.	–	= 030–840
25	8	.	.	–	
26	8	0.0	.	–	
27	8	.	.	–	$\bullet^0$ 055–218
28	8	.	.	–	
29	8	.	.	–	
30	8	.	.	–	
31	8	.	.	–	
Σ	–	52.6	–	–	UWAGI.

Czerwiec – Juin

1	7	.	.	–	
2	8	.	.	–	
3	8	.	.	–	= 325–730 ; ⌒ n – 752
4	8	13.2	.	–	
5	7	5.2	.	–	$\bullet^0$ 130–206 $\bullet^1$ – 230 $\bullet^0$ – 930 $(R_x)^0$ 2030–45 R_x^0 2045–2050–2135
6	8	0.0	.	–	$\bullet^0$ 525–640, 715–935
7	8	.	.	–	
8	7	.	.	–	
9	8	9.7	.	–	R_x^0 1535–1705–1742 ; = 2142–24
10	7	.	.	–	= 000–420 ≡ ^{0}–423 ≡ ^{1}–450 ≡ ^{2}–550 = –830, 2330–24
11	8	.	.	–	= 000–720
12	8	.	.	–	
13	8	.	.	–	
14	8	.	.	–	⌒ ^{0} n
15	8	.	.	–	
16	8	.	.	–	
17	8	.	.	–	
18	8	.	.	–	
19	8	.	.	–	
20	8	.	.	–	
21	8	.	.	–	
22	7	3.6	.	–	$\bullet^0$ 958–1225, 1325–40, 1425–1545 ; = 1545–1830, 2235–24
23	8	.	.	–	= 000–630
24	6	13.6	.	–	$\bullet^0$ 1135–1540
25	6	0.5	.	–	$\bullet^0$ 355–835, 1115–1235 $\bullet^0$ – 1505
26	8	0.0	.	–	$\ast^0$ 1828–30
27	8	.	.	–	
28	8	.	.	–	
29	8	.	.	–	
30	8	.	.	–	
31					
Σ	–	45.8	–	–	UWAGI.

Bydgoszcz $\varphi = 53°07'$ $\lambda = 17°58'$ **Lipiec – Juillet 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	113.8	111.8	110.0	111.9	14.6	26.0	21.7	21.0	28.5	13.0	90	52	67	70	1.6	16.1	8.7	8.8	8	3	1	NE 2	E 3	SE 2
2	105.7	105.6	110.4	107.2	21.9	25.2	17.5	20.5	29.0	17.3	72	72	67	70	7.5	9.1	6.6	7.7	4	8	0	S 4	WNW 4	NNW 5
3	112.2	111.7	110.0	111.3	16.8	24.0	19.5	20.0	26.6	10.7	75	40	60	58	4.8	17.8	9.0	10.5	1	3	1	NNW 6	WNW 5	NW 2
4	108.7	105.7	103.8	106.1	17.7	29.9	24.8	24.3	32.3	9.9	67	48	73	63	6.6	22.0	8.5	12.4	9	4	2	W 3	SW 6	SW 2
5	104.5	105.5	109.3	106.4	22.8	29.5	20.6	23.4	30.4	20.2	86	53	66	68	3.8	19.3	8.3	10.5	6	1	1	WSW 3	W 6	NW 4
6	112.6	112.2	112.1	112.3	16.5	24.2	19.3	19.8	26.7	11.1	75	45	62	61	4.8	16.8	8.6	10.1	1	2	0	NW 6	NW 4	NNW 3
7	113.5	112.5	110.3	112.1	17.6	27.7	22.4	22.5	30.0	9.5	66	42	58	55	6.8	21.4	11.4	13.2	3	1	0	ESE 3	C 0	ESE 2
8	107.7	107.0	106.2	107.0	17.3	29.7	24.0	23.8	32.0	12.5	94	54	75	74	1.2	19.2	7.3	9.2	7	6	8	ESE 3	WSW 2	N 2
9	107.6	108.0	106.9	107.5	17.5	17.9	17.5	17.6	24.2	16.6	93	96	98	96	1.4	0.8	0.4	0.9	10	10	6	C 0	NNW 1	C 0
10	105.3	104.3	102.0	103.9	15.8	19.7	18.9	18.3	21.9	13.4	95	77	84	85	0.9	5.3	3.5	3.2	10	9	8	C 0	ESE 3	SE 2
11	100.9	100.9	101.7	101.2	17.7	25.1	21.5	21.4	26.5	15.5	83	50	67	67	3.4	15.8	8.4	9.2	9	8	8	ENE 4	E 5	NE 5
12	102.5	103.4	102.2	102.7	16.3	18.7	18.2	17.8	21.9	15.4	96	97	98	97	0.8	0.7	0.4	0.6	10 ●	10 ●	10	ENE 3	NNE 4	N 2
13	104.9	107.4	108.5	106.9	17.9	24.3	20.6	20.8	27.4	16.7	93	62	85	80	1.4	11.6	3.7	5.6	9	6	6	WNW 2	WNW 2	C 0
14	109.0	106.9	107.8	107.9	19.6	26.3	16.6	19.8	27.6	12.4	88	54	98	80	2.8	15.6	0.4	6.3	8	8	10 ●	NNW 3	E 3	SE 2
15	104.9	104.0	104.1	104.3	17.2	21.5	17.7	18.5	22.8	15.9	92	74	90	85	1.6	6.7	2.0	3.4	10	9	9	WNW 1	WSW 3	C 0
16	103.4	101.9	100.7	102.0	17.3	20.9	14.7	16.9	21.6	14.0	92	66	93	84	1.6	8.4	1.1	3.7	7	9	10 ●	C 0	NNW 4	NNW 7
17	98.2	98.0	100.5	98.9	13.4	16.3	15.3	15.1	16.6	12.0	98	90	92	93	0.4	1.9	1.3	1.2	10 ●	10	10 ●	NW 4	NW 5	WNW 4
18	101.4	102.1	100.9	101.5	14.9	17.1	15.0	15.5	20.6	13.7	94	94	93	94	0.9	1.2	1.1	1.1	10	10 ●	1	W 5	NW 4	C 0
19	100.2	99.4	98.2	99.3	15.5	25.1	20.1	20.2	27.0	8.9	87	45	68	67	2.3	17.4	7.6	9.1	0	4	1	C 0	SW 4	SSW 2
20	97.2	96.8	96.7	96.9	19.7	28.3	18.3	21.2	28.7	15.5	78	45	90	71	5.1	21.0	2.0	9.4	2	5	10 ● R	S 2	S 8	SW 4
21	94.5	95.1	94.4	94.7	17.7	20.1	17.4	18.2	21.5	15.4	91	80	99	90	1.8	4.7	0.2	2.2	7	10	10 ● R	C 0	C 0	WNW 2
22	92.3	92.9	93.9	93.0	17.0	20.7	16.9	17.9	23.2	15.3	97	74	96	89	0.6	6.3	0.8	2.6	9	9	10	NE 2	ENE 5	C 0
23	94.8	95.4	96.6	95.6	17.9	21.7	19.0	19.4	23.7	13.1	86	77	89	84	2.8	6.0	2.4	3.7	6	9	10	N 1	NW 4	C 0
24	97.2	99.7	100.7	99.2	18.3	16.9	14.7	16.2	19.3	14.2	84	76	88	83	3.2	4.6	2.0	3.3	10	10	1	NW 4	WNW 5	W 1
25	101.3	101.3	99.7	100.8	14.5	17.9	13.3	14.8	19.5	11.1	86	62	98	82	2.4	7.8	0.4	3.5	8	7	10	W 3	W 4	SW 4
26	99.5	99.9	98.3	99.2	13.3	14.4	15.0	14.4	19.6	10.9	92	87	98	92	1.3	2.2	0.3	1.3	10	10 ●	10 ●	WSW 4	WSW 5	W 3
27	95.0	94.4	94.9	94.8	16.0	15.9	13.7	14.8	19.3	12.3	93	89	97	93	1.4	2.0	0.6	1.3	8	10 ●	8	SW 5	W 5	SW 3
28	96.5	98.1	99.5	98.0	13.3	17.9	11.5	13.6	19.6	9.7	93	67	94	85	1.1	6.7	0.9	2.9	4	7	4	SW 2	SW 6	WSW 2
29	100.2	101.8	103.9	102.0	13.9	18.1	14.5	15.2	20.5	7.9	88	73	87	83	2.0	5.6	2.2	3.3	3	7	10	WSW 3	W 4	SW 3
30	103.2	104.0	108.1	105.1	15.1	17.1	16.1	16.1	19.1	13.0	93	90	89	91	1.2	2.0	1.9	1.7	10	10 ●	8	SSW 5	W 3	W 1
31	111.4	113.1	115.4	113.3	16.4	20.2	15.0	16.6	22.5	13.4	93	69	87	83	1.3	7.3	2.2	3.6	10	7	9	WNW 4	W 7	WNW 2
M	103.2	103.3	103.5	103.3	16.8	21.9	17.8	18.6	24.2	13.2	87	68	84	80	2.5	9.8	3.7	5.3	7.1	7.2	6.2	2.8	4.0	2.3

Sierpień – Août

1	114.4	114.2	113.6	114.1	15.3	22.1	17.3	18.0	24.4	10.7	86	61	80	76	2.4	10.3	3.9	5.5	0	6	3	WSW 4	W 5	NW 1
2	113.6	112.0	113.5	113.0	15.6	18.3	13.9	15.4	20.2	11.7	86	59	76	74	2.4	8.6	3.9	5.0	1	8	0	W 4	NW 7	WNW 2
3	112.5	111.0	111.8	111.8	14.2	20.3	15.4	16.3	21.8	9.5	77	55	74	69	3.8	10.8	4.6	6.4	2	6	1	WNW 4	W 5	NW 3
4	111.7	111.9	113.2	112.3	13.7	21.4	16.9	17.2	23.7	10.7	89	53	83	75	1.8	12.0	3.3	5.7	8	6	0	WNW 4	NW 4	ENE 1
5	114.4	114.7	114.8	114.6	14.7	21.9	18.7	18.5	24.6	8.4	88	58	76	74	2.0	11.0	5.2	6.1	2	8	7	NE 1	N 4	WNW 3
6	115.7	113.9	111.6	113.7	15.9	23.6	16.3	18.0	25.0	9.2	84	47	81	71	2.9	15.4	3.4	7.2	1	4	7	N 1	ESE 1	E 2
7	108.5	104.6	100.8	104.6	16.3	23.5	17.4	18.6	25.3	11.5	78	55	88	74	4.0	12.9	2.4	6.4	8	10	9	E 2	ESE 5	NE 2
8	100.6	101.8	103.3	101.9	15.4	22.2	16.6	17.7	23.2	13.1	92	57	80	76	1.3	11.6	3.9	5.6	6	9	3	N 1	NNE 4	NE 3
9	102.0	99.8	96.4	99.4	14.7	22.4	20.1	19.3	24.4	11.3	87	59	68	71	2.2	11.2	7.4	6.9	2	9	10	ENE 2	SE 6	ESE 4
10	92.2	93.2	95.3	93.6	17.1	18.3	16.3	17.0	22.3	15.2	85	95	95	92	3.0	1.0	1.0	1.7	10	10 ●	1	SSE 4	SW 4	SW 2
11	101.6	102.1	102.1	101.9	17.1	24.1	21.0	20.8	26.9	13.2	87	59	74	73	2.6	12.3	6.4	7.1	0	8	4	SW 4	SW 5	S 4
12	102.0	102.7	103.5	102.7	19.2	20.3	16.9	18.3	24.0	15.5	82	78	88	83	4.0	5.2	2.3	3.8	9	9	8	C 0	W 1	WSW 1
13	104.9	105.8	105.8	105.5	16.4	24.2	16.1	18.2	25.2	12.1	86	50	92	76	2.7	15.1	1.6	6.5	1	8	6	WSW 3	WSW 4	C 0
14	104.7	104.4	102.0	103.7	15.6	17.9	16.4	16.6	19.4	12.4	92	84	81	86	1.3	3.2	3.4	2.6	10 ●	10	10	C 0	C 0	NE 1
15	99.4	100.4	101.7	100.5	14.8	20.9	17.7	17.8	23.5	14.0	94	73	91	86	0.9	6.6	1.8	3.1	10 ●	8	8	NW 3	WSW 4	W 1
16	102.0	102.0	102.7	102.2	17.1	21.5	14.2	16.8	23.5	14.2	91	75	99	88	1.8	6.3	0.2	2.8	10	9	10 ●	W 2	SW 2	C 0
17	101.4	101.3	100.2	101.0	13.7	17.9	14.9	15.4	20.4	12.5	95	70	81	82	0.7	6.1	3.3	3.4	6	9	9	WSW 4	W 4	W 2
18	98.1	98.1	99.7	98.6	14.0	17.8	14.3	15.1	18.8	11.9	92	74	89	85	1.3	5.4	1.8	2.8	10	9	4	SW 4	WSW 5	WSW 2
19	102.3	104.8	107.5	104.9	13.8	18.3	15.3	15.7	19.4	10.2	90	77	92	86	1.6	4.8	1.3	2.6	2	6	8	WSW 5	W 3	W 1
20	108.6	107.5	107.4	107.8	13.6	22.3	16.9	17.4	22.5	10.9	95	56	82	78	0.7	11.9	3.5	5.4	9	7	8	W 3	WSW 6	SW 3
21	106.1	104.8	103.3	104.7	16.1	20.5	13.9	16.1	22.0	12.5	98	65	97	87	0.4	8.3	0.6	3.1	10 ●	8	10 ●	WSW 2	SW 2	ENE 4
22	102.1	102.1	103.3	102.5	11.7	17.3	10.6	12.6	17.9	10.6	95	61	91	82	0.6	7.6	1.2	3.1	9	8	1	NW 4	NW 3	W 1
23	104.2	103.9	103.7	103.9	9.9	18.1	10.4	12.2	19.4	6.5	86	51	92	76	1.8	10.2	1.0	4.3	0	6	0	W 2	W 5	C 0
24	100.6	95.2	98.3	98.0	11.9	18.5	12.7	14.0	19.9	8.1	78	70	95	81	3.0	6.5	0.7	3.4	9	10	6	S 5	SSE 7	SW 5
25	104.5	102.6	99.9	102.3	10.9	19.9	16.2	15.8	21.2	7.9	85	49	69	68	7.9	11.7	5.6	6.4	0	3	0	SW 7	SW 8	SSE 6
26	100.2	99.9	100.9	100.3	12.6	16.1	11.7	13.0	18.4	10.0	82	71	90	81	2.6	5.2	1.3	3.0	8	9	6	SW 4	SW 5	SW 6
27	102.6	103.9	104.4	103.6	12.0	16.4	11.1	12.6	17.6	9.4	91	67	91	83	1.2	6.2	1.1	2.8	9	9	0	WSW 6	WSW 5	WSW 3
28	103.8	104.6	106.5	105.0	11.8	15.9	12.3	13.1	16.9	9.2	93	79	95	89	1.0	3.8	0.7	1.8	6	10	9	WSW 7	WSW 2	C 0
29	107.9	108.5	109.7	108.7	8.8	16.8	10.9	11.8	18.3	6.1	100	64	91	85	0.0	6.8	1.1	2.6	10 ≡	7	7	C 0	W 5	WSW 2
30	110.4	109.8	110.4	110.2	9.7	13.3	11.3	11.4	16.4	8.3	99	84	93	92	0.1	2.5	1.0	1.2	10	8	4	W 2	NW 2	C 0
31	108.1	106.7	105.3	106.7	10.5	15.8	9.9	11.5	17.1	6.6	90	67	89	82	1.3	5.9	1.3	2.8	10 ●	8	7	S 3	SW 5	SSW 3
M	105.2	104.8	104.9	105.0	14.0	19.6	15.0	15.8	21.4	10.8	89	65	86	80	1.8	8.3	2.6	4.2	6.1	7.9	5.2	2.9	4.1	2.2

Bydgoszcz $H_s = 70\,m$ $H_b = 70{,}5\,m$ $h_w = 10\,m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.0	.	–	▽° 10^{00-03} . = $4^{30}-6^{40}$
2	8	2.0	.	–	•° 13^{12-26}
3	8	.	.	–	
4	8	2.8	.	–	↙ $23^{30}-24$
5	8	.	.	–	•° 2^{09-20} •└ 2^{30} ▽° 2^{57} . ↙ $0^{00}-1^{40}$. (↙)° 2^{07} ↙° $2^{07}-2^{25}-5^{30}$ NW – SE
6	8	.	.	–	
7	8	5.4	.	–	
8	8	0.6	.	–	•° $5^{30}-7^{30}$. ↙ $5^{15}-7^{45}$
9	7	7.7	.	–	▽° 6^{25-45} •° $8^{55}-9^{10}$ $10^{40}-11^{45}$ 13^{20-40} $17^{30}-19^{35}$. ↙° $6^{30}-6^{40}-7^{20}$ SW – SE . = $20^{20}-24$
10	7	5.8	.	–	•° 7^{25-45} $8^{25}-10^{00}$. = $0^{00}-1^{15}$ ≡° 4^{45} = -5^{10} ≡° 5^{35} = -7^{25} . $7^{45}-8^{22}$. $21^{53}-24$
11	8	1.4	.	–	•° $3^{05}-6^{35}$. = $0^{00}-3^{05}$
12	6	10.7	.	–	•° $5^{30}-16^{25}$. = $16^{25}-24$
13	8	0.0	.	–	▽ $22^{40}-23^{05}$. = $0^{00}-6^{30}$
14	7	30.0	.	–	•° $15^{44}-16^{06}$. $16^{31}-18^{00}$ •┴ 18^{50} •° 20^{40} •┴ $21^{15}-23^{45}$. ↙° $15^{30}-15^{45}-17^{20}$ NW – SE . = $4^{20}-9^{30}$
15	7	0.6	.	–	•┴ $1^{15}-4^{45}$ •° 10^{14-25} 16^{11-32} . = $4^{35}-10^{14}$
16	7	32.7	.	–	•° $16^{11}-19^{10}$ •┴ 21^{40} •° 24 . = $5^{15}-10^{40}$
17	7	1.6	.	–	•° $0^{00}-3^{18}$ •┴ 5^{30} •° 10^{40} •┴ 11^{15} •° 12^{38} . 18^{20-58} ▽° $21^{35}-22^{46}$
18	6	2.0	.	–	•° $12^{20}-14^{15}$ ▽° 16^{15-30} . = $22^{30}-24$
19	8	.	.	–	= $0^{00}-5^{30}$
20	8	12.1	.	–	▽° 16^{25-37} . 18^{02-12} . $19^{11}-20^{10}$. $20^{40}-21^{30}$ •° 21^{51} ▽° 22^{21-30} . ↙° $16^{05-20-40}$ S-NW . $17^{45}-18^{05}$. 18^{20} S-SE . $19^{45}-20^{40}$. 21^{30-50} .
21	7	25.2	.	–	•° 2^{25-57} . $19^{45}-21^{05}$ •┴ 22^{10} . ↙ 20^{30-40} ↙° $21^{40}-22^{05}-22^{40}$ E-SW . = $0^{00}-6^{40}$ [20.VII: = $4^{15}-6^{30}$. $23^{40}-24$
22	8	8.6	.	–	•° 7^{04-20} •┴ 7^{26} ▽° 7^{35} •° 21^{05-40} . $22^{20}-24$. = $0^{30}-7^{35}$
23	8	0.2	.	–	•° $0^{00}-1^{18}$ •° 14^{03-20} . (↙)° 14^{30-40} . = $4^{40}-7^{30}$
24	7	0.0	.	–	= $2^{40}-10^{15}$
25	8	0.0	.	–	•° 2^{30-45} . $20^{25}-22^{25}$
26	6	7.5	.	–	•° 7^{12-40} . $13^{45}-14^{50}$ •° $18^{50}-19^{10}$ •° $19^{32}-24$. = $0^{40}-7^{12}$
27	6	6.4	.	–	•° 0^{00-35} . $1^{30}-4^{40}$. $13^{30}-15^{30}$. 19^{20-35} . $20^{30}-21^{25}$. = $21^{25}-24$
28	7	2.1	.	–	•° $13^{55}-14^{02}$. 15^{40-51} (↙)° 18^{55-58} •° ↙ 19^{45} . = $0^{00}-7^{20}$. $22^{10}-24$
29	7	0.6	.	–	= $0^{00}-10^{38}$. ⌒ $n-8^{20}$
30	6	18.5	.	–	•° $5^{34}-6^{06}$. •° 8^{02-50} •° 10^{40} . 11^{20} . 15^{12} . $16^{25}-17^{10}$. 20^{20-26} •┴ 20^{34} •° 21^{10} . (↙)° $15^{20}-16^{30}$. $19^{50}-20^{00}$. = $4^{10}-5^{34}$
31	8	.	.	–	= $2^{30}-8^{30}$ [30.VII: $6^{05}-8^{02}$
Σ	–	184.5	–	–	UWAGI:

Sierpień – Août

1	8	.	.	–	⌒ $n-9^{00}$
2	8	.	.	–	= $0^{00}-4^{30}$. ⌒ $n-9^{55}$
3	8	.	.	–	⌒ $n-8^{15}$
4	8	.	.	–	= $6^{20}-8^{40}$. ⌒ $n-8^{30}$
5	8	.	.	–	= $0^{30}-3^{30}$. ⌒ $n-9^{00}$. ⌒ $16^{52}-19^{35}$
6	8	.	.	–	⌒ $n-8^{20}$
7	8	0.0	.	–	↙ $21^{35}-22^{30}$ (↙) $23^{40}-24$. = $2^{40}-7^{20}$. ⌒ $0^{00}-8^{00}$
8	8	0.0	.	–	•° 2^{05-30} . 15^{11-23} . (↙)° 0^{00-20} . = $3^{30}-4^{35}$ ≡┴ 5^{30} = -7^{40} . ⌒ $n-2^{05}$
9	8	.	.	–	⌒ $n-8^{30}$
10	6	22.2	.	–	•° 8^{25-35} •┴ 12^{30} •° 14^{20} ▲ 18^{10-11} •↙ 18^{10-25} . ⌒ $n-8^{25}$
11	8	.	.	–	⌒ $n-9^{00}$
12	8	0.0	.	–	•° $12^{13}-13^{00}$. ⌒ $n-8^{30}$
13	7	0.0	.	–	= $23^{30}-24$. ⌒┴ $n-9^{00}$ $23^{00}-24$
14	6	0.0	.	–	•° $7^{46}-8^{02}$ $12^{45}-13^{15}$ 14^{15-35} . = $0^{00}-17^{30}$ $21^{20}-24$. ⌒┴ $0^{00}-7^{46}$
15	7	0.0	.	–	•° $6^{33}-8^{40}$. = $0^{00}-4^{20}$ $8^{40}-11^{40}$ $22^{35}-24$. ⌒ $22^{00}-24$
16	7	7.7	.	–	•° $15^{28}-24$. = $0^{00}-13^{30}$. ⌒ $0^{00}-9^{00}$
17	8	.	.	–	•° $0^{00}-2^{35}$ = $2^{35}-4^{58}$ ≡° 5^{25} = -9^{25}
18	7	.	.	–	⌒ $n-8^{30}$ $20^{00}-24$
19	7	.	.	–	= $4^{30}-10^{20}$. ⌒ $0^{00}-9^{00}$
20	8	1.0	.	–	= $5^{20}-9^{20}$. ⌒ $n-8^{30}$
21	7	6.8	.	–	•° $5^{35}-9^{40}$ $18^{10}-24$. ⌒ $n-5^{35}$
22	7	1.5	.	–	•° $0^{00}-1^{40}$ $14^{20}-40$. $16^{35}-17^{15}$. = $1^{40}-4^{20}$. $8^{20}-11^{15}$
23	6	.	.	–	= $4^{40}-7^{30}$. ⌒ $n-10^{00}$
24	7	1.7	.	–	•° $14^{40}-20^{15}$. ⌒ $n-9^{30}$
25	7	.	.	–	⌒ $n-9^{00}$
26	8	0.0	.	–	•° 17^{05-12} . ⌒ $0^{00}-9^{10}$
27	7	3.7	.	–	•┴ 17^{15-35} . 19^{23-28} . ↙° $17^{20-25-32}$. = $20^{30}-24$. ⌒ $n-9^{10}$
28	7	0.	.	–	•° $17^{55}-18^{05}$. $19^{55}-20^{10}$. = $0^{00}-10^{30}$. $21^{35}-24$. ⌒ $n-10^{00}$
29	8	.	.	–	= $0^{00}-7^{30}$ ≡° 9^{25} = -11^{20} . ⌒ $n-9^{30}$
30	7	0.0	.	–	•° $12^{40}-13^{05}$. $13^{50}-14^{20}$. = $4^{15}-12^{40}$. ⌒ $n-9^{30}$
31	7	9.3	.	–	•° $5^{45}-10^{10}$. ↙° $14^{54}-16^{10}$. 16^{43} SW – NE . = $3^{25}-5^{20}$. $10^{10}-12^{40}$. $19^{43}-24$. ⌒ n
Σ	–	54.1	–	–	UWAGI:

Bydgoszcz — φ = 53°07' — λ = 17°58' — Wrzesień – Septembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III.	I	II	III
1	104.9	105.8	108.4	106.4	9.4	13.0	10.7	11.0	15.6	6.2	96	85	97	93	0.5	2.3	0.4	1.1	10 ●	9	3	WSW 3	W 5	WSW 2
2	108.2	107.0	105.7	107.0	9.4	18.5	14.5	14.2	19.4	5.2	91	57	87	78	1.1	9.1	2.2	4.1	0	7	9	WSW 3	SSW 6	C 0
3	104.3	106.2	108.9	106.5	13.1	16.4	10.1	12.4	17.3	10.1	95	74	97	89	0.7	4.7	0.4	1.9	10	8	2	SSW 4	NW 3	C 0
4	111.4	112.9	114.6	113.0	8.2	17.6	10.4	11.6	19.1	4.8	89	62	87	79	1.2	7.7	1.6	3.5	2	4	0	C 0	NW 3	C 0
5	114.4	111.8	108.9	111.7	7.8	17.9	14.9	13.9	19.4	2.6	93	47	78	73	0.8	10.8	3.6	5.1	1	6	9	C 0	SW 5	S 4
6	109.3	110.1	110.7	110.0	12.7	16.1	10.3	12.4	19.4	6.2	96	80	95	90	0.5	3.6	0.6	1.6	3	9	0	W 1	SW 3	C 0
7	112.0	111.4	110.0	111.1	7.1	22.6	17.0	15.9	23.5	4.0	99	54	81	76	0.2	12.5	3.8	5.5	6	4	4	C 0	SSW 4	SSE 3
8	110.1	110.9	111.2	110.7	14.6	27.1	17.9	19.4	27.8	11.7	88	50	84	74	2.0	17.8	3.2	7.7	1	4	2	S 2	S 5	C 0
9	110.4	110.0	114.5	111.6	15.8	26.3	15.2	18.1	27.0	12.6	88	54	85	76	2.1	15.6	2.6	6.8	1	0	9	SSW 1	WSW 5	NNW 2
10	114.9	113.4	110.4	112.9	12.1	16.1	10.2	12.2	18.8	10.2	94	73	96	88	0.8	4.9	0.4	2.0	9	9	1	N 1	NW 1	C 0
11	105.1	99.6	91.5	98.7	11.3	20.1	16.9	16.3	21.2	7.9	96	58	76	77	0.5	9.9	4.6	5.0	1	6	10 ●	WSW 2	SSW 8	S 7
12	85.6	85.9	91.5	87.7	15.5	14.9	12.1	13.6	17.9	11.2	94	78	69	80	1.1	3.6	4.3	3.0	10 ●	7	7	SSW 5	W 6	WSW 7
13	95.6	94.5	92.5	94.2	9.6	14.5	12.1	12.1	16.3	8.1	82	60	79	74	2.2	6.7	3.0	4.0	1	9	7	SW 7	SW 7	SW 5
14	93.9	95.1	97.1	95.4	9.4	13.9	9.9	10.8	15.9	7.5	84	69	79	77	1.9	4.9	2.5	3.1	9	9	1	SW 8	SW 7	SSW 3
15	96.6	97.1	100.7	98.1	8.2	10.3	9.4	9.3	12.0	5.5	93	94	93	93	0.8	0.8	0.8	0.8	10 ●	10 ●	0	SSW 3	W 3	W 3
16	103.4	106.0	108.2	105.9	8.4	9.6	7.2	8.1	11.5	6.1	89	88	96	91	1.2	1.5	0.5	1.1	8	10	4	SW 5	W 2	SW 2
17	108.0	106.5	105.9	106.8	3.8	9.1	6.8	6.6	10.6	1.6	100	95	90	95	0.0	0.7	1.0	0.6	10 ≡	10	1	SW 1	SW 1	SW 1
18	103.2	102.3	102.1	102.5	6.2	12.6	10.7	10.0	13.4	1.5	95	88	87	90	0.5	0.7	1.7	1.0	10 ●	9	10	W 5	WNW 6	WNW 4
19	100.3	98.5	97.3	98.7	8.3	11.9	9.8	10.0	12.2	6.9	93	83	99	92	0.8	2.3	0.1	1.1	4	10	10	W 3	WSW 1	C 0
20	99.9	103.1	106.6	103.2	8.2	11.2	8.7	9.2	12.1	7.4	96	78	86	87	0.5	2.9	1.5	1.6	8	9	9	WSW 2	NW 4	NW 1
21	108.4	108.3	107.0	107.9	7.2	13.6	8.2	9.3	14.6	6.0	96	70	96	87	0.5	4.7	0.5	1.9	10 ●	9	7	C 0	C 0	C 0
22	102.8	101.4	100.0	101.4	8.6	11.4	14.4	12.2	14.7	5.8	96	96	100	97	0.5	0.5	0.0	0.3	10 ●	10	10 ≡	NW 2	E 1	SSE 1
23	94.5	89.7	88.3	90.8	15.1	15.9	14.2	14.8	17.3	13.5	97	98	99	98	0.6	0.4	0.2	0.4	9	10 ●	10 ●	SW 5	S 4	WNW 5
24	95.4	94.6	97.3	95.8	10.2	8.6	7.1	8.2	14.5	6.3	93	90	80	88	0.8	1.1	2.1	1.3	9	10 ●	1	W 3	WSW 3	NW 7
25	102.8	106.0	109.4	106.1	6.2	11.3	4.0	6.4	11.9	4.0	73	48	83	68	2.6	7.0	1.3	3.6	4	6	0	W 6	WNW 7	NW 2
26	108.0	108.0	110.6	108.9	1.4	11.0	3.4	4.8	12.3	-0.9	94	51	83	76	0.4	6.4	1.3	2.7	2	5	0	C 0	NNW 5	NW 1
27	109.2	105.5	94.3	103.0	3.7	9.4	8.5	7.5	9.8	-2.2	87	67	96	83	1.1	3.8	0.5	1.8	9	9	10 ●	WSW 3	WSW 4	SW 8
28	93.4	94.6	96.1	94.7	9.4	10.0	8.1	8.9	12.4	7.3	83	86	79	83	2.0	1.5	2.3	1.9	4	9 ●	0	W 6	WNW 8	W 5
29	94.3	90.9	89.7	91.6	7.6	11.1	6.0	7.7	11.8	6.0	94	78	92	88	0.6	2.9	0.8	1.4	10 ●	10	8	W 3	SW 5	NW 1
30	93.5	96.8	105.3	98.5	5.4	8.3	3.8	5.3	11.1	3.4	91	83	90	88	0.9	1.9	0.8	1.2	10	8 ●	0	W 4	WNW 5	NW 3
31																								
M	103.1	102.8	103.2	103.0	9.1	14.3	10.4	11.0	16.0	6.2	92	73	88	84	1.0	5.1	1.6	2.6	6.4	7.8	4.8	2.9	4.2	2.6

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1	106.4	107.1	110.9	108.1	3.1	6.6	2.8	3.8	9.0	0.1	93	87	91	90	0.5	1.3	0.7	0.8	7	10 ●	0	W 3	NW 5	NNW 2
2	114.7	115.4	114.4	114.8	0.2	8.4	1.2	2.8	10.0	-2.6	84	62	83	76	1.0	4.1	1.2	2.1	2	8	0	C 0	SW 4	SW 2
3	108.0	103.5	99.0	103.5	2.9	7.4	8.2	6.7	9.0	1.7	86	84	85	85	1.0	1.6	1.7	1.4	7 ⊙	10 ●	10 ●	SW 4	SW 6	SW 7
4	100.6	103.9	110.0	104.8	6.0	8.9	5.1	6.3	10.3	5.0	82	63	83	76	1.8	4.2	1.5	2.5	8	9	0	NW 6	NW 7	W 4
5	112.3	111.5	108.2	110.7	6.4	9.2	7.2	7.5	11.1	0.8	85	60	87	77	1.4	4.6	1.4	2.5	9	9	10 ●	W 7	WSW 7	SW 5
6	107.8	111.5	114.1	111.1	9.4	11.1	10.1	10.2	12.6	6.4	93	88	88	90	0.8	1.6	1.5	1.3	10 ●	9	7	WSW 4	W 1	W 2
7	113.7	114.2	117.0	115.0	11.6	14.9	12.5	12.9	16.8	9.1	85	72	85	81	1.9	4.7	2.2	2.9	10	10	10	W 5	W 5	WNW 1
8	119.4	121.0	120.9	120.4	9.0	13.7	10.2	10.8	14.3	7.6	97	82	91	90	0.3	2.9	1.1	1.4	8	9	0	NW 1	S 4	SSW 2
9	118.4	116.6	114.5	116.5	4.6	18.2	10.8	11.1	18.8	3.5	97	61	94	84	0.3	8.1	0.9	3.1	0	0	0	C 0	SSW 3	S 1
10	113.3	112.4	111.7	112.5	5.7	18.9	10.0	11.2	19.9	4.6	97	58	91	82	0.3	9.2	1.1	3.5	0	0	0	S 2	SE 5	C 0
11	111.8	112.8	112.2	112.3	7.4	10.4	9.2	9.0	11.1	5.6	93	96	100	96	0.8	0.5	0.0	0.4	7	10 ≡	10 ≡	SW 2	SSW 1	C 0
12	109.7	112.3	118.3	113.4	7.8	11.7	6.0	7.9	13.4	7.2	99	95	92	95	0.2	0.6	0.8	0.5	10	9	1	C 0	WNW 5	C 0
13	119.5	118.1	115.4	117.7	4.4	12.2	7.0	7.6	14.4	2.6	98	76	98	91	0.2	3.4	0.1	1.2	6 ≡	8	4	NW 1	SW 2	C 0
14	114.6	115.7	118.0	116.1	8.2	11.3	7.8	8.8	11.8	3.6	99	85	97	94	0.2	2.0	0.3	0.8	10	9	4	WNW 2	WNW 4	WNW 1
15	119.5	120.9	120.3	120.2	3.0	7.8	6.7	6.0	8.4	1.0	93	84	96	91	0.6	1.7	0.4	0.9	9	10	10	NW 1	W 3	C 0
16	118.1	115.8	112.0	115.3	6.4	12.7	7.2	8.4	13.5	5.0	87	68	87	81	1.3	4.7	1.4	2.5	10	4	0	W 3	SSE 4	SE 3
17	107.0	108.0	109.3	108.1	3.4	13.2	10.3	9.3	13.9	2.1	97	83	94	91	0.3	2.6	0.8	1.2	1	9	4	SE 2	W 5	WSW 2
18	104.1	100.6	100.2	101.6	8.5	14.1	14.3	12.8	15.9	5.6	96	87	84	89	0.5	2.2	2.5	1.7	10	10 ●	10	SW 2	S 7	WSW 5
19	98.6	98.7	98.1	98.5	13.0	19.4	14.3	15.2	20.1	10.9	84	65	87	79	2.5	7.8	2.2	4.2	8	9	10	SW 6	W 6	C 0
20	102.8	105.3	107.7	105.3	8.6	10.5	5.3	7.4	14.5	4.9	96	88	95	93	0.5	1.5	0.4	0.8	10 ●	10	0	C 0	W 2	W 2
21	108.7	106.6	102.9	106.1	4.2	8.0	6.7	6.4	8.8	3.5	100	84	91	92	0.0	1.6	0.9	0.8	10 ≡	9	2	S 3	SSW 5	S 6
22	97.6	95.0	95.1	95.9	3.2	12.9	7.0	7.5	13.5	2.6	97	58	96	84	0.3	6.2	0.4	2.3	8	5	0	S 4	SSE 6	SSE 2
23	98.5	100.6	104.4	101.2	6.0	10.7	4.3	6.3	12.6	2.5	95	78	88	87	0.5	2.9	1.0	1.5	8	5	0	C 0	WSW 2	W 2
24	101.0	104.1	111.6	105.6	6.5	9.5	5.3	6.6	11.2	3.6	88	89	86	88	1.2	1.3	1.3	1.3	10 ●	10	0	SSW 7	WNW 5	WNW 2
25	115.7	117.0	116.4	116.4	1.0	10.4	4.6	5.2	11.3	-0.4	96	60	90	82	0.3	5.0	0.8	2.0	0	5	10	WNW 2	NW 5	W 1
26	114.4	113.7	112.1	113.4	5.6	14.3	5.5	7.7	15.3	4.0	91	74	95	87	0.9	4.3	0.4	1.9	7	8	0	WSW 2	W 5	SW 1
27	109.8	109.5	109.8	109.7	3.5	10.1	8.7	7.8	11.9	2.3	98	85	92	92	0.1	2.0	0.9	1.0	5	6	9	WSW 2	W 4	WSW 2
28	109.7	108.9	109.4	109.3	6.3	11.3	7.5	8.2	12.3	2.1	94	73	89	85	0.5	3.6	1.2	1.8	9	9	0	WSW 3	WSW 6	SW 4
29	108.0	108.2	108.2	108.1	7.7	12.6	9.9	10.0	14.2	5.4	87	72	82	80	1.3	4.1	2.2	2.5	9	8	8	WNW 5	W 6	WSW 4
30	105.7	104.6	105.5	105.3	5.0	13.9	11.5	10.5	15.1	4.4	95	70	85	83	0.4	4.7	2.0	2.4	2	9	10 ●	SW 4	W 6	W 3
31	104.7	103.0	100.7	102.8	9.6	13.7	12.0	11.8	13.9	8.8	92	69	79	80	1.0	4.9	3.0	3.0	9	9	10	W 3	W 6	WSW 5
M	109.5	109.6	109.9	109.7	6.1	11.9	8.0	8.5	13.2	4.0	93	76	90	86	0.7	3.5	1.2	1.8	7.1	7.9	4.5	2.8	4.6	2.3

Bydgoszcz $H_a = 70\ m$ $H_b = 70{,}5\ m$ $h_w = 10\ m$ **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	OBLIŚNIENIE GU h	USŁONECZNIENIE	POGODA
1	7	1.0	.	-	●⁰ 5¹⁵–9³⁵ : = 0⁰⁰–5¹⁵, 21⁴⁰–24 : ⌒ n–5¹⁵
2	7	.	.	-	= 0⁰⁰–11³⁰, 21²⁰–24 : ⌒ n–10⁰⁰
3	7	2.8	.	-	▽¹ 10⁴⁰–11⁰⁵ ▽⁰ 14⁰⁵–45 : = 0⁰⁰–11²⁰, 22³⁰–24 : ⌒ n–10⁰⁰
4	7	0.0	.	-	●⁰ 9⁴⁰–46 : = 0⁰⁰–6³⁵ ≡ –6⁵⁵ = –9³²: ⌒ n–9³⁰, 23⁰⁰–24
5	7	.	.	-	= 4²⁰–5¹⁵ : ⌒ 0⁰⁰–9³⁰
6	7	.	.	-	= 5³⁵–12³⁵ : ⌒ n–9³⁰ 21³⁰–24
7	7	.	.	-	≡⁰ 0⁰⁰–3⁴⁰ ≡¹–7³⁵ = –7⁵⁰ ≡¹–8³⁰ = –9³⁰ : ⌒ 0⁰⁰–9⁴⁰
8	6	.	.	-	= 2³⁰–9⁴⁰ ∞–17³⁰ : ⌒⁰ n–9⁰⁰
9	7	1.1	.	-	= 4²⁰–11⁴⁰ : ⌒ n–10²⁰
10	8	.	.	-	●⁰ 1⁵⁰–2¹⁵ 2³⁰–⁴⁰ 2⁵⁴–3¹⁰ ▽⁰ 3³⁵–4⁴⁸ : = 8²⁰–9⁴⁰
11	7	0.6	.	-	●⁰ 21¹²–22⁴⁰ 23⁴⁰–24 : = 5³⁰–8³⁰
12	7	4.0	.	-	●⁰ 0⁰⁰–²⁰ 1³⁰–3⁴⁰ 7⁴⁶–11³⁰, 12⁴⁰–13¹⁰
13	8	0.9	.	-	●⁰ 14⁰⁰–¹⁰ 21²⁶–⁴⁵
14	8	0.0	.	-	●⁰ 1¹⁵–3⁴⁰
15	6	8.2	.	-	●⁰ 7⁴⁰–9¹⁵ 10³⁰–14²⁰ 14⁴⁵–18¹² : ⌒ n–7⁴⁰
16	7	2.0	.	-	●⁰ 13¹⁰–⁴⁵ 14⁵⁰–15³⁵ : = 21²⁰–24
17	6	0.0	.	-	= 0⁰⁰–1³⁵ ≡⁰–4⁰⁰ ≡²–8³⁰ = –14³⁰ 17⁴⁰–24 : ⌒ n–10²⁰
18	7	1.0	.	-	●⁰ 7⁴⁰–11³⁵ 13¹⁵–³², 14⁰⁵–¹⁵ : = 0⁰⁰–7⁴⁰
19	7	1.2	.	-	●⁰ 16²⁰–19⁴⁰ : = 5⁴⁰–11⁴⁰, 19⁴⁰–24 : ⌒ n–11⁴⁰
20	8	0.9	.	-	●⁰ 2⁵⁰–3⁴⁰ : = 0¹⁰–2⁵⁰, 3⁴⁰–8⁰⁵
21	8	1.1	.	-	●⁰ 5⁴⁵–8⁴⁰ : = 20³⁰–24
22	6	2.6	.	-	●⁰ 6²⁰–10⁴⁰ 16¹⁰–17³⁵ : = 0⁰⁰–6²⁰, 10⁴⁰–16¹⁸, 17³⁵–18³⁵ ≡⁰–24
23	6	17.9	.	-	●⁰ 1¹⁴–¹⁸ ▽⁰ 1⁵²–2¹⁰ ●⁰ 2³⁰–5³⁰ 11⁴⁰–17²⁰ ●¹–20⁴⁰ ●⁰–23¹⁰ : R 1¹⁰–20–⁴⁵ SW–SE : ≡⁰ 0⁰⁰–3⁵⁰ = – 10⁴⁰
24	6	1.9	.	-	●⁰ 12³⁰–15³⁸ ▽¹ 20³⁰–21⁰⁵
25	8	.	.	-	
26	8	.	.	-	⌴ n–7⁰⁰
27	7	6.4	.	-	●⁰ 15⁴⁰–24 ⌴ n–4³⁰ : ⌒ 4³⁰–10⁰⁰
28	6	2.2	.	-	●⁰ 0⁰⁰–³⁶ 1¹⁵–2⁵⁰ 3⁴⁰–4²² 12¹⁵–¹⁹, 12³¹–³⁵, 13⁴⁴–14¹⁶, 14²¹–³⁰, 14⁵⁰–15⁰⁰
29	8	1.1	.	-	●⁰ 1²⁰–2²⁰ ▽⁰ 6³⁰–7⁰⁵ ●⁰ 15⁴³–⁵⁷, 18⁵⁰–19²⁰ : ⌒ 20³²–21⁰⁵
30	7	3.9	.	-	●⁰ 8¹⁵–³⁶ ●⁰ 10⁵⁰–11⁰² ▽⁰ 12⁴⁵–⁵⁸ ●⁰ 13³⁰–³⁷, 13⁴²–⁴⁵, 13⁵³–14⁰¹, 14⁵²–15⁰⁵, 16⁰³–¹⁴ 16⁴³–⁵⁰ ⌒ 16⁰⁶–²⁰
31					
Σ	–	60.8	–	-	UWAGI.

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1	6	0.6	.	-	●⁰ 11¹⁵–13⁴⁰ : ⌒ n, 22⁰⁰–24
2	8	.	.	-	⌒ 0⁰⁰–2⁰⁰ : ⌴ 2⁰⁰–8³⁰ 22⁴⁵–24
3	6	0.4	.	-	●⁰ 12⁴⁰–14³⁵ 16⁴⁰–17²⁰, 19²⁰–22³⁵ : ⌴ 0⁰⁰–6³⁰
4	8	0.2	.	-	● 7³⁵–9⁰⁶
5	8	1.8	.	-	●⁰ 7¹⁵–22 18⁴⁴–24
6	7	0.3	.	-	●⁰ 0⁰⁰–3²⁵, 6⁴⁵–7³⁵, 11⁰⁵–¹², 11³¹–⁴⁰, 12¹⁵–²⁸ : = 3²⁵–6⁴⁵, 7³⁵–11²⁵
7	7	0.0	.	-	●⁰ 7⁴¹–8⁴⁰
8	7	.	.	-	= 1³⁰–5³⁰ ≡¹–6⁴⁵ = –7¹⁵ ≡¹–8¹⁵ = –9⁴⁰, 23⁴⁰–24
9	7	.	.	-	= 0⁰⁰–5⁵⁰ ≡²–6⁵⁰ = –10³⁰ 18³⁰–24
10	6	.	.	-	= 0⁰⁰–13²⁰ ∞–16³⁰ = 22³⁰–24
11	3	.	.	-	= 0⁰⁰–8⁰⁵ ≡⁰–15¹⁵ = –20⁴⁵ ≡¹–24 : ⌒ n–8³⁰
12	6	1.0	.	-	●⁰ 7⁰⁵–¹⁵ 7⁴³–9³⁰ ≡¹ 0⁰⁰–6³⁰ = –24
13	7	.	.	-	= 0⁰⁰–5⁴⁰ ≡⁰–9⁴⁰ = –11³⁰, 17³⁰–24
14	6	.	.	-	= 0⁰⁰–24
15	7	.	.	-	= 0⁰⁰–1³⁰ 5³⁰–7⁰⁰, 19³⁰–21²⁰ : ⌒² n–8³⁰ ⌒ 22⁰⁰–24
16	7	.	.	-	⌒ 0⁰⁰–9⁰⁰
17	6	0.0	.	-	●⁰ 10¹³–⁵¹ : = 2²⁰–14⁴⁰
18	6	0.0	.	-	●⁰ 11³⁵–13⁴⁰ : = 0³⁰–11³⁵ 13⁴⁰–14²⁰
19	7	1.2	.	-	= 18⁵⁰–24 : ⌒ 21⁰⁰–24
20	7	1.0	.	-	●⁰ 5²⁰–9⁴⁰ : = 20²⁰–21⁵⁰ ≡¹–24 : ⌒ 0⁰⁰–5²⁰
21	7	.	.	-	≡¹ 0⁰⁰–9⁰⁵ = –12³⁰ 16³⁰–24 : ⌒ n–9⁰⁰, 21⁰⁰–24
22	7	.	.	-	= 0⁰⁰–11⁴⁰, 14³⁰–24 : ⌒ 0⁰⁰–10³⁵
23	7	0.9	.	-	●⁰ 8⁴²–9⁰⁵ : = 0⁰⁰–12³⁰
24	7	0.7	.	-	●⁰ 2²⁰–8³⁵ : = 8³⁵–12³⁰ : ⌒ 22⁰⁰–24
25	7	.	.	-	= 4¹⁰–9²⁵ : ⌒ 0⁰⁰–1²⁰ ⌴ –9¹⁵
26	6	.	.	-	= 6¹⁵–13¹², 16³⁵–24
27	6	.	.	-	= 0⁰⁰–24
28	7	.	.	-	= 0⁰⁰–11³⁰ : ⌒ 23⁰⁰–24
29	7	0.0	.	-	= 0⁴⁰–11³⁰ : ⌒ 0⁰⁰–9⁰⁰
30	7	0.0	.	-	●⁰ 17³⁶–⁴⁵ : 20³⁵–21⁰⁵ : = 5³⁰–8⁴⁰
31	7	0.0	.	-	●⁰ 0⁴⁰–1⁴⁵ : = 1⁴⁵–11³⁰
Σ	–	8.1	–	-	UWAGI.

Bydgoszcz $\varphi = 53°07'$ $\lambda = 17°58'$ **Listopad – Novembre 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.9	95.1	98.3	96.4	8.9	12.7	9.6	10.2	13.2	8.3	-	-	-	-	-	-	-	-	9	9	6	SW 5	WSW 7	WSW 2
2	102.0	103.1	105.4	103.5	5.2	12.0	3.2	5.9	12.8	2.7	-	-	-	-	-	-	-	-	10 ≡	5	3	WSW 2	WSW 5	SW 3
3	106.9	107.1	105.2	106.4	-0.5	12.8	5.5	5.8	12.9	-1.5	-	-	-	-	-	-	-	-	3	2	3	C 0	S 3	SE 2
4	103.8	103.8	103.7	103.8	7.2	13.5	9.3	9.8	13.8	4.9	-	-	-	-	-	-	-	-	10 ≡	6	8	S 2	S 3	S 2
5	102.3	98.4	98.5	99.7	3.9	16.7	11.9	11.1	17.1	3.1	-	-	-	-	-	-	-	-	5 ≡	5	3	ESE 2	S 8	S 7
6	98.9	100.0	99.7	99.5	10.3	14.1	9.6	10.9	14.5	9.0	-	-	-	-	-	-	-	-	9	9	8	S 7	SSW 5	SE 2
7	96.3	96.8	99.3	97.5	10.7	13.6	8.7	10.4	14.3	8.5	-	-	-	-	-	-	-	-	9	10	10	S 6	WSW 6	WSW 1
8	99.9	99.7	100.4	100.0	8.5	12.5	9.8	10.2	13.2	7.7	-	-	-	-	-	-	-	-	5	8	9	E 1	SE 3	SE 2
9	99.0	99.2	100.8	99.7	8.1	9.8	8.1	8.5	10.3	7.0	-	-	-	-	-	-	-	-	10	10	9	SE 3	SE 2	ESE 1
10	103.0	104.0	106.4	104.5	8.2	10.0	9.2	9.2	11.1	7.4	-	-	-	-	-	-	-	-	10	10	9	ESE 4	SE 4	E 5
11	109.2	111.5	114.4	111.7	8.1	9.2	7.5	8.1	10.0	6.9	-	-	-	-	-	-	-	-	10	10	10	ESE 5	ENE 4	ESE 6
12	117.4	120.0	122.2	119.9	5.5	5.2	3.1	4.2	7.8	1.9	-	-	-	-	-	-	-	-	10	10	10	ENE 5	E 5	E 5
13	122.8	123.4	123.5	123.2	-0.3	0.3	0.0	0.0	3.6	-1.6	-	-	-	-	-	-	-	-	9	9	10	NE 3	ENE 3	C 0
14	123.2	124.2	124.8	124.1	-2.1	1.2	0.2	-0.1	1.7	-5.3	-	-	-	-	-	-	-	-	10	10	10	SSW 1	S 1	C 0
15	124.5	123.6	123.1	123.7	-0.7	-0.9	-2.5	-1.6	1.5	-3.1	-	-	-	-	-	-	-	-	10	9	10	S 4	SSW 2	C 0
16	122.7	123.5	124.5	123.6	-1.4	-0.1	0.6	-0.1	0.7	-3.1	-	-	-	-	-	-	-	-	10 ●	10	10	C 0	C 0	E 1
17	125.0	125.5	126.5	125.7	0.7	3.0	1.6	1.7	3.1	0.1	-	-	-	-	-	-	-	-	10	10	10	SE 1	SE 4	ESE 3
18	125.9	125.4	124.5	125.3	1.4	2.7	1.3	1.7	2.9	0.6	-	-	-	-	-	-	-	-	10	10	10	SE 2	S 3	S 2
19	125.1	127.5	130.5	127.7	1.4	2.1	1.6	1.7	2.4	0.6	-	-	-	-	-	-	-	-	10	10	10	SE 1	SE 2	SSE 3
20	131.4	131.6	131.1	131.4	-2.0	4.5	-3.2	-1.0	4.8	-3.7	-	-	-	-	-	-	-	-	9	4	0	SE 2	S 6	S 2
21	130.1	128.3	123.0	127.1	-7.9	4.2	-2.8	-2.3	5.2	-8.5	-	-	-	-	-	-	-	-	1	0	0	C 0	SW 2	SSW 1
22	114.7	110.9	108.7	111.4	-5.8	2.3	1.2	-0.3	2.8	-6.4	-	-	-	-	-	-	-	-	0	5	10	SSW 3	W 4	W 4
23	106.6	105.6	109.0	107.1	0.2	1.4	2.8	1.8	3.1	-0.4	-	-	-	-	-	-	-	-	10 ●	10 ●	10	WSW 5	W 5	NW 5
24	111.7	110.6	109.4	110.6	1.8	2.7	5.0	3.6	5.3	0.6	-	-	-	-	-	-	-	-	10	10 ●	10 ●	WNW 4	WNW 7	WNW 8
25	106.9	107.9	110.3	108.4	5.9	7.9	8.1	7.5	8.9	4.4	-	-	-	-	-	-	-	-	10 ●	10	10 ●	WNW 6	NW 7	NW 4
26	111.7	111.6	109.5	110.9	8.0	8.1	6.9	7.5	8.4	6.5	-	-	-	-	-	-	-	-	10 ●	10 ●	10 ●	NW 5	WNW 5	WNW 7
27	105.0	105.2	108.3	106.2	7.1	7.7	6.3	6.8	8.7	5.6	-	-	-	-	-	-	-	-	10 ●	9	10	WNW 5	WNW 8	WNW 5
28	103.2	100.4	95.9	99.8	8.5	8.5	7.5	8.0	8.8	5.5	-	-	-	-	-	-	-	-	10 ●	10	10	NW 6	WNW 5	NW 6
29	100.9	105.6	120.3	108.9	2.7	0.5	-5.2	-1.8	7.8	-5.7	-	-	-	-	-	-	-	-	9	10 ✳	0	NNE 9	NE 9	ENE 7
30	123.8	124.2	124.1	124.0	-5.2	-2.6	-4.6	-4.2	-2.3	-8.1	-	-	-	-	-	-	-	-	4	6	9 ✳	N 1	NE 3	NNE 2
31																								
M	111.7	111.8	112.7	112.1	3.2	6.5	4.0	4.4	7.6	1.5	-	-	-	-	-	-	-	-	8.4	8.2	7.9	3.3	4.4	3.3

Grudzień – Décembre

1	121.9	119.0	117.0	119.3	-5.8	-1.1	-1.7	-2.6	-0.9	-11.5	-	-	-	-	-	-	-	-	8	10 ✳	10 ✳	WNW 3	NW 4	WNW 1
2	117.9	118.5	119.2	118.5	-0.6	1.9	1.4	1.0	2.2	-1.9	-	-	-	-	-	-	-	-	10 ✳	10	9	C 0	N 1	C 0
3	114.9	114.0	114.4	114.4	2.0	3.4	3.9	3.3	4.3	-0.9	-	-	-	-	-	-	-	-	10	10 ●	9	N 2	NE 2	C 0
4	114.3	113.7	111.2	113.1	2.6	2.4	3.6	3.0	4.2	2.1	-	-	-	-	-	-	-	-	10	10	10	WNW 1	NW 3	WNW 4
5	108.1	109.6	104.1	107.3	5.9	6.5	5.0	5.6	6.8	3.0	-	-	-	-	-	-	-	-	10	9	10	NW 4	NNW 6	NE 5
6	118.2	118.0	114.9	117.0	1.4	4.4	-0.6	1.2	5.8	-0.8	-	-	-	-	-	-	-	-	10	7	10	N 3	C 0	WSW 5
7	105.7	102.7	96.9	101.8	-1.0	1.0	0.0	0.0	1.1	-1.9	-	-	-	-	-	-	-	-	6	10	10 ●	WSW 5	WSW 5	WSW 5
8	81.3	72.7	65.8	73.3	0.4	2.8	6.7	4.2	8.2	-1.0	-	-	-	-	-	-	-	-	10 ✳	10 ●	6	SW 7	SW 9	WNW 10
9	64.3	75.1	87.5	75.6	4.3	2.0	-2.1	0.5	7.2	-2.6	-	-	-	-	-	-	-	-	9	10	8 ✳	NW 14	NW 6	WNW 5
10	87.6	88.1	96.5	90.7	-3.2	-3.4	-4.8	-4.0	-0.3	-5.2	-	-	-	-	-	-	-	-	3	10 ✳	0	W 5	N 5	NW 5
11	99.6	99.2	95.0	97.9	-9.0	-4.8	-4.6	-5.8	-4.0	-10.2	-	-	-	-	-	-	-	-	0	7	4	C 0	ESE 2	SE 5
12	91.3	89.9	89.5	90.2	-2.0	-0.3	-2.4	-1.8	0.3	-5.4	-	-	-	-	-	-	-	-	10	10	0	ESE 3	E 6	E 3
13	86.0	82.9	77.8	82.2	-0.4	2.2	1.6	1.2	2.7	-3.5	-	-	-	-	-	-	-	-	10	10	10	E 4	ESE 3	ENE 2
14	76.0	83.3	95.3	84.9	0.8	-0.4	-1.8	-0.8	1.8	-3.4	-	-	-	-	-	-	-	-	10 ●	10 ✳	9 ✳	NE 9	E 6	NE 7
15	109.0	115.3	120.7	115.0	-5.6	-5.4	-14.3	-9.9	-1.5	-15.0	-	-	-	-	-	-	-	-	3	5	0	ENE 7	E 5	C 0
16	122.4	123.3	121.5	122.4	-15.6	-6.8	-12.3	-11.8	-6.7	-18.0	-	-	-	-	-	-	-	-	0	0	0	C 0	C 0	SE 1
17	117.7	115.5	115.2	116.1	-14.3	-7.2	-16.1	-13.4	-6.8	-16.4	-	-	-	-	-	-	-	-	0	1	0	SE 1	C 0	C 0
18	115.8	116.1	116.9	116.3	-9.8	-6.8	-6.2	-7.2	-5.9	-16.6	-	-	-	-	-	-	-	-	10	10	10	C 0	C 0	S 1
19	116.9	119.0	122.0	119.3	-5.8	-5.4	-3.6	-4.6	-3.3	-8.3	-	-	-	-	-	-	-	-	10	10	10	S 3	S 3	SW 1
20	123.2	123.5	121.4	122.7	-1.4	0.9	-0.4	-0.3	1.1	-3.6	-	-	-	-	-	-	-	-	10	9	0	W 2	WNW 5	WSW 6
21	116.2	115.8	118.1	116.7	0.4	2.6	2.1	1.8	2.7	-1.9	-	-	-	-	-	-	-	-	5	10	10 ●	W 8	W 6	W 4
22	117.6	117.3	116.8	117.2	1.4	1.7	2.0	1.8	2.2	1.1	-	-	-	-	-	-	-	-	10	10 ≡	10	W 4	WSW 4	SW 2
23	113.0	110.6	109.2	110.9	0.2	-0.2	-3.2	-1.6	2.0	-3.2	-	-	-	-	-	-	-	-	6	6	0	S 4	S 5	SW 2
24	107.7	108.3	109.5	108.5	-4.8	0.4	-4.8	-3.5	0.5	-5.6	-	-	-	-	-	-	-	-	1	1	0	S 3	SSW 3	C 0
25	109.5	108.7	110.1	109.4	-6.5	-2.0	-2.5	-3.4	-0.9	-7.3	-	-	-	-	-	-	-	-	0	7	4	SSE 1	SE 4	WSW 2
26	112.5	114.9	116.8	114.7	-0.8	0.8	1.1	0.6	1.7	-4.5	-	-	-	-	-	-	-	-	10	10	10 ●	W 3	W 4	WNW 3
27	115.8	115.4	113.8	115.0	1.1	1.1	2.2	1.6	2.3	0.8	-	-	-	-	-	-	-	-	10	10 ●	10	W 4	W 4	W 6
28	108.4	104.5	100.1	104.3	2.0	2.5	2.4	2.3	2.7	0.7	-	-	-	-	-	-	-	-	10	10	10 ●	W 6	W 7	WSW 6
29	97.3	96.4	89.8	94.5	2.8	1.8	2.2	2.2	2.8	1.5	-	-	-	-	-	-	-	-	10	10 ●	10 ●	W 6	W 5	WSW 10
30	87.0	95.8	85.7	89.5	2.5	2.0	1.0	1.6	4.1	0.5	-	-	-	-	-	-	-	-	5	10 ●	10 ✳	W 8	W 7	W 5
31	89.8	90.5	90.7	90.3	0.8	1.2	1.0	1.0	1.4	0.2	-	-	-	-	-	-	-	-	10	9	8	W 6	W 6	W 6
M	105.4	105.7	105.3	105.5	-1.9	-0.1	-1.5	-1.2	1.2	-4.5	-	-	-	-	-	-	-	-	7.3	8.4	6.7	4.1	4.1	3.6

Bydgoszcz $H_s = 70\ m$ $H_b = 70{,}5\ m$ $h_w = 10\ m$ **Listopad – Novembre 1957**

DNI	WIATR	OPAD	GRUBOŚĆ ŚNIEGU	UTRUDNIENIE	POGODA
1	7	.	.	-	= 23¹⁵—24
2	7	.	.	-	= 0⁰⁰—5⁵⁰ ≡¹—8⁰⁰ ≡⁰—8⁴⁵ =—10³⁰ 20⁴⁰—23²⁵ ≡⁰—24; ∩ 22⁰⁰—24
3	8	.	.	-	≡⁰0⁰⁰—6¹⁵ =—10³⁰ 18⁴⁰—24; ∩ 0⁰⁰—4⁰⁰ ⌴—9⁴⁰
4	6	.	.	-	= 0⁰⁰—6²⁵ ≡⁰—10³² =—24
5	7	.	.	-	= 0⁸⁰—5⁴⁵ ≡¹—6⁴⁰ ≡⁰—7³⁰ =—9⁴⁰; ∩ n
6	7	.	.	-	= 16⁴⁰—24
7	7	0.0	.	-	•⁰17⁴⁰—19³⁵; = 0⁰⁰—2³⁰ 15³⁵—17⁴⁰, 19³⁵—24
8	6	0.0	.	-	•⁰18⁵⁶—19²⁵; = 0⁰⁰—18⁵⁶, 19²⁵—24
9	6	0.0	.	-	•⁰14⁵⁰—15²⁰; = 0⁰⁰—24; ∩ n—10⁰⁰
10	6	0.0	.	-	•⁰22⁴⁵—24; = 0⁰⁰—19⁰⁵
11	6	0.0	.	-	•⁰0⁰⁰—1⁴⁰ •⁰10⁴⁰—12³⁰, 16⁵⁵—17²⁵; = 12³⁰—20³¹
12	7	.	.	-	•⁰0⁵⁰—1⁵⁵
13	7	.	.	-	= 5³⁰—10³⁰
14	7	.	.	-	
15	7	0.0	.	-	= 15³⁰—24
16	5	0.0	.	-	•⁰6¹⁵—8²⁰; = 0⁰⁰—24
17	7	.	.	-	= 0⁰⁰—8²⁵
18	7	.	.	-	
19	7	.	.	-	
20	8	.	.	-	
21	6	.	.	-	= 5³⁰—24; ⌴ n—11²⁵ ⌴⁰ 17⁵⁰—24
22	6	0.0	.	-	= 0¹⁰—13³⁰ 16⁴⁰—24; ⌴ 0⁰⁰—12⁰⁰
23	6	0.2	.	-	•⁰5¹⁰—6²⁰ •⁰—7³⁰ *⁰8⁴⁰—9¹⁶, 11⁴¹⁻⁵⁷ •⁰12⁴⁰—15⁴⁵, 16⁵⁰—17⁴⁰; = 7³⁰—18³⁵
24	6	2.2	.	-	•⁰10²⁰—24
25	7	1.1	.	-	•⁰0⁰⁰—3³⁰ •⁰—5⁴⁰ •⁰—7³⁵ •⁰—8³⁶ •¹—9²⁵ •⁰15⁴⁰—23²⁰ •¹—24
26	6	1.5	.	-	•¹0⁰⁰—7⁴⁰ •⁰—8⁴⁰ •⁰—22³⁵ •⁰—23⁴⁵; = 23⁴⁵—24
27	7	0.8	.	-	•⁰1⁴⁰—8⁴⁰; = 0⁰⁰—1¹⁰
28	7	1.9	.	-	•⁰0⁵⁰—11⁴⁰ 13⁰⁷⁻⁴⁵ 16³⁵—18⁴⁵
29	6	2.2	.	-	*⁰10³⁰—11³⁹; 12¹⁵—13⁰⁵ 13³⁵—14⁰⁵ 15⁰⁷ 17¹⁵
30	7	0.0	.	-	*⁰4²⁵—5¹⁰, 10³⁵—11⁴⁰, 20¹⁴—21²⁵
31					
Σ	—	9.9	—	-	UWAGI.

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1	6	2.3	1	-	*⁰12⁴⁰—23⁴⁰; = 23⁴⁰—24
2	4	0.3	3	-	*⁰0¹⁵—1⁵⁰ 5³⁰—8¹⁵ •⁰9⁴⁰—11²⁷, 15⁵⁴—17³⁴; = 0¹⁵—7¹⁰ ≡⁰—9⁴⁰, 11²⁷—15⁵⁴, 17³⁴—24
3	5	1.1	.	-	•⁰10²⁵—14²⁰ 16⁴⁰—18¹⁰; = 0⁰⁰—7³⁰ ≡⁰—7⁵⁰ =—10²⁵
4	6	1.2	.	-	•⁰0³⁰—6³⁰ •⁰19⁴⁰—20³⁵, 21⁵¹—24; ≡⁰5⁴⁵—6⁵⁰ =—24
5	7	.	.	-	•⁰0⁰⁰—4³⁵; = 0⁰⁰—7⁴⁰
6	6	0.0	.	-	•⁰17³⁵—19¹⁵; = 10²⁰—16³⁰ ≡¹—17³⁵ = 19¹⁵—24
7	6	0.3	.	-	•⁰14⁴⁰—17¹⁰ 20³⁵—23²⁰; = 0⁰⁰—20³⁵
8	6	9.5	1	-	*⁰0⁴⁵—7¹⁰ •⁰10⁴⁵—19³²; = 7¹⁰—10⁴⁵
9	8	0.0	.	-	•⁰2⁵⁵—4¹⁵ 9¹⁵—10²⁰, 13¹⁵⁻⁴⁵ *⁰20³⁷—21⁰²; ⩥ 2⁴⁵—4³⁰ (por. do 25 m/sek) ⩤—6⁴⁰ (por. do 25 m/sek) ⩥—7⁵⁰ (por. do 20 m/sek)
10	5	1.8	.	-	*⁰11⁴⁵—14⁰⁵
11	7	.	1	-	= 14³⁰—20³⁰
12	7	0.0	1	-	= 15²⁵—24
13	6	1.6	1	-	*⁰0⁵⁰—2⁰⁵ •⁰21²⁰—24; = 0⁰⁰—21²⁰
14	6	5.4	.	-	•⁰0⁰⁰—3⁴⁰, 4²⁵—5³⁶, 6¹⁰—12³⁵ *⁰—13⁴⁰ *⁰—21³⁵; = 2⁴⁰—4²⁵
15	7	.	3	-	
16	5	.	3	-	= 7³⁰—24
17	7	.	3	-	= 5³⁰—9³⁰, 16²⁵—20²⁰
18	6	.	3	-	= 1⁴⁵—5¹⁵, 6⁵⁰—24; V n
19	6	0.0	3	-	*⁰23³⁵—24; = 0⁰⁰—23³⁵
20	6	.	3	-	*⁰0⁰⁰—2⁰⁵; = 2⁰²—24
21	7	0.0	3	-	•⁰17²⁵—18⁵⁰, 20³²—21¹⁵; = 21¹⁵—24
22	3	0.3	0	-	•⁰15²⁵—20¹⁰; = 0⁰⁰—8⁴⁵ ≡⁰—13⁴⁵ =—24
23	6	.	pz.	-	= 0⁰⁰—24
24	7	.	.	-	= 0⁰⁰—12³⁰, 13⁴⁰—24
25	6	.	.	-	= 0⁰⁰—24
26	5	0.3	.	-	•⁰10⁴⁰—11¹⁵ •⁰16³⁰—24; ∞ 21⁴⁵—24
27	4	0.0	.	-	•⁰0⁰⁰—1¹⁰, 9¹⁵, 14⁴⁰—18⁴⁵—19¹⁵; = 0⁰⁰—24; ∞ 0⁰⁰—1¹⁰
28	5	2.6	.	-	•⁰18²⁰—24; = 0⁰⁰—18²⁰
29	6	3.3	.	-	•⁰0⁰⁰—1³⁵ 8²⁰—11⁴⁰ 12²⁰—16³⁰ 18²⁵—24; = 1³⁵—7³⁰ 11⁴⁰—12²⁰ 16³⁰—18²⁵
30	6	6.5	.	-	•⁰0⁰⁰—2⁴⁰ 3³⁵—6³⁰, 9⁴⁰⁻⁵⁰, 11¹⁵—14³⁵, 16³⁰—17³⁵ *⁰—19³⁰ *⁰20²⁰—21³⁵; = 19³⁰—20²⁰
31	7	0.0	2	-	*⁰9⁴⁰—10⁰⁵
Σ	—	96.5	—	-	UWAGI.

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ **Styczeń – Janvier 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	105.4	103.8	103.1	104.1	-10.1	-8.6	-6.4	-7.9	-6.4	-11.8	74	77	83	78	0.7	0.7	0.6	0.7	10	10 ✳	10	SE 12	SE 8	SSE 4
2	101.8	100.8	100.6	101.1	-4.8	-2.7	-1.3	-2.5	-0.9	-7.1	83	89	84	85	0.7	0.6	0.9	0.7	10	10	10	SSE 4	SE 5	SSE 9
3	103.2	105.3	106.5	105.0	-0.7	0.9	0.3	0.2	1.1	-1.7	89	94	94	92	0.6	0.4	0.3	0.4	10 ✳	10 ✳	10 ✳	S 2	SW 2	C 0
4	106.6	108.5	109.4	108.2	0.3	0.7	0.3	0.4	0.8	-0.3	100	98	96	98	0.0	0.1	0.2	0.1	10 ≡	10	10	C 0	SSW 1	S 3
5	107.3	104.2	95.7	102.4	-0.9	-0.4	1.4	0.4	1.6	-1.3	98	80	92	90	0.1	1.2	0.6	0.6	6	10	10 ●	S 3	SW 7	SSW 7
6	92.0	87.0	86.4	88.5	2.5	5.8	3.5	3.8	6.3	1.1	96	98	86	94	0.1	0.1	1.0	0.4	10 ●	10 ●	0	SW 3	SW 5	W 8
7	87.5	93.7	100.7	94.0	1.9	3.1	1.9	2.2	3.6	1.4	87	78	75	80	0.9	1.7	1.8	1.5	10 ●	9	9	W 10	WNW 7	NW 10
8	106.5	103.8	101.1	103.8	1.7	2.7	3.7	3.0	3.8	0.5	78	91	98	89	1.5	0.6	0.2	0.8	9	10 ●	10 ●	W 5	SSW 4	SW 4
9	100.0	99.1	97.2	98.8	5.9	5.9	5.7	5.8	6.1	3.3	97	92	89	93	0.3	0.7	1.0	0.7	10 ●	10	10	W 5	SSW 7	W 5
10	92.1	91.0	90.2	91.1	5.1	4.5	0.7	2.8	6.0	0.5	94	76	83	84	0.6	2.0	1.1	1.2	10 ●	10	9	SW 9	W 7	W 6
11	91.5	93.2	96.5	93.7	0.7	1.3	0.3	0.6	1.7	-0.1	81	87	86	85	1.2	0.9	0.8	1.0	9	9	10	W 3	NW 2	W 7
12	93.9	90.9	85.6	90.1	-0.8	0.0	0.1	-0.2	0.4	-1.2	89	92	85	89	0.6	0.5	1.0	0.7	8	10	10 ✳	W 7	SW 4	SW 4
13	86.6	90.6	96.9	91.4	0.1	0.7	-5.6	-2.6	1.3	-5.9	100	94	90	95	0.0	0.4	0.4	0.3	10 ✳	10 ✳	10 ✳	SW 3	S 2	NE 6
14	103.9	108.4	113.3	108.5	-8.8	-8.2	-11.1	-9.8	-5.3	-11.5	86	84	79	83	0.4	0.5	0.5	0.5	10	7	2	NE 8	NE 6	NE 4
15	114.1	112.2	110.8	112.4	-11.6	-10.5	-16.1	-13.6	-9.4	-16.8	86	84	81	84	0.4	0.4	0.3	0.4	10	0 ⊙	0	E 7	NE 3	NE 1
16	111.9	112.8	113.5	112.7	-15.8	-10.5	-11.7	-12.4	-9.6	-19.5	91	87	86	88	0.2	0.4	0.3	0.3	4	0 ⊙	10	C 0	C 0	WSW 1
17	111.3	110.7	110.2	110.7	-8.4	-4.5	-0.4	-3.4	-0.3	-12.0	86	86	92	88	0.4	0.6	0.5	0.5	10	10	10	W 2	W 4	W 4
18	107.0	106.8	106.2	106.7	-1.1	-0.9	-2.3	-1.6	0.5	-2.7	93	93	91	92	0.4	0.4	0.5	0.4	10	10	10	W 6	WNW 9	WNW 6
19	106.3	108.2	110.6	108.4	-1.1	0.0	-1.1	-0.8	0.5	-3.0	93	92	97	94	0.4	0.5	0.2	0.4	10	10	10	W 4	W 6	WNW 3
20	110.0	108.3	105.5	107.9	-4.6	-2.2	-1.9	-2.6	-0.7	-4.7	96	91	94	94	0.2	0.5	0.3	0.3	10 ✳	10	10	WSW 3	SW 6	WSW 8
21	101.1	101.4	103.2	101.9	-4.9	-1.6	-2.1	-2.7	-1.3	-5.7	88	69	81	79	0.5	1.6	1.0	1.0	5	2 ⊙	10	SW 7	WSW 9	WSW 7
22	104.9	105.8	103.1	104.6	-5.3	-4.3	-7.2	-6.0	-2.0	-8.1	90	77	82	83	0.4	1.0	0.6	0.7	10	0 ⊙	0	SW 6	SW 4	SW 3
23	101.0	102.4	103.1	102.2	-9.3	-3.9	-4.9	-5.8	-2.8	-10.0	82	89	88	86	0.5	0.5	0.5	0.5	0	10	9	SW 3	SW 5	SW 4
24	102.3	100.5	98.9	99.9	-6.1	-3.1	-3.1	-3.8	-2.4	-9.9	89	86	88	88	0.4	0.7	0.6	0.6	10	10	10	E 3	SSE 4	E 5
25	94.5	93.7	94.5	94.2	-4.1	-2.1	-1.1	-2.1	-0.8	-4.4	91	89	85	88	0.4	0.5	0.9	0.6	10	10 ✳	10	SE 3	S 1	SSW 1
26	99.6	102.4	103.4	101.8	-5.2	-1.7	-0.6	-2.0	0.8	-5.7	80	82	91	84	0.8	1.0	0.5	0.8	10 ≡	10	10	W 3	C 0	SW 4
27	97.1	97.3	97.7	97.4	-1.1	0.7	1.9	0.8	2.3	-2.2	93	86	93	91	0.4	0.9	0.5	0.6	9	10 ✳	5	SSW 4	SW 7	SW 5
28	100.1	102.7	108.4	103.7	-1.8	1.1	-0.3	-0.3	2.1	-2.3	94	89	80	88	0.3	0.7	1.2	0.7	5	6 ⊙	9	SE 3	W 5	W 2
29	112.6	113.2	111.3	112.4	0.3	1.1	0.0	0.4	1.5	-0.6	82	81	92	85	1.1	1.2	0.5	0.9	10	10	10	W 2	WSW 3	SW 3
30	108.4	106.6	105.0	106.7	0.3	0.7	0.2	0.4	1.1	-0.6	90	96	94	93	0.6	0.2	0.4	0.4	10 ●	10 ●	6	SW 3	SW 2	S 2
31	106.2	108.3	108.7	107.7	-1.0	1.3	0.3	0.2	1.9	-1.7	92	87	92	90	0.5	0.9	0.5	0.6	9	6 ⊙	10	S 3	SE 4	S 3
M	102.2	102.4	102.4	102.3	-2.9	-1.1	-1.8	-1.9	0.0	-4.6	89	87	88	88	0.5	0.7	0.6	0.6	8.8	8.4	8.4	4.4	4.5	4.5

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1	106.2	106.2	104.9	105.8	-0.9	0.1	-0.1	-0.2	0.5	-2.5	89	82	82	84	0.6	1.2	1.1	1.0	10	9	10	SSE 4	SSE 6	SSE12
2	101.6	103.9	107.0	104.2	1.2	3.9	3.2	2.9	5.2	-0.6	90	98	90	93	0.7	0.2	0.8	0.6	10 ●	10	9	SSW 8	SW 5	W 3
3	108.2	108.0	109.5	108.6	1.1	2.8	0.3	1.1	3.4	-0.1	90	89	90	90	0.6	0.8	0.6	0.7	10	10	0	W 2	W 2	W 3
4	111.8	111.4	105.7	109.6	-0.9	-0.9	0.3	-0.3	0.5	-2.1	91	91	91	91	0.5	0.5	0.5	0.5	10	10	10 ●	SW 3	S 2	SW 3
5	104.4	105.1	103.4	104.3	1.3	1.7	1.2	1.4	2.7	-0.2	98	94	98	97	0.1	0.4	0.2	0.2	10 ● ≡	10 ≡	10 ≡	WSW 2	SW 4	SSW 3
6	101.1	99.2	95.3	98.5	0.3	4.7	2.5	2.5	6.3	-0.3	98	95	98	97	0.1	0.4	0.1	0.2	3	2	0	SSW 3	SW 5	SSW 2
7	94.3	94.9	94.4	94.5	2.1	5.0	4.5	4.0	5.3	0.9	100	89	85	91	0.0	1.0	1.2	0.7	10 ●	10	9	SW 3	WSW 7	SW 7
8	95.7	93.6	87.8	92.4	1.9	4.7	2.8	3.0	5.3	1.3	82	85	93	87	1.3	1.2	0.6	1.0	10	10	10 ●	SW 6	SW 5	SSW 4
9	81.7	81.9	82.1	81.9	4.3	5.7	5.7	5.4	6.7	2.8	98	98	98	98	0.1	0.2	0.2	0.2	10 ●	10	10	SW 3	W 5	SW 3
10	82.7	85.7	89.6	86.0	1.9	2.3	2.7	2.4	5.7	1.3	94	87	95	92	0.4	0.9	0.4	0.6	10 ●	10	9	SW 6	NW 6	W 2
11	91.1	91.1	92.8	91.7	-0.9	2.5	1.2	1.0	3.1	-0.9	100	95	96	97	0.0	0.4	0.3	0.2	6	10 ●	10	SW 1	S 3	W 4
12	94.6	96.0	94.2	94.9	0.5	2.1	0.8	1.0	3.1	0.1	94	68	77	80	0.3	2.3	1.5	1.4	10	9	10	W 3	W 5	SSE 3
13	88.3	85.7	81.6	85.2	0.9	2.7	2.2	2.0	4.5	0.3	90	79	87	85	0.6	1.5	1.0	1.0	10	10	2	S 3	S 7	SSE 5
14	75.4	74.7	74.2	74.8	3.1	6.3	4.5	4.6	7.7	1.2	83	86	95	88	1.3	1.2	0.4	1.0	10	6	10 ●	SE 8	S 9	SSE 6
15	74.1	75.8	72.3	74.1	1.5	5.6	4.5	4.0	6.9	1.1	98	80	89	89	0.1	1.8	0.9	0.9	2	7	10	SSW 2	SW 5	SE 5
16	70.5	74.7	82.3	75.8	4.8	3.9	1.4	2.9	5.7	1.0	90	90	89	90	0.8	0.8	0.8	0.8	10 ●	10	7	SSW 3	SW 5	SW 4
17	87.7	90.2	91.6	89.8	0.7	3.1	0.3	1.1	4.1	-0.5	94	88	96	93	0.4	0.9	0.2	0.5	10	10	3	WSW 4	SW 5	SSW 2
18	91.9	93.0	88.3	91.1	0.3	5.7	4.3	3.6	6.7	-0.2	94	74	92	87	0.3	2.4	0.7	1.1	1	1 ⊙	10	SW 2	S 3	SE 4
19	78.1	77.3	90.1	81.8	5.3	6.1	1.2	3.4	6.3	-0.2	92	89	77	84	0.7	1.0	1.5	1.1	10	10	9	SE 6	S 5	W 8
20	96.3	97.5	96.2	96.7	-0.5	3.1	0.9	1.1	3.7	-0.8	88	88	90	89	0.7	0.9	0.6	0.7	2	7	0	SW 5	SW 5	S 3
21	94.5	93.8	94.1	94.1	1.1	5.7	1.5	2.4	6.3	0.3	87	70	91	83	0.9	2.8	0.6	1.4	10	7	0	S 5	S 6	S 3
22	94.7	95.3	95.2	95.1	0.5	0.3	-0.5	0.0	1.8	-0.8	94	96	96	95	0.3	0.2	0.3	0.3	10 ●	10 ✳	10 ≡	C 0	NW 7	NW 2
23	95.9	96.0	95.3	95.7	-2.9	1.1	-1.7	-1.3	1.6	-3.2	91	74	82	82	0.4	1.7	1.0	1.0	9	4	10 ✳	W 2	W 2	C 0
24	93.6	91.6	89.6	91.6	-3.4	-2.5	-1.6	-2.3	-0.9	-3.8	90	87	90	89	0.5	0.7	0.5	0.6	10	10	10	C 0	SSE 3	E 4
25	90.5	91.8	91.7	91.3	-3.3	0.3	-0.3	-0.9	0.7	-3.8	92	90	94	92	0.4	0.6	0.4	0.5	10	10	10 ✳	E 3	E 2	ENE 2
26	94.1	98.3	103.1	98.5	-1.1	-1.7	-3.3	-2.4	-0.1	-3.7	85	88	83	85	0.9	0.7	0.8	0.8	10 ✳	10	10	NE 2	NE 4	NE 3
27	106.8	108.5	109.6	108.3	-6.4	-3.2	-4.1	-4.4	-2.7	-6.9	83	79	73	78	0.6	1.0	1.2	0.9	10	10	10	N 1	N 1	NW 2
28	111.1	112.5	114.4	112.7	-7.4	-2.9	-3.7	-4.4	-1.0	-7.7	76	73	78	76	0.8	1.3	1.0	1.0	2	5 ⊙	3	NW 2	N 3	N 4
29																								
30																								
31																								
M	93.5	94.1	94.2	93.9	0.2	2.4	1.1	1.2	3.5	-1.0	91	86	89	89	0.5	1.0	0.7	0.7	8.4	8.5	7.5	3.3	4.5	3.8

Białystok $H_s = 139\ m$ $H_b = 140{,}8\ m$ $h_w = 11\ m$ **Styczeń – Janvier 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	2.7	6	.	$*^{0}\ 10^{20} - 19^{20}$
2	7	0.0	8	.	$*^{0}\ 0^{10} - 1^{30}$
3	6	4.3	8	.	$*^{0}\ 6^{15} - 21^{20}\ *^{1} - 24\ :=\ 17^{10} - 24$
4	6	.	12	.	$*^{1}\ 0^{00-18}\ *^{0} - 3^{02} :=\ 0^{00} - 6^{20}\ \equiv^{0} - 7^{30}\ \equiv^{1} - 8^{25}\ \equiv^{0} - 9^{30} = -20^{30}$
5	7	7.4	10	.	$\bullet^{0}\ 16^{40} - 18^{10}\ \bullet^{1} - 20^{45}\ \bullet^{0} - 22^{40} :=\ 3^{20} - 11^{20}$
6	6	8.6	5	.	$\bullet^{0}\ 0^{30} - 1^{40}\ \bullet^{1} - 2^{35}\ \bullet^{0}\ 5^{35} - 6^{00}\ \bullet^{0} - 9^{30}\ \bullet^{1} - 13^{38} :=\ 23^{0} - 6^{00}$
7	7	1.1	pż.	0.6	$\bullet^{0}\ 3^{07} - 4^{36}\ 6^{15} - 8^{20}$
8	6	0.2	.	.	$\bullet^{0}\ 12^{45} - 13^{20}\ 18^{08} - 20^{05}\ \bullet^{1} - 24 :=\ 13^{20} - 24$
9	7	0.0	.	.	$\bullet^{1}\ 0^{00} - 2^{20}\ \bullet^{0}\ 5^{00} - 7^{20}\ 8^{20} - 10^{12} :=\ 0^{00} - 8^{10}$
10	7	0.0	.	.	$\bullet^{0}\ 6^{15} - 7^{15}\ \bullet\ 23^{30} - 24 :\ \circlearrowright^{0}\ 18^{30} - 19^{20}$
11	7	0.9	1	1.2	$\triangledown^{0}\ 0^{00-10}\ 5^{30} - 6^{10}\ 6^{40} - 8^{04}\ \triangle^{1}\ 16^{15-20}$
12	7	8.8	pż.	1.5	$\triangle^{1}\ 0^{00-20}\ *^{0}\ 14^{15} - 21^{30}\ 23^{45} - 24$
13	6	4.2	7	.	$*^{0}\ 0^{00-35}\ 1^{45} - 7^{30}\ *^{1} - 10^{40}\ *^{0} - 21^{30}$
14	7	0.0	9	1.1	$*^{0}\ 0^{15} - 5^{30}\ 7^{45} - 8^{40}$
15	8	.	9	4.5	
16	7	.	9	2.1	$V^{0}\ 1^{10} - 24$
17	6	0.0	8	.	$*^{0}\ 7^{15} - 9^{30} :=\ 12^{10} - 19^{40}$
18	7	0.2	7	.	
19	7	0.0	7	.	$*^{1}\ 0^{45} - 3^{45}$
20	7	0.1	7	.	$\bullet^{0}\ 3^{20} - 5^{35}\ *^{0} - 12^{10} :=\ 0^{30} - 3^{20}$
21	8	0.0	7	3.1	$\triangle^{0}\ 2^{40} - 3^{30}$
22	7	(0.0)	7	2.0	$\bullet^{0}\ 1^{10} - 2^{18}\ 8^{35} :=\ 7^{18} - 11^{20}$
23	7	.	7	0.7	
24	7	0.3	7	.	
25	6	0.0	7	.	$*^{0}\ 0^{40} - 3^{28}\ 12^{25} - 13^{38} :=\ 9^{20} - 13^{45}$
26	4	0.0	7	.	$\bullet^{0}\ 11^{20} - 12^{05}\ \triangle^{0}\ 14^{30} - 15^{20} \equiv^{0} 3^{30} - 8^{45} = -12^{40}\ \equiv^{0} - 16^{50} = -20^{40}$
27	5	2.7	7	.	$*^{0}\ 8^{42} - 9^{05}\ *^{1} - 11^{38}\ *^{0} - 12^{20}\ *^{1} - 13^{40}\ \bullet^{1}\ 15^{33} - 16^{45} :=\ 0^{35} - 2^{30}\ 14^{30} - 18^{28}$
28	7	0.0	6	1.4	$*^{0}\ 17^{30} - 18^{35}$
29	7	0.2	5	0.2	
30	6	1.4	5	1.7	$*^{0}\ 1^{40} - 3^{25}\ \bullet^{0}\ 6^{10} - 13^{45} :=\ 8^{10} - 19^{10}$
31	7	0.0	5	.	
Σ	–	43.1	–	20.1	UWAGI.

Luty – Février

1	7	7.7	6	0.4	$*^{0}\ 1^{30} - 2^{20}\ *^{1} - 9^{20}\ *^{0} - 10^{32}\ \bullet^{0}\ 23^{40} - 24$
2	6	1.3	4	.	$\bullet^{0}\ 0^{00} - 8^{03} :=\ 8^{30} - 10^{45} \equiv -11^{45} = -15^{20}$
3	7	.	3	.	$\sqcup^{1}\ 21^{00} - 24$
4	6	1.3	3	.	$\bullet^{0}\ 18^{45} - 22^{35}$ (marznący), $23^{10} - 24$ (marznący) $:=\ 8^{10} - 24 :\ \sqcup^{1}\ 0^{00} - 8^{20}$
5	3	0.0	pż.	.	$\bullet^{0}\ 0^{00-18}\ \bullet^{0}\ 3^{30} - 8^{10} :=\ 0^{00} - 1^{40} \equiv^{2} - 19^{10} \equiv^{1} - 24$
6	7	1.3	pż.	5.0	$\equiv^{1}\ 0^{00} - 2^{00} \equiv^{0} - 2^{45} = -10^{20} :\ \sqcup^{0}\ 3^{30} - 8^{00}$
7	7	0.0	pż.	0.1	$\bullet^{0}\ 5^{15} - 7^{10}\ \bullet^{1} - 8^{20}\ \bullet^{0} - 8^{35} :=\ 8^{35} - 11^{30}$
8	7	6.8	.	0.2	$\bullet^{0}\ 19^{35} - 24 :\ \oplus^{0}\ 8^{10} - 12^{45}$
9	6	0.9	.	.	$\bullet^{0}\ 0^{00} - 9^{45}\ \bullet^{0}\ 17^{30} - 19^{45}\ \bullet^{1} - 20^{08}\ \bullet^{0}\ 21^{30}\ 22^{03} :=\ 12^{10} - 20^{00}$
10	7	0.8	.	.	$\bullet^{0}\ 5^{30} - 8^{35}\ 9^{06}\ 11^{40}\ 12^{45}\ 13^{30}\ 17^{20} - 18^{20}$
11	6	3.1	.	0.2	$\bullet^{0}\ 12^{02} - 15^{45}\ \bullet^{0}\ 18^{40} - 19^{02}\ 22^{45} - 23^{01} :=\ 3^{30} - 8^{30}\ 15^{10} - 16^{50} \equiv^{0} - 17^{40} = -24$
12	7	.	.	1.5	$\equiv^{0}\ 0^{00} - 3^{10}$
13	7	0.1	.	.	$*^{0}\ 9^{48} - 10^{40}\ \bullet^{0}\ 15^{10-20}$
14	7	7.4	.	0.9	$\bullet^{0}\ 7^{35} - 9^{43}\ 18^{35} - 24 :\ \circlearrowright^{0}\ 1^{10-40}$
15	7	3.4	.	4.7	$\bullet^{0}\ 0^{00} - 2^{15}\ \bullet^{1}\ 21^{05} - 24$
16	7	4.1	.	.	$\bullet^{1}\ 0^{00} - 2^{30}\ \bullet^{0}\ 3^{18} - 9^{35}\ 22^{35} - 23^{30}\ \bullet^{1} - 24$
17	7	0.5	.	1.4	$\bullet^{1}\ 0^{00-25}\ \bullet^{0} - 0^{45}\ \bullet^{0}\ 1^{20} - 3^{40}\ 22^{35} - 23^{05}\ 23^{10} - 24$
18	7	4.6	1	5.0	$*^{0}\ 0^{00-30}\ \bullet^{0}\ 21^{25} - 22^{15}\ \bullet^{1} - 24$
19	7	3.6	.	.	$\bullet^{0}\ 0^{00} - 2^{30}\ \bullet^{1}\ 9^{03} - 11^{42}\ \bullet^{1}\ 14^{30} - 16^{30}\ \bullet^{0} - 17^{35} :=\ 14^{15} - 15^{00}$
20	7	0.6	.	0.6	$\bullet^{0}\ 15^{02} - 16^{13}$
21	7	0.0	.	4.1	
22	6	7.8	.	3.7	$\bullet^{0}\ 5^{30} - 10^{15}\ \bullet^{0} - 12^{05}\ *^{0} - 14^{10}\ *^{1} - 17^{40}\ *^{0} - 19^{30}\ \bullet^{0} - 21^{35}$
23	7	0.0	5	.	$*^{0}\ 20^{15} - 21^{29}$
24	7	0.2	4	0.3	$*^{1}\ 18^{10} - 19^{00}\ *^{0} - 19^{40}$
25	7	0.7	3	.	$*^{0}\ 15^{15} - 18^{20}\ 19^{20} - 23^{10}$
26	6	0.0	5	.	$*^{0}\ 0^{15} - 5^{30}\ 6^{15-35}\ *^{1} - 7^{20}\ *^{0} - 9^{30}\ 13^{10} - 14^{38}$
27	7	.	5	.	
28	7	.	3	7.3	
29					
30					
31					
Σ	–	56.2	–	35.4	UWAGI.

119 728

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ **Marzec – Mars 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	114.9	114.8	114.1	114.6	-5.2	-2.5	-3.4	-3.6	-2.0	-6.8	88	72	76	79	0.5	1.5	1.1	1.0	9	9	9	NW 4	N 6	N 5
2	112.8	111.4	110.0	111.4	-7.0	-4.3	-8.4	-7.0	-3.0	-8.8	82	77	83	81	0.6	1.0	0.5	0.7	10	10	10 ✳	N 5	N 7	NNW 5
3	107.9	106.4	104.9	106.4	-9.2	-5.2	-10.3	-8.8	-4.0	-10.5	82	68	84	78	0.5	1.3	0.4	0.7	10 ✳	2 ⊙	0	N 1	NNW 1	C 0
4	101.3	98.5	92.4	97.4	-12.5	-2.9	-2.9	-5.3	-2.4	-13.3	92	64	71	76	0.2	1.7	1.4	1.1	2 ⊙	2 ⊙	10	C 0	S 5	S 6
5	91.5	93.2	94.9	93.2	-1.5	1.3	-1.1	-0.6	2.5	-4.1	78	72	73	74	1.2	1.9	1.6	1.6	10	7	2	W 2	W 5	NW 3
6	94.3	95.1	95.8	95.1	-2.1	-0.3	-2.7	-2.0	0.2	-3.7	87	86	84	86	0.6	0.9	0.8	0.8	10 ✳	10 ✳	10 ✳	W 3	WNW 4	NNW 3
7	98.1	99.7	101.3	99.7	-5.6	-0.9	-3.9	-3.6	-0.2	-6.5	85	67	80	77	0.6	1.9	0.9	1.1	9	3	4	NNW 2	N 2	ENE 3
8	103.5	104.9	107.2	105.2	-8.7	-1.3	-5.4	-5.2	0.3	-10.3	89	68	85	81	0.4	1.8	0.6	0.9	10	10	0	C 0	NE 3	N 1
9	109.8	111.0	113.0	111.3	-7.8	-0.9	-3.1	-3.7	-0.5	-8.5	87	67	75	76	0.4	1.9	1.2	1.2	2	3 ⊙	1	N 3	N 4	NNE 4
10	116.4	117.5	118.0	117.3	-9.1	1.7	-4.0	-3.8	3.6	-9.9	92	60	82	78	0.3	2.8	0.8	1.3	0 ⊙	0	2	C 0	N 1	SE 2
11	117.4	116.3	113.1	115.6	-7.4	4.7	0.9	-0.2	6.3	-8.1	90	57	68	72	0.3	3.6	2.1	2.0	2	0 ⊙	1	SW 2	W 2	W 2
12	108.5	104.3	99.8	104.2	-0.9	8.2	3.5	3.6	8.5	-3.3	79	58	78	72	1.2	4.6	1.7	2.5	10	9	9	SW 1	SSW 3	W 2
13	99.2	100.1	97.2	98.8	-0.7	3.3	6.1	3.7	7.4	-1.5	90	85	69	81	0.6	1.2	2.9	1.6	5	10	9	C 0	W 3	WSW 4
14	91.7	86.7	83.7	87.4	3.7	11.2	8.2	7.8	12.0	2.3	78	64	81	74	1.8	4.8	2.1	2.9	9	9	10	SW 4	SW 10	WSW 7
15	84.4	88.6	79.5	84.2	4.9	2.7	0.2	2.0	8.5	-0.1	89	84	96	90	1.0	1.2	0.3	0.8	10	10	10 ✳	W 8	SW 10	SW 4
16	79.1	84.8	94.2	86.0	-0.9	-5.4	-10.7	-6.9	0.5	-11.1	89	75	77	80	0.6	1.0	0.6	0.7	7	10 ✳	0	W 5	W 8	W 2
17	100.4	101.0	94.1	98.5	-13.6	-7.4	-6.2	-8.4	-6.0	-14.3	75	62	71	69	0.5	1.3	1.1	1.0	3 ⊙	6 ⊙	10	NW 3	SE 3	E 4
18	78.4	73.9	75.3	75.9	-2.5	4.2	4.5	2.7	5.7	-6.9	87	98	92	92	0.7	0.1	0.7	0.5	10 ●	10	9	SE 5	SW 4	SW 4
19	85.7	91.2	93.8	90.2	-1.5	0.0	-1.9	-1.3	4.6	-2.3	86	73	79	79	0.8	1.7	1.1	1.2	10	9	10	WNW 9	WNW 7	N 2
20	97.8	98.9	93.0	96.6	-3.1	1.4	0.0	-0.4	1.7	-3.5	79	72	82	78	1.0	1.9	1.1	1.3	10	6 ⊙	10	NE 3	E 5	SSE 7
21	86.6	91.3	93.6	90.5	3.3	10.8	5.9	6.5	12.2	-0.5	91	64	71	75	0.6	4.6	2.7	2.6	9	7	0	SSW 3	WSW 9	WSW 3
22	94.0	96.2	98.7	96.3	3.7	8.6	4.2	5.2	8.8	1.3	78	63	75	72	1.8	4.2	2.0	2.7	9	5	7	SW 3	WSW 9	SW 4
23	101.4	103.2	107.4	104.0	0.7	6.7	-0.2	1.8	7.3	-0.2	86	75	88	83	0.9	2.4	0.7	1.3	0	4	10	W 3	W 2	NNE 5
24	115.6	117.8	118.9	117.4	-4.8	0.8	-1.5	-1.8	2.5	-5.7	83	62	68	71	0.7	2.5	1.8	1.7	0	0	0	NE 3	E 7	E 6
25	119.0	117.3	116.5	117.6	-4.0	3.3	0.6	0.1	4.3	-4.7	73	56	63	64	1.2	3.3	2.4	2.3	8 ⊙	8 ⊙	0	SE 8	ESE 12	SE 12
26	114.1	113.7	111.9	113.2	-0.7	5.2	1.9	2.1	6.5	-1.8	71	51	62	61	1.7	4.3	2.7	2.9	4 ⊙	2 ⊙	0	SW 10	SSE 12	SSE 10
27	111.0	111.2	109.1	110.4	0.2	10.0	4.9	5.0	11.7	-0.7	76	55	72	68	1.5	5.6	2.5	3.2	0	0 ⊙	0	SSE 5	S 7	S 5
28	106.0	104.0	100.5	103.5	0.7	13.6	7.4	7.3	14.6	-0.6	85	50	61	65	1.0	7.8	4.0	4.3	0 ⊙	2 ⊙	0	S 3	S 4	S 2
29	99.2	99.0	100.8	99.7	0.9	11.4	6.3	6.2	13.0	-0.5	90	55	86	77	0.6	6.1	1.2	2.6	3 ⊙	9	0	C 0	SSW 2	W 1
30	103.1	104.0	105.7	104.3	0.3	15.8	7.9	8.0	17.0	-1.5	94	32	66	64	0.3	12.1	3.6	5.3	8	2	2	ESE 1	SE 2	SE 2
31	107.9	108.8	108.7	108.5	3.6	16.2	7.1	8.5	17.2	1.1	83	33	73	63	1.3	12.3	2.8	5.5	0 ⊙	0 ⊙	0	E 3	SE 3	C 0
M	101.6	102.1	101.5	101.7	-2.8	3.5	0.1	0.2	5.1	-4.7	84	65	76	75	0.8	3.3	1.6	1.9	6.1	5.6	4.7	3.3	5.2	3.9

Kwiecień – Avril

1	109.7	109.6	108.6	109.3	2.1	16.0	6.7	7.9	16.9	-0.8	91	40	81	71	0.6	11.0	1.9	4.5	0 ⊙	0	0	C 0	SE 3	E 2
2	108.1	107.2	107.0	107.4	2.3	16.8	7.0	8.3	17.1	-0.4	93	38	85	72	0.5	11.9	1.4	4.6	1 ⊙	0 ⊙	0	C 0	SE 3	S 2
3	109.1	110.2	111.4	110.2	1.3	16.4	9.2	9.0	18.2	-0.7	87	39	74	67	0.9	11.4	3.0	5.1	0	1	0	C 0	C 0	C 0
4	113.1	112.8	111.5	112.5	2.9	14.9	7.0	8.0	16.7	-0.7	95	50	75	73	0.4	8.5	2.4	3.8	0 ⊙	6 ⊙	0	C 0	WNW 2	WNW 1
5	111.2	109.1	103.8	108.0	3.5	15.4	8.0	8.7	17.4	-0.7	88	37	64	63	0.9	11.1	3.8	5.3	3 ⊙	2 ⊙	0	W 2	W 2	C 0
6	99.4	95.0	90.1	94.8	4.1	17.7	8.1	9.5	18.2	1.1	85	35	71	64	1.2	13.1	3.1	5.8	0	2 ⊙	0	C 0	SW 5	SW 1
7	89.9	92.3	96.6	92.9	6.3	9.0	3.1	5.4	9.9	2.7	95	63	84	81	0.4	4.2	1.2	1.9	10 ●	10	0	NNW 2	NNE 5	W 2
8	99.9	98.4	95.1	97.8	-0.3	3.9	1.5	1.6	4.9	-1.9	86	61	83	77	0.9	3.2	1.1	1.7	10	9	10 ✳	N 2	NW 5	W 4
9	92.8	93.4	93.7	93.3	0.3	2.3	-2.3	-0.5	3.5	-2.5	90	49	61	67	0.6	3.7	2.0	2.1	9	2 ⊙	0	W 7	NW 12	NW 3
10	93.1	90.1	83.6	88.9	-3.5	4.7	5.3	3.0	7.9	-6.0	85	34	65	61	0.7	5.6	3.2	3.2	4 ⊙	8	10	WSW 2	S 3	SSE 3
11	76.3	75.2	79.9	77.1	4.7	11.2	4.4	6.2	11.8	2.9	79	62	74	72	1.7	5.1	2.2	3.0	9	9	10	S 2	SW 3	SW 4
12	87.3	91.6	94.6	91.2	1.5	2.5	1.3	1.6	4.4	-0.4	85	67	83	78	1.0	2.4	1.1	1.5	10	10	10	NW 6	NW 5	W 1
13	96.2	96.6	97.5	96.8	-1.1	5.7	1.3	1.8	7.9	-3.5	94	51	68	71	0.3	4.6	2.1	2.3	4 ⊙	9	1	W 1	WNW 2	C 0
14	100.0	101.3	101.4	100.9	-0.3	3.3	-1.1	0.2	4.5	-1.8	90	56	81	76	0.6	3.3	1.1	1.7	9	8	2	WNW 1	W 4	C 0
15	102.0	102.0	103.3	102.4	-1.7	5.3	-0.5	0.6	5.7	-6.1	90	59	71	73	0.6	3.7	1.7	2.0	6	8	0	W 1	NW 3	NW 1
16	105.0	104.7	103.0	104.2	-1.5	4.5	5.1	3.3	7.1	-3.7	84	48	49	60	0.9	4.4	4.5	3.3	0 ⊙	6	10	WNW 2	W 3	S 4
17	100.6	101.7	102.8	101.7	4.9	7.6	5.9	6.1	9.3	2.7	95	91	92	93	0.5	0.9	0.7	0.7	10 ●	10 ●	10	SW 2	N 1	NE 1
18	102.2	99.3	97.5	99.7	1.1	2.3	1.6	1.6	6.1	0.3	94	96	96	95	0.4	0.3	0.3	0.3	10	10 ⛆	10 ⛆	N 2	NE 3	N 3
19	96.3	96.8	99.5	97.5	1.0	3.7	2.7	2.5	4.6	0.3	98	88	88	91	0.2	1.0	0.9	0.7	10 ⛆	10 ●	10	WNW 1	SW 2	SW 2
20	102.2	103.6	105.9	103.9	3.7	13.0	7.6	8.0	13.6	0.8	88	58	91	79	1.0	6.4	0.9	2.8	4	8	10 ●	SE 2	E 1	C 0
21	108.2	110.4	111.6	110.1	6.1	10.4	7.6	7.9	12.4	4.9	95	82	89	89	0.4	2.2	1.2	1.3	10 ▬	8	10	SW 1	SW 1	N 1
22	114.0	113.8	113.9	113.9	6.1	16.2	10.2	10.7	16.7	2.2	89	52	72	71	1.0	8.8	3.4	4.4	0 ⊙	6 ⊙	4	NW 1	NE 4	E 5
23	113.1	111.9	111.4	112.1	7.4	11.8	10.7	10.2	13.5	2.7	83	83	86	84	1.8	2.3	1.8	2.0	10	10	3	N 2	NE 3	NNW 2
24	110.1	109.0	107.0	108.7	7.0	19.4	13.8	13.5	19.8	4.9	94	42	61	66	0.6	13.0	6.2	6.6	8	9	1	C 0	NE 2	N 1
25	105.3	104.7	103.8	104.6	9.6	20.6	15.4	15.2	21.4	6.1	79	43	69	64	2.6	13.8	5.5	7.3	2	4 ⊙	8	NNE 1	NE 3	N 3
26	103.1	102.4	102.7	102.7	11.4	23.2	14.2	15.8	24.2	7.3	90	40	88	73	1.4	17.1	2.0	6.8	9	4	0	N 2	E 5	SW 2
27	102.5	101.8	100.2	101.5	13.0	23.8	17.4	17.9	25.6	8.2	73	37	60	57	4.1	18.7	8.1	10.3	4 ⊙	9	5	N 2	SW 2	SE 1
28	98.9	97.0	96.6	97.5	14.4	24.6	14.8	17.2	24.9	9.4	74	37	80	64	4.3	19.6	3.3	9.1	1	5 ⊙	10 ⛆	ESE 1	S 6	E 3
29	95.2	95.2	96.0	95.5	13.0	23.8	14.7	16.6	24.9	10.8	88	59	92	77	1.8	14.7	1.3	5.9	3	3	10 ●	SE 1	S 7	NW 2
30	95.8	93.8	90.0	93.2	13.8	24.2	17.0	18.0	25.6	9.7	89	52	68	70	1.8	14.5	6.2	7.5	0 ⊙	1 ⊙	10 ●	SW 3	S 4	SW 7
31																								
M	101.4	101.0	100.7	101.0	4.4	12.5	7.3	7.9	13.8	1.6	88	55	77	73	1.1	8.0	2.6	3.9	5.2	6.2	5.1	1.6	3.5	2.0

Białystok $H_s = 139\ m$ $H_b = 140.8\ m$ $h_w = 11\ m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	2	0.9	
2	7	0.0	2	.	✳° 16⁴⁵ 17¹⁰ – 23²⁰
3	7	0.0	2	6.3	✳° 6¹⁵ – 11¹⁵
4	7	3.0	2	4.2	✳° 21³⁰ – 24
5	7	0.2	4	3.1	✳° 0⁰⁰ – 1³⁰ , = 4³⁰ – 5²⁰
6	6	0.0	4	1.1	✳° 5¹⁵ – 9¹⁵ , 11⁰¹ – 16⁰⁵ , 16²⁰ – 17³⁰ , 19³⁰ – 20⁴⁰ , 21¹⁸ – 22³⁰
7	7	.	4	2.8	✳° 0¹⁸ – 4³⁰
8	7	.	2	1.0	
9	7	.	2	8.6	
10	8	.	2	8.6	⌴ 19⁰⁰ – 24
11	7	.	pł.	8.0	⌴ 0⁰⁰ – 9⁰⁰
12	7	.	pł.	1.9	⊕ ° 8¹⁵ – 35
13	6	.	pł.	1.8	= 6⁰⁵ – 13¹⁰ , ▽ 22²⁰ – 24
14	7	0.0	.	3.7	▽ 0⁰⁰ – 14⁰
15	7	10.1	.	0.6	• ° 1³⁰ – 5³⁵ , 7²⁰ – 9⁴⁰ ⁂° 10¹⁰⁻³⁰ • ° 15⁴⁰ – 18⁴⁵ ⁂° – 19⁰⁵ ✳¹ – 21³⁰ ✳° – 24 , ⩔ 0⁰⁰ – 4¹⁵
16	6	0.6	4	1.0	✳° 0⁰⁰⁻⁴⁰ , 2⁰⁵ – 3⁰¹ ✳¹ 7²⁰ – 8¹⁰ ✳° 8⁴⁰ – 9¹⁵ , 12¹⁰ – 14⁴⁵ ⁂° 15⁴⁵ – 17³⁵ , ⩔ 8¹⁰ – 10¹⁰
17	8	5.5	4	7.5	✳° 19³⁰ – 20¹⁰ ✳¹ 23¹⁰ – 24
18	6	2.7	6	.	✳¹ 0⁰⁰ – 4³⁰ ✳° – 5¹⁵ • ° – 9⁰² • ° 9¹⁰ – 11⁰¹ , 11¹⁰ – 12⁰⁵ • ¹ – 12¹⁵ • ° 21⁴⁰ – 22³⁵ , = 9⁰² – 10⁴⁵ , 12¹⁰ – 13²⁰
19	7	0.0	3	3.2	✳° 7³⁵ – 8²⁰ , ⩔ 2²⁰ – 5⁴⁰
20	8	1.5	2	0.9	⁂¹ 18¹⁵⁻⁴⁵ • ¹ 21¹⁵ – 22⁴⁰ (marznący) , ∞ 22²⁰ – 23²⁰
21	7	.	pł.	6.4	
22	7	0.1	.	6.1	• ° 15³⁰ .. 55
23	7	.	.	9.4	⌴ 1³⁰ – 8⁰⁰
24	8	.	.	10.5	
25	8	.	.	10.1	⩔ 8¹⁰ – 24
26	8	.	.	9.5	⩔ 0⁰⁰ – 24
27	8	.	.	9.8	⩔ 14⁰⁰ – 15²⁰
28	8	.	.	10.7	⌴ 2³⁰ – 7³⁰
29	7	.	.	6.1	
30	7	.	.	8.8	= 1⁴⁰ – 7¹⁵ , ⌴ 4¹⁵ – 7³⁰
31	8	.	.	11.1	⌴ 3⁰⁰ – 7⁰⁰
Σ	—	23.7	—	163.7	UWAGI.

Kwiecień – Avril

1	8	.	.	11.0	⌴ 1⁰⁰ – 8⁰⁰
2	8	.	.	10.8	⌴ 1¹⁰ – 7⁰⁰
3	7	.	.	10.8	⌴ ° 5¹⁵ – 7¹⁰
4	7	.	.	10.6	⌴ 0³⁰ – 6⁴⁰
5	8	.	.	11.2	⌴ 0⁰⁰ – 7¹⁰
6	8	0.0	.	11.7	
7	7	1.2	.	0.5	• ° 6¹⁰ – 7⁴⁵ , = 0³⁰ – 5¹⁰
8	8	0.4	.	1.7	✳° 20¹⁵ – 23⁰⁶
9	8	0.0	.	8.4	⁂ 8²⁰ – 9⁰⁷ , ⩔ 10¹⁵ – 13⁴⁰ , ⌴ ° 2⁰⁰ – 7⁴⁰
10	8	.	.	9.8	
11	7	.	.	1.6	
12	7	.	.	1.4	⌴ 23⁰⁰ – 24
13	8	0.8	.	6.8	⌴ 0⁰⁰ – 7⁰⁰
14	8	0.0	1	6.7	✳° 1¹⁰ – 4³⁰ ⁂ 16⁰⁴ – 16 , 10¹⁰⁻³⁰ , ⌴ 21³⁰ – 24
15	8	0.0	.	4.9	⌴ ° 0⁰⁰ – 8²⁰
16	8	1.8	pł.	9.4	✳° 0⁴⁴ – 1⁰² ⁂ – 3³⁵ , ⁂ 23⁰⁵⁻⁵⁰ • ° – 24 , (≤) 20¹⁵ – 23¹⁰
17	7	2.9	.	0.3	• ° 0⁰⁰ – 8³⁰ ⁂ 12¹⁵⁻³⁰ 15⁴⁵ – 17⁵⁰ 18⁴⁸ – 19²⁵
18	6	4.8	.	.	• ° 0⁰⁰ – 6⁰⁵ ⁂° – 6²⁰ 7⁴⁵ – 10¹⁵ • ° – 10⁵⁰ ⁂° – 13⁰⁵ • ° – 15⁴⁰ 17²⁷ – 19³² ⁂° – 21⁴⁰ • ° 23⁴⁰ – 24
19	7	0.3	.	.	• ° 0⁰⁰⁻¹⁰ ⁂° – 8³⁵ • ° 11⁵⁰ ⁂ 12²⁰ – 13⁴⁰ • ° 16¹⁰ 20¹⁵ , 21³⁵ , 23⁴⁰
20	7	2.0	.	6.4	• ° 15⁵⁰ – 19³⁰ 20⁰⁵ – 24 , ⌓ ° n – a
21	7	0.1	.	2.0	• ° 0⁰⁰ – 2³⁰ , 3⁰⁹ – 4³⁵ , 11³⁰ .. 12⁰⁷ , = 2³⁰ – 3⁰⁹ ≡ ° 5⁴⁰ – 9³² = – 11³⁰
22	8	.	.	6.6	⌓ n – 7¹⁰
23	7	.	.	.	⌓ 20⁰⁰ – 24
24	8	.	.	4.8	⌓ 0⁰⁰ – 6¹⁰
25	7	.	.	10.4	⌴ ° 3³⁰ – 7³⁰
26	7	.	.	8.7	∞ 18¹⁰ – 21⁰³ , ⌓ n – 7⁴⁰ , 19⁰⁰ – 24
27	8	1.0	.	9.0	⁂¹ 12³⁵ – 13⁴⁰ , 14⁵⁰ – 15⁰⁵ , ⌓ 0⁰⁰ – 9¹⁵
28	7	10.2	.	3.5	⁂ 19⁰⁶ – 20²⁰ 21¹⁰ – 22²⁵ , 23¹⁵ – 24 , (K) 15⁴³ – 17⁵⁰ 18⁴⁵ – 19⁰⁰ K 19⁰⁸ – 19⁴⁰ – 22³⁰ S – N
29	8	6.1	.	10.4	⁂ 0⁰⁰ – 1⁰⁸ , 17¹⁵ – 18²⁰ , n – n , K 17¹⁵ – 20⁴⁵ – 21¹⁰ S – N
30	8	4.0	.	10.7	⁂¹ 17⁴⁵ – 18³⁵ ⁂° 19⁴⁵ – 20³⁰ , 20⁴⁰ – 23³⁰ , K ° 7⁴⁵ – 18³⁵
31					
Σ	—	35.6	—	195.5	UWAGI.

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ **Maj – Mai 1957**

DNI	CIŚNIENIE P – 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	97.1	100.0	102.2	99.8	5.2	9.4	6.3	6.8	17.0	3.3	78	54	52	61	1.9	5.4	4.5	3.9	9	6 ⊙	0	W 4	NW 6	NNW 3
2	103.3	101.1	98.6	101.0	4.5	11.0	6.3	7.0	12.5	-1.3	70	45	75	63	2.5	7.1	2.4	4.0	2	7 ⊙	6	NE 3	NE 5	NE 2
3	96.8	94.7	92.4	94.6	6.1	11.6	8.9	8.9	13.4	3.3	79	58	80	72	2.0	5.7	2.3	3.3	8	8	9	S 3	N 1	S 1
4	86.8	89.1	92.1	90.0	7.2	9.4	5.1	6.7	13.3	4.1	66	69	67	74	1.5	3.7	2.9	2.7	10	10	0	SW 2	WSW 8	SW 3
5	92.4	93.1	93.7	93.1	3.8	8.2	2.3	4.2	9.5	0.5	70	47	84	67	2.4	5.8	1.2	3.1	1 ⊙	8	2	SW 8	SW 8	SW 1
6	95.1	93.9	91.3	93.4	2.7	7.0	3.9	4.4	9.3	-2.3	77	63	95	78	1.7	3.7	0.4	1.9	10	10 •	10	ESE 1	N 5	N 2
7	91.5	91.6	89.4	90.8	3.5	5.4	5.9	5.2	6.4	2.3	91	87	92	90	0.6	1.2	0.7	0.8	10	10	10 •	SW 1	NW 1	NW 2
8	85.1	85.7	89.1	86.6	5.9	9.8	7.0	7.4	12.2	4.9	100	87	97	95	0.0	1.6	0.3	0.6	10 ≡	10	10	NNW 5	WNW 5	WNW 4
9	92.3	92.2	91.0	91.8	6.1	13.0	13.2	11.4	17.0	5.1	98	81	88	89	0.1	2.8	1.8	1.6	10	10	4	NNW 2	N 3	NW 1
10	89.5	90.9	94.2	91.5	13.0	16.0	10.2	12.4	16.9	8.3	86	65	93	81	2.1	6.3	0.8	3.1	9	8	10	N 2	E 9	ENE 2
11	96.7	100.4	101.4	99.5	8.9	10.2	9.8	9.7	11.2	8.0	97	87	92	92	0.3	1.6	0.9	0.9	10 •	10	10	S 8	S 5	SSW 1
12	102.0	102.1	102.3	102.1	10.2	17.8	11.4	12.7	19.8	4.5	95	50	85	77	0.6	10.3	2.0	4.3	1	8	0	SSW 1	S 5	C 0
13	103.0	102.3	100.9	102.1	12.0	22.4	15.2	16.2	23.1	5.3	83	36	72	64	2.3	17.4	4.8	8.2	0 ⊙	4 ⊙	0	C 0	SSW 2	C 0
14	99.5	99.2	101.3	100.0	13.4	21.8	15.6	16.6	23.1	6.6	77	36	71	61	3.5	16.7	5.1	8.4	2 ⊙	9	3	C 0	W 2	NW 4
15	104.6	105.1	105.2	105.0	11.0	18.2	13.1	13.8	19.7	7.5	87	45	67	66	1.6	11.5	5.0	6.0	0	4	0	NW 1	W 7	NW 1
16	106.3	104.1	102.2	104.2	12.6	21.0	14.1	15.4	22.1	3.1	66	42	75	61	5.0	14.5	4.1	7.9	0 ⊙	0 ⊙	0	NE 2	E 3	C 0
17	102.0	100.7	99.7	100.8	15.0	20.2	14.0	15.8	22.3	8.7	63	48	91	67	6.2	12.3	1.5	6.7	1 ⊙	9 •	9	SE 3	ENE 4	NW 1
18	100.0	100.1	98.5	99.5	15.2	23.8	17.0	18.2	24.3	9.8	79	49	70	66	3.7	15.1	5.8	8.2	1	4 ⊙	3	NW 1	NW 2	NW 1
19	96.6	95.0	93.5	95.0	15.6	26.6	15.8	18.4	27.5	9.1	88	41	81	70	2.1	20.6	3.3	8.7	4 ⊙	4 ⊙	9	N 2	SSE 6	ESE 2
20	94.4	94.6	94.4	94.5	16.8	22.8	16.8	18.3	24.5	9.9	74	53	76	68	5.0	12.9	4.6	7.5	0 ⊙	2	2	ESE 2	SSW 4	S 1
21	95.1	96.2	97.5	96.3	17.2	19.2	12.4	15.3	19.8	11.0	82	74	93	83	3.5	5.8	1.0	3.4	9	8 ⊙	10	C 0	WNW 4	NW 5
22	96.8	96.8	95.9	96.5	9.8	16.2	15.3	14.2	19.7	8.2	95	79	88	87	0.6	3.8	2.1	2.2	10	10	6	NW 2	NNW 2	N 1
23	94.2	94.3	93.3	93.9	13.2	17.8	15.6	15.6	20.8	11.3	98	86	94	93	0.4	2.8	1.1	1.4	10 •	9	4	WNW 2	W 2	WNW 2
24	95.1	98.6	102.7	98.8	11.8	11.5	9.2	10.4	15.8	8.4	95	77	74	82	0.6	3.2	3.0	2.3	10	10	3	N 3	NNE 7	NNE 3
25	105.9	107.3	108.5	107.2	7.8	10.0	6.2	7.6	11.3	2.4	67	46	72	62	3.5	6.7	2.7	4.3	0 ⊙	10	10	NNE 4	NE 6	N 3
26	109.6	110.0	109.8	109.8	6.5	10.6	6.1	7.3	11.4	4.3	72	42	69	61	2.7	7.4	2.9	4.3	10	9	10	N 3	N 5	N 1
27	109.2	108.6	107.5	108.4	6.4	9.6	5.9	7.0	11.4	3.2	79	52	83	71	2.0	5.8	1.6	3.1	10	10	9	N 1	ENE 2	NNE 2
28	106.1	105.0	103.9	105.0	8.7	11.0	5.1	7.5	12.5	2.3	69	57	90	72	3.4	5.7	0.9	3.3	5 ⊙	9	3	NNE 3	NE 4	C 0
29	102.5	102.1	102.6	102.4	7.0	11.8	8.0	8.7	13.2	-0.9	77	49	83	70	2.3	7.0	1.8	3.7	0 ⊙	9	10	N 1	WNW 3	WNW 2
30	103.6	104.7	104.2	104.2	7.2	11.3	8.0	8.6	15.2	6.5	94	74	79	82	0.6	3.4	2.2	2.1	10	7	0	WNW 3	W 3	NW 3
31	104.7	103.0	100.1	102.6	9.7	18.2	12.2	13.1	20.7	0.1	74	38	71	61	3.1	13.0	4.2	6.8	2	4 ⊙	0	W 3	WNW 3	C 0
M	98.7	98.8	98.7	98.7	9.5	14.6	10.2	11.1	16.7	5.1	82	59	81	74	2.2	7.8	2.5	4.2	5.6	7.6	5.2	2.5	4.3	1.7

Czerwiec – Juin

1	98.4	97.2	95.8	97.1	12.6	22.4	16.4	17.0	22.5	6.3	70	41	64	58	4.4	15.9	6.7	9.0	9	8	10	SW 3	SW 5	WNW 3
2	98.1	99.7	102.0	99.9	11.8	15.8	12.4	13.1	17.1	9.3	83	70	74	76	2.3	5.3	3.7	3.8	10	10	2	W 3	W 6	W 3
3	104.7	103.6	100.8	103.0	12.3	20.0	15.4	15.8	23.3	6.2	89	53	83	75	1.5	11.1	3.0	5.2	10	3 ⊙	6	SW 3	WSW 4	SW 1
4	97.7	95.5	93.1	95.4	18.0	25.8	16.2	19.0	26.1	10.4	71	46	96	71	5.9	17.9	0.8	8.2	10	9	10	SSW 2	S 3	C 0
5	86.5	85.1	88.2	87.3	14.8	16.8	12.4	14.1	17.7	11.9	93	93	90	92	1.1	1.4	1.4	1.3	10 •	10	9	C 0	NW 1	WSW 2
6	88.3	89.8	93.8	90.6	12.3	17.3	10.8	12.8	17.8	8.7	92	66	81	80	1.2	6.7	2.5	3.5	9	6 ⊙	2	SW 2	SW 3	WSW 2
7	95.8	95.8	94.0	95.2	13.2	20.0	17.0	16.8	21.8	7.6	68	42	72	61	4.8	13.6	5.4	7.9	0 ⊙	8	9	S 5	S 7	SSW 2
8	97.1	99.0	99.0	98.4	12.4	19.4	15.8	15.8	21.8	9.5	94	67	89	83	0.9	7.4	1.9	3.4	10	6	1	NNW 1	E 2	C 0
9	99.0	97.9	96.1	97.7	16.9	26.7	20.7	21.2	27.4	10.2	85	47	70	67	2.9	18.7	7.4	9.7	1 ⊙	4 ⊙	6	ESE 2	SE 5	SE 3
10	97.2	97.9	98.0	97.7	18.7	23.4	19.2	20.1	25.5	15.8	79	64	82	75	4.6	10.3	4.0	6.3	8	10 •	7	SSE 3	S 4	C 0
11	98.4	97.6	97.2	97.7	18.6	28.2	23.6	23.5	29.6	13.4	84	53	67	68	3.5	18.1	9.5	10.4	3 ⊙	8 ⊙	7	SE 2	SE 6	SE 3
12	100.0	102.5	109.1	103.9	22.2	30.2	16.1	21.2	30.5	15.6	78	49	84	70	5.8	22.0	2.9	10.2	7 ⊙	9	8	S 2	WNW 4	NW 4
13	111.9	111.4	110.9	111.4	12.4	17.4	12.8	13.8	18.0	9.4	74	60	83	72	3.7	8.1	2.6	4.8	3 ⊙	3 ⊙	10	NW 7	W 5	W 5
14	110.0	108.9	110.3	109.7	12.1	21.2	15.8	16.2	22.5	6.6	77	41	54	57	3.2	14.9	8.3	8.8	1 ⊙	0 ⊙	1	NW 4	NW 6	NNW 2
15	111.8	111.2	108.9	110.6	13.2	20.8	15.5	16.2	22.3	7.5	66	46	67	60	5.1	13.3	5.8	8.1	2 ⊙	2 ⊙	2	N 2	NNW 4	NW 3
16	107.9	105.5	104.0	105.8	13.6	24.0	17.6	18.2	25.2	8.3	81	45	65	64	3.0	16.4	7.0	8.8	5 ⊙	6 ⊙	1	WNW 3	N 4	NW 2
17	104.0	103.6	102.3	103.3	15.0	22.2	16.2	17.4	23.6	7.1	64	40	65	56	6.0	16.2	6.5	9.6	0 ⊙	0 ⊙	1	NNW 2	NNW 4	NNW 2
18	102.4	100.0	97.1	99.8	16.5	24.9	17.6	19.2	26.9	6.9	70	33	67	57	5.7	21.2	6.6	11.2	3 ⊙	3 ⊙	0	WSW 2	WSW 6	W 1
19	94.7	92.9	93.0	93.5	19.9	27.1	19.0	21.2	29.1	8.8	57	37	65	53	10.0	22.4	7.8	13.4	0 ⊙	4 ⊙	2	SW 1	WSW 2	NNE 2
20	96.9	98.0	99.7	98.2	14.6	20.6	13.9	15.8	21.9	9.4	54	38	56	49	7.7	15.1	7.1	10.0	8 ⊙	3 ⊙	1	N 3	N 4	NW 3
21	103.2	101.7	98.9	101.3	10.2	17.5	12.8	13.3	20.1	5.4	76	28	67	57	3.0	14.3	4.9	7.4	0 ⊙	0 ⊙	0	N 3	W 4	C 0
22	94.2	90.8	86.4	90.5	16.7	25.4	19.2	20.1	27.0	9.2	49	54	87	63	9.7	14.9	2.9	9.2	8	6 ⊙	8	SE 6	SSW 6	S 3
23	89.1	92.7	94.4	92.1	17.8	20.5	16.3	17.7	22.6	16.2	88	67	82	79	2.4	7.9	3.2	4.5	10	9	4	WSW 3	WSW 6	WSW 1
24	93.3	92.5	89.6	91.8	18.1	23.0	14.0	17.3	23.9	11.3	79	62	95	79	4.5	10.6	0.7	5.3	6 ⊙	10	10	NW 2	W 3	NW 5
25	85.0	91.0	96.8	90.9	14.1	14.8	11.6	13.0	17.8	11.1	100	84	98	94	0.0	2.7	0.3	1.0	10	10	10 •	NE 3	SW 6	NW 5
26	100.2	101.9	103.3	101.8	11.0	16.0	12.3	12.9	18.5	7.8	92	59	72	74	1.0	7.5	4.0	4.2	10	9	2	W 3	W 4	W 3
27	105.2	104.7	107.0	105.6	12.4	17.7	12.6	13.8	18.8	5.4	72	47	77	65	4.0	8.7	3.4	5.4	1 ⊙	8 ⊙	2	W 3	W 6	WNW 2
28	107.3	104.9	101.6	104.6	13.4	17.0	18.1	16.6	20.2	5.7	68	62	93	74	5.0	7.4	1.5	4.6	8 ⊙	10	10	WSW 2	SW 7	W 3
29	102.8	104.1	103.8	103.6	17.8	22.7	19.2	19.7	25.5	13.9	91	69	76	79	1.8	8.6	5.2	5.2	10	8 ⊙	0	W 3	W 5	W 2
30	101.2	100.4	102.4	101.3	21.0	27.2	19.4	21.8	28.0	13.2	74	38	69	60	6.4	22.4	7.0	11.9	4 ⊙	3 ⊙	0	SW 4	W 6	NW 1
31																								
M	99.5	99.3	99.2	99.3	15.1	21.5	16.0	17.2	23.1	9.6	77	53	76	69	4.0	12.7	4.5	7.1	5.9	6.2	4.7	2.8	4.6	2.3

Białystok $H_s = 139\ m$ $H_b = 140{,}8\ m$ $h_w = 11\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	10.3	
2	8	.	.	12.3	⌴ $n - 7^{00}$
3	7	.	.	4.5	
4	7	.	.	4.0	≫ $15^{10} - 17^{40}$
5	8	.	.	10.8	
6	7	4.1	.	.	• $^0 11^{40} - 19^{35}$, ⌴ $^0 2^{05} - 5^{30}$
7	7	6.0	.	.	• $^0 7^{35} - 9^{35}$ • $^0 - 10^{20}$ $13^{04} - 14^{01}$ • $^0 15^{10} - 18^{25}$, $19^{10} - 23^{02}$
8	7	0.0	.	1.4	• $^0 0^{03} - 2^{35}$ • $^0 7^{15} - 9^{40}$, ≡ $^0 na - 7^{45}$ = $- 10^{30}$
9	7	0.0	.	4.1	• $^0 0^{15} - 5^{10}$ • $^0 8^{49}$ 9^{10} = $5^{10} - 8^{48}$
10	7	5.0	.	2.4	• $^0 8^{20} - 10^{35}$ ▽ $18^{40} - 19^{02}$ ⌓ $n - 8^{30}$
11	7	0.0	.	.	▽ $0^{00} - 2^{15}$, $3^{45} - 4^{01}$ • $^0 5^{08} - 8^{15}$ • $^0 - 9^{30}$
12	7	.	.	8.5	⌓ $^2 21^{00} - 24$
13	7	.	.	12.0	⌓ $^0 0^{00} - 7^{30}$ ⌓ $^1 20^{00} - 24$
14	8	0.0	.	7.9	• $^0 14^{05} - 15$, $14^{25} - 50$, (K) $^0 13^{25} - 14^{45}$, ⌓ $^2 0^{00} - 9^{05}$
15	7	.	.	12.9	
16	8	.	.	13.8	⌓ $^2 22^{00} - 24$
17	7	1.4	.	0.8	• $^0 12^{25}$, $15^{20} - 16^{20}$, ⌓ $^0 0^{00} - 7^{10}$
18	7	.	.	11.2	
19	8	0.0	.	7.8	▽ $15^{50} - 16^{05}$, (K) 15^{30-50} K $- 16^{05}$ (K) $- 17^{05}$
20	8	.	.	13.4	
21	7	.	.	2.2	
22	7	2.8	.	1.0	• ▽ $^1 17^{07-15}$
23	7	0.4	.	2.1	• $^0 0^{43} - 7^{35}$ • $^0 8^{30} - 11^{15}$ • ▽ $^0 16^{02-06}$ ▽ $^1 - 16^{15}$
24	7	.	.	2.4	• $^0 3^{15} - 6^{10}$
25	8	0.0	.	5.1	⌓ $^0 3^{00} - 8^{00}$
26	7	.	.	1.0	• ▽ $^0 1^{03} - 40$
27	7	0.0	.	1.2	• ▽ 13^{35-40}, 14^{05-15}, 14^{25-32}
28	8	.	.	3.4	
29	8	0.0	.	6.1	• $^0 20^{30}$ 21^{05}, ⌴ $0^{10} - 6^{00}$
30	8	.	.	6.9	• $^0 2^{40} - 4^{30}$, ⌓ $23^{00} - 24$
31	8	.	.	14.0	⌓ $^1 0^{00} - 2^{30}$ ⌴ $^0 - 5^{30}$
Σ	–	19.7	–	189.5	UWAGI

Czerwiec – Juin

1	8	9.0	.	5.3	
2	8	.	.	2.7	▽ $2^{30} - 5^{40}$, ⌓ $^0 22^{00} - 24$
3	8	.	.	9.7	⌓ $^0 0^{00} - 6^{00}$ $23^{10} - 24$
4	8	8.3	.	2.6	▽ $^0 18^{45} - 19^{30}$ ▽ $^1 - 20^{02}$ ▽ $^0 - 20^{30}$ • $^0 21^{30}$ $23^{30} - 24$, K $^0 18^{45} - 20^{30}$ ⌓ $0^{00} - 7^{10}$
5	7	5.2	.	.	• $^0 0^{00} - 1^{30}$ 2^{00-30} $4^{45} - 6^{20}$ $7^{20} - 10^{15}$, $17^{50} - 13^{10}$, = $2^{30} - 6^{20}$
6	7	1.4	.	6.2	• $^0 3^{25} - 4^{05}$ $4^{40} - 5^{10}$ ▽ $^1 14^{02-37}$, $15^{45} - 16^{10}$, $16^{45} - 17^{37}$
7	8	0.0	.	10.9	⌓ $^0 21^{00-10}$
8	7	0.4	.	6.2	• $^0 6^{40} - 7^{12}$, 8^{05-40} 9^{25}
9	8	0.0	.	13.3	≤ $22^{35} - 24$ SW – E, ⌓ $0^{00} - 8^{50}$
10	6	0.0	.	6.4	▽ $^0 0^{45} - 1^{00}$ • $^0 13^{05} - 14^{45}$, K $^0 0^{40} - 2^{35}$ SW – E, ≤ 0^{00-40}
11	8	.	.	10.9	
12	7	.	.	7.7	
13	8	.	.	11.1	
14	8	.	.	14.7	⌓ $^1 1^{00} - 8^{30}$
15	8	.	.	14.3	⌓ $^1 23^{00} - 24$
16	8	.	.	11.4	⌓ $^1 0^{00} - 8^{30}$, $23^{10} - 24$
17	8	.	.	15.4	⌓ $^1 0^{00} - 8^{10}$, $23^{00} - 24$
18	8	.	.	15.1	⌓ $^1 0^{00} - 8^{20}$
19	8	.	.	14.3	
20	8	.	.	13.1	⌓ $^0 22^{00} - 24$
21	8	.	.	15.5	⌓ $^0 0^{00} - 8^{20}$
22	7	1.0	.	5.5	▽ $^0 16^{03-16}$ $22^{03} - 23^{28}$, (K) $^0 21^{40} - 22^{03}$ S – NE K $^0 - 22^{50}$ S – NE
23	8	.	.	6.0	▽ $0^{30} - 2^{38}$ = $4^{10} - 7^{45}$
24	7	1.3	.	5.8	• $^0 14^{55} - 17^{25}$ • $^1 - 17^{40}$ ▽ $^0 17^{50} - 18^{20}$
25	7	0.4	.	1.2	▽ • $^0 2^{18-25}$ 3^{00-55} • $^0 - 4^{03}$, 8^{37} 10^{40}, 11^{37} 12^{02} ▽ $^0 19^{00-05}$ • $^0 19^{50} - 20^{40}$ • $^1 - 22^{50}$
26	8	.	.	4.5	⊕ $^0 9^{35} - 10^{40}$ ⊕ $^1 12^{30} - 13^{20}$
27	8	.	.	10.0	
28	8	0.0	.	1.4	▽ • $^0 20^{22-33}$
29	8	.	.	12.8	
30	8	.	.	7.8	⌓ $22^{10} - 24$
31					
Σ	–	18.0	–	261.8	UWAGI

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ **Lipiec – Juillet 1957**

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	104.8	105.0	104.0	104.6	17.0	23.8	18.5	19.4	25.7	11.8	86	40	60	62	2.0	17.7	8.5	9.7	7 ⊙	3 ⊙	2	N 2	NE 3	NE 2
2	103.5	100.5	98.0	100.7	18.6	25.8	17.9	20.0	27.4	12.6	65	43	99	69	7.4	18.8	0.2	8.8	9 ⊙	8	10	SE 5	SSE 5	NE 1
3	100.5	101.6	102.6	101.6	15.2	21.7	17.1	17.8	23.2	11.3	85	53	66	68	2.6	12.4	6.7	7.2	0 ⊙	4 ⊙	3	W 3	W 5	NW 3
4	103.7	102.1	99.6	101.8	14.6	23.0	19.8	19.3	25.4	7.1	86	45	64	65	2.4	15.5	8.3	8.7	8	10	2	SW 3	SSW 2	SSE 2
5	95.0	94.7	97.7	95.8	21.0	28.6	19.7	22.2	28.8	16.7	84	55	74	71	4.1	17.7	5.9	9.2	4 ⊙	5 ⊙	2	WSW 3	W 7	NW 2
6	100.4	101.6	102.4	101.5	15.8	21.8	17.2	18.0	23.5	11.5	79	46	61	62	3.7	14.1	7.6	8.5	4 ⊙	5 ⊙	0	W 6	WNW 7	WNW 2
7	105.2	105.5	105.4	105.4	15.2	23.8	16.9	18.2	24.8	8.2	78	43	69	63	3.9	16.7	5.9	8.8	0 ⊙	4	0	NW 2	NNE 3	N 1
8	105.4	101.7	98.4	101.8	16.4	26.8	22.0	22.3	29.2	8.8	56	41	68	55	9.4	20.7	8.5	12.9	9 ⊙	4 ⊙	10	S 2	S 4	C 0
9	96.0	95.2	93.8	95.0	21.6	25.4	17.8	20.6	28.2	16.2	82	47	85	71	4.6	17.2	3.0	8.3	3	9	9	SW 1	NW 5	WNW 4
10	97.1	96.0	95.3	96.1	16.3	22.9	17.8	18.7	25.4	11.0	76	50	75	67	4.3	14.0	5.2	7.8	0 ⊙	4 ⊙	1	W 1	NW 2	N 1
11	94.7	93.4	93.4	93.8	20.0	25.0	21.5	22.0	27.4	10.2	68	59	81	69	7.6	13.0	4.8	8.5	2 ⊙	9	10	NE 1	ENE 5	S 2
12	94.6	95.5	96.6	95.6	20.3	27.2	18.6	21.2	28.6	15.9	81	55	98	78	4.6	16.2	0.4	7.1	9	9	10 ●	E 5	E 5	NE 1
13	98.6	98.9	99.9	99.1	21.3	27.6	21.4	22.9	29.2	18.0	69	52	89	70	7.7	17.7	2.8	9.4	8	8	10	ESE 5	SE 3	NW 1
14	99.9	99.4	97.9	99.1	18.4	26.0	19.4	20.8	26.7	17.2	100	64	87	84	0.0	12.0	3.0	5.0	10	6	9 (R)	NW 1	W 2	N 2
15	96.0	95.2	94.8	95.3	19.9	23.0	20.4	20.9	25.7	15.6	85	70	87	81	3.4	8.4	3.2	5.0	9	10	6	NE 2	SW 2	C 0
16	93.4	90.3	89.5	91.1	19.7	27.0	18.4	20.9	29.2	14.7	90	51	90	77	2.4	17.3	2.1	7.3	6	9	10	C 0	E 3	C 0
17	87.6	88.7	89.5	88.6	17.4	19.7	15.7	17.1	21.2	15.4	98	66	86	83	0.4	7.7	2.4	3.5	10	9	8	ESE 2	SSE 7	SSE 3
18	89.4	89.8	89.1	89.4	14.8	16.3	15.8	15.7	17.3	12.3	98	95	99	97	0.3	1.0	0.1	0.5	10	10	10 ●	NW 1	NNW 1	W 4
19	90.5	91.7	92.7	91.6	14.5	20.4	16.8	17.1	24.7	13.6	88	65	86	80	2.0	8.5	2.7	4.4	10	9	1	SSW 5	W 4	WSW 1
20	93.7	93.2	91.4	92.8	18.2	26.8	20.4	21.4	28.2	10.4	77	46	78	67	4.9	19.0	5.3	9.7	0	5	3	S 1	SE 4	E 1
21	89.5	88.2	87.2	88.3	20.8	25.3	19.3	21.2	26.8	15.8	65	50	81	65	8.6	16.1	4.2	9.6	7 ⊙	8	9	E 4	E 7	E 1
22	86.8	86.8	86.6	86.7	16.6	18.2	15.3	16.4	19.6	14.1	94	86	96	92	1.2	2.9	0.8	1.6	7	10 ●	4	SE 2	SSE 2	S 2
23	86.8	86.5	84.7	86.0	14.4	23.0	18.8	18.8	24.9	10.7	98	58	81	79	0.4	11.9	4.1	5.5	10 ≡	4	1	NNW 1	W 4	W 1
24	84.9	85.4	89.4	86.6	17.4	21.8	15.8	17.7	22.1	15.6	100	77	100	92	0.0	5.9	0.0	2.0	10	7	10 ●	W 2	W 3	W 4
25	92.0	92.7	92.7	92.5	14.6	20.2	13.4	15.4	21.0	12.1	92	64	99	85	1.3	8.5	0.2	3.3	4 ⊙	9	1	W 2	W 4	SW 1
26	91.3	90.9	91.2	91.1	12.4	19.7	13.4	14.7	20.4	10.4	100	65	98	88	0.0	8.1	0.4	2.8	10 ●	7 ⊙	2	C 0	WSW 2	SW 2
27	88.0	88.5	87.0	87.8	14.2	16.9	15.1	15.3	20.3	11.4	99	84	96	93	0.2	3.1	0.8	1.4	10	10	10	SW 1	SW 5	SW 3
28	88.5	90.4	91.6	90.2	13.3	17.2	12.0	13.6	19.4	11.4	96	76	96	89	0.6	4.7	0.5	1.9	10	9	1	SW 3	S 4	SSW 2
29	94.0	94.5	97.0	95.2	13.0	21.0	14.0	15.5	22.0	8.1	89	55	94	79	1.6	11.3	0.9	4.6	0	8	7	SW 2	SW 4	C 0
30	98.3	98.3	98.8	98.5	14.5	21.8	15.8	17.0	22.3	8.3	89	57	94	80	1.8	11.1	1.1	4.7	6	6	9	S 2	SSW 5	SW 3
31	99.2	100.6	103.1	101.0	14.8	19.4	15.0	16.0	21.5	14.1	97	78	94	90	0.5	5.0	0.9	2.1	10 ●	9	3	SW 3	WSW 4	W 3
M	95.1	94.9	94.9	95.0	16.9	22.8	17.5	18.7	24.5	12.6	85	59	85	76	3.1	12.1	3.2	6.1	6.5	7.3	5.6	2.4	4.0	1.8

Sierpień – Août

1	104.4	104.5	102.8	103.9	14.8	21.1	18.2	18.1	23.9	13.8	92	68	84	81	1.3	7.9	3.3	4.2	10	8	2	W 2	WSW 5	WSW 2
2	102.5	101.3	101.2	101.7	16.0	20.0	13.4	15.7	22.1	12.3	81	49	85	72	3.4	12.0	2.3	5.9	8	7	3	W 3	W 7	W 4
3	101.3	100.0	100.0	100.4	12.7	14.4	14.4	14.0	19.4	8.9	94	97	86	92	0.9	0.6	2.4	1.3	2 ⊙	9	5	W 4	NW 4	W 1
4	99.6	100.4	101.6	100.5	13.4	17.6	16.0	15.8	21.5	11.8	98	78	87	88	0.4	4.4	2.3	2.4	10	10	10	W 3	W 4	W 3
5	102.4	103.5	103.6	103.2	15.2	19.9	17.2	17.4	23.6	13.7	89	76	86	84	1.9	5.5	2.8	3.4	6	8	3	WNW 4	NW 5	W 2
6	104.4	103.7	102.7	103.6	14.2	21.8	16.2	17.1	24.1	12.8	95	53	85	78	0.7	12.1	2.7	5.2	6	3	0	NW 3	NW 5	W 1
7	102.0	99.6	94.6	98.7	14.8	23.4	18.2	18.6	24.2	8.3	92	51	81	75	1.3	14.1	3.9	6.4	1	9 ⊙	10	C 0	SW 3	SW 2
8	89.8	90.3	93.1	91.1	15.4	21.0	16.2	17.2	22.3	13.6	98	68	86	84	0.4	7.9	2.5	3.6	10	8	9	C 0	W 3	NW 1
9	95.1	95.1	93.5	94.6	14.0	20.8	14.8	16.1	22.1	8.5	85	44	79	69	2.3	13.8	3.4	6.5	1	8	2	NE 1	SSW 1	C 0
10	90.8	86.7	87.2	88.2	15.2	23.2	16.2	17.7	23.7	10.6	69	55	96	73	5.3	12.7	0.8	6.3	1	10	5	ESE 3	ESE 7	SW 4
11	93.5	95.9	97.6	95.7	17.2	24.8	17.8	19.4	25.4	14.4	88	53	86	76	2.4	14.8	2.8	6.7	0 ⊙	3 ⊙	2	SW 3	WSW 6	SW 1
12	97.2	95.5	93.8	95.5	19.5	29.8	19.9	22.3	30.6	13.1	80	45	100	75	4.5	23.1	0.0	9.2	1 ⊙	0 ⊙	9 (R)	S 2	S 3	C 0
13	96.5	98.2	98.4	97.7	17.6	25.2	18.0	19.7	25.5	16.6	98	48	80	75	0.4	16.7	4.0	7.0	9	3 ⊙	1	W 1	W 5	W 1
14	97.7	97.7	93.2	96.2	16.8	22.0	19.2	19.3	23.1	11.3	92	81	92	88	1.6	5.1	1.7	2.8	10	10	9	C 0	NNE 5	NNE 1
15	88.4	89.6	92.6	90.2	18.8	20.6	16.4	18.0	21.7	16.2	95	71	90	85	1.1	6.9	1.9	3.3	9	9	0	S 4	SW 10	W 1
16	95.1	95.6	94.5	95.1	13.0	22.4	15.5	16.6	23.9	10.8	99	56	94	83	0.2	12.0	1.1	4.4	0	2	2	W 1	W 3	WNW 1
17	91.8	90.7	90.4	91.0	16.0	16.1	13.1	14.6	17.2	11.7	90	99	88	92	1.8	0.2	1.8	1.3	10	10 ●	10	C 0	SSW 1	SW 4
18	88.9	89.3	89.8	89.3	12.6	15.4	14.8	14.4	18.0	11.9	100	86	92	93	0.0	2.4	1.3	1.2	10 ●	10	8	SW 3	SW 5	SW 5
19	92.1	94.1	97.5	94.6	13.8	19.8	16.4	16.6	21.0	12.8	92	71	88	84	1.3	6.7	2.3	3.4	9	9	0	SW 5	SW 9	WSW 2
20	98.8	99.8	99.5	99.4	14.2	19.8	15.8	16.4	21.8	11.5	100	78	84	87	0.0	5.1	2.8	2.6	10	9	0	WSW 2	S 3	SW 1
21	98.4	97.3	95.9	97.2	14.8	19.8	16.3	16.8	21.7	11.4	94	76	99	90	0.9	5.5	0.2	2.2	2	10	10	SW 1	SW 2	C 0
22	90.5	90.7	91.6	90.9	15.4	15.2	13.5	14.4	16.6	13.0	100	90	93	94	0.0	1.7	1.1	0.9	10 ●	10	10	SSW 3	NW 3	W 2
23	92.8	92.8	95.4	93.7	11.6	17.4	10.8	12.6	18.0	10.4	95	52	86	78	0.6	9.7	1.8	4.0	6 ⊙	6	0	WSW 3	WNW 5	W 1
24	96.9	94.7	90.7	94.1	9.8	19.4	15.6	15.1	20.9	4.3	96	43	90	76	0.5	12.8	1.7	5.0	0	4	10 ●	C 0	SE 6	S 2
25	97.9	100.1	98.7	98.9	12.2	17.8	12.7	13.8	19.6	10.8	89	57	77	74	1.5	8.7	3.4	4.5	4	6 ⊙	0	SW 5	SW 5	SE 2
26	95.5	93.2	93.8	94.2	11.8	21.0	14.2	15.3	22.5	8.8	94	65	86	82	0.8	8.7	2.4	4.0	9	9	7	S 2	S 3	SW 1
27	95.2	97.5	98.4	97.0	10.8	16.0	11.3	12.4	17.2	7.7	94	64	93	84	0.9	6.5	1.0	2.8	1	7	4	SE 1	WSW 6	SW 1
28	98.2	98.1	98.0	98.1	11.2	17.2	13.6	13.9	18.4	7.1	96	75	97	89	0.5	4.9	0.6	2.0	10	10	10	SSW 1	SSE 2	S 1
29	98.6	99.9	99.8	99.4	11.4	14.0	12.4	12.6	14.5	8.9	99	99	100	99	0.2	0.2	0.0	0.1	10 ●	10 ●	10 ●	C 0	C 0	W 1
30	98.3	98.4	99.1	98.6	11.6	14.8	11.6	12.4	16.6	11.0	100	86	94	93	0.0	2.4	0.8	1.1	10 ●	10	6	WNW 1	WNW 4	SW 3
31	101.1	101.9	101.0	101.3	10.8	16.6	11.2	12.4	17.5	8.8	99	63	91	84	0.2	7.0	1.2	2.8	9	8 ⊙	0	SW 3	SW 4	C 0
M	96.6	96.6	96.5	96.6	14.1	19.6	15.2	16.0	21.2	11.2	93	68	89	83	1.2	8.1	1.9	3.7	6.3	7.6	5.1	2.1	4.3	1.6

Białystok $H_s = 139\ m$ $H_b = 140{,}8\ m$ $h_w = 11\ m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	13.8	⌒ $0^{00}-8^{00}$
2	8	3.8	.	6.5	●² 18^{03-45} ●° 19^{45} · ☇° $18^{35}-19^{45}$ E-W
3	8	.	.	12.9	⌒ $22^{00}-24$
4	8	5.9	.	7.1	⌒ $0^{00}-8^{00}$ · ⊕° $7^{10}-9^{10}$
5	7	.	.	13.0	●¹ $3^{25}-4^{10}$ ●°– 5^{02} · (☇)¹ 3^{15-25} SSW ☇¹ – 4^{05} SSW–SE · ⌒° $22^{00}-24$
6	8	.	.	14.7	⌒° $0^{00}-9^{10}$
7	8	.	.	14.8	⌒° $23^{00}-24$
8	8	0.4	.	12.0	●° $21^{55}-22^{00}$ · ⌒° $0^{00}-8^{20}$
9	8	1.2	.	5.6	●° 0^{30-45}, 2^{10-30} ●° $15^{55}-18^{30}$
10	7	.	.	13.0	
11	8	1.6	.	7.3	●° 10^{50-52} 21^{00-15} 21^{44-50} ●¹ – 22^{05} · (☇)° 21^{30-50}
12	8	1.5	.	1.1	●° 19^{10-30}, $20^{05}-22^{00}$ (☇)° 19^{10-23} NW ☇° – 19^{30} NW (☇)° – 20^{20} · ⊕ $11^{50}-13^{00}$
13	8	2.1	.	3.8	
14	8	1.7	.	6.1	●¹ $3^{15}-4^{10}$ ●° $4^{55}-5^{40}$ ●¹ $19^{56}-20^{10}$ ●°– 20^{23}, $20^{50}-21^{10}$ · (☇)° 14^{13-20}, 19^{56-58} SE ☇° $20^{25}-21^{00}$ W-N (☇)° – 22^{40} NW-N
15	7	0.0	.	2.8	●° $13^{50}-14^{40}$ · ⌒ $21^{00}-24$ · ⊕ $11^{30}-12^{30}$ ∪ 23^{00-35}
16	8	0.0	.	5.2	●° 17^{05-08}, 17^{30-35}, 17^{55-58}, 19^{08-10} · = $4^{40}-5^{30}$ · ⌒ $0^{00}-7^{00}$ · ∪° $0^{20}-3^{15}$
17	8	.	.	2.1	
18	7	6.2	.	.	●° $8^{20}-13^{20}$, 13^{45-50}, 14^{05-40}, $15^{05}-20^{45}$, $21^{05}-22^{35}$, $23^{00}-24$ · = $4^{40}-8^{20}$
19	8	.	.	6.2	●° 0^{00-30}
20	8	.	.	10.9	⌒ $2^{02}-8^{85}$
21	8	.	.	3.5	
22	6	0.6	.	1.9	●° $8^{40}-9^{06}$, $9^{35...38}$, $12^{05...10}$, 13^{27}, 15^{15}, 15^{40}, 16^{40} · = $22^{30}-24$
23	8	0.0	.	11.7	= $0^{00}-1^{40}$ ≡° 5^{40} ≡¹ – 6^{50} ≡° – 7^{45} = – 8^{40}
24	7	2.2	.	1.8	●° $6^{30}-7^{20}$ ●° 12^{25-30}, 15^{05-15}, $16^{40}-17^{40}$, 18^{30-45}, $20^{36}-23^{20}$ · (☇)° $14^{10}-15^{20}$ ENE
25	8	1.7	.	7.3	●° 0^{20-50} ●° 19^{15-25}
26	7	3.1	.	3.5	●° $6^{10}-8^{30}$ ●° $11^{46}-12^{02}$, $15^{53}-16^{01}$
27	7	4.1	.	1.0	●° $3^{18}-5^{43}$ ●¹ $17^{46}-18^{07}$ ●° $19^{38}-20^{32}$ · (☇)° 17^{45-46}
28	7	1.2	.	2.2	●² 15^{25-42}
29	8	.	.	9.7	= $2^{00}-3^{45}$
30	8	1.4	.	5.2	●° 15^{40-46}, 16^{47} 17^{40} 19^{25-36} 20^{18-21} · (☇)° 15^{05-40}, $16^{32}-17^{10}$ · = $4^{05}-7^{15}$
31	7	0.3	.	3.1	●¹ 7^{22-50} ●° 11^{20-25}, 13^{00-06}, $16^{40}-17^{00}$
Σ	–	39.0	–	209.8	UWAGI:

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1	7	.	.	6.7	
2	8	1.0	.	8.8	●¹ $16^{45}-17^{06}$ ●° $17^{49}-18^{25}$ 19^{40-52}
3	7	1.9	.	6.8	●² 11^{02-15} ●° $11^{45}-12^{00}$ 13^{12-18} ●¹ – 13^{22} ●°– 13^{25}, 13^{30-45}
4	7	(0.0)	.	3.7	●° $6^{30...40}$, $7^{28...35}$ · (☇)° 16^{25-40} SW-SE
5	8	.	.	8.4	
6	8	.	.	11.1	
7	8	0.0	.	9.5	
8	7	6.9	.	2.8	●° $1^{35}-2^{30}$ ●° $16^{40}-17^{00}$, $18^{15}-19^{15}$
9	8	.	.	11.2	
10	8	2.8	.	5.3	●¹ 16^{25-39} ●° 17^{15-47}
11	7	.	.	12.3	
12	8	0.9	.	10.2	●° 19^{15-18} ●¹ 19^{23} ●° $19^{35}-20^{10}$ · ☇° $19^{35}-20^{25}$ (☇)° -20^{40}, $20^{50}-21^{40}$ · ⌒ na
13	8	.	.	9.3	
14	7	19.4	.	1.5	●° 9^{15-55}
15	7	.	.	6.9	●° $0^{20}-2^{40}$ · ☇° $0^{15}-2^{40}$ · = $4^{40}-6^{30}$, $23^{30}-24$
16	7	.	.	10.9	= $0^{00}-5^{30}$ ≡° 6^{45} = – 7^{55}, $22^{30}-24$
17	6	42.5	.	1.6	●° 9^{15-40} ●¹ $9^{57}-17^{30}$ · = $0^{00}-2^{30}$
18	7	5.1	.	.	●° 0^{43} $2^{10}-3^{10}$ ●¹ – 11^{45}
19	7	.	.	5.5	⌒² $22^{15}-24$
20	7	0.0	.	4.7	●° $10^{45}-11^{10}$ · = $4^{05}-9^{30}$ · ⌒² $0^{00}-8^{15}$
21	7	0.4	.	1.8	= $2^{10}-24$ · ⌒ n – 10^{15}
22	7	6.5	.	.	●° $6^{26}-9^{15}$, $11^{05}-12^{25}$, $14^{45}-16^{25}$ · = $0^{00}-9^{00}$
23	8	.	.	10.1	●¹ $0^{00}-0^{15}-3^{15}$ ●°– 5^{35}
24	8	3.9	.	9.0	●° 21^{18-50}, $22^{15}-24$ · ⌒ n – 8^{10}
25	8	.	.	10.5	●° 0^{00-05}
26	8	3.5	.	5.3	●° $15^{45}-16^{00}$ ●¹ – 16^{05} ●°– 16^{10} · ☇° 16^{05-40}
27	7	.	.	7.9	⌒¹ $20^{00}-24$
28	7	1.0	.	1.3	●° 12^{05-40}, $15^{20}-16^{05}$
29	6	21.9	.	.	●° $6^{35}-9^{10}$, $10^{40}-20^{38}$, $21^{10}-24$ · ≡° $3^{30}-5^{15}$ = – 9^{30} · ⌒ n – 6^{35}
30	7	0.6	.	0.8	●° $0^{00}-12^{10}$, $14^{13...45}$ ●° 16^{03-09}, = $6^{05}-13^{20}$
31	7	5.7	.	4.8	
Σ	–	124.0	–	188.7	UWAGI:

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P−900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	98.0	98.1	99.3	98.5	11.2	13.2	9.6	10.9	14.9	8.6	97	74	96	89	0.3	4.0	0.5	1.6	10 ●	8 ⊙	7	SSW 3	SW 6	SW 2
2	102.6	102.4	101.5	102.2	9.6	17.4	10.4	12.0	18.7	6.6	99	58	96	84	0.2	8.4	0.5	3.0	2 ⊙	8	4	SW 3	SSW 3	WSW 2
3	98.8	98.1	99.1	98.7	12.3	20.8	11.8	14.2	21.2	8.9	88	63	99	83	1.7	9.0	0.1	3.6	7	8	7	SE 2	SE 3	W 1
4	101.6	103.2	104.2	103.0	11.0	15.2	12.8	13.0	16.4	7.4	99	85	94	93	0.1	2.6	0.9	1.2	10	10	10	NW 1	NW 1	C 0
5	105.3	104.7	103.5	104.5	11.2	17.8	10.0	12.2	19.2	9.5	100	57	96	84	0.0	8.7	0.5	3.1	6	7	3	C 0	W 1	WSW 1
6	101.5	101.4	102.4	101.8	13.3	18.0	11.8	13.7	19.4	8.7	91	74	94	86	1.4	5.4	0.8	2.5	10	10	9	SSW 2	SW 4	C 0
7	105.0	105.4	105.3	105.2	9.8	19.8	12.4	13.6	20.6	6.4	96	61	98	85	0.5	9.1	0.4	3.3	0	8	0	C 0	W 1	C 0
8	106.4	107.1	106.1	106.5	12.4	22.2	16.8	17.0	23.1	8.9	87	51	84	74	1.9	13.2	3.1	6.1	0	2	3	S 2	SSE 4	SSE 2
9	105.9	105.3	103.1	104.8	14.2	26.1	17.6	18.9	27.0	12.3	99	53	94	82	0.2	15.7	1.2	5.7	0 ⊙	0 ⊙	0	SSE 1	S 5	C 0
10	104.4	103.4	102.2	103.3	14.6	14.8	12.8	13.8	17.7	12.5	94	88	95	92	0.9	2.0	0.7	1.2	10	10	10	NW 5	NNW 2	W 3
11	99.3	95.6	91.7	95.5	9.8	17.2	12.4	13.0	18.4	9.1	99	62	85	82	0.1	7.4	2.2	3.2	9	9	0	W 1	SSW 2	SSE 3
12	82.9	79.8	85.0	82.6	13.8	20.0	13.8	15.4	21.6	11.5	95	76	70	80	0.7	5.6	4.7	3.7	10	10	10	SSE 3	S 6	SW 7
13	89.2	91.3	90.3	90.3	9.6	14.8	10.2	11.2	16.7	6.9	80	51	86	72	2.4	8.2	1.7	4.1	0 ⊙	9	4	SW 5	SSW 7	S 2
14	88.4	90.3	91.9	90.2	11.0	13.8	8.8	10.6	15.8	8.1	79	62	85	75	2.7	6.1	1.7	3.5	10	8	2	SSW 3	SSW 3	SSW 1
15	87.7	82.4	91.3	87.1	8.4	11.4	10.0	10.0	13.6	4.9	99	91	93	94	0.1	1.2	0.8	0.7	10 ●	10 ●	10	NE 1	SSW 8	SW 12
16	97.0	99.0	101.1	99.0	8.0	14.8	7.6	9.5	14.9	6.2	90	61	94	82	1.0	6.5	0.6	2.7	5	5	0	SW 5	SW 5	SW 1
17	100.3	97.7	94.4	97.5	3.0	13.8	7.8	8.1	14.8	1.2	100	56	90	82	0.0	7.0	1.1	2.7	9	10	9	C 0	WNW 1	W 1
18	87.7	84.5	82.1	84.8	6.7	8.2	9.2	8.3	12.2	6.3	100	99	99	99	0.0	0.2	0.1	0.1	10 ●	10 ●	10 ●	W 5	WSW 7	W 10
19	85.2	88.4	88.9	87.5	8.2	10.6	9.0	9.2	11.4	6.3	99	84	89	91	0.2	2.1	1.3	1.2	10 ●	10	10	WSW 10	WSW 7	W 1
20	88.0	90.8	94.5	91.1	8.3	11.2	9.6	9.7	12.8	7.6	99	86	96	94	0.2	1.8	0.5	0.8	10	10	9	WSW 3	W 5	W 1
21	97.3	98.8	99.0	98.4	8.2	13.8	7.8	9.4	14.2	7.1	96	62	87	82	0.5	6.1	1.4	2.7	10	10	5	SW 2	W 2	W 2
22	98.9	96.1	93.2	96.1	7.0	9.8	11.2	9.8	11.4	4.1	98	97	99	98	0.1	0.3	0.2	0.2	10	10 ●	10	C 0	SE 3	SW 2
23	90.1	86.6	77.7	84.8	13.8	19.0	15.2	15.8	19.4	10.7	99	83	100	94	0.2	3.8	0.0	1.3	10 ●	10	10 ●	S 4	S 4	S 5
24	81.2	84.4	83.2	82.9	11.6	12.8	8.2	10.2	15.8	7.7	94	65	89	83	0.8	5.2	1.2	2.4	10	8	0	W 5	W 8	WSW 6
25	83.6	89.7	96.0	89.8	5.9	7.9	6.0	6.4	8.5	4.9	89	80	97	89	1.0	2.0	0.3	1.1	10	10	10 ●	SSW 10	SSW 12	W 6
26	97.1	96.7	98.5	97.4	4.2	7.6	3.3	4.6	9.1	3.2	98	82	93	91	0.1	1.9	0.5	0.8	9	8	0	W 3	W 3	W 1
27	98.7	96.6	88.0	94.4	3.5	7.8	5.7	5.7	8.3	0.7	83	75	94	84	1.3	2.7	0.6	1.5	10	10	10 ●	SW 3	WSW 7	SW 9
28	77.3	78.5	80.5	78.8	8.2	11.0	8.0	8.8	12.2	5.1	93	77	87	86	0.8	3.1	1.3	1.7	10	10	8	WSW 8	WSW 10	WSW 5
29	84.0	85.0	81.9	83.6	7.0	11.3	7.6	8.4	11.8	4.6	90	69	99	86	1.0	4.2	0.1	1.8	10	8	10 ●	SW 5	SW 6	SW 2
30	81.0	84.3	89.6	85.0	6.7	6.3	6.5	6.5	7.9	5.5	100	100	94	98	0.0	0.0	0.6	0.2	10 ●	10 ●	10	W 3	W 3	W 3
31																								
M	94.1	94.2	93.8	94.0	9.4	14.3	10.1	11.0	15.6	7.0	94	73	92	86	0.7	5.1	1.0	2.3	7.9	8.5	6.3	3.3	4.6	3.0

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1	96.9	97.9	99.3	98.0	3.1	9.2	5.3	5.7	10.6	2.5	100	66	95	87	0.0	3.9	0.4	1.4	9	8	10 ●	W 5	SW 8	W 3
2	103.1	104.2	105.7	104.3	3.5	9.2	4.3	5.3	10.1	2.8	100	70	95	88	0.0	3.5	0.4	1.3	10	6	9	W 3	W 4	SW 2
3	103.1	98.9	92.9	98.3	1.1	9.6	7.8	6.6	9.7	-0.4	98	63	76	79	0.1	4.5	2.5	2.4	7	9	10	SSW 2	S 4	S 6
4	90.3	91.6	96.8	92.9	6.1	8.8	4.5	6.0	9.1	4.1	82	78	87	82	1.7	2.4	1.1	1.7	10	7	10	WSW 8	SW 8	W 2
5	101.4	102.3	102.1	101.9	2.5	8.3	6.3	5.8	8.7	1.5	95	73	78	82	0.4	3.0	2.1	1.8	1	10	10	W 2	SW 5	SW 4
6	98.2	99.5	103.0	100.2	5.7	9.0	9.7	8.5	10.8	5.1	98	96	99	98	0.2	0.5	0.1	0.3	10 ●	10	10	SW 4	SW 4	WSW 2
7	100.8	100.8	104.6	102.1	9.8	12.2	10.6	10.8	12.7	8.0	93	89	91	91	0.8	1.5	1.2	1.2	10	10	10	SW 9	W 9	WNW 3
8	110.7	114.6	114.6	113.3	2.8	11.4	5.3	6.2	12.0	1.4	100	52	98	83	0.0	6.5	0.1	2.2	0	2 ⊙	9	C 0	S 2	WSW 2
9	113.1	111.2	109.6	111.3	0.2	14.8	5.4	6.4	15.8	-0.5	100	57	98	85	0.0	7.2	0.2	2.5	2	2 ⊙	0	C 0	SSW 3	SW 2
10	108.4	107.6	106.9	107.6	2.7	16.6	5.9	7.8	17.7	1.0	91	53	95	80	0.6	8.9	0.5	3.3	1 ⊙	1	0	SSW 2	S 1	SSW 1
11	105.3	104.8	104.3	104.8	4.5	17.8	9.0	10.1	18.4	3.8	100	63	85	83	0.0	7.6	1.7	3.1	0	2	0	SW 1	SW 2	SW 1
12	104.7	101.5	106.2	104.1	4.6	16.1	11.0	10.7	16.5	3.6	100	67	96	88	0.0	6.0	0.5	2.2	0	8	9	SSW 1	SW 5	W 5
13	111.1	110.8	109.2	110.4	5.3	10.0	3.9	5.8	11.2	3.5	100	83	97	93	0.0	2.1	0.3	0.8	10 ═	9	0	WSW 1	SW 2	SW 1
14	105.5	104.5	106.8	105.6	6.2	11.4	9.5	9.2	12.4	3.6	98	95	87	93	0.2	0.7	1.6	0.8	7	10	10	SW 2	WSW 2	WNW 3
15	109.6	110.6	111.0	110.4	3.0	10.4	1.7	4.2	11.0	1.3	100	71	89	87	0.0	3.6	0.8	1.5	6	5	0	WSW 2	WNW 3	C 0
16	111.7	110.7	108.8	110.4	-1.0	9.0	5.5	4.8	9.5	-2.2	99	68	84	84	0.1	3.7	1.4	1.7	0	8	10	C 0	SSW 3	S 3
17	103.7	100.4	101.1	101.7	5.3	14.2	11.5	10.6	15.2	4.1	91	71	89	84	0.8	4.8	1.5	2.4	9	2 ⊙	10	SE 3	S 5	WSW 4
18	99.3	97.0	93.3	96.5	9.5	13.0	13.2	12.2	13.7	8.7	97	87	92	92	0.3	1.9	1.3	1.2	10	10	5	SW 3	SSW 5	SW 5
19	92.9	93.4	92.4	92.9	10.8	17.8	11.2	12.8	18.7	10.2	92	68	86	82	1.0	6.5	1.8	3.1	7	9	0	SSW 5	SSW 5	C 0
20	90.7	94.8	98.2	94.6	9.8	9.7	7.2	8.5	12.4	6.6	96	86	99	94	0.5	1.7	0.2	0.8	10	10	10 ●	WSW 1	NW 3	W 1
21	100.4	100.7	99.1	100.1	7.1	11.2	5.7	7.4	11.7	5.2	99	67	95	87	0.2	4.4	0.5	1.7	9	6	0	SW 1	SSW 3	S 2
22	95.7	92.8	90.7	93.1	5.3	6.6	7.0	6.5	7.9	3.2	89	96	94	93	1.0	0.4	0.6	0.7	10	10 ●	10	SE 4	SE 8	SE 5
23	90.5	92.0	94.9	92.5	7.0	7.8	7.4	7.4	8.3	6.3	98	97	97	97	0.1	0.3	0.3	0.2	10 ●	10 ●	7	SE 4	S 2	SW 2
24	95.5	94.8	99.8	96.7	3.8	6.5	8.3	6.7	8.5	3.3	98	84	87	90	0.1	1.6	1.4	1.0	9	10 ●	1	SSW 4	SW 5	WSW 7
25	104.3	106.8	108.4	106.5	3.4	8.9	3.7	4.9	9.8	2.7	93	72	92	86	0.5	3.2	0.7	1.5	2	7 ⊙	3	WSW 3	W 6	W 2
26	107.0	106.4	106.0	106.5	4.4	11.0	7.5	7.6	11.1	1.5	95	72	90	86	0.5	3.7	1.1	1.8	10	10	9	W 2	SW 4	SW 4
27	102.8	101.6	102.1	102.2	2.8	11.7	6.3	6.8	11.8	1.3	95	76	98	90	0.4	3.3	0.1	1.3	0	0	10	SSW 2	SW 5	SW 2
28	102.0	102.3	103.4	102.6	8.4	11.1	9.3	9.5	11.4	5.5	97	84	75	85	0.3	2.1	2.9	1.8	10	10	10	WSW 2	SW 3	SW 2
29	101.9	102.1	102.4	102.1	7.7	12.7	7.7	9.0	12.9	5.3	87	68	89	81	1.3	4.7	1.2	2.4	10	8	4	SSW 3	SW 7	SSW 2
30	101.0	98.9	97.7	99.2	5.3	13.7	8.5	9.0	14.4	4.7	94	66	90	83	0.6	5.4	1.1	2.4	6	2	2	S 3	S 5	S 2
31	96.5	96.0	94.1	95.5	9.3	12.3	9.7	10.2	13.4	7.1	93	87	89	90	0.8	1.9	1.2	1.3	10	10	10	SW 1	WSW 3	SW 3
M	101.9	101.7	102.1	101.9	5.2	11.4	7.4	7.8	12.2	3.7	96	75	91	87	0.4	3.6	1.0	1.7	6.6	7.1	6.4	2.7	4.3	2.7

Białystok $H_s = 139$ m $H_b = 140{,}8$ m $h_w = 11$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	8.4	.	2.8	●⁰ 3³⁶–9²⁰ ▽●⁰ 14⁴⁰–15⁰² ▽●¹ 15⁰⁷–³⁵ ▽●⁰ 16⁴⁰–18⁰⁵
2	7	.	.	9.9	⌒¹ 20⁰⁰–24
3	7	.	.	5.1	⌒¹ 0⁰⁰–8⁰⁰ ⌒ 20³⁰–24 ⊕ 9⁴⁵–10¹⁰
4	7	0.8	.	0.2	●⁰ 9⁴⁵–12³⁰ ≡⁰ 4³⁰–5³⁵ =–9⁵⁰ ⌒ 0⁰⁰–9⁰⁰
5	8	.	.	7.3	
6	7	.	.	1.8	
7	7	.	.	8.4	= 5²⁰–10³⁰ 20³⁰–24 ⌒⁰ 2⁰⁰–9²⁰ 21⁵⁰–24
8	7	.	.	10.5	= 0⁰⁰–5¹⁵ ⌒⁰ 0⁰⁰–9⁰⁵ ⌒¹ 22⁰⁰–24
9	7	.	.	10.4	⌒¹ 0⁰⁰–9¹⁵
10	7	0.0	.	.	●⁰ 11³⁰–³⁵ ⌒ n – 6⁰⁰
11	7	1.9	.	3.1	= 6³⁰–8³⁵
12	7	0.2	.	3.8	●⁰ 3³⁰–6³⁰ ▽●¹ 14⁵¹–15⁰⁹ ▽●² 15²⁰–²⁸
13	7	0.0	.	6.8	▽●⁰ 16²⁵–³⁵ 17⁰⁰–¹⁰ 17⁴⁵–18⁰⁰ ⌒ 17⁰⁰–¹⁵
14	8	0.0	.	5.7	●⁰ 7⁴⁵–8¹⁰ ⌓⁰ 2¹⁰–3⁴⁵
15	6	2.7	.	1.0	●⁰ 7¹⁰–8⁴⁰ ●¹ 10²⁰–12³⁵ ●⁰ 13⁰⁶–14⁰⁰, 20⁵⁰–21¹³ ≫ 13¹⁵–16⁰⁰ (por. do 20 m/sek)
16	7	.	.	6.6	⌒ n – a 20⁴⁰–24
17	7	0.0	.	3.9	= 6¹⁰–9¹⁰ ⌒ 0⁰⁰–9⁰⁰ ⊕⁰ 6⁴⁰–7³⁵
18	6	49.8	.	.	●⁰ 6⁵⁵–11³⁰ ●⁰–18²⁰ ●⁰–22¹⁰ ●¹–24
19	7	1.4	.	.	●¹ 0⁰⁰–8⁰⁰ ●⁰–11²⁰
20	7	.	.	0.3	●⁰ 1⁴⁰–3⁴²
21	7	0.0	.	2.0	▽●⁰ 14¹⁰–¹⁷ 14³⁰–⁴⁵ = 1³⁰–6³⁰
22	6	9.3	.	.	●⁰ 11⁰⁴–12⁰⁵ ●¹–12⁴⁵ ●⁰–15³⁸ ●⁰ 16³⁸–19³⁰ 21⁵⁵–22⁴⁰ = 23¹⁵–24
23	7	31.5	.	.	▽●⁰ 5⁴⁰–6⁵⁰ ▽●⁰–7⁰⁰ ▽●¹–7²⁰ ▽●¹ 7⁴⁰ ●⁰ 9⁴⁴ 10³⁰ 14⁰⁶–³⁰ 15⁴⁵–16⁰² ▽●¹ 16³⁵–17³⁰ ▽●⁰–18⁰⁵ ●⁰ 18¹⁵–19⁴⁰ 20²⁵–22¹⁵ 23³⁰–24
24	8	8.6	.	1.4	●¹ 0⁰⁰–⁴⁰ ●¹ 1¹⁵–5³⁰ ●⁰–6¹⁵ ▽●⁰ 14⁰⁰–18⁴⁰
25	7	1.9	.	0.1	●⁰ 1⁴⁰–4⁵⁵ ●⁰ 10¹⁰–11²⁰ ▽●⁰–13¹⁵ 14²⁰–⁴⁰ ●⁰ 19⁵⁰–21¹⁰ ▽●¹ 21²⁰–³²
26	7	.	.	2.7	
27	7	6.0	.	0.8	●⁰ 17⁴⁵–24 ≫ 22¹⁰–23¹⁵
28	7	1.5	.	4.2	●⁰ 0⁰⁰–1¹⁵ 2⁴⁵ 3¹⁵–5⁰² 8⁰⁷–9³⁵
29	7	17.5	.	3.1	▽●¹ 11⁰⁸–²¹ ▽●⁰ 15³⁰–16³⁵ 17⁴⁰–18¹⁵ ▽●¹–19⁵⁰ ▽●⁰–20¹⁰ ●⁰–21⁰⁰ ●¹–23³⁰ ●⁰–24
30	6	7.8	.	0.2	●⁰ 0⁰⁰–1¹⁰ ●¹–2⁵⁰ ●⁰ 5⁴⁵–6²⁸ ●² 7²⁸–9²⁰ 10²⁵–13²⁰
31					
Σ	–	149.3	–	102.1	UWAGI

23.IX: ⌓¹ 5⁵⁰–7⁰⁰, 16⁴⁵–17³⁰, = 0⁰⁰–7³⁰

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1	8	1.3	.	8.6	▽●⁰ 19⁴⁰–22⁴⁵
2	7	.	.	4.6	
3	8	.	.	5.9	⌓ 0⁰⁰–6²⁰
4	7	0.3	.	3.9	▽●⁰ 11⁰²–¹⁵ 16⁴²–⁵⁰ 18⁴⁰–19¹⁰
5	7	1.9	.	2.0	⌓⁰ 0³⁰–8¹⁵
6	7	(0.0)	.	.	●⁰ 3²⁷–6⁴⁰
7	7	0.0	.	.	●⁰ 10³⁰–12¹⁵
8	8	.	.	7.6	⌓ 18³⁰–19⁴⁰
9	8	.	.	6.7	⌓⁰ 0⁰⁰–6⁴⁰
10	8	.	.	9.6	⌓⁰ 1⁰⁰–7³⁰ ⌒ 21⁰⁰–24
11	8	.	.	8.7	= 5¹⁰–8³⁵ ⌓ 11⁰–6²⁰
12	7	0.8	.	5.0	●⁰ 14¹⁴–³⁰ 15²⁷–17¹⁰ 19⁴⁰–20⁰⁵ = 5²⁰–8³⁰ ⌓ 10⁰–6³⁰
13	7	.	.	2.8	≡⁰ 2³⁰–8⁴⁰ =–11²⁰ 21³⁰–24
14	7	.	.	0.8	= 0⁰⁰–⁴⁰ 6¹⁰–9¹⁰ 12¹⁵–15²⁰
15	7	.	.	5.9	= 5¹⁵–9⁰⁷ ⌓ 3¹⁵–6⁴⁰
16	7	.	.	1.0	
17	7	0.0	.	6.0	●⁰ 15⁴⁸–16¹⁸
18	7	0.0	.	.	●⁰ 16²⁰–17²⁰
19	7	.	.	3.9	
20	7	1.9	.	.	●⁰ 9⁴⁰–10²⁵ 14⁴⁵ 17¹⁰–18²⁰ ●¹–19¹⁰ ●⁰–20⁴⁰
21	7	.	.	6.9	
22	7	1.7	.	.	●⁰ 12²⁰–15³⁰
23	6	4.0	.	.	●⁰ 1²⁵–2⁰¹ 3⁴⁸–12²⁸ 13²⁰–16¹² = 18³⁰–20⁴⁰
24	6	1.9	.	.	●⁰ 9⁴⁰–11³⁸ 12²⁰–13³⁵
25	7	0.0	.	7.0	⌒¹ 20⁰⁰–24
26	7	(0.0)	.	0.7	●⁰ 6³⁵–⁴⁷ ⌒¹ 0⁰⁰–6³⁵
27	6	.	.	5.7	= 6¹⁰–24
28	7	.	.	0.1	= 0⁰⁰–11³⁰
29	7	.	.	1.3	
30	7	3.6	.	5.7	●¹ 23³⁰–24
31	6	0.0	.	1.0	●⁰ 0⁰⁰–3³⁵ ●⁰ 6³⁵–7¹⁵ = 5¹⁰–23³⁰
Σ	–	17.4	–	111.4	UWAGI

Białystok $\varphi = 53°07'$ $\lambda = 23°11'$ **Listopad – Novembre 1957**

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.4	89.4	91.6	90.8	6.8	13.5	9.8	10.0	13.6	6.1	94	69	86	83	0.6	4.9	1.7	2.4	4	3	10	S 2	SSW 7	SSW 2
2	94.8	96.6	98.3	96.6	7.1	13.9	7.3	8.9	14.0	5.1	94	71	87	84	0.6	4.6	1.3	2.2	6	4	8	SSW 2	SSW 3	S 1
3	99.4	99.8	100.4	99.9	4.4	10.1	9.3	8.3	10.4	3.1	100	93	95	96	0.0	0.8	0.6	0.5	10 ≡	10	10	C 0	S 2	SE 2
4	99.6	99.8	100.4	99.9	8.3	10.6	11.5	10.5	11.6	7.6	99	92	96	96	0.2	1.0	0.5	0.6	10	10	10	ESE 2	SE 4	SE 5
5	100.3	100.0	99.1	99.8	7.7	9.8	10.5	9.6	11.6	6.8	97	92	86	92	0.3	0.9	1.8	1.0	10	10	1	SE 4	SE 8	SE 5
6	98.4	98.9	99.1	98.8	7.3	14.5	10.3	10.6	14.5	6.4	93	65	73	77	0.7	5.8	3.3	3.3	1	3	3	SE 5	SE 7	SE 6
7	97.2	96.1	96.0	96.4	6.6	11.1	8.5	8.7	11.8	5.8	88	72	82	81	1.1	3.7	2.0	2.3	6	9	10	SE 5	SE 6	SE 6
8	96.2	96.6	97.2	96.7	6.1	9.5	9.1	8.4	9.7	5.1	92	83	83	86	0.7	2.1	2.0	1.6	10	10	10	SE 4	SE 5	SE 3
9	95.1	95.1	95.6	95.3	8.3	9.8	9.3	9.2	9.9	6.8	87	86	93	89	1.4	1.7	0.8	1.3	10	10	10	ESE 4	ESE 3	E 5
10	96.3	98.2	100.8	98.4	8.5	8.4	7.8	8.1	9.4	7.1	96	93	96	95	0.5	0.7	0.5	0.6	10	10 ●	10	E 5	E 4	E 3
11	102.6	104.0	106.3	104.3	7.7	7.7	6.3	7.0	8.1	5.7	96	82	78	85	0.5	1.9	2.1	1.5	10	10	10	E 5	ENE 6	ENE 8
12	109.2	111.5	113.0	111.2	2.8	2.8	0.5	1.6	6.3	0.1	93	84	90	89	0.6	1.2	0.6	0.8	10 ●	10	10	NE 5	NE 4	NE 1
13	113.3	113.8	114.1	113.7	-2.2	-2.3	-1.8	-2.0	0.5	-3.4	85	85	83	84	0.8	0.8	0.9	0.8	10	10	10	NE 2	N 3	N 1
14	112.7	112.9	114.6	113.4	-0.4	1.5	1.8	1.2	2.2	-2.6	90	85	93	89	0.6	1.0	0.6	0.7	10	10	10 ●	W 2	W 5	WNW 2
15	115.8	115.8	114.8	115.5	2.0	2.9	1.4	1.9	3.1	0.8	96	88	83	89	0.3	0.9	1.1	0.8	10 ●	10 ●	10	WNW 2	W 2	SW 2
16	113.4	114.3	116.0	114.6	-0.8	0.2	0.4	0.0	1.5	-1.5	79	77	88	81	1.2	1.4	0.8	1.1	10	10	10	C 0	W 1	W 1
17	116.9	117.4	118.7	117.7	1.0	3.8	2.6	2.5	3.9	-0.5	87	77	86	83	0.9	1.9	1.1	1.3	10	10	10	C 0	W 1	C 0
18	118.7	118.2	117.4	118.1	1.7	3.3	2.2	2.4	3.3	0.8	94	85	86	88	0.4	1.2	1.1	0.9	10	10	10	C 0	C 0	W 1
19	117.6	119.4	122.7	119.9	0.8	2.8	1.9	1.8	2.8	0.1	88	76	91	85	0.8	1.9	0.6	1.1	10	10	10	C 0	W 3	N 1
20	125.2	125.6	124.2	125.0	-1.2	3.4	0.2	0.6	3.4	-2.5	93	66	84	81	0.4	2.6	1.0	1.3	8	4 ⊙	10	C 0	SE 3	SE 1
21	122.1	120.4	116.1	119.5	-2.6	3.1	-2.7	-1.2	3.1	-3.5	93	68	93	85	0.3	2.5	0.3	1.0	9	3	0	SE 1	S 3	C 0
22	109.6	106.6	102.3	106.2	-4.9	2.8	-1.8	-1.4	2.8	-5.9	95	76	88	86	0.2	1.9	0.7	0.9	1	0	0	WSW 1	S 2	S 2
23	99.5	98.0	96.1	97.9	-0.6	1.0	0.9	0.6	1.1	-4.3	89	81	94	88	0.6	1.3	0.4	0.8	10	10	10	SSW 2	SSW 5	SW 3
24	98.2	98.8	96.3	97.8	1.4	3.3	3.3	2.8	3.4	0.2	92	69	91	84	0.6	2.3	0.6	1.2	10	9	10	W 5	W 7	W 5
25	94.2	95.4	98.4	96.0	5.1	6.5	6.1	6.0	6.7	2.7	92	93	98	94	0.7	0.7	0.1	0.5	10	10 ●	10 ●	W 6	W 4	WNW 1
26	100.0	101.6	98.1	99.9	5.1	5.9	7.1	6.3	7.9	4.5	100	94	94	96	0.0	0.6	0.6	0.4	10 ●	10	10 ●	C 0	WNW 1	WSW 4
27	90.8	88.8	95.9	91.8	6.5	6.9	1.7	4.2	7.4	1.0	90	90	87	89	1.0	1.0	0.9	1.0	10	10 ●	10	W 7	W 7	NW 5
28	95.0	88.2	81.2	88.1	0.5	5.5	6.8	4.9	7.3	-1.1	96	98	93	96	0.2	0.1	0.8	0.4	10 ⁂	10 ●	10	SSE 2	SW 4	W 8
29	80.7	89.4	102.5	90.9	-0.5	-7.5	-8.9	-6.4	6.8	-9.7	96	79	64	80	0.3	0.7	1.1	0.7	10	10 ✳	0	NNW 5	N 10	N 8
30	107.4	107.8	108.3	107.8	-9.1	-6.6	-7.5	-7.7	-6.6	-10.3	79	78	76	78	0.6	0.8	0.8	0.7	6	8 ✳	0	N 7	N 10	NNW 4
31																								
M	103.7	103.9	104.5	104.0	2.8	5.3	3.8	3.9	6.4	1.0	92	82	87	87	0.6	1.8	1.0	1.1	8.7	8.4	8.1	2.8	4.3	3.2

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1	107.9	107.7	108.6	108.1	-0.7	-2.1	-5.3	-5.4	-1.7	-9.6	86	68	90	81	0.4	1.6	0.4	0.8	0	6 ⊙	4	NW 3	NW 4	C 0
2	108.8	109.9	110.0	109.6	-9.7	-1.9	-8.6	-7.2	-1.7	-11.1	94	79	89	87	0.2	1.1	0.4	0.6	1	3 ⊙	0	C 0	NW 2	C 0
3	104.9	103.0	104.4	104.1	-2.7	-0.6	-1.0	-1.3	-0.6	-10.2	91	93	97	94	0.5	0.4	0.2	0.4	10	10 ✳	10 ≡	NW 2	C 0	NW 1
4	105.7	104.9	103.3	104.6	-1.6	-0.5	-1.1	-1.1	-0.3	-2.5	92	88	93	91	0.4	0.7	0.4	0.5	10	10	10	E 1	E 2	SSW 3
5	96.7	94.7	97.5	96.3	1.2	3.6	3.3	2.8	4.0	-1.7	94	95	93	94	0.4	0.4	0.5	0.4	10 ●	10	10	SW 2	W 4	NW 6
6	104.7	108.3	107.8	106.9	1.3	0.2	-4.4	-1.8	3.4	-5.1	77	70	91	79	1.5	1.9	0.4	1.3	10	2	0	N 5	N 1	N 1
7	101.1	95.9	90.7	95.9	-4.9	-0.4	-0.8	-1.7	0.6	-6.3	93	80	87	87	0.3	1.2	0.7	0.7	2	8	10	N 2	S 6	SW 3
8	79.1	71.7	59.2	70.0	-1.8	-0.4	-0.9	-1.0	0.2	-2.6	86	90	95	90	0.8	0.6	0.3	0.6	10	10 ✳	10 ⁂	SSE 6	S 6	SSE 6
9	53.4	56.8	72.6	60.9	3.3	3.2	-1.2	1.0	4.2	-1.9	95	86	70	84	0.4	1.1	1.7	1.1	10 ●	10 ●	3	SW 6	W 7	W 7
10	77.7	78.0	80.6	78.8	-2.6	0.8	-4.7	-2.8	0.9	-5.5	81	53	83	72	1.0	3.1	0.7	1.6	5	7	2	WSW 5	SW 5	W 5
11	87.9	92.7	93.7	91.4	-5.3	-1.3	-5.0	-4.2	-1.3	-6.6	73	58	83	71	1.1	2.3	0.7	1.4	8	3	6	SW 7	WSW 5	WSW 2
12	88.8	87.1	84.6	86.8	-1.8	-1.2	-0.9	-1.2	-0.8	-7.9	65	80	93	79	1.9	1.1	0.4	1.1	10	10	10	E 5	E 4	E 2
13	83.3	80.5	74.5	79.4	-0.8	3.9	5.1	3.3	5.4	-1.8	97	87	89	91	0.2	1.1	1.0	0.8	10	7	10 ●	E 3	E 2	SE 4
14	65.6	68.0	81.9	71.8	2.8	1.8	-4.3	-1.0	5.1	-5.1	96	96	89	94	0.3	0.3	0.5	0.4	10 ●	10 ●	10 ✳	ESE 1	N 5	N 8
15	96.0	104.0	110.1	103.4	-7.1	-6.7	-9.7	-8.3	-4.0	-10.7	85	70	81	79	0.5	1.1	0.5	0.7	10	9 ⊙	0	N 7	NNE 4	N 1
16	113.3	114.9	115.0	114.4	-12.6	-6.3	-10.3	-9.9	-5.8	-13.7	81	65	81	76	0.4	1.3	0.5	0.7	0	0	0	N 1	N 1	C 0
17	112.2	108.4	106.0	108.9	-12.0	-4.5	-9.8	-9.0	-4.5	-13.2	89	60	88	79	0.3	1.7	0.4	0.8	1	1	1	N 1	ESE 3	C 0
18	106.2	106.6	108.0	106.9	-8.9	-6.1	-11.3	-9.4	-4.2	-12.3	86	76	83	82	0.4	0.9	0.4	0.6	10	0	0	C 0	C 0	C 0
19	110.6	112.6	115.0	112.7	-7.8	-5.7	-4.3	-5.5	-4.2	-12.8	90	90	91	90	0.3	0.4	0.4	0.4	10	10	10	C 0	C 0	SE 1
20	114.7	114.2	113.6	114.2	-3.4	-1.0	0.0	-1.1	0.0	-4.9	90	81	94	88	0.5	1.1	0.4	0.7	10	10	10	S 3	SW 4	W 3
21	109.8	106.9	108.2	108.3	-0.1	1.6	2.2	1.5	2.4	-1.4	94	74	93	87	0.4	1.8	0.6	0.9	8	10	10 ●	SW 7	SW 5	SW 3
22	109.7	109.2	109.3	109.4	1.0	1.4	1.3	1.2	2.2	0.2	94	96	91	94	0.4	0.3	0.6	0.4	10 ≡	10 ≡	10 ●	SW 1	SW 4	SW 1
23	108.2	107.2	103.8	106.4	0.7	0.8	-1.8	-0.5	1.3	-2.3	90	81	81	84	0.6	1.3	1.0	1.0	10	10	0	S 2	S 4	SSE 3
24	101.9	102.3	103.5	102.6	-6.0	-2.3	-7.3	-5.7	-1.8	-7.8	89	76	88	84	0.4	1.3	0.4	0.7	0	1	0	SSE 1	C 0	SSE 1
25	104.2	103.4	102.2	103.3	-0.6	-1.2	-3.0	-4.0	-0.7	-9.3	89	78	84	84	0.4	1.2	0.8	0.8	0	6	10	SSE 1	SSE 1	SSE 1
26	103.4	104.3	105.5	104.7	-2.2	-0.5	0.5	-0.4	0.6	-3.8	89	98	96	94	0.6	0.2	0.2	0.3	10	10≡ ●	10	SW 1	WSW 4	SW 2
27	106.8	106.0	104.3	105.7	0.4	1.0	0.6	0.6	1.1	-0.3	96	96	92	95	0.3	0.3	0.5	0.4	10	10	10 ●	SW 4	WSW 5	SW 6
28	99.6	96.6	91.8	96.0	1.8	2.5	1.3	1.7	2.6	0.1	93	91	91	92	0.6	0.6	0.6	0.6	10	10	9	WSW 4	SW 4	SW 6
29	88.1	87.0	85.6	86.9	0.4	1.6	1.1	1.0	1.7	-0.4	96	91	90	92	0.3	0.7	0.6	0.5	10	10	10	W 7	SW 4	SW 4
30	77.5	78.2	76.7	77.5	1.5	2.8	2.2	2.2	2.9	-0.2	89	76	89	85	0.8	1.9	0.8	1.2	10	9	10	SW 4	SW 7	SW 6
31	78.5	81.0	82.1	80.5	0.1	0.5	0.2	0.2	2.2	-0.7	94	88	88	90	0.4	0.7	0.7	0.6	8	8 ✳	10	WSW 4	W 3	SW 4
M	97.0	96.8	97.1	97.0	-3.0	-0.5	-2.5	-2.1	0.3	-5.5	89	81	88	86	0.5	1.1	0.6	0.7	7.5	7.4	6.6	3.1	3.4	2.9

Białystok $H_s = 139$ m $H_b = 140{,}8$ m $h_w = 11$ m **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	3.7	
2	7	.	.	3.8	= 21³⁰ – 23³⁰ ≡° – 24 ; ⌒¹ 17³⁰ – 18¹⁰
3	6	.	.	.	≡¹ 0⁰⁰ – 7³⁰ = – 24
4	7	0.0	.	0.1	•° 9³⁵ – 10³⁶ •° 16⁴⁰ – 17⁴² ; = 0⁰⁰ – 6³⁵ ≡² – 7³⁵ = – 10²⁷ , 18¹⁵ – 20⁴⁰
5	7	.	.	.	= 5¹⁰ – 6⁵⁰ ≡° – 10³⁰ = – 11²⁵ ; ⌒¹ 13⁰ – 9⁰⁰
6	7	.	.	6.7	⌒¹ 22¹⁰ – 24
7	7	0.0	.	3.1	•° 21⁵⁰ – 22¹⁵ ; ⌒¹ 0⁰⁰ – 9⁰⁰
8	7	.	.	.	⌒ 1¹⁰ – 2³⁰
9	7	0.3	.	.	•° 12²⁸ – 14¹⁷ , 17³⁶ •¹ 19³⁰ – 20⁰²
10	6	0.7	.	.	•¹ 3³⁸ – 5¹⁰ , 9⁴⁰ – 13²⁵ ; = 5¹⁵ – 7⁴⁰
11	7	0.0	.	.	•¹ 4⁴⁰ – 5³⁸ •° 9⁴⁹ – 10⁴⁵
12	7	0.0	.	.	•¹ 0³⁰ – 3¹⁵ •° – 4³⁰ , 6²⁰ – 8³²
13	7	.	.	.	
14	7	0.4	.	.	•° 18⁴⁰ – 24
15	6	0.4	.	.	•° 0⁰⁰ – 1³⁰ •¹ – 3²⁰ •° – 6⁰⁰ •° – 7⁴⁸ , 8²⁴ 9¹³ , 12²² – 37 , 13¹⁰ 14³⁶
16	7	.	.	.	
17	7	.	.	.	= 8³⁰ – 9⁴⁰
18	7	0.0	.	.	•° 9⁴⁵ 10⁰¹
19	7	.	.	.	
20	7	.	.	4.3	
21	8	.	.	3.1	⌒° 1³⁰ – 8³⁰ ⌒¹ 20⁰⁰ – 24
22	7	.	.	3.6	⌒¹ 0⁰⁰ – 11⁰⁰ ⌒° 21²⁰ – 24
23	7	1.1	.	.	*° 15⁰⁸ – 16⁴³ , 17¹² – 20⁰⁶ *° 20⁴⁵ – 22³⁸ ; ⌒° 0⁰⁰ – 9⁰⁰
24	7	0.9	pż.	1.7	•° 3⁴⁰ – 5¹⁵ *° 13¹⁰ – 16³⁵ •° 17⁴⁵ – 18¹⁵
25	6	5.6	.	.	•° 7¹⁰ – 54 •° 9³⁰ – 12²⁰ •° – 24
26	7	3.2	.	.	•° 0⁰⁰ – 10³⁵ •¹ 16²⁵ – 18⁵⁰ 19⁴⁵ – 20²⁰ •¹ – 21¹⁵ •° – 23³¹
27	6	2.3	.	.	•° 0¹⁵ 4⁴⁸ 8⁴⁷ – 9⁰⁷ , 11⁴⁵ – 14¹⁵ , 15¹⁸
28	6	7.5	.	.	•° 0⁵⁰ – 3³⁰ *° – 6³⁵ •° – 17¹⁸ , 18⁴⁰ 20²⁵
29	6	1.0	.	.	•° 1³⁵ – 2⁴⁸ *¹ 7²⁵ – 12²⁷ *° – 12³⁵ *¹ – 14⁴⁰ *° 15³⁰ – 16²² , 18¹⁵ – 19³⁶
30	6	0.1	1	0.3	*° 1⁰⁷ 4⁰² ⚹° 7⁰³ – 11³⁵ , 12²⁰ – 15³⁰
31					
Σ	—	23.5	—	30.4	UWAGI.

Grudzień – Décembre

1	8	.	1	4.8	
2	7	.	1	3.3	⌒ 19⁰⁰ – 24
3	6	0.2	1	.	*° 7²⁰ – 35 8³⁰ – 11⁴⁰ 12¹⁰ – 14³⁰ , 15¹⁰ – 16³⁰ = 18³⁰ – 19³⁰ ≡° – 20⁴⁰ ; ⌒ 0⁰⁰ – 7⁴⁰
4	7	1.1	1	.	*° 1²⁰ – 3¹⁵ *° 10⁵⁰ – 11⁴⁵ , 13¹⁰ – 14⁴⁰ *° – 16²⁰ *° 23⁴⁰ – 24
5	6	0.0	1	.	*° 0⁰⁰ – 3⁴² •° 4³⁵ – 6¹⁰ •¹ – 10⁴⁵ •° 23⁴⁰ – 24 ; = 8⁰⁰ – 13¹⁵
6	8	.	.	4.0	•° 0⁰⁰ – 1¹³ 2⁸
7	7	.	.	0.9	= 22¹⁰ – 24 ; ⌒¹ 1¹⁵ – 24
8	6	10.3	.	.	*° 8⁰⁰ – 40 10²⁶ – 13⁰⁵ , 15²² – 17³⁰ *¹ – 18⁴⁵ *° – 20¹⁰ *¹ – 21²⁵ •° – 24 ; = 0⁰⁰ – 10 ; ⌒¹ 0⁰⁰ – 7⁰⁰
9	6	2.8	2	.	•° 0⁰⁰ – 1²⁰ •¹ 5²⁰ – 7¹⁵ •° – 10³² , 12¹⁵ – 14²⁰ *° – 16¹⁰
10	8	0.3	.	3.7	*° 17³⁰ – 18³⁰
11	8	.	1	2.9	⌒ 23¹⁰ – 24
12	7	0.0	pż.	.	*° 8³⁰ – 10⁴⁰ 16⁴⁵ – 17³⁰ ; ⌒ 0⁰⁰ – 2¹⁵
13	7	2.6	pż.	2.1	•° 19³⁵ – 20⁴⁰
14	6	5.9	.	.	•° 2⁴⁵ – 3²⁰ •° – 13³⁰ *° 18³⁰ – 22⁴⁵ ⚹ 19⁰⁰ – 23⁰⁰ , = 1³⁵ – 2⁴⁵
15	7	0.0	pż.	2.6	*° 7²⁹ 8¹⁰ ⊕¹ 11²⁵ – 13⁴⁰
16	8	.	pż.	3.1	⌒ 18³⁰ – 24
17	8	.	pż.	4.7	⌒ 0⁰⁰ – 12¹⁰ 18⁴⁵ – 24
18	7	0.0	pż.	2.2	•° 9²⁰ – 40 ; = 8³⁰ – 9⁴⁰ ≡° – 10⁴⁵ = – 11³⁰ ; ⌒ 0⁰⁰ – 10⁰⁰
19	5	.	pż.	.	≡° 1¹² – 5⁵⁰ = – 7⁴⁵ ≡° – 10²⁰ = – 24 ; V 2¹⁰ – 24
20	7	.	pż.	.	V¹ 0⁰⁰ – 4¹⁵
21	7	0.2	pż.	0.9	•° 19³⁵ – 21²⁰ 22⁴⁵ – 23³⁰
22	3	0.0	.	.	•° 0¹⁰ – 35 •° 20⁰⁰ – 21⁰¹ ; ≡° 1⁴⁵ – 17³⁰ = – 20⁰⁰
23	7	.	.	.	•° 0⁴⁰ – 3⁴⁵ = 0⁰⁰ – 11³⁰
24	7	.	.	2.1	⌒° 2¹⁵ – 8¹⁰ ⌒¹ 17⁰⁰ – 24
25	7	.	.	1.0	⌒¹ 0⁰⁰ – 24
26	3	0.0	.	.	•¹ 11²⁵ – 14³⁵ ; = 7⁰⁰ – 25 ≡° – 13⁴⁵ = – 14⁴⁵ – 24 , ⌒¹ 0⁰⁰ – 19⁰⁰
27	5	0.0	.	.	•° 14³⁶ – 21¹⁵ , 21³⁰ – 23⁴⁰ ; = 0⁰⁰ – 2²⁰ 8¹⁰ – 24
28	6	4.4	.	.	•° 8³⁰ – 9⁰⁵ , •° – 10³⁰ •° – 11³⁵ 13¹⁰ – 14⁵⁰ 15⁴⁵ – 16⁴⁰ ; = 0⁰⁰ – 20³⁵
29	7	2.2	5	.	*° 0⁰⁰ – 2¹⁵ *¹ – 5³⁰ *° – 6¹⁰ 11⁴⁵ – 12¹⁵ , 13⁰³ – 47 *° 15¹² – 23⁴⁰ *¹ – 24
30	7	6.1	2	1.4	*° 0⁰⁰ – 2⁴⁵ ⚹ 8³⁰ – 45 11⁰⁵ – 12¹⁰ •° 14¹⁵ – 40 *° – 15⁰⁵ *° – 18¹⁵ •° 21⁴⁰ – 22²⁰ *° – 24
31	6	0.2	3	.	*° 0⁰⁰ – 30 •° – 1¹⁷ *° – 2³⁵ ⚹ 12¹⁰ – 30 , 13³⁰ – 14³⁵ △° – 15³²
Σ	—	35.3	—	39.7	UWAGI.

Poznań – Ławica

$\varphi = 52°25'$ $\lambda = 16°50'$

Styczeń – Janvier 1957

DNI	CIŚNIENIE P – 900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	105.4	105.3	104.4	105.0	-4.9	-3.7	-3.1	-3.7	-2.8	-5.5	95	94	95	95	0.2	0.3	0.3	0.3	10 ≡	10	10	NNE 2	NNE 2	E 3
2	100.6	101.2	105.0	102.3	-1.1	0.4	0.8	0.2	4.2	-3.4	95	90	90	92	0.3	0.6	0.7	0.5	10	10	10	E 4	C 0	SW 3
3	109.6	110.6	110.2	110.1	0.2	0.4	-1.4	-0.6	1.2	-1.9	96	96	99	97	0.3	0.3	0.1	0.2	10	10 ✳	0 ≡	C 0	S 1	C 0
4	110.7	112.2	112.0	111.6	-4.4	0.6	0.3	-0.6	1.8	-5.4	93	88	92	91	0.3	0.8	0.5	0.5	0	9	2	C 0	S 3	S 3
5	110.4	106.2	104.8	107.1	1.7	2.5	6.9	4.5	7.3	-0.5	96	95	96	96	0.3	0.4	0.4	0.4	10	10 ●	10	SSW 6	SW 7	SW 7
6	100.3	99.3	102.8	100.8	9.1	9.5	3.9	6.6	10.1	3.3	87	93	82	87	1.6	0.8	1.5	1.3	10	9	0	W 7	W 8	W 9
7	108.4	112.9	117.0	112.8	4.3	5.7	4.7	4.8	6.0	3.0	85	74	82	80	1.2	2.4	1.5	1.7	10 ●	10	10	WNW 12	NW 10	WNW 8
8	116.8	115.7	114.4	115.6	4.5	5.4	6.4	5.7	6.7	3.6	85	84	94	88	1.3	1.4	0.6	1.1	10	10	10	W 6	WNW 10	W 9
9	111.9	109.7	106.8	109.5	6.0	7.6	5.9	6.4	7.9	5.3	91	83	89	88	0.9	1.7	1.0	1.2	10	10	10	WSW 7	W 7	WSW 5
10	103.0	102.2	102.3	102.5	5.3	5.3	2.8	4.0	6.9	2.4	86	81	77	81	1.3	1.7	1.7	1.6	10	10	7	WNW 6	W 7	W 6
11	104.8	108.5	110.1	107.8	1.3	2.9	0.1	1.1	3.3	-0.6	81	72	84	79	1.3	2.1	1.0	1.5	10	9	9	W 6	NW 3	NW 6
12	104.9	97.9	91.6	98.1	-0.3	1.1	0.7	0.6	1.3	-2.4	94	92	94	93	0.4	0.5	0.4	0.4	10 ✳	10 ✳	10 ✳	W 7	WSW 7	WSW 4
13	91.4	93.9	98.8	94.7	1.1	2.1	0.4	1.0	2.6	0.1	96	98	96	97	0.2	0.1	0.3	0.2	10 ●	10 ●	10 ✳	WSW 4	WSW 3	NE 2
14	107.2	112.7	116.4	112.1	-4.4	-5.0	-6.6	-5.6	0.6	-7.0	89	80	83	84	0.5	0.8	0.6	0.6	10	10	10	ESE 8	E 10	E 8
15	117.0	116.3	116.9	116.7	-7.5	-6.9	-7.6	-7.4	-6.3	-8.2	82	80	87	83	0.6	0.7	0.4	0.6	10	9 ✳	10 ✳	ENE 7	NE 6	ENE 5
16	120.1	121.2	122.7	121.3	-17.1	-9.5	-15.0	-14.2	-7.0	-19.0	85	79	96	87	0.2	0.6	0.1	0.3	0	0 ⊙	0	NNE 2	C 0	C 0
17	122.0	122.0	121.6	121.9	-10.5	-4.8	-4.3	-6.0	-3.6	-17.1	94	93	96	94	0.2	0.3	0.2	0.2	9	10	10 ≡	C 0	WSW 3	NW 3
18	120.5	119.9	118.2	119.5	-4.6	-4.1	-4.8	-4.6	-3.7	-5.3	93	94	95	94	0.3	0.3	0.2	0.3	10 ≡	10 ≡	10 ≡	WNW 2	NW 1	C 0
19	117.9	118.9	120.3	119.0	-2.9	-1.3	-1.8	-2.0	-1.0	-5.3	95	93	92	93	0.2	0.4	0.4	0.3	10	10	10	W 1	NW 2	NW 2
20	118.9	117.9	115.2	117.3	-1.3	-0.9	-1.8	-1.4	-0.7	-2.4	93	89	92	91	0.4	0.6	0.4	0.5	10	10	10	W 3	W 6	WSW 6
21	111.2	112.1	113.0	112.1	-6.0	-0.9	-7.8	-5.6	-0.2	-8.1	81	61	84	75	0.7	2.2	0.5	1.1	1	3	0	WSW 6	WSW 6	WSW 4
22	112.3	110.8	108.2	110.4	-8.9	-0.7	-7.6	-6.2	0.5	-11.9	83	66	84	78	0.5	2.0	0.5	1.0	0	5	0	SW 5	SW 5	SW 2
23	108.4	108.4	106.5	107.8	-7.6	-1.3	-5.8	-5.1	1.0	-9.2	82	64	87	78	0.6	2.0	0.5	1.0	7	0	0	SW 5	SW 2	SW 3
24	102.3	99.6	98.0	100.0	-3.2	-1.6	-2.1	-2.2	-1.2	-6.3	74	67	83	75	1.2	1.8	0.9	1.3	10	10	10	SE 5	ESE 5	C 0
25	97.1	98.7	102.7	99.5	-3.9	0.1	0.7	-0.6	0.7	-4.5	92	85	92	90	0.4	1.0	0.5	0.6	10	10	10	ESE 1	SSW 4	WSW 3
26	107.2	108.4	105.1	106.9	-0.9	2.2	1.2	0.9	3.5	-4.1	94	64	72	77	0.3	2.6	1.9	1.6	10	0	0	C 0	SW 4	SSW 6
27	102.0	104.4	108.3	104.9	2.5	6.9	2.2	3.4	6.9	1.0	96	77	77	83	0.3	2.3	1.7	1.4	10	8	0	WSW 3	W 7	W 2
28	107.0	112.6	119.5	113.0	0.6	1.7	0.9	1.0	2.4	-0.4	92	87	92	90	0.5	0.9	0.5	0.6	9	10 ●	4	WSW 6	WNW 8	W 3
29	119.8	118.9	116.7	118.5	-1.2	1.6	1.4	0.8	2.3	-2.3	94	81	85	87	0.4	1.3	1.0	0.9	8	9	2	WSW 3	SW 5	S 4
30	113.1	111.1	110.5	111.6	-1.0	2.7	1.7	1.3	2.9	-2.0	94	75	96	88	0.4	1.8	0.3	0.8	3	9	10	S 4	SSW 5	WSW 4
31	110.2	111.5	110.2	110.6	1.3	2.1	1.7	1.7	3.1	0.5	98	96	96	97	0.1	0.1	0.3	0.2	10 ≡	10 ≡	10 ●	SSW 2	SSW 3	S 4
M	109.4	109.7	110.0	109.7	-1.7	0.6	-0.9	-0.7	1.8	-3.7	90	83	89	87	0.6	1.1	0.7	0.8	8.3	8.4	6.6	4.2	4.8	3.9

Luty – Février

1	105.0	104.8	105.1	105.0	2.4	4.9	5.9	4.8	6.0	1.1	95	98	98	97	0.4	0.2	0.2	0.3	10	10 ●	10 ☽	S 4	S 6	SSW 6
2	109.3	112.5	114.7	112.2	8.7	8.8	5.0	6.9	9.9	5.0	92	92	98	94	0.9	0.9	0.4	0.7	9	9	10 ≡	WSW 5	SSW 4	SSW 2
3	114.2	115.5	116.3	115.3	4.0	4.7	1.3	2.8	5.2	0.8	100	95	96	97	0.0	0.4	0.2	0.2	10 ●	10 ●	10	C 0	N 3	E 1
4	113.7	111.6	111.0	112.1	1.3	5.3	2.2	2.8	6.9	-0.3	98	87	98	94	0.1	1.1	0.2	0.5	10● ≡	10	0	SE 4	S 5	SSW 4
5	110.8	109.8	107.4	109.3	0.2	8.6	3.6	4.0	10.5	-0.6	96	77	93	89	0.3	2.6	0.5	1.1	3	6 ☽	0	S 3	S 5	S 4
6	104.3	101.5	101.6	102.5	-0.1	7.0	4.2	3.8	8.3	-0.6	96	71	97	88	0.3	2.9	0.2	1.1	4	4	10 ●	SSE 2	S 6	SSW 5
7	104.5	103.3	106.0	103.3	5.5	8.4	4.9	5.9	9.4	3.8	95	68	78	80	0.4	3.6	2.0	2.0	9	6 ☽	4	W 5	WSW 8	WSW 6
8	101.3	96.7	92.1	96.7	1.2	6.3	5.9	4.8	6.9	-0.2	92	85	91	89	0.5	1.4	0.9	0.9	7	10	10	SSE 4	S 5	SSW 5
9	90.6	90.3	94.2	91.7	6.5	7.6	4.5	5.8	8.4	4.0	91	89	81	87	0.9	1.2	1.6	1.2	9	10	1	SW 6	WSW 6	WSW 7
10	96.0	96.1	95.4	95.8	0.7	6.6	2.7	3.2	6.8	0.1	92	71	96	87	0.5	2.8	0.1	1.1	0	9	8 ≡	WSW 5	SW 2	SSE 2
11	96.3	100.7	102.9	100.0	4.9	4.2	2.1	3.3	5.9	0.7	97	85	85	89	0.3	1.2	1.0	0.8	10 ●	9	9	WSW 5	W 7	SW 5
12	100.4	96.5	93.8	96.9	0.3	6.9	4.4	4.0	8.3	-0.8	96	71	87	85	0.2	2.8	1.1	1.4	7	9	10	SSE 3	S 7	SW 5
13	89.9	85.4	76.8	84.0	2.1	8.3	6.2	5.7	9.1	1.6	89	58	82	76	0.8	4.6	1.7	2.4	6	9 ☽	10 ●	S 4	S 8	S 10
14	74.7	75.1	77.4	75.7	5.5	9.0	4.5	5.9	10.1	2.8	89	75	92	85	1.0	2.9	0.7	1.5	5	9	6	S 5	SW 9	SSW 5
15	77.5	75.6	72.4	75.2	2.7	6.4	4.8	4.7	6.8	1.7	91	70	94	85	0.6	2.8	0.6	1.3	5	9	9	SSW 5	SSE 4	SSW 5
16	80.2	84.3	89.4	84.6	3.5	4.5	0.4	2.2	5.1	-0.1	85	84	96	88	1.2	1.3	0.5	0.9	10	10	2	W 7	SW 5	SSW 4
17	93.6	94.8	94.3	94.2	0.6	5.1	3.1	3.0	5.3	-0.5	94	69	84	82	0.4	2.8	1.2	1.5	10	2	10	SW 7	S 5	SSW 7
18	95.4	91.7	86.7	91.3	-1.5	5.4	4.2	3.1	6.8	-1.8	96	71	93	87	0.3	2.7	0.5	1.2	3	9 ☽	10 ●	S 2	E 7	NE 4
19	90.4	96.9	100.8	96.0	2.1	3.0	-0.1	1.2	4.5	-0.7	91	76	94	87	0.6	1.9	0.4	1.0	10 ●	9	0	WNW 10	W 10	SSW 3
20	100.6	99.6	96.9	99.0	0.9	6.2	4.0	3.8	7.8	-2.0	87	67	74	76	0.9	3.1	2.1	2.0	10 ✳	8	10	SSE 3	S 6	SSE 4
21	96.1	97.8	102.7	98.9	0.2	7.4	2.2	3.0	7.7	-0.2	94	69	87	83	0.4	3.2	1.0	1.5	7	9	10	SSE 3	WSW 6	WNW 9
22	105.9	105.9	105.9	105.2	-0.4	3.1	-1.2	0.1	4.9	-2.2	98	76	98	91	0.1	1.8	0.1	0.7	10	8	4	W 4	WNW 4	C 0
23	103.3	103.9	102.8	103.3	-1.3	1.9	-2.2	-1.0	2.9	-3.0	94	73	87	85	0.4	1.9	0.7	1.0	10 ✳	9 ☽	0	W 3	NW 5	WSW 3
24	96.2	92.4	93.3	94.0	-2.7	2.5	-0.6	-0.4	3.1	-3.5	91	72	96	86	0.5	2.1	0.2	0.9	4	9	0	E 3	ESE 6	ENE 3
25	97.5	97.3	96.7	97.2	-2.1	-0.3	-0.9	-1.0	0.0	-3.2	89	84	96	90	0.3	1.0	0.2	0.6	10	9	3	E 2	E 3	ENE 4
26	103.9	107.1	109.7	106.7	-3.0	0.9	-2.5	-1.8	1.5	-5.0	98	77	89	88	0.1	1.5	0.6	0.7	10	9	0	WNW 3	C 0	C 0
27	111.2	113.0	113.0	113.1	-5.2	3.3	0.1	-0.4	4.1	-6.4	93	53	76	74	0.3	3.6	1.5	1.8	4	6	7	E 1	E 3	SE 3
28	118.3	121.8	124.3	121.5	-0.9	0.4	-1.5	-0.9	0.7	-1.9	96	76	94	89	0.2	1.5	0.3	0.7	10	10 ✳	2	SE 1	NNW 9	N 4
29																								
30																								
31																								
M	99.3	99.4	99.4	99.4	1.3	5.2	2.4	2.8	6.2	-0.6	93	76	90	86	0.5	2.1	0.7	1.1	7.6	8.4	5.9	3.7	5.4	4.3

Poznań – Ławica $H_s = 86\ m$ $H_b = 92{,}1\ m$ $h_w = 13\ m$ Styczeń – Janvier 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	10	–	= 0⁰⁰–6²⁰ ≡⁰–6³⁰ ≡¹–9⁴⁵ =–24; V n–24
2	5	0.0	10	–	= 0⁰⁰–24
3	4	1.6	5	–	•⁰4⁴⁵–6⁰⁰ ✶⁰10³⁰–11³⁰ ✶¹–13³⁵ ✶⁰–14¹⁵; ≡²7⁵⁰–9⁰⁰ 14¹⁵–22⁴⁰ =–24
4	5	0.0	4	–	= 0⁰⁰–24 ⌴² 4⁰⁰–10⁰⁰
5	4	4.4	3	–	•⁰3³⁰–4²⁰ •⁰9²⁵–18¹⁰ = 0⁰⁰–4⁴⁵ ≡⁰–6³⁵ =–7⁴⁰ ≡⁰–8⁴⁵ =–24
6	6	4.6	.	–	•⁰7²⁰–8¹⁵ •¹–9³⁰ •⁰–10²⁰ •¹–11¹⁰ •⁰–12²⁵
7	7	0.0	.	–	•⁰0²⁰ 3³⁵ 4⁴³–8³⁰ ▽–9¹⁵
8	6	0.0	.	–	•⁰17⁵⁰–18³⁰ •¹–19¹⁰ •⁰–20²⁵ 22⁴⁵–24; = 7³⁰–17⁵⁰ 20²⁵–22⁴⁵
9	6	0.3	.	–	•¹0⁰⁰–2³⁰ •⁰–4²⁵ = 4²⁵–24
10	7	0.0	.	–	•⁰5²⁰–6³⁵ ▽18⁰⁶–10 = 0⁰⁰–7¹⁵
11	7	0.0	.	–	•⁰7⁴³ 8¹⁰ (marznący)
12	5	2.7	.	–	✶⁰6⁴⁰–16⁰⁰ 17⁴⁰–22⁰⁸ ✶¹2³⁰⁵–24
13	5	2.2	.	–	✶¹0⁰⁰–30 •¹1²⁵–7²⁵ •¹10²⁰–11²⁵ •⁰ 13¹⁵ •¹ 18²⁰ ✶¹–24; = 7²⁵–8¹⁵ ≡²–8³⁵ =–10²⁰
14	6	0.2	2	–	✶⁰0⁰⁰–5²⁰ 7²⁰–12³⁵ ✶✶ 2³⁵–5²⁰; = 5²⁰–24
15	6	0.0	2	–	✶⁰9³⁰–14⁴⁰ 15¹⁵–24; = 0⁰⁰–24
16	6	.	6	–	✶⁰0⁰⁰–30 = 0³⁰–7¹⁰ ≡¹–7⁴⁰ =–8²⁵ ≡–9¹⁰ =–17⁵⁰ ≡–19²⁵ =–24
17	5	.	5	–	= 0⁰⁰–15⁴⁰ ≡⁰–24
18	3	.	4	–	≡⁰0⁰⁰–25²⁰ =–24; V² na–24
19	4	.	4	–	= 0⁰⁰–24; V² 0⁰⁰–24
20	6	.	2	–	= 0⁰⁰–24; V² 0⁰⁰–24
21	6	.	2	–	= 0⁰⁰–11⁰⁰ ∞–16⁰⁰ =–24
22	6	.	2	–	= 0⁰⁰–10³⁰ ∞–17¹⁵ =–24
23	6	.	1	–	= 0⁰⁰–11³⁰ ∞–15⁴⁰ =–24
24	5	0.0	.	–	✶⁰23²⁰–24; = 0⁰⁰–24
25	5	0.0	1	–	✶⁰0⁰⁰–1³⁵; 3¹⁰–6²⁸; 13⁴⁵–14¹⁰; = 0⁰⁰–15⁴⁰ ≡⁰–18⁵⁰ =–24
26	5	2.0	.	–	= 0⁰⁰–7⁴⁵ ≡⁰–10¹⁵ =–12³⁰ ∞–15⁴⁰ =–24
27	6	1.8	.	–	•⁰1³⁵–4⁴⁰ •⁰8¹⁵–25 = 0⁰⁰–15³⁰
28	6	0.8	1	–	✶3⁴⁰–6⁴⁵ •⁰7⁵⁰–8²⁵ 12⁴⁰–15²⁰; = 6⁴⁵–24; ⌴⁰ 21³⁰–24
29	6	.	.	–	= 0⁰⁰–24 ⌴¹ 0⁰⁰–10⁵⁰
30	5	0.5	.	–	•⁰17¹⁵–19²⁰; = 0⁰⁰–22⁴⁰ ≡⁰–23²⁰ ≡²–24; ⌴¹2⁰⁰–11⁰⁰
31	1	3.4	.	–	•⁰12¹⁰–20 •⁰17⁴⁰–24; ≡² 0⁰⁰–16³⁰ =–24
Σ	–	24.5	–	–	UWAGI

Luty – Février

1	5	3.2	.	–	•⁰0⁰⁰–4³⁰ 7³⁰–10³⁵ 11⁰⁸–17²⁰ •¹–18¹² •⁰–20²⁰ •¹–21¹⁵ •⁰–23¹⁸; = 0⁰⁰–24
2	6	2.1	.	–	•¹21³⁰–24; = 0⁰⁰–19¹⁵ ≡²–24
3	4	1.3	.	–	•⁰0⁰⁰–2⁴⁰ •¹–7¹⁵ •⁰7³⁰–10³⁵ ••⁰11²⁰–12¹⁵ •⁰–13²⁹; ≡²0⁰⁰–4⁴⁵ =7¹⁵⁻⁴⁰ ≡²–9³⁰ =–21²⁵ ≡¹–24
4	5	6.8	.	–	•⁰6⁴³–11¹⁰; ≡¹ 0⁰⁰–4⁴⁰ ≡⁰–9¹⁵ =–24
5	3	.	.	–	= 0⁰⁰–24; ⌴¹ 3⁰⁰–8²⁰ ⌴⁰ np.
6	6	1.1	.	–	•⁰19⁴⁵–20¹⁵ •⁰–23¹⁰; = 0⁰⁰–19⁴⁵, 23¹⁰–24; ⌴⁰ 0⁰⁰–9⁰⁰
7	7	.	.	–	•⁰1¹⁰–4³⁰ = 0⁰⁰–11³⁰
8	6	5.3	.	–	•⁰13⁴⁰–24; = 0⁰⁰–24 ⌴⁰ 1⁰⁰–6⁰⁰
9	6	0.4	.	–	•⁰0⁰⁰–3³⁵ 10⁴⁰⁻⁵⁰ 11¹⁵–12¹⁸
10	6	2.5	.	–	•⁰14⁵⁰–20⁵⁰ 23¹⁵–24; = 6⁴⁰–11²⁰ ∞–13³⁰ =–14⁵⁰ ≡¹20⁵⁰–22³⁰ =–23¹⁵; ⌴⁰ na
11	6	0.8	.	–	•⁰0⁰⁰–2²⁰ 6³⁰–7⁴⁰ 8³⁵–12⁰⁵; = 2²⁰–6³⁰
12	6	0.0	.	–	•⁰18³⁵–22⁴⁰; = 3³⁰–24; ⌴⁰ 3⁰⁰–7⁰⁰
13	7	3.9	.	–	•⁰19³⁰–20¹⁰ •¹–22²⁰ •⁰–23³⁵ •¹–24; = 0⁰⁰–9²⁰
14	7	0.7	.	–	•¹0⁰⁰–42 •⁰–2⁵⁰ •¹–4³⁷ •⁰–5¹⁸ ▽7⁵⁰–8⁰⁵; 16⁵⁰–17⁰⁵
15	7	2.8	.	–	•⁰14²⁰–16²⁵; 22²⁰–24; = 16²⁵–22²⁰
16	6	1.6	.	–	•⁰0⁰⁰–2²⁰ •¹–4³⁰ •⁰13³⁰–16²⁵; = 4³⁰–24
17	7	0.0	.	–	•⁰16¹⁵–18⁴⁰; = 0⁰⁰–12³⁰; 15²⁰–24 ⌴⁰ na
18	6	10.0	.	–	•⁰16⁴⁶–24; = 0⁰⁰–14²⁰; 15³⁵–16⁴⁶
19	6	0.0	.	–	•¹0⁰⁰–2⁴⁰ •⁰–7²²
20	7	0.3	.	–	✶⁰6⁵⁰–9²⁰ = 17³⁰–24; ⊕ 12⁴⁰–15⁴⁰
21	6	0.0	.	–	•⁰16⁰⁵–20 19¹⁵–24; = 0⁰⁰–13²⁰ 16²⁰–19¹⁵; ⌴⁰ 5³⁰–7²⁰
22	7	.	.	–	= 0⁰⁰–9³⁰ 17⁴⁰–20¹⁵ ⌴⁰ 3⁰⁰–9²⁰
23	6	0.0	.	–	✶⁰6⁵⁰–7⁴⁰; ⌴¹ 21²⁰–24
24	5	.	.	–	= 2⁴⁰–24; ⌴⁰ 0⁰⁰–10¹⁰
25	6	.	.	–	= 0⁰⁰–24
26	6	.	.	–	= 0⁰⁰–24 ⌴¹ 4⁰⁰–10⁰⁰
27	7	.	.	–	= 0⁰⁰–11³⁰ 15⁵⁰–18²⁰ ∞–21³⁰ ⌴¹ 3²⁰–10⁰⁰
28	6	0.2	.	–	✶⁰10⁴⁰–11²⁰, 12²²–15⁵⁰ 16⁵⁵–17¹⁰, 23³⁵–24; = 6¹⁵–24
29					
30					
31					
Σ	–	45.2	.	–	UWAGI

Poznań – Ławica

$\varphi = 52°25'$ $\lambda = 16°50'$

Marzec – Mars 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	126.2	125.9	124.9	125.7	−2.4	1.5	−2.4	−1.4	2.6	−2.9	96	58	85	80	0.2	2.9	0.8	1.3	5	6	0	N 5	N 5	N 2
2	123.3	122.0	118.2	121.2	−6.5	0.7	−2.6	−2.8	2.2	−6.9	91	63	87	80	0.3	2.3	0.7	1.1	3	7	0	NNW 3	NW 4	WNW 3
3	114.6	113.1	109.7	112.5	−6.6	1.1	−2.5	−2.6	3.4	−7.4	91	64	89	81	0.3	2.3	0.6	1.1	2	6	0	NW 3	C 0	SE 1
4	103.9	101.0	99.9	101.6	−3.1	2.8	2.1	1.0	4.7	−4.5	90	62	93	82	0.5	2.9	0.5	1.3	7	10	10	SSE 4	S 3	W 6
5	102.8	104.5	104.7	104.0	−3.1	0.2	−2.9	−2.2	5.1	−4.5	88	88	84	87	0.6	0.7	0.8	0.7	6	6 ⊙	0	W 4	NNW 4	C 0
6	104.2	103.2	102.4	103.3	−5.5	6.3	−0.6	−0.1	6.7	−6.0	92	52	79	74	0.3	4.3	1.2	2.0	0 ⊙	0 ⊙	0	SSE 2	SE 3	ENE 4
7	102.3	102.9	104.0	103.1	−3.0	3.7	−1.6	−0.6	4.2	−3.5	88	65	75	76	0.6	2.8	1.3	1.6	0	3	0	E 3	E 6	E 5
8	105.2	106.5	109.6	107.1	−3.6	2.6	−1.3	−0.9	3.7	−4.6	76	55	74	68	1.1	3.4	1.4	2.0	2	0 ⊙	0	E 6	ESE 6	E 7
9	114.5	116.9	119.4	116.9	−3.7	2.9	−1.5	−1.0	3.7	−4.3	76	66	83	75	1.1	2.6	1.0	1.6	1	0	0	E 6	ESE 8	C 0
10	121.6	122.3	122.5	122.1	−4.7	4.8	0.3	0.3	5.6	−5.8	88	49	79	72	0.5	4.4	1.3	2.1	0	0	0	E 2	E 5	E 3
11	122.4	121.4	118.8	120.9	−5.1	8.4	0.8	1.2	10.2	−5.6	90	41	85	72	0.4	6.5	1.0	2.6	0	2 ⊙	0	SE 2	ESE 4	SE 3
12	115.0	112.0	108.8	111.9	−2.5	12.1	3.3	4.0	15.1	−3.4	89	35	71	65	0.6	9.2	2.2	4.0	9	4	0	SE 2	SW 3	W 2
13	108.3	108.5	105.2	107.3	−0.8	14.9	5.8	6.4	16.9	−1.8	89	30	71	63	0.6	11.8	2.6	5.0	10	0	3	W 1	WSW 3	SW 3
14	100.5	99.3	98.7	99.5	3.2	12.4	8.9	8.4	13.9	2.0	86	73	68	76	1.1	3.9	3.6	2.9	0	8	7	SW 6	W 11	W 11
15	99.8	99.6	91.7	96.8	7.7	9.6	10.0	9.3	10.1	7.1	76	69	81	75	2.3	3.8	2.4	2.9	10	10 ●	10	W 9	WSW 10	W 18
16	95.1	99.6	106.4	100.4	1.1	2.7	−3.1	−0.6	10.0	−3.3	85	60	72	72	1.0	2.9	1.3	1.7	9	9	10	NW 6	NW 7	ENE 5
17	104.0	100.1	90.2	98.1	−3.3	−2.6	2.6	−0.2	2.8	−4.2	65	91	100	85	1.7	0.5	0.0	0.7	10	10 ●	10 ●	ESE 5	ESE 8	SW 6
18	83.2	84.7	90.3	86.1	8.9	11.6	5.5	7.9	13.0	2.1	99	58	88	82	0.2	5.7	1.1	2.3	9	9	2	WSW 9	W 12	W 7
19	96.4	97.6	97.4	97.1	4.5	8.6	6.3	6.4	9.1	4.0	89	70	97	85	0.9	3.3	0.2	1.5	8	10	10 ●	WSW 4	W 8	C 0
20	99.0	96.9	94.1	96.7	6.1	12.4	8.0	8.6	13.1	5.0	98	87	90	92	0.1	1.9	1.0	1.0	10	10	0	ESE 1	S 5	SSW 3
21	98.0	100.4	101.4	99.9	7.2	12.6	7.5	8.7	13.8	5.5	87	46	77	70	1.4	7.8	2.4	3.9	0	7	0	SW 5	W 10	WSW 3
22	104.1	105.9	107.7	105.9	3.1	10.8	2.6	4.8	10.9	1.2	86	37	89	71	1.0	8.2	0.8	3.3	2	6	0	WSW 4	WNW 9	C 0
23	108.3	108.2	110.3	108.9	−0.1	11.1	3.0	4.2	12.0	−1.5	92	44	86	74	0.5	7.3	1.1	3.0	2	5	0	ENE 3	E 3	ENE 13
24	113.2	113.1	112.5	112.9	−0.1	2.8	2.5	1.9	3.9	−0.6	90	60	65	72	0.7	3.0	2.6	2.1	10	10	8	E 12	E 13	ESE 9
25	111.8	111.9	111.6	111.8	0.9	4.3	3.5	3.0	6.5	0.4	85	77	83	82	1.0	1.9	1.3	1.4	10	9	0	E 8	ESE 6	ESE 7
26	110.4	108.5	108.5	109.1	2.1	14.9	9.4	9.0	16.4	1.0	85	50	61	65	1.0	8.5	4.6	4.7	10	4	0	ESE 4	SSE 7	SE 5
27	109.5	109.9	108.8	109.4	5.0	15.2	8.4	9.2	15.9	2.5	57	29	58	48	3.8	12.3	4.6	6.9	9	2 ⊙	2	SSE 5	S 10	SSE 4
28	105.5	105.2	103.7	104.8	5.9	7.6	6.2	6.5	9.4	4.6	52	82	94	76	4.4	1.9	0.6	2.3	9	10	10	S 8	S 4	S 2
29	102.5	103.2	105.0	103.6	4.6	8.1	5.9	6.1	9.5	4.2	97	81	88	89	0.3	2.1	1.2	1.2	9	8	10	WNW 3	N 5	NE 2
30	106.9	107.8	109.1	107.9	6.1	12.4	8.9	9.1	13.9	4.5	94	53	76	74	0.6	6.7	2.8	3.4	10	7	0	NE 3	ENE 12	NE 5
31	109.6	111.5	112.5	111.2	4.3	12.0	7.9	8.0	14.6	3.2	87	66	79	77	1.1	4.8	2.2	2.7	4	6	0	E 5	ESE 3	NNW 2
M	107.2	107.2	106.7	107.0	0.5	7.4	3.3	3.6	9.1	−0.8	86	60	81	76	1.0	4.6	1.6	2.4	5.7	6.0	3.0	4.7	6.4	4.6

Kwiecień – Avril

1	111.5	110.4	109.1	110.3	4.6	16.5	10.3	10.5	17.8	2.6	81	36	35	57	1.7	12.0	5.8	6.5	0	1	1	NE 5	E 7	ENE 8
2	108.2	108.0	109.6	108.6	6.2	17.0	7.9	9.8	17.4	3.3	73	44	85	67	2.6	10.9	1.6	5.0	4	7	0	E 6	ESE 5	NW 2
3	112.4	114.6	116.4	114.5	6.9	17.7	13.1	12.7	18.6	4.8	92	46	56	65	0.7	8.9	6.4	5.3	6	8 ⊙	2	E 1	N 4	NNE 2
4	118.9	118.8	118.3	118.7	7.0	19.7	12.1	12.7	20.7	4.3	81	34	61	59	1.9	15.0	5.6	7.5	0 ⊙	2 ⊙	0	E 3	N 2	ENE 2
5	117.2	115.0	109.0	113.7	5.6	19.4	9.9	11.2	20.4	2.2	85	25	57	56	1.4	16.9	5.2	7.8	0 ⊙	0	0	C 0	W 1	C 0
6	103.1	99.5	99.5	100.7	6.1	19.8	7.8	10.4	20.7	3.6	73	29	83	62	2.5	16.3	1.8	6.9	2	6 ⊙	6	SE 1	SSW 4	WNW 7
7	100.3	102.1	106.1	103.5	4.0	5.3	2.2	3.4	8.1	1.5	93	92	52	79	0.5	0.7	3.5	1.6	10	10 ●	8	NW 5	N 5	N 7
8	111.0	109.3	106.7	109.0	−1.7	5.3	3.4	2.6	8.4	−4.6	84	38	63	62	0.9	5.5	2.9	3.1	3	4	6	NNW 6	NW 7	WNW 5
9	103.4	102.7	101.5	102.5	2.4	5.7	3.2	3.6	7.9	−1.3	72	68	76	72	2.1	3.0	1.9	2.3	8	10	8	W 6	N 3	ENE 3
10	97.7	92.7	86.5	92.3	−0.2	12.0	9.4	7.6	14.3	−2.9	84	41	56	60	1.0	8.3	5.2	4.8	4 ⊙	6 ⊙	9	SSE 2	SW 6	WSW 3
11	84.9	86.2	92.6	87.9	4.4	5.4	1.3	3.1	9.5	1.3	57	51	85	64	3.6	4.4	1.0	3.0	6 ⊙	9	10	W 7	WNW 9	NNW 4
12	98.2	99.5	101.9	99.9	0.7	2.8	−1.1	0.3	5.5	−1.5	75	74	73	74	1.6	2.0	1.5	1.7	9 ✳	10 ✳	0	N 3	WNW 5	N 1
13	102.2	103.3	106.2	103.9	−1.6	4.2	−2.0	−0.4	6.4	−5.1	88	47	80	72	0.6	4.3	1.1	2.0	9	7	2	SW 1	WNW 5	N 3
14	108.3	107.6	108.3	108.1	−2.0	6.1	1.4	1.7	8.3	−6.2	92	31	79	67	0.5	6.5	1.4	2.8	1	7	7	C 0	WSW 4	NE 2
15	110.5	111.2	112.2	111.3	−1.7	5.8	4.1	3.1	7.8	−3.2	96	37	47	60	0.2	5.8	4.4	3.5	10	9 ⊙	8	NNE 6	N 4	NW 1
16	112.2	110.0	108.5	110.2	1.1	10.8	10.3	8.1	13.3	−1.6	72	53	60	62	1.9	6.2	5.0	4.4	10	6	10	S 1	SW 7	W 7
17	109.6	110.3	110.8	110.2	6.1	9.2	6.2	6.9	11.5	4.6	91	66	85	81	0.8	3.9	1.5	2.1	10	9	9	NW 6	WNW 7	WNW 4
18	110.2	109.1	107.2	108.8	2.7	5.4	4.4	4.2	6.9	2.0	74	66	80	73	1.9	3.1	1.7	2.2	10	10	7	N 6	N 5	NW 4
19	104.4	102.1	102.9	103.1	3.5	9.9	5.9	6.3	10.5	0.2	93	47	92	77	0.5	6.5	0.7	2.6	7	10	10	C 0	SW 3	C 0
20	108.7	112.1	114.6	111.8	5.1	8.4	3.1	4.9	9.8	2.5	90	62	86	79	0.9	4.1	1.0	2.0	9	9	0	NW 6	NNW 6	N 2
21	117.0	117.9	118.4	117.8	2.2	7.2	3.0	3.8	9.2	−2.9	96	63	76	78	0.3	3.8	1.9	2.0	10	9	4	NNW 1	N 5	NNE 2
22	120.3	120.4	120.1	120.3	2.8	9.9	3.9	5.1	11.4	−3.1	84	62	93	80	1.2	4.6	0.6	2.1	5	9	0	NE 2	NE 4	E 2
23	119.9	119.1	119.5	119.5	2.5	12.2	7.6	7.5	14.3	0.4	96	51	84	77	0.3	7.0	1.6	3.0	10 ≡	0	0	NNW 2	NE 5	NE 2
24	118.7	118.1	116.8	117.9	4.7	13.3	11.4	10.2	14.5	3.0	90	56	77	74	0.8	6.8	3.1	3.6	4	9 ⊙	10 ●	N 4	NNE 5	NE 3
25	113.9	112.9	112.4	113.1	6.1	12.5	8.6	9.0	13.1	5.3	80	62	76	73	1.8	5.5	2.8	3.4	10 ●	8	9	N 6	NNE 9	NE 7
26	111.8	110.9	110.0	110.9	6.4	15.1	13.4	12.1	18.0	5.6	92	58	78	76	0.7	7.2	3.3	3.7	10 ●	9	4	NE 5	NE 6	ENE 2
27	108.0	106.5	103.0	106.0	9.5	17.1	12.1	12.7	17.7	7.7	84	59	87	77	1.9	8.0	1.8	3.9	4 ⊙	10	0	NE 2	W 2	N 1
28	101.0	99.3	97.6	99.3	11.8	23.8	16.4	17.1	24.7	6.0	91	32	59	61	1.1	20.0	7.6	9.6	2	4	1	E 3	SSE 4	C 0
29	99..	100.6	100.6	100.2	11.4	22.1	14.7	15.7	23.6	8.3	89	46	55	63	1.3	14.2	7.3	7.7	5	6	0	W 3	W 6	NW 4
30	99.2	97.2	103.2	99.9	12.9	20.4	7.2	11.9	20.8	6.7	68	47	78	71	1.8	12.8	2.2	5.6	0	9	2	NNE 3	N 8	NW 4
31																								
M	108.1	107.6	107.7	107.8	4.3	12.0	7.0	7.6	13.7	1.4	83	51	73	70	1.3	7.8	3.1	4.1	5.9	7.1	4.4	3.5	5.1	3.1

Poznań – Ławica $H_s = 86\ m$ $H_b = 92{,}1\ m$ $h_w = 13\ m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	–	✳⁰ 0⁰⁰–15 13⁶ 2¹⁰ 2¹⁵–5²⁵ · = 0⁰⁰–8²⁰
2	7	.	.	–	= 4²⁰–11²⁰ · 18²⁰–24 · ⌴¹ 0⁰⁰–10³⁰
3	6	.	.	–	= 0⁰⁰–9³⁰ ∞–19⁰⁰ =–24 · ⌴² 0⁰⁰–9³⁰
4	6	0.0	.	–	●⁰ 19⁴⁵–20¹⁰ · = 0⁰⁰–9³⁰ ∞–16⁴⁰ =–24 · ⌴¹ 2³⁰–7¹⁰
5	6	.	.	–	= 0⁰⁰–8¹⁰ ≡⁰–8²⁰ ≡¹–10³⁰ ≡⁰–11²⁰ =– 13¹⁵ 20³⁰–24 · ⌴¹ 1⁴⁰–11⁵⁰
6	6	.	.	–	= 0⁰⁰–9⁴⁰ ∞– 15³⁰ = 17³⁰–24 · ⌴¹ 1⁴⁰–8²⁰
7	7	.	.	–	= 0⁰⁰–10²⁰ 17²⁰–24 · ⊕ 17¹⁵–35
8	7	.	.	–	= 0⁰⁰–7³⁰ ∞ 17³⁰– 19¹⁰ =–20³⁰ · ⌴¹ 3³⁰–7⁰⁰
9	7	.	.	–	∞ 17³⁰– 18⁴⁰ =–24 · ⌴¹ 4²⁰–7³⁰ 21⁰⁰–23⁰⁰
10	6	.	.	–	= 0⁰⁰– 11⁰⁰ ∞– 19³⁰ · ⌴¹ 0⁰⁰–9⁰⁰
11	7	.	.	–	= 3³⁰–9³⁰ ∞ 17²⁰– 20⁴⁰ =–24 · ⌴¹ 2³⁰–9⁰⁵
12	6	.	.	–	= 0⁰⁰–9³⁰ ∞⁰– 13²⁰ · 19³⁵–24 · ⌴⁰ 2³⁰–8³⁰ · ⊽ 18¹⁵–40
13	6	.	.	–	= 0⁰⁰–9³⁰ ∞–23²⁰ =–24 · ⌴¹ 0⁰⁰–8⁰⁰
14	6	0.0	.	–	●⁰ 12⁴⁰–50 · = 0⁰⁰–7³⁰ ∞ 8³⁰–21²⁰ ⌴⁰ 4⁴⁰–7¹⁵
15	7	6.7	.	–	●⁰ 11¹⁴– 16³² ●¹–17²⁵ ●⁰ 18⁰⁸ · 21¹⁵–23²⁰ · ⫽ 20¹⁰–22⁴⁰
16	7	.	.	–	●¹ 0¹⁰– 13⁵ ●⁰– 4⁴³
17	6	10.1	.	–	✳⁰ 8⁰⁴ 9¹⁵ ✳¹– 10³⁵ ✳⁰– 12²⁰ ●⁰–14³⁰ ●⁰–16²⁵ ●⁰–20¹⁵ ●⁰–23³⁰ ●⁰–24
18	7	4.1	.	–	●⁰ 0⁰⁰–4²⁰ ●¹–5⁴⁰ ●⁰–6²⁰ ▽ 7⁴⁰–8¹⁰ · 13¹⁰–25 · 15⁴⁵–16²² · 16³⁵–17²⁸ · 18³⁵–19¹⁰ · 22³⁸–50
19	7	2.5	.	–	●⁰ 14⁵⁴–21³⁰ · = 21³⁰–24
20	6	0.0	.	–	●⁰ 7³⁰–9²⁵ ●⁰ 15¹⁰–35 · = 0⁰⁰–1⁴⁰ ≡⁰–4⁴⁵ =–7³⁰ ≡⁰ 7⁵⁵–9³⁰ ≡¹–10³⁸ ≡⁰–11³⁰ =–20²²
21	7	.	.	–	
22	7	.	.	–	= 5³⁰–8³⁰
23	7	.	.	–	⫸ 19²⁰–24 · = 1²⁰–8³⁰ ∞–9¹⁵ · 18³⁰–19²⁰ · ⌴² 0⁰⁰–7¹⁵ · ⊕ 12⁴⁰–14⁰⁰
24	7	0.0	.	–	●¹ 17⁴⁰–50 · ⫸ 0⁰⁰–17¹⁵
25	7	.	.	–	●⁰ 3⁴⁵–4⁴⁰
26	7	.	.	–	= 5³⁰–10⁴⁰
27	7	.	.	–	
28	7	6.7	.	–	●⁰ 10¹⁰–12²⁵ · 14⁰⁰–16⁰⁵ · = 18¹⁵–24
29	7	0.9	.	–	●⁰ 2³⁵–6¹⁰ · = 0⁰⁰–11¹⁰
30	7	.	.	–	●⁰ 1³⁰–3³⁰
31	6	.	.	–	= 6⁴⁰–12²⁰ ∞–13³⁰ = 19³⁰–24 · ⌓¹ na
Σ	–	31.0	–	–	UWAGI.

Kwiecień – Avril

1	7	.	.	–	= 0⁰⁰–8³⁰ ∞–10²⁵
2	7	0.0	.	–	●⁰ 17⁴⁵–18³⁵ · = 4²⁰–8³⁰ ∞–12⁴⁰
3	7	.	.	–	= 2²⁰–9³⁰ ∞–12²⁰ · 18⁴⁰–20³⁰
4	7	.	.	–	= 4¹⁵–8²⁰ ∞–10³⁰ · ⌓¹ n,a
5	7	.	.	–	= 4³⁰–7⁴⁰ ∞–9³⁰ · ⌓¹ n,a
6	7	.	.	–	∞ 6¹⁰–9²⁰
7	6	1.1	.	–	●¹ 11³⁸–14⁴⁰ ▽¹ 16⁴⁰–17³⁵ · = 6²⁵–11³⁸
8	8	.	.	–	⌴² n,a · ⊽ 21³⁰–22¹⁰
9	8	.	.	–	
10	7	.	.	–	= 4⁴⁰–7³⁰ · ⌴⁰ na
11	8	.	.	–	
12	7	0.3	.	–	✳ ▽ 6⁵⁰–7³⁵ 10³⁴–55 11¹¹–28 11⁴⁶–12⁰⁸ 12³³–13¹² 14¹⁴–50
13	7	0.2	.	–	✳ ▽ 8¹⁰–45 9²⁰–10⁴⁵ · = 2⁴⁰–8¹⁰ · 10⁴⁵–11¹⁰ · ⌴¹ 1²⁰–8⁴⁰
14	8	.	.	–	⌴² 4³⁰–7²⁵
15	8	0.0	.	–	✳ ▽ 13⁴³–14⁰⁸ · 16²⁵–32 · = 6⁵⁰–7³⁰
16	7	2.6	.	–	△ 8³⁰–9²⁵ · 9⁴⁰–10⁰⁰ ●¹ 22²⁰–24 · = 4³⁰–12⁴⁰
17	7	.	.	–	●⁰ 0⁰⁰–2⁴⁰
18	7	.	.	–	
19	7	1.0	.	–	●⁰ 14⁴⁰–21²⁰ · 23³⁰–24 · = 4³⁰–7³⁰ · 21²⁰–24
20	7	.	.	–	●¹ 0⁰⁰–2²⁰ · = 0⁰⁰–6³⁰ 19²⁵–24
21	7	.	.	–	= 0⁰⁰–2³⁵ ≡⁰–2⁴⁰ ≡¹–6²⁰ ≡⁰–6⁴⁰ =–9²⁰ · 20³⁰–24 · ⌴ 1⁴⁰–5³⁰
22	7	.	.	–	= 0⁰⁰–5⁰⁰ ≡²–6²⁰ =– 11⁰⁰ · ⌴² 2³⁰–7²⁰
23	7	.	.	–	= 4¹⁵–5²⁰ ≡²–8⁰⁰ =–9⁴⁰
24	7	1.1	.	–	●⁰ 20³⁶–22³⁰ 23²⁰–24 · = 5⁴⁰–7³⁰
25	7	0.3	.	–	●¹ 0⁰⁰–10 12⁶–7¹⁵ ▽ 14¹⁰–20 ●⁰ 22²⁰–24 · = 19³⁵–22²⁰
26	7	(0.0)	.	–	● 0⁰⁰ 3⁴⁰ ●⁰ 6³⁵–7⁴⁰ = 3⁴⁰–6³⁵ · 7⁴⁰–10⁵⁰ ∞–12²⁵ · 19²⁰–20³⁰ =–24
27	5	.	.	–	= 0⁰⁰–10³⁰ ∞–15⁰⁰
28	7	.	.	–	= 3²⁰–8⁴⁰ ∞–11³⁰ · ⌓¹ n,a
29	7	2.1	.	–	∞ 19¹⁵–23³⁰ =–24
30	6	0.0	.	–	▽ 2⁴⁰–3²⁰ ●⁰ 15³⁰–40 · (Ⓩ)¹ 0⁰⁰–2³⁰ SW–S; = 0⁰⁰–2⁴⁰ · 3²⁰–18³⁰
31					
Σ	–	8.7	–	–	UWAGI.

Poznań – Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ **Maj – Mai 1957**

DNI.	CIŚNIENIE P – 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	108.0	108.3	108.0	108.1	5.6	11.2	9.4	8.9	12.9	0.3	72	33	61	55	2.5	8.9	4.6	5.3	3 ⊙	8	8	W 4	NW 5	NE 1
2	107.7	105.7	105.7	105.7	7.1	14.3	7.7	9.2	14.9	1.8	62	30	57	50	3.9	11.3	4.3	6.6	9	8	5	SSE 2	ESE 2	SE 1
3	102.7	101.2	99.4	101.1	7.4	14.8	8.1	9.6	16.5	5.2	73	39	75	62	2.8	10.2	2.7	5.2	9	9 ⊙	0	SE 1	S 3	W 5
4	98.0	100.3	101.5	99.9	7.5	9.3	4.8	6.6	10.8	3.9	63	36	61	53	3.9	7.5	3.4	4.9	9	8	5	WNW 10	W 13	W 6
5	101.5	100.3	99.6	100.5	3.5	7.6	3.2	4.4	9.6	0.5	65	44	90	66	2.7	5.8	0.8	3.1	6 ⊙	7 ⊙	10	WSW 10	WSW 10	C 0
6	99.4	99.3	98.8	99.2	0.4	2.4	2.7	2.0	3.8	−0.2	98	86	93	92	0.1	1.1	0.5	0.6	10 ✳	10 ●	9	NW 1	NW 7	C 0
7	98.5	98.0	98.4	98.3	2.0	7.7	5.0	4.9	10.4	−2.4	94	59	79	77	0.4	4.3	1.8	2.2	8	9	4	NNW 1	NW 3	NNW 2
8	98.6	98.6	99.6	98.9	4.0	5.1	4.7	4.6	7.1	1.9	69	63	76	69	2.5	3.3	2.0	2.6	9	10	9	N 8	NW 6	NW 2
9	102.0	102.6	102.9	102.5	3.6	8.5	6.6	6.3	9.9	−1.0	85	56	96	79	1.2	4.9	0.4	2.2	9	10	10 ●	N 2	NE 3	N 2
10	101.8	101.6	102.4	101.9	4.2	7.3	6.7	6.2	7.4	3.3	93	88	90	90	0.5	1.2	1.0	0.9	10	10 ●	10	NNW 5	NNW 8	NW 9
11	103.3	104.2	103.7	103.7	3.3	11.9	10.7	9.7	16.1	3.0	97	55	76	76	0.3	6.3	3.1	3.2	10 ●	4 ⊙	0	W 4	WSW 2	ESE 3
12	103.9	103.7	104.6	104.1	9.3	21.0	15.6	15.4	23.1	3.3	78	36	66	60	2.7	15.9	6.0	8.2	3 ⊙	6 ⊙	8	ESE 3	SE 4	SSE 3
13	106.6	106.4	107.0	106.7	14.3	23.3	13.6	16.2	24.4	8.1	78	35	97	70	3.6	18.7	0.6	7.6	4	7	10 ●ₖ	C 0	SW 4	W 8
14	108.4	109.1	110.1	109.2	13.3	18.4	13.1	14.5	21.3	8.9	88	61	86	78	1.8	8.4	2.1	4.1	3 ⊙	8	0	W 2	SW 3	NW 2
15	112.4	111.8	109.8	111.3	12.4	20.4	16.2	16.3	21.9	4.9	88	44	65	66	1.7	13.3	6.3	7.2	1	1 ⊙	0	S 1	E 1	E 3
16	108.1	105.0	103.3	105.5	15.0	24.2	18.3	19.0	25.1	10.3	63	45	78	62	6.2	16.8	4.6	9.2	0 ⊙	4 ⊙	4	ESE 3	ESE 8	ESE 4
17	103.8	107.3	108.7	107.3	12.6	17.7	11.4	13.3	18.4	9.6	85	75	71	77	2.2	5.1	3.9	3.7	8	9	6	NNW 8	NW 8	NNW 5
18	109.1	108.0	104.3	107.1	11.8	19.2	15.2	15.4	21.0	10.4	75	62	68	68	3.4	8.3	5.5	5.7	10	2	0	N 3	NE 1	ENE 3
19	101.4	98.4	96.1	98.6	14.6	25.4	19.5	19.8	26.3	10.4	74	46	66	62	4.3	17.4	7.7	9.8	0 ⊙	7 ⊙	8	ENE 4	ESE 2	NE 4
20	97.7	99.6	103.2	100.8	15.7	21.3	11.6	15.0	22.4	10.7	82	58	77	72	3.2	10.5	3.1	5.6	5 ⊙	8	8	NNW 8	NW 10	NNW 10
21	108.0	107.4	106.3	107.3	8.7	14.6	13.3	12.5	17.0	6.7	93	39	50	61	0.7	10.0	7.7	6.1	6 ⊙	8	9	NW 6	NNW 4	N 3
22	106.2	105.4	105.0	105.5	10.8	17.0	14.6	14.2	17.9	7.7	72	37	54	53	3.7	12.2	8.1	8.0	6	7	9	ENE 4	NE 7	E 3
23	103.6	102.1	101.1	102.3	11.6	20.3	14.7	15.4	22.1	10.2	61	53	80	65	5.3	11.4	3.3	6.7	9	8	4	NE 4	ENE 5	ENE 7
24	103.3	106.7	111.5	107.2	13.2	13.5	10.3	12.4	17.3	10.0	90	69	50	70	1.6	5.5	6.3	4.5	10	10	2	NE 6	NE 7	NE 7
25	114.8	115.4	117.6	115.9	7.9	13.0	6.8	8.6	14.1	3.9	60	41	50	50	4.2	8.9	4.9	6.0	0 ⊙	8 ⊙	0	NE 8	NNE 10	NE 5
26	117.8	117.4	117.3	117.5	5.7	9.9	6.9	7.4	11.1	1.5	74	38	57	56	2.4	7.5	4.2	4.7	0	9	4	NE 9	NNE 7	NE 5
27	116.3	116.0	114.4	115.6	4.9	9.9	6.6	7.0	11.4	−1.7	78	43	72	64	2.0	7.0	2.7	3.9	10	9	7	NE 6	NE 7	NE 2
28	113.3	112.0	110.9	112.1	6.1	11.9	7.1	8.0	14.4	−0.1	74	38	67	60	2.4	8.7	3.3	4.8	2	7	3	NE 4	N 6	NNE 4
29	111.5	111.3	111.8	111.5	8.3	15.2	9.7	10.7	17.2	0.0	70	40	82	64	3.3	10.4	2.2	5.3	2 ⊙	6 ⊙	3	ENE 3	NW 2	ENE 2
30	112.1	111.3	109.6	111.0	12.0	18.1	13.6	14.3	20.5	2.1	58	27	55	47	5.8	15.1	7.0	9.3	3 ⊙	6	0	S 2	NW 3	E 1
31	109.2	107.7	105.3	107.4	13.4	21.4	14.4	15.9	22.9	4.1	59	31	67	52	6.3	17.6	5.5	9.8	0	6	0	SW 1	S 5	SSE 3
M	106.2	105.9	105.7	105.9	8.8	14.8	10.4	11.1	16.4	4.6	76	49	71	65	2.8	9.5	3.9	5.4	5.7	7.4	4.9	4.3	5.4	3.6

Czerwiec – Juin

1	104.8	105.3	105.4	105.2	12.7	21.3	15.9	15.4	22.6	8.5	68	42	60	57	4.7	14.8	6.4	8.6	9	5	2	SW 2	W 7	NW 4
2	107.4	108.3	109.8	108.5	13.2	21.6	15.1	16.2	23.2	3.9	71	41	71	61	4.5	15.3	5.0	8.3	4 ⊙	7 ⊙	0	WNW 6	W 7	N 4
3	110.6	108.1	105.4	108.0	16.4	24.4	19.8	20.1	26.3	6.3	66	45	57	56	6.3	16.9	9.9	11.0	3 ⊙	6 ⊙	10	SE 1	S 3	WSW 6
4	102.6	101.5	99.0	101.0	19.2	25.0	19.8	21.0	25.9	14.0	69	39	61	56	6.8	19.3	8.9	11.7	8	9	10	ENE 2	NW 4	NW 7
5	97.5	96.6	95.2	96.4	13.1	17.4	11.9	13.6	20.5	11.2	91	61	89	80	1.4	7.7	1.5	3.5	10	8	7	W 6	WSW 6	SW 3
6	96.1	99.8	100.5	98.8	10.1	14.6	12.5	12.4	16.8	9.4	93	49	83	75	0.8	8.5	2.4	3.9	10 ●	8 ⊙	10	WNW 9	W 10	SW 2
7	99.4	98.7	100.5	99.5	13.5	20.1	14.2	15.5	21.5	8.6	69	47	79	65	4.9	12.4	3.4	6.9	5 ⊙	9	3	S 5	SW 5	C 0
8	101.9	102.6	100.6	101.7	14.2	20.6	18.3	17.8	22.6	9.7	82	44	73	66	2.9	13.6	5.6	7.4	10	6 ⊙	7	SSE 2	SE 5	E 5
9	98.2	97.2	100.6	98.7	17.4	25.0	17.7	19.4	26.4	14.4	82	56	83	74	3.6	14.1	3.4	7.0	8	8 ⊙	9	SSE 4	S 7	C 0
10	102.3	101.8	101.0	101.7	14.9	22.1	19.3	19.0	23.7	12.4	93	55	80	76	1.1	12.1	4.3	5.9	7	7 ⊙	7	ENE 5	NE 3	ENE 3
11	98.5	95.9	97.6	97.3	20.6	29.8	23.6	24.4	30.9	16.1	73	39	76	63	6.5	25.6	7.0	13.0	3	6	5	ESE 5	S 5	W 7
12	109.4	116.4	119.4	115.1	17.2	18.4	15.2	16.5	23.6	15.1	79	63	73	72	4.1	7.8	4.6	5.5	10	5	0	WNW 6	NW 7	N 3
13	121.7	120.8	119.3	120.6	12.7	18.4	16.3	16.0	22.4	7.4	65	42	58	55	5.2	12.3	7.8	8.4	2	2 ⊙	1	NW 7	NW 6	N 4
14	119.9	119.2	118.8	119.3	14.4	23.1	17.6	18.2	24.7	7.7	74	36	48	53	4.3	18.2	10.4	11.0	1 ⊙	3 ⊙	5	NE 2	NNE 3	ENE 5
15	119.4	117.9	115.2	117.5	12.6	22.3	18.5	18.0	24.6	8.0	60	33	63	52	5.8	18.2	8.0	10.7	0	1	0	NNE 4	E 5	ENE 3
16	114.3	112.4	110.4	112.4	15.6	24.7	19.7	19.9	26.2	9.0	61	36	58	51	6.9	20.6	9.6	12.4	0 ⊙	0 ⊙	0	ENE 3	ENE 5	E 3
17	110.3	109.1	107.7	109.0	17.7	25.9	20.4	21.4	27.3	12.8	72	35	52	53	5.7	21.7	11.4	12.9	2 ⊙	5	0	ENE 5	ENE 5	ENE 4
18	106.6	104.5	101.6	104.2	19.7	27.9	22.4	23.1	29.5	11.2	48	25	53	42	11.8	28.3	12.6	17.6	0	0 ⊙	0	SE 3	SE 4	E 1
19	100.5	99.4	100.4	100.1	21.8	31.9	22.0	24.4	32.1	13.4	55	38	58	50	11.7	23.1	11.0	17.3	1 ⊙	8	4	C 0	WSW 5	ENE 5
20	103.8	105.3	106.2	105.1	14.5	18.2	17.0	16.7	23.1	11.0	74	54	66	65	4.3	9.7	6.7	6.9	9 ⊙	10	2	NE 3	ENE 7	C 0
21	107.6	104.7	100.1	104.1	16.0	24.1	19.3	19.7	26.2	11.0	53	40	56	50	8.6	18.1	9.9	12.2	3	7 ⊙	3	SE 4	SSE 3	SSE 2
22	95.6	94.1	93.7	94.5	17.0	21.0	17.8	18.4	21.8	13.7	86	80	92	86	2.8	5.0	1.6	3.1	9	7	10	SSE 2	NW 6	WSW 2
23	98.9	99.2	99.6	99.2	14.5	21.0	15.1	16.4	22.4	12.2	84	49	87	73	2.7	12.6	2.3	5.9	9	8	9	WSW 5	S 3	WNW 5
24	101.4	99.8	96.5	99.2	12.6	11.0	13.6	12.7	15.4	10.0	89	95	86	90	1.6	0.6	2.2	1.5	10	10 ●	10	NE 5	NNE 7	ENE 5
25	94.1	101.6	106.0	100.6	13.4	10.5	10.1	11.0	14.3	9.7	99	91	93	94	0.2	1.1	0.8	0.7	10	10	3	SW 5	NW 10	SW 4
26	109.2	110.6	112.4	110.7	11.0	16.1	11.1	12.3	18.1	7.0	83	53	84	74	2.3	8.2	2.1	4.2	4 ⊙	7 ⊙	4	WNW 6	W 7	W 3
27	113.1	114.2	113.4	114.2	12.7	16.1	12.1	13.2	18.3	8.4	66	41	77	61	3.1	10.7	3.2	6.3	8	8	6	WNW 6	WNW 7	SW 2
28	113..	111.7	111.8	112.2	14.6	25.1	20.2	20.0	27.9	9.1	72	52	74	66	4.6	15.3	6.3	8.7	10 ●	9 ⊙	3	SW 6	WSW 7	W 2
29	112..	112.0	110.2	111.6	21.1	28.0	23.5	24.0	30.6	15.5	65	39	72	58	9.3	23.0	8.1	13.5	3 ⊙	5 ⊙	3	WSW 5	W 6	SSW 2
30	110..	110.3	110.0	110.2	22.5	29.1	22.7	24.2	30.6	16.7	69	38	64	57	8.4	24.8	9.9	14.4	2 ⊙	4 ⊙	4	NNW 4	WNW 6	WSW 1
31																								
M	106.0	106.0	105.7	105.9	15.6	21.8	17.4	18.0	24.0	10.8	74	49	71	65	5.0	14.8	6.2	8.7	5.7	6.3	4.6	4.3	5.7	3.2

Poznań-Ławica $H_s = 86\ m$ $H_b = 92{,}1\ m$ $h_w = 13\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁOWNIECZNIENIE	POGODA
1	8	.	.	–	$\frown^{2}$ n, a
2	7	.	.	–	$\frown^{1}$ n a
3	7	0.0	.	–	$= 20^{40} - 24$
4	7	0.0	.	–	$\overset{\bullet}{\nabla} 5^{15-26}$, 6^{10-18} $7^{45}-8^{20}$ 9^{30-40}; $\gg 8^{15}-9^{05}$ $\gg -9^{20}$ $\gg -19^{35}$; $= 0^{00}-5^{15}$
5	8	6.3	.	–	$\overset{\bullet}{\nabla} 10^{10-40}$ $\overset{\bullet}{\nabla} 12^{35-45}$, 15^{25-35}, 16^{42-50}, 17^{08-17}
6	6	14.0	.	–	$\bullet^{0}\, 0^{40}-4^{30}$ $\bullet^{1}-5^{15}$ $\times^{1}-9^{50}$ $\times^{0}-10^{12}$ $\bullet^{0}-16^{20}$
7	7	0.0	.	–	$\overset{\bullet}{\nabla} 11^{18-24}$, 12^{31-36} $16^{55}-17^{03}$, 17^{25-32}; $\equiv {}^{1}0^{35}-3^{20}$ $\equiv {}^{0}-3^{42}$ $= -9^{35}$, $21^{40}-24$; $\sqcup^{0-1}\, 3^{10}-7^{20}$
8	8	.	.	–	$= 0^{00}-3^{45}$; $\circlearrowleft 20^{30}-23^{00}$
9	8	0.5	.	–	$\bullet^{0}\, 18^{10}-24$; $= 2^{40}-7^{30}$ $\sqcup^{1}$ n a
10	6	2.0	.	–	$\bullet^{0}\, 0^{00}-5^{40}$, $9^{40}-16^{18}$
11	7	(0.0)	.	–	$\bullet^{0}\, 3^{40}-7^{10}$; ∞ $19^{25}-20^{40}$ $= -24$
12	7	0.0	.	–	$= 0^{00}-7^{30}$ $\infty - 10^{20}$, $20^{25}-22^{30}$ $= -24$, $\frown$ na
13	7	1.2	.	–	$\overset{\bullet}{\nabla} 1^{35-48}$ (K) 18^{40-50} $\bullet$K$^{0}-21^{40}$ SW–N; $= 0^{00}-4^{40}$
14	7	.	.	–	$= 5^{30}-6^{30}$
15	7	.	.	–	$= 0^{00}-3^{50}$ $\equiv {}^{1}-4^{30}$ $= -7^{40}$ ∞ $19^{35}-24$, $\frown^{2}$ na
16	7	.	.	–	$\infty\ 0^{00}-1^{50} = -6^{30}$ $\infty - 8^{30} = 20^{30}-24$; $\swarrow^{0}\, 22^{40}-23^{10}$ SW-S-SE
17	7	.	.	–	$= 0^{00}-7^{20}$
18	7	.	.	–	
19	7	.	.	–	
20	7	0.3	.	–	$\bullet^{0}\, 22^{27}-23^{25}$; $\gg 12^{40}-22^{30}$, $\leq 1^{20}-3^{35}$ SW-W-NW; $= 3^{18}-6^{15}$
21	7	.	.	–	$\bullet^{0}\, 0^{35}-1^{20}$
22	7	.	.	–	
23	7	.	.	–	
24	7	0.0	.	–	$\bullet^{0}\, 9^{25}-10^{15}$; $= 3^{30}-11^{30}$
25	8	.	.	–	
26	8	.	.	–	
27	7	0.4	.	–	$\overset{\bullet}{\nabla} 12^{05-10}$, 15^{10-30}, $\sqcup^{1}$ na
28	7	.	.	–	
29	8	.	.	–	
30	7	.	.	–	
31	7	.	.	–	$= 2^{30}-6^{40}$
Σ	–	24.9	–	–	UWAGI.

Czerwiec – Juin

1	7	.	.	–	
2	7	.	.	–	$= 3^{15}-7^{30}$ $\infty - 9^{20}$
3	7	0.7	.	–	$\overset{\bullet}{\nabla} 18^{05-20}$ $22^{35}-24$; (K) $17^{20}-18^{20}$; $= 3^{30}-8^{10}$
4	7	19.2	.	–	$\overset{\bullet}{\nabla} 0^{00}-2^{10}$ $\bullet^{1}\, 22^{40}-24$; $= 3^{20}-8^{40}$
5	7	7.0	.	–	$\bullet^{1}\, 0^{00}-3^{00}$ $\bullet^{1-0}\, 4^{45}-7^{20}$ $\overset{\bullet}{\nabla} 15^{30}-16^{20}$; 19^{30-45}; $= 3^{15}-9^{10}$, $21^{30}-24$
6	7	0.8	.	–	$\bullet^{0}\, 5^{30}-7^{10}$ $\bullet^{1}-8^{15}$; $= 0^{00}-5^{30}$
7	7	.	.	–	$= 3^{30}-7^{15}$; $\frown^{2}$ n, a
8	7	.	.	–	$= 3^{30}-7^{45}$; $20^{00}-23^{00}$
9	7	.	.	–	$= 0^{00-30}$
10	7	.	.	–	$= 0^{00}-4^{20}$ $\equiv {}^{2}-6^{10}$ $= -10^{30}$, $22^{20}-24$; $\oplus$ $9^{20}-11^{10}$
11	7	.	.	–	$= 0^{00}-6^{30}$, $20^{00}-24$; $\frown^{2}$ n, a
12	7	.	.	–	
13	8	.	.	–	
14	7	.	.	–	
15	8	.	.	–	
16	8	.	.	–	
17	7	.	.	–	$= 3^{10}-6^{35}$
18	8	.	.	–	$\infty\ 22^{30}-24$
19	7	0.6	.	–	$\overset{\bullet}{\nabla} 13^{30}-14^{10}$; (K) 12^{10-45} SW–SE; ∞ $0^{00}-6^{20}$
20	8	.	.	–	$= 4^{15}-5^{10}$
21	8	.	.	–	
22	6	2.7	.	–	$\bullet^{0}\, 9^{10-25}$ $\bullet^{1}-10^{10}$ $\bullet^{0}-10^{32}$ $\overset{\bullet}{\nabla} 16^{35}-17^{05}$, 19^{03-10}, $20^{45}-21^{02}$; $\leq 2^{15-40}$ NW (K) $14^{50}-15^{10}$ S; $= 0^{00}-24$
23	7	3.6	.	–	$\bullet^{0}\, 15^{25}-16^{40}$; $= 0^{00}-4^{30}$ $16^{40}-18^{20}$, $22^{20}-23^{00}$
24	6	13.5	.	–	$\bullet^{0}\, 9^{34}-12^{45}$ $\bullet^{1}-13^{25}$ $\bullet^{0}-14^{26}$; $= 0^{00}-2^{30}$ $\equiv -4^{40}$ $= -8^{30}$
25	7	1.4	.	–	$\bullet^{0}\, 1^{36}-7^{40}$ $\bullet^{0}\, 10^{40}-11^{30}$ $\bullet^{2}-13^{25}$ $\overset{\bullet}{\nabla} 16^{10-22}$, 17^{05-25}, 21^{05-20}; $= 22^{30}-24$
26	7	0.0	.	–	$= 0^{00}-3^{40}$
27	8	.	.	–	$\bullet^{0}\, 0^{40}-1^{15}$, 3^{15-50}; $= 2^{20}-4^{15}$
28	7	0.0	.	–	$\bullet^{0}\, 8^{00}-9^{23}$; $= 9^{23}-12^{10}$ $\infty - 13^{30}$ $= 21^{40}-24$
29	7	.	.	–	$= 0^{00}-2^{30}$ $\equiv -4^{20}$ $= -5^{35}$
30	7	.	.	–	$= 2^{00}-7^{30}$
31					
Σ	–	49.3	–	–	UWAGI.

Poznań – Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI d				ZACHMURZENIE : POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	110.0	108.8	106.8	108.5	20.6	28.5	23.7	24.1	30.9	16.2	66	46	70	61	8.1	21.2	8.9	12.7	4 ⊙	0 ⊙	3	ESE 3	SE 4	ESE 5
2	103.2	105.2	109.0	105.8	23.2	25.9	17.8	21.2	29.2	18.1	67	58	52	59	9.3	14.0	9.8	11.0	4 ⊙	6 ⊙	3	S 3	NW 7	NNW 5
3	111.0	109.5	107.6	109.4	16.8	24.0	20.0	20.2	27.2	9.5	74	34	62	57	5.0	19.7	9.0	11.2	1 ⊙	5	4	NW 4	NW 5	W 1
4	105.4	104.0	102.0	103.8	16.0	29.5	26.2	24.5	32.0	13.8	80	42	64	62	3.6	23.8	12.1	13.2	9 ●	1 ⊙	5	SE 2	SSW 4	SSW 5
5	103.5	104.3	107.1	105.0	24.8	32.5	22.2	25.4	32.9	19.7	67	30	62	53	10.4	34.3	10.1	18.3	4 ⊙	4 ⊙	1	SW 3	W 10	N 4
6	111.5	110.5	109.3	110.5	17.8	26.1	21.0	21.5	27.4	11.6	59	28	53	47	8.4	24.2	11.7	14.8	1 ⊙	2 ⊙	0	NNW 4	NW 7	NE 3
7	110.3	109.3	105.7	108.8	19.9	29.7	25.7	25.2	31.5	15.3	54	33	42	43	10.6	28.0	19.1	19.2	5	1	7	E 3	E 4	E 6
8	105.3	104.6	104.1	104.7	20.0	28.7	23.9	24.1	30.7	16.6	81	48	72	67	4.6	20.7	8.2	11.2	8 (🌂)	3	10	E 2	WNW 6	N 5
9	104.4	105.1	104.8	105.1	18.0	18.2	17.6	17.8	24.0	16.4	86	88	96	90	2.8	2.5	0.8	2.0	9	9 ●	3	ENE 5	N 3	C 0
10	102.7	101.1	99.0	100.9	16.8	20.1	19.4	18.9	23.3	15.5	96	83	87	89	0.8	3.9	3.0	2.6	8	10	10	ESE 1	NE 3	ENE 3
11	97.2	97.4	98.4	97.7	17.3	24.8	20.2	20.6	25.4	16.0	87	51	81	73	2.6	15.5	4.6	7.6	10	9	10	E 6	E 8	W 9
12	100.0	100.9	101.2	100.7	17.0	20.9	18.7	18.8	23.9	16.1	85	78	92	85	3.0	5.3	1.7	3.3	10	9	6	N 4	NNW 5	NNW 2
13	103.9	103.2	106.2	105.1	17.2	26.3	21.6	21.7	28.3	13.5	98	48	77	74	0.4	17.8	5.9	8.0	5 ⊙	6 ⊙	6	WSW 3	N 3	SSE 1
14	105.6	105.0	104.1	104.9	19.6	20.5	17.5	18.8	26.9	17.4	83	84	97	88	3.9	3.8	0.6	2.8	9	9	10 ●	ENE 2	NNW 6	E 2
15	102.4	102.2	102.1	102.2	17.1	20.6	16.9	17.9	22.4	15.5	99	74	97	90	0.2	6.3	0.6	2.4	10	9	7	W 2	WSW 3	S 2
16	101.5	100.8	99.3	100.5	17.6	20.6	18.1	18.6	20.9	13.2	74	54	76	68	5.3	11.0	5.1	7.1	9	10	10 ●	N 4	NW 7	N 3
17	97.8	98.3	100.0	98.8	15.6	15.6	15.7	15.6	18.3	13.8	91	96	92	93	1.5	0.7	1.3	1.2	10	10 ●	9	WNW 7	WNW 6	W 3
18	101.3	100.3	99.1	100.3	16.0	21.9	17.4	18.2	23.8	11.8	77	43	83	68	4.2	14.9	3.4	7.5	4 ⊙	3	0	W 5	W 7	C 0
19	97.9	96.8	95.5	96.7	16.6	26.1	21.1	21.2	27.2	11.6	82	38	69	63	3.5	20.8	7.7	10.7	0 ⊙	4 ⊙	3	SSW 1	SE 2	ESE 2
20	95.8	95.0	94.7	94.5	18.9	23.6	17.5	19.4	25.6	16.3	78	67	96	80	4.7	9.7	0.8	5.1	8	9	10 ●	SE 4	SSW 6	NE 1
21	93.4	93.4	93.2	93.3	16.2	17.0	16.3	16.4	17.7	15.5	97	96	97	97	0.6	0.8	0.6	0.7	10 ●	10 ●	10 ●	W 4	WSW 4	W 3
22	90.4	89.8	91.6	90.6	16.4	19.8	18.1	18.1	21.4	14.6	98	78	91	89	0.4	5.1	1.9	2.5	10	8	10	NW 8	NE 7	NNE 3
23	92.9	94.4	95.5	94.3	16.7	20.2	18.8	18.6	23.0	15.6	99	85	77	87	0.2	3.5	4.9	2.9	10 ●	9	10 (🌂)	NNE 2	NW 7	WNW 12
24	97.4	99.5	99.6	98.8	17.0	16.3	14.9	15.8	19.3	14.0	88	79	85	84	2.4	3.8	2.5	2.9	9	10	8	WNW 8	W 8	SW 2
25	100.9	100.3	97.8	99.7	14.2	17.9	12.9	14.3	18.8	12.0	79	58	95	77	3.4	8.7	0.7	4.3	9	10	7	W 8	WSW 7	SW 2
26	98.7	98.8	97.3	98.3	13.3	16.4	14.2	14.5	18.9	12.2	87	81	97	88	2.0	3.4	0.6	2.0	9 ●	10	10	WSW 7	SW 8	SW 3
27	93.3	93.3	93.3	93.4	16.2	17.4	14.2	15.5	19.6	13.6	95	88	90	91	1.0	2.4	1.6	1.7	9	9	9	SW 6	WSW 8	WNW 1
28	95.6	96.8	97.8	96.7	13.7	17.1	13.6	14.5	19.1	11.4	85	71	90	82	2.3	5.6	1.6	3.2	6 ⊙	9	4	WSW 7	WSW 5	S 2
29	98.7	99.8	102.2	100.2	13.2	20.0	16.1	16.4	21.5	9.5	96	59	83	79	0.6	9.6	3.1	4.4	9	8 ⊙	9	SSW 4	SSW 5	SSW 4
30	102.5	104.2	107.6	104.8	14.7	15.8	13.5	15.4	16.4	13.8	97	94	96	96	0.5	1.1	0.8	0.8	10 ●	10	10 ●	SW 7	WSW 8	W 7
31	110.9	112.9	114.1	112.6	13.5	17.3	15.3	15.8	18.8	13.8	92	81	82	85	1.3	3.7	3.2	2.7	10	8	10	W 5	W 7	W 4
M	101.4	101.6	101.5	101.5	17.2	21.9	18.5	19.0	24.1	14.3	84	64	81	76	3.5	11.2	4.7	6.5	7.4	7.2	6.9	4.3	5.7	3.3

Sierpień – Août

1	113.9	113.0	112.0	113.0	15.3	21.7	17.2	17.8	23.9	10.8	82	59	83	75	3.2	10.8	3.4	5.8	4 ⊙	4 ⊙	3	W 4	WNW 5	WNW 3
2	112.4	112.0	112.3	112.3	16.4	18.8	13.5	15.6	20.6	12.8	79	96	75	70	3.8	9.5	3.9	5.7	2 ⊙	8 ⊙	1	WNW 4	WNW 10	NW 5
3	111.8	110.9	110.7	111.1	13.3	17.9	14.3	15.0	20.4	8.0	82	66	81	76	2.8	7.1	3.1	4.3	6 ⊙	8	1	WNW 5	WNW 7	WSW 5
4	110.5	111.0	111.5	111.0	13.8	20.0	17.0	17.0	22.2	10.2	92	64	79	78	1.3	8.4	4.1	4.6	8	7	9	NW 7	WNW 2	WNW 3
5	113.0	113.1	112.4	112.8	14.9	22.2	16.9	17.7	23.5	10.0	88	44	79	70	2.0	15.1	4.0	7.0	0 ⊙	3 ⊙	2	NNW 1	NW 5	NW 2
6	112.4	111.2	108.9	110.8	16.2	23.9	19.3	19.7	24.5	12.2	81	50	67	66	3.4	14.9	7.4	8.6	1 ⊙	7 ⊙	3	ESE 4	ENE 3	ESE 2
7	104.9	101.9	99.0	101.9	17.6	22.3	17.3	18.6	23.2	14.9	75	66	95	79	4.9	9.1	1.0	5.0	9	10	9	S 1	S 2	WNW 4
8	99.4	100.6	100.2	100.1	15.7	22.0	17.8	18.3	23.5	13.7	97	59	90	82	0.6	10.8	2.0	4.5	10	7	8	WNW 6	NW 2	NE 2
9	98.6	96.2	92.1	95.6	15.8	24.0	21.5	20.7	25.1	12.1	86	53	58	66	2.4	13.9	10.6	9.0	4	9	7	ESE 3	ESE 5	ESE 5
10	90.3	91.3	94.5	92.0	17.1	21.9	17.3	18.4	23.9	16.1	99	70	85	85	0.2	7.9	2.9	3.7	10 ●	8	2	WSW 6	SW 6	SW 5
11	99.7	99.9	99.9	99.8	17.2	26.3	20.2	21.0	28.0	13.2	91	46	75	71	1.8	18.6	6.1	8.8	1 ⊙	6 ⊙	4	SW 5	SSW 7	SSE 4
12	100.3	101.3	101.8	101.2	18.2	21.0	17.4	18.5	23.9	16.1	91	59	87	79	1.9	10.3	2.6	4.9	9	9	6	C 0	WSW 4	SW 2
13	103.7	104.3	103.6	103.9	16.2	23.3	18.2	19.0	24.6	12.0	85	54	79	73	2.7	13.2	4.5	6.8	3	8	9	WSW 3	SW 7	WNW 1
14	102.4	101.7	99.7	101.3	16.2	18.8	16.1	16.8	19.7	14.1	92	79	92	88	1.6	4.5	1.6	2.6	10 ●	10	10	S 3	NE 1	N 2
15	98.6	98.5	99.0	98.7	16.0	22.2	19.4	19.2	24.8	12.5	87	55	80	74	2.3	12.0	4.0	6.1	7	6	10	NW 4	WSW 1	S 1
16	99.5	101.3	101.2	100.7	17.5	15.8	14.4	15.5	19.4	14.0	95	95	95	95	1.0	0.9	0.7	0.9	10	10 ●	10	SW 2	WSW 6	SSW 2
17	100.6	99.9	99.6	100.0	12.6	17.8	13.2	14.2	19.4	10.4	89	64	90	81	1.6	7.4	1.6	3.5	9	9	0	SW 6	WSW 6	SW 4
18	97.8	97.6	99.0	98.1	13.5	19.8	14.1	15.4	20.8	11.8	90	55	90	78	1.6	10.8	1.6	4.7	9	7	3	SW 6	W 11	SW 2
19	101.9	103.6	106.1	103.9	12.8	20.5	14.1	15.4	22.1	10.3	95	63	92	83	0.7	8.9	1.3	3.6	1	6	2	WSW 4	W 6	WSW 3
20	107.2	106.4	105.9	106.5	13.6	20.8	16.2	16.7	22.2	10.0	94	52	82	76	0.9	11.8	3.2	5.3	3	6	9	WSW 5	SW 7	SSW 2
21	104.8	103.5	101.4	103.2	15.8	19.3	13.7	15.6	20.5	13.0	97	76	97	90	0.5	5.4	0.6	2.2	10	9	10 ●	SW 5	SSW 5	WNW 3
22	101.5	101.8	102.1	101.8	11.6	15.1	11.0	12.2	18.3	10.3	93	67	87	82	1.0	5.6	1.6	2.7	10	8	6	WNW 7	WNW 5	WNW 2
23	102.7	102.1	101.2	102.0	9.5	18.2	12.4	13.1	18.5	6.1	96	49	77	74	0.5	10.6	3.4	4.8	0	7	0	WSW 2	WSW 4	C 0
24	97.1	92.7	98.4	96.1	10.7	17.9	11.5	12.9	19.1	8.5	85	78	88	84	2.0	4.4	1.7	2.7	10	10 ●	0	SE 3	S 4	SW 6
25	103.0	100.7	97.7	100.5	10.8	20.1	15.9	15.7	21.4	7.6	84	47	71	67	2.2	12.6	5.3	6.7	3	6 ⊙	5	SSW 4	SW 10	S 5
26	98.5	98.4	99.8	98.9	12.1	17.6	11.6	13.2	18.9	10.4	82	59	90	77	2.5	8.2	1.3	4.0	9	7 ⊙	2	SSW 5	SW 10	SW 5
27	101.9	102.4	102.1	102.1	12.3	14.6	12.4	12.9	18.4	9.9	87	73	90	83	1.9	4.3	1.3	2.6	10	7	8	SW 6	SW 6	SSE 1
28	101.6	103.0	104.5	103.0	11.1	12.6	12.2	12.0	15.8	9.5	97	87	92	92	0.3	1.9	1.2	1.1	10	10 ●	1	S 1	W 2	SW 3
29	106.2	107.8	108.3	107.4	10.1	13.7	11.3	11.6	15.4	6.5	95	75	89	86	0.7	3.9	1.3	2.0	2	9	1	W 4	WSW 5	WSW 3
30	109.0	109.2	108.7	109.0	9.7	15.6	11.3	12.1	17.4	7.7	96	53	88	79	0.4	8.2	1.7	3.4	10	8 ⊙	9	WSW 4	WNW 10	SW 2
31	106.1	103.1	103.3	104.8	10.5	16.0	11.8	12.5	17.5	7.8	86	66	82	79	1.8	5.8	2.5	3.4	10 ●	9	10 (🌂)	SSW 3	SW 7	SW 8
M	103.6	103.3	103.1	103.3	14.0	19.4	15.2	16.0	21.3	11.0	89	65	84	79	1.8	8.9	3.0	4.6	6.5	7.7	5.2	4.0	5.5	3.2

Poznań – Ławica $H_s = 86\ m$ $H_b = 92{,}1\ m$ $h_w = 13\ m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	7	.	.	–	
2	7	0.6	\	–	●K 11⁵⁰–12³⁵ W–NE ; = 3²⁰–7³⁰ ∞–10⁰⁰
3	8	0.3	.	–	
4	7	0.0	.	–	●⁰ 6⁵⁰–8¹⁰ . = 22²⁰–24
5	7	.	.	–	(K) 3¹⁰–²⁵ NW–W–NE ; ≫ 13²⁰–17²⁵ ; = 0⁰⁰–7³⁰ ∞–10⁴²
6	8	.	.	–	= 3⁴⁰–5²⁰ ; ⌓⁰ na
7	7	6.8	.	–	
8	7	0.3	.	–	● 3⁵⁰–5⁴⁰ . K 3²⁰–5⁴⁰ W–NE (K) 7⁴⁰–8¹⁵ W–NE
9	7	6.4	.	–	▽ 5⁰⁶–⁷¹⁰ ●⁰ 9⁰⁸ 10¹⁰–11⁴⁰ 13⁴⁵ 14⁰⁸ ▽ 17²⁵–18²⁵ . K ⁰0³⁵–130 NE . K¹ 5²⁰–7¹⁵ NE–E . = 21³⁵–23¹⁰ ≡–24
10	7	8.9	.	–	●¹ 5³⁸–6⁰⁶ ●⁰–6²³ ▽ 7¹⁰–8⁰⁶ . 23⁵⁵–24 . ≡ 0¹⁰⁰–1⁰⁰ =–5³⁸ , 8⁰⁶–14⁰⁰ , 20¹⁰⁰–23⁵⁵
11	7	0.0	.	–	▽ 0⁰⁰–2⁵⁰ . = 2⁵⁰–12⁰⁰
12	7	0.0	.	–	●⁰ 6⁴⁵–8⁴⁰ ▽ 18⁰²–¹⁸ . = 21²⁰–24
13	7	.	.	–	= 0⁰⁰–3⁴⁰ ≡⁰–4²⁵ ≡¹–6⁴⁵ ≡⁰–7³⁰ =–8⁴⁰ ∞ 19²⁰–21³⁵ =–24 . ⌓² 1⁰⁰– na
14	6	19.1	.	–	● 12²⁵–⁵⁵ 17³⁰–24 . K 12⁰⁰–25–55 (K) 14⁰⁰–³⁰ 15⁵²–16²⁰ K 17³⁰–19²⁵ . = 0⁰⁰–10³⁰ , 13⁰⁰–14²⁰
15	7	.	.	–	= 0⁰⁰–7²⁰ ≡¹–7⁵⁵ =–13³⁰ ∞–21³⁵ =–24
16	7	0.3	.	–	●⁰ 21³⁵–24 . = 0⁰⁰–6⁵⁰
17	5	12.0	.	–	●⁰ 0⁰⁰..²⁰ 2⁴⁰–4¹⁰ , 6³⁵ 8²⁵ , 10⁰⁷–¹⁵ ●²–11⁰³ ●¹–11¹² ●⁰–13¹⁶ ●¹–14⁴⁰ ●⁰–21⁵⁰ . = 4¹⁰–6³⁵ , 21⁵⁵–24
18	8	.	.	–	= 0⁰⁰–5²⁰
19	7	.	.	–	= 4⁰⁰–8³⁵ ∞–12⁴⁰ 19³⁵–22⁴⁵ =–24 . ⌓² na
20	6	2.1	.	–	●⁰ 12⁴⁰ 13¹⁰ ▽ 20³²–22³⁵ . = 0⁰⁰–11⁴⁰ ∞–15³⁰ = 22³⁵–24
21	6	35.0	.	–	●⁰ 1⁴⁰–2²⁵ 4³⁵–9¹⁵ ●¹–13²⁰ ●⁰–19³⁰ 20³⁰ 21³⁵–24 . = 0⁰⁰–1⁴⁰
22	7	34.1	.	–	●⁰ 0⁰⁰–3⁵⁰ ●¹–4¹⁵ ●²–4⁴⁰ ●¹ 5⁵⁰ ●⁰ 7³⁰ 9⁰⁵–²⁵ ●¹–10⁵⁵ ▽–11¹⁵ 12¹⁰–13¹² 13¹⁷–³⁵ 16³⁷–17¹⁵ ●²³⁵⁰ 24 . =7³⁰–9⁰⁵
23	7	26.9	.	–	●⁰ 0⁰⁰ 3³⁵ 4²⁰ 6²⁰ ●² 7³⁰ ●⁰ 8³⁰ ▽ 11³⁵–12⁰⁵ 18¹⁵–³⁰ 18⁴⁵–⁵⁵ 21⁵⁵–22¹⁵ , 23⁴⁸–24 . (K)⁰ 17⁵⁰ 18⁴⁰ NE–W K 21³⁰–21⁵⁵–22³⁰ NW–E
24	7	0.0	.	–	▽ 0⁰⁰–³⁰ 1³⁵–2³⁶ 15²⁵–³⁷ . ↙ 0⁵⁰–1²⁰ = 5¹⁵–7²⁰ **23.VII:** = 8³⁰–11¹⁰ , 22¹⁵–24
25	8	7.7	.	–	●⁰ 17¹⁵–³⁵ ●²–17⁵⁰ ●⁰–18⁰⁵ 18²⁵–19²⁰ ●¹–19³⁵ ●⁰–20¹⁰ ●¹ 23³⁵–⁵⁵ ●⁰–24 . = 20¹⁰–23³⁵
26	7	3.8	.	–	●⁰ 0⁰⁰–⁴⁵ 1⁵⁰ 2²⁶ 7²⁰ 8²³ ▽ 9²⁰ 10⁴⁰ 14¹⁰–15²⁰ 16²²–17¹⁰ ●¹–21⁴⁵ ●⁰ 23²⁰–24 . = 2²⁶–6³⁰
27	7	2.8	.	–	●⁰ 0⁰⁰–¹⁰ ▽ 11²⁵–12⁰⁶ 12¹⁶–13⁰⁸ 13¹³–²³ 14⁰⁸–¹⁵ 23⁴⁹–24 . K¹ 11³⁰–43 . = 0¹⁰–11¹⁰ , 21¹⁵–24
28	7	5.6	.	–	▽ 0⁰⁰–¹⁰ 13⁰⁸–²⁰ ▲ 13¹²–¹⁶ ▽ 16²²–³⁰ 16⁴⁰–17³⁰ . = 0⁰⁰–5²⁵ 22³⁰–24
29	7	3.3	.	–	●⁰ 5⁴⁰ 7³⁵ ▽ 17²²–⁴⁰ 15⁵⁰–⁵³ 16⁵⁸–17³³ ; K⁰ 16³⁵–³⁸–⁵⁸ WSW–E . = 0⁰⁰–5⁴⁰ 7³⁵–11²²
30	7	4.7	.	–	▽ 3³⁵–4¹² ●⁰ 6³⁸–8⁴⁰ ●,,⁰–9³⁰ ●⁰–10¹⁰ ●,,⁰–10³⁵ ●⁰–13⁴⁵ ,⁰ 16¹⁵–17²⁰ ●⁰–19³⁰ , 20²⁰–23³⁵ . = 0⁰⁰–3³⁵ , 23³⁵–24
31	7	.	.	–	= 0⁰⁰–9²⁰ , 21³⁰–24
Σ	–	200.7	–	–	UWAGI.

Sierpień – Août

1	8	.	.	–	= 0⁰⁰–8¹⁵ . ⌓ 5⁰⁰– a
2	8	.	.	–	≫ 13⁴⁰–15³⁵ . = 3³⁰–7¹⁵ ; ⌓¹ n,a
3	8	.	.	–	⌓¹ na
4	7	0.0	.	–	▽ 16¹⁸–17¹² . = 7¹⁵–8⁴⁰ ; ⌓² 23⁴⁰–24
5	7	.	.	–	= 4³⁵–8¹⁵ . ⌓² 0⁰⁰–9³⁰
6	7	.	.	–	= 0⁰⁰–8¹⁵ , 8⁴⁰–9¹⁰ ∞–10²⁰ 20³⁵–24 . ⌓ n–a . ⌣ 20²⁰–24
7	6	2.3	.	–	▽ 13¹⁰–²³ 15¹²–⁴⁵ ●⁰ 20²³–21³⁰ . K 20⁰⁵–20²³–21³⁰ . ∞ 0⁰⁰–1⁵⁰ =–7⁵⁵ ∞–a ; ⌣ 0⁰⁰–1²⁰
8	7	0.8	.	–	●⁰ 7³⁰–⁵⁰ ▽ 16⁴⁰–⁵⁰ , 18⁴⁰–19⁰⁵ . = 0⁰⁰–9²⁰
9	7	5.6	.	–	= 4¹⁰–8²⁰
10	7	1.2	.	–	●⁰ 5⁴⁰–6²⁰ ●¹–11⁵⁰ . = 3³⁰–5⁴⁰
11	7	0.0	.	–	
12	7	0.0	.	–	▽ 4³⁰–⁴⁵ 10⁵⁰–11³⁰ ; (K) 3³⁰–4²⁰
13	7	0.3	.	–	= 4⁴⁰–9²⁰ . ⌓¹ na
14	6	2.1	.	–	●⁰ 6³⁵ 9⁴⁵ 11⁵³ 12⁰⁵ . = 2⁰⁰–15⁴⁰ 19⁴⁰–24
15	7	0.6	.	–	= 0⁰⁰–10³⁰ , 19²⁰–24
16	5	9.8	.	–	●⁰ 5⁵⁰–6⁴⁰ 8³⁰–9¹⁵ ▽ 10¹⁵–⁵⁰ ●⁰–18³⁰ . = 0⁰⁰–5⁵⁰ , 6⁴⁰–24
17	7	0.2	.	–	▽ 14⁵⁰–15¹⁵ 15⁴⁰–⁴⁵ . = 0⁰⁰–8²⁰ . 20²⁰–24
18	7	0.0	.	–	= 0⁰⁰–13³⁰ , 20³⁰–24
19	7	.	.	–	= 0⁰⁰–10⁴⁵ ∞ 18⁴⁰–19⁵⁰ =–24 . ⌓ 3³⁰–a
20	7	0.7	.	–	= 0⁰⁰–7³⁰ . ⌓ 2³⁰–6³⁰
21	7	5.6	.	–	●⁰ 4⁵⁰–7¹⁰ ▽ 14¹⁰–³⁵ ●⁰ 15¹³–16¹⁵ ●¹–18⁰⁰ ●⁰ 20²⁰ ●¹–23¹⁵ ●⁰–24 . = 2¹⁵–10³⁵
22	7	2.1	.	–	●⁰ 0⁰⁰–1¹⁵ ▽ 12³⁴–⁵⁴ ▲⁰ 12³⁸–⁴⁰ . = 1¹⁵–8²⁰
23	7	.	.	–	= 4³⁰–8³⁰ 20⁵⁰–24 . ⌓² n–a
24	6	9.7	.	–	●⁰ 13¹⁵ 15⁴⁰ ●¹–16⁰⁵ ●²–16²⁰ ●¹–18⁴⁰ ●⁰..20¹⁵ . = 0⁰⁰–11³⁰
25	7	.	.	–	= 3¹⁵–7²⁰
26	7	2.2	.	–	▽ 12⁴⁰–⁵⁵ 16¹⁵–³¹ 18²⁸–³⁵ 18⁴⁸–19⁵⁰ . K 19⁰²–⁴⁰ NW–NE . ≫ 13²⁵–16¹⁵ . = 2⁰⁰–5³⁰ . ⌒ 19²⁵–20⁰⁰
27	7	0.7	.	–	▽ 13²⁰–³⁰ . = 0¹⁵–5²⁸ , 19⁵⁸–24
28	6	0.7	.	–	●⁰ 1⁴⁰–2⁴⁵ 5⁴⁵–7⁴⁵ 8⁴⁰–10³⁰ 11⁵⁰–14³⁰ . = 0⁰⁰–5²⁰
29	7	.	.	–	= 2²⁰–6⁰⁰ ≡⁰–6⁴⁰ =–12²⁰ , 20³⁰–24
30	7	0.0	.	–	= 0⁰⁰–10³⁰ . ⌓¹ 3³⁰–10⁰⁰ , 21³⁰–24
31	7	1.2	.	–	●⁰ 7⁰⁴ 11¹⁵ , 22³⁰–23⁴⁵ . (K) 21³⁰–22³⁰ . = 3²⁰–11³⁰ ; ⌓¹ 0²⁰–7⁰⁴
Σ	–	45.8	–	–	UWAGI.

Poznań – Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	104.2	103.8	106.9	105.6	9.9	13.5	9.5	10.6	16.5	8.5	92	80	95	89	1.0	3.2	0.7	1.6	10	9	3	SW 5	WSW 7	SSW 4
2	106.1	104.9	103.2	104.7	8.6	18.2	14.1	13.8	20.0	5.4	94	61	92	82	0.6	8.1	1.3	3.3	8	9	10	SSE 2	SSW 5	SSE 3
3	102.8	103.0	107.4	104.1	13.3	17.8	10.8	13.2	18.2	10.2	92	51	89	77	1.3	10.0	1.5	4.3	10 ●	7 ⊙	5	SW 5	NW 5	WNW 2
4	109.2	111.2	112.3	111.0	8.5	17.4	9.7	11.3	18.5	6.5	97	44	86	76	0.3	11.2	1.7	4.4	2	7	0	C 0	WNW 4	C 0
5	112.0	109.1	107.2	109.4	7.2	19.4	16.4	14.8	20.6	3.8	99	35	57	64	0.2	14.5	7.9	7.5	3	8	10	SE 1	SSW 7	SSW 5
6	107.0	107.4	108.7	107.7	12.8	18.1	11.8	13.6	19.5	10.2	99	74	93	89	0.2	5.5	1.0	2.2	10	8	2	SW 2	SSW 3	N 2
7	109.1	108.2	107.2	108.2	9.9	23.0	17.1	16.8	24.5	8.1	99	53	84	79	0.2	13.3	3.2	5.6	8	3 ⊙	1	E 2	SE 4	SE 1
8	107.5	108.1	108.2	107.9	14.7	27.6	18.9	20.0	28.2	11.8	91	40	81	71	1.5	22.2	4.1	9.3	4	4	4	SSE 1	SSW 5	SE 2
9	107.9	109.5	113.3	110.2	15.1	22.7	15.0	17.0	24.7	12.8	94	65	84	81	1.0	9.6	2.7	4.4	2	2	10	S 2	W 8	NW 6
10	113.0	110.9	107.9	110.6	12.8	17.5	12.8	14.0	19.3	12.0	95	73	93	86	1.1	5.3	1.1	2.5	10	9	9	NE 3	W 1	SE 3
11	102.7	97.1	89.4	96.4	10.2	21.1	15.0	15.3	21.5	8.6	100	52	96	83	0.0	12.0	0.7	4.2	0 ≡	8	10 ●	S 2	S 8	S 6
12	85.8	85.4	90.7	86.6	15.4	15.6	11.2	13.4	18.2	10.6	96	58	73	76	0.8	7.4	3.6	3.9	10 ●	7	6	SSW 6	SW 8	WSW 4
13	94.3	93.1	89.9	92.4	9.1	15.8	11.4	11.9	17.3	7.0	84	60	75	73	1.9	7.1	3.5	4.2	3	8	9	SSW 8	SW 10	S 7
14	92.7	93.6	95.2	93.8	8.9	15.4	10.2	11.2	16.8	7.0	88	52	80	73	1.4	8.4	2.5	4.1	9	9	1	SSW 8	SW 12	SSW 4
15	94.7	96.3	100.6	97.2	8.5	11.8	8.7	9.4	14.1	7.4	90	82	90	87	1.1	2.5	1.0	1.5	10	10 ●	0	SW 4	W 6	SW 5
16	102.6	103.9	106.2	104.2	8.5	12.3	7.5	9.0	12.7	6.6	89	70	97	85	1.2	4.3	0.3	1.9	7	9	9	SSW 7	SSW 6	S 3
17	104.9	104.4	104.0	104.4	8.5	10.3	8.9	9.2	11.9	4.8	100	97	99	99	0.0	0.3	0.2	0.2	10 ●	10 ●	10 ●	SSW 2	SW 7	NW 3
18	103.5	102.7	102.6	102.9	6.9	14.0	8.4	9.4	14.5	6.0	100	65	92	86	0.0	5.6	0.9	2.2	4	8	2	W 6	WNW 10	W 3
19	99.6	96.8	95.6	97.3	6.8	10.6	11.4	10.0	13.6	5.0	100	100	95	98	0.0	0.0	0.7	0.2	10 ≡	10 ●	5	SW 2	S 4	W 4
20	98.9	102.4	103.0	102.1	9.0	12.2	5.8	8.2	13.4	5.4	96	68	98	87	0.5	4.5	0.1	1.7	10	7	0	NW 3	WNW 5	C 0
21	106.3	106.3	104.2	105.6	5.7	13.3	10.9	10.2	14.5	3.3	98	61	79	79	0.2	6.0	2.7	3.0	4	9	6	C 0	SSW 1	ESE 1
22	99.2	99.1	98.3	98.9	9.5	15.4	14.9	13.7	16.7	8.5	100	90	98	96	0.0	1.7	0.3	0.7	10 ●	10	10	ESE 2	SW 4	S 3
23	93.1	87.1	88.8	89.7	14.5	15.8	14.8	15.0	17.0	13.7	93	96	91	93	1.1	0.7	1.5	1.1	9	10 ●	10 ●	SSW 4	S 4	WSW 7
24	94.9	94.7	98.8	96.1	10.5	8.8	7.3	8.5	14.8	6.5	92	92	70	85	1.0	0.9	3.0	1.6	10	10 ●	0	W 5	W 6	W 10
25	103.9	106.3	108.1	106.1	5.4	12.2	2.7	5.8	12.9	2.4	78	42	91	70	2.0	8.2	0.6	3.6	1	6	1	WSW 6	WNW 13	W 2
26	106.6	106.6	108.8	107.3	0.3	11.6	2.8	4.4	12.7	−1.2	98	49	88	78	0.1	7.0	1.0	2.7	5	8	0	SSW 2	NNW 6	NNW 4
27	109.1	104.9	99.9	103.3	1.9	10.3	9.5	7.8	11.1	−1.2	96	63	86	82	0.3	4.7	1.7	2.2	9	10	10	SW 3	SW 8	SW 9
28	95.3	95.5	96.3	95.7	9.7	12.9	8.6	10.0	13.2	8.1	82	68	86	79	2.2	4.8	1.6	2.9	8	8	0	W 9	W 10	W 8
29	92.9	90.1	98.4	93.8	8.4	9.1	8.2	8.5	9.7	6.4	97	97	96	97	0.3	0.4	0.5	0.4	10 ●	10 ●	10	SW 5	SW 6	WSW 4
30	93.4	97.7	103.9	98.3	4.7	8.0	3.9	5.1	10.4	3.4	90	85	95	90	0.8	1.5	0.4	0.9	10 ●	9 ●	0	W 9	W 9	WNW 3
31																								
M	101.7	101.5	102.1	101.8	9.2	15.1	10.6	11.4	16.6	6.9	94	67	88	83	0.7	6.4	1.7	2.9	7.2	8.1	5.1	3.9	6.4	3.9

Październik – Octobre

1	105.3	105.7	109.5	106.8	2.1	9.1	2.3	4.0	10.1	0.4	100	74	98	91	0.0	3.1	0.1	1.1	10 ≡	8	1	W 1	W 8	WNW 8
2	113.3	114.2	112.5	113.3	−1.0	8.8	1.8	2.8	10.2	−3.0	98	59	94	84	0.1	4.6	0.4	1.7	6	6 ⊙	0	SW 2	WSW 4	S 1
3	106.6	102.9	99.4	103.0	−0.1	8.3	8.7	6.4	9.9	−1.3	100	71	86	86	0.0	3.2	1.5	1.6	7	10 ●	10	S 3	SW 8	WSW 9
4	101.1	103.3	109.6	105.4	5.9	4.5	4.6	4.9	10.0	4.1	79	92	76	82	2.0	0.7	2.1	1.6	9	9 ●	5	W 10	NW 8	W 6
5	111.9	111.1	107.4	110.1	6.4	10.0	8.1	8.2	11.0	4.0	79	54	75	69	2.0	5.7	2.7	3.5	9	9	10	WSW 6	WSW 8	SSW 7
6	107.2	110.8	113.3	110.4	9.0	11.8	10.3	10.4	12.9	6.6	97	81	92	90	0.3	2.6	0.9	1.3	10	10	10	SW 5	W 6	SW 5
7	113.3	114.2	113.2	114.2	11.2	13.3	9.0	10.6	14.3	8.4	94	72	97	88	0.8	4.3	0.3	1.8	10	10	0	SW 4	W 7	W 3
8	117.3	118.2	117.6	117.7	9.2	13.4	11.4	11.4	13.7	5.0	99	82	89	90	0.1	2.8	1.5	1.5	10	10	0	C 0	SE 2	ESE 1
9	114.7	113.4	111.5	113.2	6.5	18.1	11.7	12.0	19.7	5.8	99	64	88	84	0.2	7.5	1.6	3.1	0	0	0	ESE 2	SE 1	ESE 2
10	110.4	109.8	109.1	109.8	6.5	18.8	10.2	11.4	20.1	5.5	97	59	96	84	0.3	9.0	0.4	3.2	0	0 ⊙	0	ESE 2	S 4	SSE 2
11	110.1	110.1	109.5	109.9	6.8	11.7	8.7	9.0	12.5	5.7	100	89	100	96	0.0	1.5	0.0	0.5	7	10	10 ≡	SSW 1	WNW 1	NE 1
12	107.9	111.3	116.5	111.9	9.0	13.2	5.7	8.4	13.2	4.7	97	86	97	93	0.3	2.1	0.3	0.9	10	10	1	SSW 4	WNW 5	NW 5
13	117.5	115.7	115.3	115.4	1.4	13.2	7.6	7.4	13.9	0.0	100	76	100	92	0.0	3.7	0.0	1.2	4 ≡	9	0 ≡	C 0	SSE 1	SE 1
14	112.6	114.6	116.3	114.5	8.0	11.5	9.5	9.6	13.9	4.6	100	81	96	92	0.0	2.7	0.5	1.1	10 ≡	2	10	NW 3	WSW 4	NW 1
15	118.2	118.4	117.7	118.1	6.5	9.3	8.1	8.0	10.1	5.1	100	78	96	91	0.0	2.6	0.5	1.0	9	10	10	NE 1	S 1	C 0
16	114.8	112.5	108.7	112.0	7.9	14.8	8.6	10.0	15.4	7.5	94	58	92	81	0.6	7.0	1.0	2.9	9	0	0	ESE 4	SE 5	SE 1
17	105.5	107.4	108.4	107.1	6.6	14.5	9.6	10.1	14.9	4.1	96	70	96	87	0.4	5.0	0.5	2.0	8	9	10	S 5	WSW 8	SW 5
18	102.3	99.7	98.8	100.3	10.2	15.5	13.7	13.3	17.0	7.7	93	82	85	87	0.8	3.2	2.3	2.1	10	10	0	S 4	SW 6	SSW 5
19	97.2	96.6	96.0	96.6	13.8	20.4	15.9	15.3	20.9	10.0	83	59	84	75	2.6	9.9	2.5	5.0	8	6	10	SSW 6	SW 7	NNW 3
20	101.6	104.1	106.2	104.0	8.5	9.4	5.2	7.1	13.9	4.8	100	93	100	98	0.0	0.8	0.0	0.3	10 ●	10 ●	0 ≡	WSW 3	SW 2	SW 3
21	106.6	104.0	100.6	103.7	5.0	8.0	6.2	6.4	10.9	3.7	100	97	94	97	0.0	0.3	0.6	0.3	10 ≡	10	3	S 3	SE 4	S 5
22	94.9	91.8	92.4	93.0	2.0	13.7	6.3	7.1	13.9	1.4	98	61	97	85	0.2	6.2	0.2	2.2	8	4	10	SE 2	S 7	SE 2
23	96.9	100.2	102.9	100.0	7.2	9.5	4.5	6.4	10.6	2.6	99	76	93	89	0.2	2.8	0.5	1.2	10	9	0	SW 2	WSW 6	SSW 6
24	100.9	104.2	110.5	105.2	6.9	9.0	8.3	8.1	9.8	3.6	84	93	97	91	1.6	0.8	0.4	0.9	10 ●	10 ●	0	SSW 5	W 8	WSW 5
25	114.0	113.1	114.0	114.4	5.0	10.5	7.7	7.7	12.0	4.2	100	77	97	91	0.0	2.9	0.3	1.1	9 ≡	8	10	C 0	W 3	SSE 2
26	112.8	112.0	110.0	111.6	4.9	14.8	5.9	7.9	15.3	4.5	95	67	100	87	0.5	5.5	0.0	2.0	5	1	0	S 3	SW 5	S 1
27	108.3	107.8	107.8	108.0	2.2	10.9	5.1	5.8	12.3	1.8	100	81	100	94	0.0	2.4	0.0	0.8	3 ≡	9	0	S 2	SW 3	SSW 3
28	108.1	107.5	107.9	107.8	6.5	12.4	7.0	8.2	12.9	1.9	94	71	91	85	0.6	4.2	0.9	1.9	10	2	0	SW 4	SW 7	S 4
29	106.6	106.4	106.4	106.5	7.0	13.5	7.6	8.9	13.9	4.8	88	61	93	81	1.2	6.0	0.7	2.6	9	8	4	SSW 5	WSW 6	S 3
30	103.9	103.0	103.9	103.6	5.5	14.7	10.5	10.3	14.9	4.6	94	61	86	80	0.5	6.5	1.8	2.9	5	8	9 ●	SSE 4	SSW 7	SW 4
31	103.7	102.2	99.2	101.7	6.3	12.3	9.7	9.5	13.4	5.7	97	73	86	85	0.2	3.9	1.7	1.9	6	10	4	SSW 5	SW 6	SW 5
M	107.9	108.1	108.1	108.0	6.2	12.2	8.0	8.6	13.4	4.1	95	74	93	87	0.5	4.0	0.8	1.8	7.8	7.3	4.1	3.3	5.1	3.5

Poznań – Ławica $H_s = 86$ m $H_b = 92{,}1$ m $h_w = 13$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.2	.	–	●⁰ 9⁰⁵ 11⁰⁰ . = 8²⁰–9⁰⁵ , ⌓¹ 21³⁰–24
2	7	0.0	.	–	= 2²⁰–8³⁰ , 20³⁵–24 , ⌓¹ 0⁰⁰–9⁵⁰
3	7	0.0	.	–	●⁰ 6³⁵–8²⁰ , ▽ 16¹⁵–21 . = 0⁰⁰–7¹⁰
4	8	.	.	–	= 2³⁰–9²⁰ , 23⁴⁵–24 , ⌓² n.a
5	7	0.0	.	–	●⁰ 17⁵⁵–18³⁵ , 22⁴⁵–24 . = 0⁰⁰–8¹⁵ , 23¹⁵–24 . ◡ 2⁴⁰–4³⁰
6	6	0.0	.	–	●⁰ 0⁰⁰–40 . = 0⁰⁰–5²⁰ ≡²–7⁴⁵ = –2²⁰ , 17²⁰–24
7	7	.	.	–	= 0⁰⁰–1³⁰ ≡²–6⁴⁰ = –13¹⁵ , 19³⁰–24 ⌓ 0⁰⁰–10⁰⁰
8	7	.	.	–	= 0⁰⁰–10³⁰ , 21⁰⁰–24 , ⌓² n.a , a
9	6	4.2	.	–	= 0⁰⁰–8³⁰ , ∞ 12³⁰–17⁴⁰ ⌓ n.a , a
10	7	.	.	–	▽ 1¹⁰–3²⁰ . = 9³⁰–10³⁵ , 19²⁰–24
11	7	1.7	.	–	●⁰ 19⁴⁵–22³⁰ . = 0⁰⁰–3²⁰ ≡ 5²⁰–6⁴⁵ ≡²–7³⁰ ≡¹–8²⁰ = –11²⁰
12	8	5.4	.	–	●⁰ 1²⁰ 3²⁹ 5²⁵ 10²⁰ ▽ 11¹⁶–²⁵ ●↯ –11³⁵ ▽ –12¹⁰ . = 21⁴⁰–24
13	7	5.7	.	–	▽ 13¹⁰–18 , 22⁴⁵–24 . = 0⁰⁰–3²⁰
14	7	.	.	–	▽ 0⁰⁰–30
15	7	2.2	.	–	●⁰ 10⁰³–13³⁰ ▽ –14⁴⁰ . = 1²⁰–13³⁰
16	7	7.2	.	–	▽ 12³⁰–13¹⁰ 14⁰⁰–²⁰ 16²⁵–17¹⁵ . = 5¹⁰–10³⁰ , 18⁴⁵–24 . ⌓ n.a
17	6	14.4	.	–	● 5²⁰–6⁵⁰ , ●⁰–7⁵⁰ , ●¹–8¹⁰ , ●⁰–10³⁰ , 12³⁵ 19²⁵ , 21³⁰–22²⁰ . = 0⁰⁰–11³⁰ , 12³⁰–24
18	7	.	.	–	= 0⁰⁰–10²⁰ , 20²⁰–24
19	4	5.6	.	–	●⁰ 9³²–17⁴⁵ ▽ 20⁰⁴–²⁰ . = 0⁰⁰–5⁴⁵ ≡ –6¹⁵ ≡⁰–6²⁵ ≡¹–9³⁵ ≡⁰–9⁴⁵ = –24
20	7	.	.	–	●⁰ 3¹⁵–5²⁰ , ●¹–6⁵⁰ . = 0⁰⁰–10³⁰
21	7	12.5	.	–	= 5⁴⁵–8³⁵ , 18²⁵–24
22	5	3.0	.	–	●¹ 1¹⁷–5⁴⁰ ●⁰–9²⁰ ▽ 22³⁰–⁵⁵ , 23¹⁵–⁴⁵ (↯)⁰ 22²⁵–23¹⁵ W–S , 23⁴⁵–24 S–E . = 0⁰⁰–1¹⁷ , 9²⁰–22³⁰
23	5	21.0	.	–	▽ 0⁰⁰–1³⁰ , 2⁰⁰–⁴⁵ ●⁰ 10²⁵–13¹⁵ ●¹–14³⁰ ●⁰–16¹⁵ ●² 17¹⁵ ●¹–19⁴⁰ ●⁰–20⁴⁰ 21²⁵–22³⁵ , 23²⁰–2¹⁴⁵ , ≫ 16¹⁰–17⁴⁰ . = 2¹⁴⁵ 24
24	6	4.9	.	–	●⁰ 1²⁰–2³⁵ , 8⁰⁵–9²⁵ , 10⁵⁰ 11¹⁰ ●¹–12¹⁵ ●⁰–15¹⁵ , 15⁵⁰ 16¹⁵ , ≫ 15⁴⁰–16¹⁰ , 17²⁵–18⁰⁶ , 21⁵⁰–22³⁵ . = 0⁰⁰–16³⁰
25	8	.	.	–	≫ 4¹⁰–5²⁸
26	7	.	.	–	⌴¹ n.a
27	7	1.6	.	–	●⁰ 15¹¹ 16³⁰ 18¹³–21³⁵ , 23⁵⁵–24 , ≫ 16⁰²–³⁵ 17⁵⁰–18¹⁰ , 23³⁵–24 . ⌴¹ n.a
28	8	0.4	.	–	●⁰ 0⁰⁰–³⁵ 1²⁰–⁵⁰ 2³⁰–3²⁵ ▽ 11⁰⁵–¹⁰ 11⁵⁰–12³⁵ , 14⁴⁰–15¹⁰ 16¹⁰–¹⁵ 16²⁵–40 . ≫ 0⁰⁰–6⁴⁵ , 8¹⁵–9³⁰ 10³² 19²⁵ . ⌓ 16¹⁰–¹⁵
29	7	3.2	.	–	▽ 0³⁸–1²⁰ , 2⁰⁶–¹⁵ ●⁰ 6³³–7¹⁶ , 10⁴⁰–15²⁰ . = 5³⁵–6³³ , 8⁴⁵–10⁴⁰ 17⁴⁰–23⁴⁵ . ◡ 23¹⁰–24
30	7	1.0	.	–	●⁰ 6⁵⁵ 8¹⁵ ▽ 12⁰⁵–³⁰ , 12⁴⁵–15¹⁶ . ≫ 9⁰⁰–14⁰⁰ . ⌒ 15⁰⁷–¹⁰ . ◡ 0⁰⁰–2⁰⁵
31					
Σ	–	94.2	–	–	UWAGI.

Październik – Octobre

1	8	0.3	.	–	▽ 14²⁵–15¹⁰ . = 0⁰⁰–4⁰⁵ ≡⁰–4²⁵ ≡¹–4⁴⁰ ≡²–7⁴⁵ = –9³⁰ 23³⁵–24 . ⌴ 22⁰⁰–24
2	7	.	.	–	= 0⁰⁰–5¹⁰ ≡ –6³⁵ = –9⁵³ 17⁵⁰–24 . ⌴² 0⁰⁰–8¹⁰ ⌴¹ 22⁴⁰–24
3	6	0.0	.	–	●⁰ 12¹⁵ 13¹² 15¹⁵ 16³⁰ ●● ⁰–17⁴⁰ ●⁰ 19⁵⁰–20¹⁰ . = 0⁰⁰–12¹⁵ , 20¹⁰–24 . ⌴² 0⁰⁰–8¹⁰
4	7	1.2	.	–	▽ 7⁴⁰–8²⁰ 9⁵⁰–10¹⁵ , 12¹⁵–³⁵ , 12⁴⁸–13¹⁰ , 14²²–15¹⁵ . = 0⁰⁰–3³⁰
5	7	1.2	.	–	▽ 0²⁵–³⁸ , ●⁰ 18⁴⁰–24
6	7	0.0	.	–	●⁰ 0⁰⁰–40 ●● ⁰ 3⁵⁰–4¹⁰ ●⁰–6²⁰ ●8²⁰–³⁰ ●⁰ 11⁴⁰–⁵⁰ . = 1³⁰–3⁵⁰
7	7	.	.	–	= 4³⁰–11³⁰ , 18⁰⁵–24 . ⌓ 20⁴⁵–24
8	6	.	.	–	= 0⁰⁰–²⁰ ≡⁰–1⁴² = –24 . ⌓ 0⁰⁰–²⁰ ⌓² 22³⁰–24
9	5	.	.	–	= 0⁰⁰–12⁰⁰ ∞ –16⁰⁰ = –24 . ⌓² 0⁰⁰–9³⁰
10	7	.	.	–	= 0⁰⁰–9⁴⁰ ∞ –12⁵⁰ , 16⁴⁵–17⁵⁰ = –24 . ⌓ n.a – a , p – 24
11	4	.	.	–	= 0⁰⁰–8⁴⁰ ≡²–10³⁰ = –18³⁰ ≡²–24 . ⌓ 0⁰⁰– a
12	4	.	.	–	≡² 0⁰⁰–2²⁰ ≡¹–4⁰⁰ ≡⁰–5⁴⁵ = –10³⁵ ≡⁰–11⁵⁰ = –24 . ◡ 20⁴⁰–24
13	5	0.2	.	–	= 0⁰⁰–1⁰⁰ ≡⁰–1²⁵ ≡¹–9⁴⁰ = –20⁴⁵ ≡¹–22³⁰ ≡²–24 . ◡ 0⁰⁰–6¹⁵
14	6	0.0	.	–	● ⁰ 3³⁰–7¹⁸ ● ¹ 8¹⁵–40 . ≡² 0⁰⁰–5²⁵ ≡¹–8¹⁰ = 8⁴⁰–13⁵⁰ ∞ –16⁵⁵ = –24
15	6	.	.	–	= 0⁰⁰–2⁴⁰ ≡⁰–3²⁰ ≡¹–5¹⁰ ≡⁰–5⁴⁵ = –24
16	6	.	.	–	= 0⁰⁰–12²⁰ ∞ –17⁰⁰ = –24
17	6	0.0	.	–	▽ 8³⁰–45 ●⁰ 9⁴⁰ 10⁰⁵ . = 0⁰⁰–1⁴⁰ ≡⁰–5⁴⁰ = –24 . ⌓ n.a ⌓¹ 20³⁰–24
18	6	0.5	.	–	●⁰ 7³⁰ 11¹⁵ . = 0⁰⁰–7²⁰ , 11¹⁵–15²⁰ , 23⁴⁵–24 . ⌓¹ 0⁰⁰– n.a
19	7	1.8	.	–	= 0⁰⁰–8⁴⁵ , 16⁴⁵–24
20	6	1.1	.	–	●⁰ 2²⁰–10⁴⁰ ▽ 11³⁵–15²⁵ . = 0⁰⁰–20²⁰ ≡¹–20⁴⁰ ≡²–24
21	5	.	.	–	≡² 0⁰⁰–7¹⁰ ≡⁰–11¹⁰ = –24
22	6	.	.	–	= 0⁰⁰–10⁴⁰ ∞ –16³⁵ = –24 . ⌴⁰ n.a
23	6	0.2	.	–	= 0⁰⁰–45 ≡ –2²⁰ = –7¹⁰ ≡⁰–7⁵⁰ = –24
24	6	2.8	.	–	●⁰ 2¹⁵–4²⁰ 5²⁰–9²⁰ ●¹–10¹⁵ ●⁰–11²⁵ ●¹–11³⁸ ●²–13²⁰ ●¹–15³⁰ . = 0⁰⁰–2¹⁵ 15³⁰–23³⁵ ≡⁰–24
25	6	.	.	–	≡⁰ 0⁰⁰–1³⁰ ≡¹–2¹⁵ ≡⁰–5⁴⁵ = –6⁴⁰ ≡⁰–7⁰⁰ ≡²–9²⁰ ≡⁰–9³⁵ = –15³⁰ , 18²⁰–24 . ⌓ n.a ⌓⁰ n.p
26	6	.	.	–	= 0⁰⁰–11²⁰ ∞ –13³⁵ = 16⁵⁰–24 . ⌓¹ n.a
27	6	.	.	–	= 0⁰⁰–5⁵⁰ ≡²–8²⁰ = –24
28	6	.		–	= 0⁰⁰–11⁰⁰ ∞ –16⁰⁰ = –24
29	6	.	.	–	= 0⁰⁰–24
30	6	0.0	.	–	●⁰ 14⁰⁵–10 20¹⁵ 21¹⁰ . = 0⁰⁰–10³⁰ ∞ –15⁴⁵ = –20¹⁵ , 21¹⁰–24 . ⌓¹ n.a
31	4	.	.	–	= 0⁰⁰–12⁴⁵ ∞ –16⁴⁰ = –24
Σ	–	9.5	–	–	UWAGI.

Poznań – Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ Listopad – Novembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	94.3	93.7	96.6	94.9	8.9	13.3	9.4	10.2	13.8	7.0	85	66	89	80	1.7	5.2	1.3	2.7	10	9	3	S 4	SSW 8	SSW 5
2	100.1	101.1	103.1	101.4	2.8	11.9	3.4	5.4	12.2	2.3	100	60	95	85	0.0	5.5	0.4	2.0	5	8	4	S 3	SSW 6	SSW 4
3	104.8	104.3	101.8	103.6	0.5	12.5	7.3	6.9	13.1	-0.6	98	56	97	84	0.1	6.4	0.3	2.3	0	3 ⊙	0	SE 2	SE 2	SE 3
4	100.9	100.2	100.6	100.6	5.5	13.4	7.3	8.4	14.5	4.5	100	77	96	91	0.0	3.5	0.4	1.3	10 ≡	5	4	C 0	SE 3	SE 2
5	97.8	94.7	95.4	96.0	6.1	16.7	8.4	9.9	17.0	2.8	97	60	86	81	0.3	7.7	1.5	3.2	5	9	3	SE 4	SE 6	SE 2
6	95.6	97.3	96.0	96.3	6.7	11.7	7.0	8.1	12.3	5.8	96	82	96	91	0.4	2.5	0.4	1.1	7	9	6	SE 2	SSE 2	ENE 3
7	92.4	95.1	97.6	95.0	9.0	10.5	7.9	8.8	11.1	5.9	88	85	100	91	1.4	1.9	0.0	1.1	10	10	10	SE 3	SW 5	SSW 2
8	96.2	96.0	96.2	96.1	8.6	13.6	11.3	11.2	14.8	7.4	96	77	90	88	0.5	3.5	1.3	1.8	10	9	9	ENE 5	E 2	E 3
9	95.2	95.8	97.3	96.1	6.9	9.2	8.5	8.3	11.4	6.2	99	93	94	95	0.1	0.8	0.6	0.5	8	10 ●	7	E 4	E 4	E 3
10	98.9	99.8	102.4	100.4	5.7	9.1	9.1	8.2	9.9	4.7	100	100	89	96	0.0	0.0	1.3	0.4	10 ≡	10	10	E 2	ENE 7	ENE 8
11	104.6	107.0	110.4	107.3	9.2	9.7	7.8	8.6	10.3	7.3	85	78	80	81	1.7	2.6	2.1	2.1	10	10	10	ENE 8	ENE 10	ENE 12
12	113.4	116.4	118.9	116.2	6.4	5.9	3.1	4.6	8.3	2.7	76	79	88	81	2.3	2.0	0.9	1.7	10	10	10	NE 10	ENE 8	NE 5
13	119.5	120.2	120.9	120.2	2.9	2.5	-0.3	1.2	3.5	-0.6	71	67	76	71	2.2	2.4	1.5	2.0	10	10	10	ENE 3	NE 5	E 5
14	120.8	121.4	122.2	121.5	-1.9	-1.6	-2.4	-2.1	0.2	-2.7	82	78	89	83	0.9	1.2	0.5	0.9	10	9	10	ENE 4	ESE 3	ESE 3
15	121.7	121.0	119.8	120.8	-2.7	-1.8	-1.4	-1.8	-1.4	-3.4	93	92	97	94	0.3	0.4	0.2	0.3	10	10	10	SE 3	SE 2	E 2
16	119.7	120.5	121.6	120.6	-0.7	0.3	0.6	0.2	0.9	-1.9	91	92	90	91	0.5	0.5	0.6	0.5	10	10	10	E 2	ENE 3	ENE 2
17	121.5	121.8	122.2	121.8	0.6	1.9	1.0	1.1	2.2	-0.1	88	75	87	83	0.8	1.9	0.9	1.2	10	10	0	E 6	E 6	E 5
18	122.0	121.7	121.1	121.6	1.4	2.9	1.9	2.0	3.0	0.1	79	71	80	77	1.4	2.2	1.4	1.7	10	10	10	E 4	ESE 3	E 1
19	121.3	123.7	126.3	123.8	1.6	2.1	1.7	1.8	2.5	0.9	83	73	69	75	1.2	1.9	2.1	1.7	10	10	10	E 2	E 5	ESE 7
20	127.2	127.5	128.0	127.6	-1.1	3.6	-3.0	-0.9	3.9	-3.4	79	54	88	74	1.2	3.7	0.6	1.8	0	0	0	E 5	SE 6	SE 2
21	127.0	124.7	120.1	123.9	-5.2	5.0	-1.0	-0.6	5.5	-5.9	95	60	85	80	0.2	3.5	0.9	1.5	0	0	0	E 2	ESE 4	SE 2
22	112.4	108.9	106.8	109.4	-5.3	2.3	0.6	-0.4	3.1	-5.8	98	75	81	85	0.1	1.8	1.3	1.1	0	8	10	SE 3	SSW 5	SSW 3
23	105.1	104.2	109.8	106.4	1.1	2.0	2.9	2.2	3.5	0.1	75	96	88	86	1.6	0.3	0.9	0.9	10	10 ●	10 ✱	SW 5	SW 8	W 9
24	112.1	111.1	110.0	111.1	-0.3	3.1	5.7	3.6	5.9	-1.0	94	95	85	91	0.4	0.4	1.5	0.8	9	10	10	WSW 5	W 9	W 9
25	107.7	108.0	109.8	108.5	5.3	6.8	7.2	6.8	7.4	4.8	97	96	100	98	0.3	0.5	0.0	0.3	10 ●,	10 ,	10 ,	WSW 9	W 10	W 7
26	111.2	111.5	110.0	110.9	6.7	7.2	6.6	6.8	7.9	6.2	99	96	91	95	0.1	0.5	0.8	0.5	10 ,	10 ,	10	W 9	WSW 7	SW 8
27	105.9	106.0	107.8	106.6	6.5	8.7	6.0	6.8	8.9	5.1	90	76	82	83	1.0	2.7	1.8	1.8	10	10	10	WSW 9	W 11	W 8
28	103.8	101.5	97.3	100.9	8.2	8.5	8.1	8.2	9.3	5.3	94	90	79	88	0.6	1.1	2.3	1.3	10	10	7	WSW 10	WSW 10	NW 10
29	99.7	103.7	117.3	107.6	3.3	0.9	-3.6	-0.8	8.2	-4.2	90	92	71	84	0.7	0.5	1.4	0.9	7	9 ✱	5	NNW 10	NW 11	NNE 9
30	121.8	122.0	121.8	121.9	-5.1	-1.6	-5.3	-4.3	-1.1	-8.2	88	73	95	86	0.5	1.3	0.2	0.7	9	9 ✱	1	NW 6	N 5	NNW 6
31																								
M	109.2	109.4	110.3	109.6	3.1	6.4	3.9	4.3	7.4	1.4	90	79	88	86	0.8	2.3	1.0	1.4	8.0	8.6	7.0	4.8	5.9	5.0

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1	120.6	118.6	115.0	118.1	-5.7	-1.7	-1.3	-2.5	-1.1	-9.9	92	88	97	92	0.3	0.7	0.2	0.4	8	9	10 ✱	W 2	WSW 6	WSW 5
2	115.4	116.4	116.8	116.2	0.5	1.4	1.2	1.1	1.6	-1.6	98	98	98	98	0.1	0.2	0.2	0.2	10	10	10	N 3	NW 4	NW 2
3	113.5	111.6	112.7	112.6	1.6	3.2	3.1	2.8	3.4	0.7	98	100	100	99	0.2	0.0	0.0	0.1	10 ≡	10 ,	10 ,	WNW 3	NW 4	NNW 5
4	113.1	112.4	110.9	112.1	2.2	2.8	3.4	3.0	3.7	2.1	100	100	97	99	0.0	0.0	0.3	0.1	10 , ≡	10	10	NW 3	W 5	WSW 6
5	108.5	109.7	113.0	110.4	5.4	6.0	4.9	5.3	6.2	2.7	97	80	90	89	0.3	1.9	0.9	1.0	10	9	9	W 8	WNW 10	NW 5
6	116.2	116.1	112.8	115.0	-0.2	0.4	-0.8	-0.4	4.9	-1.1	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡	10 ≡	10	NW 4	SW 1	SSW 2
7	104.9	101.2	95.2	100.4	-1.8	1.0	-0.4	-0.4	1.3	-2.5	90	87	90	89	0.5	0.9	0.6	0.7	2	10	10 ✱	SW 3	SW 5	SSW 7
8	79.8	70.7	66.8	72.4	0.9	2.7	7.2	4.5	9.6	-1.0	88	98	83	90	0.7	0.1	1.8	0.9	10	10 ●	6	SSW 7	SSW 8	WSW 9
9	66.3	76.4	87.1	76.6	5.5	2.4	-1.8	1.1	8.8	-2.4	72	82	81	78	2.5	1.3	1.0	1.6	9	9 ●	3	WNW 10	WNW 10	WSW 4
10	85.9	85.9	96.6	89.5	-3.5	-0.2	-5.8	-3.8	0.9	-6.3	85	96	84	88	0.7	0.2	0.6	0.5	9	10 ✱	0	SSW 3	WSW 7	W 4
11	96.7	92.7	89.3	92.9	-8.2	-2.2	-2.4	-3.8	-1.9	-9.7	89	72	72	78	0.3	1.5	1.4	1.1	0	7	10	ESE 3	ESE 5	E 7
12	86.2	85.7	84.9	85.6	-1.8	2.1	-1.6	-0.7	2.5	-3.0	88	82	96	89	0.7	1.3	0.2	0.7	9	7	0	E 7	E 5	E 3
13	82.0	79.1	74.0	78.4	-1.1	2.4	1.3	1.0	3.1	-2.9	98	93	98	96	0.1	0.6	0.1	0.3	10	9	10 ●	ENE 4	NNE 2	NNE 3
14	74.0	80.8	92.7	82.5	1.2	0.6	-1.8	-0.4	2.1	-2.1	96	92	90	93	0.3	0.5	0.3	0.4	10 ●	10 ✱	10 ✱	N 6	NNE 6	NE 12
15	105.3	111.6	117.1	111.4	-6.0	-5.2	-11.4	-8.5	-1.3	-11.5	79	68	79	75	0.8	1.3	0.3	0.9	7	8	0	NE 7	NNE 9	ENE 5
16	118.8	119.2	118.1	118.7	-12.1	-7.2	-10.6	-10.1	-6.5	-14.5	85	74	70	76	0.4	0.9	0.8	0.7	4	2	0	E 4	ESE 3	ESE 5
17	114.1	112.8	112.2	113.0	-13.6	-9.2	-8.7	-10.0	-8.4	-14.7	84	88	92	88	0.4	0.4	0.3	0.4	3	10 ✱	10	E 3	ENE 2	C 0
18	113.4	113.6	114.1	113.7	-7.3	-5.6	-5.1	-5.8	-5.0	-9.0	90	92	90	91	0.3	0.3	0.4	0.3	10 ✱	10	10	WSW 1	C 0	S 2
19	113.7	115.4	119.2	116.1	-4.8	-2.9	-1.9	-2.9	-1.7	-5.6	91	88	90	90	0.4	0.5	0.5	0.5	10	9	10 ✱	SE 5	SE 2	SE 1
20	121.3	122.2	120.3	121.3	0.5	2.0	-0.2	0.5	2.2	-2.3	100	89	90	93	0.0	0.8	0.6	0.5	10 ≡	6	0	SW 3	SW 5	SW 5
21	115.6	115.0	116.4	115.7	0.0	1.9	1.9	1.4	2.3	-2.6	84	82	96	87	1.0	1.3	0.3	0.9	10	9	10	SSW 6	SSW 7	SW 5
22	115.3	115.3	114.3	115.0	1.1	2.2	1.8	1.7	2.5	0.4	98	93	100	97	0.1	0.6	0.0	0.2	10 ,	10	10	SSW 5	SSW 3	S 2
23	109.6	107.9	105.8	107.8	-1.9	-1.1	-2.9	-2.2	2.6	-3.5	96	75	84	85	0.2	1.4	0.8	0.8	0	7	0	SE 5	SSW 3	SSE 3
24	105.6	106.0	106.9	106.2	-4.7	-0.7	-4.2	-3.4	-0.3	-5.2	86	75	87	83	0.6	1.4	0.6	0.9	3	7	0	SSE 3	SE 2	SSE 2
25	107.3	107.1	109.2	107.9	-5.8	-0.7	-1.8	-2.5	-0.5	-6.7	95	79	90	88	0.2	1.2	0.5	0.6	2	9	0	SSE 2	S 4	SW 2
26	111.7	113.6	115.4	113.6	-2.0	1.2	1.8	0.7	2.1	-4.4	89	92	96	93	0.6	0.3	0.2	0.4	9	9	10 ≡	SW 3	W 3	WSW 3
27	114.6	114.2	112.6	113.7	0.3	1.3	1.1	1.0	2.6	-0.1	94	94	94	94	0.3	0.4	0.4	0.4	9	10	10 ●	SW 5	SW 4	SSW 4
28	107.3	104.0	99.6	103.6	0.7	1.3	1.3	1.3	2.3	0.1	94	92	92	93	0.4	0.3	0.3	0.3	9	10 ●	10 ●	SSW 5	SW 7	SW 6
29	97.3	95.8	90.3	94.5	2.4	2.3	2.4	2.4	2.9	0.8	93	93	89	92	0.6	0.4	0.8	0.6	10	10	10	WSW 7	WSW 9	SSW 11
30	87.8	85.6	85.8	86.4	2.4	3.4	2.6	2.8	4.0	0.9	91	95	89	91	0.7	0.5	0.8	0.7	10	10	9	SW 10	WSW 11	WSW 8
31	89.6	90.3	90.1	90.0	1.1	1.4	1.2	1.2	2.7	0.6	83	83	90	85	1.1	1.1	0.7	1.0	9	9	9	WSW 6	WSW 6	WSW 6
M	103.6	103.4	103.7	103.6	-1.8	0.2	-0.9	-0.8	1.3	-3.7	91	88	90	90	0.5	0.7	0.5	0.6	7.8	8.9	7.0	4.7	5.1	4.6

Poznań – Ławica $H_s = 86\ m$ $H_b = 92.1\ m$ $h_w = 13\ m$ **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	-	-	●° 16⁴⁰... 17²⁰; = 0⁰⁰–10⁰⁰, 17²⁰–24
2	7	.	.	-	= 0⁰⁰–10³⁰ ∞–12⁴⁰ = 15⁵⁰–24; ⌓ na, n/p
3	7	.	.	-	= 0⁰⁰–9⁴⁵ ∞–12³⁵ = 15⁵⁰–24; ⌴ 5³⁰–18⁵⁰
4	6	.	.	-	= 0⁰⁰–1⁴⁵ ≡¹–2²⁰ ≡²–10⁰⁰ =–24
5	7	.	.	-	= 0⁰⁰–11⁰⁰, 17³⁰–24; ⌔ 18⁰⁰–24
6	6	.	.	-	= 0⁰⁰–24; ⌓ na, n/p; ⌔ 0⁰⁰–2⁰⁰, 19³⁰–24
7	5	0.5	.	-	●°8¹⁰...⁵⁰ 9⁵⁰ 10²⁰ 14¹⁸ 17⁴⁵; = 0⁰⁰–24; ⌔ 0⁰⁰–3³⁰
8	5	0.0	.	-	●°3³⁰–4³⁵, 19²⁰ 20⁰⁰ = 0⁰⁰–24
9	5	0.0	.	-	●° 10³⁰–14⁴⁰; = 0⁰⁰–10³⁰, 12⁴⁰–24
10	4	.	.	-	= 0⁰⁰–3⁴⁰ ≡°–5³⁰ ≡²–11⁵⁰ ≡°–12³⁰ =–24
11	7	.	.	-	≫ 0²⁰–15⁴⁰, 19¹⁵–24 (20²⁰–23⁴⁵ por. ponad 15 m/sek); = 0⁰⁰–9³⁰; ⌓ 19⁵⁰–24
12	7	.	.	-	≫ 0⁰⁰–7⁴⁰; ⌓ 0⁰⁰–2⁵⁰
13	7	.	.	-	
14	6	.	.	-	= 9³⁰–24
15	5	.	.	-	= 0⁰⁰–24
16	4	.	.	-	= 0⁰⁰–24
17	7	.	.	-	= 0⁰⁰–10³⁰, 16²⁰–24
18	6	.	.	-	= 0⁰⁰–24
19	6	.	.	-	= 0⁰⁰–13⁴⁵ ∞–17³⁵ =– 18⁴⁰ ∞–24
20	7	.	.	-	∞ 0⁰⁰–3⁴⁰ = 6²⁵–8³⁵ ∞–9⁴⁰, 15³⁰–17¹⁵ =–24
21	6	.	.	-	= 0⁰⁰–11⁰⁰ ∞–15⁰⁰ =–24
22	6	.	.	-	= 0⁰⁰–10²⁰ ∞–13³⁰ =–24; ⌴ 3⁵⁰–9³⁰
23	5	0.6	.	-	✱° 10²⁰–54 ●° 11⁵⁰–12⁰⁵ ✱°–12³⁵ ●°–15⁴⁰ ✱° 18⁴⁵–19⁵⁰ 20³⁵–21²⁰ ●°23⁴² 24; ≫ 17⁴⁰–20¹⁵; = 0⁰⁰–24
24	6	0.3	.	-	●° 0⁰⁰ 1²⁷ ●° 10¹⁵ 11⁴⁵ ●°·°12¹⁰ 13⁴⁰ 15⁰⁵; ≫ 15⁴⁰–16³⁰; = 0⁰⁰–1⁴⁰ 7²⁰–17¹⁵, 21¹⁵–24
25	6	3.1	.	-	●° 2¹⁰–6⁰⁰ ●°·°7¹⁰ ●¹–8³⁰ ●°, 9¹⁵ ●°–9³⁰ ●°, 11⁰⁰ 11²⁰–14²⁰ ●°–19⁰⁰ ●¹–24 = 0⁰⁰–2¹⁰, 11⁰⁰–20
26	5	0.7	.	-	●° 0⁰⁰–3⁰⁰ ●°–6²⁰ ●¹–7⁴⁰ ●°–8³⁵ ●¹–11²⁰ ●°–16²⁵ 19³⁰–20¹⁵, 22¹⁰–24; = 8³⁵–24
27	6	1.6	.	-	●° 0⁰⁰–25, 2⁰⁰–3⁴⁵ 7²⁰ 10⁵⁰ ●° 23²⁷–24; ≫ 7³⁵–14³⁰ 15¹⁸–16¹²; = 0⁰⁰–14²⁰
28	5	6.0	.	-	●° 0⁰⁰–1²⁰ ●¹–2⁴² ●° 3¹⁰–6³⁶ 8¹⁸–9³⁰ ●° 12¹⁰ ●° 16³⁰–17⁴⁰ ●¹–18⁴⁵ ●²–19¹⁰ ●°–20⁰⁰, ≫ 6³⁰–18¹⁵, 19⁰⁰–24 (por. do 17 m/sek);
29	7	0.2	.	-	▽ 4⁰⁵–5²⁰ ●° 5⁴⁰–6⁰⁰ ▲¹–6¹² ●△ 18³⁰–42 ✱° 12¹⁰–13⁰⁰, 13⁴⁸–14¹⁰ 20²⁰–35; ≫ 0⁰⁰–7²⁰ ≫ ⩓ 9¹⁰–13³⁰ ≫ 18⁰⁵–22¹⁵
30	7	0.0	.	-	✱ 9⁴⁰–10¹⁰, 12⁴⁵–14⁵⁰; ⌓ na–a, 20³⁰–24 [28.XI: = 6³⁶–24] [29.XI: (18⁰⁵–19³⁵ por. do 18 m/sek)
31					
Σ	–	13.0	–	-	UWAGI.

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1	7	2.3	pż.	-	✱° 13¹⁵–21³², ●¹–22⁴⁵ ●°–23¹⁵ ✱°–24; ⌓ 0⁰⁰–13²⁰
2	4	0.8	1	-	✱° 0⁰⁰–1³⁰ ●°–3³¹ 22¹⁰–24; ≡¹ 7¹⁶–8⁴⁰, 14⁵⁰–15³⁵ =–24
3	4	0.6	.	-	●° 0⁰⁰–2³⁰ 3⁴⁰–4²⁰ 8¹⁵ 17⁴⁰ 19³⁰–24; = 0⁰⁰–6⁵⁰ ≡°–7⁴⁰ =–19³⁰
4	4	0.8	.	-	●° 0⁰⁰ 7²⁰ ●° 22²⁵–24; ≡° 6³⁰–7¹⁵ =–9¹⁰ ≡¹–9³⁵ =–22²⁵
5	7	.	.	-	●° 0⁰⁰–2²⁰ ●° 4¹⁵; ≫ 7³⁵–15³⁰; = 4¹⁵–8⁴⁰, 11²⁰–12¹⁰
6	3	.	.	-	≡¹ 2⁴⁰–4⁵⁰ =–6³⁵ ≡¹–13⁴⁰ =–24
7	3	0.3	.	-	✱° 20³⁵, 21¹⁰; = 0⁰⁰–24; ⌓ ¹ 21⁰–10¹⁵
8	6	10.0	1	-	✱° 1¹⁰–25 2¹⁵–4⁴⁰ ●° 7⁴⁸–10³⁰ ●¹–16⁰⁰ ●°–17³⁰ ●¹–18¹⁰; ≫ 17⁰⁰–24; = 0⁰⁰–1¹⁰
9	7	0.4	.	-	●° 9²⁰–12¹⁰ ▽ 12³⁵–13²⁶ ⁂–13³⁰ ▽ 15⁰⁸–12; ≫ 0⁰⁰–2⁵⁰ ⩓–6⁴⁰ ≫–7²⁰, 9¹⁵–10³⁵ ⩓–12¹² ≫–14¹⁸; ⌓° 19²⁵–24
10	3	0.2	.	-	✱° 12⁰⁰–13⁵⁰; ≫ 13³⁰–14⁰⁰ ⩓–14¹⁵; = 9⁴⁰–14⁴⁰; ⌓° 0⁰⁰–9³⁰; ⌔ na
11	6	.	1	-	= 6⁴⁵–13⁰⁰ ∞–19⁰⁰; ⌔ 22⁰⁰–24
12	3	0.0	1	-	●° 10⁴⁰ 11⁰⁵; = 3³⁰–24; ⌓¹ 19¹⁰–24; ⌔ 0⁰⁰–2⁰⁰
13	3	0.8	pż.	-	●° 19²⁶–20⁴⁰ ●¹–21¹⁰ ●°–22²⁰; = 0⁰⁰–19²⁶, 22²⁰–23²⁵ ≡°–24; ⌓¹ 0⁰⁰–10¹⁸
14	3	6.0	.	-	●° 6²⁰–12¹⁰ ✱°–24; ≡° 0⁰⁰–1⁴⁰ =–6²⁰
15	7	.	3	-	✱° 0⁰⁰–2¹²; = 2¹²–3¹⁵
16	3	.	3	-	= 5⁰⁰–13⁰⁰ ∞–21³⁵ =–24
17	3	0.0	3	-	✱° 8²⁰ 9¹⁰ 11⁴⁰ 13³⁰; = 0⁰⁰–24
18	3	0.0	3	-	✱° 6⁴⁵ 7⁰⁵; = 0⁰⁰–24
19	6	0.0	3	-	✱° 20³⁵–21²⁰; = 0⁰⁰–24
20	3	.	2	-	= 0⁰⁰–1³⁸ ≡¹–9⁵⁰ =–24
21	6	1.1	1	-	●° 21⁰⁸ 22¹⁵ ●¹–23¹⁰ ●°–24; = 0⁰⁰–24
22	3	0.0	pż.	-	●° 0⁰⁰–1³⁵ 4³⁵–5²⁰ 6⁴⁰–7³⁰, 8⁴⁰–9¹⁰, 14³⁰–15⁰⁵ 17⁴⁰–18¹⁰; = 0⁰⁰–24
23	6	.	pż.	-	= 0⁰⁰–24; ⌓° 6³⁰–24
24	6	.	pż.	-	= 0⁰⁰–24; ⌓° 0⁰⁰–7⁰⁵ ⌓ n/p
25	6	.	pż.	-	= 0⁰⁰–24; ⌓° na–a ⌓° n/p
26	3	.	pż.	-	= 0⁰⁰–11⁴⁵ ≡°–12²⁰ =–19¹⁸ ≡°–19⁴⁵ ≡¹–24; ⌓° na–9³⁰
27	4	0.0	.	-	≡¹ 0⁰⁰–40 ≡°–1⁴⁵ =–24
28	6	1.8		-	●° 0²⁵ 1³⁰ ●° 19²⁰–24; = 0⁰⁰–19²⁰
29	3	0.7	.	-	●° 0⁰⁰ 1⁴⁵ 11¹⁸–13³⁵ 17²⁰–18¹⁶ 20¹⁰ 21¹⁵ 22²⁰ 24; = 1⁴⁵–11¹⁸ 13³⁵–17²⁰ 18¹⁶–20¹⁰; ≫ 20²⁵–24 (22³⁰–24 por. 18 m/sek)
30	6	2.0	.	-	●° 0⁰⁰..⁴⁰ 4⁵⁰ 5¹⁵ 8³⁰ 9⁴⁵ ●¹ 9⁵⁵ ●² 10⁰⁵ ●¹–11¹⁵ ●° 11²⁰–11³⁵ ●¹–12³⁰ ●°–12⁴⁵ ▽ 13⁴⁰–14³⁰ ●° 15⁴⁵ 18³⁰ ●¹–19⁴⁰; ≫ 0⁰⁰–9¹⁰
31	7	1.3	.	-	✱ 14¹⁵–21; = 0⁰⁰–4⁰, 14²¹–19⁰⁰; ⌔ 15⁴⁵–17²⁰ [30.XI: (0⁰⁰–1³⁵ por. 16 m/sek), 12³⁰–13⁴⁰ 18¹⁵–19²⁰ 21²⁰–22³⁰; = 0⁴⁰–4⁵⁰, 5¹⁵–24]
Σ	–	29.3	–	-	UWAGI.

Warszawa – Bielany

$\varphi = 52°17'$ $\lambda = 20°58'$

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DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI ^				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	105.8	104.9	104.3	105.0	-7.0	-5.9	-3.6	-5.0	-3.6	-9.2	77	92	90	86	0.8	0.3	0.5	0.5	10	10 ✳	10	SE 5	SE 5	SE 4
2	102.2	100.5	103.3	102.0	-1.9	0.9	1.1	0.3	2.6	-3.6	87	81	92	87	0.7	1.2	0.5	0.8	10	10	10	SE 3	SE 2	C 0
3	107.9	109.5	109.6	109.0	0.6	0.7	1.2	0.9	1.5	-0.2	98	100	100	99	0.1	0.0	0.0	0.0	10	10	10	C 0	SSW 1	C 0
4	110.7	112.1	112.6	111.8	0.6	0.9	-1.8	-0.5	1.6	-3.1	98	90	94	94	0.1	0.6	0.3	0.3	5	9 ⊙	8	SSW 2	SSW 1	SSW 1
5	111.1	107.6	101.3	106.7	-1.0	1.4	2.9	1.6	3.1	-3.1	99	87	100	95	0.1	0.9	0.0	0.3	5	10	10 ●	SSW 2	SSW 3	SSW 7
6	98.5	94.4	96.0	96.3	5.6	6.7	4.2	5.2	7.4	2.9	98	97	85	93	0.2	0.3	1.2	0.6	10	10	6	SW 6	WSW 8	WSW 5
7	98.2	103.1	109.8	103.7	3.4	4.7	2.9	3.5	4.9	3.1	85	70	83	79	1.2	2.5	1.3	1.7	10	7	2	W 10	W 12	W 6
8	112.6	110.7	109.1	110.8	3.0	3.7	4.2	3.8	4.4	2.6	98	98	98	98	0.2	0.2	0.1	0.2	10 ●	10 ☽	10 ☽	SW 4	W 5	SW 6
9	107.8	106.3	104.5	106.2	5.7	6.6	6.2	6.2	6.6	4.2	97	88	88	91	0.3	1.1	1.2	0.9	10	10	10	SW 5	SW 5	W 3
10	99.3	98.1	97.4	98.3	4.9	4.7	2.5	3.6	6.4	2.5	87	85	79	84	1.1	1.2	1.5	1.3	10	10 ●	3	SW 6	W 3	W 4
11	99.0	101.8	103.8	101.5	1.3	2.4	0.9	1.4	2.8	0.9	85	75	83	81	1.0	1.8	1.1	1.3	10 ✳	6 ⊙	10	W 7	WNW 6	SW 4
12	101.5	96.5	91.2	96.4	-0.4	0.1	0.4	0.1	1.2	-0.8	82	92	98	91	1.1	0.5	0.1	0.6	9	10 ✳	10 ✳	SW 3	SW 4	SW 5
13	90.5	92.6	97.9	93.7	0.2	0.5	-0.6	-0.1	0.8	-0.6	94	92	93	93	0.4	0.5	0.4	0.4	10 ✳	10 ✳	10 ✳	S 2	S 1	ENE 1
14	105.6	110.4	114.5	110.2	-5.5	-5.8	-7.5	-6.6	-0.5	-7.6	87	79	76	81	0.5	0.8	0.8	0.7	10 ✳	10	10	NE 5	NE 5	NE 5
15	114.9	114.3	113.6	114.3	-7.4	-7.3	-10.8	-9.1	-6.5	-10.9	82	79	90	84	0.6	0.7	0.3	0.5	10	9 ⊙	0	NE 5	NE 3	NE 3
16	116.3	117.5	118.6	117.5	-14.7	-11.7	-14.3	-13.8	-10.8	-14.9	91	86	87	88	0.2	0.3	0.3	0.3	0	0 ⊙	0	C 0	C 0	C 0
17	118.1	117.2	117.3	117.5	-9.3	-4.8	-3.0	-5.0	-1.5	-14.9	95	95	97	96	0.2	0.2	0.1	0.2	10	10	10 ☽	SW 4	WSW 2	SW 3
18	114.9	113.8	113.6	114.1	-2.9	-3.0	-4.4	-3.7	-2.5	-4.4	97	95	96	96	0.1	0.3	0.2	0.2	10	10	10	W 5	W 3	W 4
19	113.6	115.4	117.1	115.4	-3.1	-1.8	-2.3	-2.4	-1.8	-4.4	97	98	93	96	0.1	0.1	0.4	0.2	10 ☽	10	10	SW 1	SW 2	W 2
20	116.7	114.6	112.2	114.5	-3.5	-2.2	-2.5	-2.7	-0.5	-3.5	97	94	91	94	0.1	0.3	0.5	0.3	10	10	10	W 3	W 5	W 7
21	108.5	108.6	110.1	109.1	-5.6	-0.5	-3.5	-3.3	0.3	-6.7	82	62	74	73	0.7	2.2	1.2	1.4	3	0 ⊙	0	SW 4	SW 3	SW 3
22	111.1	110.5	107.6	109.7	-6.9	-0.7	-4.7	-4.2	0.4	-7.9	77	62	76	72	0.8	2.2	1.0	1.3	2	6 ⊙	0	SW 3	SW 4	S 3
23	106.4	106.8	107.6	106.9	-7.4	-1.8	-5.9	-5.2	-1.0	-8.4	76	73	79	76	0.8	1.4	0.8	1.0	0	8 ⊙	0	SW 4	SW 3	S 1
24	104.1	101.1	98.9	101.4	-6.4	-1.8	-2.7	-3.4	-1.3	-8.1	91	77	80	83	0.3	1.2	1.0	0.8	8	10	10	E 2	E 6	E 3
25	96.3	97.0	99.9	97.7	-2.5	0.7	0.2	-0.4	1.6	-2.8	84	88	94	89	0.8	0.7	0.4	0.6	10	10 ⊙	10	SE 1	S 1	SW 3
26	105.1	107.4	106.9	106.5	0.5	1.1	-0.5	0.2	1.6	-0.5	100	94	92	95	0.0	0.4	0.5	0.3	10	10	0	SW 1	SW 3	SW 1
27	100.9	101.0	105.2	102.4	0.8	2.4	1.8	1.7	3.1	-1.3	92	100	93	95	0.5	0.0	0.6	0.4	10	10	1	S 5	SW 5	SW 3
28	105.5	107.6	113.6	108.9	-0.9	1.5	0.2	0.2	2.1	-1.6	92	92	100	95	0.5	0.5	0.0	0.3	6	10	4	S 2	SW 3	W 2
29	118.5	118.1	115.8	117.5	0.2	1.9	0.8	0.9	2.3	-0.3	88	89	88	88	0.7	0.8	0.8	0.8	9	9	2	W 3	W 1	C 0
30	112.8	109.9	108.4	110.4	-1.1	3.4	0.5	0.8	4.0	-1.3	94	80	90	88	0.3	1.6	0.6	0.8	3	9	0	C 0	S 2	C 0
31	109.2	111.2	111.5	110.6	-0.5	2.3	2.1	1.5	2.6	-0.5	96	91	98	95	0.3	0.6	0.1	0.3	7	10	10	C 0	C 0	SE 4
M	107.2	107.1	107.5	107.3	-2.0	0.0	-1.2	-1.1	1.0	-3.4	90	86	90	89	0.5	0.8	0.6	0.6	8.0	8.8	6.3	3.3	3.5	3.0

Luty – Février

1	107.9	107.5	107.4	107.6	0.6	1.5	1.6	1.3	2.6	0.6	98	96	91	95	0.1	0.3	0.7	0.4	10 ✳	10	10 ●	SE 5	S 8	S 6
2	106.4	110.4	112.8	109.9	4.3	6.9	6.8	5.2	7.1	1.6	100	94	98	97	0.0	0.5	0.1	0.2	10	10	10	SW 4	SW 5	SW 2
3	112.7	113.2	114.6	113.5	2.9	3.4	-0.5	1.3	5.3	-0.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10 ●	10 ≡	C 0	SW 2	SW 3
4	115.7	112.8	109.2	112.6	-1.6	0.9	1.5	0.6	1.8	-2.8	98	94	98	97	0.1	0.4	0.1	0.2	10 ≡	10 ⊙	10	SE 2	S 3	S 1
5	109.9	109.4	107.3	108.9	2.6	3.9	2.6	2.9	6.6	1.5	100	97	95	97	0.0	0.3	0.4	0.2	10 ≡	10 ⊙ ≡	0	SW 3	S 2	S 2
6	105.1	103.1	100.1	102.8	0.9	8.1	2.0	3.2	9.0	0.7	96	79	94	90	0.2	2.3	0.4	1.0	4	8 ⊙	0	S 2	S 3	SW 3
7	100.2	101.6	101.6	101.1	4.0	6.2	5.1	5.1	6.8	1.4	100	91	83	91	0.0	0.9	1.5	0.8	10 ●	10	7	SW 5	SW 6	SW 6
8	101.6	97.7	92.0	97.1	1.6	6.7	5.4	4.8	7.3	1.5	93	75	92	87	0.6	2.4	0.7	1.2	10	10	10 ●	SW 4	S 1	SW 3
9	87.8	87.8	89.1	88.2	5.7	7.8	6.3	6.5	8.8	4.9	100	90	89	93	0.0	1.1	1.0	0.7	10 ●	10	4	SW 5	S 5	SW 6
10	90.9	93.4	94.9	93.1	2.2	4.5	1.2	2.3	6.9	0.9	87	77	90	85	1.0	1.9	0.7	1.2	7	9	4	W 7	W 5	W 1
11	94.3	95.5	98.8	96.2	2.3	5.3	3.3	3.6	5.5	0.9	100	97	90	96	0.0	0.3	0.7	0.3	10 ≡	10 ●	10	SE 1	WSW 4	W 3
12	100.4	99.8	95.3	98.5	1.0	5.5	4.2	3.7	5.7	0.1	92	66	74	77	0.5	3.0	2.1	1.9	7	8 ⊙	10	SW 1	SE 5	SE 4
13	90.6	88.6	82.5	87.2	2.4	6.9	4.9	4.8	8.2	2.4	95	75	79	83	0.4	2.4	1.8	1.5	10 ●	9 ⊙	6	S 4	SSW 4	SE 7
14	76.4	77.0	76.8	76.7	5.6	9.6	6.8	7.2	10.5	4.0	80	67	82	76	1.8	4.0	1.8	2.5	10	8 ⊙	10	S 6	S 5	S 5
15	78.1	78.7	73.9	76.9	2.1	7.3	6.0	5.4	8.6	2.1	85	63	89	79	1.0	3.7	1.1	1.9	6	9 ⊙	9 ●	S 3	S 3	S 6
16	75.6	82.7	86.8	81.7	5.3	5.5	2.4	3.9	6.4	2.4	100	78	93	90	0.0	1.9	0.6	0.8	10 ●	9	7	SW 5	SW 5	SW 5
17	92.0	94.0	93.9	93.3	-0.3	4.9	3.4	2.8	5.7	-0.5	98	73	88	86	0.2	2.4	0.9	1.2	6	9	10 ●	SW 3	SW 6	SE 5
18	96.2	94.2	87.5	92.6	-0.2	6.3	5.5	4.3	6.5	-0.3	94	66	92	84	0.4	3.2	0.7	1.4	4	10	10 ●	C 0	SE 5	E 5
19	80.0	87.2	97.0	88.1	5.7	2.1	1.6	2.8	6.3	0.8	91	95	85	90	0.9	0.4	1.1	0.8	9	10 ●	2	SE 3	SE 5	SW 4
20	100.8	100.0	98.8	99.9	0.1	5.9	4.4	3.7	7.8	-1.3	96	61	68	75	0.3	3.6	2.7	2.2	9	8 ⊙	9	S 1	S 3	S 5
21	96.1	96.2	98.1	96.8	3.2	8.5	5.6	5.7	9.9	-1.3	78	61	80	73	1.7	4.3	1.8	2.6	10	8 ⊙	10	SE 4	SE 5	SW 1
22	100.5	101.3	101.1	101.0	1.1	1.9	0.7	1.1	5.8	0.7	98	78	86	87	0.1	1.5	0.9	0.8	10 △	10	9	SW 3	SW 3	SW 2
23	101.0	100.5	100.3	100.6	-0.4	3.1	-0.6	0.4	3.3	-1.0	96	71	94	87	0.2	2.2	0.3	0.9	10	10 ⊙	0	C 0	W 4	SW 1
24	97.1	93.3	90.6	93.7	-1.4	-1.3	0.2	-0.6	0.8	-2.5	97	93	98	96	0.2	0.4	0.1	0.2	5	10	10 ✳	C 0	E 6	E 4
25	93.3	94.8	94.2	94.1	-0.2	1.0	0.5	0.4	1.6	-0.3	96	90	98	95	0.2	0.7	0.1	0.3	10	10	10 ✳	C 0	N 2	NE 2
26	98.0	102.1	107.2	102.4	0.0	-0.2	-0.8	-0.4	0.8	-0.8	100	92	81	91	0.0	0.5	1.1	0.5	10	10 ●	10	N 2	N 3	N 3
27	110.6	112.7	114.1	112.5	-2.5	-2.0	-3.3	-2.8	-0.5	-3.3	87	81	76	81	0.7	1.0	1.1	0.9	10	10	10	N 3	NNE 2	E 2
28	116.0	117.5	119.8	117.8	-3.6	-0.4	-2.1	-2.0	0.5	-3.7	71	64	64	66	1.4	2.1	1.8	1.8	6 ⊙	9 ⊙	0	NNW 1	NNE 3	N 3
29																								
30																								
31																								
M	97.7	98.3	98.1	98.0	1.5	4.3	2.6	2.8	5.6	0.3	94	81	87	87	0.4	1.7	0.9	1.0	8.7	9.4	7.4	2.8	4.0	3.6

Warszawa – Bielany

$H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 17{,}7\ m$

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY ŚNIEŻNEJ h	USŁONECZNIENIE	POGODA
1	4	2.1	10	–	$*^{1}na$ $*\overset{4}{+}a-p$ $*^{1-0}a-p$
2	7	.	9	–	
3	6	2.4	9	–	$*^{0}740-a$; $\equiv^{2-0}p-n$
4	6	.	7	–	$=n-p$ $\equiv^{0-2}a$; $\vee p-n$; $\odot\ a-p$
5	7	4.7	7	–	$\bullet^{1}n\ldots n$; $=n-p$; $\vee n-a$
6	6	4.5	pż.	–	$\bullet^{1}n$
7	8	0.1	pż.	–	$\bullet n$ $\overset{\bullet}{\nabla}a$
8	7	0.5	.	–	$\bullet^{0}n-a$ $\bullet a\ldots n$
9	8	.	.	–	
10	8	0.4	.	–	$\bullet^{1}12^{30}$ $\overset{*}{\nabla}p$
11	8	0.0	.	–	$*^{0}n\ldots a$
12	6	1.5	.	–	$*^{0}n\ldots n$
13	6	0.7	1	–	$*^{0}640\ldots n$; $=a-p$
14	7	0.0	2	–	$*^{0}n-a$
15	7	0.0	2	–	$*^{0}800$; $\llcorner\!\lrcorner\ p-n$; $\odot\ a-p$
16	7	0.0	2	–	$*^{0}a\ldots p$; $\llcorner\!\lrcorner^{2}n-a$ $=\vee^{1}p-n$; $\odot\ a-p$
17	6	0.0	2	–	$*^{0}a$ $\bullet^{1}p$ $\bullet p-n$; $=n-n$; $\vee^{1}n-a$
18	6	0.0	2	–	$\bullet n$; $=n-p$
19	6	(0.0)	2	–	$\bullet n-a$
20	6	.	2	–	$\overset{\bullet}{\nabla}p$; $=n-a$
21	7	.	2	–	$\llcorner\!\lrcorner^{0}n-a$; $\odot\ a-p$
22	7	.	1	–	$=p-n$; $\vee n-a$; $\odot\ a-p$
23	6	.	1	–	$\llcorner\!\lrcorner^{0}n-a$; $\odot\ a-p$
24	7	.	1	–	$=\vee^{2}n-a$
25	6	.	1	–	$=\llcorner\!\lrcorner^{2}n-a$; $\odot\ a-p$
26	6	0.2	pż.	–	$=n-a$; $\vee^{1}p-n$
27	6	1.0	pż.	–	$\bullet a$ $\bullet^{0}p$; $=a$, p $\equiv^{1}a$; $\vee^{1}n-a$
28	6	.	pż.	–	$=n-a$; $\llcorner\!\lrcorner^{2-1}n-a-p$
29	8	.	.	–	
30	6	.	.	–	$=n-n$; $\vee^{1}n-a$
31	6	7.5	.	–	$=n-n$; $\llcorner\!\lrcorner^{1}n-a$
Σ	–	25.6	–	–	UWAGI: 1) Wartości ciśnienia atmosferycznego w miesiącach I – X są za niskie przeciętnie o około 0.4 mb. 2) Kierunki i prędkości wiatru w miesiącach I – IX – wg anemometru indukcyjnego.

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1	6	4.3	0	–	$\bullet n$ $*^{1}n-a$ $\bullet^{0}a\ldots p$, $20^{37}-n$
2	6	0.2	.	–	
3	4	3.3	.	–	$\overset{\bullet}{\nabla}n$ $\bullet^{1}a\ldots p$; $\equiv^{2}p-n$
4	4	1.2	.	–	$\bullet a\ldots p$; $\equiv^{2-1}n-a$ $=a-p$; $\llcorner\!\lrcorner^{2}n-a$; $\odot\ a-p$
5	3	.	.	–	$\equiv^{2-0}n-a-p$; $\llcorner\!\lrcorner^{0}p-n$; $\odot\ a-p$
6	4	2.7	.	–	$=\llcorner\!\lrcorner^{2}n-a$ $\llcorner\!\lrcorner^{0}p-n$; $\odot\ a-p$
7	6	0.7	.	–	$\bullet^{0}n-a$
8	6	7.5	.	–	$\bullet^{0}p-n$; $=n-a$
9	6	0.3	.	–	$\bullet^{0}n-a$
10	7	0.4	.	–	
11	6	0.6	.	–	$\bullet n$ $\bullet^{0}a-p$; $\equiv^{0}n-a$
12	6	0.6	.	–	$\odot\ a-p$; $\Box\ p-n$
13	7	1.1	.	–	$\bullet^{0}n-a$; $=n-a-p$
14	7	.	.	–	$\Box\ p-n$; $\odot\ a-p$
15	7	1.8	.	–	$\bullet^{0}p-n$; $\llcorner\!\lrcorner^{0}n-a$ $\infty\ a-p$; $\odot\ a-p$
16	6	0.4	.	–	$\overset{\bullet}{\nabla}{}^{1}n-a$ $\overset{\bullet}{\nabla}p$
17	7	0.4	.	–	$\overset{\bullet}{\nabla}n$ $\bullet^{1}20^{30}$ ▲ 20^{41-42} $\bullet^{1}20^{43}-n$; $=n-a-p$; $\llcorner\!\lrcorner^{0}n-a$
18	7	10.2	.	–	$\bullet^{0-1}p\ldots n$; $=\llcorner\!\lrcorner^{1}n-a$
19	7	2.6	.	–	$\bullet n$ $\overset{*}{\nabla}9^{30}\ldots p$
20	6	.	.	–	$=\llcorner\!\lrcorner^{1}n-a$; $\odot\ a-p$
21	7	2.0	.	–	$\odot\ a-p$
22	8	0.5	.	–	$\bullet n$ $\triangle\ n-a$
23	6	0.0	.	–	$*^{0}n$, $9^{20}-a$; $=n-a$; $\odot\ a-p$
24	6	0.0	.	–	$*^{1}p-n$; $=n-a-p$; $\llcorner\!\lrcorner^{2}n-a$
25	6	1.7	1	–	$*^{0}p-n$
26	6	.	2	–	$*n$
27	7	.	2	–	$=n-a$
28	7	.	.	–	$\odot\ a-p$
29					
30					
31					
Σ	–	42.5	–	–	UWAGI:

Warszawa – Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ Marzec – Mars 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	121.1	120.6	120.1	120.6	-4.2	-0.8	-2.1	-2.3	-0.5	-4.6	79	67	64	70	0.9	1.9	1.8	1.5	10	10	10	NNW 2	NW 5	N 4
2	118.2	116.7	113.9	116.3	-3.5	-0.2	-1.4	-1.6	0.8	-3.6	69	55	70	65	1.4	2.7	1.7	1.9	9	7 ⊙	9	E	NW 4	N 4
3	112.2	111.2	109.0	110.8	-6.5	-5.4	-6.4	-6.2	-0.9	-6.6	81	65	73	73	0.7	1.4	1.0	1.0	10	10 ✳	0	NE	0	C 0
4	105.0	101.5	96.1	100.9	-6.5	0.3	0.9	-1.1	1.9	-7.9	81	57	83	74	0.7	2.7	1.1	1.5	6 ⊙	8 ⊙	10 ✳	C 0	S 4	SW 3
5	97.9	99.9	100.8	99.5	-0.4	2.5	-0.3	0.4	4.5	-1.3	92	80	76	83	0.5	1.4	1.5	1.1	9	7 ⊙	1	C 0	W 3	SW 3
6	101.1	100.5	100.5	100.7	-2.6	4.0	-0.5	0.1	5.0	-3.5	89	45	86	73	0.6	4.4	0.9	2.0	1 ⊙	2 ⊙	0	SW 3	SW 4	C 0
7	101.3	103.5	104.7	103.2	-2.0	-0.8	-2.9	-2.2	-0.2	-2.9	87	59	71	72	0.7	2.3	1.4	1.5	10	9 ⊙	0	E 5	E 4	E 2
8	106.1	107.6	110.3	108.0	-2.8	-1.4	-3.7	-2.9	0.2	-4.6	67	56	76	66	1.7	2.4	1.1	1.7	10	10	0	E 5	E 4	E 3
9	114.2	115.3	116.8	115.4	-7.0	1.7	-1.7	-2.2	2.9	-7.2	88	44	71	68	0.4	3.9	1.6	2.0	4 ⊙	6 ⊙	0	C 0	NE 3	N 2
10	120.2	121.5	121.6	121.1	-6.2	2.0	-1.2	-1.6	3.8	-6.3	97	50	72	73	0.1	3.6	1.6	1.8	0 ⊙	0 ⊙	0	C 0	N 3	C 0
11	121.6	121.2	118.1	120.3	-3.8	5.8	1.1	1.0	8.8	-5.3	92	49	74	72	0.4	4.6	1.7	2.2	0 ⊙	0 ⊙	3	C 0	C 0	S 1
12	114.0	110.1	105.7	109.9	-1.0	11.7	6.3	5.8	11.9	-1.3	75	31	59	55	1.5	9.5	3.9	5.0	9	7	9	S 1	S 4	W 3
13	105.0	105.0	102.6	104.2	0.9	12.8	6.1	6.5	13.4	0.8	88	33	72	64	0.7	10.0	2.7	4.5	8	7 ⊙	8	W 1	SW 4	SW 5
14	97.1	94.1	92.0	94.4	4.9	14.4	9.5	9.6	14.6	2.7	67	52	70	63	2.9	7.9	3.6	4.8	3 ⊙	10 ⊙	10	SW 5	SW 8	W 7
15	93.9	95.1	85.7	91.6	7.0	8.5	8.3	8.0	9.9	6.2	73	57	94	75	2.7	4.7	0.7	2.7	9	10	10 ●	W 7	W 8	W 12
16	88.4	93.1	101.4	94.3	0.7	-2.6	-4.6	-2.8	8.6	-4.8	90	67	72	76	0.6	1.7	1.2	1.2	9	9	10	W 3	NW 8	W 5
17	104.5	102.6	93.5	100.2	-7.4	-2.8	-2.6	-3.8	-2.0	-7.6	76	47	98	74	0.8	2.6	0.1	1.2	5 ⊙	8	10 ✳△	NE 2	SE 1	SE 5
18	84.6	80.6	83.9	83.0	4.5	10.8	6.8	7.2	12.5	-2.6	100	75	87	87	0.0	3.3	1.3	1.5	10 ●	8 ⊙	10 ●	SW 2	SW 3	SW 6
19	93.0	96.2	96.8	95.3	1.1	1.9	1.6	1.6	7.2	0.9	92	89	98	93	0.5	0.8	0.2	0.5	10	10	10 ●	W 1	SW 1	E 1
20	99.8	100.0	93.6	97.8	0.9	1.9	4.4	2.9	4.6	0.9	90	89	95	91	0.6	0.8	0.5	0.6	10	10	10	E 4	E 5	SE 5
21	93.1	97.4	99.2	96.6	8.2	11.8	6.9	8.4	13.7	4.4	86	50	80	72	1.5	6.9	2.0	3.5	9	7 ⊙	1	SW 5	W 7	W 2
22	100.5	102.1	104.9	102.5	3.7	10.1	5.2	6.0	11.1	2.3	85	53	69	69	1.2	5.9	2.7	3.3	0 ⊙	8 ⊙	0	SW 4	SW 6	SW 3
23	106.5	107.2	109.5	107.7	1.2	10.1	4.0	4.8	11.2	-0.6	92	47	83	74	0.5	6.6	1.3	2.8	0 ⊙	8 ⊙	1	SW 3	E 3	E 6
24	116.3	117.9	118.4	117.5	-2.9	2.5	0.4	0.1	4.5	-2.9	71	50	55	59	1.4	3.7	2.8	2.6	3	7 ⊙	0	E 8	E 9	E 7
25	117.1	116.8	116.0	116.6	-1.6	2.8	2.7	1.6	4.3	-1.6	63	44	52	53	2.0	4.2	3.6	3.3	8 ⊙	10 ⊙	10	E 8	E 14	SE 12
26	113.6	113.5	113.2	113.4	1.7	8.3	5.1	5.0	9.6	1.7	53	41	54	49	3.2	6.6	4.1	4.6	4 ⊙	8 ⊙	0	SE 7	SE 10	SE 6
27	112.9	112.7	110.9	112.2	2.0	12.6	9.7	8.5	14.5	1.4	71	40	52	54	2.1	8.7	5.7	5.5	0 ⊙	8 ⊙	0	SE 4	S 5	S 5
28	108.8	106.4	104.4	106.5	3.0	15.4	8.5	8.8	16.2	2.4	67	22	70	53	2.5	13.6	3.3	6.5	1 ⊙	9 ⊙	10 ●	SE 5	S 4	SW 3
29	102.5	102.1	104.0	102.9	5.2	7.2	5.6	5.9	9.8	5.1	94	81	91	89	0.5	2.0	0.9	1.1	10 ●	10	0	S 4	SE 4	C 0
30	105.6	106.7	107.2	106.5	4.0	14.1	8.5	8.8	14.8	1.6	85	44	69	66	1.2	9.0	3.5	4.6	7 ⊙	9 ⊙	0	NE 1	E 4	N 2
31	109.3	110.0	111.1	110.1	4.3	15.1	9.2	9.4	16.4	2.4	76	36	52	55	2.0	11.0	5.5	6.2	0 ⊙	0 ⊙	0	E 1	E 4	E 2
M	106.0	106.1	105.4	105.8	-0.2	5.6	2.7	2.7	7.5	-1.4	81	54	74	70	1.2	4.9	2.1	2.7	5.9	7.5	4.6	3.1	4.7	3.8

Kwiecień – Avril

1	111.7	111.4	110.2	111.1	4.0	16.0	9.1	9.6	16.5	1.3	77	25	67	56	1.9	13.7	3.8	6.5	0 ⊙	0 ⊙	8	NE 1	E 5	E 1
2	109.1	108.4	109.3	108.9	5.1	17.1	10.3	10.7	19.0	3.3	80	37	65	61	1.8	12.2	4.4	6.1	1 ⊙	0 ⊙	0	E 2	SE 6	E 2
3	111.6	112.8	114.4	112.9	5.9	18.9	11.5	11.9	20.0	3.4	80	31	60	57	1.9	15.0	5.5	7.5	3 ⊙	3 ⊙	0	NE 1	E 1	E 1
4	116.4	116.4	115.6	116.1	6.0	17.6	11.2	11.5	19.0	4.0	80	33	52	55	1.9	13.5	6.3	7.2	0 ⊙	4 ⊙	6	C 0	W 2	C 0
5	115.1	113.2	108.1	112.1	7.1	18.0	10.9	11.7	19.4	4.1	81	30	49	53	1.9	14.4	6.7	7.7	0 ⊙	2 ⊙	0	C 0	SW 3	C 0
6	102.8	98.5	94.4	98.6	9.8	19.0	12.3	13.4	20.0	5.3	58	22	54	45	5.0	17.2	6.5	9.6	0 ⊙	1 ⊙	0	S 1	SW 4	S 2
7	94.8	97.1	100.8	97.6	6.9	8.2	6.1	6.8	12.7	5.2	99	78	63	80	0.1	2.4	3.5	2.0	10 ●	10	10	W 3	NE 4	N 5
8	105.3	104.1	101.4	103.6	-0.7	5.8	4.0	3.3	6.6	-1.3	90	45	58	64	0.6	5.0	3.4	3.0	5	5 ⊙	9	NNW 4	W 4	WSW 1
9	99.5	99.1	99.2	99.3	2.1	2.6	0.0	1.2	6.1	0.0	78	86	49	71	1.5	1.1	3.1	1.9	9	10 ✳△	1	NW 2	NW 2	NW 1
10	97.9	93.3	86.5	92.6	-2.0	9.0	8.9	6.2	12.0	-5.3	66	47	67	60	1.8	6.1	3.8	3.9	7 ⊙	4 ⊙	9	C 0	S 3	S 3
11	80.9	81.4	86.3	82.9	6.5	8.7	4.0	5.8	9.0	4.0	78	61	74	71	2.2	4.3	2.1	2.9	4 ⊙	10	10	SW 3	W 3	NW 3
12	94.1	97.0	98.9	96.7	1.2	3.5	1.2	1.8	5.5	0.7	79	55	68	67	1.4	3.5	2.2	2.4	10	10	6	NW 3	WSW 2	C 0
13	100.7	101.0	102.2	101.3	0.3	7.5	0.4	2.2	8.8	-2.1	90	32	100	74	0.6	7.1	0.0	2.6	4 ⊙	2 ⊙	10 ✳	W 1	S 1	C 0
14	105.4	106.0	105.7	105.7	-1.1	4.9	1.8	1.8	6.1	-1.4	97	56	57	70	0.2	3.8	3.0	2.3	10	7 ⊙	5	W 2	WSW 3	C 0
15	106.5	107.1	108.7	107.4	0.0	5.4	2.4	2.6	6.1	-1.1	82	38	66	62	1.1	5.6	2.5	3.1	4 ⊙	5 ⊙	9	NW 3	NW 5	W 3
16	110.8	109.0	106.2	108.7	-0.6	7.1	7.5	5.4	9.2	-2.7	85	27	75	62	0.8	7.4	2.7	3.6	1 ⊙	7	10	C 0	SW 2	S 1
17	105.7	106.1	106.3	106.0	6.9	8.9	6.9	7.4	12.1	6.3	97	67	84	83	0.3	3.8	1.6	1.9	10 ●	10	10	W 2	W 2	NW 3
18	104.8	104.3	102.7	103.9	3.2	4.6	2.9	3.4	7.3	2.5	100	79	91	90	0.0	1.8	0.6	0.8	10 ●	10	10	E 4	NW 1	NW 2
19	101.9	101.5	102.9	102.1	1.8	4.7	5.1	4.2	5.8	1.5	98	70	78	82	0.2	2.5	2.0	1.6	10	10	10	W 1	SW 1	SE 3
20	104.5	107.5	110.8	107.6	4.2	6.4	6.3	5.8	8.1	2.9	93	97	97	96	0.5	0.3	0.2	0.3	10	10	10	E 1	NE 1	W 1
21	112.4	114.2	116.0	114.2	3.3	10.6	6.3	6.6	11.2	1.5	100	62	84	82	0.0	4.9	1.5	2.1	10	9 ⊙	2	SW 1	SW 2	SW 3
22	117.7	116.4	115.9	116.7	6.1	12.4	9.1	9.2	16.2	5.1	89	77	92	86	1.0	3.4	1.0	1.8	10	9 ●	1	NE 3	N 2	W 2
23	116.0	115.2	115.2	115.5	8.8	15.9	12.2	12.3	17.2	6.9	86	49	80	72	1.5	9.2	2.9	4.5	6 ⊙	5 ⊙	9	NE 3	NE 5	NE 3
24	113.7	112.4	110.5	112.2	8.9	18.0	14.3	13.9	19.4	8.4	92	40	51	61	0.9	12.4	7.9	7.1	10	8 ⊙	1	NE 3	NE 4	NE 3
25	108.7	108.0	107.3	108.0	8.9	19.2	15.5	14.8	21.3	7.9	88	50	63	67	1.4	11.1	6.5	6.3	9	8 ⊙	1	NE 4	N 4	N 4
26	107.2	106.5	106.0	106.6	9.1	19.5	16.9	15.6	22.3	8.4	88	55	62	68	1.4	10.3	7.3	6.3	9 ⊙	9 ⊙	0	NNW 3	N 3	NW 3
27	104.9	102.2	102.5	103.2	13.3	24.7	18.3	18.7	25.5	10.7	77	31	49	52	3.5	21.4	10.8	11.9	2 ⊙	3 ⊙	0	NNW 1	E 4	SE 3
28	101.0	99.-	97.7	99.3	15.4	24.6	16.2	18.1	25.6	13.0	61	32	79	57	6.9	20.9	3.8	10.5	7 ⊙	8 ⊙	0	SE 3	S 5	C 0
29	97.9	98.-	98.9	98.5	15.8	25.2	15.1	17.8	25.5	13.7	68	38	75	60	5.7	19.8	4.3	9.9	2 ⊙	4 ⊙	3	SW 3	S 3	S 3
30	98.7	96.0	94.9	96.5	14.6	25.9	13.8	17.0	26.2	10.8	73	34	97	68	4.5	22.1	0.6	9.1	3 ⊙	4 ⊙	10 ●	SE 2	S 8	W 3
31																								
M	105.3	104.8	104.5	104.9	5.7	13.0	8.7	9.0	14.7	3.9	84	49	70	68	1.8	9.2	3.7	4.9	5.9	6.2	5.3	2.0	3.2	2.0

Warszawa – Bielany

$H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 17{,}7\ m$

Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.0	-	-	⚹ 8⁰⁰ 9²⁰, ⌴⁰ n – a
2	8	.	.	-	⊙ a – p
3	7	(0.0)	.	-	⚹ a – p; ⌴⁰ p – n
4	7	1.2	.	-	✶⁰ p – n; = ⌴¹ n – a; ⊙ a – p
5	7	.	2	-	= n – a; ⊙ a – p
6	7	.	.	-	= ⌴² n – a ⌴² p – n; ⊙ a – p
7	7	.	.	-	⌴¹ n – a; ⊙ a – p
8	8	.	.	-	
9	7	.	.	-	= ⌴²⁻⁰ n – a; ⊙ a – p
10	6	.	.	-	= n – n; ⌴² n – a ⌴⁰ p – n; ⊙ a – p
11	6	.	.	-	≡ n – a = a – n; ⌴² n – a ⌴⁰ p – n; ⊙ a – p
12	7	.	.	-	= ⌴¹ n – a
13	7	.	.	-	= n – a; ⌒ p – n; ⊙ a – p
14	6	.	.	-	= n – a; ⊙ a – p
15	8	11.1	.	-	• p – n; ⫽ n ⫸ a – p ⫽ p – n
16	7	0.0	.	-	• n ▲⁰ 10⁰⁰ ⚉⁰ a ⚹ p
17	7	5.8	1	-	✶ n △ ✶ p – n
18	6	2.3	.	-	•⁰ n – a ⚉¹ 20⁴³; ⊙ a – p
19	6	0.0	.	-	✶ 8³⁰ •⁰ 20³⁰ – n
20	6	.	.	-	= n – a – p
21	8	.	.	-	⊙ a – p
22	8	.	.	-	= n – a; ⊙ a – p
23	8	.	.	-	= ⌴¹ n – a; ⊙ a – p
24	8	.	.	-	⫸ n – a – p; ⊙ a – p
25	7	.	.	-	⫸ a – n ⫽ p
26	7	.	.	-	⫸ a – p; ⊙ a – p
27	6	.	.	-	∞¹ n – a; ⊙ a – p
28	6	2.2	.	-	•⁰ 20³⁵ – n; = n – a ⌴ n; ⊙ a – p
29	6	0.7	.	-	•¹ n – a
30	7	.	.	-	= n – a; ⊙ a – p
31	8	.	.	-	= n – a; ⌴¹ n – a; ⊙ a – p
Σ	–	23.3	–	-	UWAGI.

Kwiecień – Avril

1	8	.	.	-	= ⌴¹ n – a; ⊙ a – p
2	8	.	.	-	= ⌴⁰ n – a, ⊙ a – p
3	8	.	.	-	= n – a, ⊙ a – p
4	9	.	.	-	= n – a, ⊙ a – p
5	8	.	.	-	= ⌓⁰ n – a; ⊙¹ a – p
6	8	0.2	.	-	= ⌓⁰ n – a, p – n, ⊙ a – p
7	7	0.0	.	-	•⁰ n – a
8	9	.	.	-	⊙ a – p
9	8	0.0	.	-	⚹⁰ n ✶⁰△ p
10	8	.	.	-	= ⌴⁰ n – a; ⊙ a – p
11	7	.	.	-	= n – a; ⊙ a
12	8	.	.	-	
13	9	2.4	.	-	✶ p... n ⚹ p... n; ∞ n – a; ⊙ a – p
14	8	.	0	-	= n – a, p – n; ⊙ a – p
15	8	.	.	-	⊙ a – p
16	7	0.3	.	-	⌴⁰ n – a; ⊙ a
17	7	0.0	.	-	• = n – a
18	7	1.3	.	-	•⁰ n – a ⚉⁰ a, p
19	7	0.0	.	-	
20	6	1.6	.	-	•⁰ a .. p
21	8	.	.	-	= n – a; ⌓⁰ p – n, ⊙ a – p
22	7	2.7	.	-	⚉ p; ⌓⁰ n – a
23	8	.	.	-	= ⌓¹ n – a; ⊙ a – p
24	7	.	.	-	⌓⁰ n – a; ∞ a – p; ⊙ a – p
25	7	.	.	-	∞ n – a – p, ⊙ a – p
26	7	.	.	-	∞¹ n – a – p, ⌓¹ n – a ⌓⁰ p – n; ⊙ a – p
27	7	0.0	.	-	⚉(K) SW p; = ⌓⁰ n – a ∞ n – a; ⊙ a – p
28	8	0.0	.	-	⚉ 13¹⁵ p; (K) 12⁴⁵ S – N; ∞ a – p; ⊙ a – p
29	7	3.0	.	-	⚉ K p SW-NW; = ⌓⁰ n – a ∞ a – p; ⊙ a – p
30	7	2.7	.	-	⚉¹ a – p – n; (K) p W – E
31					
Σ	–	11.2	–	-	UWAGI.

Warszawa – Bielany

$\varphi = 52°17'$ $\lambda = 20°58'$

Maj – Mai 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI d				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	103.8	105.1	106.2	105.0	6.4	11.8	6.5	7.8	16.7	3.9	70	38	59	56	2.8	8.5	4.0	5.1	1 ⊙	4 ⊙	1	W 3	NW 6	N 3
2	106.5	104.1	102.1	104.2	5.3	12.0	7.8	8.2	12.4	1.0	57	31	63	50	3.8	9.7	4.0	5.8	1 ⊙	7 ⊙	1	NW 4	NW 3	C 0
3	100.(	99.0	96.9	98.9	7.4	12.4	8.9	9.4	14.2	5.2	62	43	73	59	3.9	8.2	3.0	5.0	9 ⊙	9	0	I	NE 1	S 2
4	94.5	95.1	97.8	95.8	9.3	11.4	4.4	7.4	12.4	4.4	75	51	65	64	2.9	6.7	3.0	4.2	1 ⊙	7 ⊙	0	SW 5	WSW 5	SW 3
5	98.9	98.6	98.2	98.6	4.4	9.7	3.5	5.3	11.4	1.2	65	48	68	60	3.0	6.2	2.5	3.9	1 ⊙	7 ⊙	1	SW 7	SW 6	SW 1
6	97.8	96.2	95.7	96.6	3.8	6.0	4.3	4.6	8.6	0.7	69	67	77	71	2.5	3.1	1.9	2.5	10	10 ●	10	E 2	E 6	E 2
7	95.1	95.6	94.7	95.1	3.5	5.4	4.0	4.2	5.8	2.6	88	74	97	86	0.9	2.4	0.2	1.2	10	10	10 ●	SW 2	C 0	C 0
8	92.6	92.4	95.4	93.5	3.6	6.0	4.1	4.4	6.4	3.4	95	85	100	93	0.4	1.5	0.0	0.6	10 ●	10	10 ●	NW 3	NW 3	W 1
9	97.5	98.3	96.3	97.4	4.0	5.5	6.1	5.4	6.6	3.7	95	98	100	98	0.4	0.1	0.0	0.2	10	10 ●	10 ●	N 3	NW 3	NW 4
10	94.7	94.2	96.9	95.3	6.6	10.5	8.7	8.6	11.4	3.7	100	96	99	98	0.0	0.5	0.4	0.2	10 ▬	10 ●	9	NW 2	W 3	C 0
11	100.4	103.6	104.0	102.7	6.9	9.5	9.6	8.9	12.2	6.9	99	84	87	90	0.1	1.9	1.6	1.2	10 ●	10	0	SW 2	SW 3	SSE 1
12	104.4	104.8	105.1	104.8	11.4	19.5	15.6	15.5	20.8	7.5	78	49	61	63	3.0	11.6	6.9	7.2	5	3 ⊙	1	SE 4	SE 4	C 0
13	105.6	104.9	103.8	104.8	13.1	22.3	16.4	17.0	24.6	9.1	72	40	64	59	4.3	16.2	6.7	9.1	3 ⊙	1 ⊙	1	SE 1	SE 3	C 0
14	103.9	105.4	106.7	105.3	14.7	20.5	15.9	16.8	21.5	10.7	75	51	63	63	4.1	11.8	6.7	7.5	0 ⊙	2 ⊙	1	WSW 1	NW 7	W 2
15	109.7	110.1	109.2	109.7	12.4	18.7	14.9	15.2	20.5	9.1	80	43	52	58	2.9	12.4	8.0	7.8	1 ⊙	2 ⊙	0	NW 2	W 3	C 0
16	109.3	106.8	104.7	106.9	13.9	20.9	15.8	16.6	22.3	8.7	54	29	60	48	7.4	17.6	7.1	10.7	0 ⊙	0 ⊙	0	E 2	E 3	E 2
17	104.6	104.1	103.7	104.1	14.3	21.2	16.4	17.1	23.0	9.3	68	34	70	57	5.3	16.8	5.6	9.2	4 ⊙	9	2	ENE 2	E 3	N 1
18	104.8	104.7	101.9	103.8	12.5	21.2	17.7	17.3	23.7	11.5	86	44	62	64	2.1	14.0	7.7	7.9	6 ⊙	5 ⊙	1	N 2	NE 4	NE 2
19	98.8	97.9	95.9	97.5	14.7	26.2	19.9	20.2	27.4	12.7	85	33	60	59	2.5	22.7	9.3	11.5	9	4 ⊙	6	N 3	SE 7	E 4
20	96.6	96.9	97.9	97.1	15.5	22.3	17.5	18.2	23.7	13.0	78	57	73	69	3.9	11.5	5.3	6.9	1 ⊙	6	4	E 4	E 4	S 2
21	101.5	103.0	103.3	102.6	11.3	12.9	10.8	11.4	18.1	10.8	86	76	75	79	1.8	3.6	3.3	2.9	10	10	10	W 5	W 4	NW 2
22	102.1	102.2	101.6	102.0	9.5	13.1	13.8	12.6	14.1	9.0	75	63	81	73	3.0	5.6	3.0	3.9	10	10	9	NW 4	NW 4	NW 2
23	100.3	99.7	98.8	99.6	12.2	17.8	16.1	15.6	19.9	9.9	78	72	82	77	3.2	5.8	3.1	4.0	2 ⊙	9	9	NW 2	NNW 4	NW 2
24	99.5	102.6	106.3	102.8	15.2	13.6	11.6	13.0	16.9	11.6	89	75	55	73	1.9	3.9	6.0	3.9	10	10	4	NW 2	NE 5	N 2
25	110.4	111.5	112.5	111.6	8.7	12.0	7.6	9.0	12.9	4.4	63	36	54	51	4.1	9.0	4.7	5.9	0 ⊙	10	10	N 4	N 6	N 4
26	113.6	113.6	113.7	113.6	7.5	9.7	7.3	8.0	13.0	4.5	68	59	62	63	3.4	4.9	3.9	4.1	6 ⊙	9	7	NE 4	N 6	N 4
27	112.9	112.6	111.2	112.2	6.2	9.9	8.0	8.0	11.2	3.7	72	44	63	60	2.7	6.8	3.9	4.5	9	10	8	NE 2	N 3	NE 1
28	109.8	108.8	108.0	108.9	8.0	12.3	7.1	8.6	13.7	4.0	74	40	76	63	2.8	8.6	2.5	4.6	5 ⊙	8 ⊙	1	NE 3	N 3	C 0
29	107.6	108.0	107.7	107.8	7.5	12.7	10.4	10.2	13.9	2.4	80	43	66	63	2.1	8.3	4.2	4.9	0 ⊙	10	10	NW 2	NW 4	W 1
30	109.2	109.2	108.7	109.0	8.9	15.6	12.5	12.4	17.9	5.9	80	46	60	62	2.3	9.5	5.8	5.9	4 ⊙	9	5	C 0	WNW 5	C 0
31	108.4	107.1	103.8	106.4	14.3	19.3	14.6	15.7	21.6	5.4	67	35	52	51	5.5	14.5	8.0	9.3	1 ⊙	7	4	C 0	W 1	S 1
M	103.1	103.1	102.9	103.0	9.5	14.3	10.9	11.4	16.1	6.5	77	54	70	68	2.9	8.5	4.3	5.2	5.1	7.4	4.7	2.7	3.9	1.6

Czerwiec – Juin

1	102.8	102.4	101.7	102.3	14.6	22.4	17.2	17.8	24.0	10.4	58	25	54	46	7.0	20.3	9.0	12.1	8 ⊙	7 ⊙	4	SW 1	SW 3	W 1
2	103.9	104.5	106.5	105.0	12.9	20.0	17.4	16.9	23.1	9.5	71	46	72	63	4.3	12.6	5.5	7.5	5 ⊙	8 ⊙	9	W 4	SW 3	S 3
3	109.7	107.6	104.3	107.2	15.4	23.7	20.1	19.8	25.5	10.5	74	44	62	60	4.6	16.5	9.0	10.0	0 ⊙	2 ⊙	3	NW 1	SW 2	C 0
4	101.2	99.1	97.2	99.2	19.5	25.6	16.9	19.7	26.5	16.0	65	48	97	70	7.9	17.2	0.6	8.6	8 ⊙	10 ●	10 ●	SE 1	S 1	E 1
5	92.2	93.2	93.1	92.8	15.4	15.2	13.2	14.2	17.4	13.0	98	83	88	90	0.4	3.0	1.8	1.7	10	10	6	C 0	W 7	SW 1
6	94.1	95.9	99.4	96.5	13.3	14.2	10.1	11.9	17.2	9.9	83	69	82	78	2.7	5.0	2.3	3.3	7 ⊙	9	1	SW 4	SW 8	S 1
7	100.1	98.5	97.8	98.8	14.8	23.3	16.5	17.8	24.5	8.9	62	36	81	60	6.4	18.3	3.7	9.5	0 ⊙	4 ⊙	7	SSE 3	S 4	C 0
8	100.8	101.9	101.3	101.3	14.5	20.5	18.2	17.8	22.1	13.7	87	62	75	75	2.2	9.1	5.3	5.5	9	9 ⊙	4	C 0	NW 3	E 2
9	100.1	98.9	99.1	99.4	18.4	26.2	18.0	20.2	27.9	14.1	71	47	90	69	6.1	18.2	2.0	8.8	2 ⊙	8	9 ●	E 4	SE 6	E 1
10	99.5	100.7	100.6	100.3	19.3	20.0	18.6	19.1	25.0	14.9	78	76	91	82	4.8	5.6	1.9	4.1	8 ⊙	10	2	SE 1	E 1	N 3
11	100.5	98.8	98.5	99.3	19.2	28.6	26.5	25.2	30.8	15.1	84	51	57	64	3.6	19.1	14.8	12.5	9 ⊙	1 ⊙	5	E 3	SE 4	SE 5
12	104.1	109.2	113.7	109.0	21.1	23.6	19.7	21.0	26.9	19.6	82	70	73	75	4.5	8.8	6.1	6.5	9 ⊙	10	5	SW 5	NW 7	NW 4
13	117.8	116.9	116.1	116.9	13.0	18.1	14.0	14.8	20.8	11.6	68	49	72	63	4.8	10.6	4.4	6.6	1 ⊙	1 ⊙	1	NW 4	NW 5	NNW 3
14	115.9	115.1	115.4	115.5	13.7	20.8	16.6	16.9	22.3	9.8	80	36	60	59	3.2	15.8	7.5	8.8	1 ⊙	0 ⊙	1	W 2	NW 5	NW 6
15	116.4	115.5	113.0	115.0	13.9	20.8	17.0	17.2	23.0	8.9	66	38	55	53	5.4	15.3	8.7	9.8	8 ⊙	2 ⊙	1	N 2	NW 6	NW 2
16	112.4	110.6	108.3	110.4	15.5	23.5	20.3	19.9	25.1	10.4	68	39	56	54	5.7	17.7	10.6	11.3	1 ⊙	1	1	N 1	NE 2	NE 2
17	108.3	107.3	105.6	107.1	17.3	22.8	18.5	19.3	24.6	13.2	68	31	51	50	6.3	19.1	10.3	11.9	0 ⊙	0 ⊙	1	N 1	NE 3	C 0
18	105.9	104.1	100.6	103.5	18.6	27.1	21.2	22.0	28.5	10.8	55	27	48	43	9.6	26.2	13.1	16.3	1 ⊙	1	1	C 0	SE 2	NE 2
19	98.9	97.4	96.7	97.7	21.6	30.6	22.7	24.4	31.6	16.0	56	32	58	49	11.3	30.1	11.5	17.6	0 ⊙	2	2	SE 1	W 1	NE 2
20	100.7	102.0	104.0	102.2	15.6	21.0	16.8	17.6	22.7	12.9	68	33	46	49	5.7	16.7	10.3	10.9	3 ⊙	8	2	NE 8	NE 3	NNW 2
21	107.4	105.6	101.1	104.7	12.3	20.9	18.5	17.6	24.1	9.8	66	34	45	48	4.8	16.2	11.8	10.9	2	1 ⊙	0	NE 3	NE 2	ENE 4
22	96.7	93.8	92.9	94.5	17.1	25.3	17.8	19.5	27.5	14.8	73	57	91	74	5.3	13.7	1.8	6.9	8 ⊙	10 ●	10	SE 3	SW 3	W 3
23	95.2	97.5	97.2	96.6	17.9	21.6	19.3	19.5	23.0	15.5	81	56	70	69	3.8	11.3	6.8	7.3	5	9 ⊙	9	W 7	SW 5	E 2
24	98.6	96.0	94.1	96.2	17.5	19.6	13.8	16.2	23.8	13.8	86	82	95	88	2.8	4.1	0.7	2.5	9 ⊙	10 ●	10	W 2	N 2	N 4
25	92.0	97.0	103.3	97.4	12.4	17.8	11.6	13.4	19.3	11.4	99	67	93	86	0.2	6.7	1.0	2.6	10	9	9	SW 3	W 9	WSW 1
26	106.1	107.0	108.6	107.2	10.7	16.3	13.0	13.2	18.6	8.5	89	45	65	66	1.5	10.1	5.3	5.6	10	8 ⊙	1	W 4	W 2	WSW 1
27	110.9	111.1	112.5	111.5	12.1	13.0	12.8	12.7	19.1	7.8	77	84	79	80	3.2	2.5	3.1	2.9	1 ⊙	7 ⊙	2	WSW 1	NW 2	WSW 1
28	112.7	110.2	106.8	109.9	13.7	19.6	20.6	18.6	24.1	7.9	68	51	76	65	5.1	11.1	5.8	7.3	10	10	4	SW 4	SW 5	SW 4
29	108.8	108.6	108.2	108.6	20.6	25.6	22.1	22.6	27.5	16.6	74	61	75	70	6.3	12.8	6.7	8.6	2 ⊙	4 ⊙	1	W 2	NW 3	C 0
30	105.9	105.9	107.3	106.4	22.6	29.3	21.8	23.9	30.0	18.0	74	52	67	64	7.2	19.3	8.7	11.7	0 ⊙	2 ⊙	1	W 1	NW 6	NNE 2
31																								
M	104.0	103.8	103.5	103.8	16.2	21.9	17.7	18.4	24.2	12.4	74	51	71	65	4.9	13.8	6.3	8.3	4.9	5.8	4.1	2.5	3.8	2.1

Warszawa – Bielany $H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 17{,}7\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	-	⊙ a – p
2	9	.	.	-	⊙ a – p
3	9	.	.	-	⊙ a
4	7	.	.	-	= n – a ∞ a – p; ⊙ a – p
5	9	.	.	-	⌒⁰ p – n; ⊙ a – p
6	6	0.0	.	-	•⁰ a – p; = n – a
7	8	8.7	.	-	•² p n; = n – a – p
8	8	0.5	.	-	•¹ n – a •⁰ p
9	6	12.5	.	-	•¹ a – p •² p n
10	6	11.7	.	-	•¹ a – p; ≡² n – a
11	7	0.0	.	-	▽⁰ n – a, ⌒⁰ p – n
12	7	.	.	-	= n – a – p; ⌒² n – a; ⊙ a – p
13	7	.	.	-	= n – a – p; ⌒¹ n – a, p – n; ⊙ a – p
14	7	.	.	-	= n – a; ⌒¹ n – a, p – n; ⊙ a – p
15	8	.	.	-	= ⌒¹ n – a, ⌒¹ p – n; ⊙ a – p
16	9	.	.	-	⌒⁰ n – a ⌒¹ p – n; ⊙ a – p
17	8	.	.	-	= ⌒¹ n – a ⌒¹ p – n; ⊙ a
18	8	.	.	-	∞ ⌒¹ n – a ⌒⁰ p – n; ⊙ a – p
19	8	.	.	-	⊙ a – p
20	8	0.1	.	-	▽¹ p (K) p; ⊙ a
21	7	.	.	-	
22	7	.	.	-	
23	8	.	.	-	⌒⁰ n – a; ⊙ a
24	8	.	.	-	
25	9	.	.	-	⊙ a
26	9	.	.	-	⊙ a
27	8	.	.	-	
28	8	0.5	.	-	▽¹⁻⁰ g20–36 ▲ g30–36 •¹ p; ⊙ a – p
29	9	.	.	-	⌒¹ n – a; ⊙ a
30	8	.	.	-	⊙ a
31	8	.	.	-	= ⌒⁰ n – a, p – n; ⊙ a
Σ	–	36.0	–	-	UWAGI

Czerwiec – Juin

1	7	.	.	-	= n – a ∞ a – p; ⊙ a – p
2	8	.	.	-	∞ ⌒⁰ n – a; ⊙ a – p
3	8	.	.	-	∞ n – a = p – n; ⊙ a – p
4	6	15.5	.	-	•¹ 13²⁰ 14⁵⁰ •⁰⁻⁰ 17²⁵ – n; (K) 14⁵⁰ K 18⁴⁵ (K) 19⁰⁰; = ⌒¹ n – a; ⊙ a
5	7	0.5	.	-	•¹⁻⁰ 9²⁵ – 10¹⁰; = n – a
6	8	0.6	.	-	▽¹ 14⁵⁰ •⁰ 15³⁵
7	8	1.3	.	-	•¹ 16⁴⁰ – 17¹⁰; = ⌒¹ n – a; ⊙ a – p
8	7	.	.	-	= n – a ∞ a – p; ⊙ a – p
9	8	0.5	.	-	•⁰ p; (K) SW – NE p; ⊙ a
10	6	4.8	.	-	•¹ 9⁴⁸; (K); = n – a; ⊙ a
11	8	.	.	-	∞ n – a – p; ⊙ a – p
12	9	.	.	-	∞ n – a; ⊙ a
13	9	.	.	-	⊙ a – p
14	8	.	.	-	⊙ a – p
15	9	.	.	-	⌒⁰ p – n; ⊙ a – p
16	9	.	.	-	⊙ a
17	9	.	.	-	⌒⁰ p – n; ⊙ a – p
18	9	.	.	-	= ⌒⁰ n – a ⌒⁰ ∞ p – n; ⊙ a
19	7	0.8	.	-	∞ n – a ⌒⁰ p – n; ⊙ a
20	8	.	.	-	▽¹ n – a; ⊙ a
21	9	.	.	-	⊙ a – p
22	6	0.4	.	-	▽ 13³⁶ p, 21⁴⁰; ⊙ a
23	8	.	.	-	= n – a, p – n; ⊙ a – p
24	6	6.6	.	-	▽ p; ∞ n – a; ⊙ a
25	8	.	.	-	•¹ (K) na
26	8	.	.	-	⊙ a – p
27	7	0.4	.	-	• 12³⁰ 13³⁰, ⌒⁰ n – a; ⊙ a – p
28	7	.	.	-	
29	8	.	.	-	⊙ a – p
30	8	0.3	.	-	▽⁰ 17¹⁵; ⌒¹ n – a; ⊙ a – p
31					
Σ	–	31.7	–	-	UWAGI.

Warszawa - Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	109.1	108.6	106.9	108.2	18.0	23.8	21.1	21.0	25.8	15.5	81	52	69	67	3.8	14.1	7.7	8.5	1 ⊙	3 ⊙	1	N 3	NW 2	NE 2
2	105.5	102.1	103.1	103.6	20.4	30.4	19.6	22.5	32.1	15.9	74	41	93	69	6.3	25.8	1.5	11.2	6 ⊙	5 ⊙	7	SE 4	SE 6	SW 3
3	107.3	107.2	106.5	107.0	16.0	22.3	18.7	18.9	24.1	13.5	69	45	65	60	5.6	14.9	7.7	9.4	0 ⊙	3 ⊙	1	NW 3	W 5	C 0
4	106.6	104.8	102.2	104.5	18.6	26.4	24.7	23.6	29.0	14.9	64	36	55	52	7.8	21.9	13.9	14.5	8 ⊙	9 ⊙	0	S 3	S 5	SE 5
5	101.0	100.6	102.2	101.3	22.6	31.6	24.1	25.6	33.7	21.3	79	41	68	63	5.9	27.2	9.7	14.3	10	5 ⊙	4	SW 2	W 4	NW 2
6	106.6	106.4	106.6	106.5	17.1	23.8	19.3	19.9	25.2	14.5	69	26	54	50	6.0	21.9	10.3	12.7	1 ⊙	1 ⊙	1	WSW 1	W 7	C 0
7	109.1	108.4	107.8	108.4	17.2	25.1	20.6	20.9	27.3	12.2	65	28	53	49	6.9	22.8	11.4	13.7	2 ⊙	4 ⊙	0	NE 2	N 3	N 2
8	107.6	103.7	101.4	104.2	20.6	31.6	23.9	25.0	33.0	14.2	53	30	68	50	11.4	32.6	9.6	17.9	8 ⊙	8 ⊙	9	E 1	SE 6	S 2
9	99.8	101.7	102.2	101.2	20.3	18.8	17.4	18.5	24.2	17.4	86	92	85	88	3.3	1.7	3.0	2.7	9 ⊙	10 ●	2	NW 2	NW 2	W 1
10	101.3	100.2	98.2	99.9	18.4	24.0	20.2	20.7	25.0	15.1	86	52	75	71	2.9	14.4	6.1	7.8	6 ⊙	10 ⊙	8	SW 1	W 1	NE 2
11	97.1	96.0	95.8	96.3	19.5	25.6	22.8	22.7	27.0	14.7	63	42	64	56	8.5	19.0	10.1	12.5	8 ⊙	5 ⊙	9	ENE 6	NE 5	N 3
12	96.1	96.9	97.8	96.9	18.8	23.7	20.6	20.9	25.6	18.1	97	73	86	85	0.7	8.0	3.3	4.0	10	9	6	ENE 5	ENE 4	E 2
13	101.1	103.1	104.3	102.8	19.2	23.4	21.3	21.3	26.8	18.5	97	76	82	85	0.6	7.0	4.5	4.0	10	9	3	SW 1	WSW 2	NW 2
14	104.3	103.4	101.2	103.0	17.1	26.1	21.4	21.5	27.3	15.8	99	59	77	78	0.2	13.9	5.9	6.7	9 ⊙	1 ⊙	4	N 1	NE 3	NE 3
15	99.4	99.0	99.2	99.2	18.0	22.4	19.1	19.6	24.7	17.1	98	80	88	89	0.4	5.4	2.8	2.9	10	8	8	NNW 2	W 4	C 0
16	97.5	94.6	91.7	94.6	17.9	18.3	16.9	17.5	19.7	16.7	95	98	98	97	1.0	0.4	0.4	0.6	10	10 ●	10	W 2	NW 4	N 6
17	90.5	91.7	93.3	91.8	17.0	17.1	16.1	16.6	18.7	16.0	82	82	99	88	3.6	3.5	0.2	2.4	9	10	10 ●	NE 3	NE 2	W 1
18	95.4	96.2	96.0	95.9	14.5	17.8	16.4	16.3	18.4	14.2	99	82	90	90	0.2	3.6	1.9	1.9	10	10	9	SW 4	N 6	SW 4
19	96.4	96.7	96.3	96.5	16.3	25.0	21.7	21.2	27.3	11.7	84	48	59	64	2.9	16.6	10.6	10.0	1 ⊙	4 ⊙	0	SW 2	S 2	SE 1
20	95.7	94.9	92.3	94.3	18.9	27.3	21.4	22.2	28.6	16.7	82	55	74	70	3.9	16.2	6.7	8.9	1 ⊙	2 ⊙	4	E 4	SE 3	ENE 2
21	91.1	90.2	89.7	90.3	18.5	23.0	19.2	20.0	23.7	15.8	83	74	89	82	3.5	7.3	2.3	4.4	8 ⊙	10	10	SSW 2	SE 2	ENE 4
22	88.5	89.7	90.0	89.4	16.7	19.3	17.6	17.8	22.6	16.0	92	76	86	85	1.6	5.4	2.8	3.3	10	10	10	SE 4	SE 3	SW 2
23	90.3	90.6	90.9	90.6	16.2	22.4	19.7	19.5	25.7	13.1	90	57	77	75	1.7	11.6	5.3	6.2	4 ⊙	9 ⊙	4	NE 1	C 0	SW 3
24	91.5	92.6	96.4	93.5	17.8	19.9	15.8	17.3	21.5	15.5	91	84	86	87	1.8	3.7	2.4	2.6	10	10	10	W 4	W 5	WSW 3
25	97.4	98.0	97.1	97.5	14.6	19.9	16.7	17.0	21.6	11.8	91	61	75	76	1.5	9.1	4.8	5.1	9 ⊙	6 ⊙	10 ●	SW 3	WSW 4	SW 1
26	95.9	96.6	95.2	95.9	14.3	18.8	15.2	15.9	19.5	13.2	93	66	85	81	1.1	7.5	2.6	3.7	10	9	10	SW 4	W 5	S 1
27	93.1	91.8	91.8	92.2	14.3	19.4	14.8	15.8	20.8	13.9	98	78	96	91	0.4	4.8	0.7	2.0	10	10	9	SW 2	S 2	SW 1
28	92.4	94.6	96.5	94.5	14.2	19.7	14.2	15.6	22.3	13.7	95	66	83	81	0.7	7.7	2.7	3.7	10	7 ⊙	3	SW 3	SW 3	S 1
29	97.7	98.8	101.1	99.2	15.3	17.5	15.1	15.8	21.3	10.4	82	73	88	81	3.2	5.5	2.1	3.6	6 ⊙	9 ⊙	2	SW 2	SW 3	C 0
30	102.0	101.9	103.6	102.5	15.4	19.4	15.6	16.5	20.6	13.1	89	70	95	85	1.9	6.8	0.9	3.2	8	10	10	S 2	SW 5	SW 2
31	106.1	107.4	109.4	107.6	15.6	20.8	17.0	17.6	22.3	14.3	91	72	93	85	1.5	6.8	1.4	3.2	9	9	9	W 2	W 6	SW 2
M	99.2	99.0	98.9	99.0	17.4	22.7	19.0	19.5	24.7	15.0	84	62	79	75	3.3	11.8	5.0	6.7	7.2	7.3	5.9	2.6	3.7	2.0

Sierpień – Août

1	110.5	110.2	108.4	109.7	14.5	21.3	17.3	17.6	24.0	11.7	90	65	89	81	1.6	8.9	2.2	4.2	0 ⊙	3 ⊙	1	SW 6	SW 3	SW 2
2	108.6	107.2	107.3	107.7	15.9	21.4	15.3	17.0	23.1	14.6	85	52	67	68	2.7	12.2	5.8	6.9	8 ⊙	5 ⊙	2	W 1	W 5	W 3
3	107.3	106.1	105.7	106.4	13.2	20.6	16.7	16.8	22.5	9.9	87	50	69	69	2.0	12.2	5.9	6.7	5 ⊙	3 ⊙	5	W 2	W 3	SW 1
4	106.1	107.0	107.3	106.8	13.2	17.9	15.5	15.5	22.5	11.9	93	73	89	85	1.1	5.6	1.9	2.9	9	9	8	W 2	WSW 3	SW 3
5	108.8	108.8	108.8	108.8	14.1	19.7	17.7	17.3	22.8	12.0	97	74	80	84	0.6	5.9	4.0	3.5	10	7	1	W 2	W 4	NW 2
6	110.0	109.4	107.2	108.9	14.8	21.6	17.5	17.8	23.3	12.1	92	48	74	71	1.3	13.4	5.1	6.6	1 ⊙	4 ⊙	1	NW 3	NW 4	NW 2
7	105.8	102.5	97.4	101.9	17.9	24.0	19.7	20.3	25.6	12.2	81	43	77	67	3.8	17.0	5.3	8.7	8 ⊙	9	10	C 0	SE 1	SE 3
8	94.0	96.1	97.8	96.0	15.5	20.3	16.9	17.4	21.8	15.5	99	72	84	85	0.2	6.6	3.1	3.3	10	9 ⊙	1	W 4	W 3	NW 2
9	98.3	97.7	95.3	97.1	14.6	22.4	19.6	19.0	23.6	11.8	91	55	65	70	1.5	12.2	7.9	7.2	0 ⊙	6 ⊙	9	NE 2	SE 3	E 5
10	90.8	88.5	92.6	90.6	15.9	20.3	16.2	17.2	21.1	14.9	82	85	93	87	3.3	3.5	1.4	2.7	9 ⊙	10 ●	1	E 6	SE 1	S 1
11	98.8	100.7	100.7	100.1	17.5	25.2	21.9	21.6	27.5	15.2	86	56	68	70	2.8	14.1	8.3	8.4	2 ⊙	1 ⊙	1	SW 5	S 3	S 3
12	99.4	97.2	99.6	98.7	20.9	29.2	19.7	22.4	29.9	17.7	78	53	94	75	5.3	19.1	1.3	8.6	2 ⊙	4 ⊙	8	E 1	E 5	SW 4
13	101.8	102.7	102.1	102.2	18.3	25.2	19.6	20.7	27.0	15.2	88	48	71	69	2.4	16.7	6.5	8.5	1 ⊙	9	1	SW 2	WSW 5	C 0
14	100.2	98.9	96.2	98.4	18.5	24.3	20.3	20.8	24.8	17.3	92	71	92	85	1.7	8.9	1.8	4.1	10	9 ⊙	4	E 3	NE 1	NE 2
15	94.4	95.9	97.6	96.0	17.9	20.5	17.5	18.4	22.1	17.5	94	73	91	86	1.2	6.5	1.8	3.2	8	9	2	SW 6	SW 4	W 1
16	99.4	99.0	97.5	98.6	17.7	24.3	19.4	20.2	24.8	13.7	91	61	89	80	1.8	12.0	2.3	5.4	3 ⊙	5 ⊙	10	C 0	E 1	SW 2
17	97.3	97.6	96.6	97.2	14.0	15.7	14.0	14.4	20.0	13.8	99	92	93	95	0.2	1.3	1.1	0.9	10	10 ●	10 ●	SW 4	SW 5	SW 4
18	94.9	95.2	95.9	95.3	14.1	16.9	14.9	15.2	19.9	12.4	91	77	90	86	1.5	4.4	1.6	2.5	10	9	1	SW 6	SW 5	SW 4
19	98.7	100.6	102.9	100.7	14.1	21.7	16.3	17.1	23.0	11.9	93	60	84	79	1.1	10.4	2.9	4.8	8 ⊙	3 ⊙	2	SW 2	SW 5	SW 2
20	104.7	104.5	104.3	104.5	14.4	21.3	15.3	16.6	23.1	11.9	93	60	87	80	1.1	10.1	2.3	4.5	0 ⊙	5 ⊙	0	SW 1	SW 3	SSW 1
21	102.8	101.9	99.5	101.4	16.3	19.1	16.1	16.9	20.0	13.7	84	80	93	86	2.9	4.4	1.3	2.9	6 ⊙	10	2	SW 2	WSW 3	S 1
22	95.6	97.2	97.8	96.9	13.4	14.1	12.5	13.1	16.7	12.4	100	92	98	97	0.0	1.3	0.4	0.6	10 ●	10	10	NW 2	W 4	W 2
23	99.0	99.7	100.3	99.7	10.7	14.7	12.1	12.4	18.4	8.7	96	71	84	84	0.5	4.8	2.2	2.5	0 ⊙	5	1	WSW 2	W 3	C 0
24	99.9	95.8	95.2	97.0	12.5	20.3	14.2	15.3	22.5	8.4	71	57	84	71	4.2	10.2	2.5	5.6	0 ⊙	4 ⊙	10	SE 4	SE 7	SW 4
25	102.8	103.2	100.4	102.1	12.0	20.2	16.7	16.4	21.7	9.9	88	47	60	65	1.7	12.7	7.7	7.4	0 ⊙	3 ⊙	1	SW 2	S 3	SE 5
26	98.1	97.8	98.7	98.2	12.3	20.5	14.4	15.4	20.9	11.7	89	57	78	75	1.5	10.3	3.6	5.1	6 ⊙	8	5	SE 2	WSW 5	SW 3
27	99.9	101.5	102.2	101.2	11.9	16.6	11.7	13.0	19.7	8.9	87	70	93	83	1.8	5.7	1.0	2.8	6 ⊙	7 ⊙	0	SW 5	SW 2	SW 1
28	101.2	101.6	102.0	101.6	11.6	13.3	13.7	13.1	16.4	10.0	95	95	99	96	0.6	0.7	0.2	0.5	10 ●	10	10	C 0	SE 1	C 0
29	102.9	104.1	104.6	103.9	11.7	13.5	12.5	12.6	13.9	11.0	99	94	100	98	0.1	0.9	0.0	0.3	9	10	7	W 1	C 0	C 0
30	104.8	105.3	105.7	105.3	8.2	13.8	12.1	11.6	15.4	7.5	100	80	89	90	0.0	3.2	1.5	1.6	7 ⊙	10	6	WSW 4	W 4	C 0
31	106.0	105.3	103.9	105.1	10.6	18.2	11.7	13.0	19.5	8.9	88	56	93	79	1.5	9.2	1.0	3.9	8	8	9	SW 2	S 2	SW 2
M	101.4	101.3	101.0	101.2	14.5	19.9	16.1	16.6	21.9	12.4	90	67	84	80	1.7	8.5	3.0	4.4	5.7	6.9	4.5	2.7	3.3	2.1

Warszawa – Bielany $H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 17{,}7\ m$ **Lipiec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	○ a – p
2	8	4.1	.	-	•0-1 16²⁵ – 17³⁵ ; (K) 15³⁰ – 18⁰⁰ ; ∞ n – a ; ⊙ a – p
3	8	.	.	-	= ⌒¹ p – n ; ⊙ a – p
4	8	.	.	-	∞ n – a ; ⊙ a – p
5	8	0.0	.	-	▽•¹ 9⁵⁵ ; = n – a
6	9	.	.	-	⌒⁰ p – n ; ⊙ a – p
7	7	.	.	-	∞ a – p ; ⊙ a – p
8	9	.	.	-	(K) 17⁵⁰ – p SW – NE ; ⊙ a – p
9	6	8.1	.	-	•¹ 11²⁰ – 12⁵⁰ •⁰ – 16¹⁰ ; = n – a ; ⊙ a
10	7	.	.	-	= n – a ; ⌒⁰ p – n ; ⊙ a – p
11	8	6.0	.	-	▽•⁰ 21⁵³ ; ⌒⁰ n – a ; ⊙ a – p
12	7	0.2	.	-	• na
13	7	.	.	-	▽•⁰ na ; ≡⁰ n = n – a
14	7	.	.	-	≡ 2-0 n – 7¹⁰ = – a ∞⁰ a – p ; ⌒¹ n – a ⌒⁰ p – n ; ⊙ a – p
15	7	1.5	.	-	▽•⁰ 12⁴⁴ ▽•¹ 12⁵⁷ , 16¹⁰ ; (K) 10⁰⁰ – 13³⁶ ; = n – a
16	6	37.1	.	-	•2-1 10⁰⁵ – 15²⁵ •⁰ – 16³⁰ ; (K) 13⁴⁵ – p K 14⁴⁵ (pojed. grzmot.)
17	8	11.9	.	-	▽•⁰ 21¹⁰
18	7	0.4	.	-	•1-2 na ▽•² 14⁴⁵
19	8	.	.	-	⌒² na = ⌒¹ p – n ; ⊙ a – p
20	8	0.0	.	-	▽•⁰ p ; = ⌒¹ n – a ; ⊙ a – p
21	6	0.0	.	-	(K) 17⁰⁰ – p SW – NE ; = a – p ; ⌒⁰ n – a , p – n
22	7	0.1	.	-	•⁰ na ▽•a z prz
23	7	.	.	-	= na ; ⊙ a – p
24	6	0.5	.	-	▽•⁰ 9²¹ ▽•¹ 9³⁷ , 12²⁴ ▽•⁰ 18²⁵ ; (K) 9⁴⁷ W-E ; = n – p ; ⌒⁰ n – a
25	7	0.2	.	-	▽•¹ 11⁵⁰ , 20³⁶ ▽•⁰ np ; ⌒⁰ n – a ; ⊙ a – p
26	7	3.7	.	-	▽•⁷⁵⁵ •⁰ 9³⁰ •² 9⁴³⁻⁵⁰ ▽•⁰ 21³⁹ •¹ np ; = n – a
27	6	4.7	.	-	▽•¹ 13¹¹ , 13⁵² , 14²⁵ , 16⁰⁰ •2-1 16²⁵ – 17³⁰ ; (K) 13⁴¹ – p SW – NE
28	7	.	.	-	•⁰ na ; ⌒¹ p – n ; ⊙ a – p
29	7	0.8	.	-	▽•¹ 13²⁵ , 16¹⁰ ; (K) 12³⁰ – 13⁴⁰ SW-NE , 15¹⁸ – p SW-NE ; ⌒² n – a ; ⊙ a – p
30	7	2.7	.	-	▽•¹³⁵⁰ ▽•² 14⁰⁵ ▽•¹ p ; (K) 15¹⁵⁻⁴⁵ SW – NE ; = n – a
31	8	1.9	.	-	▽•² 16⁰⁰ ▽•¹ 17⁴⁰
Σ	–	83.9	–	-	UWAGI.

Sierpień – Août

1	7	.	.	-	⌒¹ n – a ; ⊙ a – p
2	8	.	.	-	⌒⁰ p – n ; ⊙ a – p
3	9	.	.	-	⌒⁰ n – a , p – n , ⊙ a – p
4	8	1.2	.	-	•0-1 18⁵⁰ – 20⁰⁰
5	8	.	.	-	⌒⁰ p – n
6	9	.	.	-	⌒¹ n – a , p – n ; ⊙ a – p
7	8	10.3	.	-	= ⌒² n – a ; ⊙ a
8	8	.	.	-	•² K na ; ⊙ a – p
9	8	.	.	-	= ⌒² n – a ; ⊙ a – p
10	5	18.0	.	-	•0-2 a – p ; = n – a ; ⊙ a
11	8	.	.	-	= n – a ; ⌒² p – n ; ⊙ a – p
12	7	.	.	-	(K) a , p ; = ⌒¹ n – a ⌒⁰ p – n ; ⊙ a – p
13	8	0.4	.	-	= ⌒² n – a ⌒² p – n ; ⊙ a
14	7	9.8	.	-	•⁰ na •0-1 23¹⁰ ; (K) 23¹⁰ ; = n – a ; ⊙ a
15	7	.	.	-	= n – a ; ⌒² p – n
16	7	5.6	.	-	= ⌒² n – a ⌒² p – n ; ⊙ a – p
17	6	3.0	.	-	•¹ na •⁰ 13³⁰ n
18	7	0.0	.	-	▽•⁰ 16²⁰ ; = n – a
19	7	.	.	-	= ⌒² n – a ⌒¹ p – n ; ⊙ a – p
20	7	.	.	-	= ⌒² n – a ⌒¹ p – n ; ⊙ a – p
21	7	11.7	.	-	= ⌒² n – a ⌒² p – n , ⊙ a
22	7	7.5	.	-	•2-0 na n
23	8	.	.	-	⌒² n – a ; ⊙ a
24	7	0.2	.	-	• p ; 20⁴⁵ – 21⁰⁰ ; = ⌒² n – a ; ⊙ a – p
25	7	.	.	-	⌒² n – a ⌒⁰ p – n ; ⊙ a – p
26	8	0.0	.	-	▽•¹⁶²⁰ ; = ⌒¹ n – a ⌒² p – n ; ⊙ a
27	7	1.8	.	-	•² p ; ⌒¹ n – a ; ⊙ a – p
28	6	1.3	.	-	•⁰ n p
29	6	3.7	.	-	• n p
30	7	.	.	-	= ⌒² n – a ⌒⁰ p – n ; ⊙ a
31	7	6.0	.	-	•2-0 17³⁰ – 19⁰⁰
Σ	–	80.5	–	-	UWAGI.

Warszawa – Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ Wrzesień – Septembre 1957

DNI	CIŚNIENIE P – 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	102.4	102.8	105.0	103.4	10.5	12.4	10.4	10.9	14.2	10.2	88	88	95	90	1.5	1.7	0.6	1.3	5 ⊙	9 ●	9	SW 5	SW 4	S 2
2	106.7	105.4	103.4	105.2	10.0	19.3	16.7	15.7	21.3	7.3	92	58	71	74	1.0	9.3	5.5	5.3	5 ⊙	9 ⊙	10	C 0	S 4	SE 3
3	102.4	102.7	103.8	103.0	13.2	17.0	13.4	14.2	19.4	12.4	99	83	94	92	0.2	3.4	0.9	1.5	10 ●	8 ⊙	10	S 1	SE 3	SW 2
4	106.3	107.7	109.0	107.7	11.6	17.3	14.5	14.5	18.1	11.1	100	60	84	81	0.0	7.8	2.7	3.5	10	9	6	NW 2	NW 2	W 2
5	109.4	108.8	107.0	108.4	10.4	20.3	15.3	15.3	20.8	8.5	95	49	74	73	0.6	12.1	4.6	5.8	1 ⊙	2 ⊙	9	C 0	S 1	SE 1
6	105.4	106.0	106.4	105.9	13.9	17.4	13.3	14.5	20.4	12.1	90	85	88	88	1.6	3.0	1.8	2.1	9 ⊙	10	0	SSE 1	WSW 2	WSW 3
7	108.4	108.6	108.2	108.4	11.7	21.7	17.4	17.0	22.8	10.7	100	56	72	76	0.0	11.4	5.5	5.6	9	8 ⊙	0	C 0	SE 3	SE 3
8	109.0	109.0	108.6	108.9	15.1	24.5	19.8	19.8	25.5	13.7	78	57	80	72	3.9	13.3	4.7	7.3	0 ⊙	1 ⊙	0	SE 4	SE 4	SE 3
9	109.1	107.9	107.3	108.1	16.4	27.7	20.0	21.0	28.6	14.2	90	48	91	76	1.9	19.4	2.2	7.8	0 ⊙	0 ⊙	1	S 4	S 5	S 3
10	108.9	108.7	106.2	107.9	14.3	13.8	13.1	13.6	20.5	12.9	92	94	96	94	1.3	0.9	0.6	0.9	10	10	4	NW 3	NW 4	C 0
11	103.7	99.1	92.6	98.5	11.3	19.4	16.6	16.0	20.6	8.5	100	61	67	76	0.0	8.8	6.3	5.0	4 ⊙ ≡	4 ⊙	10	SW 1	SSE 5	SE 5
12	85.7	83.2	89.9	86.3	16.4	22.9	13.1	16.4	24.3	13.0	90	64	62	72	1.9	10.1	5.8	5.9	5	9 ⊙	6	SE 5	SW 7	SW 7
13	94.5	94.4	92.9	93.9	10.9	17.4	13.6	13.9	17.8	9.0	79	54	67	67	2.7	9.1	5.2	5.7	4 ⊙	4 ⊙	2	SW 5	SW 5	S 5
14	93.6	94.5	95.2	94.4	9.5	14.8	11.3	11.7	17.7	8.5	89	69	79	79	1.3	5.2	2.8	3.1	2 ⊙	9 ⊙	1	S 1	SW 4	S 1
15	90.4	93.5	98.0	94.0	8.7	10.1	9.7	9.6	12.1	8.2	100	99	96	98	0.0	0.2	0.4	0.2	10 ●	10	0	W 6	SW 4	SW 4
16	102.0	103.3	104.5	103.3	7.6	13.1	8.4	9.4	13.9	6.2	96	67	92	85	0.4	5.0	0.9	2.1	4 ⊙	9	0	SW 2	SW 5	C 0
17	104.6	102.8	99.9	102.4	6.3	11.5	8.1	8.5	13.0	4.2	98	70	94	87	0.1	4.1	0.6	1.6	2 ⊙	8	6	SW 2	SW 1	SW 1
18	96.7	94.0	94.6	95.1	6.3	10.2	10.8	9.5	12.4	4.5	100	90	72	87	0.0	1.2	3.7	1.6	9	10	9	WSW 3	W 7	W 8
19	95.2	95.1	92.5	94.3	9.2	13.2	11.3	11.2	14.5	8.9	91	67	100	86	1.1	5.0	0.0	2.0	9	9	10 ●	SW 4	W 3	C 0
20	94.1	97.8	101.1	97.7	9.5	12.2	10.3	10.6	14.2	9.4	100	70	83	84	0.0	4.3	2.1	2.1	10	9	10	W 3	W 5	SW 2
21	103.2	103.8	103.6	103.5	6.1	12.9	10.0	9.8	15.0	5.9	95	75	91	87	0.4	3.8	1.1	1.8	7 ⊙	8	3	SW 2	C 0	C 0
22	101.1	97.9	97.5	98.8	9.2	11.6	14.2	12.3	15.0	7.5	80	99	100	93	2.3	0.1	0.0	0.8	10 ●	10 ●	10	E 2	SE 2	C 0
23	94.0	89.8	82.7	88.8	14.7	19.5	14.2	15.6	20.5	13.5	94	80	95	90	0.9	4.5	0.7	2.0	9	10	10 ●	S 3	S 3	SW 9
24	90.0	91.1	91.8	91.0	11.1	13.0	7.4	9.7	14.9	7.4	89	80	87	85	1.5	3.0	1.3	1.9	7 ⊙	10 ●	0	W 5	SW 3	W 7
25	95.2	99.7	103.6	99.5	5.7	9.9	4.9	6.4	11.0	4.9	82	62	78	74	1.7	4.6	2.0	2.8	7 ⊙	9 ⊙	0	W 9	W 10	SW 1
26	103.3	102.6	104.1	103.3	2.1	9.5	3.2	4.5	11.7	0.7	96	53	91	80	0.3	5.6	0.7	2.2	4	7	0	SW 1	W 3	W 1
27	105.3	103.4	93.6	100.8	2.8	9.8	7.7	7.0	10.7	2.0	84	59	87	77	1.2	4.9	1.3	2.5	4 ⊙	9	10 ●	WSW 2	SW 6	SW 6
28	87.1	89.6	90.4	89.0	9.4	11.5	8.3	9.4	13.0	7.3	83	77	92	84	2.0	3.2	1.0	2.1	8	9	10	W 6	W 12	SW 6
29	91.4	89.2	85.8	88.8	7.5	10.5	8.5	8.8	11.2	6.3	94	85	100	93	0.6	1.9	0.0	0.8	7	10 ●	10 ●	SW 2	SW 4	C 0
30	88.8	91.8	98.0	92.9	6.0	6.3	5.6	5.9	9.8	5.6	94	91	97	94	0.6	0.8	0.3	0.6	5 ⊙	10	1	WSW 4	W 5	SW 2
31																								
M	99.6	99.5	99.2	99.4	9.9	15.0	11.7	12.1	16.8	8.5	92	72	86	83	1.0	5.6	2.2	2.9	6.2	8.0	5.2	2.9	4.2	2.9

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1	102.1	103.0	104.3	103.1	2.8	9.1	5.4	5.7	10.4	1.7	98	75	97	90	0.2	3.0	0.3	1.2	2 ⊙	9 ⊙	7	SW 2	SW 2	SW 2
2	109.3	111.5	110.7	110.5	1.4	8.3	2.7	3.8	10.3	0.9	100	70	93	88	0.0	3.3	0.5	1.3	4 ⊙	9	0	SW 2	SW 3	S 2
3	106.5	102.5	97.6	102.2	1.8	11.0	9.3	7.8	11.6	0.9	94	59	70	74	0.4	5.4	3.5	3.1	1 ⊙	8 ⊙	10	C 0	SW 5	SW 5
4	96.2	98.4	104.1	99.6	6.3	7.7	4.2	5.6	9.3	4.2	89	80	85	85	1.0	2.1	1.2	1.4	7	9 ●	2	SW 5	SW 3	SW 6
5	107.9	108.8	106.9	107.9	3.1	8.2	6.3	6.0	9.1	1.2	97	66	81	81	0.2	3.7	1.8	1.9	8 ⊙	10	9	SW 3	SW 5	SW 4
6	104.1	106.6	109.4	106.7	7.0	10.2	9.8	9.2	12.4	5.6	88	91	91	90	1.2	1.1	1.1	1.1	10	10	9	SW 4	SW 5	SW 4
7	108.6	109.1	110.8	109.5	9.9	12.5	11.8	11.5	14.7	9.5	92	86	90	89	1.0	2.1	1.3	1.5	10	10	10	SW 4	W 6	W 4
8	115.5	117.4	117.1	116.7	7.7	13.1	9.2	9.8	15.2	7.3	100	73	87	87	0.0	4.1	1.5	1.9	6 ⊙	6	0	C 0	C 0	C 0
9	115.2	114.3	112.0	113.8	6.1	17.0	12.3	11.9	18.2	3.4	86	48	63	66	1.3	10.0	5.3	5.5	0 ⊙	1 ⊙	0	C 0	SE 4	SE 5
10	110.6	110.8	109.4	110.3	5.8	18.0	13.1	12.5	18.9	5.2	85	60	79	75	1.4	8.2	3.1	4.2	0 ⊙	0 ⊙	0	C 0	SE 4	S 2
11	109.1	108.6	108.0	108.6	8.5	18.8	10.3	12.0	20.0	8.0	93	59	87	80	0.8	9.0	1.6	3.8	1 ⊙	3 ⊙	0	S 1	W 2	C 0
12	106.4	106.4	111.9	108.2	6.4	15.3	11.5	11.2	17.0	5.7	100	74	90	88	0.0	4.6	1.4	2.0	1 ⊙	9 ⊙	10	SW 2	W 3	W 4
13	115.4	115.2	112.6	114.4	3.4	8.6	6.6	6.3	11.7	3.2	100	96	100	99	0.0	0.5	0.0	0.2	10 ≡	10	2	C 0	S 2	C 0
14	109.3	110.6	112.3	110.7	7.5	10.7	9.3	9.2	11.2	6.3	99	91	96	95	0.2	1.2	0.5	0.6	9 ⊙	10	10	C 0	W 2	WSW 2
15	114.6	115.3	116.1	115.3	4.8	7.9	7.2	6.8	9.9	4.7	97	71	74	81	0.3	3.1	2.7	2.0	8	9	10	SW 2	NW 2	NW 1
16	115.0	113.8	110.8	113.2	6.3	9.5	5.6	6.8	10.4	5.6	84	65	83	77	1.5	4.2	1.6	2.4	9	10	4	C 0	SE 2	SE 4
17	105.8	104.5	106.4	105.6	6.3	16.1	10.1	10.6	16.7	4.2	92	64	93	83	0.7	6.7	0.8	2.7	0 ⊙	8	3	SE 1	SW 4	SW 1
18	102.2	99.8	98.5	100.2	9.9	14.5	14.9	13.6	15.4	9.3	93	88	87	89	0.8	2.0	2.2	1.7	10	10 ●	10	SE 2	SW 2	SW 2
19	97.8	97.5	95.4	96.9	11.6	19.4	14.3	14.9	21.0	11.0	81	59	73	71	2.6	9.1	4.5	5.4	9 ⊙	8 ⊙	7	C 0	SW 1	SW 2
20	95.9	100.7	103.4	100.0	10.3	10.3	7.6	9.0	14.8	7.6	96	82	99	92	0.5	2.2	0.1	0.9	10	10 ●	10	SW 3	WSW 3	W 1
21	104.4	103.6	102.2	103.4	7.5	12.0	5.7	7.7	12.7	5.7	99	59	94	84	0.2	5.7	0.6	2.2	9	5 ⊙	0	C 0	SW 2	S 2
22	97.1	94.1	92.8	94.7	5.9	9.9	9.1	8.5	10.1	5.5	89	76	91	85	1.0	3.0	1.1	1.7	2 ⊙	10	10 ●	SE 5	SE 4	SE 3
23	93.6	96.1	100.7	96.8	7.8	11.0	7.8	8.6	12.1	7.7	100	89	90	93	0.0	1.5	1.1	0.9	10 ●	10	10	C 0	SW 2	SW 5
24	100.3	101.5	106.4	102.7	5.6	7.2	8.6	7.5	8.9	3.1	80	88	94	87	1.8	1.2	0.6	1.2	10	10	3	S 2	SW 4	SW 3
25	110.8	112.9	112.9	112.2	5.4	10.7	4.8	6.4	11.4	4.8	97	58	94	83	0.3	5.4	0.6	2.1	4	2 ⊙	2	SW 2	WSW 4	SW 1
26	111.1	111.3	109.4	110.6	6.8	13.3	8.0	9.0	14.3	4.6	87	61	84	77	1.3	6.0	1.6	3.0	9	4	0	SW 2	SW 2	SW 1
27	106.5	106.2	106.0	106.2	4.1	12.9	9.7	9.1	13.7	4.1	100	71	92	88	0.0	4.3	0.9	1.7	0 ⊙	4 ⊙	10	C 0	SW 2	C 0
28	106.2	107.3	107.5	107.0	9.4	10.7	8.4	9.2	10.7	8.4	92	73	90	85	1.0	3.6	1.0	1.9	9	10	9	SW 1	SW 1	C 0
29	106.3	105.2	106.0	106.2	5.7	13.5	8.7	9.2	14.5	5.3	94	60	85	80	0.6	6.2	1.6	2.8	8	6 ⊙	4	S 2	S 2	C 0
30	104.2	102.7	102.2	103.0	7.1	14.8	10.2	10.6	15.9	6.0	91	63	86	80	0.9	6.2	1.7	2.9	6	6 ⊙	7	S 1	S 2	S 2
31	101.6	101.0	99.1	100.6	9.0	13.8	10.5	11.0	14.9	8.6	93	75	87	85	0.8	3.9	1.6	2.1	7	9 ⊙	10	SW 2	SW 4	SW 2
M	106.1	106.4	106.5	106.3	6.5	12.1	8.8	9.1	13.5	5.5	93	72	87	84	0.7	4.3	1.5	2.2	6.1	7.6	5.7	1.5	2.9	2.3

Warszawa – Bielany $H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w =$ IX 17,7 m, X 15 m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	2.8	.	-	• ^{1} *na*, 13^{38} ▽ *p*; ⊏ *p* S–N
2	7	0.3	.	-	= ⌒^{1} *n – a*; ⊙ *a – p*
3	7	3.0	.	-	• ^{0} *n – a*; ○ *p*; ▽ *p – n*
4	9	.	.	-	= ⌒^{1} *n – a* ⌒^{0} *p – n*
5	9	.	.	-	= ⌒^{1} *n – a* ⌒^{0} *p – n*; ⊙ *a – p*
6	6	.	.	-	= ⌒^{2} *n – a* = ⌒^{1} *p – n*; ⊙ *a*
7	7	.	.	-	= *n – a* ∞ *a – p*; ⌒^{2} *n – a*, *p – n*; ⊙ *a – p*
8	7	.	.	-	= *n – a*; ⊙ *a – p*
9	8	.	.	-	= ⌒^{2} *n – a* ⊙ *a – p*
10	7	2.0	.	-	• *a*
11	7	.	.	-	≡^{0} *n – a*, ○ *a – p*
12	7	0.0	.	-	▽ 13^{41}; ∞ *n – a – p*; ⊙ *a – p*
13	8	0.5	.	-	⊙ *a – p*
14	8	4.5	.	-	• ^{1} *n – a*; ○ *a – p*
15	7	13.5	.	-	• ^{1} *n – a* ▽ *a … p*
16	7	.	.	-	= ⌒^{1} *n – a*; ⊙ *a*
17	7	.	.	-	= ⌒^{2} *n – a* ⌒^{2} *p – n*; ⊙ *a*
18	6	1.2	.	-	• ^{0} *a – p*, ≡ *p* ≡ *p – n*, = ⌒^{2} *n – a*
19	7	6.3	.	-	• ^{0} *p – n*
20	8	.	.	-	• ^{0} *n*
21	8	.	.	-	⌒^{1} *n – a*, *p – n*; ⊙ *a*
22	5	4.5	.	-	• ^{0} *n – a* • ^{1} *a – p*; = *p – n*
23	6	25.6	.	-	• $^{2-0}$ 14^{36} *n*; ≡ *p – n*; = *n – p*; ⌒^{2} *n – a*
24	7	5.6	.	-	• $^{0-1}$ 13^{30} *p*; ⊙ *a*
25	9	.	.	-	≡ *n – a – p* ≡ *n*; ⊙ *a – p*
26	9	.	.	-	⌴^{0} *n* ⌒^{2} *n – a* ⌒^{0} *p – n*
27	7	3.8	.	-	• $^{0-1}$ *p – n*; = ⌒^{2} *n – a*; ⊙ *a – p*
28	8	0.4	.	-	• ^{0} *a … n*
29	6	5.7	.	-	• ^{1} *a – n*
30	7	0.8	.	-	• *a*
31					
Σ	–	80.5	–	-	UWAGI.

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1	8	1.1	.	-	• *a*, *p*; = ⌒^{2} *n – a*; ⊙ *a – p*
2	8	.	.	-	⌴^{0} *n – a* ⌒^{1} *p – n*; ⊙ *a*
3	6	.	.	-	= *n – p*; ⌴^{2} *n – a*; ⊙ *a – p*
4	7	1.7	.	-	▽^{1} *a … p*
5	7	0.2	.	-	⌴^{0} *n – a*; ⊙ *a*
6	6	0.2	.	-	• ^{0} *na*, *a*; = *a – p*; ⌒^{0} *p – n*
7	7	.	.	-	
8	7	.	.	-	= ⌒^{1} *n – a*, *p – n*; ⊙ *a*
9	7	.	.	-	= ⌒^{2} *n – a* ⌒^{0} *p – n*; ⊙ *a – p*
10	6	.	.	-	= *n – p*; ⌒^{1} *n – a* ⌒^{0} *p – n*; ⊙ *a – p*
11	7	.	.	-	= *n – p*; ⌒^{1} *n – a* ⌒^{0} *p – n*; ⊙ *a – p*
12	6	.	.	-	= *n – n*; ⌒^{2} *n – a* ⌒^{0} *p – n*; ⊙ *a – p*
13	6	.	.	-	≡^{2} *n – a* = *a – n*
14	5	.	.	-	= *n – n*; ⌒^{1} *n – a* ⌒^{0} *p – n*
15	7	.	.	-	= ⌒^{0} *n – a*
16	7	.	.	-	= ⌒^{1} *n – a* ⌒^{0} *p – n*
17	6	.	.	-	= *n – p*; ⌒^{0} *n – a* ⌒^{1} *p – n*; ⊙ *a*
18	6	0.2	.	-	• ▽^{0} *a*; = ⌒^{0} *n – a*
19	7	.	.	-	= *n – p*; ⌒^{0} *n – a*; ⊙ *a – p*
20	7	1.0	.	-	• $^{0-1}$ *a … p*; = *n – p*
21	7	.	.	-	= *n – a*; ⌒^{0} *p – n*; ⊙ *a – p*
22	7	0.8	.	-	• ▽^{0} *p*; = ⌒^{1} *n – a*; ⊙ *a*
23	6	.	.	-	• ^{01} *n – a*; = *n – p*
24	7	.	.	-	= *n – p*; ⌒^{0} *p – n*
25	8	.	.	-	= ⌒^{1} *n – a*, *p – n*; ⊙ *a – p*
26	6	.	.	-	= *n – p*; ⌒^{0} *n – a* ⌒^{1} *p – n*
27	6	.	.	-	= *n – n*; ⌒^{1} *n – a* ⌒^{0} *p – n*; ⊙ *a – p*
28	6	.	.	-	= *n – p*; ⌒^{0} *n – a*
29	6	.	.	-	= *n – p*; ⌒^{1} *n – a*, *p – n*; ⊙ *a – p*
30	6	0.6	.	-	• *np*; = *n – p*; ⌒^{1} *n – a*, *p – n*
31	7	.	.	-	• *na*; = *n – a*; ⊙ *a – p*
Σ	–	5.8	–	-	UWAGI.

Warszawa – Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ Listopad – Novembre 1957

DNI	CIŚNIENIE P=900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.8	94.8	96.7	95.8	6.5	14.5	9.0	9.8	14.9	6.1	96	64	86	82	0.5	6.0	1.6	2.7	7 ⊙	0 ⊙	4	S 3	S 2	S 2
2	99.8	101.3	102.9	101.3	6.8	11.5	8.7	8.9	12.1	6.3	97	82	94	91	0.3	2.5	0.6	1.1	3	10	9	S 1	S 2	SW 2
3	103.7	103.7	103.8	103.7	7.6	10.4	8.9	9.0	11.0	6.8	100	87	97	95	0.0	1.6	0.3	0.6	10	10	10	NW 2	NW 1	E 3
4	102.5	101.8	102.9	102.4	8.2	15.5	12.1	12.0	16.2	7.8	100	75	91	89	0.0	4.4	1.2	1.9	10	0 ⊙	0	E 2	SE 2	SE 3
5	102.2	100.5	99.9	100.9	8.2	15.8	11.3	11.6	16.4	7.9	97	69	91	86	0.3	5.5	1.2	2.3	3	3 ⊙	4	SE 3	SE 5	SE 6
6	101.0	99.8	99.7	100.2	8.8	15.5	11.7	11.9	15.9	8.8	92	67	82	80	0.9	5.8	2.5	3.1	5	6 ⊙	4	SE 7	SE 6	SE 7
7	96.9	96.6	98.0	97.2	10.5	13.7	11.6	11.8	14.2	9.8	80	70	83	78	2.6	4.7	2.3	3.2	8	9	10	SE 10	SE 5	SE 5
8	98.4	98.3	98.4	98.4	7.0	10.7	8.5	8.7	12.7	6.5	94	81	92	89	0.6	2.5	0.9	1.3	7	7	8	SE 3	SE 3	E 5
9	96.7	96.3	98.2	97.1	8.1	12.0	7.0	8.5	13.5	7.0	96	80	98	91	0.5	2.8	0.1	1.1	9	4 ⊙	1	E 4	E 3	E 1
10	99.5	100.7	102.6	100.9	7.3	9.6	10.0	9.2	10.0	6.2	100	97	89	95	0.0	0.4	1.3	0.6	10 ≡	10	10	C 0	E 1	E 4
11	105.0	106.8	108.7	106.8	8.3	9.1	6.4	7.6	10.3	6.4	96	97	88	94	0.5	0.4	1.1	0.7	10	10	10	NE 4	NE 6	NE 6
12	111.8	114.4	116.6	114.3	5.8	4.6	3.0	4.1	6.4	3.0	97	85	88	90	0.3	1.3	0.9	0.8	10	10	10	NE 6	NNE 7	NE 5
13	117.9	118.6	119.4	118.6	0.2	-0.4	-2.1	-1.1	3.0	-2.1	78	76	87	80	1.4	1.4	0.6	1.1	10	10	10	NE 5	NE 2	NE 2
14	119.2	119.9	120.6	119.9	-2.8	-0.3	0.1	-0.7	0.6	-3.3	80	76	86	81	1.0	1.5	0.9	1.1	10	10	10	NE 3	S 2	S 2
15	121.4	120.8	119.0	120.4	0.2	1.4	-2.8	-1.0	2.1	-2.9	88	70	86	81	0.7	2.1	0.7	1.2	10	10	0	C 0	SE 3	ESE 1
16	118.3	119.0	120.7	119.3	-4.7	-1.1	-0.1	-1.5	-0.1	-4.8	93	91	86	90	0.3	0.4	0.9	0.5	7	10	9 ≡	SE 1	C 0	SE 2
17	121.4	121.7	123.1	122.1	-0.2	2.7	1.2	1.2	2.7	-0.3	86	60	83	76	0.8	2.9	1.2	1.6	10	10	10	SE 2	SE 3	SE 2
18	123.2	122.1	121.1	122.1	1.1	3.1	2.2	2.2	3.7	1.1	90	56	70	72	0.6	3.3	2.2	2.0	10	10	10	SE 2	SE 3	SE 2
19	121.7	124.8	127.0	124.5	0.8	2.5	1.1	1.4	3.4	0.8	86	60	83	76	0.9	2.9	1.1	1.6	10	10	10	SE 1	SE 3	SE 1
20	128.4	128.8	128.2	128.5	1.2	2.7	-1.6	0.2	2.8	-1.7	90	63	88	80	0.7	2.7	0.6	1.3	9	10	9	SE 2	SE 3	C 0
21	126.6	125.2	120.6	124.1	-2.7	4.5	-1.5	-0.3	5.1	-3.2	91	57	88	79	0.5	3.6	0.7	1.6	3	1 ⊙	0	C 0	C 0	C 0
22	113.9	110.2	106.6	110.2	-3.8	4.6	-0.3	0.0	5.2	-4.8	89	62	76	76	0.5	3.3	1.5	1.8	2	0 ⊙	0	SE 1	SE 2	S 2
23	105.2	103.6	102.7	103.8	0.6	2.0	1.7	1.5	2.7	-0.8	84	75	98	86	1.0	1.8	0.1	1.0	10	10	10 ⁂	SW 2	SW 2	SW 3
24	107.4	106.8	104.9	106.4	2.0	2.4	4.5	3.4	4.7	1.7	93	84	97	91	0.6	1.2	0.3	0.7	9	10 ✳	10 ⁂	W 4	W 4	W 2
25	103.1	102.8	105.4	103.8	5.1	5.9	7.2	6.4	7.6	4.5	98	98	99	98	0.2	0.2	0.2	0.2	10 ●	10 ●	10	W 3	W 3	W 2
26	107.3	107.7	105.8	106.9	7.5	7.8	7.0	7.3	7.8	7.0	100	99	98	99	0.0	0.2	0.1	0.1	10 ●	10 ●	10	W 2	W 3	WSW 3
27	100.5	98.7	102.8	100.7	6.0	6.9	6.3	6.4	8.4	5.7	95	94	85	91	0.5	0.5	1.4	0.8	10	10 ●	10	W 6	W 5	W 4
28	100.0	96.1	90.7	95.6	5.2	7.6	7.3	6.8	8.8	4.7	98	99	88	95	0.1	0.1	1.2	0.5	10 ●	10 ●	10	SW 1	W 4	W 4
29	91.3	96.5	109.0	98.9	2.2	-3.1	-7.4	-3.9	7.3	-7.6	80	75	71	75	1.5	1.2	1.0	1.2	9	10 ✳	10	NW 8	NW 8	NW 6
30	114.5	114.9	115.6	115.0	-7.0	-4.5	-6.3	-6.0	-3.5	-7.9	72	58	73	68	1.0	1.9	1.0	1.3	1	3 ⊙	8	N 6	NNW 8	N 6
31																								
M	108.5	108.4	109.1	108.7	3.5	6.3	4.2	4.6	7.5	2.3	91	77	87	85	0.6	2.3	1.0	1.3	8.1	7.8	7.5	3.1	3.4	3.1

Grudzień – Décembre

1	115.7	114.8	113.8	114.8	-7.2	-2.4	-2.0	-3.4	-1.2	-7.9	77	68	85	77	0.8	1.6	0.8	1.1	1	10	10	W 4	W 3	SW 2
2	114.0	114.3	114.5	114.3	-2.2	-1.3	-1.8	-1.8	-1.3	-2.3	94	90	98	94	0.3	0.5	0.1	0.3	10	10	9	C 0	W 1	W 1
3	110.4	108.3	108.9	109.2	-1.7	-1.1	-0.7	-1.0	0.3	-2.8	94	95	95	95	0.3	0.3	0.3	0.3	10 ✳	10 ✳	10	W 1	SW 1	C 0
4	110.4	110.4	108.6	109.8	-0.8	0.0	0.1	-0.2	0.6	-0.8	97	96	100	98	0.2	0.2	0.0	0.1	10 ✳	10	10 ● ≡	C 0	C 0	C 0
5	103.5	103.3	105.7	104.2	1.8	4.8	3.7	3.5	5.6	-0.7	100	92	87	93	0.0	0.7	1.1	0.6	10 ●	9	9	WSW 2	W 2	W 3
6	111.3	113.3	112.8	112.5	1.0	1.3	-1.4	-0.1	4.4	-1.4	88	79	89	85	0.8	1.4	0.6	0.9	9	4	3	W 4	NW 1	NW 1
7	105.4	100.8	95.9	100.7	-2.6	0.8	-0.8	-0.8	1.6	-2.7	91	75	87	84	0.5	1.6	0.7	0.9	2	4 ⊙	2	SSE 3	SW 2	C 0
8	83.5	74.9	64.7	74.4	-0.7	1.8	4.6	2.6	4.8	-2.0	91	87	97	92	0.5	0.9	0.3	0.6	10 ✳	10	10	S 4	S 3	S 5
9	60.9	68.9	82.6	70.8	5.8	4.2	-1.4	1.8	6.6	-1.4	77	77	72	75	2.1	1.8	1.5	1.8	9	10	1	SW 8	W 8	SW 3
10	85.6	85.3	90.7	87.2	-2.6	-0.3	-5.0	-3.2	-0.3	-5.3	85	72	80	79	0.8	1.7	0.8	1.1	2	8 ⊙	1	SW 3	WSW 2	SW 3
11	97.3	97.6	94.2	96.4	-6.5	-2.3	-4.1	-4.2	-2.3	-7.7	81	61	75	72	0.7	2.0	1.1	1.3	0	9 ⊙	0	SW 3	C 0	SE 2
12	89.6	87.9	86.8	88.1	-0.9	1.2	2.6	1.4	2.6	-4.1	79	85	91	85	1.2	1.1	0.7	1.0	10	10	0	E 3	NE 2	SE 3
13	84.4	82.2	75.7	80.8	4.8	6.1	7.4	6.4	7.5	2.2	87	91	83	87	1.1	0.8	1.8	1.2	9	10	10	SE 3	SE 5	SE 4
14	69.5	74.9	86.7	77.0	4.2	1.7	-3.6	-0.3	7.7	-3.7	100	100	94	98	0.0	0.0	0.3	0.1	10	10 ●	10 ✳	C 0	NNW 3	N 3
15	101.1	109.0	114.8	108.3	-6.6	-7.1	-10.2	-8.5	0.8	-10.3	86	69	91	82	0.5	1.1	0.3	0.6	10	8	0	N 4	N 5	N 1
16	118.3	119.3	118.6	118.7	-13.5	-9.5	-11.0	-11.2	-9.0	-13.9	92	85	76	84	0.2	0.4	0.6	0.4	0	0 ⊙	5	C 0	NNW 2	ESE 4
17	114.4	112.5	110.3	112.4	-14.3	-9.4	-8.0	-9.9	-7.5	-14.7	87	79	90	85	0.3	0.6	0.3	0.4	1	10	10	E 2	E 2	W 2
18	110.6	111.6	112.8	111.7	-7.1	-6.4	-6.6	-6.7	-5.5	-8.2	93	91	91	92	0.2	0.3	0.3	0.3	10	10	10	NNW 2	NNW 2	N 2
19	114.1	116.3	119.2	116.5	-5.2	-4.3	-3.4	-4.1	-3.2	-6.9	93	82	85	87	0.3	0.8	0.7	0.6	10	10	10	SE 2	NNW 2	C 0
20	120.0	120.3	119.5	119.9	-2.1	0.4	0.3	-0.3	1.6	-3.4	87	100	98	95	0.6	0.0	0.1	0.2	10	10 ≡	9	C 0	SW 2	SW 1
21	115.9	114.1	114.5	114.8	-1.8	2.0	1.8	1.0	2.8	-2.1	94	82	87	88	0.3	1.3	0.9	0.8	2	9	10	C 0	SW 2	SW 2
22	115.2	114.8	114.5	114.8	0.8	1.5	1.0	1.1	2.5	0.8	98	92	96	95	0.2	0.5	0.3	0.3	10 ●	10	10	C 0	S 2	S 2
23	112.0	109.9	107.8	109.9	0.1	-0.3	-2.8	-1.4	1.1	-2.9	90	82	88	87	0.7	1.1	0.6	0.8	9	9 ⊙	0	SE 2	SE 3	SE 4
24	105.9	106.2	107.5	106.5	-6.0	-2.2	-4.6	-4.4	-1.8	-6.5	89	74	86	83	0.4	1.3	0.6	0.8	0	8 ⊙	0	S 3	S 3	S 1
25	108.0	107.4	106.8	107.4	-4.3	1.1	-1.2	-1.4	1.2	-5.5	94	81	93	89	0.3	1.2	0.4	0.6	0	7 ⊙	6	S 2	S 2	S 2
26	109.9	110.7	112.9	111.2	-1.3	0.8	1.0	0.4	1.4	-2.1	90	86	96	91	0.5	0.9	0.3	0.6	10	10	10	S 2	SW 3	SW 2
27	112.7	112.3	111.2	112.1	0.9	0.9	1.4	1.2	2.1	0.8	100	100	98	99	0.0	0.0	0.2	0.1	10	10 ≡	10	SW 2	SW 1	SW 1
28	106.3	103.0	98.4	102.6	2.0	2.3	1.3	1.7	2.4	1.2	91	87	85	88	0.7	0.9	1.0	0.9	9	10	7	SW 2	SW 3	SW 2
29	95.2	94.6	91.9	93.9	0.5	2.2	1.0	1.2	2.8	0.2	100	87	94	94	0.0	1.0	0.4	0.5	10	10	10 ✳	SW 3	SW 3	SW 2
30	86.0	85.4	82.9	84.8	2.6	3.2	2.3	2.6	4.4	0.9	86	86	91	88	1.1	1.1	0.6	0.9	9	10 ●	10 ⁂	SW 5	SW 4	SW 5
31	86.6	88.7	88.9	88.1	0.7	1.2	0.4	0.7	3.4	0.2	92	85	90	89	0.5	1.1	0.6	0.7	9	10	9	SW 4	W 4	SW 2
M	102.4	102.4	102.4	102.4	-2.0	-0.3	-1.3	-1.2	1.2	-3.6	90	84	89	88	0.5	0.9	0.6	0.7	7.1	8.9	6.8	2.4	2.5	2.2

Warszawa – Bielany $H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 15\ m$ **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	.	–	= ⌒¹ n – a ∞⁷ a – p; ⌒¹ p – n; ⊙ a – p
2	6	.	.	–	= n – n; ⌒⁷ p – n
3	6	.	.	–	= n – n; ⌒⁰ p – n
4	6	0.1	.	–	= n – p; ⊙ a – p
5	7	.	.	–	= n – a ∞⁰ a – p; ⌒¹ n – a, p – n; ⊙ a – p
6	7	.	.	–	= n – p; ⌒⁰ n – a; ⊙ a – p
7	8	0.3	.	–	●⁰ p
8	6	.	.	–	= n – p
9	7	.	.	–	= n – a ∞ a – p = ⌒⁰ p – n
10	6	.	.	–	≡⁰ n – a = a – p
11	6	.	.	–	= n – a – p
12	7	.	.	–	= n – a
13	8	.	.	–	
14	6	0.0	.	–	▽⁰ a; = n – p
15	7	.	.	–	= n – a, p – n
16	3	.	.	–	= n – a ≡¹⁻⁰ a – p; ⌴²⁻¹ n – a
17	7	.	.	–	
18	7	.	.	–	= n – a
19	7	.	.	–	= n – a
20	7	.	.	–	= n – a; ⌴⁰ p – n
21	6	.	.	–	= n – n; ⌴¹ n – n; ⊙ a – p
22	6	.	.	–	= n – a; ⌴²⁻⁰ n – n; ∞ ⊙ a – p
23	6	1.0	.	–	● p * p – n; = n – p; ⌴⁰ n – a
24	6	1.3	.	–	* a – p * p – n
25	6	2.7	.	–	● n – p ● p
26	6	1.2	.	–	● n... n
27	6	2.0	.	–	▽⁰ a
28	6	10.4	.	–	●¹⁻⁰ 645 ... n
29	8	0.0	.	–	*⁰ 1230 – p; ⩢ n – n
30	8	.	.	–	⩢ n ⩢ n – n; ⊙ a – p
31					
Σ	–	19.0	–	–	UWAGI. W listopadzie wartości ciśnienia atmosferycznego są za wysokie przeciętnie o około 0.4 mb.

Grudzień – Décembre

1	8	.	.	–	
2	6	0.6	.	–	△⁰ *⁰ a – p; = ⌴⁰ p – n
3	5	3.4	0	–	*⁰ n – p
4	6	2.3	2	–	*⁰ n – a ● p – n; = a – p ≡⁰ p – n
5	6	0.0	.	–	● n ● n – a; = n – p
6	8	.	.	–	⌴⁰ p – n
7	6	0.2	.	–	= p – n; ⌴¹⁻⁰ n – p; ⊙ a – p
8	6	9.6	2	–	*¹ n – a *⁰ ●⁰ p ●⁰ p – n; = p – n
9	9	0.0	.	–	▽ p; ⩢ n – a, per. ponad 15 m/sek n
10	7	0.5	.	–	*(K) p *+ p
11	6	.	1	–	= a – p; ⊙ a – p
12	6	.	1	–	= a – p
13	6	.	.	–	
14	6	13.9	.	–	● a – p △ p *¹ p – n
15	7	.	7	–	* n; ⌴⁰ p – n
16	6	.	7	–	≡ n – a = a – p; ⌴²⁻⁰ n – p; ⊙ a – p
17	6	.	6	–	⌴²⁻⁰ n – n
18	6	.	6	–	
19	6	.	5	–	
20	3	.	5	–	≡⁰ a – p
21	6	0.0	4	–	⌴¹ n – a
22	6	0.0	2	–	●⁰ n – a
23	5	.	pż.	–	= n – p; ⊙ a – p
24	6	.	pż.	–	= a – p; ⌴¹ n – n; ⊙ a – p
25	6	.	pż.	–	= n – p; ⌴²⁻⁰ n – n; ⊙ a – p
26	5	.	pż.	–	
27	3	.	pż.	–	= n – a ≡⁰ a – p
28	6	0.9	.	–	*⁰ n p
29	6	1.3	1	–	*⁰ p... n; = a – p
30	6	2.7	.	–	●¹ a – p ● p – n; = a – p
31	7	2.0	pż.	–	⩛ n * p
Σ	–	37.4	–	–	UWAGI.

Zielona Góra — φ = 51°56' — λ = 15°30' — Styczeń – Janvier 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	94.7	94.7	92.9	94.0	-9.3	-7.2	-4.1	-5.2	-3.8	-11.2	98	99	98	98	0.1	0.0	0.1	0.1	9	10 ≡	10	ENE 1	ENE 11	NE 1
2	90.1	91.3	95.6	92.3	-1.8	0.9	0.7	0.1	1.4	-4.4	98	88	92	93	0.1	0.7	0.5	0.4	10	9	10	C 0	C 0	S 2
3	99.3	99.3	98.7	99.1	-0.2	0.7	-0.4	-0.1	1.7	-1.1	98	100	96	98	0.1	0.0	0.2	0.1	2	10 ≡	2	S 1	S 1	S 2
4	100.5	101.6	101.4	101.2	1.2	2.3	2.5	2.1	2.7	-0.9	92	91	88	90	0.5	0.6	0.9	0.7	10	9	10	SSW 2	S 2	S 2
5	100.0	97.2	96.9	98.0	2.9	5.2	8.9	6.5	9.1	1.9	100	100	99	100	0.0	0.0	0.2	0.1	10	10	10 ●	S 3	SSW 5	SW 4
6	92.2	91.5	95.7	93.1	9.6	9.5	4.4	7.0	11.0	4.4	91	95	84	90	1.2	0.7	1.4	1.1	10 ●	10 ●	0	WSW 9	W 8	W 5
7	101.7	106.0	109.3	105.7	4.1	5.7	4.4	4.6	5.8	2.2	88	85	84	86	1.0	1.5	1.4	1.3	9 ●	6	9	WNW 8	WNW 7	WNW 6
8	108.2	107.8	106.2	107.4	3.2	4.7	5.8	4.9	6.5	2.5	88	85	97	90	0.9	1.2	0.3	0.8	10	10	10 ●	WNW 8	WSW 5	WSW 4
9	103.0	100.8	97.7	100.5	6.1	7.2	6.3	6.5	7.3	4.9	89	84	85	86	1.0	1.7	1.4	1.4	9	10	10	SW 3	SW 3	WSW 4
10	94.5	93.8	94.6	94.3	3.9	3.3	2.7	3.2	7.6	2.6	92	95	86	91	0.7	0.4	1.0	0.7	10	10	9	W 3	WNW 3	W 3
11	96.8	100.0	102.4	99.7	0.8	1.6	-1.0	0.1	3.0	-1.2	92	83	95	90	0.5	1.2	0.3	0.7	9	8	2	W 3	WNW 3	W 3
12	96.0	88.6	81.7	88.8	0.3	0.5	0.3	0.4	1.2	-2.4	96	98	98	97	0.2	0.1	0.1	0.1	10 ✳	10 ✳	10 ✳	WSW 2	WSW 7	WSW 4
13	81.9	84.1	88.4	84.8	1.0	1.5	0.3	0.8	1.7	0.1	98	96	98	97	0.2	0.3	0.1	0.2	10	10	9	W 1	WSW 1	C 0
14	95.8	100.5	104.5	100.3	-3.8	-5.1	-6.4	-5.4	0.9	-6.6	96	98	91	95	0.2	0.1	0.3	0.2	10 ✳	10 ✳	10 △	NE 3	NE 2	NE 3
15	105.3	105.3	106.3	105.6	-7.5	-7.3	-8.4	-7.9	-6.0	-8.5	84	93	95	91	0.5	0.2	0.2	0.3	10	10 ✳	10 ✳	NE 3	NE 4	NNE 2
16	109.5	110.8	111.9	110.7	-14.2	-7.2	-10.4	-10.6	-6.5	-15.4	96	85	90	90	0.1	0.5	0.3	0.3	0	0	0	NNE 1	N 1	C 0
17	111.8	112.2	111.9	112.0	-10.1	-4.8	-5.5	-6.5	-4.2	-11.4	91	86	97	91	0.3	0.6	0.1	0.3	2	9	10 ≡	C 0	W 2	NW 2
18	110.6	110.5	108.7	109.9	-5.9	-5.1	-5.6	-5.6	-4.6	-6.5	97	98	95	97	0.1	0.1	0.2	0.1	10 ≡	10 ≡	10 ≡	W 2	W 2	W 2
19	108.4	109.1	110.2	109.2	-3.2	-1.5	-1.2	-1.8	-1.0	-6.0	97	99	99	98	0.1	0.1	0.1	0.1	10 ≡	10 ≡	10	W 1	WSW 1	W 1
20	109.3	108.2	105.3	107.7	-1.7	-1.8	-4.1	-2.9	-0.5	-4.4	98	94	94	95	0.1	0.3	0.3	0.2	10	10	0	W 1	WSW 3	WSW 2
21	102.2	102.7	103.5	102.8	-5.3	0.4	-3.0	-3.7	1.3	-6.0	80	50	73	68	0.8	3.2	1.1	1.7	2	0	0	SW 6	SW 3	SW 5
22	102.2	100.2	98.0	100.1	-6.8	0.7	-6.0	-4.5	1.1	-7.5	77	60	79	72	0.8	2.6	0.8	1.4	4	1	0	S 3	SSW 3	S 6
23	98.4	97.3	94.3	96.7	-7.9	2.7	-2.3	-2.4	2.9	-8.5	87	52	64	68	0.4	3.6	1.9	2.0	0	0	0	S 3	S 1	ESE 3
24	89.6	88.4	87.9	88.6	-3.0	-1.0	-1.4	-1.7	-0.5	-4.0	70	71	82	74	1.5	1.7	1.0	1.4	10	10	10	SE 4	SE 1	SE 1
25	87.4	89.1	93.2	89.9	-0.7	1.2	1.1	0.7	1.8	-2.9	87	85	89	87	0.7	1.1	0.7	0.8	10	9 ✳	10	SSE 2	SW 2	SW 1
26	97.4	97.8	94.5	96.6	-2.1	3.7	2.8	1.8	4.5	-2.4	98	67	70	78	0.1	2.7	2.2	1.7	0	0	10	SW 1	SSW 3	SW 4
27	93.4	96.1	99.5	96.3	4.0	6.2	1.7	3.4	6.5	1.5	98	78	83	86	0.1	2.2	1.1	1.1	10	9	0	WSW 5	WSW 5	WSW 3
28	99.3	104.5	110.3	104.7	0.7	1.0	0.7	0.8	2.3	-0.2	96	98	96	97	0.2	0.2	0.2	0.2	9	9	0	W 5	WNW 5	WNW 2
29	109.7	108.5	106.5	108.2	-1.4	2.1	0.8	0.6	3.0	-2.4	93	91	90	91	0.3	0.6	0.7	0.5	3	8	0	SSW 2	S 3	S 2
30	102.8	101.3	101.1	101.7	0.4	4.6	2.5	2.5	5.1	-0.2	75	57	100	77	1.7	3.6	0.0	1.8	7	10	10 ●	S 2	SW 1	WSW 2
31	101.0	101.4	98.9	100.4	2.4	3.3	2.0	2.4	3.9	1.7	100	97	98	98	0.0	0.2	0.2	0.1	10 ≡	10	10 ●	WSW 2	SW 2	SSW 2
M	99.8	100.0	100.3	100.0	-1.3	0.9	-0.4	-0.3	2.1	-3.0	92	86	90	89	0.5	1.0	0.6	0.7	7.6	8.0	6.5	2.9	3.0	2.7

Luty – Février

1	94.5	94.7	96.0	95.1	3.5	5.9	7.4	6.0	7.6	1.7	97	98	100	98	0.2	0.2	0.0	0.1	10 ●	10 ●	10 ●	S 3	S 3	SSW 3
2	100.0	103.3	104.9	102.7	10.3	8.4	7.3	8.3	10.5	6.9	87	96	99	94	1.6	0.4	0.1	0.7	10	10	10 ≡●	WSW 2	W 1	C 0
3	103.2	104.3	104.7	104.1	5.4	4.5	3.3	4.1	7.5	3.2	100	100	98	99	0.0	0.0	0.1	0.0	10	10 ●	10	SSW 1	NE 3	E 3
4	102.0	101.8	101.7	101.8	3.1	7.2	3.7	4.4	9.7	2.1	100	93	95	96	0.0	0.8	0.4	0.4	10 ≡	9	0	ESE 2	S 2	SW 1
5	101.0	99.5	97.6	99.4	1.8	11.1	3.4	4.9	12.6	1.2	96	69	88	84	0.3	4.0	0.9	1.7	1	8	4	SSW 2	S 2	S 3
6	93.6	91.5	92.4	92.5	1.5	8.8	4.6	4.9	9.2	0.7	92	67	95	84	0.5	3.7	0.6	1.6	4	3	7	S 3	SSW 3	SSW 3
7	96.1	97.0	96.8	96.6	5.3	8.0	4.8	5.7	9.0	4.5	95	66	81	81	0.4	3.7	1.7	1.9	8	6	3	W 3	W 6	WSW 3
8	90.7	86.8	82.6	86.6	3.9	5.8	6.2	5.3	7.3	1.7	88	94	94	92	1.0	0.6	0.6	0.7	10	10 ●	10 ●	SSW 3	S 4	SW 7
9	81.5	81.7	85.8	83.0	5.9	7.0	4.6	5.5	7.8	4.2	94	96	79	90	0.6	0.4	1.8	0.9	6	10	0	SW 3	WSW 5	W 3
10	86.3	86.2	85.8	86.2	2.4	3.9	3.1	4.1	6.3	2.1	93	98	94	96	0.4	0.2	0.6	0.4	2	10 ●	10 ●	WSW 1	SW 1	WSW 2
11	88.1	92.3	93.8	91.4	3.8	3.9	2.0	2.9	5.3	1.7	97	85	93	92	0.3	1.2	0.6	0.7	10	8	2	WNW 5	W 2	WSW 2
12	89.4	85.9	83.2	86.2	1.3	6.8	4.3	4.2	7.8	-0.3	94	60	85	80	0.4	4.0	1.2	1.9	10	8	10	SSW 2	SSW 4	SSW 3
13	79.4	74.5	65.4	73.1	2.5	7.2	5.9	5.4	8.8	1.6	88	66	92	82	0.9	3.5	0.7	1.7	8	8	10 ●	S 3	SW 7	S 7
14	65.0	65.0	67.2	65.7	5.2	9.0	3.3	5.2	9.1	2.4	89	68	85	81	0.9	3.7	1.2	1.9	8	7	9	SSW 2	SSW 4	SSW 4
15	67.4	64.6	62.9	65.0	1.4	4.5	4.3	3.6	5.0	1.2	96	79	98	91	0.3	1.8	0.1	0.7	6	10	10 ●	SSW 3	S 2	S 2
16	71.7	74.4	79.9	75.3	2.1	2.3	0.9	1.6	4.5	0.7	95	96	98	96	0.4	0.3	0.1	0.3	7	10 ●	1	WSW 3	WSW 2	SSW 2
17	83.9	83.8	85.0	84.2	0.0	4.1	2.0	2.0	5.0	-1.0	94	75	93	87	0.4	2.0	0.6	1.0	2	10	10	SW 1	S 2	S 2
18	84.2	79.6	76.8	80.2	-1.1	4.6	2.9	2.3	5.5	-2.0	89	81	98	89	0.6	1.7	0.1	0.8	6	8	10 ●	S 2	E 3	E 1
19	84.0	88.6	91.1	87.9	0.3	2.2	1.3	1.3	3.2	-0.4	98	91	91	93	0.1	0.7	0.6	0.5	4	10	9	WNW 3	WSW 4	WSW 2
20	89.7	88.6	85.3	87.9	0.1	7.9	3.7	3.8	8.2	-0.4	98	54	72	75	0.2	4.9	2.3	2.5	9 ✳	10	0	SSW 2	S 3	SSW 1
21	86.0	89.1	94.8	90.0	2.6	5.0	1.0	2.4	6.3	0.9	86	78	94	86	1.1	1.9	0.4	1.1	8	10	9	SSW 2	SW 3	WNW 3
22	96.7	95.8	93.4	95.3	-0.7	3.7	0.2	0.8	5.1	-1.4	100	73	76	83	0.0	2.2	1.3	1.2	10	5	0	W 1	W 1	SW 1
23	94.1	94.3	92.4	93.6	-0.8	1.7	-2.1	-0.8	2.9	-2.9	93	70	83	82	0.4	2.0	0.9	1.1	10	8	0	SW 1	WNW 2	C 0
24	83.5	80.5	83.2	82.4	-2.4	2.1	-1.4	-0.8	2.9	-3.3	93	77	92	87	0.3	1.7	0.4	0.8	8	10	0	SE 4	SE 2	SE 1
25	87.0	85.9	86.1	86.3	-3.4	-0.3	-1.6	-1.7	0.7	-4.0	99	76	86	87	0.0	1.5	0.7	0.7	10 ≡	9	10	SE 1	ESE 3	E 2
26	94.2	96.5	98.5	96.4	-3.5	0.6	-2.0	-1.7	3.0	-4.3	90	88	87	88	0.5	0.8	0.7	0.7	8	1 ⊙	0	C 0	ENE 1	E 2
27	99.7	101.7	104.5	102.0	-2.9	2.4	0.3	0.0	3.1	-3.3	86	68	100	85	0.7	2.4	0.0	1.0	10	8	10 ✳	ESE 3	ESE 3	C 0
28	108.5	111.4	113.8	111.6	-0.4	-0.6	-2.4	-1.4	0.7	-2.4	100	99	98	98	0.0	0.3	0.1	0.1	10✳≡	10✳≡	0	ENE 1	E 1	ENE 1
29																								
30																								
31																								
M	89.3	89.3	89.5	89.4	1.7	4.9	2.6	3.0	6.2	0.4	94	81	91	89	0.4	1.8	0.7	1.0	7.7	8.5	5.9	2.4	2.9	2.4

Zielona Góra

$H_s = 176\ m$ $H_b = 174{,}0\ m$ $h_w = 9\ m$

Styczeń – Janvier 1957

DNI	WIATR DZIAŁ.	WIATR NOŚĆ v	OPAD R	GRUB. ŚNIEGU h	USŁO. NECZ. NIENIE	POGODA
1	2	.	12	–		= 0⁰⁰–9⁴⁰ ≡¹–10²⁰ =–11³⁰ ≡¹–13²⁰ =–15¹⁵ ≡⁰–17²⁵ =–24. ⌴⁰ 0⁰⁰–9⁴⁰. ▼⁰ 9⁴⁵–24
2	6	.	12	–		= 0⁰⁰–24. ▼⁰ 0⁰⁰–11³⁵
3	3	1.2	11	–		✶⁰ 8⁵⁰–10⁰⁰ ✶¹–11⁰¹ ✶⁰–11⁵⁹ = 0⁰⁰–11¹⁵ ≡⁰–13²⁰ =–24
4	6	0.2	11	–		●⁰ 21²⁰–22⁵⁰ ●⁰–24 = 0⁰⁰–24
5	4	6.0	7	–		●⁰ 0⁰⁰–2⁵⁰ ●⁰ 8⁰³–9¹⁴ ●⁰⁻² 9⁵³–11¹⁸ ●●⁰–12¹⁴ ●⁰–12⁵⁰ ●⁰–16²⁰ ●⁰⁻¹ 16⁴²–24. = 0⁰⁰–2⁰⁵ ≡⁰⁻² 7¹⁰ =–24
6	6	6.6	.	–		●⁰ 0⁰⁰–1⁵ 6⁵⁰–7²⁰ ●⁰–11⁴² ●¹–12⁰⁰ ●⁰–15⁰⁰ = 0⁰⁰–15¹⁰
7	7	0.7	.	–		●⁰ 1⁰³–0⁹ 1²⁰–2⁹ 4⁴⁸–5⁰⁵ ▽ 5⁰⁹–18 ●⁰ 6¹⁰–7³⁰ ▽ 7³³–39. 8⁰⁵–20
8	6	0.1	.	–		●⁰ 18¹⁵–24. = 9⁰⁵–24
9	7	.	.	–		●⁰ 0⁰⁰–3⁰⁵ = 0⁰⁰–8²⁰ 14³⁰–24
10	6	1.1	.	–		●⁰ 7⁵⁵–12⁰⁵. = 0⁰⁰–13³⁰
11	7	0.5	.	–		
12	5	2.6	pł.	–		✶⁰⁻¹ 5²⁵–8²⁴ ✶⁰ 10³⁸–11⁵⁰ ✶●⁰ 12⁰⁰–23 ✶⁰⁻¹ 13²⁷ ✶⁰ 15⁵⁰–21¹⁰. 22³⁴–23⁰² ✱⁰–23²¹. = 5⁵⁰–24
13	5	1.7	11	–		●⁰ 6¹⁸–34 △ 9¹⁰–11²⁰ ✶⁰ 11³⁵–12¹⁰ = 0⁰⁰–23⁴⁰ ≡⁰–24
14	6	0.5	2	–		✶⁰ 0⁵⁰–16⁰⁰. 18⁴²–20²⁰ △ 20⁴⁰–22⁰⁵. = ⁰ 0⁰⁰–30 =–24
15	6	1.1	3	–		✶⁰ 8⁴⁰–24. = 0⁰⁰–5³⁰
16	6	.	4	–		✶⁰ 0⁰⁰–1⁰⁰ = 9¹⁵–24
17	7	.	4	–		= 0⁰⁰–5¹⁵ 7³⁰–8¹⁵ 16⁴⁰–19⁴⁰ ≡⁰–21¹⁵ ≡¹–24. ▼⁰ 21¹⁵–24
18	2	.	3	–		≡¹ 0⁰⁰–24. ▼⁰ 0⁰⁰–3³⁰ ▼⁷–24
19	3	.	3	–		≡¹ 0⁰⁰–3³⁰ ≡⁰–16⁴⁵ =–24. ▼¹ 0⁰⁰–3³⁰ ▼⁰–16⁴⁵
20	5	.	3	–		= 0⁰⁰–24
21	7	.	3	–		= 0⁰⁰–8³⁰. ⌓ 23¹⁰–24
22	6	.	2	–		= 7⁰⁰–13⁰⁰. 15¹⁵–24
23	7	.	2	–		= 0⁰⁰–12¹⁵
24	3	0.0	2	–		✶⁰ 17¹⁰–18²⁰. = 4⁴⁵–24
25	6	0.0	2	–		✶⁰ 0¹⁰–1⁴⁵. 9¹⁰–11²⁵ 13¹⁰. = 0⁰⁰–24
26	6	1.1	2	–		= 0⁰⁰–15⁰⁰. 16⁵⁰–24. ∞⁰ 15⁰⁰–16⁵⁰
27	7	1.6	.	–		●⁰ 0⁴⁵–4¹⁵ = 0⁰⁰–8²⁰ ⌴⁰ 22⁰⁰–24
28	7	0.3	.	–		▽ 2⁵⁷–59 ✱⁰ 3⁰⁰–55 ✶⁰–5⁰³. 5³⁰ 6⁴⁰ 10³⁵–42 ●⁰–11¹⁵ ✱–12⁴⁰. = 0⁵⁰–6⁴⁰. ⌴⁰ 0⁰⁰–2⁵⁹
29	6	0.0	.	–		●⁰ 14⁵⁸ 15³⁶ = 0³⁰–24. ⌴⁰ 0²⁰–11⁰⁰
30	6	2.0	.	–		●⁰ 14³⁵–39 14⁵⁸–59 15²⁷–16⁰³ 16²³–20³⁰ ●⁰–24. = 0⁰⁰–11⁰⁰ 14³⁵–21⁴⁵ ≡⁰–24. ⌴⁰ 3³⁰–9³⁰. ∞⁰ 11⁰⁰–14³⁵
31	6	1.7	.	–		●¹ 3⁰⁵–5¹⁰ ●⁰–6⁰⁰ ●⁰ 8⁴⁵–9³⁵. 15³³–22⁵⁰. ≡⁰ 0⁰⁰–13⁰ ≡¹–8⁵⁰ =–24
Σ	–	29.0	–	–		UWAGI

Luty – Février

1	5	1.7	.	–		●⁰ 0⁰⁰ 1¹³ 6²³ 14³⁰ ●●⁰–19⁰⁰ ●⁰–21³⁵. = 0⁰⁰–14³⁰ ≡⁰–17⁴⁵ ≡¹–18²⁰ ≡⁰–20³⁰ =–24
2	6	4.9	.	–		●⁰ 10⁴³–11²⁰ 15⁴⁰ 16⁰⁵ 18³⁵–24. = 0⁰⁰–7³⁰. 10⁴⁰–18⁴⁵ ≡¹–19³⁰ ≡⁰–24
3	4	0.8	.	–		●⁰ 0⁰⁰–6⁴⁵ 7³⁰–8³⁵ 9³⁰–11⁰⁰ ●⁰⁻¹ 11¹⁰–14²⁰. ≡⁰ 0⁰⁰–15⁰ =–7⁵⁰ ≡¹⁻⁰–9²⁰ =–10⁵⁰ ≡¹⁻²–12⁴⁰ =–15⁰⁵
4	6	0.0	.	–		●⁰ 9³⁵–40 = 0¹⁰–30 ≡⁰–0⁴⁵ ≡¹–5³⁰ ≡²–9²⁰ ≡⁰–10⁴⁰ =–24
5	7	.	.	–		= 0⁰⁰–12²⁰. ⌓¹ 15⁰–10⁴⁰
6	7	1.3	.	–		●⁰ 17²⁰–20²⁵. = 2⁵⁰–9⁰⁰. 16⁴⁰–24
7	7	.	.	–		●⁰ 1¹⁰–4²⁰. = 0⁰⁰–12³⁰
8	6	5.2	.	–		●⁰ 9¹⁵–14⁴⁵. 16¹⁰ 17⁰⁵. 18¹⁵–24. = 5¹⁰–24
9	6	1.9	.	–		●⁰ 0⁰⁰–2²⁰ 10⁰⁰–12⁴⁰ 14¹⁵–52. = 0⁰⁰–7⁰⁰. 10²⁰–19³⁰
10	5	3.0	.	–		●⁰ 11³⁵–13²⁰. 20²⁰–23⁵⁹. = 8²⁰–24
11	7	1.0	.	–		●⁰ 5⁰⁵–6¹³ ●⁰ 7¹⁰ 8¹⁵ ●⁰–9²⁵ ▽ 15²²–27. = 0⁰⁰–9⁴⁰ ▽ 21⁵⁰–24
12	7	1.1	.	–		●⁰ 8¹⁵ 9¹⁸ 17⁴⁰–20⁰⁵. = 0³⁰–12⁰⁸. ▽ 0⁰⁰–2⁵⁰. 21²⁵–24
13	8	2.8	.	–		●⁰ 18¹⁵–21³⁵. ⊕ 11³⁰–13¹⁵
14	8	2.3	.	–		●⁰ 0¹⁰ 10⁵–21³. ▽ 14³³–35. 15⁴⁷–17⁰²
15	7	1.8	.	–		●⁰ 0³⁰–1²⁰ 13⁰⁰–16¹³. 17⁴⁸ 18¹⁰ 19¹⁵ 24. = 15²⁵–24
16	5	1.8	.	–		●⁰ 0⁰⁰ 2¹⁰. 9²⁵ 11⁰⁵–15²⁰. = 0⁰⁰–24
17	7	1.4	.	–		●⁰ 13⁵⁶–16¹⁰. = 0⁰⁰–12¹⁰. ⌴⁰ 13⁰–10⁰⁰
18	7	4.4	.	–		●⁰ 17³⁰–24. = 15¹⁰–22¹⁰ ≡⁰–24 ⌴⁰ 15⁰–8⁰⁰. ▽ 4⁴⁵–6³⁰
19	5	1.1	.	–		●⁰ 0⁰⁰–3¹⁵ ✱⁰ 20³²–49. ≡⁰ 0⁰⁰–50 =–3³⁰. 6²⁰–24
20	8	0.0	1	–		✶⁰ 4⁰⁰–7⁰⁵. = 0⁰⁰–7³⁰. ⊕ 10³⁰–14¹⁵
21	7	0.4	.	–		●⁰ 17³⁵–20²⁰. = 13²⁰–14²⁵. ⊕ 8²⁵–10⁰⁵
22	6	0.1	0	–		✱ 2⁵⁰–3⁰⁵. = 2³⁰–24
23	6	0.0	.	–		✶⁰ 5²⁶ 6⁰⁰ ✱⁰ 6¹⁰–50 ✶⁰ 7²⁰–8¹⁰ ✱ 16⁰⁵–15. = 5¹⁰–24
24	6	.	.	–		= 0⁰⁰–24. ⊕ 8³⁵–13²⁵ (9⁴⁰–12²⁵ halo złożone)
25	6	.	.	–		= 0⁰⁰–3⁴⁵ ≡⁰–9⁰⁰ =–24. ⌴¹ 2⁵⁰–11⁰⁰
26	6	.	.	–		= 0⁰⁰–14¹⁵. ⌴⁰ 19⁴⁵–24
27	7	6.6	.	–		✶⁰ 17¹⁶–35 ✶¹–18¹⁰ ✶⁰–24. = 6²⁵–11²⁰ 15⁴⁰–23⁵⁵ ≡⁰–24. ⌴⁰ 0⁰⁰–9³⁰
28	2	1.1	6	–		✶⁰⁻¹ 0⁰⁰–8¹⁰ ●⁰ 10³⁰–11⁰⁵ ✶●⁰–12¹⁰ ✶¹–13¹³ ✶⁰ 13⁴⁵. 14⁴⁰ 19³⁰. ≡⁰ 0⁰⁰–30 ≡¹–6¹⁵ ≡⁰–13¹³ =–24
29						
30						
31						
Σ	–	45.7	–	–		UWAGI

Zielona Góra — φ = 51°56' — λ = 15°30' — Marzec – Mars 1957

DNI	CIŚNIENIE P=900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	116.4	116.3	115.2	116.0	-3.0	0.2	-3.6	-2.5	1.4	-4.0	97	73	87	86	0.1	1.7	0.6	0.8	10	5	0	ENE 1	ENE 1	C 0
2	113.2	111.9	108.4	111.2	-5.0	1.2	-1.3	-1.6	2.7	-5.4	95	63	76	78	0.2	2.5	1.4	1.4	1	4 ⊙	0	C 0	N 1	N 1
3	104.4	102.6	99.1	102.0	-4.0	3.1	0.0	-0.2	5.0	-4.5	87	54	72	71	0.6	3.5	1.7	1.9	6	5	0	NNE 1	NNE 2	C 0
4	95.9	91.2	90.8	92.0	-1.9	6.9	4.0	3.2	7.6	-3.1	67	53	79	66	1.7	4.6	1.7	2.7	7	8	10	NNE 1	WSW 1	W 3
5	93.5	94.0	94.2	93.9	-1.6	4.4	0.9	1.2	6.5	-2.0	96	52	75	74	0.2	4.0	1.6	1.9	6	4	0	NW 1	NW 1	NW 1
6	93.5	92.1	90.8	92.1	-0.6	6.7	1.7	2.4	7.9	-1.5	71	45	63	60	1.6	5.4	2.5	3.2	0	1 ⊙	0	C 0	SE 3	ESE 3
7	90.0	90.7	91.2	90.6	-1.9	6.8	0.0	1.2	7.5	-2.0	78	42	78	66	1.2	5.7	1.3	2.7	6	6	7	ESE 3	ESE 3	ESE 6
8	92.5	94.2	97.3	94.7	-2.4	1.5	-0.8	-0.6	3.6	-3.2	82	76	75	78	0.9	1.6	1.5	1.3	10 ●	8	0	SE 3	ESE 3	ESE 3
9	102.0	104.7	108.0	104.9	-4.4	3.2	-0.6	-0.6	4.5	-4.7	61	51	64	65	0.8	3.8	2.1	2.2	0	0	0	ESE 4	E 3	ESE 3
10	109.9	110.7	110.3	110.3	-4.2	6.3	0.4	0.7	7.0	-4.6	84	48	67	66	0.7	4.9	2.1	2.6	0	0	0	ESE 3	ENE 3	ENE 3
11	110.9	109.9	107.9	109.6	-3.4	10.6	4.2	3.9	12.7	-4.0	88	30	53	57	0.6	9.0	3.8	4.5	0	0 ⊙	0	SE 3	SE 3	SE 1
12	104.6	101.7	99.3	101.9	2.2	14.5	9.0	8.7	16.0	0.5	63	24	41	43	2.7	12.6	6.8	7.4	8	1	1	SE 1	S 1	SW 1
13	99.1	98.9	95.9	98.0	4.5	14.9	11.3	10.5	16.7	4.3	60	31	58	50	3.3	11.7	5.6	6.9	5	4	0	SW 1	W 2	WSW 1
14	91.9	91.5	91.4	91.6	8.7	11.9	9.5	9.9	12.6	7.8	67	69	63	66	3.7	4.3	4.5	4.2	0	8	10	SW 5	W 9	W 10
15	92.3	90.7	85.4	89.5	7.4	8.8	9.4	8.8	9.7	7.1	80	80	88	83	2.1	2.3	1.4	1.9	10	10	10 ●	W 7	WSW 7	W 8
16	86.2	91.1	95.5	90.9	0.3	2.2	-1.2	0.0	9.6	-1.7	100	82	72	85	0.0	1.3	1.6	1.0	10 ✳	10	10	NW 3	WNW 2	NW 2
17	92.0	87.9	80.8	86.9	-3.6	-1.1	7.7	2.7	7.9	-4.0	92	99	100	97	0.4	0.1	0.0	0.2	10 ✳	10 ●	10 ●	SE 3	SE 4	SW 3
18	75.7	77.7	83.0	78.8	9.3	8.7	6.1	7.6	10.4	5.9	95	88	92	92	0.6	1.3	0.7	0.9	10	10 ●	0	W 7	WNW 5	W 6
19	87.7	88.0	87.2	87.6	5.2	9.1	7.1	7.1	9.9	4.0	97	75	99	90	0.2	3.0	0.2	1.1	10 ●	10	10 ●	WNW 2	W 1	S 1
20	89.2	86.8	84.1	86.7	8.9	12.8	9.9	10.4	13.4	6.9	99	79	76	85	0.2	3.1	3.0	2.1	10	9	0	SW 1	SW 2	SSW 2
21	89.8	91.4	92.2	91.1	6.8	11.9	8.1	8.7	12.8	6.5	87	55	64	69	1.3	6.3	3.8	3.8	0	1	1	WSW 2	SW 3	SSW 1
22	95.2	96.6	98.1	96.6	4.3	11.1	5.1	6.4	11.8	3.9	85	49	67	67	1.2	6.7	2.9	3.6	2	4	0	WSW 2	W 3	C 0
23	97.3	96.7	97.6	97.2	4.5	11.2	7.2	7.5	12.1	3.6	66	52	58	59	2.8	6.3	4.3	4.5	1	8	10	ENE 3	ESE 5	ENE 6
24	99.7	99.1	99.8	99.5	0.9	1.8	2.5	1.9	7.4	0.7	94	83	84	87	0.4	1.2	1.2	0.9	10	10	10	ENE10	E 9	ESE 9
25	99.4	99.3	99.8	99.5	2.2	9.9	6.8	6.4	12.1	2.0	91	64	88	81	0.7	4.3	1.2	2.1	10	3	10	ESE 4	SE 3	ESE 2
26	98.7	97.2	97.3	97.8	4.7	15.5	9.6	9.8	16.7	3.7	97	47	51	65	0.2	9.4	5.9	5.2	3	3	1	SE 2	SE 4	SSE 2
27	98.5	99.6	98.0	98.7	5.4	14.7	9.3	9.7	15.3	3.9	60	43	57	53	3.6	9.4	5.0	6.0	1	1	0	SSE 5	S 5	S 2
28	94.9	94.9	93.7	94.5	7.5	5.3	6.5	6.4	9.5	4.4	61	98	84	81	4.1	0.1	1.6	1.9	10 ●	10 ●	10 ●	S 5	S 5	S 2
29	93.2	94.0	95.3	94.2	4.7	5.7	5.0	5.1	6.7	4.1	100	97	93	97	0.0	0.3	0.4	0.2	10●	10 ●	10	SW 1	WSW 1	W 1
30	96.9	98.0	99.3	98.1	3.6	9.3	6.8	6.6	11.4	3.2	100	88	93	94	0.0	1.4	0.8	0.7	10	8	0	NW 1	NW 1	C 0
31	99.1	100.7	102.5	100.8	3.3	10.9	7.1	7.1	12.4	2.9	100	71	76	82	0.0	3.7	2.5	2.1	1	6	0	N 2	E 1	SSE 1
M	96.8	96.8	96.4	96.7	1.9	7.7	4.8	4.8	9.7	1.0	84	63	74	74	1.2	4.4	2.4	2.7	5.7	5.8	3.9	2.9	3.2	2.8

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1	101.0	99.7	98.3	99.7	5.1	15.9	11.6	11.0	16.4	3.9	90	49	63	67	0.9	9.2	5.0	5.0	2	2	0	ESE 1	ENE 3	SE 1
2	97.4	97.1	99.7	98.1	6.6	15.1	8.9	9.9	15.7	5.1	79	56	96	77	2.0	7.5	0.5	3.3	3	8	10	E 2	SE 2	SE 1
3	102.5	103.0	106.6	104.7	9.3	15.9	13.9	13.2	16.5	8.3	91	64	64	73	1.1	6.5	3.7	4.4	10 ●	5	8	ESE 1	ESE 1	SE 1
4	108.5	109.0	108.5	108.7	8.7	20.1	14.7	14.6	20.8	6.2	84	40	53	59	1.8	14.0	7.8	7.9	0	0	0	C 0	E 2	E 1
5	107.0	104.5	99.0	103.5	11.7	19.4	12.4	14.0	20.2	9.4	68	39	58	55	4.4	13.7	6.1	8.1	0	0	0	C 0	ESE 2	E 1
6	95.0	89.8	91.0	91.3	8.9	19.7	7.4	10.8	20.5	7.1	71	37	88	65	3.3	14.3	1.2	6.3	3	3	10	SSE 1	SW 1	NW 3
7	91.4	91.8	98.0	93.7	4.1	7.9	3.3	4.6	9.2	2.6	95	71	91	86	0.4	3.1	0.6	1.4	10	8	9	NW 3	N 4	NNE 2
8	101.4	99.8	97.6	99.6	-1.9	5.5	3.1	2.4	8.0	-3.7	89	50	69	69	0.6	4.3	2.3	2.3	2	0	1	NNE 2	N 2	NNW 1
9	94.6	92.2	91.5	92.8	2.4	10.5	4.1	5.3	11.9	0.6	73	55	82	70	2.0	5.8	1.5	3.1	2	6	6	WNW 3	WNW 4	N 1
10	87.7	82.8	77.3	82.6	2.4	13.5	8.4	8.2	14.6	0.1	96	49	66	70	0.3	7.9	3.7	4.0	0	2	0	N 1	SSW 2	WSW 1
11	76.2	77.4	83.2	78.9	3.1	5.5	0.9	2.6	8.5	0.7	78	65	90	78	0.7	3.1	0.6	1.8	1	8	6	WNW 4	NW 4	NW 1
12	88.5	89.7	91.8	90.0	-0.2	3.4	0.0	0.8	6.8	-2.0	92	76	72	80	0.5	1.9	1.7	1.4	1	9	0	NW 1	NW 2	NW 1
13	92.4	94.4	96.9	94.6	-0.8	3.5	0.6	1.0	5.5	-2.8	100	66	75	80	0.0	2.6	1.6	1.4	10 ✳	6	8	N 1	WNW 5	C 0
14	98.7	98.4	98.6	98.6	-1.0	5.5	1.8	2.0	7.8	-4.0	93	44	78	72	0.4	3.0	1.6	2.3	0	5	1	C 0	W 2	WNW 1
15	100.6	101.7	102.7	101.7	0.0	6.4	3.4	3.3	8.1	-1.0	86	48	63	66	0.9	5.0	2.9	2.9	2	5	7	WNW 1	NW 3	WNW 1
16	102.3	100.6	100.2	101.0	2.6	12.1	10.5	8.9	12.9	1.5	86	56	57	66	1.1	6.2	3.5	4.3	10	7	10	WSW 2	W 5	W 3
17	100.6	100.8	101.7	101.0	6.4	11.4	5.8	6.4	11.7	3.6	95	55	90	80	0.4	6.1	0.8	2.4	10	7	0	WNW 1	NW 2	NNW 1
18	100.3	99.1	97.3	98.9	3.4	7.3	3.1	4.2	9.6	2.0	95	62	81	79	0.4	3.9	1.4	1.9	10	4	0	NNE 1	N 2	NNE 1
19	93.3	91.6	93.1	92.7	2.0	5.6	7.2	5.6	7.7	0.4	85	94	99	93	1.1	0.6	0.2	0.6	10	10 ●	10 ●	E 2	ESE 2	C 0
20	100.1	102.3	104.3	102.3	3.3	9.3	5.0	5.7	11.3	2.2	97	53	69	73	0.2	3.6	2.7	2.8	4	4	0	WNW 3	NW 2	NW 1
21	106.6	107.4	108.7	107.6	3.4	10.9	5.5	6.3	12.1	1.7	93	51	77	74	0.5	5.4	2.1	3.0	6	6	9	NNW 1	NNW 2	N 2
22	110.1	110.0	109.5	109.9	2.8	10.7	5.1	6.4	12.3	1.0	96	55	76	76	0.3	5.8	2.2	2.8	8	4	0	C 0	N 1	E 3
23	109.9	108.8	108.6	109.1	5.1	12.8	9.5	9.2	14.8	1.9	90	49	75	71	0.9	7.6	3.0	3.8	0	2	0	E 1	N 1	NE 1
24	108.3	108.0	106.7	107.7	5.5	13.4	10.9	10.7	16.8	3.6	89	43	65	66	1.0	9.7	4.6	5.1	0	8	10	ENE 1	N 3	NNE 1
25	104.3	103.3	102.3	103.3	5.9	6.3	6.5	6.3	11.3	5.1	98	98	97	98	0.2	0.1	0.3	0.2	10 ●	10	10	C 0	N 3	NNW 1
26	101.9	101.7	100.3	101.3	6.1	10.1	10.9	9.5	14.7	5.6	100	88	90	93	0.0	1.5	1.3	0.9	10	10	8	NNW 1	N 1	NNW 1
27	98.2	96.3	93.1	95.9	10.6	16.7	14.9	14.3	19.5	8.5	91	74	75	80	1.2	5.0	4.1	3.4	2	9	2	NNW 1	ENE 2	ENE 1
28	90.7	88.8	88.2	89.2	13.3	22.7	17.6	17.8	23.7	10.9	85	43	55	61	2.3	15.7	9.0	9.0	1	4	0	ESE 2	SE 3	C 0
29	90.8	91.5	91.3	91.2	12.8	20.3	16.1	16.3	22.9	11.5	87	53	70	70	1.9	11.2	5.4	6.2	0	2	0	WSW 3	SSW 2	W 1
30	89.3	88.8	94.2	90.8	11.9	16.7	8.7	11.5	18.0	8.4	97	67	74	79	0.3	6.2	2.8	3.1	6	9	1	NNE 1	NNW 4	NW 1
31																								
M	98.3	97.8	98.0	98.0	5.1	11.9	7.7	8.1	13.7	3.3	89	58	73	74	1.1	6.3	2.9	3.5	4.4	5.4	3.9	1.4	2.4	1.2

Zielona Góra — H_s = 176 m — H_b = 174,0 m — h_w = 9 m — Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	6	–	= 0⁰⁰–10⁴⁵ 19³⁰–24
2	7	.	2	–	= 0⁰⁰–11¹⁵
3	6	.	pż.	–	= 6³⁰–12¹⁵ ∞–17³⁰ ⊕ 9³⁰–13¹⁰
4	7	0.0	pż.	–	•⁰21⁴⁰–22³⁰ = 14³⁰–15²⁰ 17²⁰–24 ⊕ 9⁰⁷⁻⁵² 10³⁵–12¹⁵ 15⁴⁰–16¹⁰
5	7	.	pż.	–	= 0⁰⁰–9³⁰ ⌴ ⁰2³⁰–8⁵⁵ ⊕ 8²⁰–10¹⁰
6	8	.	pż.	–	
7	8	0.0	.	–	⌴ ⁰3⁵⁰–9⁰⁰ ⊕ 12²⁰–17⁴⁰ ⌓ 19⁰⁰–23⁰⁵
8	7	0.0	.	–	△⁰5⁵⁰–8¹⁰
9	7	.	.	–	⌴ ⁰1³⁰–9¹⁰
10	8	.	.	–	
11	6	.	.	–	= 4⁵⁵–9³⁰ ⌴ ⁰1⁵⁰–9⁰⁰ ∞ 9³⁰–18³⁰
12	7	.	.	–	
13	6	.	.	–	= 5³⁰–10⁰⁰ ∞–24 ⌒ 18¹⁵–19³⁵
14	6	0.0	.	–	▽13³⁹–⁴⁴ ∞ 0⁰⁰–12¹⁰ = 14⁴⁵ ⩓ 17³⁰–23²⁰ ⌒ 19⁴⁵–22¹² ⌓ 20²⁵–⁴⁵
15	7	10.6	.	–	•⁰11⁴⁵ 12¹⁰ 13²⁵ 14¹⁵ 15¹²–16³⁵ 22⁰⁰ 22¹⁰–24 = 11¹⁰–12²⁰ 13²⁵–24
16	7	0.2	.	–	•⁰0⁰⁰–1²⁰ •¹–2⁰⁸ •⁰–5¹⁰ *⁰5¹⁸–8¹¹ = 0⁰⁰–12⁵⁰
17	6	11.7	1	–	*⁰5⁴⁰–7⁰⁵ •⁰7⁴⁵–8⁴⁸ •⁰–9¹⁵ •⁰9³⁵–10⁴⁷ •⁰–13²² •⁰–15⁰⁰ •⁰⁻¹17⁰⁰ •⁰18²⁸–23⁰⁵ •⁰23¹⁵–24 = 5³⁰–13⁴⁵ ≡¹⁻² 19¹⁰ ≡⁰–20¹⁵
18	6	6.6	.	–	•⁰0⁰⁻¹⁸ 2⁵⁰–3⁰⁰ •¹3⁰⁹–4⁴⁵ •⁰5⁰²6⁴⁵ 7⁰¹⁻¹⁵ •¹12²²–13³⁵ •⁰–13⁴⁸ ▽15⁴⁰⁻⁵² 17⁰⁶⁻¹⁰ 18²⁰–10⁵³ = 0⁰⁰–5⁰⁵
19	7	4.6	.	–	▽4⁴²–6⁰⁴ 6¹³–7⁰⁰ 7⁵⁸–8⁰⁰ •⁰8¹⁰⁻⁵⁰ 13⁴⁰–16¹⁰ •¹–17¹⁰ •⁰–19²⁰ •⁰–21²⁵ •⁰22¹⁵–23¹⁰ •⁰–24 = 5²⁵–12¹⁰ 13²⁵–24
20	7	0.0	.	–	•⁰0⁰⁻³⁰ = 0⁰⁰⁻³⁰ ≡¹–2²⁵ =–7⁰⁰ ≡⁰⁻¹–8⁴⁵ =–11⁴³ [17.III: =–24 ∞ 10⁵⁰–15³⁰
21	7	.	.	–	•⁰3¹⁵–²⁹ ▽4¹¹–¹⁴
22	7	.	.	–	
23	7	.	.	–	= 23⁰⁰–24 ⊕ 11¹⁵–12³⁰
24	7	.	.	–	= 0⁰⁰–4⁰⁰ 6¹⁵–7²⁰
25	6	0.6	.	–	∞ 12⁰⁵–17⁵⁵ =–18³⁰ 20¹⁰–24 ⊕ 13⁵³–14⁴⁰
26	8	.	.	–	•⁰0¹⁰–²⁵ = 0⁰⁰–8³⁰
27	8	0.0	.	–	
28	6	11.3	.	–	•⁰6²⁰ 7⁰⁰–9⁰⁴ •¹⁻⁰9³⁰ •⁰10²⁰–³⁸ •¹⁻⁰11⁴³–12⁰⁵ •⁰ 13⁰⁰ 20¹⁰ 24 = 7³⁰–24
29	5	4.5	.	–	•⁰0⁰⁰ 2⁰⁰ 6⁵⁵–7¹² •¹–7²⁰ •⁰–9⁰³ 11²⁵–14⁰⁰ •⁰23¹²–24 = 0⁰⁰–3⁴⁰ ≡⁰–3⁵⁰ ≡⁰–9⁴⁵ =–24
30	6	0.2	.	–	•⁰0⁰⁻¹⁰ •⁰0⁵⁰–1²⁵ •⁰–2¹⁰ •¹⁻⁰3⁰⁰–10²⁰ = 0⁰⁰–3¹⁵ ≡⁰–4³⁰ ≡¹–10⁵⁰ =–16²⁵ ⌓⁰20³⁰–24
31	7	.	.	–	= 0¹⁰–8²⁵ ≡⁰–9²⁰ =–12⁴⁵ ⌓⁰⁻¹0⁰⁰–13⁴⁰ ⌓⁰20³⁰–24
Σ	–	50.3	–	–	UWAGI

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1	7	0.0	.	–	(K)⁰19⁰⁰–20¹⁰ W-SW ⌓⁰0⁰⁰–10³⁰
2	8	3.4	.	–	▽4⁴⁰–⁴⁶ •⁰14³²–18⁴³ 21⁴³–24
3	7	0.0	.	–	•⁰0⁰⁰–10⁵…15 6⁴³ 7¹² = 7²⁰–11¹⁵ ⊕ 12⁵⁵–13¹²
4	7	.	.	–	⌓¹2⁰⁰–9⁴⁰ ⌓⁰19³⁵–24
5	7	.	.	–	⌓⁰0⁰⁰–8³⁰
6	8	.	.	–	⌓⁰0⁰⁰–a
7	8	0.6	.	–	▽11²⁵–⁴³ ▲⁰14⁴⁷–⁵⁶ ▽14⁵⁹–15³⁸ = 7³⁰–9¹⁵
8	8	.	.	–	
9	8	.	.	–	⌒ 19¹⁵–⁴⁰ ⌓ 20⁴⁰–21¹⁵
10	7	.	.	–	⌴⁰5⁰⁰–6⁵⁰ ⌓ 0⁴⁵–2⁰⁵
11	8	.	.	–	⌴⁰23¹⁰–24
12	7	0.0	.	–	▽10⁰⁰ 11⁴⁸ 12⁵⁰–⁵⁴ = 0⁵⁰–2⁰⁰ 5⁴⁵–6²⁵ ⌴¹ 0⁰⁰–7³⁰
13	7	2.1	pż.	–	*⁰4⁵⁰–7⁴⁰ *¹⁻⁰8²⁵ *²–9⁰⁵ *⁰–9³⁰ ▽23⁴⁷–⁵⁸ = 4³⁰–8²⁰ ≡⁰–9¹⁵ =–10⁵⁴
14	8	0.0	.	–	
15	8	.	.	–	*⁰2⁰⁰–3⁵⁷ = 10⁰–5⁴⁵
16	7	0.7	.	–	•⁰7²⁵ 8²⁰ 23⁵²–24 = 7²⁰–12¹⁰
17	7	.	.	–	•⁰0⁰⁰ 2⁴⁰–3⁴⁰ 4⁰⁸–5⁵⁹ = 0⁰⁰–7²⁰ 21³⁰–24
18	8	.	.	–	= 0⁰⁰–4⁰⁵ 5⁴⁵–7⁴⁵ ⌴⁰0⁰⁰–2⁵⁰
19	6	4.8	.	–	•⁰9³⁰–15¹⁵ •⁰17⁴⁸–18⁵⁰ •⁰–23⁰⁰ = 9¹⁰–21⁴⁰ ≡⁰–23²⁵ =–24
20	7	.	.	–	= 0⁰⁰–7²⁰ ⌓⁰20⁵⁰–24
21	8	.	.	–	= 4³⁰–5⁵⁰ ⌓⁰0⁰⁰–8²⁰ 21⁰⁰–24
22	7	.	.	–	= 5³⁰–8⁴⁰ ⌓⁰0⁰⁰–9¹⁰
23	7	.	.	–	⌓²⁻¹1⁰⁰–8⁴⁰ ⌓⁰23³⁰–24
24	8	1.0	.	–	= 0³⁰–2⁴⁵ ≡⁰⁻¹–4¹⁵ =–6⁵³ ⌓⁰0⁰⁰–8²⁵
25	6	10.6	.	–	•⁰0⁴⁵–7²⁵ •¹ 8⁴³ •⁰9¹⁸–12⁴⁵ 13⁰¹–14¹⁵ •¹⁻⁰18²⁵ = 0⁴⁰–24
26	6	.	.	–	•⁰1¹⁰ 2¹⁵ = 0⁰⁰–24 ⌓⁰20³⁰–24
27	7	.	.	–	= 0⁰⁰–10³⁵ ⌓² 0⁰⁰–8⁴⁵ ⌓⁰23⁰⁰–24
28	7	.	.	–	⌓ 0⁰⁰–7⁴⁰ ⊕ 10²⁵–³⁸
29	7	.	.	–	∞ 18²⁰–21⁵⁰
30	7	2.4	.	–	•(K)⁰0³⁰–0⁵⁶–2¹⁰ W-E ▽…3⁰⁵ •⁰14²⁶–17¹³ = 0¹⁰–4¹⁵ ≡¹–4⁴⁵ =–11³⁰ ⊕ 11²⁵–12⁴⁰
31	7	0.2	.	–	
Σ	–	27.8	–	–	UWAGI.

Zielona Góra $\varphi = 51°56'$ $\lambda = 15°30'$ Maj – Mai 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N		POGODA N,w		KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	98.5	98.3	98.0	98.3	4.7	11.9	7.9	8.1	13.7	2.6	82	42	68	64	1.5	8.1	3.3	4.3	1	4	3	NW 1	NW 1	WNW 1
2	97.1	95.3	93.5	95.3	7.4	12.9	9.9	10.0	13.8	3.5	69	47	61	59	3.2	7.9	4.8	5.3	9	7	10	NE 1	SSE 2	SSE 1
3	92.6	91.4	90.5	91.5	7.9	13.9	7.5	9.2	15.2	6.8	62	60	79	67	4.0	6.4	2.2	4.2	10	9	0	SSE 1	WSW 2	WSW 3
4	89.5	91.7	93.4	91.5	6.5	8.5	5.1	6.3	10.5	4.7	64	52	67	61	3.6	5.3	2.9	3.9	4	5	5	WNW 7	WNW 9	WNW 5
5	93.0	90.9	89.5	91.1	2.9	7.9	3.7	4.6	8.9	0.5	74	50	82	69	1.9	5.3	1.5	2.9	3	7	10	W 6	W 5	WSW 1
6	89.7	89.2	89.4	89.4	0.3	4.9	1.8	2.2	6.6	0.0	100	92	93	95	0.0	0.7	0.6	0.4	10	9	0	WNW 3	NW 1	C 0
7	88.5	88.6	88.7	88.6	1.3	6.2	2.8	3.3	9.0	−0.5	98	69	89	85	0.1	3.0	0.8	1.3	10	9	0	W 2	W 1	WNW 1
8	89.3	89.3	89.7	89.4	2.2	6.2	3.4	3.8	8.4	0.2	96	67	83	82	0.3	3.1	1.3	1.6	10	10	5	WNW 1	NW 2	N 1
9	91.8	92.4	92.6	92.3	4.0	10.0	7.7	7.4	12.2	0.9	87	47	71	68	1.1	6.6	3.1	3.6	10	9	5	C 0	N 1	ENE 1
10	92.6	91.6	92.9	92.4	4.7	12.9	7.5	8.2	14.5	1.9	82	37	72	64	1.5	9.4	3.0	4.6	4	3	7	ENE 1	WNW 3	N 1
11	93.9	93.2	92.8	93.3	5.5	16.7	13.4	12.2	19.8	1.7	80	37	55	57	1.8	12.0	7.0	6.9	1	2	0	N 1	W 1	NE 2
12	93.0	93.3	95.0	93.8	11.5	22.7	15.1	16.1	23.5	9.4	69	28	69	55	4.3	20.0	5.3	9.9	9	6	7	SE 3	SW 2	C 0
13	96.6	96.8	97.5	97.0	14.7	20.1	12.5	15.0	22.5	9.3	70	54	88	71	5.0	10.9	1.7	5.9	4	9	7	S 2	W 2	W 1
14	99.1	100.0	101.3	100.1	12.5	19.3	14.3	15.1	20.3	9.3	86	49	67	67	2.1	11.4	5.5	6.3	1	4	3	WNW 2	WNW 3	C 0
15	102.8	101.5	99.1	101.1	14.3	21.1	16.7	17.2	22.6	9.0	72	41	58	57	4.6	14.8	8.0	9.1	1	1	1	WNW 1	S 1	SE 2
16	96.4	95.5	94.4	94.8	14.1	24.4	14.7	17.0	26.0	11.3	70	40	94	68	4.8	18.3	0.9	8.0	0	2	10	SE 3	SE 3	WNW 2
17	97.1	99.5	99.9	98.8	9.9	10.0	11.3	10.6	14.9	9.3	100	97	91	96	0.0	0.3	1.2	0.5	10 ≡	10 ●	9	NW 1	NW 3	C 0
18	99.3	97.7	95.6	96.9	12.1	17.9	15.4	15.2	20.0	9.6	86	57	71	71	2.0	8.9	5.1	5.3	10	1	0	C 0	ENE 2	ENE 1
19	90.3	88.3	86.4	88.3	13.3	22.3	18.6	18.2	25.1	11.2	81	59	73	71	3.0	11.1	5.9	6.7	3	6	9	ENE 2	ENE 2	C 0
20	89.3	93.2	97.3	93.3	13.6	12.3	10.0	11.3	18.6	9.7	99	94	83	92	0.2	0.9	2.1	1.1	10	10 ●	10	NW 2	NW 3	NW 5
21	99.2	98.1	96.8	98.0	7.9	14.4	10.2	10.7	16.6	6.6	82	55	68	68	1.9	7.5	3.9	4.4	10	7	2	WNW 1	WNW 3	C 0
22	99.9	99.5	99.0	99.5	10.2	15.0	13.1	12.8	16.4	8.0	76	57	65	66	3.0	7.2	5.3	5.2	8	9	10	NNE 2	N 1	C 0
23	99.4	92.5	91.6	92.5	9.6	13.4	13.1	12.3	15.6	8.9	84	76	98	86	1.9	3.7	0.4	2.0	10	10	10 ≡	ESE 1	ENE 1	ENE 1
24	94.3	96.8	101.0	97.4	12.3	14.7	11.9	12.7	16.0	11.5	100	90	74	88	0.0	1.6	3.6	1.7	10 ≡	10	1	C 0	NE 1	NE 3
25	104.6	104.8	106.9	105.4	7.3	12.3	6.7	8.2	14.4	3.1	73	51	64	63	2.7	7.0	3.5	4.4	1	5	0	NE 4	N 4	NE 3
26	107.8	107.2	106.9	107.3	5.0	10.3	6.9	7.3	11.8	1.1	84	51	75	70	1.4	6.1	2.4	3.3	5	9	7	NE 3	NNE 5	N 1
27	105.9	105.4	104.1	105.1	5.9	8.9	5.7	6.6	11.0	0.9	71	67	77	72	2.7	3.8	2.1	2.9	2	9	5	N 2	ENE 1	C 0
28	103.0	102.0	101.1	102.0	6.9	12.1	5.5	7.5	14.1	2.5	78	51	69	66	2.2	6.9	2.7	3.9	0	8	0	NE 2	NNE 2	C 0
29	101.5	101.5	101.1	101.4	9.1	13.4	9.4	10.3	16.4	2.3	67	48	61	59	3.8	8.0	4.6	5.5	3	6	0	NE 1	C 0	C 0
30	101.8	101.1	99.5	100.8	10.6	18.5	14.3	14.4	19.9	6.0	61	38	61	53	5.0	13.3	6.3	8.2	0	1	1	WSW 1	S 3	SE 1
31	99.2	97.6	95.4	97.4	13.5	21.0	15.3	16.3	21.7	10.4	66	37	56	53	5.3	15.7	7.7	9.6	0	3	4	S 3	SSW 2	SSW 1
M	96.4	96.1	96.0	96.2	8.4	14.1	10.0	10.6	16.1	5.5	80	56	74	70	2.4	7.9	3.5	4.6	5.5	6.5	4.5	1.9	2.3	1.2

Czerwiec – Juin

1	95.6	96.7	96.7	96.3	13.6	20.1	13.9	15.4	21.3	12.5	69	55	70	65	4.9	10.5	4.7	6.7	9	4	0	SW 2	W 3	WNW 1
2	98.7	99.5	100.2	99.5	12.8	21.4	15.8	16.4	23.7	10.8	79	43	77	66	3.1	14.7	4.1	7.3	0	1	0	WNW 3	WNW 4	NW 1
3	100.2	97.7	94.7	97.5	16.4	25.4	15.5	18.2	25.7	11.5	74	47	84	68	4.7	17.2	2.8	8.2	2	6	2	NW 1	SSW 3	N 3
4	93.1	92.7	90.7	92.2	15.9	21.7	16.3	17.6	21.9	13.8	84	59	78	74	2.9	10.8	4.0	5.9	9	10	10	ENE 1	NNW 1	W 3
5	89.4	87.4	86.4	87.7	11.3	15.4	12.4	12.9	17.7	10.8	91	74	74	80	1.2	4.6	3.7	3.2	9	7	5	W 6	SW 5	WSW 2
6	88.8	90.7	90.7	90.1	8.8	14.2	13.9	12.7	16.8	8.3	93	54	66	71	0.8	7.4	5.4	4.5	10 ●	7	8	W 7	SW 5	C 0
7	89.5	89.7	90.9	90.0	13.9	20.6	13.5	15.3	21.1	9.8	63	41	69	58	5.9	14.4	4.8	8.4	1	7	4	SSW 5	W 5	C 0
8	91.8	91.7	89.8	91.1	14.7	21.7	18.8	18.5	23.8	12.6	66	47	71	61	5.7	13.9	6.3	8.6	9	4	9	S 4	SSE 5	ESE 5
9	87.9	89.9	91.1	89.6	16.5	17.7	17.1	17.1	22.1	14.6	88	80	83	84	2.4	4.0	3.4	3.3	9	9	7	S 5	W 5	C 0
10	92.0	91.1	90.7	91.3	18.2	23.9	19.3	20.2	25.3	14.2	78	54	77	70	4.7	13.4	5.2	7.8	1	6	7	SSE 2	ENE 2	ESE 1
11	86.9	85.2	90.1	87.4	20.4	28.6	20.6	22.6	31.8	16.0	73	48	81	67	6.5	20.3	4.6	10.5	1	8	9	E 3	SE 3	W 3
12	101.6	106.8	110.4	106.3	13.1	15.8	13.7	14.1	20.6	12.5	99	76	85	87	0.2	4.3	2.3	2.3	10 ●	10	0	NW 3	NW 3	C 0
13	112.7	111.5	110.0	111.4	12.1	19.5	16.3	16.0	22.5	9.0	75	41	61	59	3.5	13.4	7.2	8.0	0	6	0	NW 2	NW 2	NW 1
14	110.5	109.2	108.3	109.3	13.5	23.2	18.7	19.0	24.9	3.7	64	36	41	47	6.4	18.1	12.7	12.4	1	0	1	NW 2	NE 3	ENE 2
15	108.9	107.6	104.8	107.1	14.7	22.8	18.7	18.7	24.5	10.3	49	34	48	44	8.5	18.3	11.2	12.7	0	0	0	ENE 3	ENE 3	E 3
16	103.6	102.1	99.8	101.8	17.6	24.9	20.0	20.6	25.3	12.5	60	32	45	46	8.1	21.6	12.9	14.2	0	0	0	E 2	E 4	E 3
17	99.7	98.6	96.8	98.4	19.0	27.0	21.3	22.2	27.8	13.7	56	37	48	47	9.6	22.3	13.1	15.0	0	1	0	E 4	E 4	E 2
18	96.0	94.4	91.8	94.1	20.2	28.6	23.8	24.1	30.4	16.4	44	32	48	41	13.4	26.7	15.3	18.5	0	0	1	ESE 3	ESE 3	E 1
19	90.9	89.9	90.8	90.5	22.6	30.2	23.4	24.9	31.1	19.1	60	37	61	53	11.0	27.2	11.2	16.5	2	4	2	W 1	NW 2	C 0
20	95.8	95.0	96.5	95.1	13.7	20.4	17.2	17.1	26.1	13.7	99	80	82	87	0.2	4.9	3.5	2.9	10 ●	5	1	C 0	N 1	SE 1
21	97.2	94.1	89.9	93.7	17.5	24.4	20.4	20.7	25.2	13.6	74	46	65	62	5.1	16.5	8.5	10.0	0	5	3	ESE 1	SE 2	SE 1
22	86.2	85.2	85.4	85.6	16.9	20.3	16.0	17.3	23.9	15.8	99	84	94	92	0.2	3.7	1.2	1.7	10 ●	10 ●	10	SSW 5	WSW 4	WNW 2
23	89.5	89.2	91.7	90.1	13.2	19.5	13.7	15.0	20.7	11.9	90	68	100	86	1.6	7.3	0.0	3.0	9	9	4	W 2	SSW 3	WNW 1
24	91.8	89.7	86.1	89.2	11.4	12.9	12.9	12.5	15.2	10.6	99	94	88	94	0.2	0.9	1.8	1.0	10 ●	10	10	NE 2	E 3	E 3
25	84.7	93.8	97.4	92.0	12.1	10.8	11.0	11.2	14.8	9.6	89	95	73	86	1.5	0.7	3.2	1.8	10	10 ●	2	WSW 7	W 5	WSW 1
26	100.4	101.4	103.2	101.7	10.1	15.5	13.2	13.0	18.0	7.8	82	45	71	66	2.3	9.7	4.5	5.5	1	4	2	NW 2	WNW 4	NW 1
27	104.1	103.2	106.1	105.1	11.4	16.1	14.2	14.0	19.1	8.7	88	47	62	66	1.7	9.7	6.1	5.8	8	5	4	WNW 2	NW 5	C 0
28	104.5	102.9	102.1	103.2	12.6	23.2	22.8	20.8	28.3	12.0	95	52	65	71	0.7	13.4	9.6	8.6	10 ●	5	1	SW 5	W 4	NW 1
29	103.8	103.0	101.1	102.6	22.1	28.8	26.2	25.8	30.8	17.4	62	41	50	51	10.1	23.2	16.9	16.7	1	2	0	WNW 1	W 3	W 1
30	101.3	101.1	100.3	100.9	23.3	30.4	21.6	24.2	31.5	20.6	70	41	64	58	8.5	25.5	9.3	14.4	1	4	7	C 0	NNW 2	SSE 1
31																								
M	96.5	96.4	96.2	96.4	15.4	21.6	17.4	18.0	23.7	12.5	77	54	70	67	4.3	13.4	6.6	8.2	4.8	5.2	3.6	2.7	3.3	1.4

Zielona Góra — $H_s = 176$ m — $H_b = 174{,}0$ m — $h_w = \frac{V}{VI}\ \frac{9\text{ m}}{16\text{ m}}$ — Maj – Mai 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	–	
2	8	.	.	–	
3	8	.	.	–	
4	8	0.0	.	–	▽ 12⁰⁰–04, 17⁴¹–46, 18²⁷–³⁸, 20²⁸–³⁶; ◠ 17³⁹–⁴⁸ NE
5	8	1.5	.	–	▽ 9³¹–³⁷, 10³⁶–³⁸, ⁂ 10⁵⁴–⁵⁹, ⁂ ▽ 11⁰⁴–¹⁶, ⁂ 11³⁹–⁴², •⁰ 23⁰⁰–24
6	7	0.8	.	–	•⁰ 0⁰⁰–2⁴⁵, ▽ 10³²–³⁹, 12¹⁰–⁴³, • ⁂ 13²⁶–⁴⁷, ▽ 14¹⁷–²⁹, 15³⁴–16¹⁰, 16⁵²–17³⁹; = 3⁴⁵–9⁵⁰, 19³⁰–24; ⌓⁰ 19³⁰–24
7	8	.	.	–	= 0⁰⁰–3³⁰, 5⁵⁵–8³⁰; ⌓⁰ 0⁰⁰–3³⁰, 7¹⁰–10¹⁰; ⌴⁰ 3³⁰–7¹⁰
8	7	.	.	–	= 0³⁰–2¹⁰; ≡⁰–4¹⁰; —730; ⌴⁰ 0⁰⁰–2⁰⁰; ⌓⁰ 20³⁵–24; ⊕ 14²⁵–18³⁰; ⊔ 21⁰⁰–22³⁵
9	8	.	.	–	= 6⁵⁰–7³⁰; ⌓⁰ n – 9⁴⁵
10	8	.	.	–	= 4³⁰–6¹⁰; ⌓ 4⁰⁰–8³⁰
11	7	.	.	–	= 2⁵⁵–5⁴⁵; ⌴⁰ 3³⁰–6¹⁵
12	7	.	.	–	
13	7	10.5	.	–	▽ 7⁴²–⁵⁸, 12³⁰–³⁴, 14⁰⁹–¹³, 16⁵⁵–17⁰¹, 17²⁵–20³⁰; ⌈⁰ 11³³–12⁵⁰ SE–NW (⌈)⁰ 16¹⁵–⁵⁰ SSE–SW ⌈⁰ 16⁵⁰–17³³–19⁴⁰ W–E;
14	7	.	.	–	[13.V: ⌓ 1³⁰–7¹⁰]
15	7	.	.	–	⌓¹ 2⁰⁰–8⁴⁰
16	8	14.9	.	–	• 19¹⁵–⁴⁵ ▽ –21⁰⁵ • –21⁴⁰ ▽ …24; ⌈⁰ 19¹⁵–19⁴⁰–23⁴⁵ W–E; ⌊ –24 E
17	5	0.4	.	–	▽ 0⁰⁰–10⁵ •⁰ 2⁵⁰–5¹⁰ •⁰⁻¹ 6³⁰–7⁰⁵ •⁰ 12³²–14⁰² •⁰ 14⁴⁹–15¹⁶, 16⁰⁵–17⁵²; (⌈)⁰ 0⁰⁰–3⁰⁰ E; = 0⁰⁰–15⁵ ≡⁰–3⁴⁰ —420
18	8	.	.	–	= 0⁰⁰–6⁴⁵, 19⁴⁰–24; ⌓⁰ 20⁴⁰–24 [17.V: ≡⁰–7²⁰ ≡¹–9⁴⁰ —15¹⁰ 23⁵⁰–24]
19	7	8.7	.	–	▽ 22⁰⁴–18; ⌈⁰ 17³⁵–18¹⁵ ESE–N ⌊ 21⁵⁰–22⁴⁵ N, 23⁰⁰–24; = 0⁰⁰–3²⁰; ⌓⁰ 0⁰⁰–8³⁰
20	6	1.7	.	–	▽ 4¹⁴–6⁴⁶ •⁰ 10⁰¹–19²⁵; (⌈) 2⁴⁰–4¹⁵ ⌈⁰ 4¹⁵–4³³–5⁴⁵ SSE–NW; = 4²⁵–20¹⁰
21	8	.	.	–	
22	8	1.8	.	–	⊕ 16¹⁰–17³⁰
23	7	4.8	.	–	•⁰ 10⁵–30⁵ 9⁰¹–09 9⁵⁰–59, 12⁰⁰–11 13⁴⁵–16³⁰, 17⁴⁷–58, 18¹⁸–²⁵ 19⁰⁰–20¹⁵; = 16³⁰–20⁴⁰ ≡⁰–24
24	5	0.3	.	–	• 6⁰⁵–7¹⁰ •¹–8⁰² • ⁽⁻⁾8³²; ≡⁰ 0⁰⁰–4²⁰ —505 ≡⁰–530 ≡¹–8¹⁸ —1910
25	8	.	.	–	⌓⁰ 2³⁰–7²⁰
26	8	.	.	–	
27	7	0.0	.	–	▽ 12⁴⁰–50 14⁵⁰–59
28	8	.	.	–	⌓⁰ 2³⁰–7⁰⁰, 22¹⁵–24
29	8	.	.	–	⌓⁰ 0⁰⁰–1⁵⁰ ⌴⁰–4¹⁵ ⌓⁰–7³⁰
30	8	.	.	–	
31	7	.	.	–	
Σ	–	45.4	–	–	UWAGI.

Czerwiec – Juin

1	7	.	.	–	∞⁰ 15¹⁰–22⁵⁰; ⌓⁰ 21⁵⁰–24
2	7	.	.	–	⌓⁰ 0⁰⁰–8⁰⁰
3	7	5.2	.	–	▽ 19³⁰–20²⁵ (⌈) 18³⁵–19¹⁵ W ⌈¹ 19³⁵–20¹⁵ SW–NE
4	7	1.1	.	–	•⁰ 21³³–22²⁰; = 8²⁰–11⁵⁵ 22³⁰–24
5	8	0.0	.	–	•⁰ 0⁵⁰–2²⁰ 3¹⁵ 5³⁰ ▽ 13⁴⁵–52, 14³²–³⁵, 14⁵²–15⁰⁵; = 0⁰⁰–6³⁰
6	8	(0.0)	.	–	•⁰ 5⁰⁸…⁴⁶, 6⁴⁰…8³⁰
7	7	0.0	.	–	⊕ 11³⁰–⁴⁵
8	8	.	.	–	•⁰ 3⁵⁰ 5³⁰; ⌣ 21⁴⁵–24
9	7	0.0	.	–	•⁰ 11³⁵ 12¹⁵ ▽ 12²⁵–²⁸ (⌈) 12³⁵–13⁰⁵ NW; = 3⁵⁵–8²⁰; ⌓⁰ 4¹⁵–8³⁰, 22²⁰–24; ⌣ 0⁰²–1⁰⁰ ⊕ 14⁵⁰–16³⁰
10	7	.	.	–	⌓⁰ 0⁰⁰–8⁴⁰; ⊕ 10³⁵–55 12⁵⁰–59 ⌣ 21²⁰–24
11	7	1.0	.	–	⌊ 23²⁰–⁵⁵ (⌈) –24; = 20¹⁰–24; ⌣ 0⁰⁰–3⁰⁰
12	7	(0.0)	.	–	▽ 0²⁰–⁵⁰ 1²⁰ •⁰ 7⁰⁰–8⁰⁵ •¹–9²⁰ •⁰–9⁴⁵; (⌈) 0⁰⁰–²⁰ NW ⌈ 0²⁰–³⁰–⁵⁰ W–N; = 0⁰⁰–5²⁵ ≡⁰ 5²⁵–7¹⁵ —1040
13	8	.	.	–	
14	8	.	.	–	⌓⁰ 3³⁰–8¹⁰
15	9	.	.	–	
16	8	.	.	–	
17	8	.	.	–	
18	8	.	.	–	
19	7	6.4	.	–	▽ 14⁵⁰–15¹⁵ 17²⁰–⁴⁰; ⌈⁰ 13⁵⁰–14⁴⁰–15³⁰ N–S (⌈) 17³⁰–18²⁵ S ⌊ 22¹⁰–24 NW
20	7	1.6	.	–	▽ 1⁴⁵–8²⁵ •⁰–9¹⁰; ⌊ 0⁰⁰–53 NW ⌈⁰ 3⁵⁸–4⁴⁰ N–S; = 8²⁵–12²⁰
21	8	1.6	.	–	⌓⁰ 2⁰⁰–8²⁵
22	6	6.2	.	–	•⁰⁻² 6⁵⁶–7²⁸ •⁰–9⁴⁵ 12⁵⁰–13¹⁰ 16⁵⁰–17⁰³, 17¹⁷–18³⁵ ▽ 18⁵⁹–20⁰² 22²⁰–²⁸ (⌈)⁰ 18⁰⁵–²⁸ SE ⌈⁰ 19⁰¹–19²⁰–20¹⁰ SE–NW;
23	7	17.9	.	–	▽ 15⁵⁵–17²⁰; ⌈⁰ 15⁴⁵–16⁰⁰–17¹⁰ SSW–NNE; = 0⁰⁰–6⁴⁵ 17²⁰–24 [22.VI: = 1³⁰–24]
24	6	12.6	.	–	•⁰ 7⁴⁶–8¹⁵ •¹–10⁴⁰ •⁰–12³¹ 12⁴³–13¹⁵; = 0⁰⁰–1⁵⁰ ≡ —415 —1430
25	6	0.0	.	–	•⁰⁻¹ 0³⁷–3⁰⁵ •⁰ 3³⁵–4³⁹ •⁰ 8⁴⁵–9²⁰ … 13²⁰ •¹ 13⁵⁹ ▽ 14²⁰–⁴⁵ •⁰ 15³⁶ 16⁰³; = 0¹⁰–3¹⁰ ≡⁰–4³⁰ —555
26	7	0.3	.	–	= 1²⁰–3³⁰
27	7	0.0	.	–	•⁰ 4¹⁰–5¹³…⁵⁴; ⊕ 19⁴⁰–20⁰²
28	7	0.0	.	–	•⁰ 3⁵⁰–4⁰² 7⁴⁸ 8⁰⁵; = 6³⁰–10²⁰
29	7	.	.	–	= 5¹⁰–6⁵⁵; ⌓⁰ 0⁰⁰–8⁰⁰
30	7	0.0	.	–	▽ 18⁵⁰–19⁰¹; (⌈)⁰ 17³⁰–18³⁰–18³⁵ SW ⌈⁰ 18⁵⁰–19⁴⁵ SW–NE
31					
Σ	–	34.1	–	–	UWAGI.

