PAŃSTWOWY INSTYTUT HYDROLOGICZNO-METEOROLOGICZNY

ROCZNIK METEOROLOGICZNY

1965

ANNUAIRE MÉTÉOROLOGIQUE

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PRZEDMOWA

Układ *Rocznika meteorologicznego 1965* jest taki sam jak rocznika 1964. Materiał obserwacyjny zestawiono w czterech tablicach.

Tablica pierwsza zawiera codzienne spostrzeżenia meteorologiczne, w tablicy drugiej podano wyniki miesięczne i roczne spostrzeżeń meteorologicznych, w tablicy trzeciej zestawiono daty ostatnich przymrozków wiosennych i pierwszych przymrozków jesiennych (według spostrzeżen dokonywanych w klatce meteorologicznej — 2 m nad powierzchnią gruntu), zaś w tablicy czwartej — dzienne i miesięczne sumy godzin usłonecznienia.

Uzupełnienie stanowią objaśnienia, wykaz symboli meteorologicznych, skorowidz i mapa rozmieszczenia stacji.

Rocznik został opracowany w Ośrodku Gromadzenia i Rozpowszechniania Danych PIHM pod kierownictwem i redakcją mgr Feliksa Janiszewskiego; tablicę czwartą (*Usłonecznienie*) opracowała mgr Lutosława Kuczmarska.

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PRÉFACE

La composition de *l'Annuaire Météorologique 1965* est analogue à celle de l'annuaire 1964. Le données d'observations y sont recueillies dans quatre tableaux.

Le premier tableau contiént les observations journalières des stations météorologiques, le second — les résultats mensuels et annuels, le troisième présente les dates des dernières gelées printanières ainsi que les premières gelées d'automne d'après les observations executées sous l'abri météorologique (2 m au dessus de la surface du sol), le quatrième tableau continient les valeurs diurnes et mensueles d'insolation (en heures).

Les explications, le relevé des symboles météorologiques, ainsi que le répertoire alphabétique et la carte de la répartition des stations font le supplement de l'annuaire.

L'annuaire a été elaboré dans le Centre de Ressemblement et de Distribution des Données de l'Institut Hydrologique et Météorologique d'État sous la direction de Mr Feliks Janiszewski, rédacteur de l'annuaire. Le quatrième tableau (*Insolation*) a été elaboré par Mme Lutosława Kuczmarska.

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OBJAŚNIENIA

Użyte w niniejszym roczniku symbole mają następujące znaczenie:

φ — szerokość geograficzna.

λ — długość geograficzna.

H_s — wysokość terenu ogródka meteorologicznego nad średnim poziomem morza.

H_b — wysokość barometru nad średnim poziomem morza.

Dla stacji posiadających barometry H_s i H_b zostały wyznaczne za pomocą niwelacji, dla pozostałych stacji H_s wyznaczono z mapy topograficznej.

h_w — wysokość wiatromierza nad powierzchnią gruntu.

m — w połączeniu z literowym symbolem elementu oznacza wartość średnią miesięczną (np. U_m oznacza średnią miesięczną wilgotność względną).

P — ciśnienie atmosferyczne w milibarach, zredukowane do 0° i do ciężkości normalnej.

$P_{o,m}$ — wartość średnia miesięczna ciśnienia atmosferycznego, sprowadzona do średniego poziomu morza.

T — temperatura w °C.

Temperaturę wyznaczano za pomocą termometrów umieszczonych w klatce meteorologicznej typu angielskiego na wysokości 2 m nad powierzchnią gruntu. Skrajne dobowe wartości temperatur odnoszą się do okresu od III obserwacji dnia poprzedniego do III obserwacji danego dnia.

$\overline{\text{Max}}$ — średnia miesięczna z wartości temperatur maksymalnych dobowych.

$\overline{\text{Min}}$ — średnia miesięczna z wartości temperatur minimalnych dobowych.

e — prężność pary wodnej w milibarach

U — wilgotność względna w procentach.

Δ — niedosyt wilgotności w milibarach.

N — zachmurzenie w skali 11-stopniowej (przy tym 0 oznacza niebo bezchmurne, zaś 10 — niebo całkowicie pokryte chmurami).

W tablicy I rocznika obok wartości zachmurzenia podane są za pomocą symboli również dane o zjawiskach zaobserwowanych podczas obserwacji terminowych.

D — kierunek wiatru.

v — prędkość wiatru w m/sek.

n_D — częstotliwość występowania poszczególnych kierunków wiatru.

v_{mD} — średnia prędkość wiatru wg kierunków.

Obserwacje nad wiatrem były dokonywane (z nielicznymi wyjątkami) przy użyciu wiatromierzy Wilda.

R — wysokość opadu w milimetrach.

Wysokość opadu odnosi się do okresu od I (porannej) obserwacji jednego dnia do I obserwacji dnia następnego i jest podawana pod datą dnia poprzedniego. Obserwacje te były dokonywane za pomocą deszczomierzy Hellmanna o powierzchni otworu 200 cm², umieszczonych na wysokości 1 m nad powierzchnią gruntu, z wyjątkiem części stacji górskich, położonych powyżej 500 m nad poziomem morza, gdzie używa się deszczomierzy typu górskiego, mających powierzchnię otworu 500 cm² i umieszczonych na wysokości 1,5 m nad powierzchnią gruntu.

V — widzialność z II terminu obserwacji, wyrażona w następującej skali międzynarodowej:

0 — przedmioty są niewidoczne już z odległości mniejszej od 50 m;

1 — przedmioty są widoczne z odległości 50 m, lecz niewidoczne z odległości 200 m;

2 — przedmioty są widoczne z odległości 200 m, lecz niewidoczne z odległości 500 m;

3 — przedmioty są widoczne z odległości 500 m, lecz niewidoczne z odległości 1 km;

4 — przedmioty są widoczne z odległości 1 km, lecz niewidoczne z odległości 2 km;

5 — przedmioty są widoczne z odległości 2 km, lecz niewidoczne z odległości 4 km;

6 — przedmioty są widoczne z odległości 4 km, lecz niewidoczne z odległości 10 km;

7 — przedmioty są widoczne z odległości 10 km, lecz niewidoczne z odległości 20 km;

8 — przedmioty są widoczne z odległości 20 km, lecz niewidoczne z odległości 50 km;

9 — przedmioty są widoczne z odległości 50 km i więcej.

h — grubość pokrywy śnieżnej w centymetrach wg obserwacji dokonywanych w I terminie.

pł. — śnieg w płatach.

Usłonecznienie — w godzinach. Obserwacji dokonywano za pomocą heliografów Campbell—Stokes'a.

n — liczba dni z poszczególnymi zjawiskami.

Za dzień z mgłą przyjęto w niniejszym roczniku dzień, w którym to zjawisko powodowało zmniejszenie się widzialności poniżej 1 km.

Za dni pogodne uważa się takie, w których średnia wartość zachmurzenia wyznaczona z trzech terminów jest mniejsza od 2.0, zaś za dni pochmurne — w których wartość ta jest większa od 8.0.

I, II, III — terminy obserwacji (7^h, 13^h i 21^h średniego miejscowego czasu słonecznego).

Dies — średnia dobowa, obliczona dla temperatury według wzoru:

śr. = 1/4 (I + II + 2 × III), a dla pozostałych elementów śr. = 1/3 (I + II + III).

Natężenie zjawisk oznaczono za pomocą małych cyferek: ^{0}, ^{1} albo ^{2} umieszczonych z prawej strony u góry odpowiedniego symbolu („^{0}" oznacza zjawisko o natężeniu słabym, „^{1}" o natężeniu umiarkowanym, a „^{2}" o natężeniu silnym; w przypadku mgły cyferki te oznaczają odpowiednio: mgłę umiarkowaną, mgłę gęstą i mgłę bardzo gęstą).

Do oznaczania czasu obok godzin i minut użyto następujących symboli:

n — czas od III obserwacji dnia poprzedniego do I obserwacji dnia danego,

na — czas od północy do I obserwacji dnia danego,

a — czas między I a II terminem obserwacji,

p — czas między II a III terminem obserwacji,

np — czas od III obserwacji do północy.

Przerwy w czasie trwania zjawiska oznaczono wielokropkiem (...) lub skrótem „z prz.".

Kropka (.) postawiona na miejscu wartości liczbowej oznacza brak zjawiska, kreska (—) zaś brak danych, wartości wątpliwe podano ze znakiem zapytania (?), wartości oszacowane podano w nawiasach.

NOTE EXPLICATIVE

Les symboles employés dans le présent annuaire signifient ce qui suit:

φ — latitude géographique.

λ — longitude géographique.

H_s — hauteur du terrain du jardin météorologique, au-dessus du niveau moyen de la mer.

H_b — hauteur du baromètre au-dessus du niveau de la mer.

Pour les stations disposant d'un baromètre H_s et H_b, ces données ont été déterminées à l'aide de nivellement, pour les autres stations H_s elles l'ont été d'après la carte topograhique.

h_w — hauteur d'une girouette au-dessus du sol.

m — joint à une lettre-symbole de l'élément, indique la valeur mensuelle moyenne (p.e. U_m — indique la valeur mensuelle moyenne de l'humidité relative).

P — pression atmosphérique en millibars, réduite à 0° et à la gravité normale.

$P_{o,m}$ — moyenne d'une valeur mensuelle de la pression atmosphérique réduite au niveau moyen de la mer.

T — température en C°.

La température a été mesurée à l'aide de thermomètres installés dans un abri météorologique du type anglais à une hauteur de 2 mètres au-dessus du sol. Les températures diurnes extrêmes se rapportent à une période partant de la III-ème observation du jour précédent à la III-ème observation du jour donné.

$\overline{Max}$ — valeur mensuelle moyenne des maxima des températures diurnes.

$\overline{Min}$ — valeur mensuelle moyenne des valeurs minima des températures diurnes.

e — tension de vapeur, en millibars.

U — humidité relative en %.

Δ — déficit de l'humidité en millibars.

N — nébulosité en échelle 11° (0 signifie ciel serein, 10 — ciel entièrement couvert par les nuages). Dans la table I de l'annuaire, à côté des valeurs de la nébulosité, figurent aussi les données se rapportant aux phénomènes remarqués au cours des observations normales, et consignées à l'aide de symboles.

D — direction du vent.

v — vitesse du vent en m/sec.

n_D — fréquence de l'apparition des directions du vent.

v_{mD} — vitesse moyenne du vent selon la direction. Les observations sur le vent ont été faites (avec quelques exceptions) à l'aide d'une girouette, modèle Wild.

R — hauteur de la précipitation en mm. L'hauteur de la précipitation se rapporte à la période comprise entre la première observation (matinale) d'un jour et l'observation du jour suivant. Elle se trouve inscrite à la date du jour précédent. Ces observations ont été faites à l'aide de pluviomètres, modèle Hellmann, dont la superficie de l'ouverture mesure 200 cm², placés à 1 m au-dessus du sol, à l'exception, toutefois, de certaines stations de montagne, situées à une hauteur qui dépasse 500 m au-dessus du niveau de la mer, où l'on emploie des pluviomètres, de type montagnard, à orifice mesurant 500 cm² et placés à une hauter de 1,5 m au-dessus du sol.

V — visibilité à l'heure de la II-ème observation, exprimée d'après l'échelle internationale:

0 — les objets sont invisibles déjà à une distance inférieure à 50 m;

1 — les objets sont visibles à 50 m, mais invisibles à 200 m de distance;

2 — les objets sont visibles à 200 m, mais invisibles à 500 m de distance;

3 — les objets sont visibles à 500 m, mais invisibles à 1000 m de distance;

4 — les objets sont visibles à 1 km, mais invisibles à 2 km;

5 — les objets sont visibles à 2 km, mais invisibles à 4 km;

6 — les objets sont visibles à 4 km, mais invisibles à 10 km;

7 — les objets sont visibles à 10 km, mais invisibles à 20 km;

8 — les objets sont visibles à 20 km, mais invisibles à 50 km;

9 — les objets sont visibles à partir de 50 km de distance.

h — épaisseur de la couche de neige en centimètres selon l'observation enregistrée dans le premier délai.

pl. — neige éparse.

Insolation — en heures. Les observations effectuées à l'aide d'héliographes Campbell — Stokes.

n — nombre des jours avec phénomènes particuliers.

Dans le présent annuaire, on entend par jour avec brouillard le jour où ce phénomène entraine une diminution de visibilité au-dessous de 1 km.

Dans le présent annuaire, on entend par jours sereins les jours dont la valeur moyenne de nébulosité, résultant de trois delais, est inférieure à 2.0 et par jours couverts les jours où cette valeur est supérieure à 8.0.

I, II, III — les délais d'observations (7^h, 13^h et 21^h du temps moyen solaire local).

Dies — moyenne diurne, calculée pour la température d'après la formule:

$m = 1/4\ (I + II + 2 \times III)$, et pour les autres éléments $m = 1/3\ (I + II + III)$.

L'intensité du phénomène est marquée en petits chiffres: ^{0}, ^{1} ou ^{2} placés du coté droit en haut du symbole respectif: („^{0}" indique le phénomène dont l'intensité est faible, „^{1}" modérée et „^{2}" forte; en cas de brouillard modéré, brouillard épais et brouillard très épais).

Pour indiquer le temps (à part les heures et les minutes), on a utilisé les symboles suivants:

n — le temps écoulé depuis la III-ème observation du jour précédent jusqu'à la I-ère observation du jour donné.

na — le temps écoulé depuis minuit jusqu'à l'observation du jour donné,

a — intervalle de temps entre la I-ère et la II-ème observation,

p — intervalle de temps entre la II-ème et la III-ème observation,

np — intervalle de temps entre la III-ème observation et minuit.

Les intervalles de temps, dans la durée d'un phénomène sont indiqués par des points de suspension (...) ou par une abréviation „z prz.".

Un point (.) mis à la place d'une valeur numérique marque l'absence d'un phénomène; un trait d'union (—) indique le défaut de données; un point d'interrogation (?) signale les valeurs douteuses; les parenthèses enferment les valeurs éstimées.

WYKAZ SYMBOLI METEOROLOGICZNYCH

- deszcz
- deszcz marznący
- mżawka
- mżawka marznąca
- śnieg
- śnieg z deszczem
- krupy śnieżne
- śnieg ziarnisty
- ziarna lodowe
- grad
- słupki lodowe
- (pod symbolem opadu) opad przelotny
- mgła
- mgła lodowa
- mgła, niebo widoczne
- mgła w ławicach
- zamglenie
- mgła przyziemna
- morze mgieł
- zamieć śnieżna niska
- zamieć śnieżna wysoka
- pył wodny
- rosa
- szron
- sadź
- gołoledź
- trąba
- zmętnienie opalizujące
- zmętnienie pyłowe
- dymy
- zamieć pyłowa niska lub zamieć piaskowa niska
- zamieć pyłowa wysoka lub zamieć piaskowa wysoka
- wichura pyłowa lub wichura piaskowa
- wir pyłowy lub wir piaskowy
- halo słoneczne
- halo księżycowe
- wieniec wokół Słońca
- wieniec wokół Księżyca
- iryzacja
- gloria
- tęcza
- biała tęcza
- pierścień Bishopa
- miraż
- burza
- burza odległa
- błyskawica
- ognie św. Elma
- zorza polarna
- pokrywa śnieżna
- Słońce
- wiatr 10—15 m/sek
- wiatr > 15 m/sek
- ( ) przejrzyste powietrze
- dni pogodne
- dni pochmurne

ALFABETYCZNY SPIS STACJI METEOROLOGICZNYCH

LISTE ALPHABÉTIQUE DES STATIONS MÉTÉOROLOGIQUES

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
1	Aleksandrowice	I-XII	-	368	412	-	49°48'	19°00'	398	403,4	Wisła
2	Antołówka 1).....	I-XII	-	402	412	-	49°18'	19°59'	918	-	Dunajec
3	Augustów	I-XII	-	234	412	-	53°50'	22°58'	130	-	Biebrza
4	Babia Góra 1).....	I-XII	-	382	412	-	49°35'	19°31'	1180	-	Skawa
5	Baligród	I-XII	-	400	412	-	49°20'	22°17'	450	-	San
6	Bartoszyce	I-XII	-	218	412	-	54°15'	20°48'	60	-	Łyna
7	Barwinek	I-XII	-	396	412	-	49°26'	21°41'	420	-	Wisłoka
8	Belsk	I-XII	-	290	412	418(37)	51°50'	20°48'	180	-	Wisła
9	Biała Podlaska	I-XII	-	288	412	-	52°01'	23°08'	145	-	Bug
10	Białowieża	I-XII	-	264	412	418(42)	52°42'	23°51'	163	163,7	Narew
11	Biały Kościół	I-XII	-	354	412	-	50°10'	19°50'	400	-	Prądnik
12	Białystok	I-XII	-	254	412	418(17)	53°07'	23°11'	139	140,8	Narew
13	Biebrza	I-XII	-	240	412	418(16)	53°39'	22°36'	117	-	Biebrza
14	Biecz	I-XII	-	372	412	-	49°44'	21°15'	260	-	Wisłoka
15	Bielsk Podlaski	I-XII	-	262	412	-	52°47'	23°11'	145	-	Narew
16	Bieruń Stary	I-XII	-	358	412	-	50°05'	19°05'	236	239,0	Wisła
17	Bierutowice (Wang) 1)..	I-XII	-	326	412	-	50°47'	15°44'	860	-	Bóbr
18	Biłgoraj	I-VII, IX-XII	-	336	412	-	50°33'	22°43'	190	-	San
19	Bircza	I-XII	-	376	412	-	49°41'	22°29'	300	-	San
20	Biskupiec	I-XII	-	234	412	-	53°52'	20°57'	160	-	Łyna
21	Bochnia-Chodenice	I-XII	-	364	412	-	49°59'	20°24'	200	-	Raba
22	Bodzentyn	I-XII	-	318	412	-	30°57'	20°57'	270	-	Kamienna
23	Bolesławiec	I-XII	-	306	412	-	51°16'	15°35'	208	-	Bóbr
24	Borusowa	I-XII	-	350	412	-	50°17'	20°47'	170	-	Wisła
25	Brwinów	I-XII	-	284	412	418(32)	52°08'	20°43'	96	98,0	Bzura
26	Brzegi Dolne	I-XII	-	392	412	-	49°27'	22°38'	420	-	Strwiąż
27	Brzezna	I-XII	-	380	412	-	49°36'	20°37'	320	-	Dunajec
28	Bukowina Tatrzańska 1).	I-XII	-	398	412	-	49°21'	20°07'	880	-	Dunajec
29	Busko-Zdrój	I-XII	-	338	412	-	50°27'	20°43'	225	-	Nida
30	Bydgoszcz	I-XII	-	254	412	-	53°07'	17°58'	70	72,1	Brda
31	Bydgoszcz, IMiUZ	I-XII	-	252	412	418(13)	53°08'	18°01'	47	-	Brda
32	Bystrzyca Kłodzka	I-XII	-	346	412	-	50°18'	16°39'	370	-	Nysa Kłodzka
33	Bytom	I-XII	-	344	412	-	50°21'	18°55'	300	-	Przemsza
34	Chełm Lubelski	I-XII	-	314	412	418(46)	51°07'	23°30'	208	209,6	Bug
35	Chodzież	I-XII	-	258	412	-	52°59'	16°54'	100	-	Noteć
36	Chojnice	I-XII	52	238	412	418(6)	53°42'	17°33'	172	177,2	Brda
37	Chorzelów	I-XII	-	344	412	-	50°21'	21°27'	170	-	Wisła
38	Ciechocinek	I-XII	-	260	412	418(26)	52°53'	18°48'	44	-	Wisła
39	Cieplice Śl.-Zdrój ...	I-XII	-	322	412	-	50°52'	15°41'	345	-	Bóbr
40	Cieszyn-Bobrek	I-XII	-	372	412	418(55)	49°45'	18°39'	300	-	Olza
41	Ciężkowice	I-XII	-	370	412	-	49°47'	20°58'	280	-	Dunajec
42	Czarna Dąbrówka	I-XII	-	216	412	-	54°21'	17°34'	120	-	Łupawa
43	Czarniecka Góra	I-XII	-	312	412	-	51°08'	20°31'	256	-	Pilica
44	Czarny Dunajec	I-XII	-	390	412	-	49°27'	19°51'	676	-	Dunajec
45	Czernichów	I-XII	-	364	412	-	50°00'	19°41'	218	-	Wisła
46	Częstochowa	I-XII	-	324	412	-	50°49'	19°06'	261	262,7	Warta

1) Podane w roczniku wysokości opadów otrzymano za pomocą deszczomierza o powierzchni otworu 500 cm^2.

2) W nawiasach podane są numery, pod którymi figurują stacje w tabl. IV.

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
47	Czorsztyn	I-XII	-	392	412	-	49°26'	20°19'	496	-	Dunajec
48	Czoraztyn-Nadzamcze 1).	I-XII	-	392	412	-	49°26'	20°20'	650	-	Dunajec
49	Darłowo	I-XII	-	214	412	-	54°27'	16°23'	3	-	Wieprza
50	Dębica	I-XII	-	360	412	-	50°03'	21°24'	205	-	Wisłoka
51	Długopole-Zdrój	I-XII	-	350	412	-	50°15'	16°38'	420	-	Nysa Kłodzka
52	Dobrogoszcz	I-XII	-	326	412	-	50°46'	17°01'	175	-	Oława
53	Dolina Chochołowska 1).	I-XII	-	404	412	-	49°15'	19°49'	1028	-	Dunajec
54	Dolina Pięciu Stawów .	I-XII	-	406	412	-	49°13'	20°03'	1668	-	Dunajec
55	Duszniki-Zdrój 1).....	I-XII	-	340	412	-	50°24'	16°24'	540	-	Nysa Kłodzka
56	Dynów	I-XII	-	370	412	-	49°48'	22°14'	276	-	San
57	Dziwnów	I-XII	-	228	412	-	54°01'	14°44'	7	7,1	Przymorze
58	Elbląg	I-XII	-	222	412	-	54°10'	19°26'	38	42,8	Elbląża
59	Felin	I-XII	-	308	412	-	51°14'	22°38'	215	-	Wieprz
60	Garlica Murowana	I-XII	-	354	412	-	50°09'	19°56'	270	-	Prądnik
61	Gdańsk-Nowy Port	I-XII	-	214	412	-	54°24'	18°40'	7	-	Wisła
62	Gdańsk-Wrzeszcz	I-XII	16	214	412	-	54°23'	18°36'	13	12,4	Wisła
63	Gdynia	I-XII	-	212	412	418(8)	54°31'	18°34'	2	14,5	Przymorze
64	Giżycko	I-XII	-	226	412	-	54°03'	21°46'	132	-	Węgorapa
65	Gliwice	I-XII	-	348	412	-	50°18'	18°40'	220	-	Kłodnica
66	Głodowo	I-XII	-	260	412	-	52°50'	19°15'	129	-	Wisła
67	Głogów	I-XII	-	296	412	-	51°39'	16°06'	112	-	Odra
68	Głubczyce	I-XII	-	352	412	-	50°12'	17°50'	280	-	Odra
69	Głuchołazy	I-XII	-	346	412	-	50°18'	17°23'	344	-	Nysa Kłodzka
70	Gniezno	I-XII	-	268	412	-	52°33'	17°36'	110	-	Wełna
71	Gołdap	I-XII	-	218	412	-	54°19'	22°19'	150	-	Węgorapa
72	Gorzów Wlkp.	I-XII	-	262	412	418(18)	52°44'	15°15'	65	59,7	Warta
73	Gorzyń	I-XII	-	266	412	-	52°34'	15°54'	60	-	Warta
74	Goszyce	I-XII	-	352	412	-	50°11'	20°08'	260	-	Wisła
75	Grabowiec	I-XII	-	314	412	-	51°06'	21°23'	210	-	Wisła
76	Grabownica	I-XII	-	300	412	-	51°28'	17°27'	119	-	Barycz
77	Grodków	I-XII	-	330	412	-	50°41'	17°23'	176	-	Nysa Kłodzka
78	Grudziądz	I-XII	-	244	412	-	53°30'	18°46'	40	-	Wisła
79	Gryfice	I-XII	-	232	412	-	53°55'	15°13'	40	-	Rega
80	Gubałówka 1).....	I-XII	-	400	412	418(63)	49°18'	19°56'	1000	-	Dunajec
81	Hala Gąsienicowa 1)....	I-XII	-	404	412	418(64)	49°15'	20°00'	1520	1520,8	Dunajec
82	Hala Ornak 1).....	I-XII	-	406	412	-	49°14'	19°51'	1110	-	Dunajec
83	Hel	I-XII	-	210	412	418(7)	54°36'	18°49'	1	2,6	Przymorze
84	Hopowo	I-XII	-	218	412	-	54°16'	18°14'	220	-	Radunia
85	Horyniec	I-XII	-	354	412	-	50°11'	23°21'	240	-	San
86	Inowrocław	I-XII	-	262	412	-	52°48'	18°14'	90	-	Noteć
87	Istebna-Kubalonka 1)...	I-XII	-	378	412	418(56)	49°36'	18°54'	800	-	Olza
88	Istebna-Stecówka 1)....	I-XII	-	380	412	-	49°35'	18°57'	750	-	Wisła
89	Istebna-Zaolzie 1).....	I-XII	-	380	412	-	49°34'	18°56'	580	-	Olza
90	Iwonicz-Zdrój	I-XII	-	384	412	418(68)	49°34'	21°48'	410	-	Wisłok
91	Jabłonka 1).....	I-XII	-	388	412	418(58)	49°28'	19°43'	620	-	Czarna Orawa
92	Jabłonowo Pom.	I-XII	-	216	412	-	53°24'	19°10'	97	-	Osa
93	Jakubowice	I-XII	-	362	412	-	50°01'	17°51'	319	-	Odra

Nr	Stacja – Station	Miesiące Mois	Strona – Page Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)	φ N	λ E Gr.	H_s	H_b	Dorzecze – Basin
94	Janów Lubelski	I-XII	–	330	413	–	50°43′	22°25′	230	–	San
95	Jarosław	I-XII	–	362	413	–	50°01′	22°42′	204	–	San
96	Jasło	I-XII	–	374	413	–	49°44′	21°28′	240	–	Wisłoka
97	Jastrowie	I-XII	–	246	413	–	53°25′	16°48′	120	–	Gwda
98	Jastrzębie-Zdrój	I-XII	–	366	413	–	49°57′	18°34′	227	–	Olza
99	Jaworzyna Krynicka 1)..	I-V,VIII	–	396	413	–	49°25′	20°54′	995	–	Poprad
100	Jazy	I-XII	–	232	413	–	53°53′	23°22′	120	–	Niemen
101	Jelenia Góra	I-XII	124	320	413	–	50°54′	15°48′	342	343,9	Bóbr
102	Jeziory	I-XII	–	278	413	–	52°16′	16°48′	84	–	Warta
103	Kalisz	I-XII	–	294	413	418(39)	51°44′	18°05′	140	144,5	Prosna
104	Kamienica	I-XII	–	382	413	–	49°35′	20°21′	460	–	Dunajec
105	Kamienica Królewska ..	I-XII	–	214	413	–	54°23′	17°54′	160	–	Łupawa
106	Kamień Krajeński	I-XII	–	244	413	–	53°32′	17°32′	124	–	Brda
107	Karpacz 1).....	I-XII	–	326	413	–	50°46′	15°45′	700	708,0	Bóbr
108	Kartuzy	I-XII	–	216	413	–	54°20′	18°12′	220	–	Radunia
109	Kasprowy Wierch 1).....	I-XII	196	406	413	418(65)	49°14′	19°59′	1991	1988,8	Dunajec
110	Katowice	I-XII	–	352	413	–	50°14′	19°02′	284	283,8	Przemsza
111	Kętrzyn I	I-VI	–	224	–	–	54°06′	21°21′	110	–	Łyna
112	Kętrzyn II	I-XII	–	224	413	–	54°05′	21°22′	108	97,2	Łyna
113	Kielce	I-XII	–	322	413	–	50°51′	20°37′	268	270,1	Nida
114	Kisielnica	I-XII	–	250	413	–	53°15′	22°07′	140	–	Narew
115	Kłodzko	I-XII	–	340	413	–	50°26′	16°39′	316	317,3	Nysa Kłodzka
116	Kmiecin	I-XII	–	220	413	–	54°11′	19°10′	0	–	Wisła
117	Kolbaszowa	I-XII	–	352	413	–	50°14′	21°47′	208	–	Wisła
118	Kolno	I-XII	–	246	413	–	53°25′	21°56′	128	–	Pisa
119	Koło	I-XII	–	280	413	–	52°12′	18°38′	95	–	Warta
120	Kołobrzeg	I-XII	–	220	413	418(2)	54°11′	15°35′	3	5,4	Parsęta
121	Komańcza	I-XII	–	400	413	–	49°20′	22°04′	470	–	San
122	Kończewice	I-XII	–	252	413	–	53°11′	18°33′	94	–	Wisła
123	Kopna Góra	I-XII	–	250	413	–	53°15′	23°29′	160	–	Narew
124	Korfantów	I-XII	–	336	413	–	50°29′	17°36′	200	–	Nysa Kłodzka
125	Koszalin	I-XII	–	220	413	–	54°12′	16°10′	33	33,9	Przymorze
126	Kościerzyna	I-XII	–	222	413	–	54°08′	17°58′	180	–	Wierzyca
127	Kórnik	I-XII	–	280	413	418(23)	52°15′	17°06′	77	–	Warta
128	Kraków-Balice	I-XII	–	358	413	–	50°05′	19°48′	237	237,5	Rudawa
129	Kraków-Chełm	I-XII	–	358	413	–	50°04′	19°51′	225	–	Rudawa
130	Kraków-Nowa Huta	I-XII	–	360	413	–	50°04′	20°05′	195	–	Wisła
131	Kraków,Obserw.Astr.UJ.	I-XII	160	360	413	418(54)	50°04′	19°58′	206	219,8	Wisła
132	Krasnystaw	I-XII	–	316	413	–	50°59′	23°10′	190	–	Wieprz
133	Kraśnik Lubelski	I-XII	–	318	413	–	50°55′	22°12′	250	–	Wisła
134	Krosno	I-XII	–	376	413	–	49°41′	21°45′	282	–	Wisłok
135	Krościenko	I-XII	–	392	413	–	49°27′	20°25′	440	–	Dunajec
136	Krynica 1).....	I-XII	–	394	413	418(59)	49°26′	20°58′	613	–	Poprad
137	Krynica-Góra Parkowa 1)	I-XII	–	394	413	418(60)	49°25′	20°58′	740	–	Poprad
138	Krynica Morska	I-XII	–	216	413	–	54°23′	19°27′	4	–	Zalew Wiślany
139	Krzemień	I-XII	–	268	413	–	52°33′	22°30′	111	–	Bug
140	Krzyż	I-XII	–	258	413	–	52°53′	16°01′	31	–	Noteć
141	Kudowa-Zdrój	I-XII	–	338	413	418(50)	50°27′	16°16′	385	–	Łaba
142	Kuźnice 1).....	I-XII	–	402	413	–	49°16′	19°59′	1023	–	Dunajec
143	Kwidzyń	I-XII	–	236	413	–	53°44′	18°55′	15	–	Wisła
144	Laskowice Oławskie ...	I-XII	–	316	413	418(25)	51°03′	17°21′	135	–	Widawa
145	Lądek-Zdrój 1).....	I-XII	–	344	413	–	50°21′	16°53′	460	–	Nysa Kłodzka

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_m	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
146	Legionowo	I-XII	-	272	413	418(28)	52°24'	20°58'	93	103,7	Wisła
147	Legnica	I-XII	-	308	413	-	51°13'	16°10'	121	126,3	Kaczawa
148	Lesko	I-XII	-	390	413	418(69)	49°28'	22°20'	386	375,2	San
149	Leskowiec 1).....	I-XII	-	368	413	-	49°48'	19°27'	870	-	Skawa
150	Leszno-Strzyżewice ...	I-XII	-	290	413	-	51°50'	16°32'	91	92,4	Barycz
151	Leżajsk	I-XII	-	350	413	-	50°15'	22°26'	190	-	San
152	Lębork	I-XII	-	212	413	-	54°33'	17°45'	18	-	Łeba
153	Libertów	I-XII	-	364	413	-	49°58'	19°53'	320	-	Wisła
154	Lidzbark	I-XII	-	250	413	-	53°16'	19°50'	150	-	Drwęca
155	Lidzbark Warmiński ...	I-XII	-	222	413	-	54°08'	20°36'	90	-	Łyna
156	Limanowa	I-XII	-	374	413	-	49°42'	20°25'	440	-	Dunajec
157	Lipki	I-XII	-	248	413	-	53°21'	14°58'	30	-	Odra
158	Lipowa	I-XII	-	324	413	-	50°50'	21°27'	245	-	Wisła
159	Lubaczów	I-XII	-	356	413	-	50°09'	23°08'	214	-	San
160	Lublin	I-XII	-	308	413	-	51°14'	22°34'	171	176,7	Wieprz
161	Lubliniec	I-XII	-	332	413	-	50°40'	18°41'	256		Mała Panew
162	Luboń Wielki 1).....	I-XII	-	378	413	-	49°39'	19°59'	1023	-	Raba
163	Łagiewniki	I-XII	-	264	413	-	52°40'	18°19'	80	-	Noteć
164	Łącko	I-XII	-	386	413	-	49°33'	20°26'	360	-	Dunajec
165	Łeba	I-XII	-	210	413	-	54°46'	17°34'	2	-	Łeba
166	Łosice	I-XII	-	282	413	-	52°12'	22°43'	153	-	Bug
167	Łowicz	I-XII	-	284	413	-	52°07'	19°56'	95	-	Bzura
168	Łódź-Lublinek	I-XII	100	294	413	418(38)	51°44'	19°24'	187	-	Ner
169	Łódź-Ruda Pabianicka .	I-XII	-	296	413	-	51°42'	19°27'	181	-	Ner
170	Łysa Polana 1).....	I-XII	-	404	413	-	49°16'	20°07'	988	-	Dunajec
171	Maków Podhalański	I-XII	-	372	413	-	49°44'	19°40'	350	-	Skawa
172	Malbork	I-XII	-	228	413	-	54°02'	19°02'	20	-	Wisła
173	Maniowy 1).....	I-XII	-	390	413	-	49°28'	20°15'	520	-	Dunajec
174	Miastko	I-XII	-	230	413	-	54°00'	16°58'	145	-	Wieprza
175	Miechów	I-XII	-	342	413	-	50°22'	20°02'	292	-	Wisła
176	Mielec	I-XII	-	348	413	-	50°18'	21°27'	168	170,2	Wisłoka
177	Międzybrodzie Bialskie	I-XII	-	370	413	-	49°47'	19°12'	320	-	Soła
178	Międzylesie	I-XII	-	-	-	418(31)	52°12'	21°11'	90	-	Wisła
179	Międzyzdroje	I-XII	-	230	413	-	53°56'	14°27'	10	-	Przymorze
180	Mikołajki	I-XII	-	234	413	418(15)	53°47'	21°35'	127	131,1	Pisa
181	Mława	I-XII	-	254	413	-	53°07'	20°22'	141	145,8	Wkra
182	Młochów	I-XII	-	286	413	418(35)	52°03'	20°47'	141	-	Bzura
183	Morąg	I-XII	-	232	413	-	53°55'	19°56'	113	-	Drwęca
184	Morskie Oko 1).....	I-XII	-	406	413	-	49°12'	20°04'	1400	-	Dunajec
185	Motycz	I-XII	-	308	413	-	51°15'	22°25'	213	-	Wieprz
186	Mszana Dolna	I-XII	-	376	413	-	49°40'	20°05'	410	-	Raba
187	Muszyna	I-XII	-	398	413	418(61)	49°21'	20°53'	445	447,1	Poprad
188	Myczkowce	I-XII	-	396	413	-	49°26'	22°25'	410	-	San
189	Myślenice	I-XII	-	368	413	-	49°49'	19°56'	295	-	Raba
190	Myślenickie Turnie 1)..	I-XII	-	404	413	-	49°15'	19°59'	1360	-	Dunajec
191	Nałęczów	I-XII	-	306	413	-	51°17'	22°13'	166	-	Wisła
192	Namysłów	I-XII	-	314	413	-	51°05'	17°43'	151	-	Widawa
193	Nidzica	I-XII	-	248	413	-	53°22'	20°25'	170	-	Wkra
194	Niepokalanów	I-XII	-	282	413	-	52°12'	20°25'	92	-	Bzura
195	Nisko	I-XII	-	336	413	-	50°31'	22°09'	164	-	San
196	Nowa Wieś	I-XII	-	302	414	-	51°27'	22°45'	179	-	Wieprz
197	Nowe Miasto n.P.	I-XII	-	298	414	-	51°37'	20°35'	155	-	Pilica

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
198	Nowogard	I-XII	-	240	414	-	53°40′	15°07′	60	-	Przymorze
199	Nowy Dwór Mazowiecki .	I-XII	-	272	414	-	52°26′	20°43′	70	-	Wisła
200	Nowy Sącz	I-XII	-	378	414	-	49°37′	20°42′	292	295,4	Dunajec
201	Nowy Targ 1)	I-XII	-	388	414	-	49°29′	20°02′	600	-	Dunajec
202	Nur	I-XII	-	264	414	-	52°40′	22°19′	110	-	Bug
203	Obidowa 1)	I-XII	-	384	414	-	49°33′	19°58′	800	-	Raba
204	Oborniki Śląskie	I-XII	-	306	414	418(24)	51°18′	16°55′	180	-	Odra
205	Ochaby	I-XII	-	366	414	-	49°51′	18°46′	270	-	Wisła
206	Olecko	I-XII	-	228	414	-	54°03′	22°30′	181	177,7	Biebrza
207	Olesno	I-XII	-	320	414	-	50°53′	18°25′	238	-	Stobrawa
208	Olkusz	I-XII	-	348	414	-	50°17′	19°34′	360	-	Przemsza
209	Olsztyn-Dajtki	I-XII	40	236	414	-	53°46′	20°25′	133	135,4	Łyna
210	Oława-Zwierzyniec	I-XII	-	318	414	-	50°57′	17°18′	137	-	Odra
211	Opocno	I-XII	-	304	414	-	51°23′	20°16′	180	-	Pilica
212	Opole	I-XII	-	332	414	418(49)	50°40′	17°58′	176	177,9	Odra
213	Opole Lubelskie	I-XII	-	310	414	-	51°09′	21°59′	149	-	Wisła
214	Orneta	I-XII	-	222	414	-	54°07′	20°07′	70	-	Pasłęka
215	Ostrołęka	I-XII	-	256	414	-	53°05′	21°34′	95	96,3	Narew
216	Ostroszowice	I-XII	-	332	414	-	50°39′	16°38′	375	-	Nysa Kłodzka
217	Ostrowy	I-XII	-	274	414	-	52°18′	19°10′	120	-	Bzura
218	Ostróda	I-XII	-	240	414	-	53°42′	19°58′	106	-	Drwęca
219	Ostrów Wlkp.	I-XII	-	296	414	-	51°39′	17°49′	126	-	Prosna
220	Ostrzeszów	I-XII	-	302	414	-	51°26′	17°56′	198	-	Prosna
221	Otmuchów	I-XII	-	338	414	-	50°28′	17°10′	211	-	Nysa Kłodzka
222	Ożańsk	I-XII	-	362	414	-	50°01′	22°35′	250	-	San
223	Paproć	I-XII	-	274	414	-	52°19′	16°08′	75	-	Obra
224	Pętkowo	I-XII	-	280	414	-	52°12′	17°15′	86	-	Warta
225	Piaszczyna	I-XII	-	228	414	-	54°01′	17°10′	175	-	Brda
226	Piotrków Trybunalski .	I-XII	-	302	414	-	51°25′	19°42′	200	-	Pilica
227	Pisz	I-XII	-	242	414	-	53°38′	21°48′	118	-	Pisa
228	Piwniczna	I-XII	-	394	414	-	49°26′	20°42′	380	-	Poprad
229	Pleszew	I-XII	-	290	414	-	51°54′	17°47′	120	-	Prosna
230	Plewiska	I-XII	-	-	-	418(22)	52°22′	16°48′	80	-	Warta
231	Płock-Radziwie	I-XII	-	268	414	-	52°32′	19°40′	63	63,8	Wisła
232	Polanica-Zdrój	I-XII	-	342	414	418(51)	50°24′	16°30′	400	-	Nysa Kłodzka
233	Połczyn-Zdrój	I-XII	-	236	414	-	53°46′	16°06′	50	-	Parsęta
234	Porąbka	I-XII	-	368	414	-	49°49′	19°13′	315	-	Soła
235	Poronin 1)	I-XII	-	400	414	-	49°20′	20°02′	800	-	Dunajec
236	Poświętne	I-XII	-	266	414	-	52°38′	20°23′	101	-	Wkra
237	Poturzyn	I-XII	-	334	414	-	50°34′	23°56′	240	-	Bug
238	Poznań-Ławica	I-XII	76	272	414	422(21)	52°25′	16°50′	86	92,1	Warta
239	Poznań-Sołacz	I-XII	-	270	414	-	52°26′	16°54′	71	-	Warta
240	Prabuty	I-XII	-	238	414	418(12)	53°44′	19°13′	98	-	Wisła
241	Prudnik	I-XII	-	346	414	-	50°19′	17°34′	265	-	Odra
242	Przasnysz	I-XII	-	256	414	-	53°01′	20°53′	120	-	Narew
243	Przebędowo	I-XII	-	266	414	422(19)	52°35′	17°01′	82	-	Warta
244	Przedbórz	I-XII	-	314	414	-	51°05′	19°53′	235	-	Pilica
245	Przehyba	I-VIII, X-XII	-	390	414	-	49°28′	20°34′	1175	-	Poprad
246	Przelewice	I-XII	-	254	414	-	53°06′	15°05′	60	-	Odra
247	Przemyśl	I-XII	172	370	414	-	49°48′	22°46′	237	238,9	San
248	Przybroda	I-XII	-	270	414	418(20)	52°31′	16°40′	88	-	Warta
249	Pszczela Wola	I-XII	-	312	414	-	51°07	22°31	195	-	Wieprz

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
250	Pszczyna	I-XII	-	362	414	-	50°00'	18°55'	270	-	Wisła
251	Ptaszkowa 1)	I-XII	-	382	414	-	49°36'	20°53'	522	-	Dunajec
252	Puck	I-XII	-	210	414	-	54°43'	18°25'	1	-	Przymorze
253	Puczniew	I-XII	-	292	414	-	51°47'	19°05'	142	-	Ner
254	Puławy	I-XII	-	304	414	418(45)	51°25'	21°58'	142	-	Wisła
255	Pułtusk	I-XII	-	262	414	-	52°42'	21°06'	80	-	Narew
256	Raba Wyżna 1)	I-XII	-	382	414	-	49°34'	19°53'	600	-	Raba
257	Rabka 1)	I-XII	-	380	414	418(57)	49°37'	19°58'	511	500,8	Raba
258	Racibórz	I-XII	-	358	414	-	50°05'	18°13'	189	192,6	Odra
259	Radom	I-XII	-	304	414	-	51°25'	21°07'	178	178,8	Wisła
260	Radostowo	I-XII	-	230	414	418(11)	53°59'	18°45'	40	-	Wisła
261	Radzyń Podlaski	I-XII	-	292	414	-	51°48'	22°38'	151	-	Wieprz
262	Reguły	I-XII	-	282	414	-	52°10'	20°51'	98	-	Bzura
263	Resko	I-XII	-	234	414	418(4)	53°46'	15°25'	55	56,2	Rega
264	Rosnowo	I-XII	-	226	414	-	54°04'	16°18'	62	-	Parsęta
265	Rozewie	I-XII	-	210	414	-	54°50'	18°20'	54	-	Przymorze
266	Rożnów	I-XII	-	372	414	-	49°46'	20°41'	300	-	Dunajec
267	Różanystok	I-XII	-	242	414	-	53°38'	23°24'	160	-	Biebrza
268	Rybnik	I-XII	-	356	414	-	50°06'	18°33'	243	-	Odra
269	Rymanów-Zdrój	I-XII	-	386	414	-	49°33'	21°51'	360	-	Wisłok
270	Rypin	I-XII	-	256	414	-	53°04'	19°24'	98	-	Drwęca
271	Rzeszów-Jasionka	I-XII	-	356	414	-	50°06'	22°03'	200	201,7	Wisłok
272	Sandomierz	I-XII	148	330	414	-	50°41'	21°45'	202	200,3	Wisła
273	Sanok	I-XII	-	384	414	-	49°34'	22°12'	314	-	San
274	Sejny	I-XII	-	224	414	-	54°06'	23°21'	130	-	Niemen
275	Siedlce	I-XII	-	282	414	-	52°11'	22°16'	146	149,1	Liwiec
276	Sielec	I-XII	-	346	414	-	50°19'	20°25'	202	-	Wisła
277	Siemianice	I-XII	-	310	414	-	51°11'	18°09'	182	-	Prosna
278	Siemiatycze	I-XII	-	272	414	-	52°26'	22°52'	145	-	Bug
279	Sieniawa 1)	I-XII	-	388	414	-	49°32'	19°55'	578	-	Raba
280	Sieradz	I-XII	-	298	414	-	51°36'	18°44'	137	-	Warta
281	Silniczka	I-XII	-	318	414	-	50°55'	19°46'	215	-	Pilica
282	Sirołęka	I-XII	-	280	414	-	52°13'	21°55'	160	-	Liwiec
283	Skierniewice	I-XII	-	288	414	418(36)	51°58'	20°10'	128	129,5	Bzura
284	Skroniów	I-XII	-	334	414	418(52)	50°38'	20°16'	256	-	Nida
285	Słubice	I-XII	-	274	414	-	52°21'	14°36'	21	24,1	Odra
286	Słupca	I-XII	-	274	414	-	52°17'	17°52'	90	-	Warta
287	Słupia Nowa	I-XII	-	322	414	-	50°52'	21°05'	307	-	Kamienna
288	Słupsk	I-XII	-	212	414	-	54°28'	17°01'	16	-	Słupia
289	Smolice	I-XII	-	296	414	-	51°42'	17°11'	107	-	Barycz
290	Smolnik	I-XII	-	402	414	-	49°17'	22°07'	510	-	San
291	Sobieszyn	I-XII	-	298	414	418(44)	51°36'	22°10'	159	-	Wieprz
292	Sokołowsko 1)	I-XII	-	330	414	-	50°41'	16°14'	570	-	Nysa Kłodzka
293	Sokółka	I-XII	-	248	414	-	53°24'	23°30'	180	-	Narew
294	Spalona 1)	I-XII	-	348	414	-	50°17'	16°33'	790	-	Nysa Kłodzka
295	Stańcowa 1)	I-XII	-	384	414	-	49°33'	19°32'	850	-	Czarna Orawa
296	Stare Pole	I-XII	-	226	414	418(10)	54°04'	19°13'	3	-	Wisła
297	Stary Sącz	I-XII	-	386	414	-	49°33'	20°39'	320	-	Poprad
298	Staszów	I-XII	-	334	414	-	50°34'	21°10'	193	-	Wisła
299	Strzelna	I-XII	-	292	414	-	51°49'	19°54'	194	-	Bzura
300	Strzyżów	I-XII	-	324	414	-	50°51'	24°02'	185	-	Bug
301	Suchedniów	I-XII	-	316	415	-	51°02'	20°50'	278	-	Kamienna
302	Sulejów	I-XII	-	304	415	-	51°22'	19°53'	186	-	Pilica
303	Sulęcin	I-XII	-	270	415	-	52°26'	15°07'	80	-	Warta
304	Suwałki	I-XII	28	224	415	418(14)	54°06'	22°57'	165	169,6	Niemen

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_m	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
305	Szczawnica	I-XII	-	394	415	-	49°26′	20°29′	500	-	Dunajec
306	Szczawno-Zdrój	I-XII	-	326	415	418(47)	50°48′	16°16′	415	-	Bystrzyca
307	Szczecin-Dąbie	I-XII	64	244	415	-	53°24′	14°37′	1	6,9	Odra
308	Szczecin-Niebuszewo ..	I-XII	-	244	415	-	53°28′	14°33′	69	-	Odra
309	Szczecinek	I-XII	-	238	415	418(5)	53°43′	16°41′	137	142,6	Gwda
310	Szczekociny	I-XII	-	332	415	-	50°38′	19°49′	262	-	Pilica
311	Szczerców	I-XII	-	306	415	-	51°20′	19°07′	160	-	Warta
312	Szczuczyn	I-XII	-	242	415	-	53°34′	22°17′	130	-	Biebrza
313	Szczytno	I-XII	-	242	415	-	53°34′	21°02′	144	-	Narew
314	Szepietowo	I-XII	-	260	415	418(41)	52°51′	22°33′	150	-	Bug
315	Szklarska Poręba 1)	I-XII	-	324	415	-	50°50′	15°32′	640	-	Bóbr
316	Szprotawa	I-XII	-	300	415	-	51°34′	15°32′	122	-	Bóbr
317	Szymanów	I-XII	-	312	415	-	51°08′	16°29′	145	-	Odra
318	Ślęża	I-XII	-	320	415	-	50°53′	16°43′	718	-	Bystrzyca
319	Śliwice	I-XII	-	238	415	-	53°43′	18°11′	115	-	Czarna Woda
320	Śnieżka 1)	I-XII	136	328	415	418(48)	50°44′	15°44′	1603	1610,6	Bóbr
321	Śrem	I-XII	-	286	415	-	52°05′	17°01′	85	-	Warta
322	Świbno	I-XII	-	216	415	418(9)	54°20′	18°56′	3	-	Wisła
323	Świder	I-XII	-	284	415	418(33)	52°07′	21°15′	94	-	Świder
324	Świdnica	I-XII	-	322	415	-	50°51′	16°29′	230	-	Bystrzyca
325	Świdwin	I-XII	-	236	415	-	53°46′	15°46′	94	-	Rega
326	Świebodzin	I-XII	-	278	415	-	52°15′	15°32′	78	-	Odra
327	Świeradów-Zdrój	I-XII	-	320	415	-	50°54′	15°20′	549	-	Bóbr
328	Świerklaniec	I-XII	-	340	415	418(53)	50°26′	18°57′	284	-	Przemsza
329	Świnoujście	I-XII	-	230	415	418(3)	53°55′	14°14′	6	5,4	Przymorze
330	Tarnobrzeg	I-XII	-	334	415	-	50°34′	21°40′	175	-	Wisła
331	Tarnogród	I-XII	-	344	415	-	50°22′	22°45′	217	-	San
332	Tarnów	I-XII	-	360	415	-	50°02′	20°59′	209	209,1	Dunajec
333	Tczew	I-XII	-	226	415	-	54°05′	18°48′	10	-	Wisła
334	Terespol	I-XII	-	286	415	418(43)	52°05′	23°37′	133	135,0	Bug
335	Tęgoborze	I-XII	-	374	415	-	49°43′	20°39′	272	-	Dunajec
336	Tolkmicko	I-XII	-	218	415	-	54°19′	19°32′	1	-	Zalew Wiślany
337	Tomaszów Lubelski I ..	I-V	-	338	415	-	50°27′	23°25′	273	-	Bug
338	Tomaszów Lubelski II .	I-XII	-	340	415	-	50°27′	23°24′	270	-	Bug
339	Topola-Błonie	I-XII	-	286	415	418(34)	52°05′	19°11′	109	-	Ner
340	Toruń-Wrzosy	I-XII	-	256	415	-	53°03′	18°35′	69	70,2	Wisła
341	Trzcińsko-Zdrój	I-XII	-	258	415	-	52°58′	14°36′	60	-	Odra
342	Trzebiechów	I-XII	-	288	415	-	52°01′	15°44′	55	-	Obrzyca
343	Trzebież	I-XII	-	240	415	-	53°40′	14°31′	1	-	Zalew Szczeciński
344	Trzebinia	I-XII	-	354	415	-	50°10′	19°28′	320	-	Wisła
345	Trzemeszno	I-IX	-	268	415	-	52°34′	17°49′	105	-	Noteć
346	Turbacz 1)	I-XII	-	386	415	-	49°33′	20°07′	1308	-	Raba
347	Tychy	I-XII	-	356	415	-	50°08′	18°59′	280	-	Wisła
348	Tykocin	I-XII	-	252	415	-	53°12′	22°47′	120	-	Narew
349	Ustka	I-XII	-	212	415	418(1)	54°35′	16°52′	6	8,1	Słupia
350	Ustrzyki Górne 1)	I-XII	-	408	415	-	49°07′	22°40′	650	-	San
351	Wadowice	I-XII	-	366	415	-	49°53′	19°31′	260	-	Skawa
352	Wałcz	I-XII	-	250	415	-	53°17′	16°28′	111	117,6	Gwda
353	Warka	I-XII	-	294	415	-	51°47′	21°12′	120	-	Pilica
354	Warszawa-Bielany	I-XII	88	276	415	418(29)	52°17′	20°58′	98	99,5	Wisła

Nr	Stacja - Station	Miesiące Mois	Strona - Page				φ N	λ E Gr.	H_s	H_b	Dorzecze - Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV 2)					
355	Warszawa, Inst. Geogr. UW	I-XII	-	276	415	-	52°14′	21°01′	108	-	Wisła
356	Warszawa, Min. Kom.	I-XII	-	-	-	418(30)	52°13′	21°01′	?	-	Wisła
357	Warszawa, Obserw. Astr. UW	I-XII	-	276	415	-	52°13′	21°02′	110	114,8	Wisła
358	Warszawa-Okęcie	I-XII	-	278	415	-	52°09′	20°59′	106	106,9	Wisła
359	Warszawa, St. Pomp Rz. .	I-XII	-	276	415	-	52°13′	21°03′	85	-	Wisła
360	Wądołki Borowe	I-XII	-	258	415	-	52°57′	22°13′	130	-	Narew
361	Werbkowice	I-XII	-	328	415	418(66)	50°45′	23°46′	204	-	Bug
362	Wielichowo	I-XII	-	284	415	-	52°07′	16°21′	65	-	Obra
363	Wieliczka	I-XII	-	364	415	-	50°00′	20°03′	225	-	Wisła
364	Wieliszew	I-XII	-	270	415	-	52°27′	20°58′	78	-	Bug
365	Wieluń	I-XII	-	310	415	418(40)	51°13′	18°35′	195	198,4	Warta
366	Wieniec-Zdrój	I-XII	-	264	415	-	52°40′	19°00′	82	-	Wisła
367	Wierzchowo	I-XII	-	246	415	-	53°27′	16°06′	140	-	Drawa
368	Więcławice	I-XII	-	260	415	418(27)	52°51′	18°19′	90	-	Noteć
369	Wińsko	I-XII	-	300	415	-	51°28′	16°37′	180	-	Barycz
370	Wirty	I-XII	-	232	415	-	53°54′	18°23′	121	-	Wierzyca
371	Wisła	I-XII	-	376	415	-	49°39′	18°52′	430	-	Wisła
372	Wisznice	I-XII	-	294	415	-	51°47′	23°13′	152	-	Bug
373	Witów 1)	I-XII	-	398	415	-	49°20′	19°50′	835	-	Dunajec
374	Włodawa	I-XII	-	300	415	-	51°33′	23°33′	175	175,9	Bug
375	Wojcieszów Górny	I-XII	-	316	415	-	50°57′	15°55′	358	-	Kaczawa
376	Wolbrom	I-XII	-	342	415	-	50°23′	19°45′	373	-	Przemsza
377	Wrocław-Strachowice ..	I-XII	112	312	415	-	51°06′	16°53′	120	123,8	Odra
378	Wschowa	I-XII	-	290	415	-	51°49′	16°19′	108	-	Odra
379	Wyrzysk	I-XII	-	252	415	-	53°09′	17°16′	90	-	Noteć
380	Wysowa 1)	I-XII	-	396	415	-	49°26′	21°11′	525	-	Wisłoka
381	Wyszków	I-XII	-	266	415	-	52°35′	21°27′	96	-	Bug
382	Zakopane 1)	I-XII	184	402	415	418(62)	49°18′	19°57′	844	838,2	Dunajec
383	Zakrzów	I-XII	-	350	415	-	50°16′	18°09′	217	-	Odra
384	Zamość	I-XII	-	328	415	-	50°42′	23°15′	212	213,2	Wieprz
385	Zawiercie	I-XII	-	336	415	-	50°29′	19°26′	335	-	Warta
386	Zawodzie	I-XII	-	248	415	-	53°23′	21°24′	122	-	Narew
387	Zawoja 1)	I-XII	-	378	415	-	49°37′	19°31′	670	-	Skawa
388	Zawołocze	I-XII	-	302	415	-	51°26′	23°34′	165	-	Bug
389	Ząbkowice	I-XII	-	342	415	-	50°22′	19°17′	314	-	Przemsza
390	Zbąszyń	I-XII	-	278	415	-	52°15′	15°56′	57	-	Odra
391	Zdanów	I-XII	-	328	415	418(67)	50°43′	21°33′	236	-	Wisła
392	Zgorzelec	I-XII	-	310	415	-	51°08′	15°02′	203	202,2	Nysa Łużycka
393	Zielona Góra	I-XII	-	288	415	-	51°56′	15°30′	180	173,8	Odra
394	Zwardoń 1)	I-XII	-	388	415	-	49°30′	18°59′	690	-	Soła
395	Żarnowa	I-XII	-	366	415	-	49°52′	21°50′	256	-	Wisłok
396	Żary	I-XII	-	298	415	-	51°38′	15°08′	162	-	Bóbr
397	Żegiestów-Zdrój	I-XII	-	398	415	-	49°22′	20°49′	440	-	Poprad
398	Żelechów	I-XII	-	292	415	-	51°49′	21°54′	175	-	Wisła
399	Żelisławki	I-XII	-	220	415	-	54°10′	18°39′	68	-	Wisła
400	Żywiec-Sporysz	I-XII	-	374	415	-	49°41′	19°13′	360	-	Soła

1965

TABLICA I

SPOSTRZEŻENIA CODZIENNE STACJI METEOROLOGICZNYCH

OBSERVATIONS DIURNES DE STATIONS MÉTÉOROLOGIQUES

1. Gdańsk-Wrzeszcz
2. Suwałki
3. Olsztyn-Dajtki
4. Chojnice
5. Szczecin-Dąbie
6. Poznań-Ławica
7. Warszawa-Bielany
8. Łódź-Lublinek
9. Wrocław-Gądów Mały
10. Jelenia Góra
11. Śnieżka, Obserwatorium Wysokogórskie
12. Sandomierz
13. Kraków, Obserwatorium Astronomiczne UJ
14. Przemyśl
15. Zakopane
16. Kasprowy Wierch, Obserwatorium Wysokogórskie

Gdańsk – Wrzeszcz φ = 54°23' λ = 18°36' Styczeń – Janvier 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	94.7	95.6	96.2	95.5	3.6	4.9	4.3	4.3	5.8	2.2	86	75	77	79	1.1	2.2	1.9	1.7	6	4	0	SW 7	SW 10	SW 9
2	95.6	96.2	98.2	96.7	3.1	4.0	2.8	3.2	4.5	1.8	85	75	84	81	1.3	2.0	1.2	1.5	4	8	7	SW 3	SW 5	S 4
3	101.9	105.1	110.0	105.7	2.0	2.7	0.1	1.2	3.1	-0.3	80	79	94	84	1.5	1.5	0.4	1.1	8	8	9	SW 4	W 4	NW 1
4	115.4	118.9	118.4	117.6	0.4	2.0	-0.7	0.2	2.2	-1.7	78	64	79	74	1.4	2.6	1.2	1.7	9	3	0	NW 3	NNW 5	SW 5
5	102.9	108.9	113.8	108.5	2.5	1.6	0.8	1.4	2.6	-1.5	89	78	75	80	0.8	1.6	1.8	1.4	10 ⚹	2	3	WSW10	NW 7	NNW 8
6	118.2	120.2	121.2	119.9	-0.6	-0.7	-0.6	-0.6	1.1	-2.0	72	85	70	76	1.7	0.9	1.8	1.5	8	9 *	9	NNW 8	NNW 8	N 15
7	121.7	120.9	114.4	119.0	-0.5	-0.6	-1.9	-1.2	0.1	-3.0	68	70	67	68	1.9	1.8	1.8	1.8	9 *	7	9	NNW 7	WNW 6	SW 6
8	102.7	98.6	91.1	97.5	0.7	3.4	5.2	3.6	5.4	-2.5	85	91	89	88	1.0	0.7	0.9	0.9	10	10 •	10 •	SW 9	SW 8	W 10
9	96.6	100.0	102.9	99.8	4.2	3.2	-0.7	1.5	5.5	-0.8	85	90	91	89	1.2	0.8	0.5	0.8	10	10	10 *	W 9	NW 3	ENE 3
10	104.8	111.8	121.4	112.7	-4.6	-6.1	-5.9	-5.6	-0.4	-6.8	88	79	76	81	0.5	0.8	0.9	0.7	10 *	10 *	10	NE 7	NE 5	SSW 3
11	125.1	122.6	118.6	122.1	-10.1	-7.5	-5.2	-7.0	-4.9	-11.2	78	73	83	78	0.6	0.9	0.7	0.7	0	7	4	S 2	S 7	SSE 7
12	116.1	114.6	111.7	114.1	-4.4	-1.3	-1.8	-2.3	-0.6	-5.4	86	80	83	83	0.6	1.1	0.9	0.9	0	9	9	S 5	S 4	S 3
13	110.2	110.6	113.4	111.4	-1.4	1.8	2.2	1.2	3.1	-1.8	82	78	86	82	1.0	1.6	1.1	1.2	6	9	3	S 5	S 3	C 0
14	110.7	107.9	108.5	109.0	-0.2	1.9	1.9	1.4	2.6	-0.8	96	80	82	86	0.2	1.4	1.3	1.0	10	1	10	S 5	S 6	SW 7
15	114.2	115.6	115.7	115.2	2.7	3.5	1.0	2.0	4.1	-0.4	82	70	77	76	1.3	2.3	1.5	1.7	4	0	0	SW 7	S 6	S 6
16	112.9	112.0	110.2	111.7	-1.0	1.4	1.3	0.8	2.3	-2.1	87	74	83	81	0.8	1.8	1.1	1.2	7	10	9	SSW 5	SSW 5	S 5
17	93.1	88.2	84.6	88.6	-0.2	4.6	4.4	3.3	5.8	-0.6	88	84	85	86	0.7	1.4	1.3	1.1	10 *	10 •	10	S 9	SSW12	SSW 5
18	86.2	86.9	86.6	86.6	3.6	5.1	1.9	3.1	5.3	1.4	83	70	85	79	1.3	2.6	1.0	1.6	8	7	1	SSW 7	SW 9	S 4
19	88.5	92.0	95.4	92.0	2.9	3.2	1.2	2.1	3.6	0.7	88	83	90	87	0.9	1.3	0.7	1.0	4	9	6	SW 7	SW 3	S 1
20	97.3	98.2	97.0	97.5	-0.9	0.4	0.4	0.1	2.0	-1.2	94	86	92	91	0.3	0.9	0.5	0.6	9	10	10 *	SSE 1	SSE 2	NE 7
21	92.9	95.3	99.6	95.9	0.7	1.1	0.6	0.8	1.3	0.0	96	96	100	97	0.2	0.2	0.0	0.1	10 *	10 *	10 ≡	ENE 3	SE 2	C 0
22	101.7	104.4	110.2	105.4	0.3	1.4	-0.7	0.1	1.6	-0.9	100	91	83	91	0.0	0.7	1.0	0.6	10 *	10	0	S 1	SW 2	SW 1
23	115.5	118.6	122.3	118.8	-4.3	-3.0	-1.5	-2.6	-0.5	-5.4	96	97	96	96	0.2	0.1	0.2	0.2	3	10	9	C 0	S 1	C 0
24	124.3	125.1	125.4	124.9	-1.4	1.4	1.7	0.8	2.1	-3.5	92	89	80	87	0.4	0.8	1.4	0.9	9	9	10	C 0	C 0	NE 2
25	121.7	119.1	116.7	119.2	1.1	1.0	-2.1	-0.5	2.2	-2.6	94	92	94	93	0.4	0.5	0.3	0.4	10 *	10 •	10	NE 4	NE 4	ESE 4
26	115.6	116.0	115.9	115.8	-4.0	-2.3	-1.5	-2.3	-1.2	-4.7	87	98	92	92	0.6	0.1	0.4	0.4	10 ≡	10	10	SE 2	C 0	SE 2
27	117.3	118.5	117.3	117.7	-2.0	-1.4	-2.2	-2.0	-1.3	-3.1	89	86	85	87	0.6	0.8	0.8	0.7	10	10 *	10	SE 3	SE 3	SE 2
28	114.8	115.2	114.4	114.8	-1.2	-0.4	-0.9	-0.8	-0.1	-2.7	93	88	87	89	0.4	0.7	0.7	0.6	10	10	10	SE 3	SE 3	SSE 2
29	111.5	109.4	108.9	109.9	-1.9	-0.3	-1.1	-1.1	-0.3	-2.6	85	90	93	89	0.8	0.6	0.4	0.6	10	10	9	C 0	C 0	WNW 3
30	109.5	109.4	109.2	109.4	-0.2	1.2	-1.4	-0.4	1.5	-1.6	96	74	94	88	0.2	1.8	0.3	0.8	10	10	10 *	W 2	NNE 1	C 0
31	111.6	113.1	112.2	112.3	-1.7	-0.1	-3.4	-2.2	1.0	-3.0	82	78	88	83	1.0	1.3	0.6	1.0	2	1	9	W 3	WSW 3	SW 3
M	107.9	108.7	109.1	108.6	-0.4	0.8	-0.1	0.0	1.9	-2.2	87	82	85	85	0.8	1.2	0.9	1.0	7.6	7.8	7.3	4.5	4.5	4.1

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1	111.3	112.6	116.8	113.6	-1.4	-0.2	-0.8	-0.8	0.3	-4.3	90	78	75	81	0.5	1.3	1.4	1.1	8	7	9 *	WNW 4	W 8	NNW 8
2	120.2	124.6	126.8	123.9	-2.9	-1.4	-4.6	-3.4	-0.5	-4.9	86	90	76	84	0.7	0.5	1.0	0.7	9 *	7	3	NNW 8	N 12	WNW 5
3	121.2	120.2	121.5	121.0	0.2	0.7	-1.2	-0.4	1.4	-4.9	79	96	86	87	1.3	0.2	0.8	0.8	9	10 *	3	WNW 6	N 6	NW 3
4	121.2	124.4	124.8	123.5	0.8	-0.4	-2.1	-1.0	1.8	-2.3	88	74	75	79	0.8	1.5	1.3	1.2	9	10	9 *	NW 8	NNE10	NNE 6
5	120.9	122.5	126.1	123.2	-6.0	-6.5	-10.6	-8.4	-1.8	-11.1	76	70	80	75	0.9	1.1	0.5	0.8	10	0	2	S 3	SE 2	S 1
6	124.2	120.7	117.8	120.9	-6.5	-3.2	-2.7	-3.8	-2.1	-12.0	81	81	86	83	0.7	0.9	0.7	0.8	10	10 *	10 *	SSW 1	S 2	SSW 1
7	118.2	114.6	101.6	111.5	-3.3	0.2	0.6	-0.5	2.7	-4.4	90	89	96	92	0.5	0.7	0.3	0.5	10	9	10 ⚹	S 1	SW 7	NNW 7
8	100.2	103.0	111.4	104.9	-2.2	-0.7	-2.6	-2.0	0.9	-4.4	89	69	83	80	0.6	1.8	0.9	1.1	9 *	9	10 *	NNE14	NE 10	NNE 2
9	117.6	120.5	117.8	118.6	-3.9	-1.8	-2.9	-2.9	-1.6	-4.8	82	67	79	76	0.8	1.8	1.0	1.2	10	5	9	NE 12	NE 5	WSW 8
10	104.2	103.7	107.4	105.1	-2.5	1.8	0.0	-0.2	2.5	-4.3	87	83	63	78	0.7	1.2	2.2	1.4	10 *	6	2	WSW12	WNW 7	NW 8
11	112.7	115.1	116.6	114.8	-3.1	1.8	0.4	-0.1	3.3	-3.5	75	67	88	77	1.2	2.3	0.8	1.4	2	0	9	WNW 7	WNW 4	W 8
12	114.6	112.7	110.9	112.7	1.8	3.2	2.8	2.6	3.3	0.3	89	88	93	90	0.8	0.9	0.6	0.8	9	10 •	10	SW 4	SW 5	WSW 6
13	99.0	94.0	88.8	93.9	2.5	3.6	2.2	2.6	4.2	1.8	93	90	91	91	0.5	0.8	0.7	0.7	10	10 •	9	SW 8	SW 9	SW 6
14	80.6	87.4	97.6	88.5	1.0	1.3	-0.1	0.5	2.3	-0.4	94	94	82	90	0.4	0.4	1.1	0.6	10	9 *	9	SW 5	NW 7	NW 7
15	102.8	104.9	108.5	105.4	-2.9	-0.2	-4.4	-3.0	0.9	-4.6	79	72	86	79	1.0	1.7	0.6	1.1	7	9 *	1	SW 6	WSW 7	NW 3
16	112.2	115.6	120.0	115.9	-4.8	-1.3	-4.7	-3.9	-0.5	-5.6	86	68	86	80	0.6	1.8	0.6	1.0	2	4	1	WSW 3	NW 2	C 0
17	123.0	123.0	125.4	123.8	-1.9	-0.2	0.8	-0.1	1.1	-6.3	85	84	90	86	0.8	0.9	0.7	0.8	10	10	10	NE 7	NE 12	NE 8
18	124.8	125.4	126.7	125.6	-1.2	-1.6	-3.3	-2.4	0.9	-5.6	86	86	88	87	0.8	0.7	0.6	0.7	10	10	10	NE 6	NE 6	NE 5
19	128.3	128.0	131.8	129.4	-2.0	-2.2	-3.2	-2.6	-1.9	-5.7	85	89	70	81	0.8	0.6	1.4	0.9	10	10 *	10	NE 7	NE 5	ENE 6
20	133.4	135.3	134.4	134.4	-2.4	-1.1	-4.7	-3.2	-0.2	-5.0	76	83	86	82	1.2	1.0	0.6	0.9	10	10	0	NE 3	NE 3	C 0
21	128.2	122.1	115.2	121.8	-5.5	-1.2	-0.8	-2.1	-0.7	-7.7	87	82	89	86	0.5	1.0	0.6	0.7	9	10	10	SW 2	WSW 3	WNW 9
22	113.3	115.4	115.7	114.9	-0.2	-1.8	-6.1	-3.6	0.3	-6.4	71	83	73	76	1.8	0.9	1.0	1.2	8	9	2	NNE 7	NE 7	NW 6
23	112.2	114.1	117.3	114.6	-3.8	-2.0	-4.8	-3.8	-1.0	-6.7	82	77	91	83	0.8	1.3	0.4	0.8	9	9	10 *	W 6	NNE 7	N 8
24	116.4	110.6	100.4	109.1	-7.8	-3.7	-3.9	-4.8	-2.4	-9.6	73	78	89	79	0.9	1.0	0.7	0.9	2	9 *	10	W 3	WSW 8	WSW13
25	102.3	102.9	103.6	103.7	-6.0	-4.7	-3.5	-5.4	-3.6	-7.4	71	64	95	77	1.1	1.5	0.2	0.9	3	7	9 *	NW 7	NW14	NW 9
26	106.9	104.3	98.0	103.1	-8.8	-3.7	-6.3	-6.3	-3.6	-12.0	74	60	73	69	0.8	1.9	1.0	1.2	1	9	10	W 7	SW 4	S 1
27	87.2	88.1	100.0	91.8	-3.4	-1.4	-4.6	-4.0	-0.9	-7.9	93	90	88	91	0.2	0.5	0.3	0.4	10 *	10 *	9	SE 1	NE 8	N 12
28	107.1	110.4	112.1	109.9	-5.8	-4.8	-6.6	-6.0	-4.1	-7.0	89	66	78	78	0.4	1.4	0.8	0.9	9	7 *	10	NNW 7	N 9	NNW 1
29																								
30																								
31																								
M	113.0	113.4	114.2	113.5	-3.0	-1.1	-2.8	-2.4	0.0	-5.3	84	79	83	82	0.8	1.1	0.8	0.9	8.8	7.9	7.4	6.0	5.9	6.0

Gdańsk - Wrzeszcz $H_s = 13\,m$ $H_b = 12{,}4\,m$ $h_w = 15{,}5\,m$ *Styczeń - Janvier 1965*

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚCIEGU h	POGODA
1	8	.	.	●$^{0}0^{00}$–5^{40}, ≫10^{30}–17^{40} (por. 15 m/sek)
2	7	.	.	=8^{40}–10^{35}
3	7	0.0	.	●$^{0}16^{35}$–17^{40}; ⌴$^{0}23$–24
4	8	1.0	.	⌴$^{0}0^{00}$–10, 20–24
5	8	1.9	.	✱$^{0}3^{15}$..4^{10}–5^{15} ✱^{0}–7^{15} ✱^{1}–7^{45}; ≫10^{10}–7^{40} (por. 18 m/sek), ⌴$^{0}0^{00}$–2
6	7	0.5	2	✱$^{0}12^{01-05}$–12^{29}–15^{05} ✱$^{15-35}$ 21^{08-30} ✱^{1}–22^{20}; ≫15^{40}–24 (por. do 22 m/sek)
7	8	0.2	2	✱$^{0}1^{04-30}$, 3^{35}–4^{40} 5^{50}–6^{15} 6^{33}–7^{10}; ≫0^{00}–1^{30} (por. 15 m/sek)
8	6	1.8	2	✱$^{0}0^{40}$–4^{35} ●$^{0}12^{40}$–21^{40}, ≫20^{15}–24 (por. 18 m/sek); =7^{35}–20^{10}
9	7	3.6	.	●$^{0}8^{05}$–9^{30} 13^{15} 14^{25}–15^{10} ●^{0}–15^{30} ✱^{0}–24, ≫0^{00}–6^{35}; =9^{30}–10^{40}
10	6	0.1	6	✱$^{0}0^{00}$–6^{20} ✱^{1}–7^{35} ✱^{0}–9^{40}, 10^{15}–14^{10}
11	6	.	5	=9^{15}–21^{30}
12	6	.	5	=7^{15}–24
13	6	.	4	=0^{00}–24
14	6	0.0	2	=0^{00}–24
15	7	.	2	●$^{0}4^{10-30}$; =0^{00}–4^{10}; ⌓$^{0}22^{40}$–24
16	6	0.7	pł.	=4^{40}–24, ⌓0^{00}–4^{30}
17	7	1.8	2	✱$^{1}5^{35}$–6^{40} ✱^{0}–7^{10} ●$^{0}12^{40}$–14^{10} ✱$^{1}6^{32}$–17^{15}, ≫12^{10}–18^{30} (por. 17 m/sek); =0^{00}–7^{35}, ⌓$^{0}0^{15}$–2^{20}
18	7	0.5	.	●$^{0}1^{07-20}$ ●$^{0}22^{40}$–24
19	6	.	.	●$^{0}0^{00}$..4^{35}; =7^{30}–24
20	5	3.1	.	✱$^{0}20^{40}$–24; =0^{00}–24; ⌴$^{0}5$–20; ⌓$^{0}0^{40}$–4^{20} ⊕ $^{0}10^{30}$–14^{05}
21	4	4.9	3	✱$^{0}0^{00}$–10^{25} ✱^{0}–13^{20} ●^{0}..14^{35} ✱$^{0}17^{45}$–19^{35} 22^{10}–24; =0^{00}–17^{40} ≡^{0}–21^{40} = –24
22	6	0.8	3	✱$^{0}0^{00}$–9^{30} ✱^{1}–10^{15} ✱^{0}–10^{30} ✱^{0}–11^{35}; =0^{00}–20^{20}, 23^{10}–24
23	4	.	3	=0^{00}–3^{45} ≡^{0}–6^{10} ≡ –9^{20} ≡^{0}–10^{43} = –24
24	5	1.3	3	=0^{00}–24
25	5	1.2	3	✱$^{0}4^{40}$–10^{15} ●$^{1}11^{20}$–13^{25} ●$^{0}16^{10}$–17^{40}, =0^{00}–10^{15}, 13^{25}–24
26	4	0.8	2	✱$^{1}7^{35}$–9^{20} ✱^{0}–11^{40}, 17^{45}–20^{35}; =0^{00}–6^{40} ≡^{0}–12^{35} = –24
27	5	2.1	4	✱$^{0}12^{35}$–14^{40}, 17^{35}–18^{35}, 22^{15}–24; =0^{00}–24
28	5	0.2	6	✱$^{0}0^{00}$–6^{35}, 15^{10}–18^{25}; =0^{00}–24
29	4	0.2	4	✱$^{0}17^{10}$–19^{35}; =0^{00}–24
30	6	2.2	5	✱$^{0}14^{05}$–21^{25}; =0^{00}–24
31	7	0.5	7	✱$^{0}23^{40}$–24; =0^{00}–3^{30}
Σ	-	29.4	-	

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1	7	1.1	6	✱$^{0}0^{00}$–1^{32}, 15^{50}–16^{40} 19^{30-40}, 20^{38}–21^{10} ✱$^{1}23^{10}$–23^{20} ✱$^{0}23^{45}$–24
2	8	1.7	8	✱$^{0}0^{00-05}$ ✱$^{1}1^{05}$–1^{20} 1^{25}–2^{10} ✱$^{0}5^{15-35}$, 5^{45}–6^{10} ✱$^{0}6^{35}$–7^{15} ✱$^{0}7^{20-30}$ ✱$^{0}8^{05-30}$, 11^{05-25}, 11^{50}–12^{05} 13^{05-40} 14^{02-15} ✱^{0}–14^{20} 15^{20}–16^{05} ✱$^{1}16^{30}$–17^{05}, ⊹$^{1}8^{20}$–13^{25} ≫7^{20}–13^{25} (por. 19)
3	4	0.6	11	✱$^{0}8^{10-20}$ ✱$^{1}8^{35}$–9^{25} ✱$^{0}9^{45}$–12^{05} 12^{40}–13^{35}; =12^{05}–13^{35}
4	8	1.0	11	●$^{0}7^{40}$–8^{20} 8^{43}–9^{30} ✱^{0}–10^{35} 13^{32}..15^{15} ✱$^{0}20^{40}$–24, ≫12^{30}–14^{15}
5	6	.	9	✱$^{0}0^{00}$–2^{10}; =7^{30}–24
6	6	1.0	9	✱$^{0}7^{45}$–17^{15}, 19^{10}–24, =0^{00}–24
7	6	3.1	10	✱$^{0}0^{00}$–2^{35} ●$^{0}10^{40}$–20^{35} ✱^{1}–22^{15} ✱^{1}–23^{20}; =0^{00}–16^{40}
8	8	6.2	9	✱$^{1}1^{40}$–2^{05} ✱$^{1}3^{04-25}$ 5^{45}–6^{10} 6^{40}–7^{45} ✱^{0}–10^{30} ✱^{0}–11^{01} 13^{06-30} 14^{15}–15^{40} ✱$^{1}16^{35}$–19^{15} ✱^{0}–24, ⊹$^{1}20^{05}$–10^{30}; ≫0^{15}–24 (por. do 22 m/sek)
9	8	0.3	16	✱$^{0}0^{00}$–2^{15}, 4^{35}–5^{10}, 8^{40-50} 9^{20}–10^{05}, 10^{25-50}, 11^{30-45}, ⊹$^{0}2^{15}$–7^{10}, ≫0^{00}–8^{30} (por. 17 m/sek)
10	8	1.3	15	✱$^{0}4^{20}$–9^{15} ✱^{1}–11^{10}, ⊹$^{1}3^{30}$–10^{35}, ≫3^{55}–11^{15} (por. 19 m/sek)
11	8	.	17	
12	6	0.0	14	●$^{0}12^{40}$..14^{10}; =6^{30}–24
13	6	1.3	10	●$^{0}4^{35}$..5^{28} 7^{20} 13^{40} 14^{40} 17^{20} ✱$^{0}19^{40}$–20^{10}; =0^{00}–9^{30}
14	6	3.3	pł.	✱$^{0}1^{10}$–3^{40} 5^{28}–6^{40} ✱$^{0}7^{40}$–8^{05} ✱$^{0}8^{15-30}$ ✱$^{1}9^{20}$ ✱^{0}–10^{05}, 10^{35-50} ✱$^{1}11^{05-20}$, 12^{15}–13^{05}, 13^{45}–14^{05} ✱$^{0}16^{10-20}$, 18^{35}–19^{05}, 21^{25-45}
15	7	0.4	1	✱$^{0}8^{35-45}$ 12^{45}–13^{10} ✱$^{1}16^{48}$–17^{10} ✱^{0}–17^{35}, 18^{22}–19^{05}, ⌓$^{1}3^{15}$–5^{20}
16	7	.	2	=6^{15}–8^{30}, 17^{40}–24
17	7	0.0	2	✱$^{0}15^{40}$–17^{35}, ≫11^{35}–15^{50}; =0^{00}–6^{30}
18	7	.	2	
19	6	0.3	2	✱$^{0}12^{35}$–13^{20} ✱^{1}–14^{05} ✱^{0}–14^{20}; =12^{10}–15^{20}
20	6	.	3	=12^{10}–13^{30}, 16^{35}–24
21	6	1.8	3	✱$^{0}23^{15}$–24, =0^{00}–19^{15}
22	8	0.3	5	✱$^{0}0^{00}$–1^{10} ✱^{1}–4^{40} ✱$^{0}7^{35}$–4^{5}, 12^{35-40}, 14^{15-20}, 14^{30-40} ✱$^{1}15^{05-15}$ ✱$^{0}15^{35-40}$, 16^{25-35}, 16^{50}–17^{20}
23	7	2.4	5	✱$^{0}8^{30-40}$ ✱$^{2}0^{02}$–10^{05} 11^{45}–12^{10} ✱^{1}–12^{20} 13^{12}–14^{10} ✱$^{0}14^{30}$–15^{05} ✱$^{1}15^{45}$–16^{37} ✱$^{0}17^{20-30}$ ✱^{2}–17^{40}, 19^{10-25}, 20^{40}–21^{06}
24	7	0.7	8	✱$^{1}1^{12}$–2^{05} ✱$^{0}2^{25-35}$, 9^{14-45}, 10^{26-40}, 12^{35}, 14^{15} ✱^{0}–14^{40} ✱^{1}–15^{05} ✱^{0}–17^{35}, 18^{35}, 19^{15}, 21^{30}, 23^{05} ✱^{1}–24; ⊹$^{1}19^{15}$–24, ≫17^{15}–24 (por. do 19 m/sek)
25	8	2.4	10	✱$^{0}0^{00}$, 1^{30} ✱^{0}–2^{15} ✱$^{1}4^{05-40}$ ✱$^{0}6^{10-20}$, 15^{46}, 16^{05}, 17^{02}, 18^{10} ✱$^{1}19^{05-20}$ ✱$^{0}19^{45}$, 20^{05} ✱$^{2}20^{25}$, 21^{05} ✱^{0}–21^{15} ✱^{2}–21^{35} ✱^{1}–22^{05} ✱^{0}–23^{10} ✱$^{1}23^{40}$–24, ⊹$^{1}0^{20}$, 3^{10} ⊹$^{0}1^{40}$, 12^{15} ⊹^{1}–14^{40}
26	8	0.0	19	✱$^{1}0^{00-15}$, 0^{40}, 1^{20}, 1^{45}, 2^{05}, 2^{15-45}; =17^{30}, 19^{20}, 21^{15}–24 **25.II:** ⊹^{0}–19^{45}, ≫0^{00}–3^{30} (por. 15 m/sek) ≫11^{15}–19^{45} (por. do 19 m/sek)
27	4	7.0	17	✱$^{0}3^{35}$–5^{10}, 6^{32}–7^{35} ✱^{1}–10^{40} ✱^{0}–12^{30} ✱^{1}–19^{35} ✱$^{1}22^{40}$–24, ⊹$^{1}16^{12}$–24, ≫17^{15}–24 (por. 17 m/sek); =0^{00}–24
28	7	0.7	24	✱$^{1}0^{00-05}$, 0^{42}–1^{27}, 2^{08}–3^{15}, 5^{20}–6^{05}, 7^{10-17}, 7^{45}–8^{10}, 10^{50}–11^{05} ✱$^{1}12^{45}$–13^{05}, ⊹$^{1}0^{00}$–1^{50}; =0^{00}–1^{30}
29				
30				
31				
Σ	-	37.1	-	

Gdańsk – Wrzeszcz φ = 54°23' λ = 18°36' Marzec – Mars 1965

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	110.8	108.1	104.4	107.8	-7.4	-5.8	-5.7	-6.2	-5.2	-7.9	90	87	87	88	0.3	0.5	0.5	0.4	10 *	10 *	9	SE 3	SE 5	ESE 1
2	100.6	99.4	97.4	99.1	-4.7	-2.8	-2.3	-3.0	-2.1	-6.5	88	86	89	88	0.5	0.7	0.6	0.6	10	10 *	10 *	ENE 5	NE 6	NE 7
3	93.9	90.4	88.3	90.9	-1.8	-1.8	-1.2	-1.5	-0.9	-3.3	96	96	99	97	0.2	0.2	0.1	0.2	10 *	10 *	10 *	NE 10	NE 9	NE 9
4	88.1	90.3	95.1	91.2	-3.1	-1.6	-1.2	-1.8	-0.6	-3.5	95	84	89	89	0.3	0.9	0.6	0.6	10	10	10	C 0	NE 5	NE 4
5	101.7	106.5	112.1	106.8	-2.1	-0.8	-0.7	-1.1	-0.7	-2.6	79	73	83	78	1.1	1.5	1.0	1.2	10	10	10 *	NE 8	NE 5	N 6
6	119.3	123.3	126.8	123.2	-1.3	-0.8	-1.6	-1.3	0.1	-2.3	80	67	73	73	1.1	1.9	1.4	1.5	9	5	6	NE 7	NE 7	NE 7
7	129.8	131.5	130.8	130.7	-7.4	-3.2	-10.4	-7.8	-1.4	-10.5	87	77	87	84	0.4	1.1	0.4	0.6	4	4	0	ESE 2	NE 3	ESE 1
8	128.0	125.9	124.1	126.0	-18.4	-2.4	-8.0	-9.2	-2.1	-18.9	72	63	75	70	0.4	1.9	0.8	1.0	0	0	0	C 0	S 2	SSW 2
9	121.6	120.7	122.7	121.7	-10.7	-2.1	-0.8	-3.6	0.5	-11.9	87	85	85	86	0.4	0.7	0.9	0.7	0	10 *	9	SSE 2	W 2	WNW 4
10	126.6	127.9	127.9	127.5	-4.7	1.1	0.4	-0.7	3.1	-5.2	83	62	76	74	0.7	2.5	1.3	1.6	5	1	10	W 2	W 7	W 6
11	128.6	129.0	127.8	128.5	0.3	3.0	0.2	0.9	4.2	-0.1	88	69	84	80	0.7	2.4	1.0	1.4	1	4	0	W 7	NW 6	SSW 2
12	126.6	125.1	123.8	125.2	-2.6	5.9	0.9	1.3	7.9	-3.8	77	36	64	59	1.2	6.0	2.3	3.2	7	6	5	SW 4	W 3	SW 2
13	124.2	124.2	123.8	124.1	-2.4	7.7	2.9	2.8	10.2	-4.0	74	45	59	59	1.3	5.7	3.1	3.4	0	1	0	SW 2	S 1	SW 3
14	122.7	121.5	119.9	121.4	-3.1	6.0	2.0	1.7	6.6	-4.0	88	61	75	75	0.6	3.7	1.8	2.0	0	0	0	C 0	SSE 2	S 1
15	118.2	116.8	114.9	116.6	-2.0	7.8	5.4	4.2	9.6	-5.7	89	68	80	79	0.6	3.4	1.8	1.9	0	8	10	S 3	S 3	S 2
16	111.2	108.7	109.1	109.7	3.8	9.3	5.1	5.8	9.6	3.3	92	61	92	82	0.7	4.5	0.7	2.0	4	8	10	SE 2	SSE 6	SW 6
17	110.7	109.8	108.8	109.8	3.8	7.1	3.7	4.6	8.2	2.7	90	76	88	85	0.8	2.5	1.0	1.4	1	2	9	SW 5	S 5	S 1
18	106.7	105.1	102.9	104.9	0.8	6.8	1.4	2.6	7.1	0.6	100	74	100	91	0.0	2.6	0.0	0.9	10 ≡	4	10	C 0	SSE 4	SE 4
19	99.0	100.2	107.3	102.2	2.2	8.0	2.6	3.8	8.4	0.7	93	70	75	79	0.6	3.2	1.9	1.9	9	9	0	SSE 2	SW 8	W 5
20	112.7	113.8	113.3	113.3	0.2	5.6	1.6	2.2	6.3	0.0	80	40	78	66	1.2	5.4	1.6	2.7	1	6	5	SW 6	WSW 8	SW 5
21	109.6	106.8	105.0	107.1	-0.3	3.2	-0.9	0.3	3.2	-1.0	80	68	98	82	1.2	2.5	0.1	1.3	7	10	9	SW 5	S 2	NNW 2
22	107.9	110.6	113.0	110.5	-1.5	4.2	-0.2	0.6	5.8	-3.5	86	79	82	82	0.8	1.7	1.1	1.2	1	2	0	W 8	W 9	SW 4
23	112.6	109.8	104.7	109.0	-2.5	6.4	1.4	1.7	7.0	-2.8	84	42	70	65	0.8	5.5	2.1	2.8	6	2	0	C 0	SSE 7	SSE 4
24	99.5	98.9	99.5	99.3	0.6	5.1	5.4	4.1	9.3	0.4	88	80	86	85	0.8	1.8	1.3	1.3	5	9	6	S 3	S 5	SSE 2
25	98.9	101.9	109.7	103.5	5.7	3.5	0.5	2.6	6.5	-0.6	89	83	82	85	1.0	1.3	1.1	1.1	10	10	6	SW 6	WSW 12	WNW 8
26	112.9	113.2	118.3	114.8	0.7	5.2	2.0	2.5	5.8	-0.6	85	63	78	75	1.0	3.2	1.6	1.9	9	9	10	WSW 1	S 2	NE 1
27	125.9	128.8	130.5	128.4	-1.3	5.1	1.0	1.4	5.9	-2.4	96	57	81	78	0.3	3.8	1.3	1.8	0	0	0	N 1	NE 3	C 0
28	128.6	127.5	126.3	127.5	4.8	8.0	6.3	6.4	8.5	0.9	76	72	91	80	2.0	2.9	0.8	1.9	10	10	10 •	SSW 3	SSW 5	SSW 1
29	126.1	125.1	121.0	124.1	5.6	9.9	10.0	8.9	11.9	4.8	94	77	77	83	0.6	2.8	2.9	2.1	9	9	0	W 3	W 10	W 12
30	115.5	120.3	125.0	120.3	6.3	4.6	2.8	4.1	10.9	1.2	69	79	65	71	2.9	1.8	2.6	2.4	9	8	0	NW 4	N 8	NW 4
31	122.5	123.4	126.3	124.1	2.8	5.5	3.4	3.8	6.4	1.3	72	60	78	70	2.1	3.5	1.7	2.4	5	3	9	NW 6	NNE 9	N 7
M	114.2	114.3	114.9	114.5	-1.3	3.5	0.8	1.0	4.8	-2.7	85	69	81	78	0.9	2.6	1.3	1.6	5.5	6.1	5.6	3.5	5.4	4.0