Zielona Góra $\varphi = 51°56'$ $\lambda = 15°30'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.3	98.2	96.3	97.9	21.4	30.2	25.8	25.8	31.6	17.9	68	45	66	60	8.2	23.5	11.2	14.3	1	0	1	SE 3	ESE 2	ESE 3
2	94.3	96.8	99.8	97.0	21.3	26.4	19.1	21.5	27.2	19.1	71	63	78	71	7.3	12.9	4.8	8.3	1	4	0	SW 3	NW 4	N 1
3	101.4	100.0	97.3	99.6	18.2	24.3	20.8	21.1	26.3	13.4	68	48	55	57	6.8	16.1	11.0	11.3	1	1	1	E 2	S 1	SE 1
4	95.9	94.2	92.9	94.3	15.6	29.6	28.2	25.4	33.2	14.6	97	59	69	75	0.6	17.1	12.0	9.9	6	0	4	SE 3	S 4	C 0
5	93.0	93.2	93.2	96.1	25.2	32.9	23.6	26.3	33.1	23.0	74	41	86	67	8.4	29.3	3.9	13.9	0	1	2	W 1	NW 3	NNW 2
6	102.6	101.1	99.4	101.0	18.8	25.7	22.8	22.5	28.6	14.0	76	45	58	60	5.1	18.1	11.7	11.6	0	0	1	N 1	NW 1	E 1
7	99.2	98.6	95.5	97.8	19.5	30.6	26.7	25.9	32.3	16.7	70	50	43	54	6.9	21.9	19.8	16.2	1	0	10	E 3	E 5	ESE 4
8	95.9	96.1	94.8	95.6	21.9	29.0	24.8	25.1	29.3	17.9	65	50	68	61	9.2	20.1	9.9	13.1	3	7	9	SE 4	NNW 1	NNE 1
9	94.3	96.2	95.3	95.3	18.0	21.8	18.2	19.0	25.0	17.5	96	65	88	82	0.8	9.7	2.5	4.3	10	6	2	NW 3	NE 1	C 0
10	92.7	90.5	89.1	90.8	18.0	24.8	19.6	20.5	25.0	16.4	93	53	86	77	1.4	14.6	3.2	6.4	9	7	10	S 1	E 1	ESE 1
11	86.4	88.1	90.6	88.4	15.8	18.1	16.1	16.5	19.8	15.4	100	97	99	99	0.0	0.7	0.2	0.3	10 ●	10 ●	10 ●	NE 4	N 2	N 3
12	91.5	91.8	92.3	91.9	16.6	23.0	19.8	19.8	24.6	14.7	93	67	78	79	1.4	9.3	5.1	5.3	9	5	2	NNW 1	NNW 2	W 1
13	94.7	95.6	97.2	95.8	19.6	26.2	21.3	22.1	27.1	16.0	78	48	75	67	5.1	17.5	6.2	9.6	0	2	9	W 1	SW 2	C 0
14	95.5	96.1	94.8	95.5	20.4	21.0	17.3	19.0	22.0	17.2	78	80	97	85	5.3	5.0	0.6	3.6	9 (R)	9	7	ESE 1	SW 3	C 0
15	93.1	93.1	92.9	93.0	15.9	20.6	19.0	18.6	22.7	15.6	99	65	60	75	0.2	8.3	8.9	5.9	10	5	7	W 1	W 3	WSW 1
16	92.2	92.0	91.3	91.8	14.8	20.3	17.4	17.5	21.9	14.3	80	62	74	72	3.3	9.0	5.1	5.8	10	10	10	W 2	WNW 1	WNW 1
17	90.2	90.4	91.4	90.7	14.2	18.6	16.8	16.6	19.9	13.0	93	66	84	81	1.1	7.2	3.1	3.8	10	10	9	WNW 3	NNW 4	NNW 1
18	92.8	91.5	89.6	91.3	15.9	22.4	18.4	18.8	23.9	13.3	77	51	63	64	4.2	13.2	8.0	8.5	1	4	0	W 2	NW 3	ENE 1
19	88.0	86.7	85.2	86.6	18.3	25.0	22.3	22.0	27.7	15.1	69	44	58	57	6.6	17.7	11.3	11.9	0	3	5	SSW 1	SSE 3	ESE 2
20	83.9	83.8	85.0	84.9	16.4	16.2	14.9	15.6	22.5	14.8	94	89	98	94	1.1	1.9	0.3	1.1	10	10 ●	10	WSW 2	W 2	NW 1
21	84.4	84.0	84.0	84.1	15.5	19.2	16.8	17.1	21.0	14.2	91	74	89	85	1.5	5.8	2.1	3.1	10	10	10	C 0	SW 1	ENE 1
22	83.6	82.0	82.8	82.8	13.9	14.6	16.8	15.5	19.4	13.6	99	100	98	99	0.2	0.0	0.4	0.2	10 ●	10 ●	10	WNW 3	WNW 4	C 0
23	84.1	86.0	88.3	86.1	16.2	17.8	16.6	16.8	20.9	15.6	100	96	97	98	0.0	0.8	0.6	0.5	10 ●	10 ●	10	NNW 3	NW 4	WNW 4
24	90.4	91.4	91.2	91.0	14.5	16.4	14.8	15.1	19.2	13.7	97	68	85	83	0.6	6.0	2.5	3.0	10	9	10	W 3	W 4	W 1
25	92.0	91.2	89.0	90.7	13.3	15.8	13.7	14.1	16.5	11.2	81	76	92	83	3.0	4.3	1.3	2.9	3	10	6	W 3	WSW 4	WSW 2
26	90.1	89.6	87.5	89.1	12.4	17.8	14.0	14.6	18.2	11.6	86	83	99	89	2.0	3.4	0.2	1.9	4	9	10 ●	W 3	WSW 4	SSW 3
27	84.4	84.3	84.3	84.4	15.8	14.5	14.4	14.8	18.6	13.8	93	92	85	90	1.3	1.3	2.3	1.7	10	10 ● (R)	8	WSW 3	SW 3	SW 2
28	86.7	87.4	88.2	87.4	12.6	17.4	14.6	14.8	19.2	10.9	87	58	76	74	1.9	8.4	4.0	4.8	3	9	3	W 4	W 4	SW 2
29	89.4	90.3	93.0	91.0	12.8	18.8	14.7	15.2	20.5	12.0	98	56	85	80	0.4	9.3	2.3	4.1	9	8	10	SW 1	WSW 4	SW 3
30	94.4	96.8	99.8	97.0	13.9	13.7	14.1	14.0	15.6	13.3	98	98	97	98	0.4	0.4	0.6	0.5	10 ●	10 ●	10	WSW 3	W 4	W 2
31	102.3	104.3	105.2	104.1	13.0	14.9	13.9	13.9	16.0	12.4	100	79	84	88	0.0	3.4	2.3	2.0	10 ●	10	10	WNW 2	W 4	C 0
M	92.3	92.4	92.3	92.3	16.8	21.3	18.6	18.9	23.3	14.9	86	67	80	78	3.0	10.2	5.1	6.1	6.1	6.4	6.7	2.4	2.8	1.3

Sierpień – Août

1	104.7	104.4	102.9	104.0	14.6	20.4	18.3	17.9	23.4	12.4	85	60	74	73	2.3	9.3	5.4	5.8	1	3	2	WNW 1	NW 2	WNW 1
2	103.7	103.3	103.9	103.6	15.0	19.4	14.4	15.8	19.8	14.1	92	52	70	71	1.3	10.8	5.0	5.7	8	5	1	NW 1	NW 6	NW 1
3	103.2	103.0	102.2	102.8	11.6	15.5	14.1	13.8	18.0	10.2	87	68	78	78	1.8	5.7	3.6	3.7	9	10	0	W 3	WNW 2	W 2
4	101.9	102.2	102.7	102.3	13.2	19.5	16.7	16.5	21.2	11.4	92	59	75	75	1.3	9.4	4.8	5.2	2	7	6	NW 3	WNW 3	W 1
5	103.7	103.8	102.8	103.4	15.0	21.2	16.9	17.5	23.4	12.9	87	48	65	67	2.2	13.1	6.8	7.4	0	5	1	WNW 1	N 1	NE 1
6	102.5	101.1	98.5	100.7	19.4	24.8	19.8	21.0	25.7	14.8	62	40	59	54	8.6	18.9	9.5	12.3	0	4	7	SE 1	SE 2	SE 1
7	94.3	92.3	90.4	92.3	17.6	21.4	16.0	17.8	23.4	15.5	74	67	96	79	5.1	8.4	0.8	4.8	7	9	6	SE 2	SE 2	W 1
8	91.0	91.6	90.5	91.0	13.8	21.6	17.6	17.6	24.2	13.6	100	58	74	77	0.0	10.9	5.3	5.4	10 ▬	3	5	WNW 3	NNW 2	C 0
9	87.2	84.9	80.9	84.3	16.4	23.0	21.1	20.4	24.8	13.6	83	58	64	68	3.0	11.9	9.1	8.0	3	7	10	ESE 3	SE 6	ESE 2
10	81.1	81.9	86.0	83.0	16.5	21.6	18.8	18.9	23.7	16.2	97	64	70	77	0.6	9.3	6.5	5.5	10	7	1	SSW 3	SW 8	SW 3
11	90.3	90.1	90.3	90.2	16.7	25.6	21.8	21.5	27.8	13.8	81	46	67	65	3.7	17.6	8.5	9.9	4	4	2	S 4	SW 5	SW 1
12	91.1	92.0	92.7	91.9	17.8	22.1	19.0	19.5	24.3	16.9	94	55	63	71	1.2	12.1	8.1	7.1	10	5	6	NW 1	WSW 3	SW 1
13	94.3	94.9	93.8	94.3	17.8	22.2	18.7	19.4	24.7	14.9	73	59	65	66	5.6	11.2	7.5	8.1	2	8	6	W 1	WSW 2	W 1
14	92.8	92.7	90.4	92.0	15.2	16.9	16.4	16.2	19.5	14.1	92	83	88	88	1.3	3.3	2.3	2.3	10	10	9	NE 1	ESE 1	N 1
15	89.6	88.9	88.9	89.1	14.8	22.7	18.4	18.6	23.9	12.9	92	55	77	75	1.3	12.4	4.9	6.2	1	6	10	SW 1	SSW 2	S 1
16	90.9	92.1	91.4	91.5	15.2	15.6	14.7	15.0	18.7	13.1	85	87	94	89	2.6	2.3	0.9	1.9	9	9	8	WSW 3	WSW 1	S 1
17	91.7	91.3	90.4	91.1	11.6	16.2	13.2	13.6	18.1	10.8	88	68	95	84	1.6	6.0	0.7	2.8	7	9	10	SW 3	WSW 3	SW 4
18	89.4	88.9	90.5	89.6	13.1	18.7	14.8	15.4	19.8	12.0	92	65	90	82	1.3	7.7	1.6	3.5	10	8	0	WSW 3	WSW 4	W 2
19	92.9	93.3	97.2	95.1	12.2	17.2	15.8	15.2	20.8	11.3	98	72	77	82	0.3	5.4	4.1	3.3	3	3	0	W 3	W 3	W 2
20	98.2	97.2	96.3	97.3	13.4	19.0	16.9	16.6	21.2	11.9	86	60	77	74	2.1	8.9	4.4	5.1	2	2	6	SW 4	SW 7	SW 3
21	96.0	94.2	92.6	94.3	15.4	18.1	11.8	14.3	20.0	11.4	96	85	96	92	0.8	3.1	0.5	1.5	10	10	10	SW 3	SSW 2	N 1
22	92.8	92.7	93.5	93.0	11.2	15.6	11.2	12.3	17.1	10.7	99	64	92	85	0.2	6.4	1.0	2.5	10	7	3	WNW 2	NW 4	W 3
23	93.3	92.3	90.3	92.1	9.8	16.9	13.6	13.3	19.3	8.0	90	58	73	74	1.3	8.0	4.2	4.5	1	6	1	W 1	S 2	SE 1
24	85.6	85.2	90.2	86.3	11.1	16.4	10.9	12.3	17.9	9.7	84	81	94	86	2.1	3.4	0.8	2.1	9	10 ●	0	SE 4	SW 5	WSW 3
25	92.9	90.7	89.6	91.1	10.0	18.1	13.0	13.5	20.9	7.7	87	58	78	74	1.6	8.8	3.3	4.6	1	8	10	SSW 4	SSW 6	NW 4
26	88.8	88.7	91.1	89.5	12.2	15.6	12.0	13.0	17.2	10.1	79	65	86	76	3.0	6.5	2.0	3.8	2	9	0	S 4	SW 7	SW 4
27	93.0	92.7	92.7	92.8	11.4	16.8	11.8	13.0	17.5	9.6	90	63	89	81	1.4	7.0	1.3	3.3	8	6	10 ●	SW 3	SW 4	SSW 4
28	91.8	93.1	93.0	93.3	10.8	13.2	11.2	11.6	16.1	10.2	97	88	91	92	0.4	1.8	1.2	1.1	10 ●	10	4	WSW 1	WSW 1	W 1
29	97.2	98.3	99.3	98.4	9.4	14.3	12.0	11.9	16.9	8.4	97	75	86	85	0.3	4.3	2.0	2.3	10	6	2	W 3	SW 3	W 1
30	100.4	100.3	99.1	99.9	9.3	14.8	11.3	11.7	15.8	8.0	93	66	78	79	0.8	5.7	3.0	3.2	9	8	2	W 4	W 4	WSW 1
31	96.2	95.8	94.2	95.4	10.3	12.6	9.4	10.3	14.8	9.0	86	79	97	87	1.8	3.1	0.3	1.7	10	9	6	SW 3	SSW 2	NW 1
M	94.3	94.0	93.9	94.1	13.6	18.6	15.2	15.6	20.6	11.9	88	69	80	78	2.0	8.2	3.9	4.7	6.1	6.9	4.6	2.3	3.3	1.7

Zielona Góra — $H_s = 176$ m — $H_b = 174{,}0$ m — $h_w = 16$ m — Liniec – Juillet 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	
2	7	.	.	–	
3	8	5.1	.	–	
4	7	.	.	–	▽ 5⁰⁹–5⁸ ● 6²⁵–7²⁵ W–SE ▽ 6⁵⁹–7²⁰ . (☇)⁰ 4³⁶–5⁰⁸ ☇⁰ 5⁰⁸–5²⁸–6²⁵ W–NNE (☇)–7²⁵ W–SE
5	7	.	.	–	
6	7	.	.	–	☇¹ 23⁴⁴–24 W
7	8	1.8	.	–	☇¹ 0⁰⁰– 5⁰⁸ W–SW 21¹⁵– 24 NW, SW, N, NNW
8	7	2.3	.	–	☇¹ 0⁰⁰– 2¹⁵ NW N ☇²–3²⁷ N–SE ☇ 23¹⁰–²⁰ SW (☇)⁰–24 SW ● na
9	7	0.4	.	–	▽ 0⁰⁶–¹⁰ 1⁵⁰–2¹⁰ ●¹ 7⁴⁵–⁵¹ ●⁰ 8²⁰–³⁰ ▽ 16²⁰–17⁰⁵ . (☇)⁰ 0⁰⁰–⁰⁵ ☇ 0⁰⁵–0²⁵–2¹⁵ SW–E (☇)⁰ 3³⁰–4³⁰ W–SE. = 2¹⁰–3³⁰ .
10	7	17.4	.	–	▽ 8⁰¹–⁴² 15²⁹–16¹⁰ ●⁰ 21³⁰–⁵⁵ 23⁵² 24 . = 7⁴⁰– 10²⁰ . ⌓ ⁰ 0⁰⁰–8⁰¹ . ⊕ 13³⁰– 14¹⁵ **9.VII:** ⌓ ⁰ 21²⁰– 24
11	6	61.7	.	–	●⁰⁻¹ 0⁰⁰– 12⁰⁸ ●⁰ 13⁰⁴– 17¹² ●¹– 17⁴⁴ ●²– 17⁴⁸ ●¹– 17⁵⁶ ●²– 18⁰⁴ ●¹⁻⁰– 24
12	7	.	.	–	● 0⁰⁰– 3⁰⁵ . = 0⁰⁰– 8¹⁵
13	7	0.0	.	–	
14	6	4.3	.	–	●⁰ 7⁵⁰ 2¹⁵–3³⁵ ▽⁰ 5²⁸–6⁰⁶ . 6³⁵–⁴⁰ 9¹⁷–10⁰⁸ 14¹⁶…⁵⁷ ●⁰ 17⁴²– 18¹³ ▽ 22⁴⁶–24 . (☇)⁰ 4⁰⁸–5⁴⁵ SW 7⁴⁰–9³⁰ SW ☇⁰ 9³⁰–10⁰⁰ 10²⁸
15	7	.	.	–	▽ 0⁰⁰–⁰⁵ . ☇⁰ 0⁰⁰–¹⁰ SW–SE . = 0⁰⁰– 1⁵⁰ . 2²⁰– 5²⁰ ≡⁰– 7²⁰ = – 11¹⁰ **14.VII:** SW–NNE ☇⁰ 22⁴⁰–23³⁰–24 SW–SE. = 10²⁵– 15²⁵ . 21³⁰– 24
16	7	.	.	–	
17	8	0.0	.	–	●⁰ 20⁴³…⁵⁹ . = 4³⁰– 8⁴⁵
18	7	.	.	–	
19	7	.	.	–	
20	6	6.0	.	–	●⁰ 11¹³ 12⁴⁵ ●⁰ 12⁵² 14⁰⁸ ▽ 19³⁰–20³² ●⁰ 20⁴⁶–⁵⁹ 22²⁶–⁵³ . ☇⁰ 19³⁰–19³⁵–20²⁰ W–E . = 16¹⁵–³⁵ = – 17²⁰ . 20⁵⁹– 24
21	7	3.0	.	–	●⁰ 0¹⁰–3⁵⁹ 9⁵⁵ 10²⁰– 12²⁰ ▽ 18⁵⁵–19²⁷ . = 0⁰⁰– 10¹⁵ 21⁰⁵– 24
22	5	61.4	.	–	●⁰ 3⁵⁰ 4³⁵–6¹⁵ ●¹ 9¹⁰ ●² 9⁵⁷ ●¹ 10¹² ●⁰⁻¹ 15⁵² ●² 16¹⁵ ●¹⁻⁰ 16⁴⁰ ▽¹ 19⁵⁰–20¹⁰ ▽² 20²⁵ . = 0⁰⁰– 14⁵⁵ ≡⁰– 16⁵⁰ = 17⁴⁵ 21⁴⁵ 22⁵⁰
23	6	18.2	.	–	▽¹⁻⁰ 0³² 1⁰⁴ ▽ 3⁵⁰ 4³⁰ ●⁰⁻² 6²⁵–⁴² ▽ 7⁰⁸ 8⁰⁰ ●⁰ 9⁴⁵ 12⁵⁸ ●¹– 13⁵² ●⁰ 15¹¹ ▽ 17⁰⁹–²³ ▽⁰ 17⁵⁰ 18¹⁰ ▽² 18⁴² 20³⁰ . ☇¹ 18⁵⁵ 19⁰⁰ 20¹⁵ NW–SE
24	7	0.0	.	–	●⁰ 9¹⁰ 10¹⁵ ▽ 19⁴³–20⁰² . ☇ 0⁰⁰– 5⁶ . = 0⁰⁰– 7⁴⁵ **22.VII:** ≡ – 24
25	7	0.6	.	–	▽ 11²⁵– 12⁴⁰ 14³⁸–⁵⁷ ▽⁰ 15⁰⁰–¹⁵ ●⁰ 16⁵⁰– 17³⁵ . = 14⁵⁵– 24 **23.VII:** (☇) 20³⁰–⁵⁵ NW–N–SE ☇ 21³⁵ 24 . = 0⁰⁰ 6²⁵ = – 24
26	7	5.0	.	–	●⁰ 11⁴⁴ 13⁵⁸ ▽ 14⁰⁴–⁰⁸ 14⁴²–⁵⁰ ●⁰ 15⁴³ 16⁰⁰– 17⁰⁵ ▽⁰– 17³⁹ ●⁰– 19²⁰ 20¹²…⁵⁷ 21¹⁰ 22⁵⁸ . = 0⁰⁰ 6³⁰ 11²³– 13²⁵ 19⁵⁰– 24
27	6	5.8	.	–	●⁰ 3¹²–²⁰ 4³⁵–⁵⁰ 8⁵⁵– 10²⁰ ▽ 10³⁰–³⁴ ●⁰ 11¹⁷–²⁵ ▽ 12⁵⁵– 14²⁸ . ☇ 13⁰⁵–14³⁶ W–E . = 0⁰⁰– 14⁴³
28	7	1.4	.	–	▽ 14¹⁵–²⁷ 17⁵⁰–⁵² . = 2¹⁵– 6³⁵
29	7	1.7	.	–	●⁰ 2¹⁵– 4⁴⁸ ▽ 14⁰⁶–¹⁶ 14³²–⁵⁸ ●⁰ 23⁴⁰–24 . = 1⁴⁰– 9²⁰ . 22⁵⁰– 24
30	6	11.8	.	–	●⁰ 0⁰⁰–²² ● 4⁴⁵–⁵² ●⁰ 5⁴⁸– 6¹⁷ ●⁰⁻¹ 7⁰⁰– 9¹⁰ ●¹⁻⁰ 13⁴⁵ ●⁰– 14²⁰ ●●⁰– 15⁰⁷ ●⁰– 17⁴⁵ 18¹⁵– 19³² 20⁰⁰ . = 0⁰⁰– 24
31	7	0.1	.	–	●⁰ 1⁴⁰– 2⁴⁵ ●●⁰– 3²⁵ ●⁰⁻¹ 8⁴⁵ ●⁰– 10³⁰ ●²⁻⁰ 11²⁵–⁴⁸ . = 0⁰⁰– 4⁴⁵ ≡⁰– 6¹⁸ ≡¹– 7³⁰ ≡⁰– 10¹⁵ = – 12⁵⁵
Σ	–	208.0	–	–	UWAGI:

Sierpień – Août

1	7	.	.	–	= 2³⁰–4³⁰ 6¹⁰–7⁴⁰ . ⌓¹ 23⁰⁰– 24
2	7	.	.	–	= 4⁴⁵– 9⁴⁸ . ⌓¹ 0⁰⁰– 8²⁰ . 20⁴⁰– 24
3	7	0.0	.	–	●⁰ 9⁰⁸– 10²⁰ ●⁰– 11²⁰ . ⌓¹ 0⁰⁰– 8¹⁵
4	7	.	.	–	= 12⁵– 7⁵⁰ . ⌓ 20⁰– 11⁰⁰
5	8	.	.	–	⌓¹ 2⁰⁰– 8³⁵ ⌓ 21³⁰– 24
6	8	.	.	–	⌓¹ 0⁰⁰– 9³⁰
7	6	0.5	.	–	●⁰ 10⁰² 11⁵⁶ ▽ 18²⁰–20⁰³ . ☇⁰ 18¹⁵–19³⁵–20¹² W–E . = 11¹⁵– 24
8	7	.	.	–	= 0⁰⁰– 4⁴⁰ ≡⁰– 5³⁵ ≡¹– 9³⁰ = – 11⁵⁰
9	7	8.9	.	–	●23⁴⁰–⁵⁸ ▽–24 . (☇) 20⁴⁵–21¹⁵ W–N ☇⁰ 23⁴⁰–24 W–E . = 6¹⁰–7⁴⁰ 23⁵⁰–24 . ⌓⁰ 3⁴⁵– 9¹⁰
10	8	0.0	.	–	▽☇⁰ 0⁰⁰– 1⁴⁵ W–E ▽–21⁵ ●⁰– 4⁰⁵ ●¹⁻⁰– 6⁵⁹ ▽ 19¹⁹–²¹ . = 0⁰⁰– 9³⁰
11	9	3.7	.	–	⌓ ²⁵⁰– 8¹⁰
12	7	0.0	.	–	▽ 2²⁰–3⁴³ ●⁰ 5⁵³…7¹⁰ . ☇⁰ 13⁵–2¹⁰ W (☇)⁰–2²⁴ W ☇⁰–3⁴⁵ W–NE . = 6⁰⁰– 9⁵⁰ . ⊕ 11⁵⁵– 13⁰⁰
13	7	3.2	.	–	
14	7	2.3	.	–	●⁰ 3¹¹– 4⁴⁵ 5⁰⁵– 7¹⁷ 8⁰⁵– 10¹² 11³⁷ 12⁰⁰ . = 21³⁰– 24 . ⌓² 20²⁵– 24
15	7	0.4	.	–	▽ 0²⁴–⁴⁹ 16⁵⁰– 17²⁵ . = 0⁰⁰– 3⁴⁰ ≡²– 5²⁰ = – 11⁴⁰ . ⌓² 0⁰⁰– 24
16	7	3.4	.	–	▽ 1⁵⁰– 2⁰² ●⁰ 10¹⁹– 13³⁵ . = 2¹⁰– 13⁵⁰ . ⌓⁰ 21³⁵– 24
17	8	0.2	.	–	▽ 17⁴¹–⁴⁹ 18⁰²–⁰⁸ . = 17⁴⁹– 24 . ⌓⁰ 0⁰⁰– 3⁵⁰
18	7	1.6	.	–	▽ 14¹⁷–⁴⁵ 16²²– 18¹⁵ ☇ 16⁵⁴– 17²⁵– 18¹⁰ W–SE . = 5²⁰– 12²⁰
19	7	.	.	–	= 5³⁰– 13⁴⁰ . ⌓ 22⁴⁵– 24
20	7	2.9	.	–	⌓ 0⁰⁰– na
21	6	9.3	.	–	●⁰⁻² 10⁶–⁴⁰ ●⁰ 3³⁵– 5¹⁰ ▽ 13¹⁸ 14⁰⁴–14⁴² ●⁰ 15³⁸– 17⁴⁵ ▽ 18⁴⁵– 19⁰⁵ ●⁰⁻¹ 22¹⁵ . = 0⁰⁵– 24
22	7	8.9	.	–	▽ 11⁵³–⁵⁹ 12⁰⁴–¹² ●▲ ☇⁰ 14⁴⁵–14⁵⁵–15¹⁰ WNW–E ▲▲ ▽ 16⁴⁵– 17¹⁵ ☇⁰ 16³⁰–16⁵⁵–17¹⁵ WNW–ESE . = 0⁰⁰– 10¹⁵
23	7	.	.	–	= 6³⁵– 8⁴⁰ . ⌓⁰ 21³⁰– 24
24	6	12.5	.	–	●12⁰⁵ 14³⁵ ▽ 14⁴⁵– 15³⁵ ●⁰⁻¹ 17⁰⁶ ▽ 18⁰⁴–25 . ☇⁰ 14⁵⁵–15⁰⁰–15³⁰ W–SE . ⛆ 14⁵⁵–15¹⁰ . = 6¹⁰–10¹⁵ . ⌓⁰ 0⁰⁰– na
25	7	.	.	–	
26	7	1.4	.	–	▽ 10⁵⁴– 11⁰⁸ ●⁰ 11¹⁵ 12⁰⁵ ▽ 14⁴³–⁵⁶ . (☇)⁰ 16⁵⁵– 17²⁵ NW–ENE
27	7	2.4	.	–	▽ 21⁴⁰– 22¹⁵ . = 5²⁰– 10³⁰ . 21⁴⁰– 24 . ⌓⁰ 0⁰⁰– 9⁴⁰
28	6	2.0	.	–	▽ 3⁴⁵– 4¹⁰ ●⁰⁻¹ 4⁵⁰– 10¹⁰ ●¹⁻⁰ 10³⁴–⁵⁸ 11⁴⁵– 12⁵⁵ . = 0⁰⁰– 14⁵⁰
29	7	0.0	.	–	▽ 14⁵⁷– 15⁰⁰ . = 3¹⁵– 5³⁰ ≡⁰– 6⁵⁵ = – 10³⁰ . ⌓⁰ 20²⁰– 24
30	7	0.0	.	–	⌓¹ 0⁰⁰– 10⁵⁰
31	6	10.4	.	–	●⁰ 12⁻¹⁸ 3¹⁵ 5⁰⁰ 6⁰³…¹⁸ ●¹⁻⁰ 8²⁰–9¹⁰ ▽ 12⁵¹– 13⁴⁴ . 20¹⁶–⁴⁵ . ☇⁰ 13²⁰–³⁰–⁴⁵ W–SE ☇⁰ 20¹⁰–³⁵–⁵⁰ SW–SE . = 4¹⁰– 24
Σ	–	74.0	–	–	UWAGI:

Zielona Góra — $\varphi = 51°56'$ — $\lambda = 15°30'$ — Wrzesień – Septembre 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.9	96.9	97.4	96.7	9.4	15.4	11.4	11.9	16.4	8.1	97	70	84	84	0.3	5.3	2.2	2.6	9	7	2	SW 4	W 5	SW 1
2	95.7	94.7	93.4	94.6	9.8	16.9	13.6	13.5	18.7	8.5	87	81	91	86	1.6	3.7	1.5	2.3	8	8	9	S 2	SSW 2	SSW 2
3	94.4	96.2	97.8	96.1	12.2	12.4	12.4	12.4	16.9	11.6	93	90	90	91	1.0	1.4	1.4	1.3	10	9	9	W 3	WNW 2	C 0
4	100.4	101.8	103.1	101.8	9.0	15.6	10.2	11.2	18.0	8.7	92	55	82	76	1.0	7.9	2.2	3.7	1	5	0	WNW 1	W 3	WNW 1
5	101.7	98.7	97.6	99.3	9.7	18.4	16.0	15.0	21.0	8.0	83	46	73	67	2.0	11.4	4.9	6.1	2	7	10	S 2	SSW 4	WSW 4
6	97.3	97.8	99.0	98.0	12.8	18.4	14.1	14.8	19.4	12.1	98	69	85	84	0.4	6.7	2.4	3.2	9	9	1	WSW 1	SW 1	E 1
7	98.7	97.9	97.2	97.9	13.6	21.8	18.4	18.0	23.8	12.9	93	60	70	74	1.1	10.5	6.5	6.0	1	5	0	SE 2	SW 3	SSW 1
8	97.5	98.4	98.2	98.0	16.8	26.7	22.0	21.9	28.1	15.1	78	45	63	62	4.2	19.4	9.8	11.1	4	2	4	S 3	S 2	C 0
9	98.3	101.7	104.0	101.3	17.2	18.6	13.9	15.9	22.2	13.5	80	79	95	85	3.9	4.5	0.7	3.0	1	10	10	SSW 3	W 5	WNW 2
10	103.3	101.7	97.6	100.9	12.6	17.5	14.2	14.6	19.7	12.2	100	67	84	84	0.0	6.6	2.5	3.0	8 ≡	6	7	C 0	C 0	SSE 1
11	92.5	86.9	79.1	86.2	11.2	19.6	14.8	15.1	20.3	10.2	90	60	96	82	1.3	9.2	0.7	3.7	4	9	9	S 2	SSW 9	S 7
12	73.8	77.3	82.5	77.9	13.8	14.4	11.2	12.6	16.2	11.0	98	57	71	75	0.4	7.0	3.9	3.8	10 ●	4	1	SSW 4	WSW 10	SW 6
13	84.5	83.2	81.2	83.0	9.3	14.9	11.6	11.8	17.0	7.3	80	53	75	69	2.3	7.9	3.4	4.5	6	5	10	SW 6	SW 6	SW 10
14	83.1	84.2	85.8	84.4	8.5	13.9	10.0	10.6	15.9	6.6	88	54	79	74	1.4	7.4	2.5	3.8	8	7	10	SW 5	SW 5	SSW 4
15	85.4	88.1	92.1	88.5	7.9	11.7	9.4	9.6	14.2	6.8	90	88	84	87	1.0	1.6	1.9	1.5	10 ●	9	3	SW 3	W 5	SW 3
16	93.1	94.1	96.4	94.5	7.9	9.4	6.8	7.7	12.0	6.8	85	82	97	88	1.6	2.2	0.3	1.4	10	9	3	SW 3	WSW 4	SW 3
17	95.9	95.7	95.3	95.6	8.6	11.6	9.2	9.6	13.2	6.4	97	88	96	94	0.3	1.6	0.4	0.8	10	9	7	SW 4	W 3	W 2
18	95.2	95.2	94.0	94.8	8.0	13.6	10.2	10.5	15.2	7.5	100	58	82	80	0.0	6.5	2.2	2.9	10 ≡	3	0	NW 1	W 4	W 3
19	89.9	87.2	87.8	88.3	8.0	12.8	12.0	11.2	13.9	6.6	99	98	98	98	0.1	0.4	0.3	0.3	10	10 ●	10	SW 1	WSW 4	W 4
20	89.9	93.2	95.2	92.8	9.1	12.8	7.6	9.3	13.3	7.4	99	69	91	86	0.2	4.6	0.9	1.9	10 ≡	9	4	WNW 4	WSW 1	NW 1
21	96.1	95.6	93.2	95.0	7.0	15.4	12.2	11.7	15.9	6.5	96	61	80	79	0.4	6.9	2.9	3.4	6	4	10	E 2	SE 1	E 3
22	89.6	90.0	88.8	89.5	12.0	17.3	16.8	15.7	18.3	9.4	100	87	90	92	0.0	2.6	2.0	1.5	10 ≡	9	10 ●	S 1	WSW 2	SW 3
23	83.0	77.3	81.9	80.7	13.6	15.6	13.0	13.8	17.2	13.0	98	97	98	98	0.4	0.6	0.4	0.5	9	10	10 ●	SSW 3	SSW 2	W 4
24	85.7	86.1	91.5	87.8	10.6	8.5	6.5	8.0	13.9	6.3	96	96	90	94	0.5	0.5	1.0	0.7	10	10	0	W 3	WNW 3	WNW 3
25	96.3	98.0	99.0	97.8	3.9	10.8	5.1	6.2	13.0	3.1	87	54	80	74	1.1	6.0	1.8	3.0	0	4	0	W 4	WNW 5	C 0
26	96.5	96.8	99.6	97.6	5.6	12.4	5.4	7.2	13.3	3.5	67	44	81	64	2.9	8.1	1.7	4.2	3	8	0	C 0	N 1	C 0
27	100.2	96.0	88.3	94.8	4.2	11.3	11.0	9.4	11.7	1.4	74	56	71	67	2.1	5.9	3.8	3.9	9	10	10	WSW 2	WSW 7	W 10
28	87.9	88.2	88.3	88.1	9.9	11.7	9.0	9.9	13.3	7.9	82	72	92	82	2.2	3.7	1.0	2.3	10	5	2	W 7	W 8	W 4
29	83.7	80.3	80.5	81.5	7.9	8.4	7.2	7.7	9.0	7.0	97	100	91	96	0.2	0.0	0.9	0.4	10 ●	10 ●	10	WSW 3	SSW 1	W 5
30	86.1	90.1	94.6	90.3	3.8	9.0	4.8	5.6	9.7	3.3	92	70	94	85	0.7	3.5	0.6	1.6	10	6	1	W 7	W 5	C 0
31																								
M	92.4	92.3	92.7	92.5	9.8	14.6	11.3	11.8	16.4	8.3	91	70	85	82	1.2	5.5	2.2	3.0	7.3	7.2	5.4	2.9	3.8	3.0

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1	96.3	96.9	100.0	97.7	3.4	9.2	4.2	5.2	9.7	2.6	100	67	90	86	0.0	3.8	0.8	1.5	8 ≡	9	1	C 0	WNW 3	C 0
2	103.5	103.9	102.6	103.3	2.8	8.6	4.5	5.1	10.4	1.2	100	59	70	76	0.0	4.6	2.5	2.4	9	5	0	C 0	NW 1	WSW 1
3	96.6	93.2	91.0	93.6	1.8	8.8	8.0	6.6	9.8	0.9	93	69	89	82	0.6	3.9	1.2	1.9	9	10	7	SSW 3	SW 10	W 7
4	93.4	97.2	101.7	97.4	4.8	9.2	6.2	6.6	10.4	4.6	90	47	73	70	0.8	6.1	2.6	3.2	5	3	4	W 5	WNW 7	W 5
5	103.3	101.2	98.6	101.0	5.8	10.2	8.6	8.3	11.4	5.4	88	52	66	69	1.1	6.0	3.8	3.6	8	5	10	W 4	WSW 7	SW 4
6	99.0	101.9	104.3	101.7	8.8	12.6	11.1	10.9	12.9	7.0	96	71	83	83	0.4	4.2	2.3	2.3	10	9	9	W 3	W 3	W 1
7	104.6	104.9	105.6	105.0	11.0	13.6	11.2	11.8	14.5	10.0	97	74	84	85	0.3	4.0	2.1	2.1	10	9	0	W 3	NW 3	C 0
8	106.8	107.0	106.6	106.8	10.2	14.6	11.2	11.8	15.2	8.6	92	68	90	83	0.9	5.3	1.3	2.5	9	8	0	SE 1	SE 2	ESE 4
9	103.8	102.9	100.9	102.5	6.0	15.9	13.4	12.2	18.4	5.8	100	68	80	83	0.0	5.8	3.2	3.0	10 ≡	0	0	C 0	SSW 1	SSE 1
10	99.9	99.5	99.2	99.5	10.2	19.2	14.2	14.4	20.4	9.4	82	54	74	70	2.2	10.2	4.3	5.6	0	0	0	S 1	S 2	SW 3
11	100.1	100.0	99.4	99.8	8.8	15.4	11.9	12.0	17.4	7.2	96	70	87	84	0.4	5.3	1.8	2.5	10 ≡	5	1	WNW 1	WNW 1	E 1
12	98.7	102.7	107.0	102.8	11.0	12.0	9.1	10.3	12.8	9.0	90	100	95	95	1.3	0.0	0.7	0.7	7	10 ≡	0 ≡	SW 1	WNW 2	C 0
13	106.9	105.0	103.0	105.0	7.4	15.0	10.8	11.0	16.8	6.7	99	76	90	88	0.2	4.0	1.4	1.9	4	1	1	SE 2	S 2	SW 1
14	103.1	105.3	106.6	105.0	7.0	10.0	10.4	9.4	12.9	6.4	100	91	87	93	0.0	1.1	1.6	0.9	10 ≡	8	10	NW 1	NW 1	W 1
15	107.8	108.0	107.2	107.7	9.4	10.0	8.2	9.0	10.7	7.8	100	97	100	99	0.0	0.3	0.0	0.1	10 ≡	10	10	WNW 1	ESE 1	SE 1
16	103.8	101.6	98.4	101.3	6.7	12.8	8.9	9.3	14.9	6.6	100	72	88	87	0.0	4.1	1.4	1.8	10 ≡	0	0	SE 2	S 2	S 2
17	96.5	98.5	99.0	98.0	9.4	13.4	10.6	11.0	14.2	7.5	88	82	92	87	1.4	2.8	1.0	1.7	9	10	6	SSW 6	W 4	SW 2
18	92.4	90.3	89.4	90.7	11.4	17.0	14.0	14.1	19.2	8.9	93	70	80	82	0.7	5.8	3.2	3.2	10 ●	7	0	SSW 3	SW 6	SW 5
19	88.0	87.3	86.8	87.4	13.4	20.3	11.2	14.0	20.3	11.0	78	58	83	73	3.3	10.0	2.3	5.2	8	8	10	SSW 5	SW 4	NW 1
20	92.1	94.7	96.9	94.6	8.0	8.8	7.4	7.9	11.8	7.2	100	95	96	97	0.0	0.6	0.5	0.4	10	10	0	C 0	WSW 1	WSW 2
21	96.3	93.5	90.2	93.3	3.4	11.6	5.6	6.6	12.5	2.7	100	64	88	84	0.0	4.8	1.1	2.0	10 ≡	2	2	S 2	SW 4	SSW 3
22	84.0	81.6	82.6	82.7	3.8	12.2	8.8	8.4	13.0	3.5	93	53	73	73	0.5	6.7	3.0	3.4	6	7	10	SSW 2	SW 3	SW 2
23	87.9	91.2	93.5	90.9	6.5	8.2	5.5	6.4	9.3	4.9	97	75	88	87	0.3	2.7	1.1	1.4	8	7	0	W 3	WSW 3	SW 4
24	92.3	93.8	101.7	96.6	8.3	8.4	9.6	9.0	9.6	5.2	71	94	96	87	3.2	0.6	0.5	1.4	10	10 ●	10	SW 8	SW 6	WSW 2
25	104.2	104.7	104.0	104.3	6.8	12.5	8.2	8.9	14.1	6.2	100	71	94	88	0.0	4.2	0.6	1.6	10 ≡	6	0	WSW 1	SW 1	S 1
26	102.6	101.7	100.2	101.5	7.6	14.5	7.8	9.4	15.1	6.2	89	59	89	79	1.2	6.8	1.2	3.1	1	0	0	SSW 2	SSW 1	SSW 2
27	98.4	97.8	98.2	98.1	5.2	12.7	5.0	7.0	13.0	4.9	99	67	95	86	0.4	4.9	0.4	1.9	2	6	0	SSW 4	SW 1	SW 2
28	98.4	98.1	98.0	98.2	6.9	13.0	8.1	9.0	13.9	3.8	90	66	90	82	1.0	5.1	1.1	2.4	10	2	9	SSW 2	SW 3	SSW 2
29	96.9	97.0	96.5	96.8	7.5	13.4	8.6	9.5	13.9	6.1	87	65	89	80	1.4	5.3	1.3	2.7	6	9	3	SSW 3	SW 3	SW 2
30	93.8	93.4	94.8	94.0	7.2	13.7	10.4	10.4	15.8	6.4	88	64	82	78	1.2	5.7	2.2	3.0	4	7	2	S 3	SW 3	SW 3
31	94.3	93.0	90.0	92.4	6.6	13.2	9.2	9.6	13.8	6.2	96	66	84	82	0.4	5.1	1.8	2.4	5	10	4	SW 3	SW 3	SSW 3
M	98.3	98.4	98.5	98.4	7.3	12.6	9.1	9.5	13.8	6.1	93	70	86	83	0.7	4.3	1.7	2.3	7.7	6.2	3.5	2.4	3.1	2.2

Zielona Góra $H_s = 176\ m$ $H_b = 174{,}0\ m$ $h_w = 16\ m$ **Wrzesień – September 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	P O G O D A
1	7	.	.	–	= 0⁰⁰–12²⁵, ⌒³ 23⁴⁵–24
2	6	0.0	.	–	= 6³⁰–24, ⌒¹ 0⁰⁰– nm.
3	6	2.7	.	–	•⁰4⁴⁵ 6¹⁵ ▽ 12⁰⁷–12 12²⁸–47 13²⁷–49 17¹⁴–30, = 0⁰⁰–9⁵⁰ 13¹⁰–14⁵⁵, 19³⁰–24, ⌒¹ np–24
4	7	.	.	–	= 0⁰⁰–8²⁰, ⌒¹ 11⁰⁰–12⁰⁰ ⌒⁰ 21⁰⁰–24
5	7	0.1	.	–	•⁰ 20³⁹–42 22¹⁵–23⁵², = 19³⁵–24, ⌒¹ 0⁰⁰–10¹⁰, ⊕ 10⁵²–12³⁵, ⌓ 2⁴⁰–4⁵⁸
6	7	.	.	–	= 0⁰⁰–13⁵⁰ 17⁰⁵–24, ⌒¹ 21²⁰–24
7	7	.	.	–	= 0⁰⁰–12³⁰, ⌒ 0⁰⁰–11⁴⁰ ⌒⁰ 22⁰⁵–24
8	7	.	.	–	= 6¹⁰–7⁴⁰ ⌒⁰ 0⁰⁰–7¹⁰ ⌒¹ 21⁵⁰–24
9	6	5.3	.	–	•⁰ 17²⁰–30 22⁴⁹–23²⁰ •¹⁻⁰ 24–6⁴⁰–7⁵⁰ 9⁰⁵–15³⁰ 18¹⁰–24, ⌒¹ 0⁰⁰–0³⁰
10	7	.	.	–	•⁰ 0⁰⁰–0⁵ = 0⁰⁰–6⁴⁸ ≡⁰–8³⁰ = 9⁰³, ⌒⁰ 23¹⁵–24
11	6	4.1	.	–	•⁰ 17²⁰…35 17⁴⁵–20³⁸ 23²⁶–24, = 6⁰⁵–15²⁰ ⌒¹ 0⁰⁰–9⁴⁰
12	7	2.2	.	–	•⁰ 0⁰⁰–20 3⁴⁵–6²⁰ 7⁰²–8¹⁵ •⁰⁻² 9⁴⁸–10⁵⁰, = 5³⁰–10⁵⁰
13	8	1.7	.	–	▽ 21⁴⁸–22⁵⁸
14	7	0.0	.	–	•⁰ 6⁰⁶–14 6²⁵–58 7⁰²…59, = 6⁰⁵–56
15	7	7.2	.	–	•⁰ 7⁰⁵–8³⁰ •¹⁻⁰ 12⁰² ▽ 12⁰⁸–16 12²⁵–32 13⁰⁰–06 19²³–20⁰⁰, = 6⁴⁰–12⁵⁵, ⌓ 3⁵⁵–5⁴⁵
16	7	4.7	.	–	▽ 11¹⁷–35 11⁵⁹–12⁰⁶ ▲▽ 13¹⁰–14 ▽ 14⁴¹–43 16¹³–20 •⁰ 23¹⁵–24
17	6	12.5	.	–	•⁰0⁰⁰ 3³⁰ •⁰6⁴⁷–7³⁵ 8²⁰ 9⁷⁰ •• ⁰–10¹⁵ •⁰–12³⁸ ▽ 14²⁸–³⁴ 16³⁵–⁴¹, 17¹⁰–²¹, 17³⁰–45 ▲▽ 17⁵⁰–18⁰³ ▽–18¹⁷, 18⁴⁷–19²⁴,
18	7	.	.	–	= 0⁰⁰–7¹⁰ ≡¹–8¹⁵ =–9³⁵ [17.IX: ☈⁰ 17⁵⁷–18⁰⁰–18²⁰ W-S, = 7⁵⁰–19²⁰
19	5	6.4	.	–	•¹⁸⁷⁰–9⁰⁰ •⁰–13⁵⁰ •⁰14⁰¹–45 •⁰15³⁵ 17¹⁵ 18⁴⁵–19⁰⁰ = 1⁴⁵–9²⁰ ≡⁰–11⁵⁵ =–24, ⌒ 3⁴⁵–8¹⁰
20	7	.	.	–	= 0⁰⁰–6¹⁰ ≡⁰–9²⁰ =–12¹⁰ 20⁵⁰–24, ⌒⁰ 21³⁰–24
21	7	2.2	.	–	•⁰ 23⁵⁹–24, = 0⁰⁰–1¹⁰ ⌒¹ 0⁰⁰–11⁴⁵
22	5	4.6	.	–	☾⁰ 0⁰⁰–04 ▽ 4⁰⁰–30 •⁰4⁴⁰ 6¹⁷ ▽ 21⁵⁶–22²² 23³¹–³⁶ 23⁴⁷–24, ☾ 2³⁰–3⁴⁵ W ☈² 21⁴²–23³⁵ W-SE, = 5⁵⁰–6³⁰ ≡¹–9⁴⁰
23	6	24.8	.	–	▽⁰ 0⁰⁰–05 •⁰ 0²³–1⁵⁰ •⁰⁻¹ 9²³–12⁵⁶ •⁰ 13¹⁸–³⁵ 14¹⁸–16¹⁰ •¹ 21²⁰–23⁰⁰, = 0⁰⁰–24, ⌓ 4³⁰–5³⁰
24	6	6.6	.	–	•⁰ 8³⁰ 11⁰⁵–58 12⁰³…35 12⁵⁰–14²⁵, = 0⁰⁰–8³⁰ [22.IX: =–24, ⌒ 19³⁰–21⁵⁶
25	7	.	.	–	
26	8	.	.	–	⌴⁰ na – 8¹⁰ ⌒ 22⁴⁵–24, ⊕ 11³⁵–14⁰⁵
27	7	9.0	.	–	•⁰ 19⁴⁰ 21¹⁰ 22⁴⁵–24, = 1²⁰–5¹⁵ 22⁴⁰–24, ⌒⁰ 0⁰⁰–3⁴⁵ ⌴⁰–8⁴⁰ ⌒⁰–9⁴⁰
28	7	7.0	.	–	•⁰0⁰⁰ 15 ▽ 4²⁰–30 8¹⁰–⁴³ 9⁵⁰–10⁰⁵ 12³⁰–47 14⁰⁰–⁰³, 18⁴³–19¹⁰, 20⁵²–21⁰⁰, 21³⁰–⁴², = 0⁰⁰–2³⁰
29	5	7.0	.	–	•⁰0⁰⁰ 2¹⁰ 2⁵⁴ 8⁰⁵ 8¹⁰–13³⁵, = 8⁵⁰–24
30	7	.	.	–	= 9¹⁵–12²⁰, 21²⁵–24
31					
Σ	–	106.1	–	–	UWAGI

Październik – Octobre

1	7	0.2	.	–	▽ 15¹²–³⁸ 16¹⁶–²⁵ 16⁴⁸–17¹⁸, = 0⁰⁰–4⁴⁸ ≡⁰–5¹⁰ ≡¹–5²⁰ ≡²–5⁵⁰ ≡¹–6³⁰ ≡⁰–7⁰³ = 10³⁰ 20²⁰–24, ⌒ 1⁴⁵–11⁰⁵
2	7	.	.	–	= 0⁰⁰–5²⁰, ⌴⁰ 0³⁰–7¹⁵, 21⁰⁰–24
3	6	1.4	.	–	•⁰ 11⁴⁵ 12²⁵, 15²⁰–16⁴⁵, = 5⁰⁰–24, ⌴⁰ 0⁰⁰–7²⁰
4	8	0.0	.	–	▽⁰ 30–35
5	7	0.4	.	–	•⁰ 6¹²–¹⁴ 17³² 19⁰⁵ 21³⁵ 24, = 23³⁰–24
6	7	0.0	.	–	•⁰ 0⁰⁰…15 5¹⁵–³⁵ = 0⁰⁰–9⁵⁰
7	7	.	.	–	•⁰ 3²⁷–4⁰⁰ = 3¹⁰–12³⁵
8	7	.	.	–	= 2⁵⁰–6²⁰, = 0⁰⁰–9²⁰
9	6	.	.	–	= 0¹⁵–3¹⁷ ≡⁰–3²⁵ ≡¹–5⁴⁵ ≡²–6⁵⁰ ≡¹–8⁵⁵ =–12⁰⁰ ∞ –18³⁰ =–24, ⌒ 0³⁰–12⁰⁰ ⌒¹ 22¹⁰–24
10	7	.	.	–	= 0⁰⁰–8¹⁰, 19⁰⁰–24, ⌒¹ 0⁰⁰–12¹⁰
11	5	.	.	–	= 0⁰⁰–6⁵⁰ ≡⁰–10⁵⁰ =–24, ⌒⁰ 0⁰⁰–11⁵⁰ ⌒ 20¹⁰–24, ⌓ 1⁴⁵–5⁷
12	2	0.0	.	–	▽ 9¹⁵–²¹ •⁰ 10²³…³⁵ 16⁴⁰ 18⁰⁵, = 0⁰⁰–10⁴⁰ ≡¹–21⁴⁵ =–24, ⌒ 0⁴⁰–5³⁰, 21¹⁰–24
13	6	.	.	–	= 0⁰⁰–24 ⌒ 0⁰⁰–13⁰⁰ 19³⁰–24
14	5	0.5	.	–	•⁰⁻² 22³⁵–24 = 0⁰⁰–3⁴⁵ ≡¹–5²⁰ ≡²–11²⁵ =–23⁵⁰ ≡⁰–24, ⌒¹ 0⁰⁰–13¹⁰
15	5	0.5	.	–	•⁰⁻² 0⁰⁰–6⁰⁰ •¹⁻⁰–8²⁰ •⁰⁻² 11²⁰ •⁰–12⁴⁵, ≡⁰⁻¹ 0⁰⁰–6³⁰ ≡²–7³⁵ ≡¹⁻⁰–8⁴⁰ =–10³⁵ ≡¹–11⁴⁰ =–22²⁰ ≡⁰–24
16	5	.	.	–	≡¹ 0⁰⁰–5⁵⁰ ≡⁰–6¹⁰ ≡¹–10¹⁰ =–24, ⌒ 18⁴⁰–24
17	6	2.6	.	–	•⁰ 7⁰⁸–15 ▽ 8⁰⁵–15 •⁰–8³⁷, = 0⁰⁰–24, ⌒ 0⁰⁰–7⁰⁶
18	6	0.8	.	–	•⁰ 6¹³–8⁴⁰, 9⁴⁵–10³⁰, = 0⁰⁰–13¹⁰
19	7	4.2	.	–	▽ 18⁰²–37
20	6	0.8	.	–	•⁰ 1³⁰–6³⁰ 8⁴⁰ 10¹⁰, = 21⁰⁰–23²⁵ ≡⁰–23⁵⁰ ≡¹–24, ⌒ 23⁴⁵–24
21	7	.	.	–	≡¹ 0⁰⁰–20 ≡²–8⁴⁵ ≡¹⁻⁰–9¹⁵ =–12⁰², 18¹⁵–19³⁰, ⌒ 0⁰⁰–12⁰⁰
22	7	0.2	.	–	
23	7	0.0	.	–	•⁰ 1⁰⁵–45 •⁰4²⁸–5²⁰, = 0¹⁰–12²⁰
24	6	1.1	.	–	•⁰ 3⁵⁵ 5¹⁰ 8⁴²–13²⁵, = 2⁵⁰–6²⁰ 8⁵⁰–24
25	6	.	.	–	= 0⁰⁰–3¹⁵ ≡⁰–5⁴⁰ =–6³⁰ ≡²⁻⁰–8²⁰ =–24, ⌒ 18³⁰–24
26	6	.	.	–	= 0⁰⁰–24 ⌒¹ 0⁰⁰–12¹⁵
27	7	.	.	–	= 0⁰⁰–12¹⁵, 23⁴⁰–24, ⌒⁰ 0⁰⁰–11¹⁰
28	6	.	.	–	= 0⁰⁰–12¹⁰ ∞ –16³⁰ =–24, ⌒ 18⁴⁰–24
29	6	.	.	–	= 0⁰⁰–24, ⌒ 0⁰⁰–6³⁰ ⌒⁰ 23⁰⁰–24
30	6	.	.	–	= 0⁰⁰–24, ⌒⁰ 0⁰⁰–12⁰⁵
31	7	.	.	–	= 0⁰⁰–10²⁵, ⌒ 1⁵⁰–9⁴⁵, ⊕ 11⁵⁸–12¹⁰
Σ	–	12.7	–	–	UWAGI

Zielona Góra — φ = 51°56' — λ = 15°30' — Listopad – Novembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	84.7	84.5	87.6	85.6	9.5	11.9	8.8	9.8	12.4	7.6	79	68	97	81	2.5	4.4	0.3	2.4	10	10	6	SSW 2	SSW 3	SW 1
2	90.5	91.4	93.2	91.7	4.8	11.0	5.2	6.6	11.5	3.6	90	52	87	76	0.8	6.3	1.1	2.7	3	8	6	SW 1	SW 5	S 2
3	94.1	93.2	90.9	92.7	4.0	12.4	6.9	7.6	12.6	3.5	90	56	87	78	0.8	6.4	1.3	2.8	1	1	0	S 1	SSE 1	SE 2
4	89.8	89.6	90.1	89.8	5.2	13.4	9.0	9.2	14.5	4.9	97	70	84	84	0.2	4.7	1.9	2.3	6	8	8	SSE 4	SSE 3	S 3
5	86.5	83.8	84.9	85.1	5.4	14.8	9.8	10.0	15.5	4.8	98	63	86	82	0.2	6.2	1.7	2.7	5	6	7	SE 3	SSW 2	S 3
6	85.8	87.0	84.8	85.9	9.6	11.9	9.2	10.0	13.3	7.3	82	77	87	82	2.2	3.1	1.5	2.3	7	9	4	SW 1	SW 1	E 4
7	82.2	85.4	87.2	84.9	9.8	9.8	8.8	9.3	10.4	7.9	82	82	86	83	2.2	2.2	1.3	2.0	9	10	9	SW 3	SW 4	WSW 1
8	85.5	85.7	85.8	85.7	7.6	9.5	8.9	8.7	10.0	7.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10	10 ● ≡	ENE 2	NE 2	C 0
9	83.6	84.3	86.8	84.9	8.1	9.0	9.2	8.9	10.2	7.4	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ●	10 ≡	ENE 2	E 2	SE 1
10	88.3	87.9	90.8	89.0	7.7	9.1	7.7	8.0	10.7	7.0	100	100	98	99	0.0	0.0	0.1	0.0	9 ≡	9	10	SE 1	E 5	E 7
11	93.3	95.7	99.0	96.0	8.4	8.9	7.8	8.2	9.2	7.1	94	85	93	91	0.6	1.7	0.8	1.0	10	10	10 ●	E 2	ENE 3	ENE 6
12	103.0	105.6	108.2	105.6	5.5	5.4	3.8	4.6	8.0	3.6	92	91	100	94	0.7	0.9	0.0	0.5	10	10 ●	10	NE 4	NE 4	ENE 2
13	108.8	109.2	109.7	109.2	1.5	3.0	0.2	1.2	4.0	0.1	94	86	76	79	0.4	2.6	1.5	1.5	10	9	9	NE 1	ENE 2	E 3
14	109.7	110.1	110.8	110.2	-2.4	-1.8	-2.2	-2.2	0.6	-2.5	82	81	94	86	0.9	1.0	0.3	0.7	10	10	10	E 4	ESE 2	E 3
15	110.5	109.8	108.8	109.7	-2.0	-1.2	-0.4	-1.0	-0.2	-2.5	100	99	100	100	0.0	0.1	0.0	0.0	10 ≡	10 ≡	10 ≡	E 3	ESE 2	SE 2
16	108.7	109.8	110.5	109.7	0.4	1.2	0.6	0.7	1.4	-0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●	10 ≡	S 2	C 0	ESE 1
17	109.8	109.8	110.9	110.2	-0.9	2.6	-0.3	0.3	3.1	-1.0	99	91	96	95	0.0	0.7	0.3	0.3	10	7	4	E 2	E 3	E 3
18	110.7	110.2	110.1	110.3	0.6	2.4	1.4	1.4	3.0	-0.6	96	89	96	94	0.3	0.8	0.3	0.5	10	10	10	E 2	ESE 1	E 2
19	110.3	112.1	114.3	112.2	0.7	2.2	0.6	1.0	2.5	0.4	96	89	84	90	0.2	0.8	1.0	0.7	10	10	10	ENE 1	E 1	ESE 2
20	115.0	115.8	116.4	115.7	-1.8	2.0	-1.0	-0.4	2.6	-2.5	82	69	81	77	1.0	2.2	1.1	1.4	0	0	0	ESE 4	SE 3	SE 5
21	115.3	113.3	108.6	112.4	-0.7	5.4	-0.3	1.0	5.5	-3.0	79	57	86	74	1.2	3.9	0.9	2.0	0	0	0	SE 2	SE 2	SE 3
22	101.7	98.3	96.8	98.9	-0.8	1.3	0.8	0.5	1.9	-1.7	83	76	73	77	1.0	1.6	1.8	1.5	0	10	10	SW 4	WSW 3	SW 3
23	95.5	96.1	102.3	98.0	0.8	2.8	2.1	2.0	4.2	0.2	85	96	85	89	1.0	0.3	1.0	0.8	10	10 ●	0	SW 4	WSW 6	WNW 5
24	103.9	103.1	102.4	103.1	-0.4	4.2	5.2	3.6	5.4	-0.8	96	93	90	93	0.2	0.5	0.8	0.5	5	10	10	W 3	W 6	W 5
25	100.2	100.5	102.5	101.1	4.4	5.0	6.0	5.4	6.1	4.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ●●	10 ≡	10 ● ≡	W 8	W 6	W 5
26	103.1	103.3	102.1	102.8	5.4	5.5	5.2	5.3	6.3	5.1	100	100	97	99	0.0	0.0	0.2	0.1	10 ● ≡	10 ● ≡	10	W 5	W 5	W 5
27	98.8	98.3	99.4	98.8	5.3	7.0	7.7	6.9	8.0	4.7	97	94	91	94	0.3	0.6	0.9	0.6	10	10	9	W 8	W 7	W 5
28	96.4	94.4	90.4	93.7	7.4	7.4	8.0	7.7	11.6	6.6	94	91	92	92	0.6	0.9	0.9	0.8	9	10	10 ●	W 7	W 7	W 10
29	91.3	98.1	107.4	98.9	5.3	0.3	-2.4	0.2	8.5	-2.5	84	67	68	73	1.4	2.0	1.6	1.7	7	7	8	NW 7	N 8	NNE 5
30	113.1	112.2	112.2	112.5	-7.1	-1.4	-3.1	-3.7	-0.9	-7.5	85	72	90	82	0.5	1.5	0.5	0.8	0	7	9	NW 2	NNW 2	N 2
31																								
M	99.0	99.3	100.2	99.5	3.4	5.8	4.1	4.4	7.1	2.3	92	82	90	88	0.6	1.8	0.8	1.1	7.4	8.4	7.6	3.2	3.4	3.4

Grudzień – Décembre

1	111.3	109.5	105.9	108.9	-3.2	-2.0	-2.5	-3.0	-1.4	-5.8	90	68	95	84	0.4	1.7	0.3	0.8	6	9	10 ✳	C 0	W 3	W 7
2	105.6	106.9	107.4	106.6	0.2	1.6	1.2	1.0	2.2	-2.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	WNW 1	NW 1	NNW 1
3	104.5	102.6	103.5	103.5	1.2	2.4	3.2	2.5	3.6	0.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ● ≡	10 ≡	WNW 2	WNW 1	N 1
4	103.8	103.0	102.4	103.1	1.7	2.5	2.6	2.4	3.7	1.5	100	96	93	96	0.0	0.3	0.6	0.3	10 ≡	10	10	NW 1	WNW 3	WNW 3
5	101.0	102.2	104.3	102.5	4.6	4.4	4.3	4.4	5.0	2.5	100	87	90	92	0.0	1.1	0.8	0.6	10 ≡	9	10	NW 4	WNW 6	NW 3
6	106.3	105.8	102.0	104.7	1.9	3.8	-0.8	1.0	4.7	-1.0	98	76	100	91	0.1	1.7	0.0	0.6	8	6	0 ≡	WNW 1	S 1	S 2
7	95.6	91.9	84.7	90.7	-0.5	0.1	-0.4	-0.3	0.8	-1.6	88	88	84	87	0.7	0.8	0.9	0.8	0	10	10	S 4	WSW 3	SW 4
8	69.9	61.4	59.4	63.6	1.4	4.0	6.6	4.6	10.1	-0.7	96	100	74	90	0.3	0.0	2.5	0.9	10 ●	10 ●	1	SW 7	SW 8	W 12
9	56.8	69.7	78.6	69.0	4.2	2.0	-1.8	0.6	7.6	-1.9	93	73	86	84	0.5	2.0	0.8	1.1	10	9	7	WNW 6	W 10	WSW 3
10	76.7	77.8	87.7	80.7	-3.5	0.5	-5.6	-3.6	0.8	-6.1	85	94	95	91	0.7	0.3	0.2	0.4	7	10 ✳	0	SSW 2	W 5	W 2
11	84.9	80.8	77.1	80.9	-7.2	-2.2	-2.2	-3.4	-0.9	-7.9	88	85	85	86	0.4	0.9	0.8	0.7	2	6	4	SE 2	SE 4	ESE 5
12	74.4	74.7	73.7	74.3	-2.0	2.6	-0.5	-0.1	4.2	-3.0	94	79	96	90	0.4	1.6	0.3	0.8	10	1	0	E 5	BSE 2	E 3
13	71.2	68.0	64.3	67.8	-1.2	-0.2	-0.4	-0.6	1.8	-1.7	99	100	100	100	0.1	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	NE 1	NNE 2	N 1
14	65.5	72.3	82.6	73.5	0.4	0.2	-0.8	-0.2	1.0	-0.8	100	100	97	99	0.0	0.0	0.2	0.1	10 ● ≡	10 ✳	10 ✳	NW 2	N 1	NE 2
15	94.6	100.7	105.7	100.3	-5.6	-6.1	-10.2	-8.0	-0.5	-10.2	79	73	81	78	0.8	1.0	0.5	0.8	10	8	0	NE 5	NE 4	E 2
16	106.8	107.1	105.7	106.5	-12.3	-9.9	-12.3	-11.7	-9.6	-13.3	93	81	81	85	0.2	0.5	0.4	0.4	0	1	0	E 3	ENE 3	SE 7
17	102.4	101.8	101.4	101.9	-15.0	-10.7	-9.4	-11.1	-9.3	-15.0	87	87	91	88	0.2	0.4	0.3	0.3	0	10	10	SE 2	ESE 1	SSE 1
18	102.7	103.0	102.7	102.8	-7.4	-5.4	-5.0	-5.7	-4.6	-9.4	96	95	98	96	0.1	0.2	0.1	0.1	10	10	10 ≡	WSW 1	WSW 1	SE 2
19	102.4	104.6	108.7	105.2	-4.2	-1.8	-0.1	-1.6	0.0	-5.0	96	94	100	97	0.2	0.3	0.0	0.2	10	10	10 ≡	SE 1	SSE 2	SW 1
20	112.3	112.3	110.5	111.7	1.0	2.8	-0.4	0.8	3.2	-0.6	100	89	94	94	0.0	0.8	0.3	0.4	10 ≡	2	0	W 3	SW 2	SSW 4
21	105.8	105.8	107.1	106.2	0.8	2.4	1.4	1.5	3.0	-1.0	75	73	100	83	1.6	2.0	0.0	1.2	9	9	10 ●	SSW 7	SSW 8	SW 6
22	105.4	105.2	103.6	104.7	1.0	2.0	1.2	1.4	2.6	0.9	100	98	100	99	0.0	0.2	0.0	0.1	10	10	10 ≡	SW 1	SW 3	SSW 2
23	98.8	96.7	99.0	96.8	-3.5	-1.1	-3.1	-2.7	1.4	-4.1	94	83	86	88	0.3	0.9	0.7	0.6	0	0	0	SSE 1	S 3	SE 3
24	94.3	93.1	96.6	95.4	-3.4	0.4	-3.4	-2.4	1.3	-4.3	83	63	83	76	0.8	2.3	0.8	1.3	6	7	0	S 3	SSW 3	S 2
25	96.5	96.3	99.6	97.5	-3.9	-0.4	-0.2	-1.2	1.7	-4.3	83	80	80	82	0.7	1.2	1.2	1.0	4	8	1	S 3	S 3	SSW 3
26	102.5	104.2	105.9	104.2	0.2	3.2	3.0	2.4	3.7	-0.4	74	74	81	76	1.6	2.0	1.3	1.7	9	1	10	SW 3	W 2	WSW 1
27	105.4	104.7	103.5	104.5	0.8	3.0	1.6	1.8	3.8	-0.3	92	84	91	89	0.3	1.2	0.7	0.8	8	8	0	SW 2	SW 2	SW 2
28	98.2	95.0	90.8	94.7	0.4	2.3	1.4	1.4	3.2	-0.3	96	86	92	91	0.3	1.0	0.6	0.6	10	9	10	SW 3	SW 4	SW 6
29	89.2	87.4	82.0	86.2	1.8	2.8	3.6	3.0	3.8	0.6	93	88	73	85	0.6	1.0	2.1	1.2	10	10	9	WSW 6	SW 6	SW 14
30	80.2	78.0	78.0	78.7	1.6	3.3	1.0	1.7	4.3	0.7	96	88	94	93	0.3	0.9	0.4	0.5	10 ●	9	10	SW 10	W 9	W 6
31	81.1	81.2	81.6	81.3	0.9	0.9	1.2	1.0	1.8	0.2	88	96	92	92	0.7	0.2	0.5	0.5	9	9	7	W 5	SW 5	WSW 6
M	93.8	93.7	93.9	93.8	-1.6	0.2	-0.9	-0.8	1.7	-3.0	92	86	91	90	0.4	0.8	0.6	0.6	7.7	7.8	6.1	3.1	3.6	3.8

Zielona Góra — H_s = 176 m — H_b = 174,0 m — h_w = 16 m — Listopad - Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	–	•⁰ 19²⁵–20⁰⁷ : = 14⁰–9³⁰ 21³⁰–24
2	7	.	.	–	= 0⁰⁰–8³⁰ : ⌴ 6³⁰–11⁵⁰ : ⌣ 17¹⁵–18¹⁰
3	7	.	.	–	= 6²⁰–9⁴⁵ : 22¹⁵–24 . ⌴ 6⁰⁰–8⁰⁰ ∩ –11⁰⁰ ∩ ⁰ 23¹⁰–24
4	6	.	.	–	= 0⁰⁰–9²⁰ ∞ –18⁵⁰ = –24 . ∩¹ 0⁰⁰–10⁵⁰ : ⌣ 17¹⁰–24
5	6	.	.	–	= 0⁰⁰–12³⁵ ∞ –15²⁰ = –24 . ∩° 3⁰⁰–11¹² : ⌣ 0⁰⁰–4¹⁵ . 17⁰⁰–24
6	6	.	.	–	= 0⁰⁰–20³⁰ : ∩ 5⁵⁰–11⁰⁰ : ⌣ 0⁰⁰–3⁵⁰
7	6	1.4	.	–	▽ 10³⁰–11⁴⁵ : •⁰ 23⁰⁰–24 . = 8⁴⁵–24 : ∩ 2⁰⁰–9⁵⁰
8	4	0.7	.	–	•⁰ 0⁰⁰–1⁵⁹ •¹⁻⁰ 2⁰⁵–5¹² •⁰ 20⁵⁰–21¹⁰ : = 0⁰⁰–2⁴⁵ ≡⁰–5¹⁵ ≡¹–10²⁰ ≡⁰–12⁵⁰ = –15⁴⁵ ≡⁰–16⁰⁴ ≡¹⁻² 22⁰⁰ = –24
9	4	1.8	.	–	•⁰ 5⁴⁵–6¹⁰ •⁰ 9²⁰–14⁰⁰ : = 0⁰⁰–1³⁵ ≡¹–5⁴⁵ = –6¹⁰–14²⁰ ≡⁰–22⁵⁰ ≡¹–24
10	4	0.0	.	–	•⁰ 0⁴⁵–1³⁵ : ≡¹ 0⁰⁰–4⁵ ≡²–2²⁰ ≡¹–7⁰⁵ ≡⁰–7²⁰ = –9⁴⁰ ≡⁰–9⁵⁵ ≡¹–11⁴⁸ ≡⁰–12⁵⁰ = –24
11	6	0.2	.	–	•⁰ 3²⁰–5⁰⁵ 19⁰⁰–21¹⁷ : ≡⁰ 0⁴⁰–2³⁵ = –11³⁰ 17⁵⁰–22⁵⁴
12	6	0.0	.	–	•⁰ 0⁰⁸–29 •⁰ 6³²–40 •⁰ 11⁴⁵ 12³⁰ •⁰ 12⁴⁰–14⁴⁰ •⁰ 15⁵⁰ 17¹⁵ : = 4³⁰–24
13	7	.	.	–	= 0⁰⁰–7³⁰
14	6	.	.	–	= 6⁴⁰–24
15	2	0.0	.	–	= 0⁰⁰–6⁴⁰ ≡¹–24
16	4	0.0	.	–	•⁰ 11⁴⁵–14³⁸ : ≡¹⁻⁰ 0⁰⁰–12⁴⁰ = –14²⁰ ≡¹–24
17	4	.	.	–	≡⁰ 0⁰⁰–8³⁵ = –24
18	6	.	.	–	≡⁰ 0⁴⁰–6²⁰ = –24
19	6	.	.	–	= 0⁰⁰–2¹⁰⁰
20	7	.	.	–	⌴⁰ 6²⁰–7⁵⁰
21	7	.	.	–	∞ 15³⁰–18²⁰ : ⌴⁰ 5⁵⁰–10⁰⁰
22	7	.	.	–	= 14⁰⁵–24 : ⌴⁰ 6¹⁵–11³⁰
23	5	0.5	.	–	✳ 8²² 9¹⁵ •⁰ 10⁴⁵–11¹⁵ ••¹⁻² 12²⁰ •¹–14³⁵ : = 0⁰⁰–3³⁰
24	6	0.2	.	–	•⁰ 16²⁷..45 18⁵⁰ 20¹⁰ 20⁵⁰ 22²⁰ : = 2⁵⁰–5³⁵ ≡⁰–6¹⁰ = –24 ⌴⁰ 1⁰⁰– na
25	3	1.7	.	–	•• ⁰ 3⁴⁵–9¹⁵ •¹–10²⁶ •⁰–12¹⁷ •⁰ 13⁴²–15⁴⁵ •¹–21⁰⁵ : = 0⁰⁰–12⁵⁰ ≡⁰¹–24
26	3	0.6	.	–	•⁰ 4⁰⁵–15⁴⁵ •¹ 16⁵⁰–18⁵⁹ •⁰ 23⁴⁰–24 : ≡⁰¹ 0⁰⁰–20³⁰ = –24
27	5	0.7	.	–	•⁰ 0⁰⁰–5¹⁸ 7⁰⁵ 8³⁷ 9⁴⁵–10³⁰ 22³⁵–24 : = 0⁰⁰–18²⁰ 23²⁰–24
28	6	1.9	.	–	•⁰ 0⁰⁰–1⁴⁵ •⁰–2⁵⁰ ••⁰–3²⁰ •⁰–3⁴⁵ ••⁰–6⁰⁵ •⁰ 8³⁰–9³⁵ ••⁰–10¹⁵ •⁰ 10³⁰ 12⁰⁵ 15⁰⁹–16⁴⁵ ••⁰–18⁰⁵ •⁰–22⁰⁵ : = 0⁰⁰–3²⁰
29	8	1.1	.	–	• 7⁰³–22 ✳ ▽ 11⁵⁰–12¹⁰ 14³⁵–42 15⁴⁵–16⁰³ ⅄⁰✳ 21⁴⁵–22⁰⁰ ⅄⁰✳ 22⁵⁴–23¹⁸ [28.XI: = –6⁴⁰ = –22²⁰
30	8	0.4	.	–	✳ ▽ 13³⁵–14⁴⁵
31					
Σ	–	11.2	–	–	UWAGI.

Grudzień - Décembre

1	7	2.4	1	–	✳⁰ 14²⁵–22⁰² △⁰△ –23⁴⁰ ✳⁰–24 . = 0²⁰–6²⁰ 14¹⁵–24 : ⌴¹ 1⁴⁵–11⁰⁰
2	2	0.3	3	–	✳⁰ 0⁰⁰–5⁰ 2⁰⁵–4⁰⁰ 7⁴⁵–8³⁵ 10⁰³–17 •⁰ 17⁵⁰–18²⁰ : = 0⁰⁰–1⁴⁰ ≡⁰¹–3³⁰ ≡²–12⁴⁷ ≡¹–15¹⁵ ≡²–24
3	1	1.0	0	–	•⁰ 0³⁰–1²⁰ 6⁰⁷–7⁰⁰ 8⁴⁵–24 ≡² 0⁰⁰–20⁴⁰ ≡¹–22²⁰ ≡²–24
4	5	1.9	.	–	•⁰ 0⁰⁰–1⁴⁵ 7⁰⁰–10¹⁰ : ≡² 0⁰⁰–4³⁰ ≡¹–10⁴⁵ = –24
5	6	.	.	–	•⁰ 0⁰⁵–3¹⁰ •⁰–6⁰⁵ : = 0⁰⁰–3⁴⁰ ≡²–6³⁰ ≡¹–7³⁵ = –14⁴⁰
6	7	.	.	–	= 1¹⁰–2⁵⁵ ≡⁰–6⁴⁰ = –7³⁵ ≡⁰–9⁴⁰ = –10²⁰ 18²⁰⁻⁵⁰ ≡⁰–19³⁰ ≡¹–21¹⁵ ≡⁰–22⁴⁵ = –24 : ⌴ 22²⁰–24
7	6	0.7	.	–	✳ 23⁰⁵–20⁰ : = 0⁰⁰–4²⁰ 7¹⁵–23²⁰ ⌴ 0⁰⁰–12⁰⁰
8	6	10.0	.	–	✳⁰ 2²⁰–2⁸ 3⁴⁰–6¹⁰ •⁰ 6²⁰–13¹⁵ •¹–14⁴⁵ •⁰–16⁰⁶ •¹ 17⁴⁵–18²⁰ . = 6²⁰–15²⁵
9	8	0.7	.	–	•⁰ 2²⁵..55 3⁰⁰–4⁴⁵ 5¹⁵–8¹⁰ ✳ ▽ 15²⁹–3⁴ : = 6¹⁰–7³⁰ ▽ 20⁴⁰–24
10	5	0.7	.	–	✳⁰ 10³⁰–11⁰⁵ ✳¹⁻²–11³⁹ ✳⁰–13⁵⁵ . = 10⁰⁵–14⁰⁰ : ⌴ 1⁵⁰–11⁰⁰ : ▽ 0⁰⁰–6⁴⁰
11	7	.	1	–	= 19³⁰–24 : ▽ 22³⁰–24
12	7	.	1	–	= 0⁰⁰–11²⁰ 15¹⁵–24 : ▽ 0⁰⁰–10⁵
13	1	0.4	pł.	–	= 0⁰⁰–4⁵⁰ ≡⁰–5²⁵ ≡¹–10²⁵ ≡²–24 : ▽ 3⁴⁵–4²⁰ : ⌴ 6²⁵–12⁰⁰
14	4	13.0	.	–	•⁰ 3⁵⁰–7⁰⁵ •⁰–11¹⁵ ✳ 11⁴⁵–24 . ≡² 0⁰⁰–10¹⁵ = –24 : ⌒ 3⁵⁰–11¹⁵
15	7	.	12	–	✳⁰¹ 0⁰⁰–4⁴⁰ : = 0⁰⁰–5¹⁵ : ⊕ 10⁵⁵–11²⁰ . 13⁵⁰–14¹⁵
16	7	.	11	–	⌣ 5⁰⁰–7⁰⁰
17	7	0.0	10	–	⅄⁰ 22⁵⁰–24 : = 19⁰⁵–24
18	4	0.3	10	–	⅄⁰ 0⁰⁰–1²⁰ •⁰ 3⁰⁵–4⁰⁰ 7⁴⁰–12²⁰ : = 0⁰⁰–15⁵⁵ ≡⁰–24
19	5	0.0	9	–	•⁰ 21²⁰–24 . ≡⁰ 0⁰⁰–1⁰⁰ = –20⁴⁵ ≡⁰–21²⁰ ≡¹–24
20	6	.	8	–	•⁰ 0⁰⁰–40 5⁴⁵–6³⁵ : ≡¹ 0⁰⁰–6⁴⁰ ≡⁰–9⁰⁰ = –24
21	7	0.7	5	–	•⁰ 15²⁵–40 17⁰⁵ 22⁴⁵ •⁰–24
22	5	0.1	2	–	•⁰ 0⁰⁰–10 1¹¹⁵ 12²⁰ 17¹⁵–21³⁰ . = 2¹⁰–11¹⁵ ≡¹⁻⁰ 15³⁰–22⁴⁵ = –24
23	7	.	pł.	–	= 0⁰⁰–1⁵⁵ ≡⁰–2³⁵ = –3⁵⁰ ≡⁰–4³⁰ = –13⁰⁰ : ⌴ 8⁰⁰–14⁰⁰
24	7	.	pł.	–	
25	7	.	pł.	–	
26	6	.	pł.	–	= 12⁰⁰–15¹⁵ ≡⁰–18²⁰ = –24
27	6	.	pł.	–	= 0⁰⁰–24
28	6	2.6	pł.	–	•⁰ 19⁵⁹–20⁰⁰ •⁰–24 . = 0⁰⁰–24
29	6	4.0	.	–	•⁰ 0⁰⁰–5⁰ ✳⁰ 21³⁸–22¹⁰ : ≡⁰ 0⁰⁰–3³⁵ = –18⁰⁰ 21³⁸–24
30	6	9.2	.	–	•⁰ 0⁰⁰ 2⁰⁵ 3²⁰–7²⁵ ✳⁰–8⁰⁰ •⁰–9¹⁰ 10⁰⁰–12¹⁰ 13⁴⁰–14¹⁰ ✳⁰–14²⁶ •⁰–14⁴⁰ 16¹⁰–18¹⁵ ▽¹–18⁴⁵ . = 0⁰⁰–24
31	6	6.1	1	–	✳ 0⁰⁵–5⁰ 12⁰⁰–25 13²³–26 ✳⁰¹ 22⁴⁴–24 : = 0⁰⁰–7²⁰ 12²⁵–18²⁰ 21¹⁰–24
Σ	–	36.1	–	–	UWAGI.

Łódź – Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$

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DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	93.6	93.0	93.2	93.3	-2.8	-1.0	-0.6	-1.2	-0.4	-4.7	93	93	89	92	0.4	0.4	0.6	0.5	10 ☁	10	10	SE 4	ESE 3	ESE 3
2	90.1	89.8	94.1	91.3	-0.2	2.5	0.8	1.0	2.9	-2.1	90	82	90	87	0.6	1.3	0.7	0.9	10	9	10	ESE10	SE 7	WSW 3
3	98.1	99.5	99.8	99.1	0.5	1.2	1.1	1.0	1.4	-1.5	96	90	96	94	0.2	0.7	0.2	0.4	10	10	10	SW 2	SE 2	SE 2
4	100.2	101.8	102.9	101.6	-5.9	-0.2	-3.0	-3.0	1.2	-6.6	94	94	93	94	0.2	0.4	0.4	0.3	0 ≡	2 ⊙	0	C 0	SSW 1	S 4
5	101.2	97.5	94.1	97.6	-2.6	2.2	2.6	1.2	2.6	-5.2	93	84	98	92	0.3	1.2	0.2	0.6	2	10	10 ●	S 5	S 8	SSW 8
6	91.0	88.1	89.8	89.6	4.4	6.4	4.6	5.0	7.8	1.9	95	97	87	93	0.5	0.3	1.1	0.6	10	10 ●	3	SSW10	SW 10	W 9
7	93.5	98.1	103.6	98.4	3.6	4.8	3.7	4.0	4.8	2.2	80	76	82	79	1.6	2.0	1.5	1.7	10	9	9	W 12	WNW12	WNW10
8	105.3	103.2	102.1	103.5	2.8	3.5	4.8	4.0	4.8	2.1	96	90	92	93	0.3	0.8	0.7	0.6	10 ●	10 ☁	10 ☁	W 7	WSW 8	W 10
9	100.5	98.5	96.5	98.5	5.6	6.1	6.0	5.9	6.7	4.1	92	91	83	89	0.7	0.8	1.6	1.0	10	10	10	WSW 7	SW 7	W 7
10	91.5	90.4	90.6	90.8	4.8	2.6	2.2	3.0	6.2	1.4	78	91	91	87	1.9	0.7	0.7	1.1	10	10 ●	10	WSW 5	WSW 8	WSW 8
11	92.0	94.0	96.6	94.2	0.8	1.4	0.9	1.0	2.4	0.4	86	83	85	85	0.9	1.1	1.0	1.0	10	9	10	W 8	WNW 8	WNW 9
12	93.6	87.7	82.1	87.8	-1.2	0.2	0.2	-0.2	1.0	-2.1	89	98	94	94	0.6	0.1	0.4	0.4	10	10 ✳	10	W 9	SW 8	SSW 8
13	80.2	82.9	86.8	83.3	0.0	0.5	0.2	0.2	0.6	-0.9	98	100	98	99	0.1	0.0	0.1	0.1	10 ✳	10 ≡	10 ✳	SW 5	SW 4	C 0
14	94.1	98.7	103.0	98.6	-2.8	-5.5	-6.5	-5.3	0.3	-8.7	93	90	89	91	0.4	0.4	0.4	0.4	10 ✳	10	10	NE 8	NE 8	NE 9
15	103.3	102.0	102.3	102.5	-7.3	-6.2	-8.9	-7.8	-6.2	-9.5	88	86	83	86	0.4	0.5	0.5	0.5	10	2	9	NE 8	NE 7	NE 6
16	105.6	107.3	109.4	107.4	-14.2	-10.1	-14.9	-13.5	-8.9	-15.9	87	78	78	81	0.3	0.6	0.4	0.4	0	0 ⊙	0	NE 3	NE 2	N 1
17	109.1	108.9	109.0	109.0	-13.3	-7.2	-4.4	-7.3	-4.3	-17.3	84	90	93	89	0.4	0.3	0.3	0.3	5	10 ✳	10 ☁	WNW 1	WSW 4	W 4
18	107.3	106.7	105.7	106.6	-5.9	-4.6	-5.3	-5.3	-4.2	-6.4	100	93	95	96	0.0	0.3	0.2	0.2	10 ≡	10 ≡	10 ≡	WNW 5	W 5	W 4
19	105.3	106.8	108.1	106.7	-4.6	-3.0	-2.8	-3.3	-2.4	-6.2	93	97	97	96	0.3	0.1	0.1	0.2	10 ☁	10	10	WNW 2	WNW 3	WNW 2
20	107.1	106.5	103.9	105.8	-3.0	-2.6	-3.4	-3.1	-2.0	4.2	97	95	94	95	0.1	0.2	0.3	0.2	10	10	10	W 5	WSW 6	WSW 7
21	100.9	101.0	102.2	101.4	-6.3	-1.7	-5.5	-4.8	-0.9	-8.3	81	71	77	76	0.7	1.6	0.9	1.1	6	2	0	SW 5	SW 6	SW 4
22	102.1	100.9	97.9	100.3	-9.9	-2.6	-5.5	-5.9	-1.8	-10.3	84	79	72	78	0.4	1.1	1.1	0.9	0	5 ⊙	0	S 3	S 3	SSW 4
23	97.9	98.1	96.4	97.5	-9.7	-2.4	-6.3	-6.2	-1.4	-10.4	81	65	76	74	0.5	1.8	0.9	1.1	0	0	0	SSW 3	SSE 2	SSE 2
24	91.3	88.7	87.6	89.2	-3.6	-2.0	-1.9	-2.4	-1.5	-8.2	71	71	85	76	1.4	1.6	0.8	1.3	9	9	10	SE 7	E 6	SE 3
25	86.4	87.3	91.0	88.2	-1.0	0.3	0.8	0.2	1.3	-2.2	93	79	90	87	0.4	1.3	0.7	0.8	10 ✳	9	10 △	SW 3	SW 5	SW 4
26	96.2	97.7	96.4	96.8	0.6	2.6	-0.6	0.5	2.7	-2.0	94	81	85	87	0.4	1.5	0.8	0.9	10	0 ⊙	0	SW 3	SSW 3	S 4
27	91.9	93.3	97.6	94.3	0.9	2.2	1.2	1.4	4.4	-3.1	94	95	90	93	0.4	0.4	0.7	0.5	10 ●	10	0	SSW 9	SW 6	WSW 5
28	95.8	99.3	106.5	100.5	-0.6	0.8	0.5	0.3	1.7	-1.5	90	94	94	93	0.6	0.4	0.3	0.4	6	10 ✳	10	SSW 4	WNW 6	NW 2
29	109.1	108.5	106.2	107.9	0.0	1.3	0.9	0.8	2.3	-0.6	98	83	87	89	0.1	1.1	0.9	0.7	10	8	8	WSW 2	SW 6	SSW 3
30	102.7	100.1	98.4	100.4	-1.4	4.6	1.2	1.4	5.3	-2.3	94	76	90	87	0.3	2.1	0.7	1.0	4	7	10	S 4	SSW 3	SW 3
31	99.5	101.1	100.7	100.4	1.7	1.8	1.4	1.4	2.1	0.3	100	98	98	99	0.0	0.2	0.2	0.1	10 ☁≡	10 ≡	10	S 2	SSW 4	SE 2
M	98.0	98.0	98.5	98.2	-2.3	-0.1	-1.2	-1.2	0.9	-4.1	90	87	89	89	0.5	0.8	0.6	0.6	7.8	7.8	7.4	5.2	5.5	4.8

Luty – Février

1	96.6	96.4	97.1	96.7	1.8	2.8	2.5	2.4	3.2	0.7	96	91	96	94	0.3	0.7	0.3	0.4	10	10 ☁	10 ●	SSE 4	SSE 4	S 5
2	108.5	101.7	103.7	104.6	4.9	7.2	4.3	5.2	7.3	1.8	97	93	98	96	0.3	0.8	0.1	0.4	10	10	10 ≡	SW 5	SW 4	C 0
3	103.3	102.0	104.8	103.4	3.0	4.1	1.0	2.3	4.4	0.6	100	98	100	99	0.0	0.2	0.0	0.1	10 ≡☁	10 ●	10 ≡	C 0	ENE 3	SE 3
4	104.1	101.2	100.4	101.9	-0.2	3.4	2.2	1.9	5.4	-1.5	100	95	95	97	0.0	0.4	0.4	0.3	9	9 ⊙	0	SE 6	SE 4	WSW 2
5	100.7	99.9	97.9	99.5	0.0	7.0	3.8	3.6	7.1	-0.6	96	75	85	85	0.2	2.4	1.2	1.3	0	8	0	C 0	S 4	SSE 3
6	95.3	91.8	91.6	92.9	1.2	9.2	2.8	4.0	9.6	0.3	94	69	88	84	0.4	3.6	1.0	1.7	0	2	0	SSE 4	SSW12	SSW 8
7	92.5	94.3	95.1	94.0	4.3	6.2	4.3	4.8	7.6	1.9	97	83	88	89	0.3	1.6	1.0	1.0	10 ●	8	9	WSW 4	W 7	WSW 6
8	92.4	87.3	83.0	87.6	1.4	6.4	5.2	4.6	6.9	-0.6	94	84	92	90	0.4	1.6	0.7	0.9	0	10	10 ●	S 4	SSW 6	SSW 8
9	80.0	79.7	82.1	80.6	5.8	7.8	6.2	6.5	8.4	4.3	95	87	86	89	0.4	1.4	1.3	1.0	10 ●	9	9	SW 6	WSW 8	W 9
10	84.1	85.2	85.2	84.8	2.6	5.7	4.7	4.4	6.2	1.2	84	61	95	80	1.2	3.6	0.4	1.7	9	5	10	W 6	W 8	WSW 2
11	85.2	87.4	90.7	87.8	4.0	4.3	3.0	3.6	5.0	2.4	92	90	91	91	0.6	0.8	0.7	0.7	10 ●	10 ●	9	WSW 3	W 8	W 6
12	90.8	87.9	84.6	87.8	0.6	5.8	4.2	3.7	6.3	0.1	98	68	75	80	0.1	2.9	2.0	1.7	9	8	10	SSW 3	SSE 6	SSE 5
13	80.7	78.0	70.8	76.5	3.2	8.6	5.8	5.8	8.8	2.2	93	64	65	74	0.5	4.1	3.2	2.6	10 ●	6 ⊙	10	SSW 5	SSW 9	S 10
14	66.6	67.3	67.3	67.1	5.6	8.8	6.8	7.0	8.8	3.4	77	68	75	73	2.1	3.6	2.5	2.7	6	9	9	SSW 8	S 9	SSW 5
15	68.8	67.4	63.5	66.6	2.7	8.8	6.1	5.9	8.8	1.5	82	54	89	75	1.3	5.2	1.0	2.5	5	6 ⊙	10 ●	S 6	SSE 7	SSE 8
16	68.9	73.9	78.6	73.8	3.6	6.4	2.6	3.8	6.4	2.6	93	72	91	85	0.5	2.7	0.7	1.3	10	7	10	W 9	WSW 8	SW 5
17	83.3	84.9	84.7	84.3	0.6	5.3	4.0	3.5	5.8	-0.4	94	68	82	81	0.4	2.9	1.5	1.6	2	6 ⊙	3	SW 4	SW 6	SSW 6
18	86.1	83.0	75.6	81.6	-0.3	3.6	5.6	3.6	6.2	-1.2	92	83	85	87	0.5	1.3	1.4	1.1	9	10 ●	10 ●	ESE 3	ESE 7	E 7
19	73.4	83.0	89.6	82.0	3.2	2.8	1.6	2.3	6.5	0.3	90	81	69	80	0.8	1.5	2.2	1.5	10 ●	9	0	WNW12	WNW10	W 6
20	91.5	89.9	87.8	89.7	-0.3	5.9	4.2	3.5	7.3	-0.9	92	60	82	78	0.5	3.8	1.4	1.9	5	10	10	S 4	S 9	SSE 6
21	85.4	86.4	90.1	87.3	1.6	8.8	4.0	4.6	9.0	1.1	87	62	88	79	0.9	4.3	0.9	2.0	5	4 ⊙	10 ●	SE 5	SSW 5	WNW 7
22	92.7	93.3	92.4	92.8	0.6	2.3	-0.7	0.4	4.3	-1.3	90	68	94	84	0.6	2.3	0.4	1.1	10	9	0	NW 7	NW 9	WSW 2
23	92.1	91.7	91.1	91.6	-1.4	1.2	-2.8	-1.4	1.9	-3.7	94	79	97	90	0.3	1.4	0.1	0.6	8	9	0	SSW 3	W 6	C 0
24	86.0	81.1	79.5	82.2	-3.6	0.1	0.0	-0.9	0.4	-6.6	92	88	94	91	0.4	0.8	0.4	0.5	10 ≡	10	10	C 0	ESE 7	ENE 3
25	84.1	84.9	83.9	84.3	-0.2	0.3	-0.2	-0.1	0.7	-1.5	96	88	98	94	0.2	0.7	0.1	0.3	10	10	10	NNW 5	N 3	NE 2
26	88.9	93.5	97.5	93.3	-0.2	-0.1	-0.2	-0.2	0.6	-1.0	98	86	90	91	0.1	0.9	0.6	0.5	10 ✳	10	10	NNW 6	N 7	NW 2
27	100.2	102.1	103.8	102.0	-0.7	-1.4	-2.4	-1.7	0.3	-2.8	75	78	87	80	1.4	1.2	0.7	1.1	10	10	10	E 3	SSE 4	E 3
28	106.4	108.2	110.0	108.2	-2.6	-1.2	-1.4	-1.6	-0.7	-3.7	83	82	92	86	0.9	1.0	0.4	0.8	10	9	0	ENE 3	NNW 4	NNW 4
29																								
30																								
31																								
M	88.9	88.7	88.7	88.8	1.5	4.6	2.8	2.9	5.4	0.0	92	78	88	86	0.6	2.1	1.0	1.2	7.8	8.3	7.1	4.6	6.6	4.8

Łódź – Lublinek

H_s = 184 m H_b = 186,8 m h_w = 11 m

Styczeń – Janvier 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	5	0.0	10	.	* 00⁰⁵ 24⁴⁵ • 04⁰⁵ – 07²⁰ 17¹⁰ – 19³⁰ = 07⁴⁵ – 24
2	6	.	9	.	= 00⁰⁰ – 24
3	5	0.2	9	.	* 07⁰⁰ 11⁴⁰ = 00⁰⁰ – 14²⁰ ≡ 1 – 16⁵⁰ ≡ 0 – 17⁴⁰ = – 24
4	5	.	9	1.5	= 00⁰⁰ – 03⁵⁰ ≡ 1 – 07²⁸ ≡ 0 – 11⁴⁰ = – 24
5	6	5.5	9	.	• 13⁴⁰ – 22¹⁰ = 00⁰⁰ – 22⁴⁵ ≡ 1 – 24
6	6	6.4	4	.	• 08⁴⁵ – 09³⁰ • 1 – 13²⁰ • 0 – 14³⁰ 15⁴⁰ ≡ 1 00⁰⁰ – 03¹⁵ = – 18⁴⁵
7	7	0.4	.	.	• 02³⁰ 03⁵⁰ ▽ 0 16³⁰ – 17⁴⁰
8	5	0.6	.	.	• 04⁴⁵ – 07³⁵ 09⁴⁵ 10³⁰ •• 0 11⁴⁵ – 12⁴⁰ • 0 – 13¹⁰ 16⁴⁸ – 23¹⁵ 24 = 07³⁵ – 24
9	6	.	.	.	• 00⁰⁰ 03¹⁵ – 04⁴⁰ = 00⁰⁰ – 21²⁰
10	6	0.7	.	.	• 09⁴⁰ – 14¹⁰ 22³⁰ 24 = 08⁴⁵ – 14¹⁰ 15⁴⁰ – 19¹⁸
11	7	0.4	.	0.5	• 05⁴⁰ – 06⁰⁰ ▽ 08⁴⁵ – 09⁰² ▽ 1 – 10⁰⁵ ▽ 0 – 11²⁰
12	5	0.7	.	.	* 10⁴² – 12³⁸ 14⁴² – 15⁴³ * 1 – 16³⁸ * 0 – 20³⁴ 21¹² – 24 = 20³⁴ – 21¹²
13	2	3.2	7	.	* 00⁰⁰ – 04²⁵ * 1 – 06²⁰ * 0 – 10⁴⁵ • 0 11²⁰ * 15¹⁰ – 20²⁰ * 1 – 21¹⁵ * 0 – 24 ≡ 1 10⁴⁵ – 14¹⁰ = – 15¹⁰ ≡ 0 19³⁰ – 20¹⁵ ≡ 1 – 21⁵⁰
14	6	0.0	8	.	* 00⁰⁰ – 07³⁰ = 07³⁰ – 15⁴⁰ 13.I: ≡ 0 – 23²⁰
15	6	0.1	8	1.9	* 08⁴⁰ – 10⁴⁵ = 07⁵⁰ – 22³⁰
16	5	.	8	4.7	= 23³⁰ – 24 V 0 17³⁰ – 24
17	5	0.1	8	.	* 08³⁵ 09¹⁵ – 14³⁸ • 0 18¹⁵ – 24 = 00⁰⁰ 22⁴⁵ ≡ 0 – 24 V 0 00⁰⁰ – 24
18	2	0.0	7	.	• 00⁰⁰ – 02⁴⁰ 04³⁰ – 06¹⁰ ≡ 0 00⁰⁰ – 07¹⁵ ≡ 1 – 24 V 0 00⁰⁰ – 24
19	5	0.0	7	.	• 05⁴⁵ – 07³⁰ ≡ 1 00⁰⁰ – 05⁴⁵ = – 24 V 0 00⁰⁰ – 24
20	5	.	7	.	= 00⁰⁰ – 24 V 0 00⁰⁰ – 24
21	7	.	6	5.9	= 00⁰⁰ – 04²⁰ 06¹⁵ – 10³⁵ V 0 00⁰⁰ – 06³⁰ ⌓ 21³⁵ – 23⁵² NNW
22	6	.	5	5.4	= 07³⁰ – 19⁴⁰
23	6	.	4	6.3	= 06²⁵ – 12³⁰ ∞ – 16³⁰ = – 22²⁵
24	6	0.0	3	.	= 07³⁰ – 24 ⊕ 10⁴⁵ – 11²⁰
25	6	0.0	3	.	* 04¹⁵ 05¹⁰ – 06³⁰ 07¹⁰ △ 0 20²⁵ – 23²⁰ = 00⁰⁰ – 24
26	5	0.0	3	3.8	= 00⁰⁰ – 24
27	6	0.7	2	.	* 05⁴⁰ – 06⁴⁰ • 0 – 09⁴⁵ = 00⁰⁰ – 20⁴⁰
28	6	0.1	pż.	.	* 09²⁵ 13³² △ 0 15⁵⁵ – 16¹⁰ * 0 – 16⁴⁵ * 0 – 17⁴⁵ = 06⁴⁰ – 09⁵² 17⁴⁵ – 24
29	7	.	pż.	2.0	= 00⁰⁰ – 04²² 06¹⁸ – 07³⁶ ≡ 1 – 08⁴⁰ ≡ 0 – 09⁵⁰ = – 12²⁰ 16²⁰ – 22³⁰
30	6	0.1	pż.	3.3	= 06²⁰ – 24
31	2	2.2	pż.	.	• 02⁴⁰ – 04³⁵ • 06²⁰ – 07⁴⁵ = 00⁰⁰ – 05²⁵ ≡ 1 – 09³⁰ ≡ 0 – 11¹⁰ ≡ 1 – 16²⁰ ≡ 0 – 18⁴⁵ = – 24
Σ	–	21.4	–	35.3	UWAGI

Luty – Février

1	5	4.4	.	.	• 00⁰⁰–20 • 0 – 04³⁰ •• 0 – 05⁴⁰ • 0 12³⁰ 14³⁰ – 20²² ⊙ 0 – 24 = 00⁰⁰ – 12³³
2	6	2.0	.	.	• 00⁰⁰–40 •• 1 – 13⁵ • 0 – 03⁵⁸ 04¹⁵ – 05³⁰…50 •• 1 15⁴⁰ – 17²⁰ 18⁴⁰ – 19¹⁵ • 23⁰⁵ – 24 = 05⁵⁰ – 15²⁰ ≡ 0 – 16³⁵ ≡ 1 – 24
3	5	2.2	.	.	• 00⁰⁰–210 •• 03⁴⁰–04³⁰ • 0 – 05¹⁵ •• 0 – 08⁴⁰ • 0 – 09³⁰ •• 0 – 12¹⁶ • 0 – 17³⁰ ≡ 1 00⁰⁰ – 04³⁰ ≡ 0 – 12¹⁶ ≡ 1 20⁴² – 24
4	6	0.1	.	.	• 10⁴⁰ – 12¹⁵ 14²⁸ – 17³⁵ ≡ 1 00⁰⁰ – 02⁵⁰ ≡ 0 – 05³⁰ = – 24
5	6	.	.	4.0	= 00⁰⁰ – 24 ⌴ n – a
6	7	4.9	.	7.1	≫ 11⁴⁵ – 15²⁰ = 00⁰⁰ – 11³⁰ ⌴ 1 n – a
7	7	1.7	.	2.4	• 0 00⁰⁰ – 09³⁸ = 09³⁸ – 12²⁵
8	6	8.5	.	.	• 14¹⁰–40 15¹⁵ 17³⁵ 19³⁰ – 24 = 14⁴⁰ – 13³⁰ ⌴ 1 n – a
9	7	1.1	.	.	• 0 00⁰⁰ – 14⁵ • 1 – 05³⁵ • 0 – 06³⁰ • 1 – 07³⁰ • 0 – 08⁴⁰ 15²⁶ – 17³⁰ 18⁴⁰ = 08⁴⁰ – 12⁴⁰
10	7	1.0	.	4.4	• 18⁴⁵ 20²⁰ = 06²³ – 08³⁰ 20²⁰ – 24
11	6	2.0	.	.	• 03³⁵ – 05¹⁵ ▽ 06⁴⁰ – 07⁰⁵ • 0 10⁴⁰ 13⁰⁴ – 16³⁰ = 00⁰⁰ – 19³²
12	6	0.0	.	2.0	= 06²⁵ – 20³⁰ ⌓ 22¹⁵ – 24
13	7	2.9	.	5.2	• 05¹⁵ – 07²⁵ 21²⁵–52 • 1 – 24 ≫ 14²² – 15³⁸ 19¹⁵ – 21¹⁸ ⌓ 0⁰⁰ – 30
14	8	.	.	0.3	• 1 00⁰⁰ – 40 ≫ 3³⁰ – 4⁴⁰
15	7	1.5	.	3.4	• 0 19²⁵ – 23³⁰ = 13⁴⁵ – 19²⁵ 23³⁰ – 24 ⊕ 10⁴⁵ – 11³⁵
16	7	1.6	.	1.2	• 02⁴⁵ – 06³⁵ 08⁴⁶ 09²⁵ ▽ 0 17²⁰ – 18³⁰ ≫ 5²⁰ – 06²⁵ = 00⁰⁰ – 24⁵
17	6	0.9	.	4.2	▽ 0 16⁰⁵ – 48 • 0 18²⁹ 19³⁹ = 00⁰⁰ – 23⁰ 5³⁰ – 21²⁰ ⌴ n – a
18	6	8.6	.	1.7	• 0 11³⁵ 17⁴⁰ 18³⁰ 20³⁵ – 21¹⁵ • 1 – 24 = 3⁵⁰ – 11³⁵ ⌴ 0 n – a
19	6	2.4	.	0.7	• 1 00⁰⁰ – 10 • 0 – 07⁰⁵ • 1 – 7³⁰ * 1 – 9⁴⁰ • 0 – 10⁴⁵ • 1 – 11¹⁰ • 0 – 11⁵⁰ ≫ 6³⁰ – 16⁴⁵ = 11⁵⁰ – 19³⁰
20	7	.	.	6.0	▽ 0 22⁵–45 = 4⁴⁵ – 10³⁰ ⊕ 9³⁰ – 16³⁰
21	7	1.3	.	7.4	• 0 20²⁰ – 24 = 6³⁰ – 9²²
22	7	0.0	.	0.5	• 0 00⁰⁰ – 38
23	6	0.5	.	0.9	▽ 0 6²⁵–28 13¹⁰–30 ▽ 1 14⁰⁰ ▽ 2 14²³ ▽ 0 – 14³⁸ ▽ 1 – 14⁴² ▽ 0 – 15³⁰ = 6¹⁵ – 13¹⁰ 15³⁰ – 19⁴⁵ ≡ 0-1 20³⁵ = – 24
24	6	0.3	pż.	.	* 0 13⁴⁵ – 15²⁵ • 0 – 15⁴⁰ * 0 – 20³⁰ 21³⁵ – 22¹⁵ = 00⁰⁰ – 2³⁸ ≡ 0 – 3⁴⁵ = – 6¹⁵ ≡ 0 – 6²⁵ ≡ 1 – 7⁵⁰ = – 24
25	6	0.1	1	.	△ 0 7⁴⁵ – 11⁰⁰ 14⁰⁵ – 15⁰⁵ = 00⁰⁰ – 8²⁰ ≡ 0 – 9²⁵ = – 24
26	6	0.0	1	.	* 02⁴² – 3³² 6³⁰ – 7⁴⁵ 8³⁰ – 10³⁵ = 00⁰⁰ – 2⁴² 10³⁵ – 15¹⁰ 15⁴⁵ – 24
27	6	0.0	1	.	= 00⁰⁰–30 5⁴⁰ – 24
28	6	0.0	1	0.1	* 0 3³⁸ – 6⁴⁰ 14⁴⁵ – 15⁵⁰ = 00⁰⁰ – 19⁵⁰
29					
30					
31					
Σ	–	48.1	–	51.5	UWAGI

Łódź - Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$

Marzec - Mars 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	111.3	111.6	110.6	111.2	−2.8	−1.5	−0.6	−1.4	0.1	−4.5	91	80	81	84	0.5	1.1	1.1	0.9	10	10 ✳	9	NNW 7	N 8	NNW 6
2	108.8	107.5	104.8	107.0	−1.6	−0.5	−0.6	−0.8	0.0	−2.5	75	76	74	75	1.3	1.4	1.5	1.4	10	10	10	NNW 6	NNW 8	NW 7
3	101.6	100.7	99.0	100.4	−2.4	−3.0	−4.6	−3.6	−0.1	−5.2	82	86	79	82	0.9	0.7	0.9	0.8	8	10	0	N 5	NNE 3	NE 2
4	94.3	91.0	86.9	90.7	−5.3	3.4	2.6	0.8	4.2	−7.4	87	52	62	67	0.5	3.8	2.9	2.4	8	8	10	SSE 4	S 7	SSW 5
5	89.6	91.7	92.4	91.2	−0.4	2.2	−1.2	−0.2	4.4	−1.2	94	73	85	84	0.3	2.0	0.8	1.0	10	5 ⊙	0	WNW 6	WNW 5	NW 3
6	92.4	91.5	90.6	91.5	−3.4	4.4	0.9	0.7	5.7	−4.3	93	48	75	72	0.4	4.4	1.6	2.1	0	1	0	C 0	WNW 3	C 0
7	90.6	92.4	93.2	92.1	−2.3	−0.5	−2.6	−2.0	1.2	−3.3	89	61	87	79	0.6	2.3	0.7	1.2	2	10	0	ENE 4	ENE 6	E 5
8	94.6	95.7	98.2	96.2	−4.3	0.7	−2.0	−1.9	1.8	−5.4	77	63	68	69	1.0	2.3	1.7	1.7	0 ⊙	3 ⊙	5	E 5	E 8	E 7
9	102.9	104.8	107.0	104.9	−5.1	1.2	−1.2	−1.6	2.4	−5.7	88	56	68	71	0.5	3.0	1.8	1.8	0 ⊙	1 ⊙	0	E 5	NE 5	NE 4
10	109.3	110.7	111.0	110.3	−4.2	2.0	−0.4	−0.8	3.9	−5.4	89	61	72	74	0.5	2.8	1.7	1.7	6	0	0	ENE 3	ENE 6	E 4
11	111.3	110.6	108.6	110.2	−3.7	6.2	1.8	1.5	9.2	−5.2	85	57	78	73	0.7	4.1	1.6	2.1	4	0	5	E 3	SE 3	ESE 2
12	104.2	101.0	97.1	100.8	−0.6	11.3	5.3	5.3	13.2	−2.7	65	35	66	55	2.0	8.7	3.0	4.6	8	8	9	SE 2	SW 3	C 0
13	96.1	96.6	94.6	95.8	0.2	12.4	6.8	6.6	14.4	−0.7	82	39	70	64	1.1	8.8	3.0	4.3	8	2 ⊙	4	C 0	WNW 6	WSW 2
14	90.0	86.8	86.8	87.9	3.8	14.0	9.6	9.2	14.8	2.3	77	57	70	68	1.9	6.9	3.6	4.1	2 ⊙	10	9	SW 5	W 9	W 10
15	87.2	88.0	80.0	85.1	6.8	8.3	8.4	8.0	9.7	6.2	78	73	90	80	2.2	3.0	1.0	2.1	10	10	10 ●	W 10	W 10	WSW 10
16	81.0	84.8	93.0	86.3	1.5	2.6	−3.8	−0.9	9.5	−4.6	83	65	60	69	1.1	2.6	1.9	1.9	9	9	5	WNW 7	NW 12	NNW 6
17	93.8	91.0	81.9	88.9	−4.4	−1.5	0.4	−1.3	0.9	−5.6	67	66	96	76	1.4	1.9	0.3	1.2	8	10 ✳	10 ●	NE 2	SE 8	SE 6
18	73.5	73.5	77.6	74.9	7.4	11.5	7.0	8.2	12.2	−0.1	96	70	90	85	0.5	4.1	1.0	1.9	10 ●	8	10	SW 7	W 10	W 9
19	84.3	86.5	86.8	85.9	4.2	8.0	5.4	5.8	8.9	3.3	90	70	97	86	0.8	3.2	0.3	1.4	10	9	10 ●	W 8	W 7	C 0
20	88.6	88.3	84.2	87.0	5.4	9.7	10.3	8.9	12.4	4.5	97	88	80	88	0.3	1.4	2.5	1.4	10 ≡	10	6	C 0	SSE 4	SW 5
21	86.3	89.7	90.7	88.9	8.6	11.7	5.4	7.8	12.6	4.8	84	57	80	74	1.9	5.9	1.8	3.2	4 ⊙	5 ⊙	3	WNW 8	W 8	W 2
22	92.3	94.0	96.2	94.2	2.4	9.7	4.5	5.3	11.1	1.3	87	59	76	74	1.0	4.9	2.0	2.6	2 ⊙	5	0	WSW 2	W 12	NW 2
23	97.2	97.1	98.0	97.4	−0.3	10.4	6.8	5.9	11.7	−1.3	94	49	60	68	0.4	6.5	4.0	3.6	0	4 ⊙	0	ESE 2	SE 1	ENE 6
24	103.1	104.4	103.7	103.7	−0.4	2.6	1.4	1.2	7.1	−0.9	90	60	65	72	0.6	3.0	2.4	2.0	10	10	10	E 10	ESE 12	ESE 12
25	102.4	103.0	103.2	102.9	−0.2	3.4	1.2	1.4	5.2	−1.1	90	75	79	81	0.6	2.0	1.4	1.3	10	10	0	SE 12	SE 10	SE 8
26	101.7	101.0	100.6	101.1	2.4	11.9	6.4	6.8	13.3	0.4	77	50	63	63	1.7	6.9	3.5	4.0	8	8 ⊙	0	SSE 6	S 8	SE 7
27	102.0	101.9	101.0	101.6	3.6	14.3	7.0	8.0	15.2	1.2	63	30	55	49	2.9	11.5	4.5	6.3	2 ⊙	1 ⊙	0	S 7	SSW 9	S 6
28	98.0	96.1	94.2	96.1	3.6	12.7	6.2	7.2	14.0	1.9	49	30	78	52	4.0	10.2	2.2	5.5	7 ⊙	7 ⊙	10 ●	SSW 9	SSW 10	SSW 7
29	91.2	92.1	93.1	92.1	4.4	9.4	8.0	7.4	10.8	2.5	92	70	82	81	0.7	3.6	1.9	2.1	10 ●	6 ⊙	10	S 7	W 6	SE 5
30	94.7	96.2	96.2	95.7	5.2	12.3	9.7	9.2	14.8	3.7	80	51	59	63	1.8	7.0	4.9	4.6	8	9	0	E 4	E 6	E 7
31	98.8	100.4	100.4	99.9	4.5	13.2	9.8	9.3	15.3	2.2	77	52	61	63	1.9	7.4	4.8	4.7	3 ⊙	0 ⊙	0	SSE 3	NE 1	E 3
M	95.9	96.1	95.5	95.8	0.7	6.5	3.5	3.6	8.4	−1.1	83	60	74	72	1.2	4.4	2.1	2.6	6.4	6.4	4.7	5.1	6.9	5.1

Kwiecień - Avril

1	100.1	99.6	98.6	99.4	5.7	16.3	9.6	10.3	17.4	2.7	62	26	54	47	3.5	13.8	5.5	7.6	3 ⊙	1 ⊙	0	E 5	E 9	ESE 7
2	97.8	97.7	98.2	97.9	4.8	18.5	11.8	11.7	19.8	3.0	82	31	56	56	1.5	14.6	6.1	7.4	3 ⊙	2 ⊙	2	E 6	SSE 5	SE 5
3	101.2	102.9	104.6	102.9	7.1	18.5	12.7	12.8	20.0	3.8	70	32	52	51	3.1	14.5	7.1	8.2	5 ⊙	9	0	SSE 2	E 3	E 1
4	106.9	107.0	106.6	106.8	6.8	18.0	10.2	11.3	18.7	2.6	77	45	61	61	2.3	11.4	4.8	6.2	2 ⊙	3 ⊙	0	C 0	N 6	ENE 2
5	105.5	103.8	98.7	102.7	6.0	17.1	11.3	11.4	18.8	2.6	83	39	53	58	1.6	11.9	6.4	6.6	0 ⊙	0 ⊙	0	E 2	N 1	S 2
6	93.0	89.3	85.7	89.3	7.2	19.1	10.7	11.9	20.5	2.6	65	27	58	50	3.6	16.1	5.4	8.4	2 ⊙	1 ⊙	6	SSE 4	W 6	SSW 2
7	87.1	88.2	92.3	89.2	5.2	6.2	5.5	5.6	10.8	4.1	92	83	71	82	0.7	1.6	2.6	1.6	10 ●	10	10 ●	N 5	NNW 6	NE 9
8	96.1	95.0	93.6	94.9	−1.2	5.2	1.2	1.6	6.9	−2.3	84	55	74	71	0.9	3.9	1.8	2.2	9	7 ⊙	6	NE 4	N 6	NW 2
9	90.9	90.2	89.6	90.2	1.8	4.8	3.1	3.2	5.4	−1.8	82	70	61	71	1.3	2.6	3.0	2.3	9	9	9	WNW 3	NNE 3	ENE 3
10	87.4	82.7	76.7	82.3	0.4	10.3	7.4	6.4	12.9	−1.8	55	42	62	53	2.8	7.3	3.9	4.7	4 ⊙	5 ⊙	4	SSE 3	SW 7	SSW 3
11	72.1	73.1	78.9	74.7	3.6	7.5	3.0	4.3	8.7	0.9	88	57	79	75	0.9	4.5	1.6	2.3	7	10	10	NW 3	WNW 5	NW 7
12	85.9	87.6	89.8	87.8	0.2	3.3	2.4	2.1	5.2	−0.7	66	43	56	55	2.1	4.3	3.2	3.2	9	9	9	NW 4	NW 4	C 0
13	91.2	91.3	94.1	92.2	−2.8	6.8	0.6	1.3	7.5	−5.1	95	33	98	75	0.2	6.7	0.1	2.3	3 ≡	8	9	C 0	SW 2	NW 3
14	96.3	96.4	96.4	96.4	−2.4	3.9	0.8	0.8	5.9	−5.4	98	45	58	67	0.1	4.5	2.7	2.4	0 ⊙	6 ⊙	1	C 0	NNW 3	C 0
15	97.2	98.2	100.3	98.6	−0.8	4.7	2.0	2.0	5.9	−4.0	93	53	64	70	0.4	4.0	2.6	2.3	6 ⊙	7	6	C 0	NW 8	N 4
16	101.0	99.4	97.8	99.4	0.8	8.8	7.9	6.4	10.1	−1.4	90	42	75	69	0.7	6.6	2.6	3.3	8	9	10	E 1	W 7	SW 4
17	96.5	97.4	97.6	97.2	6.8	8.8	5.7	6.8	10.1	5.2	96	69	88	84	0.5	3.5	1.2	1.7	10 ●	9	6	W 2	NW 4	N 3
18	96.5	95.3	93.9	95.2	3.0	4.6	3.6	3.7	6.4	2.3	88	82	91	87	0.9	1.5	0.7	1.0	9	10 ●	10 ●	N 6	N 6	NNE 3
19	92.9	91.6	92.4	92.3	2.2	6.5	6.2	5.3	8.3	1.2	95	66	82	81	0.4	3.3	1.7	1.8	10	9	10	N 1	S 2	SSE 3
20	95.0	99.1	102.3	98.8	6.4	7.1	4.0	5.4	10.0	3.4	95	77	83	85	0.4	2.3	1.3	1.3	10 ●	10	0	WNW 5	NW 7	NNE 3
21	103.8	105.2	106.3	105.1	3.2	7.8	5.4	5.4	10.2	0.2	95	67	80	81	0.4	3.5	1.8	1.9	9	8	0	NW 1	NNW 2	C 0
22	108.3	108.0	107.5	107.9	4.6	7.0	4.6	5.2	7.3	1.1	82	80	92	85	1.5	2.0	0.7	1.4	10 ●	10	10 ●	N 2	N 6	N 5
23	106.7	106.5	106.1	106.4	4.2	9.1	8.6	7.6	12.5	3.0	97	87	94	93	0.2	1.6	0.6	0.8	10 ≡	6 ⊙	4	N 2	NNW 4	N 5
24	104.6	103.8	102.0	103.5	7.2	13.3	10.4	10.3	14.7	5.9	91	71	88	83	0.9	4.5	1.4	2.3	10	10	6	NNE 6	N 5	N 5
25	99.3	98.9	98.4	98.9	7.8	14.9	11.1	11.2	17.7	6.6	82	64	94	80	2.0	6.0	0.8	2.9	9	10	10	NNE 4	NE 4	N 6
26	98.2	98.2	97.8	98.1	7.6	14.7	11.7	11.4	16.6	6.2	94	77	89	87	0.6	3.8	1.5	2.0	10	10	3	NNE 3	N 2	N 2
27	95.8	93.5	92.0	93.6	10.0	22.6	15.9	16.1	23.8	7.1	95	39	65	66	0.7	16.6	6.3	7.9	7	4 ⊙	6	N 2	SSE 5	S 7
28	91.2	89.8	88.2	89.7	14.2	22.3	17.7	18.0	23.3	10.0	75	43	60	59	4.1	15.3	8.1	9.2	8	5 ⊙	8	S 3	SSE 4	SE 1
29	89.1	89.9	90.1	89.7	14.7	21.9	16.1	17.2	23.7	9.1	68	48	67	61	5.3	13.8	6.0	8.4	3 ⊙	7 ⊙	0	SSW 2	WNW 3	S 2
30	86.8	85.4	89.3	87.8	12.7	24.7	9.2	14.0	26.0	8.9	86	34	92	71	2.1	20.4	0.9	7.8	5 (R)	9	10 ●	E 1	SW 8	N 10
31																								
M	95.9	95.5	95.5	95.6	4.9	11.8	7.7	8.0	13.5	2.3	84	54	73	70	1.5	7.5	3.1	4.0	6.7	7.1	5.5	2.7	4.8	3.6

Łódź - Lublinek

$H_s = 184\ m$ $H_b = 186{,}8\ m$ $h_w = 11\ m$

Marzec - Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	pż.	2.1	$*^0 7^{30}\ 9^{10}\ 11^{05}\ 13^{30}\ 22^{40}\ 23^{20}$
2	8	0.0	pż.	1.2	$*^0 2^{42}-4^{41}\ 9^{40}\ 10^{02}$
3	7	.	.	0.8	
4	6	0.2	.	5.3	$*^0 23^{25}-24 = 7^{30}-8^{45}\ 12^{40}-20^{30}$
5	7	.	pż.	5.8	$*^0 0^{00}-15\ *^1-135 = 135-6^{40}$
6	8	.	.	8.8	$= 5^{38}-9^{20}\ \sqcup^1 n-a$
7	6	.	.	2.6	$= 5^{30}-14^{20}$
8	8	.	.	9.3	$\sqcup^0 n-a$
9	7	.	.	9.3	$= 5^{30}-9^{30}\ 17^{25}-21^{30}\ \sqcup^0 n-a$
10	7	.	.	9.3	$= 5^{30}-12^{30}\ 17^{40}-24\ \sqcup n-a$
11	7	.	.	9.8	$= 0^{00}-10^{20}$
12	6	.	.	5.2	$= 2^{40}-3^{20}\ 5^{30}-11^{20}\ \infty-19^{30}\ \sqcup^0 n-a$
13	7	.	.	7.5	$= 4^{30}-10^{22}\ 17^{30}-24\ \sqcup^0 n-a$
14	7	.	.	5.1	$\gg 13^{30}-15^{20}\ 20^{30}-24 = 0^{00}-9^{40}\ \infty\ 13^{20}-16^{30}$
15	7	9.6	.	0.3	$\bullet^0 7^{30}\ 8^{35}\ \overset{\bullet}{\nabla}{}^0 11^{20-25}\ 13^{00-15}\ 13^{40}-14^{35}\ \bullet^0 15^{35}-16^{00}\ \bullet^1-17^{27}\ \bullet^0 19^{40}\ 20^{20}-23^{35}\ \bullet^1-24\ \gg 0^{00}-13^{30}\ 19^{35}-24$
16	8	.	.	1.9	$\bullet^1 0^{00}-3^{40}\ \bullet^0-4^{20}\ \gg 0^{00-20}\ 10^{20}-17^{10}$
17	7	7.9	.	.	$*^0 12^{20}-13^{45}\ 14^{40}-16^{15}\ \overset{\bullet}{*}{}^0-19^{35}\ \bullet^0-22^{30}\ \bullet^1-23^{20}\ \bullet^0-24$
18	8	3.2	.	2.0	$\bullet^0 0^{00}-1^{32}\ 1^{40}-4^{40}\ \bullet^1 6^{10}-8^{35}\ \bullet^0-9^{20}\ \overset{\bullet}{\nabla}{}^0 15^{24}-16^{05}\ 17^{45}-18^{30}\ 23^{45}-24\ \gg 10^{30}-15^{45}\ 17^{50}-18^{40}$
19	7	3.5	.	0.5	$\bullet^0 5^{40}-6^{25}\ 16^{45}\ 17^{40}-22^{40} = 22^{40}-24$
20	6	.	.	0.8	$\bullet^0 0^{25}\ 1^{40} = 0^{00-25}\ 1^{40}-4^{40} \equiv^2-7^{35} \equiv^1-8^{25} \equiv^0-9^{33} = -19^{30}$
21	7	0.0	.	8.8	$\overset{\bullet}{\nabla}{}^0 7^{44-57}\ \gg 11^{35}-15^{20}$
22	7	.	.	9.0	$\gg 12^{30}-15^{10}$
23	7	.	.	8.2	$\gg 2^{130}-24 = 5^{40}-8^{15}\ \infty-9^{38}\ \sqcup n-a$
24	7	0.0	.	0.4	$\gg 0^{00}-8^{30}\ \gg-\ \ -24$
25	7	0.0	.	0.8	$\bullet^0 0^{00}-1^{30}$ (marznący) $1^{30-55}\ 3^{45}-4^{30}\ 7^{30}-8^{08}\ \gg-\ \ 0^{00}-8^{10}\ \gg-16^{34}$ (por. do 16 m/sek) $18^{20}\ 20^{15}\ 21^{38}-23^{32}$ **25.III:** $\boxtimes\ 5^{45}-8^{20}$
26	8	.	.	7.3	
27	8	.	.	10.0	$= 5^{15}-7^{30}$
28	7	0.5	.	7.6	$\bullet^0 16^{45}\ 17^{40}-18^{35}\ 20^{20}\ 22^{20}\ \gg 7^{30}-14^{20}$
29	7	0.1	.	1.2	$\bullet^0 0^{15}-8^{32}\ 21^{48}\ 23^{33} = 8^{32}-12^{40}\ 17^{45}-21^{48}\ 23^{30}-24$
30	7	.	.	3.7	$= 0^{00}-2^{32}\ 4^{15}-9^{40}$
31	7	.	.	10.3	$= 8^{38}-10^{26}\ 18^{40}-21^{20}$
Σ	—	25.0	—	154.9	UWAGI

Kwiecień - Avril

1	8	.	.	11.0	$= 5^{46}-7^{50}\ \infty-8^{45}$
2	7	.	.	10.0	$= 4^{30}-8^{30}\ 18^{30}-19^{50}$
3	7	.	.	9.6	$= 4^{40}-8^{30}$
4	7	.	.	11.2	$= 4^{10}-9^{20}\ \infty-10^{20} = 21^{15}-24\ \frown n-a$
5	8	.	.	11.0	$= 0^{00}-2^{20}\ 4^{35}-8^{30}\ \sqcup^0 n-5^{40}$
6	7	1.2	.	11.0	$= 4^{20}-8^{15}\ \infty-10^{31} = 21^{16}-24$
7	7	1.2	.	.	$\bullet^0 5^{45}-6^{30}\ \bullet^1-7^{05}\ \bullet^0-7^{35}\ \overset{\bullet}{\nabla}{}^0 17^{23-35}\ \bullet^0 17^{45}-20^{20}\ 21^{20} = 0^{00}-5^{45}\ 7^{35}-8^{40}$
8	8	.	.	8.3	
9	7	.	.	0.6	$\sqcup n-6^{10}$
10	8	.	.	10.5	
11	8	.	.	0.1	$= 4^{35}-8^{30}$
12	8	0.6	.	4.0	$*^0 22^{45}\ 23^{30}\ *^1-24$
13	7	2.6	1	5.1	$*^1 0^{00-10}\ *^0 0^{40}\ \overset{\bullet}{*}{}^0 14^{45}-15^{08}\ 15^{35-55}\ \overset{\bullet}{\nabla}{}^0-16^{15}\ \overset{\bullet}{\nabla}{}^0-16^{20}\ \overset{\bullet}{*}{}^1-16^{28}\ \overset{\bullet}{*}{}^0\ 16^{45}\ \overset{\bullet}{*}{}^1-17^{15}\ \overset{\bullet}{\nabla}{}^0 17^{50}\ \overset{\bullet}{*}{}^0-19^{08} = 0^{40}-24^{5}$
14	8	.	.	6.6	$= 0^{00-10} \equiv^1-5^{30} \equiv^0-6^{40} = -8^{22}\ 22^{16}-24\ \sqcup^0 n-a$ **13.IV:** $\equiv^1-6^{40} \equiv^0-7^{25} = -8^{10}\ 19^{08}-24$
15	7	0.0	.	5.6	$\Phi\ 11^{17-30} = 0^{00}-8^{30}\ \sqcup^1 n-a$
16	7	2.0	.	4.8	$\bullet^0 23^{45}\ 24 = 5^{35}-8^{25}$
17	8	0.3	.	0.8	$\bullet^0 0^{00...30}-7^{25}\ 8^{40}\ 9^{15}\ \overset{\bullet}{\nabla}{}^0 15^{50}-16^{05}$
18	7	1.6	.	.	$\bullet^0 2^{30}\ 3^{50}\ 12^{25}\ 24 = 4^{00}-7^{25}$
19	7	3.2	.	.	$\bullet^0 0^{00}\ 1^{40}\ 2^{13}\ 6^{25}\ 18^{40}-24 = 6^{25}-8^{30}$
20	7	0.1	.	2.4	$\bullet^0 0^{00}-3^{20}\ 4^{40}-8^{00...25}\ \bullet^0 9^{35}-10^{10}$
21	7	0.5	.	3.4	$= 0^{00}-9^{30}$
22	7	0.9	.	.	$\bullet^0 3^{30}-8^{23}\ 9^{32}\ 16^{43}-21^{16} = 22^{16}-24$
23	6	.	.	4.6	$= 0^{00}-3^{40} \equiv^1-7^{30} = -14^{30}\ 18^{25}-24$
24	6	.	.	0.4	$= 0^{00}-15^{38}\ \frown^1 n-a$
25	6	7.2	.	4.2	$\bullet^0 17^{01-30}\ \bullet^1-17^{58}\ \overset{\bullet}{\nabla}{}^1-19^{25}$; (K) $17^{58}-18^{10}$ S K $-19^{20} = 6^{15}-24$
26	6	0.2	.	3.0	$= 0^{00}-13^{20}\ 19^{33}-24$
27	7	0.0	.	7.1	$\overset{\bullet}{\nabla}{}^0 4^{45}-5^{35}\ \bullet$ (K) $14^{50}-15^{45} = 0^{00}-11^{30}\ 19^{30}-24$
28	8	.	.	9.5	$= 0^{00}-4^{20}\ \frown^1 n-a$
29	8	.	.	9.5	$= 5^{40}-8^{30}\ \frown^0 n-a$
30	7	8.6	.	6.6	$\overset{\bullet}{\nabla}{}^0 15^{08-12}\ 15^{49}-16^{01}\ \bullet^1 16^{35}-19^{45}\ \overset{\bullet}{\nabla}{}^0-21^{11}$ (K) $6^{20}-7^{25}\ 16^{12-35}$ S K $-19^{45}\ \gg 14^{40}-15^{02}\ 20^{22}-21^{30}$
31					**30.IV:** $= 3^{30}-7^{20}\ \frown 5^{45}-6^{15}$
Σ	—	30.2	—	160.9	UWAGI

Łódź – Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$

Maj – Mai 1957

DNI	CIŚNIENIE p = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.4	96.2	96.4	96.0	5.8	10.3	6.7	7.4	11.0	2.5	71	48	60	60	2.6	6.4	4.0	4.3	2 ⊙	6 ⊙	2	NNW 6	N 4	E 3
2	95.9	94.0	92.3	94.1	5.9	10.9	8.1	8.2	12.0	2.0	57	35	67	53	4.0	8.4	3.6	5.3	3 ⊙	8 ⊙	8	E 5	ESE 3	C 0
3	90.9	89.7	87.6	89.4	8.0	12.7	9.4	9.9	14.7	5.1	70	48	66	61	3.2	7.7	4.0	5.0	6	8	4	C 0	E 1	C 0
4	86.1	87.8	89.6	87.8	7.8	9.3	6.0	7.3	10.7	4.1	75	45	54	58	2.7	6.4	4.3	4.5	9	8	5	WSW 8	W 10	W 5
5	90.6	89.7	88.8	89.7	3.3	7.5	4.8	5.1	9.9	−0.1	68	45	59	57	2.5	5.7	3.5	3.9	1	8	10	W 9	W 7	C 0
6	86.5	85.7	86.2	86.1	4.0	4.0	2.1	3.0	7.7	−0.1	72	93	93	86	2.2	0.5	0.5	1.1	10	10 ●	10	SE 4	SE 3	W 4
7	86.0	86.1	85.4	85.8	2.0	4.8	4.0	3.7	6.4	0.8	91	82	92	88	0.7	1.5	0.6	0.9	10	10	9	WNW 3	NW 2	N 2
8	84.5	84.7	87.0	85.4	3.6	5.2	3.6	4.0	5.7	2.4	85	70	88	81	1.2	2.6	0.9	1.6	10	10	10 ●	N 5	NNW 7	NW 3
9	88.9	89.8	88.9	89.2	3.6	4.9	4.9	4.6	5.5	2.5	91	87	94	91	0.7	1.1	0.6	0.8	10	10 ●	10 ●	N 5	N 6	N 4
10	87.0	87.0	89.0	87.7	4.1	7.2	6.7	6.2	8.4	3.0	98	88	94	93	0.2	1.2	0.6	0.7	10 ≡	10	10 ●	NW 5	NW 5	WNW 3
11	91.6	93.4	93.5	92.8	6.2	13.5	10.3	10.1	16.2	5.1	92	53	77	74	0.7	7.3	2.8	3.6	10 ●	6	0	W 4	S 4	NE 2
12	94.3	94.3	94.5	94.4	9.0	19.1	15.5	14.8	20.4	4.6	92	47	60	66	1.0	11.8	7.0	6.6	6	6 ⊙	8	E 3	S 6	S 2
13	95.6	95.6	95.2	95.5	12.9	21.9	16.2	16.8	22.8	7.2	76	41	67	61	3.6	15.5	6.2	8.4	2 ⊙	4 ⊙	8	S 2	S 1	C 0
14	96.2	97.5	98.5	97.4	12.7	19.1	13.9	14.9	20.3	7.3	88	58	77	74	1.8	9.3	3.7	4.9	8	8	2	WNW 4	WNW 7	C 0
15	101.0	100.9	99.4	100.4	13.5	18.9	13.0	14.6	19.8	6.6	78	38	68	61	3.4	13.6	4.8	7.3	0 ⊙	2 ⊙	1	NNE 3	NNW 2	E 2
16	98.3	96.0	93.7	96.0	13.7	21.5	16.9	17.2	22.5	8.0	65	33	54	51	5.5	17.0	8.7	10.4	0 ⊙	2 ⊙	5	ESE 7	ESE 7	E 4
17	94.3	94.2	94.6	94.4	15.3	21.0	15.3	16.7	22.3	7.4	60	35	63	53	7.0	16.3	6.5	9.9	8 ⊙	7	3	E 4	ENE 5	NE 1
18	95.9	95.0	92.6	94.5	10.0	21.7	16.1	16.0	22.9	7.0	93	41	65	66	0.8	15.4	6.5	7.6	10	4 ⊙	1	N 4	ENE 4	NNE 2
19	88.9	86.9	85.4	87.1	16.1	24.7	17.7	19.0	25.9	11.3	73	41	67	60	4.9	18.5	6.6	10.0	4 ⊙	6	2	ENE 2	ENE 7	ESE 4
20	85.9	86.5	89.1	87.2	15.7	24.3	14.5	17.2	24.8	11.4	79	45	89	71	3.7	16.6	1.8	7.4	2 ⊙	8	9 (R)	ESE 3	ENE 4	WNW 7
21	94.4	95.2	94.7	94.8	8.8	10.7	9.8	9.8	14.8	7.7	86	71	79	79	1.5	3.7	2.5	2.6	10	10	9	NNW 7	NW 7	NNW 1
22	93.5	93.5	92.7	93.2	8.6	12.1	11.7	11.0	15.2	7.7	90	66	80	79	1.1	4.8	2.8	2.9	10 ●	10	9	N 3	N 4	NNE 2
23	91.2	89.9	89.5	90.2	12.5	20.2	15.2	15.8	21.6	8.5	71	54	83	69	4.2	11.0	3.0	6.1	7 ⊙	6 ⊙	0	NNE 2	NNW 4	NNE 3
24	91.1	92.9	97.1	93.7	13.9	15.7	12.9	13.8	16.8	9.2	97	79	65	80	0.6	3.7	5.3	3.2	10	9	7	NNE 3	N 7	NNE 5
25	100.7	101.5	103.0	101.7	8.6	12.5	8.4	9.5	13.3	4.6	58	35	50	48	4.8	9.4	5.5	6.6	1 ⊙	8	9	NE 5	NE 9	NE 8
26	103.7	104.0	103.8	103.8	6.8	9.5	7.4	7.8	10.5	3.8	67	47	62	59	3.3	6.3	3.9	4.5	4 ⊙	10	9	NE 6	NNE 6	NE 4
27	102.9	102.5	101.6	102.3	7.8	10.0	5.1	7.0	10.6	3.0	60	48	66	58	4.2	6.4	3.0	4.5	8	9	6	NE 6	E 6	NNE 3
28	99.8	98.9	98.4	99.0	8.2	10.9	6.2	7.9	13.5	0.3	69	41	83	64	3.4	7.7	1.6	4.2	1 ⊙	9	2	ENE 3	NE 6	NE 2
29	98.5	98.8	98.6	98.6	8.0	13.5	10.1	10.4	15.0	−0.5	71	35	60	55	3.1	10.1	5.0	6.1	0 ⊙	6 ⊙	8	N 4	NNW 6	WSW 2
30	100.2	100.1	99.1	99.8	9.1	16.7	11.0	12.0	17.9	1.7	77	38	66	60	2.7	11.7	4.5	6.3	4	6 ⊙	1	C 0	NNW 5	ENE 3
31	98.8	97.2	94.6	96.9	12.9	19.9	15.1	15.8	20.6	5.5	60	30	56	49	6.1	16.2	7.7	10.0	2	7 ⊙	7 ⊙	S 2	SW 3	C 0
M	93.8	93.7	93.6	93.7	9.0	14.0	10.3	10.9	15.5	4.8	77	52	71	67	2.8	8.8	3.9	5.2	5.7	7.5	5.9	4.1	5.1	2.6

Czerwiec – Juin

1	94.1	93.7	93.9	93.9	12.9	21.9	14.3	15.8	22.5	6.3	69	29	69	56	4.6	18.8	5.1	9.5	4 ⊙	5 ⊙	6	S 1	WNW 5	NW 2
2	95.8	96.3	97.5	96.5	14.3	20.8	15.3	16.4	22.7	6.9	67	36	72	58	5.5	15.8	5.0	8.8	7 ⊙	5 ⊙	3	W 3	W 8	NNE 3
3	99.2	97.5	94.2	97.0	16.3	24.5	20.3	20.4	26.9	7.1	70	35	62	56	5.6	19.9	9.0	11.5	0 ⊙	2 ⊙	8	E 2	W 3	E 2
4	91.3	89.7	88.0	89.7	18.9	24.9	17.3	19.6	26.1	14.2	67	45	88	67	7.3	17.4	2.4	9.0	9 ⊙	9	10	S 2	SSW 5	C 0
5	84.6	85.9	84.7	85.1	13.7	13.9	12.1	13.0	17.9	11.7	98	72	94	88	0.4	4.4	0.8	1.9	10 ●	9	7	NW 5	W 8	C 0
6	85.7	88.8	90.5	88.3	12.0	11.7	10.0	10.9	16.0	9.0	76	89	78	81	3.3	1.5	2.7	2.5	3	9	1	W 7	WSW 8	S 2
7	90.3	88.4	88.6	89.1	15.2	21.5	17.1	17.7	23.8	7.5	55	49	65	56	7.9	13.0	6.9	9.3	2 ⊙	8	9	S 5	S 6	W 3
8	91.2	91.2	90.9	91.1	16.9	22.1	17.5	18.5	23.7	12.7	66	57	89	71	6.4	11.5	2.2	6.7	4	9	9	E 2	SE 2	E 3
9	89.3	88.6	89.7	89.2	17.1	21.0	16.1	17.6	26.4	13.0	82	75	96	84	3.5	6.2	0.8	3.5	8	8	6	ESE 4	SE 3	C 0
10	90.1	90.4	90.5	90.3	17.1	21.4	18.1	18.7	23.8	11.5	89	72	85	82	2.2	7.1	3.1	4.1	9	6	2	NE 3	ESE 4	C 0
11	89.3	87.4	88.7	88.5	19.7	29.4	24.5	24.5	30.4	14.2	78	48	70	65	5.1	21.4	9.1	11.9	2 ⊙	6 ⊙	3	ESE 5	SE 8	ESE 2
12	96.6	101.9	106.7	101.7	19.1	21.3	15.5	17.8	25.0	15.0	80	69	96	82	4.4	7.9	0.8	4.4	8 ⊙	6	4	WNW 5	NW 8	NNW 3
13	109.7	108.3	106.5	108.2	13.1	19.1	14.5	15.3	20.4	10.1	70	48	77	65	4.5	11.4	3.8	6.6	0 ⊙	4 ⊙	1	NNW 7	W 6	NW 3
14	107.4	106.6	106.0	106.7	13.9	21.6	16.5	17.1	23.1	6.8	79	36	53	56	3.4	16.6	8.9	9.6	1 ⊙	0 ⊙	2	NW 3	N 7	N 6
15	107.0	105.9	103.3	105.4	13.7	21.5	15.4	16.5	22.5	8.0	66	37	60	54	5.4	16.1	7.0	9.5	4 ⊙	1 ⊙	1	NNE 4	NE 3	NE 3
16	102.2	101.2	98.9	100.8	17.0	22.9	17.2	18.6	24.6	9.3	55	41	65	54	8.7	16.6	6.9	10.7	0 ⊙	0 ⊙	0	E 3	ENE 2	ENE 2
17	98.7	98.2	96.6	97.8	19.8	23.7	17.5	19.6	24.8	11.7	54	38	50	47	10.6	18.2	10.0	12.9	8 ⊙	4 ⊙	0	ENE 4	N 5	NE 2
18	95.7	93.8	90.9	93.5	19.1	26.9	21.2	22.1	28.4	10.0	43	25	52	40	12.5	26.7	12.1	17.1	0 ⊙	1 ⊙	1	E 4	E 5	ENE 1
19	89.0	88.6	88.3	88.6	19.9	29.1	20.6	22.6	29.9	12.6	64	30	62	52	8.3	28.1	9.1	15.2	0 ⊙	3 ⊙	7	S 3	NW 4	NNW 1
20	90.8	92.9	94.9	92.9	17.5	20.7	15.3	17.2	22.8	12.4	65	49	60	58	7.0	12.4	7.0	8.8	5	8	3	NE 4	NE 4	NE 3
21	97.0	94.6	90.1	93.9	15.7	23.0	19.9	19.6	25.3	8.7	51	31	51	44	8.7	19.5	11.4	13.2	3 ⊙	5 ⊙	5	ENE 3	E 4	SE 2
22	86.5	84.7	83.3	84.8	18.6	21.1	17.7	18.8	27.1	12.7	86	77	87	83	2.9	5.8	2.6	3.8	10	9	9	SSE 4	S 7	SW 3
23	87.3	89.3	87.6	88.1	15.9	20.1	16.9	17.4	23.8	13.9	88	59	92	80	2.1	9.6	1.6	4.4	6	9	9 ● (R)	SW 5	WSW 2	S 4
24	89.5	87.1	84.6	87.1	16.1	14.9	13.7	14.6	18.3	13.0	85	93	93	90	2.7	1.1	1.1	1.6	9	10 ●	10 ● (R)	NNE 3	NNE 6	NE 6
25	84.1	89.3	94.8	89.4	14.9	15.1	11.5	13.2	18.2	10.9	91	67	84	81	1.5	5.6	2.2	3.1	9	10	8	SW 8	SW 8	W 3
26	97.8	98.8	100.7	99.1	10.9	15.0	11.3	12.1	17.7	6.4	84	50	72	69	2.1	8.5	3.8	4.8	6	7	4	WNW 4	WNW 6	W 2
27	102.1	101.9	103.8	102.6	10.0	15.0	11.3	11.9	18.6	5.7	93	64	84	80	0.8	6.0	2.2	3.0	10 ●	4 ⊙	1	NNE 1	W 6	C 0
28	103.7	101.8	99.4	101.6	11.7	20.0	19.5	17.7	23.5	6.3	77	44	79	67	3.1	13.1	4.7	7.0	10	9	9	SSW 4	WSW 7	WSW 4
29	101.0	100.7	99.8	100.5	20.9	26.9	21.7	22.8	28.3	13.8	73	39	70	61	6.6	21.4	7.9	12.0	2 ⊙	4 ⊙	0	W 4	WNW 8	C 0
30	98.8	98.2	98.3	98.4	21.9	29.6	21.9	23.8	30.5	16.6	72	35	68	58	7.5	26.8	8.3	14.2	0 ⊙	2 ⊙	3	WSW 3	NW 7	C 0
31																								
M	94.9	94.7	94.4	94.7	16.1	21.4	16.7	17.7	23.8	10.6	73	51	74	66	5.2	13.6	5.3	8.0	5.0	5.7	4.7	3.8	5.5	2.2

Łódź – Lublinek

$H_s = 184\,m$ $H_b = 186{,}8\,m$ $h_w = 11\,m$

Maj – Mai 1957

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	9.8	= 0^15 – 3^45
2	8	.	.	9.6	
3	7	.	.	7.9	= 3^40 – 6^40 . ⌒^0 n – a
4	8	0.0	.	4.4	•^0 23^50 24 . = 3^40 – 8^15
5	8	.	.	9.3	•^0 0^00 ... 10
6	6	3.3	.	0.4	•^0 10^37 11^20 •^1 – 12^45 •^0 – 13^18
7	7	0.0	.	.	▽^1 14^45 – 15^15 . = 2^40 – 7^45 19^45 – 24
8	8	1.3	.	.	•^0 13^57 – 14^05 15^38 – 41 16^23 19^30 – 21^32 22^16 24 . = 0^00 – 4^20
9	6	5.2	.	.	•^0 0^00 ... 13 – 4^40 8^45 9^30 – 18^30 20^40 – 21^35 22^20 – 23^40 24
10	6	5.7	.	.	•^0 0^00 ... 25 – 5^35 •^0 – 6^20 •^0 16^30 – 17^25 45 ••^0 – 18^10 •^1 – 19^50 •^0 – 24 . ≡^0 5^30 – 6^15 ≡^1 – 8^25 ≡^0 – 8^50 = – 16^30
11	8	0.0	.	7.7	•^0 0^00 – 4^30 5^50 6^35 7^20 . = 5^50 – 6^35 7^20 – 8^50 19^30 – 23^50
12	7	.	.	6.7	= 4^45 – 10^25 . ⌒ n – a
13	7	.	.	9.1	(K) 14^12 – 17^50 . = 3^30 – 10^30 . ⌒^0 n – a
14	8	.	.	8.6	= 2^10 – 8^35 . ⌒^2 n – a
15	7	.	.	12.7	≡ 2^20 – 4^30 = – 7^30 . ⌒^1 n – a
16	8	.	.	13.3	
17	8	.	.	8.1	∞ 20^30 – 21^20
18	7	.	.	(7.5)	= 3^20 – 10^15 ∞ 19^40 – 21^35 . ⌒ n – a
19	7	.	.	9.4	
20	8	6.4	.	7.6	▽^0 13^15 – 15^40 ▲ 13^45 – 14^05 ▽^0 18^36 – 40 19^10 – 20^05 . K^1 13^09 – 13^35 – 15^15 (K) – 16^16 . K^0 17^15 – 19^26 – 20^08 (K) – 23^10 .
21	8	0.4	.	.	•^0 2^145 – 22^10 [20.V: = 4^30 – 6^40 . 16^16 – 23^10
22	7	(0.0)	.	1.2	•^0 2^40 3^15 4^06 7^32
23	7	.	.	9.4	= 6^25 – 9^50 . ⌒^0 n – a
24	7	0.0	.	.	•^0 7^35 – 8^55 •^0 – 9^05 ▽^0 10^55 – 11^33 . = 1^45 – 11^16 . ⌒ n – a
25	8	.	.	7.1	
26	8	0.0	.	2.2	▽^0 13^15 – 27 13^33 – 40
27	8	.	.	2.5	= 20^00 – 22^20
28	7	0.0	.	11.9	▽^0 17^27 – 32 . ≡ 3^40 – 4^35
29	8	.	.	7.4	= 2^30 – 6^25
30	8	.	.	9.6	= 2^20 – 7^20
31	7	.	.	8.8	
Σ	–	22.3	–	202.2	UWAGI

Czerwiec – Juin

1	8	.	.	9.5	= 2^30 – 7^20 ∞ 18^35 – 21^55 = – 24
2	8	.	.	13.0	= 0^00 – 8^30 . ⌒^0 na
3	8	.	.	12.1	(K) 22^55 – 24 WSW . ≡ 3^10 – 9^10
4	7	2.8	.	2.8	▽^0 14^05 – 15 14^40 – 45 14^55 – 15^35 18^30 – 45 •^0 22^50 – 24 (K) 0^00 – 45 WSW – S . K^0 14^55 – 15^50 (K)^1 18^20 – 19^40 . = 5^40 – 9^50
5	6	3.6	.	2.6	•^0 0^00 – 6^30 •^1 – 6^45 •^0 – 10^40 ▽^1 18^50 – 19^15 . = 11^30 – 14^20 21^35 – 24
6	7	0.2	.	(7.0)	▽^1 13^05 – 10 ▽^0 – 13^26 . 13^50 – 58 . 14^03 – 10 . 14^20 – 40 . = 0^00 – 8^15
7	7	.	.	11.5	= 5^40 – 8^40
8	7	1.2	.	(3.9)	▽ K 16^55 – 18^20 SW – E (K) – 19^15 . = 5^45 – 10^40
9	7	11.4	.	3.0	▽^1 9^10 – 15 ▽^0 – 9^50 10^40 – 11^05 ▽^2 13^15 – 17 ▽^1 – 13^25 14^05 – 15^30 ▽^0 16^20 – 18^30 (K) 8^50 – 11^55 K 14^10 – 15^30 (K) – 20^45
10	7	.	.	4.8	▽^1 5^05 – 6^05 ▽^0 – 6^15 (K)^0 4^30 – 5^05 K – 6^15 (K) – 7^30 . = 0^00 – 1^45 ≡^1 – 4^30 = 7^30 – 13^20 . 21^25 – 24 [9.VI: = 22^30 – 24
11	8	.	.	7.7	= 0^00 – 7^35
12	7	.	.	9.9	= 5^15 – 7^40
13	8	.	.	13.8	
14	8	.	.	13.9	= 5^20 – 7^30
15	8	.	.	12.5	
16	8	.	.	13.9	
17	8	.	.	13.7	
18	8	.	.	13.8	
19	7	.	.	11.2	
20	7	0.0	.	5.4	▽^0 18^05 – 20
21	8	0.0	.	13.0	▽^0 22^45 – 23^20
22	7	0.0	.	2.8	•^0 10^45 – 13^15 ▽^0 18^50 – 19^05 . = 3^15 – 9^30 21^30 – 24
23	7	1.8	.	3.4	▽^0 20^45 – 21^25 ▽^1 K – 21^38 . ▽^0 – 21^50 (K)^0 21^38 – 56 SW . = 0^00 – 9^20
24	6	12.6	.	1.1	•^0 11^35 12^40 – 13^35 14^45 – 15^25 ▽^1 21^40 – 24 . K 21^50 – 23^35 SW – NE (K) – 24 . = 1^45 – 10^55 16^35 – 21^30
25	8	.	.	1.7	▽^0 0^00 – 30 ▽^0 – 3^20 •^0 – 5^30 . (K) 0^00 – 20 . ≫ 11^20 – 13^35 13^50 – 17^40 (16^15 – 17^40 por. do 16 m/sek) . = 5^30 – 7^20
26	8	0.4	.	10.2	= 3^30 – 6^28 . ⌒^1 n – a
27	7	0.3	.	7.6	•^0 7^03 – 8^04 . 8^27 – 40 ▽^0 12^35 – 40 . 12^43 – 47 ▽^1 13^14 – 17 ▽^1 – 13^25
28	7	.	.	4.1	
29	8	.	.	14.1	= 2^20 – 4^30 ≡ – 6^22 = – 7^32
30	8	.	.	13.5	
31					
Σ	–	34.3	–	257.5	UWAGI

Łódź – Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$

Lipiec – Juillet 1957

Dni	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	98.6	98.3	97.0	98.0	21.4	27.5	21.3	22.9	28.3	15.5	55	42	55	51	11.4	21.3	11.3	14.7	0 ⊙	2 ⊙	2	ENE 4	ENE 3	ENE 4
2	94.8	91.6	94.6	93.7	21.1	32.4	21.9	24.3	33.0	15.6	65	33	70	56	8.7	32.3	7.9	16.3	2	5 (R)	10	SE 4	SSW 5	WNW 6
3	99.4	98.8	97.3	98.5	15.9	22.9	20.3	19.8	25.4	9.1	68	35	42	48	5.8	18.1	13.7	12.5	1 ⊙	2 ⊙	1	NW 3	NW 5	C 0
4	97.3	95.1	92.7	95.0	18.9	28.0	25.1	24.3	31.4	11.0	58	33	57	49	9.2	25.3	13.6	16.0	8 ⊙	9 ⊙	2	S 3	S 7	S 4
5	93.2	92.5	94.1	93.3	24.5	33.1	24.5	26.6	34.0	20.8	62	31	80	51	11.6	35.1	12.2	19.6	0 ⊙	0 ⊙	5	SW 3	WNW 7	NW 3
6	99.3	98.7	98.3	98.8	17.3	24.9	19.5	20.3	26.6	12.3	62	25	55	47	7.4	23.6	10.2	13.7	0 ⊙	4 ⊙	2	NW 5	WNW 6	N 1
7	99.6	98.6	97.9	98.7	19.3	27.9	22.3	23.0	30.4	10.1	57	31	51	46	9.7	25.9	13.1	16.2	5 ⊙	2 ⊙	1	ENE 2	ENE 3	ENE 4
8	98.0	93.4	92.4	94.6	21.0	34.0	22.9	25.2	34.9	16.3	53	35	82	57	11.7	34.8	5.0	17.2	8 ⊙	8 ⊙	9 (R)	NNW 3	SSE 5	ESE 3
9	91.5	93.6	93.7	92.9	19.1	19.5	16.3	17.8	23.4	15.6	97	81	94	91	0.7	4.3	1.1	2.0	10 ● R	10 ●	2	SW 4	N 2	N 1
10	92.7	90.0	87.7	90.1	17.1	24.1	20.7	20.4	25.1	13.5	96	49	71	72	0.8	15.3	6.8	7.6	9	8	9	C 0	E 3	ENE 5
11	85.8	85.7	86.9	86.1	20.1	25.7	17.9	20.4	27.2	15.3	63	40	94	66	8.8	19.9	1.2	10.0	6 ⊙	4 ⊙	10 ●	E 5	E 8	ESE 4
12	86.5	87.5	89.1	87.7	17.8	20.8	18.9	19.1	22.6	16.6	98	90	95	94	0.4	2.5	1.0	1.3	10 ●	10 ●	7	NNE 3	N 2	WNW 3
13	92.5	94.2	95.2	94.0	17.9	24.9	20.7	21.0	26.3	15.8	95	60	73	76	1.0	12.7	6.5	6.7	7	4 ⊙	0	WNW 4	NNW 3	NE 1
14	95.1	93.4	92.3	93.6	20.3	26.5	19.1	21.2	27.4	14.6	78	49	88	72	5.2	17.7	2.5	8.5	0 ⊙	8	10	E 2	NE 7	NW 5
15	90.9	91.2	91.0	91.0	16.3	17.9	16.7	16.9	19.8	15.4	100	95	96	97	0.0	1.0	0.8	0.6	9	9 ●	9	NW 4	C 0	C 0
16	88.6	85.8	83.3	85.9	16.0	16.7	14.5	15.4	19.6	13.8	94	97	98	96	1.2	0.6	0.4	0.7	10	10 ●	10 ●	N 3	N 6	WNW 12
17	82.9	84.4	87.1	84.8	12.8	14.3	14.7	14.1	15.1	11.8	99	98	98	98	0.2	0.4	0.4	0.3	10 ●	10 ●	10 ●	NW 8	WNW 7	WNW 6
18	88.9	88.9	88.3	88.7	14.5	20.8	16.7	17.2	22.8	13.3	93	55	79	76	1.1	11.2	4.1	5.5	9	8	0	W 4	W 10	C 0
19	88.0	87.3	86.0	87.1	16.5	25.3	19.5	20.2	26.1	10.5	78	39	74	64	4.3	19.6	5.9	9.9	0 ⊙	4 ⊙	8	SSW 2	SSE 2	E 2
20	85.1	84.1	82.6	83.9	20.4	28.0	16.9	20.6	29.1	15.0	73	42	93	69	6.5	21.9	1.4	9.9	3 ⊙	5 ⊙	7	E 3	E 5	N 2
21	82.1	81.6	80.9	81.5	16.2	17.4	15.9	16.4	17.8	15.1	97	96	98	97	0.6	0.9	0.4	0.6	10 ●	10 ●	10 ●	C 0	WNW 1	W 2
22	78.5	79.7	80.1	79.4	15.1	15.7	14.9	15.2	18.4	14.2	96	85	89	90	0.8	2.6	1.8	1.7	10 ●	10	10	SW 5	SW 5	S 5
23	80.8	82.1	83.2	82.0	15.5	21.7	17.4	18.0	23.0	12.7	83	52	85	73	3.0	12.6	3.0	6.2	3 ⊙	9	2	E 2	C 0	C 0
24	84.4	86.3	88.5	86.4	14.5	18.5	13.3	14.9	18.8	12.8	99	76	92	89	0.2	5.1	1.3	2.2	10 ● R	9	4	WSW 6	W 9	WSW 3
25	89.5	89.9	88.1	89.2	13.5	17.9	14.7	15.2	19.9	10.7	95	55	85	78	0.7	9.3	2.5	4.2	10 ●	6 ⊙	10	W 4	WSW 7	SW 3
26	87.8	88.7	86.5	87.7	13.1	15.9	15.7	15.1	20.1	12.2	96	71	97	88	0.6	5.3	0.6	2.2	10 ●	8	10	W 4	WSW 5	WSW 3
27	84.3	82.3	83.5	83.4	15.7	19.4	14.1	15.8	20.7	12.3	91	75	93	86	1.5	5.6	1.1	2.7	9	9 ●	9	WSW 5	SSW 7	SE 1
28	85.1	86.4	87.5	86.3	12.7	18.1	12.3	13.8	19.5	11.7	94	60	94	83	0.9	8.3	0.9	3.4	9	6 ⊙	5	SW 4	W 3	C 0
29	88.6	90.1	92.2	90.3	13.6	16.1	15.6	15.2	19.9	9.3	89	82	84	85	1.8	3.1	2.8	2.6	5 ⊙	6	9 ● R	S 2	SW 4	SE 2
30	93.3	94.0	95.9	94.4	15.9	15.9	14.1	15.0	18.3	11.7	85	89	99	91	2.7	2.0	0.2	1.6	9	10 ●	10 ●	SW 4	SW 8	W 6
31	98.7	100.0	102.0	100.2	15.4	18.9	15.0	16.1	20.4	13.3	92	76	90	86	1.3	5.1	1.6	2.7	10	8	5	W 5	WNW 6	WNW 4
M	90.4	90.1	90.2	90.2	17.1	22.3	17.8	18.8	24.0	13.5	83	61	82	75	3.9	13.0	4.4	7.1	6.5	6.9	6.4	3.5	4.9	3.1

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1	102.4	102.2	100.2	101.6	13.2	19.8	16.6	16.6	22.4	9.6	95	63	89	82	0.7	8.5	2.2	3.8	9	2	0	WSW 2	WNW 6	C 0
2	100.2	99.1	99.7	99.7	15.9	19.9	12.9	15.4	21.4	12.4	87	61	80	76	2.3	9.1	2.9	4.8	9	7 ⊙	0	NNW 2	W 8	WNW 4
3	99.7	98.3	98.7	98.9	12.3	17.3	13.1	14.0	19.1	7.9	88	59	89	79	1.7	8.1	1.6	3.8	0 ⊙	7	1	WNW 4	WNW 7	W 2
4	98.5	98.3	99.2	98.7	13.7	20.1	14.5	15.7	21.9	10.0	90	58	84	77	1.6	9.9	2.7	4.7	5 ⊙	8	7	WNW 4	WNW 5	WNW 2
5	100.7	100.9	100.6	100.7	14.9	19.3	15.3	16.2	21.2	10.3	87	62	91	80	2.2	8.6	1.5	4.1	4 ⊙	10	1	NNW 5	NW 7	C 0
6	101.4	100.6	98.5	100.2	13.9	21.5	17.6	17.6	22.8	8.9	100	55	70	75	0.0	11.6	6.1	5.9	4 ⊙	6 ⊙	4	C 0	N 2	C 0
7	95.9	92.2	88.1	92.1	17.3	25.3	17.7	19.5	25.5	11.0	69	45	87	67	6.2	17.6	2.6	8.8	9	9	9	E 2	SE 6	C 0
8	86.4	88.3	88.6	87.8	14.9	19.2	16.0	16.5	21.4	14.3	100	77	85	87	0.0	5.0	2.7	2.6	10 ●	7 ⊙	5	W 4	WNW 6	N 2
9	88.1	87.3	83.8	86.4	16.3	23.5	19.1	19.5	24.0	12.0	88	53	72	71	2.3	13.7	6.2	7.4	2 ⊙	6 ⊙	6	ESE 3	SE 6	ESE 5
10	80.0	81.8	84.6	82.1	15.9	16.5	16.1	16.2	21.8	14.8	93	98	90	94	1.4	0.4	1.7	1.2	10 ●	9 ●	0	ESE 3	WSW 3	SSW 4
11	90.5	91.6	90.9	91.0	16.9	23.4	20.9	20.5	26.8	13.0	84	59	73	72	3.1	11.8	6.6	7.2	1 ⊙	5 ⊙	2	SW 3	SW 7	SE 2
12	89.1	89.7	90.8	89.9	18.9	20.1	17.9	18.7	23.5	14.8	88	91	95	91	2.5	2.2	1.0	1.9	9	9	5	ENE 2	WNW 3	W 1
13	92.9	93.9	92.8	93.2	17.7	24.0	19.2	20.0	25.1	14.7	94	53	86	78	1.2	13.9	3.2	6.1	5	6 ⊙	8	C 0	WNW 3	C 0
14	89.8	90.1	86.7	88.9	19.3	23.3	19.5	20.4	24.4	17.0	88	71	88	82	2.8	8.3	2.8	4.6	5 ⊙	9	10	E 2	WNW 4	NNW 3
15	87.5	97.8	88.9	91.4	15.5	20.5	17.2	17.6	22.2	14.8	91	68	91	83	1.5	7.7	1.8	3.7	10	7	0	W 5	W 6	C 0
16	89.1	89.5	89.6	89.4	16.7	18.7	13.4	15.6	24.3	12.6	90	88	99	92	2.0	2.5	0.2	1.6	7 ⊙	10	10 ● R	C 0	SW 5	W 3
17	89.0	90.1	88.8	89.3	13.0	13.9	12.5	13.0	16.6	11.4	99	93	92	95	0.2	1.1	1.2	0.8	10	10 ●	6	W 3	SW 5	SW 5
18	87.3	87.2	88.2	87.6	13.7	17.3	14.0	14.8	18.7	11.2	89	79	93	87	1.8	4.1	1.1	2.3	9	8	0	SW 8	SW 9	SSW 2
19	91.0	92.3	94.7	92.7	12.8	20.1	14.5	15.5	21.3	10.2	98	58	89	82	0.4	9.9	1.8	4.0	9	4	0	W 3	WNW 6	SW 2
20	96.0	96.3	95.6	96.0	13.3	19.7	14.5	15.5	21.6	9.2	95	66	85	82	0.7	7.9	2.5	3.7	0 ⊙	3 ⊙	5	W 2	W 7	C 0
21	94.3	93.4	89.7	92.5	15.3	17.7	16.5	16.5	20.7	12.8	88	84	92	88	2.1	3.2	1.6	2.3	10	10	9	SW 5	WSW 4	S 1
22	88.1	89.6	90.1	89.3	12.7	14.9	10.5	12.2	17.1	10.1	96	77	94	89	0.5	3.8	0.8	1.7	10	10	3	NW 4	WNW 6	WSW 2
23	91.1	91.3	91.0	91.1	10.0	15.5	12.1	12.4	17.8	8.1	95	62	80	79	0.7	6.7	2.8	3.4	4	6	0	W 3	WSW 6	C 0
24	88.9	85.1	87.5	87.2	11.7	21.9	12.3	14.6	22.9	7.1	82	51	94	76	2.5	13.8	0.9	5.7	2	9	9	ESE 4	S 9	S 5
25	94.2	93.4	90.3	92.6	10.8	19.3	14.7	14.9	21.1	7.7	86	47	72	68	1.8	11.9	4.7	6.1	0 ⊙	5	3	SSE 2	S 8	SE 2
26	88.7	89.1	90.1	89.3	14.3	18.0	11.1	13.6	19.4	10.3	84	55	91	77	2.5	9.2	1.1	4.3	9	4 ⊙	0	SSW 2	SW 8	S 2
27	92.0	92.6	92.5	92.4	11.3	15.7	10.5	12.0	17.1	8.3	91	71	96	86	1.2	5.2	0.5	2.3	9	8	0	SSW 5	S 6	C 0
28	90.9	91.2	92.5	91.5	12.3	16.1	13.1	13.6	16.8	9.5	96	74	96	89	0.5	4.7	0.6	1.9	9	9	10	SE 3	SW 3	C 0
29	93.9	94.9	96.6	94.8	10.8	15.7	10.0	11.6	17.3	9.3	97	68	89	85	0.4	5.7	1.3	2.5	9	9	0	NW 3	NW 5	WNW 2
30	96.9	97.5	97.4	97.3	9.4	12.5	10.0	10.5	15.0	5.8	97	80	87	88	0.3	2.9	1.6	1.6	10	10	3	NNW 2	N 8	W 1
31	96.7	94.9	93.8	95.3	9.8	18.3	11.3	12.7	19.3	6.2	84	50	94	76	1.9	10.4	0.8	4.4	8	8	0	S 3	SW 7	SSE 3
M	92.6	92.9	92.3	92.6	14.0	19.0	14.7	15.6	21.0	10.8	91	67	88	82	1.6	7.7	2.2	3.8	6.7	7.4	3.7	3.0	5.8	1.8

Łódź – Lublinek

H_s = 184 m H_b = 186.8 m h_w = 11 m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	8	.	.	10.2	
2	7	.	.	9.5	(K) 13⁴⁷ – 15⁵⁰
3	8	.	.	13.9	
4	8	.	.	9.9	≤ 22⁴⁰ – 23³⁰
5	8	.	.	11.5	
6	8	.	.	13.9	
7	7	.	.	12.6	
8	8	2.4	.	6.4	▽² 20¹⁰–20· (K) 17⁰⁰–20⁰⁵ SE K –20²⁰ (K)–23³⁵ SE
9	7	3.1	.	2.6	▽⁰ 6³⁰–8²⁰ ▽¹ 9¹⁵ ▽⁰–11³⁰ ●⁰–12²⁰, 13⁴⁰ 14¹⁰ ▽⁰ 14⁵⁰–15³⁵ ≤ 0⁰⁰–10· 14⁵–2³⁰ (K) 5²⁰–6³⁰ SE K–6⁴⁵ (K)–8³⁵ W–NE
10	8	.	.	3.4	= 0⁰⁰–9¹⁵ [9.VII: K–9³⁰ (K)–10⁰⁰: = 22⁴⁵ – 24
11	7	3.0	.	6.8	●⁰ 20²⁵–23²⁰, 23³² 24 = 4³⁰–8³⁰
12	6	13.4	.	3.0	●⁰ 0⁰⁰–40 2¹⁵...50–5⁴³ 6³⁸, 7¹⁵–35 8⁴⁰–9²⁵ ▽¹ 11⁷⁰–12⁰⁶, 13⁴⁰–14⁰² ▽² 14³⁰ ▽² 15³⁰ ▽¹ 15³⁵ K 15¹⁵–20–40 W–NW
13	8	.	.	8.3	= 0⁰⁰–5⁰⁵ ≡²–6²⁰ =–7⁴⁰, 23³⁰–24 [11.VII: (K)–16¹⁰ = 16¹⁰–17²⁰, 20²⁵ – 24
14	7	1.2	.	8.6	= 0⁰⁰–7³⁰· ⌒² n–a
15	6	5.8	.	.	▽¹ 3²⁵–5⁴⁵ ●⁰ 10⁰⁵–13²⁰ ▽–15⁴⁰, ≤ 22⁰–3¹⁵ (K)⁰ 5⁴⁰–6⁴⁰ = 6³⁰–10⁰⁵, 20³⁰–24
16	5	82.4	.	.	●⁰ 8⁰⁵–11³⁰ ●²–17⁴⁵ ●¹–16³⁵ ●²–16⁴⁵ ●¹–24 = 0⁰⁰–8⁰⁵
17	6	33.5	.	.	●¹ 0⁰⁰–4³⁵ ●⁰–10³⁰ ●¹–11¹⁵ ●⁰–13⁰⁵ ●¹–15²⁵ ●⁰–16³⁰ ●¹–16⁵⁰ ●⁰–20⁵² ●¹–21²⁵ ●⁰⁻²–22²⁸ ●¹–22⁴⁰ ●⁰–24
18	8	.	.	10.1	●⁰ 0⁰⁰–3¹⁵· = 3¹⁵–10²⁰
19	7	.	.	11.0	= 4³⁵–7²⁰
20	7	3.3	.	8.4	▽⁰ 17⁵⁰–18²⁵, 18⁴⁵–20³⁰· K⁰ 19³⁰–20³⁰ SW–SE = 13⁶–9³⁵
21	6	37.2	.	.	▽⁰ 20⁵–20 2⁴³–45 ●⁰ 4⁴⁰–12⁴⁵ ▽⁰–13¹⁵ ●⁰–14⁴⁰ ●²–16⁰⁹ ●²–16²⁴ ●¹–17³⁰ ●⁰–23⁰⁵ ●¹–24· (K) 0⁰⁰–12⁵
22	7	0.3	.	.	●¹ 0⁰⁰–45· ●⁰–10³⁰
23	8	37.1	.	9.7	●⁰ 2⁴⁰–3³⁵· = 7³⁰–8⁴⁰
24	7	6.9	.	0.3	▽⁰ 5⁰⁸–20 ▽⁷–9³⁵· K 4⁵⁰–5²⁰–9¹⁵ E–NW
25	8	0.0	.	3.5	●⁰ 7²⁵, 8⁴⁰
26	8	14.0	.	1.5	●⁰ 7³⁵–8³⁰ ▽⁰ 17⁰⁵–30 ▽¹ 17⁴⁰–18²⁵ ●⁰–21⁵⁰ ●¹–22¹⁵ ●⁰–23³⁰· = 3⁴⁰–7³⁵
27	7	9.2	.	1.1	●⁰ 2³⁵–4³⁵ ▽⁰ 12⁵⁰–13⁰⁴, 13⁵⁵–14⁰⁹ ▽¹–14²⁰ ▽⁰–15²⁶ ▽¹ 18⁰⁷–30 ▽⁰⁻¹ 19⁰⁵–40 ▽¹ 22⁵⁶–23⁰⁹ ▽⁰–24 K 14⁰⁵–15–43 SW–NE
28	8	0.0	.	4.7	▽⁰ 0⁰⁰–11 0³⁵–2⁴⁵, 3³⁰–4²⁵ ▽¹ 19⁵⁵–20¹²· = 4²⁵–9¹⁵
29	8	2.0	.	7.4	▽⁰ 11²³–27 ▽¹–11³⁰ ▽⁰–11³⁴, 12²⁸–13²⁴, 21⁴⁰–22⁵⁰· (K) 11⁴⁰–13³⁰ NW–N, 21²⁰–23⁴⁵ NW ⌒² n–a
30	7	3.3	.	.	▽¹ 11⁵⁵–12¹³ ▽⁰ 13⁴⁵–14²⁵, 14⁴⁵–15¹⁰ ▽¹ 15²⁰–16¹⁵ ●⁷ 16⁴⁰–17¹⁰ ●¹–18³⁵ ●⁰–19¹⁵, 19⁵⁰–24· = 5³⁵–10³⁰
31	8	0.0	.	2.4	●⁰ 0⁰⁰–25 ●⁰–2⁴⁰ ▽⁰ 15⁵⁰–16⁰⁵· = 4³⁰–7³⁵
Σ	–	258.1	–	180.7	UWAGI

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1	8	.	.	9.1	= 3³⁰–8²⁰· ⌒¹ n–a
2	8	.	.	6.1	= 4⁴⁵–7²⁰· ⌒¹ n–a
3	8	.	.	9.0	⌒¹ n–a
4	8	0.0	.	9.6	▽⁰ 22⁵²–23¹², ⌒¹ n–a
5	8	.	.	6.3	
6	8	.	.	11.3	≡¹ 3⁵⁰–6⁰⁵ =–8⁴⁰· ⌒² n–a
7	7	6.3	.	5.3	▽ 23⁴⁰–24· (K) 20¹⁰–21³⁰ S–NE K 23³⁰–23⁴⁰–24· ⌒¹ n–a
8	7	0.0	.	4.7	▽ 0⁰⁰–30 ●⁰ 4²⁵–5⁴⁰ ▽¹ 6⁴⁵–8⁰⁰ ▽⁰–8³⁵· K 0⁰⁰–10 (K)–14⁰ K 7⁰⁰–15· = 14⁰–4²⁵, 5⁴⁰–12⁴⁵
9	7	0.0	.	9.9	= 14⁰–8³⁰· ⌒¹ n–9²⁰
10	7	12.0	.	2.1	●⁰ 7³⁰, 8¹⁵ ●¹–9²⁵ ●⁹⁰–11²⁰ ●⁹¹–12⁰⁵ ●¹–13⁰⁵ ●⁰–14⁰⁶ ▽⁰ 17³⁷–57· = 9²⁵–13¹⁰· ⌒¹ 17⁵⁰–18¹⁵
11	8	.	.	12.3	
12	7	2.2	.	3.6	▽⁰ 9⁵³–10²⁸ ▽¹–10³⁶ ▽⁰–10³⁹· = 5³⁰–7⁵³, 12³⁵–13³⁶, 23³⁰–24
13	8	0.0	.	9.6	= 0⁰⁰–8⁴⁰
14	7	10.0	.	6.9	▽⁰ 4⁴⁵–5⁰⁵, 22³⁰–24 K 21⁴⁰–22³⁰–24 SSW–E = 7³⁰–9³⁰, 12³⁰–13²⁰
15	7	.	.	6.0	▽⁰ 0⁰⁰–45 2³⁵–45 ▽¹–3⁰⁵ ▽⁰–3²⁵· K 0⁰⁰–45· = 5³⁰–10³⁰
16	6	11.7	.	4.1	▽⁰ 13³⁰–14²⁵ ●⁰ 17⁴⁵, 18¹⁵, 18³⁸ 19⁴⁰ ▽¹ 20³²–22¹⁵ ▽⁰–23¹⁰ ●⁰–23⁴⁰ (K) 12⁵⁶–13⁴⁰ W–E K 20³⁶–20⁴⁰–22¹⁵
17	6	1.1	.	0.1	●⁰ 12¹⁵–14⁰⁵· = 0⁰⁰–1³⁰, 3²⁸–10³⁰ [16.VIII: SW–NW = 2⁰⁰–9³⁰ 14²⁵–17³⁰ 23⁴⁰–24· ⌒ n–10¹⁵
18	7	0.0	.	3.2	▽⁰ 7³⁰–35 12¹⁷–26, 12⁵⁵–13⁰⁸, 13²³–32, 14⁵³–15¹⁰, 15⁵⁷–16¹⁰· = 4²⁰–9³⁰
19	7	.	.	9.8	= 4²⁵–10⁴⁰· ⌒¹ n–a
20	8	.	.	10.5	≡ 4²⁵–6¹⁵ =–10⁴⁰· ⌒¹ n–9⁰⁰
21	7	3.6	.	1.3	= 5³⁰–12³⁵, 19⁴⁰–24
22	7	1.8	.	1.1	▽⁰ 2¹⁰–15 ●⁰ 3¹⁵–5³⁵ ●¹–7¹⁵ ●⁰–8²⁰ ●¹–10¹⁵ ●⁰–12¹⁰· = 0⁰⁰–2¹⁰
23	8	.	.	12.0	
24	7	4.2	.	7.3	●⁰ 15⁵⁰–17²⁰ ●¹–18⁴⁰ ▽¹–19²⁵ ●⁰–20³⁵· = 5³⁰–9³⁰· ⌒¹ n–10¹⁵
25	8	.	.	10.4	= 7³⁰–8⁴⁰· ⌒¹ n–a
26	8	0.0	.	3.8	▽⁰ 12⁰⁰–15· 12²⁵–32
27	7	0.1	.	2.4	▽⁰ 12⁵⁰–57 13²⁵–35 14⁰³–08· ⌒⁰ n–a
28	7	0.0	.	0.1	●⁰ 5¹⁵...40 ▽⁰ 14¹⁰–16 15¹²–21· = 5¹⁵–11³², 21²⁰–24
29	7	.	.	1.2	= 0⁰⁰–12³⁰· ⌒² n–a ⌒¹ 21⁰⁰–24
30	7	0.0	.	0.9	▽⁰ 15⁰⁵–15· = 2²⁰–10²⁰· ⌒¹ 0⁰⁰–3⁴⁰ ⌒² –9⁴⁰
31	7	1.9	.	2.9	▽¹ 15¹⁵–25 ▽⁰–16¹⁰· = 6³⁰–9³⁰
Σ	–	54.9	–	182.9	UWAGI.

Łódź – Lublinek $\varphi = 51°44'$ $\lambda = 19°24'$ Wrzesień – Septembre 1957

DNI	CIŚNIENIE p				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	93.9	94.8	96.4	95.0	9.0	12.1	9.4	10.0	14.8	7.1	92	80	95	89	1.0	2.8	0.6	1.5	10	9 ●	1	W 7	WSW 9	S 2
2	96.7	95.3	93.6	95.2	8.7	19.6	14.5	14.3	20.6	4.3	93	52	89	78	0.7	10.9	1.8	4.5	7	8	10	E 1	SSW 6	SE 2
3	92.6	93.8	95.0	93.8	12.9	16.1	12.5	13.5	17.0	11.4	99	79	96	91	0.2	3.8	0.5	1.5	10 ●	7	10	SSW 3	WSW 4	C 0
4	96.6	98.6	100.3	98.5	11.2	16.9	12.8	13.4	17.3	9.2	96	61	93	83	0.5	7.5	1.1	3.0	9	9	6	W 2	N 3	E 1
5	100.6	99.3	97.5	99.1	9.0	18.1	13.1	13.3	19.8	6.3	96	52	91	80	0.5	10.1	1.4	4.0	2 ⊙	5 ⊙	6	C 0	SW 2	SE 1
6	96.2	96.5	97.2	96.6	13.5	18.3	14.5	15.2	20.4	10.8	93	68	90	84	1.1	6.8	1.6	3.2	10	8 ⊙	5	W 1	NW 1	C 0
7	98.4	98.4	98.2	98.3	12.5	21.7	16.3	16.7	23.1	9.0	98	58	77	78	0.4	11.0	4.2	5.2	7	7 ⊙	0	E 1	SE 4	ESE 2
8	98.6	98.7	99.1	98.8	12.9	25.9	17.7	18.6	26.5	10.4	92	48	82	74	1.3	17.4	3.6	7.4	0 ⊙	2 ⊙	0	E 3	S 7	C 0
9	98.7	98.2	100.2	99.0	17.1	26.7	16.1	19.0	27.8	12.5	78	43	92	71	4.3	19.8	1.6	8.6	0 ⊙	0 ⊙	10	SE 5	S 7	WNW 6
10	100.4	99.8	97.3	99.2	13.4	13.7	12.5	13.0	16.1	11.9	96	94	99	96	0.6	0.9	0.2	0.6	10 ●	10	8	N 2	NNW 3	C 0
11	93.3	88.7	82.2	88.1	9.4	19.3	16.3	15.3	20.3	7.2	99	59	79	79	0.2	9.2	3.8	4.4	0 ═	7	10	E 2	E 7	SSE 5
12	75.9	75.7	81.5	77.7	16.1	14.1	10.5	12.8	22.5	9.5	85	87	71	81	2.7	2.2	3.7	2.9	5	6	1	S 7	WSW 12	WSW 3
13	85.6	85.1	82.9	84.5	10.1	15.5	13.1	13.0	17.4	7.5	78	45	67	63	2.7	9.7	5.0	5.8	2 ⊙	8	9	SW 7	SSW 10	SSE 7
14	84.5	84.8	86.1	85.1	9.0	15.8	9.8	11.1	16.6	6.9	72	48	78	66	3.2	9.3	2.7	5.1	8	5 ⊙	10	SW 7	SSW 9	S 1
15	83.3	85.5	90.7	86.5	8.6	10.5	8.9	9.2	11.1	7.8	97	84	92	91	0.3	2.1	0.9	1.1	10 ●	10 ●	0	WNW 4	WSW 7	WSW 3
16	93.2	93.9	95.3	94.1	8.4	11.9	7.8	9.0	13.6	6.2	83	70	87	80	1.8	4.1	1.4	2.4	8	9	0	SSW 4	SW 5	SSW 3
17	95.3	93.4	91.1	93.3	5.5	9.4	9.2	8.3	10.4	3.5	97	91	95	94	0.3	1.1	0.6	0.7	9	10 ●	10 ●	S 2	WSW 4	WNW 2
18	89.7	88.9	89.5	89.4	6.6	9.5	10.5	9.3	11.7	5.8	96	88	85	90	0.4	1.4	1.9	1.2	10	10	9	W 5	W 8	W 5
19	88.3	86.8	84.4	86.5	7.1	13.4	13.1	11.7	14.4	5.5	94	74	95	88	0.6	4.0	0.7	1.8	4	10 ●	10 ●	WSW 5	SW 8	SW 9
20	86.0	89.8	93.1	89.6	10.0	11.3	8.0	9.3	13.3	7.3	92	78	90	87	1.0	3.0	1.0	1.7	10 ●	8	0	W 6	WNW 4	W 2
21	94.9	95.1	94.0	94.7	4.5	13.3	8.8	8.8	14.3	1.9	93	53	84	77	0.5	7.2	1.8	3.2	6 ⊙	8 ⊙	0	S 2	WSW 4	E 1
22	89.2	88.5	89.0	88.9	10.0	16.1	13.7	13.4	18.2	7.7	89	93	95	92	1.3	1.3	0.7	1.1	10	10	0	E 4	WSW 5	SSW 2
23	84.4	79.4	77.2	80.3	15.0	17.2	14.1	15.1	18.4	7.0	92	91	93	92	1.3	1.8	1.1	1.4	9	10 ●	10 ●	SSW 4	SSW 6	WSW 6
24	83.4	81.5	85.6	83.5	10.1	11.1	7.4	9.0	14.6	7.2	93	96	81	90	0.8	0.5	1.9	1.1	4	10	2	WSW 5	C 0	WSW 6
25	90.5	93.3	95.7	93.2	4.8	9.4	5.0	6.0	11.2	3.5	82	56	83	74	1.5	5.2	1.5	2.7	2	10	1	W 10	WNW 10	WSW 1
26	94.7	94.4	95.6	94.9	1.0	9.1	5.1	5.1	10.3	-0.4	94	60	90	81	0.4	4.7	0.9	2.0	7	8	3	C 0	NW 7	C 0
27	97.1	95.5	86.1	92.9	0.2	10.3	8.0	6.6	10.8	-1.6	98	47	84	76	0.1	6.6	1.6	2.8	4	8	10 ●	W 2	WSW 9	WSW 8
28	81.6	83.2	84.1	83.0	8.8	10.1	8.2	8.8	12.3	6.5	84	85	87	85	1.8	2.0	1.4	1.7	4	8 ●	2	W 10	W 8	W 8
29	82.9	80.1	77.1	80.0	8.3	9.6	8.6	8.8	10.0	7.1	93	92	92	92	0.8	1.0	1.0	0.9	9	10 ●	10	SW 5	SW 6	SW 5
30	81.9	85.3	91.3	86.2	5.4	6.1	6.6	6.2	8.9	4.6	86	89	88	88	1.3	1.0	1.1	1.1	9	10	9	W 8	W 9	W 5
31																								
M	90.9	90.7	90.9	90.8	9.3	14.4	11.1	11.5	16.1	6.8	91	71	87	83	1.1	5.6	1.7	2.8	6.5	8.0	5.4	4.1	6.1	3.3

Październik – Octobre

1	93.7	94.7	96.4	94.8	3.9	9.2	5.0	5.8	10.1	2.3	97	69	94	87	0.3	3.6	0.5	1.5	6	9	3	SSE 2	W 5	W 4
2	101.0	102.6	101.4	101.7	1.6	5.4	3.0	3.2	8.9	0.9	98	80	88	89	0.2	1.8	0.9	1.0	10 ═	7	1	SSW 1	C 0	ESE 1
3	96.8	92.6	89.2	93.0	0.5	10.4	8.9	7.2	11.1	-0.3	96	60	69	75	0.2	5.0	3.5	2.9	0	10	10	E 2	SSW 7	SSW 8
4	89.5	92.4	97.4	93.1	5.9	3.2	4.9	4.7	9.2	1.8	83	95	81	86	1.6	0.4	1.7	1.2	9	7	1	W 9	WNW 6	WSW 4
5	100.4	100.8	98.3	99.8	5.6	8.1	6.0	6.4	9.9	0.7	89	71	77	79	1.0	3.1	2.2	2.1	9	10	4	SW 4	WSW 8	SSW 1
6	96.8	98.7	102.1	99.2	6.8	9.9	9.4	8.9	10.9	5.0	86	93	92	90	1.5	0.8	1.0	1.1	10 ●	10	9	SW 6	W 5	W 3
7	101.7	101.9	103.6	102.4	9.0	12.3	10.3	10.5	13.2	8.0	96	89	96	94	0.5	1.5	0.5	0.8	9	10	10	WSW 3	WSW 6	WSW 3
8	106.0	107.2	107.3	106.8	9.8	15.3	9.7	11.1	15.9	8.6	97	68	91	85	0.3	5.7	1.1	2.4	9	4	0	ENE 1	SE 1	E 4
9	105.0	104.0	102.0	103.7	5.6	17.3	10.0	10.7	18.6	4.4	95	48	79	74	0.4	10.2	2.5	4.4	1 ⊙	1 ⊙	0	ESE 3	SSE 7	E 2
10	100.9	100.5	99.6	100.3	8.0	19.3	11.7	12.7	19.7	4.1	89	58	89	79	1.2	9.3	1.5	4.0	0 ⊙	0 ⊙	0	SSE 3	S 6	SSW 1
11	100.1	99.3	98.8	99.4	8.1	17.8	9.6	11.3	18.4	6.7	96	58	88	81	0.5	8.5	1.5	3.5	2 ⊙	2 ⊙	0	S 2	SW 4	SW 1
12	97.6	98.2	103.9	99.9	7.0	16.3	11.7	11.7	16.8	5.8	94	77	94	88	0.6	4.2	0.8	1.9	2 ⊙	7	10	SSW 2	WSW 5	NW 1
13	106.6	105.5	102.9	105.0	6.4	12.3	8.0	8.7	14.9	5.3	100	80	97	92	0.0	2.9	0.3	1.1	10 ═	5	0	S 1	C 0	C 0
14	101.2	101.9	104.2	102.4	7.7	12.5	6.9	8.5	13.4	4.8	98	87	99	95	0.1	1.9	0.1	0.7	8	8 ⊙	0	C 0	WNW 4	C 0
15	106.4	106.5	106.3	106.4	6.4	11.1	8.0	8.4	11.6	5.7	100	67	82	83	0.0	4.3	1.9	2.1	9	6 ⊙	10	C 0	NW 5	E 2
16	104.7	102.7	99.4	102.3	7.6	12.5	8.0	9.0	13.8	6.6	84	62	84	77	1.6	5.5	1.6	2.9	9	2 ⊙	0	ESE 3	SSE 5	E 5
17	95.8	96.3	97.8	96.6	7.4	14.5	9.0	10.0	15.8	5.5	93	76	96	88	0.8	3.9	0.5	1.7	0 ⊙	10	0	SSE 3	WSW 9	SW 2
18	92.8	90.8	89.9	91.2	10.1	14.5	12.7	12.5	16.3	7.7	95	87	89	90	0.7	2.2	1.6	1.5	10	10	0	S 6	SSW 7	SSW 5
19	88.9	87.7	86.1	87.6	10.7	20.3	13.1	14.3	20.8	9.6	81	57	80	73	2.5	10.2	3.0	5.2	9	8	0	SSW 5	S 9	S 4
20	88.2	92.3	94.7	91.7	9.2	8.8	7.6	8.3	13.4	7.1	92	95	97	95	0.9	0.6	0.3	0.6	10	10 ●	10	N 7	WNW 4	C 0
21	95.8	84.7	91.8	90.8	4.8	8.5	6.6	6.6	10.0	3.8	97	77	87	87	0.3	2.6	1.3	1.4	2 ═	9	0	C 0	S 2	ESE 4
22	86.0	83.5	82.1	83.9	4.4	8.4	9.0	7.7	9.7	3.5	92	85	86	88	0.7	1.6	1.6	1.3	4	10	10	SE 6	SE 3	SE 2
23	84.2	87.8	92.8	88.3	6.7	8.8	4.3	6.0	9.9	3.9	97	86	92	92	0.3	1.5	0.7	0.8	10	10	0	C 0	W 5	WSW 2
24	91.7	93.5	99.0	94.7	4.7	6.7	8.2	7.0	9.2	2.1	79	91	97	89	1.7	0.9	0.3	1.0	9	10	4	SSW 6	SSW 6	WSW 3
25	102.4	103.5	103.4	103.1	6.6	11.1	6.4	7.6	11.6	5.7	98	61	81	80	0.1	5.1	1.9	2.4	9	6 ⊙	0	SSW 1	SW 4	SSE 1
26	102.2	101.7	99.8	101.2	4.2	13.5	6.4	7.6	14.4	3.0	95	59	89	81	0.4	6.3	1.0	2.6	4	0 ⊙	0	S 1	SSE 2	SE 3
27	98.3	97.3	96.7	97.4	3.6	12.9	10.1	9.2	13.3	3.1	98	72	91	87	0.1	4.1	1.2	1.8	0	4	10	SW 2	WSW 2	C 0
28	97.6	98.1	98.2	98.0	7.2	9.8	5.8	7.2	10.5	5.1	84	78	92	85	1.7	2.7	0.7	1.7	9	10	0	SSW 2	SSW 4	SSE 3
29	97.4	97.2	96.5	97.0	4.2	12.1	7.8	8.0	13.5	3.0	92	68	86	82	0.6	4.5	1.5	2.2	9	4	4	S 3	SW 4	S 3
30	94.9	93.2	93.4	93.8	7.2	14.7	10.3	10.6	15.3	5.9	90	63	86	80	1.1	6.2	1.7	3.0	7	9	9	C 0	SSW 3	SSW 3
31	93.3	92.2	90.0	91.8	6.9	14.0	8.6	9.5	14.5	6.0	92	72	90	85	0.7	4.4	1.1	2.1	6	6	10	SW 2	SW 6	S 2
M	97.4	97.1	97.6	97.4	6.4	12.0	8.3	8.8	13.4	4.7	93	74	88	85	0.7	4.0	1.3	2.0	6.5	6.9	3.7	2.8	4.6	2.5

Łódź - Lublinek

$H = 184\ m$ $H_b = 186.8\ m$ $h_w = 11\ m$

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DNI	WIDZIALNOŚĆ V	OPAD g	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	1.6	▽⁰ 13⁴⁰–14⁰⁴ 16⁴⁸–17⁰³ ⋙ 12⁰⁷–13³² = 22¹⁶–24
2	7	7.6	.	6.7	●⁰ 18⁴⁸ 21³⁵ ▽¹ 22³⁰–45 ▽–23¹⁰ ●⁰–24 = 0⁰⁰–13⁴⁰ ⌒² n-a
3	7	0.1	.	3.7	●⁰ 0⁰⁰–40 2⁵⁰ 3⁴⁵–6⁴⁰ ●¹–7²³ ●⁰–8²⁵ = 0⁴⁰–2⁵⁰ 8²⁵–40 20⁴⁵–24
4	7	.	.	1.5	= 0⁰⁰–9²⁰
5	8	.	.	7.4	= 4³⁵–6⁴⁵ ≡⁰–7²⁰ = –9³⁰ 22³⁸–24
6	7	.	.	4.4	= 0⁰⁰–12³⁰ 19²⁵–24 ⌒¹ n–a ⌒² p–n
7	7	.	.	8.0	= 0⁰⁰–10³⁷ 19³⁵–24 ⌒¹ n–a
8	7	.	.	10.5	= 0⁰⁰–11⁴⁵ ⌒¹ n–a
9	7	1.2	.	10.0	= 5²⁰–9³⁰ 19⁴⁶–24
10	6	0.1	.	.	●⁰ 5⁴⁰ 6¹⁵–8²⁴ ●⁰ 9⁴⁵–11⁴⁰ 12¹⁰–13¹⁷ = 0⁰⁰–5⁴⁰ 8²⁴–9⁴⁵ 13¹⁷–14²⁰ 21¹⁵–24
11	7	0.1	.	6.5	●⁰ 22³⁰–23³⁰ = 0⁰⁰–20 ≡¹–14⁵ ≡²–8⁴⁵ = –13³⁰ 20³⁰–22³⁰
12	8	0.0	.	5.4	●⁰ 0²⁵–2³⁰ ▽¹ 13³⁰–50 ⩫ 13³⁰–50 = 2³⁰–5⁴⁰
13	8	.	.	6.7	⋙ 13⁴⁰–14³⁶
14	8	7.8	.	4.8	●⁰ 2⁰⁶–3⁴³
15	7	3.6	.	.	●⁰ 1²⁵ 2³⁰–5³⁷ ●¹–6⁴⁰ ●⁰–7¹⁰ ●¹–9¹⁵ ●⁰–9³⁵ ●¹–10⁰⁷ ●⁰–11²⁸ 12¹² 13²² 16³⁸ ▽ 17¹⁰–25
16	7	0.3	.	2.3	▽⁰ 17⁴³–58 = 5³²–9⁴⁰ ⌒ 17⁴⁵–55
17	5	6.2	.	.	●⁰ 13²⁰–14⁴⁵ 15⁴⁵ 16³⁰ ▽⁰ 16⁵⁰ 18²⁰ 19⁴⁸–20⁴² 20⁴⁷–21²⁰ ▽¹–21³² ▽⁰–23⁰⁵ ▽¹–23²⁵ ▽⁰–23⁴⁰ = 2³⁰–10⁴⁰ 23⁴⁰–24 ⌒¹ n–11³⁰
18	6	1.5	.	.	▽¹ 1⁴⁰–50 ▽⁰–2²² 4³³–42 11¹⁰–12⁰⁵ 16²⁰–17⁴⁰ = 0⁰⁰–1⁴⁰ 4⁴²–13¹⁵
19	7	3.1	.	4.5	●⁰ 13⁵⁰ 14⁰⁵–19³⁵ ●¹–21¹⁵ ●⁰–22⁴⁵ = 6³⁰–11²⁰ 22⁴⁵–24
20	8	0.2	.	1.3	●⁰ 5⁴⁵ 8³⁰–11³⁵ = 0⁰⁰–a
21	8	.	.	7.9	≡⁰ 5⁴⁵–7²⁵ = –9²² 18²¹–24
22	6	2.2	.	0.3	●⁰ 8⁰⁴–08 ●¹–8²¹ ●⁰–12¹⁰ ▽⁰ 17³⁰–55 = 0⁰⁰–8⁰⁴ 12¹⁰–14¹⁵ 16³⁵–24
23	6	13.3	.	0.4	▽⁰ 11²²–30 12³⁹–13²⁰ ●⁰–14²⁵ ●¹–14³⁸ ●⁰–14⁵² 15⁵⁰ 16⁴⁸ ●¹ 17⁰⁵–45 ●⁰ 18³⁵ 20²⁵–23⁵⁰ ⩤ 1¹⁰–45 ⋙ 19³⁰–50
24	5	14.2	.	1.6	●⁰ 3²⁰–4⁴⁵ ●¹–5¹⁰ ●⁰–6²⁵ ▽⁰ 11⁴⁰–48 ●⁰ 12²⁵–13²⁰ ●¹–15⁴⁰ ●⁰–17⁴⁵ [23.IX: = 0⁰⁰–11⁴⁰
25	8	.	.	8.9	⋙ 6³⁰–14³⁰
26	8	0.0	.	6.5	▽⁰ 17²⁵–35 = 4³⁰–8²⁰ ⌴¹ n–a
27	8	2.6	.	4.0	●⁰ 20¹⁵–24 ⋙ 20⁵⁰–21¹⁵ 23²⁰–24 = 0⁰⁰–8³⁵ ⌴⁰ n–8⁴⁰
28	7	0.9	.	3.0	●⁰ 0⁰⁰–3³⁰ ▽⁰ 12⁵⁵–14¹⁵ 16³⁰–35 ▽¹–16⁴² ▽⁰–16⁴⁶ ⋙ 0⁰⁰–13²⁰ 15¹⁵–16⁴⁰
29	6	12.7	.	.	▽⁰ 0⁵³–10² ●⁰ 8⁴²–9³³ 12²⁸–15¹⁶ ●¹–17²⁵ ●⁰–20³⁴
30	7	0.6	.	0.2	●⁰ 0²⁵–2⁴⁰ ▽⁰ 8¹²–20 9⁴⁶–10¹⁶ 10⁴⁰–48 ●⁰ 11²³–12¹⁵ ▽⁰ 15³⁰–16¹⁰ 16⁵³–17²³ = 2⁴⁰–4³⁰
31					
Σ	–	78.0	–	118.1	UWAGI

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1	7	1.0	.	5.8	▽⁰ 11⁰⁶–13 17⁴⁰–55 ▽¹–19²⁰ ▽⁰ 20¹⁰–25 = 4²⁵–5⁴³ ≡–6¹⁰ = –8³⁰ 22³⁰–24
2	7	.	.	4.2	= 0⁰⁰–5¹⁰ ≡⁰–5³⁵ ≡¹–9³⁰
3	7	0.1	.	4.5	= 5³⁰–12²⁰ ⌴⁰ n–a
4	8	2.2	.	5.0	●⁰ 2⁰⁵–40 ▽⁰ 9²⁰–30 ▽¹–9³⁶ ▽⁰–9⁴⁵ ▽¹ 10⁴⁵–57 ▽⁰–11⁰⁴ ▲ 12³³–38 ⋙ 12²⁵–38 13⁴⁵–14²⁵ 14⁵⁰–15³⁰ = 24⁰–3⁴⁸
5	8	0.0	.	1.8	
6	6	0.4	.	.	●⁰ 4⁴⁰ 6³⁰ ●¹–7²⁵ ●⁰ 8³⁰–9⁰⁰ 14²³–38 = 9⁰⁰–15³⁰
7	6	.	.	.	= 5³⁰–24
8	8	.	.	5.9	= 0⁰⁰–5³⁰ ≡–6³⁵ = –8⁴⁰ 17³⁰–24
9	8	.	.	10.0	= 0⁰⁰–8²⁵ ⌒ n–a
10	6	.	.	8.5	= 0³⁰–11⁴⁰ ∞–14⁵⁰ = 17¹⁵–24 ⌒⁰ n–a 20⁰⁰–24
11	7	.	.	9.1	= 0⁰⁰–9²⁰ 17²²–24 ⌒⁰ 0⁰⁰–a
12	7	.	.	4.8	= 0⁰⁰–7³⁰ 13¹⁵–24 ⌒⁰ n–a
13	6	.	.	2.1	≡¹ 0⁴⁵–9²⁰ = –14³⁰ ∞–17¹⁵ = –24 ⌒⁰ n–a
14	5	0.2	.	0.2	●⁰ 22⁴⁰ 23³⁰–24 = 0⁰⁰–23³⁰ ≡⁰–24 ⌒ n–na
15	8	.	.	4.9	●⁰ 0⁰⁰–1⁴⁵ 55 ≡⁰ 0⁰⁰–6⁴⁰ = –9²³
16	7	.	.	5.9	= 5¹⁸–8³⁰ 16²⁰–24
17	6	.	.	3.8	= 0⁰⁰–24 ⌒ n–a
18	6	1.0	.	.	●⁰ 7⁴⁰ 9⁴⁵–11⁴⁰ = 0⁰⁰–19⁴⁵ ⌒⁰ n
19	7	.	.	3.8	= 4⁴⁵–9²⁰ 16³⁰–24
20	6	2.7	.	.	●⁰ 10²⁵ 11³⁰–17²⁵ 21⁴⁰ 22³⁰–23⁴⁵ = 0⁰⁰–6³⁵ 8³⁰–10²⁵ 23⁴⁵–24
21	7	.	.	1.8	= 0⁰⁰–30 ≡⁰ 6²⁰–30 ≡¹–8¹⁵ = –12²⁰ 16⁴⁰–21¹⁰
22	7	0.0	.	.	●⁰ 10³⁵ 12⁰⁰ = 5³⁰–12³⁰ 16³⁰–18⁴⁰
23	6	.	.	1.0	= 0³⁰–5²⁰ ≡–6²⁵ = –18³⁰ 21⁴⁰–24
24	6	0.2	.	.	●⁰ 9⁴⁰ 12³⁵ 13³⁵ 17³⁰ = 0⁰⁰–3¹⁰ 5³⁰–24
25	7	.	.	3.9	= 0⁰⁰–10²⁰ 22⁵⁰–24
26	6	.	.	7.3	= 0⁰⁰–13⁴⁰ ∞–16⁴⁰ = –24
27	6	.	.	4.4	= 0⁰⁰–22⁴⁰ ⌴ n–7⁴⁰
28	6	.	.	.	= 3³⁵–20³⁰
29	6	.	.	3.3	= 1³⁰–13³⁵ 16⁴⁰–20²⁰ 23²⁰–24 ⌒ n–a
30	7	0.0	.	3.9	●⁰ 23⁴⁰ 24 = 0⁰⁰–11⁴⁰ 15⁴⁵–23⁴⁰
31	6	.	.	5.4	●⁰ 0⁰⁰–1⁴⁰ = 0⁰⁰–24 ⌓ 17⁴⁵–20¹⁰
Σ	–	7.8	–	111.3	UWAGI

Łódź–Lublinek $\varphi = 51°44'$ $\lambda = 19°24'$ Listopad – Novembre 1957

DNI	CIŚNIENIE P−				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	85.6	84.7	87.3	85.9	5.2	13.1	9.8	9.5	13.8	4.2	95	67	82	81	0.4	5.0	2.2	2.5	4	0 ⊙	10	S 2	SSW 6	S 4
2	89.8	91.1	92.3	91.1	5.4	10.7	8.0	8.0	11.6	4.6	97	73	94	88	0.3	3.6	0.6	1.5	9	8	9	C 0	NNW 2	C 0
3	93.3	93.1	92.4	92.9	7.2	10.9	9.0	9.0	11.6	6.5	94	86	95	92	0.6	1.8	0.7	1.0	10	7 ⊙	10	C 0	C 0	ESE 5
4	91.6	91.1	91.8	91.5	7.2	16.3	10.5	11.1	17.0	6.6	96	72	95	88	0.5	5.3	0.7	2.2	4	2 ⊙	2	E 3	SE 5	ESE 3
5	90.4	87.7	87.8	88.6	6.0	15.5	11.3	11.0	16.6	5.1	98	66	82	82	0.2	6.0	2.5	2.9	2	3 ⊙	2	E 7	ESE 6	ESE 4
6	87.4	88.1	87.5	87.7	9.0	15.8	11.7	12.0	16.3	7.5	90	65	82	79	1.1	6.2	2.5	3.3	6	7	10	ESE 6	SE 6	ESE 6
7	84.7	84.8	86.4	85.3	10.3	14.1	12.3	12.2	15.5	9.5	86	74	87	82	1.7	4.3	1.9	2.6	9	9	10	ESE 6	SSE 5	SSE 2
8	86.4	86.0	86.0	86.1	10.0	14.9	10.0	11.2	15.0	9.3	87	71	87	82	1.6	4.8	1.6	2.7	8	5 ⊙	9	E 5	ESE 5	ESE 5
9	84.7	84.8	86.9	85.5	6.2	10.4	10.0	9.2	12.2	5.2	98	86	91	92	0.2	1.8	1.1	1.0	10	9	8	E 5	E 3	E 3
10	88.3	89.0	90.6	89.3	5.2	10.0	9.2	8.4	10.6	4.8	98	89	97	95	0.1	1.3	0.3	0.6	10 ≡	6 ⊙	10	E 2	E 4	ENE 5
11	92.4	94.0	96.6	94.3	8.7	9.0	6.4	7.6	9.5	6.0	88	81	84	84	1.3	2.2	1.6	1.7	10 ●	10	10	ENE 5	ENE 9	NE 10
12	100.1	102.5	105.7	102.8	4.8	5.5	3.8	4.5	6.9	3.0	79	83	70	77	1.8	1.5	2.4	1.9	10	10	3	ENE 9	ENE 9	ENE10
13	107.0	107.7	108.5	107.7	1.7	1.0	-1.8	-0.2	4.1	-2.2	83	68	78	76	1.1	2.1	1.2	1.5	10	10	10	NE 5	ENE 3	N 4
14	108.2	109.1	110.5	109.3	-3.0	-2.1	-2.2	-2.4	-1.7	-3.8	84	81	87	84	0.8	1.0	0.7	0.8	10	10	10	E 1	ENE 1	ESE 3
15	110.5	109.4	107.9	109.3	-2.9	0.2	-2.4	-1.9	1.3	-4.0	84	68	82	78	0.8	2.0	0.9	1.2	10	2	0	ESE 4	S 3	C 0
16	107.1	108.1	109.6	108.3	-0.8	0.0	0.2	-0.1	0.7	-4.7	91	94	94	93	0.5	0.4	0.4	0.4	10	10	10	C 0	C 0	ENE 1
17	110.2	110.0	111.5	110.6	0.0	1.1	0.8	0.7	1.9	-1.0	88	85	85	86	0.7	1.0	1.0	0.9	10	10	10	ENE 5	ENE 5	E 3
18	110.8	110.1	109.5	110.1	1.0	2.2	1.6	1.6	2.5	0.2	77	63	78	73	1.5	2.7	1.6	1.9	10	10	10	E 4	ESE 5	SE 1
19	110.3	112.1	115.1	112.5	0.8	1.4	1.2	1.2	1.9	-0.3	81	76	66	74	1.3	1.7	2.3	1.8	10	10	10	E 4	E 5	ENE 4
20	116.0	116.5	116.6	116.4	1.1	4.0	-1.8	0.4	4.4	-2.3	70	59	85	71	2.0	3.3	0.9	2.1	10	1 ⊙	0	E 6	ESE 7	ESE 3
21	115.8	113.8	109.8	113.1	-4.7	4.1	-2.4	-1.4	5.6	-5.3	93	59	89	80	0.3	3.3	0.6	1.4	0	0 ⊙	0	C 0	SSE 1	SE 2
22	102.7	98.7	96.0	99.1	-1.4	4.0	0.8	1.0	4.5	-4.8	76	59	85	73	1.3	3.3	1.0	1.9	0	0 ⊙	10	S 5	S 9	S 3
23	95.2	94.3	95.2	94.9	0.6	1.6	2.6	1.8	3.3	-0.3	90	83	91	88	0.6	1.2	0.7	0.8	10	6	10	SSW 4	SW 5	WSW10
24	99.4	98.6	97.4	98.5	1.6	3.0	4.5	3.4	4.8	0.2	91	88	93	91	0.7	0.9	0.5	0.7	10	10 ●	10 ●	W 7	WSW 8	W 10
25	95.6	96.0	97.9	96.5	4.7	5.2	6.2	5.6	6.3	3.6	95	95	95	95	0.4	0.4	0.5	0.4	10 ●	10 ●	10 ●	WSW 9	WSW 8	WSW 6
26	99.1	99.7	98.2	99.0	6.4	6.5	6.2	6.3	6.8	5.3	97	97	95	96	0.3	0.3	0.5	0.4	10	10	10 ●	WSW 5	WSW 7	W 6
27	93.6	92.3	95.5	93.8	5.2	6.9	5.4	5.7	7.6	4.4	95	90	80	88	0.4	1.0	1.8	1.1	10	10 ●	10	W 9	W 10	W 6
28	92.2	88.9	83.6	88.2	7.7	7.2	7.6	7.5	8.4	4.3	97	94	93	95	0.3	0.6	0.7	0.5	10 ●	10 ●	10 ●	W 8	W 9	WSW12
29	84.0	87.7	100.3	90.7	2.8	0.0	-7.1	-2.8	8.0	-7.8	86	94	82	87	1.1	0.4	0.6	0.7	9	10 ⚹	10 ⚹	NW 9	NW 10	NNW12
30	106.1	106.2	106.2	106.2	-7.0	-4.2	-6.6	-6.1	-3.9	-9.5	80	63	83	75	0.7	1.6	0.6	1.0	1	2 ⊙	0	NNW 8	N 10	N 6
31																								
M	98.0	97.9	98.7	98.2	3.3	6.3	4.2	4.5	7.4	1.5	89	78	86	84	0.8	2.4	1.2	1.5	8.1	6.9	7.8	4.8	5.5	5.0

Grudzień – Décembre

1	106.7	105.5	104.2	105.5	-9.3	-1.4	-2.9	-4.1	-1.1	-10.0	88	74	93	85	0.4	1.4	0.3	0.7	7	9	10 ⚹	NW 2	WNW 3	W 2
2	103.4	103.5	104.1	103.7	-2.4	-1.6	-1.5	-1.8	-1.2	-3.8	96	94	94	95	0.2	0.3	0.3	0.3	10	10 △	10	C 0	C 0	NNW 1
3	100.1	97.4	98.1	98.5	-1.0	0.8	1.2	0.6	1.5	-2.0	97	98	98	98	0.2	0.2	0.2	0.2	10 ⚹	10 ≡	10 ●	C 0	NW 2	N 3
4	100.1	99.6	99.4	99.7	0.2	1.2	1.0	0.8	1.5	-0.3	100	98	100	99	0.0	0.2	0.0	0.1	10 ≡	10 ●	10 ●≡	C 0	NW 1	W 1
5	95.4	95.1	98.0	96.2	2.4	4.2	3.6	3.4	4.7	-0.6	98	92	88	93	0.2	0.6	0.9	0.6	10 ●	9	10	W 5	WNW 7	NW 5
6	102.1	103.4	102.2	102.6	1.1	1.5	-1.6	-0.2	3.9	-2.2	92	80	87	86	0.5	1.4	0.7	0.9	9	5	0	N 4	NNW 2	C 0
7	94.2	91.0	85.2	90.1	-2.2	0.5	-2.2	-1.5	1.0	-3.9	85	80	91	85	0.8	1.2	0.5	0.8	6	5 ⊙	10	SSE 5	SSW 4	C 0
8	72.4	64.9	56.5	64.6	-0.4	1.5	5.8	3.2	6.1	-2.9	92	92	94	93	0.5	0.5	0.6	0.5	10 ⚹	10 ⚹	10	S 8	SSW 9	SW 8
9	54.7	62.6	75.1	64.1	5.9	3.6	-1.0	1.9	8.3	-1.5	79	85	81	82	2.0	1.2	1.1	1.4	10	9●△	6	SW 12	W 12	W 7
10	76.5	74.9	84.1	78.5	-3.8	-0.1	-5.7	-3.8	0.6	-6.3	94	80	82	85	0.3	1.2	0.7	0.7	10	7	0	SW 1	SW 6	WSW 6
11	87.4	85.3	81.2	84.6	-8.5	-3.4	-2.6	-4.3	-2.3	-9.8	80	63	79	74	0.6	1.8	1.1	1.2	0	10	10	S 1	ESE 6	NE 8
12	76.3	75.5	75.1	75.6	1.2	2.4	1.6	1.7	3.5	-4.1	83	89	94	89	1.2	0.8	0.4	0.8	10	9	0	ESE 6	E 6	E 3
13	72.7	69.9	63.8	68.8	3.6	6.2	5.2	5.0	6.9	0.7	95	86	92	91	0.4	1.3	0.7	0.8	9	9	10 ●	ESE 5	SE 3	E 3
14	59.4	66.3	78.1	67.9	4.5	1.7	-2.4	0.4	6.3	-2.9	98	98	93	96	0.1	0.1	0.3	0.2	10●≡	10 ●	10 ⚹	E 1	NW 4	NNE 5
15	90.1	97.3	104.0	97.1	-5.9	-7.5	-10.0	-8.4	-2.1	-11.5	89	84	81	85	0.4	0.5	0.5	0.5	10 ⚹	8	0	NNE 7	NE 7	ENE 4
16	106.5	106.8	106.8	106.7	-12.4	-8.3	-12.2	-11.3	-7.8	-13.5	85	75	85	82	0.4	0.8	0.4	0.5	0	0	0	E 2	NE 5	NE 6
17	102.2	100.3	100.0	100.8	-11.5	-7.9	-10.0	-9.8	-7.3	-15.1	86	87	94	89	0.4	0.4	0.2	0.3	8	10	10 ≡	ENE 4	E 2	C 0
18	100.8	100.8	102.3	101.3	-8.1	-7.7	-7.1	-7.5	-6.7	-10.4	95	96	85	92	0.2	0.1	0.5	0.3	10	10	10	C 0	N 3	SE 2
19	102.8	104.7	108.3	105.3	-6.8	-4.0	-2.6	-4.0	-2.1	-8.0	91	89	91	90	0.3	0.5	0.5	0.4	10	10	10	SE 2	ESE 4	C 0
20	109.5	111.1	110.4	110.3	-0.4	0.8	0.2	0.2	1.3	-5.6	98	98	98	98	0.1	0.2	0.1	0.1	10 ≡	10	10	SSE 3	WSW 4	SSW 5
21	106.7	105.1	106.1	106.0	-1.0	1.9	1.2	0.8	2.4	-2.2	93	82	89	88	0.4	1.3	0.8	0.8	0	6	10	SW 7	SW 8	SW 7
22	105.2	104.8	104.1	104.7	0.7	1.2	0.6	0.8	1.6	0.2	96	89	96	94	0.2	0.8	0.3	0.4	10	10	10	SW 3	S 3	S 4
23	100.5	98.3	96.7	98.5	-2.7	-0.2	-4.2	-2.8	0.9	-4.8	89	74	79	81	0.6	1.5	0.9	1.0	4	10 ⊙	0	SE 5	ESE 6	SE 5
24	95.4	95.6	97.2	96.1	-6.1	-0.8	-3.4	-3.4	-0.3	-6.8	89	75	85	83	0.4	1.4	0.7	0.8	2	7	0	SSE 3	SSE 2	SE 2
25	97.5	96.4	97.9	97.3	-5.1	2.0	-1.0	-1.3	2.4	-6.0	90	76	95	87	0.4	1.7	0.3	0.8	0	8	4	SE 2	S 4	S 4
26	100.3	101.9	103.8	102.0	-1.0	1.5	0.0	0.1	1.9	-3.2	89	83	94	89	0.7	1.1	0.4	0.7	9	10	10	SW 3	WSW 3	SW 3
27	103.6	102.4	101.9	102.6	0.8	2.2	1.2	1.4	3.3	-0.8	94	87	90	90	0.4	1.0	0.7	0.7	10	9	8	SW 3	SW 5	SW 4
28	97.3	94.1	90.0	93.8	-0.2	0.9	-0.4	0.0	2.4	-1.8	94	90	90	91	0.4	0.6	0.6	0.5	0	9	9	SW 4	SW 5	SW 7
29	86.8	86.0	82.7	85.2	0.6	1.6	1.5	1.3	2.3	-1.4	94	91	85	90	0.4	0.7	1.0	0.7	10	10	10	WSW 5	SW 7	WSW 9
30	78.2	76.4	74.5	76.4	2.2	2.2	2.6	2.4	3.3	-0.1	84	91	84	86	1.2	0.7	1.2	1.0	10 ●	9	9	SW 9	SW 9	SW 10
31	78.5	79.8	79.9	79.4	0.4	1.2	0.2	0.5	2.9	-0.6	90	87	94	90	0.6	0.9	0.4	0.6	10	7 ⊙	10	W 7	WSW 8	SW 5
M	92.4	92.2	92.6	92.4	-2.1	-0.1	-1.4	-1.2	1.2	-4.6	91	86	90	89	0.5	0.9	0.6	0.7	7.5	8.5	7.3	3.8	4.8	4.2

Łódź – Lublinek $H = 184\ m$ $H_b = 186{,}8\ m$ $h_w = 11\ m$ Listopad – Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	6.1	= 0⁰⁰–11³⁰ 16³⁰–18³⁰ . ⌒¹ n – a
2	6	5.0	.	0.5	●⁰ 23⁴⁵–24 . = 3³⁰–24 . ⌒ n – a
3	5	.	.	1.0	●⁰ 0⁰⁰...30–3³⁰ ●¹–5³⁰ . = 0⁰⁰–24
4	7	.	.	6.4	= 0⁰⁰–10³⁰ 15⁴⁵–24 . ⌒¹ n – a ⌒⁰ 20³⁰–23⁰⁰ ⌒¹–24
5	7	.	.	6.2	= 0⁰⁰–5⁶⁵ ≡⁰–6⁴⁰ = –12³⁰ . ⌒¹ 0⁰⁰– na ⌒²–11³⁰
6	7	.	.	2.9	= 5³⁰–9³⁰
7	7	0.0	.	0.7	●⁰ 14⁴⁵ 15⁴⁵–17³⁰ 19⁴⁵–20³⁸
8	7	.	.	2.8	= 6³⁰–12³⁰ 16¹⁰–24
9	6	.	.	1.1	= 0⁰⁰–14³⁰ 15³⁰–21³⁰
10	6	0.0	.	1.5	= 2³⁰–6³⁰ ≡¹–7⁴⁵ ≡²–9³⁰ ≡¹–9⁴⁰ ≡⁰–9⁵⁰ = –17⁵⁰ ≡⁰–18⁴⁰ = –24
11	7	0.0	.	.	●⁰ 6⁴⁰ 7⁵⁰ . = 0⁰⁰–9⁵⁰
12	6	0.0	.	.	●⁰ 3⁴⁵ 4³⁵ 10³⁵ 12¹⁰ 13²⁵ 14³⁰ . = 9²⁰–18³⁰
13	7	.	.	.	= 16³⁰–19¹⁵
14	5	.	.	.	= 6³⁰–24
15	7	.	.	4.0	= 0⁰⁰–9³⁰ 15¹⁵–24
16	4	.	.	.	= 0⁰⁰–24
17	6	.	.	.	= 0⁰⁰–21³⁰
18	7	.	.	.	= 6³⁰–10⁴⁰
19	7	.	.	.	= 6³⁰–10⁵⁰ 15⁴⁰–21⁵⁰
20	7	.	.	6.9	∞ 15¹⁵–16³⁵
21	7	.	.	6.1	= 5¹⁵–12³⁰ 15²⁰–24 . ⌒¹ n – 10⁰⁰ ⌒⁰ 20³⁰– n/p ⌒¹–24
22	6	.	.	6.1	= 0⁰⁰–24 . ⌒¹ 0⁰⁰– a ⌒⁰–12¹⁵
23	6	0.2	.	0.2	✳⁰ 9⁴³ 11⁴⁰ ✳⁰ 12¹²–35 ●⁰ 14⁴⁰ 19¹⁰ 21⁵⁰ 22⁴⁰ . = 0⁰⁰–9⁴³
24	6	4.1	.	0.1	●⁰ 12²⁵–19³⁵ 20⁴⁵ 21⁴⁰ . = 8¹⁵–10³⁰ 22³⁰–24
25	5	3.8	.	.	●⁰ 0²⁰–12²⁵ ●●⁰–14²⁰ ●⁰–17⁴⁰ ●●⁰–24 . = 0⁰⁰–20
26	5	1.9	.	.	●●⁰ 0⁰⁰–20 ●⁰–3³⁰ ●⁰–6⁴⁰ ●¹–7³⁸ ●⁰–11³⁵ 12³³ 13³⁴ 14¹⁶ ●⁰–14²⁶ ●●⁰–17¹⁷ ●⁰–19⁴⁰ 20³⁰ 24 . = 12³³–13³⁴ 19⁴⁰–20³⁰
27	6	3.9	.	.	●⁰ 0⁰⁰...30 ¹45–4³⁰ 5⁴⁵ 6³⁵ 9³⁰–12³⁰ ●⁰ 16⁴⁰ . = 4³⁰–5⁴⁵ 6³⁵–9³⁰
28	5	3.9	.	.	●⁰ 1⁴⁵–3¹⁵ ●¹–8³⁵ ●⁰ 9⁵⁰ 10¹⁰–13¹⁵ ●●⁰–14³⁰ ●⁰–15³⁵ 18⁴⁰–21⁴⁰ . = 15³⁵–18⁴⁰ ≫ 20¹⁰–24
29	5	0.1	.	.	●⁰ 0¹⁵–45 1⁴⁰ 2³⁵ 3³⁰ ▽⁰ 5⁵³–6⁰⁵ 6¹⁵–25 ✳⁰ 11¹⁸–35 ⛛⁰–12³⁰ ⛛⁰–13³⁵ ✳⁰ 16³⁰ 18³⁰ ✳⁰–21¹⁵ . ≫ 0⁰⁰–5³⁰
30	8	0.0	.	(6.5)	✳⁰ 15²⁰...38 **29.XI:** 7⁵⁰–22¹⁰ (por. do 18 m/sek)
31					
Σ	–	22.9	–	59.1?	UWAGI:

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1	8	0.2	.	1.3	✳⁰ 19¹⁵–22³⁵ 23²⁰ 24
2	4	0.6	.	.	✳⁰ 0⁰⁰–4³⁰ ● 9⁵⁵–10²⁰ (marznąca) △–16³⁰ . = 16³⁰–24
3	2	1.1	1	.	✳⁰ 4²⁰–7³⁰ △⁰ 8²⁰–9²⁰ ✳⁰–10²⁰ ✳⁰–10³⁵ ●⁰–12³⁰ ●¹–13³⁵–17¹⁰ ●⁰–19¹⁰ 20⁴⁵ △⁰ 23⁴⁰–24 = 0⁰⁰–4²⁰ ≡ 18³⁰–18⁴⁵
4	5	2.5	.	.	△⁰ 0⁰⁰–15 ●⁰ 1⁴⁰ 5⁴⁰–6³⁵ ●● 8⁴⁵–9¹⁰ ✳⁰–9³⁰ 11¹⁸–25 ●⁰ 12¹⁰–16⁴² 17²⁰ 18²⁵–21⁴⁰ . = 1⁴⁰–6³⁵ ≡¹–12²⁰ ≡⁰–12³⁵
5	7	0.2	.	.	●⁰ 1⁴⁵ 2²⁰–4⁴⁰ ●⁰–8⁰⁵ . = 0⁰⁰–1⁴⁵ ≡⁰ 7¹⁵–9⁴⁰ = –12¹⁰ **3.XII:** ≡⁰–19¹⁰
6	7	.	.	2.5	= 19³⁰–24 **4.XII:** = –13⁰⁵ ≡¹–19³⁵ ≡⁰–21¹⁵ = –24
7	7	0.6	.	3.4	= 0⁰⁰–10³⁰ 15⁴⁰–24 . ⌒² n – a . ⛛ 20⁴⁰–22⁴⁵ ⌣–23⁵⁰
8	6	5.7	1	.	●3³⁵–4²⁰ (marznąca) ✳⁰–7⁴⁰ 8³⁸ ✳●⁰ 12³⁰–13²⁰ ✳⁰–14²⁵ ●⁰–16³⁰ ●¹–20³² . = 0⁰⁰–30
9	6	1.2	.	.	✳⁷ 7⁵⁰–8³⁵ ●¹–10²⁰ ✳⁰ 10⁵⁰ ✳¹ 12²⁰–40 ⛛●⁰ 13²⁰ ✳¹–13⁴⁰ ✳⁰ 14⁴⁵–15¹⁰ ✳² 16⁰⁰ ✳¹–16³⁵ . ≫ 18⁰–9¹⁰ 10¹⁵–16¹⁰
10	7	0.7	.	0.9	✳⁰ 13¹⁵–35 ✳¹–14¹⁰ ✳⁰–14²⁵ ✳² 15³⁰ ✳⁰ 16¹⁰ . ≫ 16¹⁵–17³⁰ . = 7³⁵–10¹⁵ **9.XII:** (15³⁰–16¹⁰ por. 17 m/sek)
11	6	.	2	0.8	= 7³⁰–11²⁰ ∞–14⁴⁰ = –17⁴⁰
12	6	.	2	0.1	= 7³⁵–24
13	6	3.0	.	.	●⁰ 20¹⁰ 21¹⁵–24 . = 0⁰⁰–24
14	6	5.6	.	.	●⁰ 0⁰⁰–13¹⁰...45 14⁴⁵–18³⁰ ✳⁰–24 . = 0⁰⁰–6⁴⁰ ≡⁰–10⁴⁰
15	7	0.4	3	.	✳⁰ 0⁰⁰–8⁴⁰ . = 8⁴⁰–12³⁰
16	7	.	3	4.9	= 7⁵⁰–9⁴⁰
17	6	.	3	.	= 7³⁵–19⁵⁰ ≡⁰–24
18	6	0.0	3	.	✳⁰ 13⁴⁵ 15¹⁵ 16⁴⁰ 17³⁵ . ≡⁰ 0⁰⁰–20 ≡ V – 1⁴⁵ = –24
19	5	0.0	3	.	△ 11¹⁵–12²⁰ . = 0⁰⁰–24
20	4	.	3	.	●⁰ 5⁴⁵–6¹⁵ (marznąca) . = 0⁰⁰–5⁵⁰ ≡⁰–6³⁰ ≡¹–9⁴⁵ ≡⁰–11⁴⁵ = –18³⁰ ≡¹–19⁴⁵ ≡⁰–20⁴⁰ = –24
21	6	0.4	1	2.8	●⁰ 23⁵⁰ 24 . = 0⁰⁰–23⁵⁰
22	6	0.0	pł.	.	●⁰ 0⁰⁰ 1⁴⁵–4³⁰ ●⁰ 8⁴⁰ 9¹⁵ 15³⁵ 18²⁰–20³⁵ ●⁰ 21⁴⁵ 22⁴⁰ . = 4³⁰–24
23	6	.	pł.	3.1	= 0⁰⁰–12³⁰ ∞–15³⁰ = –19²⁰ . ⊕ 9⁴⁵–14³⁰
24	6	.	.	4.9	= 6³⁰–24
25	6	.	.	2.3	= 0⁰⁰–24
26	6	.	.	.	= 0⁰⁰–22⁵⁰ ≡⁰–24
27	6	.	.	0.1	≡⁰ 0⁰⁰–25 ≡¹–1⁴⁰ = –24
28	6	1.1	.	1.0	= 0⁰⁰–19⁵⁰
29	6	1.1	2	.	✳⁰ 0²⁵ 1¹⁰ ●⁰–1⁴⁰ ✳¹–2³⁰ ✳⁰–3⁴⁵ ●⁰ 7¹⁵–8³⁵ ●⁰ 15⁵⁰–16⁰⁵ ✳¹ 18⁴⁵–19¹⁰ ✳⁰–19²⁰ ✳⁰ 20¹⁰ 22⁵⁰–23⁵⁰ ✳¹ 24 . = 3⁴⁵–22¹⁵
30	6	3.1	.	.	✳⁰ 0²⁰ 2⁴⁰ ✳⁰–3³⁰ ●⁰ 4²⁰ 5³⁰ 6⁵⁰–7¹⁵ ✳⁰ 7³⁰–55 ●⁰ 10⁴⁵ 12³⁵ 13⁰² 14⁴⁰ 16⁴⁵ 18⁵⁰ 21¹⁵ 22³⁰ . ≫ 0⁰⁰–6⁰⁵ 11⁴⁰–12³⁰ 19³⁵–22⁴⁰
31	7	4.5	.	0.9	△⁰ 9⁴⁵–10⁰⁵ ✳⁰ 10³⁰–40 ✳¹–11¹⁰ ✳² 11³⁰–12²⁵ ✳¹–12³² ✳⁰ 15⁴⁰–16³⁵ ✳¹ 17⁴⁰–18³⁵ ✳ 21⁴⁰–22³⁰ . = 22³⁰–23¹⁰
Σ	–	32.0	–	29.0	UWAGI: **29.XII:** ≫ 18⁴⁰–19³⁰, 21³⁰–24 **31.XII:** = 7⁵⁵–15³⁰

Wrocław – Mały Gądów $\varphi = 51°08'$ $\lambda = 16°59'$ Styczeń – Janvier 1957

DNI	CIŚNIENIE P - 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.1	100.8	99.2	100.4	-1.1	0.7	0.6	0.2	1.2	-1.5	95	86	88	90	0.3	0.9	0.8	0.7	10	10	10	C 0	ENE 1	E 1
2	96.0	98.7	103.2	99.3	-1.9	-0.3	-1.6	-1.4	0.8	-2.6	100	100	96	99	0.0	0.0	0.2	0.1	10 ≡	9	10	C 0	C 0	C 0
3	106.7	107.1	107.6	107.1	1.0	2.0	-3.3	-0.9	2.8	-3.9	90	85	93	89	0.7	1.1	0.4	0.7	10 ● ≡	10	0	C 0	SSE 2	C 0
4	108.2	110.1	110.1	109.5	-1.7	2.1	-1.4	-0.6	2.9	-6.0	94	80	93	89	0.3	1.4	0.3	0.7	6	10	0	SW 3	SSW 1	C 0
5	109.2	106.4	104.9	106.8	2.6	4.4	5.2	4.4	5.4	-1.9	86	84	94	88	1.1	1.4	0.5	1.0	10	10 ●	10 ●	S 3	SW 6	WSW 4
6	101.0	99.2	102.5	100.9	8.3	10.3	6.0	7.6	10.6	4.7	82	85	79	82	2.0	1.9	2.0	2.0	10	10 ●	1	SW 4	WSW 9	WNW 7
7	107.9	112.2	116.3	112.1	4.6	5.6	5.3	5.2	6.1	3.2	81	74	83	79	1.7	2.4	1.5	1.9	10 ●	9	10	WNW 8	WNW 9	WNW 8
8	115.8	114.6	114.3	114.9	4.2	5.8	6.6	5.8	6.9	3.4	82	70	87	80	1.4	2.8	1.3	1.8	9	10	10	WNW 7	WNW 8	W 7
9	111.0	108.5	105.5	108.3	6.0	8.0	1.4	4.2	8.2	1.0	88	76	91	85	1.2	2.5	0.7	1.5	10	10	2	SW 3	WSW 5	SW 2
10	101.7	101.5	101.9	101.7	4.9	3.0	3.4	3.7	5.8	-0.1	67	91	81	80	2.9	0.7	1.5	1.7	10	10 ●	9	WSW 2	WNW 5	W 9
11	103.4	106.0	108.7	106.0	1.3	2.6	0.8	1.4	3.5	0.4	85	67	85	79	1.0	2.5	1.0	1.5	10	9 ⛆	9	WNW 7	WNW 9	WNW 8
12	104.2	97.6	90.7	97.5	0.6	1.4	1.6	1.3	1.8	-1.4	88	85	76	83	0.8	1.0	1.7	1.2	8	10	10	W 6	SW 4	SW 6
13	89.3	91.4	95.2	92.0	0.9	2.0	-1.1	0.2	2.7	-1.7	87	87	94	89	0.9	0.9	0.3	0.7	10	10	8	SW 3	SW 1	C 0
14	100.4	105.5	110.0	105.3	-0.2	-1.3	-4.5	-2.6	0.8	-4.9	96	86	88	90	0.2	0.8	0.5	0.5	10 ✳	10	10	C 0	NE 8	ENE 7
15	110.4	110.2	111.1	110.6	-5.5	-5.1	-6.1	-5.7	-4.2	-6.3	87	83	89	86	0.5	0.7	0.4	0.5	10 ✳	10 ✳	10 ✳	ENE 4	NE 5	NE 5
16	114.8	117.1	119.2	117.0	-7.3	-7.7	-12.6	-10.0	-5.7	-13.2	85	87	89	87	0.5	0.4	0.3	0.4	10 ✳	10 ⛆	0	N 3	WNW 3	C 0
17	119.4	119.7	118.9	119.3	-14.6	-6.7	-6.7	-8.7	-4.9	-15.4	83	75	80	79	0.3	0.9	0.7	0.6	0	9 ✳	3	C 0	W 1	W 1
18	117.9	117.5	116.3	117.2	-6.5	-6.1	-8.5	-7.4	-5.3	-8.9	97	97	92	95	0.1	0.1	0.3	0.2	10 ⛆	10	0	NW 1	WNW 1	NW 1
19	115.4	116.2	117.3	116.3	-4.2	-1.7	-0.9	-1.9	-0.6	-10.1	96	90	87	91	0.2	0.6	0.7	0.5	10	10	10	NW 2	WNW 3	C 0
20	117.3	116.4	113.3	115.7	-1.3	-1.5	-7.3	-4.4	-0.7	-7.6	84	82	93	86	0.9	1.0	0.2	0.7	10	10	0	WNW 5	WSW 4	S 1
21	110.7	110.8	111.8	111.1	-11.7	2.6	-6.7	-5.6	2.9	-12.2	82	52	80	71	0.4	3.6	0.7	1.6	4	0	0	C 0	SW 6	C 0
22	110.8	108.6	106.3	108.6	-10.5	-0.3	-6.6	-6.0	1.8	-12.3	90	70	75	78	0.3	1.8	0.9	1.0	3	6 ⊙	0	C 0	SE 3	W 2
23	107.0	105.4	102.5	105.0	-10.1	-0.1	-4.1	-4.6	1.9	-12.6	94	63	68	74	0.3	2.3	1.4	1.3	0	1	0	SE 1	ENE 3	C 0
24	97.7	95.3	94.9	96.0	-3.5	0.8	0.8	-0.3	2.0	-5.5	67	64	83	71	1.5	2.4	1.2	1.7	9	10	10	E 2	E 2	C 0
25	95.3	96.5	100.5	97.4	-1.6	3.1	1.1	0.9	3.3	-2.2	78	66	89	78	1.2	2.6	0.7	1.5	10	10	10	S 2	W 3	SW 1
26	105.4	106.2	104.1	105.2	-1.2	6.4	0.4	1.5	6.4	-4.3	91	55	80	75	0.5	4.3	1.3	2.0	1	0	0	WSW 1	S 2	S 3
27	101.6	103.9	107.8	104.4	2.8	7.2	1.0	3.0	7.4	-0.1	86	76	81	81	1.1	2.5	1.3	1.6	10	7	0	SW 5	W 8	W 3
28	106.2	110.4	117.5	111.4	1.2	2.7	0.9	1.4	2.8	-1.2	90	77	92	86	0.7	1.7	0.5	1.0	10 ✳	9	9	W 6	WNW 8	W 1
29	118.0	116.6	114.8	116.5	-2.0	4.4	0.7	1.0	4.6	-2.8	92	60	88	80	0.5	3.4	0.7	1.5	3	2	6	SW 2	SW 3	C 0
30	111.0	108.7	108.2	109.3	-4.3	5.7	2.5	1.6	7.2	-5.5	95	65	89	83	0.2	3.2	0.8	1.4	1	9	10 ●	C 0	S 3	W 1
31	108.7	109.3	107.3	108.4	3.1	6.4	3.2	4.0	6.9	1.5	91	76	83	83	0.6	2.3	1.3	1.4	10	7	10	W 3	SW 3	S 2
M	107.2	107.4	107.8	107.5	-1.5	1.8	-1.0	-0.4	2.8	-4.2	87	77	86	83	0.8	1.7	0.8	1.1	7.9	8.3	5.7	2.7	4.2	2.6

Luty – Février

1	103.7	103.7	104.8	104.1	4.6	6.2	5.2	5.3	6.7	2.6	87	91	95	91	1.1	0.9	0.4	0.8	10 ●	10 ●	10 ●	S 2	S 2	S 1
2	107.9	110.6	112.0	110.2	7.5	9.0	7.0	7.6	9.8	4.8	89	93	97	93	1.2	0.8	0.3	0.8	10	10 ●	10 ≡	SW 1	WSW 3	C 0
3	110.1	109.4	111.8	110.4	4.2	6.9	4.0	4.8	7.3	2.8	97	90	95	94	0.2	1.0	0.4	0.5	9 ≡	9	10	ESE 1	NNE 2	NE 3
4	110.3	109.6	109.3	109.7	3.0	5.9	1.9	3.2	8.4	0.0	90	83	93	89	0.8	1.6	0.5	1.0	10	10	0	SE 4	ESE 1	SW 1
5	109.0	107.7	105.8	107.5	-1.8	8.5	0.6	2.0	11.0	-2.6	98	70	86	85	0.1	3.3	0.9	1.4	0 ≡	1	0	C 0	SE 1	C 0
6	101.8	99.9	100.9	100.9	1.5	8.8	4.8	5.0	9.1	-1.4	87	60	78	75	0.9	4.5	1.9	2.4	1	1	10	S 4	SW 4	SW 4
7	103.4	104.6	104.8	104.3	5.8	8.4	2.3	4.7	9.5	1.8	94	66	86	82	0.6	3.7	1.0	1.8	10 ●	8	10	W 5	W 10	SW 3
8	99.5	95.7	91.1	95.4	4.2	7.8	7.9	7.0	8.6	-0.3	80	82	79	80	1.6	2.0	2.2	1.9	9	10 ●	10 ●	S 6	SW 4	SSW 5
9	89.8	89.3	93.2	90.8	6.4	8.2	5.2	6.2	9.1	4.1	92	90	90	91	0.7	1.1	0.8	0.9	10	10	4	SW 3	WSW 5	W 5
10	94.0	93.7	93.4	93.7	0.4	7.8	2.0	3.0	7.8	-0.1	96	87	94	92	0.3	1.4	0.4	0.7	3	10 ●	4	SW 3	SW 3	SSW 2
11	95.3	98.8	101.4	98.5	5.4	6.4	3.0	4.4	7.3	1.2	84	68	90	81	1.4	3.1	0.8	1.8	10	9	9	WNW 9	WNW 9	WNW 3
12	98.1	94.3	91.3	94.6	1.1	8.8	5.9	5.4	9.4	-1.2	92	64	80	79	0.5	4.0	1.9	2.1	9	5	10	SSE 2	S 8	S 3
13	88.5	84.2	75.8	82.8	3.5	9.1	7.8	7.0	10.2	2.8	90	60	71	74	0.8	4.7	3.1	2.9	8	4 ⊙	10	S 3	SSW 8	S 9
14	74.0	73.7	76.1	74.6	6.6	9.9	2.3	5.3	10.0	1.5	82	71	87	80	1.7	3.6	0.9	2.1	9	9	1	S 5	SW 7	SSW 2
15	76.6	72.2	70.5	73.1	2.0	7.1	6.3	5.4	8.0	1.0	87	80	85	84	0.9	2.1	1.4	1.5	2	10	10 ●	S 4	SE 3	S 5
16	79.9	82.1	87.8	83.3	2.1	7.0	2.3	3.4	8.1	1.2	89	70	95	85	0.8	3.0	0.4	1.4	9	8	8	SW 5	SW 8	SW 2
17	91.8	92.4	93.3	92.5	-1.0	4.4	1.8	1.8	5.3	-2.1	89	73	89	84	0.6	2.3	0.8	1.2	5	10 ●	0	SSW 2	S 2	S 3
18	91.9	86.6	81.2	86.6	-1.7	6.7	4.6	3.6	7.3	-3.4	91	69	97	86	0.5	3.0	0.3	1.3	4	9	10 ●	E 2	SE 5	ENE 2
19	89.2	95.5	99.1	94.6	1.5	3.8	0.3	1.5	4.7	-0.8	91	73	86	83	0.6	2.1	0.8	1.2	10	9	9	WNW 8	WNW 7	S 2
20	98.9	96.8	93.7	96.5	1.4	8.7	3.3	4.2	9.5	-1.1	78	48	79	68	1.6	5.8	1.5	3.0	6	9 ⊙	0	S 4	SSE 5	SE 2
21	93.0	95.7	101.1	96.6	-0.8	7.6	2.2	2.8	7.8	-2.1	96	68	87	84	0.3	3.3	1.0	1.5	9	10	10	C 0	WNW 6	WNW 8
22	103.6	103.2	101.2	102.7	0.3	3.3	-1.1	0.4	4.7	-2.0	92	68	89	83	0.5	2.5	0.6	1.2	10	6	0	WNW 3	NW 3	SSE 1
23	100.9	101.0	99.9	100.6	-5.5	3.0	-2.7	-2.0	3.7	-7.1	97	67	95	86	0.1	2.5	0.2	0.9	7	3	0	C 0	WNW 3	C 0
24	91.5	87.3	88.6	89.1	-2.1	0.4	0.4	-0.2	1.1	-4.7	92	90	88	90	0.4	0.6	0.8	0.6	9	10	10	C 0	ENE 4	N 1
25	93.4	92.8	91.2	92.5	-2.1	1.6	-0.6	-0.4	2.2	-2.5	91	69	98	86	0.4	2.2	0.1	0.9	3	9	10 ✳	NE 2	SE 2	ENE 5
26	100.5	103.5	106.4	103.5	-2.4	0.8	-2.5	-1.6	2.4	-3.2	93	77	93	88	0.3	1.5	0.4	0.7	10	9	4	N 2	NNE 1	SSE 1
27	107.6	108.9	111.5	109.3	-5.7	2.9	0.5	-0.4	3.2	-7.2	90	66	79	78	0.4	2.6	1.3	1.4	1	3	10	SE 1	SE 5	SE 1
28	114.8	117.5	119.7	117.3	-1.1	-1.1	-1.0	-1.0	0.5	-1.8	85	91	93	90	0.9	0.5	0.4	0.6	10	10 ✳	10 ✳	BSE 1	ENE 1	N 3
29																								
30																								
31																								
M	97.1	96.8	97.0	97.0	1.3	6.0	2.6	3.1	6.9	-0.7	90	74	88	84	0.7	2.5	0.9	1.4	7.2	7.9	6.8	2.9	4.4	2.8

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	7	–	= 0⁰⁰–24
2	5	0.0	7	–	= 0⁰⁰–5²⁵ ≡⁰–5⁴⁰ ≡¹–6²⁰ ≡²–10³⁰ =–11³⁵ ≡⁰–12³⁰ =–17⁴⁰ ≡¹–18²⁵ =–19³⁰ ≡¹–20¹⁵ =–24
3	5	0.0	6	–	•⁰5⁴⁰ 6¹⁰ •,⁰–7⁴⁰ · = 0⁰⁰–24 · ⌴ 20¹⁵–24
4	6	.	5	–	= 0⁰⁰–13³⁰ 15⁴⁰–24 · ⌴¹ 0⁰⁰–11¹⁵
5	6	2.9	4	–	•⁰11⁰⁵ 12⁴⁰–19¹⁵ 19³²–21³⁵ 23¹⁵–35 · = 0⁰⁰–20⁴⁰
6	8	6.1	.	–	•⁰0¹⁰ 1⁴⁰ •⁰7³⁰–8³⁵ •⁰9⁰² 11¹⁵–12³⁰ 14²⁵ 15¹⁰–16⁰⁰ ▽¹–16³⁸ •⁰–17¹⁵
7	7	0.0	.	–	▽⁰2⁰²–⁰⁷ ▽¹2³⁰–3⁰⁷ ▽⁰3³⁴–4⁰¹ 4¹⁰–²⁸ •⁰6²⁵ 7⁰⁵ ▽⁰7²²–³⁰ 9⁵⁰–10⁰⁵ 11³⁵–12¹⁰
8	7	0.0	.	–	•⁰20⁴⁰ 23³⁵ · ⩓ 10³⁰–12¹⁵
9	6	.	.	–	= 7³⁵–24
10	6	1.3	.	–	•⁰8³⁰ 9¹⁵–14³⁰ 15¹⁰ · = 0⁰⁰–12⁰
11	7	0.0	.	–	•⁰0⁴⁰ 1¹⁵ ✳▽⁰5³⁵–⁵⁰ 10⁵⁰–11⁰⁵ ✕⁰12⁵⁵–13¹⁰
12	7	2.5	.	–	✳⁰7¹⁰–³⁰ △⁰–8⁴⁰ ✳⁰10¹⁰–²⁵ ✳¹–11⁴⁰ ✳⁰–12³⁰, 13¹⁴–15⁴⁵, 21³⁰–22¹⁵ ✳⁰–24
13	6	0.0	1	–	✳⁰0⁰⁰–2⁴⁰ · = 3¹⁵–4²⁰ 10²⁰–24
14	6	0.2	.	–	✳⁰4⁴⁰ 5¹⁵ 6⁵⁰ 8¹⁰–10³⁸ 18³⁰ 20⁴⁰, 23¹⁰ 24 · = 0⁰⁰–10¹⁰, 12³⁰–24
15	6	0.0	.	–	✳⁰0⁰⁰..³⁵ 2⁴⁰–7¹⁵ 8⁴⁵–24 · = 0⁰⁰–24
16	7	0.0	1	–	✳⁰0⁰⁰–2³⁰ 3²⁰–4¹⁰, 5¹⁰–8³⁵ 9²⁵–10⁴⁰ △–14¹⁵ ✳⁰–16¹⁰ · = 0⁰⁰–8¹⁰, 18³⁰–24
17	6	0.0	.	–	✳⁰12¹⁰–15²⁰ · = 0⁰⁰–13²⁰ 21³⁰–24 · ⌴ n–12¹⁵
18	4	0.0	pż.	–	△ 6⁴⁰–7¹⁵ · = 0⁰⁰–7²⁰ ≡⁰–11⁴⁵ =–14³⁸ ≡⁰–16³⁰ =–24 · V 9⁰⁵–24
19	4	.	pż.	–	= 0⁰⁰–24 · V 0⁰⁰–10¹⁰
20	6	.	pż.	–	= 0⁰⁰–24
21	7	.	pż.	–	= 0⁰⁰–12²⁰, 15³⁵–24 · ⌓ 23⁰⁰–15–53
22	5	.	.	–	= 0⁰⁰–14¹⁰ ∞–16⁴⁵ =–24 · ⌴⁰ n–12⁴⁰ · ⌓ 3⁰⁵–15
23	5	.	.	–	= 0⁰⁰–13⁵⁰ ∞–16⁴⁰ =–24 · ⌴⁰ 0⁰⁰–10¹⁵
24	4	0.0	.	–	△ 15⁴⁰–19³⁵ ✳⁰23⁴⁰–24 · = 0⁰⁰–13³⁰ ∞–16³⁰ =–24
25	5	0.0	pż.	–	✳⁰1⁵⁰ 3²⁵ ✳⁰14³⁵–15⁰⁸ · = 0⁰⁰–24
26	6	2.2	.	–	= 0⁰⁰–7¹⁵ ≡–8⁴⁵ =–11³⁰ ∞–16⁴⁵ =–24
27	7	0.9	.	–	•⁰2³⁵–5⁴⁰ 6³⁵ 9¹⁰–³⁵ = 0⁰⁰–4²⁰
28	8	0.5	.	–	▽⁰5⁰⁵ 8⁴⁸ ▽⁰11³⁵–12¹⁰, 13¹¹–³⁰ 13⁴⁵–14⁰⁵ ▽⁰–14¹⁵ ▽⁰14²²–⁴⁵ ▽⁰–15⁴⁸ •⁰16³⁵ 17⁴⁰
29	7	.	.	–	= 2⁵⁰–4⁴⁰, 17³⁰–24 · ⌴⁰ 7¹⁰–10⁴⁰
30	7	1.9	.	–	•⁰17⁴⁵ 18¹⁵, 19⁴⁰ 21²⁰ · = 0⁰⁰–11⁴⁰ ∞–12⁴⁵ 13³⁰–14³⁰ = 16³⁰–24 · ⌴⁰ n–10¹⁵ · ⊕ 12¹⁰–13⁰⁰
31	6	0.2	.	–	•⁰0⁴⁰–3³⁵ •¹–4¹⁵ •⁰–4⁴⁰ •⁰18⁴⁰ 19³⁰–³⁸, 21³⁰ 22¹⁰, 23¹⁰ 24
Σ	–	18.7	–	–	UWAGI:

Luty – Février

1	5	4.5	.	–	•⁰0⁰⁰ 3³⁰ 6²⁰–13³⁰ 16²⁰–22³⁵ · = 0⁰⁰–24
2	5	0.1	.	–	•⁰10²⁵ 12¹⁰–⁴⁰ 13¹⁵ 15³⁵–16¹⁰ •⁰17³⁰–18¹⁵ · = 0⁰⁰–4⁴⁰ 7¹⁵–16²⁸ ≡⁰–16⁵⁰ ≡¹–17³⁰ ≡²–24
3	5	.	.	–	≡² 0⁰⁰–2²⁰ ≡¹–3³⁰ =–6¹⁰ ≡⁰–8¹⁰ ≡²–9¹⁰ ≡⁰–9⁴⁵ =–24
4	5	.	.	–	= 0⁰⁰–24 · ⌴ 23¹⁵–24
5	6	.	.	–	= 0⁰⁰–6⁴⁵ ≡⁰–8⁴⁰ =–24 · ⌴⁰ 0⁰⁰–9³⁰
6	7	7.1	.	–	•⁰21⁴⁵–24 · = 0⁰⁰–8²⁰, 16⁴⁰–24 · ⌴⁰ n–8⁴⁰
7	7	0.4	.	–	•⁰0⁰⁰–8¹⁵ · = 0⁰⁰–7¹⁰ · ⩔ 19¹⁰–22²⁰
8	8	3.8	.	–	•⁰11⁴⁰ 13³⁰, 15⁵⁵ 17⁴⁰ 18¹⁵–20¹⁵ 22³⁶–24 · = 3²⁵–6³⁵ · ⌴¹ n–7⁵⁰
9	7	2.1	.	–	•⁰0⁰⁰–4³⁸ 10⁴⁰ 11¹⁵–12²⁸ ▽⁰12³⁵–13²⁰, 13³⁰–14⁴⁰ · = 7³⁰–8²⁵ · ⩔ 18³⁰–19³⁰
10	6	0.5	.	–	•⁰12⁰²–13¹⁵ 13⁴⁰ 15¹⁵ · = 7²⁵–10⁴⁵ 16⁴⁰–24 · ⌴⁰ n–10⁰⁰ · ⩔ 18³⁵–19²⁰
11	7	0.0	.	–	•⁰0²⁵..⁴⁰ ▽¹⁴⁵–²⁰⁵ ²²⁵–3²⁰ 4³⁰–5¹⁷ 5³⁵–6¹⁸ 7¹⁵–8²⁰ 9³⁰–⁵⁵ 10³⁸–11³⁰ •⁰15⁴⁸ 16¹⁰ ▽⁰19¹⁰–²⁸ · = 0⁰⁰–3¹⁰
12	7	0.0	.	–	= 1²⁰–3³⁵, 6⁴⁰–12²⁵, 16⁴⁰–18¹⁰ · ⌴⁰ n–8²⁷
13	8	0.0	.	–	•⁰1¹⁰–2³⁸
14	8	.	.	–	•⁰4²⁰..⁵⁵
15	8	0.9	.	–	•⁰17³⁰ 21²⁰, 22¹⁵–⁴⁰ · ⌴⁰ n–9²⁰ · ⊕ 8¹⁰–10¹⁰
16	8	1.3	.	–	•⁰0¹⁰ 1⁰⁵–4⁴⁰ 10⁴⁵ 11¹⁰ ▽⁰16²⁴–17¹⁰, 17⁵⁰–18²⁵, 19⁴⁵–20¹⁵ · ⩓ 2²⁰–4⁴⁰ · = 6³⁵–9⁵⁰
17	6	0.1	.	–	•⁰12⁴⁵ 13⁰⁵, 13³⁵ 14³⁰, 16²⁰..³⁵ · = 4¹⁵–13¹⁰ · ⌴⁰ n–9¹⁵
18	5	17.3	.	–	•⁰18¹⁷–21⁴⁰ •¹–24 · = 5²⁰–24 · ⌴⁰ n–10¹⁵
19	6	0.0	.	–	•¹0⁰⁰–¹⁵ •⁰–2²⁰ ✳⁰–3³⁵ •¹–5¹⁰ •⁰–6⁴⁵, 13⁴⁵ 14¹⁰ · = 0⁰⁰–7¹⁰, 11⁴⁰–24
20	8	.	.	–	= 0⁰⁰–6¹⁰ · ⌴⁰ n–11⁵⁰ · ⊕ 9⁵⁰–12¹⁵
21	8	0.0	.	–	•⁰15⁴⁵ 16³⁰–17²⁵ 18²⁰ · = 4¹⁰–11³⁰ · ⌴¹ n–9⁵⁰ · ⊕ 9³⁰–13¹⁵
22	7	.	.	–	= 6⁴⁵–8⁴⁰, 17¹⁰–24
23	6	.	.	–	= 0⁰⁰–6³⁰ ≡⁰–6⁵⁰ =–10¹⁰ ∞ 11⁴⁵–14¹⁵ =–24 · ⌴¹ n–10¹⁰
24	5	0.0	.	–	✳⁰11⁴⁵ 12¹⁵ 15³⁵ 16⁴⁰ 17⁴⁰ 19³⁰ · = 0⁰⁰–24 · ⌴¹ n–11⁴⁰
25	6	4.0	.	–	✳⁰17⁰²–18³⁰ ✳⁰–22⁵⁵ ✳¹–24 · = 0⁰⁰–13³⁰, 16⁴⁰–24
26	7	.	3	–	✳¹0⁰⁰–³⁰ ✳⁰–1⁴⁰ · = 0⁰⁰–11⁴⁰, 20⁴⁰–24
27	6	.	pż.	–	= 0⁰⁰–24
28	4	1.2	pż.	–	✳⁰7⁰² 8⁵⁰–9¹⁵ ✳¹–9³⁰ ✳²–10²⁵ ✳⁰–11⁴⁰, 12⁴⁰ 14¹⁰–³⁵, 16⁵⁰–20³⁰ 22¹⁰ · = 0⁰⁰–24
29					
30					
31					
Σ	–	43.3	–	–	UWAGI:

Wrocław – Mały Gądów $\varphi = 51°08'$ $\lambda = 16°59'$ Marzec – Mars 1957

DNI	CIŚNIENIE P = 900 –				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	122.2	122.1	121.2	121.8	-7.1	-0.8	-0.9	-2.4	1.2	-11.0	93	87	79	86	0.2	0.7	1.2	0.7	9 ✳	9 ✳	9	NW 2	NE 3	N 1
2	119.1	118.0	115.2	117.4	-2.5	0.9	-3.5	-2.2	1.7	-4.3	93	71	88	84	0.4	1.8	0.6	0.9	9	8	4	NW 2	N 5	C 0
3	111.2	109.2	106.9	109.1	-6.0	1.8	-1.9	-2.0	3.1	-6.5	89	63	83	78	0.4	2.6	0.9	1.3	3 ⊙	6 ⊙	0	NW 1	NNW 2	C 0
4	102.0	98.9	97.0	99.3	-3.3	6.0	2.4	1.9	7.7	-5.3	95	56	73	75	0.3	4.2	2.0	2.2	9	10	8	ESE 1	S 2	WSW 2
5	100.0	100.9	101.2	100.7	-2.2	4.1	-0.7	0.1	6.3	-2.6	98	58	83	80	0.1	3.5	1.0	1.5	5	8	0	NW 1	NW 1	C 0
6	100.6	99.2	97.9	99.2	-6.7	6.7	1.5	0.8	7.5	-7.4	88	46	67	67	0.4	5.3	2.3	2.7	2	0 ⊙	0	C 0	ESE 5	E 1
7	97.5	98.1	99.2	98.3	-1.9	6.8	1.1	1.8	7.5	-3.1	77	50	74	67	1.2	4.9	1.7	2.6	1 ⊙	4	5	ESE 1	ESE 3	ESE 4
8	100.6	101.2	104.4	102.1	-3.5	4.4	-0.1	0.2	5.7	-4.1	83	48	86	72	0.8	4.4	0.9	2.0	7	4	0	ESE 5	ESE 5	E 4
9	109.1	111.5	114.8	111.8	-3.3	3.4	-0.1	0.0	4.4	-3.9	74	45	72	64	1.2	4.3	1.7	2.4	0	1 ⊙	0	E 3	E 7	ENE 3
10	117.3	117.9	118.0	117.7	-5.8	4.6	0.7	0.0	5.7	-6.7	92	47	69	69	0.3	4.5	2.0	2.3	0	0 ⊙	0	ENE 2	NE 4	E 2
11	118.9	117.7	115.8	117.5	-2.9	9.0	2.0	2.5	11.2	-3.7	82	35	75	64	0.9	7.5	1.8	3.4	1 ⊙	0 ⊙	4	ESE 2	ESE 3	ESE 2
12	112.0	108.7	106.0	108.9	-1.3	13.7	4.4	5.3	15.2	-3.8	86	21	68	58	0.8	12.5	2.7	5.3	9	4 ⊙	1	E 1	SW 3	W 3
13	105.9	106.0	103.5	105.1	-2.1	14.3	7.0	6.6	16.2	-3.9	94	31	69	65	0.3	11.2	3.1	4.9	9 ⊙	1 ⊙	2	C 0	W 2	SW 1
14	99.8	99.0	98.3	99.0	4.3	13.0	10.8	9.7	15.5	-1.0	74	62	66	67	2.2	5.8	4.5	4.2	4	8	10	WSW 3	W 12	W 7
15	99.9	98.9	98.1	97.3	7.8	10.2	11.2	10.1	11.8	7.1	73	70	68	70	2.8	3.7	4.2	3.6	10	9	10	W 8	W 10	W 12
16	92.3	96.9	102.3	97.2	3.6	2.6	-0.5	1.3	11.2	-0.5	90	84	77	84	0.8	1.2	1.3	1.1	10 ●	10	10	N 5	WNW 9	NE 4
17	100.4	96.6	89.4	95.5	-2.1	0.2	7.8	3.4	8.1	-3.5	77	88	91	85	1.2	0.7	0.9	0.9	10 ✳	10	10 ●	SE 3	SE 5	SW 4
18	83.3	85.1	89.6	86.0	10.4	10.0	8.4	9.3	11.2	7.3	86	86	79	84	1.8	1.8	2.2	1.9	10 ●	10 ●	9	WSW 7	W 9	WNW 8
19	95.0	95.7	94.5	95.1	6.0	10.2	7.5	7.8	11.2	4.8	89	64	94	82	1.1	4.5	0.6	2.1	9	10	10 ●	WSW 5	WNW 4	C 0
20	96.7	94.4	92.2	94.4	8.8	14.6	10.0	10.8	15.1	7.0	93	65	84	81	0.8	5.8	1.9	2.8	10	10	3	C 0	SSW 6	SE 2
21	96.9	99.0	99.5	98.5	9.7	13.4	7.7	9.6	14.2	4.7	73	44	75	64	3.2	8.7	2.6	4.8	6	1 ⊙	10	WNW 7	W 8	SW 1
22	102.3	103.6	104.8	103.6	4.7	10.4	2.1	4.8	12.8	1.5	84	59	91	78	1.3	5.1	0.6	2.3	5 ⊙	9	0	WNW 2	WNW 5	C 0
23	104.1	102.8	104.0	103.6	1.5	12.8	8.8	8.0	13.8	-2.5	94	50	60	68	0.4	7.4	4.5	4.1	1 ⊙	8 ⊙	10	E 2	E 5	ENE 5
24	106.1	106.8	108.0	107.0	3.2	4.0	3.5	3.6	8.8	2.8	88	82	80	83	0.9	1.5	1.5	1.3	10 ●	10 ●	10	ENE 8	E 6	E 5
25	107.6	107.3	108.1	107.7	2.8	11.5	6.7	6.9	13.2	2.2	82	64	82	76	1.3	4.9	1.7	2.6	10	5	9	SE 6	SE 7	ESE 5
26	107.5	106.0	106.3	106.6	4.4	14.8	8.8	9.2	15.8	3.5	95	43	52	63	0.5	9.6	5.5	5.2	10	5	0	SE 3	S 8	S 3
27	107.4	108.5	107.4	107.8	7.5	12.7	7.2	8.6	14.6	5.0	35	38	50	41	6.8	9.1	5.2	7.0	6 ⊙	3 ⊙	0	S 14	S 12	S 9
28	104.1	103.6	101.2	103.0	6.7	5.3	7.0	6.5	12.1	4.5	46	81	84	70	5.3	1.7	1.6	2.9	9	10 ●	10 ●	S 10	SSW 8	S 3
29	99.9	100.0	100.7	100.2	6.5	8.4	6.0	6.7	9.2	4.9	96	86	97	93	0.5	1.5	0.3	0.8	9	10	10 ●	W 2	C 0	W 5
30	103.0	103.9	104.0	103.6	5.3	7.2	6.3	6.3	9.6	4.1	97	94	95	95	0.3	0.6	0.4	0.4	10 ●	10	3	WNW 1	NNW 1	NW 3
31	106.4	108.0	108.5	107.6	4.9	11.2	7.8	7.9	12.7	2.4	94	59	82	78	0.6	5.4	2.0	2.7	9 ⊙	8	2	SE 3	S 2	C 0
M	104.2	104.0	103.6	103.9	1.5	8.0	4.5	4.6	10.1	-0.4	84	61	77	74	1.3	4.7	2.0	2.7	6.8	6.5	5.1	3.5	5.2	3.2

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1	107.2	105.5	104.4	105.7	4.0	15.8	8.8	9.4	17.9	1.9	97	59	85	80	0.2	7.2	1.7	3.0	1 ⊙	2 ⊙	9	C 0	NE 3	C 0
2	104.2	103.9	106.4	104.8	5.6	16.3	8.2	9.6	16.5	4.2	85	57	96	79	1.4	7.9	0.5	3.3	1 ⊙	10	4	C 0	SE 6	N 1
3	109.1	110.7	112.2	110.7	8.6	18.2	13.0	13.2	18.8	6.7	94	49	71	71	0.6	10.6	4.3	5.2	10	6	8	C 0	NNE 3	N 1
4	115.3	115.2	114.8	115.1	5.3	20.0	9.8	11.2	20.9	1.4	95	32	73	67	0.4	15.9	3.3	6.5	0 ⊙	1 ⊙	0	C 0	NE 5	NE 1
5	113.8	111.3	105.9	110.3	4.2	18.2	11.7	11.4	18.8	-0.1	97	35	52	61	0.2	13.7	6.5	6.8	0 ⊙	0 ⊙	0	C 0	SE 3	E 1
6	100.6	96.6	94.3	97.2	5.9	20.4	14.1	13.6	21.0	1.2	79	27	42	49	2.0	17.5	9.3	9.6	0	0 ⊙	8	ESE 1	S 3	N 4
7	97.1	97.1	101.6	98.6	6.5	9.8	5.1	6.6	14.1	4.6	78	61	84	74	2.2	4.8	1.4	2.8	10	10	10 ●	NW 4	N 3	N 5
8	106.2	105.5	103.9	105.2	-0.7	5.8	1.3	1.9	6.6	-1.7	79	48	68	65	1.2	4.8	2.1	2.7	6 ⊙	4 ⊙	0	N 3	NNW 6	WNW 2
9	101.3	98.9	98.0	99.4	0.7	10.3	5.1	5.3	12.4	-2.7	81	46	76	68	1.2	6.7	2.1	3.3	8	9 ⊙	9	W 4	NNW 7	ENE 3
10	94.7	90.2	84.0	89.6	3.1	12.4	6.8	7.3	14.3	-1.5	86	47	71	68	1.0	7.6	2.9	3.8	3 ⊙	3 ⊙	4	SSE 2	WSW 5	C 0
11	81.7	83.0	88.8	84.5	4.9	7.9	2.8	4.6	8.8	0.4	81	38	69	63	1.7	6.5	2.4	3.5	6 ⊙	8	7	NW 3	NW 6	NNW 1
12	94.9	96.5	98.5	96.6	-0.5	4.7	0.4	1.2	5.8	-4.0	96	53	86	78	0.3	4.0	0.9	1.7	8	10	2	NW 1	NW 3	C 0
13	99.6	100.4	103.7	101.2	-0.4	5.6	-1.6	0.5	6.2	-5.5	86	53	67	69	0.8	4.3	1.7	2.3	1 ⊙	8 ⊙	1	WSW 1	W 9	NW 1
14	105.3	104.9	105.1	105.1	-1.7	4.5	-1.9	-0.2	7.1	-6.8	90	39	82	70	0.6	5.1	0.9	2.2	3 ⊙	6	1	NW 1	WNW 1	C 0
15	106.5	107.9	109.6	108.0	-1.1	4.0	-0.3	0.6	7.6	-6.3	87	74	70	77	0.8	2.1	1.8	1.6	8 ⊙	9 ●	4	WNW 1	NNE 2	C 0
16	110.2	108.9	107.4	108.8	1.4	10.0	7.4	6.6	13.1	-4.1	72	54	77	68	1.9	5.7	2.3	3.3	2 ⊙	9 ⊙	10	SW 2	W 9	SW 2
17	106.8	106.7	107.4	107.0	7.6	11.6	5.5	7.6	12.6	5.2	89	61	83	78	1.2	5.3	1.5	2.7	10	9	0	NW 2	N 3	NNW 3
18	106.2	105.4	103.9	105.2	4.6	6.1	4.0	4.7	6.3	1.6	89	57	79	75	1.0	4.0	1.7	2.2	9	10	9	N 2	NNW 6	C 0
19	101.3	98.8	100.1	100.1	2.8	11.3	8.5	7.8	11.4	-5.4	89	49	92	77	0.9	6.0	0.9	2.6	8	10	10	SE 3	SSE 1	W 1
20	106.6	108.8	110.7	108.7	6.4	11.9	5.8	7.5	12.1	5.5	81	41	77	66	1.9	8.2	2.1	4.1	9	6	1	WNW 5	NNW 5	NE 1
21	112.9	113.3	114.6	113.6	3.0	10.9	5.8	6.4	12.6	-3.3	95	43	68	69	0.4	7.4	2.9	3.6	2 ⊙	9	3	C 0	N 4	NE 1
22	116.1	116.3	116.7	116.4	1.0	10.0	5.6	5.6	10.7	-3.0	98	57	86	80	0.2	5.3	1.3	2.3	7	9 ⊙	7	C 0	E 1	C 0
23	115.9	115.3	115.6	115.6	6.1	10.2	8.0	8.1	10.9	3.6	88	72	90	83	1.1	3.4	1.0	1.8	10	10	10	C 0	NNE 3	C 0
24	114.1	113.3	112.5	113.3	7.4	11.5	9.1	9.3	13.0	6.7	96	73	93	87	0.5	3.6	0.8	1.6	10	10	10 ●	N 2	NW 5	NNE 1
25	109.3	108.8	108.5	108.9	6.6	8.0	8.1	7.7	9.6	6.0	93	87	91	90	0.7	1.3	0.9	1.0	10	10	10	N 5	N 3	C 0
26	107.8	107.5	106.6	107.3	7.5	10.8	9.0	9.1	14.3	6.8	96	84	93	91	0.5	2.2	0.8	1.2	10	10	6	N 1	NW 3	W 3
27	104.2	101.7	99.6	101.8	8.3	20.1	12.3	13.2	20.9	3.3	99	59	90	83	0.2	9.6	1.4	3.7	9 ⊙	1 ⊙	0	C 0	ENE 4	NE 1
28	97.9	95.5	94.8	96.1	12.3	23.6	13.0	15.5	24.5	6.7	88	38	70	65	1.7	17.9	4.5	8.0	1 ⊙	6 ⊙	1	E 1	SSE 7	S 1
29	97.9	97.9	97.0	97.6	14.2	22.5	14.0	16.2	24.1	9.3	76	44	80	67	3.9	15.2	3.2	7.4	3 ⊙	1 ⊙	0	W 1	WSW 4	C 0
30	95.3	92.1	99.8	95.7	12.6	24.8	10.8	14.8	25.7	7.8	87	36	74	66	1.9	20.1	3.4	8.5	1 ⊙	9 ⊙	10	C 0	S 9	NNW 5
31																								
M	104.7	103.9	104.2	104.3	4.9	12.6	7.0	7.9	14.0	1.3	88	52	78	73	1.1	7.8	2.4	3.8	5.5	6.8	5.1	1.5	4.4	1.3

Wrocław – Mały Gądów

$H_s = 116$ m $H_b = 118.6$ m $h_w = 22.5$ m

Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.1	2	-	$*^{0}\,5^{38}\;7^{10}-9^{40}\;13^{10}\;15^{25-40}\cdot = 0^{00}-13^{30}$
2	7	.	pł.	-	
3	7	.	pł.	-	$= 5^{30}-7^{35}\cdot \sqcup^{0} n-9^{10}$
4	5	0.2	pł.	-	$= 0^{00}-13^{20}\;\infty-15^{40} = -24\cdot \sqcup^{1} n-8^{20}$
5	8	.	.	-	$\bullet^{0}0^{45}\;2^{38}\cdot = 0^{00}-4^{10}$
6	7	.	.	-	$= 2^{40}-10^{20}\;\infty-11^{15} = 17^{35}-24\cdot \sqcup^{1} n-9^{10}$
7	7	.	.	-	$= 0^{00}-9^{35}\;17^{45}-24\cdot \sqcup^{0} n-9^{15}\cdot \oplus\; 12^{30}-13^{10}$
8	6	.	.	-	$= 0^{00}-12^{55}\;\infty-16^{50} = -24\cdot \sqcup^{0} n-9^{40}$
9	7	.	.	-	$= 0^{00}-8^{20}\cdot \sqcup^{0} n-9^{30}$
10	6	.	.	-	$= 6^{40}-10^{20}\;\infty-14^{40} = 17^{35}-24\cdot \sqcup^{0} n-9^{10}$
11	6	.	.	-	$= 0^{00}-11^{15}\;\infty-18^{38} = -24\cdot \sqcup^{0} n-8^{15}$
12	8	.	.	-	$= 0^{00}-10^{20}\;19^{35}-24\cdot \sqcup^{1} n-8^{30}$
13	6	.	.	-	$= 0^{00}-9^{40}\;\infty-14^{30}\;17^{20}-21^{40} = -24\cdot \sqcup^{1} n-8^{20}$
14	6	.	.	-	$\gg 10^{35}-14^{20}\cdot = 0^{00}-7^{40}\;\infty-17^{15} = -21^{30}\cdot \sqcup^{0} n-7^{15}$
15	7	3.9	.	-	$\bullet^{0}23^{15}\;24\cdot \gg 2^{20}-3^{40}\;12^{30}-24$
16	7	1.6	.	-	$\bullet^{0}0^{00}\;10-7^{45}\;\bullet^{0}-8^{20}\;\bullet^{1}-9^{10}\;\bullet^{0}-10^{30}\;10^{50}-11^{37}\cdot \gg 0^{00}-3^{20}\cdot = 8^{20}-10^{50}$
17	5	5.9	.	-	$*^{0}3^{30}\;5^{35}\;6^{30}-9^{40}\;\bullet^{0}10^{37}-11^{10}\;\bullet^{0}-11^{25}\;12^{15}\;\bullet^{0}13^{25}-14^{40}\;\bullet^{0}15^{18-30}\;17^{45}\;20^{20}-24\cdot = 7^{25}-24$
18	7	8.7	.	-	$\bullet^{0}0^{00-25}\;4^{20}-8^{05}\;\bullet^{0}8^{20-45}\;\bullet^{1}9^{10}-10^{30}\;\bullet^{0}-11^{45}\;12^{05}-13^{38}\;14^{10}-15^{38}\;16^{10-36}\;18^{35-50}\;\bullet^{1}-19^{10}\;\bullet^{2}-19^{15}\;19^{50}-20^{30}\;21^{15}-22^{00}$
19	7	4.5	.	-	$\bullet^{0}3^{10}\;5^{35}\;14^{50}\;15^{30}-23^{30}\cdot = 16^{20}-24$ [18.III: $23^{05-15}\cdot \gg 13^{30}-14^{40}\;17^{45}-18^{10}\cdot = 0^{00}-1^{45}$
20	7	.	.	-	$= 0^{00}-12^{30}\;23^{25}-24\cdot \oplus\; 12^{20}-15^{10}$
21	8	.	.	-	$= 0^{00}-5^{20}$
22	7	.	.	-	$= 21^{30}-24$
23	6	0.3	.	-	$= 0^{00-30}\;\equiv -1^{30} = -9^{45}\;\infty-20^{27}\cdot \sqcup^{1} n-8^{40}$
24	7	0.0	.	-	$\bullet^{0}6^{32}-8^{30}\;12^{50}\;13^{15}\cdot \gg 2^{45}-3^{20}$
25	5	.	.	-	$= 5^{30}-24$
26	7	.	.	-	$= 0^{00}-3^{55}\;\equiv^{0}-4^{40}\;\equiv^{1}-5^{10}\;\equiv^{0}-5^{35}\;\equiv -11^{20}\;\infty-12^{45}$
27	8	.	.	-	$\gg 3^{40}-4^{15}\;\lll -5^{30}\;\gg -7^{40}\;\lll -12^{20}\;\gg -18^{10}\;22^{30}-24$
28	6	7.6	.	-	$\bullet^{0}11^{45}\;12^{20}\;\bullet^{0}-14^{17}\;14^{35}\;16^{10}\;17^{20}\;18^{40}\;20^{35}\;22^{10}-24\cdot \gg 0^{00}-2^{50}\;\lll -4^{40}\;\gg -9^{25}$
29	6	14.3	.	-	$\bullet^{0}0^{00}-4^{10}\;5^{35}\;7^{30}\;8^{25}-9^{38}\;10^{20}-11^{10}\;\bullet^{0}16^{30}-17^{30}\;\bullet^{1}-18^{10}\;\bullet^{1}-19^{15}\;\bullet^{0}-20^{35}\;\bullet^{1}-21^{20}\;\bullet^{0}-24\cdot \equiv 5^{50}\;7^{10} = -24$
30	6	0.4	.	-	$\bullet^{0}0^{00}-2^{35}\;\bullet^{0}3^{45}-6^{50}\;\bullet^{0}-8^{20}\;11^{40}\;14^{35}\ldots 50\cdot = 0^{00}-22^{50}\;\equiv^{0}-23^{20}\;\equiv^{2}-24$
31	8	.	.	-	$\equiv^{2} 0^{00}-3^{30}\;\equiv^{1}-4^{50} = -10^{30}$
Σ	—	47.5	—	-	UWAGI.

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1	6	.	.	-	$= 6^{20}-10^{35}\;\infty-14^{25} = 17^{20}-24$
2	7	1.3	.	-	$\bullet^{0}13^{40-45}\;14^{10-25}\;\bullet^{1}14^{30-45}\;\bullet^{0}16^{25}-17^{10}\cdot = 0^{00}-9^{30}\;18^{30}-24$
3	7	.	.	-	$\bullet^{0}1^{48}-2^{35}\;3^{15}\;5^{25}\cdot = 0^{00}-2^{35}\;4^{20}-10^{40}\;\infty-11^{35} = 22^{30}-24$
4	7	.	.	-	$= 0^{00}-4^{40}\;\equiv -6^{10} = -8^{30}\;\infty 8^{50}-11^{20}\;18^{20}-20^{30} = -24\cdot \sqcup^{0} 2^{10}-6^{20}$
5	8	.	.	-	$= 0^{00}-2^{20}\;3^{10}-4^{50}\;\equiv^{0}-6^{15} = -8^{40}\;\infty-10^{40}\cdot 20^{40}-24$
6	7	.	.	-	$\infty\; 0^{00}-1^{40} = -8^{40}\cdot \sqcup^{0} 1^{50}-5^{30}$
7	8	0.4	.	-	$\bullet^{0}13^{32}-14^{05}\;\bullet^{0}20^{15}\;21^{20}$
8	8	.	.	-	$\supset 21^{40}-22^{35}$
9	8	.	.	-	$\sqcup^{0} n-7^{45}\cdot \oplus\; 11^{30}-14^{30}$
10	8	.	.	-	$= 3^{15}-10^{20}\cdot \sqcup^{1} n-6^{40}$
11	8	.	.	-	$\frown^{0} n-9^{30}$
12	8	0.0	.	-	$*^{0}7^{15-35}\;\bullet^{0}19^{28-35}\cdot = 22^{30}-24\cdot \sqcup^{0} n-6^{10}$
13	7	0.0	.	-	$\bullet^{0}10^{25-35}\cdot = 0^{00}-8^{40}\cdot \sqcup^{0} n-7^{10}\cdot \oplus\; 8^{30}-9^{20}$
14	8	0.0	.	-	$\bullet^{0}11^{50}-12^{10}\cdot = 5^{10}-8^{20}\cdot \sqcup^{1} n-7^{45}$
15	7	0.0	.	-	$\bullet\;10^{40}-11^{00}\;\triangle\;11^{50}-12^{06}\;\bullet\;12^{15-30}\;\bullet\;12^{50}-13^{04}\cdot = 0^{00}-7^{10}\cdot \sqcup^{1} n-7^{40}$
16	7	0.4	.	-	$= 16^{30}-24$
17	7	0.0	.	-	$\bullet^{0}1^{35}\;5^{25}-6^{10}\cdot 9^{05-20}\cdot = 0^{00}-10^{20}$
18	8	.	.	-	$= 4^{30}-7^{30}$
19	7	2.2	.	-	$\bullet^{0}12^{45}\;18^{30}-22^{23}\;\bullet^{1}-22^{47}\;\bullet^{0}-23^{35}\cdot = 1^{00}-10^{15}\;15^{35}-23^{40}\cdot \sqcup^{0} n-6^{40}$
20	8	.	.	-	$\bullet^{0}0^{40}-2^{40}$
21	8	0.0	.	-	$\bullet^{0}10^{37}-11^{00}\cdot = 2^{20}-3^{10}\;\equiv -6^{15} = -8^{10}\cdot \sqcup^{1} n-6^{35}$
22	7	0.0	.	-	$\bullet^{0}21^{45}\;22^{10}\cdot = 3^{25}-9^{25}\cdot \sqcup^{0} n-5^{40}$
23	7	.	.	-	
24	6	3.0	.	-	$\bullet^{0}8^{40}-9^{25}\;16^{05}\;18^{40}\;20^{15}\;21^{40}\;23^{22}\;24\cdot = 0^{10}-13^{40}\;17^{20}-24$
25	6	0.0	.	-	$\bullet^{0}0^{00}\;1^{24}-4^{15}\;9^{30}-10^{10}\cdot = 0^{00}-7^{30}\;11^{30}-24$
26	6	0.0	.	-	$= 0^{00}-24$
27	7	.	.	-	$\bullet^{0}5^{15-30}\cdot \equiv 0^{00}-1^{50}\;\equiv^{0}-2^{35}\;\equiv^{2}-5^{10}\;\equiv^{1}-6^{40} = -11^{40}\;21^{25}-24\cdot$
28	8	0.0	.	-	$= 0^{00}-3^{45}\;\equiv^{1}-4^{20}\;\equiv^{0}-5^{40} = -9^{10}\cdot \frown\; n-7^{10}\cdot \oplus\; 10^{30}-11^{10}$
29	7	.	.	-	$\bullet^{0}\mathrm{K}^{0}2^{50}-3^{05}\;\mathrm{NW}-\mathrm{NE}\;(\mathrm{K})^{0}-3^{40}\cdot = 4^{40}-9^{20}$
30	8	0.0	.	-	$\bullet^{0}13^{05-15}\;17^{10-18}\cdot \lesssim 0^{10}-1^{40}\cdot \mathrm{K}^{0}13^{05-10-20}\;(\mathrm{K})^{0}-14^{03}\;\mathrm{SW}-\mathrm{NE}\cdot = 0^{35}-4^{15}\;\equiv -5^{15} = -7^{30}\cdot \frown^{1} n-8^{20}\cdot$
31					[30.IV: $\oplus\; 9^{40}-13^{00}$
Σ	—	7.3	—	-	UWAGI.

Wrocław – Mały Gądów — φ = 51°08' — λ = 16°59' — Maj – Mai 1957

DNI	CIŚNIENIE P − 900 −				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	104.9	104.4	104.4	104.6	6.5	13.0	6.0	7.9	13.5	1.5	65	33	66	55	3.4	10.1	3.3	5.6	2	4 ⊙	2	N 2	NNE 4	NE 2
2	103.3	101.8	100.2	101.8	7.7	12.5	6.7	8.4	13.6	1.1	56	36	57	50	4.6	9.3	4.2	6.0	4 ⊙	9 ⊙	2	ENE 3	E 4	NE 1
3	99.5	97.9	96.7	98.0	6.1	15.8	11.7	11.3	16.7	−2.1	70	39	70	60	2.8	10.9	4.1	5.9	2 ⊙	5	9	C 0	ENE 3	W 3
4	96.1	98.5	100.5	98.4	8.9	10.0	6.2	7.8	12.0	3.4	76	43	62	60	2.8	7.0	3.7	4.5	10 ●	7	4	W 4	W 10	W 5
5	101.1	98.8	96.3	98.7	4.5	8.4	1.9	4.2	10.1	0.1	60	43	76	60	3.3	6.2	1.7	3.7	5	9	8	W 8	W 9	C 0
6	94.8	96.0	96.3	95.7	0.2	5.0	1.5	2.0	6.8	−0.3	96	72	91	86	0.3	2.4	0.6	1.1	10 ✳	8 ⊙	1	NW 6	NW 7	WSW 2
7	95.4	94.9	94.8	95.0	2.7	7.6	2.2	3.7	9.6	−2.4	86	64	91	80	1.0	3.7	0.7	1.8	4	9	5	NW 4	NW 7	C 0
8	94.9	95.0	96.5	95.5	3.0	7.3	2.6	3.9	8.2	−0.4	91	67	88	82	0.7	3.3	1.0	1.7	10	10	10	NNW 3	NNW 5	C 0
9	98.3	98.6	98.7	98.5	4.2	9.6	7.0	7.0	10.5	−1.9	90	63	78	77	0.8	4.5	2.2	2.5	10	9	9	C 0	N 4	NE 1
10	98.0	98.0	99.5	98.5	5.6	9.2	8.1	7.8	10.1	4.4	89	72	85	82	1.0	3.2	1.6	1.9	10 ●	10	10	NW 2	NW 4	N 1
11	100.5	100.8	100.3	100.5	8.8	15.9	13.8	13.1	18.6	5.3	84	50	64	66	1.8	9.0	5.7	5.5	8	5 ⊙	0	W 2	W 2	SE 2
12	100.9	100.3	101.7	101.0	10.8	21.2	13.0	14.5	22.9	4.6	84	47	77	69	2.2	13.5	3.5	6.4	7	5 ⊙	6	E 1	S 6	WSW 1
13	103.6	103.0	104.2	103.6	14.8	21.8	15.3	16.8	23.0	8.3	82	53	81	72	3.1	12.1	3.4	6.2	2	8	10 ●	C 0	WSW 2	WNW 3
14	105.7	106.5	107.4	106.5	13.5	19.9	13.3	15.0	20.6	10.1	88	56	84	76	1.8	10.2	2.5	4.8	8	8	3	WNW 2	WNW 5	C 0
15	109.5	108.4	105.9	107.9	11.9	20.8	15.8	16.1	21.8	5.9	91	55	72	73	1.2	11.2	5.0	5.8	1 ⊙	4 ⊙	5	C 0	ENE 2	E 1
16	103.8	100.7	99.5	101.3	14.0	24.8	17.3	18.4	25.2	8.3	79	43	68	63	3.4	17.7	6.3	9.1	0 ⊙	2 ⊙	4	ESE 4	SSE 6	ENE 2
17	103.0	105.1	106.0	104.7	12.3	12.0	11.7	11.9	17.3	11.2	93	91	85	90	1.0	1.2	2.0	1.4	10	10	10	W 7	NW 6	WSW 5
18	105.3	103.4	99.9	102.9	11.3	19.8	14.6	15.1	22.4	8.6	83	57	79	73	2.3	9.9	3.4	5.2	9	1	3	NW 2	NE 3	NE 2
19	96.2	93.6	91.9	93.9	15.6	25.5	17.4	19.0	26.2	11.4	79	48	80	69	3.7	16.9	4.0	8.2	9	3 ⊙	8	NNE 1	ENE 5	C 0
20	94.4	96.6	102.5	97.8	15.3	20.3	11.9	14.8	20.6	9.5	87	67	83	79	2.3	7.8	2.3	4.1	10	8	10	NW 3	NW 7	NW 7
21	105.0	104.3	103.4	104.2	8.8	14.9	11.4	11.6	15.8	7.8	85	40	75	67	1.7	10.1	3.5	5.1	10	9	10	WNW 6	NW 4	C 0
22	102.0	101.3	101.3	101.5	10.1	16.2	11.3	12.2	17.3	7.6	83	50	86	73	2.1	9.2	1.8	4.4	9	9	10	WNW 1	NE 4	E 1
23	99.2	98.2	97.1	98.2	11.7	18.7	17.3	16.2	19.9	9.2	83	61	73	72	2.3	8.4	5.2	5.3	10	9	10 ●	NNE 3	ENE 1	C 0
24	99.6	101.7	105.5	102.3	14.0	15.5	13.6	14.2	17.9	13.0	94	87	72	84	0.9	2.3	4.4	2.5	10	10	10	C 0	NNW 4	NE 2
25	109.1	109.8	111.7	110.2	9.7	14.3	7.9	10.0	15.2	5.9	65	36	56	52	4.1	10.4	4.6	6.4	2	6	1	ENE 6	NE 8	N 5
26	112.6	112.4	112.0	112.3	7.6	10.4	8.0	8.5	11.6	2.6	65	43	62	57	3.6	7.2	4.1	5.0	4 ⊙	9	8	NE 4	NE 7	NE 4
27	111.1	111.0	109.9	110.7	7.1	10.5	6.7	7.8	11.9	1.4	69	44	71	61	3.2	7.1	2.8	4.4	4 ⊙	9	9	NE 4	NE 5	NNE 1
28	108.4	107.3	106.6	107.4	7.4	11.0	5.6	7.4	13.9	−1.2	72	52	83	69	2.9	6.3	1.6	3.6	0	9	2	NE 3	NE 2	N 2
29	107.9	107.9	107.9	107.9	7.0	13.4	6.9	8.6	14.9	−1.8	75	38	77	63	2.4	9.6	2.3	4.8	0	9	1	C 0	NE 2	C 0
30	109.0	108.1	106.4	107.8	10.0	18.1	10.1	12.1	19.4	−0.8	61	36	71	56	4.8	13.3	3.6	7.2	0	1 ⊙	0	C 0	SE 5	C 0
31	106.7	104.8	102.2	104.6	12.6	19.5	13.8	14.9	20.8	1.8	63	39	62	55	5.4	13.9	6.1	8.5	0	7	1	SSE 1	S 3	SSE 2
M	102.6	102.2	102.2	102.3	9.2	14.9	10.0	11.0	16.4	4.3	79	52	75	69	2.5	8.6	8.3	4.8	5.8	7.1	5.8	2.6	4.7	1.8

Czerwiec – Juin

1	102.6	102.7	102.9	102.7	13.7	21.6	14.4	16.0	23.2	3.3	66	34	72	57	5.4	17.1	4.6	9.0	0 ⊙	7	2	SW 2	WSW 5	WNW 2
2	105.6	105.8	105.9	105.8	15.2	21.5	14.8	16.6	23.5	6.2	72	45	75	64	4.8	14.1	4.1	7.7	1 ⊙	7	0	W 3	W 5	NW 1
3	106.8	104.1	100.6	103.8	13.8	26.5	20.7	20.4	28.1	6.2	81	33	58	57	3.0	23.2	10.2	12.1	0 ⊙	1 ⊙	9	C 0	NE 2	E 2
4	98.3	97.9	97.6	97.9	16.1	25.0	15.7	18.1	25.2	11.7	81	49	92	74	3.4	16.2	1.3	7.0	9	9	10 ●	C 0	WSW 3	W 4
5	96.3	94.7	93.3	94.8	12.9	18.0	11.8	13.6	19.3	11.2	92	60	83	78	1.3	8.2	2.3	3.9	10 ●	9	6	WNW 6	W 6	SSW 4
6	96.2	98.5	98.1	97.6	11.2	14.7	13.8	13.4	17.4	7.4	72	49	66	62	3.7	8.5	5.4	5.9	9	6	8	W 9	W 7	S 3
7	97.3	96.1	97.4	96.9	15.0	23.7	17.6	18.5	23.7	7.3	62	38	62	54	6.4	18.2	7.7	10.8	5	8	7	SSE 3	SW 8	NNE 2
8	98.5	98.1	96.5	97.7	14.5	22.6	20.3	19.4	24.8	11.4	80	51	74	68	3.2	13.5	6.2	7.6	10	9 ⊙	7	N 1	SSE 3	E 2
9	94.8	96.3	97.4	96.2	17.4	21.8	17.4	18.5	24.1	14.1	83	59	90	77	3.4	10.7	2.1	5.4	9	5 ⊙	8	SSE 5	W 7	C 0
10	98.1	97.3	97.0	97.5	18.3	23.9	20.4	20.8	25.3	13.7	79	57	77	71	4.4	12.6	5.5	7.5	9	6	4	NE 1	S 5	E 1
11	94.2	92.6	95.0	93.9	20.6	29.4	24.0	24.5	32.8	16.2	71	44	58	58	6.9	22.8	12.5	14.1	2 ⊙	9	8	SE 8	SSE 6	S 5
12	106.4	112.5	115.9	111.6	17.9	15.7	16.6	16.7	24.8	14.9	84	87	78	83	3.2	2.2	4.3	3.2	10	10	5	NW 4	WNW 5	NW 2
13	118.8	117.5	115.6	117.3	14.4	20.5	15.5	16.5	23.2	9.2	72	46	65	61	4.6	13.1	6.2	8.0	0 ⊙	8 ⊙	1	N 1	NW 3	N 2
14	116.4	114.9	114.2	115.2	16.6	23.0	17.3	18.6	24.4	6.7	68	40	57	55	6.1	16.8	8.5	10.5	0 ⊙	1 ⊙	0	C 0	NNE 4	NNE 3
15	114.9	113.1	110.7	112.9	15.0	23.5	18.2	18.7	25.0	8.4	58	39	63	53	7.1	17.7	7.7	10.8	0 ⊙	1 ⊙	0	E 1	N 1	NE 3
16	109.6	107.9	105.4	107.6	17.8	25.2	19.1	20.3	26.5	7.5	55	30	54	46	9.2	22.3	10.2	13.9	0 ⊙	0 ⊙	0	NE 2	E 4	NE 2
17	105.5	104.6	103.0	104.4	19.8	27.1	21.5	22.5	28.0	13.1	53	33	52	46	10.8	23.8	12.4	15.7	0 ⊙	2 ⊙	0	NE 2	NE 5	ENE 3
18	102.5	100.4	98.0	100.3	18.9	28.4	20.2	21.9	30.1	10.4	50	31	64	48	11.0	26.5	8.5	15.3	0 ⊙	1 ⊙	1	E 2	SE 5	ENE 1
19	97.9	96.3	97.1	97.1	21.4	30.1	19.8	22.8	31.1	12.5	61	37	79	59	9.8	27.0	4.9	13.9	2 ⊙	6 ⊙	7	WNW 2	WSW 3	S 2
20	99.4	101.8	102.6	101.3	16.4	17.2	18.5	17.6	22.2	14.8	83	93	86	87	3.0	1.4	2.9	2.4	9	10	6	N 4	N 1	NE 1
21	103.6	100.7	96.9	100.4	17.6	23.7	18.5	19.6	25.1	12.0	72	54	81	69	5.7	13.6	4.1	7.8	4 ⊙	7	6	E 1	E 3	SSE 2
22	93.7	91.8	91.8	92.4	18.2	26.3	17.0	19.6	27.4	13.9	88	48	81	72	2.5	17.8	3.8	8.0	10	6	6	S 4	SW 9	WSW 2
23	96.3	96.4	97.4	96.7	14.8	22.3	16.4	17.5	25.5	10.9	94	59	89	81	0.9	11.1	2.1	4.7	10	8 ⊙	9	W 2	S 5	WSW 4
24	97.5	95.5	91.9	95.0	14.0	13.6	14.3	14.0	17.3	10.0	91	95	88	91	1.5	0.7	2.0	1.4	10	10 ●	10	ENE 2	NNE 5	NE 1
25	93.8	100.9	103.7	99.5	16.6	14.2	12.0	13.7	17.1	11.0	68	65	80	71	6.1	5.6	2.8	4.8	6	10	6	W 10	W 12	W 3
26	107.2	108.1	109.8	108.4	11.7	15.7	11.4	12.6	18.5	5.7	78	45	84	69	2.9	9.7	2.2	4.9	8	7	2	W 2	WNW 5	W 1
27	111.2	111.4	113.0	111.9	11.2	17.5	10.8	12.6	20.0	4.7	85	54	84	74	2.0	9.1	2.2	4.4	10 ●	5	8	WNW 2	W 7	C 0
28	113.3	110.3	108.5	110.7	13.4	24.3	19.5	19.2	26.5	5.8	73	54	78	68	4.2	14.2	5.1	7.8	10	6 ⊙	1	SSE 3	WSW 6	WSW 3
29	110.5	109.9	108.0	109.5	20.5	28.4	22.5	23.5	30.2	13.5	72	43	74	63	6.7	22.0	6.9	11.9	1 ⊙	4 ⊙	0	WNW 2	NW 4	SW 2
30	107.5	106.8	106.7	107.0	22.2	31.6	22.1	24.5	32.1	14.9	67	38	66	57	8.9	28.9	9.0	15.6	1 ⊙	4 ⊙	9	W 2	N 6	WNW 2
31																								
M	103.2	102.8	102.4	102.8	16.2	22.6	17.4	18.4	24.7	10.3	74	50	74	66	5.1	15.0	5.6	8.6	5.2	6.1	4.9	2.9	5.0	2.2

Wrocław – Mały Gądów

$H_s = 116$ m $H_b = 118{,}6$ m $h_w = 22{,}5$ m

Maj – Mai 1957

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	-	
2	8	.	.	-	⌒⁰ n – 7¹⁰ · ⊕ 8¹⁸ – 14³⁵
3	8	0.0	.	-	⌒⁰ n – 5¹⁵
4	8	.	.	-	•⁰ 6⁴⁰ 8¹⁵ · ⩔ 10⁴⁰ – 13²⁵ = 3³⁵ – 8³⁰
5	8	7.6	.	-	▽⁰ 8⁵²-⁵⁶ ⁂⁰ 9⁰⁶ ▽⁰ 11²⁸-³² ⊕ 11⁴⁰ – 12³⁰
6	8	1.2	5	-	•⁰ 3³⁵ – 4⁵⁰ ⁂⁰ – 5¹⁰ ✳¹ – 7³⁵ ✳⁰ – 9¹⁰ ⁂⁰ – 9⁴⁵ •⁰ – 10¹⁰ 11¹⁰ ▽⁰ 15⁰⁵-¹⁰ 15⁴⁵ – 16¹⁰ ▲ – 16³⁰
7	7	.	.	-	= 2¹³⁵ – 24 · ⌒¹ n – 6⁴⁰
8	8	.	.	-	= 4³⁰ – 8³⁰ · ⌒¹ n – 8¹⁵ · ◡ 21²⁵ – 24
9	8	0.0	.	-	= 0⁴⁰ – 3⁴⁰ · ≡ – 5¹⁵ = – 8³⁵ · ⌒⁰ n – 6²⁰ · ◡ 0⁰⁰ – 10
10	8	0.0	.	-	•⁰ 1³⁰ 5⁴⁰ · 6³⁵ 7⁴⁰ 10⁴⁰ 11¹⁰ · 13⁵⁵ 16¹⁰ · 17¹⁰ 18¹⁰
11	8	.	.	-	•⁰ 1¹⁰ – 3²⁰ = 3⁴⁰ – 7⁴⁰ · 19²⁵ – 24
12	8	.	.	-	= 0⁰⁰ – 8²⁰ · ⌒¹ n – 7⁴⁰
13	8	1.8	.	-	▽⁰ 13²²-²⁶ · 19¹⁵ – 40 · 20¹⁷-²⁰ 20⁴⁵ – 21¹⁵ · (↙) 13³⁵ – 15²⁵ · 19⁵² – 20⁵⁰ · = 5²⁵ – 8³⁰
14	7	.	.	-	▽⁰ 0¹⁴ – 1¹⁰ 1³⁵ – 2¹⁵ = 3³⁰ – 7³⁰ · 22³⁵ – 24
15	7	.	.	-	= 0⁰⁰ – 3⁴⁰ ≡ – 5¹⁰ = – 9²⁰ · ⌒¹ n – 8¹⁰
16	7	0.0	.	-	↙ 18⁴⁵ – 19⁰⁵ = 6³⁰ – 8⁴⁰ ∞ – 11³⁰ = 20³⁰ – 24 · ⌒¹ n – 9¹⁵
17	6	0.0	.	-	▽⁰ 1²⁵ – 2⁰⁵ · 7²⁰ – 8²⁵ •⁰ – 9²⁰ · 10³⁵ 12³⁰ · = 0⁰⁰ – 3⁴⁰
18	8	.	.	-	
19	8	.	.	-	(↙) 14³⁰ – 16²⁵ ↙ 18²³ – 21¹⁰
20	8	0.3	.	-	•⁰ 21²⁰ · 23⁴⁵ · ⩔ 15¹⁵ – 17³⁰
21	8	.	.	-	•⁰ 3²⁰ 5²⁰
22	8	0.8	.	-	•⁰ 17²⁰ 18¹⁰ – 20²⁵ · 21³⁵ – 24 · = 3³⁰ – 8¹⁰
23	7	10.0	.	-	•⁰ 0⁰⁰ · ⁴⁵ 5⁴⁰-⁵⁰ 20⁴⁰ 21³⁰ ▽⁰ 21⁵⁰ – 23²⁰ •⁰ · 24 · ↙ 21⁵⁰ – 22⁴⁵ SE · = 3²⁰ – 9²⁵
24	6	0.0	.	-	•⁰ 0⁰⁰ · ⁴⁵ 8⁵⁵ 10²⁰ •² 10²⁵ – 11³⁰ · = 2³⁵ – 15³⁰
25	8	.	.	-	⌒⁰ 23⁰⁰ – 24
26	9	.	.	-	⌒⁰ 0⁰⁰ – 6³⁰
27	8	.	.	-	
28	8	0.2	.	-	▽⁰ 12²⁰-³⁴ 14⁵⁴ – 15⁰² 16⁵¹ – 17⁰⁰ 17⁵⁴ – 18⁰⁸
29	8	.	.	-	⌒⁰ n – 7¹⁵ 21³⁰ – 23³⁰ · ◡⁰ 23³⁰ – 24
30	8	.	.	-	= 4²⁰ – 7¹⁰ ∞ – 8¹⁰ · ◡⁰ 0⁰⁰ – 6⁰⁰
31	8	.	.	-	= 0³⁰ – 3¹⁰ ≡ – 5¹⁵ = – 7³⁰ · ⌒¹ n – 6⁰⁵
Σ	–	23.9	–	-	UWAGI:

Czerwiec – Juin

1	8	.	.	-	= 0⁰⁰ – 2³⁵ ≡ – 4¹⁰ = – 6³⁰ · ⌒¹ n – 8²⁰
2	8	.	.	-	= 0³⁰ – 4¹⁰ ≡ – 5⁴⁰ = – 7³⁰
3	7	.	.	-	≡ 2³⁰ – 5²⁵ = – 9²⁰ ∞ – 13¹⁵ · ⌒¹ n – 8¹⁰
4	7	8.7	.	-	•⁰ 15⁴⁵ 16³⁰ 19¹⁵ – 24 · = 0³⁰ – 10²⁵ ∞ – 12¹⁰ = 19¹⁵ – 24 · ⊕ 9⁴⁰ – 13⁴⁰
5	7	0.0	.	-	•⁰ 0⁰⁰ – 1²⁰ · 1⁴⁰ – 4⁴⁵ •¹ – 6⁰⁵ •⁰ 6³⁵-⁵⁰ 7¹⁵ – 8⁴⁰ ▽⁰ 18³⁰-³⁷ · = 0⁰⁰ – 11¹⁰
6	8	0.0	.	-	▽⁰ 9¹⁰ 11¹⁵
7	8	.	.	-	
8	7	0.0	.	-	•⁰ 8³⁰ · ⁴⁰ ▽ 15⁵⁰ – 16¹⁰ · = 6³⁰ – 9¹⁰ · ◡ 23³⁰ – 24
9	8	0.0	.	-	▽⁰ 20²⁵-³⁸ · = 3¹⁵ – 9²⁰ ≡ 22¹⁰-⁴⁰ · ◡ 0⁰⁰ – 1¹⁵
10	7	.	.	-	= 3³⁵ – 4¹⁵ ≡ – 5⁴⁰ = – 7³⁰
11	8	.	.	-	↙ 22⁴⁵ – 23⁴⁰ · = 5²⁰ – 7¹⁵ · ⊕ 12⁴⁰ – 13⁴⁰
12	7	0.0	.	-	• 8³⁸ – 9¹⁰ = 0³⁰ – 11⁴⁰ · 19³⁵ – 21⁴⁰
13	8	.	.	-	= 3⁴⁰ – 6¹⁵
14	8	.	.	-	⌒¹ n – 7⁴⁰
15	8	.	.	-	
16	8	.	.	-	
17	8	.	.	-	
18	8	.	.	-	
19	8	0.0	.	-	▽⁰ 14⁵⁰ 15¹⁰ 17⁰⁵-¹⁰ (↙)⁰ 14³⁰-⁵⁰ SE – NW ↙¹ – 15¹⁰ (↙)⁰ – 17¹⁰
20	6	3.5	.	-	▽⁰ 7⁰⁸-¹² 7²⁰-²⁵ 8⁴⁵ – 9⁰⁵ ▽¹ 9²⁵ ▽⁰ – 10³⁵ 11³⁵ – 12²⁵ ▽¹ – 12⁴⁴ ▽⁰ 12⁴⁹-⁵⁰ 13⁰⁷-¹⁵ · 18⁵³ – 19⁰⁵ · = 10¹⁰ – 16¹⁵
21	8	0.3	.	-	≡ 0⁴⁰ – 1¹⁵ = – 6¹⁰ 21¹⁰ – 24 · ⌒⁰ n – 9⁰⁰
22	8	1.7	.	-	•⁰ 6⁴⁰ 7³⁰ 8¹² – 10³⁵ ▽⁰ 17¹⁰-³⁰ 19¹⁰-¹⁵ = 0⁰⁰ – 2⁰⁰ ≡ – 2³⁰ = – 3²⁵ ≡ – 5³⁰ = – 7³⁰ · ⌒¹ n – 6³⁵
23	7	2.4	.	-	•⁰ 6²⁴ – 7⁴⁰ ▽⁰ 8¹⁰-²⁰ ▽¹ – 18³⁸ ▽⁰ – 19¹⁰ · ↙¹ 18³⁰ – 19⁰⁶ · = 7¹⁰ – 9³⁵ ⌒ 19²⁰-³⁰
24	5	12.0	.	-	•⁰ 8³⁰ 10¹⁰ – 11¹⁰ 11³⁵ – 12¹⁰ ▽⁰ 22⁵⁰ – 23¹⁰ 23¹⁵-²⁵ ▽¹ · 24 · ↙⁰ 23²⁰ – 24 S – NW · = 1³⁰ – 17³⁰ · ⌒ 3³⁰ – 8³⁰
25	8	.	.	-	▽¹ 0⁰⁰ – 2³⁵ · ↙⁰ 0⁰⁰ – 2³⁰ · ⩔ 7³⁰ – 8²⁵ · 9¹⁵ – 16⁴⁰ · = 2²⁰ – 3²⁰ ≡ – 4⁰⁰ = – 6³⁰ · 21⁴⁰ – 24
26	8	0.0	.	-	= 0⁰⁰ – 3³⁰
27	7	0.0	.	-	•⁰ 7¹⁶ 8⁰⁶ ⁂⁰ 12³³-⁴³ · = 7⁴⁰ – 11²⁰ · ⌒⁰ n – 7¹⁰
28	7	.	.	-	= 21¹⁵ – 24
29	8	.	.	-	= 0⁰⁰ – 4³⁰ ≡ – 5¹⁵ = – 8⁴⁰ · ⌒⁰ n – 9¹⁵
30	8	.	.	-	= 3³⁵ – 4⁴⁰ ≡ – 5¹⁰ = – 6¹⁰ · ⌒¹ n – 7⁰⁰
31					
Σ	–	28.6	–	-	UWAGI:

Wrocław – Mały Gądów $\varphi = 51°08'$ $\lambda = 16°59'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	106.1	104.8	103.3	104.7	22.7	31.2	26.7	26.8	32.2	13.7	69	39	59	56	8.6	27.5	14.2	16.8	0 ⊙	1 ⊙	2	SE 1	SSE 4	E 2
2	101.3	101.6	105.1	102.7	23.5	28.6	22.0	24.0	29.9	18.2	64	55	68	62	10.3	17.7	8.5	12.2	2 ⊙	8	6	C 0	NW 7	NW 2
3	108.3	106.9	104.4	106.5	17.7	24.9	18.7	20.0	26.8	10.4	62	38	61	54	7.7	19.6	8.4	11.9	3 ⊙	3 ⊙	1	C 0	NE 3	SE 2
4	104.1	101.7	100.4	102.1	19.0	30.5	26.2	25.5	34.8	14.8	70	45	62	59	6.6	23.9	13.0	14.5	8	1	2	NNE 2	SE 6	S 4
5	101.5	100.6	103.3	101.8	26.4	34.5	25.9	28.2	35.6	21.7	56	34	66	52	15.2	36.3	11.5	21.0	0	0	8	W 3	W 4	N 1
6	108.1	107.2	106.0	107.1	20.3	27.0	21.2	22.4	29.5	17.6	55	38	60	51	10.8	21.9	10.0	14.2	7 ⊙	0 ⊙	0	NE 1	NNE 3	NE 2
7	104.4	104.9	102.9	104.1	19.0	30.6	26.6	25.7	33.0	16.0	65	38	63	55	7.8	27.4	13.0	16.1	9	0	3	E 6	ESE 4	SE 3
8	102.5	100.4	100.2	101.0	22.1	33.2	22.1	24.9	34.1	19.6	66	36	92	65	9.0	32.3	2.2	14.5	1 ⊙	5 ⊙	9 ●	NE 8	SE 3	C 0
9	101.3	101.6	101.4	101.4	18.9	23.6	18.4	19.8	25.2	17.6	92	67	89	83	1.7	9.7	2.3	4.6	10 ●	9	4	SSE 1	WNW 5	NE 1
10	99.8	96.4	94.9	97.0	17.7	24.6	17.9	19.5	25.1	14.3	87	53	98	79	2.6	14.5	0.4	5.8	10	8	10 ●	SE 2	E 3	C 0
11	91.7	92.4	94.2	92.8	17.2	20.2	18.3	18.5	21.6	16.4	95	81	91	89	1.0	4.6	1.8	2.5	10	10 ●	10 ●	NE 1	NE 4	NNE 4
12	96.1	97.5	98.2	97.3	16.7	19.4	19.5	18.8	24.1	16.0	96	85	90	90	0.8	3.4	2.2	2.1	10 ●	9	9	NNW 3	WNW 5	W 2
13	101.2	102.2	103.4	102.3	18.6	26.2	22.1	22.2	28.0	14.7	85	47	73	68	3.1	18.2	7.3	9.5	1	4	3	W 2	WSW 2	NW 2
14	102.2	101.2	101.3	101.6	19.9	22.1	17.5	19.2	27.7	14.4	88	79	96	88	2.8	5.6	0.8	3.1	1	10 ●	10	C 0	W 8	C 0
15	100.0	99.8	99.5	99.8	16.2	20.3	16.4	17.3	20.7	13.9	95	73	93	87	1.0	6.4	1.3	2.9	10	10	8	SW 1	W 5	S 1
16	98.3	97.7	96.4	97.5	15.2	18.1	17.3	17.0	18.7	14.5	89	70	76	78	1.9	6.2	4.7	4.3	10 ●	10	10 ●	W 3	W 7	NW 6
17	95.9	97.0	98.3	97.1	14.8	16.6	14.6	15.2	17.4	13.0	86	78	87	84	2.4	4.3	2.2	3.0	10	10 ●	10	W 6	WNW 4	SW 1
18	99.5	98.1	96.2	97.9	15.1	22.4	17.0	17.9	24.4	10.2	80	48	79	69	3.5	14.2	4.1	7.3	9	8 ⊙	0	W 3	NNW 3	SSW 1
19	95.4	93.6	92.1	93.7	16.4	26.1	20.7	21.0	27.3	10.1	79	44	74	66	3.8	19.0	6.3	9.7	0 ⊙	3 ⊙	5	SE 1	SE 4	SE 3
20	91.4	91.7	91.8	91.6	19.1	19.5	16.2	17.8	24.2	15.6	81	79	97	86	4.2	4.7	0.6	3.2	9	10 ●	10	S 2	SE 2	C 0
21	91.2	90.3	90.5	90.7	15.3	19.7	15.3	16.4	22.2	14.7	92	67	96	85	1.3	7.5	0.8	3.2	10	9	10	W 3	NW 2	SSW 2
22	89.4	88.2	86.9	88.2	14.8	14.7	15.9	15.3	16.1	14.1	90	91	96	92	1.6	1.5	0.8	1.3	10	10 ●	10	W 5	WSW 9	W 4
23	88.8	90.8	93.3	91.0	16.8	21.3	17.5	18.3	22.2	14.1	79	67	95	80	4.1	8.3	1.0	4.5	9 ⊙	9 ⊙	10 ●	NNE 4	NE 4	WNW 6
24	96.0	97.7	98.1	97.3	15.6	17.2	15.6	16.0	19.3	14.5	94	73	82	83	1.1	5.2	3.2	3.2	10	8	9	W 8	W 8	W 5
25	99.4	99.5	95.5	98.1	15.1	17.0	13.7	14.9	19.0	12.7	79	69	95	81	3.7	6.0	0.7	3.5	4	10 ●	8	W 7	W 8	C 0
26	97.7	97.7	96.1	97.2	14.3	16.9	14.3	15.0	19.0	11.1	89	81	93	88	1.8	3.7	1.1	2.2	8 ⊙	10 ●	9	W 5	SSW 4	WSW 2
27	92.1	91.7	92.1	92.0	17.1	17.5	14.4	15.8	20.8	13.0	89	84	90	88	2.2	3.2	1.6	2.3	10	9	9 ●	SSW 5	SSW 5	W 4
28	94.2	95.1	95.4	94.9	13.9	17.5	14.0	14.8	19.0	10.2	84	63	89	79	2.5	7.4	1.8	3.9	8	7	9	SW 5	SW 4	S 2
29	96.6	98.2	100.7	98.5	13.4	20.6	16.5	16.8	21.4	11.5	95	61	78	78	0.7	9.5	4.3	4.8	8	8	9	C 0	SSW 6	W 3
30	102.2	103.7	106.3	104.1	16.3	16.6	14.6	15.5	17.3	13.9	83	81	93	86	3.1	3.7	1.1	2.6	9	10	10	WSW 5	W 8	W 5
31	108.9	111.1	111.7	110.6	14.6	15.8	15.2	15.2	17.3	13.8	95	84	78	86	0.7	2.8	3.9	2.5	10 ●	10	9	W 4	W 6	NW 3
M	98.9	98.8	98.7	98.8	17.5	22.4	18.5	19.2	24.3	14.4	82	63	83	76	4.1	12.1	4.4	6.9	7.0	7.1	7.2	3.1	4.8	2.4

Sierpień – Août

1	111.8	111.1	109.4	110.8	13.8	20.7	15.7	16.5	23.2	12.1	84	58	92	78	2.5	10.2	1.3	4.7	10	6	1	SW 1	NW 2	C 0
2	109.7	109.0	109.7	109.5	15.3	21.3	13.7	16.0	22.2	11.2	92	58	81	77	1.3	10.5	3.0	4.9	4	5 ⊙	2	WNW 4	NW 6	WNW 1
3	109.7	108.9	109.0	109.2	12.8	16.9	12.1	13.5	18.0	8.4	79	65	89	78	3.1	6.6	1.5	3.7	1 ⊙	9	0	WNW 3	WNW 5	W 2
4	108.7	109.0	108.8	108.8	13.1	18.0	15.1	15.3	20.2	7.6	92	67	89	83	1.3	6.7	1.9	3.3	9	9	8	W 3	W 5	W 3
5	109.9	109.6	109.0	109.5	14.3	22.0	14.6	16.4	23.6	11.8	91	48	86	75	1.5	13.8	2.4	5.9	8	6	1	WNW 2	N 3	C 0
6	109.1	108.0	105.3	107.5	14.7	22.6	15.4	17.0	24.9	8.8	87	58	87	77	2.2	11.5	2.3	5.3	0 ⊙	5 ⊙	4	C 0	SE 1	SSE 2
7	102.0	99.1	96.5	99.2	17.3	20.8	16.9	18.0	23.8	14.6	79	78	89	82	4.1	5.4	2.1	3.9	9 ⊙	10	8 (R)	SE 3	S 4	SW 2
8	97.0	98.1	97.0	97.4	15.7	19.5	15.0	16.3	22.4	13.2	91	77	94	87	1.5	5.3	0.9	2.6	9	9	4	WNW 4	NNW 4	C 0
9	94.5	92.4	88.3	91.7	16.0	24.1	21.4	20.7	25.6	10.3	89	54	65	69	2.0	13.8	8.8	8.2	2 ⊙	5 ⊙	7	E 2	SE 6	ESE 3
10	88.1	89.6	93.4	90.4	17.1	22.3	16.3	18.0	24.1	15.9	96	66	93	85	0.8	9.1	1.3	3.7	10 ●	9 ⊙	5	W 3	SW 7	SW 2
11	98.6	98.3	97.7	98.2	18.5	26.8	21.7	22.2	27.4	13.6	76	45	77	66	5.1	19.4	6.0	10.2	1 ⊙	3 ⊙	3	S 3	SW 9	S 4
12	97.9	98.9	99.1	98.6	18.3	21.5	19.7	19.8	24.6	13.7	94	75	89	86	1.2	6.5	2.6	3.4	10 ●	4 ⊙	7	C 0	W 3	WSW 2
13	101.7	101.8	100.1	101.2	17.1	24.0	18.6	19.6	26.3	13.2	81	60	85	75	3.7	12.0	3.1	6.3	7 ⊙	4 ⊙	10	SW 1	S 5	SE 2
14	98.4	98.3	95.9	97.5	18.7	22.7	17.7	19.2	24.3	16.0	87	71	96	85	2.8	7.9	0.8	3.8	8	5 ⊙	10 ●	N 1	SW 2	W 4
15	96.5	96.1	95.9	96.2	15.1	22.7	18.9	18.9	23.6	13.2	93	62	83	79	1.2	10.5	3.7	5.1	4 ⊙	6 ⊙	10	WNW 1	WSW 3	SE 1
16	97.2	99.3	98.8	98.4	18.0	15.1	14.2	15.4	19.1	13.7	89	86	97	91	2.2	2.5	0.6	1.8	9	10	10	WNW 5	NW 3	SSE 3
17	99.1	98.6	98.2	98.6	13.4	16.7	13.2	14.1	18.0	10.7	84	71	92	82	2.5	5.5	1.3	3.1	9	9	10 ●	W 5	WSW 5	WSW 4
18	96.8	96.2	97.6	96.9	13.9	18.2	13.6	14.8	20.1	11.4	84	70	90	81	2.5	6.2	1.6	3.4	10	8	0	SSW 4	W 5	WSW 3
19	100.1	102.1	103.8	102.0	14.0	19.1	14.9	15.7	20.5	9.2	91	68	86	82	1.5	7.0	2.4	3.6	2 ⊙	5 ⊙	4	W 4	W 7	W 1
20	105.5	104.7	104.1	104.8	14.2	20.4	17.8	17.6	21.9	10.2	87	51	76	71	2.2	11.8	5.0	6.3	1 ⊙	1 ⊙	10	WNW 3	W 7	WNW 2
21	103.0	101.4	97.5	100.6	15.7	20.4	17.4	17.7	21.4	13.4	90	72	87	83	1.7	6.7	2.6	3.7	10	8	8	SW 2	SSW 2	SSW 1
22	98.9	99.1	100.1	99.4	12.6	16.1	10.0	12.2	18.3	9.6	88	66	87	80	1.7	6.1	1.6	3.1	10	8 ⊙	1	WNW 5	NW 6	W 1
23	100.7	99.8	98.0	99.5	9.5	18.0	12.6	13.2	19.4	5.7	88	49	74	70	1.4	10.5	3.7	5.2	0 ⊙	4 ⊙	1	WSW 2	SSW 2	E 1
24	94.4	92.2	98.3	95.0	11.2	18.1	11.7	13.2	21.1	8.0	83	82	83	83	2.3	3.7	2.3	2.8	4 ⊙	8 ●	0	SSE 6	S 4	WSW 4
25	101.9	99.7	96.6	99.4	11.7	20.6	15.8	16.0	21.8	7.9	83	47	71	67	2.3	12.9	5.1	6.8	0	7	0	SSE 3	SSE 8	S 4
26	97.1	97.4	99.6	98.0	13.7	17.9	10.3	13.0	18.7	10.0	89	53	85	76	1.8	9.6	1.9	4.4	9	9	2	WSW 3	WSW 8	SW 2
27	101.2	100.6	99.6	100.5	11.9	16.7	12.2	13.2	18.6	9.3	84	69	94	82	2.1	5.9	0.9	3.0	9	6	10	SW 4	W 3	C 0
28	98.6	99.5	101.9	100.0	12.2	15.8	12.0	13.0	16.5	10.7	95	76	94	88	0.7	4.3	0.8	1.9	10	10	9	C 0	WNW 2	C 0
29	103.8	105.1	106.4	105.1	10.1	15.0	11.5	12.0	16.6	8.0	91	64	84	80	1.2	6.0	2.2	3.1	9	9	0	WSW 6	WNW 6	W 2
30	107.5	107.2	106.5	107.1	10.9	16.2	9.1	11.3	17.2	8.8	86	53	89	76	1.8	8.6	1.3	3.9	2 ⊙	7 ⊙	2	WNW 5	W 8	C 0
31	104.2	103.6	102.0	103.3	10.5	14.9	11.4	12.0	18.2	5.6	85	71	82	79	1.9	4.8	2.5	3.1	9	6	10	SSE 2	SSW 4	SSW 3
M	101.4	101.1	100.8	101.1	14.2	19.5	14.9	15.9	21.3	10.8	87	64	86	79	2.1	8.4	2.5	4.3	6.3	6.8	5.1	2.9	4.7	1.9

Wrocław – Mały Gądów

$H_s = 116$ m $H_b = 118{,}6$ m $h_w = 22{,}5$ m

Lipiec – Juillet 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	= 4^30 – 8^15 ∞ – 11^40
2	7	.	.	-	= 5^20 – 7^40 ∞ – 9^10
3	8	.	.	-	
4	7	0.2	.	-	•▽^0 10^43 – 52 = 11^40 – 12^30
5	8	0.0	.	-	•▽^0 17^18 – 31 (K) 17^00 – 20^05 W–S
6	8	0.1	.	-	
7	8	.	.	-	•▽^0 4^15 – 25 (K) 2^55 – 5^10 NW – E
8	8	1.0	.	-	•▽^0 17^05 – 45 19^15 – 40 20^10 – 35 21^40 – 22^07 (K) 16^20 – 17^05 K – 17^50 (K) – 20^00 ≤ 21^45 – 24 = 4^10 – 6^35
9	7	0.2	.	-	•▽^0 0^22 – 42 2^16 – 30 5^35 – 6^12 6^20 – 7^08 7^40 – 9^30 •^0 11^05 (K) 5^25 – 45 K – 7^00 (K) – 7^10 N–S = 4^10 – 5^15 7^10 – 11^40
10	7	29.6	.	-	•^0 8^10–30 •▽^0 17^07 – 19^25 •^0 – 21^50 •^1 – 22^45 •^0 – 24 (K) 16^25 – 17^07 W–E K^0 – 18^35 W–E = 3^20 – 4^15 ≡ – 5^10 = – 10^45 20^20 – 24
11	7	3.6	.	-	•^0 0^00–20 1^45 – 2^50 •^2 – 3^12 •^0 – 4^48 5^05 – 7^40 11^45 12^15 13^22 14^12 15^40 16^10 •▽^0 17^50 – 18^08 •^0 19^45 20^10 •▽^0 21^45 – 22^01 •^1 – 22^45 •^0 – 24
12	6	0.9	.	-	•^0 0^00 – 1^45 2^30 – 3^30 •^1 4^25 – 5^10 •^0 6^10 – 11^32 12^40 = 2^00 – 17^40 [11.VII: = 0^00 – 10^30
13	8	.	.	-	= 1^30 – 8^40 ⌓^0 n – 8^30
14	6	4.6	.	-	•▽^0 13^45 – 18^35 (K) 0 14^10 – 35 K^0 – 17^25 E–W = 0^30 – 3^40 ≡ – 6^30 = – 10^10 13^30 – 17^10 ⌓^0 23^00 – 24
15	7	1.3	.	-	•^0 9^35 – 11^40 •▽^0 13^37 – 42 14^08 – 45 15^12 – 16^25 •^0 16^40 17^10 = 1^30 – 12^15 17^30 – 24 ⌓^0 0^00 – 9^35
16	7	0.0	.	-	•^0 1^45 – 2^15 6^10 – 30 7^45 8^23 •▽^0 21^45 – 22^30 •^0 – 23^15 = 0^00 – 11^12
17	7	1.2	.	-	•^0 1^10 2^15 3^40 5^25 12^50 13^25 – 17^20
18	8	.	.	-	•^0 1^10 2^00 – 25 = 4^10 – 7^30
19	8	.	.	-	= 2^20 – 10^40 ⌓^1 2^30 – 10^15 ⊕ 16^40 – 20^30
20	8	13.7	.	-	•▽^0 9^25 – 10^05 •▽^0 11^03 – 12 13^08 – 14^10 16^48 – 56 •▽^0 – 17^10 •^0 – 18^27 19^48 – 21^15 22^10 – 35 •^0 – 24 K^0 17^00 – 55 E–W = 4^30 – 17^15
21	7	26.4	.	-	•^0 0^00 – 35 3^40 – 4^15 6^40 – 7^12 •▽^1 19^25 – 50 •▽^0 – 21^40 (K) 18^50 – 19^20 K^0 – 20^40 SW–NE = 1^30 – 10^30 21^10 – 24 ⊕ 13^40 – 17^10
22	6	14.1	.	-	•^0 8^25 – 16^40 = 0^00 – 17^10
23	8	31.9	.	-	•▽^0 16^05 – 12 18^10 – 19^08 20^20 – 21^30 •^0 – 24 (K)^0 19^50 – 20^45 W–E ⌓^0 n – 10^30
24	7	0.0	.	-	•^0 0^00 – 3^10 •^2 – 4^18 8^47 – 9^05 •▽^0 11^03 – 15 = 7^30 – 9^37
25	8	1.7	.	-	•▽^0 13^52 – 14^06 •^0 16^46 17^35 – 20^25 = 18^25 – 24
26	7	1.6	.	-	•^0 1^30 2^35 •▽^0 – 12^35 14^10 – 30 •^0 14^46 15^15 16^45 – 20^45 = 0^00 – 4^20 17^40 – 20^30
27	8	12.4	.	-	•^0 10^40 11^10 •▽^0 11^25 – 40 •▽^2 – 11^50 •▽^0 – 12^34 21^15 – 22^25 •^0 23^10 24 K^0 11^30 – 11^45 – 12^20 WNW – E
28	8	8.6	.	-	•^0 0^00 10 – 1^50 •▽^0 12^03 – 20 14^52 – 15^44 17^06 – 27 18^35 – 42
29	8	1.3	.	-	•▽^0 1^36 – 2^25 5^47 – 6^30 6^45 – 7^25 10^25 – 42 16^48 – 17^03
30	7	1.1	.	-	•▽^0 8^45 – 9^40 10^30 – 50 11^20 – 12^15 12^40 – 13^35 14^05 – 15^15 •^0 16^35 – 17^35 •^0 18^35 – 19^20 •^1 – 20^15 •^0 – 21^45 = 18^35 – 24
31	7	0.0	.	-	•^0 2^50 – 3^25 •^0 4^56 •^0 5^35 7^15 – 8^40 10^35 = 0^00 – 20 4^40 – 10^45
Σ	–	154.6	–	-	UWAGI:

Sierpień – Août

1	8	.	.	-	= 6^15 – 9^45 22^30 – 24
2	8	.	.	-	= 0^00 – 1^40 ≡ – 3^40 ≡ – 5^45 = – 8^20 ⌓^1 n – 9^00 ⌓ 23^30 – 24
3	8	.	.	-	⌓ 0^00 – 10^00 23^45 – 24
4	8	0.7	.	-	•▽^0 10^43 – 46 •^0 22^20 – 23^42 ⌓^0 0^00 – 8^15
5	8	.	.	-	•^0 0^50 – 1^10 ≡ 23^40 – 24
6	8	.	.	-	≡ 0^00 – 1^30 = – 4^40 ≡ – 6^25 = – 8^20 ⌓ n – 9^00
7	8	7.6	.	-	•▽^0 12^30 – 45 13^15 – 50 14^10 – 25 •^1 19^10 – 28 22^02 – 25 (K)^0 18^45 – 19^10 K^0 – 20^55 NW–SW (K)^0 21^50 – 23^30 NW–SE = 5^25 – 9^15 22^10 – 24
8	7	.	.	-	= 0^00 – 13^40 20^10 – 30 ≡ – 22^10 = – 23^25 ≡ – 24 ⌓^1 20^30 – 24 [7.VIII: ⌓^0 n – 11^00
9	6	10.9	.	-	≡ 0^00 – 3^10 = – 4^18 ≡ – 6^10 = 20^20 – 24 ⌓^1 0^00 – 10^40
10	8	11.4	.	-	•▽^0-1 2^02 – 30 •^0-1 4^35 – 6^15 •^0 6^40 – 10^30 •▽^1 16^13 – 50 •▽^0 17^30 – 18^10 19^45 – 20^01 K^0 0^03 – 30 SW–NE 16^25 – 30 – 50 W–E = 0^00 – 8^10
11	8	1.4	.	-	⌓^0 n – 10^00 23^00 – 24
12	8	1.6	.	-	•▽^0 7^23 – 9^20 10^03 – 35 (K)^0 7^05 – 40 SW–NE = 22^45 – 23^35 ≡ – 24 ⌓^0 0^00 – 7^23
13	8	0.7	.	-	•^0 23^15 – 24 ≡ 0^00 – 1^45 = – 4^15 ≡ – 6^10 ⌓^1 n – 11^20
14	7	4.9	.	-	•^0 0^00 – 12 1^25 3^35 – 4^38 9^14 – 10^20 20^12 – 23^35 = 0^00 – 5^30 ≡ – 6^15 = – 10^40 21^45 – 24
15	7	.	.	-	= 0^00 – 11^10 ⌓^0 n – 10^45 22^30 – 24
16	7	12.2	.	-	•^1 10^00 – 11^40 •^0 – 13^15 14^10 – 15^35 17^16 – 18^20 = 4^20 – 7^30 20^35 – 24 ⌓^0 0^00 – 9^10
17	8	1.6	.	-	•^0 5^35 6^10 •▽^0 15^35 – 16^10 •^0 19^43 20^22 21^13 – 22^15 = 0^00 – 3^20
18	8	0.4	.	-	•▽^0 16^02 – 14 (K) 15^40 – 16^45 SW – E
19	7	.	.	-	= 4^20 – 10^15 ⌓^0 n – 10^40 ⌓^1 21^30 – 24
20	7	0.2	.	-	= 3^30 – 8^12 ⌓^1 0^00 – 9^20
21	7	5.9	.	-	•^0 4^40 – 5^35 22^20 – 24 = 5^10 – 8^30
22	8	2.2	.	-	•^0 0^00 – 3^30 •^0 8^45 – 9^10 •▽^0 12^18 – 30 13^01 – 06 15^18 – 25 17^03 – 40 17^50 – 18^05 = 2^00 – 10^15
23	8	.	.	-	≡ 5^10 – 6^40 ⌓^0 20^40 – 24
24	7	10.5	.	-	•^0 12^45 – 13^15 14^50 15^20 – 16^53 •▽^0-1 17^25 •^0 – 18^10 ≫ 17^03 – 12 = 5^30 – 10^40 ⌓^0 0^00 – 10^40
25	8	0.0	.	-	⌓^1 n – 8^40
26	8	0.0	.	-	•^0 6^02 40 7^35 45 8^30 40 •▽^0 16^05 – 10 ◠ 6^05 – 16
27	8	4.3	.	-	•^0 8^46 9^02 •▽^0-1 11^52 – 12^17 •▽^0 14^40 – 52 15^38 – 50 17^40 – 18^15 = 21^30 – 24 ⌓^0 2^20 – 8^30
28	8	0.0	.	-	•^0 1^45 5^35 14^48 – 15^20 19^03 22 = 0^00 – 6^15 22^25 – 24
29	8	.	.	-	= 0^00 – 10^40 22^45 – 24 ⌓^1 n – 10^30
30	8	.	.	-	= 0^00 – 7^40 ⌓^1 21^30 – 24
31	7	0.1	.	-	•^0 11^53 13^20 •▽^0 23^45 – 50 = 7^30 – 10^40 ⌓^1 0^00 – 8^20
Σ	–	75.6	–	-	UWAGI:

Wrocław – Mały Gądów $\varphi = 51°08'$ $\lambda = 16°59'$ Wrzesień – Septembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE : POGODA N,w			KIERUNEK : PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	103.6	103.9	105.0	104.2	10.6	15.6	9.6	11.4	17.5	6.9	86	57	86	76	1.8	7.6	1.8	3.7	2	9	1	SW 6	W 5	C 0
2	103.9	102.3	100.9	102.4	9.3	18.6	13.8	13.9	18.9	3.4	93	59	90	81	0.8	8.7	1.6	3.7	8	10	10 ●	C 0	S 4	S 3
3	101.3	102.4	104.1	102.6	13.2	17.0	13.6	14.4	18.5	10.6	93	60	83	79	1.1	7.8	2.7	3.9	9	8	10	W 4	WNW 2	WNW 1
4	106.1	107.7	109.5	107.8	11.0	16.6	13.2	13.5	17.8	10.2	91	56	80	76	1.1	8.4	3.0	4.2	10	8 ⊙	9	WNW 3	NW 2	NW 1
5	109.4	106.7	104.8	107.0	7.4	18.1	15.1	13.9	20.4	4.2	99	57	70	75	0.2	9.0	5.1	4.8	1	6	10	C 0	SW 2	S 3
6	104.6	104.3	105.3	104.7	14.7	21.2	14.8	16.4	21.6	13.2	84	61	92	79	2.7	9.8	1.3	4.6	9	9	7	SW 1	SSW 1	W 1
7	105.9	105.1	104.6	105.2	11.3	24.2	17.4	17.6	25.0	8.5	99	51	76	75	0.2	14.7	4.8	6.6	10 ≡	4 ⊙	0	C 0	SE 4	SE 1
8	105.2	105.3	105.4	105.3	15.3	27.7	19.1	20.3	28.5	11.8	83	44	78	68	3.0	20.7	4.8	9.5	1	1 ⊙	4	C 0	SSW 4	S 4
9	105.5	106.9	109.8	107.4	16.7	24.4	16.7	18.6	25.4	13.2	82	61	81	75	3.5	11.8	3.7	6.3	0	7	10	SE 3	NW 7	NNW 5
10	109.8	107.9	104.9	107.5	13.9	17.0	14.1	14.8	20.0	13.2	94	74	89	86	0.9	5.1	1.8	2.6	9	9	9	WNW 1	C 0	SE 2
11	100.6	95.5	88.8	95.0	9.5	19.4	15.9	15.2	20.8	7.4	99	62	87	83	0.2	8.6	2.3	3.7	1 ⊙	9	10 ●	SE 1	SW 7	S 5
12	82.3	85.7	91.1	86.4	16.8	17.8	10.8	14.0	21.4	9.0	86	55	70	70	2.7	9.2	3.9	5.3	8	4 ⊙	0	SSE 5	W 10	S 5
13	93.8	92.3	89.9	92.0	10.8	17.5	10.8	12.5	18.0	7.0	74	47	80	67	3.4	10.7	2.6	5.6	3	8	5	S 5	SW 10	S 6
14	92.5	92.9	93.6	93.0	10.0	16.2	9.8	11.4	16.5	7.2	74	48	81	68	3.2	9.6	2.3	5.0	2	4	8	S 7	SSW 10	S 2
15	93.1	95.6	100.1	96.3	9.5	11.8	8.1	9.4	14.2	7.8	91	82	85	86	1.1	2.5	1.6	1.7	10	10 ●	0	SW 3	W 6	SW 3
16	101.7	101.7	104.6	102.7	8.5	13.8	6.9	9.0	14.4	5.4	84	54	94	77	1.8	7.4	0.5	3.2	10	9	2	S 6	SW 7	C 0
17	103.6	102.7	101.9	102.7	9.2	13.0	10.2	10.6	14.8	4.5	91	74	88	84	1.1	4.0	1.4	2.2	10 ●	8	10	WSW 6	WNW 6	WNW 2
18	100.8	100.9	100.3	100.7	10.2	14.8	9.2	10.8	15.1	8.9	91	51	88	77	1.1	8.2	1.4	3.6	9	6 ⊙	0	NW 3	NW 8	W 5
19	97.8	95.0	94.6	95.8	8.3	12.7	13.0	11.8	15.6	3.9	89	89	94	91	1.3	1.6	0.9	1.3	7	10 ●	10 ●	SW 3	SSW 5	W 5
20	96.3	99.8	101.6	99.2	10.8	12.0	9.4	10.4	13.4	8.8	89	80	95	88	1.5	2.8	0.6	1.6	4	9	9	W 5	NW 3	C 0
21	102.7	102.2	100.3	101.7	7.0	16.3	13.5	12.6	17.2	3.3	98	65	78	80	0.1	6.5	3.4	3.3	6	5	6	NE 1	SE 4	ESE 2
22	96.8	97.3	96.6	96.9	13.6	17.3	14.2	14.8	19.6	10.1	97	88	93	93	0.6	2.4	1.1	1.4	10 ●	10	0	S 3	WSW 4	S 3
23	91.5	86.4	89.2	89.0	16.2	16.3	14.8	15.5	17.4	13.2	84	88	86	86	2.9	2.3	2.4	2.5	10	10 ●	4	S 4	S 5	WSW 7
24	93.4	90.3	98.3	94.0	12.4	15.4	7.9	10.9	16.6	7.3	87	86	82	85	1.9	2.4	1.9	2.1	9	10 ●	8	WSW 2	WSW 2	W 8
25	103.1	104.6	105.7	104.5	5.4	11.5	4.8	6.6	12.4	4.0	84	47	86	72	1.4	7.2	1.2	3.3	0	7	1	W 5	W 6	W 2
26	103.6	102.9	105.1	103.9	2.8	11.8	3.2	5.2	12.4	-0.5	98	48	90	79	0.2	7.2	0.8	2.7	10 ≡	9	2	C 0	NE 2	SW 1
27	107.2	104.8	96.8	102.9	0.8	12.0	10.1	8.2	12.9	-0.6	92	47	68	69	0.5	7.4	4.0	4.0	7	6 ⊙	10	W 1	WSW 6	SW 8
28	95.1	95.1	95.7	95.3	10.5	13.8	10.3	11.2	14.0	9.5	82	64	81	76	2.3	5.7	2.4	3.5	8	9	9	W 7	W 8	W 5
29	92.2	87.8	87.5	89.2	8.7	11.6	9.2	9.7	12.1	8.1	94	90	91	92	0.6	1.3	1.1	1.0	10 ●	10 ●	10 ●	SW 3	S 3	W 7
30	93.6	96.7	101.6	97.3	5.8	8.3	7.0	7.0	10.1	4.8	80	69	84	78	1.8	3.5	1.6	2.3	9	10	9	W 8	W 10	WNW 1
31																								
M	99.9	99.4	99.9	99.7	10.3	16.1	11.6	12.4	17.4	7.5	89	64	84	79	1.5	7.1	2.3	3.6	6.7	7.8	6.1	3.2	5.1	3.2

Październik – Octobre

1	103.2	104.0	106.6	104.6	2.4	10.2	5.0	5.6	11.3	1.1	91	55	90	79	0.7	5.5	0.8	2.3	3	8	5	SW 2	NW 3	WNW 1
2	110.3	110.9	109.8	110.3	1.9	9.5	1.8	3.8	10.5	-1.9	98	61	96	85	0.1	4.6	0.3	1.7	9 ≡	9	0	C 0	NW 1	C 0
3	104.9	101.2	99.5	101.9	-1.4	11.8	9.2	7.2	13.0	-3.1	100	48	80	76	0.0	7.2	2.3	3.2	0 ≡	9	9	C 0	SSW 7	WSW 5
4	100.9	103.7	108.7	104.4	6.0	8.0	3.9	5.4	10.6	2.8	83	60	83	75	1.6	4.2	1.4	2.4	4 ⊙	5	2	W 7	WNW 7	WSW 4
5	111.0	109.7	106.5	109.1	6.2	11.1	6.2	7.4	12.3	3.6	86	57	79	74	1.3	5.7	2.0	3.0	9	9	9	WSW 5	SSW 5	SSW 2
6	106.8	109.0	111.9	109.2	8.0	12.0	8.4	9.2	14.6	5.4	89	80	94	88	1.2	2.8	0.6	1.5	9	10	9	SW 3	W 6	SW 1
7	111.7	112.0	112.2	112.0	9.2	13.8	6.0	8.8	14.3	6.0	89	79	92	87	1.2	3.4	0.8	1.8	9	10	0 ≡	SW 2	WSW 4	C 0
8	113.7	114.4	113.6	113.9	8.4	14.2	10.8	11.0	15.1	4.4	99	74	90	88	0.1	4.3	1.4	1.9	9 ≡	10	0	C 0	E 4	E 2
9	111.3	110.2	108.7	110.1	6.9	18.3	9.8	11.2	19.5	6.6	99	58	90	82	0.7	8.8	1.3	3.4	10 ≡	1	0	E 3	ESE 4	SE 3
10	107.8	106.9	106.8	107.2	7.0	20.2	12.4	13.0	20.7	4.8	93	52	78	74	0.7	11.3	3.2	5.1	0	0 ⊙	1	SE 2	S 7	S 4
11	107.3	105.9	106.2	106.5	4.9	19.3	9.4	10.8	20.3	3.3	97	45	88	77	0.3	12.4	1.4	4.7	1	2	0	C 0	S 2	S 2
12	108.2	109.0	113.4	109.5	7.4	15.5	12.8	12.1	16.7	3.9	87	79	94	87	1.3	3.7	0.9	2.0	7	6	10	S 1	W 7	C 0
13	114.3	112.5	110.2	112.3	10.0	15.5	7.3	10.0	17.3	6.8	99	76	97	91	0.2	4.3	0.3	1.6	10	1	0	C 0	S 3	SE 1
14	109.9	111.0	113.3	111.4	3.9	12.9	9.9	9.2	13.8	1.1	98	84	89	90	0.2	2.4	1.3	1.3	9 ≡	9	9	C 0	NW 3	NNW 1
15	114.6	114.5	114.0	114.4	6.5	12.9	9.0	9.4	13.2	2.6	99	79	95	91	0.2	3.1	0.7	1.3	10	8	8	SW 1	NNE 1	C 0
16	111.7	108.7	106.1	108.8	6.0	16.0	6.3	8.4	17.5	3.6	98	61	92	84	0.2	7.2	0.7	2.7	10 ≡	0	0	SE 1	SE 5	S 1
17	104.1	106.0	106.1	105.4	6.8	15.6	8.2	9.7	16.7	0.7	94	67	93	85	0.6	5.9	0.8	2.4	3	8	6	S 2	W 8	SSW 2
18	100.7	98.8	97.6	99.0	12.8	18.9	15.4	15.6	19.7	7.6	86	65	70	74	2.1	7.7	5.3	5.0	10	9	0	S 4	SW 9	S 6
19	96.6	94.8	93.2	94.9	12.7	21.4	13.8	15.4	22.5	9.6	77	48	74	66	3.4	13.2	4.1	6.9	9	8	0	S 5	S 5	S 5
20	98.6	101.5	103.9	101.3	9.6	9.6	8.6	9.1	14.4	7.6	83	89	96	89	2.1	1.3	0.5	1.3	10 ●	10 ●	10	NW 1	NW 1	W 1
21	104.4	101.8	97.9	101.4	5.2	10.2	5.7	6.7	12.2	2.7	100	80	86	89	0.0	2.5	1.3	1.3	10 ≡	2 ⊙	0	SSW 1	SE 6	SSE 5
22	92.4	89.0	89.2	90.2	2.5	12.6	6.1	6.8	14.1	-0.1	93	66	91	83	0.5	5.0	0.8	2.1	2	4 ⊙	1	E 2	SSE 7	SSE 4
23	94.3	98.2	101.9	98.1	7.8	9.5	4.0	6.3	10.9	1.6	90	66	83	80	1.1	4.0	1.3	2.1	10	7	0	WNW 3	WNW 7	SW 2
24	101.1	103.5	108.9	104.5	5.7	9.0	9.6	8.5	10.3	1.0	80	90	89	86	1.9	1.1	1.3	1.4	9	10 ●	8	S 5	SW 5	W 3
25	111.4	111.9	111.6	111.6	8.6	13.9	5.9	8.6	14.5	5.5	93	54	89	79	0.8	7.4	1.0	3.1	10	4 ⊙	0	W 1	SW 2	SE 2
26	110.4	108.9	107.5	108.9	-0.3	15.3	6.9	7.2	16.0	-0.8	96	60	90	82	0.3	7.0	1.0	2.8	0 ≡	0 ⊙	0	ESE 1	SE 5	S 2
27	106.4	105.1	105.0	105.5	-0.3	12.8	1.8	4.0	14.1	-1.2	98	69	93	87	0.2	4.6	0.6	1.8	10 ≡	2	0	C 0	SW 2	C 0
28	106.4	106.0	106.1	106.2	4.7	10.6	4.0	5.8	10.9	-1.8	95	71	95	87	0.4	3.7	0.4	1.5	10	10	3	W 1	SSW 4	S 1
29	105.5	104.9	104.0	104.8	2.7	15.5	9.6	9.4	16.1	-1.7	93	53	83	76	0.5	8.2	2.1	3.6	8	6	10	SE 2	SW 6	SSW 2
30	102.3	101.1	102.0	101.8	7.5	16.3	9.9	10.9	17.4	5.1	86	58	84	76	1.5	7.7	1.9	3.7	7	7 ⊙	9	S 4	SSW 6	C 0
31	102.1	100.9	98.0	100.3	4.3	15.0	7.4	8.5	15.4	2.1	92	59	88	80	0.7	6.9	1.2	2.9	1	5 ⊙	9	SW 1	SW 3	SW 2
M	105.9	106.0	105.8	105.9	5.9	13.8	7.9	8.9	15.0	2.9	92	66	88	82	0.8	5.7	1.4	2.6	7.0	6.1	3.8	1.9	4.7	2.1

Wrocław – Mały Gądów

$H_s = 116$ m $H_b = 118.6$ m $h_w = 22.5$ m

Wrzesień – Septembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌓⁰ n – 9³⁵
2	7	1.7	.	–	●⁰ 21¹⁰ 23²² · = 1¹⁰–5²⁰ ≡–6⁴⁰ = – 10⁴⁰ · ⌓¹ n – 10²⁰ · ⊕⁰ 9²⁰–10⁵⁰
3	8	0.0	.	–	●⁰ 1¹⁵–4³⁵ ▽⁰ 15⁰⁵–37 · = 3²²–9⁵⁰
4	8	.	.	–	= 7³⁰–9³⁰ · ⌓⁰ 23⁰–11⁴⁸ · ⌓ 23⁵⁵–24
5	8	.	.	–	= 2³⁰–5³⁵ ≡–7¹⁰ = –8³⁰ · ⌓⁰ n – 10²⁰ · ⌓ 0⁰⁰–0⁶ · 2⁴⁰–3⁰² · 3⁴⁰–5⁷
6	8	.	.	–	= 6²⁰–7⁵⁰ · 19³⁰–24 · ≡ 22⁴⁵–24 · ⌓⁰ 2³⁰–8²⁰
7	7	.	.	–	≡ 0⁰⁰–⁴⁰ =⁰–2⁰⁰ =¹–4⁴⁰ =²–8²⁰ =¹–8⁴⁰ =⁰–9¹⁵ = –12¹⁵ · 19⁵⁰–24 · ⌓⁰ n – 11⁵⁰
8	8	.	.	–	= 0⁰⁰–9²⁵ · ⌓⁰ 2³⁰–9⁴⁵
9	7	5.1	.	–	= 17⁴⁵–24 · ⌓⁰ n – 8²⁰
10	8	.	.	–	●¹ 0⁴⁵–3¹⁵ ●⁰–3³⁰ · = 0⁰⁰–8³⁰ · 20²⁰–24
11	7	0.0	.	–	●⁰ 1⁷¹⁰…²⁰ 17⁴⁵ 19¹² 21¹⁰–22³⁵ · = 0⁰⁰–12⁵ ≡–6¹² ≡–6²⁰ =²–7²⁵ =¹–7⁴⁰ =⁰–7⁵⁰ = –11³⁰ · ⊕ 12⁴⁵–16¹⁰
12	8	1.3	.	–	▽⁰ 1⁴⁶–2⁰⁴ 7⁰⁷–¹² 8³⁸–⁵² 10³⁰–⁴⁰ 11³⁰–³⁵ ▽¹–11⁴⁵ ▽⁰–12⁰⁵ · ≫ 11³⁰–⁵⁰ 12⁴⁰–16¹⁰
13	8	4.8	.	–	●⁰ 17⁵⁵–19¹⁵ · ≫ 10²⁰–17¹⁵ · 23³⁰–24
14	8	1.4	.	–	≫ 0⁰⁰–⁴⁰
15	7	0.2	.	–	●⁰ 0⁴⁰…¹²⁰ ●¹–2⁵⁰ ●⁰–4⁵⁰ 5¹⁰–⁴⁵ 11¹⁶–12⁴⁰ 14¹⁵
16	7	4.5	.	–	▽⁰ 14⁴⁰–15¹⁰ · 15³⁰–³⁵ 16²⁵–³⁸ 19⁴⁵–20¹⁵
17	7	3.7	.	–	●⁰ 1⁴⁵ 2³⁵ 3⁴⁰ 4³⁰–7¹⁵ 8²⁴ 9⁴⁰ 10³⁰–12²⁷ ▽⁰ 18⁰³–⁰⁵ ▽¹–18⁰⁸ ▽⁰–18¹⁵ 18⁴¹–⁵⁵ ●⁰ 22¹⁰–23⁴⁰ · = 6²⁰–12⁴⁵
18	8	.	.	–	●⁰ 5¹⁰–²⁵ · = 6³⁰–9¹⁰
19	7	10.5	.	–	●⁰ 0⁴⁰–10¹⁵ ●⁰–13²⁰ 15⁴⁵ 17³⁵…⁴⁵ 20²⁶–21⁴⁰ ●¹–22³⁰ ●⁰–23²²…²⁴ · = 0³⁰–13³⁵ 17⁴⁰–24
20	8	.	.	–	●⁰ 0⁰⁰…²⁰ · = 0⁰⁰–7¹⁵ · 22³⁰–24
21	7	4.0	.	–	= 0⁰⁰–5²⁰ ≡⁰–6⁴⁰ =¹–7¹⁰ ≡⁰–7²⁵ = –13⁴⁰ 18¹⁵–24 · ⌓¹ n – 9²⁰
22	7	0.2	.	–	▽⁰ 5³⁰–6¹⁵ ●⁰ 6³⁰–8³² 13²⁰–⁴⁰ · = 0⁰⁰–6¹⁰ ≡–7¹⁰ = –8⁴⁰ 18³⁰–24
23	7	9.8	.	–	▽⁰ 4¹⁵–³⁰ ●⁰ 9⁵⁰–12¹⁰ 12³⁰ 13⁰⁵–15³⁰ ●¹–16¹⁵ ●⁰–16³⁵ ▽⁰ 19¹⁸–⁴⁰ · = 0⁰⁰–6²⁰
24	6	2.8	.	–	●⁰ 10¹⁰…³⁰ 12²⁵…14¹⁰–17³⁰
25	8	.	.	–	⌓⁰ n – 10²⁰ np – 24
26	7	.	.	–	= 2⁰⁰–5¹⁵ ≡–7³⁰ ≡⁰–7⁵⁶ = – 12³⁰ · ⌓¹ 0⁰⁰–3³⁰ ⌴ –5³⁵ ⌓¹ np – 24
27	8	0.2	.	–	●⁰ 18³⁰–⁴⁰ 22¹²–⁴⁵ · ≫ 22²⁰–24 · ⌓¹ 0⁰⁰– na ⌴¹ –8²⁰
28	8	6.2	.	–	●⁰ 0³⁵–3²⁷ 5³²–⁴⁵ ▽⁰ 6²⁴–⁴⁰ 9²⁵–⁴⁰ 11¹⁰–³⁸ 12⁰⁵–²⁸ 14²⁰–³⁰ ▽¹ 15²⁰–⁴⁸ ▽⁰ 16¹⁰–³⁹ 18¹⁵–⁴⁵ 21⁵⁰–22⁰⁵ 22⁵²–23¹⁰
29	5	9.7	.	–	▽⁰ 0¹⁵–²⁷ 1¹⁰–³² 1³⁵–2¹⁰ 3⁴⁵–4⁰⁸ ●⁰ … 5²⁰–16²⁵ 22¹⁰–24 · = 5¹⁰–16¹⁰
30	8	0.0	.	–	●⁰ 0⁰⁰–⁴⁰ ▽⁰ 10⁰⁴–¹⁵ · ≫ 7¹⁵–13³⁰
31					
Σ	–	66.1	–	–	UWAGI.

28.IX: 23⁴⁰–⁴⁵ · ≫ 0⁰⁰–6³⁰

Październik – Octobre

1	8	0.0	.	–	▽⁰ 17²⁰–⁴⁰ · = 4³⁰–11⁴⁵ · ⌓¹ 0⁰⁰– α
2	8	.	.	–	= 0¹⁰–13⁰ ≡⁰–2⁴⁰ ≡¹–5¹⁵ ≡²–6⁴⁰ ≡¹–6⁵⁰ ≡⁰–8³⁰ = –10¹⁰ ≡ 19²⁰–20¹⁰ = –22⁴⁸ ≡¹–24 · ⌓¹ n – 10⁴⁵
3	8	0.0	.	–	●⁰ 19⁵⁰ 20¹⁰ · ≡¹ 0⁰⁰–3²⁵ ≡⁰–4⁴⁰ ≡¹–6¹⁰ ≡²–7²⁰ ≡¹–7⁵⁰ ≡⁰–8⁴⁰ = –10¹⁵ · ⌴⁰ n – 8²⁰
4	8	0.4	.	–	●⁰ 3³⁵…4³⁰ ▽⁰ 11⁰⁵–¹³ ▲⁰ 11⁴⁵–⁵⁰
5	8	1.6	.	–	= 21³⁰–24
6	6	0.0	.	–	●⁰ 3³⁸–6²⁰ 7²⁰–³⁸ · = 0⁰⁰–13¹⁰ 14²⁵–24
7	7	.	.	–	= 0⁰⁰–7³⁰ 13²⁰–19³⁰ ≡–20⁴⁵ ≡¹–21¹⁰ ≡²–24 · ⌓⁰ n – 8⁰⁰
8	6	.	.	–	≡² 0⁰⁰–3³⁰ ≡¹–3⁵⁰ ≡⁰–8³⁰ = –24 · ⌓¹ 0⁰⁰–9²⁰ · 19²⁰–24
9	6	.	.	–	= 0⁰⁰–4²⁵ ≡¹–5³⁰ ≡²–7⁴⁰ ≡¹–8¹⁵ ≡⁰–9¹⁵ = –12²⁰ ∞– 16⁴⁵ = –22⁴⁵ ≡ –24 · ⌓¹ 0⁰⁰– 11³⁰
10	7	.	.	–	≡ 0⁰⁰–3⁴⁰ = –8³⁰ · 17³⁰–24 · ⌓⁰ n – 10⁰⁰ ⌓¹ 19⁴⁰–24
11	8	.	.	–	= 0⁰⁰–5³⁵ ≡–7³⁰ ∞ 9²⁰–10⁵⁰ = 20³⁰–24 · ⌓¹ 0⁰⁰–10⁰⁰
12	5	.	.	–	= 0⁰⁰–23⁵⁰ ≡⁰–24 · ⌓¹ n – 10²⁰
13	5	.	.	–	≡⁰ 0⁰⁰–6⁵⁰ = –24 · ⌓¹ 0⁰⁰–10³²
14	5	.	.	–	= 0⁰⁰–1³⁰ ≡⁰–7²⁰ = –22⁴⁵ ≡⁰–23¹⁰ ≡¹–23⁴⁵ ≡²–24 · ⌓⁰ n – 11⁰⁰ ⌓¹ np – 24
15	5	.	.	–	≡² 0⁰⁰–3⁰⁷ ≡¹–3³⁰ ≡⁰–3⁴⁵ = –24 ≡ 21³⁰–22¹⁰
16	6	.	.	–	= 0⁰⁰–²⁰ ≡⁰–0⁵⁰ ≡¹–1³⁸ ≡²–3¹⁰ ≡⁰–4²⁵ ≡¹–5³⁸ ≡²–7²⁰ ≡¹–8¹⁰ ≡⁰–8⁴⁸ = –24 · ⌓¹ 20⁰⁰–24
17	7	.	.	–	= 0⁰⁰–10³⁰ ≡ 5²⁰–6⁴⁰ = 16⁴⁰–24 · ⌓¹ 0⁰⁰–10⁰⁰
18	7	0.5	.	–	●⁰ 7²⁰–9¹⁰ · = 0⁰⁰–11¹⁸ 16²⁰–20¹⁰
19	8	0.0	.	–	= 5²⁰–6³⁰ · ⌓⁰ n – 7⁵⁰
20	7	3.0	.	–	●⁰ 6²⁵ 7¹⁰–14³⁵ · = 16⁴⁰–19⁴⁰ ≡² 22⁵⁵–24 · ⌓¹ 23⁰⁰–24
21	6	.	.	–	≡² 0⁰⁰–5³⁰ ≡⁰–7⁴⁰ = –24 · ⌓¹ 0⁰⁰–10²⁰ ⌓⁰ 21⁴⁰–24
22	6	.	.	–	= 0⁰⁰–14³⁰ 15¹⁰–24 · ⌓⁰ 0⁰⁰–5³⁰ ⌴⁰–8⁰⁰ ⌓¹ 20⁴⁰–24
23	7	.	.	–	= 0⁰⁰–11³⁰ · ⌓¹ 0⁰⁰–9⁴⁰
24	6	0.4	.	–	●⁰ 11¹²…15⁴⁰ · = 10²⁰–24 · ⌓¹ n – 9¹⁰
25	7	.	.	–	= 0⁰⁰–11²⁵ 16²⁵–24 · ⌓⁰ 22⁴⁰–24
26	6	.	.	–	= 0⁰⁰–5²⁵ ≡⁰–7³⁸ = –13⁰⁰ ∞– 16⁰⁰ = –24 · ⌓⁰ 0⁰⁰–5²⁵ ⌴⁰–9⁰⁰
27	6	.	.	–	= 0⁰⁰–3³⁵ ≡⁰–4²⁰ =¹–6³⁵ ≡²–8⁴⁵ =¹–9⁵⁰ = –22⁵⁰ ≡¹–24 · ⌴¹ n – 7¹⁰ ⌓¹ 19³⁰–23 ⌴¹–24
28	6	.	.	–	≡¹ 0⁰⁰–4⁵⁰ = –24 · ⌴¹ 0⁰⁰–4³⁰ ⌓¹ 20³⁰–24
29	7	.	.	–	= 0⁰⁰–11³⁰ · 15²⁰–24 · ⌓¹ 0⁰⁰–3²⁰ ⌴¹–7¹⁰
30	7	.	.	–	= 0⁰⁰–2²⁰ 4³⁰–11¹⁰ 15³⁸–24
31	7	.	.	–	= 0⁰⁰–5²⁵ ≡–8⁴⁰ = –12³⁰ · 14⁴⁰–24 · ⌓¹ n – 10¹⁵ · 21¹⁰–24 · ⊕ 14²⁰–15⁴⁰ · ⊖ 17⁴⁰–21²⁰
Σ	–	5.9	–	–	UWAGI.

Wrocław – Mały Gądków $\varphi = 51°08'$ $\lambda = 16°59'$ Listopad – Novembre 1957

DNI	CIŚNIENIE p = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	93.6	93.0	95.3	94.0	4.9	13.9	8.9	9.2	15.0	1.9	95	61	84	80	0.5	6.2	1.8	2.8	2	7	9	SSE 2	WSW 5	S 2
2	97.8	99.0	100.1	99.0	8.5	11.6	9.8	9.9	12.1	7.2	81	65	75	74	2.1	4.7	3.0	3.3	9	9	9	W 1	SW 3	SW 1
3	101.4	100.0	98.4	99.9	4.3	12.5	10.3	9.4	12.9	2.6	90	55	91	79	0.8	6.6	1.1	2.8	5	8	0	C 0	SE 3	SE 2
4	98.0	97.2	98.4	97.9	5.4	16.0	6.8	8.8	16.8	3.4	97	57	93	82	0.3	7.9	0.8	3.0	0	4 ⊙	2	SE 1	SSE 6	S 2
5	94.3	91.4	92.5	92.7	6.4	17.0	9.9	10.8	18.4	5.8	94	59	81	78	0.6	8.0	2.4	3.7	4	8	2	SE 4	SSW 3	SSE 4
6	93.0	93.8	92.2	93.0	8.1	16.7	8.8	10.6	17.6	5.8	86	57	90	78	1.5	8.2	1.1	3.6	6	6 ⊙	6	SE 3	SSE 5	ESE 3
7	89.6	92.8	94.3	92.2	10.8	12.6	9.6	10.6	15.0	8.4	81	80	93	85	2.5	2.9	0.8	2.1	7	9 ●	10 ●	SSE 3	NW 3	NNW 1
8	91.9	91.9	91.8	91.9	11.0	16.3	10.8	12.2	16.8	8.8	84	64	95	81	2.1	6.7	0.7	3.2	9	6	9	E 1	SSE 5	E 1
9	90.4	91.3	93.8	91.8	10.0	13.5	11.2	11.5	14.1	8.8	92	85	91	89	1.0	2.3	1.2	1.5	10	9	9	E 1	SE 2	SE 1
10	94.6	94.4	96.6	95.2	6.3	15.7	8.8	9.9	16.5	3.6	98	57	93	83	0.1	7.6	0.8	2.8	0 ≡	0 ⊙	10	E 2	SE 5	E 7
11	98.3	100.3	103.3	100.6	10.1	10.8	8.8	9.6	11.4	8.1	85	76	84	82	2.0	3.1	1.8	2.3	10	10	10	ENE 5	NE 7	NE 5
12	107.1	110.4	113.4	110.3	6.4	6.0	5.2	5.7	9.2	4.7	89	80	86	85	1.0	1.9	1.2	1.4	10 ●	10	10	NE 4	NE 4	NE 3
13	114.5	115.8	116.0	115.3	3.4	3.6	1.4	2.4	5.7	1.0	90	68	76	78	0.8	2.5	1.7	1.7	10	10	10	NE 1	ENE 3	NE 2
14	116.4	117.2	118.0	117.2	-1.3	-0.6	-0.6	-0.8	1.8	-1.6	83	79	88	83	1.0	1.2	0.7	1.0	10	10	10	ENE 4	ENE 3	E 3
15	117.4	116.7	115.6	116.6	-0.7	-0.3	0.6	0.0	0.7	-1.5	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡	10	10	ESE 6	ESE 5	E 2
16	115.8	116.3	117.4	116.5	1.2	2.8	2.4	2.2	3.3	0.3	96	91	91	93	0.3	0.7	0.7	0.6	10	10 ≡	10	C 0	E 1	NE 1
17	117.0	116.7	117.8	117.2	1.6	2.9	2.8	2.5	3.9	1.1	91	88	88	89	0.7	0.9	1.0	0.9	10	4 ⊙	10	NE 3	E 2	E 3
18	117.5	117.0	117.1	117.2	2.2	3.2	2.6	2.6	3.5	1.7	86	81	89	85	1.1	1.5	0.8	1.1	10	10	10	E 2	SE 4	E 2
19	117.3	118.8	121.8	119.3	2.4	3.2	1.8	2.3	3.7	1.5	87	81	71	80	1.0	1.5	2.1	1.5	10	10	10	E 2	ENE 4	E 4
20	122.4	123.1	124.2	123.2	-0.9	3.2	-0.5	0.3	3.4	-2.3	77	63	80	73	1.3	2.9	1.2	1.8	9	4 ⊙	0	E 5	SE 4	E 3
21	123.2	121.0	116.9	120.4	-5.5	4.2	-1.1	-0.9	5.1	-6.7	95	64	85	81	0.2	2.9	0.8	1.3	0	1 ⊙	0	E 1	E 1	SE 3
22	109.8	105.2	104.8	106.6	-0.8	4.8	1.6	1.8	5.6	-2.7	87	62	74	74	0.7	3.2	1.8	1.9	0	6	10	S 4	S 9	SSW 7
23	104.1	104.2	108.3	105.5	1.6	5.1	3.8	3.6	5.4	0.8	76	70	78	75	1.7	2.6	1.7	2.0	10	10	8	S 2	W 10	W 7
24	110.9	110.4	109.9	110.4	2.8	5.9	5.5	4.9	6.4	0.6	81	73	83	79	1.5	2.5	1.5	1.8	9	9	10	W 6	W 8	W 9
25	107.3	108.1	109.5	108.3	5.4	5.4	6.0	5.7	6.2	4.5	83	94	92	90	1.6	0.6	0.8	1.0	10 ●	10 ●●	10 ●	W 8	W 9	W 7
26	110.4	110.4	109.6	110.1	6.0	6.9	6.6	6.5	7.2	5.3	91	85	81	86	0.9	1.4	1.8	1.4	10	10	10	W 6	W 8	W 8
27	105.9	105.2	106.3	105.8	5.8	7.4	7.4	7.0	8.3	5.2	86	84	84	85	1.3	1.6	1.6	1.5	10 ●	10	9	W 9	W 7	W 6
28	104.0	101.5	96.7	100.7	8.5	8.6	8.3	8.4	9.2	6.7	86	81	89	85	1.5	2.2	1.3	1.7	10	10	10 ●	W 9	W 10	W 11
29	95.7	102.0	111.0	102.9	5.7	1.2	-2.5	0.5	9.1	-3.1	86	61	76	74	1.3	2.7	1.2	1.7	10 ●	3 ⊙	9 ✳	WNW 7	NNW 8	N 8
30	118.2	117.7	117.6	117.8	-7.3	-3.0	-4.5	-4.8	-2.0	-7.9	85	79	81	82	0.5	1.0	0.8	0.8	6	9 ✳	4	NW 5	N 5	N 3
31																								
M	105.9	106.1	107.0	106.3	4.1	7.6	5.0	5.4	8.7	2.4	88	73	85	82	1.1	3.3	1.3	1.9	7.5	7.7	7.9	3.6	5.1	4.0

Grudzień – Décembre

1	117.8	117.0	114.0	116.3	-6.7	-5.1	-2.7	-4.3	-2.0	-9.1	86	95	89	90	0.5	0.2	0.6	0.4	1	8	10 ✳	NW 2	W 2	W 7
2	111.7	112.4	113.5	112.5	-1.3	0.3	0.6	0.0	0.8	-3.0	97	96	96	96	0.2	0.2	0.3	0.2	10	10 △	10 ✳	WNW 2	N 3	N 1
3	110.3	107.9	108.7	109.0	1.2	2.3	3.2	2.5	3.4	0.1	98	96	97	97	0.2	0.3	0.3	0.3	10	10	10	WNW 2	NW 4	NNW 4
4	109.8	109.8	109.4	109.7	2.9	3.1	3.3	3.2	3.7	1.9	96	93	90	93	0.2	0.5	0.7	0.5	10 ●	10	10	NNW 1	WNW 5	W 6
5	107.2	107.2	109.6	108.0	3.0	5.6	4.2	4.2	6.0	2.0	96	81	82	86	0.3	1.7	1.4	1.1	10 ●	9	2	W 7	NW 7	WNW 6
6	112.3	112.7	110.3	111.8	3.3	3.6	-3.2	0.1	4.6	-4.8	91	81	99	90	0.6	1.5	0.0	0.7	9	9	0 ≡	WNW 3	N 2	SE 2
7	103.2	99.7	93.3	98.7	-5.3	3.5	-1.0	-1.0	4.8	-5.6	93	62	81	79	0.3	3.0	1.1	1.5	6	4	10	C 0	WSW 2	SSW 6
8	79.3	71.7	68.1	73.0	3.2	4.0	6.8	5.2	8.9	-1.8	78	92	77	82	1.7	0.6	2.3	1.5	10	10 ●	2	SSW 6	S 8	W 8
9	65.7	76.3	85.6	75.9	6.6	3.5	-0.1	2.5	7.7	-0.5	84	68	76	76	1.5	2.5	1.5	1.8	10 ●	9	8	WSW 6	W 13	W 5
10	84.6	85.2	95.3	88.4	-2.5	2.3	-5.9	-3.0	2.9	-6.8	93	80	84	86	0.4	1.4	0.6	0.8	10	10	0	SW 1	W 9	W 3
11	93.0	89.7	84.4	89.0	-6.1	-0.1	-0.3	-1.7	0.9	-8.2	84	73	80	79	0.6	1.7	1.2	1.2	2	9	10	ESE 5	E 4	SE 3
12	81.6	81.5	80.5	81.2	-0.9	6.5	1.8	2.3	6.6	-2.6	97	71	94	87	0.2	2.9	0.4	1.2	10	1 ⊙	0	E 2	E 3	E 1
13	77.3	75.3	69.3	74.0	3.1	7.3	5.6	5.4	9.6	-0.8	95	81	94	90	0.4	1.9	0.6	1.0	9	9	10 ●	E 2	SE 3	E 1
14	70.6	77.5	86.8	78.3	0.4	1.2	-0.3	0.2	5.9	-0.8	98	94	100	97	0.1	0.4	0.0	0.2	10 ●	10 ●	10 ✳	WNW 5	W 5	N 1
15	99.3	105.9	111.7	105.6	-4.2	-5.2	-11.4	-8.0	-0.3	-11.7	91	80	86	86	0.4	0.8	0.4	0.5	10 ✳	10	0	NNE 3	NNE 3	NE 2
16	114.1	113.8	113.3	113.7	-13.6	-8.3	-11.4	-11.2	-7.1	-15.2	88	75	86	83	0.3	0.8	0.4	0.5	0	0	0	E 2	NE 4	E 4
17	109.6	108.7	108.6	109.0	-12.9	-8.5	-7.2	-9.0	-7.0	-17.6	88	86	90	88	0.3	0.4	0.3	0.3	10	10	10	E 1	C 0	C 0
18	109.8	110.3	110.7	110.3	-6.5	-5.3	-4.6	-5.2	-4.2	-7.7	94	95	91	93	0.2	0.2	0.4	0.3	10	10	10	NW 1	N 2	SE 2
19	110.2	112.1	116.8	113.0	-3.4	0.2	-0.2	-0.9	0.8	-4.8	94	90	96	93	0.3	0.6	0.2	0.4	10	9	10 ✳	ESE 2	C 0	S 2
20	119.6	120.9	118.6	119.7	1.6	2.7	-1.5	0.3	3.2	-1.8	96	93	90	93	0.3	0.5	0.5	0.4	10 ● ≡	9	0	W 3	SW 3	S 3
21	115.5	114.6	115.2	115.1	0.8	3.5	2.1	2.1	4.5	-4.8	83	85	93	87	1.2	1.2	0.5	1.0	0	6	10	SSW 8	S 4	SW 2
22	113.5	112.8	111.6	112.6	1.6	3.9	-0.3	1.2	4.1	-0.6	94	90	98	94	0.4	0.8	0.2	0.5	10	9	0	SE 1	SE 2	SE 1
23	106.4	105.1	103.9	105.1	-3.9	0.1	-4.6	-3.2	0.6	-5.4	94	72	86	84	0.3	1.8	0.6	0.9	1	3	0	SE 6	S 4	SSE 1
24	102.9	103.2	104.4	103.5	-6.0	1.0	-4.5	-3.5	1.4	-6.7	87	70	91	83	0.5	2.0	0.4	0.9	3	7	0	SE 1	SSE 2	C 0
25	105.1	104.5	107.4	105.7	-7.2	0.4	-2.5	-3.0	1.0	-9.2	88	88	93	90	0.4	0.8	0.4	0.5	2	8	4	C 0	SE 1	SW 2
26	110.1	111.4	113.5	111.7	-4.0	4.0	-0.9	-0.4	4.9	-5.7	91	82	96	90	0.4	1.5	0.2	0.7	3	2	4	C 0	W 2	SW 1
27	113.3	112.7	111.6	112.5	-2.1	3.5	-1.1	-0.2	4.9	-3.7	96	86	96	93	0.2	1.0	0.2	0.5	6	9	0	SW 2	SW 2	SW 2
28	106.4	103.5	99.5	103.1	-5.3	3.1	0.2	-0.4	3.6	-8.5	98	81	82	87	0.1	1.4	1.1	0.9	0 ≡	1	10	ESE 2	SW 3	SW 4
29	97.5	96.2	91.9	95.2	1.9	2.9	2.3	2.4	4.2	-0.2	93	83	84	87	0.5	1.3	1.2	1.0	10	8	9	SW 6	SW 6	SW 12
30	88.7	86.9	86.0	87.2	3.3	4.7	4.1	4.0	6.1	1.8	86	79	85	83	1.0	1.7	1.2	1.3	10	9	10	SW 7	SW 7	SW 8
31	88.9	89.3	89.6	89.3	1.2	3.4	2.5	2.4	4.8	0.3	89	80	86	85	0.8	1.6	1.0	1.1	3	8	6	WSW 7	W 6	SW 6
M	101.1	101.2	101.4	101.2	-1.9	1.4	-0.9	-0.6	2.9	-4.6	91	83	89	88	0.5	1.2	0.6	0.8	6.9	7.6	5.6	3.1	3.9	3.4

Wrocław – Mały Gądów

$H_s = 116$ m $H_b = 118.6$ m $h_w = 22{,}5$ m

Listopad – Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	= 0⁰⁰–2²⁵, ⌓¹ 0⁰⁰–2³⁰ ⌴⁰–7⁴⁰
2	7	0.0	.	–	•⁰ 18¹⁰...³⁰ = 15¹⁰–24
3	7	.	.	–	= 0⁰⁰–6¹⁰ ≡–7¹⁰ = –11³⁰, 16⁴⁰–24, ⌓¹ n–10⁰⁰, 20³⁰–24, ⊕ 11¹⁰–12³⁵
4	7	.	.	–	= 0⁰⁰–6¹⁰ ≡–8²³ = –12⁴⁰, 17⁵⁰–24, ⌓¹ 0⁰⁰–4²⁰ ⌴⁰–9⁴⁵ ⌓¹ 20⁴⁷–24
5	7	.	.	–	= 0⁰⁰–10¹⁵, ⌓¹ 0⁰⁰–9¹⁰
6	7	.	.	–	= 7¹⁰–9³⁵, 16⁴⁵–24, ⊖ 0²⁰–4²⁰, ◠ 23³⁰–24
7	7	0.6	.	–	•⁰ 11²⁵ 12³⁰, 15⁵⁰ 16⁴⁰ 20³⁵ 21¹⁰–22³⁸, = 0⁰⁰–7³⁰, 16³⁰–24; ⌓¹ n–9⁰⁰
8	6	1.0	.	–	•⁰ 15¹⁵...⁴⁰ 16⁴⁰–17³⁵, = 0⁰⁰–24
9	6	0.4	.	–	•⁰ 8⁰⁷–10²⁰, 10³⁰...⁴⁰ 16⁴⁰–17¹⁰, = 0⁰⁰–24
10	6	.	.	–	= 0⁰⁰–25 ≡–2⁵⁰ ≡⁰–3⁴⁰ ≡¹–7³⁰ ≡²–8²⁵ ≡⁰–9¹⁰ = –12³⁰ ∞–16⁵⁰ = –24; ⌓⁰ n–11⁵⁰
11	8	0.0	.	–	•⁰ 15²⁵–16⁰³, = 0⁰⁰–8²⁰
12	7	0.0	.	–	•⁰ 6¹⁰ 7¹⁰ 12⁰⁵–¹⁰ •⁰ 16¹⁰–18⁴³, 22²⁵–24; = 7²⁰–9⁴⁰
13	8	.	.	–	•⁰ 0⁰⁰–1¹⁰
14	7	.	.	–	= 15³⁰–19¹⁵
15	5	.	.	–	= 1²⁵–5⁴⁵ ≡⁰–9³⁰ = –24
16	3	.	.	–	= 0⁰⁰–2⁴⁰ ≡¹–4³⁵ = –7¹⁰ ≡⁰–8⁴⁰ = –12³⁵ ≡⁰–14²⁰ = –24
17	5	.	.	–	= 0⁰⁰–24
18	5	.	.	–	= 0⁰⁰–24
19	5	.	.	–	= 0⁰⁰–20³⁰
20	6	.	.	–	= 8²⁰–24; ⌓¹ 22⁴⁵–24
21	5	.	.	–	= 0⁰⁰–13⁴⁰ ∞–15¹⁵ = –24; ⌓² n–11¹⁰
22	8	.	.	–	= 0⁰⁰–1²⁵
23	6	0.0	.	–	✳⁰ 6²³...⁴⁰, = 2²⁰–23³⁰
24	8	0.0	.	–	•⁰ 17⁴⁰–18²⁷ 22¹⁵–24; ⋙ 10⁵⁰–11²⁵ 22¹⁰–20
25	5	1.9	.	–	•⁰ 0⁰⁰...³⁰ 3²⁰...⁴⁰ 5⁴⁵–6³⁰ 7²⁰ •¹–11⁴² ••¹–12³⁰ ••⁰–15⁰⁵ •⁰–15⁴⁰, 18⁴⁰–24; ⋙ 8¹⁰...¹⁰
26	6	0.0	.	–	•⁰ 0⁰⁰–4²⁰ 4³⁵–5⁴⁰ 21³⁵–22¹⁰; ⋙ 3⁵⁰–4¹⁵, = 0⁰⁰–24
27	6	0.5	.	–	•⁰ 0²⁵–3⁵⁰ 6³⁵–7⁰⁷ •⁰ 10⁴⁵ 11¹⁰ •⁰ 22⁰⁵–23³⁰; ⋙ 0¹⁰–1²⁰ 4²⁰–6⁴⁰, = 0⁰⁰–24
28	6	1.9	.	–	•⁰ 0⁴⁵–1⁵⁰ •⁰ 4¹⁰–5³⁵ 11³⁰ 12²⁵ 19²⁷–21⁴⁰; ⋙ 10⁴⁰–21³⁰, = 0⁰⁰–23²⁰
29	8	0.7	.	–	•⁰ 0¹⁰–40 ▽¹–10⁵ •⁰ 6⁰⁰ 7²⁵ ▽¹ 7³⁴–42 ▽⁰–8⁰⁵ △ 9⁴⁵–50 ✳⁰ 11²⁵–12⁰², 13⁵¹–14⁴², 16⁰⁴–³⁵ 20⁴⁰–21¹⁰ ⋙ 7³⁴–42
30	7	0.4	.	–	▽⁰ 8³⁵–9²⁵, 11¹⁸–13¹⁰, 14¹⁰–16²⁵ [29.XI]: 12³⁰–14⁴², 16⁰¹–⁴⁰
31					
Σ	–	7.4	–	–	UWAGI.

Grudzień – Décembre

1	6	0.2	.	–	✳⁰ 16²⁵ 17¹⁰–24, ≡⁰ 7⁵⁰–9³⁰, ⌴⁰ n–13⁰⁰
2	5	1.2	pż.	–	✳⁰ 0⁰⁰–4³⁵ △ 10¹⁰–11¹⁵ 11³⁵–13¹⁰ 14²⁰–⁴⁰ ✳⁰ 19⁰⁵–20³⁰, = 0⁰⁰–7⁴⁰ ≡⁰–9²⁰ ≡¹–10¹⁰ ≡⁰–10³⁰ = –16⁴⁰ 17³²–24
3	4	1.6	.	–	✳⁰ 0⁰⁷–⁴⁰ •₂ 2¹⁰ 3⁴⁰ •⁰–4¹⁰ ✳⁰ 7⁵⁰–9²⁰ •⁰–9⁵² •⁰ 11⁵⁰–12²⁵ 13⁴⁵–20²⁰ 22¹⁵–24, = 0⁰⁰–1³⁰ ≡⁰–2²⁰ = –9⁴⁰ ≡¹ 12⁵⁰ = –24
4	6	4.9	.	–	•⁰ 0⁰⁰–4²⁰ •¹–5⁴⁰ ••⁰–6⁴⁵ •⁰–7³⁰ ••⁰–10²⁵ •⁰–11¹⁵ 12³⁰ •⁰ 13²⁰–14³⁵ 18³⁰–19²⁰ •⁰ 21⁴⁰–24, = 0⁰⁰–7⁴⁰ ≡⁰–8⁴⁵ = –24
5	6	0.0	.	–	•⁰ 0⁰⁰–5²⁵ •⁰–7⁰³, = 0⁰⁰–14³⁰
6	7	.	.	–	≡ 16²⁵–19²³ ≡⁰–24
7	7	0.0	.	–	= 0⁰⁰–11²⁰ 15³⁰–24; ⌓⁰ 0⁰⁰–10⁴⁰, 18⁰⁰–24
8	8	4.4	.	–	✳⁰ 0²⁰...⁵⁰ 3¹⁰–²⁵ •⁰ 8²⁵–³⁵ 9⁴⁰ 11¹⁰ •¹–12³⁰ •⁰–14¹⁰ 17²⁵ ▽ 19⁵⁰–20¹⁵; ⋙ 15⁴⁵–19⁵⁰ ⋙ –20¹⁵ ⋙ –20⁴⁰, = 0⁰⁰–7¹⁰ ⌴⁰ 0⁰⁰ 4⁴⁰
9	8	2.5	.	–	•⁰ 4⁴⁵–9⁴⁰ 11¹⁰–³⁰ 18¹⁰–²⁰; ⋙ 0⁰⁰–2⁴⁰ 7⁵⁰–8¹⁰ 10⁴⁰–16³⁰ (por. ponad 15 m/sek 10⁴⁰–14²⁵)
10	6	0.1	.	–	✳⁰⁻¹ 10²⁰–11²⁰ ✳ 14²⁰–³⁵ ▽⁰ 15²⁷–³² ▽₂ 15³⁷ ▽¹–15⁴⁰ ▽⁰–16⁰⁵; ⋙ 14⁵⁰–15²⁰, = 6¹⁰–18²³, ⌓¹ n–11²⁰, ⊖ 0¹⁰–6³⁰
11	6	.	pż.	–	= 7³⁰–24, ⊕ 11²⁰–15²⁰
12	5	.	.	–	= 0⁰⁰–24, ⌓⁰ 22⁴⁰–24, ⊖ 0¹⁵–2³⁰, 23⁵⁰–24
13	5	1.2	.	–	= 0⁰⁰–24, ⌓⁰ 0⁰⁰–6³⁰ ⊖ 0⁰⁰–1²⁰, 3³⁰–6²⁵
14	4	6.9	.	–	•⁰ 0⁰⁰–⁴⁵ •⁰ 5³⁵–7²⁰, 8¹⁰–15²⁵ ••⁰–16¹⁵ ✳⁰–18²⁵ ✳⁰–24, = 0⁰⁰–24
15	7	0.5	s	–	✳⁰ 0⁰⁰–11³⁵
16	6	.	s	–	= 7¹⁰–20³⁰
17	4	0.0	s	–	•¹ 22⁴⁰–24, = 7⁴⁰–24
18	5	.	s	–	•⁰ 0⁰⁰–4³⁵, = 0⁰⁰–24
19	5	0.0	s	–	✳⁰ 20⁴⁰–21¹⁵ △–22⁴⁰ •⁰–24, = 0⁰⁰–24
20	5	0.0	ɔ	–	•⁰ 0⁰⁰–⁴⁵ 1²⁰–7²⁰, = 0⁰⁰–6³⁰ ≡⁰–7³⁵ = –24
21	7	0.0	pż.	–	•⁰ 20²⁰–⁴⁰ 21³⁵ 22²⁵ •⁰ 23³⁸ 24, = 0⁰⁰–6³⁰
22	5	.	.	–	•⁰ 0⁰⁰...³⁰ •⁰ 2¹⁵ 3²⁰, = 6²⁰–24
23	7	.	.	–	= 0⁰⁰–10²⁰ 15³⁰–24; ⌓⁰ n–11⁵⁰ 19¹⁰–24
24	7	.	.	–	= 0⁰⁰–11⁴⁰, 15²⁰–24; ⌓⁰ 0⁰⁰–11⁰⁰
25	6	.	.	–	= 0⁰⁰–24; ⌓⁰ 0⁰⁰–24
26	6	.	.	–	= 0⁰⁰–24; ⌓⁰ 0⁰⁰–9¹⁰
27	6	.	.	–	= 0⁰⁰–24
28	6	1.0	.	–	✳⁰ 23⁵⁰–24, = 0⁰⁰–6⁴⁵ ≡⁰–10⁰⁰ = –18³⁰; ⌴⁰ n–a
29	6	0.4	1	–	✳⁰ 0⁰⁰–³⁵ ✳¹–2⁴⁰ ✳⁰–4¹⁰, = 8¹⁰–19³⁰
30	8	0.0	.	–	△⁰ 0¹⁸, 1¹⁰ •⁰ 1³⁵–2⁴⁰ 5¹⁵–6²⁰ 20⁰² 22⁴⁰–23³²; ⋙ 10⁴⁰–12¹⁰, 20¹⁰–⁴⁰, 22¹⁵–23³⁰
31	8	2.8	.	–	•⁰ 0⁴², 1¹⁵ ✳⁰ 17⁵⁰–19¹⁰, 23¹⁵–24, = 17⁴⁰–24
Σ	–	27.7	–	–	UWAGI.

Jelenia Góra — φ = 50°54' — λ = 15°48' — Styczeń – Janvier 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	73.2	72.5	70.6	72.1	-6.1	-1.6	-3.6	-4.7	-1.3	-12.3	97	84	97	93	0.1	0.9	0.1	0.4	10	9	10	C 0	C 0	NW 2
2	68.9	71.1	75.8	71.9	-8.3	-4.0	-5.4	-4.8	-1.8	-9.8	95	99	95	96	0.2	0.1	0.3	0.2	9	9	10	C 0	C 0	C 0
3	79.2	79.3	79.9	79.5	-2.4	2.4	-3.3	-1.6	3.3	-5.7	100	89	92	94	0.0	0.8	0.4	0.4	10	7 ⊙	3	C 0	C 0	SE 1
4	80.9	82.1	82.1	81.7	-0.9	2.9	-2.3	-0.8	3.7	-5.2	93	79	95	89	0.4	1.6	0.3	0.8	7	8	10	C 0	C 0	C 0
5	82.2	79.7	79.3	80.4	-0.2	2.3	4.7	2.9	5.3	-2.6	96	95	95	95	0.2	0.4	0.4	0.3	9	10 ●	10	SW 2	C 0	SW 2
6	75.1	73.7	77.7	75.5	9.5	9.2	4.7	7.0	10.1	4.4	75	84	84	81	3.0	1.8	1.3	2.0	10	10 ●	3	SW 12	W 3	WNW 10
7	83.5	87.5	90.4	87.1	2.7	3.6	3.3	3.3	5.2	0.6	89	85	86	87	0.8	1.2	1.0	1.0	10 ●	9	10	WNW 14	WNW 12	W 10
8	89.7	88.6	87.8	88.7	2.6	5.8	5.8	5.0	6.5	1.5	84	77	83	81	1.2	2.1	1.5	1.6	9	10	10	SW 4	WNW 4	W 8
9	84.5	81.6	79.2	81.8	6.2	7.9	0.3	3.7	9.6	-0.4	85	80	98	88	1.5	2.0	0.1	1.2	10	4 ⊙	1	SW 4	NW 3	E 2
10	75.2	75.2	76.2	75.5	3.3	1.1	1.0	2.1	6.2	-0.8	68	98	94	87	2.9	0.1	0.4	1.1	9	10 ⁂	10	W 3	W 4	W 8
11	77.2	80.0	82.9	80.0	0.1	0.4	-0.1	0.1	1.9	-0.6	86	85	82	84	0.9	1.0	1.1	1.0	9	9 ✳	9	NW 7	W 5	W 4
12	77.6	70.8	63.3	70.6	0.0	1.1	1.1	0.8	1.7	-2.3	84	79	77	80	1.0	1.4	1.5	1.3	10 ✳	10	10	W 6	WSW 8	W 4
13	62.3	63.8	67.3	64.5	0.8	2.9	-3.3	-0.8	3.2	-4.0	82	59	97	79	1.2	3.1	0.1	1.5	10	8 ⊙	2	WSW 2	C 0	C 0
14	73.1	77.2	80.9	77.1	-4.7	-2.2	-3.7	-4.6	-1.6	-6.9	96	94	97	96	0.2	0.3	0.1	0.2	9	10 ✳	10	C 0	NE 2	NE 3
15	81.4	82.2	83.3	82.3	-6.2	-7.0	-7.9	-7.2	-5.1	-8.3	92	91	96	93	0.3	0.3	0.1	0.2	10 ✳	10 ✳	10 ✳	ENE 4	NE 4	C 0
16	86.8	89.0	91.0	88.9	-8.8	-9.2	-21.0	-15.0	-6.5	-22.3	95	88	82	88	0.2	0.4	0.2	0.3	10 ✳	7 ✳	0	NW 1	N 1	C 0
17	90.9	90.8	91.0	90.9	-24.2	-9.3	-7.8	-12.3	-5.2	-23.2	79	82	93	85	0.2	0.5	0.2	0.3	4	9 ⊙	9	C 0	C 0	C 0
18	90.0	89.6	88.8	89.5	-16.4	-2.6	-13.2	-11.4	-1.4	-17.5	95	61	92	83	0.1	2.0	0.2	0.8	1	3	1	C 0	C 0	C 0
19	88.2	88.6	89.7	88.8	-6.0	-1.5	-2.6	-3.2	-0.9	-16.6	97	90	91	93	0.1	0.5	0.5	0.4	10	10	10	C 0	C 0	WNW 1
20	89.3	87.9	85.4	87.5	-4.3	-3.4	-12.2	-8.0	-1.7	-13.9	91	92	95	92	0.4	0.4	0.2	0.3	10	8	0	SW 1	C 0	C 0
21	83.4	83.2	84.2	83.6	-14.4	0.1	-10.0	-8.6	1.1	-16.3	91	62	87	80	0.2	2.4	0.4	1.0	4	1 ⊙	0	SSE 1	C 0	C 0
22	83.1	80.8	78.8	80.9	-15.9	-2.9	-11.3	-10.4	-2.3	-16.2	91	68	86	82	0.2	1.5	0.4	0.7	1	1 ⊙	0	C 0	SE 4	C 0
23	79.2	76.9	72.6	76.2	-12.6	-1.0	1.8	-2.5	3.5	-15.7	92	63	57	71	0.2	2.1	3.0	1.8	0	0	0	C 0	C 0	SE 10
24	68.4	66.8	67.7	67.6	2.6	3.9	-1.2	1.0	5.1	-1.4	48	74	86	69	3.9	2.2	0.8	2.3	9	8	10	SE 4	NE 1	C 0
25	68.7	69.7	73.6	70.7	-2.4	1.5	-0.4	-0.4	3.1	-3.4	89	78	90	86	0.5	1.5	0.6	0.9	10	10	6	C 0	C 0	C 0
26	78.3	78.3	75.9	77.5	-4.1	4.0	0.7	0.3	4.8	-4.9	94	64	71	76	0.3	2.9	1.8	1.7	3	1 ⊙	3	C 0	SW 3	C 0
27	75.3	77.8	81.0	78.0	4.4	6.7	2.2	3.9	7.2	0.7	84	75	86	82	1.4	2.4	1.1	1.6	10 ●	9	0	WSW 8	W 8	W 2
28	80.5	84.3	90.7	85.2	0.3	0.1	-0.2	0.0	3.6	-0.8	92	96	90	93	0.5	0.3	0.6	0.5	9 ✳	10 ✳	7	W 8	NW 3	C 0
29	90.8	88.9	87.2	88.9	-12.2	1.3	0.0	-2.7	2.8	-13.1	89	72	92	84	0.3	1.9	0.5	0.9	3	9 ⊙	8	C 0	C 0	C 0
30	84.3	82.0	81.5	82.6	-8.9	2.8	2.8	-0.1	4.4	-9.8	95	79	89	88	0.2	1.6	0.8	0.9	4	8	10 ●	E 2	SE 2	W 3
31	82.1	81.3	79.8	81.1	2.4	5.4	1.6	2.8	5.8	1.2	93	65	98	85	0.6	3.2	0.2	1.3	10	9	10	WNW 2	W 1	C 0
M	80.1	80.0	80.5	80.2	-3.9	0.7	-2.6	-2.1	2.3	-7.3	88	80	89	86	0.7	1.4	0.6	0.9	7.7	7.6	6.2	2.7	2.3	2.3

Luty – Février

1	76.1	76.6	78.0	76.9	5.4	4.6	3.4	4.2	5.9	0.8	77	100	100	92	2.1	0.0	0.0	0.7	10 ●	10 ●	10	SW 4	C 0	C 0
2	82.1	84.1	84.6	83.6	9.9	6.8	5.3	6.8	10.8	2.9	81	99	98	93	2.4	0.2	0.1	0.9	9	10	10	SW 1	C 0	C 0
3	82.6	82.5	83.3	82.8	2.2	12.5	5.4	6.4	13.2	1.5	100	76	97	91	0.0	3.6	0.3	1.3	5	8 ⊙	10	C 0	C 0	E 3
4	81.8	83.0	83.1	82.6	1.0	7.6	-0.3	1.9	8.8	-1.2	100	76	96	91	0.0	2.5	0.3	0.9	10 ≡	9	0	C 0	E 1	E 1
5	81.6	80.2	78.9	80.2	-3.4	13.1	1.4	3.1	13.8	-4.1	99	63	89	84	0.0	5.6	0.8	2.1	0	6	0	C 0	C 0	C 0
6	74.4	72.5	74.6	73.8	1.8	7.9	2.7	3.8	9.4	0.1	89	66	98	84	0.8	3.6	0.1	1.5	3	2	10 ●	WSW 1	E 2	C 0
7	77.4	78.7	78.0	78.0	4.4	7.5	0.0	3.0	8.1	-0.4	93	70	94	86	0.6	3.1	0.4	1.4	10 ●	7	6	W 3	W 8	C 0
8	72.2	68.9	64.9	68.7	5.6	8.8	7.7	7.4	10.2	-1.9	64	65	72	67	3.3	3.9	2.9	3.4	6	9	10	SW 10	WSW 7	WSW 8
9	63.9	63.9	67.6	65.1	6.6	6.1	5.7	6.0	8.3	4.9	81	86	77	81	1.8	1.3	2.1	1.7	9	10 ●	4	SW 7	WSW 7	W 7
10	67.4	66.9	66.7	67.0	-0.1	6.6	3.8	3.5	7.3	-0.5	94	74	92	87	0.4	2.5	0.7	1.2	7	10	9 ●	C 0	SW 6	S 2
11	69.2	72.9	74.7	72.3	4.1	4.2	3.2	3.7	6.2	2.7	88	88	76	84	1.0	0.9	1.9	1.3	9	10 ●	9	W 8	W 6	W 8
12	70.3	66.2	63.5	65.7	-0.1	5.4	5.4	4.0	7.1	-1.9	94	63	71	77	0.4	3.2	2.7	2.1	10	9	10	C 0	SE 7	SSE 1
13	61.2	56.5	47.9	55.2	3.7	7.2	6.7	6.1	7.7	0.6	77	60	69	69	1.9	4.1	3.0	3.0	6	8	7 ●	S 6	SSE 5	SW 10
14	47.6	47.0	49.7	48.1	5.9	8.2	5.0	6.0	9.1	4.9	80	67	72	73	1.9	3.6	2.4	2.6	6	9	4	SE 4	SW 9	SW 8
15	49.6	44.1	44.3	46.0	3.0	6.8	5.8	5.4	8.2	1.7	76	67	76	73	1.9	3.3	2.2	2.5	3	10	9	S 3	SE 8	W 3
16	53.1	55.5	61.0	56.5	1.4	4.9	-0.4	1.4	6.3	-1.1	81	64	100	82	1.3	3.2	0.0	1.5	8	6	9	SW 4	SW 5	SW 1
17	64.2	64.0	66.5	64.9	-2.3	3.9	2.1	1.4	5.1	-3.1	91	64	73	76	0.3	2.9	1.9	1.8	10	10	0	SE 1	S 2	SW 6
18	63.0	58.4	55.1	58.8	-0.3	5.3	2.8	2.7	6.3	-3.6	80	74	100	85	1.2	2.3	0.0	1.2	6	9	10 ●	C 0	SE 4	C 0
19	65.1	69.4	71.9	68.8	0.4	2.2	0.0	0.6	3.0	-1.7	88	80	94	87	0.8	1.3	0.4	0.9	10	7	3	WNW 9	W 4	C 0
20	71.2	69.2	66.0	68.8	-0.2	6.1	3.7	3.3	7.0	-2.0	80	56	80	72	1.2	4.2	1.6	2.3	4	8	2	SSW 2	SE 4	S 3
21	66.6	69.4	74.9	70.3	-0.3	4.4	0.9	1.4	5.6	-1.0	96	74	85	85	0.3	2.2	1.0	1.2	10	10 ●	10	C 0	W 5	WNW 8
22	76.7	76.1	73.7	75.5	-0.1	3.0	-3.2	-0.9	4.7	-3.9	90	76	88	85	0.7	1.9	0.6	1.1	10	5	0	W 4	W 3	C 0
23	73.8	73.7	72.2	73.2	-6.8	1.8	-3.4	-3.0	2.7	-7.7	91	78	94	88	0.3	1.6	0.3	0.7	3	8	0	C 0	C 0	C 0
24	62.4	58.8	61.7	61.0	-0.2	3.2	-0.1	0.7	3.6	-3.8	72	74	96	81	1.7	2.0	0.3	1.3	10	10	10 ●	SE 4	E 1	C 0
25	66.2	63.6	63.3	64.4	-1.6	1.9	-1.4	-0.6	2.2	-2.8	80	71	99	83	1.1	2.0	0.1	1.1	6	10	10 ✳	SE 1	SE 1	E 4
26	73.6	75.3	77.3	75.3	-3.3	0.1	-3.0	-3.4	2.4	-6.2	94	74	90	87	0.1	1.6	0.4	0.7	10	1 ⊙	4	C 0	E 2	C 0
27	78.7	80.8	83.9	81.1	-1.2	1.6	0.6	0.4	2.3	-6.8	91	83	100	92	0.3	1.1	0.0	0.5	10	10	10 ⁂	C 0	C 0	WNW 3
28	87.7	89.9	92.3	90.0	-0.4	-0.2	-2.3	-1.3	1.2	-2.6	98	86	89	91	0.1	0.8	0.6	0.5	10 ✳	10 ✳	8	WNW 2	NW 4	N 3
29																								
30																								
31																								
M	70.0	69.6	70.0	69.9	1.2	5.4	2.0	2.6	6.7	-1.4	87	74	88	83	1.0	2.5	1.0	1.5	7.5	8.2	6.6	2.6	3.6	2.9

Jelenia Góra $H_s = 342$ m $H_b = 343{,}0$ m $h_w = 15$ m **Styczeń – Janvier 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIE GU n	USŁONECZNIENIE	P O G O D A
1	5	.	12	-	= 6^{20}–20^{10} ≡ –21^{50}
2	5	.	12	-	≡ 0^{00}–5^{35} = –24 ⌴^{1} 19^{10}–24
3	6	0.4	12	-	* 8^{40}–10^{25}, = 0^{00}–15^{20} 22^{20}–24, ⌴^{1} 0^{00}–9^{10}
4	8	0.1	12	-	●^{0} 22^{40} 24, = 0^{00}–6^{10}
5	8	1.2	10	-	●^{0} 0^{00} 5^{10} 9^{40} 12^{15}–16^{20} 19^{40}
6	8	7.9	4	-	●^{0} 8^{41}–14^{35}, 15^{26}–17^{30}, ⩓ 3^{20}–9^{10}
7	7	0.3	.	-	⛆ 6$^{05-35}$, 6^{50}–12^{30}, ⩓ 23^{0}–24
8	8	.	.	-	por wiatru ponad 10 m/sek 0^{00}–4^{25}, 19^{30}–24
9	8	.	.	-	⩓ 0$^{00-30}$ = 18^{20}–24
10	6	2.3	.	-	●^{0} 8^{40} 9^{10}–11^{20} ⁑^{0}–15^{20} ●^{0}–16^{40} ⁑ 20$^{20-45}$ = 0^{00}–7^{15}
11	7	0.3	0	-	⁑ 0^{35}–1^{35} ⛆ 3^{40}–5^{40} 6$^{20-40}$ ⁑ 12^{55}–13^{35} ⛆ 15^{50}–16^{10} 16$^{20-40}$, = 16^{40}–19^{30}
12	7	0.1	1	-	*^{0} 6^{36} 9^{30} 14^{15}–15^{50}, 21^{45}–23^{35}, ⩓ 2^{30}–6^{20}, = 23^{35}–24
13	8	.	0	-	*^{0} 4^{15} 6^{40}, = 0^{00}–6^{40}
14	5	1.3	.	-	*^{0} 7^{35} 8^{20}–10^{45} *^{1}–11^{50} *^{0}–16^{10} △^{1}–18^{35}, ⌴^{1} n
15	5	2.9	2	-	*^{0} 0^{20}.. 8^{20} *^{1}–14^{30} *^{0}–24
16	6	0.2	10	-	*^{0} 0^{00}–12^{15} 15^{25}, = 16^{15}–18^{30}, V^{0} 20^{20}–24
17	7	.	7	-	= 19^{30}–24, V^{0} 0^{00}–10^{40}
18	7	.	5	-	= 0$^{00-20}$, 3^{35}–11^{30}, 13^{45}–24
19	4	.	4	-	= 0^{00}–24
20	6	.	4	-	= 0^{00}–24, ⌴^{0} 20^{00}–24
21	8	.	3	-	= 0^{00}–7^{20} 18^{20}–24, ⌴^{0} 0^{00}–10^{15}, ⌓^{2} 23$^{05-45}$
22	7	.	3	-	= 20^{20}–24
23	8	.	3	-	= 0^{00}–6^{30}
24	8	0.0	3	-	*^{0} 16$^{20..45}$, 19^{35}–20^{45}, 22^{30}–23^{40}, = 15^{30}–18^{40}
25	6	.	2	-	= 7^{20}–24
26	7	0.2	2	-	= 0^{00}–11^{20}
27	8	2.0	.	-	●^{0} 2^{40} 8^{20}, 9^{40}–10^{10} ⛆ 15$^{10-25}$, 16$^{15-35}$
28	6	4.7	2	-	⁑ 4^{16}–7^{20}, 8$^{05-15}$ ⛆–8^{45} ⁑ 9^{07}–15^{40}
29	8	.	10	-	
30	7	0.8	7	-	●^{0} 15^{45}.. 17^{35}–24, ≡ 6^{15}–8^{20}
31	7	0.2	pż.	-	
Σ	–	29.5	–	-	UWAGI

Luty – Février

1	7	5.4	.	-	●^{0} 6^{38} 7^{15}–20^{15} = 15^{30}–23^{10}
2	8	0.4	.	-	●^{0} 9^{10}–10^{40}, 11^{40}.. 12^{50}
3	8	0.0	.	-	= 0^{00}–5^{40} ≡^{2}–6^{30} ≡–7^{10} = 16^{20}–24
4	7	.	.	-	= 0^{00}–2^{45} ≡^{1}–7^{50} ≡^{1}–8^{42} = –9^{20} 21^{45}–24
5	6	.	.	-	= 0^{00}–6^{40} ≡^{1}–8^{30} = –14^{40}, ⌴^{2} 1^{20}–8^{00}
6	8	2.2	.	-	●^{0} 17^{50} 19^{30}–24 ⌴^{1} 0^{00}–7^{20}
7	7	0.0	.	-	●^{0} 0^{00}.. 5^{20} ●^{1}–7^{15} ●^{0}.. 8^{35} = 8^{35}–10^{20}, 19^{15}–24, ⌔^{0} 19^{30}–23^{15}
8	9	0.2	.	-	●^{0} 14^{46}–17^{10} 17^{40}–18^{10} ●^{0} 20^{45}–24, = 0^{00}–6^{35}
9	7	2.0	.	-	●^{0} 0^{00} 6^{30} 10^{50}–11^{40}, 12^{30}–13^{40} ⛆ 14^{35}–15^{30}
10	8	1.9	.	-	●^{0} 19^{50} 21^{40}
11	7	0.8	.	-	⛆ 0^{48}–1^{28} 3^{40}–4^{10}, 4^{35}–5^{15}, 5$^{20-40}$, 9^{50}–10^{20} ●^{0} 12^{45} 13^{35}–16^{40}, = 17^{15}–21^{25}
12	8	.	.	-	= 0^{00}–7^{20} ⌴^{1} n–8^{15}
13	8	0.9	.	-	●^{0} 17^{45}–18^{20} ⛆ 18^{30}–23^{30}, ⩓ 15^{10}–16^{30} ⩓–18^{40} ⩓–24, ⌔^{1} 3^{35}–4^{20}
14	8	0.1	.	-	⛆ 15$^{21-42}$ ⌒^{2} 15$^{26-39}$ (nadwaina)
15	8	1.4	.	-	⛆ 15^{55}–16^{10} 17^{50}–18^{35} ●^{0} 23^{20} 24
16	7	1.4	.	-	●^{0} 0^{00} 1^{00}–4^{20} 5^{45}, 7^{45} 8^{15}, 9^{45} 10^{20} ⛆–10^{45} ⛆ 14^{50}–15^{25}, 15^{30}–17^{25}
17	7	.	.	-	⌴^{1} 4^{20}–8^{10}
18	7	11.4	.	-	●^{0} 17^{30}–21^{45} ⁑^{2}–22^{10} *^{1}–23^{25} *^{0}–24, = 8^{15}–9^{30}, ⌔ 3^{40}–5^{20}
19	6	.	3	-	*^{0} 0^{00}–1^{30} ⛆^{1}–3^{48} *^{0}–5^{05}, ⩓ 2^{45}–4^{30} ⩓–6^{20} ⩓–8^{10}, = 5^{05}–6^{30}, 7^{40}–14^{20}, 17^{40}–24
20	9	.	pż.	-	= 0^{00}–4^{15}
21	8	0.0	.	-	●^{0} 12^{38} 14^{10} ⁑^{0}–14^{50} ●^{0}.. 15^{26} *^{0} 18^{35} 19^{15}, = 15^{40}–17^{20}, ⌴^{0} 5^{10}–7^{20}
22	7	.	.	-	*^{0} 5^{10} 6^{05} 6$^{15-45}$ = 8^{15}–9^{30}
23	8	0.0	.	-	⛆ 13^{48}–14^{10}, = 15^{30}–24, ⌴^{1} 1^{00}– a
24	8	0.3	.	-	*^{0} 14^{38} 17^{10}–20^{15} ●^{1} 20^{20}–22^{20} 24, = 0^{00}–5^{15} ⌴^{0} n– a
25	7	4.3	1	-	●^{0} 0$^{00..10}$ *^{0} 14^{40} 15^{10}–19^{30} *^{1}–24 ●^{0} 0^{10}–4^{15}
26	7	.	10	-	*^{1} 0$^{00-40}$ = 1^{30}–9^{40}
27	6	5.6	8	-	*^{1} 7^{53}–9^{50} *^{0}–10^{35} ●^{0} 15^{45}–16^{50} ●●^{0}–17^{45} ⁑^{1}–18^{35} ⁑^{0}–22^{40} *^{1}–24, = 10^{35}–15^{45} ≡^{0} 16^{50}–19^{45}
28	6	3.0	10	-	*^{1} 0^{00}–1^{00} *^{0}–9^{30} 11^{16}, 12^{24}–16^{40} ⁑–17^{47}, 18^{35}–19^{10} ⛆ 21^{06}–22^{10}
29					
30					
31					
Σ	–	41.3	–	-	UWAGI

Jelenia Góra — φ = 50°54' — λ = 15°48' — Marzec – Mars 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	94.6	94.8	93.9	94.4	-3.9	-1.0	-4.6	-3.5	-0.3	-5.1	85	75	91	84	0.7	1.5	0.4	0.9	10 ✳	7	7	N 1	N 1	C 0
2	92.2	90.5	88.0	90.2	-8.6	-0.9	-8.4	-6.6	0.4	-10.7	92	67	95	85	0.3	1.9	0.2	0.7	8	6 ⊙	0	C 0	WNW 2	C 0
3	84.2	82.1	79.4	81.9	-12.4	1.4	-5.6	-5.6	3.2	-13.2	93	58	90	80	0.2	2.9	0.4	1.2	4	4	0	C 0	W 1	C 0
4	74.8	72.3	70.9	72.7	-9.2	6.9	-0.4	-0.8	8.2	-10.3	95	44	88	76	0.2	5.6	0.7	2.2	5	10	6	C 0	C 0	C 0
5	73.0	73.6	73.9	73.5	0.1	2.2	-3.8	-1.5	3.5	-4.3	98	66	87	84	0.2	2.3	0.6	1.1	10	10	0	NW 2	NW 1	C 0
6	72.7	70.4	69.2	70.8	-7.6	6.1	-0.9	-0.8	7.8	-8.9	87	64	96	82	0.4	3.3	0.2	1.3	2	0 ⊙	0	SE 1	NE 4	C 0
7	68.9	68.8	69.6	69.1	-4.2	9.5	1.8	2.2	9.7	-4.7	96	53	71	73	0.2	5.6	2.1	2.6	1	3	10	C 0	SE 2	C 0
8	71.1	72.4	73.0	72.8	0.5	5.6	1.4	1.7	4.2	-0.6	98	93	74	88	0.1	0.5	1.8	0.8	10 ●	10 ●	10	C 0	E 4	E 6
9	79.1	82.0	86.5	82.5	-4.3	1.5	-0.8	-1.1	2.8	-5.9	86	63	67	72	0.6	2.5	2.0	1.7	3	0 ⊙	0	E 7	E 7	E 7
10	88.1	88.7	89.1	88.6	-3.6	4.1	0.0	0.1	5.0	-5.4	78	45	74	66	1.0	4.5	1.6	2.4	0	2 ⊙	0	E 1	E 6	E 8
11	89.8	88.6	87.5	88.6	-5.9	13.7	-0.4	1.8	14.3	-6.9	94	19	64	59	0.2	12.8	2.1	5.0	0 ⊙	0 ⊙	2	E 1	SE 4	C 0
12	84.8	81.9	80.4	82.4	-4.0	13.6	-0.4	2.2	14.9	-5.2	94	30	90	71	0.3	11.0	0.6	4.0	8	5	2	SE 2	NW 2	C 0
13	79.9	79.8	77.7	79.1	-3.8	14.7	1.6	3.5	16.3	-5.6	94	32	96	74	0.3	11.3	0.3	4.0	5	6	3	C 0	C 0	C 0
14	74.5	73.8	73.0	73.8	0.2	11.2	10.1	7.9	13.7	-1.9	92	77	76	82	0.5	3.1	3.0	2.2	4	8 ⊙	10	C 0	W 10	W 8
15	74.5	73.2	68.8	72.2	7.0	8.1	9.7	8.6	10.5	6.2	82	75	74	77	1.7	2.7	3.1	2.5	10	10	10	W 10	W 8	W 12
16	65.3	71.1	73.7	70.0	7.3	-0.9	-0.4	1.4	10.4	-1.3	93	93	92	93	0.7	0.4	0.5	0.5	10 ●	10 ✳	10	NW 10	N 3	C 0
17	71.1	68.9	65.2	67.7	0.2	6.8	8.5	6.0	9.4	-1.2	96	85	80	87	0.3	1.4	2.3	1.3	10 ●	9	10 ●	C 0	W 6	SW 6
18	68.7	59.5	64.9	61.0	10.3	7.6	7.6	8.3	11.3	7.1	79	93	76	83	2.7	0.7	2.5	2.0	10	10 ●	6 ●	W 7	WNW 8	NW 14
19	69.2	69.1	69.0	69.1	6.4	9.4	8.7	8.3	9.9	5.0	70	64	89	74	2.8	4.3	1.2	2.8	9	10	10 ●	SW 1	W 6	W 3
20	70.7	68.3	66.6	68.5	7.5	13.5	9.0	9.8	15.5	6.7	94	53	81	76	0.6	7.3	2.2	3.4	10	9	3	C 0	SW 5	S 1
21	71.4	72.3	73.6	72.4	7.9	11.9	6.0	8.0	13.8	5.4	74	44	80	66	2.8	7.8	1.9	4.2	3	1 ⊙	9	NW 5	W 8	C 0
22	76.0	76.9	78.0	77.0	0.1	9.4	2.1	3.4	11.4	-0.7	96	55	95	82	0.3	5.3	0.4	2.0	6 ⊙	7 ⊙	0	SE 2	WNW 3	C 0
23	76.6	74.4	76.0	75.7	-1.8	11.7	6.9	5.9	13.0	-0.3	96	58	80	78	0.2	5.8	2.0	2.7	4	9	0	C 0	ENE 7	C 0
24	76.6	75.6	77.3	76.5	3.4	4.9	4.2	4.2	7.3	2.9	83	81	84	83	1.3	1.7	1.3	1.4	10	10	10	E 9	E 14	E 10
25	77.9	78.3	79.7	78.7	1.9	14.4	10.7	9.4	15.4	0.7	96	58	75	76	0.3	6.8	3.2	3.4	9	4 ⊙	4	≋ 0	SE 2	E 8
26	77.7	78.0	78.5	78.1	7.9	11.1	9.2	9.4	12.8	7.3	60	47	41	49	4.2	7.0	6.8	6.0	8	7	1	SSE 10	SSE 7	SSE 12
27	79.0	80.0	78.9	79.3	6.2	13.4	8.7	9.2	14.2	5.7	47	39	42	43	5.0	9.4	6.5	7.0	7	8	3	ESE 10	SE 5	SE 9
28	76.8	75.4	73.4	75.2	4.8	10.0	5.7	6.8	10.3	4.1	50	67	88	68	4.3	4.1	1.2	3.2	7	9	9 ●	SE 7	NE 2	SE 2
29	72.9	73.3	74.6	73.6	5.4	5.3	0.2	2.8	6.6	0.1	97	92	98	96	0.3	0.7	0.1	0.4	10 ●	10	10 ✳	W 1	WNW 1	C 0
30	76.5	77.4	78.4	77.4	0.6	2.9	2.1	1.9	3.5	-0.2	98	96	96	97	0.1	0.2	0.3	0.2	10 ●	10 ●	10	C 0	NW 1	C 0
31	78.5	80.3	81.9	80.2	1.1	7.9	2.8	3.6	9.4	0.8	100	66	93	86	0.0	3.6	0.6	1.4	2	3 ⊙	0	C 0	ESE 8	C 0
M	76.7	76.5	76.5	76.6	0.3	7.5	2.9	3.4	9.4	-1.4	87	63	81	77	1.1	4.5	1.7	2.4	6.6	6.7	5.0	2.8	4.5	3.4

Kwiecień – Avril

1	80.9	78.5	77.9	79.1	3.5	12.2	9.3	8.6	13.3	1.2	98	55	64	72	0.1	6.4	4.3	3.6	10 ●	8	10 ●	C 0	NE 2	S 10
2	76.4	77.0	79.4	77.6	6.9	11.2	6.9	8.0	12.0	3.1	70	67	90	76	3.0	4.4	1.0	2.8	4	10	10 ●	E 3	SE 4	C 0
3	81.8	84.1	86.7	84.2	9.0	13.1	6.8	8.9	15.1	5.4	81	64	95	79	2.2	5.4	0.8	2.8	10	9	0	E 3	C 0	C 0
4	88.8	86.6	88.7	88.7	0.8	17.6	7.3	8.2	18.7	-0.2	100	32	88	73	0.0	13.7	1.2	5.0	0 ≡	0	0	C 0	NE 3	C 0
5	87.3	84.2	79.0	83.5	0.9	16.4	6.6	7.6	17.6	-1.1	98	29	82	70	0.1	13.2	1.7	5.0	0 ≡	0 ⊙	0	C 0	NE 4	ESE 1
6	73.5	70.3	70.3	71.4	2.0	17.9	9.5	9.7	19.5	-0.8	91	24	70	62	0.7	15.6	3.6	6.6	0 ⊙	0 ⊙	0	C 0	SW 2	C 0
7	71.3	71.3	75.3	72.6	5.0	5.6	0.2	2.8	10.1	0.1	87	86	96	90	1.1	1.1	0.3	0.8	10	10 ●	10 ✳	C 0	NW 6	WNW 2
8	79.8	79.3	77.8	79.0	-2.2	-0.1	-1.8	-1.3	3.2	-3.8	89	78	96	88	0.6	1.4	0.2	0.7	10	8	0	N 2	W 3	C 0
9	75.0	72.9	71.3	73.1	-2.8	8.3	4.6	3.7	10.0	-3.1	95	48	84	76	0.2	5.7	1.4	2.4	3 ⊙	5 ⊙	8	C 0	W 2	C 0
10	67.8	63.7	58.3	63.3	0.0	11.5	3.2	4.5	13.8	-2.2	98	45	91	78	0.1	7.5	0.7	2.8	3	4	0	C 0	WNW 1	SE 2
11	56.6	57.6	62.6	58.9	3.6	5.7	0.7	2.7	7.1	0.1	88	51	92	77	0.9	4.6	0.5	2.0	10	8	3	W 3	WSW 4	C 0
12	67.4	69.3	71.8	69.5	-0.5	3.2	-2.0	-0.3	3.6	-3.5	96	59	94	83	0.3	3.1	0.4	1.3	10 ✳	9	3	W 1	NW 2	C 0
13	72.2	74.4	76.8	74.5	-3.2	1.2	-1.4	-1.2	4.9	-6.5	92	74	78	81	0.3	1.8	1.2	1.1	9	10	3	C 0	NW 5	C 0
14	78.1	77.7	78.0	77.9	-2.0	3.3	-2.3	-0.8	5.8	-5.1	94	44	85	74	0.4	4.3	0.8	1.8	0	8	0	C 0	W 1	C 0
15	79.7	80.8	82.9	81.1	-2.3	4.0	-1.5	-0.3	5.2	-5.5	89	66	93	83	0.6	2.8	0.4	1.3	10	8 ⊙	3	W 1	NW 1	C 0
16	83.3	82.6	81.4	82.4	-2.2	7.1	7.9	5.2	11.8	-5.6	91	76	71	79	0.5	2.5	3.1	2.0	5	10	3	C 0	NW 2	W 1
17	80.8	80.4	81.0	80.7	6.1	8.7	5.5	6.4	9.5	2.6	95	82	97	91	0.4	1.9	0.3	0.9	10 ●	9	4	W 3	W 4	C 0
18	79.5	78.1	77.0	78.2	2.9	8.1	2.2	3.8	9.9	1.0	98	62	86	82	0.1	4.1	1.1	1.8	9	5 ⊙	0	NW 1	NW 2	C 0
19	73.9	71.7	74.0	73.2	-0.7	8.7	8.0	6.0	9.2	-3.2	97	81	93	90	0.2	2.1	0.7	1.0	9	10 ●	10 ●	C 0	C 0	WNW 3
20	80.6	82.5	84.1	82.4	3.8	8.2	2.6	4.3	10.0	2.6	92	59	96	82	0.7	4.4	0.3	1.8	9	6	4	NW 4	NW 3	C 0
21	85.8	85.6	87.7	86.4	0.6	10.7	4.5	5.1	11.1	-3.0	94	49	97	80	0.4	6.6	0.3	2.4	5 ⊙	6 ⊙	10 ●	C 0	NE 2	C 0
22	88.9	88.7	88.7	88.8	0.6	8.9	2.8	3.8	11.7	-1.9	100	54	89	81	0.0	5.2	0.8	2.0	3	7	0	C 0	NE 3	C 0
23	89.0	87.6	87.9	88.2	0.4	9.3	7.6	6.2	11.2	-3.4	92	72	82	82	0.3	3.2	1.9	1.9	0	6 ⊙	1	C 0	NE 3	E 3
24	87.3	87.6	86.0	87.0	2.0	8.4	9.2	7.2	11.3	-0.9	100	90	80	90	0.0	1.0	2.3	1.1	10	10	10 ●	C 0	WNW 2	W 2
25	83.0	82.4	81.7	82.4	8.7	6.8	6.1	6.4	9.3	5.1	99	91	98	96	0.1	0.9	0.1	0.4	10 ●	10 ●	10 ●	NW 3	NW 2	C 0
26	80.8	80.9	80.3	80.7	6.3	11.5	8.3	8.6	13.2	5.7	98	82	96	92	0.1	2.5	0.3	1.0	10 ●	10	10	C 0	C 0	C 0
27	77.9	74.9	73.2	75.3	9.3	16.9	12.7	12.9	18.4	6.6	99	65	85	83	0.1	6.6	2.3	3.0	7	6	0	C 0	ENE 5	E 1
28	70.9	69.0	69.6	69.8	12.0	21.8	11.7	14.3	22.2	4.4	81	35	82	66	2.7	17.1	2.3	7.4	4 ⊙	3	3	NE 2	NW 2	SE 1
29	72.4	72.0	71.7	72.0	10.2	20.7	14.1	14.8	22.9	5.7	97	47	82	75	0.3	13.0	2.9	5.4	0 ⊙	3 ⊙	6	C 0	WNW 2	C 0
30	68.6	67.3	74.3	70.2	10.9	19.3	8.9	12.0	22.0	5.4	95	55	90	80	0.7	10.2	1.1	4.0	4	8	10	C 0	WNW 2	NW 3
31																								
M	78.0	77.4	77.9	77.8	2.9	10.2	5.3	5.9	12.1	-0.1	93	61	87	80	0.6	5.7	1.3	2.5	6.1	6.9	4.4	0.9	2.3	1.0

Jelenia Góra $H_s = 342$ m $H_b = 343{,}0$ m $h_w = 15$ m **Marzec – Mars 1957**

DNI	WILGOTNOŚĆ WZGLĘDNA	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.4	12	–	✱ 1⁴⁰–2⁴⁵ 4¹⁰–2⁶ 5⁰⁸–²⁰ ✱–6¹⁰ ✱ 6³⁹ 11⁴⁸ 14⁵³–15²⁵
2	8	.	9	–	≡° 4¹⁵–5⁵⁰ = – 11²⁰
3	6	.	7	–	= 2²⁵–14³⁰ 17⁴⁵–24
4	7	0.2	6	–	= 0⁰⁰–6³⁰
5	7	.	4	–	• ° 1⁴⁰ 3⁴⁰–6³⁰ = 2²⁰–12³⁰
6	6	.	pł.	–	= 8¹⁰–24
7	6	0.6	.	–	= 0⁰⁰–24 ◡ 19¹⁵–22¹²
8	5	3.6	.	–	• ° 3³⁰ 4⁴⁵–11³⁰ 14¹⁰–18⁴⁰ = 0⁰⁰–24
9	6	.	.	–	= 0⁰⁰–4³⁵ 10²⁰–16³⁰ ⌴ ¹ n–7³⁰
10	8	.	.	–	= 17²⁵–22¹⁵ ⌴ n–7¹⁰
11	9	.	.	–	⌴ ° 3¹⁰–7¹⁵
12	8	.	.	–	⌴ ¹ na
13	7	.	.	–	⌴ ² 1³⁰–9³⁰
14	7	0.0	.	–	⩺ 9³⁵–14⁴⁰ = 17³⁰–21¹⁵ ⌴ ¹ 1¹⁰–7³⁰ ◡ 18³⁰–20²⁰
15	8	10.0	.	–	✱ 6¹⁰–²⁵ • ° 22⁴⁵–24 ⩺ 1²⁵–7²⁰ por. ponad 10 m/sek 8⁴⁰–13¹⁵ por. ponad 15 m/sek–14²⁰ por. ponad 10 m/sek–15⁴⁰
16	6	14.1	.	–	• ° 0⁰⁰ 1⁰⁰–6¹⁰ • ¹–10¹⁶ ✱ 10²⁰–14⁴⁰ ⩺ 0⁰⁰–3⁴⁵ ⩺–7²⁰ [15.III:] ⩺–24 por. ponad 15 m/sek 20³⁰–24
17	7	4.7	3	–	• ° 1⁴⁰ 4²⁰–6¹⁰ ✱ ¹–6³⁵ • °–9³⁰ 18⁵⁰ 20³⁰–24
18	7	9.5	.	–	• ° 3⁴⁰–6³⁵ ✱ 7⁴⁵–⁵³ 8¹⁵ 15²⁰ 18⁵⁰–19¹⁰ 20⁴²–21⁰⁸ ⩺ ° 14⁰²–²⁵ W–E ⩺ 8⁴⁰–9⁰⁵ 10⁵⁰–11¹⁵ ⩺ 17¹⁵–22¹⁵
19	8	4.4	.	–	✱ 0⁰⁰–1⁴⁸ 1⁵⁰–2⁴⁵ • ° 13¹⁰ 16⁰⁵–23¹⁰ 24 ⊕ 10²⁰–11¹⁵
20	8	.	.	–	• ° 0⁰⁰ 5⁵⁵
21	8	.	.	–	
22	7	0.0	.	–	• ° 9⁴⁸ 10¹⁶ = 21²⁵–24 ⌴ ¹ 5¹⁰–7¹⁵
23	7	.	.	–	= 0⁰⁰–9³⁰ 16³⁰–18²⁰ ⌴ ¹ na
24	7	0.0	.	–	• ° 18⁵³ 19²⁰ ⩺ 5²⁰–6³⁰ 8¹⁰–21³⁵ = 17¹⁵–22²⁵
25	7	.	.	–	= 3²⁵–12³⁰ 18¹⁰–24
26	7	.	.	–	⩺ 6³⁵–12²⁵ (por. ponad 15 m/sek 6³⁵–11³⁰), 20²⁵–24 = 0⁰⁰–2⁴⁰
27	8	.	.	–	⩺ 0⁰⁰–8²⁵ (por. ponad 15 m/sek 2³⁰–6²⁰), por. ponad 10 m/sek 20⁰⁶–³⁰ por. ponad 15 m/sek–24 ◠ 22⁴³–⁵⁸
28	8	8.3	.	–	• ° 8¹⁵ 10⁵⁰ 13⁴⁰–14²⁰ 17¹⁵–19²⁵–20⁴⁰ 22⁴⁵–24 ⩺ 0⁰⁰–1⁴⁰ 2³⁵ 3⁴⁰ = 20⁴⁰–24
29	6	12.9	.	–	• ° 0⁰⁰–1³⁵ 2⁴⁰ 3²⁰ 5³⁰–6¹⁵ • ¹–7¹⁵ 8⁴⁰–9¹⁰ 10³⁰ 13³⁰–17³⁰ • ¹–18¹⁵ ✱ ¹–19¹⁰ ✱ ¹–21⁴⁰ ✱ °⁻¹ 24 = 0⁰⁰–24
30	5	5.3	2	–	• ¹ 3²⁵–4²⁵ • °–6⁴⁰ • °–9²⁵ • ¹–10³⁰ • °–15²⁰ 18³⁵ = 0⁰⁰–1⁴⁵ 3²⁰–7⁴⁰ ≡ °–10⁴² 20²⁰–24
31	8	2.9	.	–	= 0⁰⁰–5¹⁰ ≡ –7³⁰
Σ	–	76.9	–	–	UWAGI

Kwiecień – Avril

1	7	0.3	.	–	• ° 1⁰⁰ 3⁵–3⁴⁰ 4⁵⁰ 6²⁰ 7³⁵ ✱ 14³⁵–⁵⁰ 15⁴⁰–16¹⁵ 19⁴⁵–24 ⩺ 20³⁰–21¹⁵ = 4⁵⁰–6²⁰
2	7	0.4	.	–	✱ 0⁰⁰–1⁴⁰ • ° 16¹²–18¹⁵ 19²⁰–24
3	8	1.3	.	–	• ° 0⁰⁰ 5¹⁰ 7¹⁰ 20–8⁰³ • ¹–8⁵⁰ • °–9³⁵ = 20³⁰–24
4	7	.	.	–	= 0⁰⁰–5⁵⁵ ≡ °–1⁴⁵ ≡ ¹–2⁵⁰ ≡ °–7²⁰ = – 11⁰⁵
5	8	.	.	–	= 2²⁰–5⁵⁵ ≡ –8⁴⁰ ⌓ ¹ 2³⁵–9³⁰
6	8	.	.	–	⌴ ¹ 4³⁰–7¹⁰
7	6	9.9	.	–	• ° 7⁴⁵–10²⁰ ✱ ° 12³⁵–⁴⁰ • °–13⁰⁰ 14²⁵–15¹⁵ • ¹–16²¹ • °–18⁴⁶ ✱ ¹–20¹⁰ ✱ ¹–21⁰⁰ ✱ °–22¹⁵ ✱ °–24
8	8	.	2	–	✱ ° 0⁰⁰–7⁴⁵
9	8	.	.	–	⌴ ² na–a
10	7	.	.	–	= 2³⁰–7⁴⁵ ⌓ ¹ na–8⁰⁰
11	9	0.2	.	–	✱ 17⁴⁰–18⁰⁸ = 5¹⁰–8³⁵ ⌓ ¹ n–7⁰⁰
12	7	0.5	1	–	✱ ¹ 6⁰⁸–7¹⁰ ✱ °–8³⁰ ✱ ¹–8⁵⁰ ✱–10⁴⁰ 17⁴⁵–18⁰⁵ = 2³⁵–10⁴⁵ ⌴ ² n–6¹⁰ n–24
13	7	0.0	.	–	✱ ° 8³⁰–9⁰⁰ 10²⁶–12¹⁵ ✱ 12²⁰–⁵⁵ ⌴ ¹ 0⁰⁰–7⁰⁰
14	8	.	.	–	= 7⁰⁵–8¹⁰ ⌴ ¹ n–7⁰⁰ 19²⁰–24
15	7	0.0	.	–	✱ 11⁴⁰–12¹⁵ 15¹⁵–⁴⁰ = 21²⁵–24 ⌴ ¹ 0⁰⁰–8²⁰
16	7	1.5	.	–	• ° 8⁴⁵–9⁰⁰ • ° 10⁴⁷–11³² = 0⁰⁰–4²⁰ 17⁰⁵–19³⁰ ⌴ ² na–7⁴⁵
17	7	2.6	.	–	• ° 3²⁷–8³⁰ 11¹⁵ ✱ 13⁴⁰–14³⁵ ✱ ✕ 16⁴⁶–18⁰⁶ ✱–18³⁵ = 20²⁰–24
18	7	.	.	–	= 0⁰⁰–4⁴⁶ ≡ °–6⁴⁰ ≡ –8⁵⁰
19	6	5.3	.	–	• ° 10⁰²–14²⁰ 15³⁵ 16¹⁰–21¹⁰ ✱ 21⁴⁰–22²⁰ 23²⁰–24 = 5¹⁰–21²⁰
20	8	.	.	–	✱ 0⁰⁰–1⁴⁰ 2¹⁰–⁵⁰ 3⁰⁵–⁴⁰ 4⁵⁰–5¹⁵
21	8	0.3	.	–	✱ 16²⁵–17⁴⁰ 18⁵⁰–20⁰⁵ • ° 21⁴⁵ ⌴ n
22	8	.	.	–	= 0¹⁵–3⁴⁵ ≡ °–6⁵⁰ = –8²⁰
23	8	.	.	–	= 2³⁰–8²⁰
24	5	5.5	.	–	• ° 9⁴⁸ 11¹⁰–12³⁵ 18⁴⁵ 19¹⁵ 20⁴⁵ 21³⁰ 22²⁰ 24 = 3²⁰–15²⁰
25	9	2.8	.	–	• ° 0⁰⁰ 1⁰–7¹² • ¹–8¹⁰ 9⁴⁰–11²⁰ • ¹–12³⁰ • °–12⁵⁰ 13⁴⁰ • ° 18³⁵–21⁵⁰ 24 = 13⁴⁰–18³⁵
26	6	0.0	.	–	• ° 0⁰⁰ 2⁴⁵ 6⁴⁰–7²⁵ • °. 8³⁰ = 2⁴⁵–6⁴⁰ 8³⁰–15²⁰ 20⁴⁰–24
27	8	.	.	–	= 0⁰⁰–2⁴⁰ ≡ ¹–3⁴⁵ = –9²⁰ 19⁴⁰–24 ⌓ ² n
28	8	0.0	.	–	◟ 21⁴⁰–22¹⁰ = 0⁰⁰–3²⁰ ≡ –4⁴⁰ ⌓ ² n–9¹⁰
29	7	.	.	–	≡ 3²⁰–6³⁰ = 22²⁰–24 ⌓ ² n–a
30	7	2.1	.	–	✱ 15¹⁰–16²⁵ • ° 18³⁵ 19⁴⁰ ⩺ ° 15³⁸–16²² N–NW = 0⁰⁰–5¹⁵ ⌓ ° n–8¹⁰
31					
Σ	–	32.5	–	–	UWAGI

Jelenia Góra $\varphi = 50°54'$ $\lambda = 15°48'$ **Maj – Mai 1957**

Dni	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	77.8	77.4	77.3	77.5	5.6	10.4	4.9	6.4	11.6	0.6	69	50	72	64	2.8	6.3	2.5	5.9	2	7 ⊙	2	C 0	ENE 4	NE 1
2	76.3	74.7	73.5	74.8	2.4	10.1	3.1	4.7	11.3	−2.5	91	40	81	71	0.7	7.4	1.4	3.2	3 ⊙	7 ⊙	4	NE 1	E 4	C 0
3	73.1	71.7	71.6	72.1	1.9	13.6	7.6	7.7	14.1	−2.9	87	42	86	72	0.9	9.0	1.4	3.8	8	8	4	C 0	NW 3	WNW 3
4	69.8	73.0	74.7	72.5	7.3	6.4	4.4	5.6	7.9	0.5	80	65	65	70	2.0	3.4	3.0	2.8	10 ●	9	4	WSW 5	W 9	W 5
5	74.6	71.6	69.5	71.9	2.8	6.8	4.3	4.6	8.2	0.9	67	54	68	63	2.5	4.5	2.7	3.2	6	6	10 ●	W 7	W 7	NW 5
6	69.6	69.6	69.8	69.7	0.0	3.4	−0.4	0.6	5.6	−1.0	100	80	96	92	0.0	1.6	0.2	0.6	9	8	2	W 5	NW 4	C 0
7	68.9	68.4	68.9	68.7	−1.1	6.0	0.7	1.6	7.7	−4.4	95	54	92	80	0.3	4.3	0.5	1.7	10	9	1	C 0	WNW 4	NW 1
8	69.1	68.5	69.4	69.0	1.5	5.7	3.4	3.5	8.1	−1.1	96	67	83	82	0.3	3.1	1.3	1.6	10 ●	9	4	NW 3	NW 2	C 0
9	71.1	71.3	72.3	71.6	0.8	9.3	2.6	3.8	10.6	−1.4	98	53	84	78	0.2	5.5	1.2	2.3	10	8	0	C 0	NNE 3	C 0
10	72.1	71.3	72.6	72.0	1.3	11.0	7.5	6.9	13.5	−3.6	96	54	80	77	0.3	6.0	2.1	2.8	8	7	6	NE 1	NW 3	E 2
11	74.0	73.6	73.6	73.7	4.6	16.3	8.4	9.4	18.4	−1.4	90	35	81	69	0.8	12.0	2.1	5.0	5 ⊙	4 ⊙	0	C 0	NE 2	C 0
12	74.1	74.2	75.8	74.7	10.0	19.3	14.1	14.4	20.9	2.7	86	57	69	64	1.8	14.0	4.9	6.9	0	6 ⊙	9 ●	C 0	SW 1	C 0
13	77.5	77.1	78.4	77.7	10.9	18.7	12.0	13.4	20.2	5.4	85	50	90	75	1.9	10.8	1.3	4.7	6 ⊙	9 (R)	10	C 0	E 3	SE 1
14	80.0	80.7	81.9	80.9	11.8	17.1	11.1	12.8	19.3	6.4	89	48	84	74	1.5	10.1	2.1	4.4	4	7	5	E 1	NW 2	C 0
15	82.9	81.3	79.3	81.2	9.4	19.7	13.5	14.0	20.7	3.1	89	48	68	68	1.3	11.8	5.0	6.0	3	7	0	C 0	ESE 3	ESE 2
16	76.4	73.9	75.3	75.2	15.2	22.9	14.3	16.7	24.2	5.8	65	40	86	64	6.0	16.7	2.4	8.4	1 ⊙	4 ⊙	10 ● R	NE 1	SE 7	NW 4
17	78.0	80.1	80.4	79.5	9.3	9.5	9.5	9.4	14.3	8.9	99	95	96	97	0.1	0.7	0.5	0.4	10	10 ●	10	W 1	WNW 4	W 1
18	79.2	77.0	73.7	76.6	10.0	17.1	11.3	12.4	18.6	7.8	95	66	93	85	0.7	6.7	1.0	2.8	1	4 ⊙	0	C 0	E 6	C 0
19	70.1	68.0	66.9	68.3	12.3	21.5	14.6	15.8	22.7	6.1	87	59	93	80	1.9	10.4	1.1	4.5	6	4	9	C 0	NE 4	C 0
20	69.7	73.6	77.7	73.7	13.0	11.7	9.4	10.9	14.9	9.0	94	99	95	96	0.9	0.1	0.6	0.5	10	10 ●	10 ●	NW 4	WNW 3	W 2
21	79.3	78.3	77.4	78.3	8.2	12.2	7.4	8.8	14.0	6.6	75	63	91	76	2.7	5.3	0.9	3.0	8	9	7	C 0	NW 3	C 0
22	76.0	74.7	74.8	75.2	7.5	14.1	11.5	11.2	15.8	4.1	87	52	72	70	1.4	7.7	3.8	4.3	4 ⊙	9	10 ●	C 0	ENE 2	NE 6
23	72.9	72.0	71.9	72.3	8.6	13.7	12.9	12.0	16.3	7.6	92	85	96	91	1.0	2.3	0.6	1.3	10	10	8 ●	C 0	E 2	C 0
24	74.4	76.3	79.4	76.7	10.7	13.4	12.2	12.1	15.3	8.1	96	92	81	90	0.5	1.3	2.6	1.5	10	10	9	C 0	NW 2	NE 5
25	82.3	83.1	84.9	83.4	6.3	10.7	7.2	7.8	12.4	5.7	81	56	59	65	1.8	5.7	4.2	3.9	8	9	4	NE 3	NE 6	NE 6
26	85.3	85.4	85.0	85.2	4.0	8.0	5.0	6.0	8.9	2.0	85	51	66	67	1.3	5.2	3.3	3.3	8	8	7	ENE 3	NE 7	C 0
27	83.8	83.6	83.1	83.5	3.6	7.5	4.5	5.0	8.7	−0.8	83	66	81	77	1.3	3.5	1.6	2.1	9	9	9	NE 2	NNE 3	C 0
28	81.3	80.6	79.8	80.6	3.6	9.4	5.8	6.2	11.1	−2.6	86	55	77	73	1.1	5.3	2.1	2.8	2 ⊙	9	5	C 0	NNE 3	ENE 1
29	81.1	81.5	81.6	81.4	6.0	11.6	6.5	7.6	14.4	−1.9	77	47	78	67	2.2	7.2	2.2	3.9	3	7 ⊙	2	C 0	C 0	C 0
30	82.0	80.4	79.7	80.7	6.4	16.4	10.1	10.8	18.0	−1.7	79	43	77	66	2.0	10.6	2.9	5.2	0 ⊙	7 ⊙	5	C 0	SE 2	C 0
31	79.2	78.0	76.0	77.7	13.6	16.9	10.3	12.8	18.5	2.1	61	47	81	63	6.2	10.1	2.4	6.2	0 ⊙	7	2	E 2	SSE 8	C 0
M	76.2	75.8	76.0	76.0	6.7	12.6	8.1	8.9	14.4	2.2	86	58	81	75	1.6	6.7	2.1	3.5	5.9	7.6	5.4	1.2	3.7	1.5

Czerwiec – Juin

1	76.8	77.1	77.8	77.2	12.3	19.3	12.3	14.0	21.0	1.9	76	49	76	67	3.4	11.4	3.4	6.1	3	5 ⊙	0	C 0	NW 3	C 0
2	80.1	80.3	80.7	80.4	11.9	20.8	13.2	14.8	22.1	4.5	82	49	85	72	2.5	12.5	2.3	5.8	0 ⊙	1 ⊙	0	C 0	WNW 6	C 0
3	80.2	77.4	74.4	77.3	11.4	23.3	15.2	16.3	25.5	4.6	90	50	86	75	1.4	14.2	2.5	6.0	0 ⊙	8	7	C 0	E 2	C 0
4	73.1	73.7	72.3	73.0	11.0	17.1	14.0	14.0	21.1	5.7	95	82	99	92	0.7	3.5	0.2	1.5	9	10	10 ●	ESE 3	W 3	C 0
5	70.9	68.8	68.5	69.4	12.4	16.4	9.2	11.8	18.9	8.7	83	65	96	81	2.4	6.5	0.4	3.1	9	4 ⊙	9	W 5	SW 5	W 1
6	70.7	72.2	71.6	71.5	8.4	13.5	9.9	10.4	16.8	5.2	82	49	81	71	2.0	7.9	2.4	4.1	9	4	5	W 6	W 7	C 0
7	70.8	70.3	71.5	70.9	15.5	20.8	14.3	16.2	21.7	3.9	62	42	83	62	6.7	14.2	2.7	7.9	6 ⊙	9	10	SW 2	SW 6	C 0
8	72.1	71.4	70.2	71.2	13.0	21.4	15.3	16.8	23.6	11.1	87	57	80	75	1.9	11.0	3.6	5.5	9	8 ⊙	7	E 2	SE 3	C 0
9	68.3	70.8	72.1	70.4	19.8	19.3	17.1	18.3	20.7	10.9	72	69	81	74	6.3	6.8	3.7	5.7	8 ⊙	8 ⊙	9	NE 2	N 1	C 0
10	72.0	71.1	71.3	71.5	15.3	21.5	18.5	18.0	23.1	7.9	94	62	83	80	0.9	9.6	3.5	4.7	5 ⊙	3 ⊙	3	C 0	NE 3	C 0
11	66.7	66.4	71.7	68.3	23.6	28.6	19.7	22.9	29.5	14.2	58	40	77	58	12.1	23.5	5.3	13.6	4 ⊙	8 ⊙	10	E 2	SSE 6	W 2
12	81.8	87.2	90.2	86.4	12.3	12.2	13.6	12.9	19.8	11.6	98	90	91	95	0.3	1.4	1.3	1.1	10 ●	10	10	WNW 2	NW 4	W 1
13	92.4	91.5	90.2	91.4	14.0	18.7	12.9	14.6	21.2	9.6	77	57	69	68	3.7	9.4	4.6	5.9	9 ⊙	6 ⊙	6	NW 1	NW 2	C 0
14	89.9	88.9	88.1	89.0	13.7	20.7	14.6	15.9	21.7	4.7	68	48	72	63	5.1	12.6	4.6	7.4	0 ⊙	1 ⊙	0	C 0	E 3	C 0
15	87.6	86.9	84.4	86.3	14.3	20.4	13.7	15.6	21.9	6.0	63	48	76	62	6.2	12.6	3.7	7.5	0 ⊙	0 ⊙	0	E 3	NE 5	C 0
16	82.7	81.2	79.4	81.1	17.0	23.1	15.9	18.0	25.7	6.7	58	42	65	55	8.1	16.4	6.3	10.3	0 ⊙	0 ⊙	0	E 1	ENE 8	C 0
17	78.8	78.1	76.9	77.9	18.8	24.3	17.6	19.6	25.6	7.0	62	43	69	58	8.2	17.2	6.2	10.5	0 ⊙	1 ⊙	2	C 0	E 6	ESE 2
18	75.8	73.7	72.8	74.1	17.7	27.5	18.4	20.5	28.9	12.0	69	33	75	59	6.2	24.7	5.3	12.1	0 ⊙	4 ⊙	4	C 0	SE 4	C 0
19	72.4	72.0	72.1	72.2	18.6	27.0	16.9	19.8	28.6	8.7	72	34	95	67	6.1	23.4	1.0	10.2	2 ⊙	5 ⊙	9 (R)	SE 1	SW 5	C 0
20	74.5	73.7	76.7	75.6	17.5	19.6	16.5	17.5	23.6	14.3	83	78	89	83	3.4	5.1	2.2	3.6	10 ●	9	8	C 0	NW 2	C 0
21	77.2	74.2	71.1	74.2	17.0	22.1	18.1	18.8	23.9	10.7	89	65	79	78	2.2	9.2	4.3	5.2	6 ⊙	9	1	C 0	ENE 3	C 0
22	68.2	66.3	66.3	67.0	15.7	22.4	14.6	16.8	23.3	11.7	98	62	88	83	0.4	10.4	2.0	4.3	9	9	8	C 0	SW 5	W 2
23	70.5	69.6	72.2	70.8	13.8	19.9	13.8	15.3	23.6	10.7	93	84	91	83	1.1	8.3	1.5	3.6	10	9	9	NW 1	SW 2	C 0
24	70.5	69.2	69.1	68.3	12.9	12.6	12.3	12.5	14.3	10.7	93	92	98	94	1.1	1.2	0.3	0.9	10 ●	10	10 ●	E 1	E 5	E 5
25	68.8	75.0	78.6	74.1	13.2	12.3	9.9	11.3	14.9	9.5	69	71	86	75	4.7	4.2	1.8	3.6	9	9	4	W 5	W 7	C 0
26	81.3	82.1	84.0	82.5	9.3	13.0	9.0	10.1	16.9	2.6	88	65	86	80	1.4	5.3	1.6	2.8	9	8	2	NW 2	NW 2	C 0
27	84.9	85.5	86.9	85.8	8.5	16.5	10.6	11.6	18.2	2.6	93	58	81	77	0.8	7.8	2.4	3.7	9	8	4	C 0	WNW 5	C 0
28	86.3	84.7	84.0	85.0	11.1	23.0	18.0	17.5	25.3	5.2	89	56	84	76	1.5	12.3	3.2	5.7	10	3 ⊙	0	C 0	NW 6	C 0
29	84.6	84.8	83.1	84.2	18.3	27.0	19.8	21.2	28.9	9.9	83	48	81	71	3.4	18.3	4.3	8.7	0 ⊙	2 ⊙	0	C 0	NW 5	C 0
30	82.8	81.8	81.7	82.1	19.6	29.8	18.6	21.6	30.4	11.9	73	36	93	68	5.7	26.8	1.5	11.3	1 ⊙	9	6	C 0	NNE 1	C 0
31																								
M	77.1	76.9	76.9	77.0	14.6	20.5	14.8	16.2	22.6	8.2	80	57	83	73	3.7	11.6	2.9	6.1	5.6	5.9	5.1	1.4	4.0	0.4

Jelenia Góra $H_s = 342\ m$ $H_b = 343{,}0\ m$ $h_w = 15\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU	USŁONECZNIENIE	POGODA
1	9	.	.	–	
2	8	.	.	–	⌴² 0²⁰–5⁵⁰ ⌒⁰ 19³⁰–24
3	8	0.0	.	–	= 20³⁰–24, ⌴² 0⁰⁰–6³⁰
4	7	0.0	.	–	●⁰ 6⁴⁰ 7¹⁵ ▽–7⁵² 8³⁰–9¹⁵, = 0⁰⁰–7²⁰
5	8	13.9	.	–	▽ 8²⁰–³⁵, 9⁵³–10¹⁰, 10²⁰–11¹⁰, 11²⁰–12¹⁵, 12²⁶–⁴¹ ●⁰ 20⁴⁰ 24
6	7	0.6	11	–	●⁰ 0⁰⁰–¹⁰ ✳¹–3⁴⁰ ✳⁰–6¹² ▽ 8²⁰ 12¹⁵ ▽ 13⁰⁵–¹⁵ ▽ 15⁵⁵–16¹⁰, = 22¹⁵–24, ⌴⁰ 20³⁰–24
7	8	0.1	.	–	▽ 15⁴⁰–16⁰⁰ 16¹⁰–⁴⁵ = 0⁰⁰–3⁴⁰, ⌴² 0⁰⁰–7⁵⁰
8	6	1.0	.	–	●⁰ 6¹² 8⁴⁰ ✳ 9²⁰–³⁰ ▽ 9⁴⁰–10³⁵, = 4⁴⁰–13³⁰, ⌓ 21⁴⁰–23⁰⁰
9	8	.	.	–	
10	8	.	.	–	≡ 0²⁰–3¹⁰ = –8²⁰, ⌴² n–6¹⁰
11	8	.	.	–	≡ 1²⁵–3²⁰ = –6¹⁵, ⌒² 0²⁰–8¹⁰, 20²⁰–24
12	8	0.0	.	–	●⁰ 19⁴⁵ 20³⁰ ▽–21¹⁵, ⌒² 0⁰⁰–8⁰⁰
13	8	0.8	.	–	▽ 16⁰³–⁴⁰ 20²⁰–22¹⁵, (K)⁰ 10⁵⁴–16²⁰ SE, 18⁴⁸–19⁴⁰ SE
14	7	.	.	–	≡ 0²⁰–5³⁰ = –6²⁰
15	8	.	.	–	≡ 1⁰⁰–2³⁰ = –7¹⁵, ⌒² n–a
16	7	12.4	.	–	▽ 20³⁵–24, (K)⁰ 19⁵⁵ NW–S K¹ 20³⁵–24 NW–SE, = 1³⁵–6¹⁵, ⌒⁰ 0²⁰–7⁰⁵
17	6	0.1	.	–	▽ 0⁰⁰–2⁴⁵ ●¹ 7¹⁵–11⁵⁰ ●⁰ 15⁴⁰, K¹ 0⁰⁰–1⁴⁸ N–SW, = 6¹⁵–17²⁰, 22³⁰–24
18	7	.	.	–	= 0⁰⁰–7²⁰, 22²⁰–23⁵⁰ ≡ –24, ⌒⁰ 20³⁰–24
19	8	0.0	.	–	≡ 0⁰⁰–3⁴⁵ = –6⁵⁰, ⌒¹ 0⁰⁰–8¹⁰
20	6	3.3	.	–	●⁰ 3¹⁰ 4¹⁵ 7²¹ 8⁴⁰, 9⁴⁵ 10³⁰–11²⁵ 12³⁰–13³⁵ ●¹–14²⁰ ●⁰–18⁴⁰ 19⁴⁵–22⁴⁰, 23¹⁵–24, = 0⁰⁰–24
21	8	0.0	.	–	●⁰ 0⁰⁰–²⁰ ●–¹⁴⁵ ●⁰ 9²⁰..³⁵ = 0⁰⁰–²⁰ ⌒² 22¹⁰–24
22	8	0.8	.	–	●⁰ 20⁵⁵ 21³⁰–24, = 3⁴⁰–9²⁰, ⌒² 0⁰⁰–8¹⁵
23	7	0.6	.	–	●⁰ 0⁰⁰–²⁵⁵ ●⁰ 10⁴⁰–11⁴⁵ 15⁴⁵ 16²⁰ ▽–17¹⁵ ●⁰ 20⁴⁰ 21¹⁵, = 2⁵⁵–8²⁵ 21¹⁵–23³⁰ ≡ –24
24	6	2.0	.	–	●⁰ 12⁰⁶..³⁵ ▽⁰ 15²⁰–18⁴⁰, ≡ 0⁰⁰–⁵⁰ = –24
25	9	.	.	–	
26	8	.	.	–	⌴⁰ 21¹⁵–24
27	8	0.1	.	–	▽ 11⁵⁰–12¹³ ▽ 14⁵²–15⁰⁵ 15²⁰–³⁵ ⌴⁰ 0⁰⁰–5⁰²
28	8	0.0	.	–	▽ 15⁵⁵–16¹⁰, = 2³⁵–4²⁰, ⌴¹ 4¹⁰–5⁴⁰
29	8	.	.	–	= 1²⁰–4³⁵, ⌴¹ na–6⁴⁵
30	8	.	.	–	= 2²⁰–3⁴⁵ ≡ –4²⁰
31	8	.	.	–	⌒⁰ 1²⁰–5⁴⁰
Σ	–	55.7	–	–	UWAGI

Czerwiec – Juin

1	7	.	.	–	= 1⁰⁰–4⁴⁰, ⌒¹ 9⁴⁰–24
2	7	.	.	–	≡⁰ 0⁰⁰–4⁴⁵ =–10²⁰, 22⁴⁵–24, ⌒¹ 0⁰⁰–6¹⁵
3	7	0.0	.	–	▽ 17³⁵–⁴⁵ 17⁵⁰–18¹⁰, = 0⁰⁰–3²⁰ ≡ –5³⁰ = –11¹⁵, 21⁴⁰–24, ⌒² n–7²⁰
4	6	22.2	.	–	▽ 14¹⁵–15¹⁰ ●⁰ 17¹⁵–18¹⁰ ●¹–24, = 0⁰⁰–6⁰⁰, 11⁴⁰–24
5	8	2.6	.	–	●¹ 0⁰⁰–2⁴⁰ 4³⁰ 5¹⁵–7¹⁰ ▽ 10²⁰–³¹, 13²⁵–³⁸
6	8	0.0	.	–	▽ 8²⁰–9¹⁵, ≡ 0²⁰–4¹⁵ ⌴¹ n–a
7	8	3.1	.	–	= 22⁴⁰–24, ⌴¹ 0⁰⁰–8¹⁵ ⊕ 11³⁰–14⁴⁵
8	8	.	.	–	●⁰ 1¹⁵–4¹⁵ 4⁴⁰–5³⁰ 5³⁵–7³⁵ =0⁰⁰–8¹⁵
9	8	0.0	.	–	▽ 13⁴⁰–⁵⁵ 14¹⁵–15³⁰ 19⁴⁵–⁵⁵
10	7	.	.	–	= 3¹⁰–4⁴⁵ ≡¹–6⁴⁵ = –12²⁰
11	8	0.2	.	–	↙ 21⁴⁵–22⁰⁵ (K)¹–22²⁵ SW–NE ↙–23²⁰, ∞ 21¹⁰–⁴⁵ 22³⁰–24
12	6	1.0	.	–	●⁰ 2³⁵ 3²⁵ ●⁰ 4⁴⁵–6³⁰ 7⁴⁰ ●¹–12⁴², = 0⁰⁰–24
13	8	.	.	–	= 0⁰⁰–1⁴⁰ ≡ 3²⁰–6³⁰, ⌒¹ 1¹⁰–8²⁰
14	8	.	.	–	⌒¹ n–a
15	9	.	.	–	⌒⁰ na
16	8	.	.	–	⌒⁰ n–8²⁰
17	8	.	.	–	⌒¹ n–8¹⁵
18	8	.	.	–	⌒⁰ 3²⁰–7⁴⁰
19	8	2.2	.	–	(K) 11⁵⁰–13¹⁵ E ●K⁰ 15⁴⁵–17⁰⁰–17⁴⁰ W–E (K) 21⁵⁵–22¹⁰ ●K⁰ 22¹⁰–23⁰⁵–23⁴⁵ W–E, ⌒⁰ 0²⁰–8¹⁵
20	6	0.0	.	–	●⁰ 7⁵⁰ 9¹⁵ 11¹⁰..²⁴, = 2⁰⁰–11²⁰, 13³⁰–15⁴⁰, 23¹⁰–24, ⌒¹ n
21	7	2.8	.	–	= 0⁰⁰–9¹⁰, ⌒² n–8³⁵
22	6	1.3	.	–	●⁰ 6²⁰–7⁴⁰ ▽ 8⁰²–¹⁵ 22²⁵–⁴², = 0⁰⁰–5²⁰
23	8	1.6	.	–	●¹ 6²⁰–7²⁵ ▽ 17⁰⁶–²⁶, = 6³⁰–10²⁰, 23²⁰–24
24	7	11.2	.	–	●⁰ 2³⁵ 4⁴⁰, 6⁵⁰–8³⁵ ▽–9³⁵ ●⁰–11¹⁰ ▽–13¹⁵ ●⁰ 19⁴⁰..²⁰¹⁰ ●¹–20⁴⁵ ●⁰–22¹⁰ ▽ 22³⁵–24, = 0⁰⁰–13²⁵, 18⁴⁰–24
25	8	0.2	.	–	●⁰ 0⁰⁰–3²⁰ 4¹⁰ ▽ 20⁴⁵–21³⁵, *par. wiatru ponad 15 m/sek* 11²⁰–13⁴⁵, = 0⁰⁰–4¹⁵
26	8	0.1	.	–	▽ 14⁵¹–15⁰⁸, ≡ 3²⁰–6²⁵
27	7	.	.	–	●⁰ 6⁵⁰ 7²⁵, = 4⁴⁰–7¹⁵, ⌒² 22⁴⁰–24
28	6	.	.	–	= 22³⁵–24, ⌒² 0⁰⁰–8¹⁵
29	8	.	.	–	= 0⁰⁰–10²⁰, ⌒² n–8¹⁵
30	8	0.0	.	–	(K)¹ 17⁵⁰–18¹⁰ ●K–20²⁰ W–SE, ≡ 2²⁰–5²⁵, ⌒² n–8⁵⁰
31					
Σ	–	48.9	–	–	UWAGI

Jelenia Góra $\varphi = 50°54'$ $\lambda = 15°48'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			POGODA			KIERUNEK I PRĘDKOŚĆ WIATRU D,v					
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III		
1	80.1	78.9	78.1	79.0	18.5	30.4	20.2	22.3	31.6	12.1	83	35	82	66	3.5	28.2	4.4	12.0	0	3 ⊙	6	C	0	SW	5	C	0
2	76.3	77.8	80.4	78.2	23.3	26.7	20.3	22.6	27.6	16.1	69	55	77	67	8.7	15.6	5.4	9.9	4 ⊙	5	8	C	0	W	5	C	0
3	81.7	80.5	78.2	80.1	16.5	24.7	18.9	19.8	25.9	9.6	75	45	60	60	4.8	17.2	8.8	10.3	2	6	1	C	0	E	4	C	0
4	78.6	76.5	76.3	77.1	19.1	31.8	24.7	25.1	33.3	11.4	75	36	62	58	9.6	30.2	11.9	15.9	4	6 ⊙	5	SE	2	SW	7	C	0
5	77.2	77.0	79.4	77.9	25.5	32.7	25.1	27.1	35.6	16.4	67	47	71	62	10.8	26.2	9.5	15.4	0 ⊙	1	8	C	0	NNW	4	C	0
6	82.4	81.5	80.3	81.4	19.9	26.7	21.8	22.6	28.4	15.6	77	51	59	62	5.5	17.2	10.7	11.1	1	4	4	ENE	2	N	2	E	2
7	78.4	78.8	77.1	78.1	18.2	30.5	24.7	24.5	31.2	16.2	96	55	80	77	0.9	19.5	6.3	8.8	6 ⊙	0 ⊙	5	NE	1	NE	2	C	0
8	76.8	76.4	75.2	76.1	22.3	31.5	18.1	22.5	31.6	17.8	83	49	98	77	4.7	25.6	0.5	9.6	⊙	7	5	E	3	NW	2	C	0
9	76.2	76.5	76.4	76.4	17.9	23.2	16.4	18.5	25.1	16.0	97	64	96	86	0.6	10.2	0.8	3.9	10 ●	8	6	C	0	WNW	5	C	0
10	73.9	70.8	69.4	71.4	16.6	21.1	16.7	17.8	22.3	13.7	96	76	99	90	0.8	6.0	0.2	2.3	9	7	10	C	0	E	2	C	0
11	66.1	67.4	69.2	67.6	15.1	17.4	16.2	16.2	17.8	14.3	99	91	99	96	0.2	1.9	0.2	0.8	10 ●	10 ●	10 ●	C	0	C	0	C	0
12	71.5	73.5	74.1	73.0	14.9	16.3	15.7	15.6	19.6	14.5	99	93	95	96	0.1	1.3	0.9	0.8	10 ●	10	5	C	0	W	5	C	0
13	76.1	76.8	78.4	77.1	14.4	25.3	17.3	18.6	25.9	10.7	99	46	93	79	0.2	17.4	1.4	6.3	0	4 ⊙	4	C	0	N	2	C	0
14	76.8	77.3	75.7	76.6	16.5	17.1	15.0	15.9	19.8	12.7	97	87	98	94	0.6	2.6	0.3	1.2	7	10 ●	5	C	0	C	0	C	0
15	74.3	74.2	74.0	74.2	14.7	16.7	14.8	15.2	19.7	12.8	99	92	99	97	0.2	1.6	0.2	0.7	9	9	9	C	0	WNW	2	C	0
16	73.7	73.1	72.6	73.1	12.7	16.9	15.3	15.0	19.0	10.6	98	71	84	84	0.4	5.5	2.8	2.9	10	10	10	C	0	W	2	C	0
17	71.7	71.5	72.8	72.0	13.7	19.1	14.6	15.5	19.8	12.1	87	63	79	76	2.0	8.1	3.4	4.5	10	9	5	NW	4	WNW	4	C	0
18	73.7	72.6	71.1	72.5	12.2	21.0	14.7	15.6	22.9	7.1	93	53	91	79	1.0	11.7	1.5	4.7	1	4 ⊙	8	C	0	NW	5	C	0
19	69.1	67.4	66.4	67.6	14.0	24.7	20.1	19.7	25.3	7.8	90	45	70	68	1.6	17.0	7.0	8.5	4	8	8	C	0	SE	7	SE	2
20	65.4	66.2	66.6	66.1	15.7	14.9	14.1	14.7	20.3	13.7	95	97	93	95	0.9	0.3	1.1	0.8	10	10 ●	10	C	0	NW	4	C	0
21	65.8	64.5	65.3	65.2	13.5	20.6	13.0	15.0	21.6	12.0	97	56	93	82	0.6	10.6	1.1	4.1	10	9 ⊙	5	SW	1	NW	5	C	0
22	65.5	65.0	62.8	64.4	13.5	13.4	14.7	14.1	14.7	8.0	92	93	99	95	1.3	1.1	0.2	0.9	10	10 ●	10 ●	W	4	W	4	W	1
23	63.8	66.5	69.9	66.7	15.5	16.9	14.8	15.5	17.3	14.3	97	94	97	96	0.6	1.2	0.5	0.8	10	10 ●	10 ●	N	5	NW	4	W	8
24	71.8	73.1	73.1	72.7	13.1	15.4	13.6	13.9	17.7	11.8	96	77	84	86	0.6	4.1	2.5	2.4	10	9	9	W	6	W	7	WNW	2
25	73.9	72.8	69.9	72.2	13.1	15.5	11.9	13.1	16.4	10.2	80	70	99	83	3.0	5.5	0.1	2.8	8	10	7	WNW	5	SW	1	C	0
26	72.0	71.9	69.9	71.3	14.1	17.4	13.0	14.4	17.8	9.9	85	79	95	86	2.4	4.2	0.7	2.4	8	9 ●	9	W	5	W	5	C	0
27	66.2	66.5	67.0	66.6	15.3	18.2	11.8	14.5	19.4	11.4	98	61	95	85	0.4	8.1	0.6	3.0	10	6 ⊙	9	C	0	SW	6	WSW	3
28	68.0	68.7	69.7	68.8	12.6	17.9	13.5	14.4	18.2	8.7	78	55	87	73	3.2	9.3	2.0	4.8	7 ⊙	7 ⊙	8	W	5	SW	5	C	0
29	71.2	72.3	74.9	72.8	12.1	18.4	14.5	14.9	19.3	10.5	99	64	88	84	0.1	7.6	2.0	3.2	10	7	10	C	0	SW	2	C	0
30	76.8	78.7	81.2	78.9	14.1	13.6	13.2	13.5	15.6	12.7	90	93	96	93	1.6	1.1	0.6	1.1	10	10	10 ●	W	3	W	5	W	4
31	83.7	85.2	86.1	85.0	12.7	14.9	12.9	13.4	15.3	11.0	93	79	80	85	0.7	3.4	2.9	2.3	10 ●	10	10	W	3	W	4	C	0
M	73.5	73.5	73.6	73.5	15.8	21.0	16.5	17.4	22.4	12.0	90	67	87	81	2.2	10.2	2.9	5.1	6.9	7.4	7.3	1.4		3.5		0.7	

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1	85.8	85.1	83.9	84.9	12.0	20.0	14.7	15.4	21.9	9.1	90	63	92	82	1.3	8.6	1.3	3.7	10	4 ⊙	2	C	0	WNW	3	C	0
2	84.1	83.6	84.3	84.1	12.4	19.1	11.3	13.6	19.9	8.6	99	68	85	84	0.2	7.2	2.0	3.1	8	8	1	C	0	WNW	4	NW	1
3	84.1	83.3	83.3	83.6	9.0	13.9	11.9	11.7	15.5	4.0	97	97	89	94	0.3	0.6	1.3	0.8	8	10	4	C	0	W	2	C	0
4	82.8	83.3	83.9	83.3	10.3	15.0	12.9	12.8	18.0	5.0	99	82	93	91	0.1	3.1	1.1	1.4	10 ●	10	6	C	0	WNW	3	W	1
5	83.9	83.8	83.3	83.7	13.6	20.8	12.9	15.0	21.1	6.9	90	62	93	82	1.6	9.2	1.1	4.0	1 ⊙	8	3	C	0	N	1	C	0
6	82.8	81.0	79.2	81.0	11.3	23.3	14.5	15.9	23.3	6.2	98	47	92	79	0.4	15.2	1.3	5.6	0	5	4	C	0	SE	1	C	0
7	75.0	72.9	72.2	73.4	13.8	22.0	16.0	17.0	23.0	9.9	98	68	92	86	0.4	8.5	1.6	3.5	9	9	9 ●	C	0	SW	3	NW	2
8	72.3	72.2	71.2	71.9	15.2	19.6	14.4	15.9	21.8	10.6	90	67	94	84	1.7	7.5	0.9	3.4	6 ⊙	7 ⊙	5	W	3	NW	3	C	0
9	67.3	65.3	61.4	64.7	14.2	23.9	21.5	20.3	25.4	9.5	97	59	70	75	0.6	12.0	7.8	6.8	5 ⊙	7 ⊙	9	C	0	SE	7	SSE	5
10	63.1	64.6	68.3	65.4	13.9	20.6	17.3	17.8	22.0	14.9	97	67	73	79	0.6	7.9	3.2	4.6	10 ●	7 ⊙	3	C	0	WSW	8	C	0
11	72.2	72.4	72.1	72.2	16.9	25.1	16.2	18.6	26.7	10.7	81	50	86	72	3.7	16.0	2.5	7.4	4	5	3	NE	2	SW	4	C	0
12	72.2	73.2	74.0	73.1	16.4	20.9	15.7	17.2	22.9	14.1	96	74	94	88	0.8	6.4	1.1	2.8	9	6	7	SW	1	C	0	C	0
13	76.3	75.8	74.8	75.6	12.4	22.8	16.4	17.0	25.1	8.8	96	56	95	82	0.5	12.1	0.9	4.5	7	6 ⊙	10	C	0	NE	1	C	0
14	73.0	72.7	71.2	72.3	15.7	20.6	15.2	16.7	23.1	12.1	97	66	92	85	0.6	8.3	1.3	3.4	10	9	4	C	0	SW	3	NW	1
15	70.7	69.9	70.0	70.2	12.6	21.5	17.4	17.2	22.5	8.8	92	52	83	76	1.2	12.2	3.4	5.6	0 ⊙	7 ⊙	7	C	0	WSW	3	C	0
16	72.5	72.7	72.9	72.7	14.7	15.0	12.7	13.8	17.8	12.7	81	89	96	89	3.1	1.8	0.5	1.8	10 ●	10	6	C	0	C	0	C	0
17	73.0	72.7	72.3	72.7	12.4	14.5	14.1	13.8	16.7	8.6	80	69	79	76	2.9	3.1	3.4	3.8	9	10	10	SW	4	SW	4	SW	3
18	70.9	70.5	72.1	71.2	13.4	17.5	10.5	13.0	17.8	10.1	85	75	99	86	2.7	4.9	0.2	2.6	10	8	2	SW	3	W	3	C	0
19	74.5	76.1	78.3	76.3	10.1	17.5	12.4	13.1	17.8	6.5	99	73	94	89	0.2	5.5	0.9	2.2	6	7 ⊙	1	C	0	WNW	3	C	0
20	79.8	78.4	78.3	78.9	10.0	19.2	13.0	14.8	20.3	6.3	100	58	90	83	0.0	9.2	1.6	3.6	2 ⊙	6 ⊙	9	C	0	NW	3	C	0
21	77.0	75.3	74.2	75.6	15.2	18.9	12.3	14.8	19.4	12.1	90	73	98	87	1.7	5.9	0.4	2.7	10 ●	9	10 ●	C	0	WSW	3	WNW	3
22	73.3	74.1	74.6	74.0	11.2	12.7	8.0	10.0	13.3	7.7	97	78	97	91	0.3	3.3	0.3	1.3	9	9	2	W	3	W	3	C	0
23	74.3	72.8	71.2	72.8	6.5	16.1	8.2	9.8	18.3	1.6	96	53	92	80	0.5	8.6	0.9	3.3	0	5	0	C	0	WNW	1	C	0
24	66.8	65.8	72.3	68.4	11.0	18.4	7.7	11.2	19.0	4.2	94	66	94	85	0.8	7.2	0.6	2.9	6 ⊙	10	0	C	0	SW	4	C	0
25	73.3	72.6	70.3	72.8	9.3	19.4	14.1	14.3	20.3	3.8	88	47	73	70	1.4	11.9	4.1	5.8	2	6 ⊙	0	C	0	SE	4	S	3
26	71.1	71.3	73.8	72.1	12.9	14.7	7.4	10.6	16.8	6.9	62	63	97	74	5.7	6.2	0.3	4.1	2 ⊙	7 ●	2	WSW	6	WSW	7	C	0
27	74.3	73.9	73.1	73.8	9.9	15.2	10.9	11.7	17.1	5.6	92	59	81	77	1.0	7.2	2.4	3.5	10	9	10 ●	SW	1	WSW	4	NW	1
28	71.9	73.2	73.9	73.7	11.0	13.0	11.3	11.8	14.7	9.9	93	80	88	88	0.6	3.0	1.7	1.8	7	10 ●	10 ●	NE	1	NW	1	WSW	4
29	78.1	79.3	80.9	79.5	9.9	13.2	10.7	11.1	15.6	5.2	93	67	89	83	0.8	5.0	1.9	2.4	10	9	8	W	1	W	5	W	1
30	81.0	81.2	80.4	80.9	9.7	14.1	6.8	9.4	14.8	6.6	87	59	94	80	1.6	6.6	0.6	2.9	7	6	0	W	2	WNW	3	C	0
31	77.6	76.9	76.3	76.9	7.0	15.6	11.4	11.4	16.7	3.9	97	58	77	77	0.3	7.4	3.1	3.6	9	8 ⊙	10 ●	C	0	SW	7	W	3
M	75.4	75.0	75.2	75.2	12.1	18.2	13.0	14.4	19.7	8.1	92	66	89	82	1.2	7.9	1.8	3.9	6.8	7.6	5.1	0.9		3.3		1.0	

Jelenia Góra $H_s = 342\ m$ $H_b = 343{,}0\ m$ $h_w = 15\ m$ **Lipiec–Juillet 1957**

DNI	WI. DZIAŁ. WOŚC. V	OPAD R	GRUB. ŚNIE. GU h	USŁO. NECZ. NIENIE	POGODA
1	8	.	.	–	(K)^0 16^{55}–18^{55} W–SW. = 2^{00}–5^{40}; ⌒^{2} 0^{00}–10^{30}
2	7	.	.	–	⌒^{1} n/p – 24
3	9	.	.	–	= 2^{00}–4^{20}. ⌒^{2} 0^{00}–7^{40}
4	8	.	.	–	
5	7	.	.	–	(K) 16^{55}–17^{40} S-E; = 23^{30}–24
6	7	4.6	.	–	= 0^{00}–3^{15}, ⌒^{0} na – 7^{10}
7	8	.	.	–	(K) 2^{46}–5^{5} ▽^{0} K$_x$ – 6^{45} NW–SE
8	7	4.3	.	–	≤ 2^{00}–4^{00} (K) 7^{50}–10^{20} NW-E • K^0 14^{55}–16^{12} W-E ▽ 16^{50}–17^{42} (K) 18^{44}–19^{10} • ?^{0} 19^{10}–19^{50}–20^{45} SE-NW ≤ 22^{20}–23^{10}
9	8	0.4	.	–	≤ 2^{00}–4^{10} ▽ 4^{50}–5^{00} • ^{0} 8^{30} (K) 18^{52}–19^{06} • K^0 – 20^{04}
10	7	17.4	.	–	▽ 12^{00}–20 19^{20}–20^{30}, 22^{35}–24; (K)^0 17^{21} SW–S; = 0^{00}–8^{10}, 21^{10}–24
11	6	36.2	.	–	▽^{0} 0^{00}–3^{25} •^{1}–6^{50} ▽^{0}–7^{15} •^{1}–9^{30} •^{0}–10^{20} •^{1}–13^{35} •^{0}–17^{45} •^{1}–18^{30} •^{0}–19^{10} •^{1}–22^{35} •^{0}–23^{05} •^{2}–23^{10} •^{1} 24; = 0^{00}–24
12	6	0.3	.	–	•^{1} 0^{00}–10 •^{0}–6^{20} •^{1}–7^{15} •^{0}–8^{30} •^{0} 9^{46} 11^{35}; = 0^{00}–24
13	7	.	.	–	= 0^{00}–4^{43} ≡^{0}–7^{25} = –9^{35}, ⌒^{1} n – 24
14	8	9.7	.	–	(K) 10^{30}–40 S ▽ 10^{55} 11^{20} (K) 11^{40}–50 S •K^0–12^{36} ▽ 13^{50} 15^{10}–16^{15}; = 0^{00}–12^{10} ≡ 20^{45}–24 ⌒^{1} 0^{00}–8^{05} ⌒^{2} n – 24
15	6	10.2			•^{0} 10^{05} 11^{40} •^{2}K$_x^2$ 12^{30}–13^{36} ▽–13^{45} 16^{05}–40; ≡ 0^{00}–1^{30} ≡–4^{35} = –20^{10} ≡ –24; ⌒^{2} n
16	7	.	.	–	•^{0} 4^{16}. 7^{40}; ≡ 0^{00}–2^{40} = –11^{09}
17	8	0.0	.	–	▽ 16^{01}–20 ⌒^{2} n – 24
18	7	.	.	–	≡ 1^{50}–4^{45} = –10^{25}, 21^{20}–24; ⌒^{2} 0^{00}–9^{15}
19	7	0.0	.	–	= 0^{00}–5^{30}
20	6	11.3	.	–	▽ 3^{30}–45 10^{45} 12^{50}–14^{06} 16^{50}–18^{40} •^{0} 22^{40}–24; = 7^{15}–24
21	7	0.0	.	–	•^{0} 0^{00}–20, 4^{30} 5^{20} ▽ 16^{03}–15; = 0^{00}–12^{20}
22	6	45.9	.	–	•$^{0-1}$ 10^{35}–18^{48} ▽ 21^{50}–22^{25}; = 1^{20}–20^{50}
23	6	42.3	.	–	•^{0} 2^{00}–45 •^{1}–3^{40} •^{0} 4^{10}–5^{40} 6^{35}–7^{05} ▽–7^{50} •^{1} 8^{05}–11^{10} •^{0}–12^{20} 13^{30} •$^{0-1}$ 20^{15} •^{0} 20^{40}. 21^{20}–24; = 0^{00}–24; (K)^0 7^{32} W-SW
24	8	0.0	.	–	•^{0} 0^{00}–2^{00} 4^{15} 5^{40}–7^{45}; = 0^{00}–11^{35}
25	7	4.0	.	–	•^{0} 4^{06}–40 14^{45}–17^{30} ▽–19^{10} •^{1}–20^{45}; = 0^{00}–6^{20}
26	8	4.3	.	–	▽ 13^{40}–14^{20} •^{0} 15^{45} 16^{25}–19^{40} 22^{35} 23^{10}–24
27	8	8.6	.	–	•^{0} 0^{00}–2^{45} 4^{10} 4^{50}–6^{40} (K) 9^{40}–50 •K^0–10^{35} W-E ▽–11^{20}, 18^{52}–19^{15}, 19^{45}–21^{40}, 22^{35}–24
28	8	5.4	.	–	▽ 0^{00}–40 1^{15}–40 2^{10}–30 16^{45}–17^{04}
29	8	1.1	.	–	▽ 0^{00}–3^{30}, 4^{50}–5^{45} 15^{10}–25 17^{20}–35 18^{25}–30; = 5^{10}–10^{30}
30	7	6.8	.	–	•^{0} 6^{10} 7^{55} ▽ 12^{50}–13^{20} •^{0} 14^{25}–16^{20} 17^{15}, 19^{10}–24; = 17^{30}–24
31	7	0.1	.	–	•^{0} 0^{00}–3^{20} 4^{35}, 7^{10} 9^{40}; = 0^{00}–12^{15}
Σ	–	212.9	–	–	UWAGI.

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1	7	0.0	.	–	≡ 21^{30}–23^{20} = –24; ⌒^{1} n/p – 24
2	6	.	.	–	= 0^{00}–1^{45} ≡ –4^{20} ≡^{2}–6^{40} ≡–7^{30} = –14^{10}, ⌒^{1} 0^{00}–9^{15}
3	8	0.0	.	–	= 1^{15}–7^{15} ⌒^{2} 0^{20}–7^{30}
4	7	0.0	.	–	•^{0} 7^{50} 8^{10}; = 4^{10}–5^{45}, 10^{20}–12^{30}
5	8	.	.	–	= 3^{25}–5^{20} ≡–7^{10} = –8^{20} ≡ 22^{45}–24
6	8	.	.	–	≡ 0^{00}–20, 1^{15}–4^{30} ≡–7^{30}; ⌒^{2} 21^{05}–24
7	8	7.2	.	–	•^{0} 10^{38}–12^{15} (K) 20^{46}–21^{06} •K^0–21^{40} NW–E ▽–22^{15}; ⌒^{2} 0^{00}–9^{20}
8	7	.	.	–	= 1^{20}–3^{35}, 5^{20}–6^{35} 11^{30}–12^{50} ≡ 21^{30}–24; ⌒^{1} 20^{40}–24
9	7	23.2	.	–	≡ 0^{00}–3^{20} = 5^{40}–9^{15}; ≤ 23^{45}–24 NW; ⌒^{2} 0^{00}–7^{40}
10	8	0.4	.	–	▽ 0^{40}–1^{15}, 2^{58}–7^{40}, 12^{56}–13^{08}, 13^{15}–28, 14^{51}–15^{12}, 16^{10}–26; ≤ 0^{00}–45 K$_x^1$–1^{40} NW–S
11	9	1.1	.	–	⌒^{1} 3^{25}–7^{40}
12	8	.	.	–	1^{46}–3^{38} 5^{48}–7^{20}; ⌒^{0} 20^{00}–24
13	8	2.1	.	–	•^{0} 22^{10}–35, 23^{15}–50; = 3^{25}–6^{30}, ⌒^{1} 0^{00}–8^{35}
14	7	2.4	.	–	▽ 2^{08}–30 2^{53}–3^{35}, 18^{50}–19^{30}; = 4^{20}–9^{30}, 20^{20}–24
15	7	0.5	.	–	= 0^{00}–10^{40}
16	7	4.6	.	–	•^{0} 7^{30}–8^{10} 10^{20}–13^{35} ▽ 16^{26}–41; ⌒^{2} 20^{25}–24
17	8	1.2	.	–	▽ 14^{40}–50 15^{15}–16^{30}; ⌒^{2} 0^{00}–8^{25}
18	7	4.4	.	–	•^{1} 8^{45} 9^{12} 12^{20}–30 15^{40}–16^{08}, 16^{50}–18^{15}; = 19^{45}–20^{27} ≡^{0}–21^{45} = –24; ⌒^{0} 1^{20}–8^{45}
19	7	.	.	–	= 0^{00}–2^{10} ≡ –3^{30} = –13^{30}, 20^{20}–24
20	8	0.6	.	–	= 0^{00}–8^{30}
21	7	3.2	.	–	•^{0} 2^{25} 4^{40} 7^{10}–8^{15} ▽ 20^{10}–15 20^{20}–22^{35} •^{0}–24
22	7	2.0	.	–	•^{0} 0^{00}–3^{40}, 4^{45} ▽ 7^{25}–35 ▲ 13^{50}–59 ▽ 14^{06}–15; = 4^{15}–9^{45}
23	9	.	.	–	= 2^{00}–5^{30} ≡^{1}–6^{45} = –8^{20}; ⌒^{2} n – 9^{10}, 21^{20}–24
24	8	10.9	.	–	▽ 15^{51}–17^{40}, 18^{53}–19^{10}; K^0 16^{24}–55 W–E; ≫ 16^{06}–20; = 22^{20}–24 ⌒^{2} 0^{00}–9^{15}
25	6	.	.	–	= 0^{00}–2^{40} ≡ –3^{35} = –4^{50} ≡ 5^{30}–6^{15}; ⌒^{2} n/p – 9^{10}
26	8	0.5	.	–	▽ 13^{55}–14^{10}, 19^{32}–37, 19^{40}–45; (K)^0 16^{10} SW; ⌒ 19^{35}–50
27	8	1.8	.	–	•^{0} 21^{45}–24
28	7	1.0	.	–	•^{0} 0^{00}–10–3^{20} 6^{20} 11^{45}–13^{35}, 13^{40}–14^{40} 19^{09}–31 21^{50}–22^{15}; = 20^{35}–24
29	7	.	.	–	= 0^{00}–30 ≡ –1^{45} ≡–5^{40} = –10^{30}; ⌒^{2} na – 9^{15}
30	7	.	.	–	= 22^{40}–24; ⌒^{2} n – 11^{00}
31	7	0.8	.	–	•^{0} 9^{50}. 10^{40}, 11^{20}–30 ▽ 21^{25}–23^{10}; ≤ 20^{48}–21^{35}; = 0^{00}–2^{20}
Σ	–	69.9	–	–	UWAGI.

Jelenia Góra $\varphi = 50°54'$ $\lambda = 15°48'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			ELEWACJA I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dias	I	II	III	Dias	Max	Min	I	II	III	Dias	I	II	III	Dias	I	II	III	I	II	III
1	77.4	78.2	78.6	78.1	10.6	14.0	6.2	9.2	15.2	5.6	79	60	97	79	2.8	6.4	0.3	3.2	9	9	1	W 5	⚲ 6	C 0
2	76.9	75.6	74.9	75.8	5.3	14.6	11.3	10.6	17.5	1.7	97	77	99	91	0.3	3.8	0.2	1.4	8	10	9	SW 1	C 0	☾ 0
3	75.4	76.4	78.3	76.7	12.3	13.3	9.3	11.0	14.4	8.5	92	79	97	89	1.2	3.2	0.3	1.6	9 ●	9	9	W 2	WSW 4	C 0
4	80.4	82.1	83.6	82.0	9.3	15.4	6.8	9.6	16.2	6.1	95	62	97	85	0.6	6.7	0.3	2.5	10	8	0	NW 1	WNW 2	C 0
5	82.9	80.0	78.5	80.5	2.8	17.8	13.0	11.6	19.0	1.6	98	45	85	76	0.2	11.2	2.3	4.6	0	4 ⊙	8	C 0	W 3	SW 1
6	78.2	78.2	79.2	78.5	12.3	19.0	12.6	14.1	19.2	10.7	95	69	100	88	0.7	6.8	0.0	2.5	9	10	9	C 0	C 0	C 0
7	79.1	78.6	78.5	78.7	9.7	23.1	12.1	14.2	23.9	8.2	100	48	96	81	0.0	14.7	0.5	5.1	4 ⊙	4 ⊙	1	C 0	SW 3	C 0
8	79.0	79.1	79.4	79.2	11.3	27.2	15.2	17.2	27.8	8.1	98	51	94	81	0.4	17.8	1.0	6.4	2	2 ⊙	0	C 0	E 2	C 0
9	79.2	82.0	84.3	81.8	12.0	19.1	14.0	14.8	23.7	10.8	98	78	90	87	0.3	4.8	1.6	2.2	1 ⊙	9	10	C 0	W 4	WNW 2
10	83.4	81.0	78.4	80.9	11.0	18.0	12.0	13.2	18.9	9.6	99	64	98	87	0.1	7.4	0.3	2.6	10	8	10	C 0	WNW 1	C 0
11	74.2	69.1	62.1	68.5	6.2	17.6	16.3	14.2	18.4	4.9	100	63	76	80	0.0	7.3	4.6	4.0	0	10	9	C 0	S 2	SW 5
12	56.9	60.2	63.3	60.8	16.4	15.4	11.3	13.6	18.2	11.0	78	59	66	68	4.0	7.2	4.3	5.2	7	8	3	SW 6	W 8	SW 5
13	67.3	65.9	62.9	65.4	10.1	13.7	10.3	11.2	15.1	8.7	70	57	79	69	3.8	6.7	2.7	4.4	4	8	9 ●	SW 5	SSW 6	SW 8
14	65.9	66.9	67.0	66.5	9.5	13.2	10.4	10.9	14.4	6.8	68	57	71	65	3.9	6.6	3.6	4.7	3 ⊙	8 ⊙	6	SW 7	SW 8	SW 4
15	67.0	69.9	74.1	70.3	8.7	10.5	9.1	9.4	11.9	6.1	76	81	79	79	2.7	2.4	2.2	2.5	10	9 ●	0	SW 3	WNW 6	W 3
16	74.8	75.3	77.9	76.0	8.2	10.7	4.7	7.1	11.4	3.7	77	64	93	79	2.6	4.6	0.4	2.5	9	9	2	SW 3	SW 5	C 0
17	77.8	76.8	76.3	77.0	9.2	12.3	7.4	9.1	13.4	3.8	77	60	88	75	2.6	5.8	1.2	3.2	9	7	10	W 5	W 7	C 0
18	75.0	75.9	75.4	75.4	9.0	11.4	5.6	7.9	13.4	5.1	93	80	97	91	0.7	2.7	0.3	1.2	10 ●	9	0	W 4	W 6	C 0
19	71.3	69.3	68.9	69.8	5.4	13.1	14.7	12.0	15.8	0.7	97	87	74	86	0.3	1.9	4.3	2.2	9	10 ●	10	C 0	WSW 3	W 4
20	70.5	73.2	75.2	73.0	9.9	13.9	8.0	10.0	14.8	7.5	86	66	94	82	1.8	5.4	0.6	2.6	8	4 ⊙	2	WNW 2	NW 1	C 0
21	76.1	75.0	73.7	74.9	3.8	15.7	10.1	9.9	18.2	2.4	100	65	99	88	0.0	6.2	0.2	2.1	0	8	5	C 0	N 1	C 0
22	71.2	71.7	70.7	71.2	11.9	17.4	16.0	15.3	19.0	7.4	99	75	78	84	0.1	4.9	4.0	3.0	7	10	2	C 0	WSW 4	S 4
23	65.2	60.0	64.6	63.3	16.5	16.5	13.9	15.2	17.6	13.5	77	85	83	81	4.4	3.3	2.7	3.5	9	10 ●	10 ●	SSW 4	SW 3	W 12
24	67.3	65.4	72.9	68.5	12.4	14.7	6.2	9.9	15.8	5.3	87	81	85	84	1.9	3.1	1.5	2.2	8	10 ●	0	W 1	NW 3	WNW 1
25	77.1	79.0	79.5	78.5	3.5	9.6	1.6	4.1	11.9	0.7	91	54	96	80	0.6	5.5	0.3	2.1	3	3	0	C 0	W 5	C 0
26	75.6	75.5	79.0	76.7	3.4	8.1	1.0	3.4	10.0	0.5	97	66	96	86	0.3	3.7	0.3	1.4	10	9	0	C 0	E 3	C 0
27	80.7	78.1	71.4	76.7	-2.2	10.4	10.4	7.2	11.4	-3.5	100	56	62	73	0.0	5.6	4.8	3.5	5	8 ⊙	10	C 0	W 5	W 10
28	70.6	70.1	70.4	70.4	9.5	12.0	10.1	10.4	12.5	8.5	82	67	83	77	2.2	4.6	2.1	3.0	9	9	6	W 10	WNW 12	W 10
29	65.5	61.4	62.3	63.1	10.7	11.0	7.6	9.2	11.7	7.4	81	81	86	83	2.5	2.4	1.4	2.1	10 ●	10 ●	10 ●	W 7	WSW 6	W 4
30	67.6	70.9	75.5	71.3	4.5	7.4	1.2	3.6	9.1	0.6	84	65	96	82	1.3	3.6	0.3	1.7	6	9	0	W 7	W 5	C 0
31																								
M	73.6	73.3	74.0	73.6	8.8	14.3	9.6	10.6	16.0	5.7	89	67	88	81	1.4	5.9	1.6	3.0	6.7	8.0	5.0	2.4	4.2	2.4

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1	76.6	77.2	79.9	77.9	0.3	9.2	4.0	4.4	9.6	-2.1	96	60	92	83	0.2	4.6	0.6	1.8	4 ⊙	7 ⊙	9	S 2	NW 3	C 0
2	82.6	83.5	82.8	83.0	2.3	7.2	-0.2	2.3	8.9	-1.3	96	80	96	91	0.3	2.1	0.2	0.9	10 ●	9	10 ≡	C 0	C 0	C 0
3	77.3	74.7	73.5	75.2	-2.4	10.7	8.6	6.4	12.0	-4.1	93	44	76	71	0.3	7.3	2.8	3.5	4	9	10	C 0	WSW 5	W 5
4	75.1	78.3	82.6	78.7	5.7	6.2	5.4	5.7	8.9	3.6	80	82	80	81	1.9	1.7	1.8	1.8	9	7	6	WSW 7	WSW 6	W 4
5	84.0	82.2	80.3	82.2	2.9	11.3	4.6	5.9	11.7	2.1	93	45	84	74	0.3	7.3	1.4	3.1	7	2	7	W 2	SW 4	C 0
6	81.0	82.6	83.7	83.1	8.4	10.4	7.3	8.4	11.6	1.3	83	86	94	88	1.8	1.8	0.6	1.4	10	9	7	W 4	W 6	C 0
7	85.9	85.4	85.6	85.6	4.9	13.3	10.3	9.8	13.8	3.4	94	78	95	89	0.6	3.3	0.7	1.5	2 ⊙	10	10	C 0	NW 2	C 0
8	86.4	85.6	85.3	85.8	4.8	15.9	9.1	9.7	17.2	4.0	98	65	92	85	0.1	6.3	1.0	2.5	7	0 ⊙	0	C 0	E 4	E 1
9	83.3	82.2	81.3	82.3	1.6	20.1	7.1	9.0	20.3	-0.1	100	43	96	80	0.0	13.5	0.3	4.7	0 ⊙	0 ⊙	0	C 0	ESE 3	C 0
10	80.4	79.7	80.0	80.0	1.0	20.2	7.4	9.0	20.9	0.1	96	51	97	81	0.3	11.7	0.3	4.1	0	0 ⊙	1	C 0	E 2	SE 1
11	80.0	79.3	80.0	79.8	3.3	19.7	6.6	9.0	20.3	-1.0	97	48	97	81	0.2	12.0	0.3	4.2	3 ⊙	0 ⊙	0	C 0	SE 2	C 0
12	80.3	83.3	86.9	83.6	4.0	12.7	10.7	9.3	14.4	3.1	97	92	96	95	0.2	1.2	0.3	0.6	5	10	10 ●	SE 1	WNW 4	C 0
13	86.8	85.0	83.7	85.2	10.1	18.3	5.3	9.8	18.9	4.7	99	51	97	82	0.2	10.3	0.3	3.6	10 ≡	2	0	C 0	C 0	C 0
14	85.2	84.7	86.9	84.9	4.8	10.2	9.2	8.4	12.3	1.0	98	96	95	96	0.1	0.4	0.6	0.4	9	10	10	C 0	NW 1	C 0
15	87.9	87.0	86.4	87.1	5.3	12.3	4.0	6.4	13.7	2.1	100	60	97	86	0.0	5.8	0.2	2.0	10	5	0	C 0	C 0	C 0
16	84.0	81.1	79.0	81.4	0.0	16.4	6.2	7.2	18.8	-0.6	100	54	93	83	0.0	8.6	0.5	3.0	10 ≡	0 ⊙	0	C 0	SE 1	C 0
17	78.1	79.9	79.8	79.3	3.7	13.9	6.1	7.4	15.4	0.7	97	70	97	88	0.3	4.7	0.3	1.8	8	9	0	SE 1	W 4	C 0
18	74.1	73.1	71.8	73.0	14.3	18.6	17.0	16.7	18.8	4.8	77	61	61	66	3.8	8.3	7.6	6.6	10 ●	8	0	SW 2	SW 4	S 6
19	70.6	69.0	66.9	68.8	10.6	20.0	12.8	14.0	20.7	9.6	86	50	80	72	1.8	11.6	2.9	5.4	7 ⊙	6 ⊙	2	NE 2	WSW 6	E 1
20	72.0	74.9	77.3	74.7	7.9	8.8	6.0	7.2	13.2	5.6	97	90	97	95	0.2	1.1	0.3	0.5	10 ●	10	8	NW 1	NW 1	C 0
21	77.1	74.3	70.8	74.1	1.2	12.9	2.2	4.6	13.0	0.3	100	52	89	80	0.0	7.1	0.8	2.6	10 ≡	3	0	C 0	C 0	C 0
22	64.8	61.5	63.3	63.2	-1.3	13.3	5.4	5.8	13.7	-2.7	98	51	84	78	0.1	7.6	1.4	3.0	3 ⊙	3 ⊙	10	C 0	SW 2	C 0
23	69.0	72.1	75.1	72.1	6.3	9.0	0.0	5.8	9.3	-0.4	86	63	96	82	1.2	4.2	0.2	1.9	10	7	0	WNW 2	WNW 5	C 0
24	74.3	77.4	82.3	78.1	3.7	9.0	9.0	7.7	9.9	-1.1	83	76	89	83	1.4	2.8	1.3	1.8	10	10 ●	10	SE 1	SW 4	W 1
25	84.6	84.4	84.7	84.6	5.1	13.9	3.6	6.6	14.9	3.3	97	98	100	85	0.3	6.7	0.0	2.3	4	3	0	C 0	ENE 2	C 0
26	83.2	81.7	80.3	81.7	-0.9	14.7	2.2	4.6	16.0	-1.9	100	55	98	84	0.0	7.5	0.2	2.6	0	0 ⊙	0	C 0	C 0	C 0
27	79.3	78.0	78.8	78.7	0.4	7.3	1.3	2.6	11.5	-2.1	100	91	96	96	0.0	0.9	0.2	0.4	10 ≡	5 ⊙	10 ≡	C 0	[illegible]	C 0
28	[illegible]	78.8	79.3	79.2	1.4	11.3	1.6	4.0	12.2	-2.0	100	63	96	86	0.0	3.0	0.3	1.8	8	3	0	C 0	W 1	C 0
29	78.[illegible]	78.0	77.1	77.9	1.0	13.8	1.6	7.3	14.8	-2.4	96	54	89	80	0.3	7.4	1.2	3.0	6	5	9	C 0	WSW 1	NW 1
30	75.3	74.3	75.9	75.2	4.0	16.1	8.0	9.0	16.3	2.7	97	53	89	80	0.2	8.6	1.2	3.3	7	9	4	C 0	C 0	C 0
31	76.1	74.3	71.0	73.8	0.3	13.9	5.8	6.4	14.3	-1.4	98	60	94	84	0.1	6.4	0.6	2.4	1	8	5	C 0	WNW 2	C 0
M	79.1	78.8	79.2	79.0	3.7	13.3	6.3	7.4	14.4	0.9	93	64	91	83	0.3	6.1	1.0	2.5	6.6	5.5	4.9	0.8	2.9	0.6

Jelenia Góra $H_s = 342$ m $H_b = 343{,}0$ m $h_w = 15$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBŚNIENIE GU h	USŁONECZNIENIE	POGODA
1	8	0.0	.	–	▽ 1 42 – 2 40 3 43 – 4 10 4 30 – 5 13 · = 22 20 – 23 45 ≡° – 24 · ⌒¹ n – 24
2	7	2.1	.	–	• ° 11 52 13 30 16 20 17 10 – 20 40 · ≡° 0 00 – 5 40 = – 10 20 · 21 20 – 24 · ⌒² 0 00 – 9 50
3	7	2.5	.	–	• ° 2 12 3 45 ▽ 7 48 – 8 40 14 55 – 15 15 · = 0 00 – 10 20 · 23 35 – 24
4	8	0.1	.	–	= 0 00 – 10 20 ≡ 20 15 – 24 · ⌒² n – 7 20 20 40 – 24
5	8	0.6	.	–	• ° 18 03 – 10 19 40 – 20 10 · ≡ 0 00 – 2 40 = – 3 40 ≡° – 4 20 ≡° – 7 45 ≡ – 8 40 = – 10 20 · ⌒² 0 00 – 10 20
6	7	1.7	.	–	• ° 4 25 – 6 33 ▽ 14 50 – 15 25 16 05 – 35 · = 6 33 – 9 15 ≡° 19 45 – 24
7	8	.	.	–	≡° 0 00 – 7 40 = – 10 30 ≡ 20 35 – 24 · ⌒² 20 30 – 24
8	8	.	.	–	≡ 0 00 – 5 20 2 20 – 23 10 · ⌒² 0 00 – 10 15 · 20 20 – 24
9	7	7.9	.	–	▽ 22 33 – 23 10 • °– 24 · ≡ 4 35 – 8 25 = 14 40 – 22 10 · ⌒² 0 00 – 9 30
10	8	0.0	.	–	• ° 0 00 – 3 40 ▽ 3 52 – 4 10 · = 5 30 – 10 35 · 20 15 – 24 · ⌒¹ n – 24
11	8	2.1	.	–	• ° 17 40 18 20 19 40 – 20 35 21 10 · ▽ 21 20 – 50 · = 0 00 – 1 35 ≡°– 8 40 = – 9 20 · ⌒² 0 00 – 10 00
12	9	4.1	.	–	• ° 6 48 7 20 ⊠¹ 10 40 – 11 03 SW – NE ▽ – 11 15 · ≫ 10 40 – 12 20 por. ponad 15 m/sek 10 45 – 11 03 13 40 – 15 30 por. ponad 10 m/sek
13	8	3.1	.	–	▽ 16 45 – 18 36 · 21 40 – 24 **12. IX:** 20 10 – 21 15
14	8	.	.	–	▽ 0 00 – 35
15	8	0.4	.	–	• ° 9 45 11 35 13 55 – 14 10 15 50 – 16 10 16 15 – 25 · = 5 20 – 7 10 · ⊕ 15 40 – 16 20
16	8	4.2	.	–	• ° 6 10 .. 30 ▽ 14 01 – 15 14 50 – 15 15 · 18 15 – 40
17	8	1.1	.	–	• ° 0 30 2 00 – 4 25 5 40
18	6	1.0	.	–	• ° 4 45 5 30 6 10 7 10 7 30 9 20 – 10 10 ▽ 11 46 – 54 · 13 10 – 23 · = 12 20 – 15 15 · 21 15 – 24
19	7	2.8	.	–	• ° 8 20 – 14 35 · 22 56 · 23 20 – 24 · ≡° 0 00 – 6 15
20	8	.	.	–	• ° 0 00 – 2 00 · 5 45 · ⌒¹ 20 10 – 23 10 · ⌒² – 24
21	7	2.9	.	–	≡¹ 1 45 – 8 45 = – 9 30 · 18 30 – 24 · ⌒² 0 00 – 10 15
22	7	.	.	–	• ° 4 18 – 6 30 · = 0 00 – 11 20 · 18 20 – 20 15
23	8	5.0	.	–	▽ 8 50 – 9 00 • ° 10 04 11 10 12 25 – 13 15 ▽ 13 45 · 16 25 · 18 50 – 19 20 21 40 – 22 15 por. wiatru ponad 10 m/sek 15 45 – 16 05
24	6	5.6	.	–	▽ 2 50 – 3 40 · 4 15 – 20 • ° 11 45 13 30 ▽ – 15 40 • °– 16 25 • ¹ – 17 40 · ≫ 0 00 – 3 50¹
25	8	.	.	–	**23. IX:** 16 15 – 17 10 · 19 15 – 20 20 ≫ 20 20 – 24
26	8	.	.	–	= 18 45 – 24 · ⌒¹ n – 8 25
27	8	2.2	.	–	▽ 17 10 – 45 · ≫ 21 30 – 24 · ⌒² n – 9 12
28	7	3.7	.	–	• ° 0 00 – 4 35 ▽ 6 50 – 7 10 14 10 – 48 · 16 04 – 10 · 18 40 – 19 38 · ≫ 0 00 – 13 30 (por. do 20 m/sek 0 00 – 3 40) · 19 18 – 24
29	8	6.2	.	–	• ° 1 25 2 30 – 10 12 · 15 30 ▽ 15 34 – 17 40 · 18 15 – 35 · 19 46 – 22 40 · ≫ 0 00 – 1 45
30	8	.	.	–	≡ 19 45 – 24
31					
Σ	–	59.3	–	–	UWAGI.

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1	7	0.0	.	–	≡ 0 00 – 5 15 · ⌒¹ 0 20 – 7 40
2	6	0.2	.	–	• ° 6 45 7 40 8 30 10 15 • ° 10 30 11 18 · ≡ 0 00 – 2 30 = – 5 20 · 7 30 – 13 10 · 18 40 – 20 35 ≡¹ – 24
3	8	0.0	.	–	• ° 19 45 – 20 05 · ≡¹ 0 00 – 5 45 = – 9 30
4	8	0.3	.	–	▽ 7 00 – 10 · 7 40 – 50 · 8 15 – 25 · 9 56 – 10 15 · 12 05 – 10 · 12 25 – 35 · 14 10 – 20 · por. wiatru ponad 10 m/sek 6 20 – 13 40
5	8	0.6	.	–	⌒° n
6	6	0.9	.	–	• ° 3 25 4 35 7 40 – 8 45 · = 9 20 – 24 · ⌒² 19 20 – 24
7	7	.	.	–	= 0 00 – 8 20 · 16 20 – 24 · ⌒² 0 00 – 11 50
8	7	0.0	.	–	= 0 00 – 1 35 ≡° – 5 40 = – 6 50 ≡° – 8 10 = – 11 20 ≡ 20 30 – 22 45 ≡° – 24 · ⌒² na – 8 20
9	7	.	.	–	≡° 0 00 – 6 40 = – 10 15 · 20 48 – 24 · ⌒¹ 4 30 – 8 20
10	8	.	.	–	= 0 00 – 5 45 ≡° – 6 40 = – 8 25 ≡ 17 35 – 24 · ⌒° 3 05 – 8 10
11	7	.	.	–	≡ 0 00 – 7 40 = – 8 40 · 18 30 – 24 · ⌒° 3 10 – 6 40
12	6	0.0	.	–	• ° 20 40 – 21 15 • °– 23 50 · = 0 00 – 24 · ⌒² np – 8 10
13	6	.	.	–	= 0 00 – 4 40 ≡° – 8 45 = 17 40 – 21 10 ≡ – 24 · ⌒¹ 19 20 – 24
14	3	0.0	.	–	≡ 0 00 – 3 25 = 7 20 – 12 46 ≡° – 15 40 = – 22 40 ≡° – 24 · ⌒¹ 0 00 – 10 00
15	7	0.0	.	–	≡° 0 00 – 10 50 = – 12 30 ≡¹ 20 35 – 24 · ⌒² n – 9 00
16	7	0.0	.	–	≡ 7-0 00 – 8 20 ≡° – 9 40 = – 12 25 · 18 20 – 24 · ⌒² 20 00 – 24
17	8	0.0	.	–	= 0 00 – 8 20 · ⌒² 0 00 – 9 10 · ⌒° 19 15 – 24
18	7	0.0	.	–	• ° 6 45 – 9 25 · ⌒° 0 00 – 6 45
19	8	0.9	.	–	
20	6	2.0	.	–	• ° 5 10 – 11 30 · 12 20 · = 6 10 – 19 30 · 20 40 – 21 45 ≡° – 24
21	8	.	.	–	≡¹ 0 00 – 20 ≡¹ – 8 40 ≡° – 9 38 = – 10 08
22	8	0.3	.	–	⌒² 1 20 – 9 20
23	7	.	.	–	• ° 3 55 – 6 10 · = 6 10 – 11 20
24	7	0.0	.	–	• ° 10 35 – 11 35 · 12 15 – 13 40 15 30 – 16 45
25	8	.	.	–	≡¹ 6 40 – 8 40 = – 9 20 ≡¹ 20 45 – 22 40 ≡ – 24
26	7	.	.	–	≡¹ 1 00 – 7 45 = – 11 20 · 17 20 – 22 50 ≡° – 24 · ⌒° 20 20 – 24
27	5	0.0	.	–	≡° 0 00 – 5 40 ≡¹ – 10 20 = – 17 20 ≡ – 19 40 ≡° – 20 30 ≡¹ – 24 · ⌒¹ 0 00 – 8 05
28	7	0.0	.	–	≡¹ 0 00 – 6 25 ≡° – 8 40 = – 12 25 · ⌒° 0 40 – 5 25 ⌒¹ 21 15 – 24
29	8	.	.	–	= 0 50 – 1 30 ≡° – 2 40 ≡° – 3 45 = – 8 20 · ⌒¹ 0 00 – 9 10
30	7	.	.	–	= 20 35 – 24 · ⌒¹ np – 24
31	6	.	.	–	= 0 00 – 10 20 · 12 30 – 14 30 ≡ 19 25 – 20 40 · ⌒² 0 00 – 10 20
Σ	–	5.4	–	–	UWAGI.

Jelenia Góra — φ = 50°54' — λ = 15°48' — Listopad – Novembre 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	66.5	66.4	68.7	67.2	3.7	12.0	11.0	9.4	13.9	1.0	92	57	72	74	0.7	6.0	3.7	3.5	3	6	9	C 0	W 8	SW 4
2	71.2	72.2	73.6	72.3	5.4	9.0	5.8	6.5	11.4	4.3	91	61	82	78	0.9	4.5	1.7	2.4	8	10	9	C 0	C 0	C 0
3	74.4	72.3	71.3	72.7	−0.9	11.7	2.1	3.8	11.8	−2.3	94	57	95	82	0.3	5.9	0.4	2.2	3	9	1	C 0	NE 1	C 0
4	70.8	70.0	71.1	70.6	−1.3	15.5	8.6	7.8	15.8	−2.9	100	51	77	76	0.1	8.7	2.6	3.8	0	8	4	C 0	ESE 2	C 0
5	65.8	63.9	65.2	65.0	11.5	15.0	9.0	11.1	16.0	2.4	67	51	75	65	4.6	8.2	2.8	5.2	5	9	6	SE 12	SE 8	C 0
6	66.3	66.7	64.3	65.8	3.2	14.9	13.1	11.1	15.0	1.6	97	58	74	76	0.3	7.0	4.0	3.8	8	8	8	C 0	E 3	SE 3
7	62.7	65.7	67.1	65.2	10.3	12.4	9.2	10.3	15.3	7.4	81	86	95	87	2.4	2.0	0.6	1.7	10	10	10 ●	SE 2	C 0	C 0
8	64.7	64.6	65.3	64.9	11.2	12.6	11.8	11.8	15.3	7.4	85	78	84	82	2.0	3.2	2.1	2.4	10	8	10 ●	NE 5	ESE 8	E 4
9	63.2	63.8	66.7	64.6	10.8	12.3	11.1	11.3	12.6	8.4	85	78	80	82	1.5	3.2	2.6	2.4	10 ●	10	8	ENE 4	SE 4	SE 2
10	67.3	66.2	68.7	67.3	1.8	13.4	10.9	9.2	14.1	1.2	98	64	74	79	0.2	5.5	3.4	3.0	2	2	6	C 0	E 6	E 7
11	70.8	73.4	76.3	73.5	7.8	8.4	7.6	7.8	13.8	6.8	91	87	86	88	0.9	1.4	1.4	1.2	10 =	10 ●	10	NE 5	ENE 4	E 5
12	80.3	83.2	85.9	83.1	4.7	5.0	3.4	4.1	7.7	3.0	97	95	98	97	0.2	0.4	0.1	0.2	10 ●	10	10 ●	ENE 5	ENE 3	ENE 3
13	87.0	87.2	87.3	87.2	1.9	1.4	0.4	1.0	3.8	0.1	76	70	84	77	1.7	2.1	1.0	1.6	10	10	10	NE 3	E 2	E 3
14	87.0	87.2	88.1	87.4	−2.2	0.6	−3.3	−2.0	1.0	−3.8	85	77	90	84	0.8	1.5	0.5	0.9	7	3	4	E 4	ENE 3	E 2
15	87.8	88.0	87.6	87.8	−1.7	−0.4	−1.2	−1.1	−0.2	−3.9	96	100	95	97	0.2	0.0	0.3	0.2	10 ≡	10 ≡	10 ≡	C 0	C 0	C 0
16	88.0	88.3	89.1	88.5	−2.6	2.1	1.0	0.4	3.6	−3.9	93	96	96	93	0.3	0.3	0.3	0.3	10 ≡	10	10	C 0	C 0	C 0
17	88.4	87.3	88.7	88.2	−0.2	3.8	−1.0	0.9	6.4	−2.4	100	76	96	91	0.0	2.2	0.3	0.8	10 ≡	7	0	C 0	E 3	C 0
18	88.6	87.8	88.6	88.3	0.0	3.8	1.9	1.9	4.3	−3.4	90	69	80	80	0.6	2.5	1.4	1.5	10	3	10	C 0	C 0	C 0
19	88.6	90.0	92.2	90.3	1.6	2.6	0.4	1.2	4.3	0.0	71	63	73	69	2.1	2.7	1.7	2.2	10	9	10	SE 2	ESE 3	E 4
20	92.7	93.3	94.6	93.6	−1.0	2.3	0.0	0.4	3.4	−1.7	83	63	79	75	1.0	2.7	1.3	1.7	8	2	0	ESE 3	C 0	E 6
21	93.4	90.7	87.3	90.5	1.1	6.8	−2.7	0.6	6.9	−3.9	70	49	84	68	2.0	3.1	0.8	2.6	1	0	0	SE 7	SE 6	C 0
22	81.0	76.7	75.4	78.0	−1.2	4.8	−1.6	−0.6	5.1	−3.3	87	53	80	73	0.6	4.0	1.0	1.9	0	0 ⊙	4	C 0	C 0	WSW 1
23	76.5	77.9	82.6	79.0	0.7	4.0	3.2	2.8	3.9	−3.3	78	70	79	76	1.4	2.4	1.6	1.8	10	9	9	SW 4	WSW 5	W 9
24	84.4	84.3	83.9	84.2	1.7	4.3	4.3	3.7	5.3	0.4	85	73	84	81	1.0	2.3	1.4	1.6	8	9 ⊙	10	W 8	W 9	W 8
25	82.8	82.0	84.1	83.0	3.1	4.8	5.0	5.0	5.6	3.6	86	94	94	91	1.3	0.6	0.3	0.8	10	10 ●	10 9	W 7	W 7	W 7
26	84.6	84.2	83.4	84.1	4.8	6.2	4.8	5.2	6.3	4.1	94	88	86	89	0.6	1.2	1.2	1.0	10	10	10 ●	NW 7	W 2	WSW 8
27	80.3	80.0	80.7	80.3	5.5	6.3	7.2	6.6	7.3	3.8	86	89	86	87	1.2	1.0	1.3	1.2	10	10	10	W 7	W 8	W 8
28	79.0	76.5	72.3	75.9	6.8	7.6	7.3	7.2	8.3	6.4	94	80	91	88	0.6	2.0	0.9	1.2	10 ●	10 ●	10 ●	W 6	W 8	W 9
29	71.7	76.4	81.0	77.4	4.6	−0.2	−2.4	−0.1	7.8	−2.8	84	69	76	76	1.4	1.9	1.2	1.5	9	5	4	WNW 10	N 9	N 12
30	91.4	90.2	90.0	90.5	−1.4	−4.7	−4.0	−6.0	−1.9	−12.6	75	76	82	78	0.6	1.0	0.8	0.8	0	10 ✳	9	C 0	NW 1	NW 3
31																								
M	78.6	78.6	79.5	78.9	2.6	6.7	4.1	4.4	8.1	0.3	87	73	84	81	1.0	3.0	1.4	1.8	7.4	7.4	7.4	3.4	3.8	3.7

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1	89.9	89.1	86.8	88.6	−6.7	−3.5	−3.5	−4.3	−2.6	−8.6	86	74	85	82	0.5	1.2	0.7	0.8	8	9	10 ✳	C 0	W 1	W 4
2	84.9	85.2	86.3	85.5	−2.8	0.0	0.0	−0.7	0.3	−4.2	97	96	98	97	0.1	0.2	0.1	0.1	10 ✳	10 △	10 △	W 1	WNW 2	WNW 1
3	84.8	81.7	82.4	82.7	0.3	0.8	1.0	0.8	1.2	−0.4	98	96	100	98	0.1	0.3	0.0	0.1	10 ✳	10 ≡ 9	10 ●	W 2	C 0	W 1
4	83.2	83.3	83.2	83.2	0.6	1.1	1.8	1.5	2.0	0.3	100	94	87	94	0.0	0.4	0.9	0.4	10 ⁑	10 ⁑	10 9	NW 3	W 2	W 4
5	81.9	82.1	84.9	83.0	1.8	3.4	3.2	2.9	3.4	1.1	96	86	86	89	0.3	1.1	1.1	0.8	10 ●	9	10	W 2	W 3	W 3
6	83.3	84.7	81.8	84.0	1.6	2.4	−3.4	−0.7	3.8	−4.4	89	77	95	87	0.8	1.7	0.3	0.9	18	7	0	WNW 3	WNW 1	C 0
7	72.1	71.2	69.7	70.7	−6.7	1.7	−2.4	−2.4	3.4	−7.9	93	65	89	84	0.0	2.4	0.3	1.0	7	2 ⊙	9	C 0	E 3	C 0
8	52.4	43.4	43.6	47.2	4.0	5.2	6.8	5.7	8.7	−2.9	70	73	63	69	2.4	2.3	3.7	2.8	10	10 ●	9	W 9	SW 9	W 17
9	41.8	51.4	59.5	50.6	6.1	2.8	−0.7	1.9	7.2	−1.3	77	67	83	76	2.1	2.3	1.0	1.9	9 ●	7	3	W 10	W 9	W 3
10	57.2	39.8	68.1	61.7	−3.3	1.0	−7.4	−4.3	2.4	−8.4	88	80	85	84	0.6	1.3	0.5	0.8	10	8	0	W 2	W 7	C 0
11	63.3	60.0	55.4	59.6	−9.9	1.8	1.6	−1.2	2.2	−13.8	88	69	72	76	0.4	2.2	1.9	1.5	6	8	3	C 0	SE 4	SE 2
12	54.1	54.4	52.7	53.7	−3.2	7.6	6.4	3.8	8.2	−3.9	93	66	81	80	0.3	3.3	1.9	1.9	8	3	0	C 0	E 2	SE 1
13	50.5	47.8	43.1	47.1	3.2	9.5	2.3	4.3	10.2	1.1	97	71	96	88	0.3	3.4	0.3	1.3	9	10	10 ●	C 0	C 0	WNW 1
14	45.0	51.8	60.3	52.4	0.3	−0.1	−1.6	−0.8	3.1	−2.0	98	96	96	97	0.1	0.3	0.2	0.2	10	10 ✳	10 ✳	NW 4	NW 1	NW 2
15	71.6	77.8	82.4	77.3	−5.1	−6.3	−8.6	−7.2	−1.2	−8.9	88	86	86	87	0.3	0.3	0.4	0.3	10 ✳	10 ✳	10	NE 4	NE 1	ESE 2
16	83.7	82.9	82.3	83.0	−13.2	−9.6	−10.2	−9.8	−5.6	−15.1	80	57	68	68	0.4	1.7	0.9	1.0	0	0	0	C 0	E 2	E 6
17	81.1	79.7	80.1	80.3	−17.8	−5.8	−5.0	−8.4	−4.4	−19.9	79	69	83	77	0.3	1.2	0.7	0.7	0	8	10	C 0	C 0	C 0
18	81.2	81.4	81.7	81.4	−5.3	−3.4	−3.4	−3.9	−2.7	−7.1	90	92	92	91	0.4	0.4	0.4	0.4	10	10 △	10	C 0	C 0	C 0
19	81.4	83.8	89.2	84.8	−6.2	−1.2	0.4	−1.6	0.4	−6.7	89	86	94	90	0.4	0.8	0.4	0.5	7	10	10	C 0	C 0	C 0
20	92.4	92.6	90.9	92.0	2.3	3.0	−3.0	−0.7	3.0	−3.7	93	78	95	89	0.3	1.9	0.2	0.9	10	3	0	C 0	C 0	C 0
21	87.9	87.2	87.9	87.7	−7.6	4.2	1.4	−0.2	4.2	−9.6	93	64	85	81	0.2	2.9	1.0	1.4	0	9	10	C 0	SE 2	E 2
22	86.1	85.0	83.5	84.9	1.2	2.4	−0.8	0.3	3.2	−1.3	89	79	90	86	0.8	1.6	0.6	1.0	10	10	0	SE 2	E 2	C 0
23	77.3	76.7	75.2	76.4	−3.2	0.2	−3.0	−3.8	0.2	−7.0	83	63	78	75	0.7	2.3	0.9	1.3	1	1 ⊙	0	C 0	C 0	C 0
24	74.7	75.4	76.7	75.6	−4.8	−8.4	−4.0	−5.4	0.0	−6.3	81	72	82	78	0.8	1.7	0.8	1.1	7	3	0	C 0	E 2	ESE 2
25	77.2	78.8	80.2	78.1	−4.6	1.8	−1.2	−1.3	1.4	−7.7	86	75	82	81	0.6	1.7	1.0	1.1	1	8	10	SW 2	C 0	C 0
26	83.3	84.7	86.5	84.8	−4.7	2.8	−4.2	−2.6	3.9	−6.4	93	69	91	84	0.3	2.4	0.4	1.0	3	3	0	C 0	C 0	C 0
27	85.3	85.3	83.9	85.2	−9.0	2.4	−5.3	−4.6	3.9	−9.4	92	82	89	88	0.3	1.3	0.4	0.7	0	3	0	C 0	ESE 1	C 0
28	79.3	75.8	72.7	76.3	−8.4	−8.4	1.5	−1.4	3.4	−9.9	89	96	76	87	0.3	0.2	1.6	0.7	8	2	9	C 0	C 0	WNW 3
29	71.2	69.6	66.8	69.3	2.8	2.4	2.4	2.3	3.8	0.4	73	65	65	68	1.8	2.6	2.6	2.3	10	7	9	W 6	SW 6	SW 12
30	62.7	61.2	59.8	61.2	3.2	4.4	3.2	3.3	4.3	1.6	74	71	76	74	2.0	2.3	1.9	2.1	10 ●	10	10 ●	SW 17	SW 17	WSW 12
31	62.3	62.6	63.7	62.9	1.2	2.2	2.0	1.8	3.4	0.3	83	71	69	75	1.1	2.1	2.2	1.8	10	7	10 ✳	W 7	W 4	C 0
M	73.8	73.8	74.1	73.9	−5.2	1.2	−1.2	−1.1	2.4	−5.7	88	77	84	83	0.6	1.6	1.0	1.1	7.0	7.1	6.2	2.4	2.7	2.5

Jelenia Góra

$H_s = 342\ m$ $H_b = 343.0\ m$ $h_w = 15\ m$

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DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ LODU	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–3²⁰, por. wiatru ponad 10 m/sek 9⁴⁰–12¹⁵, ⌓¹ 1¹⁰–8¹⁵
2	8	.	.	–	
3	7	.	.	–	≡ 7¹⁵–8²⁰, 20¹⁵–22¹⁵ ≡≡–24, ⌴² 4²⁰–8¹⁵
4	8	.	.	–	≡ 0⁰⁰–4³⁵, ≡≡–6¹⁵ ≡≡–7⁵⁰ ≡≡–9²⁰, ⌴² 0³⁰–4³⁵
5	8	.	.	–	⩺ 3³⁰–7⁵⁰ (por. ponad 15 m/sek 6⁴⁰–7³⁵), por. ponad 10 m/sek 9³⁰–10²⁰, 11³⁰–12⁴⁰, 13⁵⁰–14¹⁰
6	7	.	.	–	= 9⁰⁰–12³⁰
7	8	3.9	.	–	•⁰ 11⁴⁵–13³⁰..45–17⁴⁵ 19⁴⁰ 21³⁰–24, = 17⁴⁵–19³⁰
8	6	1.9	.	–	•¹ 0⁰⁰–3²⁰ 4⁴⁰ ▽ 18⁴⁵–19¹⁰, 20²⁵–21⁵⁰ •⁰–24, = 8²⁰–16⁴⁵
9	7	0.8	.	–	•⁰ 0⁰⁰–4¹⁵ 7²⁰ 8²⁰ 11⁵⁰
10	7	0.2	.	–	= 1³⁰–2⁴⁰ ≡⁰⁻¹–6⁴⁵ ≡≡–7⁴⁵ ≠–9²⁰
11	6	0.3	.	–	•⁰ 1⁵³–4⁵⁰ •⁰–7¹⁵ •⁰–9²⁵ •⁰ 12⁴⁰–13¹⁰ 14²⁵–15⁴⁰ 16¹⁰–20³⁰, 20⁵⁰ 24
12	7	1.5	.	–	•⁰ 0⁰⁰ 8¹⁰–12⁴⁰ 14¹⁵–17⁴⁰ 18³⁰ 24
13	7	0.0	.	–	•⁰ 0⁰⁰–2³⁵ 6²⁰ •⁰ 9⁴⁸ 10³⁰, = 6⁰⁰–10³⁵
14	7	.	.	–	= 8¹⁵–12²⁰, 16³⁰–24
15	3	.	.	–	= 0⁰⁰–6⁴⁰ ≡⁰–24, ⌴⁰ na–24
16	5	0.0	.	–	≡¹ 0⁰⁰–10⁴⁵ ≡≡–24, ⌴⁰ 0⁰⁰–4⁰⁰
17	7	0.0	.	–	= 0⁰⁰–1⁴⁰ ≡⁰–8²⁵ ≡≡–10⁴⁰ ≡≡–12³⁰, 20⁴⁵–24
18	6	.	.	–	≡⁰ 0⁵⁰–2⁵⁰ ≡≡–24
19	7	.	.	–	= 0⁰⁰–6³⁵
20	6	.	.	–	= 7³⁰–13⁴⁵
21	8	.	.	–	⌴⁰ 2¹⁰–5²⁰ ⌴¹ 18⁰⁰–24
22	7	.	.	–	⌴¹ 0⁰⁰–10¹⁰
23	8	.	.	–	⌴⁰ 0²⁰–7¹⁵
24	7	0.0	.	–	•⁰ 17⁴⁵–18²⁰ ⩺ 3¹⁰–6³⁰
25	6	2.3	.	–	•⁰ 6¹⁰..35 10⁴⁰ 11²⁵–15²⁰ •⁰–16¹⁰ •⁰–20³⁰ •⁰–21⁴⁵ •¹–22³⁵ •⁰–24, = 12²⁵–24
26	6	0.2	.	–	•⁰ 1²⁰–4⁸, 3¹⁵–5³⁵ •⁰ 20⁴⁵ 24, = 0⁰⁰–24
27	6	0.5	.	–	•⁰ 0⁰⁰ 3³², 7⁴⁵–12⁴⁰ ⩺ 1²⁰–3³⁰ 4¹⁵–6³⁵, por. ponad 10 m/sek 8³⁵–12¹⁵ ⩺ 17⁴⁵–19²⁰, = 12⁴⁰–24
28	6	2.9	.	–	•¹ 1⁰⁰ 8⁴⁵ 11⁴⁰–16⁴⁰ 18¹⁰–20²⁰ 22²⁵–24 •¹ 20²⁰–24, por. wiatru ponad 10 m/sek 3¹⁵–6²⁰ 12⁰⁵–13¹⁰ 17³⁰–24, = 0⁰⁰–1⁰⁰
29	7	4.2	.	–	•⁰ 0⁰⁰ 1²⁰ 7⁴⁵ 8⁴⁰ ▽ 9⁴⁵–10⁰⁵ 10¹⁵⁻³⁰ ⛤ 11⁴⁸–12⁴⁰ 14⁴⁵–15¹⁰ ✱ 15¹⁵–20⁴⁰ 21²⁰–23¹⁰ ⩺ 0⁰⁰–7³⁰ por. wiatru ponad 10 m/sek 8¹⁵–9²⁰,
30	6	1.2	1	–	▽ 0²⁰–5⁵⁵ 1¹⁵–45 ✱⁰ 10⁴⁰ 11²⁰–13⁴⁰ 16¹⁵–17³⁵ 18¹⁵–20⁴⁵ [29.XI: 12¹⁰–13⁴⁰, 20¹⁰–21³⁰
31					
Σ	–	19.9	–	–	UWAGI

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1	8	3.3	3	–	✱⁰ 0⁴⁰ 5⁴⁰ 17¹⁵ 18³⁰–22¹⁰ ✱¹–23⁵⁰ ✱⁰–24
2	3	4.3	8	–	✱⁰ 0⁰⁰–2²⁵ ✱¹–5³⁵ ✱⁰–7⁵⁰ ⛫⁰–11¹⁵ ✱⁰–11⁴⁵ ⛫⁰–13⁴⁵ ✱⁰ 15¹⁰..40 ⛫¹–24, = 14²⁰–24
3	3	3.8	11	–	⛫⁰ 0⁰⁰–6¹⁰ ✱¹–8⁴⁵ ✱⁰–9³⁰ •⁰–13¹⁵ •⁰–15²⁰ •⁰–18¹⁰ •¹–20¹⁵ •⁰–21²⁰ •⁰–24, =⁰ 10⁵⁰–20⁴⁵ ≡ –24
4	3	3.2	5	–	•⁰ 0⁰⁰–6¹⁰ ✱⁰–7³⁰ •⁰–12¹² ✱⁰–13⁴⁵ •⁰–14⁵⁰, 15⁰⁵–40, 17²⁰ 24, = 0⁰⁰–38 ≡–3²⁰ = –24
5	6	0.4	3	–	•⁰ 0⁰⁰–35 •⁰ 2⁴⁵ 3²⁰–5⁴⁰ •⁰–6²⁰ •⁰–9¹⁰, = 0⁰⁰–24
6	8	.	.	–	= 0⁰⁰–11¹⁰ ≡ 17³⁰–24, ⌴² 21²⁰–24
7	8	.	.	–	≡ 0⁰⁰–30, ⩻ 22¹⁰–24, ⌴² 0⁰⁰–10⁰⁰
8	8	3.8	.	–	•⁰ 8¹⁰ 9¹⁵ 10¹⁰–17²⁵ 18³⁰–19²⁵ ▽ –20¹⁰ 21²⁰–45, ⩻ 0⁰⁰–3²⁵ ⩺ 17⁴⁰–19³⁵ ⩻ –21⁴⁵ ⩺ –24
9	8	2.2	.	–	▽ 2⁵⁵–3¹⁰ 3⁵⁰–4¹⁵, 6⁵⁵–7⁰⁵ •⁰ 7⁴⁵ 8¹⁰–9³⁰ ⩺ 0⁰⁰–7¹⁵, por. ponad 15 m/sek 8³⁵–9¹⁰ 10⁴⁰–13³⁰, 14⁴⁰–16²⁰
10	7	0.8	.	–	✱⁰ 7⁴⁵–8³⁵ 9³⁰–10³⁵ ▽ 10⁴⁵–12⁴⁰, 14²⁵–15³⁵, 15⁵⁵–16⁴⁰, ⌴¹ n–7⁴⁰
11	8	.	1	–	⌴⁰ n–10³⁰
12	7	.	pł.	–	
13	8	1.7	.	–	•⁰ 18²⁰ 19¹⁰–24, = 7³⁰–11³⁰
14	5	9.7	.	–	•⁰ 0⁰⁰–6¹⁵ 7²⁰–8⁴⁰ •⁰–9³⁰ •⁰–10¹⁰ ⛫–12²⁰ ✱⁰–24, = 0⁰⁰–24
15	7	0.0	12	–	✱⁰ 0⁰⁰–6²⁰, 6³⁵ 7⁴⁵, 8¹⁵–9⁴⁰, 10²⁰–15³⁰, 21²⁸–24
16	8	.	11	–	✱⁰ 0⁰⁰ 1⁴⁵, ✢¹ 17¹⁵–21²⁰
17	6	0.1	10	–	•⁰ ∼ (marznącaj) 21⁴⁵ 22¹⁰ ⛫–24, = 2³⁰–24
18	5	0.0	9	–	⛫⁰ 0⁰⁰–6¹⁵, 9⁴⁸–15³⁰ •⁰–19²⁵, = 0⁰⁰–24
19	6	0.1	8	–	= 0⁰⁰–24
20	6	.	7	–	•¹ 3⁴⁵, 6⁵⁰, = 0⁰⁰–15³⁰, 21⁰⁵–45
21	7	.	6	–	⌴¹ 0⁰⁰–10¹⁵
22	7	.	6	–	
23	7	.	pł.	–	
24	7	.	pł.	–	
25	8	.	pł.	–	= 19²⁰–24
26	8	.	pł.	–	= 0⁰⁰–7⁴⁰
27	7	.	pł.	–	= 8¹⁰–12³⁰, 17³⁰–21²⁵ ≡≡–24
28	9	0.1	pł.	–	≡≡ 0⁰⁰–9⁴⁵ ≡≡–14⁴⁰
29	7	0.0	pł.	–	✱⁰ 1⁰⁰ 2³⁰–5⁴⁰ 6¹⁰ 15⁴⁵ 16³⁵ 23²⁵ 24, ⩺ 20²⁵–23¹⁵ ⩻ –24
30	7	2.8	pł.	–	✱⁰ 0⁰⁰–3¹⁵ •⁰ 6⁴⁵ 7⁴⁰ 9³⁸ 10⁴⁰ 19³⁷–21¹⁵ 21⁴⁶–22²⁰ ✱–23¹⁰ ✱⁰–24, ⩺–⩻ 0⁰⁰–22⁰⁰
31	7	0.6	1	–	✱⁰ 0⁰⁰–2¹⁰ ✱⁰–3⁴⁰ 4⁰⁷–50 ✱ 11⁵⁰–12¹⁵, 13⁴⁵–14²⁰, 15¹⁰–15, 18⁵⁵–19²⁰ 20⁵⁵–22¹⁰ •⁰ 23⁴⁰ 24
Σ	–	37.1	–	–	UWAGI

Śnieżka — φ = 50°44' — λ = 15°44' — Styczeń – Janvier 1957

DNI	CIŚNIENIE P − 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			WIATR D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	28.9	29.2	29.1	29.1	-5.1	-2.7	0.7	-1.6	0.8	-5.4	98	62	56	72	0.1	1.9	2.8	1.6	2	9 ⊙	7	SW 12	SSW 7	S 9
2	28.6	30.0	32.9	30.5	1.5	2.6	-1.5	0.3	3.1	-1.8	68	61	90	73	2.2	2.9	0.6	1.9	9	8 ⊙	10	SSW10	SW 9	WNW 5
3	35.1	35.5	35.9	35.5	-2.4	-4.8	-6.7	-5.2	-0.6	-7.0	84	100	99	94	0.8	0.0	0.0	0.3	9	9	4	SW 6	WSW 10	WSW12
4	35.7	38.3	38.8	37.6	-6.1	-5.0	-4.6	-5.1	-3.6	-7.0	100	98	98	99	0.0	0.1	0.1	0.1	6	10 ≡	10 ≡	SW 12	W 9	W 10
5	39.7	37.7	37.7	38.4	-0.5	1.3	1.5	1.0	2.8	-5.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ● ≡	10 ● ≡	WSW14	W 22	WNW24
6	35.3	32.7	32.0	33.3	0.5	0.2	-6.3	-3.0	2.2	-6.4	100	100	97	99	0.0	0.0	0.1	0.0	10 ● ≡	10 ⁂ ≡	1	W 22	W 22	NNW26
7	35.6	39.3	42.4	39.1	-5.6	-6.0	-5.5	-5.6	-4.7	-7.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ⁂	10 ✳ ≡	10 ≡	NNW30	NNW 28	NNW28
8	44.1	43.9	43.7	43.8	-3.0	-2.7	2.3	-0.3	2.4	-6.4	99	100	70	90	0.0	0.0	2.1	0.7	9	9	0	N 21	NNW 20	NNW17
9	40.8	41.1	37.7	39.9	1.5	4.3	1.4	2.2	5.1	0.6	100	33	98	77	0.0	5.5	0.2	1.9	4	9 ○	4	WNW20	WNW 9	W 21
10	32.6	30.6	30.5	31.2	-1.5	-6.2	-7.5	-5.7	2.2	-7.9	99	100	99	99	0.1	0.0	0.0	0.0	8	10 ≡	10 ✳ ≡	W 20	NW 14	NW 17
11	30.8	33.3	35.6	33.2	-8.8	-8.7	-9.9	-9.3	-7.5	-10.0	98	95	97	97	0.1	0.2	0.1	0.1	10 ✳ ≡	10 ✳ ≡	10 ≡	NW 17	N 20	N 14
12	31.5	27.3	20.7	26.5	-8.9	-8.5	-8.9	-8.8	-7.9	-11.6	98	98	95	97	0.1	0.1	0.2	0.1	9 ✳	10 ✳ ≡	10 ✳ ≡	NW 17	W 14	W 17
13	20.5	22.1	23.8	22.1	-8.0	-7.8	-9.2	-8.6	-3.6	-9.8	96	99	98	98	0.1	0.0	0.1	0.1	10 ✳ ≡	5 ⊙	6	WNW 7	W 2	SSE 3
14	27.9	30.2	31.0	29.7	-9.4	-9.5	-13.0	-11.2	-8.8	-13.1	98	98	96	97	0.1	0.1	0.1	0.1	8	10 ✳ ≡	10 ≡	ENE 7	NE 10	NE 17
15	30.7	31.1	31.8	31.2	-15.2	-14.9	-14.3	-14.7	-13.0	-17.1	96	91	91	93	0.1	0.2	0.2	0.2	10 ≡	10 ≡	10 ✳ ≡	NE 17	NNE 20	NNE20
16	34.9	36.4	38.0	36.4	-15.9	-16.7	-14.7	-15.5	-14.3	-17.9	95	90	48	78	0.1	0.2	1.0	0.4	10 ✳ ≡	1 ⊙	0	N 12	N 12	NNE14
17	38.5	40.4	41.5	40.1	-14.6	-10.8	-9.4	-11.0	-9.0	-17.6	91	97	98	95	0.2	0.1	0.1	0.1	0	8	7	NNE14	NE 17	NE 17
18	42.0	42.4	41.6	42.0	-9.7	-4.4	-6.5	-6.8	-2.6	-10.1	98	35	39	57	0.1	2.9	2.3	1.8	3	3 ⊙	1	N 8	C 0	N 2
19	40.6	41.9	43.1	41.9	-3.2	0.4	0.0	-0.7	3.2	-7.1	46	37	17	33	2.6	4.0	5.1	3.9	0	1 ⊙	0	N 4	N 1	N 5
20	43.3	43.4	42.8	43.2	-0.2	1.5	0.1	0.4	2.8	-0.7	18	30	32	27	5.0	4.7	4.2	4.6	1	3 ⊙	0	C 0	SW 7	SSW 9
21	40.2	40.0	41.2	40.5	-0.1	0.5	0.9	0.6	2.9	-1.8	36	23	19	26	3.9	4.8	5.2	4.6	6	1 ⊙	0	SW 14	SW 14	SW 10
22	38.7	37.8	34.8	37.1	-1.3	-0.3	-3.0	-1.9	1.0	-3.5	23	30	27	27	4.3	4.2	3.5	4.0	4	2 ⊙	0	SSW14	SSW 10	WSW 6
23	35.1	33.9	30.4	33.1	-3.7	-1.8	-3.2	-3.0	-0.2	-6.0	43	35	43	40	2.7	3.5	2.7	3.0	1	5 ⊙	8	WSW 5	S 5	S 20
24	26.5	25.5	24.5	25.5	-6.9	-5.1	-8.2	-7.1	-3.2	-8.2	75	100	98	91	0.9	0.0	0.1	0.3	10	10 ✳ ≡	10	S 17	SSW 12	SW 12
25	25.1	27.2	30.1	27.5	-6.7	-5.1	-5.7	-5.8	-4.3	-10.2	99	100	97	99	0.0	0.0	0.1	0.0	10 ≡	10 △ ≡	8	W 12	W 12	WSW12
26	33.6	32.1	32.9	32.9	-7.5	-7.7	-7.7	-7.6	-5.4	-8.4	93	99	99	97	0.2	0.0	0.0	0.1	3	6 ⊙	8 ✳	WSW 9	SW 22	SW 24
27	32.5	34.4	35.7	34.2	-1.7	-3.6	-7.1	-4.9	-1.5	-7.9	98	99	96	98	0.1	0.1	0.1	0.1	10 ≡	10 ✳ ≡	0	W 20	W 20	W 17
28	32.2	36.8	42.8	37.3	-8.5	-7.9	-8.3	-8.2	-6.0	-9.1	98	96	95	96	0.1	0.1	0.2	0.1	10 ✳ ≡	10 △ ≡	10 ≡	NW 26	NNW 28	NNW20
29	44.5	43.8	43.2	43.8	-7.1	-4.9	-3.2	-4.6	-2.6	-9.9	72	66	99	79	1.0	1.4	0.0	0.8	8	7	10 ≡	W 6	W 10	NW 7
30	40.6	39.0	37.5	39.0	-1.5	-1.8	-4.0	-2.8	0.5	-4.6	52	75	99	75	2.7	1.4	0.1	1.4	6	7	10 ✳ ≡	W 17	W 14	NW 10
31	38.1	37.9	36.4	37.5	-4.8	-5.5	-3.6	-4.4	-1.3	-6.8	98	85	99	94	0.1	0.6	0.1	0.3	9	9	10 ≡	NW 5	SSE 12	SW 17
M	35.0	35.3	35.5	35.3	-5.3	-4.6	-5.3	-5.1	-2.3	-7.9	83	78	80	80	0.9	1.3	1.0	1.1	6.9	7.5	6.3	13.4	13.3	14.3

Luty – Février

1	32.8	35.1	37.7	35.2	-0.3	0.2	4.4	2.2	5.1	-3.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ●	SW 28	W 17	W 17
2	41.1	42.4	43.5	42.3	2.5	2.5	2.7	2.6	5.0	0.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ⁂	10 ● ≡	WSW17	WSW 17	WSW17
3	42.1	42.5	42.1	42.2	2.8	3.9	3.3	3.3	4.9	2.4	100	88	91	93	0.0	1.0	0.6	0.5	8	9	4	WSW17	SW 9	S 5
4	41.8	42.0	41.9	41.9	4.6	2.9	2.1	2.9	4.8	1.1	52	80	76	69	4.1	1.5	1.7	2.4	9	9 ⊙	10	WNW 8	W 12	W 8
5	41.4	40.1	38.5	40.0	3.7	3.0	3.6	3.5	4.7	1.6	47	71	63	60	4.2	2.2	3.0	3.1	2	3 ⊙	0	SW 8	SSW 10	SSW 7
6	34.9	33.7	33.0	33.7	2.2	3.8	-1.1	1.0	5.4	-1.6	57	56	99	71	3.2	3.5	0.1	2.3	4	2 ⊙	10 ✳ ≡	S 9	WSW 12	WSW17
7	34.3	35.1	34.9	34.8	-2.6	-4.0	-5.1	-4.2	-0.8	-5.6	100	99	98	99	0.0	0.1	0.1	0.1	10 ✳ ≡	10 ≡	8	NW 14	WSW 20	WSW17
8	29.7	27.0	24.0	26.9	-3.6	-2.5	-0.9	-2.0	-0.7	-5.6	97	100	99	99	0.2	0.0	0.0	0.1	10 ≡	9	10	SW 22	WSW 33	SW 45
9	23.3	23.1	25.8	24.1	-1.4	-1.9	-3.5	-2.6	-0.4	-3.7	99	100	99	99	0.1	0.0	0.0	0.0	10 ≡	10 ✳ ≡	7	SW 25	WSW 17	W 17
10	25.9	25.9	25.9	25.9	-4.3	-2.9	-2.8	-3.2	-2.1	-5.6	98	99	100	99	0.1	0.0	0.0	0.0	8	10 ✳ ≡	10 ≡	SW 20	WSW 20	SW 12
11	26.2	30.1	31.3	29.2	-4.3	-3.9	-6.3	-5.2	-2.7	-6.6	98	99	99	99	0.1	0.1	0.0	0.1	10 ≡	10 ✳ ≡	10 ✳ ≡	NW 20	NW 12	WNW 9
12	27.1	24.9	22.7	24.9	-5.7	-5.7	-4.7	-5.2	-4.4	-7.8	97	97	98	97	0.1	0.1	0.1	0.1	10 ✳ ≡	10 ≡	10 ≡	SW 22	SW 17	SW 17
13	18.6	14.9	7.3	13.6	-5.7	-4.5	-3.2	-4.2	-2.9	-6.0	97	98	99	98	0.1	0.1	0.0	0.1	10 ≡	10 ✳ ≡	10 ✳ ≡	SW 20	SW 23	SW 35
14	8.1	8.1	9.7	8.6	-3.2	-3.1	-5.1	-4.1	-2.5	-5.3	99	99	98	99	0.0	0.0	0.1	0.0	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	SW 20	SW 28	SW 26
15	10.1	6.2	6.0	7.4	-6.1	-4.3	-3.4	-4.3	-3.2	-6.3	97	98	99	98	0.1	0.1	0.0	0.1	10 ≡	10 ✳ ≡	10 ✳ ≡	WSW10	SW 20	WSW22
16	12.3	14.5	18.7	15.2	-6.3	-5.9	-6.8	-6.4	-3.4	-6.8	97	100	99	99	0.1	0.0	0.0	0.0	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	SW 20	SW 22	SW 17
17	21.4	21.6	22.9	22.0	-9.1	-7.1	-7.1	-7.6	-6.8	-9.3	95	96	96	96	0.2	0.1	0.1	0.1	8	10 ✳ ≡	10 △ ≡	SW 17	SW 20	SW 24
18	22.4	18.2	16.3	19.0	-6.2	-3.9	-2.3	-3.7	-1.7	-8.6	97	96	98	97	0.1	0.2	0.1	0.1	7	10 ≡	10 ✳ ≡	S 17	SSW 21	S 6
19	20.1	25.5	27.0	24.4	-8.2	-8.2	-6.7	-7.4	-1.4	-8.4	95	95	96	95	0.2	0.2	0.1	0.2	10 ✳ ≡	10 ⁂	10 ✳ ≡	N 20	W 14	SW 24
20	27.1	27.6	25.6	26.8	-7.6	-5.9	-4.9	-5.8	-4.5	-8.4	96	92	98	95	0.1	0.3	0.1	0.2	10 ≡	9	10 ≡	SW 14	SW 12	S 14
21	26.0	27.5	28.9	27.5	-4.9	-4.9	-8.3	-6.6	-4.3	-8.4	98	98	95	97	0.1	0.1	0.2	0.1	9	10	10 ✳ ≡	N 1	W 3	NNW20
22	30.9	31.6	29.9	30.8	-9.1	-6.1	-8.8	-8.2	-4.9	-9.6	95	97	89	94	0.2	0.1	0.4	0.2	10 ≡	4 ⊙	4	NNW12	NNW 4	NNW 3
23	29.4	29.1	28.0	28.8	-10.4	-9.1	-9.8	-9.8	-8.2	-11.1	87	92	97	92	0.4	0.3	0.1	0.3	3	7 ⊙	2	W 8	SW 7	SW 4
24	20.5	18.0	19.3	19.3	-9.0	-6.5	-6.7	-7.2	-5.5	-9.9	95	94	99	96	0.2	0.2	0.0	0.1	10 ≡	10 ✳ ≡	10 ≡	SSW12	SW 7	NW 4
25	22.2	22.2	20.4	21.6	-8.3	-4.3	-6.3	-6.3	-2.7	-8.4	95	98	99	97	0.2	0.1	0.0	0.1	4	10 ✳	10 ✳ ≡	NW 3	SW 8	NNE 5
26	27.5	30.5	32.8	30.3	-11.6	-8.4	-6.8	-8.4	-6.3	-11.9	65	86	96	82	0.9	0.4	0.1	0.5	1 ⊙	1 ⊙	9	NNW 9	NNW 6	NW 9
27	34.5	36.3	38.1	36.3	-5.0	-4.0	-6.5	-5.5	-2.7	-6.8	98	99	99	99	0.1	0.1	0.0	0.1	10 ≡	10 ≡	10 ✳ ≡	NW 5	NNW 4	NW 10
28	39.5	40.8	42.2	40.8	-8.5	-8.9	-10.8	-9.8	-6.5	-10.8	98	95	97	97	0.1	0.2	0.1	0.1	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	NNW14	NNW 14	N 14
29																								
30																								
31																								
M	27.6	27.6	27.7	27.6	-4.5	-3.6	-4.0	-4.0	-1.7	-6.1	91	94	96	94	0.5	0.4	0.2	0.4	8.3	8.7	8.4	14.7	14.6	15.2

Śnieżka

$H_s = 1603\ m$ $H_e = 1610\ m$ $h_w = 18\ m$

Styczeń–Janvier 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	113	6.6	
2	9	0.0	110	3.6	
3	8	0.5	108	0.3	
4	0	0.5	107	0.5	
5	0	3.9	108	.	
6	0	10.3	103	.	
7	0	8.0	101	.	
8	8	0.0	101	0.1	
9	8	.	100	7.0	
10	0	10.3	97	.	
11	0	4.4	105	.	
12	0	3.2	107	.	
13	8	0.2	109	2.1	
14	0	6.7	109	.	
15	0	5.0	110	.	
16	8	0.7	110	5.9	
17	9	0.0	110	5.1	
18	9	.	110	6.4	
19	9	.	108	8.3	
20	9	.	107	8.3	
21	9	.	107	8.3	
22	9	.	105	7.2	
23	8	.	106	7.1	
24	0	1.3	106	.	
25	0	0.0	106	.	
26	8	1.4	105	3.3	
27	0	7.0	107	.	
28	0	18.3	113	.	
29	9	.	122	5.7	
30	8	3.2	122	3.1	
31	7	1.4	123	2.0	
Σ	–	86.3	–	90.9	UWAGI. *Prędkość wiatru w ciągu całego roku wyznaczano za pomocą anemografu.*

Luty – Février

1	0	9.9	123	.	
2	0	4.9	112	.	
3	8	.	92	3.2	
4	8	.	86	1.2	
5	8	.	83	8.6	
6	9	3.0	68	7.9	
7	0	0.3	60	1.2	
8	8	3.1	60	.	
9	0	3.8	60	.	
10	0	5.0	62	.	
11	0	4.1	65	0.1	
12	0	1.5	70	.	
13	0	11.6	69	.	
14	0	9.1	76	.	
15	0	10.3	84	.	
16	0	5.8	96	.	
17	0	3.0	103	0.5	
18	0	50.1?	103	.	
19	0	15.5	120	0.8	
20	9	0.0	131	5.9	
21	7	6.6	128	0.1	
22	8	0.0	130	7.6	
23	7	0.6	122	5.9	
24	1	1.2	119	0.4	
25	7	9.5	121	1.1	
26	8	0.2	126	7.6	
27	0	10.5	124	0.6	
28	0	16.2	128	.	
29					
30					
31					
Σ	–	185.8?	–	52.7	UWAGI. *W dniu 18.II. „opad" pochodzi częściowo ze śniegu nawianego do deszczomierza.*

Śnieżka — φ = 50°44' — λ = 15°44' — Marzec – Mars 1957

DNI	CIŚNIENIE P − 800 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	43.2	43.9	43.7	43.6	-13.0	-10.4	-11.9	-11.8	-10.0	-13.0	96	94	93	94	0.1	0.2	0.2	0.2	10✳	10✳	10✳	N 14	N 12	N 10
2	41.7	42.1	39.7	41.2	-13.3	-9.4	-11.8	-11.6	-8.2	-13.4	92	85	86	88	0.2	0.4	0.4	0.3	10	2	0	N 8	N 7	N 10
3	36.1	36.4	34.7	35.7	-11.5	-8.0	-7.3	-8.5	-6.9	-12.2	51	47	41	46	1.2	1.8	2.1	1.7	4	4	5	N 14	N 10	NNW 8
4	32.0	31.1	29.4	30.8	-3.5	-2.0	-2.4	-2.6	0.0	-7.4	24	36	55	38	3.6	3.4	2.3	3.1	6	9	10	NW 9	NNW12	WNW17
5	28.8	30.0	30.5	29.8	-5.6	-5.7	-5.7	-5.7	-2.3	-9.7	100	62	35	66	0.0	1.5	2.6	1.4	9	9	1	NW 14	NW 3	NW 4
6	29.6	29.6	29.0	29.4	-4.3	-0.6	-2.4	-2.4	0.0	-6.8	96	87	89	91	0.2	0.8	0.6	0.5	1	5	0	NW 3	C 0	SW 3
7	27.9	28.2	29.2	28.4	-1.6	-2.1	-3.3	-2.6	-0.8	-3.8	75	79	99	84	1.3	1.1	0.0	0.8	1	7	7	SE 3	S 9	S 4
8	29.5	30.8	32.5	30.9	-1.2	-0.7	-1.8	-1.4	-0.5	-3.3	99	99	100	99	0.1	0.0	0.0	0.0	10✳	10✳	10	SSW 3	NNW 7	NNW 6
9	34.0	36.6	40.3	37.0	-5.5	-7.6	-6.5	-6.5	-1.8	-8.6	68	38	57	54	1.3	2.2	1.6	1.7	1	1	0	NNE 6	SE 12	SE 10
10	41.5	43.7	43.9	43.0	-7.6	-3.1	-3.3	-4.3	-2.1	-8.1	48	33	32	38	1.8	3.2	3.2	2.7	1	2	0	SE 12	ESE 6	SSE12
11	45.3	46.8	45.5	45.9	-0.5	2.0	-0.2	0.3	2.4	-3.5	19	24	33	25	4.8	5.4	4.0	4.7	1	2	2	SSE12	SSW10	S 12
12	43.1	42.0	40.2	41.8	1.3	6.0	5.3	4.5	7.9	-0.6	12	29	14	18	5.9	7.2	7.6	6.9	7	6	2	S 2	S 3	NNW 7
13	39.3	40.9	39.3	39.8	4.9	6.7	5.3	5.6	8.3	3.1	5	19	8	11	8.2	8.0	8.2	8.1	6	8	7	N 5	NW 2	SW 9
14	34.5	32.6	32.1	33.1	4.2	1.8	-0.4	1.4	6.0	-0.4	49	76	94	73	4.2	1.8	0.4	2.1	5	9	10	WSW20	W 25	W 24
15	31.3	31.1	28.6	30.3	-2.6	-1.8	-0.1	-1.2	0.3	-3.3	100	98	100	99	0.0	0.1	0.0	0.0	10	10	10	NW 24	SW 22	W 22
16	24.3	26.9	29.8	27.0	-0.1	-2.7	-5.6	-3.5	0.2	-7.1	100	100	100	100	0.0	0.0	0.0	0.0	10✳	10✳	10	WNW24	NW 17	NW 10
17	28.6	28.2	23.4	26.7	-1.7	-0.3	0.0	-0.5	0.1	-5.7	98	100	100	99	0.1	0.0	0.0	0.0	10✳	10	10	W 20	W 24	SW 32
18	21.0	21.3	23.4	21.9	1.4	0.2	-1.6	-0.4	1.8	-2.5	100	100	98	99	0.0	0.0	0.1	0.0	10	10	10	WSW20	WSW22	W 32
19	27.0	28.3	28.7	28.0	-3.7	-1.6	0.8	-0.9	1.0	-4.0	99	98	100	99	0.1	0.1	0.0	0.1	9	10✳	10	WNW28	WSW24	NW 22
20	31.2	28.7	29.9	29.9	1.3	0.3	3.5	2.2	4.0	0.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	SW 12	SW 22	SW 17
21	30.2	32.2	33.1	31.8	-2.1	-0.4	-1.4	-1.3	4.9	-2.1	74	60	80	71	1.3	2.3	1.1	1.6	3	2	8	WNW17	SW 14	WNW10
22	33.8	35.6	36.5	35.3	-3.3	-1.9	-1.4	-2.0	-0.2	-3.4	90	94	76	87	0.5	0.3	1.3	0.7	2	9	2	W 17	W 10	SW 7
23	35.0	34.7	35.0	34.9	-0.2	2.3	-0.5	0.3	3.6	-2.0	77	69	100	82	1.3	2.2	0.0	1.2	6	9	9	S 10	SSW14	SSE20
24	32.5	33.7	37.1	34.4	-3.2	-1.3	1.7	-0.3	2.0	-3.6	97	99	96	97	0.1	0.1	0.3	0.2	10	10	10	SE 24	SSE20	SSW12
25	37.2	38.6	38.8	38.2	0.5	0.9	1.3	1.0	3.2	-0.3	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	SSW12	SW 12	SW 22
26	35.3	35.9	36.4	35.9	-2.7	-1.5	-3.6	-2.8	1.3	-3.7	97	99	76	91	0.1	0.1	1.2	0.5	10	9	2	SW 34	SW 28	SW 32
27	37.0	39.1	37.9	38.0	-3.8	-1.2	-4.3	-3.4	-0.2	-5.9	68	64	86	73	1.4	2.0	0.6	1.3	4	7	9	SW 30	SW 24	SW 25
28	34.0	34.4	32.7	33.7	-5.9	-1.8	-1.4	-2.6	-0.1	-6.1	94	98	99	97	0.2	0.1	0.1	0.1	10	10	10✳	SSW22	SW 17	SW 20
29	31.4	31.4	31.9	31.6	-1.8	-2.1	-3.3	-2.6	-0.7	-4.0	98	100	99	99	0.1	0.0	0.0	0.0	10✳	10	10	W 10	SW 8	N 3
30	32.7	34.0	35.4	34.0	-4.4	-2.6	-1.7	-2.6	-1.1	-5.3	98	98	98	98	0.1	0.1	0.1	0.1	10	10✳	10✳	N 4	NE 9	NE 14
31	35.3	36.7	39.1	37.0	-4.1	-3.4	-2.7	-3.2	-1.3	-5.7	98	97	100	98	0.1	0.2	0.0	0.1	10✳	10	10	SW 12	SW 17	SW 4
M	33.7	34.4	34.4	34.2	-3.0	-1.7	-2.1	-2.2	0.3	-4.9	78	77	79	78	1.2	1.4	1.2	1.3	7.0	7.7	6.9	14.4	13.6	14.2

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1	38.5	38.0	36.9	37.8	-2.3	-0.1	-1.2	-1.2	0.3	-3.1	100	100	99	100	0.0	0.0	0.1	0.0	10✳	10	10✳	SE 10	ESE 8	S 17
2	34.8	35.6	37.2	35.9	-0.7	-0.3	-0.1	-0.3	0.1	-1.3	99	100	100	100	0.0	0.0	0.0	0.0	10	10	10✳	S 20	SW 17	SSW17
3	40.0	43.2	45.9	43.0	0.2	0.4	3.2	1.8	3.8	-0.1	100	98	87	95	0.0	0.1	1.0	0.4	10	9	1	SSE12	SSE 10	NE 9
4	47.6	48.4	48.1	48.0	4.0	4.9	4.3	4.4	5.7	2.7	42	45	62	50	4.7	4.9	3.2	4.3	1	2	0	E 9	ENE 9	ENE 9
5	45.5	45.1	40.2	43.6	2.5	5.5	3.2	3.6	7.8	2.1	30	41	58	43	5.1	5.3	3.2	4.5	1	0	0	NE 9	NE 3	SW 8
6	34.4	33.2	31.3	33.0	2.7	5.6	1.5	2.8	7.3	1.4	44	43	98	62	4.2	5.2	0.1	3.2	1	1	6	SW 14	SW 8	N 9
7	28.6	28.4	30.7	29.2	-4.0	-3.5	-6.4	-5.1	1.7	-6.4	99	99	97	98	0.1	0.0	0.1	0.1	10✳	10✳	10✳	N 14	NNW 14	N 12
8	31.4	33.2	32.6	32.4	-10.9	-9.6	-8.7	-9.5	-6.1	-13.4	97	82	95	91	0.1	0.5	0.2	0.3	5	2	0	N 17	NNE 5	N 10
9	31.1	31.2	29.6	30.6	-6.9	-2.9	-3.9	-4.4	-1.5	-8.7	94	97	96	96	0.2	0.1	0.2	0.2	5	8	10	N 8	N 3	N 3
10	27.0	25.2	20.5	24.2	-4.6	-1.4	-2.0	-2.5	0.9	-4.8	91	84	98	91	0.4	0.9	0.1	0.5	6	2	10	NNW 6	WSW 9	SW 10
11	16.5	16.8	20.7	18.0	-5.0	-6.3	-7.2	-6.4	-2.0	-7.4	98	94	99	97	0.1	0.2	0.0	0.1	10	10	10	N 14	N 10	N 8
12	24.2	25.7	28.0	26.0	-7.6	-6.4	-9.4	-8.2	-5.8	-9.6	96	97	95	96	0.1	0.1	0.2	0.1	10✳	10✳	3	C 0	N 7	N 5
13	26.9	29.4	31.7	29.3	-9.7	-8.6	-9.8	-9.5	-8.0	-10.7	94	98	97	96	0.2	0.1	0.1	0.1	9	10✳	6	WSW12	NW 10	NNW 7
14	31.4	32.6	33.1	32.4	-11.1	-7.1	-9.4	-9.2	-6.3	-11.4	100	96	91	96	0.0	0.1	0.3	0.1	10	9	1	NNW 9	N 4	N 3
15	33.9	35.7	37.3	35.6	-9.8	-6.3	-8.2	-8.1	-5.8	-10.6	97	97	98	97	0.1	0.1	0.1	0.1	4	10✳	5	N 6	NW 4	NNW10
16	38.5	39.0	38.5	38.7	-6.3	-1.3	-1.3	-2.6	-0.8	-9.1	97	99	88	95	0.1	0.1	0.7	0.3	9	10✳	5	NNW10	NW 14	NW 24
17	37.6	37.9	38.0	37.8	-1.9	-1.3	-2.6	-2.1	-1.0	-2.7	100	99	100	100	0.0	0.1	0.0	0.0	10✳	10	10✳	NW 12	NNW 10	NNW 8
18	34.6	34.7	33.9	34.4	-4.0	-2.7	-3.5	-3.4	-2.0	-4.8	99	100	99	99	0.1	0.0	0.0	0.0	10	10	10	NNW14	N 14	NNW12
19	32.4	31.3	33.1	32.3	-1.7	-1.2	0.0	-0.7	0.1	-4.7	98	99	100	99	0.1	0.1	0.0	0.1	10	10✳	10✳	NNW10	SW 8	NNW17
20	35.4	39.3	40.5	38.4	-5.0	-2.1	-4.1	-3.8	0.1	-5.6	98	98	98	98	0.1	0.1	0.1	0.1	10	7	5	NNW17	NNW 6	N 7
21	41.7	43.1	43.8	42.9	-4.7	-2.9	-3.7	-3.8	-1.7	-5.8	96	88	99	94	0.2	0.6	0.1	0.3	4	9✳	10✳	N 2	NNE 6	NE 5
22	44.7	45.1	44.7	44.8	-4.0	-3.1	-3.6	-3.6	-1.8	-4.7	96	97	94	96	0.2	0.1	0.3	0.2	4	8	0	ENE 2	NNE 6	NNE 8
23	44.5	44.9	45.5	45.0	-1.9	1.5	0.3	0.0	2.0	-4.0	100	90	90	93	0.0	0.7	0.6	0.4	10	3	0	NE 6	SSW 8	ESE 9
24	44.3	44.6	43.2	44.0	0.4	-0.2	-0.5	-0.2	1.8	-0.5	100	100	100	100	0.0	0.0	0.0	0.0	10	10✳	10	NE 12	NNE 10	N 14
25	40.1	39.9	40.0	40.0	-0.7	0.4	2.1	1.0	2.5	-1.7	99	100	86	95	0.0	0.0	0.9	0.3	10	10	0	NNE12	NE 7	E 4
26	39.5	40.8	40.4	40.2	2.0	5.3	3.5	3.6	6.3	1.2	100	94	78	91	0.0	0.6	1.6	0.7	9	8	9	E 7	S 6	E 8
27	38.4	38.1	35.8	37.4	3.2	6.9	5.7	5.4	8.3	2.8	100	89	100	96	0.0	1.0	0.0	0.3	10	9	10	SE 12	S 4	S 12
28	32.3	34.0	34.3	33.7	4.7	9.2	8.2	7.6	10.9	4.0	83	62	72	72	1.4	4.4	3.1	3.0	7	6	8	SW 17	SW 6	SW 8
29	35.0	36.6	36.1	35.9	6.5	10.6	7.9	8.2	12.9	6.4	80	51	91	74	2.0	6.3	0.9	3.1	1	4	7	SW 7	SW 6	NE 3
30	32.8	32.6	32.6	32.7	7.2	10.4	0.0	4.4	10.9	-0.2	66	65	100	77	3.5	4.4	0.0	2.6	9	10	10	SSW12	WSW 4	N 17
31																								
M	35.5	36.1	36.1	35.9	-2.3	-0.2	-1.5	-1.4	1.4	-3.7	90	87	92	90	0.8	1.2	0.6	0.9	7.5	7.6	6.2	10.4	7.9	9.8

Śnieżka — H_s = 1603 m — H_k = 1610 m — h_w = 18 m — Marzec – Mars 1957

DNI	WIATR DZIAŁALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	4.5	143	0.1	
2	9	0.0	145	6.9	
3	8	.	144	7.3	virga
4	8	1.1	139	3.3	
5	8	.	130	2.3	
6	6	0.0	128	9.4	
7	7	1.4	126	8.5	
8	0	2.2	126	.	
9	7	.	127	10.0	
10	9	.	125	10.1	
11	9	.	122	10.2	
12	9	.	118	8.8	
13	9	.	114	8.8	
14	7	0.2	106	8.2	
15	3	0.6	96	.	
16	0	9.0	95	.	
17	0	8.7	102	0.1	
18	0	8.8	97	0.5	
19	0	1.1	94	1.3	
20	0	1.7	91	0.1	
21	9	.	85	9.7	
22	6	0.0	80	5.6	
23	8	0.0	76	4.5	
24	0	0.2	74	0.3	
25	0	0.5	70	0.2	
26	7	.	65	3.3	
27	8	.	64	9.4	virga
28	0	1.9	63	.	
29	0.	7.3	63	.	
30	0	15.7	69	.	
31	0	1.9	84	.	
Σ	—	66.8	—	129.0	UWAGI.