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1	130.0	130.7	123.7	128.1	0.9	2.7	5.2	3.5	6.5	0.5	58	63	57	59	2.7	2.7	3.8	3.1	6	5	0	N 9	NE 6	W 8
2	122.1	125.1	123.9	123.7	3.4	4.6	0.4	2.2	6.7	0.3	80	50	88	73	1.6	4.3	0.8	2.2	3	2	0	NW 3	NE 5	NE 1
3	118.3	116.1	112.4	115.6	0.4	3.1	3.4	2.6	4.1	-0.7	84	76	83	81	1.0	1.8	1.3	1.4	10	10	10	C 0	SW 3	SW 3
4	108.6	109.0	111.4	109.7	4.3	9.6	1.4	4.2	10.7	1.2	85	60	100	82	1.2	4.8	0.0	2.0	10	9	10 ≡	WNW 4	NW 8	C 0
5	135.8	118.1	119.7	117.9	-1.5	9.5	1.0	2.5	10.6	-1.8	96	60	100	85	0.2	4.8	0.0	1.7	9	1	10 ≡	S 2	E 2	NE 1
6	119.1	116.7	112.1	116.0	-0.4	12.6	8.9	7.5	14.1	-1.4	98	44	71	71	0.1	8.1	3.3	3.8	0	1	0	C 0	SE 4	S 2
7	107.9	110.3	111.4	109.9	5.2	8.2	4.7	5.7	9.8	4.2	84	63	76	74	1.4	4.0	2.0	2.5	10 •	9	10	SW 3	NW 8	W 4
8	112.5	114.9	116.7	114.7	2.1	2.4	2.8	2.5	4.9	1.9	89	86	74	83	0.8	1.1	2.0	1.3	10	10	10	NNW 5	NE 8	E 6
9	118.0	117.9	118.6	118.2	1.0	5.5	4.9	4.1	7.2	0.7	72	59	56	62	1.9	3.7	3.8	3.1	10	9	9	E 7	E 8	ESE 4
10	118.6	117.4	116.7	117.6	0.2	3.8	3.4	2.7	6.9	-0.3	61	51	63	58	2.4	3.9	2.9	3.1	10	10	1	SE 5	SSE 5	SSE 4
11	114.5	112.0	112.2	112.9	0.2	9.1	6.8	5.7	10.6	-1.0	72	42	61	58	1.7	6.7	3.9	4.1	1	7	10	SE 3	SSE 8	S 4
12	113.2	113.8	112.8	113.3	4.3	6.4	4.2	4.8	7.0	2.9	72	63	84	73	2.3	3.5	1.3	2.4	10	10	10 •	SSE 3	SE 3	SSE 3
13	110.7	111.6	112.3	111.5	4.6	4.2	5.6	5.0	5.9	2.8	93	87	88	89	0.6	1.0	1.1	0.9	10	10	10	SSW 3	SSE 6	SSE 3
14	114.9	118.1	120.2	117.7	5.9	4.6	5.0	4.6	6.0	2.3	88	81	86	85	1.0	1.7	1.2	1.3	10 •	10	10	SSE 4	SSW 3	SE 2
15	120.4	120.3	116.5	119.1	2.8	7.8	5.1	5.2	8.7	2.4	86	59	73	73	1.1	4.4	2.4	2.6	10	7	0	SSE 3	SSE 4	SSE 4
16	111.6	108.6	107.6	109.3	2.1	10.2	8.4	7.3	11.7	0.7	89	51	70	70	0.8	6.1	3.3	3.4	0	7	10	S 1	SSE 6	S 3
17	106.7	108.0	102.7	105.8	7.0	8.0	6.0	6.8	9.3	3.8	90	70	77	79	1.0	3.2	2.2	2.1	10	9	5	WSW 4	WSW 8	S 5
18	92.9	91.5	98.4	94.3	6.4	7.3	5.6	6.3	10.9	5.4	79	91	78	83	2.0	0.9	2.0	1.6	10 •	10 •	1	SSE 8	SSE 6	S 2
19	103.1	103.4	103.5	103.3	3.4	6.7	5.1	5.1	9.3	1.6	91	82	98	90	0.7	1.7	0.2	0.9	9	10 •	10	C 0	NE 2	C 0
20	105.2	105.8	107.6	106.2	5.9	9.6	9.0	8.4	10.3	3.0	89	73	77	80	1.0	3.0	2.6	2.2	10	10	10	E 1	ENE 3	ESE 2
21	107.6	107.3	105.9	106.9	8.1	8.6	6.1	7.2	10.9	5.5	78	81	98	86	2.4	2.2	0.1	1.6	6	9	10 •	E 5	NE 7	NNE 2
22	104.8	103.1	103.1	103.7	6.3	9.7	6.7	7.4	10.8	5.7	91	67	74	77	0.9	4.0	2.6	2.5	9	8	4	NE 4	NE 6	E 7
23	100.8	98.5	95.9	98.4	5.9	6.3	4.7	5.4	7.4	4.3	86	84	93	88	1.3	1.3	0.4	1.1	9	10	10 •	NE 8	N 9	NNE 8
24	93.1	94.4	97.9	95.1	3.9	4.7	4.4	4.4	5.4	3.3	92	95	89	92	0.7	0.4	1.0	0.7	10 •	10 •	10	NNW 3	NE 1	NNW 2
25	100.8	104.0	106.3	103.7	5.2	9.1	5.6	6.4	11.6	3.9	87	68	92	82	1.1	3.7	0.7	1.8	9	9	9	W 6	SW 5	C 0
26	107.4	107.0	106.2	106.9	3.6	10.8	6.1	7.2	11.6	4.4	92	80	86	79	0.7	3.3	1.3	2.4	10	9	4	SW 2	SE 3	S 1
27	106.4	105.8	104.8	105.7	3.0	8.3	6.9	6.1	10.3	0.7	100	79	99	93	0.0	2.3	0.2	0.8	10 ≡	10	10	C 0	NE 5	NNW 1
28	106.3	106.1	106.9	106.4	7.1	13.4	10.2	10.8	14.0	4.3	93	65	68	75	0.8	3.3	3.9	3.3	10	8	9	E 1	NE 6	NE 7
29	108.3	109.7	112.3	110.2	7.8	11.9	8.9	9.4	12.9	6.3	79	67	80	75	2.2	4.6	2.3	3.0	7	10	9	SE 4	ENE 5	C 0
30	115.1	116.2	116.2	115.8	7.4	10.0	5.0	6.8	11.7	4.0	79	51	63	64	2.2	6.0	3.3	3.8	9	3	0	N 3	N 9	NNW 4
31																								
M	110.5	110.7	110.3	110.6	3.9	7.6	5.4	5.6	9.3	2.4	84	68	80	77	1.3	3.6	1.9	2.3	8.2	8.1	7.0	3.5	5.4	3.1

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	5	3.1	25	*0 0^40 10^40 *1 – 11^35 *0 – 16^30 *1 – 18^40 *0 – 20^15
2	6	3.7	31	*0 12^05 13^10 – 21^15 *1 – 23^30 *0 24, = 6^30 – 13^10
3	4	10.7	33	*0 0^00 – 2^30 – 10^35 *1 – 14^15 *0 – 15^20 *1 – 22^30 *0 – 24; ⊹1 2^10 – 22^30; ⩗ 2^20 – 8^40
4	7	0.0	49	*0 0^00 – 5^15 15^10 – 16^40; = 5^15 – 10^40
5	6	0.4	48	*0 9^05 – 10^20 *1 – 10^45 *0 – 12^15, 16^50 – 24, = 8^45 – 24
6	8	•	49	*0 0^00 – 3^10; = 0^00 – 6^35
7	8	•	47	= 6^30 – 10^15, 18^30 – 23^20
8	6	•	46	= 2^20 – 13^40, 16^35 – 24
9	6	0.0	42	*0 12^05 – 14^02; = 0^00 – 24
10	8	•	40	= 0^00 – 8^15
11	7	•	33	= 0^30 – 8^40, 20^30 – 24
12	7	•	25	= 0^00 – 10^35 ∞ 16^40 – 17^50 = – 24
13	6	•	20	= 0^00 – 9^10 ∞ – 19^30 = – 20^20 ∞ – 23^30 = – 24
14	5	•	17	= 0^00 – 10^40 ∞ – 18^45 = – 24
15	5	0.1	15	•0 16^20 – 40; = 0^00 – 24
16	6	0.4	5	•0 0^20 – 2^12, 17^05 – 19^20; = 0^00 – 10^30 ∞ – 16^50 = – 24
17	6	•	pł.	= 0^00 – 24
18	6	•	pł.	= 0^00 – 1^15 ≡0 – 5^40 ≡1 – 7^50 ≡0 – 9^40 = – 14^25 ≡0 – 16^10 = – 17^20 ≡0 – 17^45 ≡1 – 18^15 ≡2 – 20^10 ≡0 – 20^40 = – 24
19	7	0.0	•	•0 7^45 – 8^20; = 0^00 – 12^30
20	8	•	•	
21	6	5.4	•	*0 14^35 – 15^40 *1 – 18^30 *0 – 20^15; = 11^30 – 14^35; ⊔0 2 – 8
22	8	•	4	
23	7	•	•	
24	6	0.2	•	•0 10^15 – 11^15; = 5^30 – 24
25	6	0.0	•	•0 0^40 – 1^15 ⊹0 18^35 – 20^10; ⩗ 9^40 – 16^20 (por. do 18 m/sek); = 0^00 – 10^30, 11^40 – 14^15
26	7	•	•	= 6^10 – 9^15, 17^40 – 24
27	7	•	•	= 0^00 – 8^20 20^35 – 24; ⊔0 3 – 9
28	6	0.6	•	•0 10^10 – 22^20 •0 – 23^15; = 0^00 – 24
29	7	•	•	⩗ 12^15 – 14^05, 19^05 – 24 (por. 17 m/sek); = 0^00 – 4^40, 5^30 – 9^10
30	7	2.2	•	•0 9^33 – 11^10 *1 – 11^45 •0 – 12^05; ⩗ 0^00 – 3^30 (por. 15 m/sek), 10^50 – 11^20 (por. 18 m/sek), 14^05 – 15^35 (por. 18 m/sek)
31	8	•	•	
Σ	-	26.8	-	

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1	8	•	•	
2	8	•	•	
3	6	•	•	= 5^30 – 10^30 ∞ – 12^10 = – 24; ⊔1 1 – 9
4	6	•	•	= 0^00 – 13^30, 18^15 – 45 ≡0 – 22^20 = – 24
5	6	•	•	= 0^00 – 5^45 ≡2 – 6^40 = – 7^25 ≡0 – 8^40 = – 16^15 ≡1 – 18^25 ≡2 – 24
6	7	0.0	•	≡0 0^00 – 5^30 ≡1 – 6^15 = – 10^45 ∞ – 11^30 = 18^30 – 21^40
7	7	0.0	•	•0 5^35 – 7^25; = 4^30 – 10^40, 17^20 – 20^30
8	7	0.1	•	•0 9^40 – 11^04; = 8^30 – 12^25
9	8	•	•	
10	7	•	•	
11	7	•	•	⊔0 2 – 9
12	6	0.5	•	•0 20^35 – 24; = 6^30 – 9^40, 12^20 – 24
13	6	4.5	•	•0 0^00 – 3^0 4^40 6^35, 10^15 – 12^35, 21^10 – 24; = 0^00 – 24
14	6	4.2	•	•0 0^00 – 10^35; = 0^00 – 24
15	7	•	•	= 0^00 – 11^30
16	7	0.2	•	•0 21^10 – 23^35; = 4^10 – 10^30, 18^40 – 24; ⊔0 3 – 8
17	7	0.0	•	•0 1^10 – 2^10 – 3^45; = 0^00 – 8^15
18	6	1.1	•	•0 6^35 – 13^40 ⊹0 16^40 – 17^05; = 4^30 – 14^30
19	7	4.4	•	•0 12^20 – 19^10 20^15; = 2^30 – 10^20, 20^15 – 24
20	7	•	•	= 0^00 – 3^0 3^20 – 6^30, 17^30 – 24
21	7	13.8	•	•0 15^35 – 18^05 •1 – 18^25 •0 – 24; = 0^00 – 9^30, 18^25 – 24
22	7	•	•	•0 0^00 – 3^35; = 0^00 – 11^40
23	7	7.5	•	•0 14^32 – 10^30 22^16; ⩗ 15^30 – 20^20
24	6	2.6	•	•0 0^35 5^10 – 14^15 16^22 – 18^40 20^20 – 24; = 14^15 – 24
25	7	1.1	•	•0 0^00 – 3^15 ⊹0 15^40 – 16^05; = 0^00 – 3^15, 14^15 – 24
26	7	1.5	•	⊹0 15^10 – 20 18^32 – 19^17; = 0^00 – 10^40, 19^17 – 24; ⌒0 15^20 – 50
27	6	5.8	•	•0 13^41 – 16^10 •1 – 17^00 •0 – 17^45 •1 – 18^05; = 0^00 – 4^15 ≡0 – 5^20 ≡1 – 7^40 = – 11^40, 12^30 – 24
28	7	0.1	•	•0 8^00 – 9^30; = 0^00 – 12^40
29	7	2.5	•	⊹0 13^40 – 14^15
30	8	•	•	= 5^20 – 9^30; ⌓0 2 – 8
31				
Σ	-	49.5	-	

Gdańsk – Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ *Maj – Mai 1965*

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	116.0	118.6	119.2	117.9	6.7	7.4	3.1	5.1	7.9	2.4	53	59	59	57	4.6	4.2	3.1	4.0	1	0	1	NNW 7	N 9	NNW 4
2	120.6	121.1	120.8	120.8	3.6	5.4	3.0	3.8	6.1	-0.3	70	60	79	70	2.4	3.6	1.6	2.5	2	4	4	N 5	NE 7	N 6
3	121.0	121.6	121.1	121.2	5.1	6.1	3.6	4.6	6.8	2.5	57	46	67	57	3.8	5.1	2.6	3.8	4	1	0	NE 6	NE 8	NE 2
4	119.6	115.7	110.8	115.4	2.7	11.0	8.4	7.6	12.9	0.5	62	29	41	44	2.8	9.3	6.5	6.2	0	3	6	S 4	SSE 8	SE 4
5	107.4	106.1	106.7	106.7	6.1	10.8	10.1	9.3	13.6	4.2	53	42	57	51	4.4	7.6	5.3	5.8	10	10	9	SSE 4	SE 5	ESE 1
6	107.8	108.1	110.2	108.7	7.4	10.4	6.3	7.6	11.6	5.1	54	45	76	58	4.7	6.9	2.2	4.6	9	5	5	SE 2	NE 4	NNE 1
7	111.6	112.4	112.7	112.2	10.0	12.4	7.1	9.2	13.3	4.5	72	53	94	73	3.6	6.7	0.6	3.6	8	9	9	C 0	SW 5	C 0
8	110.5	112.5	114.0	112.3	6.7	8.3	7.5	7.5	10.2	5.5	97	90	91	93	0.3	1.1	0.9	0.8	10 •	10	9	C 0	NE 4	C 0
9	107.5	103.8	91.4	100.9	8.9	8.8	12.0	10.4	15.9	6.5	96	89	96	94	0.5	1.2	0.5	0.7	10	9	10	SSW 4	NE 5	SSW 3
10	87.6	89.6	94.5	90.6	6.5	6.3	6.2	6.3	12.1	6.2	91	84	95	90	0.9	1.5	0.5	1.0	10	10 •	10 •	WNW 8	W 9	W 2
11	104.8	110.6	115.8	110.4	7.2	11.2	5.0	7.1	11.6	4.3	93	65	98	85	0.8	4.7	0.1	1.9	9	2	8	NNE 3	N 8	NE 4
12	120.3	123.0	121.4	121.6	8.3	11.5	8.8	9.4	12.2	5.0	78	55	75	69	2.5	6.1	2.9	3.8	1	4	6	N 7	NNE 6	C 0
13	120.9	120.3	118.2	119.8	9.4	13.1	9.7	10.5	15.3	5.9	75	68	82	75	2.9	4.8	2.2	3.3	0	2	9	NW 2	ENE 5	SE 2
14	114.1	113.8	114.1	114.0	10.2	11.8	5.9	8.4	15.4	5.9	83	78	98	86	2.0	3.0	0.2	1.7	3	9	10	WNW 3	ENE 3	N 8
15	114.8	115.4	113.5	114.6	4.9	5.5	5.3	5.2	6.5	4.4	76	68	87	77	2.1	2.9	1.1	2.0	10	6	6	NE 7	NE 8	NE 4
16	111.6	111.0	107.3	110.0	6.6	8.3	7.9	7.7	10.5	5.3	82	71	86	80	1.7	3.2	1.4	2.1	10 •	10	10 •	ENE 3	E 6	ESE 2
17	104.2	102.8	100.1	102.4	10.6	15.6	14.6	13.8	19.3	7.7	88	63	86	79	1.5	6.5	2.4	3.5	10	9	7	WSW 3	SSW 5	SW 1
18	97.3	100.8	103.5	100.5	14.8	16.6	12.3	14.0	17.6	11.4	79	56	76	70	3.4	8.4	3.4	5.1	7	6	6	WSW 8	W 9	WSW 1
19	99.0	102.7	106.7	102.8	12.9	10.1	7.1	9.3	13.2	7.1	85	64	63	71	2.3	4.6	3.7	3.5	10	10	8	NW 4	N 6	WSW 6
20	112.5	115.0	117.1	114.9	7.2	10.3	6.7	7.7	11.7	4.5	71	45	61	59	2.9	6.9	3.8	4.5	2	7	1	W 7	SSW 7	SW 4
21	122.2	124.1	126.2	124.2	8.1	11.7	7.7	8.8	12.7	4.9	64	44	57	55	3.8	7.7	4.5	5.3	0	5	0	WSW 7	W 9	W 5
22	128.5	128.9	129.3	128.9	9.1	11.0	6.7	8.4	12.3	4.0	51	57	67	58	5.7	5.7	3.3	4.9	0	4	0	WNW 3	NE 5	NE 5
23	128.7	126.7	124.1	126.5	8.0	11.7	10.1	10.0	12.2	5.5	72	62	67	67	2.9	5.1	4.1	4.0	1	1	0	ENE 7	NE 9	E 2
24	122.0	119.7	118.1	119.9	10.3	15.4	9.4	11.1	15.9	8.6	63	52	95	70	4.7	8.4	0.6	4.6	9	9	10 •	E 4	E 6	ENE 4
25	116.8	117.8	118.7	117.8	8.4	8.9	8.9	8.8	9.9	8.2	97	97	96	97	0.3	0.3	0.5	0.4	10 •	10 •	9	NE 4	NE 4	NE 4
26	117.9	116.5	115.1	116.5	10.2	13.4	10.4	11.1	14.6	7.0	81	61	85	76	2.4	6.0	1.9	3.4	5	4	9	NE 1	NE 6	NNE 1
27	112.8	112.8	113.5	113.0	10.1	15.0	10.5	11.5	15.6	9.6	70	32	75	59	3.8	11.5	3.2	6.2	9	6	9	NE 5	NNE 6	NNE 2
28	113.9	113.9	113.2	113.7	10.4	12.7	10.3	10.9	13.6	8.9	80	77	76	78	2.6	3.4	3.0	3.0	3	9	9	NNE 4	NNE 7	N 6
29	110.3	110.1	110.9	110.4	10.1	11.5	7.4	9.1	12.6	6.6	79	61	79	73	2.6	5.4	2.2	3.4	2	4	3	N 8	N 9	N 10
30	109.5	109.6	109.5	109.5	7.8	9.9	5.8	7.3	10.3	5.8	76	72	79	76	2.5	3.4	2.0	2.6	7	3	1	NNW 8	NNE 10	NNE 2
31	111.4	113.0	114.0	112.8	8.3	11.4	8.9	9.4	12.5	1.9	75	47	71	64	2.8	7.1	3.3	4.4	1	2	0	NNE 1	NE 5	NE 3
M	113.0	113.5	113.3	113.3	8.3	10.8	8.0	8.8	12.4	5.5	75	61	78	71	2.7	5.2	2.4	3.4	5.6	5.9	5.9	4.5	6.5	3.2

Czerwiec – Juin

1	111.2	108.4	106.1	108.6	10.3	9.8	10.0	10.0	11.1	7.5	72	91	96	86	3.5	1.1	0.5	1.7	10	10 •	10 •	NE 6	NE 8	NE 4
2	104.5	108.3	111.9	108.2	9.9	9.6	10.6	10.2	10.9	9.2	97	92	68	86	0.3	1.0	4.1	1.8	10	10 •	9	N 3	N 7	W 5
3	114.3	116.3	118.1	116.2	10.4	14.6	11.1	11.8	16.7	9.1	76	69	84	76	3.0	5.2	2.1	3.4	6	7	9	W 7	NE 3	NNE 1
4	119.8	120.7	119.7	120.1	8.7	10.8	9.3	9.5	12.4	6.4	96	82	74	84	0.4	2.3	3.1	1.9	10 ≡	2	1	NNE 4	NNE 3	N 1
5	117.7	115.7	113.3	115.6	10.8	13.9	11.7	12.0	15.1	5.4	75	74	72	74	3.3	4.1	3.7	3.7	4	8	4	NNE 4	NE 6	NE 7
6	111.6	110.3	110.2	110.7	12.2	15.3	11.9	12.8	16.3	9.4	75	66	77	73	3.5	6.0	3.1	4.2	0	0	1	NE 5	NE 9	NNW 4
7	109.8	110.2	110.6	110.2	14.8	15.2	11.0	13.0	16.1	8.3	60	61	68	63	6.7	6.8	4.1	5.9	2	2	0	N 5	NE 6	W 1
8	113.6	113.8	113.3	113.6	12.2	18.6	13.1	14.2	18.9	6.1	71	56	82	70	4.2	9.4	2.8	5.5	1	2	0	SSE 2	E 7	NW 2
9	112.3	111.3	111.0	111.5	14.8	16.5	15.6	15.6	17.2	9.8	85	83	82	83	2.5	3.3	3.2	3.0	9	10	9	E 3	E 3	E 1
10	111.0	111.1	110.9	111.0	16.4	19.5	14.6	16.3	22.9	13.0	69	59	78	69	5.8	9.4	3.6	6.3	9	4	5	E 5	NE 6	N 2
11	110.0	109.5	109.3	109.6	15.2	17.8	14.5	15.5	19.4	12.9	86	65	76	76	2.5	7.3	3.9	4.6	7	7	6	NNE 1	N 8	NNW 2
12	109.5	110.4	111.9	110.6	15.4	17.7	13.9	15.2	20.3	12.8	74	71	65	70	4.6	5.9	5.6	5.4	10	9	9	W 2	NNE 7	WNW 8
13	110.8	111.8	112.4	111.7	12.9	15.0	11.6	12.8	15.6	11.6	88	80	94	87	1.8	3.4	0.8	2.0	9	10	10	W 4	NW 6	WNW 5
14	113.7	116.1	116.8	115.5	13.0	15.6	12.0	13.2	16.9	9.7	80	55	88	74	3.0	7.9	1.7	4.2	3	1	2	N 8	N 9	N 2
15	117.5	116.8	115.5	116.6	14.2	19.0	16.1	16.4	20.2	7.3	51	45	73	56	7.9	12.2	4.9	8.3	2	3	4	WNW 1	NE 4	SE 1
16	113.4	110.7	107.0	110.4	17.8	25.1	20.5	21.0	25.9	11.6	54	31	57	47	9.4	22.0	10.5	14.0	5	3	10	S 5	S 7	S 4
17	101.7	98.8	101.6	100.7	17.8	27.4	17.8	20.2	27.5	14.2	68	35	77	60	6.5	23.8	4.6	11.6	3	3	7	SE 5	SE 9	SW 4
18	105.8	110.2	106.7	107.6	14.6	18.6	16.8	16.7	19.9	13.2	79	52	63	65	3.4	10.2	7.1	6.9	10	7	10	SW 7	SW 7	SSW 5
19	103.1	105.5	108.9	105.8	14.3	17.1	15.3	15.5	19.9	13.7	84	72	71	76	2.5	5.4	5.1	4.3	7	9 •	10	WSW 7	WSW 8	W 8
20	112.4	114.5	113.7	114.2	13.6	19.0	15.7	16.0	20.6	13.1	72	46	63	60	4.4	11.8	6.6	7.6	10	4	0	WNW 7	W 10	W 6
21	117.1	117.2	115.3	116.5	15.7	21.7	15.1	16.9	22.2	11.9	73	38	73	61	4.8	16.1	4.6	8.5	2	8	2	WSW 5	WNW 6	C 0
22	111.1	107.4	105.1	107.9	16.2	25.8	18.4	19.7	27.6	12.4	70	51	93	71	5.4	16.2	1.5	7.7	6	10	9 • R	S 6	SSE 7	E 1
23	104.0	107.4	111.8	107.7	17.8	22.2	17.0	18.5	22.7	16.4	93	51	83	76	1.4	13.2	3.4	6.0	10	8	3	SW 2	WSW 8	SW 3
24	113.3	114.3	115.8	114.5	17.8	22.3	16.6	18.3	23.1	14.3	80	49	92	74	4.0	13.7	1.6	6.4	9	6	9	W 2	NE 5	NNW 2
25	116.9	117.2	116.0	116.7	16.2	18.5	19.7	18.5	21.6	14.0	70	82	72	75	5.4	3.9	6.5	5.3	9	6	5	C 0	NE 3	C 0
26	113.0	112.2	113.9	114.4	20.9	29.3	18.3	21.7	30.1	14.3	68	41	71	60	8.0	23.8	6.0	12.6	0	1	7	S 1	S 5	WNW 7
27	119.3	119.1	118.0	118.8	15.7	19.3	15.4	16.4	21.0	11.9	63	54	76	64	6.6	10.3	4.3	7.1	2	10	9	SW 3	SW 2	C 0
28	120.2	121.4	119.0	120.2	14.2	15.2	14.1	14.4	17.6	12.0	75	50	63	63	4.1	8.7	5.9	6.2	6	9	7	W 6	WNW 8	SSW 3
29	112.7	115.7	116.9	115.1	14.1	18.0	14.0	15.0	18.9	12.9	91	52	72	72	1.5	9.8	4.4	5.2	10 •	6	1	W 7	WNW 9	W 9
30	116.5	115.4	110.7	114.2	13.4	20.0	14.0	15.4	22.7	10.9	71	43	89	68	4.5	13.3	1.8	6.5	6	3	3	W 3	NW 6	C 0
31																								
M	112.3	112.6	112.3	112.5	14.4	18.3	14.3	15.4	19.7	11.2	76	60	76	71	4.2	9.6	4.0	5.9	6.2	5.9	5.7	4.3	6.4	3.2

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU S	POGODA
1	8	.	.	
2	8	.	.	⌴ 0 4–7
3	8	.	.	
4	7	.	.	⌴ 1 4–7
5	8	.	.	= 20 70–24
6	8	.	.	= 0 00–4 30
7	7	11.6	.	● 0 16 25–17 20; = 4 10–8 20 17 40–23 35 ≡ 1–24
8	6	3.3	.	● 0 21 5–4 40 ● 1–7 30 ● 0–11 05 12 10; ≡ 1 00–20 ≡ 0–12 5 = –4 40 ≡ 0–6 45 = –15 30; 19 10–24
9	8	7.0	.	● 0 24 0 3 40–6 35 15 05–17 10 ● 1–19 30 ● 0–20 15; = 0 00–8 45 14 30–21 30
10	7	4.5	.	▽ 0 5 20–40 ● 0–11 10 ● 1–11 40 ● 0–18 20 ● 0 19 35–20 25 ● 1–23 30 ● 0–24
11	8	1.0	.	● 0 0 00–1 40, 23 40–24; = 2 20–4 50 ≡ 0 19 50–20 45 = –24
12	7	.	.	● 0 0 00–10 ● 0–2 20; = 0 00–3 10
13	8	.	.	= 3 30–6 40 20 20–24; ⊕ 0 17 30–18 40
14	7	.	.	= 0 00–5 20, 18 20–24
15	8	0.6	.	= 0 00–4 10
16	7	1.0	.	● 0 2 35 4 30–8 10, 11 40 ... 12 10, 17 35 19 05–21 20, 23 15 ... 24
17	7	5.8	.	● 0 0 00 ... 50 ▽ 0 17 25–35, 23 40–55 ▽ 2–24; R 0 W 23 45–24; = 0 50–12 30; 21 30–24
18	7	0.5	.	▽ 2 0 00–15 ▽ 1 45–215 ▽ 0–3 06 11 10–20; R 0 00–E 0 15; = 0 00–4 30
19	8	.	.	● 0 2 35–4 28; = 0 10–8 20
20	8	0.3	.	▽ 0 13 01–10 14 35–15 10 16 10–17 20; ≫ 14 30–15 20
21	8	.	.	
22	8	.	.	
23	8	.	.	
24	8	1.0	.	● 0 19 20 ... 24
25	6	1.6	.	● 0 0 00 2 15–3 40 ● 1 6 35–7 35 ● 0–8 15 ● 0–10 20; 11 45–14 10 ● 0 17 05–40; = 10 20–14 10
26	8	.	.	
27	8	.	.	
28	7	.	.	
29	8	.	.	≫ 16 10–24 (por. 15 m/sek)
30	8	.	.	≫ 0 00–2 20 (por. 15 m/sek), 11 20–14 30
31	8	.	.	⌴ 0 2–6
Σ	–	38.2	–	

Czerwiec - Juin

1	6	20.9	.	● 0 9 10–10 05 ● 1–11 20 ● 0–14 45 ● 1–16 05 ● 0–17 40 ● 1 19 35–20 40 ● 0–21 35 ● 0 23 20–24; = 17 40–24
2	6	0.9	.	● 0 0 00–1 40 ● 0 2 10–45 ● 1–3 10 ● 2–3 25 ● 0–4 10, 11 40–16 10; = 0 00–16 10
3	7	.	.	
4	6	.	.	= 1 30–4 10 ≡ 0 6 25–7 15 = –14 30; ⌴ 1 2–6
5	8	.	.	
6	8	.	.	
7	8	.	.	⌴ 0 2–6
8	8	.	.	⌴ 0 3–7
9	7	.	.	= 3 30–6 40, 7 15–11 20; ⌴ 1 2–7
10	8	0.4	.	
11	8	.	.	▽ 0 1 10–20, 4 10–30
12	7	0.1	.	
13	8	2.5	.	● 0 1 35–4 40, 14 10–20 20, 21 40–24
14	8	.	.	● 0 0 00–10; ⌴ 0 23–24
15	8	.	.	= 21 40–24, ⌴ 0 0 00–6
16	8	.	.	= 0 00–2 30; ⊕ 0 16 30–17 40
17	7	.	.	
18	8	3.8	.	● 0 7 35–9 15 ● 0 19 36–20 35
19	8	2.9	.	● 0 0 40–4 05 ▽ 1–4 25 ● 0–6 05 ▽ 2 12 30–50 ▽ 1 14 25–40 ▽ 0 15 05–20, 15 35–40, 19 35–45, 22 10–35
20	8	.	.	≫ 12 30–16 30 (por. 15 m/sek)
21	8	.	.	
22	7	47.8	.	▽ 0 20 20–30 ▽ 2–20 35 ▽ 0–20 43 ▽ 2–20 50 ▽ 0–21 05 ▽ 2 21 25 ▽ 0–21 45 22 10–30 ▽ 2 22 40 23 05 ▽ 1–23 45 ▽ 0–24; (R) W 20 05–R 1 20 25 21 40–(R) E 22 05; (R) SW 22 40 R 1 22 50–23 30 (R) E 23 45;
23	7	.	.	▽ 0 0 00–15 ▽ 1 25–40, 3 10–35; (R) W 1 05, R 0 1 20–40 (R) E 2 10 (R) W 3 05–R 0 3 10–35 (R) E 3 40 [22.VI: ≫ 23 05–23 40 (por. 17 m/sek), = 3 20–7 10 ⊕ 0 11 20–13 10
24	7	5.9	.	▽ 0 15 05–15 ▽ 1–15 46 ▽ 0–16 05; = 1 00–5 40, 18 15–24
25	7	.	.	= 0 00–2 30
26	7	0.4	.	▽ 0 16 00–05 ▽ 2–16 10 ▽ 0–16 25; (R) W 15 45–16 05–16 10–(R) E–16 20
27	8	.	.	
28	8	0.8	.	⊕ 0 17 30–18 30
29	8	(0.0)	.	● 0 2 35 ... 3 10–4 20 ● 0 5 25–7 15
30	8	1.5	.	
31				
Σ	–	87.7	–	

Gdańsk – Wrzeszcz φ = 54°23' λ = 18°36' Lipiec – Juillet 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	107.0	109.2	110.9	109.0	13.0	17.7	13.0	14.2	18.3	12.3	92	44	69	68	1.3	11.2	4.6	5.7	9	9	1	NW 4	NW 8	W 4
2	109.8	108.3	104.6	107.6	13.5	16.7	14.0	14.6	17.4	9.0	70	44	67	60	4.7	10.6	5.3	6.9	2	9	10 •	W 5	WNW 9	SW 7
3	103.0	104.1	104.8	104.0	11.7	15.4	11.6	12.6	16.7	10.9	83	62	85	77	2.3	6.7	1.9	3.6	9	9	7	WSW 7	W 8	SW 3
4	105.1	105.0	106.6	105.6	11.5	16.0	11.7	12.7	17.7	10.3	81	55	85	74	2.7	8.2	2.0	4.3	6	8	8	SW 5	W 7	SSW 1
5	107.1	107.1	107.5	107.2	12.3	14.7	12.6	13.0	17.3	8.7	79	57	76	71	3.0	7.2	3.6	4.6	9	5	5	SW 3	W 8	SSW 3
6	106.5	105.7	107.1	106.4	10.6	14.8	11.9	12.3	15.4	8.4	76	58	75	70	3.1	7.0	3.5	4.5	9	9	3	SW 5	SW 9	WSW 5
7	108.1	108.5	105.8	107.5	12.2	14.0	12.9	13.0	16.7	10.2	74	62	92	76	3.7	6.1	1.3	3.7	5	10	10	W 6	SSW 5	C 0
8	105.3	102.9	96.4	101.5	14.3	15.8	15.8	15.4	18.4	11.8	81	90	95	89	3.1	1.7	0.9	1.9	9	10 •	10	WSW 4	SE 4	S 2
9	98.1	101.8	104.2	101.4	12.6	13.7	12.3	12.7	15.9	11.2	67	59	82	69	4.9	6.5	2.5	4.6	6	10 •	9	SW 9	WSW 10	SSW 4
10	108.6	111.4	113.6	111.2	12.2	14.5	11.6	12.5	16.7	10.8	75	64	75	71	3.5	6.0	3.4	4.3	5	7	2	WSW 7	WSW 8	W 2
11	116.0	116.5	116.0	116.2	12.2	17.7	15.0	15.0	18.1	9.6	79	46	76	67	3.0	10.9	4.0	6.0	8	7	10	WSW 2	NE 5	C 0
12	111.4	107.6	107.7	108.9	15.1	18.5	13.6	15.2	19.1	13.0	74	79	93	82	4.4	4.5	1.1	3.3	10 •	10 •	0	S 7	S 8	SW 3
13	111.2	111.5	111.1	111.3	14.4	20.8	19.4	18.5	22.8	11.8	77	48	76	67	3.8	12.9	5.4	7.4	1	5	5	SW 7	WSW 7	SSW 3
14	113.6	115.2	115.6	114.8	19.2	19.2	14.8	17.0	24.4	14.5	81	82	98	87	4.2	4.0	0.3	2.8	4	5	9	SW 2	NNE 5	NNE 1
15	115.7	117.0	117.3	116.7	19.7	23.4	18.6	20.1	23.6	14.6	87	70	89	82	3.0	8.8	2.3	4.7	5	5	9	C 0	NE 3	N 3
16	116.6	118.1	118.4	117.7	16.2	15.4	14.9	15.4	18.7	14.5	98	98	96	97	0.4	0.4	0.7	0.5	9 • K	10 •	10	NNE 9	N 7	N 7
17	117.3	117.5	117.7	117.5	14.3	14.7	14.5	14.5	15.8	14.0	97	92	88	92	0.6	1.3	2.0	1.3	10 •	10	5	NE 8	NE 8	NNE 6
18	118.5	119.6	120.3	119.5	15.8	16.4	15.3	15.7	17.4	13.7	76	77	79	77	4.3	4.2	3.7	4.1	2	4	1	NE 5	NE 9	NE 6
19	121.8	122.2	121.4	121.8	17.1	19.8	16.1	17.3	20.9	11.8	74	57	80	70	5.1	9.9	3.6	6.2	0	1	0	ENE 3	NE 5	C 0
20	121.3	119.8	117.1	119.4	16.7	22.6	18.1	18.9	24.4	11.8	77	53	81	70	4.4	12.9	3.9	7.1	0	2	3	C 0	NE 5	C 0
21	114.3	111.5	107.2	111.0	17.0	23.1	20.7	20.4	25.5	12.1	70	45	62	59	5.8	15.5	9.2	10.2	9	9	9	SE 2	SE 5	E 2
22	105.4	107.4	108.8	107.2	17.6	20.8	16.7	18.0	23.3	15.3	95	76	82	84	1.0	6.0	3.5	3.5	9	7	6	S 2	W 5	SE 3
23	107.4	105.3	104.9	105.9	15.5	21.4	15.9	17.2	22.6	13.4	94	76	93	88	1.1	6.1	1.4	2.9	4	9	5	C 0	E 2	NW 1
24	104.3	103.0	106.8	104.7	14.9	21.8	14.5	16.4	22.5	12.7	90	51	85	75	1.6	12.7	2.5	5.6	10 •	8	4	SW 2	WSW 8	S 2
25	107.8	107.9	107.8	107.8	15.0	21.1	13.8	15.9	22.9	12.8	75	44	91	70	4.1	13.9	1.5	6.5	0	7	9	SW 8	SW 9	W 7
26	105.6	105.1	103.4	104.7	13.8	18.4	15.0	15.6	19.8	12.8	83	61	83	76	2.7	8.4	2.9	4.7	9	9 •	9	SW 5	SW 8	SW 5
27	102.7	105.3	106.0	104.7	13.2	15.1	13.5	13.8	16.6	12.4	78	56	74	69	3.3	7.5	4.0	4.9	8	9	3	W 7	W 9	SW 5
28	105.6	106.6	105.4	105.9	12.7	16.3	13.9	14.2	17.6	11.3	73	65	81	73	3.9	6.5	3.0	4.5	6	9	9	W 8	WNW 9	SW 4
29	102.0	100.8	95.5	99.4	14.0	16.5	13.6	14.4	17.8	13.0	86	82	87	85	2.2	3.5	2.0	2.6	10	10 •	10	SW 3	SW 8	S 4
30	91.4	91.2	92.6	91.7	16.0	18.8	14.1	15.8	19.5	13.4	80	57	91	76	3.6	9.4	1.5	4.8	9	9	10 •	SW 5	WSW 8	SW 8
31	96.1	97.9	100.9	98.3	13.8	17.3	13.0	14.3	18.0	12.6	66	52	65	61	5.4	9.4	5.3	6.7	3	9	8	SW 8	SW 7	SW 3
M	108.5	108.7	108.5	108.6	14.5	17.8	14.6	15.4	19.4	12.1	80	63	82	75	3.2	7.7	3.0	4.6	6.3	7.7	6.4	4.8	7.0	3.4

Sierpień – Août

1	105.4	106.6	108.5	106.8	12.2	18.1	14.8	15.0	19.0	9.4	78	41	63	61	3.2	12.3	6.2	7.2	2	6	2	SW 5	SW 7	SSW 3
2	107.6	106.9	106.9	107.1	13.6	15.0	12.4	13.4	20.7	9.7	69	74	82	75	4.9	4.3	2.6	3.9	2	9 •	2	SSW 1	N 3	W 2
3	105.3	105.7	107.1	106.0	13.3	19.0	14.4	15.3	21.0	10.4	73	52	85	70	4.2	10.5	2.5	5.7	2	6	6	W 3	WNW 5	C 0
4	108.4	108.8	112.1	109.8	15.1	19.6	13.1	15.2	20.9	13.0	76	53	86	72	4.1	10.7	2.1	5.6	9	6	5	WSW 3	NE 4	SW 1
5	115.0	117.1	117.1	116.4	14.4	18.3	15.8	16.1	19.7	11.5	83	62	83	76	2.7	7.9	3.0	4.5	5	7	9	WSW 6	NW 4	C 0
6	113.8	110.4	111.6	111.9	16.1	27.8	18.2	20.1	28.1	11.9	70	48	91	70	5.4	19.2	1.9	8.8	7	9	4	SSE 4	S 8	N 1
7	111.1	110.2	110.2	110.5	16.6	16.6	17.4	17.0	23.1	15.6	93	86	93	91	1.4	2.7	1.5	1.9	10	10	10 •	C 0	NE 1	NNE 1
8	114.2	114.8	113.9	114.3	14.9	16.4	14.0	14.8	18.1	13.9	89	81	95	88	1.8	3.4	0.7	2.0	9	10 •	10 •	W 1	C 0	NE 4
9	115.2	117.2	118.5	117.0	13.6	15.4	12.6	13.6	16.6	12.5	94	83	78	85	0.9	3.0	3.2	2.4	10	10	5	NNE 3	NW 4	WNW 2
10	119.3	120.3	120.5	120.0	12.6	16.8	11.6	13.2	19.1	10.0	84	55	82	74	2.4	8.6	2.4	4.5	3	8	4	W 6	W 5	WSW 3
11	120.0	120.5	121.0	120.5	13.4	14.0	12.2	13.0	18.7	10.7	90	85	89	88	1.6	2.3	1.5	1.8	9	9 •	2	NW 2	W 3	NW 4
12	120.8	121.1	120.7	120.9	13.6	15.2	11.6	13.0	16.4	10.8	92	73	84	83	1.3	4.6	2.1	2.7	6	8 •	2	NW 3	NNE 5	NW 5
13	119.8	119.5	119.3	119.5	11.6	14.9	11.5	12.4	17.5	10.0	85	77	88	83	1.9	3.8	1.7	2.5	7 •	7	8	N 5	N 8	WNW 3
14	117.3	117.6	117.7	117.5	11.9	14.2	12.1	12.6	14.9	11.2	93	77	93	88	1.0	3.8	1.0	1.9	10	9	9	NW 5	N 8	NW 3
15	118.8	120.3	120.5	119.9	12.7	15.2	11.4	12.7	15.9	10.8	89	76	89	85	1.6	4.3	1.5	2.5	9	8	1	NW 2	NNE 6	C 0
16	120.1	119.9	117.9	119.3	12.3	14.7	11.7	12.6	16.0	9.0	88	77	95	87	1.7	3.8	0.6	2.0	4	9	3	WSW 2	NE 2	C 0
17	117.1	117.0	117.1	117.1	13.4	19.2	13.8	15.0	20.9	8.9	85	57	95	79	2.3	9.6	0.7	4.2	0	2	0	SW 1	NE 3	C 0
18	118.1	118.2	118.8	118.4	11.5	20.8	15.6	15.9	22.5	10.0	100	70	91	87	0.0	7.4	1.5	3.0	10 ≡	4	2	C 0	E 5	C 0
19	120.8	121.3	120.8	121.0	15.1	22.4	16.8	17.8	23.2	12.4	85	48	78	70	2.6	14.0	4.2	6.9	2	6	6	WNW 1	NE 2	SE 1
20	120.1	118.1	115.7	118.0	15.5	26.7	20.9	21.0	27.6	13.1	86	47	59	64	2.4	18.7	10.0	10.4	5	6	4	C 0	S 2	SSE 4
21	112.5	110.3	108.5	110.4	16.0	25.5	19.6	20.2	26.1	15.8	71	51	84	69	5.2	16.0	3.6	8.3	3	7	0	SSE 2	SSW 4	C 0
22	107.2	105.3	105.0	105.8	16.7	28.3	21.2	21.8	28.9	14.9	83	36	59	59	3.3	24.5	10.4	12.7	2	7	4	S 3	S 9	SSE 4
23	105.2	104.2	104.7	104.7	16.8	28.1	22.2	22.3	29.4	15.5	77	38	59	58	4.4	23.5	11.0	13.0	0	0	6	SSE 5	SSE 7	SE 3
24	105.6	108.2	106.8	106.9	18.1	18.8	17.1	17.8	22.4	16.1	85	83	96	87	3.5	3.7	0.8	2.7	9	9	10	NW 2	NE 5	NNW 2
25	103.6	103.7	107.1	104.8	16.8	17.2	15.2	16.1	17.8	15.0	96	96	92	95	0.8	0.8	1.3	1.0	10 •	10 •	10 •	NNW 2	NNW 2	WSW 3
26	109.9	111.4	112.9	111.4	13.1	16.0	12.3	13.4	17.5	12.2	86	69	85	80	2.1	5.6	2.2	3.3	9	10	9	WNW 4	NW 6	W 1
27	110.4	109.1	108.8	109.4	12.4	11.4	11.4	11.6	13.1	11.0	83	90	88	87	2.4	1.4	1.7	1.8	10 •	10 •	9	W 1	N 6	W 6
28	108.9	111.0	113.0	111.0	13.3	17.0	13.3	14.2	17.3	10.7	88	64	91	81	1.8	7.1	1.4	3.4	9	9 •	10	W 4	WNW 9	SW 3
29	112.0	110.4	109.2	110.5	11.7	18.9	12.8	14.0	20.1	11.6	89	47	89	75	1.5	11.5	1.6	4.9	6	8	10	SW 4	SW 6	SW 4
30	110.2	111.6	112.9	111.6	12.3	17.1	11.4	13.0	18.2	11.3	85	56	95	75	2.2	8.7	2.0	4.3	1	4	1	SW 5	NW 7	SW 3
31	113.2	113.1	112.3	112.9	10.7	16.6	11.4	12.5	17.5	8.9	90	60	88	79	1.3	7.5	1.7	3.5	1	6	0	WSW 2	ENE 3	C 0
M	113.1	113.2	113.5	113.3	13.9	18.6	14.5	15.4	20.3	11.8	85	65	84	78	2.4	8.6	2.9	4.6	5.9	7.4	5.3	2.7	4.8	2.1

Gdańsk - Wrzeszcz $H_s = 13m$ $H_t = 12.4m$ $h_w = 15.5m$ Lipiec - Juillet 1965

DNI	WIELKOŚĆ V	OPAD R	GŁĘBOKOŚĆ h	POGODA
1	8	.	.	$\bullet^{0}5^{05}-6^{40}$
2	8	0.3	.	$\bullet^{0}20^{35}-21^{10}$
3	8	1.9	.	$\overset{\bullet}{\nabla}{}^{0}6^{25-40}$ 9^{20-30}, 10^{40-50} $\overset{\bullet}{\nabla}{}^{1}16^{05-30}$ $\overset{\bullet}{\nabla}{}^{0}18^{07-25}$, $\frown^{0}18^{35-40}$
4	8	2.0	.	$\overset{\bullet}{\nabla}{}^{1}3^{35-55}$, 17^{05-12}, 20^{07-20}
5	8	1.0	.	$\overset{\bullet}{\nabla}{}^{0}9^{05-15}$ $\overset{\bullet}{\nabla}{}^{1}11^{31}-12^{02}$
6	8	1.1	.	$\overset{\bullet}{\nabla}{}^{0}13^{30-45}$, 16^{15-35}, 18^{05-15}; $\frown^{0}16^{35-45}$
7	8	4.6	.	$\bullet^{0}18^{25}-19^{35}$; $=19^{35}-23^{10}$
8	6	9.0	.	$\bullet^{0}12^{05}-13^{40}$ $\bullet^{1}15^{20}$, 17^{05} $\bullet^{0}-17^{20}$ $19^{03}-20^{40}$; $=3^{20}-6^{30}$ $13^{40}-22^{30}$
9	7	1.3	.	$\overset{\bullet}{\nabla}{}^{0}10^{27-35}$ 11^{05-25}, 12^{40} 13^{03}, 14^{30}, 15^{05}, 15^{26-40} 16^{32-45}, 18^{16-35}, 19^{15-40}, 20^{25-35}, 23^{30-40}; $\gg 8^{20}-15^{20}$ (por. do 19 m/sek)
10	8	0.2	.	$\overset{\bullet}{\nabla}{}^{0}10^{25-45}$ 11^{15-35}
11	8	0.0	.	$\bullet^{0}21^{45}-22^{00}$... 23^{10}
12	7	13.6	.	$\bullet^{0}6^{40}-13^{20}$... $14^{10}-15^{15}$ $\bullet^{1}-16^{25}$ $\overset{\bullet}{\nabla}{}^{2}17^{32-45}$ $\overset{\bullet}{\nabla}{}^{1}-18^{40}$; $\frown^{0}18^{40}-19^{00}$
13	8	0.3	.	$\bullet^{0}22^{35}-23^{20}$; $=23^{20}-24$
14	6	10.3	.	$\overset{\bullet}{\nabla}{}^{1}17^{33-45}$ $\overset{\bullet}{\nabla}{}^{0}-18^{05}$, 18^{25-45} $\overset{\bullet}{\nabla}{}^{1}-19^{05}$ $\overset{\bullet}{\nabla}{}^{0}-19^{25}$, $21^{35}-22^{10}$; $(K_1)^{0}SW$ 17^{15} $K_1^{0}17^{25-45}-(K_1)E$ 18^{10}, $(K_1)SW$ $18^{20}-K_1^{1}18^{35}$ $19^{00}(K_1)E$ 19^{30}; $=0^{00}-7^{30}$, $14^{40}-24$
15	7	21.7	.	$\overset{\bullet}{\nabla}{}^{0}10^{10-25}$; $=0^{00}-11^{05}$, $14^{40}-24$
16	6	7.0	.	$\overset{\bullet}{\nabla}{}^{1}3^{35}-6^{15}$ $\overset{\bullet}{\nabla}{}^{0}-6^{40}$ $\overset{\bullet}{\nabla}{}^{1}-$ $\overset{\bullet}{\nabla}{}^{0}-8^{10}$ $\bullet^{0}10^{32}$, 11^{05} $\bullet^{1}-11^{20}$ $\bullet^{0}-15^{45}$ $\bullet^{0}-17^{10}$; $(K_1)^{0}SW$ 2^{45} $K_1^{1}3^{35}-7^{10}(K_1)E$ 7^{30}; $=0^{00}-9^{30}$, $17^{10}-22^{30}$
17	7	0.1	.	$\bullet^{1}5^{15}-8^{30}$ $\bullet^{0}$... 10^{25}
18	8	.	.	
19	8	.	.	
20	8	.	.	$\frown^{1}2-8$ $\frown^{0}21-24$
21	7	1.4	.	$\frown^{0}0^{00}-7$; $\oplus^{0}6^{30}-8^{30}$
22	7	0.5	.	$\bullet^{0}3^{05}-6^{40}$ $\overset{\bullet}{\nabla}{}^{0}10^{05-10}$ $\bullet^{0}22^{10}-23^{40}$; $=6^{40}-7^{50}$
23	6	19.7	.	$\overset{\bullet}{\nabla}{}^{0}15^{20-30}$ $\overset{\bullet}{\nabla}{}^{1}-15^{55}$ $\overset{\bullet}{\nabla}{}^{2}-16^{10}$ $\overset{\bullet}{\nabla}{}^{1}-16^{40}$ $\overset{\bullet}{\nabla}{}^{0}-17^{20}$; $K_1^{1}SW$ $15^{25}-15^{55}$ $16^{35}E$; $=3^{30}-20^{30}$
24	7	3.1	.	$\bullet^{0}6^{40}$... 7^{35} $\overset{\bullet}{\nabla}{}^{0}14^{20-40}$ 17^{15-35}; $(K_1)^{0}NW$ 13^{45} $N-NE$ 14^{40}; $=2^{00}-10^{10}$
25	8	1.1	.	$\overset{\bullet}{\nabla}{}^{0}19^{25}-20^{15}$; $(K_1)^{0}W$ 19^{10} $K_1^{0}19^{25-40}(K_1)E$ 19^{50}
26	7	4.3	.	$\overset{\bullet}{\nabla}{}^{0}12^{40}$ 13^{25}, 14^{05-45}, 15^{45} 16^{10}, $16^{45}-17^{10}$
27	8	0.0	.	$\overset{\bullet}{\nabla}{}^{0}10^{40-50}$
28	8	1.0	.	$\overset{\bullet}{\nabla}{}^{0}10^{33-40}$, 11^{03-25} $\overset{\bullet}{\nabla}{}^{1}11^{46}$ 12^{10}
29	6	3.2	.	$\bullet^{0}12^{45}$... 13^{35} 14^{10}... 15^{03} 17^{10}... $18^{05}-19^{10}$ $\bullet^{1}-19^{30}$ $\bullet^{0}-20^{35}$ $\bullet^{1}21^{35}-22^{30}$ $\bullet^{0}-23^{20}$; $=15^{03}-20^{40}$
30	8	3.4	.	$\overset{\bullet}{\nabla}{}^{0}7^{03-10}$ $\overset{\bullet}{\nabla}{}^{1}8^{05-15}$ $\overset{\bullet}{\nabla}{}^{0}13^{50}$ 14^{10}, 16^{02} 17^{10}, 18^{52} 19^{15}, 20^{25} 21^{20}; $(K_1)^{0}NW$ 14^{05} $N-NE$ 14^{35}
31	8	.	.	
Σ	-	112.1	-	

Sierpień - Août

1	8	.	.	
2	7	2.0	.	$\overset{\bullet}{\nabla}{}^{1}12^{40-53}$ $\overset{\bullet}{\nabla}{}^{0}13^{05-30}$; $=5^{20}-6^{40}$
3	8	.	.	$=20^{20}-24$
4	8	4.0	.	$\overset{\bullet}{\nabla}{}^{1}15^{40}-16^{05}$ $\overset{\bullet}{\nabla}{}^{0}16^{15}-17^{10}$ $\overset{\bullet}{\nabla}{}^{1}-17^{45}$ $\overset{\bullet}{\nabla}{}^{0}-18^{20}$; $(K_1)SW$ 15^{10} $K_1^{0}15^{30-40}-(K_1)E$ 16^{25}; $=0^{00}-1^{30}$
5	8	.	.	
6	7	16.7	.	$\overset{\bullet}{\nabla}{}^{0}16^{05-15}$ $\overset{\bullet}{\nabla}{}^{2}-16^{20}$ $\overset{\bullet}{\nabla}{}^{1}-16^{30}$ $\overset{\bullet}{\nabla}{}^{0}-16^{50}$; 17^{15-45} $\overset{\bullet}{\nabla}{}^{2}18^{33-40}$; $(K_1)SW$ 15^{50} $K_1^{1}16^{05-45}-(K_1)E$ 17^{35}; $(K_1)W$ 18^{20} $K_1^{1}18^{25-45}-(K_1)SE$ 19^{35} $\gg 16^{15-25}$ (por. 28 m/sek); $\frown^{0}1-8$;
7	7	4.2	.	$\overset{\bullet}{\nabla}{}^{0}2^{10-25}$ $\bullet^{0}3^{35}-9^{10}$ 13^{05-20} $18^{40}-19^{30}$ $\bullet^{1}-20^{10}$ $\bullet^{0}-21^{35}$; $=7^{20}-9^{40}$ $14^{30}-17^{40}$ [6.VIII: $\oplus^{0}12^{20}-13^{30}$]
8	7	11.1	.	$\bullet^{0}11^{45}$... $13^{30}-16^{35}$ $\bullet^{1}-17^{05}$ $\bullet^{0}-17^{20}$, 20^{05-20} $\bullet^{1}-20^{40}$ $\bullet^{0}-21^{50}$; $=17^{20}-24$
9	8	.	.	$\bullet^{1}2^{05-20}$ $\bullet^{0}-4^{35}$; $=0^{00}-7^{40}$
10	8	.	.	
11	7	11.3	.	$\overset{\bullet}{\nabla}{}^{0}10^{45}$, 11^{05} $\overset{\bullet}{\nabla}{}^{1}12^{15-20}$ $\overset{\bullet}{\nabla}{}^{2}$ 12^{30} $\overset{\bullet}{\nabla}{}^{1}-13^{05}$ $\overset{\bullet}{\nabla}{}^{0}-13^{25}$; 14^{10-25}; $K_1^{0}W$ 12^{52} $13^{00}-13^{15}S$; $=3^{35}-6^{15}$
12	8	0.3	.	$\overset{\bullet}{\nabla}{}^{0}12^{35}-13^{15}$; $(K_1)NW$ 12^{48} $SW-SE$ 13^{20}; $=4^{20}-6^{40}$; $\frown^{0}2-9$
13	8	3.7	.	$\overset{\bullet}{\nabla}{}^{0}6^{20}-7^{05}$, 8^{10-15}, 12^{10-25} $\overset{\bullet}{\nabla}{}^{1}15^{20-30}$, $\oplus^{0}13^{40}-15^{10}$; $\frown^{0}6^{15-30}$
14	8	2.0	.	$\overset{\bullet}{\nabla}{}^{0}1^{30-35}$ $\bullet^{0}4^{25}-6^{10}$ $\overset{\bullet}{\nabla}{}^{0}7^{40-45}$, 8^{25-40}, 9^{15-30}, 15^{25-35}, 23^{15-25}
15	8	0.7	.	$\overset{\bullet}{\nabla}{}^{0}0^{25-40}$ $\overset{\bullet}{\nabla}{}^{1}2^{20-30}$ $\overset{\bullet}{\nabla}{}^{0}7^{20-45}$
16	8	.	.	$\frown^{0}20-24$
17	8	.	.	$\frown^{0}0^{00}-3$ $\frown^{1}4-8$ $\frown^{0}22-24$
18	7	.	.	$=2^{20}-4^{45}$ $\equiv^{0}-7^{25}$ $=-11^{30}$; $\frown^{0}0^{00}-4$, $20-24$
19	8	.	.	$=13^{30}-24$; $\frown^{0}0^{00}-8$
20	6	.	.	$=0^{00}-13^{30}$ ∞ $17^{20}-21^{40}$
21	6	.	.	$(K_1)^{0}W$ $16^{50}-N-NE$ 18^{20}; ∞ $10^{30}-18^{30}$ $=-24$
22	7	.	.	$=0^{00}-9^{30}$
23	7	.	.	
24	7	15.1	.	$\overset{\bullet}{\nabla}{}^{0}13^{40}-14^{03}$ $\bullet^{0}16^{05}-17^{15}$ $21^{05}-23^{40}$ $\bullet^{1}-24$; $=3^{30}-12^{30}$ $14^{40}-24$
25	6	11.9	.	$\bullet^{1}0^{00}-1^{25}$ $\bullet^{0}-6^{10}$ $\bullet^{1}-9^{20}$ $\bullet^{0}-11^{25}$ $\bullet^{1}12^{30}-13^{20}$ $\bullet^{0}-15^{15}$, $19^{15}-21^{25}$; $=0^{00}-11^{25}$
26	8	0.0	.	$\bullet^{0}2^{05}-3^{15}$, $9^{35}-10^{10}$
27	6	18.1	.	$\bullet^{0}6^{15}$... $8^{10}-10^{15}$ $\bullet^{1}-15^{30}$ $\bullet^{0}-18^{20}$, $22^{10}-24$
28	8	3.0	.	$\bullet^{0}0^{00}-3^{20}$, $15^{10}-16^{35}$ $20^{05}-24$
29	8	1.2	.	$\bullet^{0}0^{00}-2^{15}$, $18^{25}-20^{20}$; $=22^{30}-24$
30	8	0.4	.	$\overset{\bullet}{\nabla}{}^{0}15^{05-10}$, 17^{25-32}; $=0^{00}-5^{20}$
31	8	.	.	
Σ	-	105.7	-	

Gdańsk – Wrzeszcz φ = 54°23' λ = 18°36' Wrzesień – Septembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	111.8	112.9	116.2	113.6	10.8	17.6	15.4	14.8	18.1	8.3	94	65	86	82	0.9	7.0	2.4	3.4	8	4	2	C 0	NE 4	E 2
2	119.7	120.8	119.6	120.0	14.8	17.7	15.6	15.9	18.1	13.9	86	76	87	83	2.4	4.7	2.3	3.1	10 •	9	0	E 2	E 6	NE 2
3	113.8	110.2	108.5	110.8	14.4	21.9	20.6	19.4	27.0	13.1	83	72	77	77	2.7	7.5	5.4	5.2	9	8	8	C 0	ENE 2	C 0
4	106.1	107.2	105.9	106.4	19.0	17.9	15.4	16.9	20.9	15.4	87	88	96	90	2.8	2.4	0.8	2.0	8	10	10 •	SSE 2	NE 2	NNW 5
5	105.3	106.7	106.5	106.2	13.4	14.5	14.0	14.0	15.5	12.9	91	94	91	92	1.4	0.9	1.5	1.3	10	10 •	6	SW 5	WSW 5	SW 5
6	105.6	103.9	101.3	103.6	12.5	21.7	14.5	15.8	22.1	8.7	90	59	92	80	1.4	10.6	1.3	4.4	8	4	5	C 0	S 2	N 2
7	101.0	100.8	101.2	101.0	12.9	15.3	12.7	13.4	15.9	12.3	89	66	80	78	1.6	6.0	2.9	3.5	8	9	8	SSW 5	SSW 7	SSW 8
8	104.3	108.5	109.9	107.6	12.9	15.8	13.7	14.0	17.2	12.0	77	65	75	72	3.5	6.2	3.9	4.5	6	5	1	SSW 8	SW 8	S 2
9	107.4	108.9	112.2	109.5	10.8	19.0	14.0	14.4	20.0	9.6	90	66	88	81	1.4	7.6	2.0	3.7	4	9	6	SSE 4	SW 4	C 0
10	108.1	105.1	109.7	107.6	13.8	22.5	14.7	16.4	23.0	12.8	99	62	80	80	0.2	10.4	3.3	4.6	9 ≡	9	8	C 0	S 5	W 3
11	108.4	103.9	111.8	109.7	12.6	12.9	11.5	12.1	14.9	11.3	92	86	90	89	1.2	2.1	1.4	1.6	10 •	9	9	NNW 3	NNW 8	WSW 4
12	111.2	110.3	108.8	110.1	10.1	17.5	12.0	12.9	18.2	8.9	85	48	74	69	2.0	10.4	3.6	5.3	4	5	4	SW 2	SW 6	SW 1
13	106.8	106.9	108.2	107.3	10.8	16.6	11.0	12.4	16.8	10.7	89	63	90	81	1.5	7.0	1.3	3.3	4	6	0	SW 4	SW 8	SW 3
14	108.7	110.8	113.0	110.8	10.7	14.2	10.9	11.7	16.2	10.0	87	73	83	81	1.7	4.4	2.2	2.8	9	7	2	SSW 1	WSW 6	SW 3
15	114.5	117.8	122.7	118.3	10.7	15.7	10.2	11.7	16.9	9.4	82	57	86	75	2.3	7.6	1.7	3.9	3	7	0	WSW 3	WNW 8	W 4
16	124.9	124.5	121.6	123.7	9.6	18.8	13.2	13.7	19.7	8.7	96	46	79	74	0.5	11.7	3.2	5.1	0	3	4	C 0	WSW 2	S 2
17	117.8	116.3	116.7	116.9	10.2	22.9	14.3	15.4	23.5	9.0	92	56	93	80	0.9	12.2	1.1	4.7	0	6	3	C 0	SW 5	C 0
18	113.4	110.5	107.5	110.5	13.7	24.4	17.3	18.2	25.0	11.8	92	52	73	72	1.3	14.8	5.2	7.1	2	0	5	SSE 2	S 7	S 4
19	111.9	115.2	118.5	115.2	12.6	15.3	12.2	13.1	15.9	10.6	74	62	80	72	3.7	6.7	2.9	4.4	9	6	7	SW 5	SW 9	SW 8
20	124.1	128.2	130.8	127.7	12.5	17.0	11.5	13.1	17.3	11.4	77	46	81	68	3.4	10.6	2.7	5.6	10	2	2	WNW 3	NNW 6	WSW 7
21	130.8	129.2	125.5	128.5	9.9	16.0	13.8	13.4	17.2	9.0	91	64	77	77	1.1	6.5	3.7	3.8	9	9	6	SW 3	W 7	SW 3
22	120.1	117.9	115.6	117.9	11.6	21.3	14.1	15.3	21.9	10.8	76	29	67	57	3.2	18.0	5.3	8.8	4	0	0	SW 5	WSW 5	S 1
23	114.8	114.2	113.4	114.1	11.2	22.4	12.0	14.4	22.7	9.4	85	43	96	75	2.0	15.4	0.5	6.0	2	1	3	SSW 2	SW 2	C 0
24	112.4	112.5	113.3	112.7	10.0	22.5	13.6	14.9	23.6	7.3	99	56	90	82	0.2	12.0	1.6	4.6	0	0	0	SE 1	S 3	C 0
25	112.8	111.5	110.2	111.5	10.8	21.1	14.8	15.4	22.4	9.8	97	68	90	85	0.4	7.9	1.6	3.3	5	0	2	C 0	ENE 3	C 0
26	108.6	107.0	107.3	107.6	9.7	21.6	17.7	16.7	23.7	9.3	97	64	72	78	0.3	9.3	5.7	5.1	3	0	0	C 0	SE 4	SE 1
27	105.6	103.5	105.3	104.8	11.0	15.9	13.8	13.6	18.6	10.5	97	94	80	90	0.3	1.2	3.2	1.6	5	9	2	C 0	SE 5	S 3
28	104.9	103.2	100.7	102.9	12.0	19.6	16.2	16.0	19.8	9.6	93	72	96	87	1.0	6.3	0.8	2.7	7	9	10 •	SW 1	SSE 2	SSE 2
29	101.6	103.6	106.8	104.0	13.8	14.1	12.8	13.4	16.8	12.7	90	89	83	87	1.6	1.8	2.6	3.0	10	10 •	10 •	WSW 3	W 2	WSW 6
30	111.8	113.3	114.4	113.2	9.9	18.1	11.9	13.0	18.5	9.5	84	59	94	79	1.9	8.4	0.8	3.7	4	8	1	SW 5	SSE 2	SSE 1
31																								
M	111.6	111.7	112.1	111.8	12.0	18.4	13.8	14.5	19.6	10.6	89	65	84	79	1.6	7.9	2.6	4.0	6.0	5.8	4.1	2.3	4.8	2.7

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1	118.4	120.9	121.8	120.4	10.9	16.0	12.8	13.1	17.4	9.0	97	74	89	87	0.3	4.7	1.6	2.2	4	0	7	C 0	NE 4	NE 2
2	121.0	120.2	119.4	120.2	12.8	14.8	12.6	13.2	16.1	12.0	92	82	92	89	1.2	3.1	1.2	1.8	10	10	0	C 0	E 5	ESE 2
3	119.2	120.4	121.7	120.4	10.2	12.0	11.7	11.4	13.0	8.6	93	95	96	95	0.8	0.7	0.5	0.7	9	10 •	6	C 0	SSE 1	S 1
4	123.2	123.4	123.3	123.3	8.6	15.1	12.4	12.1	16.2	8.4	99	80	95	91	0.2	3.5	0.7	1.5	5	9	9	C 0	WNW 4	C 0
5	123.9	124.3	124.9	124.4	10.0	15.3	10.2	11.4	15.6	8.6	92	74	93	86	1.0	4.6	0.8	2.1	5	7	2	WSW 1	NE 4	NNE 1
6	124.1	123.2	121.3	122.9	8.1	15.4	10.6	11.2	16.7	6.8	97	74	91	87	0.3	4.6	1.2	2.0	7	9	0	SW 1	C 0	SW 2
7	119.3	116.9	115.5	117.2	9.3	16.4	9.5	11.2	17.6	7.5	93	61	100	85	0.8	7.2	0.0	2.7	10	4	10 ≡	C 0	SW 5	W 1
8	115.8	115.6	118.3	115.9	10.6	13.4	10.1	11.0	14.3	9.2	88	62	68	73	1.5	5.8	4.0	3.8	9	4	9	WNW 3	N 9	N 5
9	118.5	118.0	116.7	117.7	8.1	11.0	6.5	8.0	12.2	5.6	78	60	82	73	2.4	5.2	1.7	3.1	9	9	7	NW 5	N 9	NW 3
10	114.3	112.9	115.0	114.1	5.8	12.4	7.6	8.4	12.9	5.3	83	60	82	75	1.5	5.8	1.9	3.1	7	9	9	WNW 5	N 9	WNW 5
11	113.1	113.6	119.4	115.4	7.7	9.4	5.7	7.1	10.9	5.6	77	63	86	75	2.4	4.4	1.3	2.7	9	9	7	WSW 3	N 9	N 9
12	124.7	125.9	124.3	125.0	5.0	10.1	8.5	8.0	10.6	4.4	72	55	76	68	2.4	5.6	2.7	3.6	9	2	9	W 4	NNW 7	W 9
13	122.5	121.2	118.8	120.8	6.9	12.6	10.8	10.3	13.0	6.8	75	63	68	69	2.4	5.4	4.2	4.0	9	8	10	WSW 4	SW 4	SW 5
14	118.3	119.1	119.9	119.1	10.6	12.1	10.3	10.8	12.6	10.0	87	76	82	82	1.6	3.3	2.2	2.4	10	10	9	SW 2	W 5	SSW 3
15	117.5	115.2	113.1	115.3	4.9	15.2	11.4	10.7	15.4	4.8	95	59	83	79	0.5	7.2	2.3	3.3	0	9	6	SSE 2	S 3	C 0
16	111.1	112.5	114.0	112.5	10.9	11.3	10.3	10.7	12.2	9.9	89	91	82	87	1.4	1.2	2.2	1.6	10	10 •	6	W 2	WNW 2	W 6
17	120.4	123.2	123.7	122.4	6.4	13.4	7.4	8.6	13.6	6.0	83	46	86	72	1.4	8.4	1.5	3.8	0	2	0	W 5	NW 8	SW 2
18	120.8	120.8	123.7	121.8	10.0	13.6	7.2	9.5	14.2	6.6	91	74	91	85	1.1	4.0	0.9	2.0	9	9	4	WSW 5	NW 7	NNW 3
19	124.8	125.2	127.2	125.7	5.4	12.6	7.2	8.1	12.9	4.4	92	67	90	83	0.7	4.9	1.1	2.2	8	5	7	W 2	NW 7	NW 3
20	130.8	133.1	134.1	132.7	8.0	10.4	4.8	7.0	10.9	4.8	90	72	87	83	1.0	3.5	1.1	1.9	9	8	0	ESE 2	NE 2	C 0
21	134.8	135.2	135.4	135.1	2.5	10.4	5.5	6.0	11.1	1.9	89	63	66	73	0.8	4.7	3.0	2.8	9	2	0	SSW 1	S 2	SW 5
22	135.2	134.2	132.3	133.9	4.9	12.1	7.8	8.2	12.3	3.9	76	68	91	78	2.1	4.6	0.9	2.5	6	7	9	W 5	WSW 7	W 3
23	128.9	128.5	128.9	128.8	8.8	11.2	9.2	9.6	11.5	6.6	86	77	84	82	1.5	3.1	1.8	2.1	9	9	9	NW 5	N 6	NW 3
24	130.0	130.0	129.4	129.8	5.8	11.5	8.3	8.5	12.7	5.0	94	75	83	84	0.6	3.5	1.9	2.0	3	9	8	SSW 2	N 4	NW 1
25	127.4	127.7	127.6	127.6	7.6	11.4	5.3	7.4	11.9	5.2	96	84	94	91	0.4	2.2	0.6	1.1	9	8	0	WNW 3	NE 4	C 0
26	125.2	123.1	119.8	122.7	2.8	11.6	5.9	6.6	12.1	1.7	100	60	94	85	0.0	5.4	0.6	2.0	0	0	7	C 0	C 0	SSE 1
27	116.3	115.9	113.0	115.1	4.4	7.2	7.6	6.7	7.8	3.3	95	80	76	84	0.5	2.1	2.5	1.7	10	10	4	W 2	WSW 2	SW 5
28	109.5	109.1	108.5	109.0	9.1	14.0	12.3	11.9	14.2	7.6	87	75	81	81	1.6	4.1	2.7	2.8	10	10	0	S 3	SW 7	SW 7
29	106.8	105.8	107.9	106.8	10.8	14.4	9.9	11.2	16.3	9.7	92	81	81	85	1.0	3.1	2.4	2.2	9	9	1	SSE 2	S 5	WSW 9
30	111.9	112.9	110.0	111.6	7.9	10.7	7.2	8.2	11.6	7.1	79	70	86	78	2.2	3.9	1.5	2.5	6	5	0	WSW 8	WSW 8	SSW 5
31	101.3	101.7	102.1	101.7	8.4	8.9	7.1	7.9	12.1	7.1	77	80	80	79	2.5	2.3	2.1	2.3	4	4	8	SSW 8	WSW 8	SW 8
M	120.2	120.3	120.4	120.3	7.8	12.4	8.8	9.4	13.3	6.6	88	71	85	81	1.2	4.3	1.7	2.4	7.2	7.0	5.3	2.7	5.1	3.5

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.3	•	
2	7	0.7	•	●$^{0}5^{15}$..6^{20}–9^{10}
3	6	•	•	=5^{30}–24; ⌒^{1}1–8
4	6	38.8	•	●$^{1}13^{05-20}$ ●^{0}–13^{30} ●^{1}–13^{50} ●^{0}–14^{10}, 15^{45}–21^{15} ●^{1}–24; =0^{00}–7^{30}, 11^{40}–24
5	6	7.7	•	●$^{1}0^{00-30}$ ●^{0}–3^{10} ●^{1}–3^{50} ●^{0}–4^{40}, 5^{20}..6^{00}, 9^{25}–11^{20} ●^{1}–15^{15} ●^{0}–16^{10}; =0^{00}–6^{40}, 16^{10}–24
6	7	6.4	•	(K) NW 22^{38}– K^{0} 22^{50}–23^{50}–24; =0^{00}–8^{30}, 16^{40}–22^{38}
7	8	0.3	•	⚲$^{0}0^{40-120}$ ⚲^{1}–1^{52} ⚲$^{0}5^{10-28}$, 16^{40-50}, 17^{05-40}, 18^{30-50}, K^{0} 0^{00}–(K) SE 0^{40}; =1^{52}–5^{10}
8	7	•	•	
9	7	•	•	=4^{30}–11^{20}
10	6	3.4	•	=1^{20}–5^{45} ≡^{1}–6^{30} ≡^{2}–10 =–15^{30}
11	8	12.9	•	●$^{0}4^{40}$–6^{50} ●^{1}–7^{15} ●^{2}–7^{40} ●^{1}–10^{15} ●^{0}–11^{20}
12	8	•	•	
13	8	0.7	•	⚲$^{0}14^{35}$–15^{10}, 15^{20-40}; =21^{30}–24
14	8	1.1	•	⚲$^{0}11^{25-50}$, 14^{35-40} ⚲$^{1}16^{10-30}$; =0^{00}–9^{40}, ⌒$^{0}14^{35-55}$ ⌒$^{1}17^{30}$–18^{00}
15	8	•	•	⚲$^{0}0^{05-15}$, 0^{45}–1^{25}
16	8	•	•	=6^{20}–8^{20}, 18^{20}–24; ⌒^{0}3–8
17	7	•	•	=0^{00}–10^{30}, 16^{40}–24
18	7	•	•	=0^{00}–12^{30}
19	8	0.1	•	⚲$^{0}14^{08-28}$, 18^{45}–19^{03}, 21^{50}–22^{10}, 23^{35-45}
20	8	•	•	⚲$^{0}10^{-35}$; ⌒^{1}23–24
21	7	•	•	⌒$^{1}0^{00}$–9
22	7	•	•	=6^{20}–11^{10}, 17^{30}–24
23	7	•	•	=0^{00}–9^{30}, 14^{30}–22^{10} ≡^{0}–22^{30} ≡^{2}–23^{35} =–24; ⌒^{0}4–8
24	7	•	•	=0^{00-40} ≡^{2}–3^{35} ≡^{0}–6^{25} =–12^{30}, 17^{20}–24
25	6	•	•	=0^{00}–24; ⌒^{0} 20–24
26	7	•	•	=0^{00}–11^{30}, 17^{40}–24; ⌒$^{0}0^{00}$–4 ⌒^{1}5–8
27	6	3.8	•	●$^{1}11^{05-35}$ ●^{0}–12^{05}; =0^{00}–8^{30}, 12^{05}–13^{30}; ⌒^{0}23–24
28	6	6.0	•	●$^{0}19^{20}$–20^{25} ●^{1}–20^{40} ●^{0}–24; ⌒$^{0}0^{00}$–8
29	6	2.2	•	●$^{0}0^{00-20}$..1^{35}, 9^{40}–17^{15}, 19^{40}–21^{40}; =0^{00}–8^{30}, 14^{10}–24
30	7	•	•	=0^{00-30}, 17^{30}–20^{10}, 21^{20}–24
31				
Σ	-	84.4	-	

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1	7	•	•	=0^{00}–9^{30}, 23^{30}–24; ⌒^{1}1–10
2	7	•	•	=0^{00}–11^{30}
3	5	1.1	•	●$^{0}11^{05}$–14^{25}; =7^{20}–24
4	6	•	•	=0^{00}–24
5	7	•	•	=0^{00}–9^{30}, 18^{40}–24; ⌒^{1}2–10
6	7	•	•	=0^{00}–6^{50} ≡^{0}–8^{10} =–10^{30}, 17^{20}–19^{30}; ⌒^{1}2–6
7	7	0.0	•	●$^{1}23^{35}$–24; =1^{10}–3^{30}, 5^{25}–10^{30}, 16^{20}–19^{35} ≡^{1}–21^{20} =–24; ⌒$^{1}18^{19}$
8	8	•	•	●$^{1}0^{00}$–1^{25}; =0^{00}–9^{20}
9	8	0.1	•	⚲$^{0}20^{25}$–40
10	8	0.0	•	⚲$^{0}16^{25}$–40, 17^{35}–18^{10}
11	8	0.8	•	⚲$^{0}15^{15-20}$, 15^{30}–40, 19^{40}–20^{10}, 21^{40}–22^{10}, 23^{20}–40
12	8	•	•	
13	8	•	•	≫2^{30}–5^{10}
14	7	•	•	=4^{30}..10^{10}
15	6	•	•	=4^{30}–24
16	6	1.8	•	●$^{0}8^{15}$, 9^{30}–12^{30}..13^{40} ⚲$^{0}21^{34}$–23^{05}; =0^{00}–8^{15}; ⌒^{0}2–8
17	8	0.8	•	
18	7	2.0	•	●$^{0}4^{10-45}$, 5^{25}..6^{10} ⚲$^{0}10^{15-25}$, 13^{05-10}, 13^{25}–14^{20}, 15^{15-25}, 15^{35-50}; =7^{30}–9^{30}, 18^{40}–24
19	8	1.4	•	=0^{00}–5^{30}; ⌒^{1}22–24
20	7	1.5	•	⚲$^{0}6^{10-35}$, 7^{05}–8^{20}; =17^{10}–24; ⌒$^{1}0^{00}$–6 ⌒^{0}22–24; ⌒$^{1}8^{10-20}$
21	8	•	•	=0^{00}–2^{30}, 5^{20}–9^{30}, 16^{30}–18^{40}; ⌒$^{0}0^{00}$–9
22	8	•	•	=16^{30}–24
23	7	•	•	=0^{00}–6^{20}, 16^{30}–24
24	7	•	•	=0^{00}–10^{30}; ⌒^{1}3–10
25	7	•	•	=6^{30}–9^{10}, 16^{20}–24; ⌒^{1}2–10, 20–24
26	7	•	•	=0^{00}–7^{20} ≡^{1}–7^{45} ≡^{0}–8^{25} =–12^{30}, 15^{40}–24; ⌒$^{1}0^{00}$–10
27	5	•	•	=0^{00}–24
28	6	•	•	=0^{00}–24
29	6	4.2	•	⚲$^{1}16^{03-30}$ ●$^{1}17^{20}$–18^{05}; ≫22^{10}–24 (por. 16 m/sek); =0^{00}–16^{10}
30	7	•	•	⚲$^{0}2^{35}$–3^{10}; ≫0^{00}–2^{20} (por. 16 m/sek)
31	8	0.3	•	⚲$^{0}12^{25-40}$, 18^{05-20}; =0^{30}–6^{10}
Σ	-	14.0	-	

Gdańsk - Wrzeszcz φ = 54°23' λ = 18°36' Listopad - Novembre 1965

Dni	Ciśnienie P=900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	100.6	95.8	85.7	95.4	6.7	7.0	11.9	9.4	12.2	5.2	81	94	80	85	1.9	0.6	2.8	1.8	5	10 ●	9	SW 6	S 7	SW 9
2	86.3	86.5	91.2	88.0	9.7	7.3	8.1	8.3	12.1	7.1	60	83	71	71	4.7	1.7	3.1	3.2	9	9 ●	4	WSW 9	SW 14	WSW 8
3	96.7	98.5	102.3	99.2	5.4	7.7	6.1	6.3	8.3	4.5	84	67	73	75	1.4	3.5	2.5	2.5	9 ●	5	0	WSW 8	SW 8	WSW 8
4	108.2	112.6	118.1	113.0	5.0	9.0	6.7	6.8	9.3	4.6	87	72	88	82	1.1	3.2	1.2	1.8	3	9	9	SW 7	WSW 9	W 4
5	123.2	125.4	125.2	124.6	6.1	7.4	5.4	6.1	7.6	5.0	91	75	78	81	0.8	2.6	2.0	1.8	8	9	0	WNW 3	NW 3	W 7
6	123.3	123.0	121.3	122.5	7.3	8.8	8.1	8.1	9.0	4.7	90	90	87	89	1.0	1.1	1.4	1.2	10 ●	10	7	WSW 6	W 5	SW 5
7	118.7	118.8	120.4	119.3	6.8	8.8	5.3	6.6	9.1	4.6	90	80	91	87	1.0	2.3	0.8	1.4	9	8	0	WSW 5	WNW 4	WNW 2
8	122.4	123.5	123.1	123.0	3.2	8.4	3.0	4.4	8.7	1.6	97	75	91	88	0.3	2.7	0.7	1.2	6	5	0	SW 2	NW 2	C 0
9	121.4	119.8	118.2	119.8	-0.2	6.8	8.3	5.8	8.5	-1.2	98	84	96	93	0.1	1.6	0.5	0.7	9	10	10	SSE 2	W 5	NW 3
10	117.8	118.4	117.9	118.0	6.1	8.3	5.3	6.2	8.7	3.8	91	73	91	85	0.8	3.0	0.8	1.5	8	6	9	N 5	N 6	NNW 3
11	116.2	115.6	115.0	115.6	2.1	3.6	1.6	2.2	5.8	0.7	91	83	74	83	0.6	1.3	1.8	1.2	7	6 ✳	2 ✳	C 0	S 1	SE 2
12	113.9	114.5	115.4	114.6	0.4	-0.5	-0.9	-0.5	1.8	-3.4	76	90	77	81	1.5	0.6	1.3	1.1	8	9 ✳	10	E 8	E 6	E 6
13	116.3	117.1	117.6	117.0	-2.0	-3.4	-3.9	-3.3	-0.9	-4.8	66	74	64	68	1.8	1.2	1.7	1.6	9	10	10	E 6	SE 2	SE 5
14	117.5	118.0	118.2	117.9	-4.4	-4.4	-4.8	-4.6	-3.7	-5.4	65	70	76	70	1.5	1.3	1.0	1.3	10	10	10	ESE 2	E 5	SE 2
15	118.0	119.2	122.5	119.9	-5.5	-4.6	-5.2	-5.1	-4.4	-5.7	82	86	85	84	0.7	0.6	0.6	0.6	10 ✳	10 ✳	10 ✳	SSE 1	S 1	S 1
16	127.2	128.1	127.9	127.7	-4.7	-2.6	-3.0	-3.3	-2.3	-5.6	83	73	88	81	0.7	1.4	0.6	0.9	10 ✳	9	10 ✳	C 0	S 1	SW 2
17	124.8	123.8	122.1	123.6	-4.4	-5.3	-11.2	-7.5	-2.7	-11.4	81	88	90	86	0.8	0.6	0.3	0.6	9	10 ✳	4	SW 5	S 2	S 6
18	119.3	117.7	114.5	117.2	-11.2	-10.0	-10.3	-10.4	-9.3	-12.4	90	81	84	85	0.3	0.5	0.4	0.4	10 ✳	4	3	S 6	S 2	SSE 2
19	108.8	106.3	105.1	106.7	-10.5	-8.6	-8.5	-9.0	-8.3	-10.9	84	77	77	79	0.4	0.7	0.7	0.6	10	9 ✳	10	E 3	SE 3	SSE 2
20	104.2	105.1	104.9	104.7	-6.4	-5.4	-4.9	-5.4	-4.2	-8.8	89	85	83	86	0.4	0.6	0.7	0.6	10	10 ⚠	10	S 2	SW 1	SE 1
21	100.9	95.6	91.3	95.9	-5.6	-2.4	-1.8	-2.9	-0.9	-6.5	92	96	98	95	0.3	0.2	0.1	0.2	10 ✳	10 ✳	10 ✳	SE 2	NE 8	NE 7
22	96.2	102.4	108.2	102.3	-0.2	-1.0	-4.4	-2.3	0.8	-5.3	92	95	84	90	0.5	0.3	0.7	0.5	10	10 ✳	4	N 9	NNW 8	W 7
23	113.2	117.0	118.4	116.2	-6.5	-5.4	-7.3	-6.1	-5.4	-7.7	81	72	82	78	0.7	1.3	0.6	0.9	2	4	0	W 6	W 5	SW 6
24	116.8	114.4	112.3	114.5	-12.9	-9.2	-9.2	-10.1	-7.2	-13.1	84	82	79	82	0.4	0.5	0.6	0.5	8	6	4	S 3	S 3	SSE 5
25	109.5	109.7	110.3	109.8	-7.3	-4.0	-0.7	-3.2	-0.6	-10.6	88	87	93	89	0.4	0.6	0.4	0.5	10 ✳	10 ✳	6	SSE 7	S 5	S 3
26	101.6	95.3	95.8	97.6	-0.8	-0.8	1.6	0.4	2.3	-1.1	81	77	81	80	1.1	1.3	1.3	1.2	10	9	1	SSE 8	S 8	SW 5
27	97.9	95.2	82.0	91.7	-2.4	-2.5	0.3	-1.1	1.9	-3.4	89	82	96	89	0.5	0.9	0.2	0.5	1	10	10 ✳	SW 7	SSE 5	S 4
28	78.4	81.0	84.0	81.1	2.2	2.7	1.3	1.9	3.4	-0.3	89	82	89	87	0.8	1.3	0.8	1.0	6	9	10 ✳	S 4	SW 6	SW 8
29	92.3	98.1	95.3	95.2	1.6	1.6	-0.5	0.6	2.3	-1.0	80	76	94	83	1.4	1.7	0.4	1.2	10	2	9	WSW 8	WSW 7	SSE 5
30	84.7	87.5	93.8	88.7	1.6	4.0	3.1	3.0	5.9	-0.8	89	83	79	84	0.8	1.2	1.6	1.2	10 ●	9	10	S 8	S 4	SW 4
31																								
M	109.2	109.4	109.3	109.3	-0.7	0.8	0.0	0.0	2.3	-2.6	85	81	84	83	1.0	1.3	1.1	1.1	8.2	8.2	6.4	4.9	4.8	4.4

Grudzień - Décembre

1	91.1	87.2	93.2	90.5	-2.2	0.9	1.7	0.5	3.3	-2.5	86	96	85	89	0.7	0.2	1.0	0.6	3	10 ✳	9	SSE 2	SSE 7	SW 9
2	101.1	102.4	100.3	101.3	1.4	0.9	0.0	0.6	2.2	-0.6	85	77	86	83	1.0	1.5	0.9	1.1	9	9	10	SW 4	SW 6	S 4
3	92.5	92.7	95.1	93.4	0.4	2.3	1.8	1.6	2.6	-0.4	86	86	93	88	0.9	1.0	0.6	0.8	10	10	10	S 5	SSW 6	S 3
4	95.7	95.9	96.9	96.2	0.6	2.5	2.6	2.1	2.8	0.3	96	88	89	91	0.3	0.9	0.8	0.7	10	7	9	SSW 3	S 2	SW 6
5	98.9	99.0	84.0	94.0	0.5	0.1	2.1	1.2	3.0	-1.0	86	84	87	86	0.8	1.0	0.9	0.9	6	8	10 ✳	SW 7	S 6	SE 9
6	77.3	80.8	89.9	82.7	3.0	4.6	3.7	4.2	5.5	-0.1	70	77	77	75	2.6	1.9	1.9	2.1	9	9 ●	2	SW 14	SW 14	SW 12
7	96.7	99.6	102.6	99.6	2.7	4.3	3.2	3.4	4.6	2.4	86	74	88	83	1.0	2.2	0.9	1.4	9	9	10	SW 8	SW 8	SW 6
8	105.7	108.3	110.8	108.3	2.0	2.2	0.5	1.3	3.5	0.3	94	78	88	87	0.4	1.6	0.7	0.9	9	8	1	SW 1	WSW 6	SW 6
9	109.9	103.1	90.4	101.1	0.7	2.7	2.3	2.0	2.8	0.3	85	63	82	77	1.0	2.7	1.3	1.7	10	9	10 ✳	SW 7	SSW10	SSW 8
10	73.1	74.3	71.8	73.8	2.9	4.3	5.4	4.6	5.5	1.8	88	84	71	81	0.9	1.3	2.7	1.6	10 ●	9	9	SSW12	SSE 7	S 8
11	80.5	83.1	84.9	82.8	3.6	5.3	2.1	2.8	6.0	1.9	73	71	87	77	2.1	2.2	0.9	1.7	9	8	9	SW 9	SW 8	SSW 5
12	94.3	98.6	102.8	98.6	0.4	0.8	-0.1	0.2	2.4	-0.2	84	79	82	82	1.0	1.4	1.1	1.2	10	10	10	W 7	WNW 4	WNW 5
13	107.1	108.5	109.2	108.3	-1.2	-1.2	-2.7	-2.0	0.0	-3.6	76	76	71	74	1.3	1.3	1.4	1.3	10	7	9	NNW 5	NW 4	W 5
14	114.0	117.5	121.0	117.5	-3.7	-2.0	-2.2	-2.5	-1.5	-4.2	76	85	72	78	1.1	0.8	1.5	1.1	9	6 ✳	7	NW 7	NW 9	W 5
15	116.3	118.9	121.8	119.0	-2.6	-1.1	-3.2	-2.3	0.1	-4.2	95	91	79	88	0.2	0.3	1.0	0.6	10 ✳	9	7	S 1	NNW 2	WSW 3
16	121.1	120.3	119.7	120.4	-4.1	-3.2	-4.3	-4.1	-2.5	-7.1	73	79	91	81	1.2	1.0	0.4	0.9	4	4	3	W 3	W 5	W 6
17	117.3	116.6	115.7	116.5	-7.1	-5.7	-10.5	-8.4	-4.1	-11.1	82	72	84	79	0.6	1.1	0.4	0.7	0	9	0	SW 4	S 1	S 3
18	111.6	104.5	101.8	106.0	-6.7	-0.4	3.6	1.0	5.8	-12.6	91	96	95	94	0.3	0.2	0.4	0.3	10	10 ✳	10 ●	SSE 3	SSE 8	SW 5
19	101.5	101.0	100.3	100.9	9.3	10.6	9.4	9.7	11.3	5.5	93	87	91	90	0.8	1.6	1.1	1.2	10 ●	6	6 ●	SW 7	SW 9	W 8
20	106.1	110.8	111.3	109.4	3.9	5.8	4.4	4.6	9.5	3.5	92	83	80	85	0.7	1.5	1.7	1.3	6 ●	9	8	WSW 8	W 8	SW 7
21	110.7	110.5	112.1	111.1	2.7	3.7	1.2	2.2	4.5	1.1	93	77	92	87	0.5	1.9	0.5	1.0	9	9	4	SW 3	W 6	WSW 2
22	114.2	115.8	116.9	115.6	1.4	0.8	-0.5	0.3	2.1	-0.6	89	88	92	90	0.8	0.8	0.5	0.7	9	9	10	W 5	SW 3	S 1
23	114.7	112.8	107.2	111.6	-0.2	-0.2	-0.8	-0.5	0.4	-1.2	90	88	83	87	0.6	0.7	1.0	0.8	9	10	10	S 4	S 4	SSE 4
24	99.3	96.0	92.8	96.0	-1.4	0.3	-0.3	-0.4	0.7	-1.6	84	76	88	83	0.9	1.4	0.8	1.0	10	8	9	SSE 7	SSE 7	SSE 7
25	88.1	84.7	83.7	85.5	0.4	1.3	1.4	1.2	1.7	-0.3	88	81	87	85	0.8	1.3	0.9	1.0	10	10	10	SE 7	SE 6	S 7
26	82.7	87.0	91.7	87.1	1.1	3.4	2.3	2.3	3.5	1.0	96	76	73	82	0.2	1.9	1.9	1.3	10 ●	10	7	SSE 4	WSW 7	SW 7
27	96.6	96.3	93.9	95.6	2.3	2.5	0.4	1.4	2.7	0.3	73	70	88	77	1.9	2.2	0.8	1.6	9	3	10	SSW 7	S 6	S 5
28	91.8	93.6	96.8	94.1	-0.2	0.2	-0.7	-0.4	1.3	-1.2	88	77	91	85	0.7	1.4	0.5	0.9	10	9	3	SE 2	W 4	SW 6
29	102.0	104.9	104.2	103.7	-1.6	-0.8	-0.4	-0.8	0.4	-2.4	86	81	98	88	0.7	1.1	0.1	0.6	2	7	10 ✳	WSW 3	WSW 8	SW 5
30	102.7	98.6	95.5	98.9	-0.5	-0.4	0.5	0.0	0.7	-1.5	86	74	88	83	0.9	1.5	0.7	1.0	9	10	9	SW 7	S 3	SW 8
31	97.3	97.0	98.4	97.6	2.7	3.2	1.4	2.2	3.6	0.5	86	83	81	83	1.0	1.3	1.3	1.2	9	9 ●	9	SSW 5	SW 7	W 8
M	100.4	100.7	100.5	100.5	0.4	1.5	0.8	0.9	2.7	-1.2	86	81	85	84	0.9	1.3	1.0	1.1	8.4	8.4	7.7	5.5	6.2	5.9

Gdańsk - Wrzeszcz $H_s = 13\,m$ $H_b = 12{,}4\,m$ $h_w = 15{,}5\,m$ Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU k	POGODA
1	6	7.4	•	⚲°3^15–22 ●°9^35–15^40 17^05–19^20 ⚲'22^25–23^15; ⚲ 22^30–23^30
2	7	15.1	•	⚲°9^25–35 ⚲'11^40–12^10 ⚲°12^45–13^20 23^45–24; ⚲ 8^05–19^15 (por. do 22 m/sek)
3	8	3.0	•	⚲°0^00–20 ⚲'0^40–1^10 ⚲°1^20–40 ⚲'1^50–2^05 2^40–3^10 3^45–4^10 ⚲°4^25–40 5^05–6^15 6^40–7^05 7^20–30 ⚲'7^40 ⚲°8^20 ⚲'15^15–16^10; ⚲ 11^20–12^10 (por. 16 m/sek)
4	8	0.5	•	⚲°3^30–4^10 4^25–5^05; 14^02–35 15^20–30 17^35–18^15 ●°23^40–24
5	7	0.1	•	●°0^00–3^20
6	7	0.2	•	●°5^35...7^30 ●°...9^20–12^10; = 14^30–24
7	7	•	•	= 0^00–12^40; 20^30–24; ⌒'21–24
8	7	•	•	= 0^00–11^30; 15^40–23^20 ≡°–24; ⌒'0^00–10
9	5	0.1	•	≡°0^00–2^40 ≡–24; ⌣'3–9
10	7	2.1	•	●°4^35...5^40 ●°21^10–24; = 0^00–12^20; 15^30–24
11	7	1.8	•	●°0^00–20 ⚲°9^20–30 10^07–35 11^21–30; = 0^00–20; 6^10–7^15
12	6	1.0	•	⚲°8^32–45 ⚲'9^01–35 10^32–13^00 ⚲°–13^40 16^40–21^35
13	6	0.7	1	⚲°2^25–4^10 5^40 6^38 7^34 8^05 ⚲°8^20–10^05 ⚲'–10^40 ⚲°–14^25 ⚲'–15^10 ⚲°–17^20; 18^30–20^10; 23^15–24
14	8	0.1	2	⚲°0^00...6^30
15	5	2.9	2	⚲°3^35–24
16	6	0.6	4	⚲°0^00–9^35 15^40–24; = 9^35–24
17	6	0.1	4	⚲°0^00–1^40...2^15 9^35–10^15–12^30–14^15; 23^15–24; = 0^00–2^30; 9^15–24
18	6	0.0	4	⚲°0^00–8^35; = 0^00–24
19	5	1.3	4	⚲°7^15–8^05 ⚲'–10^35 ⚲°–14^45; 15^25–18^35; = 0^00–7^15; 14^45–24
20	5	0.5	4	△°10^10–14^35; = 0^00–24
21	4	11.5	4	⚲°5^35–8^05 ⚲'–10^40 ⚲°–12^20 ⚲'–24; = 0^00–24
22	4	2.3	14	⚲'0^00–5^40 △°7^35–9^05 ⚲'–10^35 ⚲°11^42–12^15 ⚲'–13^20 ⚲°–15^15; 21^10–45; 23^25–35; 23^50–24; ⚹'5^40–7^35; = 0^00–5^40
23	8	•	14	⚲°0^00–15 ⚲'–2^15
24	5	0.6	14	= 6^30–24
25	5	0.7	16	⚲°3^40–8^30 ⚲'–10^20 ⚲°–13^35; = 0^00–3^10; 13^35–24
26	6	0.6	17	⚹°10^40–11^35 ⚲°14^05...40; 15^40–19^10; ⚹°10^40–11^35 por. wiatru 17 m/sek 10^20–11^45 por. wiatru 16 m/sek 13^20–15^05; = 0^00–24
27	5	6.1	17	⚲°16^35–19^30 ⚲'–24; = 0^00–16^35
28	7	0.2	20	⚲'0^00–3^35 ⚲°–2^40 17^40...22^20; = 2^40–12^30
29	7	0.6	18	⚲°0^25...5^10; = 15^15–24
30	6	1.3	16	⚲°3^10–4^50 5^30–6^20 ⚲°–6^35 ●°–10^15; = 0^00–3^10; 10^15–24
31				
Σ	–	59.4	–	

Grudzień - Décembre

1	5	1.7	13	⚲°10^25–11^35 ⚲'–12^20 ⚲°–13^40 ⚲°–17^40 ⚲°–20^45; = 0^00–24
2	6	•	10	= 0^00–1^30 6^30–24
3	6	0.0	9	⚲°8^10...9^35; = 0^00–24
4	6	0.1	7	= 0^00–24
5	7	4.4	6	●°1^10–3^35 ⚲°20^40–22^20 ⚲'–23^05 ⚲°–24; = 0^00–7^15; 13^30–23^05
6	8	0.8	5	⚲°0^00–15 ●°–2^10 ⚲°9^05–20 10^20–11^07 11^28–12^05 12^20–13^35 13^45–14^10 14^30–15^20 23^25–35; ⚲ 14^15–24 (por. 18 m/sek)
7	7	0.6	5	⚲°7^20–35 20^30–45 22^05–17; ⚲ 0^00–4^30 (por. 18 m/sek)
8	8	•	pż.	●°5^35–8^35; = 7^10–9^35
9	7	2.6	pż.	⚲°13^10–19^35 ⚲°19^45–21^35 ●°–24; ⚲ 11^40–17^10 (por. 16 m/sek)
10	7	1.0	pż.	●°0^00–5^35 6^30–8^35; ⚲ 5^53–10^20 (por. 18 m/sek)
11	8	0.5	•	⚲°23^37–24
12	8	•	•	⚲°0^00–1^40 ⚲°–2^10 ⚲°3^05–4^20
13	7	0.0	•	
14	6	6.3	•	⚲°5^35–6^40 ⚲°8^16–40 9^05–10^45 11^10–13^05 13^20–40 14^15–25 ⚲°22^30–24
15	4	0.9	9	⚲°0^00–1^25 ⚲'–3^40 ⚲°–5^15 ⚲'–6^40 ⚲°–8^35 ⚲'14^15–30 17^35–18^05; = 8^35–13^30; 15^20–24
16	6	0.0	9	⚲°14^40–15^10; 15^45–16^08; = 0^00–24
17	6	•	9	= 0^00–24
18	4	4.6	8	⚲°11^32–12^40 ⚲°–14^28 ●°–22^15; 23^35–24; = 0^00–22^30; ∞ 14^40–22^40
19	7	2.2	pż.	●°0^00...8^30 ⚲°17^35–19^07 20^25–21^20; ⚲ 14^35–18^40 (por. 17 m/sek); = 8^30–12^20; 19^07–22^40
20	7	0.1	•	⚲°0^35–1^40; 5^32–45 ⚲'–6^05 ⚲°–7^20; 7^45–8^25
21	6	•	•	= 4^30–24
22	6	0.0	•	⚲°9^05–15; = 0^00–12^30; 15^30–24
23	6	•	•	= 0^00–24
24	6	•	•	= 0^00–24
25	6	0.3	•	⚲°13^05–15^35; = 0^00–24
26	7	0.0	•	●°3^30–5^30...8^05; = 0^00–3^30; 8^05–12^30; 15^40–24
27	7	•	•	= 0^00–1^40; 15^30–24
28	6	2.2	•	⚲'17^40–18^45 22^07–23^35; = 0^00–13^30; ⌣°4–11
29	7	10.8	6	⚲'1^14–40 ⚲°14^40–17^05 ⚲'17^43–18^10 ⚲°19^50–20^02 ⚲'–21^05 ⚲°–21^15 ⚲'21^35–22^10 ⚲°22^35–23^20
30	6	0.2	26	⚲'0^40–2^25 ⚲°3^15–5^28 13^10–15^15 ⚲'17^40–18^10 ⚲°–19^35; = 9^35–24
31	6	0.2	19	●°12^15–15^10–16^20 ⚲°21^35–24; = 0^00–20^35
Σ	–	39.5	–	

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ *Styczeń – Janvier 1965*

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	78.2	79.6	79.5	79.1	2.2	2.4	1.8	2.0	2.9	1.3	91	87	83	87	0.7	1.0	1.2	1.0	10 •	10	0	SSW 6	SSW 6	SSW 7
2	78.6	78.3	80.3	79.1	0.6	0.9	0.2	0.5	1.8	0.2	90	92	82	88	0.6	0.5	1.1	0.7	10	10	10	SSW 6	SSW 4	WSW 6
3	83.3	85.9	89.5	86.2	-1.2	0.0	-1.9	-1.2	0.2	-1.9	91	90	100	94	0.5	0.6	0.0	0.4	10	9	10 ≡	SSW 3	SSW 1	SW 1
4	93.5	96.1	97.0	95.5	-0.8	0.0	-1.8	-1.1	0.3	-3.3	89	71	77	79	0.6	1.8	1.2	1.2	10	7	0	N 3	WNW 2	W 2
5	83.9	81.4	84.0	83.1	-2.8	-1.2	-1.8	-1.9	-0.4	-4.4	86	80	88	85	0.7	1.1	0.7	0.8	10	3	10 *	SSW 8	W 8	W 12
6	88.6	90.4	93.1	90.7	-3.0	-2.8	-5.0	-4.0	-1.8	-5.0	81	73	83	79	0.9	1.3	0.7	1.0	3	8	10	W 10	NW 11	WNW 8
7	96.2	97.1	96.0	96.4	-5.3	-5.9	-8.6	-7.1	-3.9	-8.7	70	76	89	78	1.2	0.9	0.4	0.8	10 *	10	0	NNW 7	WNW 5	WSW 2
8	87.4	81.1	73.1	80.3	-4.7	-3.7	0.4	-1.9	0.6	-8.9	79	92	92	88	0.9	0.4	0.5	0.6	10	10 *	10 *	SSW 7	SSW 7	SSW 6
9	71.8	77.0	83.4	77.4	2.3	0.0	-8.5	-3.7	2.6	-8.5	93	90	71	85	0.5	0.6	0.9	0.7	10 •	10 *	6	SW 6	W 6	NE 5
10	86.1	90.1	99.4	91.9	-12.7	-13.2	-12.7	-12.8	-8.5	-13.8	77	80	85	81	0.5	0.4	0.4	0.4	6	7 *	0	ENE 6	ENE 5	WNW 2
11	106.1	107.1	106.2	106.5	-12.2	-7.3	-11.8	-10.8	-6.8	-13.1	89	76	82	82	0.3	0.8	0.4	0.5	0	2	2	SW 1	S 2	SSE 4
12	101.9	100.2	99.6	100.6	-9.9	-6.5	-7.7	-8.0	-5.6	-12.6	52	70	76	66	1.4	1.1	0.8	1.1	6	9	0	SSE 4	SSE 3	SSE 4
13	96.9	95.6	96.4	96.3	-8.3	-3.1	-5.0	-5.4	-2.7	-8.6	83	61	80	75	0.5	1.9	0.8	1.1	2	4	8	SSE 5	SE 4	S 4
14	96.7	95.0	92.9	94.9	-2.8	-0.2	-2.0	-1.8	0.3	-5.0	86	72	79	79	0.7	1.7	1.1	1.2	10	0	10	S 3	SSE 4	SSE 4
15	96.3	99.7	101.8	99.3	0.8	1.6	-1.9	-0.4	1.9	-2.1	86	78	87	84	0.9	1.6	0.7	1.1	10	10	0	SW 5	SSW 6	SSW 4
16	98.4	96.4	95.2	96.7	-1.8	-0.3	-3.2	-2.1	-0.2	-5.0	92	80	81	84	0.4	1.2	0.9	0.8	10 *	10	10 *	ESE 5	S 5	S 5
17	85.3	78.6	72.9	78.9	-2.0	-1.6	1.4	-0.2	1.6	-5.4	83	84	94	87	0.9	0.9	0.4	0.7	9	10	10 •	S 8	S 10	S 9
18	70.6	72.0	73.6	72.1	1.6	2.1	0.4	1.1	2.2	0.4	91	85	88	88	0.7	1.0	0.8	0.8	10	9	8	S 5	SSW 5	S 4
19	73.8	74.8	77.6	75.4	-0.8	-1.2	-1.4	-1.2	0.4	-1.5	94	98	100	97	0.4	0.1	0.0	0.2	10	10	10 ≡	SSE 3	S 2	SSW 2
20	80.8	81.1	77.1	79.7	-1.4	-2.5	-1.2	-1.6	-1.1	-2.5	98	98	93	96	0.1	0.1	0.4	0.2	10 ≡	10 ≡	10 *	ESE 4	E 5	ENE 5
21	76.2	78.9	83.9	79.7	-0.6	-0.2	-0.2	-0.3	0.3	-1.4	93	90	90	91	0.4	0.6	0.6	0.5	10 •	10 *	10	ESE 8	ESE 7	E 7
22	85.2	87.5	92.9	88.5	-0.8	0.4	-0.2	-0.2	0.5	-1.4	93	92	92	92	0.4	0.5	0.5	0.5	10 *	10	10	SE 3	SSE 5	SSE 2
23	97.3	98.7	100.6	98.9	-3.2	-0.7	0.1	-0.9	0.1	-3.4	90	90	98	93	0.5	0.6	0.2	0.4	10	10 *	10 △ ≡	NNE 1	NE 3	ENE 2
24	102.8	104.2	104.3	103.8	0.0	0.4	0.0	0.1	0.6	-0.1	96	96	98	97	0.2	0.3	0.1	0.2	10 *	10 ≡	10 • ≡	ESE 2	SE 1	E 1
25	101.7	100.6	99.4	100.6	-2.6	-7.2	-8.3	-6.6	0.0	-8.9	91	88	83	87	0.5	0.4	0.5	0.5	10 •	10 *	10 *	E 6	E 5	E 4
26	98.2	98.4	99.1	98.6	-6.7	-6.9	-5.5	-6.6	-5.5	-9.3	86	91	90	89	0.4	0.3	0.4	0.4	10	10 *	10	E 3	E 3	ESE 4
27	101.4	102.3	101.9	101.9	-6.2	-5.4	-4.4	-5.1	-3.6	-6.3	92	85	79	85	0.3	0.6	0.9	0.6	10	10	10	E 4	ESE 6	ESE 9
28	101.3	101.3	100.1	100.9	-7.3	-6.8	-6.6	-6.8	-4.4	-7.8	79	83	83	82	0.7	0.6	0.6	0.6	9	10	10	ESE 8	ESE 9	SE 6
29	96.3	93.6	90.2	93.4	-5.7	-3.4	-1.2	-2.9	-1.2	-6.6	87	85	93	88	0.5	0.7	0.4	0.5	10	10 •	10 •	SE 8	SE 6	SE 4
30	88.7	89.9	88.6	89.1	-0.2	-0.6	-2.1	-1.2	0.1	-2.1	96	83	96	92	0.2	1.0	0.2	0.5	10 *	9	10 *	SW 2	WNW 2	NNE 3
31	89.6	92.1	92.8	91.5	-4.2	-1.7	-4.7	-3.8	-1.5	-5.4	94	86	95	92	0.3	0.8	0.2	0.4	10	9	8	W 3	SW 4	WSW 3
M	90.1	90.5	91.0	90.5	-3.3	-2.4	-3.3	-3.1	-1.0	-5.1	87	84	87	86	0.6	0.8	0.6	0.7	8.9	8.6	7.5	4.9	4.9	4.5

Luty – Février

1	90.5	90.3	91.5	90.8	-9.9	-4.6	-5.3	-6.3	-4.4	-10.5	88	88	90	89	0.4	0.5	0.4	0.4	10 *	8	8	SW 2	WSW 2	W 2
2	94.5	97.8	102.1	98.1	-5.0	-3.6	-6.4	-5.4	-3.2	-9.3	88	85	83	85	0.5	0.7	0.6	0.6	10 *	7 *	8	WSW 3	NW 3	W 3
3	100.0	97.6	97.0	98.2	-13.3	-4.8	-1.8	-5.4	-1.8	-13.5	84	86	88	86	0.4	0.6	0.7	0.6	3	8 *	10 *	SW 2	SW 4	W 3
4	97.0	100.4	103.0	100.1	-4.9	-8.2	-17.3	-11.9	-1.8	-17.4	93	75	85	84	0.3	0.8	0.2	0.4	10 *	9 *	0	NW 3	N 6	NW 2
5	101.3	101.7	104.6	102.5	-23.8	-17.3	-18.9	-19.7	-17.2	-24.8	80	85	77	81	0.2	0.2	0.3	0.2	10	0	0	N 1	E 1	NW 2
6	105.1	104.0	101.4	103.5	-27.9	-14.7	-16.9	-19.1	-13.5	-28.0	76	78	75	76	0.1	0.4	0.4	0.3	3	8	6	C 0	SW 1	S 2
7	99.8	95.4	80.7	92.0	-17.9	-10.5	-5.4	-9.8	-5.4	-21.1	84	74	90	83	0.2	0.7	0.4	0.4	8	5	10	SW 2	SW 5	SW 6
8	72.7	77.0	86.7	78.8	-4.6	-4.4	-6.8	-5.6	-2.5	-6.8	88	84	75	82	0.5	0.7	0.9	0.7	10 *	10 *	10 *	NW 7	NNE 8	NNE 8
9	93.4	96.4	96.3	95.4	-11.8	-12.1	-13.3	-12.6	-6.8	-13.5	78	74	84	79	0.5	0.6	0.4	0.5	10	0 ←	4	N 6	WNW 3	SW 4
10	85.1	78.5	81.6	81.7	-6.2	-4.2	-3.4	-4.3	-0.8	-13.3	86	89	76	84	0.5	0.5	1.1	0.7	10 *	10 *	8	SW 9	SW 8	W 7
11	86.6	91.6	96.1	91.4	-3.0	-2.1	-5.8	-4.2	-1.7	-7.1	81	66	87	78	0.9	1.7	0.5	1.0	10 *	8	0	NW 7	NW 6	W 3
12	96.3	94.2	90.9	93.8	-4.4	-0.8	0.6	-1.0	0.6	-7.4	93	89	96	93	0.3	0.6	0.3	0.4	10 *	10	10 •	W 6	SW 6	SW 6
13	84.8	79.2	74.1	79.4	0.2	0.6	0.4	0.4	1.0	0.2	86	88	90	88	0.9	0.8	0.6	0.8	10	10 *	10	SSW 8	SSW 8	SSW 7
14	68.8	67.9	73.0	69.9	0.2	-0.2	0.2	0.1	0.7	-0.3	90	94	86	90	0.6	0.4	0.9	0.6	10	10 *	10	S 6	S 10	S 5
15	82.3	86.6	88.7	85.9	-3.4	-1.0	-7.3	-4.8	0.2	-7.4	90	67	85	81	0.5	1.9	0.5	1.0	9	2	1	SW 6	SW 3	SE 2
16	92.4	96.1	99.0	95.8	-6.7	-6.1	-7.5	-7.0	-5.4	-10.5	94	94	96	95	0.2	0.2	0.1	0.2	10	10	10	SW 2	C 0	N 3
17	97.7	99.8	102.3	99.9	-6.0	0.0	-2.5	-2.8	0.5	-7.7	92	86	80	86	0.3	0.8	1.0	0.7	10 *	10	10	NNE 8	N 8	NE 8
18	102.2	103.0	103.8	103.0	-6.5	-6.9	-5.0	-5.8	-2.5	-6.4	86	80	85	84	0.5	0.7	0.6	0.6	10	10	10	N 5	NE 6	NE 7
19	105.2	105.7	109.1	106.7	-7.9	-5.0	-5.7	-6.1	-4.6	-6.9	84	76	77	79	0.5	1.0	0.9	0.8	10	10 △	9	NNE 9	N 6	NE 6
20	112.9	114.7	113.3	113.6	-6.0	-2.7	-3.6	-4.0	-2.6	-6.4	84	73	85	81	0.6	1.3	0.7	0.9	10	9	10	E 5	NE 3	WNW 1
21	106.3	100.1	91.6	99.3	-6.5	-2.3	-2.6	-3.5	-2.2	-6.9	91	74	91	85	0.3	1.4	0.5	0.7	10	10	10 *	SW 3	WSW 6	W 6
22	90.2	90.9	92.0	91.0	-7.7	-5.6	-12.3	-9.5	-0.5	-12.3	73	64	70	69	0.9	1.4	0.7	1.0	2	3	0	NW 3	WNW 4	W 2
23	89.4	91.2	94.1	91.6	-12.5	-7.2	-12.6	-11.2	-6.9	-15.4	77	66	81	75	0.5	1.2	0.4	0.7	10	2	10 *	SW 2	NW 5	WNW 2
24	94.2	88.6	79.5	87.4	-17.7	-6.6	-6.8	-9.5	-5.6	-17.8	79	83	85	82	0.3	0.6	0.5	0.5	6	10 *	10 *	SW 2	SW 5	SW 9
25	75.7	76.8	78.8	77.1	-8.5	-5.4	-9.7	-8.3	-4.5	-9.9	86	75	81	81	0.4	1.0	0.5	0.6	7	9 *	0	WSW 6	W 6	WNW 2
26	84.5	84.3	81.4	83.4	-18.7	-8.6	-12.3	-13.0	-6.1	-19.2	84	56	85	75	0.2	1.4	0.4	0.7	5	6	7 *	SW 3	SW 3	SE 1
27	73.1	71.8	73.6	72.8	-11.3	-4.2	-5.1	-6.4	-4.0	-16.5	86	84	93	88	0.4	0.7	0.3	0.5	10 *	10 *	10 *	E 2	SE 3	E 3
28	80.5	85.5	91.6	85.9	-11.3	-11.2	-16.7	-14.0	-5.1	-16.8	86	76	80	81	0.4	0.6	0.3	0.4	10 *	10	0	NW 8	NW 8	NW 4
29																								
30																								
31																								
M	91.5	91.7	92.1	91.8	-9.4	-5.7	-7.5	-7.5	-3.8	-12.0	85	79	84	83	0.4	0.8	0.5	0.6	8.7	7.6	6.8	4.6	4.9	4.1

Suwałki — $H_s = 165\ m$ — $H_b = 169{,}6\ m$ — $h_w = 13\ m$ — Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ h	POGODA
1	6	1.5	pż.	•0^00–4^15, 5^10–9^35, = 0^00–13^10
2	5	•	pż.	= 7^05–24
3	6	•	pż.	= 0^00–18^35 ≡ 2–24
4	7	•	pż.	≡ 0^00–3^10 ≡ –5^20
5	8	5.5	pż.	*6^35–7^05, *1–9^20, *–10^20, *10^40–50, 12^15–20, ▽0–12^25, 13^05–42, 13^43, 14^35, 14^52, 16^10, 20^10–24, ⊹1^35–8^15, ⊹0–10^40, ⊹1–10^45, ⊹0–12^45, 14^50–24, ≫8^55–9^35 (por. 15 m/sek), 11^40–50 (por. 19 m/sek)
6	8	0.0	8	▽0^00–1^45, 7^05–10^30, 16^40, 17^10, *0^22^10–24, ⊹1^00–6^15, ⊹0–13^45, ≫0^00–8^00 (por. do 19 m/sek), 10^30–13^45 [5.I: 10^50–12^44, 13^10–24 (por. do 19 m/sek)]
7	8	0.0	8	*0^00–2^40, 3^10–8^15, 12^50–13^10, ≡ 23^45–24
8	5	8.0	8	*0^20–12^35, •0–13^45, 15^30–16^40, •0–18^35, •0–19^38, *0–23^45, *0–24, ≡ 1^00–1^40 ≡ –2^50, 8^10–14^45 ≡ 0–18^40 ≡ –24; ∽0^12^40–13^45, 15^30–18^35
9	6	1.5	pż.	*0^00–3^0, •0–7^5, •1–3^30, •0–8^05, •0–12^15, *0–13^10 ←→ –15^05, *0–16^40, ▽0^22^50–24, = 0^00–15^05
10	7	0.0	pż.	⊹0^00–2^0, *0^14^45–12^40
11	8	•	pż.	= 6^10–8^40, ⌣0^1–12, ⌣1^16^30–18^20
12	7	•	pż.	
13	7	0.2	pż.	◉⌣0^23^40–24, ≡ 22^10–24, ∽0^23^40–24, ▽0^19^35–20^15
14	6	0.0	pż.	◉⌣0^00–1^35, = 0^00–24, ∽0^0^00–1^35
15	7	0.1	pż.	*0^2^10–3^40, = 0^00–6^10, 17^15–24
16	6	0.5	1	*0^5^15–10^12, 12^20, 14^25–15^40, 19^20–24, = 0^00–24
17	6	3.4	2	*0^0^00–1^35, *0^9^40–10^05, *1–10^40, *0–11^45, •0^18^47–21^44, ⊹0^3^35–15^35, ≫8^20–12^50 (por. 19 m/sek), 12^50–13^40, 17^40–20^02 (por. 18 m/sek 18^05–20^02), = 0^00–2^20 ≡ 0–4^40 ≡ –9^40, 11^45–15^25
18	7	•	pż.	•0^7^15–2^10, *0–3^40, •0^4^46–5^25–6^10, = 0^00–11^30, 23^10–24
19	4	•	pż.	= 1^00–16^45 ≡ 1–24
20	3	3.9	pż.	*0^17^40–21^15, *1–24, ⊹1^23^25–24, ≡ 1^00–6^10 ≡ 0–7^15 ≡ –7^45 ≡ 0–13^20 ≡ –24
21	6	1.9	16	*1^0^00–1^40, *0–5^45, ◉0–7^35, *0–11^40, ⊹1^0^00–5^45, = 0^00–24, ∽0^5^45–13^00
22	6	1.0	16	*0^2^40–11^50, •0^14^20–15^30, *0–20^15, = 0^00–24
23	6	3.6	14	*0^11^20–14^40, 15^15–16^50, •0^17^35–20^15, △0–21^25, *0–24, = 0^00–1^35 ≡ 0–23^40 ≡ –24
24	2	1.1	15	*0^0^00–1^35, 4^40–11^30, 13^05–14^10, •0^19^35–22^20, = 0^00–1^25 ≡ 0–10^40 ≡ –11^35 ≡ 0–12^45 ≡ 1–15^25 ≡ 2–19^20 ≡ 1–24
25	6	0.1	14	◉0^4^25–7^20, *0^10^45–11^20, 15^30–17^40, 21^35, = 1^0^00–2^35 ≡ –7^40 ≡ 0–9^15 ≡ –24, ∽0^4^25–10^20
26	6	0.0	14	*0^10^30–13^15, = 0^00–24
27	6	0.0	14	△0^9^35–12^10, = 0^00–20^10
28	6	0.3	14	*2^8^35–9^40, *1–9^50, *0–10^35, ⊹1^8^45–9^50, ⊹0–13^40, = 10^35–24
29	5	3.9	16	◉⌣0^11^33–19^40, ◉⌣1–20^15, ◉⌣0–22^40, = 0^00–24, ∽1^10^33–24
30	7	6.4	16	*0^3^40–8^30, 16^15–24, = 0^00–3^50 ≡ 0–4^45 ≡ –6^35 ≡ 0–8^45 ≡ –11^30, 15^30–24, ∽0^0^00–3
31	6	0.0	22	*0^0^00–1^40, *1–4^15, *0–5^45, = 0^00–23^35 ≡ 1–24
Σ	–	42.5	–	

Luty - Février

1	6	0.8	22	*0^6^15–9^06, 9^50–10^48, ≡ 1^0^00–5^40 ≡ –6^10, 9^15–24, V1^20–13^10
2	7	0.1	24	*4^35–5^40, *1–6^10, *0–7^20, ▽0^11^40–16^40, 22^45–24, = 0^00–7^30
3	7	1.3	25	▽0^0^00–2^25, 7^20–9^45, 11^35–13^50, *0^17^20–24, = 5^05–7^10 ≡ 0–7^40 ≡ –8^00, 16^10–24, V0^7^10–12^15
4	7	0.3	27	*0^0^00–1^40, 4^10–9^15, ▽0–10^30, 11^35–13^45, = 0^00–7^10
5	6	0.0	27	←→1^8^25–9^00, = 5^15–7^35 ≡ 0–8^25 ≡ –24, V0^7^15–12^30
6	5	•	27	= 0^00–7^35 ≡ 0–10^45 ≡ –24, V0^7^35–17^30
7	6	3.6	27	*0^14^25–20^15, 21^10–23^30, *1–24, = 0^00–24
8	6	1.0	30	*1^0^00–1^45, *0–8^30, *1–12^15, *0–24, ⊹0^21^5–24, = 0^00–12^10
9	7	0.2	32	*0^0^00–6^10, ▽0^7^20–8^20, *0–9^15 ←→0^10^26–12^30, ⊹0^0^00–4^40, = 9^30–10^20
10	5	3.7	33	*0^5^40–14^25, 14^50–15^02, *1–15^05, *0–15^10, ▽0^16^17–36, 17^20–30, ⊹0^5^40–13^50, ≫8^32–12^40
11	8	0.2	38	*0^3^20–10^15, 11^45, = 23^10–24
12	6	0.6	38	←→0^0^30–5^20, *0–7^45, 9^40, 11^20, 12^15, △0^17^35–18^15, •0^10^30–21^15, •0–23^30, = 0^00–17^35 ≡ 0–18^15 ≡ –24
13	5	3.4	32	*0^9^20–10^40, 20^35–24, = 0^00–4^15, 6^10–24
14	3	2.7	34	*0^0^00–1^35, 4^50–5^40, ▽1^17–35, ▽0^8^06–48, 9^24–33, *1–9^50, ▽0–9^55, 10^48–11^05, *0–14^36, 15^05–18^50, 19^45–20^15, 21^25–23^40, ≫9^50–14^20, = 0^00–8^05
15	8	0.0	36	*0^0^40–2^15–6^20, 23^45–24
16	6	0.5	33	*0^0^00–5^0–2^40, = 5^30–24
17	6	0.6	34	*0^0^30–1^10–4^6, ⊹0^6^10–11^40, = 0^00–24
18	6	0.0	35	*0^7^15–9^50–10^15, 15^20–18^50, = 0^00–21^15
19	6	0.0	36	←→0^0^09–2^45, *0–5^10, △0^7^40–12^50, ⊹0^1^45–7^20, = 0^09–12^50
20	7	0.0	32	△0^8^35–10^15, ≡ 16^15–24
21	6	0.1	32	*0^20^15–24, = 0^00–24
22	8	0.0	32	*0^0^00–1^15, ▽0^6^43–17^38, = 0^00–2^30
23	8	0.0	33	▽0^7^35–8^10, *0–9^30, ▽0^10^40–55, *0^19^40–24, = 1^00–6^10
24	7	2.9	33	*0^0^00–2^35, 10^55–13^15, 17^40–24, ⊹0^19^30–24, = 5^10–6^15
25	6	1.5	33	*0^0^00–3^10, 5^05–50, ▽0^7^05–45, ▽1^8^02–10^10, ▽0^11^07–13^10, 13^25–14^07, 15^30–39, 16^20–35, ▽1–17^40, ▽0^21^45–22^05, ⊹0^0^00–3^40, ⊹1^8^40–11^20
26	7	0.3	37	▽0^15^01–16^10, ▽0^20^20–45, 21^05–20, = 5^20–11^40
27	5	4.3	38	*0^7^05–9^15, 12^10–24
28	7	0.2	45	*0^0^00–1^40, *1–5^10, *0–10^15, 18^30, 19^10, ⊹0^6^20–13^45
29				
30				
31				
Σ	–	28.1	–	

Suwałki

φ = 54°06′ λ = 22°57′ **Marzec – Mars 1965**

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	94.2	92.0	86.6	90.9	-24.0	-8.3	-8.9	-12.5	-7.5	-25.7	79	63	76	73	0.2	1.2	0.7	0.7	6	10 *	10	C 0	ESE 6	E 4
2	81.5	78.9	76.4	78.9	-5.8	-2.8	-1.3	-2.8	-1.3	-9.3	89	86	95	90	0.4	0.7	0.3	0.5	10 *	10 *	10 *	E 3	E 3	E 3
3	72.3	69.7	70.9	71.0	-0.2	0.7	-2.0	-0.9	0.9	-2.1	94	94	89	92	0.4	0.4	0.6	0.5	10 *	10 ●	10 *	NE 4	ENE 6	SSW 10
4	75.1	77.2	79.9	77.4	-3.8	-3.0	-4.3	-3.8	-2.0	-4.3	80	73	79	77	0.9	1.3	0.9	1.0	10	10	10	SE 6	SSE 7	SSW 6
5	82.2	84.2	89.7	85.4	-5.8	-3.2	-5.2	-4.8	-3.0	-6.3	89	77	90	85	0.4	1.1	0.4	0.6	10	10	10 *	SE 3	SW 3	W 2
6	96.8	101.0	104.6	100.8	-5.9	-4.8	-10.9	-8.1	-4.6	-11.3	87	71	80	79	0.3	1.2	0.5	0.7	10	0	0	N 5	N 4	NNE 3
7	108.6	110.1	110.4	109.7	-11.9	-8.4	-14.3	-12.3	-7.3	-15.6	86	89	87	87	0.4	0.3	0.3	0.3	10 *	1	0	NNE 2	N 3	C 0
8	109.7	108.1	106.1	108.0	-22.7	-7.7	-17.9	-16.6	-5.0	-25.2	96	62	84	81	0.0	1.3	0.2	0.5	10 ≡	3	0	C 0	SW 4	C 0
9	103.9	102.4	100.4	102.2	-24.5	-6.0	-7.9	-11.6	-5.0	-26.0	88	58	81	76	0.1	1.6	0.6	0.8	0	4	10 *	C 0	SSW 4	SW 2
10	103.8	104.1	105.8	104.6	-6.4	-1.6	-5.2	-4.6	-0.8	-7.9	94	75	90	86	0.2	1.3	0.4	0.6	10	7	10	W 4	SW 7	W 3
11	106.7	107.6	107.5	107.3	-3.5	0.8	0.4	-0.5	1.2	-3.2	94	79	76	83	0.3	1.4	1.5	1.1	10 ≡	10	10	W 2	WSW 3	W 5
12	106.8	106.1	105.1	106.0	-1.8	2.1	-4.8	-2.3	3.6	-5.5	81	57	88	75	1.0	3.1	0.5	1.5	6	5	0	WSW 3	SW 3	SW 1
13	105.2	105.1	105.5	105.3	-9.6	4.3	-2.8	-2.7	5.9	-11.6	91	46	82	73	0.3	4.5	0.9	1.9	7	0	0	SW 1	SW 3	SW 2
14	105.2	104.6	103.6	104.5	-12.1	4.2	-2.0	-3.0	6.0	-12.3	85	50	75	70	0.4	4.1	1.4	2.0	0	0	0	C 0	SW 3	SE 1
15	102.1	100.9	100.0	101.0	-9.3	5.1	1.8	-0.2	6.9	-9.3	95	58	78	77	0.2	3.7	1.6	1.8	0 ≡	0	10	E 1	SSW 2	SSW 2
16	96.6	94.0	92.2	94.3	2.4	5.4	3.4	3.6	6.5	1.3	82	68	75	75	1.3	2.9	2.0	2.1	10	10	9	S 4	S 2	S 6
17	92.6	93.2	92.2	92.7	1.7	3.2	0.6	1.5	3.4	0.6	96	97	98	97	0.3	0.3	0.1	0.2	10 ≡	10 ≡	10 ≡	SW 3	S 2	SE 1
18	88.5	87.9	87.9	88.1	1.2	2.6	2.0	2.0	4.4	0.5	98	98	94	97	0.2	0.2	0.4	0.3	10 , ≡	10 ≡	10	NE 1	SSW 1	SE 2
19	86.5	86.2	88.6	87.1	0.2	4.2	1.8	2.0	5.2	0.1	98	79	89	89	0.1	1.7	0.8	0.9	10 ≡	9	10	ESE 4	SSW 4	S 4
20	92.9	94.7	94.7	94.1	1.2	3.2	0.6	1.4	4.7	0.4	75	45	67	62	1.7	4.3	2.1	2.7	7	6	0	WSW 5	SW 6	SW 3
21	91.4	90.5	83.7	88.5	-2.0	1.8	0.0	0.0	2.4	-2.2	87	69	92	83	0.7	2.2	0.5	1.1	10	7	10 *	W 2	SSW 2	ENE 5
22	85.4	88.5	92.0	88.6	-1.4	0.8	-1.4	-0.8	1.8	-1.6	74	73	80	76	1.4	1.8	1.1	1.4	9	6	0	W 6	SW 4	W 2
23	94.5	94.1	91.4	93.3	-3.8	3.4	-1.2	-0.7	4.4	-3.9	89	52	68	70	0.5	3.8	1.8	2.0	0	7	0	SW 3	SW 4	SE 3
24	86.1	84.8	84.5	85.1	-1.4	0.3	0.9	0.2	1.3	-2.3	72	92	87	84	1.5	0.5	0.9	1.0	9	10 *	10	SE 8	SE 7	SSE 5
25	83.4	83.0	86.5	84.3	1.2	3.1	1.3	1.7	3.9	0.8	92	97	81	90	0.5	0.2	1.3	0.7	10	10 ≡	10	SE 3	S 5	SW 8
26	91.1	94.1	98.1	94.4	-0.2	2.2	0.0	0.5	4.1	-0.8	74	45	66	62	1.5	3.9	2.1	2.5	10	5	0	WSW 6	SW 2	NNW 2
27	105.0	108.8	111.7	108.5	-2.3	2.6	-1.4	-0.6	4.4	-3.2	72	50	80	67	1.5	3.7	1.1	2.1	2	0	0	NE 2	NNE 3	C 0
28	112.4	111.2	109.8	111.1	-1.3	7.4	4.6	3.8	8.0	-2.8	78	54	70	67	1.2	4.7	2.6	2.8	9	9	10	SE 1	SSW 5	S 4
29	107.0	105.9	102.6	105.2	2.4	4.2	4.6	4.0	5.3	1.7	84	92	92	89	1.2	0.6	0.7	0.8	10	10 ●	10	SE 2	SSW 3	SSW 5
30	92.2	92.7	98.2	94.4	4.4	3.8	0.0	2.0	6.6	0.0	79	90	78	82	1.8	0.8	1.3	1.3	5	10 ●	0	SW 6	WSW 3	WNW 9
31	97.5	97.5	99.9	98.3	1.4	5.6	0.2	1.8	6.5	-0.2	65	55	70	63	2.4	4.1	1.9	2.8	2	8	9	WNW 6	NW 9	NNW 6
M	95.4	95.5	95.7	95.5	-4.6	0.8	-2.2	-2.0	2.0	-6.0	85	71	82	79	0.8	2.0	1.0	1.3	7.5	6.7	6.1	3.1	4.1	3.5

Kwiecień – Avril

Dni	Ciśnienie I	II	III	Dies	Temperatura I	II	III	Dies	Max	Min	U I	II	III	Dies	Δ I	II	III	Dies	N,w I	II	III	D,v I	II	III
1	105.6	106.9	103.0	105.2	-2.8	1.8	0.0	-0.2	2.7	-3.7	80	57	63	67	1.0	3.0	2.2	2.1	0	6	10	NW 5	NW 6	WSW 6
2	97.2	100.4	102.4	100.0	0.4	2.6	-0.6	0.4	3.2	-0.6	82	46	52	60	1.1	4.0	2.8	2.6	0	2	0	WNW 7	NNW 8	N 3
3	101.1	97.7	93.7	97.5	-3.7	3.2	0.1	-0.1	4.4	-4.9	62	45	64	57	1.8	4.2	2.3	2.8	9	9	10	SE 3	C 0	SE 4
4	89.1	90.0	90.9	90.0	0.0	4.9	2.2	2.3	7.3	-1.6	82	73	89	82	1.1	2.2	0.8	1.4	10	10	0	SSW 4	WSW 2	ESE 1
5	95.4	98.3	100.6	98.1	0.2	4.0	2.6	2.4	4.4	-1.0	92	73	88	85	0.5	2.0	1.0	1.2	10	10	10	C 0	SE 3	NE 1
6	100.5	99.3	96.8	98.9	0.8	9.2	5.1	5.0	10.2	-0.1	90	50	63	68	0.7	5.8	3.3	3.3	10	9	0	SE 2	SSE 3	SSE 5
7	92.1	90.2	91.0	91.1	-0.3	9.2	4.2	4.3	10.2	-0.9	90	47	74	70	0.6	6.1	2.1	2.9	8	10	10	SE 2	S 4	WSW 1
8	90.9	93.1	98.2	94.1	2.6	2.3	-1.2	0.6	4.2	-1.2	77	80	78	78	1.7	1.4	1.2	1.4	10	10 ●	10	SW 3	WNW 2	ENE 8
9	101.3	101.8	101.9	101.7	-2.6	3.8	-0.8	-0.1	4.3	-2.8	61	42	48	50	2.0	4.7	3.0	3.2	10	4	0	ENE 6	E 8	E 6
10	101.9	101.4	100.9	101.4	-2.5	4.1	0.8	0.8	4.6	-4.1	57	36	51	48	2.2	5.2	3.2	3.5	7	10	10	E 6	ESE 7	ESE 7
11	100.4	98.6	98.0	99.0	-0.8	5.1	1.2	1.7	5.9	-2.0	63	42	54	53	2.2	5.1	3.1	3.5	5	4	0	ESE 7	SE 10	SE 6
12	98.0	97.4	98.0	97.8	0.4	8.6	3.2	3.8	9.4	-2.0	59	36	58	51	2.6	7.1	3.3	4.3	2	1	0	SE 7	ESE 9	ESE 5
13	97.7	96.3	97.6	97.2	1.0	8.4	3.8	4.2	9.6	-0.8	62	33	49	48	2.5	7.3	4.0	4.6	1	1	0	ESE 7	SE 11	SE 5
14	99.9	100.7	102.8	101.1	0.3	5.8	2.6	2.8	7.3	-1.4	69	47	74	63	1.9	4.9	2.0	2.9	6	10	10	SE 3	ESE 9	ESE 3
15	102.9	102.5	99.7	101.7	1.7	4.2	4.6	3.8	8.4	1.0	85	72	51	69	1.0	2.2	4.2	2.5	10	10 ●	9	ESE 3	SE 4	ESE 4
16	95.8	94.1	92.7	94.2	3.4	5.7	4.8	4.7	7.8	2.3	71	63	76	71	2.2	3.2	2.0	2.5	10	10	2	SE 5	SE 5	ESE 3
17	92.6	90.9	88.5	93.7	3.4	10.2	8.0	7.4	11.2	1.7	90	52	68	70	0.8	6.0	3.4	3.4	10	9	10	SE 3	SSE 8	SE 7
18	82.6	80.2	82.8	81.9	6.3	12.0	7.6	8.4	12.9	4.7	67	39	96	67	3.1	8.6	0.4	4.0	9	10 ●	10 ●	SE 10	SE 12	SSE 2
19	85.7	85.9	87.4	86.3	5.5	12.8	7.4	8.3	13.2	5.3	89	55	66	63	1.0	9.7	3.5	4.7	10 ●	7	0	ESE 6	SE 10	SE 4
20	88.9	89.3	90.6	89.6	6.2	12.6	10.0	9.7	13.7	4.8	79	45	61	62	2.0	8.0	4.8	4.9	4	10	10	ENE 6	E 9	E 5
21	89.7	88.7	87.8	88.7	6.8	9.6	8.6	8.4	13.2	6.8	90	80	80	83	1.0	2.4	2.3	1.9	10 ●	10	0	ENE 6	E 7	E 9
22	85.8	84.9	83.9	84.9	8.4	9.6	5.2	7.1	12.8	5.2	61	45	83	63	4.3	6.7	1.5	4.2	8	10	10	ENE 9	ESE 11	ENE 7
23	79.6	74.4	72.9	75.6	5.6	5.0	2.6	4.0	5.8	2.5	83	86	91	87	1.6	1.2	0.7	1.2	10	10 ●	10 ●	NNE 7	ENE 7	ENE 2
24	74.6	77.3	80.3	77.4	3.6	6.4	4.8	4.9	7.4	2.1	91	73	90	85	0.7	2.4	0.8	1.3	10 ●	9	9 ●	SE 5	SE 5	ESE 5
25	83.9	87.3	89.2	86.8	4.2	7.7	5.4	5.7	10.0	3.9	87	67	89	81	1.0	3.5	1.0	1.8	10	10	6	S 4	SSW 3	SE 2
26	90.1	89.4	89.0	89.5	5.4	13.9	6.6	8.1	14.3	3.5	92	54	90	79	0.7	7.4	1.0	3.0	8	10	10	SE 3	ESE 7	SE 4
27	88.2	87.2	88.1	87.8	7.0	13.6	10.4	10.8	16.4	5.8	94	38	62	65	0.6	8.6	4.8	4.7	10 ●	9	3	ENE 3	SE 10	E 3
28	90.0	89.3	90.3	89.9	8.6	14.6	9.4	10.5	15.7	5.3	77	39	58	58	2.6	10.0	5.0	5.9	5	7	5	E 5	ENE 10	ENE 6
29	90.0	90.2	92.3	90.8	7.3	13.2	9.4	9.8	14.2	4.5	70	46	73	63	3.0	8.1	3.2	4.8	5	5	8	ENE 4	E 3	NE 2
30	92.4	92.4	91.4	92.1	10.0	13.3	8.6	10.1	14.2	5.8	47	26	43	39	6.6	11.3	6.4	8.1	5	7	0	NW 5	NW 7	W 5
31																								
M	92.8	92.3	92.8	92.7	2.9	8.0	4.6	5.0	9.3	1.3	76	53	69	66	1.8	5.4	2.6	3.3	7.5	8.1	5.7	4.8	6.7	[illegible]

Suwałki $H_s = 165\,m$ $H_b = 169{,}6\,m$ $h_w = 13\,m$ Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	1.0	42	$*^{0}12^{20}-14^{25}$, $21^{30}-24$, $=6^{10}-10^{10}$
2	6	4.4	45	$*^{0}0^{00}-6^{15}$ $*^{1}-9^{30}$ $*^{0}-14^{20}$ 14^{45}, 16^{25} $*^{0}-21^{35}$ $22^{10}-24$, $=18^{10}-24$
3	6	7.3	50	$*^{0}0^{00}-7^{05}$ $*^{1}-8^{25}$ $*^{0}-9^{35}$ $\bullet^{0}-11^{15}$ $\bullet^{0}-13^{30}$ $*^{0}-17^{05}$ $*^{1}-19^{30}$ $*^{0}-24$; $+^{0}19^{35}-24$, $\gg 20^{10}-21^{30}$, $=0^{00}-24$
4	7	0.0	50	$*^{0}0^{00}-3^{10}$ $8^{45}-10^{10}$; $+^{0}0^{00}-4^{40}$; $=0^{00}-6^{15}$
5	6	0.0	50	$*^{0}7^{20}-9^{25}$ $\triangle^{0}13^{45}-17^{40}$ $*^{0}19^{35}-20^{15}$, $21^{45}-23^{40}$, $=9^{25}-24$
6	6	0.2	50	$=0^{00}-7^{15}$, $9^{10}-18^{20}$
7	7	0.0	50	$*^{0}1^{45}-4^{15}$, $5^{35}-9^{15}$, 10^{25}; $=1^{30}-10^{25}$; $V^{0}4^{20}-12^{15}$
8	7	.	48	$=3^{15}-5^{35}$ $\equiv^{2}-7^{40}$ $\equiv^{1}-7^{50}$ $\equiv^{0}-8^{30}$ $\equiv^{1}-9^{30}$ $=-10^{30}$; $V^{1}5^{25}-12^{10}$
9	7	0.5	46	$*^{0}19^{50}-24$, $=1^{30}-10^{30}$, $19^{20}-24$; $V^{0}7^{20}-8^{50}$
10	7	.	48	$*^{0}0^{00}-3^{35}$; $=0^{00}-10^{09}$, $23^{10}-24$
11	6	.	48	$=0^{00}-6^{20}$ $\equiv^{0}-7^{40}$ $=-15^{30}$
12	8	.	45	$=20^{15}-24$
13	6	.	38	$=0^{00}-24$
14	5	.	35	$=0^{00}-24$
15	7	0.0	34	$=0^{00}-5^{20}$ $\equiv^{0}-7^{25}$ $\equiv^{0}-7^{40}$ $\equiv^{0}-8^{10}$ $=-11^{30}$, $22^{10}-24$
16	6	1.2	26	$\bullet^{0}2^{45}-3^{15}$, $7^{40}-8^{35}$, $16^{20}-18^{30}$, $21^{25}-24$; $=0^{00}-24$
17	3	0.1	19	$\bullet^{0}0^{00}-2^{20}$, $5^{15}-8^{20}$ $\bullet^{0}21^{00}-23^{35}$; $=0^{00}-4^{28}$ $\equiv^{1}-8^{10}$ $\equiv^{0}-15^{20}$ $\equiv^{1}-24$
18	3	0.0	10	$\bullet^{1}2^{15}-6^{20}$ $\bullet^{0}-8^{15}$; $\equiv^{1}0^{00}-12^{10}$ $\equiv^{0}-14^{40}$ $=-16^{35}$ $\equiv^{1}-19^{15}$ $\equiv^{0}-20^{15}$ $=-24$
19	6	0.1	8	$=0^{00}-1^{30}$ $\equiv^{1}-7^{20}$ $\equiv^{0}-8^{40}$ $=-24$
20	8	4.6	6	$*^{0}2^{40}-4^{35}$; $23^{40}-24$; $=0^{00}-7^{20}$
21	8	3.6	8	$*^{0}0^{00}-3^{20}$ $*^{1}-5^{45}$ $*^{0}-6^{15}$, $18^{35}-24$; $=6^{10}-12^{10}$
22	8	.	6	$*^{0}0^{00}-1^{40}$
23	8	.	4	$=1^{36}-6^{50}$
24	7	0.6	pł.	$*^{0}11^{10}-15^{30}$ $\bullet^{0}-17^{45}$ $\bullet^{0}-18^{15}$
25	3	0.2	pł.	$\bullet^{0}4^{05}-5^{45}$ $\bullet^{0}16^{20}-17^{10}$ $*^{0}23^{40}-24$; $=5^{45}-8^{10}$ $\equiv^{0}-12^{38}$ $=-17^{30}$
26	8	.	pł.	$*^{0}0^{00}-1^{30}$ $*^{0}-2^{45}$
27	8	0.0	pł.	
28	7	0.5	pł.	$*^{0}5^{35}-40$ $\bullet^{0}21^{30}-24$
29	5	0.2	pł.	$\bullet^{0}0^{00}-2^{40}$, 3^{25} 6^{20}, $11^{35}-13^{40}$ $\bullet^{0}16^{15}-17^{45}$ $\bullet^{1}-18^{20}$ $\bullet^{0}-19^{35}$; $=5^{15}-13^{45}$ $\equiv^{0}-15^{48}$ $=-24$
30	6	0.5	pł.	$\bullet^{0}12^{20}-13^{15}$; $=0^{00}-8^{05}$
31	8	1.7	.	$*^{0}14^{25}-30$, $15^{15}-30$ $*^{2}16^{45}-17^{05}$ $*^{2}18^{20}-50$, $19^{25}-55$
Σ	-	26.7	-	

Kwiecień - Avril

1	8	0.0	1	$=10^{30}-24$
2	8	.	.	$*^{0}0^{10}-1^{45}$, $\gg 14^{10}-15^{50}$; $=0^{00}-5^{35}$
3	8	.	.	$\oplus^{1}9^{50}-10^{12}$
4	6	0.0	.	$*^{0}18^{50}-19^{10}$; $=6^{20}-13^{30}$, $21^{30}-24$
5	6	0.0	.	$\bullet^{0}15^{35}$.. 16^{20}, $17^{20}-18^{10}$; $=0^{00}-8^{30}$, $9^{10}-24$
6	7	.	.	$=0^{00}-10^{15}$
7	7	0.0	.	$\bullet^{0}13^{35}..45$, 14^{45} 15^{10} $16^{07}..20$; $=7^{05}-24$
8	7	0.1	.	$\bullet^{0}9^{15}..16^{15}$ $*^{0}-20^{10}$; $=0^{00}-7^{20}$
9	8	.	.	por. wiatru 15 m/sek $8^{20}-10^{15}$
10	8	.	.	
11	8	.	.	$\gg 10^{15}-15^{50}$ $16^{30}-17^{15}$
12	8	.	.	$\gg 10^{30}-11^{40}$ por. wiatru 14 m/sek $12^{50}-15^{30}$
13	8	.	.	$\gg 8^{35}-17^{25}$
14	8	0.0	.	$\bullet^{0}19^{45}..20^{05}$
15	6	0.0	.	$\bullet^{0}10^{15}..12^{35}$; $=3^{15}-7^{20}$ $9^{10}-13^{30}$, $15^{30}-18^{30}$
16	7	0.0	.	$\bullet^{0}9^{10}..30$, 10^{25} 11^{30}
17	7	0.0	.	$\bullet^{0}17^{50}-19^{35}$ $21^{45}..23^{40}$
18	6	2.6	.	$\bullet^{0}11^{10}-13^{15}$, $15^{50}-19^{20}$ $\bullet^{0}-24$; $\gg 7^{25-50}$, $8^{30}-9^{40}$, $12^{10}-17^{10}$
19	7	0.4	.	$\bullet^{0}0^{00-10}$, $5^{10}-7^{05}$; $\gg 10^{17}-16^{45}$
20	7	0.0	.	
21	7	1.4	.	$\bullet^{0}6^{10}-7^{20}$, $8^{25}-9^{35}$ $\bullet^{0}-12^{10}$; $\gg 14^{15-40}$
22	7	0.0	.	$\bullet^{0}14^{20}-15^{10}$ $16^{25}-17^{10}..20^{20}$; $\gg 8^{30}-18^{40}$ (por. 19 m/sek $9^{52}-11^{00}$, por. 18 m/sek 10^{55-58}, por. 19 m/sek 12^{59} 13^{00}, por. 17 m/sek 13^{56-59})
23	6	14.3	.	$\bullet^{0}4^{25}-5^{10}$ $8^{50}-20^{05}$ $\bullet^{1}-21^{10}$ $\bullet^{0}-24$
24	7	4.6	.	$\bullet^{0}0^{00}-5^{35}$ $6^{10}-10^{45}..11^{25}$ $\bullet^{2}-11^{45}$; 12^{40-50}, 14^{35-50}, 15^{05-25}, 17^{30-45} $\bullet^{1}19^{50}-20^{18}$ $\bullet^{2}-22^{30}$ $\bullet^{0}-24$
25	8	0.1	.	$\bullet^{0}0^{00}-4^{35}$, 7^{15-30}
26	8	3.1	.	$\bullet^{0}13^{35-45}$ $\bullet^{1}14^{15}-15^{25}$ $\bullet^{0}-17^{20}$; $K^{0}E$ 15^{05} $15^{15}-16^{38}$ W; $=2^{40}-9^{10}$
27	7	0.3	.	$\bullet^{0}0^{25-45}$, $1^{10}-2^{25}$ $\bullet^{1}3^{30-45}$ $\bullet^{0}6^{15}..8^{10}-10^{45}$ $\bullet^{0}14^{20-30}$, 15^{05-20}; $\gg 12^{25}-13^{45}$, 14^{22-50}; $=3^{05}-11^{20}$
28	8	.	.	$\gg 10^{10}-14^{50}$
29	7	0.0	.	$\bullet^{0}11^{30-35}$
30	8	0.0	.	$\bullet^{0}17^{30-32}$
31				
Σ	-	26.9	-	

Suwałki — φ = 54°06' — λ = 22°57' — Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	92.2	91.8	95.6	92.5	2.0	10.8	4.6	5.5	11.5	0.7	84	33	48	55	1.2	8.8	4.4	4.8	8	8	4	NW 5	NW 8	NNE 4
2	97.4	97.0	98.0	97.5	2.2	6.4	2.2	3.2	7.2	0.6	62	34	80	59	2.8	6.3	1.5	3.5	2	9	9	WNW 6	NW 5	W 1
3	99.5	99.7	100.4	99.9	0.3	4.0	-0.2	1.0	4.9	-1.0	84	38	67	63	0.9	5.0	2.0	2.6	9 *	9	0	N 4	N 5	NW 2
4	101.0	99.2	96.5	98.9	3.3	7.8	3.3	4.4	9.7	-3.5	43	32	61	45	4.3	7.2	3.0	4.8	0	4	0	WNW 3	SE 2	C 0
5	93.8	91.6	90.3	91.9	4.9	10.2	4.6	6.1	11.3	-1.8	49	20	45	38	4.5	9.9	4.7	6.4	4	9	0	ESE 4	SE 10	E 4
6	90.2	90.2	91.5	90.6	5.3	12.5	7.2	8.0	13.7	0.3	51	25	51	42	4.3	10.9	5.0	6.7	6	9	4	E 3	NE 4	SE 2
7	93.2	93.0	93.2	93.1	7.1	11.6	6.2	7.8	12.9	2.7	74	45	78	66	2.6	7.4	2.2	4.1	10	9	0	E 2	NE 3	SSE 1
8	92.5	92.7	93.8	93.0	7.6	14.3	8.7	9.8	14.7	3.0	73	42	88	68	2.8	9.5	1.3	4.5	5	9	10 •	SW 1	SSW 6	C 0
9	90.6	88.3	80.7	86.5	8.8	10.6	10.2	10.0	12.9	7.2	82	88	97	89	2.0	1.5	0.3	1.3	9	10 •	10	SSW 2	SSW 4	SE 5
10	73.7	75.2	79.2	76.0	7.6	10.6	6.8	8.0	11.5	6.8	82	69	75	75	1.9	4.0	2.5	2.8	10	8	2	SSW 5	SW 7	SE 1
11	84.5	88.3	92.6	88.5	7.3	14.6	11.8	11.4	16.5	2.6	96	52	66	71	0.4	8.0	4.7	4.4	0	9	9	E 2	N 3	NW 5
12	97.2	98.7	99.0	98.3	5.7	13.2	9.6	9.5	14.8	5.5	94	75	65	77	0.6	4.2	4.2	3.0	10	10	6	W 4	NW 5	WNW 3
13	100.9	99.8	98.5	99.7	8.2	14.0	10.2	10.6	16.1	3.0	53	39	68	53	5.1	9.7	3.9	6.2	2	4	2	NW 4	W 3	NW 1
14	95.6	92.4	91.5	93.2	10.2	17.6	10.8	12.4	17.7	3.2	81	40	66	62	2.4	12.1	4.5	6.3	5	9	0	C 0	SW 3	W 1
15	92.1	92.7	92.8	92.5	4.8	10.2	5.6	6.6	10.8	4.3	79	39	74	64	1.8	7.5	2.4	3.9	10	6	1	N 3	NE 3	NW 3
16	93.4	92.3	90.5	92.1	5.8	12.7	10.2	9.7	13.1	2.3	54	30	54	46	4.2	10.2	5.7	6.7	10	9	10	NE 4	E 3	SE 1
17	87.4	86.4	84.8	86.2	6.0	11.8	11.1	10.0	15.6	5.7	89	87	90	89	1.1	1.8	1.3	1.4	10	10	0	SE 4	SE 3	SE 1
18	78.2	81.9	85.4	81.8	14.8	18.7	12.8	14.8	19.5	9.4	91	53	81	75	1.5	10.1	2.8	4.8	9	9	9	SW 9	SW 8	NE 1
19	82.0	80.8	84.0	82.3	12.7	13.6	3.6	8.4	14.0	3.6	94	87	85	89	0.9	2.0	1.2	1.4	10	10	10 • R	SE 1	WNW 2	NW 7
20	92.2	94.6	97.1	94.6	5.5	8.9	6.4	6.8	10.1	1.9	73	52	68	65	2.2	5.5	3.1	3.6	10	9 •	7	SW 2	W 5	SW 2
21	101.5	103.6	106.0	103.7	5.4	12.3	6.6	7.7	12.5	1.8	80	40	79	66	1.8	8.6	2.0	4.1	5	8	6	SW 3	W 7	SW 1
22	108.3	108.2	108.5	108.3	7.2	12.8	8.4	9.2	13.0	2.0	63	42	64	56	3.8	8.6	4.0	5.5	4	6	2	W 4	WSW 4	NE 2
23	110.4	108.9	107.3	108.9	7.3	13.5	9.6	10.0	14.5	3.0	65	29	51	48	3.6	10.9	5.9	6.8	2	1	0	E 5	E 9	ENE 4
24	106.8	104.4	101.6	104.3	10.2	13.0	7.8	9.7	14.8	4.9	45	42	90	59	6.8	8.7	1.1	5.5	1	10	10 •	ESE 7	E 9	E 6
25	97.9	98.4	98.2	98.2	8.1	8.8	9.1	8.8	9.6	7.3	94	92	87	91	0.6	0.9	1.6	1.0	10 •	10 •	10	E 6	ENE 4	ENE 4
26	96.7	96.4	95.3	96.1	8.2	11.3	10.2	10.0	11.4	7.8	90	85	91	87	1.1	2.0	1.1	1.4	10	10	10	NNE 2	E 3	C 0
27	92.9	92.7	92.8	92.8	9.6	10.5	9.6	9.8	13.2	8.9	95	96	95	95	0.7	0.5	0.7	0.6	10	10 •	4	C 0	NE 1	N 1
28	94.3	93.7	92.3	93.4	9.8	16.6	14.5	13.8	18.3	8.7	95	64	75	78	0.6	6.8	4.1	3.8	10	6	8 •	E 1	E 2	ENE 2
29	89.5	88.1	85.4	87.7	10.4	10.2	9.1	9.7	14.5	8.5	86	91	83	87	1.8	1.1	2.0	1.6	10 •	10 •	9	N 4	NNE 3	N 3
30	83.7	85.7	86.9	85.4	5.8	9.2	7.6	7.6	11.1	5.2	88	71	84	81	1.1	3.3	1.6	2.0	10 •	10 •	8	E 5	NW 3	SW 3
31	90.8	93.3	95.1	93.1	9.1	14.2	10.2	10.9	15.5	3.4	63	37	64	55	4.3	10.2	4.5	6.3	1	4	1	NW 1	NW 4	NW 2
M	93.6	93.5	93.6	93.6	7.1	11.8	8.0	8.7	13.1	3.8	76	54	73	68	2.4	6.6	2.9	4.0	6.8	8.2	5.2	3.4	4.5	2.4

Czerwiec – Juin

1	94.1	91.3	88.9	91.4	11.2	10.2	10.9	10.8	11.8	5.8	60	91	94	82	5.3	1.1	0.8	2.4	9	10	10	E 7	E 7	E 4
2	88.1	88.4	90.3	88.9	11.6	13.2	10.4	11.4	15.7	9.7	95	73	95	88	0.6	3.8	0.6	1.7	9	10	10 •	SSW 2	S 3	S 3
3	92.7	95.5	97.3	95.2	9.6	16.5	12.0	12.5	17.5	8.3	83	47	70	67	2.1	10.0	4.1	5.4	9	8	2	SW 3	WNW 5	W 2
4	99.6	100.1	99.3	99.7	10.6	16.2	12.8	13.1	17.7	5.8	81	37	65	61	2.4	11.5	5.2	6.4	1	3	3	NNE 2	N 3	NE 1
5	99.0	96.8	94.5	96.8	13.4	19.0	14.2	15.2	19.5	5.1	57	33	61	50	6.6	14.7	6.3	9.2	8	7	4	ENE 4	E 6	NE 3
6	91.3	88.7	89.2	89.7	12.2	16.6	11.5	13.0	17.9	9.1	70	51	69	63	4.3	9.2	4.3	5.9	7	8	2	ENE 5	E 10	NE 5
7	85.3	86.3	91.0	87.5	9.2	10.9	10.6	10.3	12.5	9.0	88	84	71	81	1.4	2.1	3.7	2.4	10 •	10	4	NW 6	WNW 5	C 0
8	95.4	95.8	96.0	95.7	10.0	16.3	14.0	13.6	17.1	2.7	78	58	89	75	2.7	7.7	1.8	4.1	6	4	10	NW 2	NE 5	ENE 3
9	95.5	94.8	94.2	94.8	14.3	17.4	15.7	15.8	20.8	13.0	83	47	65	65	2.7	10.5	6.2	6.5	10	10	6	E 6	SE 10	E 3
10	94.2	93.5	93.3	93.7	16.2	21.8	15.2	17.1	22.7	10.9	68	35	79	61	6.0	17.1	3.7	8.9	1	9	9	E 3	ENE 9	ENE 1
11	90.3	88.9	89.2	89.5	15.4	20.0	13.4	15.6	20.2	12.9	71	40	86	66	5.1	14.0	2.1	7.1	10	10	10 •	NE 3	E 6	NE 4
12	88.4	87.9	88.3	88.2	15.0	19.2	13.6	15.4	19.8	12.8	80	57	87	75	3.4	9.6	2.0	5.0	9	10	10 •	NNE 3	N 4	W 2
13	87.8	87.4	88.5	87.9	12.0	18.8	12.8	14.1	19.4	11.9	89	74	86	83	1.3	5.7	2.1	3.1	10 •	7	9 •	W 3	WSW 7	NW 6
14	89.8	91.6	93.9	91.8	14.4	19.4	13.2	15.0	20.1	11.8	80	62	68	70	3.2	8.6	4.8	5.5	8	6	1	N 3	E 3	NNW 1
15	96.3	96.8	96.7	96.6	14.0	19.0	15.2	15.8	20.4	8.9	65	42	77	61	5.6	12.8	4.1	7.5	1	7	0	NNW 2	NW 2	NW 1
16	97.1	95.3	92.5	95.0	16.2	21.7	15.4	17.2	22.6	8.6	68	41	73	61	6.0	15.4	4.8	8.7	4	9	3	SE 2	SE 3	SE 2
17	89.9	87.4	87.7	88.3	18.0	24.4	18.0	19.6	24.8	10.4	67	31	55	51	6.7	21.0	9.2	12.3	2	3	1	SE 3	SE 10	ESE 4
18	89.5	91.6	93.0	91.4	16.3	17.8	12.8	14.9	18.6	12.6	78	55	91	75	4.0	9.2	1.4	4.9	0	9	10	S 3	S 8	SSE 2
19	86.9	86.7	89.7	87.8	13.1	18.2	12.6	14.1	19.1	12.5	94	66	91	84	0.9	7.1	1.4	3.1	10 •	8	8	S 6	WSW 8	SSW 2
20	91.6	94.6	95.9	94.0	12.4	13.2	12.8	12.8	16.4	11.8	86	73	79	80	2.0	3.8	3.1	3.0	10	10 •	0	SW 7	SW 5	SW 1
21	97.1	98.6	97.8	97.8	13.5	19.8	15.0	15.8	19.9	9.6	77	52	81	70	3.3	11.0	3.3	5.8	1	7	7	WSW 4	W 5	SSW 1
22	96.9	94.8	90.8	94.2	16.2	22.9	19.2	19.4	23.8	8.6	79	41	67	62	3.8	16.4	7.4	9.2	0	3	9	SE 2	S 3	SE 4
23	87.8	89.0	92.8	84.9	18.2	20.8	16.0	17.8	23.2	16.0	86	73	85	82	2.9	6.2	2.7	3.9	9	9	8	SSE 6	SSW 6	W 3
24	95.3	95.2	96.4	95.6	16.0	20.8	16.0	17.2	22.5	12.7	86	63	83	79	2.5	9.0	2.0	4.5	3	9	3	SW 4	SW 3	C 0
25	97.8	98.7	99.4	98.6	16.6	20.4	16.8	17.6	21.3	13.2	84	53	80	73	3.1	10.9	3.9	6.0	4	9	6	W 2	WNW 2	NE 1
26	99.1	98.3	96.1	97.8	18.0	26.1	20.4	21.2	26.4	11.9	73	42	78	65	5.2	19.6	3.3	10.0	3	1	9	SE 1	S 3	SW 2
27	99.0	99.7	98.5	99.1	15.4	20.6	17.0	17.3	21.3	14.7	77	33	59	57	4.1	13.6	8.0	9.2	8	3	10	WSW 3	NW 6	NNW 1
28	99.7	100.1	100.1	100.0	16.2	17.8	12.2	14.6	19.1	12.2	64	46	66	59	6.7	11.0	4.8	7.3	8	9	3	NW 2	WSW 3	WSW 1
29	94.0	93.4	93.3	94.4	10.8	14.3	13.0	12.8	16.8	9.6	92	81	81	85	1.0	3.1	2.8	2.3	10 •	9	7	SW 3	W 7	SW 3
30	96.6	97.1	93.1	95.6	12.8	17.3	14.8	14.9	19.8	8.7	84	51	84	73	2.4	9.3	2.7	4.9	3	7	2	SW 6	WSW 7	NE 1
31																								
M	93.5	93.5	93.7	93.6	14.0	18.4	14.2	15.2	19.6	10.4	78	53	77	70	3.6	10.2	3.8	5.9	6.1	7.6	5.9	3.7	5.6	2.3

Suwałki — $H_s = 165\,m$ — $H_b = 169.6\,m$ — $h_w = 13\,m$ — Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	•	•	⌒ 0 1–7
2	8	0.1	•	⚹ 0 12 45–48, 14 50–15 05, 15 16–55
3	8	0.0	•	⚹ 0 4 45–50, 5 35–6 05 ⚹ 2–6 15 ⚹ 0–7 02; ⌴ 1 21–24
4	8	•	•	⌴ 1 0 00–7
5	8	•	•	≫ 8 15–14 50, ⌴ 0 1–7
6	8	•	•	= 23 30–24
7	7	•	•	= 0 00–4 10
8	8	3.6	•	⚹ 0 13 50–14 15 ● 0–23 40, ⌒ 0 1–8
9	7	5.8	•	● 0 11 10–13 40 16 15–20 35 22 15–24; = 0 48–8 10 17 20–24
10	8	2.2	•	● 0 0 00–1 25 ● 1–2 10 ● 0–3 45 ⚹ 0 10 40–45, 12 03–06 ⚹ 2 13 40–55; = 0 00–3 30
11	8	0.9	•	= 1 30–4 45 = 2–5 30 = 0–6 10 = –6 20; ⌒ 0 1–4
12	7	0.0	•	● 0 3 05–4 40 7 35–8 10 11 25 ⚹ 0 17 40–18 03; = 4 40–11 30
13	8	•	•	⌒ 0 21–24
14	8	0.0	•	⚹ 0 13 02–06 13 12–15; = 1 20–3 40; ⌒ 0 0 00–7
15	8	•	•	= 0 15–5 20; ⌒ 0 1–8
16	8	2.6	•	● 0 22 15–23 45
17	6	0.4	•	⚹ 0 1 45–3 10 ● 1–5 15 ● 0–6 10 8 15–9 30–11 25; = 9 30–13 45 20 20–24; ⌒ 0 20–24
18	8	0.0	•	⚹ 0 3 35–5 20 ⚹ 0 13 30–33; ≫ 13 15–14 45; = 0 00–8; ⌒ 0 0 00–3
19	7	25.5	•	● 1 7 30–10 40 ● 0–11 07 ⚹ 0 15 12–18 16 15–20 ● 0 16 35–17 15 ● 0–17 30 ⚹ 1–21 15; R 0 NW 17 40–17 55–21 30 NE; ≫ 17 23–32; = 1 00–6 15
20	7	0.0	•	⚹ 0 12 25–32 15 05–19 17 52–18 03
21	8	1.3	•	⚹ 1 16 07–10 ▲ 0 ⚹ 1–16 15 ⚹ 1–16 20, ⌒ 1 1–9
22	8	•	•	⌒ 0 1–9
23	8	•	•	por wiatru do 14 m/sek 9 00–08, 10 55–14 45; ⌒ 0 1–7
24	8	10.0	•	● 0 13 40 14 20–24, por wiatru 14 m/sek 8 30–10 30
25	6	6.0	•	● 0 0 00–16 35 17 40
26	7	1.2	•	
27	6	1.8	•	● 0 0 40–2 35 ● 0 4 15–5 40 ● 0 9 05–10 30 12 45–13 10 ⚹ 0 16 05–40; = 2 35–14 15 21 20–24
28	8	0.5	•	⚹ 0 20 25–21 10 23 50–24; = 0 00–8 30
29	6	20.5	•	⚹ 0 0 00–1 35 ● 0 4 05–11 03 ● 1–11 10 ● 0–13 15 ● 1–14 10 ● 0–20 15
30	7	1.8	•	● 0 0 20–2 15 4 40–12 05 13 10
31	8	•	•	
Σ	-	84.0	-	

Czerwiec - Juin

1	7	6.5	•	● 0 8 20–10 20 ● 1–11 45; = 18 30–24, ⌒ 1 1–7
2	7	1.6	•	● 0 7 30–8 50 11 50–12 05 17 15–18 20 19 45–22 40 ● 0–23 15; = 2 0 20–5 35 = –5 55 8 40–10 20 18 30–24
3	8	•	•	= 0 00–1 35 2 40–4 20
4	8	•	•	= 2 10–5 20, ⌒ 0 1–8
5	8	•	•	⌒ 0 1–7
6	8	0.0	•	≫ 9 10–10 20 12 05–15 25; ⌒ 0 1–7
7	7	0.0	•	⚹ 0 2 40–3 10 3 35–4 20 ● 0–5 45 ● 0–7 35 ● 0–8 30 ● 1–9 40 ● 0–10 10
8	8	0.0	•	= 0 20–5 40, ⌒ 0 1–7
9	8	0.0	•	⚹ 0 4 35–40 14 10–22 ≫ 9 10–12 40 (por 17 m/sek 10 48–50), por wiatru do 14 m/sek 13 10–15 40
10	8	•	•	≫ 9 05–10 50, por wiatru 14 m/sek 10 50–11 05 ≫ 11 15–12 45; ⌒ 0 2–6
11	7	0.1	•	⚹ 0 11 02–05 11 25–30 13 26–40 14 32–38 ● 0–15 06 ⚹ 0 15 46–16 06 ● 0 16 35 17 15–18 20 18 35 19 15 20 10–22 35
12	8	8.7	•	⚹ 0 12 36–38 17 13–21 08 ● 0–21 35; R 0 NW 18 34–18 50–19 36 SE; = 21 40–24
13	8	20.0	•	⚹ 0 6 25–7 32 14 50–17 35 18 15–19 50 ⚹ 1–20 10 ⚹ 0–21 20 ● 0–22 45; R 0 NE 13 50–15 40–17 35 SW; = 0 00–8
14	7	•	•	● 0 0 25–2 27
15	8	•	•	⌒ 0 1–8, 21–24
16	8	•	•	⌒ 1 0 00–8; ⊕ 0 12 15–45
17	8	•	•	≫ 8 15–13 20 15 10–35 (por 15 m/sek 15 16–22); ⌒ 0 2–7
18	8	1.7	•	● 0 16 02–10
19	8	14.5	•	● 0 0 30–2 45 3 25–7 30 ● 1–8 40 ● 0–9 50 ● 1–10 35 ⚹ 1 14 15–18 ⚹ 2–14 40 ⚹ 1–15 10 ⚹ 0–15 35 ⚹ 1 19 06–40; R 0 E 14 00–14 30–15 30 W; = 3 15–10 00
20	7	0.6	•	⚹ 0 1 05–2 35 8 06–15 9 08–10 12 12 35–40; = 10 15–11 10
21	8	•	•	⌒ 1 1–8, 21–24
22	8	2.3	•	= 0 40–5 30, ⌒ 1 0 00–8
23	7	9.5	•	⚹ 0 2 32–3 00 5 20–28 7 40–50 ⚹ 1–8 20 9 40–10 08 ⚹ 0–11 35 ⚹ 1 14 35–15 04; R 0 SE 2 40–2 50–4 38 NW; R 0 SSE 7 55–8 10–8 35 NNW R 1 SW 14 40–15 00–15 45 NE; = 6 15–12 20
24	7	5.6	•	⚹ 0 20 02–22 ⚹ 1 23 55–24; = 2 10–7 16 20 30–24, ⌒ 0 20–24
25	8	•	•	⚹ 1 0 00–1 40; = 0 00–2 20 3 15–6 18
26	7	•	•	
27	8	•	•	
28	8	1.5	•	
29	7	2.8	•	● 0 4 45–7 35 ⚹ 0 11 06–12 11 20–35 12 07–20; por wiatru 15 m/sek 13 50–14 02
30	8	•	•	⌒ 1 2–8
31				
Σ	-	79.4	-	

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ *Lipiec – Juillet* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.6	88.0	90.5	88.4	14.0	12.8	11.0	12.2	16.3	10.9	82	70	71	74	2.9	4.4	5.8	3.7	10	10	2	WSW 2	WSW 5	W 2
2	91.4	89.7	87.2	89.4	12.0	17.0	13.6	14.0	17.9	7.2	76	44	73	64	3.3	10.9	4.2	6.1	5	8	8	SW 3	SW 6	SSW 1
3	84.2	85.4	86.0	85.2	12.6	14.8	11.6	12.6	16.1	10.4	72	60	75	69	4.1	6.7	3.4	4.7	8	9	9	WSW 5	W 8	WSW 2
4	86.8	87.4	87.9	87.4	11.2	15.3	10.6	11.9	16.4	7.8	79	57	87	74	2.8	7.5	1.6	4.0	8	8	4	SW 6	WSW 6	C 0
5	88.5	87.7	87.0	87.7	13.0	15.8	12.2	13.3	17.3	4.6	77	57	71	68	3.5	7.6	4.2	5.1	4	10	8	S 1	S 1	WNW 2
6	88.1	87.5	88.3	88.0	11.3	15.4	8.8	11.1	16.7	6.8	69	46	88	68	4.2	9.5	1.4	5.0	1	8	4	W 3	SW 6	SW 2
7	89.2	90.2	89.2	89.5	11.2	15.2	12.6	12.9	16.7	7.5	92	49	86	76	1.0	8.8	2.1	4.0	8	9	10	SW 6	SW 6	SSE 2
8	87.6	86.7	80.1	84.8	13.0	21.6	17.3	17.3	22.0	10.8	91	49	79	73	1.4	13.2	4.1	6.2	8	9	10	SSW 3	SSW 5	ESE 3
9	81.3	84.8	86.2	84.1	12.0	15.2	12.0	12.8	17.3	12.0	79	51	68	66	3.0	8.5	4.4	5.3	10	9	5	SW 7	SW 7	SSW 2
10	89.7	92.5	94.5	92.2	11.4	15.3	13.0	13.2	17.0	9.4	72	48	62	61	3.8	9.0	5.8	6.2	9	8	9	SW 6	WSW 6	WSW 2
11	97.5	97.8	99.1	98.1	11.2	17.4	11.8	13.0	18.1	6.3	82	50	90	74	2.5	10.0	1.3	4.6	7	9	8	SSW 1	SW 5	C 0
12	98.6	95.4	90.6	94.9	13.6	20.2	18.8	17.8	20.8	5.2	84	40	53	59	2.5	14.3	10.3	9.0	5	6	10 •	SE 3	S 5	S 9
13	92.8	94.2	95.1	94.0	14.6	19.0	15.4	16.1	21.3	10.8	82	56	85	74	2.9	9.6	2.6	5.0	4	8	2	SW 2	SW 6	SW 1
14	96.9	97.7	99.0	97.9	17.0	25.7	19.7	20.5	26.5	11.4	80	49	77	69	3.9	16.8	5.3	8.7	3	6	8	SSW 3	SSW 6	C 0
15	99.9	99.3	98.5	99.2	19.6	27.5	21.8	22.7	28.3	15.0	79	47	67	64	4.7	15.3	8.7	9.6	4	2	6	ESE 1	SSE 4	C 0
16	97.0	96.0	96.5	96.5	21.4	26.9	19.2	21.7	27.7	14.9	77	52	90	73	5.9	16.9	2.1	8.3	3	8	8	C 0	NE 3	N 4
17	97.1	97.3	97.5	97.3	16.2	16.6	15.4	15.9	19.2	15.1	89	88	71	83	1.9	2.4	5.1	3.1	10	10	9	NE 6	NE 4	ENE 4
18	98.5	98.5	99.5	98.8	14.6	19.0	15.8	16.3	20.4	12.0	69	42	63	58	5.2	12.8	6.6	8.2	6	7	0	NE 6	NE 8	NE 3
19	102.7	103.3	102.6	102.9	15.8	21.2	15.0	16.8	22.2	10.2	65	38	72	58	6.2	15.7	4.7	8.9	2	5	2	E 2	ENE 5	N 2
20	103.6	102.5	99.9	102.0	15.8	23.1	18.2	18.8	24.3	10.2	73	40	69	61	4.8	16.8	6.6	9.4	5	7	3	SE 1	ENE 3	ENE 1
21	99.1	96.7	92.8	96.2	17.2	24.5	16.6	18.7	25.1	10.2	71	36	70	59	5.6	19.7	5.7	10.3	1	8	6	E 1	SE 5	SE 1
22	90.3	89.6	89.5	89.8	17.6	18.6	16.6	17.4	23.1	14.5	67	77	96	80	6.6	4.9	0.8	4.1	9	9 •	10 •	SE 5	ESE 7	W 2
23	89.7	89.2	87.0	88.6	13.8	21.6	15.6	16.6	24.0	12.7	94	58	96	83	0.9	10.9	0.7	4.2	8	9	10 • K	NW 2	C 0	WSW 3
24	87.9	86.6	88.2	87.6	15.8	19.6	13.6	15.6	23.5	13.6	85	78	80	81	2.6	5.1	3.2	3.6	8	7	8	WSW 4	SSE 5	SE 3
25	90.3	91.2	89.9	90.5	14.4	20.4	15.2	16.3	21.7	10.7	76	49	76	68	3.9	12.4	3.9	6.7	2	8	2	SW 7	WSW 8	S 2
26	87.6	87.8	87.3	87.6	15.1	18.4	13.4	15.1	20.1	9.8	79	54	82	72	3.7	9.8	2.8	5.4	0	8	10 • K	SW 4	SW 6	SE 1
27	84.6	85.7	87.6	86.0	12.7	13.4	12.4	12.7	14.6	11.1	87	82	79	83	1.9	2.8	3.0	2.6	10 •	10	9	SSW 4	SW 5	SW 6
28	86.8	87.0	87.3	87.0	11.2	14.8	9.7	11.4	15.6	9.1	90	59	87	79	1.3	6.9	1.6	3.3	9	9	6	SSW 6	SW 9	SSW 2
29	86.0	85.5	81.8	84.4	12.4	14.3	14.6	14.0	17.4	9.1	89	83	93	88	1.6	2.7	1.1	1.8	9	10	10	SE 5	SSW 6	SSE 2
30	76.8	75.3	75.9	76.0	14.3	18.6	12.8	14.6	19.7	12.6	93	74	91	86	1.1	5.5	1.4	2.7	10	9	6	SSW 5	SSW 9	S 4
31	79.5	80.4	80.3	80.1	13.2	18.1	12.8	14.2	19.4	11.7	86	54	94	78	2.1	9.5	0.9	4.2	9	8	10	SW 6	SSW 8	SW 2
M	90.9	90.9	90.4	90.7	14.2	18.6	14.4	15.4	20.2	10.4	80	56	79	72	3.3	9.9	3.7	5.6	6.3	8.1	6.8	3.7	5.6	2.3

Sierpień – Août

1	89.5	88.3	91.2	88.3	11.0	14.3	11.4	12.0	17.1	10.2	87	56	79	74	1.6	7.1	2.8	3.8	7	9	2	W 5	WSW 7	SW 2
2	90.7	88.9	85.1	88.2	8.8	11.4	9.6	9.8	15.2	5.3	96	85	91	91	0.4	2.0	1.2	1.2	10	10 •	10 •	NE 1	SE 3	NW 3
3	85.4	86.9	88.8	87.0	11.4	17.3	12.2	13.3	18.4	8.4	85	52	78	72	2.0	9.4	3.2	4.9	6	8	8	W 4	SW 5	SW 1
4	90.2	90.1	91.8	90.7	13.3	17.8	12.4	14.0	19.6	8.6	81	58	94	78	3.0	8.5	0.9	4.1	8	10	6	SW 2	SW 4	SW 3
5	95.4	97.4	98.8	97.2	12.0	16.3	12.2	13.2	17.6	10.6	83	69	88	80	2.3	5.8	1.7	3.3	10	7	3	SW 3	SW 5	SW 2
6	99.1	97.8	93.5	96.8	13.4	22.4	20.4	19.2	23.8	7.3	82	44	79	68	2.8	15.2	5.1	7.7	4	6	9	SSW 3	S 7	S 1
7	93.8	92.1	91.2	92.4	17.0	23.1	19.0	20.0	26.6	16.2	97	36	93	75	0.6	20.5	1.5	7.5	10 •	9	9	SW 2	SW 8	SW 2
8	95.4	96.4	95.4	95.7	15.5	16.2	12.6	14.2	19.3	12.6	83	78	98	87	2.6	4.0	0.4	2.3	8	9 •	10 •	W 2	SW 1	SE 2
9	95.1	96.0	98.0	96.4	13.4	18.9	12.6	14.4	19.7	11.8	98	72	92	87	0.4	6.1	1.2	2.6	10 ≡	9	10	SE 2	SW 3	W 4
10	99.7	100.1	100.4	100.1	12.2	16.6	9.9	12.2	17.5	9.9	86	57	79	74	2.0	8.2	2.5	4.2	7	9	5	W 3	WSW 3	NW 1
11	100.4	100.1	99.0	99.8	10.2	15.8	12.2	12.6	17.1	6.8	93	59	86	79	0.8	7.2	2.0	3.3	10	8	6	NW 1	NW 2	NW 3
12	98.8	98.9	97.2	98.3	12.5	15.8	10.0	12.1	17.3	9.1	85	56	83	75	2.2	7.9	2.1	4.1	6	7	4	NW 3	W 5	W 2
13	96.1	95.2	95.6	95.6	10.8	10.8	10.2	10.5	13.4	8.7	79	87	88	85	2.8	1.7	1.4	2.0	2	9 •	9	NW 3	WNW 4	NW 3
14	95.9	96.1	96.2	96.1	8.4	13.4	11.4	11.2	15.3	7.7	96	80	88	88	0.4	3.2	1.7	1.8	10	9	10	WSW 1	C 0	NW 2
15	97.4	99.1	99.3	98.6	11.6	16.5	11.8	12.9	17.1	9.8	83	51	93	76	2.3	9.2	1.0	4.2	6	8	6	NW 3	NW 4	NW 2
16	99.8	99.0	97.9	98.9	12.6	16.4	11.4	13.0	17.5	10.4	93	60	90	81	1.1	7.4	1.4	3.3	9	8	0	NW 2	SW 4	SW 1
17	97.0	97.1	96.9	97.0	10.8	16.6	13.0	13.4	19.3	7.6	96	73	89	86	0.5	5.2	1.6	2.4	10	8	0	SW 4	WSW 4	NE 1
18	98.6	99.8	100.2	99.3	11.6	19.2	13.2	14.3	20.7	9.4	89	47	78	71	1.3	11.8	3.3	5.5	6	2	0	WNW 1	W 2	C 0
19	102.3	102.1	102.8	102.4	12.6	22.9	14.0	15.9	24.1	7.2	81	41	80	67	2.7	16.4	3.2	7.4	8	7	0	SW 1	WSW 3	NW 1
20	103.2	102.5	100.8	102.2	13.8	24.6	16.4	17.8	24.9	7.7	88	33	88	70	2.0	20.7	2.3	8.3	1	5	0	C 0	SE 1	SE 1
21	98.5	96.2	94.3	96.3	15.4	24.3	16.2	18.0	24.7	10.8	78	47	79	68	3.9	16.2	3.8	8.0	2	4	0	SE 3	SE 9	SE 3
22	93.1	92.4	91.6	92.4	16.4	26.2	16.6	19.0	27.1	14.2	88	42	82	71	2.3	19.9	3.5	8.6	0	0	0	SE 3	S 3	SE 2
23	92.4	92.1	92.2	92.2	15.8	25.1	16.8	18.6	25.8	12.7	73	33	63	58	4.4	20.7	7.1	10.7	0	0	0	SE 3	SE 9	SE 4
24	92.0	92.1	91.0	91.7	16.3	26.3	18.6	20.0	26.6	13.2	78	41	69	63	4.0	20.2	6.6	10.3	1	7	0	SE 3	SE 7	ESE 3
25	88.6	86.9	87.9	87.8	17.0	26.6	18.8	20.3	27.6	14.2	79	41	79	66	4.1	20.6	4.3	9.7	3	6	10	E 3	SE 10	C 0
26	87.7	89.3	91.9	89.7	17.3	16.2	12.2	14.3	20.3	12.1	80	80	92	84	4.0	3.6	1.2	2.9	9	10	6	C 0	NW 3	NW 3
27	86.3	83.6	85.1	85.1	12.6	20.0	12.0	14.2	20.3	11.2	98	76	98	91	0.4	3.6	0.3	2.1	10 •	9	10 ≡	N 6	E 3	SW 1
28	88.2	91.4	93.4	91.0	10.9	12.6	12.4	12.1	13.7	10.8	91	93	90	91	1.1	1.1	1.4	1.2	10 •	10 •	10	SW 3	SW 3	SW 2
29	93.0	93.3	92.3	92.9	11.4	14.8	11.2	12.2	16.8	11.1	93	74	91	87	0.7	4.3	1.2	2.1	10	10	3	SSW 3	SW 3	SE 1
30	91.2	92.3	94.2	92.6	10.4	17.2	10.6	12.2	17.8	7.8	92	63	94	83	1.0	7.2	0.8	3.0	10	6	0	SSW 1	W 3	C 0
31	93.6	92.7	92.8	93.0	9.6	17.4	12.0	12.8	17.8	6.3	93	51	81	75	0.8	9.8	2.7	4.4	2	6	6	NW 2	WNW 3	WNW 3
M	94.3	94.4	94.4	94.4	12.8	18.5	13.3	14.5	20.0	10.0	87	59	86	77	2.0	9.9	2.4	4.8	6.6	7.3	4.9	2.3	4.5	2.0

Suwałki — $H_s = 165\,m$ — $H_b = 169{,}6\,m$ — $h_w = 13\,m$ — Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU	POGODA
1	8	5.6	•	●^{0} 7^{05}–8^{05} ▽^{0}–9^{30}, 11^{30}–37, ☂^{0}E 8^{13}–8^{30}–9^{35} W; por. wiatru do 14 m/sek 14^{30}–17^{20}; ⌒^{0} 0^{00}–6, 21–24
2	8	•	•	⌒^{0} 0^{00}–8
3	8	0.2	•	▽●^{0} 8^{35}–42 10^{30}–38, 11^{13}–25 11^{53}–12^{05} 13^{05}–09
4	8	0.6	•	▽●^{0} 11^{06}–10, 10^{54}–11^{05} ▽^{1} 11^{40}–45; ⌒^{0} 21–24
5	8	•	•	= 1^{20}–6^{10}; ⌒^{1} 0^{00}–8
6	8	2.7	•	▽●^{1} 15^{10}–25, 19^{15}–20^{02}; ☂^{0}W 19^{25}–28–45 E; = 22^{40}–24; ⌒^{0} 1–8
7	8	0.3	•	▽●^{0} 10^{54}–11^{03} 21^{44}–22^{02}; = 0^{00}–4^{40}
8	7	11.8	•	▽●^{0} 0^{25}–35, 15^{02}–14 ▽^{1}–15^{19} ▽^{0}–16^{05} ▽^{1} 21^{15}–24; ☂^{0}S 14^{45}–15^{15}–15^{50} N; = 1^{30}–9^{40}
9	8	0.1	•	▽●^{1} 0^{00}–15, 21^{40}–45
10	8	0.2	•	▽●^{0} 9^{55}–10^{06}, 19^{50}–20^{10} ▽●^{1} 23^{17}–25
11	8	0.1	•	▽●^{0} 18^{35}–19^{04}; = 21^{15}–24
12	7	16.7	•	▽●^{0} 20^{20}–21^{30} ▽●^{2}–23^{40} ▽●^{0}–24; = 0^{00}–6^{10}
13	8	•	•	▽●^{0} 0^{00}–10; ≡^{0} 3^{45}–4^{05} ≡^{1}–4^{50}; ⌒^{0} 21–24
14	7	•	•	⌒^{1} 0^{00}–8^{00}
15	7	•	•	= 19^{30}–24; ⌒^{0} 1–8
16	7	•	•	= 0^{00}–7^{50}, 17^{20}–23^{10}, S 8^{10}–12^{20}
17	7	0.0	•	por. wiatru 14 m/sek 16^{30}–17^{25}; = 2^{15}–6^{10}
18	8	•	•	
19	8	•	•	⌒^{0} 1–7, 23–24
20	8	•	•	⌒^{0} 0^{00}–8
21	8	•	•	⌒^{0} 1–8; ⊕^{0} 10^{25}–40
22	7	5.8	•	▽●^{0} 12^{20}–40 13^{25}–45 14^{00}–15^{10} ●^{0}–22^{35}; = 22^{35}–24
23	0	15.4	•	▽●^{0} 19^{17}–30 ▽●^{1}–19^{33} ▽●^{2}–19^{45} ▽●^{1}–22^{00} ▽●^{0}–22^{40}; ☂^{1}E 19^{05}–19^{52}–21^{40} W; = 0^{00}–2^{40} ≡^{1}–3^{35} ≡^{2}–4^{20} ≡^{1}–5^{45} = –10^{05}
24	7	4.3	•	▽●^{0} 11^{10}–30, 11^{40}–12^{03} ▽●^{1} 15^{05}–23, 17^{42}–46 ▽●▲^{0}–17^{47} ▽●^{1}–18^{02}; ☂^{1}SW 14^{45}–15^{05}–15^{20} NE; ☂^{0}W 17^{40}–55 E; ≋ 15^{05}–10; = 12^{50}–13^{35}; ⌒^{0} 15^{55}–16^{00} ⌒^{1} $1/49$–54
25	8	•	•	≫ 10^{15}–11^{45}; ⌒^{1} 21–24
26	7	2.0	•	▽●^{0} 18^{05}–15 20^{01}–21^{05}, 22^{20}–24; ☂^{0}W 20^{08}–20^{15}–21^{35} E; por. wiatru 14 m/sek 15^{20}–16^{25}; = 3^{30}–7^{35}; ⌒^{1} 0^{00}–8
27	7	0.8	•	▽●^{0} 0^{00}–02 6^{20}–7^{40} 9^{15}–30 12^{10}–22 13^{02}–12
28	8	2.3	•	▽●^{0} 4^{50}–5^{10} ▽●^{1}–5^{12} ▽●^{2} 5^{33} 7^{55}–56 ▽●^{1}–7^{59} ▽●^{0}–8^{01} 11^{25}–35 13^{10}–20 14^{40}–45 15^{50}–16^{05} ▽●^{1} 18^{45}–19^{40}; = 6^{10}–7^{25}
29	7	6.5	•	●^{0} 11^{25}–50 17^{15}–20 ●^{1} 17^{33}–36 ●^{0} 18^{10}–19^{15} ▽●^{1} 22^{40}–24; = 2^{20}–8^{10} 17^{30}–24
30	7	3.2	•	▽●^{0} 10^{00}–30 ●^{0}–3^{45} ▽●^{0} 9^{56}–10^{05} ▽●^{1} 10^{25}–11^{00} ▽●^{0} 12^{52}–13^{01} ▽●^{1} 13^{25}–40; ☂^{0}SW 10^{20}–10^{35} 11^{40} SE; ☂^{0} 13^{09}–18–35 N; ☂^{0}S 15^{11}–20–50 N; ≫ 14^{15}–22; = 0^{00}–6^{10}; 20^{10}–24
31	8	15.9	•	▽●^{1} 14^{10}–45 ▽●^{0}–15^{0} ▽●^{1} 3^{25}–33 ▽●^{0}–3^{45} ▽●^{1} 17^{56}–18^{02} ▽●^{0}–19^{35} ●^{1}–21^{30} ●^{0} 22^{20}–24; = 0^{00}–4^{20}, 21^{30}–24
Σ	–	94.5	–	