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1	5	1.6	86	2.4	
2	0	4.0	87	.	LIV:
3	8	1.1	84	3.3	
4	8	.	74	11.6	
5	8	.	68	11.8	
6	8	1.2	60	11.4	
7	0	53.3	59	.	
8	9	0.0	95	10.8	
9	9	.	91	10.4	
10	8	0.0	90	11.5	
11	8	1.4	87	0.6	
12	0	2.4	89	.	
13	0	0.7	90	2.4	
14	8	0.0	92	6.3	
15	0	2.2	92	2.4	
16	0	1.0	93	2.7	
17	0	13.2	94	.	
18	0	0.0	100	3.0	
19	0	1.2	100	.	
20	8	.	100	7.9	
21	8	11.8	95	6.3	
22	7	.	105	2.4	
23	8	.	100	5.4	
24	0	18.2	92	.	
25	0	3.6	83	1.9	
26	7	0.5	78	6.4	
27	7	.	75	4.1	
28	8	.	70	11.0	
29	7	.	65	12.4	
30	8	3.3	55	7.0	
31					
Σ	—	120.7	—	155.4	UWAGI.

Śnieżka — φ = 50°44' — λ = 15°44' — Maj – Mai 1957

DNI	CIŚNIENIE P = 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	34.1	35.7	35.1	35.0	-5.8	-1.9	-3.5	-3.7	0.1	-5.9	97	96	92	95	0.1	0.2	0.4	0.2	7 ⊙	6 ⊙	2	NNE 12	N 9	NNE 10
2	33.1	33.4	32.3	32.9	-4.1	-1.9	-2.7	-2.8	0.3	-4.9	82	75	80	79	0.8	1.3	1.0	1.0	6 ⊙	8 ⊙	5	NNE 14	NE 10	NNE 7
3	31.8	31.5	31.7	32.0	-2.1	1.5	0.0	-0.2	1.8	-3.7	77	70	88	78	1.2	2.0	0.7	1.3	7	8 ⊙	4	NNE 7	N 5	W 4
4	29.4	30.7	30.2	30.1	-2.1	-4.4	-6.7	-5.0	1.0	-6.8	98	98	96	97	0.1	0.1	0.1	0.1	10 ✱ 〓	9 ✱	5 ✱	NW 14	NW 12	NNW 22
5	29.6	29.6	27.7	29.0	-8.8	-6.3	-6.1	-6.8	-3.9	-9.5	95	99	100	98	0.2	0.0	0.0	0.1	9 ✱	9 ✱	10 ✱ 〓	WNW 12	SW 10	SW 4
6	25.5	26.8	27.4	26.6	-8.5	-6.1	-7.6	-7.4	-5.6	-9.0	98	94	96	96	0.1	0.2	0.1	0.1	10 ✱ 〓	10 ✱ 〓	6	NW 17	NW 7	NW 9
7	25.7	26.3	26.2	26.1	-7.6	-5.1	-6.6	-6.5	-3.9	-8.8	96	95	97	96	0.1	0.2	0.1	0.1	9 ≡	9	5	NW 8	NNW 6	NNE 10
8	25.3	26.4	27.5	26.4	-6.7	-5.4	-5.7	-5.9	-4.0	-7.3	96	95	95	95	0.1	0.2	0.2	0.2	10 〓	10 ✱ 〓	10	NNE 12	NNE 10	N 4
9	28.7	30.0	30.3	29.7	-5.6	-3.0	-4.1	-4.2	-1.4	-6.9	95	93	91	93	0.2	0.4	0.4	0.3	9	9	2	N 2	NNE 5	N 7
10	28.8	31.3	32.2	30.8	-4.1	-1.3	-0.9	-1.8	0.9	-5.2	98	95	91	95	0.1	0.3	0.5	0.3	5 ⊙	8	8	N 14	N 6	N 7
11	33.5	35.5	36.0	35.0	-0.4	4.1	3.9	2.9	7.4	-1.2	80	63	61	68	1.2	3.0	3.2	2.5	3 ⊙	8	0	NNW 8	WSW 4	SSW 7
12	36.0	37.4	38.4	37.3	4.7	7.4	5.6	5.8	8.7	3.1	74	56	75	68	2.1	4.5	2.2	2.9	2 ⊙	7 ⊙	6	SSW 3	SW 7	SW 5
13	39.4	40.2	40.4	40.0	4.9	8.9	5.3	6.1	10.1	4.3	87	64	82	78	1.2	4.1	1.6	2.3	7 ⊙	8	10 ●	SW 2	SW 7	W 4
14	40.7	42.4	43.0	42.0	3.5	6.0	4.5	4.6	7.7	3.1	100	84	93	92	0.0	1.5	0.5	0.7	6 ⊙	7 ⊙	3	NW 6	NNW 4	N 6
15	43.6	43.9	41.6	43.0	4.7	7.9	6.2	6.2	11.1	4.0	83	69	86	79	1.4	3.3	1.4	2.0	6	8	1	WNW 3	SSW 3	S 9
16	38.9	38.4	37.1	38.1	6.9	11.4	6.3	7.7	13.5	5.7	75	58	100	78	2.4	5.7	0.0	2.7	2 ⊙	6 ⊙	10 (K) 〓	SSW 12	SW 10	N 12
17	37.9	39.5	40.1	39.2	5.0	2.6	4.4	4.1	6.9	1.9	97	100	97	98	0.3	0.0	0.3	0.2	9 ⊙	10 9 〓	10	NNE 5	N 6	N 3
18	39.3	39.4	37.1	38.6	4.6	6.8	5.7	5.7	9.3	2.8	100	100	95	98	0.0	0.0	0.5	0.2	8 ≡	9	1	ENE 4	E 4	SE 6
19	33.9	33.5	32.4	33.3	6.7	10.9	9.6	9.2	12.2	5.4	100	82	81	88	0.0	2.4	2.4	1.6	10 〓	9	9	E 4	SE 3	E 6
20	32.2	34.3	36.0	34.2	5.7	4.9	1.2	3.2	9.9	1.0	100	100	100	100	0.0	0.0	0.0	0.0	10 9 ≡	10 9 〓	10 9 〓	NNE 12	N 12	N 17
21	37.2	37.9	37.0	37.4	-2.1	1.7	-0.2	-0.2	2.3	-3.4	98	100	98	99	0.1	0.0	0.1	0.1	8	10 〓	7	N 6	WSW 3	N 6
22	35.4	35.5	34.9	35.3	0.3	1.8	0.8	0.9	4.6	-0.7	93	90	100	94	0.4	0.7	0.0	0.4	4 ⊙	9 ⊙	10 ● 〓	NE 4	NE 4	NE 7
23	33.0	33.7	34.8	33.8	2.5	4.4	4.5	4.0	5.8	-0.4	100	100	95	98	0.0	0.0	0.4	0.1	10 9 〓	10 9 〓	8	SE 8	S 7	SW 5
24	35.2	36.9	38.6	36.9	4.3	5.9	3.9	4.5	6.3	3.6	78	100	100	93	1.8	0.0	0.0	0.6	8 ⊙	10 〓	10 9 〓	N 9	NNE 10	NNE 14
25	38.1	39.8	40.3	39.4	-2.1	-1.5	-3.4	-2.6	3.9	-3.7	100	99	99	99	0.0	0.1	0.0	0.0	9	9	10 〓	NE 12	NNE 14	NNE 17
26	39.4	40.3	39.8	39.8	-5.2	-4.4	-4.2	-4.5	-2.9	-5.7	98	98	98	98	0.1	0.1	0.1	0.1	10 〓	10	10 〓	NE 12	NNE 12	NNE 14
27	38.7	39.6	39.1	39.1	-5.1	-3.7	-5.1	-4.8	-2.5	-5.9	98	99	98	98	0.1	0.1	0.1	0.1	10 〓	10 〓	8	ENE 12	NNE 10	NE 10
28	37.3	37.8	37.7	37.6	-4.5	-2.7	-3.0	-3.3	-0.9	-5.3	98	100	99	99	0.1	0.0	0.0	0.0	10 〓	10 ⛈	8	NE 12	NE 10	NNE 7
29	38.3	39.7	40.5	39.5	-3.0	-0.5	-0.3	-1.0	0.6	-4.1	99	98	74	90	0.0	0.2	1.6	0.6	3 ⊙	8	6	NNE 6	NNE 5	ENE 3
30	40.9	41.5	40.7	41.0	-0.2	4.2	2.8	2.4	6.9	-1.1	73	62	73	69	1.7	3.1	2.1	2.3	1 ⊙	7 ⊙	3	S 2	W 5	SW 8
31	39.0	39.3	38.5	38.9	1.4	4.3	4.2	3.5	7.1	0.4	87	76	83	82	0.9	2.0	1.3	1.4	2 ⊙	7	2	SSW 12	SW 9	SW 5
M	34.8	35.8	35.6	35.4	-0.7	1.5	0.3	0.4	3.6	-2.1	92	87	91	90	0.5	1.2	0.7	0.8	7.1	8.6	6.4	8.6	7.4	8.2

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1	38.7	39.9	40.2	39.6	4.9	7.8	6.2	6.3	9.1	2.9	80	64	80	75	1.8	3.8	2.0	2.5	9	7 ⊙	2	NW 2	N 6	NNW 8
2	41.4	43.5	43.7	42.9	4.8	9.9	8.9	8.1	11.4	4.4	87	75	76	79	1.1	3.0	2.7	2.3	4 ⊙	7 ⊙	1	NNW 12	N 4	W 4
3	43.6	42.7	39.7	42.0	8.9	12.5	11.3	11.0	15.2	7.8	69	52	67	63	3.5	6.9	4.4	4.9	0 ⊙	8	7	SW 4	SW 8	SSW 12
4	37.6	37.5	35.5	36.9	10.7	9.6	6.8	8.5	13.5	6.8	71	99	100	90	3.7	0.2	0.0	1.3	10 ⊙	10 ● 〓	10 ● 〓	N 8	SW 2	N 3
5	32.1	31.8	30.7	31.5	3.1	4.1	2.7	3.2	7.2	2.5	100	100	80	93	0.0	0.0	1.4	0.5	10 9 〓	8 ●	10	NW 17	WSW 17	WNW 10
6	30.4	33.2	33.7	32.4	-0.9	0.4	2.9	1.3	4.1	-1.4	99	94	82	92	0.0	0.4	1.3	0.6	10 ✱ 〓	6 ⊙	4	WNW 12	W 10	SW 12
7	33.8	34.4	35.0	34.4	4.7	8.1	5.9	6.2	9.6	2.5	83	71	90	81	1.4	3.1	0.9	1.8	8 ⊙	10	9	WSW 10	WSW 12	C 0
8	35.0	36.1	35.2	35.4	6.0	9.1	9.1	8.3	11.6	4.8	100	89	96	95	0.0	1.3	0.5	0.6	10 〓	8 ⊙	8	SW 7	SW 7	SW 12
9	33.1	34.7	36.0	34.6	8.2	7.8	7.6	7.8	9.6	7.0	100	100	97	99	0.0	0.0	0.3	0.1	10 〓	10 〓	9	SW 10	WSW 9	SW 4
10	35.6	36.4	36.1	36.0	7.9	11.7	10.6	10.2	12.8	7.0	100	81	97	93	0.0	2.6	0.4	1.0	10 〓	7 ⊙	6	E 6	SW 4	S 14
11	33.7	33.5	37.8	35.0	13.4	15.9	14.2	14.4	17.8	10.0	57	63	78	66	6.7	6.8	3.6	5.7	4 ⊙	6 ⊙	9	SSW 12	SW 20	SSW 3
12	43.0	47.5	50.5	47.0	12.9	10.8	7.3	9.6	14.7	7.3	100	100	100	100	0.0	0.0	0.0	0.0	10 9 〓	10 〓	10 9 〓	ENE 5	E 2	NE 3
13	51.6	51.9	50.4	51.3	9.7	7.8	6.0	7.4	11.7	5.4	75	84	79	79	3.0	1.7	2.0	2.2	1 ⊙	6 ⊙	6	NNE 6	NNE 7	N 12
14	49.5	50.4	49.7	49.9	5.5	9.1	7.7	7.5	11.7	4.2	89	82	81	84	1.0	2.1	2.0	1.7	2 ⊙	2 ⊙	1	NNE 9	NNE 7	NNE 9
15	48.3	48.8	46.9	48.0	10.0	10.6	8.0	9.2	13.7	5.3	47	64	76	62	6.5	4.6	2.6	4.6	0 ⊙	2 ⊙	0	NE 2	N 6	ENE 6
16	44.6	45.2	43.4	44.4	8.4	13.7	9.5	10.3	14.2	7.2	47	50	69	55	5.9	7.8	3.6	5.8	0 ⊙	0 ⊙	0	SE 12	S 3	E 7
17	42.2	43.3	42.1	42.5	9.4	14.9	10.8	11.5	15.6	8.4	64	54	75	64	4.2	7.9	3.3	5.1	1 ⊙	3 ⊙	2	SE 8	SE 6	E 7
18	40.9	40.8	39.5	40.4	11.9	15.3	12.3	13.0	17.4	10.3	57	51	72	60	6.1	8.6	4.1	6.3	1 ⊙	5 ⊙	4	C 0	SSW 5	SSW 7
19	38.6	39.1	38.9	38.9	12.4	13.3	13.9	13.4	17.6	10.2	65	52	64	60	5.1	7.4	5.7	6.1	2 ⊙	5 (K)	9	C 0	SW 2	SW 4
20	38.3	39.6	40.2	39.4	9.0	10.2	9.6	9.6	14.1	8.6	100	95	100	98	0.0	0.6	0.0	0.2	10 〓	9	10 〓	NNW 10	NW 8	NNW 6
21	40.4	39.5	36.8	38.9	8.4	12.8	10.3	10.4	15.5	7.9	91	77	100	89	0.9	3.5	0.0	1.5	5 ⊙	8	10 〓	SSW 1	W 2	SSW 7
22	32.3	32.4	31.4	32.0	8.8	10.4	7.7	8.6	11.1	7.5	100	100	100	100	0.0	0.0	0.0	0.0	9	10 9 〓	10 〓	SW 20	SW 14	SW 14
23	33.5	34.0	34.6	34.0	6.8	8.7	8.8	8.3	10.1	6.0	100	100	70	90	0.0	0.0	3.4	1.1	10 9 〓	10 〓	8	SW 8	SW 12	SSW 10
24	33.3	32.1	30.3	31.9	6.5	8.7	10.1	8.8	10.6	5.3	99	100	78	92	0.2	0.0	2.7	1.0	10 ●	10 9 〓	9	SE 3	S 8	SW 8
25	28.6	34.9	38.3	33.9	2.5	1.2	1.0	1.4	11.2	0.9	100	100	96	99	0.0	0.0	0.3	0.1	10 9 〓	10 9 〓	4	SW 28	WSW 17	W 8
26	39.4	41.8	44.2	41.8	-0.1	2.3	2.7	1.9	4.7	-0.2	100	93	71	88	0.0	0.5	2.1	0.9	10 〓	6 ⊙	2	NW 10	NW 5	NW 7
27	44.1	45.2	46.9	45.4	2.0	4.4	3.5	3.4	6.3	1.7	98	80	77	85	0.2	1.7	1.7	1.2	9 ●	9	8	W 10	NW 10	N 8
28	46.5	48.2	48.1	47.6	7.5	10.7	12.1	10.6	13.6	3.1	100	99	88	96	0.0	0.2	1.7	0.6	10 ⛈	8 ⊙	0	WNW 12	WNW 5	NW 9
29	48.7	50.1	49.3	49.4	11.6	16.4	15.2	14.6	18.1	10.4	89	70	66	75	1.5	5.8	5.8	4.4	2 ⊙	4 ⊙	0	NNW 6	N 2	NW 2
30	48.2	48.4	47.4	48.0	15.2	17.6	14.7	15.6	19.9	9.9	74	57	78	70	4.5	8.5	3.6	5.5	2 ⊙	6 ⊙ (K)	8	NNW 5	N 5	E 5
31																								
M	39.6	40.6	40.4	40.2	7.7	9.9	8.6	8.7	12.5	5.8	85	80	83	83	1.9	3.0	2.1	2.3	6.3	7.0	5.9	8.5	7.5	7.4

Śnieżka

$H_s = 1603\,m$ $H_p = 1610\,m$ $h_w = 18\,m$

Maj–Mai 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	‹	45	11.0	
2	9	.	42	11.0	
3	9	0.1	pł.	6.4	
4	6	0.1	pł.	2.3	
5	7	16.8	pł.	2.6	
6	1	2.2	15	3.4	
7	7	1.8	17	3.0	
8	0	0.5	18	0.8	
9	8	.	14	7.4	
10	8	.	13	5.6	
11	8	.	10	8.2	
12	8	.	pł.	7.9	
13	8	2.4	pł.	7.7	
14	8	.	pł.	8.3	
15	8	.	pł.	6.6	
16	8	16.3	pł.	12.7	
17	0	1.4	pł.	0.5	
18	7	.	pł.	5.5	
19	8	0.4	pł.	2.4	
20	0	11.7	pł.	.	
21	0	.	pł.	.	
22	8	4.8	pł.	4.9	
23	0	2.6	pł.	.	
24	0	19.0	pł.	4.3	
25	8	1.7	pł.	2.7	
26	8	0.6	pł.	0.3	
27	0	0.9	pł.	0.2	
28	7	0.1	0	1.9	
29	8	.	0	7.1	
30	8	.	pł.	8.7	
31	8	.	pł.	7.5	
Σ	—	82.8	—	150.9	UWAGI:

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1	8	.	pł.	5.4	
2	6	.	pł.	10.9	
3	7	.	pł.	10.7	
4	2	23.0	pł.	1.6	
5	7	1.8	pł.	2.4	
6	9	0.8	0	5.5	
7	8	2.6	pł.	5.2	
8	8	1.5	pł.	8.4	
9	0	0.0	pł.	0.1	
10	8	.	pł.	6.9	
11	9	0.0	pł.	9.9	
12	0	2.3	pł.	3.7	
13	9	.	pł.	13.8	
14	9	.	pł.	14.8	
15	9	.	pł.	15.1	
16	9	.	pł.	14.5	
17	9	.	pł.	14.5	
18	9	.	pł.	12.7	
19	9	12.0	pł.	7.9	
20	7	0.0	.	4.0	
21	7	1.9	.	7.5	
22	0	2.3	.	1.1	
23	0	3.9	.	1.2	
24	0	9.5	.	.	
25	0	0.2	.	2.0	
26	7	0.1	.	4.8	
27	7	0.0	.	7.2	
28	7	0.0	.	6.7	
29	8	.	.	13.3	
30	7	14.4	.	9.9	
31					
Σ	—	76.3	—	219.8	UWAGI:

Śnieżka — φ = 50°44' — λ = 15°44' — Lipiec–Juillet 1957

DNI	CIŚNIENIE p − 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	46.0	46.2	45.1	45.8	14.7	18.1	16.3	16.4	19.8	14.5	73	54	69	65	4.5	9.6	5.7	6.6	0 ○	5 ○	3	S 2	SW 4	S 10
2	42.7	43.1	44.2	43.3	15.9	14.5	11.6	13.4	18.1	11.6	56	89	100	82	7.9	1.9	0.0	3.3	3 ○	7 ○	10 ≡	SW 7	L 8	N 7
3	44.3	44.8	44.0	44.4	11.5	13.3	12.5	12.4	15.5	8.4	61	75	81	72	5.3	3.9	2.8	4.0	4 ○	8	2	NNW 1	WSW 1	SSW 5
4	43.2	43.9	44.4	43.8	13.7	17.9	18.7	17.2	20.6	11.3	84	60	53	66	2.5	8.0	10.1	6.9	5 ○	3 ○	3	SW 10	SW 12	SW 10
5	44.6	45.3	45.5	45.1	18.3	20.7	15.8	17.6	23.2	15.7	63	47	90	67	7.6	12.8	1.8	7.4	0 ○	1 ○	3	W 10	WSW 8	N 7
6	46.0	46.8	46.4	46.4	14.9	16.1	18.5	17.0	19.9	13.0	72	81	50	68	4.6	3.4	10.5	6.2	3 ○	8 ○	2	NNW 3	SW 5	WNW 5
7	45.7	46.4	45.4	45.8	18.1	19.5	18.7	18.8	22.0	11.7	49	65	76	63	10.6	8.0	5.4	8.0	6 ○	0 ○	5	WSW 1	SSW 5	SSW 8
8	43.8	44.0	42.4	43.4	19.8	19.5	17.5	18.6	22.3	12.2	65	72	50	62	8.0	6.5	9.8	8.1	5 ○	9 ○	7	ESE 4	N 6	NE 4
9	40.8	41.4	40.6	40.9	10.7	11.4	9.6	10.3	18.8	8.4	94	100	100	98	0.9	0.0	0.0	0.3	10 ●	9 ○	4	W 12	NNW 6	N 5
10	37.9	36.5	33.9	36.1	9.9	11.4	8.1	9.4	12.4	8.0	92	85	86	88	1.0	2.1	1.5	1.5	9	9 ○	10 ●	NNW 2	N 1	NNE 6
11	30.9	31.8	33.3	32.0	8.6	9.3	9.5	9.2	9.7	7.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ●≡	10 ●≡	10 ●≡	N 3	NNE 6	N 6
12	34.7	36.1	38.2	36.3	8.1	9.0	9.6	9.1	10.4	8.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ●≡	10 9≡	10 ≡	N 8	N 12	N 7
13	39.9	42.4	43.3	41.9	9.9	13.1	12.0	11.8	14.6	8.2	81	76	87	81	2.3	3.7	1.9	2.6	3 ○	8 ○	4	N 8	NNE 4	ESE 4
14	41.6	40.9	39.8	40.8	10.9	8.8	9.3	9.6	12.5	8.4	94	100	93	96	0.8	0.0	0.8	0.5	10	10 ●≡	8	SSW 7	N 3	NW 3
15	38.1	37.9	37.8	37.9	7.4	8.0	7.4	7.6	10.2	7.2	94	100	79	91	0.6	0.0	2.1	0.9	9	10 ≡	8	NW 3	NNW 5	N 4
16	35.7	35.5	35.0	35.4	5.4	6.1	6.5	6.1	7.9	5.1	92	92	100	95	0.7	0.7	0.0	0.5	10 ●	10	10 ≡	NNE 6	NNW 8	NNW 12
17	33.1	35.0	35.9	34.7	4.5	6.3	6.5	6.0	8.2	4.3	100	92	96	96	0.0	0.7	0.5	0.4	10 ≡	9 ●	8	NNW 17	NNW12	NNW 14
18	36.8	36.9	35.6	36.4	6.1	7.8	8.5	7.7	9.7	5.5	83	85	83	84	1.6	1.6	1.9	1.7	3 ○	8 ●	9	NW 14	W 5	SSW 7
19	33.8	33.8	32.3	33.3	8.6	12.6	10.6	10.6	13.5	7.6	84	74	100	86	1.8	3.8	0.0	1.9	4 ○	8 ○	10	SW 8	SW 7	SSW 14
20	30.3	31.1	30.4	30.6	9.3	8.4	6.3	7.6	10.6	6.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 9≡	SW 10	SW 6	N 8
21	29.9	30.2	30.2	30.1	5.8	7.6	7.2	7.0	10.4	3.9	100	97	82	93	0.0	0.3	1.9	0.7	10 ≡	9	5	NW 7	WSW 7	NNW 8
22	28.3	27.9	27.2	27.8	5.6	5.3	8.6	7.0	8.8	4.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●≡	10 ●≡	N 17	WNW20	NNW 12
23	27.4	29.7	32.5	29.9	8.7	7.6	7.9	8.0	9.3	7.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ●≡	10 ●≡	10 ●≡	N 17	N 20	N 22
24	33.8	34.8	35.2	34.6	6.4	4.8	4.7	5.2	8.2	4.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	7	N 14	NNW14	NNW 12
25	35.2	34.8	32.2	34.1	3.4	4.4	6.5	5.2	7.6	2.4	100	100	100	100	0.0	0.0	0.0	0.0	7	10 ●≡	10 ≡	NNW 12	WSW14	NW 17
26	33.7	35.1	33.3	34.0	5.2	7.1	6.5	6.3	7.8	3.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ●≡	WNW 20	W 14	WSW 17
27	30.8	29.5	30.0	30.1	7.4	5.4	4.1	5.2	8.1	3.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 9≡	WSW 17	WSW17	WNW 12
28	30.4	32.0	32.5	31.6	2.7	4.9	4.9	4.4	6.3	2.2	100	95	100	98	0.0	0.5	0.0	0.2	8 ○	8 ○	10 ●≡	WSW 8	WSW 8	WSW 10
29	33.0	35.2	37.0	35.1	3.1	5.4	5.4	4.8	6.5	3.0	100	100	100	100	0.0	0.0	0.0	0.0	9 ●	10 ≡	8	NNW 8	WSW10	W 14
30	38.7	39.8	41.5	40.0	5.8	6.0	6.1	6.0	6.5	5.4	100	100	100	100	0.0	0.0	0.0	0.0	10 9≡	10 ≡	10 9≡	WNW 8	WNW14	NNW 17
31	43.4	45.6	46.1	45.0	5.1	6.3	5.7	5.7	7.1	4.4	100	100	62	87	0.0	0.0	3.5	1.2	10 9≡	10 9≡	0	N 12	W 2	WNW 2
M	37.2	37.9	37.8	37.6	9.2	10.2	9.7	9.7	12.5	7.3	88	88	88	88	2.0	2.2	1.9	2.0	7.4	8.4	7.4	8.9	8.5	9.3

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1	46.1	47.3	46.8	46.7	9.5	9.7	9.3	9.4	12.9	5.4	56	99	86	80	5.3	0.1	1.6	2.3	0	10 ≡	0	N 3	NW 3	NNW 5
2	45.5	45.3	43.9	44.9	6.6	7.4	3.8	5.4	10.2	3.7	100	96	100	99	0.0	0.5	0.0	0.2	7 ○	7 ○	10 ≡	N 10	N 12	N 14
3	43.5	43.5	42.4	43.1	2.5	3.5	2.9	3.0	4.3	2.2	98	100	100	99	0.1	0.0	0.0	0.0	6	10 ≡	10	N 12	NNW 7	N 14
4	43.4	44.3	44.7	44.1	3.6	5.0	5.1	4.7	6.7	2.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	N 4	NNW 3	N 6
5	44.9	46.3	45.7	45.6	5.4	8.9	7.5	7.3	10.4	4.8	100	93	96	96	0.0	0.8	0.5	0.4	3 ○	8	4	N 5	C 0	NNE 5
6	45.4	45.1	43.1	44.5	8.1	10.3	10.3	9.8	12.5	7.4	72	86	72	77	3.1	1.8	3.5	2.8	1 ○	8	7	C 0	ESE 2	SSW 7
7	39.6	38.4	36.5	38.2	8.5	10.8	9.7	9.7	11.8	8.1	100	100	87	96	0.0	0.0	1.6	0.5	9	10 ≡	10 ●	SSW 9	SW 8	WNW 12
8	35.0	36.5	36.2	35.9	7.0	8.4	9.4	8.6	10.4	6.4	100	100	72	91	0.0	0.0	3.4	1.1	9 ≡	8	6	NNW 14	NNW 6	WSW 1
9	33.4	32.0	30.0	31.8	9.4	11.8	12.0	11.3	13.4	7.8	69	94	100	88	3.6	0.8	0.0	1.5	6	9	10 ≡	SSW 7	SSW14	S 12
10	28.0	29.7	32.6	30.1	8.0	8.4	8.1	8.2	12.4	7.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ●≡	9▲●	10 ≡	WSW 17	WSW20	WSW 21
11	35.6	37.4	38.7	37.2	8.3	13.0	13.3	12.0	14.7	7.2	96	69	76	80	0.5	4.7	3.7	3.0	5 ○	7	4	SW 20	SW 20	SSW 12
12	37.2	38.3	38.4	38.0	10.3	10.7	9.1	9.8	13.5	8.7	94	100	79	91	0.8	0.0	2.5	1.1	10	10 ≡	8	W 3	SW 5	SW 10
13	39.5	41.0	39.6	40.0	8.5	11.7	11.5	10.8	15.1	8.1	79	69	64	71	2.4	4.3	5.0	3.9	8	5 ○	10 ●	WSW 9	W 5	SSE 5
14	37.3	37.1	35.0	36.5	9.4	9.4	7.8	8.6	12.1	7.5	100	100	94	98	0.0	0.0	0.6	0.2	9	10 ≡	8	SW 8	SW 14	WNW 9
15	34.4	35.1	35.5	35.0	7.2	8.9	9.3	8.7	9.8	6.6	80	83	95	86	2.0	2.0	0.6	1.5	2 ○	8 ○	10	W 8	WSW 5	SSW 7
16	35.1	35.2	35.6	35.3	6.4	4.8	4.6	5.1	9.9	3.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	9	8	W 9	WSW 7	WSW 10
17	34.1	34.4	34.1	34.2	2.8	3.3	4.5	3.8	5.0	2.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●≡	10 ●≡	WSW 12	SW 12	WSW 14
18	32.5	33.4	34.3	33.4	4.6	5.9	5.6	5.4	6.7	3.9	100	100	84	95	0.0	0.0	1.5	0.5	10 9≡	10 ≡	6	WSW 17	SW 14	WNW 12
19	36.5	38.7	40.1	38.4	5.3	6.0	5.2	5.4	7.5	3.9	87	100	100	96	1.2	0.0	0.0	0.4	8 ○	10 ≡	10 ≡	NNW 4	NNE 5	N 10
20	41.0	41.6	41.6	41.4	5.1	8.0	7.1	6.8	9.3	4.4	85	80	100	88	1.3	2.2	0.0	1.2	3 ○	5 ○	10	WNW 7	WSW 9	WNW 8
21	39.8	39.3	35.7	38.3	8.1	8.1	5.5	6.8	9.0	5.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 9≡	10 9≡	NW 7	SSW 4	NNW 12
22	34.3	35.1	34.9	34.8	3.1	2.7	1.0	2.0	5.9	0.5	100	95	98	98	0.0	0.4	0.2	0.2	10 ≡	7 ○	3	NNW 17	NNW14	NNW 14
23	34.7	35.3	34.0	34.7	2.5	6.7	4.6	4.6	8.3	0.1	76	81	93	83	1.7	1.8	0.6	1.4	0 ○	7 ○	0	NW 5	SW 2	S 12
24	30.9	29.8	33.3	31.3	5.1	7.5	3.0	4.6	8.9	2.0	100	100	85	95	0.0	0.0	1.1	0.4	4 ○	10 ●≡	1	SW 14	SW 20	WNW 17
25	35.1	34.9	34.2	34.7	2.5	6.3	6.7	5.6	8.6	0.7	100	85	100	95	0.0	1.4	0.0	0.5	10 ≡	7 ○	10 ≡	SW 17	SSW21	SSW 14
26	31.5	32.9	34.4	32.9	1.6	3.2	2.8	2.6	6.9	1.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 20	SW 20	WSW 20
27	35.1	35.2	34.9	35.1	2.2	3.5	3.7	3.3	4.4	1.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 14	SW 14	SW 12
28	33.6	34.9	36.9	35.1	2.2	3.2	2.1	2.4	4.7	1.9	100	100	100	100	0.0	0.0	0.0	0.0	8	10 9≡	10 ●	SW 6	SSW 7	NW 9
29	37.9	39.6	40.7	39.4	1.6	2.4	2.2	2.1	4.2	1.4	100	91	100	97	0.0	0.7	0.0	0.2	10 ≡	9	10 ≡	NNW 14	NW 9	NW 12
30	40.4	41.3	39.9	40.5	1.0	2.3	1.5	1.6	4.2	0.8	100	96	84	93	0.0	0.3	1.0	0.4	10 ≡	9	2	NNW 14	WNW 6	W 14
31	37.6	37.6	36.9	37.4	2.2	2.9	2.1	2.3	3.9	1.0	100	100	100	100	0.0	0.0	0.0	0.0	8	8	10 ●≡	SSW 20	SW 17	SW 17
M	37.4	38.0	37.8	37.7	5.4	6.9	6.2	6.2	9.0	4.2	93	94	92	93	0.7	0.7	0.9	0.8	7.3	8.7	7.6	10.5	9.8	11.2

Śnieżka

$H_s = 1603\ m$ $H_b = 1610\ m$ $h_w = 18\ m$

Lipiec – Juillet 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONIECZNIENIE	POGODA
1	8	1.0	.	9.9	
2	6	0.2	.	8.4	
3	9	.	.	10.8	2.VII: ○ na. p
4	8	.	.	12.7	
5	8	0.0	.	11.2	
6	8	18.8	.	11.1	
7	8	.	.	10.7	
8	7	23.1	.	6.3	
9	7	7.3	.	4.2	
10	6	31.2	.	0.6	
11	0	89.0	.	.	9.VII: 725–930 1940–51 ≈–2005 ≫–2015 ○ a. p
12	0	3.1	.	0.1	
13	8	5.4	.	8.0	
14	3	22.4	.	2.2	
15	0	1.0	.	1.0	
16	8	0.1	.	0.7	
17	8	0.5	.	4.3	
18	7	1.2	.	4.2	
19	8	0.2	.	0.4	17.VII: ○ a. p z prz.
20	0	19.3	.	.	
21	8	0.5	.	5.2	
22	0	62.2	.	.	
23	0	69.6	.	.	
24	0	3.3	.	0.8	
25	0	7.8	.	1.5	
26	0	19.0	.	0.1	
27	0	7.6	.	.	
28	9	7.3	.	5.5	
29	0	3.3	.	1.3	
30	0	11.6	.	.	
31	0	0.2	.	.	21.VII: ○ a. p z prz 30.VII: ≫–2300 ≈–24
Σ	—	416.2	—	129.2	UWAGI.

Sierpień – Août

1	7	.	.	9.0	
2	7	.	.	5.0	
3	0	0.0	.	0.4	
4	0	0.0	.	1.3	
5	7	.	.	7.4	
6	9	.	.	6.4	
7	0	3.3	.	0.8	
8	6	.	.	5.3	
9	7	11.2	.	6.1	7.VIII:
10	8	6.2	.	1.4	
11	9	0.4	.	10.7	
12	0	0.0	.	1.5	
13	9	2.3	.	6.9	10.VIII: 12.VIII: ○ a. p z prz
14	0	0.8	.	0.7	
15	9	1.7	.	8.1	virga
16	7	5.3	.	0.6	
17	0	2.7	.	.	
18	0	2.4	.	0.3	
19	0	2.8	.	0.8	
20	7	0.4	.	9.9	
21	0	7.0	.	0.6	19.VIII:
22	8	1.1	.	4.3	
23	9	0.2	.	10.6	
24	0	13.5	.	0.7	
25	9	0.6	.	9.5	
26	0	3.0	.	0.2	
27	0	2.5	.	0.6	
28	0	2.2	.	0.1	27.VIII: ○ na. a. p z prz
29	8	.	.	1.7	virga
30	7	.	.	2.1	
31	7	4.3	.	2.0	
Σ	—	73.9	—	115.0	UWAGI. 31.VIII:

Śnieżka — φ = 50°44' — λ = 15°44' — Wrzesień – Septembre 1957

Dzień	CIŚNIENIE P − 800				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	37.0	38.6	38.6	38.1	0.7	1.9	3.0	2.2	4.2	0.4	100	98	98	99	0.0	0.1	0.2	0.1	7 ⊙	9	3	W 14	SSW10	WSW20
2	38.5	37.0	36.7	37.4	3.3	4.4	5.1	4.5	6.0	2.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ●≡	SSW 9	SSW14	SW 10
3	36.7	0.1	38.9	37.9	3.2	3.4	2.3	2.8	5.7	2.2	100	98	100	99	0.0	0.1	0.0	0.0	5 ⊙	10 ●	10	NW 6	N 2	N 3
4	39.5	42.0	43.5	41.7	1.7	2.4	2.2	2.1	3.9	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ≡	10 ≡	N 9	NNW 7	N 6
5	42.2	41.6	41.1	41.6	1.8	4.5	5.3	4.2	6.6	1.3	69	95	85	83	2.2	0.4	1.3	1.3	4 ⊙	4 ⊙	8	WSW 5	SW 12	WSW10
6	40.5	41.3	42.2	41.3	6.2	7.1	8.7	7.7	9.9	5.2	80	100	67	82	2.0	0.0	3.6	1.9	8 ⊙	9	6	WNW 5	SW 6	W 4
7	41.6	42.7	42.8	42.4	7.9	9.7	9.7	9.2	11.6	7.3	100	85	100	95	0.0	1.8	0.0	0.6	10 ≡	7 ⊙	5	SW 12	SSW 9	SSW10
8	43.7	45.3	44.4	44.5	11.4	14.6	11.2	12.1	16.7	8.5	74	63	100	79	3.5	6.2	0.0	3.2	4 ⊙	2 ⊙	10 ≡	SSW 5	SSW 8	SSW12
9	44.6	45.8	45.0	45.1	14.7	12.4	6.6	10.1	19.8	6.4	55	100	100	85	7.6	0.0	0.0	2.5	2 ⊙	10 ≡	10 ● ≡	W 3	C 0	N 6
10	44.0	42.9	40.6	42.5	5.4	6.8	5.1	5.6	9.3	3.9	92	92	100	95	0.7	0.8	0.0	0.5	4 ⊙	8 ⊙	10	WNW 5	SW 3	SSW 8
11	35.9	32.5	27.0	31.8	4.2	6.1	7.4	6.3	7.6	3.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ●≡	SW 14	SW 14	SW 17
12	21.5	23.8	26.3	23.9	7.2	3.3	0.7	3.0	8.1	0.6	100	86	100	95	0.0	1.1	0.0	0.4	10 ● ≡	7	10 ≡	SW 25	SW 17	SW 26
13	27.5	25.9	23.4	25.6	0.0	1.6	1.1	1.0	2.4	-0.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10▲≡	SW 23	SW 25	SW 21
14	26.0	26.2	28.4	26.9	-0.9	0.0	0.6	0.1	1.4	-1.5	99	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 23	SW 24	SW 12
15	27.1	31.0	33.7	30.6	-0.7	0.0	0.0	-0.2	1.1	-1.0	99	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 17	WSW12	SW 17
16	32.7	33.6	35.8	34.0	-1.9	-1.2	-1.9	-1.7	0.3	-2.8	100	99	100	100	0.0	0.1	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 21	SW 14	W 12
17	36.1	36.6	35.8	36.2	-0.6	-0.1	-0.1	-0.2	0.4	-1.9	99	100	100	100	0.0	0.0	0.0	0.0	10 ≡	7 ⊙	10 ≡	WSW 12	W 12	NW 14
18	34.1	35.2	35.2	34.8	0.3	0.9	1.1	0.8	2.0	-0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	4	NNW 17	NNW17	NNW17
19	32.7	31.7	31.9	32.1	3.9	5.4	5.3	5.0	6.0	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10●≡	W 17	WNW20	W 14
20	31.0	34.1	35.5	33.5	2.5	2.8	2.4	2.5	5.7	0.7	75	100	90	88	1.9	0.0	0.7	0.9	9	9 ⊙	10	NNW 20	NW 12	NW 7
21	35.9	37.3	37.3	36.7	2.0	6.2	7.1	5.6	8.4	1.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	WNW 12	W 12	SW 12
22	33.9	35.7	34.3	34.6	7.6	8.0	8.2	8.0	9.0	6.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	WSW 17	WSW12	WSW17
23	29.6	24.7	27.4	27.2	7.6	8.0	5.2	6.5	8.7	4.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●≡	10 ●≡	SW 17	SW 26	WNW21
24	29.5	28.3	30.9	29.6	4.1	5.9	-3.0	1.0	6.1	-3.2	100	100	97	99	0.0	0.0	0.1	0.0	10 ≡	10 ●≡	10 ≡	WSW 20	WSW20	NNW20
25	33.6	37.0	37.1	35.9	-4.8	-2.4	-2.8	-3.2	-0.1	-5.7	95	93	95	94	0.2	0.3	0.2	0.2	10 ≡	4 ⊙	4	NW 17	WNW 6	NNW 9
26	34.6	34.0	36.6	35.1	-1.2	-1.7	-3.7	-2.6	-0.2	-3.9	91	98	97	95	0.5	0.1	0.2	0.3	10	10 ≡	0	NW 3	N 3	NNE 6
27	37.4	37.4	29.7	34.8	-3.2	-1.6	-0.5	-1.4	0.6	-5.7	65	94	100	86	1.6	0.3	0.0	0.6	5 ⊙	10	10 ≡	NNW 8	SW 5	WSW31
28	28.7	29.2	30.3	29.4	-0.4	0.6	0.7	0.4	1.6	-2.3	100	100	100	100	0.0	0.0	0.0	0.0	10▲≡	9	10●≡	NNW 26	NNW23	NW 21
29	27.0	23.5	23.3	24.6	1.7	1.5	-0.9	0.4	2.2	-0.9	100	100	99	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ●≡	10✳≡	WSW 20	SW 17	WNW10
30	25.2	26.8	33.0	29.0	-5.1	-3.8	-3.6	-4.0	-0.4	-5.5	95	96	99	97	0.2	0.2	0.1	0.2	10 ≡	10 ≡	10 ≡	WNW 20	WNW14	N 6
31																								
M	34.3	34.7	34.9	34.6	2.6	3.6	2.8	3.0	5.5	0.7	93	97	98	96	0.7	0.4	0.2	0.4	8.6	8.8	8.7	14.1	12.5	13.3

Październik – Octobre

1	33.9	35.3	36.9	35.4	-4.6	-2.7	-3.3	-3.5	-1.7	-5.1	96	100	99	98	0.2	0.0	0.0	0.1	4	10△≡	10 ≡	NNW 6	NNW 5	W 10
2	39.2	40.4	39.7	39.8	-2.9	-1.8	-3.6	-3.0	-0.9	-4.4	97	100	99	99	0.1	0.0	0.1	0.1	10△≡	10 ≡	3	WNW 5	W 2	W 3
3	35.4	33.9	32.4	33.9	-3.2	-1.9	-1.0	-1.8	-0.4	-4.9	99	83	99	94	0.0	0.9	0.1	0.3	6	9	10 ≡	SW 14	SW 14	WNW17
4	31.1	33.8	39.7	34.9	-4.7	-4.4	-3.5	-4.0	-0.5	-4.9	98	98	97	98	0.1	0.1	0.1	0.1	9	4 ⊙	10 ≡	NNW 17	NNW22	NNW17
5	40.8	39.9	39.0	39.9	-4.6	-3.1	-1.9	-2.9	-1.1	-4.7	98	97	92	96	0.1	0.1	0.4	0.2	6	6 ⊙	8	WNW 7	SW 12	WSW12
6	39.3	41.8	44.4	41.8	1.1	1.4	0.6	0.9	2.4	-1.9	100	98	96	98	0.0	0.2	0.3	0.2	9	10	7	NW 12	NNW12	NNW 7
7	45.2	45.4	45.8	45.5	6.2	9.1	8.4	8.0	12.6	0.4	100	77	84	87	0.0	2.8	1.7	1.5	2 ⊙	0 ⊙	0	WNW 4	NW 1	SW 1
8	46.1	47.4	46.9	46.8	10.4	9.0	8.8	9.2	10.7	7.7	40	73	47	53	7.6	3.2	5.9	5.6	0 ⊙	1 ⊙	0	NNE 3	SSW 5	S 8
9	44.7	45.5	43.3	44.5	5.2	9.2	3.6	5.4	9.5	2.4	55	33	100	63	4.0	7.7	0.0	3.9	0 ⊙	1 ⊙	3	SSW 12	SSW12	SSW12
10	41.8	43.4	43.4	42.9	5.2	10.9	9.9	9.0	11.6	3.6	66	47	60	58	2.9	6.9	4.9	4.9	0 ⊙	0 ⊙	2	SSW 14	SW 7	WSW 3
11	42.5	42.4	42.2	42.4	8.7	10.7	10.1	9.9	11.9	4.6	58	40	44	47	4.6	7.8	7.0	6.5	6 ⊙	1 ⊙	0	SSW 1	SSW 4	W 5
12	42.1	43.7	46.5	44.1	6.9	5.8	3.2	4.8	11.4	2.7	94	100	100	98	0.5	0.0	0.0	0.2	7	10●≡	10 ≡	NNW 6	NNW10	NNW 4
13	46.4	45.6	44.7	45.6	3.3	4.3	4.5	4.2	6.0	2.6	82	89	98	90	1.3	0.9	0.1	0.8	0 ⊙	4 ⊙	10 ≡	WSW 5	SW 8	SSW 8
14	44.0	44.5	45.0	44.5	3.6	4.7	2.3	3.2	6.4	2.2	98	100	100	99	0.1	0.0	0.0	0.0	9	10● ≡	10 ≡	WNW 5	NNW 2	WSW 3
15	45.4	46.1	45.5	45.7	0.6	2.8	1.8	1.8	5.7	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	3 ⊙	10 ≡	SW 2	WSW 3	SSW 5
16	43.8	42.9	41.4	42.7	2.6	7.0	7.5	6.2	8.8	1.0	96	54	43	64	0.3	4.6	5.9	3.6	1 ⊙	0 ⊙	0	SSW 4	SW 5	SW 8
17	39.1	40.3	39.7	39.7	5.9	3.7	3.7	4.2	8.0	2.5	100	100	100	100	0.0	0.0	0.0	0.0	9	9 ⊙	10 ≡	W 14	W 17	SW 14
18	34.8	35.2	35.3	35.1	5.8	5.9	6.6	6.2	6.9	3.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10● ≡	10 ≡	SW 20	SW 17	SW 17
19	34.3	33.6	31.4	33.1	5.7	6.5	6.7	6.4	8.0	4.8	98	100	100	99	0.2	0.0	0.0	0.1	7	9	10 ≡	SW 12	SW 9	SSW14
20	32.3	34.5	36.1	34.3	2.5	0.9	-0.9	0.4	7.1	-0.9	96	100	99	98	0.3	0.0	0.0	0.1	10 ●	10 ≡	0	NW 8	WNW 3	NW 5
21	35.7	34.0	30.9	33.5	-2.1	0.1	-2.2	-1.6	1.3	-2.4	83	76	100	86	0.9	1.5	0.0	0.8	4 ⊙	2 ⊙	10 ≡	SW 5	SW 8	SW 12
22	26.0	24.6	24.6	25.1	-1.1	-0.3	-1.0	-0.8	0.3	-2.8	99	100	97	99	0.1	0.0	0.2	0.1	6	10 ≡	9	SW 12	SW 8	SW 9
23	27.1	31.2	33.1	30.5	-2.5	-1.5	-3.9	-3.0	-0.3	-4.1	100	99	96	98	0.0	0.1	0.2	0.1	10 ≡	6 ⊙	3	N 14	W 3	WSW14
24	33.6	36.7	41.0	37.1	-1.0	2.9	1.4	1.2	3.5	-4.9	99	100	100	100	0.1	0.0	0.0	0.0	10 ≡	10●≡	10 ≡	W 20	WNW14	NNW12
25	42.4	43.8	44.0	43.4	0.1	2.4	3.7	2.5	4.4	-0.2	100	96	77	91	0.0	0.3	1.9	0.7	10 ≡	5 ⊙	0	NW 12	NW 4	WNW 1
26	42.4	42.1	41.3	41.9	4.1	4.8	6.3	5.4	6.8	2.7	63	55	44	54	3.1	3.9	5.2	4.1	3 ⊙	1 ⊙	0	S 5	SSW 6	SW 6
27	39.2	39.0	38.3	38.8	4.1	5.5	4.1	4.4	7.3	1.4	70	42	52	55	2.5	5.1	4.0	3.9	1 ⊙	1 ⊙	0	SSW 8	SW 4	SW 6
28	37.8	38.6	39.2	38.5	4.7	5.5	6.1	5.6	7.0	-0.1	50	51	37	46	4.2	4.4	5.9	4.8	0 ⊙	1 ⊙	0	WSW 5	WNW 4	WSW 6
29	37.9	38.6	38.0	38.2	0.3	1.2	3.2	2.0	6.9	-0.8	100	100	65	88	0.0	0.0	2.7	0.9	10 ≡	7	8	WSW 14	SW 10	SW 12
30	36.5	36.5	38.1	37.0	3.3	5.9	6.7	5.6	8.9	1.3	72	50	36	53	2.2	4.6	6.3	4.4	7	6 ⊙	4	SW 12	SW 8	SSW 5
31	35.9	34.9	32.8	34.5	5.7	6.6	2.7	4.4	9.2	1.9	92	37	78	69	0.8	6.1	1.6	2.8	2 ⊙	8	6	WSW 14	WSW14	SW 12
M	38.6	39.2	39.4	39.1	2.2	3.6	2.9	2.9	5.7	0.1	87	80	82	83	1.2	2.0	1.8	1.7	5.7	5.6	5.6	9.4	8.2	8.6

Śnieżka

H_s = 1603 m H_b = 1610 m h_- = 18 m

Wrzesień – Septembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONIECZNIENIE	POGODA
1	9	0.0	.	1.7	
2	0	2.1	.	.	
3	7	4.0	.	0.5	
4	0	0.1	.	2.3	
5	8	0.7	.	9.6	
6	7	.	.	3.7	
7	9	.	.	7.6	
8	9	.	.	11.5	
9	0	10.2	.	6.3	
10	8	.	.	6.4	
11	0	21.2	.	0.7	
12	9	1.2	.	3.7	
13	0	5.1	.	.	
14	0	0.5	.	.	
15	0	0.3	.	0.3	
16	0	3.7	.	.	
17	8	2.2	22	2.9	
18	0	0.3	pż.	2.8	
19	0	4.5	pż.	.	
20	9	.	.	7.1	
21	1	4.7	.	6.4	
22	0	1.7	.	.	
23	0	22.7	.	.	
24	0	9.4	.	.	
25	8	.	.	8.0	
26	0	0.6	.	.	
27	9	2.4	.	4.8	
28	7	5.5	.	0.6	
29	0	7.0	.	.	
30	0	.	.	5.0	
31					
Σ	—	110.1	—	91.9	UWAGI

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1	1	0.2	1	4.0	
2	0	1.4	1	0.7	
3	8	1.1	2	4.6	
4	8	1.0	2	3.7	
5	7	0.2	2	6.5	
6	8	0.6	pż.	1.2	
7	9	.	pż.	10.2	
8	8	.	pż.	9.9	
9	9	.	pż.	9.9	
10	9	.	.	9.7	
11	8	.	.	10.0	
12	0	0.1	.	3.2	
13	6	.	.	7.7	
14	0	0.0	.	0.3	
15	8	.	.	4.0	
16	8	.	.	9.8	
17	8	1.0	.	4.2	
18	0	1.3	.	.	
19	8	1.2	.	4.2	
20	0	2.3	.	.	
21	9	.	.	9.4	
22	0	0.4	.	4.1	
23	7	.	.	3.9	
24	0	1.0	.	0.2	
25	7	.	.	6.7	
26	8	.	.	9.4	
27	9	.	.	9.2	
28	9	.	.	9.2	
29	8	.	.	0.1	
30	8	.	.	5.3	
31	8	.	.	6.6	
Σ	—	11.8	—	167.9	UWAGI

Śnieżka — φ = 50°44' — λ = 15°44' — Listopad – Novembre 1957

DNI	CIŚNIENIE P − 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,∞			WIATR i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	26.4	26.9	29.8	27.7	0.7	0.3	1.9	1.2	3.9	-1.7	100	100	100	100	0.0	0.0	0.0	0.0	9	10 =	10 =	SW 26	SW 21	SW 14
2	31.0	31.9	33.1	32.0	-1.9	-1.1	0.2	-0.6	2.1	-2.5	79	71	60	70	1.1	1.7	2.5	1.8	9	10	10	SW 12	SW 12	SW 5
3	33.4	33.1	33.1	33.2	-1.9	0.0	1.4	0.2	2.2	-2.0	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 9 =	SW 3	SSW 9	S 9
4	33.6	33.5	34.2	33.8	6.3	6.5	2.3	4.4	6.9	1.4	42	43	90	58	5.6	5.7	0.7	4.0	2 ○	8 ⊙	4	SSW 3	SSW 7	S 6
5	27.2	26.2	29.1	27.5	1.5	2.1	2.5	2.2	3.4	0.9	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 =	SSW 25	SSW20	SSW 9
6	29.9	30.7	26.0	28.9	5.3	7.7	3.9	5.2	7.9	1.9	61	41	100	67	3.5	6.2	0.0	3.2	7	8	10 =	SSW 8	SSW 6	S 23
7	27.5	29.2	28.9	28.5	6.5	3.6	3.2	4.1	6.5	1.9	82	98	100	98	1.8	0.1	0.0	0.6	9	10 ●	10 ● =	WSW 9	SW 8	S 6
8	26.9	27.0	27.8	27.2	3.8	3.2	3.6	3.6	4.1	2.6	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 = 9	10 ● =	SSW 14	SSW17	SSW 8
9	25.8	26.5	28.6	27.0	3.1	2.8	2.1	2.5	3.8	1.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● =	10 ● =	10 =	SSW 14	SW 10	SSW10
10	28.4	27.5	29.9	28.6	-0.1	2.3	2.1	1.6	3.2	-0.1	100	100	100	100	0.0	0.0	0.0	0.0	6	10 =	10 =	SSE 12	SSW20	SE 14
11	30.6	32.1	33.2	32.0	0.9	0.0	-0.7	-0.1	2.7	-2.1	96	100	99	98	0.2	0.0	0.0	0.1	6	10 =	10 9 =	E 14	NE 9	ENE 7
12	36.2	38.7	40.9	38.6	-2.7	-2.6	-2.9	-2.8	-0.7	-4.9	100	100	99	100	0.0	0.0	0.0	0.0	10 ✳ =	10 9 =	0 =	NE 17	NE 14	NE 12
13	39.5	40.9	41.2	40.5	-7.1	-3.1	-3.4	-4.2	-2.3	-8.0	99	40	45	61	0.0	2.9	2.6	1.8	10 =	1 ⊙	0	NE 14	NE 8	ENE 8
14	41.6	42.9	42.9	42.5	-1.9	2.1	0.1	0.1	3.4	-4.8	48	44	38	43	2.8	4.0	3.9	3.6	0 ○	0 ⊙	0	E 12	SE 10	SSE12
15	42.7	43.4	43.6	43.2	-4.3	-0.7	-3.5	-3.0	2.6	-5.0	96	79	99	91	0.2	1.2	0.0	0.5	10 =	1 ⊙	10 =	S 17	SSW10	SSW 5
16	43.1	44.1	44.9	44.0	-0.5	0.7	-0.2	0.0	1.1	-3.5	78	76	70	75	1.4	1.5	1.8	1.6	7	9	6	NNW 12	NNW12	NNW12
17	44.8	44.9	44.5	44.7	0.3	2.3	-1.1	0.1	4.5	-1.1	94	65	91	83	0.3	2.5	0.5	1.1	8	3 ⊙	0	NW 7	NNW 2	N 4
18	43.4	43.2	42.7	43.1	1.4	3.2	0.3	1.3	3.7	-1.6	37	36	67	47	4.3	5.0	2.0	3.8	0	0 ⊙	0	NE 3	ESE 3	SE 5
19	42.5	43.6	44.9	43.7	-0.3	-0.3	-2.0	-1.2	1.6	-2.2	47	36	54	46	3.2	3.9	2.5	3.2	0	6 ⊙	0	ESE 4	ESE 5	ESE 6
20	45.7	45.9	46.2	45.9	-2.5	-6.7	-7.3	-6.0	-0.4	-10.4	36	73	93	67	3.3	1.0	0.2	1.5	0	0 ⊙	8 =	SE 8	SSE12	SSW21
21	46.1	45.5	42.0	44.5	-8.0	-5.6	-6.7	-6.8	-3.7	-8.6	96	92	94	94	0.1	0.3	0.2	0.2	0	1 ⊙	0	SSW 20	SSW20	SSW17
22	35.2	33.6	31.9	33.6	-8.7	-6.1	-9.3	-8.4	-4.4	-9.8	98	94	98	97	0.1	0.2	0.1	0.1	10 =	0	10 =	SSW 17	SW 12	SSW12
23	32.7	32.2	36.5	33.8	-4.0	-6.7	-6.7	-6.0	-3.4	-9.4	96	99	99	98	0.2	0.0	0.0	0.1	10 =	4	10 =	NW 10	WNW23	NNW20
24	38.4	39.4	38.7	38.8	-8.9	-5.2	-4.4	-5.7	-4.0	-9.0	98	95	96	96	0.1	0.2	0.2	0.2	6	10 =	10 =	N 14	NNW14	NNW14
25	38.3	38.5	40.4	39.1	-2.0	-0.1	0.0	-0.5	0.3	-4.9	98	100	100	99	0.1	0.0	0.0	0.0	10 =	10 ● =	10 9 =	NNW 14	NNW21	NNW14
26	41.3	42.1	39.6	41.0	0.1	0.4	4.8	2.5	5.7	-0.3	88	100	21	70	0.8	0.0	6.8	2.5	3	10	0	NNW 12	NNW 3	NW 12
27	35.9	35.9	37.2	36.3	-1.4	-1.9	-1.3	-1.5	5.5	-4.5	99	100	99	99	0.1	0.0	0.1	0.1	10 =	10 =	10 =	NNW 23	NNW 23	NNW17
28	35.5	34.1	30.0	33.2	-0.8	-1.1	-0.6	-0.8	2.4	-2.4	99	99	99	99	0.0	0.1	0.0	0.0	10 =	10 =	10 9 =	NNW 23	WNW 23	WNW25
29	27.1	26.7	32.9	28.9	-4.6	-9.0	-11.9	-9.4	-0.1	-12.1	98	92	93	94	0.1	0.3	0.2	0.2	10 △ =	10 △ =	10 =	N 27	N 29	N 25
30	38.2	38.4	38.3	38.3	-19.2	-15.5	-13.5	-15.4	-11.5	-20.3	83	96	92	90	0.2	0.1	0.2	0.2	0	10 ✳ =	10 ✳ =	N 9	NNE12	N 17
31																								
M	35.6	36.0	36.4	36.0	-1.7	-1.0	-1.6	-1.5	1.6	-4.0	85	82	86	84	1.0	1.2	0.8	1.0	6.7	7.0	6.9	13.4	13.2	12.6

Grudzień – Décembre

1	38.2	39.6	38.2	38.7	-15.1	-12.4	-10.0	-11.9	-9.1	-15.2	96	89	91	92	0.1	0.3	0.3	0.2	10 ✳ =	3 ⊙	10 △ =	N 10	N 7	N 9
2	37.2	37.5	38.1	37.6	-9.8	-7.6	-7.7	-8.2	-7.0	-10.3	91	99	99	96	0.3	0.0	0.0	0.1	10 △ =	10 =	10 △ =	NNW 7	N 8	N 12
3	37.3	35.7	36.6	36.5	-7.3	-5.0	-5.2	-5.7	-4.1	-8.4	99	95	98	97	0.0	0.2	0.1	0.1	10 △ =	10 △ =	10 ✳ =	N 17	NNE16	N 12
4	37.4	37.9	37.8	37.7	-5.5	-4.2	-5.4	-5.1	-3.4	-5.9	100	96	95	97	0.0	0.2	0.2	0.1	10 ✳ =	10 =	10 =	ENE12	N 8	NNE 9
5	36.1	36.5	38.7	37.1	-3.0	-4.2	-5.6	-4.6	-2.5	-5.6	97	98	100	98	0.1	0.1	0.0	0.1	10 △ =	10 =	10 =	NW 19	N 20	N 17
6	39.1	39.9	38.4	39.1	-6.4	-5.6	-2.9	-4.4	-1.4	-7.4	99	92	45	79	0.0	0.3	2.7	1.0	10 =	3 ⊙	0	N 10	NNE 6	SSE 5
7	33.4	29.4	23.3	28.7	-4.4	-3.5	-5.5	-4.7	-0.4	-7.0	55	52	85	64	2.0	2.3	0.6	1.6	4	9 ⊙	10	WSW 8	SW 6	W 17
8	12.8	7.9	5.3	8.7	-6.2	-4.3	-2.6	-3.9	0.1	-10.7	94	98	100	97	0.2	0.1	0.0	0.1	10 =	10 ✳ =	10 △ =	WSW28	WSW31	W 24
9	1.6	8.8	15.4	8.6	-3.8	-8.9	-10.3	-8.2	-1.7	-10.3	99	95	94	96	0.1	0.2	0.2	0.2	10 △ =	2 ○	10 =	WSW30	WNW16	WNW13
10	15.8	16.3	23.2	18.4	-8.5	-8.9	-13.0	-10.8	-8.4	-13.3	95	95	96	95	0.2	0.2	0.1	0.2	10 △ =	9 ✳ =	0	WSW 8	W 17	NNW10
11	20.7	19.7	17.1	19.2	-10.4	-5.3	-4.1	-6.0	-1.1	-13.9	90	98	72	87	0.3	0.1	1.2	0.5	7	10	10	SSW22	SSW16	S 10
12	17.5	17.8	16.3	17.2	-0.2	2.1	-0.1	0.4	2.9	-4.6	32	59	100	64	4.0	2.9	0.0	2.3	10	8 ⊙	10 =	SW 10	SW 8	SSW17
13	16.0	13.3	9.0	12.8	3.3	1.1	1.4	1.8	4.3	-0.6	68	98	100	89	2.4	0.1	0.0	0.8	9	9	10 =	S 7	SSW16	SSW 9
14	8.0	11.9	18.0	12.6	-0.2	-1.7	-6.9	-3.9	1.8	-7.5	100	98	99	99	0.0	0.1	0.0	0.0	10 =	10 △ =	10 ✳ =	N 5	NNW 2	NNW 4
15	23.5	28.3	32.0	27.9	-12.5	-10.7	-15.0	-13.3	-6.0	-15.3	96	97	96	96	0.1	0.1	0.1	0.1	10 =	10 =	0	NW 12	ENE19	E 30
16	34.0	35.8	35.3	35.0	-11.1	-9.3	-8.9	-9.6	-7.9	-16.2	39	30	18	29	1.6	2.1	2.5	2.1	0	1 ⊙	0	SE 18	SE 13	SE 16
17	34.9	34.1	34.3	34.4	-6.4	-4.1	-4.1	-4.7	-2.1	-9.6	99	96	98	98	0.0	0.2	0.1	0.1	10 =	0 ⊙	0	S 5	SSW 7	SW 6
18	34.6	34.5	34.5	34.5	-5.6	-7.7	-4.5	-5.6	-3.4	-9.0	97	96	90	94	0.1	0.1	0.4	0.2	10 =	10 =	0	SW 3	WSW 4	WSW 4
19	34.6	37.8	43.1	38.5	-10.1	-5.3	-4.2	-6.0	-3.9	-11.2	87	98	94	93	0.4	0.1	0.3	0.3	1	10 =	10 =	WNW 5	NW 11	NNW13
20	45.6	47.2	46.4	46.4	-5.2	-5.1	-3.2	-4.2	-2.7	-6.4	95	98	57	83	0.2	0.1	2.1	0.8	0	3 ⊙	0	NNW16	WSW 8	SW 8
21	43.9	43.3	44.1	43.8	-4.5	-3.3	-1.2	-2.6	0.1	-6.7	55	97	99	84	2.0	0.1	0.1	0.7	0	7	9	S 9	WNW13	W 7
22	43.0	42.8	39.7	41.8	-1.2	-0.3	-2.6	-1.6	-0.5	-2.8	99	100	93	97	0.1	0.0	0.3	0.1	9	10	0	W 5	WSW 1	S 12
23	33.0	32.3	31.6	32.3	-7.0	-6.5	-6.6	-6.7	-0.5	-7.1	45	86	81	71	2.0	0.5	0.7	1.1	0	2 ⊙	0	SSW25	SW 15	SW 15
24	32.4	33.6	35.0	33.7	-3.9	-1.1	-0.5	-1.5	0.3	-8.8	82	50	56	63	0.8	2.8	2.6	2.1	0	4 ⊙	0	SW 8	SW 7	SSW 4
25	34.9	35.2	38.3	36.1	-1.1	0.5	0.1	-0.1	1.8	-2.0	50	43	63	52	2.8	3.6	2.3	2.9	4	8 ⊙	10	SSW 9	W 5	NNW 6
26	39.0	40.6	42.0	40.5	0.5	-1.0	-1.3	-0.8	1.4	-3.1	71	89	55	72	1.8	0.7	2.5	1.7	10	5 ⊙	0	NW 18	NW 16	NW 9
27	41.5	41.4	40.9	41.3	-0.1	-0.6	0.3	0.0	2.3	-2.6	61	64	47	57	2.4	2.1	3.3	2.6	0	5 ⊙	0	WNW1	NW 14	W 7
28	35.8	33.5	29.0	32.8	0.7	-0.5	-5.2	-2.6	2.0	-7.5	56	62	100	73	2.8	2.3	0.0	1.7	0	0 ⊙	10 =	W 15	WSW13	W 21
29	26.6	25.8	23.2	25.2	-7.2	-7.9	-8.0	-7.8	-3.6	-8.3	99	96	98	98	0.0	0.1	0.1	0.1	10 =	10 △ =	10 △ =	W 22	WSW20	WSW24
30	21.0	19.3	18.2	19.5	-6.5	-6.1	-6.4	-6.4	-5.7	-8.1	99	100	99	99	0.0	0.0	0.0	0.0	10 △ =	10 △ =	10 =	WSW22	WSW25	WSW26
31	19.8	20.2	20.9	20.3	-7.7	-8.1	-7.5	-7.7	-5.6	-9.2	99	95	96	97	0.0	0.2	0.1	0.1	10 △ =	10 △ =	10 ✳ =	NW 16	W 11	W 17
M	30.0	30.2	30.4	30.2	-5.4	-4.7	-5.1	-5.1	-2.1	-8.2	82	86	84	84	0.9	0.7	0.7	0.8	6.9	6.8	6.1	13.4	12.2	12.7

Śnieżka

$H_c = 1603$ m $H_c = 1610$ m $h_w = 18$ m

Listopad – Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	0	0.1	.	0.4	
2	8	0.0	.	.	
3	0	0.4	.	.	
4	9	.	.	7.9	
5	0	.	.	0.1	
6	9	.	.	3.0	
7	8	7.5	.	.	
8	0	14.6	.	.	
9	0	6.4	.	.	
10	0	.	.	.	
11	0	14.0	.	.	
12	0	10.0	.	.	
13	9	.	.	8.3	
14	9	.	.	8.7	
15	9	.	.	6.5	
16	7	.	.	3.1	
17	8	.	.	7.4	
18	9	.	.	8.4	
19	9	.	.	7.8	
20	9	0.8	.	6.1	
21	9	0.6	.	4.9	
22	8	1.6	.	2.1	
23	7	1.1	.	1.6	
24	0	1.1	.	1.4	
25	0	15.6	.	.	
26	8	0.0	.	3.2	
27	0	1.7	.	.	
28	0	7.7	.	.	
29	0	10.8	1	.	
30	0	10.4	5	.	
31					
Σ	—	104.4	—	80.9	UWAGI

Grudzień – Décembre

1	8	8.0	8	3.0	
2	0	19.7	16	.	
3	0	19.7	48	.	
4	0	9.4	67	.	
5	1	3.4	71	3.3	
6	9	.	60	7.2	
7	9	0.0	60	6.7	
8	0	7.8	60	.	
9	9	3.0	68	5.0	
10	1	4.5	71	.	
11	8	0.0	75	.	
12	8	0.5	50	5.7	
13	9	0.9	40	.	
14	0	7.9	30	.	
15	0	0.1	37	0.8	
16	9	0.0	37	7.6	
17	8	0.0	30	3.9	
18	0	0.0	29	1.1	
19	0	2.6	27	1.8	
20	8	.	27	6.2	
21	9	0.0	24	4.8	
22	4	0.0	23	0.7	
23	9	.	23	6.9	
24	9	.	21	4.6	
25	9	.	20	1.3	
26	9	.	19	4.5	
27	8	.	19	5.8	
28	8	1.1	18	7.5	
29	0	5.1	18	0.5	
30	0	9.3	21	.	
31	0	7.8	23	0.2	
Σ	—	110.8	—	89.1	UWAGI

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ Styczeń – Janvier 1957

DNI	CIŚNIENIE p − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			POGODA			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	95.0	93.7	93.5	94.1	-9.2	-6.0	-5.1	-6.4	-4.9	-10.6	82	89	93	88	0.5	0.4	0.3	0.4	10	9	7	ESE 6	SSE 3	SE 3
2	91.6	91.6	93.5	92.2	-2.5	1.1	-0.2	-0.4	3.1	-5.1	93	83	94	90	0.4	1.1	0.4	0.6	10	9	10	SE 3	ESE 3	SE 3
3	97.3	98.6	99.5	98.5	-2.1	0.6	0.3	-0.2	1.1	-2.6	98	96	94	96	0.1	0.3	0.3	0.2	10	10	10	SE 2	ESE 1	SE 2
4	100.0	102.0	102.9	101.6	-1.5	0.4	0.6	0.0	0.8	-1.5	98	98	98	98	0.1	0.1	0.1	0.1	10	10	10	SE 2	SE 2	S 2
5	103.2	100.7	95.4	99.8	-3.7	0.9	0.6	-0.4	1.7	-5.0	99	87	98	95	0.1	0.9	0.1	0.4	0	10	10 •	S 2	SW 3	SW 5
6	92.2	89.7	87.6	89.8	1.4	2.1	3.4	2.6	4.4	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ●	10	SW 7	SW 6	SW 5
7	90.1	94.1	99.5	94.6	2.4	3.9	3.2	3.2	4.7	2.3	84	78	79	80	1.2	1.8	1.6	1.5	8	7 ⊙	6	W 9	W 6	NW 7
8	103.4	102.0	100.8	102.1	2.2	2.8	2.4	2.4	3.4	2.0	95	95	98	96	0.4	0.4	0.2	0.3	10	10	10	W 6	W 5	W 5
9	99.7	98.7	96.1	98.2	3.9	4.3	2.8	3.4	5.0	2.3	98	97	96	97	0.2	0.3	0.3	0.3	10 ●	10 ●	0	WSW 6	WSW 5	SW 3
10	91.8	88.4	89.4	89.9	0.2	2.4	1.0	1.2	3.0	-0.2	96	91	96	94	0.3	0.7	0.3	0.4	4	10	10	SW 5	SW 6	WSW 3
11	89.5	91.2	93.9	91.5	0.8	1.6	0.4	0.8	2.0	0.1	90	76	82	83	0.7	1.7	1.1	1.2	10	8	10	W 5	W 5	NW 3
12	91.8	88.9	83.5	88.1	-0.4	0.0	-0.7	-0.4	0.8	-1.2	76	78	98	84	1.4	1.3	0.1	0.9	10	10	10	W 5	WSW 7	W 5
13	81.7	82.6	85.7	83.3	-2.1	-1.0	-1.5	-1.5	0.0	-3.0	87	97	99	94	0.6	0.2	0.1	0.3	10	10 ✳	10 ✳	SSW 3	SW 4	SW 3
14	90.5	95.0	99.0	94.8	-2.2	-2.1	-5.8	-4.0	-1.2	-5.8	98	83	95	92	0.1	0.9	0.2	0.4	10 ✳	10	10	ENE 2	ENE 4	NE 7
15	98.9	98.1	98.7	98.6	-5.0	-5.4	-8.3	-6.8	-4.6	-8.4	95	87	89	90	0.2	0.5	0.3	0.3	10	10 ✳	10	NE 7	NE 8	NE 7
16	101.1	103.4	106.7	103.7	-9.2	-8.6	-10.8	-9.8	-7.9	-10.9	95	92	94	94	0.2	0.3	0.2	0.2	10	10	10	NNE 5	N 5	NNE 3
17	107.0	106.8	106.1	106.6	-13.8	-7.8	-6.6	-8.7	-6.3	-14.3	92	76	94	87	0.2	0.8	0.2	0.4	3	10	10	NW 3	W 3	NW 3
18	104.9	103.6	103.1	103.9	-5.2	-4.0	-5.8	-5.2	-3.0	-6.7	98	91	97	95	0.1	0.4	0.1	0.2	10	10	5	W 3	W 5	W 3
19	103.5	104.3	105.9	104.6	-5.0	-3.6	-3.2	-3.8	-2.9	-7.1	100	92	95	96	0.0	0.4	0.2	0.2	10	10	10	W 3	NW 4	W 4
20	106.4	105.4	103.3	105.0	-4.4	-3.5	-4.2	-4.1	-2.8	-4.5	96	90	91	92	0.2	0.5	0.4	0.4	10	10	10	W 5	SW 7	WSW 6
21	100.9	100.5	101.5	101.0	-8.8	-2.0	-6.6	-6.0	-0.8	-9.3	98	71	83	84	0.1	1.6	0.6	0.8	0	0 ⊙	0	SW 7	SW 5	SW 7
22	102.8	101.6	98.6	101.0	-9.4	-5.3	-8.2	-7.8	-2.3	-10.2	91	77	95	88	0.3	0.9	0.2	0.5	6	7	0	SW 5	SW 5	SW 3
23	97.8	97.6	95.9	97.1	-12.6	-4.6	-6.4	-7.5	-3.6	-13.1	96	76	78	83	0.1	1.0	0.8	0.6	0	0 ⊙	0	SW 4	WSW 2	WSW 1
24	91.0	88.4	86.8	88.7	-4.2	-1.2	-1.8	-2.2	-0.1	-7.5	70	66	88	75	1.3	1.9	0.7	1.3	9	10	0	E 3	ESE 4	ESE 3
25	86.5	87.1	89.8	87.8	-3.8	-0.2	-1.0	-1.5	1.0	-4.5	99	98	97	98	0.1	0.1	0.2	0.1	10	9	10	ESE 2	SW 3	SW 3
26	94.7	97.3	97.7	96.6	-1.3	1.6	-2.2	-1.0	2.5	-2.3	97	87	98	94	0.2	0.9	0.1	0.4	10	10	0	WSW 2	W 1	SW 1
27	93.8	93.3	96.1	94.4	-3.5	0.2	1.0	-0.3	2.2	-6.1	99	100	100	100	0.0	0.0	0.0	0.0	9	10	10	SW 1	SW 6	SW 4
28	96.6	97.5	103.4	99.2	-2.3	-1.0	0.7	-0.5	1.0	-3.3	100	97	98	98	0.0	0.2	0.1	0.1	10	10	10	WSW 3	SW 3	WSW 2
29	108.1	108.0	106.5	107.5	0.0	1.0	-1.4	-0.4	1.4	-1.4	92	75	96	88	0.5	1.7	0.2	0.8	10	9	10	NW 2	WSW 2	WSW 3
30	102.7	100.5	98.8	100.7	-3.6	1.4	0.0	-0.6	2.2	-4.1	100	78	88	89	0.0	1.6	0.7	0.8	5	1 ⊙	7	WSW 3	SW 4	SW 2
31	99.6	101.1	102.2	101.0	-0.8	0.0	0.2	-0.1	1.0	-1.5	95	100	98	98	0.3	0.0	0.1	0.1	10	10	10	SW 2	SW 2	SSW 2
M	97.2	97.2	97.5	97.3	-3.4	-1.0	-2.0	-2.1	0.0	-4.6	94	87	94	92	0.3	0.7	0.3	0.4	8.2	8.7	7.6	4.0	4.2	3.6

Luty – Février

1	99.8	99.3	99.5	99.5	-1.2	-0.2	-0.4	-0.6	0.7	-1.7	91	98	90	93	0.5	0.1	0.6	0.4	10	10 ✳	10	S 3	WSW 3	SSW 4
2	99.5	102.0	103.1	101.5	0.4	1.3	1.0	0.9	1.6	-0.7	98	100	100	99	0.1	0.0	0.0	0.0	10 ●	10 ● ≡	10	SW 6	SW 7	SW 7
3	102.6	99.9	103.2	101.9	1.2	2.6	0.8	1.4	3.8	0.7	100	98	100	99	0.0	0.2	0.0	0.1	10 ●	9	10	SW 2	S 2	NE 3
4	104.8	101.9	99.8	102.2	-0.2	1.4	1.3	1.0	2.7	-0.8	100	98	98	99	0.0	0.2	0.1	0.1	10 ≡	10	8	E 3	ESE 4	SE 2
5	100.1	100.0	98.8	99.6	-0.2	4.9	1.0	1.7	7.0	-0.5	98	87	96	94	0.1	1.1	0.3	0.5	10 ≡	2 ⊙	0	SW 3	WSW 6	SSW 5
6	96.3	94.1	92.1	94.2	0.5	8.4	2.5	3.5	9.5	-0.2	98	74	89	87	0.1	2.8	0.8	1.2	0	0 ⊙	0	SSW 1	SW 4	SW 7
7	92.1	92.7	94.6	93.1	1.1	3.2	1.6	1.9	4.9	1.0	98	100	98	99	0.1	0.0	0.2	0.1	10 ●	10 ●	1	SW 6	WSW 3	WSW 4
8	93.2	89.0	84.9	89.0	-0.4	4.1	2.6	2.2	5.2	-0.6	98	88	91	92	0.1	1.0	0.7	0.6	9	8	10	SW 3	SW 3	SW 3
9	80.0	79.7	80.4	80.0	3.4	5.9	5.3	5.0	8.2	2.6	98	98	95	97	0.1	0.2	0.4	0.2	10 ●	10	10 ●	SW 5	WSW 5	WSW 2
10	83.3	84.4	84.6	84.1	1.8	5.1	3.6	3.5	6.2	1.1	89	83	95	89	0.8	1.5	0.4	0.9	0	10	10	WSW 5	WSW 4	WSW 2
11	85.0	86.4	89.8	87.1	1.6	5.8	3.6	3.6	6.2	1.4	96	88	90	91	0.3	1.1	0.8	0.7	10	10	9	WSW 4	WSW 5	W 5
12	91.0	89.9	86.3	89.1	-0.6	5.9	1.8	2.2	7.5	-0.7	96	70	85	84	0.2	2.8	1.1	1.4	0	5 ⊙	10	W 4	SW 4	S 3
13	82.5	80.0	74.4	79.0	2.4	7.1	3.8	4.3	7.5	1.2	89	70	87	82	0.8	3.1	1.1	1.7	10	3 ⊙	5	S 5	SSW 5	SSW 6
14	69.1	69.3	68.4	68.9	4.7	7.1	3.8	4.8	8.0	3.8	89	77	98	88	0.9	2.3	0.1	1.1	10	10	10 ●	S 6	SSW 7	SSW 4
15	70.7	69.6	65.3	68.5	1.2	7.5	6.9	5.6	9.4	0.7	98	66	82	82	0.1	3.5	1.7	1.8	1	7 ⊙	10 ●	S 3	S 5	S 5
16	68.6	74.2	78.2	73.7	5.7	7.4	2.4	4.5	7.9	2.4	74	66	87	76	2.4	3.5	1.0	2.3	10	7 ⊙	2	SW 12	WSW 7	SW 3
17	82.6	85.0	85.4	84.3	-0.1	6.1	3.9	3.4	7.1	-0.5	96	61	77	78	0.3	3.6	1.9	1.9	1	2 ⊙	5	WSW 3	WSW 3	SE 3
18	87.0	84.1	76.9	82.7	0.8	7.5	8.2	6.2	9.0	-0.2	98	76	63	79	0.2	2.5	4.0	2.2	6	10	10	S 1	S 2	SE 3
19	72.2	80.1	88.7	80.3	6.1	3.9	1.4	3.2	8.6	1.1	86	87	87	87	1.3	1.1	0.9	1.1	10	10	4	SSW 5	WSW 9	NW 5
20	92.4	91.9	89.9	91.4	-0.8	7.1	3.0	3.1	8.4	-1.4	99	48	77	75	0.0	5.2	1.7	2.3	9	8	0	WSW 3	SW 7	S 3
21	86.9	86.1	86.9	86.6	3.5	7.5	5.1	5.3	9.2	1.3	71	63	84	73	2.2	3.9	1.4	2.5	10	7	0	SSW 2	SW 5	SSW 3
22	89.0	89.8	89.5	89.4	0.3	0.6	-1.0	-0.3	5.6	-1.0	100	100	94	98	0.0	0.0	0.4	0.1	10 ✳	10 ✳	0	NNW 3	NW 6	W 4
23	91.1	91.1	90.2	90.8	-3.0	1.0	-1.0	-1.0	2.6	-4.1	93	88	92	91	0.4	0.8	0.5	0.6	0	0 ⊙	6	NW 2	SW 4	W 2
24	86.5	81.7	78.7	82.3	-4.7	0.5	-0.4	-1.2	1.5	-5.2	98	94	100	97	0.1	0.3	0.0	0.1	0	10 ✳	10 ✳	S 1	SSE 3	SSE 3
25	80.9	82.9	82.2	82.0	-1.0	1.4	-0.7	-0.2	2.0	-1.1	99	91	98	96	0.1	0.7	0.1	0.3	10 ✳	10	0	SE 1	WNW 2	NNE 1
26	84.3	88.7	94.2	89.1	-0.3	1.0	-0.5	-0.1	1.8	-1.3	98	94	92	95	0.2	0.4	0.5	0.4	10 ✳	10	10	NNE 4	N 3	N 5
27	98.1	99.9	101.8	99.9	-2.8	-2.4	-4.0	-3.3	-0.2	-4.2	88	87	84	86	0.6	0.7	0.7	0.7	10	10	10	NNE 4	N 3	NE 2
28	103.7	105.1	105.7	104.8	-5.8	-3.6	-3.8	-4.2	-1.5	-6.2	89	74	78	80	0.4	1.3	1.0	0.9	10	10	0	NNE 4	NNW 3	NE 5
29																								
30																								
31																								
M	88.3	88.5	88.3	88.4	0.5	3.9	1.8	2.0	5.4	-0.5	94	83	90	89	0.4	1.6	0.8	0.9	7.4	7.8	6.1	3.8	4.5	3.8

Sandomierz $H_s = 202\ m$ $H_b = 200{,}3\ m$ $h_w = 21$ **Styczeń – Janvier 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	6	1.4	4	-	△°6⁴⁰–7⁰³ ✶°–7¹⁴ △°8³⁵–9³⁰ ✶°–9⁴⁵ ✶¹–10²⁵ ✶°–10⁴⁵ = 0⁰⁰–3⁰ 7⁴⁰–14³⁰ 23³⁰–24
2	7	.	6	-	= 0⁰⁰–8³⁰ 18¹⁵–24
3	6	.	5	-	= 0⁰⁰–24
4	6	0.0	3	-	✶°10⁴⁰ 11⁴⁵ = 0⁰⁰–24
5	6	7.8	3	-	•°17³⁵–24 = 0⁰⁰–6⁴⁵ ≡¹–8¹⁵ ≡°–8⁴⁰ =–24
6	5	3.0	2	-	•°0⁰⁰–3³⁵ 8³⁰–9⁵⁵ •°12¹⁵–13¹⁰ •°–20²⁰ = 0⁰⁰–7⁴⁵ ≡¹–9³⁵ ≡°–10⁵⁰ =–12⁴⁷ ≡°–13⁴⁰ =–24
7	7	.	pł.	-	= 0⁰⁰–3³⁰
8	6	0.3	pł.	-	= 7³⁰–24
9	6	0.0	.	-	•°0⁰⁰–6⁴⁰ 7¹⁵ 8⁴³ •°12²⁵ 45 = 0⁰⁰–24
10	7	1.6	.	-	•°13⁴⁰–18³⁰ ✶°–19¹⁰ = 0⁰⁰–12¹⁵ 13⁴⁰–24
11	7	0.4	.	-	✶°9⁰⁵ 11¹² ✶ 14⁰⁵–45 15¹⁰–50 = 0⁰⁰–7³⁰
12	7	0.5	.	-	✶°14⁴⁰–15²⁵ 17⁴⁵–20²⁰ 22³⁵–24 = 14²⁰–24
13	5	5.3	2	-	✶°0⁰⁰–5³⁵ 11³⁰ 13¹⁰ 13⁴⁰–24 = 0⁰⁰–24
14	6	0.0	8	-	✶°0⁰⁰–7⁴⁵ = 0⁰⁰–24
15	6	0.2	6	-	✶°8⁴⁰–12³⁰ 13¹⁸ = 0⁰⁰–24
16	6	0.0	6	-	✶°9⁴⁰ 11²⁰ 12¹⁰–48 13⁴⁵ 16⁵⁰ = 0⁰⁰–24
17	7	.	5	-	= 0⁰⁰–12¹⁵
18	6	.	4	-	= 6¹⁵–24
19	6	.	4	-	= 0⁰⁰–24
20	6	.	4	-	= 0⁰⁰–24
21	6	.	3	-	= 0⁰⁰–24 ⌓ 21²⁵–24
22	7	.	3	-	= 0⁰⁰–11³⁰ 20³⁰–24 ⌓ 0⁰⁰–12
23	6	.	3	-	= 0⁰⁰–24
24	6	0.0	3	-	✶°17⁴⁰ 18¹⁵ = 0⁰⁰–24
25	6	0.0	2	-	= 0⁰⁰–24
26	6	.	2	-	✶°5²²…³⁵ = 0⁰⁰–23⁵⁰ ≡°–24
27	5	1.4	2	-	✶°8⁴⁰–12¹⁰ △–12¹⁵ ✶°–12²⁵ ≡°0⁰⁰–3⁴⁰ = –24
28	5	.	5	-	= 0⁰⁰–6⁴⁰ ≡²–9³⁰ ≡¹–9⁴⁵ ≡°–9⁵⁰ =–24
29	7	.	4	-	= 0⁰⁰–6¹⁵
30	6	.	3	-	= 7³⁰–24
31	6	0.0	3	-	= 0⁰⁰–24
Σ	–	21.9	–	-	UWAGI

Luty – Février

1	5	3.5	2	-	✶°6⁴⁵–7³⁰ ✶¹–12⁴⁰ = 0⁰⁰–24
2	3	6.7	3	-	•°2⁴⁰–7³⁵ •–9³⁰ •°11³⁷ 12²⁰ 14³⁵ •°–20⁰⁷ = 0⁰⁰–11⁴⁰ ≡°–15³⁵ =–24
3	5	0.5	.	-	•°0¹⁰–5²⁵ 6¹⁰–7³⁵ •°18³⁵–19²⁵ = 0⁰⁰–6⁴⁵ ≡¹–9⁴⁰ ≡°–10³⁵ =–24
4	6	.	.	-	= 0⁰⁰–1⁴⁵ ≡²–9¹⁵ ≡¹–9²⁵ ≡°–9³⁰ =–24
5	6	.	.	-	= 0⁰⁰–3⁴⁵ ≡°–8³⁰ =–24
6	6	0.3	.	-	= 0⁰⁰–12⁴⁵
7	5	7.3	.	-	•°5³⁵–6⁴⁰ 8¹⁰–14⁰⁵ = 5²⁰–9⁵⁰ ≡°–12²⁰ =–24
8	6	0.2	.	-	•°22⁴⁰–23⁰⁸ = 0⁰⁰–13²⁵ 20²⁰–24 ⌴ rp.–9³⁰ ⊕ 7³⁰–10¹⁵
9	6	2.0	.	-	•°4⁴⁰ 5¹⁵–³⁵ 5⁴⁵ 7³⁸–10⁴⁰ 19⁴⁰–22²⁵ = 0⁰⁰–24
10	6	.	.	-	= 0⁰⁰–24
11	6	.	.	-	= 0⁰⁰–13³⁰ 21³⁰–24
12	7	.	.	-	= 0⁰⁰–12¹⁵ ⊕ 19³⁰–23¹⁹
13	7	0.1	.	-	
14	7	4.3	.	-	•°3⁴⁵–4⁵⁰ 5³⁸ 14³⁰–15¹² 16⁴⁰–19²⁵ = 3⁴⁵–6¹⁵
15	7	1.3	.	-	•°16⁴⁰–18³⁵ 19³³–20²⁰ 24 = 0⁰⁰–9³⁰ ⊕ 10³⁵–12¹⁵
16	7	0.0	.	-	•°0⁰⁰ 1⁴⁰ • 13²⁵–⁴⁰ ⊕ 23⁴⁵–24
17	6	.	.	-	= 6¹⁵–13³⁰ ⊕ 0⁰⁰–4³⁰
18	7	0.2	.	-	•°13⁵⁰–14¹⁰ 15¹⁵ = 0⁰⁰–12¹⁵
19	7	.	.	-	•°4³⁵–5²⁵
20	7	.	.	-	= 5³⁵–11²⁵ ⌴° na–10³⁰ ⊕ 11⁴⁰–14¹⁵
21	7	5.1	.	-	
22	5	5.0	2	-	•°12⁵–3⁴⁰ •°–4¹⁵ ✶°–16¹⁰ = 0⁴⁰–16³⁰
23	6	.	4	-	= 6¹⁵–24
24	6	1.5	3	-	✶°11³⁵–19²⁰ 22⁴⁰ = 0⁰⁰–24 ⊕ 8²⁵–9¹⁵
25	6	2.1	7	-	✶°0²⁰ 2¹⁵–8²⁵ = 0⁰⁰–24
26	7	0.4	6	-	✶°2⁵⁰–8³⁰ 9¹⁰…³⁵ 10³⁰ 11²⁵ 14⁰⁵ 16²⁵ = 0⁰⁰–12¹⁵
27	6	.	4	-	= 7²⁰–24
28	7	.	4	-	= 0⁰⁰–12³⁰
29					
30					
31					
Σ	–	40.5	–	-	UWAGI.

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — Marzec – Mars 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	107.0	107.3	106.9	107.1	-6.2	-2.7	-2.8	-3.6	-2.0	-6.2	97	75	77	83	0.1	1.2	1.1	0.8	0	10 ✳	10	NNW 4	NNE 5	N 6
2	105.1	103.6	101.2	103.3	-3.7	-2.0	-3.0	-2.9	-0.8	-3.8	71	64	84	73	1.3	1.9	0.8	1.3	10	8	0	N 5	N 6	NNW 2
3	99.1	98.6	97.4	98.4	-7.1	-6.1	-8.0	-7.3	-2.5	-8.7	91	71	87	83	0.3	1.1	0.4	0.6	10 ✳	8	0	NE 5	NE 5	NNE 3
4	94.7	92.0	88.1	91.6	-7.4	-2.9	-2.9	-4.0	-1.0	-8.4	82	62	82	75	0.6	1.8	0.9	1.1	9	0 ⊙	7	SW 2	SSW 4	SSW 3
5	87.5	89.2	90.7	89.1	0.3	2.8	-0.2	0.7	4.2	-3.7	94	67	88	83	0.3	2.5	0.7	1.2	10	6 ⊙	0	WSW 5	WSW 2	WNW 3
6	90.6	90.1	88.9	89.9	-5.0	4.0	-0.3	-0.4	5.2	-5.2	98	52	74	75	0.1	3.9	1.6	1.9	1	1 ⊙	0	WSW 2	W 3	W 1
7	88.6	90.7	92.2	90.5	-2.8	-1.6	-3.0	-2.6	0.4	-3.4	97	73	73	81	0.1	1.4	1.3	0.9	5	10	9	N 3	NE 5	ENE 3
8	93.6	94.4	97.3	95.1	-4.7	0.3	-3.3	-2.8	1.6	-4.7	83	55	70	69	0.7	2.8	1.5	1.7	0 ○	3	0	ENE 3	SE 4	E 3
9	100.3	101.5	103.6	101.8	-6.2	0.9	-2.0	-2.3	2.3	-6.4	97	67	83	82	0.1	2.1	0.9	1.0	0 ○	1 ⊙	0	NE 4	NE 3	NE 3
10	106.9	108.8	109.4	108.4	-5.7	1.3	-1.4	-1.8	3.0	-5.7	97	67	83	82	0.1	2.2	0.9	1.1	0 ○	0 ⊙	0	NNE 3	NE 4	NE 3
11	109.9	109.5	107.2	108.9	-4.4	4.5	1.6	0.8	6.9	-5.3	98	54	62	71	0.1	3.9	2.7	2.2	1 ⊙	0 ⊙	0	NE 2	NE 2	WNW 2
12	103.9	100.6	95.5	100.0	-3.8	7.7	4.1	3.0	9.7	-4.2	99	51	75	75	0.1	5.2	2.0	2.4	10 ⊙	6 ⊙	6	WNW 3	SW 2	WSW 3
13	93.6	94.4	93.5	93.8	4.2	11.3	9.7	8.7	12.9	1.4	64	53	47	55	2.9	6.4	6.3	5.2	9	8 ○	3	W 3	WSW 3	W 3
14	89.9	86.8	85.5	87.4	0.8	15.2	9.5	8.8	15.5	0.1	92	49	76	72	0.5	8.8	2.8	4.0	2 ○	0 ⊙	10	WSW 5	WSW 7	WSW 5
15	86.0	86.8	80.7	84.5	7.1	8.6	7.9	7.9	9.7	6.5	73	74	78	75	2.8	2.9	2.3	2.7	10	10	10	W 9	WSW 9	WSW 12
16	78.1	80.5	89.8	82.8	1.9	3.7	-4.1	-0.6	9.0	-4.8	98	65	63	75	0.1	2.8	1.6	1.5	10	10	10	NW 4	NW 7	NNW 8
17	92.9	91.7	84.4	89.7	-4.6	-1.0	-0.6	-1.7	1.2	-5.1	74	63	95	77	1.1	2.1	0.3	1.2	10	9	10	NNE 3	S 3	SE 3
18	74.5	73.2	76.3	74.7	3.9	11.1	7.8	7.6	11.7	-0.6	98	88	78	88	0.2	1.6	2.4	1.4	10	10	9	WSW 5	WSW 7	W 9
19	82.8	85.4	85.9	84.7	4.7	8.9	5.7	6.2	9.4	4.1	84	68	92	81	1.3	3.6	0.8	1.9	9	8	10 ●	W 7	WSW 7	SW 3
20	87.6	88.6	85.2	87.1	5.2	8.0	7.1	6.8	10.4	4.8	100	92	99	97	0.0	0.9	0.2	0.4	10 ≡	10	10	SW 1	WSW 1	SE 2
21	84.2	88.4	89.5	87.4	6.5	13.8	7.3	8.7	14.6	5.8	100	56	73	76	0.0	7.0	2.7	3.2	3 ⊙	7 ⊙	0	WSW 4	WNW 3	C 0
22	90.6	91.9	94.7	92.4	6.7	12.4	5.7	7.6	13.4	4.2	72	38	80	63	2.7	9.0	1.9	4.5	9 ⊙	4	0	WNW 3	NW 5	WNW 3
23	96.3	95.6	95.8	95.9	2.8	10.5	5.3	6.0	11.9	-0.1	91	50	77	73	0.7	6.3	2.1	3.0	0 ⊙	3 ⊙	0	WSW 1	NE 1	NE 4
24	101.4	104.8	105.3	103.8	1.0	1.1	0.8	0.9	5.6	0.0	90	77	73	80	0.7	1.5	1.8	1.3	10	9 ○	9	ENE 7	E 9	E 7
25	104.5	104.8	104.5	104.6	-0.7	1.5	2.0	1.2	2.2	-1.1	79	72	54	68	1.2	1.9	3.3	2.1	10	10 ●	6	ESE 9	SE 7	SE 5
26	103.6	103.0	102.3	103.0	-0.1	8.3	3.2	3.6	9.9	-0.2	66	43	63	57	2.1	6.3	2.9	3.8	4 ⊙	0 ⊙	0	SE 3	SE 5	SE 5
27	103.3	102.8	102.0	102.7	-0.7	12.8	6.0	6.0	15.0	-1.9	83	40	71	65	1.0	9.0	2.7	4.2	0 ⊙	0 ⊙	0	SE 2	S 4	SE 3
28	99.9	97.4	95.0	97.4	0.4	14.0	6.8	7.0	15.7	-2.1	80	30	56	55	1.3	11.2	4.4	5.6	0 ⊙	2 ○	0	SE 2	SSW 5	S 3
29	92.7	92.0	92.4	92.4	4.1	11.2	7.3	7.5	13.0	3.6	69	56	74	66	2.6	5.9	2.6	3.7	10	8	0	S 3	SW 5	ESE 1
30	92.5	92.9	94.2	93.2	4.7	16.3	9.5	10.0	17.2	1.9	76	30	59	55	2.0	13.0	4.9	6.6	9 ⊙	9 ⊙	0	E 1	E 3	NE 3
31	97.7	98.6	98.5	98.3	3.2	15.2	8.9	9.0	17.1	2.0	79	40	58	59	1.6	10.4	4.8	5.6	1 ⊙	1 ⊙	0	E 3	ESE 1	ENE 3
M	94.8	95.0	94.5	94.8	-0.2	6.1	2.7	2.8	7.8	-1.5	86	59	74	73	0.9	4.5	2.1	2.5	5.9	5.5	3.8	3.7	4.4	3.8

Kwiecień – Avril

1	99.1	98.5	97.9	98.5	5.3	16.7	9.7	10.4	17.7	3.6	60	26	52	46	3.6	14.1	5.7	7.8	0 ⊙	0 ⊙	0	ENE 3	ESE 4	ESE 1
2	97.5	96.9	97.6	97.3	3.9	19.0	11.3	11.4	20.5	3.0	78	29	55	54	1.8	15.7	6.1	7.9	0 ⊙	0 ⊙	0	ESE 2	SE 2	E 2
3	99.8	101.3	102.4	101.2	6.6	18.3	11.3	11.9	19.6	5.2	68	29	55	51	3.1	15.0	6.1	8.1	9 ○	6 ⊙	0	E 1	ESE 3	E 2
4	104.6	104.8	104.7	104.5	6.2	17.5	10.9	11.4	18.5	4.8	73	35	60	56	2.6	13.0	5.2	6.9	0 ○	0 ⊙	0	E 2	N 3	NE 3
5	104.0	102.5	97.8	101.4	6.3	15.7	11.1	11.0	18.2	3.7	81	39	53	58	1.8	10.9	6.2	6.3	0 ⊙	0 ⊙	0	NE 3	NE 3	NE 2
6	93.1	89.3	84.9	89.1	5.0	18.8	14.0	13.0	20.5	3.7	70	31	46	49	2.6	14.9	8.6	8.7	0 ⊙	0 ⊙	0	E 1	SW 5	SW 2
7	82.4	84.3	86.8	84.5	7.4	10.4	5.0	7.0	14.1	5.0	73	76	97	82	2.8	3.0	0.3	2.0	1 ⊙	5 ○	10 ●	WSW 3	NNW 6	N 7
8	91.2	91.6	90.8	91.2	3.2	5.3	1.6	2.9	6.1	1.6	90	68	85	81	0.8	2.9	1.1	1.6	10	10 ○	1	N 5	N 5	NW 3
9	88.9	87.4	87.5	87.9	1.3	6.6	2.0	3.0	7.0	-0.4	83	68	93	81	1.1	3.1	0.6	1.6	10 ○	10	10	NW 5	NW 3	NNW 3
10	86.8	83.4	77.1	82.4	0.5	9.8	6.5	5.8	12.5	-2.0	79	52	82	71	1.3	5.6	1.7	2.9	2 ⊙	1 ○	0	NW 2	SW 5	S 3
11	70.9	69.8	75.7	72.1	5.8	8.5	4.8	6.0	8.7	4.7	97	97	89	94	0.3	0.3	1.0	0.5	10 ●	10 ●	10 ●	S 1	SSW 1	NNW 3
12	83.0	85.6	87.6	85.4	0.6	4.5	2.4	2.5	5.9	0.6	79	65	82	75	1.4	2.9	1.3	1.9	10 ○	9	10	N 4	NNW 3	NE 2
13	89.1	90.1	91.6	90.3	0.7	6.2	2.4	2.9	7.8	-0.6	90	49	82	74	0.6	4.9	1.3	2.3	3 ○	6 ⊙	6	NNE 1	WNW 2	SW 2
14	94.3	94.4	94.0	94.2	-0.2	4.8	1.4	1.8	5.4	-1.5	100	55	76	77	0.0	3.9	1.7	1.9	2	9	2	W 2	NNE 3	NNE 3
15	94.4	94.8	97.4	95.5	-0.9	6.7	1.7	2.3	7.7	-2.1	89	39	80	69	0.6	6.0	1.4	2.7	5 ⊙	6 ⊙	1	N 4	NNE 5	N 3
16	99.7	98.7	97.9	98.8	0.3	7.5	7.2	5.6	9.8	-2.7	82	57	62	67	1.1	4.4	3.9	3.1	0 ○	4 ○	4	NNW 2	NNW 3	NE 2
17	95.2	94.4	94.0	94.5	4.2	6.9	5.7	5.6	8.2	3.9	93	99	98	97	0.5	0.1	0.2	0.3	10	10 ●	7	S 2	S 1	N 3
18	92.3	91.7	91.1	91.7	2.0	4.1	3.0	3.0	6.0	1.8	98	85	93	92	0.2	1.2	0.6	0.7	10 ●	10	10	NE 3	NNE 3	NW 3
19	91.1	91.3	91.7	91.4	1.6	5.8	5.2	4.4	8.6	1.3	100	79	90	90	0.0	2.0	0.8	0.9	10 ●	10	8	NW 2	SW 3	S 2
20	94.2	96.8	100.0	97.0	4.3	8.7	6.4	6.4	9.7	2.5	92	94	97	94	0.7	0.6	0.3	0.5	10	10	10	S 2	WSW 3	NNW 3
21	101.9	103.1	103.6	102.9	3.7	10.8	7.5	7.4	11.4	2.1	100	57	83	80	0.0	5.6	1.8	2.5	6 ○	5 ○	3	NW 1	N 3	N 2
22	104.3	103.7	103.9	104.0	6.4	15.6	10.6	10.8	16.6	4.0	91	47	73	70	0.9	9.4	3.5	4.6	0 ○	7 ○	7	N 1	SE 3	E 2
23	103.6	102.5	102.3	102.8	7.2	13.9	11.5	11.0	14.6	5.0	90	66	96	84	1.1	5.4	0.5	2.3	5	10	10	N 4	NE 3	N 4
24	100.7	98.9	97.3	99.0	9.3	18.2	14.2	14.0	19.5	8.5	96	39	65	67	0.5	12.7	5.6	6.3	10	1 ○	0	N 4	NE 4	NE 1
25	96.4	96.2	95.4	96.0	9.2	18.0	14.7	14.2	18.7	7.2	91	61	78	77	1.1	8.0	3.6	4.2	7 ○	9 ○	8	NNW 2	SW 2	NW 4
26	95.0	94.7	93.8	94.5	12.3	21.4	16.6	16.7	22.5	10.5	82	47	67	65	2.5	13.5	6.3	7.4	8	3 ○	6	NW 3	NNE 3	NNW 3
27	93.3	92.5	92.1	92.6	13.0	22.8	15.7	16.8	23.9	10.2	84	34	65	61	2.5	18.2	6.2	9.0	0 ○	1 ○	3	NNW 1	S 3	WSW 2
28	90.7	89.1	88.2	89.3	12.2	23.8	17.4	17.7	24.2	11.0	76	38	55	56	3.4	18.3	9.0	10.2	2 ○	5 ○	1	E 2	SSW 4	SSE 3
29	89.7	89.3	89.9	89.6	13.7	24.4	15.6	17.3	25.1	10.3	80	33	78	64	3.2	20.4	3.9	9.2	0 ○	3 ○	1	SW 2	SW 4	SW 2
30	89.6	87.0	83.7	86.8	13.1	26.0	14.7	17.1	26.5	9.9	74	29	86	63	4.0	24.0	2.4	10.1	0 ○	2 ⊙	3	S 1	S 3	SE 2
31																								
M	93.9	93.5	93.3	93.6	5.5	13.2	8.7	9.0	14.5	3.8	85	54	76	72	1.5	8.7	3.2	4.5	4.7	5.4	4.4	2.4	3.3	2.6

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w = 21\,m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	3	-	$*^{0}\ 11^{40}\ 14^{37}$, $15^{25}\ 20^{05}$: $= 6^{15}-9^{25}$
2	8	0.0	3	-	
3	7	0.0	3	-	$*^{0}\ 1^{20}-9^{20}$: $= 7^{27}-9^{15}$
4	7	.	3	-	$= 19^{30}-21^{10}$
5	7	.	3	-	$= 5^{30}-7^{15}$
6	7	.	pż.	-	
7	7	.	pż.	-	
8	7	.	pż.	-	
9	7	.	pż.	-	
10	7	.	pż.	-	
11	7	.	.	-	$= 6^{15}-10^{30}$
12	7	.	.	-	$= 5^{10}-11^{30}$ ⌴ $^{0}\ 3^{30}-5^{20}$ ⌴ $^{1}-8^{15}$ ⊕ $6^{15}-11^{15}$ ⊖ $18^{30}-22^{30}$
13	6	.	.	-	$= 8^{30}-16^{30}$
14	7	.	.	-	$= 5^{15}-10^{20}$
15	7	7.2	.	-	$\gg 20^{25}-22^{45}$ $\ll -24$
16	7	.	.	-	$\bullet^{0}\ 1^{50}\ 2^{45}-6^{25}$: $= 2^{30}-8^{30}$ $\ll\ 0^{00}-30$ $\gg -3^{15}$
17	8	2.8	.	-	$*^{0}\ 17^{40}-50$ △ $18^{30}-19^{25}$ $\bullet^{0}\ 23^{45}-24$: $= 23^{45}-24$
18	7	1.3	.	-	$\bullet^{0}\ 0^{00}-3^{40}\ 8^{20}-9^{30}\ 11^{37}$: $= 0^{00}-5^{15}\ 8^{10}-11^{35}$
19	8	0.4	.	-	$\bullet^{0}\ 0^{45}-1^{00}$ ▽ $-7^{15}\ 2^{50}-3^{10}$ $\bullet^{0}\ 20^{15}-24$: $= 20^{10}-24$
20	5	.	.	-	$\bullet^{0}\ 0^{00}-20$: $= 0^{00}-5^{40}$ $\equiv^{1}-6^{37}$ $\equiv^{0}-7^{12}$ $\equiv^{2}-9^{10}$ $\equiv^{1}-9^{40}$ $\equiv^{0}-9^{50}$ $= -24$
21	7	.	.	-	$= 0^{00}-9^{25}$
22	8	.	.	-	
23	7	.	.	-	$= 6^{15}-11^{30}$
24	7	.	.	-	
25	7	1.0	.	-	$\bullet^{0}\ 11^{45}-12^{30}\ 13^{10}$, $13^{15}-17^{45}$: $= 11^{45}-18^{05}$
26	7	.	.	-	
27	8	.	.	-	
28	7	.	.	-	⌴ $^{1}\ 3^{30}-7^{25}$
29	7	0.0	.	-	$\bullet^{0}\ 7^{10}-8^{15}$
30	7	.	.	-	
31	7	.	.	-	
Σ	–	12.7	–	-	UWAGI.

Kwiecień – Avril

1	8	.	.	-	
2	8	.	.	-	$= 5^{30}-9^{40}$
3	7	.	.	-	
4	7	.	.	-	
5	7	.	.	-	
6	7	.	.	-	$= 4^{30}-8^{30}$
7	7	14.5	.	-	$\bullet^{0}\ 17^{10}-18^{43}$ $\bullet^{1}-19^{15}$ $\bullet^{0}-24$: $= 18^{30}-24$
8	8	.	.	-	$\bullet^{0}\ 0^{00}-1^{25}$: $= 0^{00}-2^{30}$ ⊕ $7^{37}-9^{30}$
9	8	.	.	-	⌴ ^{0} na $-\ 7^{30}$: ⊕ $5^{35}-7^{15}$
10	8	1.2	.	-	⌴ ^{0} na $-$ a
11	6	9.4	.	-	$\bullet^{0}\ 4^{10}\ 5^{26}-10^{30}\ 13^{15}-21^{35}$: $= 6^{20}-24$
12	8	.	.	-	$= 0^{00}-5^{30}$: ⊕ $6^{20}-7^{15}$
13	7	0.7	.	-	$*^{0}\ 22^{35}-23^{20}$
14	7	.	.	-	$= 1^{30}-12^{15}$: ⊕ $12^{50}-13^{12}$
15	8	.	.	-	
16	7	.	.	-	$= 5^{15}-8^{30}$
17	5	10.1	.	-	$\bullet^{0}\ 7^{20}-8^{50}$ $\bullet^{1}-10^{10}$ $\bullet^{0}-11^{40}\ 12^{30}$, $^{0}-13^{48}$ $\bullet^{0}-14^{30}\ 17^{45}$: $= 6^{15}-24$
18	8	3.5	.	-	$\bullet^{0}\ 4^{40}-6^{45}\ 11^{15}$: $= 0^{00}-10^{30}$
19	7	0.2	.	-	$\bullet^{0}\ 0^{30}-6^{40}\ 8^{35}$: $= 0^{30}-8^{15}$
20	6	2.2	.	-	$\bullet^{0}\ 7^{17}\ 8^{15}-10^{32}$, $^{0}\ 11^{47}\ 12^{20}$: $= 0^{30}-24$
21	7	.	.	-	$= 0^{00}-8^{30}$
22	7	.	.	-	
23	7	.	.	-	
24	7	.	.	-	$= 3^{20}-12^{20}$: $15^{30}-24$
25	6	.	.	-	$= 0^{00}-24$
26	7	.	.	-	$= 0^{00}-10^{30}$
27	7	.	.	-	(↖) $^{0}\ 15^{45}-17^{40}$ WSW : $= 3^{30}-9^{30}$
28	7	.	.	-	↘ $20^{17}-22^{10}$ SW
29	7	0.0	.	-	▽ $14^{10}-23$: (↖) $^{0}\ 13^{58}-14^{10}$ SE ↖ $^{0}\ 14^{10}-20-40$ SE – E – N
30	7	4.4	.	-	▽ $17^{20}-18^{30}$, $22^{35}-23^{05}$: (↖) $^{1}\ 16^{27}-17^{30}$ WSW ↖ $^{1}\ 17^{30}-35-40$ (↖) $^{1}-17^{50}$ ENE ≤ $19^{30}-20^{15}$ SE. **30.IV:** $21^{50}-22^{10}$ N
31					
Σ	–	46.2	–	-	UWAGI.

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — Maj – Mai 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI A				ZACHMURZENIE: POGODA Nw			KIERUNEK I PRĘDKOŚĆ WIATRU Dv		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	92.4	93.3	93.0	92.9	6.6	10.7	8.9	8.8	15.7	6.4	72	53	62	62	2.7	6.1	4.4	4.4	9	9	9	NW 3	NNE 4	NNE 4
2	92.7	97.6	90.1	91.5	5.6	7.1	5.5	5.9	9.1	4.9	78	83	91	84	2.0	1.8	0.8	1.5	10	10 ●	10	NE 4	NE 5	NE 5
3	87.9	88.0	86.9	87.6	3.8	5.6	6.3	5.5	6.7	3.8	98	97	97	97	0.1	0.3	0.2	0.3	10 ●	10 ●	10	NE 5	NNE 3	NW 1
4	84.6	85.2	88.6	86.2	5.7	11.8	5.4	7.1	14.2	3.5	98	65	69	77	0.2	4.9	2.8	2.6	6 ⊙	10	0	WSW 3	WNW 5	NW 3
5	90.2	89.3	88.2	89.2	4.8	8.9	5.6	6.2	9.9	0.8	76	41	66	61	2.0	6.8	3.1	4.0	0 ○	10 ⊙	10	W 5	W 6	NW 3
6	85.6	84.0	85.6	85.1	3.0	6.2	3.8	4.2	8.1	2.8	98	86	87	90	0.2	1.3	1.1	0.9	10 ●	10 ●	10	NE 5	SSE 3	WNW 3
7	84.5	83.9	81.9	83.4	2.1	3.4	2.5	2.6	4.1	1.3	100	93	100	98	0.0	0.5	0.0	0.2	10	10 ●	10	WSW 2	W 3	W 3
8	79.8	80.5	83.7	81.3	3.5	4.3	3.8	3.8	5.0	2.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10	10 ●	NNW 5	NW 7	NW 4
9	84.9	84.2	83.8	84.3	3.8	4.9	5.3	4.8	5.7	3.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10 ●	10	NNW 4	NW 5	NW 4
10	82.2	83.6	87.4	84.4	5.3	7.0	6.2	6.2	7.6	5.1	100	98	100	99	0.0	0.1	0.0	0.0	10 ●	10	10 ●	NW 3	WNW 3	SW 3
11	91.7	93.4	93.7	92.9	6.2	12.0	10.6	9.8	13.6	5.6	100	69	88	86	0.0	4.3	1.5	1.9	10	9	4	SW 3	SW 4	S 2
12	94.3	94.8	94.9	94.7	8.3	19.0	14.2	13.9	20.6	7.2	96	49	69	71	0.5	11.2	5.0	5.6	8	2 ○	0	S 2	S 2	SW 1
13	95.2	94.5	93.4	94.4	11.6	20.0	15.7	15.8	22.0	8.3	84	47	70	67	2.1	12.4	5.3	6.6	0 ○	3 ○	0	SW 2	NE 4	ENE 1
14	93.5	94.0	96.1	94.5	14.4	18.5	15.5	16.0	22.3	10.4	83	52	80	72	2.7	10.2	3.5	5.5	0 ○	7	8	NW 1	NW 5	NW 3
15	98.3	98.5	97.5	98.1	13.7	19.8	14.2	15.5	20.9	11.1	78	57	68	68	3.5	9.9	5.1	6.2	0 ○	5 ○	0	NW 3	NNW 2	NNE 1
16	97.3	95.0	93.0	95.1	14.0	21.1	15.1	16.3	22.3	9.3	66	39	64	56	5.4	15.2	6.2	8.9	0 ○	1 ○	2	NE 2	SSE 3	E 2
17	91.8	91.6	92.4	91.9	15.3	21.2	15.1	16.7	21.7	11.7	65	41	70	59	6.2	14.8	5.1	8.7	1 ○	5 ○	1	E 3	ENE 3	NE 1
18	92.9	91.9	89.3	91.4	15.4	21.7	18.2	18.4	23.5	10.9	75	51	73	66	4.4	12.8	5.6	7.6	6 ○	5 ○	5	NW 2	NE 4	NE 4
19	86.7	85.9	85.0	85.9	17.3	22.4	15.3	17.6	22.6	13.2	70	50	81	67	5.8	13.6	3.4	7.6	0 ○	4 ○	0	ENE 3	E 6	SE 3
20	84.8	85.6	87.8	86.1	15.3	22.2	15.6	17.2	23.1	11.0	85	52	82	73	2.6	13.0	3.2	6.3	0 ○	7 ○	10	SE 3	ESE 3	SW 3
21	89.9	91.8	91.8	91.2	14.1	11.5	11.1	12.0	15.7	11.0	90	90	86	89	1.6	1.4	1.8	1.6	10	10	10	NW 5	NW 5	NW 5
22	89.9	89.9	89.7	89.8	9.4	15.8	13.5	13.0	16.9	8.8	85	63	80	76	1.7	6.6	3.2	3.8	10	7	10	N 6	NNE 5	N 4
23	88.2	87.4	86.7	87.4	14.7	21.4	16.6	17.3	23.2	11.0	80	57	79	72	3.3	11.0	4.1	6.1	5 ⊙	6 ⊙	0	N 4	NE 2	NNE 3
24	87.4	89.5	93.0	90.0	14.5	16.9	10.9	13.3	18.0	10.4	91	74	87	84	1.5	5.0	1.6	2.7	9	10	10	NNW 4	N 4	NNE 7
25	96.1	97.5	99.1	97.6	9.1	13.3	9.0	10.1	13.8	7.0	61	40	56	52	4.6	9.2	5.1	6.3	0 ⊙	6 ⊙	10	NE 7	NE 7	NNE 3
26	99.8	100.3	100.8	100.3	6.4	10.5	7.1	7.8	11.0	5.3	76	50	64	63	2.3	6.3	3.6	4.1	9	9	10	NNE 6	NE 6	NE 5
27	99.2	99.4	98.8	99.1	5.0	9.5	6.6	6.9	10.1	1.7	81	47	76	68	1.6	6.3	2.3	3.4	10	10	10	NE 5	NE 7	E 3
28	96.5	95.9	95.2	95.9	6.7	8.7	7.1	7.4	8.9	5.1	79	86	84	83	2.0	1.5	1.6	1.7	10	10	10	NNE 4	NE 5	NNE 4
29	94.6	95.7	97.1	95.8	4.8	13.2	10.0	9.5	15.0	2.1	87	40	66	64	1.1	9.1	4.2	4.8	7 ○	7 ○	8	N 5	N 5	N 3
30	98.4	98.6	97.7	98.2	11.6	15.9	12.5	13.1	18.1	6.3	66	45	65	55	5.9	10.0	5.0	7.0	1 ○	10	8	WNW 3	W 3	NE 2
31	97.7	96.6	93.8	96.0	9.0	18.1	16.1	14.8	20.0	8.1	81	40	47	56	2.2	12.5	9.7	8.1	10	8	6	NE 3	SW 3	SSW 2
M	91.3	91.3	91.5	91.4	9.1	13.6	10.4	10.9	15.1	6.8	84	63	78	75	2.2	7.0	3.2	4.1	6.2	7.7	6.8	3.7	4.3	3.1

Czerwiec – Juin

1	92.5	92.3	91.8	92.2	13.3	19.4	15.5	15.9	22.2	11.0	71	43	60	58	4.5	12.8	7.0	8.1	9	6	2	SSW 1	W 3	W 3
2	94.0	94.8	95.4	94.7	15.0	21.2	17.7	17.9	23.2	11.3	69	46	63	59	5.2	13.6	7.4	8.7	3 ⊙	3 ⊙	4	WNW 3	WNW 5	W 2
3	97.9	96.8	93.8	96.2	17.5	24.3	19.8	20.4	25.6	10.4	71	45	64	60	5.9	16.8	8.3	10.3	0 ○	1 ○	2	WSW 2	SW 4	SW 2
4	91.7	89.6	87.7	89.7	16.5	22.6	18.0	18.8	24.1	13.5	80	67	89	79	3.9	9.2	2.2	5.1	10	10 ●	10	SW 2	SW 5	SSW 1
5	82.8	83.8	84.1	83.6	15.9	16.0	12.2	14.7	18.4	12.1	99	80	88	89	0.2	3.6	1.7	1.8	10	10	2	SW 5	W 8	WSW 3
6	84.6	87.0	90.2	87.3	12.7	13.5	11.7	12.4	17.8	10.3	93	73	69	78	1.1	4.2	4.2	3.2	3 ○	5 ○	1	W 5	WSW 5	W 3
7	91.4	89.5	88.3	89.7	10.7	22.2	17.3	16.9	23.1	5.7	81	44	84	70	2.5	15.1	3.1	6.9	0 ○	3	10	SW 1	S 5	S 2
8	90.1	90.7	90.2	90.3	14.4	21.4	17.9	17.9	22.3	13.5	95	61	82	79	0.7	9.8	3.6	4.7	10	3 ⊙	5	WSW 1	ENE 2	NE 2
9	90.5	89.3	88.8	89.5	16.9	26.4	21.0	21.3	27.0	12.3	80	49	73	67	3.8	17.7	6.7	9.4	1 ○	3 ⊙	7	SE 3	S 5	S 1
10	90.1	89.4	90.5	90.0	17.1	24.2	18.4	19.5	24.7	16.2	83	60	91	78	3.4	12.2	1.9	5.8	10	6	1	S 3	SSW 5	SSE 2
11	90.3	89.2	89.8	89.8	19.5	29.4	24.2	24.3	30.1	15.8	87	47	67	67	3.1	21.9	9.9	11.6	1 ○	4 ⊙	7	SE 2	S 4	S 3
12	93.7	96.7	101.6	97.3	22.4	31.3	21.2	24.0	32.5	17.7	77	42	85	68	6.3	26.7	3.9	12.3	2 ○	2 ○	2	S 3	W 4	N 7
13	106.4	105.3	103.7	105.1	16.7	22.0	15.2	17.3	23.6	15.2	74	40	67	60	5.0	15.9	5.6	8.8	6 ○	1 ○	0	N 3	NW 5	N 4
14	104.3	102.8	102.4	103.2	13.1	21.0	16.3	16.7	22.9	8.9	77	39	54	57	3.5	15.2	8.4	9.0	1 ○	0 ○	0	NNW 5	N 4	N 4
15	103.9	102.9	100.9	102.6	14.2	21.0	16.6	17.1	22.4	9.6	66	46	59	57	5.4	13.6	7.7	8.9	5 ○	3 ○	1	NNE 4	N 5	NNE 2
16	100.2	99.1	96.8	98.7	15.9	22.4	18.1	18.6	24.0	9.5	65	43	61	56	6.3	15.4	8.1	9.9	0 ○	0 ○	0	NW 1	NNE 3	NNE 1
17	96.6	95.4	94.1	95.4	17.7	24.2	18.3	19.6	24.5	12.3	77	45	50	55	5.9	16.8	10.4	11.0	1 ○	2 ⊙	0	NNW 1	N 1	NE 1
18	94.6	92.8	90.6	92.7	17.1	26.8	21.2	21.6	26.9	12.2	62	37	52	50	7.4	22.2	12.1	13.9	0 ○	0 ○	0	NE 2	SE 1	E 1
19	88.6	87.3	86.8	87.6	17.9	26.8	18.7	20.5	27.6	14.0	85	53	80	73	3.0	16.2	4.4	7.9	2 ○	3 ○	10	S 2	SSW 6	WSW 2
20	87.9	89.4	91.9	89.7	15.8	17.5	15.5	16.1	22.8	12.7	90	94	92	92	1.7	1.2	1.3	1.4	4 ○	10 ⊘	2	SW 2	S 3	NW 1
21	94.7	93.9	90.5	93.0	15.1	22.3	18.9	18.8	23.4	11.4	68	47	70	62	5.5	14.3	6.5	8.8	3 ○	2 ○	3	N 2	E 2	E 2
22	87.3	83.7	81.1	84.0	17.9	27.0	20.8	21.6	27.2	14.6	90	56	91	79	2.0	15.5	2.3	6.6	1 ○	5 ○	10	S 1	SSW 4	SW 1
23	86.6	87.9	86.5	87.0	18.1	23.6	20.2	20.5	26.7	14.8	90	59	89	79	2.1	11.9	2.7	5.6	9	7 ○	9	SW 4	WSW 3	SE 1
24	88.2	84.6	81.1	84.6	17.7	27.2	20.2	21.3	28.9	15.8	95	60	95	83	1.0	14.3	1.2	5.5	1 ○	10	8	WSW 1	S 4	NW 4
25	83.4	87.3	92.8	87.8	17.7	22.4	13.3	16.7	23.5	13.3	85	51	75	70	3.0	13.2	3.8	6.7	7 ○	4 ⊙	3	WSW 10	WSW 8	NW 3
26	95.1	96.1	98.3	96.5	12.4	16.5	13.6	14.0	17.6	10.7	82	55	74	70	2.6	8.5	4.0	5.0	10	9	8	NW 2	NW 4	NW 2
27	100.5	99.8	101.9	100.7	14.1	17.8	12.1	14.0	19.6	8.9	62	50	81	64	6.1	10.1	2.7	6.3	0 ○	4 ⊙	0	NW 3	NW 5	NW 1
28	102.7	101.2	98.6	100.8	14.1	19.9	18.0	17.5	22.5	9.3	71	45	73	63	4.6	12.6	5.6	7.6	2 ○	3 ○	0	NW 2	W 3	W 2
29	98.8	98.8	98.3	98.6	21.0	27.0	21.8	22.9	28.7	15.0	77	47	70	65	5.8	18.9	7.9	10.9	6	5 ○	0	W 3	WNW 5	NNW 1
30	98.0	96.0	95.5	96.5	20.0	30.7	23.0	24.2	31.7	15.0	82	43	65	63	4.2	25.1	10.0	13.1	0 ○	3 ○	0	WSW 1	NW 3	NW 1
31																								
M	93.6	93.1	92.8	93.2	16.3	22.9	17.9	18.8	24.5	12.4	79	52	74	68	3.9	14.2	5.5	7.9	3.9	4.2	3.6	2.7	4.1	2.2

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w = 21\,m$ **Maj – Mai 1957**

DNI	WIATR	OPAD	GRUBOŚĆ ŚNIEGU	USŁONECZNIENIE	POGODA
1	8	.	.	-	
2	7	3.3	.	-	•° 9⁴⁵ 15³⁸ 20⁴⁵ 21¹² 22⁴⁰ — 24
3	6	5.6	.	-	•° 0⁰⁰ — 7²⁰ •¹ — 7⁴⁰ •° — 13⁴⁰ 15³⁰ 16¹⁵
4	7	.	.	-	= 3³⁰ — 11¹⁸
5	8	1.3	.	-	⊕ 12³⁵ — 17¹⁰
6	6	1.4	.	-	•° 3²⁵ — 6³⁰ 9⁴⁰ 10²⁵ 13³⁵
7	6	6.0	.	-	•° 2⁴⁵ — 3³⁰ 5³⁸ 8¹⁸ — 9³⁵ 10⁵⁵ *° — 11⁰⁵ •° — 13²⁵ 15¹⁵ — 16³⁰ 14⁴⁰ 19⁴⁵ 20²⁰ 21³⁰ 22²⁰ — 24, = 6²⁰ — 24
8	6	0.9	.	-	•° 0⁰⁰ — 2³⁰ 6¹⁵ 9⁴² 12³⁵ 14³⁵ •° — 19⁰⁵ 19²⁵ 21²⁰ — 23¹⁵, = 0⁰⁰ — 24
9	6	12.2	.	-	•° 6¹² — 15²⁵ 17⁴⁰ 18¹⁵ — 19³⁰ 20²⁰ 21³⁰ 24: = 0⁰⁰ — 24
10	6	17.7	.	-	•° 0⁰⁰ 4¹⁵ 6¹⁵ 9¹⁵ •² — 9³⁰ •¹ — 10²⁰ •° — 11³⁵ 12¹⁵ •° 14²⁰ 16⁴⁵ 19¹⁵ — 22¹⁷. = 0⁰⁰ — 13³⁰, 14³⁰ — 24
11	7	.	.	-	= 0⁰⁰ — 12¹⁵ 21³⁰ — 24
12	7	.	.	-	= 0⁰⁰ — 10³⁰
13	7	.	.	-	⌒° na — a, 20⁰⁰ — 24
14	7	0.4	.	-	▽ 16¹⁵⁻¹⁷, 16⁴⁵ — 17¹⁸: (K)° 15⁵⁸ NW, 16²⁰ NNW; = 2³⁰ — 9¹⁵; ⌒° 0⁰⁰ — 7¹⁵
15	7	.	.	-	
16	7	.	.	-	
17	7	.	.	-	
18	7	.	.	-	↙ 20⁰⁵ — 23³⁰ S–W–NE
19	8	.	.	-	
20	8	.	.	-	= 3³⁰ — 6¹⁵; ⌒ 1³⁰ — 7³⁰
21	6	0.0	.	-	= 6¹⁵ — 24
22	7	.	.	-	•° 3³⁰ — 5¹⁵; = 0⁰⁰ — 5³⁰
23	7	.	.	-	⌒ 20³⁰ — 24
24	7	.	.	-	= 0³⁰ — 8³⁰; ⌒ 0⁰⁰ — 7³⁰
25	8	.	.	-	
26	8	.	.	-	
27	8	.	.	-	
28	7	0.0	.	-	•° 10⁴⁷ 12⁰⁸ 14⁵⁰ 15¹²
29	8	.	.	-	⌒ na — 24
30	8	.	.	-	⌒ 0⁰⁰ — a
31	7	.	.	-	= 8³⁰ — 12¹⁵
Σ	—	48.8	—	-	UWAGI:

Czerwiec – Juin

1	7	.	.	-	
2	7	.	.	-	
3	7	.	.	-	= 4³⁰ — 9¹⁵
4	6	2.1	.	-	•° 13¹⁵ ... 55, 14³⁸ ... 15⁵⁰: = 3³⁰ — 24
5	7	2.7	.	-	•° 0¹⁵ — 1⁵⁰, 2³⁵ — 4²⁵, 5⁵⁰ • 7³⁶ — 8³⁵: = 0⁰⁰ — 10³⁵, 23³⁰ — 24
6	7	0.0	.	-	•° 1⁴⁵ — 2⁵⁰ ▽ 13¹⁰⁻¹⁸: = 0⁰⁰ — 10¹⁵: ⌒¹ 22³⁰ — 24
7	7	11.5	.	-	▽ 19¹⁰⁻⁴³ 23⁰⁵⁻¹⁵: (K)° 18⁵⁰ — 19¹⁰ NW K° 19¹⁰⁻²⁵⁻⁴³ NW — E ↙ 21¹⁵ — 22¹⁵: = 4³⁰ — 7⁴⁰; ⌒¹ 0⁰⁰ — a
8	8	.	.	-	▽ 7¹⁵⁻³⁵: = 1³⁰ — 5¹⁵ 6¹⁵ — 9²⁰: ⌒ 22⁰⁰ — 24: ⌒ 21³⁰ — 24
9	7	0.0	.	-	= 4¹⁵ — 7¹⁵: ⌒ 0⁰⁰ — 8⁰⁰: ⌒ 0⁰⁰ — 2⁰⁰ 21²⁰ — 22²⁵
10	8	4.4	.	-	•° 4⁴⁰ — 5²⁰ ▽ 14⁵⁵ — 15³², 15⁵⁰ — 16⁰⁷: K° 14⁵⁰ — 15¹⁰ — 16⁴⁰ W–SE
11	8	.	.	-	= 5¹⁵ — 8²⁰
12	8	.	.	-	
13	8	.	.	-	
14	8	.	.	-	
15	8	.	.	-	
16	8	.	.	-	
17	8	.	.	-	
18	8	.	.	-	
19	7	.	.	-	(K)° 17²⁵ — 18⁵⁰ NW
20	6	17.9	.	-	•° 10¹⁴ — 11²⁰ ▽² 13¹⁵ — 31 ▽° — 14¹⁸ ▽² — 15⁰⁵ ▽° — 15⁴⁰, K° 13⁰⁶ — 15³⁰ SE–S, = 5³⁰ — 16¹⁰, 22³⁰ — 24
21	8	.	.	-	= 0⁰⁰ — 7⁴⁰: ⌒² n — a
22	7	2.9	.	-	▽ 14⁵¹ — 15¹⁵ 22²⁵ — 23⁴⁵: K° 15¹⁵ — 15²⁸ — 16¹⁰ W–NE ↙ 21²⁰ W, 21²⁵ W (K)° 22⁵⁰ — 23²⁰ W–SE, W–NE; = 5¹⁰ — 9³⁰
23	7	2.4	.	-	▲ 18⁵⁰ — 5³ ▽ — 19⁰⁴; (K)° 18³⁵ — 19²⁵ S–SE ↙ 20⁵⁵ — 21³⁰: = 4³⁰ — 8²⁰
24	8	1.9	.	-	(K)° 18³⁵ — 19³⁵ SW–NE: = 3⁴⁰ — 9³⁰
25	7	1.2	.	-	▽ 2¹⁰ — 3¹⁵: = 2³⁰ — 6³⁰
26	7	.	.	-	•° 2²⁰ — 3⁴²
27	8	.	.	-	
28	7	.	.	-	
29	7	.	.	-	
30	7	.	.	-	(K)° 16¹⁵⁻²⁰ SE
31					
Σ	—	47.0	—	-	UWAGI:

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI A				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	96.9	96.5	95.7	96.4	20.9	28.0	21.1	22.8	28.6	16.8	74	51	69	65	6.4	18.5	7.7	10.9	1 ⊙	3 ⊙	0	N 1	NNW 2	NNE 1
2	95.2	92.8	92.9	93.6	18.8	29.8	18.7	21.5	30.8	15.5	77	41	98	72	4.9	24.5	0.5	10.0	0 ⊙	0 ⊙	10 ●	NE 2	SSE 3	E 4
3	95.9	96.4	96.3	96.2	16.6	22.5	17.7	18.6	23.7	15.9	79	50	62	64	4.1	13.6	7.7	8.5	2 ⊙	0 ⊙	0	NNE 5	NW 5	N 2
4	96.7	95.1	94.0	95.3	18.1	26.6	24.2	23.3	28.5	12.4	57	26	43	42	9.0	25.6	17.2	17.3	2 ⊙	2 ⊙	1	N 1	SW 2	C 0
5	92.4	90.8	91.4	91.5	20.6	34.6	25.2	26.4	35.4	16.6	70	32	61	54	7.3	37.4	12.3	19.0	5	2 ⊙	10 ⊼	SW 5	W 5	W 5
6	95.8	96.4	96.3	96.2	20.4	26.1	20.2	21.7	27.9	19.3	77	28	46	50	5.5	24.2	12.8	14.2	0 ⊙	0 ⊙	0	NW 3	WNW 3	N 1
7	97.9	97.1	96.4	97.1	20.0	27.1	21.7	22.6	29.1	13.6	50	30	52	44	11.6	25.1	12.6	16.4	3 ⊙	4 ⊙	0	C 0	NE 2	NE 1
8	96.6	93.8	90.8	93.7	19.2	32.3	24.4	25.1	34.7	15.4	59	27	63	50	9.1	35.1	11.4	18.5	0 ⊙	0 ⊙	10	E 4	SE 3	N 4
9	91.5	89.4	90.6	90.5	19.1	27.0	17.5	20.3	27.4	15.3	90	55	88	78	2.1	16.0	2.4	6.8	10	8 ⊙	7	C 0	NW 3	NNW 2
10	91.2	89.1	86.5	88.9	17.6	23.6	19.7	20.2	25.6	15.4	79	44	62	62	4.2	16.2	8.6	9.7	1 ⊙	5 ⊙	8	NNE 2	NE 2	ENE 1
11	84.1	84.0	83.5	83.9	18.7	22.1	18.4	19.4	24.1	15.4	62	55	90	69	8.2	11.9	2.1	7.4	4 ⊙	10	10	ENE 2	SE 3	ENE 2
12	83.4	85.7	87.4	85.5	18.5	23.8	19.7	20.4	24.3	17.5	87	68	89	81	2.7	9.6	2.6	5.0	10	9	10	E 2	SE 1	NE 1
13	90.3	92.1	93.0	91.8	18.5	24.2	21.4	21.4	25.8	17.5	90	68	78	79	2.1	9.7	5.7	5.8	10	8	9	NW 1	NW 1	NW 1
14	92.7	91.8	90.0	91.5	18.8	26.0	20.2	21.3	27.7	18.0	86	46	79	70	3.1	18.3	5.0	8.8	7 ⊙	4 ⊙	8	NW 2	NNW 2	SW 2
15	88.5	88.7	88.9	88.7	16.9	22.3	18.3	19.0	23.7	15.5	95	68	84	82	1.0	8.6	3.2	4.3	10 ≡	9	9	SW 3	WSW 3	NW 1
16	95.4	82.1	81.7	86.4	16.9	20.7	16.4	17.6	21.9	16.4	92	71	83	82	1.6	7.2	3.0	3.9	10 ●	8 ⊙	9	N 3	SE 2	WSW 6
17	80.9	82.7	85.2	82.9	13.1	14.2	14.1	13.9	16.5	12.9	82	89	85	85	2.8	1.8	2.4	2.3	10	10 ●	10	SW 10	WSW 8	WSW 5
18	86.7	87.2	87.0	87.0	15.3	20.6	16.5	17.2	22.5	13.6	79	54	68	67	3.7	11.2	6.1	7.0	10	9 ⊙	0	W 7	W 5	NW 1
19	87.9	87.3	86.3	87.2	14.0	23.3	20.4	19.5	25.3	10.9	85	43	64	64	2.3	16.2	8.7	9.1	0 ⊙	1 ⊙	1	SW 3	SW 2	S 1
20	85.8	84.2	81.3	83.8	17.5	27.2	21.6	22.0	28.3	14.5	75	39	59	58	4.9	22.1	10.7	12.6	2 ⊙	3 ⊙	10	SSE 1	ESE 4	SW 4
21	80.5	80.2	80.3	80.3	16.2	17.2	15.7	16.2	21.7	15.7	94	89	86	90	1.2	2.2	2.4	1.9	10 ●	10 ●	10	SW 2	SW 3	SW 4
22	79.6	79.6	79.5	79.6	14.5	19.4	15.3	16.1	21.3	14.2	89	72	88	83	1.8	6.2	2.1	3.4	10 ●	9 ⊙	10	SW 3	C 0	C 0
23	79.2	80.5	81.4	80.4	14.7	19.5	16.5	16.8	20.9	13.6	91	62	82	78	1.5	8.7	3.5	4.6	10	9	6	C 0	WSW 1	SW 2
24	82.7	83.6	86.7	84.3	15.8	19.4	15.5	16.6	21.1	13.4	93	70	79	81	1.3	6.8	3.7	3.9	10	9	9	WSW 4	NW 6	WNW 4
25	88.6	88.9	87.9	88.5	14.4	19.9	15.3	16.2	21.0	11.4	81	55	79	72	3.1	10.4	3.7	5.7	7	10	9	WSW 4	WSW 4	WSW 1
26	86.7	88.0	86.6	87.1	15.1	17.8	16.1	16.3	20.7	13.5	79	57	79	72	3.7	8.7	3.8	5.4	8	9	9	WSW 3	WSW 6	WSW 3
27	84.5	83.1	83.6	83.7	14.9	19.7	16.7	17.0	21.3	13.2	89	68	76	78	1.8	7.3	4.6	4.6	10	9	10 ●	SW 3	SW 4	SW 3
28	84.5	86.0	86.6	85.7	14.1	17.8	15.2	15.6	20.3	13.7	87	65	81	78	2.2	7.1	3.4	4.2	10	9 ⊙	4	WSW 4	WSW 4	W 1
29	88.7	89.3	91.8	89.9	13.3	21.0	15.1	16.1	21.9	9.9	84	49	72	68	2.5	12.8	4.8	6.7	1 ⊙	4 ⊙	0	WSW 2	SSW 5	W 1
30	93.3	93.2	95.2	93.9	12.4	20.3	15.9	16.1	21.8	10.8	87	54	75	72	1.9	11.0	4.5	5.8	6 ⊙	8	10	W 2	WSW 3	W 4
31	96.2	97.4	99.1	97.6	15.3	20.0	16.7	17.2	22.6	13.9	87	57	78	74	2.3	10.1	4.2	5.5	10	5 ⊙	7	WSW 4	WNW 4	NW 2
M	89.4	88.8	88.9	89.0	16.8	23.0	18.4	19.2	24.7	14.5	81	54	74	70	3.9	14.3	5.9	8.0	6.1	6.0	6.6	2.8	3.3	2.3

Sierpień – Août

1	100.8	100.9	98.8	100.2	15.3	19.4	17.8	17.6	22.4	13.0	78	58	65	67	3.9	9.3	7.1	6.8	5	3 ⊙	0	NW 2	WNW 3	WNW 3
2	98.1	96.9	96.8	97.3	16.9	22.0	16.1	17.8	22.8	11.9	78	56	65	66	4.2	11.6	6.5	7.4	2 ⊙	9 ⊙	1	C 0	WNW 2	NW 3
3	97.6	96.4	96.6	96.9	14.0	19.3	15.3	16.0	20.3	10.4	68	40	61	56	5.1	13.5	6.9	8.5	0 ⊙	5	3	NW 4	WNW 4	W 4
4	96.4	96.4	96.9	96.6	13.7	19.3	16.1	16.3	20.2	9.5	78	53	76	69	3.5	10.4	4.4	6.1	1 ⊙	10	9	WSW 2	NW 4	W 2
5	97.6	98.1	98.0	97.9	15.0	16.1	15.7	15.6	20.6	13.6	82	81	77	80	3.1	3.4	4.7	3.5	7	9 ●	3	NW 3	WNW 2	WNW 2
6	98.5	97.9	96.7	97.7	15.7	23.1	16.4	17.9	23.6	12.9	81	46	62	63	3.4	15.1	7.0	8.5	0 ⊙	2 ⊙	0	NNW 4	NNW 4	C 0
7	95.1	92.2	87.6	91.6	16.1	24.2	20.0	20.1	25.9	11.0	67	41	68	59	6.0	17.8	7.4	10.4	8 ⊙	4 ⊙	10	C 0	S 2	SW 2
8	83.6	85.3	86.4	85.1	17.0	19.5	16.5	17.4	21.2	15.8	89	66	84	80	2.2	7.7	3.1	4.3	8	9	8	WSW 3	NW 4	NW 2
9	87.1	87.0	84.3	86.1	15.9	22.3	17.5	18.3	23.5	12.7	83	50	75	69	3.1	13.5	4.9	7.2	0 ⊙	3 ⊙	0	C 0	ESE 3	ESE 2
10	80.2	79.5	84.6	81.4	17.7	21.8	16.7	18.2	25.1	14.4	78	71	86	78	4.4	7.7	2.7	4.9	8	10	0	ESE 2	WSW 7	W 2
11	90.3	91.7	91.1	91.0	16.2	26.2	22.9	22.0	28.3	13.3	81	39	61	60	3.4	20.7	11.0	11.7	0	4 ⊙	0	SW 5	SW 5	SSW 2
12	90.0	87.4	89.0	88.8	18.1	29.2	20.2	21.9	30.3	15.9	78	41	79	66	4.7	24.0	5.0	11.2	0 ⊙	1 ⊙	0	SE 2	SW 5	W 2
13	91.4	92.6	91.5	91.8	18.7	25.4	20.8	21.4	27.0	15.4	87	50	76	71	2.8	16.2	6.0	8.3	7	5 ⊙	4	C 0	SW 2	NNE 1
14	88.2	87.9	84.4	86.8	18.6	28.2	21.7	22.6	29.5	18.6	89	58	89	79	2.3	16.2	2.8	7.1	4 ⊙	0 ⊙	10 (⊼)	BSE 3	SE 2	E 3
15	85.9	86.4	87.4	86.6	16.5	21.6	18.8	18.9	23.5	16.5	88	63	69	73	2.4	9.7	6.7	6.3	8	4 ⊙	0	W 5	WSW 4	NW 1
16	88.6	88.1	86.8	87.8	15.7	24.0	19.3	19.6	25.5	12.9	94	40	83	72	1.1	17.8	3.8	7.6	1⊙≡	2 ⊙	10 ●	C 0	SW 1	NNE 1
17	87.2	88.2	88.4	87.9	13.7	15.5	13.5	14.0	19.3	13.1	93	83	90	89	1.1	3.0	1.6	1.9	10	10	9	W 4	W 5	SW 3
18	88.0	87.2	88.0	87.7	12.3	18.6	14.3	14.9	20.3	10.7	89	61	88	79	1.5	8.3	2.0	3.9	3 ⊙	7	0	WSW 5	SW 7	SW 2
19	90.1	91.4	93.0	91.5	11.9	20.4	17.3	16.7	22.4	10.1	95	56	67	73	0.7	10.5	6.5	5.9	9	5 ⊙	0	SW 3	WSW 5	W 2
20	94.1	94.9	94.9	94.6	14.9	17.8	14.8	15.6	18.6	14.6	90	76	94	87	1.6	5.0	0.9	2.5	10	10	0	NNW 2	C 0	SW 1
21	93.8	92.1	89.5	91.8	11.2	22.6	18.5	17.7	23.7	10.4	100	51	82	78	0.0	13.3	3.9	5.7	0 ≡	3 ⊙	10	SW 1	SW 2	S 1
22	84.6	85.7	87.2	85.8	15.8	13.5	12.6	13.6	18.5	12.5	98	99	94	97	0.3	0.2	0.9	0.5	9 ≡	10 ●	10 ●	W 1	NW 4	WSW 3
23	88.8	89.9	90.3	89.7	11.2	15.1	12.8	13.0	18.5	8.8	89	67	72	76	1.5	5.6	4.1	3.7	4	7	1	W 3	W 4	WSW 2
24	89.9	87.4	86.5	87.9	9.1	21.5	17.9	16.6	22.8	7.3	89	49	66	68	1.3	13.2	6.9	7.1	0 ⊙	1 ⊙	10	SE 3	SSW 3	S 5
25	94.7	94.7	91.2	93.5	11.7	19.7	14.8	15.2	21.3	9.7	91	43	71	68	1.1	13.1	4.8	6.3	0 ⊙	1 ⊙	0	WSW 4	WSW 3	SSW 1
26	88.9	87.4	89.1	88.5	12.2	22.4	13.7	15.5	22.8	10.7	92	50	72	71	1.2	13.6	4.4	6.4	7	4 ⊙	7	SSW 1	WSW 3	W 3
27	91.4	92.3	92.2	92.0	11.8	16.8	13.5	13.9	19.1	8.0	82	60	81	74	2.5	7.7	3.0	4.4	0 ⊙	7	10	WSW 4	W 2	SW 1
28	90.5	90.5	90.6	90.5	11.5	18.1	16.0	15.4	20.4	10.7	91	71	83	82	1.2	6.0	3.1	3.4	10	7 ⊙	9	SE 1	SW 3	C 0
29	90.0	90.7	93.7	91.5	12.7	13.2	11.8	12.4	16.1	11.8	98	95	91	95	0.4	0.7	1.1	0.7	10 ●	10 ●	10	N 3	N 5	NW 3
30	94.5	95.3	96.0	95.3	10.7	16.0	11.3	12.3	17.3	9.3	89	65	79	78	1.5	6.3	2.8	3.5	3 ⊙	8 ⊙	0	W 4	W 4	NW 3
31	96.4	95.9	94.4	95.6	8.0	17.5	12.8	12.8	18.3	6.4	97	49	87	78	0.3	10.2	1.9	4.1	5	4 ⊙	10 ●	C 0	SW 4	WSW 1
M	91.4	91.2	91.0	91.2	14.2	20.3	16.4	16.8	22.2	12.0	86	59	77	74	2.3	10.7	4.4	5.8	4.5	5.6	4.6	2.4	3.5	2.0

Sandomierz

$H_s = 202$ m $H_b = 200{,}3$ m $h_w = 21$ m

Lipiec – Juillet 1957

DNI	WILGOTNOŚĆ WZGLĘDNA	OPAD R	GRUBOŚĆ POKRYWY ŚNIEŻNEJ	USŁONECZNIENIE	POGODA
1	8	.	.	-	
2	7	6.3	.	-	▽ 18¹⁵–21⁰⁵ ●⁰ 21¹⁷–22²⁰ ☇⁰ 18¹⁵–18³⁵–20⁴⁵ SW–N–NW, = 17⁵⁰–24
3	8	.	.	-	= 0⁰⁰–4²⁵
4	8	.	.	-	
5	7	2.7	.	-	▽ 17⁵⁵–18²⁰ 19¹⁵–³⁰ 21²⁸–22⁴⁰ ☇⁰ 17⁵⁰–18¹⁰–18³⁰ SW–SE ☇¹ 19¹⁰–⁵⁵ S–NE ☇⁰ 21³⁰–21⁴²–22⁵⁰ SW–S–E–NE
6	8	.	.	-	▽ 3⁵³–4³¹ ☇⁰ 3⁵⁵–3⁵⁸–5⁰⁰ S–SE, = 4⁵⁰–7¹⁵
7	8	.	.	-	
8	8	13.8	.	-	▽ 22³⁰–24, (☇)⁰ 20³⁰–24 NW
9	7	8.3	.	-	▽ 0⁰⁰–³⁰ ●⁰ 3⁴⁰ 4⁴⁰ ●¹ 5⁰⁷–6²⁰ ▽ 15¹⁴–⁴⁰, (☇) 0⁰⁰ NW, 15¹⁰–¹⁴ ☇¹ 15¹⁴–¹⁷–⁵⁰
10	8	.	.	-	= 4³⁰–8³⁰
11	7	21.5	.	-	●⁰ 13⁴⁰ 14²⁸ ▽ 16⁴⁰–17⁰⁸, 17¹⁵–²⁵ 17³⁵–⁴², 17⁴⁵–20¹³ ●⁰ 22³⁰–24, (☇)⁰ 17⁴⁴–⁵⁰ S ☇⁰ 17⁵⁰–18⁰⁶–19⁵⁵ S–SW
12	7	18.6	.	-	●⁰ 0⁰⁰–3³⁷ ▽ 14⁵⁰–17¹⁵, 17⁵⁵–18¹⁵, 18³²–⁴⁵, ☇ 14⁵⁵–15¹⁰–15⁵⁰ S–NNW
13	7	.	.	-	= 2³⁰–9³⁰, 21³⁰–24
14	7	.	.	-	= 0⁰⁰–8¹⁵, ⌓¹ 23³⁰–24
15	6	1.6	.	-	= 4³⁰–5¹⁵ ≡² 6³⁰ ≡¹ 6⁴⁰ ≡⁰ 8⁵⁰ = – 12²⁰ 21³⁰–24, ⌓¹ 0⁰⁰–5¹⁵
16	8	10.8	.	-	▽ 6³⁰–4³⁷, 6³⁷–11¹⁵ 14²⁰–⁴⁰ (☇)⁰ 9¹⁵–11²⁵ N–SE = 0⁰⁰–11³⁰, 23²⁰–24
17	6	0.9	.	-	▽ 0⁴⁵–1¹⁰ ●⁰ 1¹⁵–2³⁰, 3⁰⁵, 7³⁵–⁵⁰–13⁴⁰, 14⁴⁵, 17⁴⁰, = 0⁰⁰–4¹⁵, 8¹⁵–17⁴⁵
18	8	0.0	.	-	▽ 12¹⁵–³⁰
19	7	.	.	-	= 1³⁰–8³⁰
20	7	6.2	.	-	▽ 22⁴⁵–23¹², ☇ 23⁰⁵ SW–W = 2²⁰–8²⁰, ⌓⁰ n–8⁰⁰
21	6	6.8	.	-	▽ 0³⁶–3⁷⁸ ●⁰ 5⁴⁰–14³⁰, = 2³⁰–15³⁰
22	6	0.7	.	-	●⁰ 4³⁰–8¹⁰ 12⁴⁵–13¹⁵ 16⁰⁵–⁴⁰ 18⁰²–³⁰, = 0³⁰–24
23	7	0.7	.	-	= 0⁰⁰–13¹⁵, 22³⁰–24 ⌓¹ 22³⁰–24
24	7	4.2	.	-	●⁰ 0¹⁰–1⁴⁰ ▽ 11¹⁵–²⁷ 12¹⁵–³⁰ ●⁰ 15³⁰ 16⁴⁰ ▽ 17⁵⁰–18⁰⁵ ●⁰ 18⁴⁰ 19¹⁰, = 0⁰⁰–10³⁰, ⌓¹ 0⁰⁰–¹⁰
25	7	2.9	.	-	= 4¹⁵–10³⁰, 21³⁰–24
26	7	3.3	.	-	●⁰ 1³⁰–4²⁰, 21⁵⁵–24, = 0⁰⁰–4²⁰, 23²⁰–24
27	7	0.9	.	-	●⁰ 0⁰⁰–3²⁵ ▽ 13⁴⁵–14⁰² ●⁰ 21⁰⁸–24, = 0⁰⁰–9²⁵
28	7	.	.	-	●⁰ 0⁰⁰–1¹⁵ 3⁴⁰, = 0³⁰–6²⁰, 22²⁰–24
29	7	.	.	-	= 0⁰⁰–6⁴⁰ ⌓² n–a ⌓¹ 20³⁰–24
30	7	1.6	.	-	●⁰ 22²⁵–24, = 2³⁰–8⁴⁵, ⌓¹ 0⁰⁰–a
31	8	.	.	-	●⁰ 0⁰⁰–⁴⁵, 1¹⁵–2⁴⁰ 3³⁰–4⁴⁵, = 0³⁰–6⁴⁵, 23²⁰–24
Σ	–	111.8	–	-	UWAGI

Sierpień – Août

1	7	.	.	-	= 0⁰⁰–7³⁰
2	7	.	.	-	= 4³⁰–10²⁵
3	8	.	.	-	
4	7	0.2	.	-	▽ 13³⁸–14⁰⁸, ⌓ n–1
5	8	0.3	.	-	▽ 12⁴⁵–⁵⁰, 13¹⁷–14⁰², ⌓¹ 20⁰⁰–24
6	8	.	.	-	⌓¹ 0⁰⁰–8³⁰ ⌓ 21³⁰–24
7	7	7.9	.	-	●⁰ 19⁴⁸ 20⁰⁷ ▽ 22⁴⁰–24, (☇)⁰ 22⁵⁰–23²⁰ N–W ☇⁰ 23²⁰–³⁰–⁴⁰ W–E (☇)⁰ 24 W–E, ⌓ 0⁰⁰–8⁰⁰
8	7	0.3	.	-	▽ 0⁰⁰–³⁵ 3²⁵–4³⁰, 9²³–⁴⁰, 18⁰⁵–⁴⁰, (☇)⁰ 0⁰⁰–⁴⁰ W–E ☇ 3¹⁵–4⁴⁰ S, = 11⁵–11⁴⁰
9	7	.	.	-	= 0¹⁵–11²⁵, ⌓¹ 21¹⁵–24
10	7	.	.	-	⌓¹ 0⁰⁰–a
11	8	.	.	-	⌓⁰ 2⁰⁰–a ⌓ 22⁰⁰–24
12	8	5.9	.	-	▽ 17³⁵–18⁰⁷ ☇¹ 17³⁰–17³⁵–18¹⁵ SE–E, ☇ 21¹⁵–24 S, = 4³⁰–6³⁰, ⌓ 0⁰⁰–9³⁰
13	7	2.4	.	-	☇ 0⁰⁰–²⁰ S, = 4³⁰–11⁴⁰
14	7	12.3	.	-	▽ 1⁴⁰–²⁰⁸ 6⁴³–7⁰⁶ 18¹⁸–19¹⁰ 20⁵⁴–21⁰⁵ 22⁵²–23⁰⁸ ▲ 23⁰⁶–¹² ▽ 23⁰⁸–⁵⁵ ☇⁰ 6⁴⁰–6⁵²–7²⁰ SW–NE 18¹⁵–18⁴⁰–19³⁵ S–NE
15	7	.	.	-	= 0⁰⁰–11²⁵, ⌓² 20³⁰–24 [illegible] ☇¹ 22⁵⁰–23⁰⁸ W–N–NE, 23⁰²–⁰⁵, = 18³⁰–24
16	7	9.3	.	-	▽ 19⁴⁵–21⁴⁰ 22⁴⁵–23¹³, ☇⁰ 19⁴⁵–20⁰³–20³⁰ SW–NE, = 3³⁰–6³⁰ ≡¹ 7³⁵ = – 10³⁰, 19³⁰–24, ⌓² 0⁰⁰–6³⁰
17	7	0.2	.	-	▽ 5⁰⁴–²⁰ ●⁰ 7⁵²–8¹⁵, 10⁴⁰–13¹⁵, = 0⁰⁰–8²⁰
18	7	0.8	.	-	▽ 16²⁰–³⁸, 16⁵²–17⁰⁸, = 1³⁰–6²⁰
19	7	.	.	-	= 6³⁰–13¹⁵
20	6	0.0	.	-	●⁰ 11¹⁵–13²⁰, = 5⁴⁰–14¹⁵, 21²⁰–24, ⌓¹ 20³⁰–24
21	7	2.2	.	-	●⁰ 23³⁵–24, = 0⁰⁰–5⁴⁵ ≡² 8¹⁵ ≡¹ 8⁴⁰ ≡⁰ 9⁴⁵ = – 11³⁰, ⌓¹ 0⁰⁰–a
22	6	6.7	.	-	●⁰ 0⁰⁰–5⁰⁵, 13³⁸–⁵⁰, 18³⁰ ●¹ 18⁴⁵ ●⁰ 21⁴⁰, = 0⁰⁰–5⁴⁰ ≡¹ 6³⁸ ≡⁰ 7⁴⁵ = – 10³⁰, 12⁵⁰–14¹⁵, 17⁴⁰–24
23	8	0.0	.	-	▽ 12¹⁰–²¹, 13¹⁵–²⁸, = 0⁰⁰–³⁰, ⌓ 20³⁰–24
24	8	0.5	.	-	●⁰ 22³⁵·⁴⁸, 23³²–24, = 3³⁰–8³⁰, 23³⁰–24, ⌓¹ 0⁰⁰–10¹⁵
25	8	.	.	-	●⁰ 0⁰⁰–14⁵, = 0⁰⁰–7³⁰
26	7	.	.	-	= 4¹⁵–8³⁰, ⌓² n–a ⌓⁰ 21¹⁵–24
27	7	1.0	.	-	▽ 21²⁰–³⁰, = 3³⁰–9²⁰, ⌓¹ 0⁰⁰–a
28	7	7.4	.	-	▽ 22¹⁵–³⁰, = 23³⁵–24
29	6	8.8	.	-	●⁰ 4¹⁵–6²⁵ ●¹ 8²⁵–³⁰ ●⁰ – 15¹⁰ 16²⁰
30	7	.	.	-	= 0⁰⁰–9⁴⁰
31	7	2.3	.	-	●⁰ 20¹⁵–23²⁰, = 4²⁵–7³⁰, 21²⁰–24, ⌓² na–a
Σ	–	68.5	–	-	UWAGI

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P.. 900 ..				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	93.7	95.5	96.2	95.1	10.4	15.9	11.5	12.3	17.3	10.0	95	62	82	80	0.6	6.8	2.5	3.3	7 ⊙	7 ⊙	0	SW 2	WSW 7	WSW 1
2	97.1	95.3	93.8	95.4	9.5	20.0	15.5	15.1	20.6	7.2	92	54	80	75	1.0	10.9	3.5	5.1	7 ⊙	6 ⊙	10	SSW 1	SSW 2	SW 1
3	91.6	92.2	92.7	92.2	10.8	18.3	14.7	14.6	19.5	10.7	95	68	86	83	0.7	6.8	2.4	3.3	7 ⊙	7 ⊙	10	SE 2	WSW 3	NE 1
4	92.9	94.6	97.4	95.0	13.0	14.5	12.9	13.3	15.0	12.6	95	91	91	92	0.7	1.5	1.4	1.2	9	10 ●	10 ●	N 1	N 4	N 4
5	98.3	97.7	96.3	97.4	11.9	17.8	16.0	15.4	19.0	11.4	94	67	85	82	0.8	6.7	2.7	3.4	9	9 ⊙	10	NNW 3	NNE 1	C 0
6	94.8	94.7	95.1	94.9	14.7	19.9	16.0	16.6	20.9	13.6	92	60	76	76	1.3	9.3	4.4	5.0	10	8 ⊙	2	NNW 1	NW 1	C 0
7	97.1	97.9	98.4	97.8	12.7	21.4	16.3	16.7	22.8	11.0	94	56	79	76	0.9	11.2	3.8	5.3	0	2	0	NNW 1	E 2	E 2
8	98.8	99.4	98.8	99.0	12.3	24.0	19.4	18.8	25.8	10.7	85	54	71	70	2.2	13.7	6.4	7.4	0 ⊙	0 ⊙	0	E 2	S 2	C 0
9	99.2	98.9	97.3	98.5	14.0	25.4	20.2	20.0	27.0	12.8	92	55	69	72	1.3	14.4	7.3	7.7	0 ⊙	0 ⊙	0	SE 2	SSE 1	SW 1
10	97.5	96.3	95.7	96.5	15.7	17.3	13.6	15.0	20.3	13.6	96	85	95	92	0.7	2.9	0.7	1.4	10 ≡	10	10	NW 2	NW 5	N 2
11	93.0	89.4	84.0	88.8	11.8	19.2	15.5	15.5	19.9	10.3	95	56	78	76	0.6	9.8	3.9	4.8	2 ⊙	7 ⊙	10	NW 2	SSW 2	S 1
12	78.2	75.7	82.4	78.8	15.8	24.4	13.2	16.6	25.0	12.9	87	42	93	74	2.2	17.9	1.1	7.1	10	3 ⊙	10	SSW 4	WSW 14	SW 2
13	86.3	86.8	84.6	85.9	8.4	16.7	13.3	12.9	18.0	6.9	87	41	81	70	1.4	11.2	3.0	5.2	3 ⊙	5 ⊙	10	SSW 2	SW 12	SSW 4
14	85.5	85.6	85.2	85.4	10.3	16.9	14.1	13.8	18.0	9.1	76	43	70	63	3.0	10.9	4.8	6.2	3 ⊙	4 ⊙	8	WSW 4	SSW 7	SW 2
15	78.7	85.9	90.5	85.0	11.1	12.8	11.3	11.6	14.4	9.8	91	68	76	78	1.1	4.7	3.3	3.0	10 ●	4 ⊙	10	SW 5	WSW 7	WSW 7
16	93.6	93.3	94.2	93.7	6.9	14.3	9.1	9.8	15.6	6.5	97	52	71	73	0.3	7.8	3.4	3.8	5	7 ⊙	0	WSW 2	SW 3	WNW 2
17	94.0	92.5	89.6	92.0	4.8	11.6	9.6	8.9	13.9	4.8	94	61	89	81	0.6	5.3	1.3	2.4	0 ⊙	10	10	WSW 3	WSW 5	WSW 4
18	86.9	86.7	87.0	86.9	8.7	11.6	10.7	10.4	12.9	8.4	88	60	75	74	1.3	5.4	3.2	3.3	9	10	9	W 4	W 10	W 8
19	87.6	86.4	84.4	86.1	8.0	15.9	11.8	11.9	17.4	7.5	89	49	97	78	1.2	9.2	0.3	3.6	2 ⊙	8	10 ●	WSW 8	WSW 9	SW 5
20	84.2	87.1	90.9	87.4	11.7	15.0	9.3	11.3	15.7	9.3	93	56	85	78	1.0	7.4	1.7	3.4	10 ●	6 ⊙	4	WSW 4	NW 5	W 3
21	93.2	93.4	93.2	93.3	6.5	15.5	9.1	10.0	15.9	5.7	93	41	76	70	0.7	10.3	2.8	4.6	6 ⊙	2 ⊙	0	WNW 1	WSW 3	ENE 1
22	90.8	88.8	89.0	89.5	8.3	16.6	15.3	13.9	20.3	6.8	92	77	92	87	1.0	4.4	1.3	2.2	9	10 ●	10	SE 1	SW 3	SW 3
23	86.4	82.0	77.1	81.8	13.7	20.5	16.1	16.6	21.8	12.6	92	68	87	82	1.3	7.7	2.3	3.8	6 ⊙	10	10	SW 1	SSW 5	SW 7
24	80.6	82.0	84.2	82.3	14.0	15.7	8.5	11.7	17.4	8.5	83	71	80	78	2.7	5.2	2.3	3.4	9	4 ⊙	10 ●	W 5	W 7	WNW 5
25	88.8	91.0	94.0	91.3	5.3	11.7	7.2	7.8	12.1	4.7	84	48	71	68	1.4	7.1	2.9	3.8	2 ⊙	4 ⊙	2	WSW 7	W 8	W 5
26	93.0	92.7	93.7	93.1	4.2	9.6	6.2	6.6	10.9	1.6	74	49	72	65	2.1	6.1	2.7	3.6	1 ⊙	9	3	W 3	NW 3	WSW 3
27	94.0	94.5	88.1	92.2	1.3	10.7	7.6	6.8	12.7	0.6	98	46	71	72	0.2	7.0	3.0	3.4	8 ⊙	2 ⊙	10	SW 3	WSW 2	SW 4
28	80.3	82.2	82.9	81.8	8.3	12.7	8.6	9.6	13.4	7.0	90	61	86	79	1.1	5.7	1.6	2.8	9	7 ⊙	2	WSW 5	W 8	WSW 7
29	83.3	80.2	77.1	80.2	7.9	9.5	10.0	9.4	11.1	6.0	90	95	95	93	1.0	0.7	0.7	0.8	9	10 ●	10	WSW 5	SW 3	SW 5
30	79.9	83.6	89.0	84.2	7.0	9.1	6.5	7.3	10.5	6.0	85	56	81	74	1.4	5.1	1.9	2.8	9	7	10	W 5	W 7	WSW 5
31																								
M	90.0	90.1	90.1	90.1	10.0	16.2	12.3	12.7	17.5	8.6	90	60	81	77	1.2	7.8	2.8	3.9	6.0	6.3	6.7	3.0	5.0	3.2

Październik – Octobre

1	92.7	93.5	94.4	93.5	3.1	10.2	6.2	6.4	10.3	2.9	95	60	82	79	0.4	4.9	1.7	2.3	9	8	10	WNW 2	WSW 2	W 3
2	98.7	100.7	100.7	100.0	3.5	8.3	3.2	4.6	9.4	2.5	91	63	86	80	0.6	4.0	1.1	1.9	0 ⊙	7 ⊙	4	WNW 3	NW 4	W 3
3	97.3	93.9	90.5	93.9	-3.1	10.5	6.7	5.2	11.8	-3.4	100	43	72	72	0.0	7.2	2.7	3.3	0 ≡	1 ⊙	10	C 0	SSW 4	SW 3
4	88.2	90.4	95.9	91.5	6.9	10.2	3.8	6.2	10.6	3.7	87	48	80	72	1.3	6.4	1.6	3.1	10	4 ⊙	0	SW 3	W 7	W 6
5	99.9	100.2	98.8	99.6	1.7	9.3	3.5	4.5	10.1	0.5	87	61	86	78	0.9	4.5	1.0	2.1	0 ⊙	10	0	W 4	WSW 5	W 2
6	97.0	97.8	100.9	98.6	2.7	11.9	9.5	8.4	12.5	1.5	82	57	86	75	1.3	6.0	1.7	3.0	10	10	10	SW 5	WSW 6	W 3
7	101.2	100.9	101.3	101.1	6.7	13.3	11.9	11.0	14.5	6.7	96	65	84	82	0.4	5.3	2.1	2.6	7	10	10	SW 3	W 5	WNW 3
8	104.2	106.2	106.9	105.8	8.7	12.7	8.2	9.4	14.5	8.2	96	67	85	83	0.4	4.9	1.7	2.3	0 ⊙	9	0	NW 2	NE 1	SE 2
9	105.2	104.4	101.9	103.8	2.2	15.9	8.9	9.0	16.4	1.9	91	38	62	64	0.7	11.2	4.4	5.4	0 ⊙	0 ⊙	0	E 3	SSE 3	SE 3
10	100.8	100.9	100.0	100.6	2.7	17.1	10.9	10.4	19.4	2.2	95	57	81	78	0.4	8.3	2.4	3.7	0 ⊙	0 ⊙	0	SE 1	SW 1	SSW 2
11	100.3	99.3	98.4	99.3	3.7	16.3	10.1	10.0	17.3	2.8	98	61	85	81	0.2	7.2	2.0	3.1	10 ≡	0 ⊙	0	SSW 2	SW 3	SW 2
12	98.2	97.6	100.9	98.9	2.7	16.3	13.1	11.3	17.7	2.1	98	57	84	80	0.1	7.9	2.5	3.5	0 ≡	0 ⊙	10	SW 2	SW 5	NW 5
13	104.8	104.7	102.4	104.0	8.5	14.3	9.4	10.4	14.8	8.5	96	60	84	80	0.5	6.5	1.9	3.0	10	7 ⊙	0	NW 1	S 2	SSW 1
14	100.6	100.1	101.0	100.6	4.9	17.2	10.0	10.5	17.7	3.8	98	59	91	83	0.2	8.0	1.1	3.1	10 ≡	4 ⊙	8	SW 2	W 4	WNW 3
15	104.1	104.2	105.0	104.4	8.0	11.1	7.0	8.3	12.4	6.2	96	72	77	82	0.4	3.7	2.3	2.1	10 ≡	9	10	C 0	W 1	N 2
16	104.4	102.6	100.1	102.4	5.9	11.5	5.1	6.9	12.3	5.1	85	61	89	78	1.4	5.4	1.0	2.6	10	1 ⊙	0	N 1	SSE 3	SE 3
17	97.2	96.1	97.2	96.8	2.4	17.6	13.0	11.5	18.6	2.1	98	50	89	79	0.2	10.0	1.6	3.9	0 ⊙ ≡	0 ⊙	10	SSE 1	SSW 3	WNW 1
18	94.1	92.9	90.9	92.6	10.2	14.8	12.5	12.5	16.2	10.1	91	76	71	79	1.1	4.0	4.2	3.1	10	10 ●	0	WSW 2	SW 3	SW 4
19	90.5	89.5	87.0	89.0	8.4	19.7	13.2	13.6	20.3	8.2	77	40	60	59	2.5	13.6	6.1	7.4	6 ⊙	3 ⊙	0	SW 2	SW 3	SW 5
20	85.5	88.2	92.2	88.6	9.1	12.1	8.5	9.6	16.8	8.4	77	81	93	84	2.7	2.7	0.8	2.1	2	10	10 ●	SW 3	NW 6	NNW 3
21	94.4	94.0	92.3	93.6	6.9	10.9	8.3	8.6	11.6	6.9	96	70	83	83	0.4	3.8	1.9	2.0	10	7 ⊙	10	NNW 1	S 2	SE 4
22	86.5	83.5	81.6	83.9	6.7	9.7	8.3	8.2	10.3	6.7	90	82	94	89	1.0	2.2	0.7	1.3	10	10	10 ●	S 2	SE 3	SE 2
23	81.7	84.7	90.8	85.7	7.9	9.3	7.0	7.8	10.0	7.0	99	96	91	95	0.1	0.5	0.9	0.5	10 9	10 ●	0	SE 1	NW 1	NW 3
24	93.1	93.0	96.9	94.3	3.2	9.5	8.2	7.3	10.0	2.2	100	65	89	85	0.0	4.2	1.2	1.8	10 ≡	9	10	WSW 3	WSW 7	W 3
25	101.1	102.6	103.1	102.3	7.0	10.6	4.9	6.8	10.9	4.9	88	59	92	80	1.2	5.2	0.7	2.4	9	9	0	W 3	W 2	WSW 1
26	102.1	101.6	100.3	101.3	1.1	10.5	6.7	6.2	11.8	1.0	96	68	81	82	0.2	4.1	1.9	2.1	9	0 ⊙	0	WSW 1	SW 2	S 2
27	98.5	97.5	97.0	97.7	-0.1	13.0	9.7	8.1	13.8	-0.2	98	69	84	84	0.2	4.6	1.9	2.2	0 ≡	0 ⊙	10	C 0	SW 3	SW 1
28	97.3	97.4	97.4	97.4	7.0	11.9	10.7	10.1	12.7	7.0	96	77	81	85	0.4	3.1	2.5	2.0	10	10	10	SW 2	SW 2	SW 1
29	97.4	97.1	97.0	97.2	4.3	12.3	6.9	7.6	13.6	3.3	100	66	94	87	0.0	4.8	0.5	1.8	10 ≡	7 ⊙	0	SW 1	SW 3	SW 1
30	95.6	93.8	93.2	94.2	2.0	13.8	8.7	8.3	15.5	2.0	98	70	86	85	0.2	4.7	1.5	2.1	10 ≡	3 ⊙	5	SW 1	SW 3	SSW 2
31	92.9	92.0	90.1	91.7	5.1	13.7	8.0	8.7	14.6	4.2	95	68	89	84	0.4	5.1	1.2	2.2	9	0 ⊙	0	WSW 2	SW 4	SW 2
M	97.0	96.8	97.0	96.9	4.8	12.8	8.5	8.6	13.8	4.2	93	63	84	80	0.6	5.6	1.9	2.7	6.5	5.4	4.7	1.9	3.3	2.6

Sandomierz $H_s = 202\ m$ $H_b = 200{,}3\ m$ $h_w = 21\ m$ **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	= 0⁰⁰–10³⁰ ; 20⁰⁰–24 ; ⌒ 20³⁰–24
2	7	.	.	–	= 0⁰⁰–11²⁰ ; ⌒¹ 0⁰⁰–11¹⁵
3	7	2.0	.	–	•⁰ 21³⁰ , 23³⁵–24 ; = 4⁴⁵–11³⁰ , 21⁴⁰–24 ; ⌒⁰ na – a
4	6	3.1	.	–	•⁰ 0⁰⁰–40 •¹ 1³⁰ •⁰ 3²⁰ 4³⁵–5⁷⁰ , 9⁴⁰ 10¹⁰ , 11⁵⁰–13¹⁰⁻⁵⁰ •¹ 15¹²⁻²⁸ •⁰ 16²⁴ , 17⁴³–19¹⁵ , 20⁴⁵ 24 ; = 0⁰⁰–2⁻¹
5	7	.	.	–	•⁰ 0⁰⁰ 3¹⁵ ; = 0⁰⁰–10³⁰
6	7	.	.	–	= 2⁴⁰–11¹⁵ , 20⁴⁰–24 ; ⌒¹ 20³⁰–24
7	7	.	.	–	= 0⁰⁰–12¹⁵ , 23³⁰–24 ; ⌒² 0⁰⁰–a ⌒ 22³⁰–24
8	7	.	.	–	= 0⁰⁰–12⁴⁰ ; ⌒² 0⁰⁰–11¹⁰
9	7	.	.	–	= 5¹⁵–9³⁰ , 22⁵⁰–24 ; ⌒⁰ 4⁵⁰–9³⁰ , 20³⁰–24
10	6	1.0	.	–	•⁰ 19¹⁰ 20⁵⁰ ; = 0⁰⁰–6³⁰ ≡⁰–8¹⁵ = – 13²⁵ , 19²⁰–24 ; ⌒⁰ 0⁰⁰–a
11	7	0.4	.	–	= 0⁰⁰–8⁰⁰ ≡¹–9⁵⁰ = – 10⁴⁰
12	7	1.4	.	–	•⁰ 5³⁵–7⁰⁶ ● 16²⁵⁻⁴⁵ , 16⁵⁰–17³⁰ , 17⁵⁰–18²² , 20³⁰⁻⁴⁰ ; ≫ 13¹⁵⁻³⁹ ≫ –13⁴³ ≫ 16⁰⁸–17²² ; = 2⁰⁰–8⁴⁰ , 21²⁰–24
13	7	.	.	–	= 0⁰⁰–7⁴⁰
14	8	2.7	.	–	= 4³⁰–6¹⁵ ; ⌒ n – a
15	8	.	.	–	•⁰ 4¹⁰–45 , 5³⁵–6¹⁰ , 7³⁵ ; = 4¹⁵–10³⁰
16	7	.	.	–	= 3²⁰–11¹⁵ , 21³⁰–24 ; ⌒ 20¹⁵–24
17	7	3.4	.	–	▽ 16²⁰⁻³⁵ •⁰ 23⁵⁵–24 ; = 0⁰⁰–10⁴⁰ , 15⁴⁵–24 ; ⌒ 0⁰⁰–10²⁰
18	6	.	.	–	•⁰ 0⁰⁰–2³⁰ 5⁴⁰ ; = 0⁰⁰–8¹⁵
19	7	2.7	.	–	•⁰ 17¹⁰–19¹⁰ 20²⁰–23⁴⁰ ; = 6²⁰–9³⁰ , 17¹⁰–24
20	7	.	.	–	•⁰ 0¹⁵–2³⁵ 3²⁰–4³⁰ , 7³⁵ ; = 0⁰⁰–8²⁰ ; ⌒⁰ 20⁰⁰–24
21	7	.	.	–	= 2³⁰–9⁴⁵ , 23⁴⁰–24 ; ⌒ 0⁰⁰–10¹⁵ , 21²⁰–24
22	6	0.0	.	–	•⁰ 13¹⁵..25 11 ; = 0⁰⁰–13⁴⁵ 21¹⁵–24 ; ⌒ 0⁰⁰–a
23	7	18.2	.	–	▽ 15⁰⁵–16³⁷ 16⁴³–17¹⁰ ; = 0⁰⁰–10⁴⁰ 17⁴⁰–24
24	7	1.9	.	–	▽ 17¹⁰–17 , 18⁵⁰–19²⁵ •⁰–21⁴⁰ ; ≫ 9⁴⁰–11³⁰ ; = 0⁰⁰–6³⁰ , 19³⁰–24
25	7	.	.	–	= 0⁰⁰–6¹⁵
26	7	.	.	–	⌴⁰ 3³⁰–8¹⁰ ; ⊕ 9⁴⁰–16¹⁰
27	7	0.8	.	–	•⁰ 22¹⁰–23¹⁵ ; ⌴⁰ 3³⁰–8³⁰
28	8	2.1	.	–	•⁰ 6³⁵–7²⁵ ● ▽ 11³⁰⁻⁴⁰ , 14⁵⁵–15⁰⁵ , 16⁴⁰–17⁰⁵ , 18³⁵⁻⁵⁰ , 19⁰⁵–25 , 19³⁵–45
29	6	9.1	.	–	•⁰ 7¹⁵–20¹⁵ , 23³⁰–24 ; = 6³⁰–24
30	8	0.0	.	–	•⁰ 0⁰⁰–25 , 1²⁰ 2³⁰–5²⁷ ; = 0⁰⁰–5³⁵
31					
Σ	–	48.8	–	–	UWAGI.

Październik – Octobre

1	7	.	.	–	= 6¹⁰–9²⁰ ; ⊕ 9⁴⁰–11¹⁵
2	7	.	.	–	
3	7	.	.	–	≡² 5⁴⁵–6¹⁵ ≡¹–6²⁰ ≡⁰–8⁴⁵ = – 10²⁰ ; ⌴¹ 13³⁰–7¹⁵
4	8	0.0	.	–	• 7⁵⁰ 8⁰⁵ ▽ 13⁴⁵⁻⁵⁰ ; = 6¹⁵–8¹⁵
5	7	.	.	–	= 6¹⁵–10¹⁵ , 23³⁰–24 ; ⌴ 1⁰⁰–a ⌴¹ 22³⁰–24
6	7	0.0	.	–	•⁰ 10⁴⁸⁻⁵⁵ ; = 0⁰⁰–7¹⁵ 16³⁰–24 ; ⌴¹ 0⁰⁰–2³⁰
7	7	.	.	–	= 0⁰⁰–11³⁰ , 20⁴⁵–24
8	7	.	.	–	= 0⁰⁰–12¹⁵ ; ⌒² 20¹⁵–24
9	7	.	.	–	= 2³⁰–7³⁰ ; ⌒² 0⁰⁰–a
10	6	.	.	–	= 5³⁰–12⁴⁰ ; ⌒¹ 19³⁰–24
11	7	.	.	–	= 2³⁰–5⁵⁰ ≡¹–8¹⁰ ≡⁰–8⁴⁰ = – 11³⁰ 21³⁰–24 ; ⌒² 0⁰⁰–9⁰⁰ ⌒¹ 20¹⁵–24
12	6	.	.	–	= 0⁰⁰–1⁴⁵ ≡²–7¹⁵ ≡¹–7³⁰ ≡⁰–7⁴⁰ = – 12³⁰ , 19³⁰–24 ; ⌒¹ 0⁰⁰–1⁴⁵ ⌒²–a
13	6	.	.	–	= 0⁰⁰–24 ; ⌒⁰ 19³⁰–24
14	6	.	.	–	= 0⁰⁰–2⁵⁰ ≡⁰–2⁵⁵ ≡¹–3⁴⁰ ≡⁰–7⁵⁵ = –24 ; ⌒² 0⁰⁰–9³⁰ ⌒⁰ 22²⁰–24
15	6	.	.	–	= 0⁰⁰–5⁵⁰ ≡⁰–8⁴⁰ = – 15¹⁵ ; ⌒⁰ 0⁰⁰–10³⁰
16	7	.	.	–	= 20³⁰–24
17	6	0.0	.	–	•⁰ 19⁴⁰ 20¹⁰ ; = 0⁰⁰–6⁴⁵ ≡⁰–7¹⁰ ≡¹–7³⁵ ≡⁰–7⁵⁰ = –24 ; ⌒⁰ 3⁵⁰–10²⁰
18	6	(0.0)	.	–	•⁰ 10¹⁶ 11²⁰ , 12²⁰ 13³⁰ ; = 0⁰⁰–18³⁰
19	7	.	.	–	
20	7	3.7	.	–	•⁰ 16⁴⁵–17¹⁰ •⁰–18²⁵ , 19¹⁰ 21¹⁵–24 ; = 12²⁵–24
21	7	.	.	–	•⁰ 0⁰⁰–3³⁰ ; = 0⁰⁰–10¹⁵
22	7	6.4	.	–	•⁰ 20⁴⁰–22⁴⁰ 24 ; = 6⁴⁵–8³⁰ 18³⁰–24
23	5	7.9	.	–	•⁰ 0⁰⁰⁻²⁰ ● 2⁴⁵ ●⁰–6⁴⁵ ● –7⁴⁰ •⁰–15¹⁰ 15²⁰ 16⁴⁰ ; = 0²⁰–6⁴⁵ ≡⁰–8³⁰ = –24
24	6	.	.	–	= 0⁰⁰–3⁵⁰ ≡²–9⁴⁰ ≡¹–9⁴³ ≡⁰–9⁵⁰ = – 13³⁰ , 17³⁰–24
25	7	.	.	–	= 0⁰⁰–9²⁰ , 15¹⁵–24 ; ⌴ 20³⁰–24
26	6	.	.	–	= 0⁰⁰–24 ; ⌴ 0⁰⁰–1⁵⁰ 22³⁰–24
27	6	.	.	–	= 0⁰⁰–1⁴⁵ ≡²–2⁴⁰ ≡¹–6²⁰ ≡²–9¹⁰ ≡¹–9⁴⁰ ≡⁰–10⁵⁰ = – 13³⁰ , 18³⁰–24 ; ⌴ 0⁰⁰–a
28	6	.	.	–	= 0⁰⁰–14²⁰ , 19⁴⁰–24
29	6	.	.	–	= 0⁰⁰–5⁴⁰ ≡²–10⁰⁵ ≡¹–10²⁰ ≡⁰–10⁴⁵ = –24 ; ⌒ 6⁰⁰–11²⁵ , 19⁰⁰–24
30	6	.	.	–	= 0⁰⁰–3⁰⁰ ≡¹–5²⁰ ≡²–10³⁰ ≡¹–10⁴⁰ ≡⁰–10⁵⁰ = – 14³⁰ 18²⁵–24 ; ⌒² 0⁰⁰–9³⁰ ⌒⁰ 20³⁰–24
31	6	.	.	–	= 0⁰⁰–24 ; ⌒⁰ 0⁰⁰–11³⁰ ⌒¹ 20⁰⁰–24 ; ▽ 18³⁰–19¹⁰
Σ	–	18.0	–	–	UWAGI.

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — Listopad – Novembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	86.9	85.2	86.9	86.3	1.7	15.9	9.1	9.0	16.6	1.7	98	61	95	85	0.1	7.0	0.7	2.6	0 ≡	0	0	SSW 2	SSW 3	WSW 1
2	89.3	89.9	91.2	90.1	1.6	7.6	7.3	6.0	10.4	1.6	98	99	99	99	0.2	0.1	0.1	0.1	10 ≡	10 ≡	0 ≡	WSW 2	C 0	S 1
3	91.4	92.6	92.7	92.2	6.7	8.5	7.7	7.6	8.8	6.1	97	99	98	98	0.3	0.2	0.1	0.2	10	10 ≡	10 ≡	SSE 2	SW 3	C 0
4	91.7	91.2	92.6	91.8	7.7	15.9	11.1	11.4	17.4	6.8	98	76	91	88	0.1	4.4	1.1	1.9	10 ≡	4	0	SE 1	S 3	S 2
5	91.4	89.9	89.6	90.3	6.3	15.5	10.0	10.4	17.1	6.0	98	70	88	85	0.1	5.3	1.5	2.3	0	1 ⊙	0	ESE 3	SE 4	SE 4
6	89.5	90.9	89.4	89.9	10.3	15.9	9.1	11.1	16.5	8.4	80	57	88	75	2.5	7.9	1.4	3.9	2	2 ⊙	0	SE 7	SE 7	SE 4
7	87.4	87.1	88.0	87.5	6.4	13.6	7.7	8.8	15.8	6.4	91	67	90	83	0.9	5.2	1.0	2.4	5 ⊙	9	9	SE 3	SE 4	SE 2
8	87.5	87.1	86.4	87.0	5.9	11.3	6.9	7.8	11.4	5.1	97	78	92	89	0.3	3.0	0.7	1.3	10 ≡	9 ⊙	0	SE 2	SE 4	ESE 2
9	84.8	84.2	85.7	84.9	8.1	12.7	8.7	9.6	13.2	5.6	93	70	92	85	0.8	4.4	0.9	2.0	10	2 ⊙	5	SE 3	SE 4	E 2
10	87.4	88.0	89.5	88.3	4.1	13.5	8.4	8.6	13.9	3.9	98	74	97	90	0.2	4.0	0.3	1.5	0	3	10	ESE 2	SE 2	E 4
11	90.6	90.7	92.3	91.2	8.6	7.9	6.5	7.4	9.1	6.5	90	82	90	87	1.1	1.9	1.0	1.3	10	10	10	E 5	E 7	E 8
12	95.5	98.8	101.8	98.7	3.7	3.4	3.2	3.4	6.8	3.0	85	83	93	87	1.2	1.3	0.5	1.0	10	10	10 ●	ENE 8	ENE 7	NE 4
13	104.0	104.9	105.9	104.9	0.4	-0.1	-1.9	-0.9	3.4	-1.9	82	72	80	78	1.1	1.7	1.0	1.3	10	10	10	NE 3	NE 3	NE 3
14	106.0	107.2	109.0	107.4	-3.8	-3.0	-3.3	-3.4	-1.4	-4.0	89	86	83	86	0.5	0.7	0.8	0.7	10	10	10	ENE 2	WNW 1	SSW 3
15	109.6	108.8	107.2	108.5	-2.7	0.8	-3.3	-2.1	2.1	-3.5	82	76	90	83	0.9	1.6	0.5	1.0	10	2 ⊙	0	SSW 2	SSE 3	SE 1
16	106.2	106.4	107.6	106.7	-6.5	1.1	0.3	-1.2	1.7	-6.7	97	81	96	91	0.1	1.2	0.2	0.5	2	0 ⊙	10	SE 1	S 1	SSW 1
17	108.0	108.6	109.7	108.8	0.3	0.5	0.5	0.4	0.8	0.0	96	92	84	91	0.2	0.5	1.0	0.6	10	10	10	SSW 1	ESE 2	NE 2
18	109.7	109.0	108.2	109.0	0.5	1.9	0.7	1.0	2.2	0.1	75	64	75	71	1.6	2.5	1.6	1.9	10	10	10	ESE 3	SE 4	SE 1
19	108.1	110.1	113.5	110.6	0.2	1.8	0.5	0.8	2.2	0.0	84	67	73	75	1.0	2.3	1.7	1.7	10	10	10	SE 3	NE 3	ENE 4
20	115.2	115.7	115.6	115.5	0.8	3.7	-1.8	0.2	4.4	-1.8	77	54	86	72	1.5	3.7	0.8	2.0	10	7 ⊙	0	ENE 3	SE 5	SE 2
21	114.4	112.7	109.3	112.1	-3.3	3.4	-1.7	-0.8	4.3	-3.7	97	55	85	79	0.1	3.5	0.8	1.5	3	0 ⊙	0	SE 2	S 3	S 2
22	103.2	99.8	96.1	99.7	-6.2	2.8	-1.6	-1.6	4.2	-6.3	100	62	72	78	0.0	2.4	1.5	1.5	0	0	0	S 1	SSW 2	SSW 2
23	96.0	95.0	92.3	94.4	-5.5	-0.4	1.8	-0.6	1.9	-6.4	92	88	78	86	0.3	0.7	1.6	0.9	0	10	10	SSW 3	SW 3	SW 5
24	97.1	97.8	95.7	96.9	2.2	3.1	2.7	2.7	3.6	1.5	82	71	95	83	1.3	2.2	0.4	1.3	10	10	10 ●	W 6	W 6	WSW 8
25	94.7	94.5	95.9	95.0	3.6	5.3	5.1	4.8	5.6	2.7	97	98	95	97	0.3	0.1	0.4	0.3	10 ● ●	10 ●	10 ●	WSW 7	WSW 7	WSW 7
26	97.0	98.0	97.1	97.4	5.5	6.8	6.1	6.1	7.2	4.9	97	93	92	94	0.3	0.8	0.7	0.6	10 ●	10	10	WSW 6	W 4	W 6
27	92.2	90.3	92.7	91.7	4.8	6.0	5.7	5.6	6.9	4.7	87	91	74	84	1.1	0.9	2.4	1.5	10	10	8	W 9	WSW 9	NW 7
28	91.9	88.3	83.5	87.9	4.3	7.5	7.0	6.4	7.7	4.1	95	91	84	90	0.4	0.9	1.6	1.0	10 ●	10 ●	10	WSW 3	WSW 6	WSW 8
29	78.9	80.7	92.6	84.1	3.5	0.5	-7.9	-3.0	7.6	-8.4	76	79	78	78	1.8	1.3	0.7	1.3	7	10	10 ✳	NW 7	NW 9	N 7
30	98.0	99.0	99.9	99.0	-8.4	-6.6	-7.1	-7.3	-6.0	-9.9	79	72	69	73	0.7	1.0	1.1	0.9	1	9 ✳	8	N 7	N 9	N 8
31																								
M	96.8	96.7	97.3	96.9	2.0	5.9	3.2	3.6	7.2	0.9	90	77	87	85	0.7	2.4	0.9	1.3	7.0	6.9	6.3	3.6	4.3	3.7

Grudzień – Décembre

1	101.4	101.3	101.6	101.4	-0.4	-3.3	-3.1	-4.5	-2.4	-9.5	86	65	83	78	0.4	1.7	0.8	1.0	9	0 ⊙	9	N 8	NNW 5	NW 4
2	101.0	100.7	99.8	100.5	-5.8	-2.7	-6.3	-5.3	-2.3	-6.9	95	84	89	89	0.2	0.8	0.4	0.5	10	7	4	NNW 2	N 4	NNE 4
3	97.3	95.0	96.3	96.2	-7.0	-2.7	-4.1	-4.5	-2.0	-9.4	88	82	87	86	0.4	0.9	0.6	0.6	8	10	9	N 5	NNE 3	NE 3
4	98.2	98.3	98.0	98.2	-4.9	-2.5	-3.2	-3.4	-2.1	-5.6	90	93	98	94	0.4	0.4	0.1	0.3	10	10	10 ≡	WSW 2	SW 3	SSW 1
5	94.2	92.0	93.8	93.3	0.1	1.4	2.5	1.6	2.9	-3.2	98	91	88	92	0.2	0.7	0.9	0.6	10 ✳	10	10	SW 3	W 5	WNW 4
6	96.9	99.8	101.3	99.3	1.3	1.2	-1.9	-0.3	2.7	-2.0	89	87	91	89	0.8	0.9	0.5	0.7	10	10	1	NW 5	N 3	NNE 1
7	95.7	91.4	86.4	91.2	-5.5	0.0	-3.5	-3.1	1.4	-6.2	97	84	92	91	0.1	1.0	0.4	0.5	C ≡	3 ⊙	6	SE 2	SW 2	SW 3
8	75.4	68.7	59.7	67.9	-2.5	-1.4	0.4	-0.8	0.8	-5.6	84	78	92	85	0.8	1.2	0.5	0.8	10	10	10 ●	SSW 6	SSW 8	SW 9
9	56.4	58.9	72.5	62.6	3.3	5.6	1.1	2.8	6.4	0.4	85	81	68	78	1.2	1.7	2.1	1.7	7	10 ●	7	SW 7	WSW 8	W 7
10	76.6	74.3	80.0	77.0	-3.3	-0.5	-4.1	-3.0	1.5	-4.2	95	86	75	85	0.3	0.9	1.1	0.8	7	10	0	W 1	WSW 1	NW 9
11	87.7	87.0	82.7	85.8	-8.9	-3.6	-2.7	-4.5	-2.4	-9.6	92	62	82	79	0.3	1.8	0.9	1.0	0	7 ⊙	10	SW 3	SSW 2	ESE 5
12	77.2	76.8	76.3	76.8	1.0	4.4	2.1	2.4	5.4	-2.7	85	77	91	84	1.0	1.9	0.6	1.2	10	10	0	SE 3	S 3	S 3
13	75.2	72.7	66.1	71.3	3.9	8.9	6.9	6.6	9.0	1.9	92	80	78	83	0.7	2.3	2.2	1.7	2	9	10	S 2	SW 3	SE 3
14	57.8	63.0	74.6	65.1	5.2	6.1	0.4	3.0	7.1	0.4	98	97	96	97	0.1	0.3	0.3	0.2	10 ● ≡	10 ●	10 ✳	S 1	WSW 4	W 3
15	85.6	92.7	100.3	92.9	-3.1	-4.7	-8.1	-6.0	0.7	-8.3	86	88	81	85	0.7	0.5	0.6	0.6	10	10 △	2	NNW 5	NNE 5	NE 5
16	104.2	103.9	104.6	104.2	-10.8	-5.9	-9.1	-0.7	-5.3	-11.3	87	76	85	83	0.4	0.9	0.4	0.6	0	0 ⊙	0	NE 4	E 3	E 4
17	99.8	98.2	97.2	98.4	-6.5	-3.4	-2.4	-3.7	-1.8	-9.4	86	85	95	89	0.5	0.7	0.2	0.5	10	10	10	E 3	E 1	E 1
18	97.1	98.4	100.6	98.7	-5.6	-6.1	-5.9	-5.9	-1.8	-6.5	92	94	89	92	0.3	0.2	0.4	0.3	10	10 ✳	10	NNW 3	N 3	N 1
19	102.5	104.3	108.0	104.9	-5.4	-3.5	-3.5	-4.0	-2.8	-6.4	92	76	78	82	0.3	1.1	1.0	0.8	10	10	10	C 0	E 1	ESE 2
20	109.8	110.1	110.7	110.2	-2.5	0.0	1.1	-0.1	1.5	-3.6	89	84	87	87	0.6	0.9	0.9	0.8	10	10	10	SW 2	SW 3	WSW 4
21	107.8	106.7	105.8	106.8	-2.8	1.3	-1.2	-1.0	2.0	-3.5	91	76	84	84	0.5	1.6	0.9	1.0	0	0 ⊙	0	SW 4	SW 5	SW 6
22	106.0	105.7	104.5	105.4	-2.1	0.0	-2.8	-1.9	0.4	-3.2	87	84	88	86	0.7	1.0	0.6	0.8	6	10	0	SW 3	SW 5	SSW 3
23	101.6	98.8	96.7	99.0	-6.1	-1.6	-4.3	-4.1	-0.8	-6.1	94	78	79	84	0.2	1.2	0.9	0.8	0	9	0	SSW 2	SSE 2	SW 3
24	96.1	95.6	97.0	96.2	-9.4	-3.0	-7.4	-6.8	-1.9	-10.7	95	81	96	91	0.2	0.9	0.1	0.4	0	1 ⊙	0	S 3	SW 3	SW 3
25	97.9	97.4	97.0	97.4	-8.1	-1.3	-2.3	-3.5	1.0	-9.2	92	76	89	86	0.2	1.3	0.6	0.7	0	1	0	SW 2	S 2	SW 3
26	99.6	100.8	102.9	101.1	-4.4	-1.0	-3.0	-2.8	0.1	-5.7	96	96	99	97	0.2	0.3	0.0	0.2	10	10	0	SW 3	SW 3	SW 3
27	103.0	102.5	101.8	102.4	-0.8	0.5	-1.1	-0.6	1.5	-4.6	87	92	83	87	0.7	0.5	1.0	0.7	10	10	10	SW 1	SW 4	SW 3
28	97.6	94.4	90.6	94.2	-3.7	0.3	-3.1	-2.4	1.6	-4.5	90	79	97	89	0.5	1.3	0.1	0.6	2	0	10 ≡	SW 3	SW 2	SW 5
29	86.8	86.8	85.0	86.2	-2.6	0.9	0.1	-0.4	1.3	-3.7	91	85	80	85	0.5	1.0	1.2	0.9	10	10	5	SW 4	WSW 6	WSW 6
30	80.4	79.0	76.7	78.7	1.7	2.7	2.7	2.4	3.3	-1.5	74	77	70	74	1.8	1.7	2.2	1.9	10	10 ●	8	SW 6	SW 7	SW 10
31	77.5	79.4	80.0	79.0	0.9	1.7	-0.3	0.5	3.4	-0.6	90	76	78	81	0.6	1.6	1.3	1.2	9	7	9	WSW 4	WSW 5	SW 3
M	91.8	91.4	91.9	91.7	-3.3	-0.4	-2.1	-2.0	0.9	-5.2	90	82	86	86	0.5	1.1	0.8	0.8	6.8	7.5	5.8	3.4	3.7	4.0

Sandomierz — $H_s = 202$ m — $H_b = 200{,}3$ m — $h_w = 21$ m — Listopad – Novembre 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	.	-	= 0⁰⁰–2⁵⁰ ≡²–9²⁵ ≡¹–9⁴⁰ ≡⁰–9⁴⁵ =–12⁴⁰ 18³⁰–24; ⌒¹ 0⁰⁰–10³⁰ ⌒⁰ 18⁵⁰–24
2	1	0.0	.	-	= 0⁰⁰–2⁵⁰ ≡⁰–3³⁰ ≡¹–6¹⁵ ≡²–12⁵⁰ ≡¹–14⁰⁵ ≡⁰–15²⁰ =–17¹⁰ ≡⁰–19²⁰ ≡¹–19⁵⁰ ≡²–23³⁰ ≡¹–24; ⌒¹ 0⁰⁰–5⁰⁰ ⌒²–14⁰⁰
3	2	.	.	-	•⁰ 0⁴⁰ 1¹⁰; ≡¹ 0⁰⁰–5⁰ ≡⁰ 0⁵⁵ =–6⁴⁰ ≡⁰–7³⁵ ≡¹–7⁵⁰ ≡²–11³⁰ ≡¹–14⁴⁰ ≡²–22¹⁰ ≡¹–22³⁰ ≡⁰–22⁴⁵ =–24
4	6	.	.	-	= 0⁰⁰–5⁴⁰ ≡¹–7¹⁵ ≡²–9³⁰ ≡¹–9³⁵ ≡⁰–9⁴⁰ =–12³⁵, 20¹⁵–24; ⌒² 18⁴⁰–24
5	7	.	.	-	= 0⁰⁰–12¹⁵; ⌒² 0⁰⁰–11³⁰ ⌒¹ 20¹⁵–24
6	7	.	.	-	⌒¹ 0⁰⁰–11³⁰
7	7	.	.	-	= 6¹⁵–8³⁰ 20³⁰–24; ⌒⁰ 4⁰⁰–8³⁰ ⌒¹ 19³⁰–24
8	6	.	.	-	= 0⁰⁰–4⁴⁵ ≡²–6¹⁵ ≡¹–6³⁰ ≡⁰–7¹⁵ =–24; ⌒¹ 0⁰⁰–4⁴⁵, 20¹⁵–24
9	6	.	.	-	= 0⁰⁰–14⁰⁰, 20³⁰–24; ⌒¹ 0⁰⁰–9¹⁵
10	6	.	.	-	= 0⁰⁰–6⁴⁰ ≡⁰–6⁵⁰ ≡²–7³⁰ ≡¹–8¹⁵ ≡⁰–8⁴⁵ =–13¹⁰, 18³⁵–24; ⌒⁰ 1⁰⁰–6⁰⁰ ⌒²–11²⁰ ⌒¹–12⁵⁰, 18⁵⁰–24
11	7	.	.	-	= 0⁰⁰–7⁴⁵ 18³⁰–24; ⌒⁰ 0⁰⁰–10³⁰
12	7	0.0	.	-	• 17³⁸–18¹⁵, 19⁴⁰–24; = 0⁰⁰–6¹⁵, 19³⁰–24
13	7	.	.	-	•⁰ 0⁰⁰ 2³⁰, 3²⁰ 5³⁵; = 0⁰⁰–6¹⁵
14	7	.	.	-	
15	7	.	.	-	= 6¹⁵–9³⁰; ⌴⁰ 20¹⁰–24
16	6	.	.	-	= 0⁴⁰–24; ⌴¹ 0⁰⁰–10³⁰
17	5	0.0	.	-	• 10³⁰–12²⁰, = 0⁰⁰–24
18	8	.	.	-	= 0⁰⁰–6¹⁵
19	8	.	.	-	
20	8	.	.	-	⌴⁰ 22¹⁰–24
21	7	.	.	-	= 5¹⁵–12¹⁵; ⌴¹ 0⁰⁰–11³⁰
22	6	.	.	-	= 3³⁰–14²⁰; ⌴¹ 1⁰⁰–11⁴⁰, 21³⁰–24
23	6	.	.	-	= 7¹⁵–24; ⌴¹ 0⁰⁰–12⁰⁰
24	7	0.3	.	-	* 15⁴⁰–17³⁵ •⁰ 18²⁰–19¹⁵, 24; = 0⁰⁰–6¹⁰
25	6	0.6	.	-	•⁰ 0⁰⁰ 3³⁰ ••⁰–8¹² •⁰–10⁵⁰ 12¹⁵–17⁴⁵ 18¹⁵–19⁴⁰, 24; = 4³⁰–24
26	6	0.3	.	-	•⁰ 0⁰⁰–2⁰ 6¹⁵ 7⁴⁵ 10¹⁰ 12¹⁰ 14⁵⁵–15³⁰; = 0⁰⁰–24
27	6	0.8	.	-	•⁰ 7⁴⁵–8⁵⁰ •⁰ 9³⁵ 11⁴⁸, 22⁵⁰–24; = 0⁰⁰–24
28	6	5.3	.	-	•⁰ 0⁰⁰–2⁰ •⁰ 4⁴⁰–7⁵⁰ •¹–8³⁰ •⁰–13³⁰, 19⁴⁵–20⁴⁵–24; = 0⁰⁰–24
29	8	0.0	.	-	•⁰ 0⁰⁰–1³⁶ 4⁴⁰–5⁵⁰ ⚹ ▽ 8⁴⁰–5¹ *⁰ 13⁰⁵–18¹⁵, 19²⁵–24; = 0⁰⁰–6⁵⁰, 12⁰⁵–18²⁵
30	7	0.9	1	-	*⁰ 0⁰⁰–2⁰, 7³⁰–9¹⁰ ⚹ ▽⁰ 10²⁰–11¹⁵, 11²⁰–12³⁵, 12⁴⁰–13²⁰ ⚹ ▽ 13³⁰–45
31					
Σ	—	8.2	—	-	UWAGI

Grudzień – Décembre

1	8	.	1	-	
2	7	.	1	-	= 9³⁰–10⁴⁰
3	8	.	1	-	◡ 22⁴⁰–24
4	6	0.5	1	-	•⁰ 9³⁵–10⁴⁸ (marznąca), 12⁴⁰–16⁴⁵ (marznąca) *⁰ 23¹⁵–24; ≡⁰ 17⁵⁰–20²⁰ ≡¹–22⁴⁵ =⁰–24; ⊠ 13⁴⁵–24, ◡ 0⁰⁰–2¹⁵
5	5	2.9	2	-	*⁰ 0⁰⁰–3⁰ 3⁴⁰ 4⁸⁰–8¹⁵ *¹–9⁴⁰ *⁰–10²⁰; ≡⁰ 0⁰⁰–5⁵⁰; ⊠ 0⁰⁰–5⁵⁰
6	8	.	pł.	-	•⁰ 2⁴⁰–4¹⁰ 5⁴⁵–6¹⁵; = 0⁰⁰–5¹⁵
7	6	.	pł.	-	≡⁰ 2⁵⁰–3³⁰ ≡¹–6²⁰ ≡⁰–7³⁰ =–15⁵⁰, 23⁴⁵–24;
8	7	2.4	pł.	-	*⁰ 7²⁰–32 7⁴⁰ 8⁰⁸–²² 9²⁹–11²⁰ 15¹⁵, 16²⁰–18⁴⁰ △–19³⁵ •⁰–24; = 0⁰⁰–8²⁵ 16³⁵–24; ⊠ 19⁵⁰–24 ◡ 0¹⁵–3²⁰
9	6	0.3	pł.	-	•⁰ 0⁰⁰–1¹⁵ ⚹ ▽ 8⁵⁵–⁴⁸ 9¹²–¹⁶ 10⁵⁰–11¹², 11³⁰–12¹⁵, 12²⁸–13¹⁵ ⚹ 19²⁵–³¹ ⚹ ▽ 21⁰⁵–²⁰; = 0⁰⁰–1¹⁵; ⊠ 0⁰⁰–¹⁵
10	6	0.1	.	-	*⁰ 13³⁵–14²⁵, 15⁵⁰–16²¹; = 7¹⁰–20⁰⁵
11	7	.	1	-	= 9⁰⁵–11³⁵, 15⁴⁰–24
12	7	.	1	-	= 0⁰⁰–12¹⁵, 18¹⁵–24
13	6	3.8	.	-	•⁰ 21³⁰–23³⁰ •¹–24; = 0⁰⁰–13¹⁵ 19³⁰–24
14	5	10.7	.	-	•¹ 0⁰⁰–1³⁰ •⁰–4⁴⁰ 5¹⁵–9²⁰ •¹–9³⁵ •⁰–13²⁵ 15³⁰–18⁰⁵ ⚹–19¹⁵ •⁰–20¹⁰ *⁰–21⁰⁵ ⚹⁰–21¹⁵ •⁰–21⁵⁰ ⚹⁰–22¹⁰ •⁰–22¹⁷ *⁰–22⁴⁸,
15	7	0.0	pł.	-	△ 11⁴⁵–13⁴⁰ *⁰–15¹⁵; = 0⁰⁰–30 [14.XII: = 0⁰⁰–6⁴⁵ ≡⁰–7²⁰ =–24
16	6	.	1	-	
17	7	.	1	-	
18	6	0.0	1	-	*⁰ 9³⁰ 10¹⁵ 12¹⁵–16³⁰, = 7¹⁵–24
19	7	.	1	-	= 0⁰⁰–12¹⁵, 17³⁰–24
20	6	.	pł.	-	= 0⁰⁰–24
21	6	0.0	pł.	-	△ 23⁰¹–¹⁵; = 0⁰⁰–24
22	6	.	pł.	-	= 0⁰⁰–24
23	6	.	.	-	= 0⁰⁰–24; ⌴⁰ 1³⁰–12³⁰
24	6	.	.	-	= 0⁰⁰–7⁴⁰ ≡⁰–8⁴⁰ =–24; ⌴⁰ 3⁰⁰–24
25	6	.	.	-	= 0⁰⁰–24; ⌴¹ 0⁰⁰–12³⁰
26	6	.	.	-	= 0⁰⁰–24; ⌴¹ 4³⁰–13³⁰
27	6	.	.	-	= 0⁰⁰–24
28	6	0.0	.	-	= 0⁰⁰–7⁵⁰ ≡¹–8⁴⁰ ≡⁰–9⁴⁰ =–17²⁰ ≡⁰–21⁴⁵ =–24
29	6	0.0	.	-	*⁰ 6⁴⁰–8⁴⁵; = 0⁰⁰–2³⁰, 7³⁰–24
30	6	0.0	1	-	*⁰ 9¹⁰–⁴⁰ •⁰–10³⁰ ⚹⁰–11¹⁵ •⁰–13¹⁵, 23⁵⁰–24; = 10¹⁵–15¹⁰
31	7	0.0	.	-	•⁰ 0⁰⁰–2⁰ *⁰ 23¹⁵–23⁴⁰
Σ	—	20.7	—	-	UWAGI

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$ **Styczeń – Janvier 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	92.3	91.6	90.6	91.5	0.2	2.3	1.1	1.2	2.7	0.1	94	82	94	90	0.4	1.5	0.4	0.7	10 ✳	10	10	C 0	SW 3	C 0
2	88.2	89.4	93.9	90.5	0.7	4.8	2.6	2.7	7.4	-1.1	92	76	84	84	0.5	2.0	1.2	1.2	2	8	10	C 0	WSW 1	SW 2
3	97.7	99.4	99.8	99.0	1.4	2.4	1.4	1.6	2.8	1.4	96	82	83	87	0.3	1.3	1.1	0.9	10 ●	10	10	WSW 1	SW 1	SW 2
4	100.2	102.4	102.8	101.8	1.4	1.9	0.3	1.0	2.4	0.3	81	80	88	83	1.3	1.4	0.7	1.1	5	10	5	S 2	SW 3	SSW 2
5	102.8	101.0	99.0	100.9	1.0	2.8	2.2	2.0	3.1	0.1	85	81	87	84	1.0	1.5	1.0	1.2	10	10	10 ●	S 2	SW 3	SW 2
6	96.3	92.6	92.9	93.9	3.2	7.5	6.5	6.4	8.4	2.1	84	83	78	82	1.4	1.8	2.2	1.8	9	9	10	S 4	SW 4	SW 2
7	98.5	102.6	106.6	102.6	4.5	5.7	4.7	4.9	6.7	2.4	68	68	76	71	2.7	3.0	2.0	2.6	8	8	9	WNW 12	NW 12	NW 8
8	108.0	105.7	105.9	106.5	3.2	6.0	4.7	4.8	5.2	3.2	79	71	76	75	1.6	2.7	2.0	2.1	10	10	10	W 2	SW 3	SW 2
9	103.7	101.3	97.7	100.9	2.2	5.1	1.9	2.8	6.7	1.1	87	83	78	83	1.0	1.5	1.5	1.3	10 ●	9	0	S 2	S 3	SSE 2
10	93.4	91.7	93.2	92.8	1.3	4.1	1.6	2.2	4.3	1.1	79	67	89	78	1.4	2.7	0.8	1.6	5	10	9	SSE 1	E 2	W 2
11	94.0	96.1	98.6	96.2	1.4	1.1	1.2	1.2	2.5	0.7	72	87	81	80	1.9	0.9	1.3	1.4	9	9 ✳	10	W 2	NW 4	NW 4
12	96.2	90.7	84.4	90.4	-1.8	1.7	0.7	0.3	2.0	-1.9	81	69	85	78	1.0	2.1	1.0	1.4	5	9	10	NW 2	WSW 4	S 4
13	81.6	83.1	83.7	83.5	-0.3	0.5	-4.5	-2.2	1.3	-4.5	92	90	91	91	0.5	0.6	0.4	0.5	10 ✳	10	7	S 2	S 2	SSE 1
14	90.0	93.5	97.6	93.7	-2.6	-0.1	-2.5	-1.9	0.3	-6.4	93	84	72	83	0.3	1.0	1.5	0.9	10	10	10	SSE 1	NNE 2	E 4
15	97.6	97.5	98.4	97.8	-4.6	-4.4	-4.9	-4.7	-1.9	-4.9	84	86	81	84	0.7	0.6	0.8	0.7	10	10 ✳	10	NE 4	NE 6	NE 4
16	103.2	105.3	108.3	105.6	-7.4	-8.6	-11.3	-9.6	-4.6	-11.3	79	74	86	80	0.7	0.8	0.4	0.6	10	3	0	N 5	N 5	N 1
17	108.9	109.5	109.4	109.3	-13.4	-9.8	-11.8	-12.2	-8.0	-15.7	82	75	86	81	0.3	0.7	0.4	0.5	0	0 ⊙	10	C 0	NNE 3	C 0
18	108.2	107.3	106.9	107.5	-7.3	-5.2	-10.1	-8.2	-3.2	-11.8	82	80	97	86	0.6	0.8	0.1	0.5	6	8	10 ≡	E 1	NE 2	C 0
19	106.1	106.4	108.5	107.0	-10.9	-3.2	-1.6	-4.5	-1.4	-13.1	94	95	78	89	0.2	0.2	1.2	0.5	9 ≡	9	10	SE 1	SE 1	NE 1
20	108.3	107.6	105.3	107.1	-2.3	-2.4	-5.9	-4.1	-0.7	-5.9	74	74	79	76	1.4	1.3	0.8	1.2	10	10	0	NNW 1	S 2	S 2
21	104.1	104.0	104.5	104.2	-6.9	-2.7	-7.0	-5.9	-2.3	-7.4	83	75	74	77	0.6	1.3	0.9	0.9	5	0 ⊙	0	SE 2	S 4	SSW 3
22	103.8	101.9	99.3	101.7	-7.5	-2.5	-7.4	-6.2	-1.5	-8.5	82	67	73	74	0.6	1.7	0.9	1.1	3	6 ⊙	0	S 3	SSW 3	SW 3
23	99.0	97.3	94.6	97.0	-9.9	-2.8	-8.1	-7.2	-1.5	-9.9	78	64	84	75	0.6	1.8	0.5	1.0	0	4 ⊙	0	S 3	SSE 3	SE 1
24	89.2	86.6	87.0	87.6	-5.0	0.7	0.3	-0.9	2.3	-8.7	83	67	84	78	0.7	2.1	0.9	1.2	10	10	10	SE 1	SE 2	SSW 1
25	87.3	88.5	91.4	89.1	-3.7	0.9	-1.1	-1.2	1.7	-4.4	87	71	87	82	0.6	1.9	0.8	1.1	5	10	10	S 1	SE 2	SE 1
26	96.6	97.6	97.7	97.3	-1.4	3.5	-1.2	-0.1	5.0	-1.6	88	66	91	82	0.6	2.6	0.5	1.2	10	0 ⊙	0	SE 1	S 2	S 1
27	94.9	96.2	98.9	96.7	1.1	2.5	2.5	2.2	4.2	-2.0	85	80	86	84	1.0	1.4	1.0	1.1	10	10	10 ●	SW 4	SSE 4	W 1
28	97.2	101.0	106.9	101.7	0.7	1.7	0.6	0.9	3.0	0.4	90	81	94	88	0.6	1.3	0.4	0.8	8	10 ●	10 ✳	SSE 2	W 2	NW 3
29	110.1	108.3	106.2	108.2	-0.6	4.1	0.3	1.0	5.1	-1.0	90	59	82	77	0.6	3.3	1.1	1.7	9	5 ⊙	10	NW 1	S 3	SSE 2
30	102.7	100.6	99.9	101.1	-1.5	4.7	0.3	1.0	5.3	-1.6	84	59	84	76	0.9	3.5	0.9	1.8	3	8 ⊙	6	SSE 2	SSE 3	SE 2
31	100.6	101.3	100.8	100.9	0.2	1.7	2.3	1.6	2.7	0.1	92	90	84	82	0.5	0.6	1.2	0.8	10	10	10	SE 1	SE 1	S 2
M	98.7	98.6	99.1	98.8	-2.1	0.8	-1.4	-1.0	2.0	-3.5	85	76	84	82	0.9	1.6	1.0	1.2	7.5	7.9	7.4	2.1	3.1	2.2

Luty – Février

1	97.9	97.7	98.8	98.1	2.3	3.0	1.9	2.3	4.0	1.4	80	90	94	88	1.4	0.8	0.4	0.9	10	10 ●	10 ●	S 3	SSW 3	S 3
2	101.5	103.1	104.4	103.0	3.3	6.1	5.0	4.8	6.8	1.9	91	82	81	85	0.6	1.7	1.6	1.3	10 ●	10	10	S 2	SW 3	SW 4
3	102.6	101.0	102.3	102.0	3.3	7.7	1.7	3.6	8.4	1.7	85	67	89	80	1.2	2.5	0.8	1.8	8	9	7	SSW 4	SW 2	SSW 2
4	102.2	101.7	101.6	101.8	1.0	5.4	1.4	2.3	6.8	0.4	96	80	91	89	0.3	1.8	0.7	0.9	10 ≡	8	0	E 3	SW 4	SW 2
5	100.8	100.2	99.3	100.2	0.6	6.0	2.0	2.6	7.7	-0.6	94	77	87	86	0.4	2.2	0.9	1.2	0	0	7	SSE 2	SSE 3	SW 3
6	99.9	99.1	99.6	99.2	3.1	7.9	5.2	5.8	9.0	2.0	83	68	81	77	1.5	3.3	1.6	2.1	4	6	8	SW 3	SSW 8	SW 3
7	94.6	96.9	97.2	96.2	4.3	6.9	2.6	4.1	8.8	2.3	90	82	91	88	0.8	1.7	0.7	1.1	10 ●	7	2	WSW 2	WSW 2	SW 1
8	93.3	88.9	86.0	89.4	1.9	6.9	5.2	4.8	8.8	0.4	89	77	84	83	0.8	2.3	1.4	1.5	10	10	10	SSE 2	SW 2	SW 3
9	82.6	82.0	85.0	83.2	5.6	8.7	6.1	6.6	9.5	5.0	86	77	86	83	1.3	2.5	1.3	1.7	10	9 ●	7	SW 2	WSW 4	C 0
10	86.6	85.9	85.7	86.1	1.0	7.6	4.3	4.3	8.1	0.9	92	73	84	83	0.5	2.8	1.4	1.6	1	9	6	SSE 1	SW 3	SW 1
11	86.6	90.1	92.6	89.8	4.0	6.5	3.4	4.3	8.3	2.3	83	68	90	80	1.3	3.1	0.8	1.7	8	9 ●	9	SW 2	NW 5	NW 1
12	91.3	87.4	84.0	87.6	0.4	7.7	4.7	4.4	9.4	0.3	92	61	71	75	0.5	4.1	2.4	2.3	4	6 ⊙	10	SSW 1	S 4	SSE 2
13	81.9	78.1	69.9	76.6	4.0	9.9	7.5	7.2	10.8	4.0	83	49	65	66	1.3	6.2	3.7	3.7	9	8	10	S 2	SW 8	SSW 9
14	68.5	67.2	69.3	68.3	5.8	10.0	4.9	6.4	11.7	4.9	79	57	79	72	2.0	5.3	1.8	3.0	10	9	8	SSW 4	SW 4	SSW 2
15	70.3	64.6	63.9	66.3	2.2	8.6	6.9	6.2	9.8	0.5	78	58	80	72	1.6	4.8	2.0	2.8	2	10	10	S 3	SW 4	SSE 4
16	72.3	74.8	79.3	75.5	4.4	8.0	1.8	4.0	10.2	1.6	71	55	80	69	2.5	4.8	1.3	2.9	9	8	3	SW 5	SW 5	C 0
17	84.1	84.7	86.1	85.0	0.2	7.7	2.7	3.5	8.3	-0.8	80	55	82	72	1.2	4.8	1.3	2.4	3	9	0	SW 1	SSW 5	S 2
18	83.3	77.6	72.1	77.7	-1.5	8.7	7.6	5.6	10.2	-1.7	98	55	90	81	0.1	5.0	1.0	2.0	9	10	10 ●	C 0	SE 4	SSE 1
19	79.3	86.6	91.3	85.7	2.0	4.9	1.3	2.4	7.6	1.3	87	58	81	75	0.9	3.7	1.3	2.0	10 ●	5	0	W 12	NW 9	SW 2
20	92.1	89.8	86.7	89.5	0.2	6.9	5.4	4.5	7.8	-0.1	82	54	68	68	1.1	4.5	2.9	2.8	4	9	10	S 1	S 3	S 3
21	84.6	85.8	90.8	87.1	1.7	9.0	1.4	3.4	9.5	1.3	83	54	89	75	1.1	5.3	0.8	2.4	3	6 ⊙	10 ≡	SSW 1	SSW 3	NW 6
22	93.6	93.6	92.1	93.1	0.5	1.8	-1.5	-0.2	3.3	-1.7	86	80	93	86	0.8	1.5	0.4	0.9	10	9 ✳	0	NW 2	N 5	C 0
23	92.2	91.9	90.8	91.5	-3.8	5.0	-1.1	-0.2	6.5	-5.8	92	61	91	81	0.4	3.4	0.4	1.4	2	2	0	SSE 2	SSE 2	C 0
24	82.7	77.9	78.5	79.7	-1.9	0.8	0.7	0.1	1.3	-5.2	94	85	96	92	0.3	1.0	0.2	0.5	10 ✳	10 ✳	10 ≡ ✳	C 0	SSE 2	C 0
25	83.6	83.9	80.3	82.6	-0.5	2.5	1.0	1.0	3.1	-0.9	94	68	88	83	0.4	2.3	0.8	1.2	5	9	10 ✳	NW 1	NW 2	SE 2
26	89.3	93.2	96.7	93.1	-0.8	-0.6	-1.1	-0.9	1.1	-1.1	91	87	83	88	0.5	0.7	0.9	0.7	9	8	10	NNW 3	NW 4	C 0
27	98.5	99.7	101.8	100.0	-10.9	1.7	-6.5	-5.6	2.3	-11.1	87	61	91	80	0.4	2.7	0.3	1.1	2	3 ⊙	0	C 0	NNW 2	C 0
28	104.9	106.5	108.4	106.6	-7.8	-1.4	-2.7	-5.6	-1.2	-8.5	90	70	79	78	0.3	1.7	1.2	1.1	8	10 ✳	10 ✳	C 0	NNW 2	NNE 1
29																								
30																								
31																								
M	89.2	88.7	88.9	88.9	1.0	5.9	2.6	3.0	7.1	0.0	87	68	84	80	0.9	3.1	1.2	1.7	6.8	7.8	6.7	2.3	3.8	2.0

Racibórz

$H_s = 189\ m$ $H_b = 196{,}1\ m$ $h_w = 15\ m$

Styczeń–Janvier 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.3	8	–	$*^{1}\ 15^{15}-8^{16}$, $=5^{30}-9^{35}$, $20^{30}-24$
2	8	0.0	4	–	$=0^{00}-9^{40}$
3	7	0.0	1	–	$\bullet^{0}\ 6^{16}-9^{10}$, $=6^{15}-12^{30}$
4	8	.	p2.	–	
5	7	3.8	p2.	–	$\bullet^{0}\ 15^{20}-n$
6	8	5.1	.	–	$\bullet^{1}\ 13^{08}-15^{15}$
7	9	0.0	.	–	$\bullet\ \triangledown\ 6^{18-35}$, $7^{10}-8^{04}$
8	7	0.0	.	–	
9	7	0.0	.	–	$\bullet^{0}\ 6^{35}-8^{08}$, $=8^{10}-13^{20}$
10	6	0.8	.	–	$\bullet^{0}\ 11^{20}-12^{06}$, $15^{17}-19^{08}$, $=9^{35}-19^{30}$, $\sqcup^{0}\ n$
11	6	0.5	.	–	$\triangle\ 8^{16-28}$, $\bullet\ 9^{42}-10^{35}$, $11^{14}-16^{26}$
12	7	0.8	p2.	–	$*^{0}\ 13^{05}-14^{15}$, $=14^{40}-20^{25}$
13	6	3.0	3	–	$*^{1}\ n-8^{35}$ $*^{0}-9^{40}$ $*^{1}-11^{42}$ $*^{0}-12^{08}$, $=n-18^{15}$
14	7	.	6	–	$*^{0}\ n$, $=n-12^{15}$
15	6	0.0	5	–	$*^{0}\ 8^{37}-17^{11}$, $=8^{40}-n$
16	7	.	4	–	$*^{0}\ n$
17	7	.	4	–	$=7^{35}-13^{25}$
18	6	0.0	4	–	$=6^{40}-17^{30}$ $\equiv^{1}-24$, $V^{1}\ 18^{00}-24$
19	5	.	3	–	$\equiv^{1}\ 0^{00}-10^{25}$ $\equiv^{0}-11^{52}$ $=-14^{55}$ $\equiv^{0}-19^{58}$ $=-24$, $V^{1}\ 0^{00}-na$
20	6	.	3	–	$\rightarrow\ 0^{00}-6^{35}$, $8^{30}-13^{40}$
21	7	.	3	–	$=7^{35}-11^{28}$, $\frown\ 21^{06}-22^{00}$
22	7	.	3	–	
23	7	.	3	–	$=16^{15}-24$
24	6	.	3	–	$=0^{00}-24$
25	6	.	2	–	$=0^{00}-24$, $\oplus^{0}\ 9^{40}-11^{17}$
26	6	0.0	2	–	$*^{0}\ 7^{50}-8^{08}$, $=0^{00}-11^{45}$ $\infty-15^{50}$ $=-24$
27	6	0.4	2	–	$*^{0}\ 6^{04}-8^{08}$ $\bullet^{0}\ 20^{06}-22^{10}$, $=7^{35}-24$
28	6	5.8	p2.	–	$\bullet^{0}\ 7^{45}-8^{02}$ $*^{1}-8^{08}$ $*^{2}-8^{50}$ $*^{1}-9^{25}$ $\bullet^{0}-10^{05}$ $\bullet^{0}-14^{10}$ $*^{0}\ 17^{05}-24$, $=0^{00}-13^{40}$, $\sqcup^{0}\ n$
29	8	.	2	–	$*^{0}\ 0^{00}-25$
30	8	4.0	p2.	–	$*^{0}\ 21^{02}-24$, $=22^{40}-24$
31	5	0.9	p2.	–	$*^{0}\ 0^{00}-4^{20}$ $\bullet^{0}\ 7^{47}-11^{52}$, $=0^{00}-21^{45}$
Σ	–	25.4	–	–	UWAGI

Luty – Février

1	6	11.6	p2.	–	$\bullet^{0}\ 3^{10}-6^{18}$ $\bullet^{1}\ 7^{35}-12^{20}$ $\bullet^{0}-24$
2	7	0.0	.	–	$\bullet^{0}\ 0^{00}-10^{5}$, $6^{40}-7^{12}$, $11^{40}-12^{15}$
3	7	.	.	–	$=22^{43}-24$
4	7	.	.	–	$=0^{00}-1^{40}$ $\equiv^{1}-4^{37}$ $\equiv^{0}-7^{50}$ $=-11^{40}$
5	7	.	.	–	$=7^{08}-11^{36}$, $\sqcup^{1}\ n-10^{25}$
6	8	1.6	.	–	
7	7	2.8	.	–	$\bullet^{0}\ 1^{37}-6^{42}$ $\bullet^{1}-7^{31}$ $\bullet^{0}-9^{25}$, $=16^{40}-18^{30}$, $20^{35}-24$
8	7	1.1	.	–	$\bullet^{0}\ 14^{07}-15^{39}$ $16^{40}-17^{36}$ $19^{43}-20^{30}$, $21^{40}-22^{25}$, $=0^{00}-8^{25}$, $\sqcup^{0}\ n-8^{25}$
9	8	1.2	.	–	$\bullet^{0}\ 12^{06}-13^{15}$ $\bullet\ \triangledown\ 15^{14}-16^{08}$
10	7	0.4	.	–	$\bullet^{0}\ 13^{25}-14^{40}$, $15^{35}-16^{40}$, $=5^{08}-9^{40}$, $\sqcup^{1}\ n-a$, $\cup\ 20^{30-50}$, $21^{40}-22^{35}$
11	7	2.5	.	–	$\bullet^{0}\ 0^{40}-2^{08}$, $8^{44}-9^{46}$, 12^{26-49} $\bullet\ \triangledown\ 13^{05-27}$, $16^{45}-18^{10}$, $19^{31}-20^{15}$
12	8	.	.	–	$=6^{15}-10^{20}$, $\sqcup^{0}\ n-a$, $\bigtriangledown\ 23^{40}-24$
13	8	.	.	–	$\bigtriangledown\ 0^{00}-n$
14	7	0.4	.	–	$\bullet\ \triangledown\ 16^{43}-17^{11}$, $\cup\ 20^{25}-21^{15}$
15	7	.	.	–	$\sqcup^{0}\ n-a$, $\bigtriangledown\ 23^{30}-24$
16	8	0.0	.	–	$\bullet\ \triangledown\ 10^{08-20}$, 16^{32-38}, $\bigtriangledown\ 0^{00}-1^{29}$
17	8	.	.	–	$\sqcup^{0}\ n$, a
18	6	12.5	.	–	$\bullet^{0}\ 17^{40}-19^{28}$ $20^{45}-21^{39}$ $\bullet^{1}-22^{22}$, $=6^{20}-12^{15}$ $\infty-15^{20}$, $16^{35}-17^{20}$, $\sqcup^{1}\ n-a$
19	8	0.4	.	–	$\bullet^{1}\ 2^{26}-4^{10}$ $\bullet^{0}-8^{25}$, $\gg\ 5^{15}-7^{45}$
20	7	.	.	–	$\sqcup^{0}\ n-a$
21	7	1.4	.	–	$\bullet\ \triangledown\ 16^{40-50}$ $\bullet^{0}\ 18^{47}-20^{39}$ $\bullet^{0}-21^{50}$ $23^{05}-24$, $=7^{20}-9^{35}$
22	6	0.1	.	–	$\bullet^{0}\ 0^{00}-3^{45}$ $*^{0}-4^{40}$ $\bullet^{0}-6^{14}$ $\bullet^{0}\ 11^{25-42}$, 12^{10-16}, $12^{42}-13^{05}$ $\triangle\ -13^{18}$
23	8	0.0	.	–	$=0^{00}-9^{40}$, $\sqcup^{2}\ n-a$ $\sqcup^{1}\ na-24$
24	6	4.4	0	–	$*^{0}\ 6^{35}-13^{15}$, $14^{18}-17^{42}$ $\bullet^{0}-19^{35}$ $\bullet^{0}\ 20^{50}-21^{39}$ $*^{0}\ 22^{48}-24$, $=2^{40}-24$, $\sqcup^{2}\ 0^{00}-6^{40}$
25	7	11.3	2	–	$*^{0}\ 0^{00}-1^{10}$, $\bullet^{0}-2^{41}$ $*^{0}\ 18^{35}-24$, $=0^{00}-12^{30}$, $17^{15}-24$
26	6	0.0	11	–	$*^{0}\ 0^{00}-4^{40}$, $8^{46}-9^{32}$, $10^{50}-11^{37}$, $=0^{00}-13^{25}$
27	6	.	8	–	$=4^{29}-24$
28	5	1.2	6	–	$*^{0}\ 11^{37}-14^{16}$, $15^{35}-24$, $=0^{00}-24$
29					
30					
31					
Σ	–	52.9	–	–	UWAGI

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$ **Marzec – Mars 1957**

DNI	CIŚNIENIE P=900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	110.7	110.3	109.7	110.3	−5.0	−2.6	−1.8	−2.8	−1.7	−6.1	90	85	79	85	0.4	0.8	1.1	0.8	10	9 ✳	10 ✳	NNE 2	NW 3	NNW 3
2	108.4	107.1	105.1	106.9	−2.4	−0.4	−1.9	−1.6	0.2	−2.4	68	57	67	64	1.6	2.5	1.8	2.0	9 ✳	9	10	N 3	N 3	N 2
3	100.9	98.8	97.3	98.9	−2.2	0.7	−2.8	−1.8	1.0	−3.0	79	69	80	76	1.1	2.0	1.0	1.4	9	9	0	NNW 3	[illegible]	C 0
4	93.7	90.8	88.8	91.1	−5.2	4.1	2.9	1.2	4.3	−7.2	90	63	62	72	0.4	3.1	2.8	2.1	6	7	10	SE 2	SE 3	S 2
5	90.2	91.1	91.6	91.0	1.4	3.2	−1.1	0.6	4.4	−1.2	85	66	91	81	1.0	2.6	0.4	1.3	10 ●	9	0	W 1	NW 1	C 0
6	91.5	89.9	88.2	89.9	−4.9	5.8	−1.3	−0.4	7.5	−5.3	95	49	88	77	0.2	4.6	0.6	1.8	3 ≡	0 ⊙	0	C 0	SSE 2	C 0
7	88.2	88.3	90.0	88.8	−4.3	6.3	−0.6	0.2	7.2	−4.3	91	44	75	70	0.4	5.3	1.4	2.4	0	4 ⊙	0	C 0	S 2	E 2
8	91.2	91.4	94.3	92.3	−3.8	4.0	−0.9	−0.4	5.5	−4.0	87	48	79	71	0.6	4.2	1.2	2.0	2	3 ⊙	0	E 1	ESE 3	E 1
9	98.1	100.5	104.2	100.9	−3.2	3.2	−0.7	−0.4	4.3	−3.6	77	46	69	64	1.1	4.1	1.8	2.3	9	4 ⊙	0	ENE 2	ENE 4	NE 1
10	107.2	107.3	108.4	107.6	−5.1	4.1	−0.3	−0.4	5.3	−5.1	90	44	74	69	0.4	4.6	1.6	2.2	0 ⊙	0 ⊙	0	NE 1	E 3	E 1
11	109.2	108.2	107.1	108.2	−5.0	7.8	−0.5	0.4	11.0	−5.4	93	55	90	79	0.3	4.9	0.6	1.9	3 ⊙	0 ⊙	0	C 0	ESE 2	C 0
12	104.1	100.8	97.9	100.9	−1.1	10.7	4.0	4.4	13.3	−5.6	83	35	66	61	0.9	8.4	2.8	4.0	8	8 ⊙	3	SSE 3	SW 2	C 0
13	97.0	97.2	95.7	96.6	0.2	13.3	6.5	6.6	15.8	0.1	82	36	68	62	1.1	9.8	3.1	4.7	6 ⊙	2 ⊙	0	S 1	NW 1	C 0
14	92.3	90.1	89.9	90.8	2.7	17.2	10.1	10.0	18.4	2.3	79	43	81	68	1.5	11.2	2.4	5.0	6 ⊙	4 ⊙	10 ●	SSE 2	SW 4	C 0
15	92.1	91.3	86.4	89.9	7.3	10.9	9.7	9.4	12.7	7.0	76	60	69	68	2.5	5.2	3.7	3.8	10	9	9	NW 1	NW 3	SW 3
16	81.8	88.3	91.5	87.2	8.1	1.7	1.7	3.3	10.7	1.1	89	90	78	86	1.2	0.6	1.3	1.1	10 ●	10 ✳	9	NW 6	N 3	NW 2
17	92.0	89.3	85.8	88.4	−1.4	1.9	7.3	3.8	9.0	−1.7	80	87	90	86	1.1	0.9	1.0	1.0	10 ✳	10	10 ●	E 1	SSE 4	S 2
18	76.9	77.0	82.0	78.6	10.3	14.7	6.8	9.6	15.3	6.8	85	57	78	73	1.9	7.2	2.2	3.8	10	9	8	SW 6	WSW 4	C 0
19	87.6	87.7	86.3	87.2	5.7	11.4	9.0	8.8	12.2	5.2	85	56	92	78	1.5	5.9	1.0	2.8	7 ⊙	9	10 ●	NW 1	WNW 1	SW 1
20	88.6	87.7	85.1	87.1	7.5	14.7	12.1	11.6	16.6	7.0	91	61	76	76	0.9	6.5	3.3	3.6	3 ⊙	8 ⊙	0	WSW 1	SW 4	SW 1
21	86.2	90.2	90.8	89.1	10.6	13.3	8.0	10.0	15.4	8.0	81	62	72	72	2.4	5.8	2.9	3.7	9	6 ⊙	0	N 1	N 3	C 0
22	93.1	94.2	95.6	94.3	3.2	12.5	5.0	6.4	13.2	2.8	88	44	92	75	0.9	8.1	0.7	3.2	2 ⊙	4 ⊙	0	S 1	NW 3	C 0
23	94.9	95.0	95.3	95.7	0.3	14.7	10.7	9.1	16.3	−0.4	94	39	63	65	0.3	10.2	4.8	5.1	10	5 ⊙	10	C 0	ENE 2	E 3
24	94.1	95.3	97.4	95.7	6.6	5.1	4.1	5.0	11.1	4.1	66	78	80	75	3.2	2.0	1.6	2.3	10	9	10	E 10	E 12	E 3
25	98.6	99.3	100.0	99.3	2.3	6.7	5.3	4.9	10.3	2.3	89	88	92	90	0.8	1.2	0.7	0.9	10	9 ⊙	10	E 2	SE 3	E 3
26	100.1	98.5	99.4	99.3	3.3	14.0	7.6	8.1	15.1	2.8	98	45	65	69	0.1	8.8	3.6	4.2	10 ≡	5 ⊙	0	SSE 2	SSW 4	S 1
27	101.8	102.3	101.6	101.9	4.1	11.8	7.7	7.8	13.3	3.5	49	28	37	38	4.2	9.9	6.7	6.9	1 ⊙	1 ⊙	0	SW 4	SW 6	SSW 4
28	98.4	96.8	95.6	96.3	5.7	12.8	8.7	9.0	13.8	4.0	41	26	48	38	5.5	11.0	5.8	7.4	8 ⊙	6 ⊙	10	SSW 6	S 6	S 1
29	92.1	91.4	91.9	91.8	5.8	8.8	7.7	7.5	11.0	5.2	86	80	86	84	1.3	2.3	1.5	1.7	6	10 ●	10	S 2	S 3	SSE 2
30	92.8	93.1	93.5	93.1	4.8	7.7	7.0	6.6	8.5	4.8	94	89	90	91	0.6	1.2	1.0	0.9	10 ●	10	10 ●	N 2	NNE 2	N 2
31	97.6	98.7	97.9	98.1	2.8	11.5	9.1	8.1	12.9	0.7	89	55	74	73	0.8	6.1	3.1	3.3	8	7 ⊙	10	S 1	SE 1	NNE 1
M	95.2	95.0	94.8	95.0	1.6	8.1	4.5	4.7	10.1	0.4	83	58	76	72	1.3	5.2	2.2	2.9	7.0	6.3	5.1	2.2	3.2	1.4

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1	97.8	95.8	95.2	96.3	3.7	17.4	9.8	10.2	18.4	2.5	95	39	62	65	0.4	12.2	4.6	5.7	4 ⊙	4 ⊙	0	NE 1	ESE 3	W 1
2	95.6	95.2	96.6	95.8	3.8	16.7	12.7	11.5	18.2	2.4	90	30	52	64	0.8	9.6	7.1	5.8	0 ⊙	6 ⊙	9	SSW 1	S 3	S 1
3	99.3	100.0	102.0	100.4	9.1	18.1	12.3	13.0	19.7	6.7	88	38	47	58	1.4	12.8	7.7	7.3	6 ⊙	3 ⊙	0	C 0	N 2	C 0
4	103.6	103.0	104.8	103.1	3.0	19.1	10.2	10.6	20.1	1.0	90	27	38	58	0.8	16.1	5.2	7.4	0 ⊙	0 ⊙	0	C 0	NE 3	NE 1
5	104.0	101.3	96.8	100.8	2.3	17.4	11.8	10.8	18.8	1.1	86	26	49	54	1.0	14.8	7.0	7.6	0 ⊙	0 ⊙	0	E 1	ENE 4	C 0
6	92.8	88.6	85.8	89.1	4.0	20.2	10.2	11.2	21.2	1.8	87	26	62	58	1.1	19.5	4.6	7.7	0 ⊙	0 ⊙	1	ESE 1	SSW 4	S 1
7	86.8	87.9	89.5	88.1	6.3	6.3	4.7	5.5	10.5	4.6	85	79	92	85	1.4	2.0	0.7	1.4	10	10 ●	10 ●	NNW 3	N 4	N 2
8	93.9	94.4	94.1	94.1	0.4	2.6	1.8	1.6	5.1	0.4	88	79	71	79	0.8	1.6	2.1	1.5	10	9	0	N 4	N 4	NW 3
9	92.0	90.2	87.8	90.0	−0.6	8.5	7.2	5.6	11.4	−3.1	89	52	70	70	0.6	5.5	3.1	3.0	2 ⊙	8 ⊙	9	NW 1	NW 3	NW 1
10	86.1	82.1	76.5	81.6	4.0	12.7	9.1	8.7	14.8	2.9	88	34	72	65	0.9	9.7	3.2	4.6	8 ⊙	4 ⊙	9	NNE 1	SSW 3	SW 1
11	72.1	75.8	79.0	75.0	5.4	5.5	4.7	5.1	9.4	4.1	83	78	81	81	1.6	1.9	1.6	1.7	10 ●	10	9	NW 3	N 3	N 2
12	85.0	86.0	88.9	86.6	1.8	6.6	4.3	4.2	7.3	1.1	78	46	65	63	1.6	5.3	2.9	3.3	6 ⊙	10	10	N 1	NNE 2	NE 1
13	90.8	90.6	94.2	91.9	−0.4	7.7	0.4	2.0	9.0	−0.5	98	40	88	75	0.1	6.3	0.8	2.4	8	3 ⊙	0	NW 2	S 2	C 0
14	95.3	94.6	95.3	95.1	−0.5	5.2	2.9	2.6	6.6	−2.9	88	41	67	65	0.7	5.2	2.4	2.8	8 ⊙	3 ⊙	9	C 0	NNE 3	NE 2
15	96.3	97.3	100.2	97.9	−0.8	6.0	−0.2	1.2	7.6	−2.3	81	39	90	70	1.1	5.8	0.6	2.5	2 ⊙	9 ✳	3	NNE 2	NNW 3	N 1
16	101.4	100.1	99.2	100.2	−0.8	10.1	8.1	6.4	11.5	−3.7	83	35	67	61	1.0	8.3	3.6	4.3	0 ⊙	7	10	E 1	NW 3	WSW 1
17	97.3	97.0	96.8	97.0	6.3	9.9	5.7	6.9	11.6	5.6	85	71	89	82	1.4	3.6	1.0	2.0	10 ●	9	3	SSE 1	NNE 4	N 1
18	95.7	94.8	93.9	94.8	4.3	5.3	3.2	4.0	6.6	3.2	87	69	76	77	1.1	2.7	1.9	1.9	10	10 ●	0	NNW 2	NNW 4	N 1
19	92.8	89.7	91.5	91.3	0.8	13.3	8.4	7.7	13.6	−2.3	88	44	85	72	0.8	8.6	1.8	3.7	4 ⊙	8	10 ●	SE 1	S 2	WSW 1
20	96.4	99.0	100.3	98.6	7.1	10.3	5.7	7.2	12.6	3.0	81	50	61	64	1.9	6.3	3.6	3.9	10	8	2	NNW 3	NW 4	N 1
21	102.7	103.2	104.3	103.4	1.4	11.1	6.7	6.3	12.1	−1.1	91	41	77	70	0.7	7.8	2.3	3.6	5	9 ⊙	1	NNE 1	E 3	E 1
22	106.2	106.8	106.3	106.3	4.4	4.6	4.7	4.6	7.0	3.8	93	87	94	91	0.6	1.1	0.5	0.7	10 ●	10 ●	10 ●	NE 2	NNE 2	NE 1
23	105.4	105.3	104.8	105.2	4.7	7.1	7.7	6.8	8.9	3.4	98	88	86	91	0.1	1.2	1.5	0.9	10 ●	10	10	NE 1	N 3	N 3
24	102.4	102.3	101.3	102.1	7.1	8.6	9.1	8.3	9.7	6.7	94	89	89	91	0.6	1.3	1.3	1.1	10 ●	10	10 ●	NNW 3	N 4	N 2
25	98.3	98.3	98.6	98.3	7.3	8.3	7.7	7.8	9.4	7.3	96	89	93	93	0.4	1.3	0.7	0.8	10	10	10	NNW 2	NNW 3	NNW 1
26	97.8	97.6	97.4	97.6	7.3	10.3	10.3	9.7	11.3	7.0	97	88	94	93	0.3	1.4	0.8	0.8	10	10	10	N 1	N 3	NW 1
27	94.6	92.6	90.4	92.3	9.7	17.3	13.1	14.4	21.2	9.3	96	68	81	82	0.4	6.4	3.4	3.4	10	0 ⊙	4	N 1	[illegible] 1	SE 2
28	89.9	88.0	87.8	88.6	12.7	22.0	13.7	15.5	23.4	8.1	81	38	80	66	2.8	16.4	5.2	7.9	2 ⊙	6 ⊙	2	SE 2	[illegible] 5	SSE 1
29	89.	38.9	88.3	88.9	13.6	24.2	15.1	17.0	25.6	9.0	70	43	74	62	4.7	17.4	4.4	8.8	6 ⊙	4 ⊙	0	SE 1	WSW 3	C 0
30	87.6	85.1	89.1	87.3	13.7	24.7	12.2	15.7	24.9	8.6	78	38	87	68	3.3	19.3	1.9	8.3	0 ⊙	6 ⊙	10 ●	SE 1	SSW 6	NW 6
31																								
M	95.0	94.4	94.6	94.7	4.7	11.9	7.9	8.1	13.6	3.0	88	54	73	72	1.2	7.6	2.8	3.9	6.0	6.7	5.4	1.9	3.3	1.3

Racibórz $H_s = 189\ m$ $H_b = 196{,}1\ m$ $h_w = 15\ m$ **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.0	8	–	$*^0$ 000–125, 742–1050, 1130–1310, 1437–2144; = 000–24
2	8	0.0	6	–	$*^0$ 352–812; = 000–435
3	8	"	6	–	
4	7	0.0	5	–	= 620–1035, 1645–24
5	7	(0.0)	pł.	–	$\bullet^0$ 652–936; = 000–425 630–1050
6	7	.	pł.	–	= 000–450 $\equiv^1$–530 $\equiv^0$–725 = –1220; $\llcorner^2$ na
7	7	.	pł.	–	= 515–1220; $\llcorner^1$ n,a
8	7	.	pł.	–	= 545–936; $\llcorner^0$ n,a
9	8	.	pł.	–	$\llcorner^1$ n,a
10	7	.	pł.	–	= 630–1130; $\llcorner^1$ n,a
11	6	.	pł.	–	= 525–1220 ∞–1410; $\llcorner$ n,a
12	7	.	.	–	= 340–1138; $\llcorner^1$ n,a; $\oplus$ ^{1}910–1107
13	7	.	.	–	$\llcorner^0$ n,a
14	8	0.2	.	–	$\bullet^0$ 2034–24; $\llcorner^0$ n
15	8	1.7	.	–	$\bullet^0$ 812–915; Ψ ^{1}P 1950–2008
16	7	3.3	.	–	$\bullet^0$ 340–1108 Ψ^0–1305 $*^0$–1424
17	6	6.0	0	–	$*^0$ 512–1146 $\bullet^1$ 2018–2320 $\bullet^0$–24; = 615–1430
18	9	3.6	.	–	$\bullet^0$ 740–812 Ψ 945–1005 1322–1444, 1532–1608, 1651–1700; R ^{0} 1620-51 NE-SE; 1609-25 NW
19	8	1.8	.	–	$\bullet^1$ 000–24, 1318–2128
20	8	.	.	–	$\frown^1$ n, a, p–24; $\oplus$ 1450–1525
21	8	.	.	–	$\frown^1$ 000–n $\frown^0$ 1830–24
22	8	.	.	–	$\frown^1$ n–a
23	7	.	.	–	= 235–1224 $\llcorner^0$ n
24	8	0.5	.	–	Ψ 732–1140 $\bullet^0$ 2250–24; $\gg$ 610–1525 E
25	6	1.6	.	–	$\bullet^0$ 905–22 1005–1232; = 642–24, $\frown^1$ np–24
26	6	.	.	–	= 000–238 $\equiv^0$–330 $\equiv^1$–825 = –1315; $\frown^1$ 000–n $\frown^0$ 2033–24
27	9	.	.	–	$\frown^0$ 000–n
28	9	2.6	.	–	$\bullet^0$ 1538–2012, 2141–2208 2345–24; $\oplus$ 834–1222
29	7	4.7	.	–	$\bullet^0$ 000–515 1210–1306 1625–46 $\bullet^1$ 1708–1944
30	7	2.0	.	–	$\bullet^0$ 310–1138 1340–1414 1945–2125; = 1450–1635
31	6	0.0	.	–	$\bullet^0$ 1711–1806; = 220–525, 833–919; $\llcorner^1$ n–a; $\oplus$ 827–1115
Σ	–	28.0	–	–	UWAGI.

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1	7	.	.	–	= 525–1235; $\frown^2$ n–a, p–24
2	8	.	.	–	= 323–850; $\frown^2$ 000–a
3	7	.	.	–	= 535–918; $\frown^1$ n–a $\frown^2$ 1937–24
4	6	.	.	–	= 545–1010 ∞–1240; $\frown^2$ 000–a
5	7	.	.	–	$\llcorner^0$ n–a $\frown^2$ p–24
6	8	.	.	–	= 540–925; $\llcorner^0$ n–a
7	7	7.0	.	–	$\bullet^0$ 1015–1112, 1247–24
8	7	.	.	–	$\bullet^0$ 000–515
9	9	.	.	–	$\llcorner^2$ n–a
10	8	2.6	.	–	= 445–950; $\frown^1$ n $\frown^0$ p–24
11	7	0.3	.	–	$\bullet^1$ 506–1022; $\frown^1$ 000–506
12	8	0.0	.	–	$\bullet^0$ 2150–2215; $\oplus$ 831–1041
13	9	0.0	.	–	Ψ 1552–1600; = 515–1025; $\frown^1$ p–np $\llcorner^1$ np–24
14	8	0.0	.	–	Ψ 1146–1201; = 440–725; $\llcorner^2$ 000–a
15	7	0.0	.	–	Ψ 1240–53, 1335–49; $\llcorner^0$ n–a
16	8	0.0	.	–	$\llcorner^2$ n–a
17	7	0.3	.	–	$\bullet^0$ 640–1125 Ψ 1517–25; $\frown^1$ 2030–24
18	7	0.0	.	–	$\bullet^0$ 1047–1205 1246–1406
19	8	0.1	.	–	$\bullet^0$ 1452–2109; $\llcorner^1$ n–a
20	8	0.0	.	–	$\bullet^1$ 211–28, 748–808; = 228–330; $\frown^1$ p–24
21	7	6.5	.	–	= 722–1010; $\frown^0$ 000–na $\llcorner^1$ na–a
22	6	8.8	.	–	$\bullet^0$ 405–508 $\bullet^1$–1125 $\bullet^0$–2325
23	6	1.9	.	–	$\bullet^0$ 540–1021; = 530–24
24	6	10.5	.	–	$\bullet^1$ 212–345 $\bullet^0$–738 $\bullet^1$–809 $\bullet^0$–1015 1250–1450 1540–1736, 1838–2140 $\bullet^1$–2225 $\bullet^0$–24, = 000–24
25	6	0.0	.	–	$\bullet^0$ 000–632, 710–2007, 2135–2330; = 000–24
26	6	8.6	.	–	$\bullet^0$ 031–135 $\bullet^0$ 742–830; = 000–24
27	8	.	.	–	Ψ 206–311; = 000–1126
28	8	.	.	–	$\frown^2$ n–a, p–24
29	8	.	.	–	$\frown^2$ 000–a
30	8	5.0	.	–	Ψ 1205–08, 1935–2015 $\bullet^1$–2135 $\bullet^0$–2207; $\gg$ 1845–2020; $\frown^2$ n–a
31					
Σ	–	51.6	–	–	UWAGI.

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$ **Maj–Mai 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			WIATR D.w		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	94.2	93.8	93.5	93.8	7.6	10.7	7.4	8.5	12.4	7.4	69	55	75	66	3.2	5.8	2.6	3.9	10	9	3	NNE 3	ESE 3	C 0
2	92.1	91.4	90.2	91.2	7.3	9.1	7.7	8.0	9.9	3.8	70	63	77	70	3.0	4.3	2.4	3.2	8 ⊙	10	10	NE 3	E 3	ENE 1
3	89.7	88.7	87.7	88.7	7.0	11.8	8.3	8.8	14.6	6.3	87	55	78	73	1.3	6.4	2.3	3.4	9	9	2	NE 2	NE 2	SSE 1
4	87.8	88.8	91.7	89.4	9.0	11.1	5.1	7.6	12.6	5.0	80	65	69	71	2.3	4.6	2.8	3.2	2 ⊙	9	5	W 2	NNW 4	NNW 1
5	92.7	90.3	87.3	90.2	4.9	9.1	2.7	4.8	10.4	0.4	72	44	86	67	2.5	6.6	1.0	3.4	5 ⊙	10	0	WNW 2	WNW 3	C 0
6	85.7	86.7	86.9	86.4	2.9	7.0	2.8	3.9	8.8	0.6	84	55	82	74	1.2	4.5	1.3	2.3	10	8	4	WNW 4	WNW 5	NNW 1
7	85.7	84.7	84.3	85.0	2.3	8.1	3.0	4.1	9.0	−0.4	82	48	90	73	1.3	5.7	0.8	2.6	10	9 ●	4	N 2	W 3	C 0
8	84.7	85.0	86.7	85.5	3.8	6.3	4.3	4.8	8.1	1.8	87	65	82	78	1.1	3.4	1.5	2.0	10	10 ⛆	6	WNW 3	NNW 3	C 0
9	88.4	88.3	88.5	88.4	3.9	8.1	5.7	5.8	9.4	1.4	85	54	80	73	1.2	5.0	1.9	2.7	10	10	7	NE 1	NNW 5	NE 1
10	87.8	88.3	90.3	88.8	4.7	6.2	6.6	6.0	7.2	3.6	95	86	94	92	0.4	1.2	0.5	0.7	10 ●	10 ●	10 ●	N 2	NNW 3	C 0
11	92.2	92.2	91.9	92.1	8.2	16.1	10.2	11.2	18.2	6.0	90	51	92	78	1.1	8.9	0.9	3.6	8	4 ○	4	SSE 2	S 3	SW 1
12	93.2	92.6	93.8	93.2	12.3	21.1	14.7	15.7	22.0	6.8	71	41	67	60	4.2	14.7	5.3	8.1	2 ○	5 ○	4	S 3	S 4	SE 2
13	95.2	94.2	94.0	94.5	13.2	22.8	15.6	16.8	23.6	9.2	75	41	72	63	3.8	16.3	5.0	8.4	2 ○	4 ○	3	SE 2	SSE 3	SE 1
14	96.4	97.3	98.3	97.3	13.2	18.7	12.5	14.2	21.6	9.0	83	58	85	75	2.6	9.2	2.2	4.7	5 ○	6 ○	1	WNW 1	WNW 3	C 0
15	100.0	98.6	96.8	98.5	10.4	21.1	16.2	16.0	22.7	6.7	85	44	64	64	1.9	13.9	6.7	7.5	0 ⊙	2 ⊙	0	NW 1	N 3	C 0
16	95.2	92.4	91.0	92.9	12.7	24.0	18.4	18.4	25.2	8.6	78	41	56	58	3.3	17.6	9.3	10.1	0	8	8	ESE 1	SE 3	E 2
17	92.3	93.7	95.9	94.0	13.5	17.1	11.3	13.3	18.5	10.0	85	69	85	80	2.3	6.0	2.0	3.4	9	6	10	NNW 4	NW 4	NW 5
18	95.6	95.3	89.8	92.9	11.2	20.3	16.0	15.9	22.6	10.4	82	55	76	71	2.3	10.8	4.4	5.9	9	4 ○	4	N 3	NNE 2	C 0
19	86.2	83.5	82.6	84.1	15.2	24.8	19.1	19.6	26.2	12.9	77	45	67	63	4.1	17.1	7.4	9.5	3 ○	6 ○	4	NE 1	NE 3	NE 1
20	84.7	86.0	89.7	86.8	14.6	20.6	11.1	14.4	22.7	10.2	86	62	92	80	2.4	9.1	1.0	4.2	7 ○	8 ⊙	6	NW 2	WNW 4	NW 10
21	95.2	95.1	94.1	94.8	8.3	11.2	10.7	10.2	12.2	8.3	89	71	85	82	1.3	3.9	2.0	2.4	10	10	10	NW 4	NNW 5	C 0
22	92.1	91.6	91.1	91.6	10.7	12.8	10.0	10.9	13.4	9.8	80	64	86	77	2.6	5.4	1.8	3.3	9 ●	10	10 ●	N 1	NE 2	N 1
23	89.2	88.1	87.4	88.2	11.8	19.3	15.8	15.7	21.7	9.9	87	63	90	80	1.8	8.2	1.7	3.9	7	8	7	NNE 2	ENE 1	C 0
24	89.1	90.4	93.7	91.1	14.3	19.6	14.9	15.9	20.6	12.3	89	62	73	75	1.8	8.6	4.3	5.0	9	9	9	N 3	NNW 3	NE 4
25	96.8	98.3	99.6	98.2	10.5	12.6	9.9	10.7	15.1	9.5	68	43	50	54	4.1	8.3	6.1	6.2	8	6 ⊙	7	NE 4	NE 3	NE 3
26	100.3	100.3	100.3	100.4	6.7	10.0	7.3	7.9	11.6	3.6	64	40	61	55	3.3	7.4	4.1	5.0	8	9	9	NE 3	NE 3	NE 3
27	99.3	99.2	98.9	99.1	5.9	9.3	7.2	7.4	10.6	3.4	67	49	60	59	3.1	6.0	4.1	4.4	9 ○	9	9	NE 3	NE 3	NE 2
28	97.3	96.0	95.9	96.4	6.3	11.7	7.8	8.4	12.6	2.9	72	41	71	61	2.6	8.0	3.1	4.6	4 ⊙	8	4	NNE 2	NNE 3	NE 1
29	97.1	97.3	98.6	97.7	6.3	12.3	6.8	8.1	13.3	2.1	76	45	84	68	2.3	7.9	1.6	3.9	0	6 ⊙	1	NNE 1	SW 1	C 0
30	100.1	98.9	97.7	98.9	6.6	17.7	10.4	11.3	18.7	1.1	76	33	77	62	2.3	13.6	2.9	6.3	2	4 ⊙	0 ⊙	NE 1	SSE 4	C 0
31	97.9	96.3	93.9	96.0	10.0	18.0	10.9	12.4	19.6	3.4	72	38	85	65	3.3	12.7	1.9	6.0	0 ○	8	1	C 0	SSE 1	C 0
M	92.7	92.3	92.3	92.4	8.9	14.3	10.0	10.8	16.0	6.0	79	53	77	70	2.4	8.4	3.1	4.6	6.3	7.3	5.2	2.2	3.3	1.3

Czerwiec – Juin

1	94.3	93.9	93.9	94.0	12.1	21.0	14.2	15.4	22.6	6.4	72	36	67	58	4.0	15.9	5.3	8.4	0 ⊙	3 ○	2	C 0	W 2	C 0
2	96.9	97.1	96.8	96.9	13.1	22.3	16.0	16.9	23.6	8.3	73	41	76	63	4.1	15.9	4.4	8.1	2 ⊙	1 ⊙	0	NNW 1	NNW 3	C 0
3	97.8	95.7	92.9	95.5	13.2	27.0	19.2	19.6	27.5	9.0	79	31	60	57	3.2	24.4	8.9	12.2	0 ○	4 ○	5	E 1	SSE 4	SSE 1
4	90.5	90.9	88.2	89.9	17.1	19.3	16.8	17.5	21.8	12.0	72	76	94	81	5.4	5.4	1.2	4.0	10	10 ●	10	C 0	SW 2	SE 1
5	87.0	87.2	85.3	86.6	13.1	15.7	13.0	13.7	20.3	12.7	92	84	85	87	1.3	2.8	2.3	2.1	10 ●	9	10	NW 6	SW 2	NNW 1
6	87.3	89.8	90.8	89.3	13.3	14.8	10.7	12.4	17.0	10.6	79	62	89	77	3.2	6.4	1.5	3.7	8	7	1	SW 2	NNW 3	C 0
7	90.0	88.0	86.3	88.8	12.2	22.7	14.3	16.0	25.0	7.3	71	38	93	74	4.2	11.7	1.1	5.7	9	9 ○	10 ☾	SSE 1	SSW 4	NE 1
8	89.8	89.3	88.6	89.2	14.1	23.2	17.6	18.1	25.4	10.7	94	59	80	78	0.9	11.7	4.0	5.5	8	7 (K)	4	SSE 1	SE 1	SE 1
9	87.7	88.0	88.1	87.9	18.8	25.0	18.9	20.4	26.2	14.3	79	55	85	73	4.5	14.3	3.3	7.4	5 ○	4 ○	4	SE 1	SW 4	W 1
10	88.7	88.3	88.4	88.5	17.0	22.8	21.3	20.6	25.7	15.3	91	64	69	75	1.8	10.1	7.7	6.5	9	5 ⊙	3	ENE 2	SE 1	C 0
11	87.2	85.7	87.7	86.9	21.4	30.2	22.7	24.2	30.7	14.7	72	37	74	61	7.1	27.0	7.3	13.8	3 ○	7 ○	6	SE 2	SSW 5	C 0
12	96.7	101.2	105.7	101.2	18.2	19.8	13.6	17.3	23.1	13.6	86	80	86	84	2.9	4.3	2.4	3.3	10	9	9	NNE 4	NW 5	NNW 3
13	108.0	107.2	105.3	106.8	15.7	19.4	14.6	16.1	22.4	14.3	77	57	73	69	4.1	9.7	4.3	6.1	9	7 ○	3	NE 3	NNE 3	NNW 1
14	105.8	104.7	103.8	104.8	13.6	22.0	16.0	16.9	23.3	8.7	77	44	63	61	3.3	14.7	6.8	8.3	0 ⊙	0 ⊙	0	NE 2	NNE 3	C 0
15	104.3	102.8	100.9	102.7	13.7	22.8	13.7	17.0	24.6	10.1	71	38	73	61	4.6	17.0	4.4	8.7	1 ⊙	0 ⊙	0	NE 1	NE 3	C 0
16	99.9	97.8	95.9	97.9	15.2	25.2	17.2	18.7	25.4	10.0	67	33	68	56	5.6	21.3	6.4	11.1	0 ○	0 ○	0	NE 2	E 3	E 1
17	96.2	95.3	93.7	95.1	16.6	25.9	18.0	19.6	27.2	10.5	66	33	73	58	6.4	22.3	5.2	11.3	1 ○	2 ○	1	N 1	NE 3	E 1
18	93.3	91.8	89.4	91.6	17.1	28.0	23.2	22.9	29.7	11.2	68	44	64	59	6.2	21.2	10.2	12.5	0 ○	2 ⊙	8	ENE 1	SW 3	SSW 1
19	90.0	89.2	89.4	89.5	19.3	25.0	16.7	19.4	27.7	16.7	72	59	89	73	6.2	13.0	2.2	7.1	7 ○	4 ⊙	8	SW 3	S 5	SE 1
20	90.2	92.1	93.6	92.0	17.0	19.4	16.9	17.6	22.2	14.0	87	81	93	87	2.6	4.2	1.4	2.7	8 ⊙	10 ●	3	SSE 1	N 2	C 0
21	94.8	91.7	89.1	91.9	14.8	24.6	19.4	19.6	25.1	12.3	98	59	83	80	0.3	12.5	3.8	5.5	7 ≡	5 ⊙	10	N 1	SE 2	SSE 3
22	86.6	84.9	84.7	85.4	19.0	25.3	18.0	20.1	26.7	15.6	87	58	94	80	3.0	13.8	1.2	6.0	9	5	4	S 2	SW 4	NNE 1
23	88.0	88.0	87.0	87.7	18.3	24.4	19.4	20.4	25.6	14.4	76	53	88	72	5.0	14.4	2.8	7.4	3 ⊙	8 ⊙	6	SW 3	SW 6	C 0
24	87.7	84.2	81.6	84.5	15.3	23.4	15.3	17.3	23.7	15.0	93	73	94	87	1.2	7.7	1.0	3.3	10 ●	4 ⊙	10	NNE 2	NW 3	N 3
25	86.4	91.6	94.7	90.9	16.8	17.4	13.4	15.2	19.7	13.4	68	58	81	69	6.1	8.4	3.0	5.8	7 ⊙	8	8	SW 7	W 4	N 1
26	98.2	98.9	100.8	99.3	12.2	14.2	10.5	11.8	17.9	10.4	75	65	88	76	3.5	5.6	1.5	3.5	4 ⊙	9	2	N 3	NW 3	C 0
27	102.4	102.3	103.3	102.9	10.8	16.6	11.2	12.4	18.6	6.3	79	56	90	75	2.8	8.4	1.3	4.2	1 ⊙	6 ⊙	2	NW 1	SSW 2	C 0
28	104.4	102.8	100.9	102.6	10.6	21.2	17.0	16.4	24.7	5.4	86	45	91	74	1.8	13.8	1.8	5.8	6	9	0	NW 1	SW 1	C 0
29	101.6	101.3	100.0	101.0	17.1	27.2	19.8	21.0	28.7	13.0	85	48	87	73	3.0	18.7	3.1	8.3	4 ⊙	4 ⊙	0	W 3	W 2	C 0
30	99.6	97.7	97.3	98.2	19.2	30.3	21.3	23.1	31.3	15.3	82	48	78	69	4.0	22.3	5.6	10.7	0 ⊙	5 ⊙	3	SSE 2	NW 3	N 1
31																								
M	94.4	94.0	93.6	94.0	15.3	22.6	16.8	17.9	24.3	11.8	79	54	81	71	3.8	13.3	3.9	7.0	5.0	5.4	4.4	1.9	3.1	0.8

Racibórz $H_s = 189$ m $H_b = 196.1$ m $h_w = 15$ m **Maj-Mai 1957**

DNI	WIELKOŚĆ ZACHMURZENIA V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	⌒² p-24
2	7	.	.	-	⌒² 000-a
3	8	.	.	-	
4	8	.	.	-	⌒⁰ n-a
5	8	0.4	.	-	⌒⁰ n, ⊕ ¹ 1038-1115 1220-1615
6	8	.	.	-	•⁰ 510-45 ⊕ 1125-1217, 1340-1529 1635-1747
7	7	1.1	.	-	∴ 1246-1308 1440-50 1510-39, 1727-1909
8	7	0.0	.	-	⛆ 1236-1320 ∴ 1408-35
9	8	1.8	.	-	•⁰ 735-940 ∴ -1008
10	7	9.5	.	-	•⁰ 000-607 •¹-730 •⁰-845 •⁰-929 •⁰-1014 •¹-1320 •⁰-1516 •,-1747 •⁰ 1815-2240, = 2145-24
11	8	.	.	-	•⁰ 110-250, = 000-330, ⌒¹ 2030-24
12	8	.	.	-	⌒² n-a
13	8	.	.	-	(↖) 1630-1740 NNE-N, ⌒¹ n-a ⌒² p-24
14	8	0.0	.	-	(↖)¹ 1451-1506 ↖⁰-1535 NW-E, ⌒² 000-a
15	8	.	.	-	⌒² n,a ⌒¹ p-24
16	8	.	.	-	= 415-750, ⌒² 000-a, p-24, ⊕ ⁰ 1235-1325
17	7	.	.	-	⌒² 000-a
18	7	.	.	-	
19	7	.	.	-	(↖)¹ 1331-1435 SE-W ⌒¹ np-24
20	8	36.9	.	-	▲¹ 1508-12 •¹ 1842-1912 •⁰-2008 (↖)¹ 1455-1507 N-NE ↖¹ 1507-1608-1842 NE-SW, ≫ 1500-28 2014-2230, 20.V: ⌒¹ 000-n,a
21	7	0.0	.	-	•⁰ 540-616 •¹ 808-940 •⁰-1008
22	7	0.8	.	-	•⁰ 606-711 1212-1542, 1616-2119
23	7	.	.	-	⌒² p-24
24	7	0.0	.	-	•⁰ 714-809 ∴⁰ 1716-30, ≤¹ n, ⌒¹ n-a
25	8	.	.	-	⌒¹ np-24
26	8	.	.	-	⌒¹ 000-a
27	9	.	.	-	⊕ ¹ 840-1007
28	8	.	.	-	⌒⁰ p-24
29	8	0.0	.	-	∴ 930-1030, ⌒² 000-a
30	8	.	.	-	⌒² 000-a
31	8	.	.	-	∞ 640-830, ⌒¹ 000-a ⌒² p-24
Σ	—	50.5	—	-	UWAGI

Czerwiec - Juin

1	8	.	.	-	= 350-640, ⌒² 000-a
2	8	.	.	-	⌒⁰ n-a
3	8	.	.	-	=, n, a ∞ 1045-1130 ⌒² n-a, np-24
4	7	12.4	.	-	•⁰ 1153-1540 ∴ 1703-1928 •⁰⁻¹ 2150-24¹ = 427-716 ∞-1042 = 2145-24 ⌒² 000-a ⊕ 715-825
5	7	3.3	.	-	•¹ 100-400 •¹⁻² 402-510 ∴ 705-30 •⁰ 835 •¹-915 •⁰-1012 ∴ 1244-1304 1315-40 2118-35 2218-2305, = 000-1010
6	8	0.0	.	-	∴ 1237-46 ⌒² n,a, p-24
7	8	62.2	.	-	•↖⁰⁻² 1635-1748-2342 ▲⁰ 1744-48 1805-09, = 522-740 ∞ 810-945 ⌒² 000-a
8	8	0.0	.	-	•⁰ 1442-1500 (↖)⁰ 1355-1445 NW-NE, 1556-1624 SE-E, = 415-710, 2230-24, ⌒² n-a
9	8	16.1	.	-	∴ 2058-2124, (↖)¹ 2246-2332 S-NE ↖-24 NE-SE, = 000-610 ∞-940, ⌒² n-a
10	7	6.6	.	-	∴ 054-232, 651-708, 1150-1220, ↖¹ 000-54 NE-SE ↖⁰ 1140-1240 S-NE, (↖)⁰-1340 NE, = 845-1030
11	8	.	.	-	⌒² n-a
12	7	.	.	-	= 020-1335, ⌒² n-a
13	8	.	.	-	
14	8	.	.	-	
15	8	.	.	-	⌒² n-a
16	8	.	.	-	⌒² n-a
17	8	.	.	-	= 445-730 ∞-1015, ⌒⁰ n-a, p-24
18	7	.	.	-	= 433-935, ⌒² 000-a
19	8	8.8	.	-	∴ 2030-53 (↖)¹ 1654-1746 N-W ↖¹-1940 W-S (↖)¹-2040 S, = 2130-24, ⌒⁰ n-a
20	7	0.0	.	-	•⁰ 1330-1405 = 000-1030, ⌒² n-a
21	7	3.5	.	-	•⁰ 2046-2130, ↖¹ 1440-1610 NW-SE, ≡¹ 455-740 ≡⁰-920 = -1118, ⌒² n,a
22	8	21.4	.	-	∴ 1033-1110, 1940-2002 (↖)¹ 1722-54 NW ↖⁰ 1754-1810-1940 NW-E, = 000-915, ⌒¹ n-a
23	8	0.0	.	-	⌒¹ n,a
24	7	7.7	.	-	•⁰ 732-808, ↖¹ 1550-1705 W-NE, = 640-1108, 2030-24, ⌒⁰ n-a
25	8	.	.	-	= 000-530, ⌒² n-a
26	8	.	.	-	⌒¹ n-a, p-24, ⊕ 1030-40
27	7	.	.	-	= 237-814, ⌒² 000-a
28	8	.	.	-	= 2120-24, ⌒² n,a
29	8	.	.	-	= 000-1040 ⌒² n-a
30	8	.	.	-	(↖)⁰ 1450-1515 E, 1730-1900 E, = 445-930 ∞-1030, ⌒² n-a, ⌒ 1920-30
31					
Σ	—	142.0	—	-	UWAGI

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$ **Lipiec – Juillet 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE i POGODA N			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	97.3	96.0	94.9	96.1	20.6	30.2	21.1	23.2	31.8	15.1	77	48	82	69	5.4	22.3	4.5	10.7	0 ⊙	1 ⊙	1	C 0	NNW 1	C 0
2	93.9	92.0	93.7	93.9	20.6	29.6	18.1	21.6	31.9	16.3	79	40	93	71	5.0	25.0	1.5	10.5	4 ◯	8 (K)	10 K	SE 2	NNW 8	K 3
3	98.9	96.9	96.3	97.4	16.3	22.2	16.7	18.0	25.6	14.5	64	49	84	66	6.7	13.6	3.1	7.8	3 ⊙	1 ⊙	1	N 1	N 2	C 0
4	96.2	94.7	93.7	94.9	16.2	29.7	22.2	22.6	31.5	12.2	81	46	83	70	3.4	22.3	4.7	10.1	6	2 ⊙	1	SE 2	SW 1	C 0
5	94.0	93.0	93.8	93.6	24.3	33.4	24.2	26.6	33.2	17.9	74	41	72	62	7.9	30.1	8.6	15.5	0 ⊙	0 ⊙	6	SSE 1	WSW 4	ENE 1
6	98.1	98.1	96.7	97.6	20.7	25.6	20.9	22.0	28.5	19.2	78	59	86	74	5.3	13.4	3.4	7.4	2 ⊙	0 ⊙	0	N 3	N 2	C 0
7	98.1	96.8	95.1	96.7	18.0	27.6	23.7	23.2	30.3	16.3	94	48	80	74	1.2	19.1	5.9	8.7	10 K	0	1	SW 3	SE 2	C 0
8	94.2	91.8	92.2	92.7	22.6	34.2	20.2	24.3	35.1	16.3	84	38	96	71	4.3	33.1	2.5	13.3	3 ⊙	2 ⊙	10 (K)	SE 1	SSW 4	NW 4
9	91.6	93.1	92.3	92.3	19.7	22.6	19.7	20.4	26.1	18.0	91	71	90	84	1.9	7.9	2.4	4.1	6	8	4	NW 2	NW 2	NE 1
10	90.2	87.1	84.9	87.4	17.7	25.0	17.5	19.4	25.9	16.1	95	57	94	82	1.0	13.6	1.2	5.3	10	6 ⊙	8	N 1	E 2	C 0
11	81.7	82.7	84.5	83.0	18.2	21.6	19.3	19.6	23.4	16.5	83	76	91	83	3.5	6.1	2.0	3.9	8	9	10	ENE 2	SE 2	NE 2
12	85.6	87.4	89.3	87.4	17.9	21.1	18.0	18.8	22.5	17.0	93	84	95	90	1.4	4.7	1.0	2.4	10 ●	9	8	NNE 2	NW 5	C 0
13	92.2	93.7	94.2	93.4	19.2	24.1	19.9	20.8	27.0	16.5	84	56	87	76	3.6	13.2	3.0	6.6	7 ⊙	5 ⊙	4	N 1	NNE 2	C 0
14	93.4	92.1	92.0	92.5	18.7	23.0	17.4	19.1	25.1	15.0	86	71	94	84	3.2	8.2	1.3	4.2	2 ⊙	9	1	NE 2	SE 1	N 1
15	91.1	91.0	90.4	90.8	16.4	19.9	16.1	17.1	21.0	14.9	96	80	92	89	0.8	4.7	1.6	2.4	10 ●	9	9	C 0	NNW 3	C 0
16	87.5	86.6	88.3	87.5	15.2	15.0	12.8	14.0	16.4	12.8	94	93	95	94	1.0	1.1	0.7	0.9	10 ●	10 ●	10 ●	NNW 2	NNW 4	SW 2
17	87.1	88.1	90.0	88.4	14.0	18.3	14.5	15.3	19.4	12.7	91	65	93	83	1.5	7.3	1.1	3.3	10 ●	8	8	NW 2	NW 6	C 0
18	90.9	89.7	88.3	89.6	14.2	21.6	16.0	17.0	23.5	11.7	83	56	94	78	2.7	11.3	1.2	5.1	3 ⊙	6 ⊙	3	S 1	NNW 2	C 0
19	87.7	85.6	84.9	86.1	15.2	25.6	18.8	19.6	26.6	11.0	87	46	77	70	2.3	17.8	4.9	8.3	0 ⊙	5 ⊙	2	SSE 1	S 3	C 0
20	82.8	82.3	82.6	82.6	19.3	22.1	15.7	18.2	25.1	15.6	76	68	97	80	5.4	8.4	0.6	4.8	9	10	10	SSE 1	SW 2	C 0
21	82.5	82.2	81.5	82.1	14.7	19.2	16.7	16.8	21.3	14.3	90	68	91	83	1.6	7.2	1.8	3.5	10	9	6	NW 2	SW 2	C 0
22	80.5	81.1	80.2	80.6	13.2	18.3	14.8	15.3	20.4	11.0	92	70	83	82	1.3	6.2	2.9	3.5	6	8	10	C 0	N 3	SW 2
23	78.4	81.3	84.0	81.2	14.7	18.8	16.4	16.6	20.1	14.0	97	79	91	89	0.5	4.5	1.7	2.2	10 ●	9 ⊙	5	W 1	NE 1	N 2
24	86.2	88.6	89.9	88.2	15.2	17.6	13.9	15.2	18.6	13.9	93	76	90	86	1.2	4.7	1.6	2.5	10 ●	10	7	WNW 5	NW 4	C 0
25	90.7	91.0	87.7	89.8	14.2	15.9	14.3	14.8	19.4	12.0	88	73	88	83	2.0	4.9	2.0	3.0	9	10	10 ●	C 0	S 1	C 0
26	89.5	90.0	88.1	89.2	15.8	20.1	16.5	17.2	21.2	11.7	85	59	94	79	2.6	9.6	1.2	4.5	5	9	10 ●	SSW 1	W 5	SW 1
27	85.2	85.0	84.9	85.0	16.7	17.8	15.1	16.2	18.9	15.1	86	81	91	86	2.7	3.8	1.5	2.7	10	10	10 ●	S 2	SW 2	S 2
28	86.3	86.3	88.2	86.9	13.1	19.1	13.5	14.8	21.0	11.8	88	47	84	73	1.8	11.6	2.5	5.3	10	8	4	S 1	SW 3	SW 1
29	89.0	90.0	92.3	90.4	13.7	19.8	15.9	16.3	21.9	10.7	86	57	77	73	2.2	10.1	4.2	5.5	9	6 ⊙	7	S 3	S 3	SW 2
30	94.2	94.9	97.6	95.6	13.8	18.7	15.0	15.6	19.6	10.6	91	77	96	88	1.5	5.0	0.7	2.4	7	10	10	SE 1	NW 3	N 1
31	99.9	100.8	102.3	101.0	14.8	18.6	13.7	15.2	20.3	13.7	93	74	94	87	1.1	5.5	0.9	2.5	10	8 ⊙	0	NW 2	NW 2	C 0
M	90.2	90.0	90.2	90.1	16.9	22.5	17.4	18.6	24.3	14.4	87	63	89	80	2.8	11.5	2.5	5.6	6.7	6.6	6.0	1.5	2.8	0.8

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1	102.9	102.2	100.4	101.8	13.8	18.8	13.9	15.1	21.4	12.2	90	61	92	81	1.6	8.4	1.3	3.8	10	6 ⊙	0	C 0	NW 2	C 0
2	100.0	99.0	100.1	99.7	13.8	22.6	16.1	17.2	23.2	11.0	92	54	64	70	1.3	12.7	6.7	6.9	8	5	3	C 0	NW 4	N 3
3	100.4	99.1	99.8	99.8	13.2	18.0	14.2	14.9	19.4	9.2	78	53	81	71	3.3	9.6	3.1	5.3	2 ⊙	9	10	N 2	NNW 4	NW 3
4	99.9	99.2	99.6	99.6	14.3	18.3	13.0	14.6	19.3	8.6	82	66	88	79	2.9	7.1	1.8	3.9	5 ⊙	9	1	NW 2	NNW 3	C 0
5	100.4	100.2	100.0	100.2	14.6	21.7	13.9	16.0	22.6	9.0	85	60	95	79	2.3	10.4	1.1	4.7	1	4 ◯	2	NW 1	N 3	C 0
6	100.6	98.6	96.6	98.6	12.8	23.3	15.4	16.7	25.3	9.0	89	49	93	77	1.6	14.6	1.1	5.8	0 ⊙	4 ⊙	3	E 1	NE 1	C 0
7	94.3	91.4	88.4	91.4	15.0	22.8	19.2	19.0	25.2	11.3	90	61	93	81	1.6	10.7	1.5	4.6	7	10	10 ●	SE 1	S 4	C 0
8	88.2	86.7	88.3	88.4	16.5	21.9	14.4	16.8	22.2	14.0	88	64	93	82	2.4	9.6	1.1	4.4	0	4 ⊙	0	C 0	NW 4	C 0
9	86.7	84.8	81.0	84.2	13.3	25.2	20.2	19.7	26.4	10.7	96	43	77	73	0.6	17.7	5.5	7.9	7 ⊙	3 ⊙	0	C 0	SE 2	E 2
10	79.2	83.6	86.6	83.1	17.7	21.8	16.8	18.3	24.4	16.0	88	66	93	82	2.4	8.9	1.4	4.2	10	8	1	SE 2	SW 3	S 1
11	91.5	90.6	90.3	90.8	17.8	27.7	19.7	21.2	28.1	13.0	76	45	86	69	5.0	20.3	3.2	9.5	8	4 ⊙	0	SSW 1	S 3	C 0
12	88.3	90.0	90.0	89.4	19.0	23.9	19.6	20.5	25.6	14.8	82	55	89	79	4.0	10.2	2.6	5.6	4 ⊙	3 ⊙	5	S 2	NW 2	C 0
13	92.7	92.8	90.2	91.9	18.3	25.2	20.7	21.2	26.2	15.7	81	55	77	71	4.0	14.3	5.7	8.0	5 ⊙	7	6	NNW 1	NE 2	NE 1
14	88.6	89.4	87.1	88.4	17.8	24.6	18.2	19.7	25.2	17.0	96	70	90	85	0.8	9.1	2.1	4.0	6 ⊙	5	10	C 0	NE 2	N 2
15	88.1	87.3	88.0	87.8	15.8	23.0	16.9	18.2	24.9	13.7	94	56	93	81	1.1	12.5	1.4	5.0	1 ⊙	5 ⊙	3	SE 1	NW 1	C 0
16	88.0	89.8	90.5	89.4	16.0	16.2	13.9	15.0	21.9	13.8	86	80	94	87	2.5	3.6	0.9	2.3	9	10	10	SSE 2	N 5	C 0
17	90.6	90.5	90.1	90.4	13.0	17.0	14.6	14.8	18.9	12.1	94	66	79	80	0.9	6.5	3.4	3.6	10 ●	9	9	S 2	W 2	SW 1
18	89.3	89.1	89.4	89.3	14.2	18.3	14.2	15.2	19.7	12.0	78	66	87	77	3.6	7.1	2.2	4.3	9	9	5	S 3	SW 5	SW 1
19	91.4	92.6	94.8	92.9	11.6	17.0	14.9	14.6	18.2	9.5	94	78	94	89	0.8	4.3	0.9	2.0	5	10	10	S 1	NE 1	C 0
20	95.7	95.9	95.8	95.8	14.7	20.9	14.6	16.2	22.7	12.2	87	60	91	79	2.2	9.8	1.5	4.5	5 ⊙	4 ⊙	0	N 1	W 2	C 0
21	94.3	92.2	89.3	91.9	12.8	22.2	17.9	17.7	24.5	10.3	91	62	89	81	1.4	10.1	2.2	4.6	4 ⊙	6 ⊙	10	NW 1	SW 1	C 0
22	89.2	89.9	91.0	90.0	11.6	15.2	10.0	11.7	17.9	10.0	93	72	95	87	1.0	4.8	0.7	2.2	10 ●	10	0	NW 4	NW 5	C 0
23	92.1	91.0	89.7	90.9	8.6	17.7	10.8	12.0	19.4	5.6	90	55	90	78	1.1	9.0	1.4	3.8	4 ⊙	4 ⊙	0	NNW 1	SW 1	C 0
24	87.8	89.3	89.7	87.6	10.6	22.1	13.2	14.8	23.6	6.5	84	48	92	75	2.1	13.9	1.3	5.8	1 ⊙	5 ⊙	10	SE 1	SW 8	C 0
25	94.8	92.7	89.9	92.5	9.7	21.5	14.4	15.0	22.3	7.4	99	41	78	73	0.1	15.0	3.6	6.2	0	6 ⊙	0	SW 1	S 7	C 0
26	89.2	90.1	91.3	90.3	13.3	19.7	12.4	15.0	19.9	9.6	79	50	90	73	3.7	11.3	1.4	5.5	9	4 ⊙	2	SW 1	WSW 2	W 1
27	93.1	92.3	92.3	92.6	11.3	18.6	12.7	13.8	24.9	8.6	86	55	88	76	1.8	9.6	1.8	4.4	7 ⊙	6 ⊙	10 ●	SSE 2	SSW 4	WSW 1
28	89.8	90.3	92.0	90.7	12.3	17.8	14.0	14.5	19.4	11.6	95	57	88	80	0.7	8.9	2.0	3.9	10	9	10	S 1	SW 5	NW 2
29	93.9	95.6	97.2	95.6	11.2	15.6	9.0	11.2	16.9	9.0	91	70	95	85	1.2	5.3	0.7	2.4	9	8 ⊙	0	SW 3	NNW 3	C 0
30	98.0	98.1	97.7	97.9	11.4	17.1	10.7	12.3	17.3	7.7	88	54	94	79	1.7	9.0	0.9	3.9	9	6 ⊙	0	NW 1	NW 4	SW 1
31	96.8	95.2	94.6	95.5	9.5	19.2	11.2	12.8	19.9	6.3	92	44	94	77	1.0	12.3	0.8	4.7	9	9 ⊙	6	SW 2	SW 7	SE 2
M	92.8	92.5	92.3	92.5	13.8	20.3	14.9	16.0	22.2	10.9	88	59	88	78	2.0	10.2	2.1	4.8	5.9	6.5	4.5	1.3	3.3	0.7

Racibórz $H_s = 189\ m$ $H_b = 196{,}1\ m$ $h_w = 15\ m$ Lipiec – Juillet 1957

DNI	WIATR KIERUNEK	WIATR SIŁA	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	•	•	-		= 715–1029 ∞–1140, ⌒² n–a
2	7	22.2	.	-		(K) 0 1330–1430 NW ●K 0 1430–1530–1830 NW-SE (K) 0–1920 SE ●K 0–1940 E (K) 0–2107 NW ●K 0 2108–2320 NW-NE,
3	8	.	.	-		= 000–530, ⌒² n–a [2.VII: = 425–910 ∞–1030 = p–24, ⌒ n–a
4	7	.	.	-		= 430–1030 ∞–1220, 2310–24, ⌒² n–a
5	8	2.5	.	-		(K) 1 2315–55 NW-E–NE K 1–24 NE-E ● n, = 000–940
6	8	6.2	.	-		(K) 1 000–18 NE-E, = 435–820 2205–24, ⌒² n–a
7	8	3.8	.	-		(K) 0 400–520 W–NE ●K 1 520–55–730 NE-E K 0 745–950 W-SE, = 000–815
8	7	19.0	.	-		●K 0 2020–2120 W-E (K) 0–2205 E < 2340–24 N, = 310–930 ∞–1220, ⌒² n
9	8	0.0	.	-		(K) 0 020–230 N–E ●K 1–420 E-SE ▽ 1832–40, = 540–825
10	7	6.9	.	-		(K) 0 1720–45 S–N ●K 0–1935 N-W ▽ 1935–2000, = 520–1215, 2000–24, ⌒² n–a
11	6	0.0	.	-		(K) 0 2125–2240 S-E, = 000–1540, 2135–24, ⌒² n–a
12	7	0.0	.	-		● 0 742–830 945–1120, = 000–1210, 1915–24, ⌒ 1 n
13	7	.	.	-		= 000–1035, ⌒² n–a
14	7	6.3	.	-		▽ 1409–14 ●K 0 1414–1630 W–NE ● 0–1715, = 415–1020 ∞–1225 = 1715–24, ⌒ 0 a
15	7	4.0	.	-		● 0 720–838, 935–1220, = 000–1247
16	6	30.3	.	-		● 0 442–715 ● 1–1245 ● 0 1308–1840 ● 1–24
17	7	3.1	.	-		● 1 000–335 ● 0–612 ● 1 745–1120 ▽ 1808–25
18	8	.	.	-		= 2110–24, ⌒² n–a, p–24
19	7	.	.	-		= 000–1145, ⌒² 000–a
20	8	25.3	.	-		▽ 1813–40 ●–2015 ● 0–2110, (K) 0 1420–50 S–NE K–1540 NE–NW (K) 0–1630 NW K 0 1840–2015, = 2110–24
21	7	0.0	.	-		● 0 820–42, = 000–40 = – 345 = –715, 2230–24, ⌒² a–24
22	7	11.5	.	-		▽ 2028–40, 2202–08, = 000–940, ⌒² 000–na
23	7	5.0	.	-		● 0 418–508 ● 1–650 ● 0–742 ● 1–810 ● 0–1235
24	7	3.0	.	-		● 0 415–605 ● 1–640 ● 0–740 ● 1–910 ▽ 1018–30, = 2330–24
25	7	13.4	.	-		▽ 1951–2015 2040–2100, 2140–2206 ● 1 2230 24, = 000–1310, ⌒ 1 n–1315
26	8	4.4	.	-		● 1 000 120 ▽ 1548–1835 ● 0–1925 ● 1–2245, = 120–610
27	8	3.9	.	-		● 0 1035–1140, 1215–1338, 2018–2225 ● 1–24
28	8	0.3	.	-		● 1 000–110 ▽ 1141–1212
29	8	0.7	.	-		▽ 1810–15, ⌒ 1813–24
30	7	0.6	.	-		▽ 1835–1930, = 430–930, ⌒² n–a
31	8	0.0	.	-		● 0 1025–32
Σ	÷	192.8	–	-	UWAGI	

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1	8	.	.	-	= 2230–24, ⌒² 2110–24
2	7	.	.	-	= 000–1735, ⌒² 000–a
3	8	.	.	-	⌒ 1 n,a
4	8	.	.	-	= 2015–24, ⌒² n,a
5	8	.	.	-	= 000–915, ⌒² n–a
6	8	.	.	-	∞ 915–1220 = 2025–24, ⌒² n–a
7	7	1.0	.	-	● 0 1435–1506 ▽ 1718–1817, 2105–50, = 000–1015 ∞–1330 = 2230–24, ⌒² n–a
8	7	.	.	-	= 000–835, ⌒² n–a
9	7	.	.	-	= 240–1030 ∞–1140, ⌒² n–a
10	8	14.6	.	-	● 1 827–50 ● 2–902 ● 1–1025 ● 0–1115 ▽ 1838–47, 1905–30, = 520–1040, ⌒² n–a; ⌒ 2 1923–45
11	8	.	.	-	⌒ 0 n–a
12	7	.	.	-	⌒² n–a
13	8	7.0	.	-	▽ 2217–40 < 2225–40 K 1 2240–24 W, ⌒² n–a
14	7	13.0	.	-	● 1 1911–2014, K 0 000–210 W–NE K 1 340–400 420 SW-NE (K) –510 NE K 0 2014 2050–2142 SW-E, = 230–1150
15	7	.	.	-	⌒² n,a
16	7	6.0	.	-	▽ 1628–1738 ● 1–1850 ● 0 1951–2020, = 540–1025, 2020–24, ⌒² n,a
17	7	3.0	.	-	▽ 540–610 ● 0–730 ● 1–940 ● 0–1024 ▽ 1355–1405, 1653–1711, = 000–1020
18	8	0.0	.	-	▽ 1510–18 1930–45
19	7	0.0	.	-	● 0 1910–35, = 1935–24
20	7	.	.	-	= 000–944, ⌒² n–a ⌒ 1 2050–24
21	7	3.8	.	-	= 445–1030 ∞–1340 ⌒² 000–a
22	7	1.9	.	-	● 0 445–1030 ▽ 1503–10, 1855–1905 2025–40, = 2040–24
23	7	.	.	-	= 000–920, ⌒² n–a ⌒ 1 2045–24
24	8	7.3	.	-	▽ 1910–55 2006–45 = 620–920, ⌒ 1 n–a, ⌒ 1940–50
25	7	.	.	-	= 340–525 ≡ 2–830, ⌒² n–a
26	8	.	.	-	⌒² n–a ⌒ 1 2045–24
27	8	3.7	.	-	● 1 2120–24, ⌒ 1 n–a
28	7	3.3	.	-	● 1 000–420
29	7	1.0	.	-	▽ 030–50 ● 0–345, = 345–1235, 2130–24
30	8	.	.	-	▽ 735–40 = 000–24
31	7	3.3	.	-	▽ 0 1540–43 ▽ 1 1645–2000 ● 0–2120, K 0 1630–1850 SW-E, = 425–1140, 2120–24, ⌒² n
Σ	–	71.9	–	-	UWAGI.

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$ Wrzesień–Septembre 1957

DNI	CIŚNIENIE P=900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.5	96.0	96.7	96.1	10.8	15.9	10.0	11.7	18.4	9.0	89	62	92	81	1.5	6.8	1.0	3.1	1 ⊙	8	1	SW 1	W 1	C 0
2	96.0	94.5	93.2	94.6	10.3	19.3	13.8	14.3	20.6	7.4	94	65	95	84	0.8	7.8	1.1	3.2	4 ⊙	10	10 ●	SSE 2	SSW 2	SW 1
3	92.5	93.2	93.7	93.1	12.7	17.3	15.7	14.4	18.0	12.0	95	70	92	86	0.7	5.8	1.3	2.6	9	8	10 ●	SSE 1	WNW 3	C 0
4	93.0	97.8	99.6	97.5	11.7	13.9	12.3	12.6	14.6	11.6	94	84	96	91	0.8	2.5	0.5	1.3	10 ●	10	10	N 3	N 3	N 1
5	99.7	97.7	96.9	98.1	11.7	18.0	10.3	12.6	18.9	10.3	90	65	95	83	1.3	7.1	0.6	3.0	10	7 ⊙	0	N 1	NE 1	C 0
6	95.8	95.6	95.7	95.7	10.9	20.1	14.4	15.0	21.5	8.6	95	59	95	83	0.6	9.6	0.7	3.6	5	7 ⊙	9	E 1	ENE 2	C 0
7	97.4	96.7	96.8	97.0	11.0	23.7	14.2	15.8	24.5	10.2	100	51	92	81	0.0	14.5	1.3	5.3	10 ≡	0 ⊙	0	C 0	SE 2	C 0
8	98.1	98.3	98.2	98.2	13.6	25.9	18.3	19.0	26.2	10.9	95	49	80	74	1.1	17.1	4.2	7.5	5 ⊙	1 ⊙	0	SE 2	SSE 3	C 0
9	98.6	98.3	99.5	98.8	13.2	26.2	17.8	18.8	27.1	10.0	96	47	78	74	0.6	18.0	4.4	7.7	0 ⊙	5 ⊙	9	C 0	S 3	NNW 4
10	100.0	98.4	96.4	98.3	13.8	16.8	11.2	13.2	18.2	11.0	93	78	94	89	0.7	4.2	0.8	1.9	10 ●	10	3	NNW 2	NNW 3	C 0
11	92.7	88.1	82.8	87.9	11.1	20.0	15.0	15.3	21.3	9.3	99	60	90	85	0.2	9.4	1.6	3.7	10 ≡	7 ⊙	10 ●	SSE 2	SSW 3	SSE 1
12	77.4	78.4	84.5	80.1	17.2	17.5	11.1	14.2	22.7	11.1	79	78	74	77	4.1	4.4	3.4	4.0	6 ⊙	10 ●	0	S 3	SW 6	SW 1
13	87.6	86.3	84.2	86.0	10.2	16.0	10.7	11.9	17.1	7.3	75	53	76	68	3.1	8.6	3.1	4.9	4 ⊙	8	8	S 2	SSW 4	SSW 6
14	86.6	85.7	85.9	86.1	9.1	15.3	9.9	11.0	17.2	8.0	76	47	91	71	2.8	9.2	1.1	4.4	1 ⊙	8	10 ●	S 3	SSW 3	C 0
15	85.4	87.5	92.5	88.5	8.1	13.3	10.5	10.6	15.1	7.7	76	69	84	76	2.5	4.9	2.1	3.2	9	8	9	SW 2	SW 3	SW 1
16	94.0	94.3	96.0	94.8	8.2	12.3	8.0	9.2	14.4	6.5	82	62	90	78	2.0	5.3	1.0	2.8	4 ⊙	9	10	SW 2	WSW 4	SSW 2
17	95.6	94.3	92.9	94.3	7.3	13.0	9.4	9.8	13.7	4.8	94	64	84	81	0.6	5.4	1.9	2.6	10 ●	8	10	SSE 2	WSW 2	C 0
18	91.5	91.6	92.1	91.7	9.0	13.4	7.7	9.4	15.5	7.5	93	65	94	84	0.8	5.3	0.6	2.2	9	3 ⊙	0	W 3	WNW 3	C 0
19	90.3	88.3	86.6	88.5	7.2	12.1	14.1	11.9	14.3	5.5	91	90	87	89	0.9	1.4	2.2	1.5	3 ⊙	10 ●	10	NW 1	SSW 2	SW 3
20	87.1	90.2	92.6	90.0	11.6	14.2	9.1	11.0	15.8	9.1	96	71	93	87	0.5	4.8	0.8	2.0	10 ●	6 ⊙	3	SW 1	NW 3	C 0
21	95.3	93.0	91.8	92.8	7.0	18.1	11.2	11.9	18.4	6.9	98	54	92	81	0.1	9.3	1.0	3.5	4 ≡	8 ⊙	0	C 0	SSE 2	C 0
22	89.4	89.6	89.9	89.6	12.4	16.1	13.9	14.1	18.7	9.5	90	90	94	91	1.4	1.7	0.9	1.3	9	9	0	SSE 1	S 1	C 0
23	85.4	81.3	81.6	82.8	15.2	17.6	15.3	15.8	19.1	10.7	94	86	84	88	1.0	2.8	2.8	2.2	6 ⊙	10 ●	10 ●	S 1	SSW 7	WSW 3
24	85.3	83.1	89.4	86.0	14.7	17.1	7.0	11.4	19.3	7.0	77	73	84	78	3.8	5.3	1.6	3.6	9	9 ●	10	SW 3	SW 4	NW 1
25	94.1	95.6	97.0	95.6	3.7	11.9	4.2	6.0	12.6	2.1	93	46	93	77	0.6	7.3	0.3	2.9	1 ⊙	4 ⊙	6	C 0	NW 4	C 0
26	94.2	93.3	95.4	94.3	2.7	8.2	5.5	5.5	9.3	1.4	98	74	94	89	0.1	2.9	0.3	1.2	9 ≡	10 ●	2	N 1	C 0	N 1
27	97.9	96.8	90.3	95.0	2.7	11.0	8.5	7.7	12.8	-0.6	88	44	77	70	0.9	7.3	2.6	3.6	5 ⊙	3 ⊙	10	NNW 3	NW 2	SW 3
28	87.3	87.6	88.1	87.7	9.5	13.7	9.7	10.6	14.6	8.5	86	66	84	79	1.7	5.4	1.9	3.0	9	9	2	SW 3	W 4	NW 1
29	84.8	81.5	79.2	81.8	9.7	11.3	8.7	9.6	12.4	8.3	88	86	94	89	1.4	1.8	0.6	1.3	10 ●	10 ●	10 ●	S 2	SW 3	NW 2
30	84.8	87.7	92.6	88.4	5.3	11.9	6.2	7.4	12.9	4.8	89	46	86	74	1.0	7.3	1.3	3.3	3	6 ⊙	10	NW 2	NW 4	C 0
31																								
M	91.8	91.4	91.7	91.6	10.1	16.0	11.1	12.1	17.5	7.9	90	65	88	81	1.3	6.8	1.6	3.2	6.5	7.4	6.1	1.8	3.2	1.0

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1	94.0	94.3	96.8	95.0	2.7	12.3	3.6	5.6	12.9	1.4	98	50	97	82	0.1	7.1	0.3	2.5	9	6	2	C 0	W 2	C 0
2	101.2	101.2	100.8	101.1	0.7	8.8	2.7	3.7	10.6	-0.9	96	62	98	85	0.2	4.3	0.1	1.5	7 ⊙	4 ⊙	9	C 0	NW 2	C 0
3	97.1	93.6	91.4	94.0	0.2	13.3	9.0	7.9	14.2	0.0	98	41	72	70	0.1	9.1	3.2	4.1	2 ⊙	2 ⊙	7	S 1	SW 3	SSW 2
4	92.0	94.8	100.5	95.8	6.8	9.3	2.2	5.1	10.7	2.2	87	66	91	81	1.3	4.0	0.7	2.0	10	4 ⊙	0	NW 2	WNW 5	C 0
5	102.5	101.0	99.8	101.1	3.6	13.1	5.6	7.0	13.6	1.1	91	46	78	72	0.7	8.1	2.0	3.6	9	3 ⊙	4	WSW 1	SW 3	S 1
6	98.9	100.2	103.5	100.9	6.4	11.5	8.9	8.9	13.2	3.3	76	69	93	79	2.3	4.3	0.8	2.4	9 ●	10 ●	9	S 2	SSE 1	C 0
7	103.5	103.0	103.2	103.2	4.6	15.8	7.8	9.0	17.7	2.9	97	57	99	84	0.3	7.6	0.2	2.7	0 ⊙	9 ⊙	0	C 0	SW 1	C 0
8	104.4	104.6	104.9	104.6	8.9	16.7	9.6	11.2	17.7	5.0	97	63	91	84	0.3	7.0	1.2	2.8	9	3 ⊙	0	NE 1	E 2	SE 1
9	103.7	102.1	101.4	102.4	4.6	18.7	8.5	10.1	19.5	4.6	100	52	96	83	0.0	10.4	0.5	3.6	10 ≡	0 ⊙	0	SE 2	SSE 2	C 0
10	100.7	99.6	99.7	100.0	5.7	19.8	11.4	12.1	20.2	5.1	94	51	77	74	0.6	11.4	3.1	5.0	0 ⊙	0 ⊙	0	C 0	SSW 4	SW 1
11	100.0	99.1	99.0	99.4	6.3	18.6	8.3	10.4	19.1	4.1	95	41	86	74	0.4	12.6	1.6	4.9	1 ⊙	2 ⊙	0	C 0	SW 2	C 0
12	98.8	99.6	103.7	100.7	7.3	16.3	13.4	12.6	17.5	4.7	90	64	88	81	1.0	6.8	1.8	3.2	2 ⊙	8	8	SW 1	SW 3	W 1
13	104.9	103.6	102.0	103.5	9.3	18.1	8.2	11.0	18.4	8.1	100	55	94	83	0.0	9.4	0.6	3.3	10 ≡	3	0	W 1	SE 2	C 0
14	101.3	100.8	102.7	101.7	6.1	18.2	12.2	12.2	18.9	6.0	100	54	87	80	0.0	9.7	1.9	3.9	10 ≡	3 ⊙	10	C 0	W 1	NNW 3
15	105.6	105.1	104.8	105.2	7.0	10.2	5.5	7.0	13.4	3.5	100	85	97	95	0.0	2.0	0.3	0.8	10 ≡	6 ⊙	0	NE 1	NE 1	C 0
16	103.1	100.2	98.6	100.6	3.4	14.3	9.8	9.3	17.9	1.8	100	72	87	86	0.0	4.6	1.6	2.1	10 ≡	1 ⊙	0	C 0	ESE 1	S 1
17	97.0	97.2	98.5	97.6	7.8	17.4	11.0	11.8	18.3	7.4	90	58	87	78	1.1	8.4	1.6	3.7	2	7 ⊙	10	S 1	SW 4	C 0
18	94.5	92.8	91.8	93.0	12.5	16.6	12.8	13.7	18.9	10.9	85	64	79	75	2.4	6.8	3.1	4.1	8	8	0	SW 1	SSW 2	SSW 3
19	90.6	88.4	87.0	88.7	7.0	20.1	12.4	13.0	20.6	5.9	93	48	80	73	0.7	12.2	2.4	5.1	7 ⊙	5 ⊙	0	SSW 1	SW 3	SW 1
20	88.2	91.4	94.6	91.4	10.0	9.0	7.8	8.6	12.9	7.8	92	96	97	95	1.0	0.5	0.3	0.6	7	10 ●	10	NW 4	N 2	C 0
21	95.0	93.2	90.3	92.8	7.7	12.3	4.0	7.0	13.4	4.0	96	64	95	85	0.5	4.8	0.4	1.9	10	3 ⊙	0	N 1	SE 1	C 0
22	84.8	82.1	81.1	82.7	5.9	8.7	9.0	8.2	10.3	2.9	95	88	96	93	0.5	1.3	0.5	0.8	10	10	10	SE 1	SE 1	SE 1
23	85.0	88.8	93.4	89.1	7.3	9.0	6.7	7.4	11.0	5.7	88	80	94	87	1.2	2.3	0.6	1.4	9	10	10	NNW 2	NW 4	C 0
24	94.4	95.0	99.7	96.4	1.5	9.5	8.2	6.8	11.0	1.5	87	69	95	83	0.9	3.7	0.8	1.8	3 ⊙	10	10 ●	SE 1	SE 3	SSW 1
25	102.5	102.8	102.8	102.7	7.4	13.9	3.4	7.0	14.2	3.4	97	55	99	82	0.3	7.2	0.4	2.6	9	3 ⊙	0	C 0	SSE 2	SSE 1
26	101.7	100.6	99.7	100.7	0.8	14.7	5.3	6.5	15.4	0.1	100	59	92	84	0.0	5.9	0.7	2.5	10 ≡	2 ⊙	0	SE 1	SW 2	C 0
27	98.2	97.2	96.5	97.3	8.9	13.0	9.6	10.5	18.4	2.2	92	74	86	84	0.9	4.0	1.8	2.2	9	10	0	SW 1	S 3	S 1
28	97.3	97.7	97.9	97.6	9.3	11.3	6.6	8.4	13.2	6.3	89	80	84	84	1.3	2.6	1.3	1.8	6	10	0	S 1	SW 1	SW 1
29	98.0	97.4	96.7	97.4	3.8	14.5	6.3	7.7	15.3	1.2	92	60	92	81	0.7	6.7	0.7	2.7	3	4 ⊙	2	SW 1	S 3	S 1
30	95.2	95.4	95.7	94.1	7.1	15.3	8.4	9.8	17.0	6.2	87	54	86	76	1.3	8.1	1.3	3.6	8	7	6	SSE 2	SW 3	C 0
31	93.7	92.3	90.7	92.2	7.0	16.1	8.6	10.1	16.4	6.6	91	57	86	78	0.9	7.9	1.6	3.5	1	4 ⊙	0	SSE 1	SW 4	SSW 1
M	97.7	97.2	97.7	97.5	6.1	14.1	8.0	9.0	15.5	4.1	93	62	90	82	0.7	6.5	1.2	2.8	6.8	5.6	3.5	1.0	2.4	0.7

Racibórz $H_s = 189$ m $H_b = 196{,}1$ m $h_w = 15$ m **Wrzesień – Septembre 1957**

DNI	WIATR	OPAD	GRUB. ŚNIEGU	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–6²⁵ ⌓² n–a
2	7	26.4	.	–	▽ 19³⁵–40 ⛈ 0 19⁴⁰–20⁰⁵ W–NE ● 1 20³⁵–21⁰⁵ ● 1 17–21²⁵ E–NW ● 1 –24; = 3²⁵–10²⁰ ∞ –12²⁰ ⌓² n–a
3	7	0.9	.	–	● 1 0⁰⁰–4⁰⁰ ● 0 5⁴⁰–6¹⁸ 19⁴⁴–22⁴⁰ ● 0 –24
4	7	3.0	.	–	● 0 0⁰⁰–1¹⁰ ● 0 4⁴⁰–12²⁵, 15⁰⁴–18⁴⁷, 19⁰⁸–21²⁰; = 1¹⁰–12¹⁰, 22⁴⁰–24
5	8	.	.	–	= 0⁰⁰–9¹⁰ ⌓⁰ na
6	7	.	.	–	= 0⁰⁰–10³⁰ ∞ –13²⁵ = 20²³–24; ⌓² n a
7	6	.	.	–	= 0⁰⁰–2²⁵ ≡ 1 –10⁵⁰ = –11¹⁵ ∞ –14²⁵, ⌓² n–a
8	6	.	.	–	= 4³⁵–10¹⁵, ⌓² n–a
9	8	8.0	.	–	= 5³⁰–9²⁰, 22¹⁷–24; ⌓² n–a
10	7	0.2	.	–	● 0 3¹⁰–6³⁵, 7³⁰–8¹⁵, ● 1 –9²⁶ ● 0 –11³⁵ = 0⁰⁰–12¹², 22⁴⁴–24
11	7	7.1	.	–	● 0 4⁴⁰–5¹⁵ ● 0 18⁰⁵–21¹² ● 1 –23³⁵ ● 0 –24; = 0⁰⁰–5⁴⁰ ≡ 1 –10²⁰ = –11¹⁸
12	8	1.0	.	–	▽ 8¹⁶–23, 13⁰²–07, 13¹⁴–14³⁷
13	6	.	.	–	⌓² n–a
14	9	14.9	.	–	● 0 17³³–18⁴⁰, 19²⁵–22¹⁰; ⌓⁰ n
15	8	.	.	–	● 1 2⁵⁰–3³⁵ ● 2 –4²⁰ ● 1 –6³²
16	8	3.3	.	–	▽ 19²²–20¹², ⛈ 0 20¹²–54 NE–E; = 5³⁰–7¹⁰
17	7	0.7	.	–	▽ 6²¹–7¹⁰ ● 0 –8¹⁶
18	8	2.6	.	–	● 1 4⁴⁰–6¹⁰ ▽ 7¹⁴–50, 8¹⁵–9²⁰
19	6	2.3	.	–	● 0 11³²–12²⁰ ● 1 12³⁰–15¹⁵ ● 0 17⁰⁴–17; = 1¹⁰–9⁴⁰; ⌓² n
20	8	2.4	.	–	● 0 5¹⁰–6⁰⁸ ● 1 7¹⁷–10⁴²; = 5⁰⁸–10⁴⁵
21	7	.	.	–	= 5¹⁵–7²⁵ ≡ 1 –9⁵⁴ = –11²⁵ 20¹⁰–24; ⌓² n a; ⊕ 0 13⁴⁰–14¹⁸
22	7	4.2	.	–	● 1 8⁰⁵–10¹⁶ ● 0 –11⁰⁴ ● 1 –11²¹ ● 0 –13³⁵, 15⁴⁵–16²⁰; = 0⁰⁰–13⁴⁰, ⌓² n
23	7	3.3	.	–	● 0 9³⁰–12⁴⁰ ▽ 13¹⁰–19 13⁴⁰–14²⁹, 16²⁵–45 21⁵⁰–22¹⁰ 22⁴⁰–24; ⌓² n–a
24	8	8.0	.	–	▽ 13²⁴–40, 13⁵⁴–14⁰⁶, 14²⁵–15⁰⁴ ● 1 15¹⁶–16⁵⁰ ● 0 17⁴¹–19⁰⁶ ● 1 –21²⁰; ⊕ 0 9⁴⁰–10¹⁰
25	9	.	.	–	⌴ n–a
26	6	0.1	.	–	● 0 12⁰⁰–14³⁰ = 6⁴⁰–7²⁴ ≡ 1 –8²⁵; ⌴⁰ n,a
27	8	0.7	.	–	● 0 20²⁶–21¹⁴ ⌴¹ n–a
28	8	2.0	.	–	▽ 10³–20 ● 0 20⁶–3⁴⁰ ▽ 11¹²–54 12²¹–27 13⁴⁶–14⁰⁵ 16³⁵–50 17⁴⁰–18¹⁴ 21²⁵–33
29	6	8.2	.	–	▽ 1⁰⁰–35 ● 0 6⁰⁶–8²⁵, 11⁰⁴–13²⁵ ▽ 16⁴⁰–18¹⁰ ● 0 20²²–21⁴⁵ ● 1 –22⁵² ● 0 –24
30	8	.	.	–	● 0 0⁰⁰–1⁴⁰
31					
Σ	–	99.3	–	–	UWAGI.

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1	8	.	.	–	= 3¹⁵–9¹⁵; ⌓⁰ n–a
2	7	.	.	–	= 3²⁵–9¹⁶, 17¹⁰–24; ⌴² n–a
3	8	0.2	.	–	= 0⁰⁰–11³⁰ ⌴¹ n, a
4	8	0.3	.	–	▽ 5¹⁰–40, 11⁰⁸–17, 12¹²–24, 14⁰⁸–25, 15¹⁰–22; ⌴¹ n, ⌒⁰ 15¹⁷–24
5	8	0.0	.	–	⌴⁰ n, a
6	7	0.0	.	–	● 0 6¹²–8²³ ▽ 12³⁴–13⁰⁰; = 16³¹–24
7	7	.	.	–	= 0⁰⁰–10⁵⁰ 18²⁵–24; ⌓² n, a
8	7	.	.	–	= 0⁰⁰–12²⁵, 22⁴⁵–24; ⌓² n, a
9	7	.	.	–	= 0⁰⁰–2⁵⁸ ≡ 2 –7⁴⁰ = –11¹⁸, 18⁴⁰–24
10	8	.	.	–	= 0⁰⁰–9⁰⁰; ⌓² n
11	8	.	.	–	= 6¹⁰–9⁵⁵ ⌴⁰ n
12	8	.	.	–	= 5³⁵–9¹⁰; 16²⁴–24; ⌓² n, a ⌓⁰ n; ⊕ 0 11¹²–40
13	7	.	.	–	= 0⁰⁰–3⁵⁶ ≡ 0 –6³⁵ ≡ 2 –7¹⁰ ≡ 1 –9⁴⁸ = –11²⁰; ⌓² n, a
14	8	.	.	–	= 3³⁵–5⁵¹ ≡ 1 –8⁴⁵ = –11¹⁵, 17⁰⁵–20²⁰, ⌓² n, a
15	5	.	.	–	= 3²⁰–6⁰⁸ ≡ 0 –6²⁰ ≡ 1 –10⁴⁵ = –24, ⌓¹ n–a, p
16	5	.	.	–	= 0⁰⁰–1⁴⁵ ≡ 2 –10²⁵ ≡ 1 –11³⁰ = –13⁴⁵, 17¹⁵–24, ⌓² n–a ⌓¹ p
17	7	.	.	–	= 0⁰⁰–8³⁰
18	7	0.0	.	–	● 0 10¹⁵–11⁵²; = 3³⁰–9⁵⁰, 20³⁵–21⁴⁰; ⌓⁰ n–a
19	8	.	.	–	= 21⁵⁰–24; ⌓⁰ n–a
20	6	4.9	.	–	● 2 10⁴²–14¹⁰ ● 0 –19¹⁰; = 0⁰⁰–24, ⌓¹ n–a
21	7	.	.	–	= 0⁰⁰–12⁴⁰ 17¹⁰–23¹⁰ ≡ 2 –24; ⌓¹ n–n
22	5	0.8	.	–	● 0 7¹⁰–35 ● 0 21³⁵–22⁰⁵ ● 1 –24; ≡ 2 0⁰⁰–5²⁰ = –24; ⌓² n–a
23	7	.	.	–	● 1 0⁰⁰–1²² 2³⁸–3¹⁷; = 0⁰⁰–2⁴⁵ ≡ 2 –5²³ = –12¹⁰, 18²⁵–24
24	7	0.0	.	–	▽ 0 16²⁷–31 ● 0 18¹⁷–19¹⁰ ● 0 20⁰⁴–21³⁶; = 0⁰⁰–8⁴⁵, 21³⁶–24, ⌴⁰ n, a
25	7	.	.	–	= 0⁰⁰–12³⁸ 20²²–24; ⌓ n ⌴ n
26	8	.	.	–	= 0⁰⁰–40 ≡ 0 –12¹ ≡ 1 –23⁰ ≡ 2 –8¹⁰ = –11⁰⁸; ⌴² n–7¹⁵
27	7	.	.	–	= 4¹⁵–10³⁰, 19⁴⁰–24; ⌓¹ n, a
28	6	.	.	–	= 0⁰⁰–24; ⌓⁰ n–a
29	7	.	.	–	= 0⁰⁰–9²⁵; ⌴¹ n–a
30	7	.	.	–	= 5⁴⁰–9⁵⁰, 17³⁰–24; ⌴⁰ n, a
31	8	.	.	–	= 0⁰⁰–9²⁵, 20³²–24; ⌓¹ n–a
Σ	–	6.2	–	–	UWAGI.

Racibórz $\varphi = 50°05'$ $\lambda = 18°13'$ **Listopad – Novembre 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	86.8	86.0	88.2	87.0	5.2	14.1	7.3	8.9	15.2	3.0	95	65	95	84	0.4	5.6	0.7	2.2	0	1 ⊙	2	SSE 1	W 3	C 0
2	89.3	89.9	90.5	89.9	7.3	12.2	9.6	9.7	13.1	4.6	100	79	86	88	0.0	3.0	1.8	1.6	10 ≡	9	10 •	C 0	SSE 1	NW 2
3	92.4	91.4	90.6	91.5	7.6	11.0	9.2	9.2	12.9	7.4	96	85	96	92	0.4	1.9	0.4	0.9	9	9	9	C 0	N 1	C 0
4	90.6	89.7	91.1	90.5	6.3	16.6	6.1	8.8	17.4	5.7	100	60	94	85	0.0	7.5	0.6	2.7	9 ≡	1 ⊙	1	ESE 1	SW 2	S 1
5	87.4	84.9	85.4	85.9	3.7	18.4	13.4	12.2	18.7	3.2	97	45	67	70	0.3	11.6	5.2	5.7	0	3 ⊙	9	C 0	S 7	SE 1
6	86.1	86.1	84.8	85.7	9.9	16.5	12.2	12.7	17.0	9.0	81	56	73	70	2.4	8.4	3.8	4.9	5	6 ⊙	2	SSE 2	S 4	SE 1
7	83.2	84.7	85.5	84.5	7.0	14.2	12.5	11.4	14.7	6.8	90	67	81	79	1.0	5.3	2.7	3.0	7	10	10 •	SE 1	SSW 2	C 0
8	83.5	83.6	82.9	83.0	8.2	15.8	10.0	11.0	17.0	7.0	90	63	89	81	1.1	6.6	1.3	3.0	8	7	6	C 0	SE 1	C 0
9	82.0	82.8	85.6	83.5	9.3	12.7	11.5	11.2	13.7	7.9	97	86	89	91	0.3	2.1	1.5	1.3	10 •	8 •	10	C 0	SE 1	C 0
10	86.3	85.5	86.2	86.0	2.6	17.2	9.9	9.9	17.5	2.4	95	50	86	77	0.4	9.9	1.8	4.0	0 ≡	2 ⊙	8	SE 1	SE 2	S 3
11	87.1	88.2	91.1	88.8	7.6	10.7	7.4	8.3	11.2	6.4	96	74	94	88	0.4	3.4	0.6	1.5	10 •	10	10 ●	NE 2	NE 4	NE 4
12	94.6	98.6	101.9	98.4	6.6	4.8	4.0	4.8	8.2	4.0	91	87	87	88	0.8	1.1	1.1	1.0	10 ●	10	10	NE 5	NE 4	NE 3
13	103.7	104.2	105.5	104.5	2.7	2.9	0.4	1.6	4.8	0.4	89	79	73	80	0.8	1.6	1.7	1.4	10	10	10	NE 3	NE 3	E 3
14	106.0	106.5	108.3	106.9	-0.8	0.3	-0.4	-0.3	1.1	-1.1	75	83	88	82	1.5	1.0	0.7	1.1	10	10	10	ENE 3	ENE 2	ENE 1
15	108.2	107.5	106.6	107.4	-1.0	0.3	-0.4	-0.4	1.4	-1.3	93	94	96	94	0.4	0.3	0.2	0.3	10 ≡	10	10 ═	SSE 2	SE 2	SE 1
16	106.3	106.7	107.3	106.8	0.8	4.9	3.7	3.3	5.4	-1.4	98	82	93	91	0.2	1.6	0.6	0.8	10 ≡	10	10	SE 1	S 2	S 1
17	106.9	106.6	107.9	107.1	2.2	4.6	2.6	3.0	5.0	2.1	96	89	86	90	0.3	1.0	1.1	0.8	10	10	10	C 0	S 1	E 2
18	108.0	107.4	107.7	107.7	2.1	3.1	2.3	2.4	3.9	2.1	85	83	91	86	1.0	1.3	0.6	1.0	10	10	10	E 2	E 1	C 0
19	107.9	109.0	111.1	109.3	1.7	2.2	1.4	1.7	2.8	1.4	90	73	76	80	0.6	2.0	1.7	1.4	10	9	10	C 0	E 2	E 2
20	112.5	113.4	114.7	113.5	0.4	4.2	-2.0	0.2	4.7	-2.0	75	53	82	70	1.6	3.8	1.0	2.1	10	0 ⊙	0	E 2	ESE 2	C 0
21	114.3	112.0	108.9	111.7	-4.8	4.7	-0.8	-0.4	6.5	-5.2	95	64	83	81	0.2	3.1	1.0	1.4	10 ≡	0 ⊙	0	C 0	ESE 2	SE 1
22	102.4	98.0	96.1	98.8	0.6	5.1	2.4	2.6	5.7	-3.0	71	54	68	64	1.9	4.1	2.4	2.8	0	2 ◯	10	S 3	S 6	SSW 4
23	96.5	96.3	99.3	97.4	1.6	3.0	3.7	3.0	4.5	1.5	78	69	72	73	1.6	2.4	2.3	2.1	10	10	10	SW 4	SW 3	W 2
24	102.1	102.2	101.3	101.9	1.7	6.0	4.4	4.1	6.6	1.0	87	53	79	73	0.9	4.5	1.8	2.4	10	8	10 •	WNW 1	NW 2	SW 2
25	99.4	99.2	100.3	99.6	4.6	5.1	4.8	4.8	5.9	4.2	81	95	94	90	1.7	0.4	0.6	0.9	10	10 ●	10 •	SW 1	SW 1	SW 1
26	101.6	101.8	100.4	101.3	5.2	6.7	6.0	6.0	7.3	4.1	97	94	91	94	0.2	0.6	0.9	0.6	10 •	10	10	C 0	S 1	SSW 1
27	97.6	96.8	97.5	97.3	4.4	7.3	6.8	6.3	8.1	4.1	90	80	84	85	0.9	2.0	1.6	1.5	10	10	10	SW 1	NW 2	WNW 1
28	95.5	93.3	89.3	92.7	7.0	8.8	7.7	7.8	9.2	5.8	87	82	79	83	1.3	2.0	2.2	1.8	10	10	10 •	SW 1	SW 2	SW 4
29	86.0	89.1	99.2	91.4	5.4	1.7	-2.6	0.5	7.9	-2.7	81	92	61	78	1.7	0.3	2.0	1.4	9	9 △	3	WNW 4	NNW 6	N 8
30	105.1	105.1	105.5	105.2	-7.7	-5.8	-5.1	-5.4	-1.4	-8.6	64	51	63	59	1.2	2.3	1.5	1.7	2	6	9	N 7	N 7	N 4
31																								
M	97.0	96.9	97.7	97.2	3.6	7.7	4.9	5.3	8.9	2.3	89	73	83	82	0.8	3.4	1.5	1.9	8.0	7.3	8.0	1.6	2.6	1.8

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1	106.6	106.2	104.6	105.8	-8.7	-5.5	-5.6	-4.8	-3.1	-8.7	83	74	85	81	0.5	1.2	0.7	0.8	0	8 ✳	10	N 3	NNW 3	C 0
2	102.1	102.0	102.3	102.1	-2.8	-1.8	-1.5	-1.9	-0.7	-3.6	82	92	90	88	0.9	0.4	0.5	0.6	10	10 ●	10	C 0	C 0	NNE 1
3	99.2	96.7	97.0	97.6	-0.6	0.0	0.7	0.2	1.3	-1.5	91	92	94	92	0.5	0.5	0.4	0.5	10	10 ✳	10 ✳	N 3	C 0	N 2
4	100.1	100.1	100.5	100.2	-0.5	0.1	1.0	0.4	2.0	-0.5	90	96	94	93	0.6	0.3	0.4	0.4	10	10 ✳	10	E 1	SE 1	C 0
5	98.0	97.8	99.4	98.4	0.6	2.7	3.0	2.3	3.5	0.6	92	91	86	90	0.5	0.6	1.1	0.7	10 ✳	10	9	C 0	NW 5	NW 6
6	101.5	102.2	101.7	101.8	2.4	2.2	-1.7	0.3	3.8	-1.7	91	82	85	86	0.7	1.5	0.8	0.9	10	9	0	N 4	NNE 1	C 0
7	94.8	91.7	86.4	91.0	-3.4	1.6	0.5	-0.2	2.7	-3.9	88	66	79	78	0.6	2.4	1.3	1.4	2	2 ⊙	10	S 1	SW 4	SSW 7
8	74.0	67.6	62.2	67.9	1.6	1.5	5.6	3.6	6.0	-0.5	71	89	81	80	2.0	0.8	1.7	1.5	10 △	10 △	8	SW 8	SSW 7	S 5
9	61.2	67.5	76.5	68.4	5.3	5.3	1.0	3.2	7.2	1.0	75	63	77	72	2.2	3.3	1.5	2.3	9	3 ⊙	7	SW 5	NW 6	C 0
10	75.1	77.1	86.6	79.6	-0.5	0.3	-2.9	-1.3	2.6	-3.0	86	90	71	82	0.9	0.6	1.4	1.0	9	9	0	ESE 1	S 2	N 3
11	86.1	81.7	76.6	81.5	-7.8	0.6	-0.9	-2.2	1.7	-8.2	81	65	85	77	0.6	2.3	0.8	1.2	3	8	3	SE 1	E 1	C 0
12	74.3	74.2	73.4	74.0	0.3	9.3	6.6	5.7	10.3	-2.6	94	69	96	86	0.3	3.7	0.4	1.5	9	4 ⊙	0	S 1	S 1	C 0
13	70.4	67.9	60.2	66.2	8.0	12.3	10.3	10.2	13.4	1.3	79	66	67	71	2.2	4.8	4.1	3.7	8	10	10	SSW 1	S 3	SE 2
14	60.3	68.4	77.0	68.6	4.0	2.8	1.3	2.4	10.9	1.1	93	95	91	93	0.5	0.4	0.6	0.5	10	10 •	10	N 2	NNW 1	C 0
15	87.1	93.2	98.9	93.1	-1.4	-3.4	-4.4	-3.4	2.0	-4.4	92	85	93	90	0.4	0.7	0.3	0.5	10 ●	10	10	NNW 3	NNE 3	NE 4
16	102.4	101.3	102.2	102.0	-9.4	-5.2	-8.4	-7.8	-3.4	-10.0	85	63	83	77	0.4	1.5	0.9	0.8	0	0 ⊙	0	NE 3	NE 3	C 0
17	98.8	97.9	98.0	98.2	-6.6	-2.3	-3.4	-3.9	-1.1	-9.0	83	78	85	82	0.6	1.2	0.7	0.8	8	9	10	NNE 1	ESE 1	N 1
18	99.7	99.6	100.8	100.0	-4.5	-4.1	-4.1	-4.2	-2.7	-5.0	91	91	82	88	0.4	0.4	0.8	0.5	10	10 ≡	10	N 2	NNE 2	N 1
19	101.6	103.1	107.4	104.0	-2.9	-1.1	-0.3	-1.2	0.5	-4.4	88	89	82	86	0.5	0.6	1.1	0.7	10	10	10	SE 1	SE 2	SE 1
20	110.8	112.1	111.0	111.3	0.4	1.4	1.0	1.0	2.4	-0.5	89	91	88	89	0.7	0.7	0.8	0.7	10	10	0	SE 1	SSE 1	SSE 1
21	108.7	108.4	107.8	108.3	1.3	1.5	0.3	0.8	3.2	0.2	77	76	80	78	1.5	1.6	1.2	1.4	9	10	0	SSW 3	SW 5	S 3
22	105.8	105.6	104.0	105.1	-0.9	0.7	-1.3	-0.8	1.8	-1.6	87	78	82	82	0.7	1.4	1.0	1.0	0	8	8	S 3	S 3	WSW 2
23	99.7	98.3	97.4	98.5	-4.9	-1.8	-4.7	-4.0	-0.7	-6.2	81	63	79	74	0.8	2.0	0.9	1.2	0	2	0	SSW 2	SW 4	SSW 4
24	95.7	95.7	96.3	96.0	-4.8	-0.7	-2.0	-2.4	-0.3	-5.1	78	69	85	77	0.9	1.8	0.8	1.2	3	4 ⊙	4	S 4	SSW 4	SW 4
25	96.9	96.4	98.3	97.3	-0.6	4.2	0.4	1.1	5.3	-2.1	83	69	84	79	1.0	2.3	1.0	1.5	4	9	0	SW 2	SW 4	SW 2
26	101.0	102.3	104.9	102.8	-0.2	5.0	-2.3	0.0	5.6	-2.3	88	64	93	82	0.7	3.1	0.4	1.4	8	3 ⊙	0	SSW 2	S 2	SE 2
27	104.9	103.9	102.4	103.7	-2.8	2.3	-1.4	-0.8	3.0	-3.6	95	80	92	89	0.2	1.4	0.4	0.7	10 ═	0 ⊙	3	SSE 2	SE 2	SE 3
28	98.2	95.8	93.0	95.7	-3.9	-1.3	-2.2	-2.4	-0.3	-4.3	92	80	83	85	0.4	1.1	0.9	0.8	0	9	10	S 2	SW 4	SW 3
29	89.9	89.3	87.2	88.8	-0.8	0.3	1.1	0.4	2.3	-3.1	89	80	77	82	0.6	1.2	1.3	1.1	10 ✳	10	9	SSW 1	S 5	SW 4
30	83.2	80.8	79.3	81.2	2.2	2.9	3.0	2.8	4.2	0.4	73	71	71	72	2.0	2.2	2.2	2.1	8	6	4	SW 6	SW 6	SW 5
31	80.6	81.3	82.3	81.3	0.6	3.2	2.3	2.1	4.3	0.4	90	69	79	79	0.6	2.4	1.3	1.5	10	8	9	SW 1	WSW 2	SW 4
M	92.3	92.3	92.8	92.6	-1.3	1.1	-0.2	-0.2	2.8	-2.9	86	78	84	83	0.8	1.6	1.0	1.1	7.1	7.3	6.0	2.3	2.7	2.3

Racibórz $H_s = 189\ m$ $H_b = 196{,}1\ m$ $h_w = 15\ m$ **Listopad–Novembre 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–36 ≡⁰–4¹⁸ =–8¹⁷ ≡² 22³⁵–24 ⌴⁰ n
2	6	7.1		–	●⁰ 19²²–20¹³ ●⁰–20⁴³ ●⁰–23¹⁷; ≡² 0⁰⁰–10⁴⁵ =–24; ⌒¹ n–a
3	6	.	.	–	●⁰ 0³⁰–2³⁶; = 0⁰⁰–24
4	7	.	.	–	= 0⁰⁰–3³⁸ ≡²–6⁵³ ≡¹–8¹⁴ =–12⁰⁷, 17¹⁷–24
5	8	.	.	–	= 0⁰⁰–9¹⁶; ⌴⁰ n, a
6	8	.	.	–	= 20⁵⁰–24; ⌒ n–a
7	8	0.0	.	–	●⁰ 20⁴⁶–21¹²; = 0⁰⁰–8⁴⁰; ⌒¹ n,a
8	7	3.7	.	–	= 6⁴⁰–10³², 17⁵³–24; ⌒¹ n,a
9	5	1.2	.	–	●⁰ 0²⁷–7⁰⁰ 1¹⁶–2³⁹ 3¹³–40–9³³, 11²⁸–14¹⁸, 15¹⁰–18²⁰; = 0⁰⁰–24
10	8	0.2	.	–	= 0⁰⁰–1¹⁸ ≡²–7¹⁵ =–9¹⁹
11	6	1.7	.	–	●⁰ 4⁴⁰–5³⁵ 6²²–8⁰⁸ 10⁵²–11⁰⁵ ●¹ 16²⁴–24; = 4⁴⁰–13⁴¹, 17³⁵–24
12	6	1.0	.	–	●¹⁻² 0⁰⁰–7³⁹ ●⁰–10²⁷ ●¹ 22¹⁷–24; = 0⁰⁰–6¹⁵, 9²⁰–24
13	7	.	.	–	●⁰ 0⁰⁰–6⁰⁴; = 0⁰⁰–12¹³, 15²⁰–24
14	6	.	.	–	= 0⁰⁰–24
15	5	.	.	–	= 0⁰⁰–3⁴⁵ ≡²–7⁵⁰ ≡¹–12⁵⁰ =–15⁵⁴ ≡¹–20²⁸ ≡²–24
16	6	0.0	.	–	●⁰ 8³⁵–10⁰⁶; ≡² 0⁰⁰–5⁴⁵ ≡¹–8⁴⁸ =–24
17	4	.	.	–	= 0⁰⁰–7¹⁵ ≡¹–12²⁸ =–24; ⌒¹ n,a
18	5	.	.	–	= 0⁰⁰–24
19	5	0.0	.	–	●⁰ 14³⁵–15⁰⁶; = 0⁰⁰–24
20	7	.	.	–	= 0⁰⁰–10²⁴
21	5	.	.	–	≡² 5⁴⁰–8⁵⁵ ≡¹–9³⁸ ≡⁰–10⁴⁸ =–12¹⁵ ∞–18¹⁰ =–24; ⌴¹ n,a
22	8	.	.	–	= 0⁰⁰–6³², ⌴¹ n,a
23	7	.	.	–	
24	8	0.2	.	–	●¹ 20²⁸–21¹³
25	5	3.7	.	–	●⁰ 7⁴⁰–9¹⁷ 10¹⁴–12¹⁰ ●¹–16³⁵ ●⁰–19⁰⁸; = 0⁰⁰–24
26	5	0.6	.	–	●¹ 5¹⁰–50 ●⁰–7³⁰ ●⁰–8¹², 9⁴⁴–11⁷⁸, 17⁵⁰–18¹⁵, 20⁴⁸–21⁰³, 22³⁵–24; = 0⁰⁰–7⁴⁵ ≡⁰–11⁵⁰ =–24
27	6	0.0	.	–	●⁰ 0⁰⁰–18; = 0⁰⁰–24
28	6	4.0	.	–	●⁰ 1⁵⁵–4¹¹, 7⁴⁰–9⁰⁸ ●⁰–11¹⁴ 14³⁵–15⁰⁵, 20³⁶–24; = 0⁰⁰–24
29	7	4.0	.	–	●⁰ 0⁰⁰–2³⁵ ▽8¹²⁻²⁷, 8⁴²–9⁰⁴ ⚹ 11²⁸–45, 12⁰³–28 △ 12⁴¹–13¹¹ ✶⁰ 15⁰³–19¹⁵; ≫ 0⁰⁰–24⁰ NW ⫽ 8¹⁰⁻³⁰ NNW
30	8	.	pł.	–	
31					
Σ	–	27.4	–	–	UWAGI:

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1	8	0.0	pł.	–	✶⁰ 12²¹–15¹⁷; ⌴¹ n,a
2	6	0.4	pł.	–	✶⁰ 3⁴²–4³⁵ ●⁰ 9²⁶–14²⁵; = 8¹⁵–24
3	5	10.3	pł.	–	●¹ 8¹⁰–10¹⁶ ✶¹–12²⁷ ✶²–13³² ✶¹ 14⁴¹–16²³ ✱⁰ 17⁰²⁻³⁶ ✱¹ 18¹⁶–20²⁰ ✱⁰–24; = 0⁰⁰–24
4	5	6.0	5	–	●⁰ 0⁰⁰–4³⁵ ●⁰ 9⁴³–12⁰⁴ ✶⁰–13⁰³ ●⁰–17⁰⁹ 21¹⁵–24; = 0⁰⁰–18¹⁰, 21⁰⁶–24
5	5	3.4	4	–	●⁰ 1²⁰–2³⁹ 3¹²–5¹⁵ ✱¹ 6⁴⁸–7⁵⁵ ●⁰ 8⁰⁰–10²⁵; = 0⁰⁰–24
6	6	0.0	pł.	–	●⁰ 1¹³–2⁴¹; = 0⁰⁰–13²⁰
7	8	0.0	pł.	–	⌴² n,a
8	7	6.1	0	–	✶⁰ 3⁰⁷–6¹⁸ △–7⁴⁴ ⚹ 9⁰⁵⁻²⁰, 9³¹⁻⁴⁰ ●⁰ 11¹⁷–45 △–13¹⁶ ●¹–14⁴³ ▽¹ 15¹⁰⁻³⁹ ●⁰ 22²⁶ 24, ≫ 10³⁰–12¹⁵ SSW
9	8	0.1	.	–	●⁰ 0⁰⁰–25 ▽ 11²⁸–45
10	6	0.8	.	–	✶⁰ 7⁴⁴–10¹²; ✶¹–11³⁵; = 7¹⁰–15⁴⁵
11	6	.	0	–	∞ 12¹⁶–13⁴⁰ =–24
12	7	.	0	–	= 0⁰⁰–11⁴⁶, 17³⁰–24
13	8	1.6	.	–	= 0⁰⁰–9¹⁵
14	5	9.6	.	–	●⁰ 0¹⁰–2⁴⁶ ●⁰ 3¹¹–4⁴⁷ ●⁰ 7²⁴–12⁰⁵ ●¹–15⁰⁴ ●⁰–17¹⁸; = 13¹–20³⁰
15	6	0.0	.	–	●⁰ 6⁵⁰–11⁴³; 15³⁵–17⁰³; ∞ 10⁰⁰–24; = 6⁴⁵–24
16	7	.	.	–	= 0⁰⁰–5¹⁵; ≈ 0⁰⁰–8³⁰
17	5	.	.	–	= 3¹⁸–24; ⌴² n
18	5	.	.	–	= 0⁰⁰–7³⁶ ≡¹–13³⁵ =–24
19	5	.	.	–	= 0⁰⁰–24
20	5	0.0	.	–	●⁰ 7⁰⁷–10³⁵; = 0⁰⁰–24
21	7	.	.	–	= 0⁰⁰–6¹⁵
22	7	.	.	–	= 20⁴¹–24; ⌴⁰ n,a
23	8	.	.	–	= 0⁰⁰–8⁴⁶; ⌴¹ n,a
24	8	.	.	–	= 21²⁹–24; ⌴¹ n,a
25	7	.	.	–	= 0⁰⁰–8³⁷, 23³⁰–24; ⌴² n,a
26	7	.	.	–	= 0⁰⁰–9⁴⁰, 20⁴⁵–24; ⌴¹ n,a
27	5		.	–	= 0⁰⁰–6⁴⁰ ≡⁰–8⁴⁵ =–18³⁵; ⌴² n,a
28	7	1.2	.	–	= 20⁴¹–24; ⌴² n,a
29	6	0.0	1	–	✶⁰ 4¹⁶–7³²; = 0⁰⁰–9⁴⁵, 12³⁵–15²⁰
30	8	0.0	1	–	
31	7	.	pł.	–	▽⁰ 3¹⁸–32
Σ	–	39.5	–	–	UWAGI

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°57' — Styczeń – Janvier 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v					
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I		II		III	
1	89.3	88.8	88.2	88.8	0.0	2.1	0.9	1.0	2.9	−2.6	92	85	92	90	0.5	1.0	0.5	0.7	10 ⛆	2 ☉	10	C	0	C	0	NE	1
2	86.4	86.0	90.1	87.5	0.6	5.8	2.8	3.0	6.5	0.3	90	76	89	85	0.6	2.2	0.8	1.2	3	7 ☉	3	ENE	1	C	0	C	0
3	94.4	95.7	96.7	95.6	1.5	3.2	1.0	1.7	5.2	0.9	94	88	94	92	0.4	0.9	0.4	0.6	10	10	10 ≡	C	0	C	0	C	0
4	97.0	98.9	99.8	98.6	0.9	2.2	0.2	0.9	2.2	0.1	94	93	94	94	0.4	0.6	0.4	0.5	10 ● ≡	10	0 ≡	C	0	C	0	C	0
5	99.7	97.6	94.6	97.3	−5.2	3.2	2.8	0.9	3.5	−5.6	85	84	91	87	0.6	1.2	0.7	0.8	10 ≡	7 ☉	10 ●	C	0	C	0	C	0
6	92.6	88.4	88.8	89.9	4.2	7.2	6.6	6.2	8.9	2.2	97	87	91	92	0.2	1.4	0.8	0.8	10	10	10 ●	C	0	C	0	C	0
7	93.3	96.6	100.7	96.9	3.0	3.9	4.3	3.9	6.6	2.8	84	88	76	83	1.2	1.0	2.0	1.4	8	7 ●	10	W	5	W	4	W	4
8	103.4	101.1	101.0	101.8	3.7	5.5	5.1	4.8	6.0	3.3	78	71	76	75	1.8	2.6	2.1	2.2	10	8 ☉	10	W	2	W	3	W	2
9	99.3	97.3	94.1	96.9	5.5	6.6	3.4	4.7	6.9	3.4	81	81	85	82	1.7	1.8	1.2	1.6	10	10	0	C	0	C	0	W	1
10	90.1	87.4	88.8	88.8	2.6	6.2	1.4	2.9	6.2	0.0	84	56	94	78	1.2	4.2	0.4	1.9	9 ≡	9	10	C	0	W	1	W	1
11	89.7	91.8	93.9	91.8	1.7	1.6	1.0	1.3	1.9	0.4	76	76	83	78	1.6	1.7	1.2	1.5	10	7 ☉	10 ⛆	W	5	W	4	W	2
12	91.8	87.5	81.2	86.8	−0.4	1.2	1.5	1.0	1.5	−0.7	82	74	74	77	1.1	1.8	1.8	1.6	5	10	10	W	4	W	2	C	0
13	78.7	79.7	82.4	80.3	0.8	0.9	0.5	0.7	1.5	0.0	75	88	94	86	1.6	0.7	0.3	0.9	10	10 ✳	10 ✳	C	0	C	0	C	0
14	86.7	90.6	94.6	90.6	−1.1	−1.2	−4.5	−2.8	0.5	−4.7	95	86	88	90	0.3	0.8	0.5	0.5	10 ✳	4 ☉	10	C	0	C	0	NE	4
15	93.9	93.1	94.9	94.0	−4.4	−4.2	−6.3	−5.3	−4.2	−6.8	91	89	86	89	0.4	0.5	0.5	0.5	10	10	10	E	3	ENE	2	E	1
16	98.3	100.8	104.3	101.1	−7.8	−8.2	−11.4	−9.7	−6.3	−12.0	81	84	83	83	0.6	0.5	0.4	0.5	10	6 ☉	3	N	1	NNE	1	C	0
17	104.3	105.3	105.3	105.0	−12.7	−8.9	−7.6	−9.2	−6.9	−13.2	85	67	73	75	0.4	1.0	0.9	0.8	3	2 ☉	10	C	0	WSW	1	WSW	1
18	103.7	102.1	101.9	102.6	−5.6	−2.9	−4.8	−4.5	−2.2	−7.6	90	86	88	88	0.4	0.7	0.5	0.5	10	5 ☉	1	C	0	W	1	W	1
19	102.3	102.7	104.2	103.1	−5.0	−2.1	−2.6	−3.1	−1.4	−7.2	93	92	85	90	0.3	0.4	0.8	0.5	10	10	10	C	0	C	0	W	1
20	104.4	103.7	101.6	103.2	−3.1	−2.6	−5.3	−4.1	−2.0	−5.6	88	81	90	86	0.6	1.0	0.4	0.7	10	10	0	W	2	WNW	2	C	0
21	99.9	99.9	100.0	99.9	−7.9	−1.2	−6.1	−5.3	0.1	−8.7	81	70	84	78	0.6	1.7	0.6	1.0	3	1 ☉	2	C	0	C	0	C	0
22	100.0	99.0	95.3	98.1	−7.9	−4.3	−7.1	−6.6	−3.1	−8.4	81	79	88	83	0.6	0.9	0.4	0.6	5	7 ☉	2 ≡	C	0	C	0	C	0
23	96.2	94.7	91.8	94.2	−9.7	−3.8	−6.2	−6.5	−2.6	−10.2	85	76	86	82	0.4	1.1	0.5	0.7	0	2 ☉ ≡	6	C	0	C	0	E	1
24	86.4	84.4	83.7	84.8	−6.0	−2.4	−2.2	−3.2	−1.0	−7.9	87	76	81	81	0.5	1.2	1.0	0.9	9	10	10	C	0	C	0	C	0
25	83.9	85.1	86.2	85.7	−1.0	1.2	−0.1	0.0	2.5	−2.5	96	79	84	86	0.3	1.4	1.0	0.9	10 ≡	7 ☉	8	C	0	C	0	W	1
26	93.2	94.1	95.0	94.1	0.2	3.6	−0.4	0.8	3.8	−1.0	84	75	86	82	1.0	2.0	0.8	1.3	10	5 ☉	4 ≡	W	1	C	0	C	0
27	91.4	92.7	95.1	93.1	−0.2	2.6	3.4	2.3	3.5	−5.3	88	89	90	89	0.7	0.8	0.8	0.8	10	10	10	C	0	W	1	C	0
28	94.0	95.9	102.9	97.6	0.4	1.3	0.8	0.8	3.4	−0.6	94	92	92	93	0.4	0.5	0.5	0.5	6 ≡	10 ☉	8	C	0	C	0	C	0
29	106.0	104.8	103.4	104.7	0.6	2.6	−0.2	0.7	2.8	−0.3	84	65	92	79	1.3	2.6	0.5	1.5	9	9	8	C	0	C	0	C	0
30	99.9	97.2	95.9	97.7	−1.4	4.1	0.6	1.0	5.1	−1.8	93	63	88	81	0.3	3.1	0.8	1.4	7	6 ☉	7	C	0	C	0	C	0
31	97.1	98.1	98.0	97.7	1.1	3.8	1.3	1.9	4.3	−0.3	94	80	92	89	0.4	1.6	0.5	0.8	10	10	5	C	0	C	0	C	0
M	95.1	94.9	95.4	95.1	−1.7	0.9	−0.9	−0.6	1.8	−3.2	87	80	87	85	0.7	1.4	0.8	1.0	8.3	7.5	7.0	0.7		0.7		0.7	

Luty – Février

1	94.6	94.2	95.7	94.8	1.1	4.4	3.0	2.9	4.5	0.6	94	97	93	95	0.4	0.3	0.6	0.4	10 ●	10	10 ●	C	0	C	0	C	0
2	97.6	99.9	101.2	99.6	3.7	6.1	4.9	4.9	6.3	1.8	95	91	95	94	0.4	0.8	0.5	0.6	10 ≡	10	10	W	1	WNW	2	W	1
3	98.9	96.6	99.8	98.4	3.2	7.5	3.4	4.4	8.8	2.5	93	82	93	89	0.5	2.0	0.5	1.0	10	10	10	C	0	C	0	NE	1
4	99.9	98.6	97.8	98.8	2.1	3.7	3.4	3.2	4.3	1.2	93	88	90	90	0.5	1.0	0.8	0.8	10	10	8 ≡	E	1	WSW	1	C	0
5	98.1	97.2	96.2	97.2	−0.1	1.8	−0.5	0.2	3.4	−0.9	100	96	100	99	0.0	0.3	0.0	0.1	10 ≡	2 ☉ ≡	10 ● ≡	C	0	C	0	C	0
6	93.3	90.5	89.5	91.1	−0.6	5.2	5.9	4.1	11.1	−1.2	100	97	71	89	0.0	0.2	2.7	1.0	10 ≡	3 ☉	0	C	0	C	0	W	1
7	90.5	92.5	93.8	92.3	3.6	5.4	4.0	4.2	6.5	1.7	95	91	83	89	0.5	0.9	1.3	0.9	10	10	3	C	0	W	3	W	1
8	91.3	85.7	82.4	86.5	0.9	7.1	7.5	5.8	8.1	0.3	94	81	76	84	0.4	1.9	2.5	1.6	6 ≡	10	10 ● ●	C	0	C	0	C	0
9	79.2	78.5	80.6	79.4	6.1	9.2	6.9	7.3	10.0	4.2	92	76	88	85	0.7	2.7	1.1	1.5	10 ●	7	10 ●	W	2	WSW	4	W	2
10	83.0	82.7	82.4	82.7	3.1	8.9	6.5	6.2	9.5	2.4	91	59	78	76	0.6	4.6	2.2	2.5	5	10 ☉	7	C	0	W	2	C	0
11	83.1	85.6	89.1	85.9	2.5	5.7	3.8	4.0	6.5	0.9	96	86	83	88	0.3	1.3	1.3	1.0	10 ≡	10	7	C	0	WSW	3	SSW	1
12	88.6	85.4	82.4	85.5	2.0	7.7	4.2	4.5	8.7	0.9	93	57	74	75	0.6	4.5	2.1	2.4	5	3 ☉	10	C	0	W	1	C	0
13	79.3	76.5	69.4	75.1	4.6	9.3	4.1	5.5	9.6	2.8	81	55	80	72	1.7	5.3	1.6	2.9	7	2 ☉	10	C	0	SW	2	C	0
14	66.4	65.8	65.9	66.0	6.9	8.9	6.2	7.0	9.7	3.3	75	72	79	75	2.4	3.2	2.0	2.5	7	10 ●	2	C	0	C	0	C	0
15	68.0	64.4	62.1	64.8	3.6	9.8	7.1	6.9	9.8	2.8	76	51	78	68	1.9	5.9	2.2	3.3	6	9	10 ●	C	0	S	2	S	1
16	68.9	71.7	76.4	72.3	6.6	8.5	5.2	6.4	9.1	4.9	61	47	63	57	3.8	5.9	3.2	4.3	10	4 ☉	3	C	0	W	1	C	0
17	80.9	81.7	83.1	81.9	1.2	7.8	5.2	4.8	8.7	0.4	81	51	66	66	1.3	5.2	3.0	3.2	10	5 ☉	9	C	0	SSW	1	C	0
18	82.7	78.2	70.4	77.1	0.9	6.9	7.0	5.4	8.5	0.0	87	75	80	81	0.9	2.4	2.0	1.8	8	9	4	C	0	C	0	C	0
19	73.8	81.6	87.9	81.1	2.5	4.2	2.0	2.7	8.5	1.2	89	71	76	79	0.8	2.4	1.7	1.6	10 ●	9	8	WNW	4	WNW	6	W	1
20	89.7	87.8	85.4	87.6	−0.2	8.1	3.2	3.6	9.5	−0.5	88	48	76	71	0.7	5.7	1.9	2.8	9 ☉	8 ☉	10	C	0	C	0	C	0
21	82.7	82.9	85.6	83.7	3.5	9.6	5.0	5.8	10.1	1.2	78	57	94	76	1.7	5.2	0.5	2.5	4	6 ☉	10 ●	C	0	C	0	C	0
22	88.5	89.3	88.5	88.8	1.0	1.7	0.9	1.1	5.0	0.2	96	74	90	87	0.3	1.8	0.6	0.9	10 ✳	10	9	WSW	2	NW	1	C	0
23	89.3	88.5	87.5	88.4	−2.9	2.7	0.3	0.1	4.3	−3.6	93	57	82	77	0.3	3.2	1.1	1.5	10	6 ☉	3	C	0	C	0	C	0
24	81.9	75.6	74.9	77.5	−2.4	2.6	1.0	0.6	2.7	−3.7	91	81	96	89	0.5	1.5	0.3	0.8	10	10 ✳	10	E	1	SE	2	C	0
25	79.5	80.4	78.2	79.4	0.7	1.9	0.9	1.1	2.3	0.2	86	84	88	86	0.9	1.2	0.7	0.9	10	8 ☉	10 ✳	C	0	C	0	E	2
26	84.0	87.6	93.0	88.2	−0.2	1.1	0.1	0.3	1.1	−0.7	100	83	82	88	0.0	1.1	1.2	0.8	10 ✳	10	10	C	0	NW	2	C	0
27	95.3	96.5	98.7	96.8	−1.3	0.6	−1.0	−0.7	0.9	−1.9	68	92	87	82	1.8	0.5	0.7	1.0	9	10	10	C	0	C	0	C	0
28	101.0	102.7	103.9	102.5	−2.4	−2.6	−2.2	−2.4	−1.0	−3.7	93	71	85	83	0.3	1.6	0.8	0.9	10	10 ✳	10	C	0	N	1	C	0
29																										
30																										
31																										
M	86.1	85.7	85.8	85.9	1.8	5.5	3.5	3.6	6.7	0.6	88	74	83	82	0.9	2.6	1.4	1.6	8.8	7.9	8.0	0.4		1.2		0.4	

Kraków, Obserw. Astr. UJ $H_s = 221\ m$ $H_b = 219{,}8\ m$ $h_w = 21\ m$ Styczeń – Janvier 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.9	6	4.3	⛬ 1–8
2	7	.	6	3.0	
3	4	0.2	5	.	⛆⁰ ok. 16³⁰ ● p z prz ; = a, p ≡⁰ III
4	4	0.5	3	.	● na , a z prz. ≡⁰ n, I = a, p ≡¹ III
5	4	3.0	3	1.6	● 17³⁰–20⁵⁰ ⛇ np ⛆ np, ≡² I = II, V I
6	3	4.2	1	.	● na , a z prz. ●¹ 13¹⁵–15 ● 16–20⁵⁰ ●¹– n ; = I, II
7	5	0.4	.	1.2	●⁰ a z prz , II ⛆ ok. 18 ; = I, II
8	7	0.0	.	.	⛆⁰ ok. 10 ; = I
9	4	.	.	.	= I, II
10	4	1.7	.	1.8	●¹ p z prz ; ≡⁰ na , I = II III ; V⁰ I
11	4	0.4	.	0.7	⛇ 7⁵⁰ ✶⁰ 8–12 , p z prz ⛬ 20 , III , = I, II
12	7	.	.	1.7	⛆ na , = I
13	5	7.5	.	.	✶¹ 7–a , II , p , III
14	6	0.1	4	1.6	✶ n ⛆ I
15	6	0.2	4	.	⛬ a z prz. ⛇ ok. 18 ; = I
16	7	0.3	4	1.0	✶⁰ n z prz. , a
17	5	.	4	5.4	✶ ↔ na ; = I, II
18	6	.	4	4.1	= I, II, III
19	4	0.0	4	.	⛬⁰ 12³⁰ , = I, II, III
20	4	0.0	4	.	= I, II, III
21	4	.	4	6.8	⌴ n , I ; = I, II, III ; ⏔ I
22	4	.	3	2.0	⛢⁰ ok. 21 ⛢ 23¹⁰–47 ; = I, II ≡⁰ III ; ⌴⁰ ⏔ I
23	3	.	3	5.4	= I ≡⁰ II = III ; ⌴⁰ I
24	6	.	3	.	= I, II, III
25	4	0.0	3	1.2	≡⁰ I = II, III
26	4	.	3	2.3	✶⁰ na ; = I, II ≡⁰ III
27	4	0.4	2	.	●⁰ a z prz. ● ok. 14 ; = I, II, III
28	4	0.8	1	.	✶⁰ 11³⁰ a, p ; ≡⁰ I = II, III ; ⌴⁰ I
29	7	.	1	1.3	= I, III
30	5	.	pż.	3.3.	= I, II, III
31	5	.	pż.	.	= I,
Σ	—	20.6	—	48.7	UWAGI Kierunki i prędkości wiatru w ciągu całego roku wyznaczano za pomocą anemografu.

Luty – Février

1	4	1.9	pż.	.	●● a, I, p z prz. , III ; = I, II, III
2	4	0.1	.	.	● n ●⁰ 8³⁰ a , p z prz. ; ≡⁰ I = II, III
3	3	.	.	0.6	= I, II
4	4	0.0	.	.	= I, II ≡⁰ III
5	3	0.0	.	1.4	≡² na , I , a – 12 ≡⁰ – 18 ≡² – 20⁵⁰ , np ; ⛉⁰ n, a
6	4	.	.	4.7	● n ; ≡² na , I , a = II
7	4	0.6	.	0.2	● 7¹⁰–8³⁵ ●⁰ – ok. 10 ; = I, II
8	4	0.8	.	0.1	●⁰ ●⁰ 20⁵⁰ – n ; ≡⁰ na , I , a = II, III ; V⁰ I
9	7	2.1	.	1.0	●⁰ n , I , a – ok. 9³⁰ , 18–20⁵⁰ ● – n ; = I
10	7	.	.	4.9	●⁰ n , = ⌴⁰ I
11	7	0.1	.	0.3	≡² na , I
12	7	.	.	6.7	●⁰ n ; = I, ⏔ III
13	7	.	.	6.2	
14	7	0.6	.	.	●⁰ 12 – ok. 15
15	8	0.6	.	3.7	●⁰ 15 – 20⁵⁰ , np ; ⌴⁰ I
16	8	.	.	6.0	
17	8	.	.	6.1	⌴⁰ I
18	8	1.0	.	.	⌴⁰ I
19	7	1.3	.	1.0	●⁰ n, I, a – 10³⁰ ⛇ ok. 10 ⛆⁰ ok. 16 ; = III
20	8	.	.	3.1	⌴⁰ I
21	7	8.0	.	3.8	● ok. 18 – 18³⁰ ●⁰ ok. 18³⁰ – 20⁵⁰ , np ; = III
22	7	0.9	1	0.6	✶ na , I , a – 11³⁰ ; = I, III
23	8	.	pż.	7.9	= I, III ; ⌴⁰ I
24	7	1.8	.	.	⛬⁰ 7⁴⁰ – ok. 8 ✶⁰ ok. 8–9 ✶¹ – 11 ✶⁰ – 13³⁰ ●⁰ – ok. 14 ✶⁰ – 20 ; = III ; ⌴⁰ I
25	8	7.5	pż.	0.4	✶⁰ ok. 20 – 20⁵⁰ ; = I, III
26	7	0.1	8	.	✶ n – 6⁵⁰ ✶⁰ – ok. 10 ⛇⁰ ok. 16 ; = I, III
27	7	.	4	.	
28	7	0.0	3	.	⛬⁰ 9 – a ✶⁰ a, II, p – 15 ; = III
29					
30					
31					
Σ	—	27.4	—	60.7	UWAGI.

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°57' — Marzec – Mars 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	106.1	106.1	105.9	105.9	-3.2	-2.4	-2.1	-3.0	-1.5	-6.0	85	72	87	81	0.6	1.4	0.6	0.9	9	10 ✳	10 ✳	W 1	NNE 1	WNW 1
2	103.7	102.2	100.6	102.2	-2.6	-0.2	-1.4	-1.4	0.9	-3.6	89	61	66	72	0.6	2.3	1.9	1.6	10 ✳	8 ⊙	10	NW 1	C 0	C 0
3	96.6	95.5	94.5	95.9	-2.2	-1.4	-5.8	-3.8	-0.4	-6.2	89	82	95	89	0.6	1.0	0.2	0.6	10 ✳	10 ✳	9	W ½	C 0	C 0
4	91.5	88.5	85.6	88.5	-7.4	-0.4	0.8	-1.6	2.5	-8.3	85	78	88	84	0.5	1.3	0.8	0.9	8 ⊙	6 ⊙	10	C 0	C 0	C 0
5	85.5	87.1	88.5	87.0	1.9	4.2	0.3	1.7	4.5	0.1	84	49	90	74	1.2	4.2	0.6	2.0	10 ●	7	4	W 1	WNW 2	C 0
6	88.6	87.1	85.9	87.2	-2.9	3.8	0.0	0.2	4.4	-3.6	91	62	84	79	0.4	3.0	1.0	1.5	6 ⊙≡	5 ⊙	1	C 0	C 0	C 0
7	85.2	86.2	87.9	86.4	-3.7	2.3	-2.9	-1.8	2.9	-4.3	97	66	99	87	0.2	2.4	0.0	0.9	3 ⊙	2 ⊙	2	C 0	ENE 1	ESE 2
8	89.4	89.5	92.3	90.4	-3.9	1.0	-1.8	-1.6	1.9	-4.7	78	59	74	70	1.0	2.8	1.5	1.8	1 ⊙	0 ⊙	3	E 4	ESE 2	ESE 4
9	96.2	97.8	100.9	98.3	-4.2	1.2	-0.8	-1.2	1.6	-4.8	79	57	77	71	0.9	2.9	1.4	1.7	2 ⊙	2 ⊙	1	E 6	E 2	C 0
10	103.7	104.8	105.2	104.6	-3.0	0.4	-0.7	-1.5	1.9	-3.5	95	70	87	84	0.2	1.9	0.7	0.9	0 ⊙	4 ⊙	0	C 0	E 2	E 1
11	106.1	105.9	104.5	105.5	-5.2	4.9	1.2	0.3	6.3	-5.8	98	55	79	77	0.1	4.0	1.4	1.8	3 ⊙	0 ⊙	0	C 0	ESE 1	C 0
12	101.0	97.4	94.2	97.5	-2.9	9.9	5.9	4.7	11.9	-3.6	95	42	71	69	0.2	7.1	2.7	3.3	5 ⊙≡	7 ⊙	10	C 0	C 0	C 0
13	93.0	92.8	92.1	92.6	3.6	12.2	7.6	7.8	13.5	2.7	63	35	66	55	2.9	9.2	3.5	5.2	4 ⊙	0 ⊙	6	WNW 1	WNW 3	W 1
14	89.5	85.6	85.3	86.8	4.6	16.0	10.7	10.5	16.0	3.1	62	40	76	59	3.3	11.0	3.1	5.8	8 ⊙	0 ⊙	10 ●	W 2	SW 6	W 2
15	86.6	86.8	81.7	85.0	7.9	9.2	9.6	9.1	11.5	7.2	64	66	75	68	3.8	3.9	3.0	3.6	10	10	10 ●	WNW 8	WNW 5	W 6
16	77.2	81.5	87.8	82.2	6.4	2.6	-0.9	1.8	10.4	-1.3	88	81	81	83	1.1	1.5	1.1	1.2	10 ●	10	7	E 4	WNW 4	E 4
17	89.6	87.8	81.4	86.3	-2.4	1.0	1.6	0.4	2.8	-3.4	73	85	87	82	1.4	1.0	0.9	1.1	10	10	10	C 0	ESE 1	C 0
18	72.6	72.5	77.4	74.2	8.7	14.7	6.8	9.2	14.8	1.4	90	59	90	80	1.0	6.9	1.0	3.0	10 ●	10 ●	10 ●	C 0	W 9	W 7
19	82.6	84.3	85.2	83.4	6.1	9.3	8.1	7.9	11.4	5.2	82	66	96	81	1.7	4.0	0.5	2.1	10 ●	10	10 ●	WSW 4	WNW 3	C 0
20	85.1	85.4	82.2	84.2	9.6	13.8	11.1	11.4	15.2	6.8	89	66	84	80	1.3	5.4	2.1	2.9	10	6 ⊙	7	C 0	WNW 1	C 0
21	83.2	86.2	86.9	85.4	9.1	13.2	11.5	11.3	15.1	7.7	87	58	68	71	1.6	6.4	4.4	4.1	6 ⊙	6 ⊙	10	C 0	NW 1	C 0
22	89.2	90.1	92.4	90.6	5.8	12.7	8.0	8.6	14.0	4.8	83	43	78	68	1.5	8.3	2.4	4.1	9	6 ⊙	8	C 0	WNW 2	C 0
23	92.8	91.1	92.1	92.0	0.5	13.1	8.9	7.8	13.7	0.2	96	59	62	72	0.2	6.3	4.4	3.6	0 ⊙≡	4 ⊙	10	C 0	ENE 1	ENE 1
24	95.4	97.8	97.3	96.8	3.4	2.6	2.2	2.6	8.9	1.2	90	93	89	91	0.8	0.6	0.8	0.7	10 ●	10 ●	10	E 9	ENE 9	E 9
25	97.0	97.3	98.3	97.6	1.2	4.4	1.9	2.4	5.8	0.6	94	87	94	92	0.4	1.1	0.4	0.6	10	10	10	ESE 6	NNE 5	ENE 2
26	97.3	96.0	96.7	96.7	1.6	12.3	7.5	7.2	14.2	0.1	89	60	68	72	0.8	5.8	3.4	3.3	5 ⊙	2 ⊙	0	C 0	ESE 1	C 0
27	98.8	98.6	97.9	98.4	3.1	13.4	9.0	8.6	15.7	2.0	83	43	63	63	1.3	8.8	4.2	4.8	1 ⊙	0 ⊙	0	C 0	SW 1	C 0
28	95.8	93.4	91.4	93.5	2.6	15.2	9.3	9.1	16.3	0.6	79	29	51	53	1.6	12.3	5.7	6.5	0 ⊙	6 ⊙	8	C 0	C 0	C 0
29	89.1	88.6	88.4	88.7	6.0	11.3	8.8	8.7	12.7	5.0	83	69	88	80	1.6	4.2	1.4	2.4	10	10	9	C 0	C 0	C 0
30	89.2	89.4	90.4	89.7	5.6	12.5	11.1	10.1	13.8	5.0	89	56	50	65	1.0	6.4	6.6	4.7	9	8 ⊙	10	C 0	C 0	C 0
31	95.1	95.3	94.4	94.9	3.9	11.8	9.4	8.6	14.9	3.1	98	53	76	76	0.2	6.4	2.8	3.1	10 ≡	4 ⊙	2	C 0	C 0	C 0
M	92.0	91.9	91.7	91.9	1.4	7.2	4.4	4.4	9.0	-0.1	85	61	79	75	1.1	4.6	2.1	2.6	6.9	5.9	6.7	1.6	2.0	1.3

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1	95.4	93.7	93.1	94.1	3.3	15.0	10.3	9.7	17.8	2.6	90	51	60	67	0.7	8.4	5.0	4.7	3 ⊙	1 ⊙	0	C 0	NE 1	ENE 2
2	93.6	92.7	93.7	93.3	3.4	17.6	12.8	11.6	19.2	2.2	88	34	66	63	0.9	13.2	5.1	6.4	1 ⊙	2 ⊙	10	C 0	ESE 1	C 0
3	96.3	97.3	99.1	97.6	6.9	17.5	11.4	11.8	18.9	5.9	81	37	34	57	1.8	12.5	6.2	6.8	7 ⊙	5 ⊙	0	C 0	ENE 4	C 0
4	101.9	101.8	101.3	101.7	3.4	16.9	12.4	11.8	18.1	3.7	86	40	48	58	1.3	11.6	7.5	6.8	1 ⊙	0 ⊙	0	C 0	ENE 2	NNE 4
5	101.1	99.0	94.5	98.2	5.8	15.4	10.8	10.7	16.9	4.0	82	40	53	59	1.7	10.5	5.9	6.0	1 ⊙	0 ⊙	0	C 0	C 0	E 1
6	90.1	85.7	82.9	86.2	4.7	19.7	13.6	12.9	20.8	3.6	83	20	58	54	1.2	18.3	6.5	8.7	0 ⊙	0 ⊙	2	C 0	C 0	C 0
7	81.6	83.0	85.0	83.2	8.2	7.4	5.0	6.4	13.6	4.5	82	84	90	85	2.0	1.6	0.8	1.5	10 ⊙	10	10	C 0	NNW 2	NNE 1
8	89.2	89.7	89.3	89.4	2.6	5.3	4.4	4.2	6.6	1.5	93	75	62	77	0.6	2.2	3.3	2.0	10 ●	9 ●	8	NE 2	NNE 2	NW 2
9	87.8	86.1	84.9	86.3	0.7	7.5	5.3	4.7	9.0	-0.5	83	58	91	77	1.1	4.4	0.8	2.1	4 ⊙	8 ⊙	10	W 2	W 3	NE 1
10	83.8	79.7	73.2	78.9	3.6	11.5	10.0	8.8	13.5	2.3	88	51	69	69	0.9	6.7	3.8	3.8	9	4 ⊙	10	E 2	C 0	C 0
11	67.2	69.1	74.7	70.3	7.3	5.9	5.2	6.0	10.0	4.6	96	91	94	94	0.5	0.9	0.5	0.6	10 ●	10 ●	10	C 0	NW 2	W 1
12	81.2	82.9	84.8	83.0	2.4	6.0	4.3	4.2	6.9	1.7	80	53	69	67	1.5	4.5	2.6	2.9	5 ⊙	7 ⊙	10	NNW 2	C 0	C 0
13	86.7	87.9	90.6	88.4	1.9	6.3	3.1	3.6	7.3	0.2	91	53	91	78	0.6	4.4	0.6	1.9	7 ⊙	6 ⊙	10	C 0	C 0	C 0
14	92.0	91.3	91.4	91.6	0.4	6.0	2.6	2.9	6.4	-0.8	94	47	79	73	0.4	3.0	1.6	2.3	2 ⊙	10	10	C 0	C 0	NE 1
15	92.1	93.4	96.6	94.0	1.4	5.2	3.4	3.4	6.6	0.7	65	51	78	65	2.4	4.3	1.7	2.8	4 ⊙	7 ⊙	10	NNE 3	N 1	WNW 1
16	97.3	96.0	95.9	96.5	0.6	9.0	8.3	6.6	11.6	-0.8	90	43	67	67	0.6	6.5	3.6	3.6	0 ⊙	3 ⊙	10	C 0	W 2	SW 1
17	93.3	92.4	92.7	92.9	7.2	9.8	7.6	8.0	12.0	6.3	74	74	77	75	2.7	3.1	2.3	2.7	10 ●	9	10	C 0	NW 2	NW 1
18	90.7	89.8	89.8	90.1	6.0	6.6	5.0	5.6	7.6	4.6	80	71	81	77	1.9	2.8	1.6	2.1	9	10	10	NNW 3	W 4	W 2
19	89.4	87.4	88.1	88.3	3.6	11.4	9.4	8.4	13.0	2.7	81	55	79	72	1.5	6.1	2.5	3.4	10	7 ⊙	10	C 0	SSE 1	WNW 2
20	91.2	93.4	97.1	94.6	8.3	8.2	6.7	7.5	10.8	6.2	89	79	85	84	1.3	2.3	1.4	1.7	10	10	8	W 3	NNW 4	C 0
21	98.8	100.1	101.2	100.0	5.2	10.9	7.8	7.9	11.3	3.2	94	59	87	80	0.5	5.3	1.4	2.4	9	10	10 ●	C 0	NE 2	C 0
22	100.6	101.1	101.9	101.2	7.3	11.0	6.6	7.9	12.9	6.1	87	78	94	86	1.3	2.9	0.5	1.6	10	9 ⊙	10	C 0	WNW 2	W 1
23	101.4	100.9	100.1	100.8	5.4	11.1	10.3	9.3	13.0	4.8	97	79	94	90	0.3	2.8	0.8	1.3	10	9 ⊙	10 ●	NW 1	C 0	C 0
24	98.1	98.0	96.8	97.6	10.0	12.0	10.4	10.7	12.3	9.1	92	79	91	87	1.0	3.0	1.1	1.7	10	10 ●	10	NNE 1	C 0	W 2
25	94.3	94.2	93.8	94.2	9.8	14.1	10.5	11.2	15.1	8.6	93	77	92	87	0.8	3.7	1.0	1.8	10	10	10	C 0	S 1	SW 2
26	93.9	93.4	92.5	93.3	9.2	14.0	12.0	11.8	17.4	8.2	93	77	89	86	0.8	3.7	1.5	2.0	10 ≡	9 ⊙	9 ●	WSW 1	C 0	W 2
27	91.2	89.6	88.5	89.8	10.1	18.4	14.8	14.5	19.9	9.2	100	70	78	83	0.0	6.3	3.6	3.4	10 ≡	3	8	WNW 1	C 0	C 0
28	88.2	85.8	85.5	86.5	11.5	22.0	17.4	17.1	23.8	8.9	90	46	63	66	1.4	14.3	7.3	7.7	1 ⊙	3 ⊙	3	C 0	C 0	C 0
29	86.4	86.6	87.0	86.7	14.4	21.2	15.7	16.8	22.9	11.0	74	46	81	67	4.3	13.6	3.4	7.1	3 ⊙	8 ●☾	1	C 0	S 1	C 0
30	86.0	82.5	81.8	83.4	12.0	22.2	15.8	16.4	25.0	9.5	89	45	86	73	1.5	14.7	2.4	6.2	2 ⊙	6 ⊙☾	10 ●☾	C 0	NNE 2	S 2
31																								
M	91.4	90.9	90.9	91.1	6.0	12.2	9.1	9.1	14.0	4.3	87	59	77	74	1.2	6.7	2.9	3.6	6.3	6.6	7.6	0.7	1.3	1.0

Kraków, Obserw. Astr. UJ — $H_s = 221\ m$ — $H_b = 219{,}8\ m$ — $h_w = 21\ m$ — Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	7	0.0	2	.	✳° II, p z prz. ; III : = I, III
2	7	0.0	2	1.5	✳° na – 8¹⁵ ✳¹ – 9³⁰ : = III
3	7	0.0	1	0.5	▽* °/ a, II ; = III
4	8	0.0	1	5.2	= III : ⌴° /
5	7	0.0	pż.	2.7	•° 6⁰⁵ ok. 8 ; = I, III
6	7	.	pż.	8.3	≡° / , ⌴° /
7	7	.	.	8.7	= ⌴° /
8	7	.	.	9.3	⌴° /
9	7	.	.	8.9	= III
10	7	.	.	7.2	= ⌴° /
11	7	.	.	8.7	= ⌴° / = III
12	7	.	.	4.7	≡° n. / a = III : ⌴° /
13	7	.	.	6.7	⌣ ok. 19 – III : = I, III
14	7	0.0	.	6.3	• od 20⁴⁰ , np : = /
15	7	6.3	.	0.6	•° 20¹⁵ ... III
16	7	1.0	.	.	•° n – 9³⁰ ▽* ok. 9³⁰ 9⁵⁵ 11²⁰ •° 12 – 12³⁰
17	7	4.2	.	.	✳° 13⁰² – ok. 13³⁰ ✳¹ – ok. 15 •° – 16
18	8	11.6	.	2.2	•° n – ok. 8 , II •¹ 12⁵⁵ – 13⁵⁰ , 15⁰⁵ – 30 , 17⁰⁶ – 15 •¹ – 17²⁸ •¹ – ok. 18 •° – n. ☇ 17¹⁵–²⁸ NW-SE ; ≫ a, p
19	7	9.0	.	0.6	•° n. / , 8¹⁸ – 45 •¹ 18¹² – n
20	7	.	.	2.7	•° n . = / III
21	7	0.0	.	4.0	•° ok. 18³⁰ – 43 ; = ⌒° /
22	7	.	.	4.8	= /
23	7	2.0	.	7.6	≡° n. / a ; ⌴° /
24	4	7.7	.	.	•¹ 5 – 6²⁵ •° – 15⁰⁰ , 15⁵⁰ 20¹⁵ ; ≫ na , a, p (wiatr porywisty)
25	4	0.5	.	.	•° n – 5⁵⁰ , 7³⁸ – 50 , 13²⁸ – 55 ; ≫ n.a (wiatr porywisty) ; = I, II, III
26	7	.	.	9.0	⌒° /
27	8	.	.	10.4	= ⌴° /
28	8	3.1	.	10.2	= ⌴° /
29	7	.	.	0.5	• na
30	7	.	.	0.5	
31	7	.	.	6.4	≡² na , /
Σ	—	45.4	—	138.2	UWAGI.

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1	7	.	.	10.6	⌒° /
2	8	.	.	8.7	= III
3	7	.	.	9.2	
4	8	.	.	11.0	⌒° /
5	8	.	.	11.1	⌒° /
6	8	.	.	10.9	= I, III ; ⌒° /
7	6	14.1	.	.	•° 8²⁰ ... III
8	7	0.2	.	0.2	•° na – 6⁵⁸ ✳° – 7⁴⁰ •° – 8¹⁵ , 12²⁶ – 13²⁰
9	7	0.1	.	3.7	•° 17³⁰ ... III ; = ⌒° /
10	8	4.0	.	8.8	
11	4	9.4	.	.	•° na – II ... np ; = III
12	8	.	.	3.1	
13	7	0.0	.	5.4	✳° 10²² ... 11¹⁶ ▽* p ▽* p ; ⌒° /
14	7	.	.	2.0	= ⌴° /
15	7	0.0	.	3.9	▽* ok. 10 – 10³⁰ , 15¹² ... 16
16	7	.	.	7.6	= ⌴° /
17	7	0.1	.	1.6	•° / – 8⁴⁰ , 15⁵⁰ – 16¹⁸ ; = /
18	7	.	.	0.3	
19	7	0.6	.	3.1	•° 19¹⁵ – III , = /
20	6	.	.	0.6	•° na ... 6³⁰ ; = /
21	7	2.0	.	0.1	•° 19²⁰ – np ; ⌒° /
22	6	2.3	.	1.2	•° 7²⁵ – ok. 9 , 16¹⁰–²⁰ •¹ – 16⁴⁰ •° – ok. 17
23	7	0.9	.	0.2	•° ok. 18 ... np ; = I, III
24	7	3.4	.	.	•° 9³⁵ 13⁴⁰ •¹ – ok. 14⁵⁰ •° – 15³³ •¹ 18³⁰ – 40
25	4	0.1	.	.	▽* ok. 13 , ok. 20 ; = I, II
26	6	3.6	.	1.8	•° na , np ; (☇) 21³⁵ – ok. 23 ☇ – 23⁴⁰ N–S ; ≡° / = III
27	5	.	.	5.0	•° na ; ≡° / = II
28	8	.	.	10.6	= ⌒° / ; ↘ III
29	8	0.0	.	7.2	•° II – 13²⁰ (☇) 11²⁷ – 40 , 12³⁵ – II SE-E-NE ; ⌒° /
30	8	6.2	.	4.4	•° 12³²–³⁵ , ok. 15 – 15¹⁵ ▽* 16²⁰–²⁷ 16³¹–³⁵ •° – 16⁴⁵ ▽* 20¹⁰–³⁰ •° – III ▽* 22⁴⁵ – 23¹⁵ (☇) 12¹³ – II SE-E-NNE ,
31					[30.IV: 16⁰⁹–¹⁹ ☇ – 16²⁴ (☇) – 16³⁴ , 19³⁸ – 20⁰⁵ ☇ – III NW-SE (☇) – 20⁵⁶ ; ⌒ 16⁴⁰ ; ⌒¹ /
Σ	—	47.0	—	134.3	UWAGI.

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°57' — Maj – Mai 1957

DNI	CIŚNIENIE P=900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.0	91.0	90.8	90.9	7.6	10.5	8.0	8.5	15.8	6.9	66	52	76	65	3.5	6.1	2.5	4.0	10	10 ●	10	NW 1	C 0	C 0
2	88.9	88.1	87.0	88.0	6.9	7.3	6.6	6.8	8.0	5.8	75	83	90	83	2.4	1.7	1.0	1.7	10	10 ●	10 ●	NE 4	ENE 2	ENE 2
3	85.8	86.1	85.0	85.6	5.6	8.4	8.8	7.9	10.7	4.7	92	85	84	87	0.7	1.6	1.8	1.4	10	10 ●	10	NNE 1	C 0	C 0
4	83.8	84.7	87.7	85.4	7.8	12.2	8.3	9.2	14.2	5.0	86	60	61	69	1.5	5.7	4.3	3.8	9	9	10	W 1	WNW 4	NNW 2
5	89.3	87.1	85.0	87.1	5.0	9.0	7.8	7.4	11.7	3.5	66	42	80	56	3.0	6.7	4.2	4.6	3 ⊙	10	10	WNW 4	W 3	C 0
6	82.5	83.1	83.5	83.0	5.4	6.1	6.0	5.9	7.9	3.9	89	63	64	72	1.0	3.5	3.4	2.6	10	8 ⊙	9	C 0	W 6	WNW 1
7	82.3	81.9	80.4	81.5	3.7	4.2	4.4	4.2	6.6	2.7	82	84	87	84	1.5	1.3	1.1	1.3	10	10 ●	10	C 0	C 0	C 0
8	79.7	80.4	83.4	81.2	5.4	5.6	4.9	5.2	6.6	3.4	80	75	84	80	1.8	2.2	1.4	1.8	10	10 ●	10 ●	NW 1	NW 5	NW 2
9	84.6	84.6	84.4	84.5	2.2	5.4	5.0	4.4	7.1	1.7	96	86	94	92	0.3	1.3	0.5	0.7	10 ●	10 ●	10 ●	W 2	NW 2	WNW 1
10	82.8	83.8	86.8	84.5	4.8	5.3	6.0	5.3	6.5	4.1	97	98	96	98	0.3	0.1	0.2	0.2	10 ●	10 ●	10 ●	W 4	W 4	C 0
11	89.1	90.1	89.8	89.7	7.4	14.4	11.2	11.0	16.1	5.4	88	50	84	74	1.2	8.3	2.1	3.9	10	2 ⊙	9	C 0	C 0	C 0
12	91.0	91.1	91.4	91.2	9.8	20.1	14.6	14.8	20.9	5.8	92	43	71	69	0.9	13.5	4.8	6.4	7	3 ⊙	4	C 0	SSE 1	C 0
13	92.5	91.4	90.9	91.6	11.2	20.8	15.6	15.8	22.0	7.2	84	38	67	63	2.1	15.3	5.9	7.8	1 ⊙	1 ⊙	0	C 0	NE 1	NW 1
14	91.9	92.9	94.6	93.1	12.3	17.1	15.1	14.9	20.8	9.2	83	66	79	76	2.4	6.7	3.7	4.3	0 ⊙	9 ●	10	W 2	NW 2	C 0
15	96.5	95.9	94.5	95.6	12.0	20.0	15.9	16.0	21.2	9.1	84	43	71	66	2.2	13.3	5.3	6.9	0 ⊙	4 ⊙	0	S 1	NNE 1	C 0
16	93.5	90.8	88.9	91.1	12.7	21.2	15.8	16.4	22.0	8.9	85	41	64	63	2.3	14.8	6.4	7.8	1 ⊙	3 ⊙	7	C 0	E 3	C 0
17	88.3	88.7	90.4	89.1	13.0	19.5	14.3	15.3	21.9	8.8	76	49	82	69	3.6	11.6	2.9	6.0	1 ⊙	4 ⊙	8	C 0	NNE 1	C 0
18	91.5	90.0	86.6	89.4	12.1	20.3	18.3	17.2	21.4	11.4	83	61	70	71	2.3	9.2	6.2	5.9	10	6 ⊙	10	W 2	NNE 1	N 1
19	83.6	81.6	80.2	81.8	16.2	22.0	16.9	18.0	22.5	12.3	78	56	77	70	4.0	11.6	4.4	6.7	1 ⊙	3 ⊙	7	C 0	E 6	ENE 4
20	81.0	82.5	85.9	83.1	14.9	17.8	14.2	15.3	22.5	11.5	85	62	83	77	2.5	7.8	2.7	4.3	7 ⊙	10 ⚑	10	C 0	SSE 2	W 3
21	89.9	91.4	90.6	90.6	10.2	9.8	11.4	10.7	14.2	8.8	88	86	77	84	1.4	1.7	3.1	2.1	10	10 ●	10	WNW 4	WNW 2	W 1
22	88.9	88.3	87.6	88.3	10.1	13.4	13.4	12.6	14.2	9.2	87	56	78	74	1.6	6.8	3.3	3.9	10 ●	10	10	C 0	C 0	C 0
23	86.4	85.5	84.2	85.4	13.6	19.7	17.2	16.9	20.8	11.0	83	61	79	74	2.7	9.0	4.1	5.3	9	8	4	C 0	ESE 2	C 0
24	86.0	87.0	89.8	87.6	14.6	20.8	14.3	16.0	21.2	11.5	89	59	78	75	1.8	10.0	3.6	5.1	10	9	10	C 0	C 0	N 4
25	93.2	95.0	95.9	94.7	11.0	13.1	10.2	11.1	14.3	9.7	61	42	51	51	5.1	8.7	6.1	6.6	6 ⊙	9	10	ESE 3	NE 3	NE 2
26	97.1	97.0	97.1	97.1	7.6	11.3	8.3	8.9	12.0	5.6	68	46	61	58	3.3	7.2	4.3	4.9	9	10	10	E 1	NE 2	ENE 2
27	95.5	95.8	95.8	95.6	6.3	9.8	7.5	7.8	11.1	4.3	70	57	70	66	2.8	5.2	3.1	3.7	10	10	10	NE 2	NE 2	NE 1
28	93.6	93.2	92.7	93.2	6.4	9.6	7.4	7.7	10.5	5.3	78	64	84	75	2.1	4.3	1.6	2.7	10	9	7	NE 1	NNE 2	NE 2
29	93.3	93.7	95.3	94.1	8.1	13.3	10.3	10.5	14.6	4.9	70	44	65	60	3.3	8.6	4.4	5.4	7	7 ⊙	2	NE 2	N 1	W 1
30	96.9	96.0	94.9	95.9	8.4	17.1	14.4	13.6	18.7	4.4	68	32	58	53	3.6	13.2	6.8	7.9	0 ⊙	2 ⊙	8	SSW 1	SSE 1	C 0
31	95.2	93.3	90.7	93.1	10.5	19.4	14.9	14.9	20.2	5.9	69	34	62	55	4.0	14.9	6.4	8.4	1 ⊙	6 ⊙	7	C 0	ESE 1	C 0
M	89.2	89.1	89.1	89.1	9.1	13.7	11.2	11.3	15.4	6.8	81	59	74	71	2.3	7.5	3.6	4.5	6.8	7.5	8.0	1.2	1.9	1.0

Czerwiec – Juin

1	90.7	90.3	90.3	90.4	13.8	20.5	16.8	17.0	22.0	8.2	63	33	60	52	5.9	16.1	7.7	9.9	1 ⊙	6	2	W 2	W 2	C 0
2	92.4	93.0	93.6	93.0	13.8	21.8	17.6	17.7	23.4	9.7	70	36	67	58	4.7	16.7	6.6	9.3	0 ⊙	2 ⊙	1	C 0	WNW 3	C 0
3	95.1	93.2	90.3	92.9	15.4	25.7	21.3	21.0	26.9	11.2	76	36	62	58	4.3	21.2	9.6	11.7	0 ⊙	1 ⊙	10	C 0	W 2	C 0
4	88.1	87.8	85.4	87.1	16.7	21.0	17.3	18.2	24.1	14.7	80	66	90	79	3.9	8.5	2.0	4.8	5 ⊙	10	10	C 0	W 2	C 0
5	82.3	83.8	81.6	82.6	15.4	16.4	15.3	15.6	18.9	12.7	90	71	81	81	1.7	5.4	3.4	3.5	10 ●	9	9	W 5	WSW 4	C 0
6	83.6	85.8	88.1	85.8	13.6	15.1	14.2	14.3	18.2	11.3	75	50	64	63	3.9	8.6	5.8	6.1	7 ⊙	9	1	WNW 3	W 4	C 0
7	88.6	85.8	86.3	87.0	12.6	24.2	16.6	17.5	23.5	7.9	77	43	87	69	3.4	17.4	2.5	7.8	5 ⊙	7 ⊙	10 ●	C 0	SSW 1	C 0
8	86.9	86.8	86.6	86.8	16.4	23.1	17.4	18.6	23.8	13.3	83	56	92	77	3.0	12.5	1.7	5.7	2 ⊙	5 ⊙	2	C 0	N 1	ESE 1
9	86.3	84.9	85.1	85.4	16.7	26.6	19.0	20.3	28.4	13.5	86	46	79	70	2.7	18.7	4.6	8.7	9	9 ⊙	3	C 0	SE 2	WNW 1
10	85.9	85.9	86.7	86.0	17.1	24.0	20.4	20.5	24.6	15.6	80	52	83	72	3.9	14.2	4.2	7.4	10	9 ⚑	4	NE 2	NE 1	C 0
11	86.2	84.5	85.4	85.4	18.8	30.2	25.8	25.2	32.5	14.5	86	46	57	63	3.1	23.0	14.2	13.4	2 ⊙	6 ⊙	10	SE 1	ESE 1	C 0
12	91.4	95.0	101.2	95.9	23.4	28.0	21.0	23.4	28.6	19.2	71	61	74	69	8.4	14.9	6.4	9.9	2 ⊙	9	10	C 0	N 2	NNW 2
13	103.8	103.7	101.7	103.1	16.9	20.6	17.0	17.9	22.7	15.9	78	61	53	64	4.2	9.3	9.2	7.6	10	10	2	C 0	C 0	N 1
14	102.2	101.1	100.6	101.3	14.8	20.7	18.2	18.0	22.9	12.5	73	46	52	57	4.5	13.2	10.1	9.3	6 ⊙	1 ⊙	1	NE 2	WSW 2	NNW 1
15	101.3	100.3	98.2	99.9	15.2	21.4	18.3	18.3	22.8	11.4	65	38	55	53	6.0	15.8	9.4	10.4	1 ⊙	1 ⊙	0	C 0	C 0	C 0
16	96.9	95.5	93.2	95.2	15.3	23.2	19.9	19.6	23.9	11.3	67	40	51	53	5.8	16.9	11.4	11.4	1 ⊙	0 ⊙	0	ESE 1	C 0	E 1
17	93.7	93.0	91.2	92.6	16.9	25.0	20.4	20.7	25.4	11.6	65	41	57	54	6.8	18.7	10.3	11.9	1 ⊙	3 ⊙	0	ENE 1	NE 2	C 0
18	91.0	89.3	86.8	89.0	17.2	26.7	22.1	22.0	27.6	12.6	64	36	54	51	7.1	22.3	12.3	13.9	0 ⊙	1 ⊙	7	C 0	E 1	ENE 1
19	86.4	85.8	85.7	86.0	19.8	23.7	20.0	20.9	26.7	16.5	70	61	68	66	6.9	11.3	7.6	8.6	9 ⊙	6 ⊙	10	C 0	S 2	WNW 2
20	86.1	87.7	90.1	88.0	19.1	19.9	18.2	18.8	21.8	14.9	72	81	81	78	6.2	4.3	4.1	4.9	4 ⊙	10 ●	6	SSW 1	WNW 2	C 0
21	91.8	89.5	86.8	89.4	17.0	24.3	20.8	20.7	24.9	14.8	71	53	78	67	5.6	14.4	5.6	8.5	2 ⊙	8 ⊙	10	E 1	C 0	C 0
22	83.9	82.1	80.4	82.1	19.4	21.0	19.2	19.7	27.8	15.4	82	95	86	88	4.0	1.2	5.2	2.8	2 ⊙	5 ⊙	9	C 0	S 1	SW 2
23	84.6	84.8	83.8	84.4	19.3	25.0	22.0	22.1	27.6	15.9	72	50	72	65	6.2	16.0	7.5	9.9	1 ⊙	8 ⊙	5	SW 1	NW 1	C 0
24	83.2	80.0	78.3	81.2	18.4	27.4	20.5	21.7	31.4	16.1	82	65	88	78	3.9	13.6	2.9	6.8	8 ⊙	4 ⊙	9	C 0	C 0	C 0
25	83.2	86.5	91.4	87.0	18.8	20.7	16.6	18.2	22.7	16.1	57	40	58	52	9.4	14.6	8.0	10.7	1 ⊙	2 ⊙	10 ●	SW 2	W 6	W 2
26	93.2	94.5	96.9	94.9	13.8	16.7	15.0	15.1	18.7	12.8	74	44	63	60	4.1	10.6	6.2	7.0	9 ⊙	9	8	NW 2	NW 1	C 0
27	98.9	98.1	100.1	98.9	11.8	17.2	15.6	15.0	19.1	7.4	75	57	60	64	3.4	8.3	7.1	6.3	1 ⊙	5 ⊙	8	C 0	SW 1	WSW 1
28	100.8	99.0	97.4	99.1	12.2	20.6	19.3	17.8	23.8	8.2	79	42	66	62	3.0	14.0	7.6	8.2	1 ⊙	5 ⊙	1	SW 2	SW 1	WSW 1
29	97.7	97.1	96.6	97.1	18.9	27.6	23.3	23.3	29.6	14.9	74	43	66	62	3.5	20.3	9.6	11.9	0 ⊙	5 ⊙	2	WNW 1	W 1	C 0
30	96.3	94.2	94.0	94.8	20.3	29.2	21.6	23.2	30.4	16.6	73	44	76	64	6.4	22.6	6.1	11.7	0 ⊙	9 ⊙⚑	1	W 1	C 0	W 1
31																								
M	91.1	90.6	90.9	90.7	16.6	22.9	19.0	19.4	24.9	13.2	74	51	69	65	4.9	14.2	6.9	8.7	3.7	5.8	5.4	0.9	1.9	0.6

Kraków, Obserw. Astr. UJ $H_s = 221$ m $H_b = 219{,}8$ m $h_w = 21$ m **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.2	.	.	• ok. 1 •^{0} 12^{14-40}, ok. 15 ; = III
2	7	0.1	.	.	•^{0} na, ok. 12 – 12^{40} ∴ ok. 17, 20 – 20^{40}
3	7	0.2	.	1.1	• na, 12^{10} – ok. 13^{35} ; = III
4	5	0.0	.	1.9	∴^{0} ok. 14 ; = I, II
5	7	0.0	.	3.6	∴^{0} ok. 10
6	7	0.3	.	0.4	•^{0} 8^{45} – ok. 9^{15}
7	7	1.0	.	.	∴ na, ok. 7^{40} – ok. 13^{30} •^{1} a z prz.
8	7	6.0	.	.	• p •^{0} 11^{10} – a •^{1} p – 15^{45} •^{0} p z prz., III
9	7	9.7	.	.	•^{1} na, I, a, II •$^{0-1}$ p, III
10	4	9.2	.	.	• p •^{1} 6^{40} – ok. 12 – 12^{40} •$^{0-1}$ p • np
11	8	.	.	7.2	
12	8	0.2	.	8.4	∴^{1} ok. 11 ; ⌒ 17^{18-31} ; = I
13	7	.	.	12.6	= ⌒^{0} I
14	7	0.8	.	8.1	∴^{0} ok. 11^{30}, 12^{25} •^{1} ok. 12^{35} – 13^{15} ∴^{1} ok. 17^{20} •^{0} ok. 17^{35} (K) 11^{44} – 12^{15}, 17^{10-21} K – 17^{30} SW-SE ; ⌒ 17^{35-37} ; ⌒ I
15	7	.	.	11.0	⌒^{1} I
16	8	.	.	12.2	⊕ ok. 15 ; ⌒^{0} I
17	7	.	.	11.6	⌒^{0} I
18	7	.	.	8.0	
19	8	.	.	11.7	≫ p (wiatr porywisty)
20	8	14.2	.	3.9	•$^{0-1}$ 11^{59} – ok. 14 ▲^{0} 12^{41-44} ; (K) 11^{48} – 12^{40} K – 13^{25} (K) – 14^{40} ; ⌒^{0} I ; = III
21	6	0.8	-	.	• a, II
22	7	0.3	.	.	• na • na, I, a, 13^{25} – ok. 14
23	8	.	.	7.6	= III
24	7	0.0	.	4.8	•^{0} ok. 18^{20-40}
25	8	.	.	4.8	
26	8	.	.	0.7	
27	7	0.0	.	0.1	• ok. 14
28	7	0.1	.	0.5	•$^{0-1}$ p z prz.
29	8	0.0	.	6.2	∴^{0} ok. 14 ; = III
30	8	.	.	10.1	= III
31	8	.	.	8.7	
Σ	—	43.1	—	145.2	UWAGI.

Czerwiec – Juin

1	7	.	.	10.1	= III ; ⌒^{0} I
2	7	.	.	12.1	= I
3	7	.	.	11.4	= ⌒^{0} I
4	7	2.7	.	1.1	∴^{1} ok. 12^{30}, 13 •$^{0-1}$ p – ok. 20 ; = I
5	7	1.6	.	1.5	• na •^{1} I •$^{0-1}$ a – ok. 12 • np ; = ∪ III
6	7	0.0	.	8.8	∴^{0} ok. 10^{30} •^{1} 11^{43} – ok. 12 ∴^{1} 14^{16} ; = III
7	8	10.9	.	9.0	•^{0} p ∴ 16^{37}, 21^{35} • np ; (K) 16^{52} – 17^{57} K – 18^{33} (K) – 19^{50} K 19^{50} (K) – 22^{15} ; ⌒^{0} I
8	7	0.9	.	9.1	• na •^{1} ok. 17
9	8	3.2	.	5.5	•^{1} ok. 18 ∴ 19^{28} ; (K) 18^{14} – 20^{03} ; ∪ III
10	7	0.0	.	7.2	• na ∴ ok. 14 ; (K) 13^{35-50}
11	7	.	.	9.1	= I, III
12	7	.	.	6.4	⌒^{0} I
13	7	.	.	4.1	
14	8	.	.	12.6	
15	8	.	.	14.0	⌒^{0} I
16	8	.	.	14.1	⌒^{0} I
17	8	.	.	13.9	
18	8	.	.	13.6	
19	7	0.0	.	3.9	•^{0} ok. 18^{50-55} ; (K) 17^{16-32} K – 17^{40} (K) – 17^{50} ; = III
20	5	2.0	.	2.7	∴^{0} ok. 11 – ok. 12^{30}, 13^{40}
21	7	0.0	.	9.0	∴^{0} ok. 19^{30}
22	7	11.9	.	6.9	•^{1} 12^{47} – 13^{25} •^{0} 19 – 20^{53} ∴^{1} 21^{11} •^{0} – 21^{35} ∴^{0} np ; K 12^{57} – 13^{02} (K) 13^{07-23} K 20^{53} – 21^{11} (K) – 21^{37} ; ⌒^{0} I
23	8	.	.	9.2	⌒^{1} I
24	8	0.0	.	6.9	∴^{0} ok. 17 ; = III
25	7	0.8	.	10.6	•^{0} III, np ; ≫ a
26	8	0.0	.	1.8	∴^{0} ok. 17
27	7	0.3	.	7.7	∴^{1} ok. 12 ∴$^{0-1}$ p ; ⌒^{0} I
28	7	.	.	10.5	⌒^{0} I
29	6	.	.	10.0	⌒^{0} I
30	6	1.1	.	7.6	∴ p ▲^{0} 13^{58} ; (K) 11^{50} – 13^{48} K – 14^{01} NW-SE (K) – 19 ; = I, III
31					
Σ	—	35.4	—	250.4	UWAGI.

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°57' — Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	94.1	92.9	92.3	93.1	20.4	29.6	24.8	24.9	30.2	16.7	79	45	64	63	5.1	22.9	11.3	13.1	0 ⊙	3 ◯	2	C 0	C 0	C 0
2	91.4	89.7	91.6	90.9	20.8	28.7	20.8	22.8	30.7	17.3	76	49	85	70	6.0	20.0	3.6	9.9	0 ⊙	5 ⊙	10 ☈	C 0	SSE 2	C 0
3	93.2	94.4	93.6	94.4	17.8	23.2	20.1	20.3	24.7	16.8	65	42	61	56	7.1	16.5	9.2	10.9	3 ⊙	1 ◯	1	W 1	NNW 2	C 0
4	93.1	91.9	91.3	92.1	16.6	28.4	25.9	24.2	30.5	12.5	76	39	63	59	4.6	23.5	12.4	13.5	3 ⊙	2 ◯	2	C 0	S 1	C 0
5	91.0	89.0	89.8	89.9	25.0	34.7	28.3	29.1	35.2	20.4	61	22	54	46	12.5	42.9	17.5	24.3	0 ⊙	1 ◯	10 ●☈	W 2	WSW 4	W 2
6	94.0	94.7	93.9	94.2	22.3	27.0	23.6	24.1	28.7	21.0	69	48	58	58	8.2	18.5	12.3	13.0	1 ⊙	5 ⊙	1	C 0	WNW 1	C 0
7	95.0	94.0	92.8	93.9	20.2	25.9	24.4	23.7	28.4	16.4	69	61	72	67	7.3	13.1	8.7	9.7	10	1 ⊙	0	C 0	C 0	C D
8	92.1	89.8	87.8	89.9	20.8	33.1	26.2	26.6	34.2	17.4	78	47	58	61	5.6	27.0	14.2	15.6	3 ◯	2 ◯	10 (☈)	C 0	C 0	WSW 4
9	87.3	88.8	88.4	88.2	21.5	24.4	21.7	22.3	26.2	18.2	87	64	78	76	3.4	11.2	5.8	6.8	3 ⊙	10	7	C 0	W 2	N 1
10	87.9	85.0	82.3	85.1	18.8	24.9	21.6	21.7	25.3	17.9	86	57	61	68	3.1	13.6	10.1	8.9	10	8 ⊙	10	ENE 2	ESE 1	ENE 1
11	79.2	79.7	80.9	79.9	18.8	23.7	17.9	19.6	24.6	16.5	67	64	95	75	7.1	10.4	1.0	6.2	2 ◯	10 (☈)	9	NE 2	W 1	C 0
12	81.4	83.2	83.3	83.3	18.2	23.4	20.4	20.6	24.3	16.6	92	66	89	82	1.7	9.7	2.7	4.7	10	10	10	C 0	C 0	C 0
13	88.9	90.2	90.9	90.0	18.9	24.6	21.8	21.8	25.7	17.5	89	59	84	77	2.3	12.7	4.2	6.4	10	10	9	C 0	C 0	C 0
14	90.6	89.9	88.3	89.6	21.8	19.6	20.8	20.8	25.4	18.8	81	90	84	85	5.1	2.2	4.1	3.8	9 ⊙	10 ●	9	C 0	C 0	C 0
15	87.4	87.1	86.8	87.1	17.9	21.3	20.2	19.9	23.8	16.2	88	68	80	79	2.4	8.1	4.8	5.1	10 ≡	8	10	W 2	W 2	C 0
16	83.2	80.7	82.5	82.1	16.1	16.4	14.8	15.5	20.2	14.2	98	89	92	93	0.4	2.1	1.3	1.3	10 ●	10 ●	10 ●	N 1	W 4	W 4
17	82.6	84.0	85.8	84.1	13.5	14.7	14.9	14.5	16.5	12.5	91	89	79	86	1.5	1.8	3.4	2.2	10 ●	10 ●	10	WNW 4	W 4	W 3
18	86.8	86.7	85.4	86.3	15.6	20.3	17.6	17.8	22.6	13.8	79	52	74	68	3.7	11.3	5.3	6.8	9	10	6	WNW 2	WSW 2	SW 1
19	84.9	84.0	82.7	83.9	15.4	25.2	20.8	20.6	25.9	12.1	84	45	69	66	2.8	17.7	7.6	9.4	0 ⊙	2 ⊙	3	C 0	S 1	C 0
20	81.4	78.7	79.2	79.8	18.8	27.6	17.4	20.3	28.1	14.6	79	45	89	71	4.3	20.5	2.3	9.1	5 ◯	7 ◯	10 ●	ENE 2	SSE 1	NNW 1
21	78.6	79.1	78.8	78.8	14.6	15.3	16.2	15.6	17.4	14.2	98	93	89	93	0.4	1.2	1.9	1.2	10 ●	10 ●	10	W 2	W 3	C 0
22	77.6	76.5	77.8	77.3	15.3	20.9	15.7	17.0	21.8	14.3	90	63	87	80	1.7	9.0	2.2	4.3	10	9 ◯	10	SW 1	NW 2	W 2
23	76.4	77.6	80.2	78.1	15.3	21.2	17.8	18.0	22.1	11.9	85	61	87	78	2.6	9.8	2.6	5.0	9	9 ⊙	10	ENE 1	C 0	WSW 1
24	81.2	83.7	86.3	83.7	17.4	16.4	15.3	16.1	18.9	14.8	89	94	83	89	2.3	1.1	3.0	2.1	10	10 ●	6	WNW 1	W 3	WNW 3
25	87.3	87.3	85.4	86.7	15.0	19.4	16.7	17.0	20.1	13.3	84	58	77	73	2.7	9.3	4.4	5.5	10	10	10	W 2	WNW 4	C 0
26	86.0	85.5	85.0	85.5	14.9	20.7	17.2	17.5	23.2	13.3	83	44	89	72	2.9	13.6	2.2	6.2	10	4 ⊙	10 ●	WNW 2	W 5	W 2
27	82.4	81.3	82.2	82.0	17.1	20.8	16.5	17.7	22.2	14.8	84	66	89	80	3.2	8.4	2.2	4.6	10 ●	10 ●	10 ●	C 0	W 1	C 0
28	82.9	83.7	84.9	83.8	14.7	18.8	16.0	16.4	21.4	13.4	75	59	86	73	4.1	8.8	2.5	5.1	10	5 ⊙	1	C 0	WNW 4	W 1
29	85.9	87.0	89.2	87.4	14.3	20.0	16.7	16.9	22.0	10.8	84	54	80	73	2.5	10.9	3.9	5.8	8 ⊙	8	2	C 0	SW 2	C 0
30	91.4	91.6	94.0	92.3	15.5	21.2	15.6	17.0	23.6	12.7	78	52	90	73	3.9	12.1	1.7	5.9	5 ⊙	6 ⊙	10 ●	W 1	WNW 1	W 2
31	95.7	96.7	97.9	96.8	15.3	18.5	17.1	17.0	21.6	14.2	90	75	82	82	1.7	5.3	3.5	3.5	10 ●	9	9	C 0	W 2	W 1
M	86.9	86.6	86.9	86.8	17.7	22.9	19.5	19.9	24.7	15.3	82	60	78	73	3.9	12.7	5.5	7.4	6.8	6.9	7.3	0.9	1.8	0.9

Sierpień – Août

1	99.5	98.5	97.1	98.4	13.1	19.0	17.2	16.6	21.6	12.5	92	61	81	78	1.3	8.5	3.7	4.5	9	5 ◯	9	C 0	SW 1	W 1
2	96.8	95.3	95.7	95.9	14.3	22.0	17.5	17.8	23.6	12.0	87	59	68	71	2.2	10.8	6.4	6.5	9 ◯	8 ◯	9	W 1	WNW 2	NW 1
3	96.7	95.4	95.6	95.9	13.6	18.8	16.0	16.1	21.5	11.9	75	47	67	63	3.9	11.5	6.0	7.1	0 ◯	6 ◯	10	C 0	W 2	WNW 2
4	95.5	95.1	95.8	95.5	13.6	18.3	17.4	16.7	21.4	12.4	80	61	72	71	3.2	8.3	5.5	5.7	2 ⊙	9	9	W 2	WNW 4	W 1
5	96.6	96.3	96.3	96.4	14.4	19.5	16.6	16.8	22.2	12.5	83	66	79	76	2.7	7.7	4.1	4.8	7 ◯	5 ◯	2	WNW 3	W 1	C 0
6	96.9	96.0	94.1	95.7	13.8	22.2	18.6	18.3	24.2	11.4	88	59	73	73	2.0	11.0	5.9	6.3	0 ◯	6	4	C 0	C 0	N 1
7	91.8	88.2	85.0	88.3	15.7	25.1	20.3	20.4	26.3	13.1	84	44	71	66	2.8	17.6	6.8	9.1	3 ⊙	9	9	C 0	SSW 1	C 0
8	83.7	84.9	84.8	84.5	16.9	20.3	17.8	18.2	22.7	16.4	85	61	83	76	2.9	9.2	3.4	5.2	9	8 ◯	5	WSW 2	WNW 1	C 0
9	84.2	82.4	79.2	81.9	15.0	23.5	19.5	19.4	24.6	12.8	89	54	77	73	1.8	13.3	5.3	6.8	8 ⊙	4 ◯	1	C 0	C 0	C 0
10	76.5	80.6	83.7	80.3	17.8	19.2	18.8	18.6	23.5	15.7	81	79	80	80	3.8	4.6	4.3	4.2	10	9	6	C 0	WNW 5	W 1
11	88.2	88.4	87.8	88.1	17.8	26.8	23.4	22.8	27.9	15.9	82	45	74	67	3.6	19.2	7.4	10.1	1 ⊙	5 ◯	1	C 0	S 1	C 0
12	85.9	85.7	87.1	86.2	19.5	26.5	22.6	22.8	28.8	16.9	79	57	71	69	4.7	14.8	7.9	9.1	1 ⊙	5 ◯(☈)	9	ENE 1	W 2	C 0
13	88.7	89.0	87.8	88.5	19.9	26.8	23.1	23.2	28.1	18.4	91	57	77	75	2.0	15.2	6.4	7.9	2 ⊙	3 ⊙	9	C 0	C 0	C 0
14	85.1	85.6	85.6	84.8	20.0	26.8	22.6	23.0	28.6	18.1	91	63	85	80	2.2	13.1	4.0	6.4	0 ⊙	1 ⊙	10	C 0	W 2	WSW 10
15	84.4	84.4	85.1	84.6	17.9	22.7	20.6	20.4	24.7	16.1	88	53	74	72	2.4	13.0	6.3	7.2	6 ⊙	3 ⊙	9	C 0	C 0	C 0
16	85.4	84.5	86.5	85.5	16.9	25.5	15.8	18.5	25.9	15.4	89	53	88	77	2.1	15.4	2.1	6.5	0 ⊙	3 ⊙	8	C 0	ESE 4	WNW 2
17	86.0	87.7	86.7	86.8	13.8	14.1	15.3	14.6	18.0	12.9	90	89	76	85	1.6	1.8	4.3	2.6	10 ●	10 ●	9	W 4	WSW 3	W 2
18	86.5	85.7	86.4	86.2	14.2	20.3	15.6	16.4	22.0	11.3	79	56	81	72	3.4	10.4	3.4	5.7	1 ⊙	7 ⊙	0	SW 2	SW 4	W 1
19	88.2	89.0	91.2	89.5	13.7	20.0	17.7	17.3	21.4	11.8	89	64	79	77	1.8	8.4	4.2	4.8	9 ⊙	9	10 ●	SW 1	C 0	W 1
20	91.9	92.5	92.6	92.3	15.6	19.0	15.8	16.6	20.1	14.5	91	73	88	84	1.5	6.0	2.1	3.2	10	10 ●	3	C 0	C 0	C 0
21	91.5	88.8	85.9	88.7	13.4	22.4	19.4	18.6	23.0	11.5	91	53	76	73	1.4	12.8	5.4	6.5	0 ⊙	1 ⊙	9	W 1	C 0	C 0
22	83.9	86.0	86.6	85.5	14.2	13.1	12.2	12.9	19.4	11.9	92	93	87	91	1.3	1.1	1.9	1.4	10 ●	10 ●	1	W 2	NW 2	NW 1
23	87.9	88.0	87.3	87.7	10.8	15.8	13.3	13.3	18.4	8.7	87	62	86	78	1.7	6.7	2.1	3.5	4 ⊙	4 ⊙	2	C 0	WNW 2	C 0
24	86.2	83.6	87.3	85.7	9.5	23.9	14.4	15.6	24.5	7.7	93	47	89	76	0.8	15.7	1.8	6.1	0 ⊙	2 ⊙	10 ●	C 0	SW 2	SW 2
25	92.3	90.7	87.5	90.2	12.7	20.7	16.1	16.4	22.1	11.0	92	41	81	71	1.2	14.3	3.4	6.3	1 ⊙	2 ⊙	4	C 0	WSW 1	C 0
26	86.5	86.0	87.9	86.8	12.3	19.1	14.0	14.8	20.5	10.1	85	53	79	72	2.2	10.4	3.4	5.3	4 ⊙	9	2	C 0	WNW 6	C 0
27	89.7	89.7	88.8	89.4	11.9	18.8	14.3	14.9	20.0	9.4	80	52	80	71	2.8	10.4	3.2	5.5	0 ⊙	3 ⊙	6	C 0	W 3	C 0
28	88.0	87.9	88.4	88.1	12.8	18.1	15.4	15.4	19.9	12.3	96	66	89	84	0.5	7.2	1.9	3.2	10	7 ⊙	8	C 0	WSW 1	C 0
29	89.0	90.9	93.0	91.0	12.5	13.2	12.6	12.7	15.4	11.8	96	91	89	92	0.3	1.4	1.6	1.2	10 ●	10 ●	9	NW 2	WNW 1	W 2
30	93.9	94.6	94.4	94.3	10.9	15.4	12.3	12.8	17.0	9.7	91	63	88	81	1.1	6.5	1.7	3.1	9 ⊙	6 ⊙	7	W 3	WSW 2	W 1
31	94.0	92.6	92.0	92.9	10.0	18.6	12.8	13.6	20.0	8.4	89	50	86	75	1.3	10.7	2.1	4.7	3 ⊙	9 ⊙	10 ●	C 0	WSW 2	W 1
M	89.4	89.2	89.1	89.2	14.5	20.5	17.1	17.3	22.5	12.7	87	60	80	76	2.2	10.2	4.1	5.5	4.8	6.1	6.5	0.8	1.8	1.0

Kraków, Obserw. Astr. UJ $H_s = 221$ m $H_b = 219{,}8$ m $h_w = 21$ m Lipiec – Juillet 1957

DNI	WI. DZIAŁ. NOŚĆ V	OPAD R	GRUB. ŚNIEG. h	USŁO. NECZ. NIENIE	POGODA
1	7	.	.	12.4	⌒⁰ /
2	7	8.9	.	7.6	▽¹ 17^{30}, 18^{41} – 19^{20} ●² 20^{55} – np; (K) 12^{17-20}, 14^{21}, 21^{55} K – 22^{42} (K) – 22^{53}
3	8	.	.	12.1	
4	8	.	.	12.6	⌒⁰ /
5	7	1.6	.	12.4	●⁰ 21^{48} – np; (K) 19^{12-45} K – 19^{56} (K) – 22^{38}
6	7	.	.	11.3	▽ 1^{57} ●⁰ – ok. 2^{10}; K 1^{52-59} (K) 2^{07} – ok. 2^{30}
7	7	0.0	.	7.7	▽¹ ok. 9^{30}
8	7	20.5	.	10.1	●⁰ 15^{10} – p ▽ ok. 15^{15-34} ▲ 15^{32} 15^{43} ▽ ok. 20; K 15^{05-12} NE-SW (K) 15^{34} – np; = /
9	7	.	.	6.9	▽ na; K ok. 2^{30} – 3^{30} (K) na
10	8	.	.	6.5	
11	7	14.7	.	5.0	▽ 14^{10} – ok. 14^{30} ●⁰ p; (K) 13^{40} – ok. 16.
12	7	0.2	.	1.2	●¹ ok. 16^{30} – ok. 19 ●⁰ p; (K) ok. 16; = /
13	7	.	.	1.4	= /
14	4	2.7	.	2.5	●¹ a, II, p; (K) ok. 12; = /
15	6	28.9	.	1.5	▽¹ p; ≡⁰ /
16	7	30.6	.	.	●²⁻¹ na, / a – ok. 13 ●⁰ – 13^{40} ●¹⁻² p, III ● np; (K) na
17	6	3.3	.	.	● na, / ●¹ a, II ●⁰ p – ok. 17
18	7	.	.	7.2	= /
19	7	.	.	9.9	= /
20	8	14.8	.	8.4	▽¹ 16^{10} ●¹⁻² 18^{30} – np; (K) ok. 16 – ok. 19^{30}; = /
21	5	8.7	.	.	●¹ na, / a ●⁰ II ▽ p z prz.
22	7	1.9	.	2.3	●¹ (K) ok. 15 – 16^{30}
23	7	0.0	.	2.1	▽⁰ ok. 16^{30}
24	6	11.2	.	0.6	●¹⁻² a, II ●⁰⁻¹ p – ok. 16; = /
25	7	4.5	.	2.5	= /
26	8	2.9	.	6.6	● na ▽⁰ p ●⁰⁻¹ 21^{10} – np
27	9	2.7	.	0.5	●¹⁻² na, / ▽¹⁻² a z prz, II ▽⁰ p ●¹ ok. 19 – np
28	9	0.0	.	3.8	⌒ 18^{20}
29	8	.	.	6.3	▽⁰ 6^{50}
30	7	1.1	.	7.1	▽² ok. 20^{15} ●⁰ ok. 21 – ok. 22; ⌒¹ /
31	7	0.0	.	1.4	▽⁰ 6^{10}, ok. 7^{30} – 8^{15} ▽¹ – 15^{18}
Σ	–	159.2	–	172.1	UWAGI.

Sierpień – Août

1	7	.	.	6.2	
2	7	.	.	4.5	= /
3	8	.	.	8.2	⌒⁰ /
4	7	.	.	5.7	⌒² /
5	7	.	.	6.6	∪ III
6	8	.	.	9.3	⌒⁰ / ∪ III
7	7	10	.	5.9	▽⁰ 19^{15}; ⌒² /; ≤ ∪ III
8	7	.	.	4.9	● na; (K) ok. 0^{30} – na
9	7	.	.	10.6	≡⁰ na, = /
10	7	0.4	.	2.7	●¹ 10^{05-15} ●⁰ – ok. 12, 21^{30} .. np
11	8	.	.	11.5	⌒² /
12	7	1.2	.	10.9	(K) 13^{18-52} E ≤ ok. 20^{45} – np; ⌒¹ /
13	7	0.0	.	8.4	● na; ≤ ok. 21^{15}
14	7	1.6	.	9.0	▽¹ na ●¹ 21^{30-33} ●² – 22^{45} ●⁰ 22^{50} – np; (K) na, 21^{07} – np K² 21^{20-45} NW-SE; ≫ ok. 20 – np
15	7	.	.	10.4	● na
16	7	25.8	.	7.1	●¹⁻² 15^{50} np ▽ 22^{35}, 22^{48} (K) 15^{12-31} K – 16^{01} (K) – 17^{55}; = ⌒² /
17	6	4.3	.	3.7	●¹ 6^{55} – 8, a z prz. ▽ 13^{31} – ok. 13^{40} ●¹ p – ok. 14^{15}
18	8	.	.	9.3	⌒² /
19	7	0.2	.	1.4	▽¹ ok. 14^{30} ▽⁰ 21^{55}; = /
20	7	0.8	.	0.3	● na ●¹ 13^{42} – ok. 15; ≤ ok. 21^{30}; = I, III
21	7	3.6	.	7.7	≡¹ na; = ⌒² /
22	7	9.9	.	0.3	●¹⁻² 5^{45} – 8, a ●¹ p – ok. 15, ok. 20 – 20^{15}
23	7	.	.	8.6	
24	8	2.3	.	9.7	●¹ ok. 20^{30} – np; = ⌒² /
25	8	.	.	11.6	
26	7	0.0	.	8.4	▽⁰ 14^{03}; = ⌒¹
27	8	1.6	.	10.2	⌒¹ /
28	7	20.2	.	2.6	●¹ na – ok. 7^{30}, ok. 19 – 19^{30}; = /
29	6	6.4	.	.	●¹⁻² na ●¹ a – ok. 18
30	6	.	.	2.8	≡ I, III
31	8	1.6	.	4.7	●⁰ ok. 15^{40} – ok. 16 ▽ ok. 19^{20} – np △ 20^{42} (ok. 20 sek); = ⌒¹ /
Σ	–	80.9	–	203.2	UWAGI.

Kraków, Obserw. Astr. UJ — $\varphi = 50°04'$ — $\lambda = 19°57'$ — Wrzesień – Septembre 1957

DNI	CIŚNIENIE P=900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	92.0	92.6	93.7	92.8	11.8	16.0	11.9	12.9	17.4	10.4	87	55	85	76	1.8	8.2	2.0	4.0	10	10 ●	9	C 0	WNW 5	C 0
2	93.7	92.1	89.9	91.9	9.4	20.0	15.7	15.2	22.0	7.4	93	57	87	79	0.8	10.1	2.2	4.4	3 ⊙	9 ⊙	8	C 0	SW 1	C 0
3	89.3	89.9	89.9	89.7	12.8	17.6	14.7	15.0	18.9	12.3	99	69	93	87	0.2	6.2	1.1	2.5	10 ●	9	10 ●	W 1	C 0	C 0
4	90.8	92.8	96.0	93.2	13.2	14.8	12.6	13.5	15.5	12.3	94	88	92	91	0.9	2.0	1.2	1.4	10	10 ●	10 ●	NNE 1	NNE 1	C 0
5	96.3	95.1	93.7	95.0	12.5	17.7	15.2	15.2	18.6	11.3	95	66	87	83	0.7	6.8	2.3	3.3	10	8 ⊙	10	C 0	C 0	C 0
6	92.8	91.8	92.3	92.3	10.3	20.4	15.7	15.5	21.9	8.8	100	57	87	81	0.0	10.3	2.2	4.2	4 ⊙≡	4 ⊙	5	C 0	C 0	C 0
7	94.4	94.3	94.3	94.3	11.7	21.1	16.0	16.2	22.0	10.6	98	59	88	82	0.3	10.3	2.1	4.2	2 ⊙≡	1 ⊙	1	C 0	ESE 1	C 0
8	95.7	95.7	95.6	95.7	11.6	24.4	18.8	18.4	25.8	10.7	96	54	87	79	0.5	14.0	2.7	5.7	1 ⊙	0 ⊙	2	C 0	C 0	C 0
9	96.0	95.2	95.2	95.5	13.8	25.4	19.8	19.7	26.9	11.7	93	53	83	76	1.1	15.3	3.9	6.8	1 ⊙	0 ⊙	4	C 0	C 0	C 0
10	95.4	94.8	93.2	94.5	16.2	15.8	15.0	15.5	19.8	14.5	90	96	92	93	1.7	0.7	1.3	1.2	10	10 ●	10	C 0	C 0	C 0
11	90.2	86.1	80.9	85.7	12.1	19.0	17.1	16.3	20.7	10.4	99	58	79	79	0.1	9.3	4.1	4.5	10 ⊙≡	2 ⊙	10 ●	C 0	C 0	C 0
12	75.1	74.1	80.6	76.6	17.7	22.4	14.0	17.0	23.2	13.7	83	53	72	69	3.4	12.6	4.4	6.8	7 ⊙	9 ⊙	10	C 0	W 3	W 2
13	84.6	84.0	81.4	83.3	10.8	17.8	13.2	13.8	19.2	9.0	79	46	72	66	2.8	11.0	4.3	6.0	2 ⊙	4 ⊙	9	C 0	S 2	C 0
14	83.2	83.2	82.6	83.0	10.5	16.9	13.1	13.4	18.4	9.6	75	53	72	67	3.2	8.9	4.3	5.5	1 ⊙	8 ⊙	10 ●	W 2	WSW 1	W 1
15	80.8	84.1	89.2	84.7	8.7	14.0	11.0	11.2	15.8	8.1	90	61	86	79	1.0	6.2	1.8	3.0	10 ●	5	10	W 2	WSW 4	C 0
16	91.3	90.9	92.2	91.5	9.1	14.7	9.1	10.5	16.7	7.8	89	41	88	75	1.3	9.9	1.4	4.2	1 ⊙	4	2	C 0	W 3	C 0
17	92.5	91.2	88.7	90.8	7.5	10.8	9.2	9.2	12.2	6.1	93	86	96	92	0.8	1.8	0.4	1.0	2 ⊙	10	3	C 0	WNW 2	C 0
18	86.5	86.4	90.4	87.8	9.4	13.9	9.4	10.5	15.2	8.5	93	57	87	79	0.8	6.9	1.6	3.1	10● ≡	5 ⊙	2	W 4	WNW 7	W 1
19	86.9	85.1	83.2	85.1	9.0	15.2	13.6	12.8	16.2	7.9	92	70	90	84	1.0	5.1	1.6	2.6	3 ⊙	10	10 ●	C 0	W 4	W 2
20	83.4	86.2	89.4	86.3	13.2	12.9	10.3	11.7	15.0	9.9	93	92	95	93	1.1	1.3	0.6	1.0	10 ●	10	10	WNW 2	W 1	C 0
21	90.5	90.8	89.6	90.3	6.8	14.7	11.0	10.9	15.7	5.2	97	69	92	86	0.3	5.2	1.0	2.2	8 ⊙	6 ⊙	3	C 0	ENE 1	C 0
22	87.5	86.5	86.8	86.9	8.2	18.7	15.2	14.3	20.9	7.0	99	79	92	90	0.2	4.6	1.3	2.0	2 ⊙	6 ⊙	7	C 0	W 1	W 1
23	83.1	79.3	77.7	80.0	12.8	19.6	16.0	16.1	21.9	11.8	99	76	90	88	0.2	5.5	1.8	2.5	7 ⊙	10 ●	10	C 0	W 2	WNW 2
24	81.5	80.8	85.1	82.5	13.5	18.8	9.2	12.7	20.1	8.9	94	59	88	80	0.9	9.0	1.4	3.8	9 ●	8 ⊙	10 ●	W 1	W 4	W 1
25	89.3	91.3	93.2	91.3	6.3	10.7	6.3	7.4	12.8	5.5	84	52	86	74	1.5	6.3	1.2	3.0	2 ⊙	6	6	W 5	W 6	C 0
26	91.2	90.4	91.7	91.1	4.6	10.5	7.3	7.4	11.5	3.3	89	63	86	79	1.0	4.7	1.5	2.4	4 ⊙	10	4	C 0	C 0	C 0
27	92.6	93.2	86.8	90.9	3.2	9.8	9.5	8.0	11.5	1.7	98	56	68	74	0.2	5.3	3.9	3.1	0 ⊙	4 ⊙	10 ●	C 0	W 3	WNW 2
28	81.9	82.3	83.7	82.6	10.2	13.6	9.6	10.8	14.7	8.3	82	64	91	79	2.2	5.7	1.2	3.0	7 ⊙	7 ⊙	10 ●	W 4	WNW 9	WNW 3
29	81.6	78.8	75.2	78.5	8.9	14.0	10.5	11.0	14.4	8.1	96	69	99	88	0.5	4.9	0.2	1.9	10	10	10	C 0	SW 2	C 0
30	80.1	82.8	88.9	83.9	7.4	9.6	7.6	8.0	11.7	6.5	90	53	80	74	1.0	5.7	2.0	2.9	9	8	10	W 4	NW 5	W 2
31																								
M	88.3	88.1	88.4	88.3	10.4	16.4	12.6	13.0	17.9	8.9	92	64	86	81	1.0	7.1	2.0	3.4	5.8	6.6	7.5	0.9	2.2	0.6

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1	90.9	91.0	92.7	91.5	4.8	10.4	5.7	6.6	11.9	4.2	97	63	92	84	0.3	4.7	0.8	1.9	10	9 ⊙	10	C 0	SSE 1	WNW 1
2	97.6	98.0	97.8	97.8	3.5	8.8	3.4	4.8	9.1	2.9	93	63	91	82	0.5	4.2	0.7	1.8	9 ⊙	5 ⊙	1	WSW 1	NNE 1	C 0
3	95.9	90.9	88.5	91.1	−1.5	11.7	8.7	6.9	12.6	−1.9	99	46	73	73	0.1	7.4	3.0	3.5	2 ⊙≡	3 ⊙	10	C 0	WSW 1	C 0
4	87.4	90.1	95.8	91.1	8.0	8.3	5.0	6.6	9.8	4.4	85	57	81	74	1.5	4.8	1.6	2.6	10	3 ⊙	3	C 0	NNW 2	WSW 2
5	98.7	98.4	96.7	97.9	4.6	10.4	5.3	6.3	11.8	2.2	85	50	89	75	1.3	6.3	1.0	2.9	9	3 ⊙	1 ≡	W 1	WSW 3	C 0
6	95.3	96.5	99.8	97.2	3.7	11.4	8.0	7.8	13.5	3.1	93	58	94	82	0.6	5.6	0.6	2.3	10	9	3	C 0	W 3	C 0
7	100.1	99.4	100.2	99.9	5.7	15.1	9.0	9.7	16.0	5.1	97	55	95	82	0.3	7.8	0.7	2.9	0≡	8 ⊙	3	C 0	WNW 2	C 0
8	101.3	102.7	103.0	102.3	9.0	13.8	9.3	10.4	14.1	7.3	95	79	93	89	0.7	3.4	0.8	1.6	10 ≡	7 ⊙	1	C 0	ESE 1	C 0
9	101.1	99.9	98.5	99.8	3.0	15.5	10.2	9.7	18.4	2.5	100	65	82	82	0.0	6.2	2.2	2.8	10 ≡	0 ⊙	1	C 0	SE 1	C 0
10	98.1	97.1	96.6	97.3	3.7	16.8	11.0	10.6	19.2	3.4	97	59	90	82	0.3	7.9	1.3	3.2	2 ⊙	0 ⊙	1	C 0	C 0	C 0
11	97.1	96.1	95.5	96.2	3.8	16.2	10.0	10.0	17.9	3.3	97	57	91	82	0.3	7.9	1.1	3.1	0≡	1 ⊙	3	C 0	C 0	C 0
12	96.2	95.8	99.4	97.1	4.5	16.5	13.4	12.0	17.7	4.2	95	58	84	79	0.4	7.8	2.5	3.6	0 ⊙	3 ⊙	10	C 0	W 2	WNW 1
13	101.8	100.8	99.0	100.5	10.8	15.8	10.6	12.0	16.4	10.2	95	69	91	85	0.7	5.5	1.2	2.5	9	2 ⊙	8	C 0	C 0	C 0
14	98.2	97.6	98.7	98.2	8.0	17.4	13.9	13.5	18.1	6.3	96	59	83	79	0.4	8.3	2.7	3.8	9 ≡	4 ⊙	10	C 0	SW 2	C 0
15	101.9	101.4	101.9	101.7	6.7	13.1	10.2	10.0	13.9	6.2	100	67	87	85	0.0	5.0	1.6	2.2	10 ≡	8 ⊙	10	C 0	C 0	C 0
16	100.7	98.6	96.3	98.5	4.7	13.5	8.9	9.0	15.2	4.4	98	70	93	87	0.1	4.7	0.8	1.9	0 ⊙	0 ⊙	1	C 0	E 1	C 0
17	94.2	94.0	95.4	94.5	3.8	18.1	12.4	11.7	19.0	3.5	97	57	87	80	0.3	9.0	1.9	3.7	0≡	1 ⊙	10	C 0	WSW 2	W 1
18	92.0	89.2	88.1	89.8	10.8	19.3	15.4	15.2	20.3	10.2	94	46	66	69	0.9	12.1	6.0	6.3	9 ≡	9 ⊙	3	C 0	WSW 2	WSW 1
19	87.5	85.7	84.3	85.8	7.9	19.0	13.1	13.3	21.7	7.4	90	47	76	71	1.0	11.6	3.6	5.4	6 ⊙	10 ⊙	4	C 0	ENE 1	ESE 1
20	83.7	87.0	90.9	87.2	9.1	11.2	9.2	9.7	13.1	8.2	91	94	96	94	1.1	0.8	0.4	0.8	4 ⊙	10	10 ●	W 1	W 1	C 0
21	91.7	90.9	88.0	90.2	8.6	10.9	6.2	8.0	11.4	5.9	97	79	95	90	0.3	2.7	0.5	1.2	10	7 ⊙	3	C 0	C 0	C 0
22	82.9	80.2	77.8	80.3	2.8	9.0	9.5	7.7	9.7	1.2	98	88	91	92	0.2	1.4	1.1	0.9	9	10 ●	10	C 0	C 0	C 0
23	80.3	84.2	89.6	84.7	8.9	9.4	7.9	8.5	10.6	7.4	99	88	95	93	0.2	1.4	0.7	0.8	10≡ ●	10	10	C 0	WNW 1	C 0
24	90.9	91.3	95.8	92.7	3.2	10.4	9.4	8.1	11.4	2.9	100	60	82	81	0.0	5.0	2.2	2.4	10 ≡	9	10	C 0	WNW 5	WSW 3
25	99.0	99.6	100.1	99.6	8.4	12.5	6.5	8.5	13.0	6.2	94	61	90	82	0.6	5.7	1.0	2.4	9	6 ⊙	0	C 0	C 0	C 0
26	99.3	98.4	96.8	98.2	1.8	10.8	8.0	7.2	13.3	1.4	96	81	93	90	0.3	2.5	0.7	1.2	7 ≡	1 ⊙	0	C 0	C 0	C 0
27	95.6	94.0	93.8	94.5	1.7	13.5	10.2	8.9	15.0	1.4	98	70	88	85	0.1	4.7	1.4	2.1	8 ≡	2⊙≡	9	C 0	C 0	C 0
28	94.4	94.5	95.0	94.6	8.5	11.8	8.1	9.1	12.6	7.6	93	78	97	89	0.8	3.0	0.3	1.4	8	10	9	C 0	C 0	W 1
29	95.1	94.4	94.0	94.5	4.5	13.4	7.4	8.2	14.3	3.9	100	60	95	84	0.0	6.2	0.8	2.3	10 ≡	4 ⊙	4 ≡	C 0	W 4	C 0
30	92.4	90.4	90.9	91.2	4.4	14.6	9.6	9.6	16.6	3.9	97	63	88	83	0.3	6.2	1.3	2.7	9 ⊙	3 ⊙	4	C 0	C 0	C 0
31	90.7	89.1	87.9	89.2	6.9	13.2	9.7	10.4	15.9	6.3	96	59	93	83	0.4	7.2	0.8	2.8	2 ≡	1 ⊙	4	C 0	W 1	C 0
M	94.5	94.1	94.3	94.4	5.6	13.3	9.2	9.3	14.6	4.7	96	65	88	83	0.5	5.7	1.5	2.6	5.8	5.1.	5.4	0.1	1.2	0.4

Kraków, Obserw. Astr. UJ $H_s = 221$ m $H_b = 219{,}8$ m $h_w = 21$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.0	.	5.6	$\overset{\bullet}{\triangledown}{}^{0}$ ok. 13^{40} ; = III
2	7	2.4	.	6.5	= ⌒ I ; ⋓ III
3	7	4.9	.	2.2	• na – ok. 11 , 20^{40} – np
4	5	5.6	.	.	• n, a • $^{1-2}$ 11^{30} – 13^{40} • $^{0-1}$ – np ; = I
5	7	.	.	2.7	= I
6	7	.	.	6.1	≡ ^{1} I = III
7	7	.	.	10.0	≡ ^{0} I ; ⌒ I ; ⋓ III
8	7	.	.	10.5	= ⌒ I
9	7	.	.	10.4	= ⌒ I ; ⋓ III
10	4	0.2	.	.	• ok. 10 ... ok. 14^{30} ; = I
11	7	0.3	.	6.2	• ^{0} ok. 20^{15} – np ; ≡ ^{1} I
12	9	1.0	.	4.7	• $^{0-1}$ 15^{30} – ok. 17
13	9	0.2	.	6.8	• ok. 19 – ok. 21 ; ⌒ I ; ⋒ III
14	9	5.0	.	7.3	• ^{1} III, np ; ⌒ I
15	8	0.0	.	3.4	• ^{2} na . I $\overset{\bullet}{\triangledown}{}^{0}$ ok. 18
16	8	0.1	.	8.8	• ^{0} ok. 19 – ok. 19^{30} ; ⌒ I
17	4	4.3	.	1.9	• a z prz. • $^{0-2}$ ok. 15 – ok. 20 ; = I, II
18	7	2.0	.	4.0	• ^{0} 7^{40} – ok. 7^{50} • ^{1} – ok. 9 ; ≡ ^{0} I
19	7	0.1	.	3.9	• $^{0-1}$ ok. 14 – ok. 19^{30} • np ; = ⌒ I
20	4	2.4	.	2.1	• na • a ; = II, III
21	7	.	.	6.8	
22	7	0.0	.	2.8	$\overset{\bullet}{\triangledown}$ ok. 11^{30} , 15^{25} ; = ⌒ ^{2} I
23	6	4.0	.	1.7	• ^{1} 12^{20} – ok. 13^{30} • ^{0} ok. 13^{30} – ok. 14 $\overset{\bullet}{\triangledown}$ ok. 18 $\overset{\bullet}{\triangledown}$ ok. 20 ; ≤ $20 - 20^{30}$; = I
24	8	7.4	.	1.8	• $^{0-2}$ na • ^{1} ok. 8 – ok. 9^{30}
25	8	.	.	8.8	⌒ ^{1} I
26	7	.	.	1.0	= ⌒ ^{1} I
27	7	0.3	.	7.7	• ^{0} III $\overset{\bullet}{\triangledown}{}^{0}$ ok. 21^{50} ; = ⌣ I
28	7	4.8	.	2.8	• ^{0} na $\overset{\bullet}{\triangledown}{}^{1}$ 8^{27} • $^{1-2}$ 15^{08} – 17^{55} , 21^{10} ... np ; ≫ na, a ; ≤ np ; ⌒ 17^{45} – 58
29	7	10.1	.	0.1	• na • $^{0-1}$ 8^{40} – ok. 10 $\overset{\bullet}{\triangledown}$ ok. 14^{30} – ok. 17 • np
30	7	.	.	3.0	• na
31					
Σ	–	55.3	–	139.6	UWAGI.

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1	7	0.4	.	1.4	• ^{2} 14^{05-15} ; = I, III
2	7	.	.	4.3	⋓ III
3	7	1.0	.	7.8	≡ ^{0} na , I ≡ a – ok. 9 ; ⌣ na ; ⋓ III
4	7	0.2	.	2.0	• na • ^{1} 7^{10} – ok. 8 , 12^{18} – ok. 12^{30} $\overset{\bullet}{\triangledown}{}^{1}$ $13 - 13^{05}$ $\overset{\bullet}{\triangledown}{}^{0}$ – ok. 14^{30} ; = I
5	8	.	.	5.7	≡ ^{0} III
6	7	.	.	2.5	= ⌒ I
7	7	.	.	7.5	≡ ^{0} na , I , a – ok. 9 = III ; ⌒ ^{1} I
8	7	0.1	.	5.7	• 7^{55} – ok. 9 ; ≡ ^{0} I = ⋓ III
9	7	.	.	7.4	• na ; ≡ ^{0} na ≡ ^{2} I ≡ a – ok. 9 ; ⋓ III
10	7	.	.	9.0	= ⌣ I = ⋓ III
11	7	.	.	8.4	≡ ^{0} na , I , a – ok. 9 = III ; ⌣ I
12	7	.	.	7.0	= I , III ; ⌣ I
13	7	.	.	6.5	= I
14	7	.	.	4.6	≡ ^{0} I ≡ a – ok. 9 = III
15	6	.	.	2.6	≡ na ≡ ^{2} I , a – ok. 9
16	7	.	.	7.0	= ⌒ ^{1} I
17	7	.	.	6.9	≡ ^{0} I ⌒ ^{1} I
18	7	.	.	0.7	≡ I
19	5	.	.	6.7	= I , II , III
20	3	6.0	.	.	• $^{0-1}$ ok. 10^{30} – ok. 12 • ^{1} p , III , np ; = I , II
21	7	0.0	.	2.6	• ^{0} 7^{25} – ok. 8 ; = I
22	5	3.8	.	0.7	• na • ^{1} ok. 12^{30-50} ; = I
23	5	3.7	.	.	• ^{1} na , I , a – ok. 12 ; ≡ ^{0} I = II, III
24	7	0.0	.	1.9	≡ ^{2} na , I ≡ a – ok. 9
25	7	.	.	2.2	$\overset{\bullet}{\triangledown}{}^{0}$ na ; = I, III
26	4	.	.	6.0	≡ ^{0} na , I , a – ok. 9 = II, III
27	3	.	.	5.5	≡ na ≡ ^{2} I , a ≡ ^{0} II
28	4	.	.	.	= I, II, III
29	7	.	.	6.0	≡ ^{2} na , I ≡ a – ok. 9 ≡ ^{0} III
30	7	0.0	.	6.2	= I, III ⋓ III
31	7	0.1	.	7.2	• na ; ≡ ^{0} I = ⋓ III
Σ	–	15.3	–	140.0	UWAGI.

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°57' — Listopad – Novembre 1957

DNI	CIŚNIENIE P = +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	84.0	82.3	85.2	83.8	4.7	14.3	8.8	9.2	16.4	4.2	100	67	95	87	0.0	5.5	0.6	2.0	10 ≡	0 ⊙	0	C 0	C 0	C 0
2	86.5	86.0	87.7	86.7	5.3	14.0	9.8	9.7	14.6	4.7	100	72	95	89	0.1	4.4	0.6	1.7	10 ≡	2 ⊙	10	C 0	C 0	C 0
3	89.2	89.2	88.8	89.1	9.1	11.3	8.5	9.4	11.5	8.1	99	89	100	96	0.2	1.5	0.0	0.6	10 ≡	10	10 ≡	W 1	C 0	E 2
4	88.5	87.8	88.9	88.4	7.8	10.9	9.6	9.5	14.3	7.0	100	97	97	98	0.0	0.3	0.4	0.2	10 ≡	0 ⊙	6	C 0	C 0	C 0
5	87.3	84.6	84.7	85.5	3.0	16.0	9.7	9.6	16.9	2.6	100	73	88	87	0.0	4.9	1.4	2.1	1⊙≡	0 ⊙	1	C 0	ESE 3	C 0
6	85.0	84.6	84.1	84.6	4.3	15.6	9.7	9.8	17.1	3.3	100	67	86	84	0.0	5.9	1.7	2.5	4⊙≡	3 ⊙	9	C 0	C 0	C 0
7	82.3	82.6	83.0	82.6	6.9	15.1	10.1	10.6	16.7	6.3	97	74	86	86	0.3	4.4	1.8	2.2	4 ⊙	8	4	C 0	C 0	C 0
8	82.3	81.9	81.1	81.8	6.7	14.5	10.6	10.6	16.0	5.9	96	71	85	84	0.4	4.8	2.0	2.4	7	4	6	C 0	C 0	C 0
9	79.7	80.2	82.4	80.8	7.4	12.7	11.0	10.5	14.3	6.7	93	78	89	87	0.8	3.3	1.5	1.9	8 ⊙	5 ⊙	10	C 0	C 0	C 0
10	83.8	84.5	84.4	84.2	6.8	8.7	7.8	7.8	11.0	5.2	97	97	94	96	0.3	0.3	0.6	0.4	10	10⊙≡	7	C 0	C 0	C 0
11	84.8	85.6	87.4	85.9	8.9	9.1	6.8	7.9	9.8	6.1	93	89	99	94	0.8	1.3	0.2	0.8	7	10 ●	10 ●	ENE 5	ENE 10	NE 4
12	90.8	94.8	98.4	94.7	6.4	4.1	4.2	4.7	6.8	3.0	94	92	92	93	0.6	0.7	0.6	0.6	10 ●	10 ●	10 ●	ENE 2	E 2	ENE 2
13	100.0	101.4	102.6	101.3	2.5	1.6	0.0	1.0	4.2	−0.2	96	85	88	90	0.3	1.1	0.7	0.7	10 ●	10	10	ENE 1	ENE 1	ESE 2
14	102.9	104.0	103.9	104.3	−1.0	−1.1	−1.9	−1.5	0.0	−2.1	87	91	100	93	0.7	0.4	0.0	0.4	10	10	10 ●	E 1	NE 1	E 2
15	105.9	105.5	103.9	105.1	−2.2	−0.9	−1.4	−1.5	−0.6	−3.0	98	94	100	97	0.1	0.3	0.0	0.1	10	10	10 ≡	ESE 2	SE 1	C 0
16	104.0	104.1	104.7	104.3	−2.6	1.8	2.3	1.0	2.3	−3.2	98	96	98	97	0.1	0.3	0.1	0.2	10 ≡	10 ≡	10 ≡	C 10	WSW 1	C 0
17	104.2	104.5	105.3	104.7	2.1	2.0	1.6	1.8	2.3	1.3	98	98	96	97	0.1	0.2	0.3	0.2	10 ≡	10 ≡	10	C 0	NE 3	E 2
18	104.9	105.3	104.8	105.0	1.2	2.1	1.6	1.6	2.4	0.7	96	89	93	93	0.3	0.8	0.6	0.6	10	10	10	E 1	C 0	NE 1
19	104.5	106.2	108.6	106.4	1.4	1.2	1.3	1.3	1.6	0.7	81	85	79	82	1.3	1.1	1.4	1.3	10	10	10	NE 1	C 0	ESE 3
20	109.9	110.9	111.6	110.8	−2.1	2.6	−1.4	−0.6	3.4	−3.2	92	68	92	84	0.4	2.4	0.4	1.1	1	0 ⊙	2	ENE 2	C 0	C 0
21	111.0	109.4	106.1	108.8	−4.3	0.6	−0.5	−1.2	2.8	−4.6	96	82	90	89	0.2	1.1	0.6	0.6	2 ≡	0 ⊙	1 ≡	C 0	C 0	C 0
22	99.8	96.2	93.1	96.4	−5.9	0.2	−1.2	−2.0	2.1	−6.6	94	96	91	94	0.2	0.3	0.5	0.3	10 ≡	1 ≡	4 ≡	C 0	C 0	NW 1
23	93.5	92.8	94.4	93.6	−3.6	1.8	2.8	1.0	2.9	−3.0	97	76	79	84	0.2	1.7	1.6	1.2	10 ≡	10 ≡	10	C 0	W 1	W 3
24	97.2	97.5	96.5	97.1	2.0	4.2	4.3	3.7	4.8	1.4	82	66	66	71	1.3	2.8	2.8	2.3	8	8 ⊙	10	W 5	W 5	W 6
25	95.0	94.5	95.9	95.1	4.6	5.6	5.2	5.2	5.8	3.8	81	83	98	87	1.7	1.6	0.1	1.1	10	10	10 ●	WSW 6	W 5	W 8
26	96.6	97.6	96.4	96.9	6.0	6.6	6.4	6.4	7.2	4.6	97	94	97	96	0.3	0.5	0.3	0.4	10	9	10	W 5	W 3	W 3
27	92.8	91.6	92.6	92.3	4.5	6.2	6.6	6.0	6.6	3.7	93	82	85	87	0.5	1.7	1.4	1.2	10	10	10 ●	WSW 4	W 6	W 4
28	91.2	89.0	84.2	88.1	6.8	7.2	7.6	7.3	7.8	5.4	96	94	82	91	0.5	0.6	1.9	1.0	10 ●	9 ⊙	10 ●	W 3	W 3	W 10
29	80.3	82.9	82.4	85.2	4.9	1.8	−4.8	−0.7	7.6	−5.0	87	64	74	75	1.1	2.6	1.1	1.6	9 ●	4 ☾	10 ✳	W 4	W 10	W 10
30	99.0	99.7	99.4	99.4	−8.0	−5.0	−5.7	−6.1	−4.8	−8.4	72	54	69	65	0.9	1.9	1.2	1.3	1	8 ⊙	10 ✳	SW 3	N 4	N 6
31																								
M	93.9	93.9	94.5	94.1	2.8	6.2	4.3	4.4	7.5	1.4	94	82	89	88	0.5	2.0	0.9	1.1	8.1	6.7	8.0	1.5	2.0	2.3

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1	101.5	101.5	100.6	101.2	−7.3	−3.8	−3.7	−4.6	−3.1	−8.0	76	69	87	77	0.8	1.4	0.6	0.9	9	9	10	WNW 2	NW 4	WNW 4
2	98.9	98.3	98.2	98.5	−2.8	−1.8	−3.0	−2.6	−1.8	−4.3	93	81	81	85	0.4	1.0	0.9	0.8	10	10	9	W 2	N 1	NNE 2
3	95.5	93.6	93.7	94.3	−4.3	−2.5	−1.9	−2.6	−1.9	−5.1	89	95	94	93	0.5	0.3	0.3	0.4	10	10 ⛆	10 ⛆	N 2	C 0	C 0
4	96.0	96.4	96.0	96.1	−1.5	−0.2	0.9	0.0	0.9	−2.2	86	86	94	89	0.8	0.8	0.4	0.7	10	10 ✳	10≡✳	C 0	WSW 2	WSW 1
5	93.8	92.7	94.3	93.6	0.6	1.8	2.8	2.0	3.0	0.4	100	100	93	96	0.0	0.0	0.6	0.2	10≡✳	10	10	W 2	W 3	C 0
6	96.4	98.0	98.3	97.6	2.5	2.2	0.8	1.6	3.0	0.7	86	82	92	87	0.9	1.3	0.5	0.9	9	8 ⊙	10	C 0	C 0	C 0
7	92.4	88.7	83.6	88.2	−2.6	1.4	−1.2	−0.9	1.8	−3.3	98	74	80	84	0.1	1.8	1.1	1.0	3 ≡	3 ⊙	6	C 0	W 1	W 1
8	72.5	65.6	58.8	65.6	2.8	3.1	5.6	4.8	5.6	−2.7	67	66	81	71	2.5	3.0	1.7	2.4	10	10	8	SSW 1	NW 1	S 1
9	57.3	60.5	72.7	63.5	7.8	3.1	1.7	4.1	8.2	1.5	64	92	67	74	3.8	0.7	2.3	2.3	8	9	4	WSW 9	WNW 9	WSW 3
10	73.3	73.4	82.0	76.2	−0.8	0.2	−3.0	−1.6	1.7	−3.2	94	96	84	91	0.4	0.3	0.8	0.5	8	10 ✳	2	C 0	W 1	WNW 2
11	83.7	81.3	76.1	80.4	−9.4	−1.4	0.4	−2.5	0.4	−9.7	95	74	92	87	0.2	1.4	0.5	0.7	2 ≡	7 ⊙	9	C 0	ESE 1	ENE 1
12	72.4	71.9	72.0	72.1	2.7	6.5	4.3	4.4	9.5	0.2	88	84	90	87	0.9	1.6	0.8	1.1	8	3 ⊙	6	C 0	C 0	C 0
13	69.8	67.6	59.5	65.6	3.6	8.7	7.5	6.8	8.9	2.4	93	80	84	86	0.5	2.2	1.7	1.5	7	10	10	C 0	C 0	C 0
14	56.2	63.7	73.0	64.3	5.8	5.6	3.6	4.6	7.5	3.2	100	94	86	93	0.0	0.6	1.1	0.6	10●≡	10 ●	10	C 0	W 1	C 0
15	82.4	89.3	96.4	89.4	0.3	−2.3	−4.9	−3.0	3.6	−5.2	94	91	81	89	0.3	0.5	0.8	0.5	10 ●	10 ⛆	10	C 0	NE 1	E 3
16	99.2	99.2	99.5	99.3	−6.4	−6.2	−5.5	−5.9	−4.9	−8.1	81	78	80	80	0.7	0.8	0.8	0.8	10 ✳	4 ⊙	10	ENE 5	E 5	E 5
17	96.2	95.0	94.4	95.2	−5.2	−2.6	−2.6	−3.2	−1.6	−8.1	90	85	93	89	0.4	0.8	0.3	0.5	9	10	10	E 2	C 0	C 0
18	95.1	95.7	97.3	96.0	−3.0	−2.9	−3.7	−3.3	−1.8	−4.0	95	84	85	88	0.3	0.8	0.7	0.6	10	10	10	C 0	C 0	C 0
19	98.9	101.0	104.7	101.5	−3.6	−2.4	−1.8	−2.4	−1.8	−4.6	92	93	96	94	0.4	0.3	0.2	0.3	10	10 ✳	10	C 0	C 0	C 0
20	107.3	108.5	108.2	108.0	0.2	2.0	1.4	1.2	2.4	−2.0	84	96	98	93	1.0	0.3	0.2	0.5	10	10	7 ≡	C 0	C 0	C 0
21	105.8	104.6	104.5	105.0	−2.0	2.7	−0.9	−0.3	2.9	−4.1	96	70	83	83	0.3	2.2	0.9	1.1	2 ≡	1 ⊙	8 ≡	C 0	C 0	C 0
22	103.1	102.4	101.1	102.2	−2.4	1.0	−1.4	−1.0	1.3	−2.7	95	77	100	91	0.2	1.5	0.0	0.6	8	8 ⊙	8 ≡	C 0	C 0	C 0
23	97.6	95.5	94.1	95.7	−6.2	−3.2	−4.9	−4.8	−1.4	−6.6	100	97	88	95	0.0	0.1	0.5	0.2	10 ≡	5⊙≡	6 ≡	C 0	C 0	C 0
24	93.1	92.7	93.9	93.2	−8.3	−3.6	−4.6	−5.3	−3.4	−9.0	89	83	93	88	0.3	0.8	0.3	0.5	7 ≡	8⊙≡	9 ≡	C 0	C 0	C 0
25	94.8	93.4	94.9	94.4	−7.5	−2.7	−2.3	−3.7	−0.4	−8.2	90	89	93	91	0.3	0.6	0.4	0.4	2 ≡	7⊙≡	8 ≡	C 0	C 0	C 0
26	97.9	98.4	101.0	99.1	−1.6	2.6	1.7	1.1	2.9	−2.7	96	84	83	88	0.2	1.2	1.1	0.8	9	8 ⊙	10	C 0	C 0	C 0
27	101.6	100.5	99.5	100.5	−0.8	2.4	0.7	0.8	3.3	−1.2	92	80	92	88	0.5	1.5	0.5	0.8	9 ≡	0 ⊙	10 ≡	C 0	C 0	W 1
28	93.0	91.9	89.1	92.0	−3.4	−0.8	−1.7	−1.9	1.0	−4.0	97	91	92	93	0.2	0.5	0.4	0.4	10 ≡	8	10	C 0	C 0	W 3
29	85.8	85.9	85.5	85.1	−0.6	1.7	0.4	0.5	2.1	−3.5	97	80	80	86	0.2	1.4	1.5	1.0	10 ✳	10 ≡	7	C 0	C 0	C 0
30	79.8	77.8	76.0	77.9	3.0	4.5	3.4	3.6	4.6	−0.4	71	66	70	69	2.2	2.8	2.4	2.5	9	7 ⊙	8	WSW 3	C 0	WNW 9
31	77.3	78.6	78.7	78.2	1.6	1.6	1.7	1.6	3.9	0.7	91	89	80	87	0.7	0.8	1.4	1.0	10 ●	8	10	C 0	C 0	C 0
M	89.4	89.1	89.3	89.3	−1.6	0.6	−0.3	−0.4	1.8	−3.3	90	84	87	87	0.6	1.1	0.8	0.8	8.4	7.8	8.3	0.9	1.0	1.2

Kraków, Obserw. Astr. UJ $H_s = 221$ m $H_b = 219{,}8$ m $h_w = 21$ m **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	6	0.1	.	5.3	• na ; ≡² na , / ≡ a – ok. 10 = II, III
2	7	0.0	.	5.0	• na ; ≡² na ≡⁰ /, a – ok. 9
3	4	3.9	.	.	• na • np • np ; ≡ na ≡⁰/ ≡ a – ok. 10 = II ≡² III, np
4	4	0.1	.	2.9	• na ; ≡ na , a – ok. 10 = II, III , ≡ np ; ∪ III
5	8	0.0	.	7.8	• na ; ≡ na ≡ /, a – ok. 9
6	8	.	.	6.3	• na ; ≡ na ≡ /, a – ok. 8 ; ∪ III
7	8	0.7	.	1.0	•⁰⁻¹ 10²⁵ – ok. 12³⁰ ; ⌒¹ /, ∪ III
8	6	0.0	.	1.8	• na ▽ ok. 16³⁰ ; ⊃ III
9	7	0.0	.	3.5	▽⁰ ok. 18³⁰
10	1	.	.	0.8	= / ≡ ok. 8 – a ≡² II ≡ p – ok. 14 = ∪ III
11	7	5.6	.	.	• ok. 12³⁰ – a , II •⁰• p z prz. •⁰ III ; = /
12	7	1.0	.	.	•¹ na , / , a – ok. 8 • ok. 12³⁰ – a , II , p , III , np
13	7	0.1	.	.	•⁰ ok. 6 – ok. 9
14	4	0.0	.	.	• ok. 17⁴⁰ – p , III , np ; = /, II
15	4	.	.	.	= /, II ≡ ok. 16 – p ≡² III ≡ np
16	3	0.1	.	.	≡ na ≡² / ≡ a, II, p, III, np ; V na , a – ok. 10
17	2	0.0	.	.	• 7 – a , p z prz , np ; ≡ na ≡⁰ / ≡ a ≡¹ II ≡ p – ok. 14 = III
18	4	.	.	.	• na – ok. 6³⁰ ; = /, II
19	7	0.0	.	.	✳⁰ ok. 13¹⁵
20	7	.	.	7.3	
21	4	.	.	3.3	≡ ok. 6³⁰ – ok. 12 = II ≡ ok. 15⁴⁰ – p, III, np ; ⌴ na , /, a , II
22	3	.	.	3.9	≡ ok. 6 – ok. 10 ≡ – a , II , p , III , np ; ⌴ na , a , p , np ; V ok. 7 – a
23	3	0.0	.	.	•⁰ 20⁵⁰ – np ; = ok. 6³⁰ – a , II , p ; ⌴ na , a , p
24	6	.	.	0.3	
25	5	0.2	.	.	•⁰⁻¹ p z prz. •⁰ III •⁰⁻¹ np ; = /, II
26	4	0.1	.	.	• na •⁰⁻¹ ok. 8 – ok. 9³⁰ p ; = /, II
27	6	0.7	.	.	•⁰ na , a , p z prz. , III ; = /
28	6	7.5	.	.	• na •¹/ a ... ok. 11 •⁰ p , np , III
29	8	5.4	.	1.4	• na •⁰ / •¹ a – 8³⁰ ✳½ – 8⁴⁰ •¹ – 9⁰⁵ ⛉ ok. 10³⁰ ✳ 10⁴⁵ – ok. 11 ✳⁰ p z prz , III , np
30	8	0.0	0	2.5	✳ na ✳⁰ ok. 9 , ok. 19 – 21³⁰
31					
Σ	–	25.5	–	33.1	UWAGI:

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1	6	.	pł.	0.4	
2	7	0.0	pł.	.	△⁰ ok. 7³⁰ – ok. 11 ; = / ; ∪ III
3	4	0.8	pł.	.	✳✳ ok. 8 – a △ p , np ; = /, II
4	4	3.8	0	.	✳⁰ ok. 12³⁰ – a , II , p , III , np ; = / ≡⁰ III ≡ np
5	4	2.0	2	.	✳ na ✳¹ a – ok. 9 ✳ ok. 9 – 10 •¹ ok. 10 – 12 ; ≡ na – a = II, III
6	7	.	pł.	0.3	
7	7	0.0	.	3.7	≡ na ≡ / ≡ a – ok. 10 = III ; ⌴ na , ok. 11 – a , II, III
8	8	4.6	.	.	✳ na 7²⁶ – ok. 7³⁰ ✳ – ok. 8 •⁰⁻¹ p ; ∪ III
9	7	1.7	.	0.6	•⁰⁻¹ 9³⁰ – a
10	4	2.0	.	.	✳¹ 10³⁵ – a , II , p z prz. ; = /
11	7	.	2	1.5	≡ na ≡⁰ / ≡ a ; ∪ /
12	5	.	1	2.7	≡⁰ ok. 9 – 12 = II ≡⁰ ok. 16 – 20
13	8	2.3	pł.	.	= ∪ /
14	4	6.5	.	.	•¹ na , /, a , II •¹⁻² p – ok. 17 ≡ na ≡⁰ / ≡ a = III
15	5	0.0	.	.	• na , / , •⁰ a – ok. 12¹⁵ ✳⁰ – ok. 13
16	7	0.0	.	2.0	✳⁰ na , / , a – ok. 9
17	4	.	.	.	≡ II
18	7	.	.	.	= /, III
19	4	0.0	.	.	✳⁰ ok. 10 – a , p ; = /, III
20	4	.	0	.	= /, II ≡⁰ p, III
21	4	.	.	5.5	≡ na ≡⁰ /, III , np ; ⌴ na , a , p , np
22	4	.	.	0.9	= /, II ≡ p ≡⁰ III , np
23	3	.	.	1.2	≡ na , a , p , np ; V na , a , p , np
24	3	.	.	2.3	≡ na , a , p , np ; V na , a , p , np
25	2	.	.	2.8	≡ na , a , p , np ; V na , a , p , np
26	4	0.0	.	2.3	V na , a – ok. 10 ; = /, II, III
27	4	0.0	.	3.7	•⁰ np ; ≡ na ≡⁰ / ≡ a – ok. 9 = II ≡¹ III
28	4	0.0	.	0.6	≡ na ≡² / ≡ a – ok. 11 = II, III ⌴ na , a
29	3	0.0	.	.	✳⁰ na , / , a ; = / ≡ a ≡⁰ II ≡ p
30	7	0.0	pł.	0.3	▽⁰ ok. 16
31	3	1.4	.	.	△ na •⁰ na , / a – 7³⁵ ✳¹ – 8¹⁰ ✳ – ok. 8³⁰ •⁰ – ok. 9³⁰ ✳¹ ok. 11 – 11³⁰ ✳ p ; = II
Σ	–	23.1	–	31.0	UWAGI:

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ Styczeń – Janvier 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	92.9	91.5	90.6	91.7	-10.2	-5.9	-7.0	-7.5	-4.4	-13.0	68	59	72	66	0.9	1.6	1.0	1.2	10	4	0	SE 5	SE 6	SE 1
2	89.0	88.8	90.1	89.3	-4.6	0.5	-1.1	-1.6	1.1	-8.7	76	73	77	75	1.0	1.7	1.3	1.3	8	9	0	SE 1	SSE 1	SSE 1
3	93.3	94.2	95.0	94.2	-1.9	1.1	-0.3	-0.4	1.5	-3.4	77	70	80	76	1.2	2.0	1.2	1.5	7	10	10	C 0	SE 1	C 0
4	95.7	97.●	99.0	97.3	-3.1	0.2	-0.4	-0.9	0.8	-4.0	81	74	80	78	0.9	1.6	1.2	1.2	9	8	10	C 0	ESE 2	C 0
5	99.4	97.3	93.6	96.8	-5.5	4.3	1.7	0.6	4.7	-6.0	80	49	64	64	0.8	4.2	2.5	2.5	0	1 ⊙	10 △	C 0	WSW 4	SW 7
6	89.6	86.3	84.3	86.7	1.7	2.6	1.7	.9	2.7	0.8	80	65	72	72	1.4	2.6	1.9	2.0	10 △	10	10 ●	SW 7	W 7	W 7
7	86.6	89.0	94.1	89.9	2.2	3.4	3.6	3.2	3.8	0.0	77	70	65	71	1.7	2.4	2.8	2.3	10	9	9	W 5	NW 10	W 8
8	98.2	98.3	97.0	97.8	2.9	2.7	3.0	2.9	3.8	1.7	76	81	84	80	1.8	1.4	1.2	1.5	8 ●	10	10	W 7	W 4	W 1
9	95.5	94.7	92.8	94.3	4.4	3.9	2.7	3.4	4.8	2.4	84	77	75	79	1.4	1.9	1.8	1.7	10	10	9	W 5	W 4	C 0
10	88.6	85.8	84.9	86.4	2.8	4.7	0.8	2.3	5.7	0.0	72	65	85	74	2.1	2.9	1.0	2.0	10	9	10 ✳	W 6	W 4	W 3
11	84.9	86.3	88.3	86.5	1.4	1.7	0.4	1.0	1.7	-0.3	72	87	75	78	1.9	0.9	1.6	1.5	10	7	9 ✳	W 7	NW 6	NW 6
12	87.6	84.9	80.6	84.4	0.2	0.5	-0.4	0.0	1.1	-1.4	66	56	64	62	2.1	2.8	2.1	2.3	10 ✳	6 ⊙	9	WNW 5	W 5	W 3
13	78.6	78.5	81.3	79.5	-0.9	1.4	-0.9	-0.3	1.5	-2.1	67	63	79	70	1.9	2.5	1.2	1.9	10	10	10 ✳	WSW 3	SW 3	W 2
14	85.0	89.0	92.2	88.7	-2.5	-2.7	-3.4	-3.0	-0.9	-5.1	91	75	81	82	0.5	1.2	0.9	0.9	10 ✳	10	10	NE 1	NE 2	NE 7
15	91.5	90.6	91.1	91.1	-2.1	-4.2	-5.9	-4.5	-2.1	-6.3	75	65	79	73	1.3	1.5	0.8	1.2	10	10	10 ✳	ENE 9	ENE 12	ENE 8
16	94.1	96.7	100.1	97.0	-7.2	-7.2	-7.7	-7.4	-5.4	-8.5	77	71	73	74	0.8	1.0	0.9	0.9	10 ✳	9 ✳	10 ✳	NE 5	NNE 5	NNE 3
17	101.2	101.7	100.7	101.2	-12.2	-8.9	-8.5	-9.5	-7.7	-13.2	70	58	74	67	0.7	1.3	0.8	0.9	9	3	10	N 1	NW 1	W 3
18	99.6	97.9	97.1	98.2	-5.3	-3.7	-5.2	-4.8	-3.7	-8.9	77	73	73	74	0.9	1.2	1.1	1.1	10	10	0	WNW 5	W 6	W 5
19	98.4	99.0	101.0	99.5	-6.3	-4.4	-3.6	-4.5	-3.4	-7.0	81	79	80	80	0.7	0.9	0.9	0.8	10	10 △	10	NW 4	W 4	NW 2
20	102.3	101.7	98.8	100.9	-4.3	-3.7	-8.6	-6.3	-3.0	-9.1	79	69	74	74	0.9	1.4	0.8	1.0	10	10	0	WNW 2	WNW 4	C 0
21	96.2	96.0	97.0	96.4	-4.5	0.2	-2.9	-2.5	0.2	-10.1	69	38	62	56	1.3	3.8	1.8	2.3	3	1	0	W 7	W 7	W 5
22	98.2	97.7	94.2	96.7	-5.3	2.3	0.9	-0.3	2.7	-6.6	46	38	38	41	2.2	4.5	4.1	3.6	8	4	9	W 5	C 0	W 1
23	93.3	93.2	91.8	92.8	-3.8	-2.0	-5.2	-4.0	4.2	-7.6	37	50	65	51	2.9	2.7	1.4	2.3	2	6 ⊙	0	C 0	SE 1	NW 1
24	86.3	84.7	82.8	84.6	-5.4	-1.3	-3.1	-3.2	-0.5	-8.5	65	58	81	68	1.4	2.3	0.9	1.5	9	10	0	C 0	NE 1	NE 1
25	81.3	82.7	85.5	83.2	-4.1	0.1	0.0	-1.0	0.6	-6.1	84	79	84	82	0.7	1.4	0.9	1.0	9	10 ✳	10	NE 1	C 0	C 0
26	89.7	92.2	93.8	91.9	0.6	2.8	-0.7	0.5	3.9	-1.3	81	67	77	75	1.3	2.5	1.3	1.7	10	10	0	W 3	W 3	W 1
27	91.3	90.4	92.4	91.4	-0.7	0.8	0.6	0.3	2.6	-5.2	62	77	76	72	2.2	1.5	1.6	1.8	4	10 ✳	8	W 2	WSW 5	W 5
28	93.0	92.7	98.1	94.6	-0.6	3.0	-0.1	0.6	3.2	-1.2	75	58	86	73	1.4	3.2	0.9	1.8	5	9	10 ✳	W 1	W 3	W 2
29	102.5	103.5	102.2	102.7	0.5	1.0	-1.7	-0.5	1.5	-2.4	84	70	71	75	1.0	2.0	1.6	1.5	10	10	10	NW 2	NW 3	W 1
30	98.4	96.5	94.7	96.5	-3.3	3.6	0.1	0.1	4.0	-4.0●	79	47	70	65	1.0	4.2	1.9	2.4	9	3 ⊙	10	WNW 1	WNW 2	NW 1
31	95.8	96.8	98.2	96.9	-1.5	1.1	-0.1	-0.2	1.5	-2.0●	82	70	86	79	1.0	2.0	0.9	1.3	10 ✳	10	8	NW 2	NW 1	C 0
M	92.8	92.8	93.0	92.9	-2.5	-0.1	-1.6	-1.4	0.8	-4.8●	74	66	74	71	1.3	2.2	1.4	1.6	8.4	8.0	7.1	3.3	3.8	2.7

Luty – Février

1	96.6	96.6	96.3	96.5	-3.4	2.2	1.4	0.4	2.9	-4.0	83	61	67	70	0.8	2.8	2.3	2.0	5	9	9	C 0	E 5	S 1
2	96.2	98.0	99.2	97.8	2.2	2.7	3.4	2.9	3.6	0.0	73	82	70	75	2.0	1.3	2.4	1.9	10	10	10	WSW 2	W 5	W 7
3	97.6	95.6	97.9	97.0	3.8	6.5	2.8	4.0	7.0	2.0	73	64	77	71	2.1	3.6	1.7	2.5	10	9	10 ●	W 3	WSW 4	NW 1
4	100.2	97.9	95.2	97.8	0.0	3.7	1.2	1.5	4.4	-0.8	88	78	87	84	0.7	1.8	0.9	1.1	10 ≡	10	9	NE 1	E 3	C 0
5	95.6	95.7	95.0	95.4	2.8	9.2	3.9	5.0	10.3	0.5	79	60	75	71	1.6	4.6	2.0	2.7	2	4 ⊙	0	W 4	W 2	W 2
6	92.5	91.1	88.9	90.8	6.5	11.3	7.1	8.0	11.7	2.8	62	50	64	59	3.7	6.7	3.6	4.7	0	1 ⊙	0	C 0	SW 7	SW 7
7	88.6	88.7	91.0	89.4	6.4	6.4	2.9	4.6	7.5	2.5	62	65	79	69	3.6	3.4	1.6	2.9	8	10	0	W 4	W 5	W 2
8	90.4	85.7	82.2	86.1	1.7	7.7	7.0	5.8	8.3	0.9	76	57	63	65	1.6	4.5	3.7	3.3	2	8 ⊙	10	W 5	SW 7	SW 8
9	76.8	76.4	76.9	76.7	6.3	6.1	5.8	6.0	8.2	5.0	75	77	71	74	2.4	2.1	2.6	2.4	10 ●	10 ●	10	SW 5	W 7	W 6
10	79.8	80.0	80.8	80.2	3 7	8.3	4.0	5.0	8.8	2.4	80	51	72	68	1.6	5.5	2.2	3.1	8	4 ⊙	9	W 2	W 6	C 0
11	81.0	82.7	84.9	82.9	3.9	5.2	4.3	4.4	7.4	3.2	75	81	76	77	2.0	1.6	2.0	1.9	8	10 ●	10	W 3	W 3	W 6
12	86.8	86.1	83.6	85.5	1.5	6.3	1.3	2.6	9.4	0.0	76	55	72	68	1.6	4.3	1.9	2.6	7	6	3	NW 2	SW 3	SW 1
13	80.3	77.4	72.4	76.7	5.2	8.6	4.1	5.5	10.3	0.7	54	41	66	54	4.0	6.6	2.8	4.5	10	9	2	SSW 2	S 7	S 3
14	67.3	65.6	64.8	65.9	5.2	8.9	5.1	6.1	9.3	3.4	73	53	75	67	2.3	5.4	2.2	3.3	10 ●	9	10	S 6	SSW 7	S 4
15	67.3	66.8	63.3	65.8	4.4	10.5	7.0	7.2	10.9	3.0	71	39	74	61	2.5	7.8	2.6	4.3	7	3 ⊙	9 ●	W 4	SSW 7	S 4
16	65.7	70.9	74.3	70.3	6.6	8.1	4.0	5.7	8.9	3.5	68	53	69	63	3.1	5.1	2.5	3.6	5	10 ●	4	SW 4	WSW 6	C 0
17	77.6	80.6	82.3	80.2	3.7	7.9	4.3	5.0	8.9	2.0	70	50	66	62	2.4	5.3	2.8	3.5	10	3 ⊙	0	W 3	W 3	SW 4
18	83.2	84.2	74.5	79.6	3.4	9.5	6.3	6.4	10.4	2.1	76	53	66	65	1.9	5.6	3.2	3.6	7	9	7	NW 2	S 5	SE 2
19	68.5	76.0	84.6	76.4	8.6	4.3	1.6	4.0	14.4	1.2	63	68	71	67	4.2	2.7	2.1	3.0	8	10	0	SW 12	W 9	W 3
20	88.8	88.8	87.1	88.2	-0.8	7.6	3.3	3.4	8.9	-2.4	73	35	55	54	1.6	6.7	3.5	3.9	0	2 ⊙	0 ●	C 0	SW 7	SSW 4
21	83.3	82.4	82.4	82.7	5.7	8.7	5.4	6.3	9.4	1.3	46	46	71	54	5.0	6.0	2.7	4.6	10	9	8	S 1	SSW 5	S 1
22	83.5	83.7	84.2	83.8	1.1	1.3	-0.5	0.4	5.5	-1.0	83	83	82	83	1.1	1.1	1.1	1.1	10 ✳	10 ✳	10 ✳	W 5	NW 6	NW 6
23	86.0	86.7	85.9	86.2	-1.9	2.4	-2.0	-0.9	3.3	-2.7	85	56	81	74	0.8	3.2	1.0	1.7	9	7 ⊙	0	W 3	W 3	C 0
24	82.5	78.9	74.4	78.6	-1.2●	1.2	0.4	0.2	1.9	-4.9	64	61	83	69	2.0	2.6	1.1	1.9	7	10 ✳	10 ✳	C 0	SSE 7	SE 3
25	75.8	77.9	77.7	77.1	0.0	1.8	0.1	0.5	2.1	-1.0	90	78	86	83	0.6	1.8	0.9	1.1	10 ✳	9	10	SE 1	WSW 3	C 0
26	76.7	82.1	87.7	82.2	0.2	0.8	0.1	0.3	1.0	-0.9	88	85	85	86	0.7	1.0	1.0	0.9	10 ≡	10 ✳	10 ✳	NNE 7	NW 7	NW 5
27	91.8	93.9	96.2	94.0	-1.8	-2.2	-3.8	-2.9	0.1	-4.4	75	76	80	77	1.3	1.2	0.9	1.1	10	10	10	NW 4	NW 4	NW 3
28	97.6	99.1	99.5	98.7	-5.7	-5.4	-4.3	-4.9	-3.5	-6.3	77	77	75	76	0.9	0.9	1.1	1.0	10	10	10	NW 4	NW 6	NW 2
29																								
30																								
31																								
M	84.2	84.5	84.4	84.4	2.4	5.3	2.7	3.3	6.8	0.3	74	62	74	70	2.1	3.8	2.1	2.7	7.6	7.9	6.4	3.2	5.3	3.0

Przemyśl $H_s = 238$ m $H_b = 238{,}9$ m $h_w = 20$ m **Styczeń – Janvier 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.1	20	-	$*^{o}10^{15-55}$ · = $0^{00}-3^{30}$ $7^{45}-24$
2	6	.	19	-	= $0^{00}-24$
3	6	.	14	-	= $0^{00}-24$
4	6	0.0	12	-	$*^{o}10^{45}-11^{10}$ · = $0^{00}-24$
5	8	2.3	11	-	△ $20^{20}-22^{40}$ $\bullet^{o}-24$ · = $0^{00}-10^{55}$ · ⌴ na
6	8	2.7	6	-	$\bullet^{o}0^{00-40}$ $\triangle^{o}3^{15}-4^{25}$ $5^{40}-6^{35}$ $\bullet^{o}8^{15-34}$, 15^{16} $16^{10}-22^{30}$ $*^{o}-23^{40}$
7	8	0.0	4	-	$\bullet^{o}5^{35}-6^{10}$, $9^{10}-10^{20}$, $10^{45}-11^{15}$
8	6	2.0	pł.	-	$\bullet^{o}6^{30-34}$ $\bullet^{2}9^{45}-10^{30}$ $\bullet^{o}15^{45}-16^{20}$ $\bullet^{o}18^{30}-20^{20}$ · = $10^{30}-17^{40}$
9	6	.	pł.	-	$\bullet^{o}0^{10}-10^{5}$ $\bullet^{1}-3^{20}$ $\bullet^{o}-4^{40}$ · = $4^{40}-6^{15}$, $7^{40}-17^{16}$
10	6	2.0	.	-	$*^{o}19^{15}-23^{15}$ · = $11^{50}-14^{40}$
11	7	0.0	1	-	$*^{o}5^{40}-6^{00}$ $*-6^{10}$ $7^{21}-10^{15}$, $17^{07}-18^{20}$, $20^{10}-21^{20}$
12	7	0.0	1	-	$\bigtriangledown^{*}0^{40}-7^{15}$, $5^{20}-8^{18}$
13	7	1.5	1	-	$*^{o}20^{16}-24$
14	6	0.0	2	-	$*^{o}0^{00}-6^{29}$, $12^{50}-16^{15}$ · = 7^{25-55} = -8^{45} = -19^{10}
15	7	1.0	2	-	$*^{o}17^{30}-24$ · = $6^{15}-7^{30}$
16	5	0.5	6	-	$*^{o}0^{00}-15^{40}$, $19^{25}-24$ · = $15^{40}-24$
17	7	0.0	8	-	$*^{o}0^{00}-5^{10}$, $6^{50}-10^{30}$ ↔ -12^{15} $*^{o}16^{45}-17^{30}$, $21^{30}-22^{05}$ · = $0^{00}-5^{15}$, $6^{40}-12^{20}$, $22^{05}-24$
18	6	.	8	-	= $0^{00}-24$
19	5	0.0	7	-	$\triangle^{o}10^{45}-11^{20}$, $12^{20}-15^{15}$, = $0^{00}-7^{50}$ = $^{o}-10^{25}$ = -24
20	6	.	6	-	= $0^{00}-6^{16}$, $7^{25}-24$
21	7	.	5	-	= 0^{00-30} · ⌓ 23^{20-55} NW-N-E
22	5	.	4	-	∞ $^{2}12^{20}-24$, ⌔ $^{o}3^{40}-6^{12}$
23	6	.	3	-	∞ $4^{45}-9^{40}$ = -24
24	6	0.0	3	-	$\triangle^{o}14^{50}-15^{20}$, $16^{45}-17^{30}$ · = $0^{00}-24$
25	3	0.1	3	-	$*^{o}9^{50}$ 16^{20} · = $0^{00}-12^{40}$ = $^{o}-16^{50}$ = -24
26	6	.	3	-	$*^{o}5^{50}-6^{04}$ · = $0^{00}-24$
27	5	2.3	pł.	-	$\bigtriangledown^{*}10^{52}-12^{06}$ $*^{o}-13^{25}$ $16^{50}-18^{44}$ · = $0^{00}-6^{20}$
28	6	0.0	4	-	$\bullet^{o}16^{55}-17^{30}$ $*^{o}-22^{15}$ · = $6^{10}-24$
29	7	.	3	-	$\bullet$ $5^{40}-6^{20}$ · = $0^{00}-9^{50}$
30	7	0.2	2	-	= $6^{04}-7^{30}$, $14^{40}-24$
31	6	.	3	-	$*^{o}4^{50}-6^{40}$ · = $0^{00}-24$
Σ	–	14.7	–	-	UWAGI.

Luty – Février

1	6	0.6	3	-	$*^{o}11^{30}-12^{10}$ · = $0^{00}-20^{15}$
2	8	1.4	pł.	-	$\bullet^{o}5^{20}-6^{15}$, $6^{50}-9^{46}$, $11^{34}-12^{16}$, $14^{00}-15^{32}$, $18^{40}-19^{20}$
3	7	0.3	pł.	-	$\bullet^{o}20^{26}$ 21^{40} · = $9^{40}-11^{20}$, $22^{10}-24$
4	7	.	.	-	= $0^{00}-3^{45}$ = $^{o}-4^{40}$ = -6^{08}, = $^{1}-7^{32}$ = -10^{50}, $14^{30}-24$
5	6	.	.	-	= $0^{00}-1^{40}$ = $6^{20}-13^{15}$, $15^{42}-16^{50}$ · ⌴ n – a
6	8	.	.	-	⌴ ^{o} n – a
7	8	0.0	.	-	$\bullet^{o}15^{05}-17^{35}$
8	7	0.7	.	-	= $7^{15}-10^{10}$ · ⌴ n – a · ⊕ $^{o}7^{35}-11^{03}$
9	7	2.5	.	-	$\bullet^{o}2^{40}-13^{10}$, $20^{50}-24$
10	7	.	.	-	$\bullet^{o}0^{00-06}$ · = $6^{05}-9^{45}$
11	7	1.8	.	-	$\bullet^{o}10^{28...42}$ $\bigtriangledown^{\bullet o}11^{35}-12^{50}$ · = $7^{40}-11^{10}$
12	7	.	.	-	= $6^{20}-8^{30}$ · ⌔ $^{o}20^{25-48}$
13	8	0.0	.	-	= $7^{40}-9^{35}$
14	8	2.2	.	-	$\bullet^{o}6^{10}-8^{40}$ $\bigtriangledown^{\bullet}15^{50}-16^{46}$ · ≫ $3^{15}-4^{40}$
15	8	1.0	.	-	$\bullet^{o}18^{15}-20^{46}$, $22^{15}-23^{20}$, $23^{25}-24$
16	7	0.3	.	-	$\bullet^{o}0^{00}-10^{5}$, $12^{27}-13^{15}$
17	7	0.0	.	-	$\bigtriangledown^{\bullet}22^{35}-23^{12}$ · = $8^{40}-12^{40}$
18	8	.	.	-	
19	8	0.6	.	-	$\bigtriangledown^{\bullet}9^{28}-10^{10}$ · ≫ $12^{0}-8^{40}$ (por. do 20 m/sek)
20	8	.	.	-	= $5^{25}-10^{36}$ · ⌴ n – a
21	7	0.2	.	-	= $23^{10}-24$
22	6	2.5	.	-	$*^{o}6^{04}-21^{45}$ · = $0^{00}-5^{15}$
23	7	0.1	2	-	$\bigtriangledown^{*}16^{07-19}$ $16^{35}-17^{08}$ · = $8^{40}-10^{55}$ $17^{30}-24$
24	5	0.8	1	-	$*^{o}12^{05}-15^{15}$ $19^{36}-24$ · = $0^{00}-5^{15}$, $7^{40}-8^{35}$
25	6	2.7	1	-	$*^{o}0^{00-30}$ $6^{05}-11^{35}$ · = $5^{10}-24$
26	6	1.7	4	-	$*^{o}2^{30}-15^{32}$, $16^{08}-17^{34}$, $18^{10}-24$ · = $0^{00}-6^{10}$ = $^{o}-12^{25}$
27	7	.	6	-	$*^{o}0^{00}-6^{15}$ · = $23^{15}-24$
28	7	0.1	6	-	$*^{o}8^{20}-11^{40}$ · = $0^{00}-6^{15}$
29					
30					
31					
Σ	–	19.5	–	-	UWAGI.

Przemyśl — φ = 49°48' — λ = 22°46' — Marzec – Mars 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	100.7	100.6	100.7	100.7	-7.3	-3.6	-3.5	-4.5	-3.2	-7.8	79	71	67	72	0.7	1.4	1.5	1.2	0 ⊙	10	10 *	NW 5	NNW 8	NW 3
2	99.0	97.4	95.7	97.4	-4.8	-3.1	-4.7	-4.3	-2.8	-5.5	74	66	83	74	1.1	1.7	0.7	1.2	9 *	10	10 *	NNW 4	NW 9	N 2
3	93.6	92.9	92.2	92.9	-8.9	-7.6	-11.1	-9.7	-4.4	-11.5	70	67	72	70	0.9	1.1	0.7	0.9	10 *	2	9 *	N 7	NNE 2	C 0
4	90.4	88.4	85.0	87.9	-14.5	-4.7	-7.9	-8.8	-3.9	-15.1	61	59	67	62	0.8	1.7	1.1	1.2	4	0 ⊙	0	W 2	S 2	C 0
5	82.3	84.8	86.0	84.4	0.0	0.5	-2.1	-0.9	1.0	-8.5	69	57	72	66	1.9	2.7	1.4	2.0	10	9	0	W 7	W 4	W 3
6	86.0	85.5	84.1	85.2	-5.7	2.6	-1.4	-1.5	4.0	-7.0	72	43	60	58	1.1	4.2	2.2	2.5	4	3 ⊙	0	W 2	NW 3	W 1
7	83.3	84.7	86.6	84.9	-5.9	-0.2	-2.2	-2.6	0.1	-6.7	74	72	64	70	1.0	1.7	1.9	1.5	4	10	10	W 2	NNE 3	NE 5
8	87.6	89.0	91.4	89.3	-3.0	-0.9	-2.9	-2.4	-0.1	-4.3	75	50	68	64	1.2	2.9	1.5	1.9	9	9	9	ENE 5	E 5	NE 5
9	94.6	95.5	97.8	96.0	-6.4	0.2	-1.7	-2.4	1.4	-7.6	70	62	65	66	1.1	2.4	1.9	1.8	0	3 ⊙	0	W 1	NE 4	N 2
10	101.3	103.3	103.7	102.8	-5.5	1.1	-1.7	-2.0	2.1	-6.2	77	66	67	70	0.9	2.2	1.8	1.6	0	4 ⊙	0	N 1	NE 3	C 0
11	104.3	104.2	102.8	103.8	-6.3	3.2	0.3	-0.6	5.1	-7.1	81	50	55	62	0.7	3.9	2.8	2.5	8	0 ⊙	1	W 1	NE 2	W 2
12	99.8	96.2	91.6	95.9	-3.9	9.8	4.3	3.6	11.7	-5.3	73	22	41	45	1.2	9.4	4.9	5.2	4 ⊙	3 ⊙	10	W 2	WNW 3	WNW 2
13	88.7	89.5	89.3	89.2	3.9	10.1	7.2	7.1	10.3	2.2	47	38	51	45	4.3	7.7	5.0	5.7	9	9	1	W 4	WNW 7	WNW 3
14	86.7	83.9	82.3	84.3	6.0	15.3	10.1	10.4	16.2	3.5	58	27	61	49	3.9	12.8	4.8	7.2	8	1 ⊙	10 ●	W 4	W 6	W 2
15	82.1	82.9	78.3	81.1	7.8	8.4	8.9	8.5	10.3	6.8	56	57	51	55	4.7	4.7	5.6	5.0	10	10	9	W 6	W 7	WSW 6
16	72.7	75.0	83.0	76.9	5.1	2.6	-3.1	0.4	9.7	-3.7	80	74	70	75	1.8	2.0	1.4	1.7	10 ●	10	10	NW 6	W 7	W 12
17	87.6	87.2	81.7	85.6	-4.6	-0.7	0.7	-1.0	1.1	-6.4	55	48	69	57	1.9	3.0	2.0	2.3	9 *	9	10	NW 1	W 1	S 1
18	72.2	70.7	72.7	71.9	6.3	10.7	6.7	7.6	12.8	0.1	76	64	79	73	2.2	4.6	2.0	2.9	10	9	9	W 4	WSW 7	W 6
19	78.8	81.6	81.6	80.7	5.9	7.8	6.6	6.7	9.1	5.0	63	67	78	69	3.5	3.5	2.1	3.0	5	9	10 ●	WNW 7	W 7	W 7
20	82.8	84.4	81.9	83.0	5.3	8.2	9.6	8.2	11.9	4.4	89	87	82	86	1.0	1.4	2.2	1.5	10	10 ●	0	WNW 1	C 0	C 0
21	80.5	83.0	84.8	82.8	12.1	15.4	8.1	10.9	17.4	7.1	61	55	76	64	5.6	7.9	2.5	5.3	9	9	0	W 3	NW 5	NW 1
22	86.0	87.5	89.5	87.7	6.6	11.5	7.2	8.1	12.2	5.2	85	32	62	60	1.4	9.2	3.9	4.8	9	8	0	W 1	NW 7	C 0
23	91.3	90.6	90.2	90.7	0.4	11.5	6.8	6.4	12.4	-0.7	84	42	60	62	1.0	7.9	4.0	4.3	0	5	0	W 2	ESE 2	ENE 3
24	95.7	99.0	100.6	98.4	2.2	2.7	0.9	1.5	6.8	0.4	73	68	62	68	2.0	2.3	2.5	2.3	10	10	10	ENE 10	E 17	E 14
25	100.4	101.0	100.3	100.6	-1.3	1.3	2.1	1.0	2.2	-1.8	70	68	61	66	1.7	2.1	2.8	2.2	10	10	10	ESE 14	ESE 10	E 7
26	100.1	99.1	99.1	99.4	0.4	7.9	2.6	3.4	9.2	-1.5	42	32	52	42	3.6	7.2	3.6	4.8	4	1	0	ESE 4	ESE 6	E 1
27	100.0	99.8	98.4	99.4	-0.4	11.9	5.4	5.6	12.0	-3.1	60	36	54	50	2.4	9.0	4.1	5.2	0 ⊙	0 ⊙	0	E 2	E 3	E 2
28	96.4	94.6	92.0	94.3	0.0	14.6	6.2	6.8	15.1	-1.7	74	23	41	46	1.6	12.8	5.7	6.7	0 ⊙	0 ⊙	0	C 0	S 6	S 2
29	89.6	88.6	88.1	88.8	7.3	10.9	7.0	8.0	13.0	3.7	35	26	61	41	6.6	9.7	3.8	6.7	7	9	1	WSW 1	SSW 3	SW 1
30	87.7	88.0	89.5	88.4	2.8	13.8	8.7	8.5	15.6	0.6	72	33	54	53	2.1	10.6	5.1	5.9	10	6	0	SSW 1	E 7	C 0
31	92.9	93.4	93.2	93.2	0.1	14.6	7.8	7.6	14.9	-2.2	80	31	61	57	1.3	11.4	4.1	5.6	3	3 ⊙	0	W 1	ENE 5	C 0
M	90.2	90.4	90.1	90.2	-0.2	5.6	2.4	2.6	7.2	-2.4	69	51	63	61	2.1	5.3	2.9	3.4	6.3	6.2	4.5	3.6	5.2	2.8

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1	94.3	93.8	92.8	93.6	2.3	16.1	9.1	9.2	16.9	0.4	65	25	50	47	2.5	13.7	5.9	7.4	0 ⊙	0 ⊙	0	E 2	E 5	E 3
2	93.2	92.6	92.8	92.9	1.0	18.3	11.1	10.4	18.8	-0.4	81	40	53	58	1.3	12.5	6.2	6.7	0 ⊙	0 ⊙	0	C 0	NE 3	C 0
3	95.1	96.1	97.1	96.1	1.7	17.1	10.5	10.0	17.7	-0.2	85	33	52	57	1.0	13.0	6.1	6.7	2 ⊙	6	0	C 0	E 4	C 0
4	99.6	99.5	98.6	99.2	1.2	16.1	11.1	9.9	17.6	-0.9	85	24	57	55	1.1	13.9	5.7	6.9	1 ⊙	0 ⊙	0	E 1	NE 3	NNE 4
5	98.9	97.4	93.4	96.6	2.6	15.7	10.3	9.7	16.9	0.0	86	41	47	58	1.1	10.5	6.6	6.1	0 ⊙	1 ⊙	0	WSW 2	E 5	C 0
6	88.9	85.3	81.7	85.3	2.3	20.7	14.2	12.8	21.0	-1.0	82	34	40	52	1.3	16.1	9.8	9.1	0 ⊙	0 ⊙	0	SW 1	WSW 2	S 1
7	78.5	77.5	79.4	78.5	12.1	16.3	7.9	11.0	17.7	7.3	50	45	90	62	7.1	10.1	1.0	6.1	9	3 ⊙	3	WNW 2	NW 7	N 7
8	84.1	85.8	85.5	85.1	4.4	5.1	1.9	3.3	7.9	1.4	68	57	76	67	2.7	3.8	1.7	2.7	10	10	1	NE 5	N 6	N 1
9	84.1	82.8	82.4	83.1	2.5	7.8	4.1	4.6	7.9	-1.1	67	44	82	64	2.4	5.9	1.5	3.3	6	10	10 ●	NW 5	NW 8	NW 1
10	82.3	79.5	73.9	78.6	1.7	9.7	6.9	6.3	12.1	0.7	72	56	56	61	1.9	5.3	4.3	3.8	10	3 ⊙	0	N 1	E 4	C 0
11	66.8	65.2	70.2	67.4	7.7	9.5	5.5	7.0	9.6	5.0	87	88	84	86	1.3	1.4	1.4	1.4	10 ●	10 ●	10 ●	C 0	E 1	NW 4
12	78.4	80.0	81.9	80.1	2.5	4.6	3.1	3.3	5.7	1.3	84	53	63	67	1.2	4.0	2.8	2.7	9	9	9	NW 2	NNW 5	NE 3
13	83.7	85.6	87.2	85.5	0.4	4.1	2.6	2.4	5.8	-0.4	84	59	63	69	1.0	3.3	2.7	2.3	10 *	9	0	NE 2	NE 2	W 1
14	89.2	88.9	87.6	88.6	1.6	4.7	3.3	3.2	5.6	-1.3	78	48	58	61	1.6	4.4	3.2	3.1	9	10	10	NW 3	NE 3	NE 3
15	87.8	88.8	91.9	89.5	0.6	5.4	3.3	3.2	5.6	-0.2	77	47	53	59	1.5	4.8	3.6	3.3	10 *	9	3	N 2	NE 6	NNW 4
16	94.2	94.1	93.7	94.0	0.0	6.1	5.2	4.1	8.1	-2.4	72	39	58	56	1.7	5.7	3.6	3.7	0	7	10	NW 2	NW 3	C 0
17	91.5	89.6	88.5	89.9	1.7	9.9	4.3	5.0	10.7	-0.6	74	54	85	71	1.8	5.7	1.2	2.9	9 ●	10	10 ●	C 0	NW 4	NE 1
18	86.7	86.4	86.4	86.5	0.7	3.3	2.4	2.2	4.3	0.0	88	73	84	82	0.7	2.1	1.2	1.3	10 *	10 ●	10	NE 1	NNW 5	W 2
19	86.5	87.0	87.7	87.1	3.5	7.3	5.0	5.2	8.9	1.4	81	63	78	74	1.4	3.7	1.9	2.3	10	9	0	W 4	W 3	C 0
20	90.2	91.1	94.5	91.9	3.7	12.6	8.5	8.3	13.6	0.7	78	48	81	69	1.8	7.5	2.1	3.8	9	9	10	C 0	C 0	C 0
21	96.8	97.5	98.3	97.5	5.5	10.5	9.0	8.5	10.7	5.0	88	65	75	76	1.1	4.4	2.9	2.8	10	9	10	NW 1	NNE 2	NE 1
22	99.6	98.8	98.5	99.0	3.7	14.3	10.1	9.6	15.1	1.8	92	43	73	69	0.7	9.3	3.4	4.5	10 ▬	9	0	E 1	E 6	E 1
23	97.7	97.3	96.4	97.1	7.3	11.5	11.5	10.4	13.6	6.7	86	76	75	79	1.5	3.3	3.5	2.8	10	10	10	NW 3	NNW 3	N 5
24	95.4	93.5	92.7	93.9	10.3	17.4	12.1	13.0	18.9	8.5	82	36	74	64	2.2	12.7	3.7	6.2	7	1 ⊙	0	C 0	NE 2	W 1
25	91.7	91.3	90.3	91.1	9.7	15.7	14.9	13.8	18.5	8.5	83	64	70	72	2.0	6.4	5.0	4.5	8	9	10 ●	W 1	NW 2	W 7
26	90.2	89.8	88.3	89.4	11.8	19.4	18.3	17.0	21.0	10.2	84	49	54	62	2.1	11.4	9.7	7.7	6	1	2	W 3	NNE 3	NW 3
27	88.9	87.8	87.5	88.1	9.3	23.2	15.2	15.7	23.2	6.9	91	32	58	60	1.1	19.2	7.3	9.2	0 ⊙ ▬	7	0	NW 1	SE 3	C 0
28	86.8	86.0	84.7	85.8	10.5	21.5	16.5	16.2	23.4	7.0	84	35	53	57	2.1	16.7	8.9	9.2	7	8	0	C 0	SW 3	C 0
29	85.9	85.3	86.1	85.8	15.7	24.8	16.3	18.3	25.2	8.5	62	28	68	53	6.7	22.4	6.0	11.7	0 ⊙	4 ⊙	4	C 0	S 4	E 1
30	85.9	83.0	80.7	83.5	14.5	25.7	18.0	19.0	25.7	8.4	66	29	51	49	5.7	23.3	10.1	13.0	0 ⊙	4	3	C 0	SSE 5	C 0
31																								
M	89.1	88.6	88.4	88.7	5.1	13.1	9.1	9.1	14.2	2.7	79	48	65	64	2.0	9.2	4.4	5.2	6.1	6.2	4.2	1.5	3.7	1.6

Przemyśl $H_s = 238$ m $H_b = 238.9$ m $h_w = 20$ m **Marzec – Mars 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU	USŁONECZNIENIE	° ○ G ○ ○ ▲
1	7	0.0	6	-	*° 16³⁶–⁵⁰ ≡ 21³⁰–24 = 6¹⁵–9⁴⁰ ⌴ n–a
2	8	2.1	6	-	*° 0⁰⁰–12¹⁵ 16³⁰–24
3	7	0.0	15	-	*° 0⁰⁰–8¹⁵ 20²⁹–24
4	7	.	10	-	*° 0⁰⁰–⁴⁰ = 5⁵⁰–10⁴⁴ 16⁴⁰–23¹⁵
5	7	0.0	6	-	*° 7⁰⁰–9³⁰
6	8	.	5	-	= 2³⁶–10¹⁰
7	8	.	pż.	-	= 5⁴⁵–9²⁰
8	8	.	pż.	-	
9	7	.	pż.	-	= 5⁴⁰–9⁵³ 16⁴⁵–19⁴⁰
10	7	.	pż.	-	= 1⁴⁰–12⁰⁶ 17³⁶–24 ⌴ n–a
11	7	.	pż.	-	= 0⁰⁰–10⁴⁰ 17³⁵–24 ⌴ n–a
12	7	.	pż.	-	= 0⁰⁰–12²⁰ ⌴ n–a ▽ 18⁵⁰–20⁵⁰
13	6	.	pż.	-	= 8³⁶–24
14	7	0.0	.	-	●° 20¹⁵ 21¹⁰ = 0⁰⁰–4²⁰
15	7	6.0	.	-	= 15⁵⁰–19³⁰
16	8	3.7	.	-	●° 1²⁵–8⁰⁷ ⁂°–10⁴⁵ *°–11²⁰ ⁂°–17⁵²
17	8	3.8	.	-	*° 6¹⁰–7⁰⁵ 18²⁵–20¹⁰ ●° 23⁴⁰–24
18	8	11.0	.	-	●° 0⁰⁰–³⁰ *°–¹⁰⁵ ●°–3³⁵ 7⁴⁰–10⁰⁷ 10²⁰ 11¹⁰ ▽ 12⁵⁵–13⁰⁸, 14⁵⁸–16⁴⁰, 17¹⁵–18⁵⁵, 19⁰⁸–20²⁵, ◹° 19²⁰–55
19	7	3.4	.	-	▽ 2⁴⁰–3¹⁰ ●° 19⁴⁰–24 = 17³⁰–24
20	2	0.3	.	-	●° 0⁰⁰–5²⁰ ⁂°–10⁵⁰–11⁵⁵ ●¹–12²⁰ ●°–12⁵⁰ = 0⁰⁰–11⁴⁵ ≡–14¹⁵ = –24
21	7	2.0	.	-	= 0⁰⁰–12⁰, 17²⁰–24
22	8	.	.	-	●° 2²⁰–3⁴⁵ = 0⁰⁰–7¹⁵ ≡°–8⁰⁰ = –8³⁰, 17²⁰–20¹⁰
23	7	.	.	-	= 4¹⁵–10²⁵, 17⁴⁰–21³⁰ ⌴ n–a
24	7	.	.	-	= 2³⁰–4²⁵ ≫ 6¹⁰–12²⁰ ≪–13⁴⁰ ≫–23¹⁰ ≪–24
25	7	0.0	.	-	●° 13⁵⁰ 15³⁸, 17⁴⁰ 19⁰⁵ ≪ 0⁰⁰–5⁴⁵ ≫–13³⁰
26	7	.	.	-	
27	7	.	.	-	= 6⁰⁸–7²⁰ ⌴ n–a, ⌓ do 22⁵⁰
28	8	.	.	-	= 1⁵⁰–8¹⁶ ⌴ n–a
29	7	.	.	-	
30	7	.	.	-	= 4³⁵–9⁴⁰
31	8	.	.	-	= 6²⁰–9¹³ ⌴ n–a
Σ	–	32.3	–	-	UWAGI

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1	7	.	.	-	
2	7	.	.	-	= 4⁴⁵–9³⁰ ⌴ n–a
3	7	.	.	-	= 3⁴⁰–10³⁰
4	7	.	.	-	= 4⁵⁰–10²⁵
5	8	.	.	-	= 6¹⁵–9³⁰ ⌓ n
6	7	.	.	-	= 2⁴⁵–9⁴⁰ ⌓ n–a
7	6	0.8	.	-	▽ 19⁴⁵–20²⁰ (◹) 18⁴⁵–19⁰⁰ ◹°–19²⁵, ∞ 12¹⁰–14⁴⁰
8	8	0.0	.	-	●° 3⁴⁰–4¹⁰ ●° 12⁴⁰ 14¹⁵ 16⁴⁰ 18²⁵
9	8	0.9	.	-	▽ 15⁰³⁻²⁵ 16¹⁶–²⁷ 17⁰⁵–⁵⁰ ●° 18⁵⁵ 19¹⁰ ●°20²⁰–21¹⁵ ●°–24, = 20²⁰–24
10	7	2.7	.	-	●° 0⁰⁰–7⁵⁰ *° 4⁴⁰–5⁴⁵ = 0⁰⁰–4¹⁵
11	4	22.4	.	-	●° 2⁴⁵–4³⁰ ●¹–6¹⁰ ●°–24 = 6⁴⁵–24
12	8	2.2	.	-	●° 0⁰⁰–4²⁰ 23¹⁸–24, = 0⁰⁰–4³⁰, 8³⁰–9²⁰
13	7	0.4	.	-	●° 0⁰⁰–2⁵⁰ ⁂°–5²⁵ *°–9⁴⁵
14	7	0.3	.	-	= 6⁴⁰–11²⁵
15	8	0.0	.	-	⁂° 0¹⁵–2³⁰ *°–6⁴⁰ ⁂°–7³⁵ ▽° 8⁵⁰–9⁰³
16	7	0.0	.	-	= 6⁰⁵–8²²
17	6	3.3	.	-	▽ 6²⁷–7¹⁵ ●° 13¹⁰–24, = 7¹⁰–24
18	6	0.2	.	-	●° 0⁰⁰–2²⁵ *°–7³⁵ ⁂°–8²⁰ 9⁴⁰–10⁴⁵ 12²⁰–13⁰⁷ 15⁴⁵–16⁴⁵ = 0⁰⁰–8³⁰
19	7	(0.0)	.	-	●° 1⁰⁰–¹⁵ 2⁴⁰ 3⁵⁰ 6⁴⁵–10³⁰
20	7	1.1	.	-	▽ 12⁵⁵–14⁵⁰, 15⁰⁷–16³⁵ = 1³⁰–4³⁰ 5¹⁰–10²⁰ 17³⁰–20⁴⁰ ⌓ n
21	7	.	.	-	●° 4³⁰–5¹⁰ = 3²⁰–10³⁰ 18¹⁰–24
22	7	.	.	-	= 0⁰⁰–2⁵⁰ ≡²–8¹⁵ = –9¹⁷
23	6	0.0	.	-	●° 10¹⁰–11⁰⁵ ●° 18⁵⁰–21¹⁰, = 4¹⁵–24
24	6	.	.	-	= 0⁰⁰–12⁵⁰ 17²⁰–20³⁰
25	6	0.2	.	-	●° 20²⁰–21²⁵, = 5²⁰–24, ⌓ n–a
26	6	.	.	-	= 0⁰⁰–24
27	7	0.0	.	-	▽ 13²⁰–⁴², = 0⁵⁰–3⁵⁰ ≡°–4²⁰ ≡²–7²⁰ = –9³⁰ ∞–10²⁵, ⌓¹ n–a
28	8	.	.	-	⌓ n–a
29	8	1.4	.	-	▽ 14⁴⁵–15¹⁰ (◹) 14³⁰–45 ◹°–15¹⁰ ⌓ na
30	8	0.0	.	-	▽ 10¹⁶–55 (◹) 11⁰⁰–50 ↘ 21⁴⁵–22¹⁵ ⌓¹ n–a
31					
Σ	–	35.9	–	-	UWAGI

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ Maj – Mai 1957

DNI	CIŚNIENIE P – 900 –				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	87.0	88.4	87.9	87.8	7.1	7.7	7.1	7.2	18.5	6.0	70	60	85	72	3.1	4.2	1.5	2.9	10	10	10 ●	NW 7	NW 3	W 1
2	86.5	85.7	84.1	85.4	4.4	5.4	5.1	5.0	7.5	3.9	85	84	89	86	1.3	1.4	1.0	1.2	10 ●	10 ●	10	ENE 6	ENE 7	NE 4
3	81.9	82.5	82.3	82.2	5.0	6.6	6.4	6.1	6.9	4.3	90	84	84	86	0.8	1.5	1.6	1.3	10 ●	10	10	NNE 4	NNE 2	C 0
4	80.9	80.6	82.9	81.5	6.8	12.3	9.4	9.5	13.4	5.3	84	58	51	64	1.6	6.1	5.7	4.5	10	9	1	NW 1	WNW 3	WNW 4
5	85.5	85.0	83.4	84.6	5.7	9.7	5.3	6.5	11.1	2.6	61	34	66	54	3.6	7.9	3.0	4.8	6	5	4	WNW 4	W 6	N 1
6	80.0	79.2	80.7	80.0	5.1	5.6	3.6	4.5	5.8	3.0	87	85	81	84	1.1	1.4	1.5	1.3	10 ●	10 ●	10 ●	E 1	W 2	W 3
7	79.6	78.1	76.5	78.1	1.0	1.9	2.5	2.0	3.6	0.2	88	87	84	86	0.8	0.9	1.2	1.0	10 *	10 ●	10 ●	NW 1	NW 2	NW 4
8	74.4	75.4	77.9	75.9	2.2	4.3	4.4	3.8	4.6	1.4	87	85	87	86	1.0	1.2	1.1	1.1	10 ●	10 ●	10 ●	WNW 3	NW 5	NW 3
9	78.3	78.6	78.5	78.5	4.1	5.2	4.4	4.5	5.2	3.5	87	84	87	86	1.1	1.4	1.1	1.2	10 ●	10	10	NW 6	NW 6	WNW 5
10	75.9	78.7	84.2	79.6	5.5	6.4	6.3	6.1	6.4	3.8	88	82	81	84	1.1	1.7	1.8	1.5	10	10	10	W 5	W 7	WSW 2
11	87.4	89.2	89.4	88.7	6.9	11.8	10.1	9.7	13.5	5.0	85	68	76	76	1.4	4.4	3.0	2.9	9	10	2	C 0	C 0	C 0
12	90.1	90.4	90.8	90.4	5.3	18.8	12.7	12.4	20.5	1.4	91	44	70	68	0.8	12.2	4.4	5.8	1	7	1	SW 1	W 3	C 0
13	90.5	89.7	88.6	89.6	10.0	20.6	15.0	15.2	21.9	5.5	89	48	72	70	1.3	12.6	4.7	6.2	8	3	0	WSW 2	S 3	NE 1
14	88.6	90.0	90.7	89.8	12.8	21.5	16.7	16.9	22.3	7.4	72	38	72	61	4.1	15.8	5.4	8.4	0	2 ⊙	4	W 3	NW 4	NW 6
15	93.4	93.4	92.5	93.1	13.9	20.0	15.3	16.1	21.0	9.7	82	39	63	61	2.9	14.2	6.5	7.9	1 ⊙	4 ⊙	0	W 3	N 3	NE 2
16	92.5	90.4	88.3	90.4	10.6	20.1	13.3	14.3	20.4	5.9	84	40	73	66	2.1	14.0	4.2	6.8	4 ⊙	7 ⊙	4	NE 1	ESE 7	E 1
17	87.0	86.9	87.1	87.0	12.6	20.6	15.0	15.8	21.8	6.8	76	44	73	64	3.6	13.5	4.5	7.2	5	6	2	E 2	E 4	NE 1
18	87.7	86.9	83.7	86.1	13.2	22.4	15.7	16.8	22.7	8.8	85	55	78	73	2.3	12.2	3.9	6.1	2 ⊙	5 ⊙	8	W 2	NNE 3	N 3
19	81.7	81.5	80.4	81.2	15.4	17.8	14.4	15.5	19.4	10.7	84	70	86	80	2.8	6.1	2.4	3.8	9	8	1	E 4	E 8	E 2
20	81.1	81.8	82.7	81.9	12.9	18.4	14.4	15.0	20.0	10.7	93	72	92	86	1.1	5.9	1.3	2.8	9	9	2	E 3	E 3	SE 2
21	85.0	86.3	86.7	86.0	14.3	12.3	10.2	11.8	14.4	9.8	89	89	97	92	1.8	1.5	0.3	1.2	9	10	10	W 5	W 5	W 3
22	84.8	84.6	84.2	84.5	10.0	12.6	13.4	12.4	14.4	9.3	97	88	90	92	0.3	0.7	1.6	0.9	10 ●	10	10	WNW 1	NW 1	NW 1
23	83.8	82.7	81.6	82.7	13.1	20.3	16.5	16.6	22.0	12.0	89	59	80	76	1.6	9.8	3.9	5.1	10	7 ⊙	8	NW 1	NE 2	C 0
24	82.2	83.3	85.8	83.8	13.2	18.4	14.0	14.9	18.8	9.7	96	68	80	81	0.6	6.8	3.2	3.5	8	9	10	NW 2	N 6	NNE 6
25	89.0	91.0	92.9	91.0	8.6	11.8	8.7	9.4	14.0	7.4	81	44	63	63	2.2	7.7	4.1	4.7	10	8	9	NNE 7	NE 8	NE 4
26	93.4	93.6	94.4	93.8	7.2	11.0	7.2	8.2	11.4	5.2	76	46	65	62	2.5	7.0	3.6	4.4	9	9	9	NE 4	NE 7	NE 5
27	92.9	93.5	93.3	93.2	5.8	5.5	5.1	5.4	7.2	4.4	86	91	94	90	1.3	0.8	0.6	0.9	10 ●	10 ●	10	ENE 7	NE 7	ENE 2
28	91.1	90.4	89.0	90.2	5.5	7.7	7.2	6.9	8.4	4.0	92	80	94	89	0.7	2.1	0.6	1.1	10	10	10 ●	ENE 2	NE 2	NE 5
29	88.2	91.5	92.2	90.6	5.8	10.4	7.8	8.0	12.8	5.2	89	62	83	78	1.0	4.8	1.8	2.5	10 ●	9	6	N 6	NNW 4	NE 1
30	94.0	94.2	93.4	93.9	7.6	15.0	10.0	10.6	15.9	1.8	69	45	74	63	3.2	9.3	3.2	5.2	4 ⊙	7	9	W 3	W 2	C 0
31	93.5	92.2	89.6	91.8	10.6	18.1	14.5	14.4	19.6	3.1	75	33	63	57	3.2	14.0	6.2	7.8	1 ⊙	8	8	W 1	ESE 3	E 1
M	86.1	86.3	86.3	86.2	8.5	12.9	10.1	10.4	14.4	5.7	84	63	78	75	1.8	6.6	2.9	3.8	7.6	8.1	6.7	3.2	4.1	2.4

Czerwiec – Juin

1	87.6	87.4	87.7	87.6	12.0	18.6	13.0	14.2	20.2	8.8	83	52	79	71	2.3	10.2	3.1	5.2	9	7 ⊙	0	WSW 1	N 5	NW 1
2	89.5	90.1	91.1	90.2	13.2	21.0	17.2	17.2	21.6	8.6	75	41	59	58	3.8	14.7	8.0	8.8	7	6	8	WNW 5	WNW 6	WNW 1
3	93.7	92.9	90.6	92.4	14.6	24.4	18.7	19.1	25.8	10.0	77	37	61	58	3.8	19.3	8.4	10.5	0 ⊙	3 ⊙	2	W 1	WNW 3	C 0
4	88.7	85.7	83.6	86.0	19.0	26.3	18.5	20.6	26.5	16.0	73	42	83	66	6.0	19.8	3.5	9.8	6	8	9	C 0	SSW 6	C 0
5	79.8	79.2	79.7	79.6	16.8	18.0	13.5	15.4	19.7	13.1	95	68	90	84	1.0	6.5	1.6	3.0	9	9	3	SW 1	W 7	C 0
6	80.3	82.0	86.4	82.9	12.2	18.2	12.0	13.6	18.7	8.8	92	47	69	69	1.2	11.1	4.3	5.5	9	4	0	W 5	WNW 6	NW 1
7	87.9	86.5	84.9	86.4	12.8	21.6	16.7	17.0	23.2	4.5	70	46	70	62	4.4	13.8	5.7	8.0	1 ⊙	6 ⊙	5	WNW 1	SSW 5	C 0
8	85.5	86.2	87.2	86.3	14.5	20.4	16.4	16.9	23.0	10.6	87	67	87	80	2.2	7.9	2.5	4.2	9	8 ●	4	W 1	SW 2	SE 3
9	87.0	85.9	85.1	86.0	17.3	26.4	20.6	21.2	26.7	11.7	81	50	71	67	3.7	17.2	7.1	9.3	3	3	10	SSE 1	E 6	C 0
10	86.1	86.4	86.6	86.4	16.2	23.0	18.9	19.2	26.0	15.2	95	72	81	83	1.0	7.8	4.1	4.3	10	5	2	C 0	SSE 3	S 1
11	86.7	86.2	86.5	86.5	21.0	29.6	22.6	24.0	30.4	14.5	75	43	67	62	6.2	23.6	9.0	12.9	2 ⊙	2 ⊙	9	S 1	S 5	W 1
12	89.6	92.0	95.9	92.5	22.4	30.9	24.6	25.6	31.5	15.8	78	56	77	70	6.1	19.5	7.0	10.9	3 ⊙	2 ⊙	9	C 0	S 1	NW 3
13	101.0	100.3	98.2	99.8	17.2	19.4	15.2	16.8	24.6	14.3	67	71	69	69	6.5	6.4	5.3	6.1	8	10	1	NNE 4	N 6	NNW 3
14	98.3	97.6	97.2	97.7	12.6	19.0	15.9	15.8	21.0	9.0	86	52	65	68	2.1	10.5	6.3	6.3	6	1 ⊙	0	NNW 6	NNW 4	N 1
15	98.1	97.5	95.8	97.1	14.0	19.8	14.7	15.8	22.1	9.5	68	50	73	64	5.1	11.5	4.5	7.0	8	5 ⊙	0	N 2	N 5	C 0
16	95.2	94.2	91.8	93.7	12.6	21.7	17.3	17.2	23.0	6.7	89	49	70	69	1.6	13.3	6.0	7.0	0	0 ⊙	0	NNE 2	N 3	NE 1
17	91.6	90.7	89.3	90.5	16.0	23.1	17.5	18.5	24.0	9.0	78	51	71	67	4.0	13.9	5.9	7.9	2 ⊙	3 ⊙	0	W 2	NE 4	C 0
18	89.7	88.8	86.6	88.4	15.9	24.8	19.7	20.0	25.5	8.8	79	40	72	64	3.8	18.9	6.5	9.7	0 ⊙	0 ⊙	0	C 0	E 5	E 1
19	85.0	84.5	83.1	84.2	20.4	23.4	19.8	20.8	26.0	11.5	69	63	79	70	7.5	10.8	4.9	7.7	7 ⊙	8	6	SW 3	W 3	W 2
20	83.6	83.6	87.2	84.8	20.2	25.0	16.0	19.3	25.4	15.0	75	56	95	75	5.9	13.9	1.0	6.9	5	5	2	W 3	NW 6	NW 1
21	90.3	89.7	86.8	88.9	13.3	21.2	17.9	17.6	22.7	10.8	99	54	74	76	0.2	11.6	5.4	5.7	10 =	5	9	NW 1	E 4	E 1
22	83.7	81.5	80.0	81.7	21.0	26.6	18.7	21.2	27.6	12.2	75	58	92	75	6.2	14.6	1.7	7.5	5	5 ⊙	10 ☈	SE 2	SSW 6	SW 3
23	82.9	84.1	82.6	83.2	19.9	24.9	21.1	21.8	27.0	15.8	82	56	76	71	4.1	13.8	6.0	8.0	2 ⊙	3	9	WSW 2	W 3	C 0
24	83.5	81.7	78.0	81.1	20.6	29.5	25.2	25.1	29.5	18.2	78	53	71	67	5.2	19.5	9.3	11.3	6	8	2	W 3	S 5	SSW 4
25	80.1	82.3	86.7	83.0	21.8	24.0	17.1	20.0	25.4	16.2	76	48	70	65	6.4	15.4	5.8	9.2	3	6	7	W 6	WNW 5	NW 3
26	90.2	91.1	93.2	91.5	11.5	15.2	12.7	13.0	17.2	10.6	93	72	77	81	1.0	4.8	3.4	3.1	10	9	1	NW 4	NW 3	NW 1
27	95.4	94.9	96.5	95.6	13.2	17.6	13.3	14.4	18.6	8.2	74	55	79	69	4.0	9.0	3.2	5.4	1 ⊙	8	2	NW 2	N 5	NNW 4
28	97.8	96.9	94.8	96.5	11.6	19.0	18.0	16.6	21.0	6.7	91	54	75	73	1.1	10.2	5.0	5.4	1	4 ⊙	9	W 3	W 3	C 0
29	94.4	94.0	93.6	94.0	19.0	25.7	20.3	21.3	27.1	14.0	80	58	85	74	4.4	13.9	3.5	7.3	0	3	0	W 4	WNW 6	C 0
30	93.9	92.2	90.6	92.2	19.8	29.1	23.9	24.2	29.6	13.9	82	56	73	70	4.1	17.6	8.4	10.0	0	3	2	W 3	W 4	W 2
31																								
M	89.2	88.9	88.6	88.9	16.4	22.9	17.9	18.8	24.4	11.6	81	54	75	70	3.8	13.4	5.2	7.5	4.7	5.0	4.0	2.3	4.5	1.3

Przemyśl $H_s = 238$ m $H_b = 238.9$ m $h_w = 20$ m **Maj – Mai 1957**

DNI	WILGOTNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	3	3.2	.	-	$\bullet^0$ 1⁰⁰–⁴⁵ 3¹²–⁴³⁰ 8²⁰–⁹¹⁵ 15⁵⁵–23⁴⁰
2	7	10.4	.	-	$\bullet^0$ 0²⁰–8³⁰ $\bullet^1$ 11²⁰ $\bullet^0$–20¹⁵ $\bullet^0$ 22⁵⁰–23⁴⁰ $\bullet^1$–24
3	7	0.7	.	-	$\bullet^1$ 0⁰⁰–¹⁵ $\bullet^1$–1²⁰ $\bullet^0$–2⁴⁵ 4⁴⁰–7¹⁰ $\bullet^0$–10¹⁰ 11¹²–⁴² $\bullet^0$–12¹⁵ 12⁴⁸–13³⁰ = 2⁴⁵–10⁴⁰ 23⁵⁰–24
4	7	.	.	-	= 0⁰⁰–3¹⁵
5	8	1.4	.	-	
6	6	27.8	.	-	$\bullet^0$ 0⁴⁶–¹²⁰ $\bullet^0$ 4³⁰–21³⁰ $\ast^1$–23²⁰ $\ast^0$–24
7	6	9.9	p2.	-	$\ast^0$ 0⁰⁰–¹⁴⁵ $\ast^0$ 2¹⁵–⁴⁴⁵ $\ast^0$–6³⁵ $\ast^0$–7¹² $\bullet^0$ 8⁴⁶–9¹⁸ 11⁰⁰–12⁴⁰ 14³⁴–⁵⁰ 15²⁶–⁴⁶ 17¹⁶–24 = 6⁴⁰–15⁴⁰
8	6	3.1	.	-	$\bullet^0$ 0⁰⁰ 7³⁰ $\bullet^0$–8²⁰ $\bullet^0$–9⁴⁰ $\bullet^1$–10³⁰ $\bullet^0$–12⁵⁰ 13¹⁰–24 = 0⁰⁰–24
9	6	14.0	.	-	$\bullet^0$ 0⁰⁰–2²⁰ $\bullet^0$–5⁴⁵ 5⁵⁰–9⁴⁰ $\bullet^1$–9⁵⁰ $\bullet^0$–12⁰⁵ 12⁵⁰–20²⁰ 20⁴⁰–23⁰⁰
10	7	2.0	.	-	$\bullet^0$ 0⁵⁰–¹¹⁸ 3²⁵–⁵⁴⁵ 6³⁸–10¹⁵
11	7	.	.	-	$\bullet^0$ 0⁰⁰–2¹⁵ = 5³⁰–8⁴⁴ 18²⁸–23⁵⁰ ≡–24
12	7	0.0	.	-	$\triangledown$ 14⁰⁰–⁰⁵ ≡ 0⁰⁰–4⁵⁵ = –10²⁰
13	7	.	.	-	= 1³⁰–10²⁵ 19⁴⁰–24 ⌒ n – a
14	7	0.0	.	-	$\bullet$ 15⁵⁰–16¹⁴ = 0⁰⁰–3⁴⁰ 4¹⁰–7⁴⁰ ⌒ n – a
15	8	.	.	-	= 22⁴⁰–24 ⌒ n – a
16	8	.	.	-	= 0⁰⁰–8²⁰ 22³⁰–24 ⌒^{1} n – a
17	8	.	.	-	= 0⁰⁰–8⁵⁰ 22¹⁰–24 ⌒ n – a
18	7	1.1	.	-	$\triangledown^1$ 17⁴⁵–18¹⁰ (K) 16⁴⁰–17⁴⁵ K⁰–18³⁵ = 0⁰⁰–12²⁰
19	8	.	.	-	
20	7	0.0	.	-	$\bullet$ $\triangledown$ 14²⁵–³⁸ $\bullet^0$ 18²⁴–³⁶ = 3²⁵–9²⁰ ⌒^{1} n – a
21	6	0.0	.	-	$\bullet^0$ 11³⁰–12¹⁰ 18¹⁰–19¹⁸ = 4⁴⁰–24
22	6	0.0	.	-	$\bullet^0$ 0⁴⁰ 1⁰⁰ $\bullet^0$ 4⁵⁰–7²⁵ = 0⁰⁰–6⁴⁰ ≡^{1}–7⁴⁰ ≡^{0}–8²⁵ =–24
23	8	.	.	-	= 0⁰⁰–9¹⁹ 22⁴⁰–24
24	7	0.4	.	-	$\bullet^0$ 22⁵⁰–24 = 0⁰⁰–4⁴⁰ ≡^{1}–6²⁵ =–8⁵⁰ ⌒^{1} n–a
25	8	..	.	-	$\bullet^0$ 0⁰⁰–4⁴⁵ $\bullet^0$–5⁴⁰
26	8	0.0	.	-	
27	7	6.7	.	-	$\bullet^0$ 5⁵⁰–8⁰⁸ 8³⁰–10¹⁰–17²⁴
28	7	4.0	.	-	$\bullet^0$ 6⁵⁵–7³⁵ 8⁴⁸–9³⁵ 14¹⁸–15⁴⁵ 17⁵⁰ 23⁴⁰ = 3⁴⁰–6⁴⁵
29	8	1.4	.	-	$\bullet^0$ 0⁵⁰–9¹⁰ $\bullet^1$–9²⁵ $\bullet^0$–9⁵⁰ $\triangledown^0$ 14⁵⁵–15⁰⁸
30	8	.	.	-	⌒^{1} n – a
31	8	.	.	-	= na ⌒ na
Σ	–	86.1	–	-	UWAGI.