Sierpień - Août

1	8	•	•	●^{0} 0^{00}–35; = 0^{00}–4^{20}
2	7	15.7	•	●^{0} 11^{20}–13^{30} ●^{1}–18^{25} ●^{0}–21^{48} ●^{1}–23^{35} ●^{0}–24; = 2^{10}–7^{15}; ⌒^{1} 1–8
3	8	0.6	•	●^{0} 0^{00}–15 ▽●^{0} 14^{40}–50 ▽●^{1} 19^{00}–15; = 4^{10}…6^{08}
4	8	0.0	•	▽●^{0} 13^{15}–20 14^{55}–15^{04} 15^{52}–16^{06}; ☂^{0}SW 12^{17}–13^{05}–13^{35} NE
5	8	0.0	•	▽●^{0} 11^{25}–40; ≡^{0} 23^{50}–24; ⌒^{0} 21–24
6	8	0.6	•	▽●^{0} 20^{20}–25; ☾ 21^{10}–23^{40}; ≡^{1} 0^{00}–1^{40} ≡^{0}–2^{45} = –3^{35}
7	6	4.0	•	▽●^{1} 5^{45}–6^{15} ●^{0}–7^{35} ▽●^{0} 14^{25}–30 14^{48}–15^{02} 15^{20}–25 ▽●^{1} 15^{50}–16^{02} ▽●^{2}–16^{22} ▽●^{1} 22^{05}–23^{20}; ☾ 0^{00}–1^{30} 20^{03}–21^{10} ☂^{0}SE 22^{20}–22^{40}–23^{30} NW; = 1^{30}–12^{45}
8	8	8.2	•	▽●^{1} 0^{05}–10 0^{55}–1^{20} ●^{0} 9^{20}–10^{40} ▽●^{0} 11^{20}–12^{50} ●^{0} 18^{35}–19^{02} ●^{1}–20^{10} ●^{0}–21^{13}; ☾ 0^{00}–1^{10} SE
9	7	0.3	•	▽●^{0} 15^{18}–40 ●^{0} 17^{35}–20^{10}; = 1^{40}–4^{17} ≡^{0}–6^{40} = –12^{15}, 20^{10}–24
10	8	•	•	= 0^{00}–6^{15}; ⌒^{0} 21–24
11	8	•	•	⌒^{0} 0^{00}–8
12	8	•	•	= 1^{10}–5^{06}; ⌒^{1} 1–7
13	8	2.5	•	▽●^{0} 8^{50}–55 11^{30}–40 ▽●^{1} 12^{25}–35 ▽●^{0} 13^{15}–23 14^{55}–15^{10}; ⌒^{0} 2–7
14	8	2.5	•	▽●^{1} 0^{20}–35 ▽●^{0} 10^{40}–55 11^{30}–40 14^{45}–15^{05} 18^{40}–19^{25} 20^{05}–20 22^{10}–23^{15}; = 4^{15}–7^{30}
15	8	•	•	▽●^{0} 0^{45}–1^{30}
16	8	•	•	= 1^{15}–5^{30}
17	8	•	•	≡^{1} 2^{50}–4^{30} ≡^{0}–5^{35} = –6^{45}, 22^{30}–24; ⌒^{0} 1–3, 21–24
18	8	•	•	= 0^{00}–6^{40}; ⌒^{1} 0^{00}–8 ⌒^{0} 21–24
19	7	•	•	⌒^{1} 0^{00}–8, 20–24
20	7	•	•	= 1^{00}–4^{40}; ⌒^{1} 0^{00}–9, 21–24; S 11^{10}–19^{40}
21	8	0.2	•	= 3^{25}–7^{35}; ⌒^{1} 0^{00}–8; S 8^{20}–10^{30}, 15^{10}–19^{50}
22	7	•	•	●^{0} 10^{00}…40; 3^{15}–30; = 3^{20}–11^{20}; ⌒^{0} 21–24
23	8	•	•	⌒^{0} 0^{00}–7
24	8	•	•	≫ 9^{15}–10^{45}
25	7	•	•	≫ 11^{09}–13^{20}
26	7	8.2	•	▽●^{0} 11^{40}–12^{10} ▽●^{1} 19^{30}–45 ▽●^{0}–20^{15} ▽●^{1} 22^{27}–35; ☂^{0}SE 19^{15}–19^{30}–20^{35} NW (☂)^{0}S 22^{20}–22^{37}–23^{20} N
27	7	39.0	•	▽●^{0} 0^{42}–10 ●^{0} 6^{02}–20 ●^{0} 10^{52}–11^{02} ●^{0}–11^{40} ▽●^{1} 13^{10}–25 ▽●^{1} 13^{43} ▲^{0} 13^{47} ▽●^{1}–14^{05} ▽●^{0}–15^{10} 15^{50}–16^{10} ●^{0} 23^{40}–24; ☂^{0}S 12^{55}–13^{45}–16^{15} NE; = 3^{45}–12^{30} 17^{40}–18^{45} ≡^{0}–20^{35} = –24
28	6	0.5	•	●^{1} 0^{00}–2^{50} ●^{0}–7^{15} ●^{1} 10^{40}–13^{25}; = 0^{00}–6^{10} 8^{35}–13^{45}
29	8	•	•	●^{0} 3^{05}–46 ●^{1} 4^{10}–5^{40}; = 3^{10}–5^{40}; ⌒^{1} 21–24
30	8	0.1	•	▽●^{1} 10^{40}–50; = 20^{20}–24; ⌒^{1} 0^{00}–8 ⌒^{0} 20–24
31	8	•	•	= 0^{00}–4^{30}; ⌒^{0} 0^{00}–8, 19–24
Σ	–	68.3	–	

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ *Wrzesień – Septembre* 1965

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,w I	II	III
1	92.4	94.0	98.2	94.9	10.0	17.1	10.8	12.2	18.9	9.6	89	52	90	77	1.3	9.4	1.4	4.0	8	7	0	WSW 2	W 5	C 0
2	102.1	102.8	102.0	102.3	11.2	21.4	15.2	15.8	22.3	8.1	89	56	83	76	1.5	11.2	3.0	5.2	9	7	0	NE 2	ENE 2	NE 2
3	99.1	97.1	94.7	97.0	15.2	25.1	17.2	18.7	26.2	13.0	91	55	86	77	1.5	14.2	2.8	6.2	9	7	3	ENE 1	ESE 5	ESE 2
4	91.6	90.1	87.9	89.9	16.2	25.4	18.6	19.7	26.6	13.8	90	52	87	76	1.7	15.3	2.7	6.6	9	8	10	ESE 1	SSE 5	SE 1
5	86.5	89.2	89.7	88.5	13.8	16.2	13.6	14.3	19.3	13.5	80	71	92	81	3.2	5.2	1.3	3.2	10	10	5	S 8	SSW 8	S 3
6	88.5	87.4	85.7	87.2	12.2	21.8	17.0	17.0	22.3	9.2	92	55	78	75	1.2	11.7	4.3	5.7	8	6	8	SE 2	SE 5	SE 3
7	83.4	84.9	86.8	85.0	15.0	14.3	10.6	12.6	17.2	10.5	96	73	82	84	0.7	4.5	2.3	2.5	10 •	10	0	S 3	SW 5	SSW 3
8	88.7	90.7	92.9	90.8	9.4	16.4	9.4	11.2	17.1	7.7	85	47	85	72	1.7	9.8	1.7	4.4	0	8	0	SSW 5	SSW 8	SE 2
9	94.0	93.8	94.6	94.1	10.0	20.9	14.0	14.7	21.1	6.6	91	48	88	76	1.1	12.9	2.0	5.3	4	8	8	SSE 2	S 4	SE 1
10	94.4	92.3	91.2	92.6	13.4	24.1	19.2	19.0	24.3	9.4	91	51	67	70	1.4	14.6	7.4	7.8	3	6	9	E 2	SE 10	SSE 7
11	90.2	86.5	91.2	89.3	13.8	18.0	11.5	13.7	21.5	11.4	98	90	87	92	0.4	2.0	1.9	1.4	10	10 •	10	E 3	S 6	WSW 4
12	92.1	92.7	92.0	92.3	9.7	15.2	9.1	10.8	16.1	9.1	91	59	87	79	1.1	7.2	1.6	3.3	7	8	3	W 2	W 4	SE 1
13	90.7	89.0	89.2	89.6	8.2	14.9	10.6	11.1	16.2	5.3	93	71	88	84	0.8	4.8	1.5	2.4	9 •	7	6	W 2	S 4	SSW 2
14	90.7	91.4	93.2	91.8	8.0	15.0	8.3	10.0	15.7	6.1	94	60	94	83	0.6	6.7	0.6	2.8	2	9	6	SW 3	SW 4	SSW 2
15	93.2	94.2	100.7	96.0	9.4	13.4	8.2	9.8	14.1	7.3	88	75	86	83	1.4	3.8	1.5	2.2	9	9	0	SW 5	SW 7	W 4
16	105.0	106.6	105.8	105.8	8.6	15.3	7.4	9.7	16.7	7.4	93	55	93	80	0.8	7.9	0.8	3.2	8	8	2	WNW 2	WNW 3	C 0
17	103.3	101.5	99.7	101.5	8.3	18.3	12.6	13.0	18.8	4.3	83	47	79	70	1.9	11.1	3.1	5.4	7	5	0	S 3	SSE 6	SSE 1
18	98.3	96.5	94.3	96.4	9.8	22.0	15.9	15.9	22.5	8.2	96	57	78	77	0.5	11.4	4.0	5.3	4 ≡	0	0	C 0	S 5	SSE 2
19	92.4	96.2	99.9	96.2	11.2	16.6	10.8	12.4	16.9	10.4	94	55	78	76	0.8	8.5	3.0	4.1	10	9	0	WSW 3	WSW 7	SW 3
20	102.3	104.8	109.7	105.6	9.3	14.0	8.2	9.9	15.8	7.1	89	83	86	86	1.3	2.7	1.5	1.8	10	10	0	SW 3	WNW 3	WNW 3
21	110.6	109.9	107.0	109.2	8.0	13.4	11.8	11.2	14.1	3.0	96	71	81	83	0.4	4.5	2.6	2.5	9	10	10	S 3	SSW 3	SSW 4
22	101.2	97.9	96.3	98.5	10.6	19.2	12.2	13.6	20.3	9.9	81	30	67	59	2.4	15.6	4.6	7.5	4	0	0	SW 5	SW 9	SW 4
23	95.0	95.8	95.9	95.6	8.8	19.7	8.4	11.3	20.5	7.3	85	56	89	77	1.7	10.1	1.2	4.3	1	3	0	WSW 3	WSW 3	NNW 1
24	96.6	97.3	97.2	97.0	6.3	22.4	12.2	13.3	22.7	3.6	94	53	89	79	0.5	12.8	1.5	4.9	0	0	0	C 0	SSE 3	C 0
25	97.3	96.1	95.5	96.3	10.2	23.2	15.8	16.2	23.6	8.7	95	49	75	73	0.6	14.6	4.4	6.5	4	2	0	E 2	ESE 5	SE 3
26	94.6	93.5	94.4	94.2	12.0	21.8	15.5	16.2	22.6	11.3	91	52	73	72	1.2	12.3	4.8	6.2	7	5	0	ESE 3	ESE 9	ESE 5
27	95.6	91.0	91.1	91.9	11.8	21.4	15.2	15.9	21.4	10.9	87	56	93	79	1.8	11.2	1.2	4.7	0	8	10	SE 5	ESE 7	ESE 6
28	90.0	89.3	87.7	89.0	13.1	19.3	19.0	17.6	20.1	13.1	96	71	81	83	0.6	6.4	4.2	3.7	10	9	10	ESE 5	SE 5	ESE 5
29	85.5	83.8	88.5	85.7	16.2	21.8	11.3	15.2	22.8	11.4	89	63	91	81	1.9	9.5	1.2	4.2	7	9	10 •	SE 5	ESE 6	S 7
30	95.7	97.6	97.1	96.8	9.3	16.6	11.2	12.1	17.4	9.2	92	62	90	81	0.9	7.1	1.3	3.1	9	6	0	S 3	S 4	SSE 1
31																								
M	94.6	94.5	95.0	94.7	11.0	18.8	12.7	13.8	19.8	8.9	91	59	84	78	1.2	9.3	2.5	4.3	6.6	6.8	3.7	2.9	5.2	2.7

Październik – Octobre

1	98.4	100.2	102.0	100.2	8.4	17.6	13.0	13.0	17.7	6.2	96	51	88	78	0.4	9.8	1.8	4.0	0	0	10	C 0	NW 3	NE 2
2	102.8	102.8	103.1	102.9	10.9	15.2	7.6	10.3	15.9	7.6	92	62	76	77	1.0	6.5	2.5	3.3	10	6	0	NE 3	ENE 3	NE 3
3	104.3	104.4	103.3	104.0	4.8	15.6	12.2	11.2	16.0	3.6	73	50	44	56	2.3	8.9	8.0	6.4	0	5	10	E 3	ESE 8	SSE 5
4	103.5	103.7	103.4	103.5	10.4	14.2	8.6	10.4	15.6	8.3	82	65	90	79	2.2	5.6	1.1	3.0	10	8	5	SE 1	W 1	C 0
5	103.2	104.2	104.3	103.9	10.6	13.8	8.8	10.5	14.4	8.0	92	62	93	82	1.0	6.1	0.8	2.6	10	9	0	W 1	WNW 2	NW 2
6	104.6	104.6	103.3	104.2	6.6	13.4	10.8	10.4	13.6	2.7	93	70	92	85	0.7	4.7	1.0	2.1	9	10	10	C 0	NNW 1	C 0
7	100.6	98.6	96.6	98.6	9.3	14.8	10.2	11.1	15.3	9.2	89	53	83	75	1.3	7.9	2.0	3.7	10	7	9	SW 1	SE 7	SW 2
8	92.4	92.8	94.4	93.2	9.3	13.4	7.7	9.5	14.1	6.8	89	49	68	69	1.3	7.9	3.4	4.2	10 •	7	9	SW 2	NW 7	WNW 5
9	94.8	94.3	93.4	94.2	5.8	7.6	3.8	5.2	9.3	3.8	76	58	73	70	2.2	4.3	2.0	2.8	9	9	4	W 3	NW 4	WNW 3
10	92.5	91.1	90.7	91.4	4.0	7.6	6.3	6.0	8.6	2.4	83	79	85	83	1.2	2.2	1.4	1.6	10	10 •	7	W 3	SW 3	WNW 3
11	92.3	88.3	95.7	92.1	1.6	4.8	0.0	1.6	6.3	0.0	80	82	78	80	1.4	1.5	1.3	1.4	10	9	0	SW 2	WNW 6	WNW 2
12	100.7	103.2	103.6	102.5	1.4	6.3	5.0	4.4	6.6	-1.2	83	67	76	75	1.1	3.1	2.0	2.1	9	9	10	WSW 2	WNW 3	WSW 4
13	102.0	101.3	99.3	100.9	8.0	9.5	7.6	8.2	10.4	4.2	90	79	71	80	1.0	2.5	3.0	2.2	10	9	10	WSW 3	WSW 7	SW 5
14	97.8	98.8	101.4	99.3	7.9	10.9	9.4	9.4	11.0	7.2	90	79	88	86	1.0	2.7	1.4	1.7	10	10	10	SW 4	SW 4	WSW 1
15	101.7	100.0	97.5	99.7	5.8	14.0	8.0	9.0	14.2	5.7	91	59	75	75	0.8	6.6	2.7	3.4	4	0	4	C 0	S 4	S 3
16	93.5	92.3	92.5	92.8	5.0	11.8	8.2	8.3	12.0	3.2	92	78	92	87	0.7	3.0	0.9	1.5	9	10	10 •	SW 3	SSW 6	SW 3
17	99.8	100.0	102.7	99.3	5.6	10.0	6.6	7.2	10.4	5.2	83	62	82	76	1.6	4.7	1.7	2.7	2	8	10	WNW 6	W 7	WSW 1
18	100.7	99.7	101.3	100.6	4.2	8.4	6.2	6.2	9.3	3.0	90	93	89	91	0.8	0.7	1.0	0.8	9	10 •	0	SW 2	SW 3	WNW 4
19	103.8	103.1	104.4	103.8	2.4	9.4	5.4	5.6	10.1	2.0	93	69	86	83	0.6	3.7	1.3	1.9	9	9	10	WSW 1	WSW 5	WNW 3
20	108.8	112.7	114.9	112.1	3.0	5.6	-0.6	1.8	5.9	-0.8	88	64	90	81	0.9	3.3	0.6	1.6	10	4	0	NNE 6	NE 4	C 0
21	115.8	115.8	115.7	115.8	-2.9	6.2	2.8	2.2	6.3	-3.8	91	60	77	76	0.4	3.8	1.7	2.0	7	7	10	WSW 1	WSW 2	SW 2
22	114.0	112.5	109.4	112.0	1.6	8.7	7.2	6.2	9.0	0.0	81	76	80	79	1.3	2.7	2.1	2.0	10	9	9	SW 3	SW 4	W 7
23	105.4	106.2	107.1	106.2	7.4	9.3	4.4	6.4	9.6	4.4	84	73	89	82	1.6	3.3	1.0	2.0	9	10	0	WNW 4	W 4	NW 2
24	108.8	107.9	107.6	108.1	3.3	7.4	7.6	6.3	8.3	1.1	93	80	83	85	0.5	2.1	1.7	1.4	9	10	10	NW 1	NW 5	NW 2
25	106.4	106.8	106.8	106.7	6.8	7.8	5.8	6.6	8.0	3.1	93	89	86	90	0.6	1.2	1.3	1.0	10	9	10	NW 1	NW 2	W 2
26	105.2	104.3	102.0	103.9	5.6	8.0	4.7	5.8	8.7	4.6	91	76	87	83	0.9	2.5	1.1	1.5	10	7	10	WSW 2	SW 3	SW 4
27	97.4	96.8	96.3	96.8	4.9	6.0	3.1	3.3	6.3	4.0	84	71	86	80	1.4	2.7	1.3	1.8	10	10	10	SSW 3	SW 4	SW 3
28	93.9	92.0	91.3	92.4	1.4	8.8	9.7	7.4	11.8	0.8	96	80	87	88	0.3	2.3	1.6	1.4	10	9	10	S 4	SW 5	SSW 4
29	90.4	90.0	87.3	89.3	6.7	13.6	10.6	10.4	13.7	6.6	94	73	81	83	0.6	3.9	2.4	2.3	4	2	10	SE 4	S 3	SW 7
30	91.4	93.9	93.7	93.0	6.4	8.1	4.2	3.7	10.8	4.1	78	72	90	80	2.1	3.0	0.8	2.0	9	10	0	SW 4	SW 3	SSW 3
31	86.3	84.2	84.1	84.9	3.8	9.0	4.8	5.6	9.4	2.6	82	64	86	77	1.3	4.1	1.2	2.3	10	9	0	SSE 4	SSW 8	SSW 4
M	100.3	100.2	100.3	100.3	5.3	10.2	6.8	7.3	10.9	3.7	88	69	82	80	1.1	4.1	1.8	2.3	8.3	7.8	6.7	2.3	4.4	3.1

Suwałki — $H_s = 165\,m$ — $H_b = 169{,}6\,m$ — $h_w = 13\,m$ — Wrzesień - Septembre 1965

DNI	WIDZALNOŚĆ v	OPAD R	GRUBOŚCIE GU h	POGODA
1	8	•	•	⌒ 0^00–9 ⌒ 1^20–24
2	8	•	•	= 5^20–7^28; ⌒ 1^00–9
3	7	•	•	= 4^10–8^20; ⌒ 0^1–9, 21–24
4	7	0.0	•	= 4^20–9^40; ⌒ 0^00–9
5	8	5.8	•	● 0^00–1^08 ● 1^13–14^10 ● 0–14^25, 14^35–17^05; ≫ 4^50–5^20, 8^15–9^20, 10^30–11^40; = 17^10–24
6	7	1.7	•	▽ 0^18^45–19^10; = 0^00–8^10
7	7	0.3	•	● 0^05^5–9^15; = 5^20–10^30; ⌒ 0^21–24
8	7	•	•	≫ 11^18–25; = 0^15–9^10; ⌒ 1^00–8, 22–24
9	7	•	•	= 0^20–8^20; ⌒ 1^00–9 ⌒ 0^21–24
10	7	•	•	≫ 10^50–11^47, 12^12–14^30, 15^02–16^46; = 3^15–8^10; ⌒ 1^00–8
11	6	1.2	•	▽ 0^10^20–40 ● 0–13^10, 13^30–14^15; = 1^10–3^45 ≡ 1–5^20 ≡ 0–6^25 = –9^15, 13^30–17^25
12	7	0.9	•	
13	7	5.5	•	▽ 0^10–12 ▽ 1–6^40 ● 0 7^15 8^42 9^03 9^45 10^38 11^02–20 ▽ 1^13^50 14^07 ▽ 0^14^30–38 15^40 20^01; ⊠ 1W 6^35 7^15 7^40 E ⊠ 1SSW 13^52 14^15 14^35 NNE < SW 18^50 19^25 NE ⊠ 0 SE 20^03–26–43 NW; = 1^20 7^23 24
14	7	2.4	•	▽ 0^11^50–55 14^20–40, 15^30–35 ▽ 1–15^38 ▽ 0–16^36; ≫ 15^35–40; = 0^00–7^50
15	7	0.8	•	▽ 0^10^48–11^01 ▽ 1^11^45–12^03 ▽ 0^12^20–25; ⌒ 1^22–24
16	8	•	•	⌒ 1^00–8, 20–24
17	8	•	•	⌒ 1^00–9
18	6	0.0	•	= 1^30–4^45 ≡ 0–5^20 ≡ 1–6^15 ≡ 0–7^43 = –20^00; ⌒ 0^19–24
19	8	0.9	•	▽ 0^6^50–7^25, 7^45–8^25; = 4^15–11^40
20	8	0.0	•	▽ 0^12^35–39; ⌒ 0^1–8 ⌒ 1^20–24
21	7	•	•	= 0^2^45–4^40 ≡ 1–5^40 = –8^15; ⌒ 1^00–8
22	7	•	•	≫ 10^20–12^30; = 1^00–5^30, S 0^9^30–12^15
23	7	•	•	= 5^10–10^20, 22^05–23^20 ≡ 1–24; ⌒ 0^1–9 ⌒ 1^21–24
24	7	•	•	≡ 1^00–1^35 ≡ 0–3^50 = –8^30, 18^45–24; ⌒ 1^00–8, 19–24
25	7	•	•	= 0^00–9^20; ⌒ 1^00–9
26	7	•	•	por wiatru 14 m/sek 13^15–15^40; ⌒ 0^1–9
27	7	0.9	•	▽ 0^15^50–16^05, 16^55–18^25; ≫ 10^15–11^45 por wiatru 12 m/sek 12^10–14^15, por wiatru 14 m/sek 17^20–18^45; ⌒ 0^1^00–8^00
28	7	0.0	•	▽ 0^19^35–20^10; = 1^00–12^25
29	7	10.5	•	▽ 0^08–13 0^50–1^20 ▽ 2^15^30–40 ▽ 0–16^15, 16^45–17^15 ▽ 1^18^15–19^10 ▽ 0–21^25 ● 0–23^40; ⊠ 2 SE 15^30–15^40–16^10 NW; ≫ 15^30–40
30	8	•	•	= 4^15–11^30; ⌒ 0^20–24
31				
Σ	–	30.7	–	

Październik - Octobre

DNI	WIDZALNOŚĆ v	OPAD R	GRUBOŚCIE GU h	POGODA
1	7	•	•	= 0^00–9^30; ⌒ 0^00–9
2	8	•	•	
3	8	•	•	⌒ 0^1–7
4	7	•	•	= 18^30–24; ⌒ 1^19–24
5	8	0.0	•	▽ 0^15^30–35; = 0^00–7^10, 21^15–23^40 ≡ 0–24; ⌒ 0^00–8
6	7	•	•	≡ 0^00–1^38 = –9^30
7	7	0.0	•	= 1–4^30
8	7	0.0	•	● 0^6^10–7^05; = 5^20–8^25
9	8	•	•	⌒ 0^1–9
10	6	5.2	•	▽ 0^12^25–14^46 ▽ 1–15^05 ▽ 0–15^40, 15^50–17^20, 20^10–20
11	8	3.1	•	▽ 1^7^40–45 ▽ 0–8^05 ▽ 0–8^15 ● 0^9^25 10^15 ● 1–12^05 ▽ 0^13^01–18
12	8	0.4	•	▽ 0^7^25–27 11^12–18 13^40–14^03, 15^20–45, 18^45–19^05 ● 0^21^30–24
13	7	0.0	•	● 0^0^00–1^15, 3^05–4^40
14	6	•	•	● 0^10^0–20, 2^15–3^10–4^20; = 3^30–24
15	6	•	•	= 0^00–9^40, 17^30–24; S 11^10–17^30
16	6	9.3	•	● 0^13^45–20^45; = 0^00–24; ⌒ 0^1–10
17	8	•	•	▽ 0^2^35–5^10; = 0^00–5^25
18	6	3.9	•	● 0^9^20–10^15 ● 0^11^30–40, 12^25–35 ▽ 1^13^40–14^05, 14^35–15^03 ▽ 0–15^20 ● 0–16^15–10^15–16^40; ⌒ 0^0–9
19	8	1.2	•	▽ 0^15^45–16^25
20	8	•	•	⌣ 0^20–24
21	7	•	•	= 7^10–9^25; ⌣ 0^00–10
22	7	•	•	
23	7	•	•	= 6^10–8^10
24	7	•	•	= 1^2^35–3^05 = 0–4^15 = –10^20; ⌣ 0–3
25	6	0.0	•	● 0^8^05–50; = 6^15–13^10, 16^30–24
26	7	•	•	= 0^00–8^10, 16^15–24
27	7	•	•	= 0^00–9^20, 21^15–24
28	6	•	•	= 0^00–40 ≡ 1–1^30 ≡ 0–2^50 ≡ 1–5^20 ≡ 0–6^20 = –7^50 ≡ 0–9^50 = –24
29	7	0.5	•	● 0^21^15–22^40; = 0^00–11^30, 16^10–24; ⌒ 1^1–9
30	8	•	•	= 0^00–3^30, 22^30–24; ⌒ 1^21–24
31	6	0.1	•	● 0^8^35–9^10 ▽ 0^16^20–30; = 0^00–12^35; ⌒ 1^0^00–8
Σ	–	23.7	–	

Suwałki — φ = 54°06' — λ = 22°57' — Listopad – Novembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE : POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	84.3	82.3	71.8	79.5	4.6	6.0	6.6	6.0	6.6	3.1	85	77	94	85	1.3	2.2	0.5	1.3	10	10	10 •	SW 6	S 5	SSE 6
2	70.1	71.6	73.9	71.9	8.6	9.0	6.7	7.8	10.2	6.6	86	57	72	72	1.6	5.0	2.7	3.1	9	9	10	SSW 6	SSW 10	SSW 8
3	77.4	80.7	84.2	80.8	5.8	6.6	4.0	5.1	6.9	3.9	65	66	75	69	3.2	3.2	2.0	2.8	10	10	4	SW 9	WSW 8	SW 6
4	87.6	91.8	96.7	92.0	3.4	5.4	4.2	4.3	5.5	1.7	75	77	84	79	2.0	2.1	1.3	1.8	10	10	10	SW 6	SW 8	SW 6
5	100.7	102.4	104.1	102.4	5.4	6.2	3.8	4.8	6.5	3.5	89	80	85	85	1.0	1.9	1.2	1.4	10	10	10	WSW 3	NW 4	WSW 3
6	102.0	101.6	100.5	101.4	4.2	5.5	6.4	5.6	6.4	3.4	92	94	92	93	0.6	0.5	0.7	0.6	10 •	10	10 •	SW 5	WSW 3	SW 2
7	98.4	97.5	98.8	98.2	4.8	7.6	2.8	4.5	8.0	2.8	92	73	91	85	0.8	2.8	0.7	1.4	4	9	0	W 2	W 4	W 2
8	101.4	103.0	103.8	102.7	0.6	5.8	3.8	3.5	5.9	-0.4	92	70	80	81	0.5	2.8	1.6	1.6	8	9	10	WSW 1	WSW 2	SW 2
9	102.8	100.6	97.4	100.3	2.1	4.8	2.7	3.1	5.4	1.5	93	76	98	89	0.5	2.0	0.1	0.9	10	10	10 ≡	SW 1	SW 4	SW 2
10	95.4	96.3	96.7	96.1	5.2	4.8	1.4	3.2	6.6	1.4	86	64	85	78	1.2	3.1	1.0	1.8	10	6	9	W 2	WNW 3	WSW 2
11	96.7	96.0	95.5	96.1	-2.8	1.6	-1.6	-1.1	2.0	-3.9	97	76	88	87	0.1	1.7	0.6	0.8	10	4	10 *	WNW 1	ENE 1	NE 5
12	94.2	94.2	95.3	94.6	-3.6	-1.9	-4.6	-3.7	-1.6	-4.6	85	87	81	84	0.7	0.7	0.8	0.7	9	10	10 *	NE 5	ENE 7	NE 6
13	96.2	96.9	97.5	96.9	-6.6	-5.4	-6.0	-6.0	-4.6	-6.8	78	65	68	70	0.8	1.4	1.2	1.1	8	9	10 *	NE 5	NE 7	NE 5
14	97.2	97.8	98.0	97.7	-7.6	-5.9	-6.9	-6.8	-5.9	-7.9	70	76	72	73	1.0	0.9	1.0	1.0	10 *	9	10	ENE 6	NE 5	NNE 5
15	98.0	99.3	102.0	99.8	-7.9	-6.4	-7.5	-7.3	-6.2	-8.3	87	83	84	85	0.4	0.6	0.5	0.5	10 *	10 *	10 *	NE 4	E 4	NE 3
16	105.5	107.0	107.8	106.8	-10.3	-9.1	-13.5	-11.6	-7.5	-14.7	81	76	88	82	0.5	0.7	0.3	0.5	9	9	0	NNW 2	N 2	C 0
17	107.0	105.9	104.5	105.8	-11.3	-10.3	-12.9	-11.8	-9.8	-14.9	86	74	92	84	0.4	0.7	0.2	0.4	10	4	10 *	C 0	SW 2	S 2
18	102.2	100.9	98.5	100.5	-13.5	-10.3	-14.4	-13.2	-9.9	-14.6	92	84	87	88	0.2	0.4	0.3	0.3	10 *	7 *	0	SE 3	ESE 4	E 3
19	92.5	88.6	85.9	89.0	-13.0	-10.1	-9.1	-10.3	-9.1	-16.1	80	81	85	82	0.5	0.5	0.4	0.5	10	10 *	10 *	E 6	ESE 5	E 6
20	83.3	83.8	84.3	83.8	-7.7	-6.4	-6.7	-6.9	-6.2	-9.1	87	86	88	87	0.4	0.5	0.4	0.4	10	10	10	E 3	ENE 1	NNE 1
21	82.0	77.5	68.9	76.1	-6.7	-5.6	-4.6	-5.4	-4.6	-6.8	88	95	91	91	0.4	0.2	0.4	0.3	10	10	10 *	NE 2	NE 5	NE 5
22	70.0	75.9	84.6	76.8	-9.3	-5.4	-6.4	-6.9	-4.6	-9.6	82	82	83	82	0.5	0.7	0.6	0.6	10 *	10	7	WNW 6	W 6	WSW 3
23	90.6	94.7	98.7	94.7	-9.8	-7.5	-7.1	-7.9	-5.1	-10.5	85	90	91	89	0.4	0.3	0.3	0.3	10	10 ≡	9	SSW 2	SW 2	SW 3
24	100.2	100.8	99.1	100.0	-17.7	-11.0	-11.2	-12.8	-7.1	-19.7	79	90	90	86	0.3	0.3	0.3	0.3	3	10 *	10	SW 1	SE 3	SSE 5
25	97.9	97.0	96.9	97.3	-8.9	-5.2	-6.0	-6.5	-4.5	-11.9	89	80	79	83	0.4	0.8	0.8	0.7	10	10	10	SE 7	SE 8	SE 8
26	93.5	88.2	84.0	88.6	-7.9	-5.8	-6.0	-6.4	-5.4	-8.0	81	74	84	80	0.6	1.0	0.6	0.7	10	10	10 *	SE 7	ESE 9	SE 9
27	83.3	81.6	70.9	78.6	-4.1	-3.1	-3.6	-3.6	-2.9	-6.2	91	93	85	90	0.4	0.4	0.7	0.5	10	10	10 *	SE 4	ESE 4	SSE 9
28	63.7	64.5	67.4	65.2	1.8	2.2	0.2	1.1	2.4	-3.6	91	91	88	90	0.7	0.7	0.7	0.7	10	10	10	S 6	SSE 4	SSW 8
29	72.2	78.3	82.9	77.8	0.6	0.7	-4.0	-1.7	1.3	-4.4	82	77	87	82	1.1	1.5	0.6	1.1	9 *	10 *	7	SSW 8	SW 8	SE 4
30	76.0	75.5	77.1	76.2	-0.4	2.2	0.8	0.8	2.7	-4.4	82	70	90	81	1.1	2.2	0.7	1.3	10	10	10 •	SE 7	SE 9	SE 1
31																								
M	90.7	91.1	90.9	90.9	-3.4	-1.4	-3.0	-2.7	-0.6	-5.3	85	79	85	83	0.8	1.4	0.8	1.0	9.3	9.2	8.5	4.2	4.9	4.5

Grudzień – Décembre

1	75.3	75.7	76.6	75.9	0.2	-0.3	1.2	0.6	1.2	-0.4	94	88	83	88	0.4	0.8	1.2	0.8	10 *	8	10 •	SSW 2	SSE 4	S 8
2	82.5	83.7	84.6	83.6	-1.0	0.3	-0.4	-0.4	1.2	-1.0	81	82	86	83	1.1	1.1	0.8	1.0	8	10 *	10	SW 6	SSE 1	SSW 3
3	80.6	78.8	79.4	79.6	-2.4	-0.6	-2.8	-2.2	-0.2	-4.3	91	77	86	85	0.4	1.3	0.7	0.8	9	10	10	SE 5	SE 6	SE 2
4	77.6	77.7	80.6	78.6	-1.7	-0.8	0.2	-0.5	0.2	-3.1	90	93	98	94	0.6	0.4	0.1	0.4	10 *	10 *	10 ≡	SE 3	SSW 1	S 7
5	82.7	83.2	76.1	80.7	-0.3	0.2	-0.4	-0.2	0.7	-1.8	94	89	86	90	0.4	0.7	0.8	0.6	10	10	8	SSE 4	S 6	SE 8
6	64.7	66.8	71.7	67.7	2.2	3.6	3.0	3.0	3.6	-0.6	91	68	69	76	0.7	2.5	2.4	1.9	5	10	4	S 7	SSW 9	SSW 12
7	79.2	81.7	85.4	82.1	1.0	2.0	1.8	1.6	3.0	0.4	79	76	80	78	1.4	1.7	1.5	1.5	9	10	10	SSW 9	SSW 8	SSW 7
8	87.1	88.0	90.5	88.5	1.0	1.0	-0.6	0.2	2.1	-0.8	83	88	85	85	1.2	0.8	0.9	1.0	10	10 *	9	S 6	SSW 4	WSW 4
9	93.3	91.3	80.6	88.4	-2.9	0.0	0.4	-0.5	0.8	-3.8	86	82	72	80	0.7	1.1	1.8	1.2	4	10	10	SW 6	S 8	SSE 8
10	65.4	63.7	62.3	63.8	0.8	1.2	2.2	1.6	2.7	-0.9	65	87	87	80	2.3	0.9	1.0	1.4	9	10 *	9	S 10	SSW 9	SSE 6
11	64.5	68.0	70.7	67.7	1.8	2.2	0.2	1.1	3.2	0.1	85	73	78	79	1.1	2.0	1.4	1.5	9	9	8	SSW 7	SW 7	SSW 7
12	73.4	77.4	82.1	77.6	0.2	-0.2	-0.8	-0.4	0.6	-1.5	85	90	83	86	1.0	0.6	1.0	0.9	10	10 *	10	SW 4	SW 4	WSW 3
13	84.6	86.1	87.4	86.0	-1.4	-1.6	-3.4	-2.4	-0.8	-3.4	88	88	85	87	0.6	0.6	0.7	0.6	10 *	7	10 *	WSW 2	W 3	SW 2
14	89.4	91.5	95.5	92.1	-6.0	-4.0	-1.6	-3.3	-1.4	-8.1	94	87	84	88	0.2	0.6	0.9	0.6	9 *	10 *	10 *	SW 2	WSW 3	WNW 3
15	96.4	97.0	99.0	97.5	-3.7	-4.2	-10.6	-7.3	-1.6	-10.9	87	75	84	82	0.6	1.1	0.4	0.7	10 *	3	0	WSW 2	W 2	WSW 3
16	98.0	97.6	96.7	97.4	-6.7	-4.8	-4.0	-4.9	-3.9	-12.7	88	91	89	89	0.4	0.4	0.5	0.4	9	8	10	WSW 3	WSW 5	WSW 3
17	97.6	99.0	98.4	98.3	-7.7	-10.1	-12.1	-10.5	-4.0	-14.9	84	81	85	83	0.5	0.5	0.4	0.5	9	0	9	SW 6	SSE 3	SE 2
18	97.6	95.0	88.4	93.7	-9.5	-6.8	-0.9	-4.5	-0.8	-12.3	85	91	93	90	0.4	0.3	0.4	0.4	10	10	10 •	SE 6	SE 7	SE 9
19	85.0	84.6	83.2	84.3	2.5	5.0	4.6	4.2	5.1	-0.9	96	98	95	96	0.3	0.1	0.4	0.3	10 •	10 • ≡	10 •	SSW 4	SW 5	SSW 5
20	86.7	90.4	92.9	90.0	2.6	2.7	2.6	2.6	5.6	1.9	84	88	75	82	1.2	0.9	1.9	1.3	10	10	10	SW 6	SW 5	SW 5
21	92.1	90.7	91.1	91.3	1.3	1.6	0.2	0.8	2.6	-0.4	81	87	86	85	1.3	0.9	0.9	1.0	10	10	4	SSW 3	SSW 1	SW 3
22	93.6	95.8	97.4	95.6	-0.4	0.2	-1.0	-0.6	0.3	-1.0	90	82	89	87	0.6	1.1	0.7	0.8	10	10	9	W 2	W 2	WNW 1
23	97.3	95.9	92.4	95.2	-5.8	-2.0	-6.3	-5.1	-0.4	-7.4	95	71	91	86	0.2	1.6	0.3	0.7	0	6	0	C 0	SE 3	SE 3
24	86.6	84.2	80.1	83.6	-6.0	-4.8	-3.0	-4.2	-3.0	-7.1	87	86	90	88	0.5	0.6	0.5	0.5	10	10	10	ESE 6	SE 7	ESE 5
25	74.9	72.1	70.9	72.6	-2.2	-0.7	-0.6	-1.0	-0.2	-3.2	89	87	85	87	0.6	0.7	0.9	0.7	10 △	10	10	ESE 7	SE 8	SE 7
26	69.1	69.8	72.7	70.5	-1.0	-0.6	-0.1	-0.4	-0.1	-1.3	89	89	92	90	0.7	0.6	0.5	0.6	10	10 *	10 *	SE 8	SSE 6	SSW 2
27	78.7	80.3	77.9	79.0	-2.4	-0.4	-1.4	-1.4	0.3	-3.9	89	86	84	86	0.5	0.8	0.9	0.7	9	8	9	SW 3	SSW 6	SSE 4
28	73.2	72.7	77.2	74.4	-1.8	-1.1	-2.4	-1.9	-0.9	-2.4	90	91	85	89	0.5	0.5	0.8	0.6	10 *	10 *	9	SSE 1	SW 2	SW 4
29	80.8	83.9	84.6	83.1	-1.7	-1.4	-4.2	-2.9	-1.0	-5.9	86	78	84	83	0.8	1.2	0.7	0.9	9	8	8 *	SW 6	SW 4	SW 7
30	84.2	84.2	79.8	82.7	-2.2	-2.2	-3.0	-2.6	-0.6	-4.4	87	87	88	87	0.7	0.7	0.6	0.7	8	9	10 *	SW 5	SSW 7	S 6
31	80.0	80.4	79.8	80.1	0.8	1.0	1.2	1.0	1.2	-3.0	86	87	83	85	0.9	0.9	1.2	1.0	10	10 *	10	SW 5	SW 6	SSW 6
M	83.0	83.5	83.4	83.3	-1.7	-0.8	-1.4	-1.3	0.5	-3.9	87	85	85	86	0.7	0.9	0.9	0.8	8.9	8.9	8.6	4.7	4.9	5.0

Suwałki — $H_s = 165\,m$ — $H_b = 169{,}6\,m$ — $h_w = 13\,m$ — Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	7.6	•	•° 14^25 – 23^30
2	8	2.7	•	∇° 0^20-27 – 6^25 6^40 ∇' – 17^25 ∇° 18^25 23^45 – 24, ≫ 9^32 – 10^30 11^07-08, 11^30 – 12^18 12^20 – 13^15 por. wiatru 14 m/sek 13^30 – 14^36 ≫ 15^20 – 16^30 por. wiatru 14 m/sek 16^20 – 18^30 por. wiatru 12 m/sek 19^30 – 20^10
3	8	•	•	∇° 0^00-15, 0^30 – 1^10, ≫ 13^40 – 14^15
4	7	0.4	•	∇° 12^40 – 14^45 16^45 – 18^35 19^20-30, ⌓° 1 – 8
5	7	0.9	•	•° 1^20 – 2^40, 3^30 – 4^30 ∇° 8^40 – 9^10 •° 11^05 – 12^15 ∇° 13^35 – 14^10, 15^32-45 ∇' – 15^05 ∇° – 16^10
6	5	1.3	•	•° 3^45 – 4^15, 5^10 – 7^30 •' – 8^20 •° – 11^30 •° 18^15 – 19^25 •° – 20^20 •' – 21^16, = 5^20 – 8^00, 10^30 – 24
7	7	•	•	= 0^00 – 10^30, 18^30 – 24; ⌓' 19 – 22 ⌣° – 24
8	7	•	•	= 0^00-30; ⌣' 0^00 – 9
9	7	0.5	•	•° 22^45 – 23^10 •° – 24, = 6^10 – 11^20 14^10 – 15^50 ≡° – 22^40 = – 24; ⌓° 20 – 22
10	8	0.0	•	•° 0^00 – 2^35 3^20 – 4^40 ∇° 8^15-25, 11^02-15, = 0^00 – 9^10
11	7	0.1	•	*° 17^40 – 18^10, 20^10 – 21^16 – 24; = 3^10 – 5^30 6^20-50 ≡° – 8^40 = – 11^25, 15^35 – 18^20; ⌣° 1 – 10
12	8	0.3	1	*° 0^00 – 2^40 *' 14^05 – 15^40 *° – 20^30, 21^50 – 23^10 – 24
13	8	0.0	1	*° 0^00 – 2^45 ∇° 7^15 – 9^12, 9^30 – 10^25, 12^40 – 14^12, 14^25-50, 15^01-25, 16^50 – 20^05, 20^20 – 21^10 *° – 24
14	7	0.8	pz.	*° 0^00 – 1^45 2^20 – 10^15, 11^40 – 21^15 22^10 – 24
15	6	2.4	2	*° 0^00 – 14^05 *' – 15^40 *° – 24
16	7	0.0	5	*° 0^00 – 4^10, 23^10 – 24, ⌔ 4^25-50
17	7	0.2	5	*° 0^00 – 5^10 8^05 – 9^25 10^02 – 11^20 18^35 – 24; = 8^02 – 12^15, 18^15 – 24
18	6	0.0	6	*° 0^00 – 14^45; = 0^00 – 17^30
19	5	4.2	6	*° 8^20 – 19^45 *' – 21^15 *° – 24
20	6	0.0	13	*° 0^00 – 3^40 △° 9^10 – 11^30; = 6^10 – 24
21	5	9.2	13	△° 10^35 12^10 *° 13^40 – 14^30 *' – 15^25 *° – 22^00 *' – 24; ⊹° 22^00 – 24; = 0^00 – 24
22	6	0.0	18	*' 0^00 – 4^30 *° – 7^30 △° 8^15 – 11^18 *° 14^25 – 15^25; ⊹° 0^00 – 7^45; = 0^00 – 6^10, 12^10 – 15^20
23	5	•	18	= 8^30 – 9^40 ≡° – 13^35 = – 17^20, 23^10 – 24
24	5	0.0	18	*° 9^30 – 12^30 = 0^00 – 24; V° 2^45 – 24
25	7	•	18	⊹° 16^35 – 22^40 ≫ 11^05 – 12^30 14^10 – 18^15; = 0^00 – 10^40; V° 0^00 – 8
26	7	2.4	18	*' 19^30 – 22^10 *° – 24, ⊹° 16^40 – 24; ≫ 19^15 – 20^20
27	5	2.0	20	*° 0^00 – 4^30 16^45 – 24; ⊹° 0^00 – 4^20 18^40 – 24; ≫ 21^40 – 24; = 7^15 – 9^15 ≡° – 11^40 = – 15^50 ≡° – 16^35 = – 16^45
28	6	2.9	24	*° 0^00 – 2^20 *° – 2^45 •° – 5^15 12^35 – 16^15 *° – 17^10 22^40 – 24; ⊹° 0^00 – 2^45; ≫ 0^00 – 2^30; = 6^05 – 24
29	7	0.2	22	*° 0^00 – 3^35 ∇° 6^15 – 7^35, 9^05 – 25, 11^05 – 13^10; = 0^00 – 6^15
30	8	7.5	20	∇° 8^15 – 10^20 •° 17^30 – 18^15, 19^15 – 24; ≫ 7^18-50, 9^05 – 11^20
31				
Σ	–	45.6	–	

Grudzień - Décembre

1	6	0.5	18	•° 0^00-40 *° – 9^30 14^20 – 18^15 •° – 22^40, ≫ 17^40-50 por. wiatru 14 m/sek 20^20-50 ≫ – 24; = 1^30 – 24
2	6	1.2	14	*° 12^15 – 13^20 19^10; ≫ 0^00 – 2^35; = 0^00 – 2^30, 13^20 – 24
3	7	1.7	15	= 0^00 – 10^35, ⌔ 19^15 – 20^15
4	5	4.0	17	*' 3^50 – 4^15 *° – 7^25 *' – 11^50 *° – 15^30; = 7^50 – 19^45 ≡° – 24
5	5	4.4	20	*° 7^40 – 11^15 •° 23^15 – 24; ≡° 0^00 – 1^35 = – 16^40 ≡° – 18^35 = – 24; ≫ 22^04 – 24, ⌔ 20^40 – 21^05
6	8	0.0	23	•° 0^00-50 *' – 2^10 *° – 2^50 •° – 3^25; ⊹° 0^50 – 2^50; ≫ 0^00 – 3^10 por. wiatru 14 m/sek 3^10 – 5^15 9^30 – 11^20 12^40 – 13^10 ≫ 13^50 – 22^10; = 0^00 – 3^20
7	7	0.0	16	•° 3^50 – 5^15 *° 8^15-20 ∇° 11^10-25, 11^50 – 12^10, ≫ 0^45 – 1^25 por. wiatru 14 m/sek 5^25 – 6^35, 9^40 – 11^50
8	6	0.1	15	*° 11^10 – 13^15 14^15 – 17^15; = 7^30 – 19^10
9	7	1.4	13	*° 21^25 – 22^40 *' – 23^10 *° – 24, ⊹° 22^30 – 24 por. wiatru 12 m/sek 18^55 – 19^10, por. wiatru 14 m/sek 20^15 – 24; = 12^35 – 15^20
10	7	1.1	14	*° 0^00-50 *° 9^30 – 10^15 *° – 13^25 •° – 14^10, ⊹° 0^00 – 2^50 ⊹° 14^35 – 6^10 ⊹° – 7^40, por. wiatru 14 m/sek 0^00-50 ≫ 1^15 5^38 ↖ – 5^40 ≫ – 6^25 ↖ – 6^35 ≫ – 7^15 ↖ – 7^25 ≫ – 9^30 por. wiatru 14 m/sek – 11^25
11	7	•	12	
12	7	0.0	10	*° 11^10 – 14^15 △° – 16^20 *° 23^45 – 24, ⌔' 1^25-40
13	6	0.8	10	*° 0^00 – 9^20 *' – 10^10 *° – 11^25 14^25 – 16^20, 20^25 – 21^05 – 23^10; = 11^25 – 15^15
14	6	0.8	12	*° 1^01 – 2^20 5^10 – 7^15 *° 12^15 – 14^30 *° – 16^10, 18^10 – 24; = 0^40 – 7^10
15	7	0.0	14	*° 0^00 – 9^35
16	7	0.4	16	*° 14^15 – 20^10, 21^05 – 24; = 6^20 – 10^10, 14^25 – 24
17	6	•	16	*° 0^00 – 5^10; = 0^00 – 5^30, 8^10 – 24
18	6	5.5	16	*° 16^40 – 19^15 ◉° – 22^50 •° – 24; = 0^00 – 24; ∾ 19^15 – 22^50
19	2	12.6	14	•° 0^00 – 9^25 •° – 12^15 •' – 14^20 •° – 16^10 •° 18^45 – 19^15 •° – 24; = 0^00 – 9^45 ≡° – 10^32 =' – 14^10 ≡° – 16^50 = – 24
20	7	0.5	9	•° 0^00-40, 1^15 – 3^10 •° 4^35 – 5^45 ∇° 8^45 – 9^05, 11^15-25, = 0^00 – 6^10
21	6	•	7	= 10^30 – 24
22	7	0.0	5	*° 11^22-30, = 0^00 – 9^20
23	7	•	5	= 23^40 – 24
24	7	0.0	5	= 0^00 – 7^50
25	6	0.1	5	△° 5^15 – 7^40, 21^40 – 23^10 *° – 24, ≫ 12^18-25; = 8^15 – 14^20
26	5	4.9	6	*° 0^00 – 1^50 4^44 – 6^15 *° 7^28 – 8^15 *° 9^40 – 10^50 *' – 12^10 *° – 24; = 7^20 – 24
27	7	0.2	12	*° 0^00 – 2^15, 23^45 – 24, = 0^00 – 11^20, 16^40 – 24
28	5	1.8	13	*° 0^00 – 1^50, 3^45 – 7^20 *' – 10^15 *° – 18^30, 21^40 – 24; = 0^00 – 1^40
29	7	1.2	16	*° 0^00-30 △° 9^40 – 10^05 ∇° 20^15 – 24
30	7	0.6	19	∇° 0^00 – 1^20 *° 1^50 – 3^45 7^40 – 11^40, 18^30 – 24; ⊹° 2^40 – 3^40; por. wiatru do 14 m/sek 1^05 – 3^05
31	6	0.9	19	*° 0^00 – 5^10, 11^40 – 12^01 ∇° – 13^05 •° 21^20 – 23^40; = 7^10 – 24
Σ	–	44.7	–	

Olsztyn - Dajtki φ = 53°46' λ = 20°25' Styczeń – Janvier 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	83.1	83.6	83.7	83.5	3.7	3.8	3.8	3.8	4.5	2.2	97	83	75	85	0.3	1.3	2.0	1.2	10	9	7	SW 6	SW 4	SW 4
2	82.0	82.5	84.2	82.9	1.2	1.7	0.4	0.9	3.8	0.4	96	92	94	94	0.3	0.5	0.4	0.4	4	10	9	SW 4	SW 5	SW 3
3	87.3	90.1	93.5	90.3	0.8	1.9	-1.8	-0.2	2.4	-2.6	94	82	98	91	0.4	1.3	0.1	0.6	10	2	9	SW 3	SW 3	C 0
4	98.0	101.2	102.3	100.5	-0.6	1.2	-2.2	-1.0	1.5	-3.1	91	79	85	85	0.5	1.4	0.8	0.9	9	9	0	W 3	NW 3	W 3
5	89.4	90.6	95.0	91.7	-0.8	0.7	0.6	0.3	1.2	-3.5	95	75	62	77	0.3	1.6	2.5	1.5	10 *	3	3	SW 10	WNW 11	NW 10
6	98.8	100.3	101.9	100.3	-1.0	-0.6	-2.9	-1.8	0.6	-4.1	71	77	91	80	1.7	1.3	0.4	1.1	9	7 *	9 *	W 7	WNW 9	NW 5
7	103.7	103.0	100.3	102.3	-3.4	-1.2	-6.0	-4.2	-1.0	-6.1	92	68	94	85	0.4	1.8	0.2	0.8	9	8	0	NW 3	NW 5	SW 2
8	90.0	85.5	77.5	84.3	-3.5	0.8	2.8	0.7	2.8	-6.1	97	100	96	98	0.1	0.0	0.3	0.1	10 *	10 ≡	10 ● *	SW 6	WSW 5	SW 6
9	80.9	83.7	86.7	83.8	3.3	2.8	-1.7	0.7	4.1	-1.9	86	88	88	87	1.0	1.0	0.7	0.9	10 ●	10	10	W 7	WNW 6	NE 3
10	87.8	93.8	104.6	95.4	-7.0	-9.4	-14.2	-11.2	-1.6	-15.9	93	72	87	84	0.2	0.8	0.3	0.4	10 *	7	0	ENE 6	NE 4	N 2
11	110.1	109.7	106.8	108.9	-17.2	-9.7	-11.4	-12.4	-9.2	-18.9	85	75	79	80	0.2	0.7	0.5	0.5	0	8	4	SW 1	S 4	S 4
12	102.2	101.6	99.7	101.2	-8.4	-3.9	-5.1	-5.6	-3.2	-11.5	80	80	83	81	0.6	0.9	0.7	0.7	10	10	1	S 4	SSE 3	SSE 4
13	97.7	97.6	99.2	98.2	-4.0	-1.0	0.5	-1.0	0.6	-5.9	77	77	96	83	1.0	1.3	0.2	0.8	1	2	10 ●	S 2	S 6	SW 4
14	98.2	95.7	95.5	96.5	0.7	0.2	0.0	0.2	1.0	-1.8	92	76	84	84	0.5	1.5	0.9	1.0	10	0	9	SE 3	S 4	SW 4
15	100.6	102.7	103.6	102.3	1.7	2.6	-0.6	0.8	2.6	-1.1	87	74	85	82	0.9	2.0	0.9	1.3	10	0	4	SW 5	SW 5	SW 4
16	99.8	98.8	97.8	98.8	-0.8	0.8	0.6	0.3	1.0	-1.6	87	90	92	90	0.7	0.7	0.5	0.6	10 *	8	10	S 3	S 5	SW 4
17	84.9	79.1	73.5	79.2	-0.6	1.8	2.9	1.8	3.1	-1.5	79	85	86	83	1.2	1.1	1.0	1.1	10	9	9	SE 8	SSW 7	S 6
18	73.9	74.7	75.4	74.7	2.9	3.8	1.6	2.5	3.9	1.5	89	75	87	84	0.8	2.0	0.9	1.2	10	7	2	SW 3	SW 4	S 6
19	75.7	78.0	81.0	78.2	0.8	2.7	-1.3	0.2	3.0	-1.9	90	82	96	89	0.7	1.3	0.3	0.8	9	6	0	SSW 4	SW 2	C 0
20	82.9	83.1	79.4	81.8	-3.0	-1.4	-1.2	-1.7	-1.2	-4.4	95	96	95	95	0.2	0.2	0.3	0.2	3	10	10 *	SE 1	ENE 4	NE 5
21	77.2	80.2	85.0	80.8	0.5	0.8	0.9	0.8	1.0	-1.5	98	98	100	99	0.1	0.2	0.0	0.1	10 *	10 *	10 ●	E 3	E 4	SE 3
22	87.3	90.0	95.2	90.8	0.2	0.4	0.2	0.2	0.9	0.2	100	94	92	95	0.0	0.4	0.5	0.3	10 *	10	7	S 1	S 4	SW 2
23	99.5	102.2	105.0	102.2	-3.5	-0.8	-0.8	-1.5	0.5	-4.8	95	87	87	90	0.2	0.8	0.8	0.6	1	10	10	E 2	E 3	NE 2
24	107.3	108.5	108.5	108.1	-1.6	-1.2	-0.2	-0.8	0.0	-1.9	94	96	92	94	0.3	0.2	0.5	0.3	10	10	10	N 2	NW 2	N 3
25	104.5	102.5	101.4	102.8	-0.9	-2.2	-6.6	-4.1	-0.2	-6.9	100	94	83	92	0.0	0.3	0.6	0.3	10 *	10	10	N 2	E 3	E 3
26	100.0	100.5	101.1	100.5	-4.8	-3.0	-3.4	-3.6	-2.5	-7.2	95	97	97	96	0.2	0.1	0.2	0.2	10	10	10	ESE 2	E 3	SE 4
27	102.4	102.6	101.7	102.2	-3.0	-3.4	-2.8	-3.0	-2.4	-4.4	88	83	95	89	0.6	0.8	0.2	0.5	10	10	10 *	E 3	ESE 3	SE 5
28	100.3	101.1	99.9	100.4	-3.3	-2.8	-4.6	-3.8	-2.3	-4.9	92	93	88	91	0.4	0.4	0.5	0.4	10 *	10	10	ESE 4	SSE 4	E 4
29	95.9	94.2	92.5	94.2	-2.5	-0.2	0.9	-0.2	0.9	-4.7	91	94	100	95	0.5	0.4	0.0	0.3	10	10	10	E 3	SE 3	SW 1
30	93.4	93.4	91.8	92.9	-1.0	0.4	-1.0	-0.6	1.0	-1.6	99	96	97	97	0.1	0.3	0.2	0.2	10	10 ≡	10 *	W 1	E 2	NE 2
31	95.4	97.4	97.1	96.6	-4.6	-1.9	-7.3	-5.3	-0.7	-7.4	96	85	96	92	0.2	0.8	0.1	0.4	10 ≡	3	0	WNW 4	W 3	SW 2
M	93.2	93.8	94.2	93.7	-1.9	-0.5	-1.9	-1.6	0.5	-4.3	91	85	90	89	0.5	0.9	0.6	0.7	8.5	7.7	6.9	3.7	4.3	3.5

Luty – Février

1	95.7	96.1	98.6	96.8	-6.4	-2.4	-2.7	-3.6	-1.7	-11.4	94	91	95	93	0.2	0.4	0.2	0.3	9	4	5	W 3	WNW 4	W 4
2	101.5	104.8	108.9	105.1	-3.6	-1.4	-6.0	-4.2	-1.0	-6.8	92	78	94	88	0.4	1.2	0.2	0.6	7	3	2	W 5	N 5	W 4
3	105.3	102.9	103.7	104.0	-6.0	-0.6	-0.7	-2.0	0.2	-7.0	94	93	93	93	0.2	0.4	0.4	0.3	10 *	10	9	W 5	W 4	W 4
4	102.9	103.9	108.0	105.6	-0.6	-6.2	-15.2	-9.3	0.2	-17.4	95	68	91	85	0.3	1.2	0.2	0.6	10 *	2	0	WNW 6	N 6	C 0
5	105.2	105.9	109.0	106.7	-21.4	-13.0	-21.4	-19.3	-12.1	-23.3	81	88	81	83	0.2	0.3	0.2	0.2	2	0	0	C 0	N 3	NNE 2
6	109.4	107.0	103.9	106.8	-18.4	-10.3	-9.4	-11.9	-9.0	-24.6	84	77	91	84	0.2	0.6	0.3	0.4	9	10	10	NE 2	SSW 4	S 3
7	103.4	100.2	85.9	96.5	-12.6	-6.0	-1.8	-5.6	-1.3	-14.1	89	84	98	90	0.3	0.6	0.1	0.3	0	10	10 *	WSW 2	SW 6	W 5
8	80.8	83.8	92.3	85.6	-6.1	-4.2	-6.7	-5.9	-0.4	-7.5	86	68	75	76	0.5	1.4	0.9	0.9	3	4	9	NNW 6	NNW 8	N 7
9	99.5	102.8	102.3	101.5	-9.4	-8.4	-8.8	-8.8	-6.4	-10.3	85	66	92	81	0.4	1.1	0.3	0.6	10 *	0	8	N 4	NNW 4	WSW 4
10	91.0	86.9	90.0	89.3	-5.6	-2.1	-2.7	-3.3	-0.7	-8.8	95	96	89	93	0.2	0.2	0.6	0.3	10 *	10 *	6	SW 9	W 7	W 5
11	94.7	98.2	101.1	98.0	-4.6	-0.6	-3.3	-3.0	-0.2	-5.0	91	93	95	93	0.4	0.4	0.3	0.4	6	3	2	WNW 5	W 5	W 2
12	100.7	98.7	97.3	98.9	-2.1	0.3	1.4	0.3	1.4	-5.1	98	96	100	98	0.1	0.2	0.0	0.1	10 ≙	10	10 ●	SW 3	SW 4	WSW 5
13	87.5	82.4	76.7	82.2	0.9	1.3	1.6	1.4	1.6	0.3	92	98	94	95	0.5	0.1	0.4	0.3	10	10 *	10 ●	SW 6	SW 6	SW 4
14	69.9	71.2	80.9	74.0	0.2	0.4	0.0	0.2	1.6	-0.1	100	96	94	97	0.0	0.3	0.4	0.2	10 *	10 *	7	SSW 5	SW 6	W 5
15	87.7	89.9	92.0	89.9	-3.3	-1.0	-3.4	-2.8	0.0	-3.5	88	77	92	86	0.6	1.3	0.4	0.8	8	6	9	W 3	SW 3	WSW 3
16	95.9	99.4	103.0	99.4	-7.0	-2.1	-6.8	-5.7	-1.4	-10.5	96	79	94	90	0.1	1.1	0.2	0.5	10 *	2	10 ≡	SW 2	C 0	NE 2
17	103.1	102.9	106.0	104.0	-6.4	-3.4	-2.0	-3.4	-1.4	-7.6	94	92	89	92	0.2	0.4	0.6	0.4	10	10 *	10	N 7	N 6	NNE 5
18	106.2	107.2	108.3	107.3	-3.7	-4.9	-5.6	-5.0	-1.9	-6.5	87	86	85	86	0.6	0.6	0.6	0.6	10	10	10	NE 4	NE 7	NNE 3
19	110.1	110.2	112.9	111.1	-6.6	-4.6	-4.8	-5.2	-4.3	-8.5	94	86	81	87	0.2	0.6	0.8	0.5	10 *	10	10	NNE 5	NE 4	NE 3
20	115.6	117.5	117.2	116.8	-4.9	-1.6	-2.7	-3.0	-0.4	-5.3	81	78	86	82	0.8	1.2	0.7	0.9	10	1	10	ENE 5	E 4	NE 1
21	111.1	106.5	99.0	105.5	-3.5	-2.9	-2.2	-2.7	-2.2	-4.3	88	73	89	83	0.6	1.3	0.6	0.8	10	10	10 *	WNW 5	W 5	WNW 8
22	96.0	97.5	98.3	97.3	-4.1	-3.4	-6.9	-5.3	-1.0	-7.2	84	50	94	76	0.7	2.4	0.2	1.1	2	1	3	N 4	WNW 5	WNW 2
23	95.7	96.6	99.5	97.3	-8.4	-4.2	-13.8	-10.0	-4.1	-14.4	92	68	79	80	0.3	1.4	0.4	0.7	6	7	0	W 4	N 3	WNW 2
24	99.8	95.3	86.7	93.9	-13.7	-4.8	-5.7	-7.5	-4.3	-18.3	88	62	87	79	0.3	1.6	0.5	0.8	10	9	10 *	WSW 1	WSW 7	WSW 8
25	84.5	85.0	86.3	85.3	-7.7	-5.8	-6.3	-6.5	-4.2	-8.0	84	95	94	91	0.5	0.2	0.2	0.3	4	10 *	10 *	WNW 6	WNW 9	W 7
26	89.7	88.9	83.8	87.5	-7.7	-4.4	-7.8	-6.9	-4.4	-8.8	87	65	93	81	0.4	1.6	0.2	0.7	8 *	3	10	W 5	WSW 5	S 3
27	73.8	72.5	78.8	75.0	-5.3	-2.2	-8.0	-5.9	-1.7	-8.0	95	89	93	92	0.2	0.6	0.2	0.3	10 *	10 *	10 *	SE 2	S 3	NNW 6
28	88.1	92.8	96.3	92.4	-8.0	-6.0	-10.4	-8.7	-5.4	-10.4	87	81	90	86	0.4	0.7	0.3	0.5	6	8 *	6	NW 4	NNW 6	NW 2
29																								
30																								
31																								
M	96.6	96.8	97.4	96.9	-6.6	-3.7	-5.8	-5.5	-2.3	-9.4	90	81	90	87	0.4	0.8	0.4	0.5	7.9	6.5	7.4	4.2	5.0	3.9

Olsztyn - Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$ Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	POGODA
1	7	0.0	pż.	•0^00_1^40 ⚲0 3^52_5^35 7^05–45
2	7	•	•	= 7^20_17^10
3	6	•	•	= 6^20_7^10; ⌣0 19–24
4	7	0.8	•	= 0^00_7^10; ⌣0 0^00_11, 20–24
5	8	1.4	1	⚲0 5^40_6^30 ⚲1–9^35 ⚲0 13^35–39 15^01–09 15^33_16^20 16^45_17^40 22^44_24; ⩥ 6^45_9^45 12^30_24; ⸸1 6^45_9^45 ⸸0 14^50_19^10 ⸸0_24; ⌣0 0^00_5^40
6	8	0.4	2	⚲0 0^00_1^40 2^40_4^35 12^25–40 15^05_16^35, 19^20–40, 20^31_24; ⸸0 0^00_7^45; ⩥ 0^00_2^50, 10^30_11^30
7	8	0.3	3	⚲0 0^00–45, 8^50_11^05, 15^10_16^40
8	3	9.4	3	*0 5^45_7^50 ◎⌣–11^45 •0 14^50_15^35; •0–17^20 *0–18^10 ⚲1_21^20 •0–24; = 6^30_11^45 ≡0–15^20 = –24
9	7	1.7	•	•0 0^00_1^40 5^10_6^20 9^25 ⚲0 10^45_11^10, 14^35–50 *0 21^52_24; = 0^00_1^45
10	8	0.5	2	*0 0^00_7^30 *1–8^50 *0–10^40
11	7	•	2	
12	6	•	2	= 11^30–24; ⌣ 19^20–24
13	6	0.2	2	•0 19^25_21^20; = 0^00_24; ⌣ 0^00_3^00
14	5	0.1	2	*0 23^48–24; = 0^00_24
15	7	0.0	2	*0 0^00–1^40; = 0^00_9^30, 15^30_24
16	5	0.0	2	*0 5^52_7^15 17^25_19^40; = 0^00–24; ⌔ 0^00_3^00
17	6	2.5	2	*0 7^20–30 *1–8^40 *0–9^25 ⚲0–9^38 ◎⌣ 10^10–50 ⚲0 18^07_19^20, 23^15–24; ⸸ 7^30–9^40; = 0^00_20^20
18	8	•	pż.	⚲0 0^00–10, 1^10_4^20
19	7	0.0	•	⚲0 10^40_11^25; = 16^30–24; ⌣0 1–8, 19–24
20	5	2.8	•	*0 17^45–24; = 0^00–24; ⌣0 0^00–1 ⌣1–18; ⌔ 1^00_5^00
21	6	2.6	4	*0 0^00_16^10 •0–24; = 0^00–24
22	6	0.3	4	•0 0^00_3^35 •*0–4^15 *0–9^40, 13^35_15^40, 17^10–18^20 ⚲0–19^35; = 0^00_20^30
23	5	•	4	= 6^20–24
24	5	0.4	4	= 0^00_12^45 ≡0–13^10 = –24
25	5	0.1	4	*0 2^40_7^20 •0 7^40_8^50 ◎⌣0–11^45; = 0^00_7^45 ≡0–9^40 = –14^30, 15^30_24
26	5	•	4	= 0^00_24; V 7^40_11^50
27	7	2.3	4	*0 16^20–24; = 0^00_12^30, 13^30_24
28	5	0.2	6	*0 0^00–4^40, 5^52–7^35; = 0^00_24
29	6	0.8	7	*0 20^40–21^20; = 0^00–24
30	4	3.9	7	*0 2^35–6^20, 13^05–24; = 0^00_7^30 ≡0–12^50 = –24
31	7	•	10	*0 0^00–3^40; = 0^00–6^20 ≡0–8^20 = –9^40; V 0 6^20–8^20
Σ	–	30.7	–	

Luty - Février

1	7	1.8	11	⚲0 7^40_8^50 ⚲2–9^15 ⚲0–9^40 ⚲1_10^40 ⚲0 18^20–45, 19^40_20^10 ⚲1 21^40_23^20; = 0^30_1^30
2	8	1.0	14	⚲0 0^40_2^20 7^40–50 8^20–25 9^10_11^05, 18^10–25
3	7	1.0	16	⚲0 0^10_1^40, 2^15–40, 2^50_4^20, 4^35_12^10, 13^20–40, 17^40_18^15, 22^45_23^38
4	8	0.9	16	⚲0 2^40_3^30 5^52–9^40
5	5	•	16	= 2^30_7^40 ≡0–10^20 = –24; V 5^50–10^20
6	6	0.1	16	*0 13^48–17^10; = 0^00–24
7	6	3.4	16	*0 16^10–21^15 *1–24; = 0^00–30, 6^40–24
8	8	0.1	18	*0 0^00–40 *0–1^50, 23^55–24; ⸸ 0^50–5^10 ⸸–6^50 ⸸ 14^30–18^55; ⩥ 14^20–16^20, = 0^00–5^10
9	8	1.0	18	*0 0^00–3^35 4^10–8^40 ⚲0–9^30
10	1	4.4	20	⚲0 4^30–5^10 *0 5^25–7^10 *1–13^20 ⚲0 14^15–15^10, 18^25_19^20; ⸸ 2^40_13^20; ⩥ 7^35–11^30
11	8	0.0	22	⚲0 2^52_3^40, 4^40_6^25; = 23^30–24
12	5	0.3	22	△ 6^20_7^25 *0–7^40 △–9^45 •*0 16^05–20 •0–18^40, 20^20_23^20; = 0^00–24
13	5	4.1	18	*0 6^50_13^20 ⚲0–15^25, 17^45_18^20 •0–22^20; = 0^00_1^20, 6^35–23^30
14	6	2.7	18	⚲0 1^55_5^40 ⚲1 6^35–8^07 ⚲0–8^20 ⚲1–11^45 ⚲0–13^10 ⚲1–14^20 ⚲0 15^45–18^10, 19^10–20^05, 21^50_22^05; ⩥ 9^15–40
15	8	1.7	18	⚲0 16^20–19^40
16	7	0.0	18	⚲0 2^20_6^40, 8^05–15; = 2^20_11^20, 16^30_19^50 ≡0–21^40 = –24; V 0 20^50–24
17	6	0.2	17	*0 7^05_13^10; = 0^00_21^30; V 0 0^00_7^05
18	6	0.0	17	*0 8^45–12^20, 21^35_22^40; = 8^45–24
19	6	0.0	17	*0 5^25–8^05; = 0^00_11^30
20	6	0.0	17	*0 9^20–10^10; = 8^25–24
21	6	1.0	17	*0 14^40–15^35, 21^45–24; = 0^00–24
22	8	0.8	19	*0 0^00_5^20 ⚲0 17^20–40; = 0^00_5^20
23	7	0.3	20	⚲0 3^52_5^40 ⚲1 9^40_10^05 ⚲0–11^25
24	8	2.0	20	⚲0 17^40_20^02 *0–24; ⸸ 19^40–24
25	5	4.6	23	*0 0^00_3^20 ⚲1 8^10–15 ⚲0–8^25 ⚲1 8^35–9^20 11^45–55 12^15–25, 12^35_13^10 16^05_17^05 17^10_19^30 20^04_23^20; ⸸ 0^00_3^20 ⸸–6^40 ⸸ 10^25–24
26	8	1.4	25	⚲0 2^40_3^45 4^50_6^05, 6^20_7^10 *0 23^50–24; ⸸ 0^00_3^45
27	5	4.5	26	*0 0^00_8^10 *1–8^30 *0–8^59 9^05_14^25 *1–16^40 *0–22^20 ⚲0–24; ⸸ 20^50–24; = 9^30–24
28	7	0.3	28	⚲0 0^00_3^20, 12^28_13^02, 14^05–52; ⸸ 0^00_2^45; = 0^00_1^50
29				
30				
31				
Σ	–	37.6	–	

Olsztyn-Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ *Marzec — Mars* 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	95.1	92.1	88.1	91.8	-9.9	-5.4	-7.2	-7.4	-4.5	-12.3	88	62	82	77	0.4	1.5	0.6	0.8	10 *	8	8	E 5	E 5	E 3
2	83.5	81.3	79.2	81.3	-5.4	-5.6	-5.6	-4.0	-3.0	-7.2	95	90	92	92	0.2	0.5	0.4	0.4	10 *	10 *	10	ENE 4	NE 4	NE 4
3	75.9	72.3	72.6	73.6	-3.8	-2.5	-2.8	-3.0	-1.0	-4.5	92	95	95	94	0.4	0.3	0.2	0.3	10 *	10 *	10 *	NE 4	NE 3	S 6
4	74.4	76.0	79.7	76.7	-3.1	-3.0	-3.8	-3.4	-1.8	-4.3	81	77	92	83	0.9	1.1	0.4	0.8	9	10 *	10 *	SSE 6	SE 8	S 5
5	84.3	88.5	94.6	89.1	-3.9	-2.3	-3.6	-3.4	-1.9	-4.3	96	78	92	89	0.2	1.2	0.4	0.6	10	10	10 *	E 2	N 3	NW 4
6	101.6	105.3	108.9	105.3	-3.9	-3.1	-9.6	-6.6	-2.8	-9.9	89	77	82	83	0.5	1.1	0.5	0.7	10	2	0	NNE 4	NNE 5	N 3
7	111.8	113.7	114.1	113.2	-13.6	-6.6	-15.3	-12.7	-6.2	-16.5	92	59	86	79	0.2	1.5	0.3	0.7	10 ≡	0	0	C 0	NE 1	C 0
8	112.2	110.6	108.7	110.5	-21.9	-3.4	-12.7	-12.7	-2.7	-22.9	88	52	81	74	0.1	2.3	0.4	0.9	1	1	0	C 0	SW 1	SW 1
9	106.9	105.8	105.5	106.1	-18.6	-3.3	-5.6	-8.3	-3.2	-19.8	84	63	90	79	0.2	1.8	0.4	0.8	2	0	4	SW 2	SW 3	W 5
10	109.6	111.2	111.8	110.9	-8.8	-0.9	-4.9	-4.8	0.7	-9.2	92	59	88	80	0.3	2.3	0.5	1.0	4	1	2	WNW 3	W 3	W 3
11	112.3	112.9	112.0	112.4	-1.2	2.2	0.9	0.7	2.4	-3.2	95	71	85	84	0.3	2.1	1.0	1.1	10	10	10	W 5	W 4	W 3
12	111.0	110.0	108.8	109.9	-4.9	3.8	-1.4	-1.0	5.8	-5.3	78	43	74	65	0.9	4.5	1.4	2.3	5	6	1	W 3	WSW 5	W 2
13	109.0	109.2	109.0	109.1	-9.6	7.3	-0.1	-0.6	7.7	-9.9	91	39	78	69	0.3	6.2	1.4	2.6	0	1	0	C 0	SW 3	SW 2
14	108.1	106.9	105.8	106.9	-7.1	7.4	1.6	0.9	7.7	-8.5	93	53	76	74	0.2	4.9	1.7	2.3	0	0	0	C 0	S 2	S 3
15	103.8	103.3	101.6	102.9	-4.2	6.6	3.9	2.6	8.0	-4.7	96	53	77	75	0.2	4.6	1.9	2.2	0	9	9	S 2	SSW 5	SSW 3
16	98.0	96.3	95.2	96.5	3.7	6.0	4.2	4.5	7.7	3.1	82	80	98	87	1.5	1.9	0.1	1.2	7	9	10 •	S 4	S 5	SSW 4
17	96.9	96.4	94.9	96.1	1.8	8.7	0.9	3.1	9.4	0.8	100	72	100	91	0.0	3.1	0.0	1.0	10 ≡	1	10 ≡	WSW 2	SW 4	SE 2
18	91.5	91.1	89.7	90.8	1.0	2.2	1.4	1.5	3.4	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10	10 ≡	SE 1	S 2	SE 3
19	86.6	87.4	92.4	88.8	2.0	7.2	4.0	4.3	8.2	1.2	94	74	93	87	0.4	2.7	0.5	1.2	7	8	9	S 2	S 3	SW 3
20	97.7	99.2	98.3	98.4	-1.1	4.6	2.0	1.9	5.8	-1.6	91	51	71	71	0.4	4.2	2.1	2.2	2	2	9	WSW 2	SW 4	SW 2
21	95.6	92.2	86.1	91.3	-2.8	3.3	0.3	0.3	3.8	-3.1	100	85	100	95	0.0	1.2	0.0	0.4	10 ≡	9	10 *	SW 2	SSE 3	N 4
22	91.8	94.9	97.5	94.7	-3.2	2.0	-1.0	-0.8	3.7	-4.0	95	69	89	84	0.2	2.2	0.7	1.0	1	1	0	W 3	W 6	W 3
23	98.1	96.1	91.6	95.3	-4.1	5.3	1.4	1.0	5.6	-5.6	94	35	59	63	0.3	5.8	2.8	3.0	3	1	0	WSW 1	S 5	SE 6
24	86.1	85.6	85.7	85.8	0.8	2.3	3.6	2.6	4.0	-0.3	79	96	97	91	1.4	0.3	0.3	0.7	10	10	7	SE 4	S 3	SE 2
25	85.3	87.7	92.9	88.6	4.0	3.0	1.6	2.6	5.1	1.3	100	95	85	93	0.0	0.4	1.1	0.5	10 ≡	10 •	10 *	SW 2	WSW 5	W 5
26	97.2	97.5	101.3	98.7	-0.7	5.8	2.4	2.4	6.4	-1.3	91	33	77	74	0.5	4.1	1.7	2.1	8	4	8	C 0	S 2	NE 2
27	108.4	111.9	114.5	111.6	-1.2	6.9	-0.3	1.3	7.6	-3.0	86	52	90	76	0.8	4.8	0.6	2.1	1	1	0	C 0	NNE 4	C 0
28	114.8	113.8	111.9	113.5	2.2	8.3	5.4	5.3	8.6	-1.3	84	70	83	79	1.2	3.3	1.6	2.0	9	10	10	SW 2	S 5	SSW 3
29	109.8	110.2	106.6	108.9	4.8	7.6	6.6	6.4	8.5	4.3	100	90	97	96	0.0	1.0	0.3	0.4	10 ≡	10	1	W 2	W 5	SW 2
30	98.5	100.7	106.9	102.0	5.8	3.3	0.9	2.7	7.6	0.5	85	93	75	84	1.4	0.5	1.6	1.2	4	10	0	WSW 6	NW 8	NW 7
31	104.6	104.7	106.8	105.4	1.0	7.1	0.0	2.0	7.6	-2.1	94	52	86	77	0.4	4.8	0.9	2.0	1	5	0	NW 4	NW 10	NW 7
M	98.7	98.9	99.1	98.9	-3.4	2.5	-1.0	-0.7	3.5	-5.0	91	69	86	82	0.4	2.5	0.8	1.2	6.3	5.8	5.4	2.5	4.2	3.4

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1	111.3	112.7	108.7	110.9	-1.2	3.8	1.2	1.2	4.1	-2.6	80	46	66	64	1.1	4.3	2.3	2.6	1	3	8	NW 4	NW 5	NW 2
2	103.9	106.3	107.0	105.7	2.2	7.8	-0.5	2.2	8.0	-0.7	87	34	77	66	1.0	7.0	1.3	3.1	1	3	0	NW 4	NNW 7	NNW 3
3	103.2	99.9	98.0	100.4	-1.6	6.0	1.9	2.0	6.0	-4.2	90	48	76	71	0.5	4.9	1.7	2.4	7	10	9	S 2	S 3	W 3
4	93.5	93.5	94.9	94.0	3.2	9.4	2.8	4.6	10.9	1.4	91	56	88	78	0.7	5.2	1.0	2.3	10	10	0	WNW 6	WNW 5	N 3
5	99.3	102.0	103.2	101.5	-0.6	7.1	1.2	2.2	8.8	-0.8	100	71	90	87	0.0	2.9	0.7	1.2	10 ≡	4	0	E 1	NNW 3	C 0
6	103.2	101.8	98.6	101.2	-2.0	12.9	7.2	6.3	13.4	-2.9	98	41	65	68	0.1	8.8	3.6	4.2	7 ≡	4	0	C 0	SSW 1	S 4
7	93.7	94.0	95.4	94.4	1.6	6.4	4.5	4.2	7.2	1.1	91	81	84	85	0.7	1.9	1.3	1.3	8	10	8	SSE 3	WNW 4	W 2
8	95.8	97.6	100.2	97.9	2.8	4.1	1.1	2.3	6.1	1.0	93	83	89	89	0.4	1.4	0.7	0.8	10	9	10	WNW 6	NW 2	NE 5
9	101.7	102.4	103.0	102.4	0.3	4.6	1.2	1.8	6.8	-0.4	74	59	55	63	1.6	3.3	3.0	2.7	10	8	0	E 6	E 8	E 5
10	102.8	102.6	102.2	102.3	-1.2	3.9	2.2	1.8	3.7	-1.7	74	48	51	58	1.4	4.2	3.6	3.1	9	10	10	E 5	E 5	E 4
11	100.4	98.6	98.3	99.1	0.4	7.9	4.0	4.1	9.4	-1.3	73	47	62	61	1.7	5.6	3.0	3.4	0	1	2	SE 5	SE 6	SSE 2
12	98.7	99.0	98.4	98.7	0.8	6.0	6.9	5.2	9.1	0.3	69	58	63	64	2.0	3.9	3.4	3.1	10	10	10	SE 3	S 3	S 4
13	97.4	97.1	97.3	97.3	2.0	6.2	8.3	6.2	8.7	1.7	69	62	56	62	2.2	3.7	4.9	3.6	8	10	9	SE 7	SE 5	SE 4
14	100.6	103.4	105.1	103.0	2.0	6.4	3.7	4.0	8.3	1.3	73	52	72	66	2.0	4.6	2.3	3.0	10	9	9	SE 3	SE 4	E 2
15	105.0	104.6	101.9	103.8	2.3	5.0	4.4	4.0	6.3	-2.6	93	69	80	81	0.5	2.7	1.7	1.6	10	10	10	E 3	SE 3	E 2
16	97.4	95.2	94.1	95.6	3.3	8.1	8.0	6.8	10.1	1.7	88	54	74	72	0.9	5.0	2.8	2.9	6	9	10 •	ESE 4	SE 5	S 3
17	93.0	93.7	90.7	92.3	6.4	6.3	5.8	6.1	8.0	5.7	98	97	88	94	0.1	0.2	1.1	0.3	10 •	10 •	7	SSE 4	WSW 3	S 2
18	81.8	80.6	84.4	82.3	6.6	8.7	7.8	7.7	9.1	5.1	85	85	91	87	1.4	1.6	0.9	1.3	10	10 •	9	SE 3	S 9	S 4
19	87.7	87.6	88.2	87.8	3.2	7.8	8.8	7.2	10.6	-0.7	100	89	76	88	0.0	1.2	2.7	1.3	10	10 •	10	C 0	E 4	E 5
20	89.5	89.9	92.1	90.5	7.9	13.3	10.7	10.6	13.3	4.7	80	56	69	68	2.0	6.8	4.0	4.3	3	8	10	E 5	E 6	E 6
21	91.5	90.2	89.5	90.4	8.1	9.1	8.1	8.4	10.7	6.2	87	88	100	92	1.4	1.4	0.0	0.9	9	10 •	10 •	E 6	E 7	E 2
22	97.7	86.1	85.9	89.9	8.3	11.5	6.2	8.0	13.3	5.6	82	47	85	71	2.0	7.2	1.3	3.6	7	10	10	ENE 6	E 10	NE 6
23	83.1	79.9	77.7	80.2	6.0	3.3	4.3	5.0	6.9	3.8	94	95	97	95	0.6	0.4	0.3	0.4	10	10 •	10 •	NE 3	NNW 3	N 3
24	77.3	80.1	82.9	80.2	3.7	6.0	4.9	4.9	6.7	3.1	98	88	95	94	0.2	1.2	0.5	0.6	10 •	10	10	SW 2	SW 4	WSW 4
25	86.7	90.1	91.9	89.6	4.5	9.1	7.0	6.9	11.0	3.7	97	70	93	87	0.3	3.6	0.7	1.3	10 •	9	10 •	SW 5	SW 3	SW 2
26	92.7	93.2	91.8	92.6	3.0	5.4	3.1	3.2	8.7	3.9	98	94	97	96	0.1	0.6	0.3	0.3	10	10 •	1	SW 1	SW 1	SE 2
27	90.9	89.5	90.0	90.1	4.1	9.1	8.9	7.8	12.0	0.1	98	93	86	92	0.2	0.8	1.3	0.8	2 ≡	10	10	C 0	NE 2	SE 2
28	90.7	90.4	90.8	90.6	8.1	14.3	11.6	11.4	15.0	6.6	91	51	52	65	0.9	8.1	6.5	5.2	8	9	10	E 7	E 8	E 5
29	92.2	93.9	96.0	94.0	7.6	12.5	9.2	9.6	13.0	7.2	80	68	80	76	2.0	4.7	2.3	3.0	10	9	9	E 2	ESE 6	NE 4
30	97.8	97.5	98.7	98.0	7.9	14.2	5.4	8.2	14.8	2.3	82	40	60	61	1.9	9.8	3.6	5.1	2	4	0	NNE 1	N 6	WNW 3
31																								
M	95.4	95.1	95.2	95.2	3.4	8.0	5.4	5.6	9.4	1.6	87	66	77	77	1.0	5.9	2.1	2.3	7.6	8.3	7.0	3.1	4.8	3.3

Olsztyn - Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$ Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.6	28	$*^{0}5^{54}-7^{40}$ $*^{1}8^{10}-9^{40}$ $\overset{*}{\nabla}{}^{0}-10^{25}$; $=5^{30}-7^{30}$
2	6	0.5	29	$*^{0}3^{45}-14^{10}$; $=3^{45}-24$
3	5	10.4	30	$*^{0}1^{40}-15^{40}$ $*^{1}-22^{20}$ $*^{0}-22^{50}$, $\dot{+}\,19^{50}-22^{20}$ $\dot{+}-22^{50}$; $=0^{00}-22^{10}$
4	6	1.5	34	$*^{0}0^{55}-11^{40}$ $\overset{*}{\nabla}{}^{0}12^{35}-13^{20}$ $\overset{*}{\nabla}{}^{1}14^{40}-16^{10}$ $\overset{*}{\nabla}{}^{0}-24$; $\dot{+}\,7^{45}-22^{40}$
5	7	0.7	36	$\overset{*}{\nabla}{}^{0}0^{00}-7^{40}$ $*^{0}6^{40}-9^{10}$, $16^{35}-22^{20}$... 24; $=6^{40}-10^{20}$, $16^{40}-24$
6	7	•	36	$*^{0}0^{00}$... 5^{45}; $=0^{00}-12^{20}$
7	7	•	35	$=4^{40}-5^{50}$ $\equiv^{0}-7^{45}$ $=-9^{30}$ $21^{40}-22^{40}$ $\equiv^{0}-24$; $\vee\,5^{50}-7^{45}$, $22^{40}-24$
8	8	•	35	$\equiv^{0}0^{00}-1^{50}$; $=-9^{20}$; $\vee\,0^{00}-1^{50}$
9	7	0.1	35	$*^{0}16^{20}-20^{20}$; $=20^{20}-24$
10	7	0.0	35	$=0^{00}-7^{20}$
11	7	•	34	⊙ $2^{55}-4^{40}$; $=5^{10}-11^{20}$
12	7	•	33	
13	6	•	30	$=1^{30}-12^{20}$ $\infty-17^{40}$ $=-24$
14	6	•	27	$=0^{00}-10^{20}$ $\infty-16^{30}$ $=-24$
15	6	•	25	$=0^{00}-10^{20}$ $\infty-14^{10}$ $=-24$
16	6	2.6	25	$\bullet^{0}10^{25}-45$, $18^{50}-24$; $=0^{00}-24$
17	7	•	20	$\bullet^{0}0^{00}-3^{40}$ 4^{40}; $=0^{00}-3^{50}$ $\equiv^{0}-5^{40}$ $\equiv^{1}-10^{45}$ $=-11^{20}$, $17^{45}-20^{40}$ $\equiv^{0}-24$
18	4	•	16	$\equiv^{0}0^{00}-2^{30}$ $\equiv^{1}-11^{10}$ $\equiv^{0}-12^{40}$ $=-17^{50}$ $\equiv^{0}-19^{20}$ $\equiv^{1}-24$
19	6	0.0	10	$\bullet^{0}22^{55}-24$; $\equiv^{1}0^{00}-30$ $\equiv^{0}-0^{45}$ $=-24$
20	6	1.1	pż.	$\bullet^{0}0^{00}-40$ $\overset{*}{\nabla}{}^{0}22^{55}-23^{40}$ $\overset{*}{\nabla}{}^{1}-24$; $=0^{00}-1^{30}$
21	7	5.1	2	$\overset{*}{\nabla}{}^{1}0^{00}-1^{20}$ $\overset{*}{\nabla}{}^{0}14^{50}-16^{10}$ $*^{1}-18^{40}$ $*^{0}-22^{10}$; $=3^{35}-5^{45}$ $\equiv^{0}-7^{50}$ $=-10^{10}$, $16^{30}-22^{20}$; ⊕ $7^{40}-8^{20}$
22	8	0.1	3	$\overset{*}{\nabla}{}^{0}16^{20}-17^{10}$
23	8	•	pż.	
24	6	3.7	pż.	$\bullet^{0}7^{25}-12^{20}$, $18^{35}-19^{20}$... 20^{05} $\overset{\bullet}{\nabla}{}^{0}23^{50}-24$; $=12^{20}-24$
25	6	2.5	pż.	$\overset{\bullet}{\nabla}{}^{0}0^{00}-1^{20}$ $\bullet^{0}8^{40}-9^{25}$ $\bullet^{0}9^{47}-10^{50}$ $\overset{\bullet}{\nabla}{}^{0}-19^{40}$ $\overset{\bullet}{\nabla}{}^{0}-21^{35}$; $=0^{00}-5^{50}$ $\equiv^{0}-7^{20}$ $\equiv^{1}-8^{40}$ $\equiv^{0}-9^{25}$ $=-21^{35}$
26	8	•	pż.	$\gg 0^{20}-2^{20}$
27	8	•	pż.	
28	7	0.3	pż.	$\bullet^{0}16^{55}-20^{25}$
29	6	•	pż.	$=0^{30}-5^{45}$ $\equiv^{0}-6^{30}$ $\equiv^{1}-8^{20}$ $\equiv^{0}-9^{25}$ $=-13^{30}$, $18^{20}-24$
30	6	0.2	•	$\bullet^{0}11^{52}-12^{10}$ $\overset{\bullet}{\nabla}{}^{0}-13^{15}$ $\overset{*}{\nabla}{}^{0}-13^{20}$, $\gg 8^{40}-10^{15}$, $17^{50}-18^{10}$; $=0^{00}-2^{40}$, $10^{20}-13^{20}$
31	8	0.0	•	$\overset{*}{\nabla}{}^{0}14^{20}-15^{04}$, $17^{40}-18^{10}$; $\gg 11^{25}-15^{40}$, $17^{35}-18^{05}$
Σ	-	29.2	-	