Czerwiec – Juin

1	8	.	.	-	= 3⁴⁵–7¹⁰
2	6	.	.	-	= 8⁴⁰–9⁵⁰ ∞–17⁴⁰
3	7	.	.	-	= 1⁵⁰–11⁵⁰
4	7	12.3	.	-	$\triangledown$ 17¹⁶–¹⁹ 17⁴³–⁵⁰ 22⁵⁰–24 = 0³⁰–12⁴⁰ 19³⁶–23⁴⁰
5	7	0.8	.	-	$\triangledown$ 0⁰⁰–¹³⁰ 2²⁰–3³⁰ $\bullet^0$–7²⁰ 9⁴⁰–10⁰² $\triangledown$ 14¹⁰–⁴⁵ = 20⁴⁰–24
6	7	0.0	.	-	$\triangledown$ 15²⁰–³⁸ = 0⁰⁰–10²⁰
7	8	.	.	-	= 1⁵⁰–7²⁰ ⌒ n – a
8	6	26.7	.	-	$\triangledown$ 10⁴³–⁵³ 13²⁰–⁵⁸ 15⁰⁸–¹² 15²⁰–²⁸ $\triangledown^1$ 15³² $\triangledown^0$–17⁵⁸ $\triangledown^1$–18⁰⁶ $\triangledown$–19³⁵ (K)^0 11⁵⁰–12¹⁰ K⁰–19⁴⁰ SE-S-E = 3³⁰–11⁴⁰
9	8	6.5	.	-	(K) 16⁵⁵–17⁴⁵
10	8	2.8	.	-	$\bullet^0$ 2⁴⁵–3⁴⁰ $\bullet$ 14¹⁵–7²⁵ $\bullet^0$ 8⁰⁵–⁴⁰ $\bullet^1$–9¹⁵ $\bullet^0$–9²⁵ $\triangledown$ 11⁴²–⁵⁰ 17⁵⁰–18⁰⁵
11	8	.	.	-	= 2⁴⁵–3⁵⁰ ⌒^{0} n – a
12	8	0.0	.	-	$\triangledown$ 20⁰⁷–¹⁴ K^0 19³⁵–21⁴⁰ NW = 6²⁰–8⁵²
13	8	.	.	-	= 4⁴⁵–6⁵⁰
14	8	.	.	-	
15	8	.	.	-	
16	8	.	.	-	⌒ n – a
17	8	.	.	-	⌒ n – a
18	8	.	.	-	⌒^{2} n – a
19	8	.	.	-	⌒^{0} n – a
20	7	7.8	.	-	$\triangledown$ 14³⁴–³⁷ $\triangledown^1$–14⁴⁰ $\triangledown^0$–15¹² $\triangledown$ 15⁵⁰–16¹⁰ 16³⁶–⁵² 17⁵⁰–18¹⁰ K 14³⁴–15⁴⁰ SW–NE = 23⁴⁰–24
21	8	.	.	-	= 0⁰⁰–1⁵⁰ ≡^{1}–2⁴⁰ ≡^{2}–8⁵⁵ =–9²⁰
22	7	7.9	.	-	$\triangledown^0$ 21¹⁶–23⁵⁸ (K)^0 20⁵⁰–21¹² K^1 21¹²–21⁴⁰–22⁵⁰
23	8	.	.	-	
24	8	12.2	.	-	
25	8	1.1	.	-	$\triangledown$ 2⁰²–¹⁰ 2⁴⁰–3⁴⁰ 6³⁷–⁵⁵ 17²⁰–18⁴⁰ (K) 1⁵⁰–2⁵⁰ K^1–3²⁵ K^0–3⁴⁵ S-SE
26	7	0.0	.	-	$\bullet^0$ 6³⁵–⁵⁰
27	8	.	.	-	⌒ np
28	8	.	.	-	= 2²⁰–8²⁰ ⌒ na
29	7	.	.	-	= 2⁵⁰–13²⁰
30	7	.	.	-	= 0²⁰–5⁴⁰ 23⁵⁰–24
31					
Σ	–	78.1	–	-	UWAGI.

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ Lipiec – Juillet 1957

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	92.1	91.7	90.7	91.5	20.5	26.6	20.7	22.1	27.6	15.5	84	58	78	73	3.8	14.6	5.3	7.9	2 ⊙	3	0	W 1	NNW 3	C 0
2	90.9	89.2	87.9	89.3	18.8	27.9	22.8	23.1	28.9	13.1	80	52	75	69	4.3	18.0	6.8	9.7	0	1 ⊙	10	NE 1	NE 1	SE 2
3	89.5	91.0	91.6	90.7	18.2	22.8	16.8	18.6	24.4	16.2	98	47	73	73	0.4	14.7	5.2	6.8	10	1	1	NW 4	NW 6	C 0
4	92.4	91.3	90.6	91.4	15.2	25.4	21.8	21.0	27.9	8.3	86	47	76	70	2.1	17.0	6.1	8.4	4 ⊙	2	0	SW 1	E 2	C 0
5	89.5	88.1	87.5	88.4	24.8	32.3	28.2	28.4	33.0	16.9	71	53	63	62	9.2	22.7	14.3	15.4	1 ⊙	0 ⊙	9 (R)	WSW 5	SW 7	WSW 4
6	90.7	91.2	91.7	91.2	21.9	26.2	19.5	21.8	28.2	19.0	95	64	70	76	1.5	12.1	6.9	6.8	2	2	0	W 2	NW 6	NNW 2
7	93.2	92.9	92.1	92.7	17.0	26.8	20.3	21.1	27.4	10.2	85	47	79	70	3.0	18.8	5.0	8.9	1 ⊙	8	0	SW 1	NE 3	C 0
8	91.8	90.2	87.2	89.7	18.8	30.7	25.6	25.2	32.0	13.0	80	44	69	64	4.3	24.6	10.2	13.0	0 ⊙	0 ⊙	6	NE 1	E 6	C 0
9	88.2	84.4	85.3	86.0	20.2	27.5	20.6	22.2	28.8	17.8	92	65	92	83	2.0	12.9	2.0	5.6	10	4 ⊙	9	NNW 3	W 3	NW 5
10	85.7	84.4	81.7	83.9	17.8	23.0	18.8	19.6	24.1	16.0	94	59	82	78	1.2	11.7	3.9	5.6	10	3	4	NW 1	ENE 4	ENE 4
11	79.2	79.3	78.0	78.8	17.3	20.8	20.2	19.6	23.2	14.3	87	93	97	92	2.6	1.9	0.7	1.7	10	10 •	10 R	ENE 1	E 1	C 0
12	79.2	81.3	82.8	81.1	18.6	22.0	17.8	19.0	24.4	16.2	95	90	99	95	1.0	2.6	0.2	1.3	8	10	9	E 1	E 2	E 1
13	85.4	86.5	87.9	86.6	19.0	26.7	20.2	21.5	27.5	15.8	99	64	90	84	0.2	12.6	2.5	5.1	7	4	8	ENE 1	NW 1	W 2
14	87.8	86.7	86.2	86.9	20.0	26.1	17.3	20.2	26.8	16.2	91	56	94	80	2.2	14.8	1.2	6.1	3	5	6	W 2	NNW 3	C 0
15	84.6	83.8	84.2	84.2	18.1	24.8	19.7	20.6	25.5	15.7	91	60	93	81	1.9	12.4	1.5	5.3	3	7	10 •	N 3	W 3	W 1
16	80.4	78.0	78.6	79.0	18.4	20.2	16.2	17.8	23.2	15.7	97	86	92	92	0.7	3.3	1.6	1.9	10	9 •	10	C 0	S 4	W 5
17	80.5	80.8	82.2	81.2	14.6	18.4	15.4	16.0	19.1	12.7	90	62	68	73	1.6	8.2	5.7	5.2	9	8	9	SW 3	SW 7	WSW 5
18	83.0	83.5	83.3	83.3	15.6	18.4	15.8	16.4	21.3	12.2	80	69	76	75	3.5	6.7	4.3	4.8	10	9	3	W 4	W 5	W 3
19	83.8	83.2	83.1	83.4	17.6	25.1	18.2	19.8	25.4	13.1	74	43	74	64	5.1	18.1	5.5	9.6	0	2	1	W 3	SW 3	SW 1
20	82.1	79.9	76.9	79.6	19.4	26.4	20.9	21.9	27.5	14.1	76	47	69	64	5.4	18.3	7.6	10.4	1 ⊙	6 ⊙	7	NE 1	SE 7	C 0
21	76.7	76.5	77.1	76.8	16.4	18.1	15.0	16.1	20.9	14.4	95	89	94	93	0.9	2.3	0.9	1.4	10 •	10 •	8	SW 1	SW 1	W 1
22	75.7	75.8	75.3	75.6	15.3	16.3	15.2	15.5	20.6	13.3	93	87	97	92	1.2	2.5	0.6	1.4	10	10 R •	9	W 1	S 4	S 1
23	75.3	76.1	77.4	76.3	14.4	18.6	16.5	16.5	20.7	13.4	94	76	80	83	0.9	5.1	3.9	3.3	9	10	9	NNE 1	S 1	SW 1
24	78.7	79.0	81.8	79.8	16.2	22.3	15.6	17.4	23.0	13.5	86	66	97	83	2.5	9.3	0.6	4.1	9	8	10 •	W 4	SW 5	W 6
25	84.2	84.7	84.5	84.5	14.5	20.3	15.3	16.4	21.0	11.4	91	67	98	85	1.5	7.8	0.4	3.2	5	8	9	W 4	W 4	W 1
26	82.7	83.9	83.1	83.2	16.6	19.6	16.5	17.3	21.5	12.1	85	63	80	76	2.9	8.5	3.9	5.1	10	4	5	W 3	WNW 6	WNW 1
27	81.6	80.5	78.9	80.3	16.2	20.9	18.4	18.5	22.5	14.2	80	69	88	79	3.6	7.6	2.5	4.6	9	10	10 •	W 2	SW 5	SW 2
28	80.7	82.1	82.6	81.8	14.1	16.0	14.2	14.6	18.4	12.8	91	89	90	90	1.5	2.0	1.6	1.7	9 •	9	8	W 3	W 2	W 1
29	84.7	84.9	87.4	85.7	14.3	21.4	16.3	17.1	23.5	9.5	92	61	81	78	1.3	9.8	3.4	4.8	1 ⊙	5	8	SW 1	ESE 3	W 2
30	88.6	88.9	90.3	89.3	13.7	22.0	16.9	17.4	22.6	10.6	93	64	81	79	1.1	9.6	3.7	4.8	7 ⊙	7	4	W 4	WNW 1	NW 2
31	92.1	92.6	94.4	93.0	15.2	20.8	17.1	17.6	21.6	13.7	92	70	86	83	1.3	7.4	2.8	3.8	10	3	5	WNW 2	W 4	W 1
M	84.9	84.6	84.6	84.7	17.4	23.0	18.5	19.4	24.6	13.9	88	65	83	79	2.4	10.9	3.9	5.7	6.1	5.7	6.4	2.1	3.6	1.7

Sierpień – Août

1	95.6	95.8	94.5	95.3	15.6	19.5	16.0	16.8	20.9	14.2	91	72	88	84	1.5	6.3	2.1	3.3	10	7	0	NW 3	NW 6	WNW 2
2	94.1	92.2	91.4	92.6	14.2	22.2	18.8	18.5	23.9	10.1	93	66	80	80	1.1	9.1	4.3	4.8	0	7 ⊙	10	W 2	NW 4	NW 3
3	92.7	91.7	91.9	92.1	14.4	18.5	14.9	15.7	20.1	11.6	79	59	75	71	3.4	8.7	4.1	5.4	0 ⊙	6	8	W 2	NW 3	NW 1
4	92.0	91.7	92.1	91.9	13.5	19.6	15.7	16.1	21.0	10.0	88	61	81	77	1.8	8.8	3.4	4.7	6 ⊙	9	9	W 2	NW 3	WNW 2
5	92.6	93.1	92.9	92.9	14.8	15.8	15.1	15.2	19.3	12.4	94	85	97	92	0.9	2.6	0.6	1.4	7	10 •	9	W 3	NW 3	NW 2
6	93.4	93.0	91.9	92.8	15.5	21.5	15.9	17.2	22.7	12.3	90	61	88	80	1.7	10.0	2.1	4.6	1 ⊙	4 ⊙	1	W 3	NW 4	NW 1
7	91.0	88.3	84.4	87.9	12.7	24.5	19.1	18.8	25.3	9.0	98	62	78	79	0.4	11.6	4.8	5.6	2 ⊙	6	5	SW 1	NE 1	C 0
8	79.9	80.7	81.6	80.7	16.8	20.4	16.4	17.5	21.0	15.8	97	72	92	87	0.6	6.7	1.5	2.9	9 (R)	3 ⊙	4	W 2	NW 7	C 0
9	82.4	82.7	80.6	81.9	14.3	21.6	17.3	17.6	22.6	11.6	98	73	89	87	0.4	7.0	2.2	3.2	7	5	1	W 2	NE 3	E 1
10	77.0	75.0	81.4	77.8	16.7	28.6	16.0	19.3	28.6	14.7	95	58	97	83	1.0	16.5	0.6	6.0	8	2	0	E 1	SW 7	W 2
11	87.1	87.9	87.6	87.5	18.0	27.4	21.8	22.2	27.9	13.4	85	53	68	69	3.0	17.2	8.3	9.5	0	4	0	W 1	W 4	SW 1
12	86.2	84.3	84.0	84.8	19.0	29.6	21.6	23.0	30.0	13.5	83	50	94	76	3.8	20.5	1.6	8.6	3	3	2	C 0	S 5	W 1
13	86.6	87.8	87.2	87.2	19.4	24.8	21.0	21.6	26.0	17.5	97	68	88	84	0.6	10.2	3.0	4.6	9	3	2	NW 1	NNW 3	C 0
14	84.7	83.0	80.7	82.8	20.4	31.5	22.0	24.0	32.5	17.2	91	62	97	83	2.3	17.5	0.7	6.8	5	1 ⊙	0	ENE 1	N 1	C 0
15	81.7	82.0	82.7	82.1	18.0	21.4	17.1	18.4	24.5	16.5	96	83	98	92	0.8	4.3	0.4	1.8	9	9	0	W 4	WNW 2	C 0
16	83.7	83.0	82.0	82.9	14.4	24.6	18.6	19.0	25.3	11.9	99	70	97	89	0.2	9.1	0.6	3.3	1 ⊙	3	2	SW 1	NE 4	NE 1
17	82.4	84.0	84.6	83.7	14.4	15.2	12.6	13.7	18.6	11.6	97	93	94	95	0.6	1.2	0.9	0.9	10	10	0	W 6	W 5	W 2
18	84.7	84.1	84.3	84.4	13.8	21.8	15.1	16.4	22.1	9.6	86	56	85	76	2.2	11.5	2.6	5.4	0	6	2	C 0	WSW 6	SW 1
19	86.1	86.5	88.2	86.9	12.8	22.6	18.6	18.2	24.0	10.1	99	44	71	71	0.2	15.4	6.3	7.3	10	7	10 •	SW 1	NW 2	N 2
20	89.1	89.4	90.6	89.7	15.4	18.2	15.2	16.0	18.6	14.5	86	77	92	85	2.4	4.9	1.3	2.9	10 •	10	0	N 1	NE 3	NE 1
21	90.0	87.9	84.5	87.5	11.4	19.5	17.3	16.4	21.4	10.5	99	71	87	86	0.2	6.7	2.6	3.2	10 =	9	10	SW 1	ENE 2	E 1
22	80.1	79.4	81.8	80.4	15.3	16.5	12.5	14.2	19.4	12.0	96	86	92	91	0.8	2.8	1.2	1.6	8	10	10	SW 1	W 7	NW 5
23	84.0	85.5	85.8	85.1	10.7	16.0	10.0	11.7	17.4	9.1	91	63	91	82	1.2	6.8	1.1	3.0	9	8 ⊙	0	WNW 5	W 2	W 1
24	86.2	84.7	83.7	84.9	11.8	22.1	17.3	17.1	23.0	7.6	82	42	63	62	2.5	15.4	7.3	8.4	0 ⊙	1	2	C 0	S 6	S 1
25	90.2	90.6	87.8	89.5	12.8	19.8	15.2	15.8	20.8	12.0	93	50	84	76	1.1	11.5	2.8	5.1	8	1 ⊙	4	WNW 1	NNW 2	E 1
26	84.9	83.1	84.6	84.2	14.5	21.3	13.7	15.8	22.5	12.2	94	52	91	79	0.9	12.1	1.5	4.8	9	9	10	C 0	SW 1	W 3
27	87.7	88.1	87.9	87.9	11.6	19.0	11.7	13.5	19.5	8.6	81	51	91	74	2.6	10.9	1.1	4.9	0 ⊙	7	1	W 3	W 2	N 1
28	86.4	86.7	86.2	86.4	12.3	19.9	14.9	15.5	20.8	10.6	88	69	81	79	1.7	7.1	3.3	4.0	10	9	0	N 1	NNE 4	C 0
29	84.7	85.0	87.5	85.7	13.2	14.4	12.3	13.0	15.4	11.8	92	92	92	92	1.3	1.3	1.2	1.3	10	10	10	W 3	C 0	NW 7
30	89.3	90.7	91.9	90.6	10.9	15.5	10.7	12.0	16.4	10.1	86	66	87	80	1.8	6.0	1.7	3.2	7	6	0	WNW 7	WNW 6	NW 1
31	92.6	91.9	90.6	91.7	7.4	17.4	12.5	12.4	18.8	6.0	96	59	88	81	0.5	8.3	1.7	3.5	8	9	10	SW 1	W 2	C 0
M	87.1	86.8	86.7	86.8	14.4	21.0	16.0	16.8	22.3	11.9	92	65	87	81	1.4	9.3	2.5	4.4	6.0	6.3	3.9	1.9	3.5	1.4

Przemyśl $H_s = 238$ m $H_b = 238.9$ m $h_w = 20$ m **Liniec – Juillet 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU	USŁONECZNIENIE	POGODA
1	8	.	.	-	= 0⁰⁰–8⁴⁵ ⌒⁰ n – a
2	8	.	.	-	= 2⁴⁵–8⁴⁰ 20²³–24 ≤ 21⁵⁵–24 ⌒¹ n – a
3	8	0.0	.	-	• 9²⁰–45 = 0⁰⁰–11²⁰ ≤ 0⁰⁰–20
4	8	.	.	-	⌒⁰ n, a
5	8	7.2	.	-	(K) 20⁴⁵–22⁴⁰ NE–SW ≤ 22⁵⁰–23⁵⁰ (K)–24
6	7	.	.	-	▽ 2⁴⁵–4²⁵ (K) 0⁰⁰–2⁴⁰ K↘⁰–3⁴⁵ K↘²–3⁵⁵ K↘⁰–4⁵⁰ SW–NE = 5²⁵–9³⁰
7	8	.	.	-	
8	8	0.6	.	-	= 4⁴⁰–6⁰⁸ 6¹⁵–8⁵⁰
9	8	(0.0)	.	-	• ▽ 1¹⁰–2¹⁰ 6⁴⁸–7¹⁰ 7²⁰–8¹⁵ (K) 0⁵⁵–1¹⁰ K↘¹ 7¹⁰ 13⁰–2⁴⁰ (K)⁰ 16⁴⁰–17²⁰ ⌒ 10⁴–35 = 20⁴⁵–24
10	7	.	.	-	= 0⁰⁰–8⁴⁵ 21²⁵–24
11	6	3.7	.	-	▽ 9⁴²–45 10³⁰–11⁰⁵ •⁰ 11⁵⁵ 14⁰⁵ ▽ 17⁴⁵–50 20²⁷–50 K↘⁰ 20²⁶–50 (K) 21³⁰–22⁴⁰ = 0⁰⁰–4⁵⁰
12	7	2.0	.	-	• ⁰ 12⁴⁰–13¹⁰ ▽⁰ 17⁴⁵–53 18⁵⁰–20¹⁰ ▽¹ 21³⁰–22⁰⁵ ▽⁰–23¹⁵
13	8	.	.	-	= 0⁵⁰–3⁵⁰ ≡⁰–6⁴⁵ = –8⁴⁰
14	7	19.5	.	-	• ▽ 15¹⁵–17⁵⁵ 18⁰³–10 (K) 13⁵⁰–15¹⁵ K↘⁰–18¹⁵ = 4⁴⁰–7²⁵
15	7	2.4	.	-	▽ 17⁴⁵–18⁰⁵ 21⁰⁶–22⁰⁰ 22³⁴–23³⁵ = 0⁴⁰–6³⁵ ≡⁰–7³⁵ = –7⁵⁰ 18⁴⁵–24 (K) 16⁵⁰–18¹⁵
16	7	3.2	.	-	• ⁰ 7⁰⁹–20 8²⁵ 9¹⁰ ▽–11⁰⁵ 12⁴⁰–13⁴⁰ K↘⁰ 9²⁰–11¹⁰ S–N = 0⁰⁰–7³⁵ ≡⁰–8³⁰ = –10⁴⁰
17	8	1.7	.	-	▽⁰ 8¹⁷–23 8³³–45
18	7	0.6	.	-	▽ 2²⁰–3³⁵ 13⁵⁰–14¹⁵ = 4⁴⁰–8⁴⁵
19	7	.	.	-	= 0⁵⁰–4⁴⁰ 22¹⁶–24
20	7	6.7	.	-	(K) 22³⁵–24 = 0⁰⁰–9³⁵ ⌒⁰ n – a
21	6	7.8	.	-	▽ 2⁰⁸–5²⁵ 7²⁵–8¹⁰ •⁰–11⁰⁶ 12²⁵–40 ▽¹ 13²⁸–14⁵⁰ ▽⁰–15⁰⁰ 20¹⁰–45 (K) 0⁰⁰–1⁴⁵ = 4⁵⁰–7²⁰
22	8	5.1	.	-	• ⁰ 4²⁰–5¹⁰ ▽ 13¹⁵–14¹² 15²⁵–16¹⁰ 17⁵⁰–18⁴⁵ 22³⁴–23⁰⁰ •⁰–24 (K) 12³⁰–13¹⁵ K↘⁰–14¹⁵ (K)–14²⁵
23	7	0.4	.	-	• ⁰ 0⁰⁰–1¹⁵ 1³⁸–3⁴⁰ 4³⁰–5²⁰ 8¹⁰–12⁵⁰
24	7	6.7	.	-	▽⁰ 14¹⁰–37 ▽ 15⁵⁴–16⁴⁶ 19⁰⁶–20⁰⁹ ▽¹–21¹⁰ ▽⁰–22¹⁵ •⁰–23⁵⁰ = 23⁵⁰–24
25	6	6.6	.	-	▽ 17¹⁵–55 20³²–21¹² = 0⁰⁰–14⁴⁰ 22⁴⁰–24
26	7	0.1	.	-	▽ 4¹⁵–36 7⁴⁰–8¹⁰ = 0⁰⁰–8¹⁵
27	8	13.6	.	-	▽⁰ 0¹⁵–1¹⁰ •⁰ 19⁰⁴–10 21²⁰–45 •¹–21⁵⁵ •⁰–24
28	8	1.5	.	-	• ⁰ 0⁰⁰–3¹⁵ 6²⁰–45 7²⁵–50 8¹⁵–50 9¹²–11⁴⁰ 12⁵⁰–13²⁵ ▽ 15⁴⁰–16¹⁰
29	8	.	.	-	⌒ n – a
30	7	0.0	.	-	= 4²⁵–7²⁰ 21²⁰–24 ⌒² n – a
31	7	.	.	-	▽⁰ 3²⁰–4⁴⁰ = 0⁰⁰–3⁴⁵ 7¹⁵–8⁴⁰ 23⁵⁰–24
Σ	–	99.4	–	-	UWAGI

Sierpień – Août

1	7	.	.	-	= 0⁰⁰–15 19⁴⁵–24 ⌒ n – a, n – n
2	8	.	.	-	= 0⁰⁰–4⁵⁰ ≡¹–5²⁵ ≡²–6²⁰ ≡⁰–6⁴⁰ = –9⁴⁵ ⌒ n – a
3	8	.	.	-	⌒ na
4	8	2.2	.	-	⌒ n – a
5	5	9.1	.	-	▽ 1²⁵–3⁴⁵ 8⁴⁰–9⁰⁷ 9¹⁶–28 13²²–14⁰⁰ 18⁴³–52 19⁰⁰–04 K↘⁰ 1³⁰–5⁰ (K) 18¹⁴–40 K↘⁰–19¹⁴
6	8	.	.	-	⌒ na
7	8	5.2	.	-	≡² 4⁵⁰–6⁴⁵ = –7⁵⁰ ⌒² n, a
8	6	.	.	-	▽ 2⁴⁵–3¹⁰ 3⁵⁵–4¹⁵ 6²⁵–45 K↘⁰ 2⁴⁵–3¹⁰ (K)–5⁴⁵ SW–NE K↘⁰ 6²⁰–50 NW–SE (K)–7³⁵ = 8⁴⁰–np
9	7	.	.	-	
10	7	6.0	.	-	▽ 15¹⁰–25 16⁴⁰–18⁴⁵ = 2⁴⁰–10²⁵ ⌒ n – a
11	8	.	.	-	
12	8	.	.	-	(K)⁰ 20³⁵–21²⁰ W–E ⌒ na
13	7	.	.	-	= 3⁴⁵–8³⁰ ⌒⁰ n – a
14	8	1.0	.	-	= 0⁴⁰–10³⁶ ⌒¹ n – a
15	6	.	.	-	▽ 0¹⁵ na, (K) 0⁰⁰–15 K↘–2⁴⁰ (K)–5¹⁵ = 9²⁰–16⁴⁰ 19³⁵–24
16	6	0.0	.	-	▽ 17⁵⁰–18³⁰ (K) 17³⁵–50 K↘⁰–18⁵⁰ ≤ 20²⁵–24 = 0⁰⁰–4⁴⁰ ≡⁰–7³⁸ = –15⁵⁰ 17³⁰–24 ⌒² n – a
17	6	.	.	-	= 0⁰⁰–4⁴⁵ 10³⁵–14⁴⁰ ≤ 0⁰⁰–25
18	8	.	.	-	⌒ n – a
19	8	0.0	.	-	•⁰ 21²⁵–45 ⌒ n – a ⊕ 8⁴⁵–9⁴⁵
20	7	0.0	.	-	•⁵ 6³⁰–40 7²⁵ 9⁴⁰ = 2²⁰–4⁴⁵ 6³⁰–13¹⁵ 20³⁸–23⁴⁵ ≡⁰–24
21	6	0.4	.	-	•⁰ 21⁴⁰–22³⁸ ≡² 0⁰⁰–8³⁰ ≡¹–8⁴⁵ = –15⁴⁰ 19³⁰–24 ⌒ n – a
22	6	4.6	.	-	•⁰ 13⁴⁰–21²⁰ = 0⁰⁰–4⁴⁰ ≡¹–6⁴² = –15³⁰ ⌒⁰ n – a
23	7	.	.	-	≡ n – 10⁴⁴
24	8	0.8	.	-	= n – 8⁴⁰ ⌒ na
25	8	0.7	.	-	•⁰ 2²⁰–3³⁵
26	7	2.5	.	-	•⁰ 3³⁰–5³⁵ ▽ 16⁵⁰ 17²⁰, 18³⁰–19⁵⁵ •⁰ 21⁵⁷–22²⁵ = 5³⁵–7⁴⁰
27	8	0.0	.	-	= 19²⁵–24 ⌒ na
28	7	0.0	.	-	▽ 6⁰³–16 •⁰ 9³⁵ 10¹⁰ = 0⁰⁰–5⁴⁰ 7²⁰–9⁵⁵
29	6	11.5	.	-	•² 9¹²–20 9⁵⁰–11²² 11⁴⁵–12⁰¹ 17³⁸–18²⁰ •¹–19¹⁸ •⁰ 19²⁸–20²⁵ 23⁵⁵–24 = 0⁴⁵–19³²
30	7	.	.	-	•⁰ 0⁰⁰ 2⁰⁰ = 2⁰⁰–4⁴⁰ 23¹⁰–24
31	7	1.4	.	-	▽ 15⁰⁰–04 •⁰ 18⁰¹ 19³⁵ 22⁵⁰ 24 = 0⁰⁰–11³⁰ 18¹⁵–20⁴⁰ ⌒² n – a
Σ	–	45.4	–	-	UWAGI

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ **Wrzesień – Septembre 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.1	90.5	92.0	91.2	12.4	18.2	11.3	13.3	18.5	10.2	89	53	90	77	1.6	9.9	1.3	4.3	5	6 ⊙	0	WSW 1	W 4	SW 1
2	92.5	91.5	90.4	91.5	7.5	20.9	15.0	14.6	22.1	5.1	99	48	80	76	0.2	12.7	3.4	5.4	7	4	0	SW 1	SW 3	SW 1
3	87.4	87.4	87.7	87.5	7.6	18.7	15.3	14.2	20.3	5.8	100	68	92	87	0.0	6.9	1.3	2.7	3 ⊙ ≡	9 (R)	10 •	SW 1	NW 3	NW 1
4	87.4	88.1	91.0	88.8	13.8	17.0	13.8	14.6	17.4	13.1	91	79	89	86	1.5	4.1	1.8	2.5	10	10	10	ANE 1	N 5	N 7
5	92.7	92.7	91.9	92.4	12.0	16.2	14.6	14.4	16.8	11.4	94	81	92	89	0.8	3.4	1.3	1.8	10	9	9	N 3	N 1	NE 1
6	90.3	90.7	90.1	90.2	13.3	18.3	14.0	14.9	19.6	10.5	99	78	93	90	0.2	4.6	1.1	2.0	10 ≡	8	2	W 1	W 2	C 0
7	92.2	93.1	93.8	93.0	10.7	21.7	15.4	15.8	21.7	8.9	99	59	88	82	0.2	10.6	2.1	4.3	0 ⊙ ≡	3 ⊙	0	W 3	E 2	C 0
8	94.3	95.1	95.3	94.9	9.8	26.2	16.8	17.4	26.5	8.4	100	47	88	78	0.0	18.0	2.3	6.8	10 ≡	2 ⊙	0	C 0	SE 1	SE 1
9	95.6	94.8	93.3	94.6	15.2	27.2	18.1	19.6	27.5	12.5	90	51	82	74	1.7	17.5	3.7	7.6	0 ⊙	3 ⊙	0	C 0	SW 4	C 0
10	92.7	91.7	90.4	91.6	14.8	17.6	16.0	16.1	18.6	10.9	97	89	94	93	0.5	2.2	1.2	1.3	10	10	10	SW 1	W 1	NW 3
11	88.3	85.5	80.6	84.8	14.0	18.3	14.9	15.5	19.4	13.2	93	69	92	85	1.1	6.6	1.3	3.0	10	8	1	N 1	SW 1	NE 1
12	75.3	74.3	80.1	76.6	17.7	22.4	12.2	16.1	22.6	11.8	75	58	94	76	5.1	11.4	0.9	5.8	10	8	10 •	SW 3	SSW 7	W 1
13	82.9	83.2	81.8	82.6	9.7	19.2	13.1	13.8	19.4	7.1	91	57	77	75	1.1	9.6	3.5	4.7	7	7	10 •	W 1	SW 5	SW 2
14	81.5	81.8	81.1	81.5	11.8	18.8	14.2	14.8	19.7	9.8	85	51	75	70	2.0	10.6	4.1	5.6	3	4 ⊙	10	W 4	SW 3	C 0
15	74.9	82.3	86.5	81.2	12.6	13.7	9.5	11.3	15.1	9.0	96	63	86	82	0.5	5.9	1.7	2.7	8	5	2	WNW 1	W 8	SW 2
16	89.6	89.7	88.9	89.4	7.6	14.4	9.5	10.2	16.5	5.5	94	63	93	83	0.6	6.1	0.8	2.5	8 ⊙	8	8	SW 1	NE 1	C 0
17	88.9	88.3	86.1	87.8	7.5	12.6	9.2	9.6	12.6	7.1	94	63	91	83	0.6	5.4	1.1	2.4	7	7	10	WNW 3	WNW 5	W 4
18	82.9	83.9	83.7	83.5	9.6	11.9	11.0	10.9	12.8	8.6	87	73	74	78	1.6	3.8	3.4	2.9	8	7	10 •	W 4	W 7	W 4
19	84.0	83.4	81.8	83.1	10.0	16.1	12.7	12.9	17.0	7.8	78	51	80	70	2.7	8.9	2.9	4.8	5	4 ⊙	10 •	W 3	SW 7	SW 6
20	80.3	82.9	86.7	83.3	13.2	10.3	9.4	10.6	13.3	8.6	87	94	99	93	2.0	0.8	0.2	1.0	10	10 •	2	W 1	W 3	W 1
21	88.8	88.8	88.9	88.8	5.1	14.3	9.6	9.6	14.5	4.4	100	61	97	86	0.0	6.3	0.4	2.2	10 ≡	8	6	SW 2	W 2	C 0
22	87.5	85.5	85.2	86.1	5.8	19.5	17.4	15.0	20.9	4.0	100	70	84	85	0.0	6.9	3.2	3.4	4 ≡	10	0	C 0	SW 5	SW 3
23	83.4	79.7	74.0	79.0	14.4	23.2	18.9	18.8	23.4	12.4	92	59	74	75	1.3	11.7	5.5	6.2	6	8	9	SW 1	SW 8	SW 7
24	77.9	79.6	79.4	79.0	14.0	17.2	11.8	13.7	19.2	11.2	90	72	89	84	1.6	5.4	1.5	2.8	9	7	10 •	W 6	W 7	NW 8
25	85.3	87.2	89.8	87.4	6.4	10.5	5.1	6.8	11.8	4.5	79	61	83	74	2.0	5.0	1.5	2.8	2	5 ⊙	1	WNW 6	W 8	C 0
26	89.1	87.9	88.8	88.6	3.6	11.3	6.3	6.9	11.3	1.6	86	62	88	79	1.1	5.1	1.1	2.4	5	9	6	NW 2	W 3	NW 1
27	89.8	89.3	84.9	88.0	2.1	10.2	5.4	5.8	10.6	0.8	98	65	81	81	0.1	4.3	1.7	2.0	0 ⊙	8	9	W 1	W 3	C 0
28	77.8	78.7	79.2	78.6	8.0	11.4	8.9	9.3	11.9	4.6	85	75	86	82	1.5	3.5	1.5	2.2	9	9	10	W 6	W 8	W 6
29	80.0	78.1	74.5	77.5	8.6	13.0	10.4	10.6	13.3	7.0	89	74	96	86	1.3	4.0	0.5	1.9	6	9 •	10 •	W 2	SW 6	SW 1
30	75.4	79.7	84.8	80.0	7.3	9.4	5.6	7.0	11.9	5.2	97	66	85	83	0.3	4.0	1.4	1.9	10 •	9	1	W 3	WNW 6	W 2
31																								
M	86.0	86.2	86.1	86.1	10.2	16.7	12.2	12.8	17.5	8.0	92	65	87	81	1.1	7.2	1.9	3.4	6.7	7.1	5.9	2.1	4.3	2.1

Październik – Octobre

1	88.7	89.3	89.7	89.2	4.6	8.2	4.4	5.4	9.2	2.7	97	78	97	91	0.3	2.4	0.3	1.0	8	10	3	W 1	N 1	C 0
2	93.6	95.6	96.1	95.1	3.8	7.8	2.2	4.0	8.9	1.8	97	67	96	87	0.3	3.5	0.3	1.4	9	7	0	W 3	NW 4	C 0
3	92.9	90.0	87.4	90.1	-2.0	10.7	6.0	5.2	12.8	-3.2	98	64	74	79	0.1	4.6	2.4	2.4	10 ≡	2	1	C 0	NE 2	C 0
4	85.2	87.2	90.6	87.7	7.5	5.0	3.6	4.9	8.1	2.9	76	92	86	85	2.5	0.7	1.1	1.4	10	10 •	1	WSW 3	W 5	W 1
5	95.7	96.3	95.3	95.8	2.4	9.8	4.8	5.4	11.0	0.8	89	59	78	75	0.8	4.9	1.9	2.5	0	8	0	W 2	W 5	C 0
6	93.7	94.0	97.1	94.9	6.2	14.0	9.3	9.7	14.5	0.8	70	51	87	69	2.8	7.9	1.6	4.1	8	2	10	WSW 3	W 4	W 1
7	97.3	96.6	96.5	96.8	6.0	15.1	9.3	9.9	15.8	5.3	92	59	85	79	0.8	7.0	1.7	3.2	0	3 ⊙	9	W 1	W 7	NW 3
8	98.5	100.9	101.9	100.4	10.2	12.8	6.2	8.8	13.4	5.5	95	72	97	88	0.6	4.1	0.3	1.7	1	9	0	NW 3	NE 3	C 0
9	100.9	100.2	97.8	99.6	0.2	14.5	6.8	7.1	15.5	-0.9	100	53	82	78	0.0	7.8	1.8	3.2	0 ≡	0 ⊙	0	C 0	ENE 4	C 0
10	97.1	96.5	96.2	96.6	1.6	19.6	8.3	9.4	20.0	-0.7	98	58	96	84	0.2	9.6	0.5	3.4	0 ⊙	0	0	C 0	SSW 1	SW 1
11	96.1	95.3	94.5	95.3	2.4	20.2	8.7	10.0	20.7	1.0	98	44	84	75	0.2	13.2	1.8	5.1	0 ⊙	0 ⊙	0	C 0	SW 4	SW 2
12	94.1	93.6	95.8	94.5	8.5	19.0	12.2	13.0	19.0	5.0	85	56	82	74	1.7	9.8	2.5	4.7	0 ⊙	0 ⊙	3	C 0	WSW 5	WSW 1
13	99.8	99.8	98.1	99.2	11.4	15.3	9.1	11.2	15.5	8.6	89	71	96	85	1.5	5.1	0.5	2.4	9	9	0	N 2	NE 2	C 0
14	96.4	95.4	95.8	95.9	4.1	17.7	13.1	12.0	19.1	3.4	100	60	88	83	0.0	8.1	1.8	3.3	0 ≡	4 ⊙	10	W 2	WSW 3	NW 1
15	99.2	99.5	100.0	99.6	8.2	10.4	7.5	8.4	13.9	6.9	94	77	90	87	0.6	2.9	1.1	1.5	10	10	9	NW 1	NNW 4	C 0
16	99.7	98.0	96.0	97.9	5.7	12.2	5.6	7.3	13.1	4.8	95	67	95	86	0.5	4.6	0.4	1.8	9	0 ⊙	0	C 0	ENE 1	C 0
17	93.8	92.6	93.1	93.2	4.5	18.8	13.0	12.3	19.0	1.4	98	54	77	76	0.1	10.1	3.5	4.6	0 ⊙	0 ⊙	0	SW 2	SW 7	WSW 4
18	91.0	89.8	88.3	89.7	13.4	17.8	15.8	15.7	18.4	9.1	77	62	57	65	3.5	7.8	7.6	6.3	10	9	3	W 2	WSW 6	WSW 3
19	87.3	86.0	83.9	85.7	14.1	22.0	14.0	16.0	22.3	12.7	56	36	58	50	7.1	17.0	6.7	10.3	8 ⊙	3	0	WSW 4	SW 7	C 0
20	81.6	82.5	86.4	83.5	13.2	18.7	9.8	12.9	20.5	9.4	68	59	97	75	4.8	8.8	0.3	4.6	1 ⊙	7	10	SSW 1	W 5	NW 2
21	89.2	89.1	88.0	88.8	7.2	9.2	7.7	8.0	9.8	6.7	99	85	90	91	0.2	1.7	1.0	1.0	10 •	9	10	NNW 1	NE 1	NE 6
22	82.5	79.9	77.7	80.0	6.7	9.0	8.5	8.2	9.4	6.0	99	96	99	98	0.1	0.5	0.2	0.3	10	10	10 •	SSE 1	SSE 2	SE 1
23	77.0	79.5	85.7	80.7	7.9	10.0	9.1	9.0	10.2	7.4	100	97	95	97	0.0	0.3	0.7	0.3	10 •	10 •	10 •	ENE 1	SE 1	WNW 4
24	88.8	88.9	92.3	90.0	5.2	13.1	10.2	9.7	13.4	4.2	100	65	80	82	0.0	5.3	2.5	2.6	6	4 ⊙	10	C 0	WSW 3	W 4
25	96.3	97.8	98.3	97.5	8.2	10.0	1.4	5.2	10.2	0.8	97	74	98	90	0.3	3.2	0.2	1.2	9	9	0	NW 2	WNW 2	C 0
26	97.2	96.7	96.1	96.7	-0.8	12.6	5.3	5.6	12.8	-2.0	100	70	100	90	0.0	4.4	0.1	1.5	5 ≡	0	0	W 1	SW 1	C 0
27	94.0	92.7	92.5	93.1	2.4	16.8	7.1	8.4	17.4	0.0	100	59	97	85	0.0	7.9	0.3	2.7	0 ⊙	0 ⊙	0	C 0	SW 4	C 0
28	92.8	93.1	93.1	93.0	1.7	12.0	10.0	8.4	13.0	-0.5	100	84	92	92	0.0	2.2	1.0	1.1	10	9	8	WSW 1	C 0	C 0
29	93.3	92.5	92.9	92.9	2.2	13.3	7.5	7.6	13.6	1.3	100	75	93	89	0.0	3.8	0.8	1.5	2 ≡	1	0	WSW 3	ENE 3	C 0
30	91.2	89.9	89.2	90.1	0.6	14.8	7.6	7.6	16.4	0.1	100	64	87	84	0.0	6.0	1.3	2.4	1 ≡	1	4	WNW 2	SSE 2	SW 1
31	89.1	87.7	86.4	87.7	4.6	17.1	8.6	9.7	17.6	3.1	92	48	89	76	0.7	10.2	1.3	4.1	8	2 ⊙	0	SW 1	W 2	W 1
M	92.7	92.5	92.7	92.6	5.5	13.8	8.2	8.9	14.7	3.4	92	66	88	82	1.0	6.0	1.5	2.8	5.3	4.8	3.6	1.4	3.3	1.2

Przemyśl $H_s = 238$ m $H_b = 238{,}9$ m $h_w = 20$ m **Wrzesień – Septembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKR.	USŁONECZNIENIE	POGODA
1	8	0.3	.	-	$\bullet^0 0^{00}-50$ $1^{50}-4^{35}$ $\bullet$ $16^{03}-10$ $17^{22}-18^{14}$ $=5^{50}-9^{40}$ $\frown^1 6^{08}-15$
2	7	.	.	-	$=^0 3^{50}-7^{10}$ $=-10^{40}$ $20^{35}-24$ $\frown^2$ na
3	7	13.9	.	-	$\bullet$ $12^{50}-13^{02}$ $16^{13}-19^{30}$ $20^{50}-22^{45}$ (R) $13^{05}-45$ R ^{0} $17^{10}-19^{40}$ $21^{40}-22^{50}$ $=0^{00}-5^{45}\equiv^1-6^{54}\equiv^2-7^{40}\equiv^0-8^{40}$
4	7	0.0	.	-	$=2^{00}-4^{20}$ $8^{20}-11^{25}$ $18^{18}-21^{40}$ [3.IX: $=-11^{30}$ $\frown^2$ n – a
5	7	.	.	-	$\bullet^0 5^{50}-6^{40}$ $\bullet^0-7^{20}$ $=7^{20}-8^{40}$ $12^{40}-23^{50}\equiv^1-24$
6	6	.	.	-	$=^1 0^{00}-8^{50}$ $=-15^{15}$ $18^{30}-24$ $\frown$ n – a
7	7	.	.	-	$=0^{00}-50\equiv^1-9^{18}=-12^{38}$ $19^{18}-24$ $\frown^2$ na
8	7	.	.	-	$=0^{00}-4^{50}\equiv^0-5^{40}\equiv^1-6^{10}\equiv^2-8^{20}\equiv^0-8^{30}=-12^{30}$
9	8	.	.	-	$=1^{40}-9^{15}$ $\frown^2$ n – a
10	5	0.0	.	-	$\bullet^0 18^{40}-19^{05}$ $\bullet^0-20^{08}$ $=0^{00}-5^{45}\equiv^1-5^{55}\equiv^2-6^{20}\equiv^1-6^{35}=-24$ $\frown^2$ na
11	7	0.0	.	-	$\bullet$ $1^{40}-3^{10}$ $=0^{00}-9^{40}$ $22^{40}-24$
12	7	12.6	.	-	$\bullet^0 1^{40}$ 2^{00} $7^{46}-8^{09}$ $\bullet$ $16^{25}-43$ $17^{53}-23^{35}$ $=0^{00}-5^{20}$
13	8	3.5	.	-	$\bullet^0 20^{55}-22^{05}$ $\bullet^1-23^{45}$ $\bullet^0-24$
14	8	1.4	.	-	$\bullet^0 0^{00}-3^{25}$ $22^{05}-24$
15	8	.	.	-	$\bullet^0 0^{00}-45$ 4^{50} 6^{50} $=2^{00}-7^{50}$
16	8	12.2	.	-	$\bullet^1 23^{30}-24$ $=0^{50}-2^{45}$ $7^{20}-9^{40}$ $18^{35}-22^{30}$ $\frown^0$ n – a
17	6	.	.	-	$\bullet^1 0^{00}-1^{10}$ $\bullet^0-1^{50}$ $\bullet^1-3^{40}$ $\bullet^0-5^{35}=5^{35}-13^{40}$ $18^{40}-19^{30}$
18	7	0.0	.	-	$\bullet$ $8^{40}-50$ $9^{25}-45$ $17^{35}-45$ $\bullet^0 21^{25}-22^{10}$ $=7^{40}-8^{10}$
19	8	0.0	.	-	$\bullet^0 21^{30}-22^{10}$ $23^{55}-24$
20	6	5.1	.	-	$\bullet^0 0^{00}-15$ $8^{20}-10^{20}$ $11^{05}-50$ $\bullet^1-12^{15}$ $\bullet^0-12^{45}$ $13^{10}-15$ $\bullet^1-14^{50}$ $=21^{20}-24$
21	7	.	.	-	$=0^{00}-7^{50}\equiv^2-10^{25}=-11^{50}$ $18^{30}-24$ $\frown^2$ n – a
22	7	0.0	.	-	$\bullet^0 15^{50}$ 16^{12} $=0^{00}-1^{50}\equiv^0-3^{25}\equiv^1-4^{20}\equiv^2-6^{45}\equiv^0-8^{15}=-12^{10}$ $22^{20}-24$ $\frown^2$ n – a
23	7	6.9	.	-	$\bullet^0 17^{05}-18^{15}$ $\bullet^0 22^{40}-23^{10}$ $\bullet^0-23^{48}$ $\swarrow$ $18^{40}-20^{10}$ $=0^{00}-9^{35}$
24	8	6.0	.	-	$\bullet$ $2^{00}-40$ $8^{01}-05$ $\bullet^0$ $17^{50}-24$ $\lll$ $22^{30}-23^{40}$
25	8	.	.	-	$\bullet^0 0^{00}-1^{20}$
26	7	.	.	-	$=6^{15}-9^{25}$ $14^{20}-24$
27	8	1.1	.	-	$=0^{00}-9^{15}$ $\frown^2$ n – a
28	7	3.6	.	-	$\bullet^0 4^{45}-6^{10}$ $\bullet$ 8^{15-24} $9^{55}-10^{15}$ $10^{45}-11^{16}$ $13^{04}-12$ $13^{35}-14^{06}$ $15^{35}-16^{10}$ $17^{30}-44$
29	7	4.2	.	-	$\bullet$ $0^{15}-1^{10}$ $7^{30}-8^{02}$ $\bullet^0$ 11^{15} 13^{05} 14^{30} $17^{10}-21^{25}$ $=21^{15}-24$
30	8	0.0	.	-	$\bullet$ $3^{50}-4^{00}$ $\bullet^0-9^{20}$ $=0^{00}-2^{30}$
31					
Σ	–	70.8	–	-	UWAGI:

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1	8	.	.	-	$=16^{40}-24$
2	7	.	.	-	$=0^{00}-4^{50}$ $5^{40}-24$
3	7	.	.	-	$=0^{00-40}\equiv^1-5^{40}\equiv^2-9^{30}\equiv^1-9^{50}\equiv^0-10^{35}=-11^{30}$ $\smile^1$ n – a
4	6	1.3	.	-	$\bullet^0 8^{35}-9^{26}$ 9^{35} 11^{25} $\bullet^1-11^{28}$ $\bullet^0-13^{10}$ $=8^{35}-14^{20}$ $18^{15}-19^{40}$
5	8	.	.	-	$=1^{50}-7^{30}$ $17^{10}-24$ $\smile^0$ n – a
6	8	0.0	.	-	$\bullet^0 18^{40}$ 19^{05} $=0^{00}-4^{15}$
7	7	0.0	.	-	$=0^{40}-7^{40}$ $16^{40}-20^{20}$ $\frown$ n – a
8	8	.	.	-	$\bullet$ $1^{40}-4^{05}$ $=1^{00}-8^{48}$ $16^{34}-24$
9	8	.	.	-	$=0^{00}-4^{50}\equiv^0-5^{40}\equiv^2-7^{45}\equiv^0-8^{35}=-10^{10}$ $20^{15}-24$ $\smile^0$ n – a
10	7	.	.	-	$=0^{00}-6^{55}\equiv^0-7^{50}=-12^{20}$ $16^{45}-24$ $\smile$ n – a
11	8	.	.	-	$=0^{00}-10^{40}$ $\smile^0$ n – a
12	8	.	.	-	$=6^{20}-9^{30}$ $16^{35}-20^{05}$ $\frown$ na
13	7	.	.	-	$=1^{00}-11^{45}$ $16^{30}-23^{50}\equiv^0-24$
14	7	.	.	-	$=^0 0^{00}-1^{45}\equiv^1-2^{30}\equiv^0-8^{55}=-10^{40}$ $15^{35}-24$
15	6	.	.	-	$=0^{00}-24$
16	7	.	.	-	$=0^{00}-12^{20}$ $16^{05}-24$ $\frown$ na
17	7	.	.	-	$=0^{00}-10^{45}$ $\frown^2$ n – a
18	7	0.0	.	-	$\bullet^0 8^{10-20}$ $=5^{40}-8^{20}$
19	8	.	.	-	$=6^{15}-7^{10}$
20	8	8.0	.	-	$\bullet^0 19^{40}-24$ $=7^{10}-8^{40}$ $16^{20}-19^{20}$
21	8	.	.	-	$\bullet^0 0^{00}-7^{20}$
22	6	3.3	.	-	$\bullet^0 7^{25}$ $8^{15}-10^{15}$ 16^{25} $17^{10}-22^{35}$ $23^{40}-24$ $=7^{10}-24$
23	5	2.9	.	-	$\bullet^0 0^{00-25}$ $1^{35}-2^{16}$ $4^{20}-6^{40}$ $\bullet^0 11^{40}-13^{25}$ $\bullet^0-19^{35}$ $\bullet^0 20^{10}-21^{30}$ $=0^{00}-24$
24	7	0.1	.	-	$=0^{00}-12^{16}$ $16^{18}-17^{40}$ $22^{20}-24$
25	7	.	.	-	$\bullet^0 0^{45}-2^{40}$ $=0^{00}-9^{40}$ $16^{45}-23^{45}\equiv^0-24$
26	6	.	.	-	$\equiv^0 0^{00}-7^{50}=-22^{45}\equiv^2-24$ $\smile^2$ na
27	8	.	.	-	$\equiv^2 0^{00}-1^{10}\equiv^1-4^{48}=-11^{35}$ $23^{30}-24$ $\smile^0$ n – a
28	6	.	.	-	$=0^{00}-24$ $\frown^2$ na
29	6	.	.	-	$=0^{00}-2^{50}\equiv^0-3^{20}\equiv^1-6^{40}\equiv^0-7^{30}\equiv^1-8^{45}\equiv^0-9^{10}=-24$ $\frown^2$ n – a
30	6	.	.	-	$=0^{00}-1^{50}\equiv^1-7^{45}\equiv^0-9^{15}=-13^{40}$ $15^{25}-19^{45}$ $21^{20}-24$
31	7	.	.	-	$=5^{20}-7^{40}$
Σ	–	15.6	–	-	UWAGI:

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ **Listopad – Novembre 1957**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	83.4	81.4	82.1	82.3	5.8	18.7	10.1	11.2	19.0	5.0	97	61	92	83	0.3	8.4	1.0	3.2	2	1 ⊙	0	C 0	SW 6	SW 2
2	84.5	85.0	86.2	85.2	8.1	14.7	9.0	10.2	15.4	6.8	96	78	99	91	0.5	3.6	0.2	1.4	10	1	0	SW 1	ESE 1	SW 1
3	87.1	88.0	88.2	87.8	7.0	12.9	8.2	9.1	13.0	4.5	100	88	100	96	0.0	1.8	0.0	0.6	9	6	2	C 0	NE 1	C 0
4	87.8	87.8	88.8	88.1	8.0	19.1	11.5	12.5	19.1	6.9	100	60	90	83	0.0	8.9	1.4	3.4	9	5 ⊙	2	NE 1	SE 3	SE 2
5	88.7	87.7	87.0	87.8	5.4	16.0	8.8	9.8	16.0	4.8	100	79	95	91	0.0	3.8	0.6	1.5	0	1 ⊙	0	SE 1	SE 3	NW 1
6	87.6	87.4	87.0	87.3	6.8	17.3	8.9	10.5	17.4	5.4	97	61	94	84	0.3	7.6	0.6	2.8	8	2	0	C 0	SSE 5	E 2
7	85.5	84.2	84.5	84.7	4.0	11.0	7.0	7.2	11.3	3.4	100	87	97	95	0.0	1.6	0.3	0.6	2 ⊙	9	4	C 0	ESE 9	E 2
8	84.3	84.1	81.9	83.4	5.0	7.6	5.4	5.8	8.5	3.6	100	96	100	99	0.0	0.4	0.0	0.1	10 ≡	10	0	SE 3	SE 2	C 0
9	80.4	79.9	81.1	80.5	4.4	7.4	8.0	7.0	9.4	0.9	100	99	94	98	0.0	0.2	0.6	0.3	10 ≡	10	9	SE 1	ESE 1	SW 2
10	82.7	83.7	84.4	83.6	5.9	12.5	8.6	8.9	13.7	4.9	97	79	94	90	0.3	3.1	0.6	1.3	9	4	9	C 0	SSW 1	E 3
11	84.5	84.4	85.6	84.8	9.0	7.8	7.0	7.7	8.9	6.0	88	87	93	89	1.4	1.4	0.7	1.2	10	10	10	E 5	ENE 9	E 7
12	88.9	92.3	95.0	92.1	3.7	3.4	3.2	3.4	7.0	2.5	92	91	95	93	0.7	0.7	0.4	0.6	10 •	10	10 •	ENE 8	ENE 8	ENE 4
13	97.5	98.6	100.1	98.7	1.0	0.2	-1.0	-0.2	3.2	-1.5	87	82	91	87	0.9	1.1	0.5	0.8	10	10	10	NE 4	NE 5	NE 4
14	99.9	101.4	104.0	101.8	-3.0	-2.5	-3.1	-2.9	-1.0	-4.3	90	82	81	84	0.5	0.9	0.9	0.8	10	10	10	C 0	SW 2	N 1
15	104.3	103.5	102.5	103.4	-2.0	1.6	-2.4	-1.3	2.7	-3.9	89	71	96	85	0.6	2.1	0.2	1.0	10	1 ⊙	0	ENE 3	ESE 3	C 0
16	101.4	101.3	102.4	101.7	-5.3	5.9	1.6	1.0	5.9	-6.0	95	70	89	85	0.2	2.8	0.8	1.3	1	1 ⊙	10	C 0	W 3	C 0
17	102.6	102.7	103.8	103.0	0.8	0.8	0.6	0.7	1.9	0.1	96	98	90	95	0.3	0.2	0.6	0.4	8	10 •	10	C 0	ENE 3	ENE 3
18	104.2	104.2	103.4	103.9	0.4	1.7	0.6	0.8	1.8	-1.0	83	62	81	75	1.1	2.6	1.3	1.7	10	10	10	ENE 5	E 5	SE 1
19	102.7	104.3	107.4	104.8	0.2	1.5	0.3	0.6	1.7	-0.4	84	69	80	78	1.0	2.1	1.2	1.4	10	10	10	NE 1	E 2	ENE 3
20	109.9	110.7	110.8	110.5	-1.0	3.6	-1.4	0.0	3.6	-2.0	85	54	90	76	0.9	3.7	0.5	1.7	4	2 ⊙	0	ENE 5	E 5	E 1
21	109.8	108.1	104.6	107.5	-5.5	3.8	-2.7	-1.8	3.8	-6.5	90	64	91	82	0.4	2.9	0.5	1.3	0	0	0	C 0	C 0	C 0
22	99.1	95.5	92.1	95.6	-6.9	2.9	-4.3	-3.2	3.6	-7.8	88	59	89	79	0.4	3.1	0.5	1.3	0	0	0	C 0	E 1	C 0
23	91.7	90.8	91.1	91.2	-5.8	1.6	2.7	0.3	2.7	-7.8	92	72	70	78	0.3	1.9	2.2	1.5	0	6	0	C 0	ENE 1	WSW 3
24	92.2	93.3	92.6	92.7	2.6	3.6	3.6	3.4	3.8	1.7	81	70	67	73	1.5	2.4	2.6	2.2	10	9	10	W 6	W 6	W 8
25	91.5	91.3	91.9	91.6	3.0	4.4	3.1	3.4	4.4	1.8	86	80	86	84	1.1	1.6	1.0	1.2	10 •	10	10	W 4	W 7	W 5
26	93.1	93.8	93.4	93.4	3.6	5.2	5.0	4.7	5.2	2.3	93	87	89	90	0.5	1.1	1.0	0.9	10	10	10	W 5	W 7	W 6
27	89.1	86.8	87.4	87.8	4.2	5.5	6.8	5.8	6.8	3.5	90	86	82	86	0.8	1.2	1.8	1.3	10	10	10 •	W 7	W 7	W 7
28	88.4	85.2	81.0	84.9	5.1	6.4	6.6	6.2	7.4	4.4	84	94	88	89	1.4	0.6	1.1	1.0	10 •	10 •	10	W 3	W 5	W 5
29	73.8	75.2	84.9	78.0	5.6	1.5	-8.1	-2.3	7.0	-8.7	78	72	69	73	2.0	1.9	1.0	1.6	9	9 ✳	10 ✳	W 10	NW 10	NNW 7
30	90.2	91.4	92.2	91.3	-8.7	-8.0	-7.7	-8.0	-7.7	-10.0	68	75	73	72	1.0	0.8	0.9	0.9	10 ✳	10 ✳	10 ✳	NW 7	NNW 9	NW 8
31																								
M	92.2	92.1	92.6	92.3	2.0	6.3	3.2	3.7	7.2	0.3	91	77	88	85	0.6	2.5	0.8	1.3	7.4	6.6	5.9	2.7	4.3	2.9

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1	94.0	94.8	95.4	94.7	-9.6	-6.4	-4.3	-6.2	-4.3	-10.2	75	70	77	74	0.7	1.1	1.0	0.9	2	1 ⊙	0	NW 8	NW 8	NW 8
2	94.8	93.6	93.5	94.0	-5.7	-4.7	-7.9	-6.6	-3.7	-8.5	87	69	75	77	0.5	1.3	0.8	0.9	1	5	10 ✳	N 4	N 4	NE 7
3	89.3	86.8	90.4	89.5	-7.6	-6.8	-5.0	-6.1	-4.6	-8.9	70	85	88	81	1.0	0.5	0.5	0.7	10	10 ✳	10	NW 7	NNW 4	C 0
4	92.6	94.1	93.5	93.4	-4.9	-3.3	-2.2	-3.2	-2.2	-5.9	93	79	89	87	0.3	1.0	0.6	0.6	10 ✳	10	10	C 0	W 1	W 1
5	90.7	87.7	88.2	88.9	-0.6	0.8	2.8	1.4	2.8	-2.8	99	92	84	92	0.0	0.5	1.2	0.6	10	10	10	W 2	W 3	WNW 7
6	89.9	93.4	95.5	92.9	1.8	1.1	-0.1	0.7	2.8	-0.6	93	94	88	92	0.6	0.4	0.8	0.6	10	10 ✳	10	NW 5	N 5	N 2
7	92.0	87.8	82.6	87.5	-3.0	1.2	-0.5	-0.7	2.6	-4.1	95	85	72	84	0.3	1.1	1.7	1.0	6	0 ⊙	0	C 0	C 0	SW 4
8	73.2	67.4	58.5	66.4	-0.9	1.6	2.0	1.2	2.0	-2.1	71	71	75	72	1.6	2.1	1.8	1.8	9	9	10 △	SW 9	SW 5	SW 7
9	55.6	56.0	68.8	60.1	4.5	6.2	2.2	3.8	8.0	1.3	76	64	64	68	2.0	3.4	2.6	2.7	8	9	6	W 5	SW 7	W 5
10	72.1	69.0	73.4	71.5	-0.7	1.5	1.2	0.8	2.2	-1.4	81	78	77	79	1.1	1.5	1.6	1.4	9	10 ✳	8	C 0	ENE 1	W 6
11	83.9	83.1	78.8	81.9	-7.1	0.0	0.5	-1.5	1.4	-7.6	71	52	61	61	1.0	2.9	2.4	2.1	1	9	0	SW 1	C 0	C 0
12	74.3	73.3	73.2	73.6	4.5	8.3	6.0	6.2	8.3	-1.0	74	63	79	72	2.2	4.0	2.0	2.7	9	9	0	S 4	S 2	C 0
13	71.9	70.3	62.4	68.2	6.6	10.6	6.0	7.3	11.6	3.4	82	73	83	79	1.7	3.5	1.6	2.3	1	10	10	C 0	S 1	S 2
14	54.0	59.1	69.7	60.9	10.8	9.4	5.4	7.8	11.2	4.6	79	79	87	82	2.8	2.5	1.2	2.2	9	9 •	10	SW 7	SSW 8	NW 4
15	78.5	85.2	93.1	85.6	2.2	-1.8	-5.7	-2.8	5.4	-6.0	86	90	77	84	1.1	0.5	0.9	0.8	10	10 △	10	NW 4	N 6	NE 6
16	97.4	98.0	98.8	98.1	-8.5	-4.9	-6.4	-6.6	-4.7	-9.3	83	73	70	75	0.5	1.1	1.1	0.9	3	4 ⊙	7	NE 7	E 6	E 7
17	94.9	93.4	92.1	93.5	-4.0	-1.9	-2.0	-2.5	-1.5	-7.3	77	75	81	78	1.0	1.3	1.0	1.1	10	10	10	E 1	E 3	E 2
18	91.7	92.3	94.8	92.9	-2.2	-1.7	-4.3	-3.1	-1.7	-5.0	87	88	91	89	0.7	0.7	0.4	0.6	10	10 △	10	E 1	NNE 3	NNW 3
19	97.1	99.0	102.8	99.6	-4.2	-3.2	-3.0	-3.4	-2.9	-4.9	87	86	90	88	0.6	0.7	0.5	0.6	10	10 △	10	NNW 1	C 0	C 0
20	105.4	106.0	106.4	105.9	-2.7	1.9	1.9	0.8	2.1	-3.9	89	66	73	76	0.6	2.4	1.9	1.6	10	9	10	C 0	W 1	W 3
21	104.1	103.0	102.5	103.2	-0.2	2.0	-1.1	-0.1	2.1	-1.6	72	61	71	68	1.7	2.8	1.7	2.1	0	0 ⊙	0	W 4	SW 7	W 6
22	101.8	101.1	100.7	101.2	-1.8	2.4	-3.2	-1.4	2.5	-3.8	75	58	81	71	1.3	3.1	0.9	1.8	8	0	0	W 3	WSW 3	C 0
23	97.6	94.8	92.7	95.0	-7.0	-2.0	-2.4	-3.4	-1.2	-7.9	88	79	70	79	0.4	1.1	1.5	1.0	3	9	0	C 0	N 1	C 0
24	91.5	91.8	92.5	91.9	-6.8	-1.8	-5.0	-4.6	0.6	-8.3	85	73	90	83	0.5	1.4	0.4	0.8	2	2 ⊙	0	C 0	SE 1	C 0
25	93.3	93.0	93.2	93.2	-7.1	2.5	0.4	-1.0	2.6	-8.4	91	63	77	77	0.3	2.7	1.4	1.5	0	0 ⊙	1	C 0	E 1	C 0
26	95.1	95.9	97.9	96.3	0.4	6.0	2.2	2.7	6.0	-1.3	73	53	71	66	1.7	4.5	2.1	2.8	4	3	9	W 3	W 2	W 3
27	99.1	98.7	98.1	98.6	2.4	4.1	0.4	1.8	4.2	-0.1	79	74	88	80	1.6	2.2	0.8	1.5	9	9	9	W 1	WSW 3	W 3
28	93.3	89.9	85.9	89.7	-0.1	4.8	0.5	1.4	5.5	-1.3	84	62	79	75	1.0	3.2	1.3	1.8	1	8	4	W 6	SW 2	C 0
29	83.1	83.2	82.6	83.0	-1.4	1.1	-0.5	-0.3	1.2	-5.0	82	79	78	80	1.0	1.4	1.3	1.2	4	10	5	W 3	W 5	WSW 3
30	78.5	76.5	74.8	76.6	1.4	4.2	1.2	2.0	4.5	-1.4	70	57	72	66	2.1	3.5	1.9	2.5	9	8	6	WSW 7	WSW 8	WSW 5
31	73.9	76.0	77.1	75.7	1.6	1.3	-1.0	0.2	2.2	-2.0	69	79	87	78	2.2	1.4	0.8	1.5	9	10 ✳	4	W 4	WSW 5	W 1
M	87.2	87.0	87.4	87.2	-1.6	1.0	-0.7	-0.5	2.1	-3.9	81	73	79	78	1.1	1.9	1.3	1.4	6.4	7.2	5.8	3.1	3.4	3.1

Przemyśl $H_s = 238$ m $H_b = 238{,}9$ m $h_w = 20$ m **Listopad – Novembre 1957**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	-	$= 3^{50}-11^{25}$; $\cap^{0}$ n – a
2	6	0.0	.	-	$= 5^{10}-22^{45}$ $\equiv^{1}-23^{10}$ $\equiv^{2}-24$; $\cap$ n
3	6	1.1	.	-	$\bullet^{0}2^{51}-3^{00}$, $5^{10}-36$, 7^{08} 10^{40}; $\equiv^{2}0^{00}-1^{50}$ $=-24$
4	7	.	.	-	$\bullet^{0}0^{45}-2^{05}$; $= 0^{00}-11^{44}$, $16^{22}-24$
5	7	.	.	-	$= 0^{00}-11^{50}$, $16^{30}-20^{15}$
6	7	.	.	-	$= 2^{50}-9^{40}$
7	7	.	.	-	$= 3^{45}-7^{30}$, $13^{40}-16^{10}$; $\cap$ n – a
8	6	.	.	-	$= 0^{10}-50$ $\equiv^{2}0^{50}-10^{10}$ $=-24$
9	4	.	.	-	$= 0^{00}-50$ $\equiv^{1}-1^{40}$ $\equiv^{2}-4^{50}$ $\equiv^{1}-7^{30}$ $\equiv^{2}-10^{20}$ $\equiv^{1}-10^{40}$ $\equiv^{0}-11^{30}$ $=-22^{20}$
10	6	.	.	-	$= 5^{45}-10^{20}$ $\infty-12^{50}$ $= 18^{40}-24$
11	7	6.9	.	-	$\bullet^{0}15^{50}-17^{15}$ $\bullet^{1}-18^{40}$ $\bullet^{0}21^{15}-24$; $\gg 12^{40}-18^{30}$ (por. 20 m/sek); $= 0^{00}-6^{50}$
12	7	1.0	.	-	$\bullet^{0}0^{00}-2^{25}$ $\bullet^{1}-5^{30}$ $\bullet^{0}-8^{46}$ $\bullet^{0}15^{44}-16^{38}$ $\bullet^{0}-21^{10}$, $22^{50}-24$; $\gg 1^{00}-3^{45}$ ENE (por. do 20 m/sek)
13	7	.	.	-	$\bullet^{0}0^{00}-1^{45}$; $= 0^{00}-5^{20}$
14	6	.	.	-	$= 6^{30}-24$
15	8	.	.	-	$= 0^{00}-6^{30}$, $20^{15}-24$
16	6	.	.	-	$= 0^{00}-24$; $\sqcup^{2}$ na
17	4	0.0	.	-	$\bullet^{0}11^{10}-17^{40}$; $= 0^{00}-6^{40}$ $\equiv^{0}-7^{25}$ $\equiv^{1}-9^{40}$ $\equiv^{0}-10^{50}$ $=-13^{30}$ $\equiv^{0}-16^{20}$ $=-24$
18	7	.	.	-	$= 0^{00}-5^{50}$, $13^{30}-24$
19	7	.	.	-	$= 0^{00}-9^{36}$
20	8	.	.	-	$= 7^{20}-10^{40}$, $20^{10}-24$; $\sqcup$ na
21	6	.	.	-	$= 0^{00}-20^{15}$; $\sqcup^{2}$ n – a
22	6	.	.	-	$= 7^{40}-12^{05}$ $\infty-18^{30}$ $=-24$
23	6	.	.	-	$= 5^{40}-18^{30}$
24	7	0.0	.	-	$\bullet^{0}22^{15}-24$; $= 7^{40}-12^{15}$, $12^{50}-17^{30}$
25	6	0.0	.	-	$\bullet^{0}0^{00}$ 2^{20}, 3^{40}, 7^{40}, $9^{50}-10^{35}$; $= 7^{40}-24$
26	6	0.2	.	-	$\bullet^{0}0^{50}-6^{10}$, $14^{45}-20^{10}$; $= 0^{00}-24$
27	6	1.3	.	-	$\bullet^{0}3^{20}-6^{05}$, $7^{10}-30$ $\bullet^{0}-11^{25}$ $\bullet^{0}11^{28}$ 12^{20} $16^{10}-25$ $\bullet^{0}18^{50}-19^{20}$ $\bullet^{0}21^{10}-23^{10}$; $= 0^{00}-16^{40}$, $23^{15}-24$
28	6	16.5	.	-	$\bullet^{0}6^{10}-13^{38}$, $14^{40}-19^{10}$; $= 0^{00}-3^{20}$, $19^{10}-24$
29	8	0.3	.	-	$\bullet^{0}1^{00}-3^{25}$ $\bullet^{1}7^{20}-28$ $\triangledown-7^{40}$, $9^{50}-10^{15}$ $*^{0}12^{05}-15$ $\parallel$ $\triangledown^{0}13^{40}-16^{10}$ $*^{0}-24$; $\gg 10^{20}-17^{50}$ NW; $= 0^{00}-5^{45}$
30	6	0.1	1	-	$*^{0}0^{00}-2^{35}$, $5^{40}-9^{45}$, $10^{05}-12^{10}$, $12^{20}-15^{30}$ $*^{1}-16^{10}$ $*^{0}-18^{20}$, $19^{30}-24$; $*\dagger\!\!\rightarrow$ $8^{10}-9^{45}$ $\dagger-10^{30}$
31					
Σ	–	27.4	–	-	UWAGI.

Grudzień – Décembre

1	8	0.0	4	-	$*^{0}0^{00}-4^{10}$ $9^{34}-11^{06}$ $\leftrightarrow 11^{00-08}$; $= 8^{20}-11^{45}$
2	7	0.0	4	-	$*^{0}13^{40}-20^{40}$; $= 9^{10}-11^{20}$
3	4	3.0	3	-	$*^{0}9^{25}-14^{10}$; $= 2^{50}-6^{10}$
4	7	0.5	8	-	$*^{0}6^{05}-9^{10}$, $13^{48}-14^{00}$; $= 14^{40}-24$
5	6	4.3	9	-	$*^{0}2^{45}-5^{10}$, $7^{40}-12^{15}$ $\bullet^{0}13^{35}-15^{40}$ $\bullet^{0}-17^{50}$; $= 0^{00}-18^{20}$
6	6	1.3	5	-	$\bullet^{0}0^{50}-3^{45}$ $\ast$ $7^{35}-8^{20}$ $*^{0}-9^{40}$ $\ast-10^{10}$ $\bullet^{0}10^{50}-11^{40}$ $\ast-15^{50}$ $\bullet^{0}-16^{35}$ $\bullet^{0}-18^{45}$
7	6	.	pż.	-	$= 5^{40}-7^{10}$ $\equiv^{0}-10^{07}$ $=-13^{30}$; $\sqcup$ n – a
8	8	2.3	pż.	-	$\ast^{0}15^{25}-17^{10}$ $*^{0}-20^{15}$ $\triangle-21^{20}$ $\bullet^{0}23^{40}-24$
9	8	0.3	pż.	-	$\bullet^{u}0^{00-10}$ $\triangledown 3^{35}-4^{15}$, 13^{03}, 15^{15}
10	6	0.9	.	-	$*^{0}12^{15}-13^{10}$ $*^{1}-15^{50}$; $= 6^{20}-16^{20}$
11	6	.	1	-	$= 6^{35}-9^{30}$ $\infty-12^{40}$
12	8	.	.	-	$\infty\ 7^{45}-9^{50}$, $13^{25}-14^{40}$, $15^{38}-16^{40}$
13	7	2.1	.	-	$\bullet^{0}22^{50}-24$; $= 6^{20}-9^{40}$
14	8	0.8	.	-	$\bullet^{0}0^{00-40}$ $\triangledown 7^{20-40}$, 8^{30-38}, $11^{10}-12^{50}$, 13^{16-25}, $15^{40}-16^{10}$
15	7	0.0	.	-	$\triangle^{0}12^{10}-13^{25}$; $= 7^{10}-11^{30}$
16	8	.	.	-	
17	7	.	.	-	
18	6	0.0	.	-	$\triangle\ 8^{45}-16^{10}$; $= 6^{10}-24$
19	6	0.0	.	-	$\triangle^{0}9^{50}-13^{35}$; $= 0^{00}-24$
20	6	.	.	-	$= 0^{00}-21^{15}$
21	7	.	.	-	
22	6	.	.	-	$= 8^{20}-12^{10}$ $\infty-17^{35}$ $= 20^{15}-24$
23	5	.	.	-	$= 0^{00}-24$; $\sqcup^{1}$ n – a
24	5	.	.	-	$= 0^{00}-24$; $\sqcup^{1}$ n – n
25	5	.	.	-	$= 0^{00}-21^{45}$; $\sqcup^{1}$ n – a
26	7	.	.	-	$= 7^{30}-12^{10}$
27	7	.	.	-	$= 6^{46}-8^{10}$
28	7	.	.	-	$= 8^{40}-9^{20}$, $22^{25}-24$; $\sqcup$ na
29	7	0.0	.	-	$*^{0}9^{30-50}$; $= 0^{00}-7^{45}$; $\sqcup$ n – a
30	8	.	.	-	
31	6	0.7	.	-	$*^{0}9^{15}-12^{10}$ $\ast-15^{25}$
Σ	–	16.2	–	-	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Styczeń – Janvier 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	17.5	17.3	16.7	17.2	-2.3	0.0	-1.5	-1.3	5.2	-3.3	91	84	88	88	0.5	1.0	0.7	0.7	10 ✳	3 ⊙	7 ✳	NW 1	ENE 2	SSE 2
2	15.2	15.9	19.4	16.8	8.0	9.0	3.8	6.2	9.5	-2.7	56	54	76	62	4.8	5.4	1.9	4.0	8	6	8	SW 7	W 5	NW 2
3	22.3	23.3	24.3	23.3	-0.5	2.7	-0.7	0.2	5.7	-1.0	98	85	98	94	0.1	1.1	0.1	0.4	8	9	5	W 1	SE 1	C 0
4	24.4	26.2	27.3	26.0	-1.0	-0.1	-2.1	-1.3	0.8	-2.5	100	92	94	95	0.0	0.5	0.3	0.3	10 ≡	10	3	C 0	NNE 2	C 0
5	27.9	26.5	24.2	26.2	-5.4	0.1	0.6	-1.0	1.6	-5.8	95	83	90	89	0.2	1.1	0.6	0.6	3	7 ⊙	10 ●	C 0	NE 1	SW 1
6	22.4	19.8	17.8	20.0	4.2	6.1	3.9	4.5	7.0	-0.3	88	80	89	86	0.9	1.9	0.9	1.2	10	10	10 ●	SW 10	WSW 5	WSW 5
7	22.4	25.4	29.1	25.6	-1.3	-0.8	-0.7	-0.9	4.0	-1.9	93	95	97	95	0.4	0.3	0.2	0.3	10 ✳	10 △	10	W 6	WSW 6	SW 6
8	31.4	30.0	29.7	30.4	-0.7	2.1	1.6	1.2	3.2	-1.2	93	76	93	87	0.4	1.7	0.6	0.9	10	10	10 ◔	SW 4	W 3	NW 2
9	28.0	26.1	23.7	25.9	-0.7	-0.5	-2.8	-1.7	2.7	-3.2	100	100	97	99	0.0	0.0	0.1	0.0	10 ≡	5 ○ ≡	6	C 0	SW 1	C 0
10	19.7	15.8	16.8	17.4	0.3	7.2	-1.1	1.3	7.6	-3.4	96	24	91	70	0.2	7.8	0.4	2.8	6	8 ⊙	10 ✳	WSW 3	W 4	W 1
11	17.7	18.6	21.3	19.2	-2.8	-3.5	-4.4	-3.8	-0.6	-4.7	86	90	98	91	0.7	0.5	0.1	0.4	10 ✳	10 ✳	10 ✳	W 3	SW 4	SW 2
12	19.9	16.3	9.9	15.4	-5.9	-3.5	-4.3	-4.5	-2.8	-6.3	97	65	94	85	0.1	1.6	0.3	0.7	10	6	10	SW 2	W 3	C 0
13	7.3	8.0	10.5	8.6	-6.0	-3.4	-4.6	-4.6	-2.8	-6.8	94	88	96	93	0.2	0.6	0.2	0.3	10 ✳	9	10 ✳	C 0	NNE 1	C 0
14	13.6	15.6	18.7	16.0	-6.6	-3.4	-7.5	-6.2	-2.9	-7.9	94	92	87	91	0.2	0.4	0.4	0.3	10 ✳	10	10	C 0	NE 3	E 4
15	18.1	16.8	18.3	17.7	-7.7	-6.5	-8.8	-8.0	-5.6	-9.2	99	97	95	97	0.0	0.1	0.2	0.1	10	10 ✳	10 ✳	E 1	NE 2	NE 1
16	21.7	23.7	26.3	23.9	-10.9	-9.2	-12.4	-11.2	-8.4	-13.2	94	85	93	91	0.2	0.4	0.2	0.3	10 ✳	10 ✳	10 ✳	E 1	ENE 3	ENE 1
17	27.1	28.2	29.3	28.2	-21.5	-10.3	-17.3	-16.6	-8.9	-24.6	96	84	85	88	0.0	0.4	0.2	0.2	2	3 ⊙	2	W 1	NE 4	NE 1
18	28.7	27.8	28.4	28.3	-15.5	-1.6	-11.4	-10.0	-0.5	-19.9	81	69	97	82	0.3	1.7	0.1	0.7	4	5	0	C 0	SW 1	C 0
19	27.1	27.8	29.7	28.2	-12.1	-5.4	-9.1	-8.9	-4.1	-14.5	96	92	88	92	0.1	0.3	0.4	0.3	0	2 ⊙	10 ≡	C 0	NE 1	SW 1
20	29.1	28.8	28.7	28.9	-16.5	-5.1	-3.6	-7.2	-2.4	-20.1	90	73	58	74	0.2	1.1	2.0	1.1	0	0 ○	0	C 0	C 0	C 0
21	27.9	27.1	28.5	27.8	-10.8	-0.2	-8.8	-7.2	1.2	-13.7	90	52	77	73	0.3	2.9	0.7	1.3	0	1 ⊙	0	C 0	NW 1	C 0
22	27.5	25.9	23.3	25.6	-9.6	9.1	-6.5	-3.4	9.8	-10.6	78	19	26	41	0.6	9.4	2.8	4.3	8	8 ⊙	0	SW 2	S 3	NE 2
23	22.5	21.5	18.7	20.9	-10.8	2.1	-3.9	-4.1	3.4	-12.1	73	39	80	64	0.7	4.3	0.9	2.0	0	8 ⊙	7	W 2	NW 1	NW 1
24	14.0	11.9	12.1	12.7	-3.4	2.5	-5.2	-2.8	3.3	-6.0	85	37	93	72	0.7	4.6	0.3	1.9	10	9	5	C 0	NE 2	C 0
25	12.1	13.1	16.6	13.9	-1.8	1.4	-3.6	-1.9	2.0	-6.1	98	83	90	90	0.1	1.2	0.5	0.6	10 ✳	9	3	C 0	N 2	C 0
26	20.6	22.1	23.6	22.1	-2.8	1.2	-5.7	-3.8	2.1	-7.5	91	77	83	84	0.5	1.6	0.6	0.9	10	10	0	W 1	N 1	C 0
27	20.6	21.2	23.7	21.8	-4.5	2.0	0.8	-0.2	2.9	-9.4	86	79	88	84	0.6	1.5	0.8	1.0	8	10 ✳	10 ✳	C 0	WSW 3	SW 1
28	22.1	23.5	29.1	24.9	-2.0	-2.9	-4.1	-3.3	1.3	-4.4	89	99	94	94	0.6	0.0	0.3	0.3	10	10 ✳	10 ✳	W 1	W 4	C 0
29	32.2	31.4	30.3	31.3	-4.1	-1.4	-4.3	-3.5	0.1	-6.3	96	88	84	89	0.2	0.6	0.7	0.5	10	7	10	W 1	SW 1	SW 2
30	27.7	24.9	23.6	25.4	-7.5	1.7	-2.1	-2.5	4.5	-8.0	79	61	72	71	0.7	2.7	1.4	1.6	1	7 ⊙	1	C 0	C 0	WSW 5
31	24.4	25.5	26.1	25.3	-2.7	0.8	-2.6	-1.8	2.6	-4.3	95	82	91	89	0.2	1.2	0.5	0.6	10	3 ⊙	1	N 1	NE 2	C 0
M	22.4	22.1	22.8	22.4	-5.3	-0.3	-4.2	-3.5	1.3	-7.8	90	75	87	84	0.5	1.9	0.6	1.0	7.4	7.3	6.4	1.5	2.3	1.3

Luty – Février

1	123.9	124.0	124.9	124.3	-3.0	0.0	-1.1	-1.3	0.6	-7.9	97	94	99	97	0.1	0.4	0.1	0.2	10 ✳	10 ✳	10 ●	C 0	N 1	C 0
2	128.0	128.9	130.6	129.2	1.4	5.2	5.6	4.4	6.5	-1.3	98	85	95	93	0.2	1.3	0.4	0.6	10 ◔	10	10	SW 1	C 0	SW 1
3	129.1	126.5	127.4	127.7	1.8	8.8	0.6	3.0	9.8	0.2	98	69	96	88	0.2	3.5	0.3	1.3	8	8 ⊙	0	C 0	NE 1	C 0
4	127.4	126.3	126.3	126.7	-1.8	4.6	0.6	1.0	6.5	-2.2	98	80	94	91	0.2	1.7	0.4	0.8	9	10	5	C 0	C 0	SW 2
5	126.5	126.3	125.3	126.0	-1.6	7.9	0.1	1.6	10.1	-2.4	100	61	90	84	0.0	4.1	0.7	1.6	1	0 ⊙	0	C 0	N 1	SW 1
6	122.8	119.8	119.8	120.8	-3.3	9.5	1.9	2.5	10.4	-3.6	97	37	72	69	0.1	7.4	1.9	3.1	0	2 ⊙	0	W 1	SE 4	SW 1
7	120.4	121.6	123.1	121.7	4.9	3.8	0.9	2.6	5.6	-2.9	71	78	77	75	2.5	1.8	1.5	1.9	10	10	2	W 4	W 7	W 2
8	120.0	115.8	113.0	116.3	-3.4	4.8	1.6	1.2	8.8	-4.3	88	66	88	81	0.6	2.9	0.8	1.4	8	10	10	C 0	SE 1	C 0
9	109.5	109.7	111.0	110.1	5.4	4.8	2.4	3.8	6.1	0.3	69	69	91	76	2.8	2.6	0.7	2.0	10	8	10 ●	WSW 6	SW 3	SW 2
10	112.6	112.7	112.4	112.6	-0.7	3.7	2.5	2.0	4.9	-1.5	89	61	74	75	0.6	3.1	1.8	1.8	0	7	8	SW 1	SW 6	WSW 2
11	112.6	114.6	117.4	114.9	0.2	3.1	0.8	1.2	3.9	-1.5	90	75	90	85	0.6	1.8	0.7	1.0	10	9	10 ✳	C 0	WNW 4	W 1
12	116.9	115.2	111.5	114.5	-3.0	3.1	3.1	1.6	4.0	-3.5	88	52	57	66	0.6	3.6	3.3	2.5	7	2 ⊙	10	3 1	NE 2	W 3
13	109.1	106.7	98.3	104.7	0.6	4.4	4.6	3.6	5.8	-0.7	81	75	56	71	1.3	2.1	3.7	2.4	10	3	10	SE 3	W 6	SSW14
14	97.7	96.7	98.0	97.5	4.1	4.7	2.0	3.2	6.3	-0.4	68	69	81	73	2.6	2.6	1.4	2.2	10	10	9	NE 1	WNW 1	SW 2
15	98.7	95.1	93.8	95.9	-1.9	5.2	2.0	1.8	5.9	-2.2	89	62	93	81	0.6	3.3	0.6	1.5	9	10 ●	10 ◔	NW 2	SW 10	NE 2
16	99.7	102.2	106.1	102.7	2.4	5.2	2.4	3.1	6.3	-0.4	57	42	52	50	3.1	5.0	3.5	3.9	7	2	10	W 5	SW 2	SW 2
17	110.0	111.2	112.7	111.3	-1.4	4.0	0.8	1.0	6.4	-1.7	86	55	75	72	0.8	3.6	1.7	2.0	6	6	0	SSW 1	NE 1	SW 1
18	111.5	106.6	101.3	106.5	2.4	7.4	9.6	7.2	10.3	-3.6	71	41	54	55	2.1	6.1	5.5	4.6	10	9	6	NE 3	S 12	SW 14
19	104.4	111.9	117.1	111.1	0.7	-0.9	-2.3	-1.2	10.0	-2.9	90	81	83	85	0.6	1.1	0.9	0.9	10 ✳	10	4	W 4	W 4	WSW 1
20	118.9	117.2	113.9	116.7	-8.0	3.3	2.4	0.0	4.8	-9.0	87	33	62	61	0.4	5.1	2.8	2.8	1	9	8	C 0	SSE 4	SW 6
21	111.9	111.8	114.1	112.6	2.2	7.1	0.4	2.5	7.7	0.1	65	48	98	70	2.5	5.2	0.1	2.6	8	8	10 ✳	SW 3	SW 2	C 0
22	116.7	116.5	116.2	116.5	-2.8	-2.7	-6.3	-4.5	0.8	-6.7	95	86	91	91	0.2	0.7	0.3	0.4	10 ✳	10 ✳	9	N 1	C 0	C 0
23	116.6	116.1	115.5	116.1	-14.7	-7.4	-10.7	-9.4	1.3	-16.0	87	70	90	82	0.3	1.7	0.3	0.8	3	1	0	C 0	C 0	C 0
24	109.3	103.6	103.7	105.5	-5.8	-0.1	-2.5	-2.7	1.6	-13.2	82	57	91	77	0.7	2.6	0.5	1.3	10 ✳	10 ✳	10 ✳	ENE 2	N 5	C 0
25	107.6	108.3	105.8	107.2	-2.2	-0.4	-1.2	-1.2	0.9	-2.9	96	82	95	91	0.2	1.1	0.3	0.5	10	9	10 ✳	W 1	NE 2	C 0
26	111.7	115.6	119.2	115.5	-3.8	-3.2	-4.0	-3.8	-0.6	-4.6	94	81	94	90	0.3	0.9	0.3	0.5	10 ✳	10 ✳	10 ✳	N 3	WNW 3	C 0
27	121.3	122.3	124.0	122.5	-6.9	-3.6	-10.9	-8.1	-2.6	-11.7	83	80	94	86	0.6	0.9	0.2	0.6	10	1	0	C 0	NE 2	C 0
28	126.2	127.5	129.0	127.6	-12.0	-7.6	-8.2	-9.0	-6.1	-17.2	93	96	89	93	0.2	0.1	0.3	0.2	10	10	10	SW 1	N 1	C 0
29																								
30																								
31																								
M	115.0	114.7	114.7	114.8	-1.8	2.9	-0.1	0.2	4.9	-4.4	86	67	83	79	0.9	2.7	1.2	1.6	7.7	7.3	6.8	1.6	3.0	2.0

Zakopane

$H_s = 844\ m$ $H_b = 838{,}2\ m$ $h_w = 20\ m$

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.0	10	4.6	•°0^{30} 3^{10} ✳°6^{10}–7^{05}, 19^{40}–20^{45}; = 19^{40}–20^{30}
2	8	.	6	1.2	
3	7	0.0	4	0.4	= 18^{10}–24
4	6	0.2	pż.	.	♆ 3^{10}...20 ✳°6^{30}–7^{15}, 8^{05}...45–10^{25}; ≒ 0^{00}–6^{30} ≡^{1}–7^{55} = 8^{05}–11^{10}, 12^{15}–24
5	7	6.2	pż.	.	•°17^{35}–18^{25} 19^{30} •^{1}–19^{45} (marznąc) •°–22^{10} (marznący) •^{1}–22^{30} (marznący) •°–24 (marznący)
6	8	9.7	pż.	2.4	•°0^{00}–30 (marznący) •^{1}–1^{10} ••°–2^{30} •°15^{30} 17^{20} 18^{10}–20^{25} •^{1}–21^{05} •°–21^{30} ✳°–24; = 0^{00}–6^{15}, 20^{25}–24; ∽°0^{00}–30
7	6	6.4	2	.	✳°•°0^{00}–05 ♆°6^{10}–7^{05} △°–10^{20} △^{1}–11^{30} △°–15^{45} ♆°–19^{10} ⚹°–19^{30} ♆°21^{35}–45 ♆ 23^{20}–24; = 0^{00}–15
8	7	0.1	7	.	♆°0^{00}–2^{15} ✳°9^{20}–30 ✳°–10^{35}, 11^{05} ✳^{1}–11^{15} ✳°–11^{50} •°20^{05}–21^{30}; = 9^{15}–11^{30}, 20^{05}–24
9	3	.	4	0.7	= 0^{00}–6^{40} ≡°–8^{15} ≡^{1}–9^{30} ≡^{2}–10^{30} ≡^{1}–12^{45} ≡°–13^{15} ≡^{2}–20^{15} ≡^{2}–21^{20}; √ 19^{00}–20^{00} ⌴° n
10	9	1.8	3	3.6	✳°20^{05}–21^{15} ✳^{1}–22^{40} ✳°–24 ⌴° n – /
11	7	1.4	8	0.1	✳°0^{00}–7^{55} ⚹°–8^{10} ♆°–10^{15}, 11^{05}–10 ♆^{1}–11^{15} ♆^{2}–12^{30} ♆^{1}–13^{20} ♆°–14^{35}, 15^{08}–18 ♆^{1}–15^{20} ♆^{2}–16^{15} ♆°–19^{30} ✳°–24
12	8	0.3	15	2.1	✳°0^{00}–2^{40} ♆°7^{50}–10^{15} ✳°21^{30}–24
13	6	2.1	15	.	✳°0^{00}–10, 6^{20}–8^{30}, 15^{50} 16^{20} 16^{25}–24; = 9^{10}–15^{20}
14	7	0.0	12	.	✳°0^{00}–5^{10}, 6^{15}–7^{10}, 8^{40} 10^{30}
15	6	3.0	11	.	✳°7^{40}–24
16	7	0.7	20	.	✳°0^{00}–9^{10} ✳^{1}–10^{20} ✳°–21^{25}
17	7	.	28	5.2	= 5^{15}–6^{10}, 7^{05}–9^{40}; ⌴° n
18	8	.	25	6.7	⌴° n, 111 – n
19	6	.	22	3.0	= 9^{30}–17^{40} ≡^{1}–24; ⌴^{1} n
20	7	.	22	6.9	≡^{1}0^{00}–2^{40}; √°0^{50}–12^{30}
21	8	.	19	6.7	⌓^{1}18^{30}–19^{10} ⌓°–23^{20} ⌓^{1}–23^{40} ⌓°–24; = 19^{10}–20^{15}
22	8	.	17	3.4	= 20^{30}–21^{15}; ⊕° 13^{00}–14^{00}; ⌓° 0^{00}–30
23	8	.	15	4.3	⊕° 12^{20}–14^{30}
24	8	0.6	14	1.2	
25	7	0.0	12	.	✳°6^{10}–8^{25}, 23^{45} 24; = 18^{20}–20^{15}; ⊕° 15^{45}–55
26	7	0.0	11	0.8	✳°0^{00}...30, 4^{50}–5^{38}, 7^{50} 11^{20}; = 5^{30}–6^{20}, 8^{30}–11^{30}
27	7	1.1	9	.	✳°8^{50}, 9^{15}–10^{10}, 10^{30} 13^{30} △° 13^{40}–15^{10} ✳°–16^{25}, 20^{10}–21^{30} △^{1}–21^{40} ✳°–22^{30}; ⌴° n
28	2	8.0	10	.	✳°0^{20}–3^{20}, 11^{05}–20 ✳^{1}–11^{35} ✳^{2}–15^{20} ✳^{1}–18^{25} ✳°–24; ✳ ⁺ ⁺ ^{1} 12^{30}–13^{45}
29	9	.	25	3.1	✳°0^{00}–6^{10}
30	8	.	23	4.8	⌴° na – / ( ) a
31	8	0.0	21	3.2	= 6^{10}–9^{15}, 17^{30}–18^{40}
Σ	–	41.6	–	64.4	UWAGI

Luty – Février

1	7	6.1	18	.	✳°5^{50}–13^{30} •°18^{40}–19^{45} •^{1}–20^{35} (marznąca) •°–21^{35} •°–22^{40} (marznąca) •°–23^{10} (marznący) •^{1}–24 (marznąca); = 15^{40}–20^{00}
2	7	0.0	15	0.3	•°0^{00}–6^{30} (marznąca), 6^{30}–9^{10}, 18^{30}–20^{30}; ∽ na – 7^{45} [1.II: ∽° n – n/r
3	8	.	8	4.5	
4	7	.	5	1.8	= 9^{30}–13^{20}, 18^{40}–19^{30}, 21^{30}–24; ∽° 3^{30}–8^{10}
5	8	.	4	7.9	= 0^{00}–30, na – a
6	9	.	3	7.9	= 6^{10}–7^{30}, ⌴° n
7	8	.	3	.	
8	8	.	2	1.1	⌴° n
9	8	4.2	pż.	0.2	•°13^{50}–14^{05} ♆°17^{05}–30 ♆^{1}–20^{10} •°20^{20}–21^{40} •^{1}22^{15}–23^{10}
10	9	.	pż.	4.5	•^{1}14^{40}–22^{5}
11	8	2.2	pż.	.	⚹°13^{50}–14^{05} ⚹^{1}15^{35}–55 ⚹°–16^{10} ✳°–16^{25}, 17^{55}–18^{15}, 20^{40}–21^{30} ✳^{1}–22^{40} ✳°–23^{20}
12	8	0.0	4	7.0	✳°21^{30}–22^{15} 22^{20} 24; ≫ 23^{10}–24 W
13	8	0.0	4	4.4	✳°0^{00} 2^{30} 2^{35}–5^{15} •°21^{35} 22^{05}; ≫ 0^{00}–30 W, 15^{30}–24 SW
14	7	0.8	pż.	.	•°0^{10}–1^{05} 13^{45}–14^{10}, 15^{35}–16^{28}; ≫ 0^{00}–10 SW
15	8	0.4	pż.	4.2	•°12^{20}–13^{10} ♆°–14^{30} •°–19^{40} •°20^{25}–22^{10}, ≫ 12^{30}–13^{40} SW
16	9	0.0	pż.	4.9	
17	9	.	pż.	7.1	♆°3^{10}–12 ✳°3^{15}...30 ⌴^{1} na – a
18	8	5.1	pż.	1.5	•°18^{55} 19^{05} •^{1}–19^{20} •°19^{30} 20^{15} 21^{05}–15 21^{30} 23^{20} •^{1}23^{30}–24; ≫ 10^{30}–19^{50} (par. do 17 m/sek) ≪–23^{30} SSE
19	7	1.0	.	0.1	•°0^{00}–30 •°–2^{25} ✳^{1}6^{35}–7^{33} ✳°11^{25}, 12^{35}–14^{45}; ≫ 0^{00}–30 (par. do 17 m/sek) ⌴°na
20	8	0.0	1	4.3	≫ 22^{30}–24, ⌴° na – / [18.II: par. ponad 20 m/sek ≫–24 SW par. do 17 m/sek
21	8	21.7	pż.	4.0	△°0^{30}–2^{40} ✳°3^{30}–5^{35} ♆°17^{03}–40 ⚹°•°–18^{00} •°–18^{20} ⚹°–19^{30} ✳°–19^{45} ✳^{1}–21^{30} △^{1}–22^{40} ✳°–23^{15} ✳^{1}–24, ≫ 0^{00}–2^{40} SE
22	6	6.7	16	.	✳^{1}00–1^{40} ✳°–9^{30} ✳^{1}–10^{45} ✳°–11^{15} ✳^{1}–13^{40} ✳°–17^{30}; √°0^{30}–12^{30}
23	9	0.0	22	8.5	⌴° n – n/r
24	7	1.5	20	0.1	✳°6^{10} 8^{30}–9^{15}, 9^{25} 10^{15}, 12^{08} 14^{10} 15^{50}–24; ⌴° na
25	6	8.3	22	0.2	✳°0^{00}–5^{20} 18^{10}–24; = 8^{20}–18^{10}
26	6	1.8	31	.	✳°0^{00}–1^{30} ✳^{1}–5^{20} ✳°–7^{10} ✳^{1}–9^{35} ✳°–10^{27}, 11^{50}–12^{15} ♆°12^{55}–13^{05} ✳°13^{25}–24
27	7	.	37	7.8	✳°0^{00}–30 = 3^{20}–8^{30}
28	6	1.6	33	.	✳°10^{45} 11^{05}, 18^{25}–24; = 4^{10}–24; ⌴^{1} na
29					
30					
31					
Σ	–	61.4	–	82.3	UWAGI. *W lutym wartości ciśnienia atmosferycznego wynoszą 800 mb + wartości podane w tablicy.*

Zakopane — φ = 49°18' — λ = 19°57' — Marzec – Mars 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	30.0	30.1	30.4	30.2	-9.8	-6.5	-8.4	-8.3	-5.7	-10.5	85	70	89	81	0.4	1.1	0.3	0.6	10 ✳	10 ✳	10 ✳	W 1	ENE 1	C 0
2	29.0	27.9	26.2	27.7	-9.1	-5.3	-7.3	-7.2	-4.5	-9.8	88	62	85	78	0.4	1.5	0.5	0.8	10 ✳	9	10 ✳	C 0	SW 1	C 0
3	22.7	20.9	20.3	21.3	-8.3	-4.6	-9.9	-8.2	-3.9	-10.4	92	76	84	84	0.2	1.0	0.4	0.5	10 ✳	8	10 ✳	C 0	NW 1	C 0
4	17.2	15.5	14.9	15.9	-15.1	2.2	0.0	-3.2	4.9	-16.2	82	22	25	43	0.3	5.5	4.6	3.5	4	3 ⊙	10	C 0	ENE 1	C 0
5	13.9	14.9	16.1	15.0	-1.6	0.6	-3.9	-2.2	1.2	-4.4	73	73	82	76	1.4	1.8	0.8	1.3	10	10 ●	2	S 1	C 0	NNE 1
6	16.1	14.6	13.9	14.9	-12.6	1.1	-7.2	-6.5	2.5	-14.0	89	47	88	75	0.3	3.5	0.4	1.4	3 ⊙	0	0	C 0	NE 1	C 0
7	12.5	12.7	14.2	13.1	-10.7	2.7	-6.9	-5.4	2.8	-12.1	94	46	88	76	0.2	4.0	0.4	1.5	0	0 ⊙	0	C 0	NE 2	C 0
8	15.2	15.5	17.8	16.2	-12.9	1.1	-8.6	-7.2	1.9	-14.3	92	48	89	76	0.2	3.4	0.4	1.3	3	2 ⊙	0	W 1	ENE 3	C 0
9	20.4	22.5	26.5	23.1	-11.6	-0.5	-8.0	-7.0	-0.1	-13.6	93	38	84	72	0.2	3.7	0.5	1.5	9	1 ⊙	2	C 0	NE 3	C 0
10	28.1	29.4	31.3	29.6	-13.9	0.0	-7.8	-7.4	1.5	-15.2	87	56	90	78	0.3	2.7	0.3	1.1	0 ⊙	0	0	C 0	NE 2	C 0
11	32.0	32.1	32.1	32.1	-10.7	5.5	-4.8	-3.7	6.3	-12.7	90	30	69	63	0.3	6.3	1.3	2.6	1 ⊙	0 ⊙	0	C 0	NE 2	C 0
12	29.3	26.2	23.5	26.3	-7.4	7.0	1.5	0.6	8.6	-8.6	85	31	30	49	0.5	6.9	4.7	4.0	3	8	9	SW 1	NE 2	C 0
13	21.9	22.5	22.9	22.4	-1.2	10.4	3.5	4.0	11.4	-3.1	56	25	66	49	2.5	9.4	2.6	4.8	3 ⊙	4 ⊙	1	C 0	C 0	SSW 2
14	20.2	18.3	16.6	18.4	0.9	12.2	9.2	7.9	14.2	-0.6	85	34	63	61	1.0	9.4	4.3	4.9	7 ⊙	3 ⊙	9	SW 1	WSW 7	W 3
15	17.8	17.5	13.8	16.4	3.0	5.1	5.6	4.8	9.8	2.7	89	71	75	78	0.8	2.5	2.3	1.9	10	9	10	NNW 3	SW 2	SW 6
16	8.1	10.6	15.4	11.4	5.1	1.4	-2.5	0.4	6.9	-2.9	88	94	80	87	1.0	0.4	1.0	0.8	10 ●	10 ✳	10	SW 4	WSW 3	W 1
17	15.7	15.0	11.7	14.1	-2.8	1.9	2.8	1.2	4.8	-3.9	95	93	93	94	0.2	0.5	0.6	0.4	10 ✳	10 ●	9	NE 1	WSW 3	O 0
18	5.7	5.9	9.6	7.1	6.6	9.4	3.7	5.8	10.3	1.2	83	70	81	78	1.6	3.6	1.5	2.2	10 ●	8	10	WSW 3	W 8	W 3
19	13.3	14.9	13.5	13.9	3.9	6.1	6.2	5.6	7.7	2.4	73	62	87	74	2.2	3.6	1.2	2.3	8 ⊙	7 ⊙	10 ●	WSW 3	WNW 4	SW 2
20	16.0	16.0	14.2	15.4	5.2	11.8	12.2	10.4	13.9	4.6	95	53	43	64	0.4	6.4	7.9	4.9	10	8 ⊙	0	WSW 1	W 3	WSW 4
21	14.6	16.7	17.7	16.3	4.0	12.4	7.1	7.6	14.3	2.5	80	59	64	68	1.6	5.9	3.7	3.7	9	8	9	C 0	NW 2	WSW 2
22	18.9	20.2	21.5	20.2	1.3	7.8	0.1	2.3	9.6	-0.3	78	55	86	73	1.5	4.8	0.9	2.4	3	6	0	WSW 1	NNW 3	SW 1
23	21.5	20.3	20.5	20.8	-1.4	10.8	6.4	5.6	11.4	-3.8	89	46	79	71	0.6	7.0	2.0	3.2	6	6	10	SW 1	NNE 3	C 0
24	21.5	23.0	24.0	22.8	4.0	5.3	3.3	4.0	6.7	3.0	84	84	91	86	1.2	1.4	0.6	1.1	10 ●	10	10	NE 2	NE 4	C 0
25	24.2	25.5	26.1	25.3	3.3	6.9	3.5	4.3	10.2	2.3	97	88	97	94	0.2	1.2	0.2	0.5	10	10	5	C 0	NE 1	C 0
26	25.9	25.2	26.2	25.8	-0.1	10.5	3.9	4.6	12.5	-0.6	98	61	71	77	0.2	5.0	2.3	2.5	10 ≡	5 ⊙	0	C 0	NNE 2	NE 2
27	27.4	28.1	28.3	27.9	-0.6	10.9	0.2	2.7	12.4	-2.5	77	42	74	64	1.3	7.5	1.6	3.5	0 ⊙	0 ⊙	0	C 0	N 3	SW 2
28	25.6	24.0	21.5	23.7	-1.8	11.2	3.5	4.1	12.1	-3.6	73	20	40	44	1.4	10.6	4.7	5.6	1 ⊙	6	4	C 0	SSE 4	SW 3
29	18.8	18.1	17.9	18.3	2.4	8.5	3.8	4.6	9.9	2.0	59	69	82	70	3.0	3.5	1.5	2.7	10	10	8	E 3	NE 2	C 0
30	17.3	18.3	18.5	18.0	1.8	7.8	5.4	5.1	9.8	0.7	94	53	46	64	0.4	5.1	4.9	3.5	10	9	0	W 1	N 2	NE 3
31	23.5	23.4	24.2	23.7	-1.9	9.7	0.4	2.2	11.3	-3.7	86	47	90	74	0.7	6.3	0.7	2.6	6 ⊙	8 ⊙	2	C 0	E 2	SW 1
M	20.1	20.2	20.4	20.2	-3.0	5.3	0.2	0.7	6.9	-4.7	85	56	75	72	0.8	4.4	1.9	2.4	6.6	6.1	5.2	0.9	2.5	1.2

Kwiecień – Avril

1	123.8	123.1	123.1	123.3	0.7	14.4	3.2	5.4	15.1	-3.0	83	25	57	55	1.1	12.4	3.3	5.6	4 ⊙	1 ⊙	1	SW 1	SE 3	C 0
2	122.9	123.6	124.1	123.5	5.2	13.2	5.8	7.5	14.8	0.3	45	27	57	43	4.8	11.2	3.9	6.6	2 ⊙	7 ⊙	8	S 2	S 4	SW 1
3	125.8	126.2	128.6	126.9	3.0	16.1	3.7	6.6	16.4	0.0	68	21	74	54	2.4	14.4	2.1	6.3	5 ⊙	4 ⊙	1	C 0	NNW 2	WSW 1
4	130.9	130.9	130.8	130.9	2.1	13.2	3.3	5.5	14.4	-2.4	69	30	70	56	2.2	10.7	2.2	5.0	0 ⊙	1 ⊙	0	C 0	NE 3	C 0
5	129.2	127.3	24.3	126.9	1.2	12.8	2.5*	4.8	13.9	-2.0	87	33	78	66	1.0	10.0	1.6	4.2	0 ⊙	0 ⊙	0	C 0	NNE 5	C 0
6	120.9	117.5	114.9	117.8	2.0	15.3	8.3	8.5	16.6	-2.0	69	22	49	47	2.2	13.6	5.7	7.2	0 ⊙	0 ⊙	0	C 0	SW 4	SW 1
7	111.9	111.3	113.0	112.1	2.4	8.4	1.1	3.2	13.4	-0.6	74	74	92	80	1.9	2.9	0.5	1.8	1 ⊙	10 ●	10 ✳	C 0	NW 3	C 0
8	116.0	116.9	117.4	116.8	-0.9	0.2	-0.5	-0.4	1.2	-1.4	95	96	90	94	0.3	0.3	0.6	0.4	10 ✳	10 ✳	10	NE 1	NE 1	C 0
9	115.9	115.1	113.9	115.0	-4.5	3.4	-0.1	-0.3	4.9	-7.8	91	61	92	81	0.4	3.0	0.5	1.3	1 ⊙	7 ⊙	7	C 0	NW 2	SE 1
10	112.4	109.6	105.2	109.1	-0.8	8.2	5.2	4.4	10.6	-3.2	98	51	70	73	0.2	5.4	2.6	2.7	7 ⊙	4 ⊙	8	W 3	NE 3	C 0
11	98.7	98.8	104.5	100.7	4.0	5.9	0.2	2.6	8.5	-0.1	91	87	98	92	0.7	1.2	0.1	0.7	10 ●	10 ✳	10 ✳	C 0	N 1	C 0
12	109.8	110.5	113.0	111.1	-1.5	1.4	-1.4	-0.7	2.1	-2.2	84	63	88	78	0.9	2.6	0.6	1.4	8 ✳	9	10 ✳	C 0	ENE 3	C 0
13	114.1	115.9	118.3	116.1	-2.2	0.8	-0.9	-0.8	2.7	-2.9	91	54	93	79	0.5	3.0	0.4	1.3	10 ✳	9	10 ⛌	NE 1	N 1	SW 1
14	118.6	118.1	118.2	118.3	-3.7	0.5	-1.6	-1.6	1.2	-5.3	87	51	71	70	0.6	3.0	1.5	1.7	9 ⊙	10 ✳	9	C 0	NE 3	E 2
15	118.5	120.6	123.5	120.9	-3.4	-2.1	-2.6	-2.7	0.0	-3.6	83	77	89	83	0.8	1.2	0.6	0.9	10 ✳	10 ✳	10 ✳	NE 1	ESE 1	C 0
16	124.9	124.6	125.2	124.9	-3.8	3.6	3.0	1.4	6.7	-6.8	82	47	73	67	0.8	4.2	2.0	2.3	1 ⊙	1 ⊙	10	SW 1	NW 2	C 0
17	122.9	122.1	121.1	122.0	3.2	3.0	2.0	2.6	5.2	1.9	82	91	94	89	1.4	0.7	0.4	0.8	10 ●	10 ●	10	C 0	SW 1	C 0
18	119.1	118.5	118.2	118.6	1.0	1.8	0.0	0.7	2.6	0.0	90	88	90	89	0.7	0.8	0.6	0.7	10 ✳	10 ⛌	10	C 0	WSW 1	W 1
19	117.7	116.5	118.4	117.5	-0.4	7.2	1.6	2.5	8.8	-1.2	88	46	84	73	0.7	5.5	1.1	2.4	9	5 ⊙	2	C 0	NW 3	C 0
20	121.1	123.8	125.7	123.5	3.6	3.8	2.3	3.0	4.4	0.5	93	93	93	93	0.5	0.5	0.5	0.5	10	10 ●	10 ● ●	C 0	SW 1	NE 1
21	126.4	127.5	128.6	127.5	1.3	4.4	3.3	3.1	4.7	0.6	94	83	91	89	0.4	1.4	0.6	0.8	10	10 ●	10	C 0	C 0	C 0
22	128.5	128.5	129.8	126.9	3.0	9.5	4.3	5.3	9.8	1.9	96	74	97	89	0.3	3.2	0.3	1.3	10 ● ≡	8	10 ●	NE 1	ENE 3	NE 2
23	128.9	128.3	128.9	128.7	2.3	8.2	5.7	5.5	8.5	1.7	96	74	94	88	0.3	2.9	0.6	1.3	10	10	10 ●	C 0	E 2	C 0
24	126.6	126.6	126.2	126.5	4.6	7.1	6.0	5.9	8.6	4.2	97	85	92	91	0.3	1.5	0.8	0.9	10 ●	10	10	C 0	NE 2	C 0
25	123.5	122.9	123.4	123.3	5.5	10.4	7.6	7.8	10.9	3.4	92	86	94	91	0.7	1.8	0.6	1.0	8	10 ●	10 ●	C 0	SW 1	C 0
26	122.9	122.5	123.5	123.0	6.9	13.5	8.4	9.3	14.8	5.3	92	63	90	82	0.7	5.6	1.1	2.5	10	9	9	C 0	NE 2	C 0
27	121.2	120.7	119.9	120.6	7.7	12.0	8.0	8.9	16.7	3.2	88	81	85	85	1.2	2.7	1.5	1.8	1 ⊙	10 ● ⛆	3	C 0	SE 2	C 0
28	118.6	117.9	118.3	118.3	10.1	18.0	9.3	11.7	18.9	4.1	79	43	75	66	2.6	11.8	3.0	5.8	7 ⊙	4 ⊙	0	WNW 1	SW 4	SW 1
29	118.7	118.6	119.1	118.8	11.9	19.3	10.2	12.9	19.9	5.8	65	44	74	61	4.8	12.6	3.2	6.9	8	4 ⊙	1	SW 1	SW 4	WSW 1
30	118.0	116.8	114.6	116.5	17.2	15.5	14.9	15.6	20.3	7.7	42	56	58	52	11.3	7.8	7.1	8.7	3 ⊙	9 ●	3	SSW 5	NW 2	WSW 3
31																								
M	120.3	120.0	120.5	120.3	2.6	8.3	3.8	4.6	9.9	-0.1	83	61	82	75	1.6	5.3	1.7	2.9	6.5	7.1	6.7	0.6	2.3	0.5

Zakopane — $H_s = 844$ m — $H_b = 838{,}2$ m — $h_w = 20$ m — Marzec – Mars 1957

DZIEŃ	WIELKOŚĆ ZACHMURZENIA	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	1.2	37	.	$*^0$ 0⁰⁰–3⁴⁰, 4²⁰–5³⁵, 6¹⁰, 14¹⁰ ☆⁰14²⁰–18¹⁵ $*^0$ 18³⁰–20²⁰ $*^1$–21¹⁵ $*^0$–24. = 0⁰⁰–24
2	7	0.8	37	0.4	$*^0$ 0⁰⁰–9⁴⁰ ☆⁰14¹⁰–35 $*^0$ 15¹⁰–20¹⁵ $*^1$–21¹⁰ $*^0$–23³⁰
3	6	1.4	34	0.2	$*^0$ 2¹⁵–4³⁰ 6¹⁰ $*^1$–7¹⁵ $*^0$–8⁴⁰ $*^1$–9¹⁰ $*^0$–10⁵⁰ $*^1$–11¹⁵ $*^2$–11⁴⁵ $*^1$–11⁵⁵ $*^0$–12³⁰ ☆⁰13⁵⁰–16⁴⁵ $*^0$ 18⁴⁰–21²⁵.
4	9	0.0	31	7.8	$*^0$ 22²⁰–23⁰⁵. ⌴¹ n [3.III: = 12³⁰–13⁵⁰
5	7	0.0	32	.	Δ^0 7⁵⁰–53 $*^0$–8¹⁵ Δ^1–8⁵⁰ $\bullet^0$ 12²⁰ 14¹⁰. ⌴⁰ na
6	9	.	28	9.6	⌴¹ na – /
7	7	.	25	9.6	
8	9	.	22	9.7	⌴⁰ n, np – np
9	9	.	19	7.5	⌴⁰ na, np – np
10	9	.	16	9.8	⌴⁰ na – a
11	8	.	14	9.9	⌴¹ na – a
12	7	.	12	8.1	$\oplus^0$ 10³⁰–11⁴⁰ $\oplus^2$–13¹⁵ $\oplus$–15⁰⁰
13	9	.	8	7.0	⌴² np – np
14	9	1.3	6	8.4	⌴² ¹na
15	7	3.9	pż.	1.2	$\bullet^0$ 0²⁰–32 3³⁰–6¹⁰ 9³⁵–10⁴⁰
16	6	15.4	.	.	$\bullet^0$ 2³⁰–7³⁰ $\bullet^1$–11³² $\bullet^1$–11⁵⁵ $\bullet^1$–12⁰⁸ $\bullet^1$–13¹⁵ $*^1$–16¹⁰ $*^0$–16⁴⁰ $\bullet^0$–17⁰⁷ $*^0$–17²⁵
17	7	6.3	1	.	$*^0$ 6⁰⁵–50 10⁰⁵–11¹⁰ $\bullet^1$–13⁰⁵ $\bullet^0$–14²⁰ 15⁴⁰ 17¹⁰–18³⁰
18	9	5.8	.	2.2	$\bullet^0$ 0¹⁵–3³⁰ $\bullet^1$5⁴⁰–6⁰⁵ $\bullet^0$–6³⁵ $\bullet^1$–7¹⁰ $\bullet^0$–8³⁰ ▽⁰ 13¹⁸–45, 14⁴⁰–50 ▽⁰15⁵⁰–16¹⁰, 17²⁵–18²⁵, ☇¹ 18⁰⁵–19²⁰ W–E
19	8	7.6	.	1.4	$\bullet^0$ 7¹⁵–24
20	8	.	.	4.8	$\bullet^0$ 0⁰⁰–3⁴⁵
21	8	0.1	.	4.5	$\bullet^0$ 22¹⁵–24
22	8	.	.	6.9	$\bullet^0$ 0⁰⁰–28
23	8	0.0	.	5.7	= 21²⁰–24. ⌴¹ n
24	8	0.0	.	0.1	$\bullet^0$ 3³⁰ 4¹⁵ $\bullet^0$ 6²⁵ 7³⁰ 9⁰⁸ 10³⁰. = 0⁰⁰–4⁴⁵
25	6	.	.	1.6	$\bullet^0$ 0⁴⁰–1¹⁵ 2²⁰. = 6³⁰–14¹⁵, 19³⁰–22²⁰
26	8	.	.	8.3	= 4³⁰–5³⁰ ≡²–9⁵⁰. ⌴¹ n
27	9	.	.	10.8	⌴⁰ n
28	9	.	.	10.3	⌴¹ na – /
29	8	.	.	1.8	
30	8	0.0	.	.	$\bullet^0$ 7⁴⁰ 8¹⁰
31	9	.	.	8.5	⌴⁰ np
Σ	–	43.8	–	156.1	UWAGI:

Kwiecień – Avril

1	9	.	.	11.1	⌴¹ na – /
2	9	.	.	8.5	
3	9	.	.	9.9	⌴⁰ n, np
4	9	.	.	11.6	⌴¹ na – a
5	9	.	.	11.4	⌴⁰ n – a
6	9	.	.	11.5	⌴¹ n
7	7	13.5	.	3.3	▽⁰ 12³⁵–18⁰⁵ $\bullet^0$ 18¹⁵–20¹⁵ $*^0$–24; ⌴⁰ n
8	5	4.0	9	.	$*^0$ 0⁰⁰–40 $*^2$–138 $*^1$–4²⁵ $*^0$–18²⁵
9	8	.	10	10.3	⌴⁰ na; ⌓⁰ 21³⁰–22²⁰
10	8	0.2	pż.	10.5	⌴¹ na – /
11	6	14.4	.	.	$\bullet^0$ 3⁴⁵–4⁰⁵ $\bullet^0$ 6¹⁰, 7⁴⁰ $\bullet^0$ 9²⁵–15³⁰ $\bullet^0$–16²⁰ $*^0$–20¹⁰ $*^1$–24. = 3⁴⁵–9³⁰
12	8	1.2	8	0.7	$*^1$ 0⁰⁰–15 $*^0$–24⁰ 6¹⁰...45 17⁴⁵–21³⁰. = 24⁰–8³⁰
13	6	0.8	1	2.8	Δ^0 3⁴⁰–4¹⁵ $*^0$–8³⁵ ☆⁰–9¹⁰ 9⁵⁰–10⁰⁵ 10⁴⁵–11³⁰, 12⁵⁷–13⁰⁶ 13⁴⁵–14¹⁰ ☆⁰15²⁰–40, 17³⁵–18¹⁵ ☆20²⁰–21¹⁰ $*^0$–22⁴⁰
14	7	0.3	1	2.7	☆⁰ 12¹⁰–15²⁵ 16¹²–17¹⁰
15	6	2.2	1	1.1	$*^0$ 4³⁰ 5¹⁰–6¹⁵ $*^1$–7¹⁰ $*^0$–9²⁵, 10¹⁵–45 $*^2$–11³⁰ $*^0$–12⁴⁵ 13⁰⁸–14⁰⁵ ☆⁰14²⁰–15³⁰, 15⁵⁰–16³⁰ 17²⁰–35 18⁵⁰–19²⁵
16	9	0.0	1	9.7	☆⁰ 0⁰⁰–3³⁰ [15.IV: ☆⁰ 20³⁷–24
17	6	9.2	.	.	$\bullet^0$ 6²⁵–45 ☆⁰–7⁰⁵ $\bullet^0$–7¹⁵ 9²⁵ 10¹⁰ 10¹⁵–13²⁵ 14²⁵ 15¹⁵ $*^1$15⁴³–16⁰⁵ $\bullet^0$–16⁴⁰, 20²⁰–30. = 7¹⁵–9²⁵ 16⁴⁰–20³⁰
18	6	1.6	.	.	▽⁰ 0²⁰–35 7¹⁵–25 ☆⁰ 3³⁰–4¹⁰ $*^0$–7³⁰ Δ^0–8¹⁵, 9²⁰–10⁰⁵ Δ^1–10¹⁵, 10³⁰–45 10⁵⁰–11⁰⁷ ☆⁰–12³⁵ ☆²–12⁵⁰ ☆⁰–14⁰⁷ ☆²–15¹⁸ ☆⁰–15³⁰
19	9	0.7	.	7.4	[18.IV: ☆¹–15⁴⁰ ☆⁰–16²⁰, 18²⁷–20⁴⁰
20	6	7.9	.	.	$\bullet^0$ 1²⁰–2¹⁰ $\bullet^1$–2⁵⁰ $\bullet^0$–3¹⁵ ▽⁰ 3⁴⁵–55 $\bullet^1$–4⁰⁵ $\bullet^0$ 6⁴⁵–7⁰² $\bullet^1$–7¹⁰ $\bullet^2$–7²⁰ $\bullet^0$–10²⁵ $\bullet^1$ 19³⁵–21²⁰
21	6	0.7	.	0.1	$\bullet^0$ 0³⁰–15, $\bullet^0$ 3⁴⁵ $*^0$–4¹⁵ $\bullet^0$–5³⁰ $*^0$–6¹⁰ $\bullet^0$–6²⁵ ▽⁰ 9⁵⁰–10²⁰ 12³⁵–14³⁰ $\bullet^0$ 15²⁰ 18²⁰ $\bullet^0$ 18³⁰–20²⁰
22	6	16.6	.	0.9	$\bullet^0$ 6¹⁵ 8⁰⁵ ▽¹³⁰⁷–20 ▽¹–13²⁵ ▲²–13²⁸ ▽▲⁰–13³⁰ ▽▲¹–13³³ ▽²▲²–13³⁷ ▲²–13⁴² ▽²▲²–14⁰¹ ▽¹–14³⁷ ▽⁰ 16¹⁵–23 18⁰⁵–20 ▽¹–18²⁵ ▽△¹–18⁴⁰
23	7	15.7	.	.	$\bullet^0$ 15⁴⁵–24. ≡⁰ 0⁰⁰, 1³⁰ = 19⁵⁰–24 [22.IV: ▽¹–19⁰⁵ ▽–20¹⁰ $\bullet^0$ 20¹⁵ 21⁰⁷. = 3³⁰–5³⁰ ≡²–8³⁰ ≡–15³⁰ 18¹⁵–n
24	6	3.6	.	.	$\bullet^0$ 0⁰⁰–4¹⁵ $\bullet^1$–4⁵⁰ $\bullet^0$–6¹⁰ $\bullet^1$–7²⁵ $\bullet^0$–9³⁰ 18²⁰–20²⁵ 21³⁰ 22⁵⁰. = 0⁰⁰–11⁴⁰ 12¹⁰–20³⁰
25	6	2.9	.	1.5	▽⁰ 10⁴⁵–11⁰⁵ 11³⁸–12⁵⁰ ▽¹–13⁰³ ▽⁰–13⁴⁷ 14³⁰–15²⁰ ▽²–15³⁰ ▽⁰ 17⁵⁰ $\bullet^0$ 18³⁵ 19¹⁵ 19²⁰–21³⁰. = 8²⁵–16⁴⁰
26	7	0.4	.	1.5	▽⁰ 15²⁵–30 15³⁸–16¹⁰ 19⁵⁰–20⁰⁵ 20²⁵–35 21²⁰–22¹⁵ ↙ 20²⁰–21²⁰ W
27	6	1.6	.	5.7	▽² 11⁵⁰–12⁴⁰ ☇¹ 12¹⁰–40 SSE–W–NW ▽¹☇¹–12⁵⁵ ▽⁰☇⁰–13¹⁵ SW–NW ▽⁰14⁵⁸–15⁵⁰ (☇)⁰ 15¹⁵–50 SW–NW ↙ 20¹⁰–21³⁰ SW
28	8	.	.	11.4	
29	8	.	.	7.8	
30	8	5.2	.	6.5	▽¹ 10⁴⁵–56 ▽⁰ 11⁵⁰–14¹⁰, 15⁴⁰–45 ▽²–15⁵² ▽⁰–16¹⁰, 16²⁸–35, 17⁵⁵–18¹⁰ ▽²–18²⁰; ☇⁰ 18¹⁰–25 SW–S
31					
Σ	–	102.7	–	147.9	UWAGI: *W kwietniu wartości ciśnienia atmosferycznego wynoszą 800 mb + wartości podane w tablicy.*

Zakopane — φ = 49°18' — λ = 19°57' — Maj – Mai 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	19.0	19.2	18.3	18.8	2.8	3.3	3.0	3.0	14.9	2.1	80	84	68	77	1.5	1.2	2.4	1.7	10	10	9	NW 2	NE 2	E 3
2	16.2	15.8	14.8	15.6	1.4	2.0	2.0	1.8	3.4	1.0	96	96	93	95	0.3	0.3	0.6	0.4	10 ●	10 ●	10	NE 3	NE 3	NE 1
3	13.8	14.4	14.8	14.3	1.8	4.0	3.8	3.4	4.3	1.3	96	92	88	92	0.3	0.6	1.0	0.6	10 ●	10 ●	10	NE 1	ENW 1	SW 2
4	13.7	14.3	16.5	14.8	6.0	9.0	4.2	5.8	10.0	0.7	70	57	89	72	2.9	5.0	0.8	2.9	7 ⊙	8	10 ●	WSW 1	NW 3	WSW 1
5	17.5	15.0	13.7	15.4	0.6	6.4	0.4	2.0	7.1	−0.2	78	47	92	72	1.5	5.1	0.5	2.4	8	9	10 ✳	WNW 3	NW 3	W 1
6	11.2	11.7	12.5	11.8	0.7	1.1	−0.3	0.3	3.1	−0.6	92	91	96	93	0.5	0.6	0.3	0.5	10	10 ✳	10 ✳	C 0	W 2	N 1
7	9.7	9.6	9.3	9.5	−1.7	−0.5	−0.8	−1.0	0.6	−2.1	94	92	95	94	0.3	0.5	0.3	0.4	10 ✳	10 ✳	10	NNW 1	E 1	C 0
8	8.6	9.5	12.0	10.0	−0.3	0.7	−0.4	−0.1	1.2	−1.4	94	92	96	94	0.4	0.5	0.2	0.4	10 △	10 ✳	10 ✳	C 0	E 1	ENE 1
9	12.6	13.1	13.4	13.0	−0.4	1.1	0.5	0.4	2.9	−1.9	96	85	96	92	0.2	1.0	0.2	0.5	10 ✳	10 ✳	10 ✳	SSE 1	N 1	N 1
10	12.1	12.8	16.2	13.7	1.1	2.3	1.9	1.8	3.7	0.2	94	95	94	94	0.4	0.4	0.4	0.4	10 ● ✳	10 ●	10 ●	SW 1	SW 2	C 0
11	18.4	20.1	20.8	19.8	3.0	8.9	5.4	5.7	13.6	0.6	93	68	79	80	0.6	3.7	1.9	2.1	10	8 ⊙	3	C 0	NE 2	C 0
12	21.9	22.9	23.2	22.7	7.0	12.9	6.1	8.0	16.0	0.6	79	52	81	71	2.1	7.2	1.7	3.7	5 ⊙	9 ⊙	0	C 0	W 1	SSW 2
13	23.2	22.2	22.3	22.6	8.5	16.3	8.9	10.6	16.9	1.0	70	41	74	62	3.4	10.8	2.9	5.7	1 ⊙	6	4	SW 2	ENE 3	SW 2
14	22.4	23.9	26.1	24.1	11.0	13.1	8.9	10.5	17.6	3.9	72	65	86	74	3.7	5.2	1.6	3.5	1 ⊙	10● ⛈	4	C 0	NE 3	C 0
15	26.6	26.1	25.3	26.0	8.7	15.5	8.7	10.4	17.0	3.8	86	54	86	75	1.5	8.1	1.5	3.7	10	8	0	SW 1	E 2	C 0
16	23.6	21.2	19.9	21.6	10.1	18.4	10.0	12.1	19.4	3.5	80	46	80	69	2.5	11.5	2.4	5.5	3 ⊙	8 ⊙	4	C 0	N 2	SW 1
17	19.3	19.2	21.3	19.9	11.0	16.7	11.5	12.7	17.6	4.6	81	62	88	77	2.5	7.4	1.8	3.9	6 ⊙	9	10	WSW 1	N 3	W 2
18	21.1	20.5	17.8	19.8	9.8	15.4	12.2	12.4	16.6	8.8	88	59	84	77	1.5	7.3	2.3	3.7	10	7	10 ●	SE 1	NE 3	C 0
19	13.9	12.4	12.2	12.8	14.2	18.4	11.4	13.8	19.4	6.7	67	55	84	69	5.2	9.6	2.2	5.7	1 ⊙	6 ⊙	1	N 1	NE 4	C 0
20	13.3	14.6	17.2	15.0	11.3	15.9	9.7	11.6	16.7	5.0	85	59	93	79	2.1	7.6	0.8	3.5	7	9	10 ●	C 0	NW 1	WSW 1
21	19.6	20.3	20.4	20.1	7.5	6.4	5.3	6.1	10.1	4.9	94	95	92	94	0.6	0.4	0.7	0.6	10 ●	10 ●	10 ● ≡	W 1	NE 2	C 0
22	17.9	17.5	17.2	17.5	4.6	6.5	7.5	6.5	7.8	3.8	93	92	96	94	0.6	0.8	0.5	0.6	10 ●	10	10	C 0	C 0	C 0
23	16.2	16.1	16.3	16.2	9.5	14.1	9.6	10.7	15.4	6.1	90	79	95	88	1.2	3.5	0.7	1.8	10	9 ●	1	SW 1	NNE 2	C 0
24	16.5	18.0	19.5	18.0	10.5	13.4	11.7	11.8	15.8	5.1	95	84	84	88	0.7	2.6	2.2	1.8	9	10	9	C 0	SE 1	C 0
25	21.4	22.6	24.0	22.7	5.6	6.8	4.8	5.5	11.7	4.5	92	61	65	73	0.7	3.8	3.0	2.5	10	10	9	NE 4	NE 4	E 2
26	24.0	24.3	24.4	24.2	4.0	4.9	3.2	3.8	5.5	0.8	47	55	70	57	4.2	3.9	2.3	3.5	9	10	8	E 5	NE 5	NE 4
27	22.4	23.0	23.3	22.9	0.6	1.8	1.5	1.4	3.4	0.0	90	93	91	91	0.6	0.6	0.6	0.6	10 ✳	10 ● ✳	10	E 2	NE 2	NE 2
28	21.3	21.4	20.4	21.0	1.5	2.9	2.9	2.6	3.8	0.4	86	77	87	83	0.9	1.7	0.9	1.2	10	10	10 ●	E 1	E 1	NNE 2
29	21.2	22.9	24.6	22.9	1.8	6.0	1.8	2.8	8.1	1.1	96	80	88	88	0.3	1.9	0.8	1.0	10 ● ✳	6	1	NE 1	SE 2	SW 1
30	26.0	26.1	25.4	25.8	6.6	11.0	6.6	7.7	12.6	−2.5	57	41	72	57	4.1	7.7	2.7	4.8	1 ⊙	9	8	C 0	WNW 4	SW 1
31	24.8	23.2	21.5	23.2	7.3	13.2	9.3	9.8	14.1	−0.2	64	43	72	60	3.7	8.6	3.3	5.2	1	8	9	SW 1	NW 2	SW 1
M	18.4	18.5	18.9	18.6	5.4	8.6	5.5	6.2	10.7	2.0	84	71	86	80	1.6	4.2	1.4	2.4	7.7	9.0	7.4	1.1	2.2	1.0

Czerwiec – Juin

1	21.2	21.7	22.6	21.8	9.3	14.2	8.5	10.1	16.2	6.6	76	41	81	66	2.8	9.7	2.2	4.9	9	9	4	C 0	N 1	SW 1
2	24.1	24.7	26.0	24.9	12.1	18.1	12.0	13.6	19.8	6.3	66	42	77	62	4.7	12.1	3.2	6.7	4 ⊙	7 ⊙	3	SW 3	WNW 2	SE 1
3	26.5	25.7	23.3	25.2	14.1	20.7	15.9	16.6	21.7	4.9	71	41	53	55	4.6	14.4	8.6	9.2	0	7 ⊙	2	SW 1	SE 2	SW 2
4	20.2	20.1	17.5	19.3	18.1	17.8	15.2	16.6	19.7	12.6	54	59	80	64	9.6	8.2	3.6	7.1	8 ⊙	10	10	SW 5	SW 3	C 0
5	14.1	16.2	14.1	14.8	14.9	9.5	7.9	10.0	15.6	7.4	67	93	88	83	5.5	0.9	1.2	2.5	8 ⊙	10 ●	1	SW 4	WSW 2	SW 1
6	15.2	16.5	19.1	16.9	9.5	13.5	6.1	8.8	14.1	5.3	84	44	73	67	2.0	8.7	2.6	4.4	9	7 ⊙	0	W 2	WSW 6	SW 2
7	19.3	18.0	17.8	18.4	11.7	18.7	16.6	15.9	19.7	1.4	61	43	51	52	5.3	12.3	9.4	9.0	5 ⊙	5 ⊙	10	N 1	W 5	SSE 4
8	18.5	18.6	18.9	18.7	13.0	18.5	13.1	14.4	21.5	9.2	87	69	88	81	2.0	6.6	1.8	3.5	7 ⊙	9	6	SW 2	E 1	W 1
9	18.1	18.6	18.7	18.5	18.3	21.1	14.6	17.2	22.0	10.1	52	46	70	56	9.9	13.5	5.0	9.5	4	6 ⊙	8	N 4	S 5	SW 1
10	17.6	18.4	19.6	18.5	14.6	19.0	17.7	17.2	21.4	10.5	89	52	59	67	1.9	10.4	8.1	6.8	9	8	3	NNW 2	S 7	SW 4
11	18.9	18.2	20.1	19.1	21.2	25.9	23.2	23.4	26.6	12.3	52	35	46	44	12.3	21.7	15.2	16.4	5 ⊙	9 ⊙	10	SSW 9	S 9	SE 7
12	24.6	26.7	31.6	27.6	20.2	27.5	16.0	19.9	27.6	14.5	68	45	82	65	7.6	20.0	3.3	10.3	7	10	10● ⛈	SW 1	N 3	NE 1
13	33.5	33.0	32.1	32.9	13.7	16.4	13.3	14.2	19.7	12.8	95	88	94	92	0.7	2.4	1.0	1.4	10 ●	10	7	C 0	NE 3	WSW 1
14	30.8	30.7	31.3	30.9	11.5	17.6	9.7	12.1	18.1	3.7	74	50	87	70	3.5	9.9	1.6	5.0	1 ⊙	0 ⊙	0	NE 2	NE 4	C 0
15	30.3	30.2	28.7	29.7	12.3	18.1	9.7	12.4	18.8	4.1	61	33	81	58	5.6	13.9	2.2	7.2	1	3 ⊙	1	NE 2	E 3	C 0
16	27.1	26.0	25.0	26.0	13.2	20.2	12.7	14.7	21.3	3.0	58	46	78	61	6.4	12.7	3.3	7.5	0 ⊙	1	0	C 0	NE 3	NE 1
17	24.1	23.8	23.0	23.6	14.8	20.9	13.3	15.6	21.9	4.5	63	47	79	63	6.2	13.3	3.2	7.6	0 ⊙	3 ⊙	1	N 1	NE 4	NE 1
18	22.3	21.4	20.1	21.3	15.7	21.8	15.5	17.1	23.2	7.5	72	50	82	68	5.0	13.3	3.3	7.2	1	6 ⊙	7	C 0	NNE 3	SW 1
19	19.3	19.6	18.8	19.2	13.5	11.3	12.9	12.6	19.9	9.8	94	96	89	93	0.9	0.5	1.7	1.0	10	10● ⛈	8	SW 1	SW 2	SSW 2
20	19.4	19.3	21.5	20.1	17.0	19.4	14.9	16.6	21.5	10.4	72	68	89	76	5.4	7.1	1.9	4.8	2 ⊙	9	10	SW 1	WNW 4	C 0
21	22.7	21.3	19.6	21.2	12.1	19.1	14.8	15.2	20.6	7.8	90	62	88	80	1.4	8.4	2.1	4.0	10	9 ⊙	10	C 0	N 2	SSW 1
22	16.9	15.1	13.6	15.2	16.7	23.2	15.5	17.7	24.3	10.5	80	55	84	73	4.0	12.8	2.9	6.6	4 ⊙	3 ⊙	9	C 0	SW 5	W 3
23	17.3	18.0	16.9	17.4	17.3	21.6	14.5	17.0	23.5	7.8	67	46	78	64	6.6	14.0	3.7	8.1	1 ⊙	8	9	SE 2	SW 3	SW 1
24	16.3	13.9	11.4	13.9	18.3	24.2	23.1	22.2	25.3	11.0	76	45	47	56	4.9	16.6	15.0	12.2	6 ⊙	7 ⊙	4	SE 1	S 14	SSW 7
25	16.0	17.8	22.1	18.6	15.6	18.7	12.5	14.8	23.3	12.1	63	49	74	62	6.6	11.1	3.8	7.2	1 ⊙	2 ⊙	10 ●	W 3	NNW 6	NW 1
26	23.4	24.5	27.0	25.0	7.9	11.0	8.5	9.0	12.8	6.4	92	62	81	78	0.8	5.0	2.2	2.7	10 ●	9	8	WSW 1	N 2	W 1
27	28.4	28.6	30.6	29.2	10.7	13.1	7.7	9.8	14.3	2.7	57	53	81	64	5.6	7.0	2.0	4.9	2 ⊙	8	9	SSW 1	W 2	C 0
28	30.7	29.7	29.8	30.1	11.5	18.3	13.5	14.2	20.1	3.1	54	37	81	57	6.2	13.3	3.1	7.5	2 ⊙	3 ⊙	8	C 0	WNW 2	C 0
29	29.8	29.7	29.3	29.6	17.6	22.7	15.9	18.0	24.6	9.3	76	44	85	68	4.6	15.3	2.8	7.6	4 ⊙	8 ⊙	3	SW 1	NE 2	C 0
30	28.6	27.6	27.5	27.9	18.7	24.9	16.2	19.0	26.2	11.8	74	46	70	63	5.8	17.0	5.4	9.4	1 ⊙	5 ⊙	3	SW 1	NW 1	C 0
31																								
M	22.5	22.4	22.6	22.5	14.5	18.9	13.7	15.2	20.8	8.0	72	53	77	67	4.9	11.1	4.2	6.7	4.7	6.7	5.8	1.7	3.7	1.5

Zakopane $H_s = 844\ m$ $H_b = 838{,}2\ m$ $h_w = 20\ m$ **Maj – Mai 1957**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	8	3.9	.	.	●⁰0³⁰–1²³ ●¹–1⁵⁰ ●⁰–3⁵⁵ 7⁵⁰–12³⁰ 23⁵⁰–24
2	5	1.2	.	.	●⁰0⁰⁰–10 ✱⁰–1⁴⁵ ●⁰–4⁰⁵ ●⁰–8³⁰ 9²⁵–18⁴⁰ ●⁰21¹⁵–24 = 18⁰⁰–24
3	7	2.0	.	.	●⁰0⁰⁰–30 3³⁰–7¹⁵ ●⁰–9²⁰ 9⁴⁰–10³⁵ ●¹12³⁰–13⁵⁰ ●⁰–15¹⁰ ●¹–16¹⁰ ●⁰–17⁰⁵
4	8	2.1	.	4.8	▼¹15⁵⁵–16⁰⁰ ▼⁰–16⁰⁵ ▼¹17⁰⁸–18 ▼⁰–18⁰⁵ 20³⁰–21⁰⁸
5	8	3.5	.	2.1	●⁰19¹⁰–40 ✱⁰–21²⁵ △⁰–23²⁰
6	6	6.1	.	.	●✱⁰9²⁰–11⁰² ✱⁰–12³⁰ ✱¹–13⁴⁰ ✱⁰–16¹⁵ ✱⁰–17²⁵ ●✱⁰–18¹⁰ ✱⁰–24; = 0³⁰–3³⁰, 5³⁰–24
7	5	11.4	6	.	✱⁰0⁰⁰–6³⁰ ✱¹–7⁴⁵ ✱⁰–11²⁰ ✱¹–13⁵⁰ ✱⁰–13⁵⁵ 14²⁰–17¹⁰ 20¹⁰; = 0⁰⁰–24
8	5	16.6	10	.	△⁰0¹⁵–12²⁰ ✱⁰–15³⁰ △⁰–18¹⁰ ✱⁰–21²⁵ 22³⁰–24
9	6	3.3	15	.	✱⁰0⁰⁰–15 ✱¹–2⁴⁵ ✱⁰–5¹⁰ ✱¹–6⁰⁵ ✱⁰–21³⁰ △⁰–22²⁵; = 22²⁵–24
10	6	4.5	10	.	●²2¹⁰–3⁴⁵ △⁰–6⁰⁵ ✱⁰–6¹² ✱⁰–7³⁰ ●⁰8¹⁰–9³⁰ 10⁴⁵ 11¹⁰, 11¹⁵–16³⁰, 17⁰⁷ 18⁰⁵ 18¹⁰–20 ●⁰–22⁴⁰ ●⁰–24; = 0⁰⁰–2¹⁰, 12²⁵–24
11	7	.	.	3.8	●⁰0¹⁵–2³⁰ 3⁰⁵–4¹⁰ ●⁰–4³⁰; = 6⁵⁰–9³⁰
12	8	.	.	6.6	⌒⁰ r – nr
13	9	.	.	8.7	(K)⁰ 14¹⁰–40; ⌒⁰ na – a, III
14	7	2.9	.	7.7	▼⁰12³⁵–42 ▼²–12⁵² ▼⁰–13¹⁰; K⁰ 12³⁵–13²⁵ E-S; ⌒¹ r
15	8	.	.	4.8	⌒² r ⌒⁰ r – nr
16	8	.	.	11.1	⌒² r, r – nr
17	8	0.0	.	4.3	▼⁰17⁵⁵–18¹⁰ (K)⁰ 13³⁰–15⁵⁰ SW-E-SE K⁰ 17³⁸–18⁴⁰ SW-NW-W; ⌒² na – a
18	8	0.4	.	2.7	▼⁰20³⁵–21²⁰; = 3³⁰–11²⁰
19	9	0.5	.	7.9	▼⁰12¹³–15 ▼²14⁰⁸–11 ▲¹–14¹² ▼⁰–14¹⁷ ▼¹16²⁸–31 (K)⁰13¹⁸–14⁰⁸W K–14³⁰ (K)⁰–14⁴⁵E; ⌒² r, ⌒¹16²⁹–38 18³⁶–19⁰⁵
20	8	25.1	.	1.7	▼⁰9¹³–20 ▼²9³⁰ ▼⁰10⁰⁵ 18⁴⁵–19¹⁵ ▼²19³³ ▼¹–20¹⁵ ▼⁰–21¹⁰ ▼²21⁵⁰–22⁰² ▼¹–22⁰⁵ ▼⁰–22²³ ▼¹–22⁵⁰ ▼²–23¹⁰ ▼¹–24
21	6	2.8	.	.	▼¹0⁰²,¹⁰⁰ ▼⁰–1⁴⁵ ▼¹–2³⁰ ●¹–3³⁰ ●¹–4²⁰ ●⁰–5²⁰ ●¹–6⁰⁰ ●⁰–10³⁰ ●⁰–15³⁰ 18²⁰ 20³⁰ ●¹–21²⁰ ●¹–22⁰⁵ ●⁰–24; =²r–21⁴⁰
22	6	0.3	.	.	●⁰0⁰⁰–07 ●⁰–0⁵⁵ ●⁰–1⁵⁰ ●⁰–2¹⁰ ●⁰–8⁴⁵ ●⁰–8⁵⁵ ●⁰–9³⁰ ●⁰10¹⁰–13 ●⁰10²⁵–11²⁰ ●⁰12²⁸–32 ●⁰23³⁰–40; = 0⁰⁰–24
23	7	3.6	.	2.4	▼⁰12³⁵–13³⁷ ▼¹–13⁵⁰ ▼⁰–14⁴⁰ ▼¹14⁵⁰–15²⁰ ▼⁰–15⁴⁰; = 0⁰⁰–4³⁰, 6³⁰–7¹⁰
24	7	1.3	.	0.6	▼⁰16¹⁸–22 ●⁰21⁰⁵–22⁰⁷ 23¹⁸–24 **20.V:** (K)⁰7⁴⁵–9³⁰ S-E K–9⁵⁰ (K)⁰14⁵⁰–16¹⁵ S-W; ⌒¹ r
25	8	.	.	.	●⁰0⁰⁰–07 ●⁰1¹⁷–2⁴⁵, 3³⁵ ●¹–5⁰⁵ ●⁰–6⁰⁵
26	9	0.0	.	2.2	⌒² r
27	6	2.3	.	.	✱⁰5²⁰–9³⁰ ✱⁰–13¹⁰ ●⁰ 13²⁰ ✱¹14⁰³–35 16⁰⁵–20 ●⁰17⁰⁵–12 ●⁰–18¹² ✱⁰–18¹⁴ ✱¹–18¹⁶ ✱⁰–18²³; = 5³⁰–15⁵⁰ 16¹⁵–18³⁰, **21.V:** 19³⁰–24
28	7	2.2	.	.	●⁰20³⁵–21⁰⁵ ●¹22⁴⁹–23⁰⁰ ●⁰–23¹⁸ 23⁵⁰–24; = 20³⁰–24
29	8	1.8	.	2.7	●⁰0⁰⁰–17 10⁴–15 ●¹–1³⁰ ●⁰–2²⁵, 2⁴⁰ 3¹⁷–6²⁵ ✱⁰–7¹⁵ ✱¹–7⁴⁰ ✱⁰–9¹⁵ ✱⁰–9²⁵ △¹10²⁰–28; = 0⁰⁰ 3³⁰ 5²⁰–9⁰⁰
30	9	.	.	4.7	⌴² r
31	8	.	.	4.4	⌴⁰ r ⌒² r
Σ	–	97.8	–	83.2	UWAGI:

Czerwiec – Juin

1	8	.	.	4.4	⌒⁰ na
2	7	.	.	10.2	⌒⁰ nr
3	7	.	.	8.0	⌒¹ r
4	8	0.0	.	3.6	▼⁰15²⁵–28 ●⁰22⁵⁰–23⁰²
5	7	8.8	.	2.2	▼⁰9⁵⁸–10⁰⁵ ▼²–10¹¹ ▼⁰–10⁴⁸ ▼¹–11¹⁵ ▼⁰–12⁵⁰ ▼¹–13⁴⁰ ▼⁰–14⁰³
6	7	.	.	4.6	●⁰10⁸–13 ●¹–2²³ ●⁰–2⁴³ ●¹–2⁴⁸ ●⁰2⁴⁹–3¹⁵
7	9	2.0	.	11.6	⌴⁰ r ⌒¹ r – a
8	8	0.9	.	5.9	▼¹12⁰–20⁸ ▼⁰–22⁵ ▼¹22⁸–31 ▼⁰–12⁴⁰ ▼²–12⁴⁵ ▼–12⁴⁸, 17⁴⁰–44 ▼¹–17⁴⁸ ▼⁰–18⁰⁰ ▼¹–18⁰⁴ ▼⁰–18⁰⁸ (K)⁰ 10⁸–55 NW
9	8	11.5	.	8.1	▼⁰18²⁵–50; (K)⁰ 23³⁰–24 S **8.VI:** 14¹⁰–17⁴⁵ N, NW-NE
10	8	0.0	.	6.3	▼²0³⁰–2⁰⁵ ▼¹–3¹⁰ ▼⁰–3⁵⁰ 9⁴⁷–10¹⁰; (K)⁰ 0⁰⁰–15 S K¹⁻² 0¹⁵–0⁴⁰–2¹⁵ S–NE
11	9	.	.	9.3	≫ 7³⁰–18⁰⁰ S
12	7	7.8	.	4.0	▼⁰14²⁰–15⁰⁰ ▼¹–16²⁰ ▼⁰–18⁴⁰ ▼¹–10⁴⁰ ▼⁰–21⁴⁵; (K)¹14⁰⁷–55 SE-S-SW K¹–18³⁰ (K)⁰–22³⁰ N-E-SE; ⌒⁰20²⁰–32; ⊕¹8⁴⁵–12¹⁰
13	6	0.1	.	0.3	●¹5⁵²–57 ●⁰ 6⁰³ ●⁰–9⁰⁵ 16⁴⁵–18²⁵; = 4³⁰–9³⁰, 11⁵⁰–21¹⁰; ⌒¹ r
14	9	.	.	13.0	⌒² na – a ⌒⁰ III – r
15	9	.	.	12.9	⌒¹ na – a
16	9	.	.	13.0	⌒² r ⌒¹ nr
17	9	.	.	12.9	⌒² na – a
18	8	4.4	.	9.4	▼⁰15¹⁸–23 15⁴⁵–55 ▼²16⁰⁸ ▼⁰–16¹⁵ ▼²16³⁸–42 ▼⁰–16⁵⁰ 17³⁰–40 ▼²–17⁵² ▼⁰–18¹⁰ 19¹⁰–21¹⁵; (K)⁰ 16¹²–20 SE-S K⁰16²⁰–30 SW-W (K)–18⁴⁵
19	5	42.3	.	1.6	▼⁰4⁵⁰–5⁰⁵ ●⁰5²⁰–7³⁵ ▼²K¹12⁴⁰–13⁴⁰ SW-N-SE ▲¹12.7–45 (⌀ 4 mm) ▼¹3⁴⁰–14¹⁵ ▼⁰–14³⁰ ▼²20¹²–²⁸ ▼²–20⁴⁵ ▼⁰–21¹⁹
20	7	.	.	4.6	(K) 14⁵⁵–15¹⁵ W 15²⁵–16¹⁵ SW-S **18.VI:** SE-NW (K)⁰18⁵²–21³⁵ W-SW-S-SW-W; ⌒²na; ⌒² 17⁴⁵–56 (nadwdina)
21	7	(0.0)	.	3.8	●⁰22⁵⁰–23⁰⁵; ⌒² r
22	9	1.5	.	8.7	▼⁰18⁵⁵–20⁰¹ ▼¹–20¹² ▼⁰–20³⁰, 21¹⁹–23; (K)⁰ 18⁴⁰ SW K¹18⁵⁵–20⁴⁰ SW-N-E (K)⁰ 21¹⁷–35 W-S-SE; ⌒⁰ r, 1
23	9	0.4	.	7.4	▼⁰17⁴⁰–18⁰⁵; ⌒¹ na – a, r – nr
24	9	3.9	.	9.9	●⁰3⁴⁰–5¹⁰; < 1³⁰ SW; ≫ 10³⁰–14³⁰ (nar. do 20 m/sek)
25	9	9.8	.	12.2	▼²0⁰⁰–15 ▼¹0²⁰ ▼⁰–0²⁵ ●⁰21³⁰..45–22³⁷ ●¹–23²⁵ ●²–23³⁵ ●¹–24; K²0²⁵–30 S-N; ≫ 0⁰⁵–30 S (nar. do 20 m/sek)
26	7	0.3	.	0.3	●¹0⁰⁰–25 ●⁰–0⁴⁰ 2⁰⁵, 4⁰⁸–5⁵⁰, 6⁴⁵ 8¹⁰
27	8	.	.	5.8	⌒¹ r
28	9	.	.	12.8	⌒⁰ nr
29	8	.	.	9.5	
30	7	.	.	9.4	⌒¹ r
31					
Σ	–	93.7	–	223.7	UWAGI:

Zakopane — φ = 49°18' — λ = 19°57' — Lipiec – Juillet 1957

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	26.5	25.7	25.5	25.9	19.3	25.5	17.1	19.8	26.8	10.5	62	40	82	61	8.6	19.6	3.6	10.6	3 ⊙	3 ⊙	1	C 0	NE 2	C 0
2	24.6	22.9	23.9	23.8	19.9	26.5	15.5	19.4	27.4	12.0	71	36	89	65	6.7	22.2	2.0	10.3	1 ⊙	8(R)	10	SW 1	WSW 4	SW 1
3	25.4	25.6	25.6	25.5	14.8	19.4	12.7	14.9	21.6	12.2	94	55	88	79	0.9	10.0	1.8	4.2	10 ●	4 ⊙	0	N 1	NE 1	C 0
4	25.3	25.2	25.7	25.4	17.3	25.0	19.0	20.1	27.0	7.4	67	42	69	59	6.5	18.3	6.8	10.5	5 ⊙	3 ⊙	1	SW 1	NW 1	SW 1
5	26.0	24.6	24.5	25.0	20.1	30.6	22.2	23.8	31.8	10.7	66	23	56	48	8.0	33.7	12.0	17.9	0 ⊙	1 ⊙	2	C 0	W 5	SW 3
6	25.8	26.4	26.8	26.3	21.1	25.3	18.3	20.8	26.2	14.8	72	62	88	74	7.0	12.3	2.3	7.2	0 ⊙	3 ⊙	1	C 0	NW 3	C 0
7	26.6	26.4	26.5	26.5	18.6	26.3	19.0	20.7	28.4	13.0	74	41	79	65	5.5	20.2	4.5	10.1	10 (R)	4 ⊙	0	N 2	SW 1	SW 1
8	25.5	24.7	22.4	24.2	21.7	28.1	22.1	23.5	31.0	14.0	78	42	65	62	5.8	22.2	9.3	12.4	0 ⊙	5 ⊙	9	C 0	ENE 2	SW 1
9	21.2	21.3	20.7	21.1	17.1	19.2	15.8	17.0	25.3	15.4	94	84	91	90	1.3	3.5	1.6	2.1	6 ⊙	10 ● R	1	SW 2	NNW 3	C 0
10	19.0	16.7	14.6	16.8	16.7	27.6	14.5	16.8	21.9	11.6	86	60	96	81	2.8	10.2	0.7	4.6	8 ⊙	8 ⊙	10 ●	NW 1	E 4	C 0
11	11.0	11.9	13.1	12.0	14.5	19.5	16.1	16.6	20.7	10.2	89	69	94	84	1.9	7.0	1.2	3.4	7	10 ●	9	WSW 1	ESE 1	E 1
12	13.8	15.5	17.7	15.7	14.9	18.7	15.9	16.4	19.4	13.6	94	76	96	89	0.9	5.2	0.8	2.3	10	10 ●	10	C 0	C 0	C 0
13	20.8	22.0	23.7	22.2	15.9	18.5	16.5	16.8	18.8	14.8	92	79	95	89	1.5	4.4	1.0	2.3	10	9	10 ●	NE 1	N 2	SSW 1
14	22.4	22.9	20.6	22.0	17.6	15.9	14.1	15.4	19.8	13.8	87	95	93	92	2.5	1.1	1.2	1.6	7 ⊙	10 ● R	6	C 0	SW 1	SW 2
15	19.3	19.3	18.5	19.0	13.5	15.1	14.5	14.4	16.6	10.7	95	92	97	95	0.7	1.4	0.6	0.9	10	10	10	C 0	SW 1	C 0
16	13.8	12.6	16.3	14.2	13.2	13.9	9.9	11.7	15.3	9.5	96	91	92	93	0.6	1.5	1.0	1.0	10	10 ●	10 ●	C 0	NNE 4	WSW 3
17	15.1	17.0	18.5	16.9	10.4	11.1	11.1	10.9	15.4	8.7	93	92	90	92	0.9	1.0	1.4	1.1	10 ●	10 ●	10	W 3	SW 2	WSW 1
18	18.7	19.0	18.2	18.6	12.5	13.4	11.1	12.0	17.8	9.4	78	78	82	79	3.3	3.4	2.3	3.0	9	9	1	WSW 4	SW 2	SW 1
19	17.5	16.6	16.3	16.8	12.4	20.0	16.7	16.4	20.9	5.6	74	52	64	63	3.8	11.4	6.9	7.4	1 ⊙	7 ⊙	7	SW 1	SSE 3	C 0
20	14.0	13.1	11.8	13.0	18.9	21.6	14.1	17.2	22.1	11.6	57	51	93	67	9.5	12.6	1.2	7.8	6 ⊙	9	10	S 4	SSW 2	C 0
21	10.6	11.4	11.6	11.2	12.1	12.4	12.0	12.1	14.4	11.2	90	90	90	90	1.4	1.5	1.4	1.4	10	10 ●	10	W 2	W 3	SW 1
22	9.5	9.3	10.2	9.7	11.1	13.1	11.1	11.6	15.9	7.5	91	85	94	90	1.2	2.4	0.8	1.5	9	10 ●	10 ●	S 1	NW 1	SW 1
23	8.5	10.4	12.6	10.5	10.2	12.5	12.5	11.9	15.4	6.9	93	93	94	93	0.8	1.1	0.9	0.9	9	10 ●	10	C 0	W 1	C 0
24	13.6	16.2	18.6	16.1	13.1	12.6	10.9	11.9	13.6	10.5	89	94	93	92	1.7	0.9	0.9	1.2	10 ●	10 ●	10 ●	SW 1	SW 3	W 1
25	18.8	19.0	18.0	18.6	10.7	14.4	12.6	12.6	15.9	7.3	92	68	90	83	1.1	5.3	1.5	2.6	9	10	10	SW 1	W 2	WSW 1
26	17.7	18.5	17.8	18.0	12.5	16.4	13.7	14.1	18.7	11.5	80	49	82	70	3.0	9.5	2.9	5.1	10	6 ⊙	10 ●	WSW 4	WNW 5	C 0
27	14.7	14.2	14.2	14.4	17.2	18.1	12.5	15.1	19.3	11.5	58	53	94	68	8.3	9.8	0.9	6.3	9	10	10 ●	SW 4	WSW 7	C 0
28	14.7	15.2	16.8	15.6	9.8	15.0	11.0	11.7	16.0	9.0	88	60	81	76	1.5	6.8	2.5	3.6	10	7 ⊙	6	SW 1	WNW 3	SW 2
29	17.7	18.8	21.6	19.4	11.2	16.9	8.9	11.5	18.4	4.7	72	57	90	73	3.8	8.3	1.1	4.4	2 ⊙	7	0 ⊙	W 1	W 4	C 0
30	22.3	23.1	25.0	23.5	10.4	16.0	12.7	13.0	17.6	5.5	87	66	82	78	1.7	6.2	2.7	3.5	9	8	9	C 0	WSW 1	C 0
31	26.3	27.5	29.2	27.7	11.7	15.2	13.6	13.5	16.9	11.0	68	73	81	81	1.7	4.6	3.1	3.1	10	9	10	SW 2	W 2	ENE 1
M	18.9	19.1	19.6	19.2	14.9	18.6	14.4	15.6	20.5	10.5	82	66	86	78	3.4	9.0	2.6	5.0	7.1	7.7	6.9	1.3	2.5	0.7

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1	29.0	28.9	28.0	28.6	11.7	16.2	12.8	13.4	17.8	10.6	92	71	93	85	1.0	5.2	1.1	2.4	10	10	8	NE 1	ENE 1	C 0
2	27.3	26.2	26.8	26.8	12.4	19.3	14.5	15.2	20.4	6.9	93	60	82	78	1.1	9.0	3.0	4.4	0 ⊙	4	8	C 0	NNW 2	N 1
3	26.3	25.4	26.1	25.9	10.6	15.3	11.4	12.2	15.7	10.0	75	51	79	68	3.3	8.5	2.9	4.9	8	2	10	NE 1	N 3	WNW 1
4	25.4	26.1	27.1	26.2	10.5	14.8	11.9	12.3	17.0	9.2	82	62	84	76	2.3	6.3	2.2	3.6	9	8	9	N 1	NE 1	NNW 1
5	26.7	27.5	27.7	27.3	12.3	14.9	12.1	12.8	16.9	7.7	77	65	94	79	3.3	5.8	0.9	3.3	2 ⊙	8	8	C 0	SW 1	N 1
6	27.4	26.9	25.6	26.6	11.7	18.2	11.5	13.2	20.1	5.6	85	55	90	77	2.0	9.4	1.4	4.3	1 ⊙	7 ⊙	2	C 0	NNE 2	C 0
7	23.8	21.4	18.8	21.3	13.1	20.3	14.4	15.6	21.7	7.5	79	57	86	74	3.2	10.1	2.4	5.2	7	8 ⊙	10	C 0	NNW 1	C 0
8	16.6	16.7	17.2	16.8	14.9	17.9	11.9	14.2	18.3	11.1	84	62	85	77	2.8	7.7	2.0	4.2	8	8	5	NNW 4	WNW 3	SW 1
9	16.0	15.1	12.6	14.6	12.0	20.3	14.0	15.1	21.5	6.2	88	62	87	79	1.7	8.9	2.1	4.2	7 ⊙	8 ⊙	1	C 0	NE 2	C 0
10	9.3	13.5	17.3	13.4	19.9	17.8	13.5	16.2	23.1	11.0	63	66	75	68	8.4	7.0	3.9	6.4	6	10	1	SW 5	WSW 8	SW 2
11	21.2	21.8	21.6	21.5	14.4	23.4	17.5	18.2	25.6	10.5	74	55	72	67	4.3	12.9	5.7	7.6	5 ⊙	6	1	C 0	NE 2	C 0
12	18.7	18.7	20.1	19.2	22.0	26.3	18.0	21.1	26.8	13.4	49	43	84	59	13.6	19.5	3.1	12.1	1 ⊙	6 ⊙	3	S 1	WSW 3	SE 1
13	20.9	21.8	20.9	21.2	17.7	23.6	16.0	18.3	24.5	14.8	87	54	94	78	2.5	13.1	1.3	5.6	2	8 ⊙	2	C 0	NE 1	C 0
14	18.1	18.6	16.5	17.7	17.2	26.5	22.7	22.3	26.8	12.4	88	52	59	66	2.5	16.7	11.2	10.1	0 ⊙	1 ⊙	10	SE 1	N 2	SW 3
15	16.4	16.4	17.4	16.7	14.4	20.7	14.9	16.2	24.6	12.8	92	65	91	83	1.3	8.5	1.5	3.8	6 ⊙	7 ⊙	9	C 0	N 2	C 0
16	17.6	17.0	17.5	17.4	13.4	21.0	13.4	15.3	22.1	8.7	87	57	94	79	2.0	10.8	1.0	4.6	1	8	10	W 1	NE 1	C 0
17	17.5	18.8	19.3	18.5	9.6	10.9	7.9	9.1	13.9	7.4	95	82	91	89	0.7	2.3	0.9	1.3	10 ●	10	3	W 1	SW 3	W 1
18	18.4	18.3	18.5	18.4	10.8	15.2	9.5	11.2	18.2	4.5	74	56	87	72	3.5	7.7	1.6	4.3	3 ⊙	8	3	NW 1	WSW 4	SW 1
19	19.5	20.1	22.2	20.6	9.1	17.0	11.9	12.5	17.9	5.3	89	67	94	83	1.3	6.3	0.9	2.8	10	9	10 ●	W 1	N 1	C 0
20	22.4	23.5	24.4	23.4	11.4	12.9	11.2	11.7	13.7	10.7	98	90	95	94	0.4	1.5	0.7	0.9	10 ●	10	10	N 1	C 0	C 0
21	22.5	21.1	18.2	20.6	9.1	17.2	12.9	13.0	17.9	5.8	96	65	95	85	0.5	6.9	0.7	2.7	3 ⊙	9	10 ●	C 0	E 1	C 0
22	14.7	16.7	17.6	16.3	12.7	9.3	7.1	9.0	13.1	6.6	94	93	93	93	0.9	0.8	0.8	0.8	10	10 ●	3	W 2	SW 1	WSW 2
23	18.5	18.5	18.5	18.5	7.9	14.3	6.8	9.0	15.1	6.3	88	56	92	79	1.2	7.1	0.8	3.0	8 ⊙	2	0	WSW 2	NW 4	S 1
24	17.6	16.6	17.4	17.2	6.5	18.9	16.9	14.8	19.9	1.6	92	51	56	66	0.9	10.8	8.4	6.7	1 ⊙	3 ⊙	10	C 0	SW 7	SW 6
25	23.0	22.0	20.0	21.7	8.6	17.5	9.1	11.1	18.4	5.0	77	38	85	67	2.7	12.5	1.8	5.7	1	1 ⊙	2	SW 1	N 1	W 1
26	18.5	18.1	20.0	18.9	9.6	13.7	9.1	10.4	16.0	4.2	80	73	82	78	2.5	4.3	2.1	3.0	6 ⊙	8	3	C 0	W 1	W 1
27	20.8	20.9	20.5	20.7	8.9	14.1	7.7	9.6	15.5	4.8	78	61	91	77	2.5	6.3	0.9	3.2	1	8	5	SW 1	NW 2	C 0
28	17.9	18.7	19.4	18.7	11.7	14.9	10.9	12.1	17.1	6.7	71	61	91	74	4.0	6.6	1.2	3.9	9	9	10 ●	SW 1	NW 2	WSW 2
29	18.2	21.4	24.0	21.2	9.0	8.1	8.5	8.5	10.9	7.4	93	92	93	93	0.8	0.8	0.8	0.8	10 ●	10 ●	10	SW 2	NW 1	C 0
30	24.1	24.9	25.1	24.7	8.0	11.6	7.4	8.6	12.4	6.8	91	65	89	82	0.9	4.6	1.1	2.2	10	9	9	W 1	WNW 3	SW 1
31	24.5	23.4	22.8	23.6	4.2	14.3	8.4	8.8	15.3	1.1	93	41	90	75	0.5	9.7	1.1	3.8	4	8 ⊙	10 ●	C 0	WNW 1	SW 1
M	20.6	20.8	20.9	20.8	11.8	17.0	12.1	13.2	18.6	7.8	84	62	86	77	2.5	8.0	2.2	4.2	5.5	7.2	6.3	0.9	2.2	0.9

Zakopane $H_s = 844$ m $H_b = 838{,}2$ m $h_w = 20$ m **Lipiec – Juillet 1957**

DNI	WIL. ZACHM. V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	11.5	
2	7	4.4	.	7.9	▽² 15¹⁰⁻¹² ▽⁰–15¹⁵ ▽² 15⁴⁸–16¹⁰ ▽⁰–16²⁰, 18⁴⁵⁻⁵². (K)⁰ 13³⁰–14⁵⁰ S K⁰–16¹⁵ SW-N (K)⁰–19³⁰ N. ⌓⁰ na – a
3	8	0.2	.	5.7	▽⁰ 4⁴⁵–5⁴⁵ ▽¹–5⁵⁵ •⁰–6²⁰. 6³⁰–7²⁰ •⁰–8³⁰ •¹–9²⁰ •⁰–10¹⁵. = 4³⁰–10¹⁵
4	9	.	.	12.0	⌓⁰ np
5	8	.	.	13.0	(K)⁰ 21⁵⁰–23⁵⁰ W-NW. ⌓² na – a
6	7	.	.	12.0	
7	9	10.6	.	7.4	▽² 8⁰³⁻⁰⁸ ▽⁰–8²⁰ ▲⁰–8²² ▽² 8²⁰⁻⁴³ ▽¹–9¹⁵ ▽⁰–9²⁰ ▽¹ 9⁵⁵–10⁰⁰ ▽⁰–10³⁰ ▽¹–10⁴⁵ ▽⁰–11¹² (K)¹ 7⁴⁵–8⁰³ NW K¹ 8⁰³–9³⁰ NW-E
8	8	0.6	.	10.0	(K)⁰ 11³⁰–13³⁰ E. ⌓² na – 1 [7.VII: 10¹⁵–11⁰⁵ W-E. ⌓⁰ III-np
9	6	0.0	.	3.2	▽⁰ 5¹⁸⁻²³ 6²¹⁻²⁶ ▽² 6³¹ 12²⁸⁻³¹ ▽⁰ 12³⁸ 13³⁰⁻⁴⁵ 17⁰⁴⁻¹². (K) 2⁴⁵–4⁵⁰ SW-S-SE 6¹⁰⁻⁵⁰ SW-S-SE (K)⁰ 11¹⁵–15³⁰ SE-S. ≫ 4⁵⁰–5¹⁰
10	6	5.7	.	5.6	▽⁰ 15⁵⁸–16¹⁰ 16²⁵–17³⁵ 17⁵⁰–18⁰⁵ •¹–18³⁵ •⁰–19⁰⁵ •¹–19⁴⁵ •⁰–22²⁸. ⌓² n
11	6	1.1	.	2.1	▽⁰ 13³⁰–45 14³⁵–40 14⁴⁵–15⁰⁵. (K)⁰ 13⁵⁰–15³⁵ ≤ 22⁴⁰–24 SE
12	6	14.4	.	0.1	▽² 2³⁵⁻⁵⁵ 3²⁰⁻⁴³ •⁰ 4⁴⁰–5⁰⁵ 8²⁵⁻⁴⁵ ▽⁰ 10²⁸⁻³⁷ 13³³⁻⁴⁵ ▽¹–13⁴⁸ ▽⁰–14⁰⁵ ▽² 14²⁰ ▽¹ 14⁵⁵ ▽⁰–15⁴⁰ 17¹⁰⁻⁴⁵ ▽⁰⁻² 18²⁰ 20²⁰ ▽⁰ 23³⁰–24.
13	6	8.1	.	0.1	▽⁰ 0⁰⁰⁻¹⁰ 5⁴⁰–6¹⁰ 13³⁵–42 16¹⁰–40 ▽² 17²⁰ ▽¹–18¹⁰ ▽⁰–18³⁰ 21³⁵–50. (K) 16⁴⁰ E K¹ 16⁴⁵ 17³⁰ NW-SE-E. = 0⁰⁰–10³⁰
14	7	14.2	.	0.5	▽² 11⁵⁵–12⁵⁰ ▽¹ 13⁴⁰ ▽⁰–14⁰² 14¹⁰⁻³⁷ 16¹⁰⁻²⁵. (K)⁰ 11³⁵–11⁵⁰ NE K¹–13²⁰ NE-W (K)⁰–15⁴⁵ SE [12.VII: ≤ 0⁰⁰–2¹⁰ SE. = 21¹⁵–24
15	6	24.1	.	0.1	•⁰ 10¹⁰ 11⁰⁵ ▽⁰ 11⁴⁸–12⁵⁰ •⁰ 14¹⁰⁻³⁵ •⁰ 17³⁵–18⁰⁵ 18¹⁰–19²⁰ 19³⁵–20¹⁰. = 9³⁰–13¹⁵ 20³⁰–24
16	6	54.2	.	.	•⁰ 0⁵² 1⁰⁵ ▽² 1³² 3⁴⁰ ▽¹ 4⁰⁵ ▽² 5¹⁰ ▽¹–7⁰⁵ ▽⁰–7³⁵ •⁰ 10³² 11¹⁰ ▽⁰ 12⁰⁰⁻²⁰ ▽²–12⁵⁰ ▽¹ 13⁰⁰ ▽⁰ 13¹⁰ ▽¹ 13²⁰⁻³⁰ ▽² 14⁰² 14¹⁰⁻¹⁷ ▽²–14³⁰ ▽¹–14⁴⁰ ▽⁰–14⁵⁰
17	6	4.4	.	1.6	•⁰ 0⁰² 1¹⁵ •² 2¹⁵ •¹ 3⁰⁵ •⁰–3⁴⁵ •¹–4⁰³ •⁰–4⁵⁰ •¹ 5⁰² 6²⁰ •⁰ 8³⁰ •¹ 8⁴⁰⁻⁵⁰ •⁰ 9¹⁰ 10⁰² 11⁰⁵ 11⁴⁰–12⁰⁵ 12¹⁰⁻³⁰ •¹–12⁴⁰ •⁰–12⁴⁵ 13⁰⁰⁻²⁵ •¹–13⁴⁵ •⁰ 14⁰⁵ 14¹²⁻³⁵
18	7	0.0	.	3.2	▽¹ 11³⁰–42 13¹³–38 [16.VII: •² 15⁰⁷–18³⁰ •¹–19³⁵ •⁰–20⁰⁰ •¹–20²⁸ •⁰–21⁴⁵ 23²⁰–30 •⁰–24. K² 1⁵⁰–3³⁰ S-W K¹–4³⁰ NE
19	8	.	.	8.8	⌓⁰ np
20	8	2.9	.	2.1	▽² 13⁵⁰–55 ▽⁰–14¹⁰ 17¹⁷–30 19⁵⁸–21³⁰. (K)⁰ 13⁴⁵–55 W K⁰–14¹⁵ E. ⌓⁰ na
21	7	5.3	.	.	•⁰ 1²⁵–35 ▽¹ 1⁴⁸–2⁰⁰ •⁰–3³⁵ •¹–3³⁷ •⁰–3⁴⁰ 4³⁵–42 •¹ 7¹⁰...38 9⁰⁰–18 9³⁰–11⁰⁰ •¹–11⁵⁸ •²–12⁰⁵ •⁰–14¹⁰ 15⁰⁰ 16³⁰ 17⁰⁰–15. = 4⁴⁰–8³⁰
22	7	12.5	.	0.1	•⁰ 11²⁵–32 ▽² 11⁴⁵–12²³ •⁰–13⁰³ 13¹⁰–40 14⁰⁰–05 14²⁰–15⁰² •¹–15²⁰ •⁰–22¹⁵
23	6	1.8	.	1.0	▽⁰ 11⁵⁵–14¹⁵ •⁰ 19²⁵–21⁰⁵ 23⁰⁰–05
24	6	17.0	.	.	•¹ 5³⁵–6⁰⁵ •⁰ 7³⁵ 8⁰⁰ 8²⁰ 9¹⁰ •¹–10¹⁵ •⁰–10³⁵ •¹–11¹² •⁰–11⁵⁰ •¹–13¹⁰ •²–13⁴⁵ •¹–15⁰⁵ •⁰–16¹⁰ 16²⁰⁻⁵⁰ 17⁰⁰⁻²⁰ •¹ 19³⁰–20²⁰ •⁰–20³⁵ 20⁵⁰–22¹⁰.
25	7	1.8	.	3.3	•⁰ 13⁵⁵–14²⁵. = 0⁰⁰–1³⁰ [24.VII: = 7⁴⁰ 11³⁰ 13³⁰–16¹⁵ 19³⁰–23³⁰
26	9	2.0	.	7.8	•¹ 2³⁵–4⁰ •⁰–3¹⁰ 3⁴⁵–55 •¹ 4²²–25 •⁰–5³⁵ •¹–5³⁸ •⁰–5⁴⁰, 21²⁵–23¹⁰ •¹–23²⁵ •⁰–23³⁰
27	8	6.4	.	1.7	•⁰ 12⁰⁰–05 18⁵⁵–19⁰⁵ 19³⁵–20⁴⁰ •¹–21⁰⁰ •⁰–22²⁵ •¹–22⁴⁰ •⁰–24
28	8	0.0	.	2.1	•⁰ 0⁰⁰–12⁵ 4⁴⁰–6⁴⁵. 9⁵⁰–10¹⁰
29	9	.	.	10.6	⌓² na – a
30	8	.	.	3.2	⌓² n
31	8	0.9	.	2.9	•⁰ 9⁴⁵. 10⁰⁵ •⁰–10⁰⁸ •¹–10¹⁵ •⁰–10⁵⁰ •⁰–11⁰²
Σ	—	192.6	—	139.6	UWAGI.

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1	7	.	.	1.0	= 7³⁰–10³⁰. 21²⁰–24
2	7	.	.	6.4	= 0⁰⁰–12³⁰. ⌓² n. 1
3	8	.	.	5.0	
4	8	.	.	4.0	
5	8	2.2	.	5.1	▽⁰ 11²⁶–38. 12²⁰–59. 13²⁰–14⁴⁰ ▽² 20⁵⁰–53 ▽¹–21⁰⁷ ▽⁰–21²⁰. ⌓¹ na
6	8	.	.	10.3	⌓² 20³⁰–n
7	9	1.6	.	6.1	▽⁰ 17⁰⁵–30. ⌓² n
8	7	.	.	4.1	▽⁰ 1⁰⁵–45 ▽¹–2⁰⁰ ▽⁰–2¹⁰
9	7	.	.	7.3	= 3³⁰–5⁵⁰. ⌓¹ III–n. ⌣² n
10	8	0.9	.	6.7	▽¹ 14³³–50 ▽⁰–14⁵⁵
11	9	.	.	11.5	
12	9	0.0	.	11.1	≤ 21⁴⁰ N. ≫ 3³⁰–4²⁰. ⌣ 22⁴⁵–23
13	8	.	.	7.8	▽⁰ 1⁴⁵–2¹⁰
14	8	1.4	.	9.3	≤ 21⁵⁰–23³⁰ W. ⌓² n
15	9	.	.	5.2	▽⁰ 3²⁵–5⁰² ▽²–5⁰⁵ ▽⁰–5¹⁵. K 3²⁰–5³⁰ W-E
16	7	10.5	.	5.3	▽⁰ 14¹⁰⁻¹² 15¹⁵⁻¹⁸ 17⁰⁵⁻²⁸ ▽² 17⁴² ▽⁰–17⁵⁰ ▽² 18⁵⁰ 19⁰⁰ ▽⁰–19²⁰ ▽²–19²⁴ ▽⁰ 19²⁷⁻³⁵ •⁰ 22³⁰ 24. (K)⁰ 13⁵⁰ 15³⁰ NE K⁰ 17⁰⁵–50 18⁵⁰ 20³⁰.
17	8	5.9	.	2.3	•⁰ 0⁰⁰–4⁵⁰ •⁰–7⁴⁰ •¹–8⁵⁰ •⁰–10⁴⁵ ▽¹ 14³⁰–35. = 0⁰⁰–10³⁰ [16.VIII: = 20³⁰–24. ⌓² n
18	9	.	.	9.3	⌓¹ n – n
19	8	16.5	.	1.9	▽⁰ 15³⁰–16²⁰ 19⁴⁰–20⁰⁰ ▽²–20⁴⁰ ▽¹–21²⁰ ▽²–21⁴⁰ ▽⁰–23¹⁰. = 19⁰⁰–24. ⌓² n
20	7	0.9	.	.	•⁰ 2⁵⁰–3⁰⁰ 5¹⁵–6²⁰ 7¹⁵–8¹⁰ 9³⁰–11¹⁰ 11⁵⁵–12¹⁵. = 0⁰⁰–14³⁰
21	7	5.8	.	4.0	•⁰ 18⁵⁰–19²⁰ •¹–20³⁵ •⁰–21⁵⁰ 22⁵⁰–23¹⁰ 23²⁰–24. = 4³⁰–7³⁰. ⌓² n. a
22	6	12.7	.	.	•¹ 0⁰⁰⁻⁰⁸ •⁰–3³⁰ 4⁴⁰–5¹⁰ 6¹⁵–35 8²⁰–9⁵⁰ •¹–10¹⁰ •⁰–11⁰⁵ •¹–12²⁰ •⁰–13¹⁰ •¹–13³⁰ •⁰–15²⁰ 15⁴⁰–16³⁰
23	9	.	.	9.3	⌓² n
24	9	8.5	.	10.5	▽⁰ 21⁴⁵–22⁰³ •²–23¹² •⁰–23²⁰. ⌓² n. 1
25	9	.	.	12.0	
26	9	.	.	3.6	⌓² n
27	8	0.1	.	6.8	⌓² n. 1
28	7	22.6	.	3.5	•⁰ 4⁴⁵–5²⁵ 20⁰⁰–05 20⁵⁵–21⁴⁵ 21⁵⁸–22⁰⁵ 22¹⁵–23²⁵
29	7	21.9	.	.	•⁰ 0⁰⁰⁻⁵⁸ •¹–2⁴⁰ •⁰–3⁵⁰ •¹–4⁴⁵ •⁰–5⁵⁵ •¹–6¹⁰ •²–7⁴⁰ •¹–8⁵⁰ •²–9⁰⁵ •¹–12²⁰ •⁰–15¹⁵ •⁰ 17²⁰–18⁰⁰ •⁰–18⁴⁵ 19¹⁰–40 22³⁰–23²⁰.
30	7	0.1	.	1.3	▽⁰ 13⁵⁸–14²⁵. = 0⁰⁰–1³⁰ [29.VIII: = 23³⁰–24
31	8	1.8	.	4.0	•⁰ 19²²–20¹⁵. 21²⁵–22¹⁰. ⌣⁰ n. ⌓² a
Σ	—	112.6	—	174.7	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Wrzesień – Septembre 1957

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	22.4	23.6	24.8	23.6	6.4	13.6	5.7	7.8	14.6	4.0	88	52	92	77	1.2	7.5	0.8	3.2	6	6 ⊙	8	N 1	WNW 6	C 0
2	24.3	23.4	21.9	23.2	6.8	15.9	12.0	11.7	16.9	2.0	92	60	73	75	0.8	7.2	3.9	4.0	10	10	9	C 0	N 4	SSW 1
3	20.2	20.7	20.5	20.5	9.5	12.3	10.4	10.6	14.1	8.6	95	91	97	94	0.7	1.3	0.3	0.8	7	10	10 ●	NNW 1	C 0	C 0
4	19.9	22.4	25.2	22.5	10.4	10.3	9.1	9.7	10.7	8.6	97	97	97	97	0.3	0.3	0.4	0.3	10 ●	10 ●	10 ●	C 0	NE 1	NE 1
5	25.6	25.0	24.9	25.2	8.6	12.7	9.5	10.1	13.4	7.4	93	77	95	88	0.9	3.5	0.7	1.7	10	10	8	NE 1	ENE 1	C 0
6	23.3	23.2	24.1	23.5	9.3	16.9	8.8	11.0	17.6	6.2	92	42	95	76	1.0	11.2	0.6	4.3	1 ⊙	5 ⊙	0	C 0	NNE 3	C 0
7	25.1	25.3	26.1	25.5	8.5	19.1	9.9	11.8	19.3	4.7	96	52	93	80	0.5	10.6	0.8	4.0	0 ⊙	2 ⊙	0	C 0	E 1	C 0
8	27.3	27.8	28.7	27.9	10.2	21.6	11.3	13.6	22.3	5.6	89	53	94	79	1.3	12.0	0.8	4.7	1 ⊙	3 ⊙	0	C 0	E 1	C 0
9	28.2	27.8	27.9	28.0	9.8	22.8	14.1	15.2	23.3	5.6	87	57	86	77	1.6	11.8	2.3	5.2	1 ⊙	1 ⊙	6	C 0	NE 2	C 0
10	26.7	24.7	23.7	25.0	10.7	16.0	11.5	12.4	18.7	6.7	86	86	96	89	1.9	2.6	0.5	1.7	8 ⊙	10	10 ☽≡	C 0	N 2	C 0
11	20.7	17.6	14.2	17.5	9.6	17.2	13.1	13.2	18.6	9.1	95	68	68	77	0.7	6.3	4.8	3.9	8	3 ⊙	10	C 0	NE 2	C 0
12	8.9	8.6	13.3	10.3	14.1	19.3	8.0	12.4	19.7	7.3	82	55	80	72	3.0	10.0	2.1	5.0	6 ⊙	5 ⊙	10	SE 1	SW 6	SW 2
13	15.6	15.6	13.9	15.0	5.0	13.5	8.1	8.7	14.9	3.2	87	50	84	74	1.1	7.9	1.7	3.6	8	9	10 ☽	SW 1	SW 2	SW 2
14	14.3	14.4	12.5	13.7	8.2	12.9	8.7	9.6	13.7	5.9	71	56	85	71	3.2	6.5	1.7	3.8	4 ⊙	9	7	SW 3	NE 2	NNE 1
15	11.9	15.7	20.0	15.9	5.1	8.2	6.4	6.5	10.2	4.2	84	67	80	77	1.4	3.6	1.9	2.3	10	8	5	SW 4	W 2	W 2
16	21.5	21.0	22.1	21.5	3.5	11.7	5.1	6.4	12.4	1.6	91	48	77	72	0.6	7.1	2.0	3.2	5	3	0	NW 2	W 3	SW 2
17	22.2	21.8	20.1	21.4	4.2	6.8	4.0	4.8	9.3	1.5	80	81	86	82	1.6	1.9	1.1	1.5	8	9	5	W 2	WNW 4	SW 1
18	17.5	18.4	19.3	18.4	6.4	7.0	6.4	6.6	7.9	3.5	80	89	85	85	1.9	1.1	1.5	1.5	10 ●	9	4	NW 2	WSW 3	C 0
19	18.0	17.2	16.2	17.1	5.6	10.1	10.3	9.1	13.3	2.6	81	74	87	81	1.7	3.3	1.6	2.2	2 ⊙	10 ●	3	C 0	W 4	W 2
20	14.5	16.9	19.4	16.9	11.1	13.1	7.9	10.0	13.9	7.3	63	69	94	75	4.9	4.6	0.6	3.4	8 ⊙	10	9	WNW 2	W 5	C 0
21	20.1	20.5	21.3	20.6	7.7	15.2	6.8	9.1	16.4	6.1	96	65	94	85	0.5	6.0	0.6	2.4	10 ☽	8	0	C 0	WNW 2	SSW 1
22	19.7	19.3	19.8	19.6	5.3	15.0	10.1	10.1	16.4	2.8	92	79	95	89	0.7	3.5	0.7	1.6	6 ⊙	10	3	C 0	NE 1	C 0
23	16.4	12.3	11.5	13.4	10.7	18.0	12.2	13.3	18.8	6.4	91	56	87	78	1.2	9.0	1.9	4.0	7	10	7	NE 2	SSW 7	SW 5
24	13.9	13.8	15.1	14.3	11.3	15.9	8.3	11.0	16.8	7.8	75	52	93	73	3.3	8.6	0.9	4.3	9	9	10 ●	SW 7	WSW 8	WNW 4
25	19.6	21.0	22.9	21.2	1.4	8.5	0.3	2.6	9.3	0.2	91	54	82	76	0.7	5.1	1.1	2.3	6 ⊙	1	0	WSW 1	NW 4	C 0
26	20.1	19.3	20.3	19.9	-0.3	5.5	2.5	2.6	7.1	-3.0	94	70	95	86	0.4	2.6	0.4	1.1	9 ⊙	10 ●	10	S 1	NW 1	C 0
27	21.8	22.1	18.0	20.6	0.1	7.4	5.4	4.6	8.8	-1.4	94	54	56	68	0.4	4.7	3.9	3.0	1 ⊙	3 ⊙	10	C 0	NW 4	WSW 5
28	15.3	14.9	15.5	15.2	5.8	7.0	6.4	6.4	8.5	4.3	86	76	85	82	1.3	2.3	1.5	1.7	8	10	10 ●	W 4	WSW 4	W 2
29	13.8	10.5	7.1	10.5	6.8	11.1	9.8	9.4	11.8	5.2	76	61	73	70	2.4	5.2	3.3	3.6	10 ●	10	9 ●	W 2	SW 7	SW 4
30	10.8	13.4	18.9	14.4	2.7	5.4	1.4	2.7	10.4	0.9	91	73	83	82	0.6	2.4	1.2	1.4	10 ●	8	6	W 4	WNW 3	C 0
31																								
M	19.3	19.3	19.6	19.4	7.1	13.0	8.1	9.1	14.3	4.5	87	65	86	80	1.4	5.7	1.5	2.9	6.6	7.4	6.3	1.4	3.1	1.2

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1	20.0	19.9	21.9	20.6	0.0	5.3	2.0	2.3	5.8	-1.0	94	67	86	82	0.4	2.9	1.0	1.4	10	10	8	SW 1	NE 1	C 0
2	23.1	23.4	23.9	23.5	0.4	5.9	-1.3	0.9	6.9	-2.0	90	59	91	80	0.6	3.8	0.5	1.6	8	8 ⊙	0	SW 1	N 2	C 0
3	22.4	20.4	18.9	20.6	-3.1	8.7	0.8	1.8	9.4	-5.0	93	54	87	78	0.4	5.1	0.9	2.1	0 ⊙	1 ⊙	5	C 0	NW 1	W 2
4	17.7	20.7	23.3	21.2	5.4	1.4	1.0	2.2	6.5	0.4	73	83	81	79	2.4	1.2	1.3	1.6	10	9	7	WSW 2	SW 3	SW 4
5	27.7	26.8	25.9	26.8	0.8	8.4	-1.1	1.8	9.3	-1.9	83	55	100	79	1.2	4.9	0.0	2.0	9	1 ⊙	0	SW 1	W 1	C 0
6	25.0	26.3	29.3	26.9	-1.8	10.2	7.2	5.7	11.4	-4.8	86	58	75	73	0.8	5.2	2.6	2.9	9	4 ⊙	10	SW 1	WSW 2	NW 1
7	29.6	29.1	29.7	29.5	0.9	12.7	3.5	5.2	13.5	-1.1	90	52	91	78	0.6	7.1	0.7	2.8	5 ⊙	0	0	C 0	NW 3	C 0
8	30.3	31.1	31.8	31.1	5.2	13.2	4.4	6.8	13.7	0.6	94	67	93	85	0.5	4.9	0.6	2.0	10	2 ⊙	0	SW 1	NE 2	C 0
9	30.4	29.6	29.3	29.8	1.6	16.4	5.1	7.0	16.7	0.0	94	57	90	80	0.4	8.0	0.9	3.1	0	0 ⊙	0	C 0	ENE 2	C 0
10	28.2	28.1	27.8	28.0	1.0	15.9	4.3	6.4	16.6	-0.6	90	56	93	80	0.7	8.0	0.5	3.1	1 ⊙	0	0	C 0	NE 2	C 0
11	27.2	26.7	26.7	26.9	1.2	14.3	3.8	5.8	15.0	-0.1	94	67	93	85	0.4	5.4	0.5	2.1	0 ⊙	0	0	C 0	NE 2	C 0
12	26.2	26.4	29.8	27.5	0.4	14.8	10.1	8.8	16.7	-0.4	94	56	87	79	0.4	7.3	1.7	3.1	0 ⊙	4 ⊙	10	C 0	E 2	C 0
13	30.4	30.6	29.8	30.3	8.8	12.0	4.3	7.4	12.2	3.9	97	78	95	90	0.3	3.1	0.4	1.3	10 ≡	10	0	C 0	C 0	C 0
14	28.5	28.0	28.7	28.4	1.9	12.2	9.1	8.1	13.4	1.2	96	69	92	86	0.3	4.3	1.0	1.9	0 ⊙	9	10	C 0	NNE 1	C 0
15	30.0	29.8	30.5	30.1	7.5	11.3	5.7	7.6	12.1	4.5	93	71	92	85	0.8	4.0	0.8	1.9	10	10	10	WNW 1	N 1	C 0
16	29.5	28.2	27.2	28.3	-1.0	13.3	3.5	4.8	13.3	-1.4	96	61	91	83	0.3	5.9	0.6	2.3	0	0 ⊙	0	C 0	ENE 2	C 0
17	25.3	25.7	26.1	25.7	0.0	16.3	6.0	7.1	17.9	-0.5	98	52	90	80	0.1	9.0	1.0	3.4	0	0 ⊙	1	C 0	NE 1	C 0
18	23.3	22.0	21.6	22.3	7.1	17.9	6.1	10.3	18.5	3.8	91	36	80	69	0.9	13.1	2.2	5.4	9	9	8	E 2	SW 7	C 0
19	19.7	17.8	16.0	17.8	2.8	20.4	13.5	12.6	21.5	2.2	89	33	53	58	0.9	16.2	7.3	8.1	4 ⊙	4 ⊙	2	C 0	WSW 3	SW 4
20	15.0	16.8	20.0	17.3	4.6	11.4	6.2	7.1	13.7	3.6	92	84	92	89	0.7	2.2	0.7	1.2	9	10	10 ●	C 0	ENE 1	C 0
21	20.9	19.9	17.8	19.5	4.4	6.6	0.1	2.8	7.1	-0.2	93	72	98	88	0.6	2.8	0.2	1.2	9	10	0	E 1	C 0	C 0
22	12.7	9.9	8.2	10.3	2.2	8.1	5.8	5.5	8.6	-1.8	93	77	92	87	0.6	2.4	0.7	1.2	9	9	10 ☽	C 0	NNE 2	C 0
23	10.2	14.1	19.1	14.5	6.0	5.8	4.6	5.2	6.3	4.2	94	89	91	91	0.6	1.0	0.7	0.8	10 ●	10	10 ●	C 0	C 0	W 2
24	20.6	21.4	25.3	22.4	-0.5	9.9	6.8	5.8	10.4	-1.1	94	39	81	71	0.4	7.4	1.9	3.2	3	1	10	C 0	SW 3	W 1
25	27.9	28.6	28.7	28.4	5.3	6.4	0.6	3.2	7.3	0.3	92	73	92	86	0.7	2.6	0.3	1.3	10 ☽	9	0	C 0	N 1	SW 1
26	28.1	27.5	27.1	27.6	-0.9	12.1	1.8	3.7	12.4	-1.9	92	58	96	82	0.5	5.8	0.3	2.2	1	0 ⊙	0	C 0	NNE 2	C 0
27	25.3	24.1	24.0	24.5	-0.2	11.5	7.3	6.5	11.8	-1.0	94	59	88	80	0.4	5.5	1.2	2.4	0	2 ⊙	10	C 0	ENE 1	C 0
28	24.5	24.1	24.4	24.3	2.0	9.4	6.6	6.2	10.2	1.5	93	74	86	84	0.6	3.1	1.3	1.7	7	10	10	SSW 1	NE 2	C 0
29	25.0	24.2	24.2	24.5	0.9	11.5	2.6	4.4	11.8	0.2	94	65	93	84	0.4	4.7	0.6	1.9	0	4 ⊙	2	C 0	NE 2	C 0
30	22.7	21.3	21.8	21.9	1.9	12.9	4.6	6.0	13.1	0.7	96	62	92	83	0.3	5.8	0.7	2.3	7	7 ⊙	4	C 0	NE 1	W 1
31	21.0	20.2	19.0	20.1	3.9	13.5	3.7	6.2	14.7	2.8	93	63	91	82	0.6	5.7	0.7	2.3	7	1 ⊙	0	C 0	NE 1	C 0
M	24.2	24.0	24.6	24.3	2.2	11.3	4.5	5.6	12.2	0.2	92	65	89	81	0.6	5.4	1.1	2.4	5.4	5.0	4.4	0.4	1.7	0.5

Zakopane

$H_s = 844$ m $H_b = 838{,}2$ m $h_w = 20$ m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU n	USŁONECZNIENIE	POGODA
1	8	0.2	.	7.2	●⁰ 22⁵⁸–23⁰², ⌒¹ n
2	8	0.8	.	3.5	= 0⁰⁰–3³⁰
3	6	16.4	.	0.4	●⁰ 5¹⁰–¹² ▽¹ 5¹⁵ ●⁰–5²⁵ 5⁴⁵–6¹⁰ 6²⁵–5⁰ 12⁵⁵ 13⁰³ ▽² 13⁰⁸ ●¹–13²⁰ ▽⁰ 13⁴⁰ ●⁰ 15⁵⁰–17²⁵ ▽²–17³⁵ ●⁰ [illegible] ●⁰–[illegible] ●¹ 20⁰⁵ ●⁰–22¹⁵,
4	5	24.7	.	.	●⁰ 2³⁷–10⁵⁰ ●¹–11⁴⁰ ●⁰–13⁵⁰ ●¹ 14¹⁰ ●⁰–15⁴⁰ ●¹ 16⁰⁰ ●⁰ 17³⁰ ●¹–18³⁵ ●⁰ 22¹⁰ ●⁰–24, = a – np [X: 22⁵⁵–23¹⁰, = a – np
5	8	.	.	0.1	●⁰ 0⁰⁰–20 ●⁰–3³⁰ ●⁰–4⁵⁰, = n–9³⁰, ⌒⁰ p – np
6	9	.	.	9.2	
7	9	.	.	11.0	⌒² n – a
8	9	.	.	11.3	⌒² n, III – np
9	9	.	.	10.7	⌒² na – a
10	8	1.1	.	2.8	●⁰ 16²⁵–22⁵⁰, ≡¹ 16³⁰–24, ⌒² n – a
11	9	0.7	.	8.1	●⁰ 23⁵⁰–24, ≡¹ 0⁰⁰–5³⁰, ⌒⁰ p – np
12	8	8.2	.	3.7	●⁰ 0⁰⁰–⁴⁰ 0⁵⁵–1⁰⁵, 2⁰⁰–³⁰ ●△⁰ 11⁰⁰–¹⁵ 12²⁵–³⁵ ▽¹ 14⁴⁵–15⁰⁰ ▽⁰–16⁰⁵ ▽¹–16¹⁰ ▽²–16²⁵ ▽²–17¹⁵ ●⁰–17²⁵, 18⁰⁷–19⁴⁰
13	9	0.0	.	3.4	●⁰ p – np
14	8	7.5	.	4.0	▽⁰ 22²⁰–¹ 23²² ●¹–23⁴⁰ ●⁰–24
15	9	0.0	.	3.5	●⁰ 0⁰⁰–¹³⁰ ●¹ 2⁰⁵–⁴⁰ ●⁰–3⁴⁵ 4³⁰–⁴⁰ ●¹–4⁵⁰ ●⁰–5²⁰ ●²–5⁴⁰ ●⁰–5⁴⁵, 5⁵⁵–6³⁰ ▽⁰ 10⁰⁰–⁰⁵, 10³⁸–⁴⁰, 17⁰⁰–⁰³, 22³⁵–⁴⁰
16	8	.	.	6.8	⌒² na – a, p – np
17	8	0.0	.	1.4	▽⁰ 10⁵⁰–11²⁰, 12⁵⁵–13⁰⁵, ⌒² n
18	7	4.4	.	0.8	▽⁰ 7⁴⁰–8⁰⁵ ▽⁰ 8¹⁰–²⁰, 9⁴⁵–10¹⁰ ▽⁰–10¹⁵, 10⁴⁵–⁴⁷ ●¹ 10⁵⁵–11¹⁵ ●⁰–11²⁵, 11⁴⁵–12⁰⁰ ●¹–12⁰⁵ ▽⁰–12¹⁰, 13⁰⁵–¹⁵, 13⁵⁵–14⁰⁵, 15¹⁰–¹⁵, 16¹⁴–⁴²
19	7	1.3	.	4.1	●⁰ 13³⁰–18⁴⁰, ⌒² n
20	7	.	.	1.2	
21	7	0.0	.	4.4	●⁰ 7⁴⁰ 8¹⁰, = 0⁰⁰–10²⁰, ⌒² p – np
22	8	0.2	.	2.1	▽⁰ 12¹⁶–⁵⁰ 17³⁰–⁴⁰, = 21³⁰–24, ⌒² na – a
23	8	1.6	.	2.2	●⁰ 14⁴⁰ 15¹⁵ ▽⁰ 17²⁵–⁴⁰ ●⁰ 19²⁸ 20⁰⁵ ●⁰ 20³²–⁴² ▽¹–20⁵⁵ ●⁰–21¹⁰ ▽¹–21¹³ ▽⁰–21¹⁵ = 0⁰⁰–5¹⁵, ⌒² n
24	9	13.7	.	3.3	▽⁰ 17⁰⁰–⁰⁵ 17⁵⁵–18⁰³ ▽¹ 18¹¹–⁴⁸ ▽⁰–19¹⁰, 19¹⁸–²², 19³³–⁴⁷ ▽²–20¹⁰ ▽⁰–20³⁰, 20⁴⁰–21⁵⁸ ▽¹ 22¹⁰ ●⁰–22⁴², 22⁵⁰ 23¹⁵ ▽¹ 23⁵⁰ ▽⁰–24
25	9	.	.	10.1	▽⁰ 0⁰⁰–³⁰, ⌴⁰ na – a
26	6	4.8	.	1.2	●⁰ 13¹⁵–19²⁰, 19⁴⁰–20¹⁰, ⌴² n
27	9	0.9	.	9.3	⌴¹ n
28	7	6.8	.	0.4	●⁰ 4⁴⁰ 5³⁰ 5⁴⁵–⁵⁰ ▽¹ 7¹⁸–³⁵, 10²⁰ 11⁴⁵ 12²⁵–³⁵ ▽² 14⁴⁶–⁴⁹ ▽¹ 15⁰⁵ ▽⁰–15⁰⁹ ▽¹ 20⁰⁸–²⁶ ▽⁰ 21³⁵–22²³ ▽¹ 23³⁰–⁵⁰ ▽⁰–24, ≫ 1⁴⁵–2³⁰
29	8	4.5	.	1.4	▽⁰ 0⁰⁰–¹⁰ ●⁰ 5⁵⁰–6⁰⁰ 6³⁵–7¹⁵, 20²⁰–21¹⁵, 22³⁰–23¹⁰
30	7	0.9	.	0.9	●⁰ 1³⁵–2¹⁰, 2⁵⁰–3⁰⁵ ●¹–4⁰⁵ ●⁰–8²⁰ ▽⁰ 12¹⁰–²⁰
31					
Σ	—	98.7	—	128.5	UWAGI.

Październik - Octobre

1	8	.	.	0.6	⌴¹ na – l
2	8	.	.	2.8	⌴¹ na – a ⌴⁰ p – np
3	9	.	.	10.0	⌴² n
4	7	2.2	.	0.8	●⁰ 8⁰⁵..15–45 9¹⁵, 9³⁵–45 △▽–10³⁸ △¹–10⁵⁰ △▽¹–11⁰⁷ ▽¹–11¹² △▽¹–11¹⁵ ▽⁰–11²⁰ ▽¹△¹–11²⁵ △² 12⁰³ ✶⁰–12¹⁵ △⁰–12³⁸ 12⁵⁸–13³⁵
5	9	.	.	9.4	⌴¹ n ⌴² p – np [X: ✶⁰ 14¹⁸–²² ✶¹–14²⁵ ✶⁰–14²⁸ ✶²–14⁵² ✶¹–14⁵⁵ ✶⁰–14⁵⁷ ●⁰ 17⁴⁵–⁵⁵ ✶¹–18²⁵
6	9	.	.	4.6	⌴² na – a
7	9	.	.	9.5	⌴¹ na – a
8	7	.	.	5.5	= 6²⁰–9³⁰
9	8	.	.	9.1	⌴² n ⌒¹ p – np ⌴¹ np
10	9	.	.	9.5	⌴⁰ na – a
11	8	.	.	9.4	⌴¹ na – a
12	9	1.7	.	8.4	
13	6	.	.	0.3	●⁰ 0³⁰–6³⁰, ≡¹ 6³⁰–9³⁰ = –14³⁰, ⌒⁰ p – np ⌴⁰ np
14	7	.	.	4.3	⌴⁰ na – a
15	6	0.0	.	1.7	≡¹ 3⁴⁰–6³⁰, 8⁴⁰–9⁴⁰ = –17³⁰, 20²⁰–24
16	7	.	.	8.3	●⁰ 2²⁵–3³⁰, = 0⁰⁰–1³⁰ ≡¹–6³⁰ = –7³⁰
17	9	.	.	8.6	⌴² n ⌒⁰ p – np
18	9	.	.	1.6	⌒¹ na – a
19	9	.	.	8.9	⌒⁰ na – a
20	6	13.5	.	2.6	●⁰ 13²⁰–15¹⁰ ●¹–15³⁰ ●⁰–16¹⁵ ●⁰–18¹⁰ ●⁰–23³⁰ ●¹–24, = 12²⁰–24, ⌒⁰ n
21	7	.	.	.	●¹ 0⁰⁰–¹⁰ ●⁰–5¹⁵, = 0⁰⁰–1³⁰ 3³⁰–5³⁰ 8⁴⁰–9²⁰, ⌴¹ p – np
22	7	18.8	.	0.7	▽⁰ 8²⁵–³⁵ ●⁰ 16¹⁸–³⁵ ●⁰ 20²⁵–21³⁰ ●⁰–24, = 20³⁰–24, ⌴⁰ na ⌒² na – a
23	6	18.0	.	.	●⁰ 0⁰⁰–12¹⁵ 20²⁸–21⁰⁵, = 0⁰⁰– na
24	9	1.4	.	5.9	●⁰ 22³⁵–23²⁰ ●¹–24, = 0⁰⁰–1³⁰, ⌴¹ na – a
25	7	0.0	.	1.6	●¹ 0⁰⁰–10 ●⁰–2¹⁵ ●⁰–7³⁰
26	9	.	.	8.3	⌴² n
27	9	.	.	7.3	⌴¹ n
28	8	.	.	2.9	
29	8	.	.	7.8	
30	8	.	.	4.6	⌴¹ n
31	9	.	.	8.0	⌒⁰ p – np ⌴⁰ np
Σ	—	47.5	—	163.2	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Listopad – Novembre 1957

DNI	CIŚNIENIE P−900 I				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	15.6	14.0	13.7	15.1	−0.1	13.3	3.7	5.2	14.0	−0.9	96	63	92	84	0.3	5.7	0.7	2.2	0	0 ⊙	0	SSW 2	ENE 1	C 0
2	16.9	16.8	17.9	17.2	5.2	12.2	8.3	8.5	12.3	1.5	95	66	85	82	0.4	4.8	1.6	2.3	9	3 ⊙	10	C 0	NE 1	SE 1
3	19.2	19.0	18.6	18.9	2.8	11.3	8.2	7.6	12.1	2.3	95	72	90	86	0.4	3.8	1.1	1.8	8	9	9	C 0	NE 2	ENE 1
4	18.5	18.7	19.9	19.0	5.4	13.9	4.0	6.8	14.7	2.6	97	45	81	74	0.3	8.8	1.5	3.5	10 ≡	3 ⊙	0	SE 2	WSW 3	S 2
5	17.6	15.5	15.2	16.1	2.5	14.7	12.4	10.5	15.2	0.3	90	44	48	61	0.7	9.2	7.5	5.8	2	1 ⊙	3	NNW 2	SW 8	W 6
6	14.6	15.8	14.5	15.0	10.8	13.3	10.1	11.1	14.3	9.4	49	53	76	59	6.6	7.3	3.1	5.7	3 ⊙	4 ⊙	7	NE 4	WNW 4	E 2
7	13.2	14.5	14.6	14.1	12.7	13.6	6.8	10.1	14.0	5.6	51	48	76	58	7.3	8.2	2.4	6.0	7	9	6	NE 4	S 3	ENE 4
8	13.5	12.8	12.2	12.8	7.0	12.3	7.4	8.5	12.8	5.8	78	66	93	79	2.2	4.8	0.8	2.6	10	9 ●	9	NW 3	C 0	C 0
9	10.4	11.0	13.3	11.6	7.8	12.1	7.5	8.7	12.3	6.5	90	59	87	79	1.1	5.7	1.4	2.7	10	8	9	C 0	SSE 3	SW 1
10	14.9	14.2	14.2	14.4	1.2	11.8	2.1	4.3	13.1	−0.1	92	61	93	82	0.5	5.3	0.5	2.1	1	3 ⊙	8	WSW 1	C 0	C 0
11	12.9	13.3	14.8	13.7	4.9	6.8	3.6	4.7	8.6	1.6	94	83	93	90	0.6	1.7	0.5	0.9	9	10	10 ◑	SW 1	NE 1	NE 2
12	17.5	20.9	24.4	20.9	2.6	0.3	0.0	0.7	3.9	−0.7	95	94	98	96	0.4	0.3	0.1	0.3	10 ●	10◑ ✳	10	NE 2	NNE 3	NE 4
13	25.9	26.7	27.3	26.6	−1.5	−1.7	−3.7	−2.6	0.4	−4.5	94	94	92	93	0.3	0.3	0.4	0.3	10	10	10	NE 1	NE 3	NE 3
14	28.1	29.0	30.6	29.2	−5.0	0.4	−3.9	−3.1	2.3	−5.6	93	80	92	88	0.3	1.3	0.4	0.7	10	1	0	NE 2	NNE 1	C 0
15	31.5	31.6	31.7	31.6	−4.9	5.6	−2.1	−0.9	6.2	−6.7	90	65	96	84	0.4	3.2	0.2	1.3	0	0 ⊙	0	SSE 1	SW 1	C 0
16	30.5	30.3	31.0	30.6	−4.2	3.3	−0.1	−0.3	5.2	−5.0	94	75	92	87	0.3	1.8	0.5	0.9	6	5	10	C 0	NE 3	E 1
17	30.5	30.1	30.7	30.4	−1.2	−0.4	−1.1	−1.0	0.0	−1.8	93	84	91	89	0.4	0.9	0.5	0.6	10	10	10	C 0	NE 1	NE 2
18	30.8	31.0	30.9	30.9	−1.7	−1.4	−2.3	−1.9	−0.7	−2.8	88	86	91	88	0.7	0.8	0.5	0.7	10	10	10	SW 1	NE 1	C 0
19	30.5	31.0	33.2	31.6	−3.1	−2.8	−3.5	−3.2	−1.9	−4.0	88	93	85	89	0.6	0.4	0.7	0.6	10	10	10	SE 2	SE 1	NE 3
20	34.8	36.3	37.3	36.2	−4.2	−0.3	−3.0	−3.6	−0.1	−6.1	82	63	83	76	0.8	2.3	0.7	1.3	10	1 ⊙	0	SW 1	S 1	C 0
21	37.1	35.8	32.9	35.3	−7.7	1.8	−5.6	−4.3	2.7	−8.3	87	57	90	78	0.4	3.0	0.4	1.3	0	0 ⊙	0	C 0	NE 1	C 0
22	27.1	22.9	20.8	23.6	−8.1	1.2	−6.1	−4.8	2.5	−8.5	90	55	89	78	0.3	3.1	0.4	1.3	0	0 ⊙	0	SW 1	NE 1	C 0
23	20.8	20.4	23.4	21.5	−7.1	−0.3	−0.4	−2.0	0.6	−8.1	88	78	70	79	0.4	1.4	1.8	1.2	1	10	10	SW 1	NE 1	WNW 1
24	25.6	25.7	25.8	25.7	−1.8	0.5	0.2	−0.2	1.3	−2.6	75	58	79	71	1.3	2.7	1.3	1.8	10 △	6 ⊙	10	WSW 3	W 3	SW 3
25	24.3	24.0	25.0	24.4	1.4	2.2	1.9	1.8	2.5	0.0	76	88	91	85	1.7	0.9	0.6	1.1	10	10 ◑	10	W 4	W 3	W 2
26	26.3	26.1	25.8	26.1	3.3	5.6	2.2	3.3	6.5	1.3	91	89	93	91	0.6	1.0	0.6	0.7	10 ●	9	3	W 2	SW 2	SW 1
27	22.1	21.8	22.6	22.2	1.4	2.8	2.6	2.4	3.4	−0.6	91	85	82	86	0.7	1.1	1.4	1.1	9	10 ●	10	SW 4	W 2	W 3
28	21.5	18.9	16.0	18.8	2.9	5.2	3.3	3.7	5.7	2.0	90	79	87	85	0.7	1.8	0.9	1.1	10	10	10 ◑	W 2	W 5	W 3
29	10.9	10.7	16.2	12.6	0.7	−2.1	−7.5	−4.1	4.1	−8.2	88	83	84	85	0.8	0.9	0.5	0.7	10	9 ✳	10 ✳	SW 4	SW 6	N 6
30	22.8	23.9	23.6	23.4	−14.3	−11.8	−11.5	−12.3	−7.3	−15.2	83	82	79	81	0.3	0.4	0.5	0.4	10 ✳	9 ✳	10 ✳	NW 3	N 2	SE 1
31																								
M	22.2	22.1	22.7	22.3	0.2	4.8	1.0	1.8	6.0	−1.7	87	72	86	82	1.1	3.1	1.1	1.8	7.2	6.3	6.8	1.8	2.2	1.7

Grudzień – Décembre

1	125.6	126.1	126.2	126.0	−12.8	−9.1	−9.0	−10.0	−8.3	−15.4	77	67	82	75	0.5	1.0	0.5	0.7	9	3 ⊙	9 ✳	NE 2	E 3	C 0
2	124.2	123.2	123.0	123.5	−11.4	−6.4	−11.3	−10.1	−5.1	−12.2	86	71	86	81	0.4	1.1	0.4	0.6	9	4 ⊙	9	C 0	NE 2	C 0
3	121.3	119.3	119.8	120.1	−15.9	−6.2	−6.8	−8.9	−5.1	−16.7	81	68	85	78	0.3	1.2	0.5	0.7	6	9	10	N 2	WNW 2	C 0
4	121.9	123.0	123.9	122.9	−10.1	−6.5	−2.3	−5.3	−2.2	−10.5	84	78	91	84	0.4	0.6	0.5	0.6	10	10	10◑ ✳	W 1	SW 1	W 2
5	122.2	121.1	122.4	121.9	−1.5	0.0	−0.3	−0.6	0.4	−2.4	92	94	88	91	0.4	0.4	0.7	0.5	10 ✳	10	10 ⊼	WSW 1	SW 1	W 2
6	123.4	124.7	124.6	124.2	−1.9	−2.6	−3.5	−2.8	−0.2	−3.6	88	85	85	86	0.7	0.8	0.7	0.7	10 △	9 ✳	10	N 2	NE 3	E 2
7	120.1	116.7	112.5	116.4	−12.9	−2.0	−12.1	−9.8	−1.9	−13.5	81	75	82	79	0.4	1.4	0.4	0.7	1	6 ⊙	0	C 0	SW 1	SW 1
8	103.4	96.4	93.4	97.7	−2.1	1.3	5.7	2.6	6.0	−13.9	87	60	75	74	0.6	2.7	2.4	1.9	10 ✳	10	10	SW 3	N 3	SW 6
9	91.7	93.1	102.2	95.7	3.4	2.4	−0.9	1.0	6.7	−2.0	63	83	69	72	2.9	1.2	1.8	2.0	9 ●	10 ●	9	W 4	SW 6	WSW 4
10	101.6	101.4	109.0	104.0	−2.4	0.7	−3.1	−2.0	2.7	−3.5	89	85	81	85	0.5	1.0	0.9	0.8	10	10 ✳	9	SW 1	WSW 4	WSW 4
11	111.7	108.8	105.4	108.6	−13.7	−2.8	5.5	−1.4	5.6	−16.6	75	54	55	61	0.5	2.3	4.0	2.3	6	10	7	SW 1	NNE 3	SSW 6
12	102.8	103.8	103.1	103.2	6.4	7.8	9.7	8.4	10.0	4.6	65	66	54	62	3.3	3.6	5.4	4.1	9	9	7	SSW 4	SW 4	WSW 3
13	100.7	99.8	90.8	97.1	10.2	10.2	10.2	10.2	12.7	8.0	56	67	63	62	5.4	4.1	4.5	4.7	8	10 ●	8	SW 8	SW 5	S 10
14	89.0	94.6	102.3	95.3	4.1	6.2	3.2	4.2	10.7	2.6	97	68	76	80	0.3	3.1	1.9	1.8	10 ●	10	0	SW 1	WSW 4	C 0
15	109.3	114.3	119.4	114.4	0.3	−2.1	−6.3	−3.6	3.4	−7.0	94	99	89	94	0.3	0.6	0.4	0.4	10	10 ◑	10 ◑	SE 1	NE 2	C 0
16	122.0	122.2	123.8	122.7	−9.6	−5.3	−10.1	−8.8	−4.6	−10.9	78	55	84	72	0.6	1.8	0.4	0.9	2	0 ⊙	0	C 0	NNE 1	C 0
17	122.3	121.0	120.8	121.4	−7.9	−0.4	−2.5	−3.3	1.4	−10.9	87	86	93	89	0.4	0.8	0.4	0.5	2	6 ⊙	10	C 0	W 1	C 0
18	120.4	120.8	122.3	121.2	−2.1	−3.7	−4.7	−3.8	−1.7	−5.6	94	92	91	92	0.3	0.4	0.4	0.4	10	10	10	C 0	E 2	SE 2
19	124.1	126.2	130.3	126.9	−4.3	−4.0	−3.7	−3.9	−3.4	−5.9	91	84	78	84	0.4	0.7	1.0	0.7	10	10	10	C 0	WSW 1	C 0
20	134.1	135.2	135.3	134.9	−3.5	−0.7	−1.7	−1.9	0.8	−7.1	81	89	90	87	0.9	0.6	0.6	0.7	10	10	0	SW 2	NW 1	C 0
21	133.0	131.7	131.7	132.1	−7.4	−3.7	−7.1	−6.3	−1.7	−8.1	90	92	85	89	0.3	0.4	0.5	0.4	10 ⇄ ≡	4 ⊙	0	C 0	E 1	C 0
22	129.8	129.3	128.4	129.2	−8.8	−3.0	−6.3	−6.1	−1.8	−9.8	89	79	91	86	0.4	1.0	0.3	0.6	1	10 ⊙	10	C 0	E 1	SW 1
23	124.5	122.1	121.1	122.6	−10.1	−1.6	−7.5	−6.7	−0.2	−12.0	84	75	84	81	0.4	1.3	0.5	0.7	0	7 ⊙	0	C 0	C 0	C 0
24	120.0	120.2	121.9	120.7	−11.6	−2.9	−7.9	−7.6	−2.3	−12.7	82	64	87	78	0.4	1.7	0.4	0.8	4	6 ⊙	1	C 0	C 0	C 0
25	122.5	121.9	123.4	122.6	−6.6	1.3	−3.9	−3.8	2.9	−10.2	86	61	87	78	0.4	2.6	0.6	1.2	0	1 ⊙	4	C 0	SW 1	C 0
26	125.7	126.6	129.0	127.1	−2.2	6.1	−1.9	0.2	6.2	−7.0	94	53	83	77	0.3	4.4	1.0	1.9	9	8	1	C 0	SW 2	S 3
27	128.9	128.0	127.6	128.2	−9.9	6.0	−4.1	−1.9	6.6	−6.8	90	48	84	74	0.4	4.9	0.7	2.0	0	0 ⊙	3	C 0	SW 4	C 0
28	125.1	120.1	116.2	119.8	−6.4	2.9	−4.5	−3.2	3.5	−7.4	83	61	86	77	0.6	2.8	0.6	1.3	4	4 ⊙	6	C 0	NW 1	SSE 1
29	114.1	114.9	112.9	114.0	−0.6	−0.3	−2.1	−1.3	0.6	−7.0	81	88	86	75	1.1	0.8	2.3	1.4	9	10 △	4	SW 6	SW 3	SW 2
30	110.0	108.9	106.2	108.2	0.1	1.1	0.0	0.3	3.9	−9.7	99	95	70	60	2.9	3.0	1.8	2.6	6	9	3	WSW 3	W 4	WSW 3
31	106.5	107.3	109.0	107.7	−0.8	0.3	−0.6	−0.4	0.8	−1.9	95	63	64	73	0.4	2.3	2.1	1.6	10 ✳	7	10	W 4	W 4	W 2
M	117.1	116.9	117.4	117.1	−4.8	−0.6	−2.9	−2.8	1.3	−9.5	83	73	80	79	0.9	1.8	1.2	1.3	6.9	7.3	6.1	1.9	2.4	1.8

Zakopane $H_s = 844$ m $H_b = 838{,}2$ m $h_w = 20$ m **Listopad – Novembre 1957**

DNI	WARSTWA	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	8.2	⌴¹ na ⌴² – a
2	8	0.4	.	6.2	●⁰ 21⁵⁰ – 24
3	7	2.8	.	4.1	●⁰ 0⁰⁰…³⁰ 23²⁵ – 24
4	9	.	.	7.6	●⁰ 0⁰⁰ – 1³⁰ . = 5³⁰ – 6⁰⁵ ≡⁰ – 7⁰⁸ ⌴⁰ np
5	9	.	.	7.7	≫ 10³⁰ – 14³⁰ . ⌴¹ na – a
6	9	.	.	5.3	
7	9	.	.	1.6	
8	7	0.0	.	0.8	▽⁰ 12³⁰ – 13³⁰
9	8	.	.	0.1	●⁰ 3⁴⁰ 4¹⁵
10	9	0.1	.	7.3	⌴¹ n ⌴⁰ p – np ; ▽⁰ p – 21⁴⁵
11	7	7.0	.	0.1	●⁰ 4¹⁵ 5¹² ●⁰ 15²⁰ – 16³⁰ ●⁰ – 20¹⁰ ●² – 23¹⁵ ●⁰ – 24 . = 13⁴⁰ – 15⁵⁰ ≡² – 16³⁰ ≡¹ – 20³⁰ = – 24
12	6	2.5	.	.	●⁰ 0⁰⁰–²⁰ 3³⁰ – 8⁴⁰ ✱⁰ – 9¹⁰ ●⁰ – 10²⁰ ●⁰ – 12³⁰ ●✱⁰ – 14⁰⁵ ✱⁰ – 17³⁵ . = 0⁰⁰ – 24
13	5	.	.	.	✱⁰ 0⁵⁰ 1¹⁵ = 0⁰⁰ – 24
14	6	.	.	5.2	= 0⁰⁰ – 19³⁰ . ⌴¹ p – np
15	9	.	.	7.3	⌴² na – p
16	8	.	.	5.5	= 15³⁰ – 24 . ⌴² na – a
17	7	0.0	.	.	●⁰ 7⁵⁵ – 9⁴⁵ (marznąca) . = 0⁰⁰ – 9³⁰ , 19³⁰ – 24 . ∞⁰ 7⁵⁵ – 9⁴⁵
18	6	.	.	.	= 0⁰⁰ – 20¹⁰
19	7	.	.	.	
20	8	.	.	5.7	
21	9	.	.	6.9	⌴² 4⁰⁰ – a
22	7	.	.	6.9	⌴² n , p – np
23	8	0.0	.	1.4	⌴² na – a
24	8	0.0	.	2.7	△⁰ 6¹⁰ – 10¹²
25	7	1.5	.	.	●⁰ 9¹⁰ 10¹⁵ – 11²² ✱⁰ – 12⁰⁵ ●⁰ – 13¹⁵ ●¹ – 14³⁰ ●⁰ – 15¹⁵ 16²⁰ – 17¹⁰ ●⁰ – 17⁴⁵ ●¹ – 18⁰⁷ ●⁰ – 19³⁰ . = 13²⁰ – 15¹⁰ 20³⁰ – 24
26	8	0.2	.	.	●⁰ 6¹⁰ – 8³⁰ 9²⁰ . = 0⁰⁰ – 7¹⁵ , ⌴⁰ na
27	7	1.4	.	.	●⁰ 10⁵⁵ – 18³⁰ . ≡¹ 0⁴⁵ – 2⁴⁵ ≡⁰ – 4³⁰ = – 5⁴⁰ 6³⁰ – 7³⁰ 20²⁵ – 24
28	7	7.9	.	.	●⁰ 5⁴⁵ – 6¹⁵ 7⁴⁰ 8¹⁵ – 9⁴⁰ ●⁰ 10¹⁰ 10³⁰ – 11²⁵ ●⁰ 18²³ – 21³⁰ ●⁰ 22²⁰ – 24 . = 0⁰⁰ – 6¹⁵ 13³⁰ – 14³⁰
29	7	12.1	1	.	●⁰ 0⁰⁰ 3³⁰ ✱⁰ – 5³⁰ 7²⁰–³¹ △⁰ 7⁵⁵ – 8²⁰ ▽¹ – 9³⁰ ▽² – 10⁴⁵ ▽⁰ – 11¹⁵ ▽¹ – 11⁴⁰ ▽⁰ – 12¹⁵ ▽² – 12²⁵ ▽⁰ – 13¹⁰ ▽¹ – 13³⁰ ▽⁰ – 15⁴⁰ ▽² 16¹⁵
30	6	5.4	19	.	✱⁰ 0⁰⁰ – 11³⁰ 14¹⁰ – 24 [29.XI: ▽⁰ – 18³⁵ ▽¹ – 24 . ✱┼¹ 9⁴⁵ – 10⁴⁵
31					
Σ	–	41.3	–	90.6	UWAGI

Grudzień – Décembre

1	9	1.0	23	3.4	✱⁰ 0⁰⁰ – 1⁴⁵ 2¹⁰ 7⁰⁷ – 10³⁰ 18¹⁰ – 20³⁰ ▽⁰ – 24
2	7	0.0	24	3.4	▽⁰ 0⁰⁰ – 6¹⁰ ✱⁰ 7³⁰ 9¹⁵ . 14³⁰ 16⁴⁰
3	7	.	24	0.9	
4	7	1.8	22	.	●⁰ 15³⁰ – 18¹⁵ (marznąca) – 20²⁰ ●✱⁰ – 21¹⁵ ●⁰ – 24 . = 6¹⁰ – 7⁴⁰ . 8¹⁵ – 10³⁰ 15²⁰ – 24 . ∞⁰ 15³⁰ – 24
5	6	9.2	20	.	●⁰ 0⁰⁰ 5⁴⁵ (marznąca) ✱⁰ – 6¹⁰ ●⁰ – 6¹⁵ ✱¹ – 7³⁰ ✱⁰ – 8¹⁵ ✱¹ – 8³⁰ ✱⁰ – 9³⁰ ✱¹ – 10³⁰ ✱⁰ – 12¹⁰ ●⁰ 13⁴⁰ 14¹⁵ – 15²⁰ △⁰ 20²⁰ – 23¹⁵ →
6	7	2.0	23	.	△⁰ 0³⁰ – 4²⁰ ✱⁰ 4²⁵ – 5³⁰ △⁰ – 9¹⁰ ✱⁰ – 10²⁵ ▽⁰ – 13⁴⁰ . = 0³⁰ – 12³⁰ [5.XII: = 0⁰⁰–³⁰ . ∞ 0⁰⁰ – 10²⁵ , 21³⁰ – 24
7	8	.	23	6.1	⌴² n . ▽¹ 23¹⁰ – 24
8	8	1.7	20	1.3	✱⁰ 6³⁵ 7⁰⁵ 14³⁵ 16²⁰ ●⁰ 16³⁰ – 18²⁵ 19³⁰ 20¹⁰ . 22¹⁵ – 23³⁰ 24 . ≫ 7¹⁰–²⁵ SW , 21¹² – 23⁴⁰ WSW . ▽¹ 0⁰⁰–⁵⁰
9	7	3.6	14	.	●⁰ 0⁰⁰…²⁰ 3⁴⁵ ▽⁰ 5⁴⁰ – 9⁴⁰ ▽⁰ – 10¹⁵ ▽⁰ – 12³⁰ ●⁰ – 13⁵⁰ ✱¹ – 14¹⁰ ≫ 2³⁰ – 4³⁰ SW , W
10	6	1.1	12	.	△⁰ 7³⁰ – 8³⁵ ✱⁰ 11²⁵ – 13⁵⁰ ✱¹ – 14⁰⁷ ✱⁰ – 16⁴⁰ . = 11²⁰ – 18¹⁵
11	8	0.0	16	1.8	●⁰ 19²⁵ – 20⁰⁵ . ≫ 22²⁰ – 24 (por. 17 m/sek)
12	8	0.0	10	1.0	●⁰ 4⁵⁰ 5¹⁵ . ≫ 0⁰⁰ – 1¹⁵ (por. 17 m/sek) . 1¹⁵ – 3⁵⁰ (por. 20 m/sek)
13	7	6.2	32	.	●⁰ 0⁴⁰ – 3³⁵ . 9⁰⁸ – 13¹⁰ ●¹ 18³⁰ – 20¹⁰ ●⁰ 21²⁰ 22¹⁰ 22²⁰ – 24 . ≫ 7¹⁰ – 22³⁰ WSW , W (por. 17 m/sek) . ∪⁰ 3⁴⁵ – 6⁵⁰
14	7	0.3	.	.	●⁰ 0⁰⁰ 2⁴⁰ 3³⁰ 4²⁵ 6¹⁵ – 7²⁰ ●⁰ 8⁵⁰ 9¹⁸ ●⁰ 11²⁵ – 12³⁰ ≡ 8⁴⁵ – 10³⁰
15	9	0.4	.	.	●⁰ 8⁴⁰ – 9³⁵ . – 24 (marznąca) . ≡ 7⁴⁰ – 8³⁰ = – 24 . ∞⁰ 9³⁵ – 24
16	9	.	.	5.7	●⁰ 0⁰⁰–²⁰ . = 0⁰⁰ – 4³⁰ . ⌴⁰ p – np ; ∞⁰ 0⁰⁰–²⁰ ⊠¹ – 12⁰⁰
17	8	.	.	2.2	= 12¹⁵ – 14²⁰ . 18⁵⁰ – 24 . ⌴⁰ na
18	6	0.0	.	.	✱⁰ 14⁴⁵ – 15³⁰ △⁰ – 18²⁵ . = 0⁰⁰ – 3³⁰ , 7³⁰ – 24 . ⌴⁰ na
19	5	0.0	.	.	●⁰ 8³⁰ – 11³⁰ (marznąca) . = 0⁰⁰ – 18³⁰ . 20¹⁵ – 24 . ∞ 8³⁰ – 14⁰⁰
20	7	(0.0)	.	.	= 0⁰⁰ – 1⁴⁰ 3³⁰ – 5³⁷ . 13³⁰ – 20²⁰ 21⁴⁵ – 24
21	5	(0.0)	.	1.2	↔¹ 6³⁰ – 7¹⁵ . = 0⁰⁰ – 3³⁰ ≡¹ – 6¹⁵ ≡⁰ – 10⁵⁰ = – 17¹⁰ . V⁰ 3³⁰ – 19³⁰
22	7	.	.	4.6	= 17³⁰ – 24 . ⌴² na . ⊕⁰ 9⁴⁵ – 11²⁰
23	7	.	.	5.1	= 0⁰⁰ – 2³⁰ , 10⁴⁰ – 12²⁰ . V⁰ 0¹⁰ – 15³⁰
24	8	.	.	5.6	⌴² n
25	9	.	.	5.5	⌴² na – a
26	8	.	.	1.9	⌴² na , a
27	9	.	.	5.7	⌴² n
28	9	.	.	5.1	⌴² na , a . ▽⁰ 20³⁵ – 21³⁰
29	8	0.0	.	.	△⁰ 7³²–³³ △⁰ 12³⁰ – 13¹⁰ . = 0³⁰ – 1⁴⁵ ≡¹ – 2⁴⁰
30	9	0.0	.	2.9	≫ 1⁴⁰ – 5³⁰ (por. 17 m/sek)
31	8	0.0	.	0.6	✱⁰ 5⁴⁰–⁵⁰ 7³⁰ ▽⁰ 8²⁵ ▽¹ – 9¹⁰ ▽⁰ – 10³⁵ ▽¹ – 10⁵⁵ ▽⁰ – 11⁰⁷ 13¹⁰ – 16⁰⁸ ✱⁰ 20²⁵ . 21⁰⁵
Σ	–	27.4	–	63.6	UWAGI. *W grudniu wartości ciśnienia atmosferycznego wynoszą 800 mb + wartości podane w tablicy.*

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Styczeń – Janvier 1957

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	93.0	92.8	93.1	93.0	-4.1	-4.4	-2.5	-3.4	-2.5	-6.3	94	93	95	94	0.3	0.3	0.3	0.3	10	9	10	SE 14	SSE14	SSE14
2	91.9	93.7	95.9	93.8	-2.1	-1.9	-2.2	-2.1	-1.7	-2.9	98	98	98	98	0.1	0.1	0.1	0.1	10	10	10	SE 17	SSE17	SE 12
3	98.3	99.0	99.7	99.0	-2.8	-2.8	-3.7	-3.2	-2.0	-4.0	95	97	94	95	0.2	0.1	0.3	0.2	9	10	7	S 9	S 6	SSE 4
4	99.0	100.1	100.5	99.9	-4.2	-4.8	-7.6	-6.0	-3.4	-7.9	96	93	93	94	0.2	0.3	0.2	0.2	10	8	10	SSE 5	SSE 5	SSE 7
5	101.4	101.3	100.5	101.1	-7.1	-3.3	-0.5	-2.8	-0.1	-8.0	72	74	100	82	1.0	1.3	0.0	0.8	4	7	10	SSW 5	SW 6	WNW10
6	99.4	96.7	94.2	96.8	0.0	-0.8	-2.4	-1.4	0.3	-2.4	100	99	98	99	0.0	0.0	0.1	0.0	10	10	10	W 10	W 12	WNW10
7	94.8	97.5	101.0	97.8	-8.7	-8.3	-8.9	-8.7	-2.4	-10.5	92	92	92	92	0.3	0.2	0.3	0.3	10	10	10	NW 17	NW 17	NW 10
8	103.2	104.0	104.2	103.8	-8.7	-6.3	-3.3	-5.4	-3.2	-9.1	92	94	95	94	0.3	0.2	0.3	0.3	10	10	10	NNW 7	NNW 8	NNW 9
9	104.1	102.8	101.3	102.7	-2.8	-0.7	-0.2	-1.0	1.2	-3.3	95	83	70	83	0.2	1.0	1.8	1.0	6	6	0	NNW 8	W 5	W 4
10	97.0	92.6	91.1	93.6	-2.3	-1.9	-8.6	-5.4	1.0	-9.6	57	67	89	71	2.3	1.8	0.4	1.5	8	8	10	SW 5	SW 9	NNW 7
11	90.6	90.8	92.8	91.4	-12.0	-12.5	-12.6	-12.4	-8.6	-13.6	89	89	89	89	0.3	0.3	0.3	0.3	10	10	10	NW 9	NW 8	NNW 7
12	91.6	89.7	84.7	88.7	-14.7	-12.4	-11.1	-12.3	-9.8	-15.2	82	81	90	84	0.3	0.4	0.3	0.3	7	7	10	WNW 8	NW 2	S 10
13	81.7	82.3	83.5	82.5	-12.4	-11.0	-11.8	-11.8	-10.7	-13.0	89	98	89	89	0.3	0.3	0.3	0.3	10	9	10	S 5	S 4	C 0
14	85.9	88.4	89.6	88.0	-12.0	-10.4	-9.5	-10.4	-9.5	-13.1	89	90	48	76	0.3	0.3	1.6	0.7	10	10	3	N 4	N 4	NNE 5
15	89.5	89.0	89.1	89.2	-8.5	-7.3	-8.6	-8.2	-6.9	-10.4	57	88	89	78	1.4	0.4	0.4	0.7	9	9	10	NE 1	NE 4	N 3
16	91.0	92.9	94.9	92.9	-14.8	-15.1	-16.2	-15.6	-8.6	-16.7	87	82	86	85	0.3	0.3	0.2	0.3	10	9	9	NNE 9	NNE 8	NNE 9
17	95.1	96.6	98.4	96.7	-16.9	-14.7	-13.2	-14.5	-11.4	-19.0	35	52	64	50	1.1	0.9	0.8	0.9	0	0	1	NNE10	NNE 9	NNE 7
18	100.1	100.6	100.6	100.4	-8.2	-8.1	-8.8	-8.5	-6.5	-13.9	10	34	80	41	3.0	2.2	0.6	1.9	4	6	1	NNE 4	NNE 5	NNE 4
19	100.3	101.0	102.1	101.1	-8.2	-4.2	-5.1	-5.6	-3.1	-9.1	60	45	23	43	1.3	2.5	3.2	2.3	0	1	0	NNW 3	NNW 2	NNE 4
20	103.3	104.0	104.7	104.0	-2.5	-0.8	-1.6	-1.6	0.6	-5.1	5	4	14	8	4.8	5.6	4.7	5.0	1	1	0	S 4	SSW 8	WSW 4
21	103.9	104.1	104.5	104.2	-0.2	2.1	0.8	0.9	2.5	-1.9	12	15	15	14	5.3	6.0	5.5	5.6	1	2	4	WSW 5	WSW 9	SSW 9
22	103.4	102.3	98.2	101.3	-1.5	-2.2	-5.0	-3.4	1.2	-5.4	13	18	24	18	4.8	4.3	3.2	4.1	7	8	1	S 10	S 10	SSE17
23	97.7	97.8	95.4	97.0	-4.0	-1.8	-2.6	-2.8	-1.1	-7.8	17	26	20	21	3.8	3.9	4.0	3.9	1	8	8	SSW 8	S 4	ESE 9
24	91.0	88.5	88.0	89.2	-2.6	-5.3	-6.5	-5.5	-1.8	-8.0	24	93	94	70	3.5	0.3	0.2	1.3	10	10	10	ESE 9	SSW10	SE 5
25	88.0	88.6	90.5	89.0	-6.4	-8.6	-7.6	-7.6	-5.5	-10.0	91	83	51	75	0.3	0.5	1.7	0.8	10	9	4	C 0	NNW 1	WSW 3
26	94.1	96.3	97.4	95.9	-8.3	-8.2	-8.6	-8.4	-7.6	-9.9	92	87	62	80	0.2	0.4	1.2	0.6	10	9	0	NNW 1	WSW 2	SW 6
27	95.3	96.7	98.1	96.7	-5.8	-3.7	-6.5	-5.6	-3.7	-9.7	92	97	94	94	0.3	0.2	0.2	0.2	9	10	10	SSW14	WNW 9	WNW 5
28	96.1	95.9	99.3	97.1	-8.7	-10.4	-12.1	-10.8	-6.5	-12.6	92	87	85	88	0.3	0.4	0.4	0.4	10	10	10	SSW 4	NW 7	NNW 8
29	102.5	104.0	103.5	103.3	-11.9	-7.5	-7.4	-8.6	-6.8	-13.0	86	22	11	40	0.4	2.7	3.1	2.1	2	5	8	N 7	NNE 1	W 2
30	101.0	100.6	98.8	100.1	-5.0	-3.5	-4.9	-4.6	-2.7	-8.6	54	92	48	65	1.9	0.4	2.2	1.5	3	9	5	N 5	NNW 3	WNW 4
31	97.8	99.4	100.0	99.1	-7.9	-6.0	-6.2	-6.6	-3.7	-9.1	93	79	68	80	0.2	0.8	1.2	0.7	10	1	2	C 0	S 3	SSW 6
M	96.2	96.5	96.6	96.4	-7.0	-6.0	-6.6	-6.6	-4.0	-9.4	70	72	70	71	1.3	1.2	1.3	1.3	7.1	7.5	6.5	7.0	6.8	6.9

Luty – Février

1	98.6	99.3	100.3	99.4	-5.5	-3.4	-0.9	-2.7	-0.6	-7.5	95	97	99	97	0.2	0.2	0.0	0.1	10	10	10	S 10	SSW 7	WSW 5
2	103.9	106.0	106.8	105.6	1.3	1.6	0.8	1.1	2.2	-1.3	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	W 8	W 5	WNW 8
3	106.3	105.1	104.0	105.1	1.8	2.7	2.8	2.5	4.5	0.2	88	76	74	79	0.9	1.8	2.0	1.6	8	9	3	WSW10	S 8	W 3
4	103.9	104.2	103.5	103.9	2.6	3.6	0.9	2.0	4.3	0.7	66	46	74	62	2.6	4.2	1.8	2.9	9	9	9	SSW 2	WSW 4	NNW 2
5	103.9	104.4	103.3	103.9	2.0	3.7	1.7	2.3	3.9	-0.9	42	52	62	52	4.2	4.0	2.6	3.6	1	1	0	NW 2	S 1	SSE 8
6	99.4	97.1	96.9	97.8	-1.5	-3.6	-3.4	-3.0	1.8	-5.3	86	97	72	85	0.8	0.2	1.3	0.8	1	6	1	SE 17	SE 17	S 14
7	96.6	97.0	97.3	97.0	-3.2	-3.5	-7.0	-5.2	-1.4	-7.8	95	97	69	87	0.2	0.1	1.1	0.5	10	10	3	WSW 9	WNW10	WNW 7
8	95.6	93.7	91.5	93.6	-4.8	-2.8	-1.3	-2.6	-0.2	-7.6	95	75	58	76	0.2	1.2	2.4	1.3	10	10	10	SSE14	SSW10	SSW10
9	87.4	87.4	87.7	87.5	-3.1	-4.4	-4.3	-4.0	0.3	-5.4	97	96	94	96	0.1	0.2	0.3	0.2	10	10	10	SW 10	W 12	W 8
10	88.8	89.1	89.5	89.1	-6.3	-6.0	-5.0	-5.6	-3.8	-9.4	34	94	93	74	2.5	0.2	0.3	1.0	1	9	8	W 5	W 12	SSW 6
11	89.4	90.7	92.3	90.8	-5.8	-6.0	-7.6	-6.8	-5.0	-7.9	89	94	93	92	0.4	0.2	0.2	0.3	9	10	10	SW 6	W 5	WNW 3
12	91.6	90.8	87.1	89.8	-9.8	-7.2	-7.2	-7.8	-6.5	-10.1	91	82	93	89	0.3	0.6	0.2	0.4	9	2	10	C 0	S 12	SE 17
13	85.5	83.3	77.7	82.2	-6.8	-6.6	-5.5	-6.1	-5.5	-7.5	94	94	95	94	0.2	0.2	0.2	0.2	10	10	10	S 10	SSE12	SSE17
14	76.8	75.7	76.0	76.2	-4.6	-5.0	-6.1	-5.4	-4.2	-6.1	93	95	94	94	0.3	0.2	0.2	0.2	10	10	8	S 10	SSW 8	SW 8
15	76.6	73.0	72.2	73.9	-8.6	-5.2	-5.4	-6.2	-4.5	-8.9	92	95	95	94	0.3	0.2	0.2	0.2	7	10	10	SE 7	SSE17	S 9
16	77.2	79.9	83.0	80.0	-7.4	-7.8	-7.0	-7.3	-4.9	-8.3	90	90	76	85	0.3	0.3	0.8	0.5	8	7	10	SW 9	SSE10	S 6
17	85.3	87.7	89.1	87.4	-8.6	-7.1	-7.9	-7.9	-6.6	-9.7	92	88	90	90	0.3	0.4	0.3	0.3	10	7	1	S 2	SSE 8	SSE 7
18	87.3	83.8	81.8	84.3	-5.8	-5.7	-0.9	-3.3	-0.7	-9.3	95	90	99	95	0.2	0.4	0.0	0.2	10	9	10	SSE14	S 20	SE 17
19	80.3	85.8	90.4	85.5	-5.5	-9.3	-11.3	-9.4	-0.9	-11.5	95	88	86	90	0.2	0.4	0.4	0.3	10	10	9	WSW 5	NNW 5	W 5
20	92.3	92.5	87.4	90.7	-11.0	-8.9	-8.6	-9.3	-8.1	-12.4	86	92	83	87	0.4	0.3	0.5	0.4	1	10	8	SSW10	SE 14	SE 17
21	87.0	88.5	89.7	88.4	-6.9	-6.0	-5.6	-6.0	-5.4	-8.9	94	92	92	93	0.7	0.3	0.3	0.3	10	9	10	SSW12	S 10	NE 1
22	89.6	89.1	88.6	89.1	-10.7	-10.1	-14.4	-12.4	-5.4	-14.5	90	91	83	88	0.3	0.3	0.3	0.3	10	10	2	N 6	NNW 6	NNW 3
23	88.9	89.2	89.7	88.9	-13.6	-11.8	-13.1	-12.9	-11.3	-15.2	64	71	84	73	0.8	0.7	0.4	0.6	4	1	3	C 0	SW 3	S 6
24	83.5	79.1	79.6	80.7	-10.8	-10.6	-8.5	-9.6	-8.3	-13.6	90	90	89	90	0.3	0.3	0.3	0.3	10	10	10	S 17	SE 17	W 12
25	82.2	83.3	82.6	82.7	-9.6	-8.1	-6.3	-7.6	-6.2	-9.7	91	87	91	90	0.3	0.4	0.3	0.3	10	6	10	WNW 4	SW 6	S 10
26	83.7	87.2	91.0	87.3	-11.7	-11.0	-12.2	-11.8	-6.3	-12.4	89	90	89	89	0.3	0.3	0.3	0.3	10	10	10	NNW12	N 7	NNW 7
27	92.4	94.6	95.8	94.3	-13.0	-9.7	-11.3	-11.3	-9.0	-14.2	73	66	62	67	0.6	1.0	1.0	0.9	0	0	0	NNE 6	NNE 2	NNE 6
28	96.6	97.7	97.4	97.2	-11.7	-11.1	-16.7	-14.0	-10.7	-17.4	40	49	95	61	1.5	1.3	0.1	1.0	0	0	10	N 6	NNE 5	NNW10
29																								
30																								
31																								
M	90.4	90.5	90.4	90.4	-6.4	-5.7	-6.1	-6.1	-3.5	-8.6	84	85	85	85	0.7	0.7	0.6	0.7	7.4	7.7	7.3	8.0	9.0	8.3

Kasprowy Wierch — H_s = 1991 m — H_b = 1988,8 m — h = 15,4 m — Styczeń – Janvier 1957

DNI	WSKAŹNIK ZACHMURZENIA v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	2.7	75	.	
2	0	0.4	75	.	
3	1	0.2	75	0.1	
4	8	1.0	75	1.7	
5	9	4.1	74	3.6	
6	0	8.5	72	.	
7	0	17.3	92	.	
8	0	2.9	105	.	
9	9	.	107	4.9	
10	9	4.7	104	4.4	
11	0	5.8	106	.	
12	9	2.0	109	2.6	
13	7	2.3	108	.	
14	0	0.6	109	0.9	
15	8	2.2	108	0.7	
16	7	1.8	110	0.4	
17	9	.	114	7.9	
18	9	.	112	9.0	
19	9	.	108	8.0	
20	9	.	107	8.0	
21	9	.	106	8.0	
22	9	.	101	4.5	
23	9	.	95	4.9	
24	6	1.9	93	.	
25	9	1.4	94	.	
26	9	0.0	94	0.6	
27	1	4.1	92	.	
28	0	16.7	95	0.2	
29	9	.	108	5.8	
30	9	.	106	6.1	
31	9	0.2	104	8.0	
Σ	—	80.8	—	89.3	UWAGI.

Luty – Février

1	1	7.3	102	.	
2	0	2.3	102	0.4	
3	9	.	94	4.7	
4	9	.	86	1.6	
5	9	.	84	8.7	
6	9	.	76	4.6	
7	0	0.0	75	0.1	
8	9	0.1	74	1.0	
9	7	6.5	74	0.3	
10	8	0.0	77	5.5	
11	6	5.0	75	.	
12	9	3.8	80	6.7	
13	0	6.1	85	.	
14	0	5.7	91	.	
15	1	8.3	92	2.3	
16	9	.	94	3.2	
17	9	1.6	93	3.8	
18	9	14.3	94	0.8	
19	0	3.3	96	.	
20	6	0.0	97	4.6	
21	9	15.0	95	0.1	
22	0	17.2	110	.	
23	9	1.5	130	8.5	
24	1	4.3	120	.	
25	9	9.2	124	3.6	
26	0	16.8	130	.	
27	9	.	154	10.3	
28	9	1.4	151	9.7	
29					
30					
31					
Σ	—	129.7	—	80.5	UWAGI.

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Marzec – Mars 1957

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE, POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	97.7	98.5	97.9	98.0	-16.9	-16.4	-17.4	-17.0	-15.5	-18.1	90	90	90	90	0.2	0.2	0.2	0.2	10	10	10	N 12	N 8	N 10
2	96.7	97.0	95.5	96.4	-18.3	-14.9	-16.6	-16.6	-14.3	-19.1	84	87	85	85	0.2	0.3	0.2	0.2	0	10	10	N 10	N 9	NNW 7
3	92.4	91.1	90.2	91.2	-17.0	-12.7	-16.7	-15.8	-12.7	-18.0	85	88	85	86	0.2	0.3	0.2	0.2	10	10	0	b c	NNW12	N 9
4	89.4	90.3	90.8	90.2	-12.7	-7.5	-7.2	-8.6	-6.0	-16.7	54	44	82	60	1.0	2.0	0.6	1.2	3	2	10	N 12	N 7	WNW 9
5	89.8	89.9	90.1	89.9	-5.8	-6.7	-8.5	-7.4	-5.2	-12.7	59	94	38	64	1.6	0.2	2.0	1.3	9	10	0	N 10	WSW 4	NW 4
6	89.8	89.9	89.4	89.7	-8.5	-6.5	-6.8	-7.2	-5.2	-9.6	22	21	19	21	2.5	3.0	3.0	2.8	2	1	1	NW 5	NW 2	W 2
7	88.0	88.8	89.3	88.7	-7.5	-4.3	-6.9	-6.4	-3.6	-8.1	32	42	25	33	2.3	2.6	2.7	2.5	1	1	2	NW 3	NNW 2	WNW 3
8	89.7	90.8	91.7	90.7	-7.9	-5.3	-8.6	-7.6	-4.6	-9.5	12	39	62	38	3.0	2.5	1.2	2.2	4	2	0	NW 3	N 3	N 1
9	93.1	95.4	97.7	95.4	-9.4	-8.5	-11.6	-10.3	-5.7	-12.1	42	38	36	39	1.7	2.0	1.6	1.8	9	1	1	NNE 2	N 1	NNE 6
10	99.7	102.2	104.2	102.0	-7.9	-3.0	-4.3	-4.9	-1.4	-12.6	16	35	17	23	2.8	3.1	3.7	3.2	0	1	1	NNE 5	ENE 2	NE 2
11	105.5	105.4	106.1	106.0	-3.2	-3.1	-4.5	-3.8	-2.5	-5.4	18	37	30	28	4.0	3.0	3.1	3.4	4	1	0	NE 4	NNE 4	NNE 4
12	103.8	102.8	100.1	102.2	-2.9	-1.0	-0.6	-1.3	2.6	-4.8	16	26	20	21	4.1	4.2	4.7	4.3	6	10	9	N 2	S 3	NNW 2
13	98.4	99.7	100.5	99.5	-1.7	1.3	0.7	0.2	1.7	-3.0	12	28	84	41	4.7	4.8	1.1	3.5	7	8	4	N 8	N 7	E 5
14	98.6	97.6	95.2	97.1	2.7	2.5	0.9	1.3	4.2	0.0	38	46	84	56	4.5	3.9	1.0	3.1	8	4	10	SW 7	WSW10	WSW17
15	93.3	93.9	91.2	92.8	-4.0	-4.1	-2.5	-3.3	0.9	-4.7	96	96	98	97	0.2	0.2	0.1	0.2	10	10	8	NW 6	WSW 7	W 14
16	85.8	87.3	88.6	87.2	-2.0	-4.4	-10.0	-5.6	-1.7	-11.6	98	96	31	75	0.1	0.2	2.0	0.8	10	10	9	W 17	WNW 8	NNW 7
17	90.6	91.7	89.8	90.7	-4.0	-2.6	-2.3	-2.8	-1.6	-10.3	94	95	96	95	0.3	0.2	0.3	0.3	10	10	10	WNW14	W 10	SSE10
18	84.7	85.2	86.5	85.5	-0.9	-1.2	-4.4	-2.7	-0.1	-4.9	99	95	93	96	0.0	0.3	0.3	0.2	10	6	10	SW 7	W 17	WNW10
19	89.2	91.9	91.7	90.9	-5.4	-4.2	-0.4	-2.6	-0.4	-6.0	92	96	100	96	0.3	0.2	0.0	0.2	9	10	10	WNW14	WSW10	W 12
20	92.9	94.6	94.1	93.9	-1.9	-0.2	2.8	0.9	4.1	-2.1	98	98	57	84	0.1	0.1	3.2	1.1	10	9	3	NW 4	SSW 5	SW 10
21	94.6	96.2	95.9	95.6	5.1	1.8	1.0	2.2	5.2	0.5	27	95	53	58	6.4	0.3	3.1	3.3	9	9	9	SW 8	W 3	WSW 6
22	95.1	96.7	97.5	96.4	-4.9	-1.8	-3.5	-3.4	1.0	-5.4	66	83	69	73	1.8	0.9	1.4	1.2	3	7	1	NNW 3	NNW 1	SSW 4
23	97.5	98.3	98.3	98.0	-1.7	1.2	-0.4	-0.3	1.2	-4.2	42	71	86	66	2.8	2.0	0.8	1.9	5	7	10	WSW 5	SSW 3	S 8
24	98.7	100.0	101.0	99.9	-0.2	-0.3	1.2	0.5	1.6	-1.5	92	100	91	94	0.5	0.0	0.7	0.4	10	10	10	SSW 7	SE 8	SSE 9
25	101.3	102.5	103.1	102.3	0.8	-0.3	-1.1	-0.4	1.0	-1.1	98	98	99	98	0.2	0.2	0.1	0.2	10	10	9	SE 5	S 7	S 9
26	102.1	102.3	102.2	102.2	-2.3	-1.0	-4.0	-2.8	-0.2	-4.8	98	97	63	86	0.1	0.2	1.7	0.7	7	8	1	SE 7	SSW 7	SSE14
27	102.8	104.9	104.5	104.1	-4.1	0.7	-1.6	-1.6	1.6	-6.8	23	26	23	24	3.5	4.8	4.1	4.1	0	0	0	SSE12	S 9	SE 5
28	100.9	101.0	98.3	100.1	-3.8	-3.1	-5.7	-4.6	-1.6	-5.7	24	57	47	43	3.5	2.1	2.1	2.6	1	4	7	SE 12	SSW12	SSE10
29	94.4	95.9	94.7	95.0	-4.3	-2.0	-3.0	-3.1	-1.6	-6.6	96	96	97	96	0.2	0.2	0.1	0.2	10	10	9	S 14	SE 4	S 9
30	93.7	94.7	94.5	94.3	-4.1	-3.7	-4.4	-4.2	-2.4	-5.9	91	78	91	87	0.4	1.0	0.4	0.6	10	10	2	ESE 8	ESE12	E 14
31	98.7	100.3	100.4	99.8	-2.8	-1.0	-1.3	-1.6	0.6	-5.8	32	71	34	46	3.3	1.7	3.7	2.9	5	7	2	ESE 6	SSW 2	ESE 3
M	95.1	96.1	95.8	95.7	-5.1	-3.6	-4.8	-4.6	-1.9	-7.6	60	70	64	65	1.8	1.5	1.6	1.6	6.5	6.7	5.4	7.8	6.4	7.6

Kwiecień – Avril

1	100.4	101.3	100.7	100.8	-1.0	1.9	-0.5	0.0	2.4	-2.8	45	45	42	44	3.2	3.9	3.4	3.5	3	1	1	ESE 7	SE 4	ESE 8
2	100.0	101.2	102.1	101.1	-0.5	0.6	0.8	0.4	1.7	-1.4	52	50	54	52	2.9	3.2	3.0	3.0	3	8	9	SE 12	S 10	SSE 4
3	103.1	104.9	106.0	104.7	1.1	5.2	3.0	3.1	5.6	-0.9	46	36	30	37	3.6	5.7	5.4	4.9	3	4	2	N 3	SE 1	C 0
4	105.8	108.0	107.4	107.4	0.5	3.3	-1.1	0.4	4.1	-2.1	44	50	73	56	3.5	3.8	1.6	3.0	2	2	0	N 3	NNW 3	NNE 6
5	104.8	104.9	102.0	103.9	-1.7	2.3	0.9	0.6	3.7	-3.0	28	46	36	37	3.8	4.0	4.1	4.0	0	0	0	NNE 6	NW 1	SSE 7
6	98.9	97.0	94.6	96.8	-0.1	3.5	0.7	1.2	4.2	-0.9	57	50	58	55	2.7	3.9	2.7	3.1	0	1	1	SSE 7	SSW 8	SE 5
7	91.2	90.1	89.3	90.2	-0.8	0.7	-3.7	-1.9	1.6	-3.9	66	72	97	78	1.9	1.8	0.2	1.3	3	9	10	SE 5	S 4	C 0
8	89.9	90.9	90.9	90.6	-7.9	-7.6	-6.6	-8.2	-3.7	-9.0	93	93	92	93	0.2	0.2	0.3	0.2	10	10	10	NNE 5	N 6	N 9
9	89.9	90.4	89.9	90.1	-9.4	-5.1	-6.7	-7.0	-4.2	-13.0	72	85	75	77	0.8	0.6	0.9	0.8	2	9	8	N 10	C 0	C 0
10	88.4	87.9	84.0	86.7	-6.4	-2.1	-2.8	-3.5	-1.2	-8.1	76	74	99	82	0.9	1.3	0.1	0.8	5	6	10	C 0	S 8	SSE10
11	78.3	78.2	80.5	79.0	-1.4	-0.9	-6.6	-3.9	-0.7	-6.9	99	99	91	96	0.1	0.0	0.3	0.1	10	10	10	SSE 6	SSW 4	N 4
12	83.8	85.4	86.9	85.4	-10.2	-5.1	-9.7	-8.7	-4.8	-10.8	91	95	91	92	0.3	0.2	0.3	0.3	10	10	10	NE 3	N 3	N 5
13	87.4	90.1	91.9	89.8	-10.3	-6.9	-9.4	-9.0	-4.7	-11.0	91	86	88	88	0.3	0.5	0.4	0.4	10	10	10	NNW 5	WNW 1	WSW 2
14	91.5	91.6	91.0	91.4	-12.2	-8.8	-11.4	-11.0	-8.4	-13.4	85	92	86	88	0.4	0.3	0.4	0.4	7	10	10	NE 2	NNW 4	N 7
15	90.4	92.6	95.7	92.9	-12.7	-10.1	-10.8	-11.1	-8.6	-13.1	85	91	90	89	0.4	0.3	0.3	0.3	10	10	10	NNW12	N 6	N 5
16	95.9	98.4	100.1	98.1	-12.5	-7.0	-5.6	-7.7	-4.6	-13.8	85	72	92	83	0.4	1.0	0.3	0.6	2	1	10	N 14	N 6	N 8
17	98.1	97.3	96.0	97.1	-4.2	-3.8	-5.3	-4.6	-3.2	-5.9	94	96	93	94	0.3	0.2	0.3	0.3	10	10	10	NNW 4	NW 4	NNW 9
18	93.2	93.3	92.6	93.0	-6.5	-5.9	-8.1	-7.2	-5.3	-8.6	91	92	90	91	0.3	0.3	0.3	0.3	10	10	10	NNW 9	NNW 7	NNW 1
19	92.3	93.1	94.8	93.4	-7.7	-4.2	-4.6	-5.3	-3.0	-9.4	90	69	91	83	0.3	1.3	0.4	0.7	9	6	9	C 0	SW 3	S 7
20	97.0	99.0	100.4	98.8	-2.8	-2.9	-4.5	-3.7	-1.9	-5.2	97	97	96	97	0.1	0.1	0.2	0.1	10	10	10	C 0	NNW 1	NNE 1
21	100.8	102.4	103.4	102.2	-3.6	-2.5	-2.6	-2.8	-2.0	-4.8	94	98	98	97	0.3	0.1	0.1	0.2	10	10	10	S 2	S 3	SE 2
22	103.5	105.1	105.1	104.6	-1.8	0.5	-1.6	-1.1	0.9	-3.0	98	91	96	96	0.1	0.6	0.1	0.3	10	9	10	ESE 7	C 0	NE 3
23	103.8	104.3	104.3	104.1	-2.5	-1.0	-1.7	-1.7	-0.6	-3.8	89	99	98	95	0.6	0.1	0.1	0.3	7	10	10	N 8	N 2	N 8
24	102.1	102.9	102.7	102.6	-1.2	-0.8	-0.5	-0.8	1.0	-2.0	99	99	100	99	0.1	0.0	0.0	0.0	10	10	10	NNE 7	NE 2	NNE 4
25	100.9	101.1	101.3	101.1	0.7	2.0	1.2	1.3	3.5	-0.8	87	98	96	94	0.8	0.2	0.3	0.4	8	10	9	C 0	ESE 1	E 1
26	100.7	101.5	102.1	101.4	1.4	3.2	2.6	2.4	4.7	0.6	96	96	80	91	0.3	0.3	1.4	0.7	9	10	10	NNE 2	N 3	NNE 3
27	100.0	100.3	99.4	99.9	4.1	2.5	3.4	3.4	5.3	1.5	78	89	81	83	1.8	0.8	1.4	1.3	1	9	5	NNE 1	SE 4	E 4
28	98.1	98.6	98.3	98.3	3.5	5.1	4.0	4.2	6.5	2.2	88	78	75	80	1.0	1.8	2.0	1.6	6	7	1	ESE 3	SE 6	SSE 9
29	98.7	99.9	99.8	99.5	3.7	5.8	5.4	5.1	7.1	0.3	86	74	76	79	1.2	2.3	2.2	1.9	9	6	3	SE 10	SSE 6	SE 7
30	98.9	97.5	95.3	97.2	5.5	7.1	5.3	5.8	7.6	4.4	76	67	93	79	2.0	3.3	0.6	2.0	4	9	7	SE 5	SSE10	SSE14
31																								
M	96.3	97.0	97.0	96.8	-3.2	-1.0	-2.6	-2.4	0.1	-5.0	79	79	82	80	1.2	1.4	1.1	1.2	6.4	7.6	7.5	5.3	4.0	5.1

Kasprowy Wierch — H_s = 1991 m — H_s = 1988 m — h_w = 15,4 m — Marzec – Mars 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY h	UTRUDNIENIE	POGODA
1	↑	7.4	155	.	
2	1	4.8	162	0.3	
3	0	0.0	160	.	
4	9	0.1	170	9.5	
5	0	0.2	169	.	
6	9	.	165	10.7	
7	9	.	163	10.7	
8	9	.	159	10.8	
9	9	.	157	8.1	
10	9	.	154	10.8	
11	9	.	151	11.2	
12	9	.	148	8.0	
13	9	.	147	6.1	
14	9	0.7	125	8.3	
15	6	1.7	114	2.1	
16	0	11.3	112	.	
17	0	7.4	116	0.1	
18	8	5.0	119	1.1	
19	7	4.3	120	0.8	
20	8	.	120	3.4	
21	8	0.5	116	4.7	
22	8	0.0	112	5.9	
23	8	0.5	110	6.3	
24	7	1.8	108	0.2	
25	0	0.4	106	0.2	
26	8	.	104	2.3	
27	9	.	98	11.5	
28	9	0.3	95	10.6	
29	8	0.6	94	0.4	
30	7	0.6	90	.	
31	9	.	90	7.1	
Σ	—	52.5	—	151.2	UWAGI.

Kwiecień – Avril

1	9	.	89	11.6	
2	9	.	86	9.0	
3	9	.	83	10.6	
4	9	.	79	12.3	
5	9	.	72	12.5	
6	8	.	66	12.1	
7	8	7.2	60	3.9	
8	1	6.5	58	.	
9	9	0.0	72	6.8	
10	8	7.3	70	10.6	
11	0	18.9	74	.	
12	0	6.0	87	0.7	
13	6	5.0	92	2.1	
14	1	6.5	100	0.6	
15	1	10.8	107	0.2	
16	8	0.0	115	7.9	
17	0	19.4	112	.	
18	0	7.0	129	.	
19	9	0.4	133	8.2	
20	8	6.5	130	.	
21	0	4.5	137	.	
22	7	1.8	140	1.7	
23	0	19.7	140	1.5	
24	0	5.4	161	0.3	
25	1	2.7	163	1.7	
26	1	0.2	157	2.0	
27	7	4.7	152	6.4	
28	8	0.0	143	9.2	
29	8	0.1	110	7.9	
30	8	6.9	78	4.4	
31					
Σ	—	147.5	—	144.2	UWAGI.

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Maj – Mai 1957

DNI	CIŚNIENIE P − 700				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.6	95.5	94.2	95.1	3.2	2.8	−1.5	0.8	5.6	−2.7	94	100	99	98	0.4	0.0	0.1	0.2	9	10	10	C 0	C 0	NE 4
2	91.9	92.0	91.7	91.9	−4.1	3.0	1.7	0.6	4.3	−5.5	96	92	92	93	0.2	0.6	0.5	0.4	10	9	4	NE 4	C 0	SSE 2
3	90.7	91.6	91.5	91.2	0.2	0.4	−1.7	−0.7	2.2	−1.9	100	98	98	99	0.0	0.1	0.1	0.1	10	10	10	C 0	SW 1	C 0
4	91.0	92.2	92.7	92.0	−3.4	−1.8	−4.2	−3.4	−1.4	−5.1	92	98	91	94	0.4	0.1	0.4	0.3	9	10	10	NNE 4	N 3	WNW 4
5	91.9	91.7	89.6	91.1	−8.9	−3.1	−6.2	−6.1	−2.7	−9.5	89	83	94	89	0.4	0.8	0.2	0.5	8	9	10	WNW 1	S 1	E 1
6	87.4	87.2	87.3	87.3	−6.9	−6.2	−8.3	−7.4	−4.3	−8.6	91	94	92	92	0.3	0.2	0.2	0.2	10	10	10	W 3	NNW 3	NNE 3
7	84.6	84.4	84.3	84.4	−9.0	−7.6	−8.4	−8.4	−7.1	−10.2	92	90	89	90	0.3	0.3	0.3	0.3	10	10	10	NNE 6	NNE 6	NNE 5
8	83.6	84.3	86.3	84.7	−7.4	−6.6	−8.0	−7.5	−6.3	−9.2	90	88	87	88	0.3	0.4	0.4	0.4	10	10	10	N 9	N 6	N 7
9	86.9	87.8	88.6	87.8	−8.2	−5.1	−6.6	−6.6	−4.7	−9.5	89	93	91	91	0.3	0.3	0.3	0.3	10	10	10	NNE 6	NNE 6	NE 6
10	88.7	90.1	92.8	90.5	−0.7	0.0	−0.6	−0.5	0.7	−7.1	97	100	99	99	0.2	0.0	0.0	0.1	10	10	10	NE 5	NNE 3	WNW 3
11	95.1	97.6	99.0	97.2	−1.0	−0.5	0.3	−0.2	0.9	−1.4	99	100	87	95	0.1	0.0	0.8	0.3	10	10	9	S 5	SSW 3	SSW 2
12	99.7	101.0	101.7	100.8	−0.4	0.6	1.8	1.0	3.7	−0.6	98	96	88	94	0.1	0.3	0.9	0.4	9	10	1	SE 6	S 6	S 4
13	101.5	102.2	101.9	101.9	2.8	7.1	4.4	4.7	7.2	1.5	73	66	72	70	2.1	3.5	2.4	2.7	1	8	4	NNE 2	C 0	SW 1
14	101.8	103.0	104.0	102.9	3.7	3.4	2.2	2.9	7.0	1.3	88	98	98	95	1.0	0.1	0.2	0.4	3	9	10	NNE 4	N 6	NNE 5
15	104.4	105.3	104.3	104.7	2.3	5.3	4.8	4.3	6.6	1.3	98	92	86	92	0.1	0.7	1.2	0.7	4	9	0	E 1	C 0	ESE 2
16	102.6	102.0	100.0	101.5	4.0	8.0	4.4	5.2	8.5	3.2	98	73	82	84	0.1	2.9	1.6	1.5	9	9	7	N 3	NNE 1	SW 5
17	98.8	99.8	100.3	99.6	3.1	6.4	2.1	3.4	7.0	1.9	97	87	100	95	0.2	1.2	0.0	0.5	10	9	10	N 3	N 2	NE 5
18	99.5	100.1	98.3	99.3	2.5	5.0	4.6	4.2	6.0	1.4	98	97	97	97	0.1	0.3	0.3	0.2	9	9	9	NE 7	NNE 5	NE 3
19	95.2	94.5	93.7	94.5	6.6	8.0	4.8	6.0	9.2	3.9	68	87	96	84	3.1	1.3	0.3	1.6	1	9	2	ENE 4	N 3	SSE 4
20	93.6	95.3	96.5	95.1	4.1	5.9	3.4	4.2	6.3	2.3	97	92	89	93	0.3	0.8	0.8	0.6	10	10	10	ESE 2	C 0	NNW 1
21	97.3	98.0	97.1	97.5	1.8	3.3	1.5	2.0	3.8	1.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	N 4	N 1	NNE 6
22	95.3	95.7	95.7	95.6	3.3	5.3	3.8	4.0	7.6	0.8	98	93	89	93	0.1	0.6	0.9	0.5	8	10	4	NNE 1	E 1	NE 1
23	95.7	96.4	96.6	96.2	6.4	6.3	5.0	5.7	7.9	3.6	76	95	98	90	2.3	0.4	0.1	0.9	1	10	2	E 1	C 0	N 4
24	96.2	97.7	98.1	97.3	4.1	4.8	3.8	4.1	5.6	3.6	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	N 5	N 4	N 7
25	97.4	98.4	98.6	98.1	−1.0	−2.2	−5.2	−3.4	3.8	−5.4	99	98	95	97	0.1	0.1	0.2	0.1	10	10	8	N 7	N 7	NNE10
26	97.5	98.9	98.6	98.3	−7.2	−5.4	−6.0	−6.2	−5.2	−8.2	88	92	92	91	0.4	0.3	0.3	0.3	9	10	10	NNE12	N 8	N 7
27	96.1	97.2	97.4	96.9	−7.1	−5.1	−5.9	−6.0	−4.5	−7.9	91	95	92	93	0.3	0.2	0.3	0.3	10	10	10	NNE10	N 8	NNW 3
28	95.6	96.2	95.2	95.7	−6.1	−3.2	−4.8	−4.7	−3.0	−7.1	92	97	95	95	0.3	0.1	0.2	0.2	10	10	10	NNE 5	N 3	NNE 7
29	95.2	98.4	100.7	98.1	−5.5	−2.7	−4.8	−4.4	−1.8	−6.0	95	97	85	92	0.2	0.1	0.6	0.3	10	10	1	N 10	NNE 6	C 0
30	101.9	103.0	102.7	102.5	−3.5	−0.7	−0.8	−1.4	0.9	−4.8	71	72	91	78	1.3	1.6	0.5	1.1	1	10	9	WSW 2	SSE 1	SSW 1
31	101.8	101.8	100.0	101.2	0.0	2.0	0.9	1.0	2.3	−1.5	59	69	87	72	2.5	2.2	0.9	1.9	4	9	9	C 0	SSW 3	C 0
M	95.3	96.1	96.1	95.8	−1.0	0.9	−0.8	−0.4	2.1	−2.8	91	91	92	91	0.6	0.6	0.5	0.6	7.9	9.6	7.7	4.3	3.1	3.6

Czerwiec – Juin

1	99.0	100.6	101.6	100.4	0.5	3.9	3.0	2.6	5.2	−0.5	91	71	84	82	0.6	2.4	1.3	1.4	8	9	9	NNE 3	NW 2	N 2
2	102.8	104.8	105.7	104.4	3.0	6.2	5.7	5.2	8.9	1.9	89	70	84	81	0.9	2.9	1.5	1.8	7	7	4	NW 6	W 3	NE 2
3	106.6	106.9	104.7	105.1	5.8	10.1	7.0	7.5	12.5	4.8	76	53	80	70	2.2	5.9	2.0	3.4	1	6	7	C 0	SSW 4	SSE10
4	100.5	101.3	98.3	100.0	6.7	6.8	6.6	6.7	8.5	6.0	99	100	100	100	0.1	0.0	0.0	0.0	9	10	10	S 14	SSE 7	SSE 7
5	95.2	95.2	94.5	95.0	4.7	3.1	3.1	3.5	6.7	1.8	100	100	80	93	0.0	0.0	1.6	0.5	7	10	2	WSW 6	W 4	SSW 7
6	93.9	95.6	97.7	95.7	0.2	2.6	0.6	1.0	3.4	−0.2	98	58	71	76	0.1	3.1	1.8	1.7	9	6	1	NNW 7	WSW 8	SSE 4
7	98.3	99.2	99.1	98.9	2.6	6.2	6.0	5.2	8.0	0.0	98	82	90	90	0.2	1.8	1.0	1.0	8	7	10	SE 12	ESE10	SE 10
8	99.1	99.9	100.2	99.7	5.8	8.9	6.1	6.7	9.8	2.3	98	82	90	90	0.1	2.2	0.9	1.1	10	9	5	SSE 7	SW 7	SE 10
9	100.0	100.3	100.3	100.2	7.2	9.7	8.2	8.3	10.6	6.1	97	81	80	86	0.4	2.2	2.2	1.6	9	8	8	S 12	S 10	SSE 9
10	98.6	99.5	101.2	99.8	6.4	8.0	8.7	8.0	9.7	4.4	100	86	99	95	0.0	1.4	0.1	0.5	10	9	9	S 12	S 14	SSE 8
11	100.9	102.0	104.3	102.4	10.6	15.5	12.7	12.9	15.8	8.7	86	54	82	74	1.8	8.2	2.6	4.2	7	10	10	SSE17	S 12	S 17
12	107.7	110.4	113.6	110.6	14.9	18.2	13.6	15.1	19.5	11.8	42	62	48	51	9.7	7.9	8.1	8.6	9	10	9	SSE 8	N 4	ENE 6
13	113.0	113.0	110.9	112.3	13.0	13.8	4.9	9.2	15.8	4.7	53	87	100	80	7.1	2.0	0.0	3.0	9	6	8	SE 1	SSW 3	N 5
14	108.7	110.0	109.7	109.5	7.1	9.9	4.5	6.5	10.4	2.5	54	68	79	67	4.6	3.8	1.8	3.4	1	1	1	NNE 8	N 3	NNW 9
15	108.4	109.6	108.4	108.8	6.2	10.3	9.2	8.7	11.9	2.8	59	53	23	45	3.8	5.8	9.0	6.2	1	2	0	N 5	NNW 4	C 0
16	106.3	106.8	105.7	106.3	9.0	12.9	9.9	10.4	14.2	6.5	25	56	60	47	8.6	6.6	5.0	6.7	0	1	0	N 3	NNW 3	C 0
17	104.5	105.2	104.3	104.7	8.6	12.3	8.5	9.5	13.6	6.7	76	68	86	77	2.7	4.6	1.6	3.0	1	4	1	N 1	NW 4	SSW 4
18	103.5	103.8	102.2	103.2	9.4	12.4	9.0	10.0	13.1	7.0	76	73	88	79	2.8	4.0	1.4	2.7	1	7	7	NNW 2	NNW 1	SSE 8
19	100.4	100.3	100.6	100.4	8.2	7.1	8.7	8.2	10.7	6.6	80	100	68	83	2.2	0.0	3.5	1.9	10	9	9	N 2	S 2	N 5
20	101.1	101.3	102.0	101.5	9.6	9.5	6.9	8.2	11.9	6.6	71	99	100	90	3.5	0.2	0.0	1.2	1	9	10	N 1	WSW 7	N 3
21	103.0	102.8	101.2	102.3	7.4	8.6	8.0	8.0	9.8	5.0	75	91	100	89	2.6	1.0	0.0	1.2	9	9	9	C 0	SSW 3	SW 9
22	99.2	98.4	96.3	98.0	9.8	10.2	8.8	9.4	12.9	7.7	97	100	86	94	0.4	0.0	1.6	0.7	8	7	9	SW 12	SSW14	SW 8
23	99.1	100.7	99.0	99.6	9.4	10.5	8.6	9.3	12.5	6.7	63	81	100	81	4.4	2.4	0.0	2.3	2	8	7	SW 3	WSW 7	SSW 9
24	98.9	97.5	94.3	96.9	9.7	12.9	11.7	11.5	14.2	8.0	96	78	86	87	0.5	3.3	1.8	1.9	7	9	9	SSW12	SSW17	SSW17
25	96.9	99.6	100.8	99.1	8.5	12.2	3.9	7.1	12.4	3.6	48	56	100	68	5.8	6.3	0.0	4.0	1	3	10	WSW 7	W 3	NW 5
26	100.0	101.4	103.6	101.7	−0.4	0.5	0.4	0.2	3.9	−1.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	ENE 6	NNW 8	NNW 6
27	104.6	105.6	107.4	105.9	−0.9	2.4	0.7	0.7	2.8	−2.0	99	83	100	94	0.0	1.3	0.0	0.4	5	8	10	N 6	NNW 5	N 6
28	107.2	108.9	109.1	108.4	1.0	8.7	7.3	5.1	11.6	−1.2	84	46	92	74	1.1	6.1	0.8	2.7	1	4	9	NNE 6	N 4	N 5
29	109.9	111.2	110.7	110.6	8.9	12.0	10.3	10.4	15.0	6.0	100	86	96	94	0.0	2.0	0.5	0.8	10	8	7	NNE 4	NNW 2	N 5
30	110.1	110.3	109.8	110.1	11.0	16.8	12.0	13.0	17.6	9.0	88	50	71	70	1.6	9.7	4.1	5.1	1	3	6	N 4	NNE 2	N 3
31																								
M	102.6	103.4	103.2	103.1	6.8	9.4	7.2	7.6	11.1	4.4	81	76	84	82	2.3	3.2	1.8	2.4	5.7	7.0	6.9	6.8	5.9	6.6

Kasprowy Wierch

H_a = 1991 m H_b = 1988,8 m h_w = 15,4 m

Maj – Mai 1957

DNI	WIELKOŚĆ OPADU	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	1	5.5	64	0.2	
2	8	0.3	63	0.3	
3	1	3.1	58	.	
4	0	2.2	56	1.5	
5	8	6.8	57	4.8	
6	0	14.3	62	0.2	
7	0	17.9	76	.	
8	0	33.9	95	.	
9	0	4.3	126	.	
10	1	3.6	130	.	
11	0	0.0	128	1.2	
12	6	0.5	122	7.0	
13	8	0.7	104	7.8	
14	7	3.9	92	6.6	
15	7	.	80	4.7	
16	8	.	78	5.9	
17	6	31.0	70	2.2	
18	7	0.0	64	2.3	
19	8	5.9	54	8.7	
20	8	33.6	45	0.5	
21	1	2.4	39	.	
22	1	0.0	30	2.1	
23	1	9.8	25	5.2	
24	0	6.8	17	0.5	
25	0	0.6	11	.	
26	7	1.3	10	2.1	
27	0	3.0	pł.	.	
28	0	12.6	2	.	
29	7	6.0	15	1.4	
30	8	0.0	19	4.9	
31	8	0.1	10	5.3	
Σ	—	210.1	—	75.4	UWAGI:

Czerwiec – Juin

1	8	.	6	4.6	
2	7	.	5	5.6	
3	7	.	pł.	11.8	
4	0	3.6	pł.	0.4	
5	0	12.0	pł.	1.9	
6	9	0.0	pł.	4.8	
7	9	9.0	pł.	5.1	
8	8	0.2	pł.	3.0	
9	8	25.1	pł.	4.7	
10	9	0.2	pł.	3.2	
11	9	.	pł.	11.0	
12	8	7.7	pł.	3.1	
13	9	.	pł.	7.7	
14	9	.	pł.	15.4	
15	9	.	pł.	15.1	
16	9	.	.	15.9	
17	9	.	.	13.0	
18	9	20.4	.	7.0	
19	8	11.3	.	1.1	
20	6	1.1	.	4.0	
21	7	0.0	.	2.5	
22	8	7.1	.	4.2	
23	9	1.1	.	8.7	
24	9	3.4	.	5.5	
25	9	7.6	.	11.7	
26	0	0.7	.	.	
27	8	0.0	.	2.8	
28	8	.	.	12.2	
29	7	.	.	5.3	
30	8	.	.	11.4	
31					
Σ	—	110.5	—	202.7	UWAGI:

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Lipiec – Juillet 1957

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	108.4	108.9	108.2	108.5	12.3	16.4	12.4	13.4	18.5	10.0	74	60	82	72	3.8	7.5	2.4	4.6	6 ⊙	3 ⊙	3	N 4	N 4	NE 1
2	107.4	106.9	106.2	106.8	12.8	14.1	11.0	12.2	17.0	9.2	78	66	82	75	3.3	5.4	2.4	3.7	2 ⊙	7	9	NW 1	WNW 5	C 0
3	105.6	106.5	106.3	106.1	9.1	10.7	8.8	9.4	12.1	7.4	100	93	88	94	0.0	0.9	1.3	0.7	10 ●≡	9	1	N 3	N 1	SW 2
4	106.5	108.1	109.0	107.9	10.4	14.8	13.8	13.2	17.4	7.7	62	57	71	63	4.8	7.2	4.6	5.5	5 ⊙	5 ⊙	1	N 3	N 2	SW 3
5	109.6	109.9	109.4	109.6	16.2	20.4	16.7	17.5	23.0	13.0	36	50	61	49	11.8	11.9	7.5	10.4	1 ⊙	1 ⊙	3	W 2	BSE 4	SW 5
6	108.8	109.6	109.5	109.3	14.7	16.9	13.6	14.7	17.5	13.1	76	76	82	78	3.9	4.5	2.8	3.7	1 ⊙	6	1	NW 1	WNW 3	WNW 2
7	108.9	110.3	110.0	109.7	15.9	17.4	15.3	16.0	19.2	9.1	44	54	77	58	10.1	9.2	4.0	7.8	9	5 ⊙	1	WNW 5	N 3	W 3
8	109.2	109.4	107.3	108.6	16.4	19.7	15.6	16.8	21.1	14.6	75	56	78	70	4.5	10.0	3.9	6.1	0 ⊙	6 ⊙	9	C 0	SW 4	S 7
9	104.1	103.8	102.4	103.4	13.6	12.2	9.0	11.0	16.6	8.4	77	100	100	92	3.6	0.0	0.0	1.2	5 ⊙	10 ≡	3	S 8	NW 3	NNE 4
10	100.3	99.5	97.0	98.9	9.4	12.1	8.9	9.8	13.0	7.3	94	89	87	90	0.7	1.5	1.5	1.2	8 ⊙	9 ⊙	10 ●	C 0	C 0	SSE 5
11	93.6	94.8	95.6	94.7	9.7	9.6	9.0	9.3	11.3	6.5	84	100	94	93	2.0	0.0	0.7	0.9	8	10 ●≡	9 ●	ESE 6	W 5	NE 5
12	95.5	97.6	98.9	97.3	8.2	10.0	8.8	9.0	10.4	7.5	99	100	100	100	0.2	0.0	0.0	0.1	10	10 ●≡	10 ≡	C 0	N 1	N 6
13	101.4	103.4	104.9	103.2	8.3	10.7	10.1	9.8	11.2	7.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	N 6	NNE 3	NE 2
14	104.0	103.9	102.2	103.4	9.5	9.3	10.2	9.8	11.6	7.9	99	100	64	88	0.2	0.0	4.6	1.6	8	10 ●≡	8	SW 3	NE 1	S 6
15	100.5	100.3	99.8	100.2	9.0	9.7	8.0	8.7	10.8	7.5	91	100	100	97	1.0	0.0	0.0	0.3	10	10 ●≡	9	C 0	C 0	C 0
16	94.9	94.2	95.2	94.8	6.4	7.1	3.1	4.9	8.4	2.7	92	100	100	97	0.8	0.0	0.0	0.3	9	10 ●≡	10 ●≡	C 0	SW 3	NW 10
17	94.8	96.4	97.7	96.3	3.3	3.6	3.6	3.5	4.4	1.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●≡	10 ≡	NW 12	WNW 6	NW 6
18	98.3	99.2	98.9	98.8	3.6	5.1	5.6	5.0	8.0	2.3	100	96	87	94	0.0	0.3	1.2	0.5	10 ≡	10 ●	2	N 5	WNW 3	WSW 2
19	98.3	98.9	98.4	98.5	6.5	8.5	8.0	7.8	10.2	4.6	65	80	97	81	3.4	2.2	0.3	2.0	1 ⊙	8 ⊙	8	S 5	SW 6	S 10
20	96.5	96.0	93.6	95.4	8.1	10.8	6.9	8.2	11.5	6.7	94	81	100	92	0.7	2.6	0.0	1.1	8 ⊙	9 ●	9 ●	SSW10	SE 7	SSE 3
21	91.6	92.1	92.8	92.2	5.0	5.6	5.2	5.2	6.9	3.8	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡	10 ●≡	10	SSW 3	WNW 5	W 4
22	90.9	90.7	91.1	90.9	5.0	5.6	4.0	4.6	6.2	3.1	98	98	100	99	0.1	0.2	0.0	0.1	10	10 ●	10 ≡	C 0	C 0	WNW 2
23	89.4	91.0	93.3	91.2	3.9	5.0	5.5	5.0	6.6	2.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●≡	10 ≡	S 5	SW 1	NNE 2
24	94.5	96.1	97.8	96.1	5.8	5.8	3.8	4.8	6.2	3.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●≡	10 ●≡	W 2	N 7	N 6
25	97.8	99.1	98.5	98.5	3.0	4.3	5.1	4.4	5.6	2.2	100	98	100	99	0.0	0.1	0.0	0.0	8	9	10	NW 4	SSW 6	W 10
26	97.5	99.1	98.5	98.4	3.7	7.3	5.6	5.6	8.2	3.0	100	54	100	85	0.0	4.6	0.0	1.5	10 ≡	6	10 ●	W 10	NW 5	SSW10
27	96.2	95.6	95.0	95.6	5.7	6.6	5.1	5.6	7.5	3.9	100	100	100	100	0.0	0.0	0.0	0.0	9	10 ●	10 ●≡	SW 10	WSW14	WNW 4
28	93.8	95.5	96.5	95.3	2.1	4.1	3.6	3.4	5.9	1.2	100	100	88	96	0.0	0.0	0.9	0.3	10	9	6	SW 4	NW 3	WNW 3
29	96.9	99.0	101.3	99.1	3.1	6.4	5.0	4.9	8.6	1.8	91	75	76	81	0.7	2.4	2.0	1.7	3 ⊙	8	1	SSW 6	SW 4	C 0
30	101.5	103.1	104.3	103.0	4.1	6.1	5.1	5.1	7.7	3.2	89	100	100	96	0.9	0.0	0.0	0.3	8	10 ≡	8	SW 2	SW 1	W 3
31	104.7	106.6	107.7	106.3	4.2	6.2	5.2	5.2	7.4	3.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	N 4	N 3	NNE 3
M	100.0	100.8	100.9	100.6	8.0	9.7	8.1	8.5	11.3	6.0	88	87	91	89	1.8	2.3	1.3	1.8	7.4	8.8	7.1	4.0	3.6	4.1

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1	107.2	108.1	107.7	107.7	5.8	8.6	7.6	7.4	9.7	3.6	90	93	100	94	0.9	0.9	0.0	0.6	3 ⊙	8	10 ≡	C 0	SW 3	SSW 3
2	106.9	107.0	106.5	106.8	8.5	10.1	6.3	7.8	10.9	5.8	57	92	100	83	4.8	1.1	0.0	2.0	1 ⊙	9	10 ≡	C 0	NNE 2	N 4
3	103.8	104.3	104.4	104.2	2.1	6.4	2.9	3.6	7.4	1.2	100	82	100	94	0.0	1.8	0.0	0.6	10 ≡	6 ⊙	10 ≡	NNE 3	N 3	N 2
4	103.1	104.7	105.3	104.4	1.3	5.4	4.0	3.7	6.8	0.0	94	85	100	93	0.4	1.4	0.0	0.6	9	9	10 ≡	NNE 7	NNE 3	N 3
5	105.0	106.3	106.4	105.9	3.2	5.9	5.2	4.9	7.3	2.3	100	92	100	97	0.0	0.8	0.0	0.3	8	9	10 ●≡	NNE 3	NNE 4	N 5
6	106.3	107.0	106.1	106.5	5.7	8.2	7.3	7.1	10.4	3.5	82	91	94	89	1.6	1.0	0.6	1.1	1 ⊙	9	4	SSE 1	C 0	SW 3
7	104.2	103.4	100.6	102.7	6.6	9.8	8.1	8.2	11.4	5.4	82	71	100	84	1.8	3.5	0.0	1.8	7 ⊙	8	9	S 7	SW 6	SW 10
8	97.2	98.0	97.8	97.7	6.3	7.7	5.6	6.3	8.4	5.1	100	91	95	95	0.0	1.0	0.5	0.5	10	9	3	NW 8	N 6	NNW 3
9	96.8	97.4	95.8	96.7	6.9	10.7	8.0	8.4	11.7	4.6	71	77	100	83	2.9	2.9	0.0	1.9	8 ⊙	8	10 ≡	WSW 3	SW 3	S 10
10	92.6	95.3	99.0	95.6	9.7	9.0	8.0	8.7	10.4	7.3	100	100	78	93	0.0	0.0	2.4	0.8	10 ≡	10 ≡	2	S 14	WNW 4	W 7
11	102.7	104.5	104.4	103.9	9.4	12.8	10.7	10.9	13.9	7.3	74	70	92	79	3.1	4.4	1.1	2.9	6 ⊙	7	2	SSW 7	SW 6	S 10
12	101.5	102.7	103.0	102.4	11.4	14.9	11.9	12.5	16.2	10.4	84	68	90	81	2.2	5.4	1.3	3.0	1 ⊙	5 ⊙	2	S 12	WSW 6	S 5
13	102.9	104.8	103.8	103.8	11.3	13.1	12.6	12.4	16.1	9.7	92	98	98	96	1.1	0.4	0.4	0.6	4 ⊙	8	4	C 0	SW 1	SSW 7
14	102.2	103.3	100.0	101.8	13.5	18.7	14.3	15.2	18.9	11.3	79	62	62	68	3.2	8.1	6.2	5.8	1 ⊙	4 ⊙	10	S 12	SW 5	SW 14
15	98.0	98.5	99.2	98.6	10.7	11.4	8.3	9.7	14.3	8.0	62	80	93	78	5.0	2.7	0.9	2.9	8 ⊙	7 ⊙	3	SW 7	WSW 5	C 0
16	99.0	99.5	98.5	99.0	7.2	11.5	8.4	8.9	13.0	6.4	100	96	100	99	0.0	0.6	0.0	0.2	2 ⊙	10	9	SSW 5	N 1	S 2
17	96.4	97.6	98.4	97.5	2.9	3.1	2.6	2.8	8.4	1.4	100	100	89	96	0.0	0.0	0.9	0.3	10 ●≡	10●≡	7	N 3	C 0	W 7
18	97.5	98.7	99.0	98.4	2.3	4.7	4.6	4.0	7.9	0.9	87	92	93	91	1.0	0.6	0.6	0.7	2 ⊙	8 ●	5	SW 3	SW 3	SSW 7
19	99.5	100.9	101.8	100.7	5.5	8.1	6.4	6.6	9.6	3.6	82	91	100	91	1.6	1.0	0.0	0.9	9	10	10●≡	C 0	C 0	NNE 1
20	101.5	102.6	103.7	102.6	4.9	5.7	5.4	5.4	6.4	4.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ●● ≡	10 ●● ≡	8	NE 5	NNE 4	NNE 6
21	101.9	101.7	99.7	101.1	5.4	8.1	7.4	7.1	9.7	3.5	92	97	90	93	0.8	0.3	1.0	0.7	2 ⊙	10 ≡	10	ENE 2	E 1	C 0
22	95.7	95.4	95.9	95.7	6.6	3.0	0.7	2.8	7.4	0.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10●≡	10 ≡	C 0	NNE 5	N 6
23	96.0	97.6	97.6	97.1	−0.9	4.6	3.1	2.5	6.6	−1.6	99	100	87	95	0.0	0.0	1.0	0.3	7 ⊙	6	1	N 3	NNW 2	S 8
24	97.4	97.9	98.7	98.0	4.0	7.3	5.6	5.6	7.9	0.6	74	80	100	85	2.1	2.0	0.0	1.4	2 ⊙	3 ⊙	10●≡	SSW 9	S 12	S 10
25	101.6	102.5	100.1	101.4	3.6	9.1	4.1	5.2	9.2	1.5	56	56	93	68	3.5	5.0	0.6	3.0	1 ⊙	3 ⊙	4	W 2	SW 4	SSE 8
26	98.3	98.1	98.7	98.4	5.0	4.5	1.8	3.3	6.6	1.5	78	100	90	89	2.0	0.0	0.7	0.9	6 ⊙	10●≡	9	N 1	SW 3	NW 6
27	98.9	99.9	99.7	99.5	0.8	4.1	3.0	2.7	5.9	−0.5	84	85	89	86	1.1	1.2	0.9	1.1	1 ⊙	9	6	W 2	SSW 2	SW 4
28	96.8	98.6	98.9	98.1	2.4	3.6	3.6	3.3	5.0	1.2	100	100	100	100	0.0	0.0	0.0	0.0	10●≡	10	10●≡	S 10	SSW 7	SSW 3
29	96.3	98.3	100.9	98.5	0.9	0.4	0.7	0.7	3.6	−0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ✱≡	10 ✱≡	10 ≡	N 10	N 12	N 9
30	101.1	102.5	102.6	102.1	−0.1	1.2	0.9	0.7	1.5	−0.7	100	100	85	95	0.0	0.0	0.8	0.3	10 ≡	10	7	N 5	NNE 1	W 2
31	101.7	102.3	101.1	101.7	−0.1	3.3	1.1	1.4	4.0	−0.9	94	74	100	89	0.4	2.0	0.0	0.8	3 ⊙	9	10 ✱	SSW 7	WSW 4	SSW 5
M	100.3	101.3	101.1	100.9	5.3	7.6	5.8	6.1	9.2	3.4	88	88	94	90	1.3	1.6	0.6	1.2	5.9	8.2	7.3	4.9	3.6	5.5

Kasprowy Wierch — H_s = 1991 m — H_b = 1958,8 m — h_w = 15,4 m — Lipiec – Juillet 1957

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONIECZNIENIE	POGODA
1	8	.	.	12.8	
2	8	26.7	.	5.3	
3	8	4.1	.	4.2	
4	8	.	.	13.9	
5	8	.	.	14.6	
6	6	.	.	10.1	
7	9	12.6	.	8.2	
8	8	0.5	.	11.2	
9	1	0.0	.	3.9	
10	7	24.4	.	2.9	
11	1	4.6	.	2.2	
12	0	8.4	.	.	
13	0	2.7	.	.	
14	1	7.7	.	1.0	
15	0	39.6	.	0.1	
16	0	37.1	.	.	
17	0	5.7	.	0.6	
18	7	0.0	.	3.0	
19	8	0.0	.	10.1	
20	8	4.9	.	1.7	
21	1	5.5	.	.	
22	5	15.2	.	.	
23	0	6.0	.	0.1	
24	1	39.5	.	.	
25	8	6.0	.	0.8	
26	8	4.0	.	7.4	
27	8	12.3	.	0.1	
28	7	0.4	.	0.3	
29	9	.	.	8.5	
30	1	0.4	.	2.5	
31	1	0.1	.	0.4	
Σ	—	268.4	—	125.9	UWAGI.

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONIECZNIENIE	POGODA
1	8	.	.	3.1	
2	7	.	.	6.2	
3	9	.	.	4.6	
4	8	0.2	.	2.5	
5	8	1.2	.	1.9	
6	9	.	.	4.8	
7	0	3.8	.	6.2	
8	7	0.0	.	1.5	
9	8	.	.	6.5	
10	0	0.6	.	3.8	
11	9	.	.	11.7	
12	9	.	.	10.8	
13	8	0.3	.	5.9	
14	8	3.9	.	9.7	
15	9	.	.	7.5	
16	8	5.1	.	7.6	
17	0	8.9	.	1.7	
18	8	0.0	.	8.3	
19	9	6.2	.	1.7	
20	1	1.7	.	0.1	
21	1	6.9	.	4.4	
22	0	18.5	.	.	
23	8	.	.	9.3	
24	9	8.8	.	8.2	
25	9	.	.	12.0	
26	1	0.5	.	2.1	
27	8	1.9	.	4.6	
28	7	16.3	.	1.1	
29	0	20.8	.	.	
30	7	0.1	3	0.3	
31	8	1.1	.	2.9	
Σ	—	106.8	—	131.0	UWAGI.

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Wrzesień – Septembre 1957

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	100.5	101.9	102.8	101.7	0.5	2.3	1.8	1.6	4.0	−0.6	94	85	81	87	0.4	1.1	1.4	1.0	7	7	9	W 9	WSW 6	SW 7
2	102.4	103.1	101.6	102.4	2.3	4.7	4.6	4.0	5.4	0.8	80	86	93	86	1.5	1.1	0.6	1.1	7	9	10	SSW 7	WSW 7	SSW 8
3	99.1	100.1	99.7	99.6	4.0	5.9	4.5	4.7	6.6	3.2	100	100	91	97	0.0	0.0	0.7	0.2	9	10	10 ●	S 7	SW 4	SE 2
4	98.8	100.7	102.6	100.7	4.2	3.6	2.8	3.4	4.5	2.5	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	NE 4	NNE 6	NNE 9
5	103.2	103.7	103.9	103.6	3.8	7.2	6.5	6.0	8.0	1.7	100	100	87	96	0.0	0.0	1.3	0.4	10	10	0	NNE 3	SW 2	SSW 2
6	102.2	103.1	103.5	102.9	6.4	8.1	6.0	6.6	9.3	5.5	70	85	78	78	2.8	1.6	2.0	2.1	2 ⊙	7	5	C 0	N 1	NE 2
7	104.1	105.8	106.7	105.5	6.3	12.2	7.3	8.3	12.8	4.3	80	59	95	78	1.8	5.8	0.5	2.7	2 ⊙	4 ⊙	2	NE 4	S 1	SSW 5
8	107.7	109.4	109.4	108.8	10.2	13.0	9.1	10.4	13.9	6.4	41	58	79	59	7.3	6.4	2.5	5.4	1 ⊙	2 ⊙	1	SSW 3	SW 5	SSW 6
9	108.7	109.6	109.0	109.1	7.7	12.1	9.0	9.4	14.7	6.8	94	72	85	84	0.6	3.9	1.8	2.1	1 ⊙	2 ⊙	3	S 9	SW 7	SSE 3
10	106.8	105.4	103.0	105.1	8.0	9.6	6.2	7.5	11.1	5.8	73	86	100	86	3.0	1.7	0.0	1.6	9 ⊙	10	2	S 2	SW 4	SW 7
11	99.9	98.7	95.8	98.1	6.6	9.1	5.5	6.7	10.6	3.7	13	65	77	52	8.5	4.1	2.0	4.9	1 ⊙	3 ⊙	10	SW 3	WSW 5	S 6
12	91.8	90.6	92.6	91.7	6.8	6.4	0.6	3.6	6.9	−0.3	100	100	96	99	0.0	0.0	0.3	0.1	10	9	9	SSW10	S 14	NW 10
13	94.1	95.2	92.5	93.9	−0.7	1.4	−0.3	0.0	2.4	−1.1	75	81	100	85	1.5	1.4	0.0	1.0	9 ⊙	9	10	SSW10	SSW 9	S 10
14	92.6	93.8	92.0	92.8	−1.3	2.4	2.2	1.4	3.5	−2.0	86	72	100	86	0.8	2.1	0.0	1.0	3 ⊙	9	10	SW 8	SSW 6	S 10
15	89.4	93.4	97.2	93.3	−2.5	−1.7	−1.2	−1.6	2.8	−3.1	98	98	95	97	0.1	0.1	0.3	0.2	10	9	10	WNW 9	SW 5	WNW 6
16	98.1	98.5	98.7	98.4	−2.2	0.8	−2.1	−1.4	2.4	−2.7	98	88	94	93	0.1	0.8	0.3	0.4	9	7	1	SE 3	C 0	SW 4
17	97.7	98.2	97.1	97.7	−4.1	−2.2	−2.5	−2.8	−1.6	−5.0	96	98	98	97	0.2	0.1	0.1	0.1	9	10	10	NNW 4	NW 7	W 7
18	94.4	95.1	96.7	95.4	−1.9	−2.0	−1.6	−1.8	−1.4	−2.9	98	98	98	98	0.1	0.1	0.1	0.1	10	10	10	NW 10	NW 7	WNW 9
19	95.6	95.9	95.9	95.8	−2.4	0.8	3.4	1.3	3.6	−3.5	81	96	100	92	0.9	0.3	0.0	0.4	2 ⊙	10	10	WSW 7	WSW10	WNW10
20	94.6	96.3	98.3	96.4	3.5	3.1	2.0	2.6	3.9	1.4	63	91	96	83	2.8	0.7	0.3	1.3	9	10	10	W 10	WNW10	WNW 8
21	98.8	100.1	100.9	99.9	3.4	5.8	3.4	4.0	7.0	1.6	100	82	95	92	0.0	1.6	0.4	0.7	10	8 ⊙	0	W 8	WSW 5	NNW 3
22	99.7	100.4	100.4	100.2	5.3	7.0	6.4	6.3	7.8	3.3	60	89	98	82	3.6	1.1	0.1	1.6	6 ⊙	9	2	S 7	S 9	SSW 7
23	97.0	93.0	92.2	94.1	6.2	6.7	4.9	5.7	6.9	4.7	100	99	98	99	0.0	0.1	0.2	0.1	8	10	10 ●	S 10	SSW20	W 14
24	93.3	94.8	93.8	94.0	2.6	5.7	4.0	4.1	5.8	1.9	100	84	100	95	0.0	1.5	0.0	0.5	10	9	10 ●	NW 12	SW 10	W 10
25	94.8	97.4	98.4	96.9	−4.9	−1.3	−4.3	−3.7	4.0	−6.3	43	48	74	55	2.4	2.9	1.1	2.1	5 ⊙	1 ⊙	1	NW 10	WNW 7	WNW 4
26	96.0	95.7	95.8	95.8	−1.1	−2.5	−2.8	−2.3	0.1	−5.1	21	98	97	72	4.4	0.1	0.1	1.5	8	10	10	W 3	S 3	NW 1
27	96.1	97.7	95.1	96.3	−6.5	−3.1	−2.0	−3.4	−0.6	−7.8	94	95	48	79	0.2	0.3	2.8	1.1	2 ⊙	3 ⊙	10	NNE 6	NNW 4	WSW 6
28	91.5	92.4	92.7	92.2	−2.5	−2.1	−1.7	−2.0	−1.2	−3.5	98	98	98	98	0.1	0.1	0.1	0.1	10	10	10	WNW17	WNW12	WNW10
29	91.8	89.4	86.5	89.2	−1.4	−0.1	0.9	0.1	0.9	−2.1	99	100	100	100	0.1	0.0	0.0	0.0	10	10	10 ●	WSW10	S 17	S 14
30	87.1	89.8	94.0	90.3	−3.4	−4.5	−6.3	−5.1	1.4	−6.8	97	96	94	96	0.2	0.2	0.2	0.2	10	9	10	NNW 3	NW 5	NNW 1
31																								
M	97.6	98.3	98.3	98.1	1.8	3.6	2.2	2.4	5.2	0.0	82	87	92	87	1.4	1.3	0.6	1.1	7.0	7.9	7.2	6.9	6.9	6.7

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1	94.8	95.6	97.1	95.8	−6.2	−4.2	−4.9	−5.0	−3.8	−8.3	84	96	95	92	0.6	0.2	0.2	0.3	9	10	10	SW 6	WSW 2	N 3
2	99.1	100.4	100.5	100.0	−6.8	−2.8	−5.4	−5.1	−2.7	−7.4	94	97	90	94	0.2	0.1	0.4	0.2	9	10	0	N 4	C 0	SSW 5
3	97.6	97.2	96.1	97.0	−5.7	−1.8	−1.8	−2.8	−0.4	−6.8	82	83	51	72	0.7	0.9	2.7	1.4	1 ⊙	1 ⊙	6	S 3	SSW 6	WSW 5
4	94.6	95.3	98.9	96.3	−3.7	−6.9	−7.5	−6.4	−1.2	−8.7	94	94	93	94	0.3	0.2	0.2	0.2	10	10	10	WNW10	NNW 8	N 6
5	101.8	102.5	102.6	102.3	−6.4	−2.4	0.7	−1.8	0.7	−8.2	94	93	22	70	0.2	0.3	5.0	1.8	10	1 ⊙	0	N 4	SW 7	SSW 6
6	101.3	103.2	105.6	103.4	1.0	0.1	−1.2	−0.3	1.6	−2.0	25	94	95	71	5.0	0.4	0.3	1.9	8	8	9	W 6	N 3	NNW 2
7	105.8	106.8	107.2	106.6	6.3	5.6	4.4	5.2	7.0	−2.6	18	72	62	51	7.8	2.5	3.2	4.5	6 ⊙	1 ⊙	0	W 4	N 1	NNE 5
8	107.4	109.0	109.9	108.8	5.4	6.8	6.1	6.1	9.4	3.7	49	75	55	60	4.6	2.4	4.2	3.7	0 ⊙	1 ⊙	0	NE 3	SSW 3	C 0
9	108.8	109.2	108.6	108.9	6.7	8.9	8.1	8.0	9.7	2.5	34	38	11	28	6.6	7.0	9.6	7.7	0 ⊙	0 ⊙	1	SSE 2	SW 3	S 6
10	107.0	107.6	106.8	107.1	7.7	9.1	6.0	7.2	9.6	5.2	12	26	30	23	9.2	8.7	6.7	8.2	2 ⊙	1 ⊙	0	S 10	SW 7	S 8
11	105.7	106.0	105.8	105.8	7.5	7.7	8.9	8.2	9.6	5.4	11	45	17	24	9.3	5.8	9.4	8.2	0 ⊙	1 ⊙	0	SSE 7	S 5	SSW 5
12	104.7	105.6	107.1	105.8	7.2	9.4	3.2	5.8	10.4	2.8	21	54	100	58	8.0	5.4	0.0	4.5	1 ⊙	4 ⊙	10	SSW 1	WNW 1	NNE 6
13	107.8	108.4	107.5	107.9	2.3	4.2	4.2	3.7	4.5	1.5	100	100	65	88	0.0	0.0	2.9	1.0	10	10	1	W 1	C 0	SSW 6
14	106.1	105.1	106.3	106.2	4.8	6.2	2.2	3.8	6.8	1.7	67	87	100	85	2.8	1.3	0.0	1.4	1 ⊙	1 ⊙	10	SSE 2	SSW 1	C 0
15	106.7	107.2	107.3	107.1	1.2	3.6	5.6	4.0	5.6	0.4	100	97	23	73	0.0	0.3	7.0	2.4	10	9	0	C 0	WSW 1	C 0
16	106.4	106.5	105.4	106.1	6.8	5.6	5.4	5.8	6.8	3.0	19	60	38	39	8.0	3.6	5.6	5.7	1 ⊙	1 ⊙	0	S 2	S 4	S 7
17	104.0	105.2	105.2	104.8	6.1	8.4	5.9	6.6	8.8	4.3	38	68	76	61	5.8	3.6	2.2	3.9	0 ⊙	1 ⊙	1	SW 9	W 5	WSW 7
18	102.8	102.3	102.5	102.5	4.3	6.2	7.2	6.2	7.3	3.3	100	59	63	74	0.0	3.8	3.8	2.6	9	9	8	SW 12	SW 14	S 10
19	100.6	99.5	97.4	99.1	6.6	9.5	4.4	6.2	9.6	3.7	62	62	100	75	3.7	4.4	0.0	2.7	3 ⊙	7 ⊙	7	S 14	SSW14	S 17
20	95.8	96.5	96.9	96.4	6.0	4.7	−0.3	2.5	7.9	−0.6	76	100	100	92	2.3	0.0	0.0	0.8	7 ⊙	10	10 ●	SSW 8	C 0	NNE 4
21	96.9	96.8	95.2	96.3	−2.7	−1.0	0.9	−0.5	2.0	−2.9	95	99	31	75	0.2	0.1	4.6	1.6	6	9	2	NE 5	SSW 4	SSW 2
22	90.9	89.3	87.9	89.4	−1.5	0.1	1.2	0.2	1.5	−2.3	99	100	100	100	0.1	0.0	0.0	0.0	9	10	10 ●	SSE 8	S 10	SSE 8
23	88.4	91.1	95.4	91.6	−1.2	−1.4	−2.0	−1.6	1.6	−2.7	99	99	98	99	0.1	0.1	0.1	0.1	10	10	10	NE 3	NNE 4	C 0
24	96.7	99.2	102.2	99.4	0.5	1.3	0.9	0.9	1.7	−3.5	22	20	100	47	5.0	5.4	0.0	3.5	3	4 ⊙	10	SW 4	W 2	N 4
25	103.5	105.0	105.6	104.7	−1.3	5.4	4.7	3.4	7.4	−2.5	70	38	28	45	1.7	5.6	6.2	4.5	1	1 ⊙	0	C 0	SSW 2	S 8
26	104.8	105.5	105.1	105.1	2.6	4.0	4.5	3.9	5.1	1.3	62	61	36	53	2.8	3.2	5.4	3.8	3	1 ⊙	0	WSW 2	SSW 6	SSW 5
27	103.3	103.1	102.2	102.9	4.6	6.5	4.6	5.1	6.7	3.5	59	68	46	58	3.5	3.2	4.7	3.8	1	0 ⊙	1	SSW 5	S 5	SSE 7
28	101.5	101.9	102.2	101.9	4.6	4.0	4.8	4.6	5.9	2.6	42	79	64	62	5.0	1.6	3.1	3.2	3	1 ⊙	1	SSW 3	SSW 5	S 8
29	102.3	102.6	102.4	102.4	4.3	6.5	5.2	5.3	6.6	3.0	57	72	61	63	3.6	2.7	3.4	3.2	1	4 ⊙	2	S 9	S 4	S 8
30	101.5	101.2	101.4	101.4	5.3	7.0	6.3	6.2	7.8	3.5	51	25	64	47	4.4	7.5	3.4	5.1	7	7	7	SSW 9	S 9	S 8
31	100.4	100.2	98.9	99.8	5.8	7.0	6.1	6.2	7.7	5.3	73	73	50	65	2.5	2.7	4.6	3.3	7	1 ⊙	3	SSW 7	SSW 5	WSW 5
M	101.6	102.1	102.4	102.0	2.3	3.8	2.9	3.0	5.2	−0.1	62	72	63	66	3.4	2.7	3.2	3.1	4.8	4.6	4.2	5.4	4.5	5.5

Kasprowy Wierch

$H_3 = 1991$ m $H_s = 1988{,}8$ m $h_w = 15{,}4$ m

Wrzesień – Septembre 1957

DNI	WYSOKOŚĆ CHMUR v	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	8	.	.	3.7	
2	8	7.4	.	1.7	
3	8	13.3	.	0.3	
4	0	19.2	.	.	
5	1	.	.	6.3	
6	9	.	.	9.8	
7	9	.	.	10.8	
8	8	.	.	12.4	
9	8	.	.	11.3	
10	8	0.1	.	4.2	
11	9	3.1	.	10.4	
12	9	13.0	.	0.1	
13	9	0.6	.	3.3	
14	9	17.4	.	3.2	
15	7	0.0	1	2.7	
16	9	0.0	.	4.2	
17	0	0.2	.	0.6	
18	0	2.5	.	0.5	
19	7	1.9	3	4.5	
20	7	0.0	.	.	
21	8	.	.	1.9	
22	8	0.0	.	2.9	
23	8	10.0	.	.	
24	8	7.2	.	2.2	
25	9	.	.	10.8	
26	6	5.3	.	1.5	
27	8	0.4	5	10.4	
28	0	6.2	2	.	
29	0	5.0	5	.	
30	6	1.7	2	0.3	
31					
Σ	–	114.6	–	120.0	UWAGI.

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DNI	WYSOKOŚĆ CHMUR v	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	0	0.3	4	0.1	
2	7	0.0	4	4.1	
3	8	0.0	3	10.9	
4	1	4.5	2	0.1	
5	9	.	10	9.2	
6	9	.	3	4.2	
7	9	.	2	10.7	
8	9	.	p2.	10.7	
9	9	.	p2.	10.7	
10	9	.	p2.	10.6	
11	9	.	p2.	10.6	
12	9	1.4	p2.	9.5	
13	1	.	p2.	0.5	
14	9	0.2	.	8.1	
15	6	0.1	.	0.9	
16	9	.	.	10.2	
17	9	.	.	9.7	
18	9	.	.	1.7	
19	9	.	.	8.9	
20	0	10.8	.	3.5	
21	9	0.3	5	6.7	
22	0	13.8	3	.	
23	0	7.0	8	.	
24	9	1.1	11	7.3	
25	9	.	8	9.6	
26	9	.	6	9.5	
27	9	.	6	9.4	
28	9	.	4	9.5	
29	9	.	p2.	9.2	
30	9	.	p2.	6.6	
31	9	.	p2.	8.6	
Σ	–	39.5	–	211.3	UWAGI.

Kasprowy Wierch — $\varphi = 49°14'$ — $\lambda = 19°59'$ — Listopad – Novembre 1957

DNI	CIŚNIENIE P − 700				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.8	95.0	95.2	95.3	5.3	6.7	5.1	5.6	7.7	3.8	38	57	63	53	5.6	4.2	3.3	4.4	1	1 ⊙	0	SSW 7	SSW 8	C 0
2	94.8	95.9	96.3	95.7	0.3	2.8	1.8	1.7	5.1	−0.4	100	96	100	99	0.0	0.3	0.0	0.1	10	4 ⊙	10	SSW 7	SSW 6	SW 8
3	97.6	98.2	97.5	97.8	0.4	3.2	3.0	2.4	3.7	0.1	100	98	100	97	0.0	0.6	0.0	0.2	5	8	10	SSE 6	S 6	SSW12
4	97.2	97.6	99.0	97.9	1.7	2.4	1.6	1.8	3.0	1.0	100	96	76	91	0.0	0.3	1.6	0.6	8	3 ⊙	1	S 14	S 10	SSE12
5	96.8	95.1	94.7	95.5	1.1	2.1	1.9	1.8	2.3	0.2	100	96	96	97	0.0	0.3	0.3	0.2	5	4	7	S 14	SSE17	SSW17
6	93.3	95.0	94.5	94.3	0.9	1.6	1.5	1.4	2.2	0.7	92	100	100	97	0.5	0.0	0.0	0.2	8	7	10	S 20	S 20	S 17
7	92.9	93.2	93.5	93.2	2.2	2.2	1.2	1.7	2.8	0.9	92	96	94	94	0.6	0.3	0.4	0.4	7	9	8	S 17	SSE14	S 12
8	92.9	92.6	91.6	92.4	1.4	2.0	2.2	2.0	2.6	0.7	96	100	100	99	0.3	0.0	0.0	0.1	9	10 ●	10	SSE10	SSE 8	ESE 7
9	89.8	91.0	92.6	91.1	1.8	2.0	1.0	1.4	2.2	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10	10	7	SSE 8	SE 3	S 4
10	93.2	93.5	92.9	93.2	0.2	0.5	0.7	0.5	2.0	−1.0	63	98	86	82	2.3	0.1	0.9	1.1	0	2	9	S 4	SSW 5	SSE 9
11	92.9	92.1	91.4	92.1	3.9	4.4	−2.7	0.7	5.1	−3.3	87	86	97	90	1.0	1.2	0.1	0.8	9	10	10	SE 4	ENE 5	NNE 3
12	92.9	95.0	98.0	95.3	−3.7	−4.8	−4.8	−4.5	−2.4	−5.3	97	95	95	96	0.2	0.2	0.2	0.2	10	10	10	NNE 7	NNE 6	NE 9
13	99.0	100.3	100.8	100.0	−5.3	−2.1	−0.1	−1.9	0.0	−6.8	84	68	16	56	0.6	1.6	5.1	2.4	5	3 ⊙	1	ENE 5	ENE 3	ENE 3
14	101.8	103.9	105.7	103.8	1.0	6.0	2.2	2.8	6.0	−1.8	32	38	46	39	4.5	5.9	3.9	4.8	1	1 ⊙	1	C 0	C 0	C 0
15	107.0	107.4	107.0	107.1	1.6	2.6	0.6	1.4	3.3	−0.6	43	47	52	47	4.0	4.0	3.1	3.7	1	1 ⊙	1	S 4	SSW 5	SSW 6
16	105.6	105.2	104.8	105.2	−0.5	0.3	−0.5	−0.3	1.2	−2.6	57	71	61	63	2.6	1.8	2.4	2.3	6	3 ⊙	2	SSW 5	SSW 6	C 0
17	103.5	103.3	103.7	103.5	−0.3	−0.5	−0.8	−0.6	2.2	−2.4	68	57	35	53	2.0	2.5	3.8	2.8	4	1 ⊙	0	ENE 1	NE 2	C 0
18	103.7	104.1	103.5	103.8	−1.8	0.1	−2.3	−1.5	0.7	−2.6	59	54	50	54	2.2	2.9	2.6	2.6	0	1 ⊙	0	C 0	C 0	NE 2
19	102.4	103.1	104.7	103.4	−1.9	−3.4	−3.8	−3.2	−1.3	−5.3	28	52	40	40	3.8	2.2	2.6	2.9	1	3 ⊙	0	C 0	NNE 5	C 0
20	105.9	108.2	109.8	108.0	−4.2	−2.7	−2.5	−3.0	−0.9	−5.7	31	37	30	33	3.1	3.1	3.6	3.3	0	1 ⊙	1	SE 8	SSE 8	SE 4
21	110.2	109.9	107.2	109.1	0.1	−0.7	−1.9	−1.1	1.4	−5.2	39	32	31	34	3.7	3.9	3.6	3.7	1	0 ⊙	0	C 0	S 5	S 10
22	101.9	98.8	96.2	99.0	−1.1	0.2	0.2	−0.1	0.8	−7.1	26	20	47	31	4.2	4.9	3.3	4.1	0	0 ⊙	1	S 9	S 10	S 12
23	95.6	95.7	96.5	95.9	−1.5	0.1	−8.1	−4.4	1.0	−9.0	80	43	92	72	1.1	3.6	0.2	1.6	3 ⊙	8	10	SW 7	WSW 8	N 5
24	97.7	98.7	99.7	98.7	−10.4	−9.6	−6.4	−8.2	−6.3	−11.4	90	85	94	90	0.3	0.4	0.2	0.3	10	7 ⊙	10	N 8	N 3	NNW 5
25	98.7	99.2	100.6	99.5	−6.9	−2.6	−1.5	−3.2	−1.5	−7.6	94	98	98	97	0.2	0.1	0.1	0.1	8	10	10	N 4	N 4	NW 4
26	102.1	101.0	101.6	102.2	−0.5	−1.0	−0.9	−0.8	0.2	−2.4	100	99	99	99	0.0	0.1	0.0	0.0	10	9	3	NNE 4	WNW 3	WSW 2
27	97.9	96.8	97.1	97.3	−4.1	−4.2	−5.6	−4.1	2.2	−5.8	66	96	95	86	1.9	0.2	0.2	0.8	4	10	10	NW 6	NNW 8	N 5
28	98.0	95.7	92.4	95.4	−4.7	−0.4	−3.8	−2.4	0.1	−6.0	98	100	96	98	0.1	0.0	0.2	0.1	10	10	10	NNW 7	WNW10	WNW 9
29	85.9	83.8	85.2	85.0	−7.3	−10.7	−15.6	−12.3	−2.9	−16.1	93	90	81	88	0.2	0.3	0.3	0.3	10	10	10	NW 9	NNW 8	N 12
30	87.7	89.4	89.3	88.8	−23.5	−21.6	−20.9	−21.7	−15.6	−24.8	80	81	82	81	0.2	0.2	0.2	0.2	10	10	10	NNE12	N 14	N 14
31																								
M	97.8	98.0	98.1	98.0	−1.7	−0.8	−2.0	−1.6	0.9	−4.2	74	76	75	75	1.5	1.5	1.4	1.5	5.5	5.5	5.7	6.9	7.0	6.8

Grudzień – Décembre

1	91.5	93.4	94.3	93.1	−21.7	−19.7	−16.9	−18.8	−16.8	−22.3	81	83	85	83	0.2	0.2	0.2	0.2	3	3 ⊙	10	NNE12	NNE10	NNE12
2	93.5	93.2	91.7	92.8	−16.8	−14.7	−17.4	−16.6	−14.7	−18.1	80	57	79	72	0.3	0.8	0.3	0.5	1	2 ⊙	2	NNE 9	NNE12	NNE14
3	90.0	90.4	91.0	90.5	−17.2	−12.3	−13.5	−14.1	−12.1	−18.1	75	85	80	80	0.4	0.4	0.4	0.4	4	10	9	NNE17	NNE 8	NNE 6
4	93.2	94.7	96.1	94.7	−11.4	−10.0	−9.2	−10.0	−9.2	−13.9	83	87	92	87	0.4	0.4	0.3	0.4	10	10	10	NE 7	NNE10	NNE 9
5	95.8	95.3	95.4	95.5	−7.4	−6.4	−8.7	−7.8	−6.0	−9.4	90	94	92	92	0.3	0.2	0.3	0.3	10	10	10	NNE 5	NNE 8	N 9
6	94.9	95.2	96.8	96.0	−9.2	−9.9	−7.6	−8.6	−7.5	−12.4	92	91	51	78	0.3	0.3	1.7	0.8	10	10	0	N 10	N 7	N 4
7	94.4	92.3	87.8	91.5	−7.0	−6.6	−7.5	−7.2	−3.8	−8.7	45	44	60	50	2.0	2.1	1.4	1.8	1	5 ⊙	2	SSW 7	S 5	S 14
8	79.7	74.3	73.2	75.7	−6.9	−7.6	−1.7	−4.5	−0.7	−9.4	91	87	98	92	0.3	0.4	0.1	0.3	10	10	9	SSW20	SSW20	WNW12
9	70.8	71.4	77.8	73.3	−4.9	−5.1	−9.8	−7.4	−1.7	−10.7	95	95	72	87	0.2	0.2	0.8	0.4	10	10	9	W 12	WNW17	W 10
10	78.5	77.9	82.0	79.5	−8.3	−7.4	−12.1	−10.0	−7.0	−12.8	86	90	85	87	0.4	0.3	0.4	0.4	10	10	10	WSW 9	WNW 9	NNW 8
11	85.1	84.5	80.8	80.5	−11.0	−7.6	−4.6	−7.0	−4.6	−17.9	36	85	96	72	1.7	0.5	0.2	0.8	7	10	10	SSW14	S 20	S 20
12	80.5	82.7	82.8	82.0	−2.5	−1.8	−0.5	−1.4	−0.4	−4.8	98	98	99	98	0.1	0.1	0.0	0.1	10	10	10	S 14	SSE12	SSW17
13	80.7	79.5	71.6	77.3	−0.1	0.4	0.3	0.2	1.5	−1.2	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	SSW17	SSE17	SSE20
14	69.7	74.6	81.0	75.1	−0.9	−3.2	−3.6	−2.6	0.3	−4.1	99	97	94	97	0.0	0.1	0.3	0.1	10	10	1	SSW 9	SSW14	SSW 7
15	85.5	88.3	91.4	88.4	−3.8	−5.6	−11.2	−8.0	−3.1	−12.0	87	95	90	91	0.6	0.2	0.3	0.4	1	8	10	SSW 5	SSW 6	C 0
16	93.1	94.7	96.7	94.8	−9.4	−4.7	−5.0	−6.0	−3.6	−12.3	34	26	40	33	2.0	3.1	2.5	2.5	2	1 ⊙	1	NE 8	SW 3	S 4
17	96.5	95.9	95.0	95.8	−2.6	−4.8	−5.6	−4.6	−2.6	−6.9	69	93	92	85	1.6	0.3	0.3	0.7	1	8	0	SSW 4	S 6	SE 3
18	93.9	94.1	95.0	94.3	−7.5	−5.2	−6.5	−6.4	−4.0	−9.1	90	95	78	88	0.3	0.2	0.8	0.4	5	1 ⊙	0	NNE 6	C 0	W 2
19	96.1	98.1	101.8	98.7	−6.0	−5.5	−5.3	−5.5	−5.2	−7.8	49	72	60	60	2.0	1.1	1.6	1.6	1	1 ⊙	1	W 3	C 0	C 0
20	106.0	107.9	107.4	107.1	−7.2	−6.1	−8.0	−7.3	−4.9	−9.1	90	94	90	91	0.3	0.2	0.3	0.3	10	10	1	NNE 3	NNE 1	C 0
21	105.5	105.5	105.2	105.4	−0.8	0.5	−1.9	−1.0	1.0	−8.0	16	33	31	27	4.9	4.2	3.6	4.2	0	0 ⊙	0	SW 4	WSW 1	NE 3
22	103.6	103.0	102.3	103.0	−2.2	−0.5	−1.4	−1.4	0.1	−4.7	25	38	18	27	3.8	3.7	4.5	4.0	6	10 ⊙	3	C 0	C 0	SSW 4
23	99.7	97.8	96.2	97.9	−3.6	−5.4	−4.9	−4.7	−1.4	−5.8	15	29	20	21	4.0	2.9	3.4	3.4	1	8 ⊙	2	S 12	SSW 9	SSE10
24	90.7	95.3	95.4	95.1	−7.1	−4.3	−5.9	−5.8	−4.2	−10.4	21	38	67	42	2.8	2.8	1.3	2.3	5	4 ⊙	2	S 10	SSW 3	SSW 3
25	96.7	97.6	98.2	97.7	−6.3	−6.2	−5.3	−5.8	−5.1	−7.1	89	92	90	90	0.4	0.3	0.4	0.4	1	4	3	S 5	SSW10	WSW 5
26	101.3	102.7	103.7	102.6	−3.9	−2.3	−4.5	−3.8	−2.2	−5.4	80	76	91	82	0.9	1.3	0.4	0.9	9	7 ⊙	1	N 7	NNW 5	WNW 6
27	103.5	103.6	103.1	103.4	−3.0	−2.6	−1.6	−2.2	−1.4	−4.8	45	46	35	42	2.6	2.7	3.5	2.9	1	1 ⊙	4	WNW 5	W 4	WSW 5
28	99.6	97.1	92.3	96.3	−2.4	−1.7	−4.6	−3.3	−1.2	−5.8	46	50	93	63	2.7	2.7	0.3	1.9	4	4 ⊙	8	S 9	SSW 9	S 12
29	89.8	89.8	87.2	88.9	−6.1	−7.3	−8.9	−7.8	−4.5	−9.9	94	90	58	81	0.2	0.3	1.3	0.6	10	9	4	WNW 6	W 10	WSW14
30	85.7	84.3	82.4	84.1	−8.9	−8.8	−9.0	−8.9	−6.9	−10.9	89	92	92	91	0.4	0.3	0.3	0.3	6	9	9	W 14	SW 10	WSW 8
31	82.1	82.8	83.7	82.9	−8.7	−9.6	−9.4	−9.3	−8.1	−11.4	92	76	88	85	0.3	0.7	0.4	0.5	10	6 ⊙	10	NW 9	WNW17	WNW10
M	91.3	91.6	91.6	91.5	−6.9	−6.2	−6.8	−6.7	−4.5	−9.8	70	75	75	73	1.2	1.1	1.0	1.1	5.8	6.8	5.2	8.8	8.5	8.1

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	0.0	p2.	9.1	(m) na–a; ≫ 1110 1530 1910 1220. ○ a–p.; () 000 24
2	8	0.8	p2.	2.4	●0545 0805 ●1120 1940 2330. ¹na; ≡² 1105 1245 ≡ 310 ≡² 815 ≡ 915 1015 1215 1345 1715 m n–1715 ≡² 1830 ≡² 2010 ≡² 24; ≫ 2045 2330 (nor. 15), ○ a…p., () 000 na
3	8	12.9	p1.	4.0	●2020 2140 ●0 2315 ●¹ 24. ≡² 000 715 ≡ 330 ≡² 430 610 ≡ 1835 ≡² 24; ≫ 1635 24 (nor. do 22); ○ a. z prz., p z prz.
4	9	.	.	4.9	●1000 145 ●0 340 ≡² 000 445 ≡ 1530; ≫ 000 24 (nor. do 27), ○ …p.; () n–24
5	9	.	.	1.1	≡ 605 925 1220 1740; ≫ 1000 810 (nor. 27) ≈ –24 (nor. do 36); ○ a z prz., p z prz.; () 000 p.
6	9	.	.	0.2	≡ 1215 1330 1715 1830 ≡² 2115; ≈ 000 24 (nor. do 39); () na–p.
7	9	.	.	0.7	≡ 2220 24; ≈ 000 1045 (nor. do 39) ≫ –24 (nor. do 29); ○ a z prz.; ∪ʰ p z prz., nn z prz. ☂⁰ p.; () na–a
8	5	3.1	.	.	●1130 1730 ●0 1620 2030 24. ≡ 000 1015 ≡² 1230 ≡ 1250 ≡² 1515 ≡ 1540 ≡² 2225 ≡ 2240 ≡² 2305 ≡ 24; ≫ (000–530) (nor. do 25), 1002 1830 1540 1945 (nor. 20)
9	1	0.7	.	.	●0000 920 1250 1415 ≡ 000–15 ≡² 430 ≡ 615 ≡² 820 ≡ 945 ≡² 1005 ≡ 1030 ≡² 1445 ≡ 1530 1630 24; ≫ 540 620 (nor. 20), 915 1110 (nor. 17) ∪ʰ p, np, ☂⁰ p, np
10	9	0.5	.	4.8	⌴⁰ na–a ⌴¹ n–24. ≡ 000–30 ≡² 240 ≡ 320 m na ≡ 1140 1730; ≈ 1430–1720 2110–40 2212–2330. ○ a z prz., p z prz. ∪ʰ ☂⁰ n–np.; () na–24
11	9	4.5	.	1.1	●0240 445 530 615 ●marzn. 1930 2315 ≡¹ 2325 ≡² 24. ⌴¹ 000 na ∀⁰ n–np ∀¹ np–24 ∽¹ n–np ⊠¹ n–np (m) a m a–p. ≡ 1300–15 ≡² 1930 24; ○ a z prz., p z prz.; () 000 p.
12	1	2.2	3	.	✶⁰ 000 615 △⁰ 740 815 ✶² 930 △² 1220 ✶² 1345 △⁰ 1405 ✶⁰ 1645 △² 1730 ✶² 1845 △² 2140 ∀ 000 p. ∀¹ p. 24. ≡² 000 1505 ≡ 1530 ≡² 2240 ≡ –24
13	9	.	6	8.1	∨¹ 000 445 ≡ 000 445 m –24; ○ a–p.; ☂⁰ a.; () a–24
14	9	.	4	8.2	m 000 a (m) a 24; ○ a–p.; () 000 24
15	9	.	3	8.2	m 000 p.; ○ a–p.; () 000–24
16	9	.	3	7.8	⌴⁰ n.p.–24. (m) a–1430 m –24; ≫ 1345 1610; ○ a–p.; ⊘ Sc p.; () 000 p.
17	9	.	3	8.1	⌴⁰ 000 a. m 000–24; ○ a–p.; ☂⁰ a. zielony promień 1553 (zielony i niebieski)
18	9	.	3	8.1	⌴⁰ na–a. m 000 24; ○ a–p.; ☂⁰ a–p.; () a–p.
19	9	.	3	7.9	⌴⁰ na; m 000–24; ○ a–p. ☂⁰ a–p. zielony promień 1557 (nieb.–fioletowy); () a–24
20	9	.	3	8.0	m 000 a; ≫ 730–830; ○ a–p.; ☂⁰ a.; () 000–24
21	9	.	2	8.0	≫ 2030 24; ○ a–p.; zielony promień 1549 (niebieski); () 000 24
22	9	.	2	8.0	≫ 000 630 815 915 1040 1420 (nor. do 24) ≈ –1730 (nor. 30) ≫ 2305 (nor. 25); ○ a–p. ☂⁰ na.; () 000 24
23	9	1.2	1	1.8	⌴¹ na–a ∨¹ 1530–24. (m) na–p ≡ 1523–35 ≡² 24; ≫ 010–140; ○ a z prz.; () 000 p.
24	8	0.2	2	3.3	✶⁰ 345 430 △⁰ 1015; ∨¹ 000 a ∨⁰ 1930–24. ≡ 2000 945 ≡ –1015 1830 ≡² 24; ○ a…p.
25	1	6.3	2	.	●0800 915 ●1110 △⁰ 1215 ✶⁰ 1315 ●0 1330 1440 ●⁰ 1715 △⁰ 2000 ●⁰ 24. ∨ 0000 na ∽ 1005 24 ∨ G-1 1045 24. ≡² 000 345 ≡ –530 ≡ 815 24
26	9	1.6	3	.	●⁰ marzn. 000 215 345 415 ●⁰ 840 ●⁰ 905 ∽⁰ 000 600 730 915; ∀ 000 600 2015–30; ⌴⁰ p–np.; ≡² 000 1215 (m) a–p m p. ≡ 2015–30 (m) p–24; ∪ʰ p z prz.; () a–24
27	0	3.7	3	.	●⁰ 1130–50 ●⁰ 1220 △⁰ 1945; ∀⁰ 845 1050 ∀¹ 24. (m) 000 na m na–a ≡ 845–50 ≡² 24; ≫ 2340 430 (nor. 19), 720–35 (nor. 17); ⌓⁰ ok. 025–1005; () 000–a
28	1	11.7	4	.	✶⁰ 445 530 △⁰ 810; ✶ △⁰ 840 △⁰ 1130 ✶ △⁰ 1215 △¹ 1315 1550 2130 2220 24; ∀⁰ 000 a ∀⁰⁻¹ a. 24. ≡ 2000 1730 ≡ –1235 ≡² 1415 ≡ –1445 ≡² 2140 ≡ 2330 ≡² 24; ≫ 730 830 1115 14–
29	0	28.8	10	.	△⁰ 000 na. △¹ na. △⁰ 900 ∇⁰ 1800 ✶ 24; ∀¹ 000 a ∨⁰ a. 24. ≡ 2000 24; ≫ 0000 2330 (nor. 17), 1830 2130 (nor. 17); ✶ ⊣ ⁰ a–1730 ✶ ⊣ ¹ –24 [28.XI: (nor. 21), 2315 24 (nor. 16)
30	0	16.8	35	.	✶ 2000 24; ∨⁰ 1000 24. ≡ 2000 24; ≫ 615–24 (nor. do 21); ✶ ⊣ ¹ 000–24
31					
Σ	—	95.0	—	113.8	UWAGI.

Grudzień – Décembre

1	8	3.1	48	3.2	✶⁰ 000 315 1045 1210 1545 24. ∨⁰ 000 na ∨ na a. 24. ≡² 000 330 ≡ 510 ≡² 615 m na–a ≡ 610 1545 ≡² 24; ≫ 0002 4 (nor. do 21); ✶ ⊣ ⁰ 000 315 ⊣ ¹ 500 ⊣ ¹ 1545 24. ○ a…p.; () na–a
2	9	.	51	7.0	✶⁰ 000 430 ∨⁰ 000 550 ≡² 000 430 ≡ 445 550 (m) a m–p ≡ 1545 1830 1730 1930; ≫ 000–30 730 2105 (nor. 26) ≈ –24 (nor. 26); ✶ ⊣ ⁰ 000 430 ⊣ ¹ na ⊣ ¹ 24; ○ a–p. ☂ 810 a.p.;
3	1	0.1	48	.	∨⁰ a–p. ≡ 0020 230 1730 1115 ≡² 1345 ≡ 1615 ≈ (000–30 ≫ 330 (nor. 26) ≈ –1100 (nor. do 30)) ≫ 1100–30 ⊣ ½ 000 a.; ☂ 1830 24; () 000 a [2.XII: ⊘ na. Sc a.p.; () a–24
4	1	4.6	48	2.8	△⁰ 0245 445 ● ✶⁰ 1745 1910 △⁰ 1540 1600 2030 2105 ∽ ⁰ 1910 1215 ∨ ¹ p. 24. ≡ 430 515 (m) 545 a ≡ 1210 24; ≫ 1105–20 1245 1410 1530 1915; ○ a.; ☂ 000 1515 ☂ ⁰ 745 1030 () a
5	1	25.7	49	.	△² 440 530 △¹ 620 △⁰ 755 △¹ 830 ✶ △² 1130 △² 1630 ✶ 1745 1830 ✶ 1930 2025 2330 △ 24. ∨ 2000 a ∨² a–24. ≡² 000 24
6	0	9.7	63	1.0	△⁰ 000 615 ● 815 △¹ 1220 ✶ △⁰ 1315 ✶ 1430. ∨² 000 1430 ≡ 2000 1430 m 1430 24; ≫ 130 730 ⊣ ¹ p.; ○ p z prz.; ☂ 1530 p.; ⊘ 1530 p.; () 1530–24
7	9	0.3	66	7.5	m 000 130 (m) –320 ≫ 1840 2110 (nor. 15) ≈ 2235 ≫ 24 (nor. 23); ⊣ ⁰ a. 1215 1830 1030 ⊣ ¹ 24. ○ a–p.; ☂ ⁰ n.p.; zielony promień 1544 (nieb.); () 000 24
8	8	2.9	63	0.8	✶ 420 720 1440–1530 ✶ 1730 ⌴ ⁰ n.p.; ⌴ ¹ 24. V⁰ 530 ⊣ ¹ 24 ≡ 515 ≡ 540 ≡ ¹ 1740 ⊣ ¹ 1830 ≡ ² 2015 ≡ 2330 ≡ ² 24. ³ 000–120 (nor. 22) ☂ –130 (nor. 22) ³–5 ☂ (nor. 24) ● –1715 (nor. do 42) ≫ –24 (nor. do 28) ⊣ ¹ 5 2000–30 ⊣ ¹ 1830 ⊣ ¹ 705 ⊣ ¹ 1830 ⊣ ¹ 24 ○ a z prz.; () 000 na
9	1	3.7	63	.	△⁰ 000 330 530 615 ✶ 1330 △⁰ 1410 ∨⁰ 000 n. ≡² 2000–30 430 615 ≡ 1020 ≡² 1345 ≡ 1415 ≡² 1440 ≡ 1530 ≫ 000 830 (nor. do 26) ≈ –1530 (nor. do 40) ≫ 1020 (nor. 26), 1940 24 (nor. do 23); ✶ ⊣ ⁰ 000 330
10	1	3.7	65	.	✶⁰ 000 230 △² 345 620 △⁰ 730 ✶ ¹ 750 △⁰ 1215 ✶ △⁰ 1345 ✶ 2215; ∨⁰ 1130 2215 ≡ 820–35 ≡² 1805 ≡ 1030 ≡² 2215 ≡ 2535 ≫ 000–45 930 1145 1320 2030 (nor. 22); ⊣ ¹ 000 140 ⊣ ¹ ⁰ 1320 ⊣ ¹ 2030
11	8	4.4	67	1.9	✶⁰ 2115 24. ∨⁰ 1505 n. ∨¹ 2224 ≡ 2505 24; ≫ 520 715 (nor. 24) ≈ 24 (nor. do 36 a. 15–16 si. 24, nor. 44); ⊣ ¹ 1640 2115 ✶ ⊣ ¹ 24. ○ …p.; ☂ 530 630; () 000 a
12	0	8.4	64	.	✶⁰ 000 115 530 1035 ● ² 1730 ● ⁰ 1915 ● ² 2224 24. ∨⁰ 000 24 ≈ 000 24 ≫ 000 630 (nor. 30) ≫ 1730 (nor. do 30) ≈ –24 (nor. do 30) ✶ ⊣ ⁰ 000 115 ⊣ ¹ 530 ⊣ ¹ 1230 ⊣ ¹ 1530 ⊣ ¹ 1730 ⊣ ¹ 24
13	0	14.1	58	.	⌓⁰ 2210 (nor. do 47) ≫ 2330 –24 (nor. 24); ⊣ ¹ 000 730 ⊣ ¹ 2230 –24
14	0	2.4	47	.	✶⁰ 000 840 ● 1030 ✶ ⁰ 15; ∨⁰ 000 1715 ∨⁰ 2224 24. ≡² 000 1530 ≡ 1715 ≡² 2130 2330 –24; ≫ 000 620 (nor. 24) 740 830 1030 1415 (nor. 19) ≈ –1530 (nor. 26) ≫ 2015 (nor. 21) ⊣ ¹ 1430 ⊣ ¹ 15 ⊣ ¹ 2015
15	9	.	44	3.9	∨⁰ 000 330 a z prz., p. 24. ≡ 000 215 ≡² 330 ≡ 1120 1930 ≡² 1940 ≡ 2025 ≡² 2130 ≡ 2215 ≡² 2345 ≡ 2110 (nor.) 345 430 m –1830; ○ a z prz., p z prz. ☂⁰ a., p.; ⊘ ⁰ a., p.; () na–p
16	9	.	41	7.4	∨⁰ 000–30 ≡ 000–30. ○ a–p.; () na–24 [9.XII: ⊣ ¹ 530 ⊣ ¹ 820 ✶ ⊣ ² 1440 ⊣ ¹ 24 [10.XII: ✶ ⊣ ⁰ 2120; () n.p.–24
17	8	.	40	0.2	⌓⁰ na ∨⁰ 515–30 ∨⁰ 810 1430 2145 24 (m) na m na–515 ≡ 530 m–a (m) a–810 ≡ 840 ≡² 1140 ≡ 1430 (m) 1730 1830 ≡ 2020 (m) –2145 ≡² 24; ○ p z prz.; () na–a
18	9	.	38	5.2	∨⁰ 000 1005 ≡² 000 445 ≡ 510 ≡² 620 ≡ 705 ≡² 1005 ≡ 1215 1420 1630 m 1915 24; ○ a p ☂ 1015 p.; () 1020 24
19	9	0.0	35	7.6	m 000 24; ○ a–p.; ☂⁰ a–p.; () 000–24
20	1	0.5	33	.	✶ 2040 310 1145 1215 ✶ △⁰ 1445 1530 1630 ∨⁰ 330 a ∨⁰ a z prz., p z prz.; m 000 130 (m) –330 ≡² 520 ≡ 645 ≡² 830 ≡ 1145 ≡² 1630 ≡ 1740 ≡² 1940 ≡ 2020; () 000 330
21	9	.	32	7.5	(m) na–1800; ○ a–p.; () a–24
22	9	.	31	6.1	○ a–p.; ⊘ ¹ a.; ⊕ ⁰ a z prz., p z prz.; () 000 24
23	9	.	30	7.4	≫ 445 1215 1310 1530 (nor. 20), 1740–55 (nor. 19), 1945–24 (nor. do 21); ○ a–p.; () 000–24
24	9	.	29	7.2	≫ 000 530 (nor. 24) ≈ 610 ≫ 710 (nor. 18); ○ a–p.; () 000–24
25	9	.	28	4.3	∨⁰ na a…p.; (m) na. a ≡ 430 –na. a…p.; ≫ 1220 1630; ○ a z prz., p z prz.; () 000 24
26	9	0.0	28	1.8	✶⁰ 820 1130 ⌴⁰ p–np.; ○ a…p.; () 000 24
27	9	.	28	7.5	○ a–p.; () 000 24
28	9	0.0	27	6.9	∨⁰ p…np.; ≡ 1930 2130; ≫ 1456 30 1540 2130 (nor. do 22), 2215 24 (nor. 15); ○ a…p.; ∪ʰ p.; () 000 p.; np.–24
29	8	0.4	27	0.1	△⁵ 630 920 1145 1340; ∨⁰ na…a.; ≡ 630 930 ≡ 1230; ≫ 000–30 1050 2235 ≈ –24 (nor. 27); ✶ ⊣ ⁰ 1145 1340 ⊣ ¹ 1530; () 000 na
30	7	1.0	27	2.3	
31	9	1.4	29	0.5	
Σ	—	86.4	—	100.1	UWAGI.

1957

TABLICA II

WYNIKI MIESIĘCZNE I ROCZNE SPOSTRZEŻEŃ METEOROLOGICZNYCH

RÉSUMÉS MENSUELS ET ANNUELS DES OBSERVATIONS MÉTÉOROLOGIQUES

Rozewie

$\varphi = 54°50'$ $\lambda = 18°20'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.5	1.2	0.9	0.9	2.6	-1.2	10.1	6	-7.6	16	89	87	86	87	0.7	0.9	0.9	0.8	7.8	8.1	7.9	7.9
II	–	–	–	–	1.9	3.8	2.6	2.7	4.9	0.5	11.1	2	-3.6	25	88	80	87	85	0.8	1.7	0.9	1.1	8.6	7.6	7.1	7.8
III	–	–	–	–	0.8	3.3	2.0	2.0	4.7	-0.7	15.4	27	-6.5	16	77	73	77	76	1.5	2.3	1.7	1.8	5.5	6.0	4.6	5.4
IV	–	–	–	–	3.9	5.8	3.6	4.2	7.2	1.2	16.9	5	-4.8	13	83	78	87	83	1.5	2.4	1.1	1.7	6.4	6.1	5.7	6.1
V	–	–	–	–	8.2	9.8	7.5	8.2	11.1	5.1	18.9	31	-0.3	6	80	75	82	79	2.3	3.3	2.1	2.6	5.4	5.4	4.6	5.1
VI	–	–	–	–	13.9	15.5	13.0	13.8	17.7	9.8	23.4	18	6.5	1	78	68	81	76	3.6	5.8	3.0	4.1	5.5	5.3	4.3	5.0
VII	–	–	–	–	16.7	18.4	16.3	16.9	19.6	13.5	24.1	8	9.6	1	87	81	86	85	2.5	4.2	2.7	3.1	6.4	6.1	4.9	5.8
VIII	–	–	–	–	15.3	18.2	15.4	16.1	19.1	12.7	25.8	11	8.6	23	85	73	86	81	2.8	5.9	2.5	3.7	5.7	5.9	6.0	5.9
IX	–	–	–	–	10.8	13.7	10.9	11.6	14.9	8.4	26.6	8	3.2	26,27	90	80	90	87	1.3	3.6	1.3	2.1	6.6	6.6	6.1	6.4
X	–	–	–	–	8.3	11.4	9.3	9.6	12.1	6.6	18.0	19	2.6	15	91	76	86	84	1.0	3.3	1.7	2.0	7.6	7.3	5.7	6.9
XI	–	–	–	–	4.8	6.4	5.3	5.4	7.5	3.2	12.6	2,4	-2.9	30	88	84	87	86	1.0	1.5	1.1	1.2	8.4	7.8	7.3	7.8
XII	–	–	–	–	0.8	1.7	1.3	1.3	3.3	-1.3	8.1	8	-10.6	18	83	80	83	82	1.1	1.4	1.1	1.2	7.8	8.1	6.7	7.5
Rok	–	–	–	–	7.2	9.1	7.3	7.7	10.4	4.8	26.6	8.IX	-10.6	18.XII	85	78	85	83	1.7	3.0	1.7	2.1	6.8	6.7	5.9	6.5

Łeba

$\varphi = 54°46'$ $\lambda = 17°34'$

I	–	–	–	–	0.5	1.6	0.8	0.9	2.9	-1.4	10.0	6	-10.0	2	90	86	88	88	0.6	1.0	0.8	0.8	9.0	7.3	8.1	8.1
II	–	–	–	–	1.3	4.3	2.5	2.6	5.6	0.0	10.3	2	-6.7	25	92	80	89	87	0.5	1.7	0.8	1.0	7.5	6.8	7.8	7.4
III	–	–	–	–	0.5	4.2	1.9	2.1	6.2	-1.1	16.1	27	-6.1	10	81	70	79	77	1.2	2.7	1.5	1.8	4.7	5.6	5.0	5.1
IV	–	–	–	–	3.4	6.0	3.4	4.0	8.0	0.5	20.0	5	-5.9	15	87	79	87	84	1.1	2.4	1.0	1.5	6.7	5.9	5.7	6.1
V	–	–	–	–	8.6	10.6	7.8	8.7	12.3	4.8	24.0	16	-0.8	6	82	73	85	80	2.3	4.0	1.7	2.7	5.4	5.0	4.0	4.8
VI	–	–	–	–	13.8	16.3	13.2	14.1	18.5	9.2	28.1	9	5.0	8,21	85	72	86	81	2.6	5.5	2.2	3.4	5.1	4.3	3.1	4.2
VII	–	–	–	–	16.5	19.1	16.4	17.1	21.1	13.6	29.0	20	8.3	4	90	81	89	87	1.9	4.6	2.0	2.8	7.0	6.5	5.3	6.3
VIII	–	–	–	–	15.2	18.5	15.1	16.0	20.0	12.2	26.2	11	7.7	24	87	73	90	83	2.2	5.9	1.9	3.3	5.7	6.5	5.9	6.0
IX	–	–	–	–	10.7	14.0	10.9	11.6	15.4	8.3	26.2	8	2.7	17	87	73	85	82	1.7	4.7	2.0	2.8	6.2	6.7	6.4	6.4
X	–	–	–	–	8.4	11.5	9.4	9.7	12.5	6.6	19.5	10	2.8	21	90	76	86	84	1.1	3.3	1.6	2.0	8.2	7.3	6.5	7.3
XI	–	–	–	–	4.4	6.7	5.0	5.3	7.9	2.7	15.5	5	-4.5	20	89	81	87	86	0.9	1.9	1.1	1.3	7.9	7.7	7.0	7.5
XII	–	–	–	–	0.5	1.7	1.2	1.2	3.4	-1.5	7.8	8	-10.3	18	87	80	86	84	0.8	1.3	0.9	1.0	8.1	7.1	8.0	7.7
Rok	–	–	–	–	7.0	9.5	7.3	7.8	11.2	4.5	29.0	20.VII	-10.3	18.XII	87	77	86	83	1.4	3.2	1.5	2.0	6.8	6.4	6.1	6.4

Puck

$\varphi = 54°43'$ $\lambda = 18°25'$

I	–	–	–	–	0.6	1.6	0.9	1.0	3.0	-1.3	10.7	6	-8.1	16	89	85	87	87	0.7	1.1	0.9	0.9	9.1	8.5	8.3	8.6
II	–	–	–	–	2.1	4.2	2.7	2.9	5.5	0.5	11.1	6	-5.0	25	90	81	89	87	0.7	1.6	0.8	1.0	9.4	8.8	8.3	8.8
III	–	–	–	–	0.9	4.0	1.8	2.1	5.3	-0.9	16.4	27	-6.5	9	80	73	80	78	1.4	2.5	1.4	1.8	5.8	6.6	5.0	5.8
IV	–	–	–	–	4.0	6.6	4.1	4.7	8.5	0.9	19.2	5	-6.1	13	86	77	84	82	1.3	2.5	1.3	1.7	6.9	6.7	5.7	6.4
V	–	–	–	–	8.9	10.9	8.2	9.0	12.2	5.2	19.6	31	-0.1	2	78	72	80	77	3.1	4.0	2.3	3.1	6.0	5.9	4.5	5.5
VI	–	–	–	–	13.9	16.8	14.3	14.8	19.2	9.5	26.5	18	6.1	25	80	67	79	75	3.3	6.4	3.5	4.4	5.2	6.2	4.7	5.4
VII	–	–	–	–	16.7	19.7	17.1	17.6	21.2	13.4	27.6	8	9.0	4	87	75	82	81	2.6	5.8	3.6	4.0	6.3	6.5	5.8	6.2
VIII	–	–	–	–	15.5	18.8	15.4	16.3	20.4	12.4	27.9	13	9.1	23,24,31	86	69	88	81	2.6	7.0	2.2	3.9	5.8	6.7	6.9	6.5
IX	–	–	–	–	10.8	14.0	10.8	11.6	15.5	7.9	22.9	8	2.6	26	86	73	84	81	1.8	4.7	2.1	2.9	7.6	7.7	6.3	7.2
X	–	–	–	–	8.4	11.9	9.4	9.8	12.9	6.6	19.4	19	2.7	2	88	73	83	81	1.3	3.8	2.0	2.4	8.7	8.3	6.2	7.7
XI	–	–	–	–	4.9	6.7	5.4	5.6	7.8	3.2	12.9	5	-3.3	30	88	82	87	86	1.0	1.7	1.0	1.2	8.7	8.6	8.1	8.5
XII	–	–	–	–	0.7	1.6	1.3	1.2	3.3	-1.4	8.2	8	-10.2	18	82	82	84	83	1.1	1.2	1.1	1.1	8.7	8.0	7.6	8.1
Rok	–	–	–	–	7.3	9.7	7.6	8.0	11.2	4.7	27.9	13.VIII	-10.2	18.XII	85	76	84	82	1.7	3.5	1.8	2.3	7.4	7.4	6.4	7.1

Poraj

$\varphi = 54°39'$ $\lambda = 17°36'$

I	–	–	–	–	0.3	1.7	0.7	0.8	3.0	-2.1	10.8	6	-10.6	15	90	86	87	88	0.6	1.0	0.9	0.8	9.0	8.0	8.6	8.5
II	–	–	–	–	1.4	4.1	2.4	2.6	5.7	-1.1	11.3	2	-9.1	25	90	79	88	86	0.7	1.8	0.9	1.1	8.2	7.8	8.1	8.0
III	–	–	–	–	0.2	5.2	1.5	2.1	6.8	-3.0	15.8	31	-7.8	10	81	68	79	76	1.2	3.4	1.6	2.1	5.1	5.4	5.5	5.3
IV	–	–	–	–	3.0	8.5	3.6	4.7	9.8	-1.1	20.3	5	-8.1	16	85	66	85	79	1.2	4.6	1.2	2.3	6.0	5.5	5.7	5.7
V	–	–	–	–	9.0	12.2	7.3	9.0	13.4	2.8	23.3	16	-4.8	27	80	65	84	76	2.4	5.8	1.7	3.3	–	–	–	–
VI	–	–	–	–	13.9	18.2	12.7	14.4	19.8	6.7	26.9	11	1.1	15	81	64	87	77	3.2	8.0	2.0	4.4	5.3	4.6	3.3	4.4
VII	–	–	–	–	16.8	20.2	15.8	17.2	21.6	11.4	28.2	20	5.5	4	90	73	91	85	2.0	7.0	1.6	3.5	6.2	5.7	5.3	5.7
VIII	–	–	–	–	14.7	18.8	14.3	15.5	19.9	10.3	25.9	12	7.0	24	90	72	94	85	1.7	6.3	1.1	3.0	4.5	5.5	6.2	5.4
IX	–	–	–	–	10.3	14.0	10.1	11.1	15.4	6.2	26.7	8	-1.6	26,27	89	73	89	84	1.5	4.6	1.5	2.5	6.7	7.3	6.9	7.0
X	–	–	–	–	8.0	11.9	9.1	9.5	12.8	5.3	18.8	10	-0.1	15	92	76	88	85	0.9	3.4	1.4	1.9	7.5	7.2	7.2	7.3
XI	–	–	–	–	4.1	6.6	4.2	4.8	7.7	1.2	15.3	5	-10.6	30	90	81	88	86	0.8	1.9	0.9	1.2	8.7	8.7	8.1	8.5
XII	–	–	–	–	0.3	1.5	0.8	0.8	3.1	-2.8	9.0	8	-13.1	17	86	81	85	84	0.8	1.3	1.0	1.0	9.0	7.8	8.1	8.3
Rok	–	–	–	–	6.8	10.2	6.9	7.7	11.6	2.8	28.2	20.VII	-13.1	17.XII	87	74	87	83	1.4	4.1	1.3	2.5	–	–	–	–

Rozewie

H_s = 54 m h_w = 19 m **1957**

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0°	Max<-10	Max<-25	Opad R 0,1	1,0	10,0	Wiatr v 10	15	≡	≈	◔	●	≋
I	1.5	5.7	3	5.7	5	5.2	4	3.9	11.5	4.3	2.2	6.0	35.5	10.1	6.5	7.2	3	7.4	132	5.0	5	19	5	·	·	12	6	·	9	7	11	·	1	19	3
II	2	3.5	7	3.0	1.5	3.0	5	4.4	15	4.2	23.5	5.0	10	8.5	7	5.5	4	5.2	28.8	5.7	8	13	·	·	·	10	11	·	3	3	9	·	·	14	3
III	6	8.3	14.5	3.9	7.5	5.1	14	8.2	9.5	7.7	12	6.4	17.5	9.1	3	6.8	4	6.5	17.8	4.1	20	19	2	·	·	8	6	·	12	3	5	·	7	8	2
IV	8.5	3.5	19.5	4.2	8.5	1.8	8.5	1.9	1	4.0	1.4	5.0	3.6	4.2	1.2	4.6	2	3.8	32.4	6.4	28	8	·	·	·	10	9	·	4	·	11	1	5	10	1
V	9.5	4.4	18.5	5.3	2.5	4.2	9	4.6	8.5	3.6	6	3.6	22.5	6.5	13.5	5.4	3	5.0	16.1	3.9	9,23	1	·	·	·	12	6	·	2	1	6	2	6	7	·
VI	1.5	1.7	6	2.2	7.5	3.2	6	5.1	6	3.7	12.5	4.4	32.5	6.6	11	6.6	7	4.6	12.4	3.5	9	·	·	·	·	8	4	·	5	2	4	1	5	4	·
VII	2	1.8	5	2.1	5.5	1.8	11.5	3.7	6	3.7	14.5	3.5	30.5	6.5	11	5.0	7	4.2	112.6	28.8	12	·	·	·	·	15	13	5	3	·	9	8	1	4	·
VIII	1.5	2.3	3	2.5	2	1.8	5	3.9	14.5	4.4	2.2	4.9	24.5	6.3	14.5	5.9	6	4.8	164.4	39.5	17	·	·	·	1	18	14	7	3	1	·	2	·	3	·
IX	9	7.2	0.5	1.0	1	1.0	·	·	1.0	4.4	3.2.5	5.5	11.5	7.6	13.5	9.4	7	6.1	84.8	18.6	17	·	·	·	1	22	14	3	7	5	2	1	·	6	·
X	0.5	5.0	·	·	1	2.0	2.5	2.2	1.1	6.0	3.7	6.0	30.5	7.8	10.5	9.0	·	6.8	18.7	4.2	5	·	·	·	·	13	7	·	9	3	6	·	1	9	·
XI	3.5	10.1	8	7.5	9	5.4	5	4.4	1.8	4.6	2.6	4.5	12	9.8	5.5	6.7	3	5.8	22.4	5.9	27	8	·	·	·	11	6	·	6	4	4	·	2	18	1
XII	5	10.5	5.5	10.3	6.5	8.1	0.5	7.0	7.5	4.7	3.7.5	6.6	21.5	9.4	8	12.5	1	8.1	22.1	6.5	30	18	4	2	·	10	6	·	15	5	5	·	2	18	3
Rok	50.5	5.3	90.5	3.9	57.5	3.6	7.1	4.1	118.5	4.6	259.5	5.1	274.5	7.8	12.6	7.1	47	5.7	545.3	39.5	17.VIII	86	11	2	2	166	102	15	78	34	72	15	30	120	13

Łeba

H_s = 2 m h_w = 21 m

I	·	·	0.5	12.0	7.5	6.7	4.5	4.0	15.5	3.9	4.6	6.9	14.5	8.0	4.5	4.8	·	6.3	17.4	6.4	5	23	5	·	·	12	5	·	–	–	11	·	1	18	4
II	4.5	4.0	2.5	2.0	4	2.5	9	3.5	17.5	4.7	3.2	5.1	11.5	5.9	3	4.3	·	4.7	4.1.4	6.2	8,22	15	·	1	·	17	10	·	–	–	3	·	2	13	2
III	7	5.7	10.5	4.1	8	8.3	15	7.3	14	4.9	22.5	5.6	10	5.8	5	5.6	1	5.8	20.5	6.2	15	20	1	·	·	7	4	·	–	–	7	·	5	7	2
IV	17	3.5	22.5	4.9	2.5	2.5	2	2.5	4.5	5.0	13.5	3.6	11.5	4.9	16.5	4.1	·	4.8	48.6	17.8	2.2	13	·	·	·	15	9	1	–	–	10	·	5	12	1
V	10	3.7	20	5.8	4	3.2	4	4.2	4.5	4.6	17.5	3.8	23.5	5.9	9.5	3.9	·	4.8	23.7	8.6	9	1	·	·	·	11	4	·	–	–	3	2	7	7	·
VI	5	2.9	7.5	3.4	6	3.7	6	5.5	4.5	2.9	26.5	3.9	29	5.0	5.5	3.3	·	4.2	37.4	25.8	9	·	·	·	2	9	5	1	–	–	4	1	7	2	·
VII	5	3.3	12	3.5	5.5	4.0	4.5	5.3	9	3.6	18	4.0	3.1	4.7	8	4.2	·	4.3	20.3.0	7.4.1	2.3	·	·	·	5	17	14	6	–	–	1	6	3	6	·
VIII	3.5	3.0	4	3.5	1	3.0	5.0	4.5	13.5	3.3	3.0	4.6	2.3.5	4.7	6.5	3.0	·	4.2	10.2.1	4.0.5	16	·	·	·	1	18	14	6	–	–	·	7	2	6	·
IX	6.5	6.8	2	3.5	1	2.0	2	4.5	14.5	5.0	3.5.5	5.4	12	5.8	16.5	7.2	·	5.7	120.3	27.6	27	·	·	·	1	24	16	3	–	–	·	1	1	8	·
X	0.5	3.0	0.5	3.0	1	2.0	0.5	5.0	18	5.2	4.8.5	5.5	17.5	5.8	6.5	8.8	·	5.7	38.2	7.0	31	·	·	·	·	18	9	·	–	–	5	·	1	15	·
XI	0.5	12.0	6	9.6	11	6.1	5.5	4.7	22.5	4.0	2.6	4.7	13	7.0	5.5	12.6	·	5.9	28.7	7.0	27	10	·	·	·	9	6	·	–	–	4	·	3	18	·
XII	4.5	4.6	4	14.8	7	7.9	1	3.0	1.5	5.3	4.5	6.2	6	6.8	10.5	8.1	·	6.7	46.9	8.8	31	19	4	2	·	15	7	·	–	–	4	1	2	19	6
Rok	6.4	4.4	9.2	5.8	5.8.5	4.3	5.9	4.5	15.3	4.4	3.6.1	4.9	20.9	5.9	9.7.5	6.0	1	5.2	8.18.2	7.4.1	23.VII	102	10	2	9	172	103	17	–	–	52	18	39	131	4.3

Puck

H_s = 1 m h_w = 13 m

I	·	·	2.5	11.8	7.5	6.3	3	2.3	1	2.0	2.2	5.0	31.5	9.1	3.5	6.0	2.2	5.4	12.1	3.8	5	19	5	·	·	8	5	·	12	6	–	–	·	21	6
II	1.5	5.7	1.0	2.2	1	3.5	7.5	2.1	2	1.5	1.8	2.4	1.8	6.5	2	5.8	2.4	2.7	36.7	5.4	9	12	·	·	·	16	12	·	6	3	3	–	·	21	2
III	11	5.8	7	2.5	7.5	4.8	21.5	6.5	1	4.0	6	4.8	15	7.1	3	5.7	2.1	4.4	20.5	5.4	17	21	2	·	·	9	5	·	11	5	2	–	5	10	4
IV	8.5	2.7	2.0	5.0	3	3.0	2	1.0	0.5	2.0	12.5	3.3	3	2.8	13.5	5.0	2.7	2.8	21.5	5.6	22	9	·	·	·	13	7	·	5	2	3	–	6	12	1
V	11.5	3.1	2.0	4.8	5	2.4	8	2.2	1.5	2.3	5.5	3.5	12	6.7	11.5	4.2	1.8	3.4	25.2	6.4	10	1	·	·	·	12	7	·	3	2	3	–	5	8	·
VI	0.5	1.0	10.5	2.7	7	1.9	4	3.0	1.5	1.7	5.5	2.4	25.5	4.8	6.5	3.8	2.9	2.4	12.0	2.9	5,9	·	·	·	1	7	4	·	3	·	2	–	5	4	·
VII	1.5	1.0	5.5	1.9	1.7	2.6	1	1.0	1.5	3.3	5	3.3	23	3.2	5.5	5.0	3.3	1.9	99.3	31.8	12	·	·	·	2	15	12	3	1	·	1	–	2	6	·
VIII	3	2.7	3.5	2.8	4	2.0	3.5	4.7	2	1.0	2.0	5.0	21.5	4.7	4.5	3.2	3.1	3.0	115.3	24.0	28	·	·	·	2	14	12	5	4	·	·	–	·	10	·
IX	1	5.0	·	·	3	2.3	4	3.0	·	·	2.9	4.6	12	4.8	2.0	8.1	2.1	4.2	99.5	18.4	23	·	·	·	·	16	14	3	9	7	1	–	1	11	·
X	·	·	·	·	·	·	4	2.2	6	2.3	3.6	5.4	22.5	6.8	2.5	3.6	2.2	4.1	14.5	2.9	1	·	·	·	·	11	7	·	5	4	·	–	·	13	·
XI	1	2.0	6	8.2	12.5	6.5	8	2.6	2.5	3.6	2.0	2.9	12	6.7	2	12.5	2.6	3.8	16.4	6.5	28	7	·	·	·	10	6	·	5	3	1	–	2	24	1
XII	0.5	1.7	4	1.7	7.5	9.7	4.5	5.7	0.5	2.0	3.5.5	4.8	16.5	6.0	7	8.9	2.0	5.3	29.6	6.4	31	18	4	1	·	9	8	·	12	6	–	–	1	22	6
Rok	4.0	2.6	8.9	3.6	7.5	3.8	6.8	3.0	2.0	2.1	21.5	4.0	21.2.5	5.8	8.1.5	6.0	2.9.4	3.6	5.0.2.6	3.1.8	12.VII	8.7	11	1	5	14.2	9.3	11	7.9	3.8	–	–	27	1.6.2	2.3

Poraj

H_s = 5 m h_w = 10 m

I	1.5	3.0	1.5	9.3	7.5	4.8	4	2.8	1.8	2.6	24.5	3.6	24	8.5	6	6.1	6	4.7	16.1	6.1	5	23	5	1	·	17	4	·	6	·	–	·	·	20	–
II	3	3.2	4	1.1	5	1.0	9.5	2.4	2.1	3.1	15.5	3.1	1.8	4.3	8	1.1	·	2.9	37.1	7.5	9	17	·	·	·	15	3	·	1	·	–	·	·	17	–
III	4	3.0	3	3.7	8	3.9	22	5.4	11	5.0	9	3.3	14	6.2	8	3.4	14	4.0	18.4	7.2	15	25	1	·	·	6	4	·	4	2	–	·	8	8	–
IV	16	2.9	10	3.2	7	2.7	6	3.0	6	3.7	6	2.3	7	3.7	13	3.8	19	2.5	36.4	14.2	22	16	·	·	·	11	6	1	2	·	–	·	5	12	–
V	15	3.4	12	3.6	7	3.9	14	2.5	3	3.0	13	3.1	8	2.4	17	2.8	4	2.9	33.0	12.8	9	7	·	·	·	10	5	1	·	·	–	2	–	–	–
VI	6	2.0	6	1.7	9	2.0	9	3.0	6	1.5	16	3.3	18	3.3	14	2.9	6	2.5	46.0	34.0	9	·	·	·	3	8	6	1	1	·	–	1	11	6	–
VII	8	2.1	8.5	3.1	5.5	2.7	15	2.5	13	1.7	18	3.7	7	2.0	12	3.2	6	2.5	171.5	35.3	23	·	·	·	5	19	16	7	·	·	–	6	3	7	–
VIII	5	2.0	2	2.0	1	1.0	12	1.9	20	1.8	28	3.1	7	1.7	10	3.0	8	2.2	193.0	44.5	16	·	·	·	2	17	15	7	·	·	–	5	5	7	–
IX	4	4.8	1	8.0	1	3.0	2	1.5	27.5	3.1	17.5	5.1	15	4.5	14	4.8	8	3.8	106.0	19.5	27	2	·	·	1	16	16	3	6	1	–	2	2	14	–
X	3	3.0	1	1.0	·	·	4	4.8	22.5	3.3	37.5	4.5	18.5	3.8	3.5	4.9	3	3.9	26.4.2	3.4	5	1	·	·	·	15	11	·	4	·	–	·	2	16	–
XI	3	12.0	·	·	1.3	4.5	17	2.4	2.4	2.9	11	5.4	13	4.7	3	8.7	6	3.9	38.0	7.9	27	13	1	1	·	9	9	·	5	1	–	·	1	21	–
XII	3	2.0	4	11.8	7	4.7	·	·	2.2	3.0	3.5	5.4	9.5	4.9	5.5	10.5	7	4.8	45.2	12.0	31	22	5	4	·	13	7	1	6	2	–	1	3	22	–
Rok	71.5	3.6	5.3	4.0	7.1	2.8	11.4.5	2.7	19.4	2.3	23.1	3.8	15.9	4.2	11.4	4.6	8.7	3.4	767.1	44.5	16.VIII	126	12	6	11	158	109	21	37	6	–	[illegible]	–	–	–

Hel

$\varphi = 54°36'$ $\lambda = 18°49'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1018.0	1033.2	999.9	1018.3	0.7	1.7	1.1	1.2	2.5	-1.0	8.3	6,9	-8.0	16	92	88	91	90	0.5	0.8	0.6	0.6	7.9	8.0	7.7	7.9
II	1008.9	1036.1	983.1	1009.2	1.7	3.8	2.3	2.5	4.4	0.2	9.1	2	-7.7	25	94	84	91	90	0.4	1.3	0.6	0.8	9.0	8.0	8.0	8.3
III	1018.1	1036.9	988.5	1018.4	0.7	4.4	1.9	2.2	5.5	-1.1	11.8	27,31	-8.7	16	84	69	83	79	1.0	2.7	1.2	1.6	5.3	6.5	5.2	5.7
IV	1019.1	1032.8	991.5	1019.4	4.0	8.3	3.5	4.8	9.5	0.5	19.0	5,29	-7.9	15	89	70	90	83	0.9	3.7	0.8	1.8	6.5	6.0	6.2	6.2
V	1016.8	1030.9	1003.0	1017.1	8.3	12.0	7.1	8.6	13.1	4.3	21.9	20	-2.0	2	83	68	88	80	1.9	4.9	1.3	2.7	5.9	5.4	4.7	5.3
VI	1016.2	1032.0	1002.9	1016.5	14.2	17.6	12.9	14.4	19.4	8.9	27.8	18	2.1	21	80	64	84	76	3.4	7.5	2.4	4.4	5.2	6.1	4.9	5.4
VII	1011.1	1022.9	1001.3	1011.4	17.1	20.3	16.3	17.5	21.7	13.5	27.9	8	6.0	1	89	74	89	84	2.2	6.7	2.0	3.6	6.3	6.2	5.2	5.9
VIII	1012.0	1023.3	1000.2	1012.3	15.9	19.7	15.6	16.7	20.7	12.9	25.6	11	9.2	9	87	70	88	82	2.3	7.3	2.1	3.9	5.2	6.3	5.9	5.8
IX	1009.4	1022.7	989.7	1009.7	11.6	14.6	11.7	12.4	15.6	9.1	25.3	9	4.4	30	87	75	86	83	1.7	4.4	1.9	2.7	7.0	6.8	6.3	6.7
X	1015.9	1030.0	1001.8	1016.2	8.9	11.9	9.9	10.2	12.6	7.5	16.7	19	4.2	1	92	79	87	86	0.9	2.9	1.6	1.8	7.7	7.8	6.7	7.4
XI	1020.2	1041.2	999.3	1020.5	5.7	6.9	6.0	6.2	7.7	4.1	13.0	5	-3.4	30	89	84	87	87	0.9	1.5	1.1	1.2	8.8	8.3	8.1	8.4
XII	1012.2	1030.7	966.9	1012.5	1.5	2.1	1.9	1.8	3.4	-0.6	8.4	9	-7.2	18	88	84	86	86	0.8	1.1	0.9	0.9	7.9	8.3	6.8	7.7
Rok	1014.8	1041.2	966.9	1015.1	7.5	10.3	7.5	8.2	11.3	4.9	27.9	8.VII	-8.7	16.III	88	76	88	84	1.4	3.7	1.4	2.2	6.9	7.0	6.3	6.7

Ustka

$\varphi = 54°35'$ $\lambda = 16°52'$

I	1017.4	1031.7	998.2	1018.4	0.5	1.7	0.9	1.0	2.9	-1.0	10.4	6	-8.5	2	93	87	90	90	0.4	0.9	0.6	0.6	8.6	7.4	7.6	7.9
II	1007.5	1036.7	980.2	1008.5	1.6	4.4	2.7	2.8	5.7	0.6	11.0	2	-3.9	27	96	84	93	91	0.3	1.4	0.5	0.7	7.7	8.2	7.2	7.7
III	1016.8	1037.5	987.8	1017.8	0.7	4.1	2.4	2.4	6.4	-0.4	16.9	27	-5.8	9	86	77	84	82	0.9	2.1	1.3	1.4	6.6	6.2	4.0	5.6
IV	1018.5	1031.7	999.0	1019.5	3.3	5.9	3.8	4.2	7.7	1.4	19.1	5	-2.9	15	91	82	89	87	0.8	2.0	1.0	1.3	7.7	7.1	6.0	6.9
V	1016.1	1031.1	1002.5	1017.1	8.4	10.0	8.5	8.8	11.9	5.5	24.5	16	-0.4	6	84	81	83	83	1.8	2.9	2.1	2.3	5.9	5.4	5.2	5.5
VI	1015.3	1031.3	1002.1	1016.3	13.9	15.8	13.9	14.4	18.3	10.3	28.3	11	6.3	8	82	74	84	80	3.0	5.1	2.6	3.6	6.0	5.0	4.0	5.0
VII	1010.4	1021.4	1000.2	1011.3	16.6	19.1	17.2	17.5	20.9	14.4	28.7	20	10.1	7	91	81	87	86	1.9	4.9	2.7	3.2	7.6	6.7	5.4	6.6
VIII	1011.1	1023.4	998.2	1012.0	15.2	18.4	15.5	16.2	19.6	12.9	26.5	11	9.2	28	87	74	87	83	2.4	5.7	2.5	3.5	6.4	6.9	5.6	6.3
IX	1008.7	1022.1	988.4	1009.7	10.7	13.7	11.4	11.8	15.0	9.0	25.5	8	3.8	17	89	75	86	83	1.5	4.2	1.9	2.5	8.1	7.4	6.4	7.3
X	1014.8	1028.2	1000.1	1015.8	8.7	11.3	9.7	9.8	12.1	7.6	18.6	10	3.2	2	91	80	89	87	1.0	2.8	1.4	1.7	8.4	7.6	7.1	7.7
XI	1019.1	1039.5	998.6	1020.1	4.3	6.7	4.9	5.2	7.8	3.2	14.8	5	-3.2	21	93	84	90	89	0.6	1.7	0.8	1.0	7.8	8.5	7.4	7.9
XII	1011.4	1029.7	967.3	1012.4	0.6	1.7	1.5	1.3	3.4	-0.8	7.8	8	-10.6	18	89	85	87	87	0.7	1.0	0.8	0.8	7.7	8.1	7.6	7.8
Rok	1013.9	1039.5	967.3	1014.9	7.0	9.4	7.7	8.0	11.0	5.2	28.7	20.VII	-10.6	18.XII	89	80	87	85	1.3	2.9	1.5	1.9	7.4	7.0	6.1	6.8

Lębork

$\varphi = 54°33'$ $\lambda = 17°45'$

I	1015.6	1029.7	997.1	1018.3	0.3	1.4	0.7	0.8	2.5	-1.9	10.5	6	-11.8	16	89	85	88	87	0.7	1.1	0.8	0.9	9.0	8.7	8.6	8.8
II	1006.1	1034.1	978.9	1008.8	1.5	4.5	2.7	2.8	5.6	0.1	11.4	2	-8.0	25	89	75	87	84	0.8	2.1	1.0	1.3	8.2	8.3	8.2	8.2
III	1015.2	1035.2	986.0	1017.9	-0.1	5.6	2.0	2.4	7.1	-1.6	17.8	31	-7.8	9	83	64	81	76	1.1	3.8	1.4	2.1	5.6	6.8	4.8	5.7
IV	1016.5	1030.5	988.6	1019.2	2.9	9.3	3.8	5.0	10.3	-0.1	22.3	28	-7.9	15	87	63	84	78	1.0	5.2	1.3	2.5	7.5	7.2	5.7	6.7
V	1014.3	1028.9	1000.5	1016.9	8.3	12.4	8.2	9.3	13.7	4.0	23.6	16	-2.7	27	78	57	77	71	2.7	7.0	2.8	4.2	6.4	7.5	4.7	6.2
VI	1013.7	1029.8	1000.2	1016.3	13.5	18.5	14.1	15.0	20.3	8.0	28.4	11	2.1	15	80	59	78	72	3.2	9.2	3.7	5.4	5.9	6.5	4.2	5.5
VII	1008.7	1020.4	998.3	1011.2	16.4	20.6	16.3	17.4	22.1	12.5	28.8	20	7.0	4	87	69	85	80	2.5	8.4	2.7	4.5	7.1	7.4	5.7	6.7
VIII	1009.4	1021.4	997.3	1011.9	14.3	18.7	14.7	15.6	20.1	11.2	26.1	11	4.7	9	89	67	89	82	1.9	7.4	1.9	3.7	6.5	7.6	5.6	6.6
IX	1007.1	1020.7	988.2	1009.7	9.8	14.1	10.3	11.1	15.4	7.3	26.6	8	-0.5	26	88	69	86	81	1.5	5.6	2.0	3.0	7.2	8.0	6.3	7.2
X	1013.3	1027.0	999.1	1015.9	8.0	11.8	9.1	9.5	12.6	6.3	20.1	10	1.6	2	88	71	83	81	1.4	4.1	2.0	2.5	8.2	8.0	6.5	7.6
XI	1017.5	1038.3	997.6	1020.2	4.0	6.7	4.8	5.1	7.7	2.8	15.5	5	-7.1	30	86	76	83	82	1.2	2.5	1.5	1.7	8.2	8.3	7.6	8.0
XII	1009.7	1028.6	965.8	1012.4	-0.1	1.3	0.5	0.6	2.6	-1.9	8.5	8	-12.4	18	85	79	85	83	0.9	1.4	1.0	1.1	8.2	8.5	7.3	8.0
Rok	1012.3	1038.3	965.8	1014.9	6.6	10.4	7.3	7.9	11.7	3.9	28.8	20.VII	-12.4	18.XII	86	70	84	80	1.6	4.8	1.8	2.7	7.3	7.7	6.3	7.1

Gdynia

$\varphi = 54°31'$ $\lambda = 18°33'$

I	–	–	–	–	1.1	2.0	1.5	1.5	3.4	-0.6	11.3	6	-8.6	16	87	83	84	85	1.0	1.3	1.1	1.1	8.9	7.7	8.1	8.2
II	–	–	–	–	2.4	4.1	3.4	3.3	5.7	1.2	11.7	2	-5.8	25	88	80	84	84	0.9	1.8	1.3	1.3	9.2	8.5	8.9	8.9
III	–	–	–	–	1.4	4.1	2.8	2.8	6.3	-0.2	15.3	13	-5.7	17	76	67	75	73	1.7	2.9	1.9	2.2	5.9	7.1	4.9	6.0
IV	–	–	–	–	4.2	6.8	4.8	5.2	9.0	2.1	21.1	5	-3.7	15	84	76	83	81	1.4	2.7	1.5	1.9	7.1	7.1	6.4	6.9
V	–	–	–	–	8.4	10.4	8.9	9.2	12.0	6.0	20.4	31	1.5	6	79	73	79	77	2.5	3.5	2.6	2.9	6.8	6.9	6.0	6.6
VI	–	–	–	–	14.5	16.8	14.4	15.0	18.9	10.9	24.4	18,30	7.5	8	73	66	76	72	4.6	6.8	4.0	5.1	6.4	7.0	7.0	6.8
VII	–	–	–	–	17.2	19.6	17.4	17.9	20.9	15.0	24.8	19	11.5	1	85	73	83	80	3.0	6.4	3.5	4.3	7.3	7.3	7.2	7.3
VIII	–	–	–	–	15.9	18.7	16.2	16.8	20.0	14.0	25.2	11	10.6	23,30	82	69	84	78	3.4	7.0	3.0	4.5	5.4	7.5	5.9	6.3
IX	–	–	–	–	11.0	14.2	11.3	12.0	15.5	9.3	27.3	9	3.8	27	86	70	85	80	1.9	5.4	2.1	3.1	7.1	7.9	7.1	7.4
X	–	–	–	–	8.5	11.9	9.8	10.0	13.1	7.5	19.1	19	2.9	2	89	73	84	82	1.2	3.9	2.0	2.4	7.4	7.8	6.1	7.1
XI	–	–	–	–	5.4	6.8	5.9	6.0	8.1	4.3	13.1	5	-2.3	30	87	82	83	84	1.2	1.8	1.4	1.5	9.2	8.7	8.3	8.7
XII	–	–	–	–	1.1	2.0	1.4	1.5	3.6	-0.6	8.5	8	-8.3	18	85	80	84	83	1.0	1.5	1.0	1.1	8.1	8.0	6.6	7.6
Rok	–	–	–	–	7.6	9.8	8.2	8.4	11.4	5.7	27.3	9.IX	-8.6	16.I	83	74	82	80	2.0	3.7	2.1	2.6	7.4	7.6	6.9	7.3

Hel

$H_s = 1\,m$ $H_b = 2.6\,m$ $h_w = 24\,m$ 1957

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max 0–10	Min<0	Min>25	Opad R 0.1–1.0	1.1–10.0	>10.0	Wiatr v ≥10	≥15	=	≈	●	●	≡
I	0.5	4.0	1	12.0	7	6.9	3.5	4.9	12.5	3.4	2.5	4.4	3.0	6.9	10.5	7.0	3	5.5	17.8	4.6	26	19	5	·	·	11	7	·	8	1	1	·	·	17	7
II	1.5	2.3	5.5	2.8	2.5	2.6	4.5	4.4	25.5	4.0	12.5	4.6	1.7	4.3	9	5.2	6	3.9	40.1	5.7	1	11	·	·	·	19	15	·	1	·	6	·	·	19	2
III	8.5	4.5	10	4.4	8.5	3.9	18.5	5.6	12.5	5.9	8.5	3.8	13.5	6.0	12	4.6	1	5.0	18.4	6.7	15	20	1	·	·	7	6	·	6	1	2	·	8	11	2
IV	22.5	3.5	20.5	3.9	9	2.2	4.5	2.0	1.5	3.3	5.5	5.5	6.5	5.2	1.4	3.5	6	3.4	12.9	4.3	16	9	·	·	·	10	5	·	1	·	7	2	5	12	·
V	19.5	4.0	18.5	5.6	3.5	4.0	8.5	3.7	7	1.9	4.5	3.3	6.5	5.7	1.9	4.9	6	4.1	22.6	5.9	11	1	·	·	·	12	6	·	3	·	5	1	6	8	·
VI	6	2.8	4.3	3.7	11.5	3.1	3	3.2	2	4.0	4	4.1	2.0	4.7	21.5	3.8	9	3.5	20.0	4.8	5	·	·	·	1	11	7	·	2	·	3	·	5	7	·
VII	9	2.6	10.5	2.9	4.1	3.6	7	3.7	7.5	2.4	7	3.9	1.9	4.9	1.6	4.9	6	3.6	94.5	20.6	27	·	·	·	3	15	11	3	1	·	3	7	3	8	·
VIII	4.5	4.1	5	3.0	6	2.7	3.5	4.1	13.5	4.1	13.5	6.4	2.8	5.2	1.2	3.9	7	4.3	94.7	22.5	16	·	·	·	1	17	14	4	5	·	·	5	1	9	·
IX	3.5	3.0	1	2.0	1	1.0	4	3.0	1.7	5.4	20.5	6.2	1.6	6.8	2.5	5.8	2	5.5	122.4	18.6	20	·	·	·	1	21	18	3	9	·	·	2	·	10	·
X	·	·	·	·	1	1.0	0.5	3.0	1.6.5	5.0	3.7	5.4	3.0	5.7	7	6.1	1	5.4	12.6	3.3	4	·	·	·	·	12	5	·	6	·	1	·	1	14	·
XI	0.5	2.0	7	7.0	1.0	6.6	8.5	3.9	18.5	4.4	1.6	5.1	13.5	6.2	8	6.0	8	5.0	27.9	8.8	28	3	·	·	·	11	6	·	9	·	·	·	2	23	1
XII	1.5	5.3	5.5	9.6	6.5	7.2	1.5	3.0	12.5	5.6	28.5	5.9	2.6	6.9	9	7.1	2	6.4	41.2	13.5	31	16	4	·	·	13	8	1	12	·	1	·	2	16	6
Rok	77.5	3.2	97.5	4.7	77.5	3.7	67.5	3.7	146.5	4.1	182.5	4.9	22.6	5.7	16.3	5.2	57	4.6	525.1	22.5	16.VIII	79	10	·	6	159	108	11	63	2	29	17	33	154	18

Ustka

$H_s = 6\,m$ $H_b = 8.1\,m$ $h_w = 18\,m$

I	2	6.0	1	6.0	6	4.5	12.5	2.7	9	3.5	3.3.5	5.9	2.3.5	8.6	3.5	8.1	2	5.8	25.7	6.4	12	17	5	·	·	17	7	·	8	·	12	·	2	20	11
II	4.5	2.8	5	4.4	6	1.5	3	3.0	16.5	3.3	28.5	4.9	17	6.4	3.5	6.1	·	4.5	38.1	6.4	9	10	·	·	·	16	11	·	4	·	4	·	1	15	2
III	10.5	4.1	10	3.9	6	3.7	11	4.8	20	4.3	10.5	7.1	15	5.0	7	4.8	3	4.6	26.7	8.6	15	18	1	·	·	12	6	·	6	2	5	·	4	8	2
IV	18	3.1	25.5	4.2	7.5	2.3	0.5	3.0	2	3.2	6.5	4.8	14.5	4.4	13.5	3.6	2	3.7	22.8	6.9	16	8	·	·	·	12	7	·	·	·	7	2	5	14	2
V	6.5	4.7	23.5	5.2	3	3.5	2	3.0	7.5	3.9	6	3.0	2.9	5.1	10.5	3.6	5	4.3	45.8	15.0	9	1	·	·	·	10	6	2	4	2	4	3	6	9	·
VI	5	1.7	16.5	2.6	1.5	2.3	5	3.8	1	3.0	1.3	3.4	37.5	5.1	6.5	3.4	4	3.7	37.2	24.4	9	·	·	·	3	10	7	1	3	·	3	1	7	4	·
VII	6.5	2.4	8	3.6	3	2.7	9.5	3.9	4.5	2.1	8	3.3	28.5	4.6	20	6.4	5	4.1	149.5	29.0	17	·	·	·	4	18	16	5	5	·	2	5	1	9	·
VIII	5.5	1.6	2	4.0	2	3.0	3	3.7	1.0	3.0	2.3	4.3	3.1	5.5	14.5	5.7	2	4.5	131.2	30.1	26	·	·	·	1	16	11	5	6	·	·	3	2	11	·
IX	3.5	4.1	2	3.8	1	3.0	1.5	1.2	1.0	3.4	3.0.5	4.7	1.5	7.0	24.5	7.9	2	5.6	141.0	20.3	29	·	·	·	1	19	14	7	6	5	2	1	·	14	·
X	3	3.7	1	6.0	·	·	·	·	7.5	5.1	4.7	5.4	2.4	6.4	7.5	9.9	3	5.8	29.1	4.2	31	·	·	·	·	18	10	·	7	2	3	·	1	19	·
XI	3.5	9.1	1	14.0	1.3	4.7	8	3.0	27.5	3.2	18.5	4.0	14	8.9	2.5	1.1	2	5.0	20.1	8.2	27	8	·	·	·	11	7	·	7	·	1	·	3	18	1
XII	6	6.2	6.5	8.1	4.5	5.9	6	4.0	17	4.0	3.1	6.1	13.5	8.3	7.5	8.8	1	6.2	51.0	16.4	30	17	4	1	·	14	6	2	12	2	7	·	2	19	12
Rok	74.5	4.1	102	5.5	53.5	3.1	62	3.0	132.5	3.5	25.6	4.7	262.5	6.3	12.1	5.8	31	4.8	718.2	30.1	26.VIII	79	10	1	9	173	108	22	68	14	50	15	34	160	30

Lębork

$H_s = 18\,m$ $H_b = 21.8\,m$ $h_w = 12\,m$

I	1	1.0	1.5	3.0	16.5	2.5	7.5	1.3	7	2.0	26.5	3.9	3.0	4.8	3	4.7	·	3.5	19.0	6.7	5	21	6	1	·	16	4	·	1	·	1	·	·	22	10
II	2	2.5	11.5	1.0	12	1.3	8	2.1	11	2.3	18	3.8	18	3.8	3.5	2.7		2.6	45.8	11.4	9	13	·	·	·	16	11	1	2	·	1	·	·	19	2
III	6	1.5	12.5	1.1	2.7	2.5	6.5	3.2	5.5	3.1	10	2.3	19	4.7	5.5	3.7	1	2.8	21.8	9.4	15	21	1	·	·	10	4	·	1	1	2	·	3	8	4
IV	16	1.2	20.5	1.5	16.5	1.4	1	2.5	1.5	2.7	10	2.6	9.5	2.8	10	2.8	5	1.8	41.9	15.3	22	15	·	·	·	18	7	1	·	·	7	1	5	13	2
V	7.5	2.1	2.5	2.8	13.5	1.6	1.5	3.7	3	3.0	8.5	2.5	2.4	2.6	10	2.8	·	2.5	47.9	14.7	20	4	·	·	·	15	7	2	·	·	3	2	2	9	·
V	2	2.2	7	1.7	20.5	1.7	3	1.8	5	1.3	1.2	2.7	36.5	3.9	5	2.9	1	2.8	18.9	7.3	9	·	·	·	3	11	5	·	·	·	·	1	5	6	·
VI	5.5	1.3	11.5	1.2	1.7	1.7	5	1.6	5.5	1.6	11	2.6	27.5	2.9	6	2.7	4	2.1	146.0	38.7	16	·	·	·	7	20	16	4	·	·	3	6	·	9	·
VII	4	1.6	9	1.2	10.5	1.3	6.5	2.2	10.5	2.3	2.2	2.9	2.5	2.9	5.5	1.7	·	2.3	156.7	40.2	18	·	·	·	1	19	18	5	·	·	3	5	·	9	·
VIII	4.5	1.2	4	1.0	7	1.1	4.5	2.2	6.5	4.5	24.5	3.4	26.5	3.8	12.5	3.2	·	3.1	97.6	15.8	23	2	·	·	2	19	14	5	·	·	1	·	·	12	·
IX	1.5	1.3	1.5	1.3	4.5	1.6	3.5	2.0	1.0	3.4	3.5	3.2	3.5.5	3.2	0.5	1.0	1	3.0	31.7	4.0	3	·	·	·	·	15	11	·	·	·	5	·	1	15	·
X	2	6.2	1.2	1.7	1.8	1.9	11.5	2.0	10.5	2.3	15.5	2.3	4.6	4.1	4.5	4.4	·	2.6	45.2	8.9	28	9	1	·	·	11	9	·	2	·	1	·	1	20	1
XI	2	2.0	5.5	3.9	7	2.7	6.5	1.7	13.5	1.8	2.9	3.7	2.2	4.0	3.5	4.1	4	3.1	61.5	18.5	29	17	5	2	·	14	7	3	·	·	2	1	2	16	8
Rok	5.4	2.0	12.1.5	1.8	17.0	1.8	6.5	2.2	87.5	2.5	22.2	3.0	28.9.5	3.6	6.9.5	3.1	16	2.7	734.0	40.2	18.VIII	102	13	3	13	184	113	21	6	1	29	16	19	158	27

Gdynia

$H_s = 2\,m$ $h_w = 12.5\,m$

I	0.5	5.0	1	9.5	5	10.0	4.5	4.7	14	3.4	16.5	3.3	40.5	6.0	9	4.7	2	5.1	18.4	4.8	12	18	6	·	·	11	9	·	7	·	4	·	·	19	7
II	2	4.5	1.5	4.3	1.5	4.3	8	6.0	22	5.5	16.5	4.6	19.5	4.9	8	4.7	5	4.8	40.1	5.5	12	7	·	·	·	19	14	·	6	·	3	·	·	21	4
III	7	5.0	5	3.4	5	9.5	15.5	8.3	12.5	6.4	7.5	4.4	17.5	4.6	1.9	4.7	4	5.5	18.6	6.0	15	19	·	·	·	9	4	·	10	6	4	·	5	10	·
IV	20.5	4.4	7	6.9	3.5	3.9	3.5	2.4	5.5	4.3	8.5	4.0	1.8	2.5	19.5	4.4	4	3.9	18.9	5.0	22	7	·	·	·	15	8	·	3	·	5	1	4	14	2
V	1.4	5.6	14.5	6.8	2	5.5	8.5	4.9	7	3.6	8	4.4	1.3	4.3	2.1	4.6	5	4.8	33.5	8.0	9	·	·	·	·	14	9	·	5	·	2	3	1	8	·
VI	4.5	3.6	7	3.4	5.5	3.0	4.5	3.4	1.2	2.1	7	3.7	2.5	4.5	16.5	3.9	8	3.3	18.7	5.2	22	·	·	·	·	10	6	·	4	·	3	1	1	13	·
VII	5	2.6	2.5	1.8	5.5	3.6	9.5	3.3	12.5	2.2	8	3.0	2.4	4.1	1.7	5.1	9	3.3	119.8	28.0	12	·	·	·	·	12	10	5	1	·	4	8	1	13	·
VIII	3.5	5.1	9.1	6.2	1	4.5	5	5.1	8.5	6.5	17.5	4.9	28.5	4.9	13	3.8	12	4.3	95.0	21.6	16	·	·	·	1	18	13	4	6	·	·	5	·	10	·
IX	4	6.0	0.5	3.0	·	·	3	4.0	10.5	3.9	24.5	4.7	24	3.9	17.5	5.0	6	4.2	80.1	12.8	23	·	·	·	2	19	13	3	5	·	·	·	·	11	·
X	·	·	·	·	·	·	2	3.0	16.5	5.4	27.5	4.9	2.9	4.2	11	4.9	7	4.4	12.6	3.5	1	·	·	·	·	13	6	·	4	·	3	·	1	9	·
XI	1.5	10.7	5	10.3	10.5	6.8	4.5	4.6	19.5	5.3	17	4.1	17.5	4.1	7.5	5.7	7	5.0	15.0	4.3	27	5	·	·	·	9	5	·	7	·	1	·	·	22	4
XII	1.5	9.3	4	9.1	3.5	6.9	1.5	10.0	10	4.0	18	5.0	38	3.7	5.5	6.4	11	4.3	61.3	19.3	31	16	4	·	·	12	6	3	7	·	4	·	2	17	5
Rok	6.4	5.2	5.2	5.4	4.3	4.8	7.0	5.0	15.0.5	4.4	17.6.5	4.2	29.4.5	4.3	16.4.5	4.8	8.0	4.4	532.0	28.0	12.VII	72	10	·	3	161	103	15	65	6	33	18	15	167	19

Słupsk

$\varphi = 54°28'$ $\lambda = 17°02'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max obs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	1.6	0.6	0.8	2.7	-1.8	10.9	6	-10.1	16	90	84	90	88	0.6	1.1	0.5	0.7	8.9	7.7	8.0	8.2
II	–	–	–	–	1.2	4.4	2.3	2.6	5.8	-0.5	10.6	12	-8.9	25,26	94	83	93	90	0.4	1.5	0.5	0.8	7.9	6.8	8.4	7.7
III	–	–	–	–	0.3	6.1	2.1	2.6	7.4	-1.4	17.1	27	-7.4	17	83	66	82	77	1.1	3.6	1.4	2.0	6.4	5.0	4.2	5.2
IV	–	–	–	–	3.2	9.6	4.3	5.4	10.8	0.6	22.3	28	-5.1	15	88	67	88	81	0.9	4.9	1.1	2.3	7.0	6.5	5.3	6.3
V	–	–	–	–	8.7	13.0	8.2	9.5	14.3	4.1	24.3	16	-1.9	6	79	58	83	73	2.5	7.3	2.0	3.9	6.3	7.2	5.2	6.2
VI	–	–	–	–	14.2	19.2	13.8	15.2	21.0	8.8	28.5	11	4.0	8	81	57	84	74	3.3	10.5	2.7	5.5	5.4	5.9	3.5	4.9
VII	–	–	–	–	16.7	21.1	16.6	17.8	22.7	13.0	28.9	20	8.4	7	87	66	87	80	2.6	9.5	2.7	4.9	7.4	6.7	5.9	6.7
VIII	–	–	–	–	14.6	19.0	14.6	15.7	20.4	11.4	26.6	11	7.4	9	90	68	91	83	1.7	7.4	1.6	3.6	6.8	7.0	6.4	6.7
IX	–	–	–	–	9.9	14.4	10.1	11.1	15.5	6.9	27.0	8	-0.1	27	93	68	91	84	0.9	5.7	1.3	2.6	7.5	8.0	6.6	7.4
X	–	–	–	–	8.0	11.6	8.9	9.4	12.7	6.1	19.1	10	1.7	2	92	76	90	86	0.9	3.4	1.2	1.8	8.5	7.8	6.6	7.6
XI	–	–	–	–	4.0	6.6	4.7	5.0	7.6	2.2	15.5	5	-6.2	21	90	81	87	86	0.8	2.0	1.1	1.3	8.2	9.0	7.6	8.3
XII	–	–	–	–	-0.3	1.5	0.6	0.6	2.8	-2.2	9.0	8	-12.2	17,18	89	85	86	86	0.6	1.0	0.8	0.8	8.3	7.4	7.9	7.9
Rok	–	–	–	–	6.7	10.7	7.2	8.0	12.0	3.9	28.9	20.VII	-12.2	17,18.XII	88	72	88	83	1.4	4.8	1.4	2.5	7.4	7.1	6.3	6.9

Darłowo

$\varphi = 54°27'$ $\lambda = 16°23'$

I	–	–	–	–	0.5	1.6	1.0	1.0	2.7	-1.1	7.4	6	-7.5	1	90	80	88	89	0.6	0.8	0.8	0.7	8.1	7.3	6.9	7.4
II	–	–	–	–	1.8	4.1	2.7	2.8	5.5	0.1	9.7	2	-5.9	27	91	84	89	88	0.7	1.4	0.8	1.0	8.1	6.9	7.2	7.4
III	–	–	–	–	1.3	4.4	2.4	2.6	6.1	-0.7	16.1	27	-6.4	17	84	77	85	81	1.1	2.2	1.1	1.5	6.1	5.4	4.2	5.2
IV	–	–	–	–	3.9	6.1	4.3	4.6	7.9	1.4	17.9	1,2	-4.7	15	86	80	86	84	1.2	2.3	1.2	1.6	7.2	6.1	4.8	6.0
V	–	–	–	–	8.4	10.1	8.7	9.0	12.1	4.9	24.2	16	-1.8	6	83	77	82	81	2.0	3.2	2.2	2.5	5.6	4.5	4.7	4.9
VI	–	–	–	–	13.4	15.7	14.3	14.4	17.9	10.1	28.5	11	6.2	8	84	77	81	81	2.6	4.5	3.2	3.4	4.9	4.0	3.6	4.2
VII	–	–	–	–	16.6	18.7	17.7	17.7	20.3	14.2	27.9	1	9.0	7	88	81	83	84	2.2	4.4	3.5	3.4	6.8	6.3	6.9	6.7
VIII	–	–	–	–	15.4	18.2	16.1	16.4	19.0	13.2	25.4	11	8.8	26	–	–	–	–	–	–	–	–	6.3	6.0	6.5	6.3
IX	–	–	–	–	11.2	13.7	11.9	12.2	15.0	9.1	23.4	8	4.2	17	86	77	83	82	1.9	3.9	2.3	2.7	7.3	6.7	6.7	6.9
X	–	–	–	–	9.3	11.3	10.2	10.2	12.0	7.7	18.3	10	3.2	21	87	84	85	85	1.5	2.6	1.9	2.0	8.5	6.5	6.7	7.2
XI	–	–	–	–	4.4	6.7	4.9	5.2	7.8	3.0	14.0	5	-3.5	21,30	86	80	87	84	0.9	2.0	1.2	1.4	8.2	7.9	7.4	7.8
XII	–	–	–	–	0.9	1.7	1.7	1.5	3.4	-0.8	6.9	5	-9.9	17	87	84	85	85	0.8	1.0	1.0	0.9	8.5	7.9	6.9	7.8
Rok	–	–	–	–	7.3	9.4	8.0	8.2	10.8	5.1	28.5	11.VI	-9.9	17.XII	–	–	–	–	–	–	–	–	7.1	6.3	6.0	6.5

Rębiska

$\varphi = 54°27'$ $\lambda = 18°20'$

I	–	–	–	–	-0.9	-0.4	-1.1	-0.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.7	7.8	8.1
II	–	–	–	–	0.6	2.5	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	6.5	7.2
III	–	–	–	–	-0.5	3.5	1.0	1.2	4.8	–	13.5	27	–	–	–	–	–	–	–	–	–	–	5.7	5.7	3.9	5.1
IV	–	–	–	–	3.5	7.9	4.3	5.0	9.0	–	22.1	28	–	–	–	–	–	–	–	–	–	–	6.6	6.8	6.2	6.5
V	–	–	–	–	7.3	11.3	7.8	8.6	12.2	–	24.1	13	–	–	–	–	–	–	–	–	–	–	5.7	6.1	5.0	5.6
VI	–	–	–	–	13.3	17.6	13.7	14.8	18.9	–	26.6	18	–	–	–	–	–	–	–	–	–	–	5.5	4.8	3.5	4.6
VII	–	–	–	–	15.6	19.6	15.9	16.8	20.2	–	27.5	8	–	–	–	–	–	–	–	–	–	–	6.1	5.9	6.2	6.1
VIII	–	–	–	–	14.0	17.9	14.1	15.0	18.4	–	23.1	11	–	–	–	–	–	–	–	–	–	–	5.0	5.8	5.1	5.3
IX	–	–	–	–	9.2	13.2	9.5	10.4	14.1	6.9	25.9	9	1.3	26	–	–	–	–	–	–	–	–	7.3	6.4	5.6	6.4
X	–	–	–	–	7.0	10.4	8.1	8.4	11.0	5.5	18.1	10	0.8	1	–	–	–	–	–	–	–	–	8.8	7.3	6.0	7.4
XI	–	–	–	–	3.4	5.2	3.9	4.1	6.2	2.0	12.5	5	-5.7	30	–	–	–	–	–	–	–	–	8.5	8.0	7.0	7.8
XII	–	–	–	–	-1.0	-0.3	-0.8	-0.7	1.0	-2.9	7.0	5	-10.2	19	–	–	–	–	–	–	–	–	8.4	8.0	7.6	8.0
Rok	–	–	–	–	6.0	9.0	6.5	7.0	–	–	27.5	8.VII	–	–	–	–	–	–	–	–	–	–	7.0	6.6	5.9	6.5

Sopot

$\varphi = 54°27'$ $\lambda = 18°34'$

I	–	–	–	–	0.5	1.9	1.2	1.2	3.0	-1.3	10.8	6	-9.8	16	85	79	83	82	1.0	1.6	1.2	1.3	8.5	7.8	8.6	8.3
II	–	–	–	–	2.2	4.6	3.4	3.4	5.8	1.0	11.2	6	-5.3	25	86	76	82	81	1.0	2.2	1.4	1.5	8.8	8.0	9.3	8.7
III	–	–	–	–	1.3	4.6	2.8	2.9	6.2	-0.4	15.6	27	-6.2	16	76	65	79	73	1.7	3.3	1.7	2.2	5.7	6.7	4.5	5.6
IV	–	–	–	–	4.8	7.0	4.9	5.4	8.8	2.1	21.5	5	-3.6	16	82	73	81	79	1.7	3.0	1.7	2.1	6.5	6.6	6.4	6.5
V	–	–	–	–	8.9	10.8	8.9	9.4	12.8	5.9	22.2	31	1.4	6	78	72	80	77	2.6	4.0	2.4	3.0	6.8	6.8	5.5	6.4
VI	–	–	–	–	14.6	17.6	14.2	15.2	19.4	10.2	26.2	9	6.8	8	74	63	77	71	4.5	7.8	3.8	5.4	5.8	7.1	5.5	6.1
VII	–	–	–	–	17.2	19.8	17.2	17.8	21.9	14.5	28.7	8	10.6	1	84	72	83	80	3.2	6.9	3.4	4.5	6.9	7.0	5.6	6.5
VIII	–	–	–	–	15.8	19.2	15.8	16.6	20.4	13.4	26.3	11	9.0	24	82	67	84	78	3.3	7.7	2.9	4.6	5.8	7.6	6.3	6.6
IX	–	–	–	–	10.8	14.6	11.0	11.8	15.9	8.7	27.9	9	3.9	27	84	69	84	79	2.1	6.0	2.1	3.4	8.2	8.4	6.3	7.6
X	–	–	–	–	8.3	12.4	9.5	9.9	13.3	7.1	20.5	10	3.0	2	87	68	82	79	1.4	4.6	2.1	2.7	7.8	8.7	6.1	7.5
XI	–	–	–	–	5.1	7.0	5.6	5.8	8.0	3.7	14.4	5	-4.1	22	83	76	82	80	1.4	2.5	1.5	1.8	9.0	8.7	8.1	8.6
XII	–	–	–	–	0.9	1.9	1.3	1.4	3.3	-1.3	8.2	5	-11.3	17	79	75	80	78	1.4	1.7	1.3	1.5	8.5	8.4	6.7	7.9
Rok	–	–	–	–	7.5	10.1	8.0	8.4	11.6	5.3	28.7	8.VII	-11.3	17.XII	82	71	81	78	2.1	4.3	2.1	2.8	7.4	7.6	6.6	7.2

Stupsk

$H_s = 23\ m$ $h_w = 17\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU °D, °mD																	OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Max<0°	Max<0°	Min<-10°	Max>25°	0.1 ÷ 1.0	1.0 ÷ 10.0	10.0 ÷ 100.0	10 ÷ 15	15 ÷ 20	≡	≈	◔	●	⊞	
I	·	·	4	4,5	3	4,3	5	26	14,5	28	26,5	56	16	7,5	·	·	24	3,8	32,5	8,4	5	19	5	1	·	15	8	·	6	3	3	·	2	22	-
II	1,5	2,0	3	2,0	0,5	2,0	9,5	20	12,5	29	18	4,6	9,5	3,7	3,5	2,0	26	2,3	56,6	15,7	9	15	·	·	·	16	12	1	2	·	2	·	2	16	-
III	8,5	2,5	7,5	2,5	14	6,3	5	5,3	12,5	26	8	6,6	9,5	6,8	2	4,0	26	3,4	25,9	9,1	15	21	1	·	·	10	6	·	5	2	3	·	8	9	-
IV	17,5	2,4	8	2,6	5,5	2,2	0,5	3,0	4,5	2,0	8	3,4	9,5	3,3	8,5	5,0	28	2,1	32,2	10,8	16	13	·	·	·	17	6	1	3	·	3	1	5	12	-
V	19,5	3,0	5,5	3,1	3,5	2,6	4,5	2,4	3	2,3	14,5	2,6	1,5	5,1	13,5	3,7	14	2,8	33,7	12,7	9	4	·	·	·	11	8	1	2	1	·	3	2	12	-
VI	6,5	2,2	6,5	2,2	4,5	2,2	1,5	6,0	3	1,7	2,5	2,9	15,5	4,0	4,5	3,8	23	2,3	37,4	24,2	9	·	·	·	5	10	5	1	4	·	·	1	8	8	-
VII	9	2,3	1,5	3,0	5	1,5	4,5	2,7	6,5	1,6	1,8	2,9	23,5	2,6	4	2,0	21	1,9	119,5	24,8	25	·	·	·	9	19	14	5	·	·	·	4	1	10	-
VIII	4	1,8	1	6,0	3	1,8	6	2,4	13,5	2,9	19,5	3,0	9	3,3	4	5,2	33	1,9	108,1	18,6	14	·	·	·	1	18	13	5	1	·	1	5	1	13	-
IX	1,5	4,3	·	·	·	·	2,5	4,8	1,4	4,0	1,7	5,9	12,5	5,8	4,5	6,3	38	3,1	103,9	17,9	30	1	·	·	1	22	17	2	1	1,4	1	·	1	14	-
X	·	·	1	2,0	·	·	2	4,0	1,8	2,8	2,5	4,2	1,1	3,5	1	4,0	35	2,2	39,0	6,9	31	·	·	·	·	18	9	·	3	·	3	·	1	18	-
XI	3	3,2	5,5	3,7	7	1,9	9,5	2,9	8,5	1,9	1,2	3,9	7	5,9	1,5	4,7	36	2,0	48,2	13,1	28	10	1	·	·	10	8	2	2	·	1	·	3	22	-
XII	2	2,5	5	9,6	5	3,8	2,5	1,6	1,4	2,2	2,2,5	3,6	1,0	5,0	3	6,7	29	2,8	66,5	18,2	29	16	6	2	·	13	8	3	4	2	3	·	2	20	-
Rok	73	2,2	48,5	3,4	5,1	2,4	5,3	3,3	124,5	2,5	2,1,4	4,1	14,8	4,7	5,0	4,0	333	2,6	703,5	24,8	25.VIII	99	13	3	16	179	114	21	33	22	20	14	36	176	-

Dartowo

$H_s = 3\ m$ $h_w = 23\ m$

I	2	6,0	5	6,8	7	2,6	5	2,1	1,5	2,8	4,3	7,5	10,5	7,8	4,5	6,4	1	5,9	22,3	6,3	5	16	3	·	·	9	6	·	11	·	12	·	4	19	-
II	3	4,3	4	1,6	4,5	1,6	9	2,1	2,6	3,7	2,7,5	6,5	4	4,6	4	4,6	2	4,2	37,2	5,9	8	12	·	·	·	15	12	·	3	·	2	·	1	13	-
III	10	7,2	7,5	4,9	1,5	4,0	14,5	4,6	1,6	3,0	1,4	8,0	8,5	5,2	5,5	5,4	2	5,1	25,3	8,1	15	16	1	·	·	7	5	·	7	·	5	·	7	8	-
IV	2,6	4,4	16,5	3,7	1,1	1,8	1	1,5	8	2,9	10,5	4,7	10	4,8	6	5,5	1	3,9	13,7	6,8	16	8	·	·	·	8	4	·	3	·	7	·	5	11	-
V	1,7	4,9	1,4	5,4	9,5	2,3	3	4,7	5	3,2	1,1	4,6	2,5	4,8	7,5	4,5	1	4,5	26,9	6,6	9	2	·	·	·	11	7	·	4	1	4	3	8	8	-
VI	10,5	3,8	1,1	2,5	6	2,2	4,5	2,6	5,5	3,1	2,8	4,2	20,5	4,1	2	1,2	2	3,5	10,3	2,5	9	·	·	·	2	8	4	·	2	1	8	3			-
VII	8	4,1	5,5	2,2	9,5	1,8	6	1,9	8	3,2	10,5	5,2	3,4,5	4,6	9	4,0	2	3,8	140,9	39,2	26	·	·	·	2	14	12	4	1	·	3	5	1	11	-
VIII	5,5	2,1	2,5	3,4	3,5	1,9	6,5	3,8	1,9	3,3	2,4,5	6,1	2,3	6,9	5,5	2,5	3	4,7	123,5	35,2	26	·	·	·	1	15	13	5	7	·	1	3	1	10	-
IX	2,5	1,2	3,5	2,0	1	2,0	3	3,4	2,3,5	5,2	16,5	7,5	20,5	8,1	18,5	6,6	1	6,2	133,8	22,6	29	·	·	·	·	20	16	4	8	3	3	3	1	11	-
X	2,5	4,0	0,5	2,0	2,5	1,6	5,5	2,2	2,3	3,9	4,0	6,3	1,5	6,7	4	8,9	·	5,5	21,5	6,0	3	·	·	·	·	13	7	·	6	2	2	·	4	16	-
XI	3	13,0	9,5	6,6	12,5	2,0	17,5	1,9	19,5	2,3	12,5	6,4	9,5	9,9	3	13,3	3	4,7	26,9	9,2	27	7	·	·	·	9	7	·	7	2	7	1	3	18	-
XII	2	7,2	8,5	8,8	7,5	4,2	4	3,4	2,8	3,8	2,5,5	8,0	8	8,9	9,5	6,8	·	6,3	35,1	13,5	30	14	3	·	·	13	6	2	10	2	5	·	3	18	-
Rok	9,2	5,2	8,8	4,2	8,9,5	2,3	7,9,5	2,8	19,6,5	3,4	2,6,3,5	6,2	18,9	6,4	7,9	5,8	18	4,9	617,4	39,2	26.VII	75	7	·	5	142	99	15	68	10	53,7	16	43	146	-

Rębiska

$H_s = 150\ m$ $h_w = 15\ m$

I	·	·	1	2,0	5,5	7,1	2,5	2,4	5,5	2,0	2,2	4,2	4,0	7,6	16,5	8,1	·	6,3	18,3	6,0	5	-	-	-	·	12	7	·	7	1	-	-	·	20	-
II	5,5	2,8	1,5	3,0	0,5	2,0	1,5	3,7	9,5	4,0	2,3	4,5	2,8,5	4,8	14	4,4	·	4,4	47,5	14,0	9	-	-	-	·	20	15	1	1	·	7	·	1	12	-
III	15,5	3,9	6	4,2	4	5,2	17	5,6	9,5	4,8	11,5	5,4	20	6,3	9,5	5,2	·	5,2	14,0	6,2	15	-	5	-	·	8	3	·	4	·	2	·	7	8	-
IV	22	3,9	14	4,1	6	2,5	1	3,0	1	5,0	7	5,6	14,5	3,7	24,5	3,3	·	3,8	29,5	12,5	22	-	·	-	·	14	6	1	1	·	9	1	5	15	-
V	14	4,6	12,5	5,2	7,5	2,9	2	4,5	5,5	4,5	7,5	3,7	16,5	5,7	24,5	4,8	3	4,5	25,9	10,2	6	-	·	-	·	12	9	1	3	1	5	·	2	11	-
VI	11,5	2,6	8	3,4	3	1,3	7	2,9	1,5	6,0	5	3,6	2,9	4,2	2,5	4,7	·	3,9	11,3	3,1	6	-	·	-	2	10	4	·	3	·	4	·	6	4	-
VII	1,0	2,4	4,5	3,0	6	2,0	7,5	2,3	3	3,3	9,5	2,9	2,5,5	3,9	27	4,1	·	3,4	133,0	37,0	12	-	·	-	2	15	13	5	1	·	·	·	3	8	-
VIII	6	3,0	0,5	5,0	2	2,0	3	3,0	4,5	3,3	1,6	5,0	4,1	3,9	2,0	4,6	·	4,1	120,1	29,5	18	-	·	-	·	17	15	6	1	·	·	1,5	4	4	-
IX	2,5	5,0	0,5	3,0	·	·	·	·	1,0	3,4	3,0	5,4	19,5	3,4	27,5	5,4	·	4,7	100,6	15,0	22	·	·	·	2	18	17	3	4	·	3	·	5	10	-
X	1	4,0	·	·	2	4,0	·	·	6	5,7	3,5	5,6	4,1	4,7	8	5,2	·	5,1	19,4	5,0	1	·	·	·	·	9	7	·	4	·	1,5	·	1	16	-
XI	4	2,8	8	5,0	4	5,0	9,5	3,4	1,5,5	2,7	2,1	4,2	1,3,5	5,1	1,4,5	5,0	·	4,2	43,5	6,5	24	11	1	·	·	11	11	·	3	·	9	·	2	19	-
XII	1	6,0	6	9,5	2	6,0	1	5,0	5	2,2	2,2,5	5,9	3,5,5	4,8	2,0	4,6	·	5,2	34,6	10,0	30	23	10	1	·	7	6	1	3	·	11	·	1	21	-
Rok	9,3	3,4	6,2,5	4,0	4,2,5	3,3	5,2	3,0	7,6,5	3,9	2,1,0	4,7	3,2,4,5	4,8	2,3,1	4,8	3	4,6	59,7,7	37,0	12.VII	-	-	-	6	153	113	18	35	2	-	16	37	148	-

Sopot

$H_s = 2\ m$ $h_w = 13\ m$

I	0,5	3,0	2	11,5	4,5	11,3	5	5,2	13,5	3,4	20,5	5,5	3,1	6,9	12	8,1	4	6,2	14,4	3,8	5	20	6	·	·	9	6	·	9	4	5	·	·	21	-
II	3	5,5	2,5	4,0	1,5	2,3	2	3,8	15,5	4,7	20,5	4,3	25,5	5,2	6,5	5,5	7	4,3	46,1	6,0	9	7	·	·	·	18	13	·	2	1	7	·	·	21	-
III	11,5	7,2	4,5	5,7	6,5	8,5	12,5	10,5	12	7,8	5	5,3	15,5	7,9	15,5	7,3	10	7,0	20,4	6,0	20	18	2	·	·	8	6	·	14	5	2	·	5	8	-
IV	20,5	6,7	2,5	1,4	1	1,5	2,5	2,8	2	4,0	2,5	5,0	10,5	4,0	25,5	4,1	23	3,9	15,2	5,8	22	7	·	·	·	14	7	·	7	1	4	1	6	13	-
V	20,5	7,7	9	9,7	2	6,0	2,5	5,2	5	5,4	7	3,3	19,5	4,6	20,5	5,2	7	5,5	28,2	6,3	9	·	·	·	·	13	9	·	7	3	3	2	2	9	-
VI	8,5	5,4	2	5,0	1	4,0	3,5	3,9	5,5	3,9	7,5	3,9	2,8	4,8	2,3	4,5	11	4,0	14,1	3,8	5	·	·	·	1	9	6	·	1	·	3	·	3	8	-
VII	4,5	5,4	6	3,2	6,5	3,7	2	2,2	5,5	2,6	11,5	3,5	18,5	5,1	23,5	5,2	15	3,7	102,5	28,0	12	·	·	·	2	13	10	3	2	1	1	6	1	9	-
VIII	5,5	7,1	2,5	7,6	2	3,5	6,5	5,2	12	5,4	15,5	4,6	29,5	4,4	11,5	5,8	8	4,6	69,4	18,6	16	·	·	·	5	16	14	2	4	·	·	3	·	7	-
IX	1,5	11,3	1	10,0	1	4,0	6,5	4,6	14,5	5,8	20,5	6,0	24	5,9	14	8,7	7	5,9	85,6	15,3	27	·	·	·	2	17	11	4	7	4	1	·	·	13	-
X	1,5	6,3	·	·	0,5	5,0	3,5	4,7	19,5	5,5	30,5	5,0	23	5,5	7,5	6,2	7	5,0	9,1	2,0	1,1,9	·	·	·	·	10	2	·	3	·	4	·	1	14	-
XI	3,5	12,6	5,5	12,4	8,5	8,6	10,5	5,6	20	5,0	13	4,9	12,5	5,5	7,5	8,9	9	6,0	15,7	5,8	28	6	·	·	·	7	3	·	8	2	5	·	4	23	-
XII	3,5	11,6	4,5	11,2	3,5	8,6	7	5,8	17,5	4,9	24	5,7	22	5,7	8	5,9	3	6,0	37,2	10,5	31	16	5	1	·	9	7	1	6	3	2	·	3	17	-
Rok	8,4,5	7,5	42	6,8	3,8,5	5,6	64	5,0	14,2,5	4,9	178	4,8	2,5,9,5	5,5	1,7,5	6,3	111	5,2	4,5,7,9	28,0	12.VII	74	13	1	8	143	94	10	70	24	37	12	22	163	-

Gdańsk – Nowy Port

$\varphi = 54°25'$ $\lambda = 18°40'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.0	1.6	0.7	0.7	2.6	-1.4	10.1	6	-9.9	16	84	82	85	84	1.0	1.3	0.9	1.1	7.8	7.8	7.0	7.5
II	–	–	–	–	1.7	4.1	2.9	2.9	5.2	0.7	10.1	2	-6.5	25	86	79	85	83	1.0	1.7	1.1	1.3	8.7	7.9	7.5	8.0
III	–	–	–	–	0.5	4.8	2.2	2.4	6.0	-0.5	15.1	13,27	-6.3	17	76	64	78	73	1.5	3.4	1.6	2.2	5.5	6.4	4.6	5.5
IV	–	–	–	–	4.2	7.0	4.6	5.1	9.1	2.2	22.4	28	-3.7	15	85	77	84	82	1.3	2.8	1.4	1.8	6.5	6.2	5.4	6.0
V	–	–	–	–	8.5	11.3	8.8	9.4	13.1	6.1	22.5	16	-0.7	6	82	75	84	80	2.2	3.8	2.0	2.7	5.9	6.0	4.5	5.5
VI	–	–	–	–	14.4	18.2	14.1	15.2	20.1	10.7	28.5	18	6.7	8	80	67	83	77	3.4	7.3	2.7	4.5	5.1	5.7	4.9	5.2
VII	–	–	–	–	17.0	20.4	16.7	17.7	21.7	14.3	29.2	8	10.2	2,26	86	76	89	84	2.7	6.4	2.2	3.8	6.5	6.2	5.1	5.9
VIII	–	–	–	–	15.3	19.2	15.3	16.3	20.4	12.7	26.2	11	8.3	24	87	75	90	84	2.3	6.0	1.7	3.3	5.6	7.1	5.6	6.1
IX	–	–	–	–	10.2	14.7	10.7	11.6	15.7	8.3	27.7	9	2.7	26	89	73	90	84	1.3	5.2	1.4	2.6	7.1	7.1	5.8	6.7
X	–	–	–	–	7.6	12.4	9.0	9.5	13.2	6.6	19.7	10	2.0	17	92	72	87	84	0.9	4.2	1.5	2.2	7.3	7.3	5.7	6.8
XI	–	–	–	–	4.6	7.0	5.1	5.4	7.8	3.4	14.8	5	-4.4	22	87	78	88	84	1.0	2.1	1.0	1.4	8.7	8.6	7.8	8.4
XII	–	–	–	–	0.4	1.6	0.5	0.8	2.9	-1.5	7.9	5	-10.6	17	82	79	83	81	1.1	1.4	1.1	1.2	7.7	7.7	6.2	7.2
Rok	–	–	–	–	7.0	10.2	7.6	8.1	11.5	5.1	29.2	8.VII	-10.6	17.XII	85	75	86	82	1.6	3.8	1.6	2.3	6.9	7.0	5.8	6.6

Gdańsk – Wrzeszcz

$\varphi = 54°23'$ $\lambda = 18°36'$

I	1016.9	1031.6	998.7	1018.5	0.1	1.5	0.7	0.8	3.0	-1.8	10.8	6	-10.8	16	89	83	87	86	0.7	1.3	0.9	1.0	7.8	7.8	8.0	7.9
II	1007.5	1034.5	981.5	1009.1	1.9	4.1	3.0	3.0	5.7	0.6	10.6	2	-6.6	25	90	79	86	85	0.7	1.8	1.1	1.2	8.6	8.2	9.0	8.6
III	1016.6	1035.7	987.3	1018.2	0.5	4.8	2.4	2.5	6.7	-1.0	15.9	27	-6.8	17	80	64	78	74	1.3	3.6	1.7	2.2	6.2	6.6	4.3	5.7
IV	1017.6	1031.3	990.5	1019.2	4.3	7.8	4.5	5.3	10.1	1.7	23.0	28	-3.8	13	83	72	83	79	1.6	3.6	1.5	2.2	6.9	7.0	5.5	6.5
V	1015.4	1029.2	1001.8	1016.9	8.8	12.0	8.7	9.6	13.7	5.5	23.8	13	0.8	6	75	64	78	72	3.1	5.8	2.8	3.9	6.2	6.7	5.0	6.0
VI	1014.9	1030.7	1001.9	1016.4	14.8	18.2	14.4	15.4	20.9	10.3	29.5	11	6.3	8	71	56	75	67	5.1	9.6	4.1	6.3	5.5	6.6	5.0	5.7
VII	1009.8	1021.5	1000.0	1011.2	17.3	20.6	17.0	18.0	22.4	14.3	29.2	8,20	10.5	1	82	68	83	78	3.5	8.3	3.4	5.1	6.7	7.0	5.6	6.4
VIII	1010.8	1022.1	999.0	1012.2	15.5	19.4	15.5	16.5	20.4	13.0	26.2	11	8.4	24	82	65	85	77	3.2	8.3	2.7	4.7	5.7	7.5	6.1	6.4
IX	1008.4	1021.9	990.2	1009.9	10.4	14.5	10.8	11.6	15.7	8.1	27.7	9	3.4	26	86	67	84	79	1.7	6.1	2.1	3.3	7.7	8.2	5.7	7.2
X	1014.8	1028.2	1000.8	1016.3	7.9	12.3	9.2	9.6	13.2	6.5	20.5	10	2.3	2	89	69	83	80	1.2	4.5	2.0	2.6	7.3	7.8	5.5	6.9
XI	1018.8	1039.8	998.6	1020.3	4.7	6.8	5.2	5.5	7.7	3.0	14.7	5	-4.5	22	87	78	86	84	1.1	2.2	1.2	1.5	8.7	8.4	7.8	8.3
XII	1010.9	1029.1	966.9	1012.5	0.4	1.4	0.7	0.8	3.1	-1.9	8.3	8	-11.2	17	83	82	84	83	1.0	1.2	1.0	1.1	7.9	8.1	6.4	7.5
Rok	1013.5	1039.8	966.9	1015.0	7.2	10.3	7.7	8.2	11.9	4.9	29.5	11.VII	-11.2	17.XII	83	71	83	79	2.0	4.7	2.0	2.9	7.1	7.5	6.2	6.9

Gdańsk – Siedlice

$\varphi = 54°21'$ $\lambda = 18°36'$

I	–	–	–	–	-0.5	1.1	0.1	0.2	2.2	-2.2	9.7	6	-10.6	16	91	86	90	89	0.5	1.0	0.7	0.7	8.3	7.7	7.8	7.9
II	–	–	–	–	1.3	3.6	2.3	2.4	4.9	0.0	9.5	2	-7.1	25	95	83	92	90	0.4	1.4	0.6	0.8	9.0	8.4	8.9	8.8
III	–	–	–	–	0.0	4.5	1.8	2.0	6.0	-1.5	14.8	27	-7.2	17	84	67	81	77	1.0	3.2	1.4	1.9	6.5	6.5	4.5	5.8
IV	–	–	–	–	4.2	8.4	4.3	5.3	10.0	1.4	23.8	28	-5.0	15	85	72	86	81	1.5	3.9	1.3	2.2	7.1	7.3	5.5	6.6
V	–	–	–	–	8.3	12.3	8.2	9.2	13.6	5.1	23.5	13	-0.5	6	81	66	81	76	2.2	5.7	2.3	3.4	6.4	7.4	5.2	6.3
VI	–	–	–	–	14.4	18.6	13.5	15.0	20.5	9.6	29.3	18	5.1	21	75	59	81	72	4.3	9.4	2.9	5.5	5.6	7.2	5.6	6.1
VII	–	–	–	–	16.7	20.8	16.3	17.5	22.5	13.3	29.8	8	9.3	26	86	69	87	81	2.7	8.1	2.6	4.5	7.0	7.2	5.9	6.7
VIII	–	–	–	–	14.9	19.1	14.5	15.8	20.4	11.8	25.7	11	7.3	24	87	69	90	82	2.2	7.3	1.8	3.8	6.5	7.8	6.2	6.8
IX	–	–	–	–	9.7	14.2	9.9	10.9	15.6	7.0	27.3	9	1.7	26	91	72	90	84	1.1	5.2	1.3	2.5	8.7	8.5	5.9	7.7
X	–	–	–	–	7.1	12.0	8.6	9.1	12.8	5.6	19.4	10	1.0	17	94	73	88	85	0.6	3.9	1.4	2.0	7.6	8.4	5.3	7.1
XI	–	–	–	–	4.1	6.4	4.5	4.9	7.3	2.2	14.3	5	-6.0	22	91	81	89	87	0.7	1.8	0.9	1.1	9.3	8.8	8.1	8.7
XII	–	–	–	–	-0.3	1.0	0.1	0.2	2.4	-2.7	7.3	5,8	-12.5	17	86	82	86	85	0.8	1.1	0.8	0.9	8.1	8.2	6.7	7.7
Rok	–	–	–	–	6.7	10.2	7.0	7.7	11.5	4.1	29.8	8.VII	-12.5	17.XII	87	73	87	82	1.5	4.3	1.5	2.4	7.5	7.8	6.3	7.2

Kamienica Królewska

$\varphi = 54°23'$ $\lambda = 17°54'$

I	–	–	–	–	-0.9	-0.1	-0.7	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.6	8.5	8.7
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	4.0	9.3	4.2	5.4	10.3	0.5	22.9	28	-7.7	15	–	–	–	–	–	–	–	–	6.9	6.4	7.1	6.8
V	–	–	–	–	8.1	12.2	7.4	8.8	13.2	3.9	22.7	19	-2.4	27	–	–	–	–	–	–	–	–	6.2	6.7	6.3	6.4
VI	–	–	–	–	13.9	18.7	13.0	14.6	20.0	8.2	28.0	11	4.5	8	–	–	–	–	–	–	–	–	4.6	5.4	4.3	4.8
VII	–	–	–	–	16.4	20.8	15.6	17.1	21.8	11.6	29.2	4	4.0	4	–	–	–	–	–	–	–	–	7.6	6.0	5.7	6.4
VIII	–	–	–	–	14.3	18.2	13.8	15.0	19.5	10.9	25.2	12	6.9	9	–	–	–	–	–	–	–	–	6.7	6.9	6.8	6.8
IX	–	–	–	–	9.1	13.4	9.2	10.2	14.5	–	26.5	9	–	–	–	–	–	–	–	–	–	–	6.9	6.4	7.2	6.8
X	–	–	–	–	7.0	10.8	7.8	8.4	11.6	5.3	18.3	10	-0.1	2	–	–	–	–	–	–	–	–	8.1	7.3	7.4	7.6
XI	–	–	–	–	3.1	5.3	3.6	3.9	6.4	1.9	14.3	5	-8.9	30	–	–	–	–	–	–	–	–	7.9	7.3	7.5	7.6
XII	–	–	–	–	-1.4	-0.3	-0.9	-0.8	1.1	–	7.0	8	–	–	–	–	–	–	–	–	–	–	8.9	8.2	8.5	8.5
Rok	–	–	–	–	–	–	–	–	–	–	29.2	4.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Gdańsk – Nowy Port

$H_s = 8$ m $h_w = 13$ m **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, v m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T ≤ -10	≤ 0	≥ 10	≥ 25	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	Wiatr v ≥ 10	≥ 15	≡	≈	●	≋
I	·	·	25	6.2	6.5	4.8	7	2.6	15.5	2.2	17	4.1	31	7.4	7.5	5.1	6	4.6	87	20	25	22	7	·	·	9	4	·	–	–	–	·	1	16	5
II	4.5	2.3	3.5	3.0	2.5	1.0	7	2.5	21	2.9	14	2.6	17	5.0	7.5	6.3	7	3.2	37.6	5.5	23	10	·	·	·	17	15	·	–	–	–	·	·	18	4
III	14.5	4.8	6	2.6	14	3.5	13.5	4.0	15	3.4	3.5	8.4	15.5	4.3	7	5.9	4	4.0	142	52	20	19	1	·	·	6	3	·	–	–	–	·	5	7	3
IV	3.1	3.4	10.5	4.9	5	2.1	2	1.0	3.5	3.0	4.5	3.4	11	2.6	12.5	4.5	10	3.1	132	40	22	7	·	·	·	13	5	·	–	–	–	1	4	12	·
V	13.5	4.9	19.5	6.3	4	3.8	7	2.1	5	2.4	2	2.5	14.5	4.1	13.5	4.4	14	3.8	283	103	10	1	·	·	·	12	7	1	–	–	–	3	2	7	·
VI	13	3.6	7	2.9	6.5	1.5	5.5	2.8	4	2.8	4	3.6	22.5	4.9	13.5	3.5	14	3.0	106	51	22	·	·	·	3	7	3	·	–	–	–	·	5	5	·
VII	9	3.3	8	2.6	7	1.8	5	2.6	4	2.5	5	3.4	21	3.7	10	4.6	24	2.4	111.0	25.8	27	·	·	·	2	9	9	4	–	–	–	7	1	7	·
VIII	9	4.1	1	5.0	2	2.5	8	3.0	8	2.4	13.5	4.7	21.5	4.4	6	4.9	24	3.0	76.9	24.4	16	·	·	·	3	14	13	1	–	–	–	4	2	8	·
IX	0.5	9.0	0.5	1.0	3	1.0	5.5	1.5	1.5	4.2	17.5	4.5	17	4.7	19	6.6	12	4.0	62.9	19.8	23	·	·	·	2	16	12	1	–	–	–	·	·	7	·
X	·	·	·	·	·	·	5.5	2.1	15.5	3.3	2.6	4.3	27	5.0	9	5.2	10	3.8	7.2	1.6	1	·	·	·	·	10	3	·	–	–	–	·	·	9	·
XI	2	10.8	5.5	8.4	8	4.2	15.5	2.8	18.5	2.8	10	2.4	10.5	5.1	8	6.2	12	3.6	9.6	3.2	28	7	·	·	·	10	4	·	–	–	–	·	·	23	1
XII	2	9.0	4.5	11.2	5	3.2	10.5	2.8	17	2.7	22.5	4.3	20	3.9	5.5	5.2	6	3.9	20.1	4.4	31	16	6	1	·	11	7	·	–	–	–	·	2	14	6
Rok	9.9	4.6	68.5	4.5	63.5	2.4	9.2	2.5	14.2	2.9	13.9.5	4.0	228.5	4.6	119	5.2	143	3.5	4003	258	27.VII	82	14	1	10	134	85	7	–	–	–	15	22	133	19

Gdańsk – Wrzeszcz

$H_s = 13$ m $H_b = 12{,}4$ m $h_w = 11$ m

I	2	4.2	3	5.7	2	6.0	2.5	3.0	12	3.0	16	3.9	24.5	7.5	14	8.1	17	4.7	84	22	6	22	6	1	·	10	3	·	7	2	2	·	·	18	12
II	1.5	6.7	3	3.8	0.5	3.0	1.5	2.3	21	3.6	15	4.0	13	5.9	9.5	6.1	19	3.5	41.3	6.8	23	11	·	·	·	17	15	·	4	·	3	·	·	20	5
III	12	5.9	11.5	4.5	3	2.7	10.5	4.5	18	4.0	3.5	3.7	17.5	6.1	5	6.2	12	4.3	138	44	15	19	1	·	·	8	4	·	6	3	1	·	5	8	4
IV	14.5	4.9	3.0	4.9	1	3.0	1	1.0	2	3.0	5.5	4.6	7	4.6	7	5.0	22	3.6	17.5	4.5	22	8	·	·	·	12	6	·	3	·	2	2	4	11	1
V	12	5.2	24.5	6.0	3.5	4.4	0.5	3.0	7.5	2.9	6	4.8	12.5	6.0	11.5	4.3	15	4.3	33.2	8.3	10	·	·	·	·	14	10	·	4	·	2	3	3	9	·
VI	7	4.7	1.0	3.6	2	2.8	5	2.8	2.5	2.4	7.5	3.9	20	5.4	14	5.2	22	3.4	16.1	5.2	22	·	·	·	5	6	5	·	3	·	3	·	3	7	·
VII	4.5	5.4	11	3.9	6.5	3.4	2.5	2.8	4	2.9	8.5	3.9	12.5	5.3	16.5	5.7	27	3.2	88.1	19.6	12	·	·	·	4	10	9	4	2	·	2	6	·	8	·
VIII	5	4.9	5.5	6.5	1	6.5	1.5	3.7	9.5	3.3	13	5.0	25	5.1	8.5	5.8	24	3.7	74.9	19.3	16	·	·	·	1	13	10	4	2	·	·	4	·	9	·
IX	6	6.6	1	2.0	0.5	3.0	0.5	3.0	11.5	3.2	2.2	5.7	19.5	4.9	16	6.5	13	4.5	67.1	21.6	23	·	·	·	2	15	11	2	6	1	1	·	·	9	·
X	1	7.0	·	·	·	·	0.5	2.0	12	3.8	30.5	5.6	28.5	5.2	9.5	6.4	11	4.6	4.6	1.4	1.9	·	·	·	·	7	1	·	5	·	2	·	1	9	·
XI	1.5	11.7	4.5	10.3	7	4.9	4.5	3.7	14.5	3.8	15	3.6	9.5	5.1	9.5	6.3	24	3.7	92	39	28	8	·	·	·	8	3	·	6	1	1	·	2	22	1
XII	2.5	9.4	4	11.4	4	3.4	3.5	3.0	14.5	3.2	26.5	4.5	21	6.8	5	7.4	12	4.7	28.6	9.2	30	18	6	1	·	9	8	·	10	2	2	·	2	13	14
Rok	69.5	6.4	108	5.2	31	3.6	34	2.9	129	3.3	169	4.4	210.5	5.7	126	6.1	218	4.0	4028	246	23.IX	86	13	2	12	129	85	10	58	9	21	15	20	143	37

Gdańsk – Siedlice

$H_s = 7{,}2$ m $h_w = 10$ m

	1	4.5	1	6.0	7.5	4.9	4.5	2.1	8	3.4	14	6.0	26	7.6	12	6.2	19	4.7	10.2	2.6	6	25	6	1	·	12	4	·	7	1	3	·	·	20	14
II	2.5	2.6	2.5	2.0	1	1.5	1.5	1.7	19.5	2.8	17	3.2	16	6.8	7	4.6	17	3.2	48.5	6.8	18	16	·	·	·	18	14	·	2	·	4	·	·	20	4
III	13	4.0	7	4.8	6	4.8	9	6.3	16.5	5.3	2	4.8	16	6.7	9.5	5.1	14	4.5	19.3	5.7	15	19	2	·	·	7	5	·	4	1	2	·	5	9	5
IV	26.5	4.5	12.5	4.3	3.5	1.6	0.5	1.0	4	2.8	5	5.4	8.5	4.1	6.5	4.1	23	3.1	23.0	6.5	22	8	·	·	·	14	7	·	3	·	3	1	4	12	·
V	18	5.2	11.5	6.7	4.5	3.4	1.5	4.7	10.5	3.1	4.5	3.2	7	7.6	15.5	5.0	20	4.0	63.7	20.3	27	1	·	·	·	16	10	1	4	·	1	2	2	9	·
VI	14.5	4.7	3	3.7	3.5	3.7	2	5.5	6.5	3.5	7.5	5.1	13	5.7	16	4.8	24	3.5	16.8	6.1	22	·	·	·	4	6	5	·	2	·	2	·	3	9	·
VII	8.5	3.2	8	3.1	3.5	2.7	3	5.5	8	2.9	6	4.2	12.5	4.7	15.5	6.0	28	3.0	99.1	22.0	12	·	·	·	3	14	12	2	1	·	·	7	2	11	·
VI	7	3.5	3	4.7	·	·	2.5	3.4	8	3.2	15.5	5.3	22.5	4.6	8.5	4.8	26	3.2	107.1	24.1	7	·	·	·	1	17	12	4	2	·	·	5	1	14	·
IX	2.5	3.6	·	·	1	2.0	0.5	4.0	8.5	4.5	15	5.4	16.5	4.9	21	6.0	25	3.8	86.4	38.0	23	·	·	·	2	21	12	2	4	·	2	·	·	12	·
X	1.5	6.5	·	·	·	·	1	2.0	14.5	3.3	30.5	5.3	20.5	4.5	15	4.9	10	4.2	9.2	2.0	1	·	·	·	·	12	4	·	5	·	1	·	2	12	·
XI	2	10.0	5	7.4	9.5	3.1	4.5	3.2	11.5	3.5	9	3.1	8.5	6.0	6	6.3	34	2.9	15.1	5.6	28	9	1	·	·	10	4	·	3	·	2	·	1	24	1
XII	7	6.4	1.5	9.3	4.5	4.4	2.5	4.6	14.5	4.1	11.5	5.6	26	6.7	7.5	6.9	18	4.7	32.4	6.1	31	23	8	3	·	11	8	·	5	1	2	·	3	17	14
Rok	10.4	4.9	55	4.3	44.5	2.7	33	3.7	130	3.5	137.5	4.7	193	5.8	140	5.4	258	3.7	530.8	38.0	23.IX	101	17	4	10	158	97	9	42	3	22	15	23	169	38

Kamienica Królewska

$H_s = 16.0$ m $h_w = 11$ m

I	4	4.5	5	4.3	5	3.4	2	3.5	3.5	4.6	5	4.6	2.7	6.3	4	4.5	6	5.2	41.3	10.5	5	–	–	–	·	8	8	1	6	1	–	–	·	21	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20.7	10.4	16	–	–	–	·	8	5	1	–	–	–	–	–	–	–
IV	40.5	3.5	1.5	3.7	5	2.0	9	3.3	9	4.9	3	2.3	17	3.8	5	2.8	·	3.5	62.6	17.3	28	12	·	·	·	15	11	2	·	–	1	4	15	–	
V	27	3.6	1.9	3.8	6	3.8	2	5.0	13	5.2	4.5	4.4	15.5	5.2	4	2.0	2	4.1	33.0	12.2	9	4	·	·	·	7	6	1	3	·	–	·	1	10	–
V	18	2.8	4	1.8	3	3.0	6	3.7	14	2.9	6	2.7	22	3.9	16	4.2	1	3.5	47.8	30.5	9	·	·	·	3	9	8	1	1	1	–	1	7	4	–
VII	13	3.0	·	·	2	3.5	7	7.6	7	3.4	4	3.5	30	3.4	26	2.8	4	3.1	128.5	32.2	46	·	·	·	5	13	13	5	·	·	–	3	·	6	–
VIII	10	2.3	1	1.0	4	5.0	8	4.9	30	3.9	8	4.8	14	4.2	13	3.0	5	3.6	122.7	31.5	46	·	·	·	1	17	16	4	·	·	·	·	·	9	–
IX	8	4.2	·	·	1	3.0	·	·	2.6	4.4	22	5.0	16	3.4	15	3.2	2	4.0	107.4	18.0	26	–	·	·	2	19	17	3	4	·	·	·	1	11	–
X	7	5.0	·	·	·	·	3.5	4.8	22	6.0	19	3.8	19	3.8	8	3.1	2	4.6	39.4	5.5	5	1	·	·	·	16	15	·	·	·	–	·	·	15	–
XI	6	4.3	2	2.5	8	3.5	8	3.0	4.1	4.4	2	4.5	15	6.5	7	5.3	1	4.5	64.4	18.0	24	11	1	·	·	6	6	3	3	1	–	·	2	17	–
XII	5	5.2	1	2.0	7	5.7	5	3.8	24	4.4	11	5.2	35	3.9	3	2.3	2	4.2	53.5	11.2	30	–	9	–	·	9	9	2	2	1	–	·	·	24	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32.2	16.VII	–	–	–	11	–	–	–	–	–	–	–	–	–	–

Krynica Morska

$\varphi = 54°23'$ $\lambda = 19°27'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.1	0.5	-0.2	-0.2	1.8	-3.2	9.1	9	-11.2	16	86	87	87	87	0.7	0.8	0.7	0.7	7.2	8.3	7.9	7.8
II	–	–	–	–	1.7	3.3	2.4	2.4	4.4	-0.1	8.3	2	-4.7	25	91	88	91	90	0.6	1.0	0.7	0.8	8.4	8.6	7.1	8.0
III	–	–	–	–	0.8	4.6	2.5	2.6	6.0	-1.2	16.2	31	-7.8	17	–	–	–	–	–	–	–	–	5.2	5.4	4.9	5.2
IV	–	–	–	–	4.8	8.0	5.3	5.8	10.1	2.1	23.2	28	-3.6	13	–	–	–	–	–	–	–	–	5.7	6.2	6.2	6.0
V	–	–	–	–	9.0	11.9	8.6	9.5	13.4	5.4	23.2	19	1.7	6	81	74	84	80	2.3	4.0	1.9	2.7	6.3	5.7	5.6	5.9
VI	–	–	–	–	14.3	17.7	13.8	14.9	20.0	10.5	27.4	18	6.6	21	79	68	81	76	3.6	7.1	3.2	4.6	5.4	5.9	5.0	5.4
VII	–	–	–	–	17.4	20.4	17.3	18.1	21.9	14.3	28.6	8	9.1	1	85	74	83	81	3.0	6.9	3.4	4.4	7.2	6.5	5.9	6.5
VIII	–	–	–	–	15.3	19.4	16.0	16.7	20.5	13.2	25.0	12	9.1	23	87	72	84	81	2.4	6.4	3.0	3.9	6.3	6.8	4.1	5.7
IX	–	–	–	–	11.4	14.6	12.0	12.5	15.5	9.0	24.7	9	3.4	27	84	72	82	79	2.1	5.0	2.5	3.2	7.6	7.1	6.7	7.1
X	–	–	–	–	7.8	11.2	9.3	9.4	12.4	6.4	16.8	10	3.3	5,25	89	79	84	84	1.2	2.8	1.8	1.9	7.3	7.1	4.7	6.4
XI	–	–	–	–	5.2	6.3	5.5	5.6	7.6	3.3	13.7	5	-4.9	29	83	82	83	83	1.4	1.8	1.4	1.5	8.1	8.4	7.4	8.0
XII	–	–	–	–	-0.3	0.4	0.0	0.0	1.9	-2.7	7.8	5	-10.2	19	–	–	–	–	–	–	–	–	7.3	8.3	6.8	7.5
Rok	–	–	–	–	7.2	9.9	7.7	8.1	11.3	4.8	28.6	8.VII	-11.2	16.1	–	–	–	–	–	–	–	–	6.8	7.0	6.0	6.6

Ostrowo

$\varphi = 54°23'$ $\lambda = 22°55'$

I	–	–	–	–	-2.7	-1.6	-2.0	-2.1	–	-4.5	–	–	-16.3	15	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-0.4	1.3	0.1	0.3	–	-1.6	–	–	-9.0	28	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	-2.8	1.9	-0.8	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	4.1	10.4	6.3	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	8.8	13.0	9.0	10.0	15.0	5.0	25.0	20	-1.3	2,6	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	13.3	18.1	14.0	14.8	19.6	9.0	27.0	11	2.6	21	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	15.7	20.4	16.5	17.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	14.4	18.5	14.3	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.1	12.8	9.4	10.2	–	6.5	–	–	1.6?	22?	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	6.2	9.6	7.3	7.6	–	4.3	–	–	0.6	3	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	2.3	3.8	2.6	2.8	–	0.5	–	–	-11.3	29	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.7	-1.9	-2.6	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	5.4	8.9	6.2	6.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Frombork

$\varphi = 54°22'$ $\lambda = 19°41'$

I	–	–	–	–	-0.7	0.4	-0.2	-0.2	2.0	-2.5	9.2	6	-12.0	16	89	84	87	86	0.6	1.0	0.8	0.8	8.2	7.7	6.9	7.6
II	–	–	–	–	1.6	3.5	2.6	2.6	4.9	0.4	9.7	14	-5.3	25	93	81	89	88	0.5	1.6	0.9	1.0	8.4	7.6	7.2	7.7
III	–	–	–	–	0.1	3.5	2.3	2.0	5.7	-1.2	17.6	31	-9.9	17	80	70	77	76	1.3	2.8	1.9	2.0	5.1	6.2	4.7	5.3
IV	–	–	–	–	4.5	7.5	5.9	5.9	9.7	2.1	24.0	28	-4.9	13	84	75	82	80	1.4	3.1	1.9	2.1	6.2	6.2	6.8	6.4
V	–	–	–	–	8.7	10.9	9.4	9.6	13.3	5.6	23.2	19	-0.3	6	82	74	78	78	2.2	3.8	2.8	2.9	6.6	6.4	5.6	6.2
VI	–	–	–	–	14.2	16.1	14.9	15.2	18.7	11.0	28.1	11	7.1	21	81	72	81	78	3.1	5.7	3.3	4.0	5.3	5.8	5.1	5.4
VII	–	–	–	–	16.9	19.8	17.8	18.1	21.5	14.6	28.3	4	10.5	4	88	78	85	84	2.4	5.6	3.1	3.7	6.5	6.4	6.1	6.3
VIII	–	–	–	–	15.2	18.5	16.3	16.6	19.7	13.2	25.3	11	8.4	24	87	72	83	81	2.3	6.1	3.2	3.9	6.3	6.9	6.0	6.4
IX	–	–	–	–	14.2	14.1	11.7	12.2	15.3	8.8	26.6	9	2.4	25	88	75	86	83	1.6	4.7	2.0	2.8	7.7	7.5	6.7	7.3
X	–	–	–	–	7.8	11.0	9.4	9.4	12.2	6.8	19.2	10	3.7	17	91	80	86	86	1.0	2.7	1.7	1.8	7.7	8.3	6.3	7.4
XI	–	–	–	–	4.3	6.2	5.0	5.1	7.6	3.1	14.4	6	-5.8	30	89	82	87	86	0.9	1.8	1.1	1.3	8.8	8.4	7.8	8.3
XII	–	–	–	–	-0.6	0.7	0.0	0.0	2.3	-2.5	6.8	8,9	-10.5	19	87	83	90	87	0.8	1.1	0.8	0.9	7.6	8.2	7.0	7.6
Rok	–	–	–	–	6.9	9.4	7.9	8.0	11.1	5.0	28.3	4.VII	-12.0	16.1	87	77	84	83	1.5	3.3	2.0	2.3	7.0	7.1	6.4	6.8

Czarna Dąbrówka

$\varphi = 54°21'$ $\lambda = 17°34'$

I	–	–	–	–	-0.5	0.7	-0.3	-0.1	1.6	-2.6	10.2	6	-12.6	16	92	89	92	91	0.5	0.7	0.5	0.6	9.3	8.8	8.7	8.9
II	–	–	–	–	1.0	3.9	1.9	2.2	4.6	-0.5	10.2	2	-8.0	25	93	82	92	89	0.5	1.5	0.6	0.9	8.7	7.9	8.5	8.4
III	–	–	–	–	-0.1	5.3	1.5	2.0	6.2	-1.9	16.0	31	-8.8	17	85	70	88	81	0.9	3.1	0.9	1.6	6.9	5.9	5.6	6.1
IV	–	–	–	–	3.8	9.2	3.7	5.1	9.9	0.3	22.4	28	-6.8	15	–	–	–	–	–	–	–	–	7.1	7.6	6.6	7.1
V	–	–	–	–	8.0	12.6	7.2	8.8	–	3.4	–	–	-2.1	27	–	–	–	–	–	–	–	–	7.2	7.9	5.7	6.9
VI	–	–	–	–	13.3	19.1	13.1	14.8	–	8.0	–	–	3.2	15	–	–	–	–	–	–	–	–	6.0	6.5	5.6	6.0
VII	–	–	–	–	15.4	20.9	15.8	17.2	22.0	11.8	29.0	4	7.7	7	88	66	88	81	2.4	9.4	2.4	4.7	7.7	7.6	6.2	7.2
VIII	–	–	–	–	14.6	18.5	14.1	15.3	–	11.0	–	–	6.6	9	90	72	92	85	1.7	6.2	1.2	3.0	7.4	7.5	7.3	7.4
IX	–	–	–	–	9.7	13.7	9.9	10.8	–	6.7	–	–	-0.5	26,27	93	73	89	85	0.9	4.9	1.4	2.4	8.6	8.4	7.7	8.2
X	–	–	–	–	7.4	11.2	8.6	9.0	–	5.4	–	–	0.8	2	95	79	89	88	0.5	3.0	1.2	1.6	8.8	7.6	7.3	7.9
XI	–	–	–	–	3.6	5.9	4.1	4.4	–	1.8	–	–	-9.8	30	92	83	91	89	0.7	1.7	0.8	1.1	8.9	8.9	8.3	8.7
XII	–	–	–	–	-1.0	0.4	-0.3	-0.3	–	-3.2	–	–	-13.5	18	–	–	–	–	–	–	–	–	8.8	8.1	8.8	8.6
Rok	–	–	–	–	6.4	10.1	6.6	7.4	–	3.4	–	–	-13.5	18.XII	–	–	–	–	–	–	–	–	8.0	7.7	7.2	7.6

Krynica Morska

$H_s = 4\,m$ $h_w = 17\,m$ 1957

MIESIĄC	ROZKŁAD WIATRU °D.YmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0	Max<0	Min<-10	Max≥25	Opad R 0.1	R 1.0	R 10.0	R 100	Wiatr v ≥10	v ≥15	≡	≋	◔	●	⊠
I	1	5.0	·	·	1.1	5.7	8.5	2.0	4.5	4.6	3.8	6.7	18.5	6.4	7.5	9.5	4	5.9	15.0	4.9	12	25	8	2	·	7	4	·	8	1	4	·	3	20	24
II	1.5	3.3	1.5	2.0	6.5	2.8	8	2.6	1.0	5.4	3.4.5	4.9	1.2	5.2	6	4.3	4	4.2	28.2	4.1	18	11	·	·	·	1.9	1.1	·	2	·	2	·	1	1.6	2
III	2.5	5.6	6.5	4.2	1.9	4.8	1.3	7.8	8.5	6.9	1.6.5	6.7	1.5.5	8.6	7.5	5.8	4	6.2	15.1	4.3	15	19	2	·	·	7	5	·	9	4	·	·	1.0	1.0	3
IV	1.4	3.0	1.5.5	4.5	9.5	3.1	3.5	2.6	0.5	2.0	1.3.5	7.1	4.5	4.4	1.7	4.7	1.2	3.9	1.3.6	3.9	28	7	·	·	·	1.2	5	·	2	1	4	2	6	1.2	1
V	1.1	3.8	1.6.5	4.1	7.5	3.7	7.5	2.7	·	·	9	3.8	7	1.1.2	2.4.5	4.8	1.0	4.2	1.5.9	4.6	11	·	·	·	·	1.2	6	·	2	2	2	2	4	1.2	·
VI	1.2	3.2	7	4.1	3.5	2.0	8	3.9	2.5	2.6	1.8	5.5	1.0.5	4.1	1.8.5	3.4	1.0	3.5	3.5.2	9.7	10	·	·	·	4	1.0	7	·	·	·	1	1	7	8	·
VII	2.5	2.4	1.0	2.8	1.3	2.6	8.5	2.4	2.5	1.8	1.8.5	4.2	1.6.5	4.3	1.5.5	3.1	6	3.1	8.7.1	3.1.4	2	·	·	·	7	1.1	9	3	·	·	1	4	3	1.2	·
VIII	3.5	3.7	1	1.5	2	1.5	6.5	4.9	2	4.2	3.5.5	5.9	1.8.5	5.2	1.4	4.6	1.0	4.6	1.1.1.6	2.9.2	17	·	·	·	·	1.9	1.0	4	2	·	1	3	4	8	·
IX	2	3.5	0.5	3.0	0.5	4.0	1.5	2.0	6	7.1	3.0	6.6	2.0.5	6.0	2.1	6.4	8	5.7	1.2.5.6	4.8.7	28	·	·	·	·	2.1	1.8	4	9	4	1	·	·	1.5	·
X	·	·	·	·	·	·	0.5	5.0	8	4.1	4.4.5	5.4	2.3.5	5.3	7.5	6.5	9	4.9	1.7.1	5.2	1	·	·	·	·	8	6	·	4	2	1	·	3	8	·
XI	·	·	3	1.1.3	1.0	3.6	1.8	3.6	4	1.5	2.6.5	4.0	1.8.5	5.1	2	7.5	8	4.0	1.9.6	1.4.0	28	7	1	·	·	5	3	1	2	1	1	·	1	1.9	·
XII	2	9.5	3.5	1.0.0	4.5	5.9	2.5	8.2	6	6.1	4.3	7.0	2.3.5	7.3	7	6.9	1	7.1	2.8.2	7.3	31	2.6	7	1	·	6	5	·	9	5	·	·	3	1.7	6
Rok	5.2	3.6	6.5	4.0	8.7	3.3	8.6	4.0	5.4.5	3.9	3.2.7.5	5.6	1.8.9	6.1	1.4.8	5.6	8.6	4.8	5.1.2.2	3.1.4	2.VII	9.5	1.8	3	1.1	1.3.7	8.9	1.2	4.9	2.0	·	1.2	4.5	1.5.7	3.6

Ostojów

$H_s = 2.40\,m$ $h_w = 11\,m$

I	·	·	1	2.0	4.5	4.0	1.2.5	2.4	6.5	2.6	2.0.5	2.6	3.8.5	3.6	9.5	4.3	·	3.2	2.9.7	5.5	6	2.7	-	4	-	1.5	1.1	·	·	·	-	-	-	-	-
II	5	2.2	·	·	6	1.7	1	1.0	3	1.3	2.3	2.3	2.7	3.3	1.7	1.9	2	2.4	3.6.1	5.5	1.5	2.1	-	·	-	1.6	1.1	·	·	·	-	-	-	-	-
III	1.2	2.8	3	2.3	1.1	2.4	7	3.3	4	4.5	1.0	2.1	3.1	3.2	8	3.8	7	2.8	1.3.4	4.0	2.0	-	-	-	-	8	6	·	·	·	-	-	-	-	-
IV	4	3.0	·	·	5	1.2	1.2	1.9	6	1.8	2.1	1.9	2.8	1.8	9	3.1	5	1.9	3.3.7	1.3.2	3.0	-	-	-	-	7	6	1	·	·	-	-	-	-	-
V	2.2.5	3.2	6	4.3	7	2.6	4	2.2	7	1.4	1.3.5	1.7	1.7.5	4.4	8.5	4.8	7	3.0	4.7.8	3.4.1	2.3	2	·	·	·	1.1	5	1	2	·	-	-	-	-	-
VI	4	2.5	1	1.0	·	·	1	1.0	6.5	1.0	1.9.5	1.7	3.5	2.5	1.9	2.3	4	2.0	4.8.6	1.3.0	2.5	·	·	·	2	1.2	8	·	1	·	-	-	-	-	-
VII	3	1.3	0.5	3.0	4	2.4	5.5	3.3	7	1.6	1.7.5	1.2	3.8	2.3	5.5	2.0	1.2	1.8	1.1.9.9	4.1.2	1.9	-	-	-	-	1.3	9	3	·	·	-	-	-	-	-
VIII	2.5	3.2	·	·	3	2.3	2	2.0	1.1	1.5	2.9	1.9	3.1	2.7	1.1.5	2.4	3	2.2	1.6.4.5	4.1.1	1.8	-	-	-	-	2.4	1.7	7	·	·	-	-	-	-	-
IX	0.5	2.0	·	·	·	·	·	·	1.0.5	1.6	2.6	1.8	4.6	2.7	7	1.9	·	2.2	1.8.4.0	5.0.2	1.8	·	·	·	-	2.1	1.7	5	1	·	-	-	-	-	-
X	1	1.0	1	3.0	1	1.0	·	·	5	2.0	4.5	1.7	3.4.5	2.6	2.5	2.0	3	2.0	3.3.9	8.0	4	·	·	·	-	1.3	6	·	·	·	-	-	-	-	-
XI	8	6.4	2	3.5	3	2.7	1.5	3.1	9	2.0	1.4	1.9	2.7	1.9	8	2.5	4	2.5	4.4.8	1.6.0	2.6	1.4	-	2	-	1.3	8	1	1	·	-	-	-	-	-
XII	5	2.4	3	2.3	2	2.0	6.5	1.9	1.2	2.0	3.5	2.2	2.6.5	3.2	1	3.0	2	2.4	3.7.2	1.1.5	1.4	-	-	-	-	1.0	1.0	1	·	·	-	-	-	-	-
Rok	6.7.5	2.5	1.7.5	1.8	4.6.5	1.9	6.6.5	1.8	8.7.5	1.9	2.7.4	1.9	3.8.0	2.8	1.0.6.5	2.8	4.9	2.4	7.9.3.6	5.0.2	1.8.XI	-	-	-	-	1.6.3	1.1.4	1.9	5	·	-	-	-	-	-

Frombork

$H_s = 2\,m$ $h_w = 14\,m$

I	·	·	6	7.2	8	3.1	1.4.5	3.3	1.4.5	4.0	2.9	8.8	1.5.5	1.0	2.5	7.0	3	6.5	1.6.2	5.9	5	2.3	6	3	·	9	4	·	1.1	2	-	·	3	1.8	6
II	4	5.7	4	2.8	6	2.0	1.4.5	3.5	2.0.5	3.7	2.2.5	7.9	7.5	7.4	1	1.4	4	5.0	4.1.5	7.2	18	1.0	1	·	·	1.5	1.2	·	5	·	-	·	·	1.1	1
III	1.0	5.3	4	3.8	1.8	4.4	1.4	4.8	8	4.9	1.0	7.3	1.3	7.3	6	1.4	1.0	5.4	1.8.0	7.5	20	1.6	2	·	·	9	3	·	8	3	-	·	8	8	1
IV	2.1.5	5.8	5	5.4	4	4.5	9	2.5	8	5.0	6	6.6	1.1	5.5	1.0.5	5.4	1.5	4.3	1.2.1	4.0	20	7	·	·	·	1.1	4	·	4	·	-	3	5	1.1	1
V	1.6	7.4	7.5	5.9	9	2.7	9	3.3	4	2.0	7	6.8	1.3	6.2	2.2.5	5.5	5	5.1	2.4.5	6.4	19	2	·	·	·	1.1	8	·	7	·	-	3	4	1.2	·
VI	1.4.5	4.9	6	3.5	1.3	2.2	5	2.6	5	2.4	1.3	6.0	1.8	6.6	8.5	5.0	7	4.3	4.8.0	1.7.5	22	·	·	·	3	9	8	1	4	·	-	3	5	7	·
VII	6	4.3	3	3.0	1.9	2.7	7.5	3.5	8.5	3.1	1.1	6.6	1.7	8.5	1.4	4.6	7	4.5	8.0.5	1.8.7	2	·	·	·	5	1.0	7	4	4	1	-	8	3	9	·
VIII	5.5	3.7	3	2.0	4	2.8	1.2	3.2	1.5.5	3.7	2.5	7.6	1.2	7.2	1.2	5.3	4	5.1	8.6.8	1.9.1	16	·	·	·	1	1.7	1.3	4	1.0	2	-	5	1	1.2	·
IX	1	6.0	·	·	2	3.5	1.3.5	3.3	1.2	4.7	3.1.5	7.1	1.0.5	1.1.8	1.5.5	1.1.1	4	7.0	1.1.7.5	1.8.3	30	·	·	·	2	1.9	1.8	4	1.5	6	-	2	·	1.1	·
X	1	2.0	·	·	·	·	1.1	3.6	2.3.5	5.5	4.6.5	6.9	7	7.0	2	5.0	2	5.9	2.9.9	1.5.1	1	·	·	·	·	1.0	5	1	1.0	1	-	·	1	1.2	·
XI	2	1.1.5	9	7.2	1.1	2.6	1.3.5	3.1	1.6.5	3.8	1.4.5	6.8	4.5	9.8	2	1.1.0	1.7	4.3	1.2.9	4.5	28	7	1	·	·	8	4	·	6	3	-	·	1	2.0	·
XII	1.5	9.0	3.5	6.1	8	3.5	6	1.4	2.8.5	3.6	2.9	8.2	9	1.8	1.5	1.5	6	5.7	1.3.5	7.6	8	2.2	6	3	·	1.3	2	·	8	2	-	·	5	1.9	1
Rok	8.3	5.5	5.1	3.9	1.0.2	2.8	1.2.9.5	3.2	1.6.4.5	3.9	2.4.5	7.2	1.3.8	6.7	9.8	5.4	8.4	5.3	5.0.1.2	1.9.1	16.VIII	8.7	1.6	6	1.1	1.4.1	8.8	1.4	9.2	2.0	-	2.4	3.6	1.5.0	1.0

Czarna Dąbrówka

$H_s = 1.20\,m$ $h_w = 12\,m$

I	·	·	5	1.4	6	2.8	3	2.0	2.5	3.5	1.7	4.2	3.0	8.8	7	8.7	·	5.5	2.3.6	8.9	5	2.4	1.1	2	·	1.6	6	·	6	5	-	·	·	2.6	-
II	2	3.0	·	·	9	1.8	1	5.0	3.0	3.7	1.5	4.4	2.2	6.2	4	2.5	1	4.2	4.5.1	1.1.5	9	1.4	·	·	·	1.9	1.3	1	3	2	-	·	·	1.9	-
III	1.2	3.2	2	1.5	9	5.4	1.8	8.1	9	4.4	7	3.1	2.6	6.8	9	5.8	1	5.7	1.9.3	9.0	1.5	2.0	1	·	·	7	4	·	7	4	-	·	2	1.0	-
IV	2.4	3.8	2	2.0	1.0	3.1	5	2.4	4	2.8	3	3.7	1.8	4.1	2.4	2.8	·	3.3	4.8.1	1.6.2	2.8	1.4	·	·	·	1.6	5	2	·	·	-	2	4	1.3	-
V	2.5	3.0	4	3.2	3	4.3	1	5.0	7	4.8	3	2.0	2.7	4.2	2.3	4.3	·	3.8	5.6.5	1.6.7	9	3	·	·	-	1.4	1.0	1	1	1	-	5	2	1.1	-
VI	1.3	1.8	5	2.4	4	2.2	6	5.3	5	4.6	4	3.8	3.7	4.6	1.6	4.4	·	3.9	2.8.9	1.5.0	9	·	·	·	-	1.0	7	1	4	1	-	1	5	1.1	-
VII	9	2.7	2	1.5	3	1.3	4	2.8	1.4	3.1	5	3.8	4.2	3.8	1.4	3.5	·	3.5	1.3.5.5	3.3.0	1.6	·	·	·	-	2.4	1.6	3	·	·	-	5	·	1.1	-
VIII	7	2.6	·	·	1	4.0	2	2.5	1.7	3.6	1.7	5.5	3.8	3.8	1.0	4.3	1	3.9	1.0.8.2	2.1.2	1.6	·	·	·	-	2.2	1.2	6	1	·	-	3	·	1.3	-
IX	1	5.0	·	·	·	·	2	2.0	1.6	4.1	2.8	5.0	3.0	3.7	1.2	6.6	1	4.5	9.3.0	9.6	2.7,3.0	2	·	·	-	2.2	1.9	·	7	·	-	·	·	1.5	-
X	·	·	·	·	·	·	1	9.0	1.9	4.3	2.6	4.8	3.8	5.0	9	4.7	·	4.8	2.2.2	4.7	5	·	·	·	-	1.8	7	·	4	·	-	·	·	1.5	-
XI	5	3.6	2	1.5	1.7	3.2	9	5.4	1.7	3.5	2.3	3.6	1.1	7.6	6	8.2	·	4.4	5.0.2	1.0.5	2.9	1.2	·	·	-	1.0	8	2	4	·	-	·	1	2.2	-
XII	1	1.0	4	7.0	1.0	2.6	2	4.0	1.6	5.2	2.4	5.2	2.5	7.3	1.1	6.4	·	5.7	7.6.0	1.2.9	8	2.4	·	4	·	1.7	1.5	1	8	2	-	·	·	2.1	-
Rok	9.9	2.5	2.6	1.7	7.2	2.6	5.4	4.5	1.7.9	4.0	1.7.2	4.1	3.4.4	5.5	1.4.5	5.2	4	4.4	7.0.6.8	3.3.0	1.6.VII	1.1.3	·	6	-	1.9.5	1.2.2	1.7	4.5	1.5	-	1.6	1.4	1.8.7	-

Świbno – Ujście Wisły

$\varphi = 54°21'$ $\lambda = 18°56'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	0.3	3.6	2.2	2.1	6.2	-0.9	14.6	27	-6.4	17	82	71	83	79	1.1	2.5	1.3	1.6	6.0	6.0	5.4	5.9
IV	–	–	–	–	4.2	7.1	5.1	5.4	8.6	2.5	23.5	28	-4.8	13	88	75	86	83	1.0	3.1	1.3	1.8	6.7	6.8	6.5	6.6
V	–	–	–	–	8.6	11.2	9.4	9.6	12.9	6.5	23.7	13	-0.5	6	84	73	83	80	1.9	4.2	2.3	2.8	7.0	6.4	5.2	6.2
VI	–	–	–	–	14.3	17.1	15.0	15.4	19.3	10.4	27.7	18	5.0	1	81	70	80	77	3.2	6.4	3.4	4.3	5.8	6.5	5.6	6.0
VII	–	–	–	–	16.9	19.8	17.6	18.0	21.1	14.3	27.9	20	6.5	26	89	80	89	86	2.2	5.1	2.2	3.0	7.0	7.2	6.2	6.8
VIII	–	–	–	–	15.2	19.0	16.1	16.6	20.2	13.1	26.2	11	7.8	30	90	74	88	84	1.9	6.8	2.3	3.7	5.7	6.9	5.6	6.1
IX	–	–	–	–	10.6	14.4	11.9	12.2	15.7	8.0	27.2	9	2.9	8	91	76	86	84	1.1	4.5	1.9	2.5	7.7	7.9	6.5	7.4
X	–	–	–	–	7.2	11.7	9.1	9.3	12.5	5.9	18.5	19	1.4	15	95	76	89	87	0.5	3.3	1.3	1.7	7.3	7.2	6.1	6.9
XI	–	–	–	–	4.6	6.2	5.1	5.2	7.5	3.1	13.9	5	-4.4	30	87	83	86	85	1.0	1.6	1.2	1.3	8.6	8.5	7.8	8.3
XII	–	–	–	–	-0.3	0.7	-0.1	0.0	2.2	-2.3	9.2	5	-12.3	18	88	87	88	88	0.7	0.8	0.7	0.7	8.1	8.4	7.1	7.9
Rok	–	–	–	–	–	–	–	–	–	–	27.9	20.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Świbno

$\varphi = 54°20'$ $\lambda = 18°56'$

I	–	–	–	–	-0.9	0.9	-0.2	-0.1	2.0	-3.0	10.3	6	-11.3	16	90	88	91	90	0.5	0.8	0.6	0.6	8.3	8.3	8.0	8.2
II	–	–	–	–	1.4	3.6	2.3	2.4	4.8	0.0	8.9	15	-3.8	25	95	88	92	92	0.4	1.0	0.6	0.7	9.0	8.5	8.9	8.8
III	–	–	–	–	0.2	4.4	2.1	2.2	6.0	-4.4	15.0	27	-7.1	17	81	70	82	78	1.1	2.8	1.3	1.7	6.1	6.8	5.9	6.3
IV	–	–	–	–	4.4	7.6	5.1	5.6	9.4	2.2	23.9	28	-5.3	13	86	76	85	82	1.2	3.1	1.5	1.9	6.6	6.5	7.0	6.7
V	–	–	–	–	8.9	11.6	9.3	9.8	13.4	6.2	23.6	13	-1.2	6	80	68	80	76	2.4	4.9	2.6	3.3	6.6	6.3	5.9	6.3
VI	–	–	–	–	14.5	17.7	14.7	15.4	19.9	10.3	28.0	18	5.8	21	79	64	80	74	3.6	7.7	3.4	4.9	5.7	6.4	5.5	5.9
VII	–	–	–	–	17.1	20.3	17.2	18.0	21.6	13.8	28.5	4	9.2	26	88	75	86	83	2.5	6.4	2.9	3.9	7.2	7.5	6.9	7.2
VIII	–	–	–	–	15.1	19.3	15.5	16.4	20.3	11.9	25.8	11	6.8	24	90	69	88	82	1.9	7.4	2.2	3.8	6.3	7.1	6.4	6.6
IX	–	–	–	–	10.3	14.5	11.0	11.7	15.6	7.5	26.8	9	1.2	27	91	73	88	84	1.1	5.1	1.6	2.6	7.5	8.2	7.3	7.7
X	–	–	–	–	7.1	12.2	8.5	9.1	12.8	5.1	18.6	19	0.7	15	93	73	89	85	0.7	3.8	1.2	1.9	8.3	8.1	7.5	8.0
XI	–	–	–	–	4.5	6.5	5.1	5.3	7.7	2.7	14.1	5	-4.4	22	88	83	87	86	1.0	1.7	1.1	1.3	9.4	8.8	8.2	8.8
XII	–	–	–	–	-0.4	1.0	-0.2	0.0	2.0	-2.7	8.0	5	-11.1	17	85	85	86	85	0.8	1.0	0.8	0.9	8.5	8.0	7.2	7.9
Rok	–	–	–	–	6.8	10.0	7.5	8.0	11.3	4.4	28.5	4.VII	-11.3	16.I	87	76	86	83	1.4	3.8	1.6	2.3	7.5	7.5	7.1	7.5

Kartuzy

$\varphi = 54°20'$ $\lambda = 18°12'$

I	–	–	–	–	-1.5	0.1	-0.9	-0.8	0.7	-3.6	9.0	6	-13.0	16	–	–	–	–	–	–	–	–	9.5	9.1	9.0	9.2
II	–	–	–	–	0.5	3.3	1.4	1.6	3.7	-1.0	8.8	2	-7.1	25	–	–	–	–	–	–	–	–	8.4	8.0	8.0	8.1
III	–	–	–	–	-0.6	4.4	1.1	1.5	5.1	-2.7	15.0	31	-8.6	16	–	–	–	–	–	–	–	–	5.5	6.0	4.2	5.2
IV	–	–	–	–	3.3	8.8	3.9	5.0	9.6	0.3	22.4	28	-7.1	15	–	–	–	–	–	–	–	–	6.9	6.5	5.8	6.4
V	–	–	–	–	7.5	11.9	7.4	8.6	12.8	3.7	21.9	13,19	-2.1	6	–	–	–	–	–	–	–	–	6.3	6.5	4.9	5.9
VI	–	–	–	–	12.3	19.0	13.4	14.5	19.9	8.6	28.4	18	5.4	8	–	–	–	–	–	–	–	–	4.9	4.7	3.6	4.4
VII	–	–	–	–	15.2	20.5	16.1	17.0	21.5	12.6	28.4	4	9.3	26	–	–	–	–	–	–	–	–	6.0	6.2	5.7	6.0
VIII	–	–	–	–	13.0	18.4	14.1	14.9	19.1	11.0	23.9	11	7.1	23	–	–	–	–	–	–	–	–	5.9	7.0	6.7	6.5
IX	–	–	–	–	8.6	13.4	9.7	10.4	14.2	6.5	25.4	8,9	-0.3	27	–	–	–	–	–	–	–	–	7.9	6.4	6.2	6.8
X	–	–	–	–	6.8	11.0	7.9	8.4	11.3	4.9	18.0	10	-0.1	2	–	–	–	–	–	–	–	–	8.7	6.9	6.7	7.4
XI	–	–	–	–	3.2	5.4	3.8	4.0	5.9	1.6	14.0	5	-5.3	29,30	–	–	–	–	–	–	–	–	8.3	8.5	7.7	8.2
XII	–	–	–	–	-1.4	-0.4	-1.2	-1.0	1.0	-3.9	6.2	8	-13.2	17	–	–	–	–	–	–	–	–	8.2	8.0	7.0	7.7
Rok	–	–	–	–	5.6	9.6	6.4	7.0	10.4	3.2	28.4	18.VI,4.VII	-13.2	17.XII	–	–	–	–	–	–	–	–	7.2	7.0	6.3	6.8

Tolkmicko

$\varphi = 54°19'$ $\lambda = 19°32'$

I	–	–	–	–	-0.5	1.1	0.3	0.3	2.4	-2.8	9.9	6	-12.4	16	88	82	86	85	0.7	1.2	0.9	0.9	7.7	7.7	7.6	7.7
II	–	–	–	–	2.2	4.5	2.9	3.1	5.6	0.6	10.5	6	-5.4	25	90	82	89	87	0.7	1.6	0.9	1.1	8.3	7.8	8.4	8.2
III	–	–	–	–	0.5	3.0	2.7	2.7	6.5	-1.5	17.2	31	-9.4	17	80	68	78	75	1.4	3.2	1.8	2.1	5.2	6.2	5.2	5.5
IV	–	–	–	–	5.1	8.6	6.0	6.4	10.3	2.1	22.2	28	-5.3	13	82	71	81	78	1.7	3.9	2.0	2.5	6.5	6.3	6.6	6.5
V	–	–	–	–	9.5	11.9	9.3	10.0	13.8	5.6	24.1	19	0.0	6	79	71	80	77	2.8	4.6	2.6	3.3	6.3	6.0	5.8	6.0
VI	–	–	–	–	14.9	17.7	14.7	15.5	19.6	10.4	29.1	11	5.6	21	78	69	81	76	3.7	6.7	3.2	4.5	5.0	5.6	5.4	5.3
VII	–	–	–	–	17.7	20.6	17.8	18.5	22.0	14.2	29.5	4	9.7	1	84	76	85	82	3.4	6.5	3.2	4.4	6.3	6.6	6.2	6.4
VIII	–	–	–	–	15.6	19.4	15.9	16.7	20.4	12.5	26.6	11	8.1	30	87	73	88	83	2.4	6.2	2.1	3.6	5.8	6.8	6.3	6.3
IX	–	–	–	–	11.2	14.8	11.7	12.4	15.8	8.5	27.0	9	3.0	27	87	72	84	81	1.8	5.3	2.3	3.1	7.2	7.3	7.1	7.2
X	–	–	–	–	8.2	11.7	9.5	9.7	12.6	6.5	19.1	10	2.6	2	90	81	86	85	1.1	2.8	1.7	1.8	7.3	8.0	6.6	7.3
XI	–	–	–	–	4.9	6.6	5.4	5.6	7.9	3.1	15.1	6	-5.1	30	90	86	88	88	0.8	1.5	1.0	1.1	8.5	8.3	8.1	8.3
XII	–	–	–	–	-0.5	1.0	0.1	0.2	2.4	-2.7	7.1	8	-11.4	18	87	83	87	86	0.8	1.1	0.8	0.9	7.3	8.2	7.2	7.6
Rok	–	–	–	–	7.4	10.2	8.0	8.4	11.6	4.7	29.5	4.VII	-12.4	16.I	85	76	84	82	1.8	3.7	1.9	2.5	6.8	7.1	6.7	6.9

Świbno – Ujście Wisły

$H_s = 5\,m$ $h_w = 12\,m$ 1957

MIESIĄC	ROZKŁAD WIATRU %D.V.mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max<0	Max<-10	Max<-25	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	≡	≡	≡	≡	≡
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	145	42	75	48	75	65	145	75	155	59	8	49	155	86	8	73	2	6.2	191	78	15	17	·	·	·	6	4	·	10	2	–	·	5	10	–
IV	27	50	5	59	4	49	15	33	65	51	8	45	10	40	20	52	8	4.4	112	50	22	5	·	·	·	7	4	·	2	1	–	1	4	12	–
V	14	69	165	78	4	41	55	43	115	39	115	56	115	72	155	71	3	6.1	351	75	20	1	·	·	·	10	7	·	7	1	–	1	3	10	–
VI	115	54	10	39	35	50	6	50	7	37	15	41	20	59	12	48	5	4.7	245	94	5	·	·	·	3	9	5	·	6	1	–	1	1	7	–
VII	75	42	10	49	8	52	6	38	13	39	11	45	195	69	14	58	4	5.0	1193	271	16	·	·	·	3	13	11	6	4	·	–	6	1	10	–
VIII	75	69	35	53	3	47	4	56	15	40	285	57	235	60	8	62	·	5.6	804	285	17	·	·	·	2	13	11	2	4	·	–	5	·	6	–
IX	2	42	·	·	·	·	2	48	245	54	265	58	165	96	185	97	·	7.2	1114	309	20	·	·	·	2	17	12	3	14	6	–	1	·	9	–
X	·	·	·	·	·	·	35	43	26	51	365	62	21	71	5	82	1	6.1	156	45	30	·	·	·	·	12	6	·	7	2	–	·	1	10	–
XI	1	10	7	119	10	60	17	46	21	44	16	41	12	88	6	108	·	6.2	169	58	27	7	·	·	·	9	3	·	11	4	–	·	·	21	–
XII	25	14	45	15	7	79	3	52	35	53	235	57	125	96	5	13	·	7.3	177	37	8	21	8	2	·	9	7	·	8	3	–	·	·	17	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	309	20.IX	–	–	–	10	–	–	–	–	–	–	–	–	–	–

Świbno

$H_s = 8\,m$ $h_w = 13\,m$

I	15	90	35	80	2	65	5	28	195	32	30	32	21	47	25	74	8	3.7	152	52	12	24	7	2	·	8	6	·	5	·	6	·	1	19	–
II	45	26	2	40	·	·	6	49	215	47	195	35	10	35	25	58	18	3.3	417	56	1	18	·	·	·	19	13	·	·	·	7	·	·	22	–
III	13	61	55	71	7	29	10	76	115	51	75	26	185	34	12	53	8	4.5	224	73	15	20	2	·	·	8	6	·	4	3	2	·	3	10	–
IV	21	61	35	77	1	30	1	30	25	42	55	37	12	17	305	37	13	3.6	140	42	22	7	·	·	·	9	6	·	2	1	2	1	4	11	–
V	22	78	5	115	1	70	3	40	65	42	105	32	22	25	19	42	4	4.8	361	90	11	1	·	·	·	9	9	·	4	1	3	2	2	9	–
VI	8	45	1	70	·	·	2	40	7	30	165	22	30	20	195	36	6	2.6	271	91	5	·	·	·	2	11	5	·	·	·	1	·	2	7	–
VII	125	44	2	50	15	70	25	50	35	28	155	23	27	23	175	32	11	2.8	1173	275	16	·	·	·	4	15	12	3	·	·	·	5	·	17	–
VIII	6	58	·	·	1	30	3	66	7	51	355	29	275	35	7	39	6	3.3	979	305	16	·	·	·	2	16	14	3	4	·	·	4	·	9	–
IX	·	·	·	·	·	·	05	14	215	44	33	34	255	45	65	74	3	4.2	1145	300	20	·	·	·	2	19	13	3	5	·	5	·	·	14	–
X	·	·	·	·	·	·	05	70	12	51	535	30	205	33	05	30	6	3.2	139	47	30	·	·	·	·	7	5	·	1	·	14	·	·	15	–
XI	2	80	45	102	65	54	55	45	225	42	345	22	125	46	2	90	·	4.1	144	64	27	8	1	·	·	9	3	·	4	2	6	·	·	22	–
XII	5	85	6	72	3	57	1	20	105	43	345	35	21	40	8	33	4	4.1	252	60	30	24	8	3	·	10	6	·	5	1	·	·	·	16	–
Rok	955	52	33	56	23	34	40	44	1455	42	296	30	2475	33	1275	50	87	3.7	5397	305	16.VIII	102	17	5	10	140	98	9	31	8	46	12	12	171	–

Kartuzy

$H_s = 220\,m$ $h_w = 11\,m$

I	·	·	2	30	6	17	12	10	18	20	40	39	10	46	·	·	5	2.8	248	95	5	27	14	2	·	9	8	·	·	·	17	–	·	26	–
II	1	10	7	10	8	10	13	13	19	19	27	29	1	10	·	·	8	1.8	532	120	9	17	2	·	·	15	12	1	·	·	9	–	·	17	–
III	4	25	11	19	19	15	16	21	12	29	16	36	7	27	2	10	6	2.2	207	81	20	23	4	·	·	7	5	·	2	·	4	–	4	6	–
IV	6	13	25	16	11	10	6	10	5	10	18	24	2	20	1	30	16	1.4	280	128	22	12	·	·	·	11	6	1	·	·	10	–	5	12	–
V	10	20	17	22	10	10	16	16	15	13	10	30	6	30	6	30	3	1.9	365	95	9	3	·	·	·	15	9	·	·	·	2	–	2	6	–
VI	1	10	5	10	12	12	25	15	12	15	13	28	7	33	2	60	13	1.6	184	50	9	·	·	·	4	10	5	·	·	·	3	–	6	5	–
VII	1	30	10	14	13	10	18	11	9	10	18	24	9	26	4	20	11	1.4	1580	464	12	·	·	·	4	21	16	4	·	·	·	–	5	6	–
VIII	3	10	3	10	9	10	17	11	21	19	23	19	2	10	3	17	12	1.3	1008	228	16	·	·	·	·	19	13	4	·	·	2	–	·	10	–
IX	·	·	3	17	·	·	28	15	15	22	19	25	4	30	7	44	14	1.9	948	162	27	1	·	·	2	22	15	3	·	·	2	–	·	11	–
X	1	10	·	·	·	·	23	13	31	23	23	25	8	35	·	·	7	2.0	194	50	5	1	·	·	·	12	7	·	·	·	6	–	·	13	–
XI	·	·	6	13	16	12	22	15	13	25	17	25	2	65	4	52	10	1.9	394	76	28	13	1	·	·	13	8	·	·	·	9	–	2	21	–
XII	2	20	5	38	9	14	16	12	24	17	27	39	2	40	1	70	7	2.3	467	128	30	25	10	5	·	11	8	1	·	·	10	–	3	19	–
Rok	29	12	94	17	113	10	212	14	194	18	251	29	60	31	30	28	112	1.9	6407	464	12.VII	122	31	7	10	165	112	14	21	·	74	–	27	152	–

Tolkmicko

$H_s = 1\,m$ $h_w = 16\,m$

I	·	·	3	73	2	80	75	35	11	37	50	83	105	83	2	70	7	6.7	272	76	26	24	5	3	·	10	7	·	13	2	1	·	1	19	6
II	15	63	6	45	1	10	6	38	25	37	315	59	8	56	3	82	2	4.9	520	66	18	8	·	·	·	17	14	·	5	·	2	·	·	19	1
III	8	49	75	36	6	52	165	72	155	70	20	64	105	52	7	101	2	6.2	219	94	15	20	2	·	·	9	6	·	13	2	·	·	7	11	3
IV	105	63	45	89	2	25	95	34	11	42	115	56	135	59	225	46	5	4.9	242	66	28	7	·	·	·	15	8	·	7	·	6	3	3	13	1
V	175	67	45	70	25	68	11	49	105	27	115	47	185	65	16	60	1	5.6	284	80	11	·	·	·	·	15	8	·	7	·	3	3	3	10	·
VI	6	58	4	59	45	34	95	49	12	28	20	56	165	60	135	58	4	4.9	520	148	22	·	·	·	3	12	7	2	3	·	1	3	3	7	·
VII	15	40	14	40	4	45	165	41	11	37	22	57	125	60	145	57	7	4.6	856	202	2	·	·	·	6	14	10	4	3	·	·	7	2	9	·
VIII	2	50	2	30	05	30	7	54	105	42	39	65	13	66	11	67	8	5.5	1189	221	17	·	·	·	1	19	13	4	7	·	·	5	·	9	·
IX	1	50	·	·	·	·	55	71	23	63	335	66	13	89	10	112	4	7.1	1433	215	28	·	·	·	2	20	19	5	15	3	·	2	·	9	·
X	2	25	·	·	·	·	35	31	125	61	61	81	9	51	2	72	3	7.0	307	85	30	·	·	·	·	12	7	·	46	4	1	·	1	12	·
XI	1	17	65	103	9	43	16	52	105	44	32	62	65	65	15	133	7	5.7	263	84	28	9	1	·	·	9	8	·	13	2	1	·	·	19	·
XII	15	87	65	72	55	55	4	45	145	59	535	81	35	86	1	100	3	7.2	291	87	8	24	8	3	·	10	6	·	16	1	·	·	4	19	5
Rok	525	47	485	51	37	37	1125	48	167	46	3855	65	135	66	104	80	53	5.9	6396	221	17.VIII	92	16	6	12	160	111	15	121	16	15	23	26	156	16

Gołdap

$\varphi = 54°19'$ $\lambda = 22°19'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.2	-0.8	-1.5	-1.5	0.8	-4.5	10.7	6	-21.9	16	88	87	87	87	0.6	0.7	0.7	0.7	8.5	8.9	7.9	8.4
II	–	–	–	–	0.4	2.0	1.0	1.1	3.5	-0.9	7.0	2	-9.5	28	91	87	88	89	0.6	0.9	0.8	0.8	9.7	8.9	7.5	8.7
III	–	–	–	–	-2.6	2.8	-0.7	-0.3	4.6	-4.8	16.9	31	-14.6	17	–	–	–	–	–	–	–	–	5.7	6.0	3.5	5.1
IV	–	–	–	–	4.2	11.4	5.8	6.8	13.1	0.9	25.9	27	-7.0	14	–	–	–	–	–	–	–	–	5.8	6.5	5.4	5.9
V	–	–	–	–	8.9	13.2	8.7	9.9	15.0	4.4	25.2	19	-3.5	2	–	–	–	–	–	–	–	–	5.5	7.4	6.2	6.4
VI	–	–	–	–	14.3	18.9	13.9	15.2	20.5	8.3	27.5	11	0.8	21	–	–	–	–	–	–	–	–	5.0	6.7	4.9	5.5
VII	–	–	–	–	16.5	21.0	16.4	17.6	22.5	12.0	31.5	8	7.0	4	–	–	–	–	–	–	–	–	7.2	7.8	6.2	7.1
VIII	–	–	–	–	14.1	18.5	14.1	15.2	20.0	11.0	28.5	12	5.0	24	–	–	–	–	–	–	–	–	5.8	8.8	6.3	7.0
IX	–	–	–	–	9.0	13.2	9.6	10.4	14.9	6.6	26.1	9	0.7	17	92	77	91	87	1.0	4.2	1.2	2.1	7.5	8.6	5.3	7.1
X	–	–	–	–	6.3	10.4	7.9	8.1	11.5	5.0	18.0	10	1.5	2	92	79	88	86	0.8	2.7	1.3	1.6	7.5	7.7	5.9	7.0
XI	–	–	–	–	3.0	4.7	3.4	3.6	6.1	1.2	13.5	6	-10.5	30	90	82	88	87	0.8	1.6	0.9	1.1	9.2	9.3	8.2	8.9
XII	–	–	–	–	-2.4	-1.0	-2.1	-1.9	0.2	-4.8	5.5	5	-15.1	18	90	87	88	88	0.5	0.7	0.6	0.6	7.7	8.3	8.0	8.0
Rok	–	–	–	–	5.8	9.5	6.4	7.0	11.1	2.9	31.5	8.VII	-21.9	16.I	–	–	–	–	–	–	–	–	7.1	7.9	6.3	7.1

Hopowo

$\varphi = 54°16'$ $\lambda = 18°14'$

I	–	–	–	–	-1.2	-0.3	-1.1	-0.9	0.7	-3.3	9.3	6	-13.1	16	–	–	–	–	–	–	–	–	9.1	8.3	8.9	8.8
II	–	–	–	–	0.5	2.5	0.9	1.2	3.5	-0.5	6.8	14	-7.0	25	–	–	–	–	–	–	–	–	8.7	7.8	8.0	8.2
III	–	–	–	–	-0.6	4.1	0.1	0.9	5.2	-2.2	15.9	31	-8.3	16	–	–	–	–	–	–	–	–	5.8	6.2	6.3	6.1
IV	–	–	–	–	3.6	8.7	3.0	4.6	9.9	1.0	22.4	28	-6.8	15	–	–	–	–	–	–	–	–	7.1	7.2	6.5	6.9
V	–	–	–	–	7.6	11.3	7.2	8.3	13.1	4.3	22.0	13	-1.5	6	83	65	83	77	2.1	5.5	2.0	3.2	7.0	7.1	5.5	6.5
VI	–	–	–	–	13.6	18.3	12.6	14.3	20.1	8.8	29.0	18	4.6	15	–	–	–	–	–	–	–	–	5.2	5.9	4.6	5.2
VII	–	–	–	–	16.0	20.1	15.4	16.7	21.5	12.7	28.8	4,8	9.3	7	88	70	90	83	2.3	7.8	1.9	4.0	7.2	7.3	5.8	6.8
VIII	–	–	–	–	13.8	17.5	13.8	14.7	18.8	11.5	24.6	11	7.2	9	92	72	91	85	1.4	6.0	1.5	3.0	6.8	7.9	6.8	7.2
IX	–	–	–	–	9.1	12.7	8.8	9.8	14.2	7.0	25.6	9	1.5	27	94	77	90	87	0.8	4.2	1.3	2.1	7.8	8.1	7.4	7.8
X	–	–	–	–	6.6	10.2	6.7	7.6	10.9	–	17.7	10	–	–	–	–	–	–	–	–	–	–	8.2	8.0	7.4	7.9
XI	–	–	–	–	3.0	5.0	2.6	3.3	5.8	1.6	13.9	5	-9.3	30	–	–	–	–	–	–	–	–	8.6	8.6	7.7	8.3
XII	–	–	–	–	-1.6	-0.6	-1.5	-1.3	0.6	-3.5	5.6	5	-12.0	18	–	–	–	–	–	–	–	–	8.8	8.4	8.4	8.5
Rok	–	–	–	–	5.9	9.1	5.7	6.6	10.4	–	29.0	18.VII	-13.1	16.I	–	–	–	–	–	–	–	–	7.5	7.6	6.9	7.3

Bartoszyce

$\varphi = 54°15'$ $\lambda = 20°48'$

I	–	–	–	–	-1.4	0.2	-0.7	-0.6	1.5	-3.9	9.1	6	-20.0	16	89	85	86	87	0.6	1.0	0.8	0.8	7.7	7.0	6.8	7.2
II	–	–	–	–	1.5	3.4	2.2	2.3	4.4	-0.6	8.7	14	-4.7	28	92	82	88	87	0.5	1.4	0.9	0.9	8.0	6.9	6.2	7.0
III	–	–	–	–	-1.2	4.4	1.5	1.6	5.9	-3.4	17.6	31	-18.0	17	81	62	79	74	1.0	3.7	1.7	2.1	5.2	5.0	5.0	5.1
IV	–	–	–	–	3.7	11.5	6.1	6.8	12.8	0.6	24.9	27	-6.2	14	87	56	80	74	1.0	7.0	2.1	3.4	5.4	5.1	5.9	5.5
V	–	–	–	–	8.6	13.4	9.6	10.3	14.9	4.8	26.1	19	-2.9	2	84	59	79	74	1.9	7.2	2.7	3.9	5.4	6.0	5.4	5.6
VI	–	–	–	–	14.0	18.9	14.1	15.3	20.8	8.5	27.9	11	2.6	21	81	61	85	75	3.0	9.0	2.8	4.9	4.5	5.7	4.7	5.0
VII	–	–	–	–	16.3	21.3	16.8	17.8	22.8	12.3	29.1	8	6.9	4	90	69	87	82	2.0	8.3	2.6	4.3	7.2	6.2	5.5	6.3
VIII	–	–	–	–	14.1	19.2	15.3	16.0	20.5	10.6	28.5	12	6.2	9	92	70	87	83	1.3	7.0	2.2	3.5	5.5	6.8	5.5	5.9
IX	–	–	–	–	9.8	14.1	11.0	11.5	15.4	7.1	26.1	9	1.5	17	93	73	88	85	1.0	5.1	1.7	2.6	6.4	6.4	5.9	6.2
X	–	–	–	–	6.6	11.2	8.4	8.6	12.3	5.0	19.6	10	1.3	2	93	78	89	87	0.7	3.1	1.2	1.7	7.2	7.1	3.8	6.0
XI	–	–	–	–	3.8	5.7	4.6	4.7	7.1	2.0	14.6	6	-7.6	29	92	83	88	88	0.6	1.6	1.0	1.1	7.8	7.4	7.4	7.5
XII	–	–	–	–	-1.6	-0.1	-1.1	-1.0	–	-3.4	–	–	-11.4	19	87	86	88	87	0.6	0.8	0.6	0.7	6.6	6.9	5.9	6.5
Rok	–	–	–	–	6.2	10.4	7.3	7.8	–	3.3	29.1	8.VII	-20.0	16.I	88	72	85	82	1.2	4.6	1.7	2.5	6.4	6.4	5.7	6.2

Nowy Dwór Gdański

$\varphi = 54°13'$ $\lambda = 19°08'$

I	–	–	–	–	-1.0	1.1	-0.6	-0.3	1.8	-2.9	9.4	6	-12.5	15	88	87	88	88	0.6	0.8	0.7	0.7	8.2	8.1	7.6	8.0
II	–	–	–	–	1.4	3.9	2.1	2.4	5.0	0.4	9.3	14	-4.5	25	93	86	93	91	0.4	1.2	0.5	0.7	9.0	8.5	8.4	8.6
III	–	–	–	–	0.2	5.5	1.8	2.3	6.7	-1.5	18.1	31	-7.6	9	85	71	83	80	0.9	3.2	1.3	1.8	5.3	6.1	5.6	5.7
IV	–	–	–	–	4.5	9.8	4.9	6.0	11.1	1.7	24.6	28	-5.0	16	88	66	87	80	1.1	5.3	1.3	2.6	6.5	6.6	6.9	6.7
V	–	–	–	–	9.6	13.1	8.4	9.9	14.5	5.2	23.9	19	-3.0	6	77	64	82	74	2.9	6.1	2.1	3.7	6.4	6.0	5.3	5.9
VI	–	–	–	–	14.9	19.2	13.8	15.4	20.6	9.9	29.0	11	5.8	21	79	64	85	76	3.6	8.8	2.5	5.0	5.0	5.8	5.0	5.3
VII	–	–	–	–	17.3	21.8	16.4	17.9	22.9	13.5	29.6	4	9.4	29	86	70	90	82	2.7	8.6	2.0	4.4	7.1	6.7	6.5	6.7
VIII	–	–	–	–	15.8	19.6	14.7	16.0	21.0	11.7	26.7	12	7.3	30	–	–	–	–	–	–	–	–	6.5	7.3	6.2	6.7
IX	–	–	–	–	10.4	14.5	10.7	11.6	15.7	7.8	26.7	9	2.0	27	91	74	90	85	1.1	5.0	1.4	2.5	7.0	7.7	7.9	7.5
X	–	–	–	–	7.3	12.0	8.2	8.9	13.0	5.5	18.8	10	1.3	2	95	83	94	90	0.5	2.4	1.0	1.3	7.2	7.6	6.8	7.2
XI	–	–	–	–	4.3	6.6	4.6	5.0	7.6	2.7	14.6	5	-6.7	30	92	84	90	89	0.7	1.7	0.9	1.1	8.8	8.4	7.7	8.3
XII	–	–	–	–	-0.9	0.7	-0.7	-0.4	1.8	-2.7	7.5	5	-11.9	18	–	–	–	–	–	–	–	–	8.7	8.0	6.6	7.8
Rok	–	–	–	–	6.9	10.6	7.0	7.9	14.8	4.3	29.6	4.VII	-12.5	15.I	–	–	–	–	–	–	–	–	7.1	7.2	6.7	7.0

Gołdap

$H_s = 150\ m$ $h_w = 15\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max=0	Max 0÷10	Max 10÷25	Opad R 0,1	1,0	10,0	Wiatr ≥10	≥15				
I			35	42	6	42	15	34	85	45	245	43	24	56	35	52	8	42	400	146	6	28	10	4		16	9	1	3	1	-	-	1	21	-
II	2	2,5	1	30	4	25	8	46	17,5	25	19,5	31	15,5	33	25	46	14	27	311	57	19	17	4			16	9		1	-	-		20	-
III	5,5	31	3	23	12,5	52	12,5	55	6	28	14,5	25	13	50	7	63	19	34	228	58	15	26	9	5		11	6		3	1	-	-	10	7	-
IV	6	37	5	21	9	17	7,5	20	4	24	9,5	26	13	33	15	36	21	22	452	262	30	12			1	16	7	1	1		-	-	5	9	-
V	11	29	25	20	8,5	18	9,5	17	6	19	8	30	15	29	10,5	20	22	18	235	96	19	4			1	8	4				-	-	3	8	-
VI	8,5	24	2	32	3,5	27	7,5	24	4,5	18	13,5	33	22	31	11,5	34	17	24	343	68	5				6	10	10		1		-	-	5	8	-
VII	4,5	33	0,5	30	7,5	20	10	32	0,5	60	9	4,3	16	33	17	30	31	21	1091	154	19				6	18	15	4	1		-	-	3	15	-
VIII	1,5	40	1	10	4	18	5	34	6	23	14	6,8	15	25	17,5	30	29	21	2483	648	17				1	16	14	4	1		-	-		10	-
IX	3	10					2,5	20	7,5	24	21	29	19	45	11	34	26	24	2450	449	18				1	19	16	7	3		-	-	2	13	-
X					2	25	0,5	40	22,5	33	30	33	12	44	6	29	20	27	218	88	30					13	6		4		-	-	1	14	-
XI	6	40	6,5	38	7	28	10,5	50	11	52	13	24	7	33	6	38	23	26	392	146	28	13	1	2		11	7	1	2		-	-		23	-
XII	8	26			7,5	4,5	4,5	28	7	42	32,5	4,9	10	48	4,5	42	19	35	328	78	8,13	26	11	6		17	8		5	1	-	-	2	21	-
Rok	53	25	25	20	7,15	26	93	33	10,1	33	20,9	36	18,1,5	38	11,2	38	249	27	8931	648	17 VIII	126	35	17	16	171	111	18	25	3	-	-	32	169	-

Hopowo

$H_s = 220\ m$ $h_w = 12\ m$

I			4	5,5	2	3,0	7,5	2,0	8,5	4,0	3,7	5,7	16,5	6,8	8,5	7,7	9	5,0	123	34	12	24	12	2		11	4		5					24	-
II	1,5	3,3	3	2,7			0,5	4,0	1,8	5,2	28,5	5,0	15,5	5,4	4	6,4	13	4,3	545	126	9	14	1			20	14	1	2		-			15	-
III	7	4,4	4,5	4,9	2,5	5,6	1,7	4,4	1,5	6,9	13	4,8	11,5	6,7	9,5	4,5	13	4,7	196	74	15	19	1			9	6		3	1	-		4	13	-
IV	10,5	4,6	1,5	3,9	3	1,3	5,5	2,6	1,0	3,9	1,3	5,2	7	2,9	1,3	6,2	1,3	3,7	414	145	22	9				13	8	2	2		-	1	3	15	-
V	8,5	3,7	1,4	4,1	3,5	1,6	4	4,8	7,5	4,6	13,5	5,4	10,5	3,7	20,5	4,2	1,1	3,7	361	116	9	1				13	8	1	2		-	2	3	9	-
VI	3,5	2,4	1,4,5	2,7	2,5	1,8	5,5	2,6	2,5	5,0	2,0	4,0	2,1	3,0	1,1,5	4,7	9	3,1	166	55	28				3	6	5				-	1	5	7	-
VII	3	2,3	8,5	2,1	0,5	5,0	7	2,8	8,5	2,5	1,9	3,4	1,6	5,0	17,5	4,3	1,3	3,1	2235	541	12				4	18	15	7			-	9	1	10	
VIII	4,5	3,7	2,5	1,0	2,5	3,0	4	4,0	1,1	4,2	3,4,5	4,7	1,2	4,4	1,2	3,9	1,0	3,8	859	191	16					16	15	2	2	1	-	3		15	
IX	1	5,0					1	2,5	1,7,5	4,5	4,0	5,6	6,5	7,1	1,3	7,5	1,1	5,0	819	134	23				2	15	15	1	8	2	-			16	
X							0,5	3,0	2,2,5	5,7	4,7,5	5,4	1,7,5	6,6	3	9,0	2	5,7	194	4,5	30	-				9	8		8	2	-		1	17	
XI	3	6,8	1	3,0	4	3,9	1,7	4,0	2,1	5,9	14,5	5,0	13,5	8,7	5	7,6	1,1	5,1	26,7	6,1	24	12	1			12	6		4	2	-		2	22	-
XII	1	5,0	3	12,7	2,5	4,6	5	5,4	1,6,5	7,7	4,0,5	7,2	5	7,5	8,5	8,5	1,1	6,5	552	101	8	24	11	4		11	9	1	10	2	-		1	25	-
Rok	4,3,5	3,4	7,0	3,6	2,3	2,5	7,4,5	3,5	1,5,8,5	5,0	3,2,1	5,1	1,5,2,5	5,6	1,2,6	6,2	1,2,6	4,5	6731	541	12 VIII	-	2,6	6	9	153	113	15	4,6	10	-	1,6	20	188	-

Bartoszyce

$H_s = 60\ m$ $h_w = 13\ m$

I			6	2,7	1	2,0	11,5	1,7	2,5	2,4	3,1	2,8	2,7,5	3,9	4,5	2,9	9	2,7	188	48	12	25	6	3		10	7				4	-	1	14	-
II	2	1,0	8	1,5			7	2,0	1,3	2,2	2,4	2,0	1,2	2,8	7	3,3	1,1	1,9	335	108	18	16	2			17	8	1				-		11	-
III	8	2,4	6	1,3	9	2,2	1,8	3,5	6	3,3	5	2,6	1,7	3,9	1,2	3,4	1,2	2,7	247	66	15	23	5	1		10	8		1	1		-	7	8	-
IV	2,1	2,8	7	1,4	4	2,0	2	1,5	1	3,0	8	3,0	1,2	2,5	1,6	2,9	1,9	2,0	99	19	28	14				10	4				1	-	5	7	-
V	2,0	2,0	7	1,7	5	1,6	1	1,0	5	1,6	4	2,8	1,4	2,4	2,1	2,2	1,6	1,7	221	66	7	4			1	12	8					-	5	7	-
VI	1,0	1,3	3	1,7	4	2,0	2	2,0	3	1,7	3	3,3	1,9	2,7	2,0	2,2	2,6	1,5	552	144	22				4	10	7	2			1	-	6	4	-
VII	6	1,3	1	2,0	8	1,4	2	3,0	5	1,2	6	2,2	2,0	2,7	1,1	2,3	3,4	1,3	1098	173	30				6	18	14	3			3	-	2	8	-
VIII	6	2,3			2	1,5	3	3,3	7	2,4	1,3	3,5	2,0	2,8	1,9	1,9	2,3	2,0	1719	896	17				1	17	11	6			1	-	1	4	-
IX	2	2,0					5	2,0	8	2,1	2,1	3,2	2,8	2,6	7	4,1	1,9	2,2	1535	255	15				2	19	17	5			2	-	1	5	-
X							4	1,0	7	2,7	3,9	2,7	2,3	2,9	6	3,0	1,4	2,3	155	42	30					12	6				3	-	3	7	
XI	8	4,1	6	2,2	6	1,5	1,4	2,1	7	1,7	1,9	1,8	1,2	3,6	3	2,7	1,5	2,0	129	8,0	28	9	1			7	3					-	1	1,9	
XII	5	2,6	1	1,0	6	2,5			6	1,3	3,9	3,5	1,7	4,1	3	1,7	1,6	2,7	228	68	8	22	-	5		12	7				1	-	4	1,4	
Rok	8,8	1,8	4,5	1,3	4,5	1,4	6,9,5	1,9	7,0,5	2,1	2,1,2	2,8	2,2,1,5	3,1	1,2,9,5	2,7	2,1,4	2,1	6,5,0,6	8,9,6	17 VIII	1,1,3	-	9	1,4	1,5,4	1,0,0	1,7	1	1	1,5	-	3,6	1,0,8	

Nowy Dwór Gdański

$H_s = 0\ m$ $h_w = 13\ m$

I	1	3,0	6	4,5	9	2,0	7,5	2,2	2,8	2,6	1,7	2,9	1,7	3,6	6,5	2,3	1	2,8	202	53	26	25	7	3		10	6				2			19	-
II	3	2,2	6	2,1	4	2,9	2,1,5	2,7	1,5,5	2,2	1,1	2,2	9	2,9	6	3,5	8	2,3	489	72	8,18	10				17	13				6			19	-
III	6	3,0	10	2,5	19,5	4,8	16,5	3,0	7	3,9	4	2,2	11,5	4,3	12,5	3,7	6	3,4	231	77	15	21	2			7	6		1		2		6	11	-
IV	2,7	4,5	9	2,2	8	2,6	2	3,0	5,5	2,8	5	3,4	7,5	2,6	1,9	2,9	7	3,0	172	4,3	8,2	8				13	5		1		2	3	5	12	-
V	2,3,5	4,4	8,5	4,2	9	2,7	8,5	2,6	6,5	2,8	5	4,8	1,5	7,0	16,5	3,3	1,4	3,2	419	97	11	2				13	9				2	3	2	9	-
VI	1,9,5	3,0	12,5	2,0	6,5	3,7	3,5	4,1			1,1	2,9	1,7	2,2	1,7	2,9	3	2,7	387	99	5				3	11	7				2		6	7	-
VII	1,8	2,6	1,4,5	2,1	12,5	2,8	7	2,8	7	3,1	5	3,0	7	2,9	1,7	3,0	5	2,6	870	306	16				7	15	10	2			4	6		10	-
VIII	7,5	2,3	2	1,0	6	2,6	8	2,3	1,1,5	3,5	1,6	3,7	1,7,5	2,6	1,4,5	3,0	1,0	2,6	1114	360	16				3	19	15	2			·2	5		10	-
IX	1	1,0	1	1,0	4	2,2	1,2	2,7	1,4	3,3	1,9,5	3,8	1,9	4,4	1,2,5	4,0	7	3,3	887	147	20				2	19	14	2	2	●	2	2	1	14	-
X			1	1,0	1,5	2,3	1,4,5	3,2	2,4,5	3,4	3,1	3,0	1,0,5	3,0	6	3,2	4	3,0	181	57	30					11	6				1,1		2	13	-
XI	0,5	1,7,0	6,5	6,8	1,7,5	2,7	2,2	2,8	1,6	2,8	1,0	3,0	1,0,5	3,5	4	6,5	3	3,3	192	60	28	9	1			8	3		1	1	5			20	-
XII	2	4,0	9	4,1	3,5	2,9	1,5,5	2,4	2,8	3,5	1,8	2,9	1,1,5	3,6	3,5	5,1	2	3,2	192	55	8	22	1,0	2		12	6				9			18	-
Rok	1,0,9	3,9	8,6	2,8	1,0,4	2,8	1,3,8,5	2,8	1,6,3,5	2,8	1,5,2,5	3,2	1,3,9,5	3,6	1,3,5	3,6	7,0	3,0	5,3,3,6	3,6,0	1,6 VIII	9,7	2,0	5	1,5	1,5,5	1,0,0	6	5	1	4,9	1,9	2,2	1,6,2	

Koszalin

$\varphi = 54°12'$ $\lambda = 16°10'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI f_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1014.4	1027.7	994.7	1018.9	0.2	1.4	0.7	0.8	2.5	-1.8	10.6	6	-9.3	15	86	81	84	84	0.8	1.3	1.0	1.0	8.5	7.8	7.4	7.9
II	1004.1	1033.2	976.7	1008.8	1.5	4.6	2.8	2.9	5.6	-0.5	9.8	2	-6.8	26	87	75	84	82	0.9	2.1	1.2	1.4	7.0	7.4	6.2	6.9
III	1012.9	1034.0	985.7	1017.6	0.7	5.7	2.8	3.0	7.2	-1.6	16.1	27	-5.5	9	82	68	80	77	1.2	3.3	1.6	2.0	5.4	5.3	3.5	4.8
IV	1014.7	1027.8	987.8	1019.4	3.3	8.5	4.5	5.2	9.4	0.0	20.7	5	-5.1	15	86	67	82	78	1.2	4.6	1.7	2.5	7.6	6.3	5.8	6.6
V	1012.4	1027.2	999.9	1017.0	8.0	12.3	8.4	9.3	13.8	3.4	24.3	19	-1.7	6	80	62	78	73	2.3	6.4	2.9	3.9	5.0	6.3	4.6	5.3
VI	1011.7	1027.7	998.7	1016.2	14.2	18.3	14.2	15.2	19.8	8.6	28.7	11	4.8	1	78	58	76	71	3.8	9.4	4.0	5.7	5.3	5.4	3.8	4.8
VII	1006.9	1018.5	996.9	1011.3	16.9	19.9	17.0	17.7	21.4	12.5	29.4	1	7.8	7	84	71	83	79	3.1	7.3	3.6	4.7	7.0	6.6	5.5	6.4
VIII	1007.6	1019.9	994.8	1012.1	14.4	18.8	14.9	15.8	19.6	10.9	25.7	11	6.8	23	87	70	84	80	2.1	6.8	2.9	3.9	7.0	7.0	5.3	6.4
IX	1005.4	1018.7	984.8	1010.0	9.9	13.8	10.5	11.2	14.6	6.9	25.0	8	0.4	27	86	69	84	80	2.1	5.5	2.0	3.2	7.1	7.2	6.0	6.8
X	1011.5	1024.3	995.9	1016.1	8.1	11.7	9.3	9.6	12.2	6.0	18.6	9	1.0	2	88	73	85	82	1.3	3.8	1.8	2.3	7.9	7.2	6.7	7.3
XI	1015.3	1034.8	995.3	1020.5	4.0	6.5	4.6	4.9	7.2	1.8	14.2	5	-6.3	30	86	77	84	82	1.1	2.3	1.3	1.6	7.3	7.9	7.5	7.6
XII	1007.9	1025.9	965.7	1012.6	0.0	1.4	0.5	0.6	2.6	-2.8	8.9	8	-11.8	17	85	80	84	83	0.9	1.3	1.0	1.1	8.2	8.1	6.3	7.5
Rok	1010.4	1034.8	965.7	1015.0	6.8	10.2	7.5	8.0	11.3	3.6	29.4	4.VII	-11.8	17.XII	85	74	82	79	1.7	4.5	2.1	2.8	6.9	6.9	5.7	6.5

Kołobrzeg

$\varphi = 54°11'$ $\lambda = 15°35'$

I	1018.1	1031.8	998.6	1018.6	0.6	1.7	0.8	1.0	2.7	-1.5	10.4	6	-9.9	1	92	84	90	89	0.5	1.1	0.7	0.8	9.2	7.9	7.7	8.3
II	1007.7	1037.1	979.6	1008.4	1.5	4.6	2.8	2.9	5.7	0.0	11.2	2	-6.2	26	93	78	88	86	0.5	1.9	0.9	1.1	8.1	7.8	7.3	7.7
III	1016.6	1037.9	989.6	1017.3	1.0	5.1	2.4	2.7	6.7	-0.8	15.3	27	-5.2	2	87	70	83	80	0.8	2.9	1.3	1.7	5.9	6.3	4.8	5.7
IV	1019.1	1032.0	992.0	1019.8	3.4	6.2	4.2	4.5	7.6	1.3	20.3	5	-3.9	15	88	75	84	83	1.0	2.4	1.3	1.6	7.8	7.1	6.5	7.1
V	1016.6	1031.4	1004.6	1017.3	8.4	10.6	8.5	9.0	12.5	4.9	25.0	16	-0.8	6.29	78	69	79	75	2.6	4.4	2.4	3.1	5.8	6.3	5.4	5.8
VI	1015.7	1032.1	1002.9	1016.4	14.2	16.4	14.0	14.6	18.4	9.4	28.9	11	5.4	16	78	70	81	76	3.8	6.0	3.3	4.4	5.7	5.5	4.8	5.3
VII	1010.9	1022.5	1000.8	1011.5	17.1	19.4	17.1	17.7	20.9	13.9	28.5	1	7.6	7	88	74	84	82	2.4	6.0	3.3	3.9	7.0	6.4	6.5	6.6
VIII	1011.5	1023.9	998.3	1012.2	14.8	18.4	15.2	15.9	19.6	12.1	25.8	11	8.6	25	88	72	86	82	2.1	6.2	2.6	3.6	6.5	7.5	6.4	6.8
IX	1009.5	1022.8	988.1	1010.2	10.7	14.0	11.2	11.3	15.1	8.3	22.7	7	2.4	27	85	70	84	80	1.8	5.0	2.2	3.0	7.5	7.7	6.3	7.2
X	1015.6	1028.0	1000.3	1016.3	8.4	12.0	9.7	10.0	12.7	6.8	18.2	10	2.2	2	89	73	86	83	1.2	3.9	1.7	2.3	8.1	7.3	7.7	7.7
XI	1019.5	1038.7	999.1	1020.2	3.9	6.4	4.7	4.9	7.3	2.5	13.7	5	-4.9	30	89	81	87	86	0.9	2.0	1.1	1.3	8.1	8.6	7.9	8.2
XII	1012.2	1030.1	969.0	1012.9	0.4	1.7	1.0	1.0	3.3	-1.6	9.4	8	-11.1	17	89	82	87	86	0.7	1.2	0.9	0.9	8.6	8.7	7.5	8.3
Rok	1014.4	1038.7	969.0	1015.1	7.0	9.7	7.6	8.0	11.0	4.6	28.9	11.VI	-11.1	17.XII	87	75	85	82	1.5	3.6	1.8	2.3	7.4	7.3	6.6	7.1

Żelisławki

$\varphi = 54°10'$ $\lambda = 18°39'$

I	-	-	-	-	-1.1	0.3	-0.5	-0.4	1.7	-3.4	9.9	6	-12.9	16	92	88	90	90	0.5	0.8	0.6	0.6	7.8	6.6	6.3	6.9
II	-	-	-	-	1.1	3.6	2.0	2.2	4.7	-0.1	8.6	14	-5.5	25	96	84	93	91	0.3	1.3	0.5	0.7	8.6	6.8	7.2	7.5
III	-	-	-	-	-0.3	4.6	1.6	1.9	6.1	-1.8	15.1	27	-7.4	9	83	67	82	77	1.0	3.1	1.4	1.8	5.1	5.6	4.3	5.0
IV	-	-	-	-	3.7	9.5	4.3	5.4	11.2	1.0	23.9	28	-6.0	13	86	66	84	79	1.2	5.0	1.5	2.6	5.5	6.6	5.3	5.6
V	-	-	-	-	8.3	12.8	8.1	9.3	14.3	4.5	23.3	13	-1.8	6	80	61	82	74	2.3	6.4	2.2	3.6	5.9	6.8	5.3	6.0
VI	-	-	-	-	14.1	19.0	13.5	15.0	20.7	8.7	29.1	18	4.7	21	78	62	83	74	3.6	9.1	2.7	5.1	4.1	5.1	4.2	4.5
VII	-	-	-	-	16.5	21.3	16.0	17.4	23.2	12.6	30.1	4	9.2	4	87	69	90	82	2.5	8.7	4.9	4.4	6.8	5.9	5.6	6.1
VIII	-	-	-	-	14.7	19.5	14.4	15.8	21.2	11.5	25.6	11	7.7	23,31	88	66	90	81	2.1	8.0	1.6	3.9	4.9	6.7	6.6	6.1
IX	-	-	-	-	9.5	14.2	10.3	11.1	15.7	7.3	27.1	9	0.7	27	91	69	86	82	1.1	5.7	1.8	2.9	6.8	7.0	5.6	6.5
X	-	-	-	-	6.7	11.5	8.3	8.7	12.8	5.1	19.1	10	0.2	2	94	74	88	85	0.6	3.5	1.4	1.8	6.9	7.4	5.3	6.5
XI	-	-	-	-	3.7	5.9	4.3	4.6	7.3	2.2	15.1	5	-5.7	30	92	82	89	88	0.6	1.7	0.9	1.1	8.7	8.1	7.1	8.0
XII	-	-	-	-	-1.0	0.3	-0.6	-0.5	1.7	-3.4	7.7	5	-12.2	17	89	86	90	88	0.6	0.9	0.6	0.7	8.1	7.4	6.4	7.3
Rok	-	-	-	-	6.3	10.2	6.8	7.5	11.7	3.7	30.1	4.VII	-12.9	16.1	88	73	87	83	1.4	4.5	1.4	2.4	6.6	6.7	5.8	6.4

Elbląg

$\varphi = 54°10'$ $\lambda = 19°25'$

I	1013.3	1026.7	995.3	1018.7	-1.4	0.4	-0.8	-0.6	1.2	-3.2	9.2	6	-15.0	16	92	86	90	89	0.4	0.9	0.6	0.6	8.2	7.9	7.5	7.9
II	1004.1	1029.6	979.4	1009.5	1.5	3.8	2.3	2.5	4.4	0.7	9.3	14	-4.1	25	94	82	89	88	0.4	1.5	0.8	0.9	8.9	8.1	8.4	8.5
III	1012.9	1030.7	984.8	1018.3	-0.1	5.1	2.4	2.4	6.2	-1.4	17.9	31	-9.1	17	82	63	74	73	1.1	3.8	2.1	2.3	5.4	6.1	5.3	5.6
IV	1013.3	1026.9	986.9	1018.6	4.5	9.8	5.7	6.4	11.0	2.4	24.1	29	-5.2	16	83	62	80	75	1.6	5.7	2.3	3.2	6.5	6.7	6.7	6.6
V	1011.2	1024.1	998.4	1016.4	8.8	12.8	9.2	10.0	14.2	5.9	25.1	19	-0.1	6	78	58	75	70	2.9	7.1	3.3	4.4	6.3	6.8	5.3	6.1
VI	1010.8	1025.5	997.8	1015.9	14.2	18.6	14.6	15.5	20.6	9.9	28.9	11	5.0	21	77	60	77	71	3.7	9.2	4.0	5.8	5.6	6.5	5.2	5.8
VII	1005.9	1017.4	996.4	1011.0	16.9	21.2	17.2	18.1	22.6	13.8	29.5	8	9.2	3	84	68	81	78	3.3	9.0	4.0	5.4	7.3	6.7	5.2	6.4
VIII	1007.1	1017.9	995.9	1012.2	14.3	19.1	14.8	15.8	20.4	11.7	25.6	12	7.0	30	89	67	87	81	2.0	7.5	2.3	3.9	7.0	7.0	5.4	6.5
IX	1004.7	1017.5	985.9	1009.9	9.9	13.9	10.6	11.2	15.2	7.6	27.1	9	2.1	27	90	72	87	83	1.3	5.1	1.8	2.7	7.2	7.6	7.2	7.3
X	1011.5	1024.7	998.6	1016.7	7.0	11.1	8.5	8.8	12.1	5.5	17.8	10	1.1	16	91	77	86	85	0.9	3.0	1.6	1.8	7.2	8.3	5.6	7.0
XI	1015.1	1036.0	993.8	1020.5	4.3	6.2	4.8	5.0	7.1	3.2	13.9	5	-5.1	29	86	78	83	82	1.1	2.1	1.4	1.5	8.3	8.0	7.6	8.0
XII	1007.6	1026.3	961.7	1013.0	-1.2	0.3	-0.6	-0.5	1.3	-2.5	6.9	5	-10.6	18	91	85	89	88	0.5	0.9	0.6	0.7	7.4	7.9	7.2	7.5
Rok	1009.8	1036.0	961.7	1015.0	6.6	10.2	7.4	7.9	11.4	4.5	29.5	8.VII	-15.0	16.1	86	72	83	80	1.6	4.6	2.1	2.8	7.1	7.3	6.4	6.9

Koszalin

$H_s = 30\,m$ $H_b = 37{,}7\,m$ $h_w = 15{,}5\,m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, ∑=nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Max<0°	Max<0°	Max<-10°	Max>25°	OPAD R 0.1 ≤ < 1.0	1.0 ≤ < 10.0	≥10.0	Wiatr v ≥10 < 15	≥15	≡	≈	◔	●	▯
I	15	4,3	4,5	6,3	2,5	1,4	5	2,0	19,5	3,4	27	4,2	25,5	8,1	3,5	3,4	4	4,8	41,0	9,1	12	23	5	·	·	16	10	·	8	1	5	·	2	20	6
II	3	3,0	6	2,0	1	2,0	3	2,7	2,0	2,6	27,5	3,5	9,5	5,3	1	2,0	1,3	2,8	41,8	12,0	8	15	·	·	·	14	10	1	1	1	6	·	1	11	1
III	9,5	3,6	4,5	3,2	2	5,7	14,5	5,7	2,1	2,7	1,0	4,6	10,5	6,0	5	4,0	1,6	3,5	29,5	11,3	15	23	1	·	·	11	5	1	4	·	5	·	7	6	·
IV	3,2	3,2	6	3,8	1,5	1,7	2,5	2,2	6	3,1	5	2,1	7	6,3	7	4,4	2,3	2,6	32,0	10,7	19	15	·	·	·	14	8	1	1	·	4	·	3	11	2
V	2,8	3,9	9	4,8	5	1,6	7	3,0	6,5	1,8	5	3,0	10	5,7	13,5	4,0	9	3,5	42,1	12,3	4	8	·	·	·	10	6	2	2	·	2	2	4	8	·
VI	2,2	2,3	6,5	2,6	2	2,5	3	4,0	2	2,5	9	3,1	2,5	4,2	15,5	3,9	5	3,2	40,3	11,8	5	·	·	·	3	11	10	1	3	·	1	1	9	4	·
VII	2,3,5	2,1	2	1,5	1,5	2,3	3,5	3,6	2	2,5	12,5	2,4	14,5	3,1	21,5	4,0	1,2	2,5	163,7	50,6	21	·	·	·	5	19	16	6	1	1	3	7	2	8	·
VIII	5,5	2,6	·	·	1	1,0	4	2,5	1,7	3,2	2,1	3,8	23,5	3,8	9	2,6	1,2	2,9	122,9	26,5	16	·	·	·	1	17	15	4	3	·	1	1	·	10	·
IX	3,5	2,6	·	·	·	·	4	2,2	1,6	4,2	18,5	5,7	16,5	6,1	16,5	2,8	1,5	3,8	137,4	38,0	2	·	·	·	·	14	13	4	7	·	2	·	·	6	·
X	·	·	·	·	·	·	0,5	2,0	3,2	3,6	2,4	3,2	2,2	4,5	2,5	5,0	1,2	3,3	40,0	7,8	23	·	·	·	·	13	9	·	6	1	3	·	1	14	·
XI	1	2,0	1,1	4,2	2	2,5	1,1,5	1,9	3,4,5	2,2	3	2,7	8	7,5	8	5,9	1,1	2,9	59,7	23,4	24	11	·	·	·	11	8	2	1	·	1	1	4	1,7	1
XII	3,5	5,1	6,5	4,6	·	·	2	1,5	3,2	3,7	2,0,5	5,0	1,5,5	4,7	2	4,0	1,1	3,8	42,7	16,3	8	2,3	6	2	·	13	8	1	3	·	7	·	1	1,5	3
Rok	1,3,3	2,9	5,6	2,8	1,8,5	1,7	6,0,5	2,8	2,0,8,5	3,0	1,8,3	3,6	1,8,7,5	5,4	1,0,5	3,8	1,4,3	3,3	7,9,3,1	50,6	21.VII	1,1,8	1,2	2	9	1,6,3	1,2,0	2,3	4,0	4	4,0	1,2	3,4	1,3,0	1,3

Kołobrzeg

$H_s = 3\,m$ $H_b = 5{,}4\,m$ $h_w = 17\,m$

I	2	3,0	7	6,0	4,5	3,1	7,5	2,4	9	3,7	4,0	4,7	1,7,5	6,1	3,5	4,1	2	4,5	2,6,9	8,1	12	1,9	5	·	·	11	7	·	–	–	9	·	·	2,3	1
II	3	3,8	7	3,4	1	3,0	6,5	3,0	1,5,5	3,5	2,6,5	3,5	1,3,5	5,0	3	4,3	8	3,4	2,9,7	5,8	8	1,3	·	·	·	1,5	1,0	·	–	–	5	·	·	1,4	1
III	7	4,9	1,0,5	5,7	9	6,1	1,6,5	4,8	1,0,5	3,2	1,2	5,1	1,6	4,5	5,5	3,2	6	4,4	3,3,7	1,0,4	1,5	1,7	·	·	·	1,3	1,0	1	–	–	6	1	3	7	·
IV	1,6	3,5	2,4	5,2	0,5	3,0	1	3,0	3	2,3	4,5	4,1	1,5,5	4,5	1,3,5	3,1	1,2	3,6	2,0,3	6,9	2,7	1,0	·	·	·	1,2	6	·	–	–	5	3	2	1,2	2
V	1,3	3,9	2,1	6,2	2,5	2,4	3	3,8	1	1,0	9	2,1	2,1,5	4,8	1,6	3,0	6	4,0	2,8,6	7,8	1,3	2	·	·	·	1,0	6	·	–	–	4	3	1	1,3	·
VI	9,5	2,7	1,3	3,3	2,5	4,2	1,5	5,0	3	1,3	1,1,5	3,6	3,2,5	3,5	1,0,5	3,3	6	3,1	3,1,9	1,2,9	2,4	·	·	·	2	9	8	1	–	–	1	1	4	5	·
VII	1,1,5	3,1	4,5	2,9	·	·	5	2,8	2	2,5	1,0,5	2,0	3,6	4,0	1,6,5	3,6	7	3,1	9,6,7	2,0,7	2,9	·	·	·	3	1,9	1,6	3	–	–	2	8	·	8	·
VIII	2,5	2,8	2	4,0	4,5	3,4	2	1,0	6	4,5	3,1	3,2	2,8	4,0	1,0	4,1	7	3,4	9,1,2	2,2,3	1,6	·	·	·	1	2,0	1,6	4	–	–	1	3	·	9	·
IX	3	4,3	2	3,0	·	·	2,5	1,4	1,1,5	3,3	2,9	4,8	2,3	5,0	1,6	5,5	3	4,5	7,5,1	1,2,7	2	·	·	·	·	1,9	1,2	2	–	–	1	·	·	1,2	·
X	1,5	3,0	0,5	1,0	1	2,0	4	2,8	1,0,5	4,6	4,4,5	4,9	2,6,5	4,5	4,5	4,8	·	4,6	2,0,0	3,8	23	·	·	·	·	1,3	7	·	–	–	4	·	2,	1,8	·
XI	3	1,0,2	1,3	5,5	4,5	3,4	1,9	3,3	1,9,5	3,1	1,3,5	4,9	1,3	7,9	3,5	6,0	1	4,8	3,6,2	1,3,9	8	1,0	1	·	·	1,2	9	1	–	–	·	·	1	2,3	1
XII	2,5	3,6	8,5	9,9	3,5	3,4	2,5	3,4	1,9	4,1	3,1,5	6,0	1,2,5	7,2	1,0	4,8	3	5,6	2,8,2	9,5	8	1,6	5	1	·	1,6	7	·	–	–	8	·	·	2,0	5
Rok	7,4,5	4,1	1,1,3	4,7	3,3,5	2,8	7,1	3,1	1,1,0,5	3,1	2,6,3,5	4,1	2,5,5,5	5,1	1,1,2,5	4,2	6,1	4,1	5,1,8,5	2,2,3	16.VIII	8,7	1,1	1	6	1,6,9	1,1,4	1,2	–	–	4,3	1,3	1,3	1,6,1	1,0

Żelisławki

$H_s = 6{,}8\,m$ $h_w = 12\,m$

I	·	·	1,5	3,7	4,5	2,3	7	2,1	3	2,5	3,0	6,1	1,9	9,3	9	7,3	1,9	5,0	1,1,2	3,2	3,1	2,6	7	3	·	7	4	·	8	5	–	·	2	1,3	–
II	2	4,8	2	1,5	1	1,0	1,5	2,3	1,6,5	2,9	1,8	4,7	2,0	6,6	5	9,9	1,8	3,9	2,8,5	4,3	1,5	1,6	·	·	·	1,6	1,1	·	5	2	–	·	·	1,2	5
III	1,2	3,6	3,5	2,0	8,5	4,9	2,0,5	3,6	7,5	4,5	1,1	6,0	1,3	8,4	9	6,1	8	4,6	1,9,0	4,7	1,6	2,1	2	·	·	6	6	·	3	·	–	·	9	8	3
IV	2,5	2,9	8,5	2,9	4	2,5	2	2,0	6,5	4,1	2,5	4,8	1,4,5	3,9	1,3	5,1	1,4	3,0	1,8,6	5,1	2,2	8	·	·	·	7	3	·	1	·	–	1	7	7	·
V	2,0,5	2,9	9,5	3,9	6	2,7	5	2,4	5,5	2,4	6	6,4	1,2	5,8	1,3,5	4,1	1,5	3,2	6,2,9	2,2,9	2,0	1	·	·	·	1,0	9	2	2	1	–	2	5	9	·
VI	1,2	1,8	4,5	2,3	4	2,0	4,5	2,6	2,5	2,4	7	3,8	1,9,5	4,6	1,9	5,7	1,7	3,1	2,0,5	6,9	5	·	·	·	5	6	4	·	4	·	–	·	6	7	·
VII	7	2,8	6,5	1,8	5,5	2,5	5	2,9	3,5	3,4	8	3,2	1,8,5	4,1	1,8	5,8	2,1	3,0	8,1,7	2,8,9	1,2	·	·	·	8	1,4	1,2	3	1	·	–	7	3	8	·
VIII	5	2,6	3	1,7	1,5	1,7	2,5	1,8	8	2,6	1,6	4,6	2,9,5	4,5	1,2,5	4,7	1,5	3,3	8,5,4	2,8,7	1,6	·	·	·	4	1,7	1,4	2	1	·	–	3	2	1,0	·
IX	1,5	5,0	·	·	·	·	2	2,0	1,2	3,0	2,6	3,8	2,1,5	4,5	1,7	6,2	1,0	4,0	5,1,0	1,4,8	2,3	·	·	·	2	1,5	1,0	1	7	1	–	·	5	1,1	·
X	0,5	1,7,0	·	·	·	·	·	·	1,3	3,0	3,4	4,0	2,9	5,3	7,5	4,2	9	4,0	9,7	4,8	3,0	·	·	·	·	6	4	·	4	2	–	·	2	8	·
XI	2	9,0	1	4,0	1,0	2,0	7	2,4	2,1,5	2,6	1,9	3,4	1,4,5	6,5	5	8,2	1,0	3,5	1,0,8	5,0	2,9	9	1	·	·	6	4	·	·	·	–	·	2	2,1	1
XII	4	4,0	4,5	5,2	8	1,8	2	4,5	6,5	5,8	3,8	5,9	1,9,5	6,4	7,5	7,3	3	5,4	1,6,9	3,4	3,0	2,5	8	3	·	1,0	8	·	6	3	–	·	3	1,7	1,3
Rok	9,1,5	4,7	4,4,5	2,4	5,3	2,0	5,9	2,4	1,0,6	3,3	2,1,5,5	4,7	2,3,0,5	5,8	1,3,6	6,2	1,5,9	3,8	4,1,0,2	2,8,9	12.VII	1,0,6	1,8	6	1,9	1,2,0	8,9	8	4,2	1,4	–	1,3	4,6	1,3,1	–

Elbląg

$H_s = 3{,}8\,m$ $H_b = 4{,}2{,}8\,m$ $h_w = 14\,m$

I	0,5	1,0	3,5	8,0	6	5,3	1,1	2,8	1,5	3,7	2,4	3,3	2,0,5	3,1	6,5	3,5	6	3,3	2,6,0	6,3	3,1	2,5	9	1	·	1,3	5	·	2	·	7	·	3	1,9	2,3
II	3	4,3	4,5	3,7	2	4,5	8	4,0	2,1	3,6	1,6,5	3,7	1,7	2,5	5	4,7	7	3,3	8,2,2	1,4,2	1	9	·	·	·	1,8	1,5	2	1	·	7	·	·	2,0	1
III	7,5	5,6	4	3,5	1,1	4,4	1,8	6,3	1,4,5	4,0	5,5	3,7	1,3	4,8	1,4,5	4,5	5	4,5	2,8,2	9,9	1,5	2,0	·	·	·	9	7	·	5	1	1	·	6	1,0	4
IV	1,8	5,4	3,5	4,4	6,5	4,2	4,5	3,1	6,5	3,5	5,5	2,1	1,1	2,7	2,5,5	3,4	9	3,4	2,2,5	5,8	1,6	6	·	·	·	8	8	·	1	·	6	4	4	4,2	1
V	2,2,5	4,8	6	5,3	2,5	3,8	6,5	3,4	1,0,5	3,2	4	3,2	9,5	2,8	2,7,5	3,5	4	3,7	2,5,3	9,2	4,1	1	·	·	1	1,4	8	·	4	2	2	3	3	1,1	·
VI	1,5	4,1	6	3,5	4	2,9	3,5	3,9	7,5	3,3	8	3,1	1,7	2,3	2,2	3,0	7	2,9	5,4,2	1,7,6	5	·	·	·	4	9	7	2	·	·	·	3	4	7	·
VII	8,5	3,4	9	4,2	1,1	4,0	5	5,2	5	3,7	1,0,5	3,4	1,4,5	2,4	1,9,5	2,6	1,0	3,0	1,0,5,1	2,9,3	2,7	·	·	·	7	1,5	1,2	4	2	·	4	1,5	·	8	·
VIII	9	3,8	1	3,0	1,5	5,3	5	4,1	1,1,5	3,3	2,1	3,8	1,5,5	2,6	1,4,5	3,1	1,4	2,9	1,5,6,3	3,6,1	1,6	·	·	·	3	1,7	1,7	6	1	1	3	7	1	1,0	·
IX	1	8,0	·	·	1,5	2,3	1,1	4,5	1,7,5	5,1	1,5,5	5,5	2,0,5	3,9	1,5	3,3	8	4,0	1,5,7,5	2,5,0	8	·	·	·	2	1,9	1,7	9	5	·	2	3	·	1,1	·
X	·	·	·	·	0,5	3,0	5,5	4,4	2,4,5	4,2	3,1	4,2	2,0	2,8	9,5	2,9	2	3,7	2,6,0	9,1	3,0	·	·	·	·	1,0	8	·	1	·	8	·	2	1,1	·
XI	3	7,7	9,5	5,9	8	5,1	1,3,5	5,6	1,7	3,7	1,4	3,3	1,8,5	3,1	3,5	7,7	3	4,3	2,6,6	8,0	27,28	9	1	·	·	7	5	·	5	·	2	·	·	2,1	·
XII	4,5	6,7	3	6,3	5,5	7,6	5,5	3,9	2,0	4,9	3,0,5	4,0	1,2	3,9	6	5,7	6	4,5	2,2,5	6,0	1,3	2,3	1,1	1	·	1,2	7	·	1,0	·	4,0	·	3	1,7	4
Rok	9,2,5	4,6	5,0	4,0	6,0	4,4	9,7	4,3	1,7,0,5	3,8	1,8,6	3,6	1,8,9	3,1	1,6,9	4,0	8,1	3,6	7,4,2,4	3,6,1	16.VIII	9,3	2,1	2	1,7	1,5,1	1,1,6	2,3	3,7	4	5,2	3,5	2,6	1,5,7	3,3

Kowale Oleckie

$\varphi = 54°10'$ $\lambda = 22°25'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.8	-1.2	-2.2	-2.1	–	-4.7	–	–	-20.5	16	–	–	–	–	–	–	–	–	9.7	8.9	9.3	9.3
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	-2.7	2.4	-0.7	-0.4	–	-4.7	–	–	-13.8	17	–	–	–	–	–	–	–	–	8.1	6.8	6.0	7.0
IV	–	–	–	–	4.4	10.8	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.2	5.8	6.5
V	–	–	–	–	9.0	12.8	8.9	9.9	14.4	4.7	26.5	19	-2.2	2	–	–	–	–	–	–	–	–	6.7	7.3	5.8	6.6
VI	–	–	–	–	14.0	18.3	13.6	14.9	20.1	8.9	27.3	11	3.3	21	–	–	–	–	–	–	–	–	5.8	6.3	5.1	5.7
VII	–	–	–	–	16.9	20.5	16.7	17.7	24.9	12.4	27.0	8	9.1	4,7	–	–	–	–	–	–	–	–	5.4	5.6	8.6	6.5
VIII	–	–	–	–	14.6	18.3	14.7	15.6	19.4	11.1	28.1	12	5.6	24	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.5	13.5	9.2	10.4	14.2	6.7	25.3	9	1.1	17	–	–	–	–	–	–	–	–	8.5	8.1	7.3	8.0
X	–	–	–	–	6.1	10.4	7.2	7.7	10.8	4.5	15.7	11	0.7	3	–	–	–	–	–	–	–	–	8.0	8.3	8.3	8.2
XI	–	–	–	–	2.5	4.2	2.6	3.0	5.3	0.8	13.5	6	-10.6	30	–	–	–	–	–	–	–	–	9.6	9.5	8.7	9.3
XII	–	–	–	–	-2.8	-1.3	-2.6	-2.3	-0.5	-5.0	4.9	5	-13.3	18	–	–	–	–	–	–	–	–	8.8	8.6	7.5	8.3
Rok	–	–	–	–	–	–	–	–	–	–	28.1	12.VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Płocko

$\varphi = 54°09'$ $\lambda = 16°50'$

I	–	–	–	–	-0.6	0.8	0.0	0.0	2.1	-2.4	10.5	6	-13.4	16	–	–	–	–	–	–	–	–	9.4	8.2	7.6	8.4
II	–	–	–	–	0.8	4.0	2.2	2.3	5.2	-0.4	9.5	5	-7.0	27	9.5	8.3	9.2	9.0	0.4	1.5	0.6	0.8	8.6	7.4	7.6	7.9
III	–	–	–	–	0.1	5.8	1.9	2.4	7.0	-2.2	17.1	31	-7.4	9	–	–	–	–	–	–	–	–	6.7	5.0	3.5	5.1
IV	–	–	–	–	3.2	9.5	4.5	5.4	10.9	0.1	23.1	28	-5.4	15	–	–	–	–	–	–	–	–	6.7	6.6	5.4	6.2
V	–	–	–	–	7.9	12.5	7.8	9.0	13.9	3.8	23.6	19	-1.8	6,27	–	–	–	–	–	–	–	–	6.1	7.2	4.5	5.9
VI	–	–	–	–	12.9	19.5	15.0	15.6	21.0	8.7	29.5	18	2.2	3	–	–	–	–	–	–	–	–	4.4	5.0	4.0	4.5
VII	–	–	–	–	15.9	20.5	17.3	17.8	22.9	12.7	29.4	4	6.2	7	8.9	6.9	8.2	8.0	2.0	8.4	3.7	4.7	7.3	7.2	6.5	7.0
VIII	–	–	–	–	14.3	18.4	14.7	15.5	19.9	11.5	26.0	11	7.2	24	9.0	7.1	8.9	8.3	1.7	6.6	1.9	3.4	6.5	7.9	6.1	6.8
IX	–	–	–	–	10.0	14.0	10.3	11.2	15.0	7.2	26.0	8	0.2	26	8.9	7.3	8.8	8.3	1.4	4.8	1.6	2.6	7.5	7.4	6.3	7.1
X	–	–	–	–	7.9	11.3	9.1	9.4	12.0	6.3	19.1	10	1.2	2	9.1	7.6	8.7	8.5	1.1	3.4	1.5	2.0	7.9	6.7	6.9	7.2
XI	–	–	–	–	3.3	5.8	3.9	4.2	6.9	1.3	15.1	5	-7.3	30	9.0	8.1	8.9	8.7	0.8	1.9	0.9	1.2	8.4	8.3	7.2	8.0
XII	–	–	–	–	-4.0	0.5	-0.2	-0.2	1.9	-2.6	7.1	5	-12.4	18	–	–	–	–	–	–	–	–	8.4	8.5	7.4	8.1
Rok	–	–	–	–	6.2	10.2	7.2	7.7	11.6	3.7	29.5	18.VI	-13.4	16.1	–	–	–	–	–	–	–	–	7.3	7.1	6.1	6.8

Lidzbark Warmiński

$\varphi = 54°08'$ $\lambda = 20°36'$

I	–	–	–	–	-2.4	-0.3	-1.7	-1.5	1.2	-4.0	8.8	6	-20.7	16	–	–	–	–	–	–	–	–	8.3	6.9	8.6	7.9
II	–	–	–	–	1.1	3.2	1.6	1.9	4.3	-0.2	8.5	14	-5.0	25	–	–	–	–	–	–	–	–	8.6	6.9	9.2	8.2
III	–	–	–	–	-1.5	4.4	1.0	1.2	6.0	-2.9	18.0	31	-15.9	17	–	–	–	–	–	–	–	–	5.9	3.7	5.4	5.0
IV	–	–	–	–	3.7	11.3	5.8	6.6	12.8	0.7	25.8	29	-6.3	14	–	–	–	–	–	–	–	–	5.0	3.5	5.7	4.7
V	–	–	–	–	8.3	13.0	9.3	10.0	14.9	4.4	26.0	19	-2.2	2	–	–	–	–	–	–	–	–	4.7	3.9	4.6	4.4
VI	–	–	–	–	13.8	18.8	13.9	15.1	20.8	9.1	28.3	11	2.8	21	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	15.8	21.1	16.6	17.5	22.8	12.7	29.3	8	7.7	4	–	–	–	–	–	–	–	–	4.5	4.0	5.0	4.5
VIII	–	–	–	–	14.0	18.9	14.5	15.5	20.6	11.1	28.3	12	6.6	30	–	–	–	–	–	–	–	–	4.1	4.1	5.3	4.5
IX	–	–	–	–	9.7	13.7	10.0	10.8	14.9	7.4	26.3	9	3.0	27	–	–	–	–	–	–	–	–	6.2	5.2	5.5	5.6
X	–	–	–	–	6.7	10.7	8.0	8.4	12.0	4.7	19.7	10	0.7	2	–	–	–	–	–	–	–	–	5.5	4.2	5.1	4.9
XI	–	–	–	–	3.5	5.2	4.0	4.2	7.0	2.2	14.6	6	-7.6	29	–	–	–	–	–	–	–	–	7.9	6.9	7.9	7.6
XII	–	–	–	–	-2.2	-0.5	-1.6	-1.5	1.2	-3.8	6.6	5	-12.7	18	–	–	–	–	–	–	–	–	6.8	5.8	6.4	6.3
Rok	–	–	–	–	5.9	10.0	6.8	7.4	11.5	3.4	29.3	8.VII	-20.7	16.1	–	–	–	–	–	–	–	–	–	–	–	–

Kościerzyna

$\varphi = 54°06'$ $\lambda = 17°58'$

I	–	–	–	–	-1.6	0.0	-1.2	-1.0	0.9	-4.3	9.4	6	-16.4	16	–	–	–	–	–	–	–	–	9.6	8.5	8.8	9.0
II	–	–	–	–	0.3	3.1	1.4	1.6	4.0	-1.1	9.1	2	-6.7	25	–	–	–	–	–	–	–	–	9.3	8.4	9.4	9.0
III	–	–	–	–	-0.8	4.5	0.7	1.3	5.6	-2.8	13.7	13	-9.2	17	–	–	–	–	–	–	–	–	6.4	6.5	4.8	5.9
IV	–	–	–	–	3.8	9.4	3.6	5.1	10.4	0.1	22.3	28	-7.1	15	–	–	–	–	–	–	–	–	6.9	7.4	6.3	6.9
V	–	–	–	–	8.4	12.3	7.1	8.7	13.5	3.4	23.4	19	-3.2	6	–	–	–	–	–	–	–	–	6.6	7.5	5.7	6.6
VI	–	–	–	–	14.3	19.2	13.4	15.1	20.6	8.3	28.7	18	4.6	17	–	–	–	–	–	–	–	–	5.0	6.5	5.3	5.6
VII	–	–	–	–	16.3	20.5	15.5	17.0	21.8	12.6	29.1	8	8.3	7	–	–	–	–	–	–	–	–	7.9	7.1	6.8	7.3
VIII	–	–	–	–	13.9	18.0	13.8	14.9	19.2	10.6	23.7	11	6.8	23	–	–	–	–	–	–	–	–	6.7	7.3	7.4	7.1
IX	–	–	–	–	8.9	13.0	9.2	10.1	14.3	6.4	25.8	8	-0.1	26,27	–	–	–	–	–	–	–	–	8.2	8.1	6.9	7.7
X	–	–	–	–	7.2	10.8	7.6	8.3	11.5	4.8	17.6	19	-0.1	2	–	–	–	–	–	–	–	–	8.9	7.9	7.6	8.1
XI	–	–	–	–	3.0	5.4	3.3	3.8	6.5	1.4	14.3	5	-7.4	30	–	–	–	–	–	–	–	–	9.6	8.6	8.2	8.8
XII	–	–	–	–	-1.9	-0.6	-1.5	-1.4	0.9	-4.1	6.3	8	-15.4	18	–	–	–	–	–	–	–	–	9.5	8.8	7.5	8.6
Rok	–	–	–	–	6.0	9.6	6.1	7.0	10.8	2.9	29.1	8.VII	-16.4	16.1	–	–	–	–	–	–	–	–	7.9	7.7	7.1	7.6

Kowale Oleckie

$H_s = 210\ m$ $h_w = 10{,}5\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D. v m/D																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				R			Wiatr v		≡								
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0	Max<0	Min<-10	Max>25	0,1 ≤ R < 1,0	1,0 ≤ R < 10	R ≥ 10,0	10 < v < 15	v ≥ 15									
I	·	·	8	6,5	8	5,0	11,5	4,8	6,5	3,5	23,5	4,0	26,5	6,0	9	4,1	·	4,9	48,2	17,4	6	27	–	5	·	12	10	2	5	1	–	·	·	25	–				
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	8	3,8	8,5	1,8	7,5	4,7	12	6,9	8,5	4,5	7,5	3,9	13	6,1	1,5	4,1	13	3,9	28,3	6,7	14	26	–	4	–	10	8	·	6	·	–	·	4	13	–				
IV	16	3,5	5	3,1	4,5	1,7	5,5	2,9	11	4,1	12	3,7	16,5	3,0	11,5	3,9	8	3,1	33,4	8,1	30	–	–	–	–	14	7	·	1	·	–	1	2	12	–				
V	26,5	3,4	6,5	4,5	11,5	2,6	10	1,7	8,5	1,6	7	3,8	12,5	2,7	7,5	2,6	3	2,8	49,3	21,0	19	4	·	·	1	9	9	1	1	·	–	1	3	12	–				
VI	14,5	3,4	3,5	2,3	1	2,5	9	3,8	7	3,0	13,5	3,2	22	3,5	16,5	3,2	3	3,2	49,7	13,5	24	·	·	·	4	8	8	1	·	·	–	1	1	5	–				
VII	5,5	1,9	7	2,3	5	1,8	11	2,7	8	2,9	13	3,0	23	3,2	13,5	2,1	7	2,5	105,9	19,4	18	·	·	·	4	16	16	3	·	·	–	1	1	11	–				
VIII	3	3,3	1,0	2,6	3,5	2,2	7	4,7	12	2,6	12	4,6	17,5	7,4	2,1	3,8	7	4,0	164,4	57,1	18	·	·	·	1	13	13	4	3	1	–	·	–	–	–				
IX	3	1,3	·	·	·	·	7	2,0	8,5	3,4	30,5	3,7	22	4,1	1,5	3,3	4	3,3	254,4	62,4	18	·	·	·	1	13	13	8	1	·	–	·	1	17	–				
X	1	1,5	1,5	1,7	1	1,0	1	4,0	2,5	2,7	38,5	2,5	23,5	3,2	0,5	2,0	1	2,7	18,9	6,8	5	·	·	·	·	5	4	·	·	·	–	·	1	19	–				
XI	9,5	6,2	4	3,5	8	4,1	25,5	6,0	9	2,4	5,5	2,6	14,5	3,1	1,0	4,6	4	4,3	57,0	13,6	27	14	1	2	·	10	8	2	5	·	–	·	1	26	–				
XII	3,5	3,6	·	·	6	5,3	·	·	22,5	4,4	36,5	6,5	14,5	5,9	5	4,7	5	5,4	39,4	12,8	8	29	14	6	·	12	8	1	11	·	–	·	1	23	–				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	62,4	18.IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Płocko

$H_s = 125\ m$ $h_w = 14\ m$

I	·	·	8	3,6	5	1,4	4,5	2,2	17,5	2,7	2,8	5,6	1,3	4,4	2	1,0	1,5	3,3	44,3	15,0	5	23	7	2	·	13	10	1	3	·	–	·	2	21	–				
II	3	1,3	1	1,0	6	2,5	1,1	2,6	1,8	2,4	1,6	4,2	5	2,2	2	3,5	2,2	2,1	46,3	11,0	8	1,5	·	·	·	1,8	9	1	2	·	–	·	1	17	–				
III	9	3,1	5	1,2	9	5,0	23,5	5,1	5,5	2,2	1,3	5,8	10,5	5,3	3,5	4,9	1,4	3,9	22,5	10,0	15	2,1	1	·	·	9	6	1	2	1	–	·	9	7	–				
IV	16,5	2,2	1,0	2,3	9	1,6	1	2,0	4	2,8	2,5	2,6	13,5	3,3	6,5	1,8	2,7	1,7	51,0	15,2	16	1,4	·	·	·	1,4	12	1	·	·	–	·	7	12	–				
V	1,1	2,7	1,2	5,2	2,5	1,8	4,5	2,8	1	4,0	8	3,0	1,4	4,1	7	2,6	3,3	2,3	57,2	16,5	4	4	·	·	·	1,4	12	1	4	·	–	3	4	6	–				
VI	12,5	2,2	2,5	2,2	1	2,0	6	2,3	1	2,0	1,3	3,6	2,5	2,9	4	2,0	2,5	2,0	34,9	12,0	9	·	·	·	7	9	9	1	4	·	–	2	9	6	–				
VII	4	5,0	2	2,0	·	·	2	1,0	3	2,7	1,7	4,4	2,7	3,3	2	1,5	3,6	2,2	104,7	19,6	21	·	·	·	10	1,6	14	4	·	·	–	4	2	12	–				
VIII	2	2,0	1	3,0	0,5	1,0	5	4,1	12,5	3,8	2,4	4,4	1,8	3,5	4	2,9	2,6	2,7	108,7	17,5	14	·	·	·	1	2,2	17	3	1	·	–	4	2	11	–				
IX	·	·	·	·	1	8,0	2	2,5	1,9	4,5	2,2	5,0	1,7	3,6	6	5,2	2,3	3,3	106,8	16,5	28	·	·	·	1	2,0	18	5	5	·	–	1	1	12	–				
X	·	·	·	·	·	·	8	2,6	3,0	3,8	2,4	4,8	1,4	3,9	2	1,5	1,5	3,3	38,9	5,5	6	·	·	·	·	1,6	9	·	1	·	–	·	1	15	–				
XI	3,5	3,7	5,5	3,6	9	2,6	10,5	2,8	1,4,5	3,9	4	4,0	1,1	7,6	2	6,0	3,0	2,8	49,2	12,5	27	1,1	1	·	·	10	7	2	3	·	–	·	2	19	–				
XII	1	3,0	3	5,0	7	3,0	6	2,8	22,5	3,9	2,6,5	5,0	8	4,1	1	4,0	1,8	3,4	45,2	10,0	8,30	20	8	3	·	10	9	2	2	·	–	·	2	19	–				
Rok	62,5	2,1	5,0	2,4	5,0	2,4	8,4	2,7	1,4,8,5	3,2	1,9,8	4,4	1,7,6	4,0	4,2	3,1	2,8,4	2,8	709,7	19,6	21.VII	108	17	5	19	171	132	22	29	1	–	16	42	157	–				

Lidzbark Warmiński

$H_s = 90\ m$ $h_w = 12\ m$

I	·	·	5	4,4	5,5	3,3	10,5	3,0	1,4	5,6	3,9	8,3	1,4	6,0	3	1,5,0	2	6,5	37,2	8,5	13	2,5	8	3	·	11	9	·	11	6	–	·	1	18	–				
II	2,5	2,6	9	2,2	·	·	8	5,9	2,2	4,1	3,1,5	4,7	6,5	6,1	3,5	5,7	1	4,4	50,8	12,5	18	1,3	2	·	·	1,8	12	1	2	·	–	·	·	17	–				
III	6,5	4,0	8,5	2,3	12,5	6,6	8,5	7,1	16,5	6,4	1,5	5,5	1,4	7,2	9,5	6,6	2	5,8	24,2	6,1	15	2,3	4	1	·	9	7	·	8	3	–	·	5	4	–				
IV	22,5	5,0	17,5	3,0	1	5,0	1	4,5	7,5	3,5	20,5	4,3	6,5	6,6	11,5	4,2	2	4,2	16,6	7,8	30	1,3	·	·	1	12	5	·	5	·	–	2	7	4	–				
V	17,5	3,4	11,5	3,0	1,5	3,0	8,5	3,4	11,5	2,9	12,5	5,4	10,5	5,3	19,5	3,2	·	3,7	31,4	10,6	10	2	·	·	1	13	7	1	3	·	–	3	8	6	–				
VI	8	2,6	11,5	2,5	3,5	3,1	8,5	5,0	6,5	2,5	1,9	4,3	2,3	4,1	9	2,8	1	3,6	43,1	9,9	10	·	·	·	3	10	7	·	·	·	–	2	–	–	–				
VII	7,5	2,9	1,2	2,5	7	3,8	5,5	4,3	9,5	3,1	2,0	4,3	2,0	3,9	8,5	3,9	3	3,5	127,2	44,6	12	·	·	·	5	1,5	13	3	2	·	–	6	5	2	–				
VIII	6	3,0	3	1,3	1	4,0	6	3,2	1,9	3,9	2,9	5,1	1,7	4,3	7	3,3	5	3,9	144,4	61,5	17	·	·	·	2	2,1	12	2	2	·	–	1	3	5	–				
IX	·	·	·	·	·	·	5	4,1	2,6,5	4,6	3,0	4,5	2,2,5	7,2	5	5,5	1	5,2	152,1	27,8	24	·	·	·	1	1,7	15	6	7	1	–	·	2	7	–				
X	·	·	1	2,0	·	·	2,5	7,4	2,7	4,1	5,0	4,9	8,5	6,8	2	7,5	2	4,8	19,7	4,5	30	·	·	·	·	1,0	7	·	3	·	–	·	3	2	–				
XI	6	8,7	5	4,1	10,5	2,9	11	4,7	1,8	3,1	18,5	3,9	12	8,5	3	5,0	6	4,4	23,9	11,2	28	12	1	·	·	5	5	1	5	1	–	·	2	19	–				
XII	4	3,5	8,5	3,8	3,5	4,1	4	3,6	1,5	4,3	4,0,5	5,8	12	10,6	0,5	6,0	5	5,4	21,7	7,6	8	2,3	7	5	·	1,3	6	·	7	3	–	·	4	11	–				
Rok	80,5	3,0	92,5	2,6	4,6	3,0	7,9	4,7	1,9,3	4,0	3,2,5,5	5,1	1,6,6,5	6,4	8,2	5,7	3,0	4,6	69,2,3	61,5	17.VIII	111	22	9	13	1,5,4	105	14	55	14	–	14	–	–	–				

Kościerzyna

$H_s = 180\ m$ $h_w = 10\ m$

I	6	4,0	6	3,0	3	6,0	·	·	·		2	1,5	4,0	2,4	1,2	2,0	2,4	1,8	2,0,8	8,7	5	2,6	1,3	5	·	8	7	·	·	·	1,7	·	·	2,4	–				
II	5	1,0	·	·	·	·	1	2,0	2,5	3,8	6,5	3,3	1,9	1,8	1,4	1,5	3,6	1,1	5,2,0	1,1,1	9	2,0	1	·	·	1,4	12	1	·	·	1,0	·	·	2,3	–				
III	1,0	1,4	6	2,5	9	3,6	6	3,7	1,0	3,0	1	2,0	2,0	2,2	9	1,0	2,2	1,8	2,5,4	9,8	15	2,2	3	·	·	9	7	·	4	·	4	·	4	12	–				
IV	2,1	1,4	1,0,5	2,9	2	1,0	1	1,0	1	2,0	·	·	1,2	1,8	1,4,5	1,2	2,8	1,2	3,1,3	1,4,8	23	1,3	·	·	·	1,3	6	1	·	·	5	2	4	1,6	–				
V	1,8,5	1,1	1,1	3,3	1	1,0	2	2,5	2	2,0	·	·	1,1	2,5	1,4,5	1,1	3,3	1,2	3,2,3	2,0,3	9	3	·	·	·	1,0	5	1	·	·	3	2	2	1,2	–				
VI	1,2	1,0	2	1,0	2	1,5	1	1,0	1	1,0	·	·	7	1,6	2,0	1,2	4,5	0,6	3,5,7	2,4,2	9	·	·	·	6	9	5	1	·	·	3	1	4	9	–				
VII	1,1,5	1,0	6	1,5	3	2,0	·	·	1	1,0	2	1,0	7	1,6	2,1,5	1,2	4,1	0,7	1,6,2,6	2,9,3	1,6	·	·	·	7	1,9	1,4	7	·	·	2	3	·	1,3	–				
VIII	1,0	1,0	0,5	2,0	·	·	·	·	3	1,0	8	3,0	1,9	1,8	1,1,5	1,3	4,1	0,9	1,2,0,1	3,0,1	1,6	·	·	·	·	1,6	1,3	5	·	·	2	1	·	1,2	–				
IX	1	1,0	·	·	·	·	·	·	·	·	1,5	3,1	2,4	2,0	1,0	1,9	4,0	1,3	9,3,6	1,6,0	2,7	2	·	·	2	2,1	1,6	3	·	·	5	1	·	1,5	–				
X	1	1,0	·	·	·	·	·	·	2	1,5	1,7	3,0	3,7	2,0	6	1,5	3,0	1,5	1,8,6	3,9	3,0	1	·	·	·	1,1	8	·	·	·	2,0	·	·	1,5	–				
XI	9	1,3	1,1	3,0	1	3,0	·	·	3	1,7	3	2,3	2,0	1,6	5	2,6	3,8	1,2	3,2,3	7,1	2,4	1,4	1	·	·	1,0	7	·	·	·	1,4	·	·	2,4	–				
XII	2	3,0	8	5,1	3	1,0	1	3,0	2	4,0	5,5	4,0	2,9,5	1,9	1,2	1,4	3,0	1,7	3,6,1	1,4,0	3,0	2,4	9	6	·	6	5	2	1	1	1,1	·	·	2,0	–				
Rok	1,0,7	1,3	6,1	2,0	2,4	1,6	1,2	1,1	2,7,5	1,8	6,0	1,9	2,4,5,5	1,9	1,5,0	1,5	4,0,8	1,2	6,6,6,8	3,0,1	1,6.VIII	1,2,5	2,7	1,1	1,5	1,4,6	1,0,5	2,1	5	1	9,6	1,0	1,4	1,9,5	–				

Kętrzyn

$\varphi = 54°06'$ $\lambda = 21°21'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δm				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P 0	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1005.	1018.7	987.9	1018.8	-2.0	-0.4	-1.0	-1.1	0.8	-3.8	8.4	6	-20.7	16	90	86	87	88	0.5	0.8	0.7	0.7	8.1	8.2	7.3	7.5
II	996.5	1020.4	973.4	1009.9	1.2	2.8	1.7	1.8	3.9	0.1	7.8	2	-4.5	28	93	83	88	88	0.5	1.3	0.9	0.9	8.7	8.4	6.9	8.0
III	1005.1	1022.0	976.6	1018.7	-1.4	3.9	1.0	1.1	5.2	-3.1	17.0	31	-13.6	17	80	59	74	71	1.1	3.9	1.9	2.3	6.0	6.0	5.1	5.7
IV	1005.1	1018.6	979.3	1018.4	4.4	11.7	6.4	7.2	13.2	1.8	24.9	27,29	-5.2	14	85	51	77	71	1.4	8.0	2.5	4.0	5.6	5.8	5.4	5.6
V	1003.0	1015.2	990.6	1016.1	8.5	13.1	9.3	10.0	14.8	4.9	25.6	19	-0.9	2	84	62	78	75	1.9	6.6	2.7	3.7	5.9	6.5	5.2	5.9
VI	1003.1	1016.9	988.7	1016.0	14.4	18.6	13.8	15.2	20.3	9.4	27.5	11	3.9	21	80	63	83	75	3.3	8.6	2.8	4.9	4.8	6.9	4.5	5.4
VII	998.5	1009.5	989.0	1011.2	16.2	21.2	16.6	17.6	22.7	12.9	28.9	8	8.8	3	89	69	87	82	2.2	8.2	2.7	4.4	6.9	6.7	5.5	6.4
VIII	999.6	1009.2	988.4	1012.4	14.3	18.7	14.7	15.6	20.1	11.6	27.8	12	7.2	9	89	70	88	82	1.8	6.9	2.1	3.6	5.7	7.4	5.4	6.2
IX	997.0	1009.3	980.2	1009.8	9.9	14.0	10.4	11.2	15.0	7.9	26.0	9	3.1	27	92	73	88	84	0.9	5.0	1.6	2.5	7.1	7.4	5.4	6.6
X	1003.9	1017.7	991.1	1017.1	6.6	11.0	8.3	8.6	12.0	5.3	18.8	10	1.7	3	92	77	87	85	0.8	3.1	1.4	1.8	6.9	8.2	5.6	6.9
XI	1007.3	1028.7	982.9	1020.7	3.7	5.3	4.1	4.3	6.4	2.2	14.6	6	-8.6	29	90	82	88	87	0.8	1.6	1.0	1.1	8.8	8.9	8.7	8.8
XII	999.5	1017.5	952.9	1015.1	-2.0	-0.4	-1.4	-1.3	0.6	-3.6	6.1	5	-12.1	19	87	84	88	86	0.7	0.9	0.7	0.8	6.8	8.5	6.6	7.3
Rok	1002.0	1028.7	952.9	1015.1	6.1	10.0	7.0	7.5	11.2	3.8	28.9	8.VII	-20.7	16.1	88	72	84	81	1.3	4.6	1.8	2.6	6.8	7.4	5.9	6.7

Suwałki

$\varphi = 54°06'$ $\lambda = 22°57'$

I	997.2	1011.0	979.6	1018.7	-2.8	-1.5	-1.9	-2.0	-0.1	-4.7	7.0	9	-18.4	16	92	90	91	91	0.4	0.6	0.5	0.5	8.2	8.7	8.5	8.5
II	989.2	1011.2	966.6	1010.4	-0.1	1.6	0.5	0.6	2.8	-4.2	6.5	9	-9.2	28	94	87	90	90	0.4	0.9	0.6	0.6	9.4	9.1	8.1	8.9
III	997.4	1015.7	968.8	1018.8	-3.2	2.2	-0.7	-0.6	4.0	-4.8	16.2	31	-14.5	4	84	62	77	74	0.8	3.3	1.5	1.9	6.7	6.2	4.9	5.9
IV	997.3	1011.0	979.9	1018.1	3.9	11.1	6.4	7.0	12.8	1.6	24.1	29,30	-6.7	13	87	50	76	71	1.1	7.8	2.5	3.8	6.0	6.7	6.1	6.3
V	995.2	1006.9	982.4	1015.6	9.2	13.9	9.6	10.6	15.6	5.2	26.6	19	-1.6	6	79	55	78	71	2.5	8.0	2.7	4.4	5.9	7.1	5.9	6.3
VI	995.5	1008.9	982.4	1015.6	14.5	19.5	14.8	15.9	21.1	9.4	28.1	11	3.4	21	75	55	76	69	4.3	10.7	4.2	6.4	5.8	6.7	5.1	5.9
VII	991.3	1002.2	981.2	1011.1	16.1	21.2	16.8	17.7	22.9	12.7	27.7	8	8.0	4	85	60	83	76	2.8	10.6	3.3	5.6	7.6	7.6	6.3	7.2
VIII	992.0	1000.5	979.9	1012.0	13.9	18.6	14.3	15.3	20.1	11.2	28.7	12	5.7	24	90	67	87	81	1.7	7.7	2.1	3.8	6.7	8.0	5.8	6.8
IX	989.1	1002.3	970.0	1009.4	9.0	13.5	9.5	10.4	14.6	6.7	25.7	9	1.0	17	92	72	89	84	1.0	4.8	1.4	2.4	7.8	8.8	5.2	7.3
X	996.3	1010.5	982.8	1017.0	5.8	10.0	7.3	7.6	11.2	4.7	17.2	10	0.6	3	95	78	90	88	0.5	2.8	1.1	1.5	8.2	8.1	5.5	7.3
XI	999.6	1020.9	974.8	1021.0	2.5	4.3	3.0	3.2	5.8	1.1	13.6	6	-10.0	30	93	85	90	89	0.5	1.3	0.8	0.9	9.1	8.9	7.9	8.6
XII	991.7	1009.4	946.7	1013.1	-3.3	-1.7	-2.8	-2.6	-0.4	-5.2	4.7	5	-14.4	19	91	86	90	89	0.4	0.7	0.4	0.5	7.7	8.4	7.0	7.7
Rok	994.3	1020.9	946.7	1015.1	5.5	9.4	6.4	6.9	10.9	3.1	28.7	12.VIII	-18.4	16.1	88	74	85	81	1.4	4.9	1.8	2.7	7.4	7.9	6.4	7.2

Sejny

$\varphi = 54°06'$ $\lambda = 23°21'$

I	–	–	–	–	-2.3	-0.9	-1.4	-1.5	0.4	-4.3	7.0	9	-18.3	16	–	–	–	–	–	–	–	–	7.1	7.6	7.5	7.4
II	–	–	–	–	0.0	2.0	0.6	0.8	3.1	-1.0	7.0	2	-9.7	28	–	–	–	–	–	–	–	–	8.0	7.6	7.2	7.6
III	–	–	–	–	-3.3	2.8	-0.7	-0.5	4.1	-5.3	16.0	31	-15.8	17	–	–	–	–	–	–	–	–	5.1	4.0	4.7	4.8
IV	–	–	–	–	3.9	11.9	6.5	7.2	12.9	1.4	25.9	28	-6.6	13	–	–	–	–	–	–	–	–	5.5	5.0	6.6	5.7
V	–	–	–	–	9.1	14.4	9.4	10.6	15.9	4.9	25.9	19	-3.1	6	–	–	–	–	–	–	–	–	4.7	5.9	6.7	5.8
VI	–	–	–	–	14.5	19.6	14.2	15.6	20.8	9.0	28.4	11	4.9	15,21	–	–	–	–	–	–	–	–	4.6	5.2	5.5	5.1
VII	–	–	–	–	16.5	21.9	16.3	17.8	22.7	12.2	27.4	20	6.4	7	–	–	–	–	–	–	–	–	6.3	6.8	6.9	6.7
VIII	–	–	–	–	14.1	19.1	14.3	15.4	19.9	11.1	29.4	12	4.9	24	–	–	–	–	–	–	–	–	6.5	7.6	6.7	6.9
IX	–	–	–	–	9.3	14.0	9.7	10.7	14.7	7.0	25.9	9	2.0	17	–	–	–	–	–	–	–	–	7.4	8.0	5.9	7.1
X	–	–	–	–	6.1	10.2	7.6	7.9	11.2	4.5	17.5	10	1.0	3	–	–	–	–	–	–	–	–	8.1	7.7	6.6	7.5
XI	–	–	–	–	2.8	4.6	3.2	3.4	6.0	1.1	13.0	6	-9.7	29,30	–	–	–	–	–	–	–	–	8.6	8.0	7.8	8.1
XII	–	–	–	–	-3.1	-1.2	-2.7	-2.4	0.0	-5.3	4.5	5	-14.9	16	–	–	–	–	–	–	–	–	7.4	7.4	6.5	7.1
Rok	–	–	–	–	5.6	9.9	6.4	7.1	11.0	2.9	29.4	12.VIII	-18.3	16.1	–	–	–	–	–	–	–	–	6.6	6.7	6.6	6.6

Tczew

$\varphi = 54°05'$ $\lambda = 18°48'$

I	–	–	–	–	-0.9	1.2	-0.3	-0.1	2.2	-2.4	10.1	6	-10.8	16	90	85	89	88	0.6	1.0	0.7	0.8	6.6	6.7	6.3	6.5
II	–	–	–	–	1.7	4.5	2.7	2.9	5.2	0.8	9.3	14	-3.6	25	92	80	88	87	0.6	1.7	0.9	1.1	7.2	5.7	5.4	6.1
III	–	–	–	–	0.3	5.7	2.4	2.7	6.7	-0.9	17.7	31	-6.3	9	–	–	–	–	–	–	–	–	5.4	5.6	4.5	5.2
IV	–	–	–	–	4.4	10.5	5.2	6.3	11.5	2.6	24.4	29	-3.6	13	–	–	–	–	–	–	–	–	5.0	5.6	5.3	5.3
V	–	–	–	–	9.3	13.2	9.1	10.2	15.3	5.7	24.5	20	-0.7	6	78	64	80	74	2.7	6.2	2.5	3.8	4.8	6.5	3.9	5.1
VI	–	–	–	–	14.1	19.6	15.2	16.0	21.7	10.8	29.4	18	8.3	14	81	61	80	74	3.3	9.9	3.4	5.5	4.0	5.1	3.6	4.2
VII	–	–	–	–	16.9	22.4	17.4	18.5	23.4	14.4	34.2	8	10.5	29	–	–	–	–	–	–	–	–	6.3	6.0	4.9	5.7
VIII	–	–	–	–	14.8	20.1	15.6	16.5	21.3	12.7	26.8	11	7.9	31	–	–	–	–	–	–	–	–	4.3	6.3	5.5	5.4
IX	–	–	–	–	9.9	14.6	11.0	11.6	16.0	8.1	26.9	8	3.2	27	87	71	83	80	1.6	5.5	2.3	3.1	6.2	7.3	6.1	6.5
X	–	–	–	–	7.5	12.1	8.6	9.2	13.0	5.9	18.9	19	2.6	2	92	75	88	85	0.8	3.6	1.4	1.9	5.9	5.6	4.8	5.4
XI	–	–	–	–	4.2	6.5	4.8	5.1	7.4	3.1	14.9	5	-5.6	30	90	82	87	86	0.8	1.8	1.1	1.2	8.3	7.7	6.4	7.5
XII	–	–	–	–	-0.7	0.8	-0.2	-0.1	2.2	-2.1	8.7	6	-10.8	17	90	90	93	91	0.6	0.7	0.4	0.6	6.9	6.5	5.4	6.3
Rok	–	–	–	–	6.8	10.9	7.6	8.2	12.2	4.9	31.2	8.VII	-10.8	16.1,17.XII	–	–	–	–	–	–	–	–	5.9	6.2	5.2	5.8

Kętrzyn

$H_s = 110\ m$ $H_b = 107{,}4\ m$ $h_w = 11\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, %D) N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R ≥0,1	≥1,0	≥10,0	Wiatr V >10	>15					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n																		
I	·	·	4,5	4,3	4	2,4	13,5	5,1	15,5	8,7	26,5	4,9	19,5	4,6	5,5	3,4	4	4,2	21,3	5,3	6	24	11	3	·	12	5	·	5	·	2	·	1	17	26
II	3,5	1,6	2,5	3,6	6	2,6	13,5	3,4	18	3,3	21,5	3,8	11,5	4,6	4,5	2,7	3	3,3	28,3	6,2	18	10	2	·	·	17	9	·	·	·	2	·	·	14	2
III	8,5	2,8	8,5	2,1	11,5	3,8	20,5	6,0	7,5	4,4	10	4,0	10	4,8	13,5	4,7	3	4,2	17,9	6,4	15	22	5	1	·	10	5	·	6	·	2	·	5	8	7
IV	15,5	3,0	10,5	3,0	7,5	2,5	9	2,2	9	3,2	7	2,6	10,5	4,7	16	2,9	5	2,9	46,7	26,6	30	9	·	·	·	9	7	1	·	·	1	3	5	6	·
V	11,5	3,0	13	3,7	8	2,6	14	2,6	8	2,8	7,5	3,7	7,5	4,6	23,5	3,2	·	3,2	26,0	4,2	10	2	·	·	4	16	9	·	·	·	3	2	5	3	·
VI	11	2,2	4	2,2	2	1,7	11	3,8	5	2,4	8,5	4,2	17,5	3,7	19	3,1	12	2,8	57,2	16,1	10	·	·	·	3	11	10	2	·	·	3	4	4	5	·
VII	6	2,0	7	2,5	8,5	3,6	9	4,1	13	2,7	8,5	3,1	17,5	3,3	13,5	2,5	10	2,8	168,6	51,2	15	·	·	·	5	21	15	6	·	·	5	11	3	10	·
VIII	6	2,3	3	1,0	1	2,0	13	3,8	8,5	3,0	22,5	3,8	15	4,0	2,0	2,4	4	3,1	204,2	79,8	17	·	·	·	1	21	16	6	1	·	4	3	1	9	·
IX	0,5	2,0	·	·	·	·	7	3,8	18	3,5	26,5	3,9	24	4,9	7	5,1	7	3,9	127,5	24,0	15	·	·	·	1	19	16	5	3	·	·	1	·	11	·
X	·	·	·	·	·	·	6,5	2,9	29,5	2,8	32	3,7	16,5	4,5	4,5	3,0	4	3,3	16,6	5,7	30	·	·	·	·	11	7	·	2	·	4	·	2	12	·
XI	7	6,2	8,5	4,2	5	3,7	20	4,3	15,5	2,3	18,5	2,6	8,5	4,2	1	4,0	6	3,4	18,6	8,2	28	10	1	·	·	10	5	·	2	·	2	·	1	24	2
XII	3	6,8	3	2,3	4,5	5,3	10,5	3,0	18,5	2,8	35	4,4	8	7,3	1,5	8,0	9	3,9	18,2	4,9	8	24	11	4	·	12	7	·	3	·	4	·	4	18	6
Rok	72,5	2,7	64,5	2,4	58	2,5	147,5	3,8	166	3,0	224	3,7	166	4,7	129,5	3,9	67	3,4	754,1	79,8	17.VIII	101	30	8	11	169	111	20	22	·	32	24	31	143	43

Suwałki

$H_s = 165\ m$ $H_b = 169{,}5\ m$ $h_w = 12\ m$

I		·	3,5	7,1	6,5	4,8	13,5	5,1	4,5	3,6	23	4,6	28,5	6,2	10,5	6,8	3	5,3	34,8	10,0	6	26	11	6	·	19	7	1	7	·	7	·	1	21	26
II	3,5	2,9	5	2,4	5,5	2,8	15,6	4,5	8,5	4,2	20,5	4,2	17,5	5,3	8	3,6	·	4,2	40,5	7,1	14	19	4	·	·	21	13	·	4	·	7	·	·	20	10
III	11,5	4,4	16,5	3,3	6	5,2	13	8,5	3,5	7,6	8	4,6	15,5	6,0	13	5,4	6	5,1	17,5	4,0	20	24	9	5	·	9	5	·	9	1	2	·	3	9	15
IV	13,5	3,6	12,5	3,7	10	3,1	4	3,6	8	5,3	5	4,6	13	3,8	11	4,5	13	3,4	35,9	8,9	30	9	·	·	·	13	10	·	2	·	1	5	4	9	2
V	19	3,5	12,5	5,3	8	4,2	7,5	3,9	4	3,2	8,5	4,7	12,5	5,4	10	4,0	11	3,8	41,3	13,2	23	3	·	·	2	11	8	1	3	·	3	2	2	11	·
VI	7,5	3,2	8,5	3,9	4,5	2,7	9	4,9	4	4,5	12	5,0	16,5	4,1	23	3,9	8	3,8	49,0	12,5	6	·	·	·	5	9	8	2	2	·	2	3	4	8	·
VII	4	2,6	9	2,9	9,5	3,3	10	3,9	8,5	3,5	19,5	3,3	15	4,2	13,5	3,7	4	3,4	143,5	35,8	19	·	·	·	7	17	12	5	·	·	2	9	1	16	·
VIII	3	3,0	1	4,0	1	3,0	7,5	4,5	10	3,6	24	4,9	21,5	4,5	17	4,3	8	4,0	135,1	48,9	18	·	·	·	1	16	12	4	5	·	2	3	·	11	·
IX	2	3,0	1	4,0	·	·	5,5	4,3	17,5	3,7	20	5,7	26,5	5,3	9,5	4,4	8	4,4	176,0	36,6	18	·	·	·	1	19	16	6	6	·	4	1	·	12	·
X	·	·	·	·	·	·	4,5	3,8	13	4,1	45,5	5,1	21	5,4	4	4,5	5	4,7	16,4	3,3	30	·	·	·	·	11	6	·	4	·	7	·	1	11	·
XI	7,5	8,3	4,5	5,4	5	7,1	18	6,6	5,5	4,6	16,5	3,8	19	3,1	7	3,5	7	4,6	34,7	19,1	28	12	1	·	·	11	5	1	5	·	3	·	1	22	3
XII	4,5	5,8	6,5	3,6	5,5	4,8	1	4,5	12	4,6	34,5	5,7	13	5,5	3	6,2	13	4,6	34,7	9,8	8	27	14	5	·	16	10	·	6	·	9	·	2	18	18
Rok	7,6	3,4	8,0,5	3,8	5,8,5	3,4	10,9	4,8	9,9	4,4	23,7	4,7	21,9,5	4,9	12,9,5	4,6	8,6	4,3	75,3,4	48,9	18.VIII	120	39	16	16	172	112	20	53	1	49	23	19	168	74

Sejny

$H_s = 130\ m$ $h_w = 12\ m$

I	·	·	3	5,0	2,5	5,0	10,5	4,5	12	3,0	23,5	3,9	20	4,5	5,5	4,1	16	3,4	27,1	5,7	6	24	11	5	·	12	9	·	1	·	-	·	2	17	-
II	2	2,0	3,5	2,4	3,5	2,4	12,5	2,6	16	3,8	20	3,6	8	3,6	2,5	1,4	16	2,6	44,9	11,2	19	15	4	·	·	18	13	1	2	·	-	·	·	13	-
III	10	2,2	8,5	2,4	6	4,3	13	5,9	8	4,9	5	3,3	13	4,4	9,5	5,5	20	3,3	17,8	4,0	20	27	8	5	·	11	6	·	4	·	-	·	5	1	-
IV	4,5	2,2	1,0	3,4	8	2,9	10,5	2,2	10	5,0	8,5	3,0	4,5	2,3	12	4,0	22	2,5	26,6	9,7	30	12	·	·	1	13	8	·	1	·	-	2	·	5	-
V	15	2,9	9,5	3,7	5,5	3,3	10	2,3	8	2,2	3	4,0	11	3,4	9	2,5	22	2,2	27,8	9,3	19	3	·	·	1	12	7	·	·	·	-	1	1	6	-
VI	8	2,4	0,5	4,0	1,5	3,0	10	3,2	5,5	3,0	8,5	3,0	13,5	2,9	14,5	3,5	28	2,1	60,2	12,3	10	·	·	·	4	12	9	3	·	·	-	3	3	4	-
VII	4,5	2,2	3,5	3,0	8,5	4,2	12	3,0	17,5	2,1	7	3,6	16	4,2	7	4,2	17	2,7	148,0	37,7	18	·	·	·	6	16	11	3	·	·	-	6	1	12	-
VIII	3	2,0	1,5	1,7	0,5	1,0	9	3,4	13	3,2	17,5	4,8	22	3,4	10,5	2,8	16	2,9	125,5	41,2	18	·	·	·	1	13	10	5	·	·	-	3	·	10	-
IX	2	3,0	·	·	1	1,0	6,5	2,9	19	2,9	17	4,9	26,5	4,6	4	2,2	14	3,3	146,3	33,4	18	·	·	·	1	19	16	6	3	·	-	·	2	10	-
X	1	2,0	·	·	·	·	4	3,8	23	4,0	24	3,9	22	4,5	4	3,4	15	3,4	11,8	2,3	12	·	·	·	·	8	6	·	·	·	-	·	1	12	-
XI	8,5	6,8	5	4,0	5,5	5,7	15	5,5	15	3,6	15,5	3,2	7	5,5	3,5	3,1	15	3,8	36,9	19,1	28	12	1	·	·	9	4	2	3	·	-	·	2	20	-
XII	5	6,0	5	3,0	3	4,0	2	4,5	22,5	4,8	27	6,3	6	6,2	4,5	4,3	18	4,3	25,5	6,7	8	26	12	5	·	15	11	·	4	·	-	·	2	14	-
Rok	6,3,5	2,8	5,0	2,7	4,5,5	2,8	11,5	3,6	16,9,5	3,5	17,6,5	4,0	16,9,5	4,1	8,6,5	3,4	21,9	3,0	69,8,4	41,2	18.VIII	119	36	15	14	158	110	20	18	·	-	17	19	124	-

Tczew

$H_s = 10\ m$ $h_w = 10\ m$

I	0,5	8,0	4	3,5	4	4,8	7	4,7	12	4,4	20,5	3,1	19	5,0	4,7	3,9	9	3,1	8,8	2,9	25	21	7	2	·	10	2	·	1	·	-	·	2	13	-
II	0,5	9,0	5	1,6	2	2,5	9,5	2,1	18,5	4,8	17	2,2	13	4,5	7,5	4,1	11	2,4	33,2	6,1	18	8	·	·	·	20	14	·	·	·	-	·	2	8	-
III	21,5	4,0	2	2,5	3	4,3	10	2,6	11	3,8	4	1,2	7	3,4	13,5	3,1	21	2,6	23,4	6,4	15	20	3	·	·	7	7	·	2	1	-	·	7	10	-
IV	2,4	5,2	22,5	5,3	3,5	1,4	3	1,3	3,5	2,4	3,5	2,7	9	3,2	11	2,8	10	3,7	11,6	4,7	22	5	·	·	·	12	4	·	3	2	-	3	6	7	-
V	2,1	4,8	22,5	6,2	2,5	1,2	5,5	2,8	8,5	1,2	5	2,4	6	5,8	4,0	3,0	12	3,7	42,3	6,8	5	1	·	·	·	12	9	·	5	2	-	3	8	8	-
VI	11,5	2,9	1,0	2,7	1	1,0	6	1,3	1,5	1,3	10,5	2,1	1,9	2,1	13,5	2,4	17	2,0	29,0	6,9	5	·	·	·	7	10	6	·	·	·	-	1	8	6	-
VII	7,5	2,0	10,5	2,6	5	1,4	6,5	2,3	3	1,8	10	2,0	9,5	2,8	1,9	3,1	22	1,9	95,8	24,3	30	·	·	·	12	1,9	13	3	·	·	-	7	4	7	-
VIII	5	2,5	5	3,0	·	·	6,5	3,1	12	2,2	1,9	2,4	9,5	3,6	17	2,9	1,9	2,2	118,9	28,5	16	·	·	·	3	18	15	3	·	·	-	4	8	9	-
IX	1	1,0	·	·	·	·	4	2,0	18,5	2,2	24,5	4,7	20,5	4,2	12,5	6,1	9	3,7	60,7	16,0	23	·	·	·	2	19	13	1	5	2	-	2	4	13	-
X	0,5	1,0	·	·	·	·	4,5	1,7	20,5	1,8	35,5	2,9	9,5	3,6	7,5	4,0	1,5	2,3	12,8	4,2	20	·	·	·	·	8	5	·	·	·	-	·	3	7	-
XI	1,5	4,7	5,5	5,6	6,5	2,5	9	2,6	1,7	1,4	16,5	2,2	11	3,1	8	4,0	1,5	2,3	6,8	1,8	28,29	7	1	·	·	8	3	·	2	1	-	·	4	18	-
XII	0,5	7,0	8	2,4	3,5	2,6	2,5	1,8	2,4	1,5	2,3	1,8	1,5	3,5	8,5	3,8	8	2,1	12,1	4,2	8	18	8	2	·	12	3	·	1	1	-	·	4	12	-
Rok	9,5	4,3	9,5	3,0	3,1	1,8	7,4	2,4	15,0	1,9	18,9	2,5	14,8	3,7	14,5	3,6	16,8	2,7	45,5,4	28,5	16.VIII	80	19	4	24	155	94	7	19	9	-	5,0	66	118	-

Rasnowo

$\varphi = 54°04'$ $\lambda = 16°18'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	-0.2	6.5	1.6	2.4	7.7	-3.3	17.2	31	-10.2	3	85	67	83	78	0.9	3.6	1.2	1.9	5.3	4.2	3.0	4.2
IV	–	–	–	–	3.4	9.9	4.0	5.3	11.0	-0.7	22.9	28	-7.6	15	90	67	88	82	0.9	4.9	1.0	2.3	6.7	5.3	4.3	5.4
V	–	–	–	–	8.5	12.9	7.2	9.0	14.5	3.1	24.6	19	-1.9	6	81	64	86	77	2.3	6.5	1.6	3.5	5.7	6.7	3.6	5.3
VI	–	–	–	–	13.6	19.7	14.0	15.3	21.3	8.7	29.5	18	4.2	1	82	59	84	75	3.0	10.4	2.8	5.4	3.6	3.9	2.2	3.2
VII	–	–	–	–	16.7	21.4	17.1	18.1	23.0	12.9	31.0	4	6.6	7	88	70	87	82	2.4	8.7	2.8	4.6	6.5	6.4	4.5	5.8
VIII	–	–	–	–	14.1	19.1	14.4	15.5	20.3	11.2	26.2	11	6.8	23	–	–	–	–	–	–	–	–	6.4	7.7	4.3	6.1
IX	–	–	–	–	9.5	13.9	9.9	10.8	15.3	6.8	27.0	8	-0.5	26	92	76	91	86	1.0	4.3	1.1	2.1	6.8	7.7	4.8	6.4
X	–	–	–	–	8.3	11.9	8.6	9.4	12.5	6.0	18.6	10	0.6	2	–	–	–	–	–	–	–	–	7.9	7.3	5.3	6.8
XI	–	–	–	–	3.7	6.2	4.2	4.6	7.1	2.2	14.6	5	-8.0	30	–	–	–	–	–	–	–	–	7.2	7.7	6.9	7.3
XII	–	–	–	–	-0.5	1.1	-0.1	0.1	2.4	-2.7	8.7	5	-14.1	17	91	86	90	89	0.5	0.9	0.6	0.7	8.5	7.8	6.4	7.6
Rok	–	–	–	–	–	–	–	–	–	–	31.0	4.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Stare Pole

$\varphi = 54°03'$ $\lambda = 19°13'$

I	–	–	–	–	-1.4	0.5	-0.7	-0.6	1.7	-3.7	9.3	6	-14.8	16	90	87	88	88	0.6	0.9	0.7	0.7	8.2	8.2	7.2	7.9
II	–	–	–	–	1.5	3.9	2.2	2.4	4.9	0.0	9.7	14	-5.8	25	93	83	90	89	0.5	1.4	0.7	0.9	8.8	8.3	7.9	8.3
III	–	–	–	–	-0.5	5.3	1.8	2.1	6.6	-2.3	17.7	31	-9.8	17	85	65	80	77	0.9	3.4	1.5	1.9	4.7	5.8	4.8	5.1
IV	–	–	–	–	3.6	9.9	4.4	5.6	11.3	0.5	24.0	28	-6.1	15	89	69	88	82	0.9	4.6	1.1	2.2	5.7	6.1	6.2	6.0
V	–	–	–	–	8.8	13.1	8.4	9.7	14.3	4.1	23.8	19	-2.7	6	83	61	83	76	2.1	6.7	2.0	3.6	5.8	6.5	5.2	5.8
VI	–	–	–	–	14.2	19.1	14.2	15.4	20.4	8.6	28.7	11	3.1	21	83	65	88	79	2.8	8.3	2.0	4.4	5.3	6.8	6.2	6.1
VII	–	–	–	–	16.6	21.4	16.5	17.8	22.8	12.7	30.0	4	9.1	4	90	71	91	84	2.0	8.0	1.8	3.9	6.7	6.2	5.2	6.0
VIII	–	–	–	–	14.5	19.5	14.9	16.0	20.6	11.4	25.8	12	6.4	24	91	68	89	83	1.5	7.5	1.9	3.6	5.6	6.9	5.3	5.9
IX	–	–	–	–	9.7	14.0	10.6	11.2	15.4	7.2	26.8	9	0.8	27	92	74	88	85	1.0	4.8	1.6	2.5	6.4	7.9	6.3	6.9
X	–	–	–	–	6.9	11.2	8.4	8.7	12.5	5.0	18.3	10	0.9	2	94	80	89	88	0.6	2.7	1.3	1.5	7.0	8.4	6.0	7.1
XI	–	–	–	–	3.9	6.3	4.5	4.8	7.4	2.0	14.1	5	-7.6	30	92	82	89	88	0.6	1.8	0.9	1.1	8.9	8.3	7.9	8.4
XII	–	–	–	–	-1.4	0.2	-0.6	-0.6	1.6	-3.4	7.6	8,9	-12.0	18	90	85	90	88	0.6	0.9	0.6	0.7	7.8	7.8	6.6	7.4
Rok	–	–	–	–	6.4	10.4	7.0	7.7	11.6	3.5	30.0	4.VII	-14.8	16.I	89	74	88	84	1.2	4.2	1.3	2.2	6.7	7.3	6.2	6.7

Malbork

$\varphi = 54°02'$ $\lambda = 19°02'$

I	–	–	–	–	-0.7	1.0	0.0	0.1	2.2	-3.3	9.5	6	-13.3	16	–	–	–	–	–	–	–	–	8.3	7.8	6.1	7.4
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.5	7.1	7.7
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.6	4.3	4.9
IV	–	–	–	–	4.0	10.4	5.1	6.2	11.2	0.9	24.5	29	-4.1	9	–	–	–	–	–	–	–	–	5.8	6.3	6.0	6.0
V	–	–	–	–	9.2	13.4	9.3	10.3	14.2	5.0	24.0	19	0.9	6	–	–	–	–	–	–	–	–	5.7	6.8	4.9	5.8
VI	–	–	–	–	14.5	19.7	14.7	15.9	20.9	10.2	29.1	11,18	6.4	7,25	–	–	–	–	–	–	–	–	4.0	5.3	3.7	4.3
VII	–	–	–	–	17.1	22.1	17.3	18.4	23.1	13.8	31.7	4	11.3	7,19	–	–	–	–	–	–	–	–	6.2	5.6	5.1	5.6
VIII	–	–	–	–	14.8	19.8	15.0	16.2	20.4	12.5	25.6	12	8.9	7	–	–	–	–	–	–	–	–	5.2	6.5	4.8	5.5
IX	–	–	–	–	10.1	14.4	10.8	11.5	15.3	8.0	26.6	9	0.4	30	–	–	–	–	–	–	–	–	6.7	7.3	5.4	6.5
X	–	–	–	–	7.4	11.9	8.9	9.3	12.7	5.5	18.5	19	0.4	1	–	–	–	–	–	–	–	–	6.7	7.2	4.2	6.0
XI	–	–	–	–	4.3	6.5	4.7	5.0	7.5	2.5	14.6	5	-6.0	30	–	–	–	–	–	–	–	–	8.5	8.2	7.0	7.9
XII	–	–	–	–	-0.9	0.5	-0.3	-0.2	1.9	-3.0	8.1	8,9	-12.6	18	–	–	–	–	–	–	–	–	6.8	7.6	5.9	6.8
Rok	–	–	–	–	–	–	–	–	–	–	31.7	4.VII	–	–	–	–	–	–	–	–	–	–	6.4	6.8	5.4	6.2

Dziwnów

$\varphi = 54°01'$ $\lambda = 14°44'$

I	1018.3	1033.0	998.6	1018.8	0.8	1.7	1.0	1.1	3.0	-1.4	11.2	6	-8.0	15	92	88	94	91	0.5	0.8	0.4	0.6	9.1	6.9	8.4	8.1
II	1007.8	1038.1	979.7	1008.3	1.8	4.2	2.9	3.0	5.6	0.7	11.9	2	-4.1	26	94	86	94	91	0.4	1.2	0.5	0.7	7.7	7.1	5.9	6.9
III	1016.4	1038.4	990.4	1016.9	1.6	5.4	3.0	3.2	7.1	0.1	16.1	13	-4.5	6	90	76	88	85	0.7	2.3	1.0	1.3	5.8	5.3	4.9	5.3
IV	1019.1	1032.0	993.0	1019.6	4.2	6.0	4.8	5.0	7.4	2.6	18.5	5	-2.6	13	89	82	88	86	0.9	1.7	1.0	1.2	7.6	6.0	5.2	6.3
V	1016.6	1031.5	1005.5	1017.1	8.7	11.1	9.0	9.4	12.8	6.4	25.0	16	0.4	6	81	71	80	77	2.3	4.5	2.4	3.1	6.0	5.4	5.3	5.6
VI	1015.6	1032.6	1002.7	1016.1	14.6	16.5	15.0	15.3	18.6	12.0	29.6	11	8.1	1	79	75	80	78	3.5	5.0	3.4	4.0	5.7	4.6	3.6	4.6
VII	1011.0	1022.7	1001.0	1011.5	17.5	19.3	17.9	18.2	21.3	15.4	29.5	1	11.1	2	91	84	92	89	1.9	3.8	1.7	2.5	6.9	6.1	6.0	6.3
VIII	1011.3	1023.6	997.0	1011.8	15.4	18.7	16.2	16.6	–	13.5	–	–	9.5	23	88	73	85	82	2.1	6.1	2.9	3.7	6.6	6.7	5.8	6.4
IX	1009.6	1023.0	987.5	1010.1	11.4	14.0	11.9	12.3	–	9.5	–	–	5.0	25	87	75	85	82	1.7	4.2	2.1	2.7	7.5	6.5	5.5	6.5
X	1015.5	1027.8	999.3	1016.0	9.0	11.8	10.2	10.3	–	8.1	–	–	4.7	2	91	79	89	86	1.1	3.0	1.4	1.8	8.1	6.4	7.5	7.3
XI	1019.3	1038.0	998.5	1019.8	4.4	6.5	5.3	5.4	–	3.1	–	–	-3.9	21	91	82	87	87	0.7	1.8	1.1	1.2	8.0	8.0	7.2	7.7
XII	1012.2	1030.1	969.8	1012.7	0.8	1.8	1.4	1.4	–	-0.7	–	–	-11.0	17	93	88	93	91	0.4	0.7	0.5	0.5	8.5	8.1	6.6	7.7
Rok	1014.4	1038.4	969.8	1014.9	7.5	9.8	8.2	8.4	–	5.8	–	–	-11.0	17.XII	89	80	88	86	1.4	2.9	1.5	1.9	7.3	6.4	6.0	6.6

Rosnowo

$H_s = 62\,m$ $h_w = 12\,m$ 1957

MIESIĄC	ROZKŁAD WIATRU °D °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0	Min<-10	Max≥25	Opad R 0,1	≥1	≥10	≥100	Wiatr ≥10	≥15	≡	≈	●	◉	⊞
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41.8	12.5	12	–	–	–	–	15	8	2	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.0	8.7	8	–	–	–	–	16	8	·	–	–	·	·	·	·	·	·
III	3	2.0	8	4.5	7.5	2.3	26.5	3.6	4	2.0	7	1.1	14	4.5	2	2.0	21	2.4	33.2	11.6	15	23	·	1	·	9	6	1	3	·	6	·	9	7	1
IV	14	6.4	10	1.9	6	3.5	3	1.0	2	1.5	3	2.3	14	2.6	15	2.0	23	1.4	239	8.1	16	15	·	·	·	14	7	·	·	·	5	·	5	10	1
V	4	1.5	16	2.1	5.5	1.8	5.5	2.4	3	1.0	5	1.4	13	3.7	16	2.1	25	1.7	439	13.6	19	6	·	·	·	12	8	1	1	·	·	2	5	8	·
VI	4	2.5	6	1.0	3	1.0	5	3.2	3	1.0	5	1.6	26.5	2.7	4.5	2.0	33	1.4	422	13.6	9	·	·	·	5	11	9	1	·	·	·	1	13	2	·
VII	5	1.8	4	1.5	3	1.0	5	1.6	4	2.0	9	2.0	20.5	2.5	14.6	2.4	28	1.5	1059	18.6	29	·	·	·	10	17	16	4	·	·	·	2	6	10	·
VIII	1	3.0	1	1.0	3	1.0	10	1.9	4	1.5	24	2.2	17	2.2	6	3.0	27	1.5	1071	22.2	10	·	·	·	1	18	14	4	·	·	2	·	1	9	·
IX	·	·	·	·	1	1.0	3	1.0	10	2.2	21	4.2	17	3.5	9	3.3	29	2.3	1078	18.6	27	2	·	·	1	21	14	5	·	·	1	2	4	11	·
X	·	·	·	·	·	·	8	1.8	13.5	1.8	36	2.7	12.5	3.8	3	4.0	20	2.1	463	8.6	3	·	·	·	·	18	12	·	·	·	3	·	3	14	·
XI	3	4.7	3	2.3	8	1.8	20	1.7	7	1.8	12	3.2	11	5.1	1	1.0	25	2.0	546	14.0	27	9	1	·	·	13	9	1	·	·	·	·	5	18	1
XII	2	1.0	5	4.2	7	1.7	10	1.4	13.5	2.4	26	2.3	7.5	2.4	3	4.3	19	1.9	424	18.5	8	16	6	4	·	12	9	1	·	·	6	·	2	18	6
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6871	22.2	10.VIII	–	–	–	–	186	122	20	–	–	–	–	–	–	–

Stare Pole

$H_s = 3\,m$ $h_w = 11{,}5\,m$

I	·	·	3.5	6.0	6.5	4.3	4.5	1.3	1.6	3.4	35.5	4.6	14.5	5.2	2.5	5.4	1.0	3.9	159	4.5	12	27	6	3	·	10	6	·	2	·	–	·	3	15	9
II	4.5	3.1	2.5	2.8	6.5	2.5	8	2.9	2.1	3.1	2.3	3.8	9.5	4.1	3	4.0	6	3.2	44.3	6.4	18	15	·	·	·	18	13	·	1	·	·	·	·	17	·
III	1.0	5.1	3.5	4.0	1.3	4.4	17.5	5.9	1.2	4.3	12.5	5.1	1.1	5.2	10.5	4.5	5	4.8	217	9.2	15	25	2	·	·	8	6	·	7	2	1	·	10	9	3
IV	2.4	5.6	4.5	2.3	8.5	2.4	3	2.8	4.5	4.2	1.6	4.0	8.5	4.5	1.7	3.9	4	4.0	137	4.4	16	10	·	·	·	12	4	·	2	·	5	5	5	12	·
V	2.1	5.0	10.5	5.2	7	3.9	6.5	3.1	5	3.1	9	5.5	7.5	4.7	15.5	4.0	11	4.0	336	8.8	11	3	·	·	·	14	10	·	4	1	2	3	8	11	·
VI	16.5	2.9	4.5	1.9	8	1.9	4.5	3.8	4	1.9	15.5	3.5	2.3	3.2	9	2.7	5	2.8	385	12.0	5	·	·	·	2	10	6	1	·	·	1	·	4	10	·
VII	9	2.2	9	2.6	10.5	3.1	4.5	3.0	7	3.6	14.5	3.6	18.5	3.9	14	3.6	6	3.1	118.2	29.8	30	·	·	·	7	14	13	4	·	·	2	9	3	9	·
VIII	11.5	2.6	3	2.5	3	2.8	6	2.8	1.8	3.6	21.5	5.0	1.9	4.8	9	3.1	2	3.8	118.0	25.4	16	·	·	·	2	19	15	3	2	·	·	6	1	9	·
IX	1	1.0	0.5	1.0	0.5	1.0	6.5	2.5	2.2	4.5	2.9	4.9	20.5	5.2	8	5.1	2	4.5	72.8	13.1	23	·	·	·	2	18	15	1	1	·	3	5	2	11	·
X	·	·	0.5	1.0	1.5	1.7	7.5	2.5	2.9	4.5	4.0.5	4.7	1.0	4.8	2	5.8	2	4.3	21.1	7.4	30	·	·	·	·	10	7	·	·	·	6	·	2	8	·
XI	·	·	9.5	5.1	11.5	3.0	14.5	3.3	20.5	2.5	1.8	3.7	1.0	5.4	4	5.8	2	3.6	18.3	5.4	28	10	1	·	·	7	5	·	2	·	2	·	2	21	·
XII	3.5	5.6	4.5	3.7	7.5	3.3	2.5	3.4	2.6	3.8	3.3	5.2	9	6.7	3	6.7	4	4.5	15.0	2.7	30	23	10	2	·	13	8	·	1	·	7	·	3	12	2
Rok	10.1	2.8	5.6	3.2	8.4	2.9	8.5.5	3.1	1.8.5	3.5	2.6.8	4.5	1.6.1	4.8	9.7.5	4.6	5.7	3.9	5.2.8.1	2.9.8	30.VII	1.1.3	1.9	5	1.3	1.5.3	1.0.8	9	2.2	3	–	2.8	4.3	1.4.4	4.4

Malbork

$H_s = 20\,m$ $h_w = 10\,m$

I	·	·	3	5.7	5	3.8	9	3.8	1.7	5.0	1.4	5.5	2.6	5.6	·	·	1.9	4.1	11.9	3.0	26	26	6	3	·	8	6	·	2	·	·	·	2	15	–
II	1	3.0	2	2.0	1	2.0	6	3.8	3.1	5.0	1.1	5.1	9	4.4	5	5.6	1.8	3.7	35.1	4.2	18	–	–	–	·	17	14	·	·	·	2	·	·	13	–
III	1.0	2.9	2	1.5	1.6	5.4	1.0	5.9	1.0	5.9	1	3.0	1.5	6.0	4	7.0	2.5	3.8	14.2	3.2	29	–	–	–	·	6	4	·	6	·	2	·	10	9	–
IV	2.5	3.8	2	1.5	4	4.8	·	·	1.3	4.1	2	7.0	8	4.8	5	4.4	3.1	2.7	14.8	4.0	26	1.0	·	·	·	12	5	·	1	·	4	4	5	11	–
V	2.0	3.5	7	3.4	9	3.4	6	3.8	8	5.0	2	4.0	6	5.8	2.0	4.2	1.5	3.4	35.4	8.2	19	·	·	·	·	11	9	·	1	·	1	3	5	9	–
VI	10.5	3.8	4	3.0	4	3.0	4	5.0	8	4.4	2	3.5	1.8	4.8	13.5	4.1	2.6	3.0	42.4	10.0	22	·	·	·	4	9	7	1	·	·	1	1	6	6	–
VII	6	2.3	3	2.3	11	2.7	1.2	4.4	8	5.1	·	·	1.8	3.7	11	4.9	2.4	2.9	119.3	28.5	12	·	·	·	10	14	11	4	·	·	3	10	4	7	–
VIII	4	4.0	2	2.0	3	4.7	5	5.2	2.6	4.3	7	4.0	1.9	3.9	9	3.7	1.8	3.3	138.5	31.0	16	·	·	·	1	18	17	5	1	·	·	8	2	8	–
IX	1	3.0	1	2.0	·	·	6	4.5	2.8	5.6	7	4.0	1.8	4.2	9	5.0	2.0	3.7	68.6	16.0	23	·	·	·	2	19	16	1	·	·	2	3	1	10	–
X	·	·	·	·	·	·	8	4.0	5.4	5.0	5	3.8	1.4	4.1	·	·	1.2	4.1	18.9	7.2	30	·	·	·	·	9	7	·	1	·	3	·	2	5	–
XI	4	5.8	6	4.5	7	3.3	1.9	4.2	2.0	5.1	3	3.3	1.6	4.7	·	·	1.5	3.8	14.3	5.5	27	9	1	·	·	9	4	·	·	·	1	·	1	19	–
XII	2	3.5	3	6.3	1.2	3.2	4.5	2.9	3.3.5	4.9	5	3.2	1.7	4.5	1	3.0	1.5	3.6	16.7	5.0	8	23	·	1.9	·	7	5	·	1	·	·	·	2	14	–
Rok	8.3.5	3.0	3.5	2.8	7.2	3.0	8.9.5	4.0	2.5.6.5	5.0	5.9	3.9	1.8.4	4.7	7.7.5	3.5	2.3.8	3.5	5.3.0.1	3.1.0	1.6.VIII	–	–	–	1.7	1.3.9	1.0.5	1.1	1.3	·	1.9	2.9	4.0	1.2.6	–

Dziwnów

$H_s = 7\,m$ $H_b = 4{,}0\,m$ $h_w = 18\,m$

I	4	5.2	1	4.5	7	9.1	10.5	3.0	12.5	4.4	2.6	4.2	2.2	6.7	9	7.1	1	5.3	25.3	6.0	12	19	4	·	·	10	8	·	8	3	–	·	·	20	–
II	1.5	4.7	3.5	6.6	6.5	3.2	13.5	3.5	2.1	4.3	1.4	4.6	1.4	5.9	8	3.0	2	4.5	35.4	7.5	8	9	·	·	·	12	10	·	3	·	–	·	1	12	–
III	2.5	7.0	1.0	8.6	10.5	7.3	2.1	5.0	2.0	4.2	7	4.1	1.3	6.9	6	5.4	3	5.6	28.8	7.4	15	16	·	·	·	11	8	·	9	2	–	1	5	9	–
IV	9.5	5.3	30.5	5.7	20.5	6.0	4.5	3.6	2.5	3.4	1.5	4.7	5	7.0	1.2	7.2	4	5.6	18.1	3.6	16	3	·	·	·	11	7	·	6	1	–	·	2	8	–
V	10.5	3.7	21.5	7.8	19.5	8.3	6	4.7	4	3.9	1.5	3.7	9.5	6.1	14.5	6.0	6	6.0	15.2	5.1	4	·	·	·	·	8	3	·	9	3	–	3	2	6	–
VI	2.5	3.4	11.5	5.7	1.5	4.9	2	2.8	4.5	2.8	6	2.8	1.7	5.9	20.5	5.4	11	4.4	36.1	12.0	24	·	·	·	2	9	5	2	7	·	–	3	7	2	–
VII	1.0	4.5	1.8	4.8	6.5	5.6	7	2.7	2.5	2.0	4.5	2.3	1.2	5.6	2.7.5	6.8	5	4.9	98.0	30.7	21	·	·	·	3	16	12	3	9	·	–	7	1	9	–
VIII	3.5	6.1	3.5	3.6	3.5	4.0	11.5	3.1	1.6	3.2	1.8.5	4.2	10.5	6.4	22	7.1	4	4.6	57.1	13.1	22	·	–	·	–	18	14	2	5	·	–	2	·	8	–
IX	1.1	8.9	6	3.6	2	3.8	5	3.4	1.3	4.3	1.5	5.9	1.2	7.2	1.9	8.7	7	6.0	50.1	11.9	13	·	–	·	–	21	11	1	10	3	–	·	1	7	–
X	4	4.9	2.5	3.8	1.5	2.0	3.5	3.6	1.9	4.0	2.6.5	5.4	2.3.5	5.5	8.5	8.1	4	5.0	27.2	9.6	3	·	–	·	–	11	8	·	5	2	–	1	1	16	–
XI	2	8.8	6.5	9.1	2.2.5	5.4	1.9.5	2.9	10.5	4.2	9.5	4.8	10.5	9.9	7	4.4.3	2	6.1	24.7	10.0	9	8	–	·	–	8	6	1	10	3	–	·	3	16	–
XII	9.5	10.5	5	12.3	7.5	7.4	7.5	3.9	18.5	4.9	23	5.7	16	8.9	2	10.0	4	6.8	19.2	9.2	8	17	–	1	–	8	7	·	11	3	–	·	1	18	–
Rok	7.0.5	6.1	11.9.5	6.3	1.2.2.5	5.6	1.1.1.5	3.5	1.4.4	3.8	1.5.3	4.4	1.6.5	6.8	1.5.6	7.4	5.3	5.4	4.3.4.2	8.0.7	2.4.VII	7.2	–	1	–	1.4.3	9.9	9	9.2	2.0	–	1.7	2.4	1.3.1	–

Siejnik

$\varphi = 54°01'$ $\lambda = 22°29'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-2.8	-1.2	-1.9	-2.0	-0.4	-5.2	6.7	6,9	-19.3	16	-	-	-	-	-	-	-	-	8.7	8.6	8.9	8.7
II	-	-	-	-	0.1	2.1	0.8	1.0	2.6	-1.5	6.3	2	-9.1	28	-	-	-	-	-	-	-	-	9.6	8.6	9.1	9.1
III	-	-	-	-	-2.6	2.8	-0.6	-0.2	3.9	-5.1	15.7	31	-14.7	17	-	-	-	-	-	-	-	-	7.4	6.5	6.9	6.9
IV	-	-	-	-	4.0	11.7	6.3	7.1	12.7	1.9	25.2	27	-6.4	14	-	-	-	-	-	-	-	-	6.5	6.4	6.2	6.4
V	-	-	-	-	8.7	13.6	9.3	10.2	14.8	4.7	25.7	19	-2.4	6	83	60	80	74	2.1	7.1	2.5	3.9	5.5	6.6	6.2	6.1
VI	-	-	-	-	14.8	19.6	14.3	15.8	20.9	9.0	27.9	11	2.9	21	73	56	77	69	4.6	10.6	3.8	6.3	5.2	6.3	6.3	5.9
VII	-	-	-	-	16.4	21.1	16.5	17.6	22.3	12.6	27.2	8	8.4	4	-	-	-	-	-	-	-	-	7.1	7.7	7.5	7.4
VIII	-	-	-	-	13.9	18.7	14.2	15.2	19.8	10.8	27.9	12	4.8	24	90	69	87	82	1.7	7.0	2.2	3.6	6.0	7.7	6.3	6.7
IX	-	-	-	-	9.0	13.4	9.8	10.5	14.3	6.5	25.6	9	0.6	17	92	73	88	84	0.9	4.8	1.5	2.4	7.9	8.0	7.2	7.7
X	-	-	-	-	5.8	10.3	7.8	7.9	10.9	4.0	16.7	10	0.4	3	94	78	89	87	0.5	2.8	1.2	1.5	7.4	8.2	6.9	7.5
XI	-	-	-	-	2.5	4.3	3.2	3.3	-	1.4	-	-	-9.9	30	-	-	-	-	-	-	-	-	9.0	9.1	8.2	8.8
XII	-	-	-	-	-3.1	-1.4	-2.5	-2.4	-	-4.8	-	-	-13.5	18	-	-	-	-	-	-	-	-	8.3	7.4	7.5	7.7
Rok	-	-	-	-	5.6	9.6	6.4	7.0	-	2.8	27.9	11.VI,12.VIII	-19.3	16.1	-	-	-	-	-	-	-	-	7.4	7.6	7.3	7.4

Miastko

$\varphi = 54°00'$ $\lambda = 16°58'$

I	-	-	-	-	-1.1	0.3	-0.7	-0.6	1.7	-3.2	10.5	6	-15.1	16	-	-	-	-	-	-	-	-	8.8	7.7	7.9	8.1
II	-	-	-	-	0.6	3.6	1.7	1.9	5.2	-0.8	9.7	2	-7.4	25,27	-	-	-	-	-	-	-	-	9.1	6.8	7.4	7.8
III	-	-	-	-	-0.7	5.7	1.6	2.0	7.3	-2.3	17.1	-3.1	-7.7	2,6,9	-	-	-	-	-	-	-	-	6.0	4.6	4.1	4.9
IV	-	-	-	-	3.3	9.7	4.5	5.5	11.2	0.3	23.1	28	-6.5	15	-	-	-	-	-	-	-	-	6.9	5.4	4.9	5.7
V	-	-	-	-	8.0	13.0	8.0	9.2	14.4	3.2	25.0	19	-2.3	6	-	-	-	-	-	-	-	-	5.6	6.4	4.4	5.5
VI	-	-	-	-	13.3	19.7	14.3	15.4	21.6	8.5	29.6	18	3.7	15	74	55	72	67	4.1	11.3	4.9	6.8	4.5	4.8	3.5	4.3
VII	-	-	-	-	15.6	21.3	16.1	17.3	23.1	12.5	29.7	4	5.6	7	84	62	79	75	2.8	10.5	4.0	5.8	6.6	6.1	6.0	6.2
VIII	-	-	-	-	13.2	18.3	14.3	15.0	20.1	10.6	25.8	11	5.7	24	84	66	82	77	2.4	7.5	3.1	4.3	6.3	7.6	5.2	6.4
IX	-	-	-	-	8.7	13.6	9.7	10.4	15.1	6.4	26.7	8	-1.3	25,27	83	65	81	76	1.8	5.9	2.3	3.3	7.4	7.0	6.0	6.8
X	-	-	-	-	7.0	11.0	8.3	8.6	12.1	5.3	18.1	10	-0.7	2	84	68	82	78	1.6	4.2	1.9	2.6	8.5	6.6	5.8	7.0
XI	-	-	-	-	3.0	5.8	3.5	4.0	6.8	1.4	15.2	5	-10.5	30	81	73	79	78	1.4	2.9	1.7	2.0	8.6	8.2	7.7	8.2
XII	-	-	-	-	-1.4	0.1	-0.6	-0.6	1.8	-3.3	8.2	8	-13.9	18	-	-	-	-	-	-	-	-	8.4	7.8	7.2	7.8
Rok	-	-	-	-	5.8	10.2	6.7	7.4	11.7	3.2	29.7	4.VII	-15.1	16.1	-	-	-	-	-	-	-	-	7.2	6.6	5.8	6.5

Ramlewo Dolne

$\varphi = 53°59'$ $\lambda = 15°43'$

I	-	-	-	-	0.3	4.6	0.7	0.8	2.7	-4.8	10.9	6	-11.0	15	91	86	88	88	0.6	1.0	0.8	0.8	8.9	8.4	7.6	8.3
II	-	-	-	-	4.5	4.8	2.8	3.0	6.2	-0.6	10.6	6	-7.3	26	88	79	88	85	0.8	1.9	0.9	1.2	8.0	6.8	6.3	7.0
III	-	-	-	-	1.1	6.6	2.5	3.2	8.1	-1.2	15.7	27	-6.8	3	87	66	84	79	0.9	3.7	1.3	2.0	4.9	4.9	3.5	4.4
IV	-	-	-	-	3.4	9.7	4.6	5.6	10.8	0.2	21.0	5	-8.5	13	87	65	84	79	1.0	5.1	1.4	2.5	7.5	6.6	5.4	6.5
V	-	-	-	-	8.8	13.0	8.1	9.5	14.5	3.2	24.5	19	-1.9	29	-	-	-	-	-	-	-	-	5.1	7.1	5.2	5.8
VI	-	-	-	-	13.9	19.3	13.7	15.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.0	5.8	6.6	6.1
VII	-	-	-	-	16.9	21.1	16.6	17.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.5	4.8	6.0	5.4
VIII	-	-	-	-	14.5	18.8	14.9	15.8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.9	5.8	7.1	6.3
IX	-	-	-	-	10.0	14.0	10.4	11.2	15.6	-	24.9	8	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Radostowo

$\varphi = 53°59'$ $\lambda = 18°45'$

I	-	-	-	-	-1.2	0.6	-0.6	-0.4	1.6	-3.1	10.0	6	-12.9	16	87	85	85	86	0.8	1.0	0.9	0.9	7.8	7.6	6.9	7.4
II	-	-	-	-	1.4	3.9	2.2	2.4	4.8	0.0	8.8	14	-4.5	25	91	81	89	87	0.6	1.6	0.8	1.0	9.3	8.1	8.5	8.6
III	-	-	-	-	-0.3	5.4	1.8	2.2	6.6	-1.7	17.1	31	-7.7	9	86	66	81	78	0.8	3.1	1.3	1.7	6.1	6.1	4.7	5.6
IV	-	-	-	-	3.7	10.1	4.4	5.6	11.3	1.0	23.7	28	-5.6	16	87	65	86	79	1.1	5.4	1.3	2.6	6.4	7.0	6.1	6.5
V	-	-	-	-	8.6	13.4	8.1	9.6	14.9	4.4	24.8	19	-0.4	12	76	59	77	71	2.6	7.8	2.5	4.3	6.1	7.5	5.3	6.3
VI	-	-	-	-	14.3	19.3	13.7	15.2	20.7	8.9	29.0	11	3.9	21	78	57	82	72	3.8	10.5	3.0	5.8	5.4	6.1	5.3	5.6
VII	-	-	-	-	16.5	21.7	16.4	17.8	23.2	13.2	31.2	8	8.8	7	82	66	88	81	2.3	9.9	2.3	4.8	7.5	7.0	6.1	6.9
VIII	-	-	-	-	14.5	19.3	14.5	15.7	20.6	11.4	25.7	11	6.4	24	89	67	89	82	1.9	7.7	1.9	3.8	6.4	7.5	6.1	6.7
IX	-	-	-	-	9.5	14.3	10.3	11.1	15.5	7.3	26.7	9	1.3	27	91	70	86	82	1.1	5.6	1.8	2.8	7.8	8.1	5.8	7.2
X	-	-	-	-	6.6	11.6	8.1	8.6	12.4	5.0	18.0	19	0.9	2	92	76	87	85	0.8	3.4	1.4	1.9	7.5	8.0	5.8	7.1
XI	-	-	-	-	3.7	6.2	4.2	4.6	7.1	2.0	14.9	5	-7.6	30	89	79	86	85	0.8	2.1	1.2	1.4	8.5	8.5	7.3	8.1
XII	-	-	-	-	-4.2	0.3	-0.7	-0.6	1.5	-3.2	7.3	5	-12.1	17	90	86	91	89	0.6	0.8	0.5	0.6	7.5	7.8	7.0	7.4
Rok	-	-	-	-	6.3	10.5	6.9	7.6	11.7	3.8	31.2	8.VII	-12.9	16.1	87	71	86	81	1.4	4.9	1.6	2.6	7.2	7.4	6.2	6.9

Siejnik

$H_s = 170\ m$ $h_w = 12\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, %nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0	Max<0	Min<-10	Max>25°	Opad R ≥0.1	≥1.0	≥10.0	Wiatr ≥10	≥15	=	≥25	◔	◕	⊞
I	·		10	6.7	1	3.0	9	5.9	7	3.1	40	5.1	14	6.0	3	4.7	9	4.8	37.8	12.4	6	27	12	7	·	12	7	2	2	·	-	·	2	23	-
II	2	3.0	3	3.0	4	3.0	6	4.0	9	3.4	51.5	3.8	6.5	3.3	1	3.0	1	3.6	36.5	7.1	8	21	4	·	·	15	10	·	2	·	-	·	·	22	-
III	3.5	4.3	8.5	2.8	11.5	5.2	16.5	8.3	5	4.4	9	4.8	1.8	6.9	1.8	6.0	3	5.7	19.0	4.7	15	25	8	4	·	9	5	·	7	4	-	·	2	13	-
IV	8	3.4	7	2.3	7	3.1	5.5	2.8	9	4.9	2.5	4.1	8.5	3.5	1.4	5.6	6	3.7	20.8	11.0	3.0	8	·	·	1	8	5	1	3	·	-	1	2	8	-
V	5	3.8	10	4.3	4.5	5.1	9.5	3.9	7	3.7	6.5	5.9	12.5	6.4	2.3	4.2	15	3.9	33.4	9.7	7	2	·	·	1	11	8	·	2	·	-	1	2	6	-
VI	3	3.3	1	3.0	·	·	5	5.6	7	4.1	17.5	4.7	24.5	4.6	1.4	4.6	18	3.7	46.4	28.9	22	·	·	·	5	8	7	1	2	·	-	3	4	8	-
VII	1	2.0	5	4.2	6.5	4.8	6.5	4.5	1.4	3.5	17.5	4.3	17.5	5.1	7	2.4	18	3.4	135.3	28.0	18	·	·	·	5	21	17	4	·	·	-	5	1	17	-
VIII		·	1	3.0	1.5	3.0	6.5	4.7	14.5	3.9	2.5	5.3	2.7	4.4	3.5	3.4	14	3.8	167.8	50.0	17	·	·	·	1	13	12	5	2	·	-	1	·	8	-
IX	·	·	·	·	·	·	1	3.0	1.4	4.1	3.7	5.4	1.4	6.4	9	5.4	15	4.4	218.4	51.2	15	·	·	·	1	17	14	7	3	·	-	·	·	15	-
X	·	·	·	·	·	·	1	3.0	12.5	3.1	60.5	4.6	1.0	7.1	1	3.0	8	4.2	20.3	4.9	6	·	·	·	·	8	7	·	4	·	-	·	2	14	-
XI	1	5.0	8	3.5	1	7.0	1.6	6.1	12.5	4.5	2.8	3.5	1.2	3.6	6.5	9.6	5	4.4	38.1	15.5	28	15	-	·	·	11	8	1	3	·	-	·	1	22	-
XII	4	3.0	1	3.0	7	5.0	1	2.0	1.2	5.6	3.6	5.0	1.6	6.2	3	5.3	1.3	4.5	34.3	10.6	13	25	-	5	·	10	7	1	4	1	-	·	3	19	-
Rok	27.5	2.3	54.5	3.0	4.4	3.3	83.5	4.5	123.5	4.0	353.5	4.7	180.5	5.3	10.3	4.8	125	4.2	808.1	51.2	15.IX	123	-	16	1.4	143	107	22	34	5	-	11	19	175	-

Miastko

$H_s = 145\ m$ $h_w = 11\ m$

I	1	1.0	4	2.0	1	2.0	3	1.3	3.1	1.8	1.2	2.2	2.0	2.5	4.0	4.2	1.1	2.0	28.9	11.8	5	23	10	2	·	15	5	1	·	·	-	·	2	20	22
II	3	1.7	2	1.0	1	2.0	4	1.2	2.7	1.8	1.3	2.1	2.2	2.6	7	1.4	5	1.9	36.2	6.6	8	16	·	·	·	15	11	·	·	·	-	·	1	18	3
III	4	4.0	3	2.0	4	3.5	1.1	3.1	2.3	2.0	1.1	1.8	1.8	3.4	7	1.6	1.2	2.2	30.2	11.3	15	21	·	·	·	8	7	1	1	·	-	·	8	9	-
IV	8	1.9	2	2.0	6	2.2	2	1.0	1.0	1.2	5	3.2	2.7	1.7	1.4	2.1	1.6	1.5	30.7	7.9	30	11	·	·	·	1.4	8	·	·	·	-	2	5	7	1
V	9	2.1	2	2.5	2	3.0	7	1.9	9	1.4	8	2.2	3.6	1.7	1.3	1.8	7	1.7	44.4	8.2	5	4	·	·	·	1.3	12	·	·	·	-	3	6	10	1
VI	·	·	2	2.0	1	1.0	4	2.0	9	1.8	1.7	1.6	3.8	1.8	8	2.4	1.1	1.6	34.8	16.7	9	·	·	·	8	9	8	1	·	·	-	1	8	4	-
VII	1	3.0	1	3.0	·	·	2	2.5	1.1	1.7	1.7	1.8	4.5	1.9	9	2.6	7	1.8	117.9	20.5	21	·	·	·	11	22	1.8	3	·	·	-	9	4	8	-
VIII	1	1.0	·	·	·	·	5	1.6	1.4	2.1	1.9	2.6	3.4	1.8	4	2.0	1.6	1.7	118.7	25.5	10	·	·	·	2	20	1.7	5	·	·	-	4	1	8	-
IX	·	·	·	·	·	·	·	·	2.2	2.2	9	2.7	3.8	3.1	6	4.2	1.5	2.4	80.8	15.9	27	2	·	·	2	23	1.8	1	2	·	-	1	1	14	-
X	·	·	·	·	·	·	·	·	2.8	2.4	2.2	3.1	3.2	2.1	·	·	11	2.2	27.2	4.9	23	1	·	·	·	16	7	·	·	·	-	·	2	12	-
XI	4	2.0	3	3.3	7	2.1	1.4	2.4	1.8	1.6	1.0	2.8	1.3	2.8	9	3.3	1.2	2.1	39.2	8.7	28	12	1	1	·	13	8	·	·	·	-	·	2	20	1
XII	3	2.7	3	3.3	4	2.2	8	1.9	1.7	2.5	1.5	2.5	2.8	2.8	9	2.9	6	2.4	48.5	17.0	8	22	8	4	·	12	8	1	·	·	-	·	2	19	7
Rok	3.4	1.6	2.2	1.8	2.6	1.5	6.0	1.6	21.9	1.9	15.8	2.4	35.1	2.4	9.6	2.4	129	2.0	637.5	25.5	10.VIII	112	1.9	7	2.3	180	127	13	3	·	-	20	42	149	-

Ramlewo Dolne

$H_s = 45\ m$ $h_w = 10\ m$

I	0.5	1.0	2	5.8	6.5	7.4	6	2.7	8.5	4.4	3.7	4.3	1.9	6.5	6.5	7.0	7	4.7	36.0	11.2	12	21	6	2	·	11	9	1	4	·	-	·	1	21	-
II	1.5	3.0	5.5	3.0	2.5	1.8	2	3.2	1.2	3.4	27.5	4.2	19.5	4.2	3.5	5.6	1.0	3.4	28.5	8.1	8	15	·	·	·	10	7	·	1	·	-	·	1	10	-
III	4.5	4.1	3.5	5.6	7.5	6.1	1.5	5.2	15.5	4.3	1.3	3.6	1.3	6.5	2	7.0	1.9	4.0	30.6	12.2	15	18	·	·	·	6	6	1	5	·	-	1	11	7	-
IV	1.6	3.8	1.1	4.0	9	3.5	1.5	2.3	2	3.2	3	4.2	1.3	3.8	15.5	3.2	1.9	2.9	31.1	12.5	27	12	·	·	·	9	5	1	·	·	-	1	3	11	-
V	1.9	3.7	2.1	5.0	3.5	3.1	·	·	·	·	3.5	3.4	1.6	4.6	1.5	3.7	1.5	3.5	18.9	9.0	13	5	·	·	·	9	4	·	1	·	-	1	2	6	-
VI	2	4.5	·	·	2.0	3.2	1.3	3.3	15.5	3.2	12.5	2.8	7	3.7	7	2.7	1.3	2.7	30.1	10.5	5	-	-	-	-	6	6	1	·	·	-	1	·	5	-
VII	1	1.0	7	2.9	26.5	3.4	3.8	2.5	5.5	3.1	3	3.3	2	4.5	3	3.7	7	2.7	62.3	10.2	21	-	-	-	-	17	17	1	·	·	-	5	·	1	-
VIII	3	5.7	1.7	3.2	12.5	4.7	9.5	2.7	3.5	3.7	15.5	3.6	1.4	3.9	6	4.3	1.2	3.3	168.5	-	-	-	-	-	-	17	17	4	·	·	-	·	·	4	-
IX	0.5	2.0	1	2.0	·	·	1	2.0	4.5	4.0	2.8	4.0	2.8.5	3.6	1.3.5	4.4	1.3	3.4	102.7	20.2	3	-	-	-	-	1.3	1.3	4	·	·	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Radostowo

$H_s = 40\ m$ $h_w = 12\ m$

I	2	2.8	7.5	3.3	2	1.2	3	5.3	1.5	4.2	30.5	6.2	13.5	6.2	4.5	4.1	1.5	4.3	9.5	5.3	28	25	8	2	·	5	3	·	5	·	2	-	1	17	23
II	5.5	3.4	3	3.8	1.5	2.3	1.3	4.4	15.5	3.7	20	4.6	11.5	4.8	3	6.7	1.1	4.2	40.4	7.0	18	15	·	·	·	1.9	12	·	·	·	6	-	·	19	4
III	15.5	4.1	5.5	1.5	1.0	3.4	5.5	4.4	9.5	4.7	19.5	5.0	9	5.7	8.5	4.7	1.0	3.9	22.6	6.3	15	21	2	·	·	6	5	·	3	·	2	-	5	12	3
IV	3.5.5	4.2	5	3.0	4	1.9	1	2.0	4	4.8	6.5	4.4	9	4.4	9	3.0	1.6	3.2	16.4	5.8	22	7	·	·	·	1.0	5	·	2	·	5	-	5	12	1
V	2.6	4.4	8.5	3.9	2.5	1.2	1.0	3.2	2	3.8	11	5.7	4.5	4.2	16.5	4.6	1.2	3.8	43.9	11.5	9	1	·	·	·	11	10	1	3	·	1	-	2	9	·
VI	15.5	2.9	5	2.6	3.5	2.9	4	3.2	4.5	2.6	11.5	3.8	15.5	3.5	14.5	4.0	1.6	2.7	31.2	6.3	24	·	·	·	6	1.0	9	·	·	·	2	-	5	8	·
VII	11.5	2.3	10.5	2.0	4	1.9	5.5	3.2	4	4.5	11	3.6	11.5	3.3	1.4	5.4	2.1	2.6	79.3	21.3	16	·	·	·	11	16	10	3	2	·	·	-	1	10	
VIII	8	2.1	3	1.8	3.5	1.9	8.5	2.8	13.5	4.0	17	4.5	16.5	4.3	1.0	3.6	1.3	3.1	119.1	20.5	14	·	·	·	2	17	15	5	·	·	·	-	·	13	
IX	2	3.5	0.5	1.0	0.5	2.0	6	3.1	25.5	4.5	1.4	3.9	25.5	4.6	7	4.6	9	3.9	37.0	9.1	23	·	·	·	2	17	11	·	3	·	2	-	1	14	·
X	0.5	2.0	1.5	2.0	0.5	1.0	4	3.1	2.4	4.6	3.4	4.6	1.3	3.8	4.5	2.7	1.1	3.7	10.3	3.9	30	·	·	·	·	8	4	·	1	·	8	-	2	13	·
XI	2.5	5.0	9.5	3.2	5	2.2	8	3.6	13.5	4.1	1.7	3.2	11.5	5.5	3	7.0	2.0	3.1	13.1	3.6	28	9	1	·	·	9	5	·	1	·	1	-	1	19	1
XII	4	4.6	7	4.1	1.5	3.7	2	2.2	28.5	4.1	25.5	5.7	1.1	6.3	1.5	6.7	1.2	4.3	7.8	3.3	13	23	11	4	·	10	2	·	2	·	1	-	1	15	8
Rok	128.5	3.4	66.5	2.7	38.5	2.1	70.5	3.4	159.5	4.1	217.5	4.6	152	4.7	96	4.8	16.6	3.6	430.6	21.3	16.VII	101	22	6	2.1	138	91	9	22	·	30	-	24	151	40

Międzyzdroje

$\varphi = 53°56'$ $\lambda = 14°27'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA t								ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.p.}$	Średnia				Max	Min	Max abs.	Data	Min abs	Data										
					I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	2.1	0.9	1.2	3.1	-1.2	10.4	6	-8.9	15	89	84	88	87	0.6	1.1	0.7	0.8	8.5	7.5	7.2	7.7
II	–	–	–	–	1.7	4.7	2.9	3.0	6.1	0.2	10.9	2	-5.1	26	91	79	90	87	0.6	1.9	0.8	1.1	7.0	6.9	5.5	6.5
III	–	–	–	–	1.5	7.0	3.2	3.7	8.8	-0.2	16.9	13	-5.4	6	87	63	81	77	0.9	3.9	1.6	2.1	5.4	4.7	4.6	4.9
IV	–	–	–	–	4.4	7.8	4.9	5.5	10.2	1.6	21.6	5	-4.7	13	87	75	84	82	1.2	3.0	1.6	1.9	7.2	5.7	5.3	6.1
V	–	–	–	–	9.1	13.3	8.5	9.8	14.9	5.1	26.0	16	-1.1	9	78	61	82	74	2.7	7.0	2.2	4.0	5.9	5.4	5.0	5.4
VI	–	–	–	–	15.2	18.8	14.8	15.9	21.3	10.7	30.9	11	6.0	1	78	68	79	75	4.0	7.9	3.7	5.2	5.4	5.2	3.8	4.8
VII	–	–	–	–	17.3	20.3	17.6	18.2	22.5	14.5	30.9	1,4	10.7	16	85	74	83	81	3.1	6.9	3.8	4.6	7.0	6.2	6.9	6.7
VIII	–	–	–	–	14.9	19.1	15.5	16.2	20.5	12.5	27.4	11	8.1	23	88	68	84	80	2.1	7.3	3.1	4.2	6.4	6.6	5.1	6.0
IX	–	–	–	–	11.0	14.1	11.1	11.8	15.4	8.2	23.3	7	3.5	26	88	72	85	82	1.6	4.8	2.1	2.8	7.8	7.4	6.1	7.1
X	–	–	–	–	8.6	12.1	9.9	10.1	12.8	7.0	18.7	9	2.0	2	91	76	89	85	1.0	3.5	1.4	2.0	9.0	7.0	7.6	7.9
XI	–	–	–	–	4.3	6.6	5.2	5.3	7.4	2.8	14.3	6	-4.4	30	88	79	85	84	1.0	2.1	1.4	1.5	8.4	7.9	7.4	7.9
XII	–	–	–	–	0.4	1.8	1.0	1.0	3.2	-1.4	9.3	8	-11.5	17	89	85	87	87	0.7	1.0	0.7	0.8	8.9	8.3	6.7	8.0
Rok	–	–	–	–	7.4	10.6	8.0	8.5	12.2	5.0	30.9	11.VI, 1,4.VII	-11.5	17.XII	87	74	85	82	1.6	4.2	1.9	2.6	7.2	6.6	5.9	6.6

Świnoujście

$\varphi = 53°55'$ $\lambda = 14°16'$

I	1018.3	1032.3	998.7	1018.9	1.0	2.5	1.2	1.5	3.3	-0.8	10.3	6	-7.6	15	90	84	89	88	0.6	1.2	0.7	0.8	8.1	6.8	7.1	7.3
II	1007.7	1038.2	979.5	1008.3	1.7	5.0	2.8	3.1	6.1	0.4	10.9	2	-6.1	26	92	80	90	87	0.6	1.8	0.7	1.0	6.0	7.1	5.1	6.1
III	1016.3	1038.2	994.0	1016.9	1.5	7.1	3.2	3.8	8.5	-0.1	17.0	13	-6.2	6	89	65	83	79	0.8	3.9	1.4	2.0	5.1	5.2	3.9	4.7
IV	1019.0	1032.0	999.6	1019.6	4.3	7.4	4.7	5.3	8.7	2.0	21.9	5	-3.5	15	87	74	84	82	1.1	3.0	1.4	1.8	6.9	7.1	4.4	6.0
V	1016.5	1031.3	1006.3	1017.0	8.8	12.9	9.0	9.9	14.0	5.3	25.0	16	0.1	6,8	80	61	79	73	2.4	6.7	2.3	3.8	5.7	5.0	4.5	5.1
VI	1015.6	1032.4	1003.1	1016.1	15.0	18.7	14.9	15.9	20.5	10.6	31.2	11	6.8	24	78	64	80	74	3.9	8.4	3.5	5.3	5.3	5.2	2.9	4.5
VII	1011.1	1022.8	1001.2	1011.6	17.3	20.4	17.7	18.3	24.9	14.4	30.3	1	11.1	16	88	77	87	84	2.5	6.0	2.8	3.8	6.3	6.4	6.1	6.3
VIII	1011.5	1023.6	997.3	1012.0	15.0	19.5	15.7	16.5	20.3	12.6	26.3	11	8.0	23	90	73	87	83	1.7	6.1	2.3	3.4	5.7	6.3	5.2	5.9
IX	1009.8	1023.2	987.4	1010.3	10.6	14.6	10.7	11.6	15.5	8.1	23.3	7,8	3.4	26	90	72	89	84	1.3	5.0	1.5	2.6	6.9	7.4	4.2	6.2
X	1015.8	1027.6	999.2	1016.3	8.5	12.5	9.8	10.2	13.0	7.2	16.7	10,18	1.9	2	93	76	90	86	0.8	3.5	1.2	1.8	7.4	6.9	6.6	7.0
XI	1019.3	1037.8	998.4	1019.8	4.7	6.8	5.7	5.7	7.5	3.8	13.7	1	-4.2	21	90	82	86	86	0.8	1.9	1.2	1.3	7.8	8.0	7.8	7.9
XII	1012.5	1030.6	997.9	1013.1	0.9	2.0	1.3	1.4	3.4	-0.6	9.3	8	-8.7	17	89	84	88	87	0.7	1.1	0.8	0.9	8.3	7.8	5.7	7.3
Rok	1014.4	1038.2	979.9	1014.9	7.4	10.8	8.1	8.6	11.9	5.2	31.2	11.VI	-8.7	17.XII	88	74	86	83	1.4	4.0	1.7	2.4	6.6	6.6	5.3	6.2

Gryfice

$\varphi = 53°55'$ $\lambda = 15°13'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	14.1	19.3	14.4	15.6	20.3	10.9	26.3	11	6.6	23	91	69	91	84	1.5	7.2	1.7	3.5	7.1	7.9	7.4	7.5
IX	–	–	–	–	9.9	14.1	10.2	11.1	15.3	7.5	24.5	8	2.8	27	92	73	91	85	1.0	4.7	1.1	2.3	8.2	8.2	6.7	7.7
X	–	–	–	–	7.6	12.2	9.0	9.4	12.8	6.2	16.9	10	0.6	21	93	76	90	86	0.8	3.4	1.1	1.8	9.4	8.5	7.7	8.5
XI	–	–	–	–	3.5	6.1	4.2	4.5	7.2	1.9	12.9	1	-5.5	21	90	82	86	86	0.8	1.8	1.1	1.2	9.1	8.4	8.2	8.6
XII	–	–	–	–	-0.2	1.2	0.5	0.5	2.6	-2.3	8.7	8	-12.1	17	91	86	88	88	0.5	0.9	0.7	0.7	9.2	8.8	7.7	8.6
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wirty

$\varphi = 53°54'$ $\lambda = 18°23'$

I	–	–	–	–	-1.4	0.7	-0.6	-0.5	1.5	-3.0	9.3	6	-13.5	15	90	89	91	90	0.5	0.7	0.5	0.6	8.8	8.7	7.8	8.4
II	–	–	–	–	1.0	4.1	2.1	2.3	4.7	0.1	8.3	2	-3.0	4,25,27,28	–	–	–	–	–	–	–	–	8.6	7.0	7.4	7.7
III	–	–	–	–	-0.1	5.7	1.3	2.0	6.9	-1.6	16.8	31	-7.0	9	–	–	–	–	–	–	–	–	4.9	4.9	3.6	4.5
IV	–	–	–	–	3.8	10.0	4.6	5.8	11.0	1.1	23.3	29	-6.5	13	–	–	–	–	–	–	–	–	5.6	6.1	5.9	5.9
V	–	–	–	–	8.4	13.2	9.0	9.9	14.5	4.7	23.8	19,20	-2.0	6	–	–	–	–	–	–	–	–	5.1	5.7	4.6	5.1
VI	–	–	–	–	13.0	19.3	14.2	15.2	21.2	8.6	28.9	11	5.5	16	–	–	–	–	–	–	–	–	4.9	5.1	4.7	4.9
VII	–	–	–	–	16.2	21.6	17.5	18.2	23.7	13.3	31.4	8	9.0	7	88	70	89	82	2.5	8.7	2.3	4.5	5.8	5.6	6.0	5.8
VIII	–	–	–	–	13.8	19.7	15.5	16.1	21.0	11.1	25.3	11	7.0	26	–	–	–	–	–	–	–	–	5.6	6.3	5.4	5.8
IX	–	–	–	–	9.2	14.1	10.5	11.1	15.6	7.1	26.9	9	1.0	26	92	77	92	87	1.0	4.2	1.1	2.1	7.2	7.3	6.8	7.1
X	–	–	–	–	6.6	11.4	7.5	8.2	12.7	4.4	19.3	10	0.5	2	91	78	90	86	0.9	2.9	1.0	1.6	8.3	7.5	4.4	6.7
XI	–	–	–	–	3.6	6.1	4.3	4.6	7.1	1.8	13.8	5	-7.0	30	91	82	90	88	0.7	1.7	0.8	1.1	9.4	8.0	7.6	8.3
XII	–	–	–	–	-1.6	0.4	-0.8	-0.7	1.2	-3.1	6.8	5,8	-15.0	17	89	89	90	89	0.6	0.7	0.6	0.6	8.2	8.5	7.3	8.0
Rok	–	–	–	–	6.0	10.5	7.1	7.7	11.8	3.7	31.4	8.VII	-15.0	17.XII	–	–	–	–	–	–	–	–	6.9	6.7	6.0	6.5

Międzyzdroje

$H_s = 10\,m$ $h_w = 14\,m$ **1957**

| MIESIĄC | ROZKŁAD WIATRU °D, ᵛmD | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | |

Biskupiec

$\varphi = 53°52'$ $\lambda = 20°57'$ 1951

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.6	-0.6	-4.6	-4.6	0.4	-5.0	8.1	6	-22.3	16	93	89	91	91	0.3	0.6	0.5	0.5	9.2	8.2	7.8	8.4
II	–	–	–	–	0.7	2.9	4.1	4.4	3.6	-0.6	7.4	16	-4.8	28	95	88	93	92	0.3	0.9	0.5	0.6	9.8	8.5	8.1	8.8
III	–	–	–	–	-1.8	4.5	0.3	0.8	5.6	-3.9	17.9	31	-17.9	17	85	62	81	76	0.8	3.8	1.3	2.0	7.5	6.2	5.2	6.3
IV	–	–	–	–	4.4	12.2	5.9	7.1	13.2	0.7	25.2	27	-7.3	14	86	49	82	72	1.4	8.4	1.9	3.9	6.9	6.2	6.4	6.5
V	–	–	–	–	8.5	13.3	8.7	9.8	14.7	4.2	25.4	19	-3.1	6	84	61	83	76	2.0	6.9	2.1	3.7	6.9	7.5	6.3	6.9
VI	–	–	–	–	14.7	19.5	14.1	15.6	20.9	9.1	28.0	11	3.2	21	78	59	82	73	3.8	10.1	3.0	5.6	6.4	6.4	6.7	6.5
VII	–	–	–	–	16.7	21.7	16.2	17.7	23.1	12.3	29.4	8	6.7	7	86	66	86	79	2.7	9.2	2.7	4.9	7.9	7.2	8.0	7.7
VIII	–	–	–	–	14.2	19.1	14.6	15.6	20.3	10.7	28.0	12	5.5	24	89	68	88	82	1.8	7.6	2.0	3.8	6.8	7.6	7.0	7.1
IX	–	–	–	–	9.4	13.8	9.8	10.7	14.8	6.9	26.4	9	0.9	17	94	76	91	87	0.8	4.6	1.2	2.2	8.7	8.1	7.8	8.2
X	–	–	–	–	6.1	11.0	7.3	7.9	11.8	4.0	19.4	10	-0.2	3	96	79	91	89	0.4	3.0	0.9	1.4	8.5	8.2	7.5	8.1
XI	–	–	–	–	3.2	5.0	3.7	3.9	6.2	1.7	14.1	6	-9.1	30	92	85	92	90	0.6	1.4	0.7	0.9	9.5	9.1	9.1	9.2
XII	–	–	–	–	-2.5	-0.9	-2.0	-1.8	0.3	-4.5	5.9	5	-14.6	18	90	89	91	90	0.5	0.6	0.4	0.5	9.1	8.5	8.4	8.7
Rok	–	–	–	–	5.9	10.1	6.5	7.2	11.2	3.0	29.4	8.VII	-22.3	16.1	89	73	88	83	1.3	4.8	1.4	2.5	8.1	7.6	7.4	7.7

Nikutowo

$\varphi = 53°50'$ $\lambda = 21°18'$

I	–	–	–	–	-2.6	-0.7	-1.6	-1.6	0.6	-4.7	8.4	6	-22.5	16	92	91	93	92	0.3	0.5	0.3	0.4	9.0	8.7	8.8	8.8
II	–	–	–	–	0.9	2.6	1.4	1.6	3.8	-0.5	7.6	2	-5.4	28	95	91	94	93	0.3	0.7	0.4	0.5	9.7	9.5	9.5	9.6
III	–	–	–	–	-2.1	3.8	0.3	0.6	5.3	-3.9	17.5	31	-16.8	17	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	3.9	11.6	6.0	6.9	13.1	0.9	24.5	27	-7.9	14	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	8.4	12.9	8.8	9.7	14.5	4.3	25.5	19	-2.5	2,6	86	62	83	77	1.7	6.6	2.1	3.5	6.4	7.8	8.4	7.5
VI	–	–	–	–	14.3	18.8	14.3	15.4	20.8	9.6	28.3	11	3.7	21	82	61	81	75	3.0	9.3	3.2	5.2	6.1	7.5	7.1	6.9
VII	–	–	–	–	16.2	21.3	16.6	17.7	23.0	13.0	29.8	8	7.3	4,7	88	65	86	80	2.3	9.5	2.8	4.9	7.4	7.8	8.0	7.7
VIII	–	–	–	–	13.8	18.6	14.3	15.2	20.2	11.2	28.1	12	5.5	24	–	–	–	–	–	–	–	–	6.4	8.3	8.4	7.7
IX	–	–	–	–	9.2	13.7	9.8	10.6	15.0	7.1	26.1	9	2.0	17	94	75	92	87	0.7	4.6	1.1	2.1	8.9	8.8	9.8	9.2
X	–	–	–	–	5.9	10.8	7.7	8.0	–	4.6	–	–	0.3	3	96	80	92	89	0.4	2.7	0.9	1.3	8.0	8.6	10.0	8.9
XI	–	–	–	–	3.2	5.0	3.8	4.0	–	2.0	–	–	-8.7	30	95	89	93	92	0.4	1.1	0.6	0.7	9.6	8.9	9.9	9.5
XII	–	–	–	–	-2.6	-0.8	-2.1	-1.9	–	-4.5	–	–	-14.2	18	–	–	–	–	–	–	–	–	9.9	8.8	10.0	9.6
Rok	–	–	–	–	5.7	9.8	6.6	7.2	–	3.3	29.8	8.VII	-22.5	16.1	–	–	–	–	–	–	–	–	–	–	–	–

Orzysz

$\varphi = 53°48'$ $\lambda = 21°57'$

I	–	–	–	–	-2.6	-0.6	-1.4	-1.5	0.3	-5.0	7.0	6	-25.0	16	–	–	–	–	–	–	–	–	8.4	8.4	7.4	8.1
II	–	–	–	–	0.6	2.5	1.4	1.5	3.5	-1.0	7.6	21	-8.5	28	–	–	–	–	–	–	–	–	8.4	8.7	8.2	8.4
III	–	–	–	–	-2.3	3.8	0.1	0.4	5.1	-4.8	16.7	31	-14.1	17	–	–	–	–	–	–	–	–	5.7	6.2	4.9	5.6
IV	–	–	–	–	4.7	12.3	6.7	7.6	13.5	1.2	25.3	27,28	-6.7	14	–	–	–	–	–	–	–	–	5.2	6.0	5.2	5.5
V	–	–	–	–	9.4	13.5	9.4	10.4	15.0	4.8	25.7	19	-2.9	6	–	–	–	–	–	–	–	–	5.2	7.3	5.4	6.0
VI	–	–	–	–	13.7	19.2	16.3	16.4	21.2	9.6	28.6	11	4.9	21	–	–	–	–	–	–	–	–	5.4	6.0	5.2	5.5
VII	–	–	–	–	15.5	21.2	18.5	18.4	23.0	13.2	29.0	8	6.8	7	–	–	–	–	–	–	–	–	7.0	7.5	6.1	6.9
VIII	–	–	–	–	13.4	18.8	15.9	16.0	20.3	11.8	28.1	12	4.4	24	–	–	–	–	–	–	–	–	5.9	7.7	6.1	6.6
IX	–	–	–	–	8.8	13.6	10.7	11.0	15.0	7.2	26.3	9	1.2	17	–	–	–	–	–	–	–	–	8.0	7.9	5.9	7.3
X	–	–	–	–	6.1	11.0	7.8	8.2	12.0	4.5	18.4	10	0.5	16	–	–	–	–	–	–	–	–	6.8	7.5	5.3	6.5
XI	–	–	–	–	3.3	5.1	3.9	4.0	6.4	1.6	14.2	6	-9.9	29	–	–	–	–	–	–	–	–	8.6	8.8	8.6	8.7
XII	–	–	–	–	-2.5	-0.6	-2.1	-1.8	0.6	-4.6	5.6	5	-14.4	19	–	–	–	–	–	–	–	–	6.8	7.8	6.7	7.1
Rok	–	–	–	–	5.7	10.0	7.3	7.6	11.3	3.2	29.0	8.VII	-25.0	16.1	–	–	–	–	–	–	–	–	6.8	7.5	6.2	6.8

Mikołajki I

$\varphi = 53°47'$ $\lambda = 21°35'$

I	1002.2	1015.3	980.2	1018.9	-2.3	-0.2	-1.1	-1.2	1.0	-4.3	7.9	6	-19.9	16	91	90	91	91	0.4	0.7	0.6	0.6	8.3	8.5	7.5	8.1
II	999.6	1016.9	970.2	1010.1	0.9	2.9	1.4	1.6	4.0	-0.5	8.8	2	-5.8	28	94	84	90	89	0.3	1.2	0.7	0.7	9.2	8.9	7.3	8.5
III	1002.0	1019.3	973.8	1018.6	-1.7	3.9	0.5	0.8	5.3	-3.6	14.9	28	-14.0	17	84	57	75	72	0.9	4.0	1.8	2.2	6.6	5.6	5.8	6.0
IV	1004.9	1015.0	975.9	1018.0	4.9	11.5	6.6	7.4	12.9	1.6	25.3	29	-6.6	10	88	55	79	74	1.1	7.0	2.4	3.5	5.9	5.8	6.4	6.0
V	999.7	1011.9	987.3	1015.7	9.1	12.7	8.7	9.8	14.2	5.2	23.7	19	-1.9	6	84	68	83	78	1.9	5.1	2.1	3.0	6.2	7.2	6.3	6.6
VI	1000.0	1013.7	985.8	1015.7	14.8	19.0	14.4	15.6	20.5	9.8	26.9	11	5.2	27	80	64	82	75	3.4	8.4	3.0	4.9	4.8	5.6	4.3	4.9
VII	–	–	–	–	16.8	21.4	16.6	17.8	22.4	13.4	28.5	8	8.5	7	87	68	88	81	2.6	8.2	2.4	4.4	6.2	6.5	5.4	6.0
VIII	996.7	1006.1	986.4	1012.3	14.4	18.9	14.6	15.6	19.9	11.6	27.8	12	6.6	24	–	–	–	–	–	–	–	–	5.6	6.5	4.8	5.6
IX	994.1	1006.0	977.0	1010.0	9.7	13.8	10.1	10.9	14.5	7.5	25.9	9	1.8	26,27	93	77	91	87	0.8	4.0	1.1	2.0	7.0	7.2	5.9	6.7
X	1001.3	1014.8	988.7	1017.4	6.2	11.1	7.9	8.3	–	4.7	–	–	-0.1	3	91	76	88	85	0.8	3.3	1.3	1.8	7.5	7.9	6.2	7.2
XI	–	–	–	–	3.6	5.1	4.0	4.2	6.1	2.1	13.8	6	-8.2	29	91	85	89	88	0.7	1.4	0.9	1.0	9.4	9.0	9.0	9.1
XII	–	–	–	–	-2.3	-0.6	-1.9	-1.7	0.4	-4.3	5.7	5	-14.4	19	–	–	–	–	–	–	–	–	8.0	8.7	7.4	8.0
Rok	–	–	–	–	6.2	10.0	6.8	7.4	–	3.6	28.5	8.VII	-19.9	16.1	–	–	–	–	–	–	–	–	7.1	7.3	6.4	6.9

Biskupiec

$H_s = 160\ m$ $h_w = 14\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D,°mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0.1	1	10	Wiatr 10	15	≡	≈	◔	●	⊡
I	1	4.0	6	3.5	3	3.7	8	3.4	12	2.7	48	4.0	11	4.1	4	2.5	·	3.7	36.4	9.7	5	26	12	7	·	13	8	·	2	·	7	·	·	18	26
II	3	1.0	2	1.0	·	·	7	1.1	21	2.4	39	2.6	9	2.7	3	2.3	·	2.3	44.0	9.3	18	16	2	·	·	15	11	·	·	·	5	·	·	20	2
III	1	1.0	11	2.7	7	4.0	17	5.0	10	3.0	17	3.1	15	3.1	15	3.5	·	3.5	21.8	10.2	15	25	5	1	·	8	5	1	3	·	2	·	·	8	4
IV	10	2.6	10	1.7	4	2.5	7	2.3	7	4.1	10	2.8	12	2.8	30	2.2	·	2.5	33.2	18.2	30	12	·	·	1	14	6	1	·	·	3	4	1	7	1
V	10	1.9	2	2.5	7	2.3	11	2.2	6	2.2	15	3.0	14	2.6	28	2.6	·	2.5	50.1	16.2	14	3	·	·	1	12	8	2	1	·	3	3	1	10	·
VI	3	1.7	2	1.5	2	3.5	8	2.8	5	1.6	21	2.3	22	2.7	27	2.6	·	2.5	59.4	19.8	10	·	·	·	5	11	8	1	·	·	·	3	1	10	·
VII	3	1.0	6	2.2	8	3.5	11	1.5	7	1.9	21	2.2	27	2.3	10	1.3	·	2.1	121.7	22.6	30	·	·	·	7	16	15	5	·	·	5	7	1	15	·
VIII	·	·	1	1.0	2	3.0	4	2.5	9	2.9	40	3.2	28	2.1	9	2.4	·	2.7	147.1	66.9	17	·	·	·	1	14	14	5	·	·	5	1	·	11	·
IX	·	·	·	·	·	·	3	3.7	13	3.6	44	3.5	25	3.1	5	1.8	·	3.3	114.6	20.2	15	·	·	·	1	19	15	4	1	·	6	1	·	15	·
X	·	·	·	·	·	·	3	2.0	27	3.1	48	3.2	13	2.5	2	3.0	·	3.0	11.6	3.1	30	1	·	·	·	12	5	·	·	·	8	·	2	17	·
XI	2	1.0	7	2.7	5	4.4	17	3.5	12	2.5	24	2.6	12	2.2	11	2.9	·	2.8	22.2	8.2	28	12	1	·	·	9	5	·	·	·	6	·	·	25	·
XII	2	2.5	3	2.7	4	4.2	4	2.0	16	2.4	41	3.9	12	1.8	11	2.6	·	3.1	30.3	9.3	8	25	13	5	·	15	9	·	1	·	7	·	·	23	1
Rok	35	1.4	50	1.8	42	2.6	100	2.7	145	2.7	368	3.0	200	2.7	155	2.5	·	2.8	689.4	66.9	17.VIII	120	33	13	16	158	109	19	8	·	57	19	6	179	34

Nikutowo

$H_s = 140\ m$ $h_w = 14\ m$

I	0.5	4.0	5	3.9	3	1.7	2.5	2.4	14	3.7	30.5	4.2	21.5	5.2	2	4.0	14	3.6	43.4	10.2	13	26	11	5	·	17	10	1	1	·	–	·	·	23	25
II	4	2.2	·	·	·	·	·	·	12	3.0	37.5	3.3	14.5	3.6	8	2.8	8	2.9	42.2	10.0	18	16	4	·	·	15	12	1	·	·	–	·	·	26	5
III	6.5	2.8	3.5	2.3	6.5	3.4	6.5	3.5	7.5	2.7	18	3.3	15	3.7	16.5	3.4	13	2.8	31.5	16.9	15	24	6	3	·	11	6	1	·	·	–	·	–	–	5
IV	19	3.1	4	2.0	5.5	1.5	2	1.0	1.5	2.7	9	3.0	17	2.4	19	2.6	13	2.2	39.4	18.0	28	12	·	·	·	14	8	1	·	·	–	3	–	–	
V	25.5	2.5	8.5	1.7	3.5	1.9	·	·	·	·	9.5	2.1	15.5	2.5	24.5	2.7	6	2.3	51.5	20.4	14	3	·	·	1	14	7	1	·	·	–	4	1	16	·
VI	8	2.7	1.5	1.3	0.5	2.0	1	4.0	1.5	1.0	13.5	2.7	3.1	2.2	2.7	2.6	6	2.3	56.7	17.6	9	·	·	·	3	10	8	3	·	·	–	4	1	11	
VII	1.0	1.8	2	1.5	6	2.5	2	2.0	3	1.8	16	2.2	23.5	2.4	18.5	1.7	12	1.8	147.3	24.5	15	·	·	·	7	20	15	6	·	·	–	11	·	17	
VIII	3	2.0	1	2.0	·	·	1	1.0	4	2.2	19	2.7	24.5	1.8	15.5	1.9	25	1.5	217.3	99.5	17	·	·	·	1	17	10	6	·	·	–	1	·	16	
IX	1.5	2.3	·	·	·	·	·	·	1.5	2.6	24	2.4	4.2	2.6	8	1.9	13	2.1	161.3	41.5	18	·	·	·	1	20	15	4	·	·	–	1	·	24	
X	·	·	·	·	·	·	·	·	3	1.8	4.9	2.2	30.5	2.0	2.5	1.6	8	2.0	5.7	1.2	4	·	–	·	·	7	3	·	·	·	–	·	·	26	
XI	9.5	3.4	3	3.0	5	2.0	2	2.0	6.5	2.5	23.5	2.0	24	2.5	6.5	1.9	10	2.1	30.0	5.7	26	9	–	·	·	11	7	·	·	·	–	·	·	27	
XII	4	3.2	·	·	6	1.8	·	·	3.5	1.9	34.5	2.5	26.5	2.3	8.5	2.0	10	2.1	25.2	11.8	8	24	–	5	·	16	6	1	·	·	–	·	·	30	2
Rok	91.5	2.5	28.5	1.5	36	1.4	17	1.3	58	2.2	284	2.7	285.5	2.8	156.5	2.4	138	2.3	854.5	99.5	17.VIII	114	–	13	13	172	107	25	1	·	–	24	–	–	37

Orzysz

$H_s = 120\ m$ $h_w = 10\ m$

I	3	4.0	2.5	4.8	6.5	5.1	5.5	5.4	5.5	4.6	10	3.6	39.5	3.9	9.5	4.1	11	3.7	34.5	7.9	5	26	10	7	·	15	8	·	1	·	–	·	1	18	26
II	4	2.6	4	3.0	2	2.0	8.5	4.9	9.5	4.5	12	3.2	28.5	3.8	5.5	3.0	10	3.3	41.3	46	18,19	17	4	·	·	20	14	·	1	·	–	·	·	17	8
III	13	3.8	6	3.0	6	7.2	14.5	8.9	4.5	5.4	4.5	3.2	13	3.6	14.5	4.7	20	3.9	26.2	9.2	15	25	7	7	·	9	7	·	6	2	–	·	9	10	8
IV	13.5	4.6	7	3.3	6.5	3.1	3	4.3	3	5.8	4.5	4.2	12.5	2.8	19	3.3	21	2.8	24.2	7.5	30	11	·	·	2	10	6	·	·	·	–	2	4	8	–
V	19	3.5	7.5	3.1	5.5	3.2	6.5	2.8	3.5	3.9	4	2.5	16.5	3.9	14.5	3.1	16	2.8	39.4	7.0	7,14	4	·	·	1	12	10	·	1	·	–	1	4	8	·
VI	5.5	3.1	1	2.0	3.5	2.3	7	4.2	1.5	3.7	6	3.0	17	2.8	32.5	2.6	16	2.4	53.1	15.1	25	·	·	·	7	12	8	1	1	·	–	·	4	9	
VII	7.5	2.5	4.5	2.8	3.5	2.9	11.5	2.7	3.5	2.0	5	1.6	18.5	2.0	17	2.4	22	1.8	122.0	25.0	16	·	·	·	10	18	15	5	·	·	–	7	1	13	·
VIII	0.5	4.0	2	2.5	·	·	2.5	5.0	4.5	8.1	8.5	2.9	27.5	3.5	16.5	2.5	31	2.3	190.4	68.5	17	·	·	·	2	17	13	4	2	1	–	2	1	10	·
IX	·	·	·	·	0.5	1.0	2.5	2.6	6.5	2.9	17	3.4	23.5	3.4	19	4.2	21	2.7	130.8	35.0	15	·	·	·	1	18	15	5	2	·	–	·	2	15	·
X	·	·	·	·	·	·	1.5	2.0	3.5	3.6	26.5	3.4	2.9	3.6	12.5	3.7	20	2.7	12.6	5.2	30					12	4	·	1	1	–	·	3	10	
XI	4	7.0	2	4.2	7.5	4.0	13	5.0	7	5.1	8	2.9	19	3.6	12.5	4.8	17	3.1	25.5	8.0	28	9	1	·	·	10	7	·	1	·	–	·	1	24	·
XII	4	4.6	2.5	4.0	4.5	4.6	3	2.3	3	3.0	19.5	3.2	3.3	4.0	9.5	4.9	14	3.3	27.5	9.2	8	25	12	5	·	11	7	·	2	·	–	·	3	14	1
Rok	7.4	3.3	3.9	2.7	4.6	3.0	7.6	4.2	5.5.5	4.4	12.5.5	3.1	27.2.5	3.4	18.2.5	3.4	21.9	2.9	72.7.5	68.5	17.VIII	117	34	19	23	164	114	15	18	4	–	12	33	156	–

Mikołajki 1

$H_s = 127\ m$ $H_b = 132,1\ m$ $h_w = 14\ m$

I	2	3.5	·		1.2	3.5	9	3.2	7	2.3	·	·	40.5	2.5	13.5	2.7	9	2.4	20.0	5.3	12	26	9	5	·	14	8	·	·	·	2	·	·	17	24
II	3	2.3	·		7.5	1.3	4.5	2.7	9	3.2	16.5	2.0	2.1	1.9	1.5	1.7	2.1	1.6	37.2	6.7	18	15	3	·	·	17	13	·	·	·	4	·	·	17	3
III	1.6	2.3	3	3.7	8.5	2.9	10.5	9.2	9	4.4	6.5	2.2	20	2.2	6.5	3.3	13	3.1	17.7	8.4	15	24	6	2	·	6	5	·	3	1	·	·	2	10	5
IV	19.5	3.2	2.5	2.8	5.5	2.3	5.5	1.8	2.5	2.4	8.5	2.3	1.5	2.3	8	3.1	2.3	2.0	25.8	12.2	30	9	·	·	1	11	4	1	·	·	1	2	2	7	·
V	2.7	3.1	2	1.5	1.2	2.2	6	1.9	2.5	2.0	7.5	1.7	1.2	2.0	1.9	1.9	3	2.2	63.1	28.1	14	3	·	·	·	14	10	1	·	·	1	4	1	10	
VI	13.5	1.9	·	·	3	2.3	2.5	3.0	4	2.6	12.5	2.2	1.8	2.2	30.5	2.0	6	2.0	90.4	27.3	9			·	4	10	8	4	·	·	·	4	8	7	·
VII	11.5	2.0	4	1.8	10.5	3.4	3.5	3.3	5	2.0	11.5	1.7	11	1.8	16	2.0	20	1.7	135.1	29.8	13			·	3	19	16	4	·	·	2	8	3	8	·
VIII	5.5	2.1	2.5	1.6	2.5	4.0	3	2.7	5.5	2.6	20.5	2.5	2.4	1.9	18.5	1.9	11	1.9	201.6	78.4	17		·	·	1	19	17	6	·	·	4	·	1	7	
IX	2.5	4.0	1	2.0	·	·	·	·	9.5	2.3	27	2.4	24.5	1.9	12.5	2.8	13	2.0	107.3	22.6	15	·	·	·	1	25	15	4	·	·	1	1	1	13	·
X	1	2.0	·	·	0.5	2.0	1	2.0	6	1.9	40.5	2.1	3.0	1.6	2	2.5	12	1.7	18.0	4.1	17	1	·	·	·	12	6	·	·	·	9	·	2	13	·
XI	9	7.6	·	·	8.5	3.6	12.5	4.2	5.5	4.3	17.5	1.4	1.5	1.5	1	4.0	2.1	2.5	24.2	7.4	28	9	1	·	·	13	8	·	1	1	3	·	·	25	
XII	5.5	4.2	2.5	7.2	3	6.2	3	3.5	4.5	1.4	26.5	2.7	2.0	3.5	5	3.4	2.4	2.5	25.4	8.5	8	24	13	5	·	14	6	·	2	·	9	·	3	21	1
Rok	116	3.2	17.5	1.7	73.5	2.8	63	3.1	70	2.6	19.4	1.9	25.1	2.1	13.4	2.6	17.6	2.1	765.8	78.4	17.VIII	111	32	12	10	174	116	20	6	2	36	19	23	155	33

Mikołajki II

$\varphi = 53°47'$ $\lambda = 21°35'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max obs	Data	Min obs	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	14.3	18.3	15.5	15.9	–	11.8	–	–	8.1	26	91	71	89	84	16	6.5	20	34	66	73	56	65
IX	–	–	–	–	9.9	13.5	10.8	11.2	–	7.4	–	–	3.0	27	92	73	84	83	0.9	4.7	2.3	2.6	73	70	60	68
X	–	–	–	–	6.3	10.7	8.0	8.2	11.6	4.7	17.3	11	0.7	3	92	76	87	85	0.8	3.2	1.4	1.8	72	76	55	68
XI	–	–	–	–	3.4	4.8	4.0	4.0	6.0	2.1	13.5	6	-8.7	29	91	84	89	88	0.7	1.3	0.9	1.0	88	89	88	88
XII	–	–	–	–	-2.4	-0.8	-1.9	-1.8	0.2	-4.1	5.7	5	-14.1	19	87	84	87	86	0.6	0.9	0.7	0.7	76	84	7.0	7.7
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Resko

$\varphi = 53°46'$ $\lambda = 15°25'$

I	1012.4	1025.9	992.6	1019.6	0.0	1.4	0.4	0.6	2.5	-1.7	10.4	6	-10.8	16	91	86	90	89	0.5	1.0	0.7	0.7	8.8	7.6	7.4	7.9
II	1002.0	1031.0	974.8	1009.0	1.2	4.7	2.5	2.7	5.7	0.0	10.3	2	-8.0	26	94	81	91	89	0.5	1.7	0.7	1.0	7.9	7.7	5.9	7.2
III	1010.4	1031.7	984.9	1017.5	0.2	6.9	2.8	3.2	8.4	-0.8	17.1	13	-7.7	2	88	65	84	79	0.8	3.8	1.3	2.0	5.6	5.3	3.4	4.8
IV	1012.5	1025.4	987.2	1019.5	3.2	10.0	4.9	5.8	11.4	1.0	21.5	27,28	-6.2	15	89	64	84	79	0.9	5.4	1.6	2.6	7.6	7.0	4.3	6.3
V	1010.3	1024.8	999.7	1017.2	8.2	13.7	8.6	9.8	15.3	3.8	24.6	19	-2.1	9,19	82	54	80	72	2.1	8.2	2.4	4.2	5.4	7.3	4.9	5.9
VI	1009.7	1026.1	997.5	1016.4	14.2	20.6	14.9	16.2	21.7	8.8	29.5	18,29	3.2	1	79	54	76	70	3.6	12.3	4.4	6.8	4.8	5.8	4.3	5.0
VII	1005.2	1017.0	995.7	1011.9	16.3	20.9	17.1	17.8	22.5	13.5	30.3	4	9.2	7	91	69	86	82	1.8	8.4	3.1	4.4	7.5	7.0	6.6	7.0
VIII	1005.9	1017.5	992.6	1012.6	13.8	18.7	14.5	15.4	20.1	11.2	25.7	11	5.9	23	92	68	88	83	1.3	7.4	2.1	3.6	6.5	7.8	5.4	6.6
IX	1004.0	1017.4	983.6	1010.8	9.4	14.0	10.0	10.8	15.1	7.2	24.9	8	1.0	27	94	72	92	86	0.8	4.9	1.1	2.3	7.3	7.7	5.3	6.8
X	1010.2	1022.0	994.0	1017.1	7.5	11.9	8.9	9.3	12.8	6.1	17.9	9	-0.4	2	93	76	90	86	0.8	3.5	1.2	1.8	8.4	7.6	6.0	7.3
XI	1013.3	1031.9	993.9	1020.3	3.5	6.0	4.3	4.5	6.9	2.2	13.3	4	-6.3	30	91	82	87	87	0.7	1.8	1.0	1.2	7.7	8.2	7.3	7.7
XII	1006.4	1024.1	965.3	1013.6	-0.6	1.0	0.0	0.1	2.3	-2.4	8.6	8	-11.8	17	92	86	90	89	0.5	0.9	0.5	0.6	8.8	8.0	6.5	7.8
Rok	1008.5	1031.9	965.3	1015.5	6.4	10.8	7.4	8.0	12.1	4.1	30.3	4.VII	-11.8	17.XII	90	71	86	82	1.2	4.9	1.7	2.6	7.2	7.3	5.6	6.7

Olsztyn – Dajtki

$\varphi = 53°46'$ $\lambda = 20°25'$

I	1004.6	1013.8	984.2	1018.7	-2.2	-0.4	-1.4	-1.4	0.8	-4.2	8.9	6	-20.6	16	90	85	88	88	0.5	0.9	0.7	0.7	8.6	8.2	7.3	8.0
II	992.7	1016.6	969.3	1009.6	0.9	3.3	1.6	1.8	4.0	-0.2	8.5	2	-4.1	28	93	82	88	88	0.5	1.4	0.8	0.9	9.4	7.9	7.2	8.2
III	1004.2	1017.6	973.5	1018.2	-1.4	4.5	1.0	1.3	5.9	-3.0	17.0	31	-13.4	17	84	59	77	73	0.9	4.1	1.7	2.2	6.1	5.9	4.6	5.5
IV	1001.3	1014.3	975.8	1018.0	3.7	11.1	5.4	6.4	12.8	0.8	24.8	27	-6.9	14	88	50	80	73	1.1	7.6	2.0	3.6	6.2	6.7	5.5	6.1
V	999.4	1011.5	987.5	1015.9	8.0	13.0	8.9	9.7	14.5	4.4	25.0	19	-1.7	2	83	57	78	73	2.0	7.2	2.8	4.0	6.2	6.9	5.5	6.2
VI	999.6	1013.3	985.9	1015.8	13.9	19.0	14.5	15.5	21.1	9.6	28.9	11	4.1	21	79	58	78	72	3.4	10.2	3.8	5.8	5.3	6.8	4.9	5.7
VII	994.9	1005.9	985.9	1010.9	16.1	21.1	16.6	17.6	22.7	12.9	29.5	8	8.2	7	88	66	86	80	2.4	9.2	3.0	4.9	7.0	7.1	5.0	6.4
VIII	996.3	1006.0	984.8	1012.4	13.7	18.7	14.7	15.4	20.4	11.5	27.6	12	7.1	30	91	68	89	83	1.5	7.3	1.9	3.6	6.2	7.4	6.0	6.5
IX	993.8	1005.7	976.1	1010.2	9.1	13.4	10.2	10.7	14.8	7.4	26.2	9	1.7	17	90	71	87	83	1.2	5.1	1.7	2.7	7.0	7.6	6.1	6.9
X	1000.7	1013.4	988.5	1017.3	6.3	11.0	8.0	8.3	12.0	5.1	19.3	10	0.7	2	93	75	86	85	0.7	3.4	1.5	1.9	6.8	8.1	6.2	7.0
XI	1003.5	1024.4	981.6	1020.5	3.5	5.2	3.9	4.1	6.4	2.0	14.7	6	-8.3	29	90	81	87	86	0.8	1.7	1.0	1.2	8.2	8.7	8.1	8.3
XII	996.2	1014.5	950.4	1013.2	-2.5	-0.5	-1.7	-1.6	0.8	-4.5	6.0	5	-15.5	19	87	83	88	86	0.6	1.0	0.6	0.7	7.2	8.2	7.0	7.5
Rok	998.4	1024.4	950.4	1015.0	5.8	10.0	6.8	7.4	11.4	3.5	29.5	8.VII	-20.6	16.I	88	70	84	81	1.3	4.9	1.8	2.7	7.0	7.5	6.1	6.9

Kwidzyń

$\varphi = 53°44'$ $\lambda = 18°55'$

I	–	–	–	–	-0.8	0.7	-0.4	-0.2	1.9	-3.5	9.7	6	-15.1	16	–	–	–	–	–	–	–	–	8.3	7.6	7.9	7.9
II	–	–	–	–	1.5	4.3	2.8	2.8	5.1	-0.4	9.9	14	-6.0	24	–	–	–	–	–	–	–	–	8.3	7.4	6.9	7.5
III	–	–	–	–	0.0	5.8	3.1	3.0	7.3	-1.6	17.8	31	-7.0	10,11	–	–	–	–	–	–	–	–	4.9	5.3	5.5	5.2
IV	–	–	–	–	4.0	10.6	7.1	7.2	12.1	0.7	24.3	29	-8.0	13	–	–	–	–	–	–	–	–	5.3	6.6	6.4	6.1
V	–	–	–	–	8.8	13.9	10.7	11.0	15.6	4.7	24.8	19,20	-3.0	6	–	–	–	–	–	–	–	–	5.4	6.4	5.2	5.7
VI	–	–	–	–	13.4	19.8	17.7	17.2	22.5	9.1	29.8	11	2.5	21	–	–	–	–	–	–	–	–	4.4	5.1	3.7	4.4
VII	–	–	–	–	16.2	21.4	19.7	19.2	23.8	12.7	31.8	8	8.0	7	–	–	–	–	–	–	–	–	6.7	6.3	5.3	6.1
VIII	–	–	–	–	13.3	19.6	16.9	16.7	21.3	10.9	26.3	14	6.5	24	–	–	–	–	–	–	–	–	5.5	7.0	5.4	6.0
IX	–	–	–	–	9.1	14.4	12.4	12.1	15.6	6.8	26.3	9	-0.5	27	–	–	–	–	–	–	–	–	6.5	6.8	6.6	6.6
X	–	–	–	–	7.0	11.4	9.2	9.2	12.8	4.8	18.5	19	-1.0	2	–	–	–	–	–	–	–	–	7.5	7.2	7.3	7.3
XI	–	–	–	–	4.2	6.9	5.4	5.5	8.1	2.6	15.2	5	-9.0	30	–	–	–	–	–	–	–	–	8.5	7.5	8.6	8.2
XII	–	–	–	–	-1.4	0.1	-0.9	-0.8	1.7	-4.1	8.2	15	-15.1	18	–	–	–	–	–	–	–	–	7.4	8.2	6.7	7.4
Rok	–	–	–	–	6.3	10.7	8.6	8.6	12.3	3.6	31.8	8.VII	-15.1	16.I,18XII	–	–	–	–	–	–	–	–	6.6	6.8	6.3	6.6

Mikołajki II

$H_s = 127\ m$ $h_w = 12\ m$ **1957**

| MIESIĄC | ROZKŁAD WIATRU °/0 | | | | | | | | | | | | | | | | Średnia prędkość | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | |

Prabuty

$\varphi = 53°44'$ $\lambda = 19°13'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	P_{om}	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1,9	-0,5	-1,4	-1,2	0,9	-3,6	9,0	6	-16,0	16	90	86	89	88	0,5	0,9	0,7	0,7	8,1	8,2	6,4	7,6
II	–	–	–	–	1,0	3,0	1,8	1,9	4,2	-0,2	8,4	14	-6,5	24	93	82	89	88	0,5	1,4	0,8	0,9	8,7	7,6	5,6	7,3
III	–	–	–	–	-0,5	4,8	4,9	2,0	6,3	-2,0	16,8	31	-7,5	17	86	60	78	75	0,8	3,8	1,7	2,1	5,1	6,3	5,2	5,5
IV	–	–	–	–	3,6	9,5	4,6	5,6	11,2	0,9	24,2	29	-7,6	13	88	63	81	77	1,1	5,6	1,8	2,8	5,9	6,9	6,0	6,3
V	–	–	–	–	8,4	12,9	8,2	9,4	14,7	4,4	24,4	19	-2,4	6	80	55	77	71	2,4	7,5	2,8	4,2	6,1	7,1	4,6	5,9
VI	–	–	–	–	13,4	18,9	14,8	15,5	21,5	9,3	28,8	11	4,0	21	81	58	73	71	3,1	9,8	4,8	5,9	4,8	5,8	4,4	5,0
VII	–	–	–	–	16,4	20,9	17,3	18,0	23,0	13,0	34,0	8	7,3	7	85	65	83	78	3,0	9,6	3,7	5,4	6,4	6,2	5,1	5,9
VIII	–	–	–	–	13,8	18,8	14,5	15,2	20,8	11,5	26,2	12	7,3	30	94	66	89	83	0,9	8,2	1,9	3,7	6,6	7,5	4,6	6,2
IX	–	–	–	–	8,8	13,3	10,5	10,8	15,3	6,8	25,8	9	0,6	27	94	74	89	86	0,7	4,6	1,5	2,3	6,6	7,3	5,5	6,5
X	–	–	–	–	6,3	10,6	7,7	8,1	11,9	4,7	18,2	19	0,1	2	94	80	90	88	0,5	2,7	1,0	1,4	6,2	7,3	4,8	6,1
XI	–	–	–	–	3,6	5,3	4,1	4,3	6,4	1,7	13,9	6	-8,2	30	90	82	87	86	0,8	1,6	1,0	1,1	8,7	7,9	7,1	7,9
XII	–	–	–	–	-4,9	-0,5	-1,7	-1,4	0,9	-3,9	7,4	5	-14,0	18	89	84	89	87	0,5	0,9	0,6	0,7	7,2	7,8	6,1	7,0
Rok	–	–	–	–	5,9	9,8	6,9	7,4	11,4	3,6	34,0	8.VII	-16,0	16.1	89	71	84	81	1,2	4,7	1,9	2,6	6,7	7,2	5,4	6,4

Szczecinek

$\varphi = 53°43'$ $\lambda = 16°41'$

I	1001,2	1014,3	982,0	1019,2	-1,0	0,3	-0,6	-0,5	1,4	-2,9	9,8	6	-15,8	16	91	86	89	89	0,5	0,9	0,7	0,7	9,3	8,5	7,7	8,5
II	999,4	1018,5	965,3	1009,0	0,9	4,0	2,2	2,3	5,3	-0,2	9,9	2	-7,0	25	92	78	88	86	0,5	1,8	0,8	1,0	8,6	8,1	7,8	8,2
III	999,9	1020,0	973,7	1017,7	-0,5	5,8	2,3	2,5	7,5	-1,7	16,7	31	-7,3	3	87	63	80	77	0,8	3,8	1,5	2,0	6,2	6,9	3,9	5,3
IV	1001,4	1013,9	976,2	1019,0	2,9	10,1	5,2	5,8	11,6	0,6	22,5	28	-5,9	15	88	63	80	77	0,9	5,8	1,9	2,9	6,9	7,1	5,0	6,3
V	999,3	1012,7	988,6	1016,6	7,9	13,1	8,4	9,4	15,0	3,8	24,8	19	-2,0	27	78	54	75	69	2,5	7,9	3,0	4,5	6,1	7,6	4,9	6,2
VI	999,1	1014,2	986,7	1016,1	14,2	20,2	14,9	16,0	22,1	9,1	29,3	18	3,8	16	78	53	75	69	3,8	12,1	4,5	6,8	5,7	6,5	4,8	5,7
VII	994,4	1006,0	984,7	1011,1	16,3	21,0	16,9	17,8	23,0	13,2	30,7	4	7,6	7	88	67	80	78	2,3	9,3	4,1	5,2	7,7	7,7	6,9	7,5
VIII	995,5	1006,3	983,0	1012,4	13,7	18,2	14,5	15,2	19,7	11,5	26,0	11	7,6	23	92	71	87	83	1,3	6,3	2,3	3,3	7,5	7,8	5,6	7,0
IX	993,3	1006,1	974,4	1010,5	9,3	13,3	9,9	10,6	14,8	7,2	26,6	8	-0,6	26	93	74	91	86	0,8	4,3	1,1	2,1	8,3	8,2	6,1	7,5
X	999,5	1011,4	984,4	1016,9	6,8	11,2	8,4	8,7	12,1	5,5	17,9	10	-0,1	2	94	78	91	88	0,6	3,0	1,0	1,5	8,1	7,8	6,4	7,4
XI	1002,4	1012,9	984,2	1020,2	3,0	5,5	3,7	4,0	6,5	1,6	14,2	5	-8,5	30	91	83	88	87	0,7	1,7	1,0	1,1	8,1	8,6	7,9	8,2
XII	995,3	1012,4	955,1	1013,2	-1,1	0,1	-0,7	-0,6	1,5	-3,2	8,1	8	-13,6	17	94	88	92	91	0,4	0,7	0,4	0,5	8,2	8,7	6,6	7,8
Rok	999,7	1020,9	955,1	1015,1	6,0	10,2	7,1	7,6	11,7	3,7	30,7	4.VII	-15,8	16.1	89	72	85	82	1,3	4,8	1,9	2,7	7,6	7,7	6,1	7,1

Uwaga. Ciśnienie atmosferyczne w ciągu całego roku jest za niskie o około 0,5 mb.

Śliwice

$\varphi = 53°43'$ $\lambda = 18°11'$

I	–	–	–	–	-1,9	0,2	-1,4	-1,1	1,3	-4,0	9,7	6	-17,1	16	96	89	93	93	0,3	0,7	0,5	0,5	8,6	8,1	7,3	8,0
II	–	–	–	–	0,8	4,0	1,6	2,0	5,3	-0,9	8,5	6	-7,1	25	96	82	94	91	0,2	1,5	0,4	0,7	8,9	7,7	8,2	8,3
III	–	–	–	–	-1,3	5,9	1,1	1,7	7,5	-2,6	18,0	31	-9,8	11	91	60	88	80	0,6	4,4	0,9	2,0	5,5	6,1	4,3	5,3
IV	–	–	–	–	3,0	11,0	4,9	6,0	12,4	0,0	24,7	28	-8,0	14	90	58	82	77	0,8	7,0	1,7	3,2	5,9	6,7	5,4	6,0
V	–	–	–	–	8,4	14,3	8,3	9,8	15,7	3,4	26,1	19	-4,0	6	80	54	79	71	2,7	8,7	2,6	4,7	6,4	7,5	4,9	6,3
VI	–	–	–	–	15,1	21,0	14,9	16,5	22,6	8,7	30,2	18	3,9	16	77	56	80	71	4,3	12,2	3,7	6,7	5,0	5,6	5,4	5,3
VII	–	–	–	–	16,4	22,0	16,8	18,0	23,7	12,8	33,0	8	6,3	7	–	–	–	–	–	–	–	–	6,9	7,2	6,4	6,8
VIII	–	–	–	–	13,6	19,3	14,6	15,5	20,9	10,4	26,2	6	4,2	24	–	–	–	–	–	–	–	–	6,7	8,0	5,8	6,8
IX	–	–	–	–	8,8	14,5	9,8	10,7	15,7	6,2	27,4	8,9	-0,6	27	–	–	–	–	–	–	–	–	7,3	7,8	5,5	6,9
X	–	–	–	–	6,4	11,3	7,5	8,2	12,4	4,3	19,3	10	-0,7	2	97	83	94	91	0,3	2,5	0,7	1,2	8,2	7,7	5,1	7,0
XI	–	–	–	–	2,8	5,8	3,4	3,8	7,2	0,7	16,3	5	-9,4	30	94	84	94	90	0,4	1,6	0,7	0,9	9,2	8,3	7,5	8,3
XII	–	–	–	–	-2,1	-0,2	-1,6	-1,4	1,4	-4,5	7,2	8	-16,0	17	94	91	94	93	0,3	0,6	0,4	0,4	8,1	8,1	6,3	7,5
Rok	–	–	–	–	5,8	10,8	6,7	7,5	12,2	2,9	33,0	8.VII	-17,1	16.1	–	–	–	–	–	–	–	–	7,2	7,4	6,0	6,9

Chojnice

$\varphi = 53°42'$ $\lambda = 17°33'$

I	997,3	1009,9	979,0	1019,8	-4,6	-0,4	-1,0	-1,0	0,8	-3,6	9,4	6	-14,4	16	91	89	90	90	0,5	0,7	0,6	0,6	9,1	9,1	7,7	8,6
II	987,8	1013,8	962,2	1009,7	0,9	3,5	1,8	2,0	4,4	-0,1	7,3	2	-5,4	25	93	81	88	87	0,4	1,5	0,8	0,9	8,7	8,5	8,2	8,5
III	996,4	1015,2	969,2	1018,5	-0,5	5,0	1,9	2,1	6,5	-1,7	16,2	31	-7,0	9	85	68	81	78	0,9	3,2	1,4	1,8	6,7	6,2	5,2	6,0
IV	997,5	1010,6	978,0	1019,4	3,4	9,9	5,3	6,0	11,3	1,2	22,7	28	-5,7	14	84	63	78	75	1,3	5,8	2,2	3,1	6,8	7,3	5,4	6,5
V	995,6	1008,5	983,0	1017,3	7,9	13,6	8,6	9,7	14,9	4,2	25,0	19	-2,1	6	79	56	76	70	2,4	7,7	2,9	4,5	6,3	7,5	5,1	6,3
VI	995,6	1010,4	983,1	1016,5	14,2	20,0	15,1	16,1	22,0	9,1	29,1	11	5,5	15	76	53	72	67	4,2	12,1	5,2	7,2	5,3	6,6	5,0	5,6
VII	991,0	1002,3	981,3	1011,7	16,2	21,5	16,7	17,8	22,9	13,1	34,0	8	8,4	29	88	65	81	78	2,4	10,2	3,9	5,5	7,4	7,4	6,2	7,0
VIII	992,1	1002,9	980,1	1013,0	13,5	18,2	14,0	14,9	19,9	10,7	25,5	11	6,4	23	93	72	88	84	1,2	6,3	2,0	3,2	7,4	7,9	5,4	6,9
IX	989,7	1008,6	971,5	1010,9	8,9	13,4	9,8	10,5	14,8	6,8	26,5	8	0,0	26,27	94	74	89	86	0,7	4,6	1,5	2,3	8,2	8,1	5,1	7,1
X	996,0	1008,2	981,4	1017,5	6,4	10,8	8,0	8,3	11,7	4,9	17,8	10	0,0	2	95	81	91	89	0,5	2,6	1,0	1,4	8,5	8,4	6,9	7,9
XI	998,8	1018,1	984,0	1020,9	3,1	5,4	3,7	4,0	6,4	1,7	14,8	5	-8,0	30	91	83	88	87	0,6	1,6	0,9	1,0	8,5	8,5	8,2	8,4
XII	994,6	1009,0	954,0	1013,9	-4,6	-0,3	-0,9	-0,9	1,2	-3,3	7,3	8	-12,6	18	91	88	90	90	0,5	0,7	0,6	0,6	8,1	8,9	7,2	8,1
Rok	994,1	1018,1	954,0	1015,7	5,9	10,0	6,9	7,4	11,4	3,6	34,0	8.VII	-14,4	16.1	88	73	84	82	1,3	4,8	1,9	2,7	7,6	7,9	6,3	7,3

Prabuty

H_s = 104 m h_w = 12 m 1957

MIESIĄC	ROZKŁAD WIATRU °D, °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0	Max<0	Min<-10	Max>25	LICZBA DNI (n) Opad R 0,1 ÷ 1,0	1,0 ÷ 10	10 ÷ 100	Wiatr v >10	v >15	=	≡	◔	●	≋
I	1	20	45	37	55	46	45	26	75	28	24	33	335	40	45	31	8	33	31,3	8,4	13	24	10	3	·	40	6	·	·	·	–	·	1	16	–
II	3	33	7	30	·	·	0,5	5,0	10,5	4,1	2,7	4,1	16,5	33	11,5	24	8	32	56,4	9,7	18	16	1	·	·	16	13	·	·	·	–	·	·	11	–
III	10,5	38	7,5	36	5	4,8	17	6,4	7	6,4	9,5	4,9	15	35	15,5	43	6	44	30,5	9,2	15	23	2	·	·	7	7	·	6	·	·	·	7	12	–
IV	26	35	7	69	3	3,0	1	3,0	6,5	36	9	39	5	37	20,5	27	12	31	14,4	5,3	16	8	·	·	·	9	5	·	1	·	4	3	5	15	–
V	20,5	44	10,5	5,5	4,5	4,3	0,5	3,0	11,5	34	12,5	4,0	7	44	20	26	9	35	26,8	13,6	9	4	·	·	·	6	6	1	·	·	2	3	3	10	–
VI	18	3,2	5	3,5	0,5	3,0	5	4,3	5	4,1	10,5	4,4	13,5	26	26,5	26	6	30	34,6	13,6	5	·	·	·	6	7	6	1	·	·	·	·	5	5	–
VII	7,5	3,6	7	3,2	6	4,5	1,5	4,3	4	5,5	1,8	3,1	1,9	3,1	26	25	4	3,0	91,5	20,1	16	·	·	·	10	15	11	5	·	·	4	11	2	7	–
VIII	6,5	2,5	1	4,0	·	·	3,5	4,9	8	5,3	18,5	4,1	27,5	2,5	17	2,4	11	29	172,3	59,4	14	·	·	·	1	16	16	5	1	·	3	3	·	9	–
IX	1	3,0	·	·	·	·	1	3,0	8	5,5	3,5	4,2	2,0	2,8	1,7	3,9	8	3,5	68,8	19,1	23	·	·	·	2	13	12	1	2	·	5	1	1	9	–
X	·	·	·	·	·	·	0,5	3,0	9	4,2	4,0,5	4,3	2,9,5	3,0	5,5	2,0	8	3,3	17,4	4,9	3,0	·	·	·	·	9	7	·	·	·	8	·	2	7	–
XI	9	3,3	11,5	4,7	5	4,2	7,5	5,0	10,5	6,6	1,4	3,4	17,5	3,2	10	2,2	5	3,8	20,6	6,0	23	10	1	·	·	7	7	·	1	·	6	·	·	18	–
XII	4	3,0	5,5	5,5	4,5	3,6	·	·	7,5	4,1	4,2	4,5	16,5	4,9	6	3,2	7	4,1	28,7	7,5	8	23	11	5	·	11	7	·	3	1	9	·	2	15	–
Rok	10,7	3,0	66,5	36	31	27	42,5	37	95	46	260,5	4,0	220,5	3,4	180	28	92	34	593,3	59,4	14.VIII	108	25	8	19	126	103	13	14	1	–	21	28	134	–

Szczecinek

H_s = 137 m H_b = 142,6 h_w = 12 m

I	·	·	6,5	4,2	2	2,8	5,5	1,9	10,5	2,8	31,5	3,4	20,5	4,3	6,5	4,0	10	3,2	26,3	6,8	5	21	10	3	·	16	8	·	1	·	9	·	·	21	24	
II	4	3,5	1	1,0	2,5	3,0	6	2,8	21,5	3,0	21,5	3,2	16,5	4,1	1	6,0	10	2,9	34,8	5,4	13	13	·	·	·	16	10	·	·	·	3	·	1	21	2	
III	7	3,1	6,5	2,8	3	4,7	20,5	4,5	15,5	3,3	8,5	3,4	15,5	4,6	5,5	4,1	11	3,4	32,6	8,4	15	20	1	·	·	10	8	·	·	·	5	1	5	10	1	
IV	17,5	2,6	9,5	4,6	6	2,3	2,5	3,4	2,5	2,8	8	3,2	10,5	3,1	14,5	3,6	19	2,5	28,0	6,7	16	13	·	·	·	12	8	·	·	·	5	2	3	10	2	
V	13	4,0	18	5,2	3,5	2,7	6,5	2,8	5	2,3	10,5	1,8	12	4,0	15,5	3,7	9	3,3	12,2	4,6	5	3	·	·	·	7	6	·	1	·	2	2	2	9	·	
VI	5	1,8	15,5	2,6	3	2,7	5	2,5	5,5	1,5	1,2	3,2	22,5	3,4	11,5	3,3	10	2,6	35,2	11,8	9	·	·	·	9	10	9	1	·	·	1	2	3	6	·	
VII	4,5	1,8	3	3,3	3	1,7	6	2,8	9	2,7	1,5	2,8	2,5	3,4	13,5	3,4	14	2,6	108,7	34,9	14	·	·	·	10	23	20	2	·	·	·	10	·	12	·	
VIII	4	2,0	2	1,5	1,5	2,7	5,5	3,6	9,5	2,7	34,5	3,3	16,5	3,0	7,5	3,4	12	2,7	81,9	18,1	16	·	·	·	1	20	16	2	1	·	2	4	·	10	·	
IX	0,5	2,0	1	2,0	0,5	2,0	0,5	4,0	14,5	3,2	29,5	4,0	21,5	4,2	6	4,9	16	3,2	64,3	14,0	23	1	·	·	1	17	10	2	·	·	3	1	·	14	·	
X	·	·	·	·	·	·	1	3,0	14,5	3,3	4,7	3,4	1,6	2,8	2,5	4,6	12	2,9	23,3	7,1	3	1	·	·	·	11	8	·	·	·	5	·	2	14	·	
XI	4	5,9	5,5	4,1	12,5	2,5	1,5	3,0	18,5	2,5	15,5	4,6	8	5,8	3	5,8	8	3,4	21,7	4,2	27	11	·	·	1	11	7	·	1	·	6	·	3	22	1	
XII	2,5	4,2	6	6,6	5,5	3,3	1,5	2,3	1,4	2,4	3,4	3,9	1,5,5	3,8	4	5,2	10	3,4	29,1	12,3	8	21	10	5	·	12	7	1	1	·	15	·	2	17	1,4	
Rok	62	2,6	74,5	3,2	4,3	2,5	75,5	3,0	140,5	2,7	267,5	3,4	200	3,9	9,1	4,3	14,1	3,0	495,1	34,9	14.VIII	104	21	8	22	165	117	8	5	·	55	22	21	166	44	

Śliwice

H_s = 115 m h_w = 11 m

I	·	·	4	5,2	9	2,2	1,3	1,4	1,0	1,8	3,2	3,6	1,5	5,8	7	2,7	3	3,2	24,0	5,8	5	26	8	4	·	10	7	·	3	·	–	·	1	19	–	
II	1	2,0	4	2,0	4	2,2	2,0	1,8	2,2	2,0	2,2	3,1	5	4,2	2	4,0	4	2,4	45,1	12,3	18	19	·	·	·	19	10	1	·	·	–	·	·	21	–	
III	4	2,5	7,5	2,4	1,5	3,0	1,5	3,4	1,4,5	2,1	1,9	2,8	4,2	5,0	4	4,2	2	3,1	37,4	11,1	15	21	1	·	·	9	6	1	3	·	–	1	5	8	–	
IV	1,0	2,8	1,4	3,1	7	2,3	1,2	2,0	7,5	1,5	1,6,5	2,1	9	3,4	9	2,5	5	2,3	30,5	18,0	22	13	·	·	·	12	4	1	·	·	–	3	6	12	–	
V	1,1	2,5	1,4,5	3,6	7,5	1,9	5,5	2,1	1,1,5	1,3	1,5	2,4	1,3	2,7	1,5	3,3	·	2,6	27,8	11,5	9	4	·	·	1	10	6	1	·	·	–	4	3	8	–	
VI	4	3,0	6	3,2	·	·	1,0	2,4	1,6,5	1,8	3,2	2,4	1,5,5	2,9	3	3,7	3	2,5	37,5	8,4	9	·	·	·	9	10	8	·	·	·	–	1	4	6	–	
VII	1	2,0	5	3,2	·	·	7	2,6	1,7,5	1,9	3,5	2,4	1,5,5	3,3	7	4,4	5	2,5	203,9	40,0	16	·	·	·	12	19	17	6	·	·	–	1,3	2	12	–	
VIII	0,5	2,0	1	4,0	·	·	7	2,3	1,5	1,9	4,7	2,4	1,4	3,0	5,5	3,3	3	2,3	92,7	26,5	16	·	·	·	4	18	10	4	·	·	–	3	·	11	–	
IX	1	1,0	·	·	·	·	2,5	2,2	1,2	1,5	4,6,5	2,5	1,5	4,5	5	4,0	8	2,5	65,9	15,5	23	1	·	·	2	16	13	2	1	·	–	2	·	6	–	
X	·	·	·	·	·	·	5	1,8	1,5	1,4	5,2	2,4	9	3,1	1	3,0	11	2,0	17,7	3,8	23	1	·	·	·	12	7	·	·	·	–	·	2	12	–	
XI	·	·	6	2,8	6	2,5	2,2	1,6	1,2,5	1,2	1,7,5	2,4	1,3	4,5	2	5,0	11	2,2	10,3	3,8	24	1,5	1	·	·	8	4	·	2	1	–	·	1	20	–	
XII	3	1,7	5	4,8	6	2,2	1,0	1,7	1,3,5	1,6	3,4,5	3,5	9	4,1	5	3,4	7	2,7	39,8	11,7	8	23	11	·	·	11	8	1	·	·	–	·	3	16	–	
Rok	3,5,5	1,6	67	2,6	5,4,5	1,4	1,2,9	2,1	1,6,7,5	1,7	3,6,9	2,7	1,4,5	3,9	6,5,5	3,6	6,2	2,5	62,9,6	40,0	16.VII	123	21	4	28	154	100	17	9	1	–	27	27	151	–	

Chojnice

H_s = 173 m H_b = 177,1 m h_w = 10 m

I	2,5	2,2	9,5	3,3	4	2,0	1,5	1,3	6	3,0	28,5	4,1	2,1	5,9	1,4	5,2	6	4,0	17,8	5,2	5	25	12	3	·	13	6	·	4	1	1,1	·	1	23	25	
II	4,5	1,4	5	1,1	3,5	1,6	8	2,3	1,6,5	2,7	1,4,5	3,3	1,9,5	4,5	5,5	4,8	7	2,9	42,7	8,1	14	12	·	·	·	17	10	·	2	·	7	·	1	27	2	
III	6	2,8	1,1	2,2	1,6,5	4,3	1,1	3,5	8	3,2	6	2,7	1,2	7,6	1,4,5	3,4	8	3,6	30,1	10,0	29	20	1	·	·	9	5	1	5	2	8	1	4	13	1	
IV	2,0	2,9	1,3	2,2	6	2,5	·	·	4,5	1,3	6	3,2	9,5	3,1	2,1	2,9	1,0	2,4	17,9	4,6	2,2	1,1	·	·	·	1,2	8	·	·	·	4	2	5	1,1	2	
V	1,7	2,4	1,8	3,0	4	2,2	5,5	3,4	1,5	4,0	6,5	3,3	1,2	5,2	2,4,5	3,2	4	3,1	45,1	20,0	10	3	·	·	·	1,1	4	2	2	·	1	·	2	7	·	
VI	8,5	1,5	1,8	2,2	8,5	2,5	2	3,0	1	3,0	8,5	3,1	1,6,5	3,7	2,2	3,7	5	2,8	17,6	5,6	9	·	·	·	10	8	4	·	·	·	2	1	5	8	·	
VII	9	2,2	5,5	2,4	8	1,6	3,5	3,0	5,5	2,2	10,5	2,7	2,3	3,5	2,4	3,3	4	2,8	168,4	48,2	14	·	·	·	9	2,4	20	5	·	·	2	1,1	2	1,1	·	
VIII	5	1,5	4,5	1,1	2,5	2,2	4,5	2,4	4,5	3,1	2,2,5	3,8	2,9	3,1	1,2,5	2,8	8	2,7	113,8	22,8	14	·	·	·	1	20	15	5	1	·	4	3	·	14	·	
IX	·	·	1	2,0	3,5	1,6	1,5	2,3	1,1,5	3,3	2,5,5	4,5	2,2,5	4,3	1,7,5	4,0	7	3,8	64,8	10,3	23,27	·	·	·	2	21	16	2	6	1	6	·	·	12	·	
X	·	·	·	·	5,5	1,9	4	1,9	7,5	3,4	3,7,5	4,1	2,9	3,7	6,5	3,9	3	3,5	19,9	5,0	19	·	·	·	·	11	7	·	3	·	11	·	2,	18	·	
XI	3,5	6,4	1,4	2,9	12,5	2,0	1,4,5	2,6	5	1,4	1,4,5	3,4	1,3	8,3	7	4,5	6	3,6	9,1	2,8	28	12	1	·	·	9	4	·	4	·	9	·	3	23	1	
XII	3,5	4,3	1,0	4,2	3	3,8	3,5	1,6	9	1,9	2,8	4,8	2,0	5,9	1,1	4,7	5	4,3	33,8	14,4	8	22	10	2	·	11	7	1	5	·	1,4	·	2	19	11	
Rok	79,5	2,3	109,5	2,2	77,5	2,4	59,5	2,3	80,5	2,7	208,5	3,6	22,7	4,9	18,0	5,9	7,3	3,3	581,0	48,2	14.VII	105	24	5	22	166	106	16	32	4	82	18	27	186	42	

Ostróda

$\varphi = 53°42'$ $\lambda = 19°58'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.8	-0.3	-1.4	-1.2	0.6	-3.9	8.4	6	-16.6	16	–	–	–	–	–	–	–	–	9.1	7.9	7.8	8.3
II	–	–	–	–	1.5	3.6	1.8	2.2	4.3	0.0	8.6	14	-3.7	25	–	–	–	–	–	–	–	–	9.5	8.0	7.8	8.4
III	–	–	–	–	-0.8	5.0	1.1	1.6	6.0	-2.5	17.2	31	-10.2	17	–	–	–	–	–	–	–	–	5.3	5.2	4.9	5.1
IV	..	–	–	–	4.0	11.3	6.1	6.9	12.5	1.0	24.6	29	-5.4	10,14	–	–	–	–	–	–	–	–	6.3	5.5	5.9	5.9
V	–	–	–	–	8.6	13.4	9.1	10.0	14.7	4.5	24.9	20	-2.1	6	–	–	–	–	–	–	–	–	6.1	6.7	6.0	6.3
VI	–	–	–	–	14.6	19.7	15.2	16.2	21.4	9.6	29.0	11	4.4	21	–	–	–	–	–	–	–	–	5.5	5.6	5.0	5.4
VII	–	–	–	–	16.9	21.0	17.4	18.2	22.8	13.2	29.2	8	10.1	29	–	–	–	–	–	–	–	–	6.7	6.3	6.0	6.3
VIII	–	–	–	–	14.2	19.2	15.2	16.0	20.5	11.2	24.5	11,16	6.8	23,30	–	–	–	–	–	–	–	–	6.3	6.2	5.4	6.0
IX	–	–	–	–	9.5	13.9	10.8	11.2	15.1	7.3	26.5	9	0.7	26	–	–	–	–	–	–	–	–	7.6	6.7	6.1	6.8
X	–	–	–	–	6.6	11.0	8.3	8.6	12.0	4.9	19.0	10	-0.4	2	–	–	–	–	–	–	–	–	6.9	7.8	5.6	6.8
XI	–	–	–	–	3.8	5.6	4.3	4.5	6.8	2.2	14.7	6	-8.2	30	–	–	–	–	–	–	–	–	8.1	8.0	7.3	7.8
XII	–	–	–	–	-1.9	-0.4	-1.3	-1.2	0.8	-4.0	6.4	9	-13.5	18,19	–	–	–	–	–	–	–	–	7.5	8.0	6.9	7.5
Rok	–	–	–	–	6.3	10.2	7.2	7.7	11.5	3.6	29.2	8.VII	-16.6	16.1	–	–	–	–	–	–	–	–	7.1	6.8	6.2	6.7

Trzebież

$\varphi = 53°40'$ $\lambda = 14°31'$

I	1018.5	1032.6	998.6	1019.3	0.9	2.4	1.2	1.4	3.2	-1.1	11.2	5	-9.0	15	90	82	88	87	0.7	1.4	0.9	1.0	9.3	7.5	8.1	8.3
II	1007.8	1037.9	979.9	1008.5	1.6	5.5	3.1	3.3	6.1	0.3	14.5	2	-5.6	26	92	74	89	85	0.6	2.3	0.9	1.2	7.6	8.2	6.2	7.3
III	1016.2	1038.2	991.4	1017.0	1.4	7.6	3.1	3.8	8.6	-0.1	17.8	13	-6.1	2	87	64	81	77	0.9	3.9	1.5	2.1	6.1	6.1	5.2	5.8
IV	1018.7	1034.7	994.0	1019.5	4.3	8.9	5.7	6.2	10.4	2.1	22.0	5	-4.8	15	85	69	82	79	1.2	3.8	1.7	2.2	7.9	6.7	4.4	6.3
V	1016.2	1030.9	1004.3	1017.0	9.0	13.4	9.4	10.3	14.9	5.1	24.5	16,19	-1.8	6,9	78	57	76	70	2.5	7.4	3.0	4.3	5.9	7.2	4.9	6.0
VI	1015.4	1032.6	1003.0	1016.2	15.0	20.0	15.7	16.6	21.6	10.6	30.1	29	6.2	26	79	60	77	72	3.7	10.0	4.4	6.0	5.4	6.0	3.7	5.0
VII	1010.9	1022.9	1001.3	1011.7	17.4	21.1	18.1	18.7	22.9	14.4	32.2	4	9.8	16,29	87	70	82	80	2.7	8.3	4.2	5.1	7.4	7.0	6.3	6.9
VIII	1011.5	1023.4	997.5	1012.3	14.6	19.6	14.9	16.0	20.9	11.5	27.4	11	5.5	23	88	65	85	79	2.0	8.6	2.7	4.4	6.7	7.5	4.2	6.1
IX	1009.8	1022.9	988.0	1010.5	10.0	14.4	10.5	11.2	15.6	7.3	23.8	8	1.6	26	91	72	89	84	1.2	4.9	1.4	2.5	7.3	7.5	4.8	6.5
X	1015.9	1027.7	999.1	1016.7	7.9	12.8	9.3	9.8	13.4	6.1	18.3	10	0.6	2	91	73	88	84	1.3	4.2	1.4	2.2	7.9	7.5	6.6	7.3
XI	1019.2	1037.7	999.2	1020.0	4.0	6.7	4.9	5.1	7.4	2.6	14.3	1	-4.8	21	88	77	85	83	1.0	2.3	1.3	1.5	8.1	7.9	7.6	7.9
XII	1012.3	1030.7	970.9	1013.1	0.4	2.0	0.8	1.0	3.0	-1.6	9.4	8	-9.9	17,18	89	82	87	86	0.7	1.2	0.8	0.9	8.9	8.5	6.1	7.8
Rok	1014.4	1038.2	970.9	1015.2	7.2	11.2	8.0	8.6	12.3	4.8	32.2	4.VII	-9.9	17,18.XII	87	70	84	80	1.5	4.9	2.0	2.8	7.4	7.3	5.7	6.8

Pieńczykówek

$\varphi = 53°39'$ $\lambda = 22°36'$

I	–	–	–	–	-3.1	-1.1	-2.1	-2.1	-0.2	-5.1	6.9	9	-25.0	16	90	89	89	89	0.5	0.6	0.6	0.6	9.3	9.2	8.8	9.1
II	–	–	–	–	0.1	2.7	1.0	1.2	3.3	-0.8	7.1	14	-11.4	28	92	88	93	91	0.5	0.9	0.5	0.6	9.5	9.0	9.4	9.3
III	–	–	–	–	-2.9	3.0	-0.7	-0.3	4.4	-4.8	16.5	31	-16.7	17	–	–	–	–	–	–	–	–	7.8	7.5	7.6	7.6
IV	–	–	–	–	4.3	12.2	6.7	7.5	13.4	0.6	24.7	28	-7.7	13	–	–	–	–	–	–	–	–	6.6	6.6	5.9	6.4
V	–	–	–	–	9.5	14.3	9.3	10.6	15.6	4.1	25.7	19	-5.1	2	82	62	81	75	2.2	7.0	2.3	3.8	5.4	7.3	6.5	6.4
VI	–	–	–	–	14.2	20.1	14.5	15.8	21.9	8.2	29.7	19	2.6	22	–	–	–	–	–	–	–	–	6.0	6.5	6.3	6.3
VII	–	–	–	–	16.4	21.7	16.3	17.7	23.2	12.1	27.9	8	4.4	4	88	67	90	82	2.4	9.1	1.9	4.5	7.5	8.0	6.9	7.5
VIII	–	–	–	–	13.8	19.6	14.1	15.4	20.7	9.7	29.7	12	1.5	24	–	–	–	–	–	–	–	–	7.2	7.3	6.6	7.0
IX	–	–	–	–	9.1	14.2	9.0	10.3	15.2	5.7	26.4	9	-1.0	17	–	–	–	–	–	–	–	–	8.4	8.3	7.8	8.2
X	–	–	–	–	5.7	10.8	7.0	7.6	12.1	3.9	19.5	11	-4.3	16	93	78	93	88	0.7	3.0	0.8	1.5	8.1	7.4	7.9	7.8
XI	–	–	–	–	2.5	5.1	3.2	3.5	6.1	1.5	14.3	6	-9.2	30	93	85	91	90	0.5	1.4	0.6	0.8	8.8	8.8	8.6	8.7
XII	–	–	–	–	-2.9	-0.8	-2.7	-2.3	0.0	-5.1	5.5	5	-15.5	18,19	–	–	–	–	–	–	–	–	8.1	8.0	7.3	7.8
Rok	–	–	–	–	5.6	10.2	6.3	7.1	11.3	2.5	29.7	19.VI,12.VII	-25.0	16.1	–	–	–	–	–	–	–	–	7.7	7.8	7.5	7.7

Szczytno

$\varphi = 53°34'$ $\lambda = 21°02'$

I	–	–	–	–	-3.5	-0.4	-1.7	-1.8	0.6	-4.9	7.9	6	-19.8	16	87	84	88	86	0.6	1.0	0.6	0.7	8.7	7.8	7.6	8.0
II	–	–	–	–	0.8	2.9	1.2	1.5	3.7	-0.9	7.5	2,14,21	-6.8	28	92	84	90	89	0.5	1.3	0.6	0.8	9.2	8.2	5.8	7.7
III	–	–	–	–	-1.4	4.7	0.2	0.9	6.0	-4.1	17.3	31	-16.6	17	77	57	79	71	1.3	4.3	1.4	2.3	5.1	4.5	4.7	4.8
IV	–	–	–	–	4.5	12.5	5.4	7.0	13.4	0.3	25.4	27,30	-9.4	14	85	49	84	73	1.3	8.7	1.7	3.9	5.2	5.1	4.7	5.0
V	–	–	–	–	9.2	13.6	8.5	10.0	14.9	3.9	26.3	19	-3.5	2	78	59	86	74	2.6	7.4	1.7	3.9	5.5	6.2	5.5	5.7
VI	–	–	–	–	14.9	19.8	13.4	15.4	21.4	8.9	28.6	11	2.5	21	79	59	86	75	3.8	10.6	2.3	5.6	5.1	6.0	4.5	5.2
VII	–	–	–	–	17.6	21.7	16.2	17.9	23.1	12.3	29.4	8	6.4	7	83	65	86	78	3.6	10.1	2.8	5.5	5.8	6.0	5.3	5.7
VIII	–	–	–	–	14.8	19.1	13.9	15.4	20.4	10.3	27.4	12	3.6	24	86	68	91	82	2.4	7.4	1.5	3.8	5.5	7.1	4.3	5.6
IX	–	–	–	–	9.5	14.0	9.7	10.7	15.1	6.8	26.1	9	-0.3	27	88	73	88	83	1.5	5.1	1.5	2.7	7.1	7.2	5.0	6.4
X	–	–	–	–	5.7	11.3	7.0	7.8	12.1	3.3	19.4	10	-1.7	3	93	76	91	87	0.7	3.4	0.9	1.7	6.7	7.4	4.9	6.3
XI	–	–	–	–	3.0	5.1	3.5	3.8	6.2	1.6	15.1	6	-8.7	29	93	85	90	89	0.5	1.5	0.8	0.9	8.9	8.9	7.8	8.4
XII	–	–	–	–	-3.1	-0.7	-2.4	-2.2	0.3	-5.0	5.3	5	-15.3	18	90	88	92	90	0.4	0.7	0.4	0.5	7.4	7.4	7.0	7.3
Rok	–	–	–	–	6.6	10.3	6.8	7.3	11.4	2.7	29.4	8.VII	-19.8	16.1	86	70	88	81	1.6	5.1	1.4	2.7	6.7	6.8	5.6	6.4

Ostróda

$H_s = 106\ m$ $h_w = 10\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU °D, %D																		OPAD R				LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max>25°	≥0,1	≥1,0	≥10,0	≥10	≥15									
I	0,5	7,0	1	6,0	7,5	3,2	11	2,4	16	4,0	3,5	3,8	15,5	5,2	1,5	2,0	5	3,6	33,2	11,5	5	25	10	3	·	9	6	1	1	·	-	·	·	21	-					
II	2	2,0	3	2,3	1,5	3,0	8,5	4,1	9	3,9	30,5	3,4	18,6	4,2	4	4,1	7	3,3	56,8	10,5	18	14	·	·	·	16	14	1	·	·	-	·	·	17	-					
III	6,5	4,4	2,5	5,0	4	3,5	26,5	3,7	17,5	4,7	8,5	4,2	13	2,3	8,5	5,3	6	3,8	26,1	10,0	15	24	2	·	·	8	6	1	2	·	-	·	5	7	-					
IV	10	3,5	8	2,2	3,5	2,0	8,5	2,2	7,5	2,5	14	3,4	13	3,2	16,5	2,9	9	2,7	14,5	3,9	16	10	·	·	·	10	4	·	·	·	-	4	2	8	-					
V	7	4,5	4,5	2,3	8,5	2,4	7	2,4	8	2,4	8,5	3,9	22	3,7	19,5	3,7	8	3,1	33,5	7,4	10	3	·	·	·	12	9	·	·	·	-	3	3	10	-					
VI	8	2,5	4	2,1	1,5	3,3	8,5	3,6	8	2,8	15,5	3,0	25,5	3,9	10	3,3	9	2,8	56,8	17,2	5	·	·	·	6	9	7	3	·	·	-	1	2	5	-					
VII	3,5	2,4	5	3,4	7,5	3,5	8	3,6	6	2,5	12	2,6	29,5	3,7	6,5	2,9	15	2,7	112,7	19,2	12	·	·	·	7	14	14	4	·	·	-	5	2	7	-					
VIII	·	·	2	2,0	2	2,0	9,5	3,1	11	2,5	26,5	4,2	26,5	3,6	8,5	3,1	7	3,2	108,3	24,5	14	·	·	·	·	17	15	5	·	·	-	2	1	5	-					
IX	·	·	·	·	·	·	5	3,8	9	4,2	33,5	4,6	33,5	4,8	3	7,0	6	4,4	125,1	35,2	23	·	·	·	2	15	14	3	3	2	-	1	·	10	-					
X	·	·	·	·	·	·	4	3,8	15,5	3,1	4,5	4,2	24	4,0	4,5	4,3	3	3,8	20,8	7,4	30	1	·	·	·	11	8	·	·	·	-	·	2	10	-					
XI	5	5,2	5,5	2,6	5,5	3,7	15,5	4,9	15	2,4	24	3,3	42,5	5,6	2	4,5	5	3,7	33,1	9,8	28	11	1	·	·	8	6	·	1	·	-	·	1	16	-					
XII	2	6,5	4	4,8	2,5	3,4	5,5	3,7	11,5	3,5	28,5	4,6	25	6,6	3	3,7	11	4,4	24,8	9,4	8	25	10	5	·	9	5	·	3	2	-	·	2	17	-					
Rok	44,5	3,2	39,5	2,7	44	2,5	117,5	3,4	134	3,2	284,5	3,8	258,5	4,2	84,5	3,9	91	3,5	645,7	35,2	23.IX	113	23	8	15	138	108	18	10	4	-	16	20	133	-					

Trzebież

$H_s = 1\ m$ $H_b = 6,6\ m$ $h_w = 18\ m$

I	1,5	1,3	7,5	6,3	1,5	4,7	12,5	2,3	13,5	3,7	27,5	4,5	14	8,3	11	3,9	4	4,5	27,4	8,3	5	19	3	·	·	12	6	·	8	·	4	·	·	21	4					
II	1,5	4,3	6,5	3,3	4	3,0	20	3,0	15,5	3,7	19	3,4	11	5,4	3,5	4,6	3	3,5	28,2	5,7	8	12	·	·	·	13	9	·	3	·	7	·	1	14	·					
III	5,5	3,1	12,5	4,4	4	5,8	3,0	7,1	7,5	4,9	8	4,4	10,5	7,8	6	4,5	9	5,3	38,5	9,9	15	17	·	·	·	12	8	·	10	5	3	1	6	9	1					
IV	11,5	4,0	3,2	3,1	6,5	2,5	7	2,9	1	3,5	7,5	3,3	5,5	4,4	11	5,3	8	3,2	23,4	5,5	19	7	·	·	·	12	6	·	1	·	4	2	2	9	1					
V	1,0	3,8	3,2	4,4	8	3,8	14,5	3,0	2	1,8	7,5	2,1	6	9,3	11	5,1	2	4,1	43,4	15,5	16	2	·	·	·	10	4	2	4	1	1	3	·	5	·					
VI	8	3,4	20,5	3,1	7,5	2,7	14,5	2,6	2,5	2,0	9,5	4,5	8,5	4,8	1,5	5,0	4	3,5	36,9	19,2	24	·	·	·	7	11	7	1	1	·	2	2	5	5	·					
VII	11,5	4,1	2,0	3,0	4,5	2,4	1,0	3,7	6	2,3	16	3,1	9	4,1	12	5,5	4	3,5	64,9	22,1	21	·	·	·	7	17	11	1	1	·	2	4	1	12	·					
VIII	3,5	2,4	5,5	2,5	1	3,5	11,5	3,0	1,8	4,4	32,5	4,6	7,5	3,6	7,5	4,2	6	3,8	44,0	12,2	24	·	·	·	4	16	12	1	3	·	1	·	·	6	·					
IX	3,5	2,0	6	2,1	1,5	1,7	9	3,2	20,5	4,6	23,5	5,9	11	6,4	11	5,9	4	4,5	74,0	10,5	23	·	·	·	·	17	16	1	9	1	2	·	·	11	·					
X	1,5	2,7	·	·	·	·	9,5	1,5	2,3	4,3	3,6	4,7	9	5,9	5	4,3	9	3,9	17,8	6,0	5	·	·	·	·	11	5	·	4	·	6	·	2	14	·					
XI	3,5	9,0	6,5	5,5	1,5,5	3,5	3,2	3,6	9,5	3,5	4,5	4,9	1,3	8,6	3,5	9,1	2	4,8	17,4	5,2	9	11	·	·	·	12	5	·	5	1	2	·	2	17	2					
XII	1	1,5	6	8,4	4,5	4,2	1,8	3,2	1,4	5,2	3,0	6,2	9	5,5	9,5	6,3	1	5,4	26,5	13,3	8	18	5	·	·	10	7	1	9	4	3	·	2	18	4					
Rok	6,2,5	3,6	1,5,5	3,8	5,8,5	3,2	1,8,8,5	3,3	1,3,3	3,7	2,2,1,5	4,3	1,1,4	6,1	1,0,6	5,3	5,6	4,2	4,4,2,2	2,2,1	21.VII	3,6	8	·	1,8	1,5,3	9,8	7	5,8	1,2	3,7	1,2	2,1	1,4,1	1,2					

Pieńczykówek

$H_s = 1,17\ m$ $h_w = 12\ m$

I	1	4,5	4,5	6,2	7,5	5,1	8	4,7	10	4,6	13	5,7	2,5,5	6,8	19,5	5,1	4	5,4	32,8	9,1	6	26	11	9	·	13	8	·	4	·	-	·	·	26	2,7					
II	6	3,1	2,5	3,0	10	3,2	7,5	3,7	3,5	5,6	15	5,2	21,5	5,0	10	3,4	8	3,9	46,8	7,6	1	15	5	1	·	21	15	·	2	·	-	·	·	25	7					
III	19,5	4,4	7	4,9	7,5	4,8	5	2,6	6	6,1	5	4,6	8,5	6,2	19,5	5,2	15	4,4	2,1,6	8,9	15	27	8	·	·	9	4	·	5	·	-	·	·	17	13					
IV	18	3,4	11	2,4	10	2,5	1	2,0	2	4,5	5	4,0	6	4,5	15	1,9	22	2,2	27,1	8,9	30	13	·	·	·	12	6	·	·	·	-	3	2	9	·					
V	26	4,2	12	4,6	10	3,2	2,5	5,0	2,5	4,5	3	7,2	6,5	6,2	13,5	5,0	17	3,8	17,6	9,4	7	6	·	·	1	10	4	·	1	·	-	·	4	12	·					
VI	10,5	3,0	·	·	2	2,5	·	·	3	6,3	6	4,2	21,5	4,6	24	4,0	23	3,1	42,5	13,7	5	·	·	·	9	10	8	1	1	·	-	2	3	9	·					
VII	5,5	1,8	6	1,7	1,0	2,6	5	2,6	·	·	4	3,2	14,5	3,7	19	3,1	29	2,0	87,9	15,1	2	·	·	·	10	16	15	3	·	·	-	5	·	16	·					
VIII	2,5	2,6	2	2,5	3	2,7	1,5	3,7	1	4,5	6,5	5,8	27	3,9	25,5	2,7	24	2,6	12,7,9	57,2	17	·	·	·	1	11	10	4	·	·	-	3	·	10	·					
IX	7,5	3,0	3	1,3	1	1,0	2,5	2,0	2	3,5	8,5	4,4	30,5	4,1	20	2,2	15	2,5	17,4,6	3,9,4	18	1	·	·	1	19	15	5	3	·	-	1	·	18	·					
X	1,5	1,0	·	·	3	1,7	2	1,5	3	3,0	15,5	3,2	30	2,7	13	2,5	25	2,0	17,5	5,0	1	1	·	·	·	12	6	·	·	·	-	·	·	15	·					
XI	5,5	5,4	8,5	5,9	9	2,7	6,5	5,0	2,5	5,4	4	4,0	12	3,8	2	1,5	4,0	2,4	21,0	10,6	28	11	1	·	·	13	5	1	1	·	-	·	·	23	1					
XII	6,5	3,1	·	·	7,5	4,4	1,5	4,7	2,5	9,8	20	7,1	31,5	5,9	2,5	3,2	21	4,5	31,3	8,0	8	27	14	5	·	9	7	·	8	1	-	·	3	19	4					
Rok	1,1,0	3,3	5,6,5	2,7	8,0,5	3,0	4,3	3,6	3,8	4,8	1,0,5,5	4,9	2,3,5	4,8	1,8,3,5	3,4	2,4,3	3,3	6,4,8,6	5,7,2	17.VIII	1,2,7	3,9	1,5	2,2	1,5,5	1,0,3	1,4	2,5	1	-	1,4	1,2	1,9,9	5,2					

Szczytno

$H_s = 1,44\ m$ $h_w = 15\ m$

I	·	·	2	3,5	1,4	2,8	4,5	2,2	1,1,5	2,4	3,0	4,1	2,4,5	3,6	5,5	4,9	1	3,5	3,4,9	9,2	5	25	11	7	·	1,4	8	·	2	·	1,3	·	·	17	2,5					
II	4	2,5	3	1,7	4	2,0	9,5	2,1	1,7	2,7	2,6,5	2,7	1,5	2,5	4	1,7	1	2,5	5,4,5	8,5	18	19	3	·	·	17	1,4	·	·	·	6	·	1	1,4	7					
III	8	3,9	8	2,6	1,7	6,4	7	4,9	9	5,3	5	3,4	2,3	3,5	1,4	4,6	2	4,4	2,4,6	12,0	1,5	2,7	5	2	·	9	5	1	6	3	·	·	8	7	4					
IV	2,6	3,1	5,5	2,8	1,3,5	2,6	2,5	3,4	7	3,4	6,5	5,2	4,0	2,9	1,1	3,5	8	3,0	2,8,2	9,0	3,0	1,5	·	·	3	1,2	7	·			2	·	5	4	2					
V	1,8	3,8	1,2,5	3,6	1,0,5	3,1	1,5	6,0	5	2,8	6	3,6	1,2,5	5,8	2,2	3,3	5	3,5	4,9,3	1,8,6	2,0	5	·	·	1	1,3	5	3	1	·	4	3	5	9	·					
VI	1,9	2,4	4,5	3,0	3,5	2,6	3,5	4,9	3	3,2	9	3,3	1,7,5	2,5	2,2	3,1	8	2,6	9,0,8	2,6,0	2,2	·	·	·	5	1,2	9	3	1	1	1	2	6	1,0	·					
VII	8,5	2,1	1,0,5	2,0	1,0,5	3,3	4	1,5	9	2,6	9,5	2,7	1,5	3,5	1,6	2,7	1,0	2,4	1,1,6,8	2,4,6	1,6	·	·	·	8	1,7	1,2	4	1	1	3	5	4	1,0	·					
VIII	2,5	2,6	3,5	1,4	4	2,6	6	2,2	7,5	4,5	1,8,5	4,3	2,2	2,6	1,6	2,6	1,3	2,8	1,8,1,4	5,9,0	1,7	·	·	·	1	1,6	1,4	7	1	1	4	1	3	6	·					
IX	3	2,0	2,5	3,6	2,5	2,4	2,5	2,8	1,9,5	4,7	2,1	4,0	2,7,5	5,5	6,5	4,5	5	4,3	1,0,7,7	2,4,2	1,5	1	·	·	1	1,9	1,4	5	5	1	3	1	4	9	·					
X	·	·	·	·	3,5	1,9	6	2,9	2,1	3,0	4,0	3,1	1,6,5	4,4	3	1,8	3	3,1	1,5,2	4,0	3,0	3	·	·	·	1,2	7	·	1	·	1,2	·	2	9	·					
XI	9	1,0,8	5	2,9	1,9,5	2,6	8,5	2,7	1,0	2,2	1,2,5	2,5	1,6,5	4,2	·	·	9	3,4	2,3,4	8,0	2,8	1,1	·	·	·	1,2	6	·	4	3	1,0	·	1	2,2	·					
XII	8,5	5,3	5,5	1,5	8	2,5	1,0,5	2,0	1,0	3,1	2,3	4,9	1,7,5	3,7	5	2,8	5	3,4	3,0,5	4,1,6	8	2,5	1,3	5	·	1,6	8	1	5	1	4,2	·	5	1,9	2					
Rok	1,0,6,5	3,2	6,2,5	2,4	1,1,0,5	2,9	6,6	3,1	1,2,9,5	3,5	2,0,7,5	3,7	2,1,7,5	3,6	1,2,5	3,5	7,0	3,2	7,0,1,7	5,8,0	17.VIII	1,3,1	3,2	1,4	1,9	1,6,9	1,0,9	2,4	2,5	1,1	7,0	1,2	4,4	1,3,6	4,0					

Szczuczyn

$\varphi = 53°34'$ $\lambda = 22°17'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	–	–	–	–	-3.0	-1.2	-1.8	-2.0	0.1	-5.0	7.0	9	-22.1	16	92	89	94	91	0.4	0.6	0.5	0.5	8.4	8.4	7.5	8.1
II	–	–	–	–	0.3	2.3	4.1	1.2	3.4	-0.8	7.2	14	-9.2	28	93	86	91	90	0.4	1.0	0.6	0.7	9.3	8.4	7.0	8.2
III	–	–	–	–	-2.2	3.2	0.0	0.2	4.8	-4.6	16.2	31	-14.7	17	83	64	80	76	0.9	3.3	1.3	1.8	6.1	5.8	4.8	5.6
IV	–	–	–	–	4.3	12.0	6.8	7.5	13.5	1.2	25.7	27	-5.9	10	89	52	79	73	1.0	8.4	2.4	3.9	5.8	6.1	5.2	5.7
V	–	–	–	–	9.0	13.9	9.4	10.4	15.7	4.4	25.7	19	-2.9	6	80	59	80	73	2.3	7.3	2.4	4.0	5.1	7.4	5.4	6.0
VI	–	–	–	–	15.1	20.0	14.6	16.1	21.8	9.4	28.3	19	4.2	21	75	55	79	70	4.4	11.4	3.5	6.4	6.1	6.7	5.1	6.0
VII	–	–	–	–	16.6	21.6	16.7	17.9	23.5	12.7	28.1	8	7.1	4	84	62	86	77	3.0	10.3	2.6	5.3	7.0	7.9	6.0	7.0
VIII	–	–	–	–	13.8	19.1	14.6	15.5	20.5	11.1	28.9	12	4.9	28	90	66	88	81	1.7	8.1	2.0	3.9	6.8	7.9	5.1	6.6
IX	–	–	–	–	9.2	13.8	9.9	10.7	15.0	6.6	27.3	9	0.6	17	92	69	89	83	1.0	5.6	1.4	2.7	8.0	8.6	5.2	7.3
X	–	–	–	–	5.3	10.7	7.5	7.8	11.8	3.8	18.0	10	0.1	16	94	75	89	86	0.6	3.4	1.2	1.7	7.1	7.6	6.1	6.9
XI	–	–	–	–	2.9	4.8	3.6	3.7	6.2	1.5	13.9	6	-9.3	30	94	85	92	90	0.4	1.2	0.7	0.8	9.1	8.9	8.7	8.9
XII	–	–	–	–	-2.8	-1.0	-2.2	-2.0	0.2	-4.8	5.3	5	-12.5	18	88	85	89	87	0.5	0.8	0.5	0.6	7.5	7.9	6.9	7.4
Rok	–	–	–	–	5.7	9.9	6.7	7.2	11.4	3.0	28.9	12.VIII	-22.1	16.1	88	71	86	82	1.4	5.1	1.6	2.7	7.2	7.6	6.1	7.0

Kamień Krajeński

$\varphi = 53°32'$ $\lambda = 17°31'$

I	–	–	–	–	-1.7	-0.2	-1.2	-1.1	1.2	-3.3	10.0	6	-16.1	16	96	95	97	96	0.2	0.3	0.2	0.2	9.7	9.0	7.1	8.6
II	–	–	–	–	0.9	3.8	2.0	2.2	5.1	-0.2	8.8	2	-5.5	25	95	87	96	93	0.4	1.1	0.3	0.6	9.1	7.2	7.6	8.0
III	–	–	–	–	-0.2	5.3	2.0	2.3	7.1	-1.5	15.9	31	-6.6	11	–	–	–	–	–	–	–	–	5.4	5.7	3.8	5.0
IV	–	–	–	–	3.3	9.9	5.7	6.2	11.6	1.2	22.5	28	-5.8	13	93	66	84	81	0.6	5.5	1.7	2.6	6.1	6.7	5.7	6.2
V	–	–	–	–	8.2	13.2	9.2	10.0	14.8	4.3	24.8	19	-2.5	6	83	57	77	72	2.1	7.6	3.0	4.2	5.8	6.5	5.6	6.0
VI	–	–	–	–	13.6	19.9	15.2	16.0	21.8	9.2	28.7	11	4.9	8	79	54	75	79	3.4	11.8	4.3	6.5	4.6	5.1	4.1	4.6
VII	–	–	–	–	16.4	21.1	17.1	17.9	23.1	13.1	30.9	4	8.1	7	87	66	82	78	2.7	9.5	3.7	5.3	7.1	7.0	6.0	6.7
VIII	–	–	–	–	13.4	18.2	14.8	15.3	20.0	10.8	25.5	11	6.4	23	92	71	89	84	1.3	6.3	2.0	3.2	7.2	7.7	6.1	7.0
IX	–	–	–	–	8.8	13.1	10.0	10.5	15.0	6.7	26.4	8	-0.5	27	92	73	87	84	0.9	4.7	1.6	2.4	7.1	7.5	4.9	6.5
X	–	–	–	–	6.6	11.2	8.0	8.4	12.2	4.9	17.9	10,19	-0.2	2	95	77	90	87	0.5	3.1	1.1	1.6	8.3	7.0	5.4	6.9
XI	–	–	–	–	2.8	5.4	3.5	3.8	6.6	1.5	15.5	5	-6.5	30	94	85	92	90	0.5	1.5	0.7	0.9	8.6	8.3	7.4	8.1
XII	–	–	–	–	-1.7	-0.2	-1.1	-1.0	1.1	-3.2	8.0	9	-12.7	18	94	90	92	92	0.3	0.6	0.4	0.4	8.1	8.2	6.7	7.7
Rok	–	–	–	–	5.9	10.1	7.1	7.5	11.6	3.6	30.9	4.VIII	-16.1	16.1	–	–	–	–	–	–	–	–	7.2	7.1	5.9	6.7

Grudziądz

$\varphi = 53°30'$ $\lambda = 18°46'$

I	–	–	–	–	-1.4	0.7	-0.4	-0.4	1.8	-3.1	9.9	7	-14.2	16	87	86	86	86	0.7	0.9	0.8	0.9	7.8	8.9	8.2	8.3
II	–	–	–	–	1.7	4.3	2.8	2.9	5.5	0.5	10.3	14	-3.4	24,25	90	79	88	86	0.7	1.9	1.2	1.3	8.7	7.6	7.7	8.0
III	–	–	–	–	0.5	5.9	2.6	2.9	7.4	1.2	16.2	13	-5.9	17	81	59	80	73	1.2	4.3	1.6	2.4	5.8	5.4	4.6	5.3
IV	–	–	–	–	4.1	11.2	6.6	7.1	12.7	1.8	24.6	28	-5.7	14	78	60	78	72	1.9	6.5	2.4	3.6	4.9	6.1	6.5	5.8
V	–	–	–	–	9.1	14.6	10.1	11.0	16.3	5.7	25.3	20	-0.8	6	74	54	74	67	3.3	8.6	3.7	5.2	6.3	7.3	5.0	6.2
VI	–	–	–	–	15.2	21.4	16.8	17.6	22.9	10.9	29.8	11	7.6	16	73	55	72	67	4.5	12.5	5.5	7.5	4.7	4.5	3.5	4.2
VII	–	–	–	–	17.7	22.8	18.4	19.3	24.4	14.2	31.4	4	9.9	29	–	–	–	–	–	–	–	–	6.5	5.8	4.6	5.6
VIII	–	–	–	–	15.5	20.6	16.4	17.2	22.2	12.6	26.5	12	8.2	31	–	–	–	–	–	–	–	–	6.1	7.1	4.6	5.9
IX	–	–	–	–	9.5	14.9	11.0	11.6	16.2	7.8	27.5	8	0.9	27	91	76	88	85	1.1	5.1	1.6	2.6	7.9	7.4	6.0	7.1
X	–	–	–	–	7.0	11.8	8.6	9.0	12.8	5.3	19.1	10	0.8	2	91	75	88	85	0.9	3.6	1.3	1.9	7.4	7.9	4.8	6.7
XI	–	–	–	–	4.0	6.6	4.5	4.9	8.0	2.2	15.3	5	-7.2	29	89	78	85	84	1.0	2.3	1.0	1.5	9.2	8.5	8.5	8.7
XII	–	–	–	–	-1.5	0.1	-0.8	-0.8	1.5	-3.4	7.4	8	-13.0	18	90	88	89	89	0.5	0.8	0.6	0.6	9.0	8.4	7.2	8.2
Rok	–	–	–	–	6.8	11.2	8.0	8.5	12.6	4.6	31.4	4.VII	-14.2	16.1	–	–	–	–	–	–	–	–	7.0	7.1	5.9	6.7

Osowiec

$\varphi = 53°29'$ $\lambda = 22°39'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.5	2.4	1.5	1.5	3.8	-0.5	7.7	15	-8.2	28	93	86	90	90	0.5	1.0	0.7	0.7	9.6	8.8	9.4	9.3
III	–	–	–	–	-2.1	2.9	0.2	0.3	5.2	-4.2	17.3	31	-13.5	17	82	65	83	77	0.9	3.2	1.2	1.8	8.3	7.0	8.2	7.8
IV	–	–	–	–	4.9	12.2	7.2	7.9	13.8	2.1	26.0	27	-5.8	13	86	53	78	72	1.4	8.2	2.5	4.0	6.3	5.8	7.1	6.4
V	–	–	–	–	9.4	14.3	9.8	10.8	16.4	5.0	25.7	19	-2.9	6	81	59	80	73	2.3	7.5	2.6	4.1	5.4	6.5	7.2	6.4
VI	–	–	–	–	13.7	20.6	15.6	16.1	22.4	9.2	29.9	11	3.5	21	84	59	79	74	2.7	10.6	4.0	5.8	6.5	5.1	6.0	5.9
VII	–	–	–	–	16.7	22.0	16.9	18.1	23.8	12.1	28.9	8	6.6	4	–	–	–	–	–	–	–	–	7.1	7.2	8.4	7.6
VIII	–	–	–	–	13.9	19.6	14.8	15.8	20.9	10.8	30.6	12	5.1	9	91	70	86	82	1.6	7.5	2.3	3.8	7.0	7.3	7.7	7.3
IX	–	–	–	–	10.1	14.4	10.2	11.2	15.6	6.8	27.4	9	1.3	17	93	77	90	87	0.9	4.3	1.3	2.2	8.4	7.8	8.5	8.2
X	–	–	–	–	6.3	11.1	7.5	8.1	12.3	3.7	18.5	19	0.1	5	93	81	93	89	0.6	2.7	0.8	1.4	8.1	7.2	8.0	7.8
XI	–	–	–	–	3.2	5.4	3.4	3.8	6.5	1.5	14.5	6	-8.9	29,30	–	–	–	–	–	–	–	–	9.0	8.9	8.9	8.9
XII	–	–	–	–	-2.7	-1.0	-2.1	-2.0	0.5	-5.2	5.5	5,13	-14.5	16,17	–	–	–	–	–	–	–	–	9.1	8.5	8.9	8.8
Rok	–	–	–	–	–	–	–	–	–	–	30.6	12.VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Szczuczyn

$H_s = 130\ m$ $h_w = 15\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D, °mD																	OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Suma	Max	Data	Temperatura T				Opad R			Wiatr v									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	Średnia prędkość				Min<0°	Max<0°	Min<10	Max≥25	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	10 ≤ v < 15	v ≥ 15								
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29.5	8.1	6	26	11	7	·	18	8	·	–	–	–	·	1	19	–				
II	–	–	·	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.2	4.8	18	13	3	·	·	21	14	·	–	–	–	·	·	17	–				
III	9.5	3.7	9	2.7	8	7.0	12	7.6	6.5	4.5	10.5	4.3	15.5	6.7	11	4.8	11	4.7	18.8	9.2	15	28	7	4	·	12	5	·	12	·	–	·	7	7	–				
IV	10	3.0	8	2.7	7	3.6	4.5	3.8	8.5	6.1	8	3.0	12	3.8	15	3.9	17	3.0	23.8	5.8	17	12	·	·	1	12	8	·	3	3	–	3	4	6	–				
V	14.5	3.2	11.5	3.4	8.5	2.8	4	4.8	5.5	4.6	9.5	4.7	9.5	4.4	16	3.6	14	3.2	21.3	6.0	11	4	·	·	1	12	4	·	1	·	–	1	1	10	–				
VI	15.5	2.5	3.5	2.0	2	3.0	7	4.5	5.5	4.1	10.5	4.8	18	3.9	16	3.5	12	3.2	54.6	10.2	5	·	·	·	8	10	9	1	2	1	–	4	3	10	–				
VII	8.5	2.2	7.5	2.7	7.5	2.3	6.5	3.0	8	3.6	13	4.2	19.5	3.8	9.5	2.8	13	2.8	96.0	18.5	30	·	·	·	9	20	16	2	5	2	–	15	1	14	–				
VIII	3.5	3.6	1	1.5	2.5	5.8	7	3.8	9	3.8	22.5	6.0	23	4.2	10.5	3.0	14	3.8	130.7	56.4	17	·	·	·	1	17	13	2	2	1	–	2	·	8	–				
IX	3	2.0	0.5	3.0	·	·	4	3.9	16	4.3	2.5	6.5	26.5	6.4	5	4.1	10	5.0	118.1	24.8	18	·	·	·	1	20	20	4	8	3	–	1	1	13	–				
X	0.5	3.0	·	·	·	·	5	2.5	1.9	4.4	4.0	5.5	16.5	5.8	4	4.1	8	4.6	10.4	2.3	30	·	·	·	·	11	4	·	1	·	–	·	2	12	–				
XI	7.8	6.3	8	4.4	7.5	3.7	1.5	5.8	7.5	4.4	14.5	5.5	17	4.2	1	10.0	12	4.3	21.8	6.4	28	11	1	·	·	12	6	·	5	·	–	·	·	25	–				
XII	2.5	5.0	4.5	3.9	6	3.2	5	2.2	15.5	4.9	3.4	7.8	7.5	7.2	3	6.5	15	5.2	28.5	10.1	8	26	13	5	·	18	8	1	7	1	–	·	3	18	–				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	594.7	56.4	17.VIII	120	35	16	21	183	115	10	–	–	–	26	23	159	–				

Kamień Krajeński

$H_s = 124\ m$ $h_w = 12\ m$

I	·	·	5	5.4	6	2.3	2	4.0	6	4.3	17	4.6	25	4.6	15	3.5	17	2.7	12.9	4.8	5	24	11	4	·	11	3	·	·	·	11	·	·	21	–				
II	5	4.8	1	4.0	6	1.5	3	2.3	14	2.2	10	2.1	25	2.8	3	5.0	17	4.9	31.0	6.5	18	12	·	·	·	14	11	·	·	·	6	·	·	17	–				
III	9	2.6	6	2.3	13	4.1	16	3.9	10	2.0	1	2.0	14	4.0	9	4.1	15	2.9	29.4	9.9	29	19	1	·	·	10	7	·	1	·	3	1	7	9	–				
IV	2.1	1.4	2.0	3.0	4	1.8	3	2.3	5	2.6	3	1.7	8	2.2	11	3.3	15	2.0	40.7	3.1	27	10	·	·	·	8	5	·	·	·	2	1	5	10	–				
V	1.8	1.8	2.0	3.2	2	2.0	9	2.4	1	4.0	7	1.6	8	3.4	19	3.3	9	2.4	38.3	14.0	10	3	·	·	·	7	5	2	·	·	·	1	3	7	–				
VI	4	2.8	11	1.2	13	1.2	3	1.0	6	1.1	1	1.0	17	2.3	24	1.9	11	1.5	34.5	21.7	9	·	·	·	9	9	5	1	·	·	·	1	8	3	–				
VII	1.1	2.1	8	1.2	9	1.6	4	1.0	3	1.7	9	1.2	15	1.9	22	3.0	12	1.8	203.3	67.6	23	·	·	·	10	21	17	6	·	·	·	9	·	10	–				
VIII	8	1.5	2	1.0	7	1.1	3	2.0	6	1.7	12	3.3	26	2.0	18	1.9	11	1.8	69.0	14.4	16	·	·	·	1	15	10	2	·	·	1	3	·	12	–				
IX	2	3.0	·	·	1	1.0	2	1.0	7	2.9	20	3.0	18	2.4	18	3.9	22	2.3	63.5	13.3	23	1	·	·	2	19	11	1	·	·	1	1	2	8	–				
X	2	1.0	·	·	1	1.0	2	1.0	9	1.4	2.8	2.4	2.4	2.0	8	3.1	19	1.7	14.4	3.6	19	1	·	·	·	12	5	·	·	·	8	·	2	11	–				
XI	5	5.8	9	3.7	18	1.4	12	1.7	5	1.4	13	1.7	12	5.3	4	5.0	12	2.4	15.7	8.6	28	12	2	·	·	8	4	·	2	·	3	·	1	20	–				
XII	7	1.1	7	5.7	6	2.7	8	1.1	5	1.2	16	2.4	26	4.7	7	7.1	11	2.7	29.4	10.7	8	22	9	4	·	11	5	1	2	1	6	·	3	18	–				
Rok	92	2.1	89	2.3	86	1.8	67	1.7	77	1.7	137	2.0	218	3.1	158	3.8	171	2.2	552.1	67.6	23.VIII	104	23	8	22	146	88	13	5	1	41	17	31	146	–				

Grudziądz

$H_s = 40\ m$ $h_w = 12{,}5\ m$

I	2	3.5	4	2.6	3	3.5	5	2.8	3.5	2.3	18.5	2.7	14.5	2.0	16.5	2.4	26	1.8	19.4	5.2	5	23	9	2		13	5	·	·	·	–	–	2	23	–				
II	4.5	2.2	1.5	1.3	·	·	4	1.6	8	1.9	18.5	1.8	10	2.9	6.5	1.6	32	1.3	49.0	13.6	18	12	·	·	·	16	13	1	·	·	–	–	1	18	–				
III	3	3.2	·	·	6.5	2.7	9.5	2.4	8	2.4	10	3.0	9	6.1	14	3.0	33	2.1	26.4	10.0	15	18	1	·	·	9	6	1	2	·	–	–	10	12	–				
IV	9	2.7	10.5	2.6	5.5	1.5	1.5	3.3	2.5	1.8	6	2.8	8	2.6	19	2.2	28	1.7	18.1	6.0	22	6	·	·	·	13	8	·	·	·	–	–	7	10	–				
V	12	2.6	11.5	2.8	4	2.2	5.5	1.9	2	1.0	5.5	4.1	8.5	3.8	17	2.3	27	1.9	35.7	18.2	9	1	·	·	2	12	8	1	2	·	–	–	4	10	–				
VI	1.2	2.0	8	1.7	2	2.5	3.5	2.9	1.5	2.0	5	2.5	1.8	3.3	16	2.5	24	1.9	84.3	60.0	4	·	·	·	10	8	6	2	·	·	–	–	7	4	–				
VII	5	2.3	10	1.8	3	2.7	4.5	1.2	0.5	2.0	11	2.8	15	2.3	21	2.8	23	1.8	146.3	28.0	16	·	·	·	15	19	16	7	1	·	–	–	5	6	–				
VIII	6	2.5	5	2.0	4	1.8	3	2.0	3	3.0	7	3.7	13.5	2.9	36.5	1.6	15	1.8	67.4	14.8	10	·	·	·	8	16	13	3	·	·	–	–	3	8	–				
IX	·	·	·	·	·	·	4.5	1.3	7.5	2.5	1.9	3.3	3.2	3.2	5	4.2	22	2.4	61.9	30.3	23	·	·	·	2	16	10	1	·	1	–	–	·	11	–				
X	0.5	3.0	·	·	1	2.0	1	1.0	9.5	1.3	1.5	2.6	2.7	2.1	4	1.6	35	1.3	12.5	2.0	23	·	·	·	·	9	7	·	·	·	–	–	4	11	–				
XI	4	6.5	5.5	2.3	15.5	2.2	11	2.2	7.5	2.3	9.5	1.7	13	2.9	3	7.0	21	2.1	12.4	5.3	28	12	1	·	·	8	6	·	2	·	–	–	·	21	–				
XII	4	2.5	3	2.7	5	2.2	·	·	8	2.7	30.5	2.6	13	2.7	8.5	2.4	21	2.0	21.5	8.1	8	23	10	3	·	9	8	·	·	·	–	–	·	20	–				
Rok	62	2.8	59	1.6	49.5	1.9	53	1.9	61.5	2.1	155.5	2.8	181.5	3.1	166	2.8	307	1.8	554.9	60.0	4.VI	95	21	5	37	148	106	16	7	1	–	–	43	154	–				

Osowiec

$H_s = 110\ m$ $h_w = 10{,}5\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.7	8.9	5	–	–	–	·	12	8	·	–	–	–	–	–	–	–				
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39.2	6.5	1	14	4	·	·	22	13	·	–	–	–	·	·	22	10				
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18.7	9.5	15	25	7	3	·	11	5	·	–	–	–	·	·	17	6.2				
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24.7	9.7	30	9	·	·	3	10	5	·	–	–	–	3	4	9	1				
V	1.5	3.0	8	4.0	9	3.1	17.5	3.6	8	4.1	2.5	3.2	7	4.9	21	3.5	5	3.4	30.7	10.2	7	4	·	·	1	11	6	1	·	·	–	1	2	12	·				
VI	4	3.4	2.5	2.6	3	3.3	11	4.4	9	3.6	16	4.1	10.5	5.7	24	4.1	10	3.7	64.1	14.5	5	·	·	·	10	10	9	3	3	1	–	·	5	9	·				
VII	8	2.5	14	2.8	2	2.0	13.5	3.7	13	3.9	15.5	5.1	17	5.3	6	3.4	4	3.8	84.4	30.0	12	·	·	·	11	18	13	2	2	·	–	2	·	16	·				
VIII	2	3.2	0.5	4.0	2.5	5.8	6	4.0	12	5.2	25	5.0	23.5	4.9	10.5	4.4	11	4.3	119.6	30.4	17	·	·	·	2	16	10	4	3	·	–	2	·	14	·				
IX	1.5	3.0	·	·	·	·	4.5	4.8	24.5	3.9	3.8	7.4	17	5.4	3.5	2.1	1	5.6	170.6	47.4	18	·	·	·	1	18	15	3	7	3	–	·	·	20	·				
X	0.5	1.0	0.5	1.0	·	·	1.6	3.0	33.5	3.5	32.5	4.5	7	4.4	·	·	3	3.6	17.2	9.2	1	·	·	·	·	6	5	·	2	·	–	·	·	17	·				
XI	7.5	10.0	5	8.2	6	3.2	2.4	6.1	13.5	4.6	14.5	5.2	3	5.3	4.5	7.3	11	5.5	25.1	7.8	28	11	1	·	·	14	6	·	11	3	–	·	·	22	1				
XII	3	2.0	1.0	3.3	2	3.5	7	3.3	23.5	5.7	22.5	5.3	12.5	5.4	6.5	1.4	6	4.3	34.5	11.7	30	30	13	5	·	13	9	1	6	4	–	·	·	23	9				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	652.5	47.4	18.IX	–	–	–	28	161	104	14	–	–	–	–	–	–				

Szczecin – Łabędzia

$\varphi = 53°27'$ $\lambda = 14°33'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.0	1.5	0.5	0.6	2.5	-1.8	10.5	6	-10.5	15	91	84	90	88	0.6	1.2	0.7	0.8	8.4	7.9	7.7	8.0
II	–	–	–	–	1.5	4.7	2.9	3.0	5.7	0.2	11.1	2	-5.1	26	92	79	90	87	0.6	1.9	0.8	1.1	7.2	8.0	6.4	7.2
III	–	–	–	–	1.4	7.6	3.8	4.2	9.0	0.2	16.7	13	-4.8	17	86	60	78	76	1.0	4.5	1.9	2.5	5.9	6.0	4.7	5.5
IV	–	–	–	–	4.2	10.0	5.6	6.4	11.6	1.7	21.1	5	-4.3	15	86	63	80	76	1.3	5.2	2.1	2.9	7.1	6.6	3.8	5.8
V	–	–	–	–	8.4	13.6	9.0	10.0	15.3	4.8	25.4	16	-1.1	6	78	53	73	68	2.6	8.2	3.3	4.7	5.1	6.7	4.7	5.5
VI	–	–	–	–	14.8	20.5	15.8	16.7	22.2	10.8	30.5	14,29	6.2	1,26	74	51	71	65	4.7	12.9	5.6	7.7	5.6	5.9	4.0	5.2
VII	–	–	–	–	16.4	21.3	17.7	18.5	22.9	13.7	31.6	1,4	9.7	28	86	64	78	76	2.7	10.1	5.2	6.0	7.0	7.3	6.5	6.9
VIII	–	–	–	–	14.2	19.0	15.1	15.8	20.3	11.5	26.7	11	5.6	23	87	63	82	77	2.2	8.6	3.4	4.7	7.1	7.6	4.7	6.5
IX	–	–	–	–	9.6	13.8	10.4	11.0	15.3	7.4	25.5	8	4.8	26	91	71	88	83	1.1	4.9	1.5	2.5	7.8	7.7	4.8	6.8
X	–	–	–	–	7.4	11.9	9.4	9.5	12.9	5.9	18.1	10	0.6	2	92	75	87	85	0.8	3.6	1.5	2.0	8.3	7.4	6.1	7.3
XI	–	–	–	–	3.5	6.0	4.7	4.7	7.0	2.3	14.1	4	-3.9	24,30	90	80	86	85	0.8	2.0	1.2	1.3	8.1	8.2	7.4	7.9
XII	–	–	–	–	-0.1	1.1	0.2	0.4	–	-2.1	–	–	-11.2	17	91	85	91	89	0.5	1.0	0.6	0.7	8.9	8.2	6.5	7.9
Rok	–	–	–	–	6.8	10.9	7.9	8.4	–	4.6	31.6	1.4.VIII	-11.2	17.XII	87	69	83	80	1.6	5.3	2.3	3.1	7.2	7.3	5.6	6.7

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$

I	1018.6	1032.7	999.0	1019.5	0.7	2.1	1.0	1.2	3.2	-1.5	11.0	6	-10.2	16	88	82	87	86	0.8	1.4	0.9	1.0	8.6	7.8	7.5	8.0
II	1007.8	1037.2	980.4	1008.7	1.9	5.4	3.1	3.4	6.4	0.1	10.6	2	-7.9	26	90	77	90	86	0.7	2.1	0.8	1.2	7.7	8.0	6.5	7.4
III	1016.0	1037.7	994.5	1016.9	1.1	8.2	3.8	4.2	9.8	-0.4	17.3	27	-8.7	2	89	61	79	76	0.8	4.5	1.8	2.4	5.6	6.0	4.7	5.4
IV	1018.3	1031.2	994.2	1019.2	4.0	10.8	6.0	6.7	12.6	1.4	21.8	5	-6.6	15	90	64	82	79	0.8	5.3	1.8	2.6	7.8	6.6	4.0	6.1
V	1015.9	1030.4	1005.8	1016.8	8.6	14.4	9.6	10.6	16.1	4.4	26.0	16	-3.8	9	83	56	76	72	2.0	7.9	2.8	4.2	5.3	7.0	5.1	5.8
VI	1015.2	1032.6	1003.3	1016.1	14.9	21.2	16.6	17.3	22.9	10.1	30.9	29	5.9	21,24	81	57	77	72	3.5	12.1	4.7	6.8	5.4	5.8	4.1	5.1
VII	1010.8	1022.9	1000.8	1011.7	16.8	22.2	18.5	19.0	24.0	14.2	32.4	4	10.3	16	88	66	81	78	2.4	10.0	4.6	5.7	6.7	7.1	6.5	6.8
VIII	1011.6	1023.1	997.7	1012.5	14.3	19.6	15.4	16.2	21.1	11.9	26.6	11	7.5	23	90	65	85	80	1.6	8.4	2.9	4.3	6.8	7.6	5.4	6.6
IX	1009.9	1023.0	988.6	1010.8	10.0	14.7	10.8	11.6	16.3	7.7	25.9	8	2.9	27	92	72	91	85	1.0	5.1	1.2	2.4	7.5	8.1	5.4	7.0
X	1016.1	1027.5	999.4	1017.0	7.9	12.5	9.5	9.8	13.7	6.1	19.1	10	-0.7	2	92	75	88	85	0.9	3.6	1.5	2.0	8.1	7.7	5.5	7.1
XI	1019.1	1037.4	999.6	1020.0	3.9	6.7	5.0	5.2	7.6	2.4	14.8	4	-6.0	21	90	80	85	85	0.8	2.1	1.3	1.4	8.0	8.5	7.6	8.0
XII	1012.5	1030.9	972.1	1013.4	0.4	1.6	0.5	0.7	2.8	-2.2	9.7	8	-13.3	17	89	84	88	87	0.7	1.1	0.7	0.8	8.7	8.1	6.1	7.6
Rok	1014.3	1037.7	972.1	1015.2	7.0	11.6	8.3	8.8	13.0	4.5	32.4	4.VII	-13.3	17.XII	88	70	84	81	1.3	5.3	2.1	2.9	7.2	7.4	5.7	6.8

Wierzchowo

$\varphi = 53°27'$ $\lambda = 16°06'$

I	–	–	–	–	-1.1	0.2	-0.7	-0.6	–	–	–	–	–	–	89	87	89	88	0.6	0.8	0.6	0.7	9.0	8.4	8.4	8.6
II	–	–	–	–	0.6	4.0	1.7	2.0	–	–	–	–	–	–	92	81	91	88	0.5	1.6	0.7	0.9	7.2	6.4	7.1	6.9
III	–	–	–	–	0.3	6.5	1.9	2.6	–	–	–	–	–	–	88	68	84	80	0.8	3.6	1.2	1.9	5.4	4.6	4.1	4.7
IV	–	–	–	–	3.8	10.3	5.2	6.1	–	–	–	–	–	–	87	64	83	78	1.1	5.7	1.6	2.8	6.2	6.0	5.3	5.8
V	–	–	–	–	8.6	13.1	8.3	9.6	–	–	–	–	–	–	74	56	77	69	3.2	7.7	2.7	4.5	4.6	5.6	4.6	4.9
VI	–	–	–	–	14.6	20.5	15.0	16.3	–	–	–	–	–	–	73	52	76	67	4.9	12.8	4.4	7.4	5.1	4.6	4.4	4.7
VII	–	–	–	–	16.6	21.4	16.8	17.9	–	–	–	–	–	–	85	65	82	77	3.1	9.8	3.8	5.8	6.4	5.9	6.8	6.4
VIII	–	–	–	–	14.0	18.4	14.1	15.2	–	–	–	–	–	–	88	68	88	81	1.9	7.2	2.0	3.7	6.3	6.5	5.9	6.2
IX	–	–	–	–	9.5	13.5	9.3	10.4	–	–	–	–	–	–	91	72	90	84	1.1	4.8	1.3	2.4	7.3	6.5	6.0	6.6
X	–	–	–	–	6.7	11.4	7.5	8.3	–	–	–	–	–	–	93	79	90	87	0.7	3.0	1.0	1.6	8.0	7.0	5.8	6.9
XI	–	–	–	–	2.9	5.2	3.6	3.8	–	–	–	–	–	–	92	84	90	89	0.5	1.5	0.7	0.9	7.6	7.8	7.8	7.7
XII	–	–	–	–	-1.2	0.2	-0.9	-0.7	–	–	–	–	–	–	91	88	92	90	0.5	0.7	0.5	0.6	8.8	7.6	7.6	8.0
Rok	–	–	–	–	6.3	10.4	6.8	7.6	–	–	–	–	–	–	87	72	86	82	1.6	4.9	1.7	2.7	6.8	6.4	6.2	6.5

Kołno

$\varphi = 53°25'$ $\lambda = 21°56'$

I	–	–	–	–	-2.9	-1.0	-1.9	-1.9	0.3	-4.8	6.6	9	-18.6	16	–	–	–	–	–	–	–	–	8.5	7.6	7.1	7.7
II	–	–	–	–	0.4	2.6	1.2	1.4	3.7	0.7	7.7	14	-8.0	28	–	–	–	–	–	–	–	–	8.6	8.4	6.1	7.7
III	–	–	–	–	-2.0	3.7	0.4	0.5	5.3	-4.0	17.0	31	-15.1	17	–	–	–	–	–	–	–	–	4.9	5.0	4.1	4.7
IV	–	–	–	–	4.7	12.3	6.7	7.8	13.7	1.9	25.4	29	-7.4	10	–	–	–	–	–	–	–	–	4.6	5.1	4.0	4.6
V	–	–	–	–	9.2	14.0	5.0	10.3	15.9	5.1	26.4	19	-2.6	6	83	61	86	77	2.1	7.1	1.4	3.5	4.2	6.3	4.0	4.8
VI	–	–	–	–	14.8	20.3	15.0	16.3	–	–	–	–	–	–	79	58	84	74	3.7	11.2	3.0	6.0	5.7	4.8	3.5	4.7
VII	–	–	–	–	16.7	21.6	16.7	17.9	23.6	12.8	28.9	4	7.0	7	87	67	89	81	2.7	9.2	2.2	4.7	6.2	6.7	6.9	6.6
VIII	–	–	–	–	14.0	19.4	14.5	15.6	21.0	11.1	29.3	12	5.5	24	91	69	92	84	1.6	7.8	1.3	3.5	6.7	6.9	4.7	6.1
IX	–	–	–	–	9.3	14.3	10.1	11.0	15.8	7.1	26.7	9	0.6	27	93	73	93	87	0.7	5.3	1.1	2.4	7.9	7.8	6.1	7.3
X	–	–	–	–	5.1	11.2	7.1	7.6	12.4	3.5	19.2	10	-0.9	3,15	–	–	–	–	–	–	–	–	6.6	7.0	4.5	6.0
XI	–	–	–	–	3.0	5.1	3.7	3.9	6.8	1.8	15.2	6	-8.8	29,30	96	88	94	93	0.3	1.0	0.5	0.6	8.5	8.5	8.2	8.4
XII	–	–	–	–	-2.9	-0.9	-2.3	-2.1	0.6	-4.3	5.3	5	-12.9	18	92	87	93	91	0.4	0.7	0.3	0.5	7.4	7.8	6.6	7.3
Rok	–	–	–	–	5.8	10.2	6.3	7.2	–	–	–	–	-18.6	16.1	–	–	–	–	–	–	–	–	6.6	6.8	5.5	6.3

Szczecin – Łabędzia $H_s = 69\ m$ $h_w = 10\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU [%D, %nD]																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max≥25°	R≥0.1	R≥1.0	R≥10.0	v≥10	v≥15					
I	7.5	4.3	6.5	3.5	11.5	3.1	3.5	2.7	4.5	2.8	11.5	4.5	8.6	4.3	16	3.7	6	3.4	35.9	8.7	5	22	6	1	·	16	9	·	·	·	8	·	2	20	7
II	12.5	2.2	1.1	2.1	7.5	2.7	1.0	3.2	1.2	4.2	8	3.9	10.5	4.3	6.5	3.2	6	3.0	32.7	8.0	8	12	·	·	·	16	9	·	·	·	·	·	1	13	1
III	1.2	2.7	14.5	3.1	13.5	6.3	7	6.7	1.5	3.0	5	4.6	12.5	4.7	1.8	3.2	9	3.8	42.9	10.7	17	1.4	·	·	·	12	9	1	5	·	2	1	6	8	1
IV	30.5	2.8	17.5	2.9	1	5.0	·	·	·	·	4	3.6	6	4.2	2.6	3.0	5	2.9	18.0	4.4	19	9	·	·	·	10	6	·	·	·	3	2	2	5	·
V	40.5	3.0	1.5	4.6	2	4.2	0.5	4.0	1	3.5	2	3.8	8	4.8	1.4	3.6	10	3.2	48.8	19.9	16	2	·	·	1	8	5	2	1	·	1	3	2	5	·
VI	22.5	2.4	10.5	3.0	2	4.2	1	5.0	·	·	6	4.9	1.6	4.1	2.5	2.8	7	2.9	45.6	20.2	24	·	·	·	8	10	7	2	·	·	·	4	6	5	·
VII	2.4	2.8	4.5	3.9	1	8.0	0.5	8.0	1	6.0	5	4.1	13.5	3.4	10.5	3.1	3	3.2	73.0	24.9	21	·	·	·	7	15	11	1	·	·	2	10	1	11	·
VIII	11.5	1.9	2	1.5	2	5.0	2.5	4.0	5.5	5.9	1.5	5.7	2.3	3.9	2.7.5	2.5	4	3.5	56.8	12.0	24	·	·	·	1	1.7	1.2	1	1	·	2	2	·	8	·
IX	1.2	2.5	1.5	2.0	1	2.0	1	7.5	5.5	6.8	4.0	6.6	2.1	4.8	3.5	2.7	3	3.8	82.4	22.2	22	·	·	·	1	19	1.4	1	1	·	2	4	1	11	·
X	6	1.6	3	2.3	1	4.0	0.5	3.0	4	5.5	1.7	5.1	2.7	3.6	2.6.5	2.5	8	3.2	19.8	5.2	23	·	·	·	·	10	5	·	·	·	6	·	1	12	·
XI	21.5	3.2	2.1	3.1	9	3.7	3	4.3	3.5	4.4	7	4.6	1.7	5.0	7	4.4	1	3.8	21.8	6.1	9	1.3	1	·	·	12	6	·	1	·	·	·	2	20	·
XII	4.5	3.6	11.5	4.5	5.5	4.4	3	3.7	6.5	4.2	2.4	4.6	2.5	3.5	1.3	3.4	·	4.0	30.2	12.0	8	2.1	-	2	·	1.3	8	1	1	·	6	·	·	1.9	4
Rok	20.5	2.5	11.8.5	3.0	5.7	4.4	3.2.5	4.3	4.5	3.9	11.4.5	4.7	2.0.5.5	4.2	2.5.5	3.2	6.2	3.4	5.0.7.9	2.4.9	2.1.VII	9.3	-	3	4.8	1.5.8	1.0.4	9	1.0	·	3.2	2.6	2.4	1.3.7	1.5

Szczecin – Dąbie $H_s = 1\ m$ $H_b = 6,9\ m$ $h_w = 21,5\ m$

I	1.5	4.3	4.5	6.2	4	3.2	7.5	3.2	2.5	3.8	4.4.5	4.6	2.0	5.2	7.5	4.5	1	4.6	2.7.5	7.0	5	20	4	1	·	15	5	·	2	·	4	·	2	21	6
II	2.5	3.4	2	3.2	6.5	2.3	1.1	3.7	7.5	5.2	3.7.5	4.7	1.3	4.6	2	4.0	2	4.2	2.3.0	5.4	1.3	1.4	·	·	·	15	7	·	·	·	·	·	1	1.3	·
III	4.5	5.4	5	4.6	1.0	4.6	2.4.5	7.3	4.5	6.0	1.5.5	4.3	1.8.5	4.8	4.5	4.6	9	4.9	3.7.6	9.1	15,17	1.7	·	·	·	1.1	9	·	6	·	1	1	6	9	1
IV	2.7.5	3.9	1.8	3.8	1.1	2.5	4	2.2	1	3.0	4	4.0	1.4.5	3.4	7	4.7	3	3.5	1.2.7	3.0	1.9	9	·	·	·	8	5	·	·	·	5	2	2	6	·
V	1.0.5	4.6	2.3.5	4.1	7	1.6	1.4.5	4.0	0.5	5.0	9.5	3.0	1.2	5.0	7.5	3.3	8	3.5	3.6.8	1.2.8	1.9	4	·	·	2	6	6	2	1	·	3	3	1	5	·
VI	4	4.1	1.5.5	3.1	8	2.2	8	4.2	1	5.0	8	4.7	2.5.5	3.7	1.2	3.7	8	3.3	4.2.7	2.1.7	5	·	·	·	1.0	9	5	2	·	·	2	3	6	5	·
VII	1.2.5	3.3	9	2.2	7	1.7	5	3.6	2	6.5	1.1.5	4.0	2.6.5	3.4	1.1.5	3.8	8	3.0	1.0.5.3	3.5.4	1.4	·	·	·	1.1	1.4	1.1	3	·	·	4	9	2	1.0	·
VIII	1	2.5	2	4.0	2	2.5	1.0	3.6	4.5	4.6	3.3.5	4.7	2.7.5	3.4	8.5	3.6	4	3.8	4.2.5	1.1.6	8.4	·	·	·	2	1.7	1.2	1	1	·	3	3	·	1.0	·
IX	7.5	3.2	2	2.5	·	·	2.5	2.4	8	5.6	2.6.5	4.6	2.3.5	4.0	1.4	4.1	6	3.9	8.2.8	3.0.0	22	·	·	·	1	1.8	1.7	1	1	·	5	2	·	1.1	·
X	3	2.2	·	·	1	4.0	3	2.7	5.5	5.1	4.4	4.9	2.4.5	4.0	5	3.6	7	4.1	1.3.9	5.8	23	1	·	·	·	8	4	·	·	·	7	·	1	1.3	·
XI	5.5	4.8	6.5	5.0	1.6.5	3.4	2.3.5	4.0	3.5	5.3	1.5	5.4	1.1	5.9	4.5	5.6	4	4.4	1.8.0	3.6	8	1.2	·	·	·	1.0	8	·	·	·	1	·	2	2.2	·
XII	4	4.0	7	5.1	5.5	3.9	7.5	3.8	5.5	4.8	3.8	4.9	1.7.5	4.9	7	3.7	1	4.6	2.9.6	1.1.1	8	1.7	5	3	·	1.1	9	1	3	·	3	·	1	1.6	3
Rok	8.4	3.8	9.5	3.6	7.8.5	2.7	1.1.8	3.7	4.6	5.0	2.8.7.5	4.5	2.3.4	4.4	9.1	4.1	6.1	4.0	4.7.2.4	3.5.4	1.4.VII	9.4	9	4	2.6	1.4.2	9.8	1.0	1.4	·	3.8	2.3	2.4	1.4.1	1.0

Wierzchowo $H_s = 140\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.6.9	1.5.3	5	-	-	-	-	8	5	2	-	-	-	·	·	2.3	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.4.9	7.0	1.3	-	-	-	-	1.7	1.0	·	-	-	-	·	1	9	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.1.7	1.5.0	1.5	-	-	-	-	1.0	9	1	-	-	-	·	8	6	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.4.8	1.2.2	3.0	-	-	-	-	1.0	8	1	-	-	-	·	4	7	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.0.6	8.0	1.3	-	-	-	-	6	1	·	-	-	-	·	5	6	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.8.2	2.1.0	9	-	-	-	-	9	8	1	-	-	-	·	7	5	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.9.3	1.8.5	2.2	-	-	-	-	1.5	1.4	5	-	-	-	·	1	7	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.3.2	1.3.5	9	-	-	-	-	1.6	1.3	2	-	-	-	·	·	6	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.1.0.1	2.1.0	1	-	-	-	-	1.9	1.4	4	-	-	-	·	1	8	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.3.8	1.2.2	3	-	-	-	-	7	6	1	-	-	-	·	1	1.1	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2.1.9	4.9	27	-	-	-	-	9	8	·	-	-	-	·	2	1.9	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.1.8	2.2.8	8	-	-	-	-	1.1	7	1	-	-	-	·	·	1.8	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5.7.5.2	2.4.0	1.1.X	-	-	-	-	1.3.7	1.0.3	1.8	-	-	-	·	3.0	1.2.5	-

Kalno $H_s = 125\ m$ $h_w = 13\ m$

I	·	·	6	7.2	·	·	8	3.2	7	4.0	3.7	6.1	1.5	7.2	1	1.2.0	1.9	4.8	4.1.2	1.3.8	5	2.6	1.0	6	·	1.6	1.0	1	7	1	2	·	1	1.8	2.4
II	1	5.0	3	3.0	4.5	2.8	5	3.2	1.4	4.7	3.1.5	4.5	8	5.5	2	7.0	1.5	3.7	4.5.9	7.0	8	1.4	4	·	·	2.1	1.7	·	1	·	2	·	·	1.3	5.2
III	9	3.7	7	4.9	9	6.1	6	5.8	8	5.6	1.4	5.1	6	5.3	8	5.6	2.6	3.8	2.1.7	1.2.5	1.5	2.5	7	2	·	7	6	1	3	·	1	·	1.1	8	4
IV	1.8	4.3	2	3.0	1.1.5	2.7	4.5	2.1	1.0.5	5.1	1.2.5	4.7	6	4.2	8	4.9	1.7	3.3	1.7.4	3.5	3.0	9	·	·	1	1.3	7	·	3	·	·	4	9	5	·
V	1.4	5.1	9.5	5.1	7	2.6	6	4.0	9.5	4.1	6.5	8.9	9	4.9	1.1.5	4.4	2.0	3.8	1.4.5	6.5	1.9	4	·	·	1	9	3	·	2	4	1	4	1.0	8	·
VI	6	5.0	6	3.2	1.5	2.0	4	4.0	1.3	4.4	1.5.5	4.6	1.2	4.5	1.1	4.5	2.1	3.3	6.6.0	1.8.0	1.0	·	·	·	-	1.0	9	1	2	4	·	4	1.0	8	·
VII	8.5	3.1	4	3.6	3	2.8	6	3.8	1.4	2.3	1.4.5	2.9	1.5.5	4.0	1.5	3.3	2.6	2.3	4.0.8.0	1.3.0	2.7	·	·	·	1.0	1.6	1.6	4	1	1	2	8	2	1.6	·
VIII	·	·	·	·	1	3.0	5	3.1	1.5.5	3.4	2.6.5	5.9	1.7	4.0	8	3.8	2.0	3.5	1.6.4.7	7.8.3	1.7	·	·	·	·	1.7	1.3	3	2	·	5	1	3	9	·
IX	1.5	2.3	·	·	·	·	·	·	1.6.5	4.0	3.3.5	6.5	1.7	8.5	1.5	3.0	2.0	4.8	1.3.2.7	2.8.6	1.5	·	·	·	1	1.5	1.1	5	8	4	4	1	1.4	4	·
X	3	1.3	2	1.5	·	·	2	5.0	1.2	3.1	3.9	5.6	8	7.5	3	2.8	2.4	3.7	1.2.9	2.8	2.4	3	·	·	·	9	6	·	4	1	1.2	·	5	1.0	·
XI	8	1.1.9	1.2.5	2.9	1.2	3.9	7	5.4	9.5	3.3	1.4	4.6	1.0.5	6.9	1.5	4.3	1.5	4.3	2.2.2	5.5	27	8	1	·	·	1.1	8	·	4	3	7	·	4	2.5	·
XII	6.5	7.0	4.5	3.4	6	3.7	2.5	2.8	1.3.6	3.5	2.9.5	7.5	8	8.1	2.5	5.0	2.0	4.6	2.9.6	8.9	3.0	2.6	1.2	5	·	1.2	8	·	6	4	7	·	3	1.7	6
Rok	7.5.5	4.1	3.6.5	3.2	5.5.9	2.5	5.6	3.5	1.4.3	4.0	2.7.4	5.6	1.3.2	5.9	5.2.5	5.0	2.4.3	3.8	6.7.1.6	7.8.3	1.7.VIII	1.1.5	3.4	1.3	-	1.5.6	1.1.4	1.5	4.3	1.6	4.3	2.2	5.9	1.5.1	3.9

Świecie

$\varphi = 53°24'$ $\lambda = 18°27'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.8	1.0	-0.4	-0.2	1.8	-3.0	9.7	6	-15.1	16	87	84	87	86	0.7	1.1	0.7	0.8	8.8	8.3	7.0	8.0
II	–	–	–	–	2.3	4.8	2.6	3.1	5.6	0.1	9.7	14	-5.0	25	91	79	86	85	0.7	1.9	1.1	1.2	8.1	6.8	6.6	7.2
III	–	–	–	–	4.3	6.5	2.9	3.4	7.6	-1.3	16.9	31	-6.5	11	80	60	77	72	1.5	4.1	1.8	2.5	4.0	5.0	3.4	4.1
IV	–	–	–	–	4.7	11.2	6.3	7.1	12.7	1.2	24.4	29	-7.0	13	86	58	81	75	1.3	6.6	2.2	3.4	6.4	7.3	6.4	6.7
V	–	–	–	–	8.9	14.2	9.0	10.3	16.0	4.9	26.1	19	-1.4	6	–	–	–	–	–	–	–	–	6.3	7.0	6.1	6.5
VI	–	–	–	–	14.6	20.9	16.0	16.9	23.1	10.2	30.1	11	5.5	15	78	54	75	69	3.9	12.3	4.8	7.0	4.8	5.3	6.1	5.3
VII	–	–	–	–	16.8	22.7	17.5	18.6	24.3	13.7	32.4	8	8.4	3	–	–	–	–	–	–	–	–	6.7	6.4	7.2	6.8
VIII	–	–	–	–	14.2	19.8	15.0	16.0	21.4	11.6	26.5	11	7.4	23	90	65	89	81	1.7	8.6	2.0	4.1	5.9	7.2	5.9	6.3
IX	–	–	–	–	9.3	14.2	10.4	11.1	16.2	6.8	27.4	8	0.3	27	95	72	90	86	0.6	5.2	1.4	2.4	7.7	7.6	5.7	7.0
X	–	–	–	–	6.6	11.5	8.4	8.7	13.2	4.8	19.1	19	-0.3	2	96	79	92	89	0.4	2.9	0.9	1.4	7.9	7.4	6.0	7.1
XI	–	–	–	–	4.3	6.7	4.6	5.0	8.0	2.3	16.3	5	-7.2	30	93	78	90	87	0.6	2.2	0.8	1.2	9.3	8.5	8.2	8.7
XII	–	–	–	–	-1.1	0.5	-0.9	-0.6	1.7	-3.2	7.4	5,8	-13.6	18	92	88	92	91	0.4	0.8	0.4	0.5	8.3	8.5	6.9	7.9
Rok	–	–	–	–	6.8	11.2	7.6	8.3	12.6	4.0	32.4	8.VII	-15.1	16.1	–	–	–	–	–	–	–	–	7.0	7.1	6.3	6.8

Sokółka

$\varphi = 53°24'$ $\lambda = 23°30'$

I	–	–	–	–	-3.2	-4.8	-2.0	-2.2	-0.5	-4.9	5.7	6,9	-19.9	16	94	91	93	93	0.2	0.5	0.4	0.4	9.0	8.5	7.9	8.5
II	–	–	–	–	-0.4	4.8	0.2	0.4	2.8	-4.9	7.0	21	-13.2	28	96	88	93	92	0.2	0.8	0.4	0.5	9.4	8.2	6.3	8.0
III	–	–	–	–	-3.3	2.4	-0.8	-0.6	4.1	-5.6	15.6	28	-15.6	4	88	64	80	77	0.6	3.3	1.3	1.7	6.1	5.0	5.1	5.4
IV	–	–	–	–	5.0	11.6	6.9	7.6	13.0	2.3	24.8	30	-6.7	10	87	53	78	73	1.3	7.7	2.5	3.8	5.1	6.5	5.0	5.5
V	–	–	–	–	9.2	14.3	9.9	10.8	16.1	5.4	26.1	19	-2.1	6	82	60	82	75	2.2	7.2	2.3	3.9	5.2	7.1	5.6	6.0
VI	–	–	–	–	14.5	20.8	15.1	16.4	22.3	9.6	29.8	12	2.9	21	79	54	79	71	3.7	12.1	3.9	6.6	5.2	5.9	5.0	5.4
VII	–	–	–	–	16.3	22.1	17.0	18.1	23.9	12.8	29.2	8	7.1	7	86	62	85	78	2.8	10.8	3.1	5.6	6.1	6.6	6.5	6.4
VIII	–	–	–	–	13.7	18.5	14.4	15.2	20.5	11.1	29.1	12	4.5	24	93	73	91	86	1.2	6.3	1.5	3.0	6.4	7.0	5.4	6.3
IX	–	–	–	–	8.9	13.7	9.8	10.6	14.9	7.0	26.0	9	0.6	27	96	76	94	89	0.5	4.4	0.8	1.9	7.9	7.8	5.8	7.2
X	–	–	–	–	5.3	10.6	7.2	7.6	11.6	4.0	18.0	10,11	-0.5	16	95	77	92	88	0.4	3.3	0.9	1.5	7.3	6.6	4.9	6.3
XI	–	–	–	–	2.2	4.4	3.0	3.2	5.8	0.7	13.8	2	-10.9	30	95	84	91	90	0.4	1.4	0.7	0.8	8.5	7.9	7.8	8.1
XII	–	–	–	–	-3.9	-1.8	-3.2	-3.0	-0.5	-5.8	3.2	9	-13.0	19	92	87	92	90	0.3	0.7	0.4	0.5	7.0	7.2	6.6	6.9
Rok	–	–	–	–	5.4	9.7	6.5	7.0	11.2	2.9	29.8	12.VI	-19.9	16.1	90	72	88	83	1.2	4.9	1.5	2.5	6.9	7.0	6.0	6.6

Myszyniec - Zawadzie

$\varphi = 53°23'$ $\lambda = 21°24'$

I	–	–	–	–	-2.7	-0.6	-1.6	-1.6	0.4	-4.8	7.5	6	-19.1	16	90	87	89	89	0.5	0.8	0.6	0.6	8.2	7.6	7.0	7.6
II	–	–	–	–	0.6	3.1	1.2	1.5	3.7	-0.7	7.9	14	-7.1	28	95	86	91	91	0.4	1.1	0.6	0.7	9.0	7.2	5.9	7.4
III	–	–	–	–	-1.8	4.9	0.2	0.9	5.9	-4.0	17.3	31	-15.6	17	82	60	80	74	0.9	4.1	1.4	2.1	5.3	2.8	4.0	4.0
IV	–	–	–	–	3.9	13.1	6.4	7.4	14.0	0.8	26.7	27	-7.5	10	88	47	78	71	1.1	9.7	2.5	4.4	4.7	2.4	5.2	4.1
V	–	–	–	–	8.8	14.2	8.4	10.0	15.5	3.7	27.0	19	-4.2	2	80	56	81	72	2.4	8.1	2.3	4.3	4.5	4.5	4.1	4.4
VI	–	–	–	–	15.1	20.7	14.6	16.2	22.0	8.8	29.0	11	2.7	21	76	54	79	70	4.4	12.2	3.6	6.7	4.9	4.0	3.2	4.0
VII	–	–	–	–	16.8	22.2	16.8	18.2	23.4	12.3	30.2	8	6.8	7	83	61	82	75	3.3	11.2	3.7	6.1	4.9	4.9	4.9	4.9
VIII	–	–	–	–	13.9	19.0	14.6	15.5	20.5	10.7	27.9	12	5.0	24	89	67	87	81	1.8	7.8	2.3	4.0	5.1	5.9	5.1	5.4
IX	–	–	–	–	9.4	14.3	10.2	11.0	15.3	7.3	26.8	9	1.0	27	90	67	87	81	1.3	6.1	1.7	3.0	7.2	6.2	5.5	6.3
X	–	–	–	–	5.3	11.5	7.0	8.0	12.2	3.9	18.6	10	-0.3	3	93	71	88	84	0.7	4.1	1.4	2.1	6.1	6.1	3.9	5.4
XI	–	–	–	–	3.2	5.3	3.8	4.0	6.4	1.8	15.3	6	-12.1	29	91	81	90	87	0.6	1.8	0.8	1.1	8.0	7.9	7.9	7.9
XII	–	–	–	–	-3.0	-0.6	-2.2	-2.0	0.4	-4.9	5.6	5	-14.7	18	92	87	90	90	0.3	0.7	0.5	0.5	6.3	7.2	6.7	6.7
Rok	–	–	–	–	5.8	10.6	6.6	7.4	11.6	2.9	30.2	8.VII	-19.1	16.1	87	69	85	80	1.5	5.6	1.8	3.0	6.2	5.6	5.3	5.7

Nidzica

$\varphi = 53°22'$ $\lambda = 20°25'$

I	–	–	–	–	-2.6	-1.0	-1.9	-1.8	0.8	-5.8	8.0	8	-20.6	15	90	88	88	89	0.6	0.7	0.7	0.7	9.0	8.1	7.6	8.2
II	–	–	–	–	1.0	3.1	1.7	1.9	4.2	-1.1	8.5	14	-7.7	24	89	84	89	87	0.7	1.3	0.8	0.9	9.7	8.1	7.4	8.4
III	–	–	–	–	-1.2	4.6	0.7	1.2	5.9	-3.7	16.4	31	-14.2	17	–	–	–	–	–	–	–	–	5.4	5.3	4.3	5.0
IV	–	–	–	–	4.1	11.7	5.7	6.8	13.1	0.1	24.9	27	-10.1	14	86	54	79	72	1.3	7.7	2.0	3.7	6.3	5.7	4.6	5.5
V	–	–	–	–	8.6	13.0	8.8	9.8	14.8	3.9	26.3	19	-2.6	6	79	60	82	74	2.5	7.0	2.3	3.9	6.0	6.8	5.8	6.2
VI	–	–	–	–	14.8	19.5	14.3	15.7	21.2	8.6	28.2	11	3.1	21	78	60	80	73	3.8	10.0	3.4	5.7	4.9	6.1	4.6	5.2
VII	–	–	–	–	16.7	21.1	17.0	18.0	23.3	12.3	29.3	8	6.1	7	84	66	85	78	3.2	9.3	3.0	5.2	–	–	–	–
VIII	–	–	–	–	14.2	18.7	14.7	15.6	20.3	10.1	26.2	12	4.0	24	89	68	87	81	1.9	7.2	2.2	3.8	–	–	–	–
IX	–	–	–	–	8.9	13.4	10.4	10.8	15.1	6.4	25.8	9	0.1	27	87	72	87	82	1.2	4.8	1.6	2.5	–	–	–	–
X	–	–	–	–	5.9	10.8	7.0	7.7	11.9	3.3	18.9	10	-1.4	3	93	76	89	86	0.7	3.2	1.1	1.7	–	–	–	–
XI	–	–	–	–	3.2	5.1	3.4	3.8	6.7	1.1	14.7	5	-14.8	29	89	82	87	86	0.8	1.6	1.0	1.1	–	–	–	–
XII	–	–	–	–	-2.9	-0.9	-2.1	-2.0	0.6	-5.1	5.4	9	-14.7	18	88	85	88	87	0.6	0.9	0.6	0.7	7.7	7.6	7.0	7.4
Rok	–	–	–	–	5.9	9.9	6.6	7.2	11.5	2.5	29.3	8.VII	-20.6	15.1	–	–	–	–	–	–	–	–	–	–	–	–

Świecie

$H_s = 25\ m$ $h_w = 10\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, %nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-20	Max<0°	Min<-10°	Max>25°	Opad R 0.1 ÷ 1 mm	1 ÷ 10 mm	10 ÷ 100 mm	Wiatr v 10 ÷ 15 m/s	v > 15 m/s	=	≥ 1 mm	◔	●	▥
I	3.5	3.4	8	3.6	9	2.6	4.5	1.7	2.5	2.0	1.7	3.8	3.9.5	3.8	9	3.7	3	3.4	16.3	4.8	5	24	10	2	·	10	7	·	·	·	·	·	18	·
II	6.5	4.3	1.5	1.7	10.5	2.7	·	·	1.3.5	2.9	3.1	2.9	4.6	2.7	4	3.3	1	2.7	54.9	16.2	18	12	·	·	·	15	12	1	·	·	·	·	9	·
III	6.5	2.6	1.4	2.9	20.5	4.1	5	3.3	9	2.8	8.5	3.2	1.7	3.4	11.5	3.6	1	3.3	27.3	8.4	29	19	1	·	·	7	6	·	1	1	·	·	8	4	·
IV	24.5	2.6	1.8	2.5	11.5	2.3	3	3.5	4.5	2.1	5	2.3	9.5	1.9	6	4.0	9	2.3	24.4	17.4	22	9	·	·	·	9	3	1	·	·	·	·	5	12	·
V	3.0	2.7	13.5	2.5	4.5	2.6	5.5	1.8	5.5	1.9	9.5	2.3	3.5	3.1	1.8	4.4	3	2.8	15.3	6.4	10	2	·	·	2	3	3	·	·	·	·	·	6	·
VI	10.5	2.3	1.8	1.7	4	2.5	4.5	3.9	3	3.2	1.1	2.7	1.4	3.0	1.8	3.0	7	2.4	34.0	11.7	24	·	·	·	10	5	4	·	·	·	·	4	6	·
VII	1.3	2.3	13.5	2.7	1.4	2.6	2	4.2	3.5	2.3	2.1.5	2.6	1.1.5	2.8	10	3.3	4	2.6	175.9	28.5	14	·	·	·	15	17	1.4	8	·	·	·	3	1.1	·
VIII	6	2.5	6.5	2.3	3	3.7	4	2.0	9	3.4	3.2.5	3.3	1.4	3.2	1.2	2.5	6	2.8	75.1	1.8.5	10	·	·	·	2	1.4	1.0	3	·	·	·	·	8	·
IX	6	3.1	·	·	2.5	1.6	6.5	1.8	1.3.5	2.9	2.6	5.3	1.6.5	4.4	1.5	4.1	4	3.3	47.4	8.4	23	·	·	·	2	1.6	1.4	·	2	·	·	·	1	10	·
X	1	1.0	·	·	·	·	4.5	1.7	2.0	2.3	3.3.5	3.3	2.7	3.2	5	2.2	2	2.8	8.0	1.9	20	1	·	·	·	5	5	·	·	·	·	·	9	·
XI	3	3.0	3.5	2.7	2.2	2.8	1.6.5	2.5	1.4	2.8	7	3.3	2.0	4.8	2	2.5	2	3.2	6.6	1.8	24	1.1	1	·	·	7	3	·	1	·	·	·	1.8	·
XII	5.5	3.2	6	4.3	7	3.3	3.5	2.3	1.0.5	2.3	3.0.5	2.8	1.8	3.6	1.2	3.0	·	3.1	2.0.6	2.1	8	24	8	4	·	8	7	·	1	·	·	·	1.7	·
Rok	1.1.6	2.5	1.0.2.5	2.2	1.0.8.5	2.6	5.6.5	2.4	1.0.8.5	2.6	2.3.3.3	3.0	2.0.6.5	3.3	1.2.1.5	3.3	4.2	2.9	5.0.2.8	2.8.5	1.4.VII	10.2	2.0	6	3.1	1.1.6	8.8	1.3	5	1	·	·	2.1	1.2.8	·

Sokółka

$H_s = 18.0\ m$ $h_w = 17\ m$

I	2	2.0	2	9.5	7.5	7.9	1.0	6.8	5	5.1	2.0.5	5.3	3.4.5	7.9	1.1.5	8.1	·	7.0	4.4.0	1.3.4	6	2.8	1.7	6	·	1.8	9	1	9	·	8	·	·	2.1	2.7
II	6	5.0	4	5.5	3.5	5.7	7.5	5.9	1.4	5.4	1.9	4.8	2.5	6.3	4	5.1	1	5.5	5.6.2	6.8	22	2.0	6	1	·	2.4	1.5	·	5	1	5	·	·	1.7	1.2
III	1.9.5	6.0	4.5	5.1	1.1.5	5.8	1.2.5	7.4	8	5.6	6.5	5.3	1.6.5	6.2	1.4	7.9	·	6.4	2.1.1	8.7	1.5	2.7	1.0	8	·	1.1	6	·	1.0	3	3	·	7	1.2	1.8
IV	1.1.5	4.4	9.5	4.1	1.4	3.4	5.5	4.7	3.5	5.7	1.1.5	5.1	1.0	4.4	2.4.5	5.0	·	4.6	3.3.3	9.4	2.8	8	·	·	·	1.3	9	·	3	1	·	4	4	6	1
V	2.2.5	4.7	9.5	4.7	1.3	3.8	6	5.5	6	3.8	5	4.9	6.5	7.8	2.4.5	4.7	·	4.8	3.1.7	6.8	6	2	·	·	1	1.2	8	·	4	2	1	2	3	8	·
VI	1.6	4.2	6	2.4	6	2.7	6.5	5.9	3.5	5.3	5	5.7	1.7.5	5.0	2.9.5	5.5	·	4.8	3.4.5	8.7	9	·	·	·	1.0	1.2	8	·	4	1	1	4	5	6	·
VII	1.0	2.7	8.5	3.4	4.0	5.1	8	4.2	6.5	4.0	1.1	3.4	2.2.5	5.4	1.6.5	4.2	·	4.2	1.1.4.9	2.8.5	2.2	·	·	·	1.1	2.0	1.4	3	2	1	2	9	1	6	·
VIII	4	2.9	4	3.0	5.5	2.7	9.5	3.9	4.5	3.8	1.4	5.7	2.9.5	4.2	2.2	3.8	·	4.1	1.5.5.5	3.1.3	1.4	·	·	·	1	1.7	1.5	5	3	1	3	5	1	9	·
IX	2	2.5	·	·	3	2.7	6.5	3.2	1.3.5	3.4	1.6	6.8	3.1.5	7.4	1.6.5	4.0	1	5.4	1.5.2.0	3.8.5	2.3	·	·	·	1	2.0	1.4	5	7	3	3	3	1	1.6	·
X	1	2.5	1	2.0	·	·	6.5	4.3	8.5	4.1	3.9	4.6	3.1.5	5.1	4.5	2.3	1	4.5	2.1.4	5.4	2.3	2	·	·	·	1.2	9	·	1	·	7	·	2	1.0	·
XI	9	2.1	5.5	5.5	1.2.5	4.4	1.3.5	7.0	7	4.0	7	3.7	2.4	5.5	1.1.5	3.1	·	5.4	3.6.6	1.7.6	2.8	1.5	1.1	2	·	1.3	6	1	5	2	7	·	2	2.0	3
XII	8	5.6	6.5	2.5	9.5	4.6	7.5	2.7	4.0	4.8	2.7.5	7.2	1.7.5	8.1	6.5	3.2	·	5.7	4.6.1	1.0.5	3.0	3.0	1.7	7	·	1.4	9	2	8	2	8	·	6	1.7	1.2
Rok	1.1.1.5	4.3	6.1	4.0	9.6	4.1	9.9.5	5.1	9.0	4.6	1.8.2	5.2	2.6.6.5	6.1	1.8.5.5	4.7	3	5.2	7.4.4.9	3.3.5	2.3.IX	1.3.2	5.1	2.4	2.4	1.8.6	1.2.2	1.7	6.1	1.7	4.8	2.7	3.2	1.4.8	7.3

Myszyniec – Zawadzie

$H_s = 12.2\ m$ $h_w = 12\ m$

I	·	·	4	3.0	3	2.3	4	1.5	4.5	4.6	2.6.5	3.5	2.0	2.8	6	3.5	2.5	2.3	3.9.3	7.2	6	2.5	1.1	7	·	1.3	1.0	·	2	·	4	·	·	1.6	2.4
II	0.5	1.0	·	·	·	·	6	4.7	6	2.7	2.2.5	2.2	1.1	3.4	5	3.0	3.3	4.7	5.5.3	6.7	1.9	1.2	1	·	·	2.0	1.6	·	·	·	4	·	1	1.3	5
III	4.5	3.7	·	·	2	7.0	1.1.5	4.1	4.5	1.9	6.5	2.8	1.1.5	4.5	1.1.5	2.7	4.1	2.0	2.5.7	1.4.0	1.5	2.4	·	2	·	7	6	1	1	1	1	·	1.0	5	8
IV	1.3.5	2.1	1	1.0	1	1.0	7	2.7	4	5.0	1.0	3.3	7	1.9	6.5	4.2	4.0	4.6	2.0.1	8.3	3.0	1.2	·	·	2	9	8	·	1	·	·	2	6	4	1
V	2.0	1.2	2	1.0	4	1.0	4.5	1.4	3.5	3.3	2.5	7.4	6	5.0	1.0.5	2.5	4.0	1.3	2.0.5	8.0	7	4	·	·	1	9	7	·	2	·	·	·	1.1	6	·
VI	1.1.5	1.7	2	1.5	3	1.3	5	2.2	3	8.7	8	4.6	1.1	3.5	1.1.5	2.5	3.5	1.8	6.7.7	1.7.6	5	·	·	·	1	7	4.0	8	3	1	·	·	2	1.1	4	·
VII	7.5	1.7	3.5	2.6	6	1.7	5	2.6	7.5	3.1	1.0.5	2.8	1.7.5	3.8	6.5	3.0	2.9	1.8	9.7.4	2.6.0	1.6	·	·	·	1	7	1.7	1.4	1	·	·	1	7	5	4	·
VIII	·	·	1	1.0	0.5	1.0	3.5	1.5	4	4.0	1.6.5	4.9	1.9	2.5	9.5	1.8	3.9	1.8	1.7.6.5	5.1.7	1.7	·	·	·	1	1.9	1.3	5	1	·	3	2	4	7	·
IX	2	1.0	1	1.0	1	1.0	1	1.0	1.4.5	4.7	1.8.5	5.2	2.2	5.2	6	6.3	2.4	3.6	1.1.0.4	3.5.5	2.3	·	·	·	1	1.7	1.2	2	3	1	1	·	2	9	·
X	·	·	·	·	·	·	3	2.3	1.3.5	4.2	2.6	3.4	1.0	3.9	2.5	1.0	3.8	2.1	1.2.0	3.1	1	1	·	·	·	1.0	4	·	·	·	5	·	8	7	·
XI	6.5	8.2	4.5	1.9	4.5	2.3	4.1	2.3	5	2.2	7.5	4.1	1.0.5	4.3	0.5	9.0	4.3	2.0	2.3.8	6.4	2.8	9	1	1	·	1.2	8	·	1	1	2	·	3	1.9	·
XII	6	2.5	4.5	3.0	2.5	4.0	4.5	2.3	4.0	3.1	3.2	4.9	6	5.2	2.5	1.0.0	2.8	3.0	2.9.7	1.0.5	8	2.5	1.2	5	·	1.0	7	1	2	1	7	·	6	1.7	1
Rok	7.2	1.9	2.3.5	1.3	2.4.5	1.6	6.3	2.4	8.0	3.8	1.8.7	4.1	1.5.1.5	3.7	7.8.5	4.1	4.1.5	2.1	6.7.8.4	5.1.7	1.7.VIII	1.1.2	3.1	1.5	1.9	1.5.3	1.1.3	1.3	1.4	4	2.8	1.3	6.7	1.1.4	3.9

Nidzica

$H_s = 17.0\ m$ $h_w = 11\ m$

I	·	·	5	3.8	3	3.3	7.5	4.1	5	4.8	3.9.5	6.0	6.5	5.5	1.3.5	5.2	1.3	4.6	2.9.8	9.4	5	2.6	1.0	7	·	1.5	1.0	·	5	·	·	·	·	1.9	·
II	3	3.3	2	1.5	2	2.5	2.5	5.2	1.6.5	4.8	2.7.5	4.5	1.2.5	4.8	5	4.6	1.3	3.8	6.0.7	1.1.0	1	2.1	1	·	·	1.7	1.3	1	1	·	·	·	·	1.5	·
III	6	4.0	1	3.0	5	3.8	1.8	8.4	7.5	6.4	9	4.6	1.0	6.4	1.3.5	7.0	2.5	4.8	4.7.5	1.1.3	1.5	2.5	5	1	·	7	4	1	1.2	2	–	·	4	5	·
IV	1.5.5	4.6	4	1.5	5	3.6	2.5	3.6	3.5	4.1	1.2	4.4	5.5	2.5	2.4	3.9	4.8	3.1	2.9.2	1.4.8	3.0	4.4	·	1	·	1.3	8	1	2	1	–	4	4	6	·
V	1.9.5	3.8	4.5	3.6	·	·	4.0	4.2	5	3.0	1.0.5	4.7	5	6.1	2.4.5	3.8	4.4	3.4	3.1.7	7.8	8	5	·	·	1	1.1	1.0	·	3	·	–	1	4	9	·
VI	1.3	3.3	3.5	2.7	1	1.0	6.5	3.8	3.5	4.4	1.1	5.4	1.1.5	4.0	2.4	4.0	1.6	3.3	6.1.6	2.1.4	1.0	·	·	·	4	9	9	2	6	·	–	4	4	5	·
VII	8.5	2.1	7	2.8	6	3.9	5	5.0	3.5	4.1	2.3.5	4.0	4	4.0	2.0.5	4.2	1.5	3.2	1.2.0.6	3.8.6	1.2	·	·	·	9	1.4	1.0	4	3	2	–	8	–	–	·
VIII	2	3.5	3	3.0	7	2.4	4	3.0	4	4.0	3.6	4.5	1.0	3.6	1.9	3.0	7	3.4	1.2.3.2	3.7.7	1.7	·	·	·	1	1.4	1.4	5	2	1	–	3	–	–	·
IX	4	4.5	1	3.0	·	·	2	2.8	6	4.5	2.7	5.8	1.3	5.5	2.2	6.2	1.5	4.6	1.5.6.0	3.4.9	2.3	·	·	·	1	2.0	1.7	5	7	4	–	1	–	–	·
X	·	·	·	·	·	·	·	·	1.1.5	4.6	4.5	5.1	1.3	5.1	1.2.5	3.3	1.1	4.2	1.1.4	1.8	2.0	3	·	·	·	1.1	8	·	2	·	–	·	–	–	·
XI	6	6.2	1	4.0	3.5	2.3	1.5.5	5.2	8.5	3.3	1.3	3.9	1.0.5	5.9	1.4	5.0	1.6	3.9	2.1.5	6.4	2.8	1.3	1	2	·	9	5	·	7	·	–	·	–	–	·
XII	5.5	5.1	·	·	2	4.5	5	2.6	5	3.2	3.5.5	5.3	4.1.5	5.5	1.1.5	4.1	1.7	3.9	4.4.2	1.3.8	8	2.9	1.1	5	·	1.4	1.2	1	6	1	–	·	4	2.0	·
Rok	8.3	3.5	3.3	2.4	3.6.5	2.3	7.8.5	4.0	7.9.5	4.3	2.8.9.5	4.8	1.1.3	4.9	2.0.4	4.5	1.7.8	3.8	7.0.7.4	3.8.6	1.2.VIII	1.3.6	2.8	1.6	1.6	1.5.4	1.2.0	2.0	5.6	1.1	–	2.1	–	–	·

Kluczewo

$\varphi = 53°18'$ $\lambda = 15°01'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	1.7	0.3	0.6	2.5	-2.4	10.3	6	-14.0	15	–	–	–	–	–	–	–	–	9.7	8.1	7.9	8.6
II	–	–	–	–	1.9	5.2	2.6	3.1	6.0	-0.6	9.6	2	-5.5	26	–	–	–	–	–	–	–	–	8.8	7.6	6.2	7.5
III	–	–	–	–	4.5	7.9	3.2	3.9	9.2	-1.0	16.9	13	-5.8	17	–	–	–	–	–	–	–	–	5.6	5.4	4.0	5.0
IV	–	–	–	–	4.3	11.0	5.4	6.5	12.5	0.7	22.8	28	-4.6	8	–	–	–	–	–	–	–	–	7.0	6.5	2.8	5.4
V	–	–	–	–	9.0	14.8	9.2	10.6	16.5	3.7	26.6	16	-2.7	9	–	–	–	–	–	–	–	–	5.6	7.1	4.3	5.6
VI	–	–	–	–	15.2	21.8	16.4	17.4	–	9.2	–	–	5.0	24	77	54	71	67	4.3	13.4	5.8	7.8	5.1	5.9	4.6	5.2
VII	–	–	–	–	17.5	22.1	17.8	18.8	–	12.4	–	–	8.1	29	86	67	82	78	2.9	9.8	4.1	5.6	6.0	6.0	6.2	6.1
VIII	–	–	–	–	14.7	19.7	14.7	16.0	–	10.6	–	–	5.0	23	89	65	88	81	1.9	8.7	2.2	4.3	6.4	7.7	4.8	6.3
IX	–	–	–	–	10.3	15.0	10.4	11.5	–	6.7	–	–	-0.3	26	91	71	91	84	1.2	5.4	1.1	2.6	7.7	7.6	4.5	6.6
X	–	–	–	–	7.7	12.6	8.9	9.5	–	5.0	–	–	-2.3	2	92	79	90	87	0.9	3.2	1.2	1.8	8.5	7.1	5.9	7.2
XI	–	–	–	–	3.5	6.4	4.2	4.6	–	1.6	–	–	-5.8	21	88	81	89	86	0.9	2.0	0.9	1.3	9.2	8.1	7.3	8.2
XII	–	–	–	–	-0.4	1.3	-0.1	0.2	–	-2.8	–	–	-13.6	11	91	88	90	90	0.5	0.7	0.6	0.6	9.7	8.1	7.0	8.3
Rok	–	–	–	–	7.1	11.6	7.8	8.6	–	3.6	–	–	-13.6	11.XII	–	–	–	–	–	–	–	–	7.4	7.1	5.5	6.7

Wałcz

$\varphi = 53°17'$ $\lambda = 16°28'$

I	1005.7	1018.9	985.5	1020.3	-1.2	0.5	-0.6	-0.5	4.5	-2.8	10.0	6	-14.8	16	89	84	87	87	0.6	1.0	0.8	0.8	8.9	8.5	7.3	8.2
II	995.6	1022.4	969.3	1009.8	0.9	4.3	2.4	2.5	5.6	-0.4	10.2	5	-6.5	25,26	91	79	88	86	0.6	1.8	0.9	1.1	8.1	8.0	6.4	7.5
III	1003.8	1023.9	978.2	1018.2	-0.2	6.6	2.6	2.9	8.2	-1.3	17.0	13	-7.2	3	84	63	80	76	1.0	4.1	1.6	2.2	5.3	5.6	3.2	4.7
IV	1005.1	1017.8	980.6	1019.3	3.2	11.4	6.1	6.7	12.8	1.3	22.7	28,29	-5.5	15	86	56	79	74	1.1	7.0	2.1	3.4	6.0	7.3	5.4	6.3
V	1003.1	1016.7	993.3	1017.1	8.4	14.7	9.5	10.5	16.3	4.2	26.4	19	-1.3	27	77	49	71	66	2.1	9.5	3.8	5.3	5.5	7.4	4.9	5.9
VI	1002.9	1018.5	990.4	1016.9	14.4	21.6	16.1	17.0	23.3	10.0	30.6	19	6.1	15	77	49	71	66	4.0	14.4	5.8	8.1	5.6	5.9	4.7	5.4
VII	998.5	1010.5	988.0	1011.9	16.8	21.8	17.8	18.8	23.5	13.9	32.1	4	10.1	29	87	66	80	78	2.7	9.8	4.5	5.7	7.2	7.3	6.8	7.1
VIII	999.7	1010.3	986.9	1013.3	13.5	18.8	14.8	15.5	20.4	11.5	27.0	11	7.0	23	93	69	86	83	1.2	7.3	2.6	3.7	7.5	8.2	5.5	7.1
IX	997.6	1010.3	978.7	1011.5	9.2	13.9	10.0	10.8	15.4	7.3	27.3	8	0.8	27	95	76	93	88	0.7	4.2	0.9	1.9	8.0	8.1	5.1	7.1
X	1004.0	1015.5	988.1	1018.1	6.7	11.6	8.1	8.6	12.5	5.4	18.3	9	-0.6	2	94	77	90	87	0.6	3.3	1.1	1.7	8.5	8.2	5.1	7.3
XI	1008.6	1025.1	988.6	1021.0	2.9	5.6	3.8	4.0	6.6	1.9	14.4	5	-7.1	30	92	82	89	88	0.6	1.7	0.9	1.1	8.5	8.5	7.6	8.1
XII	999.8	1017.2	960.0	1014.2	-1.5	0.0	-0.7	-0.7	1.3	-2.8	8.5	8	-12.7	17	90	86	89	88	0.6	0.8	0.6	0.7	8.4	8.6	6.6	7.9
Rok	1001.9	1025.1	960.0	1015.9	6.1	10.9	7.5	8.0	12.3	4.0	32.1	4.VII	-14.8	16.1	88	70	84	81	1.4	5.4	2.1	3.0	7.3	7.6	5.7	6.9

Lidzbark

$\varphi = 53°16'$ $\lambda = 19°49'$

I	–	–	–	–	-2.3	-0.6	-1.9	-1.7	0.3	-5.1	8.4	6	-18.9	16	92	86	92	90	0.4	0.8	0.4	0.5	9.0	8.9	8.4	8.8
II	–	–	–	–	1.0	3.2	1.6	1.8	4.2	-0.9	10.7	7	-4.8	26	95	84	92	90	0.3	1.4	0.6	0.8	8.9	7.9	8.0	8.3
III	–	–	–	–	-0.5	4.5	1.6	1.8	6.0	-3.0	17.1	31	-8.2	9	82	61	81	75	1.1	3.8	1.4	2.1	5.5	5.5	5.4	5.5
IV	–	–	–	–	4.6	11.2	5.8	6.8	12.4	0.2	24.9	27	-7.8	10	84	51	78	71	1.4	7.7	2.2	3.8	6.1	6.2	6.4	6.2
V	–	–	–	–	8.4	12.7	9.2	9.9	14.6	4.0	25.6	19	-1.8	6	80	57	79	72	2.4	7.0	2.8	4.1	6.0	7.1	6.0	6.4
VI	–	–	–	–	14.0	19.2	15.1	15.8	21.4	9.3	27.5	11	5.1	21	78	58	77	71	3.6	10.3	4.3	6.1	5.2	5.3	4.2	4.9
VII	–	–	–	–	16.4	21.2	17.5	18.0	23.0	12.6	30.4	2,8	8.1	26,29	86	68	86	80	2.7	9.0	2.8	4.8	6.4	6.6	5.6	6.2
VIII	–	–	–	–	13.5	18.8	14.9	15.5	20.3	10.4	26.3	12	5.4	30	91	65	88	81	1.4	7.7	2.2	3.8	6.6	7.1	5.6	6.4
IX	–	–	–	–	9.0	13.7	10.7	11.0	15.1	6.4	26.3	9	-0.6	26	93	71	87	84	0.8	5.1	1.8	2.6	8.0	7.1	7.0	7.4
X	–	–	–	–	6.3	11.0	7.7	8.2	12.0	4.0	19.4	19	-0.9	2	92	77	89	86	0.7	3.2	1.2	1.7	7.4	7.5	6.1	7.0
XI	–	–	–	–	3.4	5.2	3.8	4.0	6.4	1.0	14.3	6	-9.6	30	91	80	89	87	0.7	1.7	0.9	1.1	8.8	8.0	7.9	8.2
XII	–	–	–	–	-2.4	-0.5	-2.0	-1.7	0.5	-5.2	5.9	8,9	-16.2	18	90	86	88	88	0.4	0.8	0.5	0.6	7.5	7.8	7.0	7.4
Rok	–	–	–	–	6.0	10.0	7.0	7.5	11.3	2.8	30.4	2,8.VII	-18.9	16.1	88	70	86	81	1.3	4.9	1.8	2.7	7.1	7.1	6.5	6.9

Kisielnica

$\varphi = 53°15'$ $\lambda = 22°07'$

I	–	–	–	–	-3.0	-1.1	-2.0	-2.0	-0.1	-5.1	6.0	9	-17.3	16	95	91	94	93	0.2	0.5	0.3	0.3	8.8	7.7	6.8	7.8
II	–	–	–	–	0.2	2.2	1.1	1.2	3.3	-1.0	7.5	14	-8.3	28	96	92	94	94	0.2	0.6	0.4	0.4	8.7	8.0	7.0	7.9
III	–	–	–	–	-2.1	3.3	-0.3	0.2	4.9	-4.5	16.5	31	-15.8	17	89	68	88	82	0.6	3.1	0.8	1.5	4.8	4.9	4.0	4.6
IV	–	–	–	–	4.9	12.2	6.8	7.7	13.5	1.6	25.9	27	-7.4	10	90	55	82	76	1.0	7.9	2.1	3.7	4.5	5.0	5.2	4.9
V	–	–	–	–	9.1	13.8	9.0	10.2	15.5	4.7	26.9	17,19	-3.5	6	83	59	84	75	2.0	7.5	2.0	3.8	4.8	6.9	4.6	5.4
VI	–	–	–	–	14.8	20.1	14.9	16.2	21.9	9.7	28.9	19	4.7	21	79	57	80	72	3.6	11.1	3.5	6.1	5.4	5.3	3.8	4.8
VII	–	–	–	–	16.5	21.2	16.7	17.8	23.1	12.8	28.0	8	8.1	7	88	67	88	81	2.2	9.3	2.3	4.6	5.9	6.9	5.6	6.1
VIII	–	–	–	–	13.7	18.8	14.5	15.4	20.3	10.9	28.4	12	4.3	24	94	70	90	85	1.0	7.2	1.6	3.3	6.2	7.4	4.9	6.2
IX	–	–	–	–	9.3	13.9	10.0	10.8	15.1	7.0	26.9	9	0.1	27	94	73	91	86	0.7	5.0	1.2	2.3	7.3	7.7	4.5	6.5
X	–	–	–	–	5.3	10.7	7.4	7.7	11.8	3.6	18.5	19	-0.5	16	97	78	91	89	0.3	3.1	1.0	1.5	6.7	6.6	4.6	6.0
XI	–	–	–	–	3.0	4.9	3.6	3.8	6.1	1.5	14.5	6	-9.4	30	96	88	93	92	0.3	1.1	0.5	0.6	8.2	8.4	8.0	8.2
XII	–	–	–	–	-3.1	-1.1	-2.4	-2.2	0.1	-5.2	5.0	14	-13.5	18	92	87	91	90	0.4	0.7	0.4	0.5	7.3	7.4	6.2	7.0
Rok	–	–	–	–	2.7	9.9	6.5	7.2	11.3	3.0	28.9	19.VI	-17.3	16.1	91	73	89	84	1.0	4.8	1.3	2.4	6.6	6.8	5.4	6.3

Kluczewo

$H_s = 30\ m$ $h_w = 11\ m$ 1957

| MIESIĄC | ROZKŁAD WIATRU (nD • mD) | | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | | |

Kończewice

$\varphi = 53°11'$ $\lambda = 18°33'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max obs.	Data	Min obs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.9	-0.2	-1.0	-1.0	1.0	-3.8	9.4	6	-17.3	15	93	90	94	92	0.3	0.6	0.4	0.4	9.1	8.6	8.6	8.8
II	–	–	–	–	1.2	3.9	2.5	2.5	4.9	0.1	9.6	14	-4.0	24	97	85	92	91	0.2	1.3	0.6	0.7	9.0	7.5	7.9	8.1
III	–	–	–	–	0.3	5.4	2.6	2.7	6.8	-1.1	15.6	31	-5.9	9	–	–	–	–	–	–	–	–	4.9	5.2	4.0	4.7
IV	–	–	–	–	4.1	10.5	6.2	6.8	12.1	1.4	23.9	28	-5.8	14	90	63	88	78	0.9	5.3	2.0	2.9	4.6	5.7	5.4	5.2
V	–	–	–	–	8.6	13.8	9.2	10.2	15.3	4.9	24.8	19	-0.9	6	81	55	79	72	2.3	7.8	2.7	4.3	5.2	6.0	4.4	5.1
VI	–	–	–	–	13.2	19.9	16.3	16.4	22.4	9.2	29.4	11	4.9	5	84	57	73	71	2.5	10.7	5.6	6.3	4.5	4.0	3.4	4.0
VII	–	–	–	–	16.0	21.5	18.2	18.5	23.6	13.5	31.4	8	8.4	3	90	64	82	79	2.0	10.3	4.3	5.5	6.6	5.8	5.5	6.0
VIII	–	–	–	–	13.9	19.6	14.7	15.7	21.1	11.3	26.0	11	7.0	23	91	63	89	81	1.4	8.8	2.0	4.1	6.2	6.4	5.7	6.1
IX	–	–	–	–	9.4	14.2	10.9	11.4	15.7	7.3	26.8	8,9	-0.1	27	92	72	86	83	0.9	5.3	2.0	2.7	6.9	7.5	6.0	6.8
X	–	–	–	–	5.2	11.5	8.3	8.6	12.6	4.9	19.0	10,19	-0.7	2	96	76	90	87	0.4	3.4	1.2	1.7	7.1	7.6	6.2	7.0
XI	–	–	–	–	3.6	6.2	4.2	4.6	–	–	–	–	–	–	92	79	83	86	0.6	2.1	1.0	1.2	8.3	7.6	6.5	7.5
XII	–	–	–	–	-2.5	-0.5	-1.5	-1.5	0.8	-4.0	7.7	9	-13.2	18	–	–	–	–	–	–	–	–	6.7	8.0	6.6	7.1
Rok	–	–	–	–	6.0	10.5	7.6	7.9	–	–	31.4	8.VII	–	–	–	–	–	–	–	–	–	–	6.6	6.7	5.8	6.4

Chrząstowo

$\varphi = 53°10'$ $\lambda = 17°35'$

I	–	–	–	–	-1.6	0.0	-0.9	-0.8	–	-3.9	–		-18.4	16	–	–	–	–	–	–	–	–	9.3	9.0	8.5	8.9
II	–	–	–	–	1.2	4.2	2.6	2.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	9.1	8.8
III	–	–	–	–	0.3	5.8	2.5	2.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.6	3.8	4.9
IV	–	–	–	–	4.2	11.2	6.6	7.1	–	–	–	–	–	–	88	60	80	76	1.1	6.3	2.1	3.2	5.6	6.9	6.1	6.2
V	–	–	–	–	8.5	14.2	9.4	10.4	–	–	–	–	–	–	82	56	77	72	2.3	8.1	2.9	4.4	6.1	6.9	5.8	6.3
VI	–	–	–	–	14.5	20.8	15.5	16.6	–	9.6	–	–	4.0	15	78	53	74	68	3.8	12.7	4.7	7.1	5.7	6.1	5.6	5.8
VII	–	–	–	–	16.7	21.5	17.1	18.1	–	13.3	–	–	9.5	29	86	66	84	79	2.7	9.9	3.4	5.3	7.5	7.4	7.0	7.3
VIII	–	–	–	–	13.6	19.2	14.9	15.9	–	10.9	–	–	6.5	23	91	65	84	80	1.4	8.2	2.2	4.1	7.4	7.8	5.6	6.9
IX	–	–	–	–	9.1	14.0	10.6	11.1	–	6.9	–	–	0.0	27	93	72	86	84	0.8	5.1	1.9	2.6	7.7	8.1	6.9	7.6
X	–	–	–	–	6.3	11.9	8.2	8.6	–	4.6	–	–	-0.5	2	93	76	90	86	0.7	3.4	1.1	1.7	8.8	8.1	6.5	7.8
XI	–	–	–	–	3.1	5.9	3.9	4.2	–	1.6	–	–	-0.6	30	92	82	88	87	0.6	1.8	0.9	1.1	9.0	8.5	7.9	8.5
XII	–	–	–	–	-1.6	-0.3	-1.1	-1.0	–	-3.8	–	–	-14.4	16	90	90	90	90	0.5	0.6	0.5	0.5	8.3	8.5	6.7	7.8
Rok	–	–	–	–	6.2	10.7	7.4	7.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.6	6.5	7.2

Minikowo

$\varphi = 53°10'$ $\lambda = 17°45'$

I	–	–	–	–	-1.3	-0.1	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.2	7.8	8.4
II	–	–	–	–	0.8	4.2	2.3	2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	9.1	8.3
III	–	–	–	–	-0.1	5.9	2.3	2.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.5	3.5	5.1
IV	–	–	–	–	3.8	11.1	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.5	5.9	6.0
V	–	–	–	–	8.5	14.3	9.1	10.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.0	6.9	6.7
VI	–	–	–	–	14.7	20.9	15.3	16.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.2	5.1	5.2
VII	–	–	–	–	16.5	21.7	17.1	18.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	7.6	7.3
VIII	–	–	–	–	13.5	19.2	14.7	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.2	5.8	6.5
IX	–	–	–	–	8.9	13.9	10.5	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.1	6.0	7.0
X	–	–	–	–	6.0	11.6	8.0	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	5.5	7.0
XI	–	–	–	–	3.1	5.9	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.4	7.7	8.3
XII	–	–	–	–	-1.8	-0.3	-1.1	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.6	7.0	7.9
Rok	–	–	–	–	6.0	10.7	7.3	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	6.5	7.0

Wyrzysk

$\varphi = 53°09'$ $\lambda = 17°16'$

I	–	–	–	–	-1.6	0.4	-0.5	-0.6	1.4	-3.3	9.6	6	-17.1	16	85	82	85	84	0.7	1.1	0.8	0.9	8.4	7.5	7.7	7.9
II	–	–	–	–	1.1	4.6	2.8	2.8	5.3	-0.2	9.8	5	-6.0	27	92	79	86	86	0.5	1.8	1.0	1.1	6.7	5.8	7.3	6.6
III	–	–	–	–	0.3	6.3	2.9	3.1	7.8	-1.1	16.4	13	-6.6	11	87	72	85	81	0.8	3.1	1.2	1.7	4.5	4.5	4.4	4.5
IV	–	–	–	–	4.5	11.7	6.7	7.4	13.0	1.5	23.7	29	-5.2	13	–	–	–	–	–	–	–	–	4.7	4.5	3.4	4.2
V	–	–	–	–	9.2	14.5	9.7	10.8	15.9	4.4	25.1	19	-1.9	6	–	–	–	–	–	–	–	–	4.7	4.4	3.8	4.3
VI	–	–	–	–	15.2	21.5	15.6	17.0	23.0	9.6	29.7	11	5.1	15	78	54	79	70	4.0	13.0	3.9	7.0	3.9	4.4	3.5	3.9
VII	–	–	–	–	17.0	22.3	17.4	18.5	23.8	13.7	33.0	4	9.1	7	88	69	86	81	2.6	9.5	3.1	5.1	6.4	5.7	5.8	6.0
VIII	–	–	–	–	14.0	19.5	15.0	15.9	20.9	11.2	25.9	11	5.1	29	91	72	89	84	1.5	6.7	2.0	3.4	5.7	6.1	4.7	5.5
IX	–	–	–	–	9.5	14.5	10.6	11.3	15.8	7.2	27.1	8	-1.3	27	95	75	89	86	0.6	4.7	1.5	2.3	6.0	6.2	4.7	5.6
X	–	–	–	–	7.1	12.0	8.2	8.9	12.7	5.0	19.0	19	-1.4	2	95	80	94	90	0.5	3.0	0.7	1.4	7.0	6.5	6.1	6.5
XI	–	–	–	–	3.3	6.0	3.9	4.3	7.0	1.4	15.4	5	-7.0	21	92	84	91	89	0.6	1.6	0.7	1.0	8.6	8.0	7.3	8.0
XII	–	–	–	–	-1.6	0.0	-1.3	-1.0	1.2	-3.6	8.3	8	-14.1	16	88	86	88	87	0.6	0.8	0.6	0.7	8.0	8.1	7.4	7.8
Rok	–	–	–	–	6.5	11.1	7.6	8.2	12.3	3.8	33.0	4.VII	-17.1	16.1	–	–	–	–	–	–	–	–	6.2	6.0	5.5	5.9

Kończewice — $H_s = 94$ m — $h_w = 10$ m — 1957

| MIESIĄC | ROZKŁAD WIATRU (%D, %nD) | | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | | |

Grądy - Waniecko

$\varphi = 53°09'$ $\lambda = 22°24'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max obs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.0	-0.7	-4.3	-4.4	0.3	-4.8	5.9	9	-18.5	16	94	88	91	91	0.3	0.7	0.5	0.5	9.5	8.5	8.6	8.9
II	–	–	–	–	0.7	2.8	4.4	4.6	3.7	-0.7	8.4	14	-6.4	28	93	86	90	90	0.4	1.2	0.7	0.8	9.3	8.8	8.3	8.8
III	–	–	–	–	-1.5	3.6	0.0	0.5	5.2	-4.0	16.2	31	-13.9	17	85	63	82	77	0.9	3.5	1.3	1.9	6.7	6.6	6.4	6.6
IV	–	–	–	–	5.2	12.3	8.7	7.7	13.6	1.4	25.5	30	-7.6	10	86	54	80	72	1.4	8.5	2.2	4.0	6.8	6.6	7.1	6.8
V	–	–	–	–	9.2	14.3	9.6	10.7	15.6	4.3	26.1	19	-3.8	6	82	57	80	73	2.2	7.9	2.5	4.2	6.4	7.4	7.1	7.0
VI	–	–	–	–	15.2	20.8	14.6	16.5	22.2	8.2	29.4	11	1.5	21	77	54	82	71	4.0	11.9	3.1	6.3	6.5	6.4	6.2	6.4
VII	–	–	–	–	17.1	22.1	18.3	18.0	23.5	14.7	28.5	5	5.6	7	83	59	86	76	3.5	11.5	2.7	5.9	6.7	6.5	6.9	6.7
VIII	–	–	–	–	14.0	19.5	14.2	15.5	20.7	9.9	29.3	12	3.1	24	90	65	89	81	1.7	8.6	1.9	4.1	5.3	4.4	5.3	5.0
IX	–	–	–	–	9.4	14.5	10.1	11.0	15.4	6.8	27.2	9	0.0	27	89	67	87	81	1.4	6.1	1.6	3.0	–	–	–	–
X	–	–	–	–	5.4	11.2	7.8	8.0	12.0	3.8	18.7	19	-0.6	16	92	72	86	83	0.8	3.9	1.5	2.1	6.2	5.0	5.1	5.4
XI	–	–	–	–	3.1	5.2	3.8	4.0	6.4	1.5	15.2	6	-9.5	29	92	82	87	87	0.8	1.6	1.0	1.1	8.4	7.7	7.8	8.0
XII	–	–	–	–	-2.6	-0.7	-2.2	-1.9	0.2	-5.0	5.7	14	-13.5	16	88[3]	85[2]	88[1]	87[5]	0.6[2]	0.9[2]	0.6[2]	0.7[5]	7.4	7.1	7.3	7.3
Rok	–	–	–	–	6.1	10.4	6.8	7.5	11.6	2.8	29.4	11.VI	-18.5	16.1	88[3]	69[2]	86[5]	81[3]	1.5[3]	5.5[3]	1.6[5]	2.9[3]	–	–	–	–

Bydgoszcz, IMiUZ

$\varphi = 53°08'$ $\lambda = 18°01'$

I	–	–	–	–	-1.2	0.6	-0.1	-0.2	1.9	-2.5	10.2	6	-15.0	16	85	81	83	83	0.8	1.2	1.0	1.0	8.8	9.0	8.1	8.6
II	–	–	–	–	1.6	4.7	3.0	3.1	5.7	0.7	10.3	5	-4.9	24	91	75	85	84	0.7	2.2	1.2	1.4	9.0	8.3	7.2	8.2
III	–	–	–	–	0.2	6.4	3.0	3.2	8.1	-0.9	17.0	31	-6.9	11	84	56	76	72	1.1	4.6	1.9	2.5	5.1	5.1	2.9	4.4
IV	–	–	–	–	4.0	11.4	7.2	7.4	12.9	1.9	24.1	28	-5.5	13	83	53	73	70	1.4	7.4	3.0	3.9	5.2	6.8	5.0	5.7
V	–	–	–	–	8.3	14.7	10.3	10.9	16.0	4.9	25.6	19	-2.0	6	77	45	67	63	2.7	10.0	4.4	5.7	5.8	7.0	4.1	5.6
VI	–	–	–	–	14.7	21.0	17.0	17.4	23.1	10.9	30.0	11	6.9	16	76	53	70	66	4.3	13.0	6.1	7.8	5.2	5.5	3.7	4.8
VII	–	–	–	–	16.6	22.0	18.3	18.8	23.9	14.4	32.1	8	10.4	29	86	66	82	78	2.7	10.0	4.4	5.7	6.9	7.1	6.8	6.9
VIII	–	–	–	–	14.1	19.8	15.6	16.3	21.2	11.8	26.6	11	7.6	24	88	61	83	77	2.1	9.4	3.3	4.9	6.3	7.6	4.1	6.0
IX	–	–	–	–	9.2	14.6	11.0	11.4	16.0	7.4	28.1	8	0.3	27	91	68	85	81	1.0	6.2	2.1	3.1	6.6	7.8	4.3	6.2
X	–	–	–	–	6.4	12.0	8.7	9.0	13.0	4.9	20.1	19	-0.5	2	92	72	87	84	0.9	4.1	1.5	2.2	8.3	8.0	4.0	6.8
XI	–	–	–	–	3.6	6.7	4.3	4.7	7.6	2.0	16.7	5	-7.3	30	88	74	84	82	1.0	2.8	1.3	1.7	9.8	8.3	7.8	8.6
XII	–	–	–	–	-1.4	0.1	-0.9	-0.8	1.5	-3.6	8.5	8	-15.0	16	88	84	88	87	0.7	1.0	0.7	0.8	8.0	8.6	6.6	7.7
Rok	–	–	–	–	6.3	11.2	8.1	8.4	12.6	4.3	32.1	8.VII	-15.0	15.1,16.XII	86	66	80	77	1.6	6.0	2.6	3.4	7.1	7.4	5.4	6.6

Bydgoszcz

$\varphi = 53°07'$ $\lambda = 17°58'$

I	1014.2	1023.8	992.6	1020.2	-1.6	0.4	-0.5	-0.8	1.6	-3.6	10.0	6	-18.6	16	–	–	–	–	–	–	–	–	8.6	8.8	8.0	8.5
II	1001.4	1027.0	975.1	1010.2	1.2	4.7	2.6	2.8	5.8	-0.8	10.4	5	-6.9	24	–	–	–	–	–	–	–	–	8.5	8.1	8.0	8.2
III	1009.9	1028.1	984.4	1016.8	-0.2	6.3	2.4	2.7	8.0	-2.0	16.9	31	-8.7	11	–	–	–	–	–	–	–	–	5.5	5.6	3.7	4.9
IV	1010.4	1023.5	986.0	1019.2	3.9	11.4	6.5	7.1	13.0	0.8	24.0	29	-8.5	14	–	–	–	–	–	–	–	–	5.8	6.9	5.6	6.1
V	1008.2	1020.6	997.6	1016.9	8.5	14.6	9.6	10.6	16.2	3.9	26.0	19	-2.9	6	75	52	73	68	2.5	8.8	3.5	4.9	5.9	6.8	4.5	5.7
VI	1008.1	1023.3	995.2	1016.6	15.0	21.2	16.5	17.3	23.4	9.4	30.0	11	4.4	16	77	55	73	68	4.2	12.7	5.3	7.4	5.3	5.4	3.8	4.8
VII	1003.3	1015.4	992.3	1011.6	16.8	21.9	17.8	18.6	24.2	13.2	32.3	4	7.9	29	87	68	84	80	2.5	9.8	3.7	5.3	7.1	7.2	6.2	6.8
VIII	1005.0	1015.7	992.2	1013.5	14.0	19.6	15.0	15.8	21.4	10.8	26.9	11	6.1	29	89	65	86	80	1.8	8.3	2.6	4.2	6.1	7.9	5.2	6.4
IX	1003.0	1014.9	985.6	1011.6	9.1	14.3	10.4	11.0	16.0	6.2	27.8	8	-2.2	27	92	73	88	84	1.0	5.1	1.6	2.6	6.4	7.8	4.8	6.3
X	1009.7	1021.0	995.0	1018.4	6.1	11.9	8.0	8.5	13.2	4.0	20.1	19	-2.6	2	93	76	90	86	0.7	3.5	1.2	1.8	7.1	7.9	4.5	6.5
XI	1012.1	1031.6	995.1	1020.9	3.2	6.5	4.0	4.4	7.6	1.5	17.1	5	-8.5	21	–	–	–	–	–	–	–	–	8.4	8.2	7.9	8.2
XII	1005.5	1023.3	964.3	1014.5	-1.9	-0.1	-1.5	-1.2	1.2	-4.5	8.2	8	-18.0	16	–	–	–	–	–	–	–	–	7.3	8.4	6.7	7.5
Rok	1007.3	1031.6	964.3	1016.1	6.2	11.1	7.6	8.1	12.6	3.2	32.3	4.VII	-18.6	16.1	–	–	–	–	–	–	–	–	6.8	7.4	5.7	6.6

Mława

$\varphi = 53°07'$ $\lambda = 20°22'$

I	1001.4	1013.4	984.5	1020.0	-2.4	-0.9	-2.1	-1.9	0.5	-5.0	7.9	6	-18.6	16	91	89	91	90	0.4	0.6	0.5	0.5	8.8	8.7	7.0	8.2
II	992.3	1014.4	968.3	1010.5	1.0	3.1	1.5	1.8	4.2	-0.7	9.3	14	-7.2	24	94	84	90	89	0.4	1.3	0.7	0.8	9.5	8.7	7.2	8.5
III	1000.5	1016.8	974.3	1018.9	-0.9	4.8	1.5	1.7	6.6	-2.7	16.7	31	-9.5	17	82	61	79	74	1.0	4.0	1.6	2.2	5.7	5.8	4.3	5.3
IV	1000.3	1013.7	975.4	1018.2	4.5	12.3	6.4	7.4	13.8	1.4	25.5	27	-8.0	10	85	50	79	71	1.4	8.3	2.2	4.0	5.9	6.6	4.3	5.6
V	998.5	1010.0	987.7	1016.2	8.8	13.7	9.5	10.4	15.4	4.7	27.2	19	-2.2	6	82	61	83	75	2.2	7.1	2.2	3.8	5.7	7.4	4.9	6.0
VI	998.8	1012.6	985.4	1016.5	15.3	20.6	15.5	16.7	22.5	9.8	29.2	19	4.6	21	77	57	80	71	4.1	11.4	3.8	6.4	5.6	6.6	4.2	5.4
VII	994.2	1004.9	984.1	1011.3	16.7	21.9	17.5	18.4	23.6	12.9	30.1	2	7.6	7	88	66	86	80	2.5	9.8	3.0	5.1	6.8	7.0	5.4	6.4
VIII	995.9	1005.3	983.9	1013.2	13.8	19.5	14.7	15.7	20.9	10.5	27.5	12	3.5	24	92	68	89	83	1.4	7.5	1.9	3.6	6.4	8.1	4.3	6.3
IX	993.7	1004.9	975.8	1011.3	9.0	14.5	10.4	11.1	15.7	6.7	27.1	9	-1.0	27	93	71	88	84	0.8	5.4	1.6	2.6	7.1	8.0	5.1	6.7
X	1000.7	1012.7	987.4	1018.6	5.2	11.5	7.3	7.8	12.7	3.4	20.0	10	-2.0	3	95	75	91	87	0.5	3.7	0.9	1.7	6.9	8.1	3.5	6.2
XI	1002.8	1023.2	982.6	1024.2	3.3	5.3	3.7	4.0	6.8	1.5	15.0	6	-9.0	30	90	82	90	87	0.7	1.6	0.8	1.0	8.5	8.6	7.6	8.2
XII	999.9	1013.8	985.7	1014.4	-2.9	-0.7	-2.1	-2.0	0.5	-5.1	5.6	5	-15.7	16	90	86	90	89	0.4	0.8	0.4	0.6	7.0	8.0	6.4	7.1
Rok	997.9	1023.2	985.7	1015.8	6.0	10.5	7.0	7.6	11.9	3.1	30.1	2.VII	-18.6	16.1	88	74	86	82	1.3	5.1	1.6	2.7	7.0	7.6	5.4	6.7

Grądy – Waniecko

$H_s = 110$ m

1957

MIESIĄC	ROZKŁAD WIATRU nD, ∑nD																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0	Max<0	Min<-10	Max>25	≥0,1	≥1,0	≥10,0	>10	>15							
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28.1	8.1	5	25	10	7	·	11	6	·	–	–	5	·	·	21	24				
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.7	8.1	18	14	3	·	·	20	12	·	–	–	3	·	·	21	6				
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18.7	12.3	15	26	8	2	·	6	4	1	–	–	2	·	·	11	6				
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24.7	6.0	18	10	·	·	2	9	8	·	–	–	1	3	·	10	2				
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.0	5.5	10	6	·	·	1	9	6	·	–	–	1	1	1	12	·				
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48.3	10.3	22	·	·	·	8	11	10	1	–	–	·	4	2	9	·				
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	68.4	11.7	16	·	·	·	9	15	13	2	–	–	1	12	·	12	·				
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	108.3	38.0	17	·	·	·	2	13	11	4	–	–	1	3	5	5	·				
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	134.9	58.7	23	·	·	·	1	12	11	4	–	–	1	2	–	–	·				
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	16.0	4.9	1	1	·	·	·	7	6	·	–	–	2	·	5	7	·				
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	15.2	6.0	28	10	1	·	·	6	6	·	–	–	1	·	·	17	·				
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32.7	7.8	30	25	13	4	·	11	10	·	–	–	1	·	·	15	3				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	566.0	58.7	23.IX	117	35	13	23	130	103	12	–	–	19	25	–	–	41				

Bydgoszcz, IMiUZ

$H_s = 47$ m $\quad h_w = 10$ m

I	·		7	3.6	7	1.9	1	2.0	7.5	2.2	13.5	2.6	3.6	3.9	8	4.7	13	2.9	20.6	5.7	5	20	10	1	·	11	7	·	·	·	–	·	1	22	19				
II	1.5	3.7	2.5	1.6	7.5	2.1	3.5	3.0	1.4	2.6	1.5	2.7	2.0	3.4	5	4.0	15	2.4	44.8	13.1	18	11	·	·	·	16	13	1	·	·	–	·	1	17	1				
III	7	2.6	1.5	2.7	2.0	3.6	11.5	4.3	4	2.6	0.5	3.0	1.9	4.2	3.5	5.4	2.6	2.7	28.5	10.2	29	18	·	·	·	8	5	1	3	·	–	·	11	7	·				
IV	17.5	2.5	1.2	3.1	8	2.3	1	2.0	1	3.0	1	2.0	1.5	2.6	9.5	3.5	2.5	2.0	20.2	7.4	22	8	·	·	·	14	6	·	·	·	–	2	6	11	·				
V	1.6	3.3	1.2	3.4	1.0	1.9	·	·	3.5	3.1	2	1.7	1.9.5	2.9	9	2.8	2.1	2.2	38.0	16.1	6	1	·	·	1	10	6	1	1	·	–	3	3	8	·				
VI	6.5	2.5	1.0	1.8	16.5	2.0	1.5	3.7	3	2.3	4.5	2.3	2.0	2.5	7	3.8	2.1	1.9	38.8	13.2	4	·	·	·	11	7	6	2	·	·	–	1	7	5	·				
VII	4.5	2.1	2.5	3.6	13.5	2.2	3	2.0	4	1.9	4	1.9	2.9.5	2.7	1.0	3.0	2.2	1.9	190.0	50.0	14	·	·	·	12	2.1	1.7	4	·	·	–	1.0	3	1.5	·				
VIII	0.5	1.0	2	2.2	3.5	2.0	4	2.6	9	2.5	1.8	2.1	1.7	2.4	7	2.6	3.2	1.5	55.7	14.1	1.0	·	·	·	2	12	7	3	·	·	–	·	3	7	·				
IX	1.5	3.0	·	·	2	1.5	1	1.0	4	3.1	1.4	4.2	3.5	3.3	10.5	3.6	2.2	2.6	55.6	23.3	2.3	·	·	·	2	18	1.5	1	·	·	–	1	1	7	·				
X	·	·	·	·	2.5	1.6	4	1.8	4	2.8	9.5	2.2	4.5	2.6	6	3.0	2.2	1.9	7.8	1.4	1.2	1	·	·	·	9	5	·	·	·	–	·	2	10	·				
XI	4	3.8	7	3.0	20.5	2.5	6	2.7	8.5	2.6	5	2.3	16.5	4.5	3.5	4.9	1.9	2.5	6.9	2.4	2.8	11	1	·	·	8	2	·	·	·	–	·	·	20	1				
XII	4.5	3.3	4.5	4.3	8.5	2.0	1	1.0	5	2.9	2.3	3.1	21.5	3.8	6	3.2	2.2	2.5	35.0	12.3	8	22	9	4	·	16	6	1	1	1	–	·	3	21	14				
Rok	60.5	2.3	6.1	2.4	119.5	2.1	37.5	2.2	67.5	2.6	11.0	2.5	29.4	3.2	8.5	3.7	26.0	2.2	541.9	50.0	14.VII	92	20	5	28	150	95	14	5	1	–	17	41	150	35				

Bydgoszcz

$H_s = 70$ m $\quad H_b = 70{,}5$ m $\quad h_w = 10$ m

I	0.5	3.0	6.5	4.7	6.5	3.3	3	2.8	6.5	3.8	26.5	4.0	2.8	5.0	7.5	4.7	8	4.0	24.4	9.4	5	26	11	2	·	12	6	·	·	·	9	·	1	22	20				
II	2	2.0	4	1.8	6.5	2.5	6	3.1	11	4.7	1.8	4.7	2.0	4.2	6.5	3.7	10	3.5	46.7	14.1	18	17	·	·	·	16	12	1	·	·	6	·	·	16	1				
III	7	3.6	6.5	2.8	18.5	4.8	9.5	6.3	5.5	5.7	7.5	3.3	14.5	5.6	10	3.2	14	3.9	32.4	10.6	29	20	·	·	·	9	7	1	2	·	2	·	9	8	1				
IV	22.5	3.5	14.5	3.5	11.5	3.8	0.5	2.0	3.5	2.6	8	3.8	8.5	3.6	9	4.2	12	3.1	23.1	7.0	22	11	·	·	·	6	6	·	1	·	3	1	5	12	1				
V	18	3.4	20.5	4.0	6	3.1	3.5	4.1	5	2.5	6	4.2	10.5	4.2	16.5	3.5	7	3.4	52.6	20.4	6	5	·	·	1	8	6	2	·	·	·	2	2	7	·				
VI	6.5	3.6	12.5	3.0	8	2.8	4.5	3.6	5	3.7	8	3.8	18	3.2	17.5	3.5	10	3.0	45.8	13.6	24	·	·	·	12	6	5	2	·	·	1	2	7	3	·				
VII	7.5	3.1	5	3.4	6	3.5	5	2.3	4	4.4	14.5	3.7	20.5	3.5	17.5	3.8	13	3.0	184.5	32.7	16	·	·	·	13	22	18	6	·	·	1	9	4	16	·				
VIII	4	2.5	5.5	1.9	4	2.0	4	4.9	5	4.6	2.3	4.0	2.8	3.2	10.5	3.4	9	3.1	54.1	22.2	10	·	·	·	3	9	8	1	·	·	3	4	1	9	·				
IX	2	2.2	·	·	1	1.0	1	2.0	1.0	4.1	24.5	4.3	22.5	4.0	1.5	3.3	1.4	3.2	60.8	17.9	23	2	·	·	2	19	16	1	·	·	4	1	·	7	·				
X	0.5	2.0	·	·	·	·	4.5	3.6	1.1	3.8	21.5	3.7	32.5	3.7	1.2	3.4	1.1	3.2	8.1	1.8	5	2	·	·	·	10	4	·	·	·	7	·	2	10	·				
XI	2	3.2	6	5.0	1.0	3.7	16.5	2.5	1.7	3.7	9	3.3	11.5	5.0	1.1	5.7	7	3.7	9.9	2.2	24,29	11	1	·	·	7	5	·	·	·	4	·	1	19	1				
XII	4.5	3.1	5	5.5	7.5	4.3	6	2.6	7	3.0	1.0	4.6	29.5	5.2	10.5	5.2	1.3	3.9	36.5	9.5	8	23	9	6	·	14	1.0	·	3	1	5	·	3	21	15				
Rok	77	2.9	8.6	3.0	85.5	2.9	6.4	3.3	90.5	3.9	17.6.5	4.0	2.4.4	4.2	14.3.5	4.0	12.8	3.4	578.9	32.7	16.VII	117	21	8	31	138	103	14	6	1	45	19	35	150	39				

Mława

$H_s = 142$ m $\quad H_b = 146{,}0$ m $\quad h_w = 10$ m

I	0.5	2.0	3.5	4.9	8.5	4.7	6	2.6	7.5	1.5	26.5	3.0	23.5	4.1	7	4.6	10	3.1	27.2	7.5	5	26	13	6	·	12	8	·	1	·	10	·	1	18	21				
II	3	2.5	4	2.9	4	1.9	12.5	2.5	15.5	2.4	21.5	2.1	13	3.3	3.5	3.1	7	2.3	56.1	11.1	18	18	1	·	·	18	11	1	·	·	7	·	1	17	5				
III	7	4.5	6	3.2	16	3.0	19	5.8	12	2.5	9	3.2	17.5	3.6	3.5	6.7	3	3.8	23.0	10.9	15	23	5	·	·	7	5	1	4	3	1	·	7	8	2				
IV	14.5	3.1	10	3.2	14.5	2.0	6	2.9	6.5	2.0	8.5	2.8	9.5	2.3	12.5	4.8	8	2.7	30.4	15.9	30	9	·	·	2	11	9	1	1	1	4	3	6	7	·				
V	21	3.9	17	3.2	8	3.1	9.5	3.0	5.5	2.0	6	3.5	7	3.4	12	4.0	7	3.2	51.1	24.4	20	3	·	·	1	8	5	1	·	·	1	1	6	10	·				
VI	12.5	2.5	9	2.0	14.5	2.0	8	2.7	1.5	3.7	10.5	2.9	15.5	2.9	13.5	2.9	8	2.4	52.1	15.5	22	·	·	·	9	11	8	1	·	·	·	5	6	8	·				
VII	7	1.9	11	1.8	12.	2.4	7.5	2.3	7.5	2.2	14	2.4	10.5	3.4	15.5	3.1	8	2.3	159.6	60.1	15	·	·	·	8	18	11	6	·	·	3	7	2	13	·				
VIII	5	2.0	2	1.5	4.5	1.6	9	2.4	7	1.7	2.0	3.3	19	2.4	11.5	2.5	15	2.1	83.0	20.0	14	·	·	·	2	15	9	4	·	·	4	1	2	8	·				
IX	1.5	1.3	·	·	·	·	9	2.7	1.6	2.2	23.5	3.7	2.3	4.2	4	4.4	13	2.9	103.8	28.4	23	1	·	·	2	21	14	2	3	·	3	2	1	10	·				
X	1	1.0	·	·	·	·	1.1	2.1	1.2	1.9	2.9	2.9	1.6	3.0	3	1.3	2.1	2.0	15.8	6.9	2.0	2	·	·	·	9	5	·	·	·	9	·	2	6	·				
XI	3.5	6.3	9	4.6	1.1	2.0	2.3	2.7	6	1.4	11.5	2.4	14.5	4.1	1.5	10.3	10	2.9	18.5	5.8	2.8	11	1	·	·	9	6	·	1	·	2	·	2	21	·				
XII	4	3.2	6.5	3.1	6	3.3	5	1.5	1.8	1.7	3.5	3.5	10.5	3.8	3	3.7	7	2.8	44.2	14.7	8	26	10	5	·	15	7	1	1	1	7	·	4	17	13				
Rok	90.5	2.8	78	2.5	96	2.2	125.5	2.6	11.5	2.1	21.3	3.0	17.9.5	3.4	90.5	4.3	11.7	2.7	664.8	60.1	15.VII	119	30	11	24	154	98	18	11	5	51	19	40	143	41				

Białystok

$\varphi = 53°07'$ $\lambda = 23°11'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1002.3	1014.1	985.6	1020.3	-2.9	-1.1	-1.8	-1.9	0.0	-4.6	6.3	6	-19.5	16	89	87	88	88	0.5	0.7	0.6	0.6	8.8	8.4	8.4	8.5
II	993.9	1014.4	970.5	1014.5	0.2	2.4	1.1	1.2	3.5	-1.0	7.7	14	-7.7	28	91	86	89	89	0.5	1.0	0.7	0.7	8.4	8.5	7.5	8.1
III	1001.7	1019.0	973.9	1019.3	-2.8	3.5	0.1	0.2	5.1	-4.7	17.2	31	-14.3	17	84	65	76	75	0.8	3.3	1.6	1.9	6.1	5.6	4.7	5.5
IV	1001.0	1014.0	975.2	1018.2	4.4	12.5	7.3	7.9	13.8	1.6	25.6	27,30	-6.1	15	88	55	77	73	1.1	8.0	2.6	3.9	5.2	6.2	5.1	5.5
V	998.7	1010.0	985.1	1015.7	9.5	14.6	10.2	11.1	16.7	5.1	27.5	19	-2.3	6	82	59	81	74	2.2	7.8	2.5	4.2	5.6	7.6	5.2	6.1
VI	999.3	1011.9	985.0	1016.0	15.1	21.5	16.0	17.2	23.1	9.6	30.5	12	5.4	24,27	77	53	76	69	4.0	12.7	4.5	7.1	5.9	6.2	4.7	5.6
VII	995.0	1005.5	984.7	1011.5	16.9	22.8	17.5	18.7	24.5	12.6	29.2	8,13,16	7.1	4	85	59	85	76	3.1	12.1	3.2	6.1	6.5	7.3	5.6	6.5
VIII	996.6	1004.5	986.7	1013.3	14.1	19.6	15.2	16.0	21.2	11.2	30.6	12	4.3	24	93	68	89	83	1.2	8.1	1.9	3.7	6.3	7.6	5.1	6.3
IX	994.2	1007.1	977.3	1014.2	9.4	14.3	10.1	11.0	15.6	7.0	27.0	9	0.7	27	94	73	92	86	0.7	5.1	1.0	2.3	7.9	8.5	6.3	7.6
X	1001.9	1014.6	990.3	1019.1	5.2	11.4	7.4	7.8	12.2	3.7	18.7	19	-2.2	16	96	75	91	87	0.4	3.6	1.0	1.7	6.6	7.1	6.4	6.7
XI	1004.0	1012.5.6	980.7	1021.7	2.8	5.3	3.8	3.9	6.4	1.0	14.5	6	-10.3	30	92	82	87	87	0.6	1.8	1.0	1.1	8.7	8.4	8.1	8.4
XII	997.0	1014.0.0	955.4	1014.8	-3.0	-0.5	-2.5	-2.1	0.3	-5.5	5.4	13	-13.7	16	89	81	86	86	0.5	1.1	0.6	0.7	7.5	7.4	6.6	7.2
Rok	998.8	1025.6	955.4	1016.0	5.7	10.5	7.0	7.6	11.9	3.0	30.6	12.VIII	-19.5	16.1	88	70	85	81	1.3	5.4	1.8	2.8	7.0	7.4	6.1	6.8

Przelewice

$\varphi = 53°06'$ $\lambda = 15°05'$

I	-	-	-	-	-0.5	1.2	0.1	0.2	2.4	-2.7	10.6	6	-12.6	1	-	-	-	-	-	-	-	-	8.8	7.1	6.2	7.4
II	-	-	-	-	1.4	4.9	2.8	3.0	5.8	0.0	10.0	2	-5.1	26	-	-	-	-	-	-	-	-	7.0	6.0	6.7	6.6
III	-	-	-	-	1.8	8.0	3.3	4.1	9.6	-0.1	16.7	13	-4.8	1,10	-	-	-	-	-	-	-	-	4.6	4.2	3.4	4.1
IV	-	-	-	-	4.3	11.2	5.4	6.6	12.6	1.7	22.8	28	-5.0	15	-	-	-	-	-	-	-	-	5.1	5.9	3.0	4.7
V	-	-	-	-	9.0	14.4	9.5	10.8	16.4	4.2	26.5	16	-1.9	6	-	-	-	-	-	-	-	-	5.4	6.7	5.7	5.9
VI	-	-	-	-	15.0	21.5	16.0	17.1	23.3	10.0	31.5	11	6.1	24	76	52	76	68	4.4	13.7	4.9	7.7	4.9	5.5	4.8	5.1
VII	-	-	-	-	16.8	22.0	17.9	18.6	23.8	13.3	34.8	4	9.8	29	88	66	82	79	2.5	10.2	4.4	5.7	6.3	6.1	6.9	6.4
VIII	-	-	-	-	14.7	19.5	14.6	15.8	20.8	11.4	26.6	11	6.3	23	88	67	87	81	2.2	8.1	2.2	4.2	6.7	7.1	4.9	6.2
IX	-	-	-	-	9.9	14.6	10.4	11.3	15.9	7.2	26.9	8	0.6	26	92	72	92	85	1.0	5.0	1.1	2.4	7.0	7.3	5.4	6.6
X	-	-	-	-	7.2	12.1	9.1	9.4	13.5	5.6	19.2	10	-0.7	2	93	77	89	86	0.8	3.3	1.2	1.8	7.6	7.7	5.5	6.9
XI	-	-	-	-	3.4	6.1	4.1	4.5	7.1	1.6	14.1	4	-5.2	21	92	81	90	88	0.6	1.9	0.8	1.1	7.6	7.8	7.7	7.7
XII	-	-	-	-	-0.5	0.8	-0.2	0.0	2.1	-2.5	9.1	8	-12.2	11	94	87	92	90	0.5	0.8	0.5	0.6	8.7	7.9	6.6	7.7
Rok	-	-	-	-	6.9	11.4	7.8	8.5	12.8	4.1	34.8	4.VII	-12.6	1.1	-	-	-	-	-	-	-	-	6.6	6.6	5.6	6.3

Ostrołęka

$\varphi = 53°05'$ $\lambda = 21°34'$

I	1007.4	1019.1	990.4	1018.5	-2.6	-0.6	-1.5	-1.6	0.5	-4.3	7.4	6	-19.1	16	90	86	88	88	0.5	0.8	0.7	0.7	8.4	8.1	7.2	7.9
II	998.5	1020.6	977.6	1010.7	0.9	3.0	1.7	1.8	4.1	-0.3	8.6	14	-6.2	28	92	84	88	88	0.5	1.3	0.8	0.9	9.3	8.6	7.1	8.3
III	1006.6	1022.8	979.5	1018.9	-1.5	4.7	1.0	1.4	6.3	-3.0	16.8	31	-11.3	17	82	57	76	72	1.0	4.2	1.7	2.3	5.6	5.6	4.6	5.2
IV	1005.9	1018.0	980.8	1016.0	4.3	12.9	7.1	8.0	14.2	2.1	26.1	27	-6.3	10	88	47	78	71	1.2	9.0	2.4	4.2	5.5	5.9	6.0	5.8
V	1003.9	1015.2	992.0	1015.9	9.1	14.2	9.3	10.5	15.7	4.6	26.8	19	-3.3	6	82	59	80	74	2.2	7.6	2.4	4.1	5.5	7.1	4.4	5.7
VI	1004.3	1017.9	994.0	1016.0	15.3	21.3	15.6	17.0	22.7	10.1	29.8	19	5.0	24	78	53	79	70	3.9	12.8	3.8	6.8	5.2	5.4	4.1	4.9
VII	999.6	1010.5	990.4	1011.1	16.9	22.6	17.4	18.6	24.1	12.8	34.1	8	7.6	4,7	86	61	83	77	2.9	11.6	3.5	6.0	6.5	7.0	5.4	6.3
VIII	1001.3	1010.3	989.8	1013.0	13.9	19.6	15.0	15.9	21.0	11.2	30.1	12	4.8	24	90	66	87	81	1.6	8.4	2.3	4.1	6.5	7.5	3.9	6.0
IX	999.2	1010.5	981.3	1014.0	9.5	14.8	10.6	11.4	15.8	7.7	27.7	9	1.1	27	91	68	87	82	1.1	6.3	1.7	3.0	7.0	7.6	6.1	6.9
X	1006.5	1018.9	994.2	1018.5	5.5	11.7	7.8	8.2	12.7	4.2	19.9	10,19	-0.5	3	93	71	88	84	0.7	4.3	1.3	2.1	6.5	6.5	4.6	5.9
XI	1008.7	1029.7	987.5	1020.8	3.3	5.7	4.2	4.4	6.8	2.1	15.5	6	-8.2	29,30	92	82	88	87	0.6	1.7	0.9	1.1	8.5	8.6	8.2	8.4
XII	1001.9	1020.1	957.4	1014.2	-2.5	-0.2	-1.7	-1.5	0.6	-4.3	5.1	13,14	-13.6	16	90	84	89	88	0.5	0.9	0.6	0.7	6.9	8.0	6.8	7.2
Rok	1003.6	1029.7	957.4	1015.7	6.1	10.8	7.2	7.8	12.0	3.6	34.1	8.VII	-19.1	16.1	88	68	84	80	1.4	5.7	1.8	3.0	6.8	7.2	5.7	6.6

Toruń – Wrzosy

$\varphi = 53°03'$ $\lambda = 18°35'$

I	1011.5	1024.3	993.2	1020.4	-1.5	0.4	-0.7	-0.6	1.4	-3.4	9.6	6	-20.2	16	88	85	87	87	0.7	1.0	0.8	0.8	9.1	8.4	7.9	8.5
II	1001.9	1026.4	975.8	1010.6	1.2	4.6	2.5	2.7	5.4	0.2	10.5	14	-7.1	24	93	79	88	87	0.5	2.0	1.0	1.2	8.9	8.1	8.0	8.3
III	1010.0	1027.9	984.1	1018.8	-0.2	6.1	2.2	2.6	7.5	-2.0	15.9	13	-9.8	11	84	56	80	73	1.0	4.8	1.6	2.5	6.1	6.4	4.6	5.7
IV	1010.3	1023.9	986.0	1019.0	4.3	11.1	6.0	6.8	12.8	1.0	24.3	28	-8.5	16	86	56	79	74	1.2	7.1	2.2	3.5	6.4	7.0	5.6	6.3
V	1008.3	1020.5	997.9	1016.9	8.8	14.6	9.4	10.6	15.9	4.3	25.9	19	-2.9	6	78	50	76	68	2.7	9.1	3.1	5.0	6.7	7.0	5.1	6.3
VI	1008.2	1023.0	995.1	1016.6	15.3	21.5	16.0	17.2	23.4	9.7	30.5	11	5.0	3	73	49	72	65	4.9	14.3	5.4	8.2	5.9	5.3	4.2	5.1
VII	1003.4	1015.1	992.7	1011.6	17.1	22.4	17.9	18.8	24.0	13.5	32.4	4	8.7	29	84	62	81	76	3.3	12.0	4.4	6.6	7.0	7.0	6.7	6.9
VIII	1005.2	1015.6	992.6	1013.6	14.2	20.1	15.2	16.2	21.3	11.1	26.6	11	6.6	23	88	61	84	78	2.0	9.6	3.0	4.9	6.2	7.0	4.1	5.8
IX	1003.3	1016.3	986.5	1011.7	9.3	14.7	10.7	11.4	16.0	6.9	27.3	8	-0.9	27	91	68	86	82	1.0	6.0	2.0	3.0	7.0	8.1	5.5	6.9
X	1010.1	1021.4	995.9	1018.7	6.1	12.2	7.9	8.5	13.0	4.0	19.8	19	-1.4	2	93	72	88	84	0.7	4.2	1.3	2.1	7.3	7.7	5.2	6.8
XI	1012.4	1032.2	995.4	1021.1	3.5	6.6	4.4	4.7	7.7	1.7	15.8	7	-9.7	21	87	74	83	81	1.0	2.8	1.4	1.7	8.5	8.4	8.3	8.4
XII	1005.8	1023.9	964.0	1014.7	-2.2	-0.1	-1.4	-1.3	0.9	-4.4	8.0	8,9	-18.6	16	89	85	90	88	0.5	0.9	0.5	0.6	7.9	8.8	6.8	7.8
Rok	1007.5	1032.2	964.0	1016.2	6.3	11.2	7.5	8.1	12.4	3.6	32.4	4.VII	-20.2	16.1	86	68	85	76	1.6	6.2	2.2	3.3	7.2	7.4	6.0	6.9

Białystok

$H_s = 139\ m$ $H_b = 140{,}8\ m$ $h_w = 11\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °/₀																Średnia prędkość	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C		Suma	Max	Data	Temperatura T			Opad R			Wiatr v					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0	Min<10	R≥0.1	R≥1.0	R≥10.0	v≥10	v≥15					
I	·	·	6	4.7	3	5.0	8	5.7	13	3.2	29	4.5	25	5.2	4	6.1	5	4.5	43.1	8.8	12	26	12	5	·	15	9	·	2	·	2	·	·	22	26
II	4	2.2	3.5	2.9	3.5	2.9	7.5	5.7	18.5	4.4	25.5	4.1	13.5	3.5	5	3.8	3	3.9	56.2	7.8	22	18	4	·	·	19	12	·	1	·	4	·	1	18	11
III	1.4	3.4	5.5	3.1	6.5	5.1	10	5.8	10.5	5.0	15	5.1	11	4.2	7.5	3.8	7	4.1	25.7	10.1	15	28	7	5	·	8	5	1	7	·	·	·	6	9	15
IV	1.2	2.0	7	2.7	5.5	3.0	6	2.0	7.5	3.9	13.5	2.7	13.5	2.4	1.3	3.4	1.2	2.4	35.5	10.2	28	13	·	·	2	13	9	1	1	·	1	3	5	7	1
V	18.5	2.8	1.0	3.6	5	3.7	3	2.8	8.5	3.5	8.5	3.6	1.1	3.5	20.5	2.5	8	2.8	19.7	6.0	7	3	·	·	1	6	5	·	1	·	1	2	4	1.0	·
VI	8.5	2.9	1.5	2.7	1.5	2.0	7	3.9	8	3.8	16.5	3.3	2.5	3.6	1.7	3.3	5	3.2	18.0	8.3	4	·	·	·	1.1	7	5	·	·	·	·	3	3	7	·
VII	5.5	1.6	7	2.0	8.5	3.8	7.5	3.6	11.5	2.9	1.7	2.6	1.9.5	3.4	10.5	2.3	6	2.7	39.0	6.2	18	·	·	·	1.5	1.7	1.4	·	·	·	1	8	2	1.0	·
VIII	2	3.0	2	2.0	1	5.0	4.5	3.3	10.5	2.3	27.5	3.5	25	2.8	9.5	3.1	1.1	2.7	124.0	42.5	17	·	·	·	3	16	13	3	1	·	2	4	2	1.0	·
IX	0.5	2.0	1	1.0	·	·	5.5	2.6	1.5	4.1	2.9	4.8	2.7	3.8	4	2.1	8	3.6	149.3	49.8	18	·	·	·	1	1.5	1.3	3	6	·	1	1	2	4.8	·
X	·	·	·	·	·	·	5	4.8	1.8	3.1	4.3	3.4	19.5	3.4	2.5	3.0	5	3.2	17.4	4.0	23	3	·	·	·	9	7	·	·	·	1	·	3	1.4	·
XI	8	5.6	5	3.8	7.5	4.5	2.0	4.3	9	2.5	7.5	3.1	1.9	3.7	4	3.1	1.0	3.4	23.5	7.5	28	11	1	1	·	1.2	6	·	2	·	4	·	1	2.1	1
XII	1.1.5	3.0	0.5	4.0	8	2.6	7	2.4	9.5	3.4	2.8	4.1	10.5	4.8	6	3.0	1.2	3.1	36.3	10.3	8	29	1.3	7	·	1.2	8	1	·	·	5	·	4	1.7	1.0
Rok	8.4.5	2.4	4.9	2.7	5.0	3.1	9.1	3.9	1.3.9.5	3.5	2.6.0	3.7	2.2.5.5	3.7	1.0.3.5	3.3	9.2	3.3	5.8.5.8	4.9.8	1.8.IX	1.3.1	3.7	1.8	3.3	1.4.9	1.0.6	9	2.1	·	2.2	2.1	3.3	1.6.5	6.4

Przelewice

$H_s = 60\ m$ $h_w = 10\ m$

I	·	·	1	4.0	·	·	4.5	2.7	1.8.5	2.9	3.1.5	3.3	1.6	3.1	4.5	2.0	1.7	2.5	64.5	1.8.2	26	22	1.0	2	·	1.3	1.0	3	·	·	-	-	3	1.6	-
II	·	·	·	·	0.5	2.0	4.5	1.7	2.2.5	2.9	2.0.5	2.7	9.5	4.0	0.5	4.0	2.6	2.0	61.4	1.0.3	8	1.3	·	·	·	1.5	1.3	1	·	·	-	-	4	1.1	-
III	2.5	1.8	5	1.5	8	4.0	1.8	3.5	1.2.5	2.3	2.4	2.9	1.1.5	4.8	0.5	1.0	1.1	2.7	64.8	2.2.2	17	1.8	·	·	·	7	7	2	1	·	-	-	1.4	7	-
IV	9	2.1	5	1.4	4	1.4	4.5	2.0	7	2.3	1.3.5	2.0	1.3	2.0	7	1.9	2.7	1.4	22.0	5.6	16	7	·	·	·	1.0	5	·	·	·	-	-	6	5	-
V	2.5	2.2	6	2.5	7	1.9	4.5	2.2	7	1.3	1.7	2.2	1.6	3.2	3	2.7	3.0	1.6	18.5	8.6	7	3	·	·	2	5	4	·	1	·	-	-	2	9	-
VI	2	2.0	4.5	1.9	9	2.6	6	2.3	5.5	2.6	2.4.5	2.5	1.4	2.8	9.5	2.1	1.8	2.0	34.7	1.0.3	24	·	·	·	1.0	7	6	1	·	·	-	-	8	7	-
VII	1.5	2.0	2.5	1.8	6.5	2.1	5.5	2.0	5.5	1.8	2.4.5	3.1	2.3	2.4	1.4	2.0	1.0	2.2	1.6.5.0	4.7.0	2.1	·	·	·	1.2	1.6	1.5	5	·	·	-	-	1	1.1	-
VIII	·	·	0.5	3.0	3	2.0	7.5	2.3	2.0	2.4	4.1	2.6	1.0.5	2.3	1.5	2.0	9	2.2	3.1.3	8.0	2.1	·	·	·	2	1.3	7	·	·	·	-	-	3	8	-
IX	1	1.0	·	·	3	1.0	4	3.5	2.2	3.0	3.7	3.2	1.0	3.7	3	2.7	1.0	2.8	67.6	1.9.6	23	·	·	·	1	1.9	1.5	1	1	·	-	-	2	1.2	-
X	0.5	2.0	0.5	2.0	·	·	8	2.0	2.7.5	3.0	4.5.5	3.4	5.5	4.7	0.5	1.2.0	5	3.1	1.8.4	8.8	1.9	1	·	·	·	8	5	·	2	·	-	-	1	1.1	-
XI	5.5	1.1	6	3.2	1.3.5	2.3	1.9	2.7	1.2	3.5	1.2.5	5.1	1.5	5.6	2.5	2.6	4	3.6	1.3.8	2.9	9	1.3	1	·	·	9	5	·	2	·	-	-	3	1.9	-
XII	2.5	1.2	3.5	2.0	6.5	3.1	6.5	2.9	2.0.5	3.4	3.2.5	4.3	1.1	3.1	1	2.0	9	3.2	42.7	1.4.8	8	2.1	6	3	·	1.5	9	1	·	·	-	-	1	1.7	-
Rok	2.7	1.5	3.4.5	1.9	6.1	1.9	9.2.5	2.5	1.8.0.5	2.6	3.2.1	3.1	1.5.5	3.5	4.7.5	3.1	1.7.6	2.4	6.0.4.7	4.7.0	2.1.VII	9.8	1.7	5	2.7	1.3.7	1.0.1	1.4	7	·	-	-	4.8	1.3.3	-

Ostrołęka

$H_s = 97\ m$ $H_b = 98{,}2\ m$ $h_w = 12\ m$

I	0.5	1.0	7	4.9	6	3.0	1.0.5	2.2	8.5	2.9	2.3.5	4.4	2.4.5	3.9	1.5	2.3	1.1	3.2	3.0.8	5.6	5	2.5	1.0	6	·	1.5	1.0	·	·	·	8	·	1	1.7	2.4
II	2.5	3.0	4.5	1.7	5.5	1.8	1.6	3.2	1.1.5	2.4	2.0	2.6	7	3.1	3	2.7	1.4	2.2	4.9.0	8.3	8	1.2	3	·	·	2.1	1.4	·	·	·	6	·	1	1.6	6
III	8	2.9	1.1.5	3.1	1.4	4.5	1.1.5	3.6	4	3.1	1.1.5	2.8	1.2	3.8	6.5	3.4	1.4	3.0	2.5.3	1.5.2	1.5	2.3	5	1	·	7	5	1	2	·	1	·	6	7	5
IV	1.0	2.4	1.7	2.3	1.0.5	1.5	5.5	2.5	6.5	2.5	6.5	2.6	5	2.6	1.2	3.0	1.7	1.9	2.0.9	5.2	3.0	1.1	·	·	3	1.1	9	·	·	·	1	4	5	7	1
V	1.5.5	2.9	1.7	2.6	6.5	2.0	6	3.0	1.5	3.0	4.5	3.1	6.5	3.3	1.5.5	2.7	2.0	2.2	1.7.5	7.7	1.0	4	·	·	1	8	3	·	·	·	·	1	3	8	·
VI	7.5	2.6	8	1.8	6	1.8	5.5	3.8	2.5	2.8	1.1.5	3.2	1.2.5	2.5	1.0.5	2.2	2.6	1.8	7.1.0	2.1.2	9	·	·	·	9	9	7	3	·	·	·	4	8	8	·
VII	5	1.7	9.5	1.9	9	2.0	6	1.5	1.5	1.0	1.4.5	2.1	1.3.5	2.4	7	2.3	2.7	1.5	1.0.4.8	3.6.4	1.6	·	·	·	1.3	1.6	1.4	3	·	·	2	9	3	1.3	·
VIII	3	1.5	1.5	1.0	2.5	1.6	7.5	3.1	3	2.8	2.3	3.4	1.5.5	2.3	8	1.9	2.9	1.8	1.2.2.0	4.7.5	1.7	·	·	·	3	1.7	1.3	2	·	·	2	3	1	6	·
IX	3.5	1.6	2	1.0	·	·	9.5	2.1	7	2.9	2.1	3.4	1.9.5	3.8	5.5	1.9	2.2	2.5	1.2.3.2	3.3.0	2.3	·	·	·	2	1.8	1.1	4	1	·	·	·	2	1.5	·
X	1	1.0	2	1.0	4	1.2	4.5	2.4	9	3.1	3.0	3.2	1.1.5	2.1	3	1.5	2.8	1.8	1.1.7	3.5	3.0	1	·	·	·	1.0	4	·	·	·	5	·	4	8	·
XI	6.5	6.6	1.1.5	2.6	1.2.5	2.4	1.2.5	3.0	6	1.9	1.3.5	2.8	9	3.6	0.5	1.0.0	1.8	2.5	2.1.0	9.5	2.8	8	1	·	·	1.1	4	·	2	·	3	·	1	2.1	·
XII	5.5	3.7	3.5	2.9	3.5	2.1	3.5	1.0	1.4.5	3.1	1.9	4.3	1.2	3.9	3.5	2.0	2.8	2.4	3.2.9	1.3.7	8	2.4	1.1	4	·	1.3	7	1	1	·	6	·	4	1.5	1.2
Rok	6.8.5	2.6	9.5	2.2	8.0	2.0	9.8.5	2.6	7.5.5	2.6	1.9.8.5	3.2	1.4.8.5	3.1	7.6.5	3.0	2.5.4	2.2	6.3.0.1	4.7.5	1.7.VIII	1.0.8	3.0	1.1	3.1	1.5.6	1.0.1	1.4	6	·	3.4	2.1	3.9	1.4.1	4.8

Toruń – Wrzosy

$H_s = 69\ m$ $H_b = 70{,}1\ m$ $h_w = 12\ m$

I	2.5	1.4	6	4.7	1.0	3.4	9	2.1	5.5	2.5	1.0.5	4.0	3.3.5	4.3	1.6	3.7	·	3.7	2.4.6	6.7	3.1	2.4	1.2	3	·	9	7	·	·	·	8	·	2	2.1	2.0
II	5.5	3.0	7.5	2.3	3.5	2.7	1.2	3.2	9	3.2	7.5	2.7	2.1	4.1	1.2	2.9	6	3.0	5.5.6	1.1.6	1.8	1.5	·	·	·	1.9	1.2	1	·	·	7	·	·	1.6	3
III	9.5	3.4	1.2.5	2.6	1.8	5.5	1.0.5	5.3	7.5	3.6	1.5	3.3	9	5.0	2.3.5	3.3	1	4.0	3.5.9	8.9	1.5	1.9	1	·	·	8	7	·	5	3	2	·	6	9	1
IV	3.2	4.1	8.5	3.2	9.5	4.4	3	3.3	2	3.2	4	4.0	4.5	3.7	2.1.5	3.5	5	3.6	2.5.4	1.8.1	2.2	9	·	·	·	8	3	1	·	·	5	2	5	1.4	·
V	2.6	4.4	1.9.5	4.1	1.2	2.8	4	4.2	1	2.0	3.5	2.3	8	5.6	1.8	3.9	1	4.0	2.8.3	9.2	9	3	·	·	1	8	7	·	2	·	1	1	2	9	·
VI	1.7.5	3.1	1.6.5	3.1	9	2.9	3.5	4.9	·	·	3	2.8	1.1	3.7	2.9.5	3.4	·	3.3	3.5.7	1.5.6	4	·	·	·	1.2	7	5	1	·	·	1	3	5	7	·
VII	9	2.7	8	3.3	1.2	3.2	3.5	3.4	3	2.3	5.5	4.0	2.0	3.6	3.2	3.7	·	3.5	2.1.4.2	8.0.1	1.4	·	·	·	1.3	2.1	1.9	5	2	2	3	9	4	1.4	·
VIII	9.5	2.3	3.5	2.7	4.5	2.6	7	4.3	3	3.3	6.5	4.7	2.9	3.8	2.9	2.7	1	3.3	6.9.9	2.2.0	4.0	·	·	·	2	1.3	8	3	·	·	1	3	3	8	·
IX	6	1.4	2	1.2	2.5	3.0	7.5	2.7	7	2.9	1.1.5	4.1	2.3	4.2	2.4.5	3.6	6	3.2	6.1.6	1.6.7	2.3	2	·	·	2	2.1	1.4	4	2	1	6	2	·	8	·
X	2.5	1.8	1.5	1.7	1	3.0	8	2.8	8	2.1	1.2.5	2.9	2.6.5	3.6	2.8	2.4	5	2.7	3.9	1.1	1	3	·	·	·	6	1	·	·	·	1.2	·	2	1.3	·
XI	7	6.4	9.5	3.5	1.8.5	3.1	1.5.5	3.5	2	3.7	7.5	2.8	1.1	4.3	1.0	4.8	9	3.5	1.3.4	3.2	2.4	9	1	·	·	7	6	·	1	1	3	·	2	2.0	·
XII	7.5	3.5	3.5	4.4	5.5	4.0	7.5	1.4	6.5	2.4	8	4.9	3.3	4.0	1.0.5	4.0	1.1	3.3	2.6.1	8.9	8	2.3	1.0	4	·	1.0	7	·	3	1	9	·	1	1.8	1.2
Rok	1.3.4.5	3.1	9.8.5	3.1	1.0.6	3.4	9.1	3.4	5.4.5	2.6	8.1.5	3.5	2.2.9.5	4.2	2.5.4.5	3.5	4.5	3.4	5.9.4.6	8.0.1	4.VII	1.0.7	2.4	7	3.0	1.3.7	9.6	1.2	1.5	8	5.8	2.0	3.2	1.5.7	3.6

Toruń – Podgórz

$\varphi = 53°03'$ $\lambda = 18°35'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-4.3	0.6	-0.6	-0.5	1.6	-3.4	9.7	6	-16.3	17	91	86	88	88	0.5	0.9	0.7	0.7	9.1	8.4	8.5	8.7
II	–	–	–	–	1.5	4.9	2.7	3.0	5.7	0.1	10.6	14	-6.3	24	94	81	87	87	0.4	1.8	1.0	1.1	8.7	8.5	7.2	8.1
III	–	–	–	–	0.1	6.4	2.8	3.0	7.9	-1.7	16.7	31	-10.2	11	85	56	79	73	1.1	4.9	1.7	2.6	5.6	6.3	4.3	5.4
IV	–	–	–	–	4.2	11.3	6.6	7.2	12.7	1.7	24.1	28	-7.2	13	86	57	78	74	1.2	6.9	2.4	3.5	5.7	7.1	5.4	6.1
V	–	–	–	–	9.0	14.4	10.1	10.9	15.7	5.4	25.7	19	-1.9	6	79	54	73	69	2.5	8.2	3.7	4.8	6.9	7.6	5.4	6.6
VI	–	–	–	–	13.4	21.6	17.0	17.8	23.3	10.6	30.8	11	5.6	16	75	52	70	66	4.5	13.6	6.0	8.0	5.9	6.3	4.3	5.5
VII	–	–	–	–	17.2	22.3	18.3	19.0	24.2	14.1	36.5	4	9.4	29	85	62	79	75	3.2	11.9	5.1	6.7	7.1	6.9	6.3	6.8
VIII	–	–	–	–	14.4	20.1	15.5	16.4	21.4	11.6	26.9	11	7.3	29	89	63	84	79	1.9	9.1	3.0	4.7	6.3	7.9	4.5	6.2
IX	–	–	–	–	9.6	14.6	11.1	11.6	16.2	7.4	27.3	9	-0.9	27	92	70	86	83	0.9	5.7	2.0	2.9	6.9	8.0	4.4	6.4
X	–	–	–	–	6.4	12.2	8.4	8.8	13.1	4.8	19.6	19	-1.0	2	95	73	90	86	0.5	3.9	1.2	1.9	7.4	7.8	4.4	6.5
XI	–	–	–	–	3.6	6.8	4.6	4.9	7.7	1.9	15.8	7	-9.1	21	90	76	85	84	0.8	2.6	1.2	1.5	8.2	8.0	7.6	7.9
XII	–	–	–	–	-2.1	0.1	-1.2	-1.1	1.2	-4.5	7.8	8	-20.5	16	93	88	93	91	0.4	0.8	0.4	0.5	7.6	8.0	6.9	7.5
Rok	–	–	–	–	6.5	11.3	7.9	8.4	12.6	4.0	36.5	4.VII	-20.5	16.XII	88	68	83	80	1.5	5.9	2.4	3.3	7.1	7.6	5.8	6.8

Przasnysz

$\varphi = 53°01'$ $\lambda = 20°53'$

I	–	–	–	–	-2.5	-0.5	-2.1	-1.8	0.1	-5.0	7.1	6	-19.5	16	90	85	90	88	0.4	0.9	0.6	0.6	9.4	9.2	9.4	9.3
II	–	–	–	–	1.0	3.5	1.6	1.9	3.8	-0.6	8.0	14	-4.9	28	94	85	93	91	0.4	1.2	0.5	0.7	9.6	9.4	9.2	9.4
III	–	–	–	–	-0.5	5.2	1.4	1.9	5.9	-2.6	15.7	31	-9.6	17	–	–	–	–	–	–	–	–	7.4	7.2	7.1	7.2
IV	–	–	–	–	4.6	13.0	7.2	8.0	13.5	2.0	25.4	27	-5.2	10	–	–	–	–	–	–	–	–	7.1	7.4	7.6	7.4
V	–	–	–	–	9.0	14.4	9.6	10.6	15.1	4.8	27.0	19	-2.0	6	–	–	–	–	–	–	–	–	6.8	6.5	7.2	6.8
VI	–	–	–	–	14.2	21.1	15.1	16.4	21.9	10.3	28.7	19	6.0	27	–	–	–	–	–	–	–	–	6.2	6.0	6.1	6.1
VII	–	–	–	–	16.1	22.2	17.5	18.5	23.2	12.7	30.0	8	7.4	29	–	–	–	–	–	–	–	–	8.4	7.6	7.8	7.9
VIII	–	–	–	–	13.9	19.6	15.5	16.1	20.4	10.9	26.5	12	6.4	28	92	70	89	84	1.4	6.4	2.1	3.3	7.9	7.7	8.0	7.9
IX	–	–	–	–	9.2	14.4	10.6	11.2	15.5	7.2	27.1	9	0.4	27	93	71	89	84	0.9	5.4	1.5	2.6	8.3	7.6	8.5	8.2
X	–	–	–	–	5.6	11.4	7.3	7.9	11.9	3.6	19.9	19	-0.5	3	94	77	91	87	0.6	3.2	1.0	1.6	8.0	8.0	7.4	7.8
XI	–	–	–	–	3.5	5.6	3.9	4.2	6.6	1.7	14.4	6,7	-8.5	30	90	80	88	86	0.8	2.0	0.9	1.2	8.9	8.8	8.9	8.9
XII	–	–	–	–	-2.1	-0.5	-1.6	-1.4	0.2	-4.5	4.9	5	-13.7	16	86	82	87	85	0.7	1.0	0.7	0.8	8.2	8.1	8.1	8.1
Rok	–	–	–	–	6.0	10.8	7.2	7.8	11.5	3.4	30.0	8.VII	-19.5	16.1	–	–	–	–	–	–	–	–	8.0	7.8	8.0	7.9

Trzcińsko-Zdrój

$\varphi = 52°58'$ $\lambda = 14°36'$

I	–	–	–	–	-0.3	1.4	0.4	0.5	–	–	–	–	–	–	90	85	89	88	0.6	1.1	0.7	0.8	8.6	7.5	7.3	7.9
II	–	–	–	–	1.5	5.1	3.0	3.2	–	–	–	–	–	–	92	79	90	87	0.5	1.9	0.8	1.1	8.7	7.6	5.3	7.2
III	–	–	–	–	1.3	8.1	4.1	4.4	–	–	–	–	–	–	88	62	81	77	0.8	4.4	1.7	2.3	5.9	5.9	4.5	5.4
IV	–	–	–	–	4.2	11.2	6.0	6.8	–	–	–	–	–	–	87	55	79	74	1.1	6.5	2.0	3.2	6.7	6.6	3.7	5.7
V	–	–	–	–	8.3	14.2	9.0	10.1	–	–	–	–	–	–	79	51	77	69	2.4	9.0	2.8	4.7	6.1	6.7	5.5	6.1
VI	–	–	–	–	14.1	20.5	16.6	16.9	–	–	–	–	–	–	80	53	72	68	3.4	12.5	5.6	7.2	5.6	6.0	6.0	5.9
VII	–	–	–	–	16.5	21.5	17.5	18.2	–	–	–	–	–	–	89	69	87	82	2.2	8.9	2.9	4.7	6.3	6.9	6.7	6.6
VIII	–	–	–	–	14.0	18.9	14.7	15.6	–	–	–	–	–	–	90	64	85	80	1.6	8.4	2.7	4.2	6.6	6.6	5.0	6.1
IX	–	–	–	–	9.6	14.3	11.0	11.5	–	–	–	–	–	–	92	71	90	84	1.0	5.2	1.4	2.5	7.5	7.7	4.4	6.6
X	–	–	–	–	7.2	12.4	9.0	9.4	–	–	–	–	–	–	95	75	89	86	0.8	3.7	1.2	1.9	8.2	7.4	4.9	6.8
XI	–	–	–	–	3.3	6.1	4.1	4.4	–	–	–	–	–	–	92	82	88	87	0.7	1.9	1.0	1.2	8.2	8.1	7.7	8.0
XII	–	–	–	–	-0.5	0.9	-0.2	0.0	–	–	–	–	–	–	90	87	90	89	0.6	0.8	0.6	0.7	8.8	7.6	6.2	7.5
Rok	–	–	–	–	6.6	11.2	7.9	8.4	–	–	–	–	–	–	88	69	85	81	1.3	5.4	2.0	2.9	7.3	7.0	5.6	6.6

Ciechocinek

$\varphi = 52°53'$ $\lambda = 18°48'$

I	–	–	–	–	-1.5	0.5	-0.8	-0.6	1.5	-3.1	9.4	6	-17.3	16	–	–	–	–	–	–	–	–	8.7	8.5	7.8	8.3
II	–	–	–	–	1.7	4.8	2.8	3.0	5.8	0.7	10.6	14	-3.6	24	–	–	–	–	–	–	–	–	8.5	8.2	8.2	8.3
III	–	–	–	–	0.0	6.3	2.7	2.9	8.1	-1.0	16.5	31	-7.0	10	–	–	–	–	–	–	–	–	5.4	6.2	3.4	5.0
IV	–	–	–	–	4.2	11.5	6.7	7.3	13.1	2.2	24.5	27	-4.5	14	–	–	–	–	–	–	–	–	5.5	6.5	5.6	5.9
V	–	–	–	–	8.8	14.7	10.0	10.9	16.1	5.5	25.7	19	-0.4	6	–	–	–	–	–	–	–	–	6.1	6.5	5.3	6.0
VI	–	–	–	–	15.5	21.7	16.8	17.7	23.6	11.1	31.1	11	6.0	3	–	–	–	–	–	–	–	–	4.6	5.3	4.3	4.7
VII	–	–	–	–	17.3	22.2	18.0	18.9	24.4	14.3	34.8	4	10.2	29	–	–	–	–	–	–	–	–	7.1	6.3	6.4	6.6
VIII	–	–	–	–	14.4	20.3	15.4	16.4	21.6	12.0	27.0	11	7.8	24	–	–	–	–	–	–	–	–	5.6	6.8	3.6	5.3
IX	–	–	–	–	9.6	15.0	11.0	11.8	16.4	7.8	27.0	8,9	-0.1	27	–	–	–	–	–	–	–	–	6.2	7.7	5.5	6.5
X	–	–	–	–	6.0	12.4	8.2	8.7	13.4	4.9	19.8	19	-1.0	2	–	–	–	–	–	–	–	–	6.2	7.0	4.4	5.9
XI	–	–	–	–	3.8	6.6	4.4	4.8	7.7	2.2	16.1	6	-6.8	24,30	–	–	–	–	–	–	–	–	8.2	7.9	7.4	7.8
XII	–	–	–	–	-2.1	-0.1	-1.4	-1.2	1.4	-3.9	8.2	8	-17.3	16	–	–	–	–	–	–	–	–	7.5	8.5	6.6	7.5
Rok	–	–	–	–	6.5	11.2	7.8	8.3	12.8	4.4	34.8	4.VII	-17.3	16.1,16.XII	–	–	–	–	–	–	–	–	6.6	7.1	5.7	6.5

Toruń – Podgórz

H_s = 53 m h_w = 12 m **1957**

MIESIĄC	ROZKŁAD WIATRU nD, VmD																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr V		≡	≥1	◔	●	▦
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10	Max>25	0.1 R≥	1.0 R≥	10.0 R≥	v≥10	v≥15					
I	25	21	15	22	5	19	2	18	35	26	195	34	355	45	55	41	12	31	188	48	5	24	12	4	·	11	7	·	1	·	–	·	1	23	–
II	8	17	2	15	2	12	45	32	85	39	195	36	225	45	5	42	12	31	540	137	18	15	·	·	·	21	14	1	1	·	–	·	1	16	–
III	65	40	75	25	125	47	12	52	5	28	55	49	15	51	15	31	14	36	330	76	15	19	1	1	·	7	6	·	5	·	–	·	6	10	–
IV	275	32	65	32	55	24	15	30	2	17	85	34	55	45	20	29	13	27	242	148	22	9	·	·	·	7	4	1	·	·	–	3	5	11	–
V	285	39	7	35	6	25	4	32	15	50	3	40	10	58	21	35	12	34	300	81	9	1	·	·	1	9	7	·	1	·	–	2	2	10	–
VI	205	23	75	27	3	23	4	31	5	38	55	41	185	41	21	31	5	30	295	79	4	·	·	·	10	8	6	·	1	·	–	4	3	5	–
VII	7	24	6	29	115	29	4	18	65	33	11	32	30	33	15	31	2	30	2105	596	14	·	·	·	13	21	18	4	·	·	–	12	3	15	–
VIII	5	13	1	20	2	50	2	42	85	36	15	47	37	41	125	27	10	34	618	223	10	·	·	·	2	11	7	3	3	·	–	8	1	7	–
IX	2	10	·	·	1	10	25	26	7	44	22	48	30	49	125	33	13	37	654	135	23	1	·	·	2	19	14	1	5	2	–	1	·	8	–
X	·	·	·	·	·	·	3	28	135	33	245	44	305	43	115	30	10	35	50	13	19	1	·	·	·	8	1	·	2	·	–	·	2	8	–
XI	55	24	7	33	135	29	10	33	105	50	12	45	155	54	5	42	11	35	86	40	24	10	1	·	·	5	3	·	1	·	–	·	2	21	–
XII	6	28	45	26	25	42	25	40	15	29	155	52	26	52	6	31	15	35	264	100	8	23	8	5	·	12	5	1	4	1	–	·	3	20	–
Rok	119	22	565	22	645	26	52	32	865	35	1615	42	276	46	150	34	129	33	5672	596	14.VII	103	22	10	28	139	92	11	24	3	–	30	29	154	–

Przasnysz

H_s = 120 m h_w = 8,5 m

I	·	·	25	14	45	16	85	20	18	12	265	23	255	33	35	36	4	23	197	48	31	25	13	7	·	10	6	·	·	·	6	·	·	28	17
II	15	27	2	20	1	20	15	15	235	17	27	22	55	44	25	16	6	19	325	59	18	16	2	·	·	15	9	·	·	·	3	·	·	25	3
III	25	28	5	19	10	44	19	22	125	28	18	23	125	30	55	36	8	26	180	111	15	24	5	·	·	7	4	1	1	·	1	·	·	12	2
IV	10	28	15	23	65	19	15	12	12	17	115	15	9	23	5	29	6	18	243	102	30	8	·	·	3	12	6	1	·	·	·	3	·	13	1
V	75	25	125	22	95	14	155	17	155	15	105	22	95	28	65	27	6	19	250	82	7	2	·	·	1	9	6	·	·	·	·	1	·	12	·
VI	6	28	65	15	85	11	85	14	15	17	135	17	205	24	45	20	7	17	804	153	24	·	·	·	6	11	8	4	·	·	·	3	·	7	·
VII	15	17	5	17	135	14	145	14	95	21	155	16	18	23	75	21	8	16	757	165	11	·	·	·	8	14	11	4	·	·	5	4	·	19	·
VIII	35	16	35	18	15	20	65	29	185	18	27	24	25	32	35	17	4	23	1027	299	14	·	·	·	1	16	8	4	·	·	3	2	·	12	·
IX	2	10	5	10	·	·	2	30	27	22	225	30	23	52	35	34	5	30	1107	330	24	·	·	·	1	14	10	4	2	·	1	1	·	14	·
X	2	10	·	·	·	·	2	12	24	15	38	22	19	27	·	·	8	18	98	37	20	1	·	·	·	8	5	·	·	·	4	·	·	19	·
XI	4	62	45	14	12	22	195	22	125	16	15	26	13	36	35	59	6	25	118	38	3	12	1	·	·	9	4	·	·	·	2	·	·	22	·
XII	9	18	5	13	9	13	·	·	9	13	26	22	23	36	6	33	6	22	260	128	8	27	12	4	·	11	7	1	1	·	6	·	·	19	5
Rok	195	22	665	15	76	16	126	17	197	18	251	22	2035	32	516	28	74	21	5336	330	24.IX	115	33	11	20	136	84	19	4	·	34	14	·	202	28

Trzcińsko – Zdrój

H_s = 57 m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	269	59	5	–	–	–	–	11	8	·	–	–	–	·	2	19	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	355	70	13	–	–	–	–	12	10	·	–	–	–	·	·	11	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	330	115	17	–	–	–	–	8	6	1	–	–	–	·	9	11	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	150	76	19	–	–	–	–	7	3	·	–	–	–	·	3	7	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	839	373	23	–	–	–	–	6	5	3	–	–	–	·	2	7	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	296	142	24	–	–	–	–	7	4	1	–	–	–	3	7	11	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1320	202	10	–	–	–	–	17	17	6	–	–	–	7	1	8	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	322	54	21	–	–	–	–	11	11	·	–	–	–	5	2	9	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	926	185	2	–	–	–	–	17	15	3	–	–	–	2	·	9	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	127	54	19	–	–	–	–	8	4	·	–	–	–	·	1	10	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	145	37	9	–	–	–	–	8	5	·	–	–	–	·	3	19	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	257	125	8	–	–	–	–	13	5	1	–	–	–	·	1	18	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5336	373	23.V	–	–	–	–	125	94	15	–	–	–	17	31	159	–

Ciechocinek

H_s = 43 m h_w = 14 m

I	2	10	9	27	105	25	2	10	65	15	25	27	255	33	55	24	7	25	223	66	5	22	10	2	·	12	0	·	·	·	4	·	3	21	19
II	8	13	6	13	6	23	35	17	125	31	215	24	165	30	5	26	5	24	500	120	18	9	·	·	·	22	14	1	·	·	4	·	·	18	2
III	105	18	105	28	20	56	5	54	5	54	85	28	145	42	10	53	12	34	339	86	15	19	1	·	·	9	6	·	5	2	0	·	8	9	·
IV	28	25	11	24	65	33	1	10	6	20	25	30	55	29	165	20	13	22	304	100	30	8	·	·	·	12	6	1	·	·	6	3	8	13	·
V	28	27	205	38	7	31	05	50	05	20	8	35	8	27	105	25	10	28	228	109	9	1	·	·	1	8	6	1	1	·	2	1	3	11	·
VI	17	24	17	23	85	25	2	30	25	20	95	32	9	28	155	24	9	23	206	70	4	·	·	·	12	6	6	·	·	·	2	3	9	7	·
VII	11	22	95	24	6	27	05	20	45	23	95	24	225	28	175	27	12	22	134.2	325	16	·	·	·	13	14	13	5	·	·	1	10	4	13	·
VIII	75	17	35	24	45	31	2	37	4	26	13	33	32	31	135	22	13	24	805	194	10	·	·	·	2	12	8	4	·	·		6	5	9	·
IX	2	12	1	40	3	10	45	22	95	26	185	38	29	43	135	23	9	30	760	183	22	1	·	·	2	16	12	2	4	·	3	2	1	9	·
X	25	12	55	17	3	15	3	17	2	17	345	31	27	26	105	17	8	23	82	27	20	1	·	·	·	9	4	·	·	·	2	·	6	9	·
XI	95	34	20	32	185	25	15	27	55	19	10	34	145	53	25	46	8	31	144	57	24	9	1	·	·	7	4	·	1	·	6	·	3	19	·
XII	7	21	12	22	8	29	3	12	55	18	24	44	21	46	45	21	8	31	233	80	8	21	8	4	·	12	6	·	4	2	10	·	1	16	11
Rok	133	20	1255	26	1015	28	285	26	64	24	1815	32	222	35	125	27	114	26	5167	326	15.VII	91	20	6	30	139	91	14	12	4	52	25	54	154	32

Kabylec

$\varphi = 52°51'$ $\lambda = 17°12'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA t								ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnio I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-1.4	0.4	-0.6	-0.6	1.5	-3.1	9.7	6	-17.5	16	88	85	88	87	0.6	1.0	0.7	0.8	8.5	8.3	7.9	8.2
II	-	-	-	-	1.5	4.6	2.3	2.7	5.8	-0.1	9.3	5	-5.4	27	92	78	89	86	0.6	2.0	0.8	1.1	6.9	8.0	6.4	7.1
III	-	-	-	-	0.4	6.5	3.0	3.2	8.0	-0.9	15.8	13	-6.0	6	-	-	-	-	-	-	-	-	5.8	5.1	3.7	4.9
IV	-	-	-	-	4.1	11.4	6.6	7.2	12.8	1.8	23.5	28	-6.3	14	-	-	-	-	-	-	-	-	6.2	6.6	5.8	6.2
V	-	-	-	-	8.8	14.7	9.7	10.7	16.0	4.6	25.2	19	-0.8	6	74	48	69	64	3.0	9.8	4.1	5.6	5.6	7.0	4.9	5.8
VI	-	-	-	-	14.8	21.5	16.3	17.2	23.2	10.1	30.9	19	4.6	15	78	49	73	67	4.0	14.5	5.3	7.9	5.3	5.7	4.5	5.2
VII	-	-	-	-	17.1	24.5	17.6	18.4	23.5	14.0	34.9	4	9.1	3	-	-	-	-	-	-	-	-	7.4	7.7	6.7	7.3
VIII	-	-	-	-	13.8	19.2	15.0	15.8	20.5	11.4	26.9	11	6.3	23	89	65	83	79	1.9	8.2	3.0	4.4	6.6	7.6	4.8	6.3
IX	-	-	-	-	9.1	14.4	10.5	11.2	15.7	7.1	27.4	8	-1.1	27	92	71	85	83	1.0	5.3	2.0	2.8	7.1	7.8	5.0	6.6
X	-	-	-	-	6.6	11.9	8.4	8.8	12.7	5.0	19.9	19	-1.9	2	93	76	91	87	0.7	3.3	1.0	1.7	7.7	7.6	5.5	6.9
XI	-	-	-	-	3.2	6.1	3.9	4.3	7.1	1.8	16.3	5	-7.5	30	88	78	86	84	0.9	2.3	1.1	1.4	8.0	8.6	7.9	8.2
XII	-	-	-	-	-1.6	-0.1	-0.9	-0.9	1.2	-3.4	8.9	8	-14.2	17	89	86	90	88	0.6	0.8	0.5	0.7	8.4	8.4	6.9	7.9
Rok	-	-	-	-	6.4	11.0	7.7	8.2	12.3	4.0	34.9	4.VII	-17.5	16.1	-	-	-	-	-	-	-	-	7.0	7.4	5.8	6.7

Więcławice

$\varphi = 52°51'$ $\lambda = 18°19'$

I	-	-	-	-	-2.0	0.2	-0.7	-0.8	1.0	-	8.0	6	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	1.5	4.3	2.6	2.8	5.0	-	8.5	2	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	0.4	5.9	2.7	2.9	7.3	-	14.7	31	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	5.0	11.2	6.6	7.4	12.4	-	23.2	28	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	9.2	14.5	10.2	11.0	15.8	-	25.8	19	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	15.0	20.9	16.6	17.3	22.8	-	29.4	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	16.7	21.4	17.6	18.3	23.4	-	30.7	4,8	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	14.3	19.3	15.1	16.0	20.8	-	25.8	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	9.5	14.4	11.1	11.5	15.9	-	26.6	8	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	6.0	11.9	7.8	8.4	12.9	-	19.3	10	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	6.9	-	15.5	5	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	0.6	-	7.0	9	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	12.1	-	30.7	4,8.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Szepietowo

$\varphi = 52°51'$ $\lambda = 22°32'$

I	-	-	-	-	-2.8	-1.2	-1.7	-1.8		-4.3	-	-	-14.7	16	-	-	-	-	-	-	-	-	8.3	7.6	7.0	7.6
II	-	-	-	-	0.2	2.4	1.3	1.3		-0.5	-	-	-6.0	27,28	93	88	94	92	0.5	0.9	0.4	0.6	8.9	8.5	7.7	8.4
III	-	-	-	-	-2.1	3.6	0.5	0.6		-3.5	-	-	-11.7	17	-	-	-	-	-	-	-	-	6.3	5.5	4.1	5.3
IV	-	-	-	-	4.6	12.4	7.3	7.9		2.4	-	-	-5.7	10	88	59	83	77	4.1	7.6	2.0	3.6	5.7	5.9	4.1	5.2
V	-	-	-	-	9.2	13.8	9.8	10.6		5.3	-	-	-1.3	6	84	68	82	78	1.9	5.8	2.3	3.3	5.5	6.8	5.3	5.9
VI	-	-	-	-	14.9	21.0	15.8	16.9		10.5	-	-	5.5	21	77	53	75	68	4.1	12.4	4.6	7.0	5.2	5.3	4.0	4.8
VII	-	-	-	-	16.7	21.9	17.1	18.2		12.8	-	-	8.6	7,8	84	59	82	75	3.2	11.8	3.7	6.2	6.6	6.8	6.1	6.5
VIII	-	-	-	-	13.9	19.2	15.1	15.8		11.4	-	-	6.2	24	90	66	86	81	1.6	8.4	2.5	4.2	5.5	6.9	4.2	5.5
IX	-	-	-	-	9.5	13.8	10.7	11.2		7.5	-	-	0.7	27	92	75	88	85	1.0	4.4	1.5	2.3	6.6	7.8	5.3	6.6
X	-	-	-	-	5.4	10.9	7.7	7.9		4.3	-	-	0.0	3	92	73	89	85	0.7	3.7	1.2	1.9	6.2	6.0	4.7	5.6
XI	-	-	-	-	2.8	4.9	3.6	3.7		0.8	-	-	-9.4	30	93	86	89	89	0.5	1.4	1.0	1.0	8.8	8.6	7.2	8.2
XII	-	-	-	-	-3.1	-1.0	-2.5	-2.3		-5.1	-	-	-12.4	16	89	86	90	88	0.5	0.7	0.5	0.6	6.7	7.5	5.8	6.7
Rok	-	-	-	-	5.8	10.1	7.1	7.5		3.5	-	-	-14.7	16.1	-	-	-	-	-	-	-	-	6.7	6.9	5.5	6.4

Inowrocław

$\varphi = 52°48'$ $\lambda = 18°14'$

I	-	-	-	-	-1.1	0.8	-0.9	-0.5	1.5	-3.1	9.3	6	-17.6	16	87	82	87	85	0.7	1.2	0.8	0.9	9.3	7.9	7.7	8.3
II	-	-	-	-	2.4	5.6	2.7	3.4	6.0	0.7	9.5	14	-3.6	24	88	76	88	84	0.9	2.3	0.9	1.4	8.0	7.9	7.6	7.8
III	-	-	-	-	1.8	7.3	3.0	3.8	8.3	-0.4	16.8	13	-4.6	17	82	64	81	76	1.3	4.1	1.5	2.3	5.5	6.0	3.7	5.1
IV	-	-	-	-	5.6	12.8	7.0	8.1	13.3	2.9	24.2	29	-4.6	13	82	59	79	73	1.6	7.0	2.3	3.6	5.7	6.8	5.2	5.9
V	-	-	-	-	9.0	15.4	10.0	11.1	16.1	6.1	25.9	19	0.9	6	81	56	78	72	2.3	8.4	2.9	4.5	6.0	6.6	4.2	5.6
VI	-	-	-	-	15.7	22.2	16.9	17.9	23.4	10.8	30.9	19	6.8	27	78	59	78	72	4.1	12.0	4.4	6.8	5.2	5.5	4.3	5.0
VII	-	-	-	-	18.0	22.9	17.7	19.1	24.0	14.4	34.4	4,6	9.8	29	-	-	-	-	-	-	-	-	6.5	7.1	6.6	6.7
VIII	-	-	-	-	15.4	20.3	15.6	16.7	21.2	12.0	25.9	7,11	7.3	23	91	74	90	85	1.7	6.5	1.9	3.4	6.5	7.2	5.5	6.4
IX	-	-	-	-	10.4	15.4	10.9	11.9	16.1	7.8	27.3	8	-0.1	27	91	73	90	85	1.1	5.3	1.4	2.6	6.4	7.7	5.6	6.6
X	-	-	-	-	6.3	12.9	8.1	8.8	13.4	5.1	19.8	19	-0.6	2	93	74	91	86	0.6	4.0	1.0	1.9	7.4	6.7	4.6	6.2
XI	-	-	-	-	4.1	6.7	4.3	4.8	7.5	2.5	15.8	5	-6.7	30	92	85	92	89	0.7	1.9	0.7	1.1	7.2	8.2	7.6	7.7
XII	-	-	-	-	-0.9	0.1	-1.0	-0.7	1.1	-3.2	8.1	8,9	-14.6	16	90	86	90	89	0.6	0.9	0.5	0.7	8.6	8.5	7.4	8.2
Rok	-	-	-	-	7.2	11.9	7.9	8.7	12.7	4.8	34.4	4,8.VII	-17.6	16.1	-	-	-	-	-	-	-	-	6.8	7.2	5.8	6.6

Kobylec

$H_s = 90\ m$ $h_w = 10\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (n, v m/s)																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C				Temperatura T				Opad R			Wiatr v						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	Średnia prędkość	Suma	Max	Data	Min <0°	Max <0°	Min <-10°	Max >25	0.1 ≤ R < 10	10 ≤ R < 100	R ≥ 100	10 ≤ v < 15	v ≥ 15	≡	≥5	◔	●	⊠
I	3	2.3	3	5.7	10	4.3	·	·	6	2.0	24	3.8	38	7.1	6	8.0	3	5.3	298	89	12	22	9	2	·	10	6	·	5	3	14	·	·	22	–
II	4	1.5	3	2.3	5	2.6	2	3.0	18	2.8	15	3.3	27	5.4	4	9.0	6	3.7	415	127	18	16	·	·	·	14	10	1	3	1	6	·	·	8	–
III	6	4.3	4	3.0	20	4.8	8	6.8	10	2.8	9	3.9	19	7.0	6	3.7	11	4.4	523	149	29	18	·	·	·	9	8	2	4	2	4	·	6	8	–
IV	14	3.1	13	4.8	15	2.5	1	1.0	7	1.9	4	4.5	10	4.0	15	3.9	11	3.0	224	149	25	7	·	·	·	7	4	1	1	·	2	·	3	10	–
V	12	3.6	20	4.8	10	2.2	3	3.7	8	3.2	2	2.0	18	6.4	12	6.2	8	4.2	211	144	6	4	·	·	1	6	3	1	5	2	·	1	2	7	–
VI	3	3.7	5	4.2	20	2.6	3	3.0	3	5.0	6	2.0	22	4.3	14	3.6	14	2.9	374	157	24	·	·	·	11	7	7	1	·	·	1	1	6	6	–
VII	4	4.0	8	3.0	11	2.6	·	·	10	2.2	5	4.2	24	4.8	22	4.4	9	3.4	1408	272	14	·	·	·	12	19	17	6	1	·	1	8	2	16	–
VIII	1	3.0	1	5.0	4	2.0	4	1.5	5	2.2	18	5.4	39	4.6	10	2.2	11	3.6	639	144	16	·	·	·	2	10	9	3	2	·	3	2	·	8	–
IX	·	·	·	·	2	1.0	4	2.5	10	1.6	22	4.8	37	6.1	7	4.6	8	4.4	887	224	23	2	·	·	1	18	14	2	6	2	3	·	·	7	–
X	·	·	·	·	2	1.0	2	3.0	10	3.0	33	4.1	30	5.4	9	3.9	7	4.0	96	26	4	1	·	·	·	7	5	·	3	1	11	·	2	10	–
XI	3	11.3	10	3.4	20	3.2	11	2.1	11	1.5	13	3.6	16	8.4	1	3.0	5	3.0	92	25	28	11	1	·	·	8	3	·	4	2	6	·	2	20	–
XII	1	5.0	4	8.0	7	3.0	6	2.3	12	2.0	19	3.3	34	7.2	4	12.2	6	4.9	296	129	8	22	9	3	·	13	8	1	6	3	11	·	1	20	–
Rok	51	3.5	71	3.7	126	2.6	44	2.4	110	2.5	170	3.7	314	5.9	110	5.4	99	4.0	5460	272	14.VII	107	19	5	27	128	94	18	40	16	62	12	24	142	–

Więcławice

$H_s = 90\ m$ $h_w = 22\ m$

I	1	1.0	5	3.0	6	4.0	5	2.0	·	·	19	2.8	25	3.2	17	3.7	15	2.7	136	60	31	–	12	–	·	6	5	·	1	1	–	·	–	–	–
II	2	2.0	·	·		·	4	2.2	·	·	38	2.1	22	2.9	7	2.0	11	2.0	–	–	–	–	·	–	·	–	–	–	·	·	–	·	–	–	–
III	·	·	2	2.0	9	4.3	18	3.4	·	·	20	2.3	21	4.6	14	5.7	9	3.5	364	86	18	–	·	–	·	6	6	·	3	2	–	·	–	–	–
V	9	2.7	9	4.0	1	1.0	8	3.5	2	2.5	14	2.9	7	1.9	38	3.0	2	2.9	246	124	22	–	·	–	·	6	5	1	·	·	–	3	–	–	–
V	6	3.2	12	3.2	3	3.0	5	3.2	3	2.3	15	2.4	13	3.0	32	3.6	4	3.0	361	174	20	–	·	–	1	9	6	1	2	·	–	4	–	–	–
VI	8	2.4	5	2.6	5	1.8	8	2.2	7	2.4	16	2.5	18	2.2	21	2.5	2	2.3	371	90	24	–	·	–	8	8	7	·	·	·	–	1	–	–	–
VII	2	2.0	5	1.8	3	2.3	11	2.1	1	4.0	16	1.9	13	2.5	26	2.5	16	1.9	1727	535	14	–	·	–	13	19	16	5	·	·	–	9	–	–	–
VIII	·	·	1	2.0	·	·	7	2.0	11	2.3	30	2.2	21	2.5	17	2.1	6	2.1	465	135	10	–	·	–	1	8	6	1	·	·	–	1	–	–	–
IX	2	1.5	4	3.8	·	·	5	4.8	6	2.3	25	2.6	20	4.0	14	3.4	14	2.8	639	126	23	–	·	–	2	16	15	1	2	·	–	1	–	–	–
X	·	·	·	·	3	2.3	7	2.0	4	2.0	37	2.1	18	2.3	6	4.8	18	1.9	58	24	20	–	·	–	·	5	2	·	1	·	–	·	–	–	–
XI	3	2.7	8	4.5	16	2.9	14	2.4	7	1.6	18	2.1	17	3.7	5	2.6	2	2.8	50	18	24	–	1	–	·	4	3	·	1	·	–	·	–	–	–
XII	3	3.3	4	1.5	12	2.4	2	2.5	3	2.7	10	2.6	43	2.9	6	2.0	10	2.4	192	57	8	–	11	–	·	14	5	·	1	1	–	·	–	–	–
Rok	36	1.7	55	2.4	58	2.0	94	2.7	44	1.8	258	2.4	238	3.0	203	3.2	109	2.5	–	535	14.VII	–	24	–	25	–	–	–	11	4	–	19	–	–	–

Szepietowa

$H_s = 150\ m$ $h_w = 14.5\ m$

I	2	2.0	7.5	5.5	0.5	5.0	7.5	4.1	5.5	3.0	13	3.5	46.5	6.8	10.5	6.7	·	5.6	336	92	5	24	–	6	–	13	6	·	9	1	2	·	·	15	–
II	11.5	1.9	·	·	1	2.0	1	4.0	12.5	3.3	14.5	2.8	36.5	3.4	4	2.8	3	2.9	561	74	8	13	–	·	–	21	17	·	2	·	3	·	·	18	–
III	24	3.0	5	1.8	7	7.4	7	4.0	10	5.1	4.5	2.4	19.5	5.5	15	6.0	1	4.5	277	154	15	23	–	2	–	6	4	1	8	2	1	·	6	8	–
IV	15	2.3	2	3.0	2.5	1.2	8	3.8	10.5	3.2	4	2.5	10	3.2	3.0	3.1	8	2.7	225	95	17	8	–	·	·	11	8	·	1	·	1	3	5	4	–
V	20.5	2.8	3.5	4.4	6	1.8	9	2.2	10.5	2.2	3.5	2.9	11.5	3.7	23.5	3.6	5	2.8	181	64	7	1	–	·	–	6	4	·	1	·	·	1	6	10	–
VI	18	4.0	3.5	2.3	·	·	7.5	2.7	6	5.1	11.5	3.5	25	3.7	12.5	2.9	6	3.3	125	4.2	7	·	–	·	–	7	4	·	4	·	·	1	7	7	–
VII	9.5	3.3	6.5	1.9	6	2.4	11.5	3.2	12	3.0	13.5	3.0	19.5	3.7	9.5	3.5	5	3.0	492	90	15	·	–	·	–	17	13	·	·	·	2	8	3	10	–
VIII	4	2.5	·	·	2	2.0	10	2.4	7	2.9	21	3.4	26.5	3.8	15.5	3.6	7	3.1	1030	248	17	·	–	·	–	16	13	4	1	·	2	2	2	7	–
IX	6	2.3	·	·	0.5	2.0	7	2.5	10	3.5	29	3.9	26.5	6.1	8	2.4	3	4.0	815	175	29	·	–	·	–	16	12	2	4	1	1	1	3	11	–
X	1	4.0	·	·	·	·	7.5	2.3	15	2.0	35	3.0	28.5	3.8	5	2.8	1	3.0	99	35	23	·	–	·	–	11	3	·	2	·	4	·	4	7	–
XI	17.5	4.3	6.5	2.6	9	2.9	14.5	4.0	11.5	1.4	10.5	2.0	18	5.2	1.5	8.0	1	3.6	167	79	28	11	–	·	–	9	4	·	5	1	3	·	2	18	–
XII	6	3.2	2.5	3.2	8.5	1.6	9.5	2.5	9	2.9	2.5	4.4	22.5	6.0	7	3.9	3	3.7	236	97	8	29	–	4	–	12	8	·	4	·	3	·	4	13	–
Rok	135	3.0	37	2.1	43	2.4	100	3.1	119.5	3.1	18.5	3.1	290.5	4.5	14.2	4.1	43	3.5	4614	248	17.VIII	109	–	12	–	145	96	7	41	5	22	16	42	126	–

Inowrocław

$H_s = 90\ m$ $h_w = 15\ m$

I	0.5	1.0	7	2.6	5	2.3	4	1.9	6.5	1.5	25.5	2.6	23.5	3.4	2.0	3.7	1	2.9	314	68	12	22	10	2	·	11	9	·	2	·	–	·	2	22	23
II	4	2.5	5.5	1.8	6	2.2	6	2.5	7.5	3.3	3.2	2.7	12.5	2.6	10.5	3.6	·	2.7	506	122	18	12	·	·	·	21	16	1	·	·	–	·	·	14	·
III	6.5	3.1	9.5	2.5	12	2.4	17	4.8	10.5	3.1	12.5	2.6	6.5	5.4	19.5	3.7	·	3.5	389	118	17	18	·	·	·	10	7	1	3	·	–	·	8	9	1
IV	19	3.1	2.5	2.7	7	2.5	7.5	1.9	3.5	2.0	3.5	2.3	7	2.5	17.5	2.7	·	2.7	34.9	12.5	2.5	7	·	·	·	13	7	1	·	·	–	3	6	10	·
V	19.5	3.0	19.5	2.6	4.5	1.9	11.5	2.1	3.5	2.1	5.5	1.5	9	3.2	2.0	3.6	·	2.8	37.7	16.0	2.0	·	·	·	2	11	8	1	1	·	–	3	8	8	·
VI	5	2.4	15.5	2.1	8	1.6	11	2.1	3	3.2	12	2.4	11.5	2.5	2.4	2.3	·	2.3	46.4	16.7	2.4	·	·	·	10	10	7	2	·	·	–	3	6	7	·
VII	8.5	2.2	7	1.9	7	2.6	8	2.1	3.5	2.4	12	2.0	12	2.4	3.5	2.5	·	2.3	198.4	45.2	14	·	·	·	13	20	19	4	·	·	–	14	3	13	·
VIII	3	1.8	6.5	1.6	2.5	1.4	5.5	2.1	4.5	2.6	2.5	3.7	18.5	2.7	27.5	2.5	·	2.7	62.8	16.8	7	·	·	·	2	11	8	2	·	·	–	1	1	6	·
IX	4	2.2	2	1.0	·	·	5	1.7	8	2.6	21.5	3.3	28.5	3.4	2.1	3.5	·	3.1	60.4	17.2	2.3	1	·	·	2	19	15	1	3	1	–	2	2	10	·
X	1.5	2.3	1	1.0	·	·	6	2.2	13.5	2.1	31.6	2.4	2.2	2.9	17.5	2.5	·	2.5	7.4	1.6	1.9	1	·	·	·	8	3	·	·	·	–	·	4	8	·
XI	5	4.9	9	2.2	9.5	1.7	26.5	1.9	9.5	1.7	12.5	2.3	4.5	3.7	13.5	4.7	·	2.6	6.5	1.6	2.5	9	1	·	·	7	4	·	2	·	–	·	2	18	·
XII	8	2.9	10.5	2.6	9.5	2.4	3	2.3	3	1.5	20.5	3.5	21	4.3	17.5	3.0	·	3.3	27.1	9.4	14	21	10	3	·	12	6	·	2	·	–	·	2	20	10
Rok	83.5	2.6	118	2.0	71	1.8	111	2.3	76.5	2.3	21.4	2.6	176.5	3.2	24.3.5	3.2	4	2.8	602.5	45.2	14.VII	91	21	5	29	153	109	13	43	1	–	23	39	145	34

Bielsk Podlaski

$\varphi = 52°47'$ $\lambda = 23°11'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.7	-0.9	-1.7	-1.8	0.4	-4.2	6.2	6	-16.8	16	88	85	88	87	0.5	0.8	0.6	0.6	9.2	8.7	8.3	8.7
II	–	–	–	–	0.3	2.6	1.3	1.4	3.7	-0.7	8.5	14	-7.9	28	92	86	91	90	0.5	1.1	0.6	0.7	9.0	8.5	8.2	8.5
III	–	–	–	–	-2.4	3.3	-0.1	0.2	4.8	-4.3	16.5	30	-12.7	4	85	67	81	78	0.8	3.2	1.2	1.7	6.5	6.1	4.2	5.3
IV	–	–	–	–	4.7	12.3	7.5	8.0	13.6	2.6	26.1	30	-5.4	10	88	55	81	75	1.1	7.7	2.2	3.7	6.3	6.5	5.8	6.2
V	–	–	–	–	9.6	14.5	10.1	11.1	16.1	5.8	26.6	19	-1.2	2,6	84	62	84	77	2.1	6.9	2.2	3.7	6.0	7.5	5.5	6.3
VI	–	–	–	–	15.2	21.5	15.4	15.9	22.9	10.2	30.0	12	5.2	21	76	54	79	70	4.1	12.5	3.8	6.8	6.0	6.0	4.7	5.4
VII	–	–	–	–	16.7	22.3	17.2	18.4	24.0	13.0	29.2	5	7.6	4	85	61	85	77	3.1	11.1	3.2	5.8	6.6	7.5	7.0	7.0
VIII	–	–	–	–	14.4	19.6	14.9	16.0	21.0	11.4	29.4	12	5.0	26	89	68	88	82	1.9	7.8	2.2	4.0	6.7	7.2	5.6	6.5
IX	–	–	–	–	9.8	14.4	10.4	11.2	15.8	7.9	26.6	9	0.5	27	92	70	90	84	1.0	5.5	1.4	2.6	7.9	7.8	5.7	7.1
X	–	–	–	–	5.7	11.5	7.8	8.2	–	4.3	–	–	-0.7	16	91	71	87	83	0.9	4.2	1.5	2.2	6.8	6.7	6.9	6.8
XI	–	–	–	–	2.8	5.1	3.5	3.7	–	1.3	–	–	-9.5	30	91	83	90	88	0.6	1.6	0.7	1.0	9.2	8.6	7.5	8.4
XII	–	–	–	–	-3.0	-0.6	-2.4	-2.1	0.0	-5.0	5.6	13	-12.4	16	86	81	87	85	0.6	1.1	0.7	0.8	7.5	7.5	6.5	7.2
Rok	–	–	–	–	5.9	10.5	7.0	7.6	–	3.5	30.0	12.VI	-16.8	16.1	87	70	86	81	1.4	5.3	1.7	2.8	7.3	7.4	6.3	7.0

Gorzów Wlkp.

$\varphi = 52°44'$ $\lambda = 15°15'$

I	–	–	–	–	-1.0	0.6	-0.3	-0.2	1.8	-2.5	10.8	6	-11.7	17	91	85	85	88	0.5	1.0	0.7	0.7	8.7	8.4	6.6	7.9
II	–	–	–	–	1.2	4.8	2.9	3.0	6.2	0.4	11.6	5	-4.8	26	94	80	90	88	0.4	1.8	0.7	1.0	8.1	8.7	6.6	7.8
III	–	–	–	–	0.9	7.7	4.2	4.2	9.6	0.1	17.8	27	-6.0	2	87	62	76	75	0.9	4.3	2.1	2.4	6.0	6.2	3.6	5.3
IV	–	–	–	–	3.6	11.3	7.0	7.2	13.2	2.2	24.8	28	-5.3	14	88	52	72	71	1.0	7.2	3.0	3.7	5.1	7.0	3.8	5.3
V	–	–	–	–	7.7	14.0	10.4	10.6	16.3	5.1	25.5	16	-2.2	9	81	50	67	66	2.1	8.9	4.5	5.2	5.4	7.3	5.3	6.0
VI	–	–	–	–	14.2	21.2	17.5	17.6	23.4	11.2	31.1	11	6.9	26	78	50	64	64	3.9	14.1	7.8	8.6	5.3	6.2	4.7	5.4
VII	–	–	–	–	16.2	21.4	18.4	18.6	23.2	14.2	32.3	1	10.1	29	89	67	79	78	2.1	9.6	5.0	5.6	7.1	7.4	7.8	7.3
VIII	–	–	–	–	13.3	18.8	15.2	15.6	20.8	11.7	27.3	11	6.8	23	92	64	82	79	1.2	8.3	3.4	4.3	6.9	7.5	5.2	6.5
IX	–	–	–	–	9.0	14.3	11.1	11.4	16.2	7.7	28.1	8	0.2	26	95	71	86	84	0.6	5.2	1.8	2.5	7.5	8.7	5.6	7.3
X	–	–	–	–	6.5	11.7	8.9	9.0	13.1	5.5	19.7	10	-0.7	2	95	77	91	88	0.5	3.3	1.1	1.6	8.0	7.4	5.3	6.9
XI	–	–	–	–	2.9	5.9	4.1	4.2	7.0	2.0	14.0	1,4	-5.0	30	91	81	87	86	0.7	1.9	1.0	1.2	7.7	8.5	7.3	7.8
XII	–	–	–	–	-1.1	0.1	-0.5	-0.5	1.7	-2.5	9.4	8	-13.3	17	91	88	89	89	0.5	0.7	0.6	0.6	8.5	8.5	6.8	7.9
Rok	–	–	–	–	6.1	11.0	8.2	8.4	12.7	4.8	32.3	1.VII	-13.3	17.XII	89	69	81	80	1.2	5.5	2.6	3.1	7.0	7.6	5.7	6.8

Puttusk

$\varphi = 52°43'$ $\lambda = 21°06'$

I	–	–	–	–	-1.8	0.0	-1.2	-1.0	0.9	-4.6	7.5	6	-16.5	16	86	81	85	84	0.7	1.1	0.9	0.9	8.4	8.2	6.6	7.7
II	–	–	–	–	1.5	4.1	2.5	2.6	5.0	-0.1	9.5	14	-4.7	28	89	79	87	85	0.7	1.8	1.0	1.2	8.6	7.1	7.1	7.6
III	–	–	–	–	0.2	5.6	2.4	2.6	7.2	-2.6	17.2	31	-9.2	17	–	–	–	–	–	–	–	–	5.2	4.9	3.3	4.5
IV	–	–	–	–	5.5	13.3	8.6	9.0	14.1	3.0	26.7	30	-6.9	10	84	47	72	68	1.6	9.5	3.3	4.8	5.1	4.9	4.6	4.9
V	–	–	–	–	9.4	14.5	10.6	11.3	15.9	5.3	27.5	19	-1.2	6	77	55	73	68	2.8	8.5	3.7	5.0	4.9	6.0	4.0	5.0
VI	–	–	–	–	15.7	21.3	17.0	17.8	23.0	10.9	30.6	11	6.0	27	74	52	74	67	4.7	13.1	5.2	7.7	3.5	4.6	3.4	3.8
VII	–	–	–	–	16.9	22.7	18.3	19.1	24.3	13.7	33.1	8	8.9	29	83	59	79	74	3.3	12.1	4.7	6.7	6.5	4.3	4.8	5.2
VIII	–	–	–	–	14.1	20.0	15.8	16.4	21.3	11.4	29.9	12	7.1	28	87	64	86	79	2.1	8.9	2.5	4.4	5.0	6.9	4.8	5.6
IX	–	–	–	–	9.8	15.1	11.4	11.9	16.3	7.7	27.9	9	0.5	27	88	70	85	81	1.4	5.8	2.1	3.1	6.7	6.8	4.8	6.1
X	–	–	–	–	5.9	12.2	8.0	8.5	12.9	4.1	20.0	19	0.2	3	88	69	87	81	1.2	4.5	1.4	2.4	6.3	6.1	4.4	5.5
XI	–	–	–	–	3.5	6.4	4.3	4.6	7.5	1.7	16.2	6	-8.0	30	87	76	85	83	1.0	2.5	1.2	1.6	8.4	7.6	6.9	7.6
XII	–	–	–	–	-2.0	-0.3	-1.5	-1.3	0.6	-4.5	6.5	13	-15.6	16	88	86	88	87	0.6	0.8	0.6	0.7	7.4	7.9	6.0	7.1
Rok	–	–	–	–	6.6	11.2	8.0	8.4	12.4	3.8	33.1	8.VII	-16.5	16.1	–	–	–	–	–	–	–	–	6.3	6.3	5.1	5.9

Białowieża

$\varphi = 52°42'$ $\lambda = 23°51'$

I	10001	10110	9839	10209	-2.6	-1.0	-1.9	-1.8	0.1	-4.6	6.5	6	-17.3	16	89	84	89	87	0.5	0.9	0.6	0.7	9.2	9.2	8.1	8.8
II	9949	10106	9700	10122	0.2	2.6	1.2	1.3	3.6	-1.5	7.8	15	-11.3	28	90	82	87	86	0.6	1.4	0.9	1.0	8.8	8.6	7.2	8.2
III	9993	10168	9728	10200	-3.4	3.7	-0.4	-0.4	5.2	-5.9	16.5	31	-17.3	4	80	56	76	71	0.9	4.0	1.6	2.2	5.8	5.2	4.9	5.3
IV	9986	10121	9740	10186	4.2	12.5	6.7	7.5	13.7	0.7	26.4	30	-7.4	15	84	50	75	70	1.5	9.0	2.8	4.4	5.0	5.5	5.1	5.2
V	9962	10070	9822	10139	9.5	14.3	9.8	10.8	16.3	5.0	26.2	19	-2.6	2	79	56	83	73	2.5	7.8	2.0	4.1	5.4	7.3	5.7	6.1
VI	9971	10090	9827	10164	15.1	21.1	16.0	17.0	22.8	9.6	31.6	12	4.5	21	74	50	74	66	4.5	13.2	4.8	7.5	4.8	5.6	4.3	4.9
VII	9929	10030	9828	10121	16.7	22.1	17.1	18.2	23.6	12.5	29.5	5	7.0	4	82	58	83	74	3.6	12.0	3.4	6.3	6.2	6.4	5.3	6.0
VIII	994[illegible]023		9856	10139	14.0	19.5	14.6	15.7	20.8	11.0	29.5	12	3.4	24	89	65	89	81	1.8	8.4	2.0	4.1	6.4	6.0	3.7	5.4
IX	9922	10053	9764	10118	9.4	14.4	10.1	11.0	15.4	7.1	26.0	9	0.0	27	93	69	91	84	0.9	5.8	1.1	2.6	7.4	7.3	5.3	6.7
X	9999	10122	9883	10199	4.9	11.4	7.2	7.7	12.2	3.5	18.6	19	-2.7	16	92	69	88	83	0.7	4.4	1.3	2.1	7.1	6.2	5.6	6.3
XI	10046	10228	9764	10220	2.0	4.7	3.0	3.2	6.2	0.4	14.1	1	-10.6	30	92	84	88	87	0.6	1.8	0.9	1.1	8.7	7.7	8.1	8.2
XII	9949	10128	9578	10156	-3.6	-0.9	-3.1	-2.7	0.0	-6.5	6.6	13	-15.8	16	85	79	85	83	0.7	1.2	0.7	0.9	7.4	7.1	6.6	7.0
Rok	9966	10228	9578	10465	5.5	10.4	6.7	7.3	11.7	2.6	31.6	12.VI	-17.3	16.1, 4.III	86	67	84	79	1.6	5.8	1.8	3.1	6.8	6.8	5.8	6.5

Bielsk Podlaski

$H_s = 145\ m$ $h_w = 10\ m$ **1957**

	ROZKŁAD WIATRU [%D,TmD]																OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość					Temperatura T				Opad R			Wiatr				
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max ≥ 0°	Max < 0°	Min < 10°	Max ≥ 25°	0,1 ≤ < 1,0	1,0 ≤ < 10	10 ≤ < 100	≥ 100	≥ 10 m/s	≥ 15 m/s	≥ 1	≥ 5	≥ 10	≥ 20	≥ 50
I	4	30	2	55	45	39	75	43	13	29	47	39	42	48	·	·	6	3,7	33,5	8,5	8	24	12	6	·	15	8	·	·	3	·	9	·	·	20	·
II	25	22	05	30	·	·	35	27	225	34	43	31	7	21	·	·	5	2,9	66,8	12,2	22	12	3	·	·	19	15	1	·	1	·	4	·	·	19	·
III	1	20	1	50	2	60	12	9,5	16	4,5	30	32	14	40	9	5,6	8	4,4	28,9	15,7	15	25	8	4	·	11	5	1	·	8	4	1	·	4	8	·
IV	25	50	2	20	3	23	4	23	20,5	25	28	23	11	13	7	3,0	12	2,1	22,6	6,4	30	8	·	·	3	11	7	·	·	·	·	2	1	2	8	·
V	25	38	3,5	30	2	3,0	9	2,8	19	3,1	15,5	2,6	19,5	2,6	5	3,2	17	2,4	31,1	11,3	7	3	·	·	1	10	6	1	2	·	1	2	1	12	·
VI	1	10	2	3,5	·	·	1,5	2,3	16,5	2,8	36,5	2,9	20,5	3,0	3	2,7	9	2,6	36,3	22,8	24	·	·	·	10	8	6	1	1	·	1	1	5	7	·
VII	0,5	1,0	1	1,0	3	2,7	6	2,8	19,5	2,1	32,5	2,2	17	3,4	0,5	1,0	13	2,1	79,9	12,6	24	·	·	·	11	16	15	2	·	·	2	6	2	14	·
VIII	·	·	·	·	·	·	2	5,0	14	2,1	42,5	2,9	15,5	2,7	1	3,0	18	2,2	162,9	69,5	14	·	·	·	3	13	13	3	·	·	1	3	1	10	·
IX	·	·	·	·	·	·	2	1,0	11,5	3,2	49	4,7	12,5	4,8	3	2,3	12	3,7	111,3	39,3	23	·	·	·	1	13	12	2	4	2	2	1	1	16	·
X	·	·	·	·	1	2,0	2,5	4,4	20,5	2,2	48,6	2,8	10,5	4,0	·	·	10	2,5	12,0	6,8	23	2	–	·	·	8	3	·	·	·	·	·	3	1,2	·	·
XI	4	6,8	1	2,0	5	4,4	11,5	3,6	19,5	2,2	2,3	2,3	1,1	4,7	2	6,5	13	2,8	27,8	10,5	28	10	–	·	·	11	6	1	3	·	2	·	·	2,0	·
XII	2	3,5	4	4,2	1	7,0	4	2,5	18,5	2,7	4,2	4,7	6,5	5,3	6	3,8	9	3,7	27,4	7,4	8	27	14	5	·	11	7	·	2	·	2	·	1	4,5	·
Rok	17	24	17	24	21,5	26	66,5	3,6	21,1	2,8	437,5	3,1	15,7	3,6	36,5	2,6	132	2,9	640,5	69,5	14.VIII	111	–	15	29	146	103	12	24	6	27	14	20	164	·

Gorzów Wlkp.

$H_s = 65\ m$ $h_w = 14\ m$

I	5	2,2	6,5	4,9	7,5	3,9	4	2,5	3,5	2,6	30,5	3,1	27	4,1	9	4,7	·	3,6	27,8	4,4	5	22	9	2	·	16	8	·	·	·	7	·	3	2,0	2,0
II	3,5	3,9	7	2,6	5,5	3,7	8	2,9	8,5	4,8	24,5	3,0	19	2,9	8	3,2	·	3,2	32,5	6,0	13	11	·	·	·	19	9	·	2	·	6	·	1	11	2
III	7,5	2,5	3,5	6,1	24,5	6,0	15,5	4,4	4	2,6	10	2,8	12,5	4,2	11,5	3,7	1	4,5	37,7	13,5	17	16	·	·	·	11	7	1	6	2	1	·	6	5	1
IV	28,5	3,6	13	3,0	7	3,6	6	2,1	1	2,0	4,5	3,3	10,5	3,4	22,5	3,5	·	3,4	12,0	4,3	19	9	·	·	·	9	5	·	·	·	1	·	5	6	·
V	15,5	3,3	18	3,8	7,5	2,7	2,5	3,8	1	1,5	6,5	2,4	13	3,2	2,5	3,3	4	3,1	23,5	11,0	23	3	·	·	2	9	6	1	1	·	·	5	3	2	·
VI	7	2,6	12,5	2,8	12	2,7	5,5	4,1	0,5	2,0	6	2,2	22	3,4	21,5	3,0	3	2,9	32,1	11,7	24	·	·	·	11	10	8	1	·	·	1	7	6	·	·
VII	13	2,6	3	2,7	5,5	2,9	4,5	2,7	2	1,5	9	2,6	23,5	2,6	29,5	2,9	3	2,6	194,7	36,2	22	·	·	·	9	20	19	7	·	·	1	8	1	15	·
VIII	3,5	2,1	1,5	3,0	5	2,9	4	1,9	2	4,0	27	2,9	25,5	2,4	20,5	2,4	4	2,5	50,2	14,6	24	·	·	·	3	14	11	1	·	·	3	2	·	7	·
IX	0,5	2,0	0,5	2,0	1,5	1,3	1,5	2,7	8	2,8	22	3,8	33	3,5	20	2,8	3	3,2	70,1	18,9	23	·	·	·	1	23	14	2	3	·	6	·	·	10	·
X	4	1,2	2,5	4,0	5	2,0	2,5	2,6	7	2,4	32	2,5	27	2,9	11	1,8	2	2,4	20,4	6,8	19	2	·	·	·	13	7	·	1	·	1,3	·	2	1,1	·
XI	4	3,5	8,5	3,8	29,5	3,0	1,4	2,8	3	2,5	10,5	2,4	15,5	5,2	5	5,5	·	3,5	11,0	2,2	27	12	1	·	·	10	5	·	1	·	3	·	2	1,8	·
XII	4,5	4,0	5	5,0	11,5	3,3	11,5	1,9	5	2,9	2,8	3,2	4,7	3,5	10,5	2,4	·	3,2	29,9	12,0	8	21	6	2	·	18	8	1	2	·	1,0	·	1	2,0	9
Rok	96,5	2,8	81,5	3,4	11,9	3,2	79,5	2,9	45,5	2,6	207,5	2,8	25,1,5	3,4	19,4	3,3	20	3,2	541,9	36,2	22.VIII	96	16	4	26	172	107	14	16	2	51	16	31	141	3,2

Pułtusk

$H_s = 80\ m$ $h_w = 12\ m$

I	3,5	2,3	6,5	2,3	2	1,7	3	2,2	2	4,0	28,5	3,8	24,5	4,3	9	5,0	14	3,2	39,2	10,2	6	27	12	5	·	10	8	1	3	1	–	·	2	1,7	–
II	·	·	7	2,1	0,5	5,0	11,5	2,9	19,5	2,9	17,5	3,4	16	4,1	6	3,9	6	3,0	41,1	9,9	18	13	·	·	·	15	12	·	1	1	–	·	1	1,5	–
III	9,5	3,8	9,5	3,4	4	4,6	15,5	7,7	4,5	5,4	7,5	6,3	16	5,4	13,5	4,8	13	4,6	25,8	12,1	15	19	4	·	·	7	4	1	10	3	–	·	8	5	–
IV	18,5	3,6	11	3,1	5	2,9	10	3,0	4,5	3,9	7,5	3,5	3	4,8	20,5	3,5	16	2,8	11,2	6,0	30	7	·	·	4	8	3	·	·	·	–	4	6	5	–
V	12,5	2,8	14,5	2,7	4	2,1	9	1,8	2,5	3,2	10,5	4,6	1	4,0	2,4	4,0	1,5	2,8	18,6	8,4	7	2	·	·	2	5	4	·	·	·	·	·	6	7	·
VI	12	3,1	5	2,3	1,5	2,0	5,5	2,9	5,5	4,4	8,5	3,9	1,4	3,9	2,2	3,0	1,6	2,7	63,9	19,8	4	·	·	·	10	11	7	3	·	·	–	4	9	1	·	·
VII	5,5	2,0	7	1,9	8	2,5	7,5	3,2	7,0	3,3	12,5	3,2	11,5	3,8	2,1	3,3	1,5	2,6	90,5	15,2	11	·	·	·	14	14	13	4	2	·	–	9	5	0	·	·
VIII	3	3,3	3	2,3	·	·	3,5	2,6	6,5	3,3	24,5	4,1	12	3,4	18,5	2,7	2,2	2,6	94,9	25,8	14	·	·	·	4	13	14	4	·	·	–	2	2	6	·	·
IX	2,5	2,2	1	2,5	·	·	3,5	3,1	1,4	3,3	1,7	6,0	22,5	7,0	13,5	4,1	1,6	4,2	87,8	22,3	15	·	·	·	2	16	11	3	5	3	–	2	4	3	·	·
X	·	·	·	·	·	·	2	3,0	7,5	3,5	2,7	4,4	3,3	3,6	8,5	3,4	1,5	3,1	5,6	2,6	2,0	·	·	·	·	4	2	·	1	·	–	·	3	2	·	·
XI	5,5	1,4	8,5	3,6	3,5	3,9	2,2	5,0	5	4,4	10,5	3,7	1,3	7,8	2	9,2	2,0	4,6	10,2	5,9	2,8	11	1	·	·	9	2	·	5	3	–	·	2	1,8	·
XII	4,5	4,7	4,5	3,8	·	·	4	3,0	1	6,0	4,1	4,8	5	7,6	7	4,2	2,6	3,4	29,4	9,4	8	26	10	4	·	13	7	·	2	2	–	·	1	1,4	·
Rok	7,1	2,4	7,7,5	2,5	2,8,5	2,1	9,7	3,4	7,9,5	4,0	2,1,2,5	4,3	1,7,1,5	5,0	1,6,5,5	4,3	1,9,2	3,3	5,2,0,2	2,5,8	1,4.VIII	1,0,5	2,7	9	3,6	1,1,8	7,9	1,6	2,9	1,3	–	2,1	4,9	1,0,0	·	·

Białowieża

$H_s = 163\ m$ $H_b = 163,7\ m$ $h_w = 21\ m$

I	0,5	3,0	3	6,3	6,5	7,3	8,5	5,8	13,5	2,7	20	4,0	26,5	6,8	11,5	8,8	3	5,5	32,9	9,9	6	26	13	6	·	13	10	·	8	2	3	·	·	22	2,6
II	4	6,5	3	3,2	4	3,8	8	5,1	14,5	4,4	22,5	4,9	18,5	5,5	4,5	3,3	5	4,5	61,0	12,0	22	19	4	1	·	21	15	1	4	·	4	·	2	16	8
III	4,0	5,6	5,5	3,0	7,5	7,0	12	7,8	7,5	6,3	4,5	3,7	14,5	6,9	14,5	7,5	1,7	5,3	23,0	15,2	15	28	7	8	·	5	4	1	8	5	1	·	8	9	1,5
IV	5	3,9	4	3,2	8,5	3,5	4,0	3,4	8	3,9	9	3,7	8,5	4,5	12	5,1	2,5	2,9	18,1	6,6	18	15	·	·	3	6	4	·	1	1	·	2	7	7	·
V	12,5	4,2	9,5	4,8	11,5	3,4	7,5	4,5	5,5	3,4	6	3,6	8	3,7	16,5	3,7	1,6	3,2	43,4	9,7	22	3	·	·	1	11	8	·	2	1	3	5	5	5	1,1	·
VI	8,5	3,9	1,5	3,0	2,5	3,8	8	3,9	5,5	4,0	1,7	3,5	15,5	4,5	15,5	5,0	1,6	3,4	35,7	24,2	24	·	·	·	10	7	5	1	2	·	·	3	8	5	·	·
VII	4,5	3,7	2,5	3,6	8,5	5,0	9,5	5,2	9	2,8	1,4	3,5	11,5	4,2	12,5	6,1	2,1	3,4	106,7	55,3	9	·	·	·	10	19	8	3	5	1	3	12	5	8	·	·
VIII	2,5	4,8	·	·	3	3,7	4,5	6,3	5,5	4,2	1,9	4,4	2,1	4,7	15,5	3,3	2,2	3,3	68,5	12,5	14	·	·	·	2	20	13	2	3	1	2	6	3	4	·	·
IX	2	2,5	0,5	1,0	0,5	4,0	3,5	2,1	1,3	4,2	2,1	6,0	2,6	7,9	6,5	4,8	1,7	4,8	139,4	37,7	18	·	·	·	1	19	15	2	8	1	·	3	4	14	·	·
X	1,5	2,3	·	·	·	·	4	3,2	14,5	2,5	30,5	3,1	19,5	5,3	7	4,0	1,6	3,0	12,8	5,8	23	3	·	·	·	10	4	·	1	·	3	·	4	9	·	·
XI	8,5	10,0	4,5	5,6	8	5,2	2,0	5,0	7	2,1	9	3,2	11,5	6,9	6,5	5,3	1,5	4,6	27,3	13,9	28	12	1	1	·	13	5	1	5	2	8	·	2	2,0	2
XII	6	5,7	6	3,7	7	2,6	8,5	2,2	14,5	2,8	29,5	4,8	10,5	7,8	3	5,2	8	4,0	28,1	8,4	8	28	14	9	·	14	8	·	3	2	7	·	6	1,7	8
Rok	6,8,5	4,7	4,0	3,1	6,7,5	4,1	10,4	4,5	11,8	3,6	20,2	4,0	19,1,5	5,7	12,5,5	5,2	1,8,4	4,0	5,9,0,9	5,5,3	9.VIII	1,3,4	3,9	2,5	2,7	1,5,8	9,9	1,1	5,0	1,9	3,9	3,1	5,4	1,1,2	5,9	·

Łagiewniki

$\varphi = 52°40'$ $\lambda = 18°19'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.6	0.2	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.1	6.7	7.4
II	–	–	–	–	1.8	4.6	2.6	2.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.1	5.8	6.1
III	–	–	–	–	0.9	5.9	2.7	3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.3	5.4	5.2
IV	–	–	–	–	4.5	11.2	7.2	7.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.0	6.0	5.2
V	–	–	–	–	8.9	14.4	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.1	4.9	4.9
VI	–	–	–	–	15.1	21.0	16.6	17.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.3	3.6	3.7	3.9
VII	–	–	–	–	17.5	21.8	17.6	18.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	14.9	19.5	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.7	14.6	11.2	11.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	6.0	12.4	7.8	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3.7	6.6	4.4	4.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.7	-0.4	-1.6	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.1	6.8
Rok	–	–	–	–	6.6	11.0	7.7	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wieniec-Zdrój

$\varphi = 52°40'$ $\lambda = 18°59'$

I	–	–	–	–	-1.7	0.5	-1.1	-0.8	–	-3.5	–	–	-16.9	16	89	84	88	87	0.5	1.0	0.6	0.7	8.4	8.3	7.8	8.2
II	–	–	–	–	1.3	5.2	2.5	2.9	–	-0.2	–	–	-6.5	24	92	76	88	85	0.5	2.2	0.9	1.2	7.6	7.9	7.7	7.7
III	–	–	–	–	-0.2	6.6	2.0	2.6	–	-1.8	–	–	-9.0	10	85	58	83	75	1.0	4.6	1.2	2.3	4.6	5.7	5.3	4.5
IV	–	–	–	–	4.7	12.0	6.1	7.2	–	1.3	–	–	-6.1	13	83	56	83	74	1.6	7.5	1.6	3.6	5.9	5.8	5.6	5.8
V	–	–	–	–	9.4	14.7	9.2	10.6	–	4.5	–	–	-1.9	6	77	53	80	70	2.9	8.7	2.7	4.8	5.7	5.9	4.2	5.3
VI	–	–	–	–	16.1	22.2	16.2	17.7	–	9.7	–	–	4.6	15	74	49	76	66	5.2	14.9	4.7	8.3	3.8	4.1	3.2	3.7
VII	–	–	–	–	17.6	22.6	17.9	19.0	–	13.3	–	–	9.1	3	83	62	80	75	3.8	12.4	4.5	6.9	6.3	5.7	4.7	5.6
VIII	–	–	–	–	14.6	20.4	15.0	16.2	–	11.2	–	–	5.6	30	88	63	86	79	2.1	9.2	2.5	4.6	5.9	5.9	4.7	5.5
IX	–	–	–	–	9.5	14.9	10.9	11.6	–	7.4	–	–	-1.5	27	92	69	88	83	1.0	6.1	1.6	2.9	6.7	7.8	5.6	6.7
X	–	–	–	–	6.1	12.6	7.7	8.5	–	3.9	–	–	-1.5	2,3	92	72	92	85	0.8	4.2	0.9	2.0	5.3	5.9	4.5	5.2
XI	–	–	–	–	3.6	6.7	4.4	4.8	–	1.7	–	–	-7.9	30	88	76	86	83	0.9	2.5	1.1	1.5	7.3	8.0	6.8	7.4
XII	–	–	–	–	-2.5	0.0	-1.6	-1.4	–	-4.5	–	–	-20.1	16	89	84	89	87	0.5	1.0	0.6	0.7	7.6	8.1	6.8	7.5
Rok	–	–	–	–	6.5	11.5	7.4	8.2	–	3.6	–	–	-20.1	16.XII	86	67	85	79	1.7	6.2	1.9	3.3	6.3	6.6	5.4	6.1

Nur

$\varphi = 52°40'$ $\lambda = 22°19'$

I	–	–	–	–	-2.5	-0.6	-1.5	-1.5	0.5	-4.0	7.1	6	-15.5	16	92	82	90	88	0.4	1.0	0.6	0.7	8.2	7.7	7.8	7.9
II	–	–	–	–	0.6	3.1	1.5	1.7	4.4	-0.8	9.4	14	-9.5	24	93	84	91	89	0.5	1.3	0.7	0.8	8.6	8.3	8.0	8.3
III	–	–	–	–	-1.7	4.4	0.9	1.1	6.3	-3.5	17.2	31	-12.0	4	84	62	83	76	0.9	3.7	1.2	1.9	4.5	4.6	3.9	4.3
IV	–	–	–	–	4.9	12.9	7.6	8.2	14.6	2.4	26.5	29	-6.2	10	86	53	78	72	1.4	8.3	2.5	4.1	4.3	5.6	5.3	5.1
V	–	–	–	–	9.4	14.3	9.5	10.7	16.2	5.1	27.5	19	-1.6	2	83	62	83	76	2.1	7.2	2.2	3.8	5.1	6.9	4.6	5.5
VI	–	–	–	–	15.2	21.9	15.7	17.1	23.5	10.3	30.0	11	4.8	21	79	52	79	70	3.7	13.3	3.8	6.9	4.4	5.0	3.9	4.4
VII	–	–	–	–	16.9	22.6	17.2	18.5	24.4	13.3	34.0	5,8	8.9	4	85	63	86	78	3.2	11.2	2.9	5.8	6.3	6.4	5.6	6.1
VIII	–	–	–	–	14.3	19.9	15.2	16.2	21.4	11.5	30.5	12	6.0	24	91	66	88	82	1.6	8.6	2.2	4.1	6.2	7.2	4.5	6.0
IX	–	–	–	–	9.6	14.7	10.7	11.4	16.3	7.6	28.0	9	0.6	27	94	71	90	85	0.8	5.5	1.6	2.6	6.6	7.6	5.7	6.6
X	–	–	–	–	5.7	11.8	7.7	8.2	13.0	4.1	19.7	19	0.0	3	94	71	90	85	0.6	4.4	1.1	2.0	6.8	6.5	5.5	6.3
XI	–	–	–	–	3.1	5.5	3.8	4.0	6.8	1.5	16.5	6	-9.0	29,30	91	83	90	88	0.6	1.6	0.7	1.0	8.1	8.4	7.7	8.1
XII	–	–	–	–	-2.8	-0.7	-2.2	-2.0	0.6	-5.1	6.4	13	-13.2	16	90	85	90	88	0.5	0.9	0.5	0.6	6.9	7.7	6.5	7.0
Rok	–	–	–	–	6.1	10.8	7.2	7.8	12.3	3.5	34.0	5,8.VII	-15.5	16.1	88	70	86	81	1.4	5.6	1.7	2.9	6.3	6.8	5.8	6.3

Głębokie

$\varphi = 52°39'$ $\lambda = 18°26'$

I	–	–	–	–	-1.8	-0.1	-1.1	-1.0	–	-4.1	–	–	(-19.5)	16	90	87	88	88	0.4	0.7	0.6	0.6	9.4	8.5	8.2	8.7
II	–	–	–	–	1.5	4.9	2.6	2.9	–	0.0	–	–	-3.9	24	–	–	–	–	–	–	–	–	8.8	8.4	7.8	8.3
III	–	–	–	–	0.7	6.3	2.9	3.2	–	-1.4	–	–	-7.6	11	86	65	84	78	0.9	3.8	1.2	2.0	7.2	7.0	5.1	6.4
IV	–	–	–	–	4.4	11.5	6.6	7.3	–	1.6	–	–	-6.6	13	89	60	82	77	0.9	6.4	1.9	3.1	7.7	7.5	6.8	7.3
V	–	–	–	–	8.6	14.8	9.7	10.7	–	4.6	–	–	-0.2	6	84	56	80	73	2.0	8.4	2.7	4.4	7.5	7.9	6.9	7.4
VI	–	–	–	–	14.8	21.3	15.8	16.9	–	8.3	–	–	4.6	24	–	–	–	–	–	–	–	–	6.9	6.5	6.4	6.6
VII	–	–	–	–	17.2	22.0	17.5	18.6	–	14.0	–	–	9.8	29	90	71	88	83	2.2	9.4	2.5	4.7	8.1	8.1	7.1	7.8
VIII	–	–	–	–	14.5	19.9	15.0	16.1	–	11.4	–	–	7.1	29,30	91	70	90	84	1.5	7.4	1.9	3.6	7.0	8.4	6.2	7.2
IX	–	–	–	–	9.6	14.9	11.1	11.7	–	7.1	–	–	-0.6	27	93	71	88	84	0.9	5.7	1.7	2.8	6.8	8.7	6.9	7.4
X	–	–	–	–	5.7	12.1	8.1	8.5	–	4.2	–	–	-0.7	2	95	76	91	87	0.5	3.8	1.0	1.8	7.0	7.8	5.4	6.7
XI	–	–	–	–	3.4	6.4	3.9	4.4	–	–	–	–	–	–	90	78	89	86	0.7	2.2	0.8	1.2	8.5	8.6	7.6	8.2
XII	–	–	–	–	-2.0	-0.4	-1.2	-1.2	–	–	–	–	–	–	86	85	87	86	0.6	0.8	0.6	0.7	8.4	8.6	7.2	8.1
Rok	–	–	–	–	6.4	11.1	7.6	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.0	6.8	7.5

Łagiewniki

$H_s = 80\ m$ $h_w = 10\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (°D, °mD)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10	Max>25°	0.1 ≤ < 1.0	1.0 ≤ < 10.0	10.0 ≤	10 ≤ < 15	15 ≤					
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32.3	9.0	13	–	–	–	–	9	7	·	–	–	·	2	18	16
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52.0	17.7	18	–	–	–	–	16	13	1	–	–	·	4	8	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43.8	12.0	28	–	–	–	–	10	6	1	–	–	·	7	8	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.5	12.5	25	–	–	–	–	9	4	2	–	–	·	2	7	8	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.4	10.0	20	–	–	–	–	10	6	1	–	–	·	1	5	5	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	67.5	26.5	4	–	–	–	–	9	5	3	–	–	·	2	9	3	·
VII	6.5	1.3	4.5	2.1	5.5	1.6	5	1.7	3.5	2.3	9	2.3	11.5	2.0	21.5	3.3	26	1.7	150.4	55.2	16	–	–	–	–	18	16	2	·	·	–	7	–	–	·
VIII	2.5	1.4	3	2.3	·	·	8	1.1	9	1.5	13	2.3	17.5	1.9	18	1.4	22	1.3	66.3	19.1	10	–	–	–	–	8	7	2	·	·	–	·	–	–	·
IX	0.5	1.0	·	·	·	·	4	1.6	9.5	2.6	19.5	2.6	1.8	3.4	10.5	3.6	28	2.0	100.6	34.3	23	–	–	–	–	17	15	2	·	·	–	1	–	–	·
X	1	1.0	·	·	·	·	4.5	1.2	5.5	1.4	1.9	2.5	1.9	3.6	4	2.2	4.0	1.5	6.2	2.1	20	–	–	–	–	5	4	·	·	·	–	·	–	–	·
XI	3.5	5.4	4	3.0	1.0	1.6	10.5	1.8	5.5	1.1	9	2.3	1.3	4.3	2.5	3.8	3.2	1.8	52	1.4	28	–	–	–	–	6	3	·	·	·	–	·	–	–	·
XII	3	2.0	4	1.0	4	1.5	2.5	1.0	4	1.9	1.8	2.3	1.5	3.6	7.5	1.9	3.5	1.5	21.1	8.5	14	–	–	–	–	1.0	3	·	1	·	–	·	3	1.5	7
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	603.3	55.2	16.VII	–	–	–	–	127	89	14	–	–	–	13	–	–	23

Wieniec – Zdrój

$H_s = 82\ m$ $h_w = 13\ m$

I	·	·	3.5	2.4	5	3.0	0.5	3.0	2	2.0	8	3.2	2.4	3.5	3	3.7	4.7	1.6	35.4	10.9	31	22	–	4	–	11	7	1	·	·	7	·	3	22	19
II	·	·	·	·	1	1.0	2	3.0	9	3.6	10	2.2	7	4.6	6	3.5	4.9	1.4	63.0	20.3	18	17	–	·	–	20	11	2	·	·	4	·	·	13	2	
III	2	1.0	1	1.0	1.1	3.4	8	6.0	6	4.3	1	1.0	1.4	3.8	6	4.7	4.4	2.1	43.3	12.1	28	19	–	·	–	7	6	2	2	·	4	·	9	8	1.3	
IV	1.4	1.9	1	1.0	4	2.5	·	·	0.5	5.0	3	4.0	10.5	1.5	5	3.0	5.2	0.9	24.1	9.7	30	11	–	·	–	10	6	·	·	·	4	1	8	10	·
V	1.3	2.2	7	2.0	2.5	1.4	2.5	2.2	3	4.3	·	·	6	4.5	7	3.0	5.2	1.2	33.4	11.1	9	4	–	·	–	11	4	1	·	·	2	1	6	9	·
VI	5	2.2	1	1.0	·	·	5	4.2	2	1.0	4	3.5	11.5	3.4	7.5	2.9	5.4	1.2	77.2	38.3	4	·	–	·	–	8	7	2	·	·	3	2	13	5	·
VII	1	1.0	3	3.0	7	2.4	1	3.0	3	1.7	1.5	2.3	21.5	2.8	7	3.3	4.8	1.3	147.5	37.0	12	·	–	·	–	20	14	4	·	·	1	3	6	10	·
VIII	·	·	·	·	1	2.0	1	3.0	6	4.2	5.5	2.6	17.5	3.1	7	3.3	5.5	1.3	104.3	24.7	16	·	–	·	–	13	11	5	·	·	·	4	6	7	·
IX	·	·	·	·	·		·	·	2.5	2.6	16.5	3.2	20.5	3.9	4.5	2.8	4.6	1.7	63.1	14.2	23	2	–	·	–	18	15	1	·	·	5	·	3	12	·
X	·	·	·	·	·		·	·	3	2.3	9.5	3.0	1.7	3.9	1.5	4.3	6.2	1.2	11.9	4.2	1	3	–	·	–	12	3	·	·	·	10	·	5	6	·
XI	2.5	3.8	3	4.7	4.5	4.1	2	3.0	1.1	4.5	6	3.7	13.5	4.3	1.5	4.8	4.6	2.1	18.7	5.3	24	9	–	·	–	9	4	·	·	·	5	·	4	17	·
XII	2	3.0	·	·	5	2.8	·	·	2	3.0	1.2	3.0	1.8	3.5	1	7.0	5.3	1.4	32.6	10.2	14	23	–	6	–	15	9	1	1	·	4	·	2	18	11
Rok	39.5	1.3	19.5	1.3	4.1	1.9	22	2.3	5.0	3.2	7.7	2.6	18.1	3.6	5.7	3.8	6.0.8	1.4	661.5	38.3	4.VI	110	–	40	–	154	97	19	3	·	49	11	65	137	33?

Nur

$H_s = 108\ m$ $h_w = 12\ m$

I	3	2.5	7	5.8	4.5	3.4	4.5	3.7	6.5	2.4	2.1	3.6	1.7	3.8	14.5	3.2	1.5	3.0	29.9	6.6	6	24	13	5	·	11	8	·	3	·	–	·	1	17	–
II	5.5	2.5	6.5	2.5	6.5	1.7	11.5	1.8	11.5	2.0	8	1.9	1.5	2.0	4.5	4.0	1.5	1.8	63.0	7.2	9	13	3	·	·	21	16	·	·	·	–	·	·	19	–
III	13.5	5.8	1.5	1.7	6	6.2	1.2	5.5	1	4.0	7	2.4	1.2	4.7	11.5	3.6	1.5	3.5	24.8	15.2	17	26	8	2	·	5	4	1	4	·	–	·	11	7	–
IV	11.5	3.9	1.7	2.6	8.5	1.1	1.5	2.3	5	2.6	2	2.5	1	3.0	12.5	3.4	3.1	1.8	20.1	4.3	17	7	·	·	4	9	8	·	1	·	–	3	6	6	–
V	19.5	2.9	1.6	3.0	5	1.8	4.5	2.6	2	1.5	4.5	2.4	0.5	6.0	1.1	2.4	3.0	1.8	17.5	7.1	7	2	·	·	2	6	4	·	·	·	–	2	8	11	–
VI	1.1	2.9	8.5	1.8	1	2.0	8.5	2.0	4.6	2.3	5	3.8	13.5	3.1	1.1	3.0	2.7	1.9	16.8	5.1	4			·	8	9	4	·	1	·	–	2	9	5	–
VII	3.5	2.4	1.0	1.5	13.5	2.5	6.5	1.3	5	1.6	8.5	1.3	1.0	2.6	9	4.4	2.7	1.5	102.8	14.4	24			·	11	16	16	2	2	·	–	11	5	11	–
VIII	6	2.3	·	·	5	1.4	6	2.2	2	2.0	11.5	2.6	1.2	2.2	18.5	2.4	3.2	1.5	98.8	21.0	17	·	·	·	3	16	12	5	·	·	–	2	2	7	–
IX	1.5	1.0	4	1.5	0.5	2.0	4.5	1.3	1.0	2.4	6.5	2.5	2.2	5.3	1.0	3.1	3.1	2.2	83.0	20.0	23	·	·	·	1	15	11	2	1	1	–	1	2	11	–
X	1	3.0	2	1.5	2	1.2	5	2.3	10.5	2.3	19.5	2.5	1.4	3.8	9	2.2	3.0	1.8	12.6	3.2	22					9	4	·	·	·	–	·	4	10	–
XI	6	1.6.0	9.5	2.8	1.5	2.6	9.5	2.6	2.5	1.2	7.5	2.9	5.5	6.6	9.5	3.5	2.5	3.1	22.4	9.7	28	11	1	·	·	11	6	·	3	2	–	·	2	18	–
XII	6	5.8	5	3.4	5.5	1.9	3	1.0	1.1	2.2	21.5	3.8	11.5	4.9	4.5	6.1	2.5	2.7	26.7	8.0	8	27	11	4	·	10	7	·	4	1	–	·	3	16	–
Rok	88	4.2	100.5	2.3	7.3	2.3	7.7	2.4	7.1.5	2.2	122.8	2.7	13.4	4.0	12.5.5	3.4	30.3	2.2	518.4	21.0	17.VIII	110	36	11	30	138	100	10	19	4	–	21	53	138	–

Głębokie

$H_s = 85\ m$ $h_w = 11\ m$

I	1	1.0	5.5	7.8	5	6.1	6	3.2	8.5	3.7	4.2.5	4.2	20.5	7.2	·	·	4	4.9	27.5	8.5	31	25	–	3	–	13	6	·	4	1	–	·	·	24	16
II	1.5	2.7	1	3.0	4	5.2	2	3.5	16.5	4.4	3.4	3.4	1.6	4.8	5	2.3	4	3.7	47.9	17.2	22	14	–	·	–	18	10	1	3	1	–	·	·	17	·
III	1.5	3.3	3.5	8.9	1.4	8.1	1.5	4.9	1.3	3.5	16.5	3.1	2.2	4.8	5.5	3.5	2	4.8	41.0	10.3	28	18	–	1	–	11	7	1	7	3	–	·	2	11	1
IV	12.5	4.6	6	3.4	3.5	2.7	2.5	3.2	7	3.9	13.5	2.9	2.5	3.1	1.5	2.9	5	3.1	50.2	19.5	22	7	–	·	–	11	5	3	1	·	–	2	2	14	·
V	8.5	6.0	5.5	5.2	2	4.0	4	5.5	7.5	2.1	2.2	2.2	27.5	3.2	11	3.0	5	3.2	26.0	12.0	20	1	–	·	–	9	5	1	4	·	–	·	1	12	·
VI	4	3.9	·	·	1	6.0	8	4.4	4	2.0	2.0	2.4	3.4.5	3.0	9.5	3.4	12	2.6	48.1	18.2	9	·	–	·	–	7	6	2	·	·	–	1	3	13	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	160.5	55.2	16	·	–	·	–	18	17	3	–	–	–	7	1	16	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	60.1	16.4	15	·	–	·	–	9	8	2	–	–	–	·	·	13	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	96.8	33.7	23	·	–	·	–	21	15	2	–	–	–	2		11	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.4	3.5	21	1	–	·	–	6	4	·	–	–	–	·	4	15	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.5	4.2	24	–	–	–	–	8	4	·	–	–	–	·	1	19	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	15.8	6.0	14	–	–	–	–	13	4	·	–	–	–	·	2	21	11
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	592.6	55.2	16.VII	–	–	–	–	144	91	15	–	–	–	12	16	186	88

Pośwętne

$\varphi = 52°38'$ $\lambda = 20°23'$

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N			
					Średnio				Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	–	–	–	–	-2,1	-0,4	-4,7	-4,5	0,8	-4,2	7,8	7	-16,6	16	90	87	88	88	0,5	0,8	0,6	0,5	8,5	7,9	6,0	7,5
II	–	–	–	–	1,5	4,0	2,3	2,5	4,9	0,2	9,2	14	-2,8	4,28	92	82	88	87	0,6	1,5	0,9	1,0	8,3	8,0	7,4	7,9
III	–	–	–	–	-0,3	5,3	2,2	2,4	6,9	-1,7	16,9	31	-7,0	9	85	65	82	77	1,0	3,8	1,4	2,0	4,7	4,7	3,9	4,4
IV	–	–	–	–	4,7	12,8	7,2	8,0	14,0	2,0	26,4	30	-6,7	10	86	49	78	71	1,3	8,9	2,4	4,2	6,8	5,9	4,5	5,7
V	–	–	–	–	8,7	13,9	9,7	10,5	15,7	5,0	27,2	19	-1,0	6	83	61	80	75	2,0	7,3	2,6	4,0	4,5	6,6	4,9	5,3
VI	–	–	–	–	14,9	21,0	15,8	16,9	22,6	10,4	28,9	11,19	5,0	3	82	56	82	73	3,0	11,9	3,4	6,1	4,1	5,1	3,4	4,2
VII	–	–	–	–	15,4	22,1	17,5	18,4	23,7	13,5	34,2	8	9,9	29	90	65	87	81	1,9	10,3	2,6	4,9	6,5	6,3	5,3	6,0
VIII	–	–	–	–	13,8	19,5	15,6	16,1	21,1	11,2	25,7	11	6,4	24	93	69	87	83	1,1	7,4	2,3	3,6	6,2	6,8	4,9	5,9
IX	–	–	–	–	9,4	14,8	11,1	11,8	15,8	7,7	27,2	9	0,2	26	90	69	85	81	1,2	5,9	2,2	3,1	6,3	7,1	4,5	6,0
X	–	–	–	–	6,0	11,8	8,2	8,6	12,7	4,7	20,5	19	0,5	3	91	73	87	84	0,9	4,1	1,5	2,2	6,3	6,4	3,9	5,5
XI	–	–	–	–	3,6	6,0	4,1	4,4	7,2	1,9	15,7	5	-7,7	29,30	90	80	88	86	0,7	1,9	1,0	1,2	8,2	7,4	7,4	7,7
XII	–	–	–	–	-2,1	-0,5	-1,5	-1,4	0,4	-4,0	6,3	9	-13,6	17	89	86	91	89	0,6	0,8	0,4	0,6	7,2	7,7	6,4	7,1
Rok	–	–	–	–	6,2	10,9	7,5	8,0	12,2	3,9	34,2	8.VII	-16,6	16.1	88	70	85	81	1,2	5,4	1,8	2,8	6,4	6,6	5,1	6,0

Międzychód

$\varphi = 52°35'$ $\lambda = 15°53'$

I	–	–	–	–	-0,8	1,3	-0,2	0,0	2,7	-3,0	11,3	6	-15,3	16	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1,8	5,4	2,9	3,2	7,1	0,0	11,4	5	-5,6	25	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	0,8	8,0	3,8	4,1	10,2	-0,7	17,8	13	-7,7	2	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	3,5	12,2	6,5	7,2	13,9	0,7	24,2	28	-6,6	14	89	53	81	74	0,9	7,6	2,0	3,5	–	–	–	–
V	–	–	–	–	8,9	15,1	10,0	11,0	17,0	3,8	26,0	19	-3,1	7	77	50	72	66	2,9	9,6	3,8	5,4	–	–	–	–
VI	–	–	–	–	14,7	21,9	17,2	17,8	24,1	10,2	31,8	19	5,6	8,13	84	53	76	71	2,8	13,8	5,2	7,3	–	–	–	–
VII	–	–	–	–	17,1	22,0	18,5	19,0	24,1	13,5	33,8	4	7,5	3	89	71	86	82	2,3	9,2	3,5	5,0	–	–	–	–
VIII	–	–	–	–	14,0	19,3	15,0	15,8	21,0	11,3	27,8	11	6,7	23	91	65	86	81	1,5	8,3	2,6	4,1	–	–	–	–
IX	–	–	–	–	9,7	14,7	10,9	11,6	16,5	6,9	28,3	8	-2,0	26	92	73	88	84	1,0	5,0	1,7	2,6	–	–	–	–
X	–	–	–	–	6,8	12,5	8,6	9,1	13,7	4,8	19,8	10,19	-3,1	2	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3,0	6,3	4,0	4,3	7,6	1,4	15,9	5	-7,1	21,30	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1,1	0,6	-0,5	-0,4	2,6	-3,1	10,2	8	-14,8	16	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	6,5	11,6	8,1	8,6	13,4	3,8	33,8	4.VII	-15,3	16.1	–	–	–	–	–	–	–	–	–	–	–	–

Przebędowo

$\varphi = 52°35'$ $\lambda = 17°01'$

I	–	–	–	–	-1,3	0,8	-0,5	-0,4	1,5	-3,1	9,8	6	-17,6	16	86	83	86	85	0,7	1,1	0,8	0,9	8,8	8,7	6,1	8,0
II	–	–	–	–	1,6	5,0	2,8	3,0	5,7	0,1	9,4	14	-5,6	27	90	78	87	85	0,7	2,0	1,0	1,2	–	–	–	–
III	–	–	–	–	1,0	7,2	3,4	3,8	8,4	-0,5	16,2	26	-6,8	3	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	4,4	12,0	7,2	7,7	13,6	1,6	24,5	28	-6,7	14	85	51	76	71	1,2	7,8	2,6	3,9	–	–	–	–
V	–	–	–	–	8,7	14,6	10,3	11,0	16,3	4,4	25,0	19	-1,4	7	76	49	69	65	2,8	9,4	4,2	5,5	–	–	–	–
VI	–	–	–	–	13,3	21,5	17,0	17,7	23,3	10,4	30,6	11	5,4	15	80	53	74	70	3,6	12,8	5,5	7,3	6,2	6,8	6,3	6,4
VII	–	–	–	–	17,4	21,9	18,0	18,8	24,1	13,9	31,6	5	8,6	3	–	–	–	–	–	–	–	–	6,7	5,8	6,4	6,3
VIII	–	–	–	–	14,5	19,3	14,8	15,8	21,5	11,1	28,9	16	5,8	23	–	–	–	–	–	–	–	–	6,2	6,9	6,9	6,7
IX	–	–	–	–	9,7	14,6	10,4	11,3	16,0	6,9	27,1	8	-0,8	27	91	72	88	84	1,1	5,2	1,6	2,6	7,2	7,5	5,3	6,7
X	–	–	–	–	6,8	12,2	8,2	8,8	13,1	4,6	20,1	19	-2,3	2	92	75	88	85	0,8	3,8	1,4	2,0	7,2	6,5	5,5	6,4
XI	–	–	–	–	3,4	6,4	4,2	4,6	7,2	1,7	16,8	5	-7,0	30	89	80	88	85	0,9	2,2	1,1	1,4	8,1	8,1	7,4	7,9
XII	–	–	–	–	-1,9	0,0	-0,9	-0,9	1,2	-3,7	8,7	8	-14,5	17,18	94	92	93	93	0,3	0,5	0,4	0,4	7,8	7,9	7,0	7,6
Rok	–	–	–	–	6,6	11,3	7,9	8,4	12,7	4,0	31,6	5.VII	-17,6	16.1	–	–	–	–	–	–	–	–	–	–	–	–

Wyszków

$\varphi = 52°35'$ $\lambda = 21°27'$

I	–	–	–	–	-2,5	-0,5	-1,9	-1,7	0,3	-4,5	6,0	6	-17,5	16	92	89	92	91	0,4	0,7	0,4	0,5	8,5	8,2	6,4	7,7
II	–	–	–	–	0,9	3,5	1,7	2,0	4,4	-0,4	9,6	14	-5,6	28	94	85	94	91	0,4	1,3	0,4	0,7	8,9	8,4	7,0	8,1
III	–	–	–	–	-0,8	5,3	1,3	1,8	6,5	-2,9	16,2	31	-10,0	4	84	66	86	78	1,0	3,7	1,1	1,9	5,4	5,0	3,5	4,6
IV	–	–	–	–	5,6	13,2	7,4	8,4	14,2	2,8	26,4	30	-6,7	10	87	56	84	76	1,4	7,9	1,8	3,7	5,8	5,5	5,8	5,7
V	–	–	–	–	9,5	14,3	9,2	10,6	16,6	5,3	25,8	19	-0,6	2	86	68	88	81	1,7	6,2	1,6	3,2	5,5	7,5	4,6	5,9
VI	–	–	–	–	15,7	22,1	13,5	17,2	23,6	10,3	30,8	11	4,9	27	83	63	85	77	3,1	10,8	2,7	5,5	4,1	5,4	4,0	4,5
VII	–	–	–	–	16,9	23,0	17,3	18,6	24,5	13,6	32,5	8	8,9	1	89	68	90	82	2,2	10,1	2,2	4,8	7,1	6,6	5,9	6,5
VIII	–	–	–	–	14,0	19,9	14,9	15,9	21,5	11,2	30,2	12	5,1	24	94	67	90	84	1,1	8,5	1,7	3,7	5,5	7,7	4,3	5,8
IX	–	–	–	–	9,9	14,8	10,5	11,3	16,5	7,3	27,9	9	-1,0	27	95	72	92	86	1,0	5,5	1,1	2,5	7,2	7,5	6,1	6,9
X	–	–	–	–	5,5	11,8	7,5	8,1	12,9	3,7	20,2	19	-1,0	3	95	73	92	87	0,5	4,1	0,9	1,8	6,4	6,2	4,9	5,8
XI	–	–	–	–	2,9	5,9	3,7	4,0	7,2	1,6	16,3	8	-9,4	30	94	81	91	89	0,4	2,0	0,8	1,1	8,0	7,7	7,3	7,8
XII	–	–	–	–	-2,6	-0,5	-2,0	-1,8	0,5	-4,6	7,3	13	-14,7	16	91	85	92	89	0,4	0,8	0,3	0,5	7,5	8,8	6,6	7,6
Rok	–	–	–	–	6,2	11,1	7,1	7,9	12,3	3,6	32,3	8.VII	-17,5	16.1	90	73	90	84	1,1	5,1	1,2	2,5	6,7	7,0	5,6	6,4

Pasiwętne

$H_s = 100\,m$ $h_w = 14\,m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD (mm) Suma	Max	Data	Liczba dni: Temperatura Max<0	Max>0	Min<-10	Min<-25	Opad ≥0.1	≥1.0	≥10.0	Wiatr ≥6	≥11	≥15	●	●	●	●	≡
I	1.5	4.7	6.5	5.9	4.5	4.6	8	2.8	5.5	3.9	2.6	4.6	23.5	7.1	10.5	7.1	7	5.1	21.9	8.3	31	24	18	6	.	10	6	.	7	.	.	.	2	17	21
II	3	2.2	4.0	3.0	2	3.0	4.5	2.6	1.2	3.6	2.3.5	3.4	19.5	5.0	4.5	5.9	5	3.6	70.1	18.7	18	13	1	.	.	16	12	4	3	.	.	.	1	12	3
III	6	5.7	1.3	2.5	14.5	5.7	14.5	5.1	9.5	3.5	4.5	6.3	16.5	7.5	10.5	5.9	4	5.1	24.5	8.1	15	20	5	.	.	7	4	.	10	1	.	.	10	5	1
IV	1.6	4.3	8.5	3.8	10.5	2.2	1.5	2.3	3	5.0	8.5	4.3	1.5	2.1	8.3	3.9	4	3.4	12.7	8.6	30	10	.	.	2	7	2	.	3	.	.	.	7	6	.
V	15.5	3.8	14.5	4.6	10.5	2.2	5	3.8	4	3.0	4	2.5	1.3	4.7	19.5	4.1	7	3.6	21.3	10.4	9	2	.	.	2	4	3	1	1	.	.	.	7	8	.
VI	11.5	3.7	10.5	3.3	8.5	2.9	5.5	2.8	5	2.6	7.5	5.3	1.9	3.8	19.5	4.5	3	3.7	75.6	21.5	24	.	.	.	8	10	7	3	.	.	.	6	10	5	.
VII	8.5	2.5	7.5	2.5	8	2.6	6	3.2	6	3.7	10.5	2.9	19.5	3.4	2.2	3.9	5	3.1	143.5	32.5	27	.	.	.	11	17	15	5	.	.	.	11	4	9	.
VIII	4.5	2.0	4.5	2.0	2.5	2.2	6	2.3	7.5	3.7	17.5	4.7	3.4.5	4.2	2.6	3.4	2	3.8	68.1	24.2	14	.	.	.	2	11	10	2	3	.	.	4	8	8	.
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	106.2	24.6	15	.	.	.	2	17	13	4	-	-	-	1	2	9	.
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.7	3.4	20	.	.	.	.	5	2	.	-	-	-	.	4	4	.
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16.2	5.7	28	11	2	.	.	9	4	.	-	-	-	.	2	18	.
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28.9	6.9	8	23	11	5	.	17	8	.	-	-	-	.	3	16	7
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5962	32.5	27.VII	103	31	11	27	130	86	16	-	-	-	86	37	117	32

Międzychód

$H_s = 40\,m$ $h_w = 10\,m$

I	.	.	2	3.0	7	2.4	3	2.0	5	1.2	17.5	2.3	3.8	3.5	7.5	5.0	13	2.6	25.6	6.1	31	22	6	2	.	9	8	.	1	.	.	.	.	-	-
II	2	2.0	3	2.3	.	.	5	1.8	1.6	2.5	20.5	2.5	19.5	2.9	4	2.5	1.4	2.1	27.9	5.5	18	11	.	.	.	10	9	.	1	.	.	.	.	-	-
III	.	.	2	2.0	1.4	3.2	1.2	3.3	1.2	2.0	1.0	2.9	1.6	6.2	5	4.0	2.2	3.1	38.3	15.2	17	17	.	.	.	6	6	1	6	.	.	.	.	-	-
IV	9	2.6	9	3.4	3	1.7	3	2.0	1	1.0	9.5	1.5	15.6	3.4	8	2.9	3.2	1.7	14.1	7.2	25	13	.	.	.	4	4	.	4	.	.	.	.	-	-
V	7	2.6	6	4.5	4	2.8	9	3.1	5.5	2.4	9	2.4	1.9	3.6	8.5	3.8	2.5	2.4	13.3	7.2	23	7	.	.	2	3	3	.	2	.	.	1	.	-	-
VI	4.5	4.0	5	2.2	5.5	2.2	6.5	2.7	6.5	1.9	1.2	2.8	2.2.5	3.4	8.5	3.2	2.2	2.2	44.1	10.5	24	.	.	.	1.5	6	8	4	.	.	.	2	.	-	-
VII	3.5	2.3	.	.	.	.	3.5	2.9	7	2.1	1.4	2.1	3.4.5	2.6	12.5	3.1	1.8	2.0	186.8	32.5	10	.	.	.	11	17	17	7	.	.	.	10	.	-	-
VIII	1	5.0	.	.	.	.	3	3.0	3	1.3	23.5	3.0	3.9	2.5	3.5	3.7	2.0	2.2	61.0	11.3	31	.	.	.	2	15	15	1	.	.	.	1	.	-	-
IX	.	.	.	.	.	.	.	.	6	4.0	20.5	3.4	31.5	3.6	11	3.4	2.1	2.7	51.5	7.2	21	2	.	.	1	14	14	.	3	.	.	.	.	-	-
X	.	.	.	.	.	.	.	.	8	2.1	2.2	2.2	2.8	3.1	2	2.2	3.3	1.7	15.0	4.8	19	1	.	.	.	6	4	.	.	.	.	.	.	-	-
XI	3	3.3	2	2.5	7	2.6	14.5	2.3	14.5	1.7	1.9	2.1	1.7	6.8	2	2.5	1.1	2.8	12.5	4.8	28	9	.	.	.	3	3	.	.	.	.	.	.	-	-
XII	4	2.8	1	3.0	5.5	2.2	3.5	1.7	7	1.0	2.4	2.3	2.8	3.2	5	4.3	1.5	2.2	22.6	4.0	30	20	5	3	.	8	7	.	.	.	.	.	.	-	-
Rok	3.1	2.0	3.0	1.9	4.6	4.6	6.3	2.1	9.1.5	1.9	2.0.1.5	2.5	3.0.8.5	3.7	7.7.5	3.4	2.4.6	2.3	5.1.2.7	3.2.5	10.VII	10.2	11	5	29	10.3	9.8	10	14	.	.	47	.	-	-

Przebędowo

$H_s = 82\,m$ $h_w = 11\,m$

I	4	3.2	9.5	4.5	5.5	4.5	3.5	2.4	1.3	4.5	2.8.5	5.4	2.0	5.4	.	.	9	4.4	2.3.8	5.0	31	21	11	2	.	9	7	.	.	.	.	.	4	2.2	1.8
II	3.5	3.0	1.5	2.3	7.5	2.9	6	3.2	2.1.5	4.1	1.6.5	3.7	1.7.5	4.3	2	1.8	8	3.4	3.4.0	10.6	18	12	.	.	.	13	8	1	.	.	.	.	.	-	.
III	6	2.5	8	2.9	17.5	4.0	8	3.1	12.5	3.1	8.5	4.0	12.5	6.0	3	5.0	1.7	3.2	2.2.9	10.9	17	17	.	.	.	6	5	1	.	.	.	.	.	-	.
IV	2.4	3.4	1.1	2.2	1.5	1.3	1	1.5	3	3.8	5.5	4.3	1.0	4.5	1.1	4.0	2.3	2.6	6.9	3.1	16	11	.	.	.	5	3	.	.	.	.	.	.	-	.
V	18.6	3.2	17.5	3.7	5.5	2.3	5	2.8	4.5	4.3	6.5	4.7	9	4.6	12.5	4.0	1.4	3.2	19.8	10.5	6	3	.	.	.	8	4	1	.	.	.	.	.	-	.
VI	9.5	2.1	9	2.3	7	3.3	5	2.8	2.5	3.8	11.5	3.6	1.6	4.0	11.5	2.5	1.8	2.5	5.1.3	16.3	24	.	.	.	12	7	7	2	.	.	.	.	4	1.1	.
VII	8.5	3.2	1.1	1.7	5	2.6	4.5	1.1	9.5	2.7	10.5	3.8	1.7	2.9	4.2	4.0	1.5	2.4	157.0	23.4	21	.	.	.	1.3	19	1.8	4	.	.	.	8	2	1.1	.
VIII	0.5	1.0	2.6	1.0	4.5	1.6	5.5	2.6	1.3.6	3.7	2.4	3.3	2.3.5	3.1	7	2.3	1.2	2.8	56.6	15.5	21	.	.	.	4	1.2	8	2	1	1	.	2	.	1.1	.
IX	1	1.0	1.5	1.0	1.5	1.0	3.6	2.8	2.1	3.4	2.4.5	3.7	2.0	4.8	3	2.3	1.4	3.1	9.8.0	3.3.8	23	2	.	.	1	16	1.6	2	.	.	8	2	.	7	.
X	.	.	1.5	1.7	1	1.0	6.5	3.1	2.2.5	2.8	3.4	3.2	8	2.9	6.5	3.0	1.3	2.6	7.0	2.0	5.1.9	1	.	.	.	7	2	.	.	.	1.9	.	3	1.2	.
XI	3.5	5.0	2.3.5	3.1	1.1	2.4	1.6	2.7	1.2	2.7	6	4.8	9.6	5.6	3.5	6.1	2	3.4	10.7	3.1	27	10	2	.	.	5	5	.	4	.	7	.	2	1.9	.
XII	4	4.0	8	2.2	5.5	3.3	8.5	3.1	1.4.5	3.7	2.9	4.9	1.1.5	4.6	8	2.7	4	3.8	2.9.8	9.5	8	2.2	9	5	.	1.3	8	.	2	.	1.0	.	.	1.8	1.3
Rok	8.3	2.6	10.4.5	2.4	7.6	2.6	7.3	2.6	1.5.0	3.6	2.0.5	4.1	1.7.4.6	4.4	8.0	3.1	1.4.9	3.1	4.9.7.8	3.3.8	23.IX	9.9	2.2	7	3.0	1.2.0	9.1	1.3	4	1	.	1.3	.	-	3.1

Wyszków

$H_s = 96\,m$ $h_w = 10\,m$

I	.	.	6.5	5.7	8	4.2	4.5	1.7	4	3.1	3.1	3.0	1.8	4.8	3	7.2	2.1	3.0	2.5.3	6.4	5	2.5	1.2	5	.	9	8	.	1	.	4	.	2	1.7	-
II	6	2.8	2	2.0	7.5	2.5	7.5	2.6	8.5	4.5	1.7	2.7	6.5	6.1	3	2.7	2.6	2.0	4.5.7	10.3	18	16	2	.	.	1.9	1.1	4	1	1	4	.	1	1.5	-
III	9	2.7	6	3.7	4.6	6.8	5.5	2.7	2	2.5	1.3.5	3.3	1.0	5.4	1.7	5.2	1.4	3.7	2.4.9	12.5	15	22	5	.	.	4	4	1	4	1	1	.	9	8	-
IV	13.5	3.8	6.5	1.9	3	2.3	6	2.4	2.5	3.6	8	2.5	6.5	2.8	1.7	4.0	2.7	2.2	16.9	5.4	29	8	.	.	4	8	4	.	.	.	2	6	1.0	-
V	5	4.1	1.0	3.1	1.3	3.2	4	2.2	3	1.7	7.6	2.6	9	4.0	18.5	3.7	2.3	2.5	2.5.1	10.5	7	1	.	.	1	5	3	1	.	.	2	.	4	4.0	-
VI	9	2.6	6	2.8	3	1.3	4.5	3.2	2	1.5	1.6	2.6	1.5	3.3	9.5	3.6	2.6	2.1	4.3.3	12.5	4	.	.	.	1.0	1.1	8	1	.	.	.	6	9	1	-
VII	6	1.8	2.5	1.3	7	2.4	10.5	2.2	4.5	3.0	12.5	3.2	1.6	3.4	5	2.6	2.9	1.9	8.3.9	17.2	16	.	.	.	1.4	1.5	1.3	3	.	.	2	6	3	1.3	-
VIII	2	4.0	1.5	2.6	3	1.3	0.5	3.0	2.2.5	3.9	1.9.5	3.2	8.5	3.6	3.4	2.3	7.2.8	1.6.1	1.0	.	.	.	4	1.1	9	4	.	.	3	3	3	6	-
IX	4	2.0	4	3.0	0.5	3.0	3.5	2.7	6	2.6	2.5	3.5	1.9.5	4.0	5.6	6.4	2.5	2.6	4.1.2.1	3.4.0	23	1	.	.	2	4.8	1.4	3	.	.	2	.	1	1.2	-
X	1.5	1.0	1.5	2.3	1	1.0	3	2.8	8.5	1.5	2.7.6	2.7	1.0.5	3.6	3.5	1.3	3.6	1.5	5.0	1.2	20.22	2	.	.	.	7	2	.	.	.	7	.	3	8	-
XI	8.5	6.6	8.5	2.5	1.9	2.8	9	3.8	5.5	1.7	1.3	3.3	1.1.5	5.0	3	6.7	1.9	3.1	1.3.7	6.7	28	1.1	1	.	.	3	5	.	1	.	3	.	3	2.1	-
XII	1.2	2.1	5.5	2.9	1.8	2.0	1	3.0	3.5	2.6	3.3.5	3.0	7	5.2	4	6.4	1.7	2.6	3.0.8	10.4	8	2.6	1.0	5	.	1.2	8	1	2	.	5	.	8	1.7	-
Rok	7.8.5	2.8	5.7.5	2.3	7.5.5	2.9	5.2.5	2.7	5.2.5	2.4	2.3.2	3.1	1.4.9	4.2	9.2.5	4.4	2.0.7	2.5	4.0.9.5	3.4.0	23.IX	1.1.2	3.0	8	3.5	1.2.4	8.9	1.5	9	2	3.1	1.7	4.7	1.3.6	-

Trzemeszno

$\varphi = 52°34'$ $\lambda = 17°49'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.7	0.3	-4.0	-0.8	1.3	-3.6	9.5	6	-17.9	16	92	87	89	89	0.4	0.8	0.6	0.6	8.3	7.9	7.3	7.8
II	–	–	–	–	1.6	4.7	2.4	2.8	5.7	-0.3	9.3	14	-4.5	24	93	80	89	87	0.5	1.8	0.8	1.0	9.0	8.6	6.3	8.0
III	–	–	–	–	1.0	6.4	3.2	3.4	8.1	-0.9	15.5	13	-5.7	9	85	67	81	78	1.0	3.5	1.5	2.0	6.5	6.4	4.2	5.7
IV	–	–	–	–	5.2	12.0	7.1	7.8	13.1	2.4	23.8	28	-5.2	14	86	61	81	76	1.3	6.3	2.1	3.2	6.5	7.1	5.5	6.3
V	–	–	–	–	9.6	14.8	9.9	11.0	16.0	5.0	25.1	19	0.3	6	77	55	79	70	2.9	8.6	2.8	4.8	5.9	7.8	5.5	6.4
VI	–	–	–	–	14.9	21.3	17.8	18.0	23.8	10.9	30.7	19	6.8	26	81	57	75	71	3.4	12.0	5.5	7.0	5.5	6.1	6.0	5.9
VII	–	–	–	–	17.0	22.2	18.1	18.6	24.0	13.7	32.9	5	9.0	29	88	66	86	80	2.5	10.8	3.5	5.6	7.7	7.9	7.7	7.8
VIII	–	–	–	–	14.7	19.9	15.2	16.2	21.1	11.3	27.2	11	6.9	23	89	64	89	81	1.9	8.7	2.1	4.2	6.9	8.3	6.0	7.1
IX	–	–	–	–	9.4	14.5	10.7	11.3	16.0	7.1	27.0	8	-0.4	27	93	74	89	85	0.8	4.9	1.5	2.4	7.4	8.6	6.8	7.6
X	–	–	–	–	6.4	12.2	8.2	8.8	13.0	4.6	19.9	19	-1.3	2	94	74	91	86	0.6	3.9	1.0	1.8	7.7	7.4	5.5	6.7
XI	–	–	–	–	3.2	6.3	4.2	4.5	7.2	1.5	16.5	5	-7.7	30	92	81	89	87	0.6	2.1	0.9	1.2	8.6	8.6	8.3	8.5
XII	–	–	–	–	-4.8	0.0	-0.9	-0.9	1.2	-3.9	6.8	8	-14.4	17	88	89	90	89	0.6	0.7	0.6	0.6	8.5	9.7	7.5	8.3
Rok	–	–	–	–	6.6	11.2	7.9	8.4	12.5	4.0	32.9	5 VII	-17.9	16.1	88	74	86	82	1.4	5.3	1.9	2.9	7.4	7.8	6.3	7.2

Gniezno

$\varphi = 52°33'$ $\lambda = 17°36'$

I	–	–	–	–	-1.7	0.3	-4.0	-0.6	1.4	-3.7	9.3	6	-19.3	16	88	86	88	87	0.6	0.9	0.7	0.7	8.2	7.7	7.2	7.7
II	–	–	–	–	1.4	4.8	2.8	3.0	5.9	-0.1	9.4	13,14	-6.1	27	92	80	90	87	0.5	1.8	0.7	1.0	7.9	8.2	6.8	7.6
III	–	–	–	–	0.6	6.5	3.2	3.4	8.2	-4.0	16.2	13	-7.4	10	–	–	–	–	–	–	–	–	5.7	5.9	4.3	5.3
IV	–	–	–	–	4.7	11.6	6.9	7.5	13.1	2.1	23.9	28	-4.7	14	–	–	–	–	–	–	–	–	5.8	6.9	5.2	6.0
V	–	–	–	–	8.7	14.8	9.6	10.7	15.9	4.4	25.4	19	-0.4	7	84	57	78	72	2.4	8.3	2.8	4.5	5.6	6.7	4.8	5.7
VI	–	–	–	–	15.2	21.3	16.4	17.3	23.6	10.3	30.8	19	5.1	15	79	57	77	71	3.9	12.2	4.6	6.9	4.8	5.1	4.1	4.7
VII	–	–	–	–	17.0	21.9	17.6	18.5	23.6	13.5	31.8	4,5	9.9	3	87	69	85	80	2.8	9.8	3.4	5.3	7.4	7.2	6.5	7.0
VIII	–	–	–	–	13.8	19.5	15.0	15.8	21.1	11.0	26.9	11	6.4	23	–	–	–	–	–	–	–	–	6.8	7.4	5.1	6.4
IX	–	–	–	–	9.1	14.4	10.6	11.2	16.1	6.9	27.9	8	-0.0	27	92	74	87	84	0.9	5.1	1.7	2.6	7.5	8.0	4.7	6.7
X	–	–	–	–	6.4	12.1	8.3	8.8	13.1	4.7	20.1	10	-1.6	2	92	75	91	86	0.8	3.7	1.0	1.8	7.9	7.2	4.6	6.6
XI	–	–	–	–	3.2	6.2	3.9	4.3	7.2	1.3	16.5	5	-7.9	30	91	81	88	87	0.7	2.0	1.0	1.2	8.4	8.3	7.5	8.1
XII	–	–	–	–	-1.9	-0.1	-4.0	-4.0	1.3	-3.9	8.5	8	-14.5	17	90	89	89	89	0.4	0.6	0.5	0.5	7.9	8.8	7.1	7.9
Rok	–	–	–	–	6.4	11.1	7.7	8.2	12.5	3.8	34.8	4,5 VII	-19.3	16.1	–	–	–	–	–	–	–	–	7.0	7.3	5.7	6.7

Płock – Radziwie

$\varphi = 52°32'$ $\lambda = 19°40'$

I	1012.9	1025.3	994.7	1021.0	-1.7	0.4	-4.0	-0.8	1.4	-3.5	9.4	6	-17.1	16	89	85	86	87	0.6	0.9	0.7	0.7	8.0	8.0	6.8	7.6
II	1003.2	1028.3	977.5	1011.1	1.8	4.9	2.9	3.1	5.9	0.5	9.8	14	-3.4	24	91	79	86	85	0.5	1.8	1.1	1.2	8.4	8.3	7.2	8.0
III	1011.2	1027.9	986.0	1019.0	0.3	6.3	2.8	3.0	8.0	-4.0	16.6	31	-7.2	11	85	63	81	76	1.0	4.0	1.4	2.1	5.5	6.1	4.4	5.3
IV	1010.8	1023.9	986.3	1018.7	4.9	12.4	7.8	8.2	14.3	2.8	26.0	30	-4.6	10,14	86	59	77	74	1.3	6.8	2.7	3.6	6.0	6.1	4.6	5.6
V	1008.8	1022.3	992.3	1016.5	9.2	14.7	10.9	11.4	16.3	6.0	27.9	19	0.1	6	83	65	81	76	2.0	6.4	2.6	3.7	5.7	7.0	5.5	6.1
VI	1009.1	1024.4	998.4	1016.7	15.4	21.7	17.5	18.0	23.6	11.5	30.6	19,30	6.4	4	–	–	–	–	–	–	–	–	4.4	5.2	3.6	4.4
VII	1004.4	1015.5	992.9	1011.8	17.1	22.5	18.5	19.2	–	14.4	–	–	9.7	29	–	–	–	–	–	–	–	–	6.7	7.2	5.9	6.6
VIII	1006.4	1016.2	994.4	1014.0	14.1	20.0	15.4	16.2	–	11.8	–	–	7.4	23,30	92	71	89	84	1.4	7.2	1.9	3.5	5.8	7.2	4.3	5.8
IX	1004.7	1015.8	988.1	1012.3	9.3	15.0	11.2	11.7	–	8.0	–	–	0.4	27	92	72	88	84	0.9	5.5	1.7	2.7	7.2	8.0	5.0	6.7
X	1011.7	1022.8	997.4	1019.5	6.0	12.3	8.3	8.7	–	4.6	–	–	0.1	2	92	72	89	84	0.8	4.3	1.3	2.1	5.9	6.9	4.2	5.7
XI	1013.4	1033.3	995.5	1021.3	3.8	6.4	4.3	4.7	–	2.4	–	–	-7.0	29,30	89	79	86	85	0.8	2.2	1.1	1.4	8.2	7.7	7.6	7.8
XII	1007.1	1025.4	966.1	1015.2	-1.9	-0.1	-1.1	-1.0	–	-3.8	–	–	-14.8	16	90	87	90	89	0.5	0.8	0.6	0.6	7.1	8.5	6.3	7.3
Rok	1008.6	1033.3	966.1	1016.4	6.5	11.4	8.1	8.5	–	4.5	–	–	-17.1	16.1	–	–	–	–	–	–	–	–	6.6	7.2	5.4	6.4

Przybroda

$\varphi = 52°31'$ $\lambda = 16°40'$

I	–	–	–	–	-1.5	0.6	-0.8	-0.6	1.5	-3.5	10.0	6	-15.3	16	90	84	88	87	0.8	1.1	0.7	0.8	8.3	8.3	6.5	7.6
II	–	–	–	–	1.4	5.1	2.4	2.8	6.9	0.0	9.6	5	-4.1	27	93	76	90	86	0.5	2.1	0.8	1.1	7.7	7.6	5.2	6.8
III	–	–	–	–	0.9	6.9	3.2	3.6	8.5	-0.3	15.8	13	-5.3	10	86	62	80	76	1.0	4.2	1.6	2.3	5.4	5.2	3.0	4.5
IV	–	–	–	–	4.2	11.8	6.5	7.2	13.1	1.6	23.8	28	-5.1	14	86	50	77	71	1.2	7.7	2.5	3.8	5.7	6.4	3.8	5.3
V	–	–	–	–	9.3	14.7	9.7	10.8	16.1	4.2	25.7	19	-1.7	7,27	72	45	69	62	3.6	10.3	4.0	6.0	4.7	6.2	4.3	5.1
VI	–	–	–	–	14.1	21.0	17.1	17.3	23.2	9.7	30.9	19	5.6	3	80	50	70	67	3.3	14.0	6.4	7.9	4.9	4.4	4.0	4.4
VII	–	–	–	–	18.3	21.2	18.4	18.8	23.4	14.0	31.6	5	8.3	3	89	69	82	80	2.1	9.2	4.2	5.2	7.0	6.5	6.9	6.8
VIII	–	–	–	–	13.6	18.9	14.9	15.6	20.4	11.1	26.9	11	6.3	23	92	66	85	81	1.3	7.7	2.8	3.9	6.0	7.1	4.2	5.8
IX	–	–	–	–	9.8	14.5	10.6	11.4	15.9	7.0	26.9	8	-0.1	26,27	91	71	87	83	1.0	5.4	1.8	2.7	7.2	7.5	4.3	6.3
X	–	–	–	–	6.8	12.0	8.0	8.7	12.9	4.8	20.0	19	-1.8	2	93	75	90	86	0.7	3.7	1.2	1.9	7.6	7.0	4.5	6.4
XI	–	–	–	–	3.1	6.1	4.0	4.3	7.0	1.5	15.8	5	-6.3	30	91	81	88	87	0.7	2.0	1.0	1.2	8.1	8.4	7.4	8.0
XII	–	–	–	–	-1.5	0.0	-0.8	-0.8	1.2	-3.6	8.9	8	-14.8	17	90	88	90	89	0.5	0.7	0.6	0.6	7.8	8.2	6.3	7.4
Rok	–	–	–	–	6.4	11.1	7.8	8.3	12.4	3.9	31.6	5 VII	-15.3	16.1	88	68	85	80	1.4	5.7	2.3	3.1	6.7	6.9	5.0	6.2

Trzemeszno

$H_s = 105\ m$ $h_w = 20\ m$ 1967

	ROZKŁAD WIATRU (%)																		GPAD			LICZBA DNI (n)																			
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T			Opad			Wiatr													
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max ≤ 0°	Max ≤ 10°	Max > 25°	≥ 0.1 mm	≥ 1.0 mm	≥ 10.0 mm	≥ 12 m/s	≥ 15 m/s										
I	4.5	4.0	11.5	3.2	6	1.8	2.5	1.6	6.5	2.6	19.5	3.0	37.5	5.0	8	5.5		3.9	25.0	5.5	12	25	11	2	12	8		-	-	3	19	-									
II	5.5	4.5	7.5	1.8	3	2.3	2.5	2.0	1.6	3.2	18.5	3.5	24.5	3.9	8.5	5.1		3.3	45.5	16.0	18	16			18	12	1	1	-		14	-									
III	4.5	2.4	1.2	2.5	14.5	5.8	1.2	3.4	9	3.3	7.5	2.3	19.5	6.2	14	3.9		3.9	58.2	12.9	29	18			10	8	3	5	1	-	5	9	-									
IV	15.5	2.3	2.5	2.4	5.5	3.3	3	1.3	5	1.4	3.5	3.0	8	2.9	19.5	2.7	5	2.4	28.3	17.2	2.5	6			11	6	1	-	2	2	11	-									
V	10.5	2.0	2.7.5	2.9	12.5	1.9	2	3.5	3.5	1.9	2	1.5	11	4.5	24	3.1		2.8	30.6	12.1	6			1	9	4	2	-	2	-	8	-									
VI	9	1.6	15.5	2.9	8.5	2.8	6.5	2.8	2.5	2.6	7	3.6	24.5	3.7	16.5	3.2		3.1	37.9	18.0	4			12	9	6	1	-	2	5	10	-									
VII	14.5	2.0	11	2.1	8	2.5	1.5	1.3	3	2.8	10	2.6	2.6	4.2	19	3.8		3.1	212.1	55.2	14			13	21	18	7	-	9		18	-									
VIII	6	1.7	0.5	3.0	2.5	3.2	1	3.5	9.5	3.2	18.5	4.1	11	3.7	14	2.8		3.5	56.6	12.9	16			2	11	10	2	-	1	-	11	-									
IX	3.5	1.3	-	-	1	1.0	1	1.0	1.0	2.8	2.4	4.0	3.5.5	5.1	15	4.0		4.2	83.1	23.6	23	1		2	17	15	1	3	-	1	-	8	-									
X	0.5	2.0	-	-	-	-	2	2.2	1.1	2.8	32.5	3.7	3.5	3.4	12	2.1		3.2	8.8	1.8	4,20	1			8	4		-		2	9	-									
XI	4	4.5	11.5	5.1	2.2	2.8	12.5	2.3	1.2	2.2	10.5	2.8	14.5	8.1	3	9.2		4.1	12.7	8.1	2.8	10	3		8	4		3	-		2	21	-									
XII	3.5	1.6	1.2	2.9	9	3.0	4.5	2.3	9	3.8	1.8	4.9	2.9	5.7	8	4.4		4.3	3.4.0	8.2	1.4	22	10	3	15	7		3	-		1	20	-									
Rok	7.8.5	2.0	1.3.4	2.4	9.2.5	2.5	5.1	2.3	9.7	2.7	17.1.5	3.2	3.0.6	4.6	1.5.9.5	4.2	5	3.5	6.3.4.8	5.5.2	1.4.VII	9.9	2.4	5	3.0	1.4.9	1.0.2	1.8	1.5	1	-	1.7	2.0	1.5.8	-							

Gniezno

$H_s = 110\ m$ $h_w = 11\ m$

	2	7.5	1.0	7.6	5	2.6	1	1.0	1.6.5	2.0	17.5	4.5	2.9.5	3.4	6.5	4.5	5	3.7	2.8.9	5.7	3.1	24	9	2		11	7		5	1	-			3	2.0	-					
II	6	2.2	7	1.6	3.5	3.9	6.5	2.4	2.3	1.5	2.0.5	2.8	11	3.9	3.5	5.4	3	2.5	4.1.5	14.4	1.8	14			19	11	1	3	-			14	-									
III	7	2.4	6	6.9	1.7	6.5	10.5	3.7	11.5	2.9	5	2.3	17.5	7.5	10.5	2.9	8	4.4	5.0.2	14.3	2.9	18			8	6	2	8	3	-	6	8	-									
IV	2.4	2.7	1.1	2.8	1.2	2.8	1	5.0	6	1.9	5	3.1	6.5	2.5	12.5	3.3	12	2.4	2.1.4	12.4	2.5	7			8	6	1	2	1	-	2	3	12	-								
V	21.5	1.6	20.5	5.1	6	2.8	4	3.4	1.5	1.7	4	5.9	7.5	4.3	11	5.4	17	3.1	19.1	7.0	6	2		1	10	4		5	3	-	2	2	8	-								
VI	13	1.6	1.5	2.6	5.5	2.0	5	1.8	7.5	3.8	10	2.8	6.5	4.2	14.5	2.8	13	2.3	4.1.8	22.5	4			11	8	6	2	1	-	4	7	6	-								
VII	15.5	1.8	11.5	2.4	3	1.3	2	1.0	5.5	1.5	7.5	1.7	18.5	1.9	13.5	2.6	16	1.6	17.2.1	18.1	2.1			13	21	21	9	-	9	3	18	-								
VIII	3.5	1.3	1.5	2.3	4	2.2	2.5	1.8	1.1	1.6	2.0	3.0	19.5	2.3	1.6	2.4	15	2.0	4.1.6	8.5	1.6			2	10	9		1	-	1	-	9	-								
IX	4	1.5	-	-	1	2.0	1	1.0	1.5.5	1.6	2.7	3.7	2.3.5	4.7	1.2	3.1	6	3.1	9.7.7	33.2	2.3	1		2	19	14	1	4	1	-	1	1	8	-								
X	-	-	-	-	-	-	6	1.3	1.7	2.3	2.9.5	3.2	2.4	3.5	5.5	1.5	1.1	2.5	7.6	2.2	2.0	1			8	5		2		-	2	9	-								
XI	4.5	6.0	12.5	5.8	1.9.5	2.6	1.5.5	1.8	1.1.5	1.7	6	3.3	1.6	7.7	1.5	1.1.0	3	4.0	9.0	3.8	2.8	11	3		7	3		5		-	2	1.8	-								
XII	8.5	2.2	9	6.9	5	2.3	5	1.3	1.2	3.1	2.0.5	4.0	1.5	4.5	8	5.2	10	3.5	4.2.5	9.8	8	23	7	3	13	10		5	2	-	2	1.9	-								
Rok	1.0.9.5	2.6	1.0.4	3.7	8.1.5	2.6	6.0	2.1	1.3.8.5	2.1	1.7.2.5	3.4	1.9.5	4.2	1.1.5	4.2	1.1.9	2.9	5.7.3.4	3.3.2	2.3.IX	1.0.1	4.9	5	2.9	1.4.2	1.0.0	1.6	4.1	1.1	-	1.9	3.1	1.4.7	-							

Płock – Radziwie

$H_s = 62\ m$ $H_b = 63,1\ m$ $h_w = 14\ m$

I	-	-	5	3.7	6.5	3.8	6	2.6	3	2.2	16.5	3.8	3.7	6.0	2	7.8	1.7	3.9	3.0.9	8.0	5	2.5	1.2	4		10	9		3	2	5	-	4	1.8	2.0						
II	6.5	1.9	0.5	3.0	1.5	3.0	1.0	3.6	8	3.1	13.6	3.9	2.4.5	3.9	3.5	5.4	1.6	2.9	4.7.0	11.2	1.8	11			18	12	1	2	-	4	-	1	14	1								
III	5	4.2	3.5	5.1	16.5	5.0	14.5	4.5	9.5	3.2	5	5.1	19.5	5.3	6.5	4.2	1.3	4.0	3.4.1	10.9	1.5	19	1		7	6	1	7	1		-	6	9	1							
IV	1.2	3.2	1	2.0	6.5	2.7	6.5	2.5	1	2.0	8	2.8	1.9	2.7	1.6	3.1	2.0	2.2	2.1.7	8.7	3.0	8	-	4	8	7		-	4	2	8	7	1							
V	1.2	3.8	5	3.9	1.0	2.6	7	3.1	5	2.5	4.5	2.8	1.5.5	3.8	2.2	2.9	1.2	2.8	2.3.7	11.2	9			1	9	5	1	-	2	4	9									
VI	7	3.2	5.5	3.4	5	3.0	9	2.4	4	2.8	7	4.3	2.2.5	3.4	1.1	4.3	1.9	2.7	5.2.4	17.8	9			1.0	9	7	1	1	-	1	3	6	5							
VII	2.5	3.2	7	2.9	4	2.8	7.5	2.5	6.5	3.7	9.5	2.6	3.2	3.9	7	4.3	1.8	2.8	1.2.3.5	3.1.2	2.7				1.6	1.4	4	1	1	2	7	3	1.1	-							
VIII	-	-	-	-	2.5	2.8	4.5	3.7	5	3.0	16.5	3.6	4.2.5	3.5	5	3.2	1.7	2.8	7.0.6	12.4	1.0				1.4	1.1	1	2	-	2	3	2	7								
IX	-	-	-	-	-	-	3	3.5	8	3.2	2.6.5	5.5	3.2	6.1	2.5	4.8	1.8	4.3	1.0.4.7	3.5.4	2.3				1.8	1.4	2	7	2	3	2	2	1.0								
X	-	-	-	-	1.5	4.7	3.5	2.6	1.2	2.4	2.8.5	4.4	2.6	4.1	0.5	4.0	2.1	3.0	9.1	5.0	2.0				8	2		-	-	6	-	5	8								
XI	6	5.7	4	7.4	1.0.5	4.3	2.3	3.3	7.5	3.2	9	4.0	1.4.5	6.8	2.5	8.6	1.3	4.0	2.0.5	3.8	2.7	9	-	-	8	6		4		3		2	2.0							
XII	3	3.2	2	5.5	5.5	3.2	6.5	2.1	6	2.4	1.7	5.4	2.7	5.1	6	2.8	2.0	3.4	3.1.8	8.6	1.4	23	-	3	1.3	9		4	3	5.8		2	1.3	1.1						
Rok	5.4	2.4	3.3.5	3.1	7.0	3.2	1.0.1	3.0	7.5.5	2.8	1.6.1.5	4.0	3.1.2	4.6	8.4.5	4.6	2.0.2	3.2	5.7.0.0	3.5.4	2.3.IX	9.3	-	7	1.3.8	1.0.2	1.1	3.1	9	3.5.4	1.9	4.3	1.2.9	3.4						

Przybroda

$H_s = 88\ m$ $h_w = 10\ m$

I	5.5	4.4	6.5	4.9	5.5	2.5	3.5	2.5	1.7	2.6	2.8.5	4.6	2.3	4.8	2.5	3.8	1	4.0	2.4.0	5.3	6	2.4	1.1	2		15	7		1		10		4	1.9	3						
II	4	2.6	3	3.7	10.5	3.5	7.5	3.5	2.6	3.7	1.6	3.8	1.2	5.0	2	3.2	5	3.6	3.8.2	11.0	1.8	14	1		16	12	1			2			6								
III	4	2.8	1.1	4.3	1.9	5.2	1.2	3.9	10.5	3.4	8	4.6	12.5	5.7	9	2.7	7	4.0	3.0.3	11.2	1.7	17			8	5	1	5		2		9	6								
IV	18.5	3.5	7.5	3.9	6.5	3.1	4.5	2.4	4	1.6	6.5	4.1	8.5	3.6	1.7	3.2	1.7	2.7	1.6.1	6.2	7	10			7	4				2	1	3	6								
V	1.9	3.8	1.4	3.8	7.5	3.5	3.5	2.3	6.5	2.5	4	4.1	13.6	5.1	2.1	2.9	4	3.4	9.8	3.6	1.3	6			7	4		3		1	1	3	4								
VI	6	2.9	16.5	2.7	7	2.8	3	2.5	3.5	2.1	10.5	2.8	2.1	3.6	13.5	3.4	9	2.8	4.8.9	21.2	6			13	8	5	2				8	4								
VII	9.5	2.5	6	2.7	7	2.8	3.5	2.6	5.5	2.5	1.7	3.6	2.1	4.0	1.4.5	3.2	9	2.9	1.4.4.7	2.1.3	2.1			11	2.1	1.7	6			1	8	4	1.5								
VIII	3.5	2.4	1.5	2.0	4.5	2.1	3	2.2	8.5	3.4	3.0.5	3.6	2.1.5	3.5	9	3.0	1.1	2.8	5.4.3	11.1.4	2.1			1	1.6	1.0	1			1	1	5								
IX	-	-	1	2.0	2	2.0	4.5	1.8	2.4	3.2	2.2	4.8	2.6.5	4.9	6	4.0	6	3.8	9.9.8	2.8.2	1.7	2		1	1.7	1.4	2	1		1	1	7								
X	-	-	-	-	6	2.0	9	2.8	2.3	3.5	2.7	4.2	1.6.5	2.8	4.5	4.8	7	3.2	8.1	2.0	1.9	2			10	4				1.3		4	8								
XI	4	4.9	17.5	4.0	2.2.5	3.5	1.2	2.7	7	3.1	1.1	6.3	1.2.5	7.3	3.5	6.4	-	4.6	1.0.3	3.3	2.8	1.1	3		10	4		2		3		3	2.0								
XII	3.5	4.6	1.0	4.0	5	4.1	7	2.6	1.4	3.8	2.5	4.9	1.5	4.7	1.0.5	4.3	3	4.2	2.4.6	1.0.1	8	2.2	9	3	16	6	1	2		9		2	1.7	1.1						
Rok	7.1.6	2.9	9.4.5	3.2	1.0.3	3.1	7.3	2.6	1.4.3.5	3.0	2.0.6	4.3	2.0.1.5	4.6	1.1.3	3.7	7.7	3.5	5.0.9.1	2.8.2	1.7.IX	1.0.8	2.4	5	2.8	1.8.1	9.2	1.4	1.4	-	4.8	1.2	4.2	1.1.7	1.6						

Wieliszew

$\varphi = 52°28'$ $\lambda = 20°58'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia						Max abs.	Data	Min abs.	Data										
	P_r	Max	Min	$P_{o.m}$	I	II	III	Dies	Max	Min					I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.2	-0.1	-4.2	-4.8	–	–	–	–	–	–	91	87	88	89	0.4	0.8	0.6	0.6	9.2	8.3	7.0	8.2
II	–	–	–	–	1.4	4.2	8.3	2.6	5.8	–	14.4	14	–	–	94	81	90	88	0.4	1.6	0.7	0.9	9.2	8.7	7.8	8.6
III	–	–	–	–	-0.3	5.3	8.5	2.5	8.3	-1.7	17.5	28	-8.4	4	–	–	–	–	–	–	–	–	6.6	6.4	4.6	5.8
IV	–	–	–	–	5.0	12.6	8.4	8.5	14.5	3.7	(28.5)	29	-6.7	10	87	54	74	71	4.3	8.5	3.0	4.3	7.2	6.7	5.9	6.6
V	–	–	–	–	8.3	14.1	10.4	10.8	15.8	5.8	26.8	19	-0.6	6	83	56	74	71	4.9	8.4	3.5	4.5	7.5	8.1	5.0	6.9
VI	–	–	–	–	15.7	21.6	16.7	17.7	24.0	10.6	35.0	14	6.1	1,27	75	47	74	65	4.5	14.4	5.2	8.1	6.3	6.9	4.5	5.9
VII	–	–	–	–	17.1	22.6	16.5	19.2	24.6	13.7	34.0	8	9.1	29	83	61	80	75	3.5	12.0	4.7	6.7	8.6	7.6	6.3	7.5
VIII	–	–	–	–	13.9	19.9	16.4	16.6	21.9	11.4	30.5	12	6.1	30	91	63	84	79	4.6	9.2	3.2	4.7	7.1	8.5	6.0	7.2
IX	–	–	–	–	9.7	14.9	11.9	12.1	18.0	7.8	29.0	9	0.2	26	90	68	83	80	4.3	6.3	2.7	3.4	8.0	8.0	6.9	7.6
X	–	–	–	–	6.5	12.1	8.1	8.7	13.4	4.4	20.6	19	0.4	3	91	70	88	83	4.0	4.6	4.3	2.3	–	–	–	–
XI	–	–	–	–	4.3	5.8	4.2	4.6	8.0	2.0	16.9	4	-7.3	30	91	78	89	85	0.6	2.4	1.0	1.3	8.9	8.5	7.5	8.4
XII	–	–	–	–	-1.8	-0.3	-4.1	-1.9	1.6	–	7.2	9	–	–	92	88	90	90	0.4	0.7	0.6	0.6	8.5	8.8	8.0	8.4
Rok	–	–	–	–	6.5	11.1	8.1	8.4	–	–	35.0	11.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sulęcin

$\varphi = 52°27'$ $\lambda = 15°07'$

I	–	–	–	–	-1.1	1.2	0.0	0.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.2	6.9	7.6
II	–	–	–	–	1.5	5.7	3.0	3.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.8	4.5	5.7
III	–	–	–	–	1.2	8.4	3.7	4.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.4	3.5	4.4
IV	–	–	–	–	4.5	12.3	6.3	7.4	–	–	–	–	–	–	89	56	83	76	1.1	7.0	1.8	3.3	4.2	4.6	3.2	4.0
V	–	–	–	–	9.0	14.3	9.5	10.6	–	–	–	–	–	–	78	53	77	69	2.7	8.4	3.0	4.7	4.4	6.0	3.1	4.5
VI	–	–	–	–	15.7	21.5	15.8	17.2	–	–	–	–	–	–	74	53	75	67	5.1	13.6	4.9	7.9	4.2	5.4	3.5	4.4
VII	–	–	–	–	17.4	22.2	17.5	18.6	–	–	–	–	–	–	85	66	83	78	3.2	9.9	3.9	5.7	5.7	6.9	5.6	6.1
VIII	–	–	–	–	14.8	19.2	14.5	15.6	–	–	–	–	–	–	88	66	87	80	2.1	8.0	2.3	4.1	6.6	6.3	5.1	6.0
IX	–	–	–	–	9.9	15.4	10.7	11.7	–	–	–	–	–	–	91	68	89	83	1.1	5.9	1.5	2.8	6.8	7.1	3.6	5.8
X	–	–	–	–	7.6	12.9	6.4	9.3	–	–	–	–	–	–	92	75	90	86	0.8	3.9	1.1	1.9	7.4	6.7	4.7	6.3
XI	–	–	–	–	3.3	6.9	4.3	4.6	–	–	–	–	–	–	91	82	88	87	0.7	1.9	1.0	1.2	6.0	8.2	6.7	7.5
XII	–	–	–	–	-0.9	0.9	-0.2	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	6.5	7.4
Rok	–	–	–	–	6.9	11.7	7.8	8.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	4.7	5.8

Poznań – Sołacz

$\varphi = 52°25'$ $\lambda = 16°54'$

I	1011.3	1024.4	992.7	1021.1	-1.2	1.1	-0.2	-0.1	2.0	-2.5	10.3	6	-17.1	16	91	86	91	89	0.5	1.0	0.6	0.7	8.7	8.3	8.0	8.3
II	1001.2	1026.4	974.3	1010.8	2.0	5.4	3.0	3.4	6.2	0.8	10.3	5,14	-5.2	27	92	75	92	86	0.6	2.4	0.7	1.2	7.4	7.7	7.5	7.5
III	1008.8	1028.2	984.8	1018.5	1.0	7.6	4.0	4.2	9.0	0.1	16.8	13	-6.5	3	88	62	82	77	0.9	4.4	1.6	2.3	5.3	4.9	3.5	4.6
IV	1009.6	1022.3	986.3	1019.1	4.9	12.5	7.1	7.5	13.7	2.4	24.3	28	-4.7	14	84	51	80	72	1.4	8.0	2.2	3.9	5.6	5.9	4.3	5.5
V	1007.7	1019.8	998.0	1017.0	9.5	15.2	10.7	11.5	16.4	5.4	26.8	19	-0.2	9	70	44	68	61	3.8	10.8	4.6	6.4	4.6	6.4	5.2	5.4
VI	1007.4	1023.5	993.1	1016.5	16.1	22.1	16.7	17.9	23.8	11.0	31.5	19	6.8	15	73	50	76	66	5.2	14.4	4.8	8.1	5.1	5.1	4.2	4.8
VII	1003.4	1015.5	994.0	1012.1	17.6	22.3	18.2	19.1	23.9	14.6	32.8	5	10.4	3	82	64	83	76	3.9	11.8	4.2	6.6	6.8	6.8	6.9	6.8
VIII	1005.1	1015.7	998.2	1014.3	14.5	19.9	15.2	16.2	21.3	11.7	27.4	11	6.7	23	86	62	84	77	2.5	9.4	3.1	5.0	6.2	7.1	5.3	6.2
IX	1003.3	1014.9	985.6	1012.5	9.8	14.8	10.8	11.8	16.5	7.5	28.2	8	-1.2	6	90	67	87	81	1.2	6.4	1.8	3.1	6.7	7.6	5.5	6.6
X	1009.8	1020.6	993.9	1019.2	6.8	12.2	8.8	9.0	13.3	5.1	20.6	19	-1.9	2	92	73	88	84	0.9	4.1	1.4	2.1	8.3	7.5	5.4	7.1
XI	1011.5	1029.7	994.3	1021.1	5.4	6.5	4.4	4.7	7.3	2.2	16.8	5	-6.2	30	87	75	85	82	1.0	2.6	1.3	1.6	7.6	8.9	7.7	8.1
XII	1005.4	1023.8	968.5	1015.2	-1.4	0.5	-0.4	-0.4	1.5	-2.8	9.3	8	-14.2	16	89	84	87	87	0.6	1.0	0.8	0.8	8.4	8.6	7.0	8.0
Rok	1007.0	1029.7	968.5	1016.4	6.9	11.7	8.2	8.8	12.9	4.6	32.8	5.VII	-17.1	16.1	85	66	84	78	1.9	6.3	2.2	3.5	6.7	7.1	5.9	6.6

Poznań – Ławica

$\varphi = 52°25'$ $\lambda = 16°50'$

I	1009.7	1022.7	991.4	1018.4	-1.7	0.6	-0.9	-0.7	1.8	-3.7	10.1	6	-19.0	16	90	83	89	87	0.6	1.1	0.7	0.8	8.3	8.4	6.6	7.8
II	999.4	1024.3	972.4	1010.9	4.3	5.2	2.4	2.8	6.2	-0.6	10.5	5	-8.4	27	93	76	90	86	0.5	2.1	0.7	1.1	7.6	8.4	5.9	7.3
III	1007.0	1026.2	983.2	1018.5	0.5	7.4	3.3	3.6	9.1	-0.8	16.9	13	-7.4	3	86	60	81	76	1.0	4.6	1.6	2.4	5.7	6.0	3.0	4.9
IV	1007.8	1020.4	984.9	1019.1	4.3	12.0	7.0	7.6	13.7	1.4	24.7	28	-6.2	14	85	51	78	70	1.3	7.8	3.1	4.1	5.9	7.1	4.4	5.8
V	1005.9	1017.6	996.1	1017.1	8.8	14.8	10.4	11.1	15.4	4.8	26.3	19	-2.4	7	76	49	71	65	2.8	9.5	3.9	5.4	5.7	7.4	4.9	6.0
VI	1005.9	1021.7	993.7	1016.9	15.6	21.8	17.4	18.0	24.0	10.8	32.1	19	5.9	2	74	49	71	65	5.0	14.8	5.2	8.7	5.7	6.3	4.6	5.5
VII	1001.5	1014.1	989.8	1012.3	17.2	21.9	18.5	19.0	24.1	14.3	32.9	5	9.5	3,29	84	64	84	78	3.5	11.2	4.7	6.5	7.4	7.2	6.9	7.2
VIII	1003.3	1013.9	990.3	1014.2	14.0	19.4	15.2	16.0	21.3	11.0	28.0	11	6.1	23	89	63	84	79	1.8	8.9	3.0	4.8	6.5	7.7	5.2	6.5
IX	1001.8	1013.0	985.8	1012.9	9.2	15.1	10.6	11.4	16.6	6.9	28.2	8	-1.2	26,27	94	87	88	83	0.7	6.4	1.7	2.9	7.2	8.1	5.1	6.8
X	1008.0	1018.4	994.8	1019.3	6.2	12.2	8.0	8.6	13.4	4.1	20.9	19	-3.0	2	95	74	93	87	0.5	4.0	0.8	1.8	7.8	7.9	4.1	6.4
XI	1009.6	1028.0	992.4	1021.1	3.1	6.4	3.9	4.5	7.4	1.4	17.0	5	-8.2	30	90	79	88	86	0.8	2.3	1.0	1.4	8.0	8.6	7.0	7.9
XII	1003.6	1018.2	968.3	1015.2	-1.8	0.2	-0.9	-0.8	1.5	-3.7	9.6	8	-14.7	17	91	88	90	90	0.5	0.7	0.5	0.6	7.8	8.9	7.0	7.9
Rok	1005.5	1028.0	968.3	1016.6	6.4	11.4	7.9	8.4	13.0	3.8	32.9	5.VII	-19.0	18.1	87	67	83	79	1.8	6.1	2.3	3.3	7.0	7.6	5.4	6.7

Wieliszew

$H_s = 78$ m $h_w = 13$ m 1957

Miesiąc	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T ≥ 25	≥ 10	≤ 0	≤ −10	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	Wiatr v ≥ 10	≥ 15	≥ 20	≥ 30	≥ 40	≥ 50	≥ 60	≥ 70	≥ 80	≥ 90	≥ 100
I	-	-	10	5.1	7	3.1	12.5	2.5	14.5	2.8	3.0	4.8	1.7	4.8	-	-	2	3.9	34.7	9.0	31	-	-	-	-	9	9	-	1	-	-	-	-	-	-	-	-	-	-	-
II	3	6.0	6	2.5	7	3.6	18.5	4.3	16.5	3.9	2.0	4.3	7	5.6	2	4.7	4	4.0	42.6	9.4	18	-	-	-	-	18	13	-	-	-	-	-	-	-	-	-	-	-	-	-
III	6	6.1	10	3.2	18.5	4.6	10.5	4.5	6	4.5	1.9	4.0	8	6.1	5	6.3	10	4.1	23.4	7.6	15	2	-	-	-	8	6	-	5	-	-	-	-	-	-	-	-	-	-	-
IV	1.6	3.8	1.3	4.1	8.5	3.2	6	2.7	10	3.2	8	3.4	8	4.4	8.5	4.3	12	3.2	13.0	3.7	3.0	7	-	-	4	7	6	-	8	4	-	3	4	1.3	-	-	-	-	-	-
V	1.2	4.3	1.2	4.0	1.4	2.8	6.5	2.2	6.5	3.9	8	4.2	7	4.9	1.4	4.4	1.3	3.2	26.4	9.2	1.0	1	-	-	1	4	4	-	-	-	-	-	1	1.2	-	-	-	-	-	-
VI	1.2	3.2	5	3.4	3.5	2.7	6	3.2	4.5	4.2	18.5	3.6	1.2	3.7	5.5	4.0	2.3	2.6	59.7	13.8	4	-	-	-	11	9	8	2	-	-	6	4	9	-	-	-	-	-	-	-
VII	6.5	2.7	1.3	2.7	10.5	3.2	1.0	2.2	1.1	2.7	1.8	3.6	9.5	4.4	4.5	3.7	1.0	2.8	99.0	21.7	1.6	-	-	-	15	17	14	3	-	-	5	1	4.7	-	-	-	-	-	-	-
VIII	2	2.5	1.5	3.3	6	2.1	8.5	2.8	11.5	3.7	2.6	4.1	1.1	3.7	5.5	3.1	2.1	2.7	79.5	36.0	1.4	-	-	-	4	12	11	2	-	-	3	-	1.4	-	-	-	-	-	-	-
IX	2.5	3.4	-	-	4.5	1.9	1.4	3.0	17.5	4.3	2.3	4.4	1.2	4.9	2.5	3.8	1.4	3.4	77.9	16.9	2.3	-	-	-	5	18	10	2	3	3	-	2	2	1.5	-	-	-	-	-	-
X	0.5	2.0	2.5	2.0	5.5	1.8	1.1	2.7	1.9	2.9	2.8	4.3	10.5	3.8	2	4.0	1.4	2.9	4.5	2.3	2.0	-	-	-	-	6	1	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	3	9.5	10.5	4.3	1.4	3.0	18.5	3.9	7	3.6	1.3	5.0	5.5	7.3	2.5	8.0	1.6	3.8	13.2	4.5	2.8	1.1	6	-	-	8	6	-	5	-	-	-	1	2.2	-	-	-	-	-	-
XII	4.5	4.0	5	5.3	4.5	2.7	1.5	3.1	15.5	4.6	26.5	4.6	4	4.5	4	3.2	1.4	3.9	27.6	8.1	8	-	8	-	-	13	8	-	2	2	-	-	1	2.1	-	-	-	-	-	-
Rok	6.8	4.0	8.8.5	3.3	10.3.5	2.9	13.7	3.1	13.9.5	3.7	2.3.8	4.2	11.1.5	4.8	5.6	4.1	1.5.3	3.4	7.98.5	36.0	14.VIII	-	-	-	5.8	129	96	9	16	6	-	23	-	-	-	-	-	-	-	-	-

Suleczin

$H_s = 70$ m

Miesiąc	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T ≥ 25	≥ 10	≤ 0	≤ −10	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	Wiatr v ≥ 10	≥ 15	≥ 20	≥ 30	≥ 40	≥ 50	≥ 60	≥ 70	≥ 80	≥ 90	≥ 100
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.2	6.8	28	-	-	-	-	10	9	-	-	-	-	-	2	1.8	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	45.4	9.4	8	-	-	-	-	13	13	-	-	-	-	-	3	3.7	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43.3	12.8	17	-	-	-	-	7	5	2	-	-	-	-	1.3	9	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.9	4.7	25	-	-	-	-	4	4	-	-	-	-	-	9	3	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	43.7	12.4	23	-	-	-	-	6	6	1	-	-	-	-	5	6	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.2	11.0	24	-	-	-	-	7	6	1	-	-	-	-	9	3	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	145.9	32.7	8	-	-	-	-	15	15	4	-	-	-	-	5	10	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80.3	14.7	27	-	-	-	-	15	13	2	-	-	-	-	4	6	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95.2	32.5	23	-	-	-	-	10	15	2	-	-	-	-	4	6	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	23.2	9.8	19	-	-	-	-	7	5	-	-	-	-	-	3	9	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.4	2.8	25	-	-	-	-	7	4	-	-	-	-	-	5	1.9	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.9	16.4	8	-	-	-	-	14	11	1	-	-	-	-	2	1.6	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	607.6	32.7	8.VII	-	-	-	-	124	106	13	-	-	-	-	61	112	-	-	-	-	-	-

Poznań – Sołacz

$H_s = 74$ m $H_b = 76.8$ m $h_w = 12$ m

Miesiąc	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T ≥ 25	≥ 10	≤ 0	≤ −10	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	Wiatr v ≥ 10	≥ 15	≥ 20	≥ 30	≥ 40	≥ 50	≥ 60	≥ 70	≥ 80	≥ 90	≥ 100
I	2	2.5	9	4.3	5	2.6	3	3.3	5	2.6	2.5	3.8	3.4	5.8	6	7.7	4	4.5	24.4	5.0	31	2.0	8	2	-	11	8	-	5	-	12	-	4	2.5	-	-	-	-	-	-
II	6	3.0	2	4.0	6	2.8	9	3.1	1.6	3.4	1.9	4.4	1.7	4.5	4	5.6	5	3.7	37.8	10.1	18	9	-	-	-	15	10	1	-	-	14	-	-	1.2	-	-	-	-	-	-
III	9	3.1	8	5.9	2.0	5.1	1.4	3.9	5	4.8	7	4.1	1.5	7.3	7	6.1	8	4.7	28.8	11.8	17	1.7	-	-	-	6	6	1	7	1	1.0	-	1.3	1.0	-	-	-	-	-	-
IV	1.5	4.5	1.4	2.8	7	2.7	4	3.2	2	3.0	3	4.0	1.2	4.3	1.6	5.1	1.7	3.2	10.3	3.0	2.9	9	-	-	-	9	4	-	3	-	6	-	4	7	-	-	-	-	-	-
V	1.0	4.1	2.2	4.0	8	4.8	6	3.2	1	2.0	6	3.8	1.1	5.9	2.5	4.4	4	4.2	20.9	9.4	6	1	-	-	1	9	3	-	5	-	2	1	5	8	-	-	-	-	-	-
VI	6	3.7	6	3.0	1.3	5.2	6	3.2	4	3.5	6	4.2	2.5	6.2	1.3	5.3	1.1	4.3	45.7	16.3	4	-	-	-	1.4	10	6	2	4	-	1	2	8	7	-	-	-	-	-	-
VII	4	6.2	6	4.7	8	3.2	6	4.3	3	6.3	6	4.3	2.8	5.6	1.8	4.9	1.4	4.3	172.3	34.5	1.4	-	-	-	1.3	21	15	5	5	-	3	7	6	1.6	-	-	-	-	-	-
VIII	-	-	-	-	5	4.2	7	4.7	5	4.8	1.6	6.2	3.4	5.3	1.4	4.9	1.2	4.6	42.3	10.2	24	-	-	-	2	16	9	1	3	-	-	2	3	8	-	-	-	-	-	-
IX	-	-	-	-	2	3.0	9	4.2	7	4.4	1.6	4.7	3.2	5.9	1.8	5.3	8	4.7	9.4	17.3	17	2	-	-	1	18	1.6	3	11	-	9	2	2	9	-	-	-	-	-	-
X	2	2.0	1	2.0	5	2.2	7	4.6	1.4	4.1	2.1	5.2	2.3	5.2	1.3	4.6	7	4.3	8.8	2.9	2.4	2	-	-	-	14	4	-	3	-	1.9	-	3	1.3	-	-	-	-	-	-
XI	7	4.1	1.1	4.5	2.5	4.2	1.1	3.9	9	5.6	7	4.7	1.4	9.4	3	4.0	3	5.0	12.2	6.8	2.8	1.1	2	-	-	8	2	-	5	1	6	-	2	1.9	-	-	-	-	-	-
XII	5	3.6	5	4.8	1.4	3.5	9	2.8	7	4.9	2.0	4.6	2.1	6.3	1.1	4.7	1	4.6	25.2	10.1	8	2.1	6	3	-	11	5	1	5	-	1.3	-	2	1.9	-	-	-	-	-	-
Rok	6.6	3.1	8.4	3.3	1.1.8	3.6	9.1	3.7	7.8	4.1	1.5.2	4.5	2.6.6	6.0	1.4.6	5.2	9.4	4.3	5.19.9	34.5	14.VII	9.2	1.6	5	3.1	1.4.8	8.8	4.4	5.6	2	1.0.1	1.4	5.2	1.5.1	-	-	-	-	-	-

Poznań – Ławica

$H_s = 86$ m $H_b = 92.1$ m $h_w = 13$ m

Miesiąc	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T ≥ 25	≥ 10	≤ 0	≤ −10	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	Wiatr v ≥ 10	≥ 15	≥ 20	≥ 30	≥ 40	≥ 50	≥ 60	≥ 70	≥ 80	≥ 90	≥ 100
I	1.5	2.0	4.5	3.8	6.5	5.8	2.5	4.8	9	3.6	2.2	4.5	2.6	5.4	1.1	5.4	1.0	4.3	24.5	4.6	6	2.3	9	3	-	12	8	-	3	-	1.1	-	3	1.9	1.7	-	-	-	-	-
II	3	3.7	2	3.8	7.5	3.1	7.5	3.1	2.7	4.7	1.7.5	5.0	1.2	6.1	3.5	5.9	4	4.5	45.2	10.0	18	1.8	-	-	-	16	11	1	2	-	4	-	9	-	-	-	-	-	-	-	-
III	3.5	3.9	5.5	5.1	2.2	6.2	1.4	4.1	9	4.9	8.5	4.8	1.6.5	7.5	7	4.6	5	5.2	34.0	10.1	17	1.7	-	-	-	6	5	1	8	1	2	-	6	8	-	-	-	-	-	-
IV	2.2.5	4.1	1.6	4.1	8.5	3.8	2.5	2.6	2.5	2.4	5.5	4.1	1.1.5	4.9	1.5	4.6	6	3.9	8.7	2.6	1.6	1.0	-	-	-	8	5	-	-	-	3	1	3	3	-	-	-	-	-	-
V	1.2	5.0	2.2	5.0	1.1	3.1	8	2.8	4.5	2.7	5.5	4.4	9	6.4	1.8	5.0	3	4.4	24.9	14.0	6	5	-	-	2	7	4	1	4	1	2	1	1	5	-	-	-	-	-	-
VI	5	4.0	1.2	4.0	1.1	4.1	8	3.2	8	3.8	1.2	3.8	1.7	5.8	1.3	6.2	4	4.4	49.5	19.2	4	-	-	-	1.2	9	6	2	2	-	2	3	4	7	-	-	-	-	-	-
VII	1.2	4.3	6.5	3.3	10.5	4.0	6.5	2.8	7	3.0	1.5	4.7	2.1	5.5	1.2.5	5.9	2	4.5	200.7	54.1	2.2	-	-	-	1.3	19	15	5	2	-	2	8	1	1.8	-	-	-	-	-	-
VIII	1.5	1.7	2.5	1.8	3	3.7	4.5	3.3	1.2	3.0	3.3	5.0	2.0	4.8	1.4.5	4.4	2	4.2	45.8	9.8	16	-	-	-	5	17	10	-	5	-	1	1	-	8	-	-	-	-	-	-
IX	2	3.5	1	3.0	2	1.8	7.5	2.1	1.8.5	4.5	2.6.5	5.6	2.0.5	6.3	8	5.4	4	4.9	94.2	21.0	23	2	-	-	1	17	1.5	3	9	-	4	2	-	9	-	-	-	-	-	-
X	0.5	3.0	2	1.0	2.5	2.2	1.2.5	2.2	2.1.5	3.6	2.8.5	4.8	1.5.5	5.7	6	4.2	4	3.9	9.5	2.8	2.4	2	-	-	-	9	5	-	1	-	1.4	-	2	7	-	-	-	-	-	-
XI	2.5	7.0	9.5	6.4	2.6.5	4.1	1.9	3.1	8	4.1	10.5	6.4	1.1	8.8	4	2.8	1	5.2	1.3.0	6.0	2.8	1.2	2	-	-	8	3	-	8	1	2	-	3	1.8	-	-	-	-	-	-
XII	4.5	4.8	5.5	6.3	9.5	4.5	9	3.1	1.1.5	4.2	2.8	5.2	1.4.5	5.9	8.5	4.8	2	4.8	2.9.3	10.0	8	2.3	9	3	-	1.3	7	1	7	2	9	-	-	1.9	1.1	-	-	-	-	-
Rok	7.2.5	3.9	8.9	4.0	1.2.0.5	3.9	1.0.1.5	3.1	1.3.8.5	3.7	2.1.2.5	4.9	1.9.4.5	6.1	1.2.1	6.4	4.7	4.5	5.7.6.3	54.1	22.VII	1.1.2	2.0	6	3.1	1.4.3	9.4	1.4	5.1	5	5.6	1.9	2.3	1.3.6	2.8	-	-	-	-	-

Nowy Dwór Mazowiecki $\varphi = 52°26'$ $\lambda = 20°43'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	–	–	–	–	-1,9	0,1	-1,3	-1,1	0,9	-4,0	7,0	6	-15,1	16	88	85	87	87	0,6	0,9	0,7	0,7	8,7	8,0	5,7	7,5
II	–	–	–	–	1,7	4,5	2,8	3,0	5,4	0,4	10,3	14	-3,3	28	90	80	85	85	0,7	1,9	1,1	1,2	9,3	8,7	7,3	8,4
III	–	–	–	–	0,1	5,8	2,7	2,8	–	-1,4	–	–	-7,3	4	84	58	75	71	1,2	4,5	1,9	2,5	5,8	5,3	3,8	5,0
IV	–	–	–	–	5,5	13,4	8,4	8,9	–	3,6	–	–	-4,2	10	85	49	75	70	1,5	9,4	3,0	4,6	6,1	5,5	4,2	5,3
V	–	–	–	–	9,2	14,3	11,0	11,4	–	6,1	–	–	-0,1	6	81	59	75	72	2,3	8,0	3,6	4,6	5,6	7,5	4,9	6,0
VI	–	–	–	–	15,5	21,7	17,1	17,8	–	11,7	–	–	6,9	27	78	53	76	69	3,9	12,8	4,9	7,2	5,1	6,2	4,5	5,3
VII	–	–	–	–	17,0	22,4	18,5	19,1	–	14,1	–	–	9,7	29	86	64	82	77	2,8	11,0	4,0	5,9	7,0	7,0	6,0	6,7
VIII	–	–	–	–	13,9	19,9	15,9	16,4	21,6	11,8	29,1	12	6,0	24	91	65	84	80	1,5	8,7	3,0	4,4	5,5	7,0	4,2	5,6
IX	–	–	–	–	9,7	15,1	11,3	11,8	16,2	8,0	28,3	9	0,6	26	89	69	85	80	1,3	6,0	2,4	3,2	6,5	7,4	5,8	6,6
X	–	–	–	–	5,7	12,2	8,1	8,5	13,2	4,4	20,7	19	0,1	3	92	70	86	83	0,8	4,7	1,5	2,3	5,9	6,8	3,8	5,5
XI	–	–	–	–	3,4	6,3	4,1	4,5	7,3	1,9	16,5	5	-7,3	30	88	75	85	83	0,9	2,5	1,3	1,6	8,1	7,9	7,3	7,8
XII	–	–	–	–	-2,0	-0,1	-1,4	-1,2	0,9	-3,9	6,8	9	-14,0	17	87	82	88	86	0,7	1,1	0,7	0,8	7,4	8,4	7,3	7,7
Rok	–	–	–	–	6,5	11,3	8,1	8,5	–	4,4	–	–	-15,1	16,1	86	67	82	78	1,5	6,0	2,3	3,3	6,8	7,1	5,4	6,4

Siemiatycze $\varphi = 52°26'$ $\lambda = 22°51'$

I	–	–	–	–	-2,7	-0,7	-1,7	-1,7	–	-4,1	–	–	-16,0	17	93	87	92	91	0,3	0,7	0,5	0,5	8,6	8,3	7,5	8,1
II	–	–	–	–	0,5	3,0	1,5	1,6	–	-0,8	–	–	-8,6	24	94	85	91	90	0,4	1,2	0,6	0,7	8,2	8,1	7,0	7,8
III	–	–	–	–	-2,3	3,8	0,9	0,8	–	-3,7	–	–	-13,4	4	84	62	79	75	0,9	3,6	1,5	2,0	4,0	4,5	4,2	4,2
IV	–	–	–	–	5,5	13,0	7,9	8,6	–	2,7	–	–	-8,5	10	–	–	–	–	–	–	–	–	5,2	5,2	4,3	4,9
V	–	–	–	–	10,0	14,4	10,5	11,4	–	6,3	–	–	-0,9	6	–	–	–	–	–	–	–	–	5,3	7,4	5,3	6,0
VI	–	–	–	–	16,0	22,4	17,2	18,8	–	10,2	–	–	3,2	1	77	53	74	68	4,5	13,6	5,3	7,8	4,6	5,1	3,4	4,4
VII	–	–	–	–	17,4	22,7	17,7	18,9	–	13,7	–	–	9,0	4	83	61	83	76	3,5	11,4	3,7	6,2	5,3	5,7	4,9	5,3
VIII	–	–	–	–	14,4	20,0	15,3	16,8	–	11,5	–	–	5,5	24	90	65	87	81	1,6	8,8	2,4	4,3	5,8	6,3	3,7	5,3
IX	–	–	–	–	9,9	14,8	10,7	11,5	–	7,9	–	–	1,0	27	91	69	89	83	1,1	5,9	1,4	2,8	7,1	7,7	4,3	6,4
X	–	–	–	–	5,6	11,6	7,5	8,0	–	4,2	–	–	-1,2	3	93	72	90	85	0,7	4,2	1,1	2,0	8,3	5,7	5,7	5,9
XI	–	–	–	–	3,0	5,2	3,5	3,8	–	1,5	–	–	-9,2	30	95	84	90	90	0,4	1,6	0,7	0,9	8,7	8,1	7,2	8,0
XII	–	–	–	–	-2,9	-0,9	-2,3	-2,1	–	-4,9	–	–	-14,4	16	91	86	90	89	0,5	0,7	0,5	0,6	7,4	8,0	6,3	7,2
Rok	–	–	–	–	6,2	10,8	7,4	8,0	–	3,7	–	–	-16,0	17,1	–	–	–	–	–	–	–	–	6,4	6,7	5,3	6,1

Izbica Kujawska $\varphi = 52°25'$ $\lambda = 18°46'$

I	–	–	–	–	-1,5	0,4	-0,9	-0,7	–	-3,2	–	–	-16,8	16	–	–	–	–	–	–	–	–	8,4	7,2	6,9	7,5
II	–	–	–	–	1,8	4,9	2,8	3,1	–	0,4	–	–	-4,1	28	–	–	–	–	–	–	–	–	6,1	6,4	5,6	6,0
III	–	–	–	–	1,1	6,7	3,4	3,6	–	-0,6	–	–	-6,1	1,10	–	–	–	–	–	–	–	–	4,1	5,1	3,5	4,2
IV	–	–	–	–	5,5	12,2	7,3	8,1	–	2,1	–	–	-4,2	13	–	–	–	–	–	–	–	–	5,1	4,9	4,4	4,8
V	–	–	–	–	9,5	15,3	10,1	11,2	–	5,0	–	–	0,5	27	–	–	–	–	–	–	–	–	4,8	5,7	5,4	5,3
VI	–	–	–	–	15,9	22,2	16,7	17,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3,7	3,8	4,5	4,0
VII	–	–	–	–	18,4	22,3	17,5	18,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5,4	6,0	6,7	6,0
VIII	–	–	–	–	14,9	19,2	15,0	16,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6,3	6,6	6,1	6,3
IX	–	–	–	–	8,4	13,5	9,6	10,3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7,9	7,6	7,7	7,7
X	–	–	–	–	6,2	12,3	7,5	8,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3,8	6,4	4,0	4,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7,5	7,7	7,9	7,7
XII	–	–	–	–	-1,8	-0,4	-1,6	-1,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7,3	7,4	6,7	7,1
Rok	–	–	–	–	6,8	11,2	7,6	8,3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Legionowo $\varphi = 52°24'$ $\lambda = 20°58'$

I	1007,7	1019,6	994,0	1020,9	-2,0	-0,1	-1,3	-1,2	1,1	-3,6	7,6	6	-15,8	16	91	89	91	90	0,4	0,7	0,5	0,5	8,7	8,3	6,5	7,8
II	998,6	1012,0,1	973,5	1011,5	1,5	4,2	2,4	2,6	5,6	0,1	10,3	14	-3,8	28	94	81	90	88	0,4	1,7	0,8	1,0	8,7	8,4	6,6	7,9
III	1006,4	1022,4	981,0	1019,4	-0,5	5,5	2,3	2,4	7,5	-2,0	16,8	31	-9,1	4	85	55	78	73	0,9	4,8	1,7	2,5	6,2	5,3	4,4	5,3
IV	1005,7	1014,6	981,4	1018,4	5,3	13,0	8,6	8,9	14,6	3,4	26,8	29	-6,0	10	86	50	72	69	1,4	9,1	3,4	4,6	6,9	6,4	4,8	6,0
V	1003,6	1014,5	993,1	1016,1	9,2	14,1	10,7	11,2	15,7	5,9	27,4	19	-1,0	6	79	57	73	70	2,6	8,0	3,7	4,8	5,7	7,5	4,5	5,9
VI	1004,2	1018,3	992,2	1016,5	15,8	21,9	17,3	18,1	23,8	11,8	31,5	11	7,4	27	75	49	73	66	4,7	14,2	5,6	8,2	4,9	5,9	4,2	5,0
VII	999,6	1009,8	988,6	1011,7	17,0	22,5	18,7	19,2	24,4	14,2	33,4	8	10,1	29	84	60	77	74	3,2	12,3	5,3	6,9	7,4	6,7	5,5	6,5
VIII	1004,7	1011,2	989,2	1013,9	14,0	19,7	16,0	16,4	–	11,9	–	–	6,7	24	89	62	83	78	1,8	9,4	3,2	4,8	6,1	7,1	4,1	5,8
IX	999,9	1010,4	988,4	1012,3	9,7	14,8	11,5	11,9	–	8,2	–	–	0,3	26	90	67	84	80	1,2	6,3	2,4	3,3	6,3	7,4	4,7	6,1
X	1007,0	1018,3	993,6	1019,7	6,0	12,0	8,4	8,7	–	4,8	–	–	0,7	2,3	93	69	87	83	0,7	4,7	1,5	2,3	6,5	6,8	3,8	5,7
XI	1008,5	1022,9	990,3	1021,4	3,0	6,3	3,9	4,3	–	1,7	–	–	-8,3	30	93	77	89	86	0,5	2,3	0,8	1,2	8,4	7,6	6,4	7,5
XII	1002,3	1020,0	959,3	1015,5	-2,1	-0,3	-1,5	-1,4	0,8	-4,1	6,8	9	-15,7	16	93	87	93	91	0,4	0,8	0,4	0,5	7,7	8,8	6,7	7,7
Rok	1003,8	1022,9	959,3	1016,5	6,4	11,1	8,1	8,4	–	4,4	–	–	-15,8	16,1	88	67	82	79	1,5	6,2	2,4	3,4	7,0	7,2	5,2	6,5

Nowy Dwór Mazowiecki — $H_s = 70\ m$ — $h_w = 13\ m$ — 1957

MIESIĄC	ROZKŁAD WIATRU (n, v m/s)																		OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10	Max>25°	0.1 ≤	≥1.0	≥10.0	>10	>15						
I	1	4,0	·	·	7	2,3	8,5	2,1	10,5	1,3	19	1,8	19,5	2,2	9,5	5,6	18	1,9	23,4	5,7	31	25	10	3	·	15	7	·	1	1	–	–	3	17	–			
II	5	2,9	7,5	2,3	2	1,0	4	1,1	1,9	1,9	9,5	1,3	17,5	1,6	3,5	3,0	16	1,5	49,9	11,5	18	12	·	·	·	21	14	1	·	·	–	–	1	18	–			
III	9	5,8	7	1,9	11	1,7	7,5	3,7	7	2,5	5,5	2,5	7,5	2,4	10,5	3,9	28	2,2	24,9	10,3	15	18	–	·	–	10	5	1	2	1	–	–	9	6	–			
IV	26,5	2,3	10,5	1,5	2,5	1,0	2	1,0	2,5	2,2	3,5	1,3	1	1,0	5,5	2,5	36	1,2	14,7	9,0	30	7	–	·	–	9	4	·	·	·	–	–	7	7	–			
V	1,5	2,4	1,2	2,4	1,1	1,8	5,5	1,4	4	1,2	0,5	3,0	6	2,7	1,3	3,4	26	1,7	24,3	10,7	9	1	–	·	–	8	4	1	·	·	–	–	2	9	–			
VI	10,5	2,4	9	2,2	5	1,2	2,5	1,4	1,5	1,7	4	2,1	1,7	2,5	13,5	3,0	27	1,7	54,2	15,5	9	·	·	·	–	10	6	1	·	·	–	–	4	5	–			
VII	9,5	2,1	4	1,5	3,5	1,3	2	2,0	7,5	1,8	3,5	3,0	7	1,8	1,7	2,8	39	1,3	138,0	24,1	21	·	·	·	–	19	14	6	·	·	–	–	4	14	–			
VIII	16,5	1,6	·	·	2	1,0	2	1,5	3	2,0	6	2,0	2,3	1,5	6,5	1,8	34	1,0	81,9	32,5	14	·	·	·	6	19	11	2	·	·	–	–	5	6	–			
IX	1,4	2,5	0,5	1,0	·	·	1,5	1,0	7	1,8	1,1	3,0	2,4,5	2,5	9,5	3,1	22	1,9	68,9	13,7	15	·	·	·	2	19	15	1	·	·	–	–	2	11	–			
X	7,5	2,5	·	·	·	·	·	·	5,5	1,2	1,9	1,7	1,8,5	2,1	2,5	2,6	40	1,1	6,4	3,0	20	·	·	·	·	7	1	·	·	·	–	–	4	9	–			
XI	7,5	1,1,1	4,5	5,4	8	2,8	1,1,5	1,7	3	2,5	6	2,3	9,5	2,6	1	1,2,5	39	2,3	1,3,8	7,1	28	11	2	·	·	8	3	·	2	2	–	–	3	18	–			
XII	5,5	3,4	5	3,6	5	1,2	2	1,0	6,5	4,1	2,0,5	3,2	10,5	2,6	4	3,5	34	1,9	37,9	9,6	8	24	10	3	·	15	10	·	2	1	–	–	2	17	–			
Rok	127,5	3,6	60	1,8	57	1,3	49	1,5	77	2,0	108	2,3	161,5	2,1	96	4,0	359	1,6	538,3	32,5	14.VIII	98	–	6	–	160	94	13	7	5	–	–	46	139	–			

Siemiatycze — $H_s = 145\ m$ — $h_w = 11\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28,3	10,4	5	24	–	5	–	11	6	1	–	–	3	·	2	20	24			
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	54,7	9,5	22	11	–	·	–	25	15	·	–	–	5	·	2	15	7			
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9,6	4,5	4	24	–	3	–	3	3	·	–	–	3	·	12	7	13			
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	11,6	3,8	30	9	–	·	–	8	6	·	–	–	·	1	5	7	·			
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31,7	9,3	9	1	–	·	–	9	7	·	–	–	·	4	4	12	·			
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	67,1	49,2	24	·	–	·	–	8	5	1	–	–	1	2	10	6	·			
VII	1,5	2,0	2	2,0	8	3,3	10	4,1	16	2,5	26,5	3,6	17	3,9	7	3,1	5	3,2	99,1	23,7	16	·	–	·	–	20	16	2	·	·	·	13	7	8	·			
VIII	1,5	2,0	·	·	0,5	5,0	4	5,4	6	4,7	2,3,5	4,6	3,3,5	4,7	10	3,2	14	3,8	140,7	50,0	14	·	–	·	–	16	11	4	1	·	2	7	5	6	·			
IX	2	2,5	1,5	2,3	0,5	5,0	1,5	4,3	6,5	4,1	2,9	5,4	3,3,5	7,5	5,5	3,5	10	5,2	89,4	21,9	23	·	–	·	–	17	14	3	8	5	2	3	2	10	·			
X	·	·	·	·	1	2,5	2,5	3,2	6	3,5	3,7	4,3	2,7,5	4,7	6	3,3	13	3,7	14,6	6,5	23	2	–	·	–	9	4	·	1	·	4	·	3	7	·			
XI	9	3,9	1,5	9,7	8,5	4,6	11,5	6,1	12,6	5,5	10,5	4,7	19	4,6	7,5	3,5	10	4,3	30,1	12,0	28	10	–	·	–	12	6	1	3	·	4	·	3	21	·			
XII	6,5	2,9	10	3,1	1	2,5	6,5	5,3	15,5	3,7	24	6,1	18	7,1	4,5	8,1	7	4,8	24,7	5,4	8	26	–	4	–	13	8	·	4	1	4	·	3	17	9			
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	601,6	50,0	14.VIII	107	–	12	–	151	101	12	–	–	28	30	58	136	33			

Izbica Kujawska — $H_s = 120\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34,9	8,8	31	25	–	2	–	10	6	·	–	–	–	·	4	20	17			
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	60,3	18,2	18	11	–	·	–	21	13	1	–	–	–	·	3	8	·			
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44,4	14,7	28	16	–	·	–	7	5	2	–	–	–	·	12	5	1			
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27,8	14,1	22	8	–	·	–	10	6	1	–	–	–	2	7	5	·			
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	19,4	8,0	10	·	–	·	–	10	4	·	–	–	–	2	5	10	·			
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	55,9	13,3	9	–	–	–	–	10	7	3	–	–	–	3	10	5	·			
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	161,0	42,0	16	–	–	–	–	18	13	7	–	–	–	7	6	11	·			
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	102,2½	43,3½	12	–	–	–	–	10	9	3	–	–	–	·	·	9	·			
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	76,1	14,1	22	–	–	–	–	18	15	1	–	–	–	·	1	16	·			
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9,3	4,9	20	–	–	–	–	7	2	·	–	–	–	·	–	–	·			
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	14,4	5,6	24	–	–	–	–	7	4	·	–	–	–	·	3	19	·			
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41,7	12,0	14	–	–	–	–	14	7	1	–	–	–	·	5	17	9			
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	647,4½	43,3½	12.VIII	–	–	–	–	142	91	19	–	–	–	14	–	–	27			

Legionowo — $H_s = 93\ m$ — $H_b = 103,7\ m$ — $h_w = 10\ m$

I	1	2,5	4,5	4,7	7	5,9	4,5	3,0	4,5	2,3	19	4,1	3,8	6,3	8,5	5,0	6	4,7	10,9	3,3	31	24	10	4	·	10	4	·	6	1	4	·	1	20	8			
II	3	2,8	7,5	4,5	1,5	1,0	6	4,0	15,5	4,5	17,5	4,2	22,5	5,2	7,5	3,6	3	4,2	32,6	11,2	18	12	1	·	·	17	9	1	2	1	3	·	1	15	7			
III	9	4,1	13,5	4,2	13	4,8	9	6,9	6,5	4,0	8,5	4,1	21	6,2	8,5	5,5	4	4,9	26,4	12,1	15	19	3	·	·	8	5	1	8	2	·	·	7	7	1			
IV	19	2,4	19,5	3,2	11	3,0	2	5,2	5,5	4,0	9	4,1	2,5	2,6	19,5	2,7	2	3,0	9,2	3,8	30	7	·	·	4	8	3	·	1	·	3	3	4	8	1			
V	16,5	2,9	8,4	2,8	9	3,2	6,5	2,8	3	2,7	5,5	2,5	7	5,6	14,5	3,4	7	2,9	26,5	9,0	9	2	·	·	1	6	3	·	1	·	1	·	3	9	·			
VI	1,6	2,5	15,5	2,5	4,5	2,1	1	3,0	5,5	3,4	5	4,1	2,3	4,2	10,5	4,2	9	3,0	24,6	7,5	4	·	·	·	10	7	6	·	·	·	·	4	6	7	·			
VII	10,5	2,1	1,6	2,6	8	3,0	5	3,1	8	4,1	9,5	2,8	2,0	3,7	14	3,2	2	3,0	101,0	21,5	16	·	·	·	14	18	15	2	·	·	2	8	2	12	·			
VIII	8,5	1,7	5	1,9	6	2,8	4,5	1,4	7	3,3	8,5	4,3	3,4	4,3	11,5	2,8	8	3,1	53,5	15,5	10	·	·	·	–	15	10	2	·	·	1	4	2	6	·			
IX	4,5	2,1	0,5	3,0	2	1,0	5,5	3,2	8	2,8	2,2	4,2	2,6	6,4	15,5	3,3	6	4,0	68,9	16,3	23	·	·	·	–	15	11	2	6	·	1	1	2	7	·			
X	3	1,7	1	1,0	5,5	1,4	5	1,9	8	2,1	3,1,5	3,5	2,4	4,5	8	3,2	7	3,0	5,2	2,2	20	·	·	·	–	6	1	·	·	·	4	·	4	7	·			
XI	3,5	9,3	1,3	3,7	2,1	3,4	8	3,9	4,5	5,2	10	3,3	18,5	5,5	3,5	5,9	8	4,0	9,9	5,8	28	11	–	·	–	8	2	·	6	1	3	·	2	16	·			
XII	5	2,7	6	4,2	6	2,9	5,5	2,3	8,5	2,9	2,4,5	4,7	2,2,5	4,6	5	4,4	10	3,6	25,1	7,1	8	24	9	3	·	11	7	·	3	1	5	·	1	17	11			
Rok	99,5	3,1	12,6	3,2	9,4,5	2,9	6,2,5	3,4	8,4,5	3,4	17,0,5	3,8	2,5,9	4,9	12,6,5	3,9	72	3,6	393,8	21,5	16.VII	99	–	7	–	129	76	8	33	6	27	20	35	131	28			

Michorzewo

$\varphi = 52°22'$ $\lambda = 16°21'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.3	0.7	-0.6	-0.4	1.9	-3.2	10.4	6	-15.5	16	–	–	–	–	–	–	–	–	8.1	8.2	7.4	7.9
II	–	–	–	–	1.6	5.3	2.9	3.2	6.4	0.4	10.4	2	-3.6	24,25,26	–	–	–	–	–	–	–	–	7.8	8.7	6.4	7.6
III	–	–	–	–	0.9	7.3	3.3	3.7	8.8	0.0	16.7	13	-5.1	3	–	–	–	–	–	–	–	–	4.9	5.9	4.2	5.0
IV	–	–	–	–	3.4	11.8	6.5	7.0	13.3	1.5	22.8	28,29	-4.7	14	–	–	–	–	–	–	–	–	5.4	6.5	4.4	5.4
V	–	–	–	–	8.3	14.5	10.1	10.8	16.2	4.4	25.6	19	-1.7	28	–	–	–	–	–	–	–	–	4.8	6.7	5.6	5.7
VI	–	–	–	–	14.1	21.2	17.9	17.8	23.6	9.4	30.4	30	6.0	15,16	–	–	–	–	–	–	–	–	5.2	5.6	4.7	5.2
VII	–	–	–	–	16.2	21.3	18.5	18.6	23.4	13.8	32.6	4	8.0	3	–	–	–	–	–	–	–	–	6.4	7.1	6.7	6.7
VIII	–	–	–	–	13.4	19.1	14.9	15.6	20.7	11.5	27.3	11	6.2	23	–	–	–	–	–	–	–	–	6.3	7.7	6.2	6.7
IX	–	–	–	–	9.4	14.6	11.0	11.5	16.3	7.3	27.8	8	-0.4	26	–	–	–	–	–	–	–	–	7.2	8.1	7.0	7.4
X	–	–	–	–	6.5	12.3	8.6	9.0	13.4	4.9	20.5	19	-1.7	2	–	–	–	–	–	–	–	–	7.7	6.8	6.2	6.9
XI	–	–	–	–	2.8	6.0	3.8	4.1	7.0	1.1	15.3	5	-6.5	30	–	–	–	–	–	–	–	–	8.6	8.6	7.8	8.3
XII	–	–	–	–	-1.9	-0.5	-1.1	-1.1	1.5	-3.7	8.7	8	-16.8	16	–	–	–	–	–	–	–	–	8.2	8.3	7.2	7.9
Rok	–	–	–	–	6.1	11.2	8.0	8.3	12.7	4.0	32.6	4.VII	-16.8	16.XII	–	–	–	–	–	–	–	–	6.7	7.4	6.9	7.0

Plewiska

$\varphi = 52°22'$ $\lambda = 16°48'$

I	–	–	–	–	-1.3	0.8	-0.6	-0.4	2.0	-3.4	9.6	6	-18.1	16	–	–	–	–	–	–	–	–	8.3	7.9	7.5	7.9
II	–	–	–	–	1.8	5.4	3.0	3.3	6.1	0.0	9.6	14	-4.5	27	–	–	–	–	–	–	–	–	6.6	6.9	5.1	6.2
III	–	–	–	–	1.4	7.4	3.6	4.0	8.7	-0.2	15.9	26	-5.6	3	–	–	–	–	–	–	–	–	4.8	5.1	3.7	4.5
IV	–	–	–	–	5.1	12.2	6.6	7.6	13.8	1.6	24.1	28	-4.4	14	–	–	–	–	–	–	–	–	5.7	6.5	4.6	5.6
V	–	–	–	–	9.5	14.9	10.2	11.3	16.3	4.9	25.2	19	-1.4	7	–	–	–	–	–	–	–	–	4.4	6.2	4.3	5.0
VI	–	–	–	–	16.0	22.0	16.6	17.8	23.7	11.2	34.5	19	5.7	15	–	–	–	–	–	–	–	–	3.8	5.4	3.8	4.3
VII	–	–	–	–	17.6	22.3	17.8	18.9	23.9	14.5	33.5	5	10.4	29	86	67	86	80	3.1	10.4	3.2	5.6	6.5	6.4	6.0	6.3
VIII	–	–	–	–	14.5	19.6	15.0	16.0	21.1	11.3	27.6	11	6.5	23	91	67	87	82	1.6	8.1	2.4	4.0	5.6	5.9	5.5	5.7
IX	–	–	–	–	9.9	15.2	10.9	11.7	16.7	7.3	28.1	8	0.0	27	94	74	90	86	0.8	5.3	1.4	2.5	6.4	7.7	4.5	6.2
X	–	–	–	–	6.8	12.5	8.1	8.9	13.5	4.6	20.6	19	-1.8	2	94	76	92	87	0.6	3.7	0.9	1.7	6.6	5.8	3.9	5.2
XI	–	–	–	–	3.2	6.4	4.1	4.4	7.3	1.5	16.6	5	-6.4	30	89	80	86	85	0.8	2.1	1.1	1.3	7.7	8.2	6.9	7.6
XII	–	–	–	–	-1.6	0.2	-0.7	-0.7	1.3	-3.5	9.2	8	-14.6	17	–	–	–	–	–	–	–	–	7.9	7.9	5.9	7.2
Rok	–	–	–	–	6.9	11.6	7.9	8.6	12.9	4.2	33.5	5.VII	-18.1	16.I	–	–	–	–	–	–	–	–	6.2	6.7	5.1	6.0

Słubice

$\varphi = 52°21'$ $\lambda = 14°36'$

I	–	–	–	–	-0.4	1.9	0.5	0.6	3.0	-2.6	11.6	6	-15.7	4	89	81	88	86	0.7	1.4	0.8	1.0	8.3	7.5	6.5	7.4
II	–	–	–	–	2.1	5.9	3.4	3.7	7.1	0.4	13.2	5	-7.4	26	92	77	90	86	0.6	2.2	0.8	1.2	7.0	8.4	5.4	6.9
III	–	–	–	–	1.5	8.7	4.8	5.0	10.8	0.0	17.3	13	-8.0	2	89	59	77	75	0.9	5.0	2.2	2.7	5.2	5.9	3.9	5.0
IV	–	–	–	–	4.3	12.0	6.8	7.5	13.5	1.2	23.4	28	-6.6	14	91	55	79	75	0.7	6.9	2.2	3.3	4.6	6.1	3.7	4.8
V	–	–	–	–	8.2	14.8	9.5	10.5	16.2	3.7	26.4	16	-3.8	9	82	51	76	70	2.1	9.3	3.1	4.8	5.0	6.6	3.7	5.1
VI	–	–	–	–	15.3	21.7	16.5	17.5	23.3	10.0	31.4	11,29	5.8	13,14	78	52	75	68	4.0	14.0	4.9	7.6	4.5	5.6	4.3	4.8
VII	–	–	–	–	17.0	21.7	18.1	18.7	23.5	13.7	33.6	4	8.5	3	88	68	83	80	2.6	10.0	4.2	5.6	6.7	7.0	6.5	6.7
VIII	–	–	–	–	14.0	19.2	14.9	15.6	20.9	11.0	27.0	11	6.9	23	90	66	86	81	1.7	8.1	2.6	4.1	6.6	7.5	4.7	6.3
IX	–	–	–	–	9.7	15.5	10.9	11.8	16.7	7.1	28.6	8	-1.4	26	92	67	88	82	1.0	6.2	1.7	3.0	7.4	7.7	4.9	6.7
X	–	–	–	–	7.7	13.2	9.1	9.8	14.0	5.4	20.4	10	-1.7	2	93	74	89	85	0.9	4.1	1.3	2.1	7.6	7.2	5.4	6.7
XI	–	–	–	–	3.5	7.1	4.5	4.9	8.0	1.8	15.2	4	-6.9	21	91	80	88	86	0.8	2.3	1.0	1.4	6.8	7.8	7.4	7.3
XII	–	–	–	–	-0.7	4.2	-0.1	0.1	2.4	-2.9	10.5	8	-17.2	16	92	87	91	90	0.5	0.9	0.6	0.7	8.2	7.7	6.5	7.5
Rok	–	–	–	–	6.6	11.9	8.2	8.8	13.3	4.1	33.6	4.VIII	-17.2	16.XII	89	68	84	80	1.4	5.9	2.1	3.1	6.5	7.1	5.2	6.3

Paproć

$\varphi = 52°19'$ $\lambda = 16°09'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	15.6	21.6	16.7	17.6	24.6	9.9	30.9	30	6.0	2	–	–	–	–	–	–	–	–	4.2	4.7	3.6	4.2
VII	–	–	–	–	17.3	21.9	18.3	19.0	23.5	13.6	32.6	4	6.4	3	87	69	84	80	2.8	9.6	3.9	5.4	6.3	5.6	6.2	6.0
VIII	–	–	–	–	13.9	19.2	14.6	15.6	20.9	10.8	27.4	11	4.9	23	92	69	91	84	1.3	7.3	1.5	3.4	5.9	5.6	3.1	4.9
IX	–	–	–	–	9.4	15.2	10.6	11.4	16.6	6.2	28.4	8	-2.9	26	94	72	91	86	0.7	5.3	1.2	2.4	6.2	5.8	4.0	5.3
X	–	–	–	–	6.4	13.1	8.1	8.9	13.9	4.0	20.7	19	-3.8	2	95	73	92	87	0.5	4.3	1.0	1.9	5.9	5.2	3.7	4.9
XI	–	–	–	–	3.1	6.7	4.4	4.6	7.4	1.3	16.1	5	-7.6	30	93	81	91	88	0.6	2.1	0.8	1.2	6.9	7.3	6.4	6.9
XII	–	–	–	–	-1.5	0.6	-0.5	-0.5	1.7	-3.6	9.4	8	-17.3	17	93	88	92	91	0.3	0.7	0.4	0.5	6.0	7.2	5.8	6.3
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Michorzewo $H_s = 85\,m$ 1957

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	LICZBA DNI (n) Temperatura T ≤ 0	T ≥ 25	T max ≤ 0	T max ≥ 30	Opady ≥ 0.1	≥ 1.0	≥ 10.0	Wiatr ≥ 8	≥ 15	T	▲	●	■
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	114	46	6	20	9	4		6	5		–	–	9		4	21	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	444	70	18	12				15	13		–	–	2			12	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	380	–	–	17				6	6	2	–	–	2		10	11	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	448	57	27	12				6	6		–	–	1		5	8	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	143	180	15	5			1	3	2	1	–	–		2	3	8	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	887	150	24				10	7	6	1	–	–		3	7	6	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1332	230	21				11	19	18	4	–	–		6	4	15	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	558	85	21				1	13	13		–	–		4	1	10	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	746	232	23	1			1	15	16	2	–	–	2		1	15	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51	22	24	2				4	2		–	–	8		4	15	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	88	25	28	11	2			7	4		–	–	1		2	25	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	324	128	8	23	9	4		8	7	1	–	–	4		1	19	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4595	232	23 IX	103	20	8	24	108	97	11	–	–	32	17	43	162	–

Plewiska $H_s = 80\,m$ $h_w = 10\,m$

I	·	·	3	2.7	4	4.2	6	2.5	5	2.6	3.0	2.6	20.5	4.4	3.5	7.1	21	26	–	–	–	–	25	8	2				1		–	–	4	22	–
II	2	3.5	3	3.7	2	3.5	6	3.7	9	2.6	3.2	2.7	6	4.0	3	5.7	21	23	–	–	–	–	15	1							–	–	3	6	–
III	4	2.0	2	2.0	1.5	3.9	1.3	4.7	6.5	2.5	12.5	3.1	4.2	5.7	8	3.0	20	3.0	42.7t	15.5	18		16						1		–	–	11	8	–
IV	16	2.8	10.5	1.8	3.5	2.6	3	3.7	1	2.0	7.5	2.7	9.5	3.1	11	3.0	28	19	120	30	30		11								–	–	4	8	–
V	4	3.2	1.6	3.8	7	2.9	6	3.3	2	2.5	4	2.5	10	7.7	1.9	3.5	25	29	167	8.1	6		5			1				2	–	–	6	5	–
VI	0.5	3.0	1.0	2.8	6	1.8	8	2.8	2	2.0	6	3.5	12.5	3.2	1.5	2.7	30	19	489	21.5	4					12					–	–	3	7	–
VII	5.5	2.3	2.5	2.6	4	3.0	7	3.1	3	2.2	10.5	2.6	17.5	2.9	2.3	3.3	20	23	1902	41.7	22					12				1		–	–	7	15	–
VIII	1.5	1.7	2	1.5	4	2.5	1	2.0	6	2.9	2.4	3.0	1.3	2.7	10.5	2.0	31	18	495	124	24					1					–	–	5	7	–
IX	·	·	·	·	·	·	·	·	4	2.8	2.3	3.4	1.9	3.3	7	2.8	37	19	951	21.9	23					1				1		–	–	4	9	–
X	0.5	2.0	·	·	1	2.0	2	1.5	6	2.5	3.4	2.6	12.5	2.9	4	2.6	33	17	87	27	24		4								–	–	2	18	–
XI	3	5.0	5.5	3.5	21.5	4.0	1.6	2.2	7	2.4	9.5	2.6	13.5	5.7	6	5.2	11	3.2	79	5.0	28		12	2						2	–	–	1	14	–
XII	3.5	4.0	5	3.2	11	4.0	1.8	2.8	·	·	11.5	3.3	12.5	3.3	9.5	2.5	22	2.5	–	–	–		23	9	3						–	–	4	14	–
Rok	40.5	2.5	59.5	2.3	7.9	2.9	8.6	2.7	51.5	2.2	204.5	2.9	158.5	4.1	116.5	3.6	299	2.3	–	41.7	22.VII		108	20	5	27				8	–	–	60	127	–

Słubice $H_s = 20\,m$ $h_w = 10\,m$

I	1.5	1.3	9	3.7	3.5	2.0	2	2.5	5	3.5	27.5	4.1	3.6	4.4	5.5	3.1	4	5.8	19.5	3.6	1.2	19	5	3		15	7	·	3	·	5	·	3	18	16
II	4	2.2	4	2.2	5	2.6	4	2.6	5	2.9	2.9	3.5	2.3	3.9	3	3.8	7	3.1	33.2	7.0	1.3	8				17	10		1	·	4	·	2	11	1
III	10.5	2.1	6	2.6	16.5	4.7	6.5	3.4	7.5	2.7	8	3.6	18.5	5.4	6.5	2.3	13	3.2	42.6	13.1	1.7	16				12	8	1	5	·	·	·	8	9	1
IV	19.5	3.1	1.3	3.5	4	2.0	2	2.0	·	·	2	2.0	8.5	3.9	2.0	3.0	21	2.4	15.8	5.7	2.5	12				8	4	·	1	·	3	1	5	3	
V	16.5	2.1	1.3	3.5	6.5	2.5	1.5	3.3	2	2.5	3.5	2.0	1.2	4.5	1.7	2.6	2.1	2.3	34.7	11.6	1.9	7			1	11	6	1	3	·	1	2	6	6	
VI	1.3	1.7	13.5	2.1	7	3.5	2	4.0	2	3.0	3.5	1.9	16.5	3.1	15.5	3.4	17	2.2	43.9	13.5	2.4				11	12	10	1	·	·	·	4	8	5
VII	1.3	2.7	6.5	1.5	2	2.2	1.5	2.3	0.5	3.0	6	1.8	2.5	3.3	22.5	2.8	1.6	2.3	184.3	26.8	1.0				10	19	18	6	·	1	12	3	12	
VIII	4	1.6	2.5	1.4	·	·	2	2.5	5.5	2.2	23.5	3.2	30.5	3.1	4.4	3.0	11	2.6	47.4	12.6	2.4				2	16	9	2	·	1	6	1	5	
IX	2	2.2	·	·	1	1.0	3	2.3	6.5	3.3	1.5	4.0	32.5	4.5	1.7	2.8	1.3	3.2	79.4	21.3	2.3	2			1	20	15	1	4	·	1	1	3	8	
X	2.5	1.0	1	1.0	1.5	2.3	5.5	3.0	7	2.5	26.5	3.1	2.5	3.2	7	3.8	1.7	2.5	16.1	7.7	1.9	3				11	5	·	1	·	9	·	2	12	
XI	3	4.0	1.4	3.2	17.5	2.9	5.5	2.6	6.5	2.3	9.5	3.9	1.6	5.1	3	7.8	1.5	3.1	17.1	6.7	0.8	11				9	5	·	2	·	4	·	3	15	
XII	6	2.6	6.5	2.2	2.5	1.8	6	1.7	1.3	2.6	2.0	4.4	2.1	4.7	9	2.7	9	3.1	41.9	9.2	0.8	20	4	4	·	16	10	·	4	·	7	·	2	15	11
Rok	95.5	2.2	89	2.2	67	2.3	41.5	2.7	60.5	2.5	174	3.1	263.5	4.1	140	3.4	164	2.8	575.9	28.8	10.VII	98	9	7	25	166	107	12	24	·	39	26	46	119	29

Paproć $H_s = 70\,m$ $h_w = 11\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	5.5	2.3	8	2.2	1.7	1.6	3.5	1.3	5.5	1.9	8	3.4	1.6	2.5	13.5	2.4	14	1.9	31.9	13.6	2.4				1.7	6	7	1			5	10	7	
VII	11.5	3.1	4.5	3.6	7.5	1.5	2	2.5	8.5	2.1	14.5	3.1	1.8	2.3	11.5	2.7	1.5	2.2	184.5	37.8	2.2				1.0	20	15	7			7	7	11	
VIII	6	2.3	0.5	3.0	5	2.6	1.5	3.7	10.5	2.2	21.5	3.4	1.7	2.4	11	2.3	2.0	2.1	53.1	9.7	2.4				3	17	12	·			3	5	4	5	
IX	0.5	1.0	0.5	1.0	2	1.0	2	1.5	14.5	2.0	22.5	3.7	2.5	3.6	5.5	2.8	2.0	2.4	83.7	21.0	2.3	2			1	17	17	1	2		9	3	7	6	
X	·	·	·	·	1.5	1.0	2	1.0	2.1	1.9	2.2	2.7	11.5	2.3	4	3.0	3.1	1.5	13.7	4.9	2.4	3				7	5	·	·	·	14		6	6	
XI	3	5.3	7.5	5.1	2.7	2.5	10.5	1.6	8	2.5	9.5	3.0	1.3	4.8	2.5	4.8	9	2.9	46.5	4.4	2.7	12	2			10	7	·	·	·	5	·	6	15	
XII	9	3.4	3.5	3.9	5.5	1.9	7.6	1.7	11.5	3.0	26.5	4.0	11.5	3.8	7	3.5	11	3.0	40.3	12.1	2.8	23	8	4		16	10	1	1	·	4	·	4	13	8
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Ostrowy

$\varphi = 52°18'$ $\lambda = 19°12'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max obs.	Data	Min obs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.8	0.2	-0.8	-0.8	0.9	-3.4	8.8	6	-15.6	16	–	–	–	–	–	–	–	–	8.5	7.6	7.0	7.7
II	–	–	–	–	1.8	4.7	3.1	3.2	5.2	0.6	9.6	14	-3.4	24	–	–	–	–	–	–	–	–	8.1	7.3	6.7	7.4
III	–	–	–	–	0.8	6.1	2.8	3.1	7.0	-0.6	14.6	31	-5.9	9	–	–	–	–	–	–	–	–	5.4	6.0	3.9	5.1
IV	–	–	–	–	5.2	11.9	7.3	7.9	13.0	2.6	26.2	30	-4.8	13	–	–	–	–	–	–	–	–	5.6	6.1	4.6	5.4
V	–	–	–	–	9.0	14.1	10.1	10.8	15.5	5.7	25.7	19	0.7	6	–	–	–	–	–	–	–	–	5.5	6.8	4.2	5.5
VI	–	–	–	–	16.0	21.1	16.8	17.7	23.3	11.6	28.9	19	7.1	15	–	–	–	–	–	–	–	–	3.8	4.3	3.8	4.0
VII	–	–	–	–	17.4	21.8	18.1	16.8	23.6	14.1	33.8	8	9.8	29	–	–	–	–	–	–	–	–	6.5	6.3	5.3	6.0
VIII	–	–	–	–	14.2	19.4	14.8	15.8	21.3	11.7	26.7	11	6.1	24	–	–	–	–	–	–	–	–	4.6	6.6	4.3	5.2
IX	–	–	–	–	9.5	14.6	11.3	11.7	16.0	8.0	27.6	9	0.7	27	–	–	–	–	–	–	–	–	6.5	7.2	5.5	6.4
X	–	–	–	–	6.5	12.1	8.5	8.9	12.8	5.1	19.9	19	0.3	2	–	–	–	–	–	–	–	–	5.3	6.0	3.0	4.8
XI	–	–	–	–	3.8	6.1	4.2	4.6	7.4	2.4	16.0	4,6	-7.4	29,30	–	–	–	–	–	–	–	–	7.3	7.5	6.3	7.0
XII	–	–	–	–	-2.0	-0.2	-1.9	-1.6	0.9	-4.1	8.0	9	-17.0	16,17	–	–	–	–	–	–	–	–	6.0	8.4	6.4	6.9
Rok	–	–	–	–	6.7	11.0	7.9	8.4	12.2	4.5	33.8	8.VII	-17.0	16,17.XII	–	–	–	–	–	–	–	–	6.1	6.7	5.1	6.0

Warszawa – Bielany

$\varphi = 52°17'$ $\lambda = 20°58'$

I	1007.3	1018.6	990.5	1020.6	-2.0	0.0	-1.2	-1.1	1.0	-3.4	7.4	6	-14.9	16,17	90	86	90	89	0.5	0.8	0.6	0.6	8.0	8.8	6.3	7.7
II	998.0	1019.8	973.9	1011.1	1.5	4.3	2.6	2.8	5.6	0.3	10.5	14	-3.7	28	94	81	87	87	0.4	1.7	0.9	1.0	8.7	9.4	7.4	8.5
III	1005.8	1021.6	980.6	1019.0	-0.2	5.6	2.7	2.7	7.5	-1.4	16.4	31	-7.9	4	81	54	74	70	1.2	4.9	2.1	2.7	5.9	7.5	4.6	6.0
IV	1004.9	1017.7	980.9	1017.8	5.7	11.0	8.7	9.0	14.7	3.9	26.2	30	-5.3	10	84	49	70	68	1.8	9.2	3.7	4.9	5.9	6.2	5.3	5.8
V	1003.0	1013.7	992.4	1015.7	9.5	14.3	10.9	11.4	16.1	6.5	27.4	19	0.7	6	77	54	70	68	2.9	8.5	4.3	5.2	5.1	7.4	4.7	5.7
VI	1003.8	1017.8	992.0	1016.1	16.2	21.9	17.7	18.4	24.2	12.4	31.6	19	7.8	27	74	51	71	65	4.9	13.8	6.5	8.3	4.9	5.8	4.1	4.9
VII	999.0	1009.4	988.5	1011.2	17.4	22.7	19.0	19.5	24.7	15.0	33.7	5	10.4	29	84	62	79	75	3.3	11.8	5.0	6.7	7.2	7.3	5.9	6.6
VIII	1001.2	1010.5	988.5	1013.5	14.5	19.9	16.1	16.6	21.9	12.4	29.9	12	7.5	30	90	67	84	80	1.7	8.5	3.0	4.4	5.7	6.9	4.5	5.7
IX	999.4	1009.4	982.7	1012.0	9.9	15.0	11.7	12.1	16.8	8.5	28.6	9	0.7	26	92	72	86	83	1.0	5.6	2.2	2.9	6.2	8.0	5.2	6.5
X	1006.3	1017.4	992.8	1019.2	6.5	12.1	8.8	9.1	13.5	5.5	21.0	19	0.9	2,3	93	72	87	84	0.7	4.3	1.5	2.2	6.1	7.6	5.7	6.5
XI	1008.7	1028.8	990.7	1021.8	3.5	6.3	4.2	4.6	7.5	2.3	16.4	5	-7.9	30	91	77	87	85	0.6	2.3	1.0	1.3	8.1	7.8	7.5	7.8
XII	1002.4	1020.3	960.9	1015.6	-2.0	-0.3	-1.3	-1.2	1.2	-3.6	7.7	14	-14.7	17	90	84	89	88	0.5	0.9	0.6	0.7	7.1	8.9	6.8	7.6
Rok	1003.3	1028.8	960.9	1016.2	6.7	11.2	8.3	8.6	12.9	4.9	33.7	5.VII	-14.9	16,17.I	87	67	84	78	1.6	6.0	2.6	3.4	6.6	7.6	5.7	6.6

Uwaga. Wartości ciśnienia atmosferycznego w miesiącach I–X są za niskie przeciętnie o około 0,4 mb, w XI – za wysokie o około 0,4 mb.