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1	8	•	•	⌴ $^{0}1-9$
2	8	•	•	
3	8	•	•	⌴ $^{0}2-8$
4	7	•	•	$=2^{20}-10^{30}$, $21^{40}-24$; ⊕ $12^{30}-24$
5	7	•	•	$=0^{00}-45$ $\equiv^{0}-7^{40}$ $\equiv^{1}-8^{40}$ $=-12^{10}$, $21^{20}-24$
6	8	•	•	$=0^{00}-30$ $=-4^{25}$ $\equiv^{0}-8^{50}$ $=-10^{40}$; ⌴ $^{0}0-8$
7	6	0.0	•	$\bullet^{0}9^{25}$... 10^{10}; $=7^{10}-15^{30}$
8	6	0.0	•	$\bullet^{0}11^{40}-12^{20}$; $=11^{10}-13^{10}$
9	8	•		
10	8	•	•	⊕ $10^{00}-16^{00}$
11	8	•	•	
12	7	•	•	
13	7	0.0	•	$\bullet^{0}15^{05}-16^{10}$
14	7	•	•	⊕ $6^{30}-10^{30}$
15	7	•	•	$=5^{30}-9^{45}$
16	7	0.9	•	$\overset{\bullet}{\nabla}{}^{0}20^{25}-21^{05}$; $=2^{30}-9^{30}$, $18^{30}-24$
17	4	2.3	•	$\bullet^{0}4^{05}-9^{10}$... 15^{40}; $=0^{00}-24$
18	6	1.1	•	$\overset{\bullet}{\nabla}{}^{0}9^{52}-16^{35}$; $=0^{00}-23^{10}$
19	6	1.1	•	$\bullet^{0}8^{40}-13^{10}$ $\overset{\bullet}{\nabla}{}^{0}19^{10-50}$; $=3^{10}-13^{20}$; ⌴ $^{0}3-7$
20	8	•	•	
21	7	8.7	•	$\overset{\bullet}{\nabla}{}^{0}10^{50}-11^{05}$ $12^{25}-16^{05}$ $16^{45}-17^{20}$, $18^{40}-23^{35}$
22	7	1.1	•	$\overset{\bullet}{\nabla}{}^{0}16^{05}-17^{20}$, $\gg 9^{40}-18^{30}$
23	6	5.8	•	$\overset{\bullet}{\nabla}{}^{0}0^{55}-1^{20}$ $3^{45}-4^{35}$, $10^{51}-11^{15}$, $11^{40}-20^{40}$, $21^{05}-22^{20}$
24	8	2.4	•	$\overset{\bullet}{\nabla}{}^{0}1^{50}-3^{10}$ $4^{40}-8^{35}$, $10^{55}-11^{20}$ $\overset{\bullet}{\nabla}{}^{1}13^{20-35}$ $\overset{\bullet}{\nabla}{}^{0}14^{15}-15^{20}$, $17^{40}-19^{25}$, $20^{45}-23^{50}$; $=5^{30}-9^{20}$
25	8	1.5	•	$\overset{\bullet}{\nabla}{}^{0}1^{55}-3^{50}$, $5^{40}-8^{20}$, $18^{45}-19^{10}$, $20^{05}-22^{15}$
26	6	3.7	•	$\bullet^{0}8^{35}-11^{40}$ $\bullet^{1}-12^{20}$ $\bullet^{0}-13^{30}$ $\overset{\bullet}{\nabla}{}^{0}-15^{05}$; $=2^{40}-16^{20}$, $19^{30}-24$
27	5	6.9	•	$\overset{\bullet}{\nabla}{}^{0}10^{35}-12^{35}$ 13^{20-45}, 14^{25-46} $\overset{\bullet}{\nabla}{}^{1}-15^{20}$ $\overset{\bullet}{\nabla}{}^{0}-16^{40}$, $17^{45}-19^{32}$, $19^{45}-20^{20}$, $\overset{\bullet}{\nabla}{}^{0}$E $14^{38}-15^{05}$, 15^{35}W; $=0^{00}-2^{20}$ $=-4^{50}$ $\equiv^{0}-6^{40}$ $=-8^{20}$, $12^{35}-14^{10}$; ⌴ $^{0}3-6$
28	8	•	•	$\overset{\bullet}{\nabla}{}^{0}5^{40}-6^{10}$
29	7	0.2	•	$\bullet^{0}7^{25}-10^{20}$ $\overset{\bullet}{\nabla}{}^{0}-11^{10}$
30	8	•	•	⌒ $^{0}1-8$
31				
Σ	-	35.7	-	

Olsztyn - Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Maj – Mai 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	98.3	98.5	100.9	99.2	4.9	10.4	2.3	5.0	11.2	1.1	81	53	68	67	1.7	5.9	2.3	3.3	1	4	0	WNW 5	NW 8	N 5
2	103.1	103.2	103.4	103.2	2.2	6.9	0.9	2.7	7.2	-0.1	86	42	83	70	1.1	5.7	1.1	2.6	2	7	0	N 5	N 6	NW 3
3	103.8	104.1	104.8	104.2	1.1	6.5	3.0	3.4	7.7	-2.5	81	40	58	60	1.2	5.8	3.2	3.4	0	4	0	N 3	NE 5	E 2
4	105.0	101.8	97.9	101.6	2.5	10.2	6.4	6.4	11.5	-4.8	68	30	45	48	2.3	8.6	5.3	5.4	0	0	3	E 2	SE 4	SE 5
5	93.8	92.0	91.6	92.5	5.1	11.0	7.6	7.8	11.8	2.6	49	39	58	49	4.5	8.0	4.3	5.6	9	10	9	SSE 7	SSE 7	E 4
6	92.0	92.6	94.8	93.1	6.4	12.8	9.4	9.5	13.6	3.9	58	43	67	56	4.1	8.5	3.8	5.5	10	9	9	E 4	ESE 3	SSW 2
7	96.5	96.7	97.4	96.9	6.6	11.6	8.0	8.6	13.4	1.5	94	58	90	81	0.5	5.7	1.0	2.4	9	9	10 •	SW 2	W 3	W 1
8	95.4	96.1	97.8	96.4	7.1	8.6	7.9	7.9	9.4	3.5	93	94	99	95	0.8	0.6	0.1	0.5	10	10 •	10 •	C 0	E 3	N 2
9	94.5	90.9	80.4	88.6	6.3	9.8	11.7	9.9	11.7	5.4	98	97	96	97	0.1	0.3	0.5	0.3	10 •	10 •	10 •	S 3	SW 2	S 3
10	75.5	78.1	81.5	78.4	6.3	5.9	7.0	6.6	11.7	5.4	92	92	91	92	0.7	0.7	0.9	0.8	10 •	10 •	6	WSW 6	SW 6	SW 3
11	88.0	92.8	98.8	93.2	4.7	13.0	7.9	8.4	15.8	3.3	100	64	80	81	0.0	5.4	2.0	2.5	10 ≡	9	5	ENE 2	N 1	NW 3
12	102.5	104.1	105.4	104.0	6.6	14.8	6.0	8.4	15.5	5.0	97	60	86	81	0.3	6.7	1.3	2.8	10 •	4	7	NW 4	NW 7	NNW 3
13	105.2	103.8	102.3	103.8	7.7	16.2	9.9	10.9	16.8	0.8	77	44	82	68	2.4	10.2	2.2	4.9	6	6	5	C 0	NW 5	NNW 1
14	98.8	97.3	97.3	97.8	10.2	15.2	8.2	10.4	16.6	2.3	88	50	94	77	1.4	8.7	0.6	3.6	1	7	4	WNW 1	WNW 2	NW 3
15	97.4	97.2	96.5	97.0	4.4	11.2	6.9	7.4	11.8	3.9	97	40	67	68	0.3	7.9	3.3	3.8	10	2	2	N 5	NNE 6	NNE 2
16	96.1	95.9	92.3	94.8	7.3	9.6	9.4	8.9	10.7	4.4	57	47	69	58	4.4	6.4	3.7	4.8	10	10	10	E 3	E 3	E 3
17	89.5	89.2	87.2	88.6	9.0	16.6	15.0	13.9	17.6	6.8	86	67	83	79	1.6	6.3	2.9	3.6	10 • ≡	7	4	SW 2	WSW 5	S 2
18	82.4	86.6	89.1	86.0	15.1	18.3	11.1	13.9	19.2	11.1	91	58	89	79	1.5	8.8	1.5	3.9	9	9	6	SW 4	WSW 10	N 1
19	84.3	86.0	91.2	87.2	14.0	11.0	3.6	8.0	14.5	2.9	91	85	97	91	1.5	1.9	0.3	1.2	8	10	9	SSW 2	N 6	W 1
20	96.7	99.2	102.1	99.3	5.7	10.4	4.4	6.2	10.6	2.3	89	44	93	75	1.0	7.0	0.6	2.9	8	5	2	W 3	W 5	SW 2
21	106.5	109.0	110.3	108.8	6.4	8.6	4.4	6.0	11.6	2.5	82	78	97	86	1.7	2.4	0.3	1.5	0	8	1	W 5	SSW 4	C 0
22	112.7	112.2	111.9	112.3	8.0	12.0	8.2	9.1	13.9	0.7	67	48	62	59	3.5	7.2	4.2	5.0	0	4	0	W 3	N 2	NE 3
23	112.0	110.1	108.4	110.2	9.2	14.6	11.2	11.6	15.6	2.4	65	37	47	50	4.1	10.5	7.1	7.2	0	0	1	NE 5	E 10	E 5
24	106.5	104.2	101.7	104.1	9.8	13.4	8.4	10.0	13.8	6.8	61	58	99	73	4.8	6.5	0.1	3.8	9	9	10 •	E 6	E 8	E 6
25	100.0	100.7	101.5	100.7	8.8	10.1	9.8	9.6	10.4	7.9	100	93	95	96	0.0	0.8	0.6	0.5	10 •	10 •	10	E 3	ENE 3	NE 3
26	100.7	100.0	98.9	99.9	9.4	12.4	10.2	10.6	13.1	8.5	92	74	95	87	1.0	3.7	0.6	1.8	10	10	10	NE 3	NE 3	C 0
27	95.9	96.2	97.1	96.4	9.9	12.3	10.5	10.8	13.2	8.8	99	87	94	93	0.2	1.9	0.8	1.0	10	10	6	C 0	NW 1	N 1
28	97.6	97.3	95.8	96.9	8.8	15.7	12.8	12.5	16.1	3.8	100	68	80	83	0.0	5.7	2.9	2.9	6	7	7	NNE 1	E 1	NE 1
29	92.3	91.1	91.3	91.6	12.8	15.9	8.2	11.3	16.7	7.8	79	55	79	71	3.1	8.2	2.3	4.5	5	10	5	N 3	NE 7	N 5
30	90.7	91.1	93.2	91.7	8.0	12.9	5.4	7.9	13.6	3.8	80	38	84	67	2.1	9.3	1.4	4.3	6	5	1	NW 5	NW 6	NW 1
31	95.8	96.6	97.5	96.6	5.5	15.0	11.9	11.1	16.2	-0.3	98	34	59	64	0.1	11.2	5.7	5.7	6	2	1	C 0	E 2	E 2
M	97.1	97.2	97.4	97.2	7.4	12.0	8.0	8.8	13.3	3.6	84	59	80	74	1.7	6.0	2.2	3.3	6.6	7.0	5.3	3.2	4.6	2.5

Czerwiec – Juin

1	94.1	91.6	90.8	92.2	10.3	11.1	12.6	11.6	13.5	5.8	73	96	99	89	3.3	0.5	0.2	1.3	10 •	10	4	ENE 5	ENE 6	E 1
2	90.8	91.5	96.0	92.8	11.2	11.9	9.0	10.3	12.8	9.0	86	87	97	90	1.8	1.8	0.3	1.3	7	10 •	10 •	S 2	SW 3	WNW 5
3	99.3	100.3	101.8	100.5	10.8	16.2	11.4	12.4	16.9	7.4	85	56	93	78	2.0	8.1	1.0	3.7	1	7	6	W 5	NW 4	C 0
4	103.5	103.7	103.1	103.4	9.3	16.9	12.2	12.6	17.7	4.9	91	57	61	70	1.1	8.2	5.6	5.0	7	2	3	N 1	N 3	NE 2
5	101.3	98.5	96.8	98.9	13.2	19.9	13.8	15.2	20.6	7.1	60	41	64	55	6.1	13.7	5.7	8.5	7	4	1	ENE 3	E 4	NE 2
6	94.2	92.2	93.3	93.2	14.2	18.5	13.2	14.8	19.7	9.6	72	46	66	61	4.6	11.4	5.1	7.0	1	4	2	NE 3	NE 6	NE 3
7	95.1	95.1	95.2	93.8	11.6	14.8	8.3	10.8	15.8	7.9	81	56	79	72	2.6	7.4	2.3	4.1	9	6	0	N 5	N 8	NNW 1
8	98.8	98.6	97.6	98.3	12.0	19.6	14.4	15.1	20.7	2.8	70	45	73	63	4.1	12.5	4.4	7.0	2	2	0	E 2	E 2	NE 2
9	96.3	96.0	95.9	96.1	15.2	17.1	16.7	16.4	18.7	11.5	86	72	66	75	2.5	5.4	6.4	4.8	10	9	8	ESE 5	E 5	E 5
10	95.3	95.5	95.2	95.3	16.8	21.0	17.4	18.2	23.1	12.6	64	41	63	56	6.8	14.7	7.3	9.6	1	6	8 •	E 5	ESE 7	E 6
11	93.1	93.0	93.2	93.1	15.8	18.9	14.3	15.8	19.6	14.3	74	61	76	70	4.6	8.4	3.9	5.6	10	10 •	10	NE 3	NE 4	NE 3
12	93.3	93.9	95.0	94.1	15.1	16.0	13.2	14.4	20.6	12.1	87	86	87	87	2.3	2.5	2.0	2.3	7	9 •	9	N 3	N 2	NW 7
13	94.3	95.0	95.4	94.9	11.6	13.6	11.2	11.9	14.0	10.1	99	90	97	95	0.1	1.6	0.3	0.7	10	10 •	10 •	W 5	NW 5	NW 4
14	96.0	97.5	99.7	97.7	11.0	19.2	11.6	13.4	19.2	10.1	99	52	81	77	0.1	10.5	2.6	4.4	9	1	1	NW 4	N 7	NNW 3
15	101.2	101.2	100.5	101.0	12.0	19.2	15.2	15.4	20.8	6.0	83	42	63	63	2.3	12.9	6.3	7.2	0	3	0	NNW 2	W 2	C 0
16	99.9	98.1	94.4	97.5	16.4	23.1	18.4	19.1	23.7	6.2	64	36	52	51	6.7	18.2	10.2	11.7	3	2	3	N 1	S 1	S 1
17	89.8	87.6	88.3	88.6	17.9	26.3	20.8	21.4	26.5	13.6	70	32	54	52	6.1	23.2	11.4	13.6	0	1	2	S 1	S 7	SW 2
18	93.0	96.4	95.0	94.8	13.0	14.2	15.6	14.6	20.8	12.5	81	84	67	77	2.8	2.5	5.9	3.7	9	9	10 •	SW 5	SW 3	S 1
19	89.2	91.6	94.5	91.8	15.4	13.3	12.9	13.6	19.1	11.7	95	99	96	97	1.0	0.2	0.6	0.6	10 •	7	9 •	SW 5	NW 7	WSW 6
20	97.5	99.3	100.4	99.1	13.2	17.2	14.8	15.0	19.2	12.0	79	50	64	64	3.2	9.7	6.0	6.3	10	7	2	W 6	W 8	W 4
21	101.9	102.6	101.0	101.8	14.9	18.6	15.3	16.0	20.6	10.7	76	54	83	71	4.0	9.8	3.0	5.6	1	9	1	W 2	W 5	C 0
22	98.2	95.0	92.2	95.1	17.2	25.8	19.4	20.4	26.3	9.0	69	44	93	69	6.0	18.6	1.5	8.7	0	8	10 • ☂	W 2	SSW 4	W 1
23	90.8	92.9	96.9	93.5	17.7	22.0	16.6	18.2	22.7	16.5	96	65	81	81	0.8	9.2	3.7	4.6	10 •	5	3	SW 2	WSW 4	W 1
24	98.9	99.5	99.9	99.4	16.2	22.4	16.6	18.0	23.0	12.4	90	55	92	79	1.7	12.2	1.6	5.2	5	6	10 •	SW 1	W 7	W 2
25	101.7	101.6	102.2	101.8	15.1	22.9	18.2	18.6	24.0	11.8	96	51	81	76	0.8	13.6	4.1	6.2	8	4	1	C 0	SW 5	N 1
26	101.6	100.0	99.6	100.4	19.9	27.9	22.2	23.0	29.1	13.9	66	41	67	58	7.9	22.0	8.9	12.9	0	0	4	S 1	S 4	W 5
27	104.4	104.0	102.8	103.7	15.6	20.2	15.7	16.8	22.2	13.9	73	51	86	70	4.8	11.5	2.4	6.2	1	9	9	WNW 2	NW 4	C 0
28	104.6	104.9	104.5	104.7	14.4	17.6	11.9	14.0	17.8	11.6	78	51	73	67	3.6	9.8	3.8	5.7	4	9	2	W 5	NW 7	W 2
29	98.5	99.5	102.0	100.0	11.6	15.7	13.0	13.3	18.8	10.1	98	75	78	84	0.3	4.4	3.3	2.7	10 •	9	6	WSW 4	W 7	W 3
30	101.6	100.6	95.7	99.3	12.6	19.3	17.0	16.3	21.7	8.8	86	57	66	70	2.1	9.7	6.5	6.1	1	2	2	W 3	W 5	WSW 1
31																								
M	97.2	97.2	97.3	97.2	14.0	18.7	14.8	15.6	20.3	10.2	81	59	77	72	3.2	9.8	4.2	5.7	5.4	6.0	4.9	3.1	4.9	2.5

Olsztyn - Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$ Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	-	⌴ 0 2 – 8
2	8	.	.	⌴ 0 23 – 24
3	8	.	.	⌴ 0 00 – 2 ⌴ 1 – 7 ⌴ 0 23 – 24
4	8	.	.	⌴ 0 00 – 1 ⌴ 1 – 6
5	8	.	.	≫ 10^05 – 11^15; ⊕ 7^30 – 9^40, 12^30 – 13^10
6	8	.	.	⊕ 5^40 – 11^30
7	8	0.1	.	● 0 19^25 – 21^35; = 22^30 – 24
8	6	4.7	.	● 0 7^20 – 14^20; 15^20, 17^10 – 25 ▽ 0 20^25 – 21^40; = 0^00 – 24
9	5	5.9	.	● 0 5^35 – 13^40, 14^20 – 20^45, 22^45; = 0^00 – 3^45 ≡ 0 – 5^50 = – 24
10	7	0.7	.	● 0 5^15 – 7^20 ▽ 0 8^05 – 9^35, 10^22 – 13^40, 17^52 – 18^25; = 1^00 – 4^40
11	8	0.4	.	≡ 0 2^40 – 4^30 ≡ 1 – 5^10 ≡ 2 – 7^45 = – 8^50, 23^40 – 24; ⌒ 0 22 – 24
12	7	0.1	.	● 0 5^36 – 6^20 ● 0 7^40; = 0^00 – 4^50 ≡ 0 – 5^45 = – 10^30; ⌒ 0 0^00 – 1 ⌒ 1 – 5^36
13	8	.	.	⌴ 0 2 – 5
14	8	.	.	= 2^30 – 8^50, 23 – 24; ⌒ 1 1 – 8 ⌒ 0 21 – 24
15	8	.	.	= 0^00 – 1^45 ≡ 0 – 4^50 = – 7^10; ⌒ 0 0^00 – 1 ⌒ 1 – 9
16	8	7.7	.	● 0 6^15 – 8^40, 21^10 – 20 ● 1 – 21^50 ● 0 – 22^40
17	6	2.8	.	● 1 2^10 – 3^20 ● 0 6^30 – 7^20 ● 0 10^20 – 35, 14^02 – 25; ≡ 0 6^32 – 7^45 = – 13^40, 14^30 – 17^40, 19^30 – 24
18	7	.	.	● 0 0^45 – 55 ● 1 – 2^20 ● 0 5^20 – 35; R 7^0 SW 0^40 0^50 – 1^35 NE; ≫ 11^30 – 15^20; = 2^00 – 7^20, 20^25 – 24
19	6	9.7	.	● 0 7^32 – 9^40 14^12 – 17^40 ● 1 – 18^30 ● 0 – 19^25; = 0^00 – 12^20, ⌒ 0 0^00 – 7^32
20	8	1.2	.	● 0 10^40 – 11^05, 12^02 – 10, 14^20 – 40, 16^50 – 17^05; ≫ 14^20 – 30
21	8	2.8	.	● 0 9^45 – 10^15, 10^47 – 11^07, 11^26 – 12^05, 16^45 – 50 ● 0 ▲ – 17^01 ● 0 – 17^04; = 20^00 – 23^40
22	8	.	.	⌴ 0 1 – 5
23	8	.	.	≫ 9^40 – 15^30; ⌒ 0 2 – 7
24	8	2.7	.	● 0 13^26 – 14^05, 15^05 – 20^10 – 24
25	5	0.2	.	● 0 0^00 – 1^10 ● 0 3^10 – 8^40, 11^50 – 12^30 ● 0 – 13^40, 14^40 – 15^10; = 2^30 – 24
26	7	6.0	.	● 0 21^40 – 24; = 0^00 – 8^30, 19^30 – 24
27	7	0.4	.	● 0 0^00 – 9^25 ▽ 0 9^40 – 11^35, 16^42 – 17^10; = 0^00 – 3^40 ≡ 0 – 4^50 = – 12^20, 21^30 – 22^20 = – 24
28	8	.	.	= 0^00 – 2^50 ≡ 0 – 5^40 = – 8^50
29	7	.	.	⌒ 0 1 – 8; ⊕ 16^30 – 18^40
30	8	.	.	⌒ 0 1 – 7
31	8	0.1	.	≡ 0 0^50 – 5^50 = – 6^40; ⌴ 0 0 – 6
Σ	-	45.5	-	

Czerwiec - Juin

1	6	9.4	.	● 0 5^55, 7^05 – 40 ● 1 – 9^20 ● 0 – 12^20 ▽ 0 16^02 – 40; ≫ 9^40 – 11^35; = 9^30 – 21^50 ≡ 0 – 22^20 = – 24
2	7	1.9	.	● 0 0^26 – 40, 12^35, 14^05, 14^20 – 15^10 ● 0 16^10, 18^20 – 24; = 0^00 – 3^30, 13^40 – 24
3	8	0.0	.	● 0 0^00 – 50 ● 0 15^55 – 16^10; = 0^00 – 6^45, 20^40 – 22^45; ⌒ 0 21 – 24
4	8	.	.	= 2^30 – 5^30; ⌒ 0 0^00 – 1 ⌒ 1 – 8
5	8	.	.	⌒ 0 1 – 3 ⌒ 1 – 8
6	8	0.0	.	● 0 17^55 – 18^01
7	8	.	.	⌒ 0 22 – 23 ⌒ 1 – 24
8	8	.	.	= 1^40 – 6^20; ⌒ 1 0^00 – 8
9	7	.	.	= 3^30 – 7^20; ⌒ 0 0^00 – 8
10	8	0.0	.	● 0 20^45 – 55
11	7	0.5	.	● 0 9^48 – 11^20 12^25 – 18^20
12	7	1.2	.	● 0 0^48 – 3^40 ▽ 0 11^50 – 12^10 12^35 – 45; = 3^40 – 4^50
13	6	8.0	.	● 0 1^55 – 4^40 5^40 – 6^35, 9^50 – 16^10 17^16 – 19^45 ● 1 – 20^05 ● 0 – 24; = 6^35 – 24
14	8	.	.	● 0 0^00 – 1^10 ● 1 – 12^5; = 0^00 – 7^20; ⌒ 0 22 – 24
15	8	.	.	⌒ 0 0^00 – 3 ⌒ 1 – 7 ⌒ 0 21 – 24
16	8	.	.	= 2^40 – 5^20; ⌒ 0 0^00 – 1 ⌒ 1 – 8
17	8	0.4	.	
18	8	1.7	.	● 0 0^50 – 1^20 3^54 – 4^05 ● 0 19^51 – 24; ⊕ 16^20 – 18^10
19	7	10.5	.	● 0 0^00 – 2^10 – 7^30 ▽ 0 8^15 – 55 11^46 – 12^02 ● 1 – 12^15 ● 0 – 12^35 13^10 – 25 17^35 – 18^45 ● 1 – 19^05 ● 0 – 19^20 19^50 – 20^45; R 0 W 11^46 – 11^50 – 12^30 E
20	8	.	.	
21	8	.	.	⌒ 0 1 – 8, 22 – 24
22	7	36.4	.	● 0 19^50 – 21^30 ● 1 22^10 – 24; R 1 SW 19^46 – 22^10 – 24 NE; ⌒ 0 0^00 – 1 ⌒ 1 – 8
23	8	2.0	.	● 0 0^00 – 1^20 ● 0 – 2^20 3^45 – 4^15 5^05 – 8^25 11^32 – 40; R 0 NE 0^00 1^45 NE; R 0 S 11^35 – 11^46 – 12^10 N; ⌒ 0 21 – 24
24	7	1.8	.	● 0 20^20 – 21^15; = 2^40 – 7^45 20^20 – 22^40 = – 23^50 ≡ 0 – 24; ⌒ 0 0^00 – 1 ⌒ 1 – 10
25	7	.	.	≡ 0 0^02 – 1^20 ≡ 1 – 2^10 ≡ E – 3^30 ≡ 1 – 4^35 = – 8^40; ⌒ 0 21 – 24
26	8	0.2	.	● 0 17^24 – 32; R 0 SW 16^45 – 17^40 E; ⌒ 0 0^00 – 2 ⌒ 1 – 7 ⌒ 0 – 8
27	8	0.0	.	● 0 16^55 – 17^05; ⌒ 0 21 – 24
28	8	3.9	.	⌒ 0 0^00 – 10
29	8	0.3	.	● 0 4^50 – 5^10 ● 1 – 5^40 ● 0 – 7^25, 8^45 – 9^42; = 4^00 – 10^10
30	8	3.7	.	⌒ 0 1 – 7, 22 – 24
31				
Σ	-	81.9	-	

Olsztyn-Dajtki — φ = 53°46' — λ = 20°25' — Lipiec – Juillet 1965

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	91.2	93.4	95.8	93.5	13.1	16.3	11.0	12.8	17.0	9.0	95	57	86	79	0.7	7.9	1.8	3.5	10 •	7	1	WNW 2	WNW 6	NW 1
2	95.4	93.3	90.8	93.2	11.2	17.2	13.9	14.0	17.6	6.7	95	50	61	69	0.7	9.7	6.2	5.5	1	6	9	SW 2	WSW 4	SW 2
3	88.8	89.8	90.5	89.7	12.4	14.4	11.0	12.2	16.3	10.3	78	62	80	73	3.2	6.3	2.6	4.0	9	9 •	4	SW 4	SW 5	W 2
4	91.5	91.1	91.5	91.4	10.9	16.0	11.7	12.6	17.9	8.2	87	45	74	69	1.6	10.0	3.6	5.1	4	7	1	WSW 5	SW 2	SW 1
5	91.9	91.7	92.4	92.0	11.6	13.8	9.8	11.2	17.0	6.2	90	72	84	82	1.3	4.4	1.9	2.5	4	9	2	W 1	WNW 1	WNW 1
6	93.0	92.2	92.9	92.7	10.4	13.9	9.9	10.5	15.6	6.8	82	84	91	86	2.2	2.1	1.1	1.8	6	9	4	SW 2	SW 5	WSW 2
7	94.2	94.7	91.8	93.6	11.6	11.4	12.9	12.2	16.7	8.8	81	98	95	91	2.6	0.4	0.7	1.2	4	10 •	4	WSW 4	W 2	S 2
8	91.1	88.6	82.3	87.3	13.6	19.7	14.8	15.7	21.8	10.4	93	66	99	86	1.1	7.7	0.2	3.0	2	10 •	10 •	SW 2	S 1	W 1
9	85.7	88.4	90.7	88.3	11.0	14.2	11.9	12.2	15.7	10.6	85	63	83	77	1.9	6.0	2.3	3.4	8	7	6	SW 3	SW 6	SW 3
10	94.4	96.7	98.6	96.6	11.1	15.0	9.8	11.4	16.9	9.0	86	60	96	81	1.8	6.7	0.5	3.0	6	8	1	WSW 6	SW 5	SW 1
11	100.6	101.8	102.3	101.6	11.7	13.5	12.4	12.5	17.4	7.4	91	78	93	87	1.1	3.4	1.0	1.8	2	9	3	SW 1	WNW 2	N 1
12	99.9	96.4	92.9	96.4	14.6	17.0	16.6	16.2	21.5	7.4	72	86	99	86	4.6	2.8	0.2	2.5	4	10 •	10	S 2	S 3	SW 3
13	97.1	97.8	98.1	97.7	14.3	20.0	17.8	17.5	22.2	11.9	92	62	85	80	1.3	9.0	3.0	1.4	3	3	6	W 4	W 2	SW 1
14	99.2	99.9	100.7	99.9	20.4	28.1	23.4	23.8	29.0	14.9	83	49	66	66	4.0	19.5	9.7	11.1	3	5	4	SW 2	SW 5	S 1
15	100.7	101.5	101.5	101.2	21.4	28.7	20.0	22.5	29.3	18.9	76	51	88	72	6.1	19.5	2.9	9.5	3	7	6	SSE 1	W. 2	E 1
16	100.4	100.4	100.1	100.3	18.9	20.8	19.3	19.6	22.9	15.2	90	81	92	88	2.1	4.7	1.8	2.9	8 ⊼	8	10	NW 1	N 6	N 2
17	100.1	100.0	100.6	100.2	16.6	17.0	14.8	15.8	19.4	14.8	97	95	84	92	0.6	1.0	2.7	1.4	10 •	10	10	NE 2	NE 3	N 5
18	100.7	101.4	103.3	101.8	14.4	19.2	14.4	15.6	19.9	12.6	78	56	80	71	3.6	9.8	3.2	5.5	7	7	1	NE 5	NE 6	NE 1
19	105.7	106.1	105.7	105.8	15.5	22.0	17.0	17.9	22.5	9.1	75	46	72	64	4.4	14.3	5.4	8.0	0	4	1	NE 1	NE 1	NE 1
20	106.5	104.8	102.4	104.6	17.1	23.4	18.6	19.4	24.5	9.0	72	42	64	59	5.4	16.7	7.8	10.0	0	3	0	C 0	E 1	SE 1
21	100.3	97.6	93.7	97.2	17.4	22.6	19.4	19.7	24.4	11.6	72	46	74	64	5.7	14.7	5.8	8.7	9	7	4	E 1	SE 3	E 3
22	91.9	93.0	93.7	92.9	17.6	19.4	16.5	17.5	20.4	16.3	95	88	96	93	1.0	2.8	0.8	1.5	10	10 •	9 •	S 1	SW 1	NE 1
23	92.9	91.3	90.4	91.5	14.4	23.4	16.0	17.4	23.9	12.8	100	60	99	86	0.0	11.4	0.2	3.9	10 ≡	10	7	NE 1	ENE 2	SW 1
24	90.9	89.2	93.2	91.1	15.2	21.9	13.1	15.8	22.8	11.8	94	61	92	82	1.0	10.2	1.3	4.2	8	7	2	SW 1	S 6	WSW 2
25	94.4	94.3	93.0	93.9	14.7	20.8	16.2	17.0	21.8	10.6	93	47	70	70	1.1	13.1	5.4	6.5	1	6	1	WSW 2	SW 7	SW 1
26	92.0	92.3	90.4	91.6	14.7	18.1	12.6	14.5	20.2	11.0	81	60	93	78	3.1	8.3	1.1	4.2	1	6	4	SW 5	W 5	SW 2
27	89.1	91.2	92.3	90.9	12.6	12.8	11.4	12.0	14.7	11.3	89	86	88	88	1.6	2.1	1.7	1.8	10	9 •	3	WSW 6	W 5	SW 1
28	91.4	92.0	91.8	91.7	11.1	15.3	12.8	13.0	16.8	10.5	94	69	86	83	0.8	5.5	2.1	2.8	9	7	9	W 5	WSW 6	W 6
29	89.1	88.0	83.7	86.9	13.0	16.6	14.5	14.6	17.3	11.4	93	83	93	90	1.1	3.3	1.1	1.8	10	10	10 •	SW 3	SW 4	SW 3
30	79.5	78.6	79.7	79.3	15.1	15.8	13.9	14.7	19.0	11.7	88	73	84	82	2.1	4.8	2.5	3.1	10	10 • ⊼	6	SW 4	W 6	S 2
31	83.6	83.7	85.2	84.2	12.9	18.5	12.6	14.2	19.2	12.1	81	53	98	77	2.8	10.0	0.4	4.4	4	4	8	SW 5	SW 6	W 2
M	94.3	94.2	93.9	94.1	14.2	18.2	14.5	15.4	20.1	10.9	86	65	85	79	2.3	8.0	2.6	4.3	5.7	7.5	5.0	2.7	3.8	1.8

Sierpień – Août

1	90.9	92.6	94.3	92.6	11.2	16.9	11.8	12.9	18.1	8.0	85	53	76	71	2.0	8.9	3.3	4.7	2	4	1	W 3	W 6	SW 2
2	93.1	91.8	90.9	91.9	9.6	16.6	12.1	12.6	17.0	5.0	97	59	84	80	0.4	7.9	2.2	3.5	10	10	9	C 0	C 0	WNW 3
3	90.9	91.2	92.8	91.6	11.4	17.3	11.4	12.9	19.4	7.8	88	57	88	78	1.7	8.5	1.7	4.0	2	8	8	W 2	W 5	SW 1
4	93.7	94.3	96.9	95.0	13.6	15.9	13.8	14.3	18.7	9.7	91	88	93	91	1.5	2.1	1.1	1.6	8	9	10 •	C 0	WSW 5	W 3
5	100.3	101.7	102.1	101.4	12.0	17.0	13.2	13.8	18.4	10.3	94	61	93	83	0.8	7.6	1.1	3.2	4	9	1	W 4	W 5	NW 1
6	101.6	98.7	95.6	98.6	16.1	25.5	20.5	20.6	26.7	11.0	73	50	80	68	4.9	16.2	4.8	8.6	3	5	3	S 1	S 6	S 1
7	96.3	95.2	95.2	95.6	18.1	25.3	20.3	21.0	25.7	16.8	98	61	82	80	0.5	12.6	4.4	5.8	9	9	10	C 0	WSW 6	W 4
8	99.0	99.8	98.2	99.0	15.6	16.3	13.6	14.8	20.3	13.3	94	90	99	94	1.1	1.9	0.2	1.1	9	10	6	W 1	W 2	E 1
9	98.6	101.2	102.3	100.7	14.0	13.8	12.9	13.4	15.3	11.8	97	97	95	96	0.6	0.5	0.7	0.6	10	10 •	9	W 1	W 3	NW 2
10	103.9	104.3	104.8	104.3	11.7	16.6	11.8	13.0	17.7	8.0	85	62	85	77	2.0	7.1	2.0	3.7	2	8	2	W 3	NW 4	NW 1
11	104.6	104.3	104.3	104.4	11.4	17.0	11.8	13.0	18.2	8.0	93	62	96	84	1.0	7.4	0.5	3.0	10	7	3	C 0	NW 3	NW 3
12	104.2	104.2	103.6	104.0	11.6	14.9	9.8	11.5	17.6	8.8	100	65	93	86	0.0	5.9	0.8	2.2	10 ≡	8	1	WNW 3	W 2	NW 3
13	102.7	101.9	102.1	102.2	11.2	13.6	10.6	11.5	14.5	7.4	91	77	95	88	1.2	3.5	0.7	1.8	9	9	9	NW 4	NW 9	NW 4
14	100.6	100.6	101.5	100.9	10.9	13.5	11.0	11.6	15.0	8.2	99	88	96	94	0.1	1.8	0.5	0.8	10 •	8	9	W 5	NW 4	NW 3
15	102.5	103.1	104.0	103.2	11.0	16.1	10.2	11.9	16.6	6.8	100	63	93	85	0.0	6.9	0.8	2.6	9	7	0	NW 2	NW 1	NW 3
16	104.3	103.5	102.3	105.4	8.6	16.2	9.6	11.0	16.7	5.5	100	63	95	86	0.0	6.8	0.7	2.5	0 ≡	7	2	C 0	W 2	NW 1
17	101.6	101.6	101.4	101.5	10.4	19.1	12.9	13.8	20.0	5.1	99	60	89	83	0.2	8.9	1.6	3.6	1	3	0	C 0	NW 4	C 0
18	102.9	103.5	103.6	103.3	10.2	20.5	13.3	14.3	21.7	7.8	100	53	87	80	0.0	11.4	2.0	4.5	10 ≡	3	1	C 0	W 2	C 0
19	104.9	105.8	106.0	105.6	13.8	23.2	14.5	16.5	23.6	10.4	85	49	90	75	2.3	14.6	1.6	6.2	1	3	1	C 0	N 1	C 0
20	105.3	104.5	102.7	104.2	14.4	24.5	18.4	18.9	25.3	10.9	92	56	68	72	1.3	13.5	6.8	7.2	3	7	2	C 0	C 0	S 1
21	99.8	97.1	95.1	97.3	15.8	26.1	19.6	20.3	26.9	11.6	77	46	68	64	4.1	18.1	7.3	9.8	1	3	3	SE 2	SSW 4	S 1
22	94.4	93.5	92.4	93.4	18.0	27.7	19.9	21.4	28.4	13.8	79	36	65	60	4.2	23.5	8.1	11.9	3	2	2	S 2	S 4	E 1
23	92.5	92.0	92.8	92.3	17.2	27.8	21.4	22.0	28.0	15.2	78	36	65	60	4.3	24.0	9.0	12.4	0	0	9	SE 2	SE 5	SE 6
24	92.4	93.3	91.9	92.5	18.0	26.0	21.4	21.7	27.0	17.2	82	59	73	71	3.6	13.9	6.9	8.1	9	7	9	S 2	E 1	E 1
25	89.2	88.3	90.7	89.4	17.8	24.7	18.3	19.8	25.8	17.7	87	63	99	83	2.6	11.5	0.2	4.8	10	8	10 •	E 1	S 3	WNW 3
26	93.3	95.7	97.4	95.5	13.4	12.8	10.9	12.0	18.3	10.3	99	98	99	99	0.2	0.4	0.1	0.2	10 •	10 •	9	W 4	NW 3	C 0
27	93.2	90.5	91.9	91.9	9.8	10.6	10.6	10.4	11.4	9.0	99	97	97	98	0.1	0.4	0.4	0.3	10 •	10 •	10 •	NW 3	W 6	W 6
28	95.7	96.1	97.9	95.9	11.2	13.4	12.0	12.6	16.2	9.8	97	69	93	86	0.3	3.3	1.0	2.3	8	9	9	W 6	W 3	WSW 3
29	97.0	97.0	95.0	96.3	11.8	17.2	12.7	13.6	18.4	11.2	93	57	88	80	0.6	8.3	1.8	3.6	10	6	4	SW 4	W 2	C 0
30	95.5	96.5	98.3	96.8	11.3	16.2	10.2	12.0	17.8	9.8	84	66	92	81	2.2	6.3	0.9	3.1	10	6	2	W 2	W 3	C 0
31	98.0	97.6	97.2	97.6	8.6	16.4	10.8	11.6	18.1	4.1	99	61	89	83	0.2	7.2	1.5	3.0	0	4	0	W 1	WNW 2	NNW 1
M	98.1	98.1	98.2	98.1	12.9	13.7	13.9	14.8	20.1	10.0	92	65	87	81	1.4	8.9	2.4	4.2	6.2	6.7	5.0	1.9	3.3	1.9

Ulsztyn - Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$ Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚCIE GU h	POGODA
1	8	0.5	.	●°▽ 4^45 6^02 ●¹▽ 6^20 ●°▽ 7^25, 10^05 11^15, ⌒° 0^00 4^45, 21–24
2	8	.	.	⌒° 0^00 1 ⌒¹ 9
3	8	0.4	.	●°▽ 9^35 12^40, 21^10 22^20
4	8	0.0	.	●°▽ 15^50 16^05; ⌒° 23–24
5	8	0.3	.	●°▽ 11^26–55; ⌒° 0^00 3 ⌒¹ 8 ⌒° 21–24
6	8	1.5	.	●°▽ 11^45 12^05, 13^05–30, 13^40 14^05 16^10–45; ⌒° 0^00 8
7	6	2.1	.	●°▽ 11^45 13^35, 16^35 17^05, 19^10–25, 22^40–50, K°SW 18^50 18^55 NE 19^20; = 20^30 24; ⌒¹ 1–9
8	7	12.8	.	●°▽ 12^28–45, 13^45 14^20, 17^25 18^05 ●¹▽ 19^01 ●²▽ 19^36 ●°▽ 24, K°S 18^15 18^45 19^40 N, = 0^00 9^30
9	8	0.0	.	●°▽ 0^00 1^25, 13^54 14^02; = 2^45 4^50
10	8	.	.	⌒° 1–9, 22–24
11	8	0.0	.	●°▽ 12^07–15; = 22^10 24; ⌒° 0^00 8, 21–24
12	7	10.2	.	●°▽ 12^28–45, 16^15–25, 17^10 18^45 ●¹▽ 19^25 ●°▽ 20^20 ●¹▽ 21^15–35, = 0^00 1^10 = 1^40 3^20, 20^20 22^30, ⌒° 0^00 8
13	8	.	.	= 4^30 6^20
14	7	.	.	= 1^30 5^30; ⌒° 2–8, 21–24
15	7	0.0	.	K°SE 15^20 15^40 17^20 W; ⌒° 0^00 8; 23–24
16	7	13.5	.	●°▽ 5^40–45, 6^45 7^12 ●²▽ 7^26 ●°▽ 7^40 ●¹▽ 7^45 ●°▽ 8^16 12^20–30, K°S 6^05 6^45 8^25 W, = 1^30 3^20 = 4^30 = 12^20, 17^40 24; ⌒° 0^00 6^40
17	6	8.4	.	●°▽ 5^54 8^22, 8^40–50 ●²▽ 9^15 ●°▽ 10^20, K°NE 6^52 8^20 9^35 NW, = 0^00 18^30
18	8	.	.	⌒° 23–24
19	8	.	.	⌒° 0^00 1 ⌒¹ 9 ⌒° 23–24
20	8	.	.	= 2^30 4^30; ⌒° 0^00 2 ⌒¹ 9 ⌒° 21–24
21	8	0.4	.	●°▽ 22^45 23^02; ⌒° 0^00 9
22	6	8.9	.	●°▽ 14^37 3^35 11^35 13^05 ●¹▽ 14^50 16^10 ●°▽ 16^40 17^10, 20^33–40 ●¹▽ 20^50 ●°▽ 21^15, K°SW 15^05 15^10 16^10 NE K°SW 20^50 21^00 21^10 E; = 3^35 18^20, 20^30 22^50 = 24
23	7	6.2	.	●°▽ 16^32–40 ●¹▽ 17^05 ●°▽ 18^25, K¹S 16^40 17^00 17^40 N; = 0^00 2^50 = °5^30 = ¹7^40 = °8^35 = 11^20, 18^25 24; ⊕ 9^30 15^20
24	8	0.6	.	●°▽ 8^45 9^15, 16^25–35, 23^45 24; = 0^00 4^20
25	8	.	.	●°▽ 0^00–15
26	8	1.3	.	●°▽ 19^40–55; ⌒° 2–7
27	8	1.0	.	●°▽ 12^05–40
28	8	1.1	.	●°▽ 15^4 2^10, 16^07–25, 10^05–10 11^20–30, 14^06–10, 15^45–55, 20^45 21^05
29	6	3.3	.	●°▽ 7^05 8^20 ●°▽ 15^25 16^35 ●²▽ 19^55 20^05 ●°▽ 21^45, 23^40 24, = 9^30 22^30
30	6	9.2	.	●°▽ 0^00–10 ●¹▽ 9^40 10^10, 11^05–15 ●°▽ 12^20–30 ●¹▽ 13^10 ●²▽ 13^50–54 ●²▲ 13^59 ●²▽ 14^05 ●¹▽ 14^20, K°NW 9^30 9^35 10^20 NE K¹SW 12^30 12^35 14^40 NE
31	8	3.6	.	●°▽ 15^35 18^10; = 17^30 24
Σ	-	85.3	-	

Sierpień - Août

1	8	0.0	.	●°▽ 8^32–36 8^40–55 = 0^00 3^10, ⌒° 20–24
2	8	.	.	= 3^30 4^30 = °6^30, ⌒° 0^00 3 ⌒¹ 9
3	8	4.4	.	●°▽ 13^54–58, 18^05–15 ●¹▽ 18^46–55 ●°▽ 19^55, K°SW 19^03–10–20 NE; ⌒° 0–4 ⌒¹ 8
4	7	0.3	.	●°▽ 12^05–25, 19^48 21^05
5	8	.	.	⌒° 20–24
6	8	5.2	.	⌒° 1–3 ⌒¹ 8 ⌒° 22–24
7	7	1.8	.	●°▽ 3^15–40 ●¹▽ 4^20 ●°▽ 4^25, 13^25 14^06, 14^10 15^45, 20^46 21^05, 22^44 23^15; K°SW 22^40 22^48 24 SE; = 1^30 11^40, ⌒° 0^00 3
8	7	6.0	.	●°▽ 6^53 7^13 ●¹▽ 7^20 ●°▽ 7^31 ●¹▽ 7^50 ●°▽ 10^05 ●° 15^52 18^20; K°SW 0^00–5; = 3^40 4^30, 18^30 23^45 = °24
9	6	1.3	.	●°▽ 9^40 10^50 ●¹▽ 12^20 13^15; = °0^00 1^20 = 14^30
10	8	.	.	⌒° 21–24
11	8	.	.	⌒° 0^00 1 ⌒¹ 9, 22–24; ⊕ 10^30 11^20
12	7	0.9	.	●°▽ 10^56 11^20, 12^32 13^40 15^20–42; = 3^30 5^40 = °6^50 = 8^45; ⌒° 0^00 10, 23–24
13	8	5.5	.	●°▽ 8^04–25 9^14–20 ●¹▽ 9^26 ●°▽ 10^10, 13^04–10 14^52 15^20, 19^15–30; ⌒° 0^00 8^04
14	8	2.7	.	●°▽ 0^05–20 1^40 4^35 ●¹▽ 5^50 8^20 ●°▽ 9^46–55, 10^04 11^02, 11^35–45, 12^05–36, 13^20–40
15	8	.	.	= 4^52 5^50 = 7^30; ⌒° 21–24
16	8	.	.	= 0^42 3^50 = °7^15; ⌒° 0^00 1 ⌒¹ 11 ⌒° 20–21 ⌒¹ 24
17	8	.	.	= 3^40 4^40 = °5^50 = 6^20; ⌒¹ 0^00 7 ⌒° 20–24
18	8	.	.	= 0^30 1^50 = °4^30 = ¹6^40 = ²7^30 = ¹8^50 = 9^10; ⌒° 0^00 2, 19–24
19	7	.	.	⌒° 0^00 10, 20–24
20	6	.	.	= 4^40 9^30 ∞ 21^30 = 24; ⌒° 0^00 1 ⌒¹ 9
21	7	0.0	.	●°▽ 17^40–45; K SW 17^20–25–33 N; = 0^00 8^40; ⌒° 1–8
22	7	.	.	
23	8	.	.	⌒° 1–7
24	7	1.2	.	●° 21^35 22^40
25	7	21.6	.	●° 1^40 3^35 ●°▽ 15^35 16^03 17^40 24; K NW 15^50 16^10 SE K E 16^45 18^50 20^25 W
26	7	40.0	.	●°▽ 0^00 1^20 ●¹▽ 4^40 ●°▽ 7^05 ●¹▽ 10^30 ●²▽ 12^40 ●¹▽ 13^38 ●°▽ 15^05 ●° 18^05, 18^35 19^20 ●°▽ 21^52 24; = 5^40 11^40
27	6	37.7	.	●°▽ 0^00 4^05 ●¹▽ 7^08 ●° 11^40 ●° 14^20 ●¹ 17^35 ●° 24
28	8	0.1	.	●°▽ 0^00 4^10 ●°▽ 14^40–50 16^38–40
29	8	.	.	⌒° 23–24
30	8	3.1	.	●¹▽ 13^51 14^02; = 3^10 9^40, ⌒° 0^00 11, 19–21 ⌒¹ 24
31	7	.	.	= 4^40 6^20, ⌒¹ 0^00 11, 22–24
Σ	-	131.8	-	

Olsztyn-Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ *Wrzesień — Septembre 1965*

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.7	97.6	100.9	98.4	8.4	18.1	14.6	13.9	19.8	4.4	100	63	80	81	0.0	7.7	5.3	3.7	2	3	0	C 0	C 0	E 2
2	103.9	104.4	103.4	103.9	13.2	22.5	17.5	17.7	23.4	11.3	84	57	84	75	2.5	11.6	5.2	5.8	10	4	4	E 2	E 3	ENE 3
3	99.8	97.2	95.4	97.5	16.0	26.1	20.4	20.7	28.6	15.6	93	55	74	74	1.4	15.1	6.3	7.6	8	7	2	E 1	E 2	C 0
4	93.3	92.7	89.7	91.9	17.4	23.8	16.7	18.6	23.8	16.0	90	68	97	85	2.1	9.4	0.6	4.0	6	9	10	C 0	SSW 1	NW 2
5	90.7	93.0	92.8	92.2	12.6	14.4	13.2	13.4	17.0	12.0	99	94	100	98	0.2	0.9	0.0	0.4	10 •	10 •	8	W 5	W 3	C 0
6	91.0	89.8	87.0	89.3	11.5	22.2	16.0	16.4	22.6	8.6	100	66	93	86	0.0	9.1	1.4	3.5	1 ≡	2	4	C 0	SW 1	SE 1
7	86.5	88.4	90.0	88.3	11.7	16.1	11.8	12.9	16.3	11.4	93	65	84	81	1.0	6.5	2.1	3.2	10	5	4	SE 2	SW 6	SW 4
8	91.9	95.3	96.4	94.5	11.4	14.5	11.2	12.1	15.7	9.7	89	72	90	84	1.5	4.6	1.3	2.5	2	9	3	SW 3	W 5	SW 2
9	94.9	95.3	96.9	95.7	11.2	19.4	14.8	15.0	22.2	8.6	91	72	97	87	1.2	6.2	0.5	2.6	4	8	4	SE 2	S 3	C 0
10	94.9	92.7	94.3	94.0	15.0	22.9	17.0	18.0	23.4	12.0	94	61	85	80	0.9	10.7	3.0	4.9	2	8	10	C 0	S 4	WNW 4
11	91.2	90.8	96.8	92.9	13.4	12.6	10.1	11.6	17.0	9.8	98	98	96	97	0.4	0.4	0.5	0.4	10	10 •	9	E 4	NW 6	WNW 3
12	96.7	96.3	95.2	96.1	8.3	15.3	10.3	11.0	16.3	7.5	100	70	92	87	0.0	5.3	0.9	2.1	10 ≡	6	8	WSW 3	SW 4	C 0
13	95.0	92.7	93.6	93.1	10.3	16.5	10.9	12.2	17.0	8.4	96	61	91	83	0.5	7.3	1.1	3.0	6	4	10 •	S 1	SW 5	W 2
14	94.7	95.5	98.0	96.1	8.2	15.2	9.8	10.8	15.5	6.8	99	70	97	89	0.2	5.1	0.3	1.9	6	9	3	SW 1	WSW 7	WSW 2
15	99.0	101.2	106.6	102.3	9.4	13.7	9.3	10.4	15.1	8.3	97	68	93	86	0.3	5.1	0.8	2.1	3	6	1	WSW 5	W 7	W 2
16	109.4	109.8	108.0	109.1	5.8	17.0	10.8	11.1	18.4	4.3	98	59	86	81	0.1	8.0	1.8	3.3	3	4	1	C 0	SW 2	S 1
17	104.6	103.0	102.1	103.2	10.0	20.8	14.8	15.1	21.2	8.9	91	61	92	81	1.1	9.6	1.3	4.0	0	0	0	S 1	S 3	S 1
18	100.5	97.9	95.3	97.9	11.8	22.9	16.5	16.9	23.3	9.1	100	56	81	79	0.0	12.2	3.7	5.3	0	0	0	C 0	S 3	S 3
19	97.3	101.2	104.6	101.0	13.7	14.4	11.3	12.7	16.5	10.6	85	71	78	78	2.3	4.8	3.0	3.4	8	9	0	SW 3	WSW 6	SW 3
20	107.6	111.2	115.1	111.3	11.1	14.3	7.8	10.3	15.6	7.2	92	76	97	88	1.0	3.9	0.3	1.7	6	6	0	W 4	NW 6	WNW 2
21	115.1	114.2	111.1	113.5	8.2	14.5	12.8	12.1	15.0	6.2	100	69	81	83	0.0	5.1	2.8	2.6	7	10	10	W 3	W 5	W 4
22	106.5	104.1	101.3	104.0	10.9	18.9	13.2	14.0	19.9	10.4	95	50	73	73	0.6	10.8	4.2	5.2	3	0	0	SW 5	SW 4	SW 4
23	100.1	100.1	99.1	99.8	10.2	20.8	11.1	13.3	21.9	8.9	91	50	100	80	1.1	12.4	0.0	4.5	3	2	0	SW 2	SW 3	C 0
24	98.9	99.2	99.2	99.1	9.9	22.8	11.9	14.1	23.2	6.5	100	54	94	83	0.0	12.7	0.8	4.5	0	0	0	S 1	S 3	C 0
25	98.5	97.6	96.2	97.4	7.2	23.6	14.5	15.0	24.0	5.4	96	56	89	80	0.3	12.9	1.8	5.1	1	2	0	C 0	E 2	E 1
26	94.4	93.6	94.3	94.1	13.2	22.0	16.8	17.2	23.1	11.0	94	62	82	79	0.9	10.0	3.5	4.8	1	1	0	E 3	SE 3	E 3
27	92.6	90.8	91.9	91.8	12.6	16.2	15.8	15.1	16.9	12.1	96	83	95	91	0.5	3.1	0.9	1.5	2	10	0	E 3	E 5	SE 3
28	90.7	89.8	87.2	89.2	14.0	20.1	16.6	16.8	21.3	13.1	99	71	97	89	0.2	6.8	0.6	2.5	10 •	10	4	E 3	S 3	E 3
29	87.1	88.2	93.4	89.6	15.3	13.2	11.5	12.9	17.9	11.4	97	99	97	98	0.6	0.2	0.4	0.4	10	10 •	10 •	S 1	WSW 4	SW 3
30	98.1	99.5	99.8	99.1	8.7	18.0	12.4	12.9	18.6	8.0	97	60	87	81	0.3	8.2	1.9	3.5	1	1	2	SW 2	S 3	C 0
31																								
M	97.3	97.4	97.9	97.5	11.4	18.4	13.4	14.2	19.7	9.4	95	67	89	84	0.7	7.5	1.7	3.3	4.8	5.5	3.6	2.0	3.7	1.9

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1	102.4	104.3	105.7	104.1	7.0	19.2	10.6	11.8	19.8	6.2	98	67	97	87	0.1	7.4	0.4	2.6	0 ≡	1	0	C 0	C 0	NE 2
2	105.4	105.0	104.3	104.9	9.8	14.6	10.8	11.5	15.8	9.0	100	79	92	90	0.0	3.4	1.0	1.5	9 ≡	9	0	C 0	E 5	E 3
3	104.4	105.1	106.2	105.2	9.2	13.6	12.2	11.8	14.2	8.4	92	83	99	91	0.9	2.7	0.2	1.3	2	10	10	E 2	SE 2	C 0
4	107.3	107.9	107.5	107.6	10.1	15.0	10.9	11.7	15.6	9.7	99	72	99	90	0.2	4.7	0.1	1.7	10 ≡	9	10	C 0	C 0	N 1
5	107.8	108.4	108.5	108.2	10.1	15.4	11.1	11.9	15.7	9.2	100	67	94	87	0.0	5.8	0.8	2.2	10 ≡	4	9	C 0	C 0	C 0
6	108.6	107.9	106.4	107.6	7.0	14.5	11.4	11.1	14.7	6.9	100	72	94	89	0.0	4.6	0.9	1.8	10 ≡	9	9	C 0	N 1	C 0
7	104.4	102.1	100.1	102.2	6.8	15.0	8.3	9.6	15.7	6.6	99	68	97	88	0.2	5.4	0.4	2.0	10 ≡	3	2	C 0	W 2	SW 2
8	97.5	97.8	101.3	98.9	9.3	13.9	7.5	9.6	14.5	5.0	96	72	86	85	0.5	4.4	1.5	2.1	9	8	8	WNW 2	NW 4	NW 3
9	101.1	100.5	99.2	100.3	6.4	8.3	6.0	6.7	10.7	4.8	97	84	94	92	0.3	1.7	0.6	0.9	9	4	9	NW 3	NW 5	NW 4
10	97.3	97.2	97.6	97.4	5.5	8.7	6.6	6.8	9.6	4.8	98	82	94	91	0.1	1.9	0.5	0.8	10 •	10 •	7	W 4	W 5	NW 5
11	97.1	94.9	102.1	98.0	4.8	8.2	3.0	4.8	8.4	2.3	97	87	93	92	0.3	1.4	0.6	0.8	10	9	6	NNE 3	NW 9	NW 3
12	107.2	109.3	109.2	108.6	3.3	7.8	4.4	5.0	8.7	-1.5	95	67	93	85	0.4	3.3	0.6	1.5	7	9	8	W 3	NW 4	WSW 2
13	107.6	106.7	104.4	106.2	3.4	9.1	6.4	6.3	10.4	3.3	90	70	78	79	0.8	3.6	2.1	2.2	1	9	10	WSW 5	SW 4	SW 3
14	103.1	104.1	105.0	104.1	7.8	10.0	9.1	9.0	10.6	6.1	87	86	93	79	1.4	1.8	0.8	1.3	10	10	10	W 2	W 3	SW 1
15	103.5	102.1	99.6	101.7	3.7	14.3	9.0	9.0	14.8	3.0	100	59	85	81	0.0	6.8	1.7	2.8	0 ≡	2	5	SW 1	SW 4	SW 2
16	97.0	96.9	98.6	97.5	8.8	9.8	9.1	9.2	11.4	6.8	90	99	96	95	1.1	0.1	0.5	0.6	9	10 •	9	SSW 3	W 3	W 3
17	103.3	105.8	108.2	106.1	6.1	11.3	5.4	7.0	11.7	5.4	95	64	89	83	0.4	4.8	1.0	2.1	1	4	0	W 5	WNW 6	W 2
18	105.3	105.3	106.6	105.7	7.0	9.8	8.8	8.6	10.5	4.2	98	96	95	96	0.1	0.5	0.6	0.4	10 •	10	9	W 5	SW 5	NW 3
19	108.5	108.8	110.1	109.1	4.8	10.8	7.1	7.4	11.4	2.2	100	70	93	88	0.0	3.9	0.8	1.6	8	4	5	W 3	W 5	NW 3
20	113.6	116.4	118.1	116.0	3.4	7.6	0.0	2.8	8.0	-0.3	95	69	98	87	0.4	3.2	0.1	1.2	1	7	0	NNW 2	ENE 4	NE 1
21	119.2	120.3	120.3	119.9	-3.8	7.6	1.4	1.6	7.9	-4.1	100	60	89	83	0.0	4.2	0.8	1.7	4 ≡	2	0	C 0	S 3	WSW 2
22	119.5	118.5	115.6	117.9	-0.2	6.1	7.8	5.4	7.8	-0.7	94	76	87	86	0.4	2.2	1.4	1.3	7	10	10	W 3	W 4	W 4
23	111.8	111.5	111.9	111.7	8.1	10.2	5.9	7.5	10.5	4.6	96	80	97	91	0.5	2.5	0.3	1.1	10	10	7	W 4	NW 4	NW 2
24	113.0	113.3	112.7	113.0	-0.1	9.4	8.6	6.6	9.7	-0.1	100	82	86	89	0.0	2.2	1.6	1.3	0 ≡	9	10	C 0	N 4	NNW 3
25	110.6	111.1	111.6	111.1	7.5	9.4	6.4	7.4	9.4	5.6	93	87	92	91	0.8	1.6	0.7	1.0	10	10	8	W 4	NNW 3	C 0
26	109.6	108.3	105.0	107.6	-0.2	8.5	5.4	4.8	9.8	-0.7	100	85	98	94	0.0	1.7	0.2	0.6	0 ≡	4	10	C 0	SW 3	C 0
27	100.9	101.0	100.3	100.8	4.2	2.0	2.3	2.7	6.0	1.8	93	100	96	96	0.3	0.0	0.3	0.3	7	10 ≡	10	SW 2	W 3	WSW 4
28	96.5	95.3	95.5	95.8	6.3	12.8	11.3	10.4	12.9	2.7	93	77	89	86	0.8	3.4	1.5	1.9	10	9	0	SW 4	SW 6	SW 3
29	93.7	92.7	93.0	93.1	8.2	14.6	8.7	10.0	13.9	8.0	94	76	97	89	0.6	4.0	0.3	1.6	0	6	10	SW 4	SW 4	W 3
30	97.6	98.9	97.2	97.9	5.6	7.5	6.6	6.6	9.0	3.4	93	84	88	88	0.9	1.7	1.1	1.2	10	6	0	W 7	WSW 4	WSW 4
31	88.7	88.8	88.2	88.6	6.2	9.7	5.1	6.3	9.7	4.6	79	70	92	80	2.0	3.3	0.7	2.1	9	9	6	SW 9	WSW 7	SW 7
M	104.6	104.7	104.8	104.7	5.7	10.8	7.3	7.8	11.6	4.2	95	77	93	88	0.4	3.2	0.8	1.5	6.5	7.3	6.4	2.6	5.7	2.5

Olsztyn-Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$ Wrzesień - Septembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	.	= 0^30–1^50 ≡–4^10 ≡°–6^20 =–7^40. ⌒'0^00–10 ⌒°19–24
2	7	.	.	⌒°0^00–11
3	7	.	.	= 6^10–8^40. ⌒°1–10. 21–24
4	7	13.7	.	●°12^40–14^28. 16^50–17^35 18^25–50 ●'–19^10 ●°–20^05 ●'21^02–22^34. = 16^10–24. ⌒°0^00–10
5	6	5.3	.	●°2^40–3^45 ●'–4^03 ●°–6^05 ●°6^15–13^05 ●'–14^20 ●°–15^35. = 0^00–24
6	7	10.2	.	●²21^40–22^03 ●°–22^15. = 0^00–3^20 ≡–4^40 ≡–6^50 =–12^10. 23^20–24
7	8	.	.	●'0^45–2^20 ●°–3^10. = 0^00–6^10. ⌒°21–24
8	7	.	.	= 20^10–24. ⌒°0^00–10 ⌒'23–24
9	7	.	.	= 0^00–10^20. 18^30–24. ⌒'0^00–10 ⌒°19–24
10	7	3.5	.	= 0^00–50 ≡°–4^55 ≡–8^40. ⌒°0^00–10
11	6	0.6	.	●°3^42–4^45 ●'5^55–6^10 ●°–6^20 ●°11^05–12^40 ●°–14^40 ●°16^04–15. = 5^30–24
12	7	1.4	.	= 0^00–4^50 ≡°–7^45 =–9^40 20^20–24. ⌒°18–24
13	8	0.9	.	●'1^10–45 ●°16^20–35. 20^20–21^05. (R)°S 1^50–3^35 E. = 0^00–2^20. ⌒°0^00–2^10
14	6	3.1	.	●°13^05–20 ●'13^48–55 ●°–14^40. 16^40–50. = 2^40–14^50
15	7	.	.	⌒°18–24
16	8	.	.	= 4^20–5^45 ≡°–6^30 =–7^10. ⌒°0^00–11. 18–24
17	7	.	.	= 4^40–11^10 ∞ 13^30–17^50 =–24. ⌒°0^00–1 ⌒'–10 ⌒°21–24
18	7	0.4	.	= 1–3^40 ≡–5^35 =–10^30. ⌒'1–11 ⌒°22–24
19	7	.	.	●°3^50–4^05. = 5^20–6^20. ⌒°0^00–3^50. ⊕ 15^30–16^20
20	8	.	.	⌒°1–8. 19–24
21	7	.	.	⌒°0^00–11
22	6	.	.	= 6^20–10^30 ∞ 14^30
23	7	.	.	= 3^40–10^20. 17^20–23^45 ≡°–24. ⌒°0^00–11. 18–24
24	7	.	.	≡°0^00–2^35 =–9^40. 20^20–24. ⌒°0^00–2 ⌒'–10 ⌒°19–24
25	7	.	.	= 0^00–10^40. 17^30–24. ⌒°0^00–1 ⌒'–10 ⌒°20–24
26	7	.	.	= 0^00–8^40. ⌒°0^00–1 ⌒'–9
27	7	1.2	.	●°10^10–12^10. 13^40–15^03. ⌒°3–9
28	7	3.4	.	●°6^30–45 ●°16^35–19^15 ●°23^10–24. = 2^20–8^30
29	6	32.4	.	●'0^00–40 ●°1^50 8^25 ●°–8^35 ●'9^20 ●°–11 ●'–13^25 ●°–15^10 ●°–18^05 ●'–20^40 ●°–21^10 ●°22^50–23^05. = 1^40–5^45. 6^20–24
30	8	.	.	= 0^00–9^40. 19^45–24. ⌒°18–24
31				
Σ	–	76.1	–	

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	.	= 0^00–4^45 ≡°–5^20 ≡'–6^10 ≡²–7^20 ≡'–7^40 ≡°–8^25 =–9^20. 22^40–23^50 ≡°–24. ⌒°0^00–3 ⌒'–12
2	7	.	.	≡°0^00–1 ≡'–6^20 ≡°–7^40 =–10^30. ⌒°0^00–1 ⌒'–12 ⌒°18–24
3	7	0.5	.	●°13^17–50. ⌒°0^00–11 ⌒'21–24
4	7	.	.	= 0^00–3^50 ≡°–5^10 ≡'–8^20 ≡°–9^35 =–11^30 16^30–21^45 ≡°–22^20 ≡'–24. ⌒'0^00–11 ⌒°–12. 18–21 ⌒'–24
5	7	.	.	≡'0^00–3^40 ≡°–6^20 ≡'–7^40 ≡°–8^45 =–10^20. 22^30–24. ⌒'0^00–10 ⌒°20–24
6	7	.	.	= 0^00–2^50 ≡'–6^20 ≡°–8^20 ≡'–8^50 ≡°–9^25 =–10^50. ⌒°0^00–2 ⌒'–12 ⌒°–13 ⌒'20–24
7	7	.	.	= 2^35–5^50 ≡°–6^20 ≡'–8^50 =–9^40. ⌒'0^00–11 ⌒°20–24
8	7	0.2	.	= 0^30–10^25. ⌒°0^00–1 ⌒'–11 ⌒°21–24
9	8	0.7	.	●°0^50–1^15. 11^26–40 12^20–35. 14^45–15^05. 22^50–23^05. ⌒°0^00–50. ⌒ 14^23–15^02
10	7	1.3	.	●°3^45–4^05. 5^30–7^25 10^55–11^05. 12^20–45. 13^45–14^10. 14^50–16^20. 19^40–20^03. 23^35–50
11	7	2.8	.	●°7^45–8^45. 9^30–11^25. 13^45–14^10. 17^20–30. 17^45–18^15. ⊹ 13^40–14^10. ⌴°23^30–24
12	8	.	.	⌴°0^00–2
13	8	.	.	⌒°5–9
14	7	.	.	= 13^30–24
15	7	.	.	= 0^00–3^50 ≡°–7^35 =–11^40. 16^30–24. ⌴°5–8
16	5	6.1	.	●°11^35–17^40. = 0^00–12^50 ≡°–13^25 =–19^20. ⌒°0^00–10
17	8	0.0	.	
18	6	0.9	.	●°6^45–10^35. = 10^30–15^20
19	8	.	.	= 0^45–2^30. ⌒°22–24
20	8	.	.	≡°22^50–24. ⌒°0^00–10. 19–20 ⌴°–23 ⌴'–24
21	8	.	.	≡°0^00–3^30 ≡'–5^30 ≡°–6^50 =–9^40. ⌴'0^00–10 ⌒'21–23 ⌴'–24
22	7	.	.	= 5^30–8^30. 16^20–24. ⌴'0^00–7
23	6	.	.	= 0^00–14^30. 21^30–22^50 ≡°–23^20 ≡'–24. ⌒°20–22 ⌒'–24
24	8	.	.	≡'0^00–8^40 ≡'–9^25 =–9^35. ⌒'0^00–3 ⌴'–8 ⌒²–11
25	6	0.0	.	●°10^10–11^07. = 8^40–13^30. 22^20–24
26	7	.	.	= 0^00–1^45 ≡°–2^40 ≡'–9^25 =–10^20. 16^30–24. ⌴°2–8
27	3	.	.	= 0^00–11^50 ≡°–13^45 ≡'–15^50 ≡°–17^35 =–24. ⌒°0^00–9
28	6	.	.	= 0^00–24
29	7	4.4	.	●'18^40–50 ●°–20^35. = 0^00–12^10. 15^30–19^30. 20^35–23^30. ⌒°2–11
30	8	.	.	
31	6	2.9	.	●'13^20–40 ●°14^45–15^05. = 7^20–17^20
Σ	–	19.8	–	

Olsztyn – Dajtki φ = 53°46' λ = 20°25' Listopad – Novembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	87.9	83.4	74.3	81.9	4.8	6.0	10.3	7.8	10.3	4.0	94	97	96	96	0.6	0.3	0.5	0.5	9	10 •	10 •	SW 5	SSE 7	SW 8
2	73.8	75.9	78.3	76.0	9.4	9.0	8.2	8.7	10.5	6.4	80	61	63	68	2.4	4.5	4.0	3.6	10	9	7	WSW 6	SW 9	SW 8
3	82.9	86.2	88.9	86.0	5.7	6.0	4.8	5.3	8.2	4.6	79	73	81	78	2.0	2.6	1.7	2.1	7	10	3	SW 7	SW 6	W 6
4	93.5	97.8	102.6	98.0	3.0	5.2	4.0	4.0	5.3	2.8	91	84	90	88	0.7	1.4	0.8	1.0	9	7	9	WSW 6	SW 6	WSW 6
5	106.5	108.7	109.5	108.2	4.6	6.5	5.4	5.5	6.6	3.8	98	96	91	95	0.2	0.5	0.9	0.5	10	9	9	WSW 4	W 5	W 4
6	108.0	107.7	106.2	107.3	3.5	5.2	5.2	4.8	5.5	2.9	100	98	98	99	0.0	0.1	0.1	0.1	10	10 •	10	W 7	W 5	W 4
7	103.0	102.8	103.7	103.2	5.4	7.1	4.8	5.5	7.7	3.7	97	90	100	96	0.3	1.0	0.0	0.4	9	10	7	W 3	W 3	WNW 2
8	106.8	107.7	108.1	107.5	-0.6	4.5	3.0	2.5	6.1	-1.1	100	98	100	99	0.0	0.1	0.0	0.0	10 ≡	7	10 ≡	C 0	SW 1	SW 2
9	106.4	104.7	102.6	104.6	-0.4	2.4	4.0	2.5	4.0	-0.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10	10	SW 2	SSW 2	WSW 3
10	101.0	101.7	101.7	101.5	6.3	8.2	4.4	5.8	8.6	4.0	100	70	85	85	0.0	3.3	1.3	1.5	10 • ≡	6	9	NW 3	N 4	N 2
11	99.7	99.3	98.5	99.2	-0.9	4.0	-1.4	0.1	4.8	-1.9	100	56	90	82	0.0	3.5	0.5	1.3	0 ≡	2	0	N 2	NNE 5	NE 3
12	96.4	96.7	98.2	97.1	-2.8	-0.9	-2.7	-2.3	-0.5	-2.9	97	73	84	85	0.1	1.5	0.8	0.8	7	7	10	NE 6	NE 6	NE 5
13	99.1	100.3	100.7	100.0	-4.2	-4.1	-5.1	-4.6	-2.7	-5.3	84	70	49	68	0.7	1.3	2.1	1.4	10	9	10	NE 6	E 5	NE 6
14	100.3	100.7	101.0	100.7	-6.9	-5.6	-6.1	-6.2	-4.7	-7.0	88	82	92	87	0.4	0.7	0.3	0.5	10	10	10 *	NE 5	NE 5	NE 5
15	101.0	102.1	105.1	102.7	-6.4	-5.9	-6.5	-6.3	-5.7	-6.9	91	92	94	92	0.3	0.3	0.2	0.3	10 *	10 *	10 *	ENE 3	ENE 3	NE 3
16	109.8	111.3	112.1	111.1	-8.6	-6.2	-14.0	-10.7	-6.0	-15.6	92	89	92	91	0.3	0.4	0.2	0.3	4	4	0	NE 2	NE 3	C 0
17	100.2	109.2	107.2	108.9	-10.7	-8.6	-11.6	-10.6	-7.9	-16.5	94	95	97	95	0.2	0.2	0.1	0.2	10	10	10	C 0	S 4	SSE 2
18	104.3	101.7	98.6	101.5	-13.0	-11.0	-12.2	-12.1	-10.0	-13.6	96	90	89	92	0.1	0.3	0.3	0.2	10	2	0	ESE 2	E 3	E 5
19	92.4	90.3	88.0	90.2	-11.5	-9.8	-9.0	-9.8	-9.0	-13.9	90	88	92	90	0.3	0.4	0.3	0.3	10 *	10 *	10	E 5	E 4	E 5
20	87.1	88.3	88.7	88.0	-7.8	-6.9	-6.9	-7.1	-6.4	-9.2	93	91	94	93	0.2	0.3	0.2	0.2	10	10	10	NE 3	N 2	N 3
21	83.9	79.1	72.5	78.5	-6.4	-4.6	-6.1	-5.8	-4.6	-7.2	94	96	97	96	0.2	0.2	0.1	0.2	10	10 *	10 *	NE 4	NE 4	NE 5
22	78.6	83.8	90.9	84.4	-7.0	-1.6	-2.9	-3.6	-1.5	-8.0	93	90	91	91	0.2	0.5	0.4	0.4	10	5	9	NW 3	W 5	W 6
23	96.1	99.9	103.2	99.7	-6.1	-6.1	-13.9	-10.0	-2.9	-15.4	94	86	87	89	0.2	0.5	0.3	0.3	6 *	6	0	W 5	W 2	W 2
24	102.6	101.3	100.1	101.3	-12.8	-9.1	-10.6	-10.8	-8.6	-15.1	88	82	90	87	0.3	0.5	0.3	0.4	0	0	0	S 3	S 4	SSE 4
25	97.4	97.0	97.2	97.2	-7.8	-4.4	-2.7	-4.4	-2.6	-12.2	93	86	95	91	0.2	0.6	0.2	0.3	10	10 *	10	SE 6	S 6	S 3
26	90.9	84.8	83.4	86.4	-2.0	-2.6	0.2	-1.0	0.2	-2.7	96	79	96	90	0.2	1.1	0.3	0.5	10	10	10 *	S 5	SSE 6	S 4
27	85.3	82.0	69.7	79.0	-3.9	-2.2	0.7	-1.2	1.1	-5.0	92	96	98	96	0.4	0.2	0.1	0.2	0	10	10 *	S 3	E 3	E 6
28	66.0	67.8	70.9	68.2	2.0	1.5	0.0	0.9	2.4	-0.1	100	98	98	99	0.0	0.1	0.1	0.1	10	10	10 *	S 3	SW 5	SW 4
29	77.4	84.1	83.8	81.8	1.1	0.7	0.6	0.8	1.4	-2.1	90	83	94	89	0.6	1.1	0.4	0.7	10 *	6	10	SW 6	WSW 7	S 6
30	74.4	75.9	80.2	76.8	1.8	3.9	2.4	2.6	4.2	-0.2	82	78	87	82	1.3	1.8	1.0	1.4	10	10	10	S 5	S 7	SW 2
31																								
M	94.1	94.4	94.2	94.2	-2.4	-0.6	-1.8	-1.6	0.5	-4.3	93	86	90	90	0.4	1.0	0.6	0.7	8.4	8.0	7.8	4.0	4.6	4.1

Grudzień – Décembre

1	78.4	76.0	79.6	78.0	-0.4	0.4	0.9	0.4	2.6	-0.5	88	100	90	93	0.7	0.0	0.6	0.4	3	10 *	8	S 2	S 6	WSW 6
2	86.0	87.8	87.5	87.1	-0.1	0.1	-0.9	-0.4	0.9	-1.3	88	92	89	90	0.8	0.3	0.6	0.6	9	10	10	WSW 3	WSW 3	S 3
3	80.3	80.3	81.4	80.7	0.2	1.1	0.6	0.6	1.5	-1.1	83	83	92	86	1.1	1.1	0.5	0.9	10	10	10	SE 6	S 5	SE 5
4	80.8	81.8	83.8	82.1	-0.5	0.9	1.1	0.6	1.3	-0.6	98	100	100	99	0.2	0.0	0.0	0.1	10	10	9	S 1	SW 3	SW 3
5	84.7	85.5	74.5	81.6	1.1	2.2	2.3	2.0	2.4	0.9	98	73	77	83	0.1	2.0	1.7	1.3	10 •	4	10	SW 4	S 4	SE 9
6	67.9	70.6	77.2	71.9	3.8	4.8	4.2	4.2	5.1	0.4	73	68	69	70	2.1	2.7	2.5	2.4	8	9	3	SW 6	SW 10	W 10
7	83.4	87.0	89.5	86.6	2.8	3.0	3.4	3.2	4.2	1.6	82	77	80	80	1.3	1.7	1.6	1.5	10	8	9	WSW 6	SW 7	SW 5
8	90.9	92.8	95.5	93.1	1.8	0.9	-0.3	0.5	3.4	-0.5	91	94	92	92	0.7	0.4	0.5	0.5	10	9	6	SW 5	W 5	W 1
9	97.3	92.1	81.2	90.2	0.0	1.8	0.6	0.8	1.9	-1.1	88	73	94	85	0.7	2.0	0.4	1.0	9	9 *	10	SW 5	SW 8	SW 8
10	66.1	64.6	62.8	64.5	2.2	2.8	3.7	3.1	3.7	0.3	82	82	80	81	1.3	1.3	1.6	1.4	10	10	6	S 10	SW 6	S 6
11	67.8	71.6	73.0	70.8	2.9	2.8	2.2	2.5	4.5	1.4	84	76	77	79	1.2	1.9	1.7	1.6	9	9	9	W 8	SW 5	S 6
12	79.0	82.6	86.3	82.6	0.3	0.6	-0.4	0.0	2.2	-0.5	86	77	96	86	0.8	1.5	0.2	0.8	10	10	10 *	S 6	W 6	W 3
13	90.0	91.6	92.6	91.4	-1.5	-1.9	-4.1	-2.8	-0.5	-4.2	95	77	87	86	0.3	1.2	0.6	0.7	10 *	6	3	WNW 4	W 6	W 3
14	95.7	98.8	103.1	99.2	-5.9	-5.6	-5.4	-5.6	-2.4	-6.5	87	87	85	86	0.6	0.6	0.8	0.7	4	7	9	WNW 6	W 6	W 6
15	101.2	102.1	103.1	102.8	-3.9	-5.4	-9.4	-6.5	-2.8	-10.9	94	94	98	95	0.3	0.3	0.1	0.2	10 *	6	10 ≡	W 3	NW 2	C 0
16	104.1	103.4	103.0	103.5	10.4	-6.8	-8.9	-8.8	-3.3	-13.3	97	91	92	93	0.1	0.3	0.3	0.2	2	1	0	W 2	W 1	W 2
17	102.0	101.4	100.2	101.2	-9.1	-9.2	-10.8	-10.0	-8.0	-14.7	92	98	97	96	0.3	0.1	0.1	0.2	1	3	10	SW 2	S 2	ESE 3
18	98.1	95.7	89.4	93.7	-6.2	-2.4	2.3	-1.0	2.3	-11.0	97	96	98	97	0.1	0.2	0.1	0.1	10	10 ≡	10 •	SE 4	SE 5	S 5
19	88.5	89.2	86.9	88.2	7.8	8.9	8.6	8.5	9.5	2.0	97	94	99	97	0.3	0.6	0.2	0.4	10 •	10	10 •	S 5	WSW 7	SW 6
20	92.3	96.2	97.3	95.3	2.4	4.0	3.3	3.4	9.3	2.3	95	90	83	89	0.4	0.8	1.3	0.8	10	10	9	SW 5	SW 5	SW 4
21	95.3	94.6	96.1	95.3	1.8	3.7	-0.3	1.2	3.8	-0.7	93	82	98	91	0.6	1.3	0.2	0.8	10	10	0	SW 2	W 2	WNW 3
22	98.7	100.2	101.5	100.1	0.0	0.6	-1.0	-0.4	0.6	-1.1	96	92	91	93	0.2	0.5	0.3	0.4	9	9	10	W 4	SW 3	SW 2
23	100.3	98.5	93.3	97.4	-2.0	-1.3	-2.3	-2.0	-0.9	-2.6	94	86	80	87	0.4	0.8	1.0	0.7	10	10	10	SSE 5	SW 4	SE 4
24	86.7	84.2	80.1	83.7	-2.8	-2.2	-0.2	-1.4	-0.1	-4.3	92	96	90	92	0.3	0.2	0.6	0.4	10	10	8	SE 4	SE 6	SE 3
25	74.7	72.3	71.5	72.8	-0.1	1.0	0.3	0.3	1.0	-0.6	88	77	94	86	0.8	1.3	0.3	1.0	10	7	10 *	SE 5	SE 6	SE 5
26	69.9	72.7	77.8	73.3	0.0	1.6	0.6	0.7	1.6	-0.1	100	100	98	99	0.0	0.0	0.1	0.0	10 *	10 ≡	10 *	SE 3	SW 1	SW 4
27	83.0	83.6	80.3	82.3	0.0	0.7	-1.6	-0.6	0.8	-1.9	92	90	94	93	0.3	0.6	0.3	0.5	8	8	5	W 3	SSW 3	S 4
28	76.8	78.0	82.3	79.0	-1.8	-0.6	-0.7	-1.0	-0.6	-2.4	98	93	89	93	0.1	0.4	0.6	0.4	10	10 *	9	SW 1	W 3	WSW 6
29	86.3	89.6	89.8	88.6	-1.1	-0.8	-0.9	-0.9	-0.3	-2.2	87	79	93	88	0.8	1.2	0.4	0.8	9	3	9	W 7	W 7	WSW 6
30	89.2	86.5	82.3	86.1	-0.9	-1.3	-0.3	-0.8	-0.1	-2.0	89	78	90	86	0.6	1.2	0.6	0.8	9 *	10	10	WSW 7	SW 4	SW 3
31	83.9	84.2	85.8	84.0	1.8	2.4	2.0	2.0	2.4	-0.3	93	86	96	92	0.6	1.1	0.3	0.7	10	4	10 •	SW 4	SW 3	WSW 5
M	86.4	86.9	86.7	86.7	-0.5	0.3	-0.3	-0.2	1.4	-2.4	91	86	90	89	0.6	0.9	0.7	0.7	8.7	8.1	8.1	4.4	4.7	.5

Olsztyn – Dajtki

$H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$

Listopad – Novembre 1965

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚCIOŁA	POGODA
1	6	11.1	•	●° 11^55 – 14^10 •° – 22^40, = 14^10 – 24
2	8	0.8	•	●° 13^37 – 15^25, = 0^00 – 13^30
3	8	•	•	
4	8	0.1	•	
5	6	1.2	•	●° 4^55 – 5^20, 7^25 – 9^35 •° – 11^20; = 6^10 – 13^10
6	5	0.8	•	•° 4^35 – 5^40, 8^40 – 9^10 •¹ – 11^40 •° – 15^35; = 5^30 – 6^40 ≡° – 7^45 = – 24
7	6	•	•	= 0^00 – 18^30, 20^20 – 23^40 ≡° – 24
8	5	•	•	≡° 0^00, 1^20, ≡¹ – 3^40 ≡² – 5^30 ≡¹ – 7^20 ≡° – 9^20 ≡² – 11^10 ≡¹ – 11^30 ≡° – 11^45 ≡ – 15^10 ≡° – 15^30 ≡¹ – 15^35 ≡² – 20^20 ≡° – 23^35 ≡° – 24, ⌴° 5 – 7
9	4	1.1	•	•° 23^35 – 24; ≡¹ 0^00 – 6^10 ≡² – 10^40 ≡° – 12^20 = – 22^45 ≡¹ – 23^35 ≡° – 24
10	7	0.0	•	•° 0^00 – 3^45 •¹ – 6^20 •° – 7^10 ●°? 21^52 – 22^05; ≡° 0^00 – 7^25 = – 10^20
11	8	0.0	•	= 3^30 – 4^50 ≡° – 5^20 ≡² – 8^20 ≡° – 9^45 = – 10^20, ⌴° 4 – 11^30, 23 – 24
12	8	0.0	•	✱° 2^45 – 3^10 13^52 15^10, = 6^10 – 8^20, ⌴° 0^00 – 2^45; ⊽ 4^30 – 6^20
13	7	0.0	•	✱° 8^40 – 10^20, 11^30 – 40, 19^20 – 41
14	7	1.6	•	✱° 3^50 – 6^10, 8^20 – 10^40 ✱° 20^10 – 24
15	4	3.0	3	✱° 0^00 – 24
16	7	•	5	✱° 0^00 – 3^35; = 3^35 7^20, 18^20 – 50 ≡° – 20^20 = 23^30 – 24, ∨ 18^50 – 24, ⊽ 3^40 – 5^10
17	6	0.0	5	= 0^00 – 2^20, ∨ 0^00 – 14
18	6	0.6	5	✱° 5^45 – 6^20, = 6^20 – 21^30
19	4	1.4	6	✱° 3^54 – 17^20, = 3^30 – 19^15
20	6	•	9	= 4^10 – 24
21	4	6.9	9	✱° 9^45 – 11^10, 13^30 – 24; = 0^00 – 24
22	7	1.0	15	✱° 0^00 – 6^20 △ 8^05 9^20 ✱° – 11^15 ✱° 11^45 – 12^20 13^25 – 14^08, 15^50 – 16^40 ✱¹ – 17^20 ✱° – 18^45; = 0^00 – 12^30
23	7	1.0	17	✱° 6^20 – 45, 7^48 – 9^10, 9^30 – 11^05, 11^30 – 12^20
24	7	•	18	= 15^30 – 24
25	6	0.4	18	✱° 9^40 – 11^05, 11^08 – 14^20 ✱° 15^52 – 18^40; = 0^00 – 5^40, 18^40 – 24
26	6	0.9	19	✱° 17^40 – 21^35, ⸸ 18^45 – 20^50, = 0^00 – 24
27	6	2.4	19	✱° 11^45 – 19^20, 20^35 – 24; = 0^00 – 2^30, 8^30 – 17^30
28	6	1.7	17	✱° 0^00 – 1^10 ✱° – 1^50 •° 9^20 – 12^10, 13^20 – 15^30 ✱° – 16^40, 17^20 – 19^10 ✱¹ – 21^20; = 1^50 – 24
29	8	0.0	16	✱° 6^20 – 7^15; = 0^00 – 7^20
30	7	0.0	15	✱° 3^45 – 4^25 •° 6^20 – 7^15 •° 17^40 – 19^50
31				
Σ	–	36.0	–	

Grudzień – Décembre

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚCIOŁA	POGODA
1	4	1.4	10	✱° 11^05 – 14^05 ⸸ 14^25 – 15^05 •° 19^10 – 20^05; = 11^30 – 16^30
2	6	0.0	8	✱° 9^50 – 11^10; = 11^30 – 24
3	7	0.7	8	✱° 7^32 – 8^20, 22^20 – 24; = 0^00 – 12^20, 16^30 – 20^30
4	4	0.0	9	✱° 0^00 – 20, 1^40 – 3^25; = 1^40 – 3^30 6^30 – 8^25 ≡° – 11^40 = – 13^20 ≡° – 18^40 = – 24
5	7	3.8	8	●° 6^25 – 7^15 ✱° 21^53 – 24; = 0^00 – 7^35 ≡° – 8^10 = – 11^30 14^20 – 24
6	8	•	9	✱° 0^00 – 1^40, ≫ 12^20 – 19^30; = 0^00 – 6^10
7	7	0.0	5	✱° 0^40 – 10^10
8	6	1.7	pł.	●° 7^10 – 25 ✱° 9^20 – 40 10^35 11^05 ✱¹ – 11^45 ✱° – 12^20 15^35 – 16^20; = 17^20 – 24
9	6	2.0	pł.	✱° 18^45 – 19^20 20^15 – 22^35 •° 23^50 – 24; = 0^00 – 5^30 9^30 – 18^30 22^35 – 24
10	7	0.9	pł.	•° 0^00 – 1^20 ✱° – 3^35 ✱° 4^50 – 5^20, 6^40 – 10^05; ≫ 5^10 – 9^35; = 23^30 – 7^20
11	8	0.0	pł.	●° 6^40 – 7^25 ✱° 23^35 – 24
12	8	0.9	pł.	✱° 0^00 – 20, 1^40 – 5^20, 19^05 – 24
13	7	0.5	1	✱° 0^00 – 10^20
14	7	1.2	2	✱° 4^54 – 6^20 ✱° 9^15 – 11^10, 12^40 – 13^10 13^45 – 19^15
15	6	0.9	5	✱° 1^50 – 5^40 ✱¹ – 8^30 ✱° – 10^20; = 10^20 – 17^50 ≡° – 22^20 = – 22^50, ∨ 17^50 – 22^20
16	7	0.0	5	
17	7	•	5	✱° 5^50 – 6^05; = 21^30 – 24
18	3	15.9	5	✱° 13^40 – 15^25 •° – 24; = 0^00 – 10^45 ≡° 14^10 = – 24
19	6	12.4	pł.	•° 0^00 – 10^35, 13^05 – 15^40, 17^50 – 24; = 0^00 – 24
20	7	0.2	•	•° 0^00 – 1^40 7^35 – 8^05; = 0^00 – 1^40
21	7	0.0	•	•° 13^40 – 14^15; = 15^20 – 17^30 20^40 – 24; ⌴° 23 – 24
22	7	0.0	•	✱° 7^45 – 8^10; = 0^00 – 9^40; ⌴° 0^00 – 7^45
23	7	•	•	= 7^20 – 12^10
24	5	•	•	= 9^30 – 24
25	6	0.6	•	✱° 18^35 – 22^20; = 0^00 – 23^30
26	2	2.8	2	✱° 1^10 – 3^15 4^25 – 7^40 •° 10^40 – 11^30 ✱° 18^05 – 21^40; = 7^20 – 11^20 ≡° – 12^20 ≡¹ – 14^35 = – 24
27	7	•	3	= 0^00 – 40 15^30 – 21^30
28	5	0.2	3	✱° 17^50 – 19^40; = 7^30 – 24
29	7	1.5	3	✱° 1^30 – 3^20 ✱° 4^45 – 5^15 7^40 – 9^40 18^40 – 19^15; = 0^00 – 3^30, 9^40 – 12^30
30	7	0.4	3	✱° 1^40 – 2^35 4^35 – 8^10 ✱° 16^40 – 19^05
31	6	1.9	4	•° 9^52 – 10^35 ✱° – 11^40 ✱° 14^40 – 15^10 16^35 – 17^10 ✱° – 18^40 ✱° 19^10 – 21^20; = 7^20 – 22^40
Σ	–	49.9	–	

4*

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$ *Styczeń – Janvier* 1965

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N_w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_v I	II	III
1	78.5	78.3	78.5	78.4	2.3	2.7	2.3	2.4	4.3	1.7	87	91	87	88	0.9	0.6	0.9	0.8	9	10	10	W 9	SW 6	SW 6
2	76.6	77.3	79.7	77.9	1.0	2.8	0.7	1.3	2.8	0.4	96	81	94	90	0.3	1.5	0.4	0.7	10	5	10	SW 5	WSW 6	SW 4
3	82.8	85.2	89.6	85.9	0.4	1.2	0.3	0.6	1.7	-0.9	98	83	88	90	0.1	1.2	0.7	0.7	10	9	10	WSW 2	NW 3	NW 2
4	95.4	98.7	99.4	97.8	-0.5	0.9	-2.2	-1.0	1.0	-2.6	84	75	89	83	1.0	1.6	0.6	1.1	10	5	0	N 1	N 4	W 5
5	86.8	91.5	95.7	91.3	0.1	0.7	-0.8	-0.2	1.3	-3.0	96	85	85	89	0.3	1.0	0.9	0.7	10 *	0	0	W 13	WNW 8	WNW 6
6	98.9	100.4	102.0	100.4	-3.7	-1.9	-3.8	-3.3	-0.7	-4.0	87	79	80	82	0.6	1.1	0.9	0.9	0	3	0	NW 5	NNW 7	NNW 6
7	102.5	100.4	94.6	99.2	-5.2	-2.4	-3.8	-3.8	-1.9	-6.1	90	72	87	83	0.4	1.4	0.6	0.8	2	6	10	NW 5	WNW 1	SSW 4
8	85.1	79.9	74.8	79.9	-0.2	1.2	4.0	2.2	4.1	-4.3	98	100	97	98	0.1	0.0	0.2	0.1	10	10 • ≡	10	SW 7	SW 7	W 8
9	79.2	81.2	81.4	80.6	2.5	2.3	0.7	1.6	4.1	0.4	98	93	100	96	0.1	0.6	0.0	0.2	10	10	10 •	W 7	W 5	SW 1
10	81.5	90.0	100.6	90.7	-5.1	-6.5	-11.1	-8.0	0.7	-11.4	97	83	86	89	0.1	0.6	0.4	0.4	10	10	0	E 5	NE 6	SE 1
11	102.5	100.5	97.2	100.1	-10.7	-5.6	-3.6	-5.9	-3.3	-11.3	83	85	85	84	0.4	0.6	0.7	0.6	0	10	8	SE 3	SSE 5	SSE 5
12	95.4	93.5	90.3	93.1	-4.6	-0.9	-1.0	-1.9	0.2	-4.9	93	87	89	90	0.3	0.7	0.7	0.6	2	7	8	SSE 3	SSE 3	SE 5
13	90.3	91.3	93.8	91.8	-2.6	0.4	-0.5	-0.8	1.2	-2.8	91	86	96	91	0.3	0.9	0.3	0.6	8	10	0	S 3	SW 6	SSW 3
14	90.6	87.8	90.2	89.5	-2.3	0.8	0.5	-0.1	1.2	-2.7	93	81	90	88	0.4	1.3	0.6	0.8	0	0	10	S 4	S 4	SW 6
15	95.7	96.1	95.6	95.8	1.1	1.9	-0.6	0.4	2.3	-1.2	90	80	85	85	0.6	1.4	0.9	1.0	10	2	8	SW 6	SSW 9	S 6
16	92.4	92.7	90.7	91.9	-2.9	-0.5	-0.6	-1.2	0.8	-3.6	91	94	98	94	0.4	0.4	0.1	0.3	8	10	9	S 4	SW 5	S 5
17	74.6	69.9	66.3	70.3	0.0	2.5	2.7	2.0	4.4	-2.1	98	95	96	96	0.1	0.4	0.2	0.2	10	10 •	10	SW 12	SSW11	SSW 5
18	68.2	68.7	66.5	67.8	1.1	2.8	1.7	1.8	3.2	0.7	90	84	80	85	0.6	1.2	1.4	1.1	1	8	10	SW 8	SW 8	S 9
19	69.6	72.5	75.4	72.5	0.9	1.7	-0.1	0.6	1.8	-0.2	96	87	94	92	0.2	0.9	0.4	0.5	10	7	6	SW 4	S 1	SSE 2
20	76.2	76.5	74.9	75.9	-1.3	0.0	-1.3	-1.0	0.7	-1.7	96	86	95	92	0.3	0.9	0.3	0.5	10	10	10 *	SE 3	ESE 2	NE 3
21	72.4	75.1	79.7	75.7	-1.3	0.3	-0.4	-0.4	0.5	-1.7	97	94	94	95	0.2	0.3	0.3	0.3	10 *	10	10	N 2	N 1	SW 1
22	81.7	85.0	89.6	85.4	-0.5	-0.5	-2.1	-1.3	-0.3	-3.0	100	94	100	98	0.0	0.4	0.0	0.1	10 *	10	10 ≡	W 3	SW 3	S 2
23	93.5	96.1	100.7	96.8	-5.5	-1.8	-2.8	-2.7	-1.0	-4.5	97	98	95	97	0.1	0.1	0.2	0.1	10	9	10	ESE 3	ESE 3	E 2
24	103.1	104.4	104.5	104.0	-2.6	-2.8	-5.9	-4.3	-1.4	-6.1	95	97	100	97	0.2	0.1	0.0	0.1	10	10 ≡	10 ≡	ESE 1	S 1	WNW 1
25	100.7	97.5	95.1	97.8	-3.1	-0.4	-2.6	-2.2	-0.3	-6.6	97	100	98	98	0.1	0.0	0.1	0.1	10 *	10	10	NNW 1	NE 2	NE 4
26	93.4	93.2	93.7	93.4	-3.4	-2.0	-1.7	-2.2	-1.5	-6.9	97	98	96	97	0.2	0.1	0.2	0.2	10	10	10	E 2	ESE 2	ESE 4
27	94.2	95.4	94.4	94.7	-2.7	-3.2	-5.4	-3.2	-1.4	-4.1	95	92	94	94	0.2	0.3	0.3	0.3	10 *	10 *	10	E 5	SE 6	ESE 4
28	92.1	93.1	92.6	92.6	-2.0	-0.6	-1.4	-1.4	-0.5	-3.7	98	99	94	97	0.1	0.0	0.3	0.1	10	10 ≡	10	ESE 4	SE 3	SSE 2
29	89.9	88.5	88.8	89.1	-2.5	-1.2	-1.1	-1.5	-0.9	-2.8	98	95	97	97	0.1	0.3	0.2	0.2	10	10 ≡	10	ENE 2	N 1	NNW 3
30	89.2	88.2	88.1	88.5	-2.3	0.1	-2.0	-1.6	0.5	-2.5	100	96	96	97	0.0	0.3	0.2	0.2	10 * ≡	10 *	10 *	C 0	ENE 1	NE 3
31	92.1	93.6	92.9	92.9	-5.0	-9.3	-7.9	-7.3	-1.9	-10.5	93	91	93	92	0.3	0.3	0.2	0.3	10 ≡	6	10 ≡	W 1	SW 2	SW 2
M	87.9	88.5	88.9	88.4	-1.8	-0.6	-1.5	-1.4	0.7	-3.6	94	89	92	92	0.3	0.7	0.4	0.5	8.1	8.0	8.0	4.3	4.3	3.9