Warszawa, Obserw. Astr. UW

$\varphi = 52°13'$ $\lambda = 21°02'$

I	1008.3	1017.8	989.6	1021.0	-2.0	-0.1	-1.1	-1.1	1.2	-3.4	7.5	6	-14.8	16	91	85	90	89	0.5	0.9	0.6	0.7	8.4	7.9	6.6	7.8
II	997.1	1018.4	973.1	1011.4	1.5	4.3	2.5	2.7	5.6	0.4	10.0	14	-4.0	28	92	81	89	87	0.5	1.7	0.8	1.0	7.8	9.4	6.5	7.9
III	1004.8	1020.9	979.8	1019.3	-0.2	5.9	2.6	2.7	7.6	-1.4	16.8	31	-8.3	4	83	56	78	72	1.1	4.8	1.8	2.6	5.5	5.6	4.4	5.2
IV	1004.0	1016.7	979.7	1018.2	5.7	11.2	8.8	9.1	14.9	4.1	26.0	27,29	-4.4	10	83	52	78	69	1.7	8.7	3.3	4.6	4.9	5.6	4.7	5.1
V	1002.0	1012.9	990.9	1015.9	8.9	14.3	10.7	11.2	15.9	6.7	26.3	19	0.2	6	82	60	75	72	2.2	7.6	3.5	4.4	5.1	7.6	5.2	6.0
VI	1002.8	1017.0	990.5	1016.4	15.6	22.4	17.6	18.3	24.4	12.8	31.4	19	8.8	27	79	54	74	69	3.7	13.4	5.5	7.5	4.5	5.8	3.8	4.7
VII	998.1	1008.6	987.5	1011.6	17.0	22.6	18.7	19.2	24.5	15.0	33.1	8	10.3	29	87	65	80	77	2.7	11.1	4.7	6.2	7.0	6.9	5.3	6.4
VIII	1000.3	1009.6	987.6	1013.9	14.0	20.1	16.0	16.5	21.9	12.6	30.0	12	7.5	24	91	65	84	80	1.5	8.9	3.1	4.5	5.5	7.2	4.5	5.7
IX	998.5	1008.7	984.9	1012.4	9.7	15.1	11.5	12.0	16.7	8.7	28.5	9	4.6	26	91	69	86	82	1.1	6.1	2.0	3.1	6.3	7.6	6.1	5.9
X	1005.6	1016.8	994.6	1019.8	6.2	12.2	8.7	9.0	13.3	5.4	20.5	19	4.4	2	92	72	87	84	0.8	4.4	1.6	2.2	7.2	7.2	5.8	6.7
XI	1007.0	1027.0	989.0	1021.4	3.3	6.2	3.9	4.3	7.7	1.9	16.3	4	-8.0	30	91	78	89	86	0.6	2.2	0.9	1.2	8.4	7.7	7.2	7.8
XII	1000.7	1019.1	959.2	1015.3	-2.0	-0.3	-1.4	-1.3	0.8	-3.9	6.8	9	-16.5	17	89	84	91	88	0.6	1.0	0.5	0.7	7.1	8.5	6.8	7.5
Rok	1002.3	1027.0	959.2	1016.5	6.5	11.3	8.2	8.6	12.9	4.9	33.1	8.VII	-16.5	17.XII	88	68	83	80	1.4	5.9	2.4	3.2	6.5	7.2	5.6	6.4

Warszawa – Okęcie

$\varphi = 52°11'$ $\lambda = 20°58'$

I	1008.0	1019.7	994.1	1021.6	-2.1	0.0	-1.2	-1.1	0.9	-3.9	7.5	6	-14.9	17	89	85	88	87	0.6	0.9	0.7	0.7	8.4	8.3	6.9	7.9
II	998.6	1020.2	974.1	1012.0	1.4	4.4	2.3	2.6	5.5	-0.2	9.9	21	-4.1	28	92	80	88	87	0.5	1.7	0.9	1.0	8.2	8.6	7.5	8.1
III	1006.3	1022.4	984.1	1019.8	-0.1	5.8	2.5	2.7	7.4	-1.7	16.2	31	-8.1	4	82	57	76	72	1.1	4.6	1.8	2.5	6.2	5.6	4.9	5.6
IV	1008.4	1018.4	984.2	1018.6	5.5	12.9	8.0	8.6	14.2	3.0	25.4	27	-5.0	10	85	54	75	70	1.5	8.7	2.9	4.4	6.0	5.7	5.8	5.8
V	1005.3	1014.2	992.5	1016.4	9.3	14.0	10.3	11.0	15.4	5.9	26.4	19	-1.2	6	79	57	75	70	2.6	7.7	3.3	4.5	5.1	7.3	5.4	5.9
VI	1004.0	1018.4	994.7	1016.7	15.8	21.6	17.0	17.8	23.2	11.2	30.3	11	6.1	27	77	52	74	68	4.2	13.0	5.3	7.5	4.8	5.6	4.5	5.0
VII	999.4	1009.9	988.6	1011.7	17.2	22.3	17.9	18.8	23.8	13.7	32.5	8	7.8	29	85	63	83	77	3.0	11.2	3.7	6.0	6.6	6.5	5.8	6.3
VIII	1001.6	1011.2	988.6	1014.2	14.3	19.9	15.3	16.2	21.4	11.1	29.4	12	5.4	24	89	63	86	79	1.8	9.2	2.5	4.5	5.2	7.0	4.8	5.7
IX	999.9	1010.3	983.3	1012.7	9.8	15.2	11.1	11.8	16.4	7.6	27.7	9	0.0	27	90	65	87	81	1.3	6.7	1.8	3.3	5.9	7.5	5.6	6.3
X	1007.1	1018.2	992.9	1020.3	6.1	12.3	7.9	8.6	13.2	4.3	20.7	19	0.5	3	92	70	89	84	0.8	4.7	1.3	2.3	6.3	7.0	6.0	6.4
XI	1008.3	1028.5	990.3	1021.7	3.2	6.4	3.7	4.2	7.4	1.3	16.5	4	-8.1	30	90	76	88	85	0.7	2.5	0.9	1.4	8.2	7.8	7.2	7.7
XII	1002.2	1020.5	960.7	1015.7	-2.2	-0.3	-1.6	-1.4	0.8	-4.3	7.1	13,14	-18.9	16	90	85	89	88	0.5	0.9	0.6	0.7	7.3	8.3	6.9	7.5
Rok	1003.7	1028.5	960.7	1016.9	6.5	11.2	7.8	8.3	12.5	4.0	32.5	8.VII	-18.9	16.XII	87	67	83	79	1.6	6.0	2.1	3.2	6.5	7.1	5.9	6.5

Ostrowy

$H_s = 120\ m$ $h_w = 11\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU °D. °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (r) Temperatura T Min<0°	Max<0°	Min<-10	Max>25	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v >10	>15	≡	≈	◉	▥
I	1	2.0	3	3.3	4	3.1	14	4.3	7	1.6	15	1.9	2.0	3.2	5	3.9	24	1.8	27.2	8.8	31	22	11	3	·	6	6	·	·	·	–	·	4	21	–
II	4	2.5	5	1.6	4.5	1.6	7.5	1.9	13	1.5	16	2.7	1.8	3.0	4	5.2	12	2.1	40.6	9.8	18	11	·	·	·	14	10	·	·	·	–	·	1	14	–
III	6.5	4.0	9	5.7	2.3	4.6	18.5	3.3	3.5	2.6	7.6	4.5	1.6	4.2	2	4.2	7	3.9	28.8	9.0	17	18	1	·	·	6	5	·	4	1	–	·	7	11	–
IV	1.8	3.9	8.5	3.9	5	2.0	11	3.2	8.5	2.8	8.5	2.8	10.5	3.0	10	3.4	10	2.9	11.5	5.0	30	8	·	·	1	8	5	·	1	·	–	1	8	10	–
V	14.5	4.1	12	3.6	18.5	2.7	11	3.4	10.5	2.2	4.5	4.1	6.5	3.7	11.5	3.5	4	3.2	25.4	7.2	20	·	·	·	1	6	5	·	·	·	–	1	4	8	–
VI	4.5	3.8	4.5	3.8	8.5	2.9	17.5	2.5	1.4	2.5	1.3	2.9	9.5	3.4	2.5	3.4	13	2.4	61.5	21.4	9	·	·	·	9	10	7	3	·	·	–	4	11	7	–
VII	5.5	2.9	11	3.4	9.5	3.5	8	3.1	19.5	1.8	11.5	4.0	12.5	4.4	4.5	4.9	11	2.9	157.9	26.2	12	·	·	·	13	16	12	7	·	·	–	2	6	11	–
VIII	3	2.2	3	1.2	2.5	2.5	6	2.2	23.5	2.3	23.5	2.7	19.5	2.5	8	2.3	4	2.3	84.2	25.3	16	·	·	·	3	13	9	1	·	·	–	2	5	6	–
IX	2.5	2.4	2.5	1.4	3.5	1.3	5.5	1.5	2.0	2.0	1.4	2.4	2.2	3.4	1.0	3.6	10	2.2	82.0	12.7	1	·	·	·	2	2.0	16	1	·	·	–	3	2	9	–
X	1.5	3.3	1.5	3.3	2	1.8	1.4	2.7	2.3	1.9	2.0.5	2.7	1.5.5	3.1	6	2.2	9	2.1	7.7	4.8	2.0	·	·	·	·	4	2	·	·	·	–	·	5	4	–
XI	2.5	5.4	4	2.8	2.3.5	2.6	2.4	2.9	12.5	2.5	6	3.8	9	5.0	6.5	6.2	2	3.3	13.3	4.6	2.4	10	1	·	·	7	4	·	·	·	–	·	5	17	–
XII	4	1.6	3.5	1.6	8	2.2	13	2.3	14	1.8	12.5	2.2	2.3.5	4.1	8.5	1.9	6	2.2	43.2	16.4	14	24	8	3	·	12	8	1	1	·	–	·	·	12	–
Rok	6.7.5	3.2	6.7.5	3.0	11.2.5	2.6	1.5.0	2.5	1.6.9	2.1	1.5.2.5	3.1	1.8.2.5	3.6	7.8.5	3.7	11.5	2.6	56.3.4	26.2	12.VII	9.3	2.1	6	2.9	1.2.2	8.9	1.3	6	1	–	1.5	5.5	1.3.0	–

Warszawa – Bielany

$H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w =$ I–IX 17,7 m, X–XII 15 m

I	·	·	6.5	4.1	3.5	3.5	7	3.4	11.5	2.2	3.3	3.5	2.0	4.8	0.5	6.0	11	3.3	25.6	7.5	31	25	10	3	·	12	7	·	2	·	3	·	2	18	18
II	7.5	2.5	2	2.2	4	4.2	12	4.2	20.5	3.7	2.7	3.7	5.5	4.0	0.5	4.0	5	3.5	42.5	10.2	18	12	1	·	·	20	11	1	·	·	4	·	·	19	4
III	7.5	3.1	4	2.2	2.1	5.0	9	6.0	8	3.5	1.8	3.9	1.2	4.9	2.5	5.4	11	3.9	23.3	11.1	15	18	4	·	·	6	5	1	3	2	·	·	4	9	2
IV	6.5	3.4	1.2	2.9	9	2.3	5	3.4	10	3.0	10.5	2.4	14.5	2.2	12.5	2.6	10	2.4	11.2	2.7	22.3.0	6	·	·	4	7	5	·	·	·	4	4	6	1
V	14	3.3	10	3.0	11.5	3.1	5.5	3.5	3.5	1.6	9	3.6	10.5	2.7	1.8	3.2	11	2.8	34.0	12.5	9	·	·	·	1	6	3	2	·	·	1	1	4	8	·
VI	7.5	2.2	10	3.0	7.5	2.1	8.5	2.9	4.5	2.3	1.6	3.3	1.5	3.1	1.4	4.0	7	2.8	34.7	15.5	4	·	·	·	11	11	4	1	·	·	·	4	9	6	·
VII	5.5	3.0	11.5	2.9	6.5	3.2	9	3.8	8.5	2.2	2.3.5	2.5	1.6	3.6	7.5	2.4	5	2.8	83.9	37.1	16	·	·	·	14	16	10	2	·	·	2	9	4	14	·
VIII	·	·	3	1.7	6	3.5	9	3.0	6.5	2.1	3.4.5	3.3	1.9	2.9	6	2.5	9	2.7	80.5	18.0	10	·	·	·	4	14	12	3	1	1	·	3	4	7	·
IX	·	·	·	·	1	2.0	1.2	3.2	1.3	2.8	3.1.5	3.6	1.8.5	5.4	4	2.8	10	3.3	80.5	25.6	23	·	·	·	2	16	12	2	4	2	1	1	2	9	·
X	·	·	·	·	·	·	10	3.4	11	1.8	4.3.5	2.8	8.5	3.1	2	1.5	18	2.2	5.8	1.7	4	·	·	·	·	8	3	·	·	·	1	·	3	10	·
XI	3	6.5	9.5	4.5	8.5	2.8	2.9.5	3.3	8	2.0	4.5	2.1	1.3.5	3.5	6.5	4.8	7	3.2	19.0	10.4	28	11	2	·	·	8	6	1	3	1	2	·	2	19	·
XII	7.5	2.6	1	2.0	3.5	2.6	10	3.2	12.5	2.6	2.9	2.8	12	2.9	4.5	1.7	13	2.3	37.4	13.9	14	24	9	3	·	11	7	1	1	1	3	1	1	17	14
Rok	5.9	2.2	6.9.5	2.4	8.2	2.8	12.6.5	3.6	1.1.7.5	2.5	2.8.0	3.1	1.6.5	3.6	7.8.5	3.2	1.1.7	2.9	4.7.5.4	37.1	16.VII	9.6	2.6	6	3.6	1.3.5	8.5	1.4.4	1.4	7	1.7	2.3	3.9	1.4.1	3.9

Uwaga. Kierunki i prędkości wiatru w miesiącach I–IX – wg anemometru indukcyjnego.

Warszawa, Obserw. Astr. UW

$H_s = 110\ m$ $H_b = 114{,}8\ m$ $h_w = 25\ m$

I	·	·	1	3.0	9	3.7	3.5	2.1	8.5	2.2	2.4	4.0	3.2	6.5	7	7.0	8	4.4	33.5	8.9	6	24	10	3	·	14	8	·	–	–	6	·	4	20	20
II	2.5	3.8	4	2.8	3	1.0	4	2.5	19.5	3.3	1.5.5	5.8	2.1.5	6.0	6	4.5	8	3.7	48.7	14.3	18	8	1	·	·	22	15	1	–	–	5	·	1	15	3
III	6.5	6.0	10.5	2.9	7.5	5.8	16.5	4.9	11	5.3	6.5	5.2	18.5	6.7	8	4.9	8	4.8	29.3	13.7	15	18	3	·	·	9	5	1	–	–	·	·	10	9	2
IV	7.5	3.3	1.6	3.4	2.5	2.2	10.5	2.5	5	3.6	1.2	4.2	3	2.7	19.5	3.6	14	2.9	48.6	36.6	29	6	·	·	4	11	5	1	–	–	1	3	8	8	·
V	1.8	4.3	1.8	4.3	3.5	7.6	10	4.7	6	4.2	10	5.2	8	7.1	7.5	4.3	12	4.2	41.7	16.1	9	·	·	·	1	8	5	3	–	–	1	1	4	10	·
VI	9	4.8	13.5	3.7	2	4.0	10.5	4.0	5.5	5.2	6.5	7.0	24	6.0	13	5.6	6	4.8	27.9	10.5	4	·	·	·	12	11	5	1	–	–	·	5	8	6	·
VII	5.5	2.1	7.5	2.9	7	1.7	7.5	2.6	8.5	3.1	10	4.7	27	4.2	6	5.0	14	3.0	87.5	20.7	16	·	·	·	14	18	12	3	–	–	·	7	7	14	·
VIII	5	3.0	2	3.0	·	·	5.5	3.4	7.5	3.5	8.5	3.8	3.0.5	5.5	11	4.5	23	3.4	93.2	22.1	10	·	·	·	6	17	12	2	–	–	·	2	3	9	·
IX	3.5	1.3	1.5	1.7	·	·	1	1.0	7.5	3.3	2.2	5.7	30	6.0	4.5	5.4	20	4.0	65.9	12.9	15	·	·	·	2	15	12	2	–	–	·	·	2	11	·
X	1.5	2.3	·	·	2	2.0	3	2.0	12	2.8	2.9.5	3.3	2.4.5	4.6	3.5	2.4	17	2.8	9.1	3.8	1	·	·	·	·	10	3	·	–	–	1	·	3	12	·
XI	5	11.8	·	·	7	3.0	17	2.0	13	2.3	9	3.0	13.5	6.0	2.5	10.8	23	3.1	26.0	12.4	28	11	1	·	·	8	6	1	–	–	1	·	2	18	·
XII	8.5	1.9	3	2.0	·	·	2	2.5	9.5	1.6	2.7.5	6.1	11	5.2	7.5	4.9	24	3.2	45.2	17.1	14	25	10	3	·	13	7	2	–	–	·	·	3	17	18
Rok	72.5	3.7	77	2.5	43.5	2.6	91	2.8	11.3.5	3.4	1.8.1	4.7	2.4.3.5	5.5	96	5.2	1.7.7	3.7	5.5.6.6	36.6	29.IV	9.2	2.5	6	3.9	1.5.6	9.5	1.7	–	–	1.5	1.8	5.5	1.4.9	4.8

Warszawa – Okęcie

$H_s = 106\ m$ $H_b = 106.9\ m$ $h_w = 10{,}9\ m$

I	0.5	3.0	5	5.2	6	5.9	8.5	4.2	14.5	2.2	16.5	4.2	3.0	7.0	9	5.9	3	5.0	23.1	6.0	31	25	10	3	·	10	7	·	–	–	4	·	2	18	18
II	3	4.8	4.5	4.3	5	4.2	9	5.1	2.1	4.0	15.5	4.3	1.7	5.5	4	6.0	5	4.4	43.6	9.7	18	14	1	·	·	22	11	·	–	–	6	·	·	15	4
III	7	6.0	9.5	4.6	17.5	4.7	12.5	2.5	8	4.4	6	3.9	2.0.5	3.7	6	6.5	6	5.2	29.5	11.1	15	20	3	·	·	8	4	1	–	–	·	·	5	9	1
IV	11.5	4.1	11	4.8	7	3.1	8.5	2.8	6.5	2.8	5	3.9	16	2.9	12.5	3.6	12	3.0	34.9	21.2	29	8	·	·	1	12	5	1	–	–	1	1	5	7	·
V	10	3.8	18	4.7	10	3.5	9.5	2.8	5.5	2.6	3.5	2.6	9.5	5.1	17	4.3	10	3.5	37.9	22.1	9	1	·	·	1	5	3	1	–	–	2	1	3	10	·
VI	8	4.4	11.5	2.9	8	2.2	6.5	3.0	6.5	2.7	11.5	4.4	17.5	4.6	9.5	4.5	11	3.3	37.6	9.9	4	·	·	·	8	11	6	·	–	–	·	8	5	4	·
VII	1.5	3.7	7	3.7	9	2.9	7.5	2.6	11	2.8	17.5	3.1	2.4.5	3.7	11	5.5	7	3.0	88.5	22.2	16	·	·	·	11	17	11	2	–	–	3	1.0	4	11	·
VIII	4	3.2	0.5	2.0	3.5	2.6	12	3.0	7	2.4	2.3.5	4.0	26	4.0	7.5	4.3	9	3.3	98.5	22.8	10	·	·	·	5	16	13	4	–	–	1	4	1	6	·
IX	3	3.2	2	1.8	0.5	2.0	6.5	3.0	1.7.5	3.1	2.1	5.7	2.5.5	6.3	5	4.5	9	4.3	74.4	19.3	23	·	·	·	2	18	13	4	–	–	1	1	2	9	·
X	1	5.0	0.5	1.0	1.5	1.7	12.5	2.0	2.2.5	2.5	2.8	3.9	19.5	6.2	2.5	3.0	5	3.3	9.2	2.7	4	·	·	·	·	9	5	·	–	–	4	·	3	1.0	·
XI	5	1.0.0	6.5	4.7	17.5	3.5	2.1	4.9	7.5	2.9	9.5	5.5	12	7.3	1	12.0	10	4.7	18.1	7.9	28	12	1	·	·	7	6	·	–	–	5	·	2	17	·
XII	4.5	3.1	7	4.5	6.5	3.5	10	3.4	1.6.5	3.2	2.6	5.8	12	6.0	2.5	5.8	9	4.2	32.3	14.1	14	27	10	2	·	11	5	1	–	–	5	·	1	16	12
Rok	6.9	4.5	8.3	3.7	9.2	3.3	12.4	3.7	1.4.3	3.0	1.8.3.5	4.4	2.2.7	5.3	8.7.5	5.3	9.6	3.9	5.1.8.6	22.8	10.VIII	10.7	2.5	5	2.8	1.4.6	8.9	1.1	–	–	3.2	2.8	3.3	1.3.2	3.5

Jeziory

$\varphi = 52°16'$ $\lambda = 16°48'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI D_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia																					
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.4	1.1	-0.6	-0.4	2.0	-3.6	9.5	6	-16.9	17	91	85	91	89	0.4	1.1	0.5	0.7	8.3	8.2	6.5	7.7
II	–	–	–	–	1.4	5.5	2.5	3.0	6.1	-0.7	10.3	5;14	-5.6	27	92	77	91	87	0.5	2.1	0.7	1.1	7.2	7.5	4.7	6.5
III	–	–	–	–	0.9	7.7	3.0	3.6	9.3	-0.7	16.5	13	-7.0	3	87	64	86	79	0.9	4.1	1.2	2.1	4.0	5.0	2.6	3.9
IV	–	–	–	–	5.2	12.1	6.1	7.4	13.9	1.4	24.8	29	-5.5	14	82	55	81	73	1.7	7.2	1.9	3.6	4.7	6.5	3.x	4.9
V	–	–	–	–	9.6	14.8	9.6	10.9	16.2	4.7	25.6	19	-1.7	7	72	51	73	65	3.4	9.1	3.5	5.3	5.0	6.2	3.9	5.0
VI	–	–	–	–	16.2	22.2	16.0	17.5	23.6	10.1	30.7	19,30	6.2	2,14	74	51	77	67	5.2	14.5	4.4	8.0	4.4	5.0	3.9	4.4
VII	–	–	–	–	17.4	22.4	17.6	18.8	23.8	13.9	33.7	5	7.9	3	84	64	84	77	3.6	11.9	3.7	6.4	6.7	6.8	7.0	6.8
VIII	–	–	–	–	14.3	19.4	14.6	15.7	20.9	11.0	27.2	11	6.6	23	90	66	87	81	1.8	8.3	2.3	4.1	6.0	7.1	3.7	5.6
IX	–	–	–	–	9.8	14.8	10.7	11.5	16.4	7.1	27.4	8	-1.5	27	93	73	88	85	0.9	5.2	1.6	2.6	6.6	6.8	4.7	6.0
X	–	–	–	–	7.0	12.5	8.3	9.0	13.6	4.6	20.8	19	-2.0	2	93	75	91	86	0.7	3.9	1.0	1.9	6.3	6.5	3.2	5.3
XI	–	–	–	–	3.2	6.5	4.1	4.5	7.4	1.5	17.0	5	-7.2	30	87	79	85	84	1.0	2.3	1.2	1.5	7.4	7.8	6.4	7.2
XII	–	–	–	–	-1.7	0.2	-0.8	-0.8	1.4	-3.9	9.1	8	-15.7	17	89	87	90	89	0.6	0.8	0.6	0.7	7.4	7.7	6.6	7.2
Rok	–	–	–	–	6.8	11.6	7.6	8.4	12.9	3.8	33.7	5.VII	-16.9	17.I	86	69	85	80	1.7	5.9	1.9	3.2	6.2	6.7	4.7	5.9

Świebodzin

$\varphi = 52°15'$ $\lambda = 15°32'$

I	1011.1	1023.7	992.5	1024.8	-1.2	1.3	-0.2	-0.1	2.4	-3.2	10.6	6	-13.8	16	91	83	90	88	0.5	1.2	0.6	0.8	8.5	8.0	6.4	7.6
II	1000.5	1026.5	973.7	1011.0	1.6	5.5	3.0	3.3	6.7	-0.2	13.1	5	-5.1	25	93	78	90	87	0.5	2.1	0.7	1.1	8.9	8.5	6.2	7.8
III	1008.0	1029.3	985.7	1018.5	1.2	8.1	3.9	4.3	10.1	-0.4	17.0	26	-6.4	2	90	62	81	78	0.8	4.6	1.7	2.4	6.1	6.3	3.1	5.2
IV	1009.2	1021.9	987.0	1019.6	4.5	12.4	7.0	7.7	13.9	1.6	24.2	28	-5.0	14	88	52	78	73	1.0	7.6	2.3	3.6	6.3	6.0	3.5	4.9
V	1007.2	1019.4	997.3	1017.5	9.1	15.0	9.8	10.9	16.8	3.9	26.5	16	-1.8	7	76	49	74	66	2.9	9.4	3.3	5.2	5.1	7.4	4.2	5.6
VI	1007.1	1023.7	995.1	1017.2	15.6	22.0	16.4	17.6	23.8	10.2	31.7	19	6.3	15,26	75	53	76	68	4.6	14.0	4.6	7.7	4.6	5.6	3.7	4.6
VII	1003.1	1015.7	992.2	1013.0	17.5	22.4	18.2	19.1	24.1	13.8	34.2	4	8.6	3	84	62	81	76	3.7	12.1	4.3	6.7	6.4	7.2	7.0	6.9
VIII	1004.9	1016.1	992.0	1014.9	14.1	19.7	14.6	15.8	21.3	10.9	28.3	11	5.7	23	89	62	87	79	1.8	9.1	2.3	4.4	6.6	7.5	3.8	6.0
IX	1003.3	1015.5	984.2	1013.4	9.5	15.4	10.7	11.6	17.0	6.9	28.7	8	-1.4	27	92	66	88	82	1.0	6.3	1.5	2.9	7.1	8.4	4.7	6.7
X	1009.1	1019.7	992.4	1019.4	7.0	13.0	8.5	9.2	14.1	4.9	20.9	19	-2.0	2	93	71	89	84	0.8	4.6	1.2	2.2	8.8	7.1	4.2	6.7
XI	1010.8	1028.5	992.7	1021.4	2.6	6.4	3.9	4.2	7.5	1.1	16.0	5	-6.2	22	93	80	91	88	0.5	2.1	0.8	1.1	7.7	8.5	7.4	7.9
XII	1004.9	1022.9	963.2	1015.5	-1.6	0.5	-0.7	-0.6	1.9	-3.4	9.1	8	-17.3	17	94	90	94	93	0.2	0.6	0.4	0.4	8.7	7.6	6.5	7.6
Rok	1006.6	1029.3	963.2	1018.5	6.7	11.8	7.9	8.6	13.3	3.8	34.2	4.VII	-17.3	17.XII	88	67	85	80	1.5	6.1	2.0	3.2	7.0	7.3	5.1	6.5

Zbąszyń

$\varphi = 52°15'$ $\lambda = 15°56'$

I	–	–	–	–	-1.2	1.3	-0.2	-0.1	2.3	-3.8	10.6	6	-16.7	1	87	84	85	84	0.8	1.3	0.9	1.0	8.5	8.4	6.1	8.3
II	–	–	–	–	1.7	5.6	2.9	3.3	6.6	-0.2	12.9	5	-5.2	26	90	76	88	85	0.7	2.3	0.9	1.3	8.8	8.2	7.8	8.3
III	–	–	–	–	1.2	8.3	3.9	4.3	9.8	-0.7	16.9	27	-6.8	2	85	62	77	75	1.0	4.6	2.0	2.5	5.8	5.6	5.5	5.6
IV	–	–	–	–	4.7	12.8	7.0	7.9	14.3	1.2	26.7	28	-5.1	14	85	53	77	72	1.3	7.8	2.4	3.8	5.2	5.9	5.0	5.4
V	–	–	–	–	9.3	15.4	10.0	11.2	16.9	4.0	26.9	16	-2.1	9	74	49	72	65	3.0	9.7	3.5	5.4	5.5	7.1	5.4	6.0
VI	–	–	–	–	15.7	22.6	17.0	18.1	24.0	10.1	31.6	11	5.6	14	76	49	74	66	4.5	15.1	5.3	8.3	5.2	5.2	5.7	5.4
VII	–	–	–	–	17.4	22.5	18.7	19.3	24.1	13.9	33.4	4	7.0	3	85	65	79	76	3.5	11.5	4.9	6.6	6.7	7.1	7.5	7.2
VIII	–	–	–	–	14.1	19.7	15.3	16.1	21.2	11.5	27.7	11	6.3	25	90	64	85	80	1.6	8.9	2.7	4.4	6.4	7.5	7.3	7.1
IX	–	–	–	–	9.6	15.4	11.3	11.9	16.6	7.1	28.5	8	-1.3	26	92	68	86	82	0.9	6.1	2.0	3.0	7.2	7.9	7.1	7.4
X	–	–	–	–	6.6	13.2	8.8	9.4	14.1	4.6	24.0	19	-3.1	2	93	71	88	84	0.8	4.6	1.4	2.3	8.9	7.1	6.2	7.4
XI	–	–	–	–	2.9	6.6	4.2	4.5	7.4	1.2	15.9	5	-7.4	30	89	79	86	85	0.9	2.2	1.1	1.4	8.2	8.5	7.7	8.1
XII	–	–	–	–	-1.4	0.5	-0.5	-0.5	1.9	-3.7	9.5	8	-18.2	17	90	89	90	90	0.5	0.7	0.6	0.6	8.8	8.1	8.5	8.5
Rok	–	–	–	–	6.7	12.0	8.2	8.8	13.3	3.8	33.4	4.VII	-18.2	17.XII	86	67	82	78	1.6	6.2	2.3	3.4	7.1	7.2	6.8	7.0

Kórnik

$\varphi = 52°15'$ $\lambda = 17°06'$

I	–	–	–	–	-1.4	0.9	-0.7	-0.5	–	-3.2	–	–	-15.3	17	89	83	89	87	0.6	1.1	0.6	0.8	8.6	8.2	6.6	7.8
II	–	–	–	–	1.5	5.3	2.7	3.0	–	0.2	–	–	-4.9	27	92	76	88	85	0.5	2.2	0.9	1.2	8.2	7.8	4.7	6.9
III	–	–	–	–	1.1	7.3	3.4	3.8	–	-0.3	–	–	-5.4	3	84	59	82	75	1.1	4.5	1.5	2.4	5.6	5.4	3.0	4.7
IV	–	–	–	–	4.5	11.8	6.8	7.5	–	1.5	–	–	-5.4	13	85	52	77	71	1.3	7.5	2.4	3.7	5.8	6.1	4.2	5.4
V	–	–	–	–	9.0	14.6	10.0	10.9	–	4.1	–	–	-1.3	7	74	51	71	65	3.1	9.2	3.8	5.4	4.5	5.8	4.2	4.8
VI	–	–	–	–	15.7	21.7	16.7	17.7	–	10.1	–	–	5.1	15	75	49	76	67	4.7	14.5	5.0	8.1	5.0	5.3	4.7	5.0
VII	–	–	–	–	17.6	22.1	18.0	18.9	–	14.1	–	–	9.7	3	82	63	82	76	4.0	11.5	4.1	6.5	6.8	6.6	7.4	6.9
VIII	–	–	–	–	14.3	13.6	15.3	16.1	–	11.4	–	–	7.1	23	87	63	84	78	2.2	8.8	2.9	4.6	6.1	5.7	4.4	5.7
IX	–	–	–	–	9.6	14.8	11.2	11.7	–	7.4	–	–	-0.2	26	92	70	86	83	1.0	5.8	2.0	2.9	6.8	7.1	5.6	6.5
X	–	–	–	–	6.3	12.5	8.2	8.8	–	4.7	–	–	-1.5	2	94	72	90	85	0.7	4.4	1.1	2.1	7.5	6.7	3.5	5.9
XI	–	–	–	–	3.1	6.5	4.1	4.4	–	1.4	–	–	-7.2	30	84	76	82	81	1.1	2.6	1.4	1.7	7.4	7.6	7.6	7.5
XII	–	–	–	–	-1.6	0.4	-0.8	-0.7	–	-3.6	–	–	-15.1	17	84	82	84	83	0.8	1.1	0.9	0.9	7.2	7.9	6.6	7.2
Rok	–	–	–	–	6.6	11.5	7.9	8.5	–	4.0	–	–	-15.3	17.I	85	66	83	78	1.8	6.1	2.2	3.4	5.6	6.8	5.2	6.2

Jeziory

$H_s = 84\ m$ $h_w = 12\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D i mD)																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0	Max 0	Min<0	Max≥25	0.1 ÷ 1.0	1.1 ÷ 10.0	10.1 ÷	10 ÷ 15	15 ÷	≡	≈	◔	●	⊡
I	7	1.3	13	2.4	6	1.7	2	2.5	2	2.0	32	2.1	16	2.4	15	2.9	·	2.2	21.4	4.5	12	24	8	3	·	14	6	·	·	·	12	·	4	19	18
II	4	1.0	14	1.4	9	1.4	7	1.6	6	2.2	31	1.9	8	2.0	7	2.0	1	1.8	39.2	10.8	18	17	·	·	·	14	10	1	·	·	10	·	2	8	·
III	5	1.4	26	3.0	13	3.0	5	2.4	4	2.2	16	1.7	10	2.4	14	1.9	·	2.4	30.2	11.7	17	17	·	·	·	6	5	1	·	·	6	·	14	4	·
IV	18	1.5	28	1.6	7	2.0	2	3.0	·	·	4	1.0	10	2.0	20	1.9	4	1.7	19.9	4.9	7	12	·	·	·	10	7	·	·	·	3	·	6	6	·
V	14	1.4	32	2.4	9	2.1	·	·	·	·	3	1.7	2	2.5	30	2.0	3	2.0	14.2	7.0	6	4	·	·	2	6	3	·	·	·	·	2	5	3	1
VI	4	1.8	25	1.9	4	1.8	2	1.0	2	3.0	7	2.1	10	2.9	31	2.4	5	2.1	44.6	15.8	4	·	·	·	12	8	6	1	·	·	1	2	6	6	·
VII	13	2.0	17	2.6	5	2.2	2	1.5	1	1.0	10	1.7	6	3.2	32	1.9	7	2.0	171.2	36.4	21	·	·	·	12	23	13	5	·	·	6	4	4	14	·
VIII	5	1.2	6	1.5	2	1.0	2	2.0	5	1.6	10	2.1	12	1.7	45	1.4	6	1.5	49.1	14.4	21	·	·	·	1	15	10	1	·	·	5	2	3	7	·
IX	3	1.0	3	1.0	2	1.0	6	1.5	3	2.3	30	2.1	15	2.6	23	1.8	5	1.8	89.4	17.2	23	2	·	·	1	17	15	2	1	1	7	1	5	8	·
X	2	1.5	6	1.5	5	1.4	7	1.4	5	1.6	32	2.0	9	3.0	21	2.0	6	1.8	7.6	2.2	24	2	·	·	·	7	5	·	·	·	19	·	5	5	·
XI	2	4.0	43	2.1	10	1.6	3	1.0	1	4.0	21	2.1	3	2.3	5	3.4	2	2.1	7.1	3.2	28	12	1	·	·	7	2	·	·	·	8	·	3	18	·
XII	6	1.5	17	2.1	14	1.3	6	1.3	4	1.5	22	2.2	7	1.6	15	2.0	2	1.8	36.8	13.0	14	23	9	3	·	16	7	2	·	·	12	·	4	16	15
Rok	80	1.6	230	2.0	86	1.7	44	1.6	33	1.8	215	1.9	108	2.4	258	2.1	41	1.9	527.7	36.4	21.VII	113	18	6	28	143	95	13	1	1	89	11	63	114	34

Świebodzin

$H_s = 78\ m$ $H_b = 84{,}1\ m$ $h_w = 12\ m$

I	4.5	2.9	10	3.0	1	1.0	·	·	10	2.2	22.5	2.4	22	2.8	3	5.0	20	2.1	26.3	6.2	5	22	7	3	·	13	10				–	·	3	19	19
II	2.5	2.6	4	1.9	6.5	2.2	1	2.0	16	2.8	19	2.1	14.5	3.0	1.5	3.7	22	1.8	32.5	5.7	13	14	·	·	·	13	11	·	·	·	–	·	1	16	2
III	4	1.4	8	3.0	17	3.6	5.5	3.1	6	2.1	6.5	2.4	13.5	4.6	5.5	2.4	27	2.3	35.2	13.3	17	16	·	·	·	9	5	1	3	·	–	·	6	9	1
IV	25	2.7	7.5	2.5	6	1.9	·	·	3	1.7	5.5	3.8	7.5	2.5	9.5	2.5	26	1.8	18.1	6.3	19	11	·	·	·	8	6	·	·	·	–	·	4	6	1
V	7.5	1.7	14.5	2.5	6	2.7	1	2.0	3	1.7	1	1.0	14	3.2	14	4.0	35	1.8	34.7	25.3	23	2	·	·	2	7	5	1	1	·	–	4	4	6	·
VI	9.5	2.7	15	2.4	5	2.7	1	2.5	5	1.9	6	5.3	21	3.4	8.5	2.6	19	2.4	38.1	8.0	24	·	·	·	11	11	10	·	1	·	–	5	9	6	·
VII	12.5	2.8	5	2.7	4.5	1.8	4	2.0	2	1.5	9	5.0	34.5	3.0	10.5	4.3	11	2.7	136.1	19.3	14	·	·	·	11	16	15	6	·	·	–	4	2	17	·
VIII	7.5	1.7	3.5	3.3	1.5	3.0	1	4.0	3.5	7.4	27.5	4.1	40.5	3.6	4	3.1	4	3.6	66.5	13.4	9	·	·	·	3	15	14	2	6	·	–	2	1	6	·
IX	2	1.0	1	2.0	·	·	·	·	6	3.4	26	4.8	35	4.5	1	2.5	19	3.5	81.2	20.2	23	2	·	·	1	19	17	1	3	2	–	1	·	7	·
X	1.5	2.0	0.5	3.0	2	1.5	1.5	1.7	6.5	3.7	24.5	4.3	25	3.7	1.5	2.7	30	2.5	12.4	3.7	19	2	·	·	·	10	4	·	2	·	–	·	1	12	·
XI	8	3.8	17.5	3.7	18.5	2.5	0.5	2.0	3	4.2	11.5	3.3	13	5.5	4	6.6	14	3.2	11.4	3.9	28	12	·	·	·	11	5	·	1	·	–	·	2	20	·
XII	7.5	3.1	7.5	3.9	8.5	2.4	3.5	2.1	8.5	2.8	27.5	4.4	14.5	4.6	5.5	2.9	10	3.3	46.8	12.6	8	24	5	4	·	17	9	1	3	1	–	·	3	19	16
Rok	92	2.4	91	2.8	76.5	2.1	19	1.8	72.5	3.0	186.5	3.6	252	3.7	68.5	3.5	237	2.6	539.3	25.3	23.V	105	12	7	28	154	111	12	20	3	–	16	36	143	39

Zbąszyń

$H_s = 57\ m$ $h_w = 10\ m$

I	5.5	1.9	7	2.9	5	1.0	7	1.0	10.5	1.3	26.5	2.7	21	4.1	5.5	5.4	5	2.6	24.1	6.4	5	22	7	5	·	11	7	·	1	·	1	·	·	24	17
II	4.5	2.1	3.5	1.6	7.5	1.9	11.5	1.5	22.5	2.2	18.5	2.3	11	3.9	3	3.2	2	2.3	38.9	4.7	13	12	·	·	·	19	15	·	·	·		·	·	16	1
III	4	2.2	4.5	3.1	8.6	4.8	1.5	1.9	5.5	2.4	10	3.0	12	6.2	8	2.9	8	3.4	34.9	11.5	28	16	·	·	·	8	5	2	2	1	2	1	3	11	2
IV	19.5	2.6	8	2.2	8	1.8	5	1.5	1.5	1.0	6	3.2	9.5	3.4	21.5	3.2	11	2.4	12.8	3.3	2	12	·	·	1	9	4	·	·	·	1	1	4	4	·
V	1.1	2.0	17.5	2.8	1.1	1.8	8	2.3	1.5	1.7	7.5	3.1	1.1	3.9	15.5	3.2	10	2.4	24.2	15.3	23	3	·	·	2	5	5	1	·	·	·	3	2	6	·
VI	8.5	1.8	19.5	1.6	9	1.5	4.5	2.1	2	3.0	4.5	4.3	16.5	3.3	18.5	2.4	7	2.2	33.6	9.6	24	·	·	·	13	11	8	·	·	·	4	7	8	·
VII	1.4	2.2	8.5	1.6	4.5	1.4	6	1.4	5.5	2.5	14.5	3.2	17	3.1	1.5	2.9	8	2.3	147.2	41.1	22	·	·	·	12	17	14	5	·	·	·	10	1	16	·
VIII	4.5	1.3	2.5	1.4	2.5	2.2	2	2.8	1.3	2.7	2.3	3.6	2.6	3.0	9.5	2.5	10	2.6	65.4	12.4	7	·	·	·	3	18	11	2	·	·	1	5	·	13	·
IX	2	1.0	2	3.0	2.5	2.6	4.5	1.4	1.6	3.9	21.5	3.9	2.3	4.2	6.5	3.2	12	3.2	68.0	15.2	23	2	·	·	1	17	14	1	1	·	3	3	·	13	·
X	0.5	4.0	2.5	1.0	4	1.0	1.1	1.2	17.5	1.9	2.7	3.3	12.5	3.4	4	2.4	14	2.1	10.2	4.2	19	2	·	·	·	7	3	·	1	·	5	·	·	15	·
XI	4.5	5.9	1.3	3.2	28.5	2.7	8	2.0	2	4.0	14.5	4.2	10	5.3	3.5	6.4	6	3.4	5.6	3.8	28	12	1	·	·	7	1	·	1	·	3	·	2	22	·
XII	7	3.2	5.5	3.4	1.1	2.0	1.3	1.2	9	2.1	22.5	5.3	12	3.9	8	3.5	5	3.1	34.9	10.0	7	23	6	4	·	13	9	1	2	·	1	·	·	22	11
Rok	85.5	2.5	94	2.3	119.5	2.1	95.5	1.7	106.5	2.4	196	3.6	184.5	4.0	118.5	3.4	98	2.7	499.8	41.1	22.VII	104	14	9	32	142	96	12	8	1	17	27	19	170	31

Kórnik

$H_s = 77\ m$ $h_w = 10\ m$

I	2	2.0	6.5	4.6	6	4.4	1.5	1.0	1.4	1.8	27.5	4.1	20.5	5.3	5	5.5	10	3.6	27.9	6.9	6	22	–	2	–	14	7	·	3	·	–	·	3	21	18
II	2	2.0	4	2.0	6	3.1	1.1	2.8	1.5	4.3	2.6	4.0	8	4.8	4	4.6	8	3.4	45.9	14.2	18	15	–	·	–	17	11	1	2	·	–	·	1	9	·
III	3.5	4.0	7	5.3	18.5	5.4	1.9	1.7	6	3.8	12.5	4.1	6.5	8.5	8	5.0	12	4.4	29.0	12.4	17	17	–	·	–	7	6	1	7	2	–	·	9	6	·
IV	17.5	4.5	10	3.8	9	3.3	6.5	3.3	3.5	1.7	7.5	2.8	5	4.5	10	3.3	21	2.8	10.9	4.5	24	10	–	·	–	7	4	·	1	·	–	1	4	9	·
V	12	3.8	20	4.3	13	2.0	7.5	3.7	2	2.2	4	3.8	9	5.4	12.5	5.0	13	3.4	24.5	19.2	6	7	–	·	–	5	3	1	5	·	–	1	3	4	·
VI	5.5	3.8	11.5	2.9	15.5	2.6	11.5	3.1	6.5	3.3	8.5	3.5	6	3.7	14	4.2	11	2.9	66.3	37.8	4	·	–	·	–	10	8	1	1	·	–	3	11	8	·
VII	10.5	3.1	5	2.7	6.5	2.7	6	3.7	6	2.8	14	3.4	14	3.7	15	4.6	16	2.9	146.7	32.0	23	·	–	·	–	18	17	4	1	·	–	7	5	17	·
VIII	2.5	1.6	0.5	2.0	2.5	1.2	9	2.7	1.4	3.2	2.3	2.9	2.0	3.1	9.5	3.3	12	2.5	55.3	10.0	21	·	–	·	–	13	10	1	·	·	–	4	2	7	·
IX	1	2.0	·	·	0.5	1.0	7.5	2.1	13.5	2.6	2.6	3.7	16.5	5.4	11	4.2	14	3.2	99.7	23.6	23	1	–	·	–	17	15	4	4	1	–	2	2	8	·
X	1	5.0	1	3.0	·	·	8.5	1.9	1.8	2.4	2.5	3.5	1.3	3.0	2.5	2.8	24	2.2	5.3	2.0	24	1	–	·	–	7	3	·	·	·	–	·	4	5	
XI	2.5	3.6	4	4.6	21.5	3.8	20	2.4	7	3.1	8	4.7	12.5	6.4	4.5	7.3	10	3.8	9.6	5.4	28	12	–	·	–	8	2	·	4	1	–	·	3	17	·
XII	3.5	2.3	3.5	7.0	8	2.7	10.5	2.3	13.5	2.6	29.5	4.1	12	4.5	4.5	3.6	8	3.3	27.6	10.1	8	25	–	3	–	13	9	1	2	·	–	·	2	14	11
Rok	63.5	3.6	73	3.5	107	2.7	118.5	2.8	119	2.8	211.5	3.7	114.3	4.9	100.5	4.4	159	3.2	548.7	37.8	4.VI	108	–	5	–	136	95	14	30	4	–	18	49	125	99

Radzików

$\varphi = 52°13'$ $\lambda = 20°39'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.1	0.2	-1.2	-1.1	–	-3.4	–	–	-15.4	16	90	85	89	89	0.5	0.8	0.6	0.6	8.5	8.1	5.9	7.5
II	–	–	–	–	2.0	4.5	2.7	3.0	–	0.4	–	–	-3.4	4	–	–	–	–	–	–	–	–	8.4	7.9	7.2	7.8
III	–	–	–	–	0.5	5.8	2.5	2.8	–	-1.4	–	–	-6.9	4	84	64	80	76	1.0	4.0	1.6	2.2	5.2	4.7	4.0	4.6
IV	–	–	–	–	5.7	12.8	7.2	8.2	14.0	2.5	26.9	30	-4.9	10	86	55	80	74	1.5	8.1	2.2	3.9	4.9	5.7	4.3	5.0
V	–	–	–	–	9.7	14.2	9.6	10.8	15.2	5.4	25.7	19	-1.1	6	82	59	80	74	2.4	7.7	2.6	4.2	4.7	7.3	4.5	5.5
VI	–	–	–	–	16.1	21.6	16.0	17.4	23.4	10.6	29.8	11	5.9	27	79	60	82	74	4.0	11.2	3.5	6.2	5.2	6.5	3.9	4.9
VII	–	–	–	–	17.7	22.7	17.6	18.9	24.0	13.6	32.3	8	8.6	29	86	65	87	79	3.1	10.7	2.7	5.5	6.9	6.7	6.1	6.6
VIII	–	–	–	–	14.1	19.8	15.8	16.4	21.6	11.2	29.1	12	6.9	24	90	68	85	81	1.7	8.2	2.7	4.2	5.2	5.9	4.2	5.1
IX	–	–	–	–	10.0	15.3	11.4	12.0	16.0	8.0	27.9	9	0.3	27	90	71	87	83	1.4	5.8	1.9	3.0	6.5	7.8	5.6	6.6
X	–	–	–	–	7.0	12.2	8.5	9.0	13.0	5.0	20.4	19	0.6	2,3	91	76	90	86	1.0	3.7	1.1	1.9	6.3	7.4	6.0	6.6
XI	–	–	–	–	3.6	6.4	4.4	4.7	7.4	2.0	16.4	4	-7.9	30	90	79	87	85	0.7	2.1	1.0	1.3	8.3	7.4	7.2	7.6
XII	–	–	–	–	-2.1	-0.2	-1.4	-1.3	0.7	-4.1	6.4	13	-21.0	16	90	87	91	89	0.5	0.8	0.5	0.6	7.5	8.5	7.3	7.8
Rok	–	–	–	–	6.8	11.3	7.8	8.4	–	4.2	32.3	8.VII	-21.0	16.XII	–	–	–	–	–	–	–	–	6.5	6.9	5.5	6.3

Sinołęka

$\varphi = 52°13'$ $\lambda = 21°54'$

I	–	–	–	–	-2.7	-0.9	-1.8	-1.8	0.4	-4.2	7.2	6	-16.0	17	–	–	–	–	–	–	–	–	8.5	8.3	6.9	7.9
II	–	–	–	–	0.7	3.2	1.8	1.9	4.6	-0.4	8.7	14,21	-6.7	28	94	88	92	91	0.4	1.1	0.6	0.7	9.0	7.5	5.5	7.3
III	–	–	–	–	-1.1	4.5	1.6	1.6	6.3	-2.8	16.3	31	-10.5	4	83	68	79	77	1.0	3.2	1.6	1.9	5.1	4.7	3.7	4.5
IV	–	–	–	–	5.0	12.5	7.6	8.2	14.3	2.9	27.0	30	-6.5	10	85	54	78	72	1.4	8.2	2.5	4.0	5.8	5.0	4.8	5.2
V	–	–	–	–	9.0	13.5	10.1	10.7	15.5	5.7	25.5	19	-1.5	6	82	61	78	74	2.3	7.0	2.9	4.1	5.2	7.3	5.6	6.0
VI	–	–	–	–	15.4	21.7	16.6	17.6	23.5	11.2	30.5	19	6.5	7	79	54	77	70	3.7	12.6	4.6	7.0	4.0	5.3	4.6	4.6
VII	–	–	–	–	16.7	21.7	17.8	18.5	23.7	13.9	31.8	5	9.5	29	89	70	87	82	2.3	8.9	3.1	4.8	5.6	6.4	5.9	6.0
VIII	–	–	–	–	14.0	19.4	15.5	16.1	20.9	11.6	30.0	12	6.0	24	95	70	94	85	0.9	7.6	1.5	3.3	5.4	6.6	5.7	5.9
IX	–	–	–	–	9.6	14.3	10.7	11.3	16.0	7.7	27.0	9	1.5	26	90	68	88	82	1.2	5.7	1.6	2.8	7.5	7.2	5.5	6.7
X	–	–	–	–	6.0	11.5	8.2	8.5	12.9	4.5	19.7	19	-0.5	3	91	72	88	84	0.9	4.2	1.4	2.2	6.3	5.8	5.1	5.7
XI	–	–	–	–	2.7	5.4	3.5	3.8	6.8	1.3	16.1	6	-9.0	30	93	81	88	87	0.5	1.8	0.9	1.1	7.9	7.9	7.0	7.6
XII	–	–	–	–	-2.8	-1.0	-2.3	-2.1	0.3	-4.9	6.8	13	-15.5	16	–	–	–	–	–	–	–	–	7.1	7.8	6.6	7.2
Rok	–	–	–	–	6.0	10.5	7.4	7.8	12.1	3.9	31.8	5.VII	-16.0	17.I	–	–	–	–	–	–	–	–	6.4	6.6	5.6	6.2

Pętkowo

$\varphi = 52°12'$ $\lambda = 17°15'$

I	–	–	–	–	-1.5	0.8	-0.7	-0.5	1.5	-3.6	9.5	6	-14.2	16	87	85	88	87	0.7	1.0	0.7	0.8	8.7	8.2	6.7	7.9
II	–	–	–	–	1.4	5.4	2.7	3.0	5.9	0.0	9.6	5	-4.9	27	91	77	90	86	0.6	2.2	0.8	1.2	8.0	6.8	6.5	7.1
III	–	–	–	–	1.3	7.6	4.0	4.2	8.9	-0.4	16.0	13	-5.6	10,11	83	63	82	76	1.2	4.3	1.5	2.3	5.0	4.9	3.6	4.5
IV	–	–	–	–	5.2	12.5	7.5	8.2	13.9	2.0	24.6	28	-6.1	13	86	56	77	73	1.3	7.2	2.6	3.7	5.4	6.4	4.2	5.3
V	–	–	–	–	9.4	15.2	10.3	11.3	16.3	4.7	25.5	19	-4.5	7	75	48	70	64	3.1	10.1	4.2	5.8	4.8	6.2	5.1	5.4
VI	–	–	–	–	15.8	21.8	17.5	18.2	23.5	10.8	31.1	19	6.1	1	76	51	72	66	4.6	14.3	6.0	8.3	5.0	5.1	4.7	4.9
VII	–	–	–	–	17.4	22.3	18.0	18.9	23.9	14.3	33.4	5	9.5	3	85	64	84	78	3.3	11.5	3.9	6.2	6.6	7.1	6.8	6.8
VIII	–	–	–	–	14.3	19.5	15.5	16.2	21.1	11.5	27.3	11	6.5	23	89	65	84	79	1.8	8.4	2.9	4.4	5.6	6.8	5.2	5.9
IX	–	–	–	–	9.7	15.0	11.0	11.7	16.5	7.5	28.1	8	-0.5	27	92	70	88	83	1.0	6.1	1.6	2.9	6.4	7.8	5.3	6.5
X	–	–	–	–	6.2	12.5	8.0	8.7	13.3	4.4	20.9	19	-1.9	2	95	75	92	87	0.5	4.0	0.9	1.8	6.9	6.2	3.5	5.6
XI	–	–	–	–	3.0	6.4	4.1	4.4	7.2	1.6	17.6	5	-7.8	30	94	80	89	87	0.7	2.2	0.9	1.3	8.0	7.8	7.6	7.8
XII	–	–	–	–	-2.0	0.0	-1.0	-1.0	1.2	-3.8	8.8	8	-15.1	17	94	87	89	89	0.4	0.7	0.6	0.6	7.7	8.0	6.6	7.4
Rok	–	–	–	–	6.7	11.6	8.1	8.6	12.8	4.1	33.4	5.VII	-15.1	17.XII	87	68	84	80	1.6	6.0	2.2	3.3	6.5	6.8	5.5	6.3

Koło

$\varphi = 52°12'$ $\lambda = 18°38'$

I	1008.0	1019.9	989.6	1020.9	-1.4	0.7	-0.9	-0.6	1.6	-3.0	9.4	6	-15.3	17	89	83	88	87	0.6	1.1	0.7	0.8	8.5	7.5	6.5	7.5
II	998.1	1021.2	972.0	1010.8	1.7	5.0	2.9	3.4	6.4	0.9	9.9	14	-3.3	24	92	79	88	86	0.5	1.9	0.9	1.1	8.0	7.8	6.0	7.3
III	1005.6	1022.9	983.9	1018.4	4.0	6.7	3.5	3.7	8.4	-0.4	14.8	31	-5.6	11	84	64	78	75	1.1	3.9	1.8	2.3	5.6	6.4	4.2	5.4
IV	1005.7	1019.4	982.0	1018.2	4.9	11.6	7.2	7.7	13.5	2.7	25.8	30	-5.1	13	87	58	80	75	1.2	6.9	2.3	3.5	6.4	6.9	5.7	6.3
V	–	–	–	–	9.1	14.6	10.1	11.0	16.4	5.3	26.2	19	0.1	28	78	52	77	69	2.6	8.9	3.0	4.8	5.8	6.1	4.7	5.5
VI	–	–	–	–	15.9	21.9	17.1	18.0	24.0	11.0	31.2	11	5.9	1	79	51	75	68	4.1	14.0	5.1	7.7	4.9	6.1	4.0	5.0
VII	–	–	–	–	17.5	22.4	18.0	19.0	24.1	14.3	34.3	8	10.1	3	85	65	84	78	3.4	11.4	3.6	6.1	6.9	7.1	6.3	6.8
VIII	–	–	–	–	14.4	20.0	15.6	16.4	21.9	12.2	27.3	11	7.6	31	89	64	86	80	2.0	8.8	2.6	4.5	6.5	7.6	4.7	6.3
IX	–	–	–	–	9.2	14.9	11.3	11.7	16.5	7.7	27.8	9	-0.9	27	94	73	88	85	0.8	5.5	1.7	2.7	6.9	8.0	5.0	6.6
X	–	–	–	–	5.8	12.4	8.1	8.6	13.5	4.7	21.0	19	-1.3	2	96	76	92	88	0.4	3.9	0.9	1.7	6.9	7.1	3.6	5.9
XI	–	–	–	–	3.6	6.6	4.2	4.6	7.6	2.3	16.6	6	-7.5	30	91	82	91	88	0.7	2.0	0.7	1.1	7.9	7.6	7.4	7.6
XII	–	–	–	–	-2.1	-0.4	-1.2	-1.2	1.2	-4.1	8.4	9	-17.8	17	92	88	91	90	0.4	0.7	0.6	0.6	7.0	8.5	6.3	7.5
Rok	–	–	–	–	6.6	11.4	8.0	8.5	12.9	4.6	34.3	8.VII	-17.8	17.XII	88	70	85	81	1.5	5.8	2.0	3.1	6.8	7.2	5.4	6.5

Radzików

$H_s = 90\ m$ $h_w = 11\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D, v m/D																	OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość																			
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10	Max>25°	Opad R 0.1 ≤ R < 1.0	1.0 ≤ R < 10	R ≥ 10	Wiatr v ≥ 10	v ≥ 15	≡	≈	≤ 0.5	◔	◕	●	⊞
I	2	3.0	2.5	4.0	5	4.8	10.5	3.2	2	2.5	15.5	4.2	46.5	5.9	4	8.2	5	4.9	26.8	13.4	5	24	–	3	·	7	5	1	4	1	12	·	4	18	19	·
II	0.5	9.0	2.5	2.2	11.5	3.5	8	4.5	13	4.2	21.5	4.1	18.5	6.8	1.5	8.3	7	4.3	36.3	9.9	18	10	–	·	·	15	9	·	4	·	6	·	1	13	3	·
III	5	4.0	9	4.6	19	4.8	13	7.1	7.5	4.4	5.5	3.7	25	6.9	4	5.0	5	5.3	24.3	10.5	15	19	–	·	·	6	4	1	8	6	1	·	9	5	3	·
IV	12	3.7	10	3.5	9	2.9	7	2.1	8	4.1	4	4.0	16.5	5.3	16.5	4.2	7	3.3	10.5	4.2	30	7	·	·	2	7	4	·	2	1	5	2	9	5	·	·
V	17	3.4	8.5	3.6	8	4.6	8	2.8	3	2.3	5	5.2	10.5	5.0	7.9	4.0	14	3.3	56.6	23.7	9	3	·	·	1	6	5	3	2	·	1	1	4	8	·	·
VI	11	3.1	6.5	2.5	12	3.0	4	4.2	2.5	6.0	10	4.9	21.5	4.6	16.5	3.8	6	3.7	55.9	18.3	9	·	·	·	10	8	6	2	6	3	1	3	9	7	·	·
VII	6	2.9	8	2.1	3.5	4.4	7	2.4	10	2.8	13	3.1	23.5	4.5	12	3.9	10	3.1	168.6	37.8	2	·	·	·	12	16	14	6	3	1	1	6	6	12	·	·
VIII	4	2.2	4.5	2.3	1.5	2.3	5.5	2.9	12	3.5	10	4.9	36.5	4.4	18	3.5	4	3.7	40.1	9.8	14	·	·	·	6	10	7	·	1	·	2	·	7	6	·	·
IX	2.5	3.2	·	·	·	·	1.5	3.7	13	4.3	23	5.8	26	8.6	10	6.5	14	5.4	85.3	26.3	23	·	·	·	2	19	14	1	11	8	5	1	2	12	·	·
X	1	1.0	·	·	·	·	5.5	2.3	7	3.9	31	4.6	26.5	6.7	6	4.8	17	4.1	8.0	4.4	1	·	·	·	·	7	2	·	2	1	5	·	3	11	·	·
XI	8	11.1	8	5.6	9	3.1	18.5	4.5	11.5	4.7	7	4.3	16.5	10.3	2.5	9.6	9	5.8	39.4	12.8	25	11	1	·	·	7	6	1	10	3	6	·	3	20	·	·
XII	10.5	4.3	3	3.3	4	4.2	6.5	3.8	8	3.7	28	5.3	22.5	7.8	25	6.0	8	5.0	44.2	18.2	14	24	10	3	·	9	8	1	7	3	4	·	1	16	11	·
Rok	79.5	4.2	59.5	2.8	82.5	3.1	95	3.6	97.5	3.9	173.5	4.5	289	6.2	142.5	5.5	106	4.3	596.0	37.8	2.VII	98	–	6	33	117	84	16	60	27	49	13	58	133	36	·

Sinołęka

$H_s = 153\ m$ $h_w = 11\ m$

I	1.5	3.7	3	7.0	6	5.2	5.5	4.9	7	3.6	20	4.1	32.5	5.3	10.5	6.9	7	4.7	24.4	9.1	6	24	11	5	·	10	7	·	3	·	–	–	2	19	–	·
II	4.5	4.3	4.5	3.1	1.5	2.0	6.5	4.2	21.5	4.8	17.5	4.1	17.5	5.3	3.5	7.0	7	4.2	43.1	5.9	1	12	3	·	·	19	14	·	3	·	–	–	1	10	–	·
III	8	5.3	8	7.2	11	5.7	11	7.8	10	6.1	6	5.5	17	5.5	10	9.0	12	5.7	23.0	13.5	15	21	6	1	·	4	4	1	7	2	–	–	9	4	–	·
IV	13.5	3.3	8	3.8	10	3.1	6.5	2.9	10	3.9	7.5	4.1	3.5	3.3	14	4.5	17	3.0	11.7	5.8	30	8	·	·	4	7	4	·	·	·	–	–	5	7	–	·
V	17.5	3.2	12.5	3.6	9.5	3.3	6	3.6	3	2.0	5.5	3.0	5.5	4.5	15.5	4.5	18	3.0	33.1	12.4	10	1	·	·	4	5	3	1	·	·	–	–	4	11	–	·
VI	10.5	2.5	11.5	3.5	1	2.0	7.5	3.9	9	3.7	5.5	3.6	1.5	3.8	16	4.8	14	3.2	45.4	16.9	24	·	·	·	9	9	8	1	·	·	–	–	6	3	–	·
VII	6.5	3.3	7.5	3.5	6	2.7	6	2.9	8.5	4.5	9.5	2.7	15.5	4.4	12.5	4.5	21	2.9	99.7	21.2	16	·	·	·	12	13	11	5	·	·	–	–	5	9	–	·
VIII	3	3.3	2	1.5	2	2.0	3.5	2.7	8.5	3.3	12	3.7	25.5	4.0	16.5	3.6	20	2.8	144.3	59.0	14	·	·	·	3	13	12	3	1	·	–	–	1	7	–	·
IX	3.5	2.6	2.5	2.8	·	·	2	3.0	13	3.4	14	4.6	21	5.9	11	5.5	23	3.5	84.6	24.6	23	·	·	·	1	15	13	1	4	·	–	–	1	12	–	·
X	4.5	3.0	·	·	0.5	2.0	4	3.0	7.5	3.7	27.5	3.6	20.5	4.3	9.5	4.3	22	2.9	14.5	3.2	22	1	·	·	·	7	6	·	·	·	–	–	3	7	–	·
XI	7	5.4	6.5	4.5	12	3.7	15.5	5.0	8.5	3.5	7	2.6	16.5	6.3	3	7.0	14	4.0	20.8	10.5	28	11	1	·	·	7	5	1	4	·	–	–	3	18	–	·
XII	6.5	3.1	4	4.0	3	2.5	9	2.2	13	3.0	22.5	4.6	16	5.0	9	3.8	10	3.4	26.1	9.0	14	27	13	3	·	12	6	·	·	·	–	–	1	16	–	·
Rok	83.5	3.6	70	3.7	62.5	2.8	83	3.8	119.5	3.8	154.5	3.8	206	4.8	131	5.4	185	3.6	570.7	59.0	14.VIII	105	34	9	30	121	98	13	22	2	–	–	41	123	–	·

Pętkowo

$H_s = 86\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25.0	7.0	5	24	8	3	·	11	8	·	–	–	10	·	2	18	16	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.6	17.0	18	16	·	·	·	13	9	1	–	–	7	·	·	8	·	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	22.5	9.8	17	17	·	·	·	6	5	·	–	–	5	·	12	8	·	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.1	2.2	24	10	·	·	·	7	5	·	–	–	–	1	6	9	·	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28.5	20.0	6	2	·	·	1	6	5	1	–	–	–	2	4	6	2	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	50.7	29.5	4	·	·	·	11	7	6	2	–	–	1	3	6	7	·	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	169.1	38.5	21	·	·	·	13	19	15	4	–	–	5	7	2	15	·	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	42.7	7.6	24	·	·	·	1	11	10	·	–	–	5	6	·	6	·	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	84.1	16.4	23	1	·	·	2	15	15	2	–	–	11	1	·	8	·	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.9	1.7	24	2	·	·	·	10	3	·	–	–	22	·	4	4	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	12.1	4.5	28	9	2	·	·	9	5	·	–	–	15	·	2	16	·	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31.2	8.7	8	24	8	4	·	12	10	·	–	–	18	·	2	14	6	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	529.5	38.5	21.VII	105	18	7	28	126	96	10	–	–	–	20	40	119	24	·

Koło

$H_s = 95\ m$ $H_b = 101.7\ m$ $h_w = 11\ m$

I	0.5	4.0	4	2.9	7.5	2.9	2	2.0	4.5	4.2	18.5	2.6	36	3.7		·	20	2.4	28.4	6.4	13	21	9	2	·	14	7	·	1	1	5	·	3	20	19	·
II	2	4.2	1	4.0	1.5	2.7	3.5	2.3	1.5	1.8	22	2.1	16.5	3.3	6.5	2.2	16	1.9	50.6	12.8	18	9	1	·	·	19	9	2	1	·	5	·	·	12	2	·
III	3	1.5	2.5	2.4	1.7	4.2	6.5	2.5	11.5	2.4	8	2.8	19.5	4.1	5	2.7	20	2.6	37.0	12.2	28	18	·	·	·	10	7	2	4	1	1	·	8	9	1	·
IV	7	4.4	2	1.5	7	2.7	2.5	1.2	1.5	2.0	9	2.0	16	1.7	23	2.0	22	1.7	33.5	13.1	22	7	·	·	1	8	6	2	1	·	2	3	4	12	·	·
V	1.3	3.8	1	3.0	6.5	1.6	4	2.9	2.5	1.6	5.5	1.8	25	2.3	16.5	2.4	19	1.9	18.6	6.9	20	·	·	·	1	10	5	·	·	·	·	2	4	6	·	·
VI	4	1.9	3	2.3	8.5	2.1	3	2.8	8	1.9	10.5	2.7	24.5	3.1	5.5	1.8	23	1.9	54.9	18.0	4	·	·	·	13	9	6	2	·	·	1	6	7	4	·	·
VII	3.5	1.0	3.5	1.3	10	1.7	0.5	2.0	4.5	1.6	8	3.6	26.5	3.0	9.5	2.6	27	1.8	174.8	43.8	16	·	·	·	14	14	12	5	·	·	·	7	2	15	·	·
VIII	·	·	·	·	2	1.5	2	2.0	6.5	2.1	15	3.8	35	3.4	4.5	3.2	28	2.3	87.2	23.4	10	·	·	·	4	12	9	3	·	·	1	5	1	8	·	·
IX	·	·	·	·	·	·	0.5	1.0	6.5	1.8	17	3.4	35.5	4.2	0.5	1.0	30	2.4	78.3	11.2	23	2	·	·	2	19	15	1	3	·	·	2	1	8	·	·
X	·	·	·	·	·	·	0.5	2.0	1.1	1.5	19.5	2.1	25.5	2.9	0.5	1.0	36	1.4	8.3	3.4	20	2	·	·	·	6	3	·	·	·	8	·	2	9	·	·
XI	3.5	4.9	4.5	3.3	1.3	2.5	9.5	1.4	3	1.2	8	2.0	16	5.2	4.5	5.2	26	2.4	10.1	3.2	27	10	3	·	·	5	4	·	1	·	1	·	1	18	·	·
XII	1	2.0	3	3.0	4	1.0	5	1.8	2.5	1.0	19	3.4	24.5	4.4	4	1.9	30	2.2	53.0	34.1	14	23	8	3	·	13	7	1	2	1	7	·	1	15	17	·
Rok	37.5	4.8	24.5	4.7	77	4.9	39.5	2.0	77	4.7	60	2.7	302.5	3.4	80	2.2	297	2.1	631.5	43.8	16.VII	92	21	5	35	139	90	18	13	3	31	24	34	136	39	·

Niepokalanów

$\varphi = 52°12'$ $\lambda = 20°25'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	Średnia I	II	III	Dies	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.1	0.3	-1.3	-1.1	1.4	-3.6	8.0	6	-16.0	17	88	84	88	87	0.6	1.0	0.6	0.7	7.6	7.5	6.5	7.2
II	–	–	–	–	1.7	4.9	2.7	3.0	6.1	0.5	10.8	14	-2.7	28	91	77	86	85	0.6	2.1	1.1	1.3	8.0	7.3	6.4	7.2
III	–	–	–	–	0.3	5.9	2.7	2.9	7.9	-0.8	16.3	31	-6.2	4	81	62	82	75	1.3	4.3	1.5	2.4	5.5	5.2	3.9	4.9
IV	–	–	–	–	5.2	12.8	7.7	8.4	14.4	2.8	26.8	30	-4.7	10	84	51	76	70	1.6	8.7	2.8	4.4	5.2	5.6	5.3	5.4
V	–	–	–	–	9.3	14.2	9.8	10.8	15.8	5.6	26.3	19	-0.5	6	79	57	80	72	2.6	7.9	2.6	4.4	5.3	6.9	4.9	5.7
VI	–	–	–	–	15.8	21.1	16.7	17.6	23.4	10.8	30.5	11	6.6	27	77	56	78	70	4.2	11.9	4.3	6.8	3.7	4.8	3.3	3.9
VII	–	–	–	–	17.3	22.4	17.8	18.8	24.2	13.5	33.0	8	9.0	29	85	66	85	79	3.0	10.8	3.3	5.7	5.6	6.1	5.4	5.7
VIII	–	–	–	–	14.3	20.0	15.1	16.1	21.9	11.0	28.4	12	5.1	24	91	65	88	81	1.5	8.9	2.2	4.2	4.9	6.7	3.8	5.1
IX	–	–	–	–	9.5	15.3	11.1	11.8	17.0	7.7	28.6	9	0.0	26	91	68	88	82	1.1	6.3	1.7	3.0	5.8	7.1	4.9	5.9
X	–	–	–	–	6.1	12.6	8.0	8.7	13.9	4.6	21.1	19	0.3	2	91	70	89	83	0.9	4.7	1.3	2.3	6.3	6.1	4.8	5.7
XI	–	–	–	–	3.5	6.4	3.9	4.4	7.8	2.0	17.2	4	-7.4	29,30	92	80	92	88	0.6	2.2	0.7	1.2	7.4	7.0	7.3	7.2
XII	–	–	–	–	-2.4	-0.1	-1.7	-1.5	1.2	-4.4	7.2	9	-22.2	16	90	86	92	89	0.5	0.9	0.4	0.6	6.7	7.7	6.8	7.1
Rok	–	–	–	–	6.5	11.3	7.7	8.3	12.9	4.1	33.0	8.VII	-22.2	16.XII	87	68	85	80	1.5	5.8	1.9	3.1	6.0	6.5	5.3	5.9

Łosice

$\varphi = 52°12'$ $\lambda = 22°43'$

I	–	–	–	–	-2.8	-0.9	-2.0	-1.9	0.1	-4.7	6.2	6	-17.1	17	90	87	90	89	0.4	0.7	0.4	0.5	8.8	8.6	7.5	8.3
II	–	–	–	–	0.4	3.0	1.0	1.4	3.9	-1.2	9.2	14	-6.5	27	95	86	92	94	0.4	1.2	0.5	0.7	9.5	8.6	7.0	8.4
III	–	–	–	–	-2.0	4.0	0.6	0.8	5.6	-4.0	16.4	30	-13.3	4	83	64	84	77	0.9	3.6	1.2	1.9	4.4	5.2	4.0	4.5
IV	–	–	–	–	5.1	12.6	7.3	8.1	14.0	2.2	26.4	30	-6.3	10	86	52	76	71	1.5	8.6	2.8	4.3	5.1	5.9	4.2	5.1
V	–	–	–	–	9.6	14.0	9.7	10.8	15.9	5.6	25.4	19	-1.3	2	80	60	80	73	2.5	7.3	2.4	4.1	5.7	7.8	5.1	6.2
VI	–	–	–	–	15.8	22.4	15.9	17.5	24.2	10.7	31.5	12	5.2	7	77	54	77	69	4.3	13.3	4.4	7.3	5.4	6.2	4.5	5.4
VII	–	–	–	–	17.3	22.8	17.5	18.8	24.3	13.3	30.4	13	9.5	4,7,29	85	64	83	77	3.3	10.8	3.8	6.0	6.7	7.2	5.4	6.4
VIII	–	–	–	–	14.6	20.2	15.1	16.2	21.5	11.1	29.8	12	6.4	24	90	67	85	81	1.7	8.5	2.6	4.3	5.9	7.4	4.0	5.8
IX	–	–	–	–	10.0	15.1	10.9	11.7	16.4	7.6	26.8	9	0.1	27	91	71	88	83	1.2	5.6	1.6	2.8	7.5	7.8	6.3	6.9
X	–	–	–	–	6.0	11.2	7.5	8.2	12.5	4.0	18.9	19	-0.6	3	93	74	91	86	0.7	3.8	1.0	1.8	6.8	6.8	5.0	6.2
XI	–	–	–	–	2.8	5.2	3.4	3.7	6.2	0.8	15.1	6	-9.7	30	92	84	88	88	0.6	1.5	0.8	1.0	8.5	8.3	7.8	8.4
XII	–	–	–	–	-2.9	-1.0	-2.4	-2.2	-0.1	-5.6	6.4	13,14	-16.5	16	89	87	90	89	0.5	0.7	0.5	0.6	7.5	7.7	7.0	7.4
Rok	–	–	–	–	6.2	10.8	7.0	7.8	12.0	3.3	31.5	12.VI	-17.1	17.I	88	71	85	81	1.5	5.5	1.8	2.9	6.8	7.3	5.6	6.6

Siedlce

$\varphi = 52°11'$ $\lambda = 22°16'$

I	1002.1	1013.4	986.3	1021.1	-2.6	-0.8	-1.7	-1.7	0.4	-4.0	6.9	6	-15.2	17	89	86	89	88	0.5	0.8	0.6	0.6	8.7	8.9	7.4	8.3
II	999.4	1013.3	979.4	1012.0	0.6	3.1	1.3	1.6	4.5	-0.7	9.7	14	-6.6	24	92	85	90	89	0.5	1.2	0.7	0.8	8.8	8.9	6.0	7.9
III	1000.8	1016.4	975.3	1019.5	-1.6	4.4	0.9	1.2	6.2	3.1	17.2	31	-14.3	4	84	62	80	75	0.9	3.8	1.4	2.0	5.4	5.8	4.3	5.2
IV	999.9	1012.2	975.3	1018.1	5.2	12.9	7.3	8.2	14.4	2.3	26.6	30	-6.9	10	86	51	75	71	1.5	9.3	2.7	4.5	6.2	6.4	5.3	6.0
V	997.7	1008.5	985.2	1015.8	9.5	14.0	9.8	10.8	15.6	5.4	26.1	19	-0.8	6	82	62	82	75	2.3	7.0	2.2	3.8	5.8	7.7	5.9	6.5
VI	998.6	1012.0	986.6	1016.3	15.7	22.1	16.1	17.5	23.5	10.7	30.4	19	5.1	21	80	52	78	70	3.8	13.3	4.3	7.1	5.2	6.4	4.6	5.4
VII	994.2	1004.3	984.7	1011.7	16.9	22.4	17.4	18.5	23.7	13.6	31.0	5	8.3	7	85	65	86	78	2.9	10.4	3.2	5.5	6.8	7.3	6.1	6.7
VIII	996.2	1004.9	984.0	1013.9	14.2	19.8	15.1	16.0	21.3	11.1	30.1	12	5.5	24	92	67	88	82	1.3	8.3	2.1	3.9	5.9	7.5	5.0	6.1
IX	994.4	1005.2	978.2	1012.3	9.8	14.7	10.9	11.6	16.1	7.8	27.2	9	1.3	26	93	71	88	84	0.9	5.4	1.6	2.6	7.5	8.1	6.1	7.2
X	1001.7	1014.6	983.4	1019.9	6.0	11.8	7.8	8.4	12.6	4.6	19.0	19	-0.5	3	92	73	90	85	0.8	4.1	1.1	2.0	6.4	7.4	5.7	6.5
XI	1003.0	1023.8	981.4	1021.7	2.9	5.6	3.4	3.8	6.8	1.3	16.2	6	-9.4	30	94	82	90	89	0.4	1.8	0.7	1.0	8.3	8.8	7.7	8.3
XII	999.7	1014.5	985.6	1015.6	-2.9	-0.9	-2.4	-2.2	0.2	-5.4	6.6	13	-17.3	16	93	87	91	90	0.4	0.7	0.5	0.5	7.5	8.5	7.0	7.7
Rok	998.8	1023.8	975.6	1016.4	6.1	10.8	7.2	7.8	12.1	4.2	31.0	5.VII	-17.3	16.XII	88	70	86	81	1.4	5.5	1.8	2.9	6.9	7.6	5.9	6.8

Reguły

$\varphi = 52°10'$ $\lambda = 20°51'$

I	–	–	–	–	-2.3	0.2	-1.3	-1.2	1.1	-3.7	6.9	6	-15.5	17	–	–	–	–	–	–	–	–	7.8	7.9	6.6	7.4
II	–	–	–	–	1.6	4.4	2.2	2.6	5.5	0.2	9.9	21	-4.2	24	–	–	–	–	–	–	–	–	8.4	8.2	7.4	8.0
III	–	–	–	–	-0.1	5.6	2.3	2.5	7.4	-1.5	15.6	30	-8.0	4	–	–	–	–	–	–	–	–	5.7	5.3	4.4	5.1
IV	–	–	–	–	5.2	13.1	7.6	8.4	14.5	3.0	29.9	28	-5.5	10	–	–	–	–	–	–	–	–	5.5	5.7	5.2	5.5
V	–	–	–	–	9.0	14.1	9.7	10.6	15.4	5.7	26.5	19	-1.2	6	–	–	–	–	–	–	–	–	5.4	7.5	5.6	6.2
VI	–	–	–	–	16.2	21.7	16.5	17.7	23.5	11.2	30.1	11	7.0	15,18	–	–	–	–	–	–	–	–	4.4	5.6	4.3	4.7
VII	–	–	–	–	17.4	22.5	17.8	18.9	23.8	13.9	33.4	8	8.5	29	–	–	–	–	–	–	–	–	6.5	6.9	6.5	6.6
VIII	–	–	–	–	14.1	19.6	15.1	16.0	21.4	11.6	29.5	12	6.4	24	–	–	–	–	–	–	–	–	5.2	7.3	4.6	5.7
IX	–	–	–	–	9.8	15.0	11.1	11.8	16.5	7.9	27.9	9	0.0	27	–	–	–	–	–	–	–	–	6.2	7.6	5.9	6.6
X	–	–	–	–	6.1	12.4	7.8	8.5	13.3	4.7	20.5	19	1.0	3	–	–	–	–	–	–	–	–	6.3	6.9	5.8	6.3
XI	–	–	–	–	3.3	6.2	3.7	4.2	7.3	1.8	16.3	4	-8.0	30	–	–	–	–	–	–	–	–	8.4	7.6	7.5	7.8
XII	–	–	–	–	-2.4	-0.4	-1.7	-1.6	1.0	-4.3	6.9	9	-22.2	16	–	–	–	–	–	–	–	–	7.2	8.5	6.7	7.5
Rok	–	–	–	–	6.5	11.2	7.6	8.2	12.6	4.2	33.4	8.VII	-22.2	16.XII	–	–	–	–	–	–	–	–	6.4	7.1	5.9	6.5

Niepokalanów

$H_s = 91\ m$

1957

MIESIĄC	ROZKŁAD WIATRU [%] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max<0	Min<-10	Max>25	Opad R R≥0.1	R≥1.0	R≥10.0	Wiatr v ≥10	≥15	≡	≈	◔	◕	▣
I	1	8.0	2	2.0	11.5	4.9	4.5	4.1	12.5	2.2	16	3.3	24	5.5	20.5	6.2	1	4.6	28.9	6.0	13.31	23	9	4	·	15	8	·	2	·	3	·	4	15	19
II	7	3.2	6.5	4.2	1.5	4.3	8.5	4.5	17	3.6	17	3.4	22.5	4.8	4	6.9	·	4.1	49.1	12.4	18	11	·	·	·	21	11	1	1	·	1	·	1	10	1
III	9	6.1	9.5	5.4	1.9	5.2	12.5	7.4	9	3.7	7.5	4.1	14.5	5.4	12	6.0	·	5.5	30.3	10.8	15	19	2	·	·	9	5	1	6	·	·	·	8	6	1
IV	21.5	4.4	11	3.7	11.5	4.1	6	4.2	11	3.6	4	3.0	8.5	4.4	12.5	3.9	4	3.9	15.2	6.4	30	8	·	·	4	10	3	·	2	·	3	2	7	5	·
V	2.0	3.9	17.5	4.7	3	3.8	14.5	4.7	6	3.2	2.5	3.4	14.5	4.9	14	4.4	4	4.1	45.9	16.8	9	1	·	·	1	8	4	3	·	·	·	1	4	9	·
VI	2.0	3.9	1.5	2.9	4	3.6	6	3.7	2	3.5	4.5	4.0	24.5	4.9	14	4.9	·	4.1	70.0	22.9	9	·	·	·	9	10	7	2	·	·	·	6	9	2	·
VII	1.1	3.6	1.4	3.4	4.5	3.8	7	3.9	6.5	3.4	9	3.7	25.5	4.7	14.5	4.2	1	4.0	63.8	14.4	16	·	·	·	12	18	11	2	·	·	1	9	6	10	·
VIII	8	3.8	·	·	2	2.0	2	5.2	8.5	4.3	9.5	4.9	41.5	4.7	16.5	4.3	5	4.2	49.0	13.0	10	·	·	·	6	16	10	1	·	·	1	1	4	4	·
IX	4.5	3.1	1	3.5	·	·	1	3.0	9.5	4.3	12	5.3	40.5	6.3	13.5	6.2	8	5.1	80.1	21.5	23	·	·	·	2	19	14	2	6	·	1	1	2	8	·
X	6	3.8	2	2.2	1	3.0	1	1.0	10.5	3.3	21.5	4.3	40	5.0	4	3.5	7	4.0	8.1	3.7	20	·	·	·	·	8	2	·	·	·	5	·	4	9	·
XI	1.1	6.8	3.5	3.3	15.5	4.4	2.6	3.8	9.5	3.5	3	4.7	19	6.9	2.5	10.0	·	5.1	19.3	6.1	28	11	1	·	·	9	7	·	3	·	3	·	5	16	·
XII	6	2.9	14.5	3.1	7	4.6	3	3.2	7.5	3.2	19	5.2	29.5	6.3	5.5	4.9	1	4.7	48.7	28.1	14	24	9	3	·	14	7	1	3	·	3	·	2	15	8
Rok	12.5	4.5	96.5	3.2	80.5	3.6	89	4.1	109.5	3.5	125.5	4.1	304.5	5.3	133.5	5.4	31	4.4	508.4	28.1	14.XII	97	21	7	34	157	89	13	23	·	21	20	56	109	29

Łosice

$H_s = 153\ m$ $h_w = 12.5\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	22.8	8.6	5	27	14	6	·	12	4	·	–	–	–	·	1	22	25
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.9	6.4	8	17	3	·	·	21	14	·	–	–	–	·	·	18	6
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18.9	11.0	15	26	8	3	·	5	5	1	–	–	–	·	6	8	11
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.6	3.4	17	9	·	·	4	7	1	·	–	–	–	1	6	10	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44.4	15.4	10	3	·	·	1	10	7	1	–	–	–	2	4	10	1
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43.2	33.1	24	·	·	·	11	5	5	1	–	–	–	4	4	10	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	77.6	9.6	31	·	·	·	11	20	15	·	–	–	–	11	3	10	·
VIII	2.5	2.4	·	·	6.5	2.5	11	4.2	13	2.4	21.5	3.8	15	2.2	13.5	2.9	10	2.7	112.8	42.7	29	·	·	·	4	14	12	2	·	·	–	6	3	7	·
IX	2	4.0	·	·	1.5	3.7	12.5	3.5	14.5	3.9	25	5.0	21.5	3.9	10	2.2	3	3.8	83.1	15.4	23	·	·	·	1	17	14	3	3	·	–	2	2	13	·
X	1	3.0	1	1.0	2.5	3.0	11	3.4	3.8	3.3	24.5	3.5	9.5	3.3	3.5	2.9	2	3.2	15.6	7.6	23	1	·	·	·	7	4	·	·	·	–	·	3	9	·
XI	9	7.4	8.5	4.6	12	4.3	23.5	4.5	10	3.5	8	3.1	12	5.2	4	4.5	3	4.5	31.3	11.1	28	13	1	·	·	10	9	1	3	·	–	·	1	22	1
XII	6	4.3	3.5	2.1	11.5	3.2	10.5	3.2	18	4.7	29	5.7	3	5.8	6.5	3.6	5	4.2	23.4	6.8	8	29	14	4	·	12	8	·	2	2	–	·	2	18	21
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	523.6	42.7	29.VIII	125	40	13	32	140	93	9	–	–	–	26	37	155	63

Siedlce

$H_s = 147\ m$ $H_b = 148.8\ m$ $h_w = 11\ m$

I	2	2.5	5	4.3	3	4.5	13.5	2.9	13.5	2.9	2.6	4.8	24.5	6.0	5.5	5.2	1	4.5	19.4	5.0	5	24	12	5	·	14	4	·	1	·	4	·	·	21	21
II	6.5	2.8	2.5	2.2	3.5	2.6	13	4.2	19.5	3.9	2.3	4.1	9.5	4.6	3.5	3.0	3	3.7	50.8	13.4	22	13	2	·	·	23	16	1	1	·	4	·	·	12	7
III	7.5	4.1	14.5	3.0	12.5	3.4	15	5.6	8	4.7	8.5	4.6	9	5.4	12	6.0	6	4.3	26.2	13.0	15	23	6	1	·	6	4	1	5	1	1	·	6	5	3
IV	1.3	2.0	11.5	2.5	12	1.8	1.3	2.2	9.5	3.6	4.5	2.4	10	3.1	11.5	3.4	5	2.4	12.7	3.6	30	10	·	·	4	6	6	·	·	·	·	1	4	7	·
V	1.4	3.1	15.5	3.0	13.5	2.1	8	2.6	5	3.7	4	4.9	10.5	3.6	16.5	3.2	6	2.9	34.2	14.8	10	3	·	·	1	6	5	1	·	·	1	2	2	13	·
VI	1.6	2.3	6	2.0	1	2.0	1.4	2.5	6	3.2	1.1	3.8	23.5	3.8	6.5	3.3	6	2.9	72.9	48.3	24	·	·	·	9	9	5	2	·	·	·	5	5	6	·
VII	3	2.5	8	2.0	9	2.2	17.5	2.6	4.5	2.6	17.5	3.7	1.8	3.0	8.5	3.1	7	2.7	70.1	13.2	16	·	·	·	12	16	12	2	·	·	1	10	3	14	·
VIII	2.5	4.0	1	2.0	4	1.9	8.5	3.1	8.5	3.4	23.5	3.4	18.5	3.7	17.5	2.9	9	2.9	99.0	28.2	14	·	·	·	4	14	13	2	·	·	·	4	·	7	·
IX	3.5	2.1	·	·	4.5	1.6	1.3	2.0	13.5	3.3	2.4	5.4	24.5	5.6	7	2.0	3	4.0	61.6	18.5	23	·	·	·	1	15	11	1	–	–	1	2	2	11	·
X	2	3.0	·	·	1	1.5	16.5	2.1	28.5	2.9	21.5	4.2	18.5	3.9	4	3.5	1	3.2	15.2	4.6	22	1	·	·	·	7	4	·	1	·	2	·	3	8	·
XI	7.5	5.8	8	3.5	15	2.5	22	3.1	12.5	2.4	9	4.1	14.5	5.2	0.5	10.0	1	3.6	22.1	9.9	28	11	1	·	·	10	7	·	·	·	4	·	1	21	2
XII	1.0	3.4	9	2.2	3.5	3.1	12.5	2.5	14	3.7	28.5	5.4	7	3.9	6.5	4.0	2	3.8	20.7	7.0	14	27	12	4	·	13	7	·	–	–	4	·	2	18	22
Rok	87.5	2.9	81	2.2	79.5	2.4	166.5	3.0	143	3.4	200	4.2	188	4.3	99.5	4.1	50	3.4	504.9	48.3	24.VI	112	33	10	31	139	94	10	–	–	22	24	28	143	55

Reguły

$H_s = 98\ m$ $h_w = 12\ m$

I	7.5	4.6	2	2.8	3	1.8	5	2.9	2.5	1.0	9.5	2.1	29.5	3.3	14	2.8	2.0	2.1	24.6	5.6	3.1	24	8	3	·	9	7	·	·	·	–	·	3	17	17
II	7.5	2.5	2.5	1.6	4.5	3.0	4	2.4	12	3.8	14.5	2.5	22.5	4.2	5.5	3.4	11	2.9	48.6	9.0	18	10	1	·	·	23	12	·	·	·	–	·	1	1.5	3
III	1.1	4.0	6	1.8	1.0	3.8	13.5	4.3	5	3.4	2	4.5	17.5	4.7	7	3.8	2.1	3.1	27.8	12.6	15	20	3	·	·	7	5	1	2	·	–	·	8	6	1
IV	19.5	2.4	5	2.1	2	2.0	6.5	2.2	3.5	4.1	3.5	2.6	1.0	2.8	2.0	2.2	2.0	1.9	7.2	2.8	3.0	7	·	·	4	5	4	·	1	·	–	4	6	6	·
V	21.5	2.4	8.5	2.1	9.5	1.4	8.5	2.0	0.5	3.0	3.5	1.9	7.5	3.5	21.5	2.8	12	2.1	43.1	25.6	9	1	·	·	1	6	5	1	·	·	–	1	2	10	·
VI	1.7	2.4	6.5	2.4	4.5	1.9	5	1.8	3.5	1.9	4.5	2.0	4.7	3.0	2.3	2.8	9	2.3	33.1	10.5	4	·	·	·	9	10	5	1	·	·	–	4	10	6	·
VII	8.5	1.8	5	1.5	3.5	2.4	3	2.0	3.5	1.3	5	1.9	2.3	2.3	23.5	2.3	1.8	1.7	101.6	26.5	2	·	·	·	11	15	10	3	·	·	–	4	5	13	·
VIII	6	1.6	2	3.0	5.5	1.5	5	1.8	2	2.5	4.5	2.4	2.1	2.6	3.0	2.2	1.7	1.8	94.8	20.6	10	·	·	·	5	15	11	4	·	·	–	2	3	6	·
IX	4	2.0	·	·	0.5	1.0	5.5	1.2	2	2.0	1.4	3.0	3.1	3.4	1.4	2.5	1.9	2.2	90.2	25.8	23	·	·	·	2	17	14	1	·	·	–	·	2	9	·
X	1.5	1.7	0.5	1.0	2	1.5	4	1.0	6	1.8	1.5	2.9	30.5	2.6	12.5	2.6	2.1	1.9	8.0	1.8	1	·	·	·	·	9	4	·	·	·	–	·	3	11	·
XI	7.5	5.4	7.5	2.7	9.5	1.8	1.6	3.0	5.5	3.2	3	2.0	1.4.5	3.7	7.5	4.4	1.9	2.6	19.2	7.5	28	11	1	·	·	8	6	·	·	·	–	·	2	17	·
XII	1.1	2.4	2	3.6	3.5	2.9	7.5	1.9	6	1.5	1.4	3.2	3.2	3.2	8	1.8	9	2.4	43.2	18.5	14	25	10	3	·	12	7	1	·	·	–	·	2	16	13
Rok	122.5	2.5	47.5	2.0	58	2.1	83.5	2.2	52	2.5	9.3	2.6	256	3.3	186.5	2.8	196	2.2	538.4	26.5	2.VII	98	23	6	32	136	90	12	3	·	–	15	47	132	34

Rudka

$\varphi = 52°09'$ $\lambda = 21°50'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.9	-4.0	-2.0	-2.0	0.3	-4.6	6.8	6	-17.1	17	–	–	–	–	–	–	–	–	8.9	8.4	7.0	8.1
II	–	–	–	–	0.7	3.1	1.7	1.8	4.6	-0.6	8.5	21	-6.4	28	–	–	–	–	–	–	–	–	9.1	7.9	6.7	7.9
III	–	–	–	–	-1.2	4.7	1.4	1.6	6.5	-3.0	16.1	31	-11.9	4	–	–	–	–	–	–	–	–	5.0	5.3	3.7	4.7
IV	–	–	–	–	5.3	13.0	7.2	8.2	14.4	2.3	26.5	29	-7.5	10	–	–	–	–	–	–	–	–	5.3	5.9	4.4	5.2
V	–	–	–	–	9.3	14.2	9.8	10.8	15.7	5.5	26.4	19	-2.3	6	–	–	–	–	–	–	–	–	5.6	7.0	5.8	6.1
VI	–	–	–	–	16.1	22.7	16.5	18.0	23.8	10.3	30.6	19	5.2	7	–	–	–	–	–	–	–	–	4.7	5.4	4.3	4.8
VII	–	–	–	–	17.1	22.2	17.6	18.6	24.0	13.3	33.3	5	8.4	29,30	–	–	–	–	–	–	–	–	6.5	6.7	6.1	6.4
VIII	–	–	–	–	14.2	20.0	14.9	16.0	24.4	11.1	29.4	12	4.6	24	90	66	89	82	1.7	8.1	2.0	3.9	5.7	6.6	5.6	6.0
IX	–	–	–	–	9.8	14.7	10.4	11.3	16.1	7.5	27.3	9	0.8	26	91	70	89	83	1.2	6.6	1.4	2.7	6.8	7.4	5.5	6.6
X	–	–	–	–	5.6	11.8	7.5	8.1	12.7	4.0	20.0	19	-1.2	3	91	68	90	83	0.8	4.6	1.1	2.2	6.1	6.3	4.9	5.8
XI	–	–	–	–	2.7	5.6	3.2	3.7	6.8	0.9	15.9	6	-9.2	30	92	80	91	88	0.6	1.9	0.7	1.1	8.2	8.1	7.8	8.0
XII	–	–	–	–	-2.8	-1.0	-2.4	-2.2	0.4	-5.3	6.6	13	-17.2	16	92	86	91	90	0.3	0.8	0.5	0.5	7.2	7.8	6.7	7.2
Rok	–	–	–	–	6.2	10.8	7.2	7.8	12.2	3.4	33.3	5.VII	-17.2	16.XII	–	–	–	–	–	–	–	–	6.6	6.9	5.7	6.4

Brwinów

$\varphi = 52°08'$ $\lambda = 20°42'$

I	1007.1	1018.4	990.4	1021.3	-2.0	0.3	-1.1	-1.0	1.0	-3.3	8.2	6	-16.0	16	88	84	88	87	0.6	1.0	0.7	0.8	8.1	8.1	7.0	7.7
II	997.8	1018.8	973.8	1011.7	1.8	4.7	2.7	3.0	5.8	-0.1	9.9	14	-4.1	4	91	77	87	85	0.6	2.1	1.0	1.2	9.1	8.7	6.8	8.2
III	1005.4	1021.0	980.7	1019.4	0.4	5.7	2.6	2.8	7.5	-1.4	16.2	31	-8.6	4	82	59	76	72	1.2	4.4	1.9	2.5	6.1	5.8	4.6	5.5
IV	1004.8	1016.3	984.9	1018.5	5.2	12.8	7.8	8.4	14.3	3.0	26.2	30	-6.3	10	88	54	78	73	1.2	8.2	2.4	3.9	6.2	6.7	5.2	6.0
V	1002.7	1013.6	992.6	1016.3	9.5	14.2	9.9	10.9	15.7	5.2	26.1	19	-1.2	6	78	57	79	71	2.7	8.0	2.8	4.5	5.9	8.1	6.1	6.7
VI	1003.4	1016.5	991.3	1016.7	16.0	21.4	16.4	17.6	23.4	11.1	30.0	11,19	6.0	27	76	52	79	69	4.5	13.0	4.1	7.2	5.7	6.2	5.1	5.7
VII	998.8	1009.6	988.2	1011.9	17.4	22.3	17.9	18.9	23.9	14.1	32.7	8	9.1	29	84	63	84	77	3.2	11.2	3.4	5.9	6.9	7.3	6.9	7.0
VIII	1001.0	1010.6	988.3	1014.2	14.5	19.6	15.3	16.2	21.4	11.2	29.5	12	6.3	24	89	67	87	81	1.8	8.0	2.3	4.0	6.0	7.5	5.2	6.2
IX	999.4	1009.5	982.7	1012.8	9.9	15.0	11.3	11.9	16.5	7.8	28.1	9	-0.3	27	90	67	87	81	1.3	6.4	1.9	3.2	5.8	7.7	5.9	6.5
X	1006.3	1017.2	994.9	1019.9	6.7	12.4	8.6	9.1	13.3	5.5	21.1	19	0.4	2	90	71	87	83	1.1	4.5	1.5	2.4	6.6	7.6	6.4	6.9
XI	1007.5	1027.2	989.9	1021.4	3.4	6.3	3.8	4.3	7.5	1.5	17.0	4	-8.7	30	94	79	90	87	0.6	2.2	0.8	1.2	8.5	7.9	7.4	7.9
XII	1004.3	1019.4	964.5	1015.4	-2.4	-0.2	-1.7	-1.5	0.9	-4.8	7.5	9	-22.7	16	90	83	90	88	0.6	1.0	0.6	0.7	7.9	8.8	7.2	8.0
Rok	1003.0	1027.2	964.5	1016.7	6.7	11.2	7.8	8.4	12.6	4.2	32.7	8.VII	-22.7	16.XII	86	68	84	79	1.6	5.8	2.0	3.1	6.9	7.5	6.2	6.9

Wielichowo

$\varphi = 52°07'$ $\lambda = 16°21'$

I	–	–	–	–	-1.5	1.2	-0.6	-0.4	2.2	-3.8	11.0	6	-16.8	16	87	81	87	85	0.7	1.3	0.8	0.9	7.5	7.9	6.4	7.3
II	–	–	–	–	1.5	5.7	2.5	3.0	6.5	-0.3	11.4	5	-4.1	27	94	76	89	85	0.6	2.2	0.8	1.2	7.9	7.0	5.6	6.8
III	–	–	–	–	1.3	8.1	3.7	4.2	9.4	-0.1	16.4	13	-5.9	3	86	60	80	75	1.0	4.8	1.8	2.5	4.8	5.0	3.2	4.3
IV	–	–	–	–	4.6	12.6	7.1	7.8	13.8	1.6	24.1	28	-6.6	13	85	50	75	70	1.3	8.0	2.7	4.0	4.9	5.1	3.0	4.4
V	–	–	–	–	9.2	14.9	10.2	11.1	16.5	4.5	25.6	19	-4.4	7	73	45	67	62	3.2	10.0	4.2	5.8	4.7	5.6	4.4	4.9
VI	–	–	–	–	15.7	21.7	16.8	17.8	24.4	9.9	32.4	29	4.3	26	75	50	73	66	4.7	14.0	5.5	8.1	4.8	4.4	3.5	4.2
VII	–	–	–	–	17.4	22.2	18.1	19.0	24.5	13.8	33.4	4,5	7.0	3	84	63	81	76	3.4	11.5	4.4	6.4	6.2	6.1	6.6	6.3
VIII	–	–	–	–	14.1	19.6	14.8	15.8	21.1	10.5	27.8	11	4.3	23	89	62	84	78	1.9	9.1	2.9	4.6	5.9	6.8	3.3	5.3
IX	–	–	–	–	9.5	15.4	10.9	11.7	16.7	6.7	28.2	8	-2.2	27	90	67	85	81	1.2	6.4	2.1	3.2	6.2	7.0	4.6	5.9
X	–	–	–	–	6.3	13.1	7.7	8.7	14.0	3.6	21.1	19	-4.2	2	92	68	89	83	0.8	5.0	1.2	2.3	6.9	6.0	3.9	5.6
XI	–	–	–	–	2.8	6.5	4.0	4.3	7.3	1.3	15.9	5	-7.2	22	89	81	87	86	0.8	2.1	1.1	1.3	7.5	7.8	7.1	7.5
XII	–	–	–	–	-2.1	0.2	-1.2	-1.1	1.5	-4.1	10.3	8	-19.6	17	91	88	90	90	0.4	0.7	0.5	0.5	7.5	7.5	6.3	7.1
Rok	–	–	–	–	6.6	11.8	7.8	8.5	13.2	3.6	33.4	4,5.VII	-19.6	17.XII	86	66	82	78	1.7	6.3	2.3	3.4	6.2	6.4	4.8	5.8

Borowo

$\varphi = 52°07'$ $\lambda = 16°47'$

I	–	–	–	–	-1.3	0.9	-0.6	-0.4	1.7	-2.8	9.9	6	-14.0	16,17	87	85	88	87	0.6	1.0	0.6	0.7	8.6	7.7	7.4	7.9
II	–	–	–	–	1.7	5.4	2.8	3.2	6.2	0.5	10.2	14	-3.5	27	87	76	88	84	0.9	2.3	0.9	1.4	7.8	8.1	7.4	7.8
III	–	–	–	–	1.3	7.4	3.7	4.0	9.1	0.3	16.3	13	-4.9	3,11	84	62	83	76	1.2	4.3	1.4	2.3	6.0	5.4	5.2	5.5
IV	–	–	–	–	4.7	11.8	7.0	7.6	14.1	2.2	23.2	28	-4.7	13	86	55	78	73	1.2	7.0	2.3	3.5	5.6	6.5	5.6	5.9
V	–	–	–	–	9.0	14.6	10.3	11.0	16.1	5.2	26.5	19	-1.5	7	75	49	70	65	3.0	9.6	4.1	5.6	4.7	6.2	5.4	5.3
VI	–	–	–	–	15.6	21.8	17.0	17.8	23.4	11.1	30.6	30	6.3	26	75	53	74	67	4.7	13.8	5.3	7.9	5.1	5.5	5.4	5.3
VII	–	–	–	–	17.3	22.2	18.2	19.0	24.0	14.7	33.7	5	8.2	3	84	64	83	77	3.6	11.3	4.0	6.3	7.2	7.3	7.9	7.5
VIII	–	–	–	–	14.1	19.6	15.1	16.0	21.3	11.6	27.7	11	6.8	23	89	64	85	79	1.8	8.7	2.7	4.4	6.8	7.4	6.5	6.8
IX	–	–	–	–	9.8	15.1	11.2	11.8	16.6	8.0	28.3	8	-0.4	27	91	69	87	82	1.1	6.0	1.8	3.0	6.7	7.5	6.7	7.0
X	–	–	–	–	6.9	12.7	8.6	9.2	13.6	5.0	20.3	19	-2.1	2	93	72	90	85	0.8	4.3	1.2	2.1	8.2	6.4	4.4	6.3
XI	–	–	–	–	3.1	6.4	4.2	4.5	7.3	1.9	16.6	5	-6.7	30	90	79	87	85	0.8	2.3	1.1	1.4	8.2	8.0	7.7	8.0
XII	–	–	–	–	-1.8	0.1	-1.0	-0.9	1.3	-3.4	9.6	8	-16.3	17	91	88	89	89	0.5	0.7	0.6	0.6	8.8	8.0	7.0	7.9
Rok	–	–	–	–	6.7	11.5	8.0	8.6	12.9	4.5	33.7	5.VII	-16.3	17.XII	86	68	84	79	1.7	5.9	2.2	3.3	7.0	7.0	6.5	6.8

Rudka

$H_s = 169\ m$ $h_m = 8\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, %mD)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v		=	≥0.5	◔	●	▩
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10	Max≥25	R≥0.1	R≥1.0	R≥10.0	v≥10	v≥15					
I	1	2.0	6.5	4.8	3	4.3	9.5	3.7	7.5	2.5	2.5	3.4	32.5	5.1	6	5.2	2	4.1	34.8	7.8	6	25	11	7		14	9	·	1	·	–	·	1	21	–
II	7	2.8	2.5	1.8	2.5	1.8	5	2.4	2.1	4.3	2.2	2.8	18.5	4.5	4.5	12.4	1	3.4	55.6	6.4	8	15	2	·	·	22	19	·	2	·	–	·	1	15	–
III	1.4	2.9	12.5	2.6	7.5	3.3	1.3	6.3	7	3.6	5	3.9	18.5	4.8	11.5	4.7	4	4.0	24.6	12.2	15	22	6	1	·	7	4	1	5	1	–	·	9	5	–
IV	21.5	2.7	5.5	2.5	7.5	2.3	6.5	2.4	8	3.4	7.5	3.3	8	2.3	18.5	2.8	7	2.5	14.6	6.0	30	8	·	·	3	9	6	·	·	·	–	3	6	9	–
V	14.5	2.8	13.5	2.4	8	2.3	5	2.4	4	1.2	5.5	2.1	11.5	3.3	2.9	2.3	2	2.4	45.3	14.7	7	1	·	·	1	7	7	2	·	·	–	·	3	12	–
VI	1.8	2.7	5	2.0	1.5	3.5	4.5	4.2	8.5	3.8	9	2.8	2.5	3.2	14.5	3.6	4	3.0	37.2	9.4	24	·	·	·	1.3	8	8	·	·	·	–	3	6	5	–
VII	12.5	2.1	4.5	1.2	6	2.7	6.5	2.8	6	2.3	12.5	2.2	26.5	2.7	14.5	2.2	4	2.3	96.6	19.0	16	·	·	·	1.3	16	15	3	·	·	–	3	3	13	–
VIII	2.5	3.0	1	1.0	1	4.0	5	2.0	5.5	2.5	1.8	3.1	36.5	2.4	23.5	2.0	·	2.4	143.8	43.0	14	·	·	·	4	14	14	6	·	·	–	3	2	7	–
IX	6	1.2	·	·	·	·	·	·	10.5	2.4	2.1	3.0	3.3	3.4	16.5	2.3	3	2.7	82.8	27.0	23	·	·	·	1	12	12	2	2	1	–	·	2	11	–
X	2	2.8	1.5	1.3	·	·	4	2.8	6.5	3.4	3.4.6	2.7	26.5	3.1	1.2	2.2	6	2.6	14.2	4.5	20	1	·	·	·	5	5	·	·	·	–	·	4	10	–
XI	6.5	9.5	8.5	3.6	9	2.7	1.5	3.8	16.5	2.6	9.5	2.5	1.7	4.4	4	7.5	4	3.8	29.3	7.5	24	11	1	·	·	7	7	·	4	1	–	·	1	20	–
XII	21.5	2.0	0.5	3.0	2	1.5	2	1.5	8.5	3.0	3.0	4.7	12.5	4.3	1.2	3.2	4	3.3	31.2	13.2	14	27	11	3	·	8	7	1	2	·	–	·	2	16	–
Rok	12.7	3.0	6.1.5	2.2	4.8	2.4	7.6	2.9	10.9.5	2.9	19.9.5	3.0	2.6.6	3.6	16.6.5	3.4	4.1	3.0	61.0.0	43.0	14.VIII	11.0	3.1	4.1	3.5	12.9	11.3	1.5	1.6	3	–	1.2	4.0	14.4	–

Brwinów

$H_s = 96 m$ $H_b = 111,4\ m$ $h_w = 11 m$

I	1	2.0	5.5	3.5	8.5	3.6	3.5	3.0	10	3.5	26.5	4.2	35.5	4.8	0.5	2.0	2	4.1	23.1	4.8	5	25	11	3	·	9	8	·	1	·	2	·	4	19	20
II	7	2.8	1	2.5	6.5	2.8	8.5	3.5	17.5	4.3	18	4.2	18	4.6	2.5	4.0	5	3.8	38.1	8.0	18	14	1	·	·	22	9	·	1	·	2	·	·	18	1
III	9	3.7	4	2.6	19.5	4.8	1.3	5.0	5.5	3.0	10	6.1	20.5	4.9	6.5	4.0	5	4.4	25.3	10.5	15	20	4	·	·	7	5	1	7	·	·	·	7	9	·
IV	6.5	2.4	8	2.9	12	2.2	6.5	2.8	6.5	4.0	2.5	2.8	2.3	2.6	14	2.6	11	2.4	9.1	2.4	20,30	8	·	·	3	9	4	·	1	·	3	2	6	8	·
V	15.5	2.8	5	3.2	10.5	3.6	8.5	3.4	3.5	2.9	8	4.4	12	4.5	4.8	3.7	12	3.1	37.9	21.4	9	3	·	·	1	5	4	1	2	·	1	1	2	10	·
VI	8	3.1	2	2.8	8	2.4	9.5	2.9	3.5	3.3	11	3.8	20	4.6	15	3.9	13	3.1	38.4	14.8	10	·	·	·	8	9	6	2	·	·	·	3	7	8	·
VII	3	2.2	7	2.1	6	2.8	6.5	3.3	10.5	3.2	14.5	2.8	25.5	2.8	11	3.1	9	2.6	151.7	47.7	2	·	·	·	11	15	12	4	·	·	1	7	4	16	·
VIII	2	1.5	3	1.3	3	4.0	1.0	3.2	5	4.0	27.5	3.7	27.5	3.4	12	3.0	3	3.2	70.7	15.5	14	·	·	·	6	15	11	4	·	·	·	·	1	5	·
IX	3	1.7	0.5	1.0	·	·	8.5	2.8	1.0	5.0	30.5	4.8	27	4.9	3.5	3.1	7	4.1	79.3	23.5	23	1	·	·	2	19	13	1	6	·	·	·	2	9	·
X	1	2.0	·	·	2	2.2	10.5	3.2	16.5	3.2	30.5	4.8	23	3.8	2.5	2.8	7	3.4	4.3	1.4	20	·	·	·	·	7	2	·	1	·	2	·	3	11	·
XI	6	6.6	7.5	3.3	16.5	2.8	2.0	4.7	6.5	3.6	10.5	5.3	11	7.0	2	10.0	10	4.2	14.1	6.5	28	12	1	·	·	7	4	·	3	·	5	·	2	20	·
XII	6.5	2.5	·	·	3.5	4.1	10.5	3.1	9	3.4	35.5	6.0	12.5	4.1	2.5	3.2	13	3.9	43.4	24.2	14	25	10	3	·	13	6	1	6	·	·	·	1	17	9
Rok	68.5	2.8	43.5	2.1	96	2.9	11.5.5	3.4	10.4	3.6	22.5	4.4	25.5.5	4.3	90	3.8	97	3.5	53.5.4	47.7	2.VII	10.8	2.7	6	3.1	13.7	8.4	1.4	2.8	·	1.9	1.3	3.9	16.0	3.0

Wielichowo

$H_s = 65 m$ $h_w = 10 m$

I	3	1.5	6.5	4.7	7.5	2.8	·	·	2	2.0	1.8	2.3	4.5	3.9	4	5.4	7	3.2	26.7	5.5	5	22	7	5	·	13	9	·	·	·	1	·	5	17	–
II	2.5	1.8	3.5	2.7	2.5	3.2	7	1.9	6	2.2	2.6	3.2	2.5.5	3.1	4	3.8	7	2.7	43.8	7.7	18	17	·	·	·	18	12	·	·	·	·	·	·	6	–
III	5	2.2	4.5	2.4	1.8	4.9	11.5	4.0	5	4.4	9	2.7	2.1	4.3	7	3.7	12	3.4	32.8	11.9	17	16	·	·	·	8	6	1	3	·	1	·	12	8	–
IV	13.5	2.4	24.5	2.4	5.5	2.6	4	3.1	1	4.5	5.5	2.6	9	3.1	1.5	2.3	12	2.2	19.3	4.5	29	12	·	·	·	10	7	·	·	·	2	1	6	2	–
V	1.5	2.6	11.5	2.6	8.5	2.2	4.5	2.8	3.5	1.7	3	2.5	12.5	3.5	16.5	2.9	18	2.2	12.8	4.6	23	3	·	·	4	6	5	·	·	·	·	3	4	3	–
VI	9	1.8	7	1.6	14.5	1.9	5	2.2	4	2.5	8	2.8	22.5	3.1	6	2.3	14	2.0	45.8	12.6	24	·	·	·	12	9	7	2	·	·	1	4	9	4	–
VII	6	2.4	5.5	1.6	6	2.3	2	3.2	3.5	2.1	16.5	2.4	26	2.8	7.5	2.3	20	2.0	91.7	14.6	10	·	·	·	12	19	13	4	·	·	1	6	8	13	–
VIII	2.5	1.4	0.5	3.0	3.5	1.9	2	2.5	3.5	1.7	31.5	2.6	30	2.0	5.5	2.2	14	1.9	47.6	10.8	24	·	·	·	3	19	10	1	1	·	2	7	8	4	–
IX	2	1.5	0.5	1.0	0.5	1.0	·	·	4.5	3.7	26.5	3.0	28.5	3.2	5.5	2.1	2.2	2.3	68.3	11.0	23	2	·	·	1	16	16	1	1	1	3	4	3	7	–
X		·	2	2.2	2.5	2.6	1.5	2.0	4	2.0	2.0	2.9	2.7.5	3.1	3.5	2.6	3.2	1.9	6.9	2.1	24	3	·	·	·	7	2	·	·	·	1.2	·	5	7	–
XI	5.5	1.6	10.5	3.2	20.5	2.8	9	2.4	4.5	3.3	9	2.8	17	4.8	4	4.2	13	2.8	9.2	2.9	28	12	2	·	·	10	3	·	1	1	4	1	4	18	–
XII	5.5	1.8	4.5	2.1	4.5	2.2	2.5	1.4	5	2.1	21.5	2.7	30.5	3.9	6	2.5	13	2.5	52.0	9.6	14	24	8	3	·	14	8	·	·	·	3	·	2	15	–
Rok	6.9.5	1.8	8.1	2.5	9.4	2.5	4.9	2.1	4.3.5	2.7	19.4.5	2.7	2.9.5	3.4	8.4.5	3.0	18.4	2.4	43.6.9	14.6	10.VII	11.1	1.7	8	2.9	14.9	9.8	9	6	2	3.0	2.6	6.2	10.4	–

Borowo

$H_s = 80 m$ $h_w = 10 m$

I	5	1.0	2	4.0	1.0	4.1		·	3.5	1.6	13.5	3.1	5.1	6.9	8	3.4	·	4.6	19.1	6.0	5	21	9	2	·	13	5	·	7	3	–	·	2	17	19
II	1	1.0	4	1.5	9	1.9	7.5	2.6	16.5	4.8	1.5	4.3	28.5	4.7	2.5	2.2	·	3.9	35.1	13.2	18	8	·	·	·	13	9	1	2	·	–	·	·	11	·
III	1.0	1.7	4.5	1.7	23.5	4.8	12.5	6.8	7.5	6.0	5	4.7	2.1	7.0	7	3.1	2	5.0	27.0	10.5	17	16	·	·	·	7	8	1	8	2	2	·	6	13	·
IV	3.5	2.3	5	1.4	12	1.5	4	3.6	4	3.0	2	2.5	17	2.9	9	4.0	2	2.5	15.2	5.4	24	11	·	·	·	7	5	·	·	·	4	·	5	8	·
V	14.5	2.7	11	3.8	18	2.3	7	2.3	1	1.0	3.5	2.4	12.5	4.0	24.5	3.5	1	3.0	21.7	9.6	5	2	·	·	2	6	3	·	3	1	·	1	1	8	1
VI	8.5	1.7	4	1.5	16	1.8	6.5	2.2	7	2.7	9	3.3	2.7	3.6	12	2.4	·	2.6	48.7	14.7	4	·	·	·	9	10	9	1	·	·	·	5	7	10	–
VII	4.6	2.0	5	1.4	7	2.7	6.5	2.2	1.5	2.3	4.5	1.9	33.5	4.4	17	2.9	2	3.0	133.0	26.2	23	·	·	·	12	17	14	5	·	·	1	2	2	18	·
VIII	2	2.5	2.5	2.2	1	7.0	1	7.0	4	3.9	13.5	5.1	5.6	3.5	12	2.9	1	3.6	46.8	8.5	24	·	·	·	2	12	9	·	1		1	1	·	11	·
IX	1	2.0	1	1.0	0.5	1.0	0.5	1.0	1.0	2.8	2.1.5	5.0	3.7	4.5	15.5	3.3	3	4.0	75.3	9.3	23	1		·	1	16	14	·	2	1	3	2	1	14	·
X				·	3	2.7	8	3.0	7.5	3.8	2.9	2.3	3.3	3.7	6.5	1.5	6	2.8	4.5	2.3	1	1	·	·	·	6	2	·	·	·	11	·	3	9	·
XI	5	6.4	5	3.8	3.3	2.9	8.5	2.4	6	4.8	9.5	2.9	2.1	7.9	·	·	2	4.1	6.4	2.2	28	10	2	·	·	6	3	·	5	1	5	·	3	19	·
XII	7	2.1	6	2.0	7	2.1	2.5	4.0	5	4.8	2.3.5	3.3	3.0	6.2	1.0	4.0	2	3.8	27.3	8.9	8	2.2	9	3	·	10	6	·	4	3	5	·	1	17	6
Rok	10.5	2.1	5.0	2.0	14.0	2.9	6.4.5	2.8	7.3.5	3.0	14.9.5	3.4	36.7.5	4.9	12.4	2.8	2.1	3.6	46.0.1	26.2	23.VII	9.2	2.0	5	2.6	12.3	8.5	8	3.2	1.1	–	1.4	3.4	15.3	26.1

Sękocin

$\varphi = 52°07'$ $\lambda = 20°53'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	1.5	4.6	2.4	2.7	5.9	-0.5	10.4	14,24	-4.6	28	-	-	-	-	-	-	-	-	8.9	8.1	7.2	8.1
III	-	-	-	-	-0.3	6.0	2.6	2.7	8.0	-2.4	17.3	31	-11.3	4	-	-	-	-	-	-	-	-	5.7	5.5	4.5	5.2
IV	-	-	-	-	5.3	12.8	7.4	8.2	14.7	2.3	26.3	27	-7.2	10	-	-	-	-	-	-	-	-	5.6	6.0	4.4	5.3
V	-	-	-	-	9.1	14.3	9.8	10.8	15.9	5.3	27.1	19	-2.4	6	-	-	-	-	-	-	-	-	5.6	7.4	5.5	6.2
VI	-	-	-	-	16.1	22.3	17.0	18.1	24.2	10.5	31.6	11	5.3	27	-	-	-	-	-	-	-	-	5.0	6.0	4.5	5.2
VII	-	-	-	-	17.5	22.8	18.2	19.2	24.3	13.5	34.5	5	8.8	29	-	-	-	-	-	-	-	-	6.9	7.0	7.0	7.0
VIII	-	-	-	-	14.4	20.0	15.1	16.2	21.4	10.9	30.3	12	5.7	24	-	-	-	-	-	-	-	-	5.5	7.0	4.2	5.6
IX	-	-	-	-	9.9	15.1	11.1	11.8	16.8	7.4	28.1	9	-1.0	27	-	-	-	-	-	-	-	-	6.4	7.5	5.4	6.4
X	-	-	-	-	6.3	12.1	8.3	8.7	13.7	4.3	24.2	19	-0.4	2	-	-	-	-	-	-	-	-	7.0	7.4	5.8	6.7
XI	-	-	-	-	3.4	6.2	3.9	4.4	7.7	1.2	17.3	4	-8.7	29	-	-	-	-	-	-	-	-	9.1	7.8	7.0	8.0
XII	-	-	-	-	-2.3	-0.5	-1.5	-1.4	1.2	-4.6	7.9	13,14	-21.4	16	-	-	-	-	-	-	-	-	8.1	8.9	6.6	7.9
Rok	-	-	-	-	-	-	-	-	-	-	34.5	5.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Świder

$\varphi = 52°07'$ $\lambda = 21°15'$

I	-	-	-	-	-2.1	0.3	-1.1	-1.0	1.2	-4.2	7.4	6	-17.2	17	84	78	83	82	0.8	1.3	0.9	1.0	8.3	8.7	7.3	8.1
II	-	-	-	-	1.5	4.7	2.3	2.7	5.6	-0.5	10.1	21	-4.7	28	89	76	86	84	0.7	2.2	1.0	1.3	8.7	8.6	6.8	8.0
III	-	-	-	-	-1.0	6.5	1.9	2.3	8.0	-3.5	17.3	31	-12.1	4	80	47	71	66	1.2	5.8	2.1	3.0	5.5	5.9	4.3	5.2
IV	-	-	-	-	5.7	14.0	7.7	8.8	15.2	2.3	27.6	30	-8.0	10	81	44	73	66	4.9	10.5	3.1	5.2	6.8	6.0	4.9	5.7
V	-	-	-	-	10.0	15.1	9.9	11.2	16.4	5.1	27.9	19	-2.7	6	73	53	76	67	3.5	9.3	3.2	5.3	5.6	7.8	5.5	6.3
VI	-	-	-	-	16.4	23.2	17.1	18.4	24.7	10.6	32.0	11	5.2	28	73	46	71	63	5.3	16.3	5.9	9.2	5.1	5.8	4.6	5.2
VII	-	-	-	-	17.7	23.1	18.2	19.3	25.0	13.9	35.0	8	9.2	29	84	60	84	74	4.0	12.8	4.3	7.0	6.5	6.5	5.9	6.3
VIII	-	-	-	-	14.3	20.3	15.5	16.4	22.1	11.0	31.0	12	6.2	24	88	62	86	79	2.0	9.8	2.5	4.8	5.1	6.9	4.1	5.4
IX	-	-	-	-	9.6	15.4	11.1	11.8	17.2	7.7	28.8	9	-1.5	27	90	65	86	80	1.2	7.0	2.1	3.4	5.7	7.3	4.9	6.0
X	-	-	-	-	5.5	12.5	7.8	8.4	13.9	4.3	24.3	19	-0.4	3	94	67	90	84	0.6	5.2	1.2	2.3	6.4	7.0	5.2	6.2
XI	-	-	-	-	3.2	6.3	3.7	4.2	7.9	1.3	17.7	4	-7.9	29	90	76	87	84	0.7	2.5	1.0	1.4	8.0	7.7	6.8	7.5
XII	-	-	-	-	-2.6	-0.2	-1.9	-1.6	1.2	-5.1	8.8	13	-20.3	16	88	82	87	86	0.6	1.1	0.7	0.8	7.2	8.3	6.4	7.3
Rok	-	-	-	-	6.5	11.8	7.7	8.4	13.2	3.6	35.0	8.VII	-20.3	16.XII	84	63	84	76	1.9	7.0	2.3	3.7	6.5	7.2	5.6	6.4

Łowicz – Blich

$\varphi = 52°06'$ $\lambda = 19°56'$

I	-	-	-	-	-1.9	0.6	-0.9	-0.8	-	-	-	-	-	-	88	86	88	87	0.6	0.9	0.7	0.7	8.0	8.0	6.9	7.6
II	-	-	-	-	2.0	5.2	2.8	3.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.8	7.2	7.7	7.6
III	-	-	-	-	0.8	6.6	2.8	3.2	-	-	-	-	-	-	83	65	81	76	1.1	4.0	1.5	2.2	5.1	5.3	4.4	4.9
IV	-	-	-	-	5.2	13.3	7.8	8.5	-	-	-	-	-	-	85	53	77	72	1.4	6.5	2.6	4.2	5.7	6.5	6.2	6.1
V	-	-	-	-	9.4	15.1	10.2	11.2	-	-	-	-	-	-	84	57	79	72	2.3	8.5	2.9	4.6	5.7	7.1	5.4	6.1
VI	-	-	-	-	14.8	20.9	15.4	16.1	23.9	10.9	30.0	11	6.1	15	81	54	69	68	3.3	12.1	6.9	7.4	4.8	5.5	4.1	4.8
VII	-	-	-	-	16.3	21.9	18.8	19.0	24.2	13.8	34.4	8	9.5	29	89	65	81	78	2.2	10.6	4.6	5.8	6.2	7.1	6.5	6.6
VIII	-	-	-	-	14.4	19.9	15.3	16.2	21.8	11.6	26.5	11	7.1	30	93	69	90	84	1.2	7.7	1.7	3.5	5.9	7.5	4.8	6.1
IX	-	-	-	-	10.1	15.4	11.4	12.1	17.0	7.8	28.1	9	-0.5	27	92	70	89	84	1.0	6.0	1.6	2.9	5.9	7.8	5.5	6.4
X	-	-	-	-	6.5	12.4	8.6	9.0	13.7	5.0	20.6	19	-0.4	2	94	75	89	86	0.7	4.0	1.2	2.0	6.5	7.5	6.3	6.8
XI	-	-	-	-	3.7	6.6	4.2	4.7	8.0	-	16.5	4,5	-	-	89	82	89	87	0.8	2.0	0.9	1.2	8.2	7.1	7.3	7.5
XII	-	-	-	-	-2.2	0.0	-1.3	-1.2	1.3	-4.3	7.3	9	-19.7	16	90	86	89	88	0.5	0.9	0.6	0.7	7.3	8.7	6.7	7.6
Rok	-	-	-	-	6.6	11.5	8.2	8.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.4	7.1	6.0	6.5

Uwaga. W okresie 2.VI. – 19.VII. obserwacje we wszystkich terminach wykonywano o godzinę za wcześnie.

Chylice

$\varphi = 52°06'$ $\lambda = 20°34'$

I	-	-	-	-	-2.0	0.1	-1.1	-1.0	1.1	-3.5	8.0	6	-15.9	16	87	84	89	87	0.6	1.0	0.6	0.7	8.0	7.8	6.8	7.5
II	-	-	-	-	1.8	4.7	2.7	3.0	5.7	0.3	9.5	14	-3.6	4	91	78	87	85	0.5	2.0	1.0	1.2	7.7	7.4	6.9	7.3
III	-	-	-	-	0.3	5.7	2.7	2.8	7.7	-1.2	15.8	31	-7.5	4	82	57	80	73	1.2	4.5	1.5	2.4	5.3	5.2	4.7	5.1
IV	-	-	-	-	5.4	12.7	7.4	8.2	13.9	2.7	25.6	30	-5.0	10	87	58	82	75	1.4	7.5	1.9	3.6	5.6	5.7	4.7	5.3
V	-	-	-	-	9.5	14.0	9.9	10.8	15.4	5.4	25.8	19	-1.2	6	83	60	80	74	2.2	7.4	2.6	4.1	5.5	7.3	5.5	6.0
VI	-	-	-	-	16.1	21.3	16.2	17.4	23.3	10.7	29.9	11	5.7	27	80	60	82	74	3.7	11.1	3.4	6.1	4.7	5.1	3.4	4.4
VII	-	-	-	-	17.4	22.3	17.5	18.7	23.8	13.6	33.5	8	9.4	29	-	-	-	-	-	-	-	-	6.0	6.3	5.5	5.9
VIII	-	-	-	-	14.8	19.7	15.1	16.2	21.5	11.3	29.7	12	6.7	24	92	71	93	85	1.4	7.3	1.4	3.4	5.0	6.9	3.5	5.1
IX	-	-	-	-	9.8	15.0	11.4	11.9	16.5	7.9	27.6	9	-0.5	27	93	73	90	85	0.9	5.4	1.6	2.6	5.8	7.0	5.2	6.0
X	-	-	-	-	6.8	12.4	8.5	9.0	13.6	5.3	21.4	19	0.4	2	92	73	89	85	0.9	4.2	1.3	2.1	5.5	6.7	5.2	5.8
XI	-	-	-	-	3.5	6.4	3.8	4.4	7.6	1.8	17.4	4	-7.6	29,30	90	79	87	85	0.8	2.2	1.0	1.3	8.0	7.6	6.9	7.5
XII	-	-	-	-	-2.3	-0.2	-1.4	-1.3	1.2	-4.4	7.5	9,14	-21.1	16	88	82	86	85	0.5	1.1	0.8	0.8	7.5	8.1	7.2	7.6
Rok	-	-	-	-	6.8	11.2	7.7	8.4	12.6	4.2	33.5	8.VII	-21.1	16.XII	-	-	-	-	-	-	-	-	6.2	6.8	5.4	6.1

Sękocin

$H_s = 110$ m

1957

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ 0°	Max < 0°	Min < 10	Max ≥ 25°	0,1 ≤ R < 1,0	1,0 ≤ R < 10,0	R ≥ 10,0	v ≥ 10	v ≥ 15	≡	≥ 0,5	◔	◕	⊞
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51.4	10.0	18	15	·	·	·	23	13	1	–	–	–	·	1	14	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32.4	12.8	15	19	3	1	·	9	5	1	–	–	–	·	6	5	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	28.0	14.7	29	8	·	·	3	8	6	1	–	–	–	3	6	7	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41.2	26.1	9	1	·	·	2	3	3	1	–	–	–	·	2	10	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36.3	12.4	4	·	·	·	11	10	6	1	–	–	–	1	8	8	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	127.6	29.2	17	·	·	·	12	15	11	4	–	–	–	6	3	17	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	83.1	22.3	10	·	·	·	6	15	11	3	–	–	–	1	5	9	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	97.8	20.8	23	1	·	·	2	18	14	3	–	–	–	·	2	9	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.2	2.3	1	1	·	·	·	10	4	·	–	–	–	·	4	12	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.4	12.9	28	12	1	·	·	9	7	1	–	–	–	·	2	19	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	46.6	23.7	14	26	10	3	·	10	7	1	–	–	–	·	2	20	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29.2	17.VII	–	–	–	36	–	–	–	–	–	–	–	–	–	–

Świder

$H_s = 100$ m $\quad h_w = 12$ m

I	2	4.2	5.5	3.0	7	2.6	12.5	2.2	11.5	2.3	14.5	3.1	23.5	3.8	8.5	3.5	8	2.8	25.5	5.0	5	25	11	5	·	14	7	·	·	·	3	·	3	22	22
II	4	3.0	5.5	2.0	6	2.4	23.5	2.7	12	2.8	11	3.1	12.5	2.7	4.5	3.7	5	2.6	52.4	14.1	18	16	1	·	·	24	14	1	·	·	·	8	·	1	18	4
III	6.5	3.2	13	2.1	14.5	3.6	16.5	4.6	6	3.1	3.5	3.0	17.5	4.5	7.5	3.0	8	3.3	29.3	13.2	15	23	3	2	·	8	6	1	3	·	1	·	9	9	2
IV	9	2.4	13	2.2	10.5	1.8	10.5	2.9	4	2.5	4	2.5	7.5	2.0	14.5	2.4	17	1.9	20.4	4.2	7	8	·	·	4	11	8	·	·	·	·	4	6	8	1
V	1.9	2.5	15.5	2.1	14	2.4	9	2.6	3	2.8	5	2.5	4	4.0	10.5	2.9	13	2.2	32.4	13.1	9	2	·	·	2	5	4	1	·	·	1	·	3	10	·
VI	1.1	2.2	1.0	1.8	8	1.3	9	1.9	7.5	3.3	9	3.0	10	3.2	10.5	2.9	15	2.0	35.7	8.6	24	·	·	·	12	12	10	·	·	·	2	6	6	7	·
VII	7	2.1	1.1	2.1	1.3	2.0	11.5	2.2	4.5	1.8	6	1.8	10.5	2.5	12.5	2.4	17	1.8	83.6	17.7	16	·	·	·	1.4	16	11	4	·	·	2	7	4	13	·
VIII	5.5	1.4	1.5	1.3	6.5	1.9	6.5	2.5	1.0	2.8	1.1	3.3	12	3.2	12	2.2	28	1.8	80.4	13.3	14	·	·	·	6	17	13	3	·	·	2	3	3	5	·
IX	4	1.5	1.5	1.7	1	1.5	11.5	2.0	10.5	2.8	16	3.0	17.5	3.9	8	2.2	20	2.2	78.6	18.1	23	2	·	·	2	1.7	12	3	1	·	6	1	2	8	·
X	2.5	1.4	1.5	2.3	5.5	1.7	21	1.7	11.5	2.0	12	3.0	11.5	3.2	3.5	2.3	24	1.7	9.1	2.1	30	1	·	·	·	8	5	·	·	·	4	·	3	11	·
XI	4	5.4	7.5	2.1	14.5	2.2	22.5	2.8	7	3.5	1.5	5.0	9.5	3.9	7.5	4.6	16	2.6	21.3	10.0	28	11	1	·	·	7	6	1	·	·	5	·	2	16	·
XII	6.5	1.6	6	1.8	5	1.8	13	1.7	11	3.4	13	3.3	8.5	2.8	4	3.2	26	1.8	42.0	20.3	14	25	11	3	·	12	8	2	·	·	1	·	2	14	22
Rok	8.1	2.6	91.5	2.0	105.5	2.1	16.7	2.5	98.5	2.8	106.5	3.0	144.5	3.3	103.5	2.9	197	2.2	510.7	20.3	14.XII	113	27	10	10	151	104	16	4	·	35	21	44	141	51

Łowicz – Blich

$H_s = 95$ m $\quad h_w =$ I–VI 10 m, VII–XII 12 m

I	4	2.0	7	3.1	1.5	3.7	4.5	2.7	1.5	1.3	11	3.6	26.5	4.7	2.3	5.3	14	3.1	24.7	6.4	31	–	–	–	–	8	7	·	2	1	12	·	5	19	19
II	8.5	2.0	2.5	4.0	1	5.0	8.5	2.6	1.0	3.8	9	3.6	20.5	4.3	1.7	3.9	7	3.3	51.8	12.6	19	–	–	–	–	20	12	1	3	1	4	·	2	14	·
III	1.9	2.3	1.2	4.0	2.5	11.0	8	9.6	9.5	5.7	3.5	4.8	1.4	7.3	14.5	4.0	10	4.6	22.7	6.6	17	–	–	–	–	7	5	·	7	4	2	·	9	8	·
IV	23.5	2.0	5	2.4	4.5	5.3	3	2.2	6	4.3	2	2.2	4	3.9	3.0	2.9	12	2.5	18.3	9.4	30	–	–	–	–	11	4	·	1	1	3	2	6	12	·
V	34.5	2.5	8.5	2.3	3.5	4.0	5	2.4	1	1.0	1.5	1.0	7.5	4.9	21.5	3.5	10	2.7	26.5	14.3	10	–	–	–	–	6	4	1	1	1	1	1	3	10	·
VI	14.5	2.3	13.5	2.0	6.5	2.1	8.5	3.0	8	2.9	11.5	3.5	11.5	3.4	11	3.0	5	2.6	40.5	10.0	4	·	·	·	9	9	7	1	2	1	2	4	8	6	·
VII	7.5	2.9	6.5	3.2	8.5	1.7	5.5	3.6	12.5	2.6	9.5	2.6	17	3.0	12	3.2	14	2.4	99.7	37.6	21	·	·	·	13	15	11	4	·	·	1	5	2	12	·
VIII	6	2.0	1	3.0	2	1.5	8.5	2.5	1.0	2.2	2.2	3.3	16.5	2.8	12	3.6	15	2.4	58.2	11.6	10	·	·	·	5	13	12	2	1	·	2	1	1	7	·
IX	2.5	1.0	1	2.0	1	4.0	9.5	2.6	2.1.5	3.7	2.0	4.4	1.4	5.6	10.5	3.8	10	3.5	70.6	10.8	15	1	·	·	2	20	15	2	5	2	4	·	2	8	·
X	2	2.8	3.5	1.9	1	3.0	1.4	2.9	27.5	3.1	1.7	3.4	12.5	2.9	4.5	4.6	11	2.8	5.9	3.9	20	1	·	·	·	6	1	·	·	·	5	·	3	12	·
XI	1.0	6.0	1.4	4.5	8	2.9	21.5	3.6	11	2.8	9.5	5.6	10.5	7.3	2.5	12.2	5	4.6	21.7	6.3	27	–	1	–	·	7	5	·	4	1	3	·	5	17	·
XII	6	3.5	6.5	3.0	2	2.5	1.3	3.1	1.8	4.9	1.3	7.0	1.0	4.2	8.5	3.3	16	3.6	21.5	7.5	14	25	9	3	·	10	7	·	3	2	7	·	3	15	12
Rok	1.3.8	2.6	8.1	3.0	4.2	3.9	109.5	3.4	136.5	3.2	129.5	3.7	164.5	4.5	1.6.7	4.3	1.2.7	3.2	462.1	37.6	2.1.VII	–	–	–	–	132	90	11	29	14	46.4	1.3	47	140	31

Chylice

$H_s = 98$ m $\quad h_w = 12$ m

I	0.5	2.0	4	3.0	6	2.8	3.5	2.9	5	3.0	4.1	2.7	2.6.5	2.5	3.5	3.1	3	2.6	2.6.5	9.8	5	25	11	3	·	10	6	·	·	·	1	–	4	19	–
II	5	2.1	5	1.9	1.5	1.0	6.5	1.8	3.5	2.6	2.8.5	2.8	1.3	2.9	4	2.8	1.2	2.2	2.8.0	8.3	8	1.3	1	·	·	1.8	7	·	·	·	2	–	1	1.2	–
III	9	3.5	6.5	2.6	9	4.2	1.5	4.4	9.5	2.6	6.5	3.9	2.1	3.4	7.5	2.5	9	3.2	25.1	10.0	1.5	20	3	·	·	7	4	1	2	·	·	–	7	7	–
IV	1.2	2.5	4	2.2	4	1.9	1.0	2.0	5.5	1.7	9.5	1.8	1.4	1.6	2.0	2.2	1.1	1.8	12.8	3.5	30	9	·	·	3	9	5	·	·	·	2	–	8	8	–
V	1.1.5	2.7	1.3.6	2.7	6	2.8	1.0	2.4	4	2.0	9.5	2.7	8.5	2.9	2.3	2.6	7	2.5	32.7	1.4.5	9	3	·	·	1	7	5	1	·	·	1	–	3	10	–
VI	1.4.5	2.3	7.5	2.1	2	1.7	2.5	2.8	5.5	1.7	1.5.5	2.6	1.7.5	2.4	2.4	2.3	1	2.3	1.8.2	1.9.4	9	·	·	·	9	1.1	6	1	·	·	·	–	8	5	–
VII	8.5	2.4	6	1.4	5	2.9	5	1.6	6	2.2	1.9	2.1	2.4	2.3	1.1.5	1.8	8	1.9	1.1.9.1	4.3.0	2	·	·	·	1.3	1.6	1.3	3	·	·	–	–	7	1.1	–
VIII	3.5	1.0	·	·	2	1.8	4	4.0	7.5	2.9	1.7	3.4	3.4.5	2.4	1.5.5	2.4	9	2.4	5.9.8	1.3.2	1.4	·	·	·	5	1.3	1.1	2	·	·	2	·	4	4	–
IX	2.5	1.4	·	·	·	·	6.5	2.4	1.0	3.6	2.9.5	3.7	2.7.5	2.7	6	2.1	9	2.8	7.9.5	1.6.6	2.3	1	·	·	2	1.9	1.3	2	1	·	2	·	4	7	–
X	1.5	3.7	·	·	·	·	3	2.7	1.4	2.7	3.7.5	3.0	2.6	2.6	5	2.2	6	2.6	2.3	1.6	2.0	·	·	·	·	3	1	·	·	·	3	–	3	1.0	–
XI	7.5	5.2	6	1.5	1.0	2.4	1.9	2.5	1.6.5	2.5	7.5	8.3	1.6.5	4.4	3	6.0	4	3.3	1.5.3	5.7	2.8	1.1	1	·	·	7	6	·	·	·	·	–	1	1.5	–
XII	5.5	1.6	1	3.0	3.5	2.4	9	2.0	1.2.5	2.2	3.2	3.5	1.8.5	2.7	5	2.1	6	2.6	3.7.1	1.8.0	1.4	2.5	1.0	3	·	5	5	1	1	·	·	–	3	1.8	–
Rok	8.1.5	2.5	6.3.5	2.0	4.9	2.0	9.3	2.6	1.0.4.5	2.5	2.5.3	3.0	2.4.7.5	2.7	1.2.8	2.7	8.5	2.5	4.8.6.4	4.3.0	2.VII	1.0.7	2.6	6	3.3	1.2.5	8.2	1.1	4	·	–	–	5.0	1.2.6	–

Śrem

$\varphi = 52°05'$ $\lambda = 17°01'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o,m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.5	0.9	-0.8	-0.6	2.0	-3.2	10.4	6	-14.2	17	88	85	88	87	0.7	1.0	0.7	0.8	8.5	8.1	5.8	7.5
II	–	–	–	–	1.7	5.4	2.6	3.0	6.3	0.3	10.1	5	-4.1	27	91	77	89	86	0.6	2.2	0.9	1.2	7.1	7.5	5.0	6.5
III	–	–	–	–	4.2	7.8	3.5	4.0	9.2	-0.1	16.4	13	-5.6	11	84	60	81	75	1.2	4.6	1.6	2.5	4.9	5.2	3.3	4.4
IV	–	–	–	–	5.0	12.0	7.0	7.8	13.9	2.0	25.4	28	-6.4	13	88	56	80	75	1.1	6.9	2.1	3.4	6.0	6.6	4.0	5.5
V	–	–	–	–	9.2	14.9	10.1	11.1	16.2	4.6	25.9	19	-2.6	7	78	52	74	68	2.8	9.2	3.5	5.1	4.9	6.5	4.5	5.3
VI	–	–	–	–	15.8	22.0	16.7	17.8	23.5	10.6	30.4	11,19,30	4.8	1	-	-	-	-	-	-	-	-	4.8	5.0	4.0	4.6
VII	–	–	–	–	17.8	22.2	18.2	19.1	24.0	14.3	33.6	5	8.2	3	84	66	83	78	3.8	10.8	4.0	6.3	6.4	6.8	6.6	6.6
VIII	–	–	–	–	14.6	19.7	15.1	16.1	21.4	11.4	27.8	11	6.7	23	90	67	89	82	1.8	8.0	1.9	3.9	5.9	7.4	4.3	5.9
IX	–	–	–	–	9.9	15.3	11.0	11.8	16.7	7.4	28.4	8	-0.6	27	92	70	89	84	1.0	6.1	1.6	2.9	6.7	7.5	5.7	6.6
X	–	–	–	–	6.6	12.9	7.8	8.8	13.8	4.6	20.9	19	-1.8	2	94	74	93	87	0.6	4.1	0.8	1.8	6.9	6.4	3.9	5.7
XI	–	–	–	–	2.9	6.5	4.0	4.4	7.4	1.5	17.4	5	-7.2	30	92	80	89	87	0.9	2.2	0.9	1.3	7.9	7.7	7.4	7.7
XII	–	–	–	–	-2.0	0.1	-1.0	-1.0	1.5	-3.5	9.5	8	-16.5	17	90	89	89	89	0.5	0.6	0.6	0.6	7.7	8.5	6.9	7.7
Rok	–	–	–	–	6.8	11.6	7.8	8.5	13.0	4.2	33.6	5.VII	-16.5	17.XII	-	-	-	-	-	-	-	-	6.5	6.9	5.1	6.2

Błonie – Topola

$\varphi = 52°05'$ $\lambda = 19°11'$

I	–	–	–	–	-2.2	0.4	-1.4	-1.2	1.2	-4.0	7.9	6	-15.7	17	90	86	90	89	0.5	0.9	0.5	0.6	8.6	7.7	6.9	7.7
II	–	–	–	–	1.6	5.0	2.5	2.9	5.8	0.3	10.6	14	-4.1	24	92	79	91	87	0.6	2.0	0.7	1.1	7.9	7.2	7.0	7.4
III	–	–	–	–	0.4	6.7	2.8	3.2	8.5	-1.3	15.4	30	-6.8	11	-	-	-	-	-	-	-	-	5.2	5.7	4.1	5.0
IV	–	–	–	–	4.8	12.2	7.0	7.8	13.9	2.0	25.9	30	-5.6	14	86	56	79	74	1.2	7.6	2.3	3.7	5.8	6.1	5.6	5.8
V	–	–	–	–	8.9	14.4	9.8	10.7	16.2	4.8	26.3	19	-1.0	6	82	58	81	74	2.2	8.0	2.6	4.3	5.3	6.0	5.0	5.4
VI	–	–	–	–	15.9	22.0	16.2	17.6	23.7	10.2	30.3	30	5.4	27	78	58	81	72	3.9	12.2	3.6	6.6	4.0	4.4	3.6	4.0
VII	–	–	–	–	17.4	22.6	17.5	18.8	24.2	13.3	34.5	5	8.0	3	86	66	86	79	3.1	11.2	3.1	5.8	6.3	5.9	6.5	6.2
VIII	–	–	–	–	14.4	19.8	14.9	16.0	21.8	11.1	26.8	11	6.3	30	90	68	88	82	1.8	7.9	2.1	4.0	6.0	6.2	4.4	5.5
IX	–	–	–	–	9.5	15.1	10.8	11.6	16.8	7.1	27.6	9	-1.3	26	92	74	89	85	1.1	5.2	1.6	2.6	6.5	6.8	5.2	6.2
X	–	–	–	–	6.2	12.7	7.9	8.7	13.8	4.5	21.5	10	-1.0	2	93	72	90	85	0.7	4.5	1.1	2.1	6.3	5.9	4.1	5.4
XI	–	–	–	–	3.4	6.4	4.0	4.4	7.6	1.7	17.2	4	-7.9	30	91	81	90	87	0.7	2.2	0.8	1.2	7.8	7.2	8.2	7.7
XII	–	–	–	–	-2.4	-0.5	-2.0	-1.7	0.9	-5.0	6.7	13	-20.2	16	93	90	93	92	0.4	0.6	0.4	0.5	7.3	8.4	6.8	7.5
Rok	–	–	–	–	6.5	11.4	7.5	8.2	12.9	3.7	34.5	5.VII	-20.2	16.XII	-	-	-	-	-	-	-	-	6.4	6.5	5.6	6.2

Terespol n.B.

$\varphi = 52°05'$ $\lambda = 23°37'$

I	–	–	–	–	-2.5	-0.9	-1.8	-1.8	0.4	-4.2	6.0	6	-16.0	17	91	87	90	89	0.4	0.7	0.5	0.5	8.8	8.9	7.8	8.5
II	–	–	–	–	0.4	2.9	1.2	1.4	4.2	-0.7	8.5	15,18	-6.9	27	94	86	90	90	0.4	1.1	0.6	0.7	8.8	8.7	7.1	8.2
III	–	–	–	–	-2.1	3.7	0.6	0.7	5.7	-3.6	16.6	30,31	-11.5	4	84	63	78	75	0.9	3.7	1.5	2.0	5.9	5.4	4.0	5.1
IV	–	–	–	–	5.3	12.7	8.2	8.6	14.4	3.0	27.0	30	- 6.3	10	83	51	70	68	1.7	9.0	3.6	4.8	6.0	7.1	5.3	6.1
V	–	–	–	–	9.7	14.4	10.9	11.5	16.5	6.7	25.4	19	0.8	2,5	81	60	80	74	2.3	7.4	2.6	4.1	5.9	7.7	6.1	6.6
VI	–	–	–	–	16.0	22.5	16.8	18.0	24.0	11.2	33.0	12	5.9	21	76	50	74	67	4.4	14.3	5.1	7.9	4.7	5.8	4.5	5.0
VII	–	–	–	–	17.0	22.5	17.7	18.7	24.3	13.7	34.2	5	9.3	29	84	60	83	76	3.2	11.6	3.7	6.2	6.0	7.1	5.6	6.2
VIII	–	–	–	–	14.4	20.2	15.1	15.2	21.9	11.5	30.5	12	6.0	24	91	65	88	81	1.5	8.9	2.0	4.1	6.4	6.6	3.9	5.6
IX	–	–	–	–	10.0	15.3	11.1	11.9	16.5	8.3	26.9	9	1.2	27	92	67	89	83	0.9	6.3	1.5	2.9	7.7	7.5	6.8	7.3
X	–	–	–	–	5.3	11.8	7.5	8.0	13.0	4.1	19.4	19	-0.7	3	92	68	89	83	0.8	4.6	1.2	2.2	6.1	6.6	6.0	6.2
XI	–	–	–	–	2.4	5.3	3.3	3.6	6.7	1.1	15.7	1	-9.4	30	93	82	90	88	0.5	1.8	0.8	1.0	8.0	8.5	7.3	7.9
XII	–	–	–	–	-3.5	-1.5	-2.5	-2.4	0.2	-5.4	7.5	13	-17.1	16	90	84	88	87	0.5	0.9	0.6	0.7	7.2	7.3	6.7	7.1
Rok	–	–	–	–	6.0	10.8	7.3	7.8	12.3	3.8	33.0	12.VI	-17.1	16.XII	88	69	84	80	1.5	5.9	2.0	3.1	6.8	7.5	5.9	6.7

Młochów

$\varphi = 52°03'$ $\lambda = 20°47'$

I	–	–	–	–	-2.2	-0.2	-1.1	-1.2	1.1	-3.7	8.4	6	-16.8	16	89	87	89	88	0.5	0.8	0.6	0.6	9.5	9.7	7.5	8.9
II	–	–	–	–	1.5	4.2	2.6	2.7	5.7	0.3	10.2	21	-4.1	24,28	93	82	88	88	0.5	1.7	0.9	1.0	9.4	9.7	7.1	8.7
III	–	–	–	–	-0.1	5.5	2.5	2.6	7.4	-1.5	16.4	31	-8.1	4	84	60	78	74	1.1	4.4	1.8	2.4	8.6	8.3	5.5	7.5
IV	–	–	–	–	5.4	12.5	7.5	8.2	14.2	2.8	25.3	30	-5.3	10	84	50	74	69	1.8	8.6	3.0	4.5	8.9	8.7	5.9	7.8
V	–	–	–	–	9.2	13.8	9.8	10.6	15.4	5.6	25.6	19	-1.1	6	78	56	75	70	2.7	8.1	3.2	4.7	7.3	8.3	6.1	7.2
VI	–	–	–	–	16.0	21.3	16.3	17.5	23.2	11.5	30.1	11	6.8	21,27	75	51	79	68	4.7	13.1	4.0	7.3	6.2	7.1	5.6	6.3
VII	–	–	–	–	17.2	22.0	17.6	18.6	23.7	14.2	33.1	8	11.0	7,29	84	62	84	77	3.4	11.2	3.5	6.0	8.3	8.6	8.1	8.3
VIII	–	–	–	–	14.4	19.4	15.3	16.1	21.3	12.0	29.4	12	8.3	24	88	66	85	80	2.0	8.3	2.7	4.3	6.8	8.5	4.8	6.7
IX	–	–	–	–	9.8	14.8	11.5	11.9	18.4	8.3	27.9	9	0.8	27	90	68	84	81	1.3	6.1	2.4	3.3	7.6	9.0	6.2	7.6
X	–	–	–	–	6.5	12.0	8.8	9.0	13.4	5.6	20.9	19	4.2	2	91	71	85	82	1.0	4.4	1.8	2.4	8.3	8.3	6.2	7.6
XI	–	–	–	–	3.2	6.0	3.7	4.2	7.4	1.8	16.9	4	-7.9	29,30	92	80	91	88	0.6	2.0	0.8	1.1	8.7	8.2	7.5	8.1
XII	–	–	–	–	-2.4	-0.7	-1.8	-1.7	0.9	-4.2	6.4	14	-16.6	17	90	86	92	89	0.5	0.8	0.5	0.6	7.7	9.0	6.9	7.9
Rok	–	–	–	–	6.5	10.9	7.7	8.2	12.5	4.4	33.1	8.VII	-16.6	17.XII	86	68	84	79	1.7	5.8	2.1	3.2	8.1	8.6	6.5	7.7

Śrem

$H_s = 78\ m$ $h_w = 10\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °/0, °/00																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max>25°	0,1 ≤ R < 1,0	1,0 ≤ R < 10,0	10,0 ≤ R	10 > v ≥ 15	v ≥ 15	≡	≈	≋	≋	≋
I	-	-		-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.0	5.0	6	23	7	3	·	9	7	·	-	-			3	16	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	37.8	14.5	18	13	·	·	·	16	9	4	-	-	-	·		6	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.8	10.8	17	16	·	·	·	6	4	1	-	-	-	·	12	5	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.3	6.2	24	10	·	·	1	6	4	·	-	-	-	·	6	7	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.9	15.7	6	3	·	·	2	5	2	1	-	-	-	1	3	4	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.6	22.1	4	·	·	·	11	9	8	1	-	-	-	5	9	6	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	141.0	49.8	23	·	·	·	13	16	13	6	-	-	-	5	4	16	-
VIII	2	1.5	2	1.5	3.5	1.6	3	1.7	19	2.0	18	3.0	19.5	2.5	13	1.8	13	2.0	54.8	9.4	24	·	·	·	4	13	10	·	·	·	-	4	1	8	-
IX	·	·	0.5	1.0	1.5	1.0	2.5	1.4	9.5	2.3	25.5	3.0	18.5	3.7	10	2.0	22	2.1	70.2	12.0	23	2	·	·	2	17	14	1	1	·	-	1	·	9	-
X	·	·	3	1.0	1.5	1.0	4.5	1.3	17	1.8	16.5	2.4	19	2.6	2.5	1.4	29	1.4	7.2	1.8	24	2	·	·	·	7	4	·	·	·	-		4	7	-
XI	3	3.0	1.6	2.0	1.9	1.7	6	1.3	6.5	1.4	7	3.3	14.5	4.8	3	5.3	15	2.2	68	3.1	28	11	2	·	·	8	2	·	·	·	-	·	2	17	-
XII	2	1.5	7.5	2.1	6	1.4	2	2.5	14.5	1.6	24.5	2.9	11.5	4.1	6	1.8	19	2.0	26.5	8.7	8	24	9	3	·	10	6	·	1	·	-	·	1	15	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	475.9	49.8	23.VIII	104	18	6	33	122	83	11	-	-	-	16	45	116	-

Błonie - Topola

$H_s = 109\ m$ $h_w = 10\ m$

I	·	·	6	4.0	8.5	3.5	3.5	2.7	1	3.0	3.3	3.4	29.5	4.6	6.5	5.6	5	3.8	33.2	6.2	6	23	9	5	·	16	8	·	1	·	4	·	3	19	16
II	5	1.9	4.5	1.6	2	1.8	3	1.5	1.0	2.4	2.6	3.2	1.9	3.6	5.5	5.0	9	2.7	46.0	8.8	18	12	1	·	·	18	11	·	1	·	3.1	·	2	13	
III	8	2.4	7	2.3	1.6	1.7	6.5	5.7	5	1.7	1.3	1.7	1.6	7.1	12.5	4.8	9	4.4	25.7	7.9	28	19	·	·	·	7	5	·	7	2	1	·	8	8	·
IV	1.3	3.7	1.3	3.0	6.5	2.9	1.5	3.7	1	3.0	8.5	3.9	8	4.2	23.5	3.7	15	3.0	24.5	9.7	30	9	·	·	1	10	6	·	1	·	1	3	6	10	·
V	2.1	2.8	1.8	3.0	9.5	3.1	3	2.3	0.5	2.0	0.5	2.0	1.3	5.3	17.5	4.0	10	3.1	43.8	23.8	20	2	·	·	1	9	5	1	2	·	1	1	4	9	·
VI	11.5	1.7	9	2.1	10.5	1.6	3.5	2.7	2.5	2.2	1.2	3.1	16.5	3.4	15.5	2.4	9	2.2	65.1	22.2	9	·	·	·	10	10	7	2	·	·	·	6	8	4	·
VII	7.5	4.0	7	2.6	4.5	3.1	5	2.5	4	1.8	16.5	3.8	20.5	3.9	2.1	3.5	7	3.2	167.8	42.4	16	·	·	·	13	17	13	5	·	·	·	6	3	11	·
VIII	3.5	2.7	0.5	3.0	4.5	2.6	0.5	2.0	1.5	3.3	2.7.5	3.3	22.5	3.6	19.5	3.3	13	2.8	90.0	55.6	16	·	·	·	4	11	9	1	·	·	·	2	2	6	·
IX	1.5	2.0	·	·	0.5	3.0	1	2.0	3	1.8	3.5	4.4	23.5	6.3	13.5	4.0	12	4.1	70.5	11.4	23	2	·	·	2	18	12	1	6	·	1	·	2	7	·
X	3	2.0	0.5	1.0	2.5	1.4	·	·	6.5	2.1	33.5	2.5	30.5	3.0	4.5	2.0	12	2.2	8.3	4.1	20	1	·	·	·	5	3	·	·	·	1	·	4	7	·
XI	4	8.2	9.5	2.6	2.0	3.0	1.0	2.6	9.5	2.3	14.6	5.4	11	8.8	1.5	9.3	1.0	3.9	20.1	5.3	27	10	3	·	·	8	5	·	6	·	3	·	2	18	·
XII	7	2.4	5.5	3.8	5	2.4	2	2.2	3.5	1.9	3.2.5	4.3	17.5	5.1	7	5.1	13	3.5	40.0	20.4	14	2.5	9	5	·	12	7	1	2	1	3	·	1	16	8
Rok	8.5	2.8	80.5	2.4	90	2.8	39.5	2.5	48	2.5	2.82.5	3.7	227.8	4.9	14.8	4.4	124	3.2	635.0	55.6	16.VII	103	22	10	31	141	91	11	26	3	24.8	18	45	128	24

Terespol n. B.

$H_s = 143\ m$ $h_w = 10\ m$

I	1.5	2.0	4.5	3.9	5.5	5.0	1.0	4.2	13.5	2.4	1.5	3.0	24.5	3.7	13.5	4.6	·	3.7	19.6	7.3	6	26	13	5	·	11	6	·			·	·	·	2.2	23
II	6	4.5	5	3.4	5.5	2.0	9	2.8	16.5	2.8	1.4	2.8	1.7	3.1	11	2.8	·	3.0	36.8	6.5	22	13	2	·	·	19	11	·	·	·	4	·	1	17	4
III	24.5	4.1	8.5	3.0	7.5	3.7	11.5	6.0	7.5	2.7	6.5	2.2	10.5	3.7	17.5	3.6	2	3.7	18.3	9.8	15	23	7	2	·	6	4	·	4	1	·	·	6	8	4
IV	22.6	2.4	1.1	2.4	1.3	1.8	5.5	2.0	12.5	2.5	4.5	2.1	2.5	2.3	13.5	3.1	5	2.3	17.5	8.0	30	6	·	·	4	8	5	·	·	·	1	2	5	12	·
V	25.5	3.0	1.9	2.6	7.5	2.6	5	3.0	2.5	3.8	6	1.7	6	2.5	17.5	3.1	4	2.7	53.7	20.1	9	·	·	·	1	12	8	2	·	·	·	3	4	12	·
VI	1.9	1.9	3.5	2.3	2	2.0	8.5	2.8	10.5	1.9	3.5	1.7	1.5	2.6	2.7	2.9	1	2.4	60.6	35.7	24	·	·	·	10	9	4	2	·	·	·	4	5	5	·
VII	8.5	1.5	4	1.8	1.2	2.8	8.5	1.6	8	2.2	1.0	2.0	13.5	2.7	22.5	2.5	6	2.1	68.1	17.5	9	·	·	·	13	18	9	3	·	·	1	5	2	8	·
VIII	8.5	1.8	6	1.3	2	2.0	9.5	3.0	5.5	1.7	1.1	2.2	19.5	2.7	2.9	2.7	2	2.4	124.1	32.0	29	·	·	·	4	17	12	3	·	·	2	4	1	5	
IX	1.2	1.5	1.5	1.0	2	3.0	4	2.5	1.2	2.9	1.3	2.9	2.3	5.5	20.5	3.0	2	3.3	93.5	24.1	23	·	·	·	1	13	10	3	2	1	2	1	2	1.7	
X	5	2.6	3	1.0	0.5	3.0	6	2.2	1.3	1.9	2.2.5	2.0	2.3	3.1	1.7	2.5	3	2.3	8.3	4.6	23	1	·	·	·	8	2	·	·	·	1	·	3	9	
XI	10.5	5.0	12.5	3.4	1.4	2.5	16.5	3.4	8	2.1	7.5	2.3	9	4.1	12	3.7	·	3.4	23.3	10.4	28	11	1	·	·	6	4	1	2	·	1	·	1	19	
XII	1.3	2.6	1.2	2.4	6.5	2.0	4	2.2	1.4	2.5	2.3.5	3.9	1.3	4.7	5	4.4	2	3.2	22.3	6.1	14	2.5	1.3	5	·	12	6	·	1	·	2	·	5	18	18
Rok	153.5	2.7	90.5	2.4	78	2.7	98	3.0	123.5	2.4	43.7	2.4	176.5	3.4	2.1.1	3.2	2.7	2.9	543.1	35.7	24.VI	105	36	12	33	139	81	14	9	2	14	19	35	152	49

Młochów

$H_s = 141\ m$ $h_w = 12{,}5\ m$

I	1	2.0	3.5	6.1	8.5	3.1	5	3.8	13.5	3.5	2.7.5	6.2	2.3.5	6.8	3.6	8.0	2	5.2	19.3	4.2	6	24	11	4	·	9	6	·	3	·	-	·	·	23	-
II	4.5	4.8	3	3.6	3	2.5	7.5	3.3	23.5	4.0	19.5	4.7	11	7.5	3	7.5	9	4.2	26.7	8.1	18	10	2	·	·	17	8	·	1	·	2	·	·	18	-
III	5.5	7.4	8	4.1	18.5	5.5	8.5	3.6	7.5	2.9	16	5.1	10.5	8.9	7.5	2.1	11	4.9	26.5	12.0	15	17	4	·	·	7	4	1	6	1	·	·	1	16	-
IV	8	3.6	8	4.1	4.5	5.3	10.5	2.9	7	3.8	9.5	5.1	15.5	3.1	12	4.0	15	3.2	17.8	6.8	29	8	·	·	2	8	5	·	1	·	·	3	·	12	-
V	12	4.3	9.5	3.3	8.5	3.5	7	2.1	6	2.2	8.5	5.0	6	5.3	17.5	4.4	18	3.1	35.4	21.0	9	2	·	·	1	5	3	1	·	·	1	1	1	11	-
VI	5.5	3.2	6.5	2.4	6.5	1.6	7	3.1	6	3.5	17	4.4	14.5	4.3	10	3.9	17	3.1	37.8	13.5	4	·	·	·	8	11	6	2	2	·	·	5	4	12	-
VII	3.5	2.6	4.5	2.8	5	2.5	7	3.2	15.5	3.0	24.5	3.6	15	4.4	11	4.0	7	3.3	49.2.8	44.3	12	·	·	·	10	18	16	8	·	·	1	10	·	21	-
VIII	0.5	3.0	0.5	1.0	4.5	3.0	6.5	2.9	12	3.2	28.5	4.3	23.5	4.2	8	4.2	9	3.5	74.1	14.2	10	·	·	·	6	16	12	3	·	·	·	5	·	7	-
IX	4	3.2	·	·	·	·	2.5	3.0	20	4.2	34.5	5.3	20	7.4	4	6.6	8	4.8	79.0	15.0	24	·	·	·	2	19	14	2	3	·	·	1	·	13	-
X	·	·	·	·	·	·	1.0	3.6	23.5	3.8	4.1	4.7	1.0	6.3	2.5	3.8	6	4.2	4.8	4.7	20	·	·	·	·	5	2	·	1	·	2	·	·	14	-
XI	4	8.9	8.5	3.5	14.5	3.6	14	3.3	14	3.3	6.5	4.5	13.6	9.0	2	14.2	4.4	4.4	43.1	6.3	28	12	1	·	·	10	4	·	6	1	3	·	2	19	-
XII	7	2.7	2	2.2	5	3.4	7.5	2.7	16.5	3.1	2.9.3	6.7	2.5	6.2	4	6.0	13	4.5	35.0	17.0	14	2.4	9	3	·	13	5	1	5	1	1	·	2	17	-
Rok	58.5	3.8	54	2.8	78.5	2.8	93	3.1	17.0	3.4	2.58.5	5.2	17.4.5	6.1	2.3	6.2	129	4.0	553.0	44.3	12.VII	97	27	7	29	136	85	18	28	3	-	25	10	183	-

Biała Podlaska

$\varphi = 52°01'$ $\lambda = 23°08'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1002.3	1012.9	987.1	1024.0	-2.7	-0.7	-4.7	-4.7	0.5	-4.2	6.8	6	-16.9	17	93	88	93	91	0.3	0.7	0.4	0.5	8.5	9.0	7.8	8.4
II	993.8	1011.9	970.2	1014.1	0.6	3.2	1.6	1.8	4.5	-0.7	9.1	15	-5.7	27	95	88	93	92	0.3	1.1	0.5	0.6	8.7	9.1	7.5	8.4
III	1004.0	1016.4	975.5	1019.4	-2.0	4.3	0.8	1.0	6.1	-3.8	17.3	30,31	-13.5	4	88	64	80	77	0.7	3.7	1.4	1.9	5.2	6.2	4.3	5.2
IV	999.8	1011.9	975.7	1017.7	5.1	13.1	7.7	8.4	14.6	2.1	26.9	30	-7.5	10	88	55	76	73	1.2	8.6	2.7	4.2	5.8	6.2	4.5	5.5
V	997.5	1008.1	984.2	1015.1	9.6	14.4	10.5	11.2	15.9	6.1	25.4	19	-0.1	6	84	62	83	76	2.0	7.2	2.3	3.8	6.0	7.5	6.1	6.5
VI	998.6	1009.0	986.0	1016.0	16.0	22.5	16.8	18.0	24.0	11.0	31.7	12	5.9	7	78	50	75	68	4.0	14.3	4.8	7.7	5.5	6.4	5.1	5.7
VII	994.3	1004.2	985.1	1011.5	16.9	22.8	17.8	18.8	24.5	13.6	31.7	5	9.2	29	85	60	84	76	2.9	12.0	3.5	6.1	6.9	7.0	6.3	6.7
VIII	996.2	1004.4	985.1	1013.5	14.3	20.1	15.3	16.2	21.8	11.7	30.3	12	4.8	24	91	65	87	81	1.5	9.0	2.3	4.3	6.7	6.6	4.6	6.0
IX	994.5	1006.0	980.8	1012.1	9.8	15.1	10.9	11.7	16.5	7.8	27.1	9	1.2	27	92	66	88	82	1.0	6.3	1.5	2.9	7.6	7.0	6.5	7.0
X	1001.9	1014.6	989.2	1019.8	5.5	11.8	7.5	8.1	13.0	3.9	19.8	19	-1.5	3	90	69	89	83	0.9	4.6	1.3	2.3	6.7	6.6	5.9	6.4
XI	1003.0	1023.8	979.8	1021.4	2.4	5.5	3.1	3.5	6.9	0.7	15.7	2	-9.6	30	93	82	90	88	0.5	1.8	0.7	1.0	8.0	8.8	7.8	8.2
XII	997.0	1014.9	958.1	1015.5	-3.4	-1.0	-2.5	-2.4	0.4	-5.5	7.2	13	-17.8	16	90	82	88	87	0.5	1.0	0.6	0.7	7.8	7.8	7.0	7.5
Rok	998.3	1023.8	958.1	1016.2	6.0	10.9	7.3	7.9	12.4	3.6	31.7	12VI, 5VII	-17.8	16.XII	89	69	86	81	1.3	5.9	1.8	3.0	7.0	7.4	6.1	6.8

Głowno

$\varphi = 51°58'$ $\lambda = 19°42'$

I	-	-	-	-	-1.7	0.6	-1.0	-0.8	1.6	-	8.5	6	-	-	-	-	-	-	-	-	-	-	9.2	8.0	8.8	8.7
II	-	-	-	-	2.1	5.1	2.8	3.2	6.0	-	10.4	14	-	-	-	-	-	-	-	-	-	-	8.6	6.9	8.8	8.0
III	-	-	-	-	1.1	7.0	2.7	3.4	8.3	-	16.3	27	-	-	-	-	-	-	-	-	-	-	6.2	5.9	6.8	6.3
IV	-	-	-	-	5.0	12.8	7.1	8.0	13.9	-	26.9	30	-	-	-	-	-	-	-	-	-	-	6.4	4.9	7.2	6.2
V	-	-	-	-	8.9	15.0	9.5	10.7	16.2	-	26.9	19	-	-	-	-	-	-	-	-	-	-	6.4	6.4	6.7	6.5
VI	-	-	-	-	15.5	22.1	16.5	17.6	23.8	-	30.4	30	-	-	-	-	-	-	-	-	-	-	4.4	4.3	4.3	4.3
VII	-	-	-	-	17.1	22.8	17.8	18.9	24.1	-	34.9	8	-	-	-	-	-	-	-	-	-	-	5.8	6.2	8.1	6.7
VIII	-	-	-	-	13.6	20.5	15.2	16.1	24.0	-	26.9	11	-	-	-	-	-	-	-	-	-	-	6.2	6.1	6.9	6.4
IX	-	-	-	-	9.5	15.4	11.0	11.7	16.7	-	28.3	9	-	-	-	-	-	-	-	-	-	-	6.2	7.7	7.6	7.2
X	-	-	-	-	7.3	12.9	8.5	9.3	13.9	-	21.7	19	-	-	-	-	-	-	-	-	-	-	6.4	6.1	6.8	6.4
XI	-	-	-	-	3.5	6.5	4.1	4.6	7.6	-	17.9	4	-	-	-	-	-	-	-	-	-	-	8.2	6.9	8.7	7.9
XII	-	-	-	-	-2.0	-0.1	-1.4	-1.2	0.8	-	6.4	13	-	-	-	-	-	-	-	-	-	-	8.5	8.0	8.2	8.2
Rok	-	-	-	-	6.7	11.7	7.7	8.4	12.9	-	34.9	8.VII	-	-	-	-	-	-	-	-	-	-	6.9	6.4	7.4	6.9

Skierniewice

$\varphi = 51°58'$ $\lambda = 20°09'$

I	1005.2	1016.6	987.5	1021.6	-2.3	0.0	-1.2	-1.2	1.0	-3.9	8.3	6	-16.4	17	89	86	90	88	0.5	0.9	0.6	0.7	8.0	8.1	7.2	7.8
II	995.8	1017.2	974.1	1011.8	1.6	4.6	2.6	2.8	5.6	0.3	9.3	6	-5.1	24	91	78	88	86	0.6	1.9	0.9	1.1	8.3	7.6	7.1	7.7
III	1003.3	1019.0	982.8	1019.5	0.2	5.9	2.7	2.9	7.5	-1.2	15.9	31	-7.0	4,9	85	63	77	75	1.0	4.2	1.8	2.3	5.4	5.7	5.9	5.0
IV	1002.6	1015.0	978.9	1018.5	4.9	12.4	7.5	8.1	13.7	2.8	25.8	30	-4.0	10	87	50	76	71	1.3	8.7	2.7	4.2	5.8	6.4	4.4	5.5
V	1000.7	1011.5	990.9	1016.4	9.0	14.1	10.0	10.8	15.5	5.5	26.0	19	-0.8	6	79	54	78	70	2.5	8.5	2.8	4.6	6.3	7.1	5.5	6.3
VI	1001.4	1012.0	990.1	1016.7	16.1	21.3	16.6	17.6	23.0	11.0	29.6	30	6.2	28	75	52	77	68	4.7	12.9	4.5	7.4	4.6	5.6	3.8	4.7
VII	996.9	1007.9	985.0	1012.0	17.3	21.9	17.6	18.6	23.5	14.0	34.2	8	9.3	29	83	64	85	77	3.6	11.4	3.3	6.1	6.7	7.0	6.3	6.7
VIII	999.1	1008.5	986.9	1014.5	14.4	19.7	15.3	16.2	21.4	11.7	27.2	12	6.8	24	87	61	85	78	2.2	9.5	2.7	4.8	6.3	7.0	3.6	5.6
IX	997.6	1007.5	984.5	1013.2	9.5	15.0	11.1	11.7	16.2	8.0	27.6	9	0.7	27	91	65	86	81	1.1	6.7	2.0	3.3	6.2	7.8	5.6	6.5
X	1004.3	1015.1	983.7	1020.2	6.2	12.0	8.4	8.8	13.1	5.0	20.7	19	0.4	2	92	71	87	83	0.8	4.4	1.4	2.2	6.5	7.2	5.4	6.4
XI	1005.5	1024.7	989.0	1021.6	3.4	6.2	3.9	4.4	7.2	1.6	16.5	6	-8.1	30	90	77	89	85	0.7	2.3	0.9	1.3	8.2	7.1	7.2	7.5
XII	999.4	1017.7	953.7	1015.7	-2.3	-0.4	-1.6	-1.4	0.8	-4.6	6.7	9	-21.6	16	88	84	88	87	0.6	1.0	0.7	0.8	8.4	8.1	6.9	7.8
Rok	1001.0	1024.7	953.7	1016.8	6.5	11.1	7.8	8.3	12.4	4.2	34.2	8.VII	-21.6	16.XII	86	67	84	79	1.6	6.0	2.0	3.2	6.7	7.1	5.6	6.5

Zielona Góra I

$\varphi = 51°56'$ $\lambda = 15°30'$

I	1000.0	1012.2	984.7	1022.1	-1.3	0.9	-0.4	-0.3	2.1	-3.0	11.0	6	-15.4	16	92	86	90	89	0.5	1.0	0.6	0.7	7.6	8.0	6.5	7.4
II	989.4	1014.8	962.9	1011.1	1.7	4.9	2.6	3.0	6.2	0.4	12.6	5	-4.3	26	94	81	91	89	0.4	1.8	0.7	1.0	7.7	8.5	5.9	7.4
III	996.7	1016.4	975.7	1018.3	4.9	7.7	4.8	4.8	9.7	1.0	18.7	13,26	-5.4	2	84	63	74	74	1.2	4.4	2.4	2.7	5.7	5.8	3.9	5.1
IV	998.0	1010.1	976.2	1019.4	5.1	11.9	7.7	8.1	13.7	3.3	23.7	28	-4.0	14	89	58	75	74	1.1	6.5	2.9	3.5	4.4	5.4	3.9	4.6
V	996.2	1007.8	986.4	1017.2	8.4	14.1	10.0	10.6	16.1	5.5	26.0	16	-0.3	7	80	56	74	70	2.4	7.9	3.5	4.6	5.5	6.5	4.5	5.5
VI	996.4	1012.7	984.7	1016.9	15.4	21.6	17.4	18.0	23.7	12.5	31.8	11	3.7	14	77	54	70	67	4.5	13.4	6.6	8.2	4.8	5.2	3.6	4.5
VII	992.3	1005.2	982.0	1012.7	16.8	21.5	18.6	18.9	23.5	14.9	33.2	4	10.9	28	86	67	80	78	3.0	10.2	5.1	6.1	6.1	6.4	6.7	6.4
VIII	994.1	1004.7	980.9	1014.6	13.6	18.6	15.2	15.6	20.6	11.9	27.8	11	7.7	25	88	65	80	78	2.0	8.2	3.9	4.7	6.1	6.9	4.6	5.9
IX	992.5	1004.0	973.8	1013.5	9.8	14.8	11.3	11.8	16.4	8.3	28.1	8	1.4	27	94	70	85	82	1.2	5.5	2.2	3.0	7.3	7.2	5.4	6.6
X	998.4	1008.0	984.6	1019.6	7.3	12.6	9.1	9.5	13.8	6.1	20.5	19	0.9	3	93	70	86	83	0.7	4.5	1.7	2.3	7.7	6.2	3.5	5.8
XI	999.5	1016.4	982.2	1014.2	3.4	5.8	4.1	4.4	7.1	2.3	15.5	5	-7.5	30	92	82	90	88	0.6	1.8	0.8	1.1	7.4	8.4	7.6	7.8
XII	993.8	1012.3	958.8	1015.8	-1.6	0.2	-0.9	-0.8	1.7	-3.0	10.1	8	-15.0	17	92	86	91	90	0.4	0.8	0.6	0.6	7.7	7.8	6.1	7.2
Rok	995.6	1016.4	958.8	1016.8	6.7	11.2	8.3	8.6	12.9	5.0	33.2	4.VIII	-15.4	16.1	88	70	82	80	1.5	5.5	2.6	3.2	6.5	6.9	5.2	6.2

Biała Podlaska

$H_s = 146\ m$ $H_b = 146{,}7\ m$ $h_w = 12\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D,°mD																	OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość																			
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0,1	1,0	10,0	Wiatr v 10	15	=	≥ 20 m	◔	●	■
I	4	2,2	3,5	5,0	6	6,0	6,5	5,1	13,5	3,8	2,6	4,1	28,5	4,9	7	8,9	2	4,6	26,9	9,8	6	25	11	6	·	12	6	·	1	·	4	·	·	21	24
II	3	4,5	2,5	3,2	0,5	1,0	4	3,1	2,4	4,4	3,0	3,2	1,4	5,0	4	3,9	2	3,8	46,5	7,6	16	15	2	·	·	20	14	·	·	·	4	·	·	19	7
III	7	4,3	4,5	4,3	9,5	6,1	3,1	5,5	11,5	4,1	17,5	3,8	18,5	4,4	7,5	4,9	6	4,3	48,5	8,7	15	25	7	3	·	6	4	·	2	·	·	·	6	7	7
IV	5	3,7	2,5	2,5	4,5	2,3	15,5	3,0	14,5	2,2	1,2	2,7	9	3,6	7	3,3	20	2,2	15,5	6,4	30	7	·	·	4	6	3	·	·	·	·	1	5	7	·
V	4	4,4	5	3,7	8,5	4,0	15,5	3,0	9,5	2,0	1,7	3,0	1,4	3,9	8,5	4,2	11	3,0	30,5	12,6	9	1	·	·	2	11	6	1	·	·	·	4	4	13	·
VI	2,5	3,8	·	·	1	3,0	1,4	3,3	2,3	2,9	2,9	3,6	7,5	4,5	5	3,6	8	3,1	53,7	21,3	24	·	·	·	11	6	5	3	·	·	·	3	4	5	·
VII	1	2,0	·	·	6	5,0	2,2,5	3,1	2,2	2,2	2,5,5	4,2	3	3,0	·	·	13	2,9	80,9	15,7	9	·	·	·	14	20	15	1	1	·	2	13	2	14	·
VIII	·	·	·	·	2	7,0	1,4,5	3,3	2,5,5	2,6	3,2,5	3,6	4,5	4,0	1	1,5	13	2,9	166,6	54,5	29	·	·	·	5	15	14	3	·	·	2	7	1	6	·
IX	·	·	1	2,0	1	3,0	12	2,8	2,9	2,8	3,6	4,9	1	6,8	1	3,0	6	3,6	84,7	18,5	23	·	·	·	1	14	11	2	1	·	2	2	2	11	·
X	·	·	·	·	1	2,0	11,5	3,0	3,6	2,7	3,2,5	3,8	2,5	4,4	0,5	3,0	9	2,9	12,6	7,3	23	2	·	·	·	9	3	·	·	·	3	·	1	11	·
XI	1,5	1,1,0	3,5	4,7	7,5	4,8	2,8	4,0	1,5	2,2	1,8,5	5,1	3,5	8,0	4,5	7,2	8	4,1	25,2	9,5	28	11	1	·	·	10	6	·	2	·	3	·	1	22	1
XII	3,5	3,3	1,0	2,2	3,5	4,6	9,5	2,3	2,4	4,6	2,2,5	5,1	4	6,0	4	4,8	6	4,0	24,8	7,7	14	26	13	5	·	11	7	·	3	1	5	·	1	18	20
Rok	2,5,5	3,2	2,9,5	2,3	5,1	4,1	1,6,4,5	3,5	2,4,9,5	3,1	3,0,5	3,9	1,1,3	4,9	5,0	3,9	1,0,4	3,4	5,8,6,8	5,4,5	29.VIII	1,1,2	3,4	1,4	3,7	1,4,0	9,4	1,0	1,0	1	2,5	3,0	2,7	4,5,4	5,9

Głowno

$H_s = 133\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26,0	6,0	12	-	8	-	·	11	5	·	-	-	-	·	·	23	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55,5	14,4	18	-	2	-	·	13	9	1	-	-	-	·	·	16	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22,7	9,8	15	-	1	-	·	5	4	·	-	-	-	·	3	12	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22,9	14,8	30	-	·	-	2	10	5	1	-	-	-	1	6	12	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25,6	10,8	9	-	·	-	2	6	4	1	-	-	-	1	3	11	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	64,1	25,0	4	-	·	-	11	7	6	3	-	-	-	3	10	6	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	228,6	76,2	16	-	·	-	13	19	15	5	-	-	-	5	3	14	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	51,7	15,9	16	-	·	-	6	14	9	2	-	-	-	2	1	9	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	90,1	17,7	24	-	·	-	2	22	12	2	-	-	-	·	1	12	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7,6	4,2	20	-	·	-	·	8	3	·	-	-	-	·	4	9	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27,2	8,1	28	-	2	-	·	9	6	·	-	-	-	·	2	18	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54,4	25,0	14	-	8	-	·	11	8	1	-	-	-	·	·	21	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	673,4	76,2	16.VII	-	21	-	36	135	86	16	-	-	-	12	33	163	-

Skierniewice

$H_s = 129\ m$ $H_b = 129{,}0$ $h_w = 8{,}5\ m$

I	1,5	2,6	6	4,0	2	5,0	7	3,7	14,5	3,1	2,7	3,6	2,8	4,3	5	5,1	2	3,9	17,9	4,8	31	2,5	1,0	4	·	8	5	·	3	·	9	·	4	19	19
II	7,5	2,3	3,5	2,0	3,5	3,6	8	4,1	14,5	3,8	2,4,5	3,2	1,6	4,1	5,5	3,8	1	3,4	42,0	7,8	8	1,0	1	·	·	18	12	·	·	·	3	·	·	14	2
III	5	3,4	1,0,5	4,1	4,3,5	5,3	12	6,0	1,0	3,8	8	3,6	1,7	4,8	1,0	4,6	7	4,3	19,8	7,2	15	1,9	4	·	·	8	5	·	4	2	3	·	7	7	·
IV	1,0,5	3,8	8,5	2,8	1,1	3,5	4,5	2,2	9,5	4,4	4,5	3,0	9	3,0	2,0,5	3,3	1,2	2,9	17,7	9,7	30	8	·	·	1	1,0	4	·	3	·	8	1	6	7	·
V	9,5	3,7	1,3	3,5	6,5	2,8	1,2	3,2	5,5	2,1	4	2,0	1,6	3,2	2,0,5	3,0	6	2,9	26,0	10,2	10	1	·	·	2	5	4	1	·	·	1	2	3	11	·
VI	6,5	3,8	1,1	2,5	6,5	2,3	8	2,4	3,5	3,4	1,1,5	3,9	2,3	3,2	1,3	3,7	7	2,9	60,2	25,7	4	·	·	·	8	1,0	6	2	·	·	3	5	7	6	·
VII	5	1,5	8,5	1,8	7,5	2,9	4	2,6	9	2,8	1,4	2,5	2,4,5	2,9	1,7,5	2,8	3	2,5	1,1,7,4	2,9,2	1,6	·	·	·	1,2	1,7	1,4	4	·	·	1	6	3	1,1	·
VIII	3	2,3	2,5	2,2	2	4,7	4,5	3,9	9	2,7	1,6	3,2	3,8	2,9	1,0	2,8	8	2,7	32,8	9,5	1,0	·	·	·	5	1,3	8	·	·	·	-	3	1	4	·
IX	1,5	2,0	0,5	3,0	0,5	3,0	2	3,8	4,5	3,4	3,1,5	3,8	3,1	5,0	7	3,6	1	4,0	7,4,5	1,7,0	2,4	·	·	·	2	1,9	1,6	1	3	·	2	·	2	1,0	·
X	0,5	1,0	·	·	1,5	1,3	1,1	3,1	1,9,5	3,2	3,3,5	3,4	1,9	4,4	7	4,4	1	3,5	5,6	2,5	2,0	·	·	·	·	5	3	·	1	1	1,0	·	3	1,0	·
XI	7	7,1	9	5,6	1,9	4,6	1,7,5	4,1	1,0,5	2,7	0,5	3,3	1,5,5	7,7	2	8,2	1	5,0	7,5	2,5	2,8	1,2	3	·	·	6	3	·	8	·	3	·	3	1,8	·
XII	2,5	3,6	3,5	2,4	5,5	3,2	9	3,8	1,2	3,9	2,8	5,9	2,1,5	3,6	5	3,8	6	4,0	3,2,6	1,2,4	14	2,5	9	3	·	1,2	9	1	3	·	6	·	1	2,0	1,2
Rok	6,0	3,1	7,6,5	2,6	7,9	3,5	9,9,5	3,6	1,3,2,5	3,3	2,1,1	3,4	2,5,8,5	4,1	1,2,3	4,1	5,5	3,5	4,5,4,0	2,9,2	1,6.VII	1,0,0	2,7	7	3,0	1,3,1	8,9	9	2,5	3	-	1,7	4,0	1,3,7	3,5

Zielona Góra I

$H_s = 176\ m$ $H_b = 174{,}0$ $h_w = \frac{I-V}{VI-XII}\ \frac{9\ m}{16\ m}$

I	2	1,2	3	2,3	1,5	1,7	4	2,1	1,7,5	2,4	2,3	3,3	2,7	3,4	5	4,6	5	2,8	2,9,0	6,6	6	2,2	8	3	·	1,7	1,1	·	·	·	1,0	·	4	1,7	1,9
II	·	·	2,5	1,8	9,5	2,0	6	2,2	2,3,5	2,9	2,2,5	2,8	1,4	2,6	2	3,2	4	2,5	4,5,7	6,6	2,7	1,2	·	·	·	2,0	1,7	·	·	·	8	·	·	1,0	3
III	4,5	1,3	5	3,1	1,3	4,4	1,9	3,4	9,5	2,6	1,2	2,1	1,5,5	4,4	8,5	1,7	6	3,0	5,0,3	1,1,7	1,7	1,3	·	·	·	9	6	3	2	·	5	·	7	8	3
IV	1,9,5	1,7	6	1,4	1,2	1,7	8,5	1,5	4,5	1,7	3,5	1,7	1,0	2,4	2,1	2,0	8	1,6	2,7,8	1,0,6	2,5	5	·	·	·	9	6	1	·	·	4	2	8	5	·
V	1,0	1,7	1,5	2,0	5	1,3	7	2,1	6,5	1,9	4	1,8	1,5,5	2,7	1,6	2,5	1,4	1,8	4,5,4	1,4,9	1,6	1	·	·	2	1,0	7	2	·	·	4	3	3	6	·
VI	3	1,8	4,5	2,3	1,6,5	2,8	8	2,1	5	3,1	8	3,9	1,9	3,3	1,8	2,0	8	2,5	5,4,1	1,7,9	2,3	·	·	·	1,2	1,0	9	2	·	·	3	8	7	5	·
VII	8	1,8	3,5	1,9	9	2,2	7,5	2,5	4	2,2	1,4	2,5	2,6	2,7	1,4	2,5	7	2,2	2,0,8,0	6,1,7	1,1	·	·	·	1,0	1,8	1,5	5	·	·	5	8	6	1,4	·
VIII	3,5	1,1	2	1,0	1,5	2,0	9,5	2,3	9,5	2,8	2,7	3,5	2,6	2,2	1,3	2,3	1	2,6	7,4,0	1,2,5	2,4	·	·	·	2	1,7	1,4	2	1	1	3	9	·	5	·
IX	1	1,0	·	·	3	2,0	2,5	1,4	1,3	2,8	2,7,5	3,8	2,9	4,3	6	2,1	8	3,2	1,0,8,1	2,4,8	2,3	·	·	·	1	1,7	1,6	2	3	·	5	2	2	9	·
X	0,5	1,0	·	·	2	1,8	6,5	1,7	1,6	2,3	3,6	3,3	1,7,5	3,1	7,5	1,9	7	2,6	1,8,7	4,2	1,9	·	·	·	·	1,1	4	·	1	·	1,0	·	2	7	·
XI	3	4,5	8	2,8	2,1,5	2,8	1,4,5	2,3	8	2,5	1,3	2,7	1,7	5,9	3	4,2	2	3,3	1,1,2	1,9	2,8	1,1	2	·	·	1,2	5	·	·	·	1,2	·	3	1,8	·
XII	4	1,1	5	2,9	6	3,1	1,0	2,7	1,5	3,0	2,6	4,3	1,8,5	4,6	9,5	2,4	1	3,5	6,4,1	1,3,0	1,4	2,4	6	3	·	1,7	9	2	4	·	1,4	·	2	1,6	1,4
Rok	5,9	1,5	5,9,5	4,8	1,0,0,5	2,3	1,0,3	2,2	1,2,7	2,5	2,1,6,5	3,0	2,3,5	3,5	1,2,3,5	2,6	7,4	2,6	7,2,0,4	6,1,7	1,1.VII	8,8	1,6	6	2,7	1,6,7	1,1,9	1,9	1,1	1	8,3	3,2	4,4	1,2,0	3,9

Zielona Góra II

$\varphi = 51°56'$ $\lambda = 15°30'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	13.8	18.9	15.0	15.7	20.8	11.8	28.0	11	7.8	25	88	65	84	78	2.0	8.2	3.5	4.6	–	–	–	–
IX	–	–	–	–	9.9	14.9	11.1	11.8	16.4	8.0	28.0	8	0.2	27	90	70	87	82	1.2	5.6	1.9	2.9	–	–	–	–
X	–	–	–	–	7.4	12.7	9.1	9.6	13.7	5.8	20.4	19	-0.2	2	93	71	86	83	0.8	4.4	1.7	2.3	–	–	–	–
XI	–	–	–	–	3.5	5.7	4.2	4.4	–	2.1	–	–	-8.0	30	91	82	89	87	0.7	1.9	0.9	1.2	–	–	–	–
XII	–	–	–	–	-1.5	0.5	-0.8	-0.6	–	-3.2	–	–	-16.1	17	91	86	91	89	0.4	0.9	0.6	0.6	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lućmierz

$\varphi = 51°54'$ $\lambda = 19°23'$

I	–	–	–	–	-2.1	0.1	-1.3	-1.2	–	-3.5	–	–	-16.5	17	92	88	89	90	0.5	0.8	0.6	0.6	8.5	7.1	7.2	7.6
II	–	–	–	–	1.5	4.5	2.6	2.8	–	0.5	–	–	-3.4	24	91	80	90	87	0.5	1.8	0.8	1.1	7.3	7.3	6.9	7.2
III	–	–	–	–	1.0	6.7	2.9	3.4	–	-0.7	–	–	-6.5	4	82	64	79	75	1.3	3.8	1.8	2.3	5.0	6.3	4.1	4.8
IV	–	–	–	–	5.2	12.0	6.5	7.6	–	2.5	–	–	-4.2	14	84	55	78	72	1.6	7.7	2.2	3.8	5.4	6.1	5.8	5.8
V	–	–	–	–	9.2	14.3	8.9	10.3	–	5.2	–	–	(-0.2)	28?	78	55	81	71	2.7	8.5	2.4	4.5	5.2	6.0	4.2	5.1
VI	–	–	–	–	16.1	21.4	16.0	17.4	24.0	11.2	30.3	11	6.5	1	76	55	79	70	4.7	12.5	4.0	7.1	3.5	4.3	4.1	4.0
VII	–	–	–	–	17.3	22.1	17.0	18.4	24.1	14.0	34.8	8	9.8	29	83	64	86	78	3.9	11.2	2.9	5.0	6.0	6.1	6.4	6.2
VIII	–	–	–	–	14.5	19.5	14.8	15.9	21.8	11.7	26.7	11,15	7.5	31	86	65	86	79	2.4	8.4	2.5	4.4	5.8	6.8	4.1	5.6
IX	–	–	–	–	9.6	14.8	11.1	11.8	16.3	7.7	27.5	9	-0.1	27	89	70	87	82	1.3	5.9	1.8	3.0	5.3	6.7	5.5	5.8
X	–	–	–	–	6.7	12.3	8.1	8.8	13.5	5.3	21.0	19	0.2	3	91	71	89	84	1.0	4.6	1.3	2.3	5.5	6.2	4.0	5.2
XI	–	–	–	–	3.4	6.0	3.9	4.3	7.3	2.0	17.5	4	-8.1	30	90	81	88	86	0.8	2.2	1.0	1.3	7.5	6.7	7.6	7.3
XII	–	–	–	–	-2.3	-0.6	-1.6	-1.5	0.8	-4.2	7.2	14	-18.5	17	91	87	91	90	0.4	0.8	0.5	0.6	7.3	8.1	7.0	7.5
Rok	–	–	–	–	6.7	11.1	7.4	8.2	–	4.3	–	–	-18.5	17.XII	86	70	85	80	1.8	5.7	1.8	3.1	6.0	6.4	5.6	6.0

Leszno – Antoniny

$\varphi = 51°51'$ $\lambda = 16°35'$

I	–	–	–	–	-1.1	1.2	-0.4	-0.2	2.4	-2.8	10.2	6	-14.8	17	88	86	91	88	0.6	1.0	0.5	0.7	9.0	8.5	6.5	8.0
II	–	–	–	–	1.8	5.6	2.9	3.3	6.6	0.5	11.1	5	-3.8	27	92	76	92	87	0.6	2.3	0.6	1.2	7.8	6.9	6.1	6.9
III	–	–	–	–	1.8	7.7	4.1	4.4	9.5	0.3	16.9	13	-6.0	10	86	64	81	77	1.0	4.5	1.8	2.4	6.6	4.1	2.9	4.5
IV	–	–	–	–	4.9	11.8	6.3	7.3	13.6	1.7	23.8	28	-5.5	13	–	–	–	–	–	–	–	–	6.4	4.6	3.0	4.7
V	–	–	–	–	9.2	14.6	9.9	10.9	16.3	5.2	26.1	19	-0.9	7	76	50	74	67	3.0	9.2	3.6	5.3	4.6	5.4	3.8	4.6
VI	–	–	–	–	15.7	21.4	16.9	17.7	23.4	10.8	31.1	11	5.1	2,15	76	52	76	68	4.5	13.3	4.9	7.6	4.5	4.7	3.2	4.1
VII	–	–	–	–	17.4	21.9	18.1	18.9	23.9	14.6	33.3	5	9.5	3	83	65	84	77	3.7	10.7	3.8	6.1	6.0	6.5	5.5	6.0
VIII	–	–	–	–	14.2	19.5	15.8	16.3	21.3	11.9	28.2	11	7.1	23	89	63	83	78	1.9	8.8	3.4	4.7	6.5	6.9	4.2	5.9
IX	–	–	–	–	10.1	15.1	11.5	12.0	16.9	7.9	28.3	8	-0.9	26,27	90	68	86	81	1.3	6.0	2.0	3.1	7.0	7.8	5.2	6.7
X	–	–	–	–	7.0	13.1	8.4	9.2	14.1	4.8	21.4	19	-1.4	2	91	69	89	83	0.9	5.1	1.2	2.4	7.4	6.1	3.4	5.6
XI	–	–	–	–	3.3	6.8	4.5	4.8	7.8	2.0	16.8	5	-7.7	30	90	79	88	86	0.8	2.5	1.0	1.4	7.4	7.7	6.9	7.3
XII	–	–	–	–	-2.0	0.6	-0.8	-0.8	2.0	-3.6	9.4	8	-18.9	16	91	87	90	89	0.4	0.8	0.6	0.6	8.5	7.3	7.4	7.7
Rok	–	–	–	–	6.8	11.6	8.1	8.6	13.2	4.4	33.3	5.VII	-18.9	16.XII	–	–	–	–	–	–	–	–	6.8	6.3	4.8	6.0

Leszno – Strzyżewice

$\varphi = 51°50'$ $\lambda = 16°32'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.8	15.4	11.1	11.8	16.9	7.6	28.1	8	-0.6	27	93	69	89	84	0.9	6.1	1.6	2.9	7.4	7.9	5.5	6.9
X	–	–	–	–	6.5	13.2	7.6	8.7	14.3	4.1	21.5	19	-1.6	2	95	70	93	86	0.5	4.8	0.8	2.0	7.6	8.4	4.1	6.0
XI	–	–	–	–	3.3	6.9	4.3	4.7	7.7	1.6	16.3	5,8	-7.5	30	91	79	87	86	0.7	2.4	1.0	1.4	7.9	8.1	7.5	7.8
XII	–	–	–	–	-1.9	0.3	-0.9	-0.8	1.7	-3.8	9.3	8	-18.8	17	91	86	89	89	0.5	0.8	0.6	0.6	7.8	7.7	6.3	7.3
P-k	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Zielona Góra II

$H_s = 182$ m

1957

| MIESIĄC | ROZKŁAD WIATRU (PD, %mD) | | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | | |

Pawłowice

$\varphi = 51°50'$ $\lambda = 16°45'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA t									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.3	0.9	-0.5	-0.4	2.0	–	9.9	6	–	–	89	85	90	88	0.6	1.0	0.6	0.7	8.6	7.5	6.4	7.5
II	–	–	–	–	1.5	5.3	3.0	3.2	6.1	–	10.4	14	–	–	91	78	88	86	0.6	2.0	1.0	1.2	7.5	7.5	6.3	7.1
III	–	–	–	–	1.5	7.7	4.2	4.4	9.3	–	17.0	13	–	–	88	61	80	76	0.9	4.5	1.8	2.4	5.5	5.4	4.1	5.0
IV	–	–	–	–	5.3	11.9	7.8	8.2	13.9	2.7	24.9	29	-4.5	8,13	85	56	77	73	1.4	7.0	2.4	3.6	5.1	6.0	4.9	5.3
V	–	–	–	–	9.6	14.6	10.3	11.2	16.0	4.6	25.5	19	-2.2	7	75	54	74	68	3.1	8.6	3.6	5.1	4.4	6.3	5.9	5.5
VI	–	–	–	–	15.7	24.5	17.2	17.9	23.2	10.3	30.2	30	4.8	1	79	56	76	70	4.0	12.0	5.0	7.0	4.8	5.3	4.4	4.8
VII	–	–	–	–	17.5	22.0	18.2	19.0	23.6	13.8	33.0	5	9.2	3	84	65	83	77	3.5	10.5	3.9	6.0	6.0	6.5	6.3	6.3
VIII	–	–	–	–	14.5	19.3	15.6	16.2	–	11.1	–	–	5.8	23	87	65	84	79	2.3	8.2	3.0	4.5	6.2	7.3	5.8	6.4
IX	–	–	–	–	9.9	15.3	11.4	12.0	–	7.4	–	–	-0.6	27	92	67	86	82	1.0	6.4	1.9	3.1	6.2	7.0	5.1	6.1
X	–	–	–	–	6.4	12.8	8.3	9.0	–	3.7	–	–	-2.1	2	93	71	91	85	0.7	4.5	1.1	2.1	6.6	6.0	3.1	5.2
XI	–	–	–	–	3.2	6.8	4.3	4.6	–	1.3	–	–	-7.6	30	90	78	90	86	0.8	2.4	0.9	1.4	7.9	7.7	7.6	7.7
XII	–	–	–	–	-2.0	0.2	-0.9	-0.9	1.6	-4.4	9.0	8	-18.1	17	89	86	89	88	0.5	0.8	0.6	0.6	7.6	7.2	6.5	7.1
Rok	–	–	–	–	6.8	11.5	8.2	8.7	–	–	–	–	–	–	87	68	84	80	1.6	5.7	2.2	3.2	6.4	6.6	5.5	6.2

Strzelna

$\varphi = 51°49'$ $\lambda = 19°54'$

I	–	–	–	–	-2.7	-0.4	-1.6	-1.6	0.9	-4.4	7.0	6	-19.0	17	87	85	86	86	0.6	0.9	0.7	0.7	8.4	8.5	7.2	8.0
II	–	–	–	–	1.2	4.4	2.5	2.6	5.4	-0.1	9.4	24	-7.7	24	87	77	85	83	0.9	2.1	1.2	1.4	8.9	8.5	8.1	8.5
III	–	–	–	–	0.1	6.3	2.3	2.8	7.9	-1.9	15.1	31	-10.3	4	81	62	77	73	4.3	4.3	1.9	2.5	6.4	6.5	4.0	5.6
IV	–	–	–	–	5.2	12.0	6.7	7.6	13.6	2.2	26.5	30	-4.4	15	81	53	76	70	1.8	7.9	2.6	4.1	6.9	6.8	5.9	6.5
V	–	–	–	–	8.9	13.9	8.7	10.0	15.4	4.8	25.5	19	-2.4	6	78	54	80	71	2.6	8.4	2.4	4.5	6.3	7.4	5.6	6.4
VI	–	–	–	–	16.0	21.3	15.5	17.1	23.2	10.1	30.1	11	5.0	27	76	55	81	71	4.5	12.3	3.8	6.9	4.7	5.5	4.0	4.7
VII	–	–	–	–	17.3	22.0	16.9	18.3	23.5	13.6	33.9	8	8.1	29	81	62	85	76	3.9	11.7	3.2	6.3	6.7	7.3	6.5	6.8
VIII	–	–	–	–	14.2	19.1	14.0	15.3	20.8	10.8	27.2	7	4.9	24	92	70	92	85	1.4	7.0	1.4	3.3	6.8	7.9	4.2	6.3
IX	–	–	–	–	9.3	14.8	10.3	11.2	15.9	6.9	27.1	9	-0.9	21	91	70	90	84	1.1	5.7	1.3	2.7	7.0	7.9	5.4	6.8
X	–	–	–	–	6.1	11.9	7.7	8.4	13.1	4.4	20.5	19	-0.4	2,3	93	73	90	85	0.8	4.0	1.1	2.0	6.0	5.9	4.6	5.5
XI	–	–	–	–	2.9	5.8	3.5	3.9	7.1	1.3	17.4	4	-8.5	30	91	81	90	87	0.6	1.9	0.8	1.1	8.2	7.1	7.9	7.7
XII	–	–	–	–	-2.5	-0.4	-1.8	-1.6	1.0	-4.6	7.3	14	-16.9	16	85	84	85	85	0.7	0.9	0.7	0.8	8.2	8.5	7.1	7.9
Rok	–	–	–	–	6.3	10.9	7.1	7.8	12.3	3.6	33.9	8.VII	-19.0	17.1	85	69	85	80	1.7	5.6	1.8	3.0	7.0	7.3	5.9	6.7

Warka

$\varphi = 51°48'$ $\lambda = 21°11'$

I	–	–	–	–	-2.4	-0.2	-1.3	-1.3	0.8	-3.7	6.4	9	-16.0	17	90	86	90	89	0.5	0.8	0.6	0.6	8.2	8.4	7.3	8.0
II	–	–	–	–	1.2	4.4	2.3	2.6	5.3	0.1	9.8	21	-6.2	24	94	82	90	89	0.4	1.7	0.7	0.9	8.5	7.6	6.8	7.6
III	–	–	–	–	-0.5	5.6	2.7	2.6	7.2	-4.5	16.3	28	-7.8	4	86	61	76	74	0.9	4.1	1.9	2.3	5.2	5.3	4.5	5.0
IV	–	–	–	–	5.1	13.1	8.3	8.7	14.4	3.4	26.6	30	-3.7	10	88	54	77	73	1.2	8.6	2.8	4.2	5.6	5.7	5.0	5.5
V	–	–	–	–	9.1	14.1	10.2	10.9	15.5	6.1	25.3	19	0.7	6	84	59	79	73	2.3	7.7	2.7	4.2	5.7	6.9	5.7	6.1
VI	–	–	–	–	15.7	22.4	16.9	18.0	23.9	11.4	31.2	11,19	6.4	21	79	51	76	69	3.8	14.1	4.9	7.6	4.4	5.1	3.4	4.3
VII	–	–	–	–	16.9	22.4	18.2	18.9	24.1	14.4	33.6	8	9.9	29	88	63	84	78	2.5	11.5	3.4	5.8	6.5	5.9	6.5	6.3
VIII	–	–	–	–	14.1	19.9	15.6	16.3	21.8	11.9	30.1	12	7.0	24	94	65	88	84	1.5	8.8	2.3	4.2	4.5	6.1	4.4	5.0
IX	–	–	–	–	9.7	15.2	11.6	12.0	16.9	8.3	28.0	9	0.5	27	92	66	88	82	1.0	6.6	1.8	3.1	5.3	6.8	4.3	5.5
X	–	–	–	–	5.8	12.5	8.2	8.7	13.6	4.9	21.1	19	0.0	3	94	69	90	84	0.6	4.8	1.2	2.2	6.0	5.9	5.6	5.8
XI	–	–	–	–	3.0	6.3	3.6	4.1	7.3	1.4	16.5	4	-7.8	30	92	78	89	86	0.5	2.3	0.8	1.2	7.9	7.2	7.2	7.4
XII	–	–	–	–	-2.5	-0.2	-1.7	-1.5	0.9	-4.4	8.0	13	-16.9	16	90	83	89	87	0.6	1.1	0.7	0.8	7.3	7.7	6.6	7.2
Rok	–	–	–	–	6.3	11.3	7.9	8.4	12.6	4.4	33.6	8.VII	-16.9	16.XII	89	68	85	81	1.3	6.0	2.0	3.1	6.5	6.6	5.6	6.2

Radzyń Podlaski

$\varphi = 51°48'$ $\lambda = 22°39'$

I	–	–	–	–	-2.5	-0.4	-1.8	-1.6	0.5	-4.4	6.2	6	-17.2	17	89	89	90	88	0.5	0.9	0.5	0.6	8.7	8.1	7.9	8.2
II	–	–	–	–	0.7	3.9	1.5	1.9	4.7	-0.9	10.0	14	-5.8	28	93	86	92	90	0.5	1.3	0.5	0.8	9.0	7.3	6.6	7.6
III	–	–	–	–	-1.8	5.1	0.9	1.5	6.6	-3.6	16.5	31	-12.9	4	85	67	83	78	0.8	3.7	1.2	1.9	4.8	4.9	3.8	4.5
IV	–	–	–	–	5.5	13.6	7.6	8.6	14.8	2.1	26.2	29,30	-7.0	10	85	60	80	75	1.4	6.7	2.0	3.4	5.0	5.4	4.3	4.9
V	–	–	–	–	9.9	14.6	9.6	10.9	16.1	5.9	24.8	18	0.2	6,7	80	62	84	75	2.5	7.2	2.0	3.9	5.4	7.3	5.5	6.1
VI	–	–	–	–	16.9	23.7	15.4	17.8	25.1	10.1	32.6	12	4.0	21	74	54	83	70	4.9	14.2	3.3	7.5	3.8	4.3	4.7	4.3
VII	–	–	–	–	17.7	22.9	16.7	18.5	24.7	13.0	33.2	5	7.9	7	82	64	88	78	3.9	11.1	2.5	5.8	4.8	5.9	6.2	5.6
VIII	–	–	–	–	14.9	21.0	14.3	16.1	22.5	10.5	30.2	12	4.4	24	88	64	91	81	2.1	9.7	1.6	4.5	5.3	6.0	3.9	5.1
IX	–	–	–	–	10.2	15.8	10.6	11.8	17.4	7.2	27.4	9	-0.5	26	89	69	91	83	1.4	6.3	1.2	3.0	6.3	7.1	6.0	6.5
X	–	–	–	–	5.6	12.9	7.1	8.8	13.9	3.6	20.2	19	-2.5	3	94	71	92	85	0.8	4.8	0.9	2.2	6.3	5.7	5.6	5.9
XI	–	–	–	–	2.6	5.8	3.3	3.8	7.0	0.9	16.6	1,4	-9.5	30	92	83	94	89	0.5	1.8	0.7	1.0	7.6	8.0	7.1	7.6
XII	–	–	–	–	-1.3	-0.6	-2.5	-2.2	0.3	-5.9	6.8	14	-18.9	16	89	82	88	86	0.6	1.0	0.6	0.7	7.1	7.5	6.4	7.0
Rok	–	–	–	–	6.4	11.6	6.9	7.9	12.8	3.2	33.2	5.VII	-18.9	16.XII	86	74	88	82	1.7	5.7	1.4	2.9	6.2	6.5	5.7	6.1

Pawłowice

$H_s = 101$ m $h_w = 11$ m **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, %mD)																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < 0°	Max < 0°	Min < -10°	Max > 25°	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	v ≥ 10	v ≥ 15	≈	≥ 25	●	●	≡
I	2	2.0	9	6.4	9	3.9	·	·	4.5	1.6	10.5	1.5	4.3	3.6	2	3.0	43	3.0	31.7	9.5	11	–	8	–		15	7	·	5	·	7	·	3	17	–
II	3	2.7	2	2.0	15	3.4	4	3.2	2.1	2.9	9	2.2	2.1	2.9	5	1.4	4	2.7	43.8	13.7	18	–	·	·	·	18	10	1	2	·	10	·	1	8	–
III	5	1.2	4	1.8	2.5	6.5	7	4.1	9.5	5.1	5.5	3.2	1.5	4.2	9	2.7	13	3.8	39.9	11.9	28	–	·	–	·	8	6	1	6	1	5	·	8	9	–
IV	1.9	3.3	8	2.1	11	2.9	5	2.6	2	1.0	5	2.2	1.3	1.8	1.7	3.8	10	2.5	12.7	4.0	24	9	·	·	·	6	4	·	2	·	3	1	5	6	–
V	1.9	2.4	2.2	2.6	8	1.7	8	2.2	1	1.0	1	1.0	1.3	2.6	1.7	2.9	4	2.4	29.9	14.4	23	3	·	·	1	6	3	1	1	·	·	1	2	5	–
VI	5	1.9	9.5	1.9	13.5	1.9	3	1.0	8	2.8	9.5	1.9	1.6	2.7	12.5	2.2	13	1.6	87.2	35.0	4	·	·	·	10	10	8	4	·	·	1	5	7	5	–
VII	1.0	1.2	7	1.7	6.5	3.6	2	2.0	5	1.8	1.3	2.2	2.6.5	2.4	1.4	2.4	9	2.0	157.6	54.7	23	·	·	·	12	15	12	5	·	·	1	6	3	1.3	–
VIII	3.5	1.1	2	1.0	4	2.0	1	3.0	8.5	2.8	1.1	2.3	2.8	3.1	1.3	3.2	22	2.1	56.4	11.2	24	·	·	·	–	1.1	9	2	·	·	5	5	·	5	–
IX	2	1.0	3	1.7	1	1.0	7	1.9	8	2.7	2.4	3.0	2.1	3.4	9	2.4	15	2.3	56.5	9.0	29	2	·	·	–	18	1.4	·	·	·	4	1	2	8	–
X	·	·	2	1.0	4	1.8	8	1.6	1.7	1.5	1.2	1.8	2.4.5	2.6	3.5	1.0	22	1.5	56	2.0	19	2	·	·	·	7	2	·	·	·	16	·	4	4	–
XI	1	4.0	1.3	5.5	2.7	3.0	8	2.2	1.0	2.4	8	3.0	1.6	3.9	4	6.8	3	3.5	45	2.6	28	1.2	2	·	·	7	1	·	3	·	6	·	3	1.8	–
XII	3.5	2.7	9	2.3	10.5	2.3	1.5	1.3	8	1.5	8.5	1.8	2.6	3.6	1.6	1.9	10	2.2	43.0	12.8	8	27	8	3	·	13	9	1	2	1	8	·	1	13	–
Rok	73	2.0	90.5	2.5	134.5	2.8	54.6	2.1	102.5	2.3	11.7	2.2	26.3	3.1	12.2	2.8	138	2.5	568.8	54.7	23.VII	–	48	–	–	134	85	15	21	2	64	17	39	109	–

Strzelna

$H_s = 194$ m $h_w = 19,5$ m

I	2	3.0	6.5	2.5	5.6	2.3	4	2.5	2.0	2.6	2.8	3.2	2.4	3.8	2	4.0	2	3.0	23.7	4.6	13	26	11	6	·	16	6	·	1	· ·	–	·	·	2.0	–
II	6.5	1.8	4	1.5	4	2.0	8.5	2.1	2.6.5	2.5	1.8.5	2.5	9.5	3.1	0.5	3.0	6	2.2	43.9	10.5	18	12	2	·	·	18	11	1	·	· ·	–	·	1	2.0	–
III	8	1.6	7.5	1.9	1.9	3.1	9	4.6	9.5	2.6	1.0	4.0	1.6	3.5	4	3.1	1.0	2.8	28.5	11.0	15	1.9	3	1	·	7	5	1	3	·	–	·	4	9	–
IV	1.5	2.2	1.5	1.0	8.5	2.4	8	1.8	5	1.9	3	2.5	1.3	1.9	2.5	2.3	11	1.9	20.4	8.9	30	9	·	·	4	9	7	·	·	·	–	1	4	12	–
V	1.9	2.4	8	2.0	10.5	1.8	8	1.5	2.5	1.6	7.5	2.7	5.5	1.9	2.0	2.4	4.2	1.9	30.6	12.5	10	2	·	·	1	6	5	1	·	·	–	1	3	8	–
VI	1.4.5	1.9	9	1.2	7.5	1.4	8.5	1.7	8.5	1.8	12.5	2.6	1.0	2.0	10.5	2.3	9	1.7	61.2	22.5	9	·	·	·	3	7	6	3	·	·	–	7	6	6	–
VII	9	1.9	5	1.2	1.0	1.9	6.5	1.9	9	1.9	1.4	2.4	1.8.5	2.4	1.2	1.9	9	1.9	30.4.0	12.0.2	16	·	·	·	12	17	1.4	5	·	·	–	7	3	12	–
VIII	5	1.8	·	·	2	1.2	9	1.6	11.5	2.5	1.9.5	2.7	2.3.5	2.2	5.5	2.2	1.7	1.8	49.3	14.0	16	·	·	·	4	11	1.0	2	·	·	–	2	2	8	–
IX	4	1.8	1	1.0	2.5	2.2	3	2.0	1.6	2.8	2.7.5	3.3	1.7	3.3	8	2.6	11	2.6	107.9	32.5	23	3	·	·	2	12	11	5	·	·	–	·	·	1.0	–
X	7	1.4	2	1.5	5	1.6	9.5	2.1	2.6	2.6	2.3.5	3.3	1.2.5	3.4	6.5	2.7	·	2.6	6.8	2.8	20	2	·	·	·	7	2	·	·	·	–	·	5	5	–
XI	4	4.2	11.5	2.1	1.9.5	1.7	1.8.5	2.5	7	2.8	9.5	4.1	1.2	4.1	3	7.7	5	2.8	38.3	14.5	28	11	2	·	·	8	6	1	1	·	–	·	2	1.8	–
XII	7.5	1.5	1.5	2.3	8.5	1.6	9	2.6	1.9.5	3.1	2.2.5	4.1	11	4.0	11.5	2.9	2	3.0	33.9	12.5	14	2.7	9	3	·	12	9	1	1	·	–	·	1	1.8	–
Rok	1.0.1.5	2.1	5.7.5	1.5	1.0.2.5	1.9	1.0.1.5	2.2	1.6.1	2.4	1.9.6	3.1	1.7.2.5	3.0	1.0.8.5	3.1	9.4	2.4	7.4.8.5	12.0.2	16.VII	1.1.1	2.7	1.0	2.9	1.3.0	9.2	2.0	6	·	–	1.8	3.1	1.4.6	–

Warka

$H_s = 120$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20.3	3.7	5	2.3	1.2	2	·	10	6	·	–	–	8	·	2	2.2	1.9
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.7.9	6.9	1.8	1.2	2	·	·	2.4	1.6	·	–	–	6	·	1	1.2	4
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.4	8.4	15	2.0	4	·	·	8	5	·	–	–	3	·	7	6	1
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20.5	5.4	29	8	·	·	4	10	7	·	–	·	2	4	5	7	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36.5	15.0	9	·	·	·	1	6	4	2	–	–	2	1	2	10	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	55.4	25.8	24	·	·	·	10	9	6	2	–	–	2	5	7	3	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	113.9	26.6	16	·	·	·	12	16	15	3	–	–	6	9	4	12	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	12.5.0	26.0	14	·	·	·	5	18	14	5	–	–	3	7	4	3	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.4.8	16.3	24	·	·	·	2	17	10	3	–	–	2	2	3	5	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.5	2.2	22	·	·	·	·	8	2	·	–	–	7	·	4	8	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	10.6	4.1	28	1.1	2	·	·	11	4	·	–	–	8	·	3	1.7	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24.6	10.9	14	2.5	1.1	3	·	14	4	1	–	–	1	·	2	1.6	10
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	558.4	26.6	16.VII	9.7	3.1	5	3.4	15.1	9.3	16	–	–	50	28	44	12.1	3.4

Radzyń Podlaski

$H_s = 151$ m $h_w = 10$ m

I	0.5	2.0	·	·	1.6	5.4	1.0	2.8	8	3.5	2.5	2.0	4.0.5	3.7	5.5	2.5	1.0	3.4	23.2	6.7	6	2.6	1.1	5	·	12	8	·	2	·	1	·	1	2.3	2.4
II	6	3.7	4	2.2	4	2.5	2	4.0	1.7	2.8	9	2.4	1.4	2.9	2	2.5	2.6	2.0	53.4	9.4	22	1.6	3	·	·	2.3	1.3	·	·	·	4	·	1	1.3	6
III	1.4	4.0	7	2.6	1.4.5	6.9	7	5.7	7	3.0	7.5	4.4	10.5	3.1	8.5	5.4	1.7	3.7	22.6	9.0	15	2.5	7	2	·	6	4	·	4	·	·	·	10	6	1.2
IV	1.3	2.6	12.5	4.1	1.5.5	2.2	1.2	2.9	1	2.0	6	2.3	5	2.2	5	2.8	2.0	2.2	24.4	1.4.0	17	8	·	·	3	5	3	1	·	·	·	·	9	7	·
V	2.8.5	2.7	10.5	3.6	2.5	3.3	1	2.0	1	5.0	1	3.0	5	3.6	5	3.2	1.6	2.6	39.6	13.9	10	·	·	·	·	10	6	1	·	·	·	·	5	10	1
VI	2.7.5	2.9	3	1.3	1.7	2.2	1.0	3.7	6	2.8	5	1.6	8	2.6	5.5	3.0	8	2.6	5.4.0	4.5.5	24	·	·	·	1.3	8	4	1	·	·	·	5	9	3	
VII	8.5	2.2	8.5	2.8	1.9	2.3	8	4.0	5	2.2	8	2.6	1.1	2.2	7	3.3	1.8	2.1	–	–	–	·	·	·	1.4	–	–	–	·	·	·	3	7	9	·
VIII	2.1.5	2.1	6	3.5	7	2.6	7	3.3	1	1.0	6	2.7	1.0	3.7	10.5	2.5	2.4	2.1	1.1.6.3	3.5.2	29	·	·	·	5	1.7	8.3	5	·	·	·	4	3	5	·
IX	1.1.5	2.1	2.5	2.0	1.3.5	2.2	4.5	2.2	7	2.4	9	4.7	2.0.5	5.2	7.5	4.3	1.4	3.0	6.4.6	12.5	23	2	·	·	1	1.7	1.3	1	3	·	·	1	4	1.3	·
X	4	2.2	1	1.0	1.1	2.0	6	3.3	8	2.4	8	3.0	2.9	3.7	5	3.6	2.1	2.4	12.7	6.6	23	1	·	·	·	6	3	·	·	·	5	·	3	8	
XI	5	2.0	·	·	3.0.5	4.3	1.4.5	3.1	6	2.7	3	2.0	1.6	5.1	3	1.4.0	1.2	4.5	16.2	8.0	28	1.2	2	·	·	11	5	·	3	1	·	·	4	2.6	2
XII	1.1	3.3	3	2.3	1.2	2.8	5.5	2.7	1.2.5	3.3	1.1	3.8	2.4	2.8	1	2.0	1.3	2.6	3.4.0	1.4.7	1.4	2.8	1.3	7	·	1.2	8	1	·	·	2	·	3	1.5	2.5
Rok	1.5.1	3.1	5.8	2.1	1.8.5	3.2	8.7.5	3.5	7.3.5	2.5	7.6	3.5	1.9.3.5	3.4	6.5.5	4.1	1.9.9	2.8	–	4.5.5	24.VI	1.1.8	3.6	1.4	3.5	–	–	–	1.2	1	1.8.8	1.3	5.3	1.5.2	7.0

Puczniew

$\varphi = 51°47'$ $\lambda = 19°05'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnio				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.7	0.5	-0.8	-0.7	1.5	-3.5	8.2	6	-15.8	16	–	–	–	–	–	–	–	–	7.4	7.1	7.5	7.3
II	–	–	–	–	1.6	4.8	2.8	3.0	5.8	0.1	9.9	19	-5.0	24	90	78	87	85	0.7	2.0	1.0	1.2	8.5	7.4	7.6	7.8
III	–	–	–	–	0.8	6.8	3.0	3.4	8.5	-1.4	15.2	13	-8.0	10	81	58	79	73	1.3	4.6	1.8	2.8	5.5	5.6	4.4	5.2
IV	–	–	–	–	4.9	11.8	6.4	7.4	13.4	1.7	26.0	30	-6.0	13	83	54	82	73	1.5	7.6	1.8	3.6	5.6	6.4	5.2	5.7
V	–	–	–	–	8.8	14.0	9.0	10.2	15.6	4.1	26.3	19	-1.6	28	80	56	82	73	2.4	8.0	2.2	4.2	4.6	6.4	4.8	5.3
VI	–	–	–	–	16.0	21.3	15.4	17.0	23.3	9.7	30.2	11	4.5	15	77	53	83	71	4.4	12.8	3.0	6.7	3.6	4.9	3.6	4.0
VII	–	–	–	–	17.2	22.0	17.2	18.4	23.8	13.4	34.1	8	8.5	3	85	65	88	79	3.2	11.2	2.7	5.7	6.2	6.1	5.9	6.1
VIII	–	–	–	–	14.1	19.2	14.6	15.6	21.2	10.9	26.9	11	6.5	24,30,31	89	66	90	82	1.8	8.0	1.8	3.9	5.5	6.5	3.6	5.2
IX	–	–	–	–	9.5	14.6	11.0	11.5	16.4	6.9	27.2	9	-1.4	27	90	70	88	83	1.2	5.6	1.7	2.8	6.2	7.5	5.3	6.3
X	–	–	–	–	6.6	12.3	8.1	8.8	13.5	4.8	20.9	19	-0.4	3	91	72	88	84	1.0	4.4	1.4	2.3	6.0	6.3	4.5	5.6
XI	–	–	–	–	3.5	6.6	4.0	4.5	7.7	1.6	17.2	4	-8.0	30	87	76	86	83	1.0	2.7	1.1	1.6	7.4	6.5	7.9	7.3
XII	–	–	–	–	-2.0	0.2	-1.4	-1.2	1.6	-4.6	7.8	13	-18.6	16	88	85	88	87	0.6	0.9	0.6	0.7	7.4	8.3	7.0	7.6
Rok	–	–	–	–	6.6	11.2	7.4	8.2	12.7	3.6	34.1	8.VII	-18.6	16.XII	–	–	–	–	–	–	–	–	6.2	6.6	5.6	6.1

Wisznice

$\varphi = 51°47'$ $\lambda = 23°12'$

I	–	–	–	–	-2.9	-1.0	-1.8	-1.9	0.2	-4.4	6.4	10	-17.0	17	88	82	91	87	0.5	1.0	0.5	0.7	9.2	8.3	9.2	8.9
II	–	–	–	–	0.7	3.1	1.7	1.8	4.4	-0.6	8.9	15	-6.2	27	95	89	96	93	0.3	0.9	0.3	0.5	7.7	7.6	8.4	7.9
III	–	–	–	–	-1.6	4.5	1.2	1.3	5.9	-3.1	16.3	30,31	-12.0	4	82	67	85	78	1.0	3.4	1.1	1.8	2.8	4.1	3.4	3.4
IV	–	–	–	–	5.8	12.8	8.6	9.0	14.5	2.4	26.9	30	-4.5	15	–	–	–	–	–	–	–	–	5.0	5.7	5.7	5.5
V	–	–	–	–	9.9	14.3	11.0	11.6	15.9	6.2	24.4	18,19	-0.5	5	84	66	88	79	2.1	6.1	1.6	3.3	6.4	7.6	6.1	6.7
VI	–	–	–	–	16.3	22.4	16.7	18.0	24.2	10.3	31.4	12	5.1	7,21	73	49	80	67	5.2	14.5	4.0	7.9	3.9	5.4	4.0	4.4
VII	–	–	–	–	17.1	22.8	18.6	19.3	24.2	12.5	31.9	5,8	8.4	26	81	57	85	74	3.9	13.4	3.5	6.9	6.1	6.1	6.0	6.1
VIII	–	–	–	–	14.6	20.3	16.2	16.8	21.4	11.4	30.1	11	5.2	24	–	–	–	–	–	–	–	–	5.0	5.7	5.2	5.3
IX	–	–	–	–	10.1	15.1	11.8	12.2	16.1	8.0	26.7	9	1.3	26	–	–	–	–	–	–	–	–	6.3	6.3	6.3	6.3
X	–	–	–	–	5.8	12.0	8.1	8.5	13.0	3.9	18.6	19	-2.0	4	–	–	–	–	–	–	–	–	4.5	5.0	4.7	4.7
XI	–	–	–	–	2.8	5.3	3.4	3.7	6.4	0.9	16.6	2	-9.3	30	90	82	92	88	0.7	1.7	0.6	1.0	7.4	7.2	7.2	7.3
XII	–	–	–	–	-3.6	-1.1	-1.9	-2.1	0.4	-5.5	7.9	13	-19.4	16	89	84	90	88	0.5	0.9	0.5	0.6	6.4	6.0	6.7	6.4
Rok	–	–	–	–	6.2	10.9	7.8	8.2	12.2	3.5	34.9	5.8.VII	-19.4	16.XII	–	–	–	–	–	–	–	–	5.9	6.2	6.1	6.1

Ciołkowo

$\varphi = 51°45'$ $\lambda = 16°59'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	9.4	14.9	10.1	11.1	16.8	5.4	27.0	19	-0.9	7	–	–	–	–	–	–	–	–	4.6	5.8	3.9	4.7
VI	–	–	–	–	14.4	21.9	17.6	17.9	24.3	11.4	31.6	19	6.1	15	–	–	–	–	–	–	–	–	4.4	4.3	3.8	4.2
VII	–	–	–	–	17.8	22.4	18.1	19.1	23.6	14.6	34.3	5	11.2	3,19,28	–	–	–	–	–	–	–	–	6.6	6.9	6.8	6.8
VIII	–	–	–	–	14.4	19.7	15.0	16.0	–	11.4	–	–	6.6	23	–	–	–	–	–	–	–	–	6.6	6.1	4.8	5.8
IX	–	–	–	–	9.8	15.5	11.4	12.0	17.0	8.0	26.9	8	-0.2	27	–	–	–	–	–	–	–	–	6.9	7.6	4.8	6.4
X	–	–	–	–	6.4	13.2	8.1	9.0	–	4.8	–	–	-1.4	2	–	–	–	–	–	–	–	–	6.7	6.9	4.0	5.9
XI	–	–	–	–	3.5	6.9	4.3	4.8	–	2.1	–	–	-7.6	30	–	–	–	–	–	–	–	–	7.0	7.6	7.1	7.2
XII	–	–	–	–	-1.8	0.5	-0.8	-0.7	1.7	-3.6	9.4	8	-16.9	17	–	–	–	–	–	–	–	–	7.2	7.5	6.2	7.0
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kalisz

$\varphi = 51°44'$ $\lambda = 18°05'$

I	1003.7	1015.4	985.9	1021.9	-1.6	0.7	-1.0	-0.7	1.7	-3.1	8.7	6,9	-12.1	17	90	85	89	88	0.6	1.0	0.6	0.7	7.9	7.8	6.2	7.3
II	993.7	1016.3	967.3	1011.5	1.3	4.8	2.5	2.8	5.8	0.2	10.3	14	-4.3	24	92	78	89	86	0.5	1.9	0.8	1.1	7.6	8.0	5.6	7.1
III	1000.9	1018.3	978.6	1018.8	1.0	6.6	3.7	3.8	8.4	-0.4	15.1	13	-7.2	1	88	66	78	77	0.8	3.7	1.8	2.1	6.3	6.0	3.7	5.3
IV	1001.1	1014.6	977.8	1018.6	4.3	11.5	7.5	7.7	13.4	2.4	25.4	30	-5.2	13	90	63	80	78	0.8	6.1	2.4	3.1	5.9	7.0	5.3	6.1
V	999.2	1009.9	989.7	1016.6	8.5	14.4	10.1	10.8	16.4	5.0	26.0	19	-1.4	7	81	56	78	72	2.2	8.0	2.9	4.4	5.5	7.0	5.1	5.8
VI	999.7	1015.3	988.5	1016.7	15.8	22.1	17.0	18.0	24.3	10.5	32.1	11	3.8	1	79	55	78	71	3.9	12.9	4.4	7.1	5.1	6.0	4.1	5.1
VII	995.4	1007.8	983.7	1012.2	17.2	24.9	17.8	18.7	–	–	–	–	–	–	86	67	86	80	3.2	10.6	3.5	5.8	6.2	6.8	6.5	6.5
VIII	997.3	1008.0	984.4	1014.5	14.0	19.5	15.2	16.0	–	11.3	–	–	6.6	31	91	68	86	82	1.6	7.6	2.0	3.9	5.9	7.3	5.1	6.1
IX	996.4	1006.3	979.7	1013.2	9.2	15.0	11.1	11.6	17.3	7.4	28.4	8	-0.2	27	94	73	90	86	0.7	5.3	1.4	2.5	7.1	7.9	4.9	6.6
X	1002.4	1011.8	986.6	1019.9	5.5	12.3	7.9	8.4	13.7	4.2	19.8	10	-0.8	3	95	76	92	88	0.4	3.7	0.9	1.7	6.6	6.9	5.2	5.6
XI	1003.2	1021.6	987.1	1021.1	3.0	6.4	4.0	4.4	7.7	1.6	17.7	4,5	-7.7	30	90	79	88	86	0.7	2.3	1.0	1.3	7.9	7.8	7.8	7.8
XII	997.5	1016.5	960.6	1015.5	-2.3	-0.2	-1.5	-1.4	1.2	-4.1	7.9	9	-15.9	16	91	87	90	89	0.5	0.8	0.5	0.6	7.3	8.5	7.1	7.6
Rok	999.2	1021.6	960.6	1016.7	6.3	11.2	7.9	8.3	–	–	–	–	-15.9	16.XII	89	74	85	82	1.3	5.3	1.9	2.8	6.6	7.2	5.4	6.4

Puczniew

$H_s = 135\ m$ $h_w = 10\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D, °mD																	OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0	Max<0	Min<10	Max≥25	R≥0.1	R≥1.0	R≥10.0	v≥10	v≥15				
I	1	2.5	7	4.2	1.5	2.3	2.5	1.4	6.5	2.0	4.5	2.3	15.5	3.8	3	3.3	11	2.4	21.1	6.7	5	24	9	2	·	8	5	·	1	·	11	·	5	19	19
II	1	1.5	4.5	2.8	0.5	4.0	6	3.2	1.8	4.1	31.5	3.3	8.5	4.9	6	3.6	8	3.3	47.5	8.8	8	13	1	·	·	21	12	·	1	·	7	·	2	16	3
III	4.5	4.0	6.5	3.4	1.3	6.7	11	5.2	1.3	5.2	12.5	5.8	9	7.2	8.6	4.5	15	4.6	328	89	17	18	2	·	·	9	6	·	6	1	·	·	8	8	1
IV	8.5	3.9	4.5	2.3	4	4.1	4	3.9	5	3.2	12.5	3.9	1.4	3.1	24.5	3.7	16	3.0	297	8.4	25	11	·	·	1	15	7	·	·	·	4	2	7	8	·
V	13.5	4.1	1.1	4.4	7	3.9	4	3.0	2.5	3.0	9.5	4.3	11.5	3.3	20	4.7	14	3.5	450	27.8	20	4	·	·	1	9	5	1	·	·	2	1	4	9	·
VI	5	3.3	7.5	3.0	6	2.8	7.5	3.0	6.5	3.2	27	4.1	1.1	3.5	5.5	4.4	1.4	3.0	477	20.8	9	·	·	·	9	9	6	2	·	·	·	5	10	6	·
VII	2	3.5	2	2.5	6	4.5	3.5	3.7	6.5	2.2	33.5	4.1	1.4	4.0	10.5	4.0	15	3.2	267.3	75.8	16	·	·	·	14	18	16	6	·	·	·	9	5	11	·
VIII	2	5.5	·	·	1	3.0	4	4.8	6	4.8	42.5	3.9	14.5	3.6	7	3.8	16	3.3	57.9	17.0	16	·	·	·	3	14	8	2	·	·	8	2	5	4	·
IX	·	·	1	2.0	·	·	0.5	2.0	1.0	4.6	4.5	4.4	2.0	5.4	3.5	3.6	1.0	4.1	78.7	16.0	24	2	·	·	·	23	12	3	2	·	6	·	3	7	·
X	·	·	1	2.0	·	·	7.5	4.1	1.3	4.0	4.9	3.7	1.4.5	3.8	1	3.0	1.0	3.4	8.6	3.3	20	1	·	·	·	8	3	·	·	·	1.4	·	4	7	·
XI	1	7.0	1.4.5	5.1	8.5	4.1	1.4	4.5	9	3.7	1.9	5.3	9.5	7.2	4.5	8.4	1.0	4.7	19.7	5.2	2	10	2	·	·	7	5	·	5	·	9	·	2	17	·
XII	0.5	3.0	3.5	5.9	6.5	3.3	8	2.7	1.4.5	3.9	36	4.9	9.5	3.3	9.5	3.7	5	3.9	32.7	7.6	1.4	26	8	3	·	1.8	7	·	1	·	9	·	2	1.9	1.1
Rok	3.9	3.2	6.0	3.1	5.4	3.2	7.2.5	3.5	1.1.0.5	3.7	3.6.3	4.2	1.4.8.5	4.4	1.0.3.5	4.2	1.4.4	3.5	6.8.8.7	7.5.8	1.6.VII	1.0.9	2.2	5	2.8	1.5.9	9.2	1.4	1.6	1	7.0	1.9	5.7	1.3.1	3.4

Wisznice

$H_s = 152\ m$ $h_w = 11\ m$

I	5.5	2.0	8	2.1	1.0	2.6	6	2.6	9	2.1	2.8.5	3.8	2.1	3.2	2	3.0	3	2.9	7.7	5.0	6	2.4	1.3	3	·	–	–	–	·	·		–	·	2.3	2.2
II	0.5	5.0	·	·	1	1.5	5	2.0	1.1	2.3	3.9.5	2.8	6	2.4	1.8	3.5	1.3	2.3	2.8.9	4.5	9	1.3	2	·	·	1.6	1.1	·	1	·	6	–	1	1.7	3
III	1.7.5	3.1	4.5	9.5	6	4.3	1.1	3.5	1.0	3.1	1.4	2.5	1.2	6.2	1.6	3.2	2	3.8	1.8.5	1.2.5	1.5	2.0	8	2	·	4	3	1	3	·	·	–	1.2	2	1
IV	2.4.5	3.2	2	2.5	3.5	3.3	9	2.8	1.0.5	3.0	7.5	1.9	8.5	3.2	1.6.5	3.1	8	2.7	1.5.6	7.4	1.7	6	·	·	4	4	3	·	·	·	–	5	6	·
V	3.2.5	3.0	1.1.5	2.4	4	2.5	2.5	3.2	6	3.3	2.5	1.8	4	4.7	1.8	3.8	1.2	2.7	5.1.9	2.9.0	9	1	·	·	·	6	6	1	·	·	2	–	2	1.3	·
VI	7	3.5	1.5	5.3	0.5	3.0	6	3.0	2.1	3.6	1.5.5	5.0	1.2.5	4.1	1.4	4.4	1.2	3.6	7.2.1	4.6.8	24	·	·	·	10	5	5	2	7	·	·	–	5	·	·
VII	8	1.8	7.8	3.0	5	2.9	7.5	3.1	1.0	3.6	2.2.5	3.9	1.4.5	4.2	1.1	3.5	7	3.2	6.3.2	1.8.5	1.6	·	·	·	1.4	1.0	1.0	1	2	·	·	–	·	9	·
VIII	2.5	2.8	0.5	1.0	1	1.5	0.5	2.0	2.3.5	2.7	2.7	2.8	1.9	3.4	6	3.8	1.3	2.5	1.3.8.2	5.9.0	2.9	·	·	·	3	9	9	5	·	·	2	–	3	6	·
IX	2	1.0	3.5	3.4	8	2.2	8	2.0	1.7	3.2	2.4	3.5	1.0.5	3.5	1.5	2.2	2	2.8	5.9.6	2.1.3	2.9	·	·	·	1	1.0	8	2	1	·	2	–	3	8	·
X	0.5	2.0	·	·	1	2.0	1.6.5	2.3	2.2.5	1.7	3.0	2.6	1.0	2.2	2.5	3.6	1.0	2.0	3.3	1.2	2.2	2	·	·	·	4	2	·	·	·	2	–	6	6	·
XI	1.4	6.4	7.5	3.9	2.2	2.2	1.3.5	1.9	8.5	1.4	2.5	4.0	1.0.5	3.0	5.5	4.0	6	3.0	2.2.3	7.6	2.5,29	1.1	3	·	·	9	4	·	2	·	2	–	6	1.9	·
XII	1.0.5	3.0	1.3	2.1	2.5	3.6	6.5	2.5	1.5.5	3.1	1.7	4.4	1.6	3.7	1.1	3.6	1	3.3	2.3.8	1.1.0	1.5	2.8	1.2	4	·	7	4	1	2	·	·	–	2	1.2	1.7
Rok	1.2.5	3.1	5.9.5	2.9	6.4.5	2.6	9.2	2.6	1.6.4.5	2.8	2.3.0.5	3.2	1.4.4.5	3.6	1.2.5.5	3.5	8.9	2.9	5.0.5.1	5.9.0	2.9.VIII	1.0.5	3.8	9	3.2	–	–	–	1.8	·	1.6	–	4.5	1.8.1	4.3

Ciatkowo

$H_s = 110\ m$ $h_w = 10\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	2.9.3	1.2.9	6	2	·	·	2	5	4	2	–	–	–	1	7	7	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.4.5	2.7.9	4	·	·	·	1.4	1.1	9	4	–	–	–	4	5	1.0	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1.9.4.6	1.0.6.5	2.3	·	·	·	1.3	1.9	1.7	3	–	–	–	6	3	1.4	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.2.2	1.2.1	2.4	·	·	·	–	1.5	1.1	1	–	–	–	4	5	7	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.9.0	1.2.6	1.6	1	·	·	1	2.1	1.4	2	–	–	–	1	3	9	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.7	2.0	1.9	1	–	·	–	7	3	·	–	–	–	·	5	1.0	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.5	2.3	2.8	1.0	–	·	–	1.2	3	·	–	–	–	·	5	1.8	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.9.2	1.2.2	1.4	2.4	9	3	·	1.7	1.1	1	–	–	–	·	2	1.1	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1.0.6.5	2.3.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kalisz

$H_s = 140\ m$ $H_b = 143{,}1\ m$ $h_w = 12\ m$

I	1.5	2.3	6.5	4.5	4	2.6	3.5	1.9	9.5	2.2	30.5	2.6	3.0	3.9	2.5	7.4	5	3.4	1.9.3	6.5	6	2.5	6	2	·	1.4	4	·	2	1.5	5	·	3	1.7	1.0
II	7	1.6	3	2.3	4.5	1.8	5	2.3	1.6	3.3	2.7	2.7	1.5	3.7	1.5	3.0	5	2.7	4.6.3	8.9	1.8	1.4	·	·	·	1.6	1.1	·	·	·	3	·	·	9	1
III	4.5	2.4	9	3.2	1.4	3.8	1.4	3.4	1.4.5	3.4	6.5	2.8	1.7	4.8	4.5	3.6	9	3.3	3.6.4	1.1.4	2.8	1.8	·	·	·	7	6	1	–	–	2	·	8	9	1
IV	2.0.5	3.2	7.5	3.1	4	2.6	2.5	3.0	7.5	2.9	4.5	2.9	1.1	3.4	1.1.5	2.7	2.1	2.3	2.4.6	7.6	2.4	8	·	·	1	1.2	1.0	·	1	·	3	1	4	9	·
V	9.5	3.5	2.7	3.1	8.5	2.3	5	2.4	5	2.6	5.5	2.7	1.5.5	3.3	1.0	3.4	7	2.6	2.3.3	1.3.3	2.0	1	·	·	1	6	5	1	1	·	1	·	1	6	·
VI	1.0	2.6	8.5	2.1	1.2	1.8	5	2.5	8	3.5	1.4	2.9	2.2	3.8	8.5	2.5	2	2.8	3.2.8	1.3.1	2.4	·	·	·	1.3	1.1	7	1	1	·	·	8	5	3	·
VII	8	1.6	3.5	3.3	1.1	3.2	8	3.2	5	2.9	1.7.5	2.8	2.2.5	3.6	1.0.5	2.4	7	2.7	1.6.7.8	2.3.3	2.3	·	·	·	–	2.0	1.6	8	·	·	1	8	3	1.0	·
VIII	1.5	2.0	·	·	4	2.0	2	2.8	4.5	2.8	3.0	2.9	3.6	2.5	8	2.4	7	2.4	8.5.1	2.5.8	1.0	·	·	·	–	1.2	1.1	3	·	·	·	3	·	8	·
IX	1	3.0	1.5	4.0	1	4.0	1.5	1.7	1.5	3.2	2.0	4.0	3.4	4.3	9	2.4	7	3.4	7.2.3	2.0.4	2.4	1	·	·	2	1.8	1.4	2	3	·	1	1	1	7	·
X	·	·	·	·	·	·	3.5	2.7	1.8	2.3	3.0	2.8	2.3	2.6	5.5	1.8	1.5	2.1	1.2.6	2.9	2.0	2	·	·	·	7	5	·	·	·	9	·	4	4	·
XI	4	5.4	1.0	2.9	1.9	2.8	1.3.5	2.5	9.5	3.2	9	3.6	1.4.5	6.6	1.5	5.7	9	3.4	9.1	2.3	2.7	1.0	3	·	·	7	4	·	·	·	1	·	1	1.9	·
XII	1.4	2.5	·	·	5	2.3	5	1.7	1.6	2.9	2.3.5	3.7	1.1.5	4.5	6	2.8	1.2	2.8	3.6.1	7.2	8	2.5	8	4	·	1.4	1.0	·	1	1.5	8	·	1	1.5	1.1
Rok	8.1.5	2.5	7.6.5	2.1	8.7	2.2	6.8.5	2.6	1.2.6.5	2.9	2.1.8	3.0	2.5.2	3.9	7.9	3.3	1.0.6	2.8	5.6.5.7	2.5.8	1.0.VIII	1.0.4	1.7	6	–	1.4.4	1.0.3	1.6	–	–	3.0	1.9	2.9	1.4.6	2.3

Łódź – Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$ **1957**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	998.2	1009.4	980.2	1022.0	-2.3	-0.4	-1.2	-1.2	0.9	-4.1	7.8	6	-17.3	17	90	87	89	89	0.5	0.8	0.6	0.6	7.8	7.8	7.4	7.7
II	988.8	1010.0	963.5	1012.0	1.5	4.6	2.8	2.9	5.4	0.0	9.6	6	-6.6	24	92	78	88	86	0.6	2.1	1.0	1.2	7.8	8.3	7.1	7.7
III	995.8	1014.6	973.5	1019.4	0.7	6.5	3.5	3.6	8.4	-1.1	15.3	31	-7.4	4	83	60	74	72	1.2	4.4	2.1	2.6	6.4	6.4	4.7	5.8
IV	995.6	1008.3	972.1	1018.5	4.9	11.8	7.7	8.0	13.5	2.3	26.0	30	-5.4	14	84	54	73	70	1.5	7.5	3.1	4.0	6.7	7.1	5.5	6.4
V	993.7	1004.0	984.5	1016.3	9.0	14.0	10.3	10.9	15.5	4.8	25.9	19	-0.5	29	77	52	71	67	2.8	8.8	3.9	5.2	5.7	7.5	5.9	6.4
VI	994.7	1009.7	983.3	1016.8	16.1	21.4	16.7	17.7	23.8	10.6	30.5	30	5.7	27	73	51	74	66	5.2	13.6	5.3	8.0	5.0	5.7	4.7	5.1
VII	990.2	1002.0	978.5	1012.1	17.1	22.3	17.8	18.8	24.0	13.5	34.9	8	9.1	3	83	61	82	75	3.9	13.0	4.4	7.1	6.5	6.9	6.4	6.6
VIII	992.6	1002.4	980.0	1014.7	14.0	19.0	14.7	15.6	21.0	10.8	26.8	11	5.8	30	91	67	88	82	1.6	7.7	2.2	3.8	6.7	7.4	3.7	5.9
IX	990.8	1000.6	975.7	1013.2	9.3	14.4	11.1	11.5	16.1	6.8	27.8	9	-1.6	27	91	71	87	83	1.1	5.6	1.7	2.8	6.5	8.0	5.4	6.6
X	997.4	1007.3	982.1	1020.3	6.4	12.0	8.3	8.8	13.4	4.7	20.8	19	-0.5	3	93	74	88	85	0.7	4.0	1.3	2.0	6.5	6.9	3.7	5.7
XI	998.2	1016.6	984.0	1021.5	3.3	6.3	4.2	4.5	7.4	1.5	17.0	4	-9.5	30	89	78	86	84	0.8	2.4	1.2	1.5	8.1	6.9	7.8	7.6
XII	992.4	1011.1	954.7	1016.0	-2.1	-0.1	-1.4	-1.2	1.2	-4.6	8.3	9	-15.1	17	91	86	90	89	0.5	0.9	0.6	0.7	7.5	8.5	7.3	7.8
Rok	994.0	1016.6	954.7	1016.8	6.5	11.0	7.9	8.3	12.6	3.8	34.9	8.VII	-17.3	17.I	86	68	82	79	1.7	5.9	2.3	3.3	6.8	7.3	5.8	6.6

Łódź – Ruda Pabianicka

$\varphi = 51°42'$ $\lambda = 19°27'$

I	-	-	-	-	-2.4	0.1	-1.3	-1.2	0.9	-4.7	7.2	6	-19.5	17	89	86	88	88	0.6	0.8	0.6	0.7	8.6	8.2	7.3	8.0
II	-	-	-	-	1.5	4.7	2.7	2.9	5.5	-0.3	9.6	6	-5.8	24	91	81	87	86	0.6	1.8	0.6	1.0	9.2	8.2	7.2	8.2
III	-	-	-	-	0.4	7.0	2.7	3.2	8.2	-2.0	15.5	27	-9.4	4	84	63	77	75	1.0	4.2	1.8	2.5	6.9	6.2	4.8	6.0
IV	-	-	-	-	4.9	12.5	7.0	7.8	13.9	1.9	26.3	30	-5.9	15	85	57	80	74	1.4	7.5	2.2	3.7	7.6	6.9	6.0	6.8
V	-	-	-	-	8.9	14.5	9.6	10.6	15.9	4.6	26.3	19	-1.8	6	80	57	80	72	2.4	8.3	2.6	4.4	6.2	7.3	5.8	6.4
VI	-	-	-	-	16.0	22.0	16.5	17.8	24.2	9.9	31.5	19	4.7	28	79	58	82	73	4.0	12.0	3.7	6.6	5.3	6.3	5.4	5.7
VII	-	-	-	-	17.1	22.7	17.6	18.8	24.2	13.1	35.4	8	7.9	29	85	64	85	78	3.2	12.2	3.4	6.3	7.0	7.0	6.7	6.9
VIII	-	-	-	-	14.1	19.4	14.3	15.5	21.4	10.5	27.2	11	5.1	31	92	71	89	84	1.3	6.9	1.8	3.3	7.0	7.7	4.2	6.3
IX	-	-	-	-	9.1	14.8	10.6	11.3	16.2	6.5	27.8	9	-2.3	26	92	75	90	86	1.0	5.0	1.3	2.4	7.0	7.9	6.2	7.0
X	-	-	-	-	6.2	12.4	7.9	8.6	13.4	4.2	21.5	19	-2.1	3	94	77	91	87	0.6	3.6	1.0	1.7	8.1	7.6	4.7	6.8
XI	-	-	-	-	3.1	6.2	3.7	4.2	7.1	1.0	16.6	6	-8.8	30	90	81	87	86	0.7	2.0	1.0	1.2	9.0	7.2	8.4	8.2
XII	-	-	-	-	-2.3	-0.1	-1.8	-1.5	0.8	-5.2	6.7	13	-16.5	17	92	88	89	90	0.4	0.7	0.6	0.6	8.7	8.7	7.2	8.2
Rok	-	-	-	-	6.4	11.4	7.5	8.2	12.6	3.3	35.4	8.VII	-19.5	17.I	88	72	85	82	1.4	5.4	1.7	2.8	7.6	7.4	6.2	7.1

Smolice

$\varphi = 51°42'$ $\lambda = 17°11'$

I	-	-	-	-	-1.3	1.2	-0.8	-0.4	-	-3.1	-	-	-12.8	17	88	84	89	87	0.7	1.1	0.6	0.8	8.2	7.6	6.1	7.3
II	-	-	-	-	1.5	5.3	2.5	3.0	-	0.3	-	-	-3.6	27	92	79	91	87	0.6	2.0	0.7	1.1	7.1	6.6	6.0	6.6
III	-	-	-	-	4.6	7.6	5.8	6.2	-	0.1	-	-	-4.3	4,10	88	67	84	80	0.9	3.9	1.4	2.1	5.3	5.0	4.0	4.8
IV	-	-	-	-	5.1	11.9	7.4	8.0	-	2.4	-	-	-4.9	13	87	58	79	75	1.2	6.8	2.3	3.4	5.8	6.5	4.2	5.4
V	-	-	-	-	9.1	14.6	10.1	11.0	16.3	5.3	26.5	19	-1.8	7	79	51	73	68	2.8	9.0	3.6	5.1	4.7	6.1	4.3	5.0
VI	-	-	-	-	15.8	21.9	16.9	17.9	24.0	11.0	30.9	11	5.4	1	77	54	78	70	4.4	13.1	4.6	7.4	5.1	5.5	4.0	4.9
VII	-	-	-	-	17.5	22.2	17.8	18.8	23.9	14.3	33.8	5	9.0	3	84	64	84	77	3.5	11.1	3.7	6.1	6.5	6.9	6.6	6.7
VIII	-	-	-	-	14.4	19.5	15.0	16.0	21.2	11.4	27.2	11	6.2	23	89	65	86	80	1.9	8.3	2.5	4.2	6.5	7.0	3.7	5.7
IX	-	-	-	-	9.8	15.4	11.4	12.0	16.9	7.9	28.0	8	-0.6	27	92	67	87	82	0.9	6.3	1.8	3.0	7.3	6.6	5.4	6.4
X	-	-	-	-	6.2	13.0	7.9	8.8	13.9	4.4	21.5	19	-1.4	2	95	70	92	86	0.6	4.8	0.9	2.1	7.2	6.2	2.8	5.4
XI	-	-	-	-	3.5	7.0	4.3	4.8	7.9	2.0	17.6	5	-7.2	30	89	77	87	84	0.8	2.8	1.0	1.5	7.5	7.5	7.5	7.5
XII	-	-	-	-	-2.0	0.6	-1.1	-0.9	1.6	-3.8	8.4	8	-17.7	17	89	88	89	89	0.5	0.7	0.6	0.6	7.6	7.0	6.4	7.0
Rok	-	-	-	-	6.8	11.7	7.9	8.6	-	4.4	-	-	-17.7	17.XII	87	69	85	80	1.6	5.8	2.0	3.1	6.6	6.5	5.1	6.1

Głogów

$\varphi = 51°40'$ $\lambda = 16°04'$

I	-	-	-	-	-0.5	1.6	-0.3	0.1	2.3	-2.3	10.4	6	-13.3	17	-	-	-	-	-	-	-	-	7.9	8.3	7.7	8.0
II	-	-	-	-	2.3	6.3	3.4	3.8	7.0	1.2	12.9	5	-3.9	27,28	-	-	-	-	-	-	-	-	7.6	8.3	7.9	7.9
III	-	-	-	-	2.2	8.4	4.1	4.7	9.6	1.0	16.4	13	-4.4	1,11	-	-	-	-	-	-	-	-	6.1	5.7	3.9	5.2
IV	-	-	-	-	5.3	12.2	6.8	7.8	13.5	2.3	24.9	28	-3.1	14	-	-	-	-	-	-	-	-	5.6	5.5	5.7	5.6
V	-	-	-	-	9.3	14.7	9.8	10.9	16.1	5.0	26.0	19	-0.3	7	70	46	71	62	3.6	9.9	3.5	5.7	4.6	5.3	4.4	4.8
VI	-	-	-	-	15.5	21.8	16.5	17.6	23.2	11.2	30.6	30	5.4	15	77	52	74	68	4.3	13.8	5.2	7.8	4.1	4.5	3.3	4.0
VII	-	-	-	-	17.5	22.0	18.0	18.9	23.4	14.7	32.5	5	10.1	3	83	67	84	78	3.8	10.3	3.6	5.9	6.3	6.0	6.4	6.2
VIII	-	-	-	-	14.7	19.8	14.9	16.0	21.1	11.9	27.8	11	7.1	23	85	64	85	78	2.6	8.7	2.6	4.6	5.9	5.3	3.9	5.0
IX	-	-	-	-	10.8	15.8	11.4	12.4	17.0	8.3	29.3	8	0.6	27	86	66	85	79	1.8	6.7	2.1	3.5	6.9	6.3	5.5	6.2
X	-	-	-	-	7.7	13.9	8.8	9.8	14.6	5.5	21.9	10	-0.5	2	88	67	86	80	4.3	5.5	1.7	2.8	6.6	4.7	3.2	4.8
XI	-	-	-	-	3.5	6.8	4.4	4.8	7.7	2.0	16.9	5	-6.9	30	87	77	88	84	1.1	2.5	1.0	1.5	7.3	8.2	6.1	7.2
XII	-	-	-	-	-1.3	0.9	-0.5	-0.4	2.0	-3.2	9.0	8	-19.2	17	-	-	-	-	-	-	-	-	7.5	7.5	6.0	7.0
Rok	-	-	-	-	7.2	12.0	8.1	8.8	13.1	4.8	32.6	5.VIII	-19.2	17.XII	-	-	-	-	-	-	-	-	6.4	6.3	5.3	6.0

Łódź – Lublinek

$H_s = 184\ m$ $H_b = 186.8\ m$ $h_w = 11\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D, °=D																	OPAD R			LICZBA DNI (n)																
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v		=	≥25	◔	●	■
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min ≤0°	Max ≤0°	Min ≤-10°	Max ≥25°	0.1 ÷ 1	1 ÷ 10	10 ÷ 100	10 ÷ 15	≥15						
I	4	4.0	8	6.4	2.5	5.6	9.5	3.9	14.5	4.4	27.5	5.2	22	6.4	6	5.2	2	5.2	21.4	6.4	6	24	11	4	·	15	4	·	4	·	10	·	4	20	21
II	4.5	4.7	2.5	2.6	6.5	4.5	10.5	5.0	19	6.1	15.5	5.5	14.5	6.7	7	6.1	5	5.3	48.1	8.6	8.18	13	1	·	·	20	15	·	5	·	6	·	1	15	4
III	5	6.2	8	3.5	16.5	5.7	14	6.0	9.5	6.7	8	5.9	16.5	7.6	9.5	6.1	6	5.7	25.0	9.6	15	19	1	·	·	7	4	·	10	2	1	·	5	11	·
IV	2.6	4.2	7	4.4	9.5	3.6	6	3.8	1.0	3.2	5.5	4.5	5	4.6	1.4	4.2	7	3.7	30.2	8.6	30	8	·	·	1	14	8	·	1	·	3	3	3	11	1
V	19.5	4.2	1.8	4.3	1.4	3.9	4.5	4.2	6	2.8	2	4.0	9.5	5.9	11.5	4.6	8	3.9	22.3	6.4	20	3	·	·	1	6	5	·	1	·	1	2	1	8	·
VI	7.5	4.4	1.3	3.3	1.3	3.1	6.5	3.8	9.5	3.8	7.5	5.4	1.5	5.1	1.1	4.7	7	3.8	34.3	12.6	24	·	·	·	10	9	6	2	1	·	1	7	5	6	·
VII	8.5	2.5	6	3.7	12.5	3.7	5	2.8	7.5	4.2	13.5	4.6	17.5	5.3	13.5	5.0	9	3.8	258.1	82.4	16	·	·	·	14	17	18	8	2	·	1	18	3	12	·
VIII	5.5	3.8	0.5	2.0	4.5	2.8	8	3.6	10.5	4.2	1.6	5.1	2.2	3.8	1.3	4.3	1.3	3.5	54.9	12.0	10	·	·	·	3	11	10	3	·	·	1	4	·	5	·
IX	4.5	2.1	·	·	7.5	2.7	5.5	3.5	12.5	4.6	21.5	5.8	25.5	6.1	5	4.5	8	4.5	78.3	14.2	24	2	·	·	2	19	12	3	7	1	3	·	1	8	·
X	1	7.0	0.5	1.0	7.5	2.8	1.1	3.0	2.3	3.6	2.3	3.8	12.5	4.8	3.5	3.7	1.1	3.3	7.8	2.7	20	1	·	·	·	8	4	·	1	·	5	·	4	5	·
XI	3.5	7.7	9	5.8	2.7	4.5	12.5	4.2	8.5	4.1	6	7.1	1.2	8.1	3.5	8.6	8	5.1	22.9	5.0	2	12	2	·	·	8	6	·	8	·	2	·	2	19	·
XII	6	3.5	6	6.0	9.5	3.6	1.1.5	3.6	9.5	4.2	25.5	6.0	1.0	5.6	7	2.9	9	4.3	32.0	5.7	8	29	9	4	·	17	1.0	·	4	·	9	·	1	19	12
Rok	91.5	4.3	78.5	3.6	123.5	3.9	104.5	4.0	1.40	4.3	171.5	5.2	1.62	5.8	104.5	5.0	93	4.3	635.3	82.4	16.VII	111	24	8	31	151	100	14	44	3	43	26	30	130	86

Łódź – Ruda Pabianicka

$H_s = 181\ m$ $h_w = 18\ m$

I	·	·	6	5.2	8	5.7	5.5	3.6	9.5	2.2	38.5	4.5	21.5	6.0	1	6.0	3	4.6	30.4	7.0	6	25	12	4	·	18	6	·	1	·	11	·	1	20	21
II	3.5	2.6	3	1.7	9	3.9	11	3.9	14.5	4.2	20.5	3.8	16.5	6.5	5	3.3	1	4.2	53.7	14.0	8	14	2	·	·	21	14	1	1	·	8	·	·	20	5
III	4.5	4.3	8	3.6	25.5	6.0	9	5.3	7.5	4.9	8.5	4.8	17	7.5	6	5.5	7	5.2	30.4	11.0	15	21	1	·	·	9	5	1	6	2	6	·	4	11	1
IV	1.0	4.0	7	1.7	1.3	3.5	9.5	3.3	2.5	3.4	2.5	3.4	11	3.9	27.5	3.8	2	3.2	24.9	5.0	3.0	11	·	·	1	14	9	·	1	·	6	3	2	13	1
V	13.5	3.5	11.5	3.7	19	3.3	6.5	2.8	3.5	3.7	5	5.4	10.5	5.4	17.5	4.1	6	3.6	28.6	12.4	20	2	·	·	2	10	5	1	1	·	5	1	·	8	·
VI	7.5	2.3	8.5	3.4	16	2.7	8.5	3.1	8.5	2.8	12	3.9	13	5.4	10	4.4	8	3.3	47.8	16.4	24	·	·	·	11	13	7	1	·	·	4	6	3	7	·
VII	4	1.8	3	2.5	13.5	3.9	7.5	3.0	2	3.5	21	4.1	19	4.2	15	4.3	8	3.5	246.2	91.1	16	·	·	·	14	19	15	7	·	·	3	7	1	11	·
VIII	1.5	1.7	2	1.0	6.5	2.9	8.5	3.3	3.5	4.6	22	4.5	27	3.9	8	3.7	1.4	3.2	66.4	15.6	10	·	·	·	4	15	9	3	2	·	12	4	·	6	·
IX	1.5	1.7	2.5	1.8	3.5	2.3	6.5	3.4	7.5	6.1	2.4	5.6	23.5	6.3	9	3.4	12	4.4	80.1	13.5	29	2	·	·	2	22	15	3	4	·	16	·	1	12	·
X	·	·	2	1.0	10.5	2.8	1.1	3.0	1.4.5	2.4	2.6	3.5	2.1	3.6	5	3.4	3	3.0	6.9	2.7	20	2	·	·	·	9	2	·	1	·	2.1	·	1	11	·
XI	4	5.4	6.5	3.5	3.1	4.1	17.5	4.2	5	2.8	5.5	4.5	15.5	6.9	4	6.5	1	4.6	22.8	5.0	2.28	13	2	·	·	10	6	·	3	·	12	·	2	24	·
XII	3.5	2.0	3.5	3.7	1.2	3.7	1.0	3.0	1.0	3.4	27.5	5.7	14.5	4.8	8	2.6	4	4.0	44.4	9.9	14	29	9	6	·	24	9	·	4	2	18	·	1	20	17
Rok	53.5	2.4	63.5	2.7	167.5	3.7	111	3.5	86.5	3.7	213	4.5	210	5.4	116	4.2	74	3.9	682.6	91.1	16.VII	119	26	10	34	184	102	17	24	4	128	21	15	168	46

Smolice

$H_s = 107\ m$ $h_w = 14\ m$

I	1	2.0	5	4.2	3	2.3	2	1.0	5	2.0	2.3	1.7	2.3	2.3	6	3.7	2.5	1.7	2.9.0	5.8	6.12	22	–	2	·	12	7	·	·	·	11	·	3	15	15
II	1	2.0	9	2.6	2	1.0	9	2.3	1.4	2.6	2.5	2.8	1.3	2.8	1	6.0	1.0	2.3	56.2	15.2	18	11	–	·	·	17	8	2	·	·	8	·	3	9	·
III	1	1.8	3	2.0	1.7	3.7	1.2	2.9	1.1	3.3	8	2.4	1.7	3.5	6	1.8	1.5	2.5	39.9	11.4	17	16	–	·	·	9	7	1	1	·	8	·	8	9	1
IV	1.2	3.0	8	3.0	8	2.5	1	3.5	1	1.0	7	2.1	7	3.0	1.6	2.4	2.7	1.9	26.6	16.5	27	11	–	·	·	9	5	1	·	·	7	1	1	5	·
V	9	3.2	2.1	3.3	7	2.5	3.5	2.2	1	3.5	4.5	2.8	9	2.7	1.2	2.6	2.4	2.1	22.5	12.2	6	2	·	·	1	8	5	1	·	·	·	·	1	6	·
VI	3	3.0	11.5	2.3	10.5	1.7	6	1.8	1.5	1.7	15.5	2.5	12.5	3.4	8.5	3.0	2.1	1.9	61.5	28.3	4	·	·	·	13	11	8	1	·	·	3	2	8	5	·
VII	5	1.5	3.5	2.3	8.5	2.2	2.5	1.4	5	2.3	13.5	2.1	19.5	3.0	11.5	2.9	2.4	1.8	133.5	42.6	23	·	·	·	11	20	17	3	·	·	1	7	2	15	·
VIII	·	·	1.5	1.0	2.5	1.0	6.5	2.4	2	2.5	2.8	2.5	2.1	2.9	5.5	2.9	2.6	1.8	84.0	15.1	24	·	·	·	3	14	13	4	·	·	2	5	1	4	·
IX	·	·	·	·	·	·	2	1.0	8.5	2.3	2.4	2.8	2.3	3.3	4.5	2.1	2.8	1.9	69.5	12.6	29	1	·	·	1	19	13	3	·	·	4	·	2	9	·
X	·	·	·	·	4.5	1.2	4	2.4	1.4.5	2.7	2.0.5	2.8	1.2	2.9	4.5	2.3	3.9	1.5	6.2	2.2	18	2	·	·	·	7	3	·	·	·	13	·	4	5	·
XI	1.5	2.0	10.5	2.8	2.2	2.5	10.5	1.8	3.5	1.7	7.5	2.4	13.5	3.2	4	4.8	1.5	2.2	11.2	3.6	25	8	2	·	·	11	4	·	·	·	8	·	2	4.8	·
XII	3	2.2	7.5	2.0	3.5	2.1	7.5	2.1	2.5	2.0	2.1	2.5	1.5.5	3.4	6.5	2.4	2.6	1.8	45.9	8.9	8	23	8	3	·	15	11	·	·	·	6	·	1	13	16
Rok	39.5	1.7	80.5	2.1	88.5	1.9	71.5	2.1	66.5	2.3	197.5	2.4	1.88	3.0	83	3.1	2.80	2.0	586.0	42.6	23.VII	96	–	5	–	152	101	16	1	·	68	15	46	113	84

Głogów

$H_s = 77\ m$ $h_w = 10\ m$

I	2	2.5	4	2.8	1	1.0	1	1.0	·	·	5.5	2.4	1.6	3.5	1	3.0	1.5	2.2	1.4.0	3.1	3	2.0	7	2	·	14	5	·	·	·	–	–	3	2.1	–
II	·	·	·	·	1.1	1.4	1.1	1.5	7	1.9	3.6	1.9	9	3.2	·	·	1.0	1.7	29.1	9.3	18	9	·	·	·	1.8	9	·	1	1	–	–	1	1.6	–
III	·	·	·	·	2.1	1.2	1.3	3.4	4	1.2	1.8	3.1	1.7	2.9	9	1.6	1.1	2.3	47.9	15.5	28	1.4	·	·	·	8	7	1	·	·	–	–	9	1.0	–
IV	4	2.0	9	1.4	6	1.0	3	1.3	·	·	7	2.9	1.2	1.9	1.8	2.1	3.1	1.2	34.8	21.1	7	11	·	·	·	9	2	1	·	·	6	–	2	5	–
V	8	1.4	5	1.0	3	1.0	·	·	·	·	6	1.5	2.2	1.6	7	1.1	4.2	0.8	29.1	16.5	19	2	·	·	2	6	5	1	·	·	2	–	8	5	–
VI	1	1.0	3	1.0	3	1.0	3	1.0	·	·	7	1.0	2.0	1.5	6	1.0	4.7	0.6	68.9	–	–	·	·	·	10	11	6	3	·	·	1	–	9	3	–
VII	1	1.0	·	·	4	1.5	1	1.0	1	1.0	1.6	1.8	2.1	1.9	4	1.8	4.5	0.9	144.3	32.0	23	·	·	·	10	13	12	5	·	·	·	–	2	9	–
VIII	0.5	1.0	·	·	3	1.3	·	·	1.5	1.0	2.5.5	1.3	1.5.5	1.5	2	1.0	4.5	0.7	67.4	18.9	16	·	·	·	3	11	10	2	·	·	·	–	6	4	–
IX	1	1.0	·	·	·	·	·	·	2.5	1.4	2.9	1.5	2.4.5	2.1	2	2.0	3.1	1.2	87.9	13.6	21	·	·	·	2	1.4	1.3	3	·	·	6	–	2	8	–
X	·	·	·	·	0.6	1.0	0.5	1.0	2	1.0	2.5	1.4	1.4	1.8	·	·	5.1	0.6	5.4	3.6	19	1	·	·	·	4	1	·	·	·	1.6	–	4	3	–
XI	2	1.2	7.5	1.5	6.6	1.0	3.5	1.8	3	2.2	1.9	1.9	8.5	2.9	1	2.0	4.1	1.0	9.0	2.8	8	1.1	1	·	·	5	3	·	·	·	1.6	–	3	1.6	–
XII	1	1.0	2	1.0	1	1.0	·	·	3	1.7	2.9	1.8	1.0	1.9	1	2.0	4.6	0.9	49.4	11.7	14	2.2	5	3	·	15	1.1	1	·	·	7	–	1	1.8	–
Rok	20.5	1.0	30.5	0.7	6.0	1.1	3.6	0.9	2.4	1.0	2.7.0.5	1.9	1.8.7.5	2.2	5.1	1.5	4.1.5	1.2	5.8.2.2	–	–	5.0	1.3	5	2.7	1.2.6	8.4	1.7	1	1	–	–	5.0	1.1.8	–

Sielec Stary

$\varphi = 51°39'$ $\lambda = 17°09'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min.	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dzie
I	–	–	–	–	-4.3	1.5	-0.7	-0.3	2.6	-3.4	9.9	8	-13.8	17	–	–	–	–	–	–	–	–	9.5	8.6	7.5	8.5
II	–	–	–	–	4.4	5.7	2.3	2.9	6.6	-0.1	11.1	5	-4.6	27	–	–	–	–	–	–	–	–	9.0	8.0	7.8	8.3
III	–	–	–	–	1.6	8.0	3.6	4.2	9.7	-0.3	16.6	13	-6.0	11	–	–	–	–	–	–	–	–	7.6	6.1	7.0	6.9
IV	–	–	–	–	4.9	12.8	7.2	8.0	14.4	1.4	24.9	28	-5.5	13	–	–	–	–	–	–	–	–	6.2	6.5	7.2	6.6
V	–	–	–	–	9.0	15.2	9.5	10.8	16.4	4.9	26.3	19	-2.5	7	–	–	–	–	–	–	–	–	6.8	6.2	6.3	6.4
VI	–	–	–	–	15.1	22.0	15.7	17.1	23.8	10.3	34.2	11	4.6	1	–	–	–	–	–	–	–	–	6.9	5.8	6.4	6.4
VII	–	–	–	–	17.5	22.4	17.2	18.6	24.0	13.5	34.0	5	8.2	3	–	–	–	–	–	–	–	–	7.3	7.2	8.0	7.5
VIII	–	–	–	–	14.6	19.9	14.5	15.9	21.6	11.0	28.0	11	5.8	23	–	–	–	–	–	–	–	–	7.5	7.3	6.7	7.2
IX	–	–	–	–	9.9	15.5	11.1	11.9	17.1	7.6	28.1	8	-0.4	27	–	–	–	–	–	–	–	–	8.1	7.5	7.8	7.8
X	–	–	–	–	6.0	13.4	7.3	8.5	14.2	3.8	22.0	19	-1.3	2	–	–	–	–	–	–	–	–	9.2	7.6	6.3	7.7
XI	–	–	–	–	3.4	7.1	4.2	4.7	8.2	1.8	17.9	5	-7.2	30	–	–	–	–	–	–	–	–	8.0	7.9	7.4	7.8
XII	–	–	–	–	-2.2	0.6	-1.3	-1.0	1.9	-4.8	9.4	8	-19.3	17	–	–	–	–	–	–	–	–	8.0	8.0	6.3	7.4
Rok	–	–	–	–	6.7	12.0	7.6	8.5	13.4	3.8	34.0	5.VII	-19.3	17.XII	–	–	–	–	–	–	–	–	7.8	7.2	7.1	7.4

Ostrów Wlkp.

$\varphi = 51°39'$ $\lambda = 17°49'$

I	–	–	–	–	-1.4	1.4	-0.5	-0.2	–	–	–	–	–	–	85	83	87	85	0.8	1.2	0.8	0.9	8.7	7.8	6.3	7.6
II	–	–	–	–	1.6	5.4	3.0	3.2	–	–	–	–	–	–	87	74	85	82	0.9	2.4	1.1	1.5	5.9	7.1	5.7	6.2
III	–	–	–	–	1.6	7.8	4.0	4.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	4.0	5.1
IV	–	–	–	–	5.5	12.4	7.5	8.2	–	–	–	–	–	–	81	54	76	70	1.8	7.8	2.6	4.1	5.7	7.0	4.9	5.9
V	–	–	–	–	9.6	15.2	10.4	11.4	–	–	–	–	–	–	74	50	73	66	3.3	9.7	3.7	5.6	5.2	6.4	4.6	5.4
VI	–	–	–	–	16.5	22.6	17.3	18.4	–	–	–	–	–	–	73	52	74	66	5.2	14.1	5.3	8.2	5.0	5.2	4.4	4.9
VII	–	–	–	–	18.2	22.6	18.1	19.2	–	–	–	–	–	–	80	64	83	76	4.7	11.8	4.1	6.9	6.5	6.5	6.9	6.7
VIII	–	–	–	–	14.7	20.3	15.4	16.4	–	–	–	–	–	–	84	59	85	76	2.7	10.2	2.7	5.2	6.5	7.2	5.4	6.4
IX	–	–	–	–	10.1	15.5	11.4	12.1	–	–	–	–	–	–	88	68	85	80	1.6	6.5	2.2	3.4	7.4	8.0	6.3	7.2
X	–	–	–	–	6.5	12.8	8.4	9.0	–	–	–	–	–	–	90	71	87	83	1.0	4.7	1.5	2.4	6.4	7.2	4.5	6.0
XI	–	–	–	–	3.5	6.9	4.4	4.8	–	–	–	–	–	–	87	75	84	82	1.1	3.0	1.4	1.8	7.4	8.0	7.8	7.7
XII	–	–	–	–	-2.0	0.5	-1.1	-0.9	–	–	–	–	–	–	86	82	86	86	0.7	1.1	0.7	0.8	7.4	7.9	6.8	7.4
Rok	–	–	–	–	7.0	12.0	8.2	8.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.0	5.6	6.4

Żary

$\varphi = 51°38'$ $\lambda = 15°08'$

I	–	–	–	–	-0.8	1.4	-0.3	0.0	2.6	-2.6	11.7	6	-13.7	17	93	84	91	89	0.5	1.2	0.6	0.8	7.6	7.5	6.5	7.2
II	–	–	–	–	2.2	5.6	2.9	3.4	6.9	0.8	13.2	5	-3.2	25	89	78	89	85	0.8	2.1	0.9	1.3	7.8	8.2	6.2	7.4
III	–	–	–	–	2.1	8.2	4.9	5.0	10.2	0.9	17.7	13	-5.4	2	86	62	80	76	1.1	4.7	1.9	2.6	5.5	6.1	4.8	5.4
IV	–	–	–	–	5.2	12.6	7.5	8.2	14.2	2.6	25.0	28	-3.6	14	87	51	74	71	1.2	7.8	2.8	3.9	5.2	6.0	4.2	5.1
V	–	–	–	–	8.8	14.7	9.6	10.7	16.5	4.4	26.6	16	-1.1	9	77	52	77	69	2.8	8.9	2.8	4.8	5.7	6.5	4.0	5.4
VI	–	–	–	–	15.6	22.2	16.7	17.8	24.0	11.5	32.2	30	6.6	26	80	58	78	72	3.8	13.2	4.6	7.2	4.6	5.6	4.8	5.0
VII	–	–	–	–	16.7	21.7	17.9	18.6	23.5	14.2	33.5	4	9.8	28	88	68	84	80	2.5	10.0	3.5	5.3	6.5	6.8	7.1	6.8
VIII	–	–	–	–	13.4	19.3	14.3	15.3	21.0	11.2	27.9	11	6.4	23	94	65	87	81	1.4	8.3	2.3	4.0	6.7	7.3	4.7	6.2
IX	–	–	–	–	10.0	15.3	10.8	11.7	16.8	7.6	28.5	8	-0.7	27	92	69	89	83	1.1	6.0	1.6	2.9	7.0	7.1	5.6	6.6
X	–	–	–	–	7.5	13.4	8.8	9.6	14.5	6.0	20.8	9	-1.5	3	93	71	88	84	0.8	4.8	1.5	2.4	7.1	6.2	4.2	5.8
XI	–	–	–	–	3.3	6.4	4.2	4.5	7.7	2.1	16.1	5	-8.3	30	93	82	91	89	0.5	2.1	0.8	1.1	7.9	7.8	7.5	7.7
XII	–	–	–	–	-1.5	0.6	-0.8	-0.6	2.1	-3.5	10.6	8	-15.7	16	93	87	94	90	0.4	0.8	0.5	0.6	7.9	7.7	6.3	7.3
Rok	–	–	–	–	6.9	11.8	8.0	8.7	13.5	4.6	33.5	4.VII	-15.7	16.XII	88	69	85	81	1.4	5.8	2.0	3.1	6.6	6.9	5.5	6.3

Leszkowice

$\varphi = 51°37'$ $\lambda = 16°19'$

I	–	–	–	–	-0.9	1.5	-0.2	0.0	2.5	-2.7	10.8	6	-14.6	17	–	–	–	–	–	–	–	–	7.9	7.9	5.1	7.0
II	–	–	–	–	2.1	6.2	3.3	3.7	6.6	0.8	11.9	5	-4.1	27	–	–	–	–	–	–	–	–	7.3	7.0	6.1	6.8
III	–	–	–	–	1.5	8.4	4.4	4.7	9.2	0.4	15.8	26	-6.8	6	–	–	–	–	–	–	–	–	5.5	4.9	3.3	4.6
IV	–	–	–	–	4.3	12.4	7.4	7.9	13.5	2.1	24.5	28	-2.8	13,19	–	–	–	–	–	–	–	–	5.4	5.2	3.3	4.6
V	–	–	–	–	8.8	14.9	10.3	11.1	16.3	4.1	26.3	18	-1.3	7	–	–	–	–	–	–	–	–	4.8	6.2	3.8	4.9
VI	–	–	–	–	15.7	21.7	17.0	17.8	23.3	11.0	33.2	30	6.1	15	–	–	–	–	–	–	–	–	5.0	4.8	4.2	4.7
VII	–	–	–	–	17.1	21.9	18.4	19.0	23.7	14.5	32.5	4,5	10.0	3	–	–	–	–	–	–	–	–	6.7	6.5	6.8	6.7
VIII	–	–	–	–	14.3	19.7	15.7	16.4	21.2	11.5	28.0	11	6.8	23	–	–	–	–	–	–	–	–	5.9	7.2	6.2	6.4
IX	–	–	–	–	10.2	15.5	12.0	12.4	17.0	7.9	29.0	8	0.0	26	–	–	–	–	–	–	–	–	6.6	7.1	4.6	6.1
X	–	–	–	–	7.0	13.5	8.8	9.5	14.9	4.9	22.0	19	-1.2	2	–	–	–	–	–	–	–	–	7.0	6.1	2.0	5.0
XI	–	–	–	–	3.3	7.1	4.5	4.8	8.2	1.8	16.9	4,5	-8.7	30	–	–	–	–	–	–	–	–	6.9	6.7	6.7	6.8
XII	–	–	–	–	-1.7	0.7	-0.5	-0.5	1.9	-3.7	9.1	8	-20.9	17	–	–	–	–	–	–	–	–	7.2	7.5	5.9	6.9
Rok	–	–	–	–	6.8	12.0	8.4	8.9	13.2	4.4	33.2	30.VI	-20.9	17.XII.	–	–	–	–	–	–	–	–	6.4	6.4	4.8	5.9

Sielec Stary

$H_s = 110\ m$ $h_w = 11\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, v m/s] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0°	Min<-10	Max>25°	Opad R 0.1 ΔR	1.0 ΔR	10.0 ΔR	Wiatr v 10 ΔR	v 15 ΔR	≥1.0	≥5.0	◔	●	▦
I	3	2.0	4	5.5	5	1.7	2	2.2	1.5	1.9	26.5	3.5	27.5	5.1	3	5.3	7	3.4	24.4	5.2	12	23	6	2	·	15	7	·	1	·	5	·	·	20	-
II	·	·	6	2.3	3.5	2.4	6	2.4	24.5	3.0	16.5	2.9	13.5	4.5	4	3.3	10	2.8	42.1	14.8	18	17	·	·	·	16	9	1	2	·	4	·	·	17	-
III	1	3.0	9	2.6	20.5	3.1	7.5	3.2	9.5	3.3	7	3.6	20.5	5.5	9	3.1	9	3.3	35.6	10.2	17	16	·	·	·	9	6	1	3	·	4	·	1	13	-
IV	13	3.0	18	2.8	6.5	1.9	3	2.7	2.5	2.4	2.5	4.0	1.4	2.7	10.5	2.9	20	2.2	38.6	28.4	27	11	·	·	·	7	6	1	·	·	1	2	2	7	-
V	9	2.6	22	2.7	5.5	1.9	2.5	1.4	1	1.0	3	3.0	16.5	4.0	17.5	3.1	16	2.5	30.0	11.0	6	4	·	·	1	8	5	2	·	·	·	1	2	11	-
VI	6	1.7	17	1.8	6.5	1.8	3.5	2.1	2.5	2.6	7.5	3.7	2.6	3.7	11	2.3	9	2.4	73.0	17.7	4	·	·	·	12	12	10	3	1	·	·	3	4	13	-
VII	3	1.7	5.5	2.8	3.5	2.7	4	1.8	2.5	1.4	11.5	3.2	3.4	3.6	8	2.5	21	2.4	153.1	42.5	23	·	·	·	12	22	17	4	·	·	1	5	2	19	-
VIII	1.5	1.3	1.5	2.3	1.5	3.0	2.5	2.0	3.5	2.0	15.5	3.3	4.0	3.0	7	2.9	20	2.3	98.2	25.6	14	·	·	·	5	14	13	3	·	·	5	3	3	12	-
IX	5	1.4	·	·	·	·	·	·	6	2.4	24.5	3.4	30.5	4.9	9	2.7	15	3.1	72.8	13.2	29	2	·	·	2	18	13	3	1	·	8	·	·	16	-
X	0.5	2.0	·	·	·	·	6	1.9	1.7	2.3	26.5	3.2	25.5	3.1	5.5	2.0	12	2.4	5.8	1.8	18	3	·	·	·	7	3	·	·	·	22	·	·	18	-
XI	1.5	6.7	6	4.4	1.5	3.3	18.5	2.8	7	2.7	7	4.1	16	7.7	3	7.0	16	5.8	10.2	3.2	28	8	2	·	·	12	4	·	3	·	7	·	2	20	-
XII	1.5	2.3	5	2.5	14	2.2	2.5	2.6	13.5	2.1	2.3	4.2	2.0	5.0	9.5	2.8	4	3.3	42.1	8.8	14	25	7	4	·	15	12	·	2	·	9	·	1	17	-
Rok	44	2.3	94	2.5	83.5	2.0	58	2.1	104.5	2.3	171	3.5	284	4.4	97	3.4	159	2.8	625.9	42.5	23.VII	109	15	6	32	455	105	18	13	·	60	16	17	183	-

Ostrów Wlkp.

$H_s = 126\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.1	6.5	5	-	-	-	-	11	6	·	-	-	-	·	2	16	7
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	39.1	10.7	18	-	-	-	-	13	9	1	-	-	-	·	1	7	·
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.2	10.5	17	-	-	-	-	8	7	1	-	-	-	·	9	8	1
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14.0	3.4	24	-	-	-	-	10	5	·	-	-	-	1	4	3	·
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.4	27.6	20	-	-	-	-	7	4	1	-	-	-	2	3	6	·
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.8	12.5	24	-	-	-	-	10	6	1	-	-	-	6	5	5	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	148.8	26.1	16	-	-	-	-	19	15	5	-	-	-	10	4	15	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	68.9	16.6	14	-	-	-	-	14	13	2	-	-	-	6	1	10	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	67.9	17.5	29	-	-	-	-	18	13	2	-	-	-	1	1	11	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.9	3.6	18	-	-	-	-	5	4	·	-	-	-	·	5	6	·
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	12.0	3.8	27	-	-	-	-	8	4	·	-	-	-	·	2	18	·
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	38.7	9.8	14	-	-	-	-	12	8	·	-	-	-	·	1	12	9
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	524.8	27.6	20.V	-	-	-	-	135	94	13	-	-	-	26	38	123	17

Żary

$H_s = 157\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	38.5	10.1	5	19	7	2	·	18	12	1	-	-	4	·	3	15	20
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	69.3	10.9	8	10	·	·	·	19	15	1	-	-	8	·	·	12	1
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.1	18.5	17	14	·	·	·	11	10	3	-	-	5	·	9	10	1
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19.5	4.9	19	9	·	·	·	10	5	·	-	-	2	1	4	6	1
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	65.8	26.2	19	5	·	·	2	11	6	3	-	-	4	3	4	8	·
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.2	12.3	23	·	·	·	13	12	9	3	-	-	1	5	6	6	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	198.1	49.8	22	·	·	·	10	22	16	6	-	-	3	8	2	12	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	93.2	26.7	9	·	·	·	3	19	13	2	-	-	8	6	2	7	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	83.1	12.2	29	1	·	·	1	21	13	2	-	-	7	·	·	7	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9.1	3.1	19	1	·	·	·	10	5	·	-	-	9	·	4	7	·
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.8	6.7	25	8	1	·	·	15	6	·	-	-	13	·	2	18	·
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	74.2	23.8	8	24	6	4	·	17	10	2	-	-	7	·	2	15	11
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	808.7	49.8	22.VII	91	14	6	29	185	120	25	-	-	71	23	38	124	34

Leszkowice

$H_s = 81\ m$ $h_w = 10\ m$

I	2	2.5	4	6.8	3	4.5	4	1.6	8	2.9	26.5	3.8	2.9	5.2	0.5	4.0	16	3.5	25.0	3.5	6	20	7	2	·	17	12	·	·	·	-	·	4	14	-
II	2	2.5	1.5	1.3	4.5	3.2	13.5	2.8	1.8	3.0	21.5	4.1	14.5	5.9	4.5	1.7	7	3.4	45.1	12.2	18	9	·	·	·	17	10	1	·	·	-	·	·	8	-
III	3	3.0	2	2.0	11.5	5.3	1.4	3.0	1.2	4.5	9.5	2.4	19.5	5.1	3.5	3.6	1.8	3.3	45.3	11.2	28	13	4	·	·	8	8	2	1	·	-	·	11	8	-
IV	6	3.8	8	2.2	6.5	2.3	4.5	1.8	2.5	2.6	7	3.4	13.5	2.4	9	3.6	3.3	1.8	25.5	7.3	24	11	·	·	·	8	7	·	·	·	-	·	9	4	-
V	5	5.6	1.6	3.0	7	2.4	4.5	2.1	3.5	1.9	3	3.3	2.3	4.8	8	2.9	2.3	2.7	32.5	19.2	19	3	·	·	2	5	3	1	1	·	-	2	3	4	-
VI	4.5	2.4	8.5	2.3	8.5	2.6	4	2.1	7	1.7	7.5	4.3	2.2	4.4	2	3.2	2.6	2.3	100.6	36.0	4	·	·	·	10	11	9	4	·	·	-	5	6	5	-
VII	1	4.0	6	1.9	5.5	2.8	5.5	2.2	5.5	2.1	3.6	2.6	1.5	4.7	3.5	5.7	1.5	2.6	163.3	34.1	10	·	·	·	11	17	16	6	·	·	-	7	3	14	-
VIII	·	·	·	·	·	·	6	3.2	1.0	3.8	45.5	3.2	13.5	3.4	1	2.5	1.7	2.7	68.7	22.7	14	·	·	·	4	11	10	2	·	·	-	2	·	·	-
IX	·	·	·	·	0.5	1.0	4.5	2.1	7.5	3.5	3.3	4.5	2.0	5.5	1.5	4.7	2.3	3.4	98.4	18.5	29	·	·	·	1	17	16	3	·	·	-	1	3	6	-
X	·	·	·	·	·	·	4	1.5	7	2.0	3.3	4.1	1.3	4.5	·	·	3.6	2.3	8.7	3.0	19	2	·	·	·	6	4	·	1	·	-	·	4	4	-
XI	2	3.0	6	5.2	17.5	4.5	16.5	3.1	4	2.4	12	6.2	11	7.5	4	5.0	17	3.9	10.1	6.0	28	9	·	·	·	8	2	·	1	·	-	·	4	16	-
XII	·	·	7	3.9	4	1.8	4	3.2	5	3.6	24	5.0	19	4.7	9	4.1	2.1	3.3	32.5	6.6	8	22	7	4	·	15	10	·	2	·	-	·	2	12	-
Rok	25.5	2.2	59	2.4	68.5	2.5	85	2.4	90	2.8	258.5	3.9	213	4.8	43.5	3.4	25.2	2.9	655.8	36.0	4.VI	89	18	6	28	140	107	19	6	·	-	17	49	93	-

Nowe Miasto n. P.

$\varphi = 51°37'$ $\lambda = 20°35'$

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZachmurzenIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.4	0.0	-1.2	-1.2	1.5	-3.7	6.9	6,9	-16.0	16	89	84	89	87	0.5	1.1	0.6	0.7	8.8	8.7	8.7	8.7
II	–	–	–	–	1.2	4.7	2.6	2.8	6.0	–	10.4	21	–	–	90	79	88	86	0.7	2.0	1.0	1.2	8.8	8.2	9.0	8.7
III	–	–	–	–	-0.1	6.0	2.9	2.9	7.9	-1.4	16.7	31	-8.4	4	85	63	79	76	0.9	4.1	1.8	2.3	5.0	5.0	5.4	5.1
IV	–	–	–	–	4.9	12.9	7.6	8.2	14.4	–	27.4	29	–	–	87	54	80	74	1.2	8.4	2.3	4.0	5.5	4.9	5.3	5.2
V	–	–	–	–	8.9	14.4	9.7	10.7	15.9	–	26.1	19	–	–	84	51	83	76	1.8	7.5	2.2	3.8	5.7	6.1	6.0	5.9
VI	–	–	–	–	16.2	23.2	17.3	18.5	24.8	–	32.0	11	–	–	79	51	74	68	4.0	14.9	5.3	8.1	4.0	4.3	3.6	4.0
VII	–	–	–	–	17.0	22.8	17.9	18.5	24.6	–	35.0	5,8	–	–	86	66	85	80	2.6	11.3	3.4	5.8	5.7	5.8	5.7	5.7
VIII	–	–	–	–	13.9	20.1	14.9	16.0	21.7	–	30.5	12	–	–	93	68	89	83	1.2	8.2	1.9	3.8	4.6	5.2	5.7	5.2
IX	–	–	–	–	9.5	15.5	11.4	12.0	17.1	–	28.4	9	–	–	93	69	88	83	0.8	6.2	1.7	2.9	4.9	5.4	3.7	4.7
X	–	–	–	–	6.0	12.7	8.1	8.7	14.0	–	21.4	19	–	–	95	70	89	85	0.5	4.9	1.2	2.2	7.0	4.9	3.7	5.2
XI	–	–	–	–	2.6	6.3	3.5	4.0	7.5	–	19.4	4	–	–	91	80	90	87	0.6	2.2	0.8	1.2	7.9	6.7	7.5	7.4
XII	–	–	–	–	-2.8	-0.2	-2.1	-1.7	1.3	–	8.9	9	–	–	89	85	89	88	0.6	0.9	0.5	0.7	7.9	7.4	6.3	7.2
Rok	–	–	–	–	6.2	11.6	7.7	8.3	13.0	–	35.0	5,8.VII	–	–	89	69	85	81	1.3	6.0	1.9	3.1	6.3	6.0	5.9	6.1

Sieradz

$\varphi = 51°36'$ $\lambda = 18°44'$

I	–	–	–	–	-1.5	0.9	-1.1	-0.7	1.5	-3.6	8.4	6	-14.4	17	–	–	–	–	–	–	–	–	7.8	6.5	5.9	6.7
II	–	–	–	–	1.7	5.2	2.8	3.1	5.7	0.0	9.3	9,13	-4.4	24	–	–	–	–	–	–	–	–	8.9	6.4	6.4	6.6
III	–	–	–	–	1.5	7.3	3.7	4.0	8.7	-0.7	14.9	14	-6.0	10	–	–	–	–	–	–	–	–	5.6	4.8	4.0	4.8
IV	–	–	–	–	6.0	12.3	7.2	7.9	13.5	2.1	25.4	30	-5.0	14	–	–	–	–	–	–	–	–	5.3	5.4	4.9	5.2
V	–	–	–	–	9.4	15.1	10.3	11.3	16.1	4.4	27.1	19	-1.7	7	–	–	–	–	–	–	–	–	4.8	6.0	5.1	5.3
VI	–	–	–	–	16.8	22.2	16.8	18.2	24.1	10.4	30.9	11	5.4	1	–	–	–	–	–	–	–	–	3.8	4.5	4.2	4.2
VII	–	–	–	–	17.6	22.7	17.7	18.9	24.1	13.7	35.5	8	9.0	29	86	66	87	80	3.3	11.3	2.9	5.8	6.0	6.3	6.5	6.3
VIII	–	–	–	–	14.9	19.8	14.8	16.1	21.5	11.1	27.9	11	6.0	31	87	65	86	79	2.3	8.6	2.4	4.4	4.6	6.4	3.8	4.9
IX	–	–	–	–	9.9	15.3	11.1	11.8	16.4	7.2	27.5	9	-1.0	27	90	69	86	82	1.2	6.3	1.9	3.1	5.8	6.5	5.7	6.0
X	–	–	–	–	6.5	12.6	8.1	8.8	13.6	4.2	20.5	19	-1.2	3	92	72	88	84	0.8	4.5	1.3	2.2	5.9	5.8	4.1	5.3
XI	–	–	–	–	3.3	6.6	4.0	4.5	7.4	1.4	16.5	6	-8.0	30	89	79	87	85	0.8	2.5	1.0	1.4	6.9	6.6	7.3	6.9
XII	–	–	–	–	-2.0	0.0	-1.4	-1.2	1.3	-4.6	7.3	8	-15.0	17	89	87	89	88	0.5	0.8	0.6	0.6	7.8	7.3	6.6	7.2
Rok	–	–	–	–	6.9	11.7	7.8	8.6	12.8	3.8	35.5	8.VII	-15.0	17.XII	–	–	–	–	–	–	–	–	5.9	6.0	5.4	5.8

Sabieszyn

$\varphi = 51°36'$ $\lambda = 22°10'$

I	–	–	–	–	-2.7	-0.9	-1.7	-1.8	0.5	-4.2	6.3	6,9	-17.6	17	–	–	–	–	–	–	–	–	8.2	8.9	7.6	8.2
II	–	–	–	–	0.8	3.5	1.8	2.0	4.8	-0.4	9.3	14	-6.7	28	87	81	87	85	0.9	1.6	0.9	1.1	8.9	8.3	6.5	7.9
III	–	–	–	–	-1.2	4.6	1.7	1.7	6.4	-2.5	15.7	14,30,31	-10.1	3,4	80	61	74	72	1.1	3.9	1.9	2.3	5.2	5.0	3.8	4.7
IV	–	–	–	–	5.2	12.6	8.3	8.6	14.2	3.3	25.6	30	-5.1	10	84	50	70	68	1.7	8.8	3.6	4.7	5.2	5.0	4.3	4.8
V	–	–	–	–	9.0	13.5	10.3	10.8	15.1	6.3	23.2	18	0.7	7	82	62	78	74	2.2	6.9	2.9	4.0	6.3	7.5	5.4	6.4
VI	–	–	–	–	15.6	22.2	17.4	18.2	24.1	11.3	30.1	11,19	6.5	27	78	48	70	65	4.0	14.5	6.1	8.2	4.9	5.0	4.9	4.9
VII	–	–	–	–	16.8	22.0	17.9	18.6	23.9	14.2	32.1	5	9.5	29	85	62	83	77	2.9	11.2	3.6	5.9	5.6	6.4	6.5	6.2
VIII	–	–	–	–	14.0	19.8	16.0	16.4	21.8	11.8	29.7	12	5.7	24	91	62	82	78	1.5	9.4	3.4	4.8	6.1	6.4	4.4	5.6
IX	–	–	–	–	10.0	14.9	11.7	12.1	16.5	8.3	27.1	9	0.8	26	90	68	85	81	1.2	6.1	2.1	3.1	6.5	6.9	5.0	6.1
X	–	–	–	–	5.9	12.0	8.1	8.5	12.9	4.9	19.2	19	-1.2	3	90	70	85	82	1.0	4.3	1.7	2.3	6.4	5.7	4.5	5.5
XI	–	–	–	–	2.5	5.8	3.4	3.8	7.0	1.2	16.7	4	-9.2	30	90	81	89	87	0.7	2.0	0.8	1.2	7.8	7.7	6.9	7.5
XII	–	–	–	–	-3.2	-0.9	-2.3	-2.2	0.4	-5.2	8.7	13	-15.4	16,17	86	83	87	85	0.7	0.9	0.6	0.7	7.1	7.2	6.5	6.9
Rok	–	–	–	–	6.1	10.8	7.7	8.1	12.3	4.1	32.1	5.VII	-17.6	17.I	–	–	–	–	–	–	–	–	6.5	6.7	5.5	6.2

Szprotawa

$\varphi = 51°34'$ $\lambda = 15°32'$

I	–	–	–	–	-1.2	1.3	-0.6	-0.3	2.1	-3.1	11.1	6	-15.3	17	89	80	90	86	0.7	1.4	0.7	0.9	7.8	8.0	6.5	7.4
II	–	–	–	–	1.6	5.9	2.6	3.2	6.7	0.1	13.7	5	-5.2	23	91	77	91	86	0.6	2.3	0.7	1.2	8.4	8.8	7.7	8.3
III	–	–	–	–	1.4	8.5	4.3	4.6	10.0	0.2	17.7	13	-6.9	2	88	62	81	77	0.9	4.9	1.8	2.5	5.9	5.6	4.6	5.4
IV	–	–	–	–	4.6	12.4	7.2	7.8	13.8	1.8	24.2	28	-4.5	13,14	88	51	79	73	1.0	8.0	2.2	3.7	5.5	5.9	4.8	5.4
V	–	–	–	–	8.4	14.7	9.6	10.5	16.3	4.0	25.3	16	-1.7	7	78	54	78	69	2.5	9.0	2.7	4.7	5.1	7.0	4.9	5.7
VI	–	–	–	–	15.6	22.0	16.5	17.6	23.6	10.9	32.1	30	5.4	1	78	54	76	69	4.2	13.6	4.8	7.5	6.0	6.0	5.5	5.5
VII	–	–	–	–	17.1	22.4	18.0	18.9	23.5	14.4	33.8	5	10.4	19	87	65	85	79	2.9	11.0	3.4	5.8	7.3	6.4	8.0	7.2
VIII	–	–	–	–	13.8	19.5	14.7	15.6	20.9	11.0	26.9	11	6.0	23	92	67	88	82	1.3	8.0	2.2	3.8	7.2	7.5	5.1	6.6
IX	–	–	–	–	9.7	15.7	10.9	11.8	16.8	7.5	28.8	8	-1.0	27	95	69	91	85	0.7	6.1	1.2	2.7	7.1	7.7	6.0	6.9
X	–	–	–	–	6.4	13.7	8.0	9.0	14.3	4.2	24.2	10	-2.4	3	94	70	91	85	0.7	4.9	1.1	2.2	7.5	5.4	4.1	5.7
XI	–	–	–	–	2.5	6.8	3.8	4.3	7.7	1.4	15.9	4	-7.9	30	91	79	90	87	0.7	2.3	0.8	1.3	8.0	8.3	7.7	8.0
XII	–	–	–	–	-1.7	1.1	-0.9	-0.8	1.9	-3.3	9.7	8	-18.8	17	91	83	90	88	0.5	1.2	0.8	0.8	8.5	7.9	6.7	7.7
Rok	–	–	–	–	6.5	12.0	7.8	8.5	13.1	4.1	33.8	5.VII	-18.8	17.XII	88	67	86	80	1.4	6.1	1.8	3.1	6.9	7.0	6.0	6.6

Nowe Miasto n.P. — $H_s = 162\,m$ — $h_w = 17\,m$ — 1957

MIESIĄC	ROZKŁAD WIATRU (=0, ▽=0) N n	N ▽	NE n	NE ▽	E n	E ▽	SE n	SE ▽	S n	S ▽	SW n	SW ▽	W n	W ▽	NW n	NW ▽	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max <0°	Max <0°	Min <-10°	Max >25°	Opad R 0.1 ÷ 0.9 mm	1.0 ÷ 9.9 mm	≥10.0 mm	Wiatr v ≥10 m/s	≥15 m/s	≥1	≥5	≥0	≤0	■
I	·	·	2	2.5	10	3.2	7	2.1	9.5	4.2	12	3.2	38.5	3.0	1	1.0	13	2.3	25.5	6.7	5	23	10	2	·	11	8	·	·	·	–	–	1	26	–
II	7	4.0	1	1.0	5.5	1.9	3.5	2.7	13.5	2.2	10.5	2.1	2.5	3.7	3	4.0	13	2.4	45.5	9.5	18	–	2	–	·	19	14	·	·	·	–	–	·	23	–
III	10.5	4.3	3.5	2.1	2.6	3.8	6	3.3	4	2.4	5.5	1.9	16.5	4.3	10	3.8	12	3.2	32.1	9.0	18	20	3	·	·	8	5	·	3	1	–	–	9	12	–
IV	9	4.1	6	2.5	6.5	2.2	7.5	2.1	3	3.2	5.5	3.5	17	1.8	13.5	2.5	22	2.0	14.7	3.5	30	–	·	–	2	12	8	·	·	·	–	–	9	11	–
V	15.5	3.5	4.5	2.8	9.5	3.4	4	2.8	2	2.5	2	2.2	11.5	4.0	23	3.0	21	2.5	27.9	12.3	10	–	·	–	1	8	3	1	·	·	–	–	7	13	–
VI	10	3.0	6.5	3.2	8	2.8	10	2.2	6	2.3	9	2.8	18.5	4.2	12	3.3	10	2.8	42.1	24.3	24	–	·	–	12	7	6	1	1	·	–	–	12	6	–
VII	5	3.0	5	3.5	10	3.0	9.5	3.1	3.5	3.0	7.5	1.7	24.5	3.0	9	2.8	19	2.3	130.9	36.9	21	–	·	–	14	15	12	6	·	·	–	–	10	13	–
VIII	9.5	1.6	1.5	1.7	4	2.8	3	2.3	0.5	1.0	6.5	2.4	3.3	2.1	1.4	3.3	21	1.8	70.1	19.0	14	–	·	–	6	15	13	1	·	·	–	–	8	8	–
IX	4.5	1.9	5.5	3.4	·	·	·	·	10.5	1.4	1.3	2.7	14.5	4.2	7	3.9	35	1.8	92.1	33.3	23	–	·	–	2	18	12	2	1	·	–	–	5	4	–
X	1.6	2.2	4	1.9	0.5	2.0	0.5	1.0	3.5	2.8	5	1.1	6	2.6	15.5	2.5	42	1.2	2.0	1.1	22	–	·	–	·	3	1	·	·	·	–	–	5	6	–
XI	8.5	3.0	2	3.5	10.5	3.5	5	3.8	4	3.8	3	2.3	4.5	4.8	17.5	3.7	35	2.2	13.3	9.0	28	–	2	–	·	7	3	·	·	·	–	–	3	15	–
XII	11.5	2.6	3.5	2.7	·	·	·	·	1.5	5.3	0.5	2.0	5.5	3.4	14.5	2.7	56	1.1	42.5	15.0	8	–	10	–	·	12	8	1	·	·	–	–	4	15	–
Rok	107	2.8	45	2.6	89.5	2.4	56	2.2	61.5	2.6	80	2.3	215	3.4	140	3.0	301	2.1	538.7	36.9	21.VII	–	27	–	37	133	93	12	5	2	–	–	73	152	–

Sieradz — $H_s = 137\,m$ — $h_w = 14\,m$

I	·	·	·	·	7	4.7	5	1.4	3.4	2.2	8	2.0	3.2	4.4	1	8.0	6	3.0	16.2	3.8	5	24	8	3	·	12	7	·	2	1	–	·	5	14	–
II	3	2.0	1	2.0	7	2.6	8	3.2	3.7	3.7	3	3.7	1.8	4.1	4	4.0	3	3.4	42.5	7.1	10	15	1	·	·	19	12	·	·	·	–	·	2	8	–
III	5	6.0	3	4.0	2.0	4.6	9	8.2	2.5	3.7	2	5.0	2.1	5.9	2	6.0	6	4.8	27.4	11.0	28	17	1	·	·	6	5	1	7	4	–	·	8	7	–
IV	9.5	3.3	2	4.0	10	2.0	6	2.1	2.3	2.2	·	·	23.5	2.8	7	4.4	9	2.4	35.3	8.4	30	10	·	·	4	15	9	·	·	·	–	2	5	10	–
V	4.5	2.7	3	2.0	2.0	2.6	8	1.6	10	2.4	4	1.5	1.6	3.9	14.5	3.0	13	2.4	37.8	18.9	20	3	·	·	1	8	5	1	·	·	–	2	3	8	–
VI	3	2.3	1	1.0	9	2.2	11.5	2.0	26.5	2.9	4	3.0	13	5.0	5	4.0	17	2.5	51.5	18.1	24	·	·	·	13	8	5	3	·	·	–	4	7	3	–
VII	1.5	1.7	·	·	7.5	2.2	7.5	1.5	2.8	1.6	6.5	1.8	2.6	4.2	5	2.9	9	2.4	223.1	84.9	16	·	·	·	15	19	16	8	1	·	–	8	3	9	–
VIII	0.5	4.0	·	·	4	1.8	2.5	3.6	3.4	2.1	9	3.1	28.5	4.5	0.5	4.0	14	2.7	49.8	10.1	16	·	·	·	5	14	10	1	3	·	–	3	4	2	–
IX	·	·	·	·	1	2.0	3	1.7	3.4	3.2	1.0	4.8	24.5	6.6	4.5	7.1	13	4.0	64.7	17.0	29	1	·	·	2	15	9	2	4	1	–	1	2	6	–
X	1	4.0	·	·	·	·	6	1.8	45.5	2.5	10.5	4.8	1.3	5.0	1	6.0	16	2.7	8.6	2.9	20	1	·	·	·	5	4	·	1	·	–	·	4	7	–
XI	4	9.5	·	·	3.2	4.0	9	2.8	1.4	3.6	1	6.0	1.6	11.0	2	13.0	12	5.0	14.5	6.0	28	12	3	·	·	6	4	·	9	1	–	·	4	15	–
XII	1	1.0	·	·	1.4	3.9	4	3.2	3.0	3.2	7	4.9	2.5	5.4	2	3.0	10	3.7	39.2	8.4	30	26	9	4	·	12	9	·	4	2	–	·	3	16	–
Rok	33	3.0	10	1.1	131.5	2.7	79.5	2.8	341	2.8	65	3.4	258.5	5.2	48.5	5.4	128	3.2	610.6	84.9	16.VII	109	22	7	37	139	96	14	31	9	–	20	50	105	–

Sobieszyn — $H_s = 159\,m$ — $h_w = 11\,m$

I	1	2.0	6	3.3	5.5	3.9	4.5	3.2	7	1.4	24	2.8	3.1	3.9	4	3.9	10	2.9	21.3	7.3	6	25	11	6	·	12	5	·	·	·	–	·	·	21	26
II	7.5	1.9	1.5	1.8	1.6	1.7	8	2.2	12.5	3.0	28.5	2.9	12	3.0	3.5	1.9	8	2.4	51.1	6.0	22	14	2	·	·	25	14	·	·	·	–	1	1	15	8
III	10	2.4	10	2.2	15.5	3.9	9.5	4.4	5.5	2.2	7	2.6	12	4.0	11.5	3.1	12	2.8	22.1	9.2	15	10	7	2	·	5	3	·	1	·	–	·	8	5	6
IV	11	1.7	8.5	1.6	7.5	1.5	8	2.0	8.5	1.7	5.5	2.1	6.5	1.2	16.5	1.9	18	1.4	17.7	7.8	30	8	·	·	1	10	4	·	1	–	–	2	7	6	·
V	10	1.9	13	1.5	12	1.3	6.5	1.7	4	1.2	3	1.2	9	2.1	15.5	1.8	20	1.3	39.0	12.5	7	·	·	·	·	11	5	2	·	·	–	1	4	11	·
VI	18	1.2	4.5	1.0	5	1.0	10.5	1.3	7	1.3	8	1.8	2.3	1.9	7	1.3	16	1.2	86.5	56.0	24	·	·	·	10	5	3	1	1	1	–	6	8	5	·
VII	5	1.0	1	1.5	7	1.6	8	1.5	6	1.7	18.5	2.0	16	2.0	7.5	1.8	24	1.3	92.5	25.8	18	·	·	·	13	14	12	4	·	·	–	10	5	12	·
VIII	1.5	1.0	1	1.0	4	1.5	2.5	1.0	9.5	1.8	14.5	2.1	30.5	1.9	7.5	1.6	22	1.4	89.3	30.2	29	·	·	·	4	16	13	3	·	·	–	4	2	5	·
IX	1.5	1.0	·	·	1	2.0	6.5	1.3	7	2.1	18.5	2.2	3.1	4.5	5.5	1.5	19	2.4	60.8	10.4	23	·	·	·	2	18	13	5	2	2	–	·	3	9	·
X	·	·	·	·	1	1.0	9.5	1.4	10.5	1.8	27.5	2.0	18.5	2.9	5	1.7	21	1.8	144	6.0	23	1	·	·	·	8	3	·	·	·	–	·	5	6	·
XI	6.5	1.9	8	2.8	19.5	2.1	16.5	1.9	3	2.8	7	2.6	17	4.4	1.5	6.7	11	2.6	19.7	9.5	28	11	2	·	·	9	6	·	·	·	–	·	5	20	·
XII	14.5	2.2	3	1.2	4.5	2.6	3.5	1.4	6.5	2.4	3.4	3.6	1.0	3.2	3	1.8	14	2.4	26.6	9.4	14	29	13	5	·	13	7	·	·	·	–	·	3	15	19
Rok	78.5	1.8	56.5	1.4	84	2.0	94.6	1.9	87	1.9	196	2.3	216.5	2.9	88	2.4	194	2.0	521.0	56.0	24.VI	105	35	13	30	146	88	13	5	·	–	24	51	130	59

Szprotawa — $H_s = 122\,m$ — $h_w = 14\,m$

I	2	1.5	4.5	4.1	3	5.0	3	1.8	10	2.0	50	3.3	12.5	5.0	1	5.0	7	3.2	26.2	6.2	6	22	9	2	·	15	7	·	·	·	–	6	·	3	17	14
II	8.5	4.8	8.8	3.8	2.5	2.0	11	2.2	13	3.0	35	3.4	7	4.1	1.5	1.0	13	2.5	35.2	6.4	18	12	·	·	·	19	13	·	·	·	–	7	·	1	19	2
III	8.5	3.0	4	5.8	8.5	4.6	18	3.2	7.5	2.6	22	3.6	11.5	4.6	5	2.0	18	3.0	58.1	13.8	29	15	·	·	·	9	8	3	3	·	–	6	·	9	10	2
IV	4.5	2.3	7	2.1	12	2.7	6.5	1.4	1	2.0	12	2.2	9.5	3.1	7.5	3.0	30	1.8	26.0	9.3	7	12	·	·	·	9	6	·	·	·	–	2	1	5	7	·
V	3	2.3	13.6	3.4	6	2.9	7	2.4	1.5	1.5	7	2.3	17	3.3	9	3.1	29	2.0	46.8	16.0	16	4	·	·	1	9	8	2	1	·	–	4	2	6	·
VI	·	·	5	2.9	11	3.2	6.5	2.0	3.5	1.7	15.5	2.1	15.5	3.7	4	2.5	29	1.9	105.5	40.3	30	·	·	·	10	12	10	4	1	·	–	4	6	8	·
VII	1	5.0	4	2.8	3	3.2	7.5	1.8	3.5	2.6	22.5	3.3	2.1	3.4	2.5	3.4	28	2.2	150.8	50.1	28	·	·	·	18	21	11	3	1	·	1	6	4	28	·
VIII	·	·	·	·	3	2.7	4	1.3	2	2.5	52.5	3.1	6.5	3.5	·	·	25	2.2	67.8	13.8	24	·	·	·	2	18	11	1	1	·	5	5	·	7	·
IX	·	·	·	·	1.5	1.7	2	1.5	5.5	3.3	34	4.8	2.1	4.1	1	4.5	25	2.8	104.1	18.2	29	2	·	·	1	18	14	3	2	·	–	5	2	1	14	·
X	·	·	·	·	1	1.0	6.5	1.8	6	2.2	38	3.8	8.5	4.1	1	4.5	32	1.9	8.1	3.8	19	4	·	·	·	8	3	·	·	·	–	1.9	·	3	8	·
XI	2	4.8	2.5	4.0	2.5	3.3	6.5	2.3	1.5	3.7	19	4.4	7.5	6.1	3	5.0	23	2.9	18.7	4.1	8	11	1	·	·	9	4	·	·	·	–	1.4	·	2	17	·
XII	·	·	2	5.2	7	2.9	0.5	1.0	7.5	2.4	35	3.9	11.5	4.4	2.5	4.4	27	2.7	47.4	13.0	8	21	6	3	·	15	7	1	3	·	–	12	·	2	18	10
Rok	13.5	1.6	43	2.7	81.5	2.9	79	1.9	62.5	2.4	342.5	3.2	149	4.1	38	3.2	286	2.4	679.7	50.1	22.VIII	103	18	8	24	181	102	17	12	·	–	27	22	38	151	28

Włodawa

$\varphi = 51°33'$ $\lambda = 23°33'$

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o,m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	992.2	1009.9	984.3	1021.5	-2.8	-0.7	-1.7	-1.7	0.4	-5.3	6.2	6	-16.5	17	85	84	87	84	0.7	1.1	0.7	0.8	8.5	8.6	8.2	8.4
II	990.8	1008.2	969.4	1012.6	0.5	3.3	1.5	1.7	4.4	-1.6	9.5	15	-7.2	27	90	80	87	86	0.7	1.6	0.9	1.1	8.2	8.5	6.0	7.6
III	997.7	1013.1	973.2	1019.7	-1.8	4.4	1.1	1.2	5.9	-4.3	16.4	28	-13.6	3	79	57	73	70	1.2	4.2	1.9	2.4	5.5	5.7	3.8	5.0
IV	996.5	1008.5	972.6	1017.9	5.5	12.8	8.0	8.6	14.0	2.1	26.4	30	-7.4	10	79	50	70	66	2.1	9.1	3.6	4.9	5.3	6.2	4.7	5.4
V	994.0	1004.3	980.5	1015.2	9.6	13.9	10.5	11.1	15.5	5.8	24.3	18	0.1	5,7	82	63	84	75	2.2	6.8	2.5	3.8	6.3	8.0	6.3	6.9
VI	995.7	1008.1	982.0	1016.4	16.2	22.1	16.8	18.0	23.7	10.6	31.6	12	4.8	7	76	52	75	68	4.5	13.3	4.8	7.5	4.7	6.3	4.1	5.0
VII	994.3	1001.1	982.3	1011.8	17.2	23.0	18.1	19.1	24.6	13.2	33.1	5	8.7	29	83	57	80	73	3.6	13.4	4.6	7.2	6.6	7.0	6.0	6.5
VIII	993.3	1001.8	982.4	1014.1	14.4	20.0	15.6	16.4	21.9	10.9	30.0	12	5.0	24	90	63	85	79	1.7	9.3	2.8	4.6	5.6	7.2	4.0	5.6
IX	991.7	1003.1	977.5	1012.8	10.0	15.5	11.3	12.0	16.7	7.4	27.2	9	0.3	26	91	65	87	81	1.1	6.8	1.8	3.2	7.2	7.4	6.1	6.9
X	999.1	1010.5	985.5	1020.6	5.1	12.3	7.4	8.0	13.0	2.9	20.0	19	-2.9	3	92	65	88	82	0.8	5.3	1.3	2.5	6.3	5.9	5.4	5.9
XI	993.9	1021.0	976.4	1021.8	2.4	5.5	3.4	3.7	6.5	0.0	16.6	2	-10.8	30	91	81	89	87	0.6	1.9	0.8	1.1	7.9	8.4	7.4	7.9
XII	993.9	1012.3	957.0	1016.1	-3.7	-0.7	-2.5	-2.4	0.2	-6.6	7.8	13	-17.1	16	88	80	87	85	0.5	1.2	0.7	0.8	6.9	7.2	6.4	6.8
Rok	995.3	1021.0	957.0	1016.7	6.0	11.0	7.5	8.0	12.2	2.9	33.1	5.VII	-17.1	16.XII	86	66	82	78	1.6	6.2	2.2	3.3	6.6	7.2	5.7	6.5

Włowa

$\varphi = 51°30'$ $\lambda = 15°12'$

I	–	–	–	–	-1.0	1.4	-0.7	-0.2	2.6	-3.1	11.4	6	-17.3	17	–	–	–	–	–	–	–	–	8.0	7.6	6.2	7.3
II	–	–	–	–	1.7	6.1	2.4	3.2	6.9	-0.1	13.0	5	-7.4	26	91	79	93	88	0.7	2.1	0.6	1.1	7.8	7.2	6.0	7.0
III	–	–	–	–	1.0	8.9	3.9	4.4	10.6	0.0	18.5	13	-8.3	2	90	66	86	81	0.7	4.5	1.3	2.2	5.4	5.4	4.2	5.0
IV	–	–	–	–	4.2	13.0	6.1	7.4	14.4	1.2	25.0	28	-5.2	13,14	92	56	86	78	0.7	7.5	1.4	3.2	4.9	4.4	3.6	4.3
V	–	–	–	–	8.5	15.1	8.9	10.4	16.8	3.0	26.0	19	-3.0	7	84	53	82	73	1.9	9.1	2.1	4.4	4.9	5.4	4.0	4.8
VI	–	–	–	–	15.8	22.6	15.9	17.6	24.2	9.6	32.6	30	4.3	1	86	59	86	77	2.7	12.7	2.9	6.1	3.9	4.5	4.5	4.3
VII	–	–	–	–	17.0	22.3	18.1	18.9	23.9	13.8	33.7	4	9.9	18	90	58	89	82	2.2	10.5	2.7	5.1	–	–	–	–
VIII	–	–	–	–	14.2	19.8	14.0	15.5	21.4	10.3	27.9	6	3.9	23	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	10.5	15.8	10.7	11.9	17.0	6.4	26.1	8	-2.8	27	93	72	90	85	1.0	5.7	1.4	2.7	–	–	–	–
X	–	–	–	–	6.7	13.8	7.5	8.9	15.0	4.5	22.1	9	-2.8	3	92	70	91	84	0.9	5.1	1.0	2.3	6.7	4.7	3.4	4.9
XI	–	–	–	–	2.7	7.1	3.7	4.3	8.0	1.5	17.0	5	-9.7	30	88	80	90	86	0.9	2.2	0.8	1.3	7.8	7.5	7.1	7.5
XII	–	–	–	–	1.5	1.2	-0.8	-0.5	2.1	-3.3	10.4	8	-17.3	16	–	–	–	–	–	–	–	–	7.6	7.0	6.3	7.0
Rok	–	–	–	–	6.6	12.3	7.5	8.5	13.6	3.6	33.7	4.VII	-17.3	17.I, 16.XII	–	–	–	–	–	–	–	–	–	–	–	–

Wirsko

$\varphi = 51°28'$ $\lambda = 16°37'$

I	–	–	–	–	1.0	0.9	-0.6	-0.3	2.3	-3.2	10.4	6	-13.8	17	–	–	–	–	–	–	–	–	7.8	8.1	6.5	7.5
II	–	–	–	–	1.9	5.1	2.9	3.2	6.5	0.3	11.4	5	-5.1	27	92	80	89	87	0.6	1.9	0.8	1.1	6.5	7.1	6.1	6.6
III	–	–	–	–	4.6	7.3	4.8	4.6	9.3	0.3	16.4	13	-6.4	1	86	64	76	75	1.0	4.1	2.3	2.5	5.6	5.3	5.0	5.3
IV	–	–	–	–	5.0	11.7	7.9	8.1	13.8	2.9	24.9	30	-3.7	13,15	89	56	75	73	1.1	7.0	2.8	3.6	5.1	5.7	4.8	5.2
V	–	–	–	–	8.8	14.1	10.6	11.0	16.0	5.2	25.9	19	-1.3	7	79	54	70	68	2.5	8.2	4.1	4.9	4.7	6.2	5.3	5.4
VI	–	–	–	–	15.1	21.5	17.6	18.0	23.7	11.9	31.5	11	6.3	26	80	55	72	69	3.7	12.4	6.1	7.4	4.6	4.9	4.3	4.6
VII	–	–	–	–	16.8	21.4	18.1	18.6	23.3	14.6	33.3	4	9.5	28	85	69	84	79	3.3	9.5	4.0	5.6	6.4	6.4	7.1	6.6
VIII	–	–	–	–	13.8	19.1	15.8	16.0	20.9	11.8	27.5	11	6.8	23	90	65	82	79	1.7	7.8	3.5	4.3	6.4	6.3	5.5	6.1
IX	–	–	–	–	10.5	14.8	11.8	12.2	16.6	8.6	28.3	8	0.8	27	91	71	86	82	1.3	5.6	2.4	3.1	7.0	7.4	6.3	6.9
X	–	–	–	–	7.4	13.0	9.4	9.8	14.2	6.1	21.5	19	0.4	2	92	71	86	83	0.9	4.7	1.8	2.5	6.5	5.7	3.8	5.3
XI	–	–	–	–	3.9	6.6	4.6	4.9	7.6	2.4	16.9	5	-8.7	30	90	82	89	87	0.8	2.2	0.9	1.3	7.9	7.5	7.3	7.6
XII	–	–	–	–	-1.6	0.6	-0.9	-0.7	1.9	-3.7	9.4	8	-16.3	17	92	89	89	90	0.4	0.7	0.7	0.6	7.3	7.6	6.3	7.1
Rok	–	–	–	–	6.8	11.3	8.5	8.8	13.0	4.8	33.3	4.VII	-16.3	17.XII	–	–	–	–	–	–	–	–	6.3	6.5	5.7	6.2

Osiny

$\varphi = 51°28'$ $\lambda = 22°48'$

I	–	–	–	–	-2.4	-0.7	-1.5	-1.5	0.5	-4.0	6.6	6	-17.3	17	91	86	90	89	0.4	0.8	0.6	0.6	9.3	9.5	8.7	9.2
II	–	–	–	–	0.8	3.7	2.0	2.1	5.1	-0.4	9.7	14	-7.7	24	92	82	90	88	0.5	1.5	0.7	0.9	9.5	9.3	7.9	8.9
III	–	–	–	–	-0.8	4.8	1.9	2.0	6.6	-2.1	15.9	14	-9.2	4	85	62	77	75	1.0	4.0	1.9	2.3	7.0	6.3	4.5	5.9
IV	–	–	–	–	5.4	12.8	8.0	8.6	14.3	2.8	26.3	30	-6.6	15	82	48	75	68	1.8	9.5	3.0	4.8	7.4	7.2	6.2	6.9
V	–	–	–	–	9.2	13.6	10.0	10.7	15.1	5.8	23.3	18	-0.5	29	80	59	78	72	2.5	7.4	2.8	4.2	7.3	8.8	7.1	7.7
VI	–	–	–	–	16.2	22.6	17.4	18.4	24.2	10.8	30.5	11	5.2	7	74	46	70	63	4.8	15.2	6.1	8.7	5.5	6.6	7.0	6.4
VII	–	–	–	–	17.0	23.0	17.6	18.6	23.7	13.8	32.5	5	9.1	29	84	63	84	77	3.2	11.1	3.4	5.9	6.8	7.4	5.3	7.5
VIII	–	–	–	–	14.0	19.6	15.9	16.4	21.6	11.5	29.6	12	6.2	24	90	62	83	78	1.7	9.3	3.1	4.7	7.2	8.2	6.6	7.3
IX	–	–	–	–	10.2	15.0	11.4	12.0	16.6	8.2	26.9	9	-0.2	27	88	64	85	79	1.5	6.7	2.0	3.4	7.2	8.0	7.6	7.6
X	–	–	–	–	6.3	12.2	8.2	8.7	13.1	4.6	19.4	19	-1.3	3	88	66	85	80	1.2	5.1	1.8	2.7	7.1	6.5	6.6	6.7
XI	–	–	–	–	2.8	6.0	3.5	4.0	7.0	1.1	16.4	4	-8.5	30	88	76	86	83	0.9	2.5	1.1	1.5	8.5	7.9	7.4	7.9
XII	–	–	–	–	-3.0	-0.7	-2.2	-2.0	0.5	-5.1	7.7	13	-15.7	16	88	82	87	86	0.6	1.0	0.7	0.8	7.7	8.1	7.2	7.7
Rok	–	–	–	–	6.3	10.9	7.7	8.2	12.4	3.9	32.5	5.VII	-17.3	17.I	86	66	82	78	1.7	6.2	2.3	3.4	7.5	7.8	7.1	7.5

Włodawa

$H_s = 174$ m $H_b = 175{,}5$ m $h_w = 10$ m **1957**

| MIESIĄC | ROZKŁAD WIATRU [%], [m/s] | | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | | |

Nowa Wieś

$\varphi = 51°27'$ $\lambda = 22°45'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies		II	III	Dies
I	–	–	–	–	-2.7	-0.9	-4.7	-4.8	0.3	-4.5	8.1	6	-17.2	17	90	87	91	89	0.5	0.8	0.5	0.6	8.2	8.0	7.0	7.7
II	–	–	–	–	0.8	3.5	1.7	1.9	4.9	-0.6	9.2	15	-5.9	27	92	82	94	88	0.5	1.5	0.7	0.9	8.5	8.1	6.1	7.6
III	–	–	–	–	-1.4	4.5	1.1	1.3	6.1	-2.8	16.3	31	-11.1	4	–	–	–	–	–	–	–	–	4.9	5.0	3.8	4.6
IV	–	–	–	–	5.3	12.7	7.8	8.4	14.3	3.0	26.5	30	-5.4	10	84	53	75	71	1.6	8.5	2.9	4.3	4.7	5.1	3.6	4.5
V	–	–	–	–	9.1	13.8	9.8	10.6	15.3	6.1	24.4	14	0.1	7	84	63	82	76	2.0	6.9	2.3	3.7	5.9	7.5	5.8	6.4
VI	–	–	–	–	14.5	21.9	18.1	18.2	24.3	10.9	30.9	12	5.0	21	83	52	78	71	2.9	13.3	4.8	7.0	3.5	4.3	4.1	4.0
VII	–	–	–	–	15.9	22.2	18.6	18.8	24.3	13.8	32.5	5	9.0	7,29	88	59	80	76	2.2	12.0	4.6	6.3	5.4	5.2	6.3	5.6
VIII	–	–	–	–	13.1	19.7	16.1	16.2	21.8	11.6	30.4	12	5.7	24	94	65	82	80	0.9	8.8	3.4	4.4	5.5	6.0	4.6	5.4
IX	–	–	–	–	9.3	15.0	11.5	11.8	16.8	8.1	27.4	9	0.6	27	93	66	86	82	0.8	6.2	1.8	2.9	6.5	6.6	6.0	6.4
X	–	–	–	–	5.8	12.2	7.7	8.4	13.2	4.3	20.0	19	-0.4	3	90	66	87	81	1.0	5.0	1.5	2.5	5.3	5.4	4.8	5.2
XI	–	–	–	–	2.2	5.6	3.2	3.5	6.9	0.8	17.0	4	-9.5	30	93	84	92	90	0.4	1.8	0.6	0.9	7.4	8.0	7.2	7.5
XII	–	–	–	–	-3.5	-0.8	-2.5	-2.3	0.3	-5.6	8.3	13	-16.5	17	90	84	90	88	0.5	0.9	0.5	0.6	7.4	7.0	6.2	6.9
Rok	–	–	–	–	5.7	10.8	7.6	7.9	12.4	3.8	32.5	5.VII	-17.2	17.I	–	–	–	–	–	–	–	–	6.1	6.4	5.5	6.0

Ostrzeszów

$\varphi = 51°26'$ $\lambda = 17°56'$

I	–	–	–	–	-1.1	1.2	-0.6	-0.3	2.0	-3.2	9.2	6	-15.3	17	–	–	–	–	–	–	–	–	8.5	7.5	6.6	7.5
II	–	–	–	–	1.8	5.0	2.8	3.1	5.9	0.2	9.7	14	-5.0	23	–	–	–	–	–	–	–	–	7.0	8.2	6.2	7.1
III	–	–	–	–	1.8	7.5	3.9	4.3	8.9	-0.5	16.5	13	-12.0	1	–	–	–	–	–	–	–	–	6.1	6.2	5.0	5.8
IV	–	–	–	–	5.9	11.8	7.2	8.0	13.3	2.5	25.4	30	-5.3	14	–	–	–	–	–	–	–	–	5.8	6.7	5.5	6.0
V	–	–	–	–	9.3	14.2	9.4	10.6	15.8	4.7	25.7	19	-1.5	7	–	–	–	–	–	–	–	–	5.4	6.9	4.5	5.6
VI	–	–	–	–	16.2	22.0	16.9	18.0	24.1	11.6	30.8	30	5.6	27	–	–	–	–	–	–	–	–	4.7	5.7	4.2	4.9
VII	–	–	–	–	17.5	22.0	17.8	18.8	24.0	14.4	35.6	5,8	10.7	28	–	–	–	–	–	–	–	–	6.4	7.3	6.5	6.7
VIII	–	–	–	–	14.4	19.1	15.2	16.0	21.3	11.3	28.2	11	6.4	23	–	–	–	–	–	–	–	–	5.8	7.4	4.6	5.9
IX	–	–	–	–	9.9	15.3	11.5	12.0	16.7	7.8	27.5	8,9	-1.5	27	–	–	–	–	–	–	–	–	6.5	7.5	5.8	6.6
X	–	–	–	–	7.0	12.8	8.9	9.4	13.9	5.2	20.6	19	-0.2	2	–	–	–	–	–	–	–	–	6.5	6.3	3.9	5.6
XI	–	–	–	–	3.6	6.7	4.5	4.8	7.5	1.9	17.8	5	-9.2	30	–	–	–	–	–	–	–	–	7.5	7.7	8.1	7.8
XII	–	–	–	–	-1.9	0.4	-0.8	-0.8	1.8	-4.1	8.7	13	-16.5	17	–	–	–	–	–	–	–	–	7.4	7.5	7.0	7.3
Rok	–	–	–	–	7.0	11.5	8.1	8.7	12.9	4.3	35.6	5.8.VII	-16.5	17.XII	–	–	–	–	–	–	–	–	6.5	7.1	5.7	6.4

Złoczew

$\varphi = 51°25'$ $\lambda = 18°36'$

I	–	–	–	–	-2.0	0.2	-1.6	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.9	6.1	7.2
II	–	–	–	–	1.4	4.7	2.3	2.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.6	5.3	6.4
III	–	–	–	–	1.1	7.2	3.3	3.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.3	3.6	4.6
IV	–	–	–	–	4.6	12.5	6.5	7.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.9	5.1	5.4
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	14.5	22.3	16.9	17.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3.3	4.7	3.7	3.9
VII	–	–	–	–	15.7	22.4	18.1	18.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	6.1	6.3
VIII	–	–	–	–	12.9	19.8	15.4	15.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.7	5.0	5.7
IX	–	–	–	–	8.9	15.5	11.0	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.2	6.2	6.5
X	–	–	–	–	6.1	12.9	7.7	8.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.1	4.2	5.5
XI	–	–	–	–	3.1	6.7	3.7	4.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	7.2	7.1
XII	–	–	–	–	-2.1	0.1	-1.4	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.4	6.4	6.9
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Radom – Wacyn

$\varphi = 51°25'$ $\lambda = 21°07'$

I	998.9	1010.0	982.5	1012.0	-2.3	0.0	-1.4	-1.3	0.9	-3.9	8.8	6	-16.4	17	91	85	90	89	0.5	1.0	0.5	0.7	9.0	8.5	8.0	8.5
II	989.8	1009.4	966.4	1012.4	1.2	4.6	2.3	2.6	5.9	0.1	10.7	6	-5.7	28	92	80	88	87	0.6	1.9	0.9	1.1	8.2	8.4	6.6	7.7
III	–	–	–	–	-0.1	6.4	2.4	2.8	7.7	-1.4	16.9	28	-8.2	4	85	57	76	73	1.0	4.7	1.9	2.5	6.4	5.9	4.7	5.7
IV	996.0	1007.5	972.6	1014.1	5.4	12.9	7.7	8.4	14.4	3.4	27.5	30	-3.8	15	85	52	77	71	1.5	8.9	2.7	4.4	5.9	6.0	4.5	5.5
V	994.0	1004.0	982.9	1014.9	9.1	14.0	9.9	10.7	15.5	5.9	23.4	20	-0.6	27	80	58	78	72	2.4	8.0	3.0	4.5	6.6	7.8	6.6	7.0
VI	995.2	1009.3	984.0	1016.6	16.2	23.0	16.5	18.0	24.7	12.0	34.1	19	6.3	7	76	48	75	66	4.6	15.3	4.8	8.2	4.9	5.0	3.9	4.8
VII	–	–	–	–	17.4	22.5	17.7	18.8	24.3	14.4	34.8	8	10.3	29	84	66	84	78	3.4	14.0	3.5	6.0	6.4	7.0	6.9	6.8
VIII	993.1	1002.8	980.6	1014.6	14.1	20.3	15.2	16.2	21.9	11.7	31.0	12	6.2	24	90	62	86	79	1.6	11.0	2.4	4.7	5.6	6.8	4.8	5.7
IX	991.5	1004.0	976.2	1014.3	9.9	15.6	11.2	12.0	17.1	8.3	29.0	9	1.1	26	92	66	87	82	1.0	6.9	1.8	3.2	6.4	7.3	5.8	6.7
X	998.4	1009.8	983.6	1020.6	6.2	12.8	7.9	8.7	13.5	4.9	21.6	19	-0.2	3	93	69	89	84	0.6	5.0	1.2	2.3	6.5	6.2	5.2	5.9
XI	999.0	1018.1	981.4	1021.6	2.8	6.4	3.9	4.2	7.3	1.4	16.1	6	-9.6	30	91	78	88	86	0.7	2.4	1.0	1.4	8.4	7.2	6.9	7.5
XII	993.3	1011.5	956.0	1016.3	-2.8	-0.3	-2.0	-1.8	0.7	-4.9	7.8	14	-17.9	16	92	84	90	89	0.4	0.9	0.6	0.6	7.9	8.1	7.3	7.8
Rok	–	–	–	–	6.4	11.5	7.6	8.3	12.8	4.3	34.8	8.VII	-17.9	13.XII	88	67	84	80	1.5	6.5	2.0	3.5	6.6	7.1	5.9	6.6

Nowa Wieś

$H_s = 179\ m$ $h_w = 11\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, %nD)																		OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max 0° V	Max 5° V	Max -10° V	Max > 25°	0,1 ÷ 1,0	1,0 ÷ 10,0	> 10,0	10 ÷ 15	> 15	=	≤ 0,5	◔	●	▦
I	0,5	3,0	3	2,7	4,5	4,8	8,5	4,2	3	4,5	16	27	28	34	20,5	5,2	9	3,5	22,8	8,0	6	26	14	6	·	10	5	·	2	·	2	18	17
II	4,5	2,8	4	2,2	·	·	3	2,5	10	3,8	2,5	3,3	23	4,1	5,5	3,4	9	3,1	35,1	5,5	3,22	13	2	·	·	17	10	·	2	·	5	·	1	14	3
III	9	4,4	5,5	3,5	6,5	2,8	15,5	5,3	7,5	4,8	8,5	3,0	12,5	4,4	17	5,8	11	4,0	22,0	8,8	15	20	7	1	·	6	5	·	4	·	·	·	10	7	2
IV	8,5	2,9	8	2,4	4,5	2,9	12,5	1,8	7,5	1,7	12	1,5	4,5	2,4	16,5	2,6	16	1,8	17,2	4,1	30	6	·	·	2	7	6	·	·	·	·	·	9	7	·
V	15,5	3,4	10,5	2,5	6	2,8	11	3,5	4,5	3,1	7,5	1,5	7	2,4	19	2,6	12	2,4	35,5	8,5	7	·	·	·	·	12	8	·	·	·	·	·	1	11	1
VI	6	4,0	4	2,8	2	1,0	4	1,8	7	1,9	16,5	2,6	17	2,9	16,5	3,2	17	2,2	57,4	32,2	22	·	·	·	12	7	6	1	·	·	3	7	1	·
VII	4	2,5	·	·	2,5	1,4	4,5	1,7	11	1,8	13	1,7	27,5	3,2	11,5	3,7	19	2,1	94,3	33,6	16	·	·	·	13	16	14	1	2	·	4	5	8	·
VIII	3,5	2,3	1	4,0	1	2,0	3	3,0	5,5	2,6	11	1,7	33	2,6	18	3,4	17	2,2	88,2	38,0	29	·	·	·	5	13	10	3	·	·	3	3	·	3	·
IX	3	3,0	2	2,5	·	·	·	·	7	1,7	13,5	2,4	34,5	4,2	12	6,0	18	3,1	63,2	16,4	23	·	·	·	2	15	11	2	3	·	3	·	4	12	·
X	·	·	1	1,0	·	·	1,5	2,3	9,5	1,2	18,5	2,3	31	2,5	13,5	3,7	18	2,0	12,8	7,2	23	1	·	·	·	5	3	·	·	·	1	·	5	7	·
XI	6	9,7	·	·	5,5	3,5	12,5	3,0	12	2,1	9	2,2	15,5	4,3	4,5	5,0	25	2,8	24,3	14,0	2,8	13	2	·	·	9	4	1	2	1	4	·	4	17	1
XII	1,0	2,4	6	2,7	1	2,0	6	1,6	8,5	2,1	16	2,7	29,5	3,1	6	3,0	10	2,4	26,1	9,3	14	28	13	5	·	12	8	·	·	·	2	·	4	14	15
Rok	70,5	3,4	45	2,2	33,5	1,9	82	2,5	93	2,6	166,5	2,3	263	3,3	160,5	4,0	184	2,6	498,9	33,6	16.VII	107	35	12	34	129	90	8	15	1	20	10	52	119	39

Ostrzeszów

$H_s = 198\ m$ $h_w = 10\ m$

I	1	2,0	7	2,9	1	3,0	2,5	2,0	16,5	1,9	2,1	1,9	2,4	3,2	3	6,0	17	2,1	27,1	6,8	5	23	7	2	·	17	7	·	1	·	-	·	3	18	-
II	2,5	2,8	·	·	3	2,7	10,5	2,4	2,8	3,3	14,5	1,8	1,5	3,8	4,5	2,8	6	2,7	46,3	8,5	6,18	10	1	·	·	17	10	·	2	·	-	·	·	10	-
III	2	1,5	1	1,0	2,5	3,4	5,5	3,2	14,5	2,8	9	2,1	1,5	4,7	4	1,2	17	2,6	35,7	10,4	17	15	2	1	·	8	6	1	1	·	-	·	7	12	-
IV	11	2,1	7	1,3	4	2,1	2	2,2	9	3,0	7	2,6	9	3,0	16	2,2	25	1,7	16,3	4,9	22	11	·	·	1	10	6	·	·	·	-	2	6	10	-
V	9,5	2,7	14,5	2,2	9	1,6	2	2,0	6	1,7	3	1,3	21,5	2,9	4,5	2,2	23	1,7	16,1	34,0	20	4	·	·	1	6	6	1	·	·	-	1	4	7	-
VI	1,5	2,0	9	1,1	7	1,1	6	1,4	14	1,4	10	1,9	17,5	2,5	7	1,6	18	1,4	63,3	20,2	24	·	·	·	12	7	6	3	·	·	-	3	8	6	-
VII	2,5	1,8	2	3,0	7	2,1	4,5	1,8	6,5	1,4	16	2,6	23,5	2,4	6	1,5	25	1,6	177,4	58,2	11	·	·	·	14	20	17	7	·	·	-	9	3	16	-
VIII	·	·	·	·	1	3,0	4	2,2	8,5	2,3	15	1,9	27,5	2,1	3	2,5	34	1,4	56,6	11,0	24	·	·	·	3	13	11	1	·	·	-	5	2	7	-
IX	·	·	2	1,0	0,5	1,0	3,5	1,3	20,5	1,9	27,5	2,4	21	3,0	·	·	15	1,9	74,8	11,5	29	2	·	·	2	18	16	1	·	·	-	·	2	10	-
X	·	·	·	·	·	·	1,1	1,7	2,3	2,0	2,2	2,0	1,3	2,8	2	1,0	22	1,6	6,9	2,5	2,0	1	·	·	·	7	2	·	·	·	-	·	6	5	-
XI	2	3,0	5	2,2	23,5	2,6	14	2,1	8,5	2,6	5	2,6	16	4,9	3	6,7	13	2,7	15,5	7,3	2,8	10	3	·	·	6	4	·	1	·	-	·	2	18	-
XII	·	·	5	1,8	8	2,1	1,3	1,6	1,3	2,7	15,5	3,9	21,5	3,1	4	2,0	13	2,3	29,5	9,0	14	24	8	4	·	12	9	·	1	·	-	·	2	16	-
Rok	3,2	1,5	52,5	1,4	8,9	2,1	78,5	2,0	168	2,2	165,5	2,2	224,5	3,2	57	2,5	228	2,0	595,5	38,2	11.VII	100	21	7	33	141	100	14	5	·	-	20	45	135	-

Złoczew

$H_s = 174\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	28,5	8,0	5	-	-	-	-	7	6	·	-	-	10	·	4	16	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	53,4	10,5	18	-	-	-	-	16	11	1	-	-	7	·	1	8	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33,1	12,1	1[illegible]	-	-	-	-	6	5	1	-	-	3	·	9	8	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35,2	10,5	22	-	-	-	-	10	7	1	-	-	3	2	6	11	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	37,9	19,5	24	-	-	-	-	7	5	1	-	-	4	6	9	2	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	269,8	62,5	16	-	-	-	-	15	14	7	-	-	5	4	3	10	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77,5	25,3	10	-	-	-	-	11	11	1	-	-	7	3	1	6	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	64,7	13,8	14	-	-	-	-	14	9	2	-	-	10	·	1	9	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5,8	3,0	2,0	-	-	-	-	3	2	·	-	-	2,1	·	4	6	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27,4	7,0	2,8	-	-	-	-	7	6	·	-	-	1,6	·	4	11	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44,4	9,8	14	-	-	-	-	10	8	·	-	-	1,0	·	3	15	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	62,5	16.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Radom - Wacyn

$H_s = 180\ m$ $H_b = 181,7\ m$ $h_w = 16\ m$

I	4	1,5	5	3,4	3,5	2,6	7	3,2	8	2,2	21,5	4,5	29,5	4,4	5,5	5,1	9	3,5	25,1	5,0	5	24	10	2	·	14	9	·	·	·	·	·	1	23	19
II	8	3,4	·	·	0,5	9,0	8	3,7	20	2,4	15	3,3	16	4,5	5,5	5,0	11	3,0	32,2	4,4	3	13	1	·	·	20	10	·	·	·	5	1	1	15	1
III	13	2,7	10,5	2,6	9	5,1	10,5	2,0	8,5	2,3	6,5	4,3	12	5,4	16	5,2	7	4,0	20,2	9,3	15	20	4	·	·	8	4	·	4	·	2	·	7	10	·
IV	17,5	2,1	4,5	2,2	4	3,0	3,5	4,0	4	3,1	6,5	2,8	9,5	2,0	17,5	2,5	23	1,8	26,0	11,0	30	8	·	·	3	10	6	1	·	·	1	2	5	7	·
V	23,5	2,1	7,5	2,5	3,5	3,1	5,5	2,1	2	1,5	4,5	2,8	12	3,3	19,5	2,8	15	2,2	31,5	13,1	9	1	·	·	1	4	4	2	·	·	2	·	1	14	·
VI	9,5	1,8	2	1,5	3,5	3,4	7,5	4,0	5	3,6	7,5	4,3	22,5	3,7	10,5	2,7	22	2,5	53,5	33,2	24	·	·	·	14	7	5	2	1	1	·	6	7	4	·
VII	9	2,1	3	2,3	3,5	1,7	6,5	2,9	4,5	2,7	8	3,2	22,5	3,2	14	2,6	22	2,1	96,3	22,6	8	·	·	·	14	16	13	3	·	·	1	4	3	18	·
VIII	3,5	2,5	2	1,5	1,5	4,0	2,5	2,4	4	6,2	9,5	4,4	3,1	3,6	1,5	3,3	24	2,7	90,6	25,7	14	·	·	·	7	16	13	2	1	1	1	3	1	7	·
IX	1	4,0	·	·	1,5	3,3	2,5	4,0	5	3,0	16	4,8	29	4,6	1,5	2,6	20	3,1	58,6	11,6	23	·	·	·	2	16	13	2	1	·	2	1	2	12	·
X	3	1,8	1,5	1,7	2,5	3,4	4	3,9	7	3,2	16,5	3,1	27,5	3,4	9	2,4	22	2,4	12,9	4,6	22	1	·	·	·	8	4	·	·	·	4	·	4	8	·
XI	8	3,3	12,5	3,2	1	3,5	1,9	4,1	5	2,5	5	4,2	16	6,0	4,5	3,8	19	3,3	20,0	9,0	29	13	2	·	·	8	5	·	2	·	2	·	2	19	1
XII	6	1,8	·	·	1	1,0	9,5	2,6	9	2,6	17,5	4,4	24,5	4,2	9,5	2,9	16	2,9	39,4	14,8	14	26	10	4	·	15	7	1	2	·	1	·	1	17	18
Rok	10,6	2,2	4,8,5	1,7	3,5	3,6	8,6	3,7	8,2	2,9	13,4	3,8	25,2	4,0	14,1,5	3,4	210	2,8	506,3	33,2	24.VI	108	27	6	41	142	93	13	11	2	21	17	35	152	39

Puławy, IUNiG

$\varphi = 51°25'$ $\lambda = 21°58'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.4	-0.4	-1.3	-1.4	0.7	-3.9	6.2	6,9	-16.0	17	88	82	87	86	0.6	1.0	0.7	0.8	8.6	8.4	8.2	8.4
II	–	–	–	–	0.9	4.2	2.1	2.3	5.5	-0.3	10.2	14	-6.5	24	90	80	86	85	0.7	1.9	1.0	1.2	8.6	8.0	6.7	7.8
III	–	–	–	–	-0.8	5.5	2.1	2.2	7.4	-2.0	17.1	28	-10.0	4	80	56	74	70	1.2	4.7	2.0	2.6	5.5	5.3	3.4	4.7
IV	–	–	–	–	5.3	13.2	8.6	8.9	14.7	3.2	26.8	30	-4.5	15	83	47	68	66	1.8	9.9	3.8	5.2	5.4	5.1	4.1	4.9
V	–	–	–	–	9.2	13.9	10.3	10.9	15.3	6.3	24.1	18	0.5	29	81	60	77	73	2.4	7.6	3.0	4.3	6.3	7.5	5.5	6.4
VI	–	–	–	–	16.3	22.8	17.8	18.7	24.4	11.9	30.1	19	6.5	7	73	47	69	63	5.1	15.2	6.5	8.9	3.8	5.1	4.3	4.4
VII	–	–	–	–	17.3	22.3	18.0	18.9	24.0	14.3	32.8	5	10.5	29	83	64	84	77	3.4	10.5	3.5	5.8	5.8	6.4	7.3	6.5
VIII	–	–	–	–	14.2	20.0	16.0	16.6	21.7	11.8	30.0	12	6.0	24	91	69	86	82	1.6	7.8	2.5	4.0	6.1	6.7	4.9	5.9
IX	–	–	–	–	10.5	15.5	11.5	12.2	16.8	8.4	27.4	9	0.0	27	89	66	86	80	1.4	6.9	1.9	3.4	6.5	6.9	5.7	6.4
X	–	–	–	–	6.0	12.7	8.1	8.7	13.5	4.7	19.8	19	-1.5	3	91	67	87	82	0.9	5.2	1.5	2.5	6.1	5.1	5.0	5.4
XI	–	–	–	–	2.8	6.3	3.5	4.0	7.3	1.5	17.0	4	-8.7	30	88	76	86	83	0.8	2.6	1.1	1.5	7.5	7.5	7.0	7.3
XII	–	–	–	–	-3.1	-0.5	-2.1	-2.0	0.7	-5.1	8.6	13,14	-16.2	16	88	82	88	86	0.6	1.0	0.6	0.7	7.3	7.5	6.3	7.0
Rok	–	–	–	–	6.4	11.3	7.9	8.4	12.7	4.2	32.8	5.VII	-16.2	16.XII	85	66	82	78	1.7	6.2	2.3	3.4	6.5	6.6	5.7	6.3

Puławy – Kępa

$\varphi = 51°25'$ $\lambda = 21°57'$

I	–	–	–	–	-2.4	-0.3	-1.4	-1.4	0.6	-4.5	6.4	6	-17.2	17	85	80	85	83	0.8	1.2	0.9	1.0	9.6	8.7	8.5	8.9
II	–	–	–	–	0.9	4.2	2.0	2.3	5.2	-0.6	9.6	14	-6.7	24	88	75	85	83	0.8	2.1	1.0	1.3	9.4	7.8	7.6	8.3
III	–	–	–	–	-0.9	5.9	1.6	2.0	7.3	-2.6	16.4	28	-10.7	4	82	51	75	69	1.1	5.2	1.8	2.7	6.8	5.5	4.4	5.6
IV	–	–	–	–	5.4	13.4	8.0	8.7	14.6	2.4	27.6	30	-5.5	10	83	45	71	66	1.8	10.4	3.3	5.2	6.1	6.4	4.7	5.7
V	–	–	–	–	9.2	14.1	9.6	10.6	15.6	5.5	24.0	18	-1.3	29	81	56	78	72	2.3	8.5	2.8	4.5	7.0	8.5	6.6	7.4
VI	–	–	–	–	16.4	23.2	17.1	18.4	24.8	10.8	31.4	12	5.5	7	73	44	72	63	5.1	16.5	5.7	9.1	5.2	6.4	5.7	5.8
VII	–	–	–	–	17.3	22.6	17.6	18.8	24.0	14.0	32.9	5	9.4	30	83	60	86	76	3.4	12.2	3.0	6.2	7.3	7.7	7.8	7.6
VIII	–	–	–	–	14.6	20.3	15.6	16.5	21.8	11.5	29.8	12	5.0	24	89	60	86	78	1.9	10.2	2.4	4.8	7.1	7.7	5.6	6.8
IX	–	–	–	–	10.7	15.8	11.4	12.3	17.0	8.4	27.2	9	-0.2	27	89	63	89	80	1.5	7.3	1.5	3.4	7.3	7.5	6.7	7.2
X	–	–	–	–	5.8	12.7	7.8	8.5	13.5	4.3	19.8	19	-1.8	3	91	65	89	82	0.9	5.5	1.2	2.5	7.0	6.4	6.0	6.5
XI	–	–	–	–	2.8	6.5	3.4	4.0	7.3	1.4	16.9	4	-8.6	30	91	78	89	86	0.7	2.4	0.8	1.3	8.9	7.9	7.5	8.1
XII	–	–	–	–	-3.1	-0.4	-2.1	-1.9	0.5	-5.1	8.3	13	-17.6	17	91	82	87	87	0.5	1.0	0.7	0.7	8.6	8.3	7.1	8.0
Rok	–	–	–	–	6.4	11.5	7.6	8.5	12.7	3.8	32.9	5.VII	-17.6	17.XII	86	63	83	77	1.7	6.9	2.1	3.6	7.5	7.4	6.5	7.2

Piotrków Trybunalski

$\varphi = 51°24'$ $\lambda = 19°42'$

I	–	–	–	–	-2.2	0.3	-1.3	-1.1	1.1	-3.6	7.5	6	-15.1	17	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.2	4.6	2.6	2.8	5.3	0.3	9.6	21	-5.0	24	93	84	90	88	0.5	1.8	0.7	1.0	–	–	–	–
III	–	–	–	–	0.3	6.9	2.9	3.2	7.5	-1.2	15.1	14,27	-7.5	4	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	5.5	13.0	7.6	8.4	13.5	3.1	25.8	30	-4.0	15	81	54	72	69	2.0	8.2	3.3	4.5	–	–	–	–
V	–	–	–	–	9.2	14.6	9.6	10.8	15.1	5.6	26.1	19	-0.4	6,7	76	57	75	69	3.0	8.3	3.2	4.8	–	–	–	–
VI	–	–	–	–	15.1	23.2	17.3	18.2	24.1	11.4	31.1	11,30	6.0	27	77	53	76	69	4.1	14.0	5.1	7.7	–	–	–	–
VII	–	–	–	–	16.2	23.1	18.3	19.0	23.9	14.1	34.6	8	9.9	29	86	65	83	78	2.6	11.6	4.0	6.1	–	–	–	–
VIII	–	–	–	–	13.7	20.9	15.3	16.3	21.3	11.5	27.6	11	5.5	31	86	63	85	78	2.2	9.7	2.7	4.9	–	–	–	–
IX	–	–	–	–	9.7	15.7	11.2	12.0	16.3	7.5	27.1	9	0.3	27	87	67	84	79	1.6	6.6	2.1	3.4	–	–	–	–
X	–	–	–	–	6.6	13.4	8.2	9.1	13.6	4.9	20.1	10,19	-1.4	3	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3.1	6.6	3.5	4.2	7.2	1.4	17.6	4	-8.5	30	88	76	88	84	0.9	2.9	1.0	1.6	–	–	–	–
XII	–	–	–	–	-2.3	0.1	-1.4	-1.2	0.9	-4.2	7.1	13	-15.6	17	88	85	89	87	0.8	1.0	0.6	0.7	–	–	–	–
Rok	–	–	–	–	6.3	11.9	7.8	8.4	12.5	4.2	34.6	8.VII	-15.6	17.XII	–	–	–	–	–	–	–	–	–	–	–	–

Pożóg

$\varphi = 51°23'$ $\lambda = 22°04'$

I	–	–	–	–	-2.2	-0.5	-1.2	-1.3	0.5	-3.9	6.0	9	-16.4	17	89	86	89	88	0.6	0.9	0.6	0.7	8.5	8.6	7.8	8.3
II	–	–	–	–	1.2	4.0	2.0	2.3	5.1	-0.2	9.0	14	-6.9	24	90	79	87	85	0.7	1.9	1.0	1.2	8.2	7.0	5.6	6.9
III	–	–	–	–	-0.5	5.1	1.6	2.0	6.4	-2.0	15.5	31	-10.4	4	79	62	79	73	1.3	4.1	1.5	2.3	4.7	4.6	4.1	4.5
IV	–	–	–	–	5.7	12.8	7.7	8.5	14.1	2.8	25.4	30	-4.8	15	81	50	73	68	2.0	9.0	3.2	4.7	5.3	5.5	3.4	4.7
V	–	–	–	–	9.0	13.4	9.0	10.1	14.7	5.6	22.8	18	0.0	29	86	65	86	79	1.8	6.4	1.7	3.3	5.8	7.0	5.2	6.0
VI	–	–	–	–	16.8	22.2	16.0	17.8	23.5	11.1	29.6	12	5.3	21	76	55	79	70	4.7	12.1	4.0	6.9	3.6	4.4	4.0	4.0
VII	–	–	–	–	17.2	22.1	16.7	18.2	23.6	13.3	32.3	5	8.7	7	88	68	90	82	2.5	9.5	2.1	4.7	6.0	6.1	6.5	6.2
VIII	–	–	–	–	14.6	20.0	15.5	16.4	21.6	–	30.3	12	–	–	87	62	83	77	2.3	9.5	3.0	4.9	5.5	6.0	3.9	5.1
IX	–	–	–	–	10.5	15.3	11.2	12.0	16.7	–	27.4	9	–	–	90	66	86	81	1.3	6.5	1.9	3.2	6.0	6.3	5.2	5.8
X	–	–	–	–	6.8	12.3	8.3	8.9	13.1	–	19.8	19	–	–	87	68	84	80	1.4	4.6	1.8	2.7	5.4	4.7	5.1	5.1
XI	–	–	–	–	2.7	6.0	3.1	3.7	6.9	–	16.3	4	–	–	89	78	89	85	0.8	2.4	0.9	1.4	7.0	7.4	6.7	7.0
XII	–	–	–	–	-3.0	-0.6	-2.0	-1.9	0.5	–	8.9	13	–	–	87	84	90	87	0.6	1.0	0.6	0.7	7.1	6.9	7.0	7.0
Rok	–	–	–	–	6.6	11.0	7.3	8.0	12.2	–	32.3	5.VII	–	–	86	69	85	80	1.7	5.7	1.9	3.1	6.2	6.2	5.4	5.9

Puławy, IUNiG — $H_s = 142$ m — $h_w = 12$ m — 1957

MIESIĄC	ROZKŁAD WIATRU (%D, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0°	Min<-10°	Max≥25°	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	▤	▥	◔	●	▦
I	0.5	2.0	3.5	2.6	5	2.5	8	1.5	12.5	1.4	14.5	2.1	26.5	2.5	7.5	3.1	1.5	1.8	27.6	10.4	5	24	14	5	·	13	7	1	·	·	–	·	1	24	22
II	0.5	1.0	0.5	1.0	0.5	1.0	5	2.2	20.5	2.0	16	1.7	11.5	2.0	9.5	2.5	2.0	1.5	48.8	8.1	3	10	2	·	·	22	14	·	·	·	7	1	1	14	4
III	8	2.6	2.5	2.2	7.5	2.5	1.5	3.4	7.5	1.7	5	2.2	6.5	3.5	1.7	3.3	2.4	2.1	20.6	9.1	15	18	5	·	·	5	4	·	3	·	2	·	8	6	1
IV	5.5	1.5	3.5	1.6	5	1.2	6	2.0	7.5	1.8	7.5	1.5	6	1.3	2.5	1.9	2.4	1.2	24.1	7.9	30	5	·	·	2	10	7	·	·	·	1	1	8	6	·
V	6.5	1.5	7.5	1.6	5	1.7	9.5	1.5	3	1.0	1.5	1.0	4.5	1.8	2.7.5	2.1	2.8	1.2	43.3	19.2	7	·	·	·	·	8	4	2	·	·	1	1	4	11	·
VI	7	1.6	3.5	1.6	1	1.0	3	1.7	8	1.5	9.5	1.5	15	2.1	1.5	2.3	2.8	1.3	68.6	47.0	24	·	·	·	12	7	6	2	·	·	·	6	9	4	·
VII	1	1.0	1.5	1.0	1.5	1.7	3	2.0	4.5	1.2	5.5	1.3	17.5	1.5	17.5	2.1	4.1	0.9	119.5	26.3	16	·	·	·	14	17	16	4	·	·	2	12	6	15	·
VIII	2	2.5	1	1.5	2.5	1.4	3	2.0	4	1.6	9.5	1.5	17.5	1.6	17.5	1.9	3.6	1.1	111.5	30.1	29	·	·	·	5	15	11	4	·	·	4	7	2	6	·
IX	0.5	1.0	·	·	0.5	2.0	0.5	2.0	3.5	1.1	9	1.7	28.5	2.1	17.5	2.4	3.0	1.4	55.7	10.6	23	·	·	·	2	17	15	1	·	·	3	·	3	10	·
X	0.5	5.0	·	·	3	2.0	7.5	1.5	7.5	1.3	8.5	1.3	21	1.6	10	2.0	3.5	1.0	16.8	7.8	22	1	·	·	·	7	3	·	·	·	6	·	3	9	·
XI	6.5	3.5	6.5	1.4	1.4	1.9	13.5	2.4	6.5	2.6	3.5	1.3	11	3.0	7.5	3.8	2.1	1.9	18.2	11.4	28	11	2	·	·	7	3	1	1	·	4	·	5	18	·
XII	6.5	1.5	5.5	1.3	4	1.8	7	1.1	11	2.0	1.4	2.3	11	1.8	1.5	2.1	1.9	1.5	33.1	11.9	14	28	10	3	·	13	8	1	1	·	2	·	2	16	19
Rok	3	2.1	35.5	1.3	49.5	1.7	8.1	1.9	9.6	1.6	10.4	1.6	176.5	2.1	186.5	2.5	32.1	1.4	589.8	47.0	24.VII	97	30	8	35	141	98	16	5	·	–	28	52	139	46

Puławy – Kępa — $H_s = 119$ m — $h_w = 13$ m

I	2.5	1.0	8.5	2.7	6	1.8	2	1.2	19.5	1.8	20	2.5	13	3.0	18.5	2.2	3	2.2	27.9	8.7	5	25	11	7	·	10	5	·	·	·	–	·	·	25	–
II	6	1.5	3.5	1.6	2	1.5	4	2.0	27	2.5	17	2.3	12.5	2.8	8	1.9	4	2.2	49.6	7.6	22	15	2	·	·	19	11	·	·	·	–	1	1	18	–
III	12	1.6	9	1.4	17	2.7	9	2.4	9.5	2.9	4	4.9	7.5	3.1	11	2.7	14	2.1	20.2	9.5	15	19	7	1	·	5	4	·	1	·	–	·	6	8	–
IV	17.5	1.3	10.5	1.5	8.5	1.6	4.5	1.7	9	1.9	2	1.7	4.5	1.8	17.5	1.4	1.6	1.3	25.0	7.6	30	8	·	·	4	9	7	·	·	·	–	·	4	7	–
V	23.5	1.9	14	2.2	10.5	1.8	2	1.5	3.5	1.6	4	1.5	3	2.8	19.5	2.3	13	1.7	43.5	18.7	3	1	·	·	·	9	5	2	·	·	–	2	·	13	–
VI	19.5	1.4	8	1.6	·	·	4.5	1.8	13.5	2.1	7	2.1	5.5	4.0	22	1.9	10	1.7	61.3	42.2	24	·	·	·	13	7	6	1	·	·	–	7	3	4	–
VII	13	1.2	10.5	1.5	·	·	4.5	1.7	8	1.8	8	1.7	13.5	2.3	23.5	1.6	12	1.4	106.3	26.8	16	·	·	·	13	18	15	3	·	·	–	10	1	18	–
VIII	6	1.7	6	1.7	3	1.0	4	1.8	9.5	2.0	10.5	2.2	13.5	1.7	30.5	1.5	10	1.5	119.8	29.6	29	·	·	·	5	15	12	5	1	·	–	6	·	9	–
IX	10.5	1.1	0.5	1.0	4	1.0	3	1.3	7.5	2.4	15.5	2.7	22	2.8	20	2.0	7	2.0	60.9	11.3	24	1	·	·	2	16	14	2	·	·	–	·	2	12	–
X	6	1.2	7	1.0	3	1.3	6	1.2	21.5	1.8	13.5	2.3	14	1.7	14	1.6	8	1.5	16.9	7.5	22	1	·	·	·	9	3	·	·	·	–	·	2	9	–
XI	8	3.9	16.5	1.8	14.5	1.9	16.5	1.8	7	1.9	6.5	3.5	9.5	4.0	5.5	2.4	6	2.3	20.4	12.2	28	10	2	·	·	9	5	1	·	·	–	·	2	20	–
XII	10	1.6	8.5	1.4	4.5	1.0	4	1.8	2.3	2.5	22.5	2.5	4	3.9	9.5	2.0	7	2.0	40.0	15.2	14	26	12	4	·	16	10	1	·	·	–	·	1	17	–
Rok	13.4.5	1.6	102.5	1.6	7.3	1.3	6.4	1.7	158.5	2.1	130.5	2.5	122.5	2.8	199.5	2.0	110	1.8	591.8	42.2	24.VI	106	34	12	37	142	97	15	2	·	–	26	22	158	–

Piotrków Trybunalski — $H_s = 200$ m — $h_w = 16$ m

I	7	2.1	3	1.7	2.5	2.2	1.5	2.3	16.5	2.2	17	2.8	40.5	3.0	3	6.3	2	2.7	26.7	5.9	6	23	10	3	·	10	8	·	1	·	7	–	–	–	15
II	10	2.0	1.5	2.3	5	2.0	4.5	2.1	14	1.9	14.5	2.8	26.5	4.0	6	2.8	2	2.8	51.6	9.6	18	13	2	·	·	19	14	·	1	·	1	–	–	–	5
III	12	3.4	7.5	2.4	22	2.9	3.5	2.7	12	2.8	5	5.0	2.3	4.2	2	4.2	6	3.2	27.2	8.1	17	19	3	·	·	7	5	·	2	·	1	–	–	–	3
IV	2.7	2.5	4	2.2	10	2.0	4.5	2.6	8.5	2.5	1	2.0	1.2	2.7	2.1	2.5	2	2.4	19.1	4.8	7	8	·	·	2	9	6	·	·	·	·	–	–	–	·
V	3.1	2.7	8.5	3.0	13.5	2.7	1	8.0	3	2.3	1	7.0	1.9	4.0	1.4	3.9	2	3.2	18.8	8.5	10	2	·	·	1	4	4	·	1	·	·	–	–	–	·
VI	2.0	2.2	5.5	2.7	8	2.0	3	2.8	5.5	3.0	5	3.8	26.5	3.7	9.5	3.8	7	2.8	32.9	18.0	24	·	·	·	12	6	4	1	1	·	·	–	–	–	·
VII	1.8	2.2	6.5	2.0	12	1.8	1.5	2.7	1	3.0	5	3.8	3.5	4.2	1.2	3.8	3	3.1	159.3	62.3	16	·	·	·	13	15	11	5	3	1	·	–	–	–	·
VIII	6	1.5	1	2.0	7	2.3	2	3.0	1	2.0	11.5	3.2	4.7	2.9	1.4.5	2.9	3	2.7	101.2	42.7	16	·	·	·	6	13	12	2	·	·	·	–	–	–	·
IX	7	2.1	1	3.0	2	1.0	1	5.0	1.1	2.8	1.4.5	4.8	4.2.5	4.1	1.0	4.3	1	3.8	65.4	9.8	15	·	·	·	2	1.4	1.4	·	3	·	·	–	–	–	·
X	2	1.5	3	2.0	1.5	2.7	6	2.3	19.5	2.5	1.8	2.9	2.7	3.2	8	2.4	10	2.5	4.5	1.9	2.0	1	·	·	·	4	2	·	·	·	2	–	–	–	·
XI	9	2.3	12.5	3.2	2.0	2.3	5.5	2.7	9.5	2.2	8	2.8	18.5	4.9	2	2.5	5	2.9	19.8	6.1	28	12	2	·	·	9	6	·	1	·	3	–	–	–	·
XII	10.5	2.8	1.5	3.0	1.0	2.0	5	2.8	1.2	2.3	16.5	4.5	19.5	3.8	1.2	2.5	6	3.0	46.9	9.8	14	27	10	3	·	13	10	·	3	·	3	–	–	–	15
Rok	159.5	2.3	54.5	2.5	113.5	2.2	39	3.2	113.5	2.5	115	3.8	337	3.7	114	3.5	49	2.9	573.2	62.3	16.VII	105	27	6	36	123	96	8	16	1	17	–	–	–	38

Pożóg — $H_s = 180$ m — $h_w = 17$ m

I	1.5	5.0	2.5	7.2	5.5	3.6	6.5	4.1	15.5	4.9	29.5	6.1	2.3	6.9	3	5.0	6	5.4	25.7	10.8	5	25	11	5	·	10	6	1	3	1	–	·	3	22	19?
II	5	4.0	2	2.0	·	·	7	4.2	2.4	6.1	27.5	5.5	7.5	5.3	4	6.0	7	4.9	36.8	5.5	7	13	2	·	·	16	12	·	3	·	4	1	1	10	6
III	6	4.6	4	5.4	8.5	7.2	8.5	4.3	12.5	6.4	13	7.1	16.5	6.8	8	6.1	16	5.2	19.7	10.0	15	17	7	1	·	4	4	1	7	2	·	·	8	4	1
IV	8.5	3.8	7.5	4.1	8	2.5	7.5	3.5	8.5	4.2	7	3.9	9	3.4	9	3.8	2.5	2.6	24.7	6.3	30	8	·	·	2	8	7	·	·	·	1	1	9	6	·
V	8.5	4.9	12	4.0	9	3.6	5	3.7	5	3.3	5	4.2	14	5.1	18.5	4.7	18	3.5	62.0	30.0	7	·	·	·	·	8	7	2	2	·	2	1	5	10	·
VI	6.5	3.5	7.5	2.4	0.5	4.0	3.5	3.7	16.5	4.7	13	4.8	18.5	4.5	9	4.5	15	3.6	54.2	36.4	24	·	·	·	10	5	4	2	·	·	·	3	9	3	·
VII	3	2.0	1.5	3.0	6	2.4	9	3.0	11.5	2.9	17	3.5	19	4.6	7	4.4	19	2.8	93.8	28.7	16	·	·	·	11	17	14	2	·	·	·	7	4	14	·
VIII	1	4.0	·	·	3	2.0	1.5	3.7	9	4.9	28.5	4.8	27.5	4.9	7.5	5.1	15	4.0	92.5	30.0	29	–	·	–	4	14	11	4	1	·	2	4	3	4	·
IX	1	4.0	·	·	2	1.5	5	4.4	16	4.8	18	5.3	3.1	6.2	7	4.4	10	4.7	63.2	18.3	23	–	·	–	2	16	14	2	4	·	2	–1	5	7	·
X	0.5	6.0	·	·	·	·	8	3.6	2.7	4.0	2.7	4.6	17.5	6.1	3	4.8	10	4.0	16.4	8.5	22	–	·	·	·	4	2	·	·	·	3	·	5	8	·
XI	4	2.4	6	3.2	1.4	3.0	1.5.5	4.7	13.5	4.1	11	5.5	1.4	6.9	4	9.9	8	4.6	20.7	12.1	28	–	2	–	·	6	4	1	3	1	2	·	6	17	·
XII	5.5	3.3	1.5	4.0	5.5	1.9	4	3.0	22.5	4.9	28.5	6.4	10	5.3	5.5	5.0	10	4.5	27.0	12.0	14	–	11	–	·	9	7	1	3	1	·	·	3	17	15
Rok	5.1	4.3	44.5	2.9	6.2	2.6	8.1	3.9	181.5	4.6	225	5.1	207.5	5.6	83.5	5.3	159	4.2	553.7	36.4	24.VI	–	33	–	29	117	92	16	26	5	–	18	61	122	41?

Szczerców

$\varphi = 51°20'$ $\lambda = 19°07'$ 195?

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.6	1.0	-0.9	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	7.6	7.7
II	–	–	–	–	1.5	5.3	2.5	3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.0	7.8	7.7
III	–	–	–	–	0.6	7.6	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.2	5.4	6.0
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16.0	23.0	16.2	17.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.1	5.0	4.3	4.5
VII	–	–	–	–	17.7	23.4	17.4	19.0	–	–	–	–	–	–	83	63	89	78	3.6	12.2	2.7	6.2	6.6	6.2	6.2	6.3
VIII	–	–	–	–	14.5	20.1	15.0	16.2	–	–	–	–	–	–	90	68	91	83	1.6	8.1	1.5	3.7	6.2	6.4	6.1	6.2
IX	–	–	–	–	9.8	16.0	11.5	12.2	–	–	–	–	–	–	92	69	90	84	1.0	6.4	1.5	3.0	8.1	8.0	8.2	8.1
X	–	–	–	–	6.8	13.2	8.4	9.2	–	–	–	–	–	–	92	73	91	85	0.8	4.4	1.1	2.1	6.9	6.4	5.1	6.1
XI	–	–	–	–	3.5	7.0	3.9	4.6	–	–	–	–	–	–	90	78	89	86	0.8	2.5	0.9	1.4	7.8	7.7	8.2	7.9
XII	–	–	–	–	-1.8	0.6	-4.0	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	7.2	7.5
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Oborniki Śląskie

$\varphi = 51°18'$ $\lambda = 16°55'$

I	1000.3	1012.2	982.6	1022.5	-1.5	1.4	-1.2	-0.6	2.5	-3.3	9.4	6	-14.8	17	91	81	90	87	0.5	1.4	0.5	0.8	7.9	7.5	6.2	7.2
II	999.0	1012.9	964.1	1011.8	1.1	5.4	2.2	2.7	6.6	0.1	11.3	5	-4.3	27	96	74	92	87	0.3	2.5	0.6	1.1	6.2	7.0	5.7	6.3
III	997.1	1014.8	976.6	1018.9	4.7	8.2	3.8	4.4	9.9	0.7	17.3	13	-5.4	1,3	87	61	78	75	1.0	4.9	1.9	2.6	5.9	5.8	5.7	5.1
IV	997.3	1009.7	976.1	1018.7	5.9	12.9	7.0	8.2	14.3	2.7	27.1	30	-4.1	13	85	50	78	71	1.6	8.6	2.4	4.2	4.9	6.7	2.9	4.8
V	995.6	1006.0	985.4	1016.7	9.3	15.4	9.6	11.0	16.6	5.6	27.5	19	-1.2	7	78	46	72	65	2.7	10.4	3.7	5.6	4.7	6.1	3.6	4.8
VI	996.1	1011.8	984.7	1016.7	16.1	23.1	16.7	18.2	24.5	11.9	32.5	30	6.1	26	73	49	71	64	5.3	15.9	5.9	9.0	4.2	5.2	3.6	4.3
VII	992.2	1005.1	980.6	1012.7	17.5	22.5	17.6	18.8	24.2	14.9	36.0	5	10.5	28	84	64	86	78	3.6	11.9	3.5	6.3	6.6	6.7	6.2	6.5
VIII	994.4	1005.0	981.6	1015.2	14.1	20.3	14.4	15.8	21.5	11.2	28.0	11	6.4	23,31	90	59	88	79	1.7	10.2	2.1	4.7	6.8	6.6	5.3	6.2
IX	992.9	1003.2	976.0	1014.0	10.3	16.0	10.8	12.0	17.2	7.9	28.9	8	-0.6	27	90	61	87	79	1.4	7.9	1.8	3.7	6.2	7.1	6.0	6.4
X	998.9	1007.6	982.0	1020.3	6.3	13.8	8.0	9.0	14.7	4.8	21.9	19	-0.9	2	91	60	87	79	0.9	6.8	1.5	3.1	6.7	6.5	5.3	5.5
XI	999.5	1016.8	982.9	1021.3	3.7	7.2	4.4	4.9	8.2	2.6	17.3	6	-8.6	30	86	69	83	79	1.1	3.9	1.4	2.1	7.7	7.0	7.1	7.3
XII	994.1	1014.4	958.7	1016.2	-1.9	1.1	-1.0	-0.7	2.2	-3.5	8.5	13	-15.0	17	89	79	85	84	0.6	1.4	0.8	0.9	7.7	8.1	6.0	7.3
Rok	995.7	1016.8	958.7	1017.0	6.9	12.3	7.7	8.6	13.5	4.6	36.0	5.VII	-15.0	17.XII	87	63	83	78	1.7	7.2	2.2	3.7	6.3	6.7	5.0	6.0

Antopol

$\varphi = 51°17'$ $\lambda = 22°15'$

I	–	–	–	–	-2.5	-0.7	-1.5	-1.6	0.5	-4.7	5.9	7	-18.3	17	86	82	86	85	0.8	1.0	0.8	0.9	8.3	8.6	7.6	8.2
II	–	–	–	–	0.9	3.7	1.8	2.0	5.0	-0.7	9.4	21	-8.1	24	90	82	87	86	0.7	1.6	0.9	1.1	8.2	7.8	6.7	7.6
III	–	–	–	–	-0.8	4.8	1.5	1.8	6.8	-3.0	16.4	14	-13.2	4	80	63	78	74	1.2	3.6	1.6	2.1	5.4	5.3	3.5	4.7
IV	–	–	–	–	5.6	12.9	7.7	8.5	14.3	2.9	26.5	30	-4.8	10	81	50	78	70	2.0	9.0	2.5	4.5	5.6	5.6	3.8	5.0
V	–	–	–	–	9.1	13.4	9.4	10.3	14.9	5.6	23.0	18	-0.8	29	83	64	83	77	2.2	6.6	2.0	3.6	6.4	7.3	5.6	6.4
VI	–	–	–	–	16.1	22.3	16.4	17.8	23.8	10.6	30.4	12	5.3	27	76	48	77	67	4.5	14.3	4.4	7.7	4.8	5.2	4.0	4.7
VII	–	–	–	–	17.2	22.1	17.2	18.4	23.8	13.5	33.4	5	8.0	7	84	64	86	78	3.5	10.9	3.5	6.0	6.0	6.0	6.5	6.2
VIII	–	–	–	–	14.3	19.8	15.3	16.2	21.6	11.2	28.8	12	4.9	24	91	65	86	81	1.6	8.6	2.5	4.2	6.1	6.5	4.3	5.6
IX	–	–	–	–	10.2	15.3	10.9	11.8	16.6	7.7	25.8	9	-0.9	27	90	64	88	81	1.3	6.6	1.5	3.1	6.1	6.5	6.3	6.3
X	–	–	–	–	5.7	12.2	7.5	8.3	13.1	4.1	19.4	19	-0.8	3	92	69	88	83	0.8	4.6	1.5	2.3	5.8	5.5	4.5	5.3
XI	–	–	–	–	2.5	5.9	3.0	3.6	7.0	0.9	16.7	4	-10.0	29	90	81	90	87	0.7	2.2	0.7	1.2	7.0	7.1	6.9	7.0
XII	–	–	–	–	-3.4	-0.8	-2.5	-2.3	0.3	-5.6	7.6	14	-17.4	16	89	84	87	87	0.5	0.9	0.7	0.7	7.7	7.2	5.7	6.9
Rok	–	–	–	–	6.2	10.9	7.2	7.9	12.3	3.5	33.4	5.VII	-18.3	17.1	86	68	84	79	1.6	6.8	1.9	3.1	6.4	6.6	6.4	6.1

Motycz

$\varphi = 51°16'$ $\lambda = 22°25'$

I	–	–	–	–	-3.0	-1.2	-1.8	-2.0	-0.1	-4.4	5.7	6	-17.1	17	–	–	–	–	–	–	–	–	9.4	9.2	8.7	9.1
II	–	–	–	–	0.8	3.4	1.6	1.8	4.5	-0.5	8.7	21	-6.6	28	91	85	89	88	0.6	1.3	0.8	0.9	9.1	8.1	7.4	8.2
III	–	–	–	–	-0.8	4.5	1.4	1.6	6.1	-2.4	15.5	14	-11.8	4	–	–	–	–	–	–	–	–	5.5	5.8	4.4	5.2
IV	–	–	–	–	5.6	12.6	7.8	8.4	14.2	3.3	26.2	30	-3.6	10	82	55	75	71	1.9	8.2	2.9	4.3	6.3	6.2	5.6	6.0
V	–	–	–	–	8.9	13.3	9.5	10.3	14.5	6.0	23.0	18	0.6	7,27	86	67	83	79	1.8	6.2	2.2	3.4	6.5	7.6	6.4	6.8
VI	–	–	–	–	16.1	22.0	16.0	17.5	23.3	11.2	30.0	12	6.5	7,27	–	–	–	–	–	–	–	–	4.8	6.2	5.7	5.6
VII	–	–	–	–	17.1	22.2	17.1	18.4	23.5	13.7	32.4	5	8.8	7	85	64	85	78	3.2	10.6	3.0	5.6	6.4	6.4	7.4	6.7
VIII	–	–	–	–	14.3	19.8	15.1	16.1	21.3	11.7	29.2	12	6.5	24	90	67	86	81	1.6	8.2	2.4	4.1	7.2	8.0	6.0	7.1
IX	–	–	–	–	10.3	15.2	11.1	11.9	16.5	8.2	26.4	9	0.9	26	91	69	89	83	1.2	6.1	1.6	3.0	6.8	6.8	6.5	6.7
X	–	–	–	–	5.9	12.0	7.5	8.2	12.7	4.6	19.2	19	0.2	5	–	–	–	–	–	–	–	–	7.0	5.7	6.5	6.4
XI	–	–	–	–	2.2	5.6	3.0	3.4	6.7	0.9	16.5	4,6	-12.2	30	93	82	90	88	0.5	1.9	0.7	1.0	8.1	8.0	7.4	7.8
XII	–	–	–	–	-3.3	-1.2	-2.6	-2.4	-0.1	-5.3	7.3	13	-18.6	17	88	85	90	88	0.5	0.8	0.5	0.6	8.6	7.7	7.4	7.9
Rok	–	–	–	–	6.2	10.7	7.1	7.8	11.9	3.9	32.4	5.VII	-18.6	17.XII	–	–	–	–	–	–	–	–	7.1	7.1	6.6	6.9

Szczerców — $H_s = 160$ m — 1957

MIESIĄC	ROZKŁAD WIATRU [%D, %nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0.1 ≥ R	1.0 ≥ R	10.0 ≥ R	Wiatr v >10	v >15	≡	≈	◔	●	▣
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20.4	4.2	5	–	–	–	–	9	6	·	–	–	2	·	1	17	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	58.5	10.4	18	–	–	–	–	18	12	1	–	–	3	·	·	15	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39.6	12.2	17	–	–	–	–	7	5	2	–	–	2	·	2	8	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31.4	8.1	30	–	–	–	–	12	10	·	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24.9	8.9	10	–	–	–	–	10	5	·	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.5	19.3	24	–	–	–	–	8	7	1	–	–	·	1	8	5	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	194.1	79.2	16	–	–	–	–	17	13	5	–	–	·	1	4	13	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	77.9	22.9	16	–	–	–	–	15	11	1	–	–	·	1	·	8	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	75.3	14.5	23	–	–	–	–	14	12	3	–	–	1	·	2	16	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.8	3.6	18	–	–	–	–	4	4	·	–	–	5	·	3	5	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.3	10.1	25	–	–	–	–	6	5	1	–	–	·	·	2	21	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39.4	11.2	14	–	–	–	–	9	7	1	–	–	1	·	2	17	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	635.1	79.2	16.VII	–	–	–	–	129	97	15	–	–	–	–	–	–	–

Oborniki Śląskie — $H_s = 169$ m — $H_b = 174{,}8$ m — $h_w = 22$ m

I	7.5	3.2	2	3.3	4.5	2.3	5	4.5	15.5	1.4	8	1.6	2.2	2.1	8.5	2.9	23	1.6	22.1	6.8	6	25	6	3	·	1	·	·	·	1	·	3	15	9
II	2.5	2.0	1.5	1.3	6	1.8	1.9	1.6	15.5	1.5	8.5	1.4	8.5	2.1	3.5	2.3	1.9	1.3	55.5	8.6	6	1.4	·	·	·	1.5	1.0	·	·	·	1	·	1	7	3
III	5	1.5	1.5	3.0	1.7	3.3	11.5	3.0	9.5	2.9	1.1	2.6	18.5	2.2	8	1.7	1.1	2.3	231	6.9	17	1.4				8	5	·	·	·	2	·	7	8	3
IV	19.5	1.7	9.5	1.3	8	1.4	2.5	1.6	5.5	1.9	2.5	2.2	5.5	1.2	2.1	1.5	1.6	1.3	60	3.1	16	1.0		·	2	4	2	·	·	·	1	·	7	6	
V	1.7	1.9	1.4	2.1	1.0	2.0	3.5	1.3	4	1.9	1.5	2.0	1.2	2.1	1.6	1.6	1.5	1.6	32.2	6.6	22	·		·	2	8	7	·	·	·	·	2	5	5	1
VI	8	2.3	7.5	2.1	9.5	1.6	8.5	2.1	4.5	2.6	5	2.0	19.5	2.3	14.5	2.1	1.3	1.8	33.9	14.4	4	·		·	1.3	7	5	1	·	·	1	1	8	4	
VII	1.0	1.6	4.5	1.6	7.5	2.0	3.5	2.1	4	2.0	3.5	1.7	2.1	1.9	1.8	2.2	2.1	1.5	170.9	38.8	23	·	·	·	1.2	1.6	1.5	8	·	·	·	5	7	12	
VIII	7	1.5	1	2.0	5.5	2.1	3.5	2.6	7	1.8	1.0	2.2	1.6.5	1.8	1.5.5	1.8	2.7	1.4	48.6	10.2	23	·	·	·	3	1.7	9	1	·	·	·	·	1	8	
IX	3.5	1.7	1.5	1.7	1	1.0	5.5	1.4	12.5	1.8	1.5.5	2.9	1.6.5	2.5	1.8	1.7	1.6	1.7	99.4	11.4	24	1		·	3	1.5	1.5	1	1	·	·	1	3	11	
X	2.5	1.0	·	·	2.5	1.2	9	1.4	17.5	1.5	22.5	1.8	12.5	1.7	6.5	1.4	2.0	1.2	10.0	4.6	24	2		·	·	5	2	·	·	·	1	·	5	8	
XI	8	3.2	9.5	2.7	1.5.5	2.3	1.4	2.4	1.1.5	1.8	7	3.1	1.2.5	1.4	4	4.0	8	2.6	76	3.0	25	9	1	·	·	5	2	·	·	·	1	·	4	18	
XII	5.5	1.6	4	2.1	2.5	1.4	10.5	1.4	10	2.1	1.5	2.1	1.7	2.7	1.1.5	2.1	1.7	1.7	35.0	8.8	8	24	6	3	·	1.4	10	·	·	·	3	·	2	15	4
Rok	9.6	1.9	5.6.5	1.9	8.6.5	1.9	9.6	1.9	1.1.7	1.9	1.1.0	2.1	1.8.2	2.2	1.4.5	2.1	2.0.6	1.7	6.4.4.3	3.8.8	23.VII	9.9	1.3	6	3.5	1.2.8	8.7	1.1	1		1.1	9	5.3	1.1.7	2.0

Antopol — $H_s = 203$ m — $h_w = 14{,}5$ m

I	·	·	8	3.6	5	2.3	5	3.7	11	2.1	1.9.5	2.6	2.8	1.8	3.5	1.6	1.3	2.0	46.4	16.4	7	2.6	1.3	7	·	1.1	7	1	·	·	–	·	1	20	–
II	8.5	1.9	2	1.0	1.5	2.7	7.5	4.3	1.8	3.2	2.4.5	3.7	1.0.5	1.9	4.5	1.7	1.0	2.6	46.9	7.8	22	1.4	2	·	·	1.7	1.3	·	1	·	–	·	1	11	–
III	1.0	1.8	4	1.2	1.4	4.4	4	6.0	1.0.5	2.9	7.5	3.7	1.0.5	3.4	1.1.5	2.9	2.1	2.5	17.2	8.5	15	2.0	6	2		6	4	·	5	2	–	·	7	5	–
IV	1.4	1.1	6.5	1.5	5.5	1.5	3	2.0	1.2	1.8	4	1.8	7.5	1.1	9.5	1.4	2.8	1.0	1.4.3	4.2	7	6	·	·	2	8	5	·	·	·	–	1	7	5	–
V	16.5	1.8	1.3.5	1.7	9	2.3	3	1.3	5	1.0	3	1.7	1.0	1.5	1.7	1.8	1.6	1.4	51.4	18.8	7	1	·	·	·	1.2	8	2	·	·	–	1	3	10	–
VI	3.5	1.6	6.5	1.7	1	1.0	3	3.3	1.5	2.1	1.3	1.8	1.2.5	1.6	1.0.5	1.9	2.5	1.4	70.4	32.4	22	·	·	·	1.0	8	6	2	·	·	–	5	6	3	–
VII	3	1.7	1	2.0	3	1.7	4.5	1.6	1.2	1.5	2.1	1.7	1.1.5	2.5	8	2.8	2.9	1.3	1.1.6.1	3.4.6	15	·	·	·	1.3	1.4	1.1	3	1	·	–	9	3	1.3	–
VIII	3	1.0	3	2.3	1.5	1.0	4.5	1.7	1.0	2.0	2.0	1.6	2.0	1.7	3	1.3	2.8	1.2	86.7	32.8	29	·	·	·	1.4	1.2	8	3	·	·	–	3	2	4	–
IX	1	1.0		·	1	2.0	3	3.0	1.3	2.4	2.3	2.8	1.9	2.6	5	2.4	2.5	1.9	76.7	16.3	23	1	·	·	1.2	1.3	1.2	3	2	·	–	·	3	11	–
X	·	·	·	·	·	·	6	1.8	1.2	2.3	2.0	1.7	1.4.5	1.9	4.5	1.2	3.6	1.1	1.4.4	8.3	23	2	·	·	·	6	3	·	1	·	–	·	3	6	–
XI	2.5	7.8	9	3.0	1.2	1.7	1.3	5.6	1.0.5	3.6	9	2.3	1.5	5.1	2	3.0	1.7	3.1	35.9	1.7.2	28	1.2	2	·	·	7	6	1	5	·	–	·	7	1.7	–
XII	8	3.0	1	1.0	4	2.2	9.5	2.3	1.3	4.4	2.5	2.9	8.5	3.2	3	1.7	2.1	2.4	4.1.3	1.8.1	14	2.8	1.3	3		1.1	8	1	4	1	–	·	3	1.4	–
Rok	7.0	1.9	5.4.5	1.6	5.7.5	1.9	6.6	3.0	1.4.2	2.4	1.8.6.5	2.4	1.6.7.5	2.4	8.2	2.0	2.6.9	1.8	6.1.7.7	3.4.6	15.VII	1.1.0	3.6	1.2	3.1	1.2.5	9.1	4.6	1.9	3	–	1.9	4.6	1.1.9	–

Motycz — $H_s = 213$ m — $h_w = 10$ m

I	1.5	2.3	3.5	5.9	6.5	4.8	6	5.3	1.3.5	3.0	2.5	3.5	2.7.5	4.4	7.5	4.9	2	4.0	25.1	11.1	5	2.6	1.3	6	·	1.1	5	1	1	·	5	·	1	27	3.1
II	6	4.6	3	3.0	0.5	4.0	6.5	4.2	1.6.5	4.3	2.6	4.2	1.1.5	4.2	4	5.8	1.0	3.8	38.0	5.3	3	1.3	2	·	·	1.9	1.1	·	·	·	8	·	·	1.6	3
III	1.0.5	3.5	4	3.0	1.3.5	5.8	1.3	6.0	8	3.3	9	3.1	1.6	5.8	1.0	5.0	9	4.3	1.8.0	8.1	1.5	1.9	7	2		7	4	·	4	·	3	·	9	8	9
IV	1.0.6	3.2	7.5	2.5	9.5	2.7	7.5	3.3	9	2.4	7.5	2.9	9.5	3.3	1.2	3.5	1.7	2.4	1.0.5	3.4	3.0	6	·	·	1	6	5	·	·	·	·	3	5	1.1	
V	1.0.5	3.5	1.2.5	4.1	1.2.5	3.8	7	3.5	5.5	2.5	1.5	5.0	1.2	4.2	1.9.5	4.3	1.2	3.4	5.0.1	1.1.1	7	·	·	·	·	1.1	9	1	·	·	2	2	4	1.5	
VI	6	2.6	6.5	2.3	2	1.8	7	2.6	1.3	3.0	9.5	2.9	2.0.5	3.1	1.2.5	3.6	1.3	2.5	6.9.2	3.7.6	22	·	·	·	9	1.0	7	2	·	·	–	3	4	5	·
VII	4.5	3.5	3	1.3	6.5	3.2	9.5	2.9	8.5	2.3	1.5	2.5	2.1.5	3.1	1.0.5	2.8	1.4	2.4	1.0.0.1	3.3.6	16	·	·	·	1.0	1.6	1.4	2	·	·	1	8	3	1.4	·
VIII	3.5	3.9	·	·	2.5	3.0	4.5	3.1	1.1.5	2.7	1.9.5	2.8	2.8.5	3.7	1.2	3.9	1.1	2.9	1.0.9.7	4.8.5	29	·	·	·	4	1.1	1.2	3			–	5	·	1.0	·
IX	4	1.8	1	2.0	2.5	1.0	4.5	1.1	1.2	1.9	2.5	3.1	2.5.5	5.5	8.5	3.1	7	3.3	6.3.5	1.6.2	29	·	·	·	2	1.6	1.2	1	3	1	2	·	5	1.5	
X	0.5	3.0	0.5	3.0	2.5	2.6	7	2.9	1.1.5	2.8	2.5.5	3.1	2.0.5	4.0	8	4.1	1.1	2.8	1.1.1.1	8.2	23	·	·	·	·	5	3	·	1	·	–	·	3	1.1	
XI	8	7.2	8.5	3.9	1.2	3.8	1.9.5	3.1	1.1	2.2	1.1	3.1	1.5.5	6.7	1.5	6.3	3	4.2	2.9.1	1.8.3	28	1.2	3	1	·	8	5	1	2	·	3	·	3	2.3	3
XII	9.5	3.1	6	3.2	3.5	2.1	1.5	3.0	1.6	3.5	2.9.5	1.1	1.1	5.1	7	5.1	6	3.8	3.7.1	1.1.1	1.1	2.8	1.3	3	·	1.1	8	1	1	·	–	·	1	1.7	2.1
Rok	7.5	3.5	5.6	2.8	7.1	3.2	9.6.5	3.5	1.3.9	2.8	2.0.1	3.1	2.1.9.5	4.1	1.1.3	4.1	1.1.8	3.3	5.6.5.6	1.8.5	2.9.VIII	1.0.1	3.8	1.2	2.6	1.3.1	9.5	1.2	1.2	1	–	2.1	3.8	1.7.2	7.0

Lublin

$\varphi = 51°14'$ $\lambda = 22°34'$ 195?

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o,m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	999.6	1010.5	984.4	1022.1	-2.5	-0.5	-1.4	-1.4	0.4	-4.4	5.6	6,7,9	-17.4	17	90	85	90	88	0.5	0.9	0.6	0.7	8.5	8.6	8.2	8.4
II	994.0	1008.4	968.3	1013.0	1.2	4.1	2.1	2.4	5.2	-0.4	9.8	6	-8.4	28	89	77	85	84	0.8	2.0	1.1	1.3	8.1	8.1	6.8	7.7
III	997.8	1013.1	974.4	1020.0	-1.4	5.3	1.6	1.8	6.8	-3.1	16.5	31	-12.6	4	82	54	74	70	1.1	4.7	1.9	2.6	6.0	5.6	4.2	5.3
IV	996.5	1008.3	972.5	1018.0	4.8	13.2	8.3	8.6	14.5	2.3	26.7	30	-6.1	10	85	50	73	69	1.4	9.3	3.3	4.7	5.3	5.4	4.5	5.1
V	994.2	1004.1	981.5	1015.5	9.0	14.1	10.4	11.0	15.5	5.8	23.6	18	0.1	7	84	62	80	75	1.9	7.0	2.8	3.9	6.7	7.5	6.5	6.9
VI	995.8	1008.9	983.6	1016.6	16.1	22.9	17.5	18.5	24.3	10.6	31.5	12	3.4	7	77	51	74	67	4.3	14.2	5.5	8.0	4.2	5.1	3.8	4.4
VII	994.5	1004.1	982.2	1012.2	17.1	22.7	17.9	18.9	24.5	13.6	32.7	8	7.6	30	84	61	83	76	3.4	12.1	3.7	6.4	6.4	6.6	6.3	6.4
VIII	993.7	1003.0	984.5	1014.6	13.9	20.3	15.4	16.2	22.1	11.0	30.4	12	3.7	24	92	64	87	81	1.3	9.3	2.4	4.3	5.6	6.8	4.8	5.7
IX	992.5	1002.7	978.2	1013.6	9.9	15.7	10.9	11.8	17.1	7.5	27.1	9	-0.4	27	92	66	89	82	1.0	6.7	1.5	3.1	6.6	7.0	6.5	6.7
X	999.4	1010.1	985.3	1021.1	5.1	12.6	7.1	8.0	13.4	3.3	20.2	19	-2.6	3	92	66	89	82	0.7	5.2	1.2	2.4	6.1	5.5	5.6	5.7
XI	999.9	1019.9	980.0	1022.0	2.3	6.2	3.0	3.6	7.3	0.8	17.8	4	-9.7	30	94	79	89	86	0.6	2.4	0.8	1.3	6.9	7.8	6.9	7.2
XII	994.2	1012.8	957.6	1016.6	-3.4	-0.6	-2.4	-2.2	0.5	-5.5	8.9	13	-17.8	17	89	82	86	86	0.6	1.1	0.7	0.8	7.6	7.5	6.0	7.0
Rok	995.5	1019.9	957.6	1017.1	6.0	11.3	7.5	8.1	12.6	3.5	32.7	8.VII	-17.8	17.XII	87	66	83	79	1.5	6.2	2.1	3.3	6.5	6.8	5.8	6.4

Felin

$\varphi = 51°14'$ $\lambda = 22°38'$

I	–	–	–	–	-2.9	-1.2	-1.9	-2.0	0.2	-5.0	5.4	6,7,9	-17.4	1,17	–	–	–	–	–	–	–	–	9.4	8.1	8.9	8.8
II	–	–	–	–	1.0	3.6	1.5	1.9	4.7	-0.9	9.9	15	-6.9	28	88	82	86	85	0.8	1.5	1.0	1.1	8.9	6.1	6.4	7.1
III	–	–	–	–	-0.7	4.4	1.5	1.7	6.3	-2.9	16.4	31	-11.9	3	–	–	–	–	–	–	–	–	4.8	3.5	3.9	4.1
IV	–	–	–	–	6.2	12.9	8.3	8.9	14.1	3.0	25.9	30	-4.4	10	80	52	74	69	2.2	8.8	3.2	4.7	4.3	5.2	4.4	4.6
V	–	–	–	–	9.1	13.8	10.0	10.7	15.1	6.0	22.9	14	0.1	5,7	81	64	80	75	2.3	6.7	2.6	3.9	6.7	7.7	7.6	7.3
VI	–	–	–	–	15.4	22.2	17.7	18.2	24.0	11.2	30.9	12	6.1	7,27,28	79	52	72	68	3.8	13.3	5.9	7.7	2.9	4.2	4.5	3.9
VII	–	–	–	–	16.2	22.4	18.3	18.8	24.4	13.9	33.4	5	9.6	30	87	61	80	76	2.5	11.7	4.8	6.3	6.7	6.0	6.8	6.5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	5.7	12.2	7.8	8.4	13.3	4.1	19.9	19	-0.9	3	89	68	87	81	1.0	4.8	1.5	2.4	5.4	4.6	4.8	4.9
XI	–	–	–	–	2.2	5.8	3.1	3.6	7.5	0.5	17.9	2	-9.9	30	88	81	87	85	0.8	1.9	1.0	1.2	6.5	7.3	6.6	6.8
XII	–	–	–	–	-3.2	-0.9	-2.5	-2.3	0.4	-5.8	8.1	13	-17.9	17	83	82	84	83	0.8	1.0	0.8	0.9	7.8	7.2	6.7	7.2
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Uwaga. Temperaturę maksymalną i minimalną obserwator odczytywał z dokładnością do 0,5°

Legnica

$\varphi = 51°13'$ $\lambda = 16°10'$

I	1006.2	1018.7	988.2	1022.3	-4.1	1.9	-0.3	0.0	3.4	-3.5	12.0	6	-15.1	17	88	80	87	85	1.0	1.5	0.9	1.1	8.0	8.1	6.1	7.4
II	995.6	1019.6	969.4	1011.3	2.1	5.8	3.1	3.5	7.3	0.5	13.2	5	-5.3	27	89	77	87	84	0.9	2.2	1.0	1.4	7.2	8.0	6.6	7.3
III	1002.5	1021.4	982.4	1018.2	2.3	7.6	4.7	4.8	9.7	1.2	16.8	13	-4.9	4	88	65	81	78	1.1	4.1	1.8	2.3	6.4	6.4	5.2	6.0
IV	1003.3	1015.3	984.3	1018.9	4.6	11.7	7.6	7.9	13.7	2.7	24.7	30	-2.8	15	90	59	80	76	0.9	6.4	2.2	3.2	5.7	7.1	3.8	5.5
V	1001.4	1011.9	991.0	1016.8	8.5	14.5	10.2	10.8	16.3	5.2	25.8	16	0.1	6	82	53	78	70	2.0	8.4	3.1	4.5	5.3	7.0	4.8	5.7
VI	1001.7	1017.9	990.3	1016.7	15.5	21.9	17.0	17.8	24.0	11.3	31.7	30	5.5	1	81	56	78	72	3.5	12.8	4.4	6.9	5.0	5.9	4.6	5.2
VII	997.7	1011.0	986.7	1012.6	17.4	22.2	18.2	19.0	24.0	14.8	34.8	4	10.0	19	84	64	84	77	3.4	11.4	3.8	6.2	7.0	6.7	6.9	6.9
VIII	999.9	1010.6	986.0	1015.0	14.5	20.0	15.2	16.2	21.6	11.9	28.4	11	6.9	24	87	62	85	78	2.2	9.4	2.6	4.7	6.2	7.1	4.6	6.0
IX	998.5	1009.0	984.0	1013.7	10.1	16.1	11.5	12.3	17.6	8.2	29.9	8	0.5	27	92	64	87	81	1.1	7.2	1.8	3.4	6.6	8.0	6.3	7.0
X	1004.4	1013.2	987.2	1020.0	5.8	14.1	8.2	9.1	15.3	3.9	22.7	19	-2.4	22	94	68	91	84	0.6	5.5	1.1	2.4	6.3	5.9	3.6	5.3
XI	1005.1	1022.7	987.5	1020.9	3.4	7.1	4.8	5.0	8.3	1.9	16.9	5	-8.2	30	92	79	89	87	0.7	2.3	1.0	1.3	7.8	8.2	7.4	7.8
XII	1000.0	1019.2	964.6	1016.0	-1.9	1.0	-0.9	-0.7	2.5	-4.2	11.6	8	-21.8	16	90	84	88	87	0.6	1.2	0.7	0.8	7.0	7.8	5.8	6.9
Rok	1001.4	1022.7	964.6	1016.9	6.8	12.0	8.3	8.8	13.6	4.5	34.8	4.VII	-21.8	16.XII	88	68	84	80	1.5	6.0	2.0	3.2	6.5	7.2	5.5	6.4

Wieluń

$\varphi = 51°13'$ $\lambda = 18°35'$

I	997.3	1008.5	979.6	1022.5	-1.8	0.6	-1.2	-0.9	1.7	-3.6	7.6	6	-16.0	17	87	81	86	85	0.7	1.3	0.8	0.9	7.6	8.3	6.7	7.5
II	987.4	1008.5	962.2	1012.0	1.6	4.9	2.5	2.8	6.0	0.5	9.9	9	-3.5	24	88	77	88	84	0.8	2.1	0.9	1.3	7.2	8.2	6.7	7.4
III	994.2	1010.3	973.3	1018.9	1.2	7.0	3.7	3.9	8.7	-0.2	15.6	13	-6.4	1	84	62	75	74	1.2	4.3	2.1	2.5	6.7	6.1	5.2	6.0
IV	994.2	1006.9	977.4	1018.5	5.2	12.0	7.2	7.9	13.6	3.0	25.6	30	-3.7	15	84	56	79	73	1.5	7.4	2.3	3.7	6.6	6.4	5.5	6.2
V	992.3	1002.3	983.5	1016.2	8.7	14.7	9.7	10.7	16.1	5.0	26.5	19	-0.9	7	80	52	77	70	2.3	8.9	3.0	4.7	5.9	6.7	5.4	6.0
VI	993.4	1008.5	982.7	1016.9	16.4	22.2	16.6	18.0	23.8	11.3	34.7	11	6.8	27	74	53	77	68	5.1	13.7	4.6	7.8	4.4	5.4	4.8	4.9
VII	989.1	1004.3	978.0	1018.4	17.3	22.6	17.5	18.7	23.9	14.1	34.7	8	10.1	29	84	64	84	77	3.5	12.2	3.8	6.5	6.9	6.4	6.2	6.5
VIII	991.4	1004.9	978.4	1014.5	14.1	19.7	14.6	15.8	21.1	11.6	27.6	11	5.8	31	89	64	87	80	1.9	8.5	2.3	4.2	6.7	7.4	4.3	6.1
IX	990.0	999.4	974.5	1013.8	9.9	15.2	11.2	11.9	16.8	7.9	27.5	9	-0.4	27	91	69	87	82	1.2	6.1	1.7	3.0	6.7	7.3	6.3	6.8
X	996.2	1005.2	980.4	1020.3	6.6	12.7	8.3	9.0	13.7	5.2	20.6	19	0.8	2	93	74	90	86	0.7	4.2	1.1	2.0	6.3	6.6	3.8	5.6
XI	996.7	1014.1	981.9	1021.3	3.0	6.6	3.9	4.4	7.5	1.7	17.9	5	-8.5	30	89	76	86	84	0.8	2.7	1.1	1.5	7.4	7.3	8.0	7.6
XII	991.3	1010.1	955.8	1016.4	-2.2	0.3	-1.4	-1.2	1.6	-4.5	8.9	9	-19.1	17	88	82	87	86	0.6	1.2	0.8	0.9	7.7	8.0	6.5	7.4
Rok	992.8	1015.1	955.8	1016.9	6.7	11.5	7.7	8.4	12.9	4.3	34.7	8.VII	-19.1	17.XII	86	66	84	79	1.7	6.0	2.0	3.2	6.7	7.0	5.8	6.5

Lublin

$H_s = 171\ m$ $H_b = 176.7\ m$ $h_w = 10\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D. °mD																	OPAD R			LICZBA DNI (n)																			
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr											
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min <0°	Max <0°	Min <-10°	Max >25°	≥ 0.1	≥ 1.0	≥ 10.0	> 10	> 15	=	≤ 3n	◔	●	⊞						
I	25	3.4	7	3.9	4.5	2.4	7	3.2	13	1.9	38	4.1	18	4.1	2	5.2	1	3.6	23.0	5.6	5	24	11	6	·	12	6	·	3	·	·	·	1	23	20						
II	4.5	2.8	3	2.0	4	1.8	9	2.9	17.5	4.5	27.5	3.4	9.5	4.1	4	2.9	5	3.3	36.9	8.0	22	13	2	·	·	17	12	·	3	1	4	·	1	14	3						
III	8	3.1	9.5	2.6	11	3.8	8	4.2	8.5	2.8	8.5	3.2	13.5	4.9	8	4.6	18	3.0	21.2	9.6	16	24	7	2	·	6	4	·	6	·	1		8	8	4						
IV	16	2.0	8	1.8	7	1.6	6.5	2.4	6.5	2.0	7.5	1.7	9	2.2	10.5	2.2	19	1.6	15.6	3.9	17	9	·	·	2	10	5	·	·	·	1	2	6	9	·						
V	16	2.4	14.5	2.5	8.5	2.9	3.5	2.1	6	1.8	6.5	2.8	10.5	2.7	15.5	2.1	12	2.1	46.1	9.3	7,9	·	·	·	·	9	9	·	1	·	3	1	1	15	1						
VI	8.5	2.2	3.5	2.6	1	2.0	12.5	2.7	12.5	2.8	19.5	2.8	12	3.6	9.5	2.8	11	2.5	63.7	30.9	22	·	·	·	13	8	5	2	·	·	·	7	6	1	·						
VII	3.5	2.7	2.5	1.6	6	2.8	8	1.9	8.5	2.6	26	2.4	21	2.9	9.5	1.8	8	2.2	134.3	38.0	11	·	·	·	16	18	15	3	·	·	·	8	2	15	·						
VIII	3	1.3	1	2.0	2	3.0	4	2.2	7.5	2.9	28	2.2	18.5	2.3	8	2.4	21	1.8	76.6	27.8	29	·	·	·	7	14	10	2	·	·	2	6	2	5	·						
IX	3.5	1.1	0.5	2.0	1	2.0	2.5	3.0	7	2.6	35.5	4.6	14.5	3.7	6.5	2.4	19	3.0	63.2	13.6	29	1	·	·	2	18	12	2	8	·	1	1	3	13	·						
X	0.5	1.0	1	1.0	·	·	5	2.4	14.5	2.4	27	3.1	13	3.5	4	2.4	28	2.0	14.2	7.6	23	4	·	·	·	7	3	·	1	·	3	·	2	6	·						
XI	2.5	3.4	10.5	2.6	9	2.2	18	2.7	8	2.1	17	4.3	11	4.9	4	10.0	10	3.2	23.0	15.0	28	10	2	·	·	10	5	1	5	·	5	·	6	16	2						
XII	7.5	1.7	8.5	1.6	3	1.8	5.5	1.6	12	2.7	33.5	4.2	7	4.1	6	2.8	10	2.8	37.8	13.4	14	26	11	5	·	13	8	1	3	1	·	·	3	15	24						
Rok	76	2.3	69.5	2.2	57	2.2	89.5	2.6	121.5	2.6	274.5	3.2	157.5	3.6	87.5	3.5	162	2.6	555.6	38.0	11.VII	111	33	13	40	142	94	11	30	2	20	25	41	140	54						

Felin

$H_s = 209\ m$ $h_w = 10\ m$

I	4	1.5	4.5	2.7	4	2.8	8.5	2.5	7	1.5	19	1.5	20.5	2.5	6.5	2.7	23	1.6	22.2	5.3	6	26	13	7	·	8	6	·	·	·	10	·	2	24	–						
II	3	1.7	2	1.0	·	·	2	1.8	12.5	1.7	21	1.6	11.5	1.8	4	3.0	28	1.2	36.2	6.5	3	14	2	·	·	14	11	·	·	·	7	·	2	13	–						
III	8.5	1.6	8	2.8	7.5	3.7	6.5	2.8	7	1.6	8.6	3.0	12.5	4.2	10.5	2.0	24	2.1	21.9	9.7	15	21	6	2	,	4	4	·	2	·	2	·	16	10	–						
IV	10	1.4	10	1.4	6	1.2	7	1.1	7.5	1.3	8	1.1	5	1.4	11.5	1.7	25	1.0	24.9	5.7	11	6	·	·	3	7	6	·	·	·	3	3	12	9	–						
V	6.5	1.7	16.5	2.2	13.5	1.6	4	1.6	3.5	1.6	4	1.8	5	1.9	10	1.8	30	1.2	42.3	8.7	7,9	·	·	·	·	9	9	·	·	·	3	2	2	16	–						
VI	7	1.2	4	1.0	2	1.0	6	1.1	9	1.8	5	1.3	9.5	1.7	11.5	1.6	36	0.9	44.8	26.0	22	·	·	·	11	6	6	1	·	·	1	5	12	4	–						
VII	4.5	1.3	2	1.0	5.5	1.2	1.5	1.0	4	1.4	12.5	1.4	1.4	1.4	15	1.5	34	0.9	104.8	15.8	30	·	·	·	16	16	14	4	·	·	8	6	5	14	–						
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57.4	25.1	29	–	·	·	–	11	8	2	–	–	–	–	–	–	–						
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	65.0	14.1	23	–	·	·	–	13	12	2	–	–	–	1	–	–	–						
X	1	1.6	·	·	2	2.0	4	1.5	9.5	2.3	26	3.2	22	3.7	10.5	2.7	18	2.4	11.6	6.8	23	1	·	·	·	–	3	·	·	·	–	·	6	8	–						
XI	5	6.8	6	3.7	14	2.7	15	2.8	5.6	3.0	8	4.3	12.6	4.9	2	4.5	22	2.8	26.6	10.9	28	13	1	·	·	5	4	1	·	·	–	·	7	17	–						
XII	8	3.2	5	3.6	2	3.0	1.5	2.0	12	3.2	32.5	4.4	12	4.2	4	2.8	16	3.2	50.1	20.8	14	29	12	4	·	6	6	2	·	·	–	·	3	19	–						
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	529.8	26.0	22.VI	–	34	13	–	–	89	12	–	–	–	–	–	–	–						

Legnica

$H_s = 121\ m$ $H_b = 126,3\ m$ $h_w = 13,2\ m$

I	2	3.2	5	4.7	4	2.0	1	2.0	7	1.7	6.5	2.8	37	3.5	10.5	3.1	20	2.5	10.9	2.3	6	22	4	5	·	13	5	·	1	1	2	·	3	15	12						
II	0.5	2.0	4	2.4	8	2.8	5	3.2	18.5	3.4	6	2.0	18	3.1	7	3.2	17	2.4	33.6	9.8	18	12	·	·	·	14	8	·	3	1	5	·	1	12	3						
III	4.5	1.7	1	3.0	16.5	4.4	10	5.4	8.5	6.3	3.5	2.6	25	3.9	13	2.1	11	3.5	57.8	15.9	29	15	·	·	·	10	8	2	4	2	2	·	4	9	3						
IV	7.5	2.7	5	1.8	9	2.1	6.5	2.2	·	·	2	1.5	15.5	2.6	21.5	2.9	23	1.8	22.5	6.5	7	10	·	·	·	6	4	·	·	·	3	·	5	5	1						
V	7	3.8	16	3.0	9	2.8	6.5	2.4	1	4.0	1.5	1.7	18.5	4.6	18.5	2.7	15	2.8	31.2	12.9	16	·	·	·	2	8	4	1	1	1	1	3	2	8	1						
VI	3	1.7	8.5	1.8	17	2.3	3	2.7	2	3.5	4.5	2.2	28	3.3	14	2.3	10	2.3	54.4	18.1	4	·	·	·	11	12	9	1	·	·	1	8	6	6	·						
VII	1	3.0	2.5	2.2	7	2.7	7.5	2.1	2.5	1.0	4	1.2	34.5	3.1	23	3.2	11	2.5	135.9	36.0	23	·	·	·	11	19	14	5	·	·	·	11	1	14	·						
VIII	·	·	·	·	3.5	3.3	2	2.2	5.5	2.0	13	2.4	42.5	2.5	10.5	3.0	16	2.1	43.8	7.1	24	·	·	·	3	15	11	·	·	·	·	7	2	7	·						
IX	·	·	·	·	2	1.5	2	1.8	4	3.0	10.5	2.8	42	3.3	8.5	3.6	21	2.4	75.3	11.8	29	·	·	·	2	17	15	3	2	2	3	·	1	13	·						
X	2.5	1.4	0.5	3.0	5	2.6	3.5	2.9	6.5	3.1	6.5	2.4	25.5	3.3	7	2.3	36	1.8	5.3	1.8	20	5	·	·	·	4	3	·	·	·	13	·	5	5	·						
XI	2	5.0	9.5	3.4	22.5	2.9	13	2.7	3.5	3.0	1.5	5.0	19.5	5.3	8.5	3.3	10	3.3	8.2	1.8	7	8	1	·	·	9	4	·	·	·	6	·	1	17	·						
XII	2	1.5	3.5	3.3	3.5	2.7	9.5	2.7	5.5	2.3	6	3.0	24.5	4.0	14.5	3.1	24	2.4	27.2	7.2	14	24	6	3	·	16	7	·	2	·	9	·	2	10	9						
Rok	32	2.2	55.5	2.4	107	2.7	69.5	2.7	64.5	2.8	65.5	2.5	330.5	3.5	156.5	2.9	214	2.5	506.1	36.0	23.VII	96	11	8	29	141	92	12	13	7	45	29	33	121	29						

Wieluń

$H_s = 195\ m$ $H_b = 198,4\ m$ $h_w = 11\ m$

I	5	2.2	6	4.3	5.5	3.4	4	1.8	13	3.1	30	3.6	27	3.1	4.5	5.1	·	3.3	21.6	5.8	6	24	7	3	·	15	6	·	·	·	4	·	3	18	20						
II	3.5	1.6	3	2.7	7	2.4	5	2.9	20.5	3.7	25.5	3.6	12.5	4.3	7	3.2	·	3.5	39.2	6.6	18	11	1	·	·	17	12	·	1	·	3	·	2	13	1						
III	7	2.7	9.5	2.0	20.5	4.7	7	3.4	6.5	4.7	14	4.3	18	4.4	7.5	3.1	3	3.8	27.9	7.3	17	16	·	·	·	10	6	·	5.1	1.1	1	·	6	12	1						
IV	18.5	2.8	8	2.1	7.5	2.1	3	2.7	4	2.9	10.5	3.0	13	1.9	27.5	1.9	·	2.3	38.9	13.5	30	9	·	·	1	11	7	2	·	·	3	2	4	12	·						
V	13	2.7	25.5	2.5	12	1.8	6	2.3	2.5	2.4	1.5	2.0	15	2.8	17.5	3.0	·	2.6	40.2	35.0	20	1	·	·	1	6	3	1	1	·	2	3	1	7	·						
VI	9.5	2.2	10.5	1.7	3.5	1.6	10.5	2.2	6	3.0	13	2.8	23	2.8	12	2.5	2	2.4	50.9	27.7	24	·	·	·	12	8	7	1	1	·	·	6	6	6	·						
VII	2.5	1.8	2	1.2	8.5	3.4	6.5	2.2	4	2.2	15	2.8	30.5	2.8	21	2.0	3	2.6	147.2	47.8	16	·	·	·	14	18	14	5	1	·	3	4	2	12	·						
VIII	3	1.7	·	·	2	2.8	4.5	2.4	11	2.4	16.5	3.1	38.5	2.4	18.6	2.8	1	2.6	52.5	11.5	10	·	·	·	2	15	12	1	1	·	1	7	2	7	·						
IX	2	1.8	2	1.8	1	1.5	4	2.1	10.5	3.6	24.5	3.4	33.5	3.6	10.5	2.0	·	3.2	83.4	16.4	14	1	·	·	2	16	11	2	3	1	1	·	1	9	·						
X	1.6	1.0	·	·	2	1.5	10.5	2.0	17.5	2.7	25.5	2.4	24.5	2.4	10.5	1.4	1	2.2	7.9	3.0	18	·	·	·	·	7	3	·	·	·	6	·	3	6	·						
XI	3.5	6.6	8	4.2	2.4	2.1	17	2.1	11.5	2.2	7.5	3.3	16	4.2	4.5	7.3	1	3.0	20.3	5.7	28	9	2	·	·	8	6	·	1	·	2	·	3	19	·						
XII	3	1.7	10	1.7	7	2.1	6	3.2	13	3.1	25.5	3.9	17.5	3.7	7	2.4	4	3.0	42.8	8.7	14	25	8	3	·	15	8	·	3	·	5	·	1	13	16						
Rok	68	2.4	84.5	2.0	100.5	2.6	84	2.4	120	3.0	209	3.2	271	3.2	143	3.1	15	2.9	572.6	47.8	16.VII	96	18	6	32	147	95	12	17.1	2.5	31	22	34	134	38						

Siemianice

$\varphi = 51°11'$ $\lambda = 18°09'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o,m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.7	0.6	-1.3	-1.0	1.5	-3.4	8.3	6	-15.8	17	88	85	90	88	0.7	1.0	0.6	0.8	7.6	7.8	5.9	7.1
II	–	–	–	–	1.1	4.8	2.4	2.7	5.7	0.1	9.1	9,13,14	-3.7	24,28	90	77	90	86	0.6	2.1	0.8	1.2	7.4	8.2	6.6	7.4
III	–	–	–	–	4.0	7.2	3.8	4.0	8.8	-0.1	15.5	13	-7.7	1	86	60	78	75	1.1	4.6	1.9	2.5	6.4	6.1	5.2	5.9
IV	–	–	–	–	4.6	11.9	7.2	7.7	13.3	2.8	25.2	30	-3.9	15	86	55	76	72	1.3	7.7	2.6	3.9	6.1	6.5	5.5	6.0
V	–	–	–	–	8.3	14.7	9.7	10.6	15.9	5.0	25.8	19	-0.8	7	81	52	76	70	2.1	8.8	3.1	4.7	6.0	6.9	5.6	6.2
VI	–	–	–	–	15.5	22.1	16.8	17.8	23.8	11.0	30.8	30	5.7	28	78	52	74	68	4.1	14.0	5.1	7.7	4.8	5.8	4.5	5.0
VII	–	–	–	–	16.8	22.5	17.6	18.6	23.8	14.1	34.7	5	9.3	29	86	65	85	79	3.0	11.6	3.5	6.0	6.8	7.0	6.8	6.9
VIII	–	–	–	–	13.8	19.7	14.9	15.8	21.1	11.5	28.4	11	5.9	31	88	65	87	80	1.9	8.3	2.3	4.2	5.4	6.8	5.0	5.7
IX	–	–	–	–	9.5	15.1	11.0	11.6	16.8	7.9	28.0	9	-0.4	26	93	69	88	83	0.9	5.8	1.7	2.8	7.3	7.7	5.6	6.9
X	–	–	–	–	5.5	12.4	7.8	8.4	13.4	4.3	20.9	19	-1.2	2	95	74	92	87	0.5	4.0	0.9	1.8	6.2	7.0	3.5	5.6
XI	–	–	–	–	3.4	6.8	4.2	4.6	7.7	2.2	18.2	5	-7.2	30	89	76	87	84	1.0	2.9	1.2	1.7	7.4	7.8	7.8	7.7
XII	–	–	–	–	-2.4	0.2	-1.3	-1.2	1.7	-4.1	9.0	13	-17.2	17	91	85	89	88	0.4	1.0	0.7	0.7	7.8	8.0	7.0	7.6
Rok	–	–	–	–	6.3	11.5	7.7	8.3	12.8	4.3	34.7	5.VII	-17.2	17.XII	88	68	84	80	1.5	6.0	2.0	3.2	6.6	7.1	5.8	6.5

Zgorzelec

$\varphi = 51°10'$ $\lambda = 15°00'$

I	995.7	1007.3	977.4	1023.3	-1.6	0.7	-1.0	-0.7	1.7	-4.0	10.4	6	-19.6	17	89	81	86	85	0.7	1.3	0.9	1.0	8.0	7.6	6.2	7.3
II	984.7	1009.2	957.6	1011.6	2.0	5.3	2.8	3.2	6.1	0.3	11.2	3	-3.8	23,26	89	78	88	85	0.8	2.0	0.9	1.2	7.6	8.5	6.6	7.6
III	991.4	1010.9	972.5	1018.2	2.4	8.2	5.2	5.2	9.9	0.6	17.6	13	-9.1	2	86	66	80	77	1.1	4.2	1.8	2.4	6.9	7.0	4.8	6.2
IV	992.7	1004.2	974.1	1019.3	4.5	11.4	7.6	7.8	12.9	2.1	24.6	28	-3.6	14	91	63	81	78	0.8	5.7	2.1	2.9	6.3	6.3	4.3	5.6
V	990.8	1001.5	981.0	1017.0	7.4	14.0	10.0	10.4	15.7	3.7	26.5	16	-1.6	7	86	58	78	74	1.5	7.5	2.9	4.0	6.0	6.8	4.7	5.8
VI	991.3	1007.4	979.7	1017.1	14.9	21.4	16.8	17.5	23.3	10.5	31.2	30	6.1	26	86	61	81	76	2.5	10.9	4.0	5.8	5.1	5.3	4.8	5.2
VII	987.8	1000.8	977.2	1013.4	16.7	21.6	17.8	18.5	23.1	13.6	33.9	5	9.7	18	91	73	88	84	1.9	8.6	2.9	4.5	6.7	7.3	6.9	7.0
VIII	989.6	1000.6	975.3	1015.4	13.1	18.6	14.4	15.1	20.2	10.1	27.5	11	5.2	23	95	76	93	88	0.8	5.6	1.3	2.6	7.0	7.6	4.5	6.4
IX	988.2	999.2	970.1	1014.3	10.0	15.0	11.1	11.8	16.5	7.3	27.1	8	-1.1	27	94	77	93	88	0.7	4.3	0.9	2.0	7.2	7.6	6.6	7.1
X	993.8	1002.3	977.3	1020.2	6.6	12.6	8.5	9.0	13.8	4.7	21.0	9	-1.1	3	95	80	94	90	0.5	3.2	1.0	1.6	6.6	5.8	3.0	5.1
XI	994.1	1009.7	977.3	1020.9	3.8	6.4	4.8	5.0	7.6	2.0	15.4	5	-9.1	30	92	85	92	90	0.6	1.5	0.5	0.9	7.6	8.2	7.5	7.8
XII	989.2	1007.9	954.9	1016.6	-4.3	0.7	-0.9	-0.6	1.7	-3.9	9.2	8	-21.9	17	92	88	90	90	0.4	0.8	0.6	0.6	6.6	8.1	6.6	7.1
Rok	990.8	1010.9	954.9	1017.2	6.5	11.3	8.1	8.5	12.7	3.9	33.9	5.VII	-21.9	17.XII	90	74	87	84	1.0	4.6	1.7	2.4	6.8	7.2	5.5	6.5

Dobryszyce

$\varphi = 51°09'$ $\lambda = 19°24'$

I	–	–	–	–	-2.2	0.1	-1.6	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	6.7	7.6
II	–	–	–	–	1.1	4.4	2.4	2.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	6.2	6.8
III	–	–	–	–	0.5	6.5	2.9	3.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.7	3.8	4.7
IV	–	–	–	–	4.9	12.1	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.9	4.9	5.5
V	–	–	–	–	8.7	14.2	9.7	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.8	5.0	5.9
VI	–	–	–	–	16.1	22.6	17.5	18.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.9	4.5	4.7
VII	–	–	–	–	17.1	22.6	18.1	19.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.2	6.3	6.4
VIII	–	–	–	–	14.0	19.3	15.3	16.0	–	–	–	–	–	–	88	67	84	80	1.9	7.8	2.8	4.2	5.7	7.4	4.8	6.0
IX	–	–	–	–	9.6	15.2	11.5	12.0	–	–	–	–	–	–	90	66	86	81	1.5	6.1	2.1	3.2	6.1	7.0	5.9	6.3
X	–	–	–	–	6.4	12.6	8.1	8.8	–	–	–	–	–	–	92	71	89	84	0.8	4.7	1.3	2.3	6.4	6.0	3.4	5.3
XI	–	–	–	–	2.8	6.4	3.8	4.2	–	–	–	–	–	–	90	78	87	85	0.6	2.4	0.9	1.3	6.6	6.1	7.1	6.6
XII	–	–	–	–	-2.3	0.0	-1.5	-1.3	–	–	–	–	–	–	87	85	86	86	0.6	1.0	0.7	0.8	7.6	7.4	7.4	7.5
Rok	–	–	–	–	6.4	11.3	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.4	5.5	6.1

Wrocław - Mały Gądów

$\varphi = 51°08'$ $\lambda = 16°59'$

I	1007.5	1019.7	989.3	1022.6	-1.5	1.8	-1.0	-0.4	2.8	-4.2	10.6	6	-15.4	17	87	77	86	83	0.8	1.7	0.8	1.1	7.9	8.3	6.7	7.5
II	997.0	1019.7	970.5	1011.7	1.3	6.0	2.6	3.1	6.9	-0.7	11.0	5	-7.2	27	90	74	88	84	0.7	2.5	0.9	1.4	7.2	7.9	6.8	7.3
III	1003.9	1022.2	983.3	1018.7	1.5	8.0	4.5	4.6	10.1	-0.4	16.2	13	-11.0	1	84	61	77	74	1.3	4.7	2.0	2.7	6.8	6.5	5.1	6.1
IV	1004.3	1016.7	981.7	1018.9	4.9	12.6	7.0	7.9	14.0	1.3	25.7	30	- 0.8	14	88	52	78	73	1.1	7.8	2.4	3.8	5.5	6.8	5.1	5.8
V	1002.3	1012.5	991.9	1016.7	9.2	14.9	10.0	11.0	16.4	4.3	26.2	19	- 2.4	7	79	52	75	69	2.5	8.6	3.3	4.8	5.8	7.1	5.8	6.2
VI	1002.8	1018.8	994.8	1016.9	16.2	22.6	17.4	18.4	24.7	10.3	32.8	11	3.3	1	74	50	74	66	5.1	15.0	5.6	8.6	5.2	6.1	4.9	5.4
VII	998.8	1011.7	986.9	1012.8	17.5	22.4	18.5	19.2	24.3	14.4	35.6	5	10.1	19	82	63	83	76	4.1	12.1	4.4	6.9	7.0	7.1	7.2	7.1
VIII	1004.1	1011.8	988.1	1015.3	14.2	19.5	14.9	15.9	21.3	10.8	27.4	11	5.6	31	87	64	86	79	2.1	8.4	2.5	4.3	6.3	6.8	5.1	6.1
IX	999.7	1009.8	982.3	1014.0	10.3	16.1	11.6	12.4	17.4	7.5	28.5	8	-0.5	27	89	64	84	79	1.5	7.1	2.3	3.6	6.7	7.8	6.1	6.9
X	1005.9	1014.8	989.0	1020.5	6.9	13.8	7.9	8.9	15.0	2.9	22.5	19	-3.1	3	92	66	88	82	0.8	5.7	1.4	2.6	7.0	6.1	3.8	5.6
XI	1006.3	1024.2	989.6	1021.0	4.1	7.6	5.0	5.4	8.7	2.4	18.4	5	-7.9	30	80	73	85	82	4.1	3.3	4.3	4.9	7.5	7.7	7.9	7.7
XII	1004.2	1020.9	965.7	1016.2	-1.9	1.4	-0.9	-0.5	2.9	-4.6	9.6	13	-17.5	17	91	83	89	88	0.5	1.2	0.6	0.8	6.9	7.6	5.6	6.7
Rok	1002.6	1024.2	965.7	1017.2	6.8	12.2	8.1	8.8	13.7	3.7	35.6	5.VII	-17.5	17.XII	86	65	83	78	1.8	6.5	2.3	3.6	6.6	7.2	5.8	6.5

Siemianice — $H_s = 182\ m$ — $h_w = 10\ m$ — 1957

MIESIĄC	ROZKŁAD WIATRU [%D, v m/s] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	C v	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	≡	≋	◔	●	▦
I	4	5.5	4.5	6.7	3.5	6.1	2	2.5	10.5	2.7	3.8	3.4	18	5.1	5.5	6.6	10	3.7	2.34	62	5	23	8	4	·	10	4	·	3	·	–	·	3	15	20
II	1.5	1.3	4	2.2	2.5	2.4	7.5	2.9	17.5	3.3	2.7	3.7	11	4.9	9	4.5	4	3.4	4.15	7.7	6	12	1	·	·	15	12	·	1	·	–	·	·	13	3
III	3.5	3.6	6.5	5.1	13.5	6.6	12.5	4.4	9	4.4	1.3	3.1	16	7.4	12	4.8	7	4.7	3.82	8.5	17	16	2	·	·	7	6	·	5	2	–	·	7	12	2
IV	1.6	3.9	7	3.8	1	4.0	3.5	2.0	9.5	2.3	5	2.9	17	3.3	17	4.3	14	2.9	2.89	11.1	22	10	·	·	1	10	7	1	1	·	–	1	5	12	·
V	1.6	3.0	1.9	4.6	4	4.9	7	3.1	4	2.5	8.5	2.8	9	4.4	19.5	4.3	6	3.6	4.74	37.0	20	1	·	·	1	7	5	1	3	·	–	2	1	8	·
VI	7	3.6	9	2.8	8	2.6	10	3.4	4	2.9	1.6	3.6	15	4.2	16	4.2	5	3.4	4.19	17.5	24	·	·	·	12	6	6	1	2	·	–	5	9	5	·
VII	6.5	2.8	6.6	2.6	3	3.8	9	2.9	7	2.5	1.5	3.6	2.7	4.4	1.5	5.1	4	3.7	1.51.7	61.1	1.6	·	·	·	1.4	1.7	1.2	5	1	·	–	4	2	1.4	·
VIII	2	5.5	1.5	1.7	1	2.0	5	2.7	5.5	3.0	2.5.5	3.3	2.8.5	3.3	1.7	4.2	7	3.2	6.06	11.9	21	·	·	·	4	1.3	1.0	3	·	·	–	5	4	9	·
IX	1.5	2.7	·	·	0.5	1.0	2.5	1.8	10.5	2.5	3.2	4.1	2.3.5	5.1	12.5	4.9	7	3.9	8.16	13.2	23	1	·	·	2	1.6	1.1	4	3	·	–	·	1	9	·
X	0.5	6.0	·	·	2	2.0	6	2.4	2.1	2.2	2.6	2.5	1.3	5.1	7.5	4.5	1.7	2.5	9.1	3.5	1.8	1	·	·	·	5	3	·	1	·	–	·	4	6	·
XI	2.5	1.3	5.5	5.9	1.9.5	4.3	1.5.5	3.6	8	4.9	9.5	4.4	1.6	7.1	4.5	1.1.6	9	5.0	1.6.3	1.1.5	2.8	10	1	·	·	4	3	1	8	·	–	·	2	1.7	·
XII	5.5	2.7	4.5	4.2	3	2.7	3.5	3.0	2.1.5	2.7	2.2.5	4.3	1.4.5	5.5	12	5.4	6	3.8	3.7.5	8.0	1.4	26	8	3	·	1.5	8	·	4	·	–	·	1	1.6	1.8
Rok	6.3.5	3.5	6.8	3.3	6.4.5	3.5	8.4	2.9	1.2.8	3.0	2.3.8	3.5	2.0.8.5	5.0	1.4.7.5	5.3	9.6	3.6	5.9.4.1	6.1.1	1.6.VII	1.0.0	2.0	7	3.4	1.2.5	8.7	1.6	3.2	2	–	1.7	3.9	1.3.6	4.3

Zgorzelec — $H_s = 219\ m$ — $H_b = 217{,}9\ m$ — $h_w = 18{,}3\ m$

I	3	3.3	5.5	5.5	0.5	1.0	0.5	1.0	3	3.2	4.5.5	4.0	1.2.5	4.3	4.5	5.6	1.8	3.3	3.0.2	5.6	5	2.3	1.0	4	·	1.5	9	·	1	1	1	·	3	1.6	1.9
II	2.5	3.6	0.5	6.0	4.5	1.7	2.5	1.8	8	5.5	4.2	4.3	1.0.5	3.8	3.5	3.0	1.0	3.5	4.6.9	7.8	8	1.1	·	·	·	1.8	1.4	·	2	·	1	·	·	1.2	4
III	3	1.7	5	2.0	1.4.5	5.3	4	2.1	1.0	3.5	2.4.5	4.1	1.0	4.0	4	4.5	1.8	3.0	8.1.4	1.7.1	2.9	1.3	·	·	·	1.3	9	3	6	·	·	·	3	1.0	1
IV	1.2	2.8	1.3	2.3	9	2.6	3.5	3.0	4	1.5	9	1.6	7	2.1	9.5	3.3	2.3	1.8	2.0.7	5.3	1.7	1.0	·	·	·	1.4	7	·	·	·	2	·	3	7	·
V	4.5	1.8	1.5.5	3.5	1.0	4.0	4	1.4	4	2.4	7	3.7	1.3	3.1	1.1	3.4	2.4	2.4	4.4.9	1.9.9	1.6	7	·	·	1	9	8	2	·	·	·	2	1	8	·
VI	1.5	1.3	8	3.0	1.5.5	3.5	4.5	2.4	7.5	2.1	1.7	2.5	1.5.5	5.4	7.5	3.7	1.3	2.6	7.8.4	1.7.4	2.2	·	·	·	9	1.3	1.1	4	·	·	·	3	7	9	·
VII	8.5	2.9	2.5	2.6	9	2.6	2	2.8	4	2.0	2.3	2.3	1.9.5	3.8	1.1.5	4.0	1.3	2.8	2.2.1.8	6.2.3	2.2	·	·	·	1.0	1.8	1.6	6	·	·	·	4	3	1.4	·
VIII	0.5	5.0	1	1.0	1	3.0	·	·	1.1	3.1	3.4	2.7	1.5.5	2.5	5	3.4	2.5	2.0	7.8.4	3.0.0	9	·	·	·	2	1.4	1.3	1	·	·	·	5	1	5	·
IX	1	6.0	·	·	1.5	2.3	1.5	1.7	7	1.6	4.1	4.1	1.7.5	4.2	6.5	3.3	1.5	3.1	8.4.5	1.1.1	1.9	·	·	·	1	1.9	1.5	3	·	·	·	1	·	1.1	·
X	·	·	·	·	1.5	1.3	1.5	1.3	6	2.0	5.5.5	3.4	9.5	3.1	2	3.0	1.7	2.6	7.3	2.9	1.9	1	·	·	·	7	3	·	·	·	2	·	4	3	·
XI	4.5	5.7	9	4.4	1.5	2.6	2.5	1.0	7.5	2.0	1.7	3.0	1.4	4.1	1.5	4.3	1.9	2.6	3.0.0	9.2	8	7	1	·	·	9	6	·	2	·	2	·	1	1.5	·
XII	3	1.7	3	2.8	2.5	1.6	0.5	1.0	3	2.3	4.2	4.8	1.0	4.0	1.1	2.9	1.8	3.2	4.4.5	1.1.8	3	2.7	8	2	·	1.5	1.1	1	6	·	2	·	2	1.4	1.0
Rok	4.4	3.0	6.3	2.3	8.4.5	2.6	2.7	1.6	7.5	2.8	3.5.7.5	3.4	1.5.4.5	3.5	7.6.5	3.4	2.1.3	2.7	7.6.5.7	6.2.3	2.2.VII	9.9	1.9	6	2.3	1.6.4	1.2.2	2.0	1.7	1	1.0	1.5	2.8	1.2.4	3.4

Dobryszyce — $H_s = 210\ m$ — $h_w = 10\ m$

I	3.5	3.6	5.5	5.5	3.5	3.4	7.5	2.5	1.4	2.9	3.3	3.4	2.3	4.2	3	4.7	·	3.6	1.7.2	4.5	6	–	–	–	–	1.2	5	·	1	·	–	–	2	1.6	–
II	3.5	2.4	4.5	2.0	5.5	2.6	9.5	3.5	1.7.5	3.1	2.3.5	3.5	1.4	4.8	5	3.8	1	3.4	5.1.3	1.0.0	1.8	–	–	–	–	1.6	1.1	1	·	·	–	–	2	1.3	–
III	5.5	2.7	9.5	3.2	1.8.5	4.8	1.1	3.5	6.5	2.6	1.3.5	3.0	1.5.5	6.3	9	2.8	4	3.8	2.6.0	7.2	1.7	–	–	–	–	8	4	·	3	·	–	–	8	8	–
IV	1.0	2.6	4.5	2.0	5.5	1.9	1.0.5	2.0	4	2.6	7	3.4	1.0.5	2.8	2.6	2.9	1.1	2.3	1.9.0	4.8	2.5	–	–	–	–	9	6	·	·	·	–	–	7	1.1	–
V	8	3.2	2.3.5	3.5	7	2.9	9.5	2.1	3.5	2.4	1.1	2.5	1.1	3.1	1.9.5	2.8	·	2.9	1.6.0	6.3	9	–	–	–	–	6	4	·	·	·	–	–	2	1.0	–
VI	6.5	2.0	9	2.5	5.5	1.8	9.5	3.1	6.5	2.7	1.7	3.5	2.1	3.3	1.3	2.5	2	2.8	4.8.1	2.0.4	2.4	–	–	–	–	6	6	2	·	·	–	–	5	3	–
VII	5.5	1.8	4	2.2	8.5	3.4	7.5	2.8	9	2.7	1.7.5	3.1	2.6.5	3.1	1.3.5	2.6	2	2.8	2.1.5.0	1.2.4.4	1.6	–	–	–	–	1.4	1.0	4	·	·	–	–	3	1.0	–
VIII	2.5	1.6	1	3.0	2.5	2.8	7.5	2.5	1.4.5	2.9	1.9	2.2	2.9.5	2.8	1.9.5	2.3	·	2.5	6.1.5	1.5.6	1.0	–	–	–	–	1.3	1.1	2	·	·	–	–	1	5	–
IX	5	1.6	·	·	1.5	1.7	8	2.1	1.3	4.3	2.7	4.0	2.4.5	4.4	9	2.1	2	3.5	7.1.1	1.0.4	2.9	–	–	–	–	1.3	1.1	3	2	1	–	–	2	8	–
X	1	2.0	0.5	1.0	1.5	3.7	1.3.5	1.9	1.8	2.9	2.7.5	3.2	1.6	4.2	9	1.8	6	2.8	5.5	3.5	1.8	–	–	–	–	5	2	·	1	·	–	–	5	6	–
XI	5	7.5	1.0	3.8	1.8.5	2.1	1.9.5	2.7	5	2.7	1.0.5	3.4	1.5.5	6.8	4	7.1	2	3.9	1.2.0	4.0	2.8	–	–	–	–	6	4	·	3	1	–	–	4	1.5	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.0.7	7.9	1.4	–	–	–	–	1.2	9	·	–	–	–	–	4	1.9	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.8.3.4	1.2.4.4	1.6.VII	–	–	–	–	1.2.0	8.3	1.2	–	–	–	–	4.6	1.2.4	–

Wrocław – Mały Gądów — $H_s = 116\ m$ — $H_b = 118{,}6\ m$ — $h_w = 22{,}5\ m$

I	1.5	3.0	5	3.1	5	2.5	2.5	2.0	8	2.2	1.8.5	3.5	2.3	4.8	1.0.5	5.0	1.9	3.1	1.8.7	6.1	6	2.5	6	6	·	1.0	6	·	1	·	2	·	3	1.6	7
II	4	1.9	5	2.5	4.5	2.1	1.2.5	2.4	2.0.5	3.8	1.6.5	3.7	8.5	6.1	5.5	5.6	7	3.3	4.3.3	1.7.3	1.8	1.7	·	·	·	1.3	8	1	2	·	4	·	1	1.1	1
III	4	3.1	5	4.0	1.7.6	3.6	1.3.5	4.5	9	6.2	7	3.5	1.6.5	6.3	1.0.5	2.8	1.0	4.0	4.7.5	1.4.3	2.9	1.7	·	·	·	1.1	7	1	7	2	3	·	4	1.0	1
IV	1.8.5	3.1	9	2.2	4.5	1.6	5	3.5	5	3.7	3.5	2.6	9	4.0	1.5.5	3.2	2.0	2.4	7.3	3.0	2.4	1.2	·	·	1	5	3	·	·	·	3	2	3	6	·
V	8.5	2.9	2.1.5	3.2	8	2.5	4	3.4	3.5	3.9	1.5	1.7	1.3.5	4.7	1.6.5	4.6	1.6	3.0	2.3.9	1.0.0	2.3	8	·	·	2	7	4	1	2	·	·	3	1	9	1
VI	9	2.6	1.2.5	2.3	9.5	2.0	5	1.8	9.5	3.9	7.5	4.5	2.2.5	4.7	9.5	3.1	5	3.3	2.8.6	1.2.0	2.4	·	·	·	1.4	6	5	1	1	·	·	3	6	7	·
VII	4	2.6	1.0	3.0	3.5	3.7	1.1.5	2.7	8	2.9	9	3.5	2.9	5.0	9	3.9	9	3.4	1.5.4.6	3.1.0	2.3	·	·	·	1.3	2.0	1.6	6	·	·	1	1.0	1	1.5	·
VIII	2.5	2.4	·	·	2.5	1.8	8.5	3.1	1.2	3.7	1.7.5	3.3	2.9	3.8	1.2	3.8	9	3.2	7.6.6	1.2.2	1.6	·	·	·	3	1.7	1.2	4	1	·	1	1.0	1	8	·
IX	0.5	2.0	2	1.5	0.5	2.0	7	2.6	1.8.5	4.4	1.7	4.6	2.6	5.1	9.5	3.5	9	3.9	6.6.1	1.0.5	1.9	2	·	·	2	1.6	1.3	1	6	·	4	·	·	1.1	·
X	1	4.0	.5	1.0	5	2.7	1.2.5	3.3	2.1.5	3.8	2.0	3.2	1.2	4.3	7.5	2.5	1.3	2.9	5.9	3.0	2.0	7	·	·	·	5	2	·	·	·	1.5	·	3	6	·
XI	4	5.1	1.1.5	3.4	2.2	2.7	1.5.5	3.3	9	4.1	3.5	3.3	1.9	7.6	3.5	4.6	2	4.2	7.4	1.9	25,28	7	1	·	·	8	3	·	6	·	3	·	1	1.7	·
XII	7	2.1	3	3.0	1.0.5	2.3	1.2.5	2.2	7.5	4.3	2.0	4.6	1.7.5	5.4	8	3.5	7	3.6	2.7.7	6.9	1.4	2.6	5	3	·	1.3	9	·	4	2	7	·	2	1.1	7
Rok	6.4.5	2.8	8.5	2.8	9.3	2.5	1.1.0	3.2	1.3.2	3.9	1.4.1.5	3.5	2.2.6.5	5.2	1.1.7.5	3.8	1.2.6	3.4	5.0.7.6	3.1.0	2.3.VII	1.2.1	1.2	9	3.5	1.3.1	8.8	1.5	3.0	4	4.3	2.2	2.6	1.3.0	1.7

Wrocław, WSR

$\varphi = 51°07'$ $\lambda = 17°05'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-0.6	2.3	0.3	0.6	3.1	-2.8	10.9	6	-12.5	17	87	80	84	84	0.9	1.6	1.1	1.2	-	-	-	-
II	-	-	-	-	2.4	6.5	3.9	4.2	7.2	0.9	10.9	5	-5.4	27	91	75	86	84	0.7	2.5	1.2	1.5	-	-	-	-
III	-	-	-	-	2.6	8.6	5.6	5.6	10.4	0.9	16.4	13	-5.4	2	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	6.0	13.2	8.9	9.2	14.4	3.9	27.0	30	-1.9	15	85	57	76	73	1.5	7.4	3.0	4.0	-	-	-	-
V	-	-	-	-	10.0	15.6	11.4	12.1	17.0	6.6	27.2	19	0.0	6	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	16.6	23.1	18.6	19.2	24.9	13.1	32.6	11	7.1	1	73	52	71	65	5.3	14.9	6.5	8.9	-	-	-	-
VII	-	-	-	-	18.0	22.8	18.9	19.6	24.4	15.8	35.3	5	12.1	28	81	63	82	75	4.3	12.1	4.6	7.0	-	-	-	-
VIII	-	-	-	-	14.9	20.5	16.1	16.9	21.8	12.7	28.8	11	8.2	31	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	11.0	16.5	12.6	13.2	17.7	8.9	28.8	8	2.1	27	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	7.0	14.3	9.4	10.0	14.9	5.3	22.3	19	-0.5	3	91	67	85	81	1.0	5.7	1.8	2.8	-	-	-	-
XI	-	-	-	-	4.5	8.0	5.5	5.9	8.8	3.1	18.3	5	-7.4	30	87	74	86	82	1.1	3.3	1.4	1.9	-	-	-	-
XII	-	-	-	-	-1.0	1.9	0.2	0.3	3.0	-3.3	9.4	8	-14.9	17	91	82	89	87	0.6	1.4	0.7	0.9	-	-	-	-
Rok	-	-	-	-	7.6	12.8	9.3	9.8	14.0	5.4	35.3	5.VII	-14.9	17.XII	-	-	-	-	-	-	-	-	-	-	-	-

Chełm Lubelski

$\varphi = 51°08'$ $\lambda = 23°30'$

I	993.4	1005.8	980.8	1022.2	-2.9	-1.4	-1.8	-2.0	-0.2	-4.4	5.2	7	-16.0	17	85	83	86	85	0.7	0.9	0.7	0.8	8.8	8.5	8.3	8.5
II	987.1	1003.9	965.7	1013.3	0.4	3.3	1.5	1.7	4.5	-0.8	9.7	15	-6.2	28	88	79	85	84	0.8	1.7	1.0	1.2	7.9	8.2	5.6	7.2
III	993.6	1006.6	970.2	1019.9	-1.8	4.5	0.7	1.0	6.0	-3.4	16.3	30	-15.3	4	83	56	75	71	1.0	4.4	1.8	2.4	5.2	5.5	3.7	4.8
IV	992.4	1004.2	963.7	1017.9	5.6	12.8	8.2	8.7	14.2	2.7	26.4	30	-7.5	10	80	50	71	67	2.1	9.1	3.6	4.9	5.2	6.2	4.1	5.2
V	989.9	999.9	976.6	1015.2	9.5	13.8	10.2	10.9	15.1	6.4	23.4	18	0.0	5	82	64	80	75	2.2	6.7	2.7	3.9	6.6	8.0	6.8	7.1
VI	991.8	1003.9	979.3	1016.5	16.3	22.2	17.0	18.1	23.8	11.3	31.3	12	6.3	7	75	51	75	67	4.6	13.7	5.1	7.8	4.4	5.7	3.9	4.7
VII	987.6	999.3	972.1	1012.2	17.1	22.3	18.0	18.8	24.2	13.9	33.0	5	9.4	4	82	60	80	74	3.5	12.0	4.6	6.7	6.6	6.4	6.2	6.4
VIII	989.8	998.2	978.6	1014.6	14.7	20.1	15.5	16.4	21.6	11.5	30.2	14	6.3	24	87	64	84	78	2.2	9.1	2.9	4.7	5.6	6.5	3.4	5.2
IX	988.1	999.0	974.5	1013.2	10.3	15.7	11.2	12.1	16.8	7.9	27.2	9	-0.8	27	91	65	87	81	1.2	6.8	1.8	3.3	6.3	7.4	4.6	6.1
X	995.4	1006.5	981.3	1021.0	5.5	12.1	7.5	8.2	12.8	4.0	20.1	19	-2.1	3	90	66	85	80	1.0	5.2	1.6	2.6	6.5	5.6	4.4	5.2
XI	995.6	1015.7	973.3	1024.8	2.1	5.4	3.2	3.4	6.3	0.8	16.1	1	-10.1	30	94	83	91	89	0.4	1.7	0.7	0.9	7.2	8.1	7.0	7.4
XII	989.8	1008.0	954.4	1016.4	-3.6	-1.1	-2.7	-2.5	0.2	-5.7	9.0	14	-15.8	16	90	84	89	88	0.5	0.9	0.6	0.7	6.3	7.1	5.8	6.4
Rok	991.4	1015.7	954.4	1017.0	6.1	10.8	7.4	7.9	12.1	3.7	33.0	5.VII	-16.0	17.1	86	67	82	78	1.7	6.0	2.3	3.3	6.3	6.9	5.3	6.2

Pszczela Wola

$\varphi = 51°07'$ $\lambda = 22°31'$

I	-	-	-	-	-2.7	-0.9	-4.8	-4.8	0.0	-	5.5	6	-	-	-	-	-	-	-	-	-	-	8.8	8.4	7.8	8.3
II	-	-	-	-	0.9	4.0	1.8	2.1	4.8	-0.3	9.0	6,15,24	-8.0	24	-	-	-	-	-	-	-	-	7.9	7.9	7.9	7.9
III	-	-	-	-	-1.1	5.4	1.0	1.6	6.4	-2.4	16.0	31	-14.1	3	-	-	-	-	-	-	-	-	5.5	5.6	4.0	5.0
IV	-	-	-	-	5.2	13.3	7.5	8.4	14.2	3.1	25.8	30	-4.5	10	-	-	-	-	-	-	-	-	5.6	5.4	4.4	5.1
V	-	-	-	-	9.4	14.1	9.5	10.6	15.1	6.1	23.6	18	0.5	7	-	-	-	-	-	-	-	-	6.9	7.5	6.1	6.8
VI	-	-	-	-	16.5	22.8	16.1	17.9	24.0	10.3	30.7	12	4.7	7	-	-	-	-	-	-	-	-	4.3	5.1	3.5	4.3
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Namysłów

$\varphi = 51°05'$ $\lambda = 17°43'$

I	-	-	-	-	-1.8	1.5	-0.7	-0.4	2.3	-3.4	9.3	6	-16.5	17	82	80	82	81	0.9	1.5	1.0	1.1	9.0	8.0	6.7	7.9
II	-	-	-	-	1.3	5.7	2.8	3.2	6.7	0.3	10.1	14	-4.3	27	86	74	84	81	0.9	2.5	1.2	1.5	8.9	7.9	7.1	8.0
III	-	-	-	-	1.7	8.4	4.3	4.7	9.8	0.0	16.3	13	-9.7	1	-	-	-	-	-	-	-	-	6.2	6.3	5.8	6.1
IV	-	-	-	-	5.4	12.8	7.0	8.0	14.1	2.0	26.1	30	-4.9	15	-	-	-	-	-	-	-	-	5.9	6.3	5.1	5.8
V	-	-	-	-	9.6	14.9	9.6	10.9	16.2	5.0	26.8	19	-1.1	7	78	56	79	71	2.7	8.2	2.8	4.6	5.1	6.2	5.3	5.5
VI	-	-	-	-	16.0	22.4	16.8	18.0	24.4	10.5	31.7	30	4.4	1	-	-	-	-	-	-	-	-	4.5	4.6	4.7	4.6
VII	-	-	-	-	17.6	22.7	17.8	19.0	24.6	14.1	35.6	5	10.3	3,19,29	-	-	-	-	-	-	-	-	7.0	6.7	7.3	7.0
VIII	-	-	-	-	14.6	20.3	14.7	16.1	22.0	10.7	29.3	11	4.8	31	-	-	-	-	-	-	-	-	6.5	6.3	4.2	5.7
IX	-	-	-	-	10.7	16.3	11.3	12.4	17.2	8.0	28.6	9	-1.2	26	89	64	87	80	1.5	7.4	1.9	3.6	6.9	6.7	5.8	6.5
X	-	-	-	-	6.5	13.8	7.7	8.9	14.7	3.7	22.0	19	-1.8	2	94	72	90	85	0.7	5.3	1.1	2.4	7.5	6.4	3.0	5.6
XI	-	-	-	-	4.0	7.7	5.1	5.5	8.5	2.6	18.2	5	-7.9	30	89	72	85	82	0.9	3.5	1.4	1.9	8.8	7.9	8.2	8.3
XII	-	-	-	-	-1.8	1.5	-0.6	-0.4	2.7	-3.8	11.0	13	-16.9	17	-	-	-	-	-	-	-	-	8.3	8.1	4.9	7.1
Rok	-	-	-	-	7.0	12.3	8.0	8.8	13.6	4.1	35.6	5.VII	-16.9	17.XII	-	-	-	-	-	-	-	-	7.0	6.8	5.7	6.5

Wrocław, WSR

$H_s = 117\ m$

1957

MIESIĄC	ROZKŁAD WIATRU °D, °mD																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min ≤ 0°	Max ≤ 0°	Min ≤ -10°	Max ≥ 25°	0.1 ÷ 1.0 mm	1.0 ÷ 10.0 mm	10.0 ÷ mm	10 ÷ 15 m/s	15 ÷ m/s	≡	≋	⊙	⊕	▦
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21.3	7.0	6	22	6	3	·	7	6	·	–	–	12	·	–	–	5
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43.9	16.3	18	11	·	·	·	12	8	1	–	–	7	·	–	–	2
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57.1	18.7	29	14	·	·	·	8	7	1	–	–	7	·	–	–	1
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.7	4.5	24	6	·	·	1	6	3	·	–	–	5	1	–	–	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25.1	9.3	8	·	·	·	2	7	8	·	–	–	·	1	–	–	1
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	59.5	21.0	19	·	·	·	17	10	6	3	–	–	·	1	–	–	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	157.2	33.3	10	·	·	·	12	22	17	6	–	–	·	2	–	–	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	70.4	13.6	16	·	·	·	4	16	13	2	–	–	1	1	–	–	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	78.9	13.2	19	·	·	·	2	17	14	3	–	–	4	·	–	–	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.3	3.4	20	1	·	·	·	6	2	·	–	–	16	·	–	–	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.0	3.3	25	7	1	·	·	6	2	·	–	–	14	·	–	–	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35.3	8.3	8	23	4	2	·	15	8	·	–	–	20	·	–	–	9
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	573.7	33.3	10.VII	84	11	5	38	132	92	16	–	–	86	6	–	–	18

Chełm Lubelski

$H_s = 209\ m$ $H_b = 209{,}6\ m$ $h_w = 12\ m$

I	0.5	2.0	4.5	3.7	8	4.1	11	6.3	12	2.8	20.5	5.7	2.6	6.3	6.5	8.2	4	5.1	17.7	7.0	6	26	14	5	·	7	5	·	7	·	3	·	1	24	26
II	4	2.6	4	2.6	4	1.2	10.5	3.5	17	4.2	29.5	4.7	10	5.0	5	4.5	·	4.1	32.4	8.5	3	15	2	·	·	15	10	·	·	·	3	·	2	13	5
III	10	3.0	10	2.8	6.5	4.6	17	7.4	8	2.9	10.5	3.2	13	8.8	10	5.8	10	4.7	16.7	5.8	15	22	7	2	·	6	4	·	9	2	·	·	7	5	5
IV	10.5	2.8	6	3.1	6.5	1.9	16	2.6	12.5	2.3	8.5	2.4	9	3.1	6	4.0	15	2.2	12.5	5.7	11	6	·	·	3	7	3	·	·	·	1	·	8	6	1
V	10.5	2.3	16	3.3	9.5	3.3	10.5	3.5	4	3.5	7	2.4	8	4.7	13.5	3.2	14	2.7	56.8	22.6	6	·	·	·	·	13	10	1	·	·	·	2	·	12	·
VI	5.6	3.3	4	2.2	2	2.0	10.5	2.9	19.5	2.3	16.5	4.2	12.5	4.2	6.5	4.8	13	2.7	77.9	18.2	4	·	·	·	11	9	7	4	1	·	·	5	6	4	·
VII	1	1.0	2	2.0	5	2.6	14.6	2.4	14.5	1.8	29.5	3.5	13	4.4	15	2.7	12	2.6	84.6	25.1	23	·	·	·	16	17	11	3	·	·	1	10	3	14	·
VIII	1	5.0	2	2.0	1	1.0	11.5	2.8	16.5	1.8	21	3.4	18	3.6	7	4.0	15	2.5	107.0	21.6	29	·	·	·	4	15	13	4	·	·	1	6	2	5	·
IX	4	2.2	1	1.0	0.5	1.0	9	2.4	16	4.2	28	7.1	18	7.7	5.5	3.5	8	5.1	68.8	22.9	29	1	·	·	1	14	13	2	8	5	1	·	4	10	·
X	1	3.0	0.5	2.0	1.5	1.3	4.5	3.2	17	4.1	26	4.1	10.5	3.8	4	2.2	28	2.2	8.0	4.6	25	2	·	·	·	3	3	·	3	·	1	·	6	7	·
XI	4	9.6	5.5	6.2	16	2.1	26.5	3.2	4.5	1.1	7	3.7	15	9.5	15	10.0	10	4.2	19.2	6.3	28	12	2	1	·	10	6	·	7	3	3	·	4	16	2
XII	4.5	3.3	5.5	2.3	5.5	1.1	10	2.6	13.5	4.3	28	5.7	10	6.2	2	10.2	14	3.9	18.4	7.4	8	28	12	5	·	9	5	·	6	5	1	·	5	11	26
Rok	56.5	3.3	61	2.8	66	2.2	154.5	3.6	153	2.9	232	4.2	163	5.6	69	4.8	143	3.5	549.0	25.1	23.VII	112	37	13	35	125	90	14	41	15	15	23	48	127	65

Pszczela Wola

$H_s = 198\ m$ $h_w = 18\ m$

I	6	2.7	·	·	4	2.8	5	1.4	18.5	2.2	19	1.8	14.5	2.0	1	4.0	25	1.5	21.3	8.1	6	–	13	–	·	10	4	·	·	·	–	·	1	21	–
II	3	2.0	5.5	4.2	3	3.0	2	1.5	21	2.2	19	2.2	10	2.2	3.5	2.7	17	1.7	35.7	7.2	9.22	13	2	·	·	–	–	·	·	·	–	·	·	16	–
III	3	3.3	5.5	2.5	8.5	2.8	7	2.4	14	1.6	4	2.2	2.5	2.7	2	1.0	24	1.8	22.3	10.3	15	21	8	2	·	6	4	1	·	·	–	·	8	8	–
IV	4.5	1.8	8	1.8	11	1.5	1	1.0	6	1.5	2	1.3	15.5	1.3	5	1.5	37	0.9	7.0	3.9	7	4	·	·	1	–	–	–	·	·	–	·	6	7	–
V	7.5	2.3	4.5	2.0	4	1.5	·	·	4	2.2	·	·	1.7	1.8	6	2.3	50	0.9	39.0	12.8	7	·	·	·	·	6	5	2	·	·	–	2	4	16	–
VI	6.5	1.5	2	1.5	·	·	2.5	2.2	1.9	1.5	4.5	1.6	1.8	1.8	4.5	1.8	34	1.0	44.8	13.2	10	·	·	·	11	9	8	2	·	·	–	4	6	1	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Namysłów

$H_s = 151\ m$ $h_w = 13{,}6\ m$

I	1	1.0	6.5	3.8	4.5	3.6	4	1.5	15.5	2.2	17.5	2.9	2.2	3.7	6	6.9	16	2.8	27.9	6.8	6	24	7	3	·	16	9	·	2	·	–	·	·	18	18
II	0.5	2.0	1.5	3.0	3	4.6	6.5	2.9	17	3.3	18.5	3.0	15.5	3.6	8.5	3.3	13	2.8	36.8	6.6	8	13	·	·	·	17	10	·	2	·	3	·	·	13	3
III	1.5	2.0	3	4.2	17	5.1	15.5	5.3	15.5	4.2	7.5	3.4	14.5	6.0	7.5	3.3	11	4.2	50.6	10.3	29	16	·	·	·	8	8	1	5	1	2	·	7	12	2
IV	10	2.8	8.5	2.2	1.5	2.3	4.5	2.9	8.5	3.4	7.5	4.0	1.5	2.7	19.5	2.6	15	2.4	25.5	12.6	30	10	·	·	1	10	6	1	1	·	3	1	4	7	·
V	1.5	1.7	17.5	3.4	15.5	3.6	6.5	2.8	2.6	2.8	2.5	3.0	7	3.1	19	3.2	21	2.5	42.5	26.5	20	2	·	·	2	8	5	1	·	·	1	2	5	7	·
VI	2	2.5	7.5	3.0	2.5	3.4	6	2.8	9.5	2.7	9	2.0	16.5	3.2	11	2.7	21	2.2	61.9	24.2	4	·	·	·	14	7	5	2	·	·	·	3	8	6	·
VII	0.5	2.0	2	1.5	6	2.6	5.5	2.5	2	1.8	18	2.1	2.2	2.0	14	2.0	23	1.6	110.1	37.5	16	·	·	·	14	20	18	3	·	·	2	3	4	17	·
VIII	·	·		·	·	·	3.5	2.3	5.5	1.9	23.5	1.9	1.7	2.2	12.5	1.9	3.1	1.4	49.7	10.7	24	·	·	·	6	14	9	1	1	1	1	2	2	6	·
IX	·	·	2	1.5	0.5	1.0	3	1.7	10	1.9	25	2.6	24.5	3.1	9	2.9	16	2.2	92.2	16.5	23	2	·	·	2	17	14	1	1	·	1	1	1	8	·
X	·	·	1	1.0	3	1.7	8.5	1.4	1.7	1.6	17.5	2.2	13.5	2.4	4.5	3.8	28	1.4	7.1	3.7	20	3	·	·	·	6	3	·	1	·	9	·	4	4	·
XI	3.5	1.2	6.5	6.6	19.5	4.1	16.5	2.8	12.5	2.0	8	2.2	16	5.8	1.5	6.3	6	4.0	45.2	7.2	28	8	1	·	·	8	5	·	3	1	5	·	1	21	·
XII	0.5	2.0	5	3.4	0.5	4.0	9	2.1	13	1.4	17	3.1	14.5	2.9	15.5	2.6	18	2.1	45.2	11.6	14	26	5	4	·	17	10	2	1	·	3	·	1	10	15
Rok	2.1	1.4	6.1	2.8	78.5	3.0	89	2.6	128.5	2.4	171.5	2.7	19.8	3.4	128.5	3.5	219	2.6	564.7	37.5	16.VII	104	13	7	39	148	102	12	17	3	–	12	37	129	38

Przedbórz

$\varphi = 51°05'$ $\lambda = 19°52'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.3	0.1	-2.0	-1.6	1.2	-4.6	6.6	6	-17.0	17	92	80	89	87	0.4	1.2	0.6	0.7	9.9	8.6	7.1	8.5
II	–	–	–	–	1.1	4.9	1.9	2.4	6.0	-0.4	11.5	6	-4.8	24	94	77	89	87	0.4	2.2	0.8	1.1	9.9	8.9	7.6	8.8
III	–	–	–	–	-0.1	7.2	2.3	2.9	8.7	-2.0	17.1	27	-9.4	4	88	58	79	75	0.8	4.9	1.8	2.5	–	–	–	–
IV	–	–	–	–	4.8	12.9	7.2	8.0	14.5	2.2	26.4	30	-6.4	15	89	56	79	75	1.1	8.1	2.4	3.9	6.9	7.2	6.0	6.7
V	–	–	–	–	8.7	14.3	9.3	10.4	16.0	4.8	26.5	20	-0.9	6	85	56	78	73	1.7	8.4	2.8	4.3	6.5	8.6	7.1	7.4
VI	–	–	–	–	15.8	22.7	16.2	17.7	24.3	10.4	30.6	30	4.7	26	82	58	78	73	3.3	12.2	4.2	6.6	4.4	4.8	5.1	4.8
VII	–	–	–	–	16.8	22.7	17.3	18.5	24.4	13.6	34.4	8	9.8	29	87	63	84	78	2.7	12.0	3.5	6.1	6.9	7.2	7.5	7.2
VIII	–	–	–	–	13.7	20.2	14.3	15.6	21.9	11.1	28.3	12	6.3	24	95	67	89	84	0.7	8.4	1.8	3.6	6.9	8.3	5.5	6.9
IX	–	–	–	–	9.6	15.5	11.1	11.8	16.9	7.6	27.6	9	0.1	26	94	68	88	83	0.7	6.4	1.7	2.9	8.0	7.6	6.2	7.3
X	–	–	–	–	6.5	13.2	8.0	8.9	14.0	4.6	21.4	19	-0.9	3	95	71	90	85	0.5	4.8	1.1	2.1	–	–	–	–
XI	–	–	–	–	2.8	6.4	3.1	3.8	7.5	0.9	17.4	4	-8.8	30	92	77	91	87	0.6	2.6	0.7	1.3	6.7	6.3	6.4	6.5
XII	–	–	–	–	-2.4	-0.1	-1.7	-1.5	1.3	-4.7	8.6	13	-16.7	16	93	85	89	89	0.3	0.9	0.6	0.6	–	–	–	–
Rok	–	–	–	–	6.2	11.7	7.2	8.1	13.1	3.6	34.4	8.VII	-17.0	17.I	90	68	85	81	1.1	6.0	1.8	3.0	–	–	–	–

Laskowice Oławskie

$\varphi = 51°03'$ $\lambda = 17°21'$

I	–	–	–	–	-1.6	1.6	-0.8	-0.4	2.3	-3.5	9.5	6	-15.7	17	86	79	84	83	0.8	1.5	0.9	1.1	8.0	8.0	6.3	7.4
II	–	–	–	–	1.8	5.8	2.9	3.4	6.4	0.4	10.4	14	-7.4	27	88	73	87	83	0.9	2.6	1.1	1.5	7.3	7.3	6.5	7.0
III	–	–	–	–	1.5	8.0	4.3	4.5	9.8	0.1	16.0	13	-6.9	1	86	60	79	75	1.0	4.7	2.0	2.6	6.3	6.2	5.1	5.9
IV	–	–	–	–	4.9	12.2	7.4	8.0	13.5	2.1	26.0	30	-5.0	15	91	57	81	76	0.8	7.3	2.0	3.4	5.7	7.1	5.4	6.1
V	–	–	–	–	9.3	14.8	10.1	11.1	16.1	5.3	26.1	19	-0.9	7	86	58	82	75	1.8	7.9	2.4	4.0	5.5	7.2	5.3	6.0
VI	–	–	–	–	16.4	22.4	17.2	18.3	24.2	11.1	31.2	30	4.2	1	81	59	84	75	3.6	12.2	3.2	6.3	4.6	5.6	4.8	5.0
VII	–	–	–	–	17.3	22.3	17.9	18.8	23.9	14.6	35.4	5	10.5	19	87	67	88	81	3.0	10.7	2.9	5.5	7.3	6.9	7.0	7.1
VIII	–	–	–	–	14.4	20.1	15.3	16.3	21.4	11.5	27.9	11	5.0	31	91	66	88	82	1.4	8.4	2.1	4.0	5.7	7.1	5.1	6.0
IX	–	–	–	–	10.3	16.1	11.7	12.4	17.2	7.9	27.4	8	-0.2	26	90	64	86	80	1.3	7.3	2.0	3.5	6.8	7.6	6.7	7.0
X	–	–	–	–	5.7	13.7	8.4	9.0	14.4	3.5	21.6	19	-1.7	2,3	94	68	88	83	0.7	5.4	1.4	2.5	7.1	6.7	4.0	5.9
XI	–	–	–	–	3.9	7.7	4.8	5.3	8.4	2.2	18.2	5	-7.6	30	88	72	86	82	1.0	3.5	1.2	1.9	8.5	7.9	7.9	8.1
XII	–	–	–	–	-1.9	1.0	-0.8	-0.6	2.3	-3.8	8.9	8	-17.0	17	89	81	87	86	0.6	1.3	0.8	0.9	7.2	7.9	6.2	7.1
Rok	–	–	–	–	6.8	12.1	8.2	8.8	13.3	4.3	35.4	5.VII	-17.0	17.XII	88	67	85	80	1.4	6.1	1.8	3.1	6.7	7.1	5.9	6.6

Suchedniów

$\varphi = 51°03'$ $\lambda = 20°50'$

I	–	–	–	–	-2.5	0.3	-1.8	-1.4	1.4	-5.0	7.1	6	-17.8	17	87	81	89	86	0.6	1.3	0.6	0.8	8.6	7.8	7.4	7.9
II	–	–	–	–	0.8	4.5	2.2	2.4	5.7	-0.9	10.2	21	-6.6	24	89	77	88	85	0.7	2.1	0.9	1.2	7.3	6.3	6.3	6.6
III	–	–	–	–	-1.2	6.5	1.1	1.9	9.8	-3.8	16.9	28,31	-12.0	8,9,10	–	–	–	–	–	–	–	–	5.9	4.9	3.5	4.8
IV	–	–	–	–	4.2	13.0	5.8	7.2	14.2	-0.4	25.6	30	-8.6	15	89	54	85	76	1.0	8.5	1.4	3.6	5.4	5.4	3.2	4.7
V	–	–	–	–	8.5	13.4	8.2	9.6	14.9	3.1	25.2	19	-3.5	29	83	62	87	77	2.0	7.1	1.4	3.5	5.8	7.4	5.2	6.1
VI	–	–	–	–	16.4	22.6	15.4	17.4	24.3	8.2	31.5	30	0.5	7	71	50	80	67	5.8	14.2	5.7	7.9	3.8	4.0	3.9	3.9
VII	–	–	–	–	17.3	22.2	16.8	18.3	24.3	12.2	35.2	5	6.5	4	82	64	87	78	4.0	11.3	2.8	6.0	5.6	6.0	6.6	6.1
VIII	–	–	–	–	13.9	19.7	14.0	15.4	21.7	9.1	29.8	12	1.9	24	–	–	–	–	–	–	–	–	5.4	5.8	3.5	4.9
IX	–	–	–	–	9.6	15.6	10.0	11.3	16.9	5.9	27.7	9	-2.3	26	90	66	92	83	1.3	6.9	1.1	3.1	5.1	5.4	5.8	5.4
X	–	–	–	–	5.3	13.1	6.3	7.8	14.0	2.1	21.8	10	-5.1	3	93	68	92	84	0.6	5.1	0.9	2.2	5.2	5.2	3.7	4.7
XI	–	–	–	–	2.2	6.4	2.3	3.3	7.6	-0.2	18.3	4	-9.6	30	92	78	90	87	0.5	2.4	0.7	1.2	7.5	5.3	6.3	6.4
XII	–	–	–	–	-2.9	-0.2	-1.9	-1.7	1.4	-5.4	10.3	14	-20.4	17	89	84	87	87	0.5	4.0	0.7	0.7	7.2	7.7	6.4	7.1
Rok	–	–	–	–	6.0	11.4	6.5	7.6	12.8	2.1	35.2	5.VII	-20.4	17.XII	–	–	–	–	–	–	–	–	6.1	5.9	5.2	5.7

Kluczbork

$\varphi = 50°59'$ $\lambda = 18°13'$

I	–	–	–	–	-4.5	1.4	-0.9	-0.5	–	-3.5	–	–	-17.3	17	–	–	–	–	–	–	–	–	7.0	7.7	6.9	7.2
II	–	–	–	–	2.0	5.7	2.4	3.1	–	0.0	–	–	-4.8	23	–	–	–	–	–	–	–	–	7.5	7.2	5.8	6.8
III	–	–	–	–	2.0	7.7	3.9	4.4	–	-0.5	–	–	-9.6	1	–	–	–	–	–	–	–	–	5.6	5.7	4.1	5.1
IV	–	–	–	–	4.8	12.1	6.9	7.7	–	1.7	–	–	-6.0	15	–	–	–	–	–	–	–	–	5.2	6.3	4.3	5.3
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16.3	22.7	17.2	18.4	–	10.8	–	–	3.8	28	–	–	–	–	–	–	–	–	3.7	4.4	3.5	3.9
VII	–	–	–	–	17.8	22.5	17.9	19.0	–	13.4	–	–	8.8	19	–	–	–	–	–	–	–	–	6.5	6.9	6.7	6.7
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	4.0	7.3	4.0	4.8	–	1.3	–	–	-8.0	21	–	–	–	–	–	–	–	–	6.6	7.1	7.3	7.0
XII	–	–	–	–	-1.6	1.3	-0.5	-0.3	–	-3.7	–	–	-17.3	17	–	–	–	–	–	–	–	–	6.9	7.0	6.3	6.7
Rok	–	–	–	–	–	–	–	–	–	–	–	–	-17.3	17.I,17XII	–	–	–	–	–	–	–	–	–	–	–	–

Przedbórz

$H_s = 235$ m $h_w = 10{,}5$ m **1957**

MIESIĄC	ROZKŁAD WIATRU °D.=mD																	OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość			Temperatura T				Opad R			Wiatr v						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max>25°	0.1 ≤ n < 1.0	1.0 ≤ n < 10.0	10.0 ≤ n	v ≥ 10	v ≥ 15	≡	≥5	◔	●	⊠
I	1	2.0	7	2.7	·	·	6	1.5	10	1.7	17	2.2	12	2.6	6	4.5	34	1.5	21.0	4.9	6	25	9	4	·	10	7	·	1	·	–	–	·	23	–
II	2	2.0	5	1.6	1	3.0	11	2.6	17	2.6	15	2.8	9	4.4	3	2.7	21	2.1	41.4	7.8	7	18	2	·	·	14	12	·	1	·	3	–	·	21	–
III	8	3.0	9	3.3	10.5	2.8	11.5	4.7	7	2.4	6	2.7	13.5	4.3	5.5	5.2	22	2.8	26.9	8.5	15	20	2	·	·	5	4	·	1	·	·	–	–	–	–
IV	2.1	3.1	4.5	3.4	3.5	4.3	3	3.8	0.5	2.0	4.5	4.0	5	2.4	2.3	3.3	25	2.4	22.0	6.5	7	11	·	·	1	8	6	·	·	·	·	–	6	16	–
V	1.9	3.3	19.5	3.7	7	4.5	2.5	3.8	1	3.0	2	4.0	5.5	5.4	17.5	3.6	19	3.0	30.6	9.1	20	4	·	·	2	6	5	·	·	·	·	–	1	13	–
VI	8	3.6	1.0	3.0	4	4.0	6.5	4.2	2.5	4.4	4.5	3.9	1.8	3.8	15.5	3.6	21	2.8	76.8	25.1	9	·	·	·	13	7	7	3	·	·	·	–	8	5	–
VII	1.5	2.5	5.5	2.7	7	3.9	3	4.5	4.5	5.0	2.5	2.6	1.5	4.3	22.5	4.0	1.8	3.0	196.8	75.5	16	·	·	·	14	13	12	7	·	·	·	–	3	17	–
VIII	2	2.5	·	·	0.5	5.0	2.5	4.6	2	5.0	4	3.0	1.3	3.6	3.8	3.0	31	2.2	96.4	24.5	14	·	·	·	6	14	11	4	·	·	2	–	1	9	–
IX	6.5	3.1	·	·	1	3.0	1	5.0	1	3.0	8.5	3.4	1.8	4.2	2.7	4.4	2.7	2.8	61.3	13.3	29	·	·	·	2	12	10	3	·	·	10	–	1	15	–
X	2.5	2.0	·	·	1	2.0	.5	3.6	4	3.8	13.5	3.4	1.6	4.0	1.7	3.3	3.4	2.2	8.3	3.2	18	1	·	·	·	4	4	·	·	·	18	–	–	–	–
XI	5	6.8	6	3.7	1.7	5.0	1.2	4.8	7	3.1	4.5	4.6	1.4.5	6.1	3	6.7	21	3.9	14.4	6.5	28	12	2	·	·	5	4	·	5	·	6	–	5	14	–
XII	9.5	3.9	4.5	2.2	4	2.5	8	3.2	1.5	3.4	9	4.4	11	4.2	9	2.9	23	2.6	33.9	6.5	14	26	10	3	·	11	7	·	1	·	5	–	–	–	–
Rok	99.5	3.2	71	2.2	56.5	3.3	72	3.9	71.5	3.3	91	3.2	150.5	4.1	187	3.9	296	2.6	629.8	75.3	16.VII	115	25	7	38	109	89	47	9	·	–	–	–	–	–

Laskowice Oławskie

$H_s = 135$ m $h_w = 13$ m

I	2.5	2.4	4.5	6.8	5	2.6	9	1.8	18.5	2.2	27.5	2.5	16	6.2	3	5.2	7	3.1	21.9	5.7	6	22	8	5	·	13	8	·	2	·	8	·	2	16	17
II	1	2.0	3	2.7	4	2.5	13.5	2.8	23	3.2	19.5	4.1	8	6.1	8	4.6	4	3.5	38.7	9.7	18	11	1	·	·	15	7	·	3	1	4	·	1	13	1
III	2.5	2.8	8	4.9	1.7	4.6	12.5	3.4	5	1.9	11.5	2.8	15.5	6.0	10	3.4	11	3.6	61.5	15.7	29	16	·	·	·	9	8	2	5	·	1	1	7	11	1
IV	1.2	2.9	5.5	2.4	1	2.5	9	3.6	3	5.3	9.5	2.9	9.5	1.7	1.4.5	4.0	2.6	2.2	29.0	7.4	7	11	·	·	1	13	8	·	2	·	·	3	4	10	·
V	8.5	3.4	1.4	4.2	2.5	5.4	5.5	3.3	1.5	4.7	1.5	1.3	1.4	5.2	18.5	3.9	2.7	2.9	55.2	20.8	23	2	·	·	1	10	5	3	1	·	1	5	2	9	1
VI	6.5	3.3	1.1	3.0	5.5	2.9	6	4.8	7.5	2.3	7.5	4.6	11.5	4.8	11.5	3.9	2.3	2.8	46.7	18.1	24	·	·	·	12	8	5	2	1	·	·	3	6	5	·
VII	6.5	1.9	3.5	3.7	4	2.6	6.5	2.8	5	2.6	16	3.2	17.5	4.1	1.0	3.4	2.4	2.4	150.7	27.2	14	·	·	·	11	22	19	5	·	·	7	3	17	·
VIII	0.5	3.0	·	·	3	3.3	6.5	3.8	11.5	3.6	17	3.7	2.7	5.3	4.5	2.4	2.3	2.6	46.1	9.9	24	·	·	·	3	14	10	·	1	·	·	5	2	8	·
IX	2	2.5	0.5	1.0	1.5	2.7	7.5	3.1	1.7	3.9	18.5	4.3	1.8	5.6	6	4.2	1.9	3.4	72.0	12.9	19	1	·	·	2	20	13	2	3	·	1	·	1	14	·
X	0.5	1.0	1	1.0	8.5	2.2	1.8	2.9	14.5	3.9	12.5	4.0	1.3	4.3	3	3.7	2.2	2.6	52	3.1	20	6	·	·	·	5	2	·	1	·	11	·	3	6	·
XI	2.5	5.0	1.5	5.3	18.5	4.0	1.6	3.7	2	2.5	7	5.4	1.5	8.8	4	10.1	1.0	4.9	11.3	5.8	29	8	1	·	·	8	4	·	8	·	5	·	1	20	·
XII	5.5	2.8	4	2.0	5.5	3.7	1.4	2.9	11.5	3.5	1.9	4.6	12.5	5.3	6	3.8	1.5	3.2	27.6	7.3	8	26	6	3	·	13	7	·	4	1	5	·	1	13	8
Rok	50.5	2.8	70	3.1	76	3.2	12.4	3.2	120	3.3	16.7	3.6	177.5	5.3	99	4.4	2.1.1	3.1	565.9	27.2	14.VII	103	16	8	30	150	96	14	31	2	36	22	33	14.2	28

Suchedniów

$H_s = 272$ m $h_w = 13{,}5$ m

I	1	3.0	3.5	3.0	2	3.5	4.5	2.6	6	2.2	15.6	2.9	21.5	3.5	7	4.9	3.2	2.2	32.5	7.5	6	25	8	5	·	17	9	·	1	·	4	·	3	18	18
II	4	1.5	1.5	1.0	0.5	1.0	6.5	2.7	15.5	3.8	19.5	3.5	1.3	3.7	6.5	1.9	17	2.4	27.5	5.0	2	16	2	·	·	16	11	·	·	·	3	·	4	12	2
III	3.5	4.0	4	3.9	7	4.6	12	4.5	6	2.6	9.5	2.8	1.5	4.0	7	3.0	29	2.6	22.8	8.5	15	25	3	4	·	7	3	·	1	·	·	·	11	8	·
IV	13.5	2.2	4	4.2	2	4.0	3.5	3.3	6.5	4.2	2.5	2.6	5.5	2.2	11.5	2.4	41	1.6	31.3	10.8	30	16	·	·	1	10	5	1	·	·	1	5	8	6	·
V	1.5	2.3	8.5	3.0	3	2.0	2.5	3.0	2	1.5	1.5	2.3	9.5	2.6	1.5	1.7	36	1.4	35.9	14.0	10	7	·	·	1	10	7	2	·	·	·	1	2	10	·
VI	3.5	3.0	2.5	2.2	1.5	1.7	7	2.6	9	2.3	7.5	2.9	16.5	3.0	9.5	2.1	33	1.7	33.4	9.5	7	·	·	·	12	9	7	·	·	·	5	11	3	·
VII	4	1.9	1	1.0	5.5	3.4	6	3.6	4.5	1.7	14.5	2.8	19	3.4	9.5	2.8	29	2.0	146.3	63.0	16	·	·	·	14	17	11	4	·	·	3	4	12	·
VIII	2	2.5	0.5	7.0	1	1.0	3.5	3.0	4.5	2.9	10.5	3.1	28.5	2.9	8.5	2.8	34	1.9	72.8	18.2	14	·	·	·	6	16	12	1	·	·	5	7	5	·
IX	1.5	2.3	·	·	·	·	0.5	3.0	6	3.2	1.2	4.3	3.1.5	4.3	8.5	3.1	30	2.6	66.0	15.2	29	2	·	·	2	15	12	1	·	·	1	·	5	8	·
X	·	·	·	·	1	3.0	2.5	3.0	7	2.6	1.9	2.6	1.9	3.7	4.5	2.0	4.0	1.7	6.2	4.0	22	10	·	·	·	5	2	·	·	·	2	·	8	5	·
XI	3	6.0	8.5	3.6	12.5	3.4	9.5	3.9	11.5	3.4	8	3.7	11.5	4.3	4.5	8.3	21	3.1	20.2	11.1	28	13	2	·	·	7	4	1	1	·	4	·	5	14	·
XII	1.1	1.4	1	1.0	0.5	1.0	1.5	2.3	1.2	2.6	2.1	2.8	13.5	3.6	7.5	2.3	2.5	1.9	32.1	9.4	8	30	9	6	·	9	6	·	·	·	2	·	3	15	7
Rok	6.2	2.5	35	2.5	36.5	2.4	59.5	3.1	90.5	2.8	14.1	3.0	20.4	3.4	99.5	3.1	36.7	2.1	527.0	63.0	16.VII	144	24	15	36	138	89	10	3	·	17	17	71	11.6	27

Kluczbork

$H_s = 180$ m $h_w = 16$ m

I	·	·	5	3.2	1	3.0	·	·	3.5	4.0	7.5	1.3	13.5	2.1	2.5	3.6	60	0.8	31.3	9.5	5	24	–	3	–	8	6	·	·	·	–	–	4	17	–
II	1.5	1.3	5	1.2	1.5	1.7	3.5	1.7	19.5	2.3	8.5	2.2	11	4.8	1.5	2.0	32	1.6	46.8	10.0	6	13	–	·	–	17	14	1	2	1	–	–	·	10	–
III	4	2.8	4	4.0	2.0	4.8	2	1.2	12	4.8	4	1.9	11	3.1	2	1.5	34	2.5	37.8	13.8	17	17	–	·	–	8	7	1	5	1	–	–	10	11	–
IV	1.1	1.7	6	1.8	2	1.0	1	1.0	3	2.0	2	2.5	5	2.4	4	2.2	56	0.7	38.7	11.8	22	14	–	·	–	8	6	1	·	·	–	–	8	8	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.0	19.6	19	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	8	2.2	3	1.7	5.5	2.6	3.5	1.9	9	2.9	5	2.4	9	3.3	2	2.0	45	1.3	68.6	28.0	24	·	–	·	–	7	7	3	2	·	–	–	10	4	–
VII	5	1.6	1	1.0	8	1.9	2	1.5	5	1.6	7.5	3.6	20.5	2.5	4	2.8	40	1.3	175.6	74.5	16	·	–	·	–	18	17	4	·	·	–	–	5	15	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36.4	5.8	21	–	–	·	–	11	10	·	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	106.6	17.0	23	–	–	·	–	12	11	6	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.4	3.0	8	–	–	·	–	4	4	·	–	–	–	–	–	–	–
XI	3.5	7.6	4	3.0	9	3.3	6	1.9	7.5	2.1	5.5	3.4	15	5.1	2.5	10.2	37	2.4	19.2	10.5	29	11	–	·	–	6	4	1	2	·	–	–	5	16	–
XII	1	1.0	4	2.8	·	·	5	2.4	16	2.1	10	7.6	10	3.5	5	1.6	42	1.9	35.2	7.2	14	27	–	2	–	11	9	·	3	1	–	–	2	14	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	630.6	74.5	16.VII	–	–	5	–	–	–	–	–	–	–	–	–	–	–

Krasnystaw $\varphi = 50°59'$ $\lambda = 23°10'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.9	-0.8	-1.6	-1.7	0.4	-4.3	5.5	6,7	-14.2	17	–	–	–	–	–	–	–	–	8.3	8.7	8.4	8.5
II	–	–	–	–	0.7	4.0	1.7	2.0	5.3	-0.8	10.2	6	-5.5	24	–	–	–	–	–	–	–	–	7.5	8.1	5.9	7.2
III	–	–	–	–	-1.8	4.9	1.2	1.4	6.5	-3.2	16.0	30,31	-12.9	4	–	–	–	–	–	–	–	–	5.6	5.9	3.7	5.1
IV	–	–	–	–	4.7	13.3	7.7	8.4	14.7	2.3	26.6	30	-5.3	10	–	–	–	–	–	–	–	–	5.5	6.6	5.1	5.7
V	–	–	–	–	8.9	14.5	9.7	10.7	15.8	6.2	24.9	18	-0.2	27	–	–	–	–	–	–	–	–	6.5	8.5	6.7	7.2
VI	–	–	–	–	15.2	23.0	16.5	17.8	24.3	10.4	34.7	12	5.3	7	–	–	–	–	–	–	–	–	4.5	5.7	4.2	4.8
VII	–	–	–	–	16.7	23.2	17.3	18.6	25.1	13.4	34.1	5	8.1	7	–	–	–	–	–	–	–	–	6.3	6.4	6.4	6.4
VIII	–	–	–	–	14.0	20.8	14.8	16.1	22.1	11.2	30.6	14	5.3	31	–	–	–	–	–	–	–	–	5.9	7.0	3.6	5.5
IX	–	–	–	–	9.9	16.1	10.6	11.8	17.5	7.6	27.0	9	-1.3	27	–	–	–	–	–	–	–	–	6.8	7.4	5.1	6.4
X	–	–	–	–	4.2	13.0	6.5	7.6	13.8	—	20.8	19	–	–	–	–	–	–	–	–	–	–	6.2	5.3	3.1	4.9
XI	–	–	–	–	2.0	5.8	2.9	3.4	6.9	0.4	17.3	1	-9.9	30	–	–	–	–	–	–	–	–	7.7	7.8	6.6	7.4
XII	–	–	–	–	-3.6	-0.4	-2.6	-2.3	0.7	-5.7	8.9	13	-15.0	16	–	–	–	–	–	–	–	–	7.4	7.6	5.3	6.8
Rok	–	–	–	–	5.7	11.4	7.1	7.8	12.7	–	34.1	5.VII	-15.0	16.XII	–	–	–	–	–	–	–	–	6.5	7.1	5.3	6.3

Sternalice $\varphi = 50°58'$ $\lambda = 18°34'$

I	–	–	–	–	-2.0	0.7	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.7	6.8	8.4	8.3
II	–	–	–	–	1.2	4.8	2.1	2.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.7	5.4	7.9	7.3
III	–	–	–	–	1.2	7.3	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.8	3.9	5.9	5.2
IV	–	–	–	–	5.3	11.9	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.4	5.9	6.0
V	–	–	–	–	9.1	14.6	9.1	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.4	6.0	6.6	5.7
VI	–	–	–	–	15.2	22.3	17.6	18.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.6	3.8	4.3
VII	–	–	–	–	16.4	22.3	18.3	18.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	7.0	6.6
VIII	–	–	–	–	13.1	19.3	14.9	15.6	–	–	–	–	–	–	94	70	91	85	1.0	7.2	1.7	3.3	8.6	6.5	7.9	7.7
IX	–	–	–	–	8.8	15.2	11.4	11.7	–	–	–	–	–	–	95	77	92	88	0.6	4.6	1.2	2.1	9.0	6.4	8.8	8.1
X	–	–	–	–	6.1	13.0	7.9	8.7	–	–	–	–	–	–	92	72	89	84	0.8	4.5	1.2	2.2	5.0	5.0	2.5	4.1
XI	–	–	–	–	3.1	6.9	4.0	4.5	–	–	–	–	–	–	90	77	89	85	0.8	2.8	0.9	1.5	6.9	6.6	7.6	7.0
XII	–	–	–	–	-2.3	0.5	-1.4	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	6.5	6.9
Rok	–	–	–	–	6.3	11.6	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.9	6.6	6.4

Wojcieszów Górny $\varphi = 50°57'$ $\lambda = 15°55'$

I	–	–	–	–	-2.0	0.7	-1.1	-0.9	2.2	-4.5	9.9	6	-21.0	17	78	76	79	78	1.3	1.6	1.3	1.4	7.4	7.1	5.9	6.8
II	–	–	–	–	1.3	4.8	2.2	2.6	6.2	-0.6	11.8	2	-5.9	27	81	70	80	77	1.3	2.7	1.5	1.8	6.4	7.3	5.9	6.5
III	974.1	992.2	956.2	1018.4	1.7	7.2	3.5	4.0	9.1	-0.1	16.7	13	-10.4	2	80	60	76	72	1.5	4.7	2.2	2.8	5.3	5.9	3.9	5.0
IV	975.2	986.5	954.0	1019.3	3.4	10.4	5.5	6.2	12.0	0.9	22.9	28	-4.7	13	90	59	84	78	0.8	6.1	1.6	2.8	6.0	5.9	3.7	5.2
V	973.6	982.9	964.7	1017.2	6.8	13.0	8.1	9.0	14.6	3.3	24.7	16	-2.2	7,10	83	55	80	73	1.8	7.5	2.2	3.8	5.1	6.3	4.6	5.3
VI	974.6	990.2	963.6	1017.0	14.1	20.8	15.0	16.2	22.5	9.6	30.6	30	4.8	27	83	57	81	74	2.8	11.7	3.5	6.0	4.5	4.6	3.8	4.3
VII	971.1	983.3	960.2	1013.2	15.8	20.9	16.4	17.4	22.1	13.3	33.1	5	9.2	18	88	66	85	80	2.4	10.3	3.1	5.3	6.6	6.0	5.4	6.0
VIII	972.9	983.0	959.7	1015.5	12.4	18.6	13.3	14.4	19.8	9.7	26.4	11	3.9	23	90	64	86	80	1.4	8.0	2.2	3.9	5.8	6.4	3.5	5.2
IX	971.4	981.6	954.7	1014.5	9.2	14.4	10.1	11.0	15.8	6.9	26.8	8	-1.9	27	88	68	86	81	1.4	5.7	1.8	3.0	5.5	6.9	4.3	5.6
X	976.9	984.7	960.9	1020.7	6.4	12.9	7.3	8.5	13.7	3.7	20.2	19	-1.7	3	90	73	90	84	1.1	4.3	1.2	2.2	4.9	4.6	2.9	4.1
XI	976.6	992.5	960.2	1020.9	3.3	6.5	4.6	4.8	7.6	1.7	15.6	6	-11.5	30	90	78	87	85	0.8	2.3	1.2	1.4	6.3	7.2	6.7	6.7
XII	971.6	989.2	939.5	1016.7	-1.7	1.1	-0.9	-0.6	2.3	-4.1	11.3	13	-16.0	16	89	83	88	87	0.6	1.2	0.7	0.8	5.8	6.7	6.5	6.3
Rok	–	–	–	–	5.9	10.9	7.0	7.7	12.3	3.3	35.1	5.VII	-21.0	17.1	86	67	84	79	1.4	5.5	1.9	2.9	5.8	6.2	4.8	5.6

Otława $\varphi = 50°57'$ $\lambda = 17°18'$

I	–	–	–	–	-1.7	1.8	-0.5	-0.2	2.6	-3.4	10.0	6	-13.4	17	87	78	83	83	0.8	1.6	1.1	1.2	7.9	7.7	6.0	7.2
II	–	–	–	–	1.8	6.4	3.2	3.6	7.2	0.3	10.3	9,14	-7.1	27	86	68	82	79	1.0	3.2	1.5	1.9	6.5	7.2	5.9	6.5
III	–	–	–	–	1.9	8.3	4.8	5.0	10.1	0.4	15.9	14	-7.8	1	81	59	74	71	1.4	4.8	2.3	2.8	6.3	5.6	5.0	5.3
IV	–	–	–	–	5.2	12.3	8.1	8.4	13.8	2.8	25.9	30	-3.0	14	86	57	76	73	1.3	7.3	2.6	3.7	5.2	6.7	4.9	5.6
V	–	–	–	–	9.2	15.0	10.8	11.4	16.5	5.7	26.7	19	-0.4	7	79	51	73	68	2.4	9.2	3.8	5.1	5.2	6.9	5.2	5.8
VI	–	–	–	–	16.3	22.8	17.7	18.6	24.7	11.5	31.9	30	6.0	1	76	54	77	69	4.5	13.9	5.0	7.8	4.5	4.6	3.6	4.3
VII	–	–	–	–	17.3	22.6	18.4	19.2	24.3	14.6	35.9	5	10.9	28	85	67	87	80	3.3	10.8	2.9	5.7	6.9	6.5	6.6	6.7
VIII	–	–	–	–	14.5	20.1	15.8	16.5	21.8	11.7	28.9	11	6.5	31	87	63	85	78	2.1	9.0	3.0	4.7	5.5	6.2	5.1	5.6
IX	–	–	–	–	10.4	16.5	12.0	12.7	17.7	8.2	28.7	8	0.8	26	90	64	85	80	1.3	7.4	2.1	3.6	6.6	6.7	5.1	6.1
X	–	–	–	–	6.2	13.8	8.7	9.4	15.1	4.0	22.1	19	-0.5	3	90	68	88	82	1.0	5.3	1.4	2.6	6.8	5.8	3.0	5.2
XI	–	–	–	–	4.1	7.8	5.1	5.6	8.8	2.6	18.6	5	-6.3	30	90	75	88	84	0.9	3.3	1.1	1.8	8.2	7.4	7.8	7.8
XII	–	–	–	–	-2.0	1.6	-0.4	-0.3	2.9	-3.8	9.4	13	-16.0	16	88	79	86	84	0.7	1.8	0.9	1.1	7.4	7.3	5.9	6.9
Rok	–	–	–	–	6.9	12.4	8.6	9.1	13.8	4.6	35.9	5.VII	-16.0	16.XII	85	65	82	77	1.7	6.4	2.3	3.5	6.3	6.6	5.4	6.1

Krasnystaw

$H_s = 182\,m$ $h_w = 12\,m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D.T.=D																	OPAD R			LICZBA DNI (n)											
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max≥25°	0,1 ÷ 1	1 ÷ 10	10 ÷ 100	10 ÷ 15	15 ÷	=	≡	◔	●	▦
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	22.9	7.7	5	26	11	3	·	13	6	·	–	–	–	·	2	21	26
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.5	7.4	15	15	2	·	·	20	14	·	–	–	–	·	3	13	4
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.6	9.3	15	23	6	2	·	8	8	·	–	–	–	·	10	8	5
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18.7	6.0	11	10	·	·	2	10	5	·	–	–	–	4	6	10	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5.7	19.4	18	1	·	·	·	12	8	1	–	–	–	2	2	16	·
VI	14	2.0	3	1.2	5.5	1.7	6.5	2.5	14.5	3.3	11.5	3.7	12	2.3	23	2.7	·	2.7	56.0	18.0	10	·	·	·	12	10	8	3	·	·	–	6	6	2	·
VII	5	1.6	4	1.6	6	3.3	9.5	2.7	12.5	1.9	22	3.1	18	3.1	16	2.8	·	2.7	115.5	53.0	23	·	·	·	17	19	12	2	·	·	–	9	4	13	·
VIII	6.5	2.0	3.5	1.6	2	2.8	5	3.0	13	2.8	15.5	3.3	20	2.1	28.5	2.5	·	2.6	65.4	19.0	21	·	·	·	5	17	10	3	·	·	–	9	2	5	·
IX	5	1.9	2.5	1.6	2	1.7	2	2.2	18.5	2.0	18	3.9	24.5	4.5	17.5	3.3	·	3.3	65.9	10.9	29	1	·	·	2	17	14	1	2	·	–	1	2	9	·
X	6	2.2	3.5	2.0	2	2.0	5	2.6	33.5	2.2	16.5	3.8	12	3.5	14.5	2.5	·	2.7	13.8	7.4	23	–	·	·	·	6	4	·	·	·	–	·	5	6	·
XI	8	5.4	1.0	2.8	1.1	3.3	17.5	3.5	16.5	2.2	6.5	3.8	17.5	5.0	3	7.7	·	3.8	21.6	11.4	28	13	2	·	·	11	5	1	2	·	–	·	4	14	1
XII	10.5	2.2	5.5	1.5	5	1.9	6.5	2.7	26.6	3.5	23	4.3	8	4.3	8	5.0	·	3.5	40.9	10.1	14	29	12	5	·	13	10	1	3	·	–	·	4	13	21
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	555.5	53.0	23.VII	–	33	10	38	156	105	12	–	–	–	31	50	130	58

Sternalice

$H_s = 239\,m$ $h_w = 10\,m$

I	7	4.2	7	4.0	4	2.4	2	2.5	10.5	4.4	28	3.1	28	3.7	6.5	3.5		3.5	24.6	9.8	6	–	–	–	–	8	6	·	2	–	–	·	20	–
II	6	2.2	5	2.3	3	2.0	3	2.5	17	4.6	25.5	4.5	17.5	3.9	7	2.4	·	3.8	43.3	10.0	18	–	–	–	–	15	12	1	4	1	–	·	2	14	–
III	9.5	2.6	14.5	2.9	15.5	3.9	2	2.5	9	4.5	12.5	5.2	19.5	5.2	10.5	2.9	·	4.0	35.7	9.0	18	–	–	–	–	8	6	·	5	1	–	·	8	10	–
IV	3.1	2.4	6.5	2.0	6	1.9	3	1.8	9.5	2.3	6	3.6	3	3.2	2.4	2.5	1	2.4	46.3	18.5	22	–	–	–	–	9	7	1	1	1	–	1	8	11	–
V	28.5	2.5	20.5	2.2	3	2.2	3.5	3.4	1.5	1.7	6	1.8	7.5	3.2	21.5	2.5	1	2.5	41.1	32.5	20	–	–	–	–	7	7	1	·	·	–	2	10	11	–
VI	10.5	1.8	8	1.7	2.5	2.0	2	2.8	8	2.2	14.5	2.8	1.8	2.6	25.5	2.1	1	2.2	73.6	53.2	24	–	–	–	–	7	6	1	·	·	–	4	10	7	–
VII	9.5	1.4	5.5	2.0	4	2.2	2	1.5	6	2.7	10.5	2.9	31.5	3.2	24	1.8	·	2.4	157.2	63.3	16	–	–	–	–	17	13	4	·	·	–	3	6	17	–
VIII	3.5	1.3	0.5	1.0	2	2.0	1.5	2.3	3	3.5	14.5	4.4	38.5	2.9	28.5	2.4	1	2.8	62.9	12.5	17	–	–	–	–	14	12	2	2	·	–	4	3	21	–
IX	6.5	1.5	·	·	1	2.0	1	2.0	6	5.6	27	4.2	34	3.8	14.5	2.8	·	3.7	90.5	16.0	14	–	–	–	–	10	10	4	5	·	–	·	1	20	–
X	5	1.2	0.5	1.0	0.5	1.0	4	1.8	8	1.8	32	2.1	23	2.2	20	1.6	·	1.9	6.3	2.2	18	–	–	–	–	4	3	·	·	·	–	·	5	1	–
XI	5	8.1	6.5	3.7	2.5	1.8	1.0	1.7	8.5	3.4	10	2.6	22.5	5.4	2.5	5.8	·	3.5	27.1	14.4	28	–	–	–	–	8	5	·	3	·	–	·	4	17	–
XII	7.5	2.5	5	1.6	9	1.4	1.5	1.0	12	4.1	21.5	5.3	24.5	4.1	11	2.9	1	3.6	-	-	-	–	–	–	–	-	-	-	3	·	–	·	3	15	–
Rok	129.5	2.6	79.5	2.0	75.5	2.1	35.5	2.2	99	3.4	208	3.5	267.5	3.6	195.5	2.8	5	3.0	-	63.3	16.VII	–	–	–	–	-	-	-	25	3	-	14	60	164	–

Wojcieszów Górny

$H_s = 358\,m$ $H_b = 362.1\,m$ $h_w = 23\,m$

I	5.5	1.0	0.5	1.0	1	1.0	1.5	2.0	9.5	2.4	14	2.2	13.5	2.1	3.5	2.3	44	1.1	33.0	10.2	28	23	9	5	·	13	7	1	·	·	2	·	4	11	20
II	2	1.0	·	·	1	1.0	3.5	1.1	13.5	1.7	11	2.0	7	2.0	3	1.7	43	0.8	51.2	9.2	18	16	·	·	·	16	11	·	·	·	5	·	1	8	4
III	6.5	1.3	·	·	3	1.7	4	1.1	17.5	1.8	8	2.1	7.5	2.1	3.5	2.7	43	1.0	84.1	14.8	15	15	1	1	·	13	10	3	·	·	5	·	7	8	6
IV	1.0	1.6	2	1.0	1	2.0	1.5	1.0	6	1.0	3.5	1.9	4	1.8	2	1.8	60	0.5	49.0	20.1	7	13	·	·	·	17	7	1	·	·	5	1	6	5	1
V	9.5	1.3	6	1.2	4.5	1.2	1.5	1.0	3.5	1.4	1.5	2.0	8.5	1.5	3	1.8	55	0.6	40.5	11.6	5	9	·	·	·	15	6	1	·	·	3	2	4	8	1
VI	7	1.1	·	·	·	·	0.5	2.0	1.0	1.6	6	2.0	6	1.9	7.5	1.5	53	0.7	54.5	18.9	4	·	·	·	6	12	8	2	·	·	3	4	8	5	·
VII	6	1.5	·	·	2	1.0	·	·	7	1.7	9	1.9	12.5	1.9	6.5	1.8	50	0.8	248.2	55.6	11	·	·	·	10	20	14	7	·	·	9	6	7	10	·
VIII	5.5	1.5	·	·	1	2.0	1.5	1.7	10.5	2.1	10	2.4	4.5	1.6	6	1.7	54	0.8	49.3	12.1	24	·	·	·	2	16	10	1	·	·	3	5	4	6	·
IX	2	1.2	·	·	·	·	·	·	6.5	1.9	16	2.1	16.5	2.6	8	2.6	41	1.3	83.2	12.5	29	1	·	·	1	18	15	2	·	·	3	·	2	5	·
X	1	2.0	·	·	·	·	2.5	1.0	12	1.4	10.5	1.6	3.5	1.5	4.5	1.7	57	0.6	8.8	2.0	20	4	·	·	·	11	4	·	·	·	10	·	9	3	·
XI	5.5	2.0	2	1.0	2	1.0	0.5	1.0	1.6	1.7	8.5	2.7	7.5	2.5	2	2.0	46	1.0	21.9	3.6	12	12	1	1	·	10	8	·	·	·	9	·	4	15	1
XII	5.5	1.1	1.5	1.3	3	1.3	0.5	1.0	8	2.2	16	2.2	10	2.2	2.5	3.0	46	1.0	55.5	11.9	14	26	7	3	·	13	10	1	·	·	8	·	2	12	14
Rok	66	1.4	1.2	0.5	18.5	1.0	17.5	1.1	120	1.7	114	2.1	103	2.0	52	2.0	592	0.8	779.2	55.6	11.VII	119	18	10	19	174	110	19	·	·	65	18	58	96	47

Otawa

$H_s = 137\,m$ $h_w = 10\,m$

I	4	2.8	4	2.5	1.5	2.0	9.5	1.9	13.5	1.7	26	2.2	14.5	3.5	5	2.8	15	2.0	19.4	5.8	6	22	6	5	·	9	6	·	·	·	4	·	3	15	17
II	·	·	·	·	9	2.6	11.5	1.9	22	3.1	11.5	3.6	13	3.9	3	2.7	14	2.5	33.9	7.2	18	12	1	·	·	13	8	·	2	·	1	·	4	9	3
III	2.5	2.4	2.5	3.0	12	3.0	20.5	2.7	3.5	2.1	14	2.4	15.5	3.5	8.5	1.9	14	2.3	51.1	19.1	29	15	·	·	·	10	8	2	·	·	3	1	9	10	1
IV	14.5	1.8	1	1.0	4.6	2.2	3.5	3.1	8	2.9	5	1.6	6.5	2.1	2.4	1.8	23	1.5	23.3	11.2	30	9	·	·	1	9	4	1	·	·	5	2	5	8	·
V	19.5	1.7	10.5	2.9	3	2.3	8	1.8	2.5	2.0	4	2.2	8	4.0	20.5	3.7	17	2.2	43.4	19.9	23	1	·	·	2	8	4	2	1	1	1	2	3	10	·
VI	5	1.6	7	1.3	3	1.3	7	1.8	6	1.4	4	2.0	6.5	4.8	15.5	2.7	36	1.4	46.7	18.5	24	·	·	·	14	10	7	2	·	·	·	4	8	3	·
VII	6.5	1.7	5.5	1.5	3.5	1.4	7.5	1.6	2.5	1.4	12	1.9	14	2.3	17.5	2.5	24	1.5	181.5	29.5	14	·	·	·	13	21	17	6	·	·	1	8	7	17	·
VIII	1.5	3.0	0.5	2.0	3.5	2.1	2.5	3.2	4	1.8	16	2.6	17	2.1	21	2.9	27	1.8	57.9	10.3	24	·	·	·	5	16	10	1	1	1	3	1	4	6	·
IX	1.5	3.0	·	·	1	2.0	9.5	1.5	6	2.0	25.5	3.0	19.5	3.8	11	2.6	16	2.4	64.4	12.1	23	·	·	·	2	16	13	1	·	·	8	·	2	6	·
X	0.5	2.0	·	·	2	1.8	1.5	1.7	11	1.9	16	2.3	11	2.9	7.5	2.1	30	1.4	4.3	3.0	20	3	·	·	·	6	1	·	·	·	16	·	4	6	·
XI	0.5	1.0	7.5	2.6	16	2.2	2.1	2.1	4	2.5	7	3.6	16	4.0	5	9.0	13	2.7	8.1	3.3	25	8	1	·	·	6	2	·	1	·	6	·	1	20	·
XII	5	1.8	2	1.5	3	2.8	16.5	2.1	7	2.7	17.5	4.8	13.5	3.5	13.5	3.4	15	2.6	22.1	6.6	14	25	5	3	·	12	4	·	1	·	8	·	4	14	13
Rok	61	1.9	40.5	1.5	62	2.1	132	2.1	90	2.1	158.5	2.6	165	3.4	152	3.2	244	2.0	556.1	29.5	14.VII	95	13	8	37	136	84	15	6	2	56	18	54	124	34

Bodzentyn

$\varphi = 50°57'$ $\lambda = 20°57'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.3	0.1	-2.0	-1.6	0.5	-3.6	6.8	8	-16.2	17	–	–	–	–	–	–	–	–	9.2	7.9	8.5	8.5
II	–	–	–	–	1.1	4.8	1.8	2.4	5.7	0.0	9.6	6,21	-7.1	28	–	–	–	–	–	–	–	–	7.1	7.2	8.4	7.6
III	–	–	–	–	-0.2	6.1	1.8	2.4	7.4	-2.0	16.0	28,30	-8.1	4	–	–	–	–	–	–	–	–	6.4	4.9	5.1	5.1
IV	–	–	–	–	4.7	12.7	6.2	7.4	14.0	1.4	26.1	30	-4.5	15	–	–	–	–	–	–	–	–	5.9	6.2	4.2	5.4
V	–	–	–	–	8.1	13.1	8.7	9.6	14.7	4.3	23.2	20	-1.9	27	–	–	–	–	–	–	–	–	6.6	7.6	6.2	6.8
VI	–	–	–	–	16.2	22.4	16.3	17.8	24.2	9.3	31.5	30	0.9	7	–	–	–	–	–	–	–	–	4.1	5.6	3.9	4.5
VII	–	–	–	–	16.7	22.6	16.9	18.3	24.1	12.9	35.0	5	7.6	4	–	–	–	–	–	–	–	–	6.0	5.8	6.3	6.0
VIII	–	–	–	–	13.7	19.6	14.7	15.7	21.5	10.4	29.6	12	5.6	31	–	–	–	–	–	–	–	–	5.7	6.3	4.9	5.6
IX	–	–	–	–	9.1	15.6	10.5	11.4	17.0	6.9	28.1	9	-0.1	26	–	–	–	–	–	–	–	–	5.7	6.1	5.5	5.8
X	–	–	–	–	5.4	12.8	7.1	8.1	14.0	3.1	20.4	10,19	-3.0	3	–	–	–	–	–	–	–	–	5.7	5.5	4.3	5.2
XI	–	–	–	–	2.5	6.0	2.8	3.5	7.3	0.6	17.5	4	-9.9	30	–	–	–	–	–	–	–	–	8.2	6.4	7.2	7.3
XII	–	–	–	–	-2.6	-0.2	-2.0	-1.7	1.1	-5.0	8.7	13	-16.8	17	–	–	–	–	–	–	–	–	7.7	7.4	6.8	7.3
Rok	–	–	–	–	6.0	11.3	6.9	7.8	12.6	3.2	35.0	5.VII	-16.8	17.XII	–	–	–	–	–	–	–	–	6.4	6.4	5.9	6.2

Jelenia Góra

$\varphi = 50°54'$ $\lambda = 15°48'$

I	980.2	991.0	962.3	1023.3	-3.9	0.7	-2.6	-2.1	2.3	-7.3	10.1	6	-25.2	17	88	80	89	86	0.7	1.4	0.6	0.9	7.7	7.6	6.2	7.2
II	969.9	992.5	944.1	1011.9	1.2	5.4	2.0	2.6	6.7	-1.4	13.8	5	-7.7	23	87	74	88	83	1.0	2.5	1.0	1.5	7.5	8.2	6.6	7.4
III	976.6	994.8	958.7	1018.9	0.3	7.5	2.9	3.4	9.4	-1.4	16.3	13	-13.2	3	87	63	81	77	1.1	4.5	1.7	2.4	6.6	6.7	5.0	6.1
IV	977.8	989.0	956.6	1019.7	2.9	10.2	5.3	5.9	12.1	-0.1	22.5	28,29	-6.5	13	93	61	87	80	0.6	5.7	1.3	2.5	6.1	6.9	4.4	5.8
V	976.0	985.4	966.9	1017.3	6.7	12.6	8.1	8.9	14.4	2.2	24.2	16	-4.4	7	86	58	81	75	1.6	6.7	2.1	3.5	5.9	7.6	5.4	6.3
VI	977.0	992.4	965.1	1017.2	14.6	20.5	14.8	16.2	22.6	8.2	30.4	30	1.9	1	80	57	83	73	3.7	11.6	2.9	6.1	5.6	5.9	5.1	5.5
VII	973.5	986.1	962.8	1013.6	15.8	21.0	16.5	17.4	22.4	12.0	33.6	5	7.1	18	90	67	87	81	2.2	10.2	2.9	5.1	6.9	7.4	7.3	7.2
VIII	975.2	985.8	961.4	1015.7	12.1	18.2	13.0	14.4	19.7	8.1	26.7	11	1.6	23	92	66	89	82	1.2	7.5	1.8	3.5	6.6	7.6	5.1	6.4
IX	973.6	984.3	956.9	1014.5	8.8	14.5	9.6	10.5	16.0	5.7	27.2	8	-3.5	27	89	67	88	81	1.4	5.9	1.5	3.0	6.7	8.0	5.0	6.6
X	979.0	987.9	961.5	1020.8	3.7	13.3	6.3	7.4	14.4	0.9	20.9	10	-4.1	3	95	64	91	83	0.5	6.1	1.0	2.5	6.6	5.5	4.5	5.5
XI	978.9	994.6	962.7	1021.1	2.6	6.7	4.1	4.4	8.1	0.3	16.0	5	-12.6	30	87	73	84	81	1.0	3.0	1.4	1.8	7.4	7.4	7.4	7.4
XII	973.9	992.6	941.0	1016.7	-3.2	1.2	-1.2	-1.1	2.4	-5.7	10.2	13	-19.5	17	88	77	84	83	0.6	1.6	1.0	1.1	7.0	7.1	6.2	6.8
Rok	976.0	994.8	941.0	1017.6	5.1	11.0	6.6	7.3	12.5	1.8	33.6	5.VII	-25.2	17.I	89	67	86	80	1.3	5.6	1.6	2.8	6.7	7.2	5.7	6.5

Stare Olesno

$\varphi = 50°54'$ $\lambda = 18°21'$

I	–	–	–	–	-2.2	0.3	-1.4	-1.2	1.1	–	7.9	6	–	–	87	83	85	85	0.7	1.1	0.8	0.9	7.6	6.9	6.2	6.9
II	–	–	–	–	1.2	4.6	2.3	2.6	5.4	–	9.2	9	–	–	88	74	87	83	0.8	2.3	1.0	1.4	7.2	6.4	6.5	6.7
III	–	–	–	–	0.9	7.0	3.5	3.7	8.5	–	14.8	14	–	–	83	61	79	74	1.2	4.2	1.7	2.4	5.5	5.3	5.0	5.3
IV	–	–	–	–	4.7	11.3	6.8	7.4	12.6	–	23.8	29	–	–	86	60	82	76	1.3	6.0	1.9	3.1	5.4	6.0	5.0	5.5
V	–	–	–	–	8.9	14.0	9.1	10.3	15.1	–	24.1	19	–	–	78	56	78	71	2.6	7.6	2.7	4.3	3.8	6.3	5.0	5.0
VI	–	–	–	–	16.4	21.8	15.8	17.4	23.1	–	29.7	30	–	–	77	56	81	71	4.5	12.4	3.7	6.9	3.5	4.1	3.6	3.7
VII	–	–	–	–	17.5	21.9	17.0	18.4	23.4	–	35.1	5	–	–	84	68	87	80	3.8	10.4	2.9	5.7	6.0	5.4	5.7	5.7
VIII	–	–	–	–	14.0	19.3	14.3	15.5	20.6	–	27.8	11	–	–	88	65	91	81	2.1	8.0	1.6	3.9	5.5	5.3	4.4	5.1
IX	–	–	–	–	10.0	15.3	11.1	11.9	16.3	–	27.2	9	–	–	90	68	87	82	1.3	6.1	1.7	3.0	5.6	5.6	5.4	5.5
X	–	–	–	–	6.2	12.8	7.8	8.6	13.3	4.2	19.3	19	-0.6	2	91	70	90	84	1.0	4.8	1.2	2.3	5.2	5.0	2.8	4.3
XI	–	–	–	–	3.4	6.7	4.2	4.6	7.4	1.7	17.8	5	-8.2	30	87	76	86	83	1.0	2.8	1.2	1.7	7.2	7.0	7.7	7.3
XII	–	–	–	–	-1.9	0.5	-1.2	-1.0	1.4	-3.9	9.5	13	-16.9	17	87	80	85	84	0.7	1.3	0.8	0.9	6.7	6.9	6.3	6.6
Rok	–	–	–	–	6.6	11.3	7.4	8.2	12.4	–	35.1	5.VII	–	–	86	68	85	80	1.8	5.6	1.8	3.1	5.8	5.8	5.3	5.6

Ślęża

$\varphi = 50°53'$ $\lambda = 16°43'$

I	–	–	–	–	-1.7	-0.6	-1.6	-1.4	1.1	-4.0	7.6	22	-15.4	17	–	–	–	–	–	–	–	–	7.9	7.1	6.3	7.1
II	–	–	–	–	0.5	2.4	1.1	1.3	4.3	-1.1	15.0	5	-7.1	27	–	–	–	–	–	–	–	–	5.8	7.4	6.2	6.5
III	–	–	–	–	1.1	3.8	2.4	2.4	6.4	-1.0	13.0	27	-8.2	9	–	–	–	–	–	–	–	–	6.4	6.8	4.9	6.0
IV	–	–	–	–	4.4	7.8	5.3	5.7	9.9	2.2	28.2	28	-6.3	8	–	–	–	–	–	–	–	–	6.0	6.2	5.1	5.8
V	–	–	–	–	6.6	10.1	7.7	8.0	12.2	4.0	21.8	19	-2.5	6	–	–	–	–	–	–	–	–	5.6	6.5	5.0	5.7
VI	–	–	–	–	13.7	18.2	15.1	15.5	20.0	11.3	28.3	30	5.4	6	–	–	–	–	–	–	–	–	4.9	5.6	4.2	4.9
VII	–	–	–	–	15.0	17.8	15.2	15.8	19.2	12.6	30.8	5	8.6	28	–	–	–	–	–	–	–	–	6.6	6.7	7.3	6.9
VIII	–	–	–	–	11.7	15.6	12.9	13.3	16.8	9.9	23.8	11	5.7	23	–	–	–	–	–	–	–	–	7.4	6.1	5.2	6.2
IX	–	–	–	–	8.6	12.1	9.2	9.8	12.9	6.7	24.6	8	-0.5	27	–	–	–	–	–	–	–	–	6.4	7.3	6.4	6.7
X	–	–	–	–	6.7	10.0	7.8	8.1	11.1	5.2	17.9	10	0.7	4,2	–	–	–	–	–	–	–	–	6.3	5.6	4.3	5.4
XI	–	–	–	–	2.1	3.8	2.6	2.8	4.8	0.4	15.3	6	-13.5	30	–	–	–	–	–	–	–	–	7.8	7.9	7.6	7.8
XII	–	–	–	–	-1.7	-0.8	-1.8	-1.5	0.8	-4.7	10.5	12	-15.0	16	–	–	–	–	–	–	–	–	8.0	6.9	5.7	6.9
Rok	–	–	–	–	5.6	8.4	6.3	6.6	10.0	3.5	30.8	5.VII	-15.4	17.I	–	–	–	–	–	–	–	–	6.6	6.7	5.7	6.3

Bodzentyn

$H_s = 288\ m$ $h_w = 14\ m$ **1957**

| MIESIĄC | ROZKŁAD WIATRU [%D, %nD] | | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | | |

Olesno

$\varphi = 50°53'$ $\lambda = 18°25'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{c.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.2	0.8	-1.4	-1.0	1.6	-4.1	8.1	6	-19.2	17	91	85	91	89	0.4	1.0	0.5	0.6	8.1	7.9	7.2	7.7
II	–	–	–	–	1.2	4.7	2.2	2.6	5.9	-0.1	9.5	9	-4.6	23	91	77	90	86	0.6	2.1	0.8	1.2	7.3	7.5	6.2	7.0
III	–	–	–	–	0.9	7.4	3.4	3.8	9.0	-0.8	15.4	26	-8.5	1	85	60	81	75	1.1	4.7	1.6	2.5	5.6	5.8	4.6	5.3
IV	–	–	–	–	4.7	11.6	6.7	7.4	13.1	1.7	24.5	30	-6.3	15	87	59	83	76	1.2	7.0	2.1	3.4	5.8	6.2	5.3	5.8
V	–	–	–	–	9.0	14.3	9.0	10.3	15.6	4.4	26.1	19	-1.8	7	81	59	85	75	2.2	7.5	1.9	3.9	5.3	6.6	5.1	5.7
VI	–	–	–	–	16.0	22.1	16.5	17.8	23.7	10.5	31.3	11	3.7	28	76	56	79	71	4.2	12.9	4.3	7.1	4.3	5.2	4.4	4.6
VII	–	–	–	–	17.1	22.0	17.2	18.4	23.6	13.7	35.4	5	9.9	3	86	68	86	80	3.2	10.6	3.3	5.7	6.9	6.6	6.3	6.6
VIII	–	–	–	–	13.9	19.3	14.5	15.6	20.7	10.7	27.4	14	5.4	31	90	65	90	82	1.7	8.2	1.9	3.9	6.5	6.3	4.1	5.6
IX	–	–	–	–	9.6	15.0	11.0	11.6	16.5	7.3	26.4	9	-1.7	27	94	73	90	86	0.8	5.2	1.4	2.5	6.4	6.8	6.1	6.4
X	–	–	–	–	6.4	12.7	8.0	8.8	13.6	4.1	20.3	19	-0.9	2	95	75	92	87	0.6	4.0	0.9	1.8	5.6	6.1	3.3	5.0
XI	–	–	–	–	3.2	6.7	4.3	4.6	7.7	1.6	17.9	5	-9.4	30	90	77	90	86	0.8	2.7	0.9	1.4	7.4	7.3	7.6	7.4
XII	–	–	–	–	-1.9	0.7	-1.1	-0.8	1.8	-4.3	11.3	13	-15.3	17	87	80	87	85	0.6	1.3	0.7	0.9	7.5	7.2	6.1	6.9
Rok	–	–	–	–	6.5	11.4	7.5	8.2	12.7	3.7	35.4	5.VII	-19.2	17.I	88	70	87	82	1.4	5.6	1.7	2.9	6.4	6.6	5.5	6.2