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1	92.0	93.7	97.7	94.5	-3.5	-2.4	-3.7	-3.3	-1.6	-8.0	97	96	83	92	0.1	0.2	0.8	0.4	10	10	4	W 5	NW 5	NW 4
2	100.8	105.2	107.3	104.4	-4.4	-2.9	-10.1	-6.9	-2.2	-10.4	86	91	87	88	0.6	0.4	0.4	0.5	10 *	7	0	NW 5	NW 6	W 4
3	102.6	100.7	101.6	101.6	-2.5	-1.7	-1.1	-1.6	-1.0	-11.3	95	98	91	94	0.4	0.1	0.5	0.3	10	10	10	W 6	WNW 8	NNW 4
4	102.0	102.9	103.5	102.8	-1.9	0.9	-4.6	-2.6	1.0	-6.1	96	94	86	92	0.2	0.4	0.6	0.4	10	10	9	NW 6	NNE 5	N 1
5	98.4	100.2	104.3	101.0	-6.5	-6.6	-11.7	-9.1	-4.5	-12.4	94	72	82	83	0.2	1.0	0.4	0.5	10 *	2	0	SE 2	SSW 2	SE 1
6	103.8	100.8	97.4	100.7	-10.3	-6.9	-5.6	-7.1	-5.6	-14.4	91	88	95	91	0.3	0.4	0.2	0.3	10	10 *	10 ≡	SW 3	WSW 4	S 3
7	98.0	96.2	83.0	92.4	-5.5	-3.3	0.4	-2.0	0.[illegible]	-5.8	97	97	96	97	0.1	0.1	0.3	0.2	10	10	10 *	S 2	WSW 5	W 8
8	81.1	82.6	90.7	84.8	-4.8	-2.3	-4.8	-4.2	0.5	-5.9	95	91	86	91	0.2	0.5	0.6	0.4	7	6	2	NNW 5	NNE 8	NNE 6
9	96.7	100.0	99.0	98.6	-6.3	-3.9	-8.8	-7.0	-3.7	-10.5	86	50	92	76	0.5	2.3	0.3	1.0	10	7	10	NNE 6	NNW 5	WSW 5
10	87.4	85.4	88.7	87.2	-4.8	-0.5	-5.2	-3.9	1.0	-9.0	93	100	95	96	0.3	0.0	0.2	0.2	10 *	10 *	0	WSW11	W 7	WNW 3
11	95.4	96.1	97.7	95.7	-5.4	-0.5	-2.8	-2.9	-0.3	-9.6	95	86	88	90	0.2	0.9	0.6	0.6	0	0	10	WNW 5	WNW 4	WSW 3
12	95.3	95.7	92.3	93.8	-0.4	0.8	0.8	0.5	1.6	-3.0	100	98	96	98	0.0	0.2	0.3	0.2	10 ≡	10 •	10	SW 3	WSW 7	WSW 7
13	81.2	76.0	69.9	75.7	0.5	1.8	0.4	0.8	1.9	0.2	98	94	92	95	0.1	0.4	0.5	0.3	10 •	10	9	SW 10	SW 10	SW 9
14	69.6	70.5	79.2	71.1	-0.5	0.3	-1.5	-0.8	0.9	-1.7	100	83	92	91	0.0	1.0	0.4	0.5	10 *	9	10	WSW10	WNW 9	W 5
15	83.7	83.0	88.7	85.8	-3.3	-2.4	-4.9	-4.4	-1.0	-7.5	90	85	83	86	0.4	0.8	0.7	0.6	2	9	9 *	WSW 3	WSW 2	NW 2
16	91.6	94.5	98.4	94.8	-10.7	-4.9	-6.0	-6.9	-3.4	-11.1	94	90	84	89	0.2	0.4	0.6	0.4	10	4	0	WSW 1	S 1	S 2
17	100.6	100.6	102.7	101.3	-11.9	-2.0	-0.6	-5.8	-0.3	-13.0	86	81	89	85	0.4	1.0	0.6	0.7	3	10	9	W 3	NNE10	NE 5
18	103.0	103.0	104.0	103.3	-2.3	-1.2	-3.1	-2.4	-0.2	-3.5	91	82	88	87	0.3	1.0	0.6	0.7	10	9	10	NE 6	N 5	NE 3
19	106.1	105.8	108.8	106.9	-4.3	-1.9	-5.8	-4.4	-1.5	-6.8	94	75	84	84	0.3	1.4	0.6	0.8	10	9	10	ENE 5	NNE 5	ENE 3
20	110.2	112.3	112.5	111.7	-4.8	-2.2	-3.3	-3.3	-1.0	-6.5	81	76	83	80	0.8	1.2	0.8	0.9	10	10	10	ENE 3	NE 2	E 1
21	107.4	103.0	96.6	102.3	-4.3	-3.6	-2.6	-3.3	-2.4	-4.8	82	83	93	86	0.8	0.8	0.3	0.6	10	10	10	WSW 2	WSW 3	WNW 6
22	93.2	93.2	96.2	94.9	-2.3	-1.8	-8.6	-5.3	-1.3	-10.1	96	69	89	85	0.3	1.7	0.4	0.8	10 *	0	0	NNE 3	E 3	WNW 3
23	93.2	92.7	96.7	94.2	-3.8	-2.2	-9.8	-6.9	-2.2	-10.6	92	81	91	88	0.3	1.0	0.3	0.5	10	10	0	WNW 3	WNW 6	NW 2
24	96.6	91.7	83.7	90.7	-13.7	-4.5	-6.4	-7.8	-4.1	-14.3	83	72	73	77	0.4	1.2	0.9	0.8	0	8	9 *	W 1	W 7	WSW10
25	83.8	84.3	86.9	83.0	-9.6	-3.4	-9.0	-8.2	-4.9	-11.2	72	62	76	70	0.8	1.3	0.7	1.0	6	6	0	WNW 4	NW 9	NW 3
26	87.6	83.9	76.4	82.6	-13.1	-6.7	-3.7	-7.8	-4.8	-13.8	80	88	93	88	0.4	0.4	0.2	0.3	0	9	10 *	C 0	SW 1	S 1
27	65.7	70.0	81.2	72.3	-2.6	-4.1	-7.3	-5.3	-2.3	-8.0	93	73	74	81	0.2	1.1	0.9	0.7	10 *	7	3	SW 5	WNW 8	NW 9
28	88.1	90.3	90.5	89.6	-10.3	-3.0	-7.8	-7.7	-4.3	-11.2	84	61	64	70	0.4	1.6	1.2	1.1	0	4	9	NW 8	W 1	SE 2
29																								
30																								
31																								
M	93.1	93.4	94.1	93.5	-5.6	-2.7	-5.0	-4.6	-1.7	-8.6	91	83	87	87	0.3	0.8	0.5	0.5	7.8	7.9	6.5	4.6	5.4	4.1

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 14{,}2\,m$ **Styczeń - Janvier 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	.	.	= 0^00 – 2^30
2	7	.	.	= 10^15 – 12^30
3	7	.	.	= 8^30 – 11^10
4	7	0.4	.	␣^1 21 – 24
5	7	1.9	1	✱^0 3^40 – 5^25 ✱^1 – 7^35 ✱^0 – 8^30 ✱^1 – 8^40 ; ≫ 3^20 – 8^15 ; ␣^1 0^00 – 3^00
6	7	.	2	
7	7	0.4	2	
8	1	2.6	3	✱^1 0^45 – 1^15 ✱^0 – 1^25 ✱^1 – 1^45 ✱^0 – 2^40 ●^0 5^40 – 6^30 ●^2 8^35 – 9^15 ●^1 – 9^40 ●^0 – 11^30 ●^0 – 13^15 , 14^10 – 20^10 , = 4^45 – 7^40 ≡^0 – 7^50 ≡^1 – 12^30 ≡^2 – 15^25 ≡^1 – 15^40 = – 20^30
9	7	2.6	pż.	✱̊^0 8^56 – 9^07 ●^2 20^35 – 21^15 ✱̊^0 – 21^40 ●^0 – 22^20 ✱^0 – 24 , = 18^20 – 24
10	7	0.1	1	✱^0 0^00 – 2^15 8^40 – 10^10 , = 0^00 – 4^30
11	6	.	2	= 8^20 – 19^30
12	6	.	2	= 5^15 – 24
13	6	.	2	= 0^00 – 3^20 7^30 – 24
14	6	0.3	2	✱^0 18^25 – 20^15 , = 0^00 – 24
15	7	.	2	= 1^30 – 2^40 4^15 – 8^40
16	6	1.0	pż.	✱^0 11^35 – 12^40 , = 14^0 – 17^15 20^30 – 24
17	6	1.5	2	✱^0 4^35 – 5^20 ●^0 11^35 – 12^20 ●^0 – 13^10 , 15^15 – 17^20 , ≫ 3^40 – 10^30 (por. 18 m/sek.) , 11^15 – 15^40 (por. 19 m/sek.) ; = 0^00 – 1^45 , 11^10 – 13^40
18	7	1.0	.	✱^1 21^15 – 22^40 ✱̊^1 23^10 – 24
19	6	.	pż.	✱̊^0 0^00 – 1^15 ●^0 – 2^05 , = 7^20 – 18^30 20^50 – 24
20	6	1.4	.	✱^0 20^15 – 24 , = 0^00 – 24
21	7	0.2	2	✱^0 0^00 – 1^10 2^20 – 4^40 5^05 – 7^35 23^45 – 24 , = 7^10 – 9^20
22	6	0.2	2	✱^0 0^00 – 1^0 3^45 – 11^15 , ≡^1 0^00 – 3^50 = 11^15 – 17^30 , 19^40 – 20^50 ≡^0 – 22^40 = – 23^35 ≡^0 – 24
23	5	0.0	2	≡^1 0^00 – 2^10 ≡^0 – 2^25 = 7^45 ≡^1 – 9^15 ≡^0 – 11^50 = – 24 ; V^0 7^45 – 13^40
24	5	0.0	2	= 0^00 – 11^50 ≡^0 – 13^30 ≡^1 – 15^20 ≡^2 – 21^30 ≡^1 23^50 = – 24 ; V^0 20^50 – 24
25	6	4.1	2	✱^0 6^40 – 10^20 , 13^15 – 17^25 , = 0^00 – 21^40 V^0 0^00 – 12^15
26	5	0.6	5	✱^0 17^35 – 20^10 , = 4^15 – 7^40 ≡^1 – 11^45 = – 24 , V^0 7^40 – 24
27	5	3.5	6	✱^0 5^15 – 11^10 ✱^1 – 12^35 ✱^0 – 15^30 , 21^40 – 24 , = 0^00 – 24 , V^0 0^00 – 6^30
28	2	0.0	9	✱^0 0^00 – 1^40 ⚠^0 10^35 – 11^10 , = 0^00 – 7^50 ≡^0 – 8^30 ≡^1 – 14^15 ≡^0 – 16^45 = – 24
29	2	0.5	9	✱^0 15^40 – 18^25 , = 0^00 – 7^45 ≡^0 – 11^35 ≡^1 – 18^10 ≡^0 – 19^55 = – 21^30
30	4	4.7	9	✱^0 6^40 – 14^20 ✱^1 – 16^40 ✱^0 – 22^50 , = 3^30 – 5^45 ≡^0 – 6^30 ≡^1 – 8^30 ≡^0 – 9^40 = – 22^10
31	6	0.2	13	≡^1 0^00 – 1^20 ≡^1 – 8^15 ≡^1 – 11^45 = – 18^50 ≡^1 – 20^50 ≡^2 – 23^50 = – 24 ; V^1 0^00 – 24
Σ	–	27.2	–	

Luty - Février

1	7	0.2	14	✱^0 3^15 – 5^15 , = 0^00 – 10^40 16^30 – 17^50 , V^1 0^00 – 1^50
2	7	1.7	14	✱^0 5^45 – 7^05 ✱̊^2 – 7^30 ✱̊^0 – 7^35 ✱̊^1 7^50 – 8^00 ✱̊^0 – 8^15 9^15 – 20 ✱̊^1 – 9^40 9^50 – 10^03 10^08 – 11^00 ✱̊^0 – 11^20 ✱̊^1 11^10 – 25
3	7	0.2	15	✱^0 3^05 – 35 13^35 – 14^05 ●^0 15^50 – 16^20 ✱^0 17^40 – 18^05 ●^0 18^10 – 20^20 , = 15^30 – 20^20
4	6	0.3	15	✱^0 13^40 – 15^05 , = 11^30 – 15^20
5	7	0.0	15	✱^0 3^45 – 7^10 = 23^15 – 24
6	6	0.3	15	✱^0 7^35 – 10^45 ✱^1 – 11^55 ✱^0 – 14^20 , = 0^00 – 2^30 13^30 – 17^45 ≡^1 – 18^50 ≡^2 – 19^30 ≡^1 – 24 ; V^1 18^50 – 24
7	5	1.7	15	●^0 18^05 – 19^25 ✱^1 19^35 – 20^05 , 21^15 – 22^50 , 23^20 – 24 , = ^1 0^00 – 2^25 ≡^0 2^50 = – 13^45 ≡^0 – 14^30 ≡^1 – 15^30 ≡^2 16^55 = – 20^10 V^1 0^00 – 11^50
8	7	2.0	17	✱^1 0^00 – 1^15 ✱̊^0 7^45 – 8^10 ✱̊^2 – 8^20 ✱̊^0 8^55 – 9^10 10^00 – 15 ✱̊^2 – 11^10 ✱̊^1 – 11^25 ✱̊^0 – 12^10 ✱̊^2 10^20 – 35 ✱̊^0 15^10 – 20 , 17^35 – 18^05 , 19^45 – 20^10
9	7	0.0	22	✱^0 1^00 – 2^20 7^10 9^35
10	6	0.4	22	✱^0 5^35 – 10^30 ✱^1 10^55 – 11^15 ✱^0 – 11^40 ✱^1 – 12^50 ✱^0 – 13^25 , ≫ 3^20 – 10^30 (por. 16 m/sek.)
11	7	0.0	24	= 22^30 – 24
12	5	0.5	24	✱^0 5^10 – 25 7^10 – 35 ●^0 12^10 – 14^20 = 15^25 – 5^45 ≡^0 – 7^20 ≡^1 – 10^40 ≡^0 – 11^05 = – 17^45 ≡^1 – 18^45 ≡^0 – 20^40 = – 24
13	6	2.6	18	●^0 3^35 – 4^10 ●̊^6 – 5^25 ●^0 – 7^35 ✱̊^0 9^40 ●^1 – 11^45 ✱̊^0 12^25 ●^0 15^25 – 17^20 ✱^0 22^40 – 24 , ≫ 3^15 – 13^40 22^50 – 24 , = 0^00 – 17^15
14	7	0.4	20	✱^0 0^00 – 3^10 ✱^1 – 6^15 ✱^0 – 8^35 ✱̊^0 10^10 – 35 9^50 – 10^20 10^45 – 11^05 11^50 – 12^05 ✱^0 17^40 – 18^10 ✱^1 – 18^20 ✱^0 . 19^40 , ≫ 0^00 – 9^20
15	7	0.1	20	✱^0 10^40 – 11^35 ✱̊^1 15^03 – 07 ✱̊^0 15^45 – 50 , 20^10 – 21^05
16	6	0.2	21	✱^0 7^05 – 20 , 8^15 – 9^10 , 17^35 – 19^10 , = 7^30 – 13^10
17	7	0.1	21	✱^0 14^10 – 15^35 ⚠^0 – 18^35 , ≫ 12^30 – 14^40 , = 1^20 – 3^40
18	7	0.0	21	✱^0 22^35 – 23^15
19	7	0.0	21	✱^0 14^40 – 15^20 , = 14^15 – 18^30
20	7	.	21	
21	6	1.0	18	= 6^30 – 19^10
22	7	0.3	20	●̊^0 1^55 – 3^45 ✱̊^0 3^55 – 4^10 ✱^1 – 6^20 ✱^0 – 7^05 ✱̊^1 9^45 – 10^10 14^02 – 10 15^40 – 55 , ≡^0 0^45 – 2^40 = – 7^10
23	7	0.7	20	✱̊^0 2^40 – 3^10 ✱̊^0 10^16 – 11^50 11^58 – 12^40 12^52 – 13^15 ✱̊^1 13^30 – 45 ✱̊^0 13^50 – 14^20 ✱̊^2 – 15^15 ✱̊^1 – 15^35
24	7	0.3	21	✱̊^0 20^40 – 22^20 , 23^45 – 24 , ≫ 20^30 – 23^15
25	7	.	22	✱̊^0 0^00 – 40 ✱̊^1 2^10 ✱̊^0 – 3^10 , ⸸^0 0^50 – 3^45 ⸸^1 3^40 – 16^30 ⸸^0 – 17^45 , ≫ 1^00 – 4^15
26	7	1.8	22	✱^0 17^10 – 24
27	7	0.4	24	✱^0 0^00 – 05 5^05 – 7^40 ✱̊^0 15^40 – 16^10 ✱̊^1 – 17^05 ✱^0 – 18^10 ✱̊^0 21^20 – 22^10 , ⸸^0 10^50 – 18^25 ⸸^1 – 19^10 ⸸^0 . 23^20 ⸸^1 – 24 , ≫ 18^15 – 20^30 , = 1^15 – 3^30
28	7	1.9	25	⸸^1 0^00 – 1^00 ⸸^0 – 7^30
29				
30				
31				
Σ	–	17.1	–	

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.8	85.0	82.2	84.7	-8.8	-6.5	-8.0	-7.8	-5.3	-9.0	89	91	90	90	0.4	0.3	0.3	0.3	10 *	10 *	10	E 4	E 3	ENE 3
2	78.5	77.0	75.6	77.0	-8.1	-3.0	-3.7	-4.6	-2.6	-10.5	92	81	92	88	0.2	0.9	0.4	0.5	10	10 *	10 *	ENE 5	NE 5	NE 5
3	71.4	68.5	68.0	69.3	-3.3	-2.1	-2.8	-2.8	-1.8	-4.3	92	92	97	94	0.4	0.4	0.1	0.3	10 *	10 *	10 *	NE 6	NNE 7	N 3
4	68.1	69.9	76.4	71.5	-2.6	-2.3	-3.3	-2.9	-1.8	-3.4	98	96	92	95	0.1	0.3	0.4	0.3	10 *	10 *	10 *	NW 5	NE 2	NW 5
5	81.9	86.1	92.1	86.7	-3.8	-1.8	-2.0	-2.4	-1.4	-4.2	89	86	96	90	0.5	0.8	0.2	0.5	10	10	10	NW 2	NNW 3	NNW 1
6	97.8	100.8	104.8	101.1	-2.8	-0.9	-8.3	-5.1	-0.9	-8.8	93	67	92	84	0.4	1.9	0.2	0.8	10	4	0	NNE 2	NE 6	NNE 3
7	107.7	108.8	108.6	108.4	-14.5	-1.7	-9.7	-8.9	-0.8	-15.6	96	63	75	78	0.1	2.0	0.7	0.9	2	0	0	N 2	NE 2	E 2
8	106.2	104.5	102.7	104.5	-19.7	-7.6	-11.5	-12.6	-4.8	-21.2	83	73	93	83	0.2	0.9	0.2	0.4	10 ≡	0	0	C 0	C 0	S 2
9	100.7	100.6	102.7	101.3	-16.8	-5.3	-3.2	-7.1	-2.1	-18.8	80	93	88	87	0.3	0.3	0.6	0.4	9	10 ≡	6	SW 1	WSW 2	NW 3
10	106.6	108.5	108.2	107.8	-4.8	-3.1	-2.7	-3.3	-0.4	-6.9	98	88	84	90	0.1	0.6	0.8	0.5	10 ≡	2	9	W 2	WSW 3	W 4
11	108.9	109.4	107.2	108.5	-1.3	0.9	-4.6	-2.4	2.8	-4.9	97	87	86	90	0.2	0.9	0.6	0.6	10	10	0	W 3	WSW 2	SW 2
12	105.6	104.9	104.0	104.8	-9.7	2.5	-1.7	-2.6	4.8	-10.6	91	58	61	70	0.3	3.1	2.1	1.8	8	6	0	SSW 1	SSW 1	SSW 2
13	103.8	103.5	103.2	103.5	-6.7	4.5	-0.6	-0.8	6.6	-7.5	96	51	77	75	0.1	4.1	1.3	1.8	0	0	0	SW 1	SE 1	SSE 1
14	101.7	100.6	99.1	100.5	-5.3	4.8	-0.3	-0.3	6.4	-5.7	100	56	82	79	0.0	3.8	1.1	1.6	0	0	0	SE 1	C 0	SSE 1
15	97.5	97.2	95.1	96.6	-5.1	5.3	3.0	1.6	5.4	-5.4	95	63	77	78	0.2	3.3	1.7	1.7	5	7	10	S 2	SSE 1	S 3
16	91.2	89.5	90.6	90.4	1.8	5.4	2.3	3.0	5.8	1.5	94	74	100	89	0.4	2.4	0.0	0.9	6	10	10 ≡	SSW 2	S 3	WSW 2
17	91.6	89.9	88.6	90.0	0.4	2.0	2.2	1.7	4.9	0.1	100	98	96	98	0.0	0.2	0.3	0.2	10 ≡	8 ≡	6	SW 3	SSE 1	C 0
18	86.5	84.6	81.7	84.3	0.2	2.4	2.8	2.0	5.1	-0.5	100	98	91	96	0.0	0.2	0.7	0.3	10 ≡	8	8	C 0	E 1	SE 2
19	79.4	81.9	88.4	83.2	1.9	2.7	1.7	2.0	4.5	1.3	93	96	80	90	0.5	0.2	1.4	0.7	10	10	8	S 3	SW 7	W 4
20	93.2	94.3	93.4	93.6	-3.0	2.3	-0.5	-0.4	2.7	-3.6	93	66	90	83	0.4	2.4	0.6	1.1	0	6	10	WSW 4	SW 3	WSW 2
21	90.0	85.5	85.3	86.9	-2.3	-0.5	-1.9	-1.6	-0.3	-2.8	100	100	98	99	0.0	0.0	0.1	0.0	10 ≡	10 *	10 *	S 1	E 2	NW 3
22	89.4	91.9	93.8	91.7	-7.9	1.1	-3.7	-3.6	2.1	-9.0	93	72	80	82	0.2	1.9	0.9	1.0	0	1	0	WNW 2	W 6	WSW 1
23	91.8	88.2	82.9	87.6	-4.5	3.9	1.0	0.4	4.6	-6.9	72	48	68	63	1.2	4.2	2.1	2.5	3	1	0	SSE 3	SE 6	SE 5
24	79.0	79.3	79.9	79.4	0.6	5.4	4.6	3.8	6.7	-0.2	92	80	98	90	0.5	1.8	0.2	0.8	10 •	0	10 ≡	SSE 3	SSE 3	SSW 2
25	80.8	85.1	90.8	85.6	2.9	1.0	0.1	1.0	4.6	-0.4	100	96	90	95	0.0	0.3	0.7	0.3	10 •	10	10	W 5	W 9	W 3
26	92.0	92.0	96.3	93.4	-0.2	0.9	0.9	0.6	2.2	-1.6	100	94	96	97	0.0	0.4	0.2	0.2	10 *	10	10	SE 2	ESE 3	ENE 4
27	104.3	107.8	109.2	107.1	-0.6	6.3	3.4	3.1	7.3	-1.7	89	65	70	75	0.6	3.3	2.4	2.1	9	2	10	N 1	SW 2	S 2
28	107.9	107.3	106.5	107.2	1.9	5.1	4.3	3.9	5.8	1.5	93	89	98	93	0.5	1.0	0.1	0.5	10 •	10	10 • ≡	S 3	SW 4	SW 2
29	106.5	106.5	103.5	105.5	3.8	8.0	6.4	6.2	11.4	2.7	100	92	91	94	0.0	0.9	0.9	0.6	10 ≡	10	0	W 3	W 5	SW 2
30	96.5	100.0	105.9	100.8	5.0	3.5	0.7	2.5	6.5	0.3	70	97	81	83	2.6	0.2	1.2	1.3	8	10	0	W 10	NNW 5	NW 2
31	103.8	103.0	105.3	104.0	0.5	7.7	1.2	2.6	7.8	0.0	88	53	85	75	0.7	4.9	1.1	2.2	2	4	0	NW 4	NNW 7	NW 4
M	93.8	93.9	94.6	94.1	-3.6	1.3	-1.1	-1.1	2.8	-5.0	92	79	87	86	0.4	1.5	0.8	0.9	7.5	6.4	5.7	2.8	3.4	2.6

Kwiecień – Avril

1	109.1	109.5	105.4	108.0	-1.4	5.6	1.5	1.8	7.5	-1.8	90	52	80	74	0.5	4.4	1.4	2.1	4	4	0	NNE 3	NNW 6	W 3
2	102.1	103.4	103.3	102.9	0.5	9.8	3.3	4.2	10.2	0.1	98	53	60	70	0.1	5.6	3.1	2.9	5	8	0	NW 5	NNW 4	ESE 1
3	97.4	96.2	92.8	95.5	0.7	1.8	1.5	1.4	3.9	0.0	98	82	92	91	0.1	1.3	0.5	0.6	10	10	0	C 0	WNW 4	WSW 4
4	90.1	90.0	91.3	90.5	0.9	8.0	3.2	3.8	8.4	0.7	98	70	79	82	0.1	3.2	1.6	1.6	10	10	0	W 3	W 5	N 2
5	95.2	97.5	97.9	96.9	-3.1	9.6	6.1	4.7	11.2	-3.9	97	60	76	78	0.1	4.8	2.2	2.4	10 ≡	1	0	SE 1	S 1	SE 2
6	97.9	95.6	91.3	94.9	1.5	12.7	8.2	7.6	13.4	-0.1	94	46	61	67	0.4	8.0	4.3	4.2	0	0	10	ESE 2	S 5	SE 4
7	88.8	91.2	91.5	90.5	5.1	6.6	3.5	4.7	8.3	3.1	89	85	91	88	1.0	1.4	0.6	1.0	10	10	10	WNW 5	WNW 5	NW 3
8	92.3	93.2	94.6	93.4	1.4	3.9	2.0	2.3	4.2	1.1	98	75	85	86	0.2	2.0	1.1	1.1	10	10	10	NNW 2	NE 3	ENE 3
9	94.6	94.7	95.7	95.0	0.7	6.7	3.4	3.6	7.5	-0.1	90	64	73	76	0.6	3.5	2.1	2.1	10	9	10	E 4	E 5	E 4
10	95.9	95.6	94.7	95.4	-0.6	3.3	2.8	2.1	5.6	-0.8	69	60	77	69	1.8	3.1	1.7	2.2	10	10	0	ESE 4	SE 5	SE 3
11	92.2	91.5	91.8	91.8	0.1	2.4	3.7	2.5	3.8	-0.9	78	77	78	78	1.4	1.7	1.8	1.6	0	10	10	SE 5	SSE 8	SE 2
12	92.6	92.7	92.2	92.5	3.2	5.8	3.0	3.8	6.6	2.5	84	73	91	83	1.2	2.5	0.7	1.5	10	10	10	SSE 2	ESE 2	SE 2
13	89.9	90.1	91.2	90.4	3.6	6.4	5.2	5.1	7.4	2.6	100	88	92	93	0.0	1.1	0.7	0.6	10 ≡	10	10	SE 3	SE 4	SE 3
14	93.5	97.4	99.3	96.7	4.3	4.3	4.5	4.5	6.0	3.6	100	97	93	97	0.0	0.3	0.5	0.3	10 •	10	10	E 1	ESE 2	E 1
15	98.9	97.5	94.9	97.1	2.7	8.8	4.0	4.9	9.7	1.8	86	62	80	76	1.0	4.3	1.6	2.3	10	9	0	SE 1	SSE 2	SE 4
16	89.7	87.2	86.3	87.8	1.6	10.7	7.1	6.6	11.3	0.2	93	52	88	78	0.6	6.3	1.2	2.7	0	3	10	SE 4	SE 6	SE 3
17	87.9	88.4	82.3	86.2	5.2	6.1	5.2	5.4	7.8	5.0	95	82	72	83	0.4	1.7	2.4	1.5	10	10	7	W 4	SW 4	SE 3
18	71.7	70.9	79.1	73.9	4.7	10.4	4.2	5.9	11.1	4.1	95	78	90	88	0.4	2.7	0.8	1.3	10 •	9	0	SE 7	S 8	SSW 2
19	82.5	82.4	82.2	82.4	2.8	8.2	5.4	5.4	8.5	1.2	98	73	94	88	0.2	3.0	0.6	1.3	10	10	10	C 0	E 2	ENE 3
20	82.6	84.1	86.1	84.3	5.8	10.2	10.4	9.2	12.3	5.1	89	67	69	75	1.0	4.0	3.9	3.0	10	10	10	E 4	ESE 6	E 4
21	86.3	84.9	83.9	85.0	8.9	11.5	7.6	8.9	12.8	7.4	77	60	94	77	2.6	5.5	0.6	2.9	7	9	10	E 4	E 5	NE 5
22	82.5	81.6	82.0	82.0	7.6	12.7	7.5	8.8	13.8	7.4	94	54	66	71	0.6	6.8	3.5	3.6	10	7	10	ENE 5	ENE 7	ENE 4
23	79.5	78.9	77.0	78.5	5.2	7.2	4.3	5.2	7.6	4.1	95	78	93	89	0.4	2.2	0.5	1.0	10 •	10	10 •	ENE 4	NNE 5	NNW 5
24	74.9	76.3	79.3	76.8	3.3	4.1	3.4	3.6	4.4	2.9	97	92	93	94	0.2	0.7	0.5	0.5	10 •	10 •	10 •	NW 5	W 5	W 6
25	82.5	84.7	86.5	84.6	4.6	7.6	5.1	5.6	9.9	3.2	93	87	94	91	0.6	1.3	0.6	0.8	10	10 •	10 •	WSW 5	SW 6	WSW 4
26	87.2	86.7	86.5	86.8	4.1	8.4	6.3	6.3	10.7	3.1	98	79	86	88	0.2	2.2	1.2	1.2	10	10	10	SW 4	WSW 4	ESE 1
27	84.9	83.8	83.4	84.0	4.9	10.1	8.4	8.0	11.5	2.5	92	64	90	82	0.7	4.6	1.0	2.1	0	10	10	E 4	E 5	ESE 2
28	84.3	83.6	83.8	83.9	7.4	12.7	11.6	10.8	13.3	6.5	91	70	60	74	0.9	4.4	5.4	3.6	10	10	10	ENE 3	E 6	ENE 6
29	86.2	88.4	92.2	88.9	7.2	9.6	7.7	8.0	11.6	7.1	94	71	90	85	0.6	3.5	1.0	1.7	10 •	10	2	E 3	SE 4	NE 3
30	94.8	95.1	96.4	95.4	6.0	14.4	5.7	8.0	15.0	2.8	91	43	68	67	0.9	9.4	3.0	4.4	2	9	0	NNE 1	NE 4	NW 3
31																								
M	89.6	89.8	89.8	89.7	3.3	8.0	5.2	5.4	9.2	2.4	92	70	82	81	0.6	3.5	1.7	1.9	7.9	8.6	6.6	3.3	4.6	3.2

Chojnice $H_s = 172\,m$ $H_b = 177.2\,m$ $h_w = 14.2\,m$ *Marzec - Mars* 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	5	0.8	29	$*^{0}1^{10}-4^{40}$ $*^{1}5^{15}-6^{45}$ $*^{0}-13^{20}$, $16^{10}-17^{35}$, $=11^{30}-20^{10}$
2	6	2.5	30	$*^{0}7^{40}$ $15^{10}-24$; $=6^{20}-24$
3	5	15.5	33	$*^{0}0^{00}-12^{15}$ $*^{1}-17^{30}$ $*^{0}-18^{35}$ $*^{1}-24$
4	5	4.2	44	$*^{1}0^{00}-14^{0}$ $*^{0}-22^{5}$ $*^{1}-10^{40}$ $*^{2}-11^{30}$ $*^{1}-12^{20}$ $*^{0}-22^{40}$ $*^{1}-23^{20}$ $*^{0}-24$
5	6	0.0	60	$*^{0}0^{00}-40$ $10^{5}-21^{5}$, $3^{10}-6^{35}$, $7^{35}-8^{10}$ $*^{1}-9^{25}$ $*^{0}-11^{20}$; $=6^{35}-13^{10}$, $17^{30}-24$
6	7	.	60	$=0^{00}-7^{20}$
7	7	0.0	60	$=4^{40}-5^{20}$ $=^{0}23^{45}-24$, $V^{0}4^{40}-11^{50}$ $V^{1}23^{45}-24$
8	6	.	57	$=^{0}0^{00}-4^{50}$ $=^{1}-5^{10}$ $=^{2}-7^{20}$ $=^{2}-9^{30}$ $=^{1}-9^{50}$ $=-24$, $V^{1}0^{00}-11^{50}$ $V^{0}21^{50}-24$
9	3	0.1	56	$*^{0}17^{40}$ 18^{10}, $=0^{00}-10^{0}$ $=^{0}-14^{0}$ $=^{0}-3^{45}$ $=-10^{40}$ $=^{1}-11^{15}$ $=^{0}-13^{35}$ $=-24$, $V^{0}10^{00}-23^{30}$ $V^{1}-11^{40}$
10	7	.	56	$=0^{00}-6^{30}$ $=^{0}-8^{50}$ $=^{1}-9^{10}$ $=^{0}-9^{50}$ $=-11^{10}$; $V^{0}6^{45}-11^{45}$
11	7	.	55	
12	6	.	55	$=5^{25}-23^{30}$
13	6	.	48	$=2^{15}-24$
14	6	.	42	$=0^{00}-4^{30}$ $=^{0}-8^{50}$ $=-24$; $V^{0}4^{40}-8^{50}$
15	5	1.7	36	$\bullet^{0}14^{15}-16^{10}$ $22^{40}-24$, $=0^{00}-24$
16	6	0.7	27	$\bullet^{0}0^{00-10}$ $14^{45}-17^{30}$ $\bullet^{2}-18^{20}$ $\bullet^{0}19^{35}-20^{20}$, $=0^{00}-16^{45}$ $=^{0}-17^{10}$ $=^{1}-17^{25}$ $=^{2}-24$
17	3	1.4	18	$\bullet^{2}22^{20}-23^{10}$, $=^{1}0^{00}-4^{30}$ $=^{2}-11^{15}$ $=^{1}-12^{35}$ $=-13^{30}$ $=-21^{40}$ $=^{0}-23^{40}$ $=^{0}-24$
18	4	.	10	$=^{0}0^{00-25}$ $=^{2}-1^{30}$ $=^{2}-9^{45}$ $=^{1}-10^{30}$ $=^{1}-11^{50}$ $=^{0}-12^{40}$ $=-24$
19	6	0.1	7	$\bullet^{0}11^{20}-12^{15}$; 17^{03-15}; $=0^{00}-19^{25}$
20	7	0.0	3	
21	5	7.3	2	$*^{0}11^{45}-12^{20}$ $*^{1}-14^{35}$ $*^{2}-17^{45}$ $*^{1}-18^{40}$; $=^{0}14^{5}-24^{0}$ $=^{1}-10^{40}$ $=-19^{30}$; $V^{0}5^{30}-10^{40}$
22	7	.	13	
23	7	0.0	7	
24	6	3.5	3	$\bullet^{0}6^{35}-7^{15}$ $\bullet^{0}7^{25}-8^{10}$ $\bullet^{0}18^{40}-20^{20}$; $=7^{30}-20^{30}$ $=^{0}-22^{15}$ $=^{1}-24$
25	7	0.7	pż.	$\bullet^{0}3^{40}-5^{15}$ $\bullet^{1}-7^{10}$ $\bullet^{0}-8^{20}$; $=^{1}0^{00}-3^{30}$ $=^{2}-5^{20}$ $=^{1}-5^{40}$ $=^{0}-6^{25}$ $=-8^{35}$
26	5	0.2	1	$*^{0}5^{07}-8^{05}$; $=3^{30}-24$
27	7	0.0	pż.	$=0^{00}-4^{05}$ $18^{30}-19^{40}$
28	6	0.5	pż.	$\bullet^{0}6^{45}-7^{35}$; $8^{55}-9^{10}$, $17^{50}-19^{15}$ $\bullet^{0}-21^{40}$; $=4^{20}-20^{40}$ $=^{0}-21^{15}$ $=^{1}-24$
29	7	0.0	pż.	$\bullet^{0}7^{10}-8^{20}$; $=^{1}0^{00}-1^{30}$ $=^{2}-9^{15}$ $=-12^{30}$; $22^{30}-24$
30	7	0.2	pż.	$\bullet^{0}12^{10-40}$ $\overset{*}{\nabla}{}^{0}14^{40}-15^{05}$; $\gg 6^{20}-9^{20}$ (por. 16 m/sek.); $=0^{00}-3^{15}$
31	7	0.0	pż.	$\overset{*}{\nabla}{}^{0}22^{40}-23^{05}$; $23^{45}-24$
Σ	-	39.4	-	

Kwiecień - Avril

1	7	.	.	$\overset{*}{\nabla}{}^{0}0^{00-07}$; $0^{35}-1^{25}$
2	7	.	.	$=20^{30}-24$
3	6	.	.	$=5^{10}-24$
4	6	0.0	.	$=0^{00}-23^{40}$ $=^{2}-24$
5	7	.	.	$=^{2}0^{00}-5^{35}$ $=^{2}-9^{40}$ $=^{1}-9^{55}$ $=-11^{20}$; $V^{0}4^{45}-9^{30}$
6	7	.	.	$\sqcup^{1}4-7$; $=4^{30}-10^{20}$
7	7	.	.	$=16^{15}-24$
8	7	.	.	$=0^{00}-2^{15}$; $4^{40}-8^{30}$
9	7	.	.	
10	7	.	.	$=18^{10}-20^{40}$
11	7	.	.	$\gg 10^{45}-12^{30}$
12	7	0.0	.	$\bullet^{0}7^{15}-8^{40}$ $\bullet^{0}-9^{10}$; $=4^{30}-12^{15}$; $18^{35}-24$
13	5	3.2	.	$=0^{00}-4^{45}$ $=^{0}-5^{15}$ $=^{1}-6^{30}$ $=^{2}-7^{15}$ $=^{1}-8^{45}$ $=-23^{45}$ $=^{1}-24$
14	6	3.5	.	$\bullet^{1}5^{15}-6^{20}$ $\bullet^{2}-7^{05}$ $\bullet^{1}-7^{30}$ $\bullet^{0}-7^{45}$ $\bullet^{1}-8^{20}$ $\bullet^{0}-9^{45}$; $10^{20}-11^{15}$; $=^{1}0^{00}-1^{40}$ $=^{2}-5^{35}$ $=^{1}-6^{45}$ $=-24$
15	7	.	.	$=0^{00}-10^{20}$
16	7	0.6	.	$\overset{*}{\nabla}{}^{0}16^{40}-17^{22}$; $19^{15}-20^{20}$ $\bullet^{0}-23^{35}$; $=2^{30}-12^{40}$; $17^{30}-23^{40}$ $=^{0}-24$; $\sqcup^{0}4-6$
17	6	1.0	.	$\bullet^{0}2^{40}-3^{10}$; $=^{1}0^{00}-3^{30}$ $=^{0}-4^{50}$ $=-14^{30}$
18	7	1.0	.	$\bullet^{0}2^{40}-5^{05}$ $\bullet^{0}-9^{40}$ $\bullet^{0}-10^{30}$ $\bullet^{0}-11^{15}$ $\overset{*}{\nabla}{}^{1}15^{04-15}$; $\gg 15^{50}-17^{20}$
19	6	1.2	.	$\overset{*}{\nabla}{}^{0}13^{35}-15^{10}$; 15^{17-55}; $=4^{30}-16^{40}$; $21^{10}-24$
20	7	.	.	$=0^{00}-2^{40}$; $4^{45}-9^{30}$
21	7	1.6	.	$\overset{*}{\nabla}{}^{15^{10-25}}$; 17^{25-33}; 19^{10-45}; 20^{20-45} $\bullet^{0}21^{15}-22^{30}$ $\bullet^{1}-24$; $=21^{30}-24$
22	7	0.8	.	$\bullet^{1}0^{00-15}$ $\bullet^{0}1^{30}-5^{45}$; $8^{35}-9^{10}$ $\overset{*}{\nabla}{}^{0}16^{25-33}$; $=0^{00}-9^{15}$
23	7	5.7	.	$\bullet^{0}4^{35}-7^{20}$; $17^{30}-18^{40}$ $\bullet^{1}-19^{30}$ $\bullet^{0}-23^{40}$ $\overset{*}{\nabla}{}^{0}16^{55}-17^{30}$; $=6^{10}-11^{30}$
24	6	1.0	.	$\bullet^{0}2^{10}-10^{45}$; $12^{40}-17^{25}$; $19^{40}-20^{20}$ $\bullet^{2}-21^{45}$ $\bullet^{0}-23^{45}$ $\bullet^{0}-24$; $=19^{45}-24$
25	7	4.2	.	$\bullet^{0}0^{00}-1^{30}$ $\bullet^{1}3^{15}-4^{40}$ $\overset{*}{\nabla}{}^{0}8^{25-40}$; $10^{55}-11^{07}$; $12^{40}-13^{05}$ $\overset{*}{\nabla}{}^{1}13^{40}-14^{02}$ $\overset{*}{\nabla}{}^{0}19^{40}-20^{46}$ $\overset{*}{\nabla}{}^{1}-21^{25}$ $\bullet^{0}-22^{10}$; $=0^{00}-2^{30}$; $3^{30}-6^{40}$
26	7	0.9	.	$\overset{*}{\nabla}{}^{0}11^{15-20}$ $\overset{*}{\nabla}{}^{1}-11^{25}$ $\overset{*}{\nabla}{}^{0}12^{26-35}$; $16^{55}-17^{03}$; $=0^{35}-11^{20}$
27	7	0.2	.	$\bullet^{0}18^{40}-19^{05}$; $22^{40}-23^{30}$; $=3^{15}-10^{35}$; $\frown^{1}4-8$
28	7	4.2	.	$\overset{*}{\nabla}{}^{0}13^{20-55}$ $\overset{*}{\nabla}{}^{1}-14^{02}$ $\overset{*}{\nabla}{}^{0}-14^{15}$; 16^{35-52}; 17^{35-43}; $22^{45}-23^{10}$ $\bullet^{0}-24$; $=4^{15}-8^{30}$
29	6	2.0	.	$\bullet^{0}0^{00}-4^{20}$ $\bullet^{1}-5^{10}$ $\bullet^{0}-6^{13}$ $\bullet^{1}-6^{20}$ $\bullet^{0}-8^{35}$; (K) $19^{40}-19^{20}$ NE-N; $=3^{30}-16^{15}$
30	7	0.0	.	$\overset{*}{\nabla}{}^{1}10^{22-30}$; $=4^{10}-5^{40}$
31				
Σ	-	31.1	-	

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA t I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.7	96.7	98.6	97.3	4.8	13.0	3.9	6.4	13.3	0.6	64	35	65	55	3.1	9.8	2.8	5.2	0	0	0	NW 3	N 6	E 1
2	100.1	99.0	99.8	99.6	3.4	9.2	2.2	4.2	10.8	-0.2	71	40	75	62	2.2	6.9	1.8	3.6	9	4	0	NE 4	N 5	ENE 3
3	100.0	99.3	99.2	99.5	0.5	8.7	3.0	3.8	9.4	-3.0	90	43	71	68	0.6	6.4	2.2	3.1	0	2	0	NE 2	E 3	E 3
4	97.4	93.8	88.7	93.3	3.3	11.5	7.4	7.4	12.5	-0.3	66	41	57	55	2.6	8.0	4.5	5.0	3	7	10	SE 4	SSE 6	SE 7
5	84.9	85.0	85.7	85.2	3.1	4.2	6.5	5.1	7.5	2.2	84	97	91	91	1.2	0.2	0.9	0.8	10 •	10 •	10	SE 4	ESE 6	ESE 3
6	86.4	87.7	90.4	88.2	5.7	11.1	7.0	7.7	11.9	5.5	97	71	91	86	0.3	3.9	0.9	1.7	10	10	10	E 2	SE 4	SW 1
7	91.9	92.8	92.1	92.3	6.6	9.0	8.2	8.0	10.7	5.8	100	83	82	88	0.0	2.0	2.0	1.3	10 •	10	10	NW 2	W 1	SE 2
8	88.6	91.5	93.9	91.3	6.3	8.2	7.0	7.1	11.2	6.0	100	96	91	96	0.0	0.5	0.9	0.5	10 •	10	2	ENE 2	NE 3	SE 1
9	88.4	84.0	73.8	82.1	9.5	12.5	7.8	9.4	13.1	5.6	99	80	83	87	0.2	2.9	1.8	1.6	10	10	9	SW 3	S 5	WSW 8
10	72.9	74.6	75.5	74.3	4.5	6.5	5.4	5.4	7.8	4.0	95	91	97	94	0.4	0.9	0.3	0.5	10 •	10	10 •	WNW 10	WNW 8	NW 3
11	84.0	90.2	96.4	90.2	5.9	11.4	7.2	7.9	12.7	4.6	97	71	87	85	0.3	3.9	1.4	1.9	10	10	0	NE 3	NNE 2	NNW 4
12	100.6	101.9	101.7	101.4	7.3	15.7	8.4	10.0	16.8	4.6	94	54	85	78	0.6	8.2	1.6	3.5	8	9	5	NW 6	NNW 5	NNW 2
13	101.3	100.6	98.5	100.1	6.9	14.5	11.3	11.0	16.8	4.6	92	55	78	75	0.7	7.5	3.0	3.7	2	6	10	WNW 3	WNW 5	WNW 4
14	95.1	93.8	93.6	94.2	10.0	13.7	9.5	10.7	14.7	8.6	88	68	99	85	1.5	5.1	0.2	2.3	9	10	10	NW 4	NW 7	NNW 3
15	94.0	93.0	91.9	93.0	5.4	13.2	5.8	7.6	13.4	3.4	86	51	70	69	1.3	7.5	2.8	3.9	10	2	10	NE 3	E 3	E 3
16	89.0	88.3	86.0	87.8	5.6	11.1	9.8	9.1	12.5	4.6	91	73	83	82	0.9	3.6	2.0	2.2	10 •	9	10	ESE 5	ESE 7	SE 2
17	85.2	84.4	81.2	83.6	10.1	15.8	15.3	14.2	19.3	9.0	90	73	78	80	1.3	4.8	3.9	3.3	10 •	8	10	W 2	SW 6	SSE 2
18	80.0	82.4	83.7	82.0	13.1	13.6	11.4	12.9	18.0	11.4	78	54	83	72	3.3	8.1	2.3	4.6	9	10	10	W 6	W 7	C 0
19	80.6	83.0	88.5	84.0	10.7	7.5	4.1	6.6	11.6	3.6	91	82	80	84	1.2	2.0	1.6	1.6	10 •	10	10	WNW 3	NW 6	NW 3
20	93.6	95.8	98.3	95.9	5.0	8.2	5.3	6.0	9.9	0.4	84	66	81	77	1.4	3.7	1.7	2.3	8	7	1	W 4	WNW 7	WSW 3
21	103.1	104.4	106.0	104.5	5.7	10.3	6.3	7.2	10.9	1.1	85	50	72	69	1.5	6.3	2.6	3.5	3	9	0	W 3	WNW 6	NNW 1
22	108.0	106.9	106.7	107.2	7.0	13.7	7.1	8.7	14.7	1.6	77	44	70	64	2.3	8.7	3.1	4.7	0	3	0	SW 1	S 1	NE 4
23	105.7	103.1	101.5	103.4	8.4	16.0	13.1	12.6	16.9	2.6	66	39	44	50	3.7	11.2	8.4	7.8	0	1	9	E 4	E 5	E 3
24	99.2	97.8	96.4	97.8	9.0	12.0	8.8	9.6	13.2	8.5	61	66	97	75	4.5	4.8	0.3	3.2	10	10	10 •	E 6	SE 4	E 2
25	95.8	96.4	97.7	96.6	8.2	10.3	9.3	9.3	10.6	7.8	97	91	97	95	0.3	1.1	0.3	0.6	10	10	10 •	E 2	NE 2	NE 2
26	96.7	95.9	94.8	95.8	9.7	14.8	10.7	11.5	15.5	8.5	91	61	92	81	1.1	6.5	1.0	2.9	10	10	10	ENE 3	NNE 2	C 0
27	92.6	92.2	93.1	92.6	9.7	16.4	12.5	12.8	17.5	8.6	83	43	74	67	2.0	10.6	3.7	5.4	10	9	8	NW 1	N 1	C 0
28	93.6	92.6	91.7	92.6	10.4	17.5	11.6	12.8	19.4	7.6	77	47	64	63	2.9	10.7	4.8	6.1	9	9	9	NNE 1	ENE 5	NE 4
29	88.9	88.5	90.6	89.3	11.3	17.6	7.1	10.8	18.3	6.9	69	43	59	57	4.2	11.4	4.2	6.6	0	10	0	N 4	NE 7	NNE 4
30	89.7	89.1	88.8	89.2	5.9	12.7	8.3	8.8	14.3	2.2	77	43	62	61	2.1	8.3	4.2	4.9	1	3	2	NW 5	NNE 3	ENE 1
31	90.2	91.3	92.2	91.2	8.2	16.1	10.5	11.3	17.3	2.1	62	38	58	53	4.2	11.4	5.3	7.0	1	7	1	ESE 4	E 2	ENE 4
M	92.7	92.8	92.8	92.8	7.1	12.2	8.1	8.9	13.6	4.5	84	61	78	74	1.7	6.0	2.5	3.4	6.8	7.7	6.3	3.5	4.5	2.7

Czerwiec – Juin

1	88.2	85.6	85.8	86.5	9.5	9.0	9.9	9.6	10.5	6.1	64	97	97	86	4.3	0.3	0.3	1.6	10 •	10 •	10	ENE 3	ENE 5	N 2
2	85.9	89.6	93.3	89.6	8.1	9.4	9.4	9.1	11.2	7.6	99	92	82	91	0.2	1.0	2.2	1.1	10 •	10 •	6	NW 3	NW 6	WNW 2
3	95.4	96.8	97.4	96.5	9.6	14.5	10.4	11.2	15.7	5.1	88	69	85	81	1.5	5.1	1.9	2.8	2	9	0	NW 2	W 1	N 2
4	98.9	98.3	98.3	98.5	10.2	18.4	11.3	12.8	19.1	4.6	82	55	69	69	2.2	9.6	4.2	5.3	0	6	5	ENE 2	SE 1	ENE 3
5	96.1	93.2	92.2	93.8	12.2	20.7	14.1	15.3	21.3	6.5	64	40	60	55	5.1	14.6	6.4	8.7	10	8	10	E 3	ENE 6	NE 4
6	90.2	88.7	89.8	89.6	14.4	20.2	13.0	15.2	20.8	8.4	64	42	61	56	6.0	13.7	5.9	8.5	0	3	0	NE 3	NE 6	NNE 2
7	90.4	89.7	90.6	90.2	11.5	18.1	12.4	13.6	20.2	6.9	82	48	72	67	2.5	10.6	4.0	5.8	2	7	1	NNW 1	NNE 1	E 2
8	92.1	91.7	91.8	91.9	12.3	22.1	16.2	16.7	22.3	6.5	70	46	56	57	4.3	14.2	8.1	8.9	0	4	0	SE 2	ESE 3	E 1
9	91.1	89.2	90.1	90.1	14.1	20.6	16.1	16.7	22.3	9.3	83	54	76	71	2.7	11.0	4.4	6.0	1	7	2	E 3	ENE 4	E 2
10	90.0	90.2	90.2	90.1	16.0	19.3	15.7	16.7	22.2	12.5	70	59	72	67	5.4	9.2	5.0	6.5	6	10	6	E 3	E 3	NNE 1
11	89.5	89.6	90.2	89.8	15.1	17.9	14.5	15.5	22.2	12.0	85	75	90	83	2.6	5.2	1.6	3.1	9	9	9	NE 2	E 1	C 0
12	90.7	91.9	93.7	92.1	13.7	16.9	11.2	13.2	18.0	11.1	84	72	73	76	2.5	5.3	3.6	3.8	9	10 •	8	NW 2	NW 6	WNW 5
13	92.5	92.7	93.5	92.9	11.1	15.5	11.7	12.5	16.5	8.8	89	65	87	80	1.5	6.2	1.8	3.2	10	10	10	WNW 4	NW 4	N 4
14	93.8	95.3	96.9	95.3	11.5	20.5	13.0	14.5	22.0	9.1	85	45	67	66	2.0	13.3	4.9	6.7	3	8	3	N 5	NE 4	E 2
15	97.9	97.1	95.1	96.7	11.7	21.0	15.9	16.3	22.0	6.5	74	43	64	60	3.6	14.3	6.5	8.1	2	6	3	C 0	SW 2	SSE 3
16	93.7	91.2	87.4	90.8	15.6	24.3	19.9	19.9	24.8	11.0	64	41	60	55	6.4	17.8	9.3	11.2	10	4	10	S 3	S 7	S 3
17	81.3	79.8	83.3	81.5	17.2	22.2	12.9	16.3	23.3	12.9	69	55	96	73	6.0	12.0	0.6	6.2	7	10	10 •	SE 7	S 8	S 4
18	88.9	91.4	87.7	89.3	11.3	16.5	13.1	13.5	17.3	10.5	95	61	93	83	0.7	7.3	1.1	3.0	10 •	10	10	W 5	W 7	SW 7
19	85.1	87.4	91.8	88.1	13.7	17.2	13.3	14.4	18.2	12.4	94	73	86	84	0.9	5.2	2.1	2.7	9	6	10	WSW 4	W 9	W 5
20	94.7	95.7	97.3	95.9	12.1	17.0	12.0	13.3	18.5	10.4	80	69	77	75	2.8	6.0	3.2	4.0	9	9	8	W 6	W 7	W 3
21	98.4	97.9	95.0	97.1	13.8	19.5	16.7	16.7	20.7	8.5	83	60	75	73	2.7	9.0	4.6	5.5	8	10	9	W 2	SSW 4	SE 2
22	90.5	88.0	85.3	87.9	15.8	23.7	18.7	19.2	26.5	12.4	78	61	86	75	3.9	11.3	3.2	6.1	10	10	10	SE 2	SE 6	NW 2
23	86.2	89.5	92.9	89.5	17.2	16.1	14.8	15.7	19.4	14.7	94	81	91	89	1.2	3.4	1.5	2.0	8	10	5	W 2	WSW 2	WSW 1
24	94.4	94.7	96.3	95.1	15.5	22.3	16.7	17.8	23.2	12.3	91	56	79	75	1.5	11.9	4.1	5.8	5	9	10	C 0	SW 5	NW 1
25	97.2	97.4	96.8	97.1	17.1	22.7	19.9	19.9	24.2	13.0	83	48	72	68	3.4	14.4	6.5	8.1	10	4	0	SW 2	W 5	SSW 1
26	95.2	93.3	97.7	95.4	19.4	27.7	17.3	20.4	28.3	14.7	74	50	68	64	5.8	18.7	6.3	10.3	0	8	10	S 2	S 5	NW 5
27	99.8	99.9	98.8	99.5	14.6	16.5	13.9	14.7	18.7	9.5	64	66	84	71	6.0	6.4	2.5	5.0	4	10	10	NW 2	SW 1	NW 1
28	101.1	102.2	100.5	101.3	12.6	14.8	11.3	12.5	17.3	8.5	80	51	80	70	2.9	8.2	2.6	4.6	7	8	1	WNW 4	WNW 6	W 1
29	95.2	97.6	99.0	97.3	12.6	15.8	11.0	12.6	16.9	10.5	92	59	83	78	1.2	7.2	2.3	3.6	10	9	1	W 9	WNW 9	WNW 4
30	97.8	96.2	90.6	94.9	11.8	19.9	16.6	16.2	21.8	6.9	84	49	70	68	2.1	11.7	5.7	6.5	6	0	4	W 6	W 6	W 1
31																								
M	92.7	92.7	93.0	92.8	13.4	18.7	14.1	15.1	20.2	9.6	80	59	77	72	3.1	9.5	3.9	5.5	6.2	7.8	6.0	3.1	4.7	2.5

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 14{,}2\,m$ **Maj - Mai 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GŁUB. ŚNIEGU h	POGODA
1	7	•	•	⌓ 1 23 – 24
2	7	•	•	⌓ 1 00 – 9
3	7	•	•	⌣ 0 2 – 3 ⌣ 2 4 – 7 ⌓ 0 21 – 24
4	7	1.3	•	⌓ 0 00 – 9
5	6	3.4	•	• 0 30 – 45, 545 – 620 • 1 – 820 • 0 – 845, 930 – 1230 • 1 – 1440 • 0 – 1530; = 845 – 2130
6	7	1.1	•	= 340 – 1010; ⌓ 0 21 – 24
7	7	7.5	•	• 0 030 – 140, 420 – 845 ∇ 0 1443 – 1502 2022 – 25 • 1 2355 – 24; = 315 – 45 = 0 – 430 = 2 – 615 = 1 – 630 = – 1030
8	6	1.7	•	• 0 004 – 435 • 1 445 – 510 • 0 – 715 1045 – 1130 • 1 – 1225; = 000 – 1730, 1935 – 24
9	7	21.3	•	• 0 310 – 440 505 – 620 1345 – 1504 • 1 – 1737 • 2 – 1748 • 1 – 1845 • 0 – 2015 2240 – 2330 • 1 – 24, ⚲ 2130 – 24; = 115 – 1220
10	7	5.0	•	• 1 000 – 40 • 0 – 415 • 1 – 925 • 0 – 1210 ∇ 0 1214 – 47 1355 – 1407 1551 – 1617 1740 – 1915 • 0 – 2140 • 0 – 2310; ⚲ 000 – 715
11	7	0.1	•	= 025 – 610
12	7	0.3	•	• 0 310 – 420 ∇ 0 1814 – 30 ∇ 1 – 1833 ∇ 0 – 1830; = 215 – 740
13	7	•	•	= 0 140 – 245 = – 715
14	7	0.6	•	∇ 0 1410 – 1530 • 0 – 1640 1745 – 1830; = 225 – 540 1930 – 24
15	7	0.5	•	∇ 0 2340 – 24; = 000 – 630
16	7	3.9	•	∇ 0 000 – 130 • 0 – 240 615 – 735 • 1 – 810 • 0 – 915 1950 – 2007
17	6	1.4	•	• 0 627 – 720 ∇ 0 1615 – 30; = 140 – 1330 1915 – 24
18	7	0.0	•	∇ 0 115 – 20 240 – 330 1756 – 1804; = 000 – 530; ⌓ 0 20 – 24
19	7	0.0	•	• 0 150 – 240 635 – 715; = 130 – 940; ⌓ 0 00 – 1
20	7	0.2	•	▲ 0 850 – 54 ∇ 0 1052 – 55 1135 – 39 ▲ 0 – 1144 ∇ 0 – 1147 ▲ 0 1450 – 54 ∇ 0 – 1502 1942 – 45; ⌓ 0 1 – 3 ⌓ 0 zm. 4 – 6 ⌓ 0 7 – 9
21	7	0.7	•	▲ 0 826 – 31 ∇ 1 850 – 56 ▲ 1 – 903 ∇ 0 1048 – 56; ⌓ 1 1 – 3 ⌓ 1 zm. 4 – 5 ⌓ 1 6 – 8 ⌓ 0 21 – 24
22	7	•	•	⌓ 1 000 – 3 ⌓ 1 zm. 4 – 6 ⌓ 1 7 – 8
23	7	•	•	
24	7	1.8	•	• 0 715 – 25 845 – 935 ∇ 0 1652 – 1740 ∇ 1 – 1830 • 0 1840 – 24
25	7	0.0	•	• 0 000 – 30 • 1 715 – 330 • 0 – 440 1535 – 1715 1840 – 2105; = 100 – 240 = 0 – 350 = – 1230 1610 – 24
26	7	0.3	•	• 0 2120 – 24; = 000 – 830 2015 – 24
27	7	•	•	• 0 000 – 40 410 – 30; ⌓ 0 22 – 24
28	7	0.0	•	∇ 0 1321 – 25; = 230 – 415; ⌓ 0 000 – 2 ⌓ 1 3 – 8
29	7	•	•	⌓ 0 23 – 24
30	7	•	•	⌓ 0 000 – 10, 20 – 24
31	7	0.0	•	⌓ 0 000 – 3 ⌓ 1 4 – 8
Σ	–	51.1	–	

Czerwiec - Juin

1	6	12.1	•	• 0 635 – 815 • 1 – 935 • 0 – 1240 • 1 – 1430 • 0 – 1535 • 0 – 1605 • 1 – 1620 • 0 – 1830; = 645 – 24
2	6	2.2	•	• 0 015 – 240 435 – 720 • 0 – 930 1013 – 1410; = 000 – 1250
3	7	•	•	= 230 – 615; ⌓ 2 22 – 24
4	7	•	•	= 130 – 610; ⌓ 2 000 – 6 ⌓ 1 7 – 9 ⌓ 0 23 – 24
5	7	•	•	⌓ 0 000 – 8
6	7	•	•	
7	7	2.4	•	∇ 2 1038 – 48 ∇ 0 – 1103; ⌓ 1 2 – 8
8	7	•	•	
9	7	•	•	⌓ 0 3 – 9
10	7	•	•	⌓ 0 2 – 9
11	7	2.5	•	∇ 1 1225 – 42 1313 – 20 1610 – 25 ∇ 2 – 1639 ∇ 0 – 1640 ∇ 2 1645 – 52
12	7	0.0	•	∇ 0 405 – 09 1245 – 50 1315 – 25
13	7	0.8	•	∇ 1 1528 – 32 2140 – 2220 • 0 2340 – 24; = 610 – 730
14	7	•	•	• 0 000 – 20; = 215 – 630
15	7	•	•	
16	7	•	•	= 2030 – 24
17	7	6.8	•	∇ 0 1715 – 25 ∇ 1 – 1735 ∇ 0 – 1745 ∇ 1 – 1815 ∇ 0 – 2020 • 0 – 2110; = 2100 – 2225
18	7	9.5	•	• 0 345 – 535 • 0 – 627 • 0 – 720 ∇ 0 1640 – 1707 1835 – 2035 • 0 2115 – 24; = 2040 – 24
19	7	3.5	•	• 0 000 – 27 • 0 1442 – 551 ∇ 2 – 1 625 • 0 – 638 1030 – 37 1140 – 48 1205 – 13 1306 – 15 1405 – 15 ∇ 2 1715 – 18 ∇ 0 – 1725 1745 – 52 1825 – 40 1935 – 42 ∇ 1 2025 – 40; (K) 0 1350 – 1352 – 1420 NW-NE;
20	7	•	•	∇ 0 152 – 215; ⌓ 1 22 – 24 [19.VI: ⚲ 530 – 620; = 000 – 640
21	7	•	•	= 1935 – 24; ⌓ 2 000 – 7 ⌓ 0 8 – 9, 21 – 24
22	7	12.3	•	∇ 0 1705 – 15 1902 – 20, 2130 – 35 ∇ 1 2142 – 2210 ∇ 1 – 2225 ∇ 0 – 2240 2310 – 20 K 0 NW 1540 – 1650 – 1730 NE K 0 S 1830 – 2030 NW K 1 E 2130 – 2158 – 24 W; = 220 – 1030 1920 – 24, ⌓ 0 000 – 8
23	6	0.1	•	∇ 0 835 – 41 1115 – 28 1325 – 43 1403 – 10, K 1000 – 15 W; = 000 – 30 232 – 615 815 – 1820 2130 – 24, ⌓ 1 22 – 24
24	7	0.2	•	= 000 – 730 840 – 1245 1920 – 24, ⌓ 1 000 – 1 ⌓ 2 2 – 8 ⌓ 0 21 – 22 ⌓ 1 23 – 24
25	7	•	•	∇ 0 404 – 06 ∇ 1 – 409 ∇ 0 – 455; = 000 – 715 1930 – 24; ⌓ 1 20 – 24
26	6	0.0	•	∇ 0 1512 – 20, (K) 0 1414 – 1630 N-NE; = 000 – 100 330 – 1535 1725 – 2230; ⌓ 2 000 – 7 ⌓ 1 21 – 24
27	7	•	•	⌓ 1 000 – 7, 21 – 24
28	7	•	•	⌓ 1 000 – 8 ⌓ 0 21 – 24
29	7	0.0	•	• 1 730 – 57; ⚲ 1130 – 1245; ⌓ 0 000 – 7
30	7	0.1	•	⌓ 0 2 – 4 ⌓ 2 5 – 8 ⌓ 1 21 – 24
31				
Σ	–	52.5	–	

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$ *Lipiec – Juillet* 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	87.9	90.4	92.5	90.3	12.4	17.0	9.7	12.2	17.5	9.4	90	40	75	68	1.4	11.7	2.9	5.3	10	9	0	WNW 5	WNW 7	WNW 3
2	91.2	89.4	86.5	89.0	11.5	15.4	11.4	12.4	16.4	4.8	82	46	82	70	2.5	9.5	2.5	4.8	1	9	10 •	W 1	W 6	WSW 6
3	84.9	85.9	86.7	85.8	10.5	14.2	8.9	10.6	15.3	8.3	76	55	93	75	5.0	7.3	0.8	3.7	8	7	8 •	WSW 7	SW 8	W 3
4	87.0	86.6	87.5	87.0	9.2	13.8	10.0	10.8	15.5	6.5	91	62	91	81	1.1	6.1	1.1	2.8	4	9	4	WSW 3	WSW 7	C 0
5	87.9	87.8	88.6	88.1	10.3	13.7	10.0	11.0	15.6	6.0	92	62	86	80	0.9	6.0	1.8	2.9	9	9 •	5	WSW 1	WNW 5	C 0
6	88.0	87.1	89.1	88.1	9.5	12.6	9.2	10.1	15.7	5.7	83	72	96	84	2.1	4.1	0.4	2.2	6	10	6	WSW 6	SW 6	SW 2
7	89.8	88.4	87.1	88.4	10.1	14.2	11.4	11.8	15.7	7.0	92	81	95	89	1.0	3.1	0.7	1.6	9	10	10	WSW 2	SW 3	C 0
8	85.6	80.8	77.9	81.4	12.2	15.9	13.9	14.0	17.4	8.2	95	83	94	91	0.7	3.1	0.9	1.6	10	10	10	WSW 1	SE 3	WSW 2
9	80.8	85.4	87.0	83.7	9.9	14.0	10.6	11.3	14.8	9.3	78	58	91	76	2.7	6.7	1.2	3.5	6	9	9	SW 9	W 9	W 5
10	90.3	91.8	94.7	92.3	9.9	14.6	10.6	11.4	15.9	6.9	84	55	87	75	1.9	7.5	1.6	3.7	5	6	7	W 5	WSW 6	C 0
11	96.4	96.9	95.8	96.4	11.5	15.2	14.2	13.8	17.9	8.7	84	54	75	71	2.2	8.0	4.1	4.8	1	9	10	W 2	W 5	SSE 2
12	91.1	88.4	89.6	89.7	14.5	17.4	12.1	14.0	17.6	12.0	85	82	98	88	2.5	5.6	0.3	2.1	10	10 •	2	S 6	SSW 6	W 2
13	92.6	92.5	92.6	92.6	12.3	19.2	17.2	16.5	21.3	9.0	92	64	89	82	1.2	7.9	2.2	3.8	3	8	4	NW 2	SW 5	S 1
14	94.0	94.5	94.6	94.4	18.1	27.3	17.3	20.0	28.4	14.4	93	44	94	77	1.5	20.3	1.2	7.7	1	7	10	C 0	SW 3	ESE 4
15	96.6	97.3	96.6	96.8	17.3	25.3	21.8	21.6	27.5	15.5	96	65	88	83	0.8	11.2	3.3	5.1	8	8	10	WNW 3	WSW 2	C 0
16	97.9	97.0	97.8	97.6	17.1	20.7	15.7	17.3	21.8	13.6	99	80	95	91	0.2	4.9	0.9	2.0	10	10	10	W 2	NE 5	N 4
17	96.2	95.6	96.3	96.0	14.4	16.7	14.5	15.0	17.0	13.8	95	89	79	88	0.7	2.2	3.4	2.1	10	10	10	NE 3	N 5	NE 4
18	96.7	97.4	99.4	97.8	14.9	20.6	14.3	16.0	21.0	12.0	77	58	73	70	3.8	10.1	4.1	6.0	3	6	1	NE 4	NE 6	NNE 1
19	100.7	100.8	101.0	100.8	14.0	23.2	17.4	18.0	24.3	8.4	83	46	75	68	2.7	15.4	4.9	7.7	0	3	0	NNE 2	SE 2	NE 1
20	101.1	99.1	96.1	98.8	16.3	23.1	18.3	19.0	24.1	12.5	72	42	64	59	5.1	16.4	7.5	9.7	0	1	0	E 1	SE 6	NE 2
21	93.2	90.0	87.5	90.2	14.6	23.0	16.7	17.8	24.4	12.5	78	52	97	76	3.6	13.5	0.6	5.9	4	7	10 • K	ENE 4	E 6	SE 2
22	87.1	88.4	88.6	88.0	16.0	20.6	16.3	17.3	22.0	15.2	98	64	87	83	0.4	8.7	2.5	3.9	10	6	1	SW 2	W 5	C 0
23	87.4	85.7	86.1	86.4	15.2	17.3	13.9	15.1	22.1	12.5	99	88	94	94	0.2	2.4	0.9	1.2	10	10 • K	2	C 0	SW 4	W 2
24	84.2	85.4	88.7	86.1	13.8	19.5	12.0	14.3	20.5	10.5	97	60	98	85	0.6	9.0	0.3	3.3	8	6	10 •	S 2	WSW 9	WNW 1
25	89.2	89.1	88.8	89.0	13.3	19.8	12.5	14.5	20.7	9.7	86	50	94	77	2.1	11.5	0.9	4.8	0	8	10	WSW 2	SW 7	C 0
26	87.7	86.8	85.3	86.6	12.1	16.9	12.8	13.6	18.0	10.3	90	64	91	82	1.4	7.0	1.4	3.3	9	9	10 •	W 3	SW 7	SW 5
27	85.7	88.1	87.4	87.1	10.8	11.9	11.9	11.6	14.9	9.9	91	77	88	85	1.2	3.1	1.7	2.0	10	10	10	W 9	W 9	WSW 3
28	87.9	88.4	87.6	88.0	10.4	14.8	11.2	11.9	16.0	8.5	88	54	95	79	1.4	7.7	0.7	3.3	9	9	9	W 7	W 9	W 3
29	85.4	82.2	77.3	81.0	12.5	14.3	12.9	13.2	16.3	10.6	98	97	94	96	0.4	0.6	0.9	0.6	10	10 •	10 •	SW 3	W 3	SSW 3
30	73.3	73.6	76.0	74.3	12.8	15.2	12.5	13.2	17.7	12.2	98	81	94	91	0.4	3.4	0.9	1.6	10 •	9	10	WSW 5	SW 7	WNW 9
31	79.4	79.4	82.7	80.5	10.3	14.5	10.4	11.4	15.9	9.2	87	57	95	80	1.6	7.1	0.6	3.1	7	10	9	W 9	WSW 6	C 0
M	89.5	89.3	89.5	89.4	12.8	17.5	13.3	14.2	18.9	10.1	89	64	89	81	1.7	7.7	1.8	3.7	6.5	8.2	7.0	3.6	5.7	2.3

Sierpień – Août

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	87.0	88.2	89.3	88.2	10.1	16.3	11.5	12.4	17.5	6.0	88	47	78	71	1.5	9.8	3.0	4.8	0	7	6	WSW 2	WSW 4	W 1
2	88.3	87.2	87.8	87.8	10.8	17.4	10.5	12.3	18.4	7.2	86	56	95	79	1.8	8.8	0.7	3.8	2	8 (K)	5	C 0	WNW 3	C 0
3	86.7	86.7	88.4	87.3	10.0	16.6	11.1	12.2	19.2	6.1	92	62	89	81	1.0	7.1	1.5	3.2	1	8	2	SW 2	W 2	C 0
4	89.1	90.8	94.2	91.4	12.7	13.5	11.1	12.1	17.8	10.2	95	94	89	93	0.7	0.9	1.5	1.0	10	10 • K	5	SW 1	W 2	W 1
5	96.7	97.8	97.5	97.3	11.4	17.4	14.7	14.6	19.8	7.5	93	56	78	76	1.0	8.8	3.6	4.5	2	7	2	W 3	W 3	C 0
6	94.0	91.7	92.4	92.7	15.3	25.6	18.0	19.2	26.4	12.0	85	58	92	78	2.6	13.9	1.6	6.0	10	10	10	SW 3	S 6	N 1
7	91.6	90.3	92.0	91.3	16.8	21.2	17.1	18.0	21.5	15.5	99	86	94	93	0.2	3.7	1.2	1.7	10 ≡	10 •	10	S 2	SW 3	W 3
8	94.4	95.1	93.3	94.3	14.4	15.0	13.8	14.2	17.1	13.0	85	85	98	89	2.5	2.5	0.4	1.8	9	10 •	10	C 0	C 0	C 0
9	96.4	97.5	99.4	97.8	12.2	16.3	10.1	12.2	17.7	9.9	94	73	90	86	0.9	4.9	1.3	2.4	10	6	2	NW 3	NW 4	C 0
10	100.1	100.4	101.2	100.6	10.0	15.6	9.7	11.2	17.0	6.0	99	60	89	83	0.2	7.1	1.2	2.8	10	6	10	W 2	W 3	C 0
11	100.6	100.8	101.7	101.0	10.6	16.1	9.5	11.4	17.4	6.1	97	76	91	88	0.4	4.4	1.1	2.0	9	10	0	NW 2	NW 3	NW 2
12	101.6	101.1	101.5	101.4	10.5	17.1	10.1	12.0	18.0	7.4	100	57	85	81	0.0	8.3	2.0	3.4	10	6	0	NW 1	N 2	N 2
13	100.6	100.0	100.2	100.3	10.8	15.4	11.1	12.1	17.7	6.5	92	56	80	76	1.0	7.7	2.6	3.8	7	6	3	NNW 3	NW 4	NW 1
14	98.8	98.4	98.4	98.5	11.1	14.0	10.4	11.5	14.9	8.1	89	71	95	85	1.5	4.6	0.6	2.2	9	10	10	NW 2	NW 3	NW 2
15	99.3	100.0	100.4	99.9	11.1	15.3	12.4	12.8	16.5	10.2	95	70	92	86	0.7	5.3	1.2	2.4	9	7	9	NW 1	NW 2	C 0
16	99.9	99.4	97.8	99.0	9.7	16.5	12.3	12.7	18.2	6.9	100	59	82	80	0.0	7.7	2.5	3.4	6	10	0	C 0	NW 1	C 0
17	97.3	97.3	97.1	97.2	12.2	19.9	13.6	14.8	21.0	8.9	93	53	85	77	1.0	11.0	2.3	4.8	1	7	0	C 0	W 2	C 0
18	97.8	98.6	98.6	98.3	12.4	22.1	15.4	16.3	23.4	9.7	94	47	84	75	0.9	14.1	2.8	5.9	4	4	0	E 1	C 0	C 0
19	100.3	101.3	101.1	101.0	12.8	24.0	17.6	18.0	24.8	10.8	99	42	81	74	0.2	17.2	3.8	7.1	6	10	2	C 0	SW 1	N 1
20	100.1	98.7	96.2	98.3	16.5	25.2	18.6	19.7	25.3	13.6	83	50	67	69	3.3	16.0	6.6	8.6	10	10	0	SSE 1	S 5	SE 3
21	92.6	91.4	89.3	91.1	14.4	23.0	17.3	18.0	23.4	12.7	80	62	85	76	3.2	10.6	2.9	5.6	10	8	0	SE 2	SW 8	C 0
22	87.2	85.2	84.2	85.5	16.2	26.3	20.2	20.7	27.2	14.2	88	44	58	63	2.1	19.1	10.0	10.4	0	10	0	ESE 2	SE 6	E 3
23	84.5	84.5	84.1	84.4	16.5	26.3	21.6	21.5	27.5	15.2	78	47	62	62	4.3	18.2	9.9	10.8	0	0	5	E 2	SE 6	E 3
24	87.0	88.0	87.4	87.5	16.0	21.5	17.3	18.0	22.3	15.3	96	74	97	89	0.8	6.7	0.6	2.7	5	10	10 •	C 0	C 0	C 0
25	84.6	84.8	88.3	85.9	15.1	15.9	13.1	14.3	17.3	13.0	99	91	94	95	0.2	1.6	0.9	0.9	10	10	10 •	N 2	NW 5	W 1
26	91.4	92.5	93.1	92.3	10.2	15.1	11.4	12.0	17.0	9.8	97	60	91	83	0.3	6.8	1.2	2.8	9	8	7	WNW 3	NW 4	C 0
27	90.9	89.7	90.3	90.3	10.4	13.5	8.9	10.4	15.4	8.8	93	83	100	92	0.8	2.7	0.0	1.2	10	10	1	C 0	NW 4	C 0
28	91.0	92.4	94.4	92.6	9.5	14.6	11.4	11.7	17.2	6.3	100	72	89	87	0.0	4.6	1.5	2.0	3	8	2	W 2	W 3	WNW 1
29	92.9	91.0	90.7	91.5	8.5	17.1	11.2	12.0	17.4	6.2	99	54	96	83	0.2	9.0	0.3	3.2	3	9	0	W 1	SW 7	W 1
30	91.5	92.4	93.8	92.6	9.8	14.8	9.4	10.8	16.9	7.7	97	61	91	83	0.3	6.5	1.1	2.6	0	6	4	WSW 2	W 4	C 0
31	94.0	93.1	91.7	92.9	7.7	16.2	11.4	11.7	17.3	5.6	100	59	83	81	0.0	7.6	2.3	3.3	10 ≡	5	0	C 0	WSW 2	C 0
M	93.8	93.8	94.1	93.9	12.1	18.2	13.3	14.2	19.6	9.6	93	63	87	81	1.1	8.3	2.3	3.9	6.3	7.9	4.0	1.5	3.2	0.8

Chojnice — $H_s = 172\,m$ — $H_b = 177{,}2\,m$ — $h_w = 12{,}5\,m$ — Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	7	.	.	●° 4^45–5^05, ⌓ ¹0^00–4 ⌓ °20–24
2	7	0.4	.	▽°20^15–21^20; ⌓ ²0^00–6 ⌓ ¹7–8 ⌓ °9–10
3	7	2.2	.	▽°0^30–1^20, 13^25–40, 17^52–18^04 ▽¹19^45–20^10, 20^45–21^05
4	7	0.2	.	▽°14^10–18, 16^30–35, 16^45–17^05
5	7	0.0	.	▽°12^48–13^05, 13^40–14^01; ⌓ ¹1–8, 21–24
6	7	1.7	.	▽°8^25–9^15, 11^20–32, 11^55–12^07, 14^15, 15^03, 19^40–45; = 0^30–3^15; ⌓ ¹0^00–8
7	6	5.5	.	▽°1^40–2^10 ●°9^45–10^30, 11^15 ▽°14^01–25 ▽¹–14^35 ▽²–14^45 ▽¹–15^05 ▽°–15^05 ▽¹16^50–19^05 ▽°–19^15, ☒°14^50–15^05 SW-E ☒°18^55–19^10 W-SE; = 11^15–24
8	7	3.9	.	▽° 9^31–10^40 ▽¹–11^25 ▽°14^52–15^02 ▽¹–15^48 ▽°–16^10 ●°–18^08; = 3^10–7^45, 20^40–24
9	7	2.8	.	▽°15^23–38 ▽²16^15–22 ▽°16^35–17^04, 19^25–35; = 0^00–30
10	7	0.0	.	▽°13^35–43
11	7	.	.	= 3^15–7^35; ⌓ ¹0^00–9
12	6	11.4	.	●°7^10–10^15 ▽°12^45–13^12 14^02–14 ▽¹14^25–45 ▽°–15^50, 16^10–22 ▽¹17^40–18^05 ▽°–18^10; = 2^30–11^30, 21^35–23^10
13	7	.	.	= 0^00–6^10, 19^15–24; ⌓ ¹23–24
14	7	24.6	.	▽²17^28–40 ▽°–18^10 ▽²–18^50 ▲²▽²–19^05 ▽² 19^20 ▽¹–20^15 23^45–24; ☒°16^55–☒²18^30–19^15–☒°20^30 W-NE ☒°NE 23^50–24; = 0^00–7^40, ⌓ ²0^00–7 ⌓ ¹8–9
15	7	28.0	.	▽²0^00–20 ▽°–21^5, ☒°NE 0^00–30 NW ☒°S 22^50–24; = 3^30–7^40
16	7	0.0	.	▽°0^50–1^04 ▽²–1^20 ▽¹–1^45 ▽²–1^50 ▽°–3^10 ▽²–3^30 ▽°–3^40, 7^28–32 ●°8^45–9^05, ☒°0^00–1^15–3^45 NE; = 17^40–24
17	7	.	.	= 0^00–1^40, 5^30–9^15
18	7	.	.	⌓ ¹22–24
19	7	.	.	⌓ ²0^00–10 ⌓ ¹21–24
20	7	.	.	⌓ ²8^00–8 ⌓ °9–11
21	7	11.3	.	▽°19^05–15 ▽¹–20^10 ▲°20^25–28 ▽°–21^41 ▽¹21^45–22^10 ▽°–24; ☒°E 18^50–19^20–21^45 NW; = 22^25–24; ⌓ ²0^00–5 ⌓ 6–9
22	7	0.3	.	▽°0^00–50 1^55–2^20 ●°3^10–6^15 ▽°11^15–28 ▽°17^37–40; = 0^00–9^10
23	6	6.8	.	▽°12^04–27 ▽²–12^40 ▽°–13^25 ▽²–13^30 ▽°–13^50 ▽²–13^56 ▽¹–14^40 15^45–16^05 ☒°12^25–14^40; = 1^15–2^45 ≡¹–5^55 =–9^15, 20^35–24
24	7	2.2	.	▽°4^48–5^03 5^40–57 ▽¹–6^11 ▽°15^17–21 ▽°16^02–04 ▽°–16^10, 17^58–18^20, 20^45–21^10; ☒°W 17^55–18^04–18^25 E; = 0^00–8^40, 18^10–22^30
25	7	1.0	.	▽°18^10–45, 21^15–35
26	6	5.2	.	▽°13^13–18 ▽²13^20–45 ▽¹16^20–50 ▽°–17^05, 20^45–21^15, 22^25–23^35; = 2^30–7^40
27	7	4.3	.	▽°8^20–35, 9^43–55, 10^18–30 ▽¹–10^35 ▽°–11^04, 21^15–22^20
28	7	1.7	.	▽°5^50–6^10, 16^40–17^35 ●°–20^15, ≫ 12^55–15^10
29	6	6.4	.	●°2^05–5^20 ●°–8^30, 8^45–9^10, 9^25, 10^20 ●°11^25–13^10 ▽°16^50–19^05, 20^45–21^15; = 2^20–15^30
30	7	2.9	.	▽°5^50–6^10 ▽¹6^25–7^05 ▽°10^52–11^32, 17^35–42 ▽¹–18^05 ▽°–18^12, 18^47–55, 19^10–17, 19^25–36, 21^50–23^20; ☒°NW 13^50–13^55–14^35; = 23^5–8^40
31	7	.	.	▽°12^0–35; ⌓ ¹21–24
Σ	–	122.8	–	

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1	7	.	.	⌓ ²0^00–10
2	7	1.0	.	▽°13^15–25 14^49–57 15^38–50; (☒) N 11^50–14^35 E; ⌓ °20–22 ⌓ ²23–24; ⌒ 15^48–16^13
3	7	2.2	.	▽¹12^05–08 ▽²–12^24 13^15–22 16^40–44, ⌓ ²0^00–9 ⌓ °10–11
4	6	8.8	.	▽°5^44–46 ●°7^40–8^35 ▽°12^10–15 12^25–35 ▽¹–12^45 ▽°–13^05 ▽²–13^15 ▽°–14^10 ▽°14^20–25, 15^10–35; ☒°11^55–12^40–13^30 NW-E ☒°15^15–25–40 W-NW; = 5^25–10^30
5	7	.	.	⌓ ¹20–22 ⌓ ²23–24
6	7	3.9	.	☒°NW 17^55–18^05–18^40 NE; = 1^00–5^30 20^50–24; ⌓ ²0^00–7 ⌓ °8–10
7	6	0.4	.	▽¹0^25–1^35 10^43–54 ▽°11^47–12^10 12^45–13^15 15^48–16^10 ●°17^40–18^20 20^15; ☒°SW 0^10–1^40 N; = 0^00–6^40 ≡°–7^50 =–16^30, 22^30–24
8	6	6.8	.	●°4^35–5^25 ▽°10^50–13^15 ●¹–14^30 ●°–15^05 ●²–15^20 ●°–15^35–17^05; = 0^00–8^30, 18^15–24
9	7	0.0	.	●°1^45–2^40 ●²3^15–4^50 ▽°10^50–11^20; = 0^00–9^15
10	7	.	.	⌓ ²0–8 ⌓ °9–11
11	7	1.1	.	▽°11^26–12^04, ⌓ °20–22 ⌓ ²23–24
12	7	0.0	.	●°6^10–45 ▽°15^28–35, 16^10–20; = 2^30–3^30 ≡°–3^45 ≡¹–6^05 ≡°–6^15 =–8^30; ⌓ ²0^00–7 ⌓ ¹8–9 ⌓ °10–11 ⌓ ¹22–24
13	7	.	.	⌓ ¹0^00–2 ⌓ ²3–8 ⌓ ¹9–11 ⌓ °20–24
14	7	0.4	.	▽°16^02–06 17^37–16^01 18^15–30, ⌓ ²0^00–11
15	7	0.1	.	●°0^45–1^30 ●²4^20–5^40 ●°6^10–45 ▽°10^45–11^02 ▽¹12^01–17; = 3^45–6^30, ⌓ ²22–24
16	7	.	.	≡¹1^40–3^30 ≡°–5^50, ⌓ ²0^00–1 ⌓ ¹20–21 ⌓ ²22–24
17	7	.	.	⌓ ²0^00–10 ⌓ ¹20–22 ⌓ ²23–24
18	7	.	.	⌓ ²0^00–9, 20–24
19	7	.	.	= 6^20–7^40, ⌓ ²0^00–9 ⌓ °10–11 ⌓ ¹20–22 ⌓ ²23–24
20	7	.	.	= 3^15–10^40, ⌓ ²0^00–9 ⌓ °10–11, 20–22 ⌓ ¹23–24
21	6	.	.	= 7^30–24, ⌓ ¹0^00–8 ⌓ °9–10 ⌓ ²21–24
22	7	.	.	= 0^00–8^15, ⌓ ²0^00–8 ⌓ °9–10
23	7	1.0	.	☾ S 21^15–22^30; = 18^45–24
24	7	14.6	.	▽°1^40–3^30 ▽¹20^35–21^07 ▽°22^45–24; = 0^00–30 3^30–12^40 20^05–24
25	7	12.6	.	▽¹0^00–2^20, 2^35–3^10, 3^20–4^05 ●°–6^20, 7^20–8^40, 13^15–24; = 0^00–6^45 8^40–10^30 13^30–24
26	7	.	.	●°0^00–1^40; = 0^00–4^15, ⌓ ¹20–22 ⌓ ²23–24
27	7	2.4	.	▽°12^57–13^40 ▽²15^09–20 ▽°–15^25, 16^28–42, 17^20–34 ▽¹–17^40 ▽°–17^52; = 8^20–9^30, 21^30–24; ⌓ ²0^00–10
28	7	.	.	= 0^00–7^30, ⌓ ¹21–24
29	7	1.1	.	▽°17^10–18^05 ▽¹–18^45; = 18^40–24; ⌓ ²0^00–9 ⌓ ¹10–11
30	7	0.0	.	= 0^00–8^40; ⌓ ¹20–24
31	7	.	.	
Σ	–	56.4	–	

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$ *Wrzesień — Septembre 1965*

DNI	CIŚNIENIE P= 900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	90.4	91.6	95.0	92.3	10.4	18.9	15.0	14.8	19.6	8.7	91	59	81	77	1.1	9.0	3.3	4.5	9	7	10	E 2	E 5	NE 2
2	97.1	98.2	96.8	97.4	12.4	18.8	15.9	15.8	20.8	12.0	98	79	88	88	0.4	4.5	2.1	2.3	10 •	8	4	NE 2	E 5	NE 5
3	92.0	89.0	88.6	89.9	15.3	25.7	18.9	19.7	26.3	13.5	90	56	85	76	1.7	14.6	3.7	6.7	9	8	10	NE 4	SSE 5	C 0
4	87.2	88.3	87.3	87.6	14.7	16.9	15.7	15.8	19.0	13.0	96	89	89	91	0.7	2.1	1.9	1.6	10	10	10	NW 3	NW 2	NW 2
5	87.4	88.3	87.8	87.8	12.7	15.5	12.7	13.4	17.4	12.4	98	80	99	92	0.4	3.5	0.2	1.4	10	10	2	WNW 3	W 5	C 0
6	85.9	84.2	81.8	84.0	9.7	22.2	13.3	14.6	22.2	8.1	100	61	98	86	0.0	10.4	0.4	3.6	6	7	10	C 0	S 2	NNE 2
7	81.9	82.3	83.5	82.6	10.7	10.6	10.6	10.6	13.8	10.1	96	88	92	92	0.5	1.5	1.0	1.0	10	10	10	SW 3	WSW 8	W 8
8	87.1	90.0	90.2	89.1	10.0	14.5	11.0	11.6	16.3	9.1	92	66	89	82	1.0	5.7	1.5	2.7	10	10	4	W 8	W 7	SSW 2
9	87.2	90.0	91.9	89.7	11.8	18.1	14.9	14.9	20.0	9.7	84	69	91	81	2.1	6.4	1.5	3.3	9	10	6	S 4	WSW 5	C 0
10	87.1	85.8	91.0	88.0	13.7	18.6	11.9	14.0	20.0	11.5	94	76	96	89	0.9	5.1	0.5	2.2	10	10	9	ESE 3	SSW 4	NW 2
11	88.5	90.3	92.7	90.5	10.9	11.7	8.9	10.1	12.9	8.9	96	93	100	96	0.5	1.0	0.0	0.5	10 •	9	2	NNE 6	NNW 4	C 0
12	91.8	91.2	89.8	90.9	8.0	15.3	10.2	10.9	16.0	6.5	100	60	88	83	0.0	7.0	1.4	2.8	10 ≡	7	10	SSW 1	WSW 4	SW 2
13	88.2	88.7	89.3	88.7	9.0	14.7	9.7	10.8	15.9	8.5	100	71	92	88	0.0	4.8	0.9	1.9	10	6	8	W 4	W 6	WNW 1
14	90.2	92.3	94.6	92.4	8.6	14.4	8.7	10.1	15.5	7.0	99	70	99	89	0.2	5.0	0.1	1.8	10	8	0	WSW 3	W 7	W 4
15	96.4	99.2	103.5	99.7	9.5	15.1	6.9	9.6	15.7	6.6	95	56	90	80	0.7	7.7	1.0	3.1	6	5	0	WNW 4	NW 5	WNW 1
16	105.1	104.4	101.5	103.7	5.9	16.6	11.7	11.5	18.0	3.9	97	65	84	82	0.3	6.6	2.1	3.0	0	3	0	SW 1	SSE 3	S 3
17	98.0	97.5	96.7	97.4	9.1	20.2	14.6	14.6	21.5	8.4	97	67	90	85	0.4	7.9	1.6	3.3	0	7	0	S 2	WSW 6	C 0
18	93.7	90.8	89.3	91.3	12.3	22.1	16.2	16.7	22.7	12.0	96	55	81	77	0.5	11.9	3.4	5.3	0	0	0	S 2	SSW 7	W 4
19	93.4	96.7	100.8	97.0	9.5	13.9	10.5	11.1	16.5	8.9	89	62	82	78	1.3	6.1	2.3	3.2	7	9	10	W 6	WNW 7	WNW 4
20	105.2	108.6	111.5	108.4	10.9	16.7	7.9	10.8	17.0	7.9	92	47	94	78	1.0	10.1	0.6	3.9	7	4	0	WNW 4	N 6	WNW 2
21	111.1	110.3	107.3	109.6	6.4	14.3	9.9	10.1	15.3	5.1	97	67	89	84	0.3	5.5	1.3	2.4	10	10	4	W 2	WNW 7	WSW 4
22	102.2	100.2	97.4	99.9	7.8	19.7	10.5	12.1	20.5	7.0	90	37	84	70	1.1	14.3	2.1	5.8	8	0	0	WSW 6	W 6	W 3
23	95.8	95.0	93.0	94.6	7.4	21.4	14.3	14.4	21.9	6.8	94	46	80	73	0.6	13.9	3.2	5.9	8	4	0	WSW 1	WSW 3	SSE 2
24	92.5	93.0	93.3	92.9	9.1	20.7	13.9	14.4	21.2	8.9	99	65	94	86	0.2	8.6	0.9	3.2	0	0	0	SSW 1	SW 5	SE 2
25	91.9	90.7	89.7	90.8	11.1	22.8	15.7	16.3	23.0	10.4	91	51	74	72	1.1	13.5	4.6	6.4	5	6	3	SSE 4	SSE 4	SE 4
26	87.1	85.6	86.0	86.2	10.8	22.3	17.0	16.8	22.3	10.3	92	56	74	74	1.0	11.9	5.1	6.0	0	0	0	SE 4	SE 6	SE 4
27	83.4	81.3	85.5	83.4	13.7	19.2	11.2	13.8	19.3	11.0	87	74	86	82	2.0	5.8	1.8	3.2	9	8	0	SE 4	SSE 9	SW 3
28	84.2	83.4	80.3	82.6	8.8	17.7	15.1	14.2	18.0	8.6	92	72	97	87	0.9	5.7	0.6	2.4	0	10	10 •	ENE 2	S 2	S 2
29	82.8	85.1	88.8	85.6	11.1	12.0	10.4	11.0	15.1	10.0	96	89	88	91	0.5	1.5	1.4	1.1	10	10	9	W 4	W 3	WSW 3
30	92.0	93.0	94.6	93.2	6.0	15.9	13.5	12.2	17.6	5.6	100	68	91	86	0.0	5.8	1.5	2.4	10	9	7	SSW 1	S 3	SE 2
31																								
M	91.9	92.2	92.6	92.2	10.2	17.6	12.6	13.2	18.7	9.0	95	66	89	83	0.7	7.2	1.7	3.2	7.1	6.8	4.6	3.1	5.0	2.4

Październik — Octobre

DNI	CIŚNIENIE P= 900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N.w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D.v I	II	III
1	97.8	99.2	100.4	99.1	8.6	19.7	10.4	12.3	20.1	7.4	99	66	92	86	0.2	7.9	1.0	3.0	0	5	0	E 3	E 3	E 3
2	99.8	98.2	97.6	98.5	9.4	16.6	11.5	12.2	17.6	8.8	99	70	91	87	0.2	5.7	1.2	2.4	10	0	0	E 2	ESE 4	ESE 3
3	97.7	100.4	102.0	100.0	11.5	13.8	10.1	11.4	15.0	9.9	97	90	96	94	0.4	1.6	0.5	0.8	10 •	10	6	S 1	NW 2	WSW 1
4	103.1	103.3	103.2	103.2	6.3	12.1	9.8	9.5	15.4	6.0	100	98	97	98	0.0	0.3	0.3	0.2	10 ≡	10	0	C 0	N 1	N 2
5	104.2	104.8	104.5	104.5	7.4	15.3	9.5	10.4	15.5	6.7	100	70	97	89	0.0	5.3	0.3	1.9	10 =	8	10	N 1	ENE 2	C 0
6	103.8	103.2	101.5	102.8	5.0	10.2	7.5	7.6	10.6	3.5	100	96	100	99	0.0	0.4	0.0	0.1	10 ≡	10	10 ≡	C 0	SW 2	SW 2
7	99.0	97.4	95.6	97.3	7.3	14.7	8.7	9.8	15.3	6.8	100	62	93	85	0.0	6.3	0.7	2.3	10 ≡	6	0	SW 1	SW 5	WSW 2
8	94.6	96.0	99.2	96.6	9.0	14.4	5.9	8.8	15.5	5.2	95	70	88	84	0.7	5.0	1.2	2.3	10	10	5	N 4	N 4	NNE 2
9	99.2	98.4	97.8	98.5	5.9	9.6	4.2	6.0	10.6	3.9	95	82	92	90	0.5	2.2	0.6	1.1	9	8	2	NNE 2	N 2	NNW 2
10	95.2	94.6	96.1	95.3	3.4	11.7	4.8	6.2	13.0	2.4	97	64	92	84	0.3	4.8	0.7	1.9	8	7	6	NW 3	NNW 7	NNW 3
11	93.8	94.3	99.7	95.9	6.5	11.0	3.2	6.0	12.0	2.9	100	58	79	79	0.0	5.5	1.6	2.4	10 ≡	10	0	W 4	W 6	NNE 3
12	105.1	106.3	105.9	105.8	-0.7	8.4	3.6	3.7	9.2	-1.2	90	61	86	79	0.6	4.3	1.1	2.0	7	7	2	NNW 1	WNW 4	W 4
13	104.0	102.5	100.0	102.2	1.8	10.5	3.8	5.0	11.4	0.8	82	53	90	75	1.3	5.9	0.8	2.7	7	10	0	W 4	W 7	WSW 3
14	99.4	99.9	99.6	99.6	6.5	11.9	6.5	7.8	13.5	2.7	96	69	94	86	0.5	4.3	0.6	1.8	10	10	0	W 2	NW 3	SSW 2
15	97.3	95.5	94.2	95.7	2.1	12.4	7.4	7.3	14.3	1.7	98	75	94	89	0.1	3.5	0.6	1.4	0	10	0	SW 3	WSW 4	WSW 3
16	92.0	93.9	96.2	94.0	8.4	9.9	6.8	8.0	10.0	6.6	97	97	97	97	0.3	0.3	0.3	0.3	10	10 •	0	WSW 1	NW 4	W 3
17	101.7	104.1	104.9	103.6	4.2	11.6	5.5	6.7	12.2	3.6	97	63	95	85	0.2	5.0	0.4	1.9	1	8	10	WNW 4	NW 5	W 3
18	102.3	102.2	103.6	102.7	7.6	9.7	5.9	7.3	10.7	4.4	96	96	98	97	0.4	0.4	0.2	0.3	10	10 •	10	WNW 6	W 4	NW 2
19	105.4	106.2	107.1	106.2	0.3	9.5	4.9	4.9	10.5	0.1	100	89	97	95	0.0	1.3	0.3	0.5	10	7	0	C 0	WNW 3	N 3
20	109.8	111.6	113.2	111.5	1.5	9.7	3.9	4.8	11.1	0.9	100	72	92	88	0.0	3.4	0.7	1.4	0	9	0	NNE 2	ESE 1	SE 1
21	114.0	114.7	115.2	114.6	0.1	8.0	1.6	2.8	8.3	-0.1	98	67	85	83	0.2	3.5	1.1	1.6	10	5	0	S 2	SW 2	SW 2
22	115.3	114.7	112.7	114.2	-0.9	10.0	2.5	3.5	10.8	-1.5	94	71	96	87	0.3	3.6	0.3	1.4	0	1	0	NW 1	NNE 1	NW 2
23	109.5	108.5	108.4	108.8	4.5	9.3	6.3	6.6	10.0	1.7	100	85	94	93	0.0	1.7	0.5	0.7	10 ≡	10	9	N 2	N 4	NE 4
24	108.8	109.4	109.0	109.1	6.4	12.2	4.6	7.0	13.4	3.6	97	71	97	88	0.3	4.2	0.3	1.6	10	1	0	NE 2	ENE 1	NE 1
25	107.6	107.3	106.7	107.2	4.2	9.7	6.0	6.5	11.3	0.2	98	84	95	92	0.1	1.9	0.5	0.8	10	10	0	N 1	NNE 3	ESE 2
26	104.7	102.4	99.2	102.1	3.5	8.8	2.9	4.5	9.4	1.3	100	76	100	92	0.0	2.7	0.0	0.9	10 ≡	6	0 ≡	SW 3	SSW 4	S 2
27	96.2	96.2	94.8	95.7	1.2	3.2	3.8	3.0	4.2	0.7	100	98	100	99	0.0	0.2	0.0	0.1	10 • ≡	10	10 ≡	W 3	WSW 4	SW 4
28	91.3	91.0	90.3	90.9	6.7	11.5	9.2	9.2	12.4	2.9	97	87	95	93	0.3	1.9	0.6	0.9	10	10	0	WSW 6	WSW 7	WSW 6
29	88.6	86.7	90.4	88.6	7.4	14.5	7.3	9.1	15.1	6.8	100	77	94	90	0.0	3.8	0.6	1.5	10 ≡	4	10	WSW 3	WSW 8	W 7
30	94.0	94.3	91.1	93.1	5.3	8.1	6.3	6.5	9.0	4.7	91	86	89	89	0.8	1.5	1.0	1.1	10	8	10	W 8	WSW 7	W 7
31	84.0	84.5	84.6	84.4	6.7	7.0	4.2	5.5	8.4	3.9	85	84	92	87	1.4	1.6	0.6	1.2	9	10 •	6	W 9	W 9	W 7
M	100.6	100.7	100.8	100.7	5.1	11.1	6.1	7.1	12.1	3.5	97	77	93	89	0.3	3.2	0.6	1.4	8.1	7.7	3.4	2.7	4.	3.0

Chojnice

$H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 14{,}2\,m$

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	7.7	•	▽¹21ⁱ⁻²² 22²⁵ ●⁰ 23–24; = 5¹⁵ 7²⁵ ⌒ ²0⁰⁰–8 ⌒ ¹9–10
2	7	0.3	•	●⁰ 0⁰⁰⁻¹⁰ 3⁴³–5³⁵ ●⁰ 6²⁰ 7¹⁵ = 7¹⁵–10³⁰ 18¹⁰–24
3	7	2.7	•	= 0⁰⁰–6²⁰ 19³⁰–21⁴⁰ ⌒ ⁰19–24
4	7	7.9	•	●⁰ 2¹⁵–4⁴⁰ ●¹ 7²⁰–8⁰⁵ ●⁰–8²⁰ ●⁰ 21⁴⁵–22⁴⁰ ●⁰–24 = 4⁴⁰ 9¹⁰
5	6	0.1	•	●⁰ 0⁰⁰–2¹³; = 5¹⁵ 14³⁰ 16²⁰–20⁵⁵ = ⁰–21²⁰ = ¹–24
6	7	11.2	•	●¹ 18¹⁴–20¹⁵ ▽⁰ 21⁴⁰–23¹⁰ K⁰S 18⁰⁸–20³⁵ N; = ¹0⁰⁰–5¹⁰ = ⁰–5⁴⁵ = –9¹⁵ 20¹⁵–24
7	7	6.2	•	▽⁰ 0⁴⁰–1²⁰ 12⁰⁵–⁰⁸ ●⁰ 13³² 14⁴⁰ ●¹–15¹¹ ●⁰–15⁵⁰ 16²⁹–18¹² ●¹ 18¹²⁻¹⁷ ●²–18²¹ ●¹–18³⁶ ●⁰–20⁴⁰; = 0⁰⁰–2¹⁵ 4¹⁵–8⁴⁰ 15²⁰–21¹⁵
8	7	•	•	= 4³⁰–11⁴⁰ 16¹⁵–24, ⌒ ⁰20–24
9	7	•	•	= 0⁰⁰–5¹⁵ 19¹⁰–21³⁰ ⌒ ⁰20–24
10	6	7.1	•	●⁰ 13¹⁴⁻¹⁶ = 1²⁰–14¹⁰ 18³⁵–24; ⌒ ²0⁰⁰–11
11	7	8.2	•	▽⁰ 4¹⁰–5²⁰ ●⁰ 6¹⁵ ●¹–8⁴⁰ ●⁰–11⁰³ ▽⁰ 11²⁰ 12⁰⁷ 12²²–³⁵ 13¹²–¹⁴ 13²¹–15³⁵ = 0⁰⁰–4¹⁰ 17⁴⁵–23⁴⁰ = ¹ 24
12	7	0.5	•	▽⁰ 15⁰⁶–²³ 16⁵⁰–17⁰⁵ = ¹0⁰⁰–1²⁰ = ⁰–2³⁵ = ²–3⁰⁵ = ¹ 7⁴⁵ = ⁰–8²⁵ = –11⁴⁰ 20³⁰–24
13	7	0.0	•	= 0⁰⁰–10²⁰ 18⁴⁰–24, ⌒ ²22–24
14	7	0.3	•	▽⁰ 13⁵²–14⁰³; 16⁰²–¹⁰ = 0⁰⁰–2⁵⁰ = ⁰–3²⁰ = ²–4³⁵ = ⁰–5³⁵ = –10⁴⁰ 18³⁰–24, ⌒ ²0⁰⁰–2
15	7	•	•	= 0⁰⁰–5⁵⁰; ⌒ ¹20–24
16	7	•	•	= 2¹⁵–8²⁵ 23¹⁰–24, ⌒ ²0⁰⁰–7 ⌒ ¹8–9 ⌒ ⁰10–11 ⌒ ¹21–24
17	6	•	•	= 0⁰⁰–24, ⌒ ²0⁰⁰–10 ⌒ ¹18–21 ⌒ ²22–24
18	7	•	•	= 0⁰⁰–11³⁰ 18¹⁵–20³⁰, ⌒ ²0⁰⁰–9 ⌒ ⁰10–11
19	7	0.8	•	▽⁰ 16²⁰⁻³⁰ ●⁰ 22⁴⁰–23³⁰; ⌒ 16²⁹–³⁵
20	7	•	•	⌒ ¹20–24
21	7	•	•	⌒ ¹0⁰⁰–3 ⌒ ²4–9 ⌒ ⁰10–11
22	7	•	•	= 2²⁰–12²⁵; ⌒ ⁰19–20 ⌒ ¹21–24
23	7	•	•	= 4³⁰–9⁴⁰ 17³⁵–24, ⌒ ²0⁰⁰–9 ⌒ ¹10–11, 21–24
24	7	•	•	= 0⁰⁰–11³⁰ 20²⁰–24, ⌒ ²0⁰⁰–9 ⌒ ¹10–11 ⌒ ⁰19–24
25	7	•	•	= 0⁰⁰–10¹⁵ 18⁴⁰–24, ⌒ ²0⁰⁰–10
26	7	•	•	= 0⁰⁰–11²⁰, ⌒ ⁰2–4 ⌒ ¹5–11
27	7	0.0	•	▽⁰ 9¹⁰–²⁰, ⚡ 14²⁵–17³⁰, = 6⁴⁰–11¹⁰ ⌒ ⁰19–21 ⌒ ²22–24
28	6	5.9	•	●⁰ 16⁴³–17¹⁰ 17¹⁷–²⁴ 19¹⁵–20⁴⁰ ●²–21¹⁰ ●⁰–23²⁰, = 8¹⁰–24, ⌒ ²0⁰⁰–9 ⌒ ¹10–11
29	6	0.8	•	●⁰ 0³⁰–2⁰⁵ ▽⁰ 20²⁵–⁴⁰, = 0⁰⁰–24
30	7	•	•	= 0⁰⁰–9²⁵, ⌒ ¹19–21 ⌒ ²22–24
31				
Σ	–	59.7	–	

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1	7	0.0	•	= 1³⁰–10¹⁵, ⌒ ²0⁰⁰–11 ⌒ ¹20–22 ⌒ ²23–24
2	7	5.3	•	= 3⁴⁵–5⁴⁵ = ⁰–8³⁰ = –10²⁰, ⌒ ²0⁰⁰–5 ⌒ ¹22–24
3	6	0.7	•	●⁰ 4³³–5²⁰ ●¹–6⁰⁵ ●⁰–6⁴⁵ ●¹–7³⁵; = 2²⁰–14¹⁵ 19¹⁵–24, ⌒ ²0⁰⁰–4 ⌒ ¹19–24
4	5	0.0	•	= 0⁰⁰⁻⁵⁵ = ⁰–1³⁰ = ¹–1⁴⁰ = ²–5¹⁰ = ²–11⁵⁰ = –22⁴⁰ = ⁰–23²⁵ = ¹–24, ⌒ ¹18–22
5	7	0.5	•	= ¹0⁰⁰–1³⁰ = ²–2³⁵ = 5⁴⁵ = ²–6¹⁵ = ¹–6³⁰ = ²–8²⁰ = ¹–8²³ = ⁰–8²⁹ = –10¹⁰; 17¹⁰–22¹⁵ = ²–24
6	6	0.2	•	= ²0⁰⁰–2²⁰ = ⁰–3⁴⁵ = ²–10³⁰ = ⁰–10⁴⁵ = –20⁵⁰ = ¹–21³⁰ = ²–22¹⁵ = ⁰–23⁴⁰ = ¹–24
7	7	0.0	•	= ¹0⁰⁰–3¹⁰ = ⁰–6³⁰ = ¹–7²⁰ = ²–8⁴⁵ = ¹–8⁵⁵ = –11²⁰ 17⁴⁰–22⁴⁰ = ¹–24
8	6	•	•	= ¹0⁰⁰–3⁰ = ²–2⁴⁵ = –13³⁰ ⌒ ¹19–21 ⌒ ²22–24
9	7	0.7	•	▽⁰ 11¹⁵⁻⁵⁰ 13²⁰–14²⁰ 15¹⁰⁻²⁵, ⌒ ²0⁰⁰–11 ⌒ ¹20–24
10	7	0.0	•	⌒ ²0⁰⁰–9 ⌒ ¹10–11 ⌒ ⁰21–22 ⌒ ²23–24
11	7	•	•	= 4³⁰–5³⁰ = ⁰–5⁴⁵ = ¹–7¹⁰ = –9³⁰, ⌒ ²0⁰⁰–5 ⌒ ¹19–21 ⌒ ²22–24
12	7	•	•	⌒ ⁰0⁰⁰–2 ⌒ ²zm 3–7 ⌒ ⁰zm 8–9 ⌒ ¹10–11, 20–24
13	7	•	•	⌒ ¹0⁰⁰–5 ⌒ ¹zm 6–8 ⌒ ⁰21–22 ⌒ ¹23–24
14	7	•	•	= 2³⁰–11⁴⁰ 16¹⁵–24, ⌒ ¹0⁰⁰–10
15	6	•	•	= 0⁰⁰–24, ⌒ ²0–8 ⌒ ¹9–11, 20–22 ⌒ ²23–24
16	6	5.4	•	●¹ 7³⁵⁻⁴⁵ ●⁰–14¹⁵; = 0⁰⁰–7⁴⁵ = ⁰–9³⁵ = –15⁴⁰, ⌒ ²0⁰⁰–7
17	7	•	•	= 4³⁰–6¹⁵, ⌒ ¹20–24
18	6	1.5	•	●⁰ 7⁴³–8¹⁰ 11⁵⁰–13¹⁰ 13⁵⁵–14¹⁴ 14²⁵–³⁰ 15²⁸–³⁵; = 5¹⁵–18²⁰ 20⁴⁰–24
19	7	•	•	= 0⁰⁰–1³⁵ = ¹–7¹⁵ = ¹–9⁴⁰ = –11³⁰ 21³⁰–23⁴⁵ = ⁰–24, ⌒ ¹20–22 ⌒ ²23–24
20	7	•	•	= ⁰0⁰⁰–15 = ¹–5¹⁵ = ⁰–6³⁰ = –7³⁵, ⌒ ¹18–24
21	7	•	•	= 5³⁰–10³⁰, ⌒ ¹0⁰⁰–3 ⌒ ¹zm. 4–7 ⌒ ²8–9 ⌒ ¹10–11 ⌒ ⁰18–21 ⌒ ¹zm 22–24
22	7	0.0	•	= 6⁴⁰–9³⁰, ⌒ ²zm. 0⁰⁰–8 ⌒ ²9–10 ⌒ ⁰11–12, 17–19 ⌒ ²20–24
23	6	•	•	= 0³⁰–4⁴⁰ = ⁰–5³⁰ = ¹–6¹⁵ = ²–7⁴⁵ = –24, ⌒ ²0⁰⁰–4 ⌒ ¹18–24
24	7	•	•	= 0⁰⁰–8⁴⁰ 19⁴⁵–24, ⌒ ¹0⁰⁰–10, 19–21 ⌒ ²22–24
25	7	0.2	•	= 0⁰⁰–11²⁰, 20⁵⁰–24; ⌒ ²0⁰⁰–8 ⌒ ¹9–11 ⌒ ⁰12–13 ⌒ ¹20–24
26	6	0.0	•	= 0⁰⁰–2¹⁰ = ¹–2⁴⁵ = ²–8³⁰ = ¹–8⁴⁵ = –13³⁰ = ²19⁴⁵–20³⁰ = ⁰–23¹⁰ = ¹–24, ⌒ ²0⁰⁰–2 ⌒ ¹18–19
27	5	0.3	•	▽⁰ 6¹⁵ 7²⁰; = ²0⁰⁰–7³⁰ = ¹–7⁴⁵ = ⁰–8⁴⁵ = –14⁴⁰ = ¹–15²⁰ = ²–24
28	6	•	•	= ²0⁰⁰–2²⁰ = ¹–2⁴⁰ = ⁰–3⁵⁰ = –18³⁰, ⌒ ¹19–21 ⌒ ²22–24
29	6	5.3	•	▽⁰ 15⁵⁰–⁵² ▽¹ 16⁰⁰ ▽⁰–17³⁵; = 4³⁰–6³⁰ = ⁰–6⁴⁰ = ¹–7²⁰ = ⁰–8⁵⁰ = –21²⁰, ⌒ ²0⁰⁰–6
30	7	•	•	= 15¹⁵–20³⁰
31	7	1.0	•	▽⁰ 10²⁵–³² 12²⁰–13⁰⁵ 15³⁵–16⁰⁴ ⚡ 8⁵⁰–12²⁰; = 6¹⁵–9³⁵
Σ	–	21.1	–	

Chojnice

$\varphi = 53°42'$ $\lambda = 17°33'$

Listopad – Novembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	81.9	74.6	69.0	75.2	4.6	7.7	10.1	8.1	10.3	2.9	97	98	90	95	0.3	0.1	1.3	0.6	10	10 •	10	SW 6	WSW 7	W 9
2	69.2	70.9	74.0	71.4	7.5	5.9	6.5	6.6	10.2	5.8	70	86	82	79	3.1	1.3	1.7	2.0	6	10 •	9	W 11	W 18	W 9
3	79.3	82.0	84.8	82.0	4.6	5.8	3.2	4.2	6.7	3.2	81	76	90	82	1.7	2.2	0.8	1.6	10	10	0	W 12	W 10	W 7
4	90.7	95.0	99.4	95.0	2.6	5.0	3.8	3.8	5.3	1.3	95	84	97	92	0.4	1.4	0.3	0.7	10	10	10	W 7	W 8	WNW 6
5	103.8	105.6	106.7	105.4	3.7	6.7	2.9	4.0	6.9	2.7	100	85	98	94	0.0	1.4	0.1	0.5	10	9	0	WNW 3	NW 5	W 5
6	105.2	104.5	102.7	104.1	3.2	5.3	4.8	4.5	5.5	1.9	100	98	100	99	0.0	0.1	0.0	0.0	10 •	10 •	10 =	W 8	WNW 8	W 4
7	99.4	99.0	100.2	99.5	4.7	6.5	4.0	4.8	7.2	3.4	97	90	95	94	0.2	1.0	0.4	0.5	10	10	3	W 4	W 2	NNE 2
8	102.1	102.9	102.6	102.5	0.5	7.2	1.6	2.7	7.5	-1.1	100	93	100	98	0.0	0.8	0.0	0.3	10	3	5	SE 1	SW 3	S 2
9	100.8	100.3	99.1	100.1	0.2	6.9	6.8	5.2	7.4	-0.6	100	90	100	97	0.0	1.0	0.0	0.3	9 • =	0	10 =	S 2	NW 4	WNW 3
10	97.7	98.1	97.5	97.8	6.0	6.8	2.6	4.5	7.0	2.0	100	93	98	97	0.0	0.8	0.2	0.3	10 •	10	8	NW 4	ENE 4	ENE 2
11	94.8	93.8	93.0	93.9	1.4	4.0	-1.3	0.7	4.5	-1.3	100	79	98	92	0.0	1.7	0.2	0.6	10	6	0	ENE 2	E 2	E 3
12	92.3	92.6	93.4	92.8	-3.7	-1.2	-4.9	-3.7	-0.6	-5.2	94	76	88	86	0.3	1.3	0.5	0.7	8	8	2	E 3	E 5	E 2
13	94.5	94.9	95.5	95.0	-6.4	-3.5	-5.6	-5.3	-3.2	-6.9	89	76	72	79	0.4	1.1	1.1	0.9	5	7	8	E 5	E 4	E 4
14	95.4	95.8	96.1	95.8	-6.6	-4.9	-6.6	-6.2	-4.8	-7.5	86	61	80	76	0.5	1.6	0.7	0.9	10	5	10	ENE 4	E 3	ESE 2
15	96.3	97.7	100.7	98.2	-7.3	-4.8	-6.5	-6.3	-4.0	-7.6	90	83	91	88	0.3	0.7	0.3	0.4	9	10	10 *	E 3	E 2	E 1
16	105.5	106.6	106.9	106.3	-9.2	-5.7	-7.4	-6.9	-3.5	-10.3	95	76	87	86	0.2	1.1	0.4	0.6	10	0	6	E 1	ESE 2	WNW 2
17	105.0	102.8	100.5	102.8	-11.1	-6.0	-11.6	-10.1	-5.5	-12.0	93	89	89	90	0.2	0.4	0.3	0.3	4	9 *	10	WNW 2	WSW 3	SE 2
18	96.3	94.2	90.4	93.6	-12.2	-10.4	-12.4	-11.8	-10.0	-12.7	93	90	89	91	0.2	0.3	0.3	0.3	10	9	5	SE 4	SE 4	SE 4
19	85.9	83.9	83.2	84.3	-11.7	-10.4	-9.9	-10.5	-9.6	-12.6	89	80	88	86	0.3	0.5	0.4	0.4	10	10	10	ESE 5	ESE 3	E 2
20	83.2	84.0	83.5	83.6	-8.8	-6.4	-6.3	-7.0	-5.7	-10.6	92	89	91	91	0.3	0.4	0.3	0.3	10	10	10	ENE 2	ENE 2	ESE 3
21	77.2	72.1	69.5	72.9	-7.1	-5.5	-5.9	-5.1	-3.6	-7.5	91	95	96	94	0.3	0.2	0.2	0.2	10 *	10 *	10 *	E 6	E 6	ENE 7
22	77.8	84.1	89.4	83.8	-1.5	-1.5	-6.6	-4.0	-1.2	-6.7	94	86	88	89	0.3	0.8	0.4	0.5	10	9 *	3	N 7	N 8	NW 6
23	94.0	96.8	98.0	96.3	-12.9	-7.6	-14.5	-12.4	-6.6	-14.7	88	93	87	89	0.3	0.2	0.3	0.3	0	0	0	WNW 3	W 4	SW 3
24	95.0	92.5	89.2	92.2	-11.3	-9.6	-7.5	-9.0	-7.5	-16.4	90	94	79	88	0.3	0.2	0.7	0.4	10	10	10	S 3	S 3	S 3
25	86.8	88.9	89.7	88.5	-5.8	0.4	0.1	-1.3	0.7	-8.1	97	94	98	96	0.1	0.4	0.2	0.2	10 *	10	10	SSE 7	WSW 6	SW 6
26	79.3	74.4	77.3	77.0	-2.4	-1.4	-1.3	-1.6	0.5	-5.0	87	90	93	90	0.7	0.5	0.4	0.5	10	10	3	SSE 10	S 10	WSW 7
27	78.2	72.8	60.3	70.4	-6.9	-2.6	-0.1	-2.4	0.1	-7.0	96	93	100	96	0.1	0.3	0.0	0.1	4	10	10 *	SW 4	SE 4	SSE 5
28	59.8	62.7	67.3	63.3	1.2	0.4	0.2	0.5	1.4	-0.1	100	94	86	93	0.0	0.4	0.9	0.4	10 =	10	10	SW 7	WSW 7	W 7
29	75.1	79.1	72.7	75.6	-1.6	0.4	-0.4	-0.5	0.9	-3.6	98	94	90	94	0.1	0.4	0.6	0.4	6	10	10	W 8	WSW 5	SSE 6
30	63.6	68.9	73.8	68.8	1.4	3.5	0.3	1.4	4.1	-1.2	98	88	82	89	0.2	0.9	1.1	0.7	10	10	8	S 7	WSW 9	SW 6
31																								
M	88.9	89.0	88.9	88.9	-2.8	-0.2	-2.0	-1.8	0.7	-4.4	93	87	91	90	0.4	0.8	0.5	0.6	8.7	8.2	7.0	5.0	5.3	4.4

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1	69.5	67.6	75.7	70.9	-1.1	0.0	0.1	-0.2	0.4	-4.1	81	100	94	92	1.1	0.0	0.4	0.5	10	10 *	10	SSE 9	WSW 11	W 9
2	81.7	83.1	80.0	81.6	-0.5	-1.0	-0.3	-0.5	0.5	-2.0	98	89	100	96	0.2	0.7	0.0	0.3	10	10	10	W 4	W 6	SSW 5
3	72.0	73.2	75.1	73.4	-0.6	0.7	0.6	0.3	1.2	-1.8	97	96	100	98	0.2	0.2	0.0	0.1	10	10 *	10 =	SW 8	SSW 4	SW 2
4	75.3	76.5	77.7	76.5	-0.2	0.3	1.3	0.7	1.3	-0.3	100	100	96	99	0.0	0.0	0.2	0.1	10 =	10 =	10	SSW 3	WSW 4	SW 7
5	80.2	77.8	62.6	73.5	-2.1	-2.2	0.4	-0.9	1.5	-3.0	92	100	96	96	0.4	0.0	0.3	0.2	9	10	10 *	WSW 5	S 3	S 9
6	61.7	65.5	73.5	66.9	2.9	3.0	1.4	2.2	4.3	0.4	77	84	89	83	1.7	1.2	0.8	1.2	10	6	10	WSW 15	W 16	W 10
7	78.2	81.9	84.6	81.6	1.1	2.5	1.4	1.6	2.7	0.3	92	82	91	88	0.5	1.3	0.7	0.8	10	6	10	WSW 9	W 9	WSW 7
8	85.7	89.3	91.9	89.0	1.1	0.6	-0.4	0.2	1.8	-0.7	94	88	86	89	0.4	0.8	0.8	0.7	10	7	9	WSW 5	W 7	WNW 6
9	90.2	83.6	71.2	81.7	-0.7	1.0	0.9	0.5	1.9	-1.6	97	73	88	86	0.2	1.8	0.7	0.9	10	10	10 *	SW 9	SW 10	SW 10
10	57.2	55.6	53.9	55.6	0.9	2.6	4.0	2.9	4.9	0.5	98	91	87	92	0.1	0.7	1.1	0.6	10 *	9	10 •	WSW 14	SW 9	SW 12
11	63.1	64.7	66.1	64.6	1.2	1.2	0.2	0.7	4.0	0.0	89	90	98	92	0.8	0.7	0.1	0.5	10	10 *	10	W 10	WSW 10	W 6
12	75.7	79.5	83.2	79.5	-0.5	-1.3	-1.9	-1.4	0.3	-2.1	92	93	96	94	0.5	0.4	0.2	0.4	10	10 *	10 •	WNW 7	NW 7	NW 4
13	87.2	87.9	88.7	87.9	-2.7	-3.6	-6.5	-4.8	-1.9	-6.9	93	80	91	88	0.3	0.9	0.3	0.5	9	5	4	NW 4	NW 2	NE 2
14	94.7	98.8	101.5	98.3	-5.7	-3.7	-5.8	-5.2	-3.2	-7.1	82	71	92	82	0.7	1.3	0.3	0.8	3	4	10	NNW 5	NW 6	W 5
15	95.4	97.5	101.2	98.0	-1.9	-1.5	-7.4	-4.6	0.4	-7.5	98	94	96	96	0.1	0.3	0.1	0.2	10 *	10	0 =	WNW 6	ENE 4	ENE 1
16	100.5	99.7	99.1	99.8	-10.2	-4.9	-11.7	-9.6	-4.8	-12.4	91	90	100	94	0.3	0.4	0.0	0.2	9	0	10 =	C 0	W 1	SW 2
17	96.3	94.2	93.0	94.5	-10.8	-9.7	-10.1	-10.2	-8.9	-13.9	94	94	94	94	0.2	0.2	0.2	0.2	4	10	10	S 3	SE 5	SE 4
18	89.5	83.5	84.3	85.8	-5.5	0.4	4.0	0.7	4.2	-10.1	97	100	100	99	0.1	0.0	0.0	0.0	10 =	10 • =	10 • =	SE 3	S 8	W 6
19	83.7	84.3	82.8	83.6	7.9	8.7	8.2	8.2	9.7	3.7	100	94	99	98	0.0	0.6	0.2	0.3	10 •	10 •	10 •	W 9	W 9	W 8
20	88.8	92.2	93.0	91.3	2.5	3.8	2.1	2.6	8.3	1.4	93	92	95	93	0.5	0.7	0.4	0.5	10	9	10	W 9	W 8	WSW 5
21	91.0	90.6	92.8	91.3	0.8	2.2	-0.3	0.6	2.3	-1.1	100	91	96	96	0.0	0.7	0.3	0.3	10	10	10	W 2	NNW 3	W 3
22	95.0	95.6	95.8	95.5	-1.7	-1.0	-0.7	-1.0	0.2	-2.4	94	93	94	94	0.3	0.4	0.4	0.4	10	10	10	WNW 4	WSW 2	S 2
23	93.6	91.4	84.8	89.9	-1.0	-2.3	-1.8	-1.7	-0.3	-2.8	94	93	81	89	0.4	0.4	1.0	0.6	10	10	10	S 4	SSW 7	SSE 7
24	77.5	75.0	73.5	74.7	-2.1	-0.7	-0.5	-1.0	-0.5	-2.3	85	81	94	87	0.7	1.1	0.4	0.7	10	10	10	SSE 7	S 9	SSE 4
25	66.3	63.9	63.3	64.5	-0.7	-0.4	0.6	0.0	0.7	-1.3	93	96	94	94	0.4	0.2	0.4	0.3	10	10 *	10	SSE 8	S 4	S 4
26	69.6	68.6	74.0	68.7	1.0	1.0	0.7	0.8	1.5	0.4	100	96	90	95	0.0	0.3	0.6	0.3	10 =	10	9	W 3	W 4	W 7
27	77.4	77.2	74.3	76.3	0.3	0.3	-0.7	-0.2	1.0	-0.9	94	94	92	93	0.3	0.3	0.3	0.4	10	9	10	WSW 6	WSW 7	SW 4
28	72.2	73.0	79.3	73.5	-1.5	-1.5	-0.3	-1.0	-0.5	-2.1	100	88	82	90	0.0	0.7	1.1	0.6	10	9	9	WNW 2	WNW 9	W 10
29	82.5	86.3	86.0	85.1	-1.5	-2.4	-0.6	-1.3	-0.3	-3.2	94	98	94	95	0.3	0.1	0.3	0.2	10 *	10	10	W 4	W 3	W 3
30	85.2	79.0	77.1	79.8	-2.7	-1.3	-0.4	-1.2	-0.1	-3.1	86	76	98	87	0.7	1.4	0.1	0.7	10	10	10 *	WSW 8	SW 8	WSW 9
31	78.3	78.8	81.3	79.5	0.7	1.3	-0.4	0.3	1.6	-0.8	98	94	84	92	0.1	0.4	0.9	0.5	10	10	9	WSW 7	W 9	WNW 9
M	80.9	81.2	81.3	81.1	-1.1	-0.3	-0.8	-0.8	1.1	-2.9	93	90	93	92	0.4	0.6	0.4	0.5	9.5	8.8	9.4	6.2	6.6	6.1

Chojnice — $H_G = 172m$ — $H_b = 177{,}2m$ — $h_w = 14{,}2m$ — Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	6	8.4	•	•0 6^15-36, 7^05_11^15 •1_12^35 •0_14^35, 16^40_17^30 •1_19^10 •0_20^20, = 7^15_20^40
2	6	0.4	•	⚥0 11^40_13^20, 19^35_20^05; ≫ 6^45_9^40 ≈_15^40 ≫_20^30, 21^30_24
3	7	•	•	≫ 0^00_15^10
4	7	0.2	•	•0 20^35-38; = 20^20_24
5	7	0.1	•	= 0^00_11^40, 21^30_24
6	6	0.1	•	•0 1^40_3^15 4^05 6^30 14^40, 18^50_19^15; = 0^00_17^40 ≡0_19^10 ≡1_21^40 ≡0_24
7	6	•	•	≡0 0^00_1^50 = −14^10, 15^35_20^40
8	6	0.0	•	= 1^30_13^15 15^30_24; ⌴0 3_7 ⌒1 13_20 ⌒1 zm 21_22 ⌴1 23_24
9	5	0.2	•	•0 6^35 7^10 •0 15^15_18^35; = 0^00_5^40 ≡0_7^10 ≡1_8^30 ≡2_9^15 ≡1_10^40 ≡0_11^45 = −14^35 ≡0_14^50 ≡1_18^30 ≡0_24; ⌴1 0^00_6
10	6	0.3	•	•0 2^40_8^10 9^05_10^25 11^20; ≡0 0^00_4^50 = −13^10, 15^30_24
11	7	-	•	•0 4^15_5^35; = 0^00_11^20, ⌴0 20_21 ⌴2 22_24
12	7	0.0	•	⚥0 7^50_9^15; = 7^15_11^30; ⌴2 0^00_11 ⌴1 19_24
13	7	•	•	⌴2 0^00_11 ⌴1 19_24
14	7	0.2	•	*0 7^35_10^20; ⌴1 0^00_7
15	6	1.7	1	*0 2^20_5^10, 7^20_9^30, 15^15_21^40, 22^45_24; = 7^30_24
16	7	•	2	*0 0^00_2^35 = 0^00_11^25, 16^35_24
17	6	0.0	2	*0 8^40_9^10 11^15_12^07, 12^18-35, 12^45_13^03; = 0^00_1^20, 4^10_24; ∨0 19^30_24
18	6	0.0	2	*0 1^15_2^20, 7^10_9^35; = 0^00_24; ∨0 0^00_14^00
19	6	0.3	2	*0 7^10_9^25, 10^07-15, = 0^00_23^30
20	5	0.9	2	= 5^30_24
21	5	13.0	3	*0 2^15_8^15 *1_15^30 *0_16^40 *1_21^20 *0_24; = 0^00_24
22	6	1.1	18	*0 0^00_3^10 △0 7^35_8^10 *19^10-40 *0_10^05 ⚥0 12^40_13^20 ⚥1_13^40 ⚥0_15^10, 18^50_19^10; = 0^00_11^15
23	7	•	19	= 16^20_24; ∨1 19^30_24
24	6	0.8	19	= 0^00_7^35 ≡0_7^45 ≡1_8^50 = −9^40 ≡1_10^15 = −24; ∨1 0^00_13^45
25	6	1.1	19	*0 1^53_4^10 6^05_7^12 *1_7^20 *0_7^25 8^35_12^10; = 0^00_24
26	7	1.9	20	*1 8^45_9^25 *0 11^45, 12^15 *1 13^03...10 *0 14^15-32 *1_16^32 ⚥0_17^20, ≫ 6^30_13^10, 14^55_18^15; = 0^00_10^35, 18^10_19^25
27	5	5.6	20	*0 15^20_18^05 *1_21^40 *0_23^35; = 7^20_24
28	6	0.0	23	*0 13^35_15^25, ≫ 8^30_9^15, 16^20_20^35, = 0^00_5^45 ≡0_7^20 = −24
29	7	3.7	23	= 0^00_6^25 13^20_24
30	7	0.3	20	*0 1^15_3^30 ⚥0 4^40_5^20 •0_6^30 7^35_8^25; ≫ 10^30_12^15; = 0^00_8^10
31				
Σ	-	40.3	-	

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1	6	1.3	15	*0 7^05-30 *1_8^40 *2_9^25 *1_10^03 *0_10^50 *1_11^35 *0_12^07 *1_13^20, ⚥0 15^05_19^15; ≫ 12^09_19^15; = 7^20_20^30
2	6	0.3	17	= 5^40_24
3	6	0.0	17	*0 4^35_6^40, 12^40_13^15 = 0^00_19^40 ≡0_20^15 ≡1_24
4	2	0.5	15	•0 5^15_6^30, 21^45_23^35 •0_24; ≡1 0^00_1^30 ≡2_11^30 ≡1_14^40 ≡2_16^20 ≡1_16^40 ≡0_17^35 = −24
5	5	6.2	12	•0 0^00_1^20 •0_2^05 *0 17^40_19^30 *1_20^25 ⚥0_21^20 •0_22^15, ≫ 21^30_24; = 0^00_11^20 ≡1_12^40 = −24
6	7	0.2	5	⚥0 10^45_11^05, ≫ 0^00_6^30 ≈_15^30 ≫_24
7	7	0.0	2	= 6^15_8^40 15^30_17^45
8	7	0.3	2	•1 4^40_5^35 ⚥0 7^10_8^15 ⚥0 9^20_10^05 *0 17^36_18^10; = 4^15_10^20
9	6	4.9	2	*0 16^40_17^10, 18^15_20^40 ⚥0_23^35; ≫ 9^40_24; = 4^20_24
10	7	1.1	pż.	•0 1^00_4^15 ⚥0_6^35 ⚥1_7^10 ⚥0_7^35 •0 20^35_24; ≫ 0^00_12^30 16^15_24
11	6	0.6	pż.	•0 0^00_2^10 ⚥0 12^52_13^07, 13^12-25 14^43_15^10 *0 19^40_20^35 21^30_23^45, ≫ 0^00_19^15; = 15^10_18^30
12	6	0.5	1	*0 5^45_6^30, 9^10...10^20 ⚥1 12^20_13^25 ⚥0_14^10 *0_17^05 ∩0 19^50 21^45 ⚥0_22^50 *0_24; = 10^20_11^35; ∩0 19^55_24
13	7	•	3	*0 0^00_1^20
14	7	1.3	3	*0 23^25_24
15	6	0.9	4	*0 0^00-10 *1 4^10_5^15 *0 6^25_8^10 *1 8^45_9^05 *0_11^15; = 5^30_19^30 ≡0_21^15 ≡1_24; ∨1 19^30_24
16	6	•	4	≡1 0^00_4^40 = −7^50 9^10_17^50 ≡0_17^55 ≡1_18^10 ≡2_20^40 ≡1_21^40 ≡2_24; ∨1 0^00_24
17	5	•	4	≡2 0^00_1^40 ≡1_2^20 ≡0_2^50 = −24; ∨1 0^00_24
18	3	6.8	3	∩1 10^25_12^30 •0_15^15 •2_17^30 •1_18^40 •0_22^15; = 0^00_5^45 ≡0_7^30 ≡1_8^20 ≡2_10^40 ≡1_11^30 ≡0_17^20 = −24; ∨0 5^45_10^25, ∩2 10^30_16^30
19	6	3.8	pż.	•0 1^25_6^35 •0_8^15 •0 9^15-35 11^20_13^10 16^20_19^15 •1_20^30 •0_22^20, ≫ 9^30_10^40, 13^20_14^15, 19^20_20^35, 22^10_24; ≡1 0^00_2^40 ≡0_4^50 = −24
20	7	•	•	≫ 0^00_1^30; = 0^00_6^15, 21^20_24
21	6	0.0	•	= 0^00_7^40 ≡1_10^15 ≡0_10^30 = −16^10; ⌴0 19_24
22	6	•	•	= 9^15_24; ⌴0 0^00_9
23	6	•	•	= 0^00_17^30
24	6	0.0	•	*0 10^05_11^45 △0 13^40_14^10, 15^25_16^05; = 11^10_24
25	5	1.2	•	*0 8^45_9^10 *1_9^40 *0_10^08 *1 12^05-15 *0 12^52_13^08, 13^26_14^10, = 7^16_20^30
26	6	0.1	pż.	•0 1^40_3^45 4^10_6^30 ⚥0 13^43_14^15; = 1^16_6^40 ≡0_7^45 = −24
27	6	•	•	= 0^00_3^20 7^30_24; ⌴0 21_24
28	6	0.2	•	*0 7^10_10^20, ≫ 17^40_24; = 0^00_19^16; ⌴0 0^00_2 ⌴1 3_7
29	7	2.6	1	*5^35_6^05 *1_8^02 *0_8^08 *1 14^04-15 *0_14^20, ≫ 2^20_4^10; = 1^40_10^15, 14^10_21^40
30	7	0.1	4	*0 1^35_3^45 16^40_18^20; ≫ 2^10_4^40 21^50_23^15 = 18^30_24
31	6	1.7	3	⚥1 11^15-35 14^10_15^05 ⚥0_15^20 •0 15^30_17^40; = 0^00_22^30
Σ	-	34.6	-	

Szczecin – Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ *Styczeń – Janvier 1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	99.0	98.8	98.9	98.9	3.8	5.0	4.2	4.3	7.0	2.7	87	81	82	83	1.1	1.6	1.4	1.4	10	9	9	SW 6	SW 5	SW 5
2	97.6	98.6	100.9	99.0	2.0	3.3	2.2	2.4	4.5	1.3	95	81	89	88	0.6	1.4	0.8	0.9	9	9	10	SW 5	SW 5	SW 5
3	105.8	106.8	111.9	107.5	0.4	1.6	1.1	1.0	2.7	0.1	92	87	90	90	0.5	0.9	0.6	0.7	8	10	10	SW 1	WNW 2	E 1
4	117.7	122.1	123.6	121.1	-0.7	1.8	-1.7	-0.6	2.2	-2.3	94	78	91	88	0.4	1.6	0.5	0.8	2	4	0	E 3	NW 4	WSW 3
5	114.9	117.7	121.3	118.0	2.2	4.6	0.8	2.1	4.9	-2.2	95	77	92	87	0.6	1.9	0.5	1.0	10 •	4	0	W 8	WNW 5	NW 3
6	122.6	125.8	127.1	124.5	0.9	2.1	-3.7	-1.1	2.5	-4.1	98	93	87	93	0.1	0.5	0.6	0.4	10	10	0	WSW 1	N 2	N 2
7	125.8	121.9	114.8	120.8	-4.6	-0.7	-0.1	-1.4	0.1	-7.0	95	75	92	86	0.3	1.5	0.5	0.8	2	9	10	SW 3	S 3	SW 5
8	106.7	100.0	98.9	101.9	2.7	4.0	6.3	4.8	6.9	-0.2	100	97	97	98	0.0	0.2	0.2	0.1	10 ≡	10 •	10 •	SW 6	SW 8	WSW 3
9	102.1	102.9	103.4	102.8	4.0	4.2	2.3	3.2	6.5	2.2	95	93	91	93	0.4	0.5	0.6	0.5	9	10	4	WSW 3	SW 3	WSW 3
10	100.1	111.6	121.7	111.1	0.5	-0.7	-3.9	-2.0	2.4	-4.7	98	94	73	88	0.1	0.4	1.2	0.6	10 ⁂	10	0	ENE 3	NE 6	E 3
11	120.3	117.9	115.6	117.9	-3.1	0.4	1.6	0.1	2.3	-6.7	93	91	91	92	0.4	0.6	0.7	0.6	9	10	4	SE 7	SE 8	S 3
12	114.7	112.1	109.5	112.1	-0.3	3.3	2.2	1.8	4.0	-2.3	98	76	77	84	0.2	1.8	1.7	1.2	9	9	9	SE 2	S 4	S 4
13	109.5	111.4	112.7	111.2	1.6	3.8	2.8	2.8	4.9	0.8	80	77	91	83	1.4	1.9	0.7	1.3	9	3	0	SW 8	SW 7	SW 6
14	107.6	105.9	110.9	108.1	1.1	2.8	2.7	2.3	3.2	0.4	89	76	86	84	0.7	1.9	1.0	1.2	1	9	2	SSW 8	SW 9	SW 8
15	115.3	114.4	113.3	114.3	1.5	4.3	2.6	2.8	5.3	0.8	80	69	65	71	1.4	2.6	2.6	2.2	0	5	1	SW 8	SW 8	SW 9
16	112.2	113.9	107.7	111.3	0.8	2.4	2.4	2.0	3.5	0.3	85	82	82	83	1.0	1.3	1.3	1.2	10 ✳	10	6	SW 7	SW 7	SW 8
17	91.9	86.3	84.9	87.7	4.2	9.0	5.0	5.8	9.4	-0.4	88	73	87	83	0.9	3.1	1.1	1.7	10	10 •	10	SW 10	SW 10	SW 7
18	86.1	86.7	83.9	85.6	4.0	5.2	2.8	3.7	5.9	1.5	75	67	93	78	2.0	2.8	0.6	1.8	9	9	10 •	SW 7	SW 8	SW 7
19	88.5	91.2	94.1	91.3	2.6	2.7	0.3	1.5	5.9	0.2	89	84	94	89	0.8	1.2	0.3	0.8	10	9	6	SW 5	SW 4	SW 3
20	94.9	95.3	95.2	95.1	-2.5	-0.5	-0.9	-1.2	0.9	-4.0	95	98	95	96	0.3	0.2	0.3	0.3	8	10	9	C 0	SE 2	NE 2
21	95.3	97.6	102.1	98.3	0.3	1.5	1.2	1.0	2.1	-1.7	94	94	87	92	0.3	0.4	0.9	0.5	10 ✳	10 •	10	N 4	N 4	N 3
22	103.3	105.1	108.2	105.5	0.2	1.8	-0.1	0.4	2.8	-0.7	96	83	96	92	0.3	1.2	0.3	0.6	10	9	10	SW 2	SW 3	SE 7
23	112.6	115.3	120.2	116.0	-0.2	2.6	-0.7	0.2	3.1	-1.3	98	82	96	92	0.1	1.3	0.2	0.5	10	2	10	ESE 4	SE 3	ESE 2
24	123.5	124.7	124.9	124.4	-0.5	1.8	0.4	0.5	2.4	-1.2	100	96	100	99	0.0	0.3	0.0	0.1	9 ≡	10	10 ≡	ESE 1	ESE 1	ESE 2
25	122.0	120.1	116.9	119.7	0.0	0.4	0.2	0.2	1.2	-0.7	100	90	96	95	0.0	0.6	0.3	0.3	10 ≡	10	10 ✳	ESE 5	ENE 4	NNE 2
26	113.0	113.2	113.0	113.1	0.0	-0.3	-1.1	-0.6	0.5	-1.6	100	88	95	94	0.0	0.8	0.3	0.4	10 ✳	9	10 ✳	SW 1	SE 8	NE 4
27	112.3	113.0	113.6	113.0	-0.7	-0.5	-1.7	-1.2	-0.1	-2.3	95	94	88	92	0.3	0.4	0.7	0.5	10	10 ✳	10	ESE 6	ESE 6	ESE 7
28	112.4	113.1	113.0	112.8	-1.2	0.3	-1.0	-0.7	1.1	-2.0	95	93	100	96	0.3	0.4	0.0	0.2	10	9	10 ≡	E 2	ESE 1	E 1
29	111.3	111.0	111.4	111.2	-0.6	0.3	0.2	0.0	1.0	-2.2	97	96	98	97	0.2	0.2	0.1	0.2	10	10	10	NNE 2	N 1	N 1
30	110.3	108.4	110.7	109.8	-0.1	0.0	-0.3	-0.2	0.9	-0.7	98	98	98	98	0.2	0.1	0.2	0.2	10 ✳	10 ✳	10 ✳	ENE 3	NE 2	NE 3
31	114.8	115.6	115.0	115.1	-7.1	-2.7	-4.0	-4.4	0.2	-8.2	88	93	94	92	0.4	0.3	0.3	0.3	2	7	10 ≡	SW 2	SW 4	W 3
M	108.5	108.9	109.7	109.0	0.4	2.1	0.7	1.0	3.2	-1.5	93	86	90	90	0.5	1.1	0.7	0.8	8.2	8.5	7.1	4.2	4.7	4.1

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1	116.9	118.4	122.8	119.4	-1.7	-0.6	-1.9	-1.5	-0.2	-4.3	92	83	92	89	0.4	1.0	0.4	0.6	10	9	6	W 3	W 2	NW 4
2	128.6	131.2	131.6	130.5	-4.4	0.8	-3.7	-2.8	1.4	-5.1	84	80	92	85	0.7	1.3	0.4	0.8	0	5	0	W 5	NNW 6	W 3
3	127.9	125.7	125.0	126.2	-2.7	-1.3	1.2	-0.4	1.4	-5.4	93	93	85	90	0.3	0.4	1.0	0.6	10	9	10	WSW 5	SW 4	NNW 4
4	126.8	127.7	126.2	126.9	-0.3	0.6	0.8	0.5	2.2	-1.4	96	88	94	93	0.3	0.8	0.4	0.5	10	10	10 ✳	NW 2	WSW 1	W 1
5	117.6	120.8	126.1	121.5	-0.9	-2.7	-2.8	-2.3	1.4	-3.4	97	84	80	87	0.2	0.8	1.0	0.7	10 ✳	9	10	ESE 2	ESE 6	SE 3
6	126.1	124.1	119.3	123.2	-4.3	-0.5	1.0	-0.7	1.4	-5.3	89	94	92	92	0.5	0.4	0.5	0.5	10	10	10	SW 5	SW 5	WNW 3
7	118.8	119.4	109.0	115.7	0.7	2.2	1.4	1.4	2.4	0.5	100	96	92	96	0.0	0.3	0.6	0.3	10 ≡	10	2	C 0	WSW 2	W 7
8	107.7	110.2	116.0	111.3	-1.3	-0.5	-1.3	-1.1	2.9	-5.2	86	88	80	85	0.8	0.7	1.1	0.9	6	10 ✳	10	N 8	N 8	NNE 10
9	121.3	124.4	123.9	123.2	-2.9	-1.6	-6.3	-4.3	-0.5	-6.7	84	86	83	84	0.8	0.7	0.6	0.7	6	10 ✳	1	N 5	N 2	SW 3
10	112.6	110.3	114.2	112.4	-2.7	1.6	-1.1	-0.8	3.2	-7.2	91	93	93	92	0.5	0.6	0.4	0.5	10 ✳	10	0	WSW 8	WSW 7	W 4
11	118.2	119.2	119.6	119.0	-4.3	0.2	0.4	-0.8	2.1	-5.1	94	87	96	92	0.3	0.8	0.3	0.5	0	0	10	SW 4	SW 6	SW 5
12	117.7	117.5	113.2	116.1	2.1	3.3	2.2	2.4	3.8	0.4	96	93	89	93	0.3	0.5	0.8	0.5	10	10	10	WSW 4	WSW 5	SW 7
13	101.2	96.2	89.2	95.2	3.4	3.2	1.8	2.6	4.8	0.3	91	88	78	86	0.7	0.9	1.6	1.1	10	10 •	10	SW 9	WSW 12	SW 9
14	87.7	96.5	103.9	96.0	0.6	2.1	0.2	0.8	2.9	0.0	92	73	86	84	0.3	1.9	0.9	1.1	10	10	10	W 6	NW 8	W 5
15	107.3	108.3	112.2	109.3	-1.5	-1.5	-2.3	-1.9	0.9	-2.9	80	86	89	85	1.1	0.8	0.6	0.8	6	10 ✳	9	W 5	WNW 5	N 3
16	113.6	116.6	120.3	116.8	-3.1	-1.9	-3.8	-3.2	-1.1	-5.7	93	85	87	88	0.4	0.8	0.6	0.6	10 ✳	10 ✳	9	WNW 2	NE 2	ENE 2
17	124.7	126.2	125.7	125.5	-12.2	-0.1	0.8	-2.7	1.1	-14.1	89	75	84	83	0.3	1.6	1.1	1.0	0 ⁂	2	10	C 0	NE 7	NNE 10
18	126.5	127.0	127.6	127.0	0.2	1.0	-0.9	-0.2	1.7	-1.2	83	70	75	76	1.1	2.0	1.4	1.5	10	4	10	NE 8	NE 6	NE 4
19	129.3	129.4	129.1	129.3	-3.5	0.0	-1.7	-1.7	0.5	-3.7	83	75	88	82	0.8	1.5	0.7	1.0	10	10	6	ENE 8	NE 5	NE 3
20	133.0	133.6	133.7	133.4	-3.7	-0.5	-1.3	-1.7	-0.1	-5.1	83	80	82	82	0.8	1.2	1.0	1.0	10	10	10	NE 5	ENE 6	E 3
21	130.6	127.6	122.0	126.7	-2.3	-2.1	-1.7	-2.0	-1.1	-3.0	84	77	86	82	0.8	1.2	0.8	0.9	10	10	10	C 0	SW 4	W 3
22	117.4	115.5	119.9	118.9	-0.3	-0.7	-1.8	-1.2	1.7	-3.3	96	91	65	84	0.3	0.3	1.9	0.9	10 ⁂	9	3	NW 5	NNE 4	NW 2
23	116.3	115.3	118.9	116.8	-3.9	-0.9	-4.0	-3.2	-0.1	-3.5	87	83	75	82	0.6	1.0	1.1	0.9	10 ✳	10 ✳	0	SW 2	C 0	NE 4
24	120.0	116.5	108.6	115.0	-10.9	-2.7	-3.3	-5.2	-1.8	-11.8	90	56	78	75	0.3	2.2	1.0	1.2	1	6	10	SW 2	WSW 5	SW 3
25	108.8	110.5	112.1	110.3	-4.3	-1.5	-3.7	-3.4	-0.1	-3.3	72	58	92	74	1.2	2.4	0.4	1.3	9	3	10 ✳	N 5	N 7	WNW 3
26	109.9	104.5	96.4	103.6	-3.5	-3.4	-0.9	-2.7	-0.4	-6.1	92	90	89	90	0.3	0.3	0.8	0.5	10 ✳	10 ✳	9	SW 5	SW 6	W 3
27	89.5	93.4	109.4	97.4	-3.6	-3.1	-3.1	-4.2	-0.3	-3.3	80	86	90	85	0.9	0.7	0.4	0.7	9	9 ✳	10 ✳	NW 8	WSW 4	NW 6
28	112.9	111.6	107.7	110.7	-13.5	-3.1	-3.7	-7.3	-4.3	-13.8	80	51	79	70	0.4	2.0	0.8	1.1	1	9	10 ✳	SW 4	SE 6	SE 8
29																								
30																								
31																								
M	116.7	117.2	117.2	117.0	-3.1	-0.6	-1.6	-1.7	0.9	-4.7	88	82	86	85	0.6	1.1	0.8	0.8	7.8	8.4	7.7	4.5	3.0	4.7

Szczecin – Dąbie $H_s = 1\ m$ $H_b = 6{,}9\ m$ $h_w = 24\ m$ Styczeń – Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	8	•	•	●^{0} 0^{00}…1^{45}
2	7	0.0	•	●▽^{0} 22^{35-40}
3	7	•	•	= 4^{15}–9^{35}
4	7	0.0	•	= 9^{10}–12^{30}; ⊔ 4–11 ⊔^{0} 20–24
5	8	2.6	•	✱^{0} $1^{10…45}$ ✱▽^{0} 3^{05-10} 3^{30-40} ●^{0} 6^{20}–10^{35}, por. wiatru do 14 m/sek 5^{15}–8^{40}; = 17^{15}–24; ⊔^{0} 0^{00}–1, 18–24
6	6	•	•	= 0^{00}–16^{40}; ⊔^{0} 0^{00}–10, 19–24
7	8	2.8	•	✱^{0} 17^{35}–20^{20}, 21^{40} 23^{05} ●^{0}–24; = 20^{20}–24; ⊔^{0} 0^{00}–17
8	5	7.1	•	●^{0} 0^{00}–1^{40} ●^{0}–3^{15} ●^{0} 5^{10-45} ,^{0} 11^{20-27} ●^{0}–24; por. wiatru 12 m/sek 16^{30}–17^{40}; = 0^{00}–3^{50} ≡^{0}–7^{15} =–7^{40} ≡^{0}–8^{15} ≡^{1}–10^{10} ≡^{0}–10^{20} =–24
9	6	3.8	•	●^{0} 0^{00}–1^{10}, 10^{15}…12^{10} 14^{40} 15^{15} 16^{15} 17^{10}–19^{30}; = 0^{00}–3^{10}, 9^{15}–24
10	7	0.1	1	●^{0} 3^{10}–4^{30} ●✱^{0}–7^{40}; = 0^{00}–12^{40}; ⊔^{0} 20–24
11	6	0.0	•	△^{0} 9^{30}–10^{20}; ≫ 8^{45}–10^{40}, por. wiatru 14 m/sek 11^{10}–15^{40}; = 10^{20}–24; ⊔^{0} 0^{00}–9
12	7	•	•	= 0^{00}–12^{15} 16^{40}–24; ⊔^{0} 3–11 ⌓ 19^{15}–21^{30}
13	6	•	•	= 0^{00}–24; ⌓ 1^{30}–3^{15}
14	7	0.0	•	●^{0} 13^{15}…14^{20}–15^{15}; por. wiatru do 14 m/sek 8^{45}–11^{15} ≫ 11^{15}–12^{40} (por. 15 m/sek), por. wiatru do 14 m/sek 12^{40}–15^{40}; = 0^{00}–7^{35}, 15^{15}–23^{30}
15	8	0.0	•	≫ 8^{40}–9^{45}, 17^{45}–19^{30} (por. 17 m/sek), por. wiatru do 14 m/sek 19^{30}–22^{20}, do 13 m/sek 23^{30}–24
16	7	2.6	•	✱^{0} $6^{10…30}$–7^{40}, por. wiatru 13 m/sek 0^{00}–1^{15}, 14 m/sek 18^{10}–21^{20} ≫–24 (por. 18 m/sek); = 7^{40}–12^{30}, 16^{30}–21^{15}
17	8	5.3	•	●^{0} 1^{10}–3^{20} ●✱^{0}–3^{40} ●▽^{0} 11^{08-12}, 12^{50} 13^{05} 13^{07-14} ●▽^{1}–13^{22} ●▽^{0}–14^{15} ●^{0}–15^{25}; ≫ 0^{00}–13^{35} (por. do 22 m/sek), por. wiatru do 14 m/sek 20^{30}–24
18	8	2.4	•	●▽^{0} 15^{02-05}, 16^{50}–17^{27} ●^{0}–18^{10}…19^{10}–23^{05}, por. wiatru do 14 m/sek 0^{00}–13^{15} ≫–13^{35} (por. 19 m/sek), por. wiatru do 14 m/sek 13^{35}–23^{30}
19	6	0.0	•	●^{0} 10^{20}…11^{10}; = 9^{30}–24; ⊔^{0} 23–24
20	4	0.2	•	= 0^{00}–24; ⊔^{0} 0^{00}–12, 22–24
21	6	0.1	1	✱^{0} 0^{40}, 2^{30}–11^{45} ●✱^{0}–12^{15} ●^{0} 12^{40}…13^{50}, 14^{15}…17^{40}; = 0^{00}–13^{30}, 17^{40}–24; ⊔^{0} 0^{00}–1
22	7	0.0	•	✱^{0} 21^{45}–22^{40}, 23^{45}…24; = 0^{00}–12^{40}, 15^{10}–24
23	6	•	•	✱^{0} $0^{00…45}$; = 0^{00}–24
24	4	•	•	= 0^{00}–4^{40} ≡^{0}–6^{40} ≡^{0}–9^{30} =–16^{50} ≡^{0}–17^{20} ≡^{1}–19^{30} ≡^{2}–24
25	5	1.4	•	✱^{0} 15^{45}–24; ≡^{2} 0^{00}–3^{30} ≡^{1}–5^{20} ≡^{0}–8^{40} =–24
26	7	1.4	3	✱^{0} 0^{00}–2^{40}, 3^{30} 6^{15}–8^{29} ✱^{1}–8^{40} ✱^{0}–10^{35}, 20^{10}–24; = 0^{00}–12^{20}, 13^{40}–24
27	5	0.6	5	✱^{0} 0^{00}–2^{50}, $9^{15…40}$ 10^{15} 17^{45}, 22^{45}–24; = 0^{00}–24
28	5	0.0	5	✱^{0} 0^{00}–2^{45} $10^{30…50}$; = 0^{00}–19^{50} ≡^{0}–24
29	5	1.9	4	✱^{0} 8^{35}…9^{25}; ≡^{0} 0^{00}–3^{40} =–24
30	4	5.9	5	✱^{0} 0^{50}…2^{30}–7^{55} ✱^{1}–10^{30} ✱^{0}–11^{45} ✱^{1}–12^{20} ✱^{0}–24; = 0^{00}–24
31	6	•	11	= 0^{00-45} ≡^{0}–1^{15} ≡^{1}–3^{30} ≡^{0}–4^{50} ≡^{1}–6^{40} =–11^{20} ≡^{0}–11^{50} =–19^{40} ≡^{0}–24; V^0 5–6^{40}, 11^{20-50}, 19^{40}–24
Σ	–	58.2	–	

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	7	•	11	≡^{0} 0^{00}–1^{50} =–7^{30}; V^0 0^{00}–1^{50}
2	8	0.0	11	✱▽^{0} 15^{50}–16^{10} 16^{45}–17^{05}; ≡^{0} 23^{45}–24
3	6	•	9	≡^{0} 0^{00}–1^{30} ≡^{0}–5^{45} =–13^{30}, 15^{20}–24
4	5	2.4	8	✱^{0} 20^{45}…21^{30} 22^{25}–24; = 0^{00}–2^{30} 5^{20} 8^{15} ≡^{0}–8^{40} ≡^{1}–9^{05} ≡^{0}–9^{35} =–15^{15}, 20^{30}–24
5	7	0.0	9	✱^{0} 0^{00}…9^{35} 10^{10} 19^{10}–20^{40}, 23^{25}–24; = 0^{00}–12^{50}
6	5	1.0	9	✱^{0} 0^{00} 1^{40} 2^{45} 10^{03} 11^{10} 14^{45} 20^{40}; = 2^{45}–24
7	5	0.2	5	●^{0} 0^{40}–3^{40}, por. wiatru 12 m/sek 23^{10}–24; = 0^{00}–5^{50} ≡^{0}–6^{15} ≡^{1}–10^{55} =–14^{05} ≡^{0}–15^{55} =–22^{30}
8	5	0.7	4	✱▽^{0} 1^{25-40} 3^{10-30} 6^{10-15} 7^{15-20} 8^{20-25} ✱▽^{2} 8^{35} ✱▽^{0} 8^{40} 9^{50} 10^{03} ✱▽^{1}–10^{40} ✱▽^{0} 10^{58} 11^{41} 11^{55} 13^{02} ✱▽^{1}–13^{35} 13^{50} 14^{15} ✱▽^{0}–14^{40} ✱▽^{2}–15^{30} ✱▽^{0}–15^{40} ✱^{0}…16^{40}, +→ 8^{30}–9^{20} +→^{0} 16^{50}–19^{30}, por. wiatru do 16 m/sek
9	5	0.3	9	✱▽^{0} 1^{10-30} 1^{40} 2^{35} 3^{25-45} 4^{10-30} 8^{40}–9^{32} ✱^{0} 9^{40} 10^{19} 10^{40} 11^{15} ✱▽^{0} 12^{03-06} 12^{24} 13^{35} 13^{50} 14^{33} 14^{45} 15^{10} 16^{05-22}, por. wiatru 12 m/sek 0^{00}–1^{30}
10	6	0.0	10	✱^{0} 3^{25} 10^{20}…11^{40}, +→^{2} 5^{30}–12^{05}; = 1^{40}–24; por. wiatru 13 m/sek 2^{45}–12^{06} **8.II:** 0^{00}–2^{40} ≫–2^{50} (por. 19 m/sek), por. wiatru do 16 m/sek 2^{50}–7^{20}, 8^{20}–15^{35} ≫–22^{30} (por. do 19 m/sek), por. wiatru 12 m/sek 22^{30}–24
11	7	0.0	5	✱▽^{0} 15^{10-13} ✱^{0} 15^{40} 16^{30-45}; = 0^{00} 9^{05} ≡^{0}–10^{55} =–12^{20}, 16^{45}–24; ⊔^{0} 2–13
12	6	1.3	3	●^{0} 7^{50}…8^{20} ●^{0} 8^{50}…9^{40}, $10^{05…25}$ ●^{0}…11^{20} ,^{0} 14^{05} 15^{15} ●●^{0}–15^{40}; = 0^{00}–2^{40} ≡^{0}–4^{10} =–24
13	6	6.5	pł.	●^{0} 0^{30} 3^{30}, 7^{30} 11^{20} 12^{31-43} ●✱^{0}–13^{00} ●^{0}–14^{12} ✱▽^{1} 15^{38-55} ✱▽^{0}–16^{06} ✱^{0} 19^{45} 20^{25} ●✱^{0} 22^{35} 23^{15} ●^{0}…24, por. wiatru do 14 m/sek 1^{30}–11^{30} ≫–12^{15} (por. 16 m/sek), por. wiatru 14 m/sek 12^{15-37} ≫–13^{25} (por. 18 m/sek),
14	8	0.4	1	●^{0} 0^{00}…1^{40} ●✱^{1}–2^{20} ✱▽^{0} 5^{50} 6^{04} ✱▽^{1}–6^{38} ✱▽^{0} 7^{36} 8^{02}, 8^{31-36}; ≫ 0^{00}–3^{15} (por. 17 m/sek), por. wiatru 15 m/sek 3^{15}–4^{30}, 13 m/sek 7^{45}–14^{40}, ⌓ 19^{50}–24
15	6	1.8	1	✱▽^{0} 3^{10-15} 9^{20}–10^{05} 10^{20-50}, 11^{25-40} 11^{49}–12^{10} ✱^{1} 12^{32-45} ✱^{0}–13^{10} ✱^{1}–14^{50} ✱^{2}–15^{03} ✱^{1}–15^{20} ✱^{0} 16^{40-50} ✱^{1}–17^{15} ✱^{0}–17^{28} ✱▽^{0}–18^{15}, 18^{25}–19^{10} ✱^{0} 22^{45}…23^{40}
16	5	1.9	7	✱^{0} 1^{05} 4^{10} 6^{45} 7^{10-20} ✱^{1}–7^{35} ✱^{2}–8^{10} ✱^{1}–8^{40} ✱^{0}–10^{05} ✱▽^{0} 12^{20}–14^{07}; ≡^{0} 22^{50}–24; V^0 22^{50}–24 **13.II:** por. wiatru 14 m/sek 13^{25} 14^{30}, 18^{45}–21^{15} ≫–24 (por. 17 m/sek)
17	8	•	9	por. wiatru 14 m/sek 14^{30}–20^{30} ≫–24 (por. 16 m/sek); ≡^{0} 0^{00}–2^{20} =–5^{50} ≡^{0}–7^{25} =–10^{45}; V^0 0^{00}–2^{20}, 5^{50}–7^{25}
18	8	•	6	≫ 0^{00-30} por. wiatru 14 m/sek 0^{30}–6^{30}
19	7	0.3	4	△^{0} 8^{15}–10^{05} ✱^{0}–10^{15} 15^{30}…17^{20} 19^{10}, 23^{50}–24; por. wiatru 13 m/sek 6^{30}–7^{40}
20	7	0.0	4	✱^{0} 0^{00}…1^{00} △^{0}–1^{50} ✱^{0} 8^{35}…9^{50}; = 17^{30}–18^{30}
21	6	0.0	3	= 8^{20}–24
22	8	0.2	3	●⌣^{0} 5^{25}–6^{45} △–7^{10} ✱^{0}–8^{35}…9^{10} ✱^{1}…10^{23} ✱▽^{0} 10^{35-51} ✱▽^{1} 12^{36-48} ✱▽^{0} 13^{03-46}; = 0^{00}–8^{15}; ∾ 5^{25}–6^{45}
23	7	0.8	pł.	✱^{0} 6^{40} 7^{15}–10^{20} ✱^{1}–10^{43} ✱^{0}–12^{30}…14^{10}, 14^{50}…16^{20}, 18^{30}…19^{45}; = 6^{30}–11^{30}
24	8	0.2	2	✱^{0} 21^{40}–24; = 5^{15}–11^{00}, ⊔^{0} 2–10
25	8	2.2	1	✱^{0} 0^{00}–5^{10} ✱▽^{1} 18^{20-30} ✱▽^{0}–19^{05} ✱▽^{1} 19^{50}–20^{20} ✱^{0}…21^{30}, por. wiatru 12 m/sek 3^{30}–5^{50}, 11^{10}–17^{20}, ∞ 9^{25}–10^{10}
26	5	4.2	8	✱^{0} 3^{50}–5^{10}–6^{30} ✱^{1}–9^{40} ✱^{0}–19^{15}; = 19^{15}–21^{30}
27	6	0.8	14	✱^{0} 1^{05} 2^{30}…3^{40} ✱▽^{1} 10^{14-28} ✱^{0}–11^{27} ✱^{1}–11^{43} ✱^{0}–13^{15} ✱^{1}–13^{26} ✱^{2}–13^{45} ✱^{0}–15^{10} ✱▽^{1} 16^{15-35} ✱▽^{0} 16^{40}–17^{20}, 18^{14-32} ✱▽^{1} 20^{44}–21^{10} ✱▽^{0} 22^{52}–23^{05}, +→^{0} 6^{45}–12^{45} +→^{1} 13^{45}–14^{05} +→^{2}–16^{50} +→^{1}–18^{35}
28	8	0.7	17	✱^{0} 17^{15}–18^{50} ✱^{1}–19^{30} ✱^{0}–24 **27.II:** +→^{0}–19^{45}, por. wiatru 14 m/sek 6^{15}–12^{30}, 18 m/sek 13^{55}–14^{05} ≫–16^{50} (por. 22 m/sek), por. wiatru 17 m/sek 16^{50}–19^{45}
29				
30				
31				
Σ	–	25.9	–	

Szczecin-Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ *Marzec — Mars* 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	104.9	104.6	102.9	104.1	-3.7	-3.3	-4.7	-4.1	-2.2	-6.2	87	85	86	86	0.6	0.7	0.6	0.6	10 ✳	10 ✳	10	E 5	ENE 5	NE 5
2	99.7	98.7	97.5	98.6	-6.5	-2.1	-2.7	-3.5	-1.9	-7.2	86	77	89	84	0.5	1.2	0.6	0.8	10 △	10 ✳	10	NE 5	NE 6	NE 9
3	94.2	93.5	94.9	94.2	-2.3	-1.5	-1.9	-1.9	-1.2	-3.2	93	96	94	94	0.4	0.2	0.3	0.3	10 ✳	10 ✳	10 ✳	NNE 8	N 8	N 8
4	96.7	98.4	101.3	98.8	-4.1	-3.3	-3.1	-3.4	-1.9	-4.4	89	83	84	85	0.5	0.8	0.8	0.7	10 ✳	10 ✳	10 ✳	NW 6	WNW 6	WNW 7
5	105.2	109.1	114.7	109.7	-1.3	1.0	-0.9	-0.5	1.2	-3.4	95	81	91	89	0.3	1.3	0.5	0.7	10 ✳	9 ✳	9	NW 3	N 4	NE 2
6	119.6	122.6	126.7	123.0	-1.7	-0.1	-7.3	-4.1	0.4	-7.6	92	80	88	87	0.4	1.2	0.4	0.7	10	10	0	NE 4	NE 5	NE 5
7	130.7	131.9	130.5	131.0	-12.9	-1.3	-8.9	-8.0	-0.5	-14.0	88	70	92	83	0.3	1.7	0.3	0.8	0 ≡	4	0	C 0	NE 4	C 0
8	128.0	126.0	123.5	125.8	-22.0	-3.5	-4.6	-8.7	-2.6	-22.7	96	63	81	80	0.0	1.7	0.8	0.8	0 ≡	1	4	C 0	SW 4	SW 6
9	122.2	123.9	126.3	124.1	-3.2	0.2	-3.5	-2.5	2.8	-5.1	90	81	88	86	0.5	1.2	0.6	0.8	10	6	0	SW 5	SW 4	SW 2
10	129.2	131.0	131.1	130.4	-7.3	-0.5	-2.1	-3.0	1.3	-9.2	90	80	77	82	0.3	1.2	1.2	0.9	10	4	6	SW 3	SW 3	SW 4
11	131.6	131.2	128.5	130.4	-12.4	2.7	-2.6	-3.7	4.3	-12.6	93	55	77	75	0.2	3.3	1.2	1.6	4	0	0	SW 2	SW 4	SE 1
12	127.2	126.0	124.6	125.9	-10.3	5.4	-3.9	-3.2	6.8	-11.7	87	46	82	73	0.4	4.9	0.8	2.0	0	0	0	C 0	SW 1	SSE 1
13	124.2	124.5	123.2	124.0	-9.3	3.9	-0.1	-1.4	4.6	-9.7	88	69	82	80	0.4	2.6	1.1	1.4	0	0	0	ESE 2	ESE 4	SE 3
14	121.6	119.7	117.9	119.7	-5.6	3.8	1.4	0.2	7.3	-5.9	92	70	74	79	0.3	2.4	1.8	1.5	0	0	0	ESE 2	ESE 3	SE 1
15	117.2	116.7	114.1	116.0	0.8	5.4	6.2	4.6	9.6	-0.8	90	94	82	89	0.7	0.6	1.7	1.0	9	10 •	10	SW 2	E 2	SW 5
16	110.2	108.8	111.5	110.2	4.8	5.8	5.1	5.2	7.3	4.2	87	94	97	93	1.1	0.6	0.3	0.7	9	10 •	3	SW 8	SW 7	SW 6
17	110.4	110.1	108.7	109.7	3.6	7.3	2.6	4.0	9.3	2.6	90	77	88	85	0.8	2.3	1.0	1.4	9	10	0	SW 3	SW 5	C 0
18	105.6	102.2	99.8	102.5	-1.5	11.0	4.6	4.7	11.4	-2.3	96	60	84	80	0.2	5.2	1.4	2.3	6 ≡	2	7	C 0	SSE 8	SE 3
19	97.5	103.7	111.5	104.2	5.6	7.1	1.3	5.8	7.6	1.0	91	87	76	85	0.9	1.3	1.6	1.3	10 •	10	0	SW 7	WSW 3	WSW 3
20	115.7	116.1	114.9	115.6	-1.1	4.4	0.8	1.2	6.6	-1.6	91	65	85	80	0.4	3.0	1.0	1.5	0	9	0	SW 4	SW 5	SW 5
21	109.7	105.7	108.8	108.1	-0.9	0.2	-2.3	-1.3	1.1	-2.4	96	98	100	98	0.2	0.1	0.0	0.1	10	10 ✳	0 ≡	SE 4	NE 4	SW 3
22	113.2	115.3	114.9	114.5	-4.5	3.4	-2.8	-1.7	5.1	-4.8	91	65	86	81	0.4	2.8	0.7	1.3	0	1	0	SW 4	W 5	SSW 2
23	110.6	105.5	100.0	105.4	-2.5	6.2	4.6	3.2	7.9	-3.6	80	45	60	62	1.0	5.3	3.4	3.2	3	4	9	ESE 5	SSE 10	SSE 9
24	97.6	98.3	99.1	98.3	4.9	8.6	7.4	7.1	10.4	2.5	89	81	91	87	1.0	2.2	0.9	1.4	9	9	10	S 2	SW 5	SW 4
25	105.1	109.4	112.5	109.0	2.8	5.4	2.7	3.4	7.7	2.4	89	60	93	81	0.8	3.6	0.5	1.6	10 •	9	10	WNW 8	NW 6	SE 2
26	111.8	110.6	116.5	113.0	2.5	6.8	2.4	3.5	8.4	1.4	93	68	91	84	0.5	3.2	0.7	1.5	6	8	0	SW 4	ESE 6	ENE 3
27	126.3	129.0	129.6	128.3	1.0	5.4	5.9	4.6	7.8	0.7	100	84	83	89	0.0	1.4	1.6	1.0	10 ≡	9	8	C 0	WSW 1	SW 5
28	128.2	128.5	129.0	128.6	5.8	9.0	9.8	8.6	10.2	5.4	97	95	92	95	0.3	0.7	0.9	0.6	10 •	10 •	10	SW 5	SW 4	SW 2
29	129.0	130.0	126.4	128.5	6.6	9.3	10.1	9.0	15.0	5.7	93	78	83	85	0.7	2.6	2.1	1.8	7	2	0	SW 3	WSW 4	WSW 5
30	121.5	123.8	130.0	125.1	5.4	6.6	3.0	4.5	10.1	2.8	77	79	86	81	2.1	2.0	1.1	1.7	6	10	0	WSW 4	N 8	NE 2
31	128.3	127.2	128.6	128.0	1.5	10.2	3.7	4.8	10.7	0.6	85	53	75	71	1.0	5.8	2.0	2.9	4	1	0	W 5	NNE 7	SW 3
M	115.3	115.5	116.1	115.6	-2.2	3.7	0.7	0.7	5.3	-5.5	90	75	85	83	0.6	2.2	1.0	1.3	6.5	6.4	4.1	5.6	4.9	3.6

Kwiecień — Avril

1	132.4	132.6	128.5	131.2	-0.5	9.8	6.6	5.6	11.1	-2.4	96	46	68	70	0.3	6.5	3.1	3.3	0	2	0	ENE 1	ENE 3	WSW 3
2	126.3	127.9	125.2	126.5	1.6	5.6	2.4	3.0	7.8	1.3	93	75	96	88	0.6	2.2	0.3	1.0	10	4	0	NW 4	NE 2	C 0
3	120.5	119.1	115.6	118.4	1.4	6.2	7.6	5.7	13.7	-2.0	89	73	75	79	0.8	2.6	2.6	2.0	10	6	0	NW 4	W 5	SW 4
4	112.8	111.7	112.7	112.4	3.0	13.0	4.7	6.4	13.4	2.0	86	51	81	73	1.1	7.3	1.6	3.3	1	9	0	SW 3	NW 2	ENE 2
5	116.1	116.9	116.8	116.6	-3.3	13.4	7.4	6.2	14.7	-4.1	94	30	50	58	0.3	10.8	5.1	5.4	4	2	0	SE 1	ESE 3	ESE 4
6	117.1	114.0	108.5	113.2	3.6	16.0	13.6	11.7	16.8	2.2	81	29	38	49	1.3	12.9	9.6	8.0	0	9	10	ESE 3	S 6	SSE 8
7	112.0	113.2	113.1	112.8	6.5	7.6	5.6	6.3	13.9	5.1	84	75	81	80	1.6	2.6	1.7	2.0	9	10	9	W 3	W 5	NW 2
8	112.7	112.8	112.8	112.8	5.7	7.8	4.8	5.3	9.5	3.2	88	69	75	77	1.0	3.3	2.2	2.2	9	9	0	E 5	NE 7	E 8
9	112.9	113.3	113.9	113.4	4.3	6.8	6.4	6.0	8.0	2.7	84	75	76	78	1.4	2.5	2.3	2.1	9	10	10	E 8	E 7	E 5
10	114.3	113.9	112.1	113.4	3.6	7.5	6.6	6.1	9.7	3.3	68	58	71	66	2.5	4.4	2.8	3.2	10	10	9	ESE 7	SSE 5	SSW 3
11	109.5	109.2	111.3	110.0	3.8	10.2	4.6	5.8	10.4	3.3	70	52	89	70	2.4	6.0	1.0	3.1	6	9	10	SE 8	S 8	SE 4
12	112.6	111.8	110.4	111.6	2.6	12.9	8.3	8.0	13.5	2.1	96	46	77	73	0.3	8.1	2.6	3.7	10	9	6	SE 2	SW 5	SSE 6
13	107.8	107.8	111.4	109.0	5.4	11.4	5.2	6.8	12.3	4.2	89	64	97	83	1.0	4.9	0.2	2.0	2	10	10	E 4	SW 5	C 0
14	115.6	118.3	119.7	117.9	3.4	10.0	4.0	5.4	11.3	2.1	95	51	83	76	0.5	6.0	1.3	2.6	4	8	2	WSW 3	W 3	ESE 2
15	118.3	116.1	112.6	115.7	1.6	12.0	4.4	5.6	13.4	-3.2	93	39	87	73	0.6	8.6	1.1	3.4	0	6	4	ESE 3	S 7	ESE 5
16	106.4	104.8	107.2	106.1	4.3	9.3	7.4	7.1	10.4	3.2	92	74	86	84	0.7	3.1	1.5	1.8	10	10 •	10	SE 8	SSE 8	WNW 5
17	110.1	108.4	98.4	105.6	5.1	9.2	6.4	6.8	11.3	4.6	83	56	88	76	1.3	3.1	1.1	2.6	10	9	10 •	WSW 6	SW 7	S 8
18	86.9	89.6	98.6	91.7	8.6	6.8	5.6	6.6	10.2	5.2	90	94	77	87	1.1	0.6	2.1	1.3	10 •	10 •	0	SSW 7	WSW 8	SW 4
19	101.6	101.2	101.6	101.3	3.8	11.3	8.4	8.0	12.7	1.1	80	41	71	64	1.6	8.0	3.1	4.2	5	6	9	SSW 3	S 7	ESE 4
20	102.1	103.2	104.6	103.3	5.0	6.8	9.3	7.6	11.1	4.4	100	97	87	95	0.0	0.3	1.6	0.6	10	10 •	9 •	N 6	NE 1	NE 3
21	105.6	104.8	104.8	105.1	7.8	13.4	8.5	9.6	14.9	6.8	87	60	85	77	1.4	6.2	1.7	3.1	9	10	0	NNE 3	ENE 5	NNE 4
22	102.7	102.5	102.5	102.6	7.6	12.1	7.4	8.6	13.7	5.8	99	80	94	91	0.1	2.8	0.6	1.2	10 •	10 •	4	ENE 5	ENE 5	C 0
23	102.3	102.1	102.3	102.2	5.4	10.1	6.3	7.0	10.6	4.6	91	64	82	79	0.9	4.6	1.7	2.4	10	9	10	ENE 5	ENE 6	N 6
24	99.7	100.9	102.9	101.2	6.3	7.4	5.4	6.1	9.2	5.3	94	85	91	89	0.5	1.8	0.9	1.1	10 •	10 •	10	WNW 4	NNW 5	NW 2
25	103.4	103.3	106.6	105.1	6.4	8.6	7.0	7.2	11.2	4.8	94	65	88	82	0.6	3.9	1.2	1.9	10 •	9	10	SW 5	W 5	SW 4
26	107.4	107.1	105.2	106.6	6.1	8.9	4.4	6.0	11.1	4.3	92	82	87	87	0.7	2.0	1.1	1.3	10	9	0	SW 5	SW 4	SE 3
27	102.0	101.3	102.6	102.0	6.0	11.8	7.9	8.4	12.4	2.1	91	50	86	76	0.9	6.9	1.4	3.1	8	10	10	ESE 5	SE 7	SW 1
28	102.9	101.3	102.7	102.4	7.2	14.3	9.6	10.2	15.3	4.1	94	61	91	82	0.6	6.3	1.2	2.8	9	7	10 •	ENE 3	E 8	E 9
29	104.6	107.4	112.1	108.0	8.8	7.7	8.4	8.3	11.8	7.6	93	93	86	91	0.6	0.7	1.3	0.9	10	10	6	E 4	ESE 7	ENE 2
30	116.3	116.9	119.0	117.4	5.9	13.6	8.6	9.7	16.6	1.8	92	54	66	71	0.7	8.1	3.8	4.2	0	7	3	ESE 1	ENE 4	NNE 3
31																								
M	109.8	109.9	109.9	109.9	4.3	10.1	6.8	7.0	12.1	2.8	89	63	80	77	0.9	3.0	2.1	2.7	7.2	8.3	5.8	4.2	3.3	3.8

Szczecin - Dąbie $H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 24\,m$ Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	POGODA
1	6	0.5	18	*°00–5^10, 6^40..13^40 △°–14^35 *°..15^20 20^15, 23^45..24; = 20^15–24
2	6	0.8	18	*°00–24^5 △5^45 9^20 *°..10^15 14^20 15^05–20^50; + 21^15–24; por. wiatru 12 m/sek 21^15–24; = 0^00–11^40
3	4	10.2	20	*°1^30..5^05–7^10 *¹–22^45 *°–24; + 0^00–1^15 5^20–22^30 +°–24; por. wiatru 12 m/sek 0^00–1^20, 14 m/sek 5^20–24
4	5	1.8	37	*°0^00–24; + °0^00–40; por. wiatru 14 m/sek 0^00–40
5	6	0.3	41	*°0^00–8^10 *¹–9^40 *°–12^10 12^30..13^40; = 4^30–24
6	6	0.3	35	*°8^35–9^05 △–12^15; = 0^00..13^10
7	8	•	35	= 2^30–3^50 =°–4^45 =¹–7^40 =°–8^20 = –10^30 20^30–22^20; V° 3^50–8^20
8	8	0.0	35	=°10^5–50 =¹–5^30 = –7^15 = –11^40; V° 10^5–7^15
9	7	•	28	*°4^10–5^35; = 1^30–12^15
10	7	•	22	= 6^15–8^25 =°–8^40 =¹–9^15 =°–11^25 = –12^20
11	7	•	20	= 0^00–12^40, 17^45–24
12	5	•	17	= 0^00–11^15 ∞–18^30 = –24
13	6	•	14	= 0^00–11^40 ∞–15^30 = –24
14	6	0.0	13	= 0^00–10^30 ∞–18^30 = –24
15	5	0.2	10	•°0^20..1^40 8^35 13^40 18^10..19^20; = 0^00–14^30 ∞–18^10 = 19^20–24
16	6	0.0	pł.	•°10^45..14^15; = 0^00–24
17	6	0.0	•	•°12^15..45; = 0^00–21^50 =°–24
18	7	1.4	•	=°0^00–1^50 =²–4^20 =²–6^50 =°–7^15 = –10^40 19^30–24; V° 1^50–7^25
19	6	0.8	•	•°4^10–9^35 •°10^45..11^40 •°13^50..15^25; = 0^00–16^30; ⌣°23–24
20	8	•	•	= 22^30–24; ⌣° 0^00–9
21	4	7.0	•	*°8^40–10^15 *¹–13^15 *°–13^40 *¹–14^10 *°–15^40; = 0^00–15^40 =°19^50–20^30 =¹–22^30 =°–24; ⌣° 3–8 V° 19^50–24
22	8	•	6	=°0^00–1^50 = –3^30; V° 0^00–1^50
23	8	2.4	•	•°23^30–24; ≋ 11^30–16^30
24	6	1.1	•	•°0^00–2^40, 15^24..16^10, 20^15–44, 21^50..23^30–24; = 2^40–24
25	7	0.0	•	•°0^00–20, 0^30..2^15 4^05 5^25 6^15 7^35 19^40 20^30 23^50–24; por. wiatru 13 m/sek 4^30–7^40; = 0^00–7^40, 20^30–24
26	8	•	•	•°0^00..20; = 0^00–5^30, 21^40–24
27	6	0.0	•	•°23^45..24; = 0^00–4^30 =°–5^20 =²–7^30 =°–8^20 =°–9^10 = –24; ⊕ 14^15–16^15
28	6	2.0	•	•°0^00..3^40 •°5^35–7^40 •°11^30–17^30 •°–18^10 •°–19^10; = 0^00–24
29	6	•	•	= 0^00–8^05 =°–8^45 = –15^40; ⌓°22–24
30	8	•	•	por. wiatru do 14 m/sek 11^20–14^30; ⌓° 0^00–10
31	8	•	•	⌣°1–9
Σ	–	28.8	–	