Cieplice Śl.-Zdrój

$\varphi = 50°52'$ $\lambda = 15°41'$

I	–	–	–	–	-4.1	0.6	-2.5	-2.1	2.0	-6.8	10.5	6	-26.2	17	–	–	–	–	–	–	–	–	7.5	6.8	6.0	6.8
II	–	–	–	–	1.6	5.6	2.5	3.0	6.9	-0.9	13.7	3	-7.9	23	–	–	–	–	–	–	–	–	7.3	7.8	6.6	7.2
III	–	–	–	–	0.6	7.6	3.3	3.7	9.3	-0.8	16.2	13	-12.6	3	–	–	–	–	–	–	–	–	6.5	6.3	5.3	6.0
IV	–	–	–	–	2.2	10.2	5.5	5.8	11.9	0.3	22.7	28	-6.0	13	–	–	–	–	–	–	–	–	6.0	6.9	5.0	6.0
V	–	–	–	–	6.0	12.4	8.4	8.8	14.3	2.5	24.3	16	-3.6	7	–	–	–	–	–	–	–	–	5.8	8.1	6.5	6.8
VI	–	–	–	–	14.6	20.4	15.0	16.2	22.7	8.9	30.3	30	2.6	1	–	–	–	–	–	–	–	–	5.3	5.6	5.2	5.4
VII	–	–	–	–	15.0	20.7	16.5	17.2	22.3	12.6	33.6	5	7.9	19	–	–	–	–	–	–	–	–	6.5	7.0	7.3	6.9
VIII	–	–	–	–	11.5	18.0	13.1	13.9	19.8	8.4	26.6	11	1.7	23	–	–	–	–	–	–	–	–	6.3	8.0	5.4	6.6
IX	–	–	–	–	8.0	14.3	9.8	10.5	15.9	5.7	27.8	8	-2.8	27	–	–	–	–	–	–	–	–	7.0	8.0	6.1	7.0
X	–	–	–	–	4.1	13.3	6.5	7.6	14.3	1.4	24.6	10	-3.9	3	–	–	–	–	–	–	–	–	5.3	4.7	3.6	4.5
XI	–	–	–	–	2.1	6.8	3.9	4.2	8.2	0.6	17.0	5	-12.3	30	–	–	–	–	–	–	–	–	7.8	7.6	7.2	7.5
XII	–	–	–	–	-3.4	1.5	-1.7	-1.3	2.5	-5.8	9.6	13	-26.2	17	–	–	–	–	–	–	–	–	7.1	7.9	7.6	7.5
Rok	–	–	–	–	4.8	11.0	6.7	7.3	12.5	2.2	33.6	5.VII	-26.2	17.I,17.XII	–	–	–	–	–	–	–	–	6.5	7.1	6.0	6.5

Słupia Nowa

$\varphi = 50°52'$ $\lambda = 21°05'$

I	–	–	–	–	-2.1	0.1	-1.1	-1.0	1.1	-4.2	7.0	8	-16.7	17	–	–	–	–	–	–	–	–	8.4	8.0	6.5	7.6
II	–	–	–	–	1.4	4.1	2.0	2.4	5.2	-0.4	8.5	5	-7.0	24	–	–	–	–	–	–	–	–	7.8	6.6	6.7	7.0
III	–	–	–	–	1.1	5.8	2.5	3.0	7.0	-1.1	16.0	31	-9.6	4	–	–	–	–	–	–	–	–	5.7	4.9	4.0	4.9
IV	–	–	–	–	6.7	12.2	7.9	8.7	13.2	3.7	24.4	30	-4.5	15	–	–	–	–	–	–	–	–	4.4	5.5	4.6	4.8
V	–	–	–	–	9.2	13.1	8.6	9.9	14.3	5.8	22.7	20	0.2	27	–	–	–	–	–	–	–	–	6.3	7.1	5.4	6.3
VI	–	–	–	–	16.5	21.8	17.0	18.1	23.0	11.6	29.4	12	6.1	27	–	–	–	–	–	–	–	–	4.0	4.2	4.1	4.1
VII	–	–	–	–	17.2	22.1	17.2	18.4	23.3	14.2	33.6	5	11.1	30	–	–	–	–	–	–	–	–	5.1	5.7	6.7	5.8
VIII	–	–	–	–	14.5	19.6	15.4	16.2	21.0	12.1	29.2	12	7.7	24	–	–	–	–	–	–	–	–	4.8	5.1	4.1	4.7
IX	–	–	–	–	10.3	15.2	11.7	12.2	16.4	8.0	27.5	9	0.9	26	–	–	–	–	–	–	–	–	4.7	5.2	4.6	4.8
X	–	–	–	–	–	–	–	–	13.1	5.4	19.5	10	-0.2	2	–	–	–	–	–	–	–	–	6.0	5.4	4.2	5.2
XI	–	–	–	–	2.5	5.9	3.4	3.8	8.9	0.7	15.6	5	-10.4	30	–	–	–	–	–	–	–	–	8.4	6.2	6.7	7.1
XII	–	–	–	–	-2.0	-0.6	-1.6	-1.4	0.8	-4.8	9.0	13	-15.0	16	–	–	–	–	–	–	–	–	7.2	5.8	4.7	5.9
Rok	–	–	–	–	–	–	–	–	12.1	4.2	33.6	5.VII	-16.7	17.I	–	–	–	–	–	–	–	–	6.1	5.8	5.2	5.7

Szklarska Poręba

$\varphi = 50°51'$ $\lambda = 15°32'$

I	–	–	–	–	-2.3	0.7	-2.1	-1.4	2.0	-5.8	8.0	9	-21.2	17	–	–	–	–	–	–	–	–	7.7	7.0	4.7	6.5
II	–	–	–	–	1.4	3.7	1.3	1.9	5.0	-1.3	13.7	5	-8.2	24	–	–	–	–	–	–	–	–	7.3	8.0	6.3	7.2
III	–	–	–	–	1.1	6.4	2.0	2.9	7.8	-1.9	15.1	13	-14.2	2	–	–	–	–	–	–	–	–	6.6	5.4	5.2	5.7
IV	–	–	–	–	4.1	8.2	3.1	4.6	9.8	-0.9	20.3	28	-8.2	9	–	–	–	–	–	–	–	–	6.6	7.3	4.0	6.0
V	–	–	–	–	7.4	10.5	5.5	7.2	12.0	1.4	21.9	16	-5.1	7	–	–	–	–	–	–	–	–	6.1	7.5	4.9	6.2
VI	–	–	–	–	14.6	18.5	12.7	14.8	20.5	8.3	28.1	30	2.5	26	–	–	–	–	–	–	–	–	5.7	5.4	4.8	5.2
VII	–	–	–	–	15.9	18.8	14.6	16.0	20.3	11.7	31.2	5	7.2	22	–	–	–	–	–	–	–	–	6.7	7.2	6.3	6.7
VIII	–	–	–	–	12.5	16.0	12.1	13.2	17.6	7.9	24.2	11	1.6	23	–	–	–	–	–	–	–	–	7.2	7.3	4.7	6.4
IX	–	–	–	–	9.2	12.3	8.3	9.5	13.6	4.6	25.5	8	-3.3	27	–	–	–	–	–	–	–	–	7.1	7.5	6.0	6.9
X	–	–	–	–	5.7	11.2	6.5	7.5	12.6	2.6	20.6	10	-2.7	3	–	–	–	–	–	–	–	–	4.8	4.9	3.4	4.4
XI	–	–	–	–	1.7	5.0	2.8	3.1	6.6	-0.7	17.3	4	-17.9	30	–	–	–	–	–	–	–	–	6.5	7.2	7.3	7.0
XII	–	–	–	–	-1.7	0.6	-1.5	-1.0	2.0	-6.4	11.2	13	-19.8	11	–	–	–	–	–	–	–	–	7.6	7.1	6.3	7.0
Rok	–	–	–	–	5.8	9.3	5.4	6.5	10.8	1.7	31.2	5.VII	-21.2	17.I	–	–	–	–	–	–	–	–	6.7	6.8	5.3	6.3

Olesno

$H_s = 238$ m

$h_w = 13$ m

1957

MIESIĄC	ROZKŁAD WIATRU nD, VmD																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr V		=	≈	●	●	≋
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Max<0°	Max>0°	Min<-10°	Max>25°	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	10 ≤ V < 15	V ≥ 15					
I	25	3.2	7.5	2.8	2.5	1.8	10.5	1.4	1.8	1.9	30.5	2.1	1.6	4.0	8.5	4.6	·	2.6	26.4	6.5	6	26	8	3	·	11	6	·	1	·	3	·	5	18	17
II	6	2.0	3	1.8	6	1.8	6.5	1.8	2.2	2.9	23.5	3.3	9	4.4	8	4.8	·	3.1	45.6	12.7	18	13	1	·	·	16	13	1	2	·	2	·	1	10	5
III	5.5	2.3	7.5	2.3	1.8	3.1	13	3.2	11.5	3.3	16	3.4	12	5.1	9.5	4.2	·	3.4	40.4	9.8	18	17	2	·	·	8	7	·	3	·	2	·	8	9	3
IV	1.9	2.4	9	2.2	7	1.6	10	1.4	7.5	1.9	11.5	2.3	5.5	2.1	19.5	2.6	1	2.1	39.9	12.1	22	11	·	·	·	15	9	1	·	·	3	1	4	9	·
V	1.3	2.5	18.5	2.6	1.4	2.3	8	1.6	4	2.4	8.5	2.4	8	3.7	1.6	4.2	3	2.7	34.2	16.2	20	5	·	·	1	9	5	1	·	·	·	2	2	7	·
VI	6.5	2.7	7	2.1	8	2.3	8.5	2.7	6.5	2.2	17.5	2.4	9	3.2	1.6	3.9	1.1	2.5	75.7	37.4	24	·	·	·	1.1	10	9	1	·	·	·	5	7	3	·
VII	7.5	1.8	4.5	1.9	3	1.8	8.5	1.8	5.5	1.7	1.8	2.4	2.4	3.7	1.5	3.4	7	2.5	187.1	73.4	16	·	·	1	1.3	20	17	4	1	·	3	9	3	12	·
VIII	0.5	4.0	·	·	1.5	1.0	6	1.5	8.5	2.3	20.5	2.9	2.5.5	3.1	1.9.5	2.9	1.1	2.4	70.6	21.6	12	·	·	·	2	1.6	13	1	·	·	4	5	2	7	·
IX	3	1.5	·	·	0.5	1.0	5.5	1.6	1.2	2.3	30.5	2.5	2.3	4.8	10.5	4.7	5	3.1	105.9	16.8	14	2	·	·	2	1.7	12	5	1	·	2	·	2	9	·
X	1.5	2.3	·	·	1	1.0	8.5	1.1	15.5	2.2	20.5	2.3	1.3	2.8	9	3.2	1.5	2.3	4.1	2.3	20	2	·	·	·	5	2	·	·	·	7	·	5	4	·
XI	4	4.8	7	3.2	1.5	2.4	2.5	2.0	1.0	2.4	8.5	2.4	1.3.5	5.7	6	7.4	1	3.2	28.6	12.1	28	1.3	1	·	·	9	7	1	2	·	5	·	3	2.0	1
XII	7.5	2.0	1.5	3.0	3	1.5	9.5	1.6	2.0	2.1	2.3	3.0	1.4	3.3	1.3.5	2.7	1	2.5	36.4	5.9	4	2.9	8	4	·	1.5	9	·	·	·	1.1	·	3	1.3	2.9
Rok	76.5	2.6	62.5	1.8	79.5	1.8	1.1.9.5	1.8	1.1.1	2.3	2.3.7.5	2.6	1.7.2.5	3.8	1.5.1	4.0	5.5	2.7	69.1.9	73.4	16.VII	1.1.8	1.8	8	2.9	1.5.3	1.0.9	1.5	1.0	·	4.2	2.2	4.3	1.2.4	4.6.1

Cieplice Śl.-Zdrój

$H_s = 345$ m

$h_w = 13{,}6$ m

I	3	1.7	3.5	1.3	9.5	1.1	2.5	1.0	7	2.1	8	2.2	8.5	1.9	12	4.7	3.9	1.4	24.2	9.8	6	24	11	11	·	9	5	·	1	·	7	·	4	1.1	1.9
II	2.5	1.6	6.5	2.0	7.5	1.3	3	1.2	5	2.2	15.5	2.6	10.5	3.1	11.5	2.4	2.2	1.7	45.7	10.2	18	16	·	·	·	13	10	2	1	·	2	·	·	13	4
III	5.5	2.4	3.6	3.3	8	3.5	5.5	5.0	3	6.0	2.5	3.0	7	4.3	12	4.5	4.6	2.0	67.8	18.2	16	17	1	3	·	11	10	2	2	1	6	1	4	11	7
IV	5	2.4	2	1.0	7	1.4	1.5	1.7	2	2.0	3	1.7	6.5	2.2	1.4	3.2	4.9	1.1	23.1	5.7	24	17	·	·	·	10	10	·	·	·	9	·	4	9	4
V	7	3.6	10.5	2.3	3.5	2.7	4.5	2.4	5	1.7	2.5	4.2	4	2.0	1.7	2.9	3.9	1.6	33.0	14.5	5	11	·	·	·	7	4	2	·	·	·	3	·	9	1
VI	5.5	2.5	6.5	1.8	8	1.6	6.5	2.2	6	2.5	10.5	2.4	5	2.0	1.2	3.6	3.0	1.6	53.3	22.4	4	·	·	·	7	7	6	2	·	·	3	4	4	9	·
VII	9	2.9	2	1.0	2	1.0	3	2.3	3	1.0	1.1	3.3	6	3.2	1.9	3.8	3.8	1.8	186.3	44.2	11	·	·	·	9	1.9	1.8	5	·	·	2	5	3	1.4	·
VIII	4.5	2.1	2.5	1.0	4	1.2	3	1.2	7	2.7	1.4.5	3.6	8	3.3	10.5	3.3	3.9	1.7	50.5	16.8	9	·	·	·	2	1.3	9	1	1	·	6	2	1	6	·
IX	3	2.8	2	2.5	·	·	2	2.2	5.5	2.5	1.5	4.7	1.3.5	3.3	1.1	3.5	3.8	2.1	58.6	10.6	9	1	·	·	1	1.6	11	2	1	·	7	2	2	11	·
X	6	1.8	2	1.0	4	1.0	6.5	1.6	9	1.9	10.5	3.2	4.5	3.7	9.5	4.1	4.1	1.4	38	2.1	19	11	·	·	·	5	1	·	1	·	1.9	·	9	6	·
XI	5.5	2.5	8	1.7	5.5	3.1	9	1.7	4	5.1	5	1.8	11	4.9	9	5.3	3.3	2.1	16.7	3.8	28	15	2	1	·	8	5	·	3	1	7	·	1	17	1
XII	3	2.0	2.5	1.4	3	1.0	2	1.5	3	2.7	1.4.5	4.0	1.4	2.8	1.8	1.6	3.3	1.6	32.0	10.6	14	2.7	5	4	·	12	6	1	1	·	9	·	1	1.4	2.2
Rok	5.9.5	2.4	5.1.5	1.7	6.2	1.6	4.9	2.0	5.9.5	2.7	1.1.2.5	3.1	9.8.5	3.1	1.5.5.5	3.6	4.4.7	1.7	5.9.5.0	4.4.2	1.1.VII	1.3.9	1.9	1.9	1.9	1.3.0	9.5	1.7	1.1	2	7.7	1.7	3.3	1.3.3	5.5

Słupia Nowa

$H_s = 307$ m

$h_w = 10$ m

I	2	2.5	3	2.0	2	2.0	2	1.5	1.6.5	4.5	2.5	5.2	1.8.5	4.1	10	3.8	1.4	3.6	6.2.6	2.5.1	6	2.4	9	4	·	1.6	9	2	2	·	8	·	2	1.7	2.0
II	8	2.8	0.5	3.0	·	·	·	·	2.4	4.5	2.5	4.9	1.4	3.5	4.5	3.0	8	3.7	4.1.0	9.4	2.1	1.2	3	·	·	1.8	1.3	·	·	·	4	·	2	1.1	8
III	8	4.5	2.5	1.6	7.5	2.8	4	3.5	2.0.5	4.3	1.1	3.4	1.6.5	3.2	1.3	3.1	1.0	3.2	3.2.1	1.7.7	1.5	1.8	6	·	·	9	4	1	·	·	·	·	1.0	9	6
IV	1.0.5	3.6	3	1.7	7.5	1.5	1.5	4.0	1.3	3.2	1.3	3.2	1.3.5	2.0	1.1	2.3	1.7	2.2	2.9.6	7.7	7	6	·	·	·	1.0	7	·	·	·	1	2	9	7	·
V	1.8.5	2.8	3	4.0	4	1.8	3	3.0	4	3.8	9	3.3	1.0.5	2.1	2.4	2.6	1.7	2.2	2.4.0	1.1.7	9	·	·	·	·	1.0	6	1	·	·	4	1	6	1.2	·
VI	4	3.2	·	·	1	2.0	4	1.8	1.3.5	3.5	1.3	3.8	2.3.5	2.5	1.3	2.3	1.8	2.3	4.1.5	1.4.5	7	·	·	·	7	7	5	1	·	·	1	4	1.0	3	·
VII	2.5	2.2	2	2.5	2	3.0	6.5	2.2	1.2	3.2	1.9	3.2	2.4	2.8	1.2	2.8	1.3	2.5	1.5.4.4	3.0.9	8	·	·	·	9	1.8	1.6	6	·	·	2	6	4	1.0	·
VIII	2.5	3.6	·	·	1.5	1.7	1.5	5.7	6.5	4.6	2.0.5	3.1	2.8	2.7	1.4.5	3.0	1.8	2.5	9.8.4	2.0.7	1.4	·	·	·	5	1.2	1.2	5	·	·	·	5	6	5	·
IX	3	4.3	·	·	·	·	·	·	1.2.5	3.6	3.0.5	4.0	2.2.5	2.9	5.5	3.8	1.6	3.0	6.2.5	1.4.5	2.9	·	·	·	2	1.5	1.2	2	·	·	2	·	7	5	·
X	·	·	1	2.0	·	·	·	·	2.6.5	3.3	3.2.5	3.3	1.1.5	2.8	6.5	1.9	1.5	2.6	1.3.0	5.6	2.2	1	·	·	·	5	3	·	·	·	2	·	5	6	·
XI	8.5	5.2	4.5	2.4	4.5	2.2	2	3.0	3.5.5	4.0	1.1.5	5.0	9	3.9	4.5	4.8	1.0	3.7	1.5.9	8.4	2.8	1.3	2	1	·	1.0	4	·	1	·	5	·	3	1.5	·
XII	1.3.5	3.2	·	·	1	2.0	·	·	2.1.5	4.3	2.9.5	4.5	8.5	3.3	9	2.6	1.0	3.5	3.9.4	9.2	8	2.9	1.0	1	·	1.4	1.0	·	·	·	5	·	6	9	1.4
Rok	8.1	3.2	1.9.5	1.6	3.1	1.6	2.4.5	2.1	2.0.6	3.9	2.3.9.5	3.9	2.0.0	3.0	1.2.7.5	3.0	1.6.6	2.9	6.1.4.4	3.0.9	8.VII	1.0.3	3.0	6	2.3	1.4.4	1.0.1	1.8	3	·	3.4	1.8	7.0	1.0.9	4.8

Szklarska Poręba

$H_s = 640$

$h_w = 16$ m

I	1	3.0	2	3.0	8	1.4	6	2.2	3	5.0	9.5	4.9	3.3	4.4	9.5	4.1	2.1	3.0	6.2.8	2.2.3	6	2.5	8	9	·	1.4	1.0	1	2	·	-	·	4	1.3	2.8
II	·	·	4	2.0	5	1.8	8.5	2.4	7.5	6.1	2.7.5	4.6	2.2.5	3.0	2	3.5	7	3.4	1.2.3.4	4.8.5	1.3	1.5	·	·	·	2.2	1.5	3	4	·	-	·	1	1.2	1.4
III	·	·	6	1.8	9	1.7	8.5	2.7	1.0	1.2.2	1.0.5	3.6	1.7	4.6	3	1.7	2.9	3.1	1.1.7.1	2.5.3	1.7	2.0	2	2	·	1.1	9	5	3	2	-	·	6	1.1	9
IV	2.5	2.8	5	1.8	1.3	1.5	1.1	2.0	8.5	3.1	6.5	1.9	5.5	2.5	7	2.4	3.1	1.4	6.5.5	2.7.3	7	2.0	·	·	·	1.4	8	1	·	·	-	·	4	8	2
V	3.5	2.9	8.5	2.2	1.5	1.8	9	1.7	2	2.8	5.5	2.8	7	2.6	9.5	2.7	3.3	1.5	9.6.2	2.4.7	1.9	1.3	·	·	·	1.2	9	4	·	·	-	2	1	1.0	1
VI	1	1.0	7.5	2.1	6	2.2	1.5.5	1.4	9	3.6	1.4	3.9	1.6	2.7	5	3.0	1.8	2.1	7.9.2	2.9.2	4	·	·	·	5	1.2	8	2	1	1	3	7	5	7	·
VII	1	2.0	4	1.6	7	1.6	5.5	1.8	5	4.8	1.3	3.4	3.2	2.8	6.5	4.2	1.9	2.3	2.8.4.2	8.6.8	1.1	2.4	·	·	·	2.2	1.6	7	·	·	3	5	6	1.4	·
VIII	0.5	4.0	2	1.0	5	1.2	6.5	1.2	2	6.0	2.6	3.5	2.2.5	3.0	1.5.5	2.1	1.3	2.4	7.3.5	1.7.8	2.4	·	·	·	·	1.7	1.4	2	1	1	1	2	1	7	·
IX	2	4.8	·	·	1	2.0	5	1.6	5.5	3.0	2.3	4.7	2.8	3.6	1.3.5	2.8	1.2	3.2	1.8.8.2	4.3.7	2.3	4	·	·	1	1.7	1.6	7	1	·	2	1	1	8	·
X	4.5	1.5	3.5	2.3	1.1	1.4	1.1	1.1	5	4.4	1.5.5	3.6	1.9	2.5	9.5	2.9	1.4	2.1	1.4.1	4.3	4	7	·	·	·	1.0	4	·	·	·	7	·	9	4	·
XI	1.5	2.5	3	2.0	1.2	1.4	1.8	1.8	3	2.2	8.5	3.1	2.3.5	3.3	5.5	2.6	1.5	2.0	5.0.2	1.2.1	2.8	1.6	2	1	·	1.4	9	1	1	·	1.2	·	4	1.5	1
XII	1.5	2.3	7.5	2.4	6	1.4	9.5	1.4	4.5	1.8	1.5.5	4.0	2.7	3.7	6.5	5.8	1.5	2.5	1.0.2.8	4.5.2	8	3.0	7	5	·	1.3	1.1	2	3	·	8	·	2	1.4	2.2
Rok	4.9	2.2	5.3	1.8	9.7	1.6	1.1.4	1.8	6.5	4.6	1.7.5	3.7	2.6.3	3.2	9.1	3.0	2.2.5	2.4	1.2.9.2	6.6.8	1.1.VII	1.6.0	1.9	1.7	1.3	1.7.8	1.2.9	3.5	1.6	4	-	1.7	4.4	1.2.3	7.7

Świdnica

$\varphi = 50°51'$ $\lambda = 16°30'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.6	1.8	0.0	0.3	2.9	-3.1	10.8	6	-18.2	17	–	–	–	–	–	–	–	–	8.1	6.7	6.1	7.0
II	–	–	–	–	2.8	6.2	3.3	3.9	7.0	0.8	14.7	5	-6.7	27	–	–	–	–	–	–	–	–	7.7	7.9	6.5	7.4
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	5.7	11.4	7.0	7.8	12.7	2.5	24.8	30	-4.3	15	–	–	–	–	–	–	–	–	6.0	6.7	4.8	5.8
V	–	–	–	–	9.1	13.9	9.4	10.4	15.3	4.7	24.7	16	-0.7	2	–	–	–	–	–	–	–	–	5.2	6.3	5.6	5.7
VI	–	–	–	–	16.8	21.9	16.4	17.9	23.7	11.4	31.4	11,30	6.0	15	74	56	79	70	5.3	12.8	4.2	7.4	5.2	5.0	5.2	5.1
VII	–	–	–	–	17.9	21.7	17.8	18.8	23.3	14.4	35.2	5	10.4	26	81	64	83	76	4.6	11.4	4.1	6.7	7.3	7.1	7.9	7.4
VIII	–	–	–	–	14.9	19.3	15.0	16.0	20.7	11.4	27.4	11	5.6	31	82	61	81	75	3.2	9.1	3.4	5.2	5.7	6.7	5.7	6.0
IX	–	–	–	–	11.6	15.8	11.6	12.6	16.8	8.2	27.3	8	0.7	27	80	63	81	75	2.9	7.0	2.7	4.2	6.2	6.6	6.3	6.4
X	–	–	–	–	8.5	13.5	9.8	10.4	14.5	6.3	21.8	9,19	-1.2	3	82	63	79	75	2.2	6.1	2.8	3.7	5.7	5.4	4.0	5.0
XI	–	–	–	–	4.4	7.3	5.2	5.5	8.4	2.5	17.5	5	-11.8	30	84	72	85	80	1.4	3.3	1.5	2.1	7.9	7.9	7.8	7.9
XII	–	–	–	–	-0.3	1.8	0.2	0.5	3.1	-2.9	10.5	13	-16.3	16	–	–	–	–	–	–	–	–	7.3	6.2	6.4	6.6
Rok	–	–	–	–	–	–	–	–	–	–	35.2	5.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kielce

$\varphi = 50°51'$ $\lambda = 20°37'$

I	988.4	999.5	971.9	1022.5	-2.9	0.0	-1.8	-1.6	1.0	-5.1	6.9	6	-20.3	17	92	86	93	90	0.4	0.9	0.4	0.6	8.0	8.7	7.4	8.0
II	979.4	992.5	956.0	1012.7	0.6	4.2	2.0	2.2	5.5	-0.6	9.8	21	-6.5	23	93	81	94	88	0.4	1.7	0.7	0.9	7.7	8.8	7.5	8.0
III	986.1	1000.5	965.5	1019.6	-0.5	6.4	2.2	2.6	8.1	-2.7	16.9	31	-9.7	10	86	57	75	73	0.9	4.9	1.9	2.6	6.5	6.5	5.1	6.0
IV	985.1	996.9	962.0	1017.8	5.3	12.8	6.8	7.9	14.3	2.0	26.8	30	-6.7	15	85	52	81	73	1.6	8.8	2.1	4.1	6.8	6.8	5.6	6.4
V	983.2	992.5	972.3	1015.7	9.0	13.8	8.9	10.2	15.4	4.6	24.5	20	-1.9	29	80	57	80	72	2.7	8.1	2.4	4.4	6.1	7.6	6.1	6.6
VI	985.0	998.7	973.3	1016.7	16.7	22.5	16.3	18.0	24.3	10.7	31.9	30	4.3	27	73	54	76	67	5.4	14.3	4.8	8.1	5.1	6.4	4.2	5.2
VII	980.7	991.6	971.1	1012.2	17.3	22.6	17.4	18.7	24.2	13.7	35.0	5	8.9	30	82	60	85	76	4.0	12.6	3.3	6.6	6.5	6.8	6.8	6.7
VIII	983.1	993.0	970.4	1015.0	14.1	20.0	14.6	15.8	21.7	10.5	29.6	12	4.8	31	88	62	88	79	2.0	9.8	2.2	4.7	5.7	6.5	3.8	5.3
IX	981.8	990.6	967.2	1014.1	9.7	15.5	11.1	11.8	16.8	7.3	27.6	9	-1.4	26	91	63	87	80	1.1	7.2	1.8	3.4	5.9	6.8	6.0	6.2
X	988.2	997.8	972.6	1021.0	5.9	12.7	8.0	8.6	13.6	4.0	20.4	19	-2.6	3	94	68	89	84	0.6	5.2	1.2	2.3	5.7	5.8	4.1	5.2
XI	988.2	1006.3	971.8	1021.5	2.4	6.1	3.3	3.8	7.2	0.5	16.5	5	-10.1	30	92	79	88	86	0.5	2.4	0.9	1.3	7.5	6.7	6.3	6.8
XII	982.8	1001.3	948.5	1016.7	-2.8	-0.3	-1.9	-1.7	1.2	-5.2	8.9	14	-12.8	16	91	84	89	88	0.5	0.9	0.6	0.7	6.6	7.5	6.6	6.9
Rok	984.3	1006.3	948.5	1021.0	6.2	11.4	7.2	8.0	12.8	3.3	35.0	5.VII	-20.3	17.1	87	67	85	80	1.7	6.4	1.8	3.3	6.5	7.1	5.8	6.5

Strzyżów

$\varphi = 50°51'$ $\lambda = 24°02'$

I	–	–	–	–	-3.3	-1.2	-2.1	-2.2	–	-4.8	–	–	-14.7	17	–	–	–	–	–	–	–	–	8.3	8.0	8.3	8.2
II	–	–	–	–	0.0	3.1	1.3	1.4	–	-4.9	–	–	-6.2	1	–	–	–	–	–	–	–	–	6.2	6.0	6.3	6.2
III	–	–	–	–	-1.7	4.4	0.8	1.1	–	-3.7	–	–	-16.3	4	–	–	–	–	–	–	–	–	4.0	3.7	3.8	3.8
IV	–	–	–	–	5.6	13.4	7.6	8.5	–	1.9	–	–	-5.7	10	–	–	–	–	–	–	–	–	4.3	4.3	4.9	4.5
V	–	–	–	–	10.0	14.7	10.3	11.3	–	6.4	–	–	-0.7	5	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16.1	22.8	17.1	18.3	–	10.8	–	–	4.1	2	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	18.1	23.1	18.0	19.3	–	13.4	–	–	9.2	29	–	–	–	–	–	–	–	–	5.4	4.8	5.7	5.3
VIII	–	–	–	–	15.9	20.9	16.2	17.3	–	11.3	–	–	4.4	24	–	–	–	–	–	–	–	–	4.0	4.8	4.1	4.3
IX	–	–	–	–	10.2	16.6	12.7	13.0	–	8.0	–	–	-1.6	27	–	–	–	–	–	–	–	–	5.6	5.8	5.5	5.6
X	–	–	–	–	5.1	12.6	7.4	8.1	–	2.4	–	–	-4.1	3	–	–	–	–	–	–	–	–	4.3	3.5	2.8	3.5
XI	–	–	–	–	2.0	5.5	3.3	3.5	–	0.4	–	–	-10.7	30	–	–	–	–	–	–	–	–	7.0	6.9	6.3	6.7
XII	–	–	–	–	-3.5	-1.3	-2.3	-2.4	–	-6.0	–	–	-13.7	16	–	–	–	–	–	–	–	–	7.1	6.8	5.9	6.6
Rok	–	–	–	–	6.2	11.2	7.5	8.1	–	3.2	–	–	-16.3	4.III	–	–	–	–	–	–	–	–	–	–	–	–

Lipowa

$\varphi = 50°50'$ $\lambda = 21°27'$

I	–	–	–	–	-2.9	-0.7	-1.8	-1.8	0.8	-5.1	7.5	7	-17.6	17	–	–	–	–	–	–	–	–	9.3	9.1	8.4	8.9
II	–	–	–	–	0.7	3.6	1.7	1.9	5.2	-0.7	8.6	21	-6.6	31	–	–	–	–	–	–	–	–	8.4	8.1	8.0	8.2
III	–	–	–	–	-0.1	5.5	2.1	2.4	7.4	-2.1	16.5	30,31	-9.1	3	–	–	–	–	–	–	–	–	6.7	6.7	6.0	6.5
IV	–	–	–	–	4.9	12.6	7.6	8.2	14.1	2.5	26.5	30	-3.6	10	–	–	–	–	–	–	–	–	6.7	6.8	6.5	6.7
V	–	–	–	–	8.6	13.2	9.1	10.0	15.2	5.2	23.5	19	0.4	29	–	–	–	–	–	–	–	–	7.5	8.4	7.4	7.8
VI	–	–	–	–	16.3	22.0	16.6	17.9	24.2	11.1	31.5	12	5.1	7,8	–	–	–	–	–	–	–	–	5.2	5.4	4.6	5.1
VII	–	–	–	–	17.0	22.6	17.5	18.6	24.4	13.5	34.0	5	9.6	4,26,30	–	–	–	–	–	–	–	–	6.3	6.9	7.3	6.8
VIII	–	–	–	–	14.1	19.5	15.1	16.0	21.8	11.4	30.0	12	5.6	24	–	–	–	–	–	–	–	–	5.9	6.6	5.7	6.1
IX	–	–	–	–	9.5	15.2	11.5	11.9	17.1	8.0	27.0	9	0.6	26,27	–	–	–	–	–	–	–	–	6.2	7.5	7.4	7.0
X	–	–	–	–	5.8	12.4	7.6	8.4	13.6	4.0	20.0	19	-1.9	3	–	–	–	–	–	–	–	–	7.0	6.4	6.1	6.5
XI	–	–	–	–	2.0	5.9	2.7	3.3	7.6	0.4	16.0	1,5	-9.8	30	–	–	–	–	–	–	–	–	8.1	7.7	7.0	7.6
XII	–	–	–	–	-2.8	-0.6	-2.2	-2.0	0.7	-5.1	8.6	14	-12.8	16	–	–	–	–	–	–	–	–	7.5	7.6	7.5	7.5
Rok	–	–	–	–	6.1	10.9	7.3	7.9	12.7	3.5	34.0	5.VII	-17.6	17.1	–	–	–	–	–	–	–	–	7.1	7.3	6.8	7.1

Świdnica

$H_s = 230\ m$ $h_w = 15\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU °D:°mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10	Max>25°	Opad R 0.1 ≥1 R	1.0 ≥1 R	10.0 ≥1 R	Wiatr v 10 ≥1	15 >1	≡	≋	◔	●	⊠
I	3	3.0	1	4.0	4	3.0	2	1.0	6.5	2.4	44.5	4.0	13	4.2	9	4.4	10	3.4	12.1	3.5	6	19	7	4	·	8	5	·	3	·	1	·	2	15	10
II	6.5	1.5	1	4.0	·	·	9	1.9	10	4.0	31.5	4.3	10.5	4.9	5.5	3.1	10	3.3	27.3	12.1	18	11	·	·	·	10	5	1	1		–		1	12	3
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.9	14.3	29	–	–	–	·	9	8	1	–	–	–	–	–	–	–
IV	1.7	3.4	4.5	2.1	7.5	1.8	4	3.0	5.5	2.5	7.5	3.1	8	2.1	1.5	3.2	2.1	2.2	12.7	5.0	24	9	·	·	·	9	4	·	·	·	2	·	4	7	·
V	1.1	2.4	12.5	3.0	9.5	2.3	7.5	1.5	4.5	1.1	2	2.5	6	3.3	2.5	3.5	1.5	2.3	30.0	10.3	5	5	·	·	·	7	6	1	·	·	·	3	5	1.1	1
VI	4.5	1.9	7.5	2.2	1.2	2.2	9.5	2.4	5	3.5	1.4	2.6	10.5	2.7	1.9	2.9	8	2.3	38.8	18.9	4	·	·	·	1.0	8	7	1	·	·	2	3	7	8	·
VII	9	2.9	2.5	2.6	2	2.5	9	1.9	5	2.6	16.5	2.9	16.5	2.4	2.1.5	3.0	1.1	2.4	47.4.2	28.2	23	·	·	·	1.1	18	1.7	8	·	·	2	6	2	1.6	·
VIII	2	2.0	2	2.0	1	3.0	3	1.0	6	3.2	3.0	3.8	1.5	2.3	2.0	3.0	1.4	2.6	57.0	10.8	16	·	·	·	3	1.4	1.3	1	1	·	·	3	4	7	·
IX	4	4.6	·	·	4	1.2	2.5	1.4	8	3.4	3.2.5	4.2	1.8.5	4.0	1.1.5	4.4	9	3.5	45.6	7.6	9	·	·	·	2	1.3	1.1	·	1	·	1	·	1	1.0	·
X	6.5	1.3	·	·	·		2.5	2.4	6.5	4.2	4.7	4.2	1.0	3.1	8.5	3.3	1.2	3.2	4.1	3.5	20	2	·	·	·	3	1	·	·	·	1	·	6	5	·
XI	3	8.3	5	3.2	6	3.7	2.5.5	2.0	1.0	3.1	2.0	4.0	6.5	5.8	9	5.2	5	3.4	11.4	4.2	25	8	1	1	·	8	4	·	1	·	4	·	2	1.8	·
XII	6.5	2.6	6	2.6	1	1.0	2	1.0	7	2.6	3.7	4.8	1.0	4.6	1.4.5	4.1	1.0	3.6	22.8	4.9	14	22	5	2	·	1.0	6	·	5	2	4	·	2	1.2	8
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.4.9	28.2	23.VII	–	–	–	26	1.1.7	8.7	1.3	–	–	–	–	–	–	–

Kielce

$H_s = 268\ m$ $H_b = 270{,}0\ m$ $h_w = 21\ m$

I		·	5	3.5	4.5	3.7	7.5	1.9	6.5	2.0	3.4	2.1	2.5.5	2.9	3	4.0	7	2.3	32.3	6.8	5	25	1.0	6	·	1.7	9	·	·	·	4	·	2	2.1	2.7
II	3.5	1.9	0.5	3.0	1	2.0	5	4.6	2.1.5	3.6	2.0.5	3.0	1.1.5	3.9	7.5	1.9	1.3	2.8	45.5	10.8	19	1.6	2	·	·	1.9	1.3	1	1	·	5	·	1	1.8	1.0
III	2	1.8	1.5	6.7	1.3	3.2	1.1	5.9	1.3.5	2.9	5.5	4.4	1.9	3.9	6.5	3.0	2.1	2.8	2.1.4	8.4	1.5	2.2	2	·	·	6	4	·	2	·	1	·	5	1.1	4
IV	3	2.2	2.5	4.2	2.5	2.0	4.5	2.7	1.1	2.8	8	2.3	8	2.2	1.5.5	1.7	3.5	1.4	2.8.4	6.9	7	1.0	·	·	2	1.3	7	·	·	·	1	2	3	1.3	·
V	7	1.9	12.5	4.1	1.2	3.6	6	3.2	7.5	2.1	5	2.4	1.1.5	2.8	1.5.5	2.7	1.6	2.5	3.1.2	1.3.1	9	3	·	·	·	7	4	2	·	·	1	·	2	1.2	·
VI	5	2.4	4	2.1	1.5	3.0	3.5	3.3	1.5	2.9	1.0.5	2.5	2.3	2.6	1.0.5	2.3	1.7	2.1	6.1.8	1.8.9	2.0	·	·	·	1.3	1.0	9	2	·	·	·	7	3	5	·
VII	·	·	2	2.5	5.5	4.3	4.5	3.1	1.2.5	2.3	1.6.5	2.8	2.8.5	3.1	7.5	2.5	1.6	2.4	4.6.1.6	3.7.0	2.1	·	·	·	1.2	1.6	1.2	6	·	·	·	6	3	1.2	·
VIII	·	·	·	·	·	·	2.5	3.8	1.0.5	3.9	2.1	3.1	3.0.5	2.8	7.5	2.7	2.1	2.4	8.0.4	2.3.2	7	·	·	·	6	1.6	1.3	2	·	·	1	4	4	4	·
IX	2	4.0	·	·	·	·	1	3.5	1.2.5	3.0	2.4.5	4.1	2.7	4.4	3	2.5	2.0	3.1	6.6.1	1.2.0	2.3	2	·	·	2	1.5	1.3	2	·	·	1	1	3	1.0	·
X	2	4.0	·	·	1	4.0	7.5	2.8	1.2	3.5	2.8	2.5	1.7	3.1	2.5	2.2	2.3	2.2	12.1	4.4	22	3	·	·	·	7	4	·	·	·	3	·	4	5	·
XI	3.5	6.6	7	5.6	7.5	4.6	1.9.5	3.9	1.1.5	3.4	9.5	4.4	1.1.5	5.0	3	7.7	1.7	3.7	1.8.5	7.3	28	1.1	2	1	·	9	4	·	1	·	7	·	4	1.4	1
XII	4.5	2.8	2.5	3.6	3	3.8	6.5	4.5	1.4.5	3.0	2.4.5	3.6	1.2.5	3.2	6	2.8	1.9	2.7	3.2.7	1.0.6	8	2.9	1.0	4	·	1.1	7	1	·	·	4	·	3	1.5	2.8
Rok	3.2.5	2.3	3.7.5	2.9	5.4.5	2.8	7.9	3.4	1.4.8.5	2.9	2.0.7.5	3.1	2.2.5.5	3.3	8.8	3.0	2.2.5	2.5	5.9.2.0	3.7.0	2.1.VII	1.2.1	2.6	1.1	3.5	1.4.6	9.9	1.6	4	·	2.8	2.0	3.7	1.4.0	7.0

Strzyżów

$H_s = 185\ m$ $h_w = 11.5\ m$

I	·	·	6	5.8	4.5	6.1	1.3.5	4.5	7	3.6	2.9	6.0	2.1	6.9	8	7.6	2	5.8	1.5.1	5.8	5	2.6	–	3	–	1.3	3	·	5	·	–	·	1	2.0	–
II	6.5	2.6	4	1.5	7.5	1.9	1.2	3.2	1.6	2.0	1.4.5	2.0	9	1.8	1.1.5	2.2	3	2.1	3.4.9	6.8	1.5	2.5	–	·	–	1.1	1.0	·	·	·	–	·	5	1.3	–
III	1.1	1.7	7.5	1.4	9	3.8	4.5	2.9	6	1.9	5	2.5	1.5.5	1.6	1.9.5	2.4	1.5	1.9	1.6.8	6.6	1.5	2.6	–	2	–	7	4	·	·	·	–	·	1.1	8	–
IV	1.5	1.4	5.5	1.0	4.5	1.2	4	1.2	1.0	1.8	2	1.0	3.5	1.0	1.4.5	1.7	3.1	0.9	1.7.3	-	-	1.2	–	·	–	5	3	·	1	·	–	·	9	7	–
V	1.7.5	1.7	8	1.1	2.5	1.6	5	1.2	·	·	2	2.5	7	1.0	1.9	1.8	3.2	1.0	3.6.8	1.1.6	1.8	1	–	·	–	1.1	8	1	·	·	–	1	–	–	–
VI	6	1.5	3	1.3	3	1.0	4.5	1.8	7.5	1.9	1.0	2.4	9	1.7	1.9	1.7	2.8	1.2	3.2.5	1.2.3	2.2	·	–	·	–	6	4	2	·	·	–	·	–	–	–
VII	2.5	1.6	1.0	1.6	4	2.0	8	1.7	8.5	3.2	1.5	4.2	1.5	2.4	1.5	2.8	1.5	2.3	6.8.5	1.4.1	1.6	·	–	·	–	1.3	1.1	3	·	·	–	3	6	6	–
VIII	4	3.2	3	3.3	3	3.3	6.5	3.1	4.5	3.6	9.5	3.6	1.4	2.4	2.2.5	3.0	2.6	2.2	1.0.1.9	4.1.0	1.0	·	–	·	–	8	8	2	1	1	–	2	7	3	–
IX	8	1.5	2	2.5	1	1.0	5	3.2	7	3.7	1.5	3.4	3.2.5	2.5	1.6.5	3.0	3	2.7	3.8.7	8.5	1.2	2	–	·	–	1.2	1.0	·	·	·	–	1	3	3	–
X	4	2.2	2	1.0	4	2.5	2	2.0	4	1.5	1.7	2.2	1.4	2.1	1.6	1.9	3.0	1.4	8.3	4.7	2.0	8	–	·	–	3	3	·	·	·	–	·	9	4	–
XI	7.5	2.7	1.5	2.3	4.5	2.0	1.8	2.3	0.5	1.0	1.0.5	2.4	1.4.5	2.8	1.3.5	3.3	6	2.4	2.3.7	1.0.1	2.8	1.3	–	2	–	1.0	5	1	·	·	–	·	3	1.5	–
XII	4	2.5	2	2.5	9	2.0	1.2	2.1	1.1	2.4	2.6	2.8	1.3.5	2.3	1.3.5	3.2	2	2.5	3.3.7	1.3.0	8	2.9	–	7	–	7	5	1	·	·	–	·	2	1.4	–
Rok	8.6	1.9	6.8	2.1	5.6.5	2.4	9.7	2.4	8.2	2.2	1.5.5.5	2.9	1.6.8.5	2.4	1.8.8.5	2.9	1.9.3	2.2	4.2.8.2	4.1.0	1.0.VIII	1.4.2	–	1.4	–	1.0.6	7.4	1.0	7	1	–	8	–	–	–

Lipowa

$H_s = 245\ m$ $h_w = 16\ m$

I	·	·	4	2.0	6	5.8	4	6.0	2.8	3.6	1.2	4.6	2.8	5.0	9	4.3	2	4.3	1.3.5	6.0	5	2.9	1.3	8	·	6	4	·	5	·	–	·	·	2.5	1.8.1
II	2	2.0	5	2.2	2	3.0	6	5.3	3.2	5.0	8	3.2	2.1	3.3	8	3.8	·	4.0	1.8.8	3.0	2	1.5	·	·	·	1.4	1.0	·	8	·	–	·	1	1.5	4
III	6	2.3	1.0	3.6	1.3	4.8	1.2	5.8	1.3	5.3	8	2.6	1.3	7.8	1.3	3.7	5	4.5	1.3.8	7.0	1.5	2.4	6	·	·	9	3	·	9	1	–	·	3	1.0	·
IV	1.7	2.1	3	4.0	1.2	4.7	1.0	2.6	1.3	2.9	5	1.6	2	1.0	2.2	2.2	6	2.1	3.8.3	8.2	2.9	1.0	·	·	1	9	8	·	1	·	–	1	5	1.5	·
V	2.0	2.6	2.0	2.6	4.0	4.1	1.0	2.2	7	2.1	3	3.0	6	3.0	1.4	4.3	3	2.9	2.8.9	8.0	8	·	·	·	·	8	7	·	·	·	–	2	·	1.6	·
VI	1.3	2.3	8	2.5	9	2.6	9	4.2	1.8	2.6	5	3.8	5	3.4	1.2	4.4	1.1	2.7	5.4.6	2.8.8	22	·	·	·	1.0	7	5	2	2	·	–	8	4	6	·
VII	7	3.1	7	1.8	7	2.9	7	1.9	8	3.2	1.8	4.7	1.6	5.2	1.0	3.0	1.3	3.1	1.0.3.6	3.3.5	8	·	·	·	1.0	1.5	1.1	3	2	·	–	7	4	1.7	·
VIII	1	3.0	·	·	·	·	1.0	2.7	1.1	2.4	1.7	3.4	2.3	3.5	1.6	3.1	1.5	2.6	9.7.0	1.8.1	7	·	·	·	5	1.3	1.3	4	2	·	–	5	·	5	·
IX	5	2.2	4	1.0	·	·	1.1	1.9	9	3.5	1.7	4.4	2.8	5.8	1.0	3.8	9	3.8	3.0.3	6.6	4	·	·	·	1	8	7	·	5	·	–	·	3	1.5	·
X	2	1.0	2	1.0	·	·	1.9.5	1.9	1.9	3.1	1.8.5	3.1	1.7	2.9	9	2.3	6	2.5	2.1.3	1.7.6	2.3	·	·	·	·	5	2	·	1.1	1	–	·	1	1.6	·
XI	1	9.0	5.5	3.6	1.5	4.0	2.2.5	4.0	1.7.5	3.6	5	6.3	1.3	8.4	6.5	1.1.8	6	5.0	8.1	6.5	2.8	1.3	2	·	·	5	3	·	4	·	–	·	3	1.7	·
XII	3.5	2.1	1.3.5	1.9	1	2.0	1.0.5	2.0	1.5.5	3.6	2.1.5	4.0	1.1.5	4.5	8	5.8	8	3.2	6.5	–	–	2.7	1.2	2	·	5	3	·	4	·	–	·	3	1.7	·
Rok	7.7.5	2.6	7.9	2.2	7.5	2.6	1.3.1.5	3.4	1.9.1	3.4	1.3.6	5.7	1.8.3.5	4.5	1.3.7.5	4.4	8.4	3.4	4.3.4.7	3.3.5	8.VII	1.1.8	3.3	1.0	2.7	1.0.2	7.6	1.0	5.0	2	–	2.3	2.7	1.6.9	2.2.1

Częstochowa

$\varphi = 50°49'$ $\lambda = 19°06'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	989.4	1000.6	972.0	1022.6	-2.4	0.5	-1.4	-1.2	1.5	-3.9	7.6	6	-17.2	17	89	82	88	86	0.5	1.2	0.6	0.8	7.8	8.3	7.5	7.9
II	980.0	999.7	955.6	1012.3	0.9	5.1	2.3	2.6	6.2	-0.2	14.0	21	-4.4	24	92	76	89	86	0.6	2.3	0.8	1.2	7.1	7.6	7.2	7.3
III	986.6	1001.8	967.0	1019.1	0.4	7.2	3.5	3.6	8.8	-1.1	16.8	14	-7.7	4	86	65	80	77	1.0	4.2	1.6	2.3	5.7	5.8	5.5	5.7
IV	986.2	997.7	962.9	1018.1	5.0	11.9	7.6	8.0	13.5	2.7	26.7	30	-4.2	14,15	88	58	77	74	4.2	7.2	2.6	3.7	5.9	6.7	4.8	5.8
V	984.3	993.6	975.1	1015.8	8.6	14.1	9.7	10.5	15.4	4.9	25.2	19	-1.4	7	81	55	77	71	2.2	8.2	3.0	4.5	6.2	7.7	5.6	6.5
VI	985.7	1000.2	973.7	1016.5	16.4	22.5	17.2	18.3	24.5	11.1	34.4	30	4.3	28	65	43	62	57	7.0	16.4	7.8	10.4	4.2	6.1	4.0	4.8
VII	981.7	993.8	971.3	1012.2	17.1	22.7	17.8	18.8	24.3	13.7	36.0	8	9.6	29	84	62	82	76	3.6	12.8	4.4	6.9	6.5	7.1	6.4	6.7
VIII	984.1	994.3	970.8	1015.1	13.7	19.8	14.5	15.6	21.6	10.7	27.8	11	6.4	31	91	62	87	80	1.5	9.0	2.4	4.3	7.0	7.1	3.4	5.7
IX	982.7	994.7	968.2	1014.1	9.4	15.2	11.1	11.7	16.7	7.3	27.4	9	0.0	26,27	93	70	88	84	0.8	5.8	1.6	2.7	6.6	7.4	5.4	6.5
X	988.9	997.5	972.9	1020.8	5.9	13.0	7.9	8.7	13.9	4.1	20.4	19	-0.5	3	94	69	90	84	0.5	5.0	1.1	2.2	5.8	6.5	3.8	5.4
XI	988.8	1006.4	974.4	1021.2	3.3	6.7	4.0	4.5	7.8	1.5	18.4	5	-8.8	30	90	78	88	85	0.8	2.7	1.1	1.5	7.2	6.7	7.3	7.1
XII	983.5	1002.5	949.8	1016.4	-2.3	0.5	-1.2	-1.0	1.7	-4.5	10.6	13	-15.6	16	89	83	89	87	0.5	1.1	0.6	0.7	7.0	7.6	6.6	7.1
Rok	985.2	1006.4	949.8	1017.1	6.3	11.6	7.8	8.4	13.0	3.9	36.0	8.VII	-17.2	17.1	87	67	83	79	1.7	6.3	2.3	3.4	6.4	7.0	5.6	6.3

Szczawno-Zdrój

$\varphi = 50°48'$ $\lambda = 16°15'$

I	–	–	–	–	-1.4	0.7	-1.0	-0.7	2.1	-3.8	9.1	6	-19.5	17	88	86	87	87	0.7	0.9	0.8	0.8	8.0	7.3	5.6	7.0
II	–	–	–	–	2.1	4.8	2.3	2.9	6.0	-0.3	13.8	3	-8.7	27	90	80	92	87	0.7	1.8	0.6	1.0	7.7	8.1	6.7	7.5
III	–	–	–	–	2.5	6.9	3.9	4.3	8.6	0.2	17.0	13	-6.6	3	85	70	83	79	1.3	3.5	1.6	2.1	6.5	6.4	4.4	5.8
IV	–	–	–	–	5.5	10.2	5.7	6.8	11.7	1.9	22.8	28	-3.5	15	88	71	90	83	1.2	4.6	1.0	2.3	6.4	7.3	4.5	6.1
V	–	–	–	–	8.6	12.7	7.9	9.3	14.4	4.3	23.5	16	-1.7	7	81	63	87	77	2.6	6.0	1.5	3.4	5.4	7.9	5.6	6.3
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	17.1	20.5	16.6	18.0	22.3	13.7	34.5	5	9.7	28	79	68	82	76	4.7	9.7	3.8	6.1	7.5	7.7	7.2	7.5
VIII	–	–	–	–	14.1	18.3	13.9	15.0	19.7	10.6	26.0	11	5.8	23	79	62	82	74	3.4	8.4	3.0	4.9	6.3	8.0	5.8	8.7
IX	–	–	–	–	10.7	14.6	10.6	11.6	15.8	7.6	25.8	8	-0.7	27	79	66	83	76	2.8	6.0	2.3	3.7	6.9	8.0	6.3	7.1
X	–	–	–	–	7.9	12.3	8.9	9.5	13.4	5.8	20.1	19	0.3	3	81	64	80	75	2.1	5.6	2.5	3.4	6.2	5.7	3.7	5.2
XI	–	–	–	–	3.6	6.1	4.5	4.7	7.3	2.0	15.7	6	-11.4	30	82	74	83	80	1.4	2.7	1.6	1.9	7.8	8.7	8.1	8.2
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	-19.5	17.1	–	–	–	–	–	–	–	–	–	–	–	–

Karpacz

$\varphi = 50°46'$ $\lambda = 15°46'$

I	936.3	946.6	920.5	–	-1.7	-0.1	-1.4	-1.2	1.6	-4.2	8.9	5	-15.3	16	81	77	80	79	1.2	1.6	1.3	1.4	7.1	6.8	5.8	6.6
II	927.1	947.5	902.9	–	1.4	3.1	1.3	1.8	4.2	-1.0	11.3	3	-6.3	26	82	77	84	81	1.4	1.9	1.1	1.5	7.4	7.5	6.8	7.2
III	933.5	949.3	918.6	–	1.5	5.4	2.5	3.0	6.8	-0.6	12.2	23	-9.5	3	75	65	76	72	1.8	3.6	2.0	2.5	6.7	6.6	5.6	6.3
IV	934.9	946.3	914.7	–	3.8	7.2	3.7	4.6	8.6	0.8	19.8	28	-6.4	13	82	72	86	80	1.8	3.7	1.3	2.3	6.5	6.9	5.2	6.2
V	933.8	941.7	926.0	–	6.3	9.5	6.0	7.0	11.2	2.8	21.2	16	-4.0	7	79	66	82	76	2.3	4.6	1.8	2.9	6.0	7.5	5.7	6.4
VI	935.7	949.3	924.3	–	14.2	17.9	13.5	14.8	19.6	10.4	27.8	30	5.0	26	77	63	79	73	4.5	8.2	3.5	5.4	5.7	5.7	5.2	5.5
VII	932.7	943.5	922.7	–	14.9	17.8	14.7	15.5	19.3	12.2	31.1	5	8.0	28	86	75	86	82	2.9	6.3	3.0	4.1	6.7	7.3	7.1	7.0
VIII	933.9	943.7	922.5	–	12.1	15.1	11.9	12.8	16.5	9.2	22.6	9,11	4.3	23	83	72	84	80	2.5	5.2	2.5	3.4	6.2	7.8	5.1	6.4
IX	932.1	941.9	917.9	–	8.7	11.7	8.8	9.5	12.6	6.0	23.6	8	-1.1	27	85	74	85	81	1.8	3.8	1.9	2.5	7.0	7.4	4.8	6.4
X	936.7	944.3	921.0	–	6.5	9.9	7.3	7.8	10.9	4.3	17.7	19	-0.8	1	83	73	80	79	1.8	3.6	2.3	2.6	5.1	5.0	3.7	4.6
XI	935.8	949.6	921.7	–	2.2	4.0	2.6	2.8	5.5	0.3	12.9	4	-13.9	30	86	79	87	84	1.1	2.0	1.1	1.4	6.9	7.0	7.0	7.0
XII	930.7	948.2	900.1	–	-1.2	-0.2	-1.1	-0.9	1.7	-4.2	9.6	13	-12.8	16	77	77	82	79	1.5	1.6	1.1	1.4	6.7	6.4	5.5	6.2
Rok	933.6	949.6	900.1	–	5.7	8.4	5.8	6.5	9.9	3.0	31.1	5.VII	-15.3	16.1	81	72	83	79	2.0	3.8	1.9	2.6	6.5	6.8	5.6	6.3

Dobrogostów

$\varphi = 50°46'$ $\lambda = 17°01'$

I	–	–	–	–	-1.0	1.4	-0.5	-0.2	2.5	-3.0	10.7	6	-17.0	17	86	80	85	84	0.8	1.5	0.9	1.1	8.1	7.6	6.3	7.3
II	–	–	–	–	2.3	6.1	2.8	3.5	7.0	0.9	13.2	5	-8.9	27	88	73	86	82	1.0	2.6	1.1	1.6	8.1	7.8	6.4	7.4
III	–	–	–	–	2.2	7.4	4.3	4.6	9.3	0.6	16.5	14	-8.4	1	–	–	–	–	–	–	–	–	5.4	6.1	4.7	5.4
IV	–	–	–	–	5.3	11.5	6.8	7.5	13.1	2.3	25.7	30	-4.7	15	90	65	82	79	0.9	5.9	1.9	2.9	5.3	6.8	4.9	5.7
V	–	–	–	–	9.1	14.3	9.5	10.6	16.0	4.6	26.6	19	-1.3	7	80	53	78	70	2.4	8.3	2.8	4.5	5.9	6.3	5.4	5.9
VI	–	–	–	–	16.6	22.1	16.0	17.7	24.2	11.2	34.3	11	6.5	27	78	56	84	73	4.3	12.9	3.1	6.8	5.1	5.3	4.8	5.1
VII	–	–	–	–	17.9	22.0	17.5	18.7	23.8	14.2	35.8	5	10.4	18	–	–	–	–	–	–	–	–	6.2	7.0	7.3	6.8
VIII	–	–	–	–	15.1	19.7	14.9	16.2	21.3	11.4	28.7	11	6.8	23	86	70	89	82	2.5	7.3	1.8	3.9	6.2	6.9	6.6	6.6
IX	–	–	–	–	11.2	16.3	11.6	12.7	17.4	8.1	27.9	8	0.6	27	–	–	–	–	–	–	–	–	6.1	7.0	5.1	6.1
X	–	–	–	–	7.6	13.8	9.3	10.0	14.8	5.3	21.1	19	-0.5	28	–	–	–	–	–	–	–	–	5.6	5.4	4.3	5.1
XI	–	–	–	–	4.3	7.6	4.6	5.3	8.6	2.4	18.6	5	-8.3	30	85	72	84	80	1.2	3.3	1.3	1.9	8.3	8.0	7.8	8.0
XII	–	–	–	–	-0.9	1.4	-0.4	-0.1	2.8	-3.2	10.7	13	-17.4	16	86	78	86	83	0.9	1.6	0.9	1.1	7.3	7.0	6.3	6.9
Rok	–	–	–	–	7.5	12.0	8.0	8.9	13.4	4.6	35.3	5.VII	-17.4	16.XII	–	–	–	–	–	–	–	–	6.5	6.8	5.8	6.4

Częstochowa

$H_s = 261\ m$ $H_b = 262{,}7\ m$ $h_w = 13\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D. °mD																	OPAD R			LICZBA DNI (n)																
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr		≡		◔	●	⊞
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min <0°	Max <0°	Min <-10°	Max >25°	0,1 ≤ < 1	1 ≤ < 10	10 ≤ < 100	10 ≥ > 15	15 ≥ > 15						
I	4	3,0	5	4,2	7	2,0	2,5	1,6	11,5	2,0	36,5	2,2	22,5	2,7	7	4,4	·	2,6	20,9	4,8	6	25	8	3	·	16	7	·	1	·	4	·	2	19	20
II	4	4,2	3,5	2,3	8,5	1,9	3,5	2,0	1,3	3,3	35,5	3,2	11,5	3,0	4,5	3,6	·	2,9	45,5	14,2	18	14	1	·	·	17	13	1	1	·	2	·	1	11	3
III	9	2,7	8	2,8	17,5	2,9	12,5	2,8	1,3	2,2	9	2,1	4,6	3,5	5	2,5	3	2,7	35,8	8,5	24	18	2	·	·	10	8	·	2	·	·	·	7	11	4
IV	2,6	1,8	9,5	2,4	7,5	1,8	6	2,0	8,5	2,1	4,5	2,7	11	2,4	1,3	2,7	4	2,1	31,4	8,1	26	9	·	·	1	14	6	·	·	·	3	2	5	11	·
V	17,5	2,0	2,3	2,5	15,5	2,7	4	1,9	6	2,1	4,5	3,1	9,5	2,8	1,2	2,5	1	2,4	31,1	11,2	20	2	·	·	1	10	8	1	·	·	·	2	·	10	·
VI	9	1,8	11	2,0	8,5	1,7	5,5	2,1	1,1	3,0	1,4	2,4	11,5	2,7	1,3,5	2,0	6	2,1	35,9	9,8	24	·	·	·	1,3	10	7	·	·	·	·	6	6	6	·
VII	8	2,1	4	2,4	1,0	1,8	7,5	2,1	6	2,2	1,9	2,9	2,2,5	3,0	1,2	2,3	4	2,4	148,0	64,4	16	·	·	·	1,3	17	1,4	4	·	·	·	5	3	1,4	·
VIII	6	2,2	1,5	1,7	·	·	4,5	1,4	3,5	2,4	17,5	2,2	3,2	2,2	2,1	2,3	7	2,0	108,4	25,6	16	·	·	·	6	15	1,5	2	1	·	·	4	2	3	·
IX	9	1,2	1	1,5	1	1,5	·	·	0,5	1,0	20,5	4,0	3,9,5	3,0	1,4,5	2,3	4	2,8	91,2	16,7	2	·	·	·	2	15	11	4	2	·	3	·	1	8	·
X	2	1,2	·	·	3	1,3	1	1,0	6,5	1,7	30,5	2,0	23,5	2,4	1,5,5	1,8	11	1,7	3,5	1,7	20	1	·	·	·	4	2	·	·	·	5	·	5	6	·
XI	2,5	7,2	13,5	2,6	21,5	1,8	3	1,0	1,0	2,5	1,0	2,0	18,5	3,9	5	4,3	6	2,6	27,9	7,5	28	13	1	·	·	10	6	·	·	·	2	·	6	18	·
XII	6,5	1,8	5,5	2,8	6,5	1,2	1	1,0	9	1,5	23,5	2,9	23	2,8	15	1,7	3	2,2	41,0	8,3	13	29	7	4	·	13	9	·	·	·	2	·	3	15	7
Rok	100,5	2,4	85,5	2,3	106,5	1,7	51	1,6	98,5	2,2	225	2,6	24,1	2,9	13,8	2,7	49	2,4	620,6	64,4	16.VII	111	19	7	36	151	104	12	7	·	21	19	41	132	34

Szczawno – Zdrój

$H_s = 415\ m$ $h_w = 11{,}5\ m$

I	1	2,0	3	2,0	·	·	3	2,8	3,5,5	3,8	3,1	4,5	1,2	3,2	3,5	4,0	4	3,7	28,4	6,7	6	23	8	3	·	14	9	·	3	1	2	·	3	14	23
II	·	·	·	·	1	2,0	2	1,0,5	2,6,5	6,0	2,6,5	5,2	1,2,5	2,8	1,1,5	2,6	4	4,6	40,6	11,3	18	14	·	·	·	15	8	1	4	2	4	·	·	15	4
III	3	1,3	5,5	3,9	6,5	3,9	3,5	2,3	21,5	5,4	1,8	4,3	8,5	3,5	1,6,5	1,8	10	3,4	59,2	11,3	16	14	1	·	·	14	12	2	3	1	3	1	5	10	6
IV	1,8	1,8	9,5	1,6	4	1,8	1	2,5	8	2,7	1,2	2,1	8,5	1,9	1,6	1,7	13	1,6	26,9	10,4	7	11	·	·	·	13	6	1	·	·	6	·	2	9	·
V	26,5	2,0	15,5	1,6	2	2,5	0,5	5,0	6,5	3,5	4	2,0	12,5	2,3	1,8,5	3,8	7	2,3	39,5	11,2	5	5	·	·	·	10	9	1	·	·	2	4	·	12	1
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	50,1	18,6	4	–	·	·	–	10	7	2	–	–	–	6	–	–	–
VII	1,3	1,2	3	1,5	·		·	·	1,0	2,7	2,7	3,0	2,3,5	3,0	1,2,5	2,3	4	2,4	19,9,4	4,0,2	25	·	·	·	1,0	19	1,7	8	·	·	1	9	1	1,6	·
VIII	2,5	1,8	·	·	2	1,5	·	·	1,4,5	5,2	3,7,5	3,7	2,4,5	2,3	6	3,6	6	3,2	85,5	10,5	24	·	·	·	1	16	1,5	1	4	1	·	4	1	10	·
IX	1,5	3,0	1,5	1,0	2,5	1,0	0,5	4,0	1,1	5,9	4,2	5,3	1,6,5	3,7	1,1,5	4,2	3	4,5	55,5	8,5	23	1	·	·	1	18	1,5	·	6	1	·	2	2	12	·
X	2,5	1,6	0,5	1,0	1	2,0	2	6,5	2,0	5,0	4,3,5	4,5	1,6	2,0	6,5	2,4	1	3,9	6,8	2,7	20	·	·	·	·	7	2	·	3	1	4	·	7	6	·
XI	6	4,8	3,5	3,0	1,1	2,1	8,5	1,9	2,4,5	3,9	2,1,5	6,2	1,0,5	5,0	2,5	8,4	2	4,2	2,4,5	4,4	11	1,3	1	1	·	9	8	·	7	1	9	·	1	1,9	1
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3,8,7	7,5	14	–	–	–	–	1,3	1,0	·	–	–	–	·	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6,3,5,1	4,0,2	23.VII	–	–	–	–	1,5,8	1,1,8	1,6	–	–	–	2,6	–	–	–

Karpacz

$H_s = 700\ m$ $H_b = 707{,}9\ m$ $h_w = 20\ m$

I	2	3,0	·	·	·	·	·	·	6,5	4,3	11,5	3,9	7,5	3,6	9,5	3,7	56	1,5	29,8	7,7	6	28	10	3	·	12	8	·	2	·	2	·	4	13	29
II	4,5	2,1	1,5	1,3	1	3,0	4	4,6	13,5	6,6	11	3,7	4	2,0	13,5	3,0	31	2,5	122,2	4,1,2	13	16	3	·	·	18	13	4	7	3	5	·	1	12	14
III	1	1,0	1,5	3,7	4	2,5	6,5	4,9	7,5	11,2	3	4,7	4,5	3,2	1,5	2,6	50	2,2	85,4	15,5	17	13	3	·	·	12	12	3	3	2	7	1	4	11	12
IV	6,5	1,7	2,5	1,6	5	2,5	8,5	3,3	3,5	6,7	0,5	6,0	5	1,6	1,3,5	2,2	45	1,3	106,6	44,6	7	14	1	·	·	17	12	3	1	·	5	·	2	9	4
V	9	1,6	6	1,4	3	1,7	4	2,2	2	2,0	3,5	1,9	4	1,9	2,1,5	2,5	40	1,2	66,4	18,3	5	11	·	·	·	11	7	3	·	·	3	3	·	11	3
VI	6	1,6	3	1,2	3	2,3	9,5	4,2	5,5	2,2	4	2,1	1,1,5	1,8	9,5	2,6	38	1,4	82,1	27,2	4	·	·	·	5	13	10	4	2	·	3	8	5	6	·
VII	4,5	1,9	2	1,0	3	2,7	1	1,0	3,5	3,4	2	3,3	10,5	2,1	1,8,5	2,6	42	1,4	35,8,0	58,2	11	·	·	·	7	22	1,7	9	·	·	4	12	1	1,6	·
VIII	3	1,7	2,5	1,4	·	·	6,5	5,1	9	3,4	10	4,0	1,1,5	2,5	8,5	2,7	42	1,8	69,4	16,1	24	·	·	·	·	17	1,4	2	4	·	2	5	·	9	·
IX	5,5	2,1	1	1,0	1	2,0	1	3,0	1,0	3,8	1,7	4,2	1,1,5	4,1	8	3,3	35	2,2	1,4,9,7	3,6,1	23	1	·	·	·	18	1,5	6	3	1	1	4	·	8	·
X	6	1,8	1	2,0	0,5	3,0	3,5	2,1	9	4,4	8	3,6	7,5	2,3	4,5	2,4	53	1,3	13,2	4,8	20	2	·	·	·	8	5	·	·	·	3	·	9	4	·
XI	5	2,1	2	1,5	2,5	3,6	4	3,9	6,5	8,1	4,5	3,1	5,5	2,6	1,3	3,5	47	1,8	54,2	11,2	8	14	2	1	·	11	9	2	3	1	6	·	4	14	1
XII	1	3,0	·	·	1	1,0	3	6,3	3,5	11,3	10,5	3,6	9	2,6	2,1	2,8	44	2,0	91,6	27,3	8	28	8	3	·	15	12	1	1	1	6	·	3	8	25
Rok	54	2,0	2,3	1,3	24	2,0	51,5	3,4	80	5,6	91,5	3,7	92	2,5	1,5,6	2,8	523	1,7	12286	58,2	11.VII	127	27	7	12	174	134	37	26	8	47	33	33	121	88

Dobrogostów

$H_s = 170\ m$ $h_w = 15\ m$

I	3	7,0	7,5	2,9	5	2,2	8	4,9	1,5,5	5,6	2,6	8,1	2,5	6,2	3,5	8,1	22	4,7	13,5	3,7	27	21	7	4	·	8	4	·	7	3	–	–	2	16	10
II	4	2,5	3	2,3	3,5	2,0	8	2,0	16	5,8	22	6,2	3,5	7,1	8	5,8	16	4,1	35,0	11,3	18	8	1	·	·	12	8	1	6	·	–	–	2	14	3
III	5,5	3,0	11	2,1	18	3,2	14	2,7	11,5	5,3	8,5	5,1	2,5	6,4	8	5,4	14	3,2	76,3	26,8	29	15	2	·	·	10	8	2	1	·	–	–	9	12	2
IV	19,5	3,8	17	2,1	9	1,5	4,5	2,1	5	4,5	6	4,2	1	2,5	1,6	3,4	12	2,6	16,4	4,3	19	11	·	·	1	9	5	·	1	·	–	–	3	6	·
V	15	3,2	28,5	2,2	19,5	1,7	2,5	1,8	2,5	4,0	5,5	2,8	1	1,0	1,4,5	5,4	4	2,7	25,4	13,2	5	5	·	·	2	9	4	1	·	·	–	–	1	9	·
VI	8,5	2,8	15,5	1,8	20	1,6	12	1,7	2,5	3,8	4	5,0	1	2,0	10,5	4,6	16	2,1	72,8	26,7	24	·	·	·	11	8	6	3	1	·	–	–	6	5	·
VII	8	3,2	16,5	1,6	14,5	1,3	6,5	1,4	8	4,1	7	3,4	4	4,2	2,5,5	4,3	3	2,8	20,5,1	3,4,8	11	·	·	·	11	19	1,6	8	·	·	–	–	3	15	·
VIII	18,5	3,6	11,5	2,2	18	1,8	5,5	2,0	7	3,2	16	5,5	7	5,1	6,5	3,7	3	3,3	58,7	17,8	16	·	·	·	3	12	11	2	3	·	–	–	·	8	·
IX	4	3,8	3	2,7	12	1,4	8,5	2,3	10	3,6	24	5,9	11,5	6,3	11	4,3	6	3,9	37,2	11,3	9	·	·	·	3	14	11	1	2	1	–	–	1	8	·
X	3,5	3,3	2,5	1,4	10,5	1,4	15,5	2,3	13,5	4,1	25,5	4,4	5	4,0	5	3,4	12	2,9	0,5	0,2	6,18	1	·	·	·	3	·	·	·	·	–	–	6	4	·
XI	5,5	8,1	10,5	4,2	27	3,0	17,5	2,7	4,5	4,7	7,5	8,5	7	9,5	8,5	9,9	2	5,0	21,5	8,9	25	7	1	·	·	8	5	·	9	1	–	–	1	17	·
XII	7,5	3,8	8,5	2,6	5	1,2	8	2,6	11,5	5,7	20	8,4	5,5	5,5	11	5,1	18	4,2	26,9	7,1	14	22	4	2	·	8	5	·	9	1	–	–	1	13	7
Rok	102,5	4,0	13,3	2,3	16,2	1,9	110,5	2,4	107,5	4,3	17,2	5,6	5,1,5	5,0	12,8	5,3	126	3,5	609,3	34,8	11.VII	90	15	6	34	120	83	18	39	6	–	–	35	127	22

Werbkowice

$\varphi = 50°45'$ $\lambda = 23°46'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	–	–	–	–	-3.2	-1.1	-2.1	-2.1	0.1	-4.7	4.5	9	-14.7	17	87	83	89	86	0.6	1.0	0.5	0.7	8.3	8.0	8.3	8.2
II	–	–	–	–	0.2	3.8	1.1	1.6	5.1	-1.2	11.3	6	-5.5	28	88	79	85	84	0.7	1.9	1.0	1.2	7.4	8.1	6.2	7.2
III	–	–	–	–	-1.8	4.7	0.5	1.0	6.5	-3.6	16.7	28	-17.2	4	–	–	–	–	–	–	–	–	5.0	4.5	3.5	4.3
IV	–	–	–	–	5.0	13.4	8.0	8.6	14.8	2.2	26.6	29	-5.2	10	84	50	73	69	1.6	9.2	3.3	4.7	6.0	6.0	5.2	5.7
V	–	–	–	–	9.4	14.3	10.3	11.1	16.1	6.4	25.2	18	-1.2	5	83	64	80	76	2.1	6.8	2.5	3.8	6.9	7.7	7.6	7.4
VI	–	–	–	–	16.1	23.0	16.8	18.2	24.6	10.6	32.0	12	4.6	28	77	53	76	69	4.4	13.7	4.7	7.6	3.5	3.3	3.5	3.4
VII	–	–	–	–	17.0	23.5	17.4	18.8	24.9	13.3	34.2	5	8.4	7	86	58	85	76	2.8	13.3	3.2	6.4	5.5	4.9	6.2	5.5
VIII	–	–	–	–	14.5	20.8	15.4	16.5	22.5	10.8	31.4	14	5.0	24,31	92	62	86	80	1.4	10.2	2.5	4.7	4.7	5.6	4.4	4.9
IX	–	–	–	–	9.5	16.7	10.9	12.0	17.9	7.4	28.0	9	-2.0	27	95	63	91	83	0.6	7.4	1.3	3.1	6.2	6.0	4.4	5.5
X	–	–	–	–	3.9	13.2	6.7	7.6	14.2	2.1	21.7	19	-3.5	3	94	65	90	83	0.6	5.9	1.1	2.5	5.3	4.5	2.9	4.2
XI	–	–	–	–	1.7	5.7	2.7	3.2	6.7	-0.1	18.1	1	-10.3	30	94	83	91	89	0.4	1.8	0.6	0.9	8.3	7.6	6.7	7.5
XII	–	–	–	–	-3.8	-0.5	-2.6	-2.4	0.5	-6.1	7.6	13,14	-13.3	16	90	81	89	87	0.5	1.1	0.6	0.7	7.8	7.3	5.2	6.8
Rok	–	–	–	–	5.7	11.5	7.1	7.8	12.8	3.1	34.2	5.VII	-17.2	4.III	–	–	–	–	–	–	–	–	6.2	6.1	5.3	5.9

Śnieżka

$\varphi = 50°44'$ $\lambda = 15°44'$

I	833.3	844.5	820.5	–	-5.3	-4.6	-5.3	-5.1	-2.3	-7.9	5.1	9	-17.9	16	83	78	80	80	0.9	1.3	1.0	1.1	6.9	7.5	6.3	6.9
II	827.6	843.5	806.0	–	-4.5	-3.6	-4.0	-4.0	-1.7	-6.1	5.4	6	-11.9	26	91	94	96	94	0.5	0.4	0.2	0.4	8.3	8.7	8.4	8.5
III	834.2	846.6	821.0	–	-3.0	-1.7	-2.1	-2.2	0.3	-4.9	8.5	13	-13.4	2	78	77	79	78	1.2	1.4	1.2	1.3	7.0	7.7	6.9	7.2
IV	835.9	848.4	816.5	–	-2.3	-0.2	-1.5	-1.4	1.4	-3.7	12.9	29	-13.4	8	90	87	92	90	0.8	1.2	0.8	0.9	7.5	7.6	6.2	7.1
V	835.4	843.9	825.3	–	-0.7	1.5	0.3	0.4	3.6	-2.1	13.5	16	-9.5	5	92	87	91	90	0.5	1.2	0.7	0.8	7.1	8.0	6.4	7.4
VI	840.2	851.9	828.6	–	7.7	9.9	8.6	8.7	12.5	5.8	19.9	30	-1.4	6	85	80	83	83	1.9	3.0	2.1	2.3	6.3	7.0	5.9	6.4
VII	837.6	846.8	827.2	–	9.2	10.2	9.7	9.7	12.5	7.3	23.2	5	2.2	28	88	88	88	88	2.0	2.2	1.9	2.0	7.4	8.4	7.4	7.7
VIII	837.7	847.3	828.0	–	5.4	6.9	6.2	6.2	9.0	4.2	15.1	13	0.1	23	93	94	92	93	0.7	0.7	0.9	0.8	7.3	8.7	7.6	7.9
IX	834.8	845.8	821.5	–	2.6	3.6	2.8	3.0	5.5	0.7	19.8	9	-5.7	27	93	97	98	96	0.7	0.4	0.2	0.4	8.6	8.8	8.7	8.7
X	838.1	847.4	824.6	–	2.2	3.6	2.9	2.9	5.7	0.1	12.6	7	-5.1	1	87	80	82	83	1.2	2.0	1.8	1.7	5.7	5.6	5.6	5.6
XI	836.0	846.2	825.8	–	-1.7	-1.0	-1.6	-1.5	1.6	-4.0	7.9	6	-20.3	30	86	82	86	84	1.0	1.2	0.8	1.0	6.7	7.0	6.9	6.9
XII	830.2	847.2	804.6	–	-5.4	-4.7	-5.1	-5.1	-2.1	-8.2	4.3	13	-16.2	16	82	86	84	84	0.9	0.7	0.7	0.8	6.9	6.8	6.1	6.6
Rok	835.3	851.9	801.6	–	0.4	1.7	0.9	1.0	3.8	-1.6	23.2	5.VII	-20.3	30.XI	87	86	88	87	1.0	1.3	1.0	1.1	7.1	7.7	6.9	7.2

Zamość

$\varphi = 50°44'$ $\lambda = 23°15'$

I	994.9	1005.5	980.0	1022.7	-2.8	-0.6	-1.5	-1.6	0.2	-4.4	4.5	9	-14.6	17	–	–	–	–	–	–	–	–	8.5	7.9	8.0	8.1
II	988.5	1003.4	965.7	1013.6	0.8	4.2	1.9	2.2	5.4	-0.5	10.5	15	-5.8	28	–	–	–	–	–	–	–	–	7.5	7.4	4.4	6.4
III	992.9	1007.7	970.6	1020.3	-1.3	5.2	1.2	1.6	6.3	-3.2	16.6	31	-13.3	4	–	–	–	–	–	–	–	–	5.7	5.6	3.7	5.0
IV	994.6	1003.0	968.0	1018.2	5.2	13.4	7.9	8.6	14.6	2.6	26.7	30	-4.2	10	85	50	76	70	1.6	9.3	2.9	4.6	5.0	5.4	4.8	5.0
V	989.1	998.4	976.5	1015.4	9.3	14.1	10.1	10.9	15.5	6.4	24.6	18	0.5	5	86	66	84	79	1.7	6.5	2.1	3.4	6.2	7.9	7.3	7.1
VI	994.2	1003.1	979.8	1016.9	16.1	23.2	17.3	18.5	24.8	11.1	32.2	11	5.1	7	79	52	77	69	3.9	14.2	4.7	7.6	3.5	4.1	3.0	3.5
VII	987.0	996.2	977.3	1012.6	16.9	23.1	17.6	18.6	24.9	13.8	34.6	5	9.1	4,30	87	62	85	78	2.7	12.2	3.3	6.1	5.7	5.5	5.7	5.6
VIII	989.0	997.8	977.6	1014.8	14.4	20.9	15.5	16.6	22.6	11.3	31.5	14	5.6	24	93	65	88	82	1.2	9.5	2.3	4.3	5.1	5.7	3.5	4.7
IX	987.8	997.8	975.0	1013.9	10.0	16.4	11.3	12.2	17.6	7.9	28.0	9	-1.1	27	94	66	90	83	0.7	6.8	1.4	3.0	6.9	6.9	6.1	6.6
X	994.9	1005.2	980.2	1021.6	4.7	12.9	6.7	7.8	13.8	2.9	20.8	19	-3.2	3	92	65	89	82	0.8	5.7	1.2	2.6	5.7	5.3	3.8	4.9
XI	994.9	1014.4	974.8	1022.1	1.9	5.8	2.8	3.3	6.8	0.2	17.5	1	-10.8	30	91	80	89	87	0.5	2.0	0.8	1.1	7.7	8.0	6.7	7.5
XII	989.5	1008.0	955.2	1017.2	-3.1	-0.2	-2.3	-2.0	0.7	-5.3	9.3	13	-14.8	16	89	81	88	86	0.5	1.1	0.6	0.7	7.0	7.5	5.7	6.7
Rok	990.6	1014.4	955.2	1017.3	6.0	11.5	7.4	8.1	12.8	3.6	34.6	5.VII	-14.6	17.1	–	–	–	–	–	–	–	–	6.2	6.4	5.2	5.9

Kochcice

$\varphi = 50°43'$ $\lambda = 18°41'$

I	–	–	–	–	-2.4	0.5	-1.6	-1.3	2.0	-4.0	7.5	6	-17.0	17	–	–	–	–	–	–	–	–	6.9	6.8	7.1	6.9
II	–	–	–	–	0.9	4.9	2.3	2.6	5.7	-0.2	9.9	21	-4.8	23	88	78	87	84	0.8	2.1	1.0	1.3	6.8	6.9	7.2	7.0
III	–	–	–	–	0.8	7.1	3.6	3.8	8.7	-0.7	14.9	14,26	-7.9	4	82	67	79	78	0.9	3.9	1.8	2.2	6.0	5.3	4.5	4.9
IV	–	–	–	–	5.5	11.8	7.2	7.9	13.1	2.2	27.1	30	-4.9	15	84	56	79	73	1.7	7.3	2.4	3.8	4.7	6.4	6.0	5.7
V	–	–	–	–	9.5	14.0	9.6	10.7	15.3	5.1	24.9	19	-1.2	7	–	–	–	–	–	–	–	–	4.5	6.6	4.6	5.2
VI	–	–	–	–	16.5	22.1	16.9	18.1	23.4	11.2	34.0	30	5.1	28	73	52	75	67	5.3	13.6	5.1	8.0	3.7	5.0	3.9	4.2
VII	–	–	–	–	17.7	22.2	17.6	18.8	23.8	14.0	34.4	8	10.5	30	81	66	83	77	4.4	11.1	4.0	6.5	3.5	5.9	3.7	6.0
VIII	–	–	–	–	14.7	19.7	15.1	16.2	21.2	11.1	27.9	11	6.9	31	86	63	85	78	2.6	8.9	2.7	4.7	6.3	6.7	4.2	5.4
IX	–	–	–	–	9.7	14.8	10.9	11.8	16.9	7.5	26.6	9	-1.2	27	91	70	89	83	1.1	5.7	1.5	2.8	6.0	6.9	7.3	6.7
X	–	–	–	–	6.8	12.8	8.1	9.0	13.9	4.7	19.9	19	0.3	2	98	68	87	82	0.9	5.1	1.5	2.5	5.6	5.3	3.7	5.5
XI	–	–	–	–	3.2	6.6	3.9	4.4	8.2	1.9	18.1	6	-8.8	30	92	78	89	86	0.7	2.7	1.0	1.5	7.3	6.4	5.9	6.5
XII	–	–	–	–	-2.3	0.2	-1.8	-1.4	–	-4.4	–	–	-14.9	17	88	86	88	87	0.6	0.9	0.6	0.7	6.8	6.9	6.3	6.7
Rok	–	–	–	–	6.7	11.4	7.6	8.3	–	4.0	34.4	8.VII	-17.0	17.1	–	–	–	–	–	–	–	–	5.8	6.2	5.7	5.9

Werbkowice

$H_s = 207\ m$ $h_w = 12\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °/0, °/mD																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max>25°	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	v ≥ 10	v ≥ 15						
I	25	58	5	5.9	5	6.2	8	5.3	14.5	3.3	16	6.1	34	7.0	6	7.8	2	5.9	14.0	5.6	5	26	11	3	·	14	3	·	5	·	6	·	1	20	·
II	15	7.7	1	2.0	2	2.0	13	4.2	15.5	4.4	19.5	4.1	20.5	4.8	6	5.7	5	4.2	36.6	6.2	2	17	1	·	·	13	1.1	·	1	·	12	·	2	14	·
III	8	5.0	6	4.2	10	5.0	10	8.6	6	4.8	10.5	5.0	21	6.9	13.5	6.2	8	5.7	16.7	7.1	15	24	6	2	·	7	3	·	8	·	2	·	10	6	·
IV	15	2.9	8	2.8	7.5	2.6	9.5	2.5	8	3.0	5	3.0	10	3.2	23	3.2	4	2.8	17.7	6.8	11	9	·	·	3	12	3	·	·	·	·	·	7	9	·
V	29.5	3.0	14.5	2.3	10.5	2.4	5	3.6	5	1.6	3	1.8	8	2.6	19.5	3.3	1	2.8	36.7	11.4	18	1	·	·	1	12	6	1	·	·	·	1	3	16	·
VI	16.5	3.2	0.5	3.0	1	2.0	5	2.0	2.0	3.0	8.5	2.9	23	2.6	15.5	3.3	·	2.9	32.2	14.1	4	·	·	·	12	5	3	1	·	·	·	4	8	·	·
VII	10	2.1	3	2.0	3.5	2.4	7.5	2.5	19.5	2.1	20.5	2.6	11.5	2.3	16.5	2.7	1	2.4	87.7	26.6	8	·	·	·	15	2.1	13	1	·	·	·	6	5	7	·
VIII	15	2.2	0.5	1.0	3.5	1.4	2.5	3.0	1.7	1.7	21.5	1.7	13.5	2.1	15.5	2.6	4	1.9	81.2	27.7	29	·	·	·	7	22	13	2	·	·	·	4	4	5	·
IX	11.5	2.1	1.5	7.3	0.5	4.0	5	2.1	1.4	2.3	22.5	2.6	2.1	3.9	12	2.3	2	2.7	42.0	9.9	12	2	·	·	2	1.7	10	·	·	·	·	·	1	5	·
X	9.5	1.4	1.5	1.7	2	2.2	9.5	1.9	12.5	2.4	1.9	2.2	18.5	2.4	14.5	2.0	6	2.0	10.9	3.6	20	12	·	·	·	6	4	·	·	·	4	·	10	6	·
XI	9.5	5.0	8	2.2	10	3.3	20.5	2.5	7	2.1	11	2.4	13	4.3	8	4.8	3	3.2	15.9	8.0	28	14	2	1	·	10	4	·	2	·	5	·	3	16	·
XII	9.5	2.7	3.5	2.6	4	2.5	6	2.4	1.1	3.0	30.5	2.7	20	2.8	6.5	3.8	2	2.7	30.5	7.1	14	29	12	8	·	11	9	·	·	·	·	·	5	14	·
Rok	13.8	3.6	5.0	3.1	5.9.5	3.0	10.4.5	3.4	15.0	2.8	18.7.5	3.1	21.4	3.7	15.6.5	4.0	3.8	3.3	422.1	27.7	29.VIII	134	32	14	40	150	82	5	16	·	29	15	57	118	·

Śnieżka

$H_s = 1603\ m$ $H_b = 1610\ m$

I	16	14.5	7.5	15.4	0.5	7.0	0.5	3.0	8	11.2	19	12.1	25	14.1	14.5	16.8	2	13.7	86.3	18.3	28	30	19	7	·	18	14	3	30	25	24	·	2	14	31
II	8	10.1	0.5	5.0	·	·	·	·	7	10.9	39.5	18.6	15.5	14.4	13.5	9.5	·	14.8	185.8	50.1	18	24	22	3	·	23	20	6	26	21	27	·	1	20	28
III	14	8.5	2.5	10.4	0.5	6.0	7.5	12.8	11	9.9	28	17.9	13.5	20.4	15	11.7	1	14.1	66.8	15.7	30	29	14	3	·	17	13	1	28	20	24	1	3	15	31
IV	31	9.2	12.5	7.0	6.5	7.2	4	10.4	7.5	11.8	14	10.0	1.5	8.3	12	11.6	1	9.3	120.7	53.3	7	23	12	4	·	17	15	4	22	14	27	·	2	12	30
V	29.5	8.7	21	9.4	4.5	5.2	3	5.7	6	6.8	14	6.4	5	4.8	10	10.0	·	8.1	82.8	19.0	24	20	8	·	·	18	11	4	24	9	24	3	·	14	10
VI	14.5	6.7	5.5	5.4	6	5.4	4	7.2	7	7.6	26.5	9.8	9.5	9.1	14	8.1	3	7.8	76.3	23.0	4	2	·	·	·	14	11	3	25	9	20	2	3	11	1
VII	31.5	9.1	3	5.0	1	4.0	1	4.0	5	7.0	19	8.5	15.5	10.1	17	9.8	·	8.9	116.2	89.0	11	·	·	·	·	27	21	10	25	14	30	10	1	17	·
VIII	17	9.2	1	5.0	0.5	2.0	1	3.5	8	10.9	32.5	13.1	15	10.4	16	8.9	2	10.5	73.9	13.5	24	·	·	·	·	21	16	2	26	11	29	5	·	18	·
IX	12	9.0	0.5	6.0	·	·	·		4.5	9.4	36.5	15.6	19	13.4	16.5	13.2	1	13.3	110.1	22.7	23	13	3	·	·	22	16	3	28	19	30	1	·	20	2
X	8.5	10.1	0.5	3.0	·	·	·		9	7.6	11.5	9.3	17	8.3	16.5	8.0	·	8.7	11.8	2.3	20	14	6	·	·	13	8	·	24	11	27	·	8	10	5
XI	16	15.5	8.5	11.2	4	9.1	7	8.8	17.5	12.9	21.5	12.7	25	20.6	13	14.2	·	13.1	104.4	15.6	25	24	9	3	·	17	13	6	28	21	27	·	3	15	2
XII	17	10.8	2.5	12.4	2	22.8	3.5	14.1	9.5	10.1	22	12.5	22.5	15.4	14	11.5	·	12.8	110.8	19.7	2,3	31	21	9	·	17	14	2	29	19	26	·	5	12	31
Rok	21.5	10.1	6.5.3	7.3	25.5	5.7	31.5	5.8	10.0	9.7	31.4	12.2	16.1.5	12.4	17.2	11.1	10	11.3	1445.9	89.0	11.VII	210	114	29	·	224	172	44	345	190	315	22	28	178	171

Uwaga. Prędkość wiatru wyznaczano za pomocą anemografu.

Zamość

$H_s = 217\ m$ $H_b = 218{,}6\ m$ $h_w = 14\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	17.5	4.3	5	26	10	2	·	14	5	·	–	–	1	·	3	21	24
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35.0	6.6	15	12	2	·	·	15	10	·	–	–	5	·	3	9	5
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	15.6	7.4	15	22	8	2	·	9	5	·	–	–	1	·	8	6	4
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	17.7	6.5	11	8	·	·	3	8	4	·	–	–	·	1	8	10	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20.8	24.7	6	·	·	·	·	13	10	4	–	–	3	2	4	14	·
VI	3.5	2.1	·	·	5.5	2.2	5.5	2.2	4	5.2	8.5	4.2	2.2	3.2	15	2.8	26	2.2	43.2	19.6	4	·	·	·	14	7	6	2	·	·	·	5	10	1	·
VII	4	1.5	1.5	1.7	4.5	3.4	6	2.1	4	2.9	24.5	3.5	12.5	3.3	14	2.1	22	2.2	79.9	19.0	23	·	·	·	16	17	15	3	·	·	·	10	7	7	·
VIII	2	1.0	·	·	6.5	2.2	3.5	2.4	7	2.4	20.5	2.3	3.2	2.2	8.5	2.1	13	1.9	93.7	32.0	16	·	·	·	7	15	12	3	·	·	3	7	4	3	·
IX	6	2.7	3.5	1.6	·	·	1.5	2.3	8.5	3.8	3.5	3.9	2.4	3.6	5.5	2.6	6	3.3	78.6	15.6	12	1	·	·	2	16	13	3	4	·	2	·	5	13	·
X	6	1.0	0.5	1.0	4.5	1.2	4.5	1.7	4.5	2.9	33.5	2.1	16.5	2.8	10	1.4	13	1.8	14.9	4.6	23	9	·	·	·	4	4	·	·	·	5	·	4	6	·
XI	2	7.2	1.2	2.2	1.4	2.1	2.2	1.9	4.5	2.0	10.5	4.7	9.5	4.7	4.5	8.8	11	2.8	21.4	9.8	28	12	2	1	·	9	7	·	2	·	5	·	3	17	2
XII	1.5	2.7	4.5	1.2	2	2.0	7	1.5	9.5	4.8	36	3.4	5.5	3.9	10.5	3.0	3	3.0	28.9	8.8	14	29	11	4	·	11	7	·	2	·	2	·	6	16	10
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	372.2	32.0	16.VIII	119	33	9	42	138	97	16	–	–	27	25	63	123	46

Kochcice

$H_s = 280\ m$ $h_w = 15\ m$

I	2	1.8	2	3.5	3	3.3	3.5	3.0	26.5	3.8	16	4.2	16	4.7	2	4.5	22	3.0	24.4	6.0	5	24	8	3	·	13	7	·	·	·	4	–	3	15	–
II	3	2.2	·	·	5	2.4	3.5	3.1	27.5	4.5	14	5.2	10.5	5.1	4.5	4.7	16	3.6	47.4	9.3	18	12	1	·	·	15	12	·	2	·	5	–	2	11	–
III	2.5	3.1	4	3.5	17.5	4.4	2	2.8	11	4.1	10.5	4.4	16.5	5.9	7	3.7	16	3.6	51.9	10.8	18	17	2	·	·	10	10	2	4	·	3	–	9	9	–
IV	14	2.5	3	2.5	4.5	2.6	4.5	3.2	7	3.1	2	3.2	18	3.6	17	3.3	20	2.4	30.3	10.4	30	10	·	·	1	12	6	1	·	·	4	–	7	10	–
V	14.5	3.6	11	4.4	9	3.1	4	2.8	4.5	2.9	1	4.0	14	5.2	11	4.0	24	2.9	41.2	30.5	20	3	·	·	·	7	5	1	·	·	·	–	5	8	–
VI	3.5	2.1	4.5	2.0	4.5	2.2	·	·	1.3	3.5	12	4.4	13	3.9	11.5	2.4	28	2.2	66.9	21.3	6	·	·	·	10	7	7	2	·	·	·	–	9	5	–
VII	1	2.0	·	·	6	2.0	4	2.0	4.5	2.7	8.5	3.6	2.6	3.5	7	2.6	36	1.9	17.5.2	54.2	16	·	·	·	15	17	15	5	·	·	2	–	5	12	–
VIII	2	2.5		·	·	·	3	2.5	16.5	2.5	14.5	3.4	13.5	2.9	10.5	2.5	34	1.8	66.9	16.0	10	·	·	·	2	12	12	2	·	·	2	–	3	4	–
IX	4.5	3.6	2.5	3.6	2	1.8	4	3.1	10.5	4.9	19.5	5.3	20	4.4	4	5.0	23	3.4	103.8	18.4	2	1	·	·	2	16	14	5	2	·	6	–	2	12	–
X	2	3.0	·	·	4	2.0	2.5	2.0	1.9	3.2	17	4.4	12.5	4.3	8	2.5	30	2.4	0.8	0.8	20	·	·	·	·	1	·	·	1	·	11	–	6	8	–
XI	2	5.0	7	4.0	13	1.7	4.5	1.7	12.5	4.6	7.5	5.9	13	7.5	2.5	6.2	28	3.1	37.9	13.4	28	9	2	·	·	8	7	1	2	·	12	–	6	13	–
XII	1	2.0	3.5	2.6	1	2.0	9	2.4	25.5	3.8	12.5	5.1	12	5.2	3.5	2.3	25	2.6	47.6	10.5	8	28	–	3	·	11	9	1	1	·	11	–	4	14	–
Rok	5.8	2.8	37.5	2.2	69.5	2.3	44.5	2.4	17.7	3.6	13.6	4.4	18.5	4.5	86.5	3.6	30.2	2.7	69.4.3	54.2	16.VII	104	–	6	30	129	104	20	12	·	60	–	61	121	–

Zdanów

$\varphi = 50°43'$ $\lambda = 21°33'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-3.4	-4.2	-2.1	-2.2	-0.1	-5.0	4.7	6,9	-16.4	17	90	88	91	90	0.5	0.7	0.4	0.5	9.2	8.4	9.2	8.9
II	–	–	–	–	0.2	3.4	4.2	4.5	4.7	-1.0	8.4	15	-6.2	28	91	84	92	89	0.6	1.3	0.6	0.8	8.0	7.1	7.0	7.4
III	–	–	–	–	-0.3	5.4	4.8	2.2	7.2	-2.0	16.7	30	-9.5	3	–	–	–	–	–	–	–	–	4.7	4.4	4.2	4.4
IV	–	–	–	–	5.3	12.3	7.7	8.2	14.1	2.8	26.6	30	-3.6	15	81	54	75	70	1.8	8.3	3.1	4.4	4.0	5.7	4.2	4.6
V	–	–	–	–	8.7	12.6	9.1	9.9	14.4	5.7	22.4	18	0.3	27	84	64	81	76	2.1	6.3	2.3	3.6	5.9	7.7	6.2	6.6
VI	–	–	–	–	16.0	21.9	15.8	17.4	23.7	10.9	30.7	12	4.1	7	79	55	80	71	4.0	12.4	3.5	6.6	3.9	4.6	4.2	4.2
VII	–	–	–	–	16.7	22.2	17.1	18.3	24.2	13.6	34.6	5	9.4	29	–	–	–	–	–	–	–	–	5.5	5.7	5.7	5.6
VIII	–	–	–	–	14.2	19.7	14.7	15.8	21.6	11.0	29.6	12	5.4	31	89	62	85	79	1.9	9.5	2.5	4.6	3.8	5.4	3.8	4.3
IX	–	–	–	–	9.6	15.4	11.2	11.8	16.9	7.5	26.5	9	-0.2	27	–	–	–	–	–	–	–	–	4.8	6.0	6.8	5.9
X	–	–	–	–	5.3	12.2	7.4	8.4	13.4	3.4	19.5	19	-2.6	3	94	65	89	83	0.5	5.2	1.1	2.3	5.6	5.5	4.5	5.2
XI	–	–	–	–	1.6	5.6	2.6	3.1	7.1	0.0	16.8	5	-10.2	30	91	81	89	87	0.5	2.1	0.7	1.1	7.4	6.5	6.2	6.7
XII	–	–	–	–	-3.6	-1.0	-2.6	-2.4	0.5	-5.8	7.0	13	-11.9	16	–	–	–	–	–	–	–	–	6.9	7.7	5.7	6.8
Rok	–	–	–	–	5.9	10.7	7.0	7.6	12.3	3.4	34.6	5.VII	-16.4	17.1	–	–	–	–	–	–	–	–	5.8	6.2	5.6	5.9

Sokołowsko

$\varphi = 50°41'$ $\lambda = 16°14'$

I	–	–	–	–	-4.4	-4.7	-3.1	-3.1	-0.4	-6.2	6.8	6	-21.3	17	–	–	–	–	–	–	–	–	8.1	9.4	7.1	8.2
II	–	–	–	–	-0.1	2.5	0.3	0.8	3.8	-1.9	9.9	3	-9.0	26	–	–	–	–	–	–	–	–	8.7	8.7	7.8	8.4
III	–	–	–	–	-0.3	5.7	4.6	2.2	7.2	-1.9	14.1	13	-11.5	3	–	–	–	–	–	–	–	–	6.6	6.6	5.0	6.1
IV	–	–	–	–	3.6	8.8	3.5	4.8	10.3	-0.4	21.9	29	-7.6	15	–	–	–	–	–	–	–	–	6.2	7.2	4.9	6.1
V	–	–	–	–	7.0	11.4	6.1	7.6	13.1	1.9	22.7	16	-5.5	7	–	–	–	–	–	–	–	–	5.4	7.6	5.3	6.1
VI	–	–	–	–	14.8	19.6	13.2	15.2	21.5	8.5	29.5	30	1.8	27	–	–	–	–	–	–	–	–	5.0	5.8	3.7	4.8
VII	–	–	–	–	15.6	19.3	14.9	16.2	21.0	11.8	32.0	5	6.9	18	–	–	–	–	–	–	–	–	6.6	7.3	6.3	6.7
VIII	–	–	–	–	12.2	16.5	12.0	13.2	18.2	8.3	24.8	11	2.3	23	–	–	–	–	–	–	–	–	6.7	7.5	5.5	6.6
IX	–	–	–	–	8.5	12.8	8.3	9.5	14.0	5.2	24.5	8	-3.2	27	–	–	–	–	–	–	–	–	7.7	7.8	5.6	7.0
X	–	–	–	–	5.0	9.8	6.3	6.8	11.2	2.8	17.5	9	-3.1	3	–	–	–	–	–	–	–	–	7.1	6.6	5.6	6.4
XI	–	–	–	–	2.5	4.6	3.4	3.5	5.7	1.1	14.0	5	-12.2	30	–	–	–	–	–	–	–	–	8.3	8.6	8.3	8.4
XII	–	–	–	–	-2.8	-1.2	-2.5	-2.2	0.3	-5.3	8.9	13	-17.8	17	–	–	–	–	–	–	–	–	8.9	8.5	7.6	8.3
Rok	–	–	–	–	5.1	9.0	5.3	6.2	10.5	2.0	32.0	5.VII	-21.3	17.1	–	–	–	–	–	–	–	–	7.1	7.6	6.1	6.9

Grodków

$\varphi = 50°41'$ $\lambda = 17°23'$

I	–	–	–	–	-1.5	1.4	-0.7	-0.4	2.8	-3.8	10.6	6	-15.4	17	89	87	87	88	0.6	1.0	0.8	0.8	8.3	7.8	7.4	7.8
II	–	–	–	–	1.5	6.1	3.0	3.4	7.2	-0.2	10.7	2,14	-9.5	27	91	79	91	87	0.6	2.1	0.8	1.2	7.8	7.8	7.0	7.5
III	–	–	–	–	2.0	7.9	4.6	4.8	10.2	0.4	15.9	13,20	-7.6	1	86	69	85	80	1.1	3.9	1.4	2.1	5.8	6.4	5.9	6.0
IV	–	–	–	–	5.2	11.7	7.4	7.9	13.3	2.6	25.3	30	-4.0	15	91	62	84	79	0.9	6.2	1.8	3.0	5.7	7.2	5.4	6.1
V	–	–	–	–	8.9	14.1	9.9	10.7	15.9	5.3	26.0	19	-0.8	7	85	58	82	75	1.8	7.4	2.4	3.9	5.8	6.9	6.2	6.3
VI	–	–	–	–	16.1	21.8	16.9	17.9	24.1	11.2	31.5	11	5.3	1	81	57	81	73	3.7	12.3	3.9	6.6	4.6	6.2	5.4	5.4
VII	–	–	–	–	17.2	21.7	17.7	18.6	23.9	14.2	36.2	5	10.5	19	85	66	87	79	3.4	10.3	2.9	5.5	6.7	7.3	7.1	7.0
VIII	–	–	–	–	14.5	19.6	15.3	16.2	21.5	11.1	29.0	11	5.0	23	86	65	86	79	2.4	8.2	2.5	4.4	5.7	6.7	6.3	5.9
IX	–	–	–	–	10.3	16.0	11.4	12.3	17.5	7.6	27.8	8	-0.4	26	88	63	86	79	1.6	7.2	2.0	3.6	6.3	7.3	6.2	6.6
X	–	–	–	–	5.5	14.0	7.9	8.8	15.1	3.2	21.7	19	-0.9	2	94	67	89	83	0.6	5.7	1.3	2.5	6.4	5.9	5.9	5.4
XI	–	–	–	–	3.5	7.7	4.8	5.2	8.9	1.6	18.8	5	-8.6	30	90	74	87	84	0.8	3.2	1.2	1.7	8.4	7.7	7.4	7.8
XII	–	–	–	–	-1.7	1.6	-0.4	-0.2	3.2	-4.0	11.1	13	-15.0	16	89	82	88	86	0.6	1.3	0.8	0.9	6.8	6.5	5.6	6.3
Rok	–	–	–	–	6.8	12.0	8.2	8.8	13.6	4.1	36.2	5.VII	-15.1	17.1	88	69	86	81	1.5	6.7	1.8	3.0	6.5	7.0	6.1	6.5

Sandomierz

$\varphi = 50°41'$ $\lambda = 21°45'$

I	997.3	1008.1	981.7	1022.9	-3.4	-1.0	-2.0	-2.1	0.0	-4.6	5.0	9	-14.3	17	94	87	94	92	0.3	0.7	0.3	0.4	8.2	8.7	7.6	8.2
II	988.4	1005.7	965.3	1013.4	0.5	3.9	1.8	2.0	5.4	-0.5	9.5	6	-6.2	28	94	83	90	89	0.4	1.6	0.8	0.9	7.4	7.8	6.1	7.1
III	994.8	1009.9	973.2	1019.8	-0.2	6.1	2.7	2.8	7.8	-1.5	17.2	30	-8.7	3	86	59	74	73	0.9	4.5	2.1	2.5	5.9	6.5	3.8	5.1
IV	993.6	1004.8	969.8	1018.1	5.5	13.2	8.7	9.0	14.5	3.8	26.5	30	-2.7	16	85	54	76	72	1.5	8.7	3.2	4.5	4.7	5.4	4.4	4.8
V	991.4	1000.8	979.8	1015.6	9.1	13.6	10.4	10.9	15.1	6.8	23.5	18	0.8	5	84	63	78	75	2.2	7.0	3.2	4.1	6.2	7.7	6.8	6.9
VI	993.2	1006.4	981.1	1016.9	16.3	22.9	17.9	18.8	24.5	12.4	32.5	12	5.7	7	79	52	74	68	3.9	14.2	5.5	7.9	3.9	4.2	3.6	3.9
VII	985.0	999.1	979.2	1012.5	16.8	23.0	18.4	19.2	24.7	14.5	35.4	5	9.9	29	81	54	74	70	3.9	14.3	5.9	8.0	6.1	6.0	6.6	6.2
VIII	991.2	1000.5	979.5	1014.9	14.2	20.3	16.4	16.9	22.2	12.0	30.3	12	6.4	31	86	59	77	74	2.3	10.7	4.4	5.8	4.5	5.6	4.6	4.9
IX	990.1	999.4	975.7	1014.2	10.0	16.2	12.3	12.7	17.5	8.6	27.0	9	0.6	27	90	60	81	77	1.2	7.8	2.8	3.9	6.0	6.3	6.7	6.3
X	996.9	1006.9	981.6	1021.4	4.8	12.8	8.5	8.6	13.8	4.2	20.5	19	-3.4	3	93	63	84	80	0.6	5.6	1.9	2.7	6.5	5.4	4.7	5.5
XI	996.9	1015.7	978.9	1021.9	2.0	5.9	3.2	3.6	7.2	0.9	17.4	4	-9.9	30	90	77	87	85	0.7	2.4	0.9	1.3	7.0	6.9	6.3	6.7
XII	991.7	1010.7	956.4	1017.1	-3.3	-0.4	-2.1	-2.0	0.9	-5.2	9.0	13	-11.3	16	90	82	86	86	0.5	1.1	0.6	0.8	6.8	7.5	5.8	6.7
Rok	992.9	1015.7	956.4	1021.5	6.0	11.6	8.0	8.4	12.8	4.3	35.4	5.VII	-14.3	17.1	88	68	81	78	1.5	6.6	2.6	3.6	6.1	6.4	5.6	6.0

Zdanów — H_s = 236 m — h_w = 16 m — 1957

MIESIĄC	ROZKŁAD WIATRU (°D, °mD)																	OPAD R			LICZBA DNI (n)																
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość																			
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	Wiatr v ≥ 10	v ≥ 15	≡	≈	◔	◕	⊞
I	3	4,3	5,5	6,6	4,5	5,0	7	5,1	5	4,4	36	3,8	19,5	5,5	7,5	5,5	8	4,3	19,5	6,2	6	28	13	6	·	8	6	·	2	·	2	·	·	26	20
II	8,5	5,8	4,5	3,3	2,5	4,8	5,5	5,4	24	4,0	22,5	3,9	10	6,6	3,5	4,0	3	4,1	33,5	7,0	21	17	2	·	·	13	9	·	3	·	4	·	1	15	9
III	11	5,0	7	4,2	11	7,1	8,5	10,9	12	5,5	9,5	7,5	14	7,0	7	5,0	13	5,7	86	4,4	15	21	4	·	·	5	3	·	9	6	1	·	10	6	5
IV	17,5	2,8	5,5	2,3	5,5	1,9	4	3,8	6	3,1	4	2,9	10,5	2,8	15	3,0	22	2,1	30,4	9,5	17	8	·	·	1	9	8	·	·	·	·	3	9	5	·
V	21,5	3,9	15,5	6,8	9	4,3	4	2,6	2,5	2,2	1,5	2,0	5,5	5,5	17,5	6,0	16	4,1	39,1	10,0	14	·	·	·	·	9	7	·	7	1	1	2	3	12	·
VI	10,5	3,8	6,5	1,8	4	2,2	8,5	2,7	7,5	2,9	5	4,0	17	3,6	13	4,1	18	2,7	64,2	20,6	22	·	·	·	11	9	9	3	3	·	1	6	8	1	·
VII	5,5	2,1	4,5	3,3	7	3,2	3,5	3,3	6	2,1	17	3,9	18	5,5	8,5	4,4	23	2,9	101,5	26,0	8	·	·	·	12	19	15	2	3	·	4	7,1	4	10	·
VIII	2,5	7,6	·	·	2	3,5	4	3,5	6,5	3,5	13	3,7	23,5	4,3	19,5	3,9	22	3,1	61,1	12,7	14	·	·	·	6	13	11	2	4	·	·	4	8	3	·
IX	6	3,6	·	·	3	2,0	1,5	3,0	10,5	3,6	21,5	5,7	22	7,4	9,5	4,9	16	4,5	33,7	9,3	29	2	·	·	1	13	10	·	6	3	3	·	3	7	·
X	2	1,0	2	1,0	4,5	3,2	4	2,4	13	2,3	16,5	3,9	13	4,4	8	3,2	30	2,2	14,5	7,3	22	2	·	·	·	4	3	·	1	·	7	·	3	7	·
XI	7	5,8	8	6,9	14,5	4,7	15,5	5,1	6	4,1	9	8,9	9	12,1	4	16,0	17	5,8	5,3	4,0	28	13	2	1	·	4	1	·	9	5	9	·	5	14	·
XII	9,5	6,3	2	3,7	3	1,7	7,5	3,1	1,5	4,2	22,5	6,8	8	8,1	8,5	6,9	17	4,7	19,1	8,5	14	29	12	5	·	10	4	·	10	3	8	·	3	12	8
Rok	104,5	4,2	61	3,3	67,5	3,6	73,5	4,2	114	3,5	178	4,8	170	6,0	121,5	5,8	205	3,8	430,5	26,0	8.VII	120	33	12	34	116	86	7	57	18	40	22,5	57	118	42

Sokołowsko — H_s = 570 m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35,3	8,3	6	29	15	7	·	14	10	·	–	–	6	·	·	18	31
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	63,3	14,3	18	20	·	·	·	17	11	1	–	–	6	·	1	21	16
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	73,6	12,3	15	18	2	1	·	14	14	1	–	–	5	1	6	13	12
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	40,7	14,0	7	17	·	·	·	14	7	1	–	–	4	·	5	10	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	30,7	13,3	5	12	·	·	·	10	7	1	–	–	·	2	1	9	2
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39,8	17,0	4	·	·	·	5	7	6	1	–	–	2	3	6	5	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	285,8	50,2	23	·	·	·	7	18	18	9	–	–	3	5	4	14	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	70,7	15,3	24	·	·	·	·	17	14	1	–	–	·	2	2	12	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	101,0	23,0	23	3	·	·	·	20	16	2	–	–	5	1	2	12	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	11,0	5,6	20	8	·	·	·	8	3	·	–	–	1	·	2	10	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	50,3	11,2	25	12	1	1	·	11	9	1	–	–	5	1	1	22	1
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52,3	8,8	3	28	16	3	·	16	11	·	–	–	5	·	1	22	31
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	854,5	50,2	23.VII	147	34	12	12	166	126	18	–	–	42	15	31	168	94

Grodków — H_s = 176 m — h_w = 13,5 m

I	4,5	4,1	5	5,6	2	1,8	12	1,8	13	2,9	34,5	3,4	10	4,6	8	3,1	4	3,2	18,9	4,3	6	24	6	5	·	9	7	·	2	·	5	·	·	16	13
II	2,5	2,4	2	2,0	8	3,4	12,5	2,2	14,6	2,4	23	2,3	8	4,3	6,5	2,2	7	2,4	30,2	6,0	18	14	1	·	·	12	10	·	·	·	3	·	1	14	3
III	3,5	2,6	12,5	3,1	14,5	4,3	12	3,0	12,5	3,7	13	4,0	6	6,0	15	3,4	4	3,5	34,5	6,1	29	15	·	·	·	8	7	·	4	·	4	2	4	10	3
IV	17,5	3,3	5	1,8	4,5	2,3	10	3,0	5,5	2,5	7,5	2,5	9,5	2,8	24,5	3,3	6	2,7	30,1	18,5	30	8	·	·	1	9	4	1	·	·	5	2	2	9	·
V	17	2,8	19	3,1	3,5	2,7	10,5	2,0	3	2,0	7	3,4	11,5	3,8	19,5	4,1	2	3,1	32,1	13,5	20	1	·	·	1	8	7	1	·	·	·	2	·	9	·
VI	10	2,3	9,5	2,7	6,5	2,0	16	2,1	10	2,4	10	2,8	11,5	3,0	11,5	2,8	5	2,4	72,2	29,5	24	·	·	·	11	8	6	2	·	·	3	5	2	5	·
VII	6	1,7	6	1,5	9,5	1,8	11	2,6	9	2,9	18	3,0	16	2,7	12,5	2,6	5	2,4	144,4	30,6	14	·	·	·	11	21	16	5	·	·	3	9	·	15	·
VIII	2,6	1,4	0,5	2,0	5	1,8	13,5	2,6	11	2,7	22	3,2	20,5	2,5	15	2,1	3	2,5	44,4	7,4	24	·	·	·	4	13	10	·	·	·	·	5	1	4	·
IX	1,5	2,0	1	1,0	7,5	1,4	14,5	1,9	16	3,4	28,5	3,5	12	4,0	6	2,2	3	2,9	49,1	8,8	23	1	·	·	2	17	12	·	·	·	1	1	·	7	·
X	0,5	6,0	·	·	5,5	1,6	9,5	1,7	28	1,9	23,5	3,1	10	3,4	9	3,7	7	2,4	4,5	4,2	20	5	·	·	·	4	1	·	1	·	13	·	4	4	·
XI	4	4,8	10,5	3,1	13	2,5	20	3,0	10	2,6	7	4,6	16,5	4,6	3	6,6	6	3,2	11,2	6,2	25	9	1	·	·	7	2	·	2	·	8	·	1	20	·
XII	4	1,9	5,5	2,4	3,5	2,3	8,5	2,6	16,5	2,5	24	5,1	13,5	3,8	14,5	3,2	5	3,4	22,5	4,3	14	26	5	2	·	10	8	·	2	·	4	·	1	11	9
Rok	73,5	2,9	76,5	2,4	83	2,3	150	2,4	149	2,7	218	3,4	146	3,7	144,5	3,3	65	2,8	494,1	30,6	14.VII	103	13	7	30	126	90	9	11	·	49	26	16	124	28

Sandomierz — H_s = 202 m — H_b = 200,3 m — h_w = 21 m

I	2	4,5	6	6,0	5	3,1	10,5	2,7	3,5	2,3	36,5	4,0	23,5	4,3	6	3,7	·	3,9	21,9	7,8	5	26	12	5	·	10	6	·	·	·	5	·	2	20	25
II	6	3,4	5	3,3	4,5	3,3	3,5	2,6	18	3,6	31	4,8	12,5	4,1	4,5	3,8	·	4,0	40,5	7,3	7	17	2	·	·	16	10	·	1	·	5	·	1	11	9
III	7	4,5	17	3,5	10	4,2	12,5	3,7	5,5	3,5	14,5	4,0	18	4,6	7,5	4,2	1	4,0	12,7	7,2	15	20	4	·	·	5	4	·	2	2	1	·	10	8	5
IV	22	3,4	13,5	2,7	9,5	1,9	6	2,4	10,5	2,1	11	3,0	3	2,3	14,5	2,8	·	2,8	48,2	14,5	7	6	·	·	2	9	7	2	·	·	·	3	9	8	·
V	16,5	4,0	27	4,2	6,5	3,2	3,5	3,0	5	2,1	7,5	2,7	6	3,9	21	3,6	·	3,7	48,8	17,7	10	·	·	·	·	9	7	2	·	·	·	1	4	14	·
VI	14,5	3,3	5,5	2,0	3,5	1,7	4,5	1,8	15	3,0	16,5	3,2	16,5	3,7	17	2,8	·	3,0	42,0	17,9	20	·	·	·	11	9	9	2	1	·	·	8	8	3	·
VII	10	2,3	9	1,8	3	2,8	5,5	2,4	2,5	2,2	25	3,6	18	3,8	14	2,5	6	2,8	111,8	21,5	11	·	·	·	13	18	14	4	1	·	1	8	6	13	·
VIII	5	3,0	1	1,0	3	2,7	6	2,2	5	2,3	24,5	3,0	24	3,2	15,5	3,0	9	2,6	68,5	12,3	14	·	·	·	7	17	11	1	1	1	3	4	5	5	·
IX	6	2,3	2	1,0	3,5	1,9	3,5	1,8	6,5	2,6	32	4,2	24,5	5,5	9	2,7	3	3,7	48,8	18,2	25	·	·	·	2	13	11	1	4	1	2	·	3	8	·
X	3	1,7	1	1,0	1	3,0	9,5	2,4	8,5	2,2	36,5	2,6	20	3,3	10,5	2,8	3	2,6	18,0	7,9	23	2	·	·	·	3	3	·	·	·	11	·	2	8	·
XI	4	2,8	8,5	3,8	11	4,1	24,5	3,2	12,5	2,0	13	4,0	11	5,8	3,5	6,7	2	3,9	6,2	5,3	28	10	2	·	·	6	1	·	·	·	6	·	5	14	1
XII	9,5	3,9	5	3,7	7	2,4	4,5	2,8	9,5	2,7	41,5	4,0	9,5	4,1	5,5	5,0	1	3,7	20,7	10,7	14	20	11	2	·	7	4	1	1	·	6	·	4	13	12
Rok	102,8	3,7	100,5	2,8	64,8	2,9	96	2,6	102	2,6	289,5	3,6	186,5	4,0	128,5	3,6	25	3,4	493,1	21,5	14.VII	109	31	7	35	122	87	13	11	4	40	24	69	126	52

Opole

$\varphi = 50°48'$ $\lambda = 17°58'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1000.1	1011.4	982.8	1023.0	-2.0	0.9	-1.2	-0.9	2.1	-4.1	9.7	6	-17.6	17	93	86	93	91	0.4	1.0	0.4	0.6	7.4	7.6	6.1	7.0
II	990.1	1011.0	964.6	1012.6	1.1	5.3	2.4	2.8	6.4	-0.3	10.4	8.	-7.0	28	95	80	94	90	0.3	1.9	0.5	0.9	6.7	7.5	6.5	6.9
III	996.7	1013.3	977.3	1019.1	0.9	3.1	4.2	4.4	9.8	-0.4	16.5	20	-8.4	1	90	64	82	79	0.7	4.2	1.8	2.2	6.0	6.4	4.9	5.8
IV	996.6	1009.4	974.4	1018.7	4.6	12.2	7.5	8.0	13.7	2.2	25.8	30	-5.0	15	91	61	82	78	0.8	6.7	2.0	3.2	5.6	7.0	5.3	6.0
V	994.5	1003.7	985.1	1016.3	8.8	14.9	10.2	11.0	16.1	5.2	25.6	16,19	-0.7	7	86	60	82	76	1.7	7.5	2.5	3.9	6.1	6.9	5.3	6.1
VI	995.5	1010.4	984.0	1015.8	16.4	23.0	17.5	18.6	–	11.2	–	–	4.1	1	79	56	77	71	4.1	13.7	5.0	7.6	5.1	5.6	4.4	5.0
VII	994.6	1004.1	980.7	1012.8	17.1	22.6	18.0	18.9	–	14.2	–	–	9.5	19	88	68	87	81	2.7	10.7	3.2	5.5	7.0	7.0	6.6	6.9
VIII	994.0	1004.7	980.6	1014.4	14.0	20.3	15.5	16.3	–	11.3	–	–	6.5	24	91	67	86	81	1.5	8.1	2.5	4.0	5.5	6.5	5.1	5.7
IX	992.8	1002.0	977.5	1014.4	9.9	16.1	11.6	12.3	–	7.9	–	–	-0.3	26	94	71	88	84	0.8	6.0	1.6	2.8	6.6	7.5	5.4	6.5
X	998.8	1007.1	982.5	1020.8	5.6	13.5	8.4	9.0	–	4.2	–	–	-0.8	2	96	72	92	87	0.4	4.7	0.9	2.0	6.0	6.0	3.4	5.0
XI	998.8	1016.6	983.5	1021.2	3.7	7.4	4.6	5.1	–	2.3	–	–	-8.8	30	93	77	90	87	0.6	2.8	0.9	1.4	6.8	7.1	7.2	7.0
XII	993.8	1013.4	959.8	1016.6	-1.9	1.3	-1.0	-0.5	–	-4.0	–	–	-14.5	17	92	88	90	90	0.5	0.9	0.6	0.7	7.0	6.9	6.0	6.6
Rok	995.3	1016.6	960.2	1017.3	6.5	12.1	8.1	8.7	–	4.1	–	–	-17.6	17.1	91	71	87	83	1.2	5.7	1.8	2.9	6.3	6.8	5.5	6.2

Przewodziszowice

$\varphi = 50°39'$ $\lambda = 19°23'$

I	–	–	–	–	-3.1	-0.6	-2.1	-2.0	0.4	–	5.7	6	–	–	–	–	–	–	–	–	–	–	8.1	7.6	7.9	7.9
II	–	–	–	–	0.3	4.0	1.6	1.9	5.0	–	9.2	6	–	–	–	–	–	–	–	–	–	–	7.9	6.4	7.8	7.4
III	–	–	–	–	0.1	5.3	2.3	2.6	7.7	–	15.7	14	–	–	–	–	–	–	–	–	–	–	5.7	4.3	5.2	5.1
IV	–	–	–	–	6.0	11.2	6.7	7.5	12.2	–	24.5	29	–	–	–	–	–	–	–	–	–	–	5.5	5.5	4.9	5.3
V	–	–	–	–	8.4	12.8	8.6	9.6	14.4	–	22.7	19	–	–	–	–	–	–	–	–	–	–	5.6	6.5	5.6	5.9
VI	–	–	–	–	16.4	21.6	15.3	17.2	23.8		32.2	30	–	–	–	–	–	–	–	–	–	–	3.4	4.0	4.0	3.8
VII	–	–	–	–	16.9	21.7	16.4	17.8	23.6	–	34.9	8	–	–	–	–	–	–	–	–	–	–	6.2	6.1	5.6	6.0
VIII	–	–	–	–	14.1	18.8	13.9	15.2	20.9	–	29.9	12	–	–	–	–	–	–	–	–	–	–	5.9	5.7	4.2	5.3
IX	–	–	–	–	9.9	14.8	10.3	11.3	15.9	–	26.9	9	–	–	–	–	–	–	–	–	–	–	6.3	6.7	5.6	6.2
X	–	–	–	–	6.4	12.5	7.8	8.6	13.5	–	20.1	19	–	–	–	–	–	–	–	–	–	–	5.9	5.5	4.0	5.1
XI	–	–	–	–	2.7	6.0	3.1	3.7	7.0	–	17.7	5	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.5	6.7
XII	–	–	–	–	-2.8	-0.6	-2.0	-1.8	0.8	–	9.9	13	–	–	–	–	–	–	–	–	–	–	7.9	7.3	7.3	7.5
Rok	–	–	–	–	6.5	10.7	6.8	7.6	12.1	–	34.9	8.VII	–	–	–	–	–	–	–	–	–	–	6.3	6.0	5.7	6.0

Skroniów

$\varphi = 50°38'$ $\lambda = 20°16'$

I	–	–	–	–	-3.0	-0.3	-2.6	-2.1	0.6	-5.5	6.2	6	-19.0	17	94	86	94	91	0.3	0.9	0.3	0.5	8.7	8.4	7.6	8.2
II	–	–	–	–	0.4	4.5	1.8	2.2	5.7	-0.6	10.5	6	-5.6	24	94	79	91	88	0.4	2.0	0.7	1.0	8.2	7.7	7.8	7.9
III	–	–	–	–	-0.1	6.5	2.3	2.7	8.0	-2.0	16.6	28	-9.8	4	89	62	85	78	0.7	4.5	1.4	2.2	6.0	5.9	5.3	5.7
IV	–	–	–	–	4.9	12.5	6.9	7.8	13.9	2.2	26.4	30	-4.5	16	89	55	80	75	1.0	7.9	2.0	3.6	6.5	7.1	6.3	6.6
V	–	–	–	–	8.5	13.7	8.7	9.9	15.1	4.6	23.7	20	-1.2	7	82	58	82	74	2.2	7.6	2.2	4.1	6.3	8.2	6.8	7.1
VI	–	–	–	–	16.2	20.6	15.0	17.7	24.0	10.4	31.8	30	3.9	1	76	51	79	69	4.5	14.3	3.9	7.6	4.2	5.9	4.8	5.0
VII	–	–	–	–	17.2	22.3	16.9	18.5	23.7	13.5	34.7	5	9.1	29	84	61	87	77	3.6	12.0	2.8	6.1	6.2	7.2	7.4	6.9
VIII	–	–	–	–	13.9	20.1	14.5	15.8	21.6	10.7	29.1	12	6.3	31	91	62	88	80	1.5	9.8	2.0	4.4	5.6	6.8	4.3	5.6
IX	–	–	–	–	9.5	15.8	11.4	12.0	16.9	7.3	27.7	9	0.0	27	94	63	86	81	0.8	7.2	2.0	3.3	6.2	7.0	7.4	6.9
X	–	–	–	–	5.4	12.9	7.7	8.4	13.7	3.7	20.9	19	-2.5	3	94	66	89	83	0.6	5.4	1.1	2.4	7.1	6.4	4.9	6.1
XI	–	–	–	–	1.7	5.6	2.7	3.2	6.3	0.1	17.2	1	-9.9	30	94	81	94	90	0.3	2.0	0.5	0.9	8.4	7.3	7.3	7.7
XII	–	–	–	–	-2.8	-0.1	-1.8	-1.6	0.9	-5.1	6.6	14	-11.8	16,24	91	83	91	88	0.5	1.1	0.5	0.7	7.2	7.6	7.2	7.3
Rok	–	–	–	–	6.0	11.4	7.0	7.8	12.6	3.3	34.7	5.VII	-19.0	17.1	89	67	87	81	1.4	6.2	1.6	3.1	6.7	7.1	6.4	6.7

Chmielnik

$\varphi = 50°37'$ $\lambda = 20°46'$

I	–	–	–	–	-3.3	0.0	-2.3	-2.0	0.7	-5.3	6.1	6	-16.3	17	–	–	–	–	–	–	–	–	9.2	8.9	7.0	8.4
II	–	–	–	–	1.2	4.3	1.8	2.3	5.4	-0.8	10.0	6	-4.9	28	–	–	–	–	–	–	–	–	9.0	8.9	7.6	8.5
III	–	–	–	–	0.3	6.5	2.2	2.8	8.0	-1.7	16.6	28,30	-7.9	4	–	–	–	–	–	–	–	–	6.5	6.5	6.0	6.0
IV	–	–	–	–	5.4	13.0	7.3	8.2	14.4	2.7	25.2	25	-4.5	16	–	–	–	–	–	–	–	–	6.4	5.9	5.8	6.0
V	–	–	–	–	9.3	13.9	9.1	10.4	15.4	5.5	24.3	20	0.3	4	–	–	–	–	–	–	–	–	6.0	7.0	7.0	6.7
VI	–	–	–	–	16.6	23.0	16.4	18.1	24.7	10.6	34.4	30	4.6	7	–	–	–	–	–	–	–	–	4.5	5.8	5.5	5.3
VII	–	–	–	–	17.7	23.0	17.7	19.0	25.0	13.4	35.8	5	8.1	29	–	–	–	–	–	–	–	–	6.9	6.5	6.8	6.7
VIII	–	–	–	–	14.4	20.6	15.3	16.4	22.3	10.6	31.0	12	5.1	24,31	–	–	–	–	–	–	–	–	5.2	6.2	4.9	5.4
IX	–	–	–	–	9.6	16.2	11.4	12.2	17.5	7.3	27.6	9	0.1	26,27	–	–	–	–	–	–	–	–	6.8	6.9	7.2	6.6
X	–	–	–	–	5.3	13.2	7.1	8.2	14.0	2.8	24.2	19	-3.5	3	–	–	–	–	–	–	–	–	7.7	6.4	5.6	6.6
XI	–	–	–	–	2.1	6.3	2.9	3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.6	7.9	9.0	8.8
XII	–	–	–	–	-3.3	0.2	-2.1	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	7.8	7.3
Rok	–	–	–	–	6.3	11.7	7.2	8.1	–	–	35.8	5.VII	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.6	6.9

Opole

$H_s = 176$ m $H_b = 180{,}7$ m $h_w = 13$ m **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, ▼mD]																	OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C					Temperatura T				Opad R			Wiatr ▼									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	Średnia prędkość	Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max>25°	0,1 ≤ R < 1,0	1,0 ≤ R < 10,0	R ≥ 10,0	10 ≤ ▼ < 15	▼ ≥ 15	≡	≤ 10%	◔	●	⊠
I	2,5	2,4	3,5	6,7	1	4,0	·	·	17	2,4	33,5	4,7	17	3,1	7,5	5,5	11	2,4	30,3	8,3	6	25	9	6	·	11	7	·	–	–	4	·	2	14	15
II	2	4,2	2,5	2,0	1	3,0	2,5	2,2	2,5	2,9	30,5	2,7	12,5	3,5	6	3,2	4	2,7	43,2	7,7	18	12	1	·	·	15	10	·	–	–	1	·	1	12	3
III	2	3,2	2,5	3,8	6,5	5,2	9,5	4,4	18,5	3,3	22	2,8	19	3,0	7	3,3	6	3,2	35,7	7,0	17	16	1	·	·	10	9	·	–	–	1	·	7	9	4
IV	8	2,8	2	3,5	0,5	2,0	1,5	3,0	6,5	2,8	17	1,9	23,5	1,9	18	2,5	13	1,9	35,5	13,5	30	11	·	·	1	10	7	1	–	–	1	1	2	8	·
V	6	2,0	1,5	4,9	4,5	6,0	1,5	5,3	8	1,8	10	1,7	23,5	2,8	14,5	4,3	10	3,0	34,3	13,7	20	1	·	·	2	6	5	2	–	–	·	3	1	8	·
VI	2	2,8	5,5	2,1	2,5	2,0	0,5	5,0	12,5	1,9	25,5	2,4	23,5	2,9	9	3,7	9	2,3	86,2	41,8	24	·	–	·	–	11	7	3	–	–	1	9	5	5	·
VII	3,5	2,6	2	1,7	1	3,0	1	6,0	10,5	1,5	24,5	2,4	31	2,8	11,5	3,2	8	2,3	141,9	53,1	16	·	–	·	–	19	14	3	–	–	2	7	1	13	·
VIII	·	·			·	·	2,5	1,2	6	3,0	27,5	2,5	34,5	2,8	11,5	4,8	11	2,6	42,6	7,2	10	·	–	·	–	11	9	·	–	–	1	4	2	4	·
IX	·	·	·	·	·	·	·	·	14,5	2,3	46,5	2,6	19,5	3,3	7,5	4,5	2	2,8	92,6	43,9	14	1	–	·	–	4,5	15	4	–	–	4	2	3	8	·
X	·	·					0,5	8,0	2,3	2,1	39,5	1,8	21	2,0	4	1,6	5	1,8	34	8,4	20	2	–	·	–	2	2	·	–	–	12	·	5	4	·
XI	3,5	7,0	3,5	3,7	7	4,0	1,1	1,9	28,5	2,5	13,5	1,8	12,5	4,5	5,5	5,4	5	3,0	29,9	9,9	25	9	–	·	–	7	5	·	–	–	5	·	5	15	·
XII	2,5	2,4	3	1,7	3	3,0	2,5	1,6	17,5	2,1	32,5	2,8	18	2,8	9	2,1	5	2,4	29,2	6,0	8	23	–	3	–	11	8	·	–	–	7	·	1	12	3
Rok	3,2	2,2	3,7,5	2,5	2,7	2,7	3,3	3,2	137,5	2,4	322,5	2,3	256,5	2,9	111	3,7	89	2,5	604,8	59,1	16.VII	100	–	9	–	128	98	13	–	–	39	26	35	112	25

Przewodziszowice

$H_s = 380$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26,2	6,2	6	–	10	–	·	21	6	·	–	–	–	·	3	21	27
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44,5	5,1	18	–	2	–	·	21	13	·	–	–	–	·	·	9	8
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51,3	15,9	18	–	3	–	·	11	7	1	–	–	–	·	10	9	5
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36,9	13,4	7	–	·	–	·	17	6	1	–	–	–	3	7	9	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29,9	11,9	13	–	·	–	·	8	5	1	–	–	–	1	2	7	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	58,3	15,0	7	–	·	–	12	8	8	3	–	–	–	6	7	3	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	195,8	70,6	16	–	·	–	12	16	13	4	–	–	–	3	4	13	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	120,7	40,4	14	–	·	–	5	14	12	3	–	–	–	3	2	4	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	98,1	15,5	23	–	·	–	2	17	13	4	–	–	–	1	2	10	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6,2	2,6	22	–	·	–	·	6	2	·	–	–	–	·	8	7	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	30,3	10,2	28	–	2	–	·	10	6	1	–	–	–	·	6	19	1
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41,3	9,8	14	–	12	–	·	13	10	·	–	–	–	·	2	16	27
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	739,5	70,6	16.VII	–	29	–	31	162	101	18	–	–	–	17	53	127	68

Skroniów

$H_s = 256$ m $h_w =$ I–VII 11 m, VIII–XII 16 m

I	1,5	3,0	5,5	5,2	6,5	2,8	2	2,5	2	2,0	19	3,6	28	6,4	12,5	5,2	16	4,0	24,7	6,2	6	24	10	6	·	12	7	·	1	1	3	·	1	20	–
II	3,5	2,0	2	3,0	5	3,0	9	3,6	11	3,9	13,5	3,8	19,5	5,5	10,5	4,2	10	3,6	18,0	3,5	22	14	2	·	·	15	7	·	1	·	3	·	1	15	–
III	4,5	3,8	7	2,0	2,1	5,7	4	6,1	4,5	3,0	6	5,5	15	6,5	14	5,9	17	4,4	24,1	9,3	15	20	3	·	·	9	5	·	8	1	1	·	6	10	–
IV	1,2	3,8	4	3,5	9	2,4	4	2,2	4	2,6	4,5	4,0	9	3,0	19,5	4,5	24	2,6	42,8	13,9	7	9	·	·	2	12	9	1	·	·	3	2	4	14	–
V	1,3	2,8	1,5	4,5	7,5	4,2	3	2,2	1,6	2,7	25	3,8	6,5	5,9	22	4,8	2,2	3,2	28,1	12,1	10	1	·	·	·	5	5	2	·	·	·	1	·	13	–
VI	8	1,9	6,5	2,1	6	1,9	9	2,4	2	3,0	6	3,2	21	4,9	13,5	3,6	18	2,7	43,1	21,7	7	·	·	·	13	7	6	1	1	1	·	5	5	4	–
VII	5	2,8	2	2,0	9	3,7	4	2,8	3	2,5	9	4,3	25	5,0	19	3,9	17	3,3	197,4	63,5	16	·	·	·	13	17	12	7	3	1	·	6	3	16	–
VIII	3,5	3,7	·	·	4,5	2,8	1,5	3,0	2,5	4,2	8,5	3,4	27,5	4,1	17	4,6	2,8	2,8	91,4	27,8	13	·	·	·	6	16	13	2	2	2	·	3	2	3	–
IX	·	·	2	3,5	2,5	1,8	2,5	2,6	4,5	2,4	20,5	5,6	25,5	5,5	13,5	6,3	1,9	4,1	41,3	8,3	19	·	·	·	2	13	11	·	3	1	4	2	1	11	–
X	0,5	2,0	·	·	3,5	2,0	8,5	2,8	5	2,4	9,5	3,9	19,5	3,4	12,5	4,0	3,4	2,4	8,8	4,2	22	1	·	·	·	5	3	·	·	·	7	·	2	9	–
XI	1,5	7,7	3,5	5,6	3,5,5	3,1	6	3,0	1	3,0	1,5	2,3	18,5	6,5	3,5	8,1	1,9	3,5	12,9	7,1	28	12	3	·	·	7	3	·	1	1	8	·	3	19	–
XII	3,5	3,9	3,5	4,1	9,5	3,0	7,5	2,9	2	2,5	15	6,1	16,5	4,4	13,5	4,7	2,2	3,4	24,3	7,8	14	28	11	6	·	11	6	·	2	·	·	·	1	13	–
Rok	5,6,5	3,1	51	3,0	119,5	3,0	61	3,0	43	3,0	113,5	4,1	234,5	5,1	171	5,0	246	3,3	556,9	63,5	16.VII	109	29	12	36	129	87	13	22	8	29	19	89	146	–

Chmielnik

$H_s = 255$ m $h_w = 15{,}5$ m

I	3	2,6	5,5	4,4	14,5	2,2	6	2,1	9,5	2,8	13	4,2	36,5	4,7	6	3,7	·	3,8	25,9	7,3	5	27	9	6	·	13	6	·	1	·	–	·	·	20	13
II	6,5	2,1	3	2,0	9,5	3,3	8	2,8	15	3,0	8,5	3,0	26	3,7	7,5	2,5	1	3,1	36,4	7,3	8	17	2	·	·	16	11	·	·	·	–	·	·	18	1
III	8	3,0	2,5	1,9	2,9	3,9	2,5	1,8	4	3,1	4	5,2	31,5	4,6	5,5	2,6	·	3,2	21,8	5,6	15	20	3	·	·	9	6	·	3	·	–	·	3	10	·
IV	9	2,0	4,5	1,8	17	2,2	3,5	2,1	7,5	2,0	4	4,0	24,5	2,7	2,0	2,8	·	2,5	52,3	14,0	30	7	·	·	2	17	8	2	·	·	–	1	2	8	·
V	1,5	3,4	1,0	3,0	1,7	1,9	4,5	2,3	0,5	1,0	2,5	3,6	2,4	3,5	1,8,5	2,4	1	2,8	56,8	17,0	20	·	·	·	·	10	9	2	1	·	–	2	1	10	·
VI	8	2,2	1	1,0	1,1	2,8	4	2,0	5	2,8	1,1	3,5	3,1,5	2,8	16,5	2,9	2	2,7	39,8	12,8	22	·	·	·	13	9	6	1	·	·	–	7	3	2	·
VII	2	1,5	1	3,0	1,0	3,0	6	2,4	9	2,1	18,5	2,5	36,5	3,8	9	1,7	2	2,9	99,9	23,7	8	·	·	·	16	20	15	3	1	·	–	5	1	13	·
VIII	1	1,0	·	·	4,5	5,3	2	3,0	5,5	2,4	4,5	2,1	34	2,9	16,5	2,7	5	2,7	107,5	26,3	14	·	·	·	7	13	12	2	·	·	–	2	·	4	·
IX	4,5	4,0	·	·	·	·	·	·	1,1	2,7	2,1	3,8	4,7	5,0	9,5	1,7	·	4,0	47,8	10,2	29	·	·	·	2	17	10	1	3	·	–	·	1	6	·
X	2	2,5	2	3,0	5,5	3,7	9,5	1,9	8	1,6	1,9,5	2,5	3,7,5	2,9	6	2,8	3	2,6	1,6,9	6,1	20	4	·	·	·	12	3	·	2	·	–	·	2	10	·
XI	3	1,8,7	6,5	3,7	1,7	1,7	3,0,5	3,3	1,1	1,8	2	6,5	1,4,5	3,4	2,5	1,1,8	·	1,8	2,2,6	2,9	2,8	–	–	–	·	1,4	5	·	3	1	–	·	·	2,1	·
XII	2,5	3,6	4	3,5	·	·	6	1,8	6,5	2,9	3	7,3	2,9	5,4	3	5,1	2,9	3,5	2,8,2	1,1,7	3	–	–	–	·	7	6	1	5	2	–	·	1	12	·
Rok	6,0,5	3,2	4,6	2,5	1,3,5	2,7	3,0,5	2,4	9,5,5	2,3	1,1,6,5	4,0	3,9,2,5	4,2	1,2,5,5	3,6	4,3	3,3	5,5,6,7	2,6,5	1,4.VIII	–	–	–	40	1,6,7	9,7	1,2	2,4	3	–	1,7	1,4	1,3,4	1,4

Opolnica

$\varphi = 50°31'$ $\lambda = 16°44'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.4	0.3	-4.3	-4.2	1.5	-4.3	10.1	6	-20.5	17	85	79	84	83	0.8	1.4	1.0	1.1	6.5	6.5	5.2	6.1
II	–	–	–	–	1.9	5.1	2.6	3.0	6.2	-0.3	10.1	14	-10.2	27	86	75	84	82	1.1	2.1	1.3	1.5	7.1	7.0	6.0	6.7
III	–	–	–	–	4.2	6.9	3.5	3.8	8.9	-0.7	14.6	20	-9.5	3	86	66	83	78	1.1	3.9	1.6	2.2	6.5	5.9	3.9	5.4
IV	–	–	–	–	3.7	10.8	5.9	6.6	12.3	1.6	24.6	29	-4.9	15	91	62	84	79	0.7	6.1	1.6	2.8	5.1	7.2	4.6	6.6
V	–	–	–	–	7.7	13.8	8.3	9.5	15.3	4.0	25.1	16	-1.8	7	80	53	82	72	2.2	7.8	2.0	4.0	5.5	6.4	5.3	5.7
VI	–	–	–	–	13.2	21.3	16.9	17.0	23.6	10.1	31.0	11	4.4	1	–	–	–	–	–	–	–	–	4.3	4.4	4.0	4.2
VII	–	–	–	–	16.2	21.1	17.7	18.2	22.9	13.6	35.0	5	9.7	26	–	–	–	–	–	–	–	–	6.3	6.2	6.5	6.3
VIII	–	–	–	–	13.0	19.1	14.3	15.2	20.4	10.1	27.7	11	4.7	23	88	61	87	79	1.8	8.9	2.3	4.3	5.2	6.1	4.5	5.3
IX	–	–	–	–	10.1	15.2	10.6	11.6	16.4	7.5	25.6	8	-1.3	27	86	66	85	79	1.9	6.2	2.1	3.4	6.0	6.6	3.8	5.5
X	–	–	–	–	6.8	13.0	7.8	8.8	14.0	4.1	19.2	18,19	-0.3	1,2,3	86	66	85	79	1.5	5.4	1.9	2.9	5.5	4.7	2.2	4.1
XI	–	–	–	–	4.2	6.5	4.8	5.1	7.9	2.1	16.9	5	-8.4	30	84	75	83	81	1.4	2.8	1.6	1.9	7.2	8.0	7.3	7.5
XII	–	–	–	–	-1.0	1.0	-0.2	-0.1	2.4	-3.3	11.6	13	-12.2	16,17	85	78	85	83	0.9	1.6	1.0	1.2	6.5	7.0	6.6	6.7
Rok	–	–	–	–	6.2	11.2	7.6	8.2	12.6	3.7	35.0	5.VII	-20.5	17.1	–	–	–	–	–	–	–	–	6.0	6.3	5.0	5.8

Nisko

$\varphi = 50°31'$ $\lambda = 22°10'$

I	–	–	–	–	-2.9	0.0	-4.6	-4.5	0.8	-4.4	6.2	6,9	-15.7	17	–	–	–	–	–	–	–	–	7.7	8.1	8.0	7.9
II	–	–	–	–	1.4	5.0	2.3	2.8	6.2	-0.2	11.2	17	-6.1	28	–	–	–	–	–	–	–	–	7.5	7.2	6.0	6.9
III	–	–	–	–	-0.3	6.5	2.0	2.6	8.3	-2.4	20.0	30	-11.7	4	–	–	–	–	–	–	–	–	5.5	5.7	4.0	5.1
IV	–	–	–	–	5.5	14.1	8.1	9.0	15.3	2.5	26.8	30	-4.1	16	–	–	–	–	–	–	–	–	4.4	5.9	3.4	4.6
V	–	–	–	–	9.5	14.4	9.8	10.9	15.5	5.9	23.8	18	0.2	7	–	–	–	–	–	–	–	–	5.7	8.7	6.2	6.9
VI	–	–	–	–	17.3	24.1	17.5	19.1	25.3	11.0	32.9	12	3.5	28	–	–	–	–	–	–	–	–	4.1	5.2	2.9	4.1
VII	–	–	–	–	17.8	23.8	18.3	19.6	25.5	13.2	36.9	5	7.5	4	–	–	–	–	–	–	–	–	6.4	6.3	5.7	6.1
VIII	–	–	–	–	14.7	21.1	16.3	17.1	22.9	11.7	30.7	14	6.7	24	–	–	–	–	–	–	–	–	5.8	6.3	5.1	5.7
IX	–	–	–	–	10.8	17.1	12.0	13.0	18.2	8.3	28.5	9	-1.2	27	–	–	–	–	–	–	–	–	5.3	7.1	6.6	6.3
X	–	–	–	–	5.6	13.5	7.8	8.6	14.7	3.2	20.9	19	-5.3	3	–	–	–	–	–	–	–	–	5.3	5.3	4.5	5.0
XI	–	–	–	–	2.3	6.5	3.0	3.7	7.5	0.7	18.0	4	-9.8	30	–	–	–	–	–	–	–	–	8.2	6.8	6.9	7.3
XII	–	–	–	–	-2.4	0.5	-1.9	-1.4	1.9	-5.3	10.7	13	-11.3	3	–	–	–	–	–	–	–	–	7.5	7.1	5.3	6.6
Rok	–	–	–	–	6.6	12.2	7.8	8.6	13.5	3.7	36.9	5.VII	-15.7	17.1	–	–	–	–	–	–	–	–	6.1	6.6	5.4	6.0

Ławica, IUNiG

$\varphi = 50°28'$ $\lambda = 16°40'$

I	–	–	–	–	-3.7	-0.1	-2.4	-2.2	0.9	-6.2	9.6	6	-23.5	17	85	77	84	82	0.8	1.5	0.8	1.0	7.4	7.9	6.2	7.2
II	–	–	–	–	1.1	5.0	2.2	2.6	5.6	-0.7	10.3	14	-12.1	27	88	72	86	82	0.8	2.5	1.2	1.5	8.3	7.9	7.5	7.9
III	–	–	–	–	1.0	7.2	3.3	3.7	8.9	-0.9	15.5	15	-10.0	3,4	85	62	83	77	1.2	4.3	1.6	2.4	7.6	6.2	4.0	5.9
IV	–	–	–	–	3.1	11.0	5.5	6.3	12.4	0.8	24.9	29	-5.9	15	91	59	85	78	0.8	6.2	1.5	2.8	6.5	7.5	5.3	6.4
V	–	–	–	–	7.1	14.0	8.3	9.4	15.7	3.5	24.9	16	-3.2	7	82	50	80	71	1.8	8.6	2.3	4.2	5.7	7.4	5.7	6.3
VI	–	–	–	–	14.6	22.0	15.1	16.7	23.6	8.7	30.8	30	1.7	1	78	50	82	70	3.8	14.2	3.2	7.1	5.3	5.8	4.3	5.1
VII	–	–	–	–	16.4	21.6	16.8	17.8	23.1	13.1	35.0	5	8.4	19	86	66	87	80	2.8	10.4	2.7	5.3	7.1	6.6	7.3	7.0
VIII	–	–	–	–	12.4	18.7	13.9	14.7	20.6	9.3	28.2	11	3.1	23	90	64	87	80	1.4	8.3	2.1	3.9	6.0	7.7	5.6	6.4
IX	–	–	–	–	9.7	15.5	10.3	11.4	16.7	6.5	26.1	9	-2.8	27	88	65	87	80	1.6	6.6	1.8	3.3	8.3	7.7	5.9	7.3
X	–	–	–	–	6.0	12.9	6.8	8.1	14.0	3.2	19.7	19	-4.0	2	90	66	88	81	1.2	5.4	1.3	2.6	7.4	5.2	4.1	5.6
XI	–	–	–	–	3.2	6.4	4.7	4.8	7.7	1.8	16.4	5	-9.0	30	86	75	86	82	1.1	2.7	1.3	1.7	8.6	8.1	8.2	8.3
XII	–	–	–	–	-1.8	0.5	-0.8	-0.7	2.1	-3.8	11.2	13	-14.4	17	86	82	86	85	0.8	1.2	0.9	1.0	8.5	7.3	7.2	7.7
Rok	–	–	–	–	5.8	11.2	7.0	7.8	12.6	2.9	35.0	5.VII	-23.6	17.1	86	66	85	79	1.5	6.0	1.7	3.1	7.2	7.1	5.9	6.7

Otmuchów

$\varphi = 50°28'$ $\lambda = 17°10'$

I	–	–	–	–	-4.8	1.7	-1.3	-0.7	3.4	-4.8	10.4	6	-20.5	17	83	72	82	79	1.0	2.1	1.1	1.4	7.4	7.2	6.0	6.9
II	–	–	–	–	1.7	6.4	3.0	3.5	7.7	-0.2	13.7	3	-13.6	27	84	65	81	77	1.3	3.5	1.6	2.1	7.0	7.2	6.5	6.9
III	–	–	–	–	1.7	8.2	4.1	4.5	9.9	0.3	17.1	13	-8.0	4	83	60	79	74	1.5	5.0	2.0	2.8	6.8	6.5	5.1	6.1
IV	–	–	–	–	5.0	11.3	6.9	7.5	13.4	2.2	23.5	30	-4.6	15,19	84	59	80	74	1.5	6.7	2.0	3.4	6.4	7.3	5.7	6.5
V	–	–	–	–	9.0	14.4	9.7	10.7	16.0	4.8	25.1	19	-0.9	7,29	79	51	75	68	2.7	8.6	3.2	4.8	6.6	7.1	5.6	6.4
VI	–	–	–	–	16.1	22.7	16.4	17.5	24.7	10.2	32.0	11,30	3.0	1	74	48	78	67	4.9	15.4	4.4	8.2	8.5	5.7	4.3	5.2
VII	–	–	–	–	17.6	22.1	17.8	18.7	23.9	14.0	38.1	5	9.4	19	83	63	85	77	3.8	11.2	3.4	6.1	8.1	8.1	8.3	8.2
VIII	–	–	–	–	14.5	20.1	15.2	16.2	21.5	10.7	27.6	11	8.0	31	85	59	84	76	2.5	9.9	2.8	5.1	8.2	8.4	8.1	8.2
IX	–	–	–	–	10.7	16.4	11.0	12.3	17.6	7.6	28.1	8	0.3	27	86	62	83	77	2.0	7.9	2.3	4.1	6.6	6.8	6.2	6.5
X	–	–	–	–	6.2	14.6	7.6	9.0	18.6	3.2	22.2	19	-0.9	3	91	58	87	79	1.0	7.3	1.5	3.3	7.5	8.0	4.2	5.9
XI	–	–	–	–	3.5	7.8	5.0	5.3	8.7	2.1	20.1	5	-8.4	30	88	74	87	83	1.2	3.4	1.4	2.0	7.8	7.8	7.7	7.7
XII	–	–	–	–	-1.5	2.3	-0.1	0.2	3.7	-3.4	18.6	13	-14.6	16	87	74	86	82	0.9	2.1	0.9	1.3	7.0	6.7	5.6	6.4
Rok	–	–	–	–	6.9	12.3	7.9	8.8	13.8	3.9	36.1	5.VII	-20.5	17.1	84	62	82	76	2.0	6.9	2.2	3.7	6.7	6.7	5.8	6.4

Opalnica

$H_s = 282$ m $h_w = 11{,}8$ m **1957**

MIESIĄC	ROZKŁAD WIATRU (%, ‰) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min <0°	Max <0°	Min <-10°	Max >25°	Opad R 0.1	1.0	10.0	Wiatr v 10	15	—	25	●	●	⊠
I	1,5	1,0	3,5	4,9	2	2,0	·	·	·	·	28,5	2,4	31,5	2,3	·	·	26	1,6	11,8	3,2	15	20	9	6	·	11	4	·	·	·	–	–	5	8	–
II	2	1,5	1,5	1,0	0,5	1,0	·	·	1	1,0	18,5	2,3	34,5	1,9	·	·	26	1,4	38,1	9,2	25	13	·	1	·	12	7	·	·	·	–	–	1	11	–
III	2	1,0	8	2,2	7	1,3	1	1,0	·	·	16	2,2	46	2,1	·	·	43	1,0	49,5	10,4	30	17	1	·	·	12	10	1	1	1	–	–	6	10	–
IV	1	1,0	11	1,2	7	1,4	·	·	·	·	3,5	1,1	10,5	1,4	·	·	57	0,5	59,2	37,6	30	12	·	·	·	8	7	1	·	·	–	–	4	7	–
V	6	1,1	14	1,2	11	1,4	·	·	·	·	7,5	1,3	5	1,7	1,5	2,0	48	0,6	16,2	8,5	8	8	·	·	1	4	4	·	·	·	–	–	·	8	–
VI	2	1,0	6,5	1,2	11,5	1,0	·	·	·	·	14,5	2,1	11,5	1,3	·	·	44	0,8	47,6	26,8	24	·	·	·	10	7	6	1	·	·	–	–	9	6	–
VII	·	·	8,5	1,2	3,5	1,0	1	1,0	·	·	24,5	1,1	10	1,3	0,5	1,0	45	0,6	158,7	29,5	20	·	·	·	11	20	18	5	·	·	–	–	4	12	–
VIII	0,5	1,0	2,5	1,0	1	1,0	·	·	·	·	24,5	1,4	15,5	1,4	·	·	49	0,7	60,8	25,0	16	·	·	·	3	12	11	1	·	·	–	–	3	4	–
IX	·	·	·	·	0,5	1,0	0,5	1,0	·	·	42,5	1,7	16,5	1,8	·	·	30	1,2	54,9	16,5	9	1	·	·	2	15	13	1	·	·	5	–	4	5	–
X	0,5	1,0	3	1,0	0,5	1,0	·	·	0,5	1,0	3,3	1,8	18,5	2,1	·	·	37	1,1	54	5,0	20	3	·	·	·	2	1	·	·	·	9	–	6	1	–
XI	2,5	2,6	13	1,5	8,5	1,1	·	·	·	·	20	2,2	19	3,3	·	·	27	1,6	15,7	–	–	9	1	·	·	5	4	·	1	·	12	–	2	18	–
XII	3	1,0	3	1,3	4	1,2	·	·	·	·	32,5	2,5	24,5	3,3	1	1,0	25	1,9	25,0	11,2	3	24	8	2	·	6	5	1	·	·	4	–	2	12	–
Rok	21	1,0	74,5	1,2	57	1,2	2,5	0,2	1,5	0,2	265,5	1,8	213	2,0	3	0,3	457	1,1	536,9	37,6	30.IV	107	19	9	27	114	90	11	2	1	–	–	48	101	–

Nisko

$H_s = 164$ m $h_w = 16$ m

I	1,5	1,6	4	8,8	6	2,5	23,5	3,7	14,5	2,2	16	3,6	25	4,6	1,5	2,3	1	3,7	26,9	13,2	6	25	10	4	·	12	5	1	3	1	–	·	3	19	–
II	7,5	3,0	1	2,0	1	5,0	18,5	3,1	23,5	3,7	18,5	3,4	10,5	4,4	3,5	3,3	·	3,5	45,4	9,0	2	15	1	·	·	14	8	·	·	·	–	·	2	12	–
III	13,5	3,4	6	1,8	19	5,4	15	4,4	12	3,7	3	3,3	19,5	6,3	4	7,0	1	4,6	19,2	7,8	15	23	4	1	·	5	3	·	6	2	–	·	9	9	–
IV	18,5	2,6	7	1,6	11,5	2,6	20	2,4	9	2,7	4,5	2,4	13	2,7	5,5	3,5	1	2,5	22,2	7,0	11	9	·	·	3	7	4	·	·	·	–	2	8	5	–
V	17	2,4	10,5	4,2	11	2,7	8,5	4,1	8	2,2	5,5	3,5	11	3,3	17,5	4,1	4	3,2	59,7	22,0	9	·	·	·	·	11	8	1	2	·	–	·	2	14	–
VI	14,5	2,9	2	4,0	4,5	2,1	17,5	2,5	14,5	3,1	8	4,0	17	3,5	9	5,2	3	3,2	37,9	14,4	22	·	·	·	15	7	6	1	·	·	–	8	9	1	–
VII	9,5	2,6	3	2,7	10,5	3,4	8,5	3,0	12,5	2,6	14,5	3,0	19,5	3,8	11	4,2	4	3,1	148,2	52,0	16	·	·	·	17	17	16	3	·	·	–	6	6	8	–
VIII	6	3,4	1	4,0	4,5	2,2	9,5	3,3	12	3,3	9	4,1	26,5	3,3	16,5	3,2	8	3,0	71,5	16,5	8	·	·	·	7	16	13	2	·	·	–	2	3	5	–
IX	6	3,0	0,5	3,0	2	4,0	10,5	1,9	17,5	3,3	15	3,8	29	4,6	9,5	2,2	·	3,4	69,8	12,3	29	1	·	·	2	12	11	2	3	1	–	·	3	10	–
X	4	2,4	0,5	1,0	5,5	2,6	15	2,2	20,5	2,9	12,5	2,6	19,5	3,7	5,5	4,0	10	2,6	17,3	9,2	23	4	·	·	·	4	3	·	1	·	–	·	7	9	–
XI	5	11,0	3	5,3	15	3,5	28,6	3,5	18,5	2,4	4	4,4	14	6,6	1	7,0	1	4,3	23,8	8,3	26	10	2	·	·	8	7	·	4	1	–	·	3	16	–
XII	13	3,2	1	3,0	6	2,3	16	1,8	20,5	2,7	17,5	2,5	12	5,3	6	5,0	1	3,0	20,8	7,2	13	28	10	6	·	8	5	·	2	2	–	·	4	14	–
Rok	11,6	3,5	39,5	3,4	96,5	2,9	19,1	3,0	18,3	2,9	12,8	3,4	216,5	4,3	90,5	4,2	34	3,3	562,7	52,0	16.VII	115	27	11	44	121	89	10	21	7	–	18	59	122	–

Ławica, IUNiG

$H_s = 286$ m $h_w = 10$ m

I	6	1,9	2	1,2	·	·	·	·	14	2,1	10	3,8	14	1,8	·	·	47	1,3	17,1	4,4	15	23	10	9	·	8	6	·	1	·	31	·	3	13	18
II	3	2,8	4	2,9	·	·	·	·	13	6,0	17,5	11,1	14	5,0	1,5	5,0	31	4,4	24,5	6,3	25	12	·	2	·	15	6	·	7	5	3	·	1	14	2
III	5	3,6	22,5	5,6	2	4,5	·	·	7,5	8,6	14	9,5	14,5	5,9	0,5	2,0	27	4,8	39,8	11,6	30	18	2	·	·	12	10	1	9	3	3	1	5	11	3
IV	17	2,0	10,5	3,7	·	·	·	·	2	3,0	2,5	4,4	3,5	2,0	1,5	2,0	53	1,1	34,0	10,9	30	14	·	·	·	8	6	1	·	·	2	1	3	9	·
V	9,5	2,1	19,5	4,1	1,5	2,0	·	·	5	3,6	4	2,0	2,5	7,4	3	1,5	48	1,6	12,6	8,8	5	10	·	·	·	7	2	·	1	1	·	2	1	8	1
VI	1	2,0	2,2	3,4	·	·	·	·	2	7,0	8	5,3	12,5	3,4	1,5	2,5	43	2,0	41,6	22,6	24	·	·	·	9	8	7	1	2	·	·	4	7	8	·
VII	5	1,4	7,6	1,7	0,5	2,0	12,5	2,8	8	2,9	3,5	3,6	3,5	1,0	1,5	1,7	51	1,0	159,5	26,2	10	·	·	·	11	21	18	6	·	·	2	7	3	16	·
VIII	4	1,2	1,5	1,7	0,5	1,0	2,5	6,4	4,5	2,0	11,5	3,4	9,5	3,1	2	1,5	57	1,1	72,7	24,6	16	·	·	·	3	13	12	2	1	·	8	·	2	9	·
IX	2,5	2,6	4,5	1,7	·	·	·	·	9	4,9	21	5,1	16	4,1	5	2,0	35	2,0	61,6	15,4	9	3	·	·	2	17	15	1	·	·	8	·	2	14	·
X	·	·	3	1,7	·	·	1	1,0	19	4,1	16,5	3,1	9,5	3,0	·	·	44	1,8	62	5,0	20	4	·	·	·	3	2	·	1	·	17	·	4	6	·
XI	7	5,3	13	2,3	1	1,0	2	1,5	12,5	5,5	10	6,8	14,5	1,9	1	6,0	29	2,7	20,9	8,1	11	10	1	·	·	6	5	·	6	1	3	·	1	21	·
XII	7	2,9	3,5	4,0	3	2,5	7,6	6,7	13	8,2	13	5,7	5	4,0	3	2,7	36	3,4	24,2	6,6	14	23	7	2	·	13	7	·	6	4	3	·	1	16	·
Rok	6,7	2,3	110,5	2,8	8,5	1,1	25,5	1,5	109,5	4,8	133,5	5,3	119	3,6	20,5	2,2	501	2,3	511,7	26,2	10.VII	117	20	13	25	131	96	12	34	14	52	15	33	145	–

Otmuchów

$H_s = 211$ m $h_w = 11{,}6$ m

I	1	3,0	3	4,0	1	6,0	0,5	4,0	2	2,2	7,5	2,5	33,5	2,8	15,5	4,4	29	2,2	20,6	4,7	28	22	6	7	·	11	7	·	1	·	5	·	2	15	18
II	·	·	·	·	·	·	2	2,7	5	3,1	15,5	4,1	23,5	3,1	10	3,0	28	2,2	32,9	8,3	25	13	1	1	·	12	8	·	3	·	3	·	1	10	3
III	0,5	2,0	5	3,2	8,5	4,8	4,5	3,2	5	8,7	5	6,8	18,5	3,8	10	2,8	36	2,7	37,5	8,2	13	14	·	·	·	8	8	·	4	2	10	1	6	12	5
IV	0,5	3,0	1	2,0	·	·	2,5	3,0	6	3,0	5,5	2,4	29	2,6	10,5	3,4	35	1,7	30,3	10,4	30	11	·	·	1	10	4	1	·	·	7	·	3	10	·
V	1,5	4,0	5,5	3,9	5,5	4,6	2	4,0	9	2,2	8	1,5	20	3,4	14,5	4,6	29	2,4	23,0	6,2	22	4	·	·	1	11	6	·	1	·	1	1	·	8	·
VI	·	·	1,5	3,0	2,5	3,0	3	2,7	10	2,4	13	3,0	22	3,0	5	3,2	33	1,8	57,9	34,1	24	·	·	·	16	8	8	1	1	·	4	6	6	6	·
VII	·	·	·	·	·	·	1	2,0	2,5	1,6	11,5	3,7	21,5	3,3	7,5	4,5	49	1,7	160,7	22,5	23	·	·	·	12	21	19	7	·	·	·	6	7	16	·
VIII	·	·	1	2,0	·	·	1	3,0	4,5	3,6	16	3,1	31,5	3,1	5	3,7	34	2,0	35,4	6,4	16	·	·	·	4	13	9	·	·	·	1	1	1	5	·
IX	·	·	·	·	·	·	·	·	4	2,6	18,5	4,0	36	3,7	6,5	4,4	25	2,7	61,5	8,6	29	·	·	·	2	19	14	·	1	·	5	·	1	8	·
X	·	·	·	·	·	·	2	5,0	3	3,2	14,5	2,3	26	3,5	6,5	4,3	41	1,9	5,5	4,5	20	5	·	·	·	3	1	·	·	·	13	·	3	8	·
XI	2,5	4,8	8	3,0	8,5	3,9	7,5	3,2	12,5	1,9	9,5	4,6	16,5	3,9	8	3,9	19	2,8	15,6	3,9	11	10	1	·	·	7	6	·	1	·	4	·	3	19	·
XII	2	2,2	1,5	2,7	1,5	2,0	·	·	5	5,1	10,5	3,2	29	3,8	8,5	3,9	35	2,9	18,4	4,2	3,14	23	5	3	·	10	5	·	4	1	1	·	3	11	2
Rok	8	1,8	24,5	2,0	27,5	2,0	26	2,7	68,5	3,3	133	3,8	307	3,3	107,5	3,8	393	2,2	496,9	34,1	24.VI	102	13	11	36	133	93	9	18	3	54	15	36	128	28

Kudowa-Zdrój

$\varphi = 50°27'$ $\lambda = 16°16'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOT. WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data														
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	975.7	986.4	958.6	1024.0	-4.0	-0.6	-2.9	-2.6	0.3	-6.5	7.8	6	-19.0	17	91	83	90	88	0.4	1.0	0.5	0.6	8.5	8.5	7.0	8.0
II	965.9	985.7	940.8	1013.0	0.4	3.9	1.7	1.9	4.7	-4.0	8.2	13	-8.9	26	92	80	90	87	0.5	1.7	0.7	1.0	8.6	8.6	7.4	8.2
III	972.0	988.0	955.7	1019.1	0.3	7.2	3.0	3.4	8.6	-1.1	14.7	23	-11.4	3	89	63	82	78	0.8	4.1	1.5	2.1	6.7	7.0	5.0	6.2
IV	972.2	983.1	950.7	1018.7	4.1	10.9	5.4	6.4	12.3	0.6	23.9	30	-6.5	15	88	59	82	76	1.4	6.3	1.8	3.2	5.6	6.2	4.0	5.3
V	970.4	979.0	961.9	1016.4	7.7	13.1	8.1	9.2	14.8	3.2	24.5	16	-3.6	7	79	56	79	71	2.6	7.2	2.4	4.0	5.1	7.5	4.5	5.7
VI	972.0	985.4	960.0	1016.8	14.6	20.9	15.0	16.4	22.8	9.1	29.7	11	2.7	1	81	56	80	72	3.4	11.9	3.5	6.3	5.2	5.0	4.2	4.8
VII	968.7	980.1	958.3	1013.2	15.9	20.8	16.1	17.2	22.3	12.8	33.6	5	8.6	18	91	71	89	84	2.0	9.2	2.5	4.6	7.2	7.1	6.6	7.0
VIII	970.8	980.3	958.0	1015.9	12.2	18.0	13.3	14.2	19.5	9.1	27.2	11	3.7	23	94	70	90	85	0.9	6.7	1.6	3.1	7.1	7.3	5.5	6.6
IX	969.4	978.6	954.9	1014.1	8.9	14.5	9.7	10.7	15.3	6.3	25.6	8	-2.4	27	94	72	90	85	0.8	5.1	1.4	2.4	7.3	7.1	5.8	6.7
X	974.9	982.3	958.3	1021.5	4.7	11.8	6.1	7.2	12.6	2.1	19.3	19	-2.5	3	95	71	93	86	0.5	4.5	0.7	1.9	8.0	5.9	4.4	6.1
XI	974.2	989.1	958.3	1021.3	3.2	6.0	4.2	4.4	7.0	1.3	16.5	6	-12.1	30	86	77	86	83	1.1	2.5	1.2	1.6	8.5	8.7	7.6	8.3
XII	969.8	988.1	951.8	1017.6	-2.3	0.1	-1.6	-1.4	1.3	-4.8	10.5	13	-13.7	17	90	83	90	88	0.5	1.1	0.6	0.7	9.2	8.4	8.1	8.6
Rok	971.3	989.1	938.9	1017.8	5.5	10.6	6.5	7.3	11.8	2.6	33.6	5.VII	-19.0	17.1	89	70	87	82	1.2	5.1	1.5	2.6	7.2	7.3	6.8	6.8

Busko-Zdrój

$\varphi = 50°27'$ $\lambda = 20°43'$

I	–	–	–	–	-2.8	0.0	-1.9	-1.6	0.8	-5.0	6.9	6	-16.7	17	95	91	95	94	0.2	0.5	0.2	0.3	8.5	7.6	6.8	7.6
II	–	–	–	–	0.7	4.7	2.1	2.4	5.7	-0.7	10.9	6	-5.5	28	94	83	92	90	0.4	1.6	0.6	0.9	8.5	7.0	6.9	7.5
III	–	–	–	–	0.8	6.5	3.2	3.4	8.1	-4.0	17.7	28	-8.5	4	89	68	84	79	0.8	3.8	1.6	2.1	6.1	6.1	5.2	5.8
IV	–	–	–	–	6.5	12.7	8.3	9.0	14.2	3.6	26.1	30	-3.5	16	87	59	80	75	1.4	7.2	2.5	3.7	6.3	5.5	5.6	5.8
V	–	–	–	–	9.2	13.6	9.9	10.6	14.8	5.9	23.8	20	0.9	29	85	64	82	77	2.0	6.8	2.4	3.7	6.4	7.1	5.7	6.4
VI	–	–	–	–	16.6	23.0	17.7	18.8	24.4	12.1	32.0	30	6.0	7	83	54	77	71	3.3	13.8	4.8	7.3	5.1	5.0	5.2	5.1
VII	–	–	–	–	17.8	23.3	18.4	19.5	24.7	14.2	35.0	5,8	9.5	29	86	62	83	77	3.3	12.5	4.0	6.6	6.7	6.1	6.5	6.4
VIII	–	–	–	–	14.9	21.0	15.8	16.9	22.5	11.3	31.3	12	7.0	31	87	58	83	76	2.5	11.4	3.3	5.7	4.5	5.4	4.8	4.9
IX	–	–	–	–	10.3	16.1	12.0	12.6	17.6	7.8	27.7	9	0.8	26	91	62	85	79	1.1	7.5	2.2	3.6	4.7	6.3	6.3	5.8
X	–	–	–	–	6.5	13.5	8.6	9.3	14.2	4.3	21.7	19	-1.3	3	93	66	88	82	0.7	5.8	1.4	2.6	5.9	5.5	4.8	5.4
XI	–	–	–	–	2.4	6.4	3.4	3.9	7.5	0.5	17.7	4	-10.3	30	94	79	91	88	0.5	2.7	0.7	1.3	7.3	6.4	6.3	6.7
XII	–	–	–	–	-2.5	0.2	-1.1	-1.3	1.4	-5.1	8.7	13	-12.7	25	–	–	–	–	–	–	–	–	7.5	7.4	6.8	7.2
Rok	–	–	–	–	6.7	11.8	8.0	8.6	13.0	4.0	35.0	5,8.VII	-16.7	17.1	–	–	–	–	–	–	–	–	6.5	6.3	5.9	6.2

Dęba-Rozalin

$\varphi = 50°27'$ $\lambda = 21°45'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	5.3	13.9	8.0	8.8	15.1	2.2	27.1	30	-4.3	15	–	–	–	–	–	–	–	–	5.9	6.1	4.9	5.6
V	–	–	–	–	9.3	14.2	10.2	11.0	15.6	5.2	24.2	13	0.1	5	–	–	–	–	–	–	–	–	6.1	8.6	8.1	7.6
VI	–	–	–	–	16.9	24.1	18.4	19.4	26.2	12.0	34.8	12	5.8	7	–	–	–	–	–	–	–	–	4.4	5.3	4.1	4.6
VII	–	–	–	–	17.8	23.9	18.9	19.9	25.6	14.3	38.1	5	7.6	4	–	–	–	–	–	–	–	–	6.5	6.3	5.4	6.1
VIII	–	–	–	–	16.0	21.2	16.5	17.3	22.8	11.5	31.2	12	6.9	31	–	–	–	–	–	–	–	–	5.7	6.8	4.3	5.6
IX	–	–	–	–	10.6	16.7	13.0	13.3	17.8	8.6	28.8	9	1.2	27	–	–	–	–	–	–	–	–	6.0	6.9	6.3	6.4
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Tomaszów Lubelski

$\varphi = 50°27'$ $\lambda = 23°25'$

I	–	–	–	–	-3.4	-1.2	-2.5	-2.4	-0.4	-5.8	3.9	9,10	-14.4	17	94	89	89	90	0.4	0.6	0.6	0.5	9.2	8.5	9.0	8.9
II	–	–	–	–	0.8	3.7	1.5	1.9	4.8	-1.3	10.4	6	-6.9	28	90	80	87	86	0.6	1.8	1.0	1.1	8.9	8.1	4.6	7.2
III	–	–	–	–	-1.4	4.4	0.6	1.1	6.0	-4.0	16.0	31	-16.4	4	–	–	–	–	–	–	–	–	6.1	6.2	4.8	5.7
IV	–	–	–	–	5.3	12.7	6.9	8.0	13.9	1.3	26.0	30	-4.3	16	80	50	76	69	2.1	8.9	2.7	4.6	5.9	5.9	4.1	5.3
V	–	–	–	–	8.8	13.1	9.0	10.0	14.5	5.6	23.0	18	0.3	5,7	85	67	86	79	1.9	6.1	1.7	3.2	7.2	8.8	7.7	7.9
VI	–	–	–	–	15.3	22.6	16.6	18.0	23.9	10.4	31.1	12	4.6	7	75	50	78	68	4.8	14.1	4.5	7.8	4.7	5.8	4.8	5.1
VII	–	–	–	–	16.8	22.3	17.3	18.4	24.1	13.1	34.5	5	7.4	4	85	62	83	77	3.0	11.4	3.4	5.9	6.4	6.6	7.0	6.7
VIII	–	–	–	–	14.2	20.5	14.9	16.1	22.0	10.8	31.1	14	4.1	24	89	60	86	78	4.7	10.3	2.4	4.8	5.8	6.2	3.5	5.2
IX	–	–	–	–	9.8	15.0	10.9	11.9	17.5	7.3	27.0	9	-1.9	27	92	62	87	80	4.0	7.4	4.7	3.4	7.7	7.2	5.0	6.6
X	–	–	–	–	4.9	12.4	6.5	7.6	13.7	1.9	24.2	19	-4.5	3	89	63	86	79	1.1	5.8	1.6	2.8	6.4	6.5	3.5	5.4
XI	–	–	–	–	1.4	5.3	2.2	2.8	6.4	-1.1	17.2	4	-11.4	29	94	83	94	90	0.4	1.7	0.4	0.8	8.9	8.2	7.1	8.1
XII	–	–	–	–	-3.5	-0.8	-2.7	-2.4	0.4	-6.3	10.6	13	-11.9	16,25	89	86	89	88	0.5	0.9	0.5	0.6	7.8	8.4	6.8	7.7
Rok	–	–	–	–	5.8	10.9	6.8	7.6	12.2	2.7	34.5	5.VII	-16.4	4.III	–	–	–	–	–	–	–	–	7.1	7.1	6.7	6.6

Kudowa – Zdrój

$H_s = 385\ m$ $H_b = 383{,}3\ m$ $h_w = 12\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, %nD)																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v											
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max≥25°	0,1 ÷ 1,0	1,0 ÷ 10,0	10,0 ÷ 100,0	10 ÷ 15	≥15	≡	≈	◔	●	⊠
I	2	2,8	3,5	1,9	15	2,6	17,5	2,5	8	1,4	16,5	1,5	18	1,7	11,5	2,0	1	2,0	36,0	8,9	6	28	12	9	·	15	8	·	1	·	21	·	1	18	28
II	2	2,2	2	2,8	8	1,7	13	2,0	8,5	2,7	19	2,4	21	1,9	9,5	1,9	1	2,1	58,3	14,9	18	15	·	·	·	21	15	1	·	·	13	·	·	19	4
III	0,5	4,0	·	·	1,5	1,8	18,5	4,4	7	5,7	6,5	2,5	24,5	2,3	17	2,1	4	2,8	60,1	15,3	17	17	1	1	·	13	11	2	2	1	4	1	4	12	5
IV	0,5	2,0	2	1,8	20,5	2,2	24	1,9	4,5	1,4	5,5	1,8	18,5	1,9	14,5	1,7	·	1,9	47,7	21,3	30	14	·	·	·	9	6	1	·	·	2	1	5	7	·
V	3,5	1,4	5	2,9	20,5	3,8	21,5	2,8	3,5	1,7	3,5	3,0	16	1,9	17,5	2,0	2	2,6	30,2	9,7	19	10	·	·	·	11	7	·	·	·	5	6	1	4	1
VI	0,5	3,0	3,5	1,3	3,0	3,1	15,5	2,7	3,5	2,3	6,5	2,5	20,5	2,7	10	1,4	·	2,6	77,5	24,6	4	·	·	·	8	11	11	2	2	·	6	7	6	6	·
VII	0,5	1,0	2,5	1,2	14,5	2,0	17	1,7	5,5	1,9	10,5	1,5	22,5	2,2	15	1,7	5	1,8	347,6	60,7	10	·	·	·	9	23	18	9	·	·	16	10	4	14	·
VIII	0,5	1,0	3	2,3	6	1,0	21	1,1	6,5	1,9	11,5	2,2	27	2,0	13,5	2,0	4	1,7	80,5	10,3	15	·	·	·	1	17	14	1	·	·	21	8	·	11	·
IX	3	4,5	3	2,3	8,5	1,8	11,5	1,9	7,5	2,3	13	2,8	26	2,2	11,5	2,7	4	2,3	107,3	27,8	23	1	·	·	1	19	15	3	·	·	23	1	1	10	·
X	1	1,0	3,5	1,0	9	1,1	21	1,4	13	1,8	11	1,9	20	1,7	11,5	1,6	3	1,5	9,0	4,8	20	8	·	·	·	9	3	·	·	·	24	·	2	8	·
XI	4,5	3,3	6,5	4,2	18	3,9	12	2,9	10,5	1,8	11	2,0	16,5	2,9	10	3,7	1	3,0	23,3	6,4	25	10	1	1	·	11	8	·	2	·	12	·	·	20	1
XII	6,5	2,2	3	2,3	8	2,9	10	2,2	6	3,3	17,5	2,4	28	2,3	14	1,9	·	2,4	43,1	15,1	8	28	11	3	·	15	10	1	1	·	14	·	1	20	26
Rok	25	2,4	37,5	2,0	173	2,3	202,5	2,3	84	2,4	132	2,2	260,5	2,1	155,5	2,1	25	2,2	890,6	60,7	10.VII	131	25	14	19	174	126	20	8	1	162	34	25	149	63

Busko – Zdrój

$H_s = 225\ m$ $h_w = 14\ m$

I	3	2,0	9	3,4	6	2,0	13,5	1,4	16	1,8	9,5	2,9	26,5	2,6	4,5	3,1	5	2,2	33,0	12,2	6	26	10	5	·	10	8	2	·	·	–	·	·	18	23
II	5	2,8	3	1,3	4	1,5	13	3,1	18	2,5	15	2,7	18	2,2	8	1,9	2	2,4	34,5	5,0	21	17	1	·	·	15	12	·	·	·	–	·	·	13	5
III	9	2,6	7	3,4	19,5	3,7	8,5	2,8	13	2,5	11	2,1	12	4,2	10	2,5	5	2,9	23,8	7,8	18	14	4	·	·	8	8	·	·	·	–	·	7	12	·
IV	20,5	2,3	10	2,5	11	2,3	9	1,7	9,5	2,3	5	2,8	12	1,8	11	2,1	2	2,1	28,6	12,3	7	5	·	·	1	10	5	1	1	1	–	1	5	9	·
V	19	2,6	21,5	3,0	9	2,8	10,5	2,5	5	1,4	3,5	2,3	6	2,2	13,5	2,4	5	2,4	50,6	24,3	20	·	·	·	·	9	7	1	·	·	–	3	2	11	·
VI	14,5	2,5	4,5	2,9	7	1,7	8	2,2	14	2,6	9,5	2,1	15,5	3,0	11	2,1	6	2,3	22,8	7,0	5	·	·	·	12	8	5	·	·	·	–	6	4	2	·
VII	10	2,9	3	3,3	5	2,8	5	3,0	9,5	2,2	17	2,6	23	2,5	15,5	2,5	4	2,6	103,7	25,0	16	·	·	·	14	16	14	4	·	·	–	7	2	13	·
VIII	5,5	2,7	4	2,5	3,5	2,6	5	2,5	7	2,9	13	2,2	25,5	2,5	21,5	2,3	8	2,2	52,0	11,5	14	·	·	·	6	9	7	1	1	1	–	3	4	5	·
IX	5,5	2,5	0,5	2,0	3	2,0	7,5	2,0	9,5	2,9	17	3,5	35,5	3,5	3,5	1,9	8	2,8	30,8	7,0	19,29	·	·	·	2	12	8	·	1	·	–	·	4	9	·
X	3	4,0	2	2,0	3,5	2,2	15	2,1	17,5	2,0	12,5	2,6	15,5	2,5	12	2,1	10	2,0	41,6	4,6	22	3	·	·	·	3	3	·	·	·	–	·	4	8	·
XI	3,5	5,7	2,5	3,6	24,5	2,9	17	2,8	12,5	2,4	7	2,7	16,5	4,5	3,5	6,3	3	3,3	10,9	5,6	28	13	2	1	·	6	2	·	2	·	–	·	5	16	·
XII	3,5	3,4	7,5	3,2	3	3,0	13	3,1	21,5	2,3	18	3,5	16	3,9	6,5	2,7	2	3,0	16,8	6,5	8	27	9	3	·	6	5	·	2	1	–	·	3	14	3
Rok	10,2	3,0	74,5	2,8	101	2,5	125	2,4	153	2,3	138	2,7	222	3,0	121,5	2,7	58	2,5	448,9	25,0	16.VII	105	26	9	35	112	82	9	7	3	–	20	40	130	34

Dęba – Rozalin

$H_s = 166\ m$ $h_w = 10\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	9	3,9	5,5	2,3	5	2,1	16,5	2,3	19	2,2	6,5	3,2	5	2,5	9,5	3,7	14	2,3	43,1	8,8	7	10	·	·	3	10	9	·	·	·	–	1	5	9	·
V	13	3,1	12,5	4,0	11,5	2,4	15,5	1,8	8,5	1,7	9,5	2,6	8,5	3,2	6	3,8	8	2,5	47,2	14,7	9	·	·	·	·	11	8	2	·	·	–	3	·	16	·
VI	10	2,8	0,5	2,0	2,5	1,0	10,5	2,6	2,6	3,4	13	3,9	11	3,7	5,5	3,9	11	2,9	27,0	8,7	22	·	·	·	18	10	6	·	·	·	–	4	4	2	·
VII	4,5	3,1	4	2,9	5,5	1,7	10	2,0	23,5	2,4	19,5	3,1	11	2,8	6	3,7	9	2,4	102,9	25,5	8	·	·	·	15	17	12	5	·	·	–	5	5	13	·
VIII	1,5	4,3	2	3,8	1,5	3,0	8	1,9	28,5	2,0	21	2,5	22	3,1	4,5	4,1	4	2,5	83,2	22,7	16	·	·	·	7	14	10	2	1	1	–	3	1	4	·
IX	4,5	2,1	0,5	3,0	·	·	12	2,0	15	3,0	2,8	3,7	21	4,6	5	2,3	4	3,2	57,2	12,2	29	·	·	·	3	11	10	2	·	·	–	·	8	10	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Tomaszów Lubelski

$H_s = 273\ m$ $h_w = 12\ m$

I	2,5	4,0	4,5	4,0	6	2,8	10	2,6	12,5	2,4	17,5	3,8	9,0	3,5	6	3,5	4	3,2	21,9	4,6	6	28	13	4	·	14	8	·	·	·	–	·	1	25	22
II	7,5	3,7	·	·	·	·	14	3,3	19,5	3,2	17	3,3	14,5	3,5	4,5	3,2	7	3,1	26,2	6,1	15	19	2	·	·	15	10	·	·	·	–	·	1	11	6
III	12,5	3,2	4,5	1,9	8	3,6	15,5	4,6	7,5	3,3	10,5	3,9	14,5	4,2	14	2,9	9	3,2	20,0	6,6	13	23	6	2	·	9	4	·	1	·	–	·	8	11	3
IV	14,5	3,0	7,5	2,5	7,5	2,9	11	2,9	9	2,1	7	2,9	7	2,9	5,5	2,8	21	2,1	19,8	8	17	17	·	·	1	8	6	·	·	·	–	1	7	11	1
V	22,5	3,2	16	3,3	9,5	2,7	5,5	3,3	3	2,3	3	2,7	8,5	1,9	12	2,8	13	2,5	73,9	18,7	9	·	·	·	·	15	12	2	·	·	–	2	2	20	·
VI	12,5	3,0	0,5	3,0	1,5	2,3	10,5	2,8	12,5	3,1	10	2,9	13	3,6	12,5	3,4	17	2,5	58,7	23,4	4	·	·	·	12	10	5	3	·	·	–	4	6	5	·
VII	7,5	2,2	2	2,7	6,5	2,7	8	2,4	9,5	2,6	19,5	3,3	14,5	2,8	6,5	2,9	19	2,2	108,2	18,5	8	·	·	·	13	21	17	3	·	·	–	8	2	16	·
VIII	3	2,8	1	1,0	0,5	3,0	11	2,8	9,5	2,8	11	3,3	18,5	2,6	17,5	2,8	21	2,1	55,1	16,3	10	·	·	·	5	15	10	2	·	·	–	5	3	4	·
IX	6	3,5	2	2,0	1	3,0	5,5	2,4	11,5	3,3	18,5	3,4	28,5	4,0	7	3,1	10	3,1	61,9	12,5	29	1	·	·	2	16	12	2	·	·	–	·	2	10	·
X	2,5	2,2	4	2,0	2	1,5	6,5	2,5	11	2,7	20,5	2,6	20	3,0	7,5	2,4	11	2,3	13,8	5,8	20	10	·	·	·	6	5	·	·	·	–	·	6	9	·
XI	7	4,1	6,5	4,2	10,5	3,5	17,5	3,1	14,5	2,9	19,5	3,5	6	4,2	1,5	6,7	7	3,2	30,5	14,8	28	14	3	2	·	10	6	1	·	·	–	·	2	20	1
XII	10,5	3,1	3,5	2,0	4	2,8	10	2,8	22,5	3,0	3,1	3,4	3	3,7	3,5	3,3	5	2,9	42,3	12,3	8	29	14	8	·	10	7	1	·	·	–	·	1	19	13
Rok	10,8,5	3,2	5,2	2,4	5,7	2,5	12,5	2,9	15,0,5	2,8	18,5	3,2	17,5	3,3	9,8	3,2	14,4	2,7	5,5,2,3	23,4	4.VI	144	38	16	33	149	102	14	1	·	–	20	41	161	45

Kłodzko

$\varphi = 50°26'$ $\lambda = 16°39'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia						Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies	$\overline{Max}$	$\overline{Min}$					I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	983.6	994.4	966.0	1023.4	-3.7	-0.5	-2.4	-2.2	1.1	-6.5	9.6	6	-22.1	17	89	83	87	86	0.6	1.1	0.8	0.8	7.8	7.5	6.6	7.3
II	973.4	983.8	948.1	1012.8	1.2	4.6	2.2	2.6	5.8	-0.2	9.9	14	-13.1	27	89	76	87	84	0.8	2.1	1.0	1.3	8.2	8.2	7.3	7.9
III	979.7	996.3	962.0	1019.1	0.7	6.9	3.6	3.7	8.9	-0.5	15.7	13	-10.1	3	89	66	82	79	0.9	3.9	1.6	2.1	7.2	6.4	5.6	6.4
IV	980.1	991.6	958.2	1019.1	3.1	10.8	6.3	6.6	12.2	1.4	24.5	29	-4.9	15	94	60	83	79	0.5	6.3	1.8	2.9	6.1	7.2	5.6	6.3
V	978.2	986.7	968.9	1016.7	7.0	13.7	9.0	9.7	15.3	3.8	25.0	16	-2.4	7	84	51	75	70	1.6	8.2	3.0	4.3	6.0	7.2	6.0	6.4
VI	979.5	994.1	967.8	1017.0	14.0	21.7	16.1	17.0	23.8	9.3	31.0	11	2.4	1	81	51	77	70	3.1	13.9	4.6	7.2	5.1	5.8	4.2	5.0
VII	976.0	988.1	965.4	1013.3	16.1	24.3	16.7	17.7	23.0	13.6	34.0	5	8.9	18	88	68	86	81	2.4	9.7	2.6	4.9	6.6	6.8	6.7	6.7
VIII	978.1	988.8	965.7	1015.9	12.2	18.5	14.0	14.7	20.3	9.6	27.7	11	3.4	23	93	67	88	83	1.1	7.5	2.1	3.6	6.5	7.5	5.6	6.5
IX	976.9	986.2	964.5	1015.1	9.5	16.2	10.5	11.4	16.6	7.0	26.9	9	-2.5	27	91	68	87	82	1.2	5.9	1.8	3.0	7.5	7.3	5.3	6.7
X	982.5	990.3	966.0	1021.2	6.0	12.6	7.7	8.5	13.8	4.1	18.7	18	-1.0	3	92	68	88	83	0.9	5.0	1.5	2.5	7.1	5.8	3.0	5.3
XI	981.9	998.3	966.4	1021.2	3.5	6.3	4.7	4.8	7.7	2.4	16.2	10	-10.4	30	88	76	86	83	1.0	2.6	1.3	1.6	7.8	8.0	8.2	8.0
XII	977.5	996.6	945.6	1017.5	-1.6	0.2	-0.8	-0.8	2.0	-3.7	10.7	13	-13.0	16	89	83	87	86	0.7	1.1	0.8	0.9	8.1	7.7	7.0	7.6
Rok	979.0	998.3	945.6	1017.7	5.7	10.9	7.5	7.8	12.5	3.4	34.0	5.VII	-22.1	17.1	89	68	86	81	1.2	5.6	1.9	2.9	7.0	7.1	5.9	6.7

Bobrowniki Śląskie

$\varphi = 50°26'$ $\lambda = 18°52'$

I	-	-	-	-	-2.5	-0.1	-1.6	-1.4	1.1	-	6.6	6	-	-	90	86	88	88	0.4	0.8	0.6	0.6	6.5	6.4	5.8	6.2
II	-	-	-	-	0.9	4.6	2.2	2.5	5.6	-	9.1	9,13	-	-	-	-	-	-	-	-	-	-	5.9	5.0	6.0	5.6
III	-	-	-	-	0.8	6.9	3.5	3.7	8.6	-	16.5	14	-	-	87	63	82	77	0.9	4.3	1.6	2.3	5.2	4.7	4.7	4.9
IV	-	-	-	-	4.8	11.3	7.1	7.6	12.8	-	24.6	30	-	-	87	55	79	74	1.3	7.4	2.5	3.7	5.6	5.0	4.9	5.2
V	-	-	-	-	7.8	13.2	9.5	9.9	14.7	-	24.2	19	-	-	-	-	-	-	-	-	-	-	5.3	5.5	5.9	5.6
VI	-	-	-	-	16.2	22.0	16.5	17.8	23.5	-	30.8	30	-	-	75	54	78	69	4.8	12.8	4.5	7.4	3.5	3.8	3.9	3.7
VII	-	-	-	-	17.2	24.6	17.5	18.4	23.5	-	35.4	8	-	-	84	66	84	78	3.7	10.8	3.8	6.1	6.0	5.4	6.2	5.9
VIII	-	-	-	-	14.3	19.2	14.6	15.7	20.7	-	27.3	11	-	-	87	65	87	80	2.3	7.9	2.3	4.2	5.0	4.5	4.1	4.5
IX	-	-	-	-	10.3	15.1	10.9	11.8	16.2	-	26.5	9	-	-	91	70	90	84	1.2	5.7	1.4	2.8	5.6	5.2	4.3	5.0
X	-	-	-	-	6.9	12.9	8.6	9.2	13.8	-	20.0	19	-	-	92	70	89	84	0.9	4.9	1.4	2.4	4.9	4.3	2.9	4.0
XI	-	-	-	-	3.7	6.6	4.1	4.6	7.6	-	18.0	5	-	-	91	81	89	87	0.8	2.5	1.0	1.4	6.9	6.0	6.4	6.4
XII	-	-	-	-	-2.4	0.5	-1.1	-1.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.7	7.0	6.4	6.7
Rok	-	-	-	-	6.5	11.2	7.6	8.2	-	-	35.4	8.VII	-	-	-	-	-	-	-	-	-	-	5.6	5.2	5.1	5.3

Świerklaniec

$\varphi = 50°26'$ $\lambda = 18°57'$

I	-	-	-	-	-2.3	0.4	-1.2	-1.1	1.0	-3.9	6.6	6	-18.3	17	-	-	-	-	-	-	-	-	7.0	6.6	7.1	6.9
II	-	-	-	-	1.5	4.9	1.9	2.6	5.5	0.3	9.5	14	-4.6	28	-	-	-	-	-	-	-	-	7.2	6.4	6.5	6.7
III	-	-	-	-	1.0	7.1	3.4	3.7	8.4	-1.0	16.1	14,28	-12.0	4	-	-	-	-	-	-	-	-	6.5	4.8	5.4	5.2
IV	-	-	-	-	5.1	11.7	7.1	7.8	13.3	2.2	25.0	30	-5.2	15	86	52	79	72	1.4	7.7	2.4	3.8	4.9	5.5	4.0	4.8
V	-	-	-	-	8.7	13.6	9.1	10.1	14.9	4.8	24.1	19	-1.6	6	76	52	78	69	2.9	8.4	2.7	4.7	4.3	6.0	3.6	4.6
VI	-	-	-	-	16.4	22.1	16.4	17.8	23.6	-	31.0	30	-	-	74	50	78	67	5.1	14.1	4.4	7.9	3.6	5.3	3.3	4.1
VII	-	-	-	-	17.0	22.0	17.2	18.4	23.6	13.5	35.3	8	9.4	30	83	64	88	76	3.8	11.3	3.8	6.3	5.0	4.9	4.5	4.8
VIII	-	-	-	-	13.8	19.3	14.5	15.5	20.9	10.3	27.0	11	5.7	23	88	62	86	79	1.9	8.9	2.5	4.4	5.6	5.3	3.8	4.9
IX	-	-	-	-	9.6	15.3	10.7	11.6	16.3	7.0	26.0	9	-0.4	26	90	63	87	80	1.3	6.8	1.7	3.3	5.7	5.9	4.3	5.3
X	-	-	-	-	6.4	13.1	8.2	9.0	13.8	4.2	19.7	19	-1.2	26	90	65	86	80	1.0	6.4	1.7	2.7	5.4	5.5	3.1	4.7
XI	-	-	-	-	3.2	6.8	4.2	4.6	7.6	1.3	18.3	5	-10.1	30	90	76	87	85	0.8	3.0	1.2	1.7	7.2	6.6	7.1	7.0
XII	-	-	-	-	-2.1	0.5	-1.0	-0.9	1.5	-4.3	13.0	13	-13.2	17	88	85	87	87	0.6	1.1	0.7	0.8	7.4	6.2	6.8	6.8
Rok	-	-	-	-	6.6	11.4	7.5	8.2	12.5	-	35.3	8.VII	-18.3	17.1	-	-	-	-	-	-	-	-	5.7	5.7	5.0	6.5

Uwaga. Termometr minimalny nie posiadał świadectwa sprawdzenia.

Duszniki – Zdrój

$\varphi = 50°24'$ $\lambda = 16°24'$

I	-	-	-	-	-3.9	-0.5	-2.6	-2.4	0.5	-6.1	6.8	6	-18.3	17	-	-	-	-	-	-	-	-	8.4	7.2	5.1	6.2
II	-	-	-	-	0.7	3.9	1.7	2.0	4.7	-1.2	10.5	3	-9.1	27	-	-	-	-	-	-	-	-	7.6	7.4	8.6	7.2
III	-	-	-	-	0.5	6.5	2.3	2.9	7.5	-1.6	13.4	13	-11.6	3	-	-	-	-	-	-	-	-	5.8	5.6	4.6	5.3
IV	-	-	-	-	3.3	9.4	4.6	5.5	10.8	0.6	22.7	30	-6.3	14,15	-	-	-	-	-	-	-	-	5.7	6.3	4.9	5.6
V	-	-	-	-	6.3	12.3	7.2	8.2	-	3.1	-	-	-3.5	7	79	52	76	69	2.0	7.2	2.4	3.9	5.5	7.4	5.3	6.1
VI	-	-	-	-	13.7	19.7	13.8	15.2	-	9.5	-	-	4.0	1	83	67	84	75	2.8	10.9	2.8	5.4	4.6	5.6	3.4	4.5
VII	-	-	-	-	15.3	19.6	14.8	16.1	21.1	12.3	32.6	5	8.9	18	88	73	90	84	2.4	7.8	2.0	4.1	6.5	6.5	6.4	6.5
VIII	-	-	-	-	11.9	17.3	12.6	13.6	18.5	9.0	26.6	11	4.0	23	90	70	89	83	1.6	6.5	1.6	3.2	5.7	6.8	3.9	5.5
IX	-	-	-	-	8.8	13.4	9.3	10.2	14.3	6.1	25.1	8	-1.7	27	90	73	87	83	1.2	4.7	1.6	2.5	6.6	6.6	4.8	6.0
X	-	-	-	-	6.0	11.6	6.5	7.6	12.5	3.1	20.0	19	-2.2	3	89	69	87	82	1.1	4.8	1.5	2.4	6.1	5.3	3.8	5.1
XI	-	-	-	-	2.6	4.8	3.1	3.4	6.0	0.8	15.0	6	-12.5	30	88	80	90	86	1.0	2.1	0.9	1.3	6.8	7.8	5.8	7.1
XII	-	-	-	-	-2.7	-0.4	-1.9	-1.7	0.9	-5.1	10.7	13	-14.7	17	93	87	92	91	0.3	0.9	0.5	0.6	7.2	7.4	6.6	7.1
Rok	-	-	-	-	5.2	9.8	6.0	6.8	-	2.5	-	-	-18.3	17.1	-	-	-	-	-	-	-	-	6.2	6.7	5.2	6.0

Kłodzko

$H_s = 318$ m $H_b = 320{,}1$ m $h_w = 15$ m **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, v=D)																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v		=							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min <0°	Max <0°	Min <-10°	Max >25°	0,1 ≤ R < 1,0	1,0 ≤ R < 10,0	R ≥ 10,0	10 ≤ v < 15	v ≥ 15									
I	5	3,7	4	3,4	·	·	2,5	4,8	2,8	4,3	6	3,3	16	4,0	55	6,3	26	3,0	48,3	4,2	15	20	10	10	·	11	6	·	2	·	4	·	3	14	23				
II	4,5	3,0	1	1,0	1,5	1,3	3,5	3,9	30,5	5,9	6,5	6,1	12	4,7	4,5	4,9	20	3,7	38,7	13,5	18	10	·	2	·	12	6	1	3	2	1	·	1	17	3				
III	13,5	2,4	5	3,4	1,5	3,3	3,5	5,4	14,5	7,9	9	4,9	9	6,0	2	3,0	35	3,1	46,7	13,2	30	16	2	1	·	12	10	1	4	1	5	1	4	13	5				
IV	19	2,8	10	2,6	·	·	1,5	8,0	5	5,5	1,5	3,7	4	3,6	7	2,2	42	1,7	57,0	11,3	7	12	·	·	·	8	6	2	1	·	4	1	3	10	2				
V	17	3,0	14	4,0	1,5	4,7	1,5	6,0	4	3,2	1,5	6,7	4	3,2	16,5	3,8	33	2,4	13,3	8,7	5	7	·	·	1	7	3	·	·	·	·	2	1	11	1				
VI	14,5	2,1	7	3,9	1,5	5,3	3	4,5	10,5	3,6	8	5,3	10	3,9	7,5	2,7	28	2,4	41,3	20,2	24	·	·	·	10	7	7	1	1	·	1	8	7	6	·				
VII	6	2,1	5	1,4	1	1,0	3,5	4,3	5,5	3,6	1,5	3,7	16,5	3,8	13,5	2,8	27	2,3	184,4	26,3	8	·	·	·	10	22	18	8	·	·	4	10	4	15	·				
VIII	3	1,7	·	·	2	3,0	2	4,2	12	4,0	12	3,4	17	3,3	11	2,8	34	2,1	91,5	25,6	16	·	·	·	1	15	12	3	·	·	8	3	2	10	·				
IX	2,5	3,2	1,5	2,7	·	·	2,5	3,4	14	5,6	17,5	5,1	22	4,7	1	1,0	29	3,2	65,0	14,9	9	2	·	·	1	20	15	1	6	·	4	·	2	11	·				
X	1,5	1,7	0,5	1,0	·	·	3	6,8	30,5	5,0	6	3,9	13	4,5	6,5	2,5	32	3,0	5,2	5,1	20	3	·	·	·	2	1	·	1	·	9	·	3	6	·				
XI	6,5	4,7	9,5	3,1	3	2,7	3,5	5,9	21,5	6,2	8	6,4	17,5	4,8	3,5	5,6	17	4,1	19,3	11,1	12	9	1	1	·	7	4	1	6	·	2	·	1	19	1				
XII	13,5	1,9	0,5	3,0	·	·	2,5	6,0	2,3	6,2	1,3	6,0	1,0	6,4	8,5	2,5	22	3,8	30,8	6,9	14	23	8	2	·	13	6	·	6	1	1	·	2	16	14				
Rok	106,6	2,7	5,8	2,5	1,2	1,8	32,5	5,3	19,9	5,1	10,4	4,9	15,1	4,4	8,7	3,1	34,5	2,9	591,5	26,3	8.VII	102	21	16	23	136	94	18	30	4	43	25	33	148	49				

Babrowniki Śląskie

$H_s = 300$ m

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25,1	8,0	6	-	9	-	·	14	8	·	-	-	-	·	4	10	-				
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59,9	14,6	18	-	1	-	·	18	9	1	-	-	-	·	1	6	-				
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58,8	25,3	18	-	3	-	·	11	8	1	-	-	-	·	9	6	-				
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31,2	10,4	7	-	·	-	·	12	6	1	-	-	-	2	6	7	-				
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30,3	12,9	20	-	·	-	·	10	6	1	-	-	-	3	5	7	-				
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59,0	27,2	7	-	·	-	9	9	7	1	-	-	-	7	11	2	-				
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	181,6	64,6	16	-	·	-	10	19	16	4	-	-	-	7	5	7	-				
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	148,9	43,9	14	-	·	-	2	13	13	5	-	-	-	2	5	3	-				
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100,5	16,7	14	-	·	-	2	16	14	4	-	-	-	1	3	4	-				
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5,4	2,5	22	-	·	-	·	3	2	·	-	-	-	·	7	5	-				
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20,0	5,9	28	-	2	-	·	7	6	·	-	-	-	·	6	15	-				
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33,9	6,0	3	-	-	-	·	12	8	·	-	-	-	·	1	13	-				
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	754,6	64,6	16.VII	-	-	-	23	144	103	18	-	-	-	22	63	83	-				

Świerklaniec

$H_s = 284$ m $h_w = 17$ m

I	·	·	5	2,2	·	·	3	1,7	·	·	39	3,4	6	4,7	21	3,6	19	2,7	24,2	6,3	6	25	11	5	·	14	9	·	3	1	-	·	·	9	20				
II	·	·	3	1,3	·	·	5	3,2	1	1,0	57	3,9	1	2,0	7	2,1	10	3,1	49,2	13,3	18	8	1	·	·	13	11	1	3	·	-	·	·	6	4				
III	·	·	16	2,2	8	3,8	8	2,0	3	2,3	15	3,1	4	4,8	18	4,1	21	2,6	55,9	22,6	18	15	1	2	·	10	7	1	3	·	-	·	5	7	5				
IV	8	1,6	8	1,5	1	2,0	3	1,3	5	1,6	5	2,2	9	1,6	18	1,5	35	1,0	29,2	8,5	7	8	·	·	·	13	8	·	·	·	-	1	7	6	·				
V	20	1,4	24	1,3	7	1,4	3	1,3	6	1,5	1	6,0	9	2,3	5	1,0	18	1,2	26,5	12,8	20	3	·	·	·	8	5	1	·	·	-	1	3	4	·				
VI	3	1,3	5	1,0	9	2,3	6	1,3	4	1,8	11	3,5	14	2,6	10	1,7	28	1,5	77,5	31,0	7	-	·	·	10	10	8	2	·	·	-	4	8	2	·				
VII	·	·	·	·	·	·	7	1,1	1	1,0	18	2,3	9	1,3	7	1,1	51	0,8	147,2	64,0	16	·	·	·	9	18	18	5	·	·	-	1	6	5	·				
VIII	5	1,2	·	·	1	2,0	5	2,2	4	2,5	16	3,8	16	2,6	28	2,1	18	2,1	131,1	34,0	14	·	·	·	2	15	14	5	·	·	-	4	4	2	·				
IX	6	1,0	1	1,0	1	1,0	2	1,0	6	1,2	21	2,1	19	2,3	12	2,7	22	1,5	95,6	17,6	23	1	·	·	1	17	13	5	·	·	-	2	3	5	·				
X	·	·	·	·	·	·	6	1,2	·	·	30	2,0	6	1,8	13	1,6	36	1,1	6,0	2,6	22	1	·	·	·	3	3	·	·	·	-	·	5	5	·				
XI	3	3,3	5	2,8	1,6	2,0	4	1,2	6	2,0	7	2,4	13	2,7	6	3,3	30	1,7	22,6	7,3	28	9	3	1	·	9	5	·	·	·	-	·	6	17	·				
XII	5	1,0	4	1,2	3	1,7	1	1,0	3	1,3	17	4,1	23	2,8	6	1,8	31	1,8	31,4	6,3	4	2,8	9	4	·	12	7	·	·	·	-	·	3	14	17				
Rok	5,0	1,1	7,1	1,2	4,6	1,4	5,3	1,5	3,9	1,4	23,7	3,2	13,1	2,6	14,9	2,2	31,9	1,8	723,4	64,0	16.VII	-	25	12	22	142	108	20	9	1	-	15	50	78	46				

Duszniki-Zdrój

$H_s = 540$ m $h_w = 16$ m

I	2,5	2,2	6,5	3,8	1,5	3,3	1,5	2,3	1,1	4,4	3,2	3,9	4	2,8	1	1,0	33	2,4	46,2	16,2	6	25	13	8	·	16	10	1	4	·	-	·	5	9	26				
II	2,5	1,8	4,5	2,6	1,5	1,7	·	·	6,5	4,2	38,5	3,8	13,5	3,9	2	1,3	15	3,0	101,1	23,5	15	16	1	·	·	20	18	3	3	·	3	·	3	14	5				
III	1,2	2,8	4	2,6	1	4,0	1	4,0	6,5	6,5	33,5	4,0	6	3,0	4	4,1	25	2,7	100,6	25,6	17	18	2	1	·	15	10	2	2	·	5	1	7	10	9				
IV	12,5	2,6	7,5	2,8	1,5	2,3	1,5	1,7	1,5	1,7	20,5	2,2	7,5	2,3	4,5	2,9	33	1,5	46,8	11,3	24	12	·	·	·	15	8	1	·	·	·	1	4	10	1				
V	2,2	3,1	15,5	4,3	1	3,5	·	·	4,5	3,2	8,5	2,2	6,5	1,5	4	2,8	31	2,1	42,2	12,6	5	10	·	·	-	11	8	1	1	·	1,8	1	1	8	1				
VI	6	2,6	7	3,2	·	·	2,5	2,0	8,5	4,8	13	2,8	4,5	1,8	3,5	2,3	45	1,2	114,7	29,3	30	·	·	·	·	14	12	3	·	·	1	7	8	5	·				
VII	7	1,9	1	4,0	·	·	·	·	3,5	2,9	2,2	2,0	13,5	1,9	2	1,2	44	1,1	319,9	43,7	22	·	·	·	7	23	20	12	·	·	-	7	4	14	·				
VIII	1	1,5	3	2,0	0,6	2,0	·	·	7	2,2	31	2,1	16	2,3	1,5	1,3	33	1,4	119,0	17,4	15	·	·	·	1	19	17	3	·	·	·	1	5	6	·				
IX	1	3,6	1	2,0	·	·	2,6	2,0	10,5	3,5	34,5	3,6	14,5	2,3	1	3,5	25	2,3	44,9	29,4	23	1	·	·	1	20	17	6	1	·	1,9	·	3	7	·				
X	2	1,8	0,5	4,0	·	·	1,6	3,3	2,5	3,2	24	2,6	11,5	3,2	1	2,0	50	1,3	8,5	6,3	20	3	·	·	·	7	2	·	·	·	2	·	5	6	·				
XI	1,0	4,0	11,5	3,3	0,5	2,0	1,6	4,0	4,0	5,5	2,2	5,2	3	3,4	1,5	2,0	25	3,1	27,7	6,7	12	13	2	1	·	15	6	·	5	·	3	·	2	14	1				
XII	9,5	2,5	6,5	2,6	·	·	·	·	5,6	5,4	28,6	4,4	4	2,1	2	1,8	37	2,2	57,9	22,3	8	29	14	4	·	16	11	1	2	·	5	·	4	18	21				
Rok	3,6	2,5	6,8,5	3,1	7,5	1,6	1,2	1,8	7,7,5	3,6	30,8	3,2	10,2,5	2,5	2,8	2,2	39,6	2,0	1131,6	43,7	22.VII	128	32	14	-	189	139	33	18	·	-	1,8	51	121	64				

Polanica-Zdrój

$\varphi = 50°24'$ $\lambda = 16°30'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-3.5	-0.2	-2.1	-2.0	1.1	-5.4	9.1	6	-18.5	17	91	82	88	87	0.5	1.5	0.7	0.9	7.5	7.8	6.1	7.1
II	–	–	–	–	0.8	4.6	2.0	2.4	5.7	-1.2	9.9	2	-9.7	27	91	77	87	85	0.6	2.1	1.0	1.2	8.5	8.1	7.0	7.9
III	–	–	–	–	0.4	6.4	2.8	3.1	8.2	-1.2	14.4	13	-10.3	3	88	67	84	80	1.0	3.7	1.4	2.0	7.1	6.8	5.5	6.5
IV	–	–	–	–	3.9	10.3	5.4	6.2	11.7	1.1	23.6	29	-5.4	15	88	61	84	78	1.1	6.0	1.6	2.9	6.2	7.4	5.3	6.3
V	–	–	–	–	7.7	13.3	8.1	9.5	14.5	3.6	23.8	16	-2.5	7	81	54	81	72	2.0	7.5	2.1	3.9	6.6	7.7	6.1	6.8
VI	–	–	–	–	14.7	20.7	15.0	16.4	22.0	9.0	29.8	11	3.5	1	82	60	83	75	3.2	11.0	3.2	5.8	5.6	6.2	4.9	5.6
VII	–	–	–	–	16.2	20.8	16.0	17.2	22.7	13.2	33.7	5	8.9	18	88	73	92	84	2.4	8.4	1.7	4.2	6.8	7.3	7.0	7.0
VIII	–	–	–	–	12.8	18.3	13.7	14.6	19.9	9.4	27.3	11	3.6	23	92	68	90	83	1.3	7.1	1.7	3.4	6.3	7.5	5.9	6.6
IX	–	–	–	–	9.3	14.9	10.0	11.0	16.1	6.7	26.3	8	-1.9	27	92	70	89	84	1.1	5.5	1.4	2.7	7.3	7.5	5.6	6.8
X	–	–	–	–	8.7	12.6	6.8	8.0	13.6	3.1	19.5	19	-1.6	3	94	69	92	85	0.7	4.8	0.9	2.1	6.8	6.3	3.2	5.4
XI	–	–	–	–	3.5	6.0	4.4	4.6	7.4	1.8	16.6	6	-10.8	30	91	79	89	86	0.8	2.3	1.0	1.4	7.7	8.2	8.1	8.0
XII	–	–	–	–	-2.0	0.4	-0.8	-0.8	1.9	-4.3	11.4	13	-12.6	16	93	84	89	89	0.4	1.1	0.7	0.7	8.1	7.3	7.3	7.6
Rok	–	–	–	–	5.8	10.7	6.8	7.5	12.1	3.0	33.7	5.VII	-18.5	17.1	89	70	87	82	1.3	5.1	1.4	2.6	7.0	7.3	6.0	6.8

Wałbrom

$\varphi = 50°23'$ $\lambda = 19°45'$

I	–	–	–	–	-2.5	0.0	-2.0	-1.6	1.1	-4.9	6.3	2	-18.3	17	–	–	–	–	–	–	–	–	7.9	7.8	6.7	7.5
II	–	–	–	–	0.8	4.5	1.9	2.3	5.6	-0.9	11.0	5	-6.2	23,24	–	–	–	–	–	–	–	–	7.7	7.9	7.0	7.5
III	–	–	–	–	-0.2	5.9	2.4	2.6	7.6	-2.6	15.8	14	-14.1	4	–	–	–	–	–	–	–	–	5.7	5.8	4.8	5.4
IV	–	–	–	–	4.6	11.3	6.8	7.4	12.7	1.6	23.5	30	-5.4	14	–	–	–	–	–	–	–	–	6.8	6.6	5.9	6.4
V	–	–	–	–	8.1	12.7	8.3	9.4	14.2	3.5	22.4	19	-2.2	29,30	–	–	–	–	–	–	–	–	6.0	7.0	4.8	5.9
VI	–	–	–	–	15.2	21.9	15.6	17.1	23.4	8.6	30.5	11	0.7	28	–	–	–	–	–	–	–	–	4.0	5.0	3.9	4.3
VII	–	–	–	–	16.8	21.8	16.1	17.7	23.0	12.0	33.6	5	6.4	29	–	–	–	–	–	–	–	–	6.5	6.4	5.5	6.1
VIII	–	–	–	–	13.2	19.6	13.6	15.0	21.1	9.1	27.8	12	4.9	31	–	–	–	–	–	–	–	–	6.2	6.3	3.6	5.4
IX	–	–	–	–	8.7	15.1	9.9	10.9	16.2	5.5	27.3	9	-1.9	27	–	–	–	–	–	–	–	–	5.8	6.7	5.2	5.9
X	–	–	–	–	5.2	12.9	7.4	8.2	13.8	2.5	20.9	19	-1.6	26	–	–	–	–	–	–	–	–	5.8	5.9	4.2	5.3
XI	–	–	–	–	1.9	6.0	2.7	3.3	7.2	-0.3	17.7	4	-11.1	30	–	–	–	–	–	–	–	–	7.2	6.7	7.4	7.1
XII	–	–	–	–	-2.7	-0.2	-1.6	-1.5	1.3	-5.1	9.9	13	-12.0	11	–	–	–	–	–	–	–	–	7.8	7.6	6.7	7.4
Rok	–	–	–	–	5.8	11.0	6.8	7.6	12.3	2.4	33.6	5.VII	-18.3	17.1	–	–	–	–	–	–	–	–	6.4	6.6	5.5	6.2

Rakitnica

$\varphi = 50°22'$ $\lambda = 18°48'$

I	–	–	–	–	-2.6	0.2	-1.5	-1.4	–	–	–	–	–	–	90	80	88	86	0.5	1.3	0.6	0.8	8.1	7.9	8.5	8.2
II	–	–	–	–	0.6	4.7	2.1	2.4	6.0	-0.7	10.5	16	-7.1	23	92	74	89	85	0.6	2.5	0.8	1.3	8.0	7.0	7.9	7.6
III	–	–	–	–	0.5	7.2	2.9	3.4	9.1	-1.2	16.8	14	-11.5	4	88	58	85	77	0.8	5.0	1.3	2.4	6.8	6.2	6.6	6.2
IV	–	–	–	–	4.8	11.6	6.8	7.5	13.2	2.0	24.1	29,30	-6.1	16	86	53	77	72	1.4	7.8	2.6	3.9	6.2	6.3	6.5	6.3
V	–	–	–	–	8.7	13.6	8.9	10.0	15.2	4.8	24.7	19	-1.9	7	77	52	78	69	2.7	8.3	2.7	4.6	5.5	7.3	6.5	6.4
VI	–	–	–	–	16.1	22.2	16.0	17.6	23.8	10.6	30.9	11	2.1	27	74	51	80	68	4.9	13.7	4.0	7.5	4.8	5.2	5.1	5.0
VII	–	–	–	–	16.9	21.6	17.2	18.2	23.9	13.6	34.7	8	8.2	30	84	64	84	77	3.5	11.3	3.6	6.1	6.6	6.4	6.7	6.6
VIII	–	–	–	–	13.4	19.5	14.0	15.2	21.3	9.8	27.5	11	4.0	23	91	62	88	80	1.5	9.0	2.0	4.2	7.2	5.8	6.0	6.3
IX	–	–	–	–	9.3	16.4	10.5	11.4	16.4	7.1	26.4	9	-1.8	27	91	65	88	81	1.0	6.7	1.5	3.1	6.9	6.7	8.2	7.3
X	–	–	–	–	5.5	13.2	7.5	8.3	14.0	3.3	20.2	19	-1.9	2	92	64	88	81	0.8	5.8	1.3	2.6	7.5	5.9	6.4	6.6
XI	–	–	–	–	3.5	6.9	4.2	4.7	8.0	1.9	18.5	5	-9.6	30	88	73	86	82	1.1	3.4	1.3	1.9	9.2	7.0	8.2	8.1
XII	–	–	–	–	-2.1	0.3	-1.1	-1.0	1.7	-4.0	13.2	13	-11.1	11	89	81	87	86	0.6	1.3	0.8	0.9	7.9	7.3	7.8	7.7
Rok	–	–	–	–	6.2	11.4	7.3	8.0	–	–	34.7	8.VII	–	–	87	65	85	78	1.6	6.3	1.9	3.3	7.1	6.5	7.0	6.9

Ząbkowice

$\varphi = 50°22'$ $\lambda = 19°18'$

I	–	–	–	–	-2.4	0.5	-1.7	-1.3	1.1	-4.6	7.4	2	-19.1	17	83	75	83	80	0.8	1.6	0.9	1.1	7.3	7.0	7.8	7.4
II	–	–	–	–	0.9	6.0	2.1	2.5	5.8	-0.7	10.6	6	-5.8	23	87	70	86	81	0.8	2.9	1.0	1.6	8.6	7.8	7.4	7.9
III	–	–	–	–	0.6	7.2	3.0	3.4	8.5	-1.8	16.5	14	-12.3	4	80	55	75	70	1.3	5.3	1.9	2.8	5.6	4.5	4.7	4.9
IV	–	–	–	–	6.0	12.1	7.3	8.2	13.5	2.6	26.9	30	-7.1	16	80	54	76	70	2.3	8.1	2.8	4.4	6.4	6.1	5.7	6.1
V	–	–	–	–	9.2	13.7	8.6	10.0	15.0	4.7	24.0	19	-1.5	7	73	51	78	67	3.5	8.7	2.7	5.0	6.3	6.8	5.3	6.1
VI	–	–	–	–	17.2	23.0	16.7	17.9	24.2	10.8	32.3	11	2.2	27,28	67	47	75	63	6.9	15.8	4.9	9.2	3.4	4.6	3.5	3.8
VII	–	–	–	–	17.8	22.0	17.1	18.5	23.9	13.6	36.0	8	7.9	29	81	63	84	76	4.7	12.1	3.6	6.8	5.9	6.8	4.8	5.8
VIII	–	–	–	–	14.5	19.8	14.0	15.6	21.5	10.0	28.6	11	4.4	23	87	61	88	79	2.5	9.4	2.0	4.6	6.1	6.4	4.2	5.6
IX	–	–	–	–	10.0	15.2	10.5	11.6	16.8	6.9	27.4	9	-2.1	27	90	65	88	81	1.4	6.7	1.5	3.2	6.5	6.8	6.3	6.5
X	–	–	–	–	5.9	13.2	7.6	8.6	14.1	3.6	21.5	19	-1.1	2,3,5,28	93	63	88	81	0.6	6.2	1.3	2.7	6.3	5.4	4.0	5.2
XI	–	–	–	–	2.7	6.9	3.5	4.2	8.0	1.1	19.2	6	-10.0	30	89	73	85	82	0.9	3.5	1.2	1.9	8.0	6.4	6.7	7.0
XII	–	–	–	–	-2.5	0.1	-1.5	-1.4	1.5	-4.8	12.5	13	-10.9	11	88	81	87	85	0.7	1.3	0.8	0.9	6.3	6.9	5.6	6.3
Rok	–	–	–	–	6.7	11.6	7.2	8.2	12.8	3.4	36.0	8.VII	-19.1	17.1	88	63	83	76	2.2	6.8	2.0	3.7	6.4	6.3	5.5	6.1

Polanica - Zdrój

$H_s = 400$ m $h_w = 10{,}6$ m 1957

MIESIĄC	ROZKŁAD WIATRU (%D, %nD)																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max ≤ 0°	Max ≤ 0°	Min ≤ -10°	Max ≥ 25°	0,1 ≤ n < 1,0	1,0 ≤ n < 10,0	n ≥ 10,0	10 ≤ v < 15	v ≥ 15	≡	≈ 0,5	◔	●	⊞
I	3	2,0	4	4,2	3	4,0	1	4,0	1,5	2,3	13	3,3	22,5	3,5	7	2,9	38	2,0	49,0	6,4	6	25	10	7	·	10	6	·	·	·	11	·	3	17	24
II	3	2,3	1	3,0	1	2,0	4,5	3,1	5,5	3,7	13,6	4,3	15	3,3	13,5	2,4	27	2,2	50,8	12,1	25	18	·	·	·	16	10	2	·	·	6	·	1	16	8
III	9	2,7	3	3,3	4	3,2	2	3,0	5	3,4	6	4,9	18	3,3	5	2,4	39	1,9	68,1	18,2	30	18	2	1	·	13	12	2	1	·	7	1	4	14	10
IV	7	2,9	7	3,0	3	2,3	3	3,0	1,5	3,0	5,5	3,4	8,5	3,0	8,5	2,7	46	1,4	38,5	11,6	7	12	·	·	·	8	7	1	·	·	5	1	3	10	1
V	9,5	2,3	1,6	3,3	5,5	3,3	2	2,5	1	4,0	3	3,0	8,5	3,3	13,5	2,3	34	1,9	22,8	7,3	13	10	·	·	·	7	5	·	·	·	1	2	·	13	1
VI	3,5	2,6	3,5	2,3	·	·	3	2,0	2	5,5	8,5	3,6	17	2,6	21,5	2,2	31	1,7	60,5	19,9	24	·	·	·	8	10	7	3	·	·	6	7	5	9	·
VII	2	3,0	·	·	·	·	1	2,0	3	3,0	5,5	2,6	33	2,7	21,5	2,3	27	1,8	213,3	28,1	2	·	·	·	9	20	18	10	·	·	5	8	2	15	·
VIII	3	3,8	1	2,0	2	2,5	3	3,0	·	·	12,5	3,6	18,5	3,0	15	2,2	38	1,7	71,4	10,2	16	·	·	·	1	17	12	1	·	·	7	6	1	10	·
IX	1	4,0	·	·	0,5	4,0	0,5	4,0	0,5	4,0	1,3	3,4	3,2	3,1	10,5	3,0	32	2,0	97,3	22,5	23	1	·	·	2	19	14	2	·	·	9	·	2	12	·
X	2	2,0	·	·	2	2,0	2	2,5	4	3,4	16,5	3,0	13	3,2	6,5	2,2	47	1,4	9,5	7,0	20	5	·	·	·	2	2	·	·	·	17	1	3	5	·
XI	5,5	4,5	5,5	3,8	1,5	3,3	11,5	3,1	8	3,2	6,5	3,4	23,6	3,6	6	3,2	22	2,6	12,8	4,3	12	10	1	1	·	5	5	·	·	·	11	·	1	20	1
XII	8,5	2,6	2	3,0	·	·	3	3,7	0,5	5,0	11,5	3,3	21	3,5	10,5	2,6	36	1,9	31,9	7,5	8	27	8	3	·	11	9	·	·	·	9	·	2	17	18
Rok	57	2,9	4,3	2,3	22,5	2,2	36,5	3,0	32,5	3,4	11,7	3,5	230,5	3,2	139	2,6	417	1,9	695,9	28,1	2.VII	126	21	12	20	138	107	21	1	·	94	26	27	158	55

Wałbrom

$H_s = 260$ m $h_w = 12{,}5$ m

I	·	·	2	6,0	5	3,8	·	·	2	4,0	23	3,6	18	3,6	2	3,0	41	2,0	28,8	11,2	6	27	9	4	·	14	7	1	·	·	4	·	3	16	24
II	·	·	·	·	6	3,2	6	5,0	10	3,8	12	3,6	19	3,4	4	3,0	27	2,5	30,8	7,6	21	17	3	·	·	14	10	·	·	·	5	·	1	13	7
III	3	1,7	·	·	21	4,6	3	6,3	6	3,2	4	4,0	17	4,4	5	6,2	34	2,8	46,2	23,6	18	22	3	1	·	8	6	1	2	1	2	·	6	9	6
IV	6	2,0	·	·	6	2,5	6	2,7	2	3,0	3	3,3	13	1,8	11	2,6	43	1,2	39,8	16,0	7	13	·	·	·	14	7	1	·	·	2	2	4	11	·
V	12	2,8	5	3,8	10	2,5	4	3,8	2	3,5	·	·	1,5	3,2	4	4,0	41	1,8	28,9	11,7	10	5	·	·	·	10	3	1	·	·	·	1	6	12	·
VI	5	2,0	3	2,0	9	2,3	8	2,5	4	3,5	11	3,8	15	2,9	5	3,2	30	1,9	47,1	21,2	7	·	·	·	11	10	7	1	·	·	·	2	9	4	·
VII	4	2,8	·	·	8	3,0	4	2,5	3	2,0	6	2,5	3,0	3,3	4	1,8	34	1,8	198,6	52,5	8	·	·	·	9	16	12	5	·	·	·	4	2	5	·
VIII	1	2,0	·	·	3	1,3	3	2,3	4	4,0	5	3,0	27	2,4	4	2,5	46	1,3	73,9	16,4	21	·	·	·	4	14	13	2	·	·	2	3	3	4	·
IX	1	2,0	·	·	3	2,0	2	1,5	7	7,7	13	3,1	28	3,4	3	3,0	33	2,0	66,9	13,0	23	3	·	·	2	16	10	3	·	·	3	1	4	8	·
X	·	·	·	·	6	1,7	2	1,5	6	2,3	9	2,8	13	2,8	1	2,0	56	1,0	10,0	5,5	22	7	·	·	·	4	2	·	·	·	9	·	5	6	·
XI	2	8,5	3	3,7	17	1,8	7	3,4	3	2,0	1	1,0	18	3,8	3	5,7	36	1,9	22,6	11,5	28	14	3	1	·	10	5	1	1	·	10	·	5	16	·
XII	7	2,3	2	3,0	5	3,0	4	3,2	2	1,5	19	3,9	16	3,1	3	3,3	35	2,0	37,5	8,1	3	29	10	3	·	12	11	·	2	·	8	·	1	14	6?
Rok	41	2,2	1,5	1,6	99	2,6	49	2,9	51	3,1	10,6	2,9	229	3,2	49	3,3	456	1,8	631,1	52,5	8.VII	137	28	9	26	142	93	16	5	1	45	13	49	118	43?

Rokitnica

$H_s = 300$ m $h_w = 20$ m

I	2,5	1,8	7	3,4	0,5	1,0	2,5	4,2	14,5	2,2	2,8	4,0	21,5	2,9	5,5	4,3	11	2,8	27,9	8,5	6	–	–	–	·	15	8	·	1	1	3	·	·	20	20
II	2	1,5	2,5	2,2	8	2,3	3	3,2	18,5	3,9	2,9	4,2	9	3,8	6	4,6	6	3,5	60,0	13,4	18	14	1	·	·	15	12	1	1	·	2	·	·	10	5
III	6,5	2,1	2,5	2,0	21	6,3	8,6	2,5	7,5	2,6	14	2,9	17,5	3,6	8,5	2,2	7	3,1	42,8	17,5	18	17	1	1	·	11	8	1	4	4	1	1	3	10	5
IV	1,2	1,9	4	1,9	7	1,7	8	3,4	2,5	2,4	6,5	5,3	14	3,1	2,7	2,4	9	2,3	30,1	8,3	7	11	·	·	·	18	7	·	1	·	4	2	3	10	·
V	8,5	3,4	16,5	3,5	9	3,9	3,5	3,7	4	3,9	8	1,7	13,5	3,0	2,1	3,2	9	2,9	46,1	28,9	20	4	·	·	·	9	7	1	·	·	·	4	·	10	·
VI	5,5	2,8	5,5	3,0	7	2,0	3	2,7	11	3,7	16	4,0	16,5	4,2	15,5	2,7	10	3,0	74,4	38,0	7	·	·	·	14	10	8	2	2	2	·	6	3	3	·
VII	2,6	1,0	4	2,6	5,5	2,5	7	2,2	6,5	3,3	13	3,4	27	2,7	20,5	3,3	7	2,7	132,7	50,1	16	·	·	·	13	20	16	3	·	·	·	9	1	9	·
VIII	0,5	1,0	1	2,5	1	2,5	7	2,0	6,5	3,6	15	4,3	29,5	3,0	20,5	3,4	12	2,9	127,5	36,6	14	·	·	·	5	14	12	4	2	1	·	1	1	5	·
IX	3	2,0	0,5	3,0	1	1,0	2,5	4,0	9	3,4	2,9	4,4	19	3,7	2,2	3,3	4	3,5	104,1	18,0	14	2	·	·	2	20	15	5	1	·	3	1	1	12	·
X	3	1,8	3,5	1,1	2,5	1,6	3,5	4,8	1,0	1,8	2,9,5	3,2	14,5	2,6	12,5	3,2	14	2,2	4,5	2,4	22	5	·	·	·	3	2	·	1	·	3	·	·	9	·
XI	4	8,6	6,5	3,2	17,5	3,2	12,5	2,2	1,2	4,1	1,4	3,1	13,5	4,9	3	7,5	7	3,5	17,1	4,5	28	9	2	·	·	8	6	·	3	1	4	·	·	19	·
XII	5	2,3	2	3,0	5,5	3,1	7	2,1	1,5	2,6	3,3	6,2	15,5	2,8	8	3,4	2	3,6	33,0	6,4	14	27	10	4	·	14	9	·	3	1	5	·	1	15	13
Rok	5,5	2,5	5,5,5	2,6	8,5,5	2,5	6,8	2,3	11,7	3,1	2,3,5	3,6	2,1,1	3,4	1,7,0	3,6	9,8	3,0	7,0,0,2	5,0,1	16.VII	–	–	–	3,4	1,5,5	1,1,0	1,7	1,9	1,0	2,5	2,4	1,3	1,3,2	4,3

Ząbkowice

$H_s = 314$ m $h_w = 13{,}5$ m

I	2	2,2	9,5	4,1	3	1,7	1,5	1,3	3	1,7	31,5	1,9	13	2,1	0,5	1,0	29	1,5	19,5	4,4	5	25	9	5	·	12	5	·	·	·	10	·	3	15	20
II	4,5	2,0	2	1,8	9	2,9	1,5	4,3	1,3	2,2	21	2,1	12	4,1	5	2,1	18	2,1	37,7	6,8	21	15	2	·	·	15	9	·	·	·	8	·	·	16	6
III	6,6	2,5	7	2,1	2,4	6,6	2,5	1,8	3,5	2,1	8	3,4	14	3,9	9,5	2,2	18	3,3	49,0	18,1	18	18	3	2	·	11	7	1	3	1	3	·	9	10	4
IV	16,5	2,9	8,5	2,4	11,5	2,9	5	2,1	8,5	5,4	7	2,1	6	1,8	1,9	2,6	16	2,2	33,4	10,5	7	8	·	·	1	15	10	1	·	·	6	2	6	11	·
V	14,5	2,6	2,6,5	4,5	9	3,1	1	3,0	1	3,0	1,5	2,3	10,5	6,8	1,7	2,2	13	2,9	33,5	16,3	20	3	·	·	·	8	4	1	2	·	1	1	4	13	·
VI	10,6	2,7	7,6	3,1	13,6	2,8	2	3,5	3,5	3,1	10	2,6	9	3,7	1,3	2,3	21	2,2	64,9	31,5	7	·	·	·	14	7	7	2	·	·	·	5	8	1	·
VII	8,5	1,6	6,5	2,8	11	2,6	2,5	2,2	3	2,3	12,5	2,8	16,5	2,5	15,5	2,2	16	2,0	14,5,1	49,2	16	·	·	·	13	18	14	4	·	·	2	9	5	8	·
VIII	1,0	1,8	8	2,1	5,5	2,5	3	1,6	2	1,5	14,5	3,7	17	2,1	16	2,2	17	2,0	11,7,8	28,8	14	·	·	·	5	13	12	4	2	2	6	3	4	7	·
IX	10,6	1,9	2,5	2,4	9	1,9	1,5	1,3	4	1,5	24	2,9	16	2,8	12,5	2,5	10	2,2	64,8	19,2	23	2	·	·	2	17	11	2	·	·	4	1	3	10	·
X	6	2,2	5	1,8	14,5	1,6	5	1,7	7	1,6	20	1,7	18	2,0	11,5	2,2	6	1,7	6,9	3,2	22	4	·	·	·	5	2	·	·	·	8	1	4	6	·
XI	4	5,5	12,5	3,7	3,4	2,0	5,5	2,0	3,5	2,6	9	2,4	10,5	3,6	2	11,2	9	2,7	18,5	8,8	28	13	2	·	·	8	4	·	2	1	7	·	8	17	·
XII	1,2	2,5	4,6	3,9	8	2,4	6	1,4	4,5	2,6	2,1,5	2,9	14	1,9	7,5	2,0	15	2,0	29,9	5,8	8	29	11	4	·	14	7	·	·	·	6	·	3	10	10
Rok	10,4,6	2,5	9,9	2,9	1,5,2	2,7	3,7	2,2	5,0,5	2,5	1,8,0,5	2,6	1,5,8,5	2,8	1,2,9	2,9	1,8,7	2,2	6,2,1,0	4,9,2	1,6.VII	1,1,7	2,7	1,1	3,5	1,4,3	9,2	1,5	9	4	8,1	2,1	5,5	1,2,4	3,9

Miechów $\varphi = 50°22'$ $\lambda = 20°02'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.0	0.6	-2.3	-1.5	1.5	-4.8	6.3	6,7	-18.6	17	–	–	–	–	–	–	–	–	8.8	7.4	6.6	7.6
II	–	–	–	–	1.0	5.2	2.6	2.8	6.1	-0.7	10.2	6	-6.0	23,24	–	–	–	–	–	–	–	–	8.3	7.6	7.9	7.9
III	–	–	–	–	0.6	6.6	2.6	3.1	7.9	-2.1	16.4	28	-12.1	4	–	–	–	–	–	–	–	–	5.6	5.7	4.3	5.2
IV	–	–	–	–	5.5	11.7	7.9	8.2	13.3	2.0	24.0	29,30	-4.0	14	–	–	–	–	–	–	–	–	6.3	6.6	6.9	6.6
V	–	–	–	–	9.5	13.3	9.8	10.6	14.6	4.6	22.6	20	-1.4	30	–	–	–	–	–	–	–	–	6.2	7.5	6.4	6.7
VI	–	–	–	–	17.3	22.8	17.6	18.8	23.6	9.4	31.0	30	1.1	27	–	–	–	–	–	–	–	–	4.7	5.4	4.5	4.9
VII	–	–	–	–	18.1	22.2	18.1	19.4	23.6	12.7	35.0	5	7.6	30	–	–	–	–	–	–	–	–	6.4	5.9	6.8	6.4
VIII	–	–	–	–	15.3	20.5	15.5	16.7	21.9	9.3	29.0	12	3.6	24	–	–	–	–	–	–	–	–	4.8	6.1	5.5	5.5
IX	–	–	–	–	9.7	16.1	11.5	12.2	17.1	6.7	27.8	9	-2.4	27	–	–	–	–	–	–	–	–	5.7	6.4	6.0	6.0
X	–	–	–	–	4.2	13.9	7.9	8.5	14.8	2.2	20.8	19	-3.8	3	–	–	–	–	–	–	–	–	6.5	5.4	4.9	5.6
XI	–	–	–	–	1.4	6.5	3.0	3.5	7.4	-0.5	18.6	1	-10.0	22,30	–	–	–	–	–	–	–	–	7.9	7.0	6.7	7.2
XII	–	–	–	–	-2.9	0.5	-4.5	-4.4	1.5	-4.8	7.6	13	-11.0	11,25	–	–	–	–	–	–	–	–	8.2	6.9	6.3	7.1
Rok	–	–	–	–	6.5	11.7	7.7	8.4	12.8	2.8	35.0	5.VII	-18.6	17.1	–	–	–	–	–	–	–	–	6.6	6.4	6.1	6.4

Tarnogród $\varphi = 50°22'$ $\lambda = 22°45'$

I	–	–	–	–	-2.8	-0.8	-2.2	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.4	8.5	8.3
II	–	–	–	–	0.9	4.5	2.0	2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	6.1	6.7
III	–	–	–	–	-0.6	5.6	1.7	2.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.0	3.5	4.3
IV	–	–	–	–	5.8	13.6	7.7	8.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.1	4.5	4.8
V	–	–	–	–	9.5	13.7	9.6	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	6.9	6.6
VI	–	–	–	–	17.3	23.0	16.9	18.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3.2	2.8	2.5	2.8
VII	–	–	–	–	18.2	23.1	17.6	19.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.0	6.1	5.6
VIII	–	–	–	–	15.2	21.0	15.5	16.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.6	4.0	4.4
IX	–	–	–	–	10.8	16.3	11.8	12.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.5	6.0	5.9
X	–	–	–	–	5.9	13.0	7.5	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.4	3.2	4.8
XI	–	–	–	–	1.9	6.1	3.0	3.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	5.8	6.8
XII	–	–	–	–	-3.1	0.2	-1.9	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.4	6.2	6.5
Rok	–	–	–	–	6.6	11.6	7.4	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	5.2	5.6

Lądek - Zdrój $\varphi = 50°21'$ $\lambda = 16°53'$

I	–	–	–	–	-3.2	0.1	-2.0	-1.8	1.4	-5.8	8.9	6	-21.1	17	84	76	82	81	0.9	1.5	1.0	1.1	7.7	7.1	7.1	7.3
II	–	–	–	–	1.4	4.4	2.1	2.5	5.7	-1.3	11.3	5	-11.6	27	83	72	81	79	1.3	2.5	1.5	1.8	8.3	8.8	7.3	8.1
III	–	–	–	–	2.6	6.4	2.7	3.4	7.9	-1.8	14.8	13	-10.0	3	82	63	81	75	1.3	4.1	1.6	2.3	7.5	6.8	4.1	6.1
IV	–	–	–	–	3.6	9.5	5.2	5.9	11.3	0.8	24.2	29	-6.1	15	86	64	84	78	1.3	5.3	1.5	2.7	6.3	8.1	6.0	6.8
V	–	–	–	–	7.2	12.8	7.5	8.8	14.5	3.1	24.6	16	-3.9	7	80	54	80	71	2.2	7.4	2.2	3.9	6.6	7.9	6.0	6.8
VI	–	–	–	–	14.7	20.3	14.8	16.2	22.6	9.1	29.9	11	2.9	27	77	54	80	70	4.0	11.9	3.7	6.5	5.6	6.9	4.8	5.8
VII	–	–	–	–	15.9	20.2	15.8	16.9	21.8	12.3	33.0	5	7.8	22	85	68	87	80	3.1	9.0	2.6	4.9	6.4	7.4	7.4	7.1
VIII	–	–	–	–	12.3	17.9	13.1	14.1	19.6	8.8	27.5	11	2.9	23	90	63	88	80	1.5	8.1	2.0	3.9	6.5	7.8	5.9	6.7
IX	–	–	–	–	9.1	14.2	9.7	10.7	15.5	6.2	24.8	9	-2.8	27	87	65	86	79	1.7	6.0	2.0	3.2	7.0	7.8	6.1	7.0
X	–	–	–	–	6.5	12.3	7.6	8.5	13.5	4.7	19.0	18	-2.2	3	87	83	84	78	1.5	5.5	2.0	3.0	6.4	6.2	3.4	5.3
XI	–	–	–	–	3.4	5.9	4.4	4.5	7.1	1.5	15.7	10	-11.2	30	83	73	84	80	1.5	2.8	1.5	1.9	8.1	8.1	8.8	8.3
XII	–	–	–	–	-1.7	0.2	-1.1	-0.9	1.9	-4.8	10.8	13	-14.3	17	85	80	84	83	0.9	1.5	1.0	1.1	7.6	7.6	7.4	7.5
Rok	–	–	–	–	5.8	10.4	6.6	7.4	11.9	2.6	33.0	5.VII	-21.1	17.1	84	66	83	78	1.8	5.4	1.9	3.0	7.0	7.5	6.2	6.9

Bytom, park $\varphi = 50°21'$ $\lambda = 18°55'$

I	–	–	–	–	-2.0	0.4	-1.0	-0.9	1.4	-3.1	7.1	6	-16.0	17	86	79	84	83	0.7	1.3	0.9	1.0	8.5	8.3	7.1	8.0
II	–	–	–	–	1.4	5.1	2.6	2.9	6.1	0.5	10.5	6	-4.2	28	88	71	84	81	0.8	2.8	1.3	1.6	8.1	7.7	6.5	7.4
III	–	–	–	–	1.4	7.2	4.0	4.2	9.0	0.0	16.7	14	-10.0	1	81	57	75	71	1.3	4.8	2.2	2.8	7.2	5.8	6.5	6.2
IV	–	–	–	–	5.3	11.5	7.9	8.2	13.5	3.4	25.1	30	-2.5	16	85	54	72	70	1.5	7.5	3.6	4.2	7.2	6.8	5.8	6.6
V	–	–	–	–	8.6	13.6	9.7	10.4	15.0	5.8	24.7	19	0.0	7	78	55	76	70	2.6	8.0	3.1	4.6	6.6	7.9	5.5	6.6
VI	–	–	–	–	16.6	22.3	17.1	18.3	24.0	12.3	31.4	11	5.2	28	71	51	74	65	5.6	14.0	5.4	8.3	4.6	5.9	4.9	5.1
VII	–	–	–	–	17.2	21.8	17.7	18.6	23.8	14.7	35.5	6	10.7	29	82	65	82	76	4.0	11.3	4.2	6.5	7.1	8.9	7.1	7.0
VIII	–	–	–	–	13.9	19.6	14.7	15.7	21.3	11.4	28.0	11	7.4	23	88	62	86	79	2.0	9.1	2.5	4.5	7.0	7.4	4.1	6.2
IX	–	–	–	–	9.6	16.4	11.2	11.8	16.6	8.1	27.0	9	-0.1	27	91	63	87	80	1.2	6.9	1.8	3.3	6.7	7.2	6.6	6.8
X	–	–	–	–	6.5	13.1	8.8	9.3	14.1	5.3	20.5	19	-0.8	26	90	63	84	79	1.0	6.0	1.9	3.0	7.6	6.6	4.8	6.1
XI	–	–	–	–	3.8	7.0	4.5	5.0	8.1	2.4	18.8	5	-9.7	30	86	71	84	70	1.2	3.6	1.6	2.1	8.8	7.7	7.2	7.9
XII	–	–	–	–	-1.8	0.5	-0.6	-0.5	2.0	-3.3	13.9	13	-10.7	1	88	80	85	84	0.7	1.4	0.9	1.0	8.6	7.4	6.8	7.6
Rok	–	–	–	–	6.7	11.4	8.1	8.6	12.9	4.8	35.5	5.VII	-16.0	17.1	84	64	84	76	1.9	6.4	2.4	3.6	7.3	7.1	5.9	6.8

Miechów

$H_s = 290\ m$ $h_w = 16\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU °/D, °/mD																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ 0°	Max ≤ 0°	Min ≤ -10°	Max ≥ 25°	≥ 0,1	≥ 1,0	≥ 10,0	≥ 10	≥ 15	=	≥ 0,5	◔	●	⊞
I	4	1,5	6,5	6,8	6,5	4,3	1,5	2,7	5	3,0	9	3,7	34,5	4,9	6	2,7	20	3,2	17,4	4,5	13	26	9	5	-	8	6	-	3	1	-	-	2	17	21
II	3	2,0	3	1,7	12	3,1	12	2,6	4	2,0	13	3,2	14,5	4,8	8,5	2,8	14	2,6	18,2	4,4	25	16	2	-	-	7	7	-	1	1	-	-	1	19	7?
III	4	5,5	9,5	2,9	22	5,0	3,5	2,1	2	2,0	5,5	5,0	15	4,8	8,5	3,2	23	3,2	23,2	8,6	19	22	4	1	-	6	5	-	4	-	-	1	9	10	5
IV	12	2,2	8	2,7	12,5	2,1	3,5	1,6	0,5	3,0	3	2,3	5,6	4,1	2,2	3,6	23	2,1	58,9	20,9	30	11	-	-	-	12	9	2	2	-	-	3	4	14	-
V	8,5	2,5	20,5	3,9	12,5	3,6	2	2,5	0,5	1,0	2	2,0	8,5	5,1	16,6	3,2	22	2,7	36,5	11,6	10	4	-	-	-	8	5	2	3	-	-	1	2	12	-
VI	9	1,7	10,5	2,2	9	2,9	4	2,5	1	3,0	5	5,0	12,5	3,3	16	3,9	23	2,3	34,6	18,8	7	-	-	-	10	9	6	1	1	-	-	3	5	3	-
VII	6,5	2,4	7	3,1	6,5	2,1	3,5	1,6	2	3,0	6,5	3,2	23,5	3,9	17,5	2,9	20	2,4	2400	69,5	16	-	-	-	13	15	12	5	2	-	-	4	2	9	-
VIII	9	2,6	2	1,2	5,5	2,1	0,5	1,0	2,5	1,8	7	3,9	23	3,7	14,5	3,1	29	2,1	68,2	19,8	22	-	-	-	6	14	13	3	2	-	-	-	4	7	-
IX	3,5	3,0	3	1,5	4,5	2,2	3,5	2,4	3,5	1,7	11,5	5,6	30,5	5,2	9	3,3	21	3,2	41,4	7,6	23	2	-	-	2	12	11	-	5	1	-	1	3	7	-
X	2,5	2,6	1,5	2,3	7	2,6	1,6	3,0	2	2,5	4,5	3,2	19	3,7	13	2,3	42	1,6	8,0	4,2	22	11	-	-	-	2	2	-	-	-	-	-	4	9	-
XI	2,5	10,4	17,5	4,0	24,5	1,9	1,5	2,7	-	-	4	2,6	18	4,5	4	5,0	18	2,9	16,0	4,2	29	13	3	-	-	6	6	-	1	-	-	-	5	19	-
XII	7,5	2,6	4	4,6	11	2,4	5	1,4	1,5	4,3	20	3,6	17,5	4,4	8,5	3,4	18	2,8	16,4	4,5	5	28	10	4	-	6	5	-	2	-	-	-	1	14	-
Rok	7,2	3,2	9,3	3,1	133,5	2,6	4,2	2,2	24,5	2,3	9,1	3,6	222	4,4	144	3,3	273	2,6	548,8	69,5	16.VII	130	28	10	31	105	87	15	26	3	-	13	42	140	-

Tarnogród

$H_s = 217\ m$ $h_w = 16\ m$

I	2	1,5	8	3,1	4	1,0	2	2,5	7	2,7	15	3,4	28	2,8	·	·	30	2,0	26,4	-	-	-	-	-	-	4	4	1	2	·	-	·	3	21	-
II	7	1,4	·	·	·	·	2,3	2,9	19	3,5	16	3,0	1	4,0	19	2,2	43,4	11,2	15	-	-	-	-	18	11	1	1	·	-	·	4	14	-
III	13	3,1	4	4,8	3	2,3	7	6,9	7	3,3	6	3,7	16	4,5	7	5,1	30	2,7	16,0	8,2	18	-	-	-	-	5	3	·	3	·	-	·	12	6	-
IV	6	1,8	4	1,2	5	1,4	3	1,3	8	1,6	5	1,7	10	1,8	6	1,5	43	0,8	24,0	13,2	11	-	-	-	-	7	6	1	·	·	-	·	12	9	-
V	13	1,8	10	3,2	4	1,8	1	2,0	·	·	2	1,0	18	1,8	17	2,2	28	1,5	73,1	18,2	7	-	-	-	-	11	10	3	·	·	-	2	6	16	-
VI	4	1,0	·	·	·	·	4	1,5	9	2,2	9	2,7	17	2,5	11	1,7	36	1,4	36,9	21,4	4	-	-	-	-	8	4	1	·	·	-	3	16	1	-
VII	1	1,0	5	1,4	5	1,6	7	1,3	9	1,3	13	1,8	11	1,9	4	2,0	38	1,0	99,8	31,6	16	-	-	-	-	21	14	3	·	·	-	6	7	9	-
VIII	1	2,0	·	·	1	2,0	3	1,7	7	2,1	10	1,4	16	2,1	16	2,2	37	1,2	58,5	24,6	10	-	-	-	-	14	9	1	·	·	-	3	9	6	-
IX	5	1,6	·	·	2	2,0	·	·	1,5	3,3	1,4	3,9	2,4	3,0	6	3,7	24	2,3	115,5	24,7	12	-	-	-	-	14	11	4	2	·	-	·	5	10	-
X	3	2,0	·	·	1	1,0	·	·	1,3	1,5	1,1	2,7	1,9	1,6	4	2,0	1,2	1,0	16,3	6,0	20	-	-	-	-	5	5	·	·	·	-	·	11	8	-
XI	2	4,5	4	1,8	1,5	3,7	1,0	2,0	1,0	1,5	1,0	1,8	1,2	3,9	4	4,2	23	2,1	25,3	8,3	28	-	-	-	-	8	6	·	1	·	-	·	5	16	-
XII	9	2,4	5	2,2	5	2,8	1	2,0	1,5	3,1	1,8	3,5	1,1	3,6	2	1,0	27	2,1	27,9	8,8	8	-	-	-	-	8	6	·	·	·	-	·	7	15	-
Rok	6,8	2,3	4,0	1,5	4,2	1,6	3,8	1,8	12,3	2,1	13,0	2,6	11,3	2,7	7,8	2,5	377	1,7	563,1	31,6	16.VII	-	-	-	-	121	89	15	9	·	-	14	97	131	-

Lądek - Zdrój

$H_s = 495\ m$ $h_w = 14,3\ m$

I	2,5	1,0	17,5	1,3	2	1,0	8,5	1,8	18,5	2,5	17	2,4	10,5	2,3	2,5	1,6	14	1,7	29,4	7,8	15	29	10	8	-	11	9	-	·	·	2	·	2	17	26
II	5,5	1,3	3,5	1,4	4	1,0	5	2,0	21	3,2	23,5	3,3	9	2,4	0,5	2,0	12	2,3	37,5	8,2	25	17	·	1	-	18	9	-	·	·	2	·	2	18	7
III	2,5	1,4	23,5	1,8	8,5	1,4	4,5	3,0	14,5	3,5	16,5	3,4	3,5	4,3	1,5	1,7	18	2,1	53,7	14,2	30	19	2	·	·	12	10	1	3	·	1	1	6	12	7
IV	11	1,4	27	1,4	9	1,1	5,5	1,3	3,5	2,3	3,5	2,6	4	1,2	1,5	1,0	25	1,0	58,5	23,8	7	12	·	·	·	13	6	2	·	·	2	1	2	11	4
V	11,5	1,6	39,6	1,4	6	1,1	5,5	1,0	7	1,4	4	3,4	3,5	2,0	3	1,7	13	1,3	20,2	7,4	5	10	·	·	·	10	6	·	·	·	1	1	1	11	1
VI	1	1,0	30,5	1,2	6,5	1,0	6	3,2	10	2,0	14	1,9	2	3,0	2	1,0	18	1,3	87,8	41,7	24	·	·	·	8	10	8	3	·	·	2	8	6	7	·
VII	6	1,2	19,5	1,2	6,5	1,0	5	1,1	18,5	2,3	12	2,3	2,5	2,2	4	1,5	19	1,3	180,2	23,2	20	·	·	·	7	21	17	8	·	·	·	10	4	17	·
VIII	2,5	1,2	10	1,2	12	1,0	2,5	1,4	16	2,4	17,5	2,4	4	1,2	3,5	1,7	25	1,4	57,9	11,0	21	·	·	·	2	21	12	1	1	1	2	3	4	11	·
IX	3	1,0	9	1,0	6	1,0	4,5	1,8	18	3,6	26	3,0	10	2,0	0,5	1,0	13	2,1	38,1	13,2	23	3	·	·	·	22	17	3	4	1	·	·	2	14	·
X	2	1,0	7	1,1	8	1,0	15,5	1,6	20,5	2,4	18	2,3	5	1,7	1	2,0	16	1,6	6,1	4,4	20	6	·	·	·	5	1	·	·	·	1	·	7	7	·
XI	5	1,6	9,5	1,6	12,5	1,0	8,5	2,0	17	3,1	21	2,7	8	2,1	1,5	3,3	7	2,1	34,2	10,8	11	11	2	1	·	10	7	1	2	1	2	·	2	21	1
XII	4,5	1,6	12	1,4	2	1,0	3	2,8	22	3,2	21	3,5	3	2,0	5,5	1,1	20	2,1	39,3	12,8	3	29	9	4	·	15	9	1	2	·	·	·	4	16	16
Rok	5,7	1,3	20,8,5	1,3	8,3	1,0	7,4	1,9	18,8,5	2,7	19,4	2,8	6,5	2,2	2,7	1,6	200	1,7	690,9	41,7	24.VII	136	23	14	17	168	111	20	12	3	15	24	42	162	62

Bytom, park

$H_s = 300\ m$ $h_w = 22\ m$

I	3	1,3	7	2,9	3	2,0	1	1,0	3,5	1,7	36,5	3,1	1,5	2,2	,5	2,8	19	2,1	30,3	7,7	6	24	9	2	-	14	8	·	·	·	-	·	1	19	-
II	1,6	1,3	4	1,5	4,5	2,3	0,5	3,0	12,5	2,9	32,5	3,1	6,5	2,2	6	4,2	16	2,3	51,9	12,8	18	9	1	·	·	14	9	1	·	·	-	·	·	11	5
III	5,5	2,4	7	2,4	2,0	3,9	2,5	3,0	2	3,0	13	3,1	9,5	3,2	10,5	2,4	23	2,3	52,0	19,9	18	14	2	·	·	11	8	1	·	·	-	1	4	12	5
IV	1,5	2,6	4,5	2,2	6	2,1	6	2,6	4,6	2,3	4	1,5	4,5	1,3	18,5	2,3	27	1,6	36,1	10,6	30	8	·	·	1	11	9	1	·	·	-	3	2	10	·
V	10,5	2,4	1,9	3,1	9	2,8	2	1,5	3,5	2,0	2,5	2,8	6	3,3	14,5	3,2	26	2,1	30,1	12,7	20	·	·	·	·	9	5	1	·	·	-	3	·	10	·
VI	8	3,0	9	2,9	5	1,8	3,5	3,3	9,5	3,3	10,5	3,9	6,5	2,1	12	3,2	28	2,1	68,1	29,7	7	·	·	·	14	9	6	2	1	·	-	6	4	3	·
VII	5,5	1,7	3,5	3,0	7	2,4	3	1,7	4	2,9	10,5	2,9	12	1,7	18,5	3,2	29	1,8	144,7	58,9	16	·	·	·	12	22	19	4	·	·	-	6	2	14	·
VIII	2	2,5	·	·	4,5	2,1	1,5	1,0	1	5,0	14,5	3,2	8	2,8	22,5	3,1	39	1,7	111,1	31,8	14	·	·	·	4	12	12	4	2	2	-	1	·	4	·
IX	4	2,2	1	1,5	3,5	1,7	1	1,0	5,5	3,3	27	3,4	1,5	3,4	10	3,2	23	2,3	94,1	17,1	14	1	·	·	2	17	13	4	2	·	-	2	·	10	·
X	0,5	1,0	2	1,5	4	1,5	3,5	1,1	4	2,8	22,5	3,0	10,5	2,4	7	2,1	39	1,4	59	28	22	1	·	·	·	3	2	·	1	·	-	·	1	7	·
XI	2	5,2	9,5	3,2	19	2,0	6,5	2,1	6	3,1	10,5	3,8	13	2,8	3,5	3,7	20	2,2	20,3	7,7	28	9	2	·	·	7	4	·	1	·	-	·	1	20	1
XII	5	1,8	·	·	5	4,2	3	1,0	10,5	2,6	26,5	3,8	9,5	2,8	9,5	2,1	24	2,2	38,6	8,9	3,14	24	8	1	·	9	8	·	1	1	-	·	1	13	7
Rok	60,5	2,3	66,5	2,0	90,5	2,4	34	1,9	68,3	3,0	210,5	3,1	118	2,5	137,5	3,0	313	2,0	683,2	58,9	16.VII	90	22	3	35	138	103	18	8	3	-	22	46	133	-

Chorzelów

$\varphi = 50°21'$ $\lambda = 21°27'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{a.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.3	0.5	-1.4	-1.2	1.3	-4.1	6.5	9	-16.4	17	87	80	89	85	0.7	1.3	0.5	0.9	7.9	8.2	7.0	7.7
II	–	–	–	–	1.3	4.9	2.4	2.8	6.1	-0.1	10.2	21	-5.0	28	89	77	86	84	0.8	2.1	1.1	1.3	7.4	7.2	6.6	7.1
III	–	–	–	–	-0.3	6.7	2.6	2.9	8.3	-2.0	17.9	30	-13.4	4	85	61	80	75	1.1	4.6	1.7	2.5	5.3	5.0	3.6	4.6
IV	–	–	–	–	5.0	13.7	8.1	8.7	14.9	2.5	26.9	30	-3.3	16	89	54	78	74	1.0	8.7	2.5	4.1	5.6	5.5	4.9	5.3
V	–	–	–	–	9.2	13.8	10.1	10.8	15.1	5.9	23.2	14,20	1.0	7	84	64	82	77	2.1	6.8	2.4	3.8	5.5	7.8	7.1	6.8
VI	–	–	–	–	16.7	24.0	18.0	19.2	25.4	11.5	32.4	12	5.0	27	76	48	74	66	4.8	16.4	5.6	8.9	3.2	4.6	3.2	3.7
VII	–	–	–	–	17.7	24.1	18.5	19.6	25.2	14.0	36.6	5	7.8	4	86	59	83	76	3.1	14.2	4.0	7.1	6.1	5.9	5.8	5.9
VIII	–	–	–	–	14.2	21.3	16.0	16.9	23.0	11.2	34.8	12	5.3	24	90	60	84	78	1.8	11.1	3.1	5.3	4.6	5.5	4.3	4.8
IX	–	–	–	–	10.2	16.7	12.0	12.7	18.0	8.3	28.8	9	-0.2	27	93	66	87	82	0.9	7.0	1.8	3.2	5.0	6.3	6.6	6.0
X	–	–	–	–	5.0	13.8	7.9	8.6	14.8	3.1	20.9	19	-3.2	3	93	64	87	81	0.7	6.1	1.6	2.8	5.2	5.3	4.2	4.9
XI	–	–	–	–	2.2	6.8	3.5	4.0	7.9	0.6	17.7	1,4	-9.8	22	90	75	86	84	0.8	3.0	1.0	1.6	5.7	6.6	6.0	6.4
XII	–	–	–	–	-2.5	0.9	-1.0	-0.9	2.1	-4.7	11.8	14	-11.9	3	88	79	85	84	0.6	1.4	0.9	1.0	6.7	7.4	5.5	6.5
Rok	–	–	–	–	6.4	12.3	8.0	8.7	13.5	3.8	36.6	5.VII	-16.4	17.1	88	66	83	79	1.5	6.9	2.2	3.5	5.8	6.3	5.4	5.8

Prudnik

$\varphi = 50°18'$ $\lambda = 17°34'$

I	–	–	–	–	-2.3	2.0	-2.0	-1.1	–	–	–	–	–	–	85	81	84	83	0.8	1.4	0.9	1.0	6.6	6.1	5.1	5.9
II	–	–	–	–	1.7	6.0	2.6	3.2	–	–	–	–	–	–	85	69	84	79	1.1	3.0	1.3	1.8	6.4	6.4	5.1	6.0
III	–	–	–	–	1.9	7.7	4.1	4.4	–	–	–	–	–	–	81	60	78	73	1.6	4.7	2.0	2.8	5.5	5.0	5.1	5.2
IV	–	–	–	–	5.3	11.0	6.8	7.5	–	–	–	–	–	–	86	63	83	77	1.3	5.8	2.0	3.0	5.2	6.7	5.2	5.7
V	–	–	–	–	8.9	13.9	9.0	10.2	–	–	–	–	–	–	82	62	81	75	2.3	6.5	2.2	3.7	6.8	7.0	4.6	6.1
VI	–	–	–	–	16.4	22.0	16.0	17.6	–	–	–	–	–	–	75	54	80	70	5.0	13.1	4.0	7.4	3.8	4.8	3.4	4.0
VII	–	–	–	–	17.6	21.6	17.1	18.4	–	–	–	–	–	–	84	65	85	78	3.8	10.3	3.3	5.8	6.5	6.6	7.0	6.7
VIII	–	–	–	–	15.0	19.6	14.5	15.9	–	–	–	–	–	–	83	61	85	76	3.0	9.3	2.7	5.0	5.4	6.4	4.5	5.4
IX	–	–	–	–	10.8	15.9	11.3	12.3	–	–	–	–	–	–	84	64	82	76	2.3	7.1	2.5	4.0	6.2	6.5	4.8	5.8
X	–	–	–	–	6.1	14.1	8.2	9.2	–	–	–	–	–	–	90	60	83	78	1.2	7.6	2.0	3.4	5.5	5.7	3.9	5.0
XI	–	–	–	–	4.2	7.2	5.0	5.4	–	–	–	–	–	–	85	72	81	79	1.4	3.4	1.6	2.2	7.2	7.2	7.2	7.2
XII	–	–	–	–	-1.3	2.0	-0.1	0.1	–	–	–	–	–	–	84	78	84	82	1.0	1.8	1.1	1.3	6.6	5.8	5.8	6.1
Rok	–	–	–	–	7.0	11.9	7.7	8.6	–	–	–	–	–	–	84	66	82	77	2.1	6.1	2.2	3.5	6.0	6.1	5.1	5.7

Lipiny

$\varphi = 50°19'$ $\lambda = 18°54'$

I	–	–	–	–	-1.7	0.3	-0.6	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.8	4.9	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.1	7.0	4.5	4.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	6.3	11.4	8.1	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	9.3	13.4	9.9	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16.7	21.9	18.2	18.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	17.1	21.4	18.6	18.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	14.3	19.4	16.2	16.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	10.5	15.2	11.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	7.6	13.1	9.8	10.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	4.4	7.2	5.1	5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.5	0.4	-0.5	-0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	7.2	11.3	8.7	9.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Dąbrowa Górnicza

$\varphi = 50°19'$ $\lambda = 19°11'$

I	–	–	–	–	-1.8	0.7	-1.0	-0.8	4.5	-3.2	7.0	6	-12.0	17	86	76	85	82	0.7	1.6	0.8	1.0	7.1	6.7	6.8	6.9
II	–	–	–	–	1.4	5.3	2.8	3.1	6.1	0.6	10.5	6	-5.0	23	88	74	86	83	0.9	2.5	1.1	1.5	6.5	6.6	6.0	6.4
III	–	–	–	–	1.2	7.4	4.2	4.2	8.9	0.0	16.6	14	-8.2	4	82	58	74	71	1.3	4.9	2.3	2.8	5.5	4.5	4.8	4.9
IV	–	–	–	–	5.4	13.1	8.4	8.6	13.5	3.6	26.0	30	-2.5	15	85	63	72	70	1.6	8.3	3.4	4.4	5.3	5.3	4.7	5.1
V	–	–	–	–	8.5	13.9	10.2	10.7	15.0	5.9	21.9	19	0.5	6	78	53	72	68	2.6	8.4	3.7	4.9	6.1	6.5	4.6	5.7
VI	–	–	–	–	16.3	22.7	17.9	18.7	24.1	12.3	31.2	11	5.9	1	74	51	69	65	4.9	14.3	6.7	8.6	3.4	4.0	3.8	3.7
VII	–	–	–	–	17.1	22.2	18.4	19.0	23.8	14.6	35.6	8	8.4	31	84	63	79	75	3.5	11.9	5.2	6.9	7.1	6.8	6.1	6.7
VIII	–	–	–	–	13.8	19.9	15.5	16.2	21.4	11.8	28.0	11	8.1	31	90	64	83	79	1.7	8.9	3.1	4.8	6.5	7.1	5.5	6.4
IX	–	–	–	–	10.0	15.8	11.6	12.2	16.7	8.3	27.1	9	1.4	27	90	65	84	80	1.3	6.8	2.2	3.4	6.1	5.8	4.8	5.6
X	–	–	–	–	6.5	13.7	9.3	9.7	14.3	5.4	21.1	19	0.3	26	90	62	83	78	1.0	6.4	2.0	3.1	4.6	4.8	3.6	3.9
XI	–	–	–	–	3.4	7.3	4.4	4.9	8.1	2.1	19.1	5	-2.8	30	90	73	86	83	0.8	3.4	1.4	1.9	7.1	6.4	7.1	6.9
XII	–	–	–	–	-1.8	0.6	-0.8	-0.7	1.8	-3.5	13.0	13	-10.0	16	89	80	87	85	0.6	1.3	0.8	0.9	7.2	6.6	5.4	6.4
Rok	–	–	–	–	6.7	11.8	8.4	8.8	12.9	4.8	35.6	8.VII	-12.0	17.1	86	64	80	77	1.7	5.6	2.7	3.7	6.0	5.9	5.2	5.7

Chorzelów $H_s = 170\,m$ $h_w = 16\,m$ 1957

| MIESIĄC | ROZKŁAD WIATRU (%D, %nD) | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | |

Sielec Pińczowski

$\varphi = 50°19'$ $\lambda = 20°25'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.5	0.4	-2.4	-1.7	1.3	-5.4	6.8	6	-16.7	16	–	–	–	–	–	–	–	–	8.1	6.9	5.8	6.9
II	–	–	–	–	0.8	5.1	2.2	2.6	6.3	-0.4	10.8	8	-4.6	23	93	82	91	89	0.5	1.8	0.8	1.0	7.5	7.1	6.1	6.9
III	–	–	–	–	0.2	6.9	2.8	3.2	8.6	-1.7	17.2	14,28	-8.8	4	89	70	84	81	0.7	3.8	1.3	1.9	5.2	4.7	5.4	4.4
IV	–	–	–	–	4.7	12.9	7.2	8.0	14.3	2.2	26.7	30	-4.0	16	91	60	84	78	0.8	7.1	1.7	3.2	5.2	5.8	4.7	5.2
V	–	–	–	–	8.7	14.0	9.6	10.5	15.4	5.1	23.7	16	-0.7	30	85	64	82	77	1.9	7.0	2.3	3.7	5.5	7.2	6.1	6.3
VI	–	–	–	–	16.3	23.3	16.3	18.0	24.9	10.2	32.5	11	2.7	1	–	–	–	–	–	–	–	–	3.9	4.7	3.5	4.0
VII	–	–	–	–	17.5	22.9	17.5	18.8	24.4	13.1	34.6	8	8.4	30	88	67	89	81	2.6	10.6	2.3	5.2	6.1	5.2	6.4	5.9
VIII	–	–	–	–	14.3	21.0	15.1	16.4	22.5	10.1	29.8	12	4.7	24	–	–	–	–	–	–	–	–	4.0	5.2	4.5	4.6
IX	–	–	–	–	9.7	16.4	11.4	12.2	17.6	6.7	28.2	9	-1.4	26	93	68	88	83	0.8	6.4	1.7	3.0	5.6	5.8	5.4	5.6
X	–	–	–	–	4.0	13.8	6.9	7.9	14.5	1.8	22.1	19	-4.1	3	96	68	93	86	0.4	5.3	0.8	2.2	6.9	5.5	3.5	5.3
XI	–	–	–	–	1.3	6.4	2.7	3.3	7.5	-0.3	18.0	1	-5.2	30	94	80	93	89	0.4	2.3	0.5	1.1	8.7	6.9	6.6	7.4
XII	–	–	–	–	-2.9	0.2	-1.8	-1.6	1.2	-5.0	7.8	9	-12.2	24	90	83	90	88	0.5	1.1	0.5	0.7	6.4	6.5	5.4	6.1
Rok	–	–	–	–	6.0	11.9	7.3	8.1	13.2	3.0	34.6	8.VII	-16.7	16.1	–	–	–	–	–	–	–	–	6.1	6.0	5.1	5.7

Bystrzyca Kłodzka

$\varphi = 50°18'$ $\lambda = 16°39'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	7.1	13.2	8.5	9.3	14.8	3.7	24.4	16	-4.3	7	81	56	76	71	2.1	7.3	2.8	4.1	5.0	5.9	5.3	5.4
VI	–	–	–	–	14.5	20.9	15.7	16.7	23.2	9.8	30.4	11	8.3	1	77	53	74	68	3.9	13.0	4.9	7.2	4.7	5.2	5.0	5.0
VII	–	–	–	–	16.3	20.9	16.3	17.4	22.5	13.2	33.3	8	8.3	22	86	68	86	80	2.9	9.3	3.0	5.1	6.3	6.4	6.9	6.5
VIII	–	–	–	–	12.8	18.4	13.9	14.8	19.9	9.4	27.1	11	3.3	23	88	64	85	79	1.9	8.0	2.5	4.1	6.3	6.8	4.9	6.0
IX	–	–	–	–	9.8	14.8	10.4	11.4	16.2	7.2	25.3	9	-2.5	27	86	67	86	80	1.8	8.0	2.0	3.3	6.7	7.0	6.0	6.6
X	–	–	–	–	6.2	12.4	8.0	8.6	13.5	4.5	19.0	18	-2.7	3	87	65	84	79	1.5	5.4	1.9	2.9	6.3	5.6	3.5	5.1
XI	–	–	–	–	3.5	6.3	4.6	4.8	7.5	2.5	15.4	5	-10.3	30	86	76	85	82	1.2	2.6	1.4	1.7	7.8	7.6	7.9	7.8
XII	–	–	–	–	-1.5	0.1	-0.6	-0.6	2.2	-3.5	10.4	13	-12.2	16	90	84	89	88	0.6	1.1	0.7	0.8	8.4	7.5	7.8	7.9
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Głuchołazy – Zdrój

$\varphi = 50°18'$ $\lambda = 17°23'$

I	–	–	–	–	-1.5	1.3	-1.0	-0.6	3.0	-4.0	10.7	6	-18.7	17	84	78	83	82	0.9	1.6	1.0	1.2	6.7	6.5	4.5	5.9
II	–	–	–	–	2.2	6.1	2.9	3.5	7.5	0.0	14.8	3	-8.5	27	82	69	83	78	1.4	3.1	1.4	2.0	6.6	5.9	5.6	6.0
III	–	–	–	–	2.4	7.5	3.9	4.4	9.3	0.0	16.9	14	-6.9	4	78	66	78	74	1.9	4.2	2.0	2.7	5.3	5.7	4.5	5.2
IV	–	–	–	–	5.7	10.4	6.2	7.1	12.0	2.7	24.0	30	-3.3	13	–	–	–	–	–	–	–	–	5.0	6.7	5.3	5.7
V	–	–	–	–	8.8	13.0	8.1	9.5	14.6	5.0	24.9	16	-0.1	8	78	62	83	74	2.7	6.0	1.9	3.5	6.2	7.4	4.9	6.2
VI	–	–	–	–	16.8	21.0	15.2	17.0	23.0	11.3	29.2	11	6.3	28	74	61	83	73	5.3	10.6	3.2	6.4	4.3	4.9	4.5	4.6
VII	–	–	–	–	17.6	21.1	16.2	17.8	22.8	13.7	35.0	5	10.2	25	–	–	–	–	–	–	–	–	6.8	6.5	6.4	6.6
VIII	–	–	–	–	15.1	18.9	13.8	15.4	20.6	10.8	29.2	11	5.7	23	–	–	–	–	–	–	–	–	6.4	7.1	4.4	6.0
IX	–	–	–	–	10.9	15.2	10.6	11.8	16.7	7.9	27.3	8	0.3	27	87	68	86	80	1.9	6.0	1.9	3.5	6.1	6.7	3.8	5.5
X	–	–	–	–	7.1	13.9	8.2	9.4	15.0	5.0	22.5	10,19	0.0	24	89	65	85	80	1.2	6.0	1.8	3.0	5.5	5.4	3.9	4.9
XI	–	–	–	–	4.0	6.8	4.4	4.9	8.2	2.1	17.7	5	-10.1	30	87	76	85	82	1.2	2.8	1.4	1.8	7.2	7.3	6.8	7.1
XII	–	–	–	–	-1.0	1.6	-0.3	0.0	3.1	-3.4	12.4	13	-12.1	17	86	78	87	84	0.9	1.6	0.9	1.1	6.5	5.7	5.3	5.8
Rok	–	–	–	–	7.3	11.4	7.4	8.4	13.0	4.5	35.0	5.VII	-18.7	17.1	–	–	–	–	–	–	–	–	6.0	6.3	5.0	5.8

Urbanowice

$\varphi = 50°18'$ $\lambda = 18°02'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	17.2	22.8	17.7	18.8	24.2	14.3	36.0	8	10.8	28	–	–	–	–	–	–	–	–	6.9	6.5	6.8	6.7
VIII	–	–	–	–	14.4	20.4	15.2	16.3	22.0	11.1	28.7	11	6.2	31	–	–	–	–	–	–	–	–	5.6	6.6	4.6	5.6
IX	–	–	–	–	10.5	16.2	11.7	12.5	17.8	8.1	27.8	9	0.2	27	–	–	–	–	–	–	–	–	6.4	6.9	5.7	6.3
X	–	–	–	–	6.6	13.9	8.8	9.5	15.2	5.0	20.2	9	-1.4	26	–	–	–	–	–	–	–	–	6.2	5.9	3.4	5.2
XI	–	–	–	–	4.4	7.5	5.1	5.5	9.1	2.3	18.4	5	-8.3	30	–	–	–	–	–	–	–	–	7.7	7.2	7.2	7.4
XII	–	–	–	–	4.1	4.2	-0.4	-0.2	3.0	-3.4	11.9	13	-10.5	16,17	–	–	–	–	–	–	–	–	6.9	6.7	6.1	6.6
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sielec Pińczowski

$H_s = 202\ m$ $h_w = 10{,}5\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%] n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	OPAD R 0,1	1,0	10,0	Wiatr v >10	>15	≡	≥5	◔	●	⊞
I	3	1,7	6	6,0	5,5	3,3	2	2,8	0,5	4,0	16,5	3,7	29	3,9	9,5	4,4	21	3,0	22,9	5,6	5,13	26	9	8	·	12	8	·	3	·	3	·	2	11	19
II	4,5	3,0	2	3,0	4	2,8	9,5	4,3	7	2,4	13	4,4	17	4,9	13	3,5	14	3,3	22,4	4,4	2,1	18	2	·	·	12	7	·	1	·	3	·	3	12	7
III	4	4,4	6	4,4	14	8,3	9,5	4,3	2	3,0	4,5	4,7	15,6	5,7	16,5	3,4	21	3,8	21,1	6,9	1,8	21	2	·	·	9	6	·	2	·	1	·	5	5	4
IV	10	3,0	4,5	2,6	4,5	3,0	4	3,2	3	3,3	6	3,2	15	2,9	2,0	3,8	13	2,4	44,0	13,8	7	10	·	·	1	13	9	1	·	·	1	2	8	7	·
V	5	3,8	1,9	4,2	1,0	3,2	4,5	3,0	0,5	3,0	3	3,0	1,5	4,0	1,4	3,7	2,2	2,8	38,5	16,5	1,0	2	·	·	·	6	4	2	·	·	·	·	4	11	·
VI	2,5	2,2	6,6	2,7	7,5	3,0	8,5	4,1	2,5	3,0	6,5	3,7	2,3	4,2	1,2	4,6	2,1	2,8	25,9	10,5	1,9	·	·	·	12	10	5	1	·	·	1	4	7	3	·
VII	3	1,7	1,5	1,7	3	6,0	9,5	2,9	1,5	2,3	16,5	4,6	3,0	3,8	9	4,1	1,9	3,1	174,1	36,0	2	·	·	·	14	16	15	6	1	·	·	4	3	9	·
VIII	2,5	2,2	2,5	3,8	2,5	2,6	3	3,0	4,5	2,8	8	3,8	2,6,5	3,9	16,5	2,8	2,7	2,4	88,5	16,6	1,4	·	·	·	6	11	8	6	·	·	1	1	7	3	·
IX	2	3,5	2	3,5	1	3,0	2	3,0	1,5	3,0	19,5	4,9	3,0,5	5,2	7,5	5,4	2,4	3,6	40,3	8,3	1,7	2	·	·	2	14	8	·	1	·	10	·	3	7	·
X	·	·	0,5	1,0	3	2,3	4	3,2	2,5	3,4	9	4,7	2,1	3,3	8	2,8	4,5	1,8	12,7	4,6	2,0	11	·	·	·	3	3	·	1	·	1,7	·	7	8	·
XI	0,5	3,0	1,0	1,6	1,9	3,9	6	1,0	3,5	2,1	4,5	4,7	1,5,5	7,4	6	9,3	2,5	3,8	19,0	6,1	2,9	13	2	·	·	7	4	·	1	1	1,3	·	2	1,8	·
XII	2,5	1,6	4	3,2	4,5	5,0	8,5	2,5	3	2,7	1,5	5,6	1,9	4,9	1,1,5	5,3	2,5	3,5	21,1	6,3	1,4	27	1,2	3	·	9	5	·	4	2	5	·	6	1,0	5
Rok	39,5	2,7	6,4,5	3,6	7,8,5	3,6	7,1	3,4	3,2	2,7	1,2,2	4,2	2,5,7	4,5	1,4,3,5	4,3	2,8,7	3,0	5,3,0,6,2	3,6,0	2.VII	1,8,0	2,7	1,1	3,5	1,2,2	8,2	1,6	1,7	3	5,5	1,1	5,7	1,0,4	3,5

Bystrzyca Kłodzka

$H_s = 370\ m$ $h_w = 13{,}5\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	1,3	2,5	4,5	2,8	0,5	4,0	2,5	2,2	1,6	3,1	9	4,4	2,5	3,4	5	3,6	3,7	1,9	11,9	3,1	1,9	7	·	·	·	8	6	·	-	-	·	1	2	5	·
VII	1,5	2,7	1,5	1,7	·	·	4,5	2,3	1,3,5	2,1	10,5	2,9	5,5	2,8	8,5	2,9	3,4	1,8	76,2	38,1	2,4	·	·	·	9	8	6	3	1	·	2	5	6	3	·
VIII	7	1,4	1	1,0	0,5	1,0	4,5	2,2	2,2,5	3,0	6,5	2,5	6,5	2,0	1,5	1,3	4,3	1,3	216,8	44,0	2,0	·	·	·	9	2,1	1,8	6	·	·	2	8	4	1,5	·
IX	5,5	1,5	1,5	2,3	1	1,0	4	3,2	2,3,5	3,5	1,6	3,5	10,5	3,0	5	1,9	2,3	2,3	81,9	21,3	9	1	·	·	1	18	14	2	3	1	4	·	2	9	·
X	3,5	1,0	1,5	1,0	1	1,0	6,5	3,1	3,9,5	4,2	5	5,1	4	4,4	2	1,0	3,0	2,5	4,0	3,7	2,0	5	·	·	·	4	1	·	·	·	9	·	4	3	·
XI	1,3	4,1	3,5	3,9	0,5	3,0	5,5	2,2	3,1,5	4,3	8,5	3,8	4,5	3,4	2	3,0	2,1	3,0	9,0	3,6	1,2	1,0	1	1	·	6	3	·	1	1	2	·	1	1,8	1
XII	1,3,5	2,4	2,5	3,6	·	·	4	2,6	3,6	3,7	9,5	3,8	4,5	8,0	5	2,7	1,8	2,9	62,8	16,9	8	2,4	8	2	·	1,3	9	2	1	·	·	·	1	1,8	3,1
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	44,0	20.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Głuchołazy – Zdrój

$H_s = 344\ m$ $h_w = 10\ m$

I	2	4,5	4	5,8	1	1,0	3	1,2	2,1,5	1,3	2,4,5	2,0	1,0	3,0	5	4,2	2,2	1,8	24,7	5,1	2,8	25	8	4	·	11	6	·	·	·	·	·	7	11	1,3
II	1	3,0	·	·	7	2,6	6,5	3,0	2,0	4,4	2,8	2,5	9,5	2,6	2	4,0	1,0	2,7	45,0	10,8	2,5	11	1	·	·	1,5	8	2	3	1	2	·	2	8	4
III	1,5	3,7	3	3,3	12,5	3,2	9	4,2	1,4,5	3,2	1,7,5	3,2	1,0,5	2,1	8,5	3,1	1,8	2,6	40,1	12,1	1,6	1,4	2	·	·	1,2	7	2	2	·	2	1	8	9	4
IV	7,5	2,7	3,5	1,6	5	2,8	·	·	1,7	2,4	4	1,2	1,4,5	1,7	1,9,5	2,0	1,9	1,6	44,3	11,1	7	1,0	·	·	·	11	8	2	·	·	2	·	4	8	1
V	9,5	2,5	1,0,5	2,6	6	2,3	2,5	1,4	7,5	2,1	9,5	1,6	1,4,5	2,3	2,2	2,5	1,1	2,0	38,9	19,1	2,0	1	·	·	·	11	6	1	·	·	·	2	5	12	·
VI	6	1,9	5,5	2,5	4,5	3,4	1	1,0	1,8,5	3,6	1,0	1,8	1,4	2,0	1,4,5	2,3	1,6	2,1	100,2	38,5	2,4	·	·	·	9	1,2	1,0	4	1	1	1	2	8	4	·
VII	6	2,2	2,5	2,8	2	2,0	·	·	6,5	2,5	1,5	2,2	3,0,5	2,0	1,1,5	2,3	1,9	1,7	193,3	36,5	8	·	·	·	9	2,2	1,9	9	·	·	2	7	4	1,3	·
VIII	5	1,6	1	2,0	1	1,0	·	·	1,5	2,2	1,0	2,2	3,6	1,8	1,4	2,2	1,1	1,7	53,8	8,6	1,6	·	·	·	2	1,8	1,3	·	·	·	·	5	5	9	·
IX	5	1,2	1,5	2,0	0,5	2,0	·	·	9	2,3	2,1	1,9	3,1,5	2,5	5,5	1,8	1,6	1,7	89,0	22,7	3	·	·	·	2	1,8	1,3	3	·	·	·	·	2	5	·
X	1,1	1,5	2	1,5	1	1,0	1	3,0	1,2,5	1,7	1,8	2,0	1,1,5	2,0	1,4	2,1	2,2	1,5	9,0	5,2	2,0	·	·	·	·	3	2	·	·	·	4	·	8	4	·
XI	5	5,6	5	2,6	9	2,7	6,5	2,8	2,4,5	2,7	7,5	3,4	1,1	2,8	2,5	4,8	1,9	2,4	2,3,6	7,5	1,1	1,1	1	1	·	8	6	·	1	·	3	·	4	1,7	·
XII	1,5	2,0	3,5	2,4	2	1,0	·	·	1,5,5	4,6	1,0,5	5,3	1,7,5	2,9	9,5	2,0	3,3	2,3	3,4,3	1,4,6	3	2,4	6	2	·	1,0	6	1	4	·	6	·	7	1,2	1,1
Rok	6,1	2,7	4,2	2,4	5,1,5	2,3	2,9,5	1,4	1,8,2	2,8	1,7,5,5	2,4	2,1,1	2,3	1,2,8,5	2,2	2,1,4	2,0	6,9,6,2	3,8,5	2,4.VII	9,6	1,8	7	2,2	1,5,1	1,0,4	2,4	1,1	2	2,2	1,7	6,4	1,1,2	3,9

Urbanowice

$H_s = 200\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20,5	6,8	3,0	-	-	-	-	1,2	6	·	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24,9	6,1	2,5	-	-	-	-	1,3	9	·	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	42,2	10,1	2,8	-	-	-	-	8	8	1	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	33,8	7,8	2,2	-	-	-	-	1,2	8	·	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35,3	23,1	2,0	-	-	-	-	9	6	1	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	59,7	24,8	1,9	-	-	-	-	8	7	2	-	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1,9,0,0	4,4,5	1,6	·	·	·	1,2	2,3	1,7	7	·	·	1	7	5	1,2	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52,8	9,3	2,4	·	·	·	6	1,3	1,0	·	1	·	·	2	5	6	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73,5	13,0	9	·	·	·	2	1,4	1,4	3	2	·	2	·	2	1,1	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8,6	3,0	2,0	2	·	·	·	4	3	·	·	·	1,1	·	4	4	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	16,4	3,3	6	1,1	·	·	·	8	6	·	·	·	3	·	3	1,9	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26,6	6,4	1,4	2,7	8	2	·	9	7	·	3	·	3	·	5	1,3	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5,8,2,1	4,4,5	1,6.VII	-	-	-	-	1,3,3	1,0,1	1,4	-	-	-	-	-	-	-

Gliwice, park — φ = 50°18' — λ = 18°40' — 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	–	–	–	–	-2.1	0.6	-1.2	-1.0	–	-3.1	–	–	-16.2	17	84	79	85	83	0.8	1.4	0.9	1.0	7.7	7.5	6.7	7.3
II	–	–	–	–	1.2	5.4	2.4	2.8	6.4	0.5	10.4	15	-5.0	27	86	70	85	80	1.1	2.8	1.2	1.7	6.8	7.1	6.3	6.7
III	–	–	–	–	1.4	7.6	4.1	4.3	9.3	0.2	17.3	14	-7.9	1	83	64	79	75	1.2	4.4	1.8	2.5	5.1	5.3	4.8	5.1
IV	–	–	–	–	5.1	11.9	7.4	8.0	13.5	3.0	24.6	30	-3.6	15	87	57	76	73	1.3	7.2	2.8	3.8	4.8	6.0	5.4	5.4
V	–	–	–	–	9.0	14.3	9.6	10.6	15.6	6.4	24.9	19	-0.6	7	79	56	78	71	2.5	8.1	2.8	4.5	5.3	7.4	3.7	5.6
VI	–	–	–	–	16.6	23.1	16.1	18.0	24.2	11.8	31.8	30	4.8	28	76	53	81	70	4.7	14.0	3.6	7.4	4.4	5.2	3.5	4.4
VII	–	–	–	–	17.2	22.4	16.8	18.4	24.3	13.8	37.0	5	9.8	30	86	66	88	80	3.1	11.2	2.8	5.7	6.1	6.9	6.0	6.3
VIII	–	–	–	–	14.0	20.4	14.8	16.0	22.1	10.8	28.1	11	6.6	31	91	62	88	80	1.6	9.4	2.0	4.3	5.9	6.0	4.1	5.3
IX	–	–	–	–	10.0	15.9	11.2	12.1	17.2	7.7	26.8	9	-0.5	27	92	67	89	83	1.1	6.5	1.5	3.0	5.5	7.0	6.6	6.4
X	–	–	–	–	6.1	13.8	7.9	8.9	14.7	4.1	21.1	19	-0.1	2,26	93	64	88	82	0.8	6.1	1.3	2.7	5.2	5.4	4.3	5.0
XI	–	–	–	–	3.7	7.4	4.6	5.1	8.7	2.6	18.3	5	-8.7	30	88	74	86	83	0.9	3.2	1.3	1.8	7.6	6.2	6.8	6.9
XII	–	–	–	–	-1.9	0.7	-0.6	-0.6	–	-3.4	–	–	-9.9	1	87	79	86	84	0.7	1.4	0.8	1.0	7.9	7.1	6.2	7.1
Rok	–	–	–	–	6.7	12.0	7.8	8.6	–	4.4	37.0	5.VII	-16.2	17.1	86	66	84	79	1.6	6.3	1.9	3.3	6.0	6.4	5.4	5.9

Mielec, WSK — φ = 50°18' — λ = 21°27'

I	1004.2	1011.9	985.3	1022.8	-2.0	0.6	-1.2	-1.0	1.5	-3.8	6.8	9	-16.1	17	86	79	87	84	0.7	1.4	0.7	0.9	8.3	8.6	7.7	8.2
II	992.1	1009.3	968.9	1013.1	1.7	5.0	2.8	3.1	6.2	0.3	10.3	21	-5.1	24	86	74	83	81	1.1	2.5	1.4	1.7	7.6	8.0	7.0	7.5
III	998.4	1013.4	977.7	1019.6	-0.2	6.7	2.9	3.1	8.2	-2.0	17.8	30	-13.1	4	82	60	77	73	1.2	4.8	2.0	2.7	6.2	5.9	4.3	5.5
IV	987.1	1008.3	973.3	1017.7	5.4	13.5	8.6	9.0	14.7	2.6	26.3	30	-3.1	15,16	86	57	78	74	1.3	8.2	2.7	4.1	6.4	6.4	5.8	6.2
V	994.9	1003.9	983.9	1015.4	9.2	13.9	10.4	11.0	15.3	5.9	23.5	17	0.8	7	85	67	84	79	1.9	6.4	2.1	3.5	6.1	8.5	7.6	7.4
VI	996.7	1010.0	984.0	1016.6	16.8	23.7	18.7	19.5	25.5	12.2	33.3	12	5.7	27	79	52	73	68	4.3	14.9	6.1	8.4	5.1	6.1	4.8	5.3
VII	992.5	1002.5	982.7	1012.5	17.7	23.7	19.0	19.8	25.2	14.7	36.6	5	8.3	4	85	61	83	76	3.4	13.3	4.1	6.9	6.8	7.1	6.9	6.9
VIII	994.8	1004.8	982.7	1014.8	14.3	21.2	16.7	17.2	22.7	11.6	31.0	12	6.6	24	89	63	84	79	1.9	10.2	3.3	5.1	5.7	6.9	4.8	6.8
IX	994.0	1002.6	979.8	1014.3	10.4	16.5	12.5	13.0	17.5	8.7	28.0	9	-0.2	27	91	65	84	80	1.2	7.0	2.3	3.5	6.7	7.4	6.5	6.9
X	1000.6	1010.2	984.5	1021.3	5.6	13.6	8.4	9.0	14.3	3.5	20.7	19	-3.4	3	90	65	85	80	1.0	5.7	1.9	2.9	5.9	6.2	4.0	5.4
XI	1000.5	1018.9	985.6	1021.6	2.5	6.9	3.9	4.3	7.7	0.6	17.3	4	-9.5	22	90	76	86	84	0.9	2.9	1.2	1.7	7.0	6.7	6.2	6.6
XII	995.5	1014.8	961.4	1016.9	-2.2	1.1	-0.9	-0.7	2.2	-4.3	12.0	14	-11.7	24	88	83	86	86	0.7	1.2	0.9	0.9	7.4	8.1	6.3	7.3
Rok	996.5	1018.9	961.4	1017.1	6.6	12.2	8.5	9.0	13.4	4.2	36.6	5.VII	-16.1	17.1	86	67	82	78	1.8	6.5	2.4	3.5	6.6	7.2	6.0	6.6

Spalona — φ = 50°17' — λ = 16°32'

I	–	–	–	–	-3.2	-2.1	-2.9	-2.8	-1.2	-4.1	4.0	9	-13.9	18	–	–	–	–	–	–	–	–	7.6	6.5	7.2	7.1
II	–	–	–	–	-0.2	0.9	-0.1	0.1	1.8	-1.3	6.6	4	-7.3	26,27	–	–	–	–	–	–	–	–	9.4	8.7	9.5	9.2
III	–	–	–	–	0.6	3.9	1.2	1.7	4.6	-1.2	10.9	23	-8.1	1	–	–	–	–	–	–	–	–	6.5	5.2	6.2	6.0
IV	–	–	–	–	2.3	6.8	3.5	4.0	7.8	-0.2	21.2	28	-6.1	14	–	–	–	–	–	–	–	–	5.8	5.3	6.8	5.9
V	–	–	–	–	5.4	8.9	6.0	6.6	9.6	2.6	15.7	31	-2.3	5	–	–	–	–	–	–	–	–	7.0	6.0	6.8	6.6
VI	–	–	–	–	12.7	18.1	14.1	14.8	19.5	9.2	26.7	11	3.6	26	–	–	–	–	–	–	–	–	4.6	4.9	4.3	4.6
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	11.7	16.5	11.9	13.0	17.3	8.0	24.4	11	3.4	27	–	–	–	–	–	–	–	–	5.6	5.5	6.7	5.6
IX	–	–	–	–	8.5	12.6	8.9	9.7	13.4	4.6	19.1	5,6	-2.3	27	–	–	–	–	–	–	–	–	6.1	6.3	5.4	5.9
X	–	–	–	–	4.2	8.8	5.3	5.9	9.6	1.9	15.6	18	-1.5	1	–	–	–	–	–	–	–	–	5.2	5.1	4.6	5.0
XI	–	–	–	–	0.7	2.8	1.0	1.4	3.8	-1.6	11.1	10	-14.7	30	–	–	–	–	–	–	–	–	7.8	7.7	7.4	7.6
XII	–	–	–	–	-3.3	-2.6	-2.9	-2.9	-0.8	-5.7	6.9	13	-13.6	16	–	–	–	–	–	–	–	–	8.4	7.9	8.1	8.1
Rok	–	–	–	–	–	–	–	–	–	–	–	–	-14.7	30.XI	–	–	–	–	–	–	–	–	–	–	–	–

Świętochłowice — φ = 50°17' — λ = 18°56'

I	–	–	–	–	-2.0	0.3	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	6.9	7.2
II	–	–	–	–	1.3	5.1	2.6	2.9	–	-0.2	–	–	-8.1	23	88	72	84	81	0.8	2.6	1.2	1.5	6.5	7.0	5.6	6.4
III	–	–	–	–	1.8	7.4	4.4	4.5	9.3	–	17.0	14	–	–	78	56	73	69	1.6	5.1	2.4	3.0	6.2	5.4	5.0	5.5
IV	–	–	–	–	5.9	11.7	8.3	8.6	13.5	–	26.6	30	–	–	80	53	69	67	2.1	7.9	3.6	4.5	6.0	6.2	6.2	6.1
V	–	–	–	–	8.9	13.5	10.5	10.8	15.2	–	24.9	19	–	–	79	57	74	70	2.5	7.5	3.5	4.5	6.0	7.6	6.2	6.6
VI	–	–	–	–	15.7	22.0	18.8	18.8	23.9	–	30.9	30	–	–	76	52	66	65	4.5	13.4	7.8	8.6	3.8	4.9	3.8	4.2
VII	–	–	–	–	17.3	21.6	18.3	18.9	23.9	–	35.9	5	–	–	82	65	80	76	4.0	11.3	4.9	6.7	6.4	6.5	6.4	6.4
VIII	–	–	–	–	14.3	19.7	15.9	16.4	21.5	–	28.2	11	–	–	87	61	80	76	2.3	9.2	3.8	5.1	6.7	6.4	5.6	6.2
IX	–	–	–	–	10.2	15.5	11.8	12.3	16.8	–	27.0	9	–	–	90	63	84	79	1.2	6.9	2.2	3.4	6.4	7.6	6.4	6.8
X	–	–	–	–	6.5	13.4	8.9	9.4	14.4	–	20.4	10,19	–	–	92	63	86	80	0.9	6.0	1.7	2.9	5.8	6.5	3.8	5.3
XI	–	–	–	–	3.6	7.4	4.8	5.2	9.0	–	18.5	5	–	–	89	74	84	85	0.9	3.3	1.5	1.9	8.5	7.3	7.0	7.6
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	36.9	5.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Gliwice, park

$H_s = 220\ m$ $h_w = 16\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU (%D, %n D)																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max>25°	0.1 ≤	1.0 ≤	10.0 ≤	10 ≤	15 ≤							
I	·	·	·	·	·	·	·	·	2.5	3.8	14	2.3	7.5	1.4	2	1.0	67	0.6	26.8	10.2	6	22	–	3	·	5	3	1	1	·	–	·	3	17	20				
II	·	·	·	·	2	1.0	0.5	1.0	8.5	3.2	14	3.1	3	1.7	1	1.0	55	1.0	52.1	19.0	18	9	1	·	·	10	9	2	·	·	–	·	1	11	5				
III	3.5	1.1	2.5	4.8	1.0	2.3	3.5	1.6	6	1.2	7.5	1.5	3.5	2.4	3.5	1.1	53	0.8	28.7	–	–	16	2	·	·	6	6	1	·	·	–	1	8	11	4				
IV	4.5	1.7	0.5	1.0	1	1.0	1	2.0	6	1.6	5	1.3	3	2.7	1.3	1.5	56	0.6	39.0	6.9	7	8	·	·	·	11	9	·	·	·	–	2	6	8	·				
V	9.5	2.4	1.5	2.3	3.5	3.1	2	1.5	4.5	1.6	3.5	1.1	7.5	1.9	11.5	2.1	36	1.3	37.2	24.4	20	1	·	·	·	7	5	1	·	·	–	2	4	7	·				
VI	4.5	1.7	6	1.2	4.5	1.0	2	1.0	7	1.8	17.5	2.4	8.5	2.0	5	1.5	35	1.1	89.6	32.4	7	·	·	·	11	11	7	3	·	·	–	3	10	6	·				
VII	4	1.2	·	·	4.6	1.6	3.5	1.1	1.2	1.5	12	1.5	17.5	1.7	10.5	1.6	29	1.1	134.7	65.0	16	·	·	·	13	19	13	3	·	·	–	5	4	12	·				
VIII	1.5	1.0	·	·	·	·	0.5	1.0	4	1.5	20.5	1.7	14.5	1.4	8	1.8	44	0.8	87.7	23.1	14	·	·	·	5	14	13	2	·	·	–	2	4	7	·				
IX	3	2.7	·	·	·	·	2	1.0	5	1.9	29	2.2	6	1.9	7	1.9	39	1.1	94.7	16.4	14	1	·	·	2	18	14	4	·	·	–	2	3	12	·				
X	1	1.0	1	1.0	2	1.0	3	1.0	9.5	1.1	20.5	1.5	9.5	1.7	3.5	1.0	43	0.7	6.1	3.2	20	2	·	·	·	4	2	·	·	·	–	·	8	6	·				
XI	5	6.3	7.5	1.4	11.5	1.5	6	1.2	9.5	1.2	11.5	1.7	11	2.0	1	2.5	27	1.4	111.1	5.3	28	9	1	·	·	6	4	·	1	·	–	·	5	17	·				
XII	5	1.4	1.5	1.7	4	1.5	1	1.0	9	2.7	27	2.9	3.5	2.3	6	1.2	36	1.4	31.9	10.0	3	25	–	·	·	7	7	1	·	·	–	·	5	17	–				
Rok	41.5	1.7	3.4	1.1	4.3	1.2	2.5	1.1	83.5	1.9	182	1.9	9.4	2.2	7.2	1.5	520	1.0	636.1	65.0	16.VII	93	–	3	31	118	92	18	2	·	–	17	64	131	–				

Mielec, WSK

$H_s = 168\ m$ $H_b = 170,1\ m$ $h_w = 18\ m$

I	2.5	3.0	6.5	3.8	5	3.3	11	2.3	19	2.8	15.5	2.5	22.5	3.8	2	4.2	9	2.8	21.5	6.6	5	25	7	4	·	10	6	·	1	·	·	·	1	21	23				
II	3	1.5	2	3.5	1.5	2.0	1.8	4.7	27.5	3.7	10	2.6	12.5	3.0	3.5	2.1	6	3.2	29.0	5.2	21	12	1	·	·	12	10	·	·	·	3	·	3	17	7				
III	5.5	2.5	9	1.8	14.5	5.2	6	1.8	10	3.8	8.5	3.6	18	3.7	6.5	4.5	15	3.2	19.8	5.8	18	18	4	2	·	8	6	·	3	·	1	1	5	9	5				
IV	10.5	2.9	6	3.1	5	3.6	5	2.9	9	2.8	9	1.6	9.5	2.3	10	2.5	26	1.8	42.2	12.0	11	12	·	·	1	9	7	1	·	·	7	3	5	12	·				
V	10.5	3.4	14.5	2.8	7	3.4	1.5	3.3	4	1.0	3.5	2.0	16.5	3.1	9.5	3.0	26	2.1	51.3	20.3	9	·	·	·	·	11	7	2	·	·	·	2	·	15	·				
VI	8	2.5	0.5	6.0	2	1.0	1.8	3.3	8.5	3.2	11.5	3.1	19.5	3.1	12	2.7	10	2.7	23.0	10.3	10	·	·	·	17	8	6	1	2	·	·	6	3	4	·				
VII	3	1.2	5	1.4	5	2.3	4	2.9	12	2.1	18.5	3.5	19.5	3.2	8	2.6	18	2.2	134.0	44.1	11	·	·	·	14	16	14	3	1	·	·	9	·	14	·				
VIII	4.5	1.7	0.5	1.0	4	1.2	3	1.3	12	2.3	12.5	2.3	29	2.8	9.5	2.9	21	1.9	121.6	38.5	28	·	·	·	7	11	11	3	2	1	2	6	1	3	·				
IX	4.5	1.2	0.5	1.0	1	1.0	3	1.3	14.5	2.2	20	4.3	28	4.7	0.5	1.0	18	2.9	46.7	10.4	29	1	·	·	2	14	9	1	2	·	4	1	2	11	·				
X	0.5	1.0	0.5	1.0	3	2.0	3	2.3	21	2.5	14	2.5	17	3.1	2	1.5	32	1.7	16.8	6.7	23	6	·	·	·	3	3	·	·	·	6	·	4	6	·				
XI	3.5	11.1	1.3	3.7	12.5	2.4	12	3.8	8	3.6	9	5.1	10	6.4	2	11.0	20	3.6	10.5	5.8	28	10	2	·	·	8	2	·	3	·	7	·	5	15	·				
XII	8	3.6	5	3.5	2	1.5	9.5	4.6	19.5	3.2	20	3.6	9.5	4.0	4.5	3.9	15	3.0	17.9	6.4	13	26	9	4	·	6	4	·	4	·	3	·	3	15	1				
Rok	6.1	3.0	6.3	2.7	6.2.5	2.4	9.4	3.1	16.5	2.8	15.2	3.1	21.1.5	3.6	7.0	3.7	216	2.6	534.3	44.1	11.VII	109	23	10	41	116	85	11	18	1	33	28	52	142	36				

Spałona

$H_s = 810\ m$ $h_w = 13,5\ m$

I	·	·	1.2	4.2	6	1.0	·	·	5.6	4.1	1.2	3.6	4	3.5	3	5.3	·	3.9	44.3	–	–	25	2.0	3	·	18	9	2	3	·	15	·	3	17	26				
II	1.4	3.9	·	·	1	2.0	1.1	7.0	2.0	3.8	2.7	4.1	·	·	1.1	3.0	·	4.2	98.5	14.2	8	18	8	·	·	18	1.4	2	3	1	10	·	·	21	15				
III	1	10.0	3.0	3.2	·	·	·	·	3.7	6.2	2.5	6.6	·	·	·	·	·	5.5	76.4	19.4	18	15	8	·	·	10	10	3	7	3	3	1	4	8	14				
IV	1.3	4.0	4.4	4.0	·	·	·	·	2.5	3.0	6	2.7	·	·	2	3.0	·	3.5	38.6	–	–	11	1	·	·	12	9	1	·	·	7	1	6	11	2				
V	3	4.7	5.1	5.8	·	·	3	2.0	·	·	·	·	·	·	3.6	4.0	·	4.9	39.0	8.6	2.0	6	·	·	·	10	10	·	4	1	4	·	4	10	1				
VI	·	·	1.9	3.9	·	·	7	2.1	3.5	3.9	2.9	3.2	·	·	·	·	·	3.5	79.8	27.2	4	·	·	·	2	11	8	2	2	·	3	5	7	5	·				
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	320.6	40.6	20	–	–	–	–	24	22	14	–	–	–	–	–	–	–				
VIII	2	3.0	7.6	2.0	1.5	2.0	5	1.8	6	3.3	6.3	3.2	·	·	3	2.7	5	2.5	–	–	–	·	·	·	·	–	–	–	2	·	·	1	1	5	·				
IX	1	2.0	·	·	·	·	·	·	9	1.9	7.6	4.1	·	·	4	2.0	·	3.8	230.4	34.8	29	4	·	·	·	21	19	8	2	1	7	2	5	9	·				
X	4	2.0	·	·	·	·	2.1	4.4	9	2.2	5.3	2.7	·	·	6	2.0	·	3.0	7.7	5.0	20	2	·	·	·	6	2	·	·	·	3	·	6	6	·				
XI	5	15.2	2.3	5.9	4	4.8	2	6.0	4.5	6.2	5.0	4.8	0.5	3.0	1	6.0	·	5.6	27.5	8.9	11	19	8	1	·	13	5	·	9	5	12	·	1	18	1				
XII	1.2	3.8	1.3	4.9	2	2.5	5	6.6	11.5	8.9	16.5	5.2	3	4.3	·	·	·	5.4	59.6	27.5	8	30	23	3	·	20	11	1	7	3	6	·	·	17	28				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	40.6	20.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	87				

Świętochłowice

$H_s = 300\ m$ $h_w = 16\ m$ 1957

I	2.5	2.8	5.5	5.5	0.5	3.0	·	·	1	6.0	36.5	4.1	1.9	4.0	5	4.0	23	3.1	23.5	8.0	6	–	–	–	·	14	8	·	3	·	–	·	·	15	–				
II	4.5	1.6	3.5	2.0	3.5	2.3	2.5	2.0	6.5	4.9	30.5	4.3	1.4	3.6	9	4.3	10	3.3	53.0	13.0	18	11	–	·	·	16	11	1	1	·	–	·	1	7	–				
III	9	2.3	9	2.6	2.0	2.8	2.5	2.6	3	2.7	19.5	3.7	8.6	3.9	10.5	3.2	11	2.7	39.7	9.1	18	–	3	–	·	10	8	·	1	·	–	1	5	10	–				
IV	20.5	2.5	4.5	4.6	6	2.2	1.5	1.7	4	2.0	2	2.6	9.5	2.2	11	2.5	31	1.5	36.4	12.4	7	–	·	–	1	11	7	1	·	·	–	3	5	10	–				
V	1.9	2.2	1.4	2.3	1.3	2.3	1	1.0	1	2.0	3	1.8	8.5	2.2	14.5	2.6	19	1.8	23.7	7.3	10	–	·	–	·	8	7	·	·	·	–	1	·	10	–				
VI	5.5	1.9	9.5	1.7	9.5	1.7	3.5	1.3	6	3.9	7	2.8	1.6	2.6	9	2.3	24	1.7	69.1	36.3	7	–	·	–	1.3	9	7	2	1	·	–	5	6	1	–				
VII	8	1.8	4	1.4	6	1.6	5	1.8	2	1.5	12.5	3.1	2.5	2.0	12.5	2.5	19	1.7	139.2	39.4	16	–	·	–	1.3	19	1.8	4	1	·	–	7	5	11	–				
VIII	6.5	3.6	2	4.8	4	2.0	2	1.5	1	2.0	17	3.2	16.5	2.4	18	2.6	26	2.0	112.6	40.5	14	–	·	–	6	12	11	2	2	2	–	4	·	6	–				
IX	9.6	2.2	1	1.0	2	2.0	1	2.0	2	1.6	21	4.5	23.6	4.7	13	3.1	17	3.1	89.5	22.6	23	–	·	–	1	19	15	4	3	·	–	1	1	11	–				
X	2.5	2.8	·	·	7	2.1	1	1.0	2.5	1.4	22	3.1	19.5	3.0	8.5	3.5	30	2.0	9.1	4.2	20	–	·	–	·	3	3	·	2	·	–	·	5	7	–				
XI	4	6.1	7	3.4	24.5	2.2	4	2.1	6.5	2.6	17	3.7	12	4.2	3	4.2	12	2.8	14.2	5.2	28	–	1	–	·	8	5	·	3	·	–	·	4	20	–				
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	–	–	–	–	–	–	–	–	–				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	40.5	14.VIII	–	–	–	34	–	–	–	–	–	–	–	–	–				

Chorzów, park

$\varphi = 50°17'$ $\lambda = 19°00'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max obs.	Data	Min obs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	16.9	21.6	17.9	18.6	23.7	14.7	35.2	8	10.4	29	83	64	79	75	3.6	11.2	4.9	8.6	7.0	6.4	7.6	7.0
VIII	–	–	–	–	14.1	19.2	15.6	16.1	24.3	–	27.8	11	–	–	88	62	79	76	2.2	8.3	4.0	5.0	7.6	6.7	6.0	6.8
IX	–	–	–	–	10.0	15.1	11.7	12.1	16.5	–	26.9	9	–	–	91	66	84	80	1.1	6.3	2.3	3.2	7.4	7.1	7.0	7.2
X	–	–	–	–	6.7	13.2	8.6	9.5	14.1	–	24.0	19	–	–	89	64	87	80	1.1	5.8	1.5	2.8	6.7	5.0	6.9	6.2
XI	–	–	–	–	3.4	6.9	4.3	4.7	7.9	–	18.5	5	–	–	89	74	85	83	0.9	3.3	1.4	1.9	6.1	5.6	6.3	6.0
XII	–	–	–	–	-2.1	0.5	-0.8	-0.8	1.9	-4.2	13.8	13	-10.1	1,11,16	–	–	–	–	–	–	–	–	5.8	6.3	7.1	6.4
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sosnowiec

$\varphi = 50°17'$ $\lambda = 19°06'$

I	–	–	–	–	-1.7	0.9	-0.9	-0.6	2.8	-3.5	7.6	6	-15.7	17	87	81	86	85	0.7	1.3	0.8	0.9	8.0	7.4	7.3	7.6
II	–	–	–	–	1.4	5.6	3.7	3.1	7.9	0.3	12.6	15	-5.3	23	87	71	83	81	0.8	2.8	1.1	1.6	8.4	7.1	8.5	8.0
III	–	–	–	–	1.2	7.8	4.2	4.4	9.9	-0.5	17.4	14	-7.4	4	82	59	78	73	1.3	5.1	1.9	2.8	6.3	5.4	6.4	6.0
IV	–	–	–	–	5.7	12.5	8.2	8.6	–	3.1	–	–	-3.3	16	84	54	77	71	1.6	8.4	2.8	4.3	6.0	7.0	7.1	6.7
V	–	–	–	–	9.0	14.6	10.3	11.0	–	5.8	–	–	0.6	7	77	54	72	68	2.8	8.9	3.7	5.1	6.3	6.5	6.3	6.4
VI	–	–	–	–	11.1	23.4	18.5	19.4	25.0	12.2	32.5	11,30	5.5	28	–	–	–	–	–	–	–	–	5.0	5.3	6.3	5.5
VII	–	–	–	–	17.7	22.4	18.6	19.3	25.4	14.3	36.7	5,6	10.0	29	–	–	–	–	–	–	–	–	6.7	6.6	6.7	6.7
VIII	–	–	–	–	14.5	20.1	16.1	16.7	–	–	–	–	–	–	85	63	82	77	2.5	9.3	3.4	5.1	6.0	5.7	4.0	5.2
IX	–	–	–	–	9.9	16.2	11.7	12.4	–	8.4	–	–	0.4	27	–	–	–	–	–	–	–	–	5.9	7.1	5.6	6.2
X	–	–	–	–	5.9	13.5	8.6	9.2	–	3.9	–	–	0.5	26	92	66	90	83	0.8	5.7	1.2	2.6	4.6	4.8	2.7	4.0
XI	–	–	–	–	3.6	7.4	4.5	5.0	8.7	1.7	19.4	5	-7.0	30	91	77	87	85	0.8	3.0	1.1	1.6	8.3	6.9	7.5	7.5
XII	–	–	–	–	-2.2	0.5	-0.8	-0.8	2.0	–	12.0	13	–	–	89	82	86	86	0.6	1.3	0.8	0.9	8.3	6.2	5.8	6.8
Rok	–	–	–	–	6.8	12.1	8.5	9.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.2	6.4

Borusowa

$\varphi = 50°17'$ $\lambda = 20°47'$

I	–	–	–	–	-2.5	0.3	-2.1	-1.6	1.2	-5.0	6.8	7	-13.8	23	87	79	88	85	0.7	1.3	0.6	0.9	8.4	7.0	8.3	7.9
II	–	–	–	–	1.0	5.2	2.9	3.0	6.5	-0.3	12.0	6	-4.4	28	89	77	87	84	0.8	2.2	1.0	1.3	8.4	6.3	7.4	7.4
III	–	–	–	–	0.0	6.8	3.1	3.2	8.6	-1.7	17.0	30	-9.9	4	85	58	78	74	0.9	4.8	1.3	2.5	6.0	5.5	5.8	5.8
IV	–	–	–	–	5.5	12.9	8.3	8.8	14.1	2.2	25.1	30	-3.9	16	85	55	78	73	1.4	7.8	2.0	3.9	6.1	5.0	6.9	6.0
V	–	–	–	–	8.4	13.8	10.4	10.8	15.2	5.3	23.6	20	-1.0	30	86	62	79	76	1.6	7.2	2.8	3.9	–	–	–	–
VI	–	–	–	–	16.7	23.2	17.3	18.5	24.4	10.3	30.8	30	4.0	1	82	53	80	72	3.4	13.3	4.2	7.1	–	–	–	–
VII	–	–	–	–	17.4	23.1	17.8	19.0	24.4	13.8	34.8	8	9.0	30	86	61	85	77	2.8	12.7	3.5	6.3	–	–	–	–
VIII	–	–	–	–	14.6	21.0	16.3	17.0	22.4	10.9	30.6	12	5.5	24	90	60	84	78	1.8	10.7	3.0	5.2	–	–	–	–
IX	–	–	–	–	9.9	16.3	12.1	12.8	17.5	7.5	27.5	9	-0.5	26	93	63	85	80	0.8	7.1	2.2	3.4	6.0	5.5	6.1	5.9
X	–	–	–	–	4.8	13.6	8.0	8.6	14.6	2.8	24.5	19	-4.8	3	–	–	–	–	–	–	–	–	8.1	4.5	4.2	4.9
XI	–	–	–	–	2.4	6.8	3.5	4.0	7.7	0.6	18.6	7	-9.3	30	–	–	–	–	–	–	–	–	8.0	6.4	7.1	7.2
XII	–	–	–	–	-2.5	0.4	-1.2	-1.1	1.7	-4.7	10.0	14	-11.8	24	–	–	–	–	–	–	–	–	8.1	6.6	8.1	7.6
Rok	–	–	–	–	6.3	12.0	8.0	8.6	13.2	3.5	34.8	8.VII	-13.8	23.1	–	–	–	–	–	–	–	–	–	–	–	–

Zakrzów

$\varphi = 50°15'$ $\lambda = 18°10'$

I	–	–	–	–	-2.1	0.8	-1.2	-0.9	1.7	-4.5	9.0	6	-18.2	17	88	81	86	85	0.7	1.3	0.8	0.9	7.3	6.6	6.4	6.8
II	–	–	–	–	0.9	5.7	2.4	2.8	6.4	-1.0	10.6	14	-10.7	27,28	86	74	86	82	0.9	2.6	1.0	1.5	6.8	7.2	5.4	6.5
III	–	–	–	–	1.7	8.2	4.2	4.5	9.5	-0.8	17.7	14	-10.2	1	83	59	79	74	1.3	5.0	1.8	2.7	6.4	5.7	6.5	5.9
IV	–	–	–	–	5.5	12.0	7.4	8.1	13.1	1.8	25.4	30	-5.1	16	86	57	79	74	1.4	7.2	2.3	3.6	6.1	6.9	5.8	6.3
V	–	–	–	–	9.4	14.6	9.6	10.8	15.7	4.7	25.5	19	-1.3	7	–	–	–	–	–	–	–	–	6.7	6.9	5.4	6.0
VI	–	–	–	–	15.2	22.5	17.0	17.9	24.0	9.9	30.6	30	3.3	27	83	56	79	73	3.1	12.5	4.3	6.6	4.2	4.7	4.1	4.3
VII	–	–	–	–	16.7	22.6	17.9	18.8	23.9	13.5	36.2	8	9.4	30	–	–	–	–	–	–	–	–	6.7	6.4	6.6	6.6
VIII	–	–	–	–	14.5	20.2	15.1	16.2	21.4	10.3	27.7	11	5.2	25,31	–	–	–	–	–	–	–	–	5.8	6.6	4.4	5.5
IX	–	–	–	–	10.5	16.0	11.5	12.4	17.1	7.2	26.8	9	-0.6	26	88	66	84	79	1.6	8.5	2.2	3.4	6.6	6.7	6.0	6.4
X	–	–	–	–	6.6	13.8	8.4	9.3	14.7	3.7	19.9	19	-1.7	24	–	–	–	–	–	–	–	–	6.5	5.8	3.1	5.1
XI	–	–	–	–	3.8	7.7	4.8	5.3	8.4	1.3	18.2	8	-9.0	30	–	–	–	–	–	–	–	–	8.1	7.1	7.1	7.4
XII	–	–	–	–	-1.4	1.4	-0.6	-0.5	2.1	-3.9	12.5	13	-11.7	17	88	82	88	86	0.6	1.4	0.7	0.9	7.1	6.1	6.8	6.7
Rok	–	–	–	–	6.8	12.1	8.0	8.7	13.2	3.5	36.2	8.VII	-18.2	17.1	–	–	–	–	–	–	–	–	6.4	6.4	5.5	6.1

Uwaga. W okresie 2.VI. – 20.VII. obserwacje we wszystkich trzech terminach wykonywano o godzinę za wcześnie.

Chorzów, park

$H_s = 316$ m — $h_w = 16$ m — 1957

MIESIĄC	ROZKŁAD WIATRU (°D, °mD)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C					Temperatura T				Opad R			Wiatr v						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	Średnia prędkość	Suma	Max	Data	Min < 0°	Max < 0°	Min < -10°	Max > 25°	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	v ≥ 10	v ≥ 15	=	≥ 25°	◔	●	⊠
I	–	–	·	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	166	7.2	6	–	–	–	–	6	5	·	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	456	11.6	18	–	–	–	–	12	7	1	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.9	9.8	18	–	–	–	–	7	7	·	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.8	11.2	7	–	–	–	–	11	4	1	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	19.3	8.4	20	–	–	–	–	6	4	·	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	58.0	22.0	7	–	–	–	–	10	6	2	–	–	–	–	–	–	–
VII	10	2.2	6.5	1.9	6	3.1	10	3.6	4.5	3.1	13	3.8	21	3.6	12	3.8	10	2.9	132.2	41.8	16	·	·	·	12	20	14	4	1	·	–	7	·	14	–
VIII	7.5	3.6	3.5	3.0	1	1.0	5.5	2.5	4.5	3.3	14.5	5.6	21.5	3.3	17	3.6	18	3.0	125.6	50.5	14	–	·	–	4	14	11	2	3	2	–	1	·	6	–
IX	5	3.8	3	2.6	1	1.0	5.5	2.5	6.5	3.9	19.5	5.3	21.5	5.1	14	5.2	17	3.8	86.7	18.8	23	–	·	–	2	17	14	3	2	·	–	1	·	10	–
X	7	2.1	1.5	1.0	3	1.3	10	1.9	5	1.6	27	3.0	18	2.6	11.5	2.4	10	2.2	8.9	4.0	22	–	·	–	·	4	3	·	·	·	–	·	·	5	–
XI	4	12.4	4.5	6.0	22.5	4.1	20	3.2	11.5	3.9	9.5	3.8	13	5.7	4	6.1	1	4.6	16.6	7.7	28	–	3	–	·	8	4	·	3	·	–	·	8	14	–
XII	9.5	2.2	5.5	1.3	6.5	4.3	9.5	3.6	5	6.9	29	5.1	17	5.9	11	5.0	·	4.6	29.1	5.2	14	28	11	3	·	14	12	·	6	3	–	·	5	11	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	600.3	50.5	14.VIII	–	–	–	–	129	91	13	–	–	–	–	–	–	–

Sosnowiec

$H_s = 250$ — $h_w = 17$ m

I	·	·	6.5	3.9	1.5	3.7	1	2.0	·	·	3.0	2.6	1.0	3.4	6	4.6	39	1.8	30.0	6.7	27	24	5	3	·	8	8	·	2	·	6	–	3	17	2.0
II	3.5	2.0	·	·	4	1.5	3	1.7	12.5	2.9	2.5	2.5	1.3	3.1	6	1.8	17	2.0	49.9	8.1	18	12	·	·	·	13	10	·	·	·	3	–	·	13	6
III	4.5	1.4	3	3.2	15.5	3.0	12	2.0	3.5	1.0	17.5	2.0	14.5	3.8	8.5	2.5	16	2.1	43.8	12.6	18	14	·	·	·	9	8	1	·	·	1	–	7	14	4
IV	14.5	2.3	7	1.7	4	1.0	10.5	1.8	5.5	2.5	7	2.1	8.5	1.9	16	2.0	17	1.6	30.8	10.6	7	5	–	·	–	8	6	1	·	·	3	–	4	13	·
V	7.5	1.5	2.0	2.9	8.5	2.9	9	2.4	4.0	1.4	3	1.7	5	2.6	2.3	2.3	7	2.2	25.8	8.5	20	·	–	·	–	7	5	·	·	·	1	–	3	12	·
VI	5	1.8	3.5	1.9	9.5	1.6	6	1.3	10.5	1.5	6.5	2.4	2.1	1.9	1.9	1.9	9	1.6	92.7	18.3	7	·	·	·	1.5	9	8	5	·	·	·	–	5	6	·
VII	6.5	1.9	3	1.7	4	2.5	4.5	2.2	5	1.8	2.2	2.5	2.6.5	2.7	8.5	2.5	13	2.1	96.3	27.2	8	·	·	·	1.4	13	12	3	·	·	4	–	1	12	·
VIII	3	4.3	4.5	3.0	6.5	3.6	2	4.0	4.5	3.1	14	4.5	21	3.0	16.5	2.4	21	2.6	115.4	34.6	14	–	–	–	–	12	12	3	2	2	11	–	2	1	·
IX	6	3.1	3.5	2.3	1.5	1.0	5	1.4	7	2.7	17.5	4.0	21	4.1	7.5	3.7	21	2.6	80.5	11.1	29	·	–	·	–	20	20	2	1	·	9	–	1	6	·
X	3.5	2.7	0.5	1.0	3	2.0	4	2.2	8.5	2.8	11	3.4	9	2.4	7.5	2.9	4.6	1.4	11.3	4.2	20	·	–	·	–	5	4	·	·	·	16	–	9	5	·
XI	3.5	12.4	2	5.8	1.8	2.9	7.5	1.7	10.5	2.1	5.5	4.1	14	6.4	4	7.6	2.5	3.2	49.9	7.2	28	11	2	·	·	5	5	·	4	2	11	–	2	19	·
XII	1.0	1.8	·	·	·	·	1	3.0	5	2.2	20.5	3.7	18.5	4.5	4	3.1	3.4	2.2	34.5	6.6	13	–	11	–	·	11	10	·	4	2	25	–	2	13	3
Rok	67.5	2.9	52.5	2.3	7.6	2.1	65.5	2.1	82.5	2.0	179.5	3.0	182	3.3	124.5	3.1	26.5	2.1	630.9	34.6	14.VIII	–	–	–	–	120	108	15	13	6	90	–	39	131	33

Borusowa

$H_s = 170$ m — $h_w = 16$ m

I	2.5	2.6	7.5	3.5	·	·	1	4.0	7	3.0	11.5	3.4	20.5	4.7	7	4.4	36	2.4	24.1	7.6	5	26	10	5	·	8	7	·	1	·	2	·	1	20	2.1
II	5	4.1	0.5	2.0	1.5	2.0	7	3.6	8	4.2	8.5	5.5	20.8	4.4	2	5.2	31	2.7	24.2	7.4	21	15	1	·	·	10	8	·	2	1	1	·	1	12	3
III	7.5	4.3	7.5	2.7	15.5	4.0	4	4.0	5.5	2.4	8	3.4	15.5	5.7	8.5	4.2	21	3.2	16.3	7.1	19	20	3	·	·	8	4	·	2	·	5	1	5	12	·
IV	1.4	3.3	2	2.8	5	2.0	3.5	3.7	4.5	2.2	1	4.0	11.5	3.4	7.5	2.9	4.1	1.7	44.3	11.3	7	7	·	·	1.4	14	10	1	·	·	3	2	6	12	·
V	15.5	1.9	1.2	1.9	4.5	3.1	2	2.0	2	3.0	·	·	9.5	3.7	11.3	3.3	3.6	1.8	48.1	13.3	20	1	·	·	·	8	8	2	·	·	·	1	–	–	·
VI	1.3	3.1	·	·	4	1.2	2	2.5	5	3.0	2.5	3.2	2.3	3.7	4.5	2.3	3.6	1.9	48.9	38.2	22	·	·	·	1.3	7	6	1	1	·	·	5	–	–	·
VII	4.5	2.2	1	1.5	2.5	1.8	1.5	2.0	9	2.8	2.5	3.4	2.6	3.4	5	3.2	4.1	1.7	140.1	54.4	16	·	·	·	1.3	17	15	3	·	·	·	7	–	–	·
VIII	5	1.8	1	2.0	6.5	1.9	1	2.5	4.5	1.3	5	2.4	28.5	3.7	15.5	3.8	2.9	2.2	73.5	21.0	28	·	·	·	6	10	8	3	2	·	2	3	–	–	·
IX	5.5	2.8	2	2.0	·	·	0.5	4.0	3.5	2.3	11	4.8	2.9	5.1	4.5	4.2	3.4	2.8	29.4	6.2	29	2	·	·	2	14	9	·	3	·	7	·	3	8	·
X	4	2.0	1	2.5	4.5	1.9	2	2.8	7.5	2.7	3.5	2.6	18.5	3.7	3	3.2	4.9	1.4	12.9	5.1	22	5	·	·	·	3	3	·	·	·	13	·	6	5	·
XI	0.5	10.0	6	3.8	1.8	2.8	5.5	4.5	7.5	3.7	·	·	2.0	6.6	5.5	5.8	2.7	3.3	3.8	2.0	28	11	3	·	·	4	2	·	5	·	8	·	4	16	·
XII	2.5	2.6	0.5	4.0	8	3.6	3	3.5	4	3.0	12	3.6	16	4.8	7	6.9	4.0	2.4	19.6	6.4	14	26	10	3	·	6	5	·	3	1	3	·	2	19	1
Rok	79.5	3.4	41	2.4	70	2.0	33	3.3	65	2.8	65.5	3.0	238.5	4.4	81.5	4.2	42.1	2.3	479.2	54.4	16.VII	113	27	8	35	109	85	10	18	2	44	19	–	–	25

Zakrzów

$H_s = 217$ m — $h_w = 13$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	22.6	7.8	30	25	9	5	·	8	5	·	–	–	1	·	2	12	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.2	16.0	25	15	1	2	·	12	10	1	–	–	1	·	1	9	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	37.7	7.1	28	17	1	1	·	10	9	·	–	–	1	1	7	11	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.3	9.3	22	10	·	·	2	9	6	·	–	–	1	·	3	9	–
V	2.1	3.2	5	3.0	3.5	2.7	1.5	1.6	2	2.5	1.5	3.3	16	1.8	25.5	4.0	17	2.5	25.9	11.5	20	5	·	·	1	7	6	1	·	·	·	3	1	8	–
VI	8	3.0	8	1.5	9.5	2.5	10.5	2.1	10.5	3.2	3.5	3.7	2	5.0	8	5.1	3.0	2.0	70.0	19.6	9	·	·	·	1.3	9	7	4	1	·	2	5	5	2	–
VII	19.5	2.5	3.5	1.1	4	1.1	5.5	2.1	12	1.8	0.5	2.0	6	2.0	18	2.3	2.4	1.6	132.0	36.4	16	·	·	·	1.3	19	13	5	·	·	2	5	4	13	–
VIII	20.5	3.0	1.5	1.0	5.5	1.5	5.5	3.2	8	3.2	2	4.7	9.5	2.6	12.5	3.3	2.8	2.0	54.3	7.6	10	·	·	·	5	12	11	·	·	·	1	1	4	6	–
IX	14.5	3.7	·	·	·	·	4	3.1	12.5	3.7	10.5	3.0	13.5	2.5	11	3.1	2.4	2.4	73.7	14.1	2	2	·	·	2	18	13	3	1	·	3	1	2	10	–
X	7.5	3.7	2	1.2	1.5	1.3	3	2.0	2.2	3.2	9	3.4	7.5	2.5	7.5	3.3	3.3	2.0	6.3	3.5	20	5	·	·	·	5	2	·	2	·	10	·	3	4	–
XI	8	8.4	3	4.0	11.7	2.6	6.5	2.3	1.6	2.4	3.5	2.7	7	2.4	8.5	4.0	2.7	2.5	16.9	5.5	2	10	1	·	·	8	5	·	2	·	5	·	2	18	–
XII	4.1	3.0	3	1.8	7.5	2.3	4	3.6	26.5	4.0	5.5	5.2	6	3.2	8.5	2.9	2.1	2.6	34.4	11.0	4	30	9	3	·	10	7	1	1	·	2	·	3	12	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	560.3	36.4	16.VII	119	21	11	36	127	94	15	–	–	29	16	37	114	–

Leżajsk

$\varphi = 50°15'$ $\lambda = 22°25'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δm				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.9	-0.4	-2.0	-1.8	0.6	-4.6	6.2	9	-13.9	17	–	–	–	–	–	–	–	–	7.9	7.9	7.5	7.8
II	–	–	–	–	1.7	4.7	2.4	2.8	6.2	0.3	11.4	19	-6.4	28	–	–	–	–	–	–	–	–	8.3	8.0	6.5	7.6
III	–	–	–	–	-0.4	5.9	2.6	2.7	7.8	-1.8	17.1	30	-12.5	4	–	–	–	–	–	–	–	–	4.7	5.6	4.1	4.8
IV	–	–	–	–	5.3	13.6	8.8	9.1	15.0	3.3	26.2	30	-1.9	18	65	51	73	70	1.5	9.1	3.5	4.7	5.9	6.2	5.1	5.7
V	–	–	–	–	9.1	13.6	10.4	10.9	15.3	6.7	24.1	18	0.3	7	85	65	79	76	1.9	6.6	3.0	3.8	6.7	8.2	7.5	7.5
VI	–	–	–	–	16.7	23.3	18.2	19.1	24.9	11.8	33.1	12	4.6	7	75	51	72	67	4.2	14.6	6.0	8.3	3.8	5.5	4.9	4.7
VII	–	–	–	–	17.7	23.3	18.9	19.7	28.2	14.6	36.7	5	8.3	4	84	62	79	75	3.5	12.5	5.1	7.0	6.9	6.4	7.2	6.8
VIII	–	–	–	–	14.5	20.8	16.5	17.1	22.7	12.2	31.7	14	6.3	31	88	61	82	77	2.0	10.4	3.6	5.3	6.0	6.4	5.3	5.9
IX	–	–	–	–	10.5	16.5	12.4	12.9	18.0	9.0	27.9	9	-0.1	27	91	63	84	79	1.1	7.2	2.2	3.5	7.3	6.8	6.8	6.9
X	–	–	–	–	5.1	13.3	8.0	8.6	14.3	3.9	20.8	19	-3.4	3	92	62	86	80	0.9	6.1	1.7	2.9	6.2	5.8	3.5	5.2
XI	–	–	–	–	2.3	5.9	3.2	3.6	7.4	0.6	17.8	4	-9.0	30	93	80	90	88	0.4	2.1	0.7	1.1	5.4	6.9	6.8	7.4
XII	–	–	–	–	-2.5	0.3	-1.7	-1.4	1.7	-4.3	10.4	14	-10.0	1	88	83	88	86	0.6	1.1	0.6	0.8	6.9	7.7	6.3	7.0
Rok	–	–	–	–	6.4	11.7	8.1	8.6	13.3	4.5	36.7	5.VII	-13.9	17.1	–	–	–	–	–	–	–	–	6.6	6.8	6.0	6.5

Katowice

$\varphi = 50°14'$ $\lambda = 19°02'$

I	987.4	998.3	970.5	1023.4	-2.2	0.4	-1.3	-1.1	4.2	-4.1	6.9	6	-18.4	17	86	78	84	83	0.7	1.4	0.8	1.0	7.8	7.8	7.0	7.5
II	978.0	996.7	953.6	1013.2	0.7	5.0	2.2	2.5	6.0	-0.9	10.8	6	-6.4	28	90	72	86	83	0.8	2.6	1.1	1.4	7.3	7.6	7.4	7.4
III	984.2	998.7	965.9	1019.5	0.9	7.2	3.4	3.7	8.9	-1.4	16.7	14	-9.7	4	82	66	77	72	1.2	5.1	1.8	2.7	6.7	6.0	5.8	6.2
IV	983.8	995.2	960.6	1018.4	5.2	11.6	7.5	8.0	13.3	2.4	26.3	30	-4.8	9	87	56	76	73	1.4	7.4	2.7	3.8	6.3	6.7	5.8	6.3
V	981.8	990.0	972.9	1016.2	8.7	13.5	9.1	10.1	14.8	4.6	23.6	19	-1.2	5	79	57	77	71	2.5	7.5	2.8	4.3	6.4	7.9	5.5	6.6
VI	983.5	997.1	974.0	1017.0	16.3	22.3	16.8	18.0	23.9	10.8	31.4	11,30	4.3	28	76	56	77	70	4.6	12.7	4.7	7.3	4.2	6.1	3.9	4.7
VII	979.7	991.3	968.8	1013.0	17.1	21.8	17.2	18.3	23.8	13.6	35.7	8	9.0	19,29	83	64	84	77	3.7	11.3	3.5	6.2	6.5	6.9	6.5	6.6
VIII	982.1	992.3	969.0	1015.9	13.7	19.5	14.1	15.4	21.4	10.0	28.2	11	5.8	23	89	63	88	80	1.8	8.7	2.1	4.2	6.3	6.5	4.5	5.8
IX	981.0	988.9	967.2	1015.5	9.5	15.3	10.8	11.6	16.6	6.8	26.5	9	-1.1	27	94	68	89	84	0.8	6.0	1.5	2.8	6.7	7.0	5.7	6.5
X	986.8	995.0	970.6	1021.5	5.6	13.3	7.6	8.5	14.2	2.8	20.7	19	-2.7	26	95	66	91	84	0.5	5.6	0.9	2.3	5.8	6.2	3.1	5.0
XI	986.5	1003.9	972.1	1024.7	2.9	6.9	3.8	4.4	8.0	0.8	19.1	5	-10.2	30	92	75	88	85	0.6	3.1	1.0	1.6	7.5	6.9	7.4	7.3
XII	981.6	1001.0	948.9	1017.4	-2.4	0.4	-1.1	-1.0	1.8	-4.6	14.5	13	-12.5	11	90	81	87	86	0.5	1.3	0.3	0.9	7.1	7.3	6.8	7.1
Rok	983.0	1003.9	948.9	1017.8	6.3	11.4	7.5	8.2	12.8	3.4	36.7	8.VII	-18.4	17.1	87	66	84	79	1.6	6.1	2.0	3.2	6.6	6.9	5.8	6.4

Kolbuszowa

$\varphi = 50°14'$ $\lambda = 21°47'$

I	–	–	–	–	-2.5	0.2	-1.5	-1.3	1.1	-4.1	6.5	9	-18.0	17	85	82	88	85	0.8	1.2	0.6	0.9	8.0	8.0	7.7	7.9
II	–	–	–	–	1.2	4.4	2.3	2.6	5.6	0.0	11.4	19	-6.0	28	–	–	–	–	–	–	–	–	7.7	7.8	7.0	7.5
III	–	–	–	–	-0.3	6.0	2.1	2.5	7.8	-1.9	17.1	14	-13.7	4	–	–	–	–	–	–	–	–	5.5	6.2	3.8	5.2
IV	–	–	–	–	5.4	13.1	7.8	8.5	14.5	2.7	26.0	30	-3.4	16	89	55	81	75	1.2	8.3	2.2	3.9	6.7	6.8	6.1	6.5
V	–	–	–	–	8.9	13.6	9.4	10.3	15.1	5.2	23.0	18	-0.1	5	87	62	84	78	1.7	7.2	2.0	3.6	6.5	8.0	7.6	7.4
VI	–	–	–	–	16.9	23.5	16.2	18.2	24.9	10.1	33.2	12	2.8	28	78	50	82	70	4.6	15.2	3.5	7.8	4.7	5.9	5.3	5.3
VII	–	–	–	–	17.5	23.4	17.8	19.1	25.0	14.0	36.6	5	6.3	4	84	58	84	75	3.3	13.9	3.4	6.9	6.8	6.8	7.2	6.9
VIII	–	–	–	–	14.4	20.1	15.5	16.5	22.5	10.9	30.9	14	4.9	31	89	61	85	78	2.0	10.6	2.9	5.2	5.8	7.1	6.1	6.3
IX	–	–	–	–	10.2	16.3	11.5	12.4	17.4	7.9	27.8	9	-1.7	27	93	65	87	82	0.9	6.9	1.8	3.2	6.9	7.1	7.1	7.0
X	–	–	–	–	5.3	13.3	7.3	8.5	14.2	3.0	20.0	19	-4.7	3	92	62	87	80	0.8	6.1	1.7	2.9	5.8	6.3	5.1	5.7
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2.3	0.7	-1.4	-1.1	1.9	-4.4	10.5	13	-11.2	11	–	–	–	–	–	–	–	–	7.1	7.3	7.1	7.2
Rok	–	–	–	–	–	–	–	–	–	–	36.6	5.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Śnieżnik Kłodzki

$\varphi = 50°12'$ $\lambda = 16°49'$

I	–	–	–	–	-4.6	-3.1	-4.4	-4.1	–	-6.7	–	–	-17.0	16,17	–	–	–	–	–	–	–	–	6.6	6.0	4.7	5.8
II	–	–	–	–	-2.5	-1.3	-2.1	-2.0	–	-4.3	–	–	-10.4	26	–	–	–	–	–	–	–	–	8.2	8.4	7.3	8.0
III	–	–	–	–	-1.4	0.9	-0.6	-0.4	–	-3.4	–	–	-11.1	1	–	–	–	–	–	–	–	–	6.4	6.5	3.9	5.6
IV	–	–	–	–	0.6	3.3	1.3	1.8	–	-1.2	–	–	-8.8	13,15	–	–	–	–	–	–	–	–	4.5	6.3	6.0	5.6
V	–	–	–	–	2.6	5.5	3.4	3.7	–	0.6	–	–	-5.3	5,6	–	–	–	–	–	–	–	–	7.0	7.2	6.5	6.9
VI	–	–	–	–	10.6	13.8	11.3	11.8	–	7.6	–	–	-0.2	25	–	–	–	–	–	–	–	–	6.1	6.1	5.6	5.3
VII	–	–	–	–	11.7	13.6	12.2	12.4	–	9.8	–	–	4.2	28	–	–	–	–	–	–	–	–	6.6	6.9	6.5	6.6
VIII	–	–	–	–	8.5	10.9	9.1	9.4	–	6.4	–	–	1.8	23	–	–	–	–	–	–	–	–	7.1	8.2	5.9	7.1
IX	–	–	–	–	5.4	7.1	5.2	5.7	–	2.9	–	–	-3.3	30	–	–	–	–	–	–	–	–	8.0	7.9	6.5	7.5
X	–	–	–	–	3.5	5.8	4.0	4.3	–	1.7	–	–	-3.3	1	–	–	–	–	–	–	–	–	4.5	6.7	5.7	5.6
XI	–	–	–	–	-0.4	0.0	-0.9	-0.6	–	-2.6	–	–	-12.0	30	–	–	–	–	–	–	–	–	7.4	7.9	7.1	7.5
XII	–	–	–	–	-3.8	-3.3	-3.8	-3.7	–	-7.1	–	–	-14.4	1	–	–	–	–	–	–	–	–	7.6	6.9	6.0	6.8
Rok	–	–	–	–	2.5	4.4	2.9	3.2	–	0.3	–	–	-12.0	30.XII	–	–	–	–	–	–	–	–	6.7	7.1	5.8	6.5

Leżajsk

$H_s = 190\ m$ $h_w = 16{,}5\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, V=D)																		OPAD R			LICZBA DNI (n)																			
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr											
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min <0°	Max <0°	Min <-10°	Max >25°	0,1 ≤ R < 1,0	1,0 ≤ R < 10,0	R ≥ 10,0	v ≥ 10 m/s	v ≥ 15 m/s	≡	≈	◎	●	⊞
I	2	3,0	2,5	5,4	4	5,6	16,5	6,2	4	4,6	21,5	6,6	28,5	6,1	4	3,0	13	5,1	29,8	9,4	5	26	9	3	·	12	8	·	7	2	2	·	1	18	18
II	2,5	4,2	1	1,0	·	·	7,5	4,7	18	4,6	32	6,4	44,5	5,1	6,5	3,2	5	4,5	35,3	7,5	15	10	1	·	·	12	9	·	4	·	4	·	1	15	6
III	6	2,5	6	1,0	10	4,8	16	5,7	2,5	2,4	18,5	4,6	17	5,4	7	6,8	10	4,2	17,7	8,8	18	20	4	1	·	6	3	·	5	1	3	·	9	8	5
IV	15,5	2,9	1,5	2,3	4,6	2,0	18	2,5	5,5	2,5	8,5	2,4	12	2,5	10,5	2,6	14	2,2	25,9	14,8	11	4	·	·	2	6	6	1	·	·	3	2	7	10	·
V	15	2,7	14,5	3,6	11	3,8	4,5	2,7	5,5	2,4	2,5	4,0	15,5	4,5	13,5	4,1	11	3,2	66,0	14,4	9	·	·	·	·	12	10	2	1	·	·	1	1	17	1
VI	4	2,2	6	1,2	1,5	1,7	11,5	2,7	15	2,7	13	3,6	17,5	3,0	13,5	3,0	8	2,6	35,9	15,2	4	·	·	·	16	9	7	1	1	·	1	5	4	3	·
VII	2,5	3,4	5,5	1,4	5,5	2,3	7	3,0	7,5	1,9	24,5	3,1	17	4,0	11,5	3,0	12	2,6	116,4	29,5	24	·	·	·	15	18	13	4	·	·	·	7	3	14	·
VIII	1	1,0	·	·	2	3,5	12,5	2,1	2	4,8	18,5	3,2	36	4,0	10	2,4	11	2,9	49,4	9,1	10	·	·	·	7	15	11	·	·	·	2	5	2	4	·
IX	2	2,5	0,5	1,0	3	2,2	3	2,2	10,5	3,0	28	4,1	29	6,4	6	2,8	8	4,1	65,4	17,1	3	1	·	·	2	16	12	2	7	1	3	1	3	11	·
X	2	1,0	0,5	1,0	4	2,0	11	2,8	12	2,4	21	3,1	22,5	2,8	4	2,0	16	2,2	14,7	5,4	20	2	·	·	·	5	4	·	·	·	8	·	7	8	·
XI	·	·	6	3,1	11,5	4,8	31	3,0	6	1,2	4,5	3,4	19	6,3	4	8,5	8	3,8	17,4	7,4	28	11	2	·	·	6	5	·	3	·	4	·	2	16	1
XII	6,5	4,2	4	3,5	3	4,7	10,5	3,4	10	4,3	33,5	4,3	4,5	4,7	11	3,0	10	3,6	15,0	4,2	8	27	10	·	·	8	5	·	2	1	1	·	4	13	7
Rok	59	2,2	4,8	2,0	6,0	3,1	14,9	3,4	9,8,5	3,1	22,6	4,0	22,7	4,6	101,5	3,7	126	3,4	488,9	29,5	24.VII	101	26	4	42	127	93	10	30	5	31	21	44	137	38

Katowice

$H_s = 285\ m$ $H_b = 285{,}4\ m$ $h_w = 20\ m$

I	2	3,0	4,5	4,8	2,5	6,2	·	·	3	2,5	3,7	4,9	17	4,3	11	5,8	16	4,0	22,2	7,2	6	26	9	3	·	13	8	·	4	·	5	·	1	18	19
II	5	2,7	1,5	1,3	2	1,0	5	3,2	8,5	4,8	39,5	5,2	11	3,9	4,5	5,7	7	4,1	46,3	11,2	18	16	1	·	·	16	9	1	7	2	3	·	1	12	7
III	7	3,0	4	2,6	1,8	5,1	10,5	3,8	2	3,5	16,5	4,6	12,5	4,6	10,5	4,9	12	3,9	42,8	10,0	18	20	3	·	·	11	8	1	5	1	4	1	6	13	4
IV	16,5	3,3	8	2,1	4,5	3,3	7	3,5	4,5	4,0	6	3,2	7,5	2,7	11	3,1	25	2,2	32,1	11,2	7	8	·	·	1	15	7	1	1	1	4	·	4	10	·
V	7	3,4	19,5	3,9	7,5	3,5	1	5,5	3	1,8	7	3,1	8	3,5	15	3,7	25	2,6	18,7	6,0	10	4	·	·	·	6	4	·	·	·	1	1	2	11	·
VI	9	2,9	7	2,3	5,5	2,4	2,5	2,8	4,5	4,0	19,5	4,2	11,5	4,6	4,5	4,7	26	2,6	69,4	34,5	7	·	·	·	13	11	9	1	1	·	1	6	5	2	·
VII	4	3,1	3,5	2,9	4,5	3,0	6	2,4	2	3,5	21,5	4,2	15,5	4,5	9	3,3	27	2,7	137,7	39,5	16	·	·	·	12	18	14	5	1	·	4	9	2	13	·
VIII	1,5	4,3	·	·	0,5	4,0	0,5	4,0	4	4,0	15,5	4,7	15,5	3,4	14,5	4,0	4,1	2,2	103,5	34,4	14	·	·	·	6	12	11	2	1	1	7	4	1	5	·
IX	2,5	2,0	2	2,0	1,5	1,3	3,5	2,6	4	4,1	2,6	5,8	1,9	5,1	10,5	4,5	2,1	3,7	91,4	22,2	23	1	·	·	2	20	15	4	6	·	5	·	1	8	·
X	6	2,3	·	·	2,5	3,8	5	3,6	4	2,5	2,8	4,4	2,1	4,3	4,5	4,7	22	3,1	11,4	5,7	20	4	·	·		4	3	·	1	·	1,3	·	6	3	·
XI	4,5	8,1	1	5,5	1,9	4,7	1,4	3,4	8,5	4,8	11	3,8	15,5	5,8	2,5	6,2	14	4,1	25,2	9,2	28	11	3	1		8	7	·	·	·	6	·	5	20	1
XII	7,5	3,7	5,5	3,3	4,5	6,9	5,5	3,1	9,5	3,9	3,8	6,0	11,5	5,0	4	5,2	7	4,6	32,5	7,1	14	28	11	5		12	9	·	6	1	6	·	1	14	8
Rok	72,5	3,5	56,5	2,6	72,5	3,7	60,5	3,2	57,5	3,6	265,5	4,5	165,6	4,3	101,5	4,6	243	3,3	633,2	39,5	16.VII	118	27	9	35	146	105	15	33	6	59	21	35	129	39

Kolbuszowa

$H_s = 208\ m$ $h_w = 16\ m$

I	2,5	3,8	6	6,5	3	3,5	5	3,2	2,9	3,2	14	4,0	19,5	4,5	1	4,0	13	3,4	35,7	18,7	6	24	8	4	·	14	6	1	1	·	·	·	1	18	16
II	4,5	4,4	·	·	2	4,0	4,5	5,0	37,5	5,5	14,5	2,8	7	3,3	5	4,6	9	4,0	33,6	6,5	15	13	1	·	·	14	11	·	5	·	1	·	1	16	6
III	6,5	2,4	10	3,6	1,5	7,1	8,5	3,8	9	3,4	9	5,3	11	5,1	5	4,0	19	3,7	34,3	14,8	18	18	4	1	·	11	6	1	5	1	1	·	8	6	5
IV	13	2,9	5,5	1,3	7	2,5	8,5	2,6	5,5	3,2	7	2,3	7	1,7	7,5	2,7	29	1,7	32,7	11,2	11	10	·	·	2	12	8	1	·	·	4	·	5	14	·
V	16	3,9	12	3,7	8,5	4,1	4,5	2,9	2	2,0	6	3,2	12,5	2,5	11,5	2,4	20	2,5	52,4	21,2	9	1	·	·	·	14	10	2	·	·	·	1	1	17	·
VI	7,5	1,9	0,5	2,0	2	1,2	9,5	2,1	16	5,1	9,5	4,2	12,5	4,0	7,5	2,8	25	2,6	26,1	9,8	10	·	·	·	16	10	6	·	2	·	·	·	4	3	·
VII	4	1,8	4	2,5	6,5	2,5	6,5	2,4	11	2,6	21	3,6	13,5	3,9	4,5	2,7	22	2,4	123,1	37,0	16	·	·	·	14	18	12	2	·	·	3	1	15	·
VIII	3	3,6	1	2,5	4	2,5	2,5	2,2	7	4,4	13	2,5	23	3,5	6,5	2,3	33	2,0	51,5	10,3	16	·	·	·	7	14	12	1	·	·	4	1	6	·
IX	1	1,5	0,5	2,0	1,5	1,0	4	2,8	14	3,7	24,5	4,8	19,5	4,6	3	2,7	22	3,1	59,7	16,3	29	2	·	·	2	14	10	1	5	·	2	·	3	12	·
X	0,5	1,0	1	2,0	6	2,8	2	1,2	16	3,6	13	3,4	12,5	2,2	2	1,0	40	1,6	24,3	9,9	23	5	·	·	·	6	3	·	·	·	2	·	4	10	·
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8,0	-	-	-	-	-	-	6	4,1	2	-	-	-	-	-	-	-
XII	13,5	3,4	3,5	3,3	3	3,7	6	3,9	3,1	4,0	1,5	2,9	6	5,2	4	4,5	11	3,3	21,0	5,4	13	27	9	2	·	10	6	·	2	·	·	·	3	13	2
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	502,4	37,0	16.VII	-	-	-	44	143	113	98	-	-	-	-	-	-	29

Śnieżnik Kłodzki

$H_s = 1218\ m$ $h_w = 7\ m$

I	2	5,5	9	6,5	2	2,5	12	3,7	7	4,6	22	3,4	7	4,0	17	3,6	15	3,4	96,3	22,7	28	29	-	4	-	15	13	4	3	·	-	·	8	12	31
II	5	3,2	4	2,0	2	1,0	13	3,8	15	4,9	28	6,1	6	5,7	8	4,4	3	4,6	72,4	13,7	1	24	-	1	-	18	14	2	6	1	-	·	1	17	28
III	6,5	2,5	10	1,8	4,5	2,8	15	3,4	17,5	4,1	5	3,7	13	4,5	6,5	3,0	15	2,8	94,7	16,6	17	25	-	2	-	15	12	3	2	·	-	1	8	10	22
IV	15	1,3	8,5	1,7	17	1,5	5,5	1,5	11	2,5	3	2,5	1	1,0	1	1,0	28	1,2	74,1	25,2	30	18	-	·	-	11	7	3	·	·	-	2	4	9	9
V	11	2,7	39	4,2	7	3,7	7	2,6	3	2,7	5	3,0	3	4,7	12	2,7	6	3,3	24,7	7,2	24	15	-	·	-	11	5	·	1	·	-	2	4	15	5
VI	7	2,2	12	4,2	6	3,0	17	2,8	7	3,4	15	3,7	13	3,7	6	2,5	7	3,1	142,1	30,6	9	1	-	·	-	11	10	5	3	1	-	10	11	10	·
VII	15	2,3	6	2,3	5	2,4	5	2,6	9	3,6	26	3,7	18	3,1	6	3,5	3	3,0	269,8	37,5	14	·	-	·	-	25	25	10	1	·	-	5	6	18	·
VIII	6	2,3	8	1,9	2	1,0	6	3,8	5	3,8	36	3,7	9	2,3	16	2,0	5	2,8	93,7	12,0	24	·	-	·	-	18	16	3	1	·	-	2	2	12	·
IX	·	·	5	2,4	3	5,0	13	3,7	1	8,0	34	6,6	17	3,8	11	4,1	6	5,8	125,5	22,4	23	5	-	·	-	22	18	3	12	5	-	·	3	17	·
X	·	·	2	2,0	·	·	18	4,6	25	3,5	11	2,8	8	1,9	3	1,7	26	2,4	21,7	16,0	22	9	-	·	-	7	3	1	2	·	-	·	7	10	·
XI	1	6,0	8	7,2	1	2,0	30	6,8	8	4,0	12	8,5	12	2,3	8	8,1	10	5,5	37,0	7,4	29	19	-	2	-	9	9	·	10	7	-	·	4	20	1
XII	1	3,0	18	3,6	4	5,0	31	7,0	6	2,8	16	6,4	1	4,0	7	3,4	10	4,8	20,5	29,7	3	30	-	7	-	18	12	2	10	3	-	·	4	16	31
Rok	99,5	2,6	129,6	3,3	53,5	2,5	172,5	4,3	143,5	4,0	213	4,5	108	3,2	101,5	3,3	134	3,6	1132,8	37,5	14.VII	176	-	16	-	180	144	36	51	17	-	22	62	168	127

Głubczyce

$\varphi = 50°12'$ $\lambda = 17°49'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.9	1.3	-1.2	-0.8	2.1	-3.4	10.9	6	-13.4	17	87	76	83	82	0.7	1.7	1.0	1.1	–	–	–	–
II	–	–	–	–	1.1	5.4	2.4	2.8	6.3	0.0	9.9	5	-5.4	27	86	71	85	81	0.9	2.7	1.1	1.6	–	–	–	–
III	–	–	–	–	1.6	7.5	4.2	4.4	9.2	0.3	18.0	14	-5.7	4	84	62	80	75	1.2	4.4	1.8	2.5	–	–	–	–
IV	–	–	–	–	5.0	11.3	7.0	7.6	12.9	2.9	24.5	30	-3.1	14	85	59	82	75	1.4	6.5	2.0	3.3	–	–	–	–
V	–	–	–	–	8.9	14.3	9.5	10.6	15.6	5.5	26.0	19	-0.2	7	80	54	80	71	2.3	8.0	2.5	4.3	–	–	–	–
VI	–	–	–	–	16.1	22.3	16.6	17.9	23.8	11.1	31.1	30	5.5	28	78	55	82	72	4.0	13.3	3.8	7.0	–	–	–	–
VII	–	–	–	–	16.8	22.2	17.2	18.4	23.3	14.3	33.9	5	10.7	22,28	88	67	89	81	2.6	10.5	2.5	5.2	–	–	–	–
VIII	–	–	–	–	13.9	20.1	14.6	15.8	21.2	10.7	27.8	11	5.7	23	89	62	89	80	1.8	9.3	2.0	4.4	–	–	–	–
IX	–	–	–	–	9.8	15.6	10.8	11.8	16.5	7.7	25.8	9	-0.4	27	90	60	88	81	1.2	6.4	1.6	3.1	–	–	–	–
X	–	–	–	–	6.4	13.7	8.0	9.0	15.0	4.7	19.5	9	-1.5	24	89	65	89	81	1.2	5.8	1.3	2.8	–	–	–	–
XI	–	–	–	–	3.6	7.2	4.5	5.0	8.3	2.2	17.7	5	-8.9	30	89	76	86	84	0.9	2.8	1.3	1.7	–	–	–	–
XII	–	–	–	–	-1.4	1.2	-0.7	-0.4	2.3	-3.1	12.2	13	-11.7	16	90	80	90	86	0.6	1.4	0.6	0.9	–	–	–	–
Rok	–	–	–	–	6.7	11.8	7.7	8.4	13.0	4.4	33.9	5.VII	-13.4	17.1	86	66	85	79	1.6	6.1	1.8	3.2	–	–	–	–

Murcki

$\varphi = 50°12'$ $\lambda = 19°03'$

I	–	–	–	–	-2.3	0.6	-1.5	-1.2	1.8	-3.8	7.3	2	-17.1	17	–	–	–	–	–	–	–	–	8.5	8.2	7.3	8.0
II	–	–	–	–	1.1	5.3	2.2	2.7	6.4	-0.3	11.2	6	-6.3	27	–	–	–	–	–	–	–	–	7.0	7.7	7.5	7.4
III	–	–	–	–	1.2	7.7	3.7	4.1	9.4	-0.3	17.0	14	-9.5	1	–	–	–	–	–	–	–	–	5.0	5.8	5.1	5.3
IV	–	–	–	–	5.6	12.2	7.3	8.1	13.8	3.2	27.1	30	-3.9	15	–	–	–	–	–	–	–	–	5.9	7.3	5.7	6.3
V	–	–	–	–	9.0	13.6	9.1	10.2	15.0	5.6	23.9	19	0.4	29	–	–	–	–	–	–	–	–	6.7	8.4	5.6	6.9
VI	–	–	–	–	15.9	22.3	17.0	18.0	24.1	11.7	34.8	11	5.9	7	–	–	–	–	–	–	–	–	3.7	7.3	4.3	5.1
VII	–	–	–	–	17.0	21.9	17.4	18.4	24.0	14.0	35.9	8	10.6	29	–	–	–	–	–	–	–	–	6.8	7.0	6.9	6.9
VIII	–	–	–	–	13.9	20.0	14.9	15.9	21.6	11.2	28.9	11	6.4	23	–	–	–	–	–	–	–	–	6.3	7.5	4.9	6.2
IX	–	–	–	–	10.2	15.3	11.0	11.9	16.8	7.9	27.5	9	0.2	27	–	–	–	–	–	–	–	–	5.9	7.8	6.5	6.7
X	–	–	–	–	6.6	13.7	8.5	9.4	14.6	4.7	21.5	19	-0.5	3	–	–	–	–	–	–	–	–	4.7	5.2	2.8	4.2
XI	–	–	–	–	3.0	6.8	3.8	4.4	8.2	1.4	19.8	5	-10.5	30	–	–	–	–	–	–	–	–	7.3	6.6	6.8	6.9
XII	–	–	–	–	-2.2	0.3	-1.3	-1.1	1.9	-4.3	14.3	13	-11.3	11	–	–	–	–	–	–	–	–	6.5	7.0	6.9	6.8
Rok	–	–	–	–	6.6	11.6	7.7	8.4	13.1	4.2	35.9	8.VII	-17.1	17.1	–	–	–	–	–	–	–	–	6.2	7.2	5.9	6.4

Goszyce

$\varphi = 50°11'$ $\lambda = 20°08'$

I	–	–	–	–	-2.4	0.3	-2.1	-1.6	1.2	-4.4	8.7	6	-16.9	17	–	–	–	–	–	–	–	–	8.2	7.2	5.3	6.9
II	–	–	–	–	1.2	5.0	2.5	2.8	6.3	-0.2	10.3	6.13	-5.5	24	–	–	–	–	–	–	–	–	7.7	7.3	6.3	7.1
III	–	–	–	–	0.2	6.5	2.8	3.1	8.2	-1.3	17.3	28	-12.0	4	–	–	–	–	–	–	–	–	5.5	5.4	4.4	5.1
IV	–	–	–	–	4.8	12.0	7.6	8.0	13.6	3.0	25.2	30	-2.8	14	90	60	81	77	1.0	6.5	2.1	3.2	5.4	6.5	5.7	5.9
V	–	–	–	–	8.3	13.1	9.6	10.2	14.5	5.2	22.7	20	0.8	30	84	63	80	76	1.9	6.6	2.6	3.7	6.1	7.6	6.7	6.8
VI	–	–	–	–	15.8	22.2	16.4	17.7	24.0	10.8	30.9	11	4.3	1	80	56	79	72	3.6	12.3	3.9	6.6	3.5	4.8	4.2	4.2
VII	–	–	–	–	16.7	22.1	17.8	18.6	23.8	13.8	34.0	8	8.8	4	86	65	84	78	2.7	10.8	3.5	5.7	5.9	6.2	6.4	6.2
VIII	–	–	–	–	13.7	20.0	15.3	16.1	21.7	11.2	28.8	12	5.1	24	90	65	85	80	1.6	8.8	2.7	4.4	3.7	5.7	4.5	4.6
IX	–	–	–	–	9.2	15.5	11.7	12.0	16.9	7.6	27.8	9	0.4	27	92	68	86	82	1.0	6.1	1.9	3.0	5.5	6.2	5.0	5.6
X	–	–	–	–	4.6	13.1	8.0	8.4	14.0	3.1	20.9	19	-2.9	3	94	66	89	83	0.5	5.7	1.3	2.5	5.4	5.0	3.6	4.7
XI	–	–	–	–	1.4	5.8	3.1	3.4	7.0	0.0	17.4	5	-9.6	30	90	81	88	86	0.7	2.2	1.0	1.3	7.7	7.0	6.9	7.2
XII	–	–	–	–	-2.7	-0.2	-1.5	-1.5	1.1	-4.4	8.2	13	-11.2	11	–	–	–	–	–	–	–	–	7.3	7.3	5.9	6.8
Rok	–	–	–	–	5.9	11.3	7.6	8.1	12.7	3.7	34.0	8.XII	-16.9	17.1	–	–	–	–	–	–	–	–	6.0	6.4	5.4	5.9

Haryniec

$\varphi = 50°11'$ $\lambda = 23°21'$

I	–	–	–	–	-4.1	-0.8	-2.8	-2.6	0.2	-6.2	4.2	10	-15.4	17.22	86	80	89	85	0.6	1.2	0.5	0.8	8.3	8.2	8.0	8.2
II	–	–	–	–	0.7	4.4	1.5	2.0	–	-1.3	–	–	-6.6	24	86	75	89	83	1.0	2.3	0.8	1.4	8.7	6.9	5.3	7.0
III	–	–	–	–	-4.6	5.5	0.5	1.2	–	-4.4	–	–	-19.0	4	81	65	81	76	1.1	4.1	1.3	2.2	6.2	5.5	4.4	5.4
IV	–	–	–	–	6.2	13.5	6.6	8.2	–	1.4	–	–	-7.0	16	78	51	80	70	2.4	9.0	2.2	4.5	5.8	5.4	4.3	5.2
V	–	–	–	–	9.3	13.5	9.1	10.2	–	5.1	–	–	-2.2	5	86	68	88	81	1.8	6.0	1.4	3.1	7.1	8.3	7.0	7.5
VI	–	–	–	–	15.1	22.5	16.4	17.6	–	8.9	–	–	3.0	7	–	–	–	–	–	–	–	–	3.9	3.9	3.7	3.8
VII	–	–	–	–	16.9	23.0	16.9	18.4	–	12.4	–	–	5.6	7	88	61	88	79	2.4	12.0	2.6	5.7	6.1	5.5	6.5	6.0
VIII	–	–	–	–	15.1	20.9	14.4	16.2	–	9.7	–	–	2.2	31	89	62	93	81	2.1	9.8	1.3	4.4	6.2	6.1	3.9	5.4
IX	–	–	–	–	10.8	16.4	10.5	12.0	–	6.8	–	–	-3.2	27	92	65	93	83	1.1	6.9	1.0	3.0	6.3	6.7	5.3	6.1
X	–	–	–	–	4.6	12.9	5.2	7.0	–	1.2	–	–	-4.3	3	91	64	91	82	0.8	5.9	1.0	2.6	6.2	4.8	3.2	4.7
XI	–	–	–	–	1.7	6.2	2.4	3.2	–	-0.5	–	–	-10.6	30	90	80	91	87	0.6	2.3	0.7	1.2	7.7	6.6	6.4	6.9
XII	–	–	–	–	-3.4	0.0	-2.5	-2.1	–	-6.3	–	–	-12.5	2	–	–	–	–	–	–	–	–	6.4	7.5	6.0	6.6
Rok	–	–	–	–	5.9	11.5	6.5	7.6	–	2.2	–	–	-15.4	17.22.1	–	–	–	–	–	–	–	–	6.8	6.3	5.3	6.1

Głubczyce

$H_s = 290\ m$ $h_w = 13\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °/0, ∇=0																	OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min ≤0°	Max ≥0°	Min ≤-10°	Max ≥25°	0.1 ≤ ∆N < 1.0 mm	1.0 ≤ ∆N < 10.0 mm	∆N ≥ 10.0 mm	10 ≤ ∆V < 15 m/s	∆V ≥ 15 m/s	≡	≤ 0.5 km	◔	●	▦
I	14	2.8	3	5.7	-	-	1.5	2.0	2.5	4.4	10	5.6	4.5	4.3	6	4.9	29	2.9	17.4	5.7	30	23	10	4	-	9	6	-	4	1	-	-	-	-	13
II	6	3.0	-	-	-	-	4	1.9	2.8	3.5	14.5	5.7	4	4.0	6.5	4.5	21	3.0	22.7	6.7	25	14	1	-	-	12	7	-	4	-	-	-	-	-	4
III	1.4	2.8	1.5	3.7	-	-	7.5	3.9	2.6	5.7	6	4.6	4.5	3.8	5.5	4.2	28	3.1	29.1	7.6	17	13	1	-	-	10	8	-	6	-	1	1	-	-	6
IV	2.2	3.2	0.5	2.0	2	2.5	-	-	9.5	4.7	1.5	6.0	2.5	3.0	1.2	2.9	40	1.9	31.5	14.6	24	9	-	-	-	13	6	1	3	-	-	-	-	-	2
V	3.7	3.9	3.5	3.4	2	1.5	0.5	1.0	8.5	2.9	3	4.3	1.5	2.0	1.1	4.1	26	2.6	15.8	6.7	20	2	-	-	1	9	6	-	2	-	-	3	-	-	-
VI	4	2.8	1	1.0	5	2.2	4	3.9	1.1	4.9	9	4.2	9.5	3.7	15.5	4.1	34	2.5	55.1	10.2	7,24	-	-	-	9	9	7	3	6	-	-	8	-	-	-
VII	18.5	2.8	2	1.5	-	-	8	3.1	1.0	3.0	2	5.2	4	2.5	16.5	3.5	32	2.0	186.3	23.2	16	-	-	-	9	21	17	11	1	-	-	4	-	-	-
VIII	18.5	2.1	-	-	-	-	1	6.5	16.5	3.3	6	4.5	1.0	3.1	8	2.5	33	1.9	41.4	8.9	15	-	-	-	1	14	9	-	2	-	-	2	-	-	-
IX	1.2	3.0	2.5	1.8	1.5	2.3	1	2.0	13.5	6.3	1.0	6.6	9	3.4	8.5	3.4	32	2.8	79.5	13.6	14	1	-	-	2	16	15	3	6	-	-	1	-	-	-
X	7.5	2.2	-	-	-	-	3	2.8	2.4.5	5.4	11.5	5.1	5	3.8	4.5	2.1	37	2.6	4.1	3.3	20	1	-	-	-	4	1	-	4	-	4	-	-	-	-
XI	10.5	3.6	3	2.0	2	1.5	3	2.5	1.7	3.8	7	6.2	1.0	2.0	6.5	5.8	31	2.4	20.4	4.7	12	12	1	-	-	7	6	-	4	-	4	-	-	-	1
XII	15.5	2.0	-	-	1	1.0	2	5.0	21.5	4.7	11.5	5.7	4	2.8	3.5	3.3	34	2.5	21.1	6.9	14	26	9	1	-	9	4	-	3	-	2	-	-	-	6
Rok	172.5	2.8	17	1.7	13.5	0.9	35.5	2.9	21.1	4.4	92	6.3	68.5	3.2	104	3.8	374	2.5	524.5	23.2	16.VII	101	22	5	22	133	92	18	45	1	11	17	-	-	37

Murcki

$H_s = 321\ m$ $h_w = 16\ m$

I	1	1.0	2	3.5	9	5.7	4	1.0	3.5	1.1	51.5	3.6	13.5	2.1	5.5	8.0	3	3.5	23.5	5.4	5	25	8	3	-	11	8	-	5	1	8	-	2	22	21
II	-	-	1	2.0	3	2.7	10.5	2.3	1.3	3.9	34.5	3.3	9	3.8	11	3.4	2	3.2	64.2	17.0	25	14	1	-	-	16	8	2	3	1	5	-	1	12	5
III	4.5	1.9	4.5	3.9	6.5	7.5	28.5	3.6	5	1.8	28	3.5	9	3.3	7	3.6	2	3.5	46.7	10.2	17	16	3	-	-	11	7	1	5	1	6	1	11	11	4
IV	9.5	2.6	9.5	4.8	7	1.4	14	2.1	7	1.4	10	2.4	6.5	1.9	19.5	2.6	7	2.0	42.3	15.5	7	7	-	-	1	13	8	1	1	-	9	1	4	11	-
V	5	2.0	16	3.8	16	3.4	15.5	1.8	7.5	1.3	7	2.4	6	2.2	15	2.5	5	2.5	24.4	7.7	10	-	-	-	-	10	4	-	1	-	7	2	1	13	-
VI	1	3.0	9	2.9	4	2.8	11	1.6	6	2.6	1.9	2.4	1.9	2.2	15	2.4	6	2.2	64.7	35.2	7	-	-	-	14	8	8	1	-	-	1	5	6	4	-
VII	3	2.3	3	2.3	4	1.5	10.5	2.2	7.5	1.8	27	2.7	17	2.4	12	1.9	9	2.1	128.5	37.2	16	-	-	-	12	19	18	2	1	-	5	4	3	14	-
VIII	0.5	3.0	2	1.5	-	-	6	2.5	1	1.0	47	2.5	14.5	3.6	10	2.9	12	2.3	106.9	23.3	14	-	-	-	6	14	12	3	1	1	8	1	3	8	-
IX	1	2.0	5	2.4	-	-	4	1.0	8.5	2.1	28.5	3.3	18.5	3.5	11.5	3.2	13	2.5	77.0	16.0	23	-	-	-	2	17	15	2	1	-	6	-	2	10	-
X	1	2.0	1	3.0	-	-	11	1.7	2	1.5	46	2.6	7.5	2.5	9.5	2.8	15	2.1	13.8	4.8	20	2	-	-	-	4	4	-	-	-	11	-	10	2	-
XI	8.6	3.8	11.5	3.9	3	5.0	19.5	2.4	13.5	2.5	14	3.1	4	2.8	2	3.2	14	2.6	24.7	10.1	28	11	3	1	-	8	7	1	2	-	8	-	6	18	-
XII	3	3.3	6	3.3	3	7.0	10.5	1.9	10.5	3.0	36	4.5	12	4.4	5	6.0	7	3.7	41.3	7.6	14	29	9	4	-	16	11	-	3	1	5	-	3	16	10
Rok	38	2.2	70.5	2.9	55.5	3.1	14.3	2.0	8.5	2.0	34.8.5	3.0	136.6	2.9	123	3.5	95	2.7	658.0	37.2	16.VII	104	24	8	35	147	110	13	23	5	80	14	52	141	40

Goszyce

$H_s = 260\ m$ $h_w = 14\ m$

I	2	2.5	6	4.3	4	6.7	3.5	3.0	17.5	3.0	2.6	4.3	20.5	6.4	8.5	5.0	6	4.3	24.1	7.0	13	26	10	3	-	13	6	-	2	-	-	-	2	14	22
II	6	3.6	2	4.0	3	4.8	7.5	5.0	1.7	4.2	28	5.3	11.5	6.0	7	5.1	2	4.8	19.4	4.8	26	13	2	-	-	13	7	-	1	-	2	-	4	15	6
III	3	3.2	5	4.1	28.5	5.8	8.5	4.2	6	3.8	11	6.4	14	5.5	10	5.5	7	4.9	27.2	6.6	19	19	2	1	-	12	8	-	4	-	-	1	9	5	6
IV	6.5	3.8	5.6	4.7	15.5	3.8	7	3.4	4	5.0	7	3.7	14	3.8	17.5	4.5	13	3.5	54.8	12.6	7	7	-	-	1	15	12	2	-	-	1	3	5	9	-
V	9.5	4.3	18.5	5.8	17.5	4.5	7	3.9	6.5	2.4	5	4.6	12	6.0	12	5.7	5	4.7	34.8	14.4	10	-	-	-	-	10	5	2	6	-	-	2	1	13	-
VI	11	3.8	6.5	4.2	7	4.1	9	4.7	8	4.6	14	5.6	13.5	4.4	15	3.1	6	4.0	37.9	10.7	7	-	-	-	13	10	8	1	1	-	-	7	9	2	-
VII	2	2.5	-	-	10.5	5.0	6.5	4.2	1.5	5.0	17.5	6.5	17.5	5.3	2.2	5.5	2	5.2	167.3	64.4	16	-	-	-	13	19	15	4	9	-	-	6	4	13	-
VIII	2.5	3.8	-	-	4	6.5	2.5	4.4	7.5	3.8	19.5	4.2	3.3	5.3	1.3	4.6	11	4.2	64.5	14.3	14	-	-	-	6	15	10	2	3	-	-	3	5	5	-
IX	1	4.0	1	4.0	-	-	9	3.7	1.3	4.5	17.5	6.4	33.6	5.9	6	5.9	9	5.0	50.1	8.9	29	-	-	-	2	14	11	-	6	-	5	-	2	7	-
X	1	2.0	1	2.0	8	2.9	12	3.0	10.5	2.8	18.5	4.4	17.5	4.5	10.5	3.7	14	3.1	43.3	5.3	20	5	-	-	-	4	3	-	-	-	11	-	5	5	-
XI	2	8.0	9.5	8.1	23.5	5.3	15.5	3.4	9	3.3	10	4.2	16.5	8.0	4	9.9	1	5.6	19.9	5.3	28	13	3	-	-	7	5	-	7	-	9	-	4	15	-
XII	4.5	3.4	3.5	5.4	7.5	4.9	8.5	3.7	13.5	2.6	2.8	4.3	1.3	5.9	10.5	4.6	4	4.1	25.2	11.4	8	28	12	3	-	10	7	1	-	-	1	-	3	12	4
Rok	5.1	3.7	58.5	3.9	12.9	4.8	96.5	3.9	127.5	3.8	20.1	5.0	21.5.5	5.6	13.6	5.3	80	4.4	535.5	64.4	16.VII	111	29	7	35	142	97	12	39	-	29	22	57	116	38

Boryniec

$H_s = 240\ m$ $h_w = 12\ m$

I	-	-	4.5	2.4	4.5	3.3	9	2.6	6	2.3	11.5	3.3	2.9	4.1	2.5	5.4	26	2.5	24.8	9.0	5	28	12	6	•	14	6	-	-	-	3	-	2	20	-
II	4.5	3.0	-	-	0.5	2.0	3	2.8	2.4	3.3	12.5	3.7	4.4	4.0	4.5	2.3	24	2.5	30.1	8.2	15	18	-	-	-	14	11	-	-	-	1	-	2	12	-
III	2	1.5	3	5.8	9	4.2	7.6	4.4	6.5	3.7	7	4.1	2.0	4.7	6	4.0	32	2.8	19.6	7.2	18	25	-	3	-	9	6	-	1	-	1	-	7	10	-
IV	6	2.6	4	2.4	10	2.0	4	2.9	8	3.1	4.6	2.9	13	3.1	3.5	2.8	37	1.6	33.7	15.0	20	14	-	-	-	6	5	1	-	-	2	-	8	9	-
V	4	4.2	14	3.1	7	2.4	-	-	4	2.7	4	2.2	2.0	3.1	11	2.3	29	2.0	62.0	23.9	9	1	-	-	-	14	10	2	-	-	3	-	1	16	-
VI	2	3.2	2	2.2	0.5	2.0	4.6	2.6	11.5	2.8	1.6	3.2	11.5	3.3	8	2.8	36	1.8	49.4	18.2	4	-	-	-	-	7	5	2	-	-	4	-	6	4	-
VII	-	-	-	-	6	2.5	1.5	2.7	6	3.4	2.0	4.0	18.5	3.1	3	3.7	39	2.0	99.8	23.0	8	-	-	-	-	20	14	5	1	-	2	-	4	10	-
VIII	-	-	-	-	1	2.0	4	2.8	7	1.9	11	2.5	2.5	3.6	1	5.0	44	1.6	69.4	28.5	22	-	-	-	-	15	13	1	-	-	3	-	4	5	-
IX	1	2.0	1	5.0	1	2.0	1.5	2.3	9	2.7	14.5	3.9	2.8	4.9	4	4.1	3.C	2.7	53.2	13.3	29	2	-	-	-	12	11	2	3	-	1	-	3	7	-
X	1	3.0	1	4.0	1.5	2.0	4.5	1.7	4	2.5	11.5	3.0	1.5	4.3	4.5	3.3	56	1.3	10.4	5.0	20	14	-	-	-	5	4	-	-	-	8	-	7	5	-
XI	2	8.0	6	2.9	9.5	2.7	10	2.4	8	2.4	9.5	4.8	13.5	5.4	3.5	5.7	28	2.6	29.2	12.7	28	14	-	1	-	8	5	4	1	-	3	-	4	14	-
XII	5	3.2	4.5	2.8	1.5	2.7	3.5	2.7	7.5	3.9	21	3.7	1.3	4.1	5	1.3	32	2.3	24.4	8.0	8	28	-	8	-	9	5	-	2	-	2	-	0	14	-
Rok	34.5	2.4	40	2.2	51	2.5	50	2.5	101.5	2.9	14.3	3.4	220.5	4.0	51.5	3.6	413	2.1	543.0	28.5	22.VIII	144	-	18	-	133	95	14	8	-	33	-	54	123	-

Modzurów

$\varphi = 50°10'$ $\lambda = 18°08'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnio				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.4	0.1	-1.6	-1.4	1.1	-4.3	7.5	6	-17.3	17	84	81	85	83	0.8	1.2	0.8	0.9	9.2	8.5	10.0	9.2
II	–	–	–	–	0.8	5.2	2.0	2.5	6.2	-0.7	10.2	14	-8.2	27	90	75	89	85	0.6	2.2	0.8	1.2	7.1	7.5	6.9	7.2
III	–	–	–	–	1.6	7.8	4.0	4.4	9.5	-0.5	17.9	14	-8.5	1	84	63	80	76	1.2	4.4	1.8	2.5	5.7	5.7	4.7	5.4
IV	–	–	–	–	5.0	10.9	7.4	7.7	12.4	2.5	24.8	29	-4.0	15	85	60	76	74	1.3	5.2	2.8	3.4	6.1	6.9	5.6	6.2
V	–	–	–	–	8.5	13.3	9.3	10.1	14.8	5.0	24.1	19	-0.6	7	–	–	–	–	–	–	–	–	6.6	7.5	5.2	6.4
VI	–	–	–	–	16.0	21.6	16.9	17.8	23.1	11.0	29.8	30	5.4	28	–	–	–	–	–	–	–	–	4.7	5.0	4.4	4.7
VII	–	–	–	–	17.0	21.7	17.4	18.4	23.2	13.6	33.6	8	9.9	18	–	–	–	–	–	–	–	–	6.9	6.8	6.5	6.7
VIII	–	–	–	–	13.9	19.3	15.2	15.9	20.7	10.9	26.8	11	5.8	23	–	–	–	–	–	–	–	–	5.7	6.8	4.5	5.7
IX	–	–	–	–	10.2	15.1	11.2	11.9	16.4	7.4	25.8	9	1.0	27	87	67	84	79	1.6	6.0	2.2	3.3	5.5	6.7	6.7	6.3
X	–	–	–	–	6.8	13.2	8.7	9.4	14.1	4.6	19.0	9	-0.2	24	89	65	84	79	1.2	5.7	1.8	2.9	5.7	4.9	3.5	4.7
XI	–	–	–	–	4.2	7.0	4.5	5.0	8.0	1.6	17.8	5	-9.7	30	88	76	86	83	1.1	2.8	1.3	1.7	7.8	7.2	8.0	7.7
XII	–	–	–	–	-1.5	0.3	-0.8	-0.7	1.8	-4.2	12.8	13	-11.6	16	88	82	87	86	0.7	1.2	0.8	0.9	7.8	7.4	6.1	7.1
Rok	–	–	–	–	6.7	11.3	7.8	8.4	12.6	3.9	33.6	8.VII	-17.3	17.1	–	–	–	–	–	–	–	–	6.6	6.7	6.0	6.4

Trzebinia

$\varphi = 50°10'$ $\lambda = 19°28'$

I	–	–	–	–	-2.0	0.8	-1.6	-1.1	1.5	-3.8	9.7	2	-16.7	17	–	–	–	–	–	–	–	–	8.9	7.4	7.1	7.8
II	–	–	–	–	1.2	4.9	2.3	2.7	5.9	0.2	10.7	6	-5.2	28	–	–	–	–	–	–	–	–	7.9	7.6	6.6	7.4
III	–	–	–	–	1.8	7.1	3.6	4.0	8.6	-0.3	16.4	14	-10.5	1	–	–	–	–	–	–	–	–	6.6	6.1	4.3	5.7
IV	–	–	–	–	6.4	12.2	7.8	8.8	13.4	4.0	25.6	30	-3.5	16	–	–	–	–	–	–	–	–	6.4	6.0	6.1	6.2
V	–	–	–	–	9.2	13.7	9.2	10.3	14.9	5.9	23.1	13	0.3	5,7	78	58	79	72	2.7	7.7	2.7	4.4	6.9	7.9	6.2	7.0
VI	–	–	–	–	15.8	23.2	16.6	18.0	24.3	12.3	32.1	30	4.8	28	77	48	75	68	4.2	15.0	5.1	8.1	4.0	6.1	4.8	5.0
VII	–	–	–	–	17.3	22.0	17.3	18.5	23.6	14.4	35.2	8	9.9	29	83	66	86	78	3.9	11.1	3.2	6.1	6.6	7.1	6.5	6.7
VIII	–	–	–	–	14.8	20.1	15.0	16.2	21.6	11.2	28.0	11	6.6	23	87	66	86	80	2.6	8.6	2.6	4.6	6.2	7.0	6.1	6.4
IX	–	–	–	–	9.7	15.6	11.1	11.9	16.7	8.0	27.4	9	0.1	27	95	69	90	85	0.6	6.1	1.4	2.7	7.0	7.5	5.4	6.6
X	–	–	–	–	6.6	13.6	8.6	9.4	14.5	4.6	22.6	19	0.1	5,6	–	–	–	–	–	–	–	–	5.6	5.7	3.6	5.0
XI	–	–	–	–	3.2	6.6	3.8	4.4	7.7	1.4	19.1	5	-10.5	30	91	80	90	87	0.7	2.4	0.9	1.3	7.6	6.9	7.3	7.3
XII	–	–	–	–	-2.2	0.2	-1.4	-1.2	1.8	-4.3	13.1	13	-11.1	1	86	84	86	85	0.7	1.2	0.8	0.9	8.3	7.4	7.1	7.6
Rok	–	–	–	–	6.8	11.7	7.7	8.5	12.9	4.5	35.2	8.VII	-16.7	17.1	–	–	–	–	–	–	–	–	6.8	6.9	5.9	6.5

Dąbrowa Tarnowska

$\varphi = 50°10'$ $\lambda = 20°59'$

I	–	–	–	–	-2.3	1.0	-1.7	-1.2	1.5	-4.4	7.2	6	-14.8	17	–	–	–	–	–	–	–	–	8.3	8.1	7.1	7.8
II	–	–	–	–	1.3	5.5	2.5	3.0	6.6	-0.5	11.9	6	-7.0	23	–	–	–	–	–	–	–	–	7.2	7.9	7.0	7.4
III	–	–	–	–	0.5	7.3	3.0	3.4	8.8	-1.6	17.8	30	-12.8	4	–	–	–	–	–	–	–	–	5.4	5.9	4.7	5.3
IV	–	–	–	–	5.8	12.9	7.8	8.6	14.3	2.8	26.8	28	-3.7	14	–	–	–	–	–	–	–	–	6.2	6.7	5.6	6.2
V	–	–	–	–	9.2	14.0	9.6	10.6	15.5	5.4	24.5	20	0.0	7	–	–	–	–	–	–	–	–	6.7	7.5	7.0	6.7
VI	–	–	–	–	17.0	24.1	16.9	18.7	25.5	10.8	32.5	12	3.9	1,27	–	–	–	–	–	–	–	–	5.0	5.5	3.7	4.7
VII	–	–	–	–	17.7	23.8	17.5	19.1	25.3	13.6	36.6	5,8	8.0	4	87	61	85	78	3.0	13.6	3.3	6.6	6.3	6.5	5.9	6.2
VIII	–	–	–	–	14.4	21.8	15.4	16.8	23.2	10.9	32.0	12	6.4	24	90	59	87	79	1.8	11.8	2.5	5.4	4.6	6.2	4.2	5.0
IX	–	–	–	–	10.5	16.7	11.4	12.5	17.8	7.8	27.6	9	-0.4	27	92	66	88	82	1.1	7.0	1.6	3.2	5.6	6.8	6.2	6.2
X	–	–	–	–	5.8	14.0	7.8	8.8	14.8	3.6	21.5	19	-3.7	3	92	65	88	82	0.8	6.1	1.4	2.8	5.2	5.9	4.0	5.0
XI	–	–	–	–	2.6	6.8	3.5	4.1	7.6	0.5	19.0	4	-10.0	30	91	80	83	86	0.7	2.5	1.0	1.4	6.7	6.4	6.1	6.4
XII	–	–	–	–	-2.3	0.8	-0.9	-0.8	2.0	-4.7	10.3	13	-11.9	24	88	81	85	86	0.7	1.3	0.9	1.0	6.5	7.6	6.1	6.8
Rok	–	–	–	–	6.7	12.4	7.7	8.6	13.6	3.7	36.6	5,8.VII	-14.8	17.1	–	–	–	–	–	–	–	–	6.1	6.8	6.6	6.2

Garlica Murowana

$\varphi = 50°09'$ $\lambda = 19°56'$

I	–	–	–	–	-2.0	0.4	-1.5	-1.2	1.2	-4.5	6.9	6	-17.4	17	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.3	5.0	2.7	2.9	5.9	-0.4	11.8	6	-4.8	28	–	–	–	–	–	–	–	–	7.0	6.0	6.0	6.3
III	–	–	–	–	1.0	6.5	3.5	3.6	7.9	-1.3	15.8	29	-11.8	4	–	–	–	–	–	–	–	–	5.0	4.3	5.1	4.8
IV	–	–	–	–	5.6	11.8	8.2	8.4	13.1	3.2	23.6	28	-2.5	14	–	–	–	–	–	–	–	–	6.4	5.4	6.9	6.6
V	–	–	–	–	8.6	12.9	9.6	10.2	14.4	5.5	22.6	20	0.3	30	–	–	–	–	–	–	–	–	6.7	6.8	6.3	6.6
VI	–	–	–	–	16.0	22.2	16.4	17.7	23.6	10.5	31.0	12	4.2	28	–	–	–	–	–	–	–	–	2.9	3.9	3.7	3.5
VII	–	–	–	–	16.5	21.9	17.3	18.3	23.4	13.2	34.4	6	7.8	29	–	–	–	–	–	–	–	–	6.0	5.0	5.2	5.4
VIII	–	–	–	–	13.2	19.7	15.3	15.9	21.2	10.4	27.9	12	5.1	24	–	–	–	–	–	–	–	–	3.5	4.2	3.5	3.7
IX	–	–	–	–	9.4	15.6	11.4	12.0	16.4	6.9	26.9	9	-0.8	27	–	–	–	–	–	–	–	–	4.7	4.8	4.1	4.5
X	–	–	–	–	5.6	13.3	8.5	9.0	14.3	3.3	21.9	19	-2.0	3	–	–	–	–	–	–	–	–	4.9	4.1	3.0	4.0
XI	–	–	–	–	2.3	6.1	3.6	3.9	7.0	0.4	17.3	5	-9.9	30	–	–	–	–	–	–	–	–	5.5	5.0	5.8	5.4
XII	–	–	–	–	-2.4	0.2	-1.1	-1.1	1.2	-4.8	8.7	13	-11.6	11	–	–	–	–	–	–	–	–	6.0	5.6	6.0	5.5
Rok	–	–	–	–	6.2	11.3	7.8	8.3	12.5	3.5	34.4	6.VII	-17.4	17.1	–	–	–	–	–	–	–	–	–	–	–	–

Mrzeżyno — $H_s = 271$ m — $h_w = 15$ m — 1957

MIESIĄC	ROZKŁAD WIATRU [%D, %nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	Wiatr v 10 ≤ v < 15	v ≥ 15	=	≡ 50	◔	●	▦
I	9.5	3.7	0.5	2.0	1.5	2.0	3	1.5	16.5	2.6	3.2	7.7	13.5	5.0	8.5	3.4	8	4.6	24.3	6.5	30	24	10	5	·	9	6	·	8	2	–	·	·	27	17
II	1.5	1.3	·	·	0.5	2.0	3.5	1.9	14.5	3.8	2.3	5.4	5.5	4.6	5.5	3.2	3.0	2.8	42.1	10.7	25	16	1	·	·	15	11	1	3	1	–	·	2	13	4
III	0.5	1.0	·	·	2.5	4.8	4	5.6	8.5	3.7	11	5.7	4.5	2.0	7	1.5	55	1.6	30.8	7.0	18	16	1	·	·	12	8	·	2	·	5	1	8	10	6
IV	2.2	2.4	3.5	3.0	2.5	1.6	1.5	2.7	5.5	2.5	11.5	2.5	1	1.5	21.5	2.6	21	1.9	41.6	14.4	24	9	·	·	·	10	7	1	·	·	6	·	5	10	·
V	2.3	3.1	18.5	3.0	4.5	3.1	2.5	2.4	3.5	3.6	4.5	3.1	4	3.1	19.5	3.2	13	2.7	58.3	36.5	20	1	·	·	·	8	6	2	·	·	·	1	2	13	·
VI	6.5	3.3	0.5	3.0	·	·	2.5	2.0	8	2.4	1.5	3.2	10.5	2.6	11	3.3	36	1.8	70.7	20.3	7	·	·	·	9	7	6	4	·	·	·	7	7	6	·
VII	1.2	2.5	·	·	1	1.0	6	2.9	7	2.5	1.0	3.4	8.5	3.1	14.5	2.6	34	1.8	162.3	41.5	16	·	·	·	11	19	16	6	·	·	2	8	4	16	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.9	7.5	16	·	·	·	3	14	10	·	–	–	·	2	4	7	·
IX	2.5	5.6	·	·	·	·	0.5	3.0	12.5	4.8	3.3	5.0	13.5	5.4	6	3.2	22	3.7	78.4	14.5	2	·	·	·	1	19	15	2	6	1	3	2	4	9	·
X	1.5	2.0	1	1.0	1	2.0	1	1.5	4.5	3.6	28.5	4.8	7	4.4	4	4.0	34	2.6	52	3.5	20	2	·	·	·	6	1	·	5	·	7	·	5	3	·
XI	6.5	5.3	5.5	4.6	2.5	4.2	5.5	2.3	11.5	3.6	17	5.8	4	3.5	5.5	4.4	32	2.9	19.3	4.9	2	11	1	·	·	9	5	·	7	1	4	·	2	18	·
XII	4.5	1.7	1.5	2.3	·	·	4	1.0	9	6.0	3.6	7.4	3.5	8.4	23.5	2.5	11	4.6	36.3	11.2	3	30	9	3	·	10	4	1	8	1	3	·	2	14	11
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	615.2	41.5	16.VII	109	22	8	24	138	95	17	–	–	–	21	45	146	38

Trzebinia — $H_s = 320$ m — $h_w = 14$ m

I	8	1.3	1.2	3.1	7.5	1.8	·	·	·	·	1	2.0	32.5	2.6	24	1.9	8	2.1	26.0	6.0	5	24	9	4	·	12	7	·	2	1	–	·	1	18	20
II	8	1.8	6	2.3	9	2.8	2	2.0	2.5	2.2	4.5	3.0	30.5	2.3	19.5	1.6	2	2.1	36.4	14.0	21	11	1	·	·	10	7	1	2	1	–	·	1	12	6
III	16.5	1.7	18.5	2.3	19.5	7.6	·	·	2	1.0	3	2.2	16.5	3.4	14	2.2	3	3.4	54.1	17.5	18	14	2	1	·	10	8	2	4	3	–	·	7	10	4
IV	29.5	1.9	16.5	1.9	16.5	1.4	0.5	2.0	0.5	2.0	4.5	1.3	8.5	1.2	11.5	1.8	3	1.6	36.5	16.0	30	5	·	·	1	11	8	1	·	·	–	1	5	10	·
V	20.5	1.2	2.7	2.6	21.5	2.0	1	3.0	·	·	·	·	4	1.8	12	2.4	7	1.9	36.3	10.0	20	·	·	·	·	7	5	1	2	·	–	1	·	15	·
VI	10.5	1.3	8.5	1.2	16	1.5	1.5	1.3	3.5	2.2	5.5	2.7	15.5	2.5	22	1.9	7	1.7	48.8	25.0	7	·	·	·	13	9	7	1	·	·	–	4	2	1	·
VII	14.5	1.6	9.5	1.3	2	1.8	·	·	2	4.5	1.5	4.3	27.5	2.3	30	1.5	6	1.8	210.5	91.0	16	·	·	·	8	18	18	5	2	1	–	6	2	12	·
VIII	11	1.2	4	1.1	1.5	1.0	·	·	·	·	2.5	2.0	36	1.8	37	1.4	1	1.5	98.9	17.5	21	·	·	·	6	14	12	3	·	·	–	4	1	10	·
IX	7.5	1.7	3.5	1.4	6.5	1.4	0.5	1.0	3	1.3	9	2.6	41.5	2.9	16.5	2.0	2	2.3	87.8	15.0	29	·	·	·	2	16	14	4	3	1	–	·	3	12	·
X	4	1.5	4.5	1.4	14.5	1.6	·	·	0.5	1.0	6.5	1.6	34.5	2.1	17.5	1.2	11	1.5	13.6	6.5	20	·	·	·	·	8	3	·	1	·	–	·	5	5	·
XI	3	9.7	3.5	6.0	4.0	3.4	5	1.6	5	2.9	2.5	6.0	19.5	3.0	4.5	6.9	7	3.5	40.8	14.5	28	11	3	1	·	9	6	1	5	2	–	·	2	17	·
XII	7	1.4	3.5	2.0	12	3.7	1	1.0	4.5	1.2	5.5	4.7	38	2.3	12.5	2.8	9	2.3	34.3	7.0	16	25	8	3	·	16	11	·	2	1	–	·	·	18	7
Rok	14.0	2.2	11.7	2.2	16.5.5	2.5	11.5	1.0	23.6	1.5	4.6	2.7	30.4.5	2.4	22.1	2.3	66	2.1	719.2	91.0	16.VII	90	23	9	30	140	106	19	23	10	–	16	29	140	37

Dąbrowa Tarnowska — $H_s = 210$ m — $h_w = 10$ m

I	3	2.7	5.5	6.9	2	6.8	0.5	3.0	17.5	3.6	11.5	2.8	21.6	3.4	11.5	5.5	20	3.1	28.7	10.2	5	23	7	6	·	14	8	1	5	1	–	·	·	17	24
II	0.5	3.0	2	2.0	·	·	5.5	9.2	26.5	5.6	8.5	4.6	11.6	4.2	10.5	2.1	19	3.7	38.2	7.5	21	15	2	·	·	14	10	·	6	2	–	·	1	15	8
III	11.5	4.6	4	1.5	11	6.6	8	6.8	6	4.6	3	3.8	14	3.9	13.5	4.8	22	3.4	33.5	10.5	18	17	3	1	·	11	6	1	8	1	–	1	8	8	5
IV	14.5	1.9	6	1.9	4	2.4	0.5	2.0	6.5	3.8	3.5	1.4	7	2.4	18	2.7	30	1.6	57.9	14.7	11	9	·	·	3	15	10	2	·	·	–	3	5	11	1
V	14.6	2.4	13	2.9	5.5	3.9	0.5	5.0	4	3.1	3	2.5	11.5	2.0	18	2.6	23	2.0	68.9	23.7	10	·	·	·	15	10	8	3	·	·	–	2	3	16	·
VI	8.5	1.7	6	2.3	1	3.5	5.5	4.6	10	4.5	3	3.2	11.5	2.9	23.5	3.6	21	2.5	20.4	6.0	22	·	·	·	15	10	6	·	2	·	–	4	6	2	·
VII	4.5	1.7	5.5	2.2	1	5.5	5	4.2	3.5	1.7	8.5	2.8	15.5	3.7	20.5	2.6	29	2.0	92.1	22.6	16	·	·	·	14	19	14	1	2	·	–	7	4	9	·
VIII	1.5	2.3	1	1.0	1.5	3.0	4	3.1	6.5	3.1	4.5	2.3	10.5	3.7	22.5	3.0	41	1.7	107.3	26.4	7	·	·	·	9	16	11	4	1	·	–	5	4	3	·
IX	2.5	1.4	2.5	1.8	0.5	2.0	1	1.5	1.0	2.6	15.5	3.4	15.5	3.7	9.5	3.3	33	1.9	57.7	10.7	4	2	·	·	3	14	12	1	1	·	–	1	3	9	·
X	·	·	1	3.0	2	2.5	8.5	2.4	14.5	2.1	6	2.2	9.5	2.6	8.5	1.7	43	1.2	19.4	6.2	20	2	·	·	·	6	4	·	·	·	–	·	5	6	·
XI	1.5	7.3	6	4.1	9	3.6	14.5	3.6	8.5	5.0	6.5	5.0	10.5	6.0	6.5	6.9	27	3.4	9.3	2.6	29	11	3	·	·	8	5	·	5	·	–	·	7	16	·
XII	2	1.5	3.5	2.9	2.5	2.8	8	4.6	1.3	3.3	10.5	3.9	10	3.7	6.5	3.2	37	2.1	26.0	8.7	8	28	8	4	·	1.1	6	·	2	·	–	·	4	13	2
Rok	6.4.5	2.3	56	2.7	40	3.5	6.1.5	4.2	12.6.5	3.6	8.4	3.1	14.8.5	3.5	16.9	3.5	34.5	2.4	560.4	26.4	7.VIII	107	23	11	44	148	100	13	32	4	–	23	50	125	40

Garlica Murowana — $H_s = 270$ m — $h_w = 17$ m

I	·	·	1.0	4.5	0.5	1.0	2	1.0	1.5	1.3	1.2	2.8	26.5	3.2	3.5	3.7	37	1.9	17.2	6.4	13	26	10	4	·	11	4	·	·	·	–	·	–	–	–
II	1.5	1.3	2	1.5	6.5	2.7	6.5	3.4	3	2.2	9.5	2.5	14.5	3.1	2.5	2.4	38	1.6	31.2	9.2	26	15	2	·	·	14	9	·	·	·	–	·	3	11	–
III	3	2.2	4	2.5	2.2	4.1	2	2.7	1.5	1.6	6	4.2	13	4.6	7.5	3.7	34	2.6	43.3	13.5	18	17	3	1	·	11	6	1	3	·	–	1	8	8	–
IV	9	2.1	7.6	2.0	8.5	2.3	4	3.0	2.5	2.4	8.5	2.0	14	2.2	6	3.6	30	1.6	55.3	22.0	7	5	·	·	·	11	7	1	1	·	–	3	7	8	–
V	5.5	2.9	2.6	3.3	5.5	5.2	1.5	5.0	·	·	4.5	2.5	11.5	2.9	9.5	3.0	29	2.2	33.7	11.0	10	·	·	·	·	8	5	1	·	·	–	2	3	14	–
VI	6	3.4	8.5	2.3	13.5	2.0	5	3.3	1	4.0	6.5	2.5	16	3.6	7.5	3.9	26	2.1	33.2	12.4	7	·	·	·	12	8	6	1	1	·	–	7	10	2	–
VII	3	2.0	2	2.0	6.5	3.8	3.5	3.4	·	·	8	2.9	18.5	2.9	9.5	3.2	42	1.7	152.9	33.4	16	·	·	·	9	16	14	7	·	·	–	8	5	7	–
VIII	2.5	4.0	2.5	2.2	3	4.0	·	·	2.5	2.2	12	2.8	22.5	3.4	9	2.9	39	1.8	70.9	14.6	28	·	·	·	4	15	11	2	2	1	–	4	11	3	–
IX	3	2.4	3.5	3.1	2	2.7	5	2.5	1	2.0	14.5	4.1	8.2	4.0	3	3.5	26	2.6	50.5	11.3	23	1	·	·	2	16	11	1	·	·	–	·	4	4	–
X	1	1.5	3	2.2	6	3.3	3	1.7	·	·	8	2.9	8.5	3.8	3.5	2.9	60	1.1	9.6	5.4	20	2	·	·	·	3	2	·	·	·	–	·	9	2	–
XI	3.5	6.7	9.5	3.2	24.5	2.8	4.5	3.3	·	·	5	3.8	13	4.2	2	5.2	28	2.5	17.0	7.2	28	13	3	·	·	9	6	·	1	·	–	·	5	10	–
XII	7.5	3.5	4	4.0	9.5	3.4	1.5	2.0	·	·	14.5	3.6	28	3.3	4	4.4	24	2.6	18.1	6.2	8	28	10	3	·	12	5	·	·	·	–	·	4	9	–
Rok	4.5.5	2.7	82.5	2.7	108	3.1	38.5	2.8	13	1.3	109	3.0	21.8	3.4	67.5	3.6	413	2.0	532.9	33.4	16.VIII	107	28	8	27	134	86	14	8	1	–	25	–	–	–

Lubaczów

$\varphi = 50°09'$ $\lambda = 23°08'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies																		
I	-	-	-	-	-3.6	-0.4	-2.3	-2.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8.9	8.6	8.5	8.7
II	-	-	-	-	0.9	4.9	1.8	2.4	5.8	-	11.9	6	-	-	-	-	-	-	-	-	-	-	8.4	7.6	7.0	7.7
III	-	-	-	-	-0.7	6.2	1.6	2.2	6.8	-	16.4	21,31	-	-	-	-	-	-	-	-	-	-	6.4	6.1	5.2	5.9
IV	-	-	-	-	6.0	13.8	7.4	8.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.2	6.3	5.1	5.9
V	-	-	-	-	9.3	13.6	9.5	10.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.4	8.2	7.6	7.7
VI	-	-	-	-	16.6	23.3	16.5	18.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4.8	5.6	4.3	4.9
VII	-	-	-	-	17.4	23.2	17.3	18.8	-	-	-	-	-	-	87	62	87	79	2.8	11.9	2.8	5.8	6.9	6.5	7.1	6.8
VIII	-	-	-	-	14.7	20.9	15.1	16.4	-	-	-	-	-	-	91	64	94	82	1.6	9.4	1.6	4.2	6.2	6.4	4.8	5.8
IX	-	-	-	-	10.3	16.6	11.2	12.3	-	-	-	-	-	-	94	65	91	83	0.8	7.0	1.2	3.0	6.9	7.4	6.2	6.8
X	-	-	-	-	4.5	13.4	5.9	7.4	-	-	-	-	-	-	95	64	91	83	0.5	6.1	1.0	2.5	7.5	5.3	4.2	5.7
XI	-	-	-	-	2.1	6.3	2.5	3.4	-	-	-	-	-	-	88	76	88	84	0.8	2.5	0.8	1.4	8.0	7.4	6.6	7.3
XII	-	-	-	-	-3.2	0.4	-1.8	-1.6	-	-	-	-	-	-	84	76	82	81	0.8	1.6	1.0	1.1	8.3	7.6	6.5	7.5
Rok	-	-	-	-	6.2	11.8	7.1	8.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7.2	6.9	6.1	6.7

Tychy

$\varphi = 50°08'$ $\lambda = 18°59'$

I	-	-	-	-	-2.1	0.8	-1.3	-1.0	1.5	-3.8	7.2	6	-16.7	17	91	80	89	87	0.5	1.3	0.6	0.8	7.6	7.0	7.3	7.3
II	-	-	-	-	0.8	5.3	2.6	2.8	6.4	-0.4	10.9	15	-10.2	27	92	77	88	86	0.6	2.3	1.0	1.3	6.9	7.4	6.9	7.1
III	-	-	-	-	1.1	7.4	4.0	4.1	9.3	-0.2	19.4	26	-10.2	1	87	70	88	82	0.9	3.8	1.1	1.9	6.8	5.8	5.4	6.0
IV	-	-	-	-	4.6	11.9	7.6	7.9	13.6	2.9	26.1	30	-2.9	16	93	65	84	81	0.7	6.2	1.9	2.9	5.8	7.0	5.7	6.2
V	-	-	-	-	8.1	13.8	9.5	10.2	15.1	5.2	24.3	19	0.1	6,7,30	87	63	82	77	1.4	6.6	2.2	3.4	5.9	8.5	6.2	6.9
VI	-	-	-	-	15.8	22.8	17.1	18.2	24.3	11.1	31.7	30	4.8	27	84	59	82	75	2.9	12.1	3.8	6.3	4.1	6.4	4.2	4.9
VII	-	-	-	-	16.6	22.1	17.2	18.3	23.8	13.8	35.8	8	8.7	29	-	-	-	-	-	-	-	-	6.6	7.0	6.9	6.8
VIII	-	-	-	-	13.1	20.1	14.7	15.6	21.7	10.6	28.9	11	4.2	31	94	65	89	83	1.1	8.7	2.0	3.9	6.6	6.9	4.7	6.1
IX	-	-	-	-	9.1	15.7	11.1	11.8	17.2	7.4	27.9	8,9	0.1	27	95	71	91	86	0.6	5.6	1.2	2.5	5.6	7.1	5.9	6.2
X	-	-	-	-	4.7	13.6	7.5	8.3	14.7	3.2	21.9	19	-1.4	26	96	70	93	86	0.4	5.0	0.8	2.1	6.4	5.3	3.2	5.0
XI	-	-	-	-	2.7	6.7	3.9	4.3	7.7	1.2	19.4	5	-9.4	30	95	81	91	89	0.4	2.3	0.8	1.2	8.9	7.0	7.5	7.8
XII	-	-	-	-	-2.1	0.4	-0.9	-0.9	1.8	-4.0	13.9	13	-13.1	11	91	83	89	88	0.5	1.3	0.6	0.8	8.4	6.2	6.2	6.9
Rok	-	-	-	-	6.0	11.7	7.8	8.5	13.1	3.9	35.8	8.VII	-16.7	17.1	-	-	-	-	-	-	-	-	6.6	6.8	5.8	6.4

Rybnik

$\varphi = 50°06'$ $\lambda = 18°33'$

I	-	-	-	-	-1.9	0.8	-1.0	-0.8	-	-3.2	-	-	-17.4	17	-	-	-	-	-	-	-	-	9.1	7.7	8.3	8.4
II	-	-	-	-	1.5	5.5	2.9	3.2	-	0.1	-	-	-8.3	28	-	-	-	-	-	-	-	-	7.5	8.5	7.8	7.9
III	-	-	-	-	2.0	8.0	4.4	4.7	9.5	0.2	17.1	14	-7.7	1	-	-	-	-	-	-	-	-	7.2	6.4	5.1	6.2
IV	-	-	-	-	5.6	11.9	8.4	8.6	13.6	3.1	25.5	29	-3.0	16	84	59	76	73	1.7	7.1	2.8	3.9	6.6	7.1	6.5	6.7
V	-	-	-	-	9.3	14.0	9.9	10.8	15.3	5.8	25.1	19	0.3	7	79	57	78	71	2.6	7.7	2.9	4.4	7.2	7.9	8.1	7.7
VI	-	-	-	-	16.0	22.6	17.5	18.4	24.2	12.1	31.4	11	5.4	28	79	57	77	71	3.9	12.6	4.9	7.1	5.1	6.3	5.8	5.7
VII	-	-	-	-	17.0	22.4	18.1	18.9	24.0	14.6	35.3	8	11.6	19,29,30	87	66	85	79	2.8	10.4	3.4	5.5	7.8	7.1	7.5	7.5
VIII	-	-	-	-	13.8	20.4	15.6	16.4	22.1	11.4	29.7	11	6.8	24	88	58	81	76	2.0	10.5	3.5	5.3	6.7	6.5	4.4	5.9
IX	-	-	-	-	10.0	15.9	11.7	12.3	17.1	8.2	27.5	9	0.6	27	89	67	88	81	1.4	6.6	1.7	3.2	7.0	7.2	7.3	7.2
X	-	-	-	-	6.7	13.9	8.8	9.6	14.7	4.8	20.2	19	-1.1	26	90	63	85	79	1.0	6.3	1.8	3.0	6.8	5.5	3.9	5.4
XI	-	-	-	-	3.8	7.7	4.7	5.2	8.4	2.6	19.5	5	-8.7	30	90	75	87	84	0.9	3.2	1.3	1.8	8.1	7.2	8.0	7.8
XII	-	-	-	-	-1.7	1.0	-0.3	-0.3	2.2	-3.0	13.6	13	-11.7	11	-	-	-	-	-	-	-	-	8.3	7.6	7.5	7.8
Rok	-	-	-	-	6.8	12.0	8.4	8.9	-	4.7	35.3	8.VII	-17.4	17.1	-	-	-	-	-	-	-	-	7.3	7.1	6.7	7.0

Igołomia

$\varphi = 50°06'$ $\lambda = 20°16'$

I	-	-	-	-	-2.4	0.9	-2.0	-1.4	1.4	-5.6	7.2	2	-18.5	17	-	-	-	-	-	-	-	-	8.5	7.3	7.9	7.9
II	-	-	-	-	0.8	5.7	2.1	2.7	6.9	-1.1	12.2	6	-5.3	24	-	-	-	-	-	-	-	-	8.1	7.0	7.8	7.6
III	-	-	-	-	0.6	7.9	2.9	3.6	9.1	-2.0	18.0	14	-10.5	4	-	-	-	-	-	-	-	-	6.1	5.4	5.0	5.5
IV	-	-	-	-	5.9	13.0	7.9	8.7	14.1	2.4	25.7	30	-3.9	14	-	-	-	-	-	-	-	-	6.3	6.7	6.4	6.5
V	-	-	-	-	9.5	14.1	10.1	11.0	15.8	5.3	23.8	18	1.1.0	30	-	-	-	-	-	-	-	-	6.6	6.6	6.7	6.6
VI	-	-	-	-	16.2	23.1	16.7	18.2	24.9	10.4	31.5	11	4.9	27	-	-	-	-	-	-	-	-	4.0	4.7	3.5	4.1
VII	-	-	-	-	17.6	23.2	17.6	19.0	24.4	13.1	35.4	5	8.4	30	-	-	-	-	-	-	-	-	5.6	5.5	6.8	6.0
VIII	-	-	-	-	14.3	21.0	15.8	16.7	22.4	10.5	29.7	12	5.4	24	-	-	-	-	-	-	-	-	5.4	5.9	6.7	6.0
IX	-	-	-	-	10.0	16.9	11.6	12.5	17.9	6.9	27.9	9	-0.8	25	-	-	-	-	-	-	-	-	5.3	5.8	5.6	5.6
X	-	-	-	-	4.9	14.4	7.4	8.5	15.1	1.9	22.8	19	-3.4	3	-	-	-	-	-	-	-	-	4.7	3.8	3.6	4.0
XI	-	-	-	-	2.1	6.7	3.4	3.9	-	-0.1	-	-	-9.7	30	-	-	-	-	-	-	-	-	7.6	7.0	6.8	7.1
XII	-	-	-	-	-2.7	0.7	-1.5	-1.2	-	-5.5	-	-	-12.2	11	-	-	-	-	-	-	-	-	7.5	7.1	7.3	7.3
Rok	-	-	-	-	6.4	12.3	7.7	8.6	-	3.0	35.4	5.VII	-18.5	17.1	-	-	-	-	-	-	-	-	6.3	6.1	6.1	6.2

Lubaczów

$H_s = 214$ m $h_w = 16$ m 1957

MIESIĄC	ROZKŁAD WIATRU °D, °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Sumo	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0,1 ÷ 1	1,0 ÷ 10	10,0 >	Wiatr v 10 ÷ 15	15 >	III	25	◔	●	◧
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20,9	5,1	6	-	-	-	·	14	8	·	-	-	1	·	·	23	24
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26,8	5,2	15	-	2	-	·	13	9	·	-	-	2	·	1	16	6
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	26,5	11,4	18	-	6	-	·	8	5	1	-	-	·	·	4	9	3
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	14,9	8,3	11	-	-	-	-	6	2	·	-	-	·	1	5	10	·
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	73,8	21,5	9	-	-	-	-	12	12	3	-	-	·	1	·	17	·
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	56,1	16,8	4	-	-	-	-	7	6	3	-	-	1	3	2	2	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92,6	19,6	8	-	-	-	-	16	12	2	-	-	·	5	1	14	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55,8	14,5	10	-	-	-	-	14	10	2	-	-	2	2	1	5	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	70,0	18,4	12	-	-	-	-	15	12	2	-	-	5	1	1	12	·
X	6,5	1,0	·	·	4	1,0	7	1,3	8,5	1,4	1,3	1,3	2,2	1,8	9	1,2	2,3	1,1	10,8	6,8	20	-	-	-	-	4	3	·	·	·	5	·	3	7	·
XI	4,5	6,3	6,5	2,1	1,4	2,0	2,1,5	2,0	7,5	1,4	6,5	1,3	11,5	4,4	9	5,6	9	2,6	36,8	16,7	28	-	-	-	-	7	6	1	1	·	2	·	1	16	1
XII	12,5	2,2	1	2,0	2	2,0	19,5	2,0	4	1,8	3,0	1,7	10,5	1,9	7,5	1,7	6	1,7	36,3	17,3	8	-	-	-	-	8	5	1	·	·	2	·	·	17	7
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	521,3	21,5	9,V	-	-	-	-	124	90	15			20	13	19	148	41

Tychy

$H_s = 280$ m $h_w = 15,5$ m

I	6	4,2	8	4,0	2	1,0	·	·	·	·	11	3,9	3,5	3,8	2,0	5,1	11	3,6	27,5	6,3	5	25	10	3	·	10	8	·	4	·	-	·	2	17	22
II	3	3,3	7	3,9	3	3,7	4	4,0	7	3,9	14	4,9	27,5	3,9	9,5	5,6	9	3,8	50,1	12,0	25	15	1	1	·	15	11	1	2	·	-	·	·	11	5
III	7,5	3,2	8,5	4,6	22,5	6,4	1,5	3,0	·	·	8,5	3,5	1,8	4,5	13,5	4,7	1,3	4,2	50,7	15,1	18	13	2	1	·	10	8	1	5	1	-	1	6	11	4
IV	13,5	3,1	9,5	2,8	8,5	2,5	4,5	3,1	5	3,0	4	2,8	6	3,4	2,3	3,5	1,6	2,6	41,3	14,4	7	6	·	·	1	12	10	1	1	·	-	·	4	9	·
V	7	2,8	18,5	5,2	15,5	4,4	2	5,0	2	2,5	1,5	2,0	8	3,5	17,5	4,2	2,1	3,2	28,0	7,2	10,20	·	·	·	·	8	6	·	1	·	-	1	·	15	·
VI	6,5	3,4	4	3,5	11,5	2,9	3,5	3,1	3	2,7	12	5,1	1,7	3,2	10,5	3,3	2,2	2,7	64,4	22,1	8	·	·	·	1,3	7	7	2	2	·	-	5	5	4	·
VII	3	2,8	4	1,8	9	3,7	1	3,0	1	3,0	1,8	3,2	2,3	3,4	1,3	3,2	2,1	2,5	141,9	32,2	20	·	·	·	1,2	16	16	4	·	·	-	4	2	14	·
VIII	3,5	2,0	1,5	2,7	2,5	3,2	2	2,5	3	4,3	1,1	3,8	2,5	4,3	1,3,5	3,5	3,1	2,5	93,3	22,2	14	·	·	·	6	10	10	3	2	1	-	2	2	8	·
IX	2,5	2,6	0,5	3,0	3	1,7	5	3,2	3	2,7	1,3	5,9	2,7,5	3,9	10,5	5,2	2,5	3,1	77,6	14,7	2	·	·	·	2	1,6	1,6	2	3	·	-	·	3	11	·
X	1	2,0	4	1,2	4	2,6	1	3,5	2	3,0	1,3,5	3,2	2,0,5	3,2	7	2,7	4,0	1,7	10,0	5,1	20	3	·	·	·	2	2	·	·	·	-	·	3	3	·
XI	4	7,0	1,4	6,0	2,1	3,7	4,5	3,1	3,5	3,1	8	4,3	1,4	5,5	1	1,7,0	2,0	3,8	22,0	7,4	28	10	3	·	·	7	7	·	3	1	-	·	·	19	·
XII	6	3,0	3	3,2	6	4,8	5	3,2	4	3,5	2,2,5	6,4	2,0,5	4,2	7	3,6	1,9	3,7	39,6	7,4	8	2,6	1,1	2	·	1,1	1,1	·	5	2	-	·	3	1,4	6
Rok	6,3,5	3,3	8,2,5	3,5	10,8,5	3,4	3,4	2,9	3,3,5	2,6	1,3,7	4,1	2,4,2	3,9	1,4,6	5,1	2,4,8	3,1	64,6,4	3,2,2	20.VII	9,8	2,7	7	3,4	1,2,4	1,1,2	1,4	2,8	5	-	1,3	3,0	1,3,6	3,7

Rybnik

$H_s = 243$ m $h_w = 11,5$ m

I	0,5	4,0	4,5	4,2	·	·	·	·	2,5	5,0	4,1	3,5	6,5	2,7	5	2,6	3,3	2,2	7,5	4,2	6	2,2	-	4	·	9	2	·	2	·	·	·	·	23	18
II	1	1,0	1	1,0	2	2,5	3	2,0	4,5	3,4	4,6	3,0	6	3,6	6,5	1,6	1,4	2,4	36,6	17,2	18	1,2	-	·	·	11	5	1	·	·	2	·	1	15	4
III	2,5	2,4	1,2	4,2	7	5,3	7	1,9	0,5	4,0	2,0,5	3,9	1,2	2,2	4,5	2,7	2,7	2,4	39,3	9,3	17	1,3	2	·	·	11	7	·	2	2	2	1	4	10	2
IV	7,5	2,6	4	3,0	1	2,0	6	2,0	1	1,0	4,6	2,7	8,5	2,4	2,5,5	2,5	5,2	1,6	40,0	11,4	7	7	·	·	1	11	7	1	·	·	3	·	3	13	·
V	6,5	3,5	17,5	4,0	2	3,0	2,5	2,4	3	2,0	5,5	2,3	1,6,5	2,2	19,5	2,2	2,1	2,2	80,2	6,5,5	20	·	·	·	1	7	4	1	·	·	·	1	·	17	·
VI	5	2,2	4,5	2,7	1	1,0	6	2,5	1	5,0	2,2	2,3	1,3	2,1	11,5	2,7	2,6	1,7	87,1	31,5	7	·	·	·	1,3	10	8	4	·	·	·	4	4	7	·
VII	3	2,3	1	3,0	2	3,0	4	2,5	·	·	2,4,5	3,1	11,5	2,1	10	2,2	3,7	1,8	134,2	52,5	16	·	·	·	1,3	16	14	3	·	·	·	6	·	18	·
VIII	1	1,0	·	·	·	·	1	2,0	1	1,0	2,0,5	2,4	14,5	1,9	15	2,2	4,0	1,2	83,9	38,2	14	·	·	·	6	10	10	1	·	·	·	2	2	7	·
IX	1	1,0	·	·	·	·	3,5	3,4	2,5	3,4	3,4,5	3,5	16	2,7	7,5	2,5	2,5	2,3	88,0	14,1	14	·	·	·	2	1,9	14	3	·	·	1	·	·	14	·
X	·	·	1	4,0	0,5	1,0	1,5	1,7	1	2,0	2,9	2,7	10	2,6	6	1,2	4,4	1,3	8,7	3,8	20	1	·	·	·	3	3	·	·	·	1,1	·	4	5	·
XI	5	4,0	1,6	2,7	8,5	1,6	8,5	1,5	1	6,0	2,1,5	2,7	5,5	2,4	3	3,3	2,1	2,0	16,8	8,9	28	9	1	·	·	7	3	·	·	·	5	·	3	2,1	·
XII	3	1,7	5	2,0	1	1,0	4	1,5	2	1,0	4,1	3,8	1,1	1,6	9	1,1	1,7	2,2	26,5	8,7	8	2,5	7	2	·	1,1	6	·	·	·	2	·	1	17	3
Rok	3,6	2,1	5,6,5	2,6	2,5	1,7	4,7	2,0	2,0	2,8	3,1,0,5	3,0	1,3,0	2,4	1,2,3	2,2	3,3,7	1,9	64,8,8	6,5,5	20.V	8,9	-	6	3,6	1,2,5	8,3	1,4	4	2	2,6	1,4	2,2	1,6,7	2,7

Igołomia

$H_s = 202$ m $h_w = 14$ m

I	3	2,7	1	1,0,0	7	6,5	0,5	3,0	1,5	3,0	1	6,0	3,3	4,2	3	5,5	4,3	2,5	32,1	10,1	13	2,7	9	5	·	1,4	7	1	3	·	-	·	2	17	-
II	4,5	2,0	1,5	3,0	8	2,7	2	5,0	9,5	3,1	6,5	5,0	11	4,4	1,3	4,4	2,8	2,5	33,8	11,7	21	2,0	2	·	·	11	6	2	1	·	-	·	·	14	-
III	3	3,7	5	2,2	2,2	5,6	5	4,0	·	·	4	3,0	1,6	6,2	8	3,5	3,0	3,1	37,3	11,1	19	2,1	2	1	·	7	6	2	5	·	-	1	6	8	-
IV	19,5	3,5	3,5	2,6	1,0	2,9	2	2,0	3	2,3	7	3,0	8	2,9	1,3	2,6	2,4	2,2	58,5	11,7	7	8	·	·	1	1,6	1,2	2	·	·	-	5	2	11	-
V	2,3	3,5	17,5	4,0	1,6	4,0	2	5,0	2	3,0	1	2,0	3	3,3	13,5	3,2	1,5	3,1	35,4	11,1	10	·	·	·	·	7	4	2	1	·	-	1	4	12	-
VI	1,1	2,7	9	2,3	9	3,3	1	1,0	3	3,3	1	2,0	8	4,4	2,2	3,1	2,6	2,2	58,0	26,2	22	·	·	·	1,6	11	7	1	1	·	-	8	5	1	-
VII	2,0	2,2	5	1,6	6	4,3	·	·	2	3,0	2	3,0	1,7	3,5	1,7	3,9	2,4	2,3	199,3	53,0	16	·	·	·	1,4	1,6	1,6	4	·	·	-	7	·	7	-
VIII	2,6	2,6	3	2,7	1	2,0	·	·	2	5,5	3	5,7	1,6	4,0	1,4	3,3	2,8	2,3	67,0	19,7	28	·	·	·	8	1,2	9	2	·	·	-	2	2	6	-
IX	1,1	2,6	1,5	3,0	3	2,0	1	3,0	·	·	1	2,0	3,1	4,7	1,5,5	3,5	2,6	2,7	54,2	14,0	23	2	·	·	2	1,4	1,2	1	2	·	-	·	3	5	-
X	1,3,5	2,0	1	1,0	3	3,7	2	4,0	1	3,0	1	2,0	1,6	4,1	3,5	2,9	5,2	1,4	1,4,0	5,4	23	6	·	·	·	5	3	·	·	·	-	·	6	4	-
XI	9	7,7	1,2	2,5	2,4	5,1	·	·	3	2,7	·	·	7	8,1	1,0	7,7	2,5	4,0	1,9,1	5,5	28	1,2	-	·	·	1,0	6	·	7	1	-	·	5	1,7	-
XII	9,5	3,4	9,5	5,0	5	2,7	1	3,0	1	3,0	2	6,0	1,9,5	4,1	6,5	5,1	3,9	2,4	2,0,9	8,2	1,4	2,9	-	3	·	1,2	5	·	1	·	-	·	2	1,6	-
Rok	1,5,3	3,2	6,2,5	3,3	1,1,4	3,7	1,6,5	2,5	2,8	2,7	2,9,5	4,3	1,8,5,5	4,4	1,3,9	4,0	3,6,0	2,6	6,2,9,6	5,3,0	16.VII	1,2,5	-	9	4,1	1,3,5	9,3	1,7	2,1	1	-	2,4	3,7	1,1,8	-

Rzeszów - Jasionka

$\varphi = 50°06'$ $\lambda = 22°03'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	998.4	1009.0	982.8	1023.6	-2.3	-0.3	-4.7	-4.5	0.8	-4.4	5.5	2	-15.6	17	87	80	87	85	0.7	1.3	0.7	0.9	8.5	8.2	7.6	8.1
II	989.6	1006.0	967.2	1014.2	1.6	4.4	2.4	2.7	6.8	0.4	12.1	19	-6.2	28	88	77	85	83	0.9	2.1	1.1	1.4	7.4	8.3	6.4	7.4
III	995.7	1010.3	975.5	1020.4	-0.5	5.4	2.0	2.2	7.5	-2.1	17.2	31	-13.8	4	84	66	80	77	1.1	3.7	1.5	2.1	5.7	6.0	4.1	5.3
IV	994.1	1005.5	970.6	1018.2	4.9	13.2	7.7	8.4	14.7	2.6	26.2	30	-3.1	16	88	56	82	75	1.1	7.9	2.0	3.7	6.4	5.8	5.5	5.9
V	991.8	1000.2	980.3	1015.6	8.5	13.5	9.7	10.4	15.0	5.6	23.7	18	0.1	7	89	65	85	80	1.2	6.7	1.9	3.3	6.8	7.7	7.7	7.4
VI	994.0	1006.5	981.9	1017.3	16.5	23.1	17.0	18.4	24.7	10.5	33.2	12	4.6	28	79	50	79	69	4.2	14.8	4.3	7.8	4.6	5.4	3.9	4.6
VII	989.8	999.6	980.1	1012.9	17.2	23.2	18.3	19.2	24.9	13.8	35.6	5	8.4	4	86	60	83	76	2.9	12.9	3.6	6.5	6.5	6.6	6.8	6.6
VIII	992.0	1004.6	980.7	1015.3	14.4	21.0	15.9	16.8	22.5	11.2	30.7	14	4.8	24	91	59	86	79	1.5	11.0	2.7	5.1	5.3	5.9	5.1	5.4
IX	991.3	1000.4	978.5	1015.0	10.2	16.2	12.0	12.6	17.5	8.2	27.0	9	0.0	27	94	64	87	81	1.2	7.0	1.8	3.3	6.8	6.7	6.9	6.8
X	997.9	1007.4	982.3	1022.1	5.2	13.3	7.1	8.2	14.2	3.1	20.2	19	-4.4	3	93	63	88	81	0.9	6.1	1.5	2.8	6.0	5.6	3.6	5.1
XI	997.7	1016.3	979.8	1022.4	4.9	6.6	3.1	3.7	7.7	0.1	17.9	4	-9.4	30	94	76	89	86	0.4	2.7	0.9	1.3	7.2	6.8	6.4	6.8
XII	992.7	1012.2	958.7	1017.6	-4.9	0.7	-4.0	-3.8	1.7	-4.1	10.5	13	-14.0	11	89	78	87	85	0.6	1.4	0.7	0.9	6.5	7.4	6.4	6.8
Rok	993.8	1016.3	958.7	1017.9	6.3	11.7	7.7	8.4	13.4	3.7	35.6	5.VII	-15.6	17.1	88	66	85	80	1.4	6.5	1.9	3.3	6.5	6.7	5.9	6.4

Racibórz

$\varphi = 50°05'$ $\lambda = 18°13'$

I	998.8	1010.1	981.6	1023.7	-2.1	0.8	-1.4	-1.0	2.0	-3.5	8.4	6	-15.7	17	85	76	84	82	0.9	1.6	1.0	1.2	7.5	7.9	7.4	7.6
II	988.9	1008.4	963.9	1013.1	1.0	5.9	2.6	3.0	7.1	0.0	11.7	14	-11.1	27	87	68	84	80	0.9	3.1	1.2	1.7	6.8	7.8	6.7	7.1
III	995.0	1010.7	976.9	1019.3	1.6	8.1	4.5	4.7	10.1	0.4	18.4	14	-7.2	4	83	58	76	72	1.3	5.2	2.2	2.9	7.0	6.3	5.1	6.1
IV	994.7	1006.8	972.1	1018.6	4.7	11.9	7.9	8.1	13.6	3.0	25.6	29	-3.7	16	88	54	75	72	1.2	7.6	2.8	3.9	6.0	6.7	5.4	6.0
V	992.4	1000.5	982.6	1016.0	8.9	14.5	10.0	10.8	16.0	6.0	26.2	19	-0.4	7	79	53	77	70	2.4	8.4	3.1	4.6	6.3	7.5	5.2	6.3
VI	994.0	1008.0	984.2	1017.2	15.5	22.6	16.8	17.9	24.5	11.8	31.3	30	6.4	1.28	79	54	81	71	3.8	13.3	3.9	7.0	5.0	5.4	4.4	4.9
VII	990.1	1002.3	978.4	1013.1	16.9	22.5	17.4	18.6	24.3	14.4	35.2	5	10.6	30	87	63	89	80	2.8	11.5	2.5	5.6	6.7	6.6	6.0	6.4
VIII	992.5	1002.9	979.2	1015.7	13.8	20.5	14.9	16.0	22.2	10.9	28.1	11	5.6	23	88	59	88	78	2.0	10.2	2.1	4.8	5.9	6.5	4.5	5.6
IX	991.6	1000.0	977.4	1015.1	10.1	16.0	11.1	12.1	17.5	7.9	27.1	9	-0.6	27	90	65	88	81	1.3	6.8	1.6	3.2	6.5	7.4	6.1	6.7
X	997.5	1005.6	981.1	1021.4	6.1	11.1	8.0	9.0	15.5	4.1	20.6	19	-0.9	2	93	62	90	82	0.7	6.5	1.2	2.8	6.8	5.6	3.5	5.3
XI	997.2	1014.7	982.0	1021.5	3.6	7.7	4.9	5.3	8.9	2.3	18.7	5	-8.6	30	89	73	83	82	0.8	3.4	1.5	1.9	8.0	7.3	8.0	7.8
XII	992.6	1012.1	960.2	1017.3	-4.3	1.1	-0.2	-0.8	2.8	-2.9	13.4	13	-14.0	16	86	78	84	83	0.8	1.6	1.0	1.1	7.1	7.5	6.0	6.9
Rok	993.8	1014.7	960.2	1017.7	6.6	12.1	8.0	8.7	13.7	4.5	35.2	5.VII	-15.7	17.1	86	64	83	78	1.6	6.6	2.0	3.4	6.6	6.9	5.7	6.4

Bieruń Stary

$\varphi = 50°05'$ $\lambda = 19°05'$

I	993.0	1004.5	976.7	1023.6	-2.5	1.3	-1.6	-1.1	2.2	-4.2	8.5	6	-17.0	17	89	77	89	85	0.6	1.6	0.6	0.9	7.5	7.3	6.7	7.2
II	988.6	1002.7	959.4	1013.2	1.1	6.0	2.1	2.8	7.2	-1.2	12.0	15	-7.6	28	91	71	90	84	0.7	2.9	0.8	1.5	6.9	7.2	6.1	6.7
III	989.7	1004.3	971.4	1019.3	1.5	8.2	3.2	4.0	10.0	-1.1	17.3	14	-10.9	1	86	59	84	76	1.2	5.2	1.4	2.6	6.1	5.9	4.8	5.6
IV	989.2	1000.6	966.0	1018.3	5.9	12.5	7.0	8.1	14.1	2.3	25.5	30	-3.9	9	86	55	83	75	1.5	8.0	1.9	3.8	5.5	6.6	5.8	6.0
V	987.1	995.1	978.0	1016.0	9.5	14.4	8.9	10.4	15.2	4.8	25.0	19	-0.6	29	79	57	83	73	2.6	8.2	2.0	4.3	6.7	7.3	5.7	6.6
VI	989.0	1008.2	975.6	1017.1	16.9	23.6	16.1	18.2	25.1	10.7	32.6	30	3.8	27	78	54	82	71	4.4	14.4	3.4	7.4	4.3	4.9	3.8	4.3
VII	985.0	996.8	974.3	1013.0	17.4	22.5	17.0	18.5	24.5	13.7	35.6	8	8.5	29	86	67	90	81	3.0	10.9	2.2	5.4	6.9	6.5	6.4	6.6
VIII	987.3	997.5	974.3	1015.6	13.9	21.0	14.3	15.9	22.6	10.1	28.8	11	3.9	31	92	62	91	82	1.4	9.9	1.6	4.3	5.6	5.9	4.3	5.3
IX	986.2	994.1	972.6	1014.8	10.6	16.5	11.1	12.2	17.9	6.9	28.2	9	-0.8	27	93	68	91	84	1.0	6.7	1.2	3.0	5.1	6.7	4.9	5.6
X	992.3	1001.0	976.2	1021.5	5.0	11.5	6.7	8.2	15.3	2.1	21.5	19	-2.2	26	96	66	94	85	0.4	6.1	0.7	2.4	6.1	5.5	3.2	4.9
XI	992.0	1009.3	977.4	1021.7	2.6	7.4	3.3	4.2	8.2	0.5	20.4	5	-9.4	30	94	80	93	89	0.5	2.7	0.5	1.2	8.7	6.6	7.2	7.5
XII	987.5	1006.6	955.2	1017.4	-2.0	1.2	-0.9	-0.6	2.3	-4.5	14.8	13	-14.9	11	92	82	89	88	0.6	1.4	0.7	0.9	7.5	7.1	6.1	6.9
Rok	988.5	1009.3	955.2	1017.6	6.6	12.4	7.3	8.4	13.7	3.3	35.6	8.VII	-17.0	17.1	88	66	88	81	1.5	6.5	1.4	3.1	6.4	6.4	5.4	6.1

Kraków - Rakowice

$\varphi = 50°05'$ $\lambda = 19°59'$

I	995.8	1006.8	979.1	1023.3	-2.6	0.5	-2.1	-1.6	1.3	-4.9	7.9	6	-17.4	17	89	81	89	86	0.6	1.2	0.6	0.8	7.9	7.5	6.0	7.1
II	986.4	1004.6	968.3	1013.2	0.8	5.5	2.3	2.7	6.5	-0.7	10.9	6	-5.3	24	89	73	86	83	0.8	2.7	1.1	1.5	7.5	7.3	7.2	7.3
III	992.6	1006.9	973.2	1019.5	0.3	7.4	3.0	3.4	8.9	-1.4	17.2	28	-10.5	4	87	60	84	76	0.8	4.9	1.6	2.4	5.7	5.7	5.5	5.6
IV	991.7	1003.0	968.2	1016.0	5.6	12.2	7.8	8.4	13.8	3.0	25.2	30	-3.6	16	87	59	83	76	1.2	6.7	1.9	3.3	6.2	6.5	6.8	6.5
V	989.6	997.8	979.9	1015.6	8.9	13.5	9.7	10.4	15.2	5.7	22.8	19	0.6	30	82	62	82	75	2.1	6.9	2.6	3.9	6.8	7.4	7.0	7.0
VI	991.2	1004.8	978.5	1016.6	16.0	23.3	16.5	18.2	24.7	10.7	32.2	14	3.5	1	75	52	79	69	4.8	14.5	4.0	7.8	3.4	5.2	3.8	4.1
VII	987.1	998.2	976.5	1014.3	17.4	23.1	18.0	19.1	24.5	13.7	35.7	5	8.4	29	83	60	83	75	3.7	13.1	4.3	7.0	6.5	6.5	6.3	6.4
VIII	989.5	999.7	976.4	1015.1	14.1	20.9	16.2	16.4	22.5	10.9	29.5	12	5.2	24	89	61	85	78	4.9	10.5	2.8	5.1	4.1	5.7	4.4	4.7
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Rzeszów – Jasionka

$H_s = 198\ m$ $H_b = 197{,}5\ m$ $h_w = 16\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (°D, v m/s)																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<0°	Max<0°	Min<-10°	Max>25°	0,1 ≤ R < 1	1 ≤ R < 10	10 ≤ R < 100	v ≥ 10 m/s	v ≥ 15 m/s							
I	1	5,0	5	6,5	10,5	5,2	5,5	2,0	8,5	4,4	27,5	5,6	20,5	5,2	7,5	4,5	7	4,7	22,4	11,2	6	26	8	2	·	10	6	1	5	1	·	·	4	19	23			
II	5	3,5	0,5	4,0	3,5	3,9	0,5	3,0	2,3	6,4	27,5	4,9	15,5	2,7	6,5	4,0	2	4,6	22,3	4,9	15	9	1	·	·	13	7	·	6	1	1	·	1	12	6			
III	5,5	5,5	3,5	2,0	2,1	6,1	3,5	1,4	5	5,3	12	4,4	10,5	5,6	8	4,4	2,4	3,7	23,9	10,3	18	19	4	2	·	9	5	·	4	1	1	1	7	8	6			
IV	10,5	3,3	1,0	2,6	1,0	3,3	2,5	4,0	3,5	3,4	5,5	2,4	17,5	2,7	5,5	3,0	2,5	2,2	22,6	13,0	11	8	·	·	1	12	4	1	·	·	3	3	5	10	·			
V	7	3,8	15,5	3,8	1,3	3,6	3	2,7	2	2,2	3,5	3,1	11,5	3,6	16,5	3,4	2,1	2,7	56,8	17,4	9	·	·	·	1,6	11	9	1	·	·	3	2	·	16	1			
VI	6	2,9	5	2,2	1,5	3,3	4,5	2,0	11,5	4,2	16,5	3,2	13,5	3,1	12,5	4,0	1,9	2,6	28,3	7,5	4	·	·	·	1,8	8	6	·	1	·	1	5	5	2	·			
VII	5,5	1,9	1	2,0	9,5	3,6	1,5	3,0	7,5	2,6	18,5	3,2	23,5	3,7	9	3,3	1,7	2,6	124,0	43,3	8	·	·	·	1,5	17	12	3	2	2	·	11	1	14	·			
VIII	3,5	2,3	1	1,0	6	3,0	1	1,0	5,5	2,9	12,5	3,5	24,5	3,6	1,8	3,9	2,4	2,5	36,8	11,6	10	·	·	·	7	12	6	1	·	·	5	6	1	3	·			
IX	4	2,6	1	3,5	3	1,3	·	·	7	4,6	1,6	3,8	3,2	4,6	8	3,6	1,9	3,2	67,9	20,0	3	·	·	·	2	14	11	3	3	·	3	2	3	11	·			
X	2	2,0	·	·	1,0	1,8	2	1,5	4,5	5,8	1,7	3,6	2,0	3,5	4,5	2,4	3,3	2,1	15,6	7,0	20	3	·	·	·	4	4	·	·	·	2	·	6	6	·			
XI	3	9,0	6,5	5,1	2,4,3	3,9	6,5	3,8	10,5	4,2	4,5	4,0	15,5	7,3	3	9,7	1,6	4,3	16,3	6,0	28	11	2	·	·	9	7	·	5	·	2	·	5	14	1			
XII	11,5	4,0	3	5,5	6	3,2	1,5	1,7	11,5	4,1	34,5	5,0	11	3,9	5	4,5	9	4,0	15,2	4,6	5	28	9	2	·	8	4	·	1	·	·	·	4	12	8			
Rok	64,5	3,6	52	3,2	118,5	3,5	32	2,2	100	4,2	195,5	3,9	212,5	4,1	104	4,2	21,6	3,3	454,1	43,3	8.VII	104	24	6	41	127	81	10	25	5	32	30	39	127	45			

Racibórz

$H_s = 189\ m$ $H_b = 196{,}1\ m$ $h_w = 15\ m$

I	3,5	3,7	6	3,2	3,6	2,1	1,7	1,6	2,5,5	2,4	16,5	2,6	7	2,6	8	5,1	6	2,5	25,4	5,8	28	19	9	4	·	11	5	·	1	·	2	·	2	16	19			
II	3	3,0	0,5	1,0	1,5	2,7	7	2,4	20	2,8	29	3,2	2,5	6,4	9,5	3,5	1,1	2,7	52,9	12,5	18	11	1	1	·	15	11	3	1	·	1	·	2	11	5			
III	1,1	2,4	5	1,7	14,5	3,3	8	2,4	15,5	2,4	11,5	3,7	2,5	1,6	1,1	2,4	1,4	2,3	28,0	6,0	17	1,1	1	·	·	10	9	·	2	1	2	1	6	13	5			
IV	27,5	2,5	1,3	1,7	5	1,7	7	1,4	9,5	2,5	4,5	2,3	2,5	1,4	1,4	2,7	7	2,0	51,6	10,5	24	7	·	·	1	11	8	1	1	·	·	·	3	8	·			
V	1,6	2,6	2,5	2,5	4	2,0	7,5	2,1	5,5	2,8	2	1,0	4,5	2,9	1,4,5	3,6	1,4	2,3	50,5	36,9	20	1	·	·	2	6	4	1	1	·	·	4	4	10	·			
VI	12,5	2,0	10,5	2,3	5	1,5	1,2	1,4	7	2,7	1,3	3,3	5	2,0	10	2,8	1,5	1,9	1,4,2,0	62,2	7	·	·	·	1,4	9	9	4	·	·	1	9	6	4	·			
VII	1,4	2,1	6	1,6	2	1,8	8,5	1,5	10,5	1,9	12,5	2,0	3	3,5	1,5,5	3,2	2,1	1,7	1,9,2,8	50,3	16	·	·	·	1,4	2,0	1,7	6	·	·	1	9	3	1,1	·			
VIII	8,5	2,6	5	1,4	2	1,5	7	1,6	1,0	2,8	1,7	2,6	4	1,6	1,6,5	2,5	2,3	1,8	7,1,9	1,4,6	10	·	·	·	7	1,2	1,2	2	·	·	1	3	1	5	·			
IX	8,5	2,0	2	1,8	1,5	1,3	6,5	2,1	1,5	3,0	2,0	2,9	5	2,8	1,1,5	2,4	2,0	2,0	99,3	26,4	2	1	·	·	2	2,0	1,5	2	·	·	4	2	·	6	·			
X	5	1,5	3	1,0	1,5	1,7	1,3,5	1,4	1,7	1,6	2,2	2,0	2,5	2,2	5,5	3,1	2,3	1,3	6,2	4,9	20	1	·	·	·	4	1	·	·	·	9	·	3	4	·			
XI	5,5	5,5	9,5	3,3	9,5	1,9	1,4,5	1,3	1,4	2,6	1,2,5	2,0	3,5	2,3	5	2,4	1,6	2,0	27,4	7,1	2	8	1	·	·	11	6	·	1	1	9	·	1	1,9	·			
XII	1,3	2,2	5,5	2,5	3	1,0	1,2,5	1,5	2,0	2,9	2,1,5	3,8	1	2,0	4,5	4,1	1,2	2,4	3,9,5	10,3	3	2,4	8	·	·	10	7	1	1	·	2	·	2	13	7			
Rok	1,2,8	2,7	9,1	2,0	5,3	1,9	1,2,1	1,7	1,6,9,5	2,5	1,8,2	2,6	1,4,3	2,6	1,2,5,5	3,2	1,8,2	2,1	7,8,7,5	62,2	7.VII	86	20	5	4,0	1,3,9	1,0,6	2,0	8	2	32	28	3,0	1,2,2	3,6			

Bieruń Stary

$H_s = 236\ m$ $H_b = 239{,}0\ m$ $h_w = 30\ m$

I	1	1,0	4,5	1,8	1,5	2,0	·	·	0,5	1,0	2,4,5	2,5	1,8	2,3	4	2,9	3,9	1,4	1,9,0	4,5	5	2,6	9	3	·	1,0	5	·	·	·	·	·	3	1,3	2,0			
II	·	·	·	·	4	1,6	3	1,5	4	2,2	3,0	2,4	1,1	1,9	4	2,0	2,8	1,4	3,5,0	9,1	2,1	1,8	1	·	·	1,3	8	·	·	·	1	·	1	9	5			
III	5,5	1,5	4	1,9	1,6,5	3,0	3	2,3	·	·	1,3,5	2,8	1,1,5	2,4	7	2,2	3,2	1,6	4,9,0	1,3,8	1,8	1,8	1	1	·	1,0	9	1	1	·	·	1	6	9	4			
IV	8,5	1,9	3,5	1,1	4	1,6	7	1,6	1	2,0	8	1,8	7	1,3	1,1	1,8	4,0	0,9	4,2,8	17,0	7	9	·	·	1	12	8	1	·	·	4,2	2	5	10	·			
V	2	2,2	16,5	1,7	1,2	1,5	5	1,5	1,5	1,7	2,5	1,6	1,1,5	1,8	1,3	2,2	2,9	1,2	2,9,2	9,8	20	3	·	·	·	9	5	·	·	·	1	3	2	1,3	·			
VI	2	2,0	3	2,0	6	1,7	5,5	1,4	2	3,0	1,1	2,3	1,1,5	2,5	1,3	2,0	5,6	1,3	5,3,2	2,4,7	7	·	·	·	1,5	7	6	2	·	·	·	5	5	5	·			
VII	2	1,0	2	1,5	4,5	1,4	2,5	1,4	3	1,2	2,1,5	2,2	1,9	1,9	1,1,5	2,2	2,7	1,4	1,4,0,0	2,8,5	1,6	·	·	·	1,3	1,7	1,7	4	·	·	·	1,0	3	1,0	·			
VIII	·	·	2	1,5	·	·	4	1,2	2,5	2,6	1,7,5	2,9	1,1,5	2,3	1,1,5	2,2	4,4	1,3	7,4,4	1,8,3	2,8	·	·	·	7	1,3	1,1	2	·	·	·	3	4	6	·			
IX	0,5	1,0	1	1,0	1	1,0	·	·	2,5	3,5	2,5,5	3,5	1,7,5	2,8	1,2	2,4	3,0	2,0	7,3,2	1,5,5	2,9	1	·	·	2	1,8	1,4	1	·	·	5	·	4	7	·			
X	0,5	1,0	·	·	1	2,0	2	1,5	1	1,5	1,2	2,6	1,1,5	2,2	5	2,1	6,0	0,8	1,1,4	6,4	2,0	,5	·	·	·	4	2	·	·	·	3	·	5	5	·			
XI	3	1,7	7,5	2,5	1,2,5	2,1	3	1,8	5,5	2,5	1,3,5	2,7	5,5	2,7	1,5	5,3	3,8	1,5	1,8,4	7,6	2,8	1,1	3	·	·	8	6	·	·	·	2	·	1	1,9	·			
XII	3	1,7	3	2,0	6	1,7	1	2,0	1	1,5	2,2,5	3,4	1,5,5	2,6	7	1,9	3,4	1,7	4,0,1	7,7	8	2,8	9	3	·	1,5	1,2	·	·	·	·	·	3	1,5	1,0			
Rok	2,8	1,5	4,7	1,4	6,9	1,6	3,6	1,4	2,4,5	1,9	2,0,2	2,6	1,5,1	2,2	1,0,0,5	2,4	4,3,7	1,4	5,8,5,7	2,8,5	1,6.VII	1,1,9	2,3	7	3,9	1,3,6	1,0,3	1,1	1	·	1,6,1	2,5	4,2	1,1,7	3,9			

Kraków – Rakowice

$H_s = 210\ m$ $H_b = 216{,}0\ m$ $h_w = 23\ m$

I	1,5	2,3	1,3	1,4	2	1,2	0,5	2,0	·	·	6,5	1,5	3,2,5	1,0	1	1,5	3,3	2,5	1,8,7	7,2	1,3	2,5	9	5	·	1,2	5	·	2	·	9	·	2	1,3	2,0			
II	1,5	2,7	1	2,1	6,5	2,7	2	1,0	3,5	3,4	3,5	3,4	2,0	3,6	6	2,2	3,7	1,7	2,9,5	8,4	2,1	1,7	1	·	·	1,4	8	·	2	1	1	·	1	1,3	6			
III	1,5	2,0	1,3,5	3,9	1,6,5	5,3	1,5	2,0	0,5	2,0	1,5	6,0	2,0,5	3,8	1,0,5	3,0	2,7	2,8	3,9,1	1,1,7	1,8	1,9	3	1	·	9	8	1	6	1	2	1	8	1,1	5			
IV	7,8	2,3	1,5	2,1	8,5	1,9	1	2,0	1	2,0	3,5	2,9	1,8,5	2,5	8	2,5	2,7	1,6	4,7,7	1,3,5	7	8	·	·	1	1,4	8	1	1	·	1	3	4	1,3	·			
V	1,0,5	2,8	2,4,5	3,9	9	3,6	·	·	1	3,0	1,5	2,3	1,7,5	3,4	1,0	2,5	1,9	2,7	4,0,5	1,1,4	2,0	·	·	·	·	1,3	6	2	·	·	·	2	2	1,5	·			
VI	6,5	3,0	1,2	3,0	8,5	2,8	2	3,0	·	·	2	3,5	2,0	3,5	1,4	2,6	2,5	2,2	2,7,6	9,2	7	·	·	·	1,2	1,0	7	·	1	1	·	8	6	1	·			
VII	1,5	1,3	9,5	2,5	7,5	3,7	2	2,0	·	·	2	4,2	3,3	3,7	8,5	2,8	2,9	2,3	1,3,8,0	3,1,0	1,6	·	·	·	1,5	1,6	1,5	4	1	·	·	1,0	4	9	·			
VIII	1,5	2,0	1,5	1,7	4,5	3,2	·	·	1	1,0	5,5	2,6	3,0,5	3,5	1,4,5	2,7	3,4	1,9	6,8,7	1,7,6	1,6	·	·	·	1,0	1,7	1,0	2	·	·	1	3	3	5	·			
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5,1,5	8,6	2,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–			
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–			
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–			
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–			
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3,1,0	1,6.VII	–	–	–	–	–	–	–	–	–	–	–	–	–			

Kraków – Czyżyny

$\varphi = 50°05'$ $\lambda = 20°01'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	988.9	997.1	974.9	1014.4	10.0	16.6	11.7	12.5	17.5	7.4	27.4	9	−0.7	27	89	59	83	77	1.5	8.2	2.3	4.0	5.7	6.5	5.5	5.9
X	995.2	1003.8	978.6	1021.3	4.4	14.0	7.6	8.4	14.9	2.4	23.3	19	−4.0	3	94	61	88	81	0.5	6.6	1.3	2.8	6.5	5.0	3.2	4.9
XI	994.9	1012.6	980.4	1021.5	2.1	6.5	3.5	3.9	7.8	0.4	19.0	5	−11.4	30	91	76	87	85	0.7	2.7	1.0	1.5	7.8	6.7	7.5	7.3
XII	990.2	1009.3	956.8	1017.1	−2.4	0.8	−1.1	−0.9	2.0	−4.5	11.0	12	−13.5	11	87	80	84	84	0.8	1.4	1.0	1.1	7.9	7.5	6.6	7.3
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kraków, Obserw. Astr. UJ

$\varphi = 50°04'$ $\lambda = 19°57'$

I	995.1	1006.0	978.7	1023.0	−4.7	0.9	−0.9	−0.6	1.8	−3.2	8.9	6	−13.2	17	87	80	87	85	0.7	1.4	0.8	1.0	8.3	7.5	7.0	7.6
II	985.9	1003.9	962.1	1013.3	1.8	5.5	3.5	3.6	6.7	0.6	11.1	6	−3.7	24,28	88	74	83	82	0.9	2.6	1.4	1.6	8.8	7.9	8.0	8.2
III	994.9	1006.1	972.5	1019.1	1.4	7.2	4.4	4.4	9.0	−0.1	16.5	28	−8.3	4	85	61	79	75	1.1	4.6	2.1	2.6	6.9	5.9	6.7	6.5
IV	994.1	1001.9	967.2	1017.8	6.0	12.2	9.1	9.1	14.0	4.5	25.0	30	−0.8	14,16	87	59	77	74	1.2	6.7	2.9	3.6	6.3	6.6	7.6	6.8
V	989.1	997.1	979.7	1015.5	9.1	13.7	11.2	11.3	15.4	6.8	22.5	19,20	1.7	9	81	59	74	71	2.3	7.5	3.6	4.5	6.8	7.5	8.0	7.4
VI	990.7	1003.8	978.3	1016.4	16.6	22.9	19.0	19.4	24.9	13.2	32.5	11	7.4	27	74	51	69	65	4.9	14.2	6.9	8.7	3.7	5.8	5.4	5.0
VII	986.8	997.9	976.4	1012.4	17.7	22.9	19.5	19.9	24.7	15.3	35.2	5	10.8	29	82	60	78	73	3.9	12.7	5.5	7.4	6.8	6.9	7.3	7.0
VIII	989.2	999.5	976.5	1015.1	14.5	20.5	17.1	17.3	22.5	12.7	28.8	12	7.7	24	87	60	80	76	2.2	10.2	4.1	5.5	4.8	6.1	6.5	5.8
IX	988.3	996.3	974.1	1014.5	10.4	16.4	12.6	13.0	17.9	8.9	26.9	9	1.7	27	92	64	86	81	1.0	7.1	2.0	3.4	5.8	6.6	7.5	6.8
X	994.4	1003.0	977.8	1021.1	5.6	13.3	9.2	9.3	14.6	4.7	21.7	19	−1.9	3	96	65	88	83	0.5	5.7	1.5	2.6	6.8	5.1	5.4	5.8
XI	994.1	1011.6	979.7	1021.3	2.8	6.2	4.3	4.4	7.5	1.4	17.1	6	−8.4	30	94	82	89	88	0.5	2.0	0.9	1.1	8.1	6.7	8.0	7.6
XII	989.3	1008.5	956.2	1017.0	−1.6	0.6	−0.3	−0.4	1.8	−3.3	9.5	12	−9.7	11	90	84	87	87	0.6	1.1	0.8	0.8	8.4	7.8	8.5	8.2
Rok	990.5	1011.6	956.2	1017.1	6.9	11.9	9.1	9.2	13.4	5.1	35.2	5.VIII	−13.2	17.1	87	67	81	78	1.6	6.3	2.7	3.5	6.8	6.7	7.2	6.9

Kraków, Inst. Geogr. UJ

$\varphi = 50°03'$ $\lambda = 19°57'$

I	–	–	–	–	−2.0	1.0	−1.3	−0.9	2.3	−3.2	7.6	2	−15.2	17	–	–	–	–	–	–	–	–	7.7	6.8	5.9	6.8
II	–	–	–	–	1.9	5.5	3.4	3.5	6.9	1.1	12.8	6	−4.2	23	–	–	–	–	–	–	–	–	7.1	7.2	6.0	6.8
III	–	–	–	–	2.4	7.6	4.1	4.6	9.2	0.0	17.2	27	−8.2	1	–	–	–	–	–	–	–	–	5.3	4.1	4.7	4.7
IV	–	–	–	–	6.5	12.0	9.0	9.1	14.0	4.7	25.8	30	−2.0	14	83	58	75	72	4.8	6.8	3.1	3.9	5.5	5.7	6.1	5.7
V	–	–	–	–	9.5	13.6	11.0	11.3	15.2	7.1	22.7	13,19,20	1.8	9	80	63	78	74	2.6	6.6	3.1	4.1	5.6	6.4	5.4	5.8
VI	–	–	–	–	16.7	22.7	18.8	19.2	24.8	13.1	32.4	11	7.0	27	–	–	–	–	–	–	–	–	2.6	4.7	2.3	3.2
VII	–	–	–	–	17.4	22.9	19.3	19.7	24.5	15.5	36.2	5	11.8	29	–	–	–	–	–	–	–	–	5.5	5.1	6.4	5.3
VIII	–	–	–	–	14.5	20.6	17.0	17.3	22.5	12.6	29.4	12	7.3	24	85	62	77	75	2.7	10.1	4.7	5.8	3.7	3.6	3.6	3.6
IX	–	–	–	–	11.0	16.2	12.8	13.2	17.6	8.9	28.2	9	1.2	27	84	62	80	75	2.2	7.7	3.2	4.4	4.8	4.7	4.3	4.6
X	–	–	–	–	5.8	13.8	9.3	9.6	15.1	4.3	22.7	19	−0.5	3	91	62	85	79	0.9	6.5	1.9	3.1	5.9	3.1	2.6	3.9
XI	–	–	–	–	2.8	6.7	4.3	4.5	8.0	1.6	19.8	5	−8.1	30	88	76	86	83	0.9	3.0	1.2	1.7	7.1	5.8	6.7	6.5
XII	–	–	–	–	−1.4	0.7	−0.4	−0.4	2.2	−3.0	11.0	13	−8.6	16.24	85	81	85	84	0.8	1.3	0.9	1.0	6.5	5.5	5.0	5.7
Rok	–	–	–	–	7.1	11.9	8.9	9.2	13.5	5.2	36.2	5.VIII	−15.2	17.1	–	–	–	–	–	–	–	–	5.6	5.2	4.8	5.2

Krzesławice

$\varphi = 50°05'$ $\lambda = 20°03'$

I	–	–	–	–	−2.0	1.1	−1.8	−1.1	2.2	−4.8	8.2	2	−16.0	17	–	–	–	–	–	–	–	–	6.7	6.7	5.6	6.3
II	–	–	–	–	1.1	5.6	3.1	3.2	7.0	0.1	12.6	6	−3.6	24	–	–	–	–	–	–	–	–	5.8	5.6	6.1	5.8
III	–	–	–	–	0.8	7.3	3.7	3.9	9.0	−0.7	17.5	27	−8.7	1	–	–	–	–	–	–	–	–	5.2	4.4	4.1	4.6
IV	–	–	–	–	5.6	12.2	8.3	8.6	13.9	3.6	26.2	30	−1.9	14	–	–	–	–	–	–	–	–	4.8	5.3	5.5	5.2
V	–	–	–	–	8.9	13.5	10.1	10.6	16.0	5.9	23.2	19	1.1	30	–	–	–	–	–	–	–	–	6.4	5.9	5.9	6.0
VI	–	–	–	–	14.8	22.2	17.9	18.2	24.4	11.4	32.1	11	4.3	1	–	–	–	–	–	–	–	–	2.3	2.8	2.1	2.4
VII	–	–	–	–	16.6	22.6	18.7	19.2	24.3	14.1	35.3	5	8.1	29	–	–	–	–	–	–	–	–	5.3	4.1	4.3	4.5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.3	16.4	12.7	12.7	17.7		27.2	9	–	–	–	–	–	–	–	–	–	–	3.7	4.5	5.2	4.4
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kraków - Czyżyny

$H_s = 213\ m$ $H_b = 213{,}4\ m$ $h_w = 22\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU *D, *wD																	OPAD R			LICZBA DNI (n)																
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v								
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max>25°	≥0.1	≥1.0	≥10.0	>10	>15	=	≥0.5	◔	☁	⊠
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	4	3.8	6	2.2	8.5	2.4	3.5	2.0	4	2.6	14.5	5.1	33.5	4.1	6	3.5	10	3.5	51.5	8.6	29	1	·	·	2	15	12	·	7	·	4	1	3	8	·	·	·
X	3	2.3	7.5	2.5	16	2.8	2.5	2.6	1	2.0	.7	4.3	30.5	3.3	12.5	2.2	13	2.5	14.7	5.5	20	3	·	·	·	6	4	·	·	·	10	·	6	5	·	·	·
XI	5	7.5	18	4.2	25	4.2	4.5	3.4	1.5	1.7	2.5	2.8	19	6.4	3.5	6.4	11	4.3	21.8	6.2	28	10	3	1	·	11	5	·	5	·	10	·	3	17	1	·	·
XII	8	3.3	6.5	4.3	10	4.1	2.5	3.0	1	2.5	1.3	4.4	3.6	4.1	6	3.9	10	3.6	20.0	5.0	14	25	10	3	·	10	7	·	2	·	8	·	1	17	8	·	·
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Kraków, Obserw. Astr. UJ

$H_s = 221\ m$ $H_b = 219{,}8\ m$ $h_w = 21\ m$

I	1.5	1.0	3.5	2.0	4	1.8	·	·	·	·	1	1.0	22.5	2.1	0.5	2.0	6.0	0.7	20.6	7.5	13	21	9	3	·	14	4	·	·	·	9	·	·	16	22	·	·	·
II	1	1.0	1	1.0	3	1.3	1	2.0	3	1.3	4	2.0	14.5	1.9	3.5	2.6	5.3	0.7	27.4	8.0	21	8	1	·	·	15	7	·	·	·	6	·	·	16	4	·	·	·
III	3	3.7	3.5	2.9	1.3	3.7	3.5	2.4	·	·	2.5	3.6	14.5	3.3	7	8.4	4.6	1.6	45.4	11.6	18	13	2	·	·	9	8	1	3	·	4	1	5	13	4	·	·	·
IV	6	2.2	9.5	1.8	4	1.9	1	1.0	3.5	1.3	2.5	1.4	12.5	2.0	9	1.8	4.2	1.0	47.0	14.1	7	3	·	·	·	14	8	1	·	·	2	3	4	13	·	·	·	·
V	6	1.7	15.5	1.9	6.5	2.8	3	1.7	3	1.2	0.5	1.0	14	2.6	10.5	2.0	3.4	1.3	43.1	14.2	20	·	·	·	·	14	5	1	1	·	·	2	2	18	·	·	·	·
VI	4.5	1.4	5	1.6	5.5	1.0	3.5	1.3	3	1.3	8.5	1.6	16	2.4	7	1.6	3.7	1.0	35.4	11.9	22	·	·	·	13	10	7	2	1	·	·	6	4	4	·	·	·	·
VII	3	1.2	3	1.7	2.5	1.4	1.5	1.3	3	1.2	5	1.9	30.5	2.3	6.5	2.2	3.8	1.2	159.2	30.6	16	·	·	·	13	17	16	6	·	·	1	11	3	15	·	·	·	·
VIII	1.5	1.3	0.5	1.0	1	2.5	0.5	4.0	1.5	1.0	1.0	2.3	2.9	2.1	8	2.2	4.1	1.2	80.9	25.8	16	·	·	·	6	15	12	2	1	·	·	4	·	6	·	·	·	·
IX	1	1.0	1.5	1.0	1	1.0	0.5	1.0	1	2.0	3	1.8	29	2.7	5	4.0	4.8	1.2	55.3	10.1	29	·	·	·	2	18	12	1	1	·	4	·	3	11	·	·	·	·
X	1	1.5	1	1.0	2.5	1.0	2.5	1.0	0.5	1.0	5	1.9	15.5	1.8	3	2.0	6.2	0.5	15.3	6.0	20	1	·	·	·	8	4	·	·	·	16	·	3	6	·	·	·	·
XI	2	5.0	8.5	2.5	11.5	2.3	3	2.0	·	·	2.5	3.4	20.5	4.9	1	4.0	4.1	1.9	25.5	7.5	28	10	2	·	·	13	5	·	3	·	13	·	3	17	1	·	·	·
XII	2.5	1.6	2.5	2.0	5.5	3.4	0.5	1.0	1.5	1.0	3	3.2	14	2.6	4.5	4.0	5.9	1.0	25.1	6.5	14	24	10	·	·	9	8	·	·	·	15	·	·	18	5	·	·	·
Rok	3.3	1.9	5.5	1.7	6.0	2.0	2.0.5	1.6	2.0	0.9	4.7.5	2.1	2.3.2.5	2.6	6.5.5	2.3	5.6.1	1.1	5.8.0.2	3.0.6	1.6.VII	8.0	2.4	3	3.4	1.5.6	9.6	1.4	1.0	·	7.0	2.7	2.7	1.5.3	3.6	·	·	·

Kraków, Inst. Geogr. UJ

$H_s = 202\ m$ $h_w = \frac{I-VII}{VIII-XII}\ \frac{9\ m}{7\ m}$

I	1	2.5	6.5	3.2	9	1.6	0.5	1.0	2.5	1.0	3.9.5	1.5	30	1.7	4	2.4	·	1.7	23.7	7.0	13	21	9	3	·	13	6	·	·	·	·	·	4	15	·	·	·	·
II	3	1.3	2	1.5	9	1.9	2	1.5	5.5	1.7	33.5	2.0	21	1.9	8	1.7	·	1.8	26.5	8.1	21	7	1	·	·	18	8	·	·	·	·	·	4	12	·	·	·	·
III	1.5	1.7	10.5	2.3	27	2.5	3	1.0	3.5	1.1	21	1.9	20.5	2.0	6	2.4	·	2.1	41.7	13.0	18	14	2	·	·	10	7	1	·	·	·	1	9	7	·	·	·	·
IV	9.5	2.2	12	1.9	15	2.0	8	1.1	·	·	21	1.8	15	1.7	9.5	2.1	·	1.8	46.1	14.7	7	3	·	·	1	14	8	1	·	·	·	2	7	9	·	·	·	·
V	8.5	2.3	24.5	2.7	14.5	1.8	2	1.0	1	1.5	8.5	2.1	21	2.0	13	1.9	·	2.1	33.8	9.4	9	·	·	·	·	10	5	·	·	·	·	2	7	11	·	·	·	·
VI	2	2.0	7	2.4	17.5	1.3	6.5	1.3	·	·	22	1.8	27	1.7	8	2.8	·	1.8	32.6	11.8	22	·	·	·	13	11	6	2	·	·	·	6	11	·	·	·	·	·
VII	4.5	1.4	5.5	1.5	11.5	1.5	5	1.7	2	1.0	19.5	1.7	36.5	1.7	8.5	2.0	·	1.7	158.2	34.9	15	·	·	·	14	18	16	8	·	·	·	6	5	7	·	·	·	·
VIII	1.5	2.7	5	1.1	11	1.2	3.5	1.0	0.5	1.0	11	1.7	5.1	1.4	5.5	2.2	1	1.4	77.5	20.8	16	·	·	·	7	14	13	3	·	·	·	5	10	2	·	·	·	·
IX	·	·	1.2	1.6	5	1.2	0.5	1.0	7	1.6	16.5	2.8	36.5	2.1	12.5	2.0	·	2.0	50.5	9.3	29	·	·	·	2	14	11	·	·	·	·	·	8	5	·	·	·	·
X	0.5	1.0	8	1.2	1.0	1.1	2	1.0	1.5	1.0	29.5	1.3	32.5	1.2	8	1.4	1	1.2	14.0	6.2	20	2	·	·	·	4	3	·	·	·	·	·	8	4	·	·	·	·
XI	4	3.9	23	1.9	28.5	1.6	·	·	4	1.4	17.5	2.0	10	2.0	3	2.2	·	1.9	27.4	11.1	28	10	1	·	·	8	4	1	·	·	·	·	7	17	·	·	·	·
XII	6	2.1	8.5	1.9	13.5	1.4	·	·	·	·	21	3.1	32	1.6	12	1.8	·	1.8	23.4	6.4	14	24	9	·	·	15	6	·	·	·	·	·	6	9	·	·	·	·
Rok	4.2	1.9	12.4.5	1.9	17.1.5	1.6	3.3	1.0	2.7.5	0.9	26.3.5	2.0	33.3	1.8	9.8	2.1	2	1.8	55.5.4	34.9	15.VII	8.1	2.2	3	3.7	14.9	9.3	1.4	·	·	·	2.2	8.6	9.8	·	·	·	·

Krzesławice

$H_s = 200\ m$ $h_w = 15\ m$

I	1.5	1.7	4	3.1	1.2	1.7	9	1.2	1	2.0	13.5	1.5	36.5	2.2	2.5	2.0	1.3	1.6	18.9	9.9	13	2.5	9	4	·	5	4	·	·	·	·	·	3	7	·	·	·	·
II	4	1.2	7	1.4	3	2.2	6	1.4	8.5	1.4	24.5	1.6	28	1.8	2	2.2	1	1.8	27.0	11.1	21	13	1	·	·	11	7	1	·	·	·	·	4	5	·	·	·	·
III	6	1.0	14.5	2.0	23	2.4	4.5	1.3	1	1.5	5	1.4	23	2.6	6	1.8	1.0	1.8	40.1	10.8	18	18	2	·	·	8	7	1	·	·	·	1	10	7	·	·	·	·
IV	9	1.3	10	1.4	7.5	1.1	5.5	1.0	1.5	1.7	5.5	1.6	20.5	1.5	6.5	1.5	2.4	1.0	50.0	10.8	7	4	·	·	1	9	8	1	·	·	·	2	7	8	·	·	·	·
V	10.5	1.7	21.5	2.2	14.5	1.9	6	1.2	3	1.0	4	1.2	22	1.7	5.5	1.4	9	1.6	28.7	9.7	9	·	·	·	·	9	5	·	·	·	·	3	5	14	·	·	·	·
VI	1.2	1.5	10.5	1.6	6	1.2	5.5	1.3	1.5	1.4	4.5	1.5	20	1.9	3	1.3	27	1.1	35.2	15.3	7	·	·	·	13	10	10	1	·	·	·	8	13	2	·	·	·	·
VII	7	1.4	5	1.0	2	1.0	1.5	1.0	3	1.3	9.5	1.1	31	1.7	8	1.5	26	1.1	46.2.8	48.0	16	·	·	·	13	18	17	5	·	·	·	6	6	4	·	·	·	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	·	·	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	2.5	1.0	2	1.0	·	·	3	1.0	1	3.0	13	1.4	32	1.8	2.5	1.8	34	1.0	52.4	8.0	23	-	·	·	2	15	15	·	·	·	·	·	6	6	·	·	·	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48.0	16.VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Chełm k. Krakowa

$\varphi = 50°04'$ $\lambda = 19°51'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.9	0.7	-1.3	-1.0	1.9	-4.4	8.0	6	-17.9	17	–	–	–	–	–	–	–	–	8.5	7.7	8.0	8.1
II	–	–	–	–	1.5	5.2	3.3	3.3	–	-0.4	–	–	-4.9	24	–	–	–	–	–	–	–	–	7.7	7.4	7.6	7.6
III	–	–	–	–	1.2	6.9	3.7	3.9	–	-1.0	–	–	-10.4	4	–	–	–	–	–	–	–	–	7.3	6.2	6.3	6.6
IV	–	–	–	–	5.6	12.1	8.6	8.7	–	3.0	–	–	-4.4	14	86	59	75	73	1.3	6.9	3.0	3.7	7.4	6.7	7.4	7.2
V	–	–	–	–	8.9	13.2	10.1	10.6	–	5.7	–	–	0.9	7	80	62	76	73	2.3	6.6	3.0	4.0	7.4	7.7	7.1	7.4
VI	–	–	–	–	15.9	22.8	17.0	18.2	–	10.7	–	–	3.6	27	78	54	76	69	4.0	13.6	4.9	7.5	5.2	5.4	5.6	5.4
VII	–	–	–	–	17.0	22.5	17.9	18.8	–	13.4	–	–	8.1	29	85	64	82	77	3.1	11.4	3.9	6.1	7.5	6.6	7.5	7.2
VIII	–	–	–	–	13.9	20.5	15.9	16.6	22.5	10.6	29.1	12	4.6	24	90	62	82	78	1.9	9.9	3.3	5.0	6.4	5.8	5.5	5.9
IX	–	–	–	–	9.8	16.2	11.9	12.4	17.7	7.3	28.1	9	0.1	26	88	63	80	77	1.5	7.4	2.7	3.9	7.3	6.8	6.1	6.7
X	–	–	–	–	4.9	13.8	8.1	8.7	15.0	2.3	22.0	19	-2.1	3	93	63	86	81	0.6	6.2	1.6	2.8	8.3	6.0	5.0	6.4
XI	–	–	–	–	2.3	6.4	3.9	4.1	8.2	0.5	20.5	5	-9.4	30	90	78	88	85	0.7	2.7	1.0	1.5	8.7	7.5	8.1	8.1
XII	–	–	–	–	-2.2	0.4	-0.5	-0.7	2.4	-4.6	11.5	13	-15.4	25	–	–	–	–	–	–	–	–	9.4	7.4	7.5	8.1
Rok	–	–	–	–	6.4	11.7	8.2	8.6	–	–	–	–	-17.9	17.1	–	–	–	–	–	–	–	–	7.6	6.8	6.8	7.1

Dębica

$\varphi = 50°03'$ $\lambda = 21°24'$

I	–	–	–	–	-1.3	0.9	-0.9	-0.6	–	-3.3	–	–	-14.6	17	–	–	–	–	–	–	–	–	9.0	7.8	7.5	8.1
II	–	–	–	–	2.4	5.1	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.1	6.6	7.1
III	–	–	–	–	0.6	6.4	3.1	3.3	8.6	-2.7	18.0	14	-16.2	4	–	–	–	–	–	–	–	–	5.4	5.1	4.9	5.1
IV	–	–	–	–	5.5	12.7	8.7	8.9	14.5	2.3	25.5	30	-3.1	15	–	–	–	–	–	–	–	–	6.2	5.7	6.3	6.1
V	–	–	–	–	8.7	13.5	10.1	10.6	15.2	5.4	23.1	13	0.0	28	–	–	–	–	–	–	–	–	6.4	7.8	7.3	7.2
VI	–	–	–	–	16.8	23.1	18.1	19.0	25.0	11.9	32.3	12	6.0	16,27	–	–	–	–	–	–	–	–	4.0	4.5	4.2	4.2
VII	–	–	–	–	17.7	23.1	18.9	19.6	25.1	14.6	36.6	5	8.1	4	–	–	–	–	–	–	–	–	6.6	6.5	6.9	6.7
VIII	–	–	–	–	14.6	21.0	16.4	17.1	22.8	11.8	30.2	14	5.1	24	–	–	–	–	–	–	–	–	5.5	5.9	4.8	5.4
IX	–	–	–	–	10.7	16.5	12.6	13.1	18.1	8.7	28.4	9	-0.6	27	–	–	–	–	–	–	–	–	6.0	6.5	6.5	6.3
X	–	–	–	–	6.2	13.8	8.4	9.2	15.0	4.0	20.6	19	-3.4	3	–	–	–	–	–	–	–	–	5.3	5.2	4.5	5.0
XI	–	–	–	–	3.5	6.9	4.1	4.6	8.2	–	17.6	4	–	–	–	–	–	–	–	–	–	–	6.7	6.0	6.0	6.2
XII	–	–	–	–	-1.4	1.1	-0.4	-0.3	2.7	–	11.9	14	–	–	–	–	–	–	–	–	–	–	6.8	7.4	6.3	6.8
Rok	–	–	–	–	7.0	12.0	8.5	9.0	–	–	36.6	5.VII	–	–	–	–	–	–	–	–	–	–	6.3	6.3	6.0	6.2

Tarnów

$\varphi = 50°02'$ $\lambda = 20°59'$

I	996.6	1007.6	980.7	1023.0	-1.9	0.8	-1.3	-0.9	1.8	-4.1	7.4	6	-16.4	17	84	73	84	80	0.9	1.8	0.9	1.2	8.5	7.8	6.5	7.6
II	987.5	1004.3	964.1	1014.4	1.9	5.3	2.9	3.2	6.7	0.7	11.6	6	-5.2	23	83	72	80	78	1.3	2.8	1.6	1.9	7.6	7.5	6.8	7.3
III	993.6	1008.2	973.7	1019.6	0.7	6.8	3.4	3.6	8.5	-1.0	17.3	14	-12.5	4	78	57	72	69	1.6	5.1	2.4	3.0	6.0	6.1	4.8	5.6
IV	992.4	1003.6	968.7	1017.8	6.0	12.2	8.1	8.6	13.7	3.7	25.5	30	-2.7	15	85	61	79	75	1.7	6.9	2.6	3.7	6.0	6.6	6.1	6.2
V	990.3	998.5	979.7	1015.5	8.7	13.2	9.9	10.4	14.7	6.0	22.4	20	0.3	7	83	63	80	75	2.1	6.9	2.6	3.9	6.2	8.0	7.1	7.1
VI	992.1	1004.8	979.5	1016.7	16.5	22.8	17.7	18.8	24.8	14.6	34.8	30	5.1	1	77	53	73	68	4.6	14.0	5.8	8.1	4.6	6.1	4.6	5.1
VII	988.1	998.6	978.0	1012.5	17.9	23.0	18.2	19.3	24.7	14.4	37.0	5	8.8	4	83	61	83	76	3.8	12.5	4.0	6.8	6.6	6.8	6.9	6.8
VIII	990.4	1000.4	977.6	1015.1	14.9	21.0	16.0	17.0	22.3	11.8	31.3	12	6.7	31	86	59	82	76	2.5	11.1	3.6	5.7	4.9	6.1	5.2	5.4
IX	989.7	997.9	976.3	1014.8	10.7	16.3	11.8	12.6	17.2	8.5	26.9	9	0.4	27	88	61	84	78	1.6	7.6	2.2	3.8	6.3	7.4	6.9	6.9
X	995.9	1005.2	979.2	1021.3	6.7	13.8	8.6	9.4	14.6	4.7	20.8	19	-1.5	3	89	63	85	79	1.2	6.3	2.0	3.2	5.6	5.5	3.7	4.9
XI	995.6	1013.5	979.9	1021.5	3.5	7.0	4.4	4.8	7.9	1.7	19.1	4	-10.1	30	86	74	84	81	1.1	3.1	1.5	1.9	6.7	6.3	6.6	6.5
XII	991.0	1010.6	957.1	1017.4	-1.6	1.0	-0.3	-0.3	2.3	-3.6	10.9	13	-10.7	3	84	76	80	80	1.0	1.7	1.3	1.3	7.1	7.6	6.6	7.1
Rok	991.9	1013.5	957.1	1017.2	7.0	11.9	8.3	8.9	13.3	4.5	37.0	5.VII	-16.4	17.1	84	64	80	76	2.0	6.6	2.5	3.7	6.3	6.8	6.0	6.4

Tyniec

$\varphi = 50°01'$ $\lambda = 19°48'$

I	–	–	–	–	-2.4	0.7	-1.7	-1.3	1.9	-4.7	8.8	6	-17.5	17	–	–	–	–	–	–	–	–	7.5	7.3	6.6	7.1
II	–	–	–	–	1.1	5.5	2.9	3.1	6.8	-0.6	12.3	6	-5.2	23	–	–	–	–	–	–	–	–	7.7	7.7	7.1	7.5
III	–	–	–	–	0.5	7.5	3.3	3.6	9.2	-1.4	17.9	27	-10.5	4	–	–	–	–	–	–	–	–	5.7	5.9	5.6	5.7
IV	–	–	–	–	5.1	12.2	8.0	8.4	14.1	2.8	25.4	30	-3.0	14	87	58	80	75	1.1	7.0	2.4	3.5	6.1	6.9	6.8	6.6
V	–	–	–	–	8.2	13.7	9.7	10.3	15.4	5.8	23.1	19	4.0	30	83	60	84	75	1.8	7.2	2.3	3.8	7.0	8.0	7.0	7.3
VI	–	–	–	–	15.5	22.7	16.9	18.0	24.6	10.5	32.5	11	4.2	7	–	–	–	–	–	–	–	–	4.0	6.0	4.9	5.0
VII	–	–	–	–	16.8	22.5	18.0	18.8	24.7	13.9	35.3	5	8.7	29	–	–	–	–	–	–	–	–	6.6	6.8	7.4	6.9
VIII	–	–	–	–	13.2	20.0	15.8	16.2	22.1	11.2	28.8	11	5.2	24	91	64	84	80	1.4	8.9	2.9	4.4	4.5	6.2	5.1	5.3
IX	–	–	–	–	9.4	16.3	11.5	12.2	17.5	7.6	28.0	9	0.5	27	92	64	86	81	1.0	7.2	1.9	3.4	6.3	6.6	4.8	5.9
X	–	–	–	–	4.4	13.7	7.6	8.3	14.8	2.6	21.1	19	-2.5	3	95	63	91	83	0.4	6.1	1.0	2.5	7.2	4.8	2.9	5.0
XI	–	–	–	–	2.5	6.2	3.7	4.0	7.7	0.5	19.9	5	-9.5	30	90	78	89	86	0.8	2.5	0.9	1.4	7.8	6.7	7.4	7.3
XII	–	–	–	–	-2.5	0.9	-1.2	-1.2	2.0	-4.9	13.3	13	-15.0	11	86	80	85	84	0.8	1.4	0.9	1.0	7.9	7.5	6.3	7.2
Rok	–	–	–	–	6.0	11.8	7.9	8.4	13.4	3.6	35.3	5.VII	-17.5	17.1	–	–	–	–	–	–	–	–	6.5	6.7	6.0	6.4

Chełm k. Krakowa — $H_s = 225$ m — $h_w = 17{,}5$ m — 1957

MIESIĄC	ROZKŁAD WIATRU °/0, V m/s																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v							
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max>25°	0,1 ≤ R < 1	1 ≤ R < 10	10 ≤ R < 100	v ≥ 10	v ≥ 15	=	20	◔	●	▣
I	·	·	5,5	4,9	2,5	1,6	·	·	1	1,0	2,5	2,2	1,7	3,4	1	1,0	4,1	1,5	18,5	8,4	6	26	9	4	·	8	4	·	·	·	–	·	·	19	–
II	·	·	·	·	6	1,8	2	4,5	3,5	2,3	1,9	2,2	9,5	2,8	2	1,0	4,2	1,2	20,0	4,3	19	15	–	·	–	8	7	·	·	·	–	·	1	16	–
III	1	2,0	8	2,1	2,0	3,7	·	·	·	·	6	2,4	1,3	4,0	5	3,4	4,0	1,9	41,5	12,8	18	20	–	1	–	8	8	1	·	·	–	1	1	12	–
IV	1	2,0	7	2,0	1	1,0	·	·	1	1,0	15,5	1,9	8,5	1,9	6	1,7	5,0	0,8	42,1	15,0	7	4	–	·	–	10	8	1	·	·	–	3	1	15	–
V	5,5	1,4	1,4	2,2	1,1	1,5	0,5	2,0	1,5	2,0	6,5	2,6	1,5	2,5	3,5	2,3	3,9	1,2	26,3	9,4	20	·	–	·	–	8	6	·	·	·	–	2	·	16	–
VI	1	1,0	3	1,7	3	1,0	3	1,7	0,5	1,0	10,5	2,5	1,3	2,2	6	2,3	5,0	0,9	24,9	10,7	7	·	–	·	–	8	7	1	·	·	–	6	3	4	–
VII	2,5	1,6	1	2,0	5	1,4	1	2,0	1	3,0	9	2,4	1,8	2,6	4,5	2,4	5,1	1,0	194,5	36,7	11	·	–	·	–	17	17	7	·	·	–	7	·	13	–
VIII	1	3,0	·	·	3	1,0	·	·	1	1,0	7	1,6	2,6	1,8	2	1,0	5,3	0,7	93,1	25,6	16	·	·	·	8	14	12	4	·	·	–	2	1	7	–
IX	·	·	2	1,5	2	1,5	1	1,0	1	2,0	1,9	2,3	2,5	3,2	1	3,0	3,9	1,5	45,6	7,0	29	·	·	·	2	12	12	·	·	·	–	·	1	10	–
X	·	·	3	1,0	2	1,0	·	·	·	·	1,5	1,0	1,4	2,7	0,5	1,0	7,2	0,5	12,7	6,4	20	3	·	·	·	3	3	·	·	·	–	·	·	8	–
XI	1,1	3,8	3	3,3	1,7	2,1	·	·	1,5	3,7	6,5	2,2	1,5	3,5	2	3,0	4,1	1,5	22,9	7,8	28	1,1	2	·	·	7	5	·	·	·	–	1	·	17	–
XII	5	1,6	·	·	5,5	2,2	0,5	2,0	1	2,0	13,5	2,7	1,5,5	2,6	3	1,8	4,9	1,2	19,2	9,0	8	27	9	3	·	12	6	·	·	·	–	·	·	15	–
Rok	21	14	46,5	17	78	17	8	1,1	13	1,6	139	24	1,8,6	28	36,5	2,2	56,7	1,2	561,3	36,7	11.VII	106	–	8	–	115	95	14	·	·	–	22	8	152	–

Dębica — $H_s = 205$ m — $h_w = 21$ m

I	·	·	1,6	5,7	4,5	4,6	1,5	6,3	2,8	5,0	1,1	4,7	9	5,9	·	·	2,4	4,0	39,8	18,6	6	23	–	2	·	12	6	1	7	·	–	·	2	17	13?
II	2	2,5	3	2,7	2,5	5,4	1,9	7,0	3,8	6,4	9	5,6	4,5	4,0	1	4,0	5	5,6	26,5	5,6	21	–	–	–	–	13	9	·	9	·	–	·	2	13	6
III	5,5	2,1	3,5	3,9	1,9,5	4,3	1,6	3,5	2,0,5	6,4	1,1,5	7,5	1,5	7,0	2	4,2	1,3	4,3	3,9,9	1,5,7	1,8	1,8	3	2	·	9	6	1	6	·	–	1	8	6	5
IV	8	1,7	4,5	1,6	1,5,5	3,1	1,8	2,7	2,5	3,5	8,5	3,8	1	3,5	0,5	3,0	9	2,7	6,1,0	1,6,8	1,1	1,1	·	·	1	1,5	9	2	·	·	–	3	6	1,1	1
V	2,5	1,8	1,4	2,9	2,1,5	2,5	1,4	1,9	1,2	3,6	3,5	4,4	4,5	6,2	3	4,3	1,8	2,4	6,8,5	2,0,7	9	·	·	·	·	1,2	1,0	2	·	·	–	1	2	1,6	·
VI	1,5	1,7	5,5	1,7	4,5	3,3	2,5,5	5,2	1,8,5	4,4	4	5,1	5,5	5,3	1	5,0	2,4	3,3	3,0,9	9,4	2,3	·	·	·	1,6	8	7	·	·	·	–	5	8	1	·
VII	1	1,5	2	1,8	6	2,8	2,5	3,2	2,5	4,4	8,5	6,7	4	5,0	0,5	1,0	2,1	3,1	9,7,0	2,3,9	1,6	·	·	·	1,5	1,8	1,2	4	1	·	–	4	3	1,4	·
VIII	1	2,0	1,5	1,0	8	1,6	1,9	3,2	1,6,5	3,7	1,1	4,0	4,5	5,9	0,5	3,0	3,1	2,3	6,4,6	1,9,1	2,8	·	·	·	7	1,3	9	3	1	1	–	5	2	3	·
IX	·	·	2,5	2,6	3	1,3	1,7,5	3,4	2,2,5	4,2	1,8,5	6,8	4	7,8	·	·	2,2	3,6	5,1,3	9,5	1,2	1	·	·	2	1,4	1,1	·	2	·	–	1	4	1,1	·
X	1,5	1,0	1,5	1,3	5,5	2,2	2,1	3,4	2,5	4,2	9,5	3,6	0,5	5,0	0,5	1,0	2,8	2,5	2,4,9	8,6	2,0	4	·	·	·	4	3	·	1	·	–	·	7	7	·
XI	2,5	5,8	2,4,5	2,2	1,2,5	2,3	1,0	4,4	8,5	4,5	7	4,4	9,5	5,3	3,5	6,4	1,2	3,2	2,0,3	–	–	–	1	–	·	6	5	·	·	·	–	·	6	1,6	1
XII	7,5	2,5	9	2,3	5	2,5	1,0	5,1	2,7,5	4,6	1,4,5	3,3	6,5	5,5	8	3,2	5	3,6	1,7,0	5,7	8	–	7	–	·	7	4	·	·	·	–	·	3	1,4	3
Rok	3,3	1,9	7,3	2,5	1,0,8	3,0	2,1,0	4,1	2,6,7	4,6	1,1,6,5	5,0	5,5	5,5	2,0,5	2,9	2,1,2	3,4	5,3,8,7	2,3,9	1,6,VII	–	–	–	4,1	1,3,1	9,1	1,3	2,7	1	–	2,0	5,3	1,2,9	2,9?

Tarnów — $H_s = 209$ m — $H_b = 209{,}1$ m — $h_w = 14$ m

I	1,5	2,3	3,5	4,4	7	4,7	5,5	2,9	1,2,5	3,0	1,1	2,5	1,9,5	4,0	1,4,5	3,7	1,8	2,8	2,1,5	7,2	5	2,5	8	5	·	9	5	·	2	·	·	·	·	1,5	1,8
II	3,5	2,1	4	1,8	1,5	2,3	7	3,5	2,5	4,1	1,3,5	3,5	1,2,5	4,2	8	4,2	9	3,3	2,3,1	5,6	2,1	1,1	1	·	·	1,2	8	·	3	·	1	·	3	1,4	9
III	5	3,7	6	3,8	1,6	4,4	1,5,5	5,1	6,5	5,1	3	4,5	9	4,9	1,0	4,2	2,2	3,5	3,1,7	1,1,8	1,8	1,4	4	2	·	9	7	1	4	·	1	1	5	9	6
IV	8	2,9	8,5	3,6	1,2,5	2,3	8,5	2,0	7,5	3,2	3,5	1,9	1,2,5	2,2	1,4	2,2	1,5	2,1	4,3,6	1,3,1	1,1	5	·	·	1	1,7	1,1	2	·	·	3	3	4	1,2	·
V	1,1	2,0	2,0	2,9	9	3,7	9	1,8	5,5	2,0	2	1,5	8	2,9	1,7,5	3,0	1,1	2,4	7,6,9	1,8,6	1,0	·	·	·	·	1,4	1,0	3	·	·	·	1	1	1,6	·
VI	1,0,5	2,7	5,5	2,8	6	1,4	8	3,3	1,3	2,9	2	1,7	1,2,5	3,2	1,5,5	2,8	1,7	2,3	2,1,2	5,8	5	·	·	·	1,3	1,2	9	·	2	·	·	6	5	5	·
VII	2	2,5	·	·	3,5	3,4	1,2,5	2,0	6	2,0	4	2,5	2,1	2,9	1,6	2,9	2,8	1,8	9,9,8	2,1,9	1,6	·	·	·	1,3	1,8	1,4	3	·	·	·	9	2	1,5	·
VIII	2	1,8	1,5	1,0	4	1,8	9	2,1	5	1,7	7	1,5	1,6,5	2,8	2,4	3,1	2,4	1,8	1,1,9,0	5,1,3	1,6	·	·	·	7	1,6	1,2	4	1	·	2	6	2	3	·
IX	3,5	1,9	2	1,5	1	1,5	8	1,6	4	2,0	4	1,6	2,6	3,7	1,9,5	3,8	2,2	2,3	6,3,6	1,3,2	4	·	·	·	2	1,5	1,2	2	2	1	2	·	3	1,2	·
X	1,5	1,0	1,5	1,0	3	1,3	1,2,5	2,2	1,0,5	2,1	3,5	1,4	1,1,5	2,2	1,2	2,4	3,7	1,2	2,3,2	7,8	2,0	1	·	·	·	7	5	·	·	·	3	·	6	6	·
XI	3	8,7	3	5,2	2,3,5	3,1	1,2	3,0	1,0,5	4,8	2	1,7	1,7	6,8	4	6,0	1,5	3,9	2,2,1	1,0,4	1,1	1,0	3	1	·	9	4	1	4	·	5	·	6	1,6	1
XII	1,1	2,7	5	3,7	5,5	3,2	9,5	3,7	1,3,5	3,4	1,2	2,9	1,3,5	1,7	1,0	3,6	1,3	3,0	1,9,1	9,1	1,4	2,4	8	3	·	1,1	5	·	4	1	1	·	4	1,1	5
Rok	6,2,5	2,9	6,0,5	2,6	9,2,5	2,8	1,1,7	2,8	1,1,9,5	3,0	6,7,5	2,5	1,7,9,5	3,7	1,6,5	3,5	2,3,1	2,5	5,6,4,8	5,1,3	1,6,VIII	9,0	2,4	1,1	3,6	1,4,9	1,0,2	1,6	2,2	2	1,8	2,5	4,1	1,3,7	3,9

Tyniec — $H_s = 210$ m — $h_w = 16$ m

I	0,5	6,0	3,5	2,9	5	1,4	·	·	1	1,0	1,7,5	2,2	1,7,5	3,0	·	·	4,8	1,2	1,8,7	5,5	6	2,6	9	5	·	6	4	·	·	·	–	·	3	1,6	1,8
II	3	1,0	2	1,0	7	1,9	·	·	6	1,9	1,6	2,7	1,7	2,9	·	·	3,3	1,4	2,3,4	1,1,1	2,5	1,4	1	·	·	9	4	1	·	·	–	·	1	1,4	3
III	6	2,2	7	2,3	2,0	3,0	·	·	0,5	2,0	9	3,8	1,1,6	3,0	·	·	3,9	1,7	4,0,0	1,0,4	1,8	1,9	2	2	·	1,0	7	1	·	·	–	1	9	1,2	4
IV	3	2,7	1,1,5	1,7	9,5	1,4	1	1,0	3	1,0	1,5	1,9	1,4	2,0	·	·	3,3	1,1	4,7,8	1,5,6	7	5	·	·	1	1,3	1,1	1	·	·	–	3	5	1,1	·
V	7	1,1	1,4	2,3	1,3	1,9	·	·	1	1,0	4	1,1	1,2	3,3	3	1,3	3,9	1,4	1,7,5	1,8,6	1,4	·	·	·	·	9	6	1	·	·	–	2	1	1,4	·
VI	1,4	1,5	1,4	1,7	1,4,5	1,6	2,5	1,4	·	·	1,2,5	2,5	1,6,5	2,5	·	·	3,6	1,2	2,4,3	9,5	7	·	·	·	1,5	1,1	7	·	·	·	–	5	8	9	·
VII	1,4	1,7	3	1,0	1,9	1,3	2	1,5	2	1,0	1,7,5	2,9	2,1,5	2,7	·	·	3,4	1,5	1,9,7,7	4,3,6	1,6	·	·	·	1,5	1,8	1,6	5	·	·	–	5	1	1,5	·
VIII	·	·	·	·	1,4	1,2	·	·	·	·	1,3	2,0	2,9	2,2	·	·	1,7	1,0	8,4,7	2,8,2	1,6	·	·	·	1,7	1,1	1,0	3	·	·	–	3	5	5	·
IX	1	1,0	1	1,0	3	1,0	·	·	1	1,0	1,6,5	2,5	2,2,5	3,0	·	·	3,9	1,5	1,7,7	1,0,1	2,9	·	·	·	1,2	1,6	1,2	1	·	·	–	·	3	1,0	·
X	·	·	·	·	1,5	1,0	·	·	·	·	6	2,1	1,7	2,1	·	·	6,5	0,6	7,3	3,5	2,2	2	·	·	·	1,4	2	·	·	·	–	·	5	6	·
XI	5	1,8	7,5	2,5	2,2	1,8	2	1,2	2,5	1,0	1,4,5	1,4	1,5	6,0	·	·	3,2	2,0	1,7,4	7,5	1,1	1,0	2	·	·	6	1,4	·	·	·	–	1	1,4	1,8	1
XII	1	2,0	1,4	2,2	7	1,9	·	·	1,4	1,0	1,1,4	1,5,0	1,1,4	3,0	·	·	5,2	1,2	1,3,7	1,4,9	8	2,5	1,0	2	·	6	6	·	1,4	·	–	·	2	1,6	–
Rok	3,1,6	2,0	5,7,6	1,6	1,1,9	1,6	7,5	0,4	1,8	1,2	1,5,5,5	3,0	2,0,3	3,0	3	0,1	4,9,7	1,3	5,7,0,2	1,3,6	1,6,VIII	1,0,4	2,4	9	3,0	1,1,9	8,9	1,3	4	·	–	2,0	4,7	1,4,6	–

Jarosław $\varphi = 50°01'$ $\lambda = 22°42'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.8	-0.5	-2.0	-1.8	0.5	-4.8	4.7	9	-13.0	1,17	–	–	–	–	–	–	–	–	8.7	8.0	7.1	7.9
II	–	–	–	–	2.0	4.8	2.7	3.0	8.3	0.2	12.1	19	-6.3	28	–	–	–	–	–	–	–	–	8.5	8.2	6.3	7.7
III	–	–	–	–	0.0	5.6	2.7	2.8	7.2	-2.1	16.3	30	-12.0	4	–	–	–	–	–	–	–	–	5.7	6.2	4.6	5.5
IV	–	–	–	–	5.7	13.1	9.3	9.4	14.4	3.2	26.0	29	-1.7	16	–	–	–	–	–	–	–	–	6.2	6.6	5.6	6.1
V	–	–	–	–	8.8	13.1	10.5	10.7	14.7	6.2	23.4	18	-0.3	7	88	67	81	79	1.4	6.1	2.7	3.4	7.3	8.5	7.4	7.7
VI	–	–	–	–	16.3	23.0	18.7	19.2	24.5	12.3	32.6	12	5.5	7	79	53	68	67	4.1	13.7	7.0	8.3	4.6	5.9	4.9	5.1
VII	–	–	–	–	17.5	23.0	18.9	19.6	24.5	14.2	33.2	5	8.9	4	86	65	81	77	3.0	11.1	4.6	6.2	6.8	6.4	7.4	6.9
VIII	–	–	–	–	14.8	20.9	16.9	17.5	22.1	12.3	31.5	14	6.3	31	91	68	83	81	1.5	8.6	3.5	4.5	5.6	6.2	5.0	5.6
IX	–	–	–	–	10.6	16.5	12.6	13.1	17.6	8.8	27.0	9	1.3	27	91	66	84	80	1.3	6.5	2.4	3.4	6.7	7.5	6.0	6.7
X	–	–	–	–	5.4	13.3	8.5	8.9	14.2	3.8	22.0	19	-3.8	3	90	63	83	79	1.1	6.3	2.1	3.2	6.2	5.8	3.3	5.1
XI	–	–	–	–	2.0	6.0	3.0	3.5	7.1	0.4	18.1	4	-9.8	30	92	81	91	88	0.5	2.1	0.7	1.1	8.3	7.0	6.1	7.1
XII	–	–	–	–	-2.2	0.3	-1.4	-1.2	1.6	-4.3	11.0	14	-10.2	1	–	–	–	–	–	–	–	–	7.9	7.1	6.1	7.0
Rok	–	–	–	–	6.5	11.6	8.4	8.7	12.9	4.2	33.2	5.VII	-13.0	1,17.1	–	–	–	–	–	–	–	–	6.9	7.0	5.8	6.6

Pszczyna $\varphi = 50°00'$ $\lambda = 18°55'$

I	–	–	–	–	-2.3	0.4	-1.5	-1.2	1.5	–	7.7	6	–	–	92	86	92	90	0.5	0.9	0.5	0.6	8.6	7.7	6.9	7.7
II	–	–	–	–	1.2	4.9	2.3	2.7	6.1	–	10.3	18	–	–	89	78	84	84	0.8	2.1	1.2	1.4	6.4	6.7	6.0	6.4
III	–	–	–	–	1.3	7.4	3.8	4.1	8.7	–	16.3	14	–	–	85	71	84	80	1.2	3.6	1.5	2.1	5.9	5.0	4.5	5.1
IV	–	–	–	–	5.2	11.6	6.6	7.5	12.6	–	24.0	30	–	–	90	63	87	80	1.0	6.2	1.5	2.9	5.9	6.6	5.2	5.9
V	–	–	–	–	8.7	13.4	9.0	10.0	14.6	–	23.4	19	–	–	85	67	86	79	1.7	5.9	1.7	3.1	6.1	6.2	5.0	5.8
VI	–	–	–	–	16.2	22.5	16.7	18.0	23.6	–	30.5	30	–	–	–	–	–	–	–	–	–	–	3.9	5.4	5.6	5.0
VII	–	–	–	–	16.6	22.0	17.1	18.2	23.6	–	34.9	8	–	–	92	72	91	85	1.6	9.0	2.0	4.2	6.0	6.2	6.8	6.3
VIII	–	–	–	–	14.3	20.1	14.9	16.0	21.5	–	28.2	11	–	–	92	65	90	82	1.4	8.6	1.7	3.9	4.6	4.9	4.6	4.7
IX	–	–	–	–	10.3	15.6	11.4	12.2	16.7	–	26.0	8,9	–	–	93	72	94	86	1.0	5.6	0.8	2.5	5.1	5.9	6.4	5.8
X	–	–	–	–	7.0	13.8	7.6	9.0	14.9	–	21.0	19	–	–	–	–	–	–	–	–	–	–	4.1	4.5	2.2	3.6
XI	–	–	–	–	2.9	7.1	3.7	4.4	8.3	–	18.6	4	–	–	–	–	–	–	–	–	–	–	6.9	6.5	6.2	6.5
XII	–	–	–	–	-1.4	0.7	-0.7	-0.5	1.9	–	14.6	13	–	–	–	–	–	–	–	–	–	–	7.0	6.3	5.6	6.3
Rok	–	–	–	–	6.7	11.6	7.6	8.4	12.8	–	34.9	8.VII	–	–	–	–	–	–	–	–	–	–	5.9	6.0	5.4	5.8

Czernichów $\varphi = 50°00'$ $\lambda = 19°41'$

I	–	–	–	–	-2.9	0.8	-2.2	-1.6	2.0	-5.5	9.2	6	-18.6	17	87	78	87	84	0.6	1.5	0.7	0.9	8.8	7.7	7.0	7.8
II	–	–	–	–	1.0	5.5	2.8	3.0	6.8	-0.3	13.0	6	-6.4	23	88	72	84	81	0.8	2.8	1.3	1.8	8.0	7.6	6.3	7.3
III	–	–	–	–	0.4	7.6	3.7	3.8	9.2	-1.2	17.6	28	-10.2	1	89	60	80	76	0.8	5.0	1.8	2.5	6.8	6.0	4.7	5.8
IV	–	–	–	–	5.5	12.0	7.7	8.2	13.9	3.1	26.5	30	-4.0	14	88	58	80	75	1.2	7.0	2.3	3.5	6.3	7.1	6.5	6.6
V	–	–	–	–	8.5	13.6	9.8	10.4	15.3	5.6	23.2	19	0.4	30	82	58	80	73	2.0	7.6	2.5	4.0	6.7	8.0	7.4	7.4
VI	–	–	–	–	16.4	23.4	17.2	18.6	25.0	11.2	33.1	11	5.6	7	76	52	78	69	4.5	14.7	4.3	7.8	4.5	6.2	5.2	5.3
VII	–	–	–	–	17.2	22.9	17.8	18.9	24.5	14.2	35.8	8	9.5	30	84	61	86	77	3.2	12.7	3.2	6.4	6.7	7.1	7.3	7.0
VIII	–	–	–	–	13.8	20.6	15.4	16.3	22.4	11.0	29.1	11	5.5	31	88	61	86	78	2.0	10.2	2.5	4.9	5.9	6.6	4.6	5.7
IX	–	–	–	–	9.7	16.6	11.5	12.3	17.7	7.7	28.2	9	-0.2	26	91	61	86	79	1.2	7.8	1.9	3.6	6.7	6.2	5.6	6.2
X	–	–	–	–	4.0	14.3	7.5	8.3	15.1	2.5	21.5	19	-4.6	3	98	62	92	84	0.2	6.7	1.0	2.6	7.5	4.5	3.4	5.1
XI	–	–	–	–	2.2	6.9	3.6	4.1	8.0	0.4	19.9	5	-9.9	30	94	77	90	87	0.4	2.8	0.8	1.3	8.5	6.4	7.5	7.5
XII	–	–	–	–	-2.6	0.5	-1.4	-1.2	2.1	-5.0	14.4	13	-14.3	11	86	82	87	87	0.7	1.3	0.7	0.9	8.2	7.1	7.0	7.4
Rok	–	–	–	–	6.1	12.1	7.8	8.4	13.5	3.6	35.8	8.VII	-18.6	17.1	88	65	85	79	1.5	6.7	1.9	3.4	7.0	6.7	6.0	6.6

Wieliczka $\varphi = 50°00'$ $\lambda = 20°03'$

I	–	–	–	–	-1.7	1.1	-1.3	-0.8	3.4	-4.4	12.0	2	-18.0	17	85	77	88	82	0.9	1.7	0.9	1.2	9.0	8.1	8.4	8.5
II	–	–	–	–	1.8	5.7	3.2	3.5	8.3	0.4	14.0	6	-5.2	23	84	75	81	80	1.2	2.6	1.6	1.8	8.4	7.2	8.2	7.9
III	–	–	–	–	0.9	7.3	4.0	4.0	10.3	-1.0	19.0	14	-11.6	4	84	67	81	77	1.2	4.1	2.0	2.4	7.4	6.4	6.6	6.8
IV	–	–	–	–	5.4	12.2	8.3	8.6	14.5	3.3	27.3	30	-2.1	15	90	65	80	78	1.1	6.1	2.6	3.3	7.3	7.5	8.3	7.7
V	–	–	–	–	8.7	13.1	9.7	10.3	15.9	5.6	23.8	19	0.9	9	84	65	81	77	1.9	6.3	2.4	3.5	7.7	7.9	7.9	7.8
VI	–	–	–	–	17.1	22.6	17.2	18.5	26.1	11.5	33.1	11	5.8	1	77	60	81	73	4.5	11.4	3.7	6.5	4.8	6.3	5.4	5.5
VII	–	–	–	–	17.7	23.0	18.0	19.2	25.7	13.9	37.8	8	9.7	4	84	64	85	78	3.5	11.7	3.3	6.2	7.2	6.9	8.0	7.4
VIII	–	–	–	–	14.9	20.9	15.8	16.8	23.7	11.5	34.4	12	6.4	24	86	63	83	77	2.6	9.8	3.3	5.2	5.4	6.3	7.2	6.3
IX	–	–	–	–	10.8	16.7	12.2	13.0	18.7	7.9	28.9	9	1.5	27	–	–	–	–	–	–	–	–	6.8	7.0	6.8	6.9
X	–	–	–	–	5.3	14.4	8.2	8.0	16.6	3.3	25.9	19	-3.1	3	–	–	–	–	–	–	–	–	8.6	5.9	5.5	6.6
XI	–	–	–	–	1.9	6.8	3.7	4.0	9.2	0.2	21.4	5	-10.2	30	98	88	89	88	0.5	2.3	0.9	1.2	9.0	8.0	8.0	8.3
XII	–	–	–	–	-1.7	0.9	-0.6	-0.5	3.6	-4.0	14.4	13	-10.1	25	85	80	82	82	0.9	1.5	1.2	1.2	9.0	7.9	8.3	8.4
Rok	–	–	–	–	6.8	12.1	8.2	8.8	14.6	4.0	37.8	8.VII	-18.0	17.1	–	–	–	–	–	–	–	–	7.8	7.1	7.4	7.3

Jarosław

$H_s = 204\ m$ $h_w = 20\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D, °mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	C Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Max<0	Max<0	Max<10	Max>25	LICZBA DNI (n) Opad R ≥0.1	≥1.0	≥10.0	Wiatr ≥10	≥15	=	≈	●	◉	⊞
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	13.8	5.2	6	27	10	2	·	10	6	·	-	-	-	·	·	19	18
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	21.3	4.2	8	13	1	·	·	12	8	·	-	-	-	·	·	15	6
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	31.0	14.6	18	20	4	1	·	8	6	1	-	-	-	·	6	10	5
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.5	18.2	11	6	·	·	2	11	8	1	-	-	-	·	4	10	·
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85.3	21.3	9	1	·	·	·	12	9	4	-	-	-	·	·	18	·
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	60.6	15.5	9	·	·	·	14	10	7	1	-	-	-	7	3	1	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	157.4	51.1	9	·	·	·	13	16	14	3	-	-	-	3	1	13	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	48.6	12.2	5	·	·	·	6	14	10	1	-	-	-	3	3	5	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.0	12.0	12	·	·	·	2	12	10	1	-	-	-	·	2	8	·
X	·	·	·	·	1	3.0	1.7	1.8	1.5	1.1	3.7	3.1	9	3.7	1.3	2.5	1	2.5	14.1	7.8	20	5	·	·	·	5	3	·	3	·	·	·	6	6	·
XI	1	6.0	3	3.7	3	5.0	4.2	2.7	8	1.5	1.4	2.6	7	4.6	1.0	14.6	2	4.1	19.4	8.0	28	12	2	·	·	8	5	·	4	3	·	·	1	14	·
XII	5	4.0	2	5.0	3	2.3	5	1.8	2.0	2.4	3.9	6.2	9	3.2	1.0	5.8	·	4.6	13.4	3.8	5	28	1.0	1	·	7	5	·	7	2	·	·	2	16	3
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	552.4	51.1	9.VII	112	27	4	37	125	91	12	-	-	-	13	28	135	31

Pszczyna

$H_s = 270\ m$ $h_w = 18\ m$

I	·	·	10.5	2.7	5.5	3.3	4.5	2.0	2.5	2.4	16.5	2.3	32.5	2.6			21	2.0	27.4	8.5	5	-	1.0	-	·	10	9	·	·	·	-	·	·	13	19
II	1.5	3.7	9	2.1	6	1.3	2.5	2.6	12.5	3.0	2.2	3.8	1.5	3.4	1.5	3.7	1.4	2.6	39.2	10.0	22	-	1	-	·	13	10	1	2	·	-	·	3	9	5
III	3	1.3	2	1.2	2.5	4.4	3	1.8	7	2.3	1.3	1.7	15.5	2.8	7.5	2.1	1.7	2.4	45.7	10.0	29	-	3	-	·	10	9	1	1	1	-	1	7	9	4
IV	1.1	1.3	4.5	2.3	1.0	1.6	1.5	1.3	1.5	2.0	2.5	2.6	2.5	3.0	15.5	1.9	4.1	1.0	59.3	17.5	7	-	·	-	·	11	10	1	1	·	-	3	6	10	·
V	6.5	1.8	14.5	1.9	1.0	1.8	5.5	1.5	5.5	1.9	7.5	2.1	4	2.1	10.5	1.6	2.9	1.2	54.3	32.0	20	-	·	-	·	8	6	2	·	·	-	2	4	12	·
VI	6.5	2.1	1.5	1.0	3	1.3	6	2.0	6.5	1.3	1.1	1.8	8.5	2.3	1.0	1.8	3.7	1.1	62.5	23.8	7	-	·	-	1.0	8	8	2	·	·	-	4	3	4	·
VII	3	1.0	1.5	1.7	5.5	1.5	1	2.0	4	2.0	2.9	2.4	6.5	2.3	5.5	1.8	3.7	1.3	183.2	44.0	16	-	·	-	1.0	22	21	5	·	·	-	8	3	1.0	·
VIII	3	1.7	·	·	2	1.5	·	·	4	2.1	2.0	2.3	5	1.8	6	2.0	5.3	0.9	64.7	17.2	28	-	·	-	4	10	8	1	1	1	-	2	5	2	·
IX	3	2.0	1	2.0	1	2.0	1	1.0	7	2.2	2.9	2.7	8	2.6	7	2.1	3.3	1.6	87.7	16.2	29	-	·	-	2	18	17	2	·	·	-	·	3	7	·
X	·	·	3	1.7	2	1.0	·	·	1	2.0	9	1.8	1.3	2.1	1.2	1.8	5.3	0.8	11.3	5.8	20	-	·	-	·	2	2	·	·	·	-	·	11	2	·
XI	·	·	7	2.0	1.3	2.1	·	·	7	2.9	1.8	2.6	1.1	2.2	5	4.8	2.9	1.7	23.2	9.8	28	-	1	-	·	8	8	·	·	·	-	·	6	17	·
XII	2	2.0	3	1.7	6	2.7	1	2.0	4	2.0	3.6	2.8	7	2.9	3	1.3	3.1	1.7	25.6	7.0	2.13	-	7	-	·	5	5	·	·	·	-	·	6	12	1
Rok	39.5	1.4	57.5	1.7	89	2.0	26	1.4	62.5	2.2	213.5	2.4	128.5	2.5	83.5	2.1	39.5	1.5	684.1	44.0	16.VII	-	22	-	26	125	113	15	5	2	-	20	57	107	29

Czernichów

$H_s = 218\ m$ $h_w = 16\ m$

I	6.5	1.5	5	2.2	1	1.0	0.5	3.0	0.5	3.0	9.5	2.5	25.6	2.6	5.5	1.6	3.9	1.3	28.4	6.8	6	27	9	5	·	11	8	·	·	·	-	·	1	18	-
II	4.5	1.7	4.5	1.7	·	·	3	2.3	4.5	1.8	13.5	2.9	22.5	2.6	6.5	1.4	2.5	1.6	21.5	8.3	25	15	1	·	·	13	6	·	·	·	3	·	·	11	-
III	7.5	2.7	15.5	4.5	4.5	5.6	1	2.0	1	2.0	7	2.9	18.5	3.8	4	2.4	3.4	2.4	41.8	12.8	18	18	1	·	·	10	7	1	3	2	1	1	6	10	-
IV	1.2	1.5	7.5	1.7	·	·	2	2.5	2	2.5	3	1.0	16.5	1.3	7	1.7	4.0	0.9	51.4	21.2	7	7	·	·	2	15	12	1	1	1	3	2	3	12	-
V	9	1.9	15.5	2.4	4.5	1.9	2	2.8	4	2.5	4.5	1.8	11.5	2.4	6	1.8	3.6	1.3	34.3	9.4	10	·	·	·	·	11	7	·	·	·	1	2	3	17	-
VI	6.5	1.8	8.5	1.7	6.5	1.8	1	4.5	1.5	3.7	8.5	2.2	18.5	2.4	7	4.6	3.2	1.6	36.1	8.3	22	·	·	·	1.6	10	9	·	2	2	1	6	4	5	-
VII	3.5	2.7	4.5	2.1	6	3.2	3.5	1.9	2	2.2	8	3.6	20.5	3.0	6	2.8	3.9	1.7	173.6	32.5	16	·	·	·	1.3	19	17	5	·	·	·	8	1	15	-
VIII	7.5	2.5	0.5	3.0	1.5	1.7	·	·	·	·	6.5	2.3	26	2.1	12	2.1	3.9	1.3	103.9	-	-	·	·	·	8	15	13	3	·	·	2	1	2	7	-
IX	3	1.0	2	2.0	1	3.0	·	·	1.5	2.0	1.4	5.1	3.1	4.2	1.5	3.7	3.6	2.5	76.7	11.7	3	1	·	·	2	18	12	2	1	·	6	·	2	8	-
X	5	1.0	4.5	1.6	1.5	2.7	·	·	1	1.0	3.5	4.0	18.5	3.0	3	4.5	5.6	1.1	14.4	7.3	20	5	·	·	·	6	3	·	·	·	17	·	4	5	-
XI	5.5	4.8	13.5	3.4	11.5	5.0	2.5	1.4	3	2.8	7	5.5	12.5	4.7	2.5	4.8	3.2	2.8	25.0	8.1	27	11	3	·	·	9	6	·	3	·	12	·	1	17	-
XII	9	1.9	7	2.8	3.5	3.0	·	·	1.5	1.0	9	4.9	20.5	3.8	4.5	3.1	3.8	2.0	32.5	7.6	14	26	1.0	4	·	15	10	·	1	1	4.3	·	3	20	-
Rok	79.5	2.1	88.5	2.4	41.5	2.4	15.5	1.7	22.5	2.0	9.4	3.2	24.2	3.0	65.5	2.9	44.6	1.7	639.6	32.5	16.VII	110	24	9	41	152	110	12	11	6	-	20	30	145	-

Wieliczka

$H_s = 225\ m$ $h_w = 25\ m$

I	1	1.0	9.5	3.6	2.5	1.0	7	1.9	11.5	1.6	3.8	2.4	4.2	4.7	5.5	2.2	6	2.5	29.7	7.5	13	27	8	3	·	12	8	·	1	·	4	·	·	21	22
II	3	1.7	2.5	1.0	5.5	1.5	4.5	1.4	2.1	3.1	2.6.5	2.6	1.0	4.8	1.1	1.8	·	2.7	28.8	9.1	25	1.0	1	·	·	15	9	·	3	1	4	·	·	15	7
III	3	2.3	2.1	2.8	1.2	3.9	3	1.8	7.5	1.6	2.1.5	4.8	1.3	4.1	2	2.0	1.0	3.1	44.7	11.4	19	1.6	2	2	·	10	7	1	5	2	3	1	2	14	6
IV	4	2.2	12.5	2.3	12.5	1.6	3	2.7	6	1.8	1.5.5	2.2	1.7	1.9	11.5	1.9	8	2.1	67.4	20.3	7	5	·	·	1	17	9	3	·	·	5	3	·	18	·
V	6	1.5	26.5	2.2	7	1.7	2	1.5	4	1.5	8	2.1	1.4.5	2.3	1.3	2.3	1.2	1.8	36.3	10.2	9	·	·	·	·	11	6	1	·	·	2	2	1	17	·
VI	5	1.4	4.5	1.9	1.2	2.0	1.0	1.4	1.5.6	1.8	1.7	2.7	1.0	1.8	6	1.8	1.0	1.7	44.2	14.4	19	·	·	·	1.7	10	7	2	·	·	·	7	4	7	·
VII	1.5	1.3	1.5	1.0	1.1	1.7	7	1.7	10.5	2.0	3.4.5	2.6	1.5	2.5	6	1.8	6	2.1	188.0	50.2	11	·	·	·	1.5	18	17	5	1	·	·	7	2	17	·
VIII	1	1.0	1	1.0	3.5	1.1	4	1.5	9.5	2.2	3.9.5	2.0	2.0	2.3	3.5	1.9	1.1	1.8	81.7	26.6	16	·	·	·	1.1	15	10	8	2	2	2	3	2	8	·
IX	·	·	7	1.7	2	1.5	4	1.0	10.5	3.2	4.2.5	4.0	1.5	3.2	5	1.6	4	3.1	48.6	9.2	29	·	·	·	2	18	13	·	3	1	1	1	1	12	·
X	1.5	1.0	5.5	1.2	1.2	1.3	1.5	1.0	7.5	2.1	3.2	1.8	1.4	1.6	5	1.1	1.4	1.4	16.0	6.1	20	3	·	·	1	5	3	·	·	·	13	·	·	9	·
XI	4.5	6.1	2.6	2.2	1.4	1.3	3	2.0	5.5	1.8	1.5	5.7	6	3.7	5	4.1	1.1	2.8	33.3	8.5	11	1.2	1	1	·	8	5	·	2	·	1	1	1	19	1
XII	4.5	1.4	6.5	2.7	4	1.4	5.5	2.4	1.2.5	3.3	3.0	2.8	1.0	2.1	8	2.0	7	2.5	20.9	4.6	1.4	2.5	9	1	·	13	8	·	2	1	4	·	·	21	3
Rok	3.5	1.7	12.4	2.0	9.8	1.7	6.4.5	1.7	1.8.6.5	2.2	3.2.0	3.0	1.5.6.5	2.9	6.1.5	2.0	9.9	2.3	64.0.5	50.2	14.VII	9.8	21	7	47	152	102	20	19	7	49	25	13	178	39

Skawina

$\varphi = 49°59'$ $\lambda = 19°48'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.3	0.8	-4.5	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	6.6	7.1
II	–	–	–	–	1.4	5.8	2.7	3.2	7.2	-0.7	12.3	6.	-5.1	23,24,27	–	–	–	–	–	–	–	–	7.6	7.2	7.1	7.3
III	–	–	–	–	0.4	7.8	3.8	4.0	8.9	-4.7	17.9	27	-12.2	1	–	–	–	–	–	–	–	–	6.6	6.2	5.2	6.0
IV	–	–	–	–	5.2	12.1	8.2	8.4	13.9	2.5	26.4	30	-4.7	14	–	–	–	–	–	–	–	–	6.4	7.2	6.8	6.8
V	–	–	–	–	8.3	13.5	9.4	10.2	15.4	4.8	22.5	19	0.9	9	–	–	–	–	–	–	–	–	7.4	7.5	7.2	7.4
VI	–	–	–	–	16.3	22.9	16.2	17.9	24.7	9.5	34.9	11	2.7	7	–	–	–	–	–	–	–	–	5.1	5.9	5.3	5.4
VII	–	–	–	–	16.7	22.7	17.4	18.5	24.6	13.5	36.6	8	8.1	4	–	–	–	–	–	–	–	–	7.6	7.0	7.2	7.3
VIII	–	–	–	–	13.8	20.1	15.7	16.3	22.2	10.3	28.5	13	4.7	31	–	–	–	–	–	–	–	–	6.2	6.2	5.9	6.1
IX	–	–	–	–	10.0	16.2	11.8	12.4	17.3	7.2	27.7	9	-0.8	27	–	–	–	–	–	–	–	–	6.3	6.4	6.4	6.4
X	–	–	–	–	3.9	14.1	7.5	8.2	15.0	1.9	24.0	19	-3.3	3	–	–	–	–	–	–	–	–	6.7	5.9	5.2	5.9
XI	–	–	–	–	2.5	7.0	3.8	4.3	7.9	0.4	19.5	5	-9.1	30	–	–	–	–	–	–	–	–	7.8	7.5	7.5	7.6
XII	–	–	–	–	-2.4	0.8	-1.1	-1.0	1.9	-5.0	13.8	13	-16.2	11	–	–	–	–	–	–	–	–	7.5	7.5	6.9	7.3
Rok	–	–	–	–	6.2	12.0	7.8	8.4	–	–	36.6	8.VII	–	–	–	–	–	–	–	–	–	–	6.9	6.8	6.4	6.7

Grodkowice

$\varphi = 49°59'$ $\lambda = 20°16'$

I	–	–	–	–	-2.0	0.2	-1.4	-1.2	1.4	-4.0	7.8	6	-15.5	17	–	–	–	–	–	–	–	–	9.0	7.8	6.0	7.6
II	–	–	–	–	1.6	5.0	2.9	3.1	6.7	0.4	12.5	6	-4.9	23,28	–	–	–	–	–	–	–	–	7.4	7.6	6.6	7.2
III	–	–	–	–	0.9	6.4	4.1	3.9	8.5	-0.5	17.0	14	-9.7	4	–	–	–	–	–	–	–	–	6.0	5.8	4.8	5.5
IV	–	–	–	–	5.4	11.3	8.6	8.5	13.4	4.0	25.8	30	-1.4	14	–	–	–	–	–	–	–	–	6.1	6.7	6.5	6.4
V	–	–	–	–	8.2	12.4	10.3	10.3	14.4	6.2	21.7	19	0.5	9	–	–	–	–	–	–	–	–	6.5	7.9	7.7	7.4
VI	–	–	–	–	15.8	21.7	18.4	18.6	24.4	12.7	32.0	11	7.4	1	–	–	–	–	–	–	–	–	3.4	5.4	4.4	4.4
VII	–	–	–	–	16.9	21.9	18.5	19.0	24.0	14.4	35.1	5	10.1	30	–	–	–	–	–	–	–	–	6.6	7.2	7.2	7.0
VIII	–	–	–	–	14.0	19.9	16.8	16.9	21.8	11.9	29.0	12	6.6	24	–	–	–	–	–	–	–	–	3.8	5.9	6.5	5.4
IX	–	–	–	–	10.2	15.6	12.3	12.6	17.3	8.0	27.0	9	2.0	27	–	–	–	–	–	–	–	–	5.6	6.5	6.3	6.1
X	–	–	–	–	6.5	13.2	9.3	9.6	14.6	4.9	23.2	19	-1.0	3	–	–	–	–	–	–	–	–	5.9	4.8	3.9	4.9
XI	–	–	–	–	2.9	6.4	4.0	4.3	8.0	1.5	19.0	1	-9.1	30	–	–	–	–	–	–	–	–	7.3	6.4	6.6	6.8
XII	–	–	–	–	-1.8	0.2	-0.8	-0.8	2.7	-3.6	12.0	13	-9.8	24	–	–	–	–	–	–	–	–	7.3	7.7	7.2	7.4
Rok	–	–	–	–	6.6	11.2	8.6	8.8	13.1	4.7	35.1	5.VII	-15.5	17.1	–	–	–	–	–	–	–	–	6.2	6.6	6.1	6.3

Bochnia – Chodenice

$\varphi = 49°59'$ $\lambda = 20°24'$

I	–	–	–	–	-2.0	0.9	-2.1	-1.3	2.0	-5.2	8.1	1	-20.1	17	–	–	–	–	–	–	–	–	8.6	7.9	6.1	7.5
II	–	–	–	–	1.7	6.0	3.2	3.5	7.2	-0.1	13.6	6	-4.6	23	–	–	–	–	–	–	–	–	8.0	8.0	7.4	7.8
III	–	–	–	–	0.2	7.4	3.5	3.6	9.2	-1.8	18.5	14	-11.8	4	–	–	–	–	–	–	–	–	6.7	6.2	5.4	6.1
IV	–	–	–	–	4.8	12.3	7.3	7.9	13.8	2.5	25.9	30	-2.4	15	93	61	85	80	0.6	6.8	1.7	3.0	6.7	7.1	6.7	6.8
V	–	–	–	–	8.7	13.2	9.1	10.0	15.0	5.2	22.4	19,23	1.0	9	84	62	84	77	1.9	6.8	2.0	3.6	6.7	8.2	7.3	7.4
VI	–	–	–	–	16.4	22.9	16.7	18.2	24.6	10.2	31.7	11	3.6	7	78	52	80	70	4.3	14.0	4.0	7.4	4.2	6.8	4.7	5.2
VII	–	–	–	–	17.3	22.5	17.9	18.9	24.3	13.6	35.1	5,8	6.8	4	85	63	84	77	3.1	11.5	3.6	6.1	6.8	7.2	7.3	7.1
VIII	–	–	–	–	14.4	20.2	15.5	16.4	21.9	11.1	29.7	12	3.8	24	88	62	86	79	2.1	9.7	2.6	4.8	4.9	6.4	5.7	5.7
IX	–	–	–	–	9.9	16.6	11.8	12.5	17.5	7.7	27.5	9	0.3	26	90	62	87	80	1.4	7.8	1.8	3.7	6.4	7.2	6.4	6.7
X	–	–	–	–	4.5	11.1	7.2	8.2	14.9	2.3	23.1	19	-4.3	3	95	62	91	83	0.6	6.6	1.2	2.8	7.5	5.5	3.4	5.5
XI	–	–	–	–	1.6	7.2	3.2	3.8	8.3	-0.2	20.2	1	-9.5	30	92	76	89	86	0.6	3.3	0.9	1.6	7.6	7.1	7.3	7.3
XII	–	–	–	–	-2.1	0.8	-0.6	-0.6	2.3	-4.5	13.1	13	-13.3	11	84	80	84	83	1.0	1.4	1.0	1.1	7.7	8.0	6.7	7.5
Rok	–	–	–	–	6.3	12.0	7.7	8.4	13.4	3.4	35.1	5,8.VII	-20.1	17.1	–	–	–	–	–	–	–	–	6.8	7.1	6.2	6.7

Jastrzębie – Zdrój

$\varphi = 49°57'$ $\lambda = 18°34'$

I	–	–	–	–	-1.9	0.9	-1.0	-0.8	1.5	–	7.2	6	–	–	83	76	81	80	0.9	1.5	1.1	1.2	8.9	8.0	7.7	8.2
II	–	–	–	–	1.2	5.7	2.7	3.1	6.5	–	11.1	6	–	–	84	68	81	78	1.1	3.2	1.5	1.9	8.1	7.7	6.6	7.5
III	–	–	–	–	1.5	8.1	4.0	4.4	9.7	–	16.5	14	–	–	83	57	81	74	1.3	5.2	1.7	2.7	7.4	6.2	5.5	6.4
IV	–	–	–	–	5.6	12.3	7.4	8.2	13.7	–	25.7	30	–	–	83	56	80	73	1.8	7.8	2.2	3.9	5.9	6.6	6.4	6.3
V	–	–	–	–	9.1	14.2	9.5	10.6	15.7	–	24.9	19	–	–	79	57	80	72	2.4	7.8	2.4	4.2	7.3	7.2	6.8	7.1
VI	–	–	–	–	16.4	22.9	16.3	18.0	24.7	–	34.8	30	–	–	80	54	85	73	3.9	13.6	3.0	6.8	5.2	5.4	5.7	5.4
VII	–	–	–	–	17.2	22.6	17.5	18.7	24.3	–	35.0	8	–	–	86	64	88	79	2.9	11.6	2.7	5.7	6.9	6.1	7.4	6.8
VIII	–	–	–	–	13.8	20.6	14.7	16.0	22.5	–	29.1	11	–	–	88	59	88	78	1.9	10.3	2.1	4.8	6.0	5.8	5.5	5.8
IX	–	–	–	–	9.8	15.9	11.1	12.0	17.4	–	27.5	9	–	–	89	63	88	80	1.4	7.1	1.6	3.4	6.8	7.2	6.2	6.7
X	–	–	–	–	5.4	13.9	6.8	8.2	15.1	–	21.3	10	–	–	92	61	90	81	0.8	6.5	1.0	2.8	7.0	5.5	4.7	5.7
XI	–	–	–	–	3.6	7.6	4.3	5.0	8.5	1.8	19.7	5	-9.3	30	88	72	86	82	1.1	3.5	1.5	2.0	8.6	7.5	7.8	8.0
XII	–	–	–	–	-1.9	1.0	-0.1	-0.3	2.3	-3.3	14.5	13	-13.2	11	88	79	84	84	0.8	1.5	1.0	1.1	8.3	7.1	7.1	7.5
Rok	–	–	–	–	6.6	12.1	7.8	8.6	13.5		35.0	8.VII	–	–	85	64	84	78	1.7	6.6	1.8	3.4	7.2	6.7	6.4	6.8

Skawina

$H_s = 210\ m$ $h_w = 16\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, ∑nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R 0.1 ≤ R < 10	10 ≤ R < 100	R ≥ 100	Wiatr v 10 ≤ v < 15	v ≥ 15	≡	≈	◔	●	▦
I	0.5	4.0	5.5	6.0	3	4.2	1	1.0	·	·	11.5	1.7	44.5	3.0	2	2.0	25	2.2	24.0	8.8	6	–	–	–	–	11	7	·	·	·	–	·	2	12	–
II	1.5	2.7	3	3.7	5	3.5	2	3.8	2	5.0	17.5	4.1	37	4.4	3	3.2	13	3.5	34.4	15.5	25	17	1	·	·	14	7	1	5	1	–	·	1	11	–
III	4	5.1	10.5	4.1	14.5	6.0	·	·	·	·	9	4.7	29.5	6.1	3.5	3.0	14	4.6	36.9	14.0	19	20	3	2	·	8	6	1	6	5	–	1	2	10	–
IV	4.5	2.9	8	3.9	7.5	3.9	2.5	2.2	·	·	2	2.2	42.5	3.4	7	3.2	16	2.8	57.2	22.5	7	10	·	·	1	12	10	2	3	·	–	2	3	12	–
V	9.5	3.2	18	4.1	12	3.3	1	1.0	2.5	2.2	4	2.6	29.5	2.9	7.5	2.9	9	2.9	28.9	9.0	9	·	·	·	1	11	6	·	1	1	–	2	·	16	–
VI	6	2.9	8	2.6	6	2.8	1.5	3.0	3.5	4.1	9	2.9	33.5	2.8	3.5	3.1	19	2.2	36.1	14.5	22	·	·	·	14	12	9	1	·	·	–	5	5	5	–
VII	5.5	4.9	6	2.7	5	2.8	1.5	3.3	1	4.5	13.5	2.3	42.5	2.6	5	2.2	13	2.2	24.4	6.2.1	15	·	·	·	13	17	17	7	·	·	–	5	·	13	–
VIII	4.5	3.1	4	2.0	1.5	2.0	·	·	0.5	1.0	4.5	3.2	52.5	2.4	4.5	2.8	21	1.9	65.8	15.1	28	·	·	·	6	11	9	4	·	·	–	2	1	10	–
IX	10.5	1.5	5	1.5	0.5	3.0	2.5	1.4	2.5	2.0	11.5	3.7	42	3.0	6.5	2.2	9	2.4	55.8	10.2	29	1	·	·	2	11	11	1	·	·	–	·	1	9	–
X	11	1.2	9	1.8	3	1.5	0.5	1.0	0.5	1.0	3	3.0	25	2.2	13	2.0	28	1.3	16.4	7.7	20	7	·	·	·	5	3	·	·	·	–	·	·	8	–
XI	1.4	1.7	20.5	3.0	14.5	2.9	2	2.0	2	4.0	2	3.5	21	3.9	3	4.2	11	2.6	22.9	8.2	28	11	3	·	·	8	5	·	·	·	–	1	1	18	–
XII	3.5	1.0	7.5	2.6	3.6	3.0	0.5	1.0	2	1.8	11	2.4	44	2.6	9	1.7	12	2.1	29.9	7.0	13	26	11	3	·	12	7	·	·	·	–	·	·	14	–
Rok	75	2.4	113	3.2	76	3.2	15	1.6	16.5	2.1	98.5	3.0	443.5	3.3	67.5	2.7	190	2.6	650.5	62.1	15.VII	–	–	–	37	132	97	17	15	7	–	18	46	138	–

Gradkowice

$H_s = 280\ m$ $h_w = 10\ m$

I	0.5	4.0	7.5	6.4	1	8.0	1.5	4.0	1.5	5.0	1.5	5.5	31	7.4	4	7.0	31	4.4	27.3	5.9	13	24	11	5	·	15	9	·	10	·	–	·	2	16	–
II	1.5	5.3	1	5.5	1.5	4.3	5	3.2	15.5	4.3	17	7.4	22	6.6	8.5	4.4	12	4.9	21.6	7.6	21	9	2	·	·	12	7	·	8	1	–	·	3	16	–
III	5.5	3.5	4	4.2	15.5	6.5	·	·	5	6.0	5	6.3	16	9.6	7	6.4	35	4.2	46.5	11.8	19	15	3	·	·	10	8	2	6	1	–	1	7	9	–
IV	1.0	5.4	5	5.2	5	4.6	·	·	3	2.3	2	7.2	19	6.6	10	5.0	36	3.3	46.3	12.5	7,11	5	·	·	1	16	9	2	1	·	–	5	4	13	–
V	8.5	3.4	1.5	5.5	5.5	3.7	0.5	1.0	1.5	4.0	3.5	2.3	17	6.7	8.5	5.6	33	3.3	58.8	12.8	20	·	·	·	·	12	9	3	5	·	–	2	1	17	–
VI	9	4.1	4	2.2	3	2.8	3	3.0	2	2.2	5.5	2.7	21.5	5.3	16	3.9	26	2.9	46.2	5.5	22	·	·	·	12	10	7	·	4	·	–	6	6	4	–
VII	10.5	2.1	3	4.3	4	4.2	·	·	4	2.8	11.5	3.6	29.5	6.7	7.5	4.5	23	3.6	164.3	44.4	16	·	·	·	11	18	14	4	4	·	–	6	3	14	–
VIII	2	4.2	1	2.0	2	3.5	1	1.0	·	·	9	4.1	37	5.1	15	4.4	26	3.3	98.3	34.0	28	·	·	·	6	12	9	4	4	·	–	3	4	5	–
IX	5.5	3.0	1.5	3.0	·	·	·	·	4	4.8	15	5.2	47	6.1	3	3.5	14	4.6	28.4	5.0	4	·	·	·	3	11	9	·	10	1	–	·	3	9	–
X	6	1.8	·	·	·	·	1	4.0	7	1.9	6	6.2	35.5	3.0	15.5	2.3	22	2.2	19.0	10.2	23	1	·	·	·	3	2	1	1	·	–	·	8	5	–
XI	1.3	3.5	4.9	3.7	3	1.7	6	3.6	8	2.6	5	6.8	19	9.9	3	8.7	14	4.6	13.7	10.0	11	13	3	·	·	4	4	1	10	1	–	·	5	16	–
XII	1.3	2.8	1.0	3.8	0.5	3.0	5.5	2.6	2	2.0	13.5	7.7	33	5.1	4.5	4.1	11	4.2	20.0	8.5	5	25	8	·	·	5	5	·	7	2	–	·	3	18	–
Rok	8.5	3.6	7.1	3.8	4.1	3.5	2.3.5	4.6	5.3.5	3.2	10.8	5.4	327.5	6.5	102.5	5.0	283	3.8	559.4	44.4	16.VII	92	27	5	33	128	92	17	70	6	–	23	49	142	–

Bochnia – Chodenice

$H_s = 200\ m$ $h_w = 16\ m$

I	·	·	4	5.4	5.5	4.7	1.5	1.6	2.2	2.3	2.6	3.6	18.5	5.6	1	1.5	1	3.5	30.7	8.7	5	26	11	8	·	12	6	·	3	·	1	·	2	18	23	
II	1.5	1.7	1	2.0	6.5	2.5	14.5	3.3	2.5	3.9	22.5	5.0	9.5	7.5	3.5	2.1	·	4.3	23.0	6.2	21	13	1	·	·	11	6	·	3	2	3	·	2	18	7	
III	1.5	4.7	3	5.2	24.5	4.6	17	2.4	12	2.4	16.5	4.7	43.5	6.9	6	4.2	·	4.3	44.5	12.4	19	18	2	2	·	10	7	2	6	·	1	1	7	13	6	
IV	5	2.5	4.5	2.1	13.5	2.3	18.5	1.9	14	2.4	22.5	3.5	4.5	4.2	7.5	3.5	·	2.7	44.7	12.6	11	9	·	·	1	17	10	2	·	·	3	3	5	17	·	
V	4.5	4.0	9	4.7	18.5	2.9	16	1.8	11.5	2.0	16.5	3.7	9	5.3	7	4.2	1	3.3	52.9	17.1	10	·	·	·	·	12	7	2	2	·	·	2	2	16	·	
VI	5.5	2.2	2.5	4.4	9	2.3	17.5	2.5	16	2.7	21.5	3.2	8.5	7.6	9.5	3.4	·	3.3	31.2	8.6	22	·	·	·	12	12	8	·	1	1	·	8	4	5	·	
VII	2.5	1.8	2	2.0	6.5	2.5	11.5	2.4	23.5	2.5	27.5	3.6	13	5.1	5.5	2.8	1	3.2	199.1	72.8	16	·	·	·	12	19	14	4	1	·	2	9	2	14	·	
VIII	0.5	2.0	1.5	1.0	4.5	1.4	15.5	2.0	17	2.6	29	4.0	17	4.4	7	4.0	1	3.2	86.3	28.0	16	·	·	·	5	14	8	3	1	·	2	4	1	7	·	
IX	3.5	1.7	0.5	2.0	3.5	1.7	15	1.6	18.5	3.4	29	4.9	14	7.6	2	2.0	4	3.9	35.8	6.2	4	·	·	·	2	13	10	·	4	1	1	·	2	10	·	
X	0.5	2.0	·	·	14.5	1.6	26	1.5	20.5	2.0	19	3.0	11	4.0	1.5	2.0	·	2.2	19.8	7.0	20	9	·	·	·	5	4	·	·	·	11	·	3	6	·	
XI	1	9.0	5	5.5	22.5	3.3	22	1.9	11.5	1.8	11.5	5.1	12	9.0	3.5	9.1	1	4.1	17.7	5.6	11	13	3	·	·	11	5	·	6	·	8	·	5	18	1	
XII	2.5	3.4	5.5	4.5	7	2.5	14.5	3.1	27.5	2.5	19.5	6.0	8.5	6.6	6	2.6	2	3.8	16.5	6.3	14	27	9	5	·	12	6	·	3	2	2	·	3	19	2	
Rok	2.8.5	2.9	3.8.5	3.2	136	2.7	203	2.2	219	2.5	261	4.2	139	6.2	59	3.4	11	3.5	602.2	72.8	16.VII	115	26	15	32	148	91	13	30	5	34	27	38	159	39	

Jastrzębie – Zdrój

$H_s = 227\ m$ $h_w = 13\ m$

I	9.5	4.2	4.5	2.6	1.5	3.0	4	1.4	6.5	1.3	23.6	2.3	15.5	2.2	15	2.0	13	1.7	26.8	6.4	5	–	10	–	·	12	9	·	·	·	–	·	·	18	23	
II	6.5	1.7	2.5	2.4	1	2.0	1	2.0	2.0	2.1	17.5	2.4	12	2.5	10.5	2.1	13	1.9	81.7	33.2	18	–	1	–	·	15	13	2	·	·	–	·	·	11	6	
III	6	1.5	14.5	2.7	11.5	2.8	1	2.0	5.5	2.0	7	2.9	9.5	3.0	9	1.9	2.9	1.7	48.0	16.1	17	–	·	–	·	12	9	1	·	·	–	1	3	12	4	
IV	9	1.7	7	2.0	7	1.9	3.5	2.1	3.5	2.0	1.5	2.6	2.5	2.0	2.7	1.8	2.9	1.3	60.7	14.9	7	–	·	–	1	15	10	1	·	·	–	2	4	8	·	
V	7	2.2	27.5	2.2	4	1.6	3.5	2.0	·	·	2	2.5	4	2.0	2.7	1.9	2.1	1.6	44.2	24.0	20	–	·	·	·	10	7	1	·	·	–	2	·	14	·	
VI	4	1.8	6	2.1	6.5	1.9	5.5	1.9	7	1.8	6	2.7	5	3.5	2.5	1.9	2.5	1.5	74.0	23.3	7	–	·	–	1.4	10	8	2	·	·	–	5	4	6	·	
VII	2	2.0	0.5	2.0	4	2.0	4	1.9	12	2.0	6.5	2.2	4.5	2.8	3.4.5	2.0	2.5	1.5	153.8	39.3	16	–	·	–	13	19	16	4	·	·	–	6	2	14	·	
VIII	6.5	1.3	·	·	·	·	5.6	1.2	9.5	1.3	6.5	1.8	9	1.6	3.6	1.5	2.0	1.2	132.4	73.4	14	–	·	–	6	13	9	2	2	2	–	2	·	5	·	
IX	3.5	1.7	1.5	1.3	1	1.0	4.5	1.8	5.5	2.0	14	2.8	15.5	2.6	20.5	1.8	2.4	1.6	122.7	34.2	2	–	·	–	2	19	16	5	·	·	–	1	1	10	·	
X	4.5	1.6	·	·	·	·	1	2.0	1	1.0	9.5	2.2	8	2.3	2.7	1.6	4.2	1.0	12.2	6.8	20	–	·	–	·	4	2	·	·	·	–	·	3	7	·	
XI	3.5	2.3	18.5	2.1	10.5	2.0	1.3	1.9	8	1.8	6	2.8	11.5	2.4	5	2.3	4.4	1.8	28.8	9.7	9	9	4	·	·	9	6	·	·	·	–	·	1	20	1	
XII	2.5	2.0	7.5	2.1	4.5	1.8	1.5	2.3	4	1.8	24.5	3.4	14.5	2.2	15	1.9	2.2	1.8	33.1	6.4	6	25	9	1	·	10	8	·	·	·	–	·	·	17	8	
Rok	6.4.5	1.8	90	1.8	5.1.5	1.7	4.8	1.9	8.2.5	1.6	12.1.5	2.6	10.8.5	2.4	2.5.1.5	1.9	2.7.7	1.8	8.1.8.4	7.3.4	14.VIII	–	2.1	–	3.6	1.4.8	1.1.3	1.8	2	2	–	19	1.8	1.4.2	4.2	

Goczałkowice

$\varphi = 49°57'$ $\lambda = 18°55'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data														
	P_m	Max	Min	$P_{o,m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	1.1	4.0	2.3	2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.1	6.1	6.1
III	–	–	–	–	1.9	6.2	3.9	3.8	8.2	–	14.3	14	–	–	–	–	–	–	–	–	–	–	6.1	5.2	4.7	5.3
IV	–	–	–	–	5.4	10.7	7.7	7.9	12.8	–	23.8	28	–	–	–	–	–	–	–	–	–	–	5.2	6.2	5.9	5.8
V	–	–	–	–	8.7	12.5	9.9	10.3	14.3	–	22.5	19	–	–	–	–	–	–	–	–	–	–	7.1	6.8	6.5	6.8
VI	–	–	–	–	16.6	21.6	17.3	18.2	23.7	–	34.2	30	–	–	–	–	–	–	–	–	–	–	4.6	5.2	5.2	5.0
VII	–	–	–	–	17.3	21.9	18.1	18.8	23.6	–	34.3	8	–	–	–	–	–	–	–	–	–	–	6.2	6.0	6.9	6.4
VIII	–	–	–	–	14.5	19.8	15.9	16.5	21.0	–	27.2	11	–	–	–	–	–	–	–	–	–	–	5.1	5.5	4.5	5.0
IX	–	–	–	–	10.6	15.2	12.1	12.5	16.8	–	25.7	9	–	–	–	–	–	–	–	–	–	–	5.8	6.1	6.0	6.0
X	–	–	–	–	6.4	13.2	8.7	9.2	14.3	4.1	19.6	19	–	–	–	–	–	–	–	–	–	–	4.2	3.7	3.6	3.8
XI	–	–	–	–	3.4	6.8	4.4	4.8	8.2	–	17.5	4,5	–	–	–	–	–	–	–	–	–	–	7.4	6.7	6.8	7.0
XII	–	–	–	–	-1.6	0.6	-0.6	-0.6	2.5	–	14.5	13	–	–	–	–	–	–	–	–	–	–	7.6	6.6	6.5	6.9
Rok	–	–	–	–	–	–	–	–	–	–	34.3	8.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wodowice

$\varphi = 49°53'$ $\lambda = 19°31'$

I	–	–	–	–	-2.9	0.9	-1.9	-1.4	1.9	-5.5	9.0	6	-19.8	17	86	81	85	84	0.7	1.6	0.8	1.0	8.2	8.1	6.9	7.7
II	–	–	–	–	1.4	5.5	3.0	3.2	6.6	-0.4	12.4	6	-9.3	28	84	68	78	77	1.2	3.2	1.9	2.1	8.1	8.0	6.7	7.6
III	–	–	–	–	0.7	7.3	4.0	4.0	9.1	-1.0	17.0	27	-12.0	1	83	62	75	73	1.1	4.7	2.4	2.7	6.5	5.9	4.8	5.7
IV	–	–	–	–	5.6	11.7	7.5	8.1	13.2	3.3	25.5	30	-2.7	14	84	59	78	74	1.6	7.1	2.4	3.7	6.4	7.4	6.5	6.8
V	–	–	–	–	8.7	13.0	9.3	10.1	14.5	5.3	22.8	19	0.2	9	82	62	82	75	2.2	6.8	2.2	3.7	7.5	7.8	6.9	7.4
VI	–	–	–	–	16.9	22.6	16.6	18.2	24.2	11.0	31.7	11	4.7	27	74	51	81	69	5.3	14.3	3.8	7.8	4.9	6.4	5.2	5.5
VII	–	–	–	–	17.6	22.1	17.4	18.6	23.6	14.1	34.8	5	9.3	30	83	65	86	78	3.8	10.8	2.9	5.8	7.2	7.4	7.2	7.3
VIII	–	–	–	–	14.5	19.8	15.0	16.1	21.5	11.2	28.6	11	5.4	31	83	63	84	77	2.9	9.3	2.9	5.0	5.5	7.1	4.7	5.8
IX	–	–	–	–	10.5	15.9	11.8	12.5	17.1	8.0	28.4	9	0.0	27	85	61	81	76	2.0	7.6	2.7	4.1	6.6	7.3	4.8	6.2
X	–	–	–	–	5.5	13.8	7.5	8.6	14.5	3.3	20.4	19	-1.0	3	92	61	90	81	0.9	6.4	1.3	2.9	5.7	5.5	3.1	4.8
XI	–	–	–	–	3.2	7.3	4.2	4.7	8.3	1.1	18.7	5	-9.8	30	87	73	83	81	1.1	3.4	1.6	2.0	7.6	6.9	7.2	7.2
XII	–	–	–	–	-1.8	0.9	-0.9	-0.7	2.3	-4.4	14.9	13	-11.5	11	85	80	83	83	1.0	1.6	1.0	1.2	7.7	7.8	5.6	7.0
Rok	–	–	–	–	6.7	11.7	7.8	8.5	13.1	3.8	34.8	5.VII	-19.8	17.1	84	66	82	77	2.0	6.4	2.2	3.5	6.8	7.1	5.8	6.6

Łapanów

$\varphi = 49°52'$ $\lambda = 20°18'$

I	–	–	–	–	-2.9	0.7	-3.2	-2.2	2.5	-6.6	9.1	6	-19.4	17	86	73	87	82	0.7	1.9	0.6	1.1	7.9	7.4	6.2	7.2
II	–	–	–	–	1.2	6.4	2.5	3.2	8.0	-1.0	13.9	3	-8.3	23	85	66	81	77	1.2	3.7	1.6	2.2	6.8	6.8	7.3	7.0
III	–	–	–	–	-0.2	7.6	2.8	3.2	9.7	-1.9	18.1	14	-12.2	1	86	59	84	76	0.9	5.3	1.4	2.5	5.5	5.2	4.7	5.1
IV	–	–	–	–	4.6	12.0	6.7	7.5	13.6	2.3	26.5	30	-3.2	14	90	58	84	77	1.0	7.1	1.7	3.3	5.2	6.8	6.9	6.3
V	–	–	–	–	7.8	12.8	8.8	9.6	15.0	4.4	22.8	13	-1.3	30	85	65	84	78	1.6	6.3	1.8	3.2	6.5	8.1	7.4	7.3
VI	–	–	–	–	–	–	–	–	24.7	8.8	34.5	24	2.7	1	–	–	–	–	–	–	–	–	3.7	5.5	4.4	4.5
VII	–	–	–	–	16.0	22.2	17.4	18.2	24.6	12.7	35.8	5	6.3	4	88	63	85	79	2.3	11.2	3.2	5.6	6.3	6.7	6.9	6.6
VIII	–	–	–	–	12.6	20.4	15.3	15.9	22.8	10.4	34.2	12	3.6	24	92	61	88	80	1.2	10.3	2.2	4.6	5.0	5.4	5.8	5.4
IX	–	–	–	–	9.0	15.9	11.3	11.9	17.8	7.1	29.1	9	-1.8	27	90	62	86	79	1.2	7.4	1.9	3.5	5.8	7.1	7.4	6.8
X	–	–	–	–	4.6	11.4	6.2	7.8	15.6	1.7	23.8	19	-3.8	3	91	59	92	81	1.0	7.3	1.0	3.1	5.3	4.3	3.9	4.5
XI	–	–	–	–	1.9	7.5	3.5	4.1	9.2	0.2	20.1	4	-9.3	30	89	73	88	83	0.9	3.9	1.0	1.9	6.4	6.6	6.8	6.6
XII	–	–	–	–	-2.5	1.1	-0.9	-0.8	3.1	-4.8	12.8	13	-16.3	11	84	78	86	83	0.8	1.6	1.0	1.1	6.5	7.0	6.1	6.5
Rok	–	–	–	–	–	–	–	–	13.9	2.8	35.8	5.VII	-19.4	17.1	–	–	–	–	–	–	–	–	5.9	6.4	6.2	6.2

Żarnowa

$\varphi = 49°52'$ $\lambda = 21°49'$

I	–	–	–	–	-1.2	0.4	-1.2	-0.8	–	-4.2	–	–	-14.9	17	–	–	–	–	–	–	–	–	8.1	7.7	6.9	7.6
II	–	–	–	–	2.1	4.8	3.1	3.3	–	-0.4	–	–	-6.0	28	–	–	–	–	–	–	–	–	8.6	7.5	7.1	7.7
III	–	–	–	–	-0.3	6.3	2.8	2.9	–	-2.8	–	–	-17.1	4	–	–	–	–	–	–	–	–	6.3	5.8	4.6	5.6
IV	–	–	–	–	5.1	13.3	8.3	8.8	–	1.8	–	–	-2.9	16	–	–	–	–	–	–	–	–	6.5	6.5	5.2	6.1
V	–	–	–	–	8.2	13.5	9.4	10.1	–	4.6	–	–	-0.3	7	–	–	–	–	–	–	–	–	6.9	7.6	6.7	7.1
VI	–	–	–	–	16.0	22.9	16.9	18.2	–	10.0	–	–	3.8	7	–	–	–	–	–	–	–	–	4.1	4.9	3.8	4.3
VII	–	–	–	–	17.2	23.2	18.1	19.2	–	13.6	–	–	7.1	4	–	–	–	–	–	–	–	–	6.5	6.5	6.6	6.5
VIII	–	–	–	–	14.2	20.8	15.8	16.6	22.2	11.1	30.4	14	4.9	24	–	–	–	–	–	–	–	–	6.0	6.2	5.2	5.8
IX	–	–	–	–	10.1	16.0	11.7	12.4	17.2	7.8	26.6	9	-0.2	27	–	–	–	–	–	–	–	–	7.2	6.6	6.3	6.7
X	–	–	–	–	5.6	13.4	7.5	8.5	14.8	3.5	19.4	19	-3.6	3	–	–	–	–	–	–	–	–	6.4	5.0	3.5	5.0
XI	–	–	–	–	3.5	6.8	3.5	4.3	8.2	1.4	18.0	3	-8.8	29	–	–	–	–	–	–	–	–	6.6	6.4	5.6	6.2
XII	–	–	–	–	-1.2	0.7	-0.5	-0.4	2.0	-3.0	12.0	13	-10.2	11	–	–	–	–	–	–	–	–	6.7	7.1	7.0	6.9
Rok	–	–	–	–	8.0	11.8	8.0	8.6	–	3.6	–	–	-17.1	4.III	–	–	–	–	–	–	–	–	6.8	6.5	5.7	6.3

Goczałkowice

$H_s = 260$ m $h_w = 10$ m **1957**

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr V									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Max<0°	Min<0°	Max<10°	Max≥25°	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	V ≥ 10	V ≥ 15														
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	15	40	35	16	35	37	25	46	105	75	245	58	30	46	7	40	4	50	354	85	21	-	-	-	-	11	10	-	8	5	4	-	3	9	6			
III	2	20	14	52	175	70	15	30	35	60	165	68	20	51	7	53	11	59	693	116	15	-	3	-	-	13	11	2	10	3	6	1	7	11	5			
IV	165	32	165	29	45	22	05	40	45	24	45	30	10	36	18	28	16	28	642	240	7	-	-	-	-	12	10	1	1	1	7	4	5	9	-			
V	9	36	21	39	175	41	05	40	-	-	4	44	155	38	65	33	17	36	438	220	20	-	-	-	-	8	6	1	-	-	2	4	2	14	-			
VI	10	23	105	30	9	36	25	18	65	38	11	69	16	48	95	33	15	33	905	203	7	-	-	-	42	8	7	2	3	2	2	9	5	4	-			
VII	5	31	1	15	6	32	4	26	45	47	81	56	165	63	11	35	24	36	1519	348	16	-	-	-	42	15	15	6	2	1	5	8	3	10	-			
VIII	25	18	05	30	06	30	15	17	15	47	17	84	22	42	145	32	33	39	657	231	28	-	-	-	4	12	9	1	5	3	3	4	7	3	-			
IX	65	28	2	22	05	50	·		3	62	30	83	185	60	65	63	23	50	868	146	29	-	-	-	4	19	15	2	11	1	5	·	3	7	·			
X	15	57	7	16	3	25	1	10	5	73	155	48	15	42	8	40	37	25	641	94	20	2	·	·	·	3	3	·	2	1	18	·	11	4	·			
XI	25	78	175	48	175	39	15	30	75	63	12	84	85	76	8	08	17	47	485	75	26	-	1	-	·	8	7	·	6	1	11	·	6	16	1			
XII	45	24	5	38	3	55	1	95	6	72	215	84	24	53	6	53	22	47	347	71	8	-	9	-	·	9	6	·	6	2	5	·	5	16	5			
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54.8	16.VII	-	-	-	29	-	-	-	-	-	-	-	-	-	-	-	-	-

Wadowice

$H_s = 260$ m $h_w = 21$ m

I	·	·	6	30	7	19	4	10	14	11	275	27	135	30	1	10	20	18	307	60	6	28	9	7	·	14	9	·	·	·	5	·	1	17	23			
II	1	20	25	10	8	14	45	32	95	24	28	34	105	26	3	20	17	21	396	143	25	15	2	·	·	14	10	1	1	·	5	·	2	12	8			
III	1	20	35	44	23	37	85	16	8	15	17	40	165	28	15	20	14	26	434	87	19	18	3	2	·	14	9	·	3	1	1	1	7	10	6			
IV	55	19	4	34	5	31	10	12	13	14	175	23	205	19	25	20	12	17	582	247	7	4	·	·	1	19	10	2	·	·	5	2	3	12	·			
V	2	15	10	43	18	27	75	11	125	13	75	26	215	25	4	24	10	22	302	90	8	·	·	·	·	10	7	·	·	·	1	2	1	16	·			
VI	2	15	25	18	105	22	95	12	185	25	145	22	205	30	4	35	8	22	473	169	30	·	·	·	13	12	7	1	1	·	·	6	4	6	·			
VII	·	·	·	·	5	26	55	17	23	12	305	26	225	21	35	13	3	19	1905	643	5	·	·	·	11	20	18	5	2	1	2	8	·	15	·			
VIII	2	30	05	50	25	26	7	10	18	10	315	22	22	24	55	21	4	19	1032	320	28	·	·	·	6	17	13	2	·	·	1	2	1	5	·			
IX	1	10	·	·	4	18	5	10	145	11	36	30	19	37	05	10	10	23	1062	262	3	·	·	·	2	20	14	3	·	·	2	·	3	7	·			
X	15	23	2	15	8	12	14	11	22	10	16	23	125	23	2	25	15	13	216	113	20	1	·	·	·	7	4	1	·	·	7	·	8	4	·			
XI	·	·	6	48	23	24	8	11	14	24	195	37	65	30	4	12	9	26	481	56	28	12	1	·	·	10	5	·	2	·	6	·	3	17	·			
XII	·	·	3	20	6	28	6	10	175	22	285	33	185	22	05	30	13	22	276	64	14	24	9	4	·	12	6	·	3	·	6	·	3	16	4			
Rok	16	13	40	26	120	24	895	14	1845	16	1274	28	1204	25	32	22	135	21	7164	643	5.VII	102	24	13	33	169	112	15	12	2	41	21	36	137	41			

Łapanów

$H_s = 240$ m $h_w = 13$ m

I	35	10	65	20	25	16	7	14	85	11	12	23	185	23	275	15	7	16	331	90	6	27	8	10	·	14	10	·	-	-	-	·	1	14	23			
II	55	10	1	10	05	30	65	19	75	22	125	28	205	28	8	18	22	17	384	110	25	21	1	·	·	10	8	2	-	-	-	·	4	13	8			
III	55	15	17	19	55	27	2	12	3	18	5	40	145	32	125	23	28	17	478	107	18	19	2	2	·	11	6	2	-	-	-	1	8	11	6			
IV	95	18	5	19	2	20	2	58	2	68	2	30	14	16	195	14	34	12	592	149	11	10	·	·	·	15	12	2	-	-	-	3	4	12	·			
V	19	18	135	19	85	15	05	10	·	·	05	10	11	21	21	15	19	14	506	120	9	1	·	·	·	13	9	2	-	-	-	2	2	17	·			
VI	35	14	6	15	35	14	15	14	05	10	35	14	105	26	21	17	40	10	439	88	10	·	·	·	14	12	11	·	-	-	-	8	7	3	·			
VII	55	11	15	17	25	22	1	25	25	16	45	20	25	21	185	12	32	11	2035	756	16	·	·	·	14	17	13	5	-	-	-	9	2	14	·			
VIII	35	17	15	17	15	23	25	18	05	10	25	20	205	21	185	16	42	10	986	192	28	·	·	·	10	17	14	4	-	-	-	5	5	6	·			
IX	85	10	35	11	1	20	15	13	·	·	10	26	27	31	105	19	28	16	533	120	4	2	·	·	2	15	11	1	-	-	-	·	2	11	·			
X	105	10	3	22	35	13	1	10	3	28	6	19	17	17	10	20	39	10	222	72	20	9	·	·	·	5	4	·	-	-	-	·	10	7	·			
XI	4	26	21	20	6	26	2	22	4	46	3	37	15	38	8	26	27	20	330	145	11	13	1	·	·	8	6	1	-	-	-	1	7	16	·			
XII	85	21	·	·	1	30	1	30	4	52	16	39	155	30	14	13	33	18	240	37	14	27	7	4	·	9	7	·	-	-	-	·	6	14	-			
Rok	87	15	795	16	38	21	285	20	365	23	775	26	209	25	189	17	351	14	6985	756	16.VII	129	19	16	40	146	111	19	-	-	-	29	58	138	-			

Żarnowa

$H_s = 240$ m $h_w = 16$ m

I	9	36	15	43	·	·	6	29	27	53	21	29	115	31	15	30	2	37	227	78	6	25	-	1	-	9	7	·	1	·	·	-	2	15	7			
II	4	24	·	·	15	40	2	45	43	58	135	28	95	23	105	22	·	42	260	75	25	14	-	·	-	12	5	·	2	·	·	-	·	16	5			
III	225	20	85	43	1	40	15	30	25	41	8	36	105	34	14	31	2	32	386	159	18	20	-	3	-	9	6	1	·	·	3	-	6	9	4			
IV	245	21	3	25	2	30	5	18	17	26	11	26	8	24	195	26	·	24	323	126	11	11	-	·	-	13	7	1	·	·	2	-	6	10	·			
V	265	32	65	33	05	30	1	30	8	28	7	25	14	28	285	26	1	28	702	189	9	2	-	·	-	13	11	1	·	·	2	-	2	15	·			
VI	85	21	·	·	3	17	115	39	21	39	9	21	95	39	235	22	4	29	206	47	9	·	-	·	-	10	8	·	·	·	1	-	3	·	·			
VII	7	23	45	24	05	30	3	30	195	32	24	24	18	19	165	24	·	25	749	149	16	·	-	·	-	17	13	3	·	·	1	-	3	15	·			
VIII	12	16	1	10	1	20	25	14	215	28	175	18	21	21	145	19	2	20	429	138	10	·	·	·	7	14	11	1	·	·	6	-	3	3	·			
IX	10	21	25	20	·	·	2	35	195	42	245	27	17	24	115	14	3	26	710	169	3	1	·	·	1	11	12	2	2	·	5	-	2	10	·			
X	145	12	2	18	1	10	2	15	38	29	14	20	9	22	75	15	5	21	187	79	20	4	·	·	·	6	3	·	1	·	8	-	4	5	·			
XI	19	33	65	37	35	27	8	41	295	35	85	22	7	49	8	49	·	35	343	105	28	11	2	·	·	11	8	1	3	·	2	-	6	14	·			
XII	15	31	3	20	1	10	4	22	435	48	95	33	2	50	14	32	1	38	204	64	5	25	9	1	·	11	7	·	2	·	·	-	1	13	1			
Rok	1725	24	39	25	15	21	486	21	3128	38	1467.5	26	137	30	168	28	20	36	4726	189	9.V	113	-	5	-	139	98	10	11	·	30	-	38	125	17			

Ochaby

$\varphi = 49°51'$ $\lambda = 18°46'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.6	1.2	-1.1	-0.6	2.0	-3.7	10.6	2	-19.8	17	84	76	85	82	1.0	1.7	0.9	1.2	8.5	6.9	7.2	7.5
II	–	–	–	–	1.7	5.4	2.8	3.2	6.4	-0.5	11.3	18	-12.6	27	84	74	82	80	1.3	2.5	1.6	1.8	6.7	7.1	6.2	6.7
III	–	–	–	–	1.4	7.2	4.2	4.2	9.0	–	15.9	14	–	–	–	–	–	–	–	–	–	–	5.7	5.3	5.4	5.5
IV	–	–	–	–	5.8	11.3	7.4	8.0	12.7	3.1	24.3	30	-2.8	14	85	61	79	75	1.6	6.5	2.5	3.5	5.8	6.8	6.5	6.4
V	–	–	–	–	9.2	13.3	9.4	10.3	14.5	5.6	22.5	19	-0.2	29	80	61	80	74	2.4	6.5	2.5	3.8	7.4	7.3	6.3	7.0
VI	–	–	–	–	17.0	22.2	16.4	18.0	24.0	10.8	31.5	30	3.6	1	76	55	81	71	4.9	13.2	3.8	7.3	4.8	5.7	5.0	5.2
VII	–	–	–	–	17.9	22.2	17.1	18.6	23.6	14.6	34.6	5	10.4	4	82	65	87	78	4.1	11.0	2.7	5.9	6.7	6.6	6.9	6.7
VIII	–	–	–	–	14.6	19.7	14.9	16.0	21.5	11.3	29.0	11	6.1	31	85	64	86	78	2.6	8.5	2.5	4.5	5.9	5.8	4.7	5.5
IX	–	–	–	–	10.8	15.3	11.7	12.4	16.9	8.1	27.0	9	0.0	27	86	65	85	79	2.1	6.6	2.0	3.6	5.8	6.6	6.5	6.3
X	–	–	–	–	5.8	13.7	7.9	8.8	14.7	3.3	21.9	19	-1.7	3	90	64	86	80	1.0	6.1	1.7	2.9	6.4	5.0	4.3	5.2
XI	–	–	–	–	3.6	7.5	4.5	5.0	8.3	1.7	18.3	4	-9.5	30	86	74	84	81	1.3	3.2	1.5	2.0	7.5	7.2	7.2	7.3
XII	–	–	–	–	-1.4	1.3	-0.2	-0.1	3.0	-3.4	14.6	13	-13.3	11	84	78	82	81	1.0	1.7	1.2	1.3	8.4	7.2	6.1	7.2
Rok	–	–	–	–	7.1	11.7	7.9	8.6	13.0	–	34.6	5.VII	–	–	–	–	–	–	–	–	–	–	6.6	6.5	6.0	6.4

Porąbka

$\varphi = 49°49'$ $\lambda = 19°13'$

I	–	–	–	–	-1.3	1.6	-0.6	-0.2	2.9	-3.6	11.8	2	-17.2	17	–	–	–	–	–	–	–	–	8.0	7.6	7.0	7.5
II	–	–	–	–	2.5	5.4	3.2	3.6	7.2	0.0	12.4	19	-8.4	28	–	–	–	–	–	–	–	–	7.5	8.0	6.5	7.3
III	–	–	–	–	4.3	7.5	4.0	4.2	9.5	-0.3	17.0	14	-8.5	1	–	–	–	–	–	–	–	–	6.9	5.9	5.1	5.9
IV	–	–	–	–	5.0	11.3	7.0	7.6	13.2	3.0	25.7	30	-3.5	14	86	63	81	77	1.4	6.4	2.1	3.3	6.0	7.3	6.0	6.5
V	–	–	–	–	8.2	13.0	8.5	9.6	14.8	5.4	23.1	19	0.2	26	84	65	84	78	1.8	6.2	1.8	3.3	7.2	8.2	6.3	7.2
VI	–	–	–	–	15.6	22.6	16.3	17.7	24.7	11.4	31.9	30	5.2	27	76	55	79	70	4.3	13.1	4.3	7.2	5.1	6.6	4.0	5.2
VII	–	–	–	–	16.9	22.2	17.3	18.4	24.5	14.4	37.4	5	10.8	25	85	66	85	78	3.2	11.0	3.4	5.9	7.4	7.8	6.6	7.3
VIII	–	–	–	–	13.2	20.0	14.9	15.8	22.0	11.2	29.4	11	6.7	31	90	65	85	80	1.5	8.7	2.5	4.2	5.7	7.1	6.4	6.4
IX	–	–	–	–	10.3	15.7	11.9	12.4	17.5	8.2	27.5	8,9	1.1	26,27	85	65	81	77	2.0	6.9	2.8	3.8	6.9	7.0	7.4	7.1
X	–	–	–	–	7.3	14.5	8.9	9.9	15.7	5.0	22.7	19	-0.1	3	87	61	85	77	1.6	6.9	2.1	3.5	5.6	4.1	3.4	4.4
XI	–	–	–	–	4.4	7.8	4.7	5.4	9.0	2.0	19.0	4	-10.5	30	84	76	85	82	1.6	3.4	1.5	2.2	7.8	6.6	6.9	7.1
XII	–	–	–	–	-0.5	1.5	0.0	0.2	3.5	-3.4	14.8	13	-10.0	1	–	–	–	–	–	–	–	–	7.3	7.0	6.8	7.0
Rok	–	–	–	–	6.9	11.9	8.0	8.7	13.7	4.4	37.4	5.VII	-17.2	17.1	–	–	–	–	–	–	–	–	6.8	6.9	6.0	6.6

Myślenice

$\varphi = 49°49'$ $\lambda = 19°56'$

I	–	–	–	–	-2.1	1.4	-1.3	-0.8	2.5	-4.3	11.4	2	-18.3	17	88	79	89	85	0.7	1.6	0.6	1.0	7.5	7.0	6.1	6.9
II	–	–	–	–	2.0	6.1	2.7	3.4	7.6	-0.2	14.2	3	-8.8	23	88	70	86	81	0.9	3.2	1.2	1.8	6.5	6.7	5.9	6.4
III	–	–	–	–	0.9	7.8	3.8	4.1	9.4	-1.1	18.4	14	-11.4	4	83	63	80	75	1.3	4.8	1.9	2.7	5.8	5.4	4.3	5.2
IV	–	–	–	–	5.4	11.8	7.5	8.0	13.4	3.1	25.7	30	-3.3	15	87	63	82	77	1.4	6.5	2.2	3.4	5.2	6.5	5.9	5.9
V	–	–	–	–	8.0	12.8	9.2	9.8	14.7	5.2	22.1	19	0.8	9	83	66	85	78	1.8	6.1	1.8	3.2	6.2	7.5	7.0	6.9
VI	–	–	–	–	15.6	22.7	16.7	17.9	24.6	10.9	31.9	11.	5.1	27	–	–	–	–	–	–	–	–	2.9	5.5	4.5	4.3
VII	–	–	–	–	17.1	22.6	17.3	18.6	24.2	13.9	36.0	5	9.0	30	85	64	85	78	3.2	11.4	3.1	5.9	6.6	6.7	6.5	6.6
VIII	–	–	–	–	13.7	20.4	15.1	16.1	22.2	11.3	30.0	12	6.4	31	89	65	87	80	1.8	9.1	2.4	4.4	4.5	6.0	6.0	5.2
IX	–	–	–	–	10.7	16.6	11.5	12.6	17.8	8.1	29.1	9	0.6	26	90	67	88	82	1.4	6.7	1.7	3.3	6.2	6.4	6.5	6.4
X	–	–	–	–	6.5	14.8	8.3	9.5	16.1	4.5	25.1	19	-0.7	3	90	59	87	79	1.2	7.6	1.7	3.5	5.2	3.7	3.3	4.1
XI	–	–	–	–	3.0	7.8	3.8	4.6	8.7	0.9	21.6	1	-10.5	30	90	74	89	84	0.8	3.8	0.9	1.8	6.7	6.5	7.0	6.7
XII	–	–	–	–	-4.2	1.7	-0.4	-0.1	3.0	-3.9	14.9	13	-14.1	11	86	75	85	82	1.0	2.0	1.0	1.3	6.9	6.6	6.1	6.5
Rok	–	–	–	–	6.6	12.2	7.8	8.6	13.7	4.0	36.0	5.VII	-18.3	17.1	–	–	–	–	–	–	–	–	5.8	6.2	5.7	5.9

Aleksandrowice

$\varphi = 49°48'$ $\lambda = 19°00'$

I	973.0	984.1	956.9	1023.4	-1.7	0.8	-1.0	-0.7	2.5	-3.6	10.1	2	-17.8	17	86	79	84	83	0.9	1.6	1.0	1.2	7.9	7.8	7.1	7.5
II	964.1	981.7	940.5	1014.4	1.9	4.7	2.8	3.0	6.3	-0.1	12.1	3	-9.9	28	82	73	79	78	1.4	2.5	1.8	1.9	7.3	7.4	6.6	7.1
III	969.9	983.4	953.3	1019.3	1.6	6.3	4.0	4.0	8.1	-0.4	15.1	14	-9.6	4	78	64	73	72	1.7	4.1	2.5	2.8	6.8	6.3	4.7	5.9
IV	969.8	980.7	947.1	1018.5	5.4	10.2	7.4	7.6	11.9	3.2	24.3	30	-4.8	14	83	61	74	73	2.0	6.3	3.4	3.9	5.8	6.8	6.6	6.4
V	967.9	975.4	959.3	1016.2	8.2	11.7	8.6	9.3	13.3	5.3	21.5	19	0.1	6	82	67	79	76	2.2	5.4	2.5	3.4	7.0	7.5	7.3	7.3
VI	970.1	982.8	957.7	1017.1	16.8	21.1	16.3	17.6	23.0	11.6	29.6	30	4.6	27	70	57	73	67	5.8	11.6	5.4	7.6	4.6	5.8	4.6	5.0
VII	966.6	977.6	955.5	1013.3	17.4	21.0	16.8	18.0	22.9	14.6	34.6	5	11.6	19,22	80	66	82	76	4.6	10.0	3.9	6.2	6.5	6.8	6.7	6.7
VIII	968.8	978.1	956.0	1016.0	14.2	18.8	14.4	15.4	20.5	11.0	27.5	11	6.3	31	84	65	80	76	2.8	8.0	3.4	4.7	6.1	6.5	5.3	6.0
IX	967.6	975.6	954.9	1015.4	10.6	14.7	11.5	12.1	16.2	8.0	25.9	9	-0.5	27	84	69	82	78	2.2	5.8	2.6	3.5	6.2	7.0	6.5	6.6
X	973.0	980.1	956.8	1021.5	7.4	13.1	8.7	9.5	14.3	5.1	24.1	19	-0.5	3	84	64	88	76	1.8	5.9	2.5	3.4	5.3	5.2	3.6	4.7
XI	972.1	988.4	958.1	1021.4	4.0	6.8	4.5	5.0	7.9	2.2	18.2	5	-11.7	30	83	74	81	79	1.7	3.3	2.0	2.3	7.4	6.6	7.2	7.1
XII	967.5	986.6	936.1	1017.4	-1.5	0.5	-0.6	-0.6	2.6	-3.8	15.0	13	-14.0	1	84	82	84	83	1.1	1.4	1.2	1.2	7.3	7.3	6.7	7.1
Rok	969.2	988.4	936.1	1017.8	7.0	10.8	7.8	8.4	12.6	4.4	34.6	5.VII	-17.8	17.1	82	68	79	76	2.4	5.5	2.7	3.5	6.5	6.7	6.1	6.4

Ochaby

$H_s = 270\ m$ $h_w = 18\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0°	Min<-10	Max>25	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	≡	≈	◔	●	▣
I	1.5	1.7	3.5	6.1	3	8.3	·	·	11.5	4.0	33	3.8	10.5	3.6	1	8.5	29	2.9	23.0	5.2	6	23	10	4	·	9	7	·	4	·	3	·	2	18	20
II	3	3.0	4	1.5	·	·	2	4.2	24	4.4	22.5	3.9	9	3.4	3.5	3.3	16	3.1	43.6	10.0	21	13	1	1	·	12	9	1	2	·	4	·	3	9	9
III	2.5	1.8	15.5	3.5	6.5	3.2	3	4.5	10	4.1	15	3.9	4	3.9	3.5	3.0	31	2.4	59.1	12.6	17	-	2	-	·	14	12	1	2	1	4	1	7	11	6
IV	7.5	2.3	6.5	3.0	3.5	2.9	2.5	2.8	9.5	3.0	4.5	2.6	6.5	3.3	5.5	2.5	4.4	1.4	81.5	26.6	7	6	·	·	·	15	11	2	1	·	5	4	5	11	·
V	2.5	4.8	1.7	4.5	13.5	3.6	1.5	4.3	4.5	2.3	9	3.1	9	2.9	6	3.1	30	2.4	60.6	35.7	20	1	·	·	·	12	6	2	·	·	1	5	2	13	·
VI	3.5	2.1	6	3.3	5	2.3	4	2.9	14.5	3.1	12	3.6	6.5	3.2	5.5	3.5	33	2.0	57.5	20.0	7	·	·	·	13	9	9	1	·	·	·	4	6	4	·
VII	2	2.0	1	4.0	3.5	2.1	2	2.5	16.5	2.5	22.5	3.5	7	2.8	4.5	3.3	37	1.8	197.4	44.4	16	·	·	·	10	21	19	4	·	·	·	11	3	15	·
VIII	1	3.0	1.5	2.3	1	1.0	0.5	1.0	9.5	2.7	19.5	3.6	6	3.0	9	2.3	45	1.5	91.0	24.6	28	·	·	·	5	13	11	3	1	1	2	3	1	6	·
IX	4	2.0	2.5	2.2	·	·	·	·	15.5	3.5	28.5	4.7	9	3.6	3.5	3.7	27	2.7	89.7	16.9	29	·	·	·	2	19	15	3	1	·	3	1	2	10	·
X	2	1.0	4	1.8	·	·	1.5	1.0	10	3.2	12.5	2.8	6.5	2.8	3.5	2.3	54	1.2	47.7	9.5	20	3	·	·	·	3	2	·	·	·	12	·	6	5	·
XI	4	6.0	20.5	3.7	4.5	3.0	5.5	2.5	10	4.9	18.5	4.4	3	3.3	1	7.0	23	3.1	74.9	6.4	28	11	1	·	·	9	5	·	3	·	8	·	4	17	1
XII	3.5	2.1	11.5	2.5	·	·	2	5.5	19.5	6.7	26.5	5.4	5.5	2.8	3.5	2.0	21	3.7	43.2	9.4	8	23	8	2	·	14	9	·	4	3	6	·	2	15	10
Rok	37	2.6	93.5	3.2	42.5	2.2	24.5	2.8	145.5	3.7	224	3.8	84.5	3.2	47	3.7	387	2.4	779.2	44.4	16.VII	-	22	-	30	150	115	17	18	5	48	29	43	134	46

Porąbka

$H_s = 315\ m$ $h_w = 12\ m$

I	7.5	2.5	6.5	2.1	·	·	2.5	3.0	25.5	3.6	27.5	2.1	0.5	1.0	6	1.7	17	2.2	39.0	8.0	6	21	8	4	·	12	9	·	1	·	-	·	1	19	19
II	2	1.0	2	1.0	1	3.0	8	3.3	38	4.5	13.5	3.3	5.5	4.0	3	1.7	11	3.1	63.1	14.5	25	12	1	·	·	13	12	2	3	2	-	·	2	13	8
III	1.5	1.7	2	1.5	·	·	3	1.7	23.5	2.7	21.5	3.0	7	3.0	9	1.4	12	2.1	67.4	19.4	16	13	2	·	·	13	9	2	·	·	-	1	7	11	7?
IV	9.5	1.6	12.5	1.5	1	1.0	2.5	2.2	8.5	1.9	20	2.5	8	1.4	7	3.0	21	1.5	77.3	32.7	7	6	·	·	1	17	10	2	·	·	-	3	6	13	1
V	1.5	2.1	1.2	2.1	2.5	3.8	3	1.7	8.5	1.7	16	2.3	6.5	1.8	6.5	1.8	17	1.7	42.2	13.5	20	·	·	·	·	13	6	2	·	·	-	1	2	16	·
VI	9	2.0	4	2.0	3	1.0	8.5	2.4	17	2.8	26	2.0	9.5	2.1	7	1.6	6	2.0	56.7	17.9	21	·	·	·	15	11	7	3	1	·	-	2	5	4	·
VII	7	2.4	1	1.0	1	1.0	7	3.1	27.5	1.8	25	2.0	8.5	2.2	4	1.0	12	1.7	243.1	55.8	16	·	·	·	13	21	19	7	·	·	-	5	2	18	·
VIII	4.5	1.4	4.5	1.2	1	2.0	7	2.4	11.5	2.6	39	1.9	7.5	2.1	10	1.1	8	1.7	81.0	28.0	28	·	·	·	7	16	12	2	·	·	-	1	2	9	·
IX	7.5	1.5	0.5	3.0	·	·	8	2.5	25.5	2.6	30.5	2.3	9	1.2	5	2.2	4	2.1	126.4	31.5	5	·	·	·	2	18	13	4	·	·	-	·	2	15	·
X	5	1.8	·	·	·	·	3.5	2.7	30	2.5	30.5	2.3	5	1.6	4	1.0	16	1.9	18.7	9.0	20	1	·	·	·	7	4	·	·	·	-	·	10	5	·
XI	14.5	2.6	5	1.8	·	·	6	3.3	25	2.2	17.5	2.5	0.5	2.0	4.5	3.0	17	2.0	34.6	11.5	28	11	1	1	·	11	5	1	·	·	-	·	6	19	1
XII	6.5	1.3	5.5	1.5	1.5	3.7	8	4.6	31	4.5	15	2.8	3.5	2.4	2	2.0	20	2.7	25.3	5.1	4	23	7	·	·	14	9	·	1	1	-	·	4	17	6
Rok	10.3	1.8	55.5	1.6	11	1.3	73	2.7	271.5	2.8	282	2.4	71	1.8	68	1.8	160	2.1	871.8	55.8	16.VII	87	19	5	38	166	115	25	6	3	-	13	49	159	42?

Myślenice

$H_s = 295\ m$ $h_w = 16\ m$

I	4	2.9	6	2.8	·	·	·	·	13	3.8	36.5	2.6	9.5	2.3	1	4.0	23	2.1	32.4	7.6	6	25	10	5	·	12	9	·	1	·	-	·	2	14	22
II	·	·	·	·	·	·	1	2.0	14	3.9	32.5	4.6	11.5	4.1	·	·	2.5	3.0	31.5	10.7	21	10	2	·	·	10	6	2	4	2	-	·	5	12	8
III	12.5	3.0	9	3.9	2	2.0	1	1.0	8.5	5.2	34.5	4.0	9	4.3	1.5	1.7	1.5	3.2	55.2	15.6	16	13	3	1	·	11	9	1	1	1	-	1	9	10	8
IV	7	2.1	8	3.1	0.5	1.0	·	·	5.5	2.2	28.5	2.9	10	3.2	1.5	1.3	2.9	1.9	71.0	26.0	7	6	·	·	1	18	11	2	·	·	-	1	7	11	1
V	13.5	2.3	16.5	2.5	3	2.3	·	·	3.5	4.3	16	2.2	11.5	2.2	6	1.8	23	1.8	58.6	13.4	14	·	·	·	·	14	10	2	·	·	-	2	3	16	·
VI	6	1.8	4	2.5	3	2.3	·	·	6.5	3.8	30.5	3.3	16.5	2.5	8.5	1.8	15	2.3	36.0	9.2	5	·	·	·	13	11	7	·	1	1	-	7	8	4	·
VII	2	2.0	1.5	3.0	2	1.5	1	1.0	3.5	2.4	36.5	2.4	13	2.4	0.5	3.0	33	1.5	185.8	33.8	5	·	·	·	12	20	18	6	·	·	-	6	3	12	·
VIII	1.5	2.0	4	2.8	·	·	·	·	3	4.7	27	2.9	21.5	2.4	4	2.1	32	1.8	138.4	51.7	16	·	·	·	6	16	11	4	2	1	-	4	3	6	·
IX	3	2.0	2	1.5	1	2.0	·	·	4	3.4	43	3.1	5	5.6	2	3.0	30	2.1	89.3	11.3	3	·	·	·	2	17	13	3	2	2	-	·	4	12	·
X	2	1.5	4	1.8	·	·	0.5	2.0	3.5	4.4	38	3.3	14	3.8	·	·	31	2.2	24.1	8.4	20	1	·	·	1	5	4	·	1	1	-	·	11	5	·
XI	8.5	3.3	12.5	4.0	·	·	1	4.0	5	2.6	33.5	3.5	9	3.9	1.5	1.5	19	2.7	42.9	19.1	11	11	2	1	·	8	6	1	·	·	-	·	5	17	1
XII	3.5	3.0	7	2.3	·	·	2	1.0	6.5	5.9	37.5	4.5	4	3.5	2.5	2.2	30	2.8	26.5	6.2	14	28	9	2	·	11	8	·	3	2	-	·	6	13	7
Rok	6.3.5	2.2	74.5	2.5	11.5	0.9	6.5	0.7	76.5	3.9	394	3.3	134.5	3.4	29	1.8	305	2.3	782.7	51.7	16.VIII	94	26	9	35	153	112	21	15	10	-	21	66	132	47

Aleksandrowice

$H_s = 398\ m$ $H_b = 403.4\ m$ $h_w = 20\ m$

I	0.5	10.0	2	9.5	5.5	6.4	1.5	2.0	8	5.9	14	6.9	23	4.1	15	6.3	37	3.3	21.0	5.9	11	24	9	3	·	11	7	·	8	1	2	·	1	18	21
II	0.5	2.0	·	·	·	·	6	2.9	15.5	3.6	26.5	7.4	12	4.4	5.5	3.0	18	5.1	52.0	15.1	21	13	2	·	·	15	11	2	14	7	2	·	1	10	9
III	1.5	3.7	2.5	3.4	17.5	3.8	9.5	2.8	6.5	3.5	8.5	7.3	20	6.0	4	2.6	23	3.5	94.1	25.3	17	14	3	·	·	16	13	3	10	4	2	1	7	11	9
IV	3	2.5	6.5	2.5	3	3.2	10.5	3.7	5.5	6.0	7.5	3.3	9.6	2.8	9.5	2.8	35	2.0	72.5	29.3	7	7	·	·	·	17	12	2	3	2	8	1	5	12	3
V	2.5	2.6	14.6	4.6	2.2	5.3	8.5	3.6	5	2.8	10	3.8	14.5	4.3	10	3.5	6	4.0	52.5	20.0	20	·	·	·	·	15	6	1	1	·	1	2	2	15	·
VI	6	2.2	6	3.5	14.5	3.5	8	3.8	9	7.5	17	5.7	17	4.7	10.5	3.6	2	4.4	34.0	8.4	7	·	·	·	9	9	7	·	5	1	·	6	7	4	·
VII	5	2.5	6.5	3.4	9.5	3.1	7	4.6	6.5	4.7	20	5.7	22	4.3	12.5	3.6	4	4.1	229.6	56.0	15	·	·	·	8	21	20	6	3	·	1	8	2	13	·
VIII	4.6	2.0	1	3.0	8	2.9	9	2.6	13.5	5.4	13	4.8	22	4.1	20	3.6	2	3.8	103.1	28.0	28	·	·	·	4	15	13	3	5	·	1	2	2	7	·
IX	4.6	3.2	2.5	3.6	6.5	3.1	9.5	3.4	8.5	6.5	30.5	6.3	23	5.7	4	4.0	1	5.2	117.6	26.6	29	1	·	·	2	18	15	4	9	·	·	·	2	9	·
X	6.5	1.8	4.5	2.3	7.5	2.5	18.5	2.9	13	5.0	15.5	6.3	16	4.3	9.5	3.6	2	3.9	19.3	10.6	20	1	·	·	·	5	2	1	5	2	4	·	8	5	·
XI	4.5	6.2	10	4.8	16	5.3	16	4.0	10.5	6.4	8.5	5.4	16	3.8	5.5	2.9	3	5.0	26.3	11.2	28	11	1	1	·	8	5	1	7	1	7	·	5	17	1
XII	4.5	1.8	4	4.9	9	3.5	10	3.4	9.5	9.6	16.5	8.2	19	4.7	10.5	2.3	10	4.7	36.9	11.5	8	25	10	1	·	14	9	1	9	7	6	·	3	17	9
Rok	4.3.5	3.4	60	3.8	11.9	3.6	11.4	3.3	11.1	6.1	18.7.5	5.9	21.4	4.6	10.3	3.5	14.3	4.1	852.9	56.0	16.VII	96	25	5	23	184	120	24	79	25	34	20	45	138	52

Leskowiec

$\varphi = 49°48'$ $\lambda = 19°27'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o,m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.6	-1.1	-1.9	-1.9	0.9	-4.5	7.3	2	-16.4	17	–	–	–	–	–	–	–	–	7.2	7.7	6.4	7.1
II	–	–	–	–	-0.3	2.2	0.6	0.8	3.6	-4.8	13.1	5	-8.6	28	–	–	–	–	–	–	–	–	6.6	7.4	6.6	6.9
III	–	–	–	–	0.5	3.9	1.5	1.8	5.4	-4.9	13.9	14	-10.2	5	–	–	–	–	–	–	–	–	6.0	5.4	5.8	5.7
IV	–	–	–	–	4.7	7.2	5.1	5.5	9.0	2.1	21.4	30	-6.0	14	–	–	–	–	–	–	–	–	5.7	6.7	7.2	6.5
V	–	–	–	–	5.9	8.2	6.3	6.7	10.5	–	18.6	19	–	–	–	–	–	–	–	–	–	–	6.8	7.8	7.3	7.2
VI	–	–	–	–	14.2	17.8	15.2	15.6	20.1	10.5	26.9	11	6.0	26	–	–	–	–	–	–	–	–	4.5	5.8	4.5	4.9
VII	–	–	–	–	14.8	17.4	14.9	15.5	19.5	12.0	30.7	8	7.8	16,28	–	–	–	–	–	–	–	–	6.9	7.4	7.3	7.2
VIII	–	–	–	–	12.5	15.6	12.8	13.4	17.3	9.6	24.9	12	5.5	23	–	–	–	–	–	–	–	–	5.7	6.8	5.7	6.1
IX	–	–	–	–	8.2	11.5	9.0	9.4	13.0	6.2	23.3	9	-0.3	27	–	–	–	–	–	–	–	–	6.1	6.7	7.2	6.7
X	–	–	–	–	6.8	10.4	7.4	8.0	11.6	4.8	19.7	19	-0.5	2	–	–	–	–	–	–	–	–	5.0	4.4	3.2	4.2
XI	–	–	–	–	1.9	3.6	2.1	2.4	5.3	0.1	14.9	1	-16.1	30	–	–	–	–	–	–	–	–	6.9	6.5	6.7	6.7
XII	–	–	–	–	-2.4	-1.1	-2.5	-2.1	0.5	-5.8	9.4	13,14	-13.7	1	–	–	–	–	–	–	–	–	7.4	6.9	6.6	7.0
Rok	–	–	–	–	5.4	8.0	5.9	6.3	9.7	–	30.7	8.VII	-16.4	17.1	–	–	–	–	–	–	–	–	6.2	6.6	6.2	6.3

Dynów

$\varphi = 49°48'$ $\lambda = 22°14'$

I	–	–	–	–	-2.1	-0.2	-1.6	-1.4	1.0	-4.6	5.5	2	-14.0	17	–	–	–	–	–	–	–	–	8.6	8.0	7.6	8.0
II	–	–	–	–	1.8	4.4	2.5	2.8	5.7	-0.4	13.4	19	-6.9	28	–	–	–	–	–	–	–	–	8.7	7.5	6.9	7.7
III	–	–	–	–	-0.7	6.1	2.0	2.4	7.4	-3.0	16.4	21	-19.0	4	–	–	–	–	–	–	–	–	6.3	5.2	3.8	5.1
IV	–	–	–	–	4.7	12.9	7.9	8.4	14.0	1.8	25.1	30	-3.9	16	87	51	76	71	1.2	8.5	2.7	4.1	6.4	6.7	4.1	5.7
V	–	–	–	–	8.1	12.8	8.9	9.7	14.3	4.6	22.6	14	-0.5	5,7	89	68	85	81	1.3	6.1	1.8	3.1	7.8	8.0	6.2	7.3
VI	–	–	–	–	15.4	22.6	16.2	17.6	23.9	10.0	32.4	12	4.3	28	82	54	81	72	3.4	13.1	3.7	6.7	4.3	4.9	3.6	4.3
VII	–	–	–	–	16.7	23.0	17.6	18.7	24.5	12.8	32.8	8	6.0	4	88	61	85	78	2.5	12.1	3.4	6.0	6.9	6.8	7.1	6.9
VIII	–	–	–	–	13.9	20.9	15.2	16.3	21.8	10.8	30.9	14	5.4	24	90	61	86	79	1.6	10.3	2.5	4.3	7.1	6.3	4.3	5.9
IX	–	–	–	–	9.9	16.0	11.4	12.2	17.0	7.3	26.1	9	-0.9	27	91	69	88	83	1.1	5.9	1.5	2.8	8.5	7.4	6.6	7.5
X	–	–	–	–	5.5	13.6	7.4	8.5	14.0	2.6	19.8	19	-2.9	3	91	62	85	79	1.0	6.4	1.8	3.1	7.7	5.0	3.9	5.5
XI	–	–	–	–	2.1	6.5	2.9	3.6	7.4	0.0	17.0	14	-10.5	30	90	78	88	85	0.8	2.6	1.0	1.5	7.3	6.9	6.0	6.7
XII	–	–	–	–	-1.6	0.4	-0.6	-0.6	1.7	-4.0	13.3	14	-11.0	1	–	–	–	–	–	–	–	–	6.9	6.6	6.6	6.7
Rok	–	–	–	–	6.1	11.6	7.5	8.2	12.7	3.2	32.8	8.VII	-19.0	4.III	–	–	–	–	–	–	–	–	7.2	6.5	5.6	6.5

Przemyśl

$\varphi = 49°48'$ $\lambda = 22°46'$

I	992.9	1003.5	978.5	1023.3	-2.5	-0.1	-1.6	-1.4	0.8	-4.8	5.7	10	-13.2	17	74	66	74	71	1.3	2.2	1.4	1.6	8.4	8.0	7.1	7.8
II	984.4	1000.2	963.3	1013.9	2.4	5.3	2.7	3.5	6.8	0.3	14.4	19	-6.3	28	74	62	74	70	2.1	3.8	2.1	2.7	7.6	7.9	6.4	7.3
III	990.2	1004.3	970.7	1020.0	-0.2	5.6	2.4	2.6	7.2	-2.4	17.4	21	-15.1	4	69	51	63	61	2.1	5.3	2.9	3.4	6.3	6.2	4.5	5.7
IV	988.7	999.6	965.2	1017.7	5.1	13.1	9.1	9.1	14.2	2.7	25.7	30	-2.4	16	79	48	65	64	2.0	9.2	4.4	5.2	6.1	6.2	4.2	5.5
V	986.2	994.4	974.4	1015.0	8.5	12.9	10.1	10.4	14.4	5.7	22.7	18	0.2	7	84	63	78	75	1.8	6.6	2.9	3.8	7.6	8.1	6.7	7.6
VI	988.9	1001.0	978.0	1017.1	16.4	22.9	17.9	18.8	24.4	11.6	34.5	12	4.5	7	81	54	75	70	3.8	13.4	5.2	7.5	4.7	5.0	4.0	4.6
VII	984.7	994.4	975.3	1012.7	17.4	23.0	18.5	19.4	24.6	13.9	33.0	5	8.3	4	88	65	83	79	2.4	10.9	3.9	5.7	6.1	5.7	6.4	6.1
VIII	986.8	995.8	975.0	1015.1	14.4	21.0	16.0	16.8	22.3	11.9	32.5	14	6.0	31	92	65	87	81	1.4	9.3	2.5	4.4	6.0	6.3	3.9	5.4
IX	986.1	995.6	974.0	1014.7	10.2	16.7	12.3	12.8	17.5	8.0	27.6	9	0.8	27	92	65	87	81	1.1	7.2	1.9	3.4	6.7	7.1	5.9	6.6
X	992.6	1001.9	977.0	1021.7	5.5	13.8	8.2	8.9	14.7	3.4	22.3	19	-3.2	3	92	66	88	82	1.0	6.0	1.5	2.8	5.3	4.8	3.6	4.6
XI	992.3	1010.8	973.8	1022.1	2.0	6.3	3.2	3.7	7.2	0.3	19.1	4	-10.0	30	91	77	88	85	0.6	2.5	0.8	1.3	7.4	6.6	5.9	6.6
XII	987.2	1006.4	954.0	1012.5	-1.8	1.0	-0.7	-0.5	2.1	-3.9	11.6	13	-10.2	1	81	73	79	78	1.1	1.9	1.3	1.4	6.4	7.2	5.8	6.5
Rok	988.6	1010.8	954.0	1017.5	6.5	11.8	8.2	8.7	13.0	3.9	33.0	5.VII	-15.1	4.III	83	63	78	75	1.7	6.5	2.6	3.6	6.6	6.5	5.4	6.2

Międzybrodzie

$\varphi = 49°47'$ $\lambda = 19°12'$

I	–	–	–	–	-1.6	1.0	-0.2	-0.2	2.7	-3.2	11.1	2	-17.9	17	–	–	–	–	–	–	–	–	8.2	7.5	7.5	7.8
II	–	–	–	–	2.4	4.8	3.2	3.4	6.2	0.1	11.4	19	-7.5	24	–	–	–	–	–	–	–	–	7.1	7.6	6.7	7.1
III	–	–	–	–	1.1	6.7	3.7	3.8	8.6	-0.4	16.4	14	-9.0	4	–	–	–	–	–	–	–	–	8.5	6.0	6.0	6.1
IV	–	–	–	–	4.7	10.5	7.0	7.3	12.2	2.7	24.2	30	-3.4	14	–	–	–	–	–	–	–	–	6.0	6.8	6.6	6.5
V	–	–	–	–	7.9	12.0	9.1	9.6	13.7	5.6	22.0	19	1.1	30	–	–	–	–	–	–	–	–	7.0	7.9	6.9	7.3
VI	–	–	–	–	15.6	21.6	16.3	17.4	23.1	11.2	30.8	11	4.2	27	80	57	80	72	3.8	11.7	4.0	6.5	4.9	5.4	4.8	5.0
VII	–	–	–	–	17.0	21.3	17.3	18.2	23.0	14.0	34.3	5	9.4	4	86	66	85	79	2.9	9.9	3.4	5.4	7.0	7.3	6.2	6.8
VIII	–	–	–	–	13.7	19.6	14.7	15.7	20.9	11.1	28.6	11	6.4	31	89	63	83	78	1.8	8.9	3.0	4.6	5.9	6.5	5.7	6.0
IX	–	–	–	–	10.2	15.2	11.5	12.1	16.5	8.0	25.6	9	0.6	27	84	63	81	76	2.1	7.0	2.6	3.9	7.2	7.1	6.6	7.0
X	–	–	–	–	7.1	13.4	8.5	9.4	14.8	–	22.5	19	–	–	86	63	85	78	1.6	6.1	1.9	3.2	6.6	5.0	4.3	5.3
XI	–	–	–	–	4.0	7.5	4.7	5.2	8.7	–	17.5	4	–	–	–	–	–	–	–	–	–	–	7.6	6.3	7.2	7.0
XII	–	–	–	–	-0.7	4.2	0.2	0.2	3.2	–	14.1	13	–	–	–	–	–	–	–	–	–	–	7.4	6.6	7.0	7.0
Rok	–	–	–	–	6.8	11.2	8.0	8.5	12.8	–	34.3	5.VII	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.3	6.6

Leskowiec — $H_s = 870\ m$ — $h_w = 16\ m$ — 1957

MIESIĄC	ROZKŁAD WIATRU [%D, %nD]																		OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr										
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max>25°	0.1 ÷ 1.0	1.0 ÷ 10.0	>10.0	10 ÷ 15	>15								
I	3	2.5	9	5.2	3	3.3	6.5	3.9	19.5	5.7	20	4.0	13.5	5.6	10.5	6.8	8	4.7	49.8	9.0	6	29	11	4	·	15	8	·	3	2	13	·	3	14	30				
II	2.5	4.6	·	·	2.5	3.4	10	4.4	25.5	9.5	12.5	5.2	12.5	5.1	11.5	8.5	7	6.0	66.6	19.5	21	20	7	·	·	16	13	2	9	5	11	·	3	11	13				
III	5	8.8	3	4.3	5.5	6.5	19.5	4.4	19	5.8	10	4.9	13.5	4.3	8.5	6.5	9	4.8	68.0	14.8	16	16	7	2	·	16	11	2	4	3	12	1	6	11	15				
IV	4.5	4.3	8	2.8	11	3.9	8	3.4	16.5	6.6	5.5	4.3	5.5	5.8	2.8	4.3	3	4.4	84.3	26.5	7	12	1	·	·	19	13	2	3	1	13	3	5	14	11				
V	4.5	3.9	5.5	5.5	20	5.0	8.5	3.7	6	4.3	1	3.0	8	5.6	3.2.5	5.1	7	4.5	72.1	19.4	8	–	1	·	·	15	11	2	1	·	14	2	1	15	5				
VI	1	3.0	3	4.3	6.5	4.5	7.5	5.7	17.5	7.8	7	3.6	16	4.6	3.1.5	4.8	·	5.3	60.8	19.4	5	·	·	·	6	14	12	1	3	1	6	9	5	2	·				
VII	4	2.6	0.5	4.0	4	5.5	7.5	4.4	20	4.4	11	3.4	20.5	5.6	23.5	4.8	2	4.5	287.6	69.8	16	·	·	·	6	25	23	8	2	·	14	10	2	16	·				
VIII	1	10.0	2	3.0	·	·	4.5	3.3	16.5	6.6	6.5	3.3	2.2	3.5	33.5	4.5	7	4.2	132.4	33.5	28	·	·	·	·	17	14	4	3	2	13	2	2	7	·				
IX	2.5	6.2	3	6.7	3	1.7	7	5.0	24.5	6.2	7	5.3	28.5	7.0	12.5	5.8	2	5.9	177.8	36.0	4	1	·	·	·	21	18	4	11	8	9	·	3	13	·				
X	0.5	1.0	1	3.0	·	·	6	4.2	33	5.9	8.5	3.2	22	3.8	18	4.4	4	4.4	34.8	14.8	20	1	·	·	·	12	6	1	5	3	10	·	9	3	·				
XI	2	7.8	7	5.9	7	9.1	12.5	4.4	25	6.3	11.5	2.9	7	8.3	6	5.8	12	5.1	44.3	8.5	29	17	8	1	·	15	8	·	8	6	13	·	7	17	5				
XII	4	2.5	6	2.8	7.5	5.8	3.5	6.4	28	8.7	11.5	8.5	13.5	7.0	9	5.1	10	6.2	43.0	9.2	4	29	18	4	·	20	10	·	9	7	14	·	6	10	25				
Rok	34.5	4.8	4.8	4.0	70	4.1	101	4.4	25.1	6.5	11.2	4.3	18.2.5	5.6	22.5	6.4	7.1	5.0	112.5	69.8	16.VII	–	55	11	18	205	147	26	61	38	142	27	52	139	102				

Dynów — $H_s = 270\ m$ — $h_w = 17{,}5\ m$

I	8.5	1.7	2.5	4.4	1.5	5.0	·	·	3.5	4.6	19.5	4.7	11.5	2.7	10.5	3.0	4	3.7	11.5	4.6	6	27	10	4	·	12	4	·	2	·	·	·	1	20	21				
II	4.5	2.2	·	·	·	·	·	·	4.8	5.2	13.5	4.8	6.5	2.3	6.5	2.4	5	4.2	24.7	5.0	25	14	1	·	·	16	9	·	6	1	1	·	3	17	5				
III	12.5	3.1	6.5	4.9	6	4.1	·	·	2.5	3.6	1.4	4.1	11	3.9	9	2.6	9	3.3	38.1	13.4	18	21	4	2	·	7	6	2	5	·	2	1	8	7	8				
IV	18.5	2.2	3	2.0	2	2.0	·	·	1.6	2.0	9	2.2	7	1.9	15.5	1.9	19	1.6	33.2	17.0	11	13	·	·	1	9	7	1	·	·	3	1	7	9	·				
V	2.6	2.1	7.5	3.5	1	5.0	0.5	1.0	11.5	1.9	5	1.9	9	2.0	17.5	1.8	15	1.8	84.6	19.8	6	2	·	·	·	14	11	3	·	·	2	2	3	17	·				
VI	7.5	2.1	1.5	1.0	2	2.5	·	·	2.9	2.9	12	2.8	12.5	2.3	4.5	2.3	21	2.0	59.1	33.1	12	·	·	·	12	8	7	2	·	·	1	5	9	4	·				
VII	9	1.4	1.5	1.7	3	1.0	0.5	1.0	2.4	2.5	16.5	2.5	20.5	1.8	8	1.7	10	1.8	68.5	12.0	16	·	·	·	12	19	16	1	·	·	·	4	3	16	·				
VIII	8.5	1.8	0.5	3.0	1	3.0	1	2.0	1.8	3.0	17.5	2.6	10.5	2.3	16	2.4	20	2.0	77.6	23.5	29	·	·	·	6	17	12	3	1	·	7	·	3	9	·				
IX	6	1.8	·	·	1.5	1.7	2.5	1.4	20	3.0	19	3.5	20	3.0	8	2.2	13	2.5	86.3	18.5	3	1	·	·	1	21	12	2	1	·	7	2	1	14	·				
X	8.5	1.1	1	3.0	0.5	1.0	0.5	1.0	1.6	4.6	16.5	4.6	20.5	2.0	10.5	1.2	19	2.3	19.9	8.6	20	8	·	·	·	13	4	·	2	·	12	·	3	6	·				
XI	11.5	3.6	8	2.5	9	2.7	·	·	13.5	4.7	11.5	4.7	11.5	4.5	6	5.4	19	3.2	25.8	13.6	28	13	2	1	·	11	7	1	4	1	3	·	4	15	·				
XII	1.5	3.1	2.5	3.4	1.5	2.7	0.5	1.0	3.1	5.1	25.5	5.3	5	4.1	11	3.3	1	4.4	17.7	4.2	5	28	10	1	·	10	6	·	6	2	·	·	5	14	2				
Rok	13.6	2.2	3.4.5	2.4	29	2.6	5.5	0.6	2.8.7	3.6	17.9.5	3.6	14.5.5	2.7	12.3	2.5	15.5	2.7	54.7.0	33.1	12.VII	127	27	8	32	157	101	15	27	4	38	15	50	150	36				

Przemyśl — $H_s = 238\ m$ — $H_b = 238{,}9\ m$ — $h_w = 20\ m$

I	2	2.5	9.5	3.8	2	7.8	7.5	2.3	1	1.0	4.5	5.1	38.5	4.1	15	3.2	13	3.3	14.7	2.7	6	26	9	3	·	11	7	·	2	·	3	·	1	17	27				
II	0.5	7.0	1.5	3.0	2	4.0	3.5	2.7	12	4.0	15.5	6.5	27	4.2	13	4.0	9	3.8	19.5	2.7	25	10	1	·	·	17	8	·	2	·	2	·	2	13	7				
III	7	4.6	8	4.1	13.5	6.5	2.5	7.0	5	2.6	3.5	2.9	31.5	3.4	13	4.4	9	3.9	32.3	11.0	18	20	5	2	·	8	7	1	3	2	2	1	7	8	6				
IV	10.5	3.4	14.5	2.7	11	3.0	1.5	3.7	2.6	3.0	3	2.0	9.5	2.0	17.5	3.5	20	2.3	35.9	22.4	11	10	·	·	2	12	6	1	·	·	2	3	5	10	·				
V	8	4.0	20	3.8	13.5	3.4	2	3.5	1	3.0	2	1.5	20	3.3	19.5	3.5	7	3.2	86.1	27.8	6	·	·	·	·	14	12	3	·	·	4	1	1	17	·				
VI	10	3.8	3	2.7	5	3.4	3	2.3	8	3.2	7	3.0	22.5	3.2	17.5	3.0	14	2.7	78.1	26.7	8	·	·	·	15	9	8	3	·	·	1	6	6	·	·				
VII	4	2.4	7.5	1.7	8.5	2.3	1.5	2.3	4	2.6	15.5	3.4	32	2.8	11	3.2	9	2.5	99.4	19.5	14	·	·	·	13	18	15	3	1	1	3	9	3	10	·				
VIII	6.5	1.6	7.5	2.2	5	1.1	·	·	3	4.0	10.5	1.8	27	2.9	21.5	3.3	12	2.3	45.4	11.5	29	·	·	·	7	12	9	1	·	·	6	5	2	7	·				
IX	5.5	3.2	3.5	1.0	1	2.0	2	1.0	0.5	7.0	2.5	1.2	33	3.6	8.5	3.4	11	2.8	70.8	13.9	3	·	·	·	2	12	11	3	1	·	9	1	2	8	·				
X	3.5	2.0	7	2.6	1.5	2.0	3.5	1.3	2	1.5	17	3.0	25	2.8	9.5	2.4	24	2.0	15.6	8.0	20	5	·	·	·	5	4	·	·	·	10	·	6	5	·				
XI	3	3.7	11.5	3.7	16.5	3.9	10.5	2.4	1	3.0	7	2.3	17.5	5.9	5	6.8	18	3.3	27.4	16.5	28	12	2	·	·	8	5	1	3	·	5	·	4	15	1				
XII	8	3.4	4	5.5	7.5	2.9	1	1.0	4.5	2.9	13	5.4	26	3.5	9	5.7	20	3.2	16.2	4.3	5	28	9	1	·	10	5	·	·	·	1	·	4	12	7				
Rok	68.5	3.5	97.5	3.1	87	3.5	38.5	2.5	44.5	3.1	123.6	3.3	309.5	3.5	160	3.8	166	2.9	541.4	27.8	6.V	111	26	6	39	136	97	16	12	3	48	26	45	122	48				

Międzybrodzie — $H_s = 320\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	225?	–	–	24	6	2	·	–	–	–	–	–	–	·	·	18	20				
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	403?	–	–	12	1	·	·	–	–	–	–	–	–	·	2	11	9?				
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57.2	14.4	16	15	3	·	·	13	9	2	–	–	–	1	4	11	6				
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44.7	14.4	11	6	·	·	·	18	9	2	–	–	–	1	3	13	·				
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	149?	57?	20	·	·	·	·	10?	4?	·	–	–	2	1	1	13	·				
VI	–	–	·	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.2	8.1	7	·	·	·	9	9	5	·	–	–	1	4	4	6	·				
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	191.8	58.5	16	·	·	·	9	21	17	4	–	–	1	8	·	11	·				
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	69.3	28.0	28	·	·	·	4	13	12	1	–	–	4	2	1	2	·				
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	97.0	28.3	5	·	·	·	2	16	11	4	–	–	2	·	1	8	·				
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	16.5	7.2	20	–	·	–	–	4	3	·	–	–	9	·	3	6	·				
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27.3	12.2	28	–	·	–	·	11	8	1	–	–	8	·	5	17	1				
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.1	5.5	14	–	7	–	·	14	9	·	–	–	4	·	·	16	6?				
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	635.6?	58.5	16.VII	–	17	–	24	–	–	–	–	–	–	17	24	131	42?				

Ciężkowice

$\varphi = 49°47'$ $\lambda = 20°58'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-2.5	-0.4	-2.2	-1.8	1.7	-4.6	6.3	9.26	-15.4	17	78	68	82	76	1.2	2.1	0.9	1.4	7.6	7.7	6.4	7.2
II	-	-	-	-	1.3	4.9	2.3	2.7	6.7	-0.3	11.5	6	-5.6	24	77	63	76	72	1.6	3.6	1.9	2.4	7.9	7.4	6.8	7.4
III	-	-	-	-	-0.4	6.7	2.5	2.8	8.9	-1.8	18.5	14	-11.9	4	75	63	73	67	1.7	5.5	2.3	3.2	6.4	5.4	4.4	5.4
IV	-	-	-	-	3.7	12.0	7.7	7.8	13.7	2.6	25.5	30	-1.8	14,16	85	54	74	71	1.2	7.8	3.0	4.0	6.8	7.5	6.4	6.9
V	-	-	-	-	6.3	12.8	9.3	9.4	15.0	4.8	23.5	19	-0.3	30	89	65	82	78	1.1	6.7	2.1	3.3	6.8	8.0	7.1	7.3
VI	-	-	-	-	14.4	22.5	16.8	17.6	24.7	10.4	31.4	12	4.3	28	86	54	78	73	2.5	13.2	4.6	6.8	4.9	6.7	4.3	5.3
VII	-	-	-	-	15.9	22.7	17.8	18.6	24.8	13.6	36.2	5	7.6	4	90	63	85	79	1.9	11.6	3.3	5.6	6.8	7.3	6.6	6.9
VIII	-	-	-	-	12.7	20.6	15.5	16.1	22.8	10.7	30.7	12	3.9	24	93	61	84	79	1.2	10.3	3.0	4.8	5.3	6.4	4.9	5.5
IX	-	-	-	-	9.2	16.3	11.4	12.1	17.9	7.5	28.0	8	-1.0	27	92	63	87	81	1.0	7.4	1.8	3.4	6.4	7.5	7.1	7.0
X	-	-	-	-	4.6	14.0	3.7	6.5	15.4	2.9	20.6	19	-2.8	3	93	61	88	81	0.8	6.7	1.5	3.0	7.0	5.3	3.1	5.1
XI	-	-	-	-	3.4	7.2	4.1	4.7	8.4	1.8	19.1	4	-10.0	30	88	74	84	82	1.0	3.4	1.4	1.9	6.6	6.5	6.5	6.5
XII	-	-	-	-	-1.5	0.9	-0.9	-0.6	2.4	-3.9	11.0	13	-10.4	11	88	78	86	84	0.7	1.4	0.9	1.0	7.4	7.6	6.8	7.3
Rok	-	-	-	-	5.6	11.7	7.3	8.0	13.5	3.6	36.2	5.VII	-15.4	17.1	86	63	82	77	1.3	6.6	2.2	3.4	6.7	6.9	5.9	6.5

Rożnów

$\varphi = 49°46'$ $\lambda = 20°41'$

I	-	-	-	-	-2.1	0.8	-1.3	-1.0	2.0	-3.4	8.7	6	-12.5	17	-	-	-	-	-	-	-	-	8.2	7.3	6.4	7.3
II	-	-	-	-	1.8	5.3	3.0	3.3	6.5	0.6	12.0	6	-4.7	28	-	-	-	-	-	-	-	-	7.9	6.8	7.1	7.3
III	-	-	-	-	0.8	7.2	3.4	3.7	8.9	-0.7	18.1	14	-9.0	4	-	-	-	-	-	-	-	-	6.0	5.1	4.1	5.1
IV	-	-	-	-	5.4	11.6	7.9	8.2	13.5	3.8	25.2	30	-1.8	14	-	-	-	-	-	-	-	-	6.4	7.0	6.4	6.6
V	-	-	-	-	8.0	12.2	9.6	9.8	14.3	6.0	22.1	17	0.7	7,9	-	-	-	-	-	-	-	-	7.0	7.6	6.8	7.1
VI	-	-	-	-	15.9	22.0	17.7	18.5	24.4	12.2	30.8	11	4.1	14	-	-	-	-	-	-	-	-	4.5	6.4	4.4	5.1
VII	-	-	-	-	17.3	21.6	18.3	18.9	23.9	15.1	36.2	5	10.5	30	-	-	-	-	-	-	-	-	6.7	7.1	6.8	6.9
VIII	-	-	-	-	14.6	20.0	16.5	16.9	21.9	12.7	30.1	12	6.6	31	-	-	-	-	-	-	-	-	5.4	6.4	5.6	5.8
IX	-	-	-	-	10.9	15.6	12.4	12.8	17.1	9.2	27.9	9	1.7	27	-	-	-	-	-	-	-	-	6.6	6.8	6.9	6.8
X	-	-	-	-	7.0	13.8	9.3	9.8	14.6	5.4	22.1	19	-0.2	3	-	-	-	-	-	-	-	-	6.1	4.6	3.2	4.6
XI	-	-	-	-	4.3	7.2	4.7	5.2	8.5	2.8	18.6	4	-9.8	30	-	-	-	-	-	-	-	-	6.5	6.3	7.1	6.6
XII	-	-	-	-	-1.1	1.4	-0.4	-0.1	2.7	-2.9	13.6	13	-9.3	1	-	-	-	-	-	-	-	-	7.5	7.0	6.8	7.0
Rok	-	-	-	-	6.9	11.6	8.4	8.8	13.2	5.1	36.2	5.VII	-12.5	17.1	-	-	-	-	-	-	-	-	6.6	6.5	6.0	6.4

Cieszyn

$\varphi = 49°45'$ $\lambda = 18°38'$

I	-	-	-	-	-2.0	1.3	-1.3	-0.8	2.3	-4.1	10.6	2	-17.4	17	82	75	83	80	1.0	1.8	0.9	1.2	8.4	8.1	7.1	7.9
II	-	-	-	-	1.6	5.5	2.5	3.0	7.1	-0.6	11.4	6	-9.2	28	87	76	84	82	0.9	2.3	1.3	1.5	8.3	8.0	7.2	7.8
III	-	-	-	-	1.5	8.2	4.3	4.6	9.8	-0.4	17.9	14	-9.8	1	85	63	76	75	1.1	4.8	2.2	2.7	7.4	5.3	6.0	6.2
IV	-	-	-	-	5.0	11.5	7.7	8.0	13.5	3.2	25.9	29	-3.3	14	87	61	77	75	1.5	6.8	2.9	3.7	6.2	7.0	7.1	6.8
V	-	-	-	-	8.6	13.4	9.7	10.4	15.1	5.7	24.1	19	0.9	29	82	64	80	75	2.1	6.4	2.7	3.7	7.5	7.8	7.5	7.6
VI	-	-	-	-	16.5	22.4	17.3	18.4	24.3	11.4	31.2	11	4.4	27	77	59	76	71	4.6	12.0	5.0	7.2	5.3	6.4	5.9	5.9
VII	-	-	-	-	17.6	22.2	17.5	18.7	23.7	14.2	35.3	5	11.1	17,28	87	72	87	82	3.2	9.7	3.0	5.3	7.6	7.5	8.0	7.7
VIII	-	-	-	-	14.1	20.4	15.0	16.1	22.0	11.4	28.8	11	6.4	23	88	67	88	81	2.1	8.6	2.2	4.3	6.1	6.3	6.3	6.2
IX	-	-	-	-	10.4	15.7	11.2	12.1	17.4	8.0	27.5	9	-0.4	27	92	72	92	85	1.3	5.6	1.2	2.7	6.6	7.2	7.0	6.9
X	-	-	-	-	6.9	14.7	8.5	9.6	15.8	4.7	22.7	19	0.0	3	92	67	91	83	0.9	5.9	1.3	2.7	6.1	5.8	3.6	5.2
XI	-	-	-	-	4.2	7.8	4.8	5.4	9.0	2.5	19.6	4	-9.9	30	91	75	88	85	1.0	3.5	1.4	2.0	8.2	7.4	8.2	7.9
XII	-	-	-	-	-1.0	1.4	-0.3	0.0	3.0	-3.4	14.7	13	-9.5	1,11	85	82	85	84	1.0	1.4	1.0	1.1	7.4	7.4	6.7	7.2
Rok	-	-	-	-	7.0	12.0	8.1	8.8	13.6	4.4	35.3	5.VII	-17.4	17.1	86	69	84	80	1.7	5.7	2.1	3.2	7.1	7.0	6.7	6.9

Cieszyn – Bobrek

$\varphi = 49°45'$ $\lambda = 18°39'$

I	-	-	-	-	-2.0	1.3	-1.1	-0.7	2.3	-3.9	11.1	2	-19.8	17	86	74	86	82	0.9	1.9	0.9	1.2	8.4	7.7	7.3	7.8
II	-	-	-	-	1.9	5.5	2.6	3.2	6.7	-0.4	11.0	6	-10.9	28	83	68	82	78	1.3	3.1	1.5	2.0	7.6	7.8	6.6	7.3
III	-	-	-	-	1.3	7.7	4.0	4.2	9.3	-0.9	17.0	14	-12.8	1	83	61	78	74	1.4	5.0	2.1	2.8	6.9	6.3	5.5	6.2
IV	-	-	-	-	5.5	11.3	7.1	7.8	13.0	2.7	24.8	29	-4.4	14	85	60	80	75	1.9	7.0	2.4	3.8	6.1	7.1	7.1	6.8
V	-	-	-	-	9.0	13.0	9.1	10.0	14.6	5.0	23.2	19	-0.5	30	80	63	82	75	2.5	6.5	2.3	3.8	7.3	8.0	7.2	7.5
VI	-	-	-	-	16.5	22.1	16.0	17.6	23.9	10.5	34.3	11	2.7	27	77	57	83	72	4.5	12.1	3.5	6.7	5.1	6.0	5.2	5.4
VII	-	-	-	-	17.7	22.0	16.9	18.4	23.7	14.2	36.8	5	10.0	4	83	66	88	79	4.0	10.9	2.5	5.8	7.5	7.3	7.1	7.3
VIII	-	-	-	-	14.3	20.4	14.8	16.9	22.0	10.8	29.6	11	4.8	23	88	61	89	79	2.3	9.8	2.1	4.7	6.3	6.1	6.2	6.2
IX	-	-	-	-	10.5	15.8	11.3	12.2	17.3	7.7	27.9	9	-1.0	27	90	69	91	83	1.6	6.4	1.3	3.1	6.7	7.3	6.5	6.8
X	-	-	-	-	6.7	14.2	7.9	9.2	15.5	3.7	21.6	19	-4.5	3	90	64	90	81	1.1	6.3	1.4	2.9	5.5	5.8	3.6	5.0
XI	-	-	-	-	4.1	7.8	4.4	5.2	8.8	2.1	19.1	4	-9.7	30	88	73	86	82	1.2	3.6	1.4	2.1	7.4	7.0	8.1	7.5
XII	-	-	-	-	-0.7	1.3	-0.1	0.1	3.1	-3.5	14.5	13	-13.1	11	86	80	86	84	1.0	1.5	1.1	1.2	7.3	7.3	6.3	7.0
Rok	-	-	-	-	7.1	11.9	7.7	8.6	13.3	4.0	34.8	5.VIII	-19.8	17.1	85	66	86	79	2.0	6.2	1.9	3.4	6.8	7.0	6.4	6.7

Ciężkowice

$H_s = 280$ m $h_w = 16$ m **1957**

MIESIĄC	ROZKŁAD WIATRU [%, m/s] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD [mm] Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max<10	Max>25	Opad R ≥0.1	≥1.0	≥10.0	Wiatr ≥10	≥15	≡	≈	▲	●	⊛
I	25	26	2	25	25	18	15	20	17	14	14.5	12	12	16	8	21	33	1.0	36.0	11.6	6	24	10	5	·	12	7	2	·	·	·	·	1	14	24
II	15	13	·	·	2	2.0	3	1.7	2.0	2.0	17.5	12	13	14	6	20	21	1.2	30.0	7.3	25	13	2	·	·	14	10	·	·	·	1	·	2	15	9
III	5	1.8	2	1.3	11	1.5	8.5	1.7	6.5	1.6	10	1.2	13.5	2.1	9.5	1.6	29	1.1	56.1	15.1	18	18	3	1	·	13	7	3	·	·	3	1	4	8	7
IV	5	1.9	4.5	1.4	4	1.4	4	1.5	6	1.2	6.5	1.3	13.5	1.2	11.5	1.9	35	0.9	56.2	16.3	11	10	·	·	1	17	14	1	·	·	12	2	4	16	·
V	9.5	1.7	6.5	2.0	6	1.7	3	1.3	4.5	1.2	1.5	1.0	13.5	1.4	15.5	1.7	33	1.0	79.0	18.8	9	1	·	·	·	16	13	2	·	·	10	1	1	16	1
VI	4.5	2.2	0.5	3.0	3.5	1.6	3.5	1.7	1.4	1.5	4.5	1.2	7	1.3	10.5	2.2	42	0.9	54.2	17.7	23	·	·	·	15	14	7	2	·	·	4	5	5	3	·
VII	2.5	1.4	0.5	1.0	4.6	1.4	4	1.8	3.5	1.1	8	1.4	20.5	1.7	6.5	1.5	43	0.8	122.4	27.0	15	·	·	·	13	18	15	4	·	·	8	6	1	13	·
VIII	3.5	1.6	·	·	3.5	1.6	0.5	1.0	6.5	1.3	7	1.2	17.5	1.6	9.5	2.1	45	0.8	79.2	20.8	28	·	·	·	8	16	11	4	·	·	13	5	2	6	·
IX	4.5	1.2	1.5	1.0	3	1.3	1	1.0	8.5	1.1	16.5	1.3	21.5	1.8	5.5	2.0	28	1.0	66.4	24.2	4	2	·	·	2	18	11	1	·	·	10	·	2	12	·
X	0.5	1.0	·	·	5	1.2	5	1.0	1.3	1.3	10.5	1.0	16.5	1.2	8.5	1.6	36	0.8	27.4	8.3	20	5	·	·	·	6	4	·	1	·	21	·	5	7	·
XI	3.5	2.4	5.5	2.0	10.5	1.5	8.5	1.5	20.5	1.4	7	1.2	11.5	2.1	5	3.4	18	1.4	31.3	12.9	11	10	2	·	·	10	6	1	·	·	5	·	6	15	1
XII	4.5	2.2	1.5	1.3	3	1.7	1.5	1.0	2.0	1.4	2.1	1.3	7	1.1	12.5	2.0	22	1.2	25.5	6.2	14	27	7	1	·	13	7	·	·	·	3	·	5	17	10
Rok	4.5	1.8	24.5	1.3	58.5	1.6	44	1.4	14.0	1.4	12.4.5	1.2	16.7	1.5	106.5	2.0	385	1.0	663.7	27.0	15.VIII	110	24	7	39	167	112	20	1	·	68	20	58	142	52

Raźnów

$H_s = 300$ m $h_w = 20$ m

I	1	3.0	4	2.5			23.5	2.3	12.5	3.6	6	5.1	14.5	7.6	9.5	2.6	22	3.0	28.1	9.2	5	25	10	3	·	14	6	·	2	2	-	·	2	14	22
II							23.5	3.7	2.5	6.2	8.5	4.9	6	5.3	12	3.2	9	4.2	22.5	6.1	24	9	2	·	·	13	7	·	4	2	-	·	2	14	7
III	3.5	3.0	3.5	1.7	5	3.0	3.0	2.7	8.5	4.0	2	9.2	16	6.3	7.5	4.2	17	3.2	42.5	10.8	24	13	3	·	·	13	6	2	4	1	-	1	7	8	7
V	6	2.2	3.5	2.1	0.5	1.0	18.5	2.4	3.5	3.7	4	3.1	14.5	2.7	18.5	2.2	21	1.9	68.5	16.9	11	3	·	·	1	19	10	2	·	·	-	3	5	13	1
V	8	4.4	6.5	2.8	3	1.7	4.4	1.6	4	1.8	3	1.3	7.5	2.9	3.1	2.8	16	2.2	86.9	21.8	10	·	·	·	·	17	12	4	·	·	-	2	1	15	·
VI	3	3.0	·	·	0.5	2.0	2.9	3.1	1.7	4.0	2	3.5	15.6	3.0	1.2	3.8	11	3.0	50.9	15.2	12	·	·	·	1.2	12	10	2	2	·	-	6	5	3	·
VII	3	2.3	2	1.5	·	·	2.8	2.2	8.5	2.2	3.5	2.1	1.8	3.6	9	1.7	21	1.9	128.2	29.4	15	·	·	·	1.3	17	13	6	·	·	-	8	3	15	·
VIII	3.5	1.1	1	2.0	1	1.0	20.5	2.2	8.5	1.6	3	3.0	1.7	4.3	14.5	3.7	24	2.1	84.8	34.2	28	·	·	·	6	15	11	2	2	2	-	5	2	4	·
IX	3	2.3	2	2.0	2.5	1.4	16.5	2.4	7	3.3	6.5	3.5	21.5	4.8	11	3.4	20	2.7	64.6	23.1	4	·	·	·	2	14	11	1	1	·	-	·	2	12	·
X	3.5	1.0	·	·	2.5	1.8	3.3	1.9	7.5	4.1	5.5	1.8	8	2.3	5	2.0	28	1.6	28.9	10.8	20	1	·	·	·	5	3	1	·	·	-	·	6	4	·
XI	2	2.5	9	2.1	8.5	1.9	22.5	3.3	1.1	6.1	4	4.8	1.1	7.2	9	5.7	13	3.6	30.5	18.0	11	10	2	·	·	9	5	1	4	1	-	·	6	15	1
XII	3	2.3	1	1.0	2.5	1.4	2.3	3.0	1.5	5.3	5	5.9	8.5	4.3	1.5	4.3	20	3.1	17.8	3.8	5	25	6	·	·	14	7		3	·	-	·	4	17	6
Rok	39.5	2.3	32.5	1.5	26	1.3	28.2	2.6	12.8	3.8	5.3	4.0	15.8	4.5	15.4	3.3	222	2.7	651.2	34.2	28.VIII	86	23	3	34	162	101	21	22	8	-	25	45	134	44

Cieszyn

$H_s = 300$ m $h_w = 16$ m

I	5	1.5	5.5	3.6	1	3.0	16	3.0	20.5	2.2	16	1.3	6.5	2.0	6.5	1.4	16	1.8	30.7	7.6	6	25	10	6	·	11	9					·	2	17	20
II	1	4.0	2	2.5	·	·	12.5	2.8	2.7	2.6	24.5	2.0	4	2.1			13	2.0	68.3	17.2	25	13	·	·	·	15	13	2						14	7
III	6	1.7	1.7	1.7	4.5	2.0	16.5	2.1	14.5	2.0	12	2.5	4	3.4	2.5	1.4	16	1.7	54.4	12.1	16	14	2	·	·	14	11	1			2	1	6	14	8
IV	9.5	1.2	12.5	1.4	·	·	1.0	1.8	9.5	1.6	12	1.5	2.5	2.0	8	1.2	26	1.0	76.8	17.3	7	7	·	·	2	17	13	2			4	1	3	13	·
V	14.5	2.7	2.2	2.8	0.5	1.0	7.5	1.3	3	1.3	6.5	1.8	5.5	1.6	17.5	1.6	16	1.8	65.1	33.0	20	·	·	·	·	12	6	2				2	1	17	·
VI	5	1.8	5	1.9	·	·	1.2	1.4	1.4	2.4	11.5	2.4	2	1.0	10.5	1.9	30	1.3	45.1	12.1	7	·	·	·	11	11	8	2				6	5	10	·
VII	3.5	1.4	2	1.8	1.5	1.0	11	1.6	1.6	1.8	1.8	2.2	6	2.1	6	1.6	29	1.3	199.2	55.3	16	·	·	·	11	19	18	6	1	1	1	7	1	20	·
VIII	2.5	1.4	·	·	1	1.0	1.3	1.6	16.5	2.1	10	1.6	9	1.3	12	1.6	29	1.1	78.4	22.2	28	·	·	·	7	13	12	1	2	1		1		7	·
IX	1	1.0	2	1.5	0.5	1.0	13.5	1.8	22.5	1.9	1.8	2.5	5.5	3.0	8	1.0	19	1.6	86.9	11.0	29	1	·	·	2	20	15	2			1	·	2	14	·
X	1.5	1.0	1.5	1.0	2	1.0	21.5	1.3	23.5	1.7	7.5	1.3	5	1.5	10.5	1.0	20	1.2	24.4	9.9	22	·	·	·	·	4	3	·	·	·	2	·	5	5	·
XI	7	3.2	14.5	2.2	6	1.5	16	2.3	12.5	2.2	12.5	2.1	1.5	2.3		·	20	1.8	18.4	9.0	28	10	1	·	·	8	4	·	·	·	3	·	1	18	·
XII	8	1.2	11.5	1.4	5.5	1.0	18.5	1.9	16.5	2.1	17	3.6	1	1.0	8	1.0	7	1.8	32.6	6.2	3	26	7	·	·	14	8	·	1	·	·	·	1	16	10
Rok	64.5	1.8	95.5	1.8	22.5	1.0	168	1.9	196	2.0	165.5	2.1	52.5	1.9	89.5	1.1	241	1.5	777.3	55.3	16.VII	96	20	6	33	158	120	18	4	2	13	18	27	165	45

Cieszyn – Bobrek

$H_s = 300$ m $h_w = 15{,}5$ m

I	6.5	1.4	9.5	4.6	0.5	1.0	9.5	3.6	1.3	3.3	1.4	2.8	1.5	2.8	1.9	1.7	6	2.6	29.3	6.6	6	24	10	5	·	12	9	·	·	·	1	·	2	19	18
II	4.5	1.6	5	2.6	0.5	2.0	9.5	4.5	2.0.5	4.9	1.6	3.8	1.3	2.3	9	2.1	6	3.2	58.4	14.5	21	13	1	1	·	15	13	3	·	·	5	·	1	11	7
III	14.5	1.6	3.0	2.9	2	1.0	9.5	4.7	6.5	4.4	5	5.2	9.5	5.8	9	1.6	7	3.0	47.8	11.2	16	14	3	2	·	15	10	1	4	·	4	1	5	11	7
IV	2.3	1.6	19.5	2.7	3.5	1.9	6	3.3	4	2.4	5.5	5.5	1	4.0	17.5	1.7	10	2.1	85.7	20.6	7	11	·	·	·	17	11	3	·	·	4	2	3	12	1
V	15.5	1.4	42.5	3.8	·	·	2.5	3.0	1	2.5	3.5	4.0	4.5	3.0	18.5	2.0	5	2.8	53.0	21.0	20	2	·	·	·	13	6	2	·	·	·	2	1	14	·
VI	12.5	1.8	11	2.9	2.5	2.0	6.5	3.3	9	4.2	7.5	4.4	6.5	2.9	15.5	2.7	12	2.5	58.3	11.7	7	·	·	·	12	12	8	1	·	·	·	7	5	7	·
VII	14.5	1.7	9.5	2.0	0.5	3.0	14.5	3.2	1	3.5	8.5	4.6	2.0	3.4	14.5	2.5	10	2.6	184.5	50.2	16	·	·	·	9	2.0	2.0	5	·	·	·	10	·	16	·
VIII	2.1	1.6	5.5	1.5	·	·	4	3.5	4	4.1	7	5.2	1.1	3.5	2.0.5	2.1	2.0	2.0	70.8	2.0.9	28	·	·	·	6	14	11	1	1	·	1	2	2	10	·
IX	7	1.6	7	1.6	1	1.0	2.5	4.0	7.5	3.1	2.1	4.7	1.6	3.7	12	1.7	14	2.7	84.1	14.9	29	1	·	·	2	2.1	14	2	1	·	2	1	1	11	·
X	9	1.2	14	1.2	1	1.0	11.5	2.3	8.5	3.0	5.5	3.6	1.1	3.5	11.5	2.1	2.1	1.8	17.1	7.9	22	4	·	·	·	5	3	·	·	·	3	·	5	5	·
XI	5	1.1	2.7	2.8	·	·	1.3	3.0	6	4.3	7.5	3.3	9.5	2.8	6	1.9	16	2.5	16.7	8.4	28	11	1	·	·	8	4	·	·	·	4	·	2	19	·
XII	1.1	1.4	10	3.0	0.5	1.0	9.5	3.3	1.5	4.9	1.1	5.7	12.5	3.1	17.5	1.5	6	3.0	33.5	6.1	3	25	8	2	·	14	9	·	2	·	1	·	3	16	7
Rok	15.1	1.8	190.5	2.6	12	1.2	98.5	3.5	96	3.7	11.2	4.4	13.1.5	3.4	170.5	2.0	133	2.6	719.2	50.2	16.VII	105	23	10	29	166	118	18	8	·	2.5	2.5	30	151	40

Klimczok

$\varphi = 49°44'$ $\lambda = 19°00'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-4,7	-2,4	-4,0	-3,8	-0,0	-6,9	3,5	23	-17,1	16	–	–	–	–	–	–	–	–	7,7	7,7	8,0	7,8
II	–	–	–	–	-2,2	-0,2	-1,4	-1,3	1,3	–	9,5	5	–	–	–	–	–	–	–	–	–	–	7,8	7,3	8,0	7,7
III	–	–	–	–	-1,3	2,0	0,1	0,2	3,8	–	13,0	14	-12,1	1	–	–	–	–	–	–	–	–	7,2	5,7	7,4	6,8
IV	–	–	–	–	2,3	4,9	2,4	3,0	6,4	0,1	19,5	30	-6,5	15	–	–	–	–	–	–	–	–	6,9	6,8	8,2	7,3
V	–	–	–	–	3,6	6,1	4,2	4,5	7,9	1,8	17,5	19	-5,4	6	–	–	–	–	–	–	–	–	7,7	7,4	7,7	7,6
VI	–	–	–	–	12,1	15,3	13,1	13,4	17,6	9,4	27,0	12	3,3	6	–	–	–	–	–	–	–	–	5,1	5,7	6,8	5,9
VII	–	–	–	–	12,7	15,6	12,9	13,5	17,3	10,7	28,2	8	6,3	28	–	–	–	–	–	–	–	–	7,7	7,4	8,0	7,7
VIII	–	–	–	–	10,0	12,9	10,6	11,0	15,2	8,2	22,3	14	3,8	22	–	–	–	–	–	–	–	–	7,1	6,6	7,1	6,9
IX	–	–	–	–	6,2	8,7	7,0	7,2	10,5	4,7	21,2	9	-1,2	27	–	–	–	–	–	–	–	–	8,2	7,5	7,6	7,8
X	–	–	–	–	4,2	7,9	6,0	6,0	9,2	2,4	16,5	9	-1,8	2	–	–	–	–	–	–	–	–	7,2	5,6	5,4	6,0
XI	–	–	–	–	0,9	2,2	1,2	1,4	3,8	-0,3	13,0	5	-6,5	19	–	–	–	–	–	–	–	–	7,9	7,5	7,1	7,5
XII	–	–	–	–	-1,8	-3,1	-1,8	-2,4	-1,1	-2,2	6,2	13,14	-13,9	2	–	–	–	–	–	–	–	–	8,2	8,1	7,2	7,8
Rok	–	–	–	–	3,2	5,8	3,9	4,2	7,6	–	28,2	8.VII	–	–	–	–	–	–	–	–	–	–	7,4	6,9	7,4	7,2

Maków Podhalański

$\varphi = 49°44'$ $\lambda = 19°40'$

I	–	–	–	–	-3,1	1,7	-2,1	-1,5	2,5	-5,4	11,5	2	-17,2	17	–	–	–	–	–	–	–	–	7,3	7,1	6,9	7,1
II	–	–	–	–	0,2	5,3	1,7	2,2	6,5	-1,9	13,0	6	-12,0	23	–	–	–	–	–	–	–	–	7,1	6,6	6,7	6,8
III	–	–	–	–	-0,4	7,9	2,8	3,3	9,1	-2,3	16,5	14	-14,1	4	–	–	–	–	–	–	–	–	5,6	4,8	5,0	5,1
IV	–	–	–	–	4,9	11,7	6,4	7,4	12,5	2,3	24,4	29	-3,4	14,16	–	–	–	–	–	–	–	–	6,1	6,1	5,7	6,0
V	–	–	–	–	7,4	12,8	8,8	9,4	13,8	4,4	23,5	19	0,0	9	–	–	–	–	–	–	–	–	6,5	7,4	7,0	7,0
VI	–	–	–	–	15,5	22,5	15,3	17,1	23,5	9,5	30,5	11,24	3,1	27	–	–	–	–	–	–	–	–	3,8	5,1	3,8	4,2
VII	–	–	–	–	16,6	21,9	16,7	18,0	22,8	12,9	34,4	5	7,6	30	–	–	–	–	–	–	–	–	7,1	6,7	6,1	6,6
VIII	–	–	–	–	12,9	20,5	13,9	15,3	21,7	9,3	29,4	11	3,7	24	–	–	–	–	–	–	–	–	5,2	6,1	6,1	5,8
IX	–	–	–	–	9,0	15,7	10,6	11,5	17,0	7,0	29,1	9	-0,9	26	–	–	–	–	–	–	–	–	6,6	5,5	6,8	6,3
X	–	–	–	–	3,9	14,0	6,4	7,7	15,0	1,6	24,0	19	-4,9	3	–	–	–	–	–	–	–	–	5,4	3,2	4,5	4,4
XI	–	–	–	–	2,4	7,5	3,5	4,2	8,8	0,2	18,6	5	-11,3	30	–	–	–	–	–	–	–	–	7,2	6,5	7,0	6,9
XII	–	–	–	–	-2,3	1,5	-1,4	-0,9	3,1	-5,1	15,0	13	-14,1	11	–	–	–	–	–	–	–	–	6,5	6,3	6,7	6,5
Rok	–	–	–	–	5,6	11,9	6,9	7,8	13,0	2,7	34,4	6.VII	-17,2	17,1	–	–	–	–	–	–	–	–	6,2	6,0	6,0	6,1

Tęgoborze

$\varphi = 49°44'$ $\lambda = 20°38'$

I	–	–	–	–	-1,8	0,6	-1,1	-0,8	2,2	-3,9	7,2	6	-14,9	17	83	72	84	80	1,0	1,8	0,9	1,2	7,7	7,2	6,1	7,0
II	–	–	–	–	2,2	5,0	3,2	3,4	6,4	0,6	10,4	19	-4,7	28	82	66	79	76	1,4	3,2	1,8	2,1	7,6	7,1	6,6	7,1
III	–	–	–	–	1,5	6,8	3,8	4,0	8,9	-0,2	12,5	14	-9,9	4	75	63	72	70	1,9	4,5	2,6	3,0	6,5	4,8	4,8	5,4
IV	–	–	–	–	5,8	11,4	8,5	8,6	13,1	4,2	22,8	30	-1,2	14	81	60	75	72	1,8	6,2	3,0	3,7	6,2	6,9	6,4	6,5
V	–	–	–	–	8,1	13,1	10,1	10,4	14,4	6,5	22,1	14	1,2	7	83	66	80	76	1,8	6,0	2,6	3,5	6,9	8,0	7,6	7,5
VI	–	–	–	–	15,9	22,1	17,7	18,4	24,0	12,9	30,6	30	7,6	1	80	59	79	73	3,9	11,2	4,6	6,6	4,2	6,3	5,2	5,2
VII	–	–	–	–	17,4	22,2	18,6	19,2	24,3	15,3	36,0	5	11,1	30	85	66	82	78	3,1	10,4	4,0	5,8	7,3	7,5	7,3	7,4
VIII	–	–	–	–	14,7	20,6	16,7	17,2	–	12,8	–	–	7,2	31	86	63	81	77	2,4	9,5	3,8	5,2	5,9	6,4	6,1	6,1
IX	–	–	–	–	11,2	16,2	12,7	13,2	17,4	9,2	27,1	8	2,4	26,27	84	63	82	76	2,2	7,1	2,7	4,0	6,5	7,0	7,5	7,0
X	–	–	–	–	7,3	13,9	9,6	10,1	14,9	5,8	20,2	19	0,4	3	86	64	84	78	1,2	6,0	2,1	3,1	5,8	4,6	2,4	4,3
XI	–	–	–	–	4,9	7,4	5,4	5,8	8,2	3,6	17,0	4	-9,3	30	81	71	80	77	1,8	3,4	2,0	2,4	6,8	6,2	5,8	6,3
XII	–	–	–	–	-0,9	4,3	0,0	0,1	–	–	–	–	–	–	83	73	81	76	1,0	1,9	1,3	1,4	7,6	7,0	6,8	7,1
Rok	–	–	–	–	7,2	11,7	8,8	9,1	–	–	–	–	-14,9	17,1	82	66	80	76	2,0	5,9	2,6	3,5	6,6	6,6	6,0	6,4

Biecz

$\varphi = 49°44'$ $\lambda = 21°15'$

I	–	–	–	–	-2,2	0,0	-2,2	-1,6	0,8	-4,8	6,1	9	-15,5	17	81	79	81	80	1,0	1,3	1,0	1,1	8,5	7,1	5,7	7,1
II	–	–	–	–	1,7	4,4	2,5	2,8	5,5	-0,2	10,6	19	-7,3	1	81	74	78	78	1,4	2,4	1,6	1,8	8,2	6,8	6,1	7,0
III	–	–	–	–	-0,5	6,3	2,5	2,7	7,7	-2,1	17,8	14	-15,8	4	75	65	75	72	1,5	4,3	2,0	2,6	5,5	5,0	3,8	4,8
IV	–	–	–	–	4,6	11,9	7,5	7,9	13,1	2,5	24,7	30	-1,1	6,16	88	60	80	76	1,0	6,7	2,3	3,3	6,3	7,0	6,0	6,4
V	–	–	–	–	7,6	12,7	8,9	9,5	14,3	5,0	22,3	17	-0,4	30	86	66	83	78	1,5	6,4	2,0	3,3	6,7	7,4	6,8	6,9
VI	–	–	–	–	15,6	22,2	16,0	17,4	23,7	10,2	31,3	12	4,6	7	81	55	80	72	3,6	12,6	3,9	6,7	4,2	5,3	4,1	4,5
VII	–	–	–	–	16,7	22,4	17,1	18,3	24,1	12,9	35,7	5	6,7	4	86	63	84	78	2,8	11,5	3,4	5,9	6,2	6,9	6,2	6,4
VIII	–	–	–	–	13,9	20,4	15,2	16,2	22,0	10,7	30,6	14	3,8	24	88	60	85	78	2,0	10,3	2,8	5,0	5,0	5,2	4,5	4,9
IX	–	–	–	–	9,5	16,1	11,3	12,0	17,2	7,5	27,4	9	-0,9	26	89	67	86	81	1,4	6,4	1,8	3,2	5,8	6,9	6,1	6,3
X	–	–	–	–	4,7	13,6	7,6	8,4	14,6	2,7	19,4	12	-4,7	3	90	59	85	78	1,1	6,6	1,9	3,2	5,7	4,5	3,5	4,6
XI	–	–	–	–	3,3	6,8	4,1	4,6	7,7	1,4	17,7	9	-11,8	30	85	72	81	79	1,4	3,2	1,7	2,1	6,4	5,9	6,1	6,1
XII	–	–	–	–	-2,0	0,5	-0,9	-0,8	1,4	-3,9	10,1	14	-13,2	11	80	78	81	80	1,0	1,4	1,1	1,2	7,7	7,8	6,7	7,1
Rok	–	–	–	–	6,1	11,4	7,5	8,1	12,7	3,5	35,7	5.VII	-15,8	4.III	84	66	82	77	1,6	6,1	2,1	3,3	6,4	6,2	5,4	6,0

Klimczok

$H_s = 1010\ m$ $h_w = 16\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU nD, vmD																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Sumo	Max	Data	Temperatura T				Opad R			Wiatr v					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max>25°	0,1 ÷ 1	1,0 ÷ 10	10 ÷ 100	10 ÷ 15	15 ÷					
I	9,5	6,4	·	·	·		·	·	34,5	4,8	11,5	7,0	6,5	6,8	5	6,3	29	4,0	58,0	13,4	6	30	17	5	·	13	9	2	6	·	17	–	·	18	31
II	9	5,3	1	3,0	·		·	·	37,5	5,3	12,5	8,0	5	8,8	2	6,8	17	4,8	57,4	7,4	7	–	9	–	·	13	12	·	6	1	10	·	·	15	28
III	10,6	4,5	2	7,0	2	4,0	4	5,5	38	5,2	11	5,3	4	4,0	4,5	4,4	17	4,1	39,3	7,4	18	–	11	–	·	11	9	·	7	·	11	–	·	12	23
IV	17,5	3,8	12,5	3,3	1	2,0	2	3,5	23,5	3,6	12,5	3,5	6	2,8	3	3,0	12	3,0	30,8	5,3	7	16	7	·	·	13	11	·	·	·	10	–	1	16	14
V	26,5	3,2	20	3,6	1	3,0	1	4,0	11	2,9	2	3,5	8	2,8	15	2,0	22	2,4	31,8	7,4	21	15	4	·	·	8	7	·	·	·	12	1	1	15	5
VI	11	2,5	11	2,7	1	3,0	2	3,0	29,5	3,9	10,5	3,0	4	4,8	7	2,8	14	2,8	21,2	5,3	18	·	·	·	1	8	8	·	·	·	2	–	·	7	·
VII	15	2,8	2	3,5	3	3,0	4	4,0	34,5	4,4	15	4,3	5	3,8	9,5	3,3	8	3,5	42,6	10,7	16	·	·	·	4	21	20	11	·	·	17	–	·	13	·
VIII	10,5	3,0	4,5	3,3	·	·	2	3,5	30	5,3	16	4,4	5	3,6	8	3,5	17	3,5	12,6	7,8	28	·	·	·	·	13	13	3	1	·	11	–	·	8	·
IX	8	5,1	1	5,0	·	·	·	·	4,5	5,7	12	4,9	6	5,0	14	3,5	4	4,9	18,3	8,0	3	4	·	·	·	20	19	6	·	·	19	–	·	17	·
X	12,6	2,7	2,5	2,8	·	·	·	·	5,3	6,0	9,5	3,9	2,5	4,2	4	5,0	9	4,6	23,9	8,2	22	7	·	·	·	5	5	·	·	·	5	–	·	3	·
XI	3	3,3	4	4,8	2	4,0	13,5	3,7	43,5	5,5	16,5	5,4	4,5	3,9	2	4,5	4	4,9	31,5	9,5	11	16	11	·	·	9	8	·	·	·	–	–	·	14	2
XII	1	3,0	4	2,2	2	1,5	4	4,1	50,5	5,6	12,5	5,4	1,5	4,5	4	3,0	·	4,9	42,5	4,0	13	30	19	9	·	13	6	·	·	·	16	–	·	16	31
Rok	134	3,8	64,5	3,4	12	1,7	32,5	2,6	424,5	4,8	141,5	4,9	71,5	4,6	64,5	4,0	150	4,0	744,6	10,7,0	16.VII	–	78	–	5	147	127	22	20	1	–	–	2	154	134

Maków Podhalański

$H_s = 350\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32,1	6,2	8	28	7	7	·	13	12	·	–	–	–	·	3	17	20
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	55,1	15,6	25	20	2	1	·	12	8	2	–	–	–	·	3	12	8
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35,3	8,7	16	19	1	3	·	9	8	·	–	–	–	·	9	12	7
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	64,8	13,4	11	8	·	·	·	18	17	1	–	–	–	1	6	14	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	59,5	10,1	8	·	·	·	·	12	12	1	–	–	–	1	3	15	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48,0	12,4	22	·	·	·	10	10	10	2	–	–	–	2	7	6	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27,8,2	5,4,2	5	·	·	·	9	19?	19?	6?	–	–	–	7	2	13	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	11,2,8	2,6,9	28	·	·	·	7	14	13	5	–	–	–	4	2	8	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	79,5	22,3	4	1	·	·	2	15	13	2	–	–	–	·	5	8	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	20,6	7,1	20,22	8	·	·	·	5	4	·	–	–	–	·	10	7	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27,0	9,9	29	11	1	1	·	7	6	·	–	–	–	·	4	16	1
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25,5	5,3	4	26	7	3	·	10	9	·	–	–	–	·	7	16	9
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	836,4	54,2	XII	121	18	15	28	144,1	131,1	19?	–	–	–	15	61	144	45

Tęgoborze

$H_s = 300\ m$ $h_w = 18\ m$

I	4,5	4,0	2	3,0	4,5	3,1	5	5,0	19,5	3,9	4,5	4,5	6	2,8	0,5	1,0	3,9	2,2	24,8	6,6	5	25	9	5	·	11	6	·	1	·	–	·	1	13	22
II	5	4,2	·	·	5	2,8	0,5	2,0	2,8	6,1	4,1	4,3	7,5	3,8	5	1,9	2,2	3,3	36,4	7,5	25	10	2	·	·	11	9	·	6	1	–	·	3	17	5
III	5	4,9	3	4,5	7,5	3,6	4	3,6	15,5	4,1	6	3,2	8	2,3	2	1,5	4,2	4,8	45,5	15,2	24	14	2	·	·	11	7	1	1	·	–	1	8	9	5
IV	9	2,2	2,5	1,6	2	1,8	2,5	1,6	8,5	2,1	2,5	7,6	1,5	1,7	5,5	1,5	5,6	0,9	66,2	23,0	7	4	·	·	·	15	8	2	1	1	–	2	5	13	·
V	8	2,2	3	1,7	5	4,4	0,5	2,0	6,5	1,8	4	1,4	1	1,5	2,1	1,5	4,4	1,0	101,9	25,9	20	·	·	·	·	14,4	13	3	·	·	–	2	1	16	·
VI	9,5	1,5	0,5	1,0	3,5	2,0	0,5	2,0	25,5	2,7	4,5	2,1	7	1,4	8	1,3	3,1	1,4	24,9	5,0	12	·	·	·	11	11	9	·	1	·	–	6	5	3	·
VII	5,5	1,5	0,5	1,0	5,5	2,1	0,5	5,0	22,5	2,2	2	2,2	1,7	1,6	9,5	1,6	3,0	1,3	136,5	34,7	15	·	·	·	12	16	12	6	·	·	–	5	2	16	·
VIII	9	1,1	0,5	1,0	3	1,3	1,5	1,0	24,5	2,1	4	2,6	8,5	1,5	1,2	2,3	3,0	1,3	94,9	30,3	28	·	·	·	–	16	12	2	2	·	–	4	·	7	·
IX	9	1,2	·	·	1,5	1,3	0,5	2,0	2,0	2,5	8,5	4,8	21,5	2,8	3	1,3	2,6	1,8	69,0	23,0	4	·	·	·	2	14	11	1	1	·	–	·	2	14	·
X	7	1,1	2	2,0	1,5	1,7	4	1,2	3,7	2,0	4	3,4	2,5	1,8	6	1,2	2,9	1,3	33,3	11,6	20	·	·	·	·	4	4	2	·	·	–	·	8	4	·
XI	7,5	3,3	4,5	3,7	4	4,4	6	2,5	3,0	4,4	2	2,2	3	1,7	5	3,2	2,8	2,6	33,8	18,4	11	10	1	·	·	8	5	1	·	·	–	·	6	13	·
XII	4,5	1,6	1,5	2,3	·	·	8	1,6	2,5	4,1	3,5	3,3	0,5	4,0	4	1,6	4,6	1,6	18,6	4,2	5,14	–	–	–	–	8	6	·	2	·	–	·	4	18	–
Rok	80,5	1,6	20	1,2	4,3	2,4	33,5	2,5	262,5	3,2	67	3,5	8,4	2,2	81,5	1,7	42,3	1,7	688,8	34,7	15.VII	–	–	–	–	139	102	15	15	2	–	20	45	11,3	–

Biecz

$H_s = 260\ m$ $h_w = 16\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29,0	11,2	6	25	11	7	·	11	7	1	–	–	·	·	1	14	21?
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	33,1	10,0	25	12	3	·	·	11	7	1	–	–	·	·	2	12	3
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	46,7	8,7	18	18	4	3	·	12	7	·	–	–	1	1	11	7	6
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	55,4	17,5	11	11	·	·	·	18	15	2	–	–	1	1	5	15	·
V	17	3,6	13	3,0	4	4,0	1	1,0	3	3,0	3	1,3	13	3,1	12	3,8	27	2,3	83,1	21,2	9	1	·	·	·	13	11	3	·	·	·	1	4	15	·
VI	6	3,2	4	2,0	4	2,8	3	1,7	17	4,4	2	1,5	7	4,1	7	4,1	40	2,2	75,4	45,3	12	·	·	·	11	9	7	1	·	·	·	3	6	2	·
VII	3	1,7	2	2,5	3	2,0	2	3,5	8	2,0	4	2,8	14	3,6	14	3,4	45	1,6	101,7	17,5	20	·	·	·	11	20	10	6	·	·	·	9	4	12	·
VIII	4	3,0	1	4,0	4	2,5	·	·	7	3,4	4	3,0	5	2,2	25	4,0	43	1,9	73,3	18,3	10	·	·	·	7	12	12	2	·	·	1	2	3	2	·
IX	5	2,8	1	2,0	3	2,0	·	·	7	3,4	17	3,0	9	4,1	10	3,9	38	1,9	74,7	18,5	4	1	·	·	2	16	11	3	·	·	5	1	3	9	·
X	1	4,0	1	4,0	3	2,7	3	1,3	8	4,5	15	3,0	6	2,3	9	2,3	47	1,4	21,9	7,5	20	4	·	·	·	5	4	·	1	·	9	·	9	4	·
XI	6	8,3	14	3,2	7	2,0	1	4,0	16	6,3	14	3,1	9	4,7	1	4,0	22	3,3	88,4	21,0	11	10	3	1	·	8	6	1	5	·	4	·	8	14	1
XII	9	3,7	4	5,2	3	1,7	1	4,0	14	5,6	30	4,5	6	3,7	11	4,5	15	3,7	23,0	5,5	5	28	9	1	·	9	6	·	4	·	·	·	4	15	8
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	645,7	45,3	12.VI	110	30	12	31	144	103	20	–	–	21	18	60	121	39?

Jasło

$\varphi = 49°44'$ $\lambda = 21°28'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	Średnia II	Średnia III	Średnia Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.0	-0.3	-1.7	-1.4	0.8	-4.0	6.2	9	-18.0	17	83	77	83	81	0.9	1.4	0.9	1.1	8.1	7.6	8.0	7.2
II	–	–	–	–	1.4	3.9	2.5	2.6	5.2	0.4	10.2	19	-5.0	28	89	76	83	83	0.8	2.1	1.4	1.4	7.9	7.2	6.2	7.1
III	–	–	–	–	-0.4	6.4	2.8	2.9	8.0	-1.5	16.5	31	-15.8	4	91	61	77	73	1.3	4.5	2.0	2.6	5.5	5.8	5.3	4.9
IV	–	–	–	–	5.0	12.8	8.4	8.6	14.1	3.4	25.0	30	-1.2	16	87	56	77	73	1.3	7.9	2.8	4.0	5.6	6.5	5.3	5.8
V	–	–	–	–	8.4	13.6	10.2	10.6	15.2	–	23.8	17	–	–	86	64	83	78	1.7	7.1	2.4	3.7	6.8	7.7	7.3	7.3
VI	–	–	–	–	15.8	22.8	17.6	18.4	24.2	–	32.3	12	–	–	82	55	77	71	3.5	13.0	4.7	7.1	3.9	5.3	3.9	4.4
VII	–	–	–	–	16.9	23.1	18.3	19.2	24.6	–	34.1	5.8	–	–	87	64	86	79	2.6	11.5	3.9	6.0	6.5	6.7	6.6	6.6
VIII	–	–	–	–	14.2	20.6	16.1	16.8	22.3	–	31.5	14	–	–	90	66	86	81	1.9	9.1	2.6	4.5	4.9	5.9	4.5	5.1
IX	–	–	–	–	9.9	16.3	11.9	12.5	17.3	–	27.2	9	–	–	92	67	89	83	1.0	6.6	1.6	3.1	6.3	7.1	5.9	6.4
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.5	3.5	4.4
XI	–	–	–	–	3.6	6.7	4.0	4.6	–	2.2	–	–	-9.2	30	88	76	86	83	1.0	2.7	1.2	1.6	6.6	6.2	5.8	6.1
XII	–	–	–	–	-1.9	0.3	-1.0	-0.9	–	-3.6	–	–	-10.8	11	88	79	86	84	0.6	1.3	0.9	0.9	7.1	6.9	5.4	6.5
Rok	–	–	–	–	–	–	–	–	–	–	34.1	5.8.VII	-15.8	4.III	–	–	–	–	–	–	–	–	6.2	6.4	5.3	6.0

Zbyszyce

$\varphi = 49°43'$ $\lambda = 20°40'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	16.8	21.9	18.4	18.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	6.9	7.1
VIII	–	–	–	–	13.9	20.0	16.8	16.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.4	6.0	5.5	5.3
IX	–	–	–	–	10.6	15.6	12.6	12.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	6.1	6.4
X	–	–	–	–	6.6	13.7	9.3	9.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.4	3.8	3.1	4.1
XI	–	–	–	–	4.1	7.0	4.7	5.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.5	6.7
XII	–	–	–	–	-1.4	1.2	-0.6	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	5.4	6.8
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Limanowa

$\varphi = 49°42'$ $\lambda = 20°25'$

I	–	–	–	–	-3.1	0.4	-2.6	-2.0	1.8	-6.1	7.4	6	-18.4	17	86	75	86	82	0.7	1.6	0.7	1.0	8.8	7.9	7.1	7.9
II	–	–	–	–	0.4	4.9	1.4	2.0	6.5	-1.8	12.8	6	-13.6	23	86	69	84	80	1.0	3.1	1.2	1.8	8.4	7.5	7.2	7.7
III	–	–	–	–	-0.7	6.6	4.7	2.3	8.5	-3.1	16.3	14	-16.8	4	–	–	–	–	–	–	–	–	6.8	5.5	5.3	5.9
IV	–	–	–	–	4.9	11.0	5.5	6.7	12.5	1.5	24.4	30	-6.5	14	85	61	89	78	1.6	6.3	1.1	3.0	6.8	7.3	6.8	7.0
V	–	–	–	–	8.0	11.6	7.7	8.8	13.7	3.7	22.3	19	-1.7	30	83	68	89	80	2.0	5.4	1.2	2.9	7.3	8.9	7.4	7.9
VI	–	–	–	–	–	–	–	–	23.9	6.0	30.6	24	1.9	27	–	–	–	–	–	–	–	–	4.2	6.4	5.7	5.4
VII	–	–	–	–	–	–	–	–	23.5	11.7	35.0	5	6.9	4	–	–	–	–	–	–	–	–	7.5	7.9	7.5	7.6
VIII	–	–	–	–	13.5	19.5	13.2	14.8	21.5	9.1	29.4	12	2.4	31	91	68	95	85	1.5	7.8	0.8	3.4	5.7	7.1	6.2	6.3
IX	–	–	–	–	9.4	15.3	9.8	11.1	16.9	6.0	27.3	9	-2.1	26	91	73	94	86	1.2	5.1	0.7	2.3	6.0	7.1	7.1	6.7
X	–	–	–	–	4.3	13.8	5.3	7.2	14.9	1.4	22.9	19	-3.7	3	95	64	96	85	0.4	6.2	0.5	2.4	6.1	4.9	3.5	4.8
XI	–	–	–	–	2.4	6.7	3.2	3.9	8.0	0.4	18.8	4	-11.0	30	90	76	89	85	0.8	3.1	0.9	1.6	7.2	6.8	6.9	7.0
XII	–	–	–	–	-2.5	0.7	-1.6	-1.2	2.2	-5.3	12.6	13	-14.1	11	89	79	88	85	0.6	1.5	0.7	0.9	7.7	7.2	6.9	7.3
Rok	–	–	–	–	–	–	–	–	12.8	2.1	35.0	5.VII	-18.4	17.1	–	–	–	–	–	–	–	–	6.9	7.0	6.5	6.8

Krosno

$\varphi = 49°42'$ $\lambda = 21°45'$

I	–	–	–	–	-2.1	-0.5	-2.1	-1.7	0.2	-3.6	5.1	3	-11.7	17	–	–	–	–	–	–	–	–	8.1	7.2	7.3	7.5
II	–	–	–	–	1.3	3.8	2.1	2.3	4.9	0.2	9.7	17	-5.7	28	–	–	–	–	–	–	–	–	9.0	8.0	6.9	8.0
III	–	–	–	–	-0.1	5.8	2.1	2.5	7.3	-4.7	17.0	31	-16.2	4	–	–	–	–	–	–	–	–	4.7	4.4	3.8	4.4
IV	–	–	–	–	5.5	12.5	8.0	8.5	13.8	3.4	25.4	30	-1.7	16	–	–	–	–	–	–	–	–	5.8	6.5	5.3	5.9
V	–	–	–	–	8.1	12.8	9.3	9.9	14.7	5.6	23.1	17,18,19	0.3	30	–	–	–	–	–	–	–	–	6.9	7.9	6.4	7.1
VI	–	–	–	–	15.9	23.2	16.8	18.2	25.2	11.4	33.0	12	4.9	1	–	–	–	–	–	–	–	–	4.1	4.3	3.1	3.8
VII	–	–	–	–	16.4	23.2	17.8	18.8	24.9	14.3	34.5	8	9.1	4	–	–	–	–	–	–	–	–	7.0	5.7	5.9	6.2
VIII	–	–	–	–	14.2	20.7	15.5	16.6	22.0	11.2	30.5	14	6.3	27,31	–	–	–	–	–	–	–	–	5.2	5.4	5.4	5.3
IX	–	–	–	–	10.0	15.9	11.4	12.2	17.1	8.0	26.7	9	-0.6	26	–	–	–	–	–	–	–	–	7.1	6.7	6.4	6.7
X	–	–	–	–	5.7	13.4	7.7	8.6	14.3	4.0	19.5	14	-2.9	3	–	–	–	–	–	–	–	–	5.6	4.7	3.9	4.7
XI	–	–	–	–	3.8	6.6	3.6	4.4	7.8	1.9	17.2	9	-8.9	30	–	–	–	–	–	–	–	–	6.9	6.6	5.9	6.5
XII	–	–	–	–	-1.8	-0.2	-1.3	-1.2	1.1	-3.4	16.0	14	-9.5	11	–	–	–	–	–	–	–	–	6.4	6.8	4.9	6.0
Rok	–	–	–	–	6.4	11.4	7.6	8.2	12.8	4.3	34.5	8.VII	-16.2	4.III	–	–	–	–	–	–	–	–	6.4	6.2	5.4	6.0

Jasło

$H_s = 240\ m$ $h_w = 16\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%D, %nD)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ 0°	Max ≤ 0°	Min < -10°	Max ≥ 25°	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	v ≥ 10	v ≥ 15	≡	≤ 2.5	◔	◕	●
I	2.5	2.8	4.5	3.3	2	3.2	1.5	3.0	38.5	6.7	1.5	3.7	13	5.2	14.5	3.4	15	4.4	34.9	13.4	6	26	11	3	-	11	7	1	6	1	-	-	-	13	21
II	4.5	4.3	1	1.0	3.5	1.6	2.5	4.6	42.5	5.6	1.5	1.3	9	2.4	7.5	3.7	12	3.7	28.1	11.7	25	10	2	-	-	11	8	1	3	-	2	-	1	13	6
III	4	3.1	11.5	2.2	8.5	5.1	3.5	4.7	16	5.0	2.5	2.2	10	4.5	9	3.2	28	2.8	42.0	14.8	18	17	4	2	-	9	7	1	1	-	4	1	10	6	7
IV	4.3	2.4	9.5	2.1	2.5	2.0	0.5	3.0	10	3.2	0.5	3.0	10.5	2.1	14.5	2.6	29	1.7	54.6	16.4	11	6	-	-	-	15	11	1	-	-	3	2	6	9	-
V	16.5	2.3	12.5	2.8	4	3.0	0.5	3.0	2.5	2.2	-	-	7.5	5.5	27.5	2.2	22	1.9	87.4	21.2	9	-	-	-	-	14	11	3	-	-	-	1	1	16	-
VI	4	3.0	3	2.5	3.5	2.4	1.5	3.0	18.5	4.7	2	1.0	9	2.3	17.5	2.9	31	2.2	75.2	46.4	12	-	-	-	13	11	8	1	-	-	1	3	6	2	-
VII	3	1.0	4.5	1.4	3	3.0	2	1.0	8.5	2.6	3.5	1.9	25	2.6	12.5	2.2	31	1.5	99.1	20.0	16	-	-	-	13	20	16	5	-	-	-	9	5	12	-
VIII	3.5	1.6	5	1.6	2	2.5	4	4.0	7	4.6	1.5	2.3	13	3.4	20	2.4	37	1.7	93.8	18.2	10	-	-	-	7	14	13	4	1	-	4	4	5	2	-
IX	3	1.8	5	1.7	2	1.2	1	2.0	14.5	4.4	2.5	2.6	21	4.7	12	3.5	29	2.5	92.3	16.5	3	-	-	-	2	15	14	3	1	-	5	1	3	12	-
X	4	2.2	8	1.4	2.5	1.6	3.5	2.3	16.5	4.2	3	1.3	12	2.3	9.5	2.5	34	1.7	24.7	8.5	23	-	-	-	-	4	4	-	1	-	15	-	10	5	-
XI	10	3.8	16	2.5	2	3.0	9.5	3.8	14	5.0	2.5	2.6	12.5	5.7	4.5	11.0	22	3.2	32.9	14.1	11	11	-	-	-	10	9	1	3	-	5	-	6	14	1
XII	8	3.4	9	3.1	1.5	3.0	1	6.0	39	6.3	3	2.8	7	4.4	10.5	3.2	14	4.1	20.3	5.8	5	27	-	1	-	12	6	-	2	-	1	-	5	11	7
Rok	76	2.4	89.5	2.1	37	2.6	31	3.4	227.5	4.5	24	2.1	149.5	3.6	156.5	3.6	304	2.6	682.3	46.4	12.VI	-	-	6	35	146	114	21	18	1	40	21	58	115	42

Zbyszyce

$H_s = 315\ m$ $h_w = 16\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98.7	25.2	15	-	-	-	-	17	11	4	-	-	-	6	1	14	-
VIII	15.5	1.4	1	1.0	2	1.5	2.6	1.8	38.5	1.5	3	1.3	7	2.4	11.5	1.5	12	1.4	69.9	28.5	28	-	-	-	-	15	11	3	-	-	-	5	-	3	-
IX	11	1.3	5	1.2	2	1.5	1	2.0	33	2.0	7	2.7	16	2.5	8	1.8	7	1.8	66.8	19.8	12	-	-	-	-	13	11	2	-	-	-	-	3	10	-
X	6	1.2	5	1.0	3	1.0	6	1.3	50	2.1	-	-	4	2.2	10	1.3	9	1.6	23.9	8.1	22	-	-	-	-	4	3	-	-	-	-	-	8	5	-
XI	4	10.5	9	2.0	8	1.2	5	2.2	40	3.8	8	2.6	6	2.8	1	10.0	9	3.1	26.8	17.1	11	-	-	-	-	6	4	1	3	-	-	-	6	14	-
XII	14	2.4	6	1.0	-	-	2	2.0	42	2.9	7	4.6	4	4.5	6	1.7	12	2.4	25.7	11.7	14	-	-	-	-	9	5	1	2	-	-	-	4	15	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Limanowa

$H_s = 440\ m$ $h_w = 16\ m$

I	1	1.5	5.5	2.5	9	4.2	25.5	3.6	12.5	3.2	3.5	2.7	18.5	5.5	12.5	4.8	5	3.8	29.7	7.7	6	28	9	8	-	17	8	-	1	-	1	-	-	18	27
II	5	2.8	1.5	1.0	10.5	4.8	26	4.6	9	4.9	5.5	2.6	16	5.2	9.5	3.8	1	4.3	31.7	6.1	25	19	2	1	-	12	8	-	2	-	-	-	2	16	10
III	4	2.0	·	·	10	4.2	30	3.0	4	2.6	6	3.2	13.5	7.1	13.5	3.9	12	3.4	51.2	17.6	24	19	3	5	-	14	6	1	3	-	-	1	5	10	14
IV	9.5	2.8	3.5	2.9	5	4.3	17	3.5	5.5	2.3	6	2.2	10	2.8	25.5	2.8	8	2.7	75.4	18.1	7	10	-	-	-	19	14	2	-	-	4	4	4	16	2
V	13	3.3	12.5	3.3	8	3.9	13	3.1	4	2.1	2	2.5	5.5	3.0	26	3.5	9	3.0	83.0	17.1	11	3	-	-	-	19	10	4	-	-	-	2	-	18	-
VI	5	2.9	5	2.1	5.5	2.1	19.5	2.8	5.5	3.5	1.5	1.0	9	4.4	20	3.2	19	2.4	44.9	15.4	8	-	-	-	11	12	8	2	-	-	-	6	5	4	-
VII	4	1.5	3.5	1.6	4	2.2	16	2.4	3	2.0	2.5	2.4	12.5	3.1	25.5	3.0	22	2.0	19.1.8	69.8	15	-	-	-	9	18	13	7	-	-	1	9	1	18	-
VIII	11	2.4	4.5	1.9	5	2.9	11.5	2.1	2	2.2	0.5	2.0	7.5	4.0	29	3.1	22	2.2	80.9	27.0	28	-	-	-	5	16	11	2	-	-	-	3	1	10	-
IX	3.5	1.9	1	2.0	4.5	2.4	10.5	2.5	1	2.5	4	1.9	26.5	4.8	18	3.6	21	2.8	60.6	14.4	4	2	-	-	2	16	12	1	1	-	1	-	3	12	-
X	4	2.1	1.5	2.3	10	2.3	15	2.3	7	2.1	12	2.9	4	3.4	15.5	2.3	24	1.8	31.2	9.4	20	8	-	-	-	5	4	-	-	-	3	-	5	6	-
XI	2	3.0	6.5	2.3	17	3.0	24.5	2.7	6	3.6	3.5	3.1	12.5	6.2	12	7.2	6	3.7	33.6	11.2	11	11	2	1	-	10	5	2	2	-	3	-	4	14	1
XII	5	1.8	2.5	2.0	5	3.6	31	3.6	8	2.2	6	3.2	13.5	5.2	18	4.0	4	3.5	17.9	5.6	8	26	8	3	-	14	7	-	2	-	2	-	2	17	11
Rok	67	2.3	47.5	2.0	93.5	3.3	239.5	3.0	67.5	2.8	53	2.5	149	4.5	225	3.8	153	3.0	731.9	69.8	15.VII	128	24	18	27	172	106	21	11	-	15	25	32	159	65

Krosno

$H_s = 270\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20.9	11.8	6	25	12	1	-	9	5	1	-	-	-	-	2	18	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.9	6.0	9	11	3	-	-	9	6	-	-	-	-	-	1	16	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.3	12.5	18	18	6	2	-	10	5	1	-	-	-	-	13	6	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.5	21.5	11	6	-	-	1	8	6	1	-	-	-	-	7	10	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	92.4	31.5	9	-	-	-	-	13	12	3	-	-	-	1	4	13	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	27.4	9.6	9	-	-	-	17	9	7	-	-	-	-	3	9	2	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	17.3.8	63.4	13	-	-	-	15	19	16	5	-	-	-	5	6	14	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	79.3	22.0	10	-	-	-	8	14	13	2	-	-	-	-	6	5	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	98.8	23.6	12	1	-	-	2	17	12	2	-	-	-	1	2	11	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.0	9.4	20	4	-	-	-	4	4	-	-	-	-	-	9	7	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.4	19.2	11	11	2	-	-	8	8	2	-	-	-	-	4	14	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.0	7.7	5	27	12	-	-	7	7	-	-	-	-	-	6	10	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	693.7	63.4	13.VII	103	35	3	43	127	101	17	-	-	-	10	69	128	-

Żywiec – Sporysz

$\varphi = 49°41'$ $\lambda = 19°13'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.9	1.3	-4.0	-0.5	2.6	-3.9	10.0	2	-19.9	17	83	73	81	79	1.0	2.0	1.1	1.4	7.9	6.7	6.9	7.2
II	–	–	–	–	1.5	5.2	2.8	3.1	7.0	-0.5	12.6	5	-10.6	23	84	70	79	78	1.2	2.9	1.8	2.0	7.6	7.5	5.7	6.9
III	–	–	–	–	0.8	8.0	3.6	4.0	9.6	-1.5	18.0	20	-11.5	4	81	59	78	73	1.5	5.2	2.1	2.9	6.0	5.5	5.1	5.6
IV	–	–	–	–	4.5	11.4	6.5	7.2	12.9	2.0	25.5	30	-4.0	14	88	58	84	77	1.1	7.3	1.8	3.4	6.0	6.7	6.7	6.5
V	–	–	–	–	7.8	12.7	8.6	9.4	14.6	4.6	24.1	16	-0.8	30	82	63	85	77	2.0	6.7	1.7	3.5	6.6	7.7	6.8	7.0
VI	–	–	–	–	15.0	22.6	15.8	17.3	24.0	9.9	31.5	11	3.4	27	84	52	83	72	3.3	14.3	3.3	7.0	4.1	5.0	3.7	4.3
VII	–	–	–	–	16.5	21.7	17.1	18.1	23.8	13.3	35.0	5,8	7.2	4	–	–	–	–	–	–	–	–	6.2	7.0	6.8	6.7
VIII	–	–	–	–	12.7	20.1	14.3	15.4	21.7	10.0	28.9	11	3.7	31	91	61	87	80	1.5	9.9	2.2	4.5	5.1	5.7	4.7	5.2
IX	–	–	–	–	9.8	15.5	11.0	11.8	16.9	7.5	26.6	9	-0.4	26	88	64	86	79	1.6	7.0	2.0	3.5	7.0	6.7	6.5	6.7
X	–	–	–	–	5.6	14.3	7.4	8.7	15.3	3.0	22.6	19	-3.5	3	90	58	88	79	1.0	7.2	1.5	3.2	5.4	4.1	3.3	4.3
XI	–	–	–	–	3.4	7.8	4.1	4.8	8.8	1.2	18.5	4	-10.8	30	84	68	82	78	1.6	4.1	1.7	2.5	7.4	6.3	6.7	6.8
XII	–	–	–	–	-1.5	1.4	0.1	0.0	3.0	-3.7	14.5	13	-13.9	11	82	78	80	80	1.2	1.7	1.4	1.4	6.5	7.0	6.9	6.6
Rok	–	–	–	–	6.2	11.8	7.5	8.2	13.4	3.5	35.0	5,8.VII	-19.9	17.1	–	–	–	–	–	–	–	–	6.3	6.3	5.8	6.1

Mszana Dolna I

$\varphi = 49°41'$ $\lambda = 20°04'$

I	–	–	–	–	-2.3	1.4	-1.8	-1.1	2.9	–	8.9	2	–	–	–	–	–	–	–	–	–	–	8.3	7.7	7.2	7.7
II	–	–	–	–	0.8	5.4	1.8	2.4	6.9	–	13.0	5	–	–	–	–	–	–	–	–	–	–	7.4	7.4	7.0	7.3
III	–	–	–	–	-0.8	7.5	2.7	3.0	9.3	–	16.0	14,23	–	–	–	–	–	–	–	–	–	–	6.5	5.5	5.3	5.8
IV	–	–	–	–	4.3	11.2	6.6	7.2	12.6	–	25.4	30	–	–	–	–	–	–	–	–	–	–	6.5	6.4	6.6	6.5
V	–	–	–	–	7.6	12.0	8.0	8.9	13.6	–	21.8	19	–	–	–	–	–	–	–	–	–	–	7.1	8.0	6.5	7.2
VI	–	–	–	–	15.6	22.4	14.4	16.7	24.1	–	31.6	11	–	–	–	–	–	–	–	–	–	–	4.6	5.7	3.3	4.5
VII	–	–	–	–	16.2	21.6	16.2	17.6	23.7	–	35.8	5	–	–	–	–	–	–	–	–	–	–	7.6	7.0	7.4	7.3
VIII	–	–	–	–	13.4	20.1	14.4	15.6	21.8	–	29.4	12	–	–	–	–	–	–	–	–	–	–	6.2	6.5	6.5	6.4
IX	–	–	–	–	9.3	15.6	11.4	11.9	17.2	–	27.0	9	–	–	–	–	–	–	–	–	–	–	7.1	6.1	6.8	6.7
X	–	–	–	–	5.1	14.1	7.4	8.5	15.4	–	24.4	19	–	–	–	–	–	–	–	–	–	–	6.7	4.8	3.5	5.0
XI	–	–	–	–	1.3	7.5	3.8	4.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	6.0	6.7
XII	–	–	–	–	-2.2	1.4	-0.9	-0.6	3.0	–	13.5	13	–	–	–	–	–	–	–	–	–	–	7.0	6.4	6.4	6.6
Rok	–	–	–	–	5.7	11.7	7.0	7.8	–	–	35.8	5.VII	–	–	–	–	–	–	–	–	–	–	6.9	6.5	6.0	6.5

Mszana Dolna II

$\varphi = 49°40'$ $\lambda = 20°05'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.6	15.4	10.8	11.6	–	–	–	–	–	–	87	63	84	78	1.7	7.2	2.1	3.7	6.9	6.4	6.6	6.6
X	–	–	–	–	5.2	13.9	6.6	8.1	–	–	–	–	–	–	91	61	89	80	0.9	6.7	1.1	2.9	5.0	4.0	3.0	4.0
XI	–	–	–	–	1.9	7.3	3.0	3.8	–	-0.2	–	–	-11.6	30	87	72	88	82	1.0	3.7	1.0	1.9	6.6	6.1	6.7	6.5
XII	–	–	–	–	-2.7	1.3	-1.2	-0.9	–	-4.6	–	–	-15.0	3	–	–	–	–	–	–	–	–	6.3	6.1	6.5	6.3
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Bircza

$\varphi = 49°41'$ $\lambda = 22°29'$

I	–	–	–	–	-2.0	0.1	-4.2	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.1	6.9	7.3
II	–	–	–	–	1.9	4.2	2.7	2.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.2	7.9	7.6
III	–	–	–	–	-1.4	5.1	1.1	1.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	3.6	5.0
IV	–	–	–	–	4.0	12.4	7.2	7.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.1	5.2	5.9
V	–	–	–	–	7.8	12.0	8.7	9.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.1	7.1	7.6
VI	–	–	–	–	15.8	22.0	16.2	17.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.8	5.9	5.5
VII	–	–	–	–	16.7	22.3	17.1	18.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	7.4	7.0
VIII	–	–	–	–	13.8	20.6	14.9	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	5.1	6.1
IX	–	–	–	–	9.4	15.6	11.2	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.8	7.0	7.5
X	–	–	–	–	5.7	13.6	6.7	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.6	3.4	5.4
XI	–	–	–	–	2.4	6.6	2.8	3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	6.4	6.9
XII	–	–	–	–	-1.6	0.7	-0.7	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	6.8	7.3
Rok	–	–	–	–	6.0	11.3	7.2	7.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.1	6.6

Żywiec – Śnorysz

$H_s = 360$ m $h_w = 14$ m **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, %nD]																	OPAD P			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr		=	≥0.5	◔	●	⊞
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Max<0°	Max<0°	Min<0°	Max>25°	≥0.1 mm	≥1.0 mm	≥10.0 mm	> 10	> 15					
I	1.5	1.0	6	2.9	2.5	1.4	3.5	1.1	10.5	3.0	24.5	3.6	5.5	3.8	3	5.5	36	1.9	33.7	7.1	6	23	7	5	·	12	8	·	3	·	–	·	2	15	20
II	0.5	1.0	1	1.0	1.5	1.3	6	1.8	18	2.6	22.5	2.9	6	3.6	3.5	4.9	25	1.8	32.5	12.4	25	16	1	1	·	14	9	1	·	·	–	·	2	10	6
III	1.5	1.3	4.5	2.0	5	1.1	4.5	1.0	11	1.5	11.5	2.5	7.5	3.1	7.5	1.4	40	1.1	3.56?	–	–	19	3	1	·	14	9	·	·	·	–	1	7	10	6
IV	3	1.3	7.5	1.7	4	1.8	2.5	1.8	1.5	1.7	6	2.0	4.5	3.4	11	2.6	50	1.0	68.5	22.4	7	10	·	·	1	16	12	2	1	1	–	2	5	13	1
V	3.5	1.3	10.5	2.1	12	1.9	3.5	1.7	3	1.8	2	2.2	5.5	2.2	10	2.3	43	1.1	65.9	29.7	20	1	·	·	·	10	7	3	·	·	–	3	1	13	·
VI	1	1.5	1.5	2.7	2.5	1.6	2	1.2	7.5	2.0	14.5	2.7	9.5	3.1	6.5	3.2	45	1.3	65.2	24.3	19	·	·	·	13	8	7	3	1	·	–	7	8	5	·
VII	·	·	1	5.0	2.5	1.8	8	1.8	7	1.9	13.5	1.9	10	2.5	8	1.8	43	1.1	49.7.7	48.4	16	·	·	·	12	23	18	5	·	·	–	9	3	11	·
VIII	1.5	1.0	1	1.0	2	1.5	0.5	3.0	3	2.5	12	2.1	13	2.0	10	2.0	50	0.9	84.2	24.3	28	·	·	·	6	15	13	1	·	·	–	2	3	5	·
IX	1.5	1.0	0.5	1.0	1	1.0	1.5	1.3	6	3.2	26.5	3.5	16	3.1	7	2.0	30	2.0	97.5	30.5	4	1	·	·	2	14	13	3	2	·	–	2	2	9	·
X	1.5	1.0	1.5	1.0	7	1.1	9.5	1.1	9.5	2.4	15.5	2.5	4.5	3.4	5	1.2	39	1.1	26.1	11.1	20	2	·	·	·	7	5	1	·	·	–	·	8	2	·
XI	3.5	3.1	8	1.9	5	1.6	7	1.7	9	1.8	13.5	2.9	3.5	3.7	2.5	4.2	38	1.4	21.7	9.5	28	10	1	1	·	8	5	·	1	·	–	·	6	15	1
XII	4	1.2	3.5	3.0	6	2.2	13.5	2.7	12.5	5.4	18	6.6	6.5	3.2	2	1.8	28	3.0	25.1	8.8	8	25	7	2	·	10	8	·	6	1	–	·	6	16	10
Rok	23	1.2	46.5	2.0	50	1.5	62	1.7	98.5	2.3	180	3.0	92	3.1	76	2.4	467	1.5	950.7?	48.4	16.VII	107	19	10	34	151	114	19	14	2	–	26	53	124	44

Mszana Dolna I

$H_s = 380$ m $h_w = 13$ m

I	·	·	4	2.8	1	4.0	4	3.2	12	3.2	7	5.7	8	3.9	1	1.0	56	1.5	28.7	7.8	6	–	7	–	·	10	7	·	1	·	–	·	1	16	21
II	·	·	·	·	·	·	3	1.3	14	4.4	12	4.6	3	5.7	2	4.0	50	1.7	43.9	13.9	25	–	1	–	·	11	7	2	1	·	–	·	3	14	8
III	·	·	5	2.2	5	3.2	2	3.5	3	4.3	9	5.2	5	3.0	1	1.0	63	1.2	43.9	7.9	18	–	3	–	·	11	9	·	2	·	–	1	6	9	10
IV	4	2.0	4	2.2	1	3.0	1	2.0	1	8.0	5	3.2	8	2.4	15	2.6	51	1.2	56.4	16.3	11	–	·	–	1	16	11	1	·	·	–	·	5	14	1
V	6	4.3	5	2.8	1	3.0	2	3.0	4	4.0	3	4.0	7	3.3	6	2.5	59	1.2	77.7	16.4	20	–	·	–	·	13	10	4	·	·	–	2	2	17	·
VI	3	3.7	1	2.0	·	·	·	·	1.5	4.1	5	3.4	·	·	8	2.8	58	1.2	30.6	5.8	22	–	·	–	12	8	8	·	·	·	–	1	7	2	·
VII	·	·	2	4.5	1	6.0	·	·	7	4.1	2	1.5	5	5.8	2	3.0	74	0.9	199.9	40.5	16	–	·	–	11	17	17	5	1	·	–	3	1	14	·
VIII	·	·	·	·	·	·	·	·	3	7.0	4	7.0	9	4.1	4	4.5	73	1.1	158.7	28.4	16	–	·	–	6	16	13	7	3	·	–	3	1	7	·
IX	1	4.0	·	·	·	·	·	·	1.1	5.4	2.2	6.0	1	4.0	4	5.0	51	2.4	113.3	20.5	4	–	·	–	2	17	14	4	4	·	–	1	2	13	·
X	·	·	1	4.0	1	4.0	2	1.5	1.6	4.4	5	3.6	·	·	5	3.0	63	1.2	36.2	11.3	23	–	·	–	·	6	5	1	·	·	–	·	4	5	·
XI	5	7.6	1	8.0	2	4.0	7	7.4	13	6.3	1	4.0	·	·	5	6.4	56	2.5	38.0	10.8	28	–	·	–	·	9	8	2	4	·	–	·	5	15	1
XII	4	3.5	5	4.0	1	6.0	2	3.0	2.4	7.0	6	9.3	·	·	·	·	51	2.9	33.9	8.6	5	–	7	–	·	10	7	·	5	·	–	·	·	13	11
Rok	2.3	2.1	2.8	2.7	1.3	2.9	2.3	2.1	12.3	5.2	8.1	4.8	4.6	2.7	5.3	3.0	70.5	1.6	861.2	40.5	16.VII	–	–	–	32	144	116	26	21	·	–	11	37	139	52

Mszana Dolna II

$H_s = 410$ m $h_w = 16$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	3.5	2.6	3.5	1.7	4.5	2.0	5	1.0	13	2.1	15	2.2	9.5	2.4	7	2.7	29	1.4	75.0	11.2	18	–	–	–	–	17	13	2	·	·	1	·	4	11	·
X	2.5	1.0	3.5	1.1	5	1.6	7	1.6	9	1.8	9.5	1.6	5.5	1.2	2	1.2	49	0.7	30.0	11.0	22	–	–	–	–	7	4	1	·	·	1	·	10	4	·
XI	5	4.2	1.0	1.7	5	2.1	7	1.8	5.5	2.4	9	2.0	5.5	2.5	6	4.1	37	1.5	41.0	15.2	29	11	–	1	–	10	6	1	1	·	2	·	7	15	1
XII	4.5	2.8	8	2.2	6	2.5	13	1.6	9.5	2.5	16.5	3.1	2.5	1.4	1.0	2.1	23	1.8	32.2	7.3	5	26	–	2	–	9	8	·	·	·	3	·	7	15	10
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Bircza

$H_s = 300$ m $h_w = 16$ m

I	2.5	1.8	3.5	2.4	6.5	4.1	8.5	2.3	4.5	2.0	25.5	6.0	18	4.0	3	4.3	24	2.9	16.8	3.1	6	–	–	–	–	12	8	·	·	·	–	–	1	11	23?
II	5	2.7	·	·	3	4.3	4	4.5	13	6.1	23	6.9	12	4.9	7	2.2	19	3.9	34.0	6.1	26	–	–	–	–	19	10	·	5	2	–	–	1	14	9
III	5	4.4	3.5	3.7	10.5	6.0	1	4.5	3	6.3	8.5	5.1	13	5.9	7.5	6.3	41	3.1	42.2	13.5	18	–	–	–	–	11	9	1	4	1	–	–	7	8	14
IV	4.5	3.1	8.5	3.6	9	4.1	3.5	4.3	3	2.7	2	1.8	9.5	2.7	8	2.2	42	1.7	46.8	24.1	11	–	–	–	–	11	10	1	·	·	–	–	5	8	2
V	9	2.9	10.5	3.4	11	5.4	3	2.5	·	·	1.5	2.3	12.5	2.6	8.5	2.6	37	2.0	108.4	32.6	6	–	–	–	–	16	12	3	·	·	–	–	·	16	1
VI	4.5	2.0	1	1.0	3	2.3	3.5	2.1	8	3.1	9	4.1	9	2.8	12	2.3	40	1.5	87.7	21.8	4	–	–	–	–	9	9	4	·	·	–	–	4	3	·
VII	3	2.5	2.5	1.6	4.5	2.8	3.5	2.3	2	3.0	17	3.3	12.5	3.2	8	3.1	33	1.9	77.3	14.2	27	–	–	–	–	16	15	1	·	·	–	–	·	13	·
VIII	4	2.1	4.5	1.7	2.5	3.0	3	2.8	2.5	2.2	10	3.5	16.5	3.4	8	2.5	46	1.5	48.0	11.7	29	–	–	–	–	17	12	1	·	·	–	–	1	6	·
IX	1	1.0	·	·	3	3.3	1	2.0	4.5	2.9	12	4.4	22.5	4.0	8	2.9	36	2.1	130.3	35.8	3	–	–	–	–	17	15	5	·	·	–	–	2	16	·
X	3	1.7	·	·	1	5.0	4.5	2.2	0.5	2.0	11.6	4.0	17.5	3.7	3	2.8	52	1.5	16.9	8.0	20	–	–	–	–	6	4	·	·	·	–	–	3	4	·
XI	2	3.2	8.5	3.1	9.5	5.5	9.5	3.2	6.5	3.4	6.5	3.9	11	6.0	9.5	5.7	27	3.2	43.6	19.9	28	–	–	–	–	10	6	2	2	·	–	–	3	15	1
XII	8.5	3.2	4.5	4.0	4.5	4.6	5	2.7	5.5	5.2	34	4.3	10	2.7	3	3.2	48	3.0	25.0	5.6	5	–	–	–	–	10	8	·	2	1	–	–	2	11	11
Rok	5.0	2.7	4.4	2.0	6.8	4.2	5.0	3.0	5.0	3.2	16.0.5	4.0	17.1	3.8	8.5.5	3.3	416	2.4	674.0	35.8	3.IX	–	–	–	–	154	118	18	13	4	–	–	29	125	61?

Wisła

$\varphi = 49°39'$ $\lambda = 18°52'$ **1957**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.5	0.5	-1.6	-1.3	1.6	-4.8	7.9	2	-20.1	17	–	–	–	–	–	–	–	–	8.1	7.5	6.9	7.5
II	–	–	–	–	0.2	4.4	1.5	1.9	5.3	-2.1	11.0	5	-13.6	23	–	–	–	–	–	–	–	–	7.5	7.5	6.1	7.0
III	–	–	–	–	-0.4	7.2	2.3	2.8	8.1	-2.7	16.0	14	-12.0	6	–	–	–	–	–	–	–	–	5.3	5.0	5.2	5.2
IV	–	–	–	–	4.1	10.3	5.3	6.2	11.5	0.8	23.5	2	-5.1	14	–	–	–	–	–	–	–	–	5.2	6.7	6.9	6.3
V	–	–	–	–	7.7	11.8	7.9	8.8	13.2	3.5	23.4	19	-1.5	30	–	–	–	–	–	–	–	–	6.8	7.8	6.9	7.2
VI	–	–	–	–	15.1	21.6	15.3	16.8	23.2	9.3	30.0	11	1.7	27	–	–	–	–	–	–	–	–	3.7	5.8	3.9	4.5
VII	–	–	–	–	16.1	20.7	16.5	17.4	22.4	12.4	34.0	5	7.7	19	–	–	–	–	–	–	–	–	6.9	7.1	6.6	6.9
VIII	–	–	–	–	12.3	18.8	13.4	14.5	19.9	8.6	26.8	12	2.7	31	–	–	–	–	–	–	–	–	5.8	6.6	5.1	5.8
IX	–	–	–	–	9.0	14.3	10.2	10.9	15.7	5.7	26.1	9	-1.8	26	–	–	–	–	–	–	–	–	6.3	7.7	6.8	6.9
X	–	–	–	–	6.0	13.3	6.7	8.2	14.2	2.7	20.7	9	-3.9	3	–	–	–	–	–	–	–	–	5.2	4.8	3.6	4.5
XI	–	–	–	–	3.1	7.2	3.5	4.3	8.1	0.7	16.8	4	-12.0	30	–	–	–	–	–	–	–	–	7.4	6.5	6.9	6.9
XII	–	–	–	–	-1.1	0.7	-0.8	-0.5	2.3	-4.0	14.0	13	-14.2	11	–	–	–	–	–	–	–	–	7.6	7.9	6.8	7.4
Rok	–	–	–	–	5.8	10.9	6.7	7.5	12.1	2.5	34.0	5.VII	-20.1	17.1	–	–	–	–	–	–	–	–	6.3	6.7	6.0	6.3

Jordanów

$\varphi = 49°39'$ $\lambda = 19°50'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.4	4.6	2.0	2.2	6.1	-1.3	12.5	5	-11.6	23	86	69	82	79	1.0	3.0	1.4	1.8	–	–	–	–
III	–	–	–	–	-0.7	6.7	2.7	2.8	8.5	-2.4	16.1	14	-15.1	4	82	61	81	75	1.2	4.7	1.7	2.5	5.4	4.7	5.0	5.0
IV	–	–	–	–	3.9	10.3	6.1	6.6	11.7	1.6	24.5	30	-7.5	14	86	60	80	75	1.3	6.6	2.0	3.3	5.8	6.7	7.1	6.5
V	–	–	–	–	6.9	11.4	8.5	8.8	13.0	4.0	21.5	16,19	-4.0	30	82	63	78	74	1.9	6.0	2.5	3.5	7.5	7.7	7.8	7.7
VI	–	–	–	–	13.5	21.6	16.4	17.0	23.2	9.1	30.1	11	2.0	27	78	50	70	66	3.7	14.0	5.8	7.8	2.8	4.4	4.2	3.8
VII	–	–	–	–	14.9	20.8	17.3	17.6	22.4	12.6	34.6	5	6.9	30	87	63	78	76	2.3	10.4	4.8	5.8	6.5	7.4	6.8	6.9
VIII	–	–	–	–	11.9	19.1	14.8	15.2	20.9	10.0	29.1	12	4.3	31	–	–	–	–	–	–	–	–	4.6	6.8	5.6	5.7
IX	–	–	–	–	8.9	14.7	10.8	11.3	16.2	6.7	26.1	8.9	-1.7	26	86	62	81	76	1.8	6.9	2.6	3.8	5.7	6.4	6.0	6.0
X	–	–	–	–	5.6	13.9	7.7	8.7	14.9	3.0	23.5	19	-2.5	3	–	–	–	–	–	–	–	–	4.7	3.6	3.6	4.0
XI	–	–	–	–	1.9	6.8	3.1	3.7	7.7	-0.1	18.5	1	-12.2	30	–	–	–	–	–	–	–	–	6.1	5.9	6.7	8.2
XII	–	–	–	–	-2.0	0.7	-1.2	-0.9	1.9	-4.7	12.1	13	-11.7	3,11	–	–	–	–	–	–	–	–	6.5	6.4	6.2	6.4
Rok	–	–	–	–	–	–	–	–	–	–	34.6	5.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lubań Wielki

$\varphi = 49°39'$ $\lambda = 19°59'$

I	–	–	–	–	-4.1	-2.5	-3.4	-3.4	-1.2	-6.6	4.1	2,23	-19.5	17	–	–	–	–	–	–	–	–	6.8	7.1	6.8	6.9
II	–	–	–	–	-2.0	0.5	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	6.2	7.0
III	–	–	–	–	-1.1	2.6	-0.1	0.3	4.1	-3.3	11.5	27	-14.9	1	–	–	–	–	–	–	–	–	6.0	5.6	4.7	5.4
IV	–	–	–	–	3.3	6.6	3.7	4.3	8.2	0.5	21.8	30	-7.5	14	–	–	–	–	–	–	–	–	5.8	6.7	6.8	6.4
V	–	–	–	–	4.6	7.2	5.1	5.5	9.1	2.2	17.0	20	-3.7	7	–	–	–	–	–	–	–	–	7.2	8.4	7.5	7.7
VI	–	–	–	–	13.1	17.4	13.9	14.8	19.4	9.5	26.3	11	3.9	27	–	–	–	–	–	–	–	–	3.5	6.1	5.1	4.9
VII	–	–	–	–	13.2	16.8	14.0	14.5	18.5	10.8	30.4	5	6.7	17,24,28	–	–	–	–	–	–	–	–	7.1	7.4	7.0	7.2
VIII	–	–	–	–	11.5	15.2	12.3	12.8	17.3	6.7	26.9	11	4.2	23,31	–	–	–	–	–	–	–	–	4.6	7.1	7.0	6.2
IX	–	–	–	–	6.6	10.7	8.1	8.4	12.4	4.8	23.0	9	-2.6	27	–	–	–	–	–	–	–	–	6.4	7.0	6.3	6.6
X	–	–	–	–	4.6	8.9	6.2	6.5	10.4	2.7	19.2	19	-2.5	6	–	–	–	–	–	–	–	–	5.0	4.0	4.0	4.3
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-4.5	-2.6	-3.8	-3.7	-1.1	-7.1	7.7	13	-15.6	1	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wysokie

$\varphi = 49°39'$ $\lambda = 20°34'$

I	–	–	–	–	-3.4	-1.3	-2.6	-2.5	0.8	-5.3	5.8	7	-14.8	17	–	–	–	–	–	–	–	–	7.5	6.5	6.5	6.8
II	–	–	–	–	0.1	2.5	1.1	1.2	4.1	-2.6	9.1	6	-7.9	28	–	–	–	–	–	–	–	–	7.0	6.4	7.0	6.8
III	–	–	–	–	0.6	4.9	2.4	2.6	–	-2.6	–	–	-10.9	4	–	–	–	–	–	–	–	–	5.9	5.0	5.5	5.5
IV	–	–	–	–	5.6	9.4	7.0	7.2	–	2.7	–	–	-4.6	16	–	–	–	–	–	–	–	–	5.5	6.9	7.0	6.5
V	–	–	–	–	6.7	10.3	7.7	8.1	–	4.2	–	–	-2.3	9	–	–	–	–	–	–	–	–	6.9	7.9	7.1	7.3
VI	–	–	–	–	15.7	19.8	16.0	16.9	–	11.9	–	–	3.9	7	–	–	–	–	–	–	–	–	3.5	6.2	4.7	4.5
VII	–	–	–	–	16.2	23.2	16.7	18.8	–	13.2	–	–	9.8	17	–	–	–	–	–	–	–	–	6.8	6.8	6.4	6.7
VIII	–	–	–	–	13.5	17.9	14.7	15.2	–	11.2	–	–	6.6	24	–	–	–	–	–	–	–	–	4.7	6.1	6.2	5.7
IX	–	–	–	–	9.7	14.0	11.0	11.4	–	7.5	–	–	2.2	27	–	–	–	–	–	–	–	–	5.9	6.6	7.1	6.5
X	–	–	–	–	6.4	11.7	8.2	8.8	–	4.9	–	–	-0.8	3	–	–	–	–	–	–	–	–	5.0	4.4	3.6	4.3
XI	–	–	–	–	2.5	5.2	3.0	3.4	–	0.6	–	–	-12.4	30	–	–	–	–	–	–	–	–	6.9	6.3	6.6	6.6
XII	–	–	–	–	-3.2	-1.5	-3.0	-2.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	6.4	6.5
Rok	–	–	–	–	8.9	8.7	6.8	7.5	–	–	–	–	-14.8	17.1	–	–	–	–	–	–	–	–	6.0	6.2	6.2	6.1

Wisła

$H_s = 430\,m$ $h_w = 16\,m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °/0, °/00																		OPAD R			LICZBA DNI (n)																
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10°	Max≥25°	≥0.1	≥1.0	≥10.0	≥10	≥15							
I	12	2.0	3	1.0	1	1.0	11	2.6	39	2.5	3	2.0	1	1.0	21	2.1	2	2.2	44.4	19.7	6	25	8	4	·	15	9	1	·	·	·	·	2	20	-			
II	9	1.6	·	·	·	·	10	1.9	40	2.8	9	1.6	1	2.0	13	1.5	2	2.1	61.8	11.6	25	18	1	2	·	16	10	1	·	·	·	·	2	12	-			
III	17	1.5	2	1.0	·	·	13	2.1	23	2.3	·	·	·	·	28	2.1	10	1.8	45.5	12.4	16	19	3	3	·	14	7	1	1	·	·	1	8	11	-			
IV	30	1.7	3	1.3	·	·	3	1.3	14	1.9	3	3.3	2	1.5	32	1.9	3	1.8	44.5	8.7	7	15	·	·	·	20	12	·	·	·	5	2	5	13	-			
V	38	1.8	4	2.0	·	·	1	3.0	6	2.2	·	·	4	1.5	39	1.7	1	1.8	77.2	26.0	20	4	·	·	·	14	10	3	·	·	1	2	1	15	-			
VI	37.5	1.4	1	1.0	·	·	2	2.0	17	2.7	·	·	3	1.7	26.5	1.8	3	1.7	41.2	18.0	7	·	·	·	8	13	9	1	·	·	·	8	6	4	-			
VII	22.5	1.3	0.5	1.0	·	·	4	1.8	14	2.0	2	1.5	3	1.5	39	1.7	8	1.5	256.0	65.0	16	·	·	·	7	22	21	8	·	·	3	9	2	16	-			
VIII	25	1.6	2	1.0	·	·	3	2.3	8	2.8	·	·	4	1.5	37	1.8	14	1.5	101.5	32.7	28	·	·	·	4	15	13	3	1	·	1	3	4	6	-			
IX	18.5	1.6	2	1.0	·	·	6	1.3	17	2.5	1.5	3.3	5	2.2	34	1.7	6	1.7	107.1	16.4	29	2	·	·	1	22	16	5	·	·	·	·	2	12	-			
X	21.5	1.1	1	1.0	·	·	10.5	1.7	23	2.6	1.5	1.3	3	1.7	27.5	1.4	5	1.6	21.1	7.6	22	7	·	·	·	6	4	·	·	·	2	·	9	5	-			
XI	24.5	1.8	1	1.0	·	·	12	2.0	18.5	2.7	2.5	2.0	3.5	1.9	25	1.7	3	1.9	24.8	13.8	28	11	1	1	·	8	6	1	·	·	1	·	7	19	-			
XII	16.5	1.9	·	·	·	·	20	2.6	27.5	2.5	1	1.5	3.5	2.3	20.5	1.7	4	2.1	31.8	7.2	4	26	7	4	·	13	9	·	·	·	4	·	3	19	-			
Rok	27.2	1.6	12.5	0.9	1	0.1	95.5	2.0	24.7	2.5	23.5	1.4	33	1.6	342.5	1.8	61	1.8	850.7	65.0	16.VII	127	20	14	20	178	126	24	2	·	17	25	51	152	-			

Jordanów

$H_s = 500\,m$ $h_w = 16\,m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	39.8	9.8	5	-	-	-	·	-	-	·	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.6	10.2	25	16	2	1	·	13	9	1	-	-	-	-	-	-	-	-	-
III	4.5	2.6	11.5	2.2	3	2.7	8	1.8	5	1.8	6.5	3.5	5	2.9	7.5	3.4	42	1.4	40.7	12.4	16	16	3	5	·	12	7	1	·	·	·	1	10	10	-			
IV	5	3.5	8	2.9	4.5	2.1	3.5	2.8	2	3.5	2.5	4.6	6.5	2.6	9	3.7	49	1.4	47.1	15.1	7	11	·	·	·	14	10	1	·	·	2	1	6	15	-			
V	22.5	2.7	20	3.0	7	1.8	3	1.3	2.5	2.4	·	·	7	3.0	10	3.6	21	2.2	36.0	6.4	8	2	·	·	·	13	8	·	·	·	1	1	2	19	-			
VI	10	1.5	8	1.9	9	1.6	7.5	1.8	8.5	2.3	17.5	2.8	10	2.1	8.5	4.2	11	2.2	23.8	6.8	9	·	·	·	10	7	6	·	·	·	1	6	11	3	-			
VII	4.5	1.9	6	2.7	5.5	1.3	10	1.7	6	1.5	12.5	2.8	14.5	1.6	17	2.6	17	1.7	213.6	30.4	2	·	·	·	8	21	19	8	·	·	3	7	3	16	-			
VIII	12.5	2.2	9	2.4	2	1.2	6	1.9	9	1.8	10.5	3.0	12	2.4	20	2.6	12	2.1	66.1	16.6	17	·	·	·	5	10	10	3	·	·	6	3	4	6	-			
IX	4	2.5	3.5	1.6	4	1.9	11	1.7	6	3.3	14	3.3	16	3.4	7.5	2.7	24	2.0	43.2	6.3	4	1	·	·	2	15	10	·	·	·	4	·	7	12	-			
X	0.5	2.0	1.5	1.7	4	1.5	19.5	2.0	21	2.4	9	2.9	7.5	2.5	5	2.9	25	1.7	19.9	10.2	23	5	·	·	·	5	4	1	·	·	·	·	10	6	-			
XI	1.5	1.7	13.5	2.9	13	2.2	14.5	2.3	8.5	2.1	10	2.6	9	2.8	7	5.4	13	2.4	14.7	6.0	29	11	1	1	·	11	5	·	·	·	4	·	7	15	-			
XII	4.5	2.3	7	3.4	4.5	1.8	15.5	2.9	12	3.4	15.5	3.7	9	2.8	8	4.6	17	2.6	22.9	6.5	5	27	9	4	·	12	8	·	·	·	1	·	8	15	-			
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	597.4	30.4	2.VII	-	-	-	25	-	-	15	-	-	-	-	-	-	-	-	-

Luboń Wielki

$H_s = 1024\,m$ $h_w = 15\,m$

I	8.5	3.3	5	6.3	·	·	·	·	14	12.0	27.5	3.2	12	5.1	16	5.5	10	6.5	63.7	14.0	6	30	16	7	·	18	13	1	13	6	18	·	4	15	31			
II	3	3.3	1	6.0	·	·	·	·	9	9.3	41.5	6.8	8.5	5.1	17	3.0	4	5.7	55.1	15.8	21	-	-	-	·	16	9	2	9	3	15	·	3	16	28			
III	10	3.8	10	4.9	1.5	5.0	·	·	6.5	9.7	27.5	6.8	16.5	4.4	15	2.9	6	5.0	67.2	15.3	1	20	8	4	·	12	10	2	14	2	12	1	6	10	31			
IV	18.5	2.0	8	2.6	2.5	3.6	3.5	4.3	2	5.0	11.5	4.1	9	2.9	27	2.0	8	2.5	83.2	21.4	7	15	4	·	·	18	15	2	1	·	15	·	5	13	13			
V	36.5	3.7	20.5	4.1	2	3.0	·	·	4.5	4.7	5.5	1.9	2	1.8	17	2.9	5	3.2	75.2	25.1	20	13	3	·	·	18	11	2	3	·	19	2	2	18	5			
VI	13.5	2.7	14	3.8	1	1.0	·	·	12	4.4	26	4.8	6	4.0	13.5	3.0	2	3.8	64.1	12.6	5	·	·	·	3	13	9	4	3	1	5	4	6	4	·			
VII	14	1.6	9.5	1.7	1.5	2.3	5	1.4	8	2.4	15	3.7	11.5	2.9	25.5	3.0	3	2.5	284.6	60.1	16	·	·	·	5	22	19	9	1	·	17	4	1	14	·			
VIII	5.5	2.3	1.5	4.0	0.5	8.0	·	·	3	2.7	14.5	3.5	17	3.0	4.7	2.3	4	2.6	142.3	24.9	12	·	·	·	1	16	11	7	1	·	11	3	1	10	·			
IX	9	2.8	1.5	4.3	·	·	·	·	8.5	5.3	30.5	6.1	23.5	3.6	12	3.0	5	4.3	93.7	15.9	4	1	·	·	·	19	17	2	5	·	15	·	3	12	·			
X	1	1.0	1	2.0	1	6.0	·	·	5.5	5.0	39.5	4.5	27	4.8	14	4.6	4	3.0	38.3	11.0	22	7	·	·	·	8	6	2	2	1	6	·	12	6	·			
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	63.4	36.0	29	-	-	-	·	10	8	·	-	-	-	-	-	-	-			
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	38.5	7.0	10	29	19	5	·	15	10	·	-	-	18	·	-	-	13			
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1062.3	60.1	16.VII	-	-	-	9	185	138	33	-	-	-	-	-	-	-			

Wysokie

$H_s = 645\,m$ $h_w = 14\,m$

I	6	3.5	4	7.0	·	·	·	·	38.5	5.9	16.5	4.8	10	6.9	17	7.8	1	6.0	34.2	10.0	5	29	11	4	·	10	9	1	4	1	-	-	2	11	28			
II	6	3.0	·	·	·	·	1	8.0	43	6.7	20	4.8	5	3.4	9	5.3	·	5.7	21.3	4.2	14	21	4	·	·	9	9	·	8	1	-	·	2	12	10			
III	11	4.1	12	4.7	4	3.5	7.5	5.3	20.5	5.5	1	12.0	12	4.6	18	5.5	7	4.6	50.3	23.4	24	21	-	1	-	7	7	1	3	·	-	1	8	11	12			
IV	11	3.0	13	3.9	1	3.0	5.5	3.8	20.5	4.4	4	3.7	7.5	3.0	23.5	4.3	4	3.8	60.8	14.2	11	10	-	·	-	17	14	1	1	·	-	3	4	13	2			
V	18	3.8	21	4.1	·	·	2	2.3	10	3.7	4	2.5	14.5	3.4	17.5	4.2	6	3.6	72.2	17.3	10	5	-	·	-	14	13	2	·	·	-	2	2	15	·			
VI	10.5	4.3	5	2.8	3.5	2.6	6	5.3	23	6.2	5	3.6	17	2.9	16	3.5	4	4.1	39.6	6.2	12	·	·	·	-	15	12	·	3	2	-	11	5	3	·			
VII	4.5	1.9	3.5	3.0	0.5	5.0	7	3.1	21	3.8	21.5	3.2	12	1.1	21	3.8	2	3.2	199.2	59.5	15	·	·	·	-	19	16	6	3	2	-	11	2	12	·			
VIII	5.6	3.3	7.5	2.9	·	·	·	·	14.5	4.6	16	5.9	21.5	3.4	26	3.3	2	3.5	98.8	32.1	28	·	·	·	-	16	15	2	1	1	-	5	·	5	·			
IX	5	3.0	1	5.0	·	·	1	3.0	25	3.4	30	4.3	16	3.8	13	3.7	·	3.7	96.1	27.4	4	·	·	·	-	16	14	2	1	·	-	1	1	9	·			
X	4	1.2	3	2.0	·	·	2.5	3.8	5.1	2.9	11.5	2.5	7	2.4	13	2.2	1	2.6	35.5	15.5	22	1	·	·	-	6	3	2	·	·	-	·	10	4	·			
XI	8.5	7.7	11	3.2	0.5	2.0	3.5	3.7	48.5	4.6	12	8.0	6	4.0	4	4.5.0	1	4.7	30.7	9.5	11	16	-	1	-	8	8	·	4	4	-	·	5	14	1			
XII	12	4.8	·	·	2	3.5	4	5.8	47	5.6	13	2.4	4	3.5	11	5.9	·	5.4	16.7	5.7	5	-	-	-	-	8	5	·	8	3	-	·	4	13	10			
Rok	9.7	3.5	8.1	3.0	11.5	1.6	4.0	3.7	362.5	4.8	164.5	4.2	134.5	3.5	189	5.4	28	4.2	764.2	59.5	15.VII	-	-	-	-	145	125	17	36	14	-	34	45	122	63			

Aleksandrówka $\varphi = 49°38'$ $\lambda = 20°42'$ 1957.

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data												
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-3.3	0.8	-2.5	-1.9	-	-6.1	-	-	-15.8	21,22	92	79	92	88	0.5	1.5	0.4	0.8	8.7	7.6	7.2	7.8
II	-	-	-	-	1.0	5.2	2.7	2.9	-	-0.8	-	-	-6.8	1	92	72	86	83	0.6	2.7	1.2	1.5	8.5	7.1	7.5	7.7
III	-	-	-	-	0.1	7.3	3.1	3.4	-	-1.4	-	-	-12.3	4	88	62	82	77	0.9	4.9	1.6	2.5	6.7	5.8	6.5	6.0
IV	-	-	-	-	4.1	11.7	7.6	7.8	-	2.1	-	-	-2.1	10	93	65	85	81	0.4	6.2	1.7	2.2	7.7	7.7	7.0	7.5
V	-	-	-	-	7.6	12.5	9.5	9.8	-	4.7	-	-	-0.8	30	91	69	87	82	1.0	5.7	1.7	2.8	8.1	8.5	7.9	8.2
VI	-	-	-	-	15.3	22.6	16.8	17.9	-	9.8	-	-	3.2	7	83	52	80	72	3.2	14.3	4.3	7.3	5.0	6.0	5.8	5.6
VII	-	-	-	-	16.6	22.0	17.4	18.4	-	13.0	-	-	7.1	4,30	88	67	87	81	2.5	7.1	2.8	4.1	7.5	7.5	6.8	7.3
VIII	-	-	-	-	13.5	20.5	15.2	16.1	24.7	10.4	29.5	12	3.7	24	91	61	89	80	1.6	10.1	2.1	4.8	6.9	6.7	6.3	6.6
IX	-	-	-	-	9.7	16.1	11.3	12.2	-	7.7	-	-	-0.8	26	91	63	89	81	1.2	7.5	1.5	3.4	7.1	6.8	7.1	7.0
X	-	-	-	-	4.3	14.1	7.0	8.1	15.1	2.6	21.6	19	-3.8	3	91	55	90	79	0.9	7.7	1.2	3.3	7.3	5.1	4.9	5.8
XI	-	-	-	-	3.2	7.5	4.2	4.8	-	1.5	-	-	-9.3	30	82	67	81	77	1.7	4.2	1.9	2.6	7.2	6.5	7.1	6.9
XII	-	-	-	-	-2.3	1.5	-0.9	-0.6	-	-4.3	-	-	-13.3	11	86	72	83	80	0.9	2.1	1.1	1.4	7.2	6.9	6.5	6.9
Rok	-	-	-	-	5.8	11.8	7.5	8.2	-	3.3	-	-	-15.8	21,22.1	89	65	86	80	1.3	6.2	1.8	3.1	7.3	6.8	6.6	6.9

Zawoja $\varphi = 49°37'$ $\lambda = 19°31'$

I	-	-	-	-	-2.5	1.1	-1.5	-1.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.1	5.8	6.5
II	-	-	-	-	0.8	3.6	1.5	1.8	5.4	-1.4	13.7	5	-10.9	28	-	-	-	-	-	-	-	-	6.4	7.1	5.9	6.5
III	-	-	-	-	-0.4	5.5	1.7	2.1	7.2	-2.3	14.6	27	-12.9	4	-	-	-	-	-	-	-	-	5.0	6.2	5.0	5.1
IV	-	-	-	-	4.1	8.4	4.8	5.5	10.2	1.5	21.5	30	-7.6	14	-	-	-	-	-	-	-	-	4.9	6.7	6.8	6.1
V	-	-	-	-	6.5	9.4	6.8	7.4	11.5	3.5	20.1	16	-1.4	5	-	-	-	-	-	-	-	-	6.8	8.5	7.4	7.6
VI	-	-	-	-	15.7	19.5	15.2	16.4	21.2	9.5	27.9	11	3.2	1	-	-	-	-	-	-	-	-	3.9	5.4	4.2	4.5
VII	-	-	-	-	15.9	19.3	15.4	16.5	21.4	12.1	34.0	8	7.2	29	-	-	-	-	-	-	-	-	6.6	7.3	6.7	6.9
VIII	-	-	-	-	13.0	17.0	13.2	14.1	19.2	9.7	28.6	14	3.9	31	-	-	-	-	-	-	-	-	4.9	7.0	5.9	5.9
IX	-	-	-	-	8.7	12.6	9.3	10.0	14.3	6.3	23.8	9	-1.1	26,27	-	-	-	-	-	-	-	-	6.2	6.3	6.2	6.2
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	2.2	5.2	2.6	3.2	8.1	0.7	18.2	10	-13.3	30	-	-	-	-	-	-	-	-	6.0	5.8	6.2	6.0
XII	-	-	-	-	-2.4	0.5	-1.5	-1.2	3.6	-4.9	16.9	13	-13.3	11	-	-	-	-	-	-	-	-	6.6	6.3	6.0	6.3
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Świniarsko $\varphi = 49°37'$ $\lambda = 20°39'$

I	-	-	-	-	-2.7	0.4	-1.9	-1.5	1.4	-5.4	6.2	8,9	-17.0	17	-	-	-	-	-	-	-	-	8.4	7.5	5.6	7.1
II	-	-	-	-	1.1	5.6	2.5	2.9	6.7	-1.0	11.2	6,21	-8.7	27	-	-	-	-	-	-	-	-	8.6	7.5	6.8	7.6
III	-	-	-	-	0.1	7.5	2.9	3.4	9.4	-2.3	17.6	14	-14.5	4	-	-	-	-	-	-	-	-	6.3	6.3	5.1	5.9
IV	-	-	-	-	3.8	12.3	7.1	7.6	13.7	1.4	24.5	30	-3.7	5	-	-	-	-	-	-	-	-	6.5	7.4	7.4	7.1
V	-	-	-	-	7.7	13.2	8.8	9.6	14.7	3.9	23.0	13	-2.1	30	-	-	-	-	-	-	-	-	7.6	8.8	8.7	7.7
VI	-	-	-	-	15.5	23.2	15.8	17.6	24.5	8.3	30.5	11,30	1.4	7	-	-	-	-	-	-	-	-	5.5	5.7	5.4	5.5
VII	-	-	-	-	16.6	22.6	17.0	18.3	24.6	11.7	35.5	5	6.2	4	-	-	-	-	-	-	-	-	7.3	7.9	7.1	7.4
VIII	-	-	-	-	13.8	21.0	15.3	16.3	22.5	9.6	31.7	12	2.3	24	-	-	-	-	-	-	-	-	6.2	6.7	5.7	6.2
IX	-	-	-	-	9.8	16.7	11.3	12.3	17.7	6.5	28.1	9	-2.1	26	-	-	-	-	-	-	-	-	6.9	7.6	7.4	7.3
X	-	-	-	-	4.6	14.6	7.3	8.4	15.8	1.3	21.5	19	-4.9	3	-	-	-	-	-	-	-	-	6.2	5.0	3.5	4.9
XI	-	-	-	-	3.2	7.8	4.1	4.8	8.6	0.7	18.4	4	-10.7	30	-	-	-	-	-	-	-	-	7.8	6.5	7.1	7.1
XII	-	-	-	-	-2.0	1.0	-0.7	-0.6	2.4	-4.8	12.6	13	-14.4	11	-	-	-	-	-	-	-	-	7.5	7.1	7.3	7.3
Rok	-	-	-	-	6.0	12.2	7.5	8.3	13.5	2.5	35.5	5.VII	-17.0	17.1	-	-	-	-	-	-	-	-	7.1	7.0	6.3	6.8

Nowy Sącz $\varphi = 49°37'$ $\lambda = 20°42'$

I	985.7	996.5	969.0	1023.3	-3.3	0.7	-2.3	-1.8	2.3	-4.9	8.9	2	-14.6	22	86	70	87	81	0.7	2.0	0.7	1.1	7.8	7.3	6.4	7.2
II	976.9	993.6	953.9	1013.8	1.1	6.7	2.8	3.1	7.3	-0.1	14.9	6	-5.7	24	85	61	76	74	1.1	3.9	2.0	2.3	8.0	7.7	7.7	7.8
III	982.6	992.0	964.4	1019.7	0.5	7.5	3.4	3.7	9.7	-0.9	18.7	14	-12.7	4	81	54	72	69	1.4	5.8	2.5	3.2	6.6	6.2	6.1	6.0
IV	984.7	993.3	958.5	1018.1	4.1	12.1	8.1	8.1	14.0	2.9	25.2	30	-1.6	5	91	58	75	75	0.8	7.2	3.0	3.7	6.5	7.1	6.7	6.8
V	979.6	987.9	969.1	1015.6	7.2	13.0	9.7	9.9	15.2	5.0	23.5	13,20	0.2	30	88	64	84	78	1.2	6.7	2.5	3.5	6.9	8.2	7.4	7.5
VI	981.9	994.5	965.9	1017.1	14.7	23.3	17.7	18.4	25.4	10.8	32.0	11	4.3	7	87	54	76	72	2.5	14.4	5.2	7.4	4.7	6.3	5.9	5.6
VII	978.0	988.7	967.8	1012.9	16.3	22.5	18.1	18.8	24.9	13.8	36.7	5	8.5	29	91	65	85	80	4.9	11.4	3.3	5.5	6.6	7.7	6.7	7.0
VIII	980.2	989.8	967.3	1015.6	13.3	21.1	15.7	16.4	22.9	11.3	34.1	12	5.7	31	93	59	86	79	4.3	11.1	2.7	5.0	5.1	6.1	4.8	5.3
IX	979.4	987.7	966.5	1015.3	9.8	16.6	11.6	12.2	18.0	7.8	28.3	9	-0.5	26	92	61	88	80	1.0	7.7	1.6	3.4	6.7	6.7	6.1	6.7
X	985.3	993.8	970.6	1021.9	4.4	11.4	7.7	8.6	15.8	3.0	23.0	19	-3.9	3	94	60	89	81	0.6	7.0	1.3	3.0	5.5	4.4	3.3	4.4
XI	984.7	1002.4	970.8	1021.7	3.4	7.6	4.5	5.0	8.9	2.0	19.5	4	-9.5	30	84	71	84	80	1.5	3.8	1.7	2.3	7.2	6.3	7.4	7.0
XII	980.1	998.9	946.7	1017.7	-1.9	1.5	-0.8	-0.4	2.9	-3.8	14.1	13	-11.5	11	85	73	86	80	0.9	2.1	1.1	1.4	7.4	7.8	7.1	7.4
Rok	981.3	1002.4	946.7	1017.7	5.8	12.2	8.0	8.5	15.1	3.2	36.7	5.VII	-14.6	22.1	88	62	82	77	1.2	6.9	2.3	3.5	6.9	6.8	6.8	6.6

Aleksandrówka

$H_s = 280$ m $h_w = 18$ m **1957**

MIESIĄC	ROZKŁAD WIATRU (%, ‰D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min <0°	Max <0°	Min <-10°	Max >25°	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	v ≥15	≡	≥0.5	≈	●	≋
I	2	2.0	3	2.3	0.5	2.0	2	2.8	6.5	3.6	6.5	3.1	10.5	3.5	6	3.6	56	1.3	28.3	7.5	6	27	-	8	-	11	8	-	2	-	-	-	-	14	24
II	1.5	4.7	1	1.0	·	·	6	5.3	14.5	6.1	12.5	4.0	3	4.7	6.5	4.5	39	2.6	21.4	6.7	25	19	-	·	-	9	5	·	3	2	-	·	·	12	7
III	2.5	2.0	4.5	1.9	4	2.4	2.5	4.8	6.5	3.3	7	2.8	8.5	4.8	9.5	4.2	46	1.7	39.1	18.9	24	17	-	1	-	10	6	1	1	·	-	1	1	8	6
IV	5.5	2.7	2	1.2	4.5	1.9	2.5	4.0	2	2.5	1	8.0	2.5	2.6	10	3.0	60	1.0	62.1	18.5	11	9	-	·	-	17	10	2	·	·	-	2	1	15	·
V	1.0	1.3	6	2.1	0.5	3.0	·	·	1	2.0	1	2.0	7.5	3.5	14	2.4	53	1.0	100.3	20.3	10	1	-	·	-	15	12	5	·	·	-	1	·	18	·
VI	4.5	1.3	0.5	1.0	3.5	1.6	3	7.8	6.5	6.5	3	1.7	5	2.7	13	3.1	51	1.5	37.9	7.6	12	·	-	·	-	13	12	·	2	1	-	5	1	4	·
VII	3	2.0	0.5	1.0	2	3.5	3	3.5	2.5	2.8	0.5	5.0	4	1.9	5.5	2.7	72	0.5	120.9	23.5	16	·	-	·	-	18	10	6	·	·	-	5	·	11	·
VIII	4	1.9	1	2.0	1	3.0	1.5	7.0	4.5	3.2	3	3.8	5	3.5	10	2.4	63	1.0	102.7	30.7	28	·	·	·	5	18	11	3	2	1	-	3	·	8	·
IX	1.5	2.0	0.5	2.0	0.5	2.0	1.5	3.3	3	3.0	8	3.6	10	4.4	7	4.0	58	1.3	73.4	22.5	4	1	-	·	-	14	12	2	1	·	-	·	1	10	·
X	0.5	3.0	1	3.0	·	·	2.5	2.0	4	2.2	5.5	1.7	6	2.8	4.5	2.9	69	0.6	33.9	11.4	20	4	·	·	·	4	3	3	·	·	-	·	1	8	·
XI	2.5	1.2	6	1.9	9	1.7	8	3.8	9	4.2	6	1.9	10.5	5.0	4	8.2	35	2.2	37.0	11.7	11	10	-	·	-	7	4	2	3	2	-	·	3	14	·
XII	4.5	2.3	2	2.0	2.5	3.8	3.5	7.9	4.5	4.1	13.5	5.0	7	3.1	9.5	4.1	46	2.1	19.1	8.0	14	25	-	4	-	10	5	·	3	1	-	·	2	12	3
Rok	4.2	2.2	2.8	1.8	2.8	2.1	3.6	4.4	6.4.5	3.6	6.7.5	3.6	7.9.5	3.5	9.9.5	3.8	650	1.4	674.1	30.7	28.VIII	113	-	10	-	146	98	24	17	7	-	17	10	132	40

Zawoja

$H_s = 670$ m $h_w = 17$ m

I	4	1.5	·	·	·	·	2.5	1.2	11	5.1	8	4.1	14.5	2.0	5	1.5	48	1.4	56.7	22.3	6	-	-	-	·	11	10	1	1	1	5	·	4	15	25
II	4.5	1.2	·	·	·	·	·	·	16.5	8.5	2.4	4.6	7.5	2.7	4.5	1.4	27	3.4	52.9	10.2	25	15	3	1	·	14	13	1	6	2	1	·	3	11	9
III	1.3	1.3	1.5	1.6	·	·	·	·	3	6.3	1.3	3.4	4.5	2.3	6	1.5	52	1.1	113.8	27.7	19	17	4	3	·	10	9	4	1	·	1	1	9	10	13
IV	15.5	1.5	1	1.0	2	1.7	1.5	3.3	5.5	5.6	3.5	1.7	1	1.5	3	1.5	57	0.8	75.3	24.0	7	8	·	·	·	15	13	2	·	·	7	2	5	11	6
V	20.5	1.8	7	1.7	1.5	1.7	·	·	2.5	5.0	4.5	1.0	1	1.0	10	1.1	46	0.9	61.2	10.6	8	4	·	·	·	13	11	1	·	·	2	2	1	16	1
VI	14.5	1.9	2	1.0	1	1.0	3	5.2	6	4.7	2.3	4.0	7.5	2.3	8	2.6	25	2.3	38.0	13.9	22	·	·	·	5	15	6	1	1	·	1	5	6	3	·
VII	10.5	1.6	1.5	2.3	0.5	3.0	0.5	2.0	4.5	2.3	2.2	2.2	12.5	1.9	4	2.1	37	2.1	24.2.7	60.0	16	·	·	·	8	22	20	8	1	1	1	4	3	16	·
VIII	7.5	1.7	·	·	·	·	·	·	2.5	4.8	2.2	2.8	8.5	2.6	13.5	1.9	39	1.4	98.2	28.8	28	·	·	·	3	17	11	3	1	·	1	1	1	8	·
IX	8	1.4	1	1.0	4.5	2.8	3.5	2.7	5	3.3	23.5	2.8	9	1.7	8.5	1.7	27	1.6	137.7	28.3	4	2	·	·	·	21	19	3	·	·	3	1	4	9	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	35.7	13.5	22	-	-	-	-	6	4	2	-	-	-	-	-	-	·
XI	1.4	1.9	1.5	2.0	3	1.3	1	1.0	1.5	3.8	12.5	1.7	7.5	1.4	4.5	1.9	31	1.5	42.9	24.9	28	14	3	1	·	8	7	1	·	·	2	·	7	12	1
XII	7.5	1.8	·	·	·	·	1	4.0	1.5	2.2	14.5	2.9	6.5	2.8	5.5	1.9	43	1.3	22.9	6.9	14	28	7	4	·	9	7	·	1	·	-	·	6	15	11
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	985.0	60.0	16.VIII	-	-	-	-	161	130	27	-	-	-	-	-	-	66

Świniarsko

$H_s = 295$ m $h_w = 14$ m

I	9	2.3	·	·	·	·	1	7.0	3.6	3.8	1	2.5	16	3.4	3	2.7	27	2.5	19.3	5.8	6	27	10	·	·	10	5	·	·	·	-	·	1	14	21
II	6	2.8	·	·	·	·	0.5	5.0	14.5	4.3	3	3.3	16	2.4	·	·	14	3.1	12.2	4.9	25	20	2	·	·	9	4	·	1	·	-	·	·	14	8
III	1.5	1.9	2	2.5	2	1.0	0.5	5.0	1.9	3.7	2.5	4.8	1.5	3.3	3	2.3	34	1.9	37.9	16.6	24	18	3	2	·	6	6	1	·	·	-	·	3	10	8
IV	2.2	2.4	2	3.5	1	3.0	·	·	9	2.2	1	7.0	6.5	2.3	4.5	2.4	44	1.3	52.7	13.9	11	12	·	·	·	15	10	1	·	·	-	1	5	17	1
V	2.9	2.6	1	3.5	3	1.3	1	1.0	3.5	3.0	2.5	2.2	10.5	2.1	5.5	2.3	37	1.5	69.5	15.3	10	1	·	·	·	13	10	1	·	·	-	2	1	16	·
VI	1.2	2.3	·	·	4	1.5	·	·	2.3	2.7	1	4.0	7.5	2.6	4.5	2.1	38	1.4	41.1	12.3	21	·	·	·	13	13	11	1	·	·	-	11	5	2	·
VII	1.4	2.6	·	·	1	1.0	1	2.5	9	3.4	1	4.0	1.5	3.1	1	3.0	51	1.3	115.0	28.1	15	·	·	·	14	16	11	4	1	·	-	5	1	16	·
VIII	11.5	2.3	·	·	·	·	0.5	3.0	1.0	3.0	1.5	2.3	18.5	2.7	2	2.5	49	1.2	96.2	28.9	18	·	·	·	8	17	12	3	·	·	-	5	2	7	·
IX	1.2	1.9	·	·	·	·	1	2.0	11.5	2.9	8	3.1	18.5	2.9	2	4.0	37	1.6	49.9	-	-	2	·	·	2	12	9	1	·	·	-	·	1	12	·
X	1.4	1.5	1	2.0	·	·	·	·	2.0	3.0	2	2.0	1.0	2.8	2	1.2	44	1.2	27.2	10.5	22	12	·	·	·	3	3	1	·	·	-	·	7	7	·
XI	1.0	3.4	3	2.5	1	2.0	1	3.0	2.5.5	3.6	6.5	2.2	1.5	4.7	1	3.5	27	2.5	19.1	9.7	29	11	2	1	·	7	4	·	2	·	-	·	3	17	1
XII	1.3	2.7	1	3.0	1	1.2	·	·	3.2.5	5.6	3.5	4.3	8.5	3.0	2.5	7.4	28	3.0	15.5	5.9	5	27	9	1	·	7	3	·	5	·	-	·	2	16	5
Rok	16.7.5	2.4	1.0	1.1	1.6	0.9	6.5	2.4	2.4.3.5	3.4	3.3.5	3.5	1.5.7	2.9	3.1	2.8	430	1.9	555.4	28.9	28.VIII	130	26	4	37	128	88	13	9	·	-	24	31	148	42

Nowy Sącz

$H_s = 285$ m $H_b = 300{,}6$ m $h_w = 24.4$ m

I	5	2.6	5	3.0	1	2.9	2	2.0	7.5	3.5	15.5	2.4	12.5	3.5	8.5	4.1	36	1.9	27.6	6.6	6	27	8	8	·	13	7	·	1	·	·	·	1	13	25
II	6.5	1.5	0.5	2.0	1.5	3.3	2.5	3.2	21.5	5.0	12	3.2	8.5	3.0	6	3.8	25	2.6	22.2	6.6	25	14	1	·	·	12	8	·	3	·	·	·	2	18	6
III	11	3.1	7	1.4	8.5	2.1	4	1.9	9	3.3	4.5	5.0	11.5	4.1	5.5	3.0	32	2.0	40.6	15.9	24	16	2	1	·	10	6	1	1	·	·	·	6	10	7
IV	12	2.4	4.5	2.1	4	1.5	3.5	1.4	7	2.4	0.5	2.0	1.5	1.7	12	2.6	48	1.1	58.8	15.6	11	9	·	·	1	19	11	2	·	·	1	3	4	14	·
V	21	2.3	11	4.0	5	3.3	1.5	1.7	4	2.8	3	1.3	4.5	3.1	20	2.6	23	2.0	86.8	21.1	10	·	·	·	·	16	13	3	·	·	·	2	1	16	·
VI	16.5	2.4	6	2.6	2	3.5	3.5	4.0	11	4.8	5.5	2.5	3.5	1.9	10	2.9	33	2.0	43.7	10.2	12	·	·	·	16	13	11	1	1	·	·	7	3	5	·
VII	12.5	2.0	3.5	1.9	3.5	2.3	2.5	3.6	6.5	1.7	4.5	1.7	8.5	2.9	5.5	2.0	46	1.1	122.8	27.3	15	·	·	·	15	18	12	5	·	·	·	10	1	12	·
VIII	1.4	2.5	2.5	2.6	2.3	1.4	3	1.7	5.5	3.3	6	2.5	7.5	5.0	12	2.6	40	1.6	104.5	24.4	28	·	·	·	8	19	11	3	2	·	3	7	·	4	·
IX	5.5	2.8	1	3.0	1	2.0	·	·	3	3.7	1.3	2.9	15.5	3.5	7	3.0	44	1.6	67.8	21.5	4	1	·	·	2	15	12	1	·	·	2	·	2	12	·
X	4.5	2.7	1	1.0	·	·	·	·	5	4.8	8	2.4	4.5	3.6	6	1.4	64	0.9	27.4	10.5	22	3	·	·	·	3	3	2	·	·	4	·	6	4	·
XI	4.5	6.9	8	2.8	5.5	2.5	4	3.4	15	4.2	14.5	2.7	6.5	3.6	4	4.8	28	2.5	32.4	13.1	29	10	1	·	·	9	4	1	2	·	2	·	4	15	1
XII	9	3.7	2.5	3.4	4.5	1.9	3	2.7	11	4.7	11.8	3.3	5.5	4.9	7.5	3.7	32	2.4	22.3	8.0	14	25	8	1	·	13	5	·	4	1	·	·	2	16	8
Rok	12.2	2.9	5.1.5	2.5	3.9	2.2	2.9.5	2.2	10.6	3.7	10.5	2.7	9.0	3.4	10.4	3.0	448	1.8	656.9	22.3	15.VIII	105	20	10	42	160	103	19	14	1	12	29	32	139	47

Istebna – Kubalonka

$\varphi = 49°36'$ $\lambda = 18°54'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnio				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	-4,5	-1,8	-3,6	-3,4	-0,4	-	6,4	23	-	-	-	-	-	-	-	-	-	-	8,6	7,5	7,7	7,9
II	-	-	-	-	-1,2	1,2	-0,2	-0,1	2,8	-	7,6	18	-	-	-	-	-	-	-	-	-	-	8,2	8,0	7,7	8,0
III	-	-	-	-	0,2	5,3	1,9	2,3	7,1	-	16,0	14	-	-	-	-	-	-	-	-	-	-	5,8	5,6	5,0	5,5
IV	-	-	-	-	4,3	8,0	4,9	5,5	9,8	-	21,5	29,30	-	-	-	-	-	-	-	-	-	-	5,5	6,3	6,3	6,0
V	-	-	-	-	6,2	9,4	6,7	7,2	11,2	-	21,6	19	-	-	-	-	-	-	-	-	-	-	6,8	7,1	6,6	6,8
VI	-	-	-	-	14,6	19,2	14,9	15,9	20,8	-	28,0	30	-	-	-	-	-	-	-	-	-	-	4,0	4,5	4,1	4,2
VII	-	-	-	-	14,6	18,6	15,1	15,8	20,2	-	32,0	8	-	-	-	-	-	-	-	-	-	-	6,5	6,5	6,6	6,5
VIII	-	-	-	-	12,0	17,0	12,5	13,5	18,2	-	24,9	11	-	-	-	-	-	-	-	-	-	-	5,6	5,3	4,5	5,1
IX	-	-	-	-	8,0	12,0	8,7	9,4	13,3	-	23,0	9	-	-	-	-	-	-	-	-	-	-	6,7	6,9	6,4	6,7
X	-	-	-	-	5,7	10,7	6,8	7,5	11,7	-	17,8	9	-	-	-	-	-	-	-	-	-	-	5,9	3,8	3,9	4,5
XI	-	-	-	-	2,1	4,5	2,5	2,9	5,6	-	14,5	5	-	-	-	-	-	-	-	-	-	-	7,0	6,4	6,8	6,7
XII	-	-	-	-	-3,3	-1,5	-2,5	-2,4	0,0	-	10,5	13	-	-	-	-	-	-	-	-	-	-	8,1	7,8	8,7	8,2
Rok	-	-	-	-	4,9	8,6	5,6	6,2	10,0	-	32,0	8.VII	-	-	-	-	-	-	-	-	-	-	6,6	6,3	6,2	6,4

Istebna – Stecówka

$\varphi = 49°35'$ $\lambda = 18°57'$

I	-	-	-	-	-4,7	-2,2	-3,6	-3,5	-1,0	-6,5	6,1	2	-21,0	17	-	-	-	-	-	-	-	-	8,5	7,6	7,5	7,9
II	-	-	-	-	-1,3	0,7	-0,5	-0,4	2,5	-5,3	7,6	18,19	-10,3	28	-	-	-	-	-	-	-	-	8,0	8,3	7,6	8,0
III	-	-	-	-	-0,4	4,9	1,8	2,0	6,4	-2,5	13,4	14	-10,8	4	-	-	-	-	-	-	-	-	6,3	6,7	4,2	5,4
IV	-	-	-	-	3,9	7,4	4,5	5,1	9,3	0,9	21,0	30	-7,0	14	-	-	-	-	-	-	-	-	6,1	6,7	6,3	6,4
V	-	-	-	-	5,8	8,9	5,9	6,6	10,7	3,0	20,5	19	-2,6	7	-	-	-	-	-	-	-	-	7,0	7,5	6,7	7,1
VI	-	-	-	-	13,3	17,8	13,7	14,6	20,0	9,7	26,6	30	2,8	27	-	-	-	-	-	-	-	-	4,9	5,6	4,7	5,1
VII	-	-	-	-	14,3	17,8	14,8	15,4	-	11,5	-	-	7,8	28	-	-	-	-	-	-	-	-	6,8	7,0	6,4	6,7
VIII	-	-	-	-	12,2	16,1	12,6	13,4	-	8,4	-	-	3,8	31	-	-	-	-	-	-	-	-	6,3	6,5	4,0	5,6
IX	-	-	-	-	8,1	11,6	8,7	9,3	-	5,4	-	-	-1,5	27	-	-	-	-	-	-	-	-	7,8	7,2	6,5	7,2
X	-	-	-	-	5,9	10,4	6,8	7,5	-	3,6	-	-	-2,2	3	-	-	-	-	-	-	-	-	6,5	4,6	3,5	4,9
XI	-	-	-	-	1,9	4,1	2,5	2,8	-	0,0	-	-	-14,5	30	-	-	-	-	-	-	-	-	6,9	6,5	6,7	6,7
XII	-	-	-	-	-3,5	-2,1	-2,8	-2,8	-	-5,9	-	-	-13,5	4	-	-	-	-	-	-	-	-	8,4	7,9	9,1	8,5
Rok	-	-	-	-	4,6	8,0	5,4	5,8	-	2,0	-	-	-21,0	17,1	-	-	-	-	-	-	-	-	7,0	6,8	6,1	6,6

Istebna – Zaolzie

$\varphi = 49°34'$ $\lambda = 18°56'$

I	-	-	-	-	-5,5	-0,7	-5,4	-4,2	0,6	-10,1	6,2	2	-28,0	17	-	-	-	-	-	-	-	-	8,7	7,6	8,0	8,1
II	-	-	-	-	-1,1	2,6	-0,5	0,1	4,4	-5,3	9,4	19	-18,7	28	-	-	-	-	-	-	-	-	8,3	7,8	7,2	7,8
III	-	-	-	-	-1,0	6,6	-0,6	1,1	8,0	-6,7	15,2	23	-19,4	6	-	-	-	-	-	-	-	-	6,9	5,5	5,4	5,9
IV	-	-	-	-	5,1	10,2	5,2	5,4	11,5	-1,4	23,8	30	-9,8	14	-	-	-	-	-	-	-	-	5,8	6,3	6,4	5,8
V	-	-	-	-	7,8	11,4	8,2	7,9	13,0	1,4	23,2	19	-4,1	30	-	-	-	-	-	-	-	-	7,4	7,5	5,9	6,9
VI	-	-	-	-	16,2	20,5	13,5	15,8	22,4	-	29,0	30	-	-	-	-	-	-	-	-	-	-	4,1	5,7	4,1	4,6
VII	-	-	-	-	16,3	20,1	14,6	16,4	22,3	-	33,3	8	-	-	-	-	-	-	-	-	-	-	7,0	7,6	6,6	7,1
VIII	-	-	-	-	12,8	18,8	12,1	14,0	20,3	7,2	27,6	13	3,0	27	-	-	-	-	-	-	-	-	5,9	4,6	4,8	5,1
IX	-	-	-	-	8,4	13,4	8,9	9,9	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7,7	6,5	7,2	7,1
X	-	-	-	-	4,6	12,6	3,9	6,2	13,6	-0,7	19,7	19	-6,7	3	-	-	-	-	-	-	-	-	5,7	4,4	3,6	4,6
XI	-	-	-	-	2,0	5,8	1,8	2,8	7,2	-1,5	15,9	4	-12,8	30	-	-	-	-	-	-	-	-	7,4	6,8	7,3	7,1
XII	-	-	-	-	-3,6	-0,6	-1,9	-2,0	1,1	-6,7	12,1	13	-21,2	11	-	-	-	-	-	-	-	-	8,0	8,0	8,2	8,1
Rok	-	-	-	-	5,2	10,0	4,8	6,1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6,9	6,5	6,1	6,5

Rabka

$\varphi = 49°36'$ $\lambda = 19°58'$

I	955,4	965,9	939,6	-	-3,1	0,8	-2,7	-1,9	2,0	-4,9	8,4	10	-17,9	17	85	70	88	81	0,8	2,1	0,5	1,2	7,9	7,6	6,7	7,4
II	947,1	962,9	925,9	-	0,0	4,3	1,1	1,6	5,8	-1,5	11,9	19	-11,8	23	88	70	85	81	0,8	2,8	1,1	1,6	7,7	7,7	6,4	7,3
III	952,7	965,5	936,4	-	-1,7	6,3	1,8	2,0	8,4	-2,6	14,9	26	-15,8	4	88	60	81	76	0,8	4,5	1,5	2,3	7,1	6,0	4,7	5,9
IV	952,3	963,0	930,0	-	3,1	10,6	5,9	6,4	11,9	2,0	24,4	30	-6,2	14	92	62	82	79	0,7	6,2	1,8	2,9	6,9	7,2	6,6	6,9
V	950,5	958,2	940,7	-	6,3	11,3	7,9	8,4	12,8	4,2	21,5	19	-0,5	30	88	69	84	80	1,2	5,1	2,0	2,8	7,7	8,5	7,9	8,0
VI	955,5	965,7	941,5	-	14,2	21,8	15,7	16,8	23,1	9,8	30,4	24	2,9	27	83	51	75	70	3,0	13,9	4,7	7,2	4,9	6,3	5,5	5,6
VII	943,9	960,3	939,4	-	15,6	21,0	16,5	17,4	22,7	12,8	35,0	5	8,0	30	88	65	85	79	8,4	10,4	3,3	5,4	7,3	7,6	7,3	7,4
VIII	951,9	960,8	940,1	-	11,7	19,1	13,9	14,8	20,6	9,8	28,2	12	4,0	31	92	62	86	80	1,2	9,2	2,4	4,3	6,0	7,2	5,9	6,4
IX	950,7	959,2	938,8	-	8,4	14,4	9,8	10,6	15,7	7,0	25,6	8	-1,0	26	90	66	88	81	1,2	6,2	1,5	3,0	7,8	7,3	6,1	7,1
X	956,1	963,8	939,7	-	4,9	13,3	6,7	7,9	14,4	3,3	22,7	19	-2,9	3	94	60	89	80	1,1	6,7	1,2	3,0	6,1	5,4	3,2	4,9
XI	954,8	971,1	944,6	-	1,1	6,5	2,3	3,0	7,6	0,0	18,1	4,5	-11,7	30	91	72	89	84	0,6	3,6	0,8	1,6	7,2	6,2	4,1	6,8
XII	949,9	968,6	922,5	-	-2,6	0,6	-1,8	-1,4	1,5	-4,8	14,9	13	-13,2	11	87	74	86	82	0,8	1,8	0,8	1,1	6,6	7,3	5,9	6,6
Rok	952,1	971,1	922,5	-	4,8	10,8	6,4	7,1	12,2	2,9	35,0	5.VII	-17,9	17,1	89	65	85	80	1,2	6,0	1,8	3,0	6,9	7,0	6,1	6,7

Istebna – Kubalonka

H_s = 800 m h_w = 25 m 1957

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max ≥ 25	Max ≥ 0	Min < 0	Min < -25	Opad R ≥ 0,1	≥ 1,0	≥ 10,0	≥ 100,0	Wiatr v ≥ 10	≥ 15							
I	15	3,2	8	3,8	15	5,0	3,5	2,4	3,7	3,5	16,5	4,8	3,5	2,1	7	2,6	3	3,4	52,9	18,9	6	-	17	-	-	15	10	4	-	-	8	-	2	2,8	3,1
II	5	3,2	-	-	-	-	2	7,8	4,0	6,1	1,9	4,1	5	2,0	7	2,7	6	4,5	92,3	16,8	25	-	5	-	-	16	14	3	1	1	15	-	2	4,7	5,0
III	4	4,0	1	5,0	0,5	7,0	5	3,2	1,0,5	4,3	2,7,5	4,2	10	3,0	15,5	3,0	10	3,5	88,7	20,2	17	-	4	-	-	14	12	3	2	2	3	1	3	4,1	4,0
IV	2,7	2,6	6,5	2,8	2,5	3,8	4,5	4,5	1,2	3,7	9	3,7	1	2,0	2,6,5	2,8	2	3,0	79,5	22,4	7	-	-	-	-	13	11,5	2	1	1	3	2	6	7,0	5
V	3,2	2,9	2,0,5	4,6	1,5	2,3	5	2,0	6	4,2	3	3,3	4	2,8	9	2,9	1,2	2,9	89,6	26,0	3,0	-	-	-	-	14	12	3	-	-	5	2	1	4,1	3
VI	1,3	2,5	7	3,4	-	-	3	4,8	2,2,5	5,1	1,3,5	3,8	5	2,4	1,8	2,6	8	3,3	69,8	18,0	7	-	-	-	5	13	9	3	1	-	4	3	4,0	3	-
VII	1,9	1,9	6	3,0	2	3,0	4	2,8	1,5,5	3,8	1,3,5	3,0	5	2,4	1,5	2,3	1,3	2,4	29,3,5	6,9,9	0,5	-	-	-	7	22	1,8	1,1	-	-	7	6	3	4,5	-	-
VIII	2,2,5	2,1	3,5	1,8	0,5	1,0	3,5	4,0	1,9	4,6	1,5,5	3,0	4,5	1,9	1,2	2,3	1,2	2,5	99,7	37,8	2,8	-	-	-	-	16	1,3	3	1	1	6	1	2	5	-	-
IX	1,5	2,9	3	2,3	-	-	2,5	4,6	2,2	5,0	1,5,5	4,3	8,5	2,8	10,5	2,6	1,3	3,2	138,6	1,8,6	2,9	-	-	-	-	23	1,5	7	2	-	6	1	5	1,5	-	-
X	9	1,8	1	1,0	2	1,0	5,5	2,8	3,9	3,9	1,1	3,6	4,6	2,3	9	1,6	1,2	2,7	30,0	1,1,6	2,0	-	-	-	-	8	5	2	-	-	4	-	6	8	-	-
XI	5,8	4,8	9	4,0	2,5	3,4	1,0	3,4	3,9,5	5,6	7,5	3,2	3	1,0	4	3,5	9	4,1	59,2	20,0	2,8	-	5	-	-	9	8	4	2	2	6	-	3	1,5	4	-
XII	1,0	2,3	5,5	3,3	0,5	1,0	6,5	5,3	3,0,5	4,8	1,6	4,6	3	1,7	1,8	2,5	5	3,6	49,5	9,3	4	-	2,0	-	-	15	1,3	2	-	-	8	-	3	3,2	1,6	-
Rok	1,2,5	2,9	7,4	2,9	1,5,5	2,1	5,5	3,8	3,0,2,5	4,6	1,6,7,5	3,8	5,7	2,2	1,4,8,5	2,6	1,0,5	3,3	1,1,4,2,3	6,9,9	16 VII	-	5,1	-	1,0	1,8,3	1,4,4	4,0	1,7	7	8,6	1,1	5,2	1,5,4	9,9	-

Istebna – Stecówka

H_s = 750 m h_w = I–VI 10 m, IX–XII 12,5 m

I	2,0	3,9	7	2,4	5	2,6	-	-	2,2	2,0	3,7,5	3,0	1,5	9,3	-	-	-	3,0	69,8	18,7	6	3,0	1,8	7	-	15	10	2	2	-	7	-	2	7,1	3,1
II	1,3	2,4	5	2,2	-	-	4	3,2	1,8	5,0	3,6	4,6	6	3,0	2	3,0	-	4,0	78,8	14,2	2,5	2,6	6	4	-	10	1,3	2	4	2	7	-	3	6,2	2,8
III	1,4,5	2,2	1,4,5	3,2	1,1	2,7	4	2,8	1,5,5	3,6	1,8	3,1	1,2,5	3,5	2	2,5	1	3,0	87,2	25,3	1,7	2,1	5	1	-	1,4	1,3	2	1	-	3	1	3	5	1,6
IV	3,7	2,4	2,5	1,9	8	2,9	3	4,3	3	1,7	1,1	3,1	2	1,5	1	3,0	-	2,6	66,8	20,2	7	1,3	-	-	-	1,7	1,1	2	-	-	1,0	2	6	1,1	4
V	2,7,5	2,5	3,5	1,1	6,3	3,8	3	2,0	7	1,9	8	2,5	1	1,0	5	2,4	-	3,2	62,5	2,5,9	2,0	6	-	-	-	1,5	1,0	1	-	-	5	1	3	4	3
VI	1,8	2,8	1,2,5	1,8	1,5	2,6	3	1,8	1,2	4,0	2,5,5	3,6	0,5	1,0	2,5	3,0	1	3,0	80,9	2,4,7	7	-	-	-	1	1,0	9	3	1	-	3	2	7	6	-	-
VII	2,2,5	2,4	1,6,5	2,2	6,5	2,0	8,5	2,7	6,5	3,8	2,3,5	3,0	2,5	3,0	4,5	3,2	2	2,6	3,0,4,3	4,7,7	1,8	-	-	-	-	2,1	2,1	1,1	1	-	5	5	2	1,4	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	95,3	32,6	2,8	-	-	-	-	1,5	1,2	3	-	-	1,1	1	-	1,1	-	-
IX	1,6,5	2,5	8	1,8	1	1,0	4	2,0	6,5	2,9	3,2	3,5	1,2,5	3,5	5,5	2,5	4	2,8	1,2,6,5	1,1,6	2,9	2	-	-	-	2,3	1,5	7	-	-	9	-	1	1,6	-	-
X	5	1,8	8,5	1,5	6	1,4	1	1,5	2,3,5	3,0	3,4	2,7	9	1,7	4	1,5	4	2,3	2,8,2	1,0,9	2,0	5	-	-	-	8	5	1	-	-	6	-	5	6	-	-
XI	6	5,3	6,5	2,5	7	1,7	7	2,4	1,7	5,2	3,1,5	3,3	6	2,5	6	4,2	3	3,5	1,1,7	1,9,5	2,8	1,8	-	1	-	1,2	6	2	1	1	6	-	7	1,9	1	-
XII	1,2,5	2,3	2,5	1,8	2	2,0	2	4,0	1,1	3,4	1,6	3,5	3,5	5,7	9,5	2,7	1	3,1	1,7,9	6,9	4,1,4	2,8	-	1,1	-	1,6	1,0	-	1	-	9	-	1	2,4	1,6	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1,0,9,2,5	4,7,7	1,6 VII	1,4,9	-	1,1	-	1,8,2	1,3,5	3,6	-	-	7,5	1,2	4,8	1,5,1	9,8	-

Istebna – Zaolzie

H_s = 580 m h_w = 19 m

I	2	2,0	4	3,8	2	1,5	-	-	3,5	1,7	1,8,5	2,0	5	1,5	1,6	2,4	4,2	4,2	6,0,6	1,5,1	6	3,1	4,3	4,4	-	1,1	1,0	2	-	-	2	-	2	2,3	3,1
II	8,5	2,2	0,5	1,0	1,5	1,0	2,5	4,0	1,5	2,8	1,4	2,4	1,1,5	1,7	4,5	2,3	2,6	1,6	8,1,5	1,5,3	1,5	2,7	-	6	-	1,6	1,2	3	-	-	4	-	-	1,3	2,3
III	7,5	1,9	1,5	1,3	6	3,0	4,5	2,9	1,1	2,8	1,5	2,8	9,5	2,2	3	2,0	3,5	1,6	8,9,7	3,0,0	1,7	2,5	3,1	4,2	-	1,0	9	2	-	-	3	1	8	1,3	1,5
IV	2,0,5	1,7	5,5	2,5	3,5	2,0	3,5	2,9	5	2,5	4,5	2,6	2	2,2	1,9,5	1,6	2,6	1,4	6,3,8	1,4,3	7	2,1	-	-	-	1,4	1,2	4	-	-	6	2	6	1,0	1
V	1,4	1,7	1,4,5	2,7	2,5	3,8	2	3,0	1	4,0	4,5	1,8	8,5	1,5	1,9	2,3	2,7	1,6	6,7,1	1,9,9	2,0	1,0	-	-	-	1,1	9	2	-	-	5	4	2	1,4	-
VI	8,5	1,5	4	3,0	5,5	1,9	3	2,3	7,5	4,3	7,5	2,4	1,0	1,9	1,4	1,9	3,0	1,5	6,7,7	2,1,4	7	-	-	-	5	1,0	9	2	-	-	6	2	7	3	-	-
VII	3	1,7	1	1,0	1	2,0	-	-	5	1,8	1,2	1,7	8,5	1,9	1,7,5	1,5	4,5	0,9	2,5,2,3	6,7,4	1,6	-	-	-	8	2,0	1,8	8	-	-	5	6	2	1,5	-	-
VIII	3	2,2	0,5	2,0	6	1,5	1	1,0	1,1	1,9	1,6	1,8	1,2	2,0	9,5	1,6	3,4	1,2	–	–	…	…	…	…	5	–	–	–	–	–	4	2	3	4	-	-
IX	7,5	2,0	2,5	1,4	1	1,0	-	-	5,5	1,5	2,1,5	1,6	1,5	3,0	8	2,1	2,9	1,2	1,1,7,0	1,5,5	1,4	-	-	-	-	1,7	1,5	6	-	-	7	1	2	1,7	-	-
X	4	1,2	2	1,0	1	1,0	-	-	1,5	3,0	2,4,5	2,0	1,2	1,5	8	1,6	4,0	1,0	2,7,6	4,3,0	2,0	2,3	-	-	-	0	3	2	-	-	3	-	5	5	-	-
XI	7,5	3,2	8,5	2,5	3	1,2	6	2,3	8,5	4,4	1,7	3,2	6	2,4	4,5	1,9	2,9	2,0	4,9,1	2,4,2	2,8	1,7	1,4	3	-	8	5	2	-	-	4	-	5	1,7	1	-
XII	3	2,7	9	2,0	-	-	-	-	1,2	2,4	1,5,5	2,8	3,5	2,1	1,5	2,1	3,5	1,5	4,0,8	9,0	1,4	2,9	1,5	5	-	1,1	9	-	-	-	2	-	2	2,8	1,5	-
Rok	8,9	2,0	5,3,5	2,0	3,3	1,7	2,2,5	1,5	8,6,5	2,8	1,7,0,5	2,3	1,0,3,5	2,0	1,3,8,5	1,9	3,9,8	1,4	–	6,7,4	1,6 VII	–	3,2	4,4	–	–	–	–	–	–	6,7	1,8	4,4	1,1,6	8,4	-

Rabka

H_s = 510 m H_b = 552,4 m h_w = 18 m

I	1,5	2,7	6,5	4,4	-	-	1,0	2,0	2,3,5	2,6	2,2	1,8	9	2,6	4,5	7,2	1,6	2,3	4,1,2	9,8	6	2,5	9	5	-	1,6	1,1	-	2	1	4	-	1	1,5,3	3,9
II	2,5	2,4	-	-	1	3,0	8	2,2	1,3	3,5	2,6	3,9	1,2,5	3,2	5	1,7	1,6	2,6	4,5,4	1,2,4	2,5	1,6	3,1	1,1	-	1,5	9	2	5	1	-	-	3	1,3	4,1
III	3,5	3,0	1,1,5	2,8	4	3,2	9,5	1,5	1,1	2,5	1,8	2,9	1,0,5	2,3	5	2,4	2,0	2,0	4,1,6	1,1,5	1,6	1,9	3	6	-	4,1	3,1	1	5	1	-	1	5	3	1,5
IV	7	1,9	1,0,5	2,7	1,5	4,0	5	1,8	6,5	2,2	1,1	2,2	1,2,5	1,8	7	2,8	2,9	1,5	6,3,1	1,8,3	1,1	1,1	-	-	-	1,7	1,1	2	1	1	2	2	3	1,7	1
V	2,0	2,6	1,5,5	2,5	2,5	2,4	1,0,5	1,5	4	1,2	4	2,1	6,5	2,3	1,0	2,6	2,0	1,8	6,2,4	1,1,8	2,0	1,1	-	-	-	1,5	9	2	-	-	1	1	-	1,0	-	-
VI	6,5	2,7	8	2,3	1,5	2,0	1,1	1,0	1,0,5	1,8	1,9	3,5	8,5	2,9	6	2,8	1,9	2,0	4,2,3	8,4	5	1,1	-	-	9	1,1	7	-	3	1	-	1	3	1,5	-	-
VII	3,5	1,4	6	2,4	2,5	1,4	7,5	1,3	1,0	1,8	1,7	2,1	8,5	2,5	7	2,3	3,1	1,5	2,9,2,5	4,8,0	1,1	-	-	-	1,0	1,9	1,0	9	1	-	-	1,5	-	1,5	-	-
VIII	1,5	2,3	3,5	1,2	1	1,0	9	1,3	1,3	2,1	1,1	3,5	1,5	2,5	1,2	2,4	2,2	1,8	1,1,5,0	2,7,6	1,5	-	-	-	5	1,5	1,0	5	3	2	1	3	-	6	-	-
IX	5	1,7	1	2,0	1	1,0	5	1,0	9	2,7	3,4	3,0	1,0	2,1	6	3,9	1,9	2,1	7,2,4	1,1,1	1,5	-	-	-	2	1,7	1,4	2	1	-	2	1	2	1,6	-	-
X	2	1,5	3,5	1,6	2	1,8	1,1,5	1,9	1,1,5	1,8	2,1	2,0	8,5	1,5	2	1,5	3,1	1,2	3,2,1	1,1,5	2,2	1,5	-	-	-	8	4	1	-	-	1	-	1	-	-	-
XI	9,5	6,4	1,3,5	2,7	1	1,0	1,1,5	1,7	8	2,4	1,4,5	2,4	9,5	3,2	4,5	5,6	1,8	2,5	3,4,9	8,4	2,8	1,1	1,3	1,1	-	1,2	7	-	2	1	2	-	1	1,6	1,1	-
XII	2	2,0	6	2,2	2	2,0	1,0	2,7	2,6,5	3,5	2,2	4,4	6	1,8	7,5	4,3	1,2	3,0	2,7,7	9,1	5	2,7	1,0	3	-	1,1	8	-	5	3	3	-	3	1,3	1,3	-
Rok	6,7,5	2,6	8,7,5	2,2	2,0	1,9	1,0,8,5	1,7	1,1,5,5	2,3	2,1,9,5	2,8	1,1,7	2,4	7,6,5	3,3	2,5,3	2,0	8,7,0,6	4,8,0	1,4 VIII	1,1,6	8,6	4,5	2,5	1,6,5	1,1,7	3,4	2,5	1,1	2,5	1,1	4,5	2,5	1,5,4	1,1,8

Brzezna

$\varphi = 49°36'$ $\lambda = 20°37'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA WILGOTNOŚĆ WZGLĘDNA $U_{śr}$				ŚREDNI NIEDOSYT WILGOTNOŚCI $\Delta_{śr}$				ŚREDNIE ZACHMURZENIE $N_{śr}$			
					Średnia																				
	P_m	Max	Min	P_{om}	I	II	III	Dias	Max	Min	Max obs.	Data	Min obs.	Data		II	III	Dias	I	II	III	Dias	I	II	III	Dias
I	–	–	–	–	-2.8	0.8	-1.7	-1.4	2.0	-4.7	7.8	6	-12.7	17	80	75	82	79	1.1	1.7	1.0	1.3	7.4	6.5	6.9	6.9
II	–	–	–	–	1.1	5.5	2.7	3.0	6.8	-0.3	11.9	6	-6.2	23	83	67	77	76	1.2	3.2	1.7	2.0	7.1	6.8	7.1	7.0
III	–	–	–	–	0.2	7.4	3.0	3.4	9.2	-1.3	17.8	14	-13.7	4	76	57	73	69	1.5	5.4	2.3	3.1	6.3	4.9	4.9	5.4
IV	–	–	–	–	4.6	12.1	7.7	8.0	13.7	2.2	24.7	30	-2.1	14	88	68	79	78	1.0	6.5	2.4	3.3	6.2	6.7	6.8	6.6
V	–	–	–	–	7.5	12.6	9.2	9.6	14.5	4.8	22.5	13,19	0.2	30	–	–	–	–	–	–	–	–	7.0	8.0	7.1	7.3
VI	–	–	–	–	15.4	22.8	16.5	17.6	24.7	10.6	38.0	30	3.8	9	–	–	–	–	–	–	–	–	3.3	5.5	4.8	4.6
VII	–	–	–	–	16.8	22.1	17.6	18.5	24.8	13.5	36.8	5	9.4	20	–	–	–	–	–	–	–	–	6.2	7.5	6.9	6.9
VIII	–	–	–	–	13.5	20.9	15.4	16.3	22.5	11.1	30.1	12	4.6	24	–	–	–	–	–	–	–	–	5.4	6.5	6.0	6.0
IX	–	–	–	–	9.7	16.6	11.3	12.2	17.6	7.3	27.8	9	-0.5	26	–	–	–	–	–	–	–	–	6.5	6.5	7.3	6.8
X	–	–	–	–	5.2	11.0	7.7	8.0	13.1	3.1	21.2	17	-1.3	3	–	–	–	–	–	–	–	–	5.5	4.5	5.2	5.1
XI	–	–	–	–	3.5	7.5	4.3	4.9	8.5	1.8	20.0	4	-10.6	30	–	–	–	–	–	–	–	–	7.5	6.8	7.6	7.0
XII	–	–	–	–	-1.9	1.3	-0.6	-0.4	2.7	-3.8	14.6	14	-11.3	19	–	–	–	–	–	–	–	–	7.9	6.0	6.5	6.9
Rok	–	–	–	–	6.1	12.0	7.8	8.4	13.6	3.7	36.2	6.VII	-13.7	4.III	–	–	–	–	–	–	–	–	6.4	6.4	6.4	6.4

Ptaszkowa

$\varphi = 49°36'$ $\lambda = 20°53'$

I	–	–	–	–	-3.5	-0.9	-2.1	-2.2	1.3	-5.1	7.5	8	-14.5	17	–	–	–	–	–	–	–	–	8.4	7.6	6.9	7.6
II	–	–	–	–	1.1	3.4	1.5	1.9	5.1	-0.8	10.4	19	-7.0	28	–	–	–	–	–	–	–	–	8.1	7.2	6.9	7.4
III	–	–	–	–	0.0	5.2	2.1	2.3	7.2	-2.1	15.5	14	-11.5	4	–	–	–	–	–	–	–	–	6.4	5.5	5.1	5.7
IV	–	–	–	–	5.3	9.8	7.2	7.4	11.7	3.1	22.9	30	-3.2	14	–	–	–	–	–	–	–	–	6.5	7.5	6.5	6.7
V	–	–	–	–	6.9	10.4	8.2	8.4	12.5	4.8	19.5	17,19	-4.5	2	–	–	–	–	–	–	–	–	7.1	8.4	7.0	7.6
VI	–	–	–	–	15.9	20.6	16.9	17.8	22.5	11.5	29.2	12	5.8	27	–	–	–	–	–	–	–	–	4.7	5.8	4.6	5.0
VII	–	–	–	–	16.5	20.5	17.1	17.8	22.8	13.7	35.3	5	9.4	29	–	–	–	–	–	–	–	–	6.9	7.3	6.3	6.8
VIII	–	–	–	–	14.0	18.9	15.1	15.8	20.5	11.6	28.3	12	6.5	31	–	–	–	–	–	–	–	–	5.5	6.3	5.4	5.7
IX	–	–	–	–	9.8	14.5	11.1	11.6	15.9	8.1	26.3	9	0.5	27	–	–	–	–	–	–	–	–	5.8	6.8	6.8	6.5
X	–	–	–	–	6.2	12.4	8.0	8.6	13.7	4.1	19.6	19	-3.0	3	–	–	–	–	–	–	–	–	6.5	4.5	3.5	4.5
XI	–	–	–	–	2.8	5.3	3.4	3.7	6.5	1.3	17.1	4	-12.2	30	–	–	–	–	–	–	–	–	6.9	6.8	6.8	6.8
XII	–	–	–	–	-2.5	-0.1	-2.0	-1.8	1.1	-4.9	12.9	13	-14.0	1	–	–	–	–	–	–	–	–	7.5	7.5	6.9	7.2
Rok	–	–	–	–	6.0	10.0	7.2	7.6	11.8	3.8	35.3	5.VII	-14.6	1.II	–	–	–	–	–	–	–	–	6.6	6.8	6.4	6.5

Babia Góra

$\varphi = 49°35'$ $\lambda = 19°31'$

I	–	–	–	–	-4.0	-2.6	-3.5	-3.4	-1.0	-5.9	5.4	19	-16.6	17	–	–	–	–	–	–	–	–	7.5	8.0	6.2	7.2
II	–	–	–	–	-2.4	-0.8	-1.9	-1.8	0.9	-4.1	7.5	3	-15.1	28	–	–	–	–	–	–	–	–	7.5	8.4	7.0	7.6
III	–	–	–	–	-1.3	2.2	-0.7	-0.1	3.3	-3.8	9.4	14	-14.2	4	–	–	–	–	–	–	–	–	6.1	5.8	5.8	5.9
IV	–	–	–	–	2.8	4.5	1.6	2.6	6.0	0.6	17.0	29	-9.0	16	–	–	–	–	–	–	–	–	6.1	7.2	6.6	6.6
V	–	–	–	–	4.0	5.4	2.9	3.8	7.1	0.9	16.8	19	-5.6	7	–	–	–	–	–	–	–	–	7.4	8.9	7.1	7.8
VI	–	–	–	–	12.7	16.1	11.6	13.0	17.6	8.5	23.0	11	0.3	27	–	–	–	–	–	–	–	–	5.3	6.6	4.9	5.6
VII	–	–	–	–	13.0	15.3	12.0	13.1	16.8	9.9	28.2	5	5.9	29	–	–	–	–	–	–	–	–	7.5	7.2	7.2	7.3
VIII	–	–	–	–	10.1	12.8	9.5	10.5	14.4	7.2	22.4	12	2.7	31	–	–	–	–	–	–	–	–	5.7	7.9	5.6	6.4
IX	–	–	–	–	5.7	8.0	6.2	6.5	9.7	4.0	19.1	9	-2.1	26	–	–	–	–	–	–	–	–	7.0	7.5	6.8	7.1
X	–	–	–	–	4.6	7.6	4.8	5.4	8.4	2.5	14.9	9	-3.5	3	–	–	–	–	–	–	–	–	5.0	5.7	3.5	4.7
XI	–	–	–	–	0.3	1.2	0.0	0.4	2.5	-1.7	11.4	4	-17.4	30	–	–	–	–	–	–	–	–	7.3	7.2	6.8	7.0
XII	–	–	–	–	-3.7	-3.1	-3.9	-3.6	-1.5	-6.8	6.9	13	-17.9	1	–	–	–	–	–	–	–	–	7.2	7.4	6.5	7.0
Rok	–	–	–	–	3.5	5.5	3.2	3.8	7.0	0.9	28.2	5.VII	-17.4	30.XI	–	–	–	–	–	–	–	–	6.6	7.3	6.2	6.7

Kamienica

$\varphi = 49°35'$ $\lambda = 20°21'$

I	–	–	–	–	-4.5	0.4	-3.6	-2.8	1.6	-7.1	7.9	6	-19.2	17	–	–	–	–	–	–	–	–	7.8	6.9	6.8	7.0
II	–	–	–	–	-0.2	4.8	1.3	1.8	6.4	-2.0	11.9	18	-3.1	28	–	–	–	–	–	–	–	–	7.7	6.9	6.5	7.1
III	–	–	–	–	-0.8	5.9	2.0	2.5	8.6	-3.0	16.3	14	-16.3	4	–	–	–	–	–	–	–	–	6.4	5.0	5.0	5.5
IV	–	–	–	–	4.4	11.3	5.9	6.9	12.9	1.7	23.6	30	-3.5	14	85	59	81	74	1.7	6.7	1.9	3.4	5.8	7.0	6.1	6.3
V	–	–	–	–	7.7	11.4	7.7	8.6	13.6	3.8	21.5	12	-1.5	30	81	66	83	77	2.1	5.4	1.7	3.1	7.0	8.5	7.3	7.6
VI	–	–	–	–	15.8	21.8	14.0	16.4	23.6	8.5	30.5	30	2.0	27	75	55	84	71	4.6	13.1	2.7	6.8	3.9	5.8	4.0	4.6
VII	–	–	–	–	16.2	21.4	16.0	17.4	23.5	11.7	34.7	5	6.0	29	–	–	–	–	–	–	–	–	6.7	7.2	6.7	6.9
VIII	–	–	–	–	13.4	20.0	13.9	15.3	21.7	9.5	30.1	14	3.0	31	86	60	87	78	2.3	10.2	2.3	4.9	4.5	6.5	5.9	5.6
IX	–	–	–	–	9.2	15.4	10.4	11.4	16.9	6.1	27.3	9	-2.2	26	89	62	85	78	1.6	7.2	2.0	3.6	5.8	6.7	6.5	6.3
X	–	–	–	–	4.2	11.0	6.0	7.6	15.2	1.6	21.8	19	-4.8	3	93	60	88	80	0.6	6.7	1.2	2.8	5.5	4.5	3.7	4.5
XI	–	–	–	–	1.9	6.8	2.3	3.3	8.2	-0.2	18.4	4	-10.5	30	85	73	86	82	1.0	3.5	1.0	1.8	7.1	6.4	6.8	6.8
XII	–	–	–	–	-3.5	0.5	-2.3	-1.9	2.0	-6.0	12.9	13	-13.2	3	84	76	85	82	0.7	1.7	0.9	1.1	7.6	6.5	5.8	6.5
Rok	–	–	–	–	5.3	11.2	6.1	7.2	12.9	2.0	34.7	5.VII	-19.2	1.II	–	–	–	–	–	–	–	–	6.3	6.5	5.9	6.2

Brzezna

$H_s = 320\ m$ $h_w = 18\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU [%] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max<0	Max<10	Max>25	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	≡	≤0	≤-5	≤-10	≤-20
I	6.5	4.1	2	5.2	0.5	4.0	6.5	3.8	25.5	4.3	7.5	4.1	40.5	4.3	8	2.2	28	28	25.8	8.5	5	26	7	7	-	10	7	-	4	-	-	-	-	10	-
II	2	2.5	-	-	0.5	5.0	14.5	5.3	24.5	6.5	15	8.6	8	3.4	6.5	3.8	13	3.7	18.4	6.8	25	15	2	-	-	8	6	-	4	4	-	-	3	15	-
III	16	2.8	5.5	3.0	1	1.0	13	5.9	12	4.5	7.5	3.3	4	3.4	10	3.0	24	2.8	34.9	12.5	24	16	4	1	-	7	6	1	1	-	-	-	6	9	-
IV	14	3.1	4.5	2.6	3	1.2	4	1.7	14.5	2.1	3	1.0	16.5	2.5	6.5	3.6	25	1.8	47.8	13.1	11	9	-	-	-	16	10	2	-	-	-	4	4	13	-
V	25.5	2.7	4	2.0	8	1.2	5	2.1	12.5	2.6	2.5	2.0	16	3.0	11.5	2.5	8	2.3	64.2	16.0	10	-	-	-	-	13	11	2	1	-	-	2	1	10	-
VI	5.5	2.9	1.5	1.7	3.5	1.0	13.5	4.2	20.5	4.8	6	3.7	8.5	2.8	14	3.1	18	2.9	39.9	9.4	22	-	-	-	15	15	12	-	-	-	-	6	3	2	-
VII	6.5	4.5	0.5	3.0	1	1.5	6.5	2.3	12	3.1	8	2.6	17.5	2.4	7	2.9	34	1.8	141.9	30.9	24	-	-	-	14	17	13	6	1	1	-	5	2	12	-
VIII	8	2.5	2.5	1.0	1.5	1.7	3	1.7	1.5	2.4	12	3.2	23	2.9	5	3.2	23	2.0	94.5	23.2	28	-	-	-	8	17	13	3	1	-	-	4	-	8	-
IX	11.5	2.7	3.5	4.4	0.5	7.0	2	1.5	10.5	3.4	1.4	3.7	1.4	3.7	11	3.9	23	2.6	63.4	18.8	4	1	-	-	2	15	10	2	1	-	-	-	1	10	-
X	7	1.9	6	3.4	6.5	2.2	9.5	2.7	12.5	2.2	6	2.7	5	2.0	3.5	1.3	37	1.4	29.6	11.0	22	3	-	-	-	4	3	1	1	-	-	-	5	5	-
XI	8.5	4.3	7.5	2.7	1	1.0	20.5	4.2	1.5	4.2	11.5	4.3	3	4.2	7	2.2	16	3.6	30.2	11.4	29	10	2	1	-	7	4	1	2	-	-	-	5	16	-
XII	9.5	3.5	4	10.4	2	12.2	7.5	6.1	1.7	3.8	11.5	4.6	5.5	3.4	10	3.2	21	4.1	48.2	5.7	5	26	9	1	-	8	5	-	7	5	-	-	8	17	-
Rok	12.0.5	3.1	4.1.5	3.3	3.4	3.0	10.4.5	3.5	19.4.5	3.6	10.4.5	3.2	13.0.5	3.2	9.8	3.3	27.0	2.6	60.5.5	30.9	24.VIII	10.6	24	10	39	13.7	10.0	48	23	7	-	18	36	13.2	-

Ptaszkowa

$H_s = 522\ m$ $h_w = 17\ m$

I	1	2.0	7	3.9	11	1.9	10	4.0	11	3.5	21	4.9	11	3.5	3	9.3	18	3.2	50.3	15.0	5	29	9	3	-	14	10	2	1	-	-	-	-	14	27
II	-	-	6	2.2	5	3.0	15	4.7	26	5.2	19.5	4.5	9	4.2	10	4.0	7	4.0	34.8	7.5	25	16	2	-	-	11	9	-	1	-	-	-	2	14	13
III	3.5	4.7	4	2.9	1.5	3.1	3.5	3.9	10	5.2	17.5	6.0	12	5.8	9.5	4.3	18	3.8	45.3	18.7	24	17	6	1	-	11	8	1	1	1	-	-	6	10	13
IV	13	3.0	10.5	3.0	7	2.9	25	4.0	13.5	3.9	11	3.5	8.5	3.5	4	4.1	20	2.6	68.3	18.5	11	7	-	-	-	16	11	2	-	-	-	2	5	15	5
V	5	2.4	1.5	3.9	9	2.9	2	3.5	6	3.4	11	4.5	21	3.1	9	3.8	16	2.9	95.9	22.2	10	2	-	-	-	16	12	3	-	-	-	1	1	16	3
VI	5	2.7	5	2.6	3.5	3.4	5	5.3	11	5.2	22	3.9	9	4.1	6.5	3.5	23	3.0	47.9	9.0	20	-	-	-	7	14	9	-	1	-	-	5	5	2	-
VII	1	5.0	4	3.0	4	3.0	1.5	3.7	6.5	3.6	23	3.4	26	4.0	4	3.8	23	2.8	178.2	32.0	15	-	-	-	9	22	17	5	1	-	-	7	2	12	-
VIII	0.5	4.0	2	3.5	3	3.3	2	6.5	5.5	5.3	28.5	3.5	21	4.1	8.5	3.8	22	2.9	128.5	27.8	28	-	-	-	4	18	16	3	-	-	-	6	1	3	-
IX	6.5	2.6	3.5	2.3	4	2.0	1	3.0	6.5	3.9	22.5	4.4	27.5	4.4	3.5	3.4	15	3.3	102.1	27.2	4	-	-	-	2	17	13	1	1	-	-	-	4	12	-
X	1.5	3.3	2	2.5	8	2.4	0.5	3.0	19.5	3.1	12	4.1	15.5	2.7	4	3.0	30	2.1	41.8	15.8	20	1	-	-	-	8	4	2	-	-	-	7	5	-	-
XI	-	-	1.8	4.3	10	2.7	2	3.5	13	6.4	10	7.3	8	5.5	5	7.0	24	3.8	43.8	15.0	11	13	3	1	-	10	6	1	4	-	-	-	6	14	1
XII	3	3.7	8	3.0	10	2.1	6	5.6	8.5	5.3	15.5	5.2	8	4.9	10	3.4	24	3.1	25.0	8.0	5	28	11	2	-	14	6	-	3	-	-	-	4	16	11
Rok	40	2.8	8.5	3.1	89.5	2.7	37.5	4.2	13.6	4.5	21.3.5	4.6	17.6.5	4.2	7.7	4.4	24.0	3.1	85.8.9	32.0	15.VII	11.3	3.1	7	2.2	17.1	12.1	20	16	1	-	21	43	13.5	7.3

Babia Góra

$H_s = 1180\ m$ $h_w = 16\ m$

I	-	-	-	-	-	-	4.5	4.0	16.5	4.2	22	5.3	8.5	4.0	11.5	7.8	30	3.5	80.4	24.0	6	28	17	4	-	12	10	2	5	-	8	-	3	18	31
II	3.5	2.9	-	-	-	-	3	11.3	27	6.4	19.5	5.6	7	5.1	13	4.5	11	5.0	78.8	14.0	25	24	11	3	-	16	14	2	4	-	12	-	3	14	28
III	7.5	2.8	2	2.0	1	2.0	1	2.0	22.5	4.3	12.5	4.4	16	4.5	8.5	7.6	22	3.4	115.4	28.2	15	23	6	4	-	13	12	4	4	-	7	1	8	12	31.1
IV	14	2.4	6	3.0	4	4.0	2	3.0	19	3.8	4	3.5	6.5	2.7	9.5	3.3	25	2.3	100.8	23.1	7	17	4	-	-	19	17	3	-	-	11	2	5	15	-
V	13	3.2	11.5	4.0	1.5	4.3	2.5	3.4	16	2.7	5	2.4	5	2.0	12.5	3.1	26	2.2	102.1	19.4	14	16	5	-	-	15	12	4	-	-	14	2	1	19	7
VI	8.5	3.0	3	2.7	1	2.0	5.5	6.2	32.5	4.8	5	4.8	6.5	3.5	9	3.8	19	3.4	46.7	13.1	22	-	-	-	-	13	11	1	2	-	4	4	5	7	-
VII	5.5	2.7	1	2.0	-	-	-	-	1.8	3.9	8	5.0	13	4.3	19.5	4.4	28	2.9	298.7	67.8	16	-	-	-	2	23	20	11	-	-	14	6	-	18	-
VIII	7.5	2.4	-	-	-	-	3	1.7	15.5	5.0	9.5	4.0	16	3.7	11.5	3.6	30	2.6	122.2	47.5	28	-	-	-	-	16	12	3	1	-	8	2	1	7	-
IX	3	2.0	2	5.0	1	2.0	-	-	17.5	4.5	10.5	3.9	3.2	5.0	5	5.2	19	3.8	154.5	39.2	4	4	-	-	-	19	16	6	2	-	9	1	4	15	-
X	0.5	2.0	-	-	-	-	-	-	2.8	4.5	17	5.6	9	3.3	9.5	3.5	29	3.1	50.0	17.1	22	6	-	-	-	8	8	2	1	-	9	-	9	7	-
XI	-	-	5	2.6	0.5	3.0	0.5	3.0	3.2	5.9	6	5.0	17.5	4.8	0.5	7.0	28	3.6	59.8	20.4	28	18	11	2	-	10	9	2	4	-	14	-	7	18	-
XII	-	-	-	-	2	3.5	2	13.5	13	8.1	22	7.8	14	4.4	1	3.5	39	4.0	40.0	7.7	13	31	19	6	-	10	10	-	7	1	16	-	5	8	-
Rok	5.5	2.0	30.5	1.8	11	1.7	24	4.0	25.7.5	4.8	14.1	4.9	13.1	3.9	11.1	4.8	30.6	3.3	12.8.4	67.8	15.VII	16.7	73	19	2	17.4	15.1	40	30	1	12.6	18	51	15.8	-

Kamienica

$H_s = 460\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	30.8	9.1	6	28	9	8	-	19	9	-	-	-	21	-	-	11	27
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.4	8.9	25	24	2	-	-	12	9	-	-	-	3	-	2	13	13
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	45.8	13.4	16	19	3	3	-	10	6	1	-	-	1	-	5	7	11
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.2	13.7	11	10	-	-	-	18	9	1	-	-	2	2	4	12	2
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	66.3	12.1	20	-	-	-	-	16	12	1	-	-	1	2	-	19	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.8	5.2	22	-	-	-	10	9	7	-	-	-	2	6	6	2	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	178.4	59.2	15	-	-	-	11	18	15	7	-	-	-	4	1	18	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78.0	28.0	28	-	-	-	6	14	10	3	-	-	-	3	2	8	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	65.8	15.7	4	2	-	-	2	14	10	2	-	-	3	-	2	10	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.6	10.8	22	6	-	-	-	6	4	1	-	-	6	-	8	3	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.4	14.7	29	11	2	1	-	9	6	2	-	-	3	-	4	14	1
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	22.5	5.6	8	27	9	4	-	11	6	-	-	-	1	-	2	10	11
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	658.0	59.2	15.VII	127	25	16	29	156	103	18	-	-	24.1	17	36	119	65

Raba Wyżna

$\varphi = 49°34'$ $\lambda = 19°53'$ **1957**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-3.3	0.5	-2.1	-1.8	1.6	-4.6	9.4	10	-16.3	17	–	–	–	–	–	–	–	–	8.3	7.2	5.6	7.0
II	–	–	–	–	0.0	4.4	1.8	2.0	5.8	-1.3	11.1	21	-10.5	23	–	–	–	–	–	–	–	–	6.2	6.0	5.7	6.0
III	–	–	–	–	-0.5	6.3	3.5	3.2	8.0	-2.5	14.7	21	-4.5.2	4	–	–	–	–	–	–	–	–	5.3	5.1	4.6	5.0
IV	–	–	–	–	4.6	10.4	6.8	7.2	11.8	2.1	24.1	30	-5.9	15	–	–	–	–	–	–	–	–	6.1	6.3	6.2	6.2
V	–	–	–	–	7.4	11.0	8.4	8.8	12.6	4.6	21.6	19	0.1	25	–	–	–	–	–	–	–	–	6.4	6.9	7.1	6.8
VI	–	–	–	–	14.7	24.2	16.4	17.2	22.8	10.1	29.4	11,30	5.1	27	–	–	–	–	–	–	–	–	3.6	4.3	4.2	4.0
VII	–	–	–	–	16.2	20.7	17.0	17.7	22.3	13.0	33.4	5,8	8.6	30	–	–	–	–	–	–	–	–	5.9	6.2	6.7	6.3
VIII	–	–	–	–	12.5	19.6	14.1	15.1	20.5	9.8	28.9	12	5.1	31	–	–	–	–	–	–	–	–	4.3	5.1	5.0	4.8
IX	–	–	–	–	9.4	14.6	10.4	11.2	15.7	7.2	25.0	9	0.0	27	–	–	–	–	–	–	–	–	5.8	6.5	5.9	6.0
X	–	–	–	–	5.8	13.6	7.0	8.4	14.2	3.2	22.0	19	-1.8	3	–	–	–	–	–	–	–	–	4.7	4.1	2.8	3.9
XI	–	–	–	–	2.0	6.6	2.8	3.5	7.5	0.1	18.2	5	-12.5	30	–	–	–	–	–	–	–	–	6.4	5.8	6.4	6.2
XII	–	–	–	–	-2.2	0.4	-1.3	-1.1	2.1	-5.3	12.5	13,14	-13.5	3	–	–	–	–	–	–	–	–	5.8	5.8	6.7	6.4
Rok	–	–	–	–	5.6	10.8	7.1	7.6	12.1	3.0	33.4	5.8.VII	-16.3	17.1	–	–	–	–	–	–	–	–	5.8	5.8	5.6	5.7

Iwonicz

$\varphi = 49°34'$ $\lambda = 21°48'$

I	972.9	983.4	958.0	1023.6	-2.9	-1.6	-2.7	-2.5	-0.6	-5.1	4.7	3	-14.0	17	86	82	86	85	0.7	1.0	0.7	0.8	7.9	8.0	7.5	7.8
II	964.8	980.6	942.4	1014.5	0.6	2.4	1.4	1.4	3.8	-0.9	10.9	19	-7.9	28	93	83	88	88	0.4	1.3	0.8	0.8	9.0	8.0	6.5	7.8
III	970.3	983.8	953.0	1020.1	-1.0	4.8	1.2	1.6	6.2	-3.1	15.8	30	-16.7	4	83	68	80	77	1.1	3.5	1.5	2.0	5.9	5.5	4.5	5.3
IV	969.3	980.1	946.2	1018.0	5.5	11.5	7.0	7.8	12.8	2.7	24.3	30	-2.7	16	87	63	82	77	1.6	6.4	2.1	3.4	6.4	6.8	4.9	6.0
V	967.1	975.3	955.8	1015.4	7.9	11.4	7.7	8.7	13.2	4.5	21.4	17,20	-0.6	7	88	72	92	84	1.4	4.6	0.9	2.4	7.4	8.3	6.1	7.3
VI	970.2	982.2	959.3	1017.3	16.4	21.4	15.3	17.1	22.8	10.9	31.2	12	5.4	28	84	62	86	76	3.8	10.3	2.8	6.6	5.1	5.4	3.5	4.7
VII	966.3	976.2	956.3	1013.0	16.8	21.7	16.3	17.8	23.1	13.2	31.9	8	8.4	4	–	–	–	–	–	–	–	–	6.7	6.7	6.9	6.8
VIII	966.2	977.3	956.3	1015.4	14.5	19.7	14.3	15.7	20.9	10.8	29.8	14	6.2	23,31	90	69	93	84	1.9	7.8	1.4	3.7	5.6	6.4	5.0	5.7
IX	962.4	975.8	956.2	1015.8	9.9	14.6	10.9	11.8	15.8	7.5	25.0	9	-0.5	27	94	76	92	87	0.8	4.3	1.2	2.1	7.0	7.3	6.1	6.8
X	973.3	984.7	957.3	1021.9	6.6	12.6	8.1	8.8	13.2	4.3	17.3	19,20	-3.4	3	89	66	83	79	1.2	5.3	2.1	2.8	5.3	4.6	4.4	4.8
XI	972.3	983.8	956.6	1021.8	3.3	5.4	3.2	3.8	6.5	1.3	16.4	9	-11.6	30	86	79	86	84	1.1	2.5	1.3	1.6	7.3	6.5	6.3	6.7
XII	969.2	986.5	953.3	1017.5	-2.5	-1.2	-1.7	-1.8	0.0	-4.7	11.5	14	-11.9	11	86	82	87	85	0.7	1.1	0.8	0.9	6.8	7.6	7.1	7.2
Rok	969.1	980.8	955.3	1017.8	6.3	10.2	6.8	7.5	11.5	3.4	31.9	8.VII	-16.7	4.III	–	–	–	–	–	–	–	–	6.2	6.8	5.7	6.4

Sanok

$\varphi = 49°34'$ $\lambda = 22°12'$

I	–	–	–	–	-2.1	0.0	-2.0	-1.5	1.2	-4.6	6.7	3	-12.1	19	–	–	–	–	–	–	–	–	8.9	8.7	9.3	9.0
II	–	–	–	–	1.7	4.4	2.6	2.8	5.9	0.0	14.1	19	-7.1	28	–	–	–	–	–	–	–	–	9.4	8.8	8.5	8.9
III	–	–	–	–	-0.8	6.0	1.5	2.0	7.9	-2.8	18.2	30	-18.4	4	–	–	–	–	–	–	–	–	5.8	6.7	5.1	5.9
IV	–	–	–	–	4.4	12.6	7.5	8.0	14.2	2.3	25.5	30	-3.6	16	–	–	–	–	–	–	–	–	6.6	7.6	5.7	6.6
V	–	–	–	–	7.7	12.4	9.0	9.5	14.7	4.7	23.5	14	-0.1	7	–	–	–	–	–	–	–	–	7.6	9.0	7.9	8.2
VI	–	–	–	–	15.7	22.6	16.1	17.6	24.1	10.8	33.1	12	3.9	1	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	16.7	22.5	17.2	18.4	24.7	13.5	33.2	8	8.4	29	–	–	–	–	–	–	–	–	6.5	8.3	6.9	7.2
VIII	–	–	–	–	13.5	20.9	14.9	16.0	22.4	11.0	31.5	14	5.4	31	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	9.9	15.5	11.2	12.0	17.2	7.8	26.1	9	0.1	26	–	–	–	–	–	–	–	–	8.2	8.3	8.0	8.2
X	–	–	–	–	5.1	13.6	7.1	8.2	14.7	3.2	19.9	19	-3.6	3	–	–	–	–	–	–	–	–	5.6	5.5	5.2	5.4
XI	–	–	–	–	2.4	6.8	2.9	3.8	8.2	0.5	16.7	2,3,5	-9.8	29	–	–	–	–	–	–	–	–	7.0	7.4	6.4	6.9
XII	–	–	–	–	-1.9	0.4	-0.6	-0.7	2.9	-3.5	13.7	13	-10.6	11	–	–	–	–	–	–	–	–	7.6	8.2	7.8	7.9
Rok	–	–	–	–	6.0	11.5	7.3	8.0	13.2	3.6	33.2	8.VII	-18.4	4.III	–	–	–	–	–	–	–	–	–	–	–	–

Konieków

$\varphi = 49°33'$ $\lambda = 18°57'$

I	–	–	–	–	-4.3	-1.8	-3.5	-3.3	-0.2	-5.5	6.6	23	-18.8	17	–	–	–	–	–	–	–	–	9.0	7.6	7.8	8.1
II	–	–	–	–	-0.8	1.1	0.1	0.1	3.1	-2.2	8.5	19	-8.7	28	–	–	–	–	–	–	–	–	8.6	8.4	8.5	8.5
III	–	–	–	–	0.2	5.0	2.1	2.4	6.7	-1.1	13.5	23	-8.9	1	–	–	–	–	–	–	–	–	6.6	6.1	4.4	5.7
IV	–	–	–	–	4.3	8.0	5.4	5.8	9.9	2.5	21.7	30	-4.7	14	–	–	–	–	–	–	–	–	6.0	6.8	6.6	6.5
V	–	–	–	–	6.4	9.2	7.1	7.4	11.4	4.3	21.5	19	-1.6	7	–	–	–	–	–	–	–	–	7.1	8.3	6.4	7.3
VI	–	–	–	–	14.5	19.1	15.6	16.2	21.1	11.3	27.2	30	5.6	2	–	–	–	–	–	–	–	–	4.4	6.2	4.4	5.0
VII	–	–	–	–	14.8	18.6	15.5	15.1	20.5	12.8	34.1	8	8.7	17,28	–	–	–	–	–	–	–	–	7.2	6.9	6.4	6.8
VIII	–	–	–	–	12.3	16.9	12.9	13.8	18.6	10.0	25.4	12	5.7	31	–	–	–	–	–	–	–	–	6.5	6.8	3.8	5.7
IX	–	–	–	–	7.8	11.7	9.2	9.5	13.7	6.6	23.0	9	-0.4	27	–	–	–	–	–	–	–	–	6.7	6.9	5.8	6.5
X	–	–	–	–	6.0	10.7	7.5	7.9	11.9	4.9	18.0	19	-0.5	3	–	–	–	–	–	–	–	–	5.0	4.5	3.4	4.3
XI	–	–	–	–	2.3	4.5	2.7	3.0	6.1	1.0	14.6	4	-13.4	30	–	–	–	–	–	–	–	–	7.3	6.7	6.6	6.9
XII	–	–	–	–	-3.3	-1.9	-2.5	-2.6	0.1	-5.0	11.5	13	-13.0	1	–	–	–	–	–	–	–	–	8.2	8.2	8.6	8.3
Rok	–	–	–	–	5.0	8.4	6.0	6.4	10.2	3.3	34.1	8.VII	-18.8	17.1	–	–	–	–	–	–	–	–	6.9	7.0	6.1	6.7

Raba Wyżna

$H_s = 600\ m$ $h_w = 16\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU [%] N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (-) Temperatura T Max≤0	Max≥10	Max≥25	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	≡	≤0.2	≥0.2	≥0.5	≥0.8
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n																		
I	3.5	2.7	·	·	8	1.5	2	4.0	46	18	5	2.2	3	4.3	3.5	2.4	22	1.5	50.0	11.2	28	25	8	5	·	10	8	1	–	–	–	·	2	12	27
II	8.5	2.3	·	·	·	·	0.5	2.0	4.5	2.0	5.5	2.4	4	2.2	2.5	1.8	18	1.6	54.4	28.6	26	15	2	1	·	12	9	1	–	–	–	·	4	10	10
III	24.5	1.8	2	2.2	·	·	3	2.5	4.8	2.1	5	2.7	2	2.0	2.5	2.8	9	1.9	42.1	17.1	17	16	3	4	·	10	7	1	–	–	–	1	9	10	14
IV	2.9	1.5	2.5	2.0	10	2.4	2.5	2.0	24.5	1.8	2	2.5	4	1.8	2.5	1.4	13	1.5	67.2	16.9	7	7	·	·	·	18	12	2	–	–	–	·	6	15	4
V	4.0	2.1	8	2.6	1	3.0	2	1.5	10.5	1.7	1.5	1.7	3	1.3	2	2.0	25	1.5	42.1	14.1	20	·	·	·	·	11	8	2	–	–	–	·	5	18	·
VI	1.4	1.8	3	1.7	1	3.0	4.5	1.0	3.2	1.7	4.5	2.2	1	3.0	7	1.6	23	1.3	37.9	7.0	5	·	·	·	9	9	8	·	–	–	–	3	6	2	·
VII	7	1.4	2	1.5	2	4.0	1.2	1.6	1.8	2.0	1.3	1.8	2	1.0	4	2.0	33	1.2	44.9	30.4	15	·	·	·	9	19	18	4	–	–	–	5	6	14	·
VIII	1.0	1.2	·	·	·	·	3	1.0	1.8	1.3	1.6	1.8	2	2.0	1.7	1.2	27	1.0	83.0	18.5	28	·	·	·	4	10	8	5	–	–	–	3	8	5	·
IX	5	1.0	3	1.0	1	1.0	5	1.0	2.6	1.8	1.7	2.8	5	1.4	1.0	1.2	18	1.4	62.2	12.8	4	·	·	·	·	14	12	1	–	–	–	·	5	10	·
X	3	1.0	·	·	·	·	1.4	1.5	1.0	1.2	1.7	1.0	·	·	3	1.0	26	0.8	26.1	12.0	22	2	·	·	·	4	4	1	–	–	–	·	1.0	5	·
XI	1	3.0	8	1.5	3	1.0	2.0	1.0	2.4	1.2	7	1.0	2	2.0	6	3.5	19	1.1	24.8	8.2	29	11	1	1	·	8	4	·	–	–	–	·	7	14	1
XII	4	1.0	·	·	2	1.0	3.5	1.4	1.9	2.4	2.1	2.0	1	1.0	8	2.0	3	1.7	37.0	12.5	8	29	10	3	·	12	8	1	–	–	–	·	8	15	11
Rok	14.6.5	1.7	28.5	1.0	28	1.4	10.3.5	1.4	3.5.1	1.8	10.4.5	2.0	29	1.8	6.8	1.9	2.56	1.4	666.7	30.4	16.VII	1.05	24	1.4	21	1.37	1.06	1.9	–	–	–	1.2	76	1.30	67

Iwonicz

$H_s = 410\ m$ $H_b = 403{,}4\ m$ $h_w = 16\ m$

I	5.5	1.7	2.5	4.4	0.5	4.0	3	5.5	36.5	5.6	17.5	5.5	4.5	2.0	6	1.2	17	3.8	24.9	6.4	6	28	14	3	·	11	9	·	7	3	·	·	1	16	30
II	3	1.5	·	·	·	·	8	5.9	4.1	5.7	9	3.7	1.5	3.3	4.5	2.1	17	4.0	38.8	13.1	25	14	4	·	·	14	10	1	5	·	2	·	1	16	13
III	9.5	2.1	9	2.7	1.5	2.7	2	5.0	1.8	3.9	6	2.9	5	2.1	6	2.0	33	1.9	42.7	10.7	16	19	9	6	·	10	9	2	1	·	3	·	8	9	14
IV	10.5	2.0	4.5	2.4	·	·	2	1.8	1.4	2.4	4	1.6	1	1.5	9	1.6	45	1.0	58.2	18.8	11	8	·	·	·	15	11	1	·	·	7	1	5	11	1
V	1.7	2.3	9	3.2	1	1.0	·	·	4.5	1.9	3	1.7	4	1.6	1.4.5	1.6	40	1.2	118.4	3.3.2	9	2	·	·	·	18	12	5	·	·	3	3	·	1.5	3
VI	4.5	1.9	2.5	1.0	·	·	6.5	1.8	2.5	1.0	2.5	2.4	1	2.5	9	2.3	39	1.9	117.0	5.4.1	8	·	·	·	5	10	8	3	2	·	1	8	4	1	·
VII	2.5	2.4	1	3.0	1	3.0	1.5	2.0	1.6	2.1	9.5	1.9	1	3.0	5.5	1.6	55	0.8	160.3	3.7.1	14	·	·	·	9	20	1.7	6	·	·	1	8	2	1.5	·
VIII	4	1.8	3.5	1.9	·	·	3	5.8	11.5	3.7	5	2.5	5	1.5	1.2	1.8	49	1.2	78.7	24.2	29	·	·	·	5	15	10	3	1	·	1	2	2	6	·
IX	2.5	1.2	3.5	1.0	·	·	0.5	4.0	2.1	3.0	12.5	2.8	4.5	1.7	6.5	3.1	39	1.5	93.0	26.3	12	1	·	·	·	16	12	2	·	·	4	1	3	13	·
X	1	1.5	·	·	·	·	1.5	3.3	26.5	5.5	1.6	2.9	2	1.5	5	1.9	41	2.3	23.1	11.0	20	3	·	·	·	1	3	1	3	1	1	·	10	7	·
XI	2.5	1.2.0	1.1	2.7	·	·	6	2.2	2.9.5	4.5	1.1	2.6	3	3.7	1	5.9	23	3.1	39.0	13.1	11	1.5	2	1	·	8	5	2	5	1	2	·	1	1.4	1
XII	1.3	2.8	1.5	2.3	·	·	3	6.0	3.5.5	5.2	1.9	5.1	1.5	1.3	6.5	2.8	1.3	3.9	22.9	7.2	5	29	1.3	2	·	7	6	·	3	2	1	·	5	1.8	1.2
Rok	7.5.5	6.3	7.8.5	2.0	4	0.9	3.7	4.0	2.56.5	4.0	1.17	3.0	3.5	2.1	88.5	2.3	4.11	2.2	8.17.0	54.1	8.31	1.19	47	1.2	1.9	1.49	1.1.2	2.6	27	7	2.9	2.3	45	1.41	7.4

Sanok

$H_s = 314\ m$ $h_w = 16\ m$

I	1	4.0	3.5	4.3	6.5	4.6	2.6	4.4	1.4	4.9	1	3.0	1.2	5.5	1	3.0	2.8	3.3	1.8.6	5.6	2.8	2.7	1.0	5	·	1.0	8	·	2	·	1	–	·	2.6	2.4
II	3	3.7	·	·	2.5	5.0	1.8	4.4	1.9	5.6	2.5	3.0	6	5.3	5	4.2	2.8	3.2	2.6.8	8.4	2.5	1.6	·	·	·	1.3	8	·	3	·	·	–	·	2.2	9
III	5.5	4.5	3	4.7	1.0	3.9	1.1	3.9	7	5.6	·	·	9	5.4	4.5	5.2	4.3	2.5	4.3.8	1.1.0	2.5	2.1	3	2	·	9	6	1	·	·	·	–	·	7.1	2.2	1.4
IV	7.5	2.5	8.5	3.5	4.5	3.7	6.5	3.5	3.5	3.0	0.5	3.0	1.0.5	3.3	4.5	4.0	44	1.7	4.8.2	1.3.5	1.1	1.1	·	·	1	1.1	9	1	·	·	2	–	6	1.4	·
V	1.0.5	3.8	1.8.5	3.7	1.5	2.3	5	2.8	2	2.5	·	·	4.5	3.4	9	2.9	42	1.9	1.1.9.6	2.9.2	6	1	·	·	·	1.6	1.4.4	4	·	·	1	–	·	1.1.1	1
VI	7.5	3.0	3.5	4.1	3.5	4.1	1.9.5	3.8	9.5	4.7	0.5	4.0	7	3.9	3	3.0	3.6	2.3	9.7.9	2.5.0	4	·	·	·	1.2	1.0	1.0	3	·	·	·	–	–	–	·
VII	2	3.0	2	4.0	2.5	2.6	1.1	3.1	1.3	3.4	1.5	3.0	1.1	2.2	2	3.0	4.8	1.5	1.3.2.5	1.7.6	2.1	·	·	·	1.2	1.6	1.4	8	·	·	·	–	·	1.6	·
VIII	4.5	2.4	·	·	4	2.5	9	3.0	1.2	4.2	3	2.3	1.1.5	4.3	4	3.6	4.5	1.8	8.8.6	3.1.0	2.9	·	·	·	7	1.5	1.2	1	·	·	2	–	–	–	·
IX	2.5	3.6	0.5	2.0	6	5.0	1.1.5	3.3	1.4.5	4.7	3	3.7	7	6.6	4	2.8	4.1	2.4	1.1.6.2	2.3.1	1.2	4	·	·	2	1.7	1.3	3	1	·	3	–	2	2.3	·
X	0.5	3.0	3	3.0	4	5.2	1.2.5	3.9	1.4.5	4.3	2.5	3.0	2.5	5.4	2.5	4.6	5.1	1.8	9.3.1	6.7	2.0	4	·	·	·	3	2	·	·	·	1	–	6	9	·
XI	0.5	9.0	1.0	4.4	5.5	4.5	9	2.4	1.5	5.0	6.5	5.4	2	6.5	4.5	9.9	3.7	2.9	3.0.9	4.0.8	2.8	1.2	1	·	·	6	3	2	2	·	·	–	4	1.6	1
XII	8.5	3.8	5.5	3.5	7.5	3.7	1.1	4.9	2.7	5.3	1	9.0	2	3.0	6.5	6.4	2.1	3.7	3.3.3	8.9	1.1	2.7	7	1	·	9	7	·	3	·	·	–	·	1.6	1.1
Rok	5.3.5	3.9	5.8	3.1	5.8	3.8	1.5.3	3.6	1.5.1	4.4	2.2	3.3	8.5	4.6	5.0.5	4.4	1.6.4	2.4	1.7.6.5	3.4.0	2.9.VIII	1.2.0	2.1	8	8.4	1.1.5	1.0.6	2.3	1.1	·	1.0	–	–	–	6.0

Koniaków

$H_s = 740\ m$ $h_w = 16\ m$

I	8.5	1.0	5.5	3.2	4.5	2.1	3.5	2.1	3.4.5	2.4	1.3	3.6	2	3.2	1.1.5	3.5	1.8	2.3	4.5.9	2.5.2	6	3.0	1.6	7	·	1.3	8	1	·	·	6	·	·	2.1	2.9
II	5.5	2.2	4	2.1	4.6	2.7	3	3.7	3.7	2.7	1.7.5	3.6	1.5	3.0	5	2.5	6	2.7	6.0.5	1.1.3	2.5	2.3.1	5	·	·	1.8	1.3	1	·	·	9	·	·	2.0	2.4
III	6	2.9	6.5	3.6	2.0	4.4	6	3.1	2.3.5	4.1	1.4	3.9	3.5	3.7	8.5	2.8	5	3.6	8.3.8	8.3.5	1.9	1.7	4	·	·	1.5	1.0	2	1	1	2	1	6	1.0	1.5
IV	1.4	3.6	1.5.5	3.2	1.1.5	3.2	9.5	2.7	8	4.1	2.5	3.0	4.5	3.3	1.5.5	2.9	9	2.9	6.5.6	1.1.8	7	1.2	·	·	·	1.7	1.1	1	·	·	8	2	3	1.2	4
V	1.9	3.9	2.6.5	5.0	6.5	3.6	7.5	2.8	9.5	2.8	4	2.6	3.5	2.9	1.0.5	3.5	6	3.6	6.8.4	2.4.0	2.0	4	·	·	·	1.3	9	2	·	·	6	1	1	1.5	1
VI	6.5	3.0	8	3.4	1.1.5	3.8	7	2.9	2.5.5	3.4	7.5	3.7	5	2.0	1.0	2.4	9	2.9	5.1.9	4.8.2	9	·	·	·	5	1.0	7	1	·	·	2	5	6	5	·
VII	4	1.4	5.5	1.8	1.2	2.9	7	2.7	2.8	3.3	8.5	3.1	4	3.2	1.9	3.0	5	2.8	2.4.0.7	5.7.3	1.5	·	·	·	7	2.2	2.1	8	·	·	7	8	3	1.5	·
VIII	7.5	1.8	7	1.5	3.5	2.9	8	2.6	2.3.5	3.6	4	3.4	6.5	3.9	1.5	3.3	2.0	2.4	7.9.9	2.5.0	2.8	·	·	·	3	1.6	1.0	2	1	1	3	3	1	4	·
IX	5	2.5	2.5	2.0	8	1.3	5.5	1.9	2.9.5	3.8	1.7	4.1	5	5.0	7.5	3.0	1.0	3.0	1.2.4.7	1.7.2	2.3	1	·	·	·	1.9	1.5	6	·	·	7	·	4	1.0	·
X	3	1.7	7.5	1.7	6	2.3	9.5	2.4	3.6.5	3.6	1.5.5	3.1	2	2.2	2	2.0	1.1	2.6	2.2.7	9.6	2.2	2	·	·	·	6	3	·	·	·	4	·	7	4	·
XI	5.5	6.2	8.5	6.1	1.0.5	3.5	1.7	3.1	2.5	4.3	1.1.5	8.2	1.5	4.3	3.5	6.7	7	3.9	3.0.2	1.8.9	2.3	1.6	3	1	·	9	4	1	3	·	7	·	4	1.7	1
XII	8.5	3.5	8	4.1	5	3.4	5.6	2.5	4.1	3.8	1.5	5.0	1.5	3.7	8.5	3.4	2	3.8	3.6.8	1.2.1	1.4	2.8	1.9	2	·	1.4	8	1	·	·	7	·	2	2.4	1.1
Rok	8.5	2.8	1.0.3	3.1	1.0.3.5	3.0	8.9	2.7	3.2.1.5	3.5	1.2.3	3.5	4.0.5	3.5	1.1.6.5	3.2	4.0.8	3.0	9.1.1.1	5.7.3	1.5.VII	1.3.3	4.7	4.0	1.5	1.7.2	1.1.9	2.6	5	2	6.8	2.2	3.5	1.5.7	9.1

Stańcowa

$\varphi = 49°33'$ $\lambda = 19°32'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA t										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI d_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	Średnia I	II	III	Dzień	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień
I	–	–	–	–	-3.8	-0.3	-2.9	-2.5	0.6	-5.8	5.9	2	-21.1	17	–	–	–	–	–	–	–	–	7.2	7.0	7.2	7.1
II	–	–	–	–	-1.4	1.6	-0.4	-0.2	3.0	-2.8	9.8	3	-11.0	28	–	–	–	–	–	–	–	–	7.8	8.4	7.6	7.9
III	–	–	–	–	-4.0	5.4	0.6	1.4	6.5	-5.4	13.9	20	-13.5	6	–	–	–	–	–	–	–	–	5.6	6.0	5.3	5.6
IV	–	–	–	–	3.8	8.7	3.8	5.0	9.9	0.6	20.6	29	-7.2	14	–	–	–	–	–	–	–	–	5.6	5.9	6.9	6.5
V	–	–	–	–	5.6	8.9	6.3	6.3	10.7	2.8	20.4	19	-2.1	9	–	–	–	–	–	–	–	–	7.0	7.9	6.7	7.2
VI	–	–	–	–	14.0	19.4	13.6	15.2	20.5	9.6	27.9	12	4.0	7	–	–	–	–	–	–	–	–	4.5	5.1	4.8	5.0
VII	–	–	–	–	14.6	19.1	14.2	15.5	20.0	11.6	30.5	5	7.3	29,30	–	–	–	–	–	–	–	–	6.5	6.9	6.8	6.7
VIII	–	–	–	–	12.2	16.9	12.3	13.4	18.5	8.7	26.0	14	3.4	31	–	–	–	–	–	–	–	–	4.5	6.1	4.9	5.2
IX	–	–	–	–	7.2	11.9	8.0	8.0	13.2	5.5	22.8	9	-0.7	27	–	–	–	–	–	–	–	–	6.8	7.5	7.1	7.1
X	–	–	–	–	5.3	11.1	5.9	7.0	12.1	2.9	19.2	19	-2.9	3	–	–	–	–	–	–	–	–	5.4	4.8	3.2	4.4
XI	–	–	–	–	1.4	4.1	1.4	2.1	5.4	-0.6	15.0	1	-15.1	30	–	–	–	–	–	–	–	–	6.8	6.7	6.8	6.8
XII	–	–	–	–	-3.6	-4.0	-3.1	-2.7	0.6	-5.4	8.2	13	-14.0	2	–	–	–	–	–	–	–	–	7.1	7.6	7.4	7.4
Rok	–	–	–	–	4.5	8.8	4.9	5.8	10.1	1.9	30.5	5.VIII	-21.1	17.I	–	–	–	–	–	–	–	–	6.2	6.8	6.2	6.4

Rdzawka na Obidowej

$\varphi = 49°33'$ $\lambda = 19°58'$

I	–	–	–	–	-4.0	-1.9	-3.4	-3.2	-0.7	-6.0	4.5	10	-19.0	17	–	–	–	–	–	–	–	–	8.3	7.9	6.3	7.5
II	–	–	–	–	-1.3	1.6	0.0	0.1	3.1	-2.9	9.7	3	-10.3	23	–	–	–	–	–	–	–	–	8.3	8.0	7.6	8.0
III	–	–	–	–	-4.4	4.0	1.6	1.4	6.2	-3.0	15.5	21	-11.0	6	–	–	–	–	–	–	–	–	7.3	6.1	5.0	6.1
IV	–	–	–	–	3.0	7.7	5.3	5.3	9.2	1.3	21.7	30	-4.9	8	–	–	–	–	–	–	–	–	7.4	7.8	6.9	7.4
V	–	–	–	–	5.2	8.5	6.6	6.8	10.2	3.2	18.7	19	-2.6	8	–	–	–	–	–	–	–	–	8.3	8.6	8.2	8.4
VI	–	–	–	–	13.4	18.6	15.1	15.6	20.2	10.2	26.9	30	4.9	7	–	–	–	–	–	–	–	–	6.9	7.0	6.8	6.6
VII	–	–	–	–	14.0	18.1	15.6	15.8	20.0	12.0	30.4	5,6	9.9	29	–	–	–	–	–	–	–	–	8.5	7.6	7.8	8.0
VIII	–	–	–	–	11.3	16.8	12.9	13.5	18.2	9.3	25.3	12	3.0	31	–	–	–	–	–	–	–	–	8.1	7.0	6.1	6.4
IX	–	–	–	–	7.7	11.8	9.3	9.5	13.2	5.8	22.7	9	-1.3	26	–	–	–	–	–	–	–	–	7.2	7.5	7.2	7.2
X	–	–	–	–	4.6	10.4	6.9	7.2	11.3	2.9	19.2	19	-3.3	3	–	–	–	–	–	–	–	–	7.0	5.3	3.6	5.3
XI	–	–	–	–	0.9	4.0	1.4	1.9	5.1	-1.6	14.7	5	-15.0	30	–	–	–	–	–	–	–	–	7.7	6.5	6.8	7.0
XII	–	–	–	–	-4.2	-2.1	-3.1	-3.1	-0.7	-6.5	9.9	13	-13.5	29	–	–	–	–	–	–	–	–	7.4	7.2	6.4	7.0
Rok	–	–	–	–	4.1	8.1	5.7	5.9	9.6	2.1	30.4	5,8,VII	-19.0	17.I	–	–	–	–	–	–	–	–	7.4	7.2	6.6	7.1

Turbacz

$\varphi = 49°33'$ $\lambda = 20°07'$

I	–	–	–	–	-5.1	-2.8	-4.8	-4.4	-0.8	-6.9	6.4	3	-17.5	17	–	–	–	–	–	–	–	–	7.1	5.7	5.3	6.0
II	–	–	–	–	-3.5	-0.6	-2.6	-2.3	1.7	–	9.5	6	–	–	–	–	–	–	–	–	–	–	7.1	6.7	6.7	6.8
III	–	–	–	–	-2.6	1.6	-1.8	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	4.9	5.5
IV	–	–	–	–	1.1	4.9	2.0	2.5	6.5	-0.6	17.9	30	-10.0	14	–	–	–	–	–	–	–	–	6.4	7.2	7.0	6.9
V	–	–	–	–	2.4	5.1	3.2	3.5	7.8	–	17.1	19	–	–	–	–	–	–	–	–	–	–	6.6	8.1	7.6	7.4
VI	–	–	–	–	10.4	15.4	11.5	12.2	18.0	8.3	29.4	11	2.0	21	–	–	–	–	–	–	–	–	4.5	6.0	5.3	5.3
VII	–	–	–	–	11.6	14.9	12.2	12.7	17.2	–	28.0	8	–	–	–	–	–	–	–	–	–	–	6.7	6.7	6.4	6.6
VIII	–	–	–	–	8.8	13.0	10.0	10.4	15.7	–	24.0	14	–	–	–	–	–	–	–	–	–	–	5.8	7.3	6.0	6.4
IX	–	–	–	–	5.0	8.2	5.9	6.2	10.6	3.8	20.4	9	-3.6	25,27	–	–	–	–	–	–	–	–	6.6	7.3	7.5	7.1
X	–	–	–	–	3.6	7.2	4.4	4.9	9.4	–	16.3	19	–	–	–	–	–	–	–	–	–	–	5.4	4.1	3.7	4.4
XI	–	–	–	–	-0.9	1.5	-0.7	-0.2	–	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.2	6.2	5.9
XII	–	–	–	–	-5.4	-3.8	-4.7	-4.6	–	-7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	7.5	7.4
Rok	–	–	–	–	2.1	5.4	2.9	3.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.5	6.2	6.3

ącko

$\varphi = 49°33'$ $\lambda = 20°26'$

I	–	–	–	–	-3.1	1.0	-2.5	-1.8	2.2	-5.4	8.4	2	-15.0	22	–	–	–	–	–	–	–	–	8.0	7.1	6.4	7.2
II	–	–	–	–	1.0	5.5	2.6	2.0	6.6	-0.6	12.5	6	-6.8	23,24	–	–	–	–	–	–	–	–	7.5	7.0	6.5	7.0
III	–	–	–	–	0.7	7.7	5.4	3.8	9.2	-4.0	16.4	16,27	-13.2	4	–	–	–	–	–	–	–	–	6.5	5.2	4.8	5.5
IV	–	–	–	–	4.8	12.0	7.3	7.8	13.1	2.7	24.2	28	-2.6	14	–	–	–	–	–	–	–	–	5.8	6.8	6.8	6.5
V	–	–	–	–	7.7	12.3	8.9	9.4	14.0	4.9	21.6	19	0.5	9	–	–	–	–	–	–	–	–	7.0	8.6	7.5	7.7
VI	–	–	–	–	15.4	22.5	15.5	17.2	23.9	9.3	30.1	11,12	2.8	2	82	55	82	73	3.5	+3.1	3.5	6.6	3.8	5.9	4.8	4.8
VII	–	–	–	–	16.0	21.8	17.0	18.0	23.9	12.5	34.4	5	6.5	29	–	–	–	–	–	–	–	–	5.6	7.2	7.1	7.0
VIII	–	–	–	–	13.1	20.7	15.2	15.0	21.9	10.5	30.4	14	5.1	31	–	–	–	–	–	–	–	–	5.6	6.8	6.1	6.1
IX	–	–	–	–	9.6	15.1	11.1	12.0	17.2	7.4	28.3	9	-0.3	27	89	63	86	79	1.4	7.4	2.1	3.6	6.0	7.0	6.7	6.6
X	–	–	–	–	4.9	11.4	6.9	8.3	15.2	2.9	25.2	19	-2.4	3	95	60	90	82	0.6	7.2	1.1	3.0	6.3	4.5	3.3	4.7
XI	–	–	–	–	3.1	7.4	3.7	6.0	8.4	1.0	18.3	4	-10.3	30	84	77	86	83	1.3	3.3	1.3	2.0	7.3	6.7	6.7	6.9
XII	–	–	–	–	-2.4	1.2	-1.2	-0.9	2.6	-4.5	14.3	13	-14.6	11	–	–	–	–	–	–	–	–	8.0	7.1	6.3	7.1
Rok	–	–	–	–	5.5	11.9	7.3	8.1	13.2	3.3	30.4	5.VII	-15.9	22.I	–	–	–	–	–	–	–	–	6.5	6.6	6.1	6.4

Stańcowa

$H_s = 850$ m $h_w = 25$ m **1957**

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	LICZBA DNI (n) Temperatura T Max>0	Max>25	Min<0	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15	≡	≤5	◔	●	▣
I	3	10	8	11	3	13	·	·	·	·	17	19	38	17	24	19	·	17	85.1	24.8	6	30	11	6	·	15	11	3	·	·	·	·	4	17	31
II	·	·	2	2.0	1	1.0	·	·	4	1.5	25	16	50	18	·	·	1	1.7	55.5	9.0	25	21	4	1	·	17	14	·	·	·	·	·	2	16	28
III	5	1.2	14	1.5	1	1.0	·	·	·	·	28	1.3	29	17	8	11	·	1.5	82.1	13.8	18	20	5	6	·	13	11	4	·	·	·	1	8	11	16
IV	2	1.0	29	1.3	10	11	3	3.0	5	2.0	24	15	9	12	6	18	2	1.4	72.7	16.6	11	1.3	·	·	·	19	16	3	·	·	·	2	4	12	8
V	6	17	34	20	5	14	·	·	·	·	30	12	13	15	5	24	·	1.6	72.9	27.0	24	6	·	·	·	13	11	2	·	·	·	3	5	14	·
VI	4	1.0	8	1.4	·	·	·	·	·	·	19	16	20	16	9	12	·	1.5	44.2	9.5	9	·	·	·	4	7	7	·	·	·	·	5	5	4	·
VII	3	3.3	·	·	·	·	·	·	4	1.0	12	13	31	11	11	5.5	2	1.7	258.7	37.9	15	·	·	·	·	20	19	10	3	1	·	6	2	13	·
VIII	·	·	3	1.0	·	·	3	1.0	·	·	3.9	16	11	15	4	1.0	3	1.4	90.0	29.0	29	·	·	·	2	13	10	3	·	·	·	2	3	3	·
IX	·	·	6	1.5	·	·	·	·	·	·	33	15	12	14	7	31	2	1.6	105.9	13.0	3	·	·	·	·	14	13	4	·	·	·	1	4	17	·
X	·	·	·	·	·	·	·	·	·	·	20	18	60	10	13	12	·	1.2	34.2	12.8	23	5	·	·	·	5	4	2	·	·	·	·	4	8	·
XI	1	7.0	2	5.0	26	15	·	·	·	·	10	25	32	16	19	25	·	2.0	76.4	26.3	28	17	8	1	·	19	8	2	1	·	·	·	6	15	2
XII	1	1.0	20	14	·	·	·	·	·	·	15	22	37	24	17	19	3	2.3	49.8	19.0	6	26	16	6	·	14	11	1	3	·	·	·	4	19	31
Rok	25	1.4	126	1.5	1.6	0.3	6	0.3	1.3	0.4	355	1.5	1.12	1.5	121	2.1	1.3	1.6	1035.6	37.9	15.08	144	1.2	20	6	1.60	1.33	34	7	1	·	22	1.3	151	116

Rożawka na Obidowej

$H_s = 800$ m $h_w = 17$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Max>0	Max>25	Min<0	≥0.1	≥1.0	≥10.0	≥10	≥15	≡	≤5	◔	●	▣
I	7	26	3	3.7	·	·	3	2.5	30.5	3.5	24.5	5.6	8	7.3	3	3.0	14	3.7	32.4	6.4	6	3.4	1.2	3	·	15	9	·	4	2	5	·	·	15	3.4
II	5.5	2.5	·	·	·	·	4	2.8	3.0	5.3	2.5	5.4	2	4.0	5.5	2.6	1.2	4.1	43.8	13.8	25	2.3	7	1	·	12	10	1	4	1	5	·	1	17	12
III	9	2.4	·	·	3	2.7	6	2.9	19.5	3.3	14.5	4.5	7	4.8	6	2.8	2.8	2.5	48.6	16.2	16	1.9	4	1	·	11	10	1	1	·	2	·	6	10	1.5
IV	2.5	2.5	6.5	2.8	0.5	3.0	1.2	2.5	8.5	3.2	7	3.7	2	3.5	2.5	2.4	2.5	2.0	63.5	19.4	27	4.1	·	·	·	17	14	2	·	·	1.1	1	3	17	6
V	3.0.5	2.8	10.5	2.8	2.5	2.5	7	2.5	3.5	2.5	4	3.0	4	3.0	1.1	2.3	2.1	2.1	112.4	37.5	14	3.1	1	·	·	16	12	4	·	·	7	2	·	21	4
VI	9	2.9	2.5	3.2	2	2.0	1.0	2.8	17.5	3.3	9.5	6.0	5	3.2	7.5	2.3	2.7	2.4	41.9	8.8	7	·	·	·	1.4	10	9	·	·	·	2	1.4	3	9	·
VII	1.0	2.2	1	2.5	1	2.0	1.1	2.4	10.5	2.8	1.6	3.4	5.5	3.6	6	3.2	3.2	1.9	205.5	34.9	15	·	·	·	1.8	21	16	6	·	·	3	1.4	·	20	·
VIII	9	2.1	2	2.0	1	2.0	1.3	2.0	13.5	3.4	1.4.5	4.2	6.5	2.2	10.5	3.7	2.3	2.3	111.8	26.5	29	·	·	·	2	1.3	9	4	2	1	2	2	1	7	·
IX	4	2.8	3	2.7	·	·	4	2.4	1.2	3.7	3.1	4.9	11.5	3.7	4.5	2.8	2.0	3.1	74.2	14.4	4	2	·	·	·	16	12	2	2	·	4	·	3	16	·
X	5	2.2	1	2.0	·	·	1.0	2.5	33.5	3.1	16.5	4.2	2	3.0	2	3.0	2.3	2.4	42.6	14.5	22	6	·	·	·	5	5	1	1	·	4	·	4	7	·
XI	6	5.5	2	3.5	4	3.0	14.5	3.3	2.2	2.9	7	5.6	7.5	4.2	4	9.0	2.6	2.0	30.0	7.9	29	4.0	7	1	·	9	7	·	2	·	3	·	4	15	2
XII	6.5	3.5	1	3.0	·	·	·	·	1.1	3.6	2.1	6.7	2	3.5	3.5	2.7	1.8	3.5	25.2	5.3	10	2.9	2.4	7	·	12	6	·	1	·	5	·	1	15	13
Rok	1.27.5	2.8	3.2.5	2.6	1.4	1.1	9.1.0	2.4	2.1.7	3.1	1.67.5	4.8	1.0	3.8	6.6	3.3	2.6.9	2.7	1.3.1.0	3.7.3	1.1.7	1.4.6	1.3.2	1.8	1.4.4	1.57	1.1.9	2.3	1.0	1.4	5.3	1.5	2.9	1.6.9	8.3

Turbacz

$H_s = 1308$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Max>0	Max>25	Min<0	≥0.1	≥1.0	≥10.0	≥10	≥15	≡	≤5	◔	●	▣
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	78.5	19.5	6	23	16	6	·	14	13	3	-	-	-	·	5	11	31
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	72.6	15.3	25	-	8	-	·	12	9	3	-	-	-	·	3	13	28
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	80.9	24.0	15	-	-	-	·	11	11	4	-	-	-	1	7	10	31
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	85.1	22.1	11	16	5	-	·	19	16	3	-	-	-	3	3	13	13
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	47.0.4	40.4	20	-	3	-	·	12	16	4	-	-	-	2	1	18	8
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	55.6	12.7	4	·	·	·	3	14	12	2	-	-	-	7	3	3	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	282.4	50.1	16	-	·	·	3	20	20	5	-	-	-	8	4	14	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	135.8	41.6	30	-	·	·	·	20	15	3	-	-	-	1	·	8	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	122.1	17.3	24	6	·	·	·	19	17	3	-	-	-	1	3	15	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58.8	15.6	22	·	·	-	·	8	7	2	-	-	-	·	5	C	·
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	58.3	20.1	29	19	-	8	·	6	6	2	-	-	-	·	6	18	9
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	61.0	16.4	6	28	-	6	·	12	10	2	-	-	-	·	3	17	21
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.25.1.6	50.1	1.6.1.0	·	·	·	6	1.75	1.5.4	4.0	·	·	·	25	1.46	1.10	1.1.0

Łącko

$H_s = 360$ m $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Max>0	Max>25	Min<0	≥0.1	≥1.0	≥10.0	≥10	≥15	≡	≤5	◔	●	▣
I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.9	5.3	5	17	9	5	·	10	4	·	-	-	-	-	2	15	24
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.8	6.4	25	20	1	·	·	9	2	·	-	-	-	-	4	12	4
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	25.4	7.4	24	15	3	1	·	8	4	·	-	-	-	-	6	8	4
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52.1	12.1	7	7	·	·	·	16	8	2	-	-	-	-	5	14	·
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	83.6	26.4	20	·	·	·	·	14	12	3	-	-	-	·	·	17	·
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	38.7	22.5	22	·	·	·	1.1	10	7	1	-	-	-	7	3	·	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1.60.5	44.0	15	·	·	·	1.1	15	13	5	-	-	-	-	3	12	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.1	33.3	28	·	·	·	7	13	13	2	-	-	-	-	1	7	·
IX	4.5	2.1	5	1.8	5	1.8	0.5	1.0	3	2.0	8.5	3.2	3.7.6	3.2	9	5.0	4.6	2.5	47.4	14.9	4	9	·	·	8	12	10	1	-	-	-	-	3	12	·
X	5	1.2	2	1.5	3	1.5	2	1.8	5	2.0	1.3.5	2.1	2.7.5	1.8	3.5	1.7	3.2	1.8	3.0.4	1.6.0	12	3	·	·	·	4	4	1	-	-	-	-	7	6	·
XI	6	1.8	9	2.0	1	1.0	2.5	1.8	1.1.5	2.7	9	3.0	2.3.5	2.1	4.5	2.9	2.0	2.1	3.1.8	1.3.5	12	1.1	5	6	·	6	5	1	-	-	-	-	4	1.5	1
XII	5	1.5	6	1.7	6	1.5	1	1.0	6.5	2.2	1.2.5	1.0	2.5	2.5	1.0	1.0	2.0	1.0	1.1.3	1.8	9	2.6	6	2	·	5	5	·	-	-	-	-	2	1.7	6
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3.6.3.9	1.4.4	1.5.1.1	1.1.0	2.1	9	3.4	1.2.2	8.7	1.6	-	-	-	-	4.4	1.3.6	3.6

Stary Sącz

$\varphi = 49°33'$ $\lambda = 20°39'$ **1957**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T								ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI f_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.8	-0.1	-1.9	-1.7	1.0	-4.4	6.4	26	-15.7	17,18	–	–	–	–	–	–	–	–	8.3	7.8	7.7	7.9
II	–	–	–	–	1.1	5.0	2.5	2.8	6.9	-0.2	12.7	16	-6.2	23	–	–	–	–	–	–	–	–	7.2	6.7	6.6	6.8
III	–	–	–	–	0.4	7.0	3.1	3.4	8.9	-1.4	20.0	14	-14.5	4	–	–	–	–	–	–	–	–	6.5	5.3	4.4	5.4
IV	–	–	–	–	5.0	11.8	7.1	7.8	15.0	2.6	23.8	30	-2.7	5	–	–	–	–	–	–	–	–	5.9	6.5	6.7	6.4
V	–	–	–	–	7.9	12.6	8.6	9.5	14.1	4.5	24.9	13,16	-0.5	30	–	–	–	–	–	–	–	–	7.2	7.8	7.9	7.6
VI	–	–	–	–	14.3	22.5	17.1	17.8	24.0	10.8	30.6	30	3.6	27	–	–	–	–	–	–	–	–	4.5	5.6	4.8	5.0
VII	–	–	–	–	16.4	22.5	17.2	18.3	24.5	13.4	35.8	5	7.7	4	–	–	–	–	–	–	–	–	5.9	7.3	6.5	6.6
VIII	–	–	–	–	14.0	21.0	15.1	16.3	22.1	10.8	29.7	14	5.0	31	–	–	–	–	–	–	–	–	4.1	5.8	6.0	5.3
IX	–	–	–	–	10.2	16.5	11.7	12.5	17.1	7.8	27.1	9	-0.5	26	–	–	–	–	–	–	–	–	5.6	6.6	7.4	6.5
X	–	–	–	–	6.2	11.3	7.9	9.1	15.4	3.7	20.4	19	-2.1	3	–	–	–	–	–	–	–	–	5.5	4.5	3.5	4.5
XI	–	–	–	–	4.0	7.3	4.8	5.2	8.4	2.6	17.8	4	-10.3	30	–	–	–	–	–	–	–	–	6.8	6.4	7.0	6.7
XII	–	–	–	–	-1.0	0.9	-0.6	-0.4	2.2	-3.4	13.8	13	-10.0	11	–	–	–	–	–	–	–	–	8.0	6.7	6.6	7.1
Rok	–	–	–	–	5.3	11.8	7.7	8.4	13.1	3.9	35.8	5 VII	-15.7	17,18 I	–	–	–	–	–	–	–	–	6.3	6.4	6.3	6.3

Rymanów – Zdrój

$\varphi = 49°33'$ $\lambda = 21°51'$

I	–	–	–	–	-2.8	-1.3	-2.6	-2.3	-0.3	-4.6	4.9	3	-12.4	17	–	–	–	–	–	–	–	–	9.0	7.0	7.5	7.8
II	–	–	–	–	1.2	2.7	1.6	1.8	4.3	-0.5	12.2	19	-6.9	28	–	–	–	–	–	–	–	–	7.5	7.3	6.9	7.3
III	–	–	–	–	-0.8	4.7	0.6	1.3	6.4	-4.1	16.7	30	-19.9	4	–	–	–	–	–	–	–	–	5.1	4.7	4.1	4.6
IV	–	–	–	–	5.8	11.6	6.1	7.4	13.3	1.9	24.5	30	-3.0	16	–	–	–	–	–	–	–	–	5.3	6.0	4.8	5.4
V	–	–	–	–	8.6	14.7	7.8	9.0	13.6	4.3	21.4	17	-0.8	30	–	–	–	–	–	–	–	–	7.0	7.6	6.6	7.1
VI	–	–	–	–	16.0	21.4	14.8	16.8	23.7	9.8	32.4	12	5.0	2	–	–	–	–	–	–	–	–	4.4	3.2	3.3	3.6
VII	–	–	–	–	16.2	21.6	15.9	17.4	23.0	12.4	31.4	8	7.2	4	–	–	–	–	–	–	–	–	5.9	5.5	5.2	5.5
VIII	–	–	–	–	14.5	19.7	13.8	15.4	20.9	9.8	28.5	14	4.7	31	–	–	–	–	–	–	–	–	4.5	4.8	5.2	4.8
IX	–	–	–	–	10.3	15.1	11.0	12.0	16.5	7.3	25.1	9	-2.8	27	–	–	–	–	–	–	–	–	6.4	6.5	6.0	6.3
X	–	–	–	–	6.7	13.0	7.0	8.4	14.2	3.4	25.7	20	-4.4	3	–	–	–	–	–	–	–	–	4.3	4.5	4.1	4.5
XI	–	–	–	–	3.4	5.8	3.3	4.0	7.3	1.1	16.8	8,9	-10.9	30	–	–	–	–	–	–	–	–	6.6	5.9	6.7	6.4
XII	–	–	–	–	-2.4	-0.3	-1.7	-1.6	0.6	-4.3	13.8	14	-12.7	11	–	–	–	–	–	–	–	–	6.9	7.8	6.7	7.1
Rok	–	–	–	–	6.4	10.4	6.5	7.4	12.0	3.0	32.4	12 VI	-19.9	4 II	–	–	–	–	–	–	–	–	6.1	5.9	5.6	5.9

Pilsko

$\varphi = 49°32'$ $\lambda = 19°19'$

I	–	–	–	–	-4.0	-2.6	-3.6	-3.4	-0.6	-5.0	5.4	9,10	-13.8	16	–	–	–	–	–	–	–	–	7.1	6.7	7.0	6.9
II	–	–	–	–	-2.9	-1.3	-2.4	-2.2	0.5	-4.6	8.5	5	-12.7	28	–	–	–	–	–	–	–	–	8.3	7.8	8.5	8.2
III	–	–	–	–	-4.5	0.9	-0.6	-0.4	2.7	-4.2	9.5	13	-13.5	1	–	–	–	–	–	–	–	–	4.7	5.1	5.7	5.2
IV	–	–	–	–	1.6	3.5	1.9	2.2	5.8	-0.8	16.5	30	-9.2	14	–	–	–	–	–	–	–	–	6.6	7.4	7.3	7.1
V	–	–	–	–	2.8	4.7	3.2	3.5	6.3	–	15.6	19	–	–	–	–	–	–	–	–	–	–	6.9	8.7	7.6	7.7
VI	–	–	–	–	11.3	13.9	11.6	12.1	15.9	7.8	23.3	11	2.9	28,29	–	–	–	–	–	–	–	–	5.7	6.5	6.4	6.2
VII	–	–	–	–	12.1	14.0	12.2	12.6	16.0	9.5	26.6	8	5.3	28	–	–	–	–	–	–	–	–	7.7	7.4	7.5	7.5
VIII	–	–	–	–	9.1	11.0	9.3	9.7	–	6.2	–	–	1.0	12	–	–	–	–	–	–	–	–	6.2	7.4	7.1	6.9
IX	–	–	–	–	5.0	7.8	6.3	6.4	9.5	2.9	19.6	9	-3.6	25,26,27	–	–	–	–	–	–	–	–	7.7	8.1	7.4	7.7
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sieniawa

$\varphi = 49°32'$ $\lambda = 19°55'$

I	–	–	–	–	-3.7	0.0	-3.4	-2.5	1.0	-6.4	6.6	10	-22.1	17	–	–	–	–	–	–	–	–	8.2	6.9	5.5	6.9
II	–	–	–	–	-0.4	3.6	0.8	1.4	5.4	-2.6	10.9	19	-14.6	23	–	–	–	–	–	–	–	–	8.0	7.6	6.6	7.4
III	–	–	–	–	-2.0	6.4	0.5	1.4	8.2	-4.1	14.9	27	-18.4	4	–	–	–	–	–	–	–	–	6.8	5.6	4.8	5.7
IV	–	–	–	–	3.5	9.7	4.3	5.1	11.3	0.9	23.6	30	-7.1	14	–	–	–	–	–	–	–	–	6.6	7.0	6.5	6.7
V	–	–	–	–	6.3	10.4	6.6	7.5	12.3	3.2	21.3	19	-4.5	30	–	–	–	–	–	–	–	–	7.5	8.2	7.3	7.7
VI	–	–	–	–	10.4	20.6	13.5	13.5	22.5	8.5	23.4	11	4.7	27	–	–	–	–	–	–	–	–	4.0	5.7	6.3	5.0
VII	–	–	–	–	13.4	20.0	14.3	16.3	21.8	11.6	32.7	8	6.8	30	–	–	–	–	–	–	–	–	6.9	7.3	7.2	7.1
VIII	–	–	–	–	10.2	16.4	12.3	14.0	20.0	8.5	28.8	12	2.8	31	–	–	–	–	–	–	–	–	5.4	5.8	4.8	5.3
IX	–	–	–	–	7.2	13.7	9.1	10.0	15.4	6.0	23.0	9	-1.9	26	–	–	–	–	–	–	–	–	6.6	6.7	6.6	6.5
X	–	–	–	–	4.2	10.4	6.5	6.9	13.1	1.8	21.9	19	-3.0	3	–	–	–	–	–	–	–	–	5.6	4.7	3.6	4.6
XI	–	–	–	–	0.8	5.5	1.6	2.5	7.2	-0.9	17.8	6	-13.6	30	–	–	–	–	–	–	–	–	7.9	5.9	6.8	6.9
XII	–	–	–	–	-3.7	-0.5	-2.8	-2.4	1.0	-5.4	11.2	13	-15.9	5,11	–	–	–	–	–	–	–	–	7.5	7.3	5.9	6.9
Rok	–	–	–	–	2.1	10.0	5.1	6.3	11.6	1.1	32.7	8 VII	-22.1	17 I	–	–	–	–	–	–	–	–	6.8	6.6	5.9	6.4

Stary Sącz

H_s = 320 m h_w = 18 m 1957

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max	Min	Min<-25	Opad R 0.1	1.0	10.0	Wiatr 10	15					
I	4	1.0	8	3.4	·	·	·	·	4.4	13.2	2	8.5	3	6.0	4	15.5	28	7.6	16.4	–	–	2.5	9	6	·	8	4	·	18	11	4	·	1	2.0	26
II	5	1.7	4	1.6	·	·	2	8.8	17.5	13.6	2	6.5	5.5	8.8	1	5.0	17	8.9	23.0	13.0	25	1.1	1	·	·	8	6	1	19	14	·	·	5	1.5	9
III	7.5	1.4	10.5	2.2	·	·	·	·	25.5	10.8	1.5	3.0	7	4.6	3	4.7	38	3.9	21.8	8.1	24	4.6	3	1	·	9	5	·	10	5	·	1	8	1.1	7
IV	6.5	3.1	5	3.5	1	3.0	1.5	3.0	10.5	6.1	·	·	1.5	2.7	3	2.8	64	1.4	67.6	16.4	11	1.6	·	·	·	16	1.5	2	2	·	3	2	5	1.5	1
V	9.5	2.2	9	1.9	·	·	·	·	9.5	5.1	2.5	3.4	1	2.0	2.5	2.2	59	1.1	96.6	17.4	10	1	·	·	·	12	1.6	5	1	·	3	2	2	1.7	·
VI	8.5	2.8	3	2.2	·	·	3	5.7	2.3	8.6	2.5	3.8	1.5	5.0	1.5	5.7	47	3.0	78.2	42.0	12	·	·	·	12	1.5	8	1	6	3	2	6	4	1	·
VII	2	2.2	1.5	2.3	·	·	1	10.0	8	3.9	1	3.0	1	8.0	0.5	2.0	78	0.6	128.1	31.9	16	·	·	·	13	1.8	1.3	5	1	·	·	8	1	1.3	·
VIII	6	1.4	2	2.2	1	2.5	0.5	10.0	8.5	10.0	2	8.0	0.5	5.0	3.5	6.3	69	1.6	72.4	22.4	28	·	·	·	8	1.5	1.0	2	4	2	3	3	1	7	·
IX	4	1.2	1	2.0	0.5	1.2.0	0.5	12.0	1.5	4.9	2	6.5	7	7.0	1	4.0	59	1.8	63.9	18.7	4	2	·	·	2	1.5	9	1	3	·	1	·	1	1.3	·
X	1	1.0	1	2.0	·	·	·	·	3.2	8.1	2.3	3.0	2.5	3.0	·	·	54	3.0	30.4	12.4	8.2	3	·	·	·	4	3	1	7	2	8	·	7	5	·
XI	5.5	1.3.0	1.0	2.8	1	1.0	0.5	1.0	3.1.5	1.1.3	·	·	8	3.2	1.5	3.0	3.2	5.5	38.6	9.0	1.4	0.0	0	·	·	8	5	·	2.1	4	7	·	7	1.7	1
XII	6.5	2.2	7	3.3	·	·	1.5	3.0	4.3.6	1.1.3	5	5.0	4	7.8	1.5	2.7	24	6.5	12.4	4.2	1.8	0.6	0.2	·	·	6	4	·	1.4	1.0	3	·	4	1.6	6
Rok	6.5	2.8	6.2	2.4	3.5	1.5	1.0.5	5.2	2.8.5	8.9	2.3	4.2	4.2.5	6.5	2.3	4.5	5.6.6	3.7	6.4.1.4	4.2.3	3.0	1.0.0	2.6	7	3.5	1.4.1	2.3	1.8	9.6	5.4	8.7	2.4	5.5	1.5.3	5.0

Rymanów – Zdrój

H_s = 360 m h_w = 17 m

I	7.5	1.9	1	1.0	·	·	·	·	5.1	6.5	9	2.1	1	1.0	7.5	2.0	1.6	4.1	1.4.4	4.3	6	2.8	1.6	3	·	1.1	5	·	7	5	·	·	·	1.8	–
II	6.5	1.7	·	·	·	·	·	·	5.1	6.3	5	5.6	2	1.0	4.5	1.6	1.5	4.4	4.4.4	2.0.9	2.5	1.5	4	·	·	1.5	9	1	8	4	·	·	1	1.5	–
III	1.1	1.5	·	·	·	·	·	·	2.9.5	4.0	6.5	2.1	6	1.2	1.2	1.6	2.8	1.9	1.0.5	8.8	1.5	2.1	6	7	·	1.0	8	·	2	2	2	1	1.1	9	–
IV	6.5	1.5	·	·	·	·	·	·	1.7.5	1.4	1.5.5	2.3	2	1.0	2.0.5	1.5	2.8	1.2	1.6.0	1.5.9	1.1	1.0	·	·	·	1.5	1.0	1	·	·	3	2	8	9	–
V	1.2	2.6	1	3.0	·	·	·	·	5.5	3.4	1.1.5	1.3	·	·	3.8	1.7	2.5	1.5	1.0.5.8	2.4.6	9	1.6	·	·	·	1.2	1.5	3	·	·	1	3	4	1.6	–
VI	7	1.1	·	·	·	·	·	·	3.9	3.1	1.4	2.0	2.5	1.6	7.5	1.4	2.0	1.9	8.0.6	2.5.0	1.2	·	·	·	1.3	9	6	2	·	·	1	1.0	9	2	–
VII	3.5	1.4	1.5	1.3	·	·	0.5	1.0	1.1.5	2.7	8	2.4	3	1.5	1.0	1.2	2.5	1.7	1.3.5.9	1.6.1	3.1	·	·	·	9	1.9	1.6	6	·	·	2	1.1	6	9	–
VIII	7	1.9	·	·	1	1.0	1	1.0	3.0	1.5	6	1.3	3	1.0	1.2	1.5	3.3	1.9	1.0.1.9	2.7.2	2.9	·	·	·	5	1.7	1.0	3	5	2	1	5	4	3	–
IX	1.2	1.8	·	·	0.5	1.0	2.5	2.6	4.6	3.9	5	2.0	2	2.0	9	1.0	1.3	2.6	1.0.2.1	3.8.9	3	2	·	·	1	1.6	1.4	2	1	·	2	2	2	8	–
X	1.2	1.7	3	1.7	·	·	·	·	7	5.6	3.8	4.9	·	·	1	4.0	3.2	2.7	2.0.6	8.8	2.0	8	·	·	1	4	4	·	3	1	4	·	1.1	7	–
XI	1.6.5	4.7	7.5	3.3	·	·	·	·	4.5	4.1	3.3	4.0	1	2.0	·	·	1.8	3.2	3.5.3	1.2.7	2.8	1.2	3	1	·	9	6	2	4	1	2	·	5	1.5	–
XII	2.2	3.9	4.0	4.4	·	·	·	·	1.3.5	6.2	4.0.5	5.8	·	·	2	2.5	5	4.9	2.3.0	7.0	1.3	2.8	1.0	1	·	1.2	7	·	3	2	3	·	3	1.5	–
Rok	1.2.2.5	2.2	2.4	1.2	1.5	0.5	4	0.6	3.4.6.5	4.5	1.9.2	3.0	2.2.5	1.0	1.2.4	1.7	2.5.8	2.7	7.5.1.3	3.8.7	5.1.0	1.2.4	1.0.2	4.2	2.9	1.5.4	1.1.2	2.0	3.1	1.1	3.1	3.4	6.4	1.2.4	–

Pilsko

H_s = 1270 m h_w = 13 m

I	2	1.5	2	5.8	4.0	4.4	1.5	2.0	2.6.5	3.5	4.1	4.8	5.5	5.3	4.5	6.2	·	4.4	4.4.1	1.4.2	6	3.2	1.6	4	·	1.3	1.1	1	3	·	1.2	·	5	1.9	–
II	·	·	4	2.2	3	2.3	·	·	2.9	6.0	3.5.5	5.6	6.5	5.5	6	2.8	·	5.3	6.1.1	1.1.7	1.5	2.5	1.6	3	·	1.1	1.1	3	7	·	1.6	·	2	2.0	–
III	3	2.7	4.5	4.0	4.5	2.3	9.5	6.4	1.8	7.4	4.4.5	4.7	6.5	5.8	0.5	1.0.0	2	5.2	9.2.0	2.2.3	1.6	2.6	7	5	·	8	8	4	8	1	1.0	1	9	1.1	–
IV	2.5	1.6	1.4	2.4	1.7.5	2.2	6	2.9	2.3	3.2	1.3	2.3	2	1.2	6	1.9	6	2.3	8.2.5	1.4.8	7	0.5	0	·	·	1.5	1.4	2	·	·	1.3	2	4	1.8	–
V	1.0.5	5.9	2.6.5	4.5	7	3.5	4.5	3.4	1.4.5	2.2	1.8.5	2.8	6.5	1.6	4	1.9	1	3.5	6.9.6	1.5.1	1.3	1.5	5	·	·	1.3	1.1	2	1	·	1.6	2	·	1.7	–
VI	1.0.5	2.1	7	3.9	2	3.8	3.5	3.0	2.3.5	5.0	2.7	3.9	4.5	1.7	5	1.3	7	3.3	5.4.6	1.6.9	6	·	·	·	2	2.0	1.9	1.1	·	·	3	3	5	1.2	–
VII	4	1.7	7.5	1.8	0.5	4.0	4	2.4	2.1.5	3.5	3.7.5	3.0	1.1.5	2.5	1.5	1.6	5	2.7	3.6.5.0	8.6.6	1.6	·	·	·	·	2.0	1.9	1.1	·	·	1.3	3	2	1.6	–
VIII	7	1.8	5	1.6	3	1.3	1	3.0	2.5	3.0	2.4.5	3.1	1.3.5	2.5	9	2.4	5	2.5	1.0.0.6	3.6.0	2.8	·	·	·	·	1.1	1.1	3	·	·	1.2	·	1.4	·	–
IX	·	·	3.5	4.1	2.5	2.2	3.5	1.4	1.9.5	4.0	4.5.5	5.8	1.2.5	1.8	·	·	2	4.6	–	–	–	1.8	·	·	·	1.4	1.3	0	6	1	1.3	1	2	1.7	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sieniawa

H_s = 578 m h_w = 16 m

I	·	·	1.3	1.8	1.1	1.7	1.9.5	2.1	5	3.5	1.5.5	2.9	1.2	3.1	·	·	1.3	2.2	6.5.9	6.2	6	2.9	9	7	·	1.4	9	·	·	·	·	·	2	1.3	3.0
II	1	1.0	1	3.0	1.0.5	2.0	1.4.5	2.3	8.5	2.0	2.6	3.3	1.2	1.8	1.5	1.7	3	2.2	4.5.7	1.5.3	8.5	2.1	1	2	·	1.3	9	2	·	·	·	·	2	1.5	1.0
III	1	1.0	6	1.0	5	1.0	1.4	1.7	3.5	3.1	2.6	2.4	1.3.5	2.0	6	1.5	1.8	1.6	4.7.2	9.2	1.8	0.5	3	7	·	1.2	9	·	·	·	·	1	6	1.0	1.5
IV	3	1.2	1.3	1.6	8	1.5	8	1.7	1.5	1.3	7.5	2.3	7	2.4	2.4	1.7	1.8	1.4	5.6.9	1.7.7	1.1	1.4	·	·	·	1.7	1.2	2	·	·	·	·	3	1.5	3
V	2.5	1.4	2.1.5	1.6	1.4	1.3	4	1.5	0.5	1.0	2.5	1.4	1.1.5	2.0	1.8.5	1.5	1.8	1.3	8.6.7	2.2.5	2.0	5	·	·	·	1.5	1.0	3	·	·	·	2	·	1.7	2
VI	7.5	2.1	5.5	1.7	3.5	1.3	1.2	2.1	4.5	3.3	2.0.5	2.2	6	2.8	2.0.5	1.5	1.0	1.8	4.6.0	9.2	8	·	·	·	7	9	9	·	·	·	·	3	8	7	·
VII	3	1.7	4.5	1.7	2	2.0	1.0	1.9	2	3.0	2.2	2.5	8.5	1.8	2.1	2.0	2.0	1.6	1.9.4.3	3.4.7	1.5	·	·	·	9	2.0	1.9	8	·	·	·	4	3	1.8	·
VIII	1.5	2.3	5	1.2	2	1.0	4	1.8	4	2.5	1.7.5	2.8	4.9	2.2	2.4	1.9	4.6	1.8	9.5.4	2.3.5	2.9	·	·	·	5	1.4	1.0	4	·	·	·	1	3	2.0	·
IX	2	1.0	3.5	1.0	4.5	1.0	4	3.0	3.5	2.7	2.9.5	2.9	1.2.5	3.4	9.5	4.5	2.1	1.9	6.2.2	1.5.7	4	2	·	·	·	1.2	1.3	2	·	·	·	3	·	3	1.1	·
X	1	2.0	·	·	1.3.5	1.5	8.5	1.3	8	1.6	2.8	2.0	2	1.5	1.2	1.2	2.0	1.3	3.6.4	1.2.4	2.2	6	·	·	·	6	5	2	·	·	·	·	7	6	·
XI	4	1.5	7.5	1.7	8	1.3	2.9	1.3	2.5	2.2	1.3.5	1.7	7	2.1	3.5	1.9	1.5	1.3	2.2.5	7.1	2.3	0.4	1	1	·	1.0	6	·	·	·	·	1	4.3	1
XII	·	·	1	1.5	6	1.2	1.6.5	1.5	1.0	2.1	2.8.5	2.9	9	1.3	7	1.6	1.3	1.3	3.9.5	1.0.7	8	0.3	0.2	5	·	1.5	8	1	1	·	1	·	3	1.1	1.1
Rok	2.6.5	1.3	8.4.5	1.5	8.8	1.4	1.4.3	1.8	5.5.5	2.4	2.4.1	2.5	1.2.0	2.2	1.4.7.5	1.5	1.9.1	1.7	7.6.3.5	3.4.7	4.5.8	4.0.1	2.6	2.3	2.1	1.4.6.2	1.1.9	3.1	4	·	1	·	1.3	4.3	4.4.4	1.5

Zwardoń

$\varphi = 49°30'$ $\lambda = 18°59'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-4.4	-4.8	-3.6	-3.4	-0.2	-6.8	7.1	2,3	-18.8	17	–	–	–	–	–	–	–	–	8.5	6.8	7.1	7.5
II	–	–	–	–	-0.8	1.6	0.4	0.3	3.5	-3.4	8.9	7	-13.5	23	–	–	–	–	–	–	–	–	7.9	7.5	8.0	7.8
III	–	–	–	–	-1.3	5.7	1.5	1.8	7.2	-3.5	13.6	21	-13.0	6	–	–	–	–	–	–	–	–	5.0	5.0	4.7	4.9
IV	–	–	–	–	2.8	8.9	4.6	5.2	10.4	0.0	22.1	30	-7.7	9,14	–	–	–	–	–	–	–	–	5.6	6.3	6.7	6.2
V	–	–	–	–	6.2	9.7	6.7	7.5	11.8	2.3	21.6	19	-2.4	26	–	–	–	–	–	–	–	–	6.9	7.5	7.4	7.2
VI	–	–	–	–	12.6	14.9	15.4	14.1	21.6	7.8	27.6	14,30	4.5	27	–	–	–	–	–	–	–	–	2.9	4.9	3.8	3.9
VII	–	–	–	–	14.8	19.0	16.0	16.4	24.5	10.3	32.1	8	7.0	19	–	–	–	–	–	–	–	–	6.9	6.7	6.2	6.6
VIII	–	–	–	–	14.1	17.1	13.3	13.7	19.0	7.8	25.6	11,13	4.9	31	–	–	–	–	–	–	–	–	5.8	5.4	4.0	5.0
IX	–	–	–	–	7.6	12.6	9.3	9.7	14.0	5.1	23.6	9	-2.6	26,27	–	–	–	–	–	–	–	–	7.0	6.8	6.5	6.7
X	–	–	–	–	4.9	11.0	6.1	7.0	12.1	2.1	18.6	19	-4.3	3	–	–	–	–	–	–	–	–	5.0	3.3	3.5	3.9
XI	–	–	–	–	1.7	4.8	2.1	2.7	6.1	-0.6	14.6	4,5,8,10	-12.5	30	–	–	–	–	–	–	–	–	6.9	6.3	6.3	6.5
XII	–	–	–	–	-3.4	-4.3	-2.3	-2.3	0.4	-6.2	11.9	13	-16.3	11	–	–	–	–	–	–	–	–	8.1	7.7	7.4	7.7
Rok	–	–	–	–	4.3	2.9	5.8	6.2	10.6	1.3	32.1	8.VII	-18.8	17.I	–	–	–	–	–	–	–	–	6.4	6.2	5.9	6.2

Nowy Targ

$\varphi = 49°29'$ $\lambda = 20°02'$

I	–	–	–	–	-6.2	-2.1	-5.6	-4.9	-0.7	-9.2	4.2	6	-21.0	17	–	–	–	–	–	–	–	–	8.3	6.8	5.9	7.0
II	–	–	–	–	-2.2	2.5	-0.6	-0.2	4.2	-4.3	9.6	21	-17.0	23	–	–	–	–	–	–	–	–	8.5	7.1	6.5	7.4
III	–	–	–	–	-3.5	5.7	0.7	0.9	7.6	-5.4	15.3	21	-20.4	4	–	–	–	–	–	–	–	–	5.7	4.7	4.7	5.0
IV	–	–	–	–	2.5	10.4	5.1	5.8	12.1	0.3	23.4	30	-4.9	9,14	–	–	–	–	–	–	–	–	5.9	6.4	6.5	6.3
V	–	–	–	–	5.8	11.2	7.2	7.8	12.9	2.7	22.7	19	-2.8	30	–	–	–	–	–	–	–	–	7.2	8.1	6.8	7.4
VI	–	–	–	–	13.7	21.4	14.4	16.0	23.1	7.6	30.0	30	0.7	7,27	–	–	–	–	–	–	–	–	2.8	4.5	4.0	3.8
VII	–	–	–	–	14.5	21.0	15.6	16.8	22.8	10.8	33.6	8	4.4	30	–	–	–	–	–	–	–	–	6.1	6.6	6.3	6.3
VIII	–	–	–	–	10.9	19.6	13.1	14.2	20.9	7.9	29.0	14	0.9	24	–	–	–	–	–	–	–	–	4.8	5.6	4.5	5.0
IX	–	–	–	–	7.1	14.4	9.3	10.0	16.0	5.2	25.7	9	-1.9	26	–	–	–	–	–	–	–	–	6.4	5.8	6.7	6.3
X	–	–	–	–	2.2	12.8	5.2	6.4	13.9	0.2	23.8	19	-5.1	3	–	–	–	–	–	–	–	–	6.0	3.5	3.5	4.3
XI	–	–	–	–	0.1	5.7	1.8	2.4	7.3	-1.8	18.5	5	-13.0	30	–	–	–	–	–	–	–	–	8.0	5.8	7.0	6.9
XII	–	–	–	–	-5.4	-4.1	-3.4	-3.3	0.4	-8.0	11.3	13	-18.5	4	–	–	–	–	–	–	–	–	7.4	7.2	7.5	7.4
Rok	–	–	–	–	3.3	10.1	5.2	6.0	11.7	0.5	33.5	8.VII	-21.0	17.I	–	–	–	–	–	–	–	–	6.4	6.0	5.8	6.1

Jabłonka

$\varphi = 49°28'$ $\lambda = 19°42'$

I	–	–	–	–	-5.0	-1.8	-5.2	-4.3	-0.3	-8.3	5.9	2	-18.9	17	–	–	–	–	–	–	–	–	8.5	7.4	6.3	7.4
II	–	–	–	–	-1.1	2.2	-0.3	0.1	3.8	-3.4	8.1	19	-14.5	23	–	–	–	–	–	–	–	–	8.1	7.6	6.9	7.5
III	–	–	–	–	-3.3	4.7	0.3	0.5	6.8	-5.4	14.9	21	-19.0	4	–	–	–	–	–	–	–	–	7.8	5.3	4.2	5.8
IV	–	–	–	–	2.0	9.9	4.7	5.4	11.0	0.2	23.1	30	-6.5	16	–	–	–	–	–	–	–	–	6.3	6.5	6.2	6.3
V	–	–	–	–	5.7	10.8	7.1	7.7	12.3	2.6	24.6	16	-2.6	30	–	–	–	–	–	–	–	–	6.9	7.8	7.3	7.3
VI	–	–	–	–	13.0	20.9	14.6	15.9	22.2	7.5	28.3	14,30	0.0	27	–	–	–	–	–	–	–	–	5.3	5.1	4.1	4.8
VII	–	–	–	–	15.1	20.4	15.7	16.7	21.9	10.8	32.5	5	4.1	30	–	–	–	–	–	–	–	–	6.8	7.2	6.5	6.8
VIII	–	–	–	–	14.3	18.8	13.1	14.1	20.0	7.6	28.1	14	0.4	24	–	–	–	–	–	–	–	–	6.6	5.9	4.6	5.8
IX	–	–	–	–	7.8	13.8	9.0	9.9	14.9	5.1	24.3	9	-2.5	26	–	–	–	–	–	–	–	–	8.0	6.8	6.3	7.0
X	–	–	–	–	3.2	11.5	5.4	6.4	12.9	0.6	20.0	19	-4.1	3	–	–	–	–	–	–	–	–	7.6	4.4	2.9	5.0
XI	–	–	–	–	0.6	5.0	1.6	2.2	6.1	-1.5	15.5	5	-13.5	30	–	–	–	–	–	–	–	–	8.3	6.2	7.2	7.2
XII	–	–	–	–	-4.4	-0.9	-2.4	-2.5	0.9	-6.7	10.9	13	-17.3	7	–	–	–	–	–	–	–	–	7.5	7.3	5.9	6.9
Rok	–	–	–	–	3.8	9.5	5.3	6.0	11.0	0.8	32.5	5.VII	-19.0	4.III	–	–	–	–	–	–	–	–	7.3	6.5	5.7	6.5

Maniowy

$\varphi = 49°28'$ $\lambda = 20°15'$

I	–	–	–	–	-5.8	-2.0	-5.4	-4.6	-0.3	-9.6	5.4	6	-24.5	17	–	–	–	–	–	–	–	–	8.7	7.5	6.9	7.7
II	–	–	–	–	-1.8	2.9	0.1	0.3	4.5	-4.5	9.6	18,19	-14.3	27	–	–	–	–	–	–	–	–	7.9	7.7	7.6	7.7
III	–	–	–	–	-2.3	6.4	1.2	1.8	8.5	-4.6	16.7	21	-19.5	4	–	–	–	–	–	–	–	–	7.2	5.7	5.3	6.1
IV	–	–	–	–	3.0	11.5	5.7	6.4	12.7	0.2	22.7	28	-4.2	6,14	–	–	–	–	–	–	–	–	7.0	7.1	6.3	6.8
V	–	–	–	–	5.9	11.4	7.5	8.1	13.2	2.8	21.8	19	-3.0	30	–	–	–	–	–	–	–	–	8.5	8.3	7.4	8.1
VI	–	–	–	–	12.8	19.5	15.1	16.1	23.6	7.0	34.1	12	-0.1	7	–	–	–	–	–	–	–	–	5.4	6.0	5.5	5.8
VII	–	–	–	–	14.7	20.9	15.8	16.8	23.2	10.6	33.6	5	4.7	30	–	–	–	–	–	–	–	–	8.1	7.7	7.1	7.6
VIII	–	–	–	–	11.8	18.0	13.4	14.6	21.6	8.1	30.0	14	1.0	24	–	–	–	–	–	–	–	–	7.4	6.6	5.8	6.6
IX	–	–	–	–	7.8	13.4	10.0	10.7	16.5	5.4	26.9	9	-3.0	26	–	–	–	–	–	–	–	–	8.1	6.9	6.6	7.2
X	–	–	–	–	3.0	12.8	5.5	6.7	14.3	0.9	24.7	19	-4.2	3	–	–	–	–	–	–	–	–	9.1	4.4	3.9	6.0
XI	–	–	–	–	1.1	5.7	2.5	3.0	7.5	-0.8	16.7	4	-12.5	30	–	–	–	–	–	–	–	–	8.7	6.5	7.6	7.6
XII	–	–	–	–	-4.7	-0.6	-2.7	-2.7	1.2	-7.4	11.2	13	-16.0	8	–	–	–	–	–	–	–	–	7.5	7.3	7.2	7.3
Rok	–	–	–	–	3.1	10.4	5.7	6.4	12.2	0.7	33.6	6.VIII	-24.5	17.I	–	–	–	–	–	–	–	–	7.8	6.8	6.4	7.0

Zwardoń

$H_s = 690\ m$ $h_w = 16\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (0/00) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Dat.	LICZBA DNI (o) Temperatura T ≥ 10°	≥ 0°	≤ 0°	≤ -10°	Opad R ≥ 0.1 mm	≥ 1.0 mm	≥ 10.0 mm	Wiatr v ≥ 10 m/s	≥ 15 m/s	≥ 20 m/s	≡	!	•	◆	○
I	4.5	3.1	9	2.4	1	2.0	0.5	1.0	22.5	2.1	32.5	2.1	7.5	2.4	5.5	2.4	1.0	2.0	60.4	22.4	5	30	14	8	·	15	12	1	·	·	·	–	·	4	21	31
II	4.5	3.1	3.5	2.6	·	·	0.5	5.0	2.7	3.4	27.5	3.0	7	2.1	2	2.0	1.3	2.6	74.4	12.4	25	28	2	3	·	15	12	3	1	·	·	–	·	2	18	27
III	11.5	2.4	4.0	2.3	1.5	1.7	0.5	1.0	14.5	3.1	21.5	2.3	3	1.8	8.5	2.6	2.2	1.9	67.1	11.6	17	20	3	5	·	13	11	3	·	·	·	–	1	12	11	15
IV	12.5	2.8	2.1	2.5	3	2.7	·	·	5.5	2.0	9.5	2.6	1.5	2.7	1.0	2.8	2.7	1.8	80.3	16.0	7	13	·	·	·	17	15	3	·	·	·	–	2	6	13	3
V	1.6	2.7	3.5.5	3.2	3	4.3	2	1.5	2.5	2.5	5.5	2.6	5	2.2	7.5	1.9	1.6	2.4	68.8	22.7	2.0	9	·	·	·	17	10	2	·	·	·	–	3	4	17	1
VI	8	3.2	1.2	2.9	7	1.6	1	1.0	18.5	2.6	1.6	2.3	7	2.1	5.5	2.5	1.3	2.2	64.4	15.7	2.2	·	·	·	6	10	8	4	·	·	·	–	6	9	3	·
VII	5	2.5	5.5	2.0	4	1.5	1.5	2.0	1.7	2.6	1.6.5	2.5	8	1.5	1.3.5	1.7	2.2	1.7	234.9	70.0	1.6	·	·	·	9	1.9	1.9	5	·	·	·	–	5	6	1.6	·
VIII	9	1.3	2	4.0	·	·	1	2.0	1.5.5	3.4	1.2	3.1	4	2.1	1.4.6	2.5	3.5	1.7	103.9	37.0	2.8	·	·	·	4	1.4	1.2	3	·	·	·	–	4	5	5	·
IX	4.5	2.2	9	1.8	1.5	2.2	0.5	1.0	2.4	3.4	1.7.5	2.7	1.1	2.5	6	2.1	1.7	2.2	135.4	15.3	2.8	2	·	·	·	2.1	1.7	8	·	·	·	–	1	4	1.5	·
X	7.5	1.7	5.5	3.5	2	1.0	·	·	2.7	2.7	2.0	2.3	4	2.2	3	3.0	2.4	1.9	2.9.9	1.2.5	2.2	7	·	·	·	7	3	2	·	·	·	–	·	1.1	4	·
XI	5.5	5.2	8	4.6	8	1.8	4.5	2.0	2.3	3.0	1.7	2.2	5.5	2.2	0.5	2.8	1.7	2.4	4.8.6	2.3.0	2.8	1.7	3	1	·	9	7	2	·	·	·	–	·	7	1.7	1
XII	1.1.6	2.8	1.0.5	2.7	3.6	1.9	2	3.0	2.5	4.0	2.8	3.9	1.5	2.7	4	2.5	1.2	2.9	3.9.9	8.1	1.1	2.8	1.7	6	·	1.7	9	·	·	·	·	–	·	3	2.0	1.5
Rok	1.0.1	2.8	1.3.1.5	2.8	3.5.5	1.8	1.4	1.6	2.2.2	2.9	2.2.0.5	2.7	6.5	2.2	7.8.5	2.3	2.2.7	2.1	1.0.0.5.0	7.0.0	1.6.VII	1.4.6	3.9	2.4	1.9	1.7.4	1.3.5	3.6	1	·	·	–	2.2	7.3	1.6.0	9.3

Nowy Targ

$H_s = 600\ m$ $h_w = 20\ m$

I	7	4.1	3	1.7	2.2	2.3	2	1.5	7	1.5	1	8.0	1.8	4.9	1.0	4.1	2.3	2.3	2.9.1	·	·	3.0	1.2	1.3	·	1.5	9	·	1	·	1	–	2	1.6	–
II	9.5	1.8	5.5	1.6	2.5.5	2.7	·	·	·	·	·	·	1.5.5	6.8	1.2	3.2	1.6	2.3	2.7.3	1.2.4	2.5	2.3	3	4	·	1.2	9	1	4	1	3	–	2	1.2	–
III	1.2	1.7	6.5	3.0	1.8	4.4	1	2.0	·	·	3.5	3.8	1.8	4.8	1.8	3.0	1.6	2.9	3.3.9	7.8	1.8	2.1	3	9	·	1.0	8	·	3	1	1	–	9	1.0	–
IV	4.8.5	1.6	1.3	1.6	1.0	2.1	1	4.0	2	2.5	1	4.5	7.5	2.7	1.4	3.0	2.3	1.6	4.6.1	1.2.5	3.1	1.6	·	·	·	1.5	1.0	1	·	·	1	–	6	1.3	–
V	1.9	2.1	1.1.5	2.6	2.3	2.5	2	2.0	3	1.7	·	·	8	3.6	1.5.5	2.8	1.1	2.2	5.1.8	1.2.2	1.4	5	·	·	·	1.6	1.0	1	·	·	·	–	4	1.9	–
VI	1.3.5	1.4	4	1.0	1.7	1.6	·	·	5	4.2	1	4.0	2.3	3.4	1.0.5	1.8	1.6	1.3	6.5.8	2.4.0	2	·	·	·	8	9	7	1	1	·	·	–	1.0	2	–
VII	1.2	1.4	4	1.4	9	1.9	1.5	1.0	1	1.0	2.5	4.2	1.2	2.3	1.5	1.7	5.6	1.1	1.5.1.7	2.8.0	1.1	·	·	·	9	2.1	1.7	5	·	·	·	–	5	1.2	–
VIII	9.5	1.6	3	1.0	4	1.0	·	·	·	·	4.5	1.9	2.1.6	2.9	2.4.5	1.8	2.6	1.5	6.2.9	2.1.0	2.8	·	·	·	5	1.5	1.0	2	·	·	6	–	5	6	–
IX	5.5	1.3	1.5	1.7	1.1	1.1	·	·	·	·	2.5	5.0	3.6.5	3.4	1.4	2.1	1.9	2.1	6.4.3	1.0.6	3	2	·	·	2	1.6	1.3	2	·	·	5	–	4	1.2	–
X	1.7.5	1.1	4	1.0	1.4	1.3	·	·	·	·	·	·	1.9	2.7	1.6.5	1.4	2.2	1.2	2.5.4	1.1.9	3.2	1.5	·	·	·	5	4	1	·	·	8	–	1.0	6	–
XI	5.5	2.0	8.5	1.7	3.8	2.4	1	1.0	·	·	1.7.5	3.2	8.5	3.5	1.1	2.2	2.2.4	7.6	2.9	1.6	3	2	·	·	9	4	·	1	·	·	8	–	3	1.7	–
XII	6	1.0	7	1.9	2.9	1.9	·	·	·	·	4	2.9	2.5.5	4.4	8.5	1.5	1.3	2.3	2.8.2	9.7	5	3.0	1.7	1.1	·	1.0	8	·	2	·	1	–	6	1.9	–
Rok	1.3.5.5	1.5	7.1.5	1.7	2.2.0.5	2.1	8.5	1.0	1.8	0.9	2.0	2.9	2.2.2	3.8	1.1.6.7	2.5	2.3.2	2.0	6.1.9.9	2.8.0	1.1.VII	1.5.8	3.8	2.9	2.4	1.5.3	1.0.9	1.4	1.2	2	3.4	–	6.6	1.4.4	–

Jabłonka

$H_s = 620\ m$ $h_w = 21\ m$

I	3	4.3	1.1	2.3	1.1	1.2	2	1.5	2	3.2	2.7.5	2.7	3	5.7	2.5	8.6	3.4	1.9	2.1.7	6.2	6	2.8	1.2	1.2	·	1.3	9	·	1	·	3	·	2	1.8	2.8
II	5.5	2.5	5	1.4	3	1.3	0.5	1.0	1.5	7.7	3.9.5	5.2	2	2.8	2	2.0	2.5	3.0	3.5.1	8.6	2.5	2.1	3	4	·	1.3	1.1	·	3	·	3	·	1	1.3	1.1
III	2.5	1.6	1.2	2.2	3.5	2.9	0.5	1.0	·	·	2.7	4.3	2.5	4.6	1	3.0	4.4	1.9	4.1.5	1.1.5	1.7	2.2	3	1.0	·	1.1	8	1	2	1	5	1	4	7	1.1
IV	1.5	3.0	1.7	3.0	4.5	1.7	2	2.2	3	3.3	8.5	2.4	0.5	2.0	5.5	1.9	3.4	1.7	5.7.7	1.6.4	1.1	1.6	·	·	·	1.6	1.2	1	·	·	3	2	4	1.3	2
V	1.2	3.1	3.8.5	3.4	6.5	1.7	·	·	1.5	2.7	6	2.9	1	4.5	3.5	3.7	2.4	2.3	3.6.5	7.3	1.4	5	·	·	·	1.2	8	·	·	·	2	4	2	1.5	1
VI	6	3.2	1.2.5	3.0	6	1.9	0.5	5.0	2.5	6.2	2.2	5.0	2	3.0	3.5	3.0	3.5	2.4	4.3.4	1.2.4	9	·	·	·	6	1.3	8	1	4	2	5	6	4	3	·
VII	5.5	2.4	7	2.6	5.5	2.0	2	2.5	2.5	3.6	3.1	3.2	6	2.9	2.5	2.2	3.1	1.9	1.8.0.8	2.0.9	1.5	·	·	·	9	2.2	1.7	3	1	·	3	8	2	1.3	·
VIII	8	2.2	6	1.9	2	1.2	1	1.0	2.5	1.2	2.2	3.5	1.5	3.0	5	4.1	4.5	1.5	7.8.8	1.7.6	2.8	·	·	·	5	1.7	1.1	5	2	2	1.0	3	2	6	·
IX	4.5	2.7	5.5	2.2	1	1.0	0.5	2.0	2.5	5.0	3.4	4.3	1.2	2.5	4	2.5	2.6	2.5	8.4.4	2.1.1	4	2	·	·	·	2.2	1.4	2	2	2	7	1	1	1.4	·
X	5	1.8	5	1.4	6.5	1.3	3	1.3	1.5	1.7	2.5.5	3.7	·	·	2.5	1.4	4.4	4.4	2.9.0	1.4.5	2.2	1.6	·	·	·	1.1	4	1	·	·	8	·	4	5	·
XI	6	4.2	1.2.5	3.7	1.2.5	1.7	3	1.0	1	3.0	2.7	4.1	2	2.0	·	·	2.6	2.4	2.9.8	1.2.5	2.8	1.6	3	2	·	1.3	7	1	2	·	7	·	3	1.5	1
XII	1.0.5	2.8	8	2.9	6	1.7	3.5	1.1	·	·	3.2	5.4	3	3.7	2	4.0	2.8	2.8	2.0.3	4.3	9	2.8	1.1	1.0	·	1.4	9	·	2	1	1	·	6	1.5	1.0
Rok	8.3.6	2.8	1.4.0	2.5	6.8	1.6	1.8.5	1.6	2.0.5	3.1	3.0.2	3.9	3.5.5	3.1	3.4	3.0	3.9.3	2.1	5.9.9.0	2.1.1	4.1.X.	4.5.4	3.2	3.8	2.0	1.7.7	1.1.8	1.3	1.9	8	5.7	2.5	3.4	1.3.5	6.4

Maniowy

$H_s = 520\ m$ $h_w = 16\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3.0.9	7.4	6	3.1	1.5	1.3	·	1.6	1.0	·	·	·	4	·	1	1.8	2.8
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	2.2.9	8.1	2.5	2.8	2	5	·	1.5	6	·	·	·	5	·	1	1.5	1.6
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	3.5.0	8.4	1.9	2.1	3	7	·	9	6	·	·	·	2	1	4	1.2	1.2
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.9.5	1.4.5	1.1	1.6	·	·	·	1.7	8	1	·	·	3	1	3	1.4	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.0.2	1.2.0	8	5	·	·	·	1.7	1.3	1	·	·	7	2	·	1.8	·
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	4.2.4	1.7.0	1.2	1	·	·	1.1	1.3	8	2	·	·	5	4	2	5	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1.6.8.7	5.4.0	1.5	·	·	·	9	2.1	1.5	5	·	·	5	4	·	1.6	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	8.0.1	2.0.4	2.9	·	·	·	5	1.7	1.3	2	·	·	1.3	1	·	3	·
IX	·	·	1	1.0	8.5	3.1	0.5	3.0	·	·	0.5	5.0	3.1	3.9	1.3.5	3.5	3.5	2.2	8.0.9	1.6.3	3	2	·	·	2	2.5	1.3	1	·	·	1.0	·	·	1.1	·
X	2.5	1.4	2.5	1.8	6.5	2.2	1.5	2.7	1	2.0	2.5	2.2	2.1.5	2.0	5	1.6	5.0	0.9	3.3.1	1.2.7	2.2	1.2	·	·	·	2.0	4	1	·	·	1.7	·	·	5	·
XI	5	4.9	6	5.2	2.4	5.0	4.5	5.2	·	·	·	·	1.8	3.9	9.5	5.4	2.3	3.6	2.9.8	1.0.1	2.9	1.4	2	1	·	1.4	5	·	2	·	7	·	1	1.6	1
XII	·	·	3.5	3.6	2.0	2.5	1.5	2.7	·	·	0.5	2.0	2.4	4.3	1.1.5	4.0	3.2	2.3	1.6.7	4.5	5	3.0	1.1	9	·	1.1	5	·	1	1	2	·	·	1.4	1.3
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5.0.2	5.4.0	1.5.VII	1.6.0	3.1	3.5	2.7	1.9.5	1.0.6	1.3	·	·	8.0	1.3	1.2	1.6.3	7.1

Lesko

$\varphi = 49°28'$ $\lambda = 22°20'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia																					
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies	Max	Min	Max obs	Data	Min obs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	976.2	986.4	961.6	1023.2	-2.6	-0.4	-1.9	-1.6	0.6	-4.6	8.2	3	-13.9	22	82	73	80	78	4.0	4.7	4.1	4.3	8.4	8.0	6.9	7.8
II	968.0	983.3	946.9	1014.0	4.3	3.8	2.4	2.5	5.4	-0.5	14.4	19	-7.1	28	81	70	76	76	4.4	2.6	1.9	2.0	8.1	8.1	7.2	7.8
III	973.2	986.9	955.7	1019.6	-1.0	5.4	2.1	2.2	7.2	-3.0	17.4	30	-10.4	4	76	55	67	66	1.6	5.0	2.6	3.1	6.3	6.0	4.8	5.7
IV	–	–	–	–	4.1	11.9	7.7	7.8	13.5	2.3	24.9	30	-2.0	16	68	52	72	70	1.7	8.2	3.5	4.5	5.4	6.7	6.7	5.9
V	–	–	–	–	6.9	11.4	8.9	9.0	13.5	4.8	22.2	17	-0.4	30	59	70	82	80	4.1	5.3	2.3	2.9	7.8	8.5	6.8	7.7
VI	–	–	–	–	14.6	21.5	16.7	17.4	22.8	10.8	31.4	12	4.9	28	84	54	77	72	2.9	12.3	4.6	6.6	4.7	5.0	4.3	4.7
VII	–	–	–	–	15.8	21.8	17.5	18.2	23.3	13.3	32.7	8	7.6	29	88	64	83	78	2.2	10.6	3.8	5.5	6.2	6.4	6.2	6.3
VIII	–	–	–	–	12.8	19.9	15.2	15.8	21.4	10.8	31.9	14	5.7	31	93	62	84	80	1.1	9.9	3.1	4.7	6.0	5.5	4.4	5.3
IX	–	–	–	–	9.6	15.2	11.5	12.0	16.4	7.8	25.5	9	-4.0	26	91	66	86	84	1.2	6.3	2.0	3.2	7.4	7.0	5.6	7.0
X	–	–	–	–	6.3	13.2	7.9	8.6	14.2	3.4	23.9	20	-4.6	3	87	58	83	75	1.5	7.0	2.4	3.6	5.0	4.7	3.6	4.4
XI	–	–	–	–	2.6	6.7	5.2	3.9	7.6	0.8	16.8	5	-11.3	30	87	70	84	80	1.0	3.5	1.4	2.0	7.1	6.5	5.3	6.6
XII	–	–	–	–	-3.0	0.5	-0.8	-0.8	2.1	-4.4	14.7	13	-14.0	1	90	69	76	78	4.2	2.1	1.6	1.6	7.0	7.2	6.2	6.8
Rok	–	–	–	–	5.6	10.9	7.5	7.9	12.3	3.5	32.7	6 VII	-14.0	4 III	83	69	79	76	1.4	5.2	2.5	3.1	6.5	6.5	5.5	6.0

Czarny Dunajec

$\varphi = 49°27'$ $\lambda = 19°51'$

I	–	–	–	–	-5.4	-2.3	-4.5	-4.2	-0.2	-7.6	4.5	24	-17.8	17	–	–	–	–	–	–	–	–	9.0	7.6	5.8	7.3
II	–	–	–	–	-2.0	2.2	-0.5	-0.2	4.3	-5.8	9.1	18	-15.9	23	–	–	–	–	–	–	–	–	8.4	7.5	6.1	7.3
III	–	–	–	–	-3.1	4.6	0.6	0.6	7.2	-4.5	14.7	21	-14.8	4	–	–	–	–	–	–	–	–	6.7	6.0	4.7	5.8
IV	–	–	–	–	2.1	9.2	4.9	5.3	11.1	0.4	22.9	30	-7.6	9	–	–	–	–	–	–	–	–	6.2	6.9	6.6	6.6
V	–	–	–	–	5.4	10.2	7.1	7.4	12.0	2.8	22.5	19	-4.7	2	–	–	–	–	–	–	–	–	7.2	8.9	7.6	7.9
VI	–	–	–	–	13.4	20.7	16.0	16.0	22.1	8.7	29.1	11	1.4	28	–	–	–	–	–	–	–	–	4.1	5.8	5.4	5.1
VII	–	–	–	–	15.0	20.2	15.0	16.8	21.7	11.5	33.1	8	6.0	29	–	–	–	–	–	–	–	–	6.9	6.9	7.0	6.9
VIII	–	–	–	–	11.3	18.2	13.3	14.0	19.6	7.9	27.2	12	0.7	31	–	–	–	–	–	–	–	–	4.7	6.5	5.8	5.7
IX	–	–	–	–	7.2	13.6	9.3	9.8	14.7	5.0	24.5	9	-3.0	26	–	–	–	–	–	–	–	–	6.7	7.0	6.9	6.9
X	–	–	–	–	3.0	11.9	6.3	6.9	12.8	0.9	20.4	19	-4.9	3	–	–	–	–	–	–	–	–	5.7	4.6	3.5	4.6
XI	–	–	–	–	0.4	5.1	4.5	2.2	6.3	-4.5	17.0	6	-13.5	30	–	–	–	–	–	–	–	–	8.0	6.2	7.5	7.2
XII	–	–	–	–	-4.3	-1.1	-3.0	-2.8	0.6	-6.7	12.0	13	-14.6	11	–	–	–	–	–	–	–	–	7.9	7.3	6.1	7.2
Rok	–	–	–	–	3.6	9.4	5.5	6.0	11.0	1.1	33.1	8 VII	-17.8	17 I	–	–	–	–	–	–	–	–	6.8	6.8	5.9	6.6

Brzegi Dolne

$\varphi = 49°27'$ $\lambda = 22°38'$

I	–	–	–	–	-2.9	-0.3	-3.3	-2.4	1.0	-6.5	8.0	3	-15.2	22	83	77	85	82	0.8	1.5	0.7	1.0	9.1	9.0	7.2	8.5
II	–	–	–	–	1.2	3.2	1.5	2.0	5.7	-1.0	14.4	19	-9.0	24	85	74	81	80	1.0	2.3	1.4	1.6	8.3	9.0	7.5	8.4
III	–	–	–	–	-2.4	5.0	1.7	-0.2	6.6	-6.1	17.4	21	-24.8	4	60	61	82	74	1.3	4.3	1.1	2.2	7.0	6.5	4.6	5.9
IV	–	–	–	–	3.5	11.5	4.2	6.0	13.3	-0.1	24.7	30	-6.5	4	86	55	88	76	1.3	7.7	1.0	3.3	6.7	7.2	4.6	6.2
V	–	–	–	–	6.0	11.1	6.6	7.8	13.2	3.1	21.9	14	-2.7	30	93	72	93	86	0.8	4.8	0.8	2.1	7.8	9.3	7.1	8.0
VI	–	–	–	–	15.5	21.6	17.3	18.0	22.8	8.2	30.5	12	1.7	2	79	54	89	74	4.0	12.2	2.0	6.1	5.8	6.7	5.6	6.0
VII	–	–	–	–	15.9	21.7	15.2	17.0	23.7	–	32.1	8	4.9	29	87	62	90	80	2.5	10.9	1.8	5.1	7.0	7.5	6.4	7.0
VIII	–	–	–	–	13.3	19.8	12.5	14.5	21.3	8.2	31.0	14	1.8	31	93	64	94	84	1.2	9.4	1.1	3.9	7.3	7.2	5.3	6.6
IX	–	–	–	–	8.9	15.1	9.7	10.5	16.5	6.0	25.5	9	-4.0	26	93	68	92	84	1.0	6.0	1.1	2.7	8.2	8.0	6.5	7.6
X	–	–	–	–	3.9	13.4	4.8	6.7	14.3	1.0	19.9	19,20	-5.1	3	90	59	88	79	1.1	7.0	1.4	3.2	6.0	4.2	4.5	5.1
XI	–	–	–	–	0.6	6.2	0.3	2.2	7.6	-4.5	17.3	5	-11.5	30	84	74	90	85	0.8	3.1	0.7	1.5	8.0	7.3	6.5	7.3
XII	–	–	–	–	-2.5	0.4	-1.2	-1.3	2.3	-4.9	10.9	13	-14.7	11	84	74	79	78	1.1	4.0	1.4	1.5	7.7	8.0	6.4	7.4
Rok	–	–	–	–	5.2	10.8	5.2	6.6	12.4	–	32.1	8 VII	-24.8	4 II	87	66	88	80	1.4	5.9	1.2	2.8	7.4	7.5	6.2	7.0

Czorsztyn, leśnictwo

$\varphi = 49°26'$ $\lambda = 20°19'$

I	–	–	–	–	-5.9	-1.3	-4.3	-4.0	-0.6	-7.6	5.3	9	-20.7	17	–	–	–	–	–	–	–	–	8.4	7.3	6.7	7.5
II	–	–	–	–	-2.0	2.3	-0.1	0.3	4.6	-5.8	10.5	18	-13.8	23	–	–	–	–	–	–	–	–	8.1	8.4	7.0	7.8
III	–	–	–	–	-4.7	5.2	0.4	0.6	8.0	-4.4	15.9	21	-17.6	4	–	–	–	–	–	–	–	–	5.9	4.5	4.3	5.0
IV	–	–	–	–	3.8	11.3	4.4	6.0	12.3	1.0	22.2	30	-3.4	6,14	–	–	–	–	–	–	–	–	5.6	6.2	6.1	6.0
V	–	–	–	–	5.5	11.4	6.3	7.5	12.5	4.1	21.6	19	-2.2	30	–	–	–	–	–	–	–	–	7.0	8.2	6.7	7.3
VI	–	–	–	–	13.7	21.0	14.1	15.9	23.0	8.4	30.2	12	0.4	7	–	–	–	–	–	–	–	–	3.2	4.5	5.0	3.6
VII	–	–	–	–	14.2	21.0	15.5	16.6	23.0	11.6	33.4	9	5.9	29,30	–	–	–	–	–	–	–	–	5.3	6.1	5.3	5.4
VIII	–	–	–	–	11.5	17.9	13.1	14.2	21.2	9.3	30.5	11	4.0	31	–	–	–	–	–	–	–	–	6.5	5.8	4.5	5.6
IX	–	–	–	–	7.6	13.1	8.9	10.2	16.2	5.9	28.5	9	-1.5	26	–	–	–	–	–	–	–	–	6.9	5.6	6.0	6.1
X	–	–	–	–	3.1	12.0	5.3	6.8	14.4	1.6	21.6	13	-3.0	3,5	–	–	–	–	–	–	–	–	9.2	4.4	5.0	5.2
XI	–	–	–	–	1.1	5.5	2.3	2.9	6.8	-0.3	16.5	6	-11.8	30	–	–	–	–	–	–	–	–	7.8	5.7	5.8	6.8
XII	–	–	–	–	-4.0	-0.8	-1.2	-1.9	0.8	-6.6	11.2	13	-14.3	11	–	–	–	–	–	–	–	–	7.2	6.3	5.8	6.6
Rok	–	–	–	–	4.0	10.2	5.1	6.2	11.8	1.6	33.4	11 VIII	-20.7	17 I	–	–	–	–	–	–	–	–	6.9	5.9	5.7	6.2

Lesko

$H_s = 386\ m$ $H_b = 375{,}2\ m$ $h_w = 18\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU (%D, %nD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<0	Max=0	Min<-10	Max≥25	Opad R R≥0.1	R≥1.0	R≥10.0	Wiatr v v≥10	v≥15					
I	5	2,1	3,5	3,6	5	4,8	0,5	3,0	31,5	4,3	6,5	4,5	6,5	5,1	7,5	4,2	27	3,0	23,5	4,8	28	26	12	3	·	15	9	·	1	·	2	·	·	16	27
II	3,5	3,0	·	·	1,5	1,0	5,5	6,9	35,5	6,9	12,5	6,4	5	5,1	9,5	3,1	11	5,0	34,8	8,5	25	12	2	·	·	20	7	·	10	3	1	·	1	17	11
III	7,5	3,9	5	2,6	12,5	3,2	12,5	4,6	16	4,0	6,5	6,5	7	5,5	5	3,8	21	2,8	26,6	6,0	16	20	7	3	·	13	6	·	1	·	·	·	5	9	11
IV	5	3,1	1,3	2,8	7	2,3	8,5	2,2	11	2,8	3	3,7	4	2,4	14,5	2,2	24	1,9	54,7	13,2	11	13	·	·	·	17	10	2	·	·	3	2	6	9	2
V	5	2,5	15,5	3,4	14,5	3,6	4,5	1,2	6	2,2	1,5	2,0	3	4,2	2,3	3,4	20	2,4	141,4	44,3	6	3	·	·	·	18	16	4	1	·	4	2	·	17	2
VI	9,5	2,3	5,5	3,2	0,5	3,0	8,5	2,1	2,5	4,4	10,5	5,3	5,5	3,5	11	2,0	14	3,0	89,4	36,3	12	·	·	·	9	13	7	4	5	·	7	8	5	1	·
VII	8	2,0	5	1,2	2	1,0	10,5	1,2	14	2,1	13	3,6	8	2,7	9,5	2,0	23	1,6	113,2	24,4	27	·	·	·	10	21	15	4	2	·	6	9	1	12	·
VIII	3,5	1,9	0,5	1,0	3,5	1,0	4	1,0	12	3,0	9,5	4,4	3	2,8	20	2,8	35	1,7	56,1	27,2	29	·	·	·	6	15	8	2	1	·	6	3	1	6	·
IX	6	1,7	2,5	1,0	2,5	1,0	3	2,7	14	4,7	20	5,1	7,5	3,1	13,5	3,6	21	2,9	108,9	30,9	3	1	·	·	1	20	16	3	·	·	3	6	2	14	·
X	4,5	1,9	3	1,0	0,5	2,0	7,5	1,3	25,5	3,6	10,5	5,1	4,5	1,7	6	1,9	31	2,0	17,0	7,4	20	5	·	·	·	7	3	·	3	1	6	·	10	5	·
XI	4	7,2	4	1,4	16,5	2,5	6,5	1,0	17	2,9	11,5	6,3	4,5	6,2	3	5,8	23	2,8	30,2	10,5	11	13	2	1	·	8	5	1	2	·	·	·	4	14	1
XII	1,5	3,0	5,5	4,7	4	2,2	4,5	1,8	27,5	5,4	19	6,6	2	3,2	4,5	3,9	11	4,2	26,5	8,4	5	27	9	2	·	11	6	·	12	4	·	·	3	13	12
Rok	78,5	2,9	6,3	2,2	7,0	2,3	7,6	2,2	23,5	3,9	12,4	4,9	6,0,5	3,8	12,7	3,2	26,1	2,8	722,3	44,8	6.V	120	32	9	26	178	108	20	·	8	36	20	38	133	66

Czarny Dunajec

$H_s = 680\ m$ $h_w = 16\ m$

I	1	1,0	9,5	3,6	7,5	2,3	1	1,0	1	1,0	12,5	4,1	17	4,9	1,5	7,7	42	2,2	26,9	9,4	6	31	12	9	·	16	6	·	-	-	3	·	·	15	29
II	1	3,0	3,5	2,1	1	1,0	0,5	1,0	1	12,0	19,5	3,9	15	3,8	5,5	5,5	37	2,1	55,4	10,0	25	21	4	4	·	12	9	1	-	-	3	·	2	14	11
III	2	3,0	6	2,5	9,5	2,4	·	·	0,5	3,0	11,5	4,4	18	3,7	4,5	2,9	41	1,9	45,8	9,1	17	21	3	8	·	9	9	·	-	-	3	1	7	11	15
IV	9,5	5,0	16,5	3,4	4	2,8	2	3,0	2,5	2,6	3	3,0	3	3,7	2,5	4,2	47	1,8	51,7	15,1	11	14	·	·	·	16	12	2	-	-	3	2	5	15	2
V	8	2,9	2,8	3,1	13,5	2,7	0,5	3,0	·	·	1,5	1,0	4	6,0	4,5	3,9	33	2,0	46,9	12,1	20	5	·	·	·	19	13	1	-	-	·	4	1	19	2
VI	5,5	5,9	7,5	3,4	1,0	1,8	1,5	2,3	4,5	2,3	11	4,7	10	3,7	7	4,2	33	2,3	60,1	11,7	8	·	·	·	7	12	11	1	-	-	3	8	7	6	·
VII	4,5	4,6	1,1	2,9	4	1,6	0,5	1,0	0,5	1,0	2,3	3,0	12,5	2,4	2	1,5	35	1,7	175,9	29,6	12	·	·	·	9	21	18	7	-	-	7	10	5	16	·
VIII	7	2,6	9,5	2,9	2,5	2,5	·	·	·	·	1,0	4,1	1,5	3,8	6	3,4	43	1,8	108,6	29,2	28	·	·	·	4	16	12	4	-	-	5	4	2	4	·
IX	6,5	3,2	8,5	2,5	1,5	1,0	·	·	·	·	2,0	3,8	2,4	3,8	4,5	4,1	25	2,5	81,3	13,7	4,2,4	2	·	·	·	16	13	3	-	-	10	2	4	15	·
X	6	1,9	7,5	1,9	2,5	1,4	·	·	0,5	1,0	11	2,5	18,5	3,6	·	·	47	1,3	32,5	15,3	22	16	·	·	·	4	4	1	-	-	8	·	9	7	·
XI	4,5	10,4	6,5	2,5	2,0	2,6	0,5	3,0	5	2,8	9	3,2	10	4,4	0,5	1,2	34	2,3	22,1	8,6	28	15	2	1	·	9	6	·	-	-	6	·	4	18	1
XII	3	3,2	5,5	2,7	3	2,0	2	2,3	2,5	2,0	1,3	4,6	14,5	5,0	2,5	6,6	47	2,0	25,6	5,4	5	29	15	10	·	12	9	·	-	-	3	·	2	16	11
Rok	58,5	3,9	119,5	2,8	79	2,0	8,5	1,4	18	2,3	114,5	3,5	161,5	4,1	41	3,5	464	2,0	722,8	29,6	12.VII	154	36	32	20	162	125	20	-	-	54	81	48	156	71

Brzegi Dolne

$H_s = 420\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	20,5	2,7	8	29	10	8	·	16	10		-	-	-	·	·	20	31
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32,4	6,5	25	14	2	·	·	16	8		-	-	-	·	1	20	10
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46,2	11,0	18	25	8	9	·	11	7	1	-	-	-	1	4	10	13
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	57,1	12,6	25	15	·	·	·	16	12	2	-	-	-	3	6	12	2
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	128,1	33,4	6	4	·	·	·	21	16	4	-	-	-	3	·	17	2
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	104,0	44,6	12	·	·	·	9	11	8	2	-	-	-	8	3	9	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	82,0	26,9	27	·	·	·	13	17	12	1	-	-	-	5	1	15	·
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	70,3	28,1	29	·	·	·	7	16	9	2	-	-	-	4	1	8	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	71,8	17,0	12	2	·	·	1	20	15	2	-	-	-	1	2	15	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	19,1	8,0	20	16	·	·	·	11	4		-	-	-	·	5	9	·
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	54,9	19,0	11	16	3	3	·	12	7	3	-	-	-	·	3	17	1
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40,8	11,2	14	28	9	5	·	10	8	1	-	-	-	·	2	16	12
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	727,2	44,6	12.VI	147	32	25	30	177	116	18	-	-	-	25	28	168	71

Czorsztyn, leśnictwo

$H_s = 496\ m$ $h_w = 24\ m$

I	13,5	1,2	6	1,5	12,5	1,3	4	2,4	·	·	1,5	1,0	12	1,2	43,5	1,4	·	1,4	26,5	6,4	6	28	14	11	·	13	8		·	·	-	·	3	18	30
II	14	1,1	3	1,7	18	2,1	15	4,6	2	1,0	·	·	5,5	1,8	26,5	1,2	·	1,5	17,4	4,2	25	25	3	4	·	10	7	·	2	1	-	·	1	12	16
III	17	1,3	26,5	1,6	23	1,4	3	2,2	·	·	·	·	5	2,6	19,5	1,8	·	1,6	26,0	6,8	19	19	3	7	·	9	5	·	·	·	-	·	7	8	13
IV	20	1,4	20	1,4	11	1,5	8	1,9	·	·	·	·	0,5	1,0	29,5	1,4	1	1,4	41,9	11,3	11	13	·	·	·	14	10	1	·	·	-	1	7	15	·
V	16	1,2	36	1,4	8	1,4	1	2,5	·	·	·	·	5	1,0	28	1,4	·	1,4	57,3	13,6	8	2	·	·	·	14	12	2	·	·	-	·	1	16	·
VI	16	1,4	17	1,4	12,5	2,3	11,5	2,3	1	1,0	·	·	1,5	2,3	30,5	1,7	·	1,8	46,9	25,4	12	·	·	·	8	9	8	1	·	·	-	6	9	3	·
VII	28	1,1	18	1,3	7	1,0	5	1,4	1	1,0	·	·	6,5	1,2	26,5	1,4	1	1,2	144,4	44,1	15	·	·	·	8	17	14	5	·	·	-	6	5	15	·
VIII	23,5	1,1	18,5	1,1	8,5	1,4	5	2,1	·	·	·	·	5	1,3	32,5	1,2	·	1,2	76,4	21,2	29	·	·	·	5	15	11	2	·	·	-	2	4	7	·
IX	12	1,1	18,5	1,1	12	1,1	·	·	·	·	·	·	9,5	1,6	38	1,6	·	1,1	61,5	8,1	4	2	·	·	2	16	12	·	·	·	-	·	2	10	·
X	22,5	1,1	32	1,2	6,5	1,0	0,5	1,0	·	·	·	·	0,5	1,0	31	1,2	·	1,1	29,1	14,6	22	7	·	·	·	4	4	1	·	·	-	·	·	9	·
XI	15	1,2	14,5	1,1	25,5	2,0	2,5	1,8	2	1,0	·	·	2,5	1,1	28	1,4	·	1,5	19,0	8,4	29	13	2	1	·	8	6	·	·	·	-	·	3	13	1
XII	13	1,1	4	1,0	34	1,1	1	1,0	4	1,2	·	·	5	1,2	32	1,4	·	1,2	18,3	5,8	5	31	13	8	·	8	6	·	·	·	-	·	3	12	14
Rok	21,0,5	1,2	21,2	1,8	17,8,5	1,4	5,6,5	1,7	1,0	0,4	1,5	0,1	5,8,5	1,5	36,5,5	1,4	2	1,4	56,4,4	44,1	15.VII	140	35	31	23	137	103	12	2	1	-	15	45	134	74

Czorsztyn – Nadzamcze

$\varphi = 49°26'$ $\lambda = 20°20'$. 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-5.9	-2.2	-4.4	-4.2	-1.8	-6.8	4.7	2	-18.5	17	–	–	–	–	–	–	–	–	7.7	6.8	7.2	7.2
II	–	–	–	–	-2.2	1.9	-0.4	-0.3	2.7	-3.2	9.1	18,19	-12.4	23	–	–	–	–	–	–	–	–	6.6	6.7	6.8	6.7
III	–	–	–	–	-3.0	5.1	0.8	0.9	5.7	-3.9	14.6	21	-16.8	4	–	–	–	–	–	–	–	–	5.4	5.4	5.0	5.3
IV	–	–	–	–	2.0	9.9	5.4	5.7	10.2	1.3	20.0	28	-4.1	14	–	–	–	–	–	–	–	–	5.9	6.9	6.5	6.4
V	–	–	–	–	4.9	10.4	6.9	7.3	11.1	3.6	20.5	18,19	-1.2	30	–	–	–	–	–	–	–	–	6.6	7.9	7.2	7.2
VI	–	–	–	–	13.1	20.2	15.1	15.9	20.7	9.4	28.7	12	3.6	7	–	–	–	–	–	–	–	–	3.5	6.0	4.9	4.8
VII	–	–	–	–	13.4	19.7	15.6	16.1	20.2	11.9	32.3	5	6.9	30	–	–	–	–	–	–	–	–	6.1	7.7	6.6	6.8
VIII	–	–	–	–	10.9	18.2	13.4	14.0	18.9	9.5	28.5	14	2.9	31	–	–	–	–	–	–	–	–	4.6	6.5	5.2	5.4
IX	–	–	–	–	7.6	13.7	9.3	10.0	14.0	5.9	23.5	9	-2.1	26	–	–	–	–	–	–	–	–	5.3	6.8	6.9	6.3
X	–	–	–	–	2.9	11.7	6.3	6.8	12.0	1.8	20.0	19	-4.4	3	–	–	–	–	–	–	–	–	4.8	4.8	4.3	4.6
XI	–	–	–	–	0.5	4.5	2.2	2.3	5.3	-0.4	16.0	4	-13.5	30	–	–	–	–	–	–	–	–	6.3	6.7	7.3	6.8
XII	–	–	–	–	-4.7	-1.3	-2.9	-3.0	-0.4	-6.7	10.4	14	-13.2	11	–	–	–	–	–	–	–	–	6.8	6.9	7.2	7.0
Rok	–	–	–	–	3.3	9.5	5.6	6.0	9.9	1.9	32.3	5.VII	-18.5	17.1	–	–	–	–	–	–	–	–	5.8	6.6	6.3	6.2

Szczawnica – Zdrój

$\varphi = 49°26'$ $\lambda = 20°29'$

I	–	–	–	–	-4.3	-0.6	-3.6	-3.0	0.1	-5.8	6.2	2	-19.0	17	–	–	–	–	–	–	–	–	7.5	6.6	7.0	7.0
II	–	–	–	–	-0.8	4.0	1.1	1.4	4.7	-2.1	10.0	6	-12.0	23	–	–	–	–	–	–	–	–	7.2	6.7	6.2	6.7
III	–	–	–	–	-1.8	7.1	0.8	1.7	7.8	-3.1	16.6	21	-16.4	4	–	–	–	–	–	–	–	–	6.3	5.1	5.1	5.5
IV	–	–	–	–	3.0	11.8	5.6	6.5	12.3	1.6	23.4	30	-3.5	14,16	–	–	–	–	–	–	–	–	6.1	6.1	5.7	6.0
V	–	–	–	–	6.2	11.6	7.8	8.4	12.7	3.7	22.8	17	-1.0	30	–	–	–	–	–	–	–	–	7.2	8.1	7.0	7.4
VI	–	–	–	–	14.0	22.1	16.0	17.0	22.6	9.3	30.9	12	3.7	28	–	–	–	–	–	–	–	–	3.3	4.8	4.9	4.3
VII	–	–	–	–	14.6	21.1	16.8	17.3	21.9	12.2	34.2	5	6.8	29	–	–	–	–	–	–	–	–	6.2	7.2	6.4	6.6
VIII	–	–	–	–	11.7	19.9	14.8	15.3	20.9	9.8	30.7	14	4.0	31	–	–	–	–	–	–	–	–	6.0	5.6	5.9	5.8
IX	–	–	–	–	7.7	16.6	10.2	10.9	16.1	6.3	26.4	9	-2.0	26	–	–	–	–	–	–	–	–	7.1	6.6	6.8	6.8
X	–	–	–	–	3.6	13.4	6.4	7.4	13.8	1.7	21.3	19	-4.5	3	–	–	–	–	–	–	–	–	7.1	3.6	3.7	4.8
XI	–	–	–	–	2.0	6.4	3.0	3.6	7.3	0.9	17.4	4	-11.7	30	–	–	–	–	–	–	–	–	7.1	5.8	7.1	6.7
XII	–	–	–	–	-3.5	-0.1	-2.2	-2.0	0.7	-6.5	12.4	13	-11.6	11	–	–	–	–	–	–	–	–	6.9	6.5	6.3	6.6
Rok	–	–	–	–	4.4	11.0	6.4	7.0	11.7	2.4	34.2	5.VII	-19.0	17.1	–	–	–	–	–	–	–	–	6.5	6.1	6.0	6.2

Piwniczna

$\varphi = 49°26'$ $\lambda = 20°42'$

I	–	–	–	–	-3.8	-0.5	-2.8	-2.5	1.3	-6.2	6.5	26	-14.9	23	–	–	–	–	–	–	–	–	9.2	6.4	7.9	7.8
II	–	–	–	–	-0.1	4.2	1.3	1.7	5.8	-2.0	9.9	10	-11.5	23	–	–	–	–	–	–	–	–	8.2	7.1	7.4	7.6
III	–	–	–	–	-0.7	7.5	1.8	2.6	9.5	-3.0	17.7	14	-17.5	4	–	–	–	–	–	–	–	–	6.3	4.6	4.5	5.1
IV	–	–	–	–	4.2	12.1	6.2	7.2	13.8	1.5	24.5	30	-3.0	14	–	–	–	–	–	–	–	–	6.2	7.0	6.0	6.4
V	–	–	–	–	7.4	12.4	8.4	9.2	14.4	4.3	22.9	13,19	-1.7	30	–	–	–	–	–	–	–	–	7.4	8.3	6.5	7.4
VI	–	–	–	–	15.2	22.5	15.7	17.3	24.6	9.4	32.7	29	3.4	7	–	–	–	–	–	–	–	–	4.0	5.0	3.4	4.1
VII	–	–	–	–	16.6	22.1	16.8	18.1	24.8	12.8	36.6	5	8.2	4,19,30	–	–	–	–	–	–	–	–	6.6	7.2	6.0	6.7
VIII	–	–	–	–	13.3	20.7	14.6	15.8	22.7	9.9	31.7	12,14	4.4	24	–	–	–	–	–	–	–	–	5.6	5.8	5.2	5.5
IX	–	–	–	–	9.2	16.1	10.5	11.6	17.8	6.8	28.1	9	-1.6	26	–	–	–	–	–	–	–	–	8.1	6.1	5.6	6.6
X	–	–	–	–	4.4	14.0	6.0	7.6	15.3	2.0	20.5	9	-3.4	3	–	–	–	–	–	–	–	–	8.3	5.7	3.6	5.2
XI	–	–	–	–	3.0	7.0	3.4	4.2	8.5	0.7	17.9	4	-10.7	30	–	–	–	–	–	–	–	–	8.0	6.2	6.9	7.0
XII	–	–	–	–	-2.5	-0.1	-1.6	-1.4	1.5	-5.0	13.0	13	-12.9	11	–	–	–	–	–	–	–	–	8.4	7.5	7.7	7.9
Rok	–	–	–	–	5.5	11.5	6.7	7.6	13.3	2.6	36.6	5.VII	-17.5	4.III	–	–	–	–	–	–	–	–	7.2	6.2	5.9	6.4

Wysowa

$\varphi = 49°26'$ $\lambda = 21°11'$

I	–	–	–	–	-4.5	-3.0	-4.3	-4.0	-1.9	-6.8	2.4	8	-14.1	17,23	–	–	–	–	–	–	–	–	9.5	8.1	8.2	8.5
II	–	–	–	–	-0.9	1.2	-0.1	0.0	2.3	-2.6	7.5	18,19	-7.4	23,28	–	–	–	–	–	–	–	–	8.6	7.8	8.3	8.2
III	–	–	–	–	-2.5	5.0	-0.3	0.5	6.3	-5.0	15.4	31	-21.3	4	–	–	–	–	–	–	–	–	6.7	4.7	4.7	5.4
IV	–	–	–	–	4.4	10.7	4.8	6.2	11.9	0.4	22.4	30	-4.6	5,16	–	–	–	–	–	–	–	–	5.8	6.2	6.1	6.0
V	–	–	–	–	7.4	10.9	6.6	7.9	12.5	3.1	21.2	18	-3.2	30	–	–	–	–	–	–	–	–	6.9	7.9	6.7	7.2
VI	–	–	–	–	15.0	20.7	13.5	15.7	21.9	8.4	29.8	12	1.3	27	–	–	–	–	–	–	–	–	4.7	4.7	4.8	4.7
VII	–	–	–	–	16.2	20.2	14.7	16.4	22.0	11.0	34.4	5	5.0	29	–	–	–	–	–	–	–	–	7.0	6.8	5.8	6.5
VIII	–	–	–	–	13.5	19.4	12.4	14.4	20.4	8.0	28.4	14	3.1	31	–	–	–	–	–	–	–	–	4.7	5.4	5.5	5.2
IX	–	–	–	–	8.3	14.4	8.8	10.2	15.4	5.0	24.9	9	-3.9	26	–	–	–	–	–	–	–	–	6.5	6.9	5.8	6.4
X	–	–	–	–	4.0	11.5	5.7	6.7	12.2	1.3	16.8	9,12	-6.5	3	–	–	–	–	–	–	–	–	6.3	4.5	4.2	5.0
XI	–	–	–	–	2.0	4.6	2.1	2.7	5.5	-0.3	14.4	4	-12.1	30	–	–	–	–	–	–	–	–	7.9	6.9	6.9	7.2
XII	–	–	–	–	-3.5	-2.0	-3.2	-3.0	-1.0	-6.0	8.9	14	-17.7	11	–	–	–	–	–	–	–	–	9.1	8.5	8.5	8.7
Rok	–	–	–	–	5.0	9.5	5.1	6.2	10.6	1.4	34.4	5.VII	-21.3	4.III	–	–	–	–	–	–	–	–	7.0	6.5	6.3	6.6

Czorsztyn – Nadzamcze

$H_s = 650\,m$ $h_w = 16\,m$ **1957**

MIESIĄC	ROZKŁAD WIATRU °D, v m/D																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr v		≡	≥5	◔	●	⊞
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<0°	Max<0°	Min<-10	Max>25°	0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0	10 ≤ v < 15	v ≥ 15					
I	2	2.0	12	3.2	8	2.6	1	4.0	·	·	5	2.2	47	3.7	4	2.2	14	2.8	26.2	9.4	6	31	21	8	·	12	9	·	1	·	6	·	1	14	31
II	1	1.0	2	2.6	12.5	3.3	11.5	8.3	1	1.0	3	7.0	27	3.5	7	2.6	19	3.3	20.3	8.0	25	24	7	1	·	8	5	·	7	2	4	·	2	14	22?
III	1	1.0	19	3.2	11	4.5	5	5.3	·	·	6	4.5	28	4.7	5	2.6	18	3.3	29.7	12.2	16	21	7	8	·	7	5	1	4	2	1	1	4	6	11
IV	4	2.2	18	3.1	10.5	3.0	5.5	6.2	·	·	3	4.3	26	2.8	10	3.7	13	2.8	67.5	11.9	11	14	·	·	·	19	4	1	1	·	4	1	3	11	·
V	8	2.5	23	3.4	6	2.7	4	3.0	1	2.0	4	2.8	28	3.6	3	2.3	16	2.7	66.1	14.8	8	4	·	·	·	15	14	2	·	·	5	1	·	14	1
VI	5	2.6	9	3.3	11.5	3.0	10.5	7.3	·	·	5	3.2	25	3.8	7	2.9	17	3.2	43.3	20.9	12	·	·	·	4	8	7	1	3	1	1	4	2	1	·
VII	2	2.5	11	2.7	2	2.5	8	4.4	1	6.0	1	2.0	34	3.0	8	3.6	26	2.3	117.3	54.0	15	·	·	·	5	17	14	2	·	·	3	1	·	12	·
VIII	1	1.0	8	3.6	8	2.2	2	3.0	·	·	6	4.5	31	2.9	10	2.1	27	2.1	70.5	20.9	28	·	·	·	2	14	12	1	2	·	12	2	·	5	·
IX	1	1.0	11	2.4	5	2.6	3	3.3	·	·	9	6.0	46	4.6	2	3.5	13	3.6	74.1	10.7	4	2	·	·	·	19	14	1	6	1	8	·	1	6	·
X	2	1.5	7	2.1	13	2.3	3	4.7	1	1.0	5	2.8	29	2.9	5	2.2	28	1.8	25.8	11.7	20	9	·	·	·	5	3	1	·	·	20	·	4	1	·
XI	1	1.0	13	3.4	18.5	4.4	12.5	8.8	·	·	2	2.5	20	5.0	9	8.4	14	4.6	28.5	8.7	28	16	8	1	·	8	7	·	7	2	9	·	4	14	1
XII	·	·	18	2.6	9	2.7	9	4.4	1	1.0	5	9.2	23	4.4	13	3.8	15	3.3	14.6	4.4	8	30	17	9	·	8	6	·	4	1	2	·	1	12	12
Rok	28	1.5	151	3.0	115	3.0	75	5.2	5	0.9	54	4.2	364	3.7	83	3.3	220	3.0	583.9	54.0	15.VIII	151	60	25	11	140	100	10	35	9	75	14	22	110	78?

Szczawnica – Zdrój

$H_s = 500\,m$ $h_w = 32\,m$

I	8	1.6	20.5	1.6	20.5	2.0	2	2.0	1	2.0	2.5	2.6	5.5	3.9	2.2	2.3	11	1.8	28.6	4.8	28	27	12	8	·	14	10	·	·	·	3	·	·	14	29
II	2	1.5	9	1.7	26	2.3	9	5.7	3	6.6	5	5.6	6	2.2	18	2.7	6	2.8	30.4	7.4	25	22	5	2	·	14	9	·	4	·	1	·	4	·	13
III	9.5	1.8	15	1.7	19.5	2.0	7	3.0	3	1.7	7	3.8	10	2.9	16	2.2	6	2.2	34.0	7.4	16	18	3	5	·	9	8	·	2	·	1	1	5	10	11
IV	20.5	2.1	11.5	1.3	13.5	1.8	8.5	2.1	3	4.7	3	2.0	6	2.2	16	2.1	8	1.8	54.9	12.2	17	10	·	·	·	19	12	1	·	·	4	2	6	11	4
V	11.5	2.3	15.5	1.7	8	1.8	1.5	3.0	1	2.0	3	2.7	12	2.0	38.5	2.1	2	2.0	87.9	17.4	20	1	·	·	·	18	14	4	·	·	5	2	1	17	1
VI	1.5	2.7	12.5	1.6	1.5	2.0	9	3.3	5	4.4	6	4.2	8.5	1.6	14	3.0	5	2.5	41.6	12.2	12	·	·	·	7	12	10	1	1	·	1	7	5	·	·
VII	15.5	1.6	10.5	1.6	5	2.6	2	1.0	2.5	3.0	3.5	2.7	13	2.8	23	1.8	18	1.6	169.0	42.1	16	·	·	·	7	23	19	5	1	·	1	6	3	11	·
VIII	13.5	1.5	11.5	1.7	4.5	1.9	7.5	2.5	3	2.3	2.5	2.4	18	1.8	22.5	2.3	10	1.8	83.3	24.6	29	·	·	·	6	17	13	2	·	·	8	4	·	7	·
IX	14.5	1.6	4.5	1.2	5	1.6	4	2.8	2	1.5	10.5	2.6	24.5	2.1	11.0	2.0	14	1.7	64.6	7.7	12	2	·	·	2	19	14	·	·	·	6	·	2	11	·
X	7.5	1.7	15.5	1.5	20	1.7	8	1.6	5	1.6	7	1.8	12.5	1.8	7.5	2.1	10	1.5	29.4	11.1	22	6	·	·	·	4	4	1	·	·	8	·	3	2	·
XI	8	1.8	1.5	1.2	24	3.0	12	3.3	1	2.0	5	3.2	11.5	2.6	12.5	2.8	1	2.5	32.7	10.7	29	12	4	1	·	10	7	1	·	·	4	·	6	13	1
XII	4	2.0	10.5	1.4	20	2.3	5.5	4.6	5	3.8	3	2.0	16.5	2.1	23.5	2.2	5	2.2	28.3	6.4	5	29	13	4	·	16	8	·	1	·	2	·	3	12	13
Rok	129.5	1.8	154.5	1.5	181	2.1	76	2.9	34.5	3.0	58	3.0	144	2.3	224.5	2.3	96	2.0	681.7	42.1	16.VIII	127	37	20	22	175	128	15	9	·	44	22	38	108	72

Piwniczna

$H_s = 380\,m$ $h_w = 16\,m$

I	·	·	1	2.0	17	2.2	22	2.7	1	1.0	1	3.0	23	1.9	4	2.0	24	1.7	37.7	11.2	5	29	8	7	·	12	8	1	·	·	-	·	1	16	31
II	·	·	·	·	13	3.8	25	2.6	2	1.5	2	2.5	16	2.0	2	3.5	24	1.9	35.9	10.0	25	21	2	1	·	13	11	1	·	·	-	·	1	15	13
III	·	·	·	·	10	2.5	11	2.5	2	1.5	2	2.5	25	2.2	7	3.0	36	1.5	36.0	10.7	16	19	3	5	·	10	8	1	·	·	-	1	7	7	8
IV	·	·	1	2.0	4	2.2	7	3.3	1	2.0	·	·	2.4	1.6	13	1.8	40	1.1	46.7	13.0	11	10	·	·	·	17	11	1	·	·	-	2	7	15	·
V	1	1.0	1	2.0	3	1.3	4	1.5	·	·	2	2.0	37	1.8	19	2.0	26	1.3	92.8	20.6	10	1	·	·	·	20	14	3	·	·	-	3	2	14	·
VI	·	·	1	1.0	17	2.7	6	3.2	1	2.0	4	1.5	33	2.2	3	2.0	25	1.7	60.6	24.6	12	·	·	·	14	15	10	1	·	·	-	5	8	3	·
VII	·	·	1	2.0	7	1.4	8	1.8	·	·	1	2.0	23	1.6	1	2.0	52	0.7	117.2	23.7	16	·	·	·	14	19	14	4	·	·	-	10	5	14	·
VIII	·	·	·	·	6	2.7	2	2.5	2	1.5	2	1.5	37	1.8	1	2.0	43	1.0	86.2	21.2	28	·	·	·	8	16	12	3	·	·	-	5	1	5	·
IX	·	·	1	2.0	12	1.9	1	2.0	1	1.0	2	3.0	29	2.2	4	2.2	40	1.2	67.2	10.8	3	2	·	·	2	18	11	2	·	·	-	1	1	7	·
X	·	·	1	2.0	10	1.5	6	2.7	3	1.3	1	1.0	18	1.5	3	1.3	5.1	0.8	30.9	11.6	22	5	·	·	·	6	4	1	·	·	-	·	3	4	·
XI	·	·	·	·	10	2.2	8	2.4	7	2.0	1	2.0	22	2.4	6	3.8	36	1.5	36.4	17.9	29	11	1	1	·	8	5	1	·	·	-	·	3	15	1
XII	1	5.0	·	·	21	2.9	13	2.8	5	2.2	4	1.8	23	2.7	5	2.2	21	2.1	34.5	10.6	5	29	11	1	·	14	6	1	·	·	-	·	·	15	12
Rok	2	0.5	7	1.1	130	2.3	113	2.5	25	1.3	22	2.1	310	2.0	68	2.3	418	1.4	679.1	24.6	12.VI	127	25	15	38	168	114	20	·	·	-	27	59	130	65

Wysowa

$H_s = 525\,m$ $h_w = 16{,}5\,m$

I	3	3.2	2	3.5	·	·	43.5	5.4	15.5	3.5	·	·	4	6.5	22	4.8	3	4.7	44.2	11.3	5	30	22	7	·	15	10	2	2	·	8	·	·	20	31
II	1	6.0	·	·	2	6.8	40	6.8	18.5	4.2	1.5	2.3	1	5.0	18	4.2	2	5.4	36.3	9.9	25	26	7	·	·	15	11	·	7	·	10	·	·	18	21
III	4	4.5	2	2.5	1.5	4.3	33	4.5	8.5	2.7	1	5.0	6.5	2.2	26.5	4.3	11	3.6	39.8	11.3	24	21	6	9	·	12	9	1	3	·	1	·	7	10	12
IV	5	3.4	4.6	2.6	2	3.2	18	3.1	7	2.7	1	4.0	1	3.5	44.5	3.3	7	3.0	57.6	15.4	11	14	·	·	·	16	12	1	·	·	1	1	7	11	3
V	40	3.8	1.5	4.3	1	4.0	12	2.3	7	1.4	·	·	·	·	66.5	3.9	5	3.3	99.6	17.9	10	3	·	·	·	20	13	3	·	·	1	·	1	16	3
VI	5.5	3.1	1.5	2.0	1.5	6.3	25.5	4.8	13	3.8	4	1.1	1.6	1.7	25.5	3.2	12	3.2	62.9	29.3	8	·	·	·	6	13	9	1	·	·	·	5	8	4	·
VII	6.5	3.9	2.5	4.0	6.5	4.2	20	5.1	8	4.9	4.5	1.8	4.5	2.2	26.5	3.4	14	3.3	177.4	35.0	15	·	·	·	8	16	14	5	1	·	4	6	3	11	·
VIII	2.5	4.0	0.5	5.0	1.5	4.7	19	4.2	7.5	3.2	1	4.0	5	2.3	4.2	3.5	14	3.0	65.2	14.5	28	·	·	·	4	17	13	1	·	·	1	3	2	1	·
IX	·	·	0.5	4.0	2.5	3.4	20	3.3	8.5	3.1	2.5	1.8	6.5	2.1	29.5	3.3	20	2.4	101.5	31.3	3	3	·	·	·	18	14	3	·	·	3	2	5	11	·
X	·	·	·	·	1.5	4.0	3.3	3.2	1.3	2.6	3.6	1.9	1.5	3.3	21.5	2.3	19	2.2	29.0	8.8	23	12	·	·	·	8	5	·	·	·	7	·	6	6	·
XI	7.5	4.8	1.5	1.3	2	4.8	34	4.1	16	2.4	1	1.0	5.5	2.4	14.5	4.5	8	3.4	60.8	22.6	12	16	5	1	·	11	8	2	3	·	4	·	3	15	1
XII	3.5	6.7	·	·	1.5	6.0	43.5	4.6	14.5	3.2	0.5	2.0	3	1.3	24.5	4.5	2	4.2	33.3	8.7	5	30	21	3	·	18	9	·	4	·	3	·	1	23	14
Rok	48.6	3.6	16.5	2.4	23.5	4.3	341.5	4.3	137	3.1	20.5	1.8	39	2.7	384.5	3.8	117	3.5	807.0	35.0	15.VII	155	61	20	18	179	127	19	20	·	43	17	43	146	85

Barwinek

$\varphi = 49°26'$ $\lambda = 21°41'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-3,9	-2,7	-4,0	-3,6	-1,0	–	5,3	2,3	–	–	–	–	–	–	–	–	–	–	9,6	9,3	8,6	9,2
II	–	–	–	–	-0,3	1,2	0,4	0,4	3,1	-1,7	9,0	19	-7,6	28	–	–	–	–	–	–	–	–	9,5	9,1	8,9	9,2
III	–	–	–	–	-2,5	4,8	-0,5	0,3	6,5	-5,4	16,6	31	-24,0	4	83	65	80	76	4,0	3,8	1,4	2,1	5,5	5,0	4,4	5,0
IV	–	–	–	–	4,3	11,3	4,6	6,2	12,9	0,4	23,8	30	-5,7	14	–	–	–	–	–	–	–	–	5,9	6,4	6,0	6,1
V	–	–	–	–	6,9	11,1	6,5	7,8	13,5	3,3	21,3	13,17	-3,5	30	90	72	91	84	1,1	4,9	0,9	2,3	7,4	8,2	6,8	7,5
VI	–	–	–	–	13,0	20,5	13,9	15,8	22,2	8,5	30,6	12	2,0	7	–	–	–	–	–	–	–	–	4,9	4,4	4,7	4,7
VII	–	–	–	–	15,5	20,5	15,2	16,6	22,5	11,2	30,7	8	4,0	4	92	74	93	86	1,5	7,2	1,6	3,4	7,0	7,4	7,1	7,2
VIII	–	–	–	–	13,1	19,0	12,9	14,5	20,8	8,5	28,6	14	2,5	31	92	67	92	84	1,4	7,6	1,4	3,5	5,5	6,2	4,6	5,4
IX	–	–	–	–	9,1	14,3	9,4	10,6	16,1	5,2	24,3	9	-3,4	26	95	72	92	86	0,6	4,8	1,1	2,2	7,2	7,6	6,0	6,9
X	–	–	–	–	4,6	11,6	6,2	7,2	12,7	1,5	17,0	9	-2,1	3	94	88	89	84	0,6	4,7	1,3	2,2	5,6	5,4	3,5	4,8
XI	–	–	–	–	2,4	4,7	2,1	2,8	6,4	-0,2	15,2	9	-11,7	30	89	84	92	88	0,8	1,8	0,7	1,1	8,4	7,1	6,8	7,4
XII	–	–	–	–	-3,5	-2,2	-2,6	-2,7	-0,2	-5,6	10,1	14	-17,2	11	–	–	–	–	–	–	–	–	9,6	9,1	9,3	9,3
Rok	–	–	–	–	5,1	9,5	5,3	6,3	11,3	–	30,7	8.VII	–	–	–	–	–	–	–	–	–	–	7,1	7,1	6,4	6,9

Krynica

$\varphi = 49°26'$ $\lambda = 20°58'$

I	949,2	958,5	934,3	–	-5,1	-2,6	-4,4	-4,1	-1,0	-6,8	4,0	26	-16,0	23	94	82	89	87	0,4	0,9	0,5	0,6	9,1	7,8	7,8	8,2
II	941,3	956,7	920,3	–	-4,3	1,9	0,0	0,2	3,4	-3,0	8,9	19	-8,5	1,24	92	76	85	84	0,5	1,8	1,0	1,1	8,8	7,7	7,5	8,0
III	946,5	958,9	930,5	–	-2,5	5,0	0,4	0,8	7,1	-3,9	16,0	14	-16,2	4	84	59	75	73	1,0	4,3	1,8	2,4	5,8	4,8	3,9	4,8
IV	945,9	956,6	923,6	–	2,5	9,7	5,1	5,6	11,1	1,2	22,5	30	-3,8	9	91	62	82	78	0,6	5,8	1,6	2,7	5,7	6,7	5,0	5,8
V	943,9	952,1	932,5	–	5,4	10,3	7,0	7,4	11,8	3,7	22,0	19	-1,2	30	91	69	84	81	0,8	4,9	1,8	2,5	6,8	8,4	6,5	7,2
VI	947,6	959,4	937,8	–	13,2	20,6	15,4	16,2	22,6	9,8	30,4	12	3,7	7	84	53	75	71	2,5	12,1	4,7	6,4	3,9	5,5	4,5	4,6
VII	944,0	953,8	933,8	–	14,6	19,9	16,0	16,6	22,8	12,3	34,6	5	7,5	29	89	67	84	80	1,9	8,8	3,3	4,7	6,6	7,5	6,2	6,8
VIII	945,7	954,5	933,3	–	11,6	18,8	13,6	14,4	20,7	9,6	30,3	14	4,0	24	91	59	84	78	1,3	9,7	2,6	4,6	5,4	6,5	4,0	5,3
IX	944,6	953,6	932,2	–	7,6	14,3	9,3	10,1	16,1	5,9	26,1	9	-2,1	26	93	64	88	82	0,8	6,4	1,5	2,9	6,5	6,7	4,7	6,0
X	950,1	958,0	934,1	–	3,1	11,8	5,9	6,7	13,4	1,8	18,4	12	-5,1	3	95	64	88	82	0,5	5,3	1,3	2,4	8,1	4,2	4,2	5,5
XI	948,6	965,1	934,2	–	1,5	4,8	1,9	2,5	6,2	0,0	15,4	4	-13,8	30	90	80	89	86	0,7	2,2	0,9	1,3	7,9	7,0	7,3	7,4
XII	943,7	962,3	913,6	–	-4,1	-1,9	-3,1	-3,0	-0,2	-6,1	8,9	13,14	-15,7	11	91	85	89	88	0,4	0,8	0,6	0,6	8,6	8,4	8,4	8,5
Rok	943,9	965,1	913,6	–	3,9	9,4	5,6	6,1	11,2	2,0	34,6	5.VII	-16,2	4.III	90	68	84	81	1,0	5,2	1,8	2,7	6,9	6,8	5,8	6,5

Krynica – Góra Parkowa

$\varphi = 49°25'$ $\lambda = 20°58'$

I	–	–	–	–	-6,5	-3,1	-4,9	-4,8	-2,1	-6,9	3,0	26	-15,2	17	–	–	–	–	–	–	–	–	9,0	7,4	7,6	8,0
II	–	–	–	–	-1,9	1,1	-0,8	-0,6	2,2	-3,1	7,6	19	-8,4	28	–	–	–	–	–	–	–	–	9,1	7,8	7,2	8,0
III	–	–	–	–	-1,7	4,6	0,7	1,1	6,3	-3,1	15,0	14	-12,7	4	–	–	–	–	–	–	–	–	6,0	5,1	3,5	4,9
IV	–	–	–	–	4,4	9,3	5,4	6,4	10,8	2,4	21,0	30	-4,4	9	–	–	–	–	–	–	–	–	5,9	6,9	5,2	6,0
V	–	–	–	–	6,0	9,8	6,6	7,2	11,5	3,9	20,3	19	-2,1	7	–	–	–	–	–	–	–	–	6,9	8,6	6,8	7,4
VI	–	–	–	–	14,3	20,2	15,1	16,2	21,6	10,8	29,9	12	5,4	27	–	–	–	–	–	–	–	–	4,9	5,5	4,9	5,1
VII	–	–	–	–	14,7	19,2	15,7	16,3	21,7	12,8	33,2	5	7,8	29	–	–	–	–	–	–	–	–	7,0	7,5	6,5	7,0
VIII	–	–	–	–	12,5	18,3	13,7	14,8	19,9	10,2	30,0	14	5,9	24	–	–	–	–	–	–	–	–	4,6	6,8	3,9	5,1
IX	–	–	–	–	8,3	13,8	9,4	10,2	15,4	5,5	24,1	9	-0,1	26	–	–	–	–	–	–	–	–	6,2	7,0	5,2	6,1
X	–	–	–	–	4,2	11,3	6,6	7,2	12,4	3,1	17,0	9	-2,8	3	–	–	–	–	–	–	–	–	6,8	4,5	3,7	5,0
XI	–	–	–	–	1,2	4,2	1,6	2,2	5,3	-0,1	14,9	4	-13,6	30	–	–	–	–	–	–	–	–	8,5	6,6	7,1	7,4
XII	–	–	–	–	-4,5	-2,7	-3,8	-3,7	-1,6	-5,3	8,5	14	-12,5	1	–	–	–	–	–	–	–	–	9,0	8,3	7,7	8,3
Rok	–	–	–	–	4,5	8,8	5,4	6,0	10,3	2,5	33,2	5.VII	-15,2	17,1	–	–	–	–	–	–	–	–	7,0	6,8	5,8	6,5

Jaworzyna Krynicka

$\varphi = 49°25'$ $\lambda = 20°54'$

I	–	–	–	–	-3,8	-2,9	-3,6	-3,6	-1,3	-6,5	4,0	23,24	-18,8	16	–	–	–	–	–	–	–	–	7,7	7,5	6,8	7,3
II	–	–	–	–	-2,0	-0,1	-1,6	-1,2	1,0	-3,8	7,0	5	-10,5	28	–	–	–	–	–	–	–	–	8,1	7,6	8,2	8,0
III	–	–	–	–	-1,4	2,4	-0,1	0,2	3,7	-3,7	11,8	21	-13,7	4	–	–	–	–	–	–	–	–	6,0	5,9	5,4	5,8
IV	–	–	–	–	3,9	6,7	4,2	4,8	7,9	1,5	19,5	30	-6,0	15,16	–	–	–	–	–	–	–	–	6,1	6,9	6,5	6,5
V	–	–	–	–	5,0	7,2	5,0	5,6	9,0	2,7	18,5	19	-4,0	7	–	–	–	–	–	–	–	–	7,2	8,4	7,3	7,6
VI	–	–	–	–	13,2	17,4	13,5	14,4	18,8	9,7	27,2	12	5,1	27	–	–	–	–	–	–	–	–	4,8	5,7	5,0	5,2
VII	–	–	–	–	14,1	16,9	14,1	14,8	18,7	11,8	29,4	5	7,4	29	–	–	–	–	–	–	–	–	6,9	7,5	6,9	7,1
VIII	–	–	–	–	11,2	15,4	12,0	12,6	16,9	9,2	26,6	14	5,3	25,31	–	–	–	–	–	–	–	–	5,6	6,7	5,7	6,0
IX	–	–	–	–	7,3	11,0	7,8	8,5	12,3	5,5	21,4	9	-0,7	26	–	–	–	–	–	–	–	–	7,4	8,2	7,3	7,6
X	–	–	–	–	4,5	8,9	4,6	6,2	9,9	2,9	14,0	9,18,20	-2,0	3	–	–	–	–	–	–	–	–	6,1	5,6	4,6	5,4
XI	–	–	–	–	0,5	2,8	0,4	0,8	3,5	-1,2	14,0	4	-13,3	30	–	–	–	–	–	–	–	–	7,9	6,9	7,8	7,5
XII	–	–	–	–	-4,8	-3,5	-4,6	-4,4	-2,2	-7,4	6,0	14	-16,6	1	–	–	–	–	–	–	–	–	9,5	8,8	8,4	8,9
Rok	–	–	–	–	4,0	6,8	4,4	4,9	8,2	1,7	29,4	5.VII	-18,8	16,1	–	–	–	–	–	–	–	–	6,9	7,2	6,6	6,9

Barwinek

$H_s = 420\ m$ $h_w = 16\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU (°D, °mD)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Opad R			Wiatr v		III	IV	●	●	■
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min <0°	Max <0°	Min <-10°	Max >25°	0,1 – 1 mm	>1 – 10 mm	>10 – 100 mm	>100 mm	>10 m/s	>15 m/s					
I	16,5	2,7	2,5	3,4	·	·	3	3,0	3,1	4,3	29,5	3,5	1	5,0	9,5	4,6	·	3,7	46,3	11,6	6	–	19	–	·	20	13	2	2	·	–	–	·	26	–
II	6,5	2,2	0,5	3,0	0,5	1,0	5,5	1,5	4,3	4,3	18	3,4	·	·	9	2,7	1	3,5	67,9	13,0	25	22	5	·	·	23	13	1	2	1	–	–	·	22	–
III	27,5	2,6	5	2,3	·	·	6	1,7	2,1	2,6	19,5	1,6	2,5	1,8	9,5	3,6	2	2,3	30,6	7,6	16	23	7	8	·	14	8	·	·	·	–	–	9	8	–
IV	3,2	2,6	6,5	1,5	1,5	1,7	6,5	1,5	1,7	3,1	6	1,6	1	1,0	17,5	2,5	2	2,4	52,7	16,6	11	13	·	·	·	15	11	1	·	·	–	–	6	13	–
V	3,3	3,2	7,5	2,3	·	·	2	2,0	8,5	1,6	9	1,9	1	3,0	3,1	3,7	1	3,0	114,0	24,1	9	2	·	·	·	17	14	5	·	·	–	–	·	18	–
VI	1,8	1,9	2	1,2	·	·	2	4,2	3,0	4,3	1,2	2,0	0,5	4,0	20,5	2,1	5	2,7	118,7	34,2	25	·	·	·	6	12	9	6	·	·	–	–	5	1	–
VII	1,5	1,6	3	1,7	3	1,2	3,5	1,0	3,1	1,7	19,5	1,7	1	1,0	1,3	1,4	4	1,5	193,6	35,4	14	·	·	·	9	22	17	7	·	·	–	–	3	15	–
VIII	2,2	1,9	3	1,7	·	·	0,5	1,0	2,6,5	3,0	8,5	1,6	0,5	1,0	2,6	2,0	6	2,1	69,7	17,6	10	·	·	·	5	13	11	2	·	·	–	–	1	4	–
IX	1,6	2,2	1,5	1,7	1	1,0	3,5	1,9	2,5,5	2,8	1,5,5	1,9	4,5	1,7	2,0,5	2,1	2	2,2	104,3	32,1	3	3	·	·	·	21	14	2	·	·	–	–	2	13	–
X	12,5	1,6	4,5	1,2	·	·	6	1,8	2,9	3,3	18,5	2,1	5,5	1,1	11	1,5	6	2,1	30,0	8,7	23	12	·	·	·	8	4	·	1	·	–	–	9	4	–
XI	12,5	2,6	4,5	2,4	0,5	1,0	6,5	1,5	3,5,5	2,7	1,8	1,9	2	3,0	7,5	6,5	3	2,6	44,2	12,1	29	17	2	1	·	11	8	2	2	·	–	–	2	17	–
XII	2,1,5	2,7	5	3,0	0,5	1,0	5	2,4	2,6	2,6	2,7	3,2	2	2,0	6	4,5	·	2,9	4,7,0	9,6	13	2,9	1,9	3	·	13	10	·	·	·	–	–	·	2,6	–
Rok	2,3,3	2,3	4,5,5	2,1	7	0,6	5,0	2,0	3,2,4	3,0	2,0,1	2,2	2,1,5	2,0	1,8,1	3,1	3,2	2,6	9,1,7,0	3,5,4	14.VII	–	5,2	–	2,0	1,8,9	1,3,2	2,8	7	1	–	–	3,7	1,6,7	–

Krynica

$H_s = 604\ m$ $H_b = 609,6\ m$ $h_w =$ I–VII 17 m, VIII–XII 18,5 m

I	9	3,3	·	·	0,5	1,0	11	3,5	19,5	2,9	11,5	3,4	7	9,8	11,5	4,9	2,3	3,1	4,4,3	10,9	6	3,0	18	8	·	16	10	1	3	1	8	·	·	21	3,1
II	6	3,5	·	·	0,5	5,0	17	3,3	20,5	4,2	12	4,0	2	4,5	9	3,4	1,7	3,0	36,0	9,4	25	26	6	·	·	14	8	·	1	·	8	·	·	17	2,4
III	14	3,2	3	2,7	·	·	9	2,7	1,8	3,4	10	4,4	5,5	6,6	10,5	4,8	2,8	2,7	3,5,6	9,9	24	21	5	5	·	11	10	·	1	·	·	·	8	8	1,1
IV	2,8,5	2,4	3,5	1,6	2	3,0	4	3,5	9	2,1	3	2,3	0,5	7,0	11,5	2,8	2,8	1,7	6,3,0	15,2	11	15	·	·	·	19	11	1	·	·	3	2	7	11	4
V	3,9	3,0	·	·	·	·	3,5	3,4	5	1,7	0,5	3,0	3	2,5	2,2	3,1	2,0	2,3	8,7,9	19,2	10	3	·	·	·	17	12	4	·	·	3	3	·	15	4
VI	14,5	3,0	2	1,5	·	·	1,4	3,9	1,6	3,1	5	4,0	2	4,0	10,5	4,0	2,6	2,4	4,1,2	10,8	22	·	·	·	6	13	9	1	·	·	2	6	6	1	·
VII	9	2,7	1	1,0	1	1,0	9,5	3,6	13,5	2,3	7	3,0	4,5	4,1	9,5	3,4	3,8	1,8	8,8,2	17,7	15	·	·	·	8	19	13	2	·	·	4	5	3	14	·
VIII	7	2,6	4,5	1,8	3,5	1,9	7,5	4,3	7,5	2,6	6	3,2	4,5	4,3	18,5	3,0	3,4	1,9	7,7,8	20,3	28	·	·	·	6	17	12	2	1	·	4	3	1	3	·
IX	3,5	2,4	5	1,8	·	·	7,5	1,9	6,5	2,6	1,4	3,9	8,5	5,2	1,4	3,4	3,1	2,2	7,9,1	16,1	12	1	·	·	1	17	14	2	·	·	2	2	4	8	·
X	9	3,1	·	·	1,5	3,0	13,5	2,7	1,4,5	2,3	8,5	3,5	2	3,0	4	2,2	4,0	1,6	2,3,7	8,7	22	7	·	·	·	7	4	·	·	·	1,4	·	3	3	·
XI	10,5	4,3	2,5	2,2	·	·	2,1	2,7	12,5	3,2	9,5	4,5	4,5	7,2	7,5	5,0	2,2	2,9	5,7,4	19,4	29	14	4	1	·	11	7	2	3	·	8	·	2	15	1
XII	7,5	2,9	1	3,0	2	3,0	10,5	2,6	2,9	2,8	10,5	2,9	2	4,0	14,5	3,8	1,6	2,5	3,3,0	10,3	5	2,9	1,7	3	·	14	10	1	·	·	3	·	1	2,3	1,6
Rok	1,5,7,5	3,0	2,2,5	1,3	1,1	1,5	1,2,8	3,2	1,6,6,5	2,8	9,7,5	3,5	4,6	5,2	1,4,3	3,6	3,2,3	2,5	6,6,7,2	20,3	28.VIII	1,4,6	5,0	1,7	2,1	1,7,5	1,2,0	1,6	9	1	6,9	2,1	3,5	1,4,1	9,1

Krynica – Góra Parkowa

$H_s = 740\ m$ $h_w = 19\ m$

I	13,5	2,7	3,5	2,6	·	·	7	1,9	4,7	2,5	3	3,3	·	·	1,3	3,9	6	2,6	4,5,5	10,9	6	3,1	2,2	7	·	20	9	1	1	·	12	–	1	18	–
II	7,5	3,1	·	·	0,5	2,0	13,5	3,7	4,4	3,5	7	3,6	2	3,0	6,5	3,2	3	3,3	3,4,3	10,5	25	2,6	7	·	·	15	9	1	4	·	9	–	·	16	–
III	19,5	2,7	6,5	1,8	1	1,0	12,6	2,6	2,8,5	2,8	7	3,6	·	·	1,1	4,3	7	2,7	3,7,0	10,4	24	19	9	4	·	13	8	1	·	·	1	–	8	8	–
IV	3,5	2,5	8,5	1,9	1,5	2,0	1,4	1,9	1,8,5	1,9	0,5	1,0	·	·	1,0	2,4	2	2,1	5,7,5	1,4,3	11	9	·	·	·	19	11	1	·	·	5	–	5	10	–
V	4,4	3,1	8	2,8	1,5	1,3	7	1,9	1,2	1,8	·	·	·	·	1,7,5	2,8	3	2,6	8,3,8	18,6	10	4	·	·	·	18	12	2	·	·	8	–	·	15	–
VI	2,0	2,4	8,5	1,7	·	·	12,5	2,6	3,0	3,3	4,5	4,1	1	3,0	1,3,5	2,4	·	2,7	5,4,7	7,5	22	·	·	·	6	13	7	·	·	·	3	–	5	5	–
VII	1,8,5	2,6	3	3,3	1,5	1,3	9	2,9	3,8	2,6	8,5	3,2	3	2,5	8,5	3,1	3	2,7	9,6,3	2,0,6	15	·	·	·	8	19	13	3	·	·	5	–	1	13	–
VIII	3,0,5	2,8	1	2,0	·	·	8	2,9	2,4,5	3,7	6,5	3,1	·	·	2,0,5	3,1	2	3,1	6,8,3	1,9,0	28	·	·	·	6	16	11	2	1	·	1	–	1	2	–
IX	1,6	3,2	3	2,0	·	·	5	2,8	2,6,5	2,8	1,9,5	3,9	4,5	4,4	1,2,5	4,0	3	3,2	7,7,4	1,6,4	12	1	·	·	·	18	14	1	2	·	6	–	4	9	–
X	13	2,3	3,5	1,4	1	1,5	1,5	2,7	4,4,5	2,6	3,5	2,7	·	·	7,5	2,9	5	2,4	2,5,3	9,6	22	4	·	·	·	9	4	·	·	·	1,0	–	7	3	–
XI	1,4,5	4,9	7	3,8	0,5	5,0	1,2,5	3,9	3,8,6	3,2	2,5	3,6	2,5	4,0	7	8,1	5	3,9	5,5,3	2,1,0	29	1,6	7	1	·	10	7	2	2	·	1,2	–	2	16	–
XII	1,2,5	4,7	1,5	4,0	·	·	8	4,6	4,7,5	3,2	5,5	3,6	2	1,5	1,3	4,9	3	3,5	3,4,5	1,2,1	5	2,9	2,3	5	·	14	10	1	2	·	8	–	·	21	–
Rok	2,4,4,5	3,1	5,4	2,3	7,5	1,4	1,2,4	2,9	3,0,9,6	2,8	6,8	3,0	1,5	1,5	1,4,0,5	3,8	4,2	2,9	6,5,0,9	2,1,0	29.XII	1,3,9	6,8	1,7	2,0	1,8,4	1,1,5	1,5	1,2	·	8,0	–	3,4	1,3,6	–

Jaworzyna Krynicka

$H_s = 995\ m$ $h_w = 15\ m$

I	11	2,8	4	3,0	3	4,0	·	·	11,5	3,1	2,3	3,3	3,4,5	2,7	6	3,5	·	3,0	5,0,9	1,5,5	6	3,1	1,4	4	·	16	11	1	·	·	–	·	1	1,5	3,1
II	1,1	2,5	2	2,0	1	2,0	2	4,0	1,6	2,5	2,7	2,0	1,8	2,7	7	2,4	·	2,4	3,2,2	5,8	14	2,8	8	1	·	14	8	·	·	·	–	·	1	1,5	2,8
III	1,6,5	3,0	8	2,4	7,5	1,7	6	1,7	1,0	2,2	1,6,5	2,9	1,9,5	4,3	9	2,2	·	2,8	3,3,8	9,0	24	2,1	1,0	7	·	1,0	9	·	·	·	–	·	2	1,1	2,3
IV	2,9	2,4	1,3,5	2,0	2	2,5	1,0,5	1,2	1,1	1,7	8,5	1,8	6,5	2,0	9	2,3	·	2,0	6,0,3	1,1,5	11	1,1	4	·	·	1,7	1,2	2	·	·	–	2	3	1,3	6
V	3,9,5	3,0	1,2	2,7	6,5	2,5	3,5	2,1	0,5	1,0	9	2,2	1,4	3,2	8	2,5	·	2,8	7,6,3	1,6,4	10	1,3	3	·	·	1,6	1,4	2	·	·	–	2	·	1,6	6
VI	1,9	3,3	9,5	2,2	7	2,0	3	2,3	1,1	2,0	1,9	2,4	1,3	3,5	8,5	2,6	·	2,7	6,2,4	2,0,6	8	·	·	·	1	1,4	1,2	1	·	·	–	3	2	4	·
VII	1,6	2,4	1,0	1,6	3	1,7	2,5	2,6	5,5	1,9	1,8,5	1,5	2,7	2,6	1,0,5	2,5	·	2,2	1,3,4,0	1,7,4	1,6	·	·	·	2	2,0	1,6	7	·	·	–	6	·	1,4	·
VIII	2,4	3,0	3	1,9	2	1,5	4,5	2,4	6,5	3,8	1,5,5	1,8	1,1,5	2,5	2,0	2,6	·	2,5	9,1,6	2,2,6	2,9	·	·	·	1	1,6	1,2	2	·	·	–	2	·	4	·
IX	1,2,5	2,6	8,5	1,8	0,5	5,0	·	·	8	1,7	2,5	4,4	2,4,5	4,3	6	4,1	5	2,8	1,0,9,5	1,8,3	1,2	3	·	·	·	1,7	1,5	4	1	·	–	1	2	1,9	·
X	5,5	2,0	·	·	·	·	1	2,0	1,7	2,4	3,5,5	2,7	1,3	3,2	6	2,2	1,5	2,2	3,2,2	1,0,4	2,2	6	·	·	·	6	5	1	·	·	–	·	6	8	·
XI	5	3,0	1,1	3,3	1,5	3,0	1,0	3,4	1,0,5	3,4	2,5,5	3,2	1,5,5	2,7	6	2,8	5	2,6	5,8,4	1,6,4	2,9	1,7	9	2	·	1,0	9	1	1	·	–	·	4	1,9	1,5
XII	1,1	6,0	2,5	3,4	0,5	1,0	·	·	1,3,5	3,6	3,8	3,8	1,2	3,9	7,5	3,6	3,7	4,0,3	1,2,4	5	2,9	2,3	8	·	·	1,1	1,1	1	2	1	–	·	·	2,3	3,1
Rok	2,8,0	3,4	9,0	2,5	3,4,5	2,2	4,3	1,8	1,2,1	2,4	2,6,1	2,5	2,0,9	3,6	1,0,3,6	3,4	3,3	2,8	7,8,4,8	2,2,6	2,9.VIII	1,5,9	7,1	2,2	4	1,6,7	1,3,4	2,2	7	1	–	1,6	2,1	1,6,1	1,4,0

Żegiestów – Zdrój

$\varphi = 49°22'$ $\lambda = 20°49'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnie				— Max	— Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-4,5	-4,2	-3,7	-3,3	-0,1	-6,4	5,3	26	-18,1	23	–	–	–	–	–	–	–	–	8,9	7,8	7,9	8,2
II	–	–	–	–	-4,0	3,5	0,8	1,0	4,9	-2,6	9,7	17	-9,8	1	–	–	–	–	–	–	–	–	8,8	8,3	8,0	8,4
III	–	–	–	–	-1,8	7,0	4,2	4,9	8,7	-3,8	17,3	14,31	-17,6	4	–	–	–	–	–	–	–	–	7,1	4,9	4,9	5,6
IV	–	–	–	–	3,0	11,6	5,7	6,5	13,3	1,0	24,5	30	-2,9	2	–	–	–	–	–	–	–	–	7,1	7,4	6,4	7,0
V	–	–	–	–	6,2	11,4	7,7	8,2	13,5	4,1	22,3	17	-1,7	30	86	64	82	77	1,5	6,1	2,1	3,2	6,8	8,9	7,8	7,9
VI	–	–	–	–	13,1	22,6	15,4	16,6	24,2	9,6	32,6	12	3,5	7	89	50	78	72	4,9	14,5	4,2	6,9	4,9	5,3	5,0	5,1
VII	–	–	–	–	15,0	22,0	16,0	17,2	24,0	12,2	36,0	5	7,7	4	92	63	87	81	4,5	13,3	2,7	4,8	7,5	7,2	7,1	7,3
VIII	–	–	–	–	11,8	20,7	14,0	15,1	22,3	9,7	32,1	14	4,1	24	94	58	88	80	0,9	11,2	2,0	4,7	6,8	6,7	6,2	6,6
IX	–	–	–	–	8,2	16,2	9,9	11,0	17,6	6,1	27,8	9	-2,0	26	94	63	93	83	0,7	7,4	0,9	3,0	8,6	7,2	6,9	7,6
X	–	–	–	–	4,0	13,8	5,8	7,4	14,7	1,9	19,8	12	-4,0	3	96	60	90	82	0,5	7,0	1,0	2,8	9,3	4,4	6,5	6,7
XI	–	–	–	–	2,5	6,6	3,1	3,8	7,7	0,4	18,6	4	-11,8	30	91	71	87	83	0,7	3,4	1,1	1,7	8,3	6,6	7,8	7,6
XII	–	–	–	–	-2,9	-0,3	-2,1	-1,8	0,5	-5,3	10,3	13	-14,6	11	87	81	86	84	0,6	1,2	0,8	0,9	9,2	8,6	8,4	8,7
Rok	–	–	–	–	4,5	11,2	6,2	7,0	12,6	2,2	36,0	5.VII	-18,1	23.I	–	–	–	–	–	–	–	–	7,8	6,9	6,9	7,2

Bukowina Tatrzańska

$\varphi = 49°21'$ $\lambda = 20°07'$

I	–	–	–	–	-4,2	-1,8	-3,3	-3,2	-0,3	-6,7	7,0	2	-20,8	17	–	–	–	–	–	–	–	–	7,5	6,8	5,8	6,7
II	–	–	–	–	-0,8	1,6	0,0	0,2	3,6	-3,7	10,5	5	-13,8	28	–	–	–	–	–	–	–	–	7,3	6,6	6,2	6,7
III	–	–	–	–	-0,9	4,0	1,3	1,4	5,6	-3,6	12,5	21	-13,8	4	–	–	–	–	–	–	–	–	5,9	5,2	4,3	5,1
IV	–	–	–	–	4,0	8,2	4,8	5,4	9,2	0,8	20,3	30	-6,0	14	–	–	–	–	–	–	–	–	5,8	6,4	6,5	6,2
V	–	–	–	–	5,6	8,3	6,1	6,5	10,0	2,6	18,3	19	-3,0	7	–	–	–	–	–	–	–	–	7,3	8,3	7,7	7,8
VI	–	–	–	–	14,7	18,7	14,7	15,7	20,1	9,7	27,0	11	4,6	27	–	–	–	–	–	–	–	–	4,6	5,9	5,5	5,3
VII	–	–	–	–	15,0	18,0	15,2	15,8	19,8	11,4	30,5	5	8,6	29	–	–	–	–	–	–	–	–	6,7	7,3	7,1	7,0
VIII	–	–	–	–	12,6	16,3	13,1	13,8	17,7	9,0	26,4	14	4,5	31	–	–	–	–	–	–	–	–	5,0	6,7	6,0	5,9
IX	–	–	–	–	8,2	12,1	9,0	9,6	13,5	5,4	22,4	9	-0,3	26,27	–	–	–	–	–	–	–	–	5,8	6,6	6,1	6,2
X	–	–	–	–	4,9	10,1	6,7	7,1	11,0	2,4	20,0	19	-2,3	3	–	–	–	–	–	–	–	–	5,0	4,5	4,1	4,5
XI	–	–	–	–	1,1	3,6	1,1	1,7	5,0	-1,5	14,8	5	-16,5	30	–	–	–	–	–	–	–	–	6,7	5,7	6,6	6,3
XII	–	–	–	–	-3,6	-1,8	-2,5	-2,6	0,4	-7,0	12,0	13	-16,2	1	–	–	–	–	–	–	–	–	6,8	6,5	6,7	6,7
Rok	–	–	–	–	4,7	8,1	5,5	6,0	9,6	1,6	30,5	5.VII	-20,8	17.I	–	–	–	–	–	–	–	–	6,2	6,4	6,0	6,2

Muszyna

$\varphi = 49°21'$ $\lambda = 20°53'$

I	968,1	977,4	952,6	1024,4	-4,5	-4,7	-4,1	-3,6	-0,3	-6,7	5,9	2	-19,1	23	91	81	90	87	0,5	1,1	0,5	0,7	9,1	8,0	8,1	8,4
II	959,6	975,9	937,5	1014,5	-0,8	3,2	1,1	1,2	4,5	-2,2	10,0	19	-10,9	1	94	74	84	84	0,4	2,2	1,2	1,3	8,5	8,1	7,5	8,0
III	964,7	978,2	948,8	1019,7	-1,9	6,5	1,5	1,9	8,5	-3,4	16,8	14	-17,3	4	86	56	78	73	1,0	5,2	1,8	2,7	7,2	6,0	4,4	5,9
IV	963,8	975,0	940,8	1017,8	3,0	11,2	6,1	6,6	13,0	1,1	23,5	30	-3,0	2	91	57	81	76	0,7	6,7	1,8	3,1	6,9	7,3	5,7	6,6
V	961,5	970,3	950,5	1015,1	6,4	11,7	7,9	8,6	13,2	4,0	21,5	17,19	-1,8	30	88	64	86	79	1,2	6,2	1,7	3,0	7,5	9,0	7,0	7,8
VI	964,9	976,8	953,9	1017,0	13,7	22,0	15,4	16,6	23,4	9,1	31,7	12	2,6	7	85	49	79	71	2,7	14,1	4,0	6,9	5,1	5,8	5,4	5,4
VII	961,0	971,0	950,8	1012,7	15,2	21,3	16,4	17,3	23,6	12,2	35,4	5	6,9	4	90	64	86	80	2,0	10,6	2,8	5,1	7,5	7,9	6,3	7,2
VIII	962,9	971,8	952,2	1013,2	14,8	20,1	14,2	15,1	21,5	9,5	31,5	14	3,2	24	94	58	88	80	0,9	10,8	2,1	4,6	6,4	6,9	4,5	5,9
IX	962,1	971,1	949,8	1015,1	8,0	15,7	9,7	10,8	17,0	6,1	26,0	9	-2,3	26	94	62	92	83	0,7	7,2	1,1	3,0	8,1	7,1	5,8	7,0
X	968,1	976,3	951,8	1022,2	3,6	12,8	5,4	6,8	14,2	1,8	19,0	9	-3,7	3	96	64	93	84	0,4	5,7	0,8	2,3	9,4	4,5	3,6	5,8
XI	966,8	984,1	952,5	1021,7	2,4	6,1	3,0	3,6	7,5	0,6	16,9	4	-10,8	30	91	76	88	85	0,7	2,8	1,1	1,5	8,3	7,1	7,8	7,7
XII	962,3	984,6	930,2	1017,8	-2,8	-0,4	-2,1	-1,8	0,8	-5,1	11,5	13	-15,9	11	88	79	88	85	0,7	1,3	0,7	0,9	8,7	8,0	7,4	8,0
Rok	963,5	984,1	930,2	1017,7	4,5	10,7	6,2	6,8	12,2	2,2	35,4	5.VII	-19,1	23.I	91	65	86	81	1,0	6,2	1,6	2,9	7,7	7,1	6,1	7,0

Witów

$\varphi = 49°20'$ $\lambda = 19°50'$ 1957

I	–	–	–	–	-5,7	-0,6	-4,4	-3,8	1,2	-8,4	9,3	2	-26,2	17	–	–	–	–	–	–	–	–	6,8	6,3	6,7	6,8
II	–	–	–	–	-1,6	2,9	-0,2	0,2	4,5	-4,0	10,4	5,6	-16,5	28	–	–	–	–	–	–	–	–	7,2	6,5	6,9	6,9
III	–	–	–	–	-3,4	4,8	-0,4	0,2	6,2	-5,4	13,9	21	-18,2	4	–	–	–	–	–	–	–	–	5,9	5,6	5,4	5,6
IV	–	–	–	–	2,0	8,2	3,2	4,2	9,6	-0,4	20,7	30	-8,5	9	–	–	–	–	–	–	–	–	5,8	7,2	6,5	6,6
V	–	–	–	–	5,5	8,9	5,3	6,2	10,4	2,0	19,6	19	-2,5	7	–	–	–	–	–	–	–	–	7,3	8,8	7,6	7,8
VI	–	–	–	–	12,0	19,0	14,4	15,0	21,1	8,0	26,7	30	1,5	7	–	–	–	–	–	–	–	–	4,8	6,2	5,6	5,5
VII	–	–	–	–	13,6	18,5	15,1	15,6	20,4	11,1	31,5	5	6,3	29	–	–	–	–	–	–	–	–	6,6	7,6	7,4	7,2
VIII	–	–	–	–	10,0	16,9	12,4	13,5	18,7	7,8	26,7	14	1,9	24	–	–	–	–	–	–	–	–	5,6	6,9	7,0	6,5
IX	–	–	–	–	6,6	12,6	8,4	9,0	14,2	4,8	24,4	9	-2,4	26	–	–	–	–	–	–	–	–	6,1	6,8	6,6	6,5
X	–	–	–	–	2,5	11,2	4,8	5,8	12,1	0,4	20,8	19	-4,5	3	–	–	–	–	–	–	–	–	5,5	4,9	4,4	4,9
XI	–	–	–	–	0,8	4,8	0,9	1,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6,7	6,0	6,6	6,4
XII	–	–	–	–	-4,9	-0,5	-3,4	-3,0	1,4	-7,4	12,5	13	-17,0	3	–	–	–	–	–	–	–	–	6,6	6,6	6,6	6,6
Rok	–	–	–	–	3,1	8,9	4,7	5,4	–	–	34,5	5.VII	-26,2	17.I	–	–	–	–	–	–	–	–	6,2	6,6	6,4	6,4

Żegiestów - Zdrój

$H_s = 440\ m$ $h_w = 16\ m$ 1957

MIESIĄC	ROZKŁAD WIATRU (%D, %D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0	Min<-10	Max>25°	Opad R 0.1 ≤ R < 1.0	1.0 ≤ R < 10	10 ≤ R < 100	Wiatr v 10 ≤ v < 15	v ≥ 15	≡	≋	◔	●	≋
I	-	-	0,5	3,0	8,5	1,9	7,5	2,4	18,5	2,0	9,5	2,5	16,5	2,9	2	4,0	30	1,6	40,0	12,5	5	30	15	·	·	13	8	·	·	·	·	·	2	17	31
II	3	2,3	2,5	1,8	2,5	1,6	5	1,8	1,8	2,8	12,5	2,7	12	3,2	2,5	2,6	26	1,8	28,8	10,1	25	22	4	·	·	10	7	1	·	·	1	·	1	20	18
III	·	·	6	1,4	11,5	1,7	6,5	1,7	1,6	2,3	4,5	1,9	21,5	2,5	1	4,0	27	1,5	20,5	5,0	24	21	4	6	·	10	6	·	·	·	3	·	8	12	10
IV	1	1,0	6	1,5	1,0	1,4	3	2,3	7	2,4	3,5	2,3	31,5	2,1	2	1,5	26	1,4	34,0	10,1	11	15	·	·	·	15	8	1	·	·	5	·	3	14	·
V	5	2,0	4,5	1,3	10,5	1,3	1	2,0	3	1,5	4,5	1,4	3,7	2,1	1,5	1,0	26	1,3	64,0	16,8	10	1	·	·	·	15	11	2	·	·	2	3	2	18	2
VI	4,5	1,6	3	1,7	1,3	1,7	5	1,4	1,2	2,4	12,5	2,6	13,5	2,5	0,5	2,0	26	1,5	39,7	8,1	4	·	·	·	1,4	12	11	·	·	·	3	4	5	5	·
VII	6	1,7	4	1,8	1,0	1,2	·	·	9	1,8	1,1	2,5	2,1	2,4	·	·	32	1,3	124,2	32,3	15	·	·	·	1,1	19	11	5	·	·	2	5	3	15	·
VIII	4	1,2	2	1,0	9	1,6	1	2,0	1,1	1,8	1,2	2,7	1,9	1,8	3	1,3	32	1,2	74,9	26,3	28	·	·	·	1,0	17	11	2	·	·	9	1	2	10	·
IX	2	1,0	·	·	4,5	1,7	1,5	1,7	6,5	1,8	1,3,5	2,0	2,3	2,4	3	2,2	36	1,2	59,9	12,2	3	·	·	·	2	16	11	1	·	·	8	1	·	16	·
X	5	1,8	1	1,0	5	2,2	3,5	1,7	8	1,8	8,5	2,0	1,3,5	1,8	0,5	2,0	1,8	0,9	21,6	10,6	22	7	·	·	·	4	3	1	·	·	15	·	1	11	·
XI	4	2,8	2,5	2,0	3,5	2,9	3,5	2,3	1,4	2,3	4,5	2,0	1,7	3,1	6	1,7	35	1,5	47,6	25,1	29	13	1	1	·	12	5	1	·	·	5	·	2	17	1
XII	1	1,0	2	1,0	3	1,3	6,5	1,6	2,0,5	2,2	5	2,0	2,4,5	2,7	3,5	2,9	27	1,7	26,6	10,1	5	30	15	3	·	11	7	1	·	·	1	·	·	22	13
Rok	3,5,5	1,1	33	1,7	9,1	1,7	44	1,7	1,4,3,5	2,1	1,0,1,5	2,2	2,5,0	2,5	2,6,5	2,1	3,7,1	1,4	5,8,1,8	3,2,3	1,5.VII	1,3,9	3,9	1,0	3,7	1,5,4	1,0,2	1,5	·	·	5,4	1,4	2,9	1,7,7	7,5

Bukowina Tatrzańska

$H_s = 880\ m$ $h_w = 14\ m$

I	·	·	1	3,0	2	4,5	3,5	2,0	4	2,0	1,7	4,8	12,5	6,9	2	4,5	5,1	2,9	30,2	9,0	5	3,1	1,5	5	·	1,4	8	·	3	·	4	·	3	13	31
II	·	·	1	2,0	0,5	6,0	3	8,5	3	5,5	1,5	5,4	1,6	5,2	3,5	4,3	4,2	2,7	28,2	5,8	25	2,6	5	1	·	1,3	1,0	·	4	1	3	·	3	12	2,2
III	1	5,0	5	4,8	2	3,5	3,5	3,1	1,5	2,0	2,5	5,1	1,4,5	6,3	6,5	3,3	3,4	3,1	27,9	9,0	16	2,1	5	6	·	1,0	6	·	5	·	1	1	6	7	1,5
IV	1,5	2,7	5	2,8	2,5	2,8	9,5	2,4	7	2,7	1,4	2,9	7	3,6	7,5	4,3	3,6	1,8	69,1	1,4,8	2,3	1,2	1	·	·	1,8	1,3	1	·	·	·	2	6	1,5	7
V	1	2,0	4,5	3,1	5,5	4,4	9,5	2,8	4	2,4	1,8	2,8	1,3,5	3,3	6	4,6	3,1	2,1	7,7,7	1,3,7	1,4	1,0	·	·	·	2,1	1,7	2	·	·	2	2	2	1,8	6
VI	1	5,0	3,5	3,0	0,5	5,0	5	5,1	1,0	3,3	2,5	3,5	1,4,5	4,9	8,5	4,5	2,5	2,9	5,4,8	2,1,2	1,2	·	·	·	4	1,2	9	2	1	·	·	5	5	5	·
VII	·	·	1	7,0	2	4,0	1,5	2,7	3,5	1,7	3,0,5	3,3	1,1	3,9	5,5	3,2	3,8	2,0	1,8,0,7	3,9,8	1,5	·	·	·	6	2,1	1,7	6	·	·	·	7	2	1,4	·
VIII	0,5	3,0	2,5	2,2	·	·	3	2,0	7	1,8	3,1,5	3,6	1,5	5,0	5,5	5,0	2,8	2,6	7,6,6	1,9,6	2,9	2	·	·	·	1,5	1,2	2	1	·	2	2	2	7	·
IX	0,5	5,0	1	4,5	1,5	3,0	3	2,5	1,4	2,5	3,3,5	5,1	1,5,5	7,5	3	4,2	1,8	3,9	8,7,2	2,4,6	3	2	·	·	·	1,8	9	2	5	1	2	·	4	1,0	·
X	0,5	4,0	2	2,5	1	2,0	2,5	3,4	9	1,6	2,3,5	3,1	7,5	4,2	4	3,5	4,3	1,6	3,6,0	1,6,8	2,2	8	·	·	·	6	4	1	·	·	2	·	7	7	·
XI	1,5	3,3	4,5	3,9	4	4,2	1,0	3,5	1,1	1,7	1,5	4,6	1,2	7,1	4	7,9	2,8	3,1	2,0,7	7,0	1,1	1,7	7	1	·	1,1	5	·	3	1	4	·	6	1,1	5
XII	·	·	1	5,0	2,5	3,0	5	3,7	1,3	2,5	2,2	4,8	1,8,5	6,8	1	5,5	3,0	3,2	1,0,6	2,6	5	3,0	1,6	9	·	1,2	4	·	5	2	4	·	6	1,3	1,4
Rok	7,5	2,5	3,2	3,6	2,4	3,5	5,9	3,5	8,7	2,5	2,7,0	4,1	1,5,4,5	5,4	5,7	4,6	4,0,4	2,7	6,3,9,7	3,3,8	1,5.VII	1,6,7	4,9	2,2	1,2	1,7,1	1,1,4	1,6	2,7	5	2,4	1,9	5,5	1,5,2	1,0,0

Muszyna

$H_s = 445\ m$ $H_b = 447,5\ m$ $h_w = 24\ m$

I	4	1,7	1,1	2,5	·	·	2	1,0	4,5	1,9	1,8,5	2,3	4,5	2,3	0,5	3,0	5,1	1,0	3,3,7	1,0,4	5	3,0	1,3	9	·	1,5	9	1	·	·	·	·	·	1,6	3,1
II	6,5	1,4	4	1,2	1	1,0	1	1,0	7	2,4	2,1,5	3,4	4	2,9	1	1,5	3,8	1,4	2,8,0	6,5	2,5	2,2	3	1	·	1,5	8	·	·	·	1	·	·	1,9	2,0
III	4	1,9	1,7	2,3	3	2,0	2	1,5	3,5	1,3	2,0,5	2,8	6	2,2	·	·	3,7	1,4	1,9,5	4,9	1,6	2,0	4	6	·	1,1	6	·	1	·	2	·	6	1,1	1,2
IV	2	1,5	2,6	2,2	2,5	2,2	3,5	1,9	4,5	1,9	3,5	2,0	9,5	1,2	2,5	1,0	3,7	1,1	2,7,5	-	-	1,2	·	·	·	1,4	7	1	·	·	3	3	4	1,5	·
V	7,6	1,7	2,7,5	2,3	3	1,8	1	1,5	3	1,5	5,5	1,5	1,4,5	1,6	1	2,0	3,0	1,3	7,2,5	2,3,7	1,0	2	·	·	·	1,3	1,0	2	·	·	3	4	·	1,6	1
VI	9,5	2,1	1,0,5	2,0	2	2,0	0,5	2,0	9	1,5	1,8,5	4,0	5,5	1,7	1,5	1,0	3,3	1,5	4,1,7	8,3	4	·	·	·	1,0	1,2	1,0	·	1	·	2	5	5	5	·
VII	4	1,8	1,0,5	2,8	·	·	2,6	1,4	1	2,5	1,9,5	2,3	5	1,4	0,5	2,0	5,0	1,0	1,1,0,8	2,0,9	1,6	·	·	·	9	1,8	1,2	4	·	·	1	6	3	1,6	·
VIII	1,2,5	1,5	9,5	2,7	4	2,4	·	·	1	2,0	1,8	3,1	1,3	1,4	1	2,0	3,4	1,4	6,0,4	1,2,8	2,3	·	·	·	6	1,3	8	2	·	·	7	2	1	6	·
IX	5	2,2	1,1	2,4	3	1,0	1	2,0	1	2,0	1,9,5	3,3	4,5	3,4	1	1,0	4,4	1,4	7,5,6	1,4,8	3	1	·	·	1	1,6	1,2	2	·	·	6	2	·	1,0	·
X	1,0	1,5	9	2,0	4	1,2	1	1,0	3	2,0	1,1	2,7	3	2,3	1	1,0	5,1	0,9	2,6,0	1,1,4	2,2	7	·	·	·	4	3	1	·	·	1,3	·	1	6	·
XI	3,5	4,3	1,7	2,8	2,5	1,2	2,5	1,0	4,5	1,2	2,2,5	2,7	1,5	2,0	1	1,0	2,9	1,7	4,1,4	1,7,2	2,9	1,1	1	1	·	1,1	7	1	·	·	4	·	2	1,2	1
XII	3	1,3	1,8	2,6	4	2,0	0,5	1,0	6,5	1,8	1,9	3,3	5	2,2	3	1,3	3,4	1,6	2,0,1	8,2	5	2,8	1,3	1	·	1,1	5	·	·	·	·	·	·	2,0	1,2
Rok	7,1,5	1,9	1,7,0	2,3	2,9	1,4	1,7,5	1,3	1,8,5	1,8	2,0,3,5	2,8	7,3	2,0	1,4	1,4	4,6,8	1,3	5,4,9,6	2,3,7	1,0.V	1,3,3	3,4	1,8	2,6	1,5,3	9,6	1,4	2	·	4,4	2,2	2,2	1,6,0	7,7

Witów

$H_s = 835\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3,5,4	8,8	6	3,0	1,1	1,0	·	1,5	8	·	-	-	2	·	3	1,0	3,1
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5,9,2	1,5,9	2,1	2,4	4	4	·	1,3	1,0	2	-	-	·	·	2	1,3	1,5
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	5,0,8	1,4,4	1,6	2,2	5	9	·	1,0	9	1	-	-	·	1	6	8	1,5
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1,0,6,1	1,8,0	1,1	1,7	1	·	·	1,9	1,4	5	-	-	2	2	4	1,3	6
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	8,3,8	1,4,6	8	6	·	·	·	2,0	1,4	4	-	-	3	3	·	1,7	5
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4,8,0	1,1,0	9	·	·	·	5	1,1	1,0	1	-	-	1	8	4	2	·
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2,0,9,4	4,0,3	1,4	·	·	·	7	2,3	1,6	8	-	-	4	7	1	1,5	·
VIII	-	-	·	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1,0,8,5	5,4,3	2,9	·	·	·	4	1,4	1,0	3	-	-	·	2	·	9	·
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9,1,6	2,2,8	4	3	·	·	·	1,6	1,2	3	-	-	·	·	2	1,0	·
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	4,5,4	1,9,4	2,2	1,4	·	·	·	5	4	2	-	-	2	·	6	6	·
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3,5,0	1,3,1	2,9	-	-	-	·	8	6	1	-	-	1	·	4	1,4	2
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	2,7,5	6,8	9	2,8	1,4	1,2	·	1,2	8	·	-	-	3	·	4	1,3	1,2
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	9,0,0,7	4,0,3	1,4.VII	-	-	-	1,6	1,6,6	1,2,1	3,0	-	-	1,8	2,3	3,6	1,3,0	8,6

Poronin

$\varphi = 49°20'$ $\lambda = 20°02'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies.							I	II	III	Dies.	I	II	III	Dies.	I	II	III	Dies.
I	–	–	–	–	-6.7	-0.5	-5.8	-4.7	0.4	-9.9	9.5	2	-26.9	17	–	–	–	–	–	–	–	–	7.3	6.6	6.5	6.8
II	–	–	–	–	-2.6	2.9	-0.8	-0.3	4.4	-6.0	10.6	18,19	-21.3	23	–	–	–	–	–	–	–	–	6.7	6.3	6.2	6.4
III	–	–	–	–	-4.7	3.7	-2.1	-0.8	6.8	-7.6	14.2	21	-22.7	4	–	–	–	–	–	–	–	–	5.6	5.4	4.7	5.2
IV	–	–	–	–	2.3	8.9	2.7	4.2	9.9	-1.4	21.1	30	-13.4	9	–	–	–	–	–	–	–	–	5.9	7.0	6.5	6.5
V	–	–	–	–	5.6	9.3	5.0	6.2	10.7	1.2	19.6	16,19	-4.4	30	–	–	–	–	–	–	–	–	7.8	8.4	7.1	7.8
VI	–	–	–	–	11.3	19.9	12.6	14.1	21.1	5.9	28.4	12	-4.0	7	–	–	–	–	–	–	–	–	4.0	4.9	4.7	4.5
VII	–	–	–	–	13.0	19.5	13.8	15.0	24.0	8.3	32.1	5,8	3.0	29	–	–	–	–	–	–	–	–	6.8	6.9	6.9	6.9
VIII	–	–	–	–	9.2	17.4	11.7	12.5	18.9	6.1	27.1	14	-1.5	31	–	–	–	–	–	–	–	–	4.2	6.4	5.2	5.3
IX	–	–	–	–	5.1	12.9	7.2	8.1	14.2	3.1	24.1	9	-4.9	26	–	–	–	–	–	–	–	–	5.8	6.6	6.3	6.2
X	–	–	–	–	4.3	11.8	2.9	4.7	12.7	-1.8	21.6	19	-7.4	3	–	–	–	–	–	–	–	–	4.7	3.8	4.2	4.2
XI	–	–	–	–	-0.8	5.0	0.0	1.0	6.2	-3.2	15.6	5	-14.9	30	–	–	–	–	–	–	–	–	6.3	5.6	6.5	6.1
XII	–	–	–	–	-6.0	-0.3	-3.9	-3.5	1.5	-8.8	13.0	13	-21.5	3	–	–	–	–	–	–	–	–	6.5	6.1	5.9	6.2
Rok	–	–	–	–	2.2	9.4	3.6	4.7	10.6	-1.2	32.1	5,8 VII	-26.9	17.1	–	–	–	–	–	–	–	–	6.0	6.2	5.9	6.0

Komarnicza

$\varphi = 49°20'$ $\lambda = 22°04'$

I	–	–	–	–	-3.7	-1.3	-3.7	-3.1	-0.2	-6.5	4.5	3	-16.7	19	–	–	–	–	–	–	–	–	9.7	9.0	8.3	9.0
II	–	–	–	–	0.4	2.2	0.9	1.1	3.7	-1.1	11.2	19	-7.8	28	–	–	–	–	–	–	–	–	9.4	8.9	9.7	9.3
III	–	–	–	–	-2.3	3.7	0.1	0.9	6.8	-4.8	17.0	30,31	-25.1	4	–	–	–	–	–	–	–	–	6.0	5.6	3.8	5.1
IV	–	–	–	–	4.0	12.0	6.2	7.1	13.3	0.6	24.2	30	-5.8	9	–	–	–	–	–	–	–	–	6.9	6.8	6.1	6.6
V	–	–	–	–	7.4	11.5	7.7	8.6	13.1	3.4	21.5	14,17,18	-2.8	30	–	–	–	–	–	–	–	–	7.4	7.5	6.5	7.1
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.2	6.5	7.2
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.5	5.3	5.9
IX	–	–	–	–	9.6	14.9	10.1	11.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.8	6.4	7.3
X	–	–	–	–	4.8	12.4	6.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.0	4.6	3.2	4.3
XI	–	–	–	–	2.4	5.7	2.2	3.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.1	7.0	7.3
XII	–	–	–	–	-3.2	-4.2	-2.0	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.1	8.6	8.5
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Baligród

$\varphi = 49°20'$ $\lambda = 22°17'$

I	–	–	–	–	-2.3	-0.3	-1.9	-1.6	–	-4.6	–	–	-13.3	22	–	–	–	–	–	–	–	–	8.5	7.2	6.8	7.5
II	–	–	–	–	1.7	3.4	2.2	2.4	5.1	0.1	13.1	19	-7.4	28	–	–	–	–	–	–	–	–	8.0	7.8	7.6	7.8
III	–	–	–	–	-0.8	5.8	0.4	1.4	7.2	-3.8	17.6	30	-20.4	4	–	–	–	–	–	–	–	–	5.6	5.6	4.9	5.4
IV	–	–	–	–	4.7	11.8	6.0	7.1	13.2	1.9	23.6	30	-3.9	4	–	–	–	–	–	–	–	–	5.6	6.4	5.0	5.7
V	–	–	–	–	7.6	11.2	7.1	8.2	12.7	3.8	21.1	17	-0.3	7	–	–	–	–	–	–	–	–	7.1	8.4	6.6	7.4
VI	–	–	–	–	14.9	21.4	15.8	16.9	22.3	9.9	29.7	30	3.1	27	–	–	–	–	–	–	–	–	4.7	4.6	4.1	4.5
VII	–	–	–	–	15.6	21.6	16.0	17.3	22.4	12.6	34.0	8	6.0	4	–	–	–	–	–	–	–	–	6.6	6.5	5.7	6.3
VIII	–	–	–	–	12.8	19.7	13.5	14.9	20.8	10.2	31.4	14	4.6	31	–	–	–	–	–	–	–	–	6.7	5.8	3.8	5.4
IX	–	–	–	–	9.9	15.0	10.4	11.4	15.8	7.1	24.3	9	-0.9	26	–	–	–	–	–	–	–	–	6.3	7.2	6.1	6.5
X	–	–	–	–	6.0	13.0	7.1	8.3	13.8	3.0	19.1	20	-5.3	3	–	–	–	–	–	–	–	–	4.7	4.2	3.0	4.0
XI	–	–	–	–	2.5	6.4	2.7	3.6	7.3	0.7	16.6	2	-11.4	30	–	–	–	–	–	–	–	–	7.0	6.0	6.4	6.5
XII	–	–	–	–	-2.2	0.0	-0.5	-0.8	–	-3.7	–	–	-14.1	11	–	–	–	–	–	–	–	–	7.5	7.1	7.0	7.2
Rok	–	–	–	–	5.9	10.8	6.5	7.4	–	-3.1	34.1	14.VIII	-20.4	4.III	–	–	–	–	–	–	–	–	6.5	6.4	6.0	6.2

Gubałówka

$\varphi = 49°18'$ $\lambda = 19°56'$

I	–	–	–	–	-2.7	0.2	-2.0	-1.6	1.9	-5.6	9.1	21	-19.6	17	79	69	81	76	1.1	2.1	1.0	1.4	7.4	7.3	6.5	7.1
II	–	–	–	–	-0.7	2.3	0.4	0.6	4.4	-2.9	12.7	3	-14.6	28	84	67	82	78	1.0	2.7	1.2	1.6	7.8	7.4	6.7	7.3
III	–	–	–	–	0.2	4.6	1.2	1.8	6.0	-2.5	13.7	21	-12.3	4	75	56	73	68	1.7	4.1	2.0	2.6	6.5	6.1	5.2	5.9
IV	–	–	–	–	4.1	6.8	4.1	4.8	8.5	0.9	19.1	30	-6.7	9,16	76	67	74	72	2.6	4.3	2.7	3.2	6.6	7.2	6.8	6.9
V	–	–	–	–	5.2	7.3	5.0	5.5	9.2	2.4	18.9	13	-3.5	7	82	74	83	80	2.0	3.4	1.7	2.4	7.8	8.1	7.5	8.2
VI	–	–	–	–	13.7	17.4	14.0	14.8	19.4	9.7	26.3	12	3.8	27	70	56	68	65	4.9	9.5	5.5	6.6	4.5	6.8	5.9	5.7
VII	–	–	–	–	14.7	17.4	14.2	15.1	19.2	11.4	30.7	6	7.0	29	79	70	81	77	4.2	7.4	3.7	5.1	7.3	8.0	6.9	7.4
VIII	–	–	–	–	12.4	15.7	12.2	13.1	17.5	9.1	26.2	12	3.9	31	77	65	81	74	3.7	7.1	2.9	4.6	7.5	7.5	6.2	6.4
IX	–	–	–	–	8.1	11.7	8.4	9.2	13.4	5.4	22.7	9	-1.4	27	79	68	80	76	2.6	5.0	2.3	3.3	6.8	7.4	6.3	6.8
X	–	–	–	–	5.5	10.3	6.3	7.0	11.4	2.8	20.2	19	-2.1	5	82	66	84	77	1.7	4.7	1.7	2.7	5.5	5.9	4.3	4.9
XI	–	–	–	–	4.1	3.7	1.4	1.9	5.3	-1.0	14.7	5	-16.6	30	82	76	85	80	1.5	2.5	1.3	1.9	7.3	6.4	6.8	6.8
XII	–	–	–	–	-3.1	-0.4	-2.8	-2.3	1.5	-6.4	10.8	13	-19.7	1	81	75	85	80	1.0	1.8	0.7	1.2	7.1	7.5	6.2	6.9
Rok	–	–	–	–	4.9	8.1	5.2	5.8	9.8	1.9	30.7	5.VII	-19.6	17.1	79	67	80	75	2.3	4.6	2.2	3.0	6.7	7.1	6.3	6.7

Paronin

$H_s = 800$ m $h_w = 16$ m **1957**

MIESIĄC	ROZKŁAD WIATRU [%D, %mD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<0°	Max<0	Min<-10	Max>25°	Opad R ≥0.1 mm	≥1.0 mm	≥10.0 mm	Wiatr ≥10 m/s	≥15 m/s	≡	≋	◔	◕	▦
I	4	4.5	3	4.7	21.5	14	0.5	2.0	·	·	2	2.5	39	17	1	4.0	22	1.2	33.4	7.6	28	31	14	12	·	11	9	·	·	·	-	-	·	4	14	31
II	5	4.1	1	4.0	8.5	4.3	4.5	4.3	0.5	21.0	5.5	4.6	34.5	22	5.5	4.8	25	1.6	40.1	8.0	25	27	4	4	·	11	4.0	·	1	1	-	-	3	10	15
III	10.5	4.8	1.5	4.3	2.2	1.5	·	·	·	·	6	3.3	26	2.3	3	1.5	25	1.5	40.7	13.6	16	24	4	4.0	·	10	7	1	1	·	-	1	7	9	15
IV	5.5	1.4	2.5	2.2	15.5	1.4	1	4.0	1	2.5	1.5	2.7	30.5	1.5	1.5	1.3	31	1.0	91.3	18.1	11	18	1	1	·	17	1.4	3	·	·	-	·	7	15	6
V	1.1	1.4	6.5	1.8	1.7	1.5	·	·	·	·	0.5	2.0	23.5	1.5	5.5	1.5	29	1.1	95.7	19.4	8	10	·	·	·	20	1.7	3	·	·	-	4	1	16	6
VI	5.5	1.2	3.5	1.2	1.2	1.3	·	·	2	7.5	7.5	3.7	29.5	2.5	3	1.3	27	1.6	75.9	24.0	19	2	·	·	5	9	9	3	2	·	-	5	6	5	·
VII	1	2.0	·	·	3	1.0	·	·	1	2.0	8	2.8	4.5	1.8	4	1.0	31	1.2	216.0	41.8	16	·	·	·	8	1.7	1.7	7	·	·	-	5	6	16	·
VIII	2	1.0	2	1.2	11.5	1.3	1	1.5	1.5	1.0	4	2.6	22.5	1.3	3.5	1.0	45	0.7	97.8	30.6	29	·	·	·	4	11	1.1	3	·	·	-	2	4	4	·
IX	3	1.2	0.5	1.0	10.5	1.1	0.5	1.0	·	·	2.5	2.4	39.5	2.6	1.5	1.3	32	1.4	87.2	19.6	4	7	·	·	·	15	1.3	2	1	·	-	·	6	8	·
X	1.1	1.4	3	1.5	1.9	1.0	·	·	·	·	2.5	6.0	16.5	1.5	7	1.2	35	0.9	45.8	17.5	22	2.6	·	·	·	6	6	2	1	·	-	·	9	6	·
XI	6.5	1.3	2.5	1.4	2.9	1.3	·	·	·	·	5	5.2	27.5	2.4	1.5	1.7	18	1.6	34.6	7.8	11	2.1	3	5	·	10	7	·	1	·	-	·	6	1.4	·
XII	8.5	1.2	1	1.0	1.6	1.2	·	·	3.5	3.4	7	5.3	2.6	2.8	1	1.5	31	1.6	20.1	7.5	6	2.8	1.2	1.4	·	6	6	·	1	·	-	·	7	1.3	12
Rok	73.5	1.4	27	1.5	188.5	1.3	4.5	0.6	9.5	3.1	51	3.6	355	2.0	38	1.3	351	1.3	878.6	41.8	16.VII	193	38	46	17	143	126	24	8	1	-	17	65	130	-

Komańcza

$H_s = 470$ m $h_w = 14$ m

I	1.5	3.0	1	5.0	3	4.7	·	·	1.0	3.1	5	4.0	4.6	2.5	5	2.6	8	2.6	30.1	6.5	5	2.9	1.5	8	·	13	12	·	·	·	-	·	·	2.4	31
II	8	2.2	·	·	4	3.8	7	4.3	1.5	4.0	2	3.0	4.0	2.0	4	2.2	4	2.6	64.5	17.8	15	1.6	5	·	·	12	12	1	·	·	-	·	·	2.3	17.1
III	18.5	3.3	5	3.2	4	3.0	3	4.0	7	2.7	3	2.3	2.7	2.5	0.5	4.0	25	2.1	23.7	6.2	16	2.1	5	7	·	10	9	·	·	·	-	·	8	8	8
IV	1.5	2.6	9	1.9	2	2.0	·	·	1.2	2.9	2	3.0	1.4	1.9	4	1.0	32	1.5	65.4	21.2	17	1.2	·	·	·	11	9	3	·	·	-	·	5	1.5	·
V	3.8	2.3	7	2.4	6	3.7	3	1.3	7	2.6	·	·	1.0	2.2	3	2.3	19	1.9	124.5	32.0	6	1	·	·	·	17	1.6	2	·	·	-	·	1	1.6	2
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	2	3.0	·	·	1	3.0	2	3.0	2.7	2.4	8	2.4	1.6	2.1	2	2.5	35	1.5	167.1	52.8	16	·	·	·	·	1.8	1.5	4	·	·	-	1	4	1.9	·
VIII	2	2.5	1	2.0	2	2.5	4	4.0	1.6	3.1	3	2.0	2.0.5	2.4	2.5	3.4	42	1.5	58.8	16.1	29	·	·	·	·	1.5	1.1	2	·	·	-	·	4	8	·
IX	2	2.0	2	1.5	·	·	1.0	2.8	2.3	2.2	9	4.8	1.5	3.0	3	3.0	26	1.7	109.9	31.7	3	·	·	·	·	2.0	1.7	3	·	·	-	·	2	1.2	·
X	7	1.6	3	1.0	3	2.7	6	2.3	1.3	2.3	9	2.0	1.9	1.5	3	1.0	30	1.2	14.7	5.3	24	·	·	·	·	3	3	·	·	·	-	·	9	4	·
XI	1.7	2.6	·	·	8	1.9	7.5	2.1	9.5	1.9	4.5	1.8	2.5.5	1.8	4	7.7	14	2.0	39.0	14.5	28	·	·	·	·	9	7	2	1	·	-	·	3	1.6	1
XII	2.1	2.3	5	2.0	1.7.5	2.1	5.5	4.3	5	1.6	4	2.0	1.8	2.2	1.2	2.2	5	2.2	61.2	18.0	13	·	·	·	·	9	8	2	1	·	-	·	1	2.4	1.2
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	71.1

Baligród

$H_s = 450$ m $h_w = 17,5$ m

I	2	3.0	1	1.0	3	3.7	·	·	3.7	6.5	3	3.7	4	8.0	1.4	2.7	29	3.6	23.9	7.7	28	2.6	-	3	·	10	7	·	5	2	-	-	3	1.7	19
II	3	3.0	·	·	·	·	1	1.0	5.7	5.2	2	2.0	3	4.0	6	2.7	12	4.0	49.4	15.3	15	1.3	4	·	·	8	7	1	3	2	-	-	1	1.4	5
III	4	3.0	5	1.7	4	1.5	1	3.0	3.0	4.2	2	3.0	4	1.5	1.4	3.0	31	2.2	20.3	7.0	18	1.9	4	7	·	9	6	·	5	·	-	-	8	9	12
IV	1.1	2.3	2	3.0	4	2.0	·	·	1.4	2.0	2	4.0	2	2.0	1.0	2.2	45	1.1	61.9	14.3	11	1.2	·	·	·	1.4	1.1	3	·	·	-	-	6	9	2
V	1.0	2.0	8	2.8	4	2.0	1	3.0	1.4	2.6	·	·	3	4.0	1.8	2.2	35	1.4	154.8	30.9	9	1	·	·	·	1.8	1.7	5	·	·	-	-	·	1.5	4
VI	·	·	1	1.0	2	1.0	2	2.0	4.1	3.2	3	2.3	2	7.0	1.0	2.2	29	2.0	121.1	62.6	12	·	·	·	4	8	8	3	·	·	-	-	6	2	·
VII	3	3.0	·	·	3	1.7	2	2.0	3.1	2.2	3	1.7	6	2.2	7	2.9	38	1.3	91.2	23.9	27	·	·	·	10	1.5	1.5	2	·	·	-	-	4	1.0	·
VIII	4	2.8	·	·	2	2.0	·	·	2.7	2.7	1	5.0	6	2.7	1.4	2.5	39	1.5	60.5	23.8	29	·	·	·	6	1.0	7	2	2	·	-	-	3	6	·
IX	·	·	·	·	4	1.5	1	3.0	3.5	2.9	2	3.0	6	2.3	1.2	3.0	3.0	1.9	77.8	18.4	3	1	·	·	·	1.7	1.3	2	1	·	-	-	3	1.0	·
X	1	3.0	1	2.0	2	1.0	3	1.7	3.3	4.0	4	2.5	2	3.0	1.0	2.0	37	1.9	16.5	7.4	20	9	·	·	·	4	3	·	2	1	-	-	1.3	5	·
XI	6	4.7	4	2.5	9	2.3	2	1.0	3.0	3.2	1	3.0	5	1.4	6	2.7	27	2.0	44.7	14.6	11	1.2	2	1	·	6	6	2	1	·	-	-	4	1.4	1
XII	2	2.0	1	1.0	2	2.0	2	2.0	5.1	5.2	1	3.0	3	1.7	1.7	3.5	1.4	3.7	57.6	17.7	13	2.9	-	2	·	9	8	2	3	1	-	-	1	1.5	1.2
Rok	46	2.4	21	1.2	39	1.7	1.5	1.6	4.0.0	3.7	2.4	2.8	46	3.1	1.3.8	2.6	3.6.6	2.2	773.7	62.6	12.VI	122	-	13	2.0	1.2.8	1.0.8	2.2	2.0	6	-	-	5.2	1.2.6	55

Gubałówka

$H_s = 1000$ m $h_w = 16$ m

I	21.5	1.5	3	2.0	5	1.2	·	·	3	2.7	3.5	4.3	4.7	2.8	6	1.4	4	2.2	53.0	10.4	6	3.0	9	6	·	1.5	1.2	1	1	·	-	·	2	1.3	3.1
II	11.5	1.4	0.5	2.0	1	1.0	·	·	9.5	6.2	5	8.2	5.1.5	4.2	1	1.0	4	4.0	64.1	21.0	21	2.4	5	1	·	1.3	1.2	1	7	3	-	·	3	1.4	1.9
III	32.5	1.5	3.5	1.3	2	2.0	0.5	4.0	8	1.9	5.5	4.7	38	3.8	·	·	3	2.6	39.9	13.7	16	1.6	4	4	·	11	7	1	5	·	-	·	6	11	1.6	-
IV	36.5	1.2	2.5	1.6	6	2.2	·	·	1.0	2.8	2.5	2.2	32.5	1.2	·	·	·	1.5	88.5	15.3	11	1.4	1	·	·	2.1	1.6	3	·	·	-	2	3	1.6	-	-
V	29.5	1.5	4.5	2.4	11.5	2.4	0.5	2.0	1.1	1.4	7	2.1	2.8	1.3	·	·	1	1.6	94.0	26.9	20	1.2	1	·	·	2.2	1.7	3	·	·	-	5	·	2.0	6.9	
VI	20.5	1.8	1.5	3.3	3	1.7	·	·	10.5	5.4	4.5	3.7	4.5	2.2	·	·	5	2.5	104.9	60.5	19	·	·	·	1	1.3	1.1	3	3	·	-	9	4	6	·	
VII	1.1	1.2	0.5	4.0	2	3.0	·	·	2.5	1.4	1.1	3.4	60.5	2.2	0.5	1.0	5	2.1	222.2	52.4	16	·	·	·	6	2.1	1.9	7	2	·	-	10	1	1.7	·	
VIII	22.5	1.9	0.5	4.0	1	2.0	·	·	1.0	3.1	8.5	4.0	4.1.5	3.1	·	·	9	2.6	116.3	23.0	29	·	·	·	2	1.5	1.3	5	2	·	-	1	1	7	·	
IX	11.5	1.9	1	4.0	2	2.5	·	·	4	3.5	12.5	7.8	5.1	4.1	1	1.0	7	3.9	108.8	26.0	4	4	·	·	·	1.6	1.2	3	9	3	-	·	2	1.3	·	
X	2.6	1.4	0.5	1.0	1	1.0	·	·	8	1.4	8.5	2.5	3.5.6	1.7	0.5	3.0	1.3	1.4	52.7	22.3	22	8	·	·	·	7	6	2	·	·	-	·	7	7	·	
XI	1.8.5	1.7	2	3.0	8	2.1	0.5	1.0	1.2	1.4	1.5.5	4.2	32	3.1	0.5	2.0	4	2.6	48.3	13.5	29	1.7	7	1	·	1.4	8	1	3	·	-	·	5	1.5	1	
XII	1.5	1.5	1	1.0	1	1.0	·	·	8	5.5	1.5	7.6	44	3.3	·	·	9	3.5	30.0	9.7	5	2.8	1.2	8	·	11	8	·	7	3	-	·	3	1.4	1.3.3	
Rok	253.5	1.5	21	2.5	43.5	1.9	1.5	0.8	96.5	3.1	99	4.6	306.5	2.8	9.5	0.8	64	2.5	1019.9	52.4	16.VII	151	39	20	9	179	141	30	38	9	-	27	37	152	-	

Zakopane

$\varphi = 49°18'$ $\lambda = 19°57'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				— Max	— Min	Max abs.	Data	Min abs.	Data										
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	922.4	932.2	907.3	–	-5.3	-0.3	-4.2	-3.5	1.3	-7.8	9.8	22	-24.6	17	90	75	87	84	0.5	1.9	0.6	1.0	7.4	7.3	6.4	7.0
II	914.8	930.6	893.8	–	-1.8	2.9	-0.1	0.2	4.9	-4.4	10.4	6	-17.2	28	86	67	83	79	0.9	2.7	1.2	1.6	7.7	7.3	6.8	7.3
III	920.2	932.1	905.7	–	-3.0	5.3	0.2	0.7	6.9	-4.7	14.3	21	-16.2	4	85	56	75	72	0.8	4.4	1.9	2.4	6.6	6.1	5.2	6.0
IV	920.3	930.9	898.7	–	2.6	8.3	3.8	4.6	9.9	-0.1	20.3	30	-7.8	9	83	61	82	75	1.6	5.3	1.7	2.9	6.5	7.1	6.7	6.8
V	918.6	926.6	908.6	–	5.4	8.6	5.5	6.2	10.7	2.0	19.4	16,19	-2.5	30	84	71	86	80	1.6	4.2	1.4	2.4	7.7	9.0	7.4	8.0
VI	922.5	933.5	914.4	–	14.5	18.9	13.7	15.2	20.8	8.0	27.6	12	1.4	7	72	53	77	67	4.9	11.1	4.2	6.7	4.7	6.7	5.8	5.7
VII	919.2	929.2	908.5	–	14.9	18.6	14.4	15.6	20.5	10.5	31.8	5	4.7	29	82	66	86	78	3.4	9.0	2.6	5.0	7.1	7.7	6.9	7.2
VIII	920.8	929.0	909.3	–	11.8	17.0	12.1	13.2	18.6	7.8	26.8	12,14	1.1	31	84	62	86	77	2.5	8.0	2.2	4.2	5.5	7.2	6.3	6.3
IX	919.4	928.7	907.1	–	7.1	13.0	8.1	9.1	14.3	4.5	23.3	9	-3.0	26	87	65	86	80	1.4	5.7	1.5	2.9	6.6	7.4	6.3	6.8
X	924.3	931.8	908.2	–	2.2	11.3	4.5	5.6	12.2	0.2	21.5	19	-5.0	3	92	63	89	81	0.6	5.4	1.1	2.4	5.4	5.0	4.4	4.9
XI	922.3	937.5	910.4	–	0.2	4.8	1.0	1.8	6.0	-4.7	15.2	5	-15.2	30	87	72	86	82	1.1	3.1	1.1	1.8	7.2	6.3	6.8	6.8
XII	917.1	935.3	889.0	–	-4.8	-0.6	-2.9	-2.8	1.5	-7.5	12.7	13	-16.7	3	83	73	80	79	0.9	1.8	1.2	1.3	6.9	7.5	6.1	6.8
Rok	920.2	937.5	889.0	–	3.6	9.0	4.7	5.5	10.6	0.6	31.8	5.VII	-24.6	17.1	85	65	84	78	1.7	5.2	1.7	2.9	6.6	7.0	6.5	6.6

Antałówka

$\varphi = 49°18'$ $\lambda = 19°59'$

I	–	–	–	–	-3.9	-0.5	-2.8	-2.5	1.2	-6.3	9.1	2	-23.9	17	–	–	–	–	–	–	–	–	7.9	7.4	7.0	7.4
II	–	–	–	–	-1.2	2.2	0.0	0.2	4.1	-3.5	11.1	3,5	-14.9	28	–	–	–	–	–	–	–	–	7.9	7.2	7.4	7.5
III	–	–	–	–	-1.4	4.5	0.8	1.2	6.0	-3.4	13.6	21	-13.6	4	–	–	–	–	–	–	–	–	6.4	5.9	5.6	6.0
IV	–	–	–	–	3.2	7.7	3.9	4.7	9.4	0.6	19.9	30	-6.4	16	–	–	–	–	–	–	–	–	6.4	7.1	7.0	6.8
V	–	–	–	–	5.2	8.1	5.2	5.9	10.0	2.4	18.9	19	-2.9	7	–	–	–	–	–	–	–	–	7.9	9.1	7.7	8.2
VI	–	–	–	–	14.8	18.5	14.0	15.3	20.3	9.3	27.6	12	3.7	27	–	–	–	–	–	–	–	–	4.5	6.6	5.3	5.5
VII	–	–	–	–	14.8	18.1	14.4	15.4	20.0	11.2	31.0	5	5.2	29	–	–	–	–	–	–	–	–	7.0	7.8	7.0	7.3
VIII	–	–	–	–	11.9	16.5	12.5	13.4	18.3	8.7	26.3	12,14	2.5	31	–	–	–	–	–	–	–	–	5.1	7.3	6.4	6.3
IX	–	–	–	–	7.3	12.5	8.2	9.0	13.7	5.1	22.9	9	-1.4	26,27	–	–	–	–	–	–	–	–	6.5	7.1	6.7	6.8
X	–	–	–	–	3.7	10.7	5.6	6.4	11.5	1.6	19.6	19	-3.6	3	–	–	–	–	–	–	–	–	5.6	5.0	4.7	5.1
XI	–	–	–	–	0.9	4.1	1.4	2.0	5.3	-2.2	14.5	6	-16.0	30	–	–	–	–	–	–	–	–	7.0	6.0	6.7	6.6
XII	–	–	–	–	-3.9	-0.9	-2.8	-2.6	0.8	-7.2	11.6	13	-15.5	1	–	–	–	–	–	–	–	–	7.1	7.3	6.3	6.9
Rok	–	–	–	–	4.3	8.5	5.0	5.7	10.0	1.4	31.0	5.VII	-23.9	17.1	–	–	–	–	–	–	–	–	6.6	7.0	6.5	6.7

Gładówka

$\varphi = 49°18'$ $\lambda = 20°07'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	-1.0	3.9	0.5	1.0	5.6	-3.5	16.8	21	-12.8	1	–	–	–	–	–	–	–	–	5.4	5.3	3.8	4.8
IV	–	–	–	–	2.4	6.2	3.3	3.8	8.0	-0.2	18.6	30	-10.3	13	–	–	–	–	–	–	–	–	5.8	6.2	7.1	6.4
V	–	–	–	–	4.3	6.5	4.3	4.8	8.6	1.2	19.0	19	-4.9	7	–	–	–	–	–	–	–	–	7.3	8.9	8.4	8.2
VI	–	–	–	–	13.2	17.1	12.9	14.0	19.2	9.0	27.1	12	3.7	27	–	–	–	–	–	–	–	–	4.9	5.9	5.9	5.6
VII	–	–	–	–	13.8	16.1	13.6	14.3	18.9	10.8	29.8	5	5.2	28	–	–	–	–	–	–	–	–	7.1	8.3	6.4	7.3
VIII	–	–	–	–	11.2	14.7	11.5	12.2	16.9	8.4	25.7	14	3.8	31	–	–	–	–	–	–	–	–	5.5	7.3	5.7	6.2
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	0.6	3.0	0.6	1.2	6.0	-1.6	19.8	5	-17.3	30	–	–	–	–	–	–	–	–	6.6	6.1	6.7	6.5
XII	–	–	–	–	-3.7	-1.5	-3.1	-2.8	1.8	-6.8	8.7	13	-16.3	1	–	–	–	–	–	–	–	–	6.6	7.0	6.1	6.6
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kuźnice

$\varphi = 49°16'$ $\lambda = 19°59'$

I	–	–	–	–	-3.7	-0.4	-3.4	-2.7	1.0	-6.6	7.5	22	-19.5	17	–	–	–	–	–	–	–	–	7.4	6.9	6.9	7.1
II	–	–	–	–	-1.4	1.6	-0.6	-0.2	3.6	-4.2	12.8	3	-16.0	28	–	–	–	–	–	–	–	–	8.1	7.3	7.1	7.5
III	–	–	–	–	-2.0	4.1	-0.1	0.5	5.5	-4.6	13.2	14	-14.5	4	–	–	–	–	–	–	–	–	6.2	6.0	4.9	5.5
IV	–	–	–	–	1.9	6.5	2.3	3.3	8.0	-1.1	18.0	30	-8.5	16	–	–	–	–	–	–	–	–	6.0	6.9	6.6	6.5
V	–	–	–	–	4.2	6.8	3.8	4.6	8.7	1.0	17.4	19	-3.6	7	–	–	–	–	–	–	–	–	7.8	9.2	7.9	8.3
VI	–	–	–	–	13.7	17.2	12.2	13.8	18.9	7.6	25.7	12	2.4	27	–	–	–	–	–	–	–	–	4.6	6.8	5.9	5.7
VII	–	–	–	–	14.0	16.7	12.8	14.1	18.5	9.4	30.1	5	4.8	29	–	–	–	–	–	–	–	–	6.7	8.1	7.0	7.3
VIII	–	–	–	–	11.2	15.1	11.3	12.2	16.8	7.0	26.2	14	1.4	31	–	–	–	–	–	–	–	–	5.2	7.5	6.0	6.2
IX	–	–	–	–	7.1	11.2	7.3	8.2	12.7	3.8	22.7	9	-2.3	26	–	–	–	–	–	–	–	–	6.4	7.5	6.8	6.9
X	–	–	–	–	2.9	9.6	4.0	5.1	10.5	0.5	18.1	19	-3.7	3	–	–	–	–	–	–	–	–	5.3	4.8	4.3	4.8
XI	–	–	–	–	0.5	3.4	0.9	1.4	4.6	-1.8	16.4	4	-16.4	30	–	–	–	–	–	–	–	–	6.8	6.2	6.9	6.5
XII	–	–	–	–	-3.6	-0.8	-3.1	-2.6	0.9	-7.2	10.2	13	-16.4	1	–	–	–	–	–	–	–	–	6.4	7.0	6.2	6.5
Rok	–	–	–	–	3.7	7.6	4.0	4.8	9.1	0.3	30.1	5.VII	-19.5	17.1	–	–	–	–	–	–	–	–	6.6	7.0	6.5	6.7

Zakopane

$H_s = 844\ m$ $H_b = 838{,}2\ m$ $h_w = 14\ m$ **1957**

MIESIĄC	ROZKŁAD WIATRU (%)																	OPAD R			LICZBA DNI (n)																	
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Opad R			Wiatr									
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Max<0	Min<0	Max≥10	Max≥25	R≥0,1	R≥1,0	R≥10,0	R≥100	v≥10	v≥15								
I	5	1,3	13,6	1,8	4,5	2,0	0,5	2,0	1,5	2,7	18,5	3,3	15	2,9	6,5	1,6	2,8	1,7	41,6	9,7	6	31	10	8	·	14	9	·	1	·	4	·	2	12	28
II	6	2,0	9,5	1,8	0,5	2,0	3,5	2,9	3,5	6,4	21,5	3,4	14	3,3	25	2,4	2,4	2,2	61,4	21,7	21	25	3	4	·	13	11	1	8	1	·	·	3	14	18
III	6	1,9	1,6	2,0	2,5	2,6	0,5	4,0	2	2,0	1,8	2,4	11,5	3,0	3,5	2,3	3,3	1,5	43,8	15,4	16	22	4	9	·	10	8	1	·	·	1	1	6	12	15
IV	3	1,8	13,5	2,0	3,5	2,1	3,5	1,9	2,5	3,4	15,5	1,8	4,5	1,7	6	2,2	3,8	1,1	102,7	16,6	22	15	·	·	·	20	14	4	·	·	2	2	3	15	7
V	8	1,5	1,9	2,6	1,0	2,0	3,5	1,3	1	1,5	14,5	1,3	8	1,6	7	2,2	2,2	1,5	97,8	25,1	20	7	·	·	·	21	18	3	·	·	1	5	·	20	4
VI	8,5	2,3	10,5	2,3	2	2,0	5,5	2,7	7	6,7	26,5	2,5	10,5	2,5	4,5	2,2	1,5	2,5	93,7	42,3	13	·	·	·	4	13	9	2	3	·	·	8	4	6	·
VII	4,5	2,0	4,5	1,7	3,5	2,0	1	2,0	3,5	2,3	3,0,5	1,7	15,5	2,6	5	2,2	2,5	1,5	192,8	54,2	16	·	·	·	8	21	18	7	1	·	·	10	2	17	·
VIII	11,5	1,6	8	1,3	1,5	1,0	2	1,0	2	1,0	17,5	2,3	16	2,2	8,5	1,8	2,6	1,3	112,6	22,6	28	·	·	·	3	16	12	5	1	·	·	2	1	8	·
IX	4,5	2,1	9,5	1,5	2,5	1,0	1	1,0	2,5	2,2	1,6	3,7	1,6	3,1	10	2,7	2,8	1,9	98,7	24,7	4	2	·	·	·	18	12	3	1	·	2	·	2	11	·
X	5,5	1,4	12,5	1,6	5	1,6	·	·	0,5	1,0	1,3	2,4	6	1,7	3,5	1,5	4,7	0,3	47,6	18,8	22	1,6	·	·	·	6	6	3	·	·	3	·	7	8	·
XI	4	2,9	22,5	2,1	3	1,8	6	1,5	4,5	2,0	1,6	2,5	13,5	3,0	3,5	2,7	1,7	1,9	41,3	12,1	29	1,8	4	1	·	11	8	1	1	1	3	·	4	15	2
XII	5,5	1,9	5	2,2	4	2,0	2,5	1,4	2,5	6,2	2,6,5	3,2	1,4	3,0	2	1,2	3,1	1,9	27,6	9,3	5	2,8	1,3	1,2	·	10	8	·	6	·	3	·	3	1,3	1,2
Rok	7,2	1,9	1,4,3	1,9	4,2,5	1,8	2,9,5	1,8	3,3	3,4	2,3,4	2,5	1,4,4,5	2,6	6,2,5	2,1	3,3,4	1,8	961,6	54,2	16.VII	1,6,4	3,4	3,4	1,5	1,7,3	1,3,3	3,0	2,2	2	1,9	2,8	3,7	1,5,1	8,6

Antałówka

$H_s = 918\ m$ $h_w = 18\ m$

I	4	1,4	9	2,1	4	4,2	0,5	3,0	9	4,2	19,5	3,3	14	5,8	3	5,0	3,0	2,6	3,9,9	7,9	6	29	10	6	·	14	9	·	8	1	8	·	2	17	27
II	1,5	6,0	3	1,7	5	1,2	4,5	7,6	1,5	6,7	12,5	4,6	16,5	4,4	5	3,1	2,1	3,6	60,6	19,2	21	23	5	2	·	17	13	1	10	4	4	·	3	15	18
III	4	2,5	12	2,3	·	·	4,5	1,8	9	3,2	15,5	3,4	15	5,3	1	3,0	3,2	2,2	44,5	13,3	16	19	4	7	·	11	7	1	9	1	2	1	6	13	15
IV	4	1,5	1,5	2,8	3,5	3,0	4	3,4	1,7	2,1	12,5	2,0	4,5	2,1	5,5	2,0	2,4	1,7	102,5	17,3	23	11	1	·	·	20	13	3	5	·	7	3	5	16	7
V	6,5	2,1	2,4	2,9	6,5	2,6	6	1,9	18,5	1,7	9	2,0	3	2,8	5,5	2,4	1,4	2,0	104,9	22,6	20	9	·	·	·	22	19	3	·	·	5	5	·	20	6
VI	9,5	2,0	9,5	2,5	2,5	1,6	6,5	3,1	2,4,5	4,8	1,1	2,9	7,5	4,4	7	2,1	1,2	2,9	79,5	24,1	19	·	·	·	3	12	10	4	7	1	1	1,2	4	6	·
VII	5	2,8	2	2,2	·	·	4,5	1,9	1,8,5	1,8	2,8,5	2,7	1,0	4,2	4,5	2,3	2,0	2,0	203,7	49,6	16	·	·	·	8	21	17	6	3	·	3	1,4	4	1,8	·
VIII	1,0	1,7	4,5	1,4	0,5	1,0	3	3,5	1,5,5	3,5	1,6	2,8	1,0	3,6	7,5	2,1	2,6	2,0	128,3	31,5	19	·	·	·	3	15	13	5	4	·	5	4	1	7	·
IX	9	2,6	6	2,4	·	·	4,5	2,6	5,5	3,9	1,8,5	5,0	2,2,5	4,4	4	3,4	2,0	3,1	105,3	23,1	4	3	·	·	·	18	14	3	6	2	2	1	2	14	·
X	1,8,5	1,9	8	1,9	1,5	2,7	6,5	1,8	11	3,3	10,5	2,8	5	2,9	2	2,0	3,0	1,6	58,9	1,8,5	22	10	·	·	·	7	6	3	1	·	3	·	6	9	·
XI	6,5	2,2	1,4,5	3,1	·	·	3	5,7	1,0	9,0	2,2,5	2,4	9	4,6	3,5	5,6	2,1	3,1	41,5	9,5	29	1,7	6	1	·	9	8	·	6	2	5	·	6	15	4
XII	4	1,8	4	1,4	1	2,0	2,5	2,2	7,5	9,0	2,2	4,2	1,3	6,0	5	2,1	3,4	2,9	24,6	8,6	5	2,8	1,4	1,1	·	1,1	6	·	8	5	7	·	2	1,3	1,2
Rok	8,2,5	2,4	1,1,1,5	2,2	2,4,5	1,5	5,0	3,4	1,6,1	4,4	1,9,8	3,2	1,3,0	4,2	5,3,5	2,9	2,8,4	2,5	982,2	49,6	16.VII	1,4,9	4,0	2,7	1,4	1,7,7	1,3,5	2,9	6,7	1,6	5,2	4,0	4,1	1,6,3	8,9

Głodówka

$H_s = 1149\ m$ $h_w = 16\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	71,4	12,2	7	-	-	-	-	15	12	1	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	16	1,7	3	1,3	1,3	2,2	2	4,5	2	4,0	1	2,0	4,9	3,7	2	2,0	5	2,8	24,9	4,8	19	22	5	5	·	11	9	·	1	·	-	·	10	5	1
IV	8	1,9	3	2,0	13,5	2,0	1,5	1,7	12,5	3,3	10,5	2,8	2,6	2,5	1	2,0	1,4	2,1	60,5	10,2	8	16	3	1	·	17	11	1	·	·	-	·	4	10	-
V	7	3,1	5	2,4	1,3	2,3	3	3,3	1,6	3,2	4	3,2	3,9	3,1	2	3,5	4	2,9	98,9	14,8	20	15	3	·	·	18	16	2	·	·	-	·	·	19	-
VI	9,5	1,4	0,5	1,0	5	1,9	2,5	3,6	1,8,5	3,9	4	2,5	3,8	1,9	2	1,0	1,0	2,1	106,3	64,2	12	·	·	·	1	11	8	2	·	·	-	1	3	8	-
VII	3	1,3	·	·	4	2,2	·	·	4	3,8	1,2	3,0	5,2	2,7	1	3,0	1,7	2,2	248,9	48,2	16	·	·	·	4	22	21	9	·	·	-	1	2	17	-
VIII	1,0	2,2	3	1,7	9	2,2	·	·	1	10,0	9	2,7	5,2	2,9	3	2,0	6	2,6	92,2	26,0	29	·	·	·	1	11	10	4	1	·	-	1	4	11	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	5	1,6	·	·	1,8	3,5	·	·	1,1	2,7	·	·	3,5	2,7	·	·	2,1	2,2	43,6	9,5	11	1,9	6	2	·	10	7	·	1	1	-	·	7	16	-
XII	1	3,0	1	2,0	4,5	1,9	2,5	1,0	5	4,8	1	8,0	4,1	4,4	·	·	3,7	2,5	22,3	7,8	5	2,9	1,2	6	·	9	8	·	2	2	-	·	7	14	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	64,2	12.VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Kuźnice

$H_s = 1023\ m$ $h_w = 21\ m$

I	9,5	2,5	6	4,2	·	·	·	·	2,1,5	2,9	1,8,5	2,7	1	1,0	2,5	1,4	3,4	1,8	66,4	14,3	28	29	12	6	·	15	10	3	2	2	3	·	4	15	31
II	4,5	1,7	3,5	1,6	2	1,0	0,5	9,0	2,4,5	4,8	24	4,8	·	·	1	2,0	2,4	3,0	92,8	23,2	21	25	6	4	·	19	15	2	4	4	4	·	3	15	28
III	9,5	1,7	7	1,7	2	1,0	1,5	1,0	2,6,5	3,3	2,2	2,8	·	·	1,5	1,0	2,3	2,0	50,2	16,2	16	21	5	8	·	12	10	1	2	·	1	1	6	9	21
IV	8	1,5	2,5	1,8	·	·	2	3,5	22	2,3	18	2,2	·	·	7,5	1,8	3,0	1,4	124,1	20,5	11	22	2	·	·	20	18	5	1	·	6	1	5	15	8
V	1,6	1,2	5	1,6	1	1,0	·	·	8,5	1,6	6,5	1,8	1	3,0	6	1,0	4,9	0,7	166,9	47,3	20	13	2	·	·	25	19	4	·	·	12	5	·	20	6
VI	8,5	1,9	5	2,0	·	·	1,5	3,7	2,6	3,7	1,8,5	3,3	·	·	7,5	1,7	2,3	2,2	104,6	20,4	9	·	·	·	2	14	11	5	3	·	1	5	4	7	·
VII	8,5	1,5	6,5	1,9	·	·	1,5	1,7	1,4	2,4	1,3,5	2,4	0,5	1,0	3,5	1,0	4,5	1,0	257,6	55,6	16	·	·	·	4	22	21	7	·	·	4	7	2	1,8	·
VIII	1,0	1,1	3	2,4	1	3,0	0,5	3,0	1,9	3,0	1,8,5	2,4	·	·	3	1,7	3,3	1,5	140,6	37,3	22	·	·	·	2	16	13	4	·	·	3	2	1	8	·
IX	9,5	1,4	5	1,6	2	3,0	0,5	1,0	2,4	2,0	2,0,5	1,8	·	·	3,5	1,3	2,5	1,3	129,1	22,5	4	5	·	·	·	1,6	1,6	5	·	·	4	·	3	1,6	·
X	1,1,5	1,2	2,5	1,4	·	·	1	1,0	2,4,5	2,0	2,3,5	2,1	·	·	6	1,0	2,4	1,3	59,8	18,2	22	1,6	·	·	·	7	6	2	1	·	4	·	8	7	1
XI	1,3	1,6	4,5	2,3	·	·	2	4,2	2,0	4,2	1,3	3,3	1,5	3,7	4	1,5	3,2	2,0	72,2	18,5	29	1,7	7	1	·	12	9	2	3	1	4	·	6	1,5	5
XII	4,5	1,9	2,5	2,6	·	·	1	10,5	2,5	4,6	1,6	3,8	·	·	·	·	4,4	2,2	50,3	14,3	13	2,8	1,2	9	·	1,3	10	2	4	1	4	·	5	1,3	1,2
Rok	1,1,3	1,6	5,8	2,1	8	0,8	1,2	3,2	2,6,5,6	3,1	2,1,2,6	2,6	4	0,7	4,6	1,3	3,8,6	1,7	1,4,4,6	5,5,6	16.VII	1,7,6	4,6	2,8	8	1,9,1	1,5,8	4,2	2,0	8	5,0	2,1	4,7	1,5,8	1,1,2

Łysa Polana

$\varphi = 49°16'$ $\lambda = 20°07'$ 1957

MIESIĄC	CIŚNIENIE p				TEMPERATURA t										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					Średnia				Max	Min	Max abs.	Data	Min abs.	Data													
	P_m	Max	Min	$P_{o.m}$	I	II	III	Dies							I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-5.0	-0.3	-4.6	-3.6	4.7	-7.6	10.0	22	-21.9	17	–	–	–	–	–	–	–	–	6.6	6.2	5.9	6.2
II	–	–	–	–	-2.9	2.1	-1.5	-1.0	4.3	-5.1	14.0	5,5	-17.5	28	–	–	–	–	–	–	–	–	6.9	7.0	6.4	6.8
III	–	–	–	–	-4.1	4.6	-1.7	-0.7	6.2	-6.1	14.0	14	-16.5	4	–	–	–	–	–	–	–	–	6.0	5.3	4.4	5.2
IV	–	–	–	–	1.4	7.0	1.7	3.0	8.7	-1.6	19.2	30	-7.8	16	–	–	–	–	–	–	–	–	6.1	6.3	6.2	6.2
V	–	–	–	–	3.8	7.1	3.4	4.4	9.2	0.5	18.4	19	-3.1	30	–	–	–	–	–	–	–	–	7.6	8.6	7.7	8.0
VI	–	–	–	–	13.5	17.5	14.8	13.6	19.7	6.9	27.6	12	1.3	7	–	–	–	–	–	–	–	–	4.6	5.5	5.6	5.2
VII	–	–	–	–	13.5	16.9	12.6	13.9	19.2	9.3	30.6	5	4.5	29	–	–	–	–	–	–	–	–	6.5	7.2	6.6	6.8
VIII	–	–	–	–	10.4	15.5	11.0	12.0	17.5	6.8	28.4	14	-0.1	31	–	–	–	–	–	–	–	–	5.3	6.7	6.4	6.1
IX	–	–	–	–	5.4	11.6	6.6	7.6	13.5	3.2	22.2	9	-4.1	26	–	–	–	–	–	–	–	–	5.9	6.4	5.8	6.0
X	–	–	–	–	1.5	10.0	3.0	4.4	11.9	-0.7	21.0	19	-5.2	3	–	–	–	–	–	–	–	–	5.1	4.5	4.3	4.6
XI	–	–	–	–	-0.8	3.8	-0.4	0.6	5.8	-3.0	14.3	1,7	-16.3	30	–	–	–	–	–	–	–	–	6.5	5.6	6.2	6.1
XII	–	–	–	–	-5.5	-1.3	-4.0	-3.7	1.8	-8.4	11.4	13	-16.6	1	–	–	–	–	–	–	–	–	6.1	6.3	5.5	6.0
Rok	–	–	–	–	2.6	7.9	3.2	4.2	10.0	-0.5	30.6	5.VII	-21.9	17.1	–	–	–	–	–	–	–	–	6.1	6.3	5.9	6.1

Dolina Chochołowska

$\varphi = 49°15'$ $\lambda = 19°49'$

I	–	–	–	–	-4.6	-1.1	-4.1	-3.5	0.9	-7.2	7.9	2,22	-21.8	17	–	–	–	–	–	–	–	–	6.1	5.8	5.4	5.8
II	–	–	–	–	-1.8	1.8	-0.7	-0.4	3.8	-4.7	11.3	5	-18.3	28	–	–	–	–	–	–	–	–	6.2	6.4	6.5	6.4
III	–	–	–	–	-3.3	4.2	-1.4	-0.5	5.4	-5.5	13.1	21	-18.3	4	–	–	–	–	–	–	–	–	5.0	5.3	3.8	4.7
IV	–	–	–	–	0.8	6.2	1.8	2.6	7.6	-1.7	17.5	29	-9.4	9	–	–	–	–	–	–	–	–	5.6	6.6	5.8	6.0
V	–	–	–	–	2.3	6.7	3.8	4.2	8.4	0.5	17.1	16	-3.6	7	–	–	–	–	–	–	–	–	7.0	8.3	6.7	7.3
VI	–	–	–	–	11.2	17.1	11.5	12.8	18.8	7.1	26.1	12	1.6	7	–	–	–	–	–	–	–	–	3.4	4.8	3.7	4.0
VII	–	–	–	–	12.2	16.7	12.1	13.3	18.3	9.2	29.5	5	4.4	30	–	–	–	–	–	–	–	–	6.4	7.0	6.0	6.5
VIII	–	–	–	–	9.3	15.2	11.0	11.6	16.8	6.7	27.6	14	0.4	31	–	–	–	–	–	–	–	–	4.4	5.9	5.9	5.4
IX	–	–	–	–	5.8	11.2	7.0	7.8	12.6	3.8	22.6	9	-3.3	26	–	–	–	–	–	–	–	–	5.3	6.4	5.8	5.8
X	–	–	–	–	2.1	9.8	4.2	5.1	10.8	0.2	19.0	19	-4.3	3	–	–	–	–	–	–	–	–	4.1	3.6	3.5	3.7
XI	–	–	–	–	-0.2	3.2	0.9	1.2	4.7	-1.7	15.9	1	-16.3	30	–	–	–	–	–	–	–	–	5.7	5.0	6.3	5.7
XII	–	–	–	–	-4.3	-1.3	-3.1	-3.0	0.8	-7.0	10.3	13	-15.8	1	–	–	–	–	–	–	–	–	5.8	5.8	6.4	6.0
Rok	–	–	–	–	2.5	7.6	3.6	4.3	9.1	0.0	29.5	5.VII	-21.8	17.1	–	–	–	–	–	–	–	–	5.4	5.9	5.5	5.6

Myślenickie Turnie

$\varphi = 49°15'$ $\lambda = 19°59'$

I	–	–	–	–	-3.0	-1.5	-3.2	-2.7	0.3	-6.3	9.5	21	-16.0	17									7.5	7.5	6.4	7.1
II	–	–	–	–	-1.8	-0.6	-1.4	-1.3	1.6	-4.3	10.4	3	-13.0	27	–	–	–	–	–	–	–	–	7.6	7.9	7.7	7.7
III	–	–	–	–	-0.8	1.5	-0.5	-0.1	3.5	-3.9	11.0	21	-14.6	2	–	–	–	–	–	–	–	–	7.1	6.6	5.2	6.3
IV	–	–	–	–	1.3	3.5	1.2	1.8	5.3	-1.3	15.0	30	-9.3	15	–	–	–	–	–	–	–	–	7.0	7.8	7.1	7.3
V	–	–	–	–	2.6	4.2	2.8	3.1	6.3	0.4	15.1	19	-6.4	7	–	–	–	–	–	–	–	–	8.1	9.6	8.2	8.6
VI	–	–	–	–	11.5	14.0	11.7	12.2	16.6	8.2	24.0	12	2.7	27	–	–	–	–	–	–	–	–	5.7	7.3	6.9	6.6
VII	–	–	–	–	12.6	14.2	12.6	13.0	16.4	9.9	28.3	5	5.3	17,28	–	–	–	–	–	–	–	–	7.5	8.5	7.5	7.8
VIII	–	–	–	–	9.6	12.0	10.5	10.6	14.5	7.3	23.7	14	2.6	23	–	–	–	–	–	–	–	–	6.0	8.3	6.5	6.9
IX	–	–	–	–	6.0	8.2	6.7	6.9	10.4	3.8	20.6	9	-3.5	27	–	–	–	–	–	–	–	–	6.7	7.7	7.0	7.1
X	–	–	–	–	5.2	6.6	5.5	5.7	8.8	2.3	15.3	19	-3.7	5	–	–	–	–	–	–	–	–	5.2	5.5	3.8	4.8
XI	–	–	–	–	0.1	1.6	0.2	0.5	3.8	-2.8	14.1	1	-23.9	30	–	–	–	–	–	–	–	–	6.9	6.5	6.5	6.6
XII	–	–	–	–	-3.6	-2.4	-2.9	-3.0	0.0	-6.7	7.9	13	-18.4	1	–	–	–	–	–	–	–	–	6.8	7.5	6.0	6.8
Rok	–	–	–	–	3.3	5.1	3.6	3.9	7.5	0.6	28.3	5.VII	-23.9	30.XI	–	–	–	–	–	–	–	–	6.8	7.6	6.6	7.0

Hala Gąsienicowa

$\varphi = 49°15'$ $\lambda = 20°00'$

I	845.1	853.1	830.1	–	-4.4	-2.6	-4.1	-3.8	-0.5	-7.1	7.3	21	-16.5	17	76	73	76	75	1.3	1.7	1.3	1.4	7.4	7.2	6.1	6.9
II	838.5	854.6	819.3	–	-2.7	-1.8	-2.6	-2.4	0.8	-6.1	8.3	4	-16.8	23	74	77	78	76	1.5	1.5	1.3	1.4	7.2	7.2	7.1	7.2
III	843.9	854.6	832.0	–	-2.0	0.5	-1.3	-1.0	2.2	-5.3	9.1	21	-14.1	2	62	62	61	62	2.2	2.8	2.4	2.5	6.7	6.3	4.8	5.9
IV	844.6	855.3	824.3	–	0.2	2.2	0.6	0.9	3.4	-2.8	13.3	30	-12.6	14	77	74	78	76	1.8	2.5	1.8	2.0	6.3	7.2	6.7	6.7
V	843.3	852.1	832.3	–	2.0	3.1	1.4	2.0	4.9	-1.0	13.4	19	-7.4	7	86	85	89	87	1.3	1.5	0.9	1.2	7.5	9.2	7.9	8.2
VI	842.4	851.1	841.0	–	11.1	13.1	10.3	11.2	14.6	6.7	22.6	12	1.2	27,28	67	64	73	68	4.8	5.9	3.6	4.8	5.1	6.7	5.9	5.9
VII	846.5	853.2	836.0	–	12.0	13.2	11.1	11.8	14.6	8.3	26.6	5	4.2	29,30	77	76	82	78	4.1	4.4	2.7	3.7	6.9	8.1	6.5	7.2
VIII	847.4	854.3	837.9	–	9.3	10.9	9.3	9.7	12.6	6.0	22.9	14	1.6	23	77	78	83	79	3.1	3.2	2.2	2.8	5.0	7.2	5.7	6.0
IX	845.1	853.4	833.7	–	5.2	7.2	5.5	5.8	9.0	2.3	18.2	9	-5.6	27	75	76	79	77	2.4	2.8	2.0	2.4	6.1	7.4	6.7	6.7
X	849.1	856.6	834.7	–	4.3	7.0	4.8	5.2	8.9	1.2	15.8	10	-5.6	3	63	71	64	66	3.8	3.5	3.6	3.6	4.7	4.7	3.6	4.3
XI	846.0	858.2	833.5	–	-0.4	1.5	-0.6	0.0	3.8	-3.4	12.3	1	-20.9	30	74	74	76	75	1.9	2.3	1.8	2.0	6.1	5.7	6.3	6.7
XII	840.2	856.8	816.0	–	-4.6	-3.0	-4.3	-4.0	-1.0	-7.9	7.0	13	-21.0	1	73	76	74	74	1.3	1.4	1.3	1.3	6.2	6.9	5.5	6.2
Rok	844.9	853.1	816.0	–	2.5	4.3	2.5	3.0	6.1	-0.8	25.6	5.VII	-21.0	1.XII	73	74	76	74	2.5	2.8	2.1	2.5	6.3	7.0	6.0	6.4

Łysa Polana

H_s = 988 m h_w = 18 m 1957

| MIESIĄC | ROZKŁAD WIATRU [%D, %nD] | | | | | | | | | | | | | | | | | | OPAD R | | | LICZBA DNI (n) | | | | | | | | | | | | | | | | | |

Hala Ornak

$\varphi = 49°14'$ $\lambda = 19°51'$ 1957

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Średnia I	II	III	Dies	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-5.2	-0.7	-4.7	-3.8	–	-8.0	–	–	-22.8	17	–	–	–	–	–	–	–	–	6.2	5.8	5.1	5.7
II	–	–	–	–	-3.3	1.4	-2.1	-1.5	3.0	-6.5	10.2	3	-18.7	23	–	–	–	–	–	–	–	–	7.3	6.6	7.1	7.0
III	–	–	–	–	-4.2	4.3	-2.1	-1.0	5.2	-6.5	12.4	21	-19.5	4	–	–	–	–	–	–	–	–	5.5	4.7	4.6	4.9
IV	–	–	–	–	0.4	6.2	0.9	2.1	7.5	-2.6	19.3	27	-10.1	9,14	–	–	–	–	–	–	–	–	4.9	6.2	5.6	5.6
V	–	–	–	–	2.5	6.4	2.8	3.6	8.1	-0.2	17.4	19	-4.4	30	–	–	–	–	–	–	–	–	6.6	8.6	6.9	7.4
VI	–	–	–	–	11.6	11.1	10.8	11.2	13.2	5.8	27.2	12	-0.3	7	–	–	–	–	–	–	–	–	3.9	5.3	3.5	4.2
VII	–	–	–	–	12.4	16.6	11.9	13.2	17.8	7.8	29.2	5	2.6	19,30	–	–	–	–	–	–	–	–	6.5	8.7	5.3	6.2
VIII	–	–	–	–	8.9	15.1	10.5	11.2	16.3	5.3	27.1	14	1.2	31	–	–	–	–	–	–	–	–	4.6	6.2	5.5	5.4
IX	–	–	–	–	5.5	10.9	6.4	7.3	12.0	2.7	22.1	9	-5.4	26	–	–	–	–	–	–	–	–	6.8	7.0	6.8	6.5
X	–	–	–	–	1.4	10.1	2.5	4.1	10.9	-1.4	16.8	19	-6.4	3	–	–	–	–	–	–	–	–	4.9	3.1	3.8	3.9
XI	–	–	–	–	-0.2	3.3	0.1	0.8	4.7	-3.1	15.3	1	-17.2	30	–	–	–	–	–	–	–	–	5.8	5.9	6.2	6.0
XII	–	–	–	–	-5.4	-0.7	-3.5	-3.3	0.8	-8.4	8.3	13	-16.0	1	–	–	–	–	–	–	–	–	6.4	6.4	5.7	6.2
Rok	–	–	–	–	2.0	7.5	2.8	3.8	–	1.3	29.2	5.VII	-22.8	17.1	–	–	–	–	–	–	–	–	5.8	6.0	5.5	5.8

Kasprowy Wierch

$\varphi = 49°14'$ $\lambda = 19°59'$

I	796.4	804.7	781.7	–	-7.0	-6.0	-6.6	-6.6	-4.0	-9.4	2.5	21	-19.0	17	70	72	70	71	1.3	1.2	1.3	1.3	7.1	7.5	6.5	7.0
II	790.4	806.8	772.2	–	-6.4	-5.7	-6.1	-6.1	-3.5	-8.6	4.5	3	-17.4	28	84	85	85	85	0.7	0.7	0.6	0.7	7.4	7.7	7.3	7.5
III	795.7	806.4	784.7	–	-5.1	-3.6	-4.8	-4.6	-1.9	-7.6	5.2	21	-19.1	2	60	70	64	65	1.8	1.5	1.6	1.6	6.5	6.7	5.4	6.2
IV	796.8	808.0	778.2	–	-3.2	-1.0	-2.6	-2.4	0.1	-5.0	7.6	30	-13.8	16	79	79	82	80	1.2	1.4	1.1	1.2	6.4	7.6	7.5	7.2
V	795.8	805.3	783.6	–	-1.0	0.9	-0.8	-0.4	2.1	-2.8	9.2	19	-10.2	7	91	91	92	91	0.6	0.6	0.5	0.6	7.9	9.6	7.7	8.4
VI	803.1	813.6	793.9	–	6.8	9.4	7.2	7.6	11.1	4.4	19.5	12	-2.0	27	81	76	84	80	2.3	3.2	1.8	2.4	5.7	7.0	6.9	6.5
VII	800.6	810.3	789.4	–	8.0	9.7	8.1	8.5	11.3	6.0	23.0	5	1.2	28	88	87	91	89	1.8	2.3	1.3	1.8	7.4	8.4	7.1	7.6
VIII	800.9	808.1	792.6	–	5.3	7.6	5.8	6.1	9.2	3.4	18.9	14	-1.6	23	88	88	94	90	1.3	1.6	0.6	1.2	5.9	8.2	7.3	7.1
IX	798.1	803.6	786.5	–	1.8	3.6	2.2	2.4	5.2	0.0	14.7	9	-7.8	27	82	87	92	87	1.4	1.3	0.6	1.1	7.0	7.9	7.2	7.4
X	802.0	809.9	787.9	–	2.3	3.8	2.9	3.0	5.2	-0.1	10.4	12	-8.7	4	62	72	63	66	3.4	2.7	3.2	3.1	4.8	4.6	4.2	4.5
XI	798.0	810.2	783.8	–	-1.7	-0.8	-2.0	-1.6	0.9	-4.2	7.7	1	-24.8	30	74	76	75	75	1.5	1.5	1.4	1.5	5.5	5.5	5.7	5.6
XII	791.5	807.9	768.7	–	-6.9	-6.2	-6.8	-6.7	-4.5	-9.8	1.5	13	-22.3	1	70	75	75	73	1.2	1.1	1.0	1.1	5.8	6.8	5.2	5.9
Rok	797.4	813.6	768.7	–	-0.6	1.0	-0.3	0.0	2.6	-2.8	23.0	5.VII	-24.8	30.XI	77	80	81	79	1.5	1.6	1.2	1.4	6.4	7.3	6.5	6.7

Dolina Pięciu Stawów

$\varphi = 49°13'$ $\lambda = 20°03'$

I	–	–	–	–	-5.9	-4.1	-5.6	-5.3	-1.4	-9.4	6.0	22	-22.0	17	–	–	–	–	–	–	–	–	7.0	7.2	6.2	6.5
II	–	–	–	–	-5.1	-2.5	-4.2	-4.0	-0.5	-7.8	7.0	4	-20.7	27	–	–	–	–	–	–	–	–	7.7	7.1	6.8	7.2
III	–	–	–	–	-3.9	-0.3	-3.3	-2.7	1.6	-7.2	7.0	21	-19.5	2	–	–	–	–	–	–	–	–	6.5	6.2	5.4	6.0
IV	–	–	–	–	-1.6	1.5	-0.5	-0.3	3.5	-4.2	11.0	30	-14.9	9	–	–	–	–	–	–	–	–	6.9	7.1	7.0	7.0
V	–	–	–	–	0.7	2.2	0.5	1.0	4.2	-2.2	11.8	16	-7.7	7	–	–	–	–	–	–	–	–	6.6	8.7	7.2	7.5
VI	–	–	–	–	9.3	11.4	9.2	9.8	13.6	6.2	22.1	30	1.5	1	–	–	–	–	–	–	–	–	5.4	7.6	5.8	6.3
VII	–	–	–	–	10.7	12.1	10.7	11.0	13.8	8.3	23.5	5	4.1	16,17	–	–	–	–	–	–	–	–	6.6	7.8	6.5	7.0
VIII	–	–	–	–	8.0	10.3	8.9	9.0	11.8	6.2	21.9	14	4.0	23	–	–	–	–	–	–	–	–	5.5	7.3	6.9	6.6
IX	–	–	–	–	4.4	6.2	5.3	5.3	7.8	2.5	16.1	8,9	-5.0	27	–	–	–	–	–	–	–	–	6.6	7.5	6.8	7.0
X	–	–	–	–	3.4	6.0	4.2	4.4	7.9	1.2	13.4	12	-5.5	4	–	–	–	–	–	–	–	–	3.5	3.7	3.7	3.6
XI	–	–	–	–	-0.8	1.2	-1.0	-0.4	2.9	-3.1	9.5	1	-21.0	30	–	–	–	–	–	–	–	–	5.7	5.7	5.3	5.6
XII	–	–	–	–	-5.2	-4.5	-5.6	-5.2	-2.4	-8.6	5.3	14	-19.4	1	–	–	–	–	–	–	–	–	5.7	6.1	4.8	5.5
Rok	–	–	–	–	1.2	3.3	1.6	1.9	5.2	-1.5	23.5	5.VII	-22.0	17.1	–	–	–	–	–	–	–	–	6.1	6.8	6.0	6.3

Morskie Oko

$\varphi = 49°12'$ $\lambda = 20°04'$

I	–	–	–	–	-4.6	-3.2	-4.8	-4.4	-0.4	-8.2	8.5	21	-21.4	17	–	–	–	–	–	–	–	–	5.8	5.6	5.3	5.6
II	–	–	–	–	-2.8	-0.5	-2.2	-1.9	2.3	-6.5	10.5	3	-18.3	27	–	–	–	–	–	–	–	–	6.1	6.3	6.4	6.3
III	–	–	–	–	-2.5	2.1	-1.7	-1.0	4.0	-6.3	10.5	21	-23.1	2	–	–	–	–	–	–	–	–	5.3	6.4	4.0	4.9
IV	–	–	–	–	-0.3	3.1	0.6	0.9	5.4	-3.0	14.6	28	-12.4	14	–	–	–	–	–	–	–	–	6.7	6.3	6.4	6.3
V	–	–	–	–	1.2	3.9	1.7	2.1	5.9	-1.0	15.2	19	-6.3	7	–	–	–	–	–	–	–	–	7.3	9.1	7.0	7.8
VI	–	–	–	–	10.7	11.3	10.9	11.1	11.6	6.8	25.0	12	1.7	28	–	–	–	–	–	–	–	–	4.3	6.4	4.0	5.5
VII	–	–	–	–	11.2	11.2	11.2	11.2	12.0	–	8.4	–	–	4.1	29	–	–	–	–	–	–	–	6.5	7.5	6.0	6.6
VIII	–	–	–	–	8.7	12.2	9.9	10.2	–	5.9	–	–	0.6	31	–	–	–	–	–	–	–	–	5.0	6.6	6.2	5.9
IX	–	–	–	–	5.1	8.6	6.3	6.4	–	2.6	–	–	-4.5	27	–	–	–	–	–	–	–	–	5.6	6.7	6.3	6.2
X	–	–	–	–	3.1	8.2	3.7	4.9	–	0.6	–	–	-4.9	3	–	–	–	–	–	–	–	–	4.9	4.2	2.8	4.0
XI	–	–	–	–	-0.4	0.9	-0.8	-0.3	–	-3.2	–	–	-19.7	30	–	–	–	–	–	–	–	–	5.1	5.5	5.4	5.3
XII	–	–	–	–	-4.6	-3.2	-4.0	-4.0	–	-6.0	–	–	-19.5	1	–	–	–	–	–	–	–	–	5.4	5.6	4.1	5.0
Rok	–	–	–	–	2.0	5.0	2.5	3.0	–	-1.0	–	–	-23.1	2.III	–	–	–	–	–	–	–	–	5.6	6.3	5.5	5.8

Hala Ornak

$H_s = 1110$ m $h_w = 15$ m 1957

MIESIĄC	ROZKŁAD WIATRU (%D, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<-10°	Max>25°	Opad R ≥0.1	≥1.0	≥10.0	Wiatr v ≥10	≥15					
I	·	·	1	1,0	·	·	7	3,2	1	3,5	·	·	1	1,0	21	4,2	62	1,3	78,9	18,2	7	28	–	12	·	16	11	3	·	·	–	·	6	11	31
II	·	·	·	·	·	·	16,5	4,8	1,5	6,7	1,0	5,0	·	·	17	4,1	39	2,5	96,7	17,2	21	28	6	7	·	19	15	2	6	·	–	·	3	15	28
III	·	·	·	·	·	·	14,5	3,3	1,5	3,3	5	3,0	·	·	24	2,1	48	1,3	75,3	19,0	16	22	4	12	·	13	10	4	·	·	–	·	8	6	26
IV	·	·	1,3	2,5	0,5	4,0	2,1	2,6	1,5	2,3	2	2,5	·	·	3	2,3	49	1,1	134,0	15,0	18	26	3	2	·	21	21	3	·	·	–	3	5	11	10
V	·	·	1,6	2,4	·	·	4	1,5	·	·	2	2,0	·	·	2	1,5	69	0,6	163,9	40,5	20	18	3	·	·	23	19	6	·	·	–	3	·	17	8
VI	·	·	7	2,4	·	·	2,2	4,1	·	·	2	5,5	·	·	4	2,0	55	1,4	120,5	23,3	10	1	·	·	1	14	14	7	1	·	–	8	7	3	·
VII	·	·	7	1,6	·	·	2,5	1,6	2,5	3,0	3	2,8	0,5	4,0	1,5	2,0	76	0,4	208,0	57,8	17	·	·	·	4	21	19	5	·	·	–	9	5	13	·
VIII	·	·	10,5	2,3	0,5	4,0	2	5,0	1,5	6,3	5,5	3,5	·	·	3	1,7	70	0,8	137,3	37,0	30	·	·	·	1	15	12	4	·	·	–	2	2	4	·
IX	·	·	6	1,8	0,5	5,0	17,5	2,8	1	7,5	3	2,7	·	·	6	1,7	56	1,0	160,9	21,0	13	4	·	·	·	17	16	8	·	·	–	1	5	11	·
X	0,5	1,0	13,5	1,7	·	·	6,5	4,0	2	5,0	1,5	2,7	·	·	·	·	67	0,7	109,4	14,0	23	24	·	·	·	7	6	2	·	·	–	·	9	6	·
XI	·	·	1,0	2,0	·	·	1,6	5,6	3	5,7	1	4,0	·	·	1,0	3,4	50	1,2	67,6	25,4	30	22	6	3	·	11	11	1	·	·	–	·	7	14	3
XII	·	·	1,9	3,5	·	·	1,7	4,6	·	·	1	2,0	·	·	7	2,0	49	1,8	71,7	18,0	9	30	16	12	·	14	10	2	·	·	–	·	8	14	14,3
Rok	0,5	0,1	10,6	1,8	1,5	1,1	146,6	3,6	15,5	3,6	3,6	3,0	1,5	0,4	98,5	2,2	690	1,2	1345,7	57,8	16.VII	203	–	48	6	191	164	47	7	·	–	26	65	125	119,2

Kasprowy Wierch

$H_s = 1991$ m $H_b = 1988,8$ m $h_w = 15,4$ m

I	1,7	5,4	8	5,3	1	9,0	9	10,9	1,8	7,7	10,5	6,6	10,5	6,4	1,6	7,8	3	6,9	80,8	17,3	7	31	25	11	·	20	16	2	20	5	23	·	3	15	31
II	8,5	6,0	3	3,5	·	·	12,5	14,1	23,5	9,8	12,5	7,3	1,5	7,2	7	5,8	2	8,4	129,7	17,2	22	26	22	9	·	19	18	4	23	10	24	·	2	16	28
III	2,2	6,4	5	3,5	3,5	8,4	10,5	7,9	1,3	8,2	10,5	7,6	14,5	9,9	1,4	5,4	·	7,3	52,5	11,3	16	29	19	9	·	18	9	1	21	10	17	1	5	11	31
IV	27,5	5,6	8,5	3,2	4,5	4,0	1,8	6,1	1,5	6,7	2,5	4,0	1	1,5	7,5	4,4	9	4,8	147,5	19,7	23	25	15	6	·	21	18	3	10	2	21	4	4	15	30
V	3,4	5,2	1,9	4,9	5,5	1,5	3,5	3,3	7,5	3,2	5,5	2,3	3	2,7	3	2,5	12	3,7	210,1	33,9	8	19	10	1	·	25	20	6	5	·	25	6	·	20	30
VI	25,5	4,0	4,5	4,3	1	8,0	9,5	8,5	1,8	10,0	1,2	8,2	6	5,2	9,5	4,6	4	6,3	110,5	25,1	9	5	·	·	·	15	12	4	1,4	5	17	1,0	3	12	2
VII	1,7	3,8	6	2,5	1	5,0	3	5,3	9,5	5,6	16,5	4,5	1,4	4,7	1,4	4,6	12	3,9	268,4	39,6	15	·	·	·	·	23	19	8	9	1	21	1,4	1	19	·
VIII	21,5	4,4	7	3,6	1,6	1,3	1	4,5	1,8	8,0	22,5	5,1	8	4,3	3,5	5,3	10	4,7	106,8	20,8	29	5	·	·	·	19	1,4	3	1,7	4	24	2	·	12	1
IX	5,5	4,4	5	4,4	0,5	3,0	2,5	2,6	20,5	8,1	2,2	6,4	1,6	8,4	1,6	7,5	2	6,9	114,6	19,3	4	15	4	·	·	18	14	5	19	5	27	1	1	15	6
X	8	4,4	5	5,1	1	1,0	3	5,7	33,5	6,3	21,5	6,0	1,0	3,8	2	5,2	9	5,1	33,5	13,6	22	13	4	·	·	10	6	2	9	2	15	·	10	7	1,5
XI	1,4	7,2	8,5	4,7	3	4,0	9	7,6	2,7	10,2	8,5	7,3	2,5	6,4	6,5	6,8	11	6,9	95,0	28,2	29	22	7	3	·	15	11	4	1,9	4	17	·	9	10	1,9
XII	1,3	8,5	1,1	8,1	1	4,0	3	10,5	2,3	10,3	1,5	9,5	1,1	6,4	6	5,4	7	8,5	86,4	25,7	5	31	27	13	·	17	13	2	2,0	1,3	19	·	4	9	3,1
Rok	21,3,5	5,4	90,5	4,4	23,5	4,1	84,5	7,3	22,3	8,0	159,6	6,2	114,5	5,7	10,5	5,8	8,1	6,1	1441,8	39,6	15.VIII	221	133	52	·	220	170	44	186	61	250	38	42	161	224

Dolina Pięciu Stawów

$H_s = 1668$ m $h_w = 12$ m

I	·	·	·		6	2,3	2	5,5	2	9,5	2,9	6,7	2,7	5,9	·	·	2,7	4,3	74,0	17,7	7	31	16	13	·	18	11	2	4	2	5	·	5	11	31
II	·	·	·		3	2,0	·	·	3	4,0	1,7	8,3	4,4	10,0	·	·	1,7	6,4	60,6	10,0	18	26	17	7	·	17	12	1	1,0	6	5	·	3	16	28
III	1,4	5,0	1,4	5,0	7	3,7	1,4	3,0	1,6	5,1	2,0	7,2	2,6	3,6	·	·	2,1	3,8	28,9	5,3	19	27	6	12	·	17	8		6	3	1,4	·	5	9	31
IV	·	·	6	2,7	11	4,1	3	4,3	4	2,0	8	4,4	1,6	2,7	·	·	4,2	1,8	139,3	22,9	17	24	8	4	·	21	18	5	·	·	13	1,4	4	15	30
V	4	2,8	1,8	3,0	3,4	3,0	·	·	1	2,0	4	3,0	6	2,8	·	·	2,6	2,1	94,4	10,4	8	19	8	·	·	24	20	2	·	·	15	2	·	15	31
VI	1	2,0	1	2,0	2,3	3,2	1	3,0	2	9,5	1,6	6,4	2,6	7,6	·	·	2,0	4,8	151,6	25,3	9	·	·	·	·	16	15	7	5	2	3,5	1,4	3	8	1,1
VII	·	·	·	·	8	2,5	·	·	2	4,0	9	5,7	3,2	4,9	·	·	4,2	2,5	371,0	68,7	15	·	·	·	·	21	20	10	4	·	6	3	1	13	·
VIII	3	3,0	2	3,5	1,7	3,4	1	2,0	2	4,5	6	6,3	3,9	8,6	·	·	2,3	4,9	151,3	73,2	29	·	·	·	·	15	14	3	1,0	3	8	·	1	7	·
IX	1	3,0	·	·	1,3	2,5	·	·	2	11,0	1,8	2,1	4,6	5,8	·	·	1,0	5,0	149,5	24,1	3	9	·	·	·	21	19	6	6	3	4	·	2	12	6
X	2	3,5	·	·	5	2,8	·	·	·	·	1,9	4,4	3,3	4,7	·	·	3,4	2,8	30,9	10,7	20	12	2	·	·	6	5	1	2	1	6	·	1,4	7	7
XI	·	·	·	·	7	5,6	7	7,0	8	14,5	1,6	6,6	2,8	8,5	·	·	2,4	6,1	111,3	32,4	29	20	7	2	·	15	14	3	8	5	3	·	2	13	1,7
XII	·	·	7	4,8	8	6,0	4	7,2	2,0	7,6	2,6	15,0	6	6,2	2	3,5	2,0	7,4	64,6	26,7	13	30	23	11	·	15	9	2	1,4	9	4	·	6	10	31
Rok	1,2	4,6	3,5	1,8	1,4,2	3,4	1,9	2,7	6,2	6,1	1,8,8	6,8	3,2,9	5,9	2	0,3	3,0,6	4,3	1424,4	73,2	29.VIII	198	87	49	·	206	165	42	69	34	73	1,0	5,0	135	223

Morskie Oko

$H_s = 1400$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	70,8	19,2	5	26	1,4	10	·	20	12	2	–	–	2	·	8	12	31
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	107,5	15,7	15	27	8	7	·	21	8	3	–	–	·	·	5	12	28
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	57,9	11,1	17	24	5	9	·	17	9	1	–	–	·	·	7	5	31
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	116,7	19,3	23	24	6	3	·	21	19	3	–	–	·	2	5	14	30
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	93,6	12,1	20	18	6	·	·	25	20	2	–	–	8	1	·	17	21
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	126,9	23,5	9	·	·	·	·	16	13	6	–	–	2	6	4	4	·
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	277,4	55,1	15	·	·	·	–	21	19	7	–	–	2	1	2	11	·
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	103,2	20,5	29	·	–	·	–	17	14	4	–	–	3	·	1	7	·
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	168,1	28,4	14	8	–	·	–	19	12	8	–	–	5	·	4	10	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45,1	27,3	22	12	–	·	–	7	4	1	–	–	5	·	11	5	2
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	78,4	19,0	3	21	–	3	–	14	11	2	–	–	7	·	7	7	19
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	53,4	10,0	5	28	–	11	–	15	12	·	–	–	3	·	9	7	31
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1298,0	55,1	15.VII	190	–	43	–	213	165	39	–	–	37	10	63	111	194

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TABLICA III

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

DATES LIMITES DU GEL

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Aleksandrowice	19.IV	27.IX	160
Aleksandrówka	30.V	26.IX	118
Antałówka	28.V	25.IX	119
Antopol	29.V	27.IX	120
Babia Góra	30.V	25.IX	117
Baligród	7.V	26.IX	141
Bartoszyce	28.V	12.XI	167
Barwinek	30.V	25.IX	117
Biała Podlaska	6.V	3.X	149
Białowieża	6.V	3.X	149
Białystok	29.V	3.X	126
Biecz	30.V	26.IX	118
Bielsk Podlaski	29.V	3.X	126
Bieruń Stary	30.V	27.IX	119
Biskupiec	6.V	3.X	149
Błonie-Topola	6.V	26.IX	142
Bochnia-Chodenice	16.IV	2.X	168
Bodzentyn	27.V	26.IX	121
Borowo	9.V	27.IX	140
Borusowa	30.V	26.IX	118
Brwinów	29.V	27.IX	120
Brzegi Dolne	31.V	26.IX	117
Brzezna	21.IV	26.IX	157
Bukowina Tatrzańska	28.V	26.IX	120
Busko-Zdrój	16.IV	3.X	169
Bydgoszcz	9.V	26.IX	139
Bydgoszcz, IMiUZ	6.V	2.X	148
Bystrzyca Kłodzka	30.V	27.IX	119
Bytom, park	21.IV	27.IX	158
Chełm k.Krakowa	16.IV	3.X	169
Chełm Lubelski	16.IV	27.IX	163
Chmielnik	21.IV	2.X	163
Chojnice	29.V	12.XI	166
Chorzelów	21.IV	27.IX	158
Chrząstowo	-	2.X	-
Chylice	29.V	27.IX	120
Ciechocinek	6.V	27.IX	143
Cieplice Śl.-Zdrój	30.V	27.IX	119
Cieszyn	19.IV	27.IX	160
Cieszyn-Bobrek	30.V	27.IX	119
Ciężkowice	30.V	26.IX	118
Ciołkowo	7.V	27.IX	142
Czarna Dąbrówka	29.V	26.IX	119
Czarny Dunajec	30.V	26.IX	118
Czernichów	16.IV	26.IX	162
Częstochowa	7.V	3.X	148
Czorsztyn, leśnictwo	31.V	26.IX	117
Czorsztyn-Nadzamcze	30.V	26.IX	118
Darłowo	6.V	15.XI	192
Dąbrowa Górnicza	16.IV	13.XI	210
Dąbrowa Tarnowska	16.IV	26.IX	162
Dęba-Rozalin	16.IV	-	-
Dębica	16.IV	27.IX	163
Dobrogostów	29.V	28.X	151
Dobryszyce	29.V	3.X	126
Dolina Chochołowska	31.V	25.IX	116
Dolina Pięciu Stawów	31.V	16.IX	107
Duszniki-Zdrój	29.V	27.IX	120
Dynów	7.V	27.IX	142
Dziwnów	15.IV?	14.XI	212?
Elbląg	6.V	13.XI	190
Felin	16.IV	-	-
Frombork	6.V	13.XI	190
Garlica Murowana	16.IV	27.IX	163
Gdańsk-Nowy Port	6.V	15.XI	192
Gdańsk-Siedlce	6.V	15.XI	192
Gdańsk-Wrzeszcz	16.IV	15.XI	212
Gdynia	16.IV	15.XI	212
Gliwice, park	7.V	27.IX	142
Głębokie	6.V	27.IX	143
Głodówka	29.V	-	-
Głogów	9.V	2.X	145
Głubczyce	8.V	27.IX	141
Głuchołazy-Zdrój	9.V	13.XI	187
Gniezno	7.V	27.IX	142
Gołdap	29.V	12.XI	166
Gorzów Wlkp.	9.V	1.X	144
Goszyce	16.IV	3.X	169
Grądy-Woniecko	31.V	16.X	137
Grodkowice	16.IV	3.X	169
Grodków	7.V	26.IX	141
Grudziądz	6.V	13.XI	190
Gryfice	-	13.XI	-
Gubałówka	29.V	25.IX	118
Hala Gąsienicowa	31.V	15.IX	106
Hala Ornak	7.VI	25.IX	109
Hel	2.V	22.XI	203
Hopowo	6.V	-	-
Horyniec	5.V	26.IX	133
Igołomia	16.IV	26.IX	162
Iłowa	30.V	26.IX	118
Inowrocław	16.IV	27.IX	163
Istebna-Stecówka	10.V	26.IX	138
Istebna-Zaolzie	31.V	-	-
Iwonicz	9.V	27.IX	140
Izbica Kujawska	22.IV	-	-
Jabłonka	31.V	26.IX	117
Jarosław	7.V	3.X	148
Jaworzyna Krynicka	29.V	25.IX	118
Jelenia Góra	30.V	27.IX	119
Jeziory	29.V	26.IX	119
Jordanów	30.V	26.IX	118
Kalisz	7.V	27.IX	142
Kamienica	30.V	26.IX	118
Kamienica Królewska	29.V	-	-
Kamień Krajeński	29.V	27.IX	120
Karpacz	28.V	27.IX	121
Kartuzy	29.V	27.IX	120
Kasprowy Wierch	28.VI	23.VIII	55
Katowice	29.V	27.IX	120
Kętrzyn	6.V	12.XI	189
Kielce	29.V	26.IX	119
Kisielnica	31.V	3.X	124
Klimczok	29.V	25.IX	118
Kluczbork	-	26.IX	-
Kluczewo	29.V	26.IX	119
Kłodzko	30.V	26.IX	118
Kobylec	29.V	26.IX	119
Kochcice	7.V	27.IX	142
Kolbuszowa	5.V	26.IX	143
Kolno	6.V	2.X	148
Koło	22.IV	26.IX	156
Kołobrzeg	29.V	13.XI	167
Komańcza	30.V	-	-
Koniaków	9.V	27.IX	140
Kończewice	6.V	27.IX	143
Koszalin	29.V	13.XI	167

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Kościerzyna	29.V	26.IX	119
Kowale Oleckie	6.V	12.XI	189
Kórnik	30.V	26.IX	118
Kraków-Czyżyny	-	27.IX	-
Kraków, Inst.Geogr.UJ	16.IV	3.X	169
Kraków, Obserw.Astr.UJ	16.IV	3.X	169
Kraków-Rakowice	16.IV	-	-
Krasnystaw	27.V	27.IX	122
Krosno	17.IV	26.IX	161
Krynica	30.V	26.IX	118
Krynica-Góra Parkowa	9.V	26.IX	139
Krynica Morska	16.IV	15.XI	212
Krzesławice	16.IV	-	-
Kudowa-Zdrój	30.V	27.IX	119
Kuźnice	30.V	17.IX	109
Kwidzyń	6.V	27.IX	143
Laskowice Oławskie	7.V	26.IX	141
Lądek-Zdrój	30.V	25.IX	117
Legionowo	6.V	13.XI	190
Legnica	22.IV	3.X	163
Lesko	30.V	26.IX	118
Leskowiec	29.V	27.IX	120
Leszkowice	28.V	2.X	126
Leszno-Antoniny	9.V	26.IX	139
Leszno-Strzyżewice	-	27.IX	-
Leżajsk	16.IV	27.IX	163
Lębork	29.V	16.IX	119
Lidzbark	28.V	26.IX	120
Lidzbark Warmiński	6.V	12.XI	189
Limanowa	31.V	26.IX	117
Lipowa	16.IV	3.X	169
Lublin	16.IV	27.IX	163
Luboń Wielki	28.V	27.IX	121
Lućmierz	28.V?	27.IX	121?
Łapanów	30.V	26.IX	118
Ławica, IUNiG	30.V	25.IX	117
Łącko	16.IV	27.IX	163
Łeba	6.V	15.XI	192
Łosice	6.V	3.X	149
Łowicz-Blich	-	27.IX	-
Łódź-Lublinek	29.V	26.IX	119
Łódź-Ruda Pabianicka	29.V	26.IX	119
Łysa Polana	31.V	31.VIII	91
Maków Podhalański	16.IV	26.IX	163
Malbork	16.IV	13.XI	210
Maniowy	7.VI	26.IX	110
Miastko	29.V	26.IX	119
Michorzewo	29.V	26.IX	119
Miechów	30.V	26.IX	118
Mielec, WSK	21.IV	27.IX	158
Międzybrodzie	16.IV	-	-
Międzychód	29.V	26.IX	119
Międzyzdroje	29.V	13.XI	167
Mikołajki	6.V	3.X	149
Minikowo	29.V	2.X	125
Mława	6.V	27.IX	143
Młochów	6.V	13.XI	190
Modzurów	7.V	3.X	148
Morskie Oko	31.V	16.IX	107
Motycz	16.IV	13.XI	210
Muroki	16.IV	3.X	169
Muszyna	30.V	26.IX	118
Myszyniec-Zawodzie	31.V	3.X	124
Myślenice	16.IV	3.X	169
Myślenickie Turnie	30.V	17.IX	109

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	po raz ostatni	po raz pierwszy	
Namysłów	7.V	26.IX	141
Nidzica	28.V	2.X	126
Niepokalanów	6.V	13.XI	190
Nikutowo	6.V	13.XI	190
Nisko	16.IV	27.IX	163
Nowa Wieś	16.IV	3.X	169
Nowy Dwór Gdański	6.V	13.XI	190
Nowy Dwór Mazowiecki	6.V	13.XI	190
Nowy Sącz	16.IV	26.IX	162
Nowy Targ	31.V	26.IX	117
Nur	6.V	13.XI	190
Oborniki Śląskie	9.V	27.IX	140
Ochaby	29.V	3.X	126
Olesno	30.V	26.IX	118
Olsztyn-Dajtki	28.V	13.XI	168
Oława	7.V	2.X	147
Opole	7.V	26.IX	141
Opolnica	29.V	27.IX	120
Orzysz	31.V	13.XI	165
Osiny	29.V	27.IX	120
Osowiec	29.V	13.XI	167
Ostojów	6.V	12.XI	189
Ostrzeżka	29.V	3.X	126
Ostrowy	22.IV	13.XI	204
Ostróda	6.V	2.X	148
Ostrzeszów	29.V	26.IX	119
Otmuchów	30.V	2.X	124
Paproć	-	26.IX	-
Pawłowice	9.V	26.IX	139
Pętkowo	7.V	27.IX	142
Pieńczykówek	31.V	17.IX	108
Pilsko	-	15.IX	-
Piotrków Trybunalski	7.V	3.X	148
Piwniczna	30.V	26.IX	118
Plewiska	29.V	2.X	125
Płock-Radziwie	22.IV	13.XI	204
Płocko	29.V	13.XI	167
Polanica-Zdrój	30.V	27.IX	119
Poraj	29.V	26.IX	119
Porąbka	16.IV	3.X	169
Poronin	27.VI	24.VIII	57
Poświętne	6.V	13.XI	190
Poznań-Ławica	28.V	26.IX	120
Poznań-Sołacz	9.V	26.IX	139
Pożóg	17.IV	3.X	168
Prabuty	29.V	13.XI	167
Przasnysz	6.V	3.X	149
Przebędowo	9.V	26.IX	139
Przedbórz	29.V	3.X	126
Przelewice	27.V	2.V	127
Przemyśl	17.IV	3.X	168
Przybroda	29.V	26.IX	119
Pszczela Wola	16.IV	-	-
Ptaszkowa	9.V	3.X	146
Puck	2.V	15.XI	196
Puczniew	29.V	26.IX	119
Puławy, IUNiG	16.IV	3.X	169
Puławy-Kępa	29.V	27.IX	120
Pułtusk	6.V	13.XI	190
Raba Wyżna	16.IV	2.X	168
Rabka	30.V	26.IX	118
Racibórz	7.V	27.IX	142
Radom-Wacyn	27.V	3.X	128
Radostowo	12.V	13.XI	184
Radzików	29.V	13.XI	167

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
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Ramlewo Dolne	29.V	-	-
Rdzawka na Obidowej	10.V	26.IX	138
Reguły	6.V	13.XI	190
Resko	29.V	2.X	125
Rębiska	-	16.XI	-
Rokitnica	30.V	26.IX	118
Rosnowo	29.V	26.IX	119
Rozewie	6.V	15.XI	192
Rożnów	16.IV	3.X	169
Rudka	6.V	3.X	149
Rybnik	21.IV	26.X	187
Rymanów-Zdrój	30.V	26.IX	118
Rzeszów-Jasionka	16.IV	3.X	169
Sandomierz	16.IV	3.X	169
Sanok	7.V	26.IX	141
Sejny	6.V	12.XI	189
Sękocin	6.V	27.IX	143
Siedlce	29.V	3.X	126
Siejnik	6.V	12.XI	189
Sielec Pińczowski	30.V	26.IX	118
Sielec Stary	9.V	26.IX	139
Siemianice	7.V	26.IX	141
Siemiatycze	6.V	3.X	149
Sieniawa	30.V	26.IX	118
Sieradz	29.V	27.IX	120
Sinołęka	6.V	3.X	149
Skawina	16.IV	27.IX	163
Skierniewice	6.V	13.XI	190
Skroniów	7.V	3.X	148
Słubice	29.V	26.IX	119
Słupia Nowa	16.IV	2.X	168
Słupsk	29.V	27.IX	120
Smolice	7.V	27.IX	142
Sobieszyn	16.IV	3.X	169
Sokołowsko	30.V	26.IX	118
Sokółka	6.V	3.X	149
Sopot	16.IV	15.XI	212
Sosnowiec	16.IV	13.XI	210
Spalona	27.V	25.IX	120
Stańcowa	30.V	27.IX	119
Stare Pole	28.V	13.XI	168
Stary Sącz	30.V	26.IX	118
Strzelna	30.V	21.IX	113
Strzyżów	5.V	26.IX	143
Suchedniów	29.V	26.IX	119
Suwałki	6.V	12.XI	189
Szczawnica-Zdrój	30.V	26.IX	118
Szczawno-Zdrój	28.V	27.IX	121
Szczecin-Dąbie	29.V	2.X	125
Szczecin-Łabędzia	9.V	13.XI	187
Szczecinek	29.V	26.IX	119
Szczuczyn	29.V	12.XI	166
Szczytno	29.V	27.IX	120
Szepietowo	6.V	13.XI	190
Szklarska Poręba	30.V	25.IX	117
Szprotawa	29.V	26.IX	119
Ślęża	27.V	27.IX	122
Śliwice	29.V	27.IX	120
Śnieżka	6.VI	13.IX	98
Śnieżnik Kłodzki	25.VI	24.IX	90
Śrem	29.V	26.IX	119
Świbno	6.V	13.XI	190
Świbno-Ujście Wisły	6.V	15.XI	192
Świder	6.V	26.IX	142

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków /dni/
	po raz ostatni	po raz pierwszy	
Świdnica	9.V	2.X	145
Świebodzin	9.V	26.IX	139
Świecie	8.V	2.X	146
Świerklaniec	30.V	26.IX	118
Świniarsko	30.V	26.IX	118
Świnoujście	21.IV	14.XI	206
Tarnów	16.IV	3.X	169
Tczew	6.V	13.XI	190
Terespol n.B.	16.IV	3.X	169
Tęgoborze	16.IV	13.XI	210
Tolkmicko	16.IV	13.XI	210
Tomaszów Lubelski	20.IV	27.IX	159
Toruń-Podgórz	6.V	27.IX	143
Toruń-Wrzosy	30.V	26.IX	118
Trzebież	9.V	13.XI	187
Trzebinia	16.IV	13.XI	210
Trzemeszno	16.IV	27.IX	163
Turbacz	-	17.IX	-
Tychy	16.IV	3.X	169
Tyniec	16.IV	3.X	169
Ustka	6.V	15.XI	192
Wadowice	16.IV	3.X	169
Wałcz	29.V	2.X	125
Warka n.P.	16.IV	13.XI	210
Warszawa-Bielany	16.IV	13.XI	210
Warszawa, Obserw.Astr.UW	16.IV	13.XI	210
Warszawa-Okęcie	6.V	13.XI	190
Werbkowice	5.V	26.IX	143
Wielichowo	27.V	26.IX	121
Wieliczka	16.IV	3.X	169
Wieliszew	6.V	13.XI	190
Wieluń	7.V	27.IX	142
Wieniec-Zdrój	7.V	26.IX	141
Wińsko	7.V	14.XI	190
Wirty	6.V	13.XI	190
Wisła	30.V	26.IX	118
Wisznice	5.V	4.X	151
Witów	30.V	25.IX	117
Włodawa	18.IV	3.X	167
Wojcieszów Górny	29.V	27.IX	120
Wolbrom	30.V	21.IX	113
Wrocław-Mały Gądów	30.V	26.IX	118
Wrocław, WSR	19.IV	3.X	166
Wyrzysk	29.V	27.IX	120
Wysokie	10.V	3.X	145
Wysowa	30.V	25.IX	117
Wyszków	2.V	27.IX	147
Zakopane	31.V	26.IX	117
Zakrzów	30.V	26.IX	118
Zamość	18.IV	27.IX	161
Zawoja	26.V	26.IX	122
Ząbkowice	30.V	26.IX	118
Zbąszyń	9.V	26.IX	139
Zdanów	16.IV	26.IX	162
Zgorzelec	29.V	27.IX	120
Zielona Góra I	7.V	14.XI	190
Zwardoń	30.V	26.IX	118
Żarnowa	7.V	27.IX	142
Żary	29.V	27.IX	120
Żegiestów-Zdrój	30.V	26.IX	118
Żelisławki	6.V	13.XI	190
Żywiec-Sporysz	30.V	26.IX	118

M. BAŁTYCKIE
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