Kwiecień - Avril

1	8	•	•	= 6^00–7^30; ⌣°4–7; ⌓°21–24
2	7	•	•	= 5^40–11^45, 18^30–24; ⌓° 0^00–2 ⌣°3–6
3	6	•	•	= 0^00–1^10 =°–3^40 = –11^40 ∞ 12^30–16^30
4	7	•	•	= 0^30–8^30 ∞–11^30 =°23^50–24; ⌣°3–8
5	8	•	•	=°0^00–30 =²–6^40 = –7^35 =°–8^15 = –9^30; ⌣°3–7
6	8	1.1	•	•°23^20–24; ⊕ 12^30–17^15
7	7	•	•	•°0^00–40; = 0^30–9^20; 10^30–12^30
8	8	•	•	= 1^30–8^40
9	7	1.5	•	•°12^17–40 17^10–20^40
10	8	•	•	•°0^15..2^15
11	8	0.3	•	•°17^10–22^15, por. wiatru 13 m/sek 5^10–13^30; = 22^15–24
12	8	•	•	= 0^00–9^40, ⌓°2–10
13	7	0.1	•	⚲°13^06–15 15^12–46; = 1^00–7^30 13^15–14^40; ⌓°2–9, 20–24
14	8	•	•	= 2^30–10^15 23^30–24; ⌓° 0^00–2 ⌣°3–6 ⌓°19–24
15	8	0.0	•	⚲°17^20–25, por. wiatru 14 m/sek 14^20–15^40; = 0^00–3^35 =°–6^10 = –9^30; ⌓° 0^00–2 ⌣°3–6
16	7	1.2	•	•°9^50..15^05–40 •¹–16^30 •°–17^05 18^05 •°–19^05, por. wiatru 14 m/sek 10^05–35, 12 m/sek 11^45–12^30; = 20^30–23^30; ⌓° 0^00–6
17	8	6.6	•	•°17^45–24; por. wiatru 14 m/sek 17^30–24; ⊕ 11^40–16^20
18	7	2.3	•	•°0^00–6^30..8^15 ⚲°9^10–35 •°12^05 14^40 ⚲°15^28–40, 17^45–52; por. wiatru 14 m/sek 0^00–13^20
19	8	10.4	•	⌓°23–24
20	5	10.2	•	•¹3^25–8^45 •°–9^15 •¹–9^50 •°–10^50 11^10 11^25..45 •°–13^50; = 13^50–16^05; ⌓° 0^00–3
21	7	1.8	•	⚲°17^15–30
22	7	4.4	•	⚲°3^10–17 •°6^05..10^30 11^45 12^40..13^40 ⚲°15^10–17 ⚲°16^30–38 ⚲°17^24–28; R° 14^50–15^15–15^45 NE-SW R° 16^15–25–50 E-W; = 4^15–11^50 17^30–24
23	8	2.8	•	= 0^00–4^30 6^30–8^30
24	7	1.1	•	•°0^35–4^10 5^15–12^15 13^40; = 4^00–12^15
25	7	3.0	•	•°5^35–7^40 •¹–8^05 •°–8^35 ⚲°15^40–16^20; = 4^50–8^35, ⌓° 0^00–5
26	7	0.2	•	•°4^40 5^05 ⚲°10^15–11^03 11^06–31 11^43–12^05; = 6^30–8^00; ⌓°21–24
27	7	0.1	•	⚲°2^00–27 8^42 9^05 11^34–40 13^03–10 13^16–21 14^40–44 15^22–26 16^04–12; = 3^15–8^35 16^30–24; ⌓° 0^00–2
28	8	4.1	•	⚲°6^10–28 13^06–10 ⚲¹14^42–15^05 ⚲°17^05–15 •°20^05–10 •¹–21^20 •°22^20–24; R° 14^50–15^10–15^35 E-W; R° 17^05–20 E-W; por. wiatru 14 m/sek 10^40–19^30; = 0^00–8^30
29	6	0.0	•	•°0^00..2^40 ⚲°12^05–10; por. wiatru 14 m/sek 1^00–2^40; = 12^10–13^10 21^30–24
30	7	0.3	•	⚲°13^05–14^05 ⚲¹–14^15 ⚲°–14^23; R° 14^10–35 SW; = 0^00–8^20, ⌓°2–9, 22–24
31				
Σ	–	51.7	–	

Szczecin – Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ *Maj – Mai* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	119.3	119.0	119.4	119.2	7.0	15.6	8.0	9.6	16.7	1.3	70	54	68	64	3.0	8.1	3.4	4.8	1	4	2	WSW 1	N 5	E 1
2	121.1	120.1	119.8	120.3	5.4	13.4	5.5	7.4	14.8	1.4	72	40	68	60	2.5	9.3	2.9	4.9	9	2	0	ESE 3	ENE 2	NE 5
3	120.6	119.4	117.3	119.1	2.6	11.1	7.0	6.9	13.5	-0.2	75	29	56	53	1.9	9.3	4.4	5.2	0	0	0	E 5	ESE 6	SE 6
4	113.7	109.3	104.1	109.0	6.4	15.2	10.6	10.7	17.0	2.6	48	31	85	55	5.0	12.0	2.0	6.3	2	7	10 •	SE 8	SE 10	S 8
5	101.7	101.4	103.5	102.2	8.2	14.2	8.8	10.0	15.5	6.5	90	82	95	89	1.1	2.9	0.6	1.5	9	5	10	ESE 6	SE 5	SE 5
6	105.8	109.0	111.8	108.9	8.8	9.6	9.5	9.4	10.3	7.5	95	82	79	85	0.6	2.2	2.5	1.8	10 •	10	10	WNW 5	NW 3	NNW 5
7	113.8	113.4	111.6	112.9	8.2	9.4	8.8	8.8	12.1	5.6	87	82	89	86	1.4	2.2	1.2	1.6	9	10 •	10 •	W 5	WNW 3	SE 4
8	109.6	113.4	113.9	112.3	8.8	13.4	12.3	11.7	15.6	7.8	95	65	79	80	0.6	5.3	3.0	3.0	10	7	10	NE 2	WSW 3	SSW 4
9	109.3	101.3	97.5	102.7	11.2	12.4	8.1	10.0	14.2	7.7	94	93	89	92	0.8	1.0	1.2	1.0	10	10 •	10 •	SW 3	SSW 7	W 12
10	98.6	99.2	100.0	99.3	8.6	9.7	8.4	8.8	11.0	7.3	82	83	92	86	2.0	2.0	0.9	1.6	9	9	10 •	WNW 8	NW 7	NW 7
11	106.9	113.8	119.6	113.4	7.8	10.0	8.4	8.6	11.2	7.1	87	78	90	85	1.4	2.7	1.0	1.7	10	10	10 •	N 7	N 6	NNW 3
12	123.8	124.4	123.6	124.0	7.8	15.8	11.2	11.5	17.2	6.3	97	56	89	81	0.3	7.9	1.5	3.2	10 ≡	6	5	C 0	NE 3	N 1
13	123.9	122.9	120.8	122.5	8.6	16.1	13.3	12.8	18.0	6.8	86	55	85	75	1.6	8.2	2.3	4.0	1	5	10 •	W 2	NW 4	C 0
14	117.3	114.9	114.3	115.5	11.4	15.5	11.4	12.4	17.6	10.7	91	76	93	87	1.2	4.3	1.0	2.2	10	8	10	W 1	SW 2	E 2
15	113.6	112.4	109.2	111.7	8.9	15.4	13.0	12.6	15.7	8.5	90	67	70	76	1.1	5.8	4.5	3.8	10	8	5	E 3	ESE 4	SE 5
16	107.2	106.7	107.3	107.1	9.4	15.2	13.4	12.8	16.3	7.8	74	80	75	76	3.1	3.5	3.8	3.5	7	10	10	SE 6	WSW 3	NW 3
17	105.6	103.7	99.6	103.0	11.2	20.6	15.4	15.6	21.5	8.7	94	52	89	78	0.8	11.6	1.9	4.8	10	7	10 •	C 0	WSW 6	NNE 2
18	101.0	103.3	102.0	102.1	13.6	16.1	13.7	14.3	17.0	12.0	79	62	78	73	3.4	7.0	3.5	4.6	7	9	10	W 5	WSW 7	S 5
19	103.5	106.0	111.1	106.9	7.4	9.8	8.2	8.4	13.7	7.2	87	63	61	70	1.3	4.5	4.3	3.4	10	9	2	NNW 8	N 6	WNW 3
20	116.3	118.3	121.4	118.7	5.4	9.8	6.4	7.0	12.7	2.8	84	44	84	71	1.4	6.8	1.6	3.3	3	8	6	WSW 4	NW 5	W 3
21	125.9	127.0	127.3	126.7	6.2	12.0	7.4	8.2	13.3	3.8	79	42	79	67	2.0	8.1	2.2	4.1	1	5	1	W 3	W 5	WSW 1
22	128.2	126.8	124.5	126.5	8.0	15.2	10.2	10.9	16.7	-0.1	67	44	60	57	3.5	9.6	4.9	6.0	0	2	0	C 0	SE 4	E 3
23	124.6	121.4	119.2	121.7	9.9	17.8	15.6	14.7	18.8	4.1	54	40	52	49	5.7	12.2	8.6	8.8	2	2	10	E 5	ESE 10	ESE 6
24	117.7	117.3	117.0	117.3	12.4	12.2	10.2	11.2	15.7	10.1	63	78	96	79	5.3	3.2	0.4	3.0	10	10	10 •	E 4	ESE 6	NE 4
25	117.3	118.0	118.5	117.9	10.6	11.6	11.0	11.0	11.9	9.8	95	89	94	93	0.7	1.5	0.8	1.0	10	10	10 •	N 4	NE 3	NE 2
26	117.7	117.1	116.0	116.9	10.6	12.0	11.0	11.2	12.7	10.1	97	91	95	94	0.4	1.2	0.6	0.7	10 •	10 •	10	ENE 3	E 4	NE 4
27	114.7	114.2	114.1	114.3	9.4	17.0	11.3	12.2	18.4	6.1	83	55	34	74	2.0	8.7	2.2	4.3	4	8	4	N 2	N 2	NNE 3
28	114.1	113.2	112.1	113.1	7.7	18.8	12.7	13.0	19.6	6.2	97	56	72	75	0.3	9.5	4.1	4.6	6	6	6	NE 3	NNE 5	N 5
29	111.4	110.8	112.7	111.6	10.8	17.3	9.0	11.5	18.4	7.8	79	44	71	65	2.8	10.9	3.4	5.7	3	4	0	NE 6	NNE 8	NNE 6
30	113.3	111.3	109.4	111.3	8.8	15.0	9.3	10.6	15.4	5.1	71	45	64	60	3.3	9.3	4.3	5.6	2	3	6	NE 3	N 3	E 2
31	109.3	109.8	110.2	109.8	9.1	16.6	13.4	13.1	17.8	3.5	68	36	56	53	3.7	12.2	6.8	7.6	1	7	1	ESE 3	SSE 5	E 2
M	113.8	113.5	113.2	113.5	8.7	14.0	10.4	10.9	15.5	6.2	82	61	79	74	2.1	6.5	2.8	3.8	6.3	6.9	6.7	3.8	4.9	3.9

Czerwiec – Juin

1	109.3	108.0	109.1	108.8	10.0	10.6	8.9	9.6	13.5	8.5	72	84	94	83	3.5	2.1	0.6	2.1	10	10 •	10	NE 7	NNE 7	NNE 7
2	111.7	113.3	115.1	113.4	10.0	17.2	11.0	12.3	17.3	8.3	69	63	87	73	3.8	7.2	1.6	4.2	8	6	0	NW 5	NE 6	C 0
3	117.1	118.2	118.3	117.9	10.4	13.0	10.3	11.0	14.5	8.0	82	69	85	79	2.2	4.6	1.9	2.9	9	9	4	W 2	NW 1	ENE 1
4	119.4	118.2	116.5	118.0	11.0	19.4	15.1	15.2	20.7	4.0	84	64	85	78	2.1	8.2	2.6	4.3	3	6	0	NE 1	NNE 4	NE 1
5	115.4	112.4	111.5	113.1	13.7	21.1	16.2	16.8	22.0	9.8	71	49	72	64	4.6	12.8	5.1	7.5	2	8	5	NE 3	E 6	SE 2
6	110.5	109.0	110.4	110.0	14.3	21.8	14.9	16.5	22.8	10.2	74	40	73	62	4.3	15.6	4.5	8.1	2	3	2	N 2	E 6	NE 3
7	111.4	110.4	109.9	110.6	11.8	20.6	15.6	15.9	21.2	6.7	80	54	59	64	2.8	11.0	7.2	7.0	2	5	1	E 2	NE 4	ENE 2
8	109.8	109.2	108.9	109.3	14.6	23.3	19.5	19.2	24.3	9.3	74	39	53	55	4.3	17.6	10.7	10.9	0	0	0	ESE 5	SE 8	E 5
9	109.3	108.2	108.6	108.7	16.4	22.9	18.4	19.0	23.4	13.4	62	46	80	63	7.0	15.0	4.3	8.8	2	5	4	ENE 5	E 8	NE 5
10	109.9	110.2	111.2	110.4	16.7	21.6	15.7	17.4	22.4	13.5	85	69	97	84	2.9	8.0	0.6	3.8	0	7	6	NNE 3	N 4	NNW 2
11	110.9	110.8	113.3	111.7	15.8	22.5	16.6	17.3	23.3	10.5	85	63	79	76	2.6	10.2	4.1	5.6	2	6	10	NE 3	NNE 5	NNW 5
12	114.5	115.8	116.4	115.6	14.8	16.8	13.6	14.7	17.7	13.1	83	58	76	72	2.9	8.0	3.7	4.9	9	9	10	NW 4	WNW 4	WNW 2
13	115.1	115.2	115.7	115.3	12.6	14.8	13.8	13.8	16.6	8.9	82	68	82	77	2.6	5.3	2.9	3.6	10	9	7	WSW 1	NW 1	N 2
14	117.6	118.4	118.4	118.1	14.3	20.4	15.2	16.3	21.8	9.7	83	60	81	75	2.7	9.7	3.4	5.3	3	3	4	N 5	NNE 5	C 0
15	118.4	116.8	114.0	116.4	14.8	21.9	19.0	18.7	23.6	6.8	72	46	59	59	4.7	14.2	9.1	9.3	0	4	8	C 0	SW 3	S 4
16	111.1	108.6	103.7	107.8	18.6	26.1	22.8	22.6	27.3	16.0	68	48	54	57	6.8	17.5	12.7	12.3	4	6	10	SSW 6	SSW 7	S 7
17	97.4	97.4	102.9	99.2	18.4	18.4	11.8	15.1	23.4	11.7	66	75	93	78	7.2	5.3	1.0	4.5	9	9	10 •	S 7	SW 9	SW 7
18	111.2	110.5	107.2	109.6	13.1	18.2	15.8	15.7	19.5	11.4	80	55	94	76	3.0	9.3	1.1	4.5	5	10	10 •	SW 5	SW 8	SW 8
19	106.4	109.6	114.9	110.3	16.3	17.2	16.0	16.4	20.1	13.3	82	70	65	72	3.2	5.8	6.3	5.1	6	6	6	WSW 8	WSW 7	W 6
20	117.6	118.1	118.7	118.1	14.9	20.3	15.6	16.6	20.6	11.1	74	52	77	68	4.3	11.3	4.1	6.6	6	6	3	W 5	W 5	WSW 2
21	118.7	117.3	113.2	116.4	15.4	20.9	18.8	18.5	22.8	13.3	81	55	63	66	3.4	11.2	8.1	7.6	9	9	3	WSW 1	W 1	SE 5
22	107.7	106.1	104.4	106.1	19.4	25.6	18.0	20.2	26.8	16.9	65	58	92	72	7.8	13.6	1.6	7.7	9	7	9	SSE 5	SW 6	C 0
23	107.4	110.3	113.3	110.3	16.6	19.6	15.9	17.0	20.8	15.6	82	65	89	79	3.5	7.9	2.0	4.5	9	9	3	SW 5	WSW 6	SW 1
24	114.1	115.2	116.5	115.3	16.9	23.2	19.2	19.6	24.0	12.7	80	51	73	68	3.8	14.0	6.0	7.9	9	5	8	SSW 3	WSW 5	C 0
25	118.0	116.9	115.7	116.9	17.8	25.2	20.4	21.0	27.1	12.0	66	42	76	61	6.9	18.5	5.7	10.4	2	3	0	SW 2	SW 6	C 0
26	112.8	113.0	119.2	115.0	19.9	22.7	17.4	19.4	27.8	14.7	79	84	80	81	4.9	4.6	4.0	4.5	4	10 • R	6	C 0	SW 4	NE 3
27	120.5	119.8	120.4	120.2	16.4	20.4	17.5	18.0	22.1	10.2	73	45	58	59	4.9	13.1	8.4	8.8	7	9	9	SW 2	WSW 5	WNW 4
28	124.7	124.8	121.9	123.8	15.4	17.5	16.0	15.7	19.7	9.6	72	48	62	61	4.4	10.4	7.0	7.3	3	6	2	NW 5	WNW 5	WSW 3
29	119.0	120.5	121.2	120.2	15.2	19.0	16.1	16.6	19.8	13.6	79	51	61	64	3.7	10.9	7.2	7.3	10	6	0	W 6	NW 8	WNW 2
30	120.7	117.1	111.3	116.4	14.2	21.4	17.6	17.7	23.9	9.7	86	46	71	68	2.4	13.9	5.9	7.4	1	4	7	W 4	SW 3	C 0
31																								
M	113.6	113.3	113.4	113.4	14.9	20.1	16.1	16.8	21.7	11.1	76	57	76	70	4.1	10.6	4.8	6.5	5.2	6.9	5.8	3.7	3.2	3.0

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	= 2^30 – 4^30; ⌓° 0^00 – 9, 21 – 24
2	8	•	•	⌓° 0^00 – 2 ⌣° 3 – 6 ⌓° 22 – 24
3	8	•	•	⌓° 0^00 – 2 ⌣° 3 – 6
4	8	3.8	•	•° 10^25...25 20^10...22^05 – 23^10 •¹ – 23^50 •° ... 24; par. wiatru 14 m/sek 3^30 – 8^45 ≫ – 16^05 (par. 18 m/sek), par. 14 m/sek 16^05 – 18^30 22^30 – 24
5	7	17.3	•	•° 0^00 1^10 ▽° 12^08–53 13^45–50 ▽▲° 15^55 ▽° 13^57 ▽¹ – 14^10 ▽° 14^30 16^23–33 16^58 17^05 ▽¹ – 17^17 •° 19^10 20^30; K¹ 13^35 13^50 14^40 S-N; par. wiatru 14 m/sek 0^00 1^10; = 9^30 11^30 19^30 – 24
6	6	1.6	•	•° 4^30 – 5^45 6^30 – 8^30 •• – 9^10 • – 10^25 • 13^15 ... 14^40; = 0^00 – 24
7	7	2.2	•	▽° 10^02–05 12^19–26 12^35 – 13^06 13^44 14^12 • 18^30 ... 21^30 – 24; = 0^00 – 3^40 5^55 7^30 22^30 – 24
8	7	2.6	•	•° 0^00 – 3^45 22^50 23^15 – 24; = 0^00 – 8^40 20^40 – 24
9	6	27.2	•	•° 0^00 – 0^35 10^30 – 14^15 • ¹ 14^40 ▽² 15^05 ▽¹ 15^30 ▽° 15^48 ▽¹ 16^25–43 ▽° 16^53 17^05 • 19^10 21^10 • ¹ 22^30 • ° 23^10; K¹ 14^40 15^40 NE; par. wiatru 13 m/sek 13^15 14^30, 14 m/sek 16^30 17^15 ≫ – 24 (par. do 19 m/sek); = 0^00 – 8^10
10	8	30.1	•	▽° 3^15–35 4^05–20 7^25–43 9^42–47 10^12 11^26 12^12–20 13^02 16^32 16^37–45 • ° 20^10 • ¹ – 24; ≫ 0^00 – 3^30 (par. 16 m/sek), par. wiatru 13 m/sek 3^30 – 4^30, do 14 m/sek 17^15 – 24
11	8	0.2	•	•° 0^00–10 • – 2^10 20^40 ... 22^15; par. wiatru 12 m/sek 0^00 – 8^30; = 22^20 – 24
12	8	•	•	= 0^00 – 6^05 ≡° – 7^15 = – 9^30 20^30 – 23^10
13	7	0.5	•	•° 20^40 23^10 – 24; = 1^30 – 8^30
14	7	•	•	•° 0^00–30 ... 1^45 5^20 6^45; = 1^45 11^05 20^30 – 24; ⌓° 22 – 24
15	8	0.0	•	•° 17^50 19^05; = 0^00 – 6^30; ⌓° 0^00 – 7
16	7	0.0	•	•° 10^05 – 50; = 13^30 – 16^30
17	7	2.3	•	•° 3^10 ... 4^20 7^10...40 20^30 ... 21^10 – 22^05 •¹ – 22^25 •° – 22^45; (K) 18^30 – 19^25 W-NE; ≡° 0^50 2^45 = – 10^30
18	8	1.4	•	•° 0^30 1^05 ▽¹ 10^10–20 ▽° – 1^35 14^02–30 14^42–57 • ° 21^50 ... 22^20; par. wiatru 13 m/sek 10^05 – 14^30; = 5^30 – 6^30 19^30 – 24
19	8	•	•	•° 4^50 – 6^10; = 0^00 – 5^30
20	8	0.4	•	▽° 11^20–25 11^35–38 ▽° 19^40–45
21	8	•	•	⌓° 2 – 9, 20 – 24
22	8	•	•	⌓° 0^00 – 2 ⌣° 3 – 5
23	8	•	•	par. wiatru 14 m/sek 7^40 – 9^05 ≫ – 13^35 (par. 17 m/sek), par. wiatru 14 m/sek 13^35 – 19^15
24	8	4.3	•	•° 11^10 ... 12^05 • ° 15^50 ... 17^40 • ° ... 18^20 – 23^10 ... 24
25	7	1.8	•	•° 1^00 ... 10 20^30 ... 22^15 • ° 22^40 – 24; = 4^30 – 7^50 17^30 – 24
26	6	5.9	•	•° 0^00 ... 4^20 •¹ – 4^50 •° – 16^05 •¹ – 16^15 •° – 17^40 22^20 ... 24; = 0^00 – 17^40 21^30 – 24
27	8	•	•	•° 0^00 ... 1^40; = 0^00 – 4^30 = – 6^20 = 23^00 – 24; ⌓° 19 – 24
28	8	0.0	•	▽° 15^05–20; par. wiatru do 16 m/sek 15^05–18; = 0^00 – 1^15 ≡° – 1^45 ≡° – 2^30 ≡¹ – 6^15 ≡° – 6^25 = – 8^20; ⌓° 0^00 – 10
29	8	•	•	par. wiatru 14 m/sek 11^20 – 19^30; ⌓° 1 – 10
30	8	•	•	⌓° 0^00 – 9, 21 – 24
31	8	•	•	⌓° 0^00 – 8, 21 – 24
Σ	–	101.6	–	

Czerwiec - Juin

1	7	2.4	•	•° 10^20 ... 11^30 – 13^30 ... 14^05 14^35 16^05 18^20...45 – 20^20; par. wiatru 12 m/sek 9^50 – 21; ⌓° 0^00 – 9
2	8	0.0	•	▽° 13^50–52, 16^45–47; par. wiatru 12 m/sek 0^00 – 1^30; = 21^30 – 24; ⌓° 20 – 24
3	7	•	•	= 0^00 – 4^30; ⌓° 0^00 – 9, 21 – 24
4	8	•	•	= 2^30 – 3^30 ≡° – 5^35; ⌓° 0^00 – 9, 21 – 24
5	8	•	•	⌓° 0^00 – 9
6	8	•	•	par. wiatru 14 m/sek 9^30 – 10^40; ⌓° 0^00 – 10, 21 – 24
7	8	•	•	⌓° 0^00 – 9, 22 – 24
8	7	•	•	par. wiatru do 14 m/sek 10^30 – 18^30; ⌓° 0^00 – 8
9	8	•	•	
10	8	3.6	•	▽° 14^10–12 ▽¹ – 14^20 ▽° – 14^15 15^20–30 16^50–55 19^12–15 ▽¹ – 19^20 ▽° – 19^25; = 20^50 – 23^45 ≡° – 24; ⌓° 1 – 8
11	8	0.0	•	▽° 20^30–33; ≡° 0^00 – 1^50 = – 3^30 = – 4^30
12	8	•	•	▽° 3^40–45
13	7	•	•	= 3^30 – 4^30 22^30 – 24; ⌓° 1 – 10
14	8	•	•	= 0^00 – 5^35; ⌓° 1 – 8, 20 – 24
15	8	•	•	= 2^30 – 4^20; ⌓° 0^00 – 9
16	8	0.0	•	▽° 17^47–51 18^03–06; ∞ 9^30 12^30; ⊕ 9^15–35
17	8	3.5	•	▽° 7^35 – 8^10 ▽° 12^35–55 •° 15^40 ... 16^50, 20^35 – 24; par. wiatru 14 m/sek 7^20 – 11^15 12^40–50 do 18 m/sek 18^10 – 24
18	8	8.8	•	•° 0^00 – 1^10 13^40 15^10 •¹ – 15^25 •° – 15^40 16^05–15 •¹ – 18^10 •° ... 19^15, 20^45 – 22^05 ▽° – 22^15; K° 22^05–20 SW-NE; = 1^10 – 2^15
19	8	0.2	•	•° 2^25 – 3^55 ▽¹ – 4^50 ▽° 9^17–21 13^12–17 16^02–05; K° 3^50 – 4^55 SW-NE; par. wiatru do 17 m/sek 8^30 – 20^30
20	8	•	•	⌓° 20 – 24
21	8	•	•	⌓° 0^00 – 9
22	7	5.6	•	▽° 18^05–07 ▽¹ – 18^32 ▽° – 18^35; (K) 17^46 – K 18^05–55 SW-NE; ⌒ 18^35–40
23	7	•	•	= 9^15 – 10^20, 20^30 – 24; ⌓° 21 – 24
24	8	•	•	= 0^00 – 5^30; ⌓° 0^00 – 9, 22 – 24
25	8	•	•	⌓° 0^00 – 8
26	7	0.3	•	▽° 12^15 – 13^05; (K) 12^10 – K 12^15 – 13^05 SW-NE, (K) 14^20 – 15^05 W-E; ⌓° 2 – 10, 22 – 24
27	8	•	•	= 3^20 – 9^50; ⌓° 0^00 – 9
28	8	•	•	
29	8	•	•	par. wiatru 14 m/sek 9^50 – 10^40
30	8	0.0	•	⌓° 1 – 10, 23 – 24
31				
Σ	–	24.4	–	

Szczecin – Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ *Lipiec – Juillet* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	WIATR D,v I	II	III
1	111.4	113.3	114.2	113.0	13.6	17.3	14.8	15.1	19.1	13.0	77	42	51	57	3.5	11.4	8.2	7.7	9	8	2	NW 5	WNW 5	NW 3
2	113.7	111.5	108.3	111.2	12.0	15.6	13.3	13.6	16.3	8.4	77	56	77	70	3.2	7.7	3.5	4.8	2	9	10 •	W 4	W 7	WSW 6
3	107.5	107.6	108.5	107.9	11.3	12.8	11.7	11.9	16.9	9.3	76	70	72	73	3.3	4.4	3.7	3.8	8	7	6	WSW 8	SW 4	WSW 4
4	107.9	108.3	108.2	108.1	9.8	12.4	11.9	11.5	16.0	7.6	87	81	80	83	1.6	2.7	2.8	2.4	10	9	4	SW 6	WNW 5	SW 2
5	108.5	109.1	110.0	109.2	10.7	16.1	11.0	12.2	17.4	9.0	89	53	84	75	1.5	8.6	2.1	4.1	9	6	6	SW 2	W 5	SW 4
6	108.9	109.0	110.7	109.5	10.2	13.2	11.8	11.8	16.9	8.5	91	76	85	84	1.1	3.7	2.0	2.3	10	7	3	SW 7	WSW 8	SW 1
7	110.4	108.1	107.4	108.6	11.2	17.1	13.6	13.9	18.5	8.6	92	67	89	83	1.0	6.3	1.8	3.0	10 •	9	6	SSW 3	SW 6	WSW 4
8	104.3	99.4	99.1	100.9	13.0	18.3	12.0	13.8	18.7	10.4	92	74	77	81	1.3	5.4	3.2	3.3	9	10	9	E 2	SSW 6	SW 8
9	103.2	105.2	109.4	105.9	10.6	12.2	11.4	11.4	15.3	8.5	81	90	86	86	2.4	1.4	1.8	1.9	9	9	6	WSW 7	WSW 6	WSW 1
10	112.0	113.1	115.3	113.5	10.8	15.3	11.5	12.3	16.9	8.2	86	62	90	79	1.8	6.7	1.4	3.3	7	8	9	WSW 3	SW 5	SW 2
11	117.4	116.7	114.6	116.2	11.2	16.8	14.4	14.2	18.4	8.5	88	63	93	81	1.7	7.1	1.1	3.3	8	10	10	SW 4	SSW 5	SSW 2
12	109.3	107.0	110.5	108.9	16.0	17.6	16.1	16.4	19.9	14.4	94	93	82	90	1.2	1.4	3.1	1.9	10 •	10 •	1	SW 8	SW 7	WSW 2
13	113.3	112.1	111.7	112.4	14.0	20.7	19.0	18.2	25.0	10.6	84	75	83	81	2.5	6.1	3.8	4.1	6	10	6	SW 2	SW 5	SW 2
14	113.7	113.2	115.5	114.1	16.4	28.3	19.8	21.1	30.1	14.9	94	54	87	78	1.1	17.5	3.1	7.2	8	5	10 • K	NE 2	SSW 3	WSW 3
15	116.5	116.8	117.5	116.9	18.0	24.2	18.6	19.8	25.6	14.1	93	72	95	87	1.4	8.4	1.0	3.6	9	7	9	C 0	SW 2	W 2
16	117.4	117.5	118.1	117.7	15.4	22.1	17.0	17.9	23.7	14.9	100	80	88	89	0.0	5.4	2.4	2.6	10 ≡	4	10	N 4	NNE 6	NE 8
17	117.5	116.3	117.0	116.9	14.8	16.2	15.0	15.2	17.0	14.4	91	94	87	91	1.5	1.2	2.2	1.6	10	10 •	10	NE 5	NNE 5	NE 7
18	117.9	117.9	119.3	118.4	14.6	22.3	16.8	17.6	23.6	12.2	85	58	82	75	2.5	11.3	3.5	5.8	6	3	2	NE 4	NE 6	NE 3
19	121.1	120.4	119.1	120.2	14.3	23.5	19.1	19.0	25.0	11.7	86	44	86	72	2.4	16.1	3.2	7.2	2	4	4	E 2	E 3	C 0
20	119.1	117.7	114.1	117.0	17.0	23.6	19.5	19.9	24.6	13.3	75	45	73	64	4.9	16.0	6.1	9.0	7	4	1	ESE 7	SE 8	ESE 1
21	110.5	107.0	106.4	108.0	17.4	25.0	17.3	19.2	25.4	14.9	78	61	97	79	4.4	12.3	0.6	5.8	3	3	10 •	ESE 6	SE 7	SW 1
22	108.1	108.6	107.9	108.2	16.4	21.8	18.0	18.6	22.7	15.6	90	62	85	79	1.9	9.9	3.0	4.9	9	5	3	SW 4	SW 4	C 0
23	106.2	106.6	106.0	106.3	15.2	16.2	16.0	15.8	20.4	12.3	93	84	82	86	1.2	2.9	3.3	2.5	10	9	1	SW 3	WSW 2	SW 3
24	104.6	105.9	109.3	106.6	15.1	18.1	16.0	16.3	20.7	13.3	91	67	68	75	1.5	7.0	5.8	4.8	10	8	9	WSW 7	WSW 8	WSW 4
25	109.3	108.6	108.5	108.8	14.4	21.0	13.0	15.4	22.4	12.0	78	46	91	72	3.6	13.4	1.4	6.1	0	7	8	SW 5	SW 6	SW 5
26	107.9	107.2	107.3	107.5	13.4	16.8	12.8	14.0	17.3	11.8	88	66	91	82	1.8	6.4	1.4	3.2	2	9	10 •	SW 7	SW 7	WSW 7
27	108.7	109.5	109.1	109.1	12.2	16.1	12.6	13.4	17.6	11.3	80	60	89	76	2.9	7.4	1.6	4.0	9	9	7	WSW 6	WSW 6	SW 4
28	110.6	110.5	107.8	109.6	12.3	14.1	13.2	13.2	15.7	10.6	83	82	92	86	2.4	2.9	1.3	2.2	9	10 •	10	WSW 7	WSW 7	SW 5
29	103.1	100.2	95.3	99.3	14.5	17.4	15.8	15.9	18.3	12.9	94	80	83	86	0.9	4.0	3.0	2.6	10 •	10	9	SW 5	SW 5	SW 6
30	92.7	92.3	97.4	94.3	14.6	17.4	14.4	15.2	17.7	14.3	89	61	78	76	1.8	7.7	3.6	4.4	10 •	9	9	SW 7	WSW 8	WSW 9
31	99.8	100.0	104.3	101.4	11.3	16.4	12.8	13.3	17.0	9.3	84	49	78	70	2.2	9.4	3.3	5.0	5	9	6	SW 5	W 4	WSW 2
M	110.1	109.6	109.9	109.9	13.6	18.3	14.8	15.4	20.0	11.6	87	67	83	79	2.1	7.5	2.8	4.1	7.6	7.6	6.6	4.7	5.5	3.6

Sierpień – Août

1	108.0	108.6	108.6	108.4	10.8	17.7	14.1	14.2	19.1	8.2	86	46	68	67	1.8	10.9	5.1	5.9	0	7	5	SW 5	WSW 6	SW 3
2	108.8	108.6	108.6	108.7	11.7	18.4	11.3	13.2	19.4	8.5	81	49	86	72	2.6	10.9	1.8	5.1	2	4	2	SW 2	W 3	SE 1
3	106.3	106.4	107.7	106.8	13.2	19.1	14.0	15.1	20.3	9.2	84	58	89	77	2.5	9.3	1.8	4.5	0	6	6	C 0	SW 9	S 1
4	110.8	112.8	113.7	113.1	14.6	17.9	14.4	15.3	19.1	12.4	93	66	77	79	0.7	6.9	3.8	3.8	10	9	1	W 4	WNW 6	WSW 2
5	118.3	118.3	116.1	117.6	13.4	21.0	16.8	17.0	23.6	11.0	82	51	84	72	2.8	12.2	3.1	6.0	8	1	2	W 1	WSW 3	SW 4
6	111.8	112.5	112.4	111.9	19.2	24.9	18.8	20.4	25.4	15.7	76	63	87	76	5.4	10.9	2.7	6.3	6	9	10	SW 6	WSW 2	NNE 5
7	111.2	109.7	113.4	111.4	16.4	20.6	17.0	17.8	20.9	16.3	94	87	94	92	1.1	3.1	1.2	1.8	10	10	7	NE 2	SW 5	W 1
8	114.7	113.0	114.6	114.1	15.0	13.1	13.9	14.0	18.1	12.9	93	98	94	95	1.1	0.4	0.9	0.8	9	10 •	10	C 0	ESE 5	NW 6
9	118.9	119.2	120.4	119.5	11.8	17.2	12.2	13.4	17.7	10.3	90	59	88	79	1.3	8.0	1.7	3.7	9	9	3	WSW 3	WNW 3	WSW 1
10	121.8	122.3	122.9	122.3	11.1	17.1	12.2	13.2	18.4	9.2	91	60	83	78	1.1	7.8	2.4	3.8	2	7	3	WSW 2	NE 3	C 0
11	123.1	124.0	124.1	123.7	11.8	16.2	11.6	12.8	17.8	8.5	90	71	90	84	1.3	5.2	1.3	2.6	9	9	0	WSW 1	NNW 3	C 0
12	123.5	123.3	123.8	123.5	11.3	18.3	12.9	13.8	20.2	9.9	98	70	86	85	0.4	6.4	2.1	3.0	10 ≡	7	0	W 2	N 3	N 5
13	123.2	123.0	121.7	122.6	9.6	19.6	13.0	13.8	19.9	6.1	100	53	84	79	0.0	10.7	2.5	4.4	9 ≡	2	3	WSW 2	N 6	WSW 1
14	120.7	120.6	120.8	120.7	12.0	19.5	14.2	15.0	20.3	10.2	88	59	78	75	1.7	9.2	3.6	4.8	9	6	9	WSW 1	NNE 3	NNE 2
15	121.6	121.6	121.2	121.5	12.6	16.7	12.6	13.6	18.5	10.9	96	73	91	86	0.5	5.5	1.4	2.5	10	7	3	C 0	NNE 2	E 2
16	120.8	119.7	118.1	119.5	11.5	19.7	14.4	15.0	21.1	8.3	94	55	85	78	0.9	10.3	2.5	4.6	4	3	0	E 2	NE 2	NE 2
17	117.7	117.7	117.1	117.5	11.1	21.5	15.5	15.9	23.1	5.9	99	53	83	78	0.2	12.0	3.0	5.1	0	5	0	C 0	C 0	NNE 1
18	117.5	118.2	118.7	118.1	14.0	23.4	17.4	18.0	24.9	11.5	89	52	76	72	1.8	13.9	4.8	6.8	2	3	0	C 0	N 1	ESE 1
19	120.9	121.8	120.9	121.2	13.5	23.2	18.2	18.3	23.6	9.3	94	69	81	81	0.9	8.9	4.1	4.6	3	2	0	C 0	NNE 2	ESE 2
20	118.6	117.0	114.8	116.8	17.2	26.5	18.3	20.1	27.3	14.6	94	51	85	77	1.2	16.8	3.0	7.0	6	4	10	C 0	SW 2	N 3
21	112.9	111.1	107.1	110.4	16.2	22.4	20.5	19.9	23.5	15.5	94	59	72	75	1.2	11.0	6.7	6.3	10	3	9	SW 2	SW 1	SSE 4
22	104.1	102.4	99.5	102.0	17.3	27.0	19.4	20.8	28.2	16.5	95	52	69	72	1.0	17.1	7.0	8.4	9	8	3	C 0	SE 7	SE 3
23	101.3	103.3	105.2	103.3	17.1	22.2	16.7	18.2	22.9	16.5	87	61	91	80	2.6	10.4	1.8	4.9	10	8	10 •	SW 4	SW 3	SE 1
24	106.6	108.5	107.9	107.7	15.0	18.0	16.8	16.6	21.9	13.8	98	88	94	93	0.3	2.4	1.2	1.3	6	9	10	W 1	SW 2	WNW 1
25	106.5	106.2	109.2	107.3	14.3	17.8	14.7	15.4	18.4	13.8	94	80	79	84	0.9	4.0	3.4	2.8	10	10	8	SW 2	SW 4	WSW 4
26	113.3	113.1	113.7	113.4	10.0	17.7	14.2	14.0	18.4	8.9	89	50	74	71	1.3	10.0	4.3	5.2	3	8	10	SW 4	W 4	SW 3
27	113.1	111.4	111.8	112.1	9.4	17.6	13.6	13.6	18.4	8.3	97	54	93	82	0.3	9.1	0.7	3.4	3	8	10 •	SW 2	WNW 3	SW 1
28	113.8	113.1	113.9	114.9	10.6	17.0	10.4	12.1	18.4	8.3	91	69	92	84	1.2	6.0	1.0	2.7	3	7	0	WNW 2	NW 3	C 0
29	112.4	110.7	111.8	111.6	12.0	14.6	13.8	13.6	16.3	5.5	72	78	91	80	4.0	3.6	1.3	3.0	6	10	8	SW 4	SW 3	SW 2
30	112.7	113.2	114.2	113.4	10.4	15.9	12.2	12.7	17.4	9.4	91	64	87	81	1.1	6.5	1.9	3.2	2	8	6	SW 4	WSW 5	SW 2
31	114.5	112.6	110.1	112.4	9.0	16.6	13.6	13.2	17.9	8.3	96	62	83	80	0.5	7.1	2.7	3.4	9	7	10	SW 2	SW 4	SE 4
M	114.5	114.4	114.5	114.5	13.0	19.3	14.8	15.5	20.7	10.8	91	63	84	79	1.4	8.6	2.7	4.2	6.1	6.7	5.1	1.9	3.5	2.2

Szczecin - Dąbie $H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 24\,m$ *Lipiec - Juillet 1965*

DNI	WIDZIALNOŚĆ V	OPAD R	OBLUDZENIE GU L	POGODA
1	8	.	.	•$^{0}5^{10}$ ... 6^{15}, ⌒ $^{0}0^{00}$ – 5
2	8	0.0	.	•$^{0}20^{55}$ ... 21^{50}, por. wiatru 12 m/sek 17^{50} 19^{10}, ⌒ $^{0}2$ – 8
3	8	1.6	.	▽$^{0}9^{35-37}$, 11^{16-17} ▽$^{1}11^{52-55}$ ▽$^{0}15^{45-54}$, por. wiatru 12 m/sek 11^{50} 12^{05}
4	7	0.4	.	•$^{0}7^{35}$ ... 9^{25} ▽$^{0}12^{30-35}$ 12^{45-50}, ⌒ $^{0}23$ – 24
5	8	1.1	.	▽$^{0}16^{18-28}$, ⌒ $^{0}0^{00}$ – 8
6	8	2.7	.	•$^{0}4^{40}$ – 5^{15}, 5^{35} ... 6^{20} ▽$^{0}9^{45}$, 10^{05} 10^{10-13} ▽$^{1}10^{15}$ ▽$^{0}10^{20}$, 11^{12-17} 11^{20-25}, 12^{40-47}, 13^{03-10}, 17^{35-42}, por. wiatru 12 m/sek 7^{30} 9^{40}, 12^{10-45}, 14^{10} 17^{30}, = 6^{20} – 8^{30}
7	7	0.1	.	•$^{0}4^{50}$ – 5^{15}, 6^{20}, 8^{45}, 18^{45} 19^{40}, = 5^{15} – 9^{20}
8	6	8.8	.	•$^{0}10^{45}$, 11^{40}, 14^{20-45} ▽^{0} $^{0}15^{25-30}$ ▽$^{1}15^{43}$ ▽$^{0}15^{53}$ ▽$^{1}16^{06}$, 17^{01-10} ▽$^{0}17^{25}$, ↖$^{0}15^{30}$ 16^{15} NE, por. wiatru 13 m/sek 18^{30} – 21^{15}, = 2^{50} – 9^{30}, 10^{30} – 15^{20}, ⌒ $^{0}1$ – 9
9	8	5.0	.	▽$^{0}9^{43-46}$, 10^{12-21} 11^{07-12}, 11^{40-44}, 12^{31-37} ▽$^{1}12^{09}$ ▽$^{0}12^{43}$ ▽$^{1}12^{45}$ ▽$^{0}12^{52}$ ▽$^{0-1}13^{03-09}$, 13^{15-20}, 16^{48-53}, 19^{32-35} ▽$^{1}19^{42}$ ▽$^{0}19^{45}$, por. wiatru 12 m/sek 14^{30} – 18^{30}, ⌒ 19^{42} – 20^{10}
10	8	0.3	.	▽$^{0}12^{25-30}$ 14^{45-53}, = 22^{50} – 24
11	8	3.1	.	•$^{0}13^{05}$, 14^{40}, 18^{40} 19^{10}, = 0^{00} – 1^{50}
12	5	16.8	.	•$^{0}2^{25}$, 3^{10} 6^{30} •$^{1}7^{10}$ ... $^{0}7^{25}$ 9^{15} 10^{10} •^{1} – 11^{15}, •$^{0}12^{45}$ •^{1} – 13^{10} •^{2} – 13^{40} •^{1} – 13^{50} •^{0} – 14^{15}, por. wiatru 12 m/sek 1^{30} – 4^{30}, ⌒ $^{0}22$ – 24
13	7	.	.	⌒ $^{0}0^{00}$ – 8, 21 – 24
14	8	13.4	.	▽^{0} $^{0}14^{29-35}$ ▽^{2} – 14^{50} ▽^{0} – 15^{05}, 19^{45} 20^{10} ▽^{2} – 20^{15} ▽^{1} – 22^{52} ▽^{0} – 22^{55}, ↖^{0} NW 14^{25} – 15^{10} NE, ↖ NW 19^{45} – 22^{50} S, ⚡ 14^{38-43} (por. 19 m/sek), por. wiatru 14^{43-50}, = 5^{15} – 6^{40}, ⌒ 0^{00} – 9
15	7	.	.	= 2^{30} – 6^{40}, 18^{30} – 24, ⌒ $^{0}18$ – 24
16	7	.	.	= 0^{00} – 5^{25} ≡ ^{0} – 7^{45} = – 10^{30}, ⌒ $^{0}0^{00}$ – 10
17	7	5.6	.	•$^{0}9^{20}$ ... 10^{00} – 16^{40} ▽$^{0}19^{12}$ – 17, 21^{48} – 55
18	8	.	.	
19	8	.	.	⌒ $^{0}1$ – 8, 21 – 24
20	8	.	.	⌒ $^{0}0^{00}$ – 8, 22 – 24
21	8	8.4	.	▽$^{0}14^{42}$ – 15^{04}, 15^{10} – 33, 15^{50} – 16^{07}, 16^{41-52} ▽^{1} – 16^{57} ▽^{0} – 17^{35} •$^{0}18^{45}$ 19^{15} – 21^{30}, ↖$^{0}14^{45}$ 15^{40} SE – NW, ↖$^{0}15^{42}$ 17^{25} SE – N, = 17^{00} – 24, ⌒ $^{0}0^{00}$ – 7
22	8	.	.	= 0^{00} – 7^{45}, 22^{30} – 24
23	7	8.3	.	•$^{0}7^{05}$ – 8^{35} – 9^{02} •^{1} – 9^{20} •^{0} – 10^{20} •^{1} – 10^{45} •^{0} – 11^{50}, = 0^{00} – 11^{30}, ⌒ $^{0}1$ – 7, 21 – 24
24	8	0.3	.	•$^{0}1^{50}$, 2^{10} ▽$^{0}12^{40}$ – 14^{30-37}, 17^{53-56}, 18^{55} – 19^{04}, por. wiatru 12 m/sek 13^{15} – 16^{30}, = 5^{30} – 7^{30}, ⌒ $^{0}0^{00}$ – 1
25	8	4.0	.	•$^{0}15^{52-57}$ ▽^{1} – 16^{05} •^{0} – 16^{34} 18^{50} 19^{45}, ↖$^{0}15^{40}$ – 16^{00} – 16^{25} SW – NE, ⚡ 15^{55} – 16^{06} (por. 18 m/sek)
26	8	4.0	.	•$^{0}13^{32-37}$ •^{0} ... 14^{40} 16^{50} ... 17^{05} •^{1} – 17^{40} •^{0} – 21^{40} 23^{10} ... 30, por. 12 m/sek 8^{35} – 19^{40}
27	8	1.6	.	▽$^{0}17^{42}$ – 18^{20}, 18^{25-35} •$^{0}22^{40}$ ... 23^{15}, ↖$^{0}17^{45}$ W – 18^{00} – E 18^{10}, por. wiatru 10^{30} – 14^{30}
28	7	6.1	.	•$^{0}12^{15}$ 13^{30} •^{1} – 13^{45} •^{0} – 17^{30} •^{1} – 18^{10} •^{0} – 19^{25}, 21^{30} – 24, por. wiatru do 14 m/sek 6^{30} – 12^{30}, = 20^{30} – 24
29	7	5.4	.	•$^{0}0^{00}$ – 1^{40}, 2^{20} 6^{15} – 11^{05} ▽$^{0}14^{07}$ 15^{00} •^{0} – 16^{35}, 17^{12} – 18^{30}, por. wiatru do 17 m/sek 14^{32} – 15^{05}, = 0^{00} – 12^{15}
30	8	0.3	.	▽$^{0}0^{28-32}$ •$^{0}1^{45}$ – 2^{40} ▽$^{0}5^{51}$ – 6^{08}, 6^{34} – 7^{15}, 8^{57} – 9^{03}, 14^{30} – 47, 15^{06} – 14, por. wiatru do 17 m/sek 7^{30} – 15^{06} ⚡ – 15^{12} (por. 19 m/sek), por. wiatru 14 m/sek 15^{12} – 20^{30}
31	8	.	.	⌒ $^{0}22$ – 24, ⊕ 9^{10} – 10^{30}
Σ	–	97.3	–	

Sierpień - Août

1	8	.	.	⌒ $^{0}0^{00}$ – 8, 22 – 24
2	8	0.0	.	▽$^{0}19^{28-45}$, ⌒ $^{0}0$ – 8
3	8	1.2	.	
4	8	0.9	.	•$^{0}0^{10}$ – 1^{40} •^{1} – 2^{10} •^{0} – 2^{45}, 6^{35-45} ▽$^{1}11^{26-35}$, = 2^{45} – 11^{40}, ⌒ $^{0}21$ – 24
5	8	.	.	⌒ $^{0}0^{00}$ – 9, 22 – 24
6	7	1.2	.	▽$^{0}21^{36}$ – 22^{35}, (↖)$^{0}12^{15-40}$ SW – NE, ↖$^{0}21^{25}$ – 22^{15} S – N, ⌒ $^{0}0^{00}$ – 6, 20 – 24
7	7	0.5	.	▽$^{0}4^{06-15}$, 5^{38}, 6^{04}, 6^{22-34} •$^{0}10^{05}$ – 11^{15}, 12^{10} ... 15^{10} ... 16^{20}, = 4^{30} – 12^{20}, 17^{30} – 24
8	6	13.8	.	•$^{0}8^{20}$ – 11^{10} •^{1} – 12^{25} •^{2} – 12^{32} •^{1} – 12^{50} •^{0} – 13^{43} ▽$^{0}16^{50}$ – 17^{40}, = 0^{00} – 7^{30}, 13^{43} – 14^{30}, 15^{15} – 24
9	8	.	.	= 0^{00} – 4^{30}, ⌒ $^{0}21$ – 24, ⊕ 8^{10} – 40
10	8	.	.	⌒ $^{0}0^{00}$ – 10, 20 – 24
11	8	.	.	= 21^{40} – 23^{45}, ⌒ $^{0}0^{00}$ – 2 ⌒ $^{1}3$ – 10 ⌒ $^{0}20$ – 24
12	7	.	.	= 5^{30} – 6^{45} ≡ ^{0} – 7^{35} = – 11^{30} = 23^{30} – 24, ⌒ $^{0}0^{00}$ – 3 ⌒ $^{1}4$ – 10 ⌒ $^{0}20$ – 24
13	8	.	.	= 0^{00} – 1^{45} ≡ ^{0} – 4^{30} ≡ ^{1} – 5^{30} ≡ ^{0} – 6^{15} ≡ ^{1} – 6^{25} ≡ ^{0} – 7^{10} = – 7^{35}, ⌒ $^{0}0^{00}$ – 2 ⌒ $^{1}3$ – 7 ⌒ $^{0}8$ – 9, 20 – 24
14	8	1.6	.	= 6^{30} – 8^{30}, ⌒ $^{0}0^{00}$ – 10, 20 – 24
15	8	0.4	.	•$^{0}2^{15}$ – 3^{05} – 4^{45} 5^{20} – 6^{40} ▽$^{0}7^{18-32}$, 9^{50} – 10^{02}, ⌒ $^{0}0^{00}$ – 2
16	8	.	.	= 1^{15} – 4^{30} = – 5^{15} = – 6^{30}, ⌒ $^{0}1$ – 10, 20 – 24
17	8	.	.	= 0^{30} – 6^{30}, ⌒ $^{0}0^{00}$ – 3 ⌒ $^{1}4$ – 9 ⌒ $^{0}21$ – 24
18	7	.	.	⌒ $^{0}0^{00}$ – 9
19	7	.	.	= 1^{00} – 8^{30} ∞ 9^{30} 17^{30} = 23^{30} – 24, ⌒ $^{0}1$ – 8, 20 – 24
20	7	.	.	= 0^{00} – 9^{30} ∞ – 16^{30}, 17^{30} – 20^{30} = – 24, ⌒ $^{0}0^{00}$ – 10
21	7	0.0	.	•$^{0}8^{20}$ ... 9^{20}, = 0^{00} – 11^{40}, ⌒ $^{0}2$ – 8
22	7	.	.	•$^{0}3^{50}$ ... 4^{40}, = 3^{30} – 9^{30}
23	8	12.6	.	•$^{0}20^{25}$ – 21^{15} •^{1} – 24, = 6^{30} – 9^{15}
24	6	.	.	•$^{1}0^{00-15}$ •^{0} – 0^{30}, ≡ $^{0}5^{40}$ – 6^{45} = – 13^{30} 19^{30} – 24, ⌒ $^{0}19$ – 24
25	7	0.2	.	▽$^{0}16^{25-40}$ •$^{0}17^{30}$ ... 18^{15}, = 0^{00} – 10^{30}, 19^{30} – 18^{30}, ⌒ $^{0}0^{00}$ – 9
26	8	.	.	⌒ $^{0}1$ – 9
27	8	0.0	.	•$^{0}20^{40}$ – 22^{15}, = 4^{30} – 9^{45}, ⌒ $^{0}1$ – 11, 20^{00-40}
28	8	0.0	.	▽$^{0}13^{02-04}$, ↙ NE 18^{20} – 21^{10}, = 3^{30} – 7^{35}, 21^{50} – 23^{45} ≡ ^{0} – 24, ⌒ $^{0}19$ – 24
29	6	2.5	.	•$^{0}9^{05}$ ... 30, 11^{20} – 12^{30}, 13^{05} ... 14^{05} •^{1} – 14^{40} •^{0} – 15^{20} ▽$^{0}19^{35-55}$, ≡ $^{0}0^{02}$ – 2^{40} = 12^{30} – 16^{30}, ⌒ $^{0}0^{00}$ – 9
30	8	.	.	
31	8	0.0	.	•$^{0}22^{15}$ ... 23^{35}, = 3^{30} – 7^{25} ≡ ^{0} – 8^{15} = – 8^{45}, ⌒ $^{0}1$ – 11
Σ	–	34.9	–	

Szczecin – Dąbie *φ = 53°24'* *λ = 14°37'* *Wrzesień – Septembre* *1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	108.3	110.7	114.4	111.1	12.8	17.5	14.8	15.0	18.4	11.9	86	64	93	81	2.1	7.2	1.1	3.5	10	9	10 •	S 1	SW 2	WNW 2
2	114.0	114.0	112.8	113.6	15.2	23.4	21.4	20.4	24.9	14.1	96	60	71	76	0.8	11.4	7.4	6.5	10	2	10	E 3	ESE 9	ESE 7
3	107.1	105.6	107.8	106.8	19.3	24.8	18.4	20.2	25.8	18.0	71	50	79	67	6.4	15.7	4.5	8.9	3	10	10	ESE 9	SSW 8	SW 2
4	107.4	106.9	108.5	107.6	13.8	21.2	14.6	16.0	21.8	13.4	91	44	80	72	1.5	14.0	3.3	6.3	4	4	9	SE 1	SE 7	SW 2
5	108.5	108.6	107.9	108.3	13.5	19.2	13.9	15.1	21.2	12.9	92	54	91	79	1.3	10.2	1.5	4.3	9	7	0	SW 2	SW 2	C 0
6	105.2	104.1	104.0	104.4	10.8	17.9	12.6	13.5	20.4	7.5	99	77	98	91	0.2	4.6	0.4	1.7	8	9	10 •	E 1	SW 5	SW 4
7	101.2	101.7	104.0	102.3	11.8	12.5	12.2	12.2	13.9	11.2	95	92	86	90	1.0	1.2	2.0	1.4	10	10 •	10	SW 5	WSW 6	WSW 7
8	107.6	109.1	107.7	108.2	11.8	17.3	15.7	15.1	18.7	10.2	90	58	70	73	1.3	8.3	5.3	5.0	9	7	8	SW 6	SW 8	SSW 7
9	105.2	109.3	110.7	108.4	13.4	18.4	14.2	15.6	20.0	13.7	82	50	84	72	3.2	10.7	2.5	5.5	10	8	10	SSW 8	SW 6	SE 4
10	107.4	108.6	111.3	109.1	13.0	15.6	11.6	13.0	17.3	11.5	99	83	95	92	0.2	3.0	0.6	1.3	10 •	9	9	NE 2	NW 2	SE 2
11	111.4	111.9	112.7	112.0	11.4	15.1	9.2	11.2	16.3	8.8	100	75	95	90	0.0	4.3	0.6	1.6	10 •	9	3	SW 2	WSW 2	ESE 2
12	111.1	110.5	109.1	110.2	10.2	17.4	11.4	12.6	17.6	6.3	81	55	89	75	2.4	9.0	1.5	4.3	4	8	9	SW 3	SW 8	SW 4
13	109.0	109.9	109.9	109.6	9.4	14.0	10.8	11.2	15.8	8.8	96	77	92	88	0.5	3.7	1.0	1.7	8	9	6	SW 4	WSW 5	SW 2
14	111.8	114.4	116.3	114.2	10.6	15.8	13.3	13.2	16.8	10.0	92	69	86	82	1.0	3.3	2.1	2.9	10	7	9	SW 3	SW 5	W 3
15	119.7	122.1	124.5	122.1	11.0	15.4	12.3	12.8	16.9	9.8	92	72	90	85	1.0	3.0	1.4	2.3	9	9	0	W 3	W 2	SW 2
16	124.8	125.0	119.8	122.5	9.1	20.4	17.0	15.9	21.9	6.6	99	56	66	74	0.2	10.5	6.7	5.8	0	2	0	C 0	S 6	S 8
17	117.8	117.5	115.7	117.0	13.4	21.3	14.7	16.0	22.0	12.8	88	67	93	83	1.8	8.3	1.1	3.7	2	9	4	SW 3	SW 2	SE 4
18	110.8	108.1	110.4	109.8	17.0	24.3	14.0	17.3	24.7	13.9	81	58	80	73	3.8	12.6	3.2	6.5	2	6	3	SSW 5	SSW 8	SW 4
19	115.1	119.1	124.3	119.6	12.0	16.4	12.6	13.4	16.7	10.6	80	53	70	68	2.8	8.8	4.4	5.3	6	6	9	WSW 5	W 8	W 3
20	129.4	132.0	133.8	131.7	8.4	16.1	10.8	11.5	17.4	7.4	90	62	86	79	1.0	7.0	1.8	3.3	9	5	3	WSW 2	NNW 3	SW 2
21	133.2	132.3	128.7	131.4	8.8	16.4	12.5	12.6	17.0	7.5	89	60	76	75	1.2	7.4	3.6	4.1	10	8	4	SW 3	SW 4	SW 3
22	123.8	122.1	117.8	121.2	9.5	18.9	13.3	13.8	20.3	8.7	86	59	82	76	1.7	9.0	2.8	4.5	8	3	0	SW 4	SW 5	SW 3
23	116.0	114.0	111.3	113.8	6.4	21.6	13.2	13.6	22.5	5.3	94	52	93	80	0.6	12.3	1.1	4.7	2	1	0	C 0	S 3	E 2
24	111.2	111.8	111.3	111.4	11.6	21.5	12.8	14.7	22.6	10.8	90	62	95	82	1.3	9.8	0.7	3.9	0	0	0	SW 2	SW 3	E 1
25	109.7	107.9	105.9	107.8	10.8	22.0	15.8	16.1	23.6	8.9	94	60	82	79	0.9	10.6	3.2	4.9	3	3	0	ESE 4	SE 6	SE 3
26	103.3	101.2	101.6	102.0	12.5	22.6	15.8	16.7	23.2	11.6	87	50	73	71	1.9	13.7	4.4	6.7	0	1	3	ESE 3	SE 11	SE 4
27	99.7	95.2	103.4	99.4	12.0	18.4	10.8	13.0	19.1	10.6	94	80	82	85	0.8	4.3	2.3	2.3	7	10 •	0	E 3	SE 9	SSW 5
28	103.2	102.1	101.8	102.4	10.4	17.8	13.0	13.6	19.3	7.4	85	67	98	83	1.9	6.7	0.4	3.0	9	10	10 •	ESE 6	S 3	SW 1
29	103.1	105.3	108.4	105.6	11.4	15.2	10.8	12.0	16.5	10.2	96	78	86	87	0.5	3.9	1.8	2.1	10	9	0	SW 3	SW 5	SW 3
30	110.4	111.1	113.6	111.7	7.4	15.5	12.1	11.8	16.9	6.3	94	73	95	87	0.6	4.8	0.7	2.0	9	9	0	C 0	ESE 6	NE 2
31																								
M	111.3	111.7	112.3	111.8	11.7	18.3	13.5	14.3	19.6	10.2	90	64	85	80	1.5	8.1	2.4	4.0	6.7	6.6	5.0	3.2	5.3	3.3

Październik – Octobre

1	116.7	118.1	118.7	117.8	9.4	21.6	14.0	14.8	22.4	7.5	97	58	89	81	0.3	10.9	1.8	4.3	2	3	0	E 3	ESE 4	E 2
2	117.6	115.3	116.0	116.3	9.6	19.8	15.7	15.2	20.3	9.4	97	64	96	86	0.4	8.3	0.7	3.1	0	1	10 •	E 3	ESE 9	S 1
3	119.6	121.4	122.2	121.1	12.2	14.2	9.5	11.4	17.3	9.4	96	82	99	92	0.5	2.9	0.2	1.2	10	7	2 ≡	SW 2	SW 3	C 0
4	123.9	124.3	124.1	124.1	6.3	16.6	8.8	10.1	17.6	5.7	100	72	95	89	0.0	3.3	0.6	2.0	10 ≡	2	3	C 0	NE 1	C 0
5	124.8	125.6	125.1	125.2	6.8	10.4	9.7	9.2	12.9	5.7	100	96	92	96	0.0	0.5	0.9	0.5	10 ≡	9	10	ESE 1	ESE 3	SE 3
6	123.9	123.2	121.3	122.8	9.0	10.4	5.6	6.6	12.2	3.1	92	87	100	93	1.0	1.6	0.0	0.9	10	10	10 ≡	SE 4	SE 3	ESE 1
7	118.8	118.0	116.6	117.8	7.0	12.1	6.2	7.9	13.3	2.9	100	89	100	96	0.0	1.5	0.0	0.5	10 ≡	8	0 ≡	SE 1	C 0	C 0
8	116.8	119.0	121.3	119.1	9.6	12.5	8.2	9.6	14.8	5.5	100	87	86	91	0.0	1.9	1.5	1.1	10 • ≡	9	4	W 1	NNW 2	NE 5
9	121.7	120.8	120.4	121.0	4.9	12.2	4.4	6.5	13.4	3.5	97	70	93	87	0.3	4.3	0.6	1.7	4	9	4	W 2	NE 2	C 0
10	118.9	118.5	118.8	118.7	3.7	12.4	6.7	7.4	13.0	2.0	93	67	91	84	0.6	4.8	0.9	2.1	9	9	9	WSW 1	NW 2	WSW 1
11	117.5	117.7	121.7	119.0	4.0	12.8	6.2	7.3	13.3	3.5	97	74	83	85	0.2	3.9	1.6	1.9	0	4	4	WSW 2	NNW 3	E 2
12	127.3	128.8	128.1	128.1	-1.9	11.2	4.9	4.8	12.2	-3.2	100	48	82	77	0.0	6.9	1.6	2.8	10 ≡	1	2	C 0	SW 3	SW 3
13	126.1	123.6	121.8	123.8	2.4	12.8	8.0	7.8	14.3	1.7	82	51	89	74	1.3	7.3	1.2	3.3	4	5	9	SW 4	SW 5	SW 3
14	121.3	120.6	118.7	120.2	4.1	11.4	4.4	6.1	14.2	0.6	100	85	100	95	0.0	2.0	0.0	0.7	10 ≡	6	4 ≡	WSW 1	C 0	C 0
15	117.0	115.8	113.9	115.6	-0.4	12.7	12.6	9.4	16.0	-1.0	100	76	81	86	0.0	3.6	2.7	2.1	10 ≡	8	2	C 0	SW 4	SW 3
16	114.7	117.3	120.5	117.5	10.7	11.2	8.8	9.9	12.7	7.6	95	91	86	91	0.7	1.2	1.5	1.1	10 •	10	6	NW 2	WNW 4	W 4
17	126.4	127.9	127.6	127.3	5.2	12.2	7.4	8.0	12.4	5.2	92	62	84	79	0.7	5.4	1.6	2.6	2	7	5	SW 2	NW 3	W 2
18	125.4	125.3	126.9	125.9	8.2	11.8	5.4	7.7	13.3	5.3	94	87	92	91	0.6	1.8	0.7	1.0	10	10 •	0	SW 4	WSW 4	WSW 2
19	127.9	128.7	129.6	128.7	3.6	11.4	5.6	6.6	12.6	2.8	98	69	98	88	0.1	4.2	0.2	1.5	4	9	3	SW 1	NW 2	WSW 2
20	131.5	133.2	133.5	132.7	5.0	11.2	3.8	6.0	12.2	3.3	100	73	98	90	0.0	3.6	0.1	1.2	10 ≡	5	0	E 1	SE 4	E 2
21	134.5	135.4	135.8	135.2	1.7	10.8	1.4	3.8	11.0	0.6	98	59	89	82	0.1	5.4	0.8	2.1	7	3	0	E 2	SE 4	SE 2
22	137.0	137.0	135.4	136.5	-4.3	8.5	-1.5	0.3	9.7	-4.4	96	64	100	87	0.2	4.0	0.0	1.4	0 ≡	0	0 ≡	C 0	NE 1	C 0
23	133.5	132.2	130.9	132.2	-2.7	12.2	5.2	5.0	12.4	-4.5	97	55	98	83	0.1	6.4	0.1	2.2	1	7	9 ≡	WSW 1	C 0	NE 1
24	130.9	131.5	130.7	131.0	6.8	9.9	1.2	4.8	10.0	1.1	94	66	100	87	0.6	4.2	0.0	1.6	10	10	0 ≡	C 0	E 5	C 0
25	129.7	129.4	127.7	128.9	-0.7	7.2	6.4	4.8	9.9	-1.8	100	97	91	96	0.0	0.3	0.9	0.4	10 ≡	4	10	C 0	NE 3	SE 3
26	125.0	121.7	119.5	122.1	5.2	10.6	2.5	5.2	10.9	2.2	94	64	100	86	0.5	4.6	0.0	1.7	10	0	10 ≡	SE 3	SSE 6	SW 1
27	118.6	117.3	114.0	116.6	2.0	5.7	10.9	7.4	11.2	1.8	100	98	79	92	0.0	0.2	2.7	1.0	10 ≡	10	0	SW 3	WSW 4	SW 6
28	111.9	111.3	110.2	111.1	10.8	14.8	12.8	12.8	16.0	8.9	86	76	84	82	1.8	4.0	2.4	2.7	10	9	4	SW 7	SW 6	SW 6
29	108.3	107.5	113.4	109.7	11.7	12.7	7.6	9.9	13.3	7.4	87	93	79	86	1.8	1.1	2.2	1.7	10	10 •	7	SW 6	SW 6	WSW 5
30	116.1	115.8	111.1	114.3	5.0	11.4	9.9	9.0	12.2	4.6	92	70	71	78	0.7	4.1	3.6	2.8	0	8	10	SW 7	SW 7	SW 8
31	105.7	106.1	107.1	106.3	8.6	10.8	5.6	7.6	10.9	5.1	76	62	85	74	2.8	5.0	1.4	3.1	7	9 •	6	WSW 7	WSW 8	WSW 5
M	122.2	122.2	122.0	122.1	5.3	12.1	7.0	7.8	13.5	3.3	95	74	91	87	0.5	3.9	1.0	1.8	7.1	6.5	4.6	2.3	3.6	2.4

Szczecin - Dąbie $H_s = 1\,m$ $H_b = 6.9\,m$ $h_w = 24\,m$ *Wrzesień - Septembre 1965*

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ LODU h	POGODA
1	7	0.6	•	•^{0} 1^{15}...^{45} 6^{05-25} 19^{05} 21^{15} 22^{40} 24; = 7^{15}–11^{20} 18^{30}–24
2	7	•	•	•^{0} 0^{00}–2^{20}, 3^{10}...5^{05-40}...6^{15}, por. wiatru do 16 m/sek 9^{30}–17^{50}; = 0^{00}–8^{40}
3	7	1.4	•	•^{0} 21^{25}–24; por. wiatru 14 m/sek 8^{30}–15^{15}; ⊕ 9^{30}–10^{15}
4	8	0.0	•	•^{0} 0^{00}–2^{25}; por. wiatru 12 m/sek 11^{30}–14^{30}
5	7	•	•	•^{0} 0^{50}–1^{45}; = 19^{30}–24; ⌓^{0} 19–24
6	7	2.8	•	•^{0} 17^{10}...20^{10} •^{1}–21^{20} •^{0}–23^{10}; = 0^{00}–1^{15} =^{0}–2^{30} =^{1}–5^{30} =^{0}–6^{20} =–9^{10} ∞ 13^{20}–15^{30} = 23^{10}–24; ⌓^{0} 0^{00}–9
7	6	14.8	•	•^{0} 5^{40}–6^{20}, 7^{10}...8^{30}–9^{02} •^{1}–9^{40} •^{0}–13^{40}, 14^{12-45} ▽^{1}–14^{53} ▽^{0}–15^{00} •^{0}–20^{15}; = 0^{00}–13^{30}
8	7	0.0	•	por. wiatru 14 m/sek 9^{35}–13^{30}; = 1^{30}–9^{30}
9	8	16.6	•	•^{0} 5^{40}–6^{10}, 21^{05}–22^{40}, por. wiatru 12 m/sek 12^{30}–13^{30}
10	7	15.6	•	•^{0} 0^{00}–2^{05} •^{1}–5^{50} •^{0}–8^{10} •^{1}–10^{30} •^{0} 11^{10}; = 2^{30}–12^{30}, 19^{30}–24
11	8	2.6	•	•^{0} 0^{20}–6^{20}, 7^{40}, 8^{35}, 10^{36} •^{0} ▽^{0}–19^{03-06}, 18^{25-36} •^{1}–18^{45} •^{0} ▽^{0}–19^{08}; ↖^{1} 18^{35-40} SW-NE; = 0^{00}–9^{45} =^{0} 23^{40}–24
12	7	2.6	•	•^{0} ▽^{1} 14^{50}–15^{05} 16^{40-46} 17^{15-30} 18^{05-10} 18^{15-25}; =^{0} 0^{00}–1^{35} =–2^{30}
13	7	•	•	= 1^{00}–7^{35} =^{0}–8^{35} =–11^{40}, 21^{30}–24; ⌓^{0} 19–24
14	7	0.0	•	•^{0} 7^{20}–8^{15} •^{0} ▽^{1} 14^{45}–15^{05}; = 0^{00}–12^{30}, 20^{30}–24; ⌓^{0} 0^{00}–7, 20–24
15	8	•	•	= 0^{00}–6^{30}, 18^{15}–24; ⌓^{0} 0^{00}–11, 19–24
16	7	•	•	= 0^{00}–1^{10} =^{0}–3^{30} =^{1}–4^{45} =^{0}–5^{40} =^{1}–6^{10} =^{0}–6^{40} =–9^{30}, 18^{30}–20^{10}; ⌓^{0} 0^{00}–10
17	7	•	•	= 4^{50}–12^{30}, 17^{30}–23^{30}; ⌓^{0} 3–8, 20–24
18	7	2.0	•	•^{0} ▽^{0} 16^{57-59} •^{2} ▽^{2} 17^{03} •^{0} ▽^{0} 17^{12} •^{2} ▽^{2} 17^{16} •^{0} ▽^{0} 17^{30}; ↖^{2} 16^{55}–16^{58}–17^{35} SW-NE; por. wiatru 17 m/sek 16^{56}–17^{05}; = 4^{30}–8^{30} ∞–16^{57} = 17^{30}–24; ⌓^{0} 0^{00}–8
19	8	•	•	por. wiatru 14 m/sek 8^{30}–14^{15}; = 0^{00}–4^{30}
20	8	•	•	⌓^{0} 1–9, 21–23
21	7	•	•	⌓^{1} 0^{00}–6 ⌓^{0} 7–9
22	6	•	•	= 4^{30}–10^{30} ∞–18^{20} =–24
23	6	•	•	= 0^{00}–1^{10} =^{0}–1^{55} =–5^{45} =^{0}–6^{25} =–10^{30} ∞–17^{30} =–24, ⌓^{0} 1–11, 18–24
24	6	•	•	= 0^{00}–11^{45} ∞–17^{30} =–24; ⌓^{0} 0^{00}–2 ⌓^{1} 3–10 ⌓^{0} 11–12, 19–24
25	7	•	•	= 0^{00}–10^{30} ⌓^{0} 0^{00}–9, 23–24
26	7	•	•	≫ 9^{30}–15^{40}, ⌓^{0} 0^{00}–8
27	6	0.2	•	•^{0} ▽^{0} 9^{31-34} •^{0} ▽^{0} 10^{45} 11^{10}, 11^{42} 12^{15} •^{0} 12^{46} 13^{06} •^{0} 13^{50} $14^{10...40}$, por. wiatru do 14 m/sek 11^{35}–13^{32} ≫–14^{25} (por. 16 m/sek), por. wiatru 14 m/sek 14^{25}–16^{25} ≫–17^{15} (por. 18 m/sek), por. wiatru do 14 m/sek
28	8	3.6	•	•^{0} 17^{35}–23^{40}; = 16^{30}–24; ⌓^{0} 1–10 [27.IX: 17^{15}–20^{10}; = 5^{30}–7^{40}; ⌓^{0} 1–8
29	6	•	•	= 0^{00}–13^{30}; ⌓^{0} 20–24
30	7	0.0	•	•^{0} $3^{00...20}$; = 3^{30}–8^{30} = 18^{20}–19^{40} =–19^{45} =^{0}–19^{55} =–22^{30} =^{0}–24; ⌓^{0} 0^{00}–8, 20–24
31				
Σ	–	62.8	–	

Październik - Octobre

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ LODU h	POGODA
1	8	•	•	= ^{0} 0^{00}–5^{50} =–9^{30}; ⌓^{0} 0^{00}–5 ⌓^{1} 6–11 ⌓^{0} 19–24
2	7	0.4	•	•^{0} 19^{20}–22^{15}; = 4^{30}–8^{40}, 19^{30}–24; ⌓^{0} 0^{00}–2 ⌓^{1} 3–9 ⌓^{0} 10–11
3	6	•	•	= 0^{00}–14^{10} = 17^{40}–18^{40} =^{0}–22^{50} =^{1}–23^{50} =^{0}–24, ⌓^{0} 17–24
4	7	•	•	= ^{0} 0^{00}–4^{30} =^{1}–5^{30} =^{2}–9^{40} =^{1}–10^{10} =^{0}–10^{20} =–10^{50} = 18^{30}–19^{40} = 20^{30}–21^{50} =^{0}–24, ⌓^{1} 0^{00}–8 ⌓^{0} 9–11, 20–24
5	5	•	•	= ^{0} 0^{00}–30 =^{1}–2^{30} =^{2}–8^{30} =^{1}–10^{25} =^{0}–10^{35} =–24, ⌓^{0} 0^{00}–2 ⌓^{1} 3–11 ⌓^{0} 12–13
6	6	•	•	= 0^{00}–18^{40} =^{0}–20^{30} =^{1}–24, ⌓^{0} 19–22 ⌓^{1} 23–24
7	5	0.0	•	= ^{2} 0^{00}–3^{45} =^{1}–9^{30} =^{0}–10^{35} =–17^{50} =^{0}–18^{30} =^{1}–23^{30} =^{1}–24; ⌓^{1} 0^{00}–11 ⌓^{0} 12–13, 18–24
8	6	0.0	•	•^{0} 6^{40}–8^{45}; = ^{1} 0^{00}–3^{15} =^{0}–6^{50} =^{0}–8^{15} =–15^{20}; ⌓^{0} 0^{00}–6, 18–24
9	8	•	•	= ^{0} 0^{45}–4^{50} = =–7^{00} = 19^{30}–24, ⌓^{0} 0^{00}–1 ⌓^{1} 2–9 ⌓^{0} 21–24
10	7	•	•	= 0^{00}–5^{30}, 18^{30}–24; ⌓^{0} 0^{00}–12, 17–24
11	7	•	•	= 0^{00}–2; ⌓^{0} 0^{00}–2 ⌓^{1} 3–8 ⌓^{0} 9–10, 18–24
12	8	•	•	= 3^{30}–4^{50} =^{0}–6^{30} =^{1} 7^{30} =^{0}–8^{25} =–9^{30}; ⌓^{0} 0^{00}–2 ⌴^{0} 3–8 ⌓^{0} 19–24
13	8	•	•	= 16^{45}–24; ⌓^{0} 0^{00}–3 ⌴^{0} 4–7 ⌓^{0} 18–24; ⊕ 10^{30}–11^{40}
14	5	•	•	= 0^{00}–4^{35} =^{0}–4^{50} =^{1}–5^{15} =^{2}–7^{00} =^{1}–7^{45} =^{0}–8^{15} =^{1}–8^{30} =^{2}–8^{50} =^{1}–9^{00} =^{0}–10^{00} =–17^{45} =^{0}–20^{30} =^{1}–24; ⌓^{0} 0^{00}–4 ⌓^{1} 5–12 ⌓^{0} 18–24
15	6	1.4	•	= ^{1} 0^{00}–5^{30} =^{2}–7^{30} =^{1}–8^{45} =–14^{30} ∞–16^{30} =–24; ⌓^{0} 0^{00}–5 ⌴^{0} 6–7
16	6	1.5	•	•^{0} 3^{35}–10^{30}...11^{25} •^{0} ▽^{1} 14^{48-50} 15^{07-15}; = 0^{00}–13^{30}
17	8	•	•	
18	6	0.0	•	•^{0} 12^{45}–13^{40} •^{0} ▽^{1} 15^{14-16}; = 6^{30}–14^{20}; ⌓^{0} 18–24
19	7	•	•	= 4^{30}–7^{10} =^{0}–8^{40} =–11^{30}, 17^{15-35} = =–18^{30} =–24, ⌓^{0} 0^{00}–1 ⌓^{1} 2–11 ⌓^{0} 12–13, 16–24
20	8	•	•	= 0^{00-50} =^{0}–2^{50} =–3^{50} =^{1}–5^{30} =^{1}–6^{30} =^{2} 7^{30} =^{1}–10^{10} =^{0}–10^{25} =–11^{50}, 17^{40}–20^{30} = =–23^{50} =^{0}–24, ⌓^{0} 0^{00}–3, ⌓^{1} 4–6 ⌓^{2} 7–10 ⌓$^{1-0}$ 11–12 ⌓^{0} 17–21
21	8	•	•	= ^{0} 0^{00}–2^{50} =–9^{35} ⌓^{1} 0^{00}–1 ⌓^{2} 2–7 ⌓$^{1-0}$ 8–11 ⌓^{0} 22–24 [20.X: ⌓^{1} 22–24
22	8	•	•	= 10^{00}–6^{50} =^{0}–8^{05} =^{2}–9^{40} =–11^{30}, 17^{30}, 19^{46} =^{0}–21^{40} =–22^{50} =^{0}–23^{30} =^{1}–24; ⌴^{0} 1–9 ⌓^{0} 10–12 ⌴^{0} 21–24
23	6	•	•	= ^{1} 0^{00}–3^{30} =^{0}–5^{40} =–7^{50} =^{0}–8^{40} =–14^{15} ∞–13^{20} =–20^{50} =^{0}–21^{25} =–24, ⌴^{0} 0^{00}–9 ⌓^{0} 10–12, 18–24
24	8	•	•	= 0^{00}–11^{30}, 19^{10-50} =^{0}–22^{45} =^{1}–24, ⌓^{0} 0^{00}–9, 17–22 ⌴^{0} 23–24
25	6	•	•	= ^{1} 0^{00}–1^{50} =^{1}–6^{30} =^{2}–8^{25} =^{1}–11^{50} =^{0}–12^{20} =–13^{30}, 15^{40}–19^{30}, 23^{32}–24; ⌴^{0} 0^{00}–9 ⌓^{0} 10–14
26	6	•	•	= 0^{00}–7^{15} ∞ 10^{30}–15^{30} =–18^{50} =^{0}–19^{25} =^{1}–19^{45} =^{2}–24; ⌓^{0} 17–19 ⌓^{1} 20–24
27	4	•	•	= ^{2} 0^{00}–30 =^{0}–2^{15} =^{1}–6^{20} =^{2}–10^{30} =^{1}–11^{40} =^{0}–12^{45} =–24, ⌓^{1} 0^{00}–10 ⌓^{0} 11–14
28	6	•	•	= 0^{00}–11^{30} ∞–17^{30} =–24
29	4	1.4	•	•^{0} 11^{40}...12^{15}–14^{15}; = 0^{00}–14^{30}
30	7	0.1	•	= 6^{15}–10^{50} ⌓^{0} 2–9
31	7	7.3	•	•^{0} 1^{10}...2^{05} ▽^{0} 12^{58}–13^{05} ▽^{1}–13^{18}, 13^{25-45} ▽^{0} 14^{55}–15^{05} ▽^{2} 15^{12-20} ▽^{0}–15^{40}; por. wiatru do 19 m/sek 13^{0}–18^{30}
Σ	–	12.1	–	

Szczecin – Dąbie $\varphi = 53°24'$ $\lambda = 14°37'$ *Listopad – Novembre 1965*

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.0	93.6	87.9	93.5	7.5	12.1	12.2	11.0	12.4	5.4	94	84	70	83	0.6	2.2	4.3	2.4	10 ●	10	3	SSW 8	SW 7	SW 10
2	89.9	92.3	97.1	93.1	8.0	10.0	7.4	8.2	12.4	7.4	62	57	77	65	4.1	5.3	2.3	3.9	4	10	6	SW 9	SW 12	SW 6
3	102.8	104.2	107.1	104.7	3.8	8.4	4.2	5.2	9.1	3.6	87	65	84	79	1.1	3.8	1.3	2.1	1	6	0	SW 7	SW 7	SW 6
4	113.8	118.0	122.3	118.0	1.1	6.9	4.0	4.0	7.5	0.8	96	78	93	89	0.2	2.2	0.5	1.0	4	9	1	ESE 5	WSW 5	SW 4
5	127.1	129.1	130.8	129.0	0.7	4.2	3.5	3.0	4.8	0.6	100	98	95	98	0.0	0.1	0.4	0.2	0 ≡	10	10	WSW 4	WSW 4	SW 3
6	129.9	128.3	124.9	127.7	3.6	5.0	6.0	5.2	6.2	2.4	93	95	94	94	0.5	0.4	0.6	0.5	10	10 ●	10	WSW 4	WNW 5	WSW 3
7	121.0	120.2	121.4	120.9	5.4	7.2	3.4	4.8	8.0	2.8	94	71	97	87	0.6	2.9	0.3	1.3	10	9	7	SW 2	SSW 3	E 2
8	122.0	122.7	122.7	122.5	2.4	8.3	6.2	5.8	10.0	0.4	98	73	94	88	0.2	3.0	0.6	1.3	9	9	10	E 4	ESE 3	C 0
9	121.9	122.3	121.6	121.9	6.5	6.3	5.4	5.9	6.8	5.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ● ≡	SW 3	SW 3	SW 1
10	120.4	119.9	118.5	119.6	5.6	7.0	7.1	6.7	7.9	4.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ●	10	SW 2	SW 1	NE 1
11	115.6	114.3	113.3	114.4	2.4	5.5	1.5	2.7	7.1	0.9	98	84	92	91	0.2	1.4	0.5	0.7	4	4	8	ENE 3	NE 4	ENE 3
12	113.3	113.9	114.9	114.0	-1.7	1.4	-2.3	-1.2	2.1	-2.3	90	85	89	88	0.6	1.0	0.6	0.7	2	5	0	NE 4	ENE 6	ENE 5
13	115.4	115.3	115.9	115.5	-5.1	-0.5	-4.4	-3.6	-0.3	-6.7	90	62	84	79	0.4	2.2	0.7	1.1	6	3	0	NE 3	E 5	E 5
14	116.7	117.3	117.5	117.2	-3.9	-2.9	-5.9	-4.6	-2.0	-8.8	78	64	89	77	1.0	1.7	0.4	1.0	10	9	10	E 4	ENE 4	SE 1
15	118.4	120.5	123.7	120.9	-5.2	-2.3	-5.2	-4.5	-2.0	-6.3	83	72	85	80	0.7	1.5	0.6	0.9	9	9	8	E 2	ENE 1	W 2
16	126.9	128.5	129.0	128.1	-2.9	-0.5	-7.2	-4.4	-0.4	-8.5	86	90	96	91	0.7	0.6	0.1	0.5	10	9	0	WSW 3	S 1	ESE 5
17	126.2	123.8	119.9	123.3	-9.0	-2.5	-8.8	-7.3	-2.2	-10.8	95	76	86	86	0.2	1.2	0.4	0.6	8	1	2	ESE 2	ENE 5	SE 7
18	115.0	112.6	109.7	112.4	-9.6	-6.8	-8.0	-8.1	-6.1	-10.1	88	83	78	83	0.4	0.6	0.7	0.6	6	10	10	E 8	ENE 10	SE 9
19	105.9	103.9	104.0	104.6	-8.1	-5.5	-6.4	-6.6	-4.5	-8.8	81	75	75	77	0.6	1.0	0.9	0.8	10 ✱	6	9	ENE 7	E 5	E 5
20	104.4	105.1	103.3	104.3	-6.4	-2.4	-3.0	-3.7	-1.9	-7.3	83	74	81	79	0.6	1.3	0.9	0.9	10	4	10 ✱	ENE 4	ENE 4	ENE 6
21	95.0	90.2	93.4	92.9	-3.9	-2.9	-0.7	-2.0	-0.7	-4.3	92	93	91	92	0.4	0.3	0.5	0.4	10 ✱	10 ✱	10 ✱	ENE 8	ENE 8	NE 7
22	104.3	109.2	114.8	109.4	-0.5	-1.0	-7.4	-4.1	0.5	-7.7	82	85	90	86	1.1	0.9	0.3	0.8	9	10 ✱	2	NNW 5	NW 5	W 3
23	118.8	119.6	118.6	119.0	-9.6	-6.3	-8.2	-8.1	-3.2	-11.2	91	78	87	85	0.3	0.8	0.4	0.5	6	4	10	WSW 4	SW 4	SW 3
24	112.9	108.1	104.1	108.4	-6.4	-2.1	-0.9	-2.6	-0.8	-8.3	78	68	87	78	0.8	1.6	0.7	1.0	7	10	10	S 3	S 8	S 11
25	106.1	110.1	107.3	107.8	2.0	2.5	1.1	1.7	2.7	-1.1	84	82	70	79	1.2	1.3	2.0	1.5	10	8	6	SW 7	WSW 6	S 8
26	93.6	91.8	97.6	94.3	2.1	2.5	1.2	1.8	2.9	0.8	78	89	75	81	1.5	0.8	1.7	1.3	10	10 ●	4	S 10	SW 7	SW 7
27	96.6	87.5	77.4	87.2	-0.5	0.6	1.7	0.9	1.9	-1.1	75	81	96	84	1.5	1.3	0.3	1.0	10	7	10 ●	SW 5	SE 9	WSW 7
28	79.9	83.0	89.1	84.0	2.3	2.1	2.0	2.1	3.2	1.4	82	80	89	84	1.3	1.4	0.8	1.2	10	9	10	SW 8	WSW 8	SW 6
29	97.5	98.0	87.3	94.3	2.0	3.6	2.7	2.8	3.7	0.8	89	78	65	77	0.8	1.7	2.6	1.7	10	4	10	WSW 6	SW 6	SSW 10
30	78.0	87.5	92.1	85.9	4.9	4.3	1.5	3.0	6.5	0.8	82	71	74	76	1.6	2.4	1.8	1.9	10 ●	10	0	SSW 10	SW 8	SW 7
31																								
M	109.6	109.7	109.6	109.6	-0.4	2.1	0.1	0.5	3.0	-2.2	88	80	86	85	0.8	1.5	0.9	1.1	7.8	7.8	6.5	5.2	5.5	5.0

Grudzień – Décembre

DNI	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	82.2	89.7	98.1	90.0	1.2	1.7	0.3	0.9	2.0	0.0	94	83	90	89	0.4	1.1	0.6	0.7	10 ✱	10	10	SW 8	WSW 6	SW 4
2	104.0	103.0	96.3	101.1	0.1	1.3	1.3	1.0	2.1	-1.0	94	92	79	88	0.4	0.5	1.4	0.8	10	10 △	6	WSW 5	SW 5	S 9
3	90.0	91.3	93.0	91.4	1.9	3.1	3.5	3.0	4.3	0.6	93	90	88	90	0.5	0.8	0.9	0.7	9	6	2	SSW 7	SW 6	SW 5
4	94.3	96.2	99.0	96.5	2.7	3.9	1.6	2.4	4.4	1.4	91	83	91	88	0.6	1.4	0.7	0.9	9	8	10	SW 5	SW 5	W 4
5	99.7	93.6	74.9	89.4	-1.5	1.9	6.5	3.4	6.5	-2.8	92	89	91	91	0.4	0.8	0.9	0.7	4	10 ●	10	SSW 2	SE 8	SSW 10
6	82.3	88.4	95.9	88.9	5.4	5.9	1.9	3.8	8.9	1.6	68	70	83	74	2.9	2.8	1.0	2.2	9	7	1	WSW 10	WSW 10	SW 8
7	99.2	102.4	104.9	102.2	3.8	5.2	3.4	4.0	5.7	1.6	72	73	85	77	2.2	2.3	1.2	1.9	9	9	9	SW 8	SW 8	SW 7
8	108.8	111.4	114.7	111.6	0.1	2.3	1.1	1.2	3.9	0.1	96	93	85	91	0.3	0.5	1.0	0.6	1	10 ●	2	SW 3	SW 4	SW 5
9	108.5	101.7	86.5	98.9	1.7	1.1	3.9	2.6	3.9	-0.1	72	92	90	85	1.9	0.5	0.8	1.1	10	10 ✱	10 ●	SW 8	SW 9	SW 10
10	73.7	70.1	74.1	72.6	5.8	8.0	3.5	5.2	8.1	2.2	86	58	90	78	1.3	4.5	0.8	2.2	9	10	10 ●	SW 9	SW 10	WSW 9
11	83.4	83.5	90.3	85.7	3.1	3.1	2.0	2.6	4.4	1.8	74	86	93	84	1.9	1.0	0.6	1.2	9	10 ●	10 ●	SW 9	SW 9	W 7
12	98.9	102.1	106.3	102.4	0.7	0.7	-1.2	-0.2	2.2	-1.3	85	69	76	77	1.0	2.0	1.3	1.4	10	7	2	W 4	NW 5	WSW 3
13	109.3	108.8	108.9	109.0	-5.3	-0.6	-2.3	-2.6	-0.4	-6.9	93	81	89	88	0.3	1.1	0.6	0.7	0	5	2	SW 1	ESE 4	ENE 4
14	119.4	123.4	123.7	122.2	-3.3	-0.6	-3.0	-2.5	0.1	-3.5	90	70	90	83	0.5	1.8	0.5	0.9	3	5	0	W 1	NNW 2	SW 4
15	119.9	120.5	122.0	120.8	0.9	2.7	0.4	1.1	2.9	-3.7	94	96	100	97	0.4	0.2	0.0	0.2	10	10 ● ,	10	WSW 5	WNW 3	E 1
16	121.2	120.8	119.6	120.5	-2.5	-2.5	-3.1	-2.8	0.7	-3.3	91	84	66	80	0.5	0.8	1.7	1.0	10	9	10	SE 4	ESE 7	ESE 5
17	115.7	113.3	111.7	113.6	-4.0	-3.5	-3.7	-3.7	-3.0	-4.2	70	83	94	82	1.3	0.8	0.3	0.8	10	10 ✱	10 ✱	SE 6	ESE 6	ESE 4
18	106.1	102.1	105.0	104.4	0.2	7.1	9.4	6.5	9.5	-3.7	92	96	96	95	0.5	0.5	0.5	0.5	10 ✱●	10 ●	10 ●	ESE 5	SW 9	SW 6
19	104.7	104.5	106.2	105.1	10.1	11.4	8.1	9.4	12.0	8.0	93	86	89	89	0.8	1.8	1.2	1.3	10 ●	10	10 ●	SW 7	SW 8	WNW 6
20	112.4	114.7	114.3	113.8	4.6	5.5	3.7	4.4	8.2	3.3	89	88	93	90	1.0	1.1	0.6	0.9	10	9	9	SW 5	SW 5	SW 3
21	112.4	113.5	115.0	113.6	2.6	2.9	-0.1	1.3	3.8	-0.2	100	91	96	96	0.0	0.6	0.3	0.3	10 ≡	9	9	W 2	WNW 2	WSW 4
22	115.5	115.4	115.3	115.4	1.1	2.0	1.9	1.7	2.4	-1.1	89	85	91	88	0.7	1.1	0.6	0.8	10	9	10	SW 4	SSW 4	SSW 2
23	111.8	109.7	101.5	107.7	1.5	1.4	-0.3	0.6	2.1	-0.3	94	87	78	86	0.4	0.9	1.4	0.9	10	9	7	SSE 4	SE 7	SE 9
24	93.8	91.3	87.9	91.0	0.1	2.7	2.0	1.7	3.5	-1.1	84	82	85	84	1.0	1.3	1.1	1.1	10	9	10	SE 8	S 8	SSE 8
25	81.7	80.0	79.7	80.5	1.0	3.2	4.2	3.2	4.5	-0.1	87	88	92	89	0.9	0.9	0.6	0.8	10 ●	9	10 ●	SE 9	S 6	S 7
26	84.4	89.8	96.0	90.1	3.1	2.5	1.2	2.0	5.2	1.0	83	82	89	85	1.3	1.3	0.8	1.1	9	10	2	WSW 4	WSW 5	SW 6
27	97.7	96.7	93.9	96.1	0.6	1.8	0.5	0.8	1.9	0.0	86	76	82	81	0.9	1.7	1.1	1.2	1	0	10	SW 5	SW 7	SW 5
28	94.2	97.5	102.8	98.2	-0.9	0.3	-0.9	-0.6	0.9	-1.1	89	84	91	88	0.6	0.9	0.5	0.7	10	10 ✱	0	WSW 5	SW 7	WSW 5
29	106.7	109.4	109.3	108.5	0.1	0.7	1.1	0.8	1.3	-1.2	96	82	85	88	0.3	1.2	1.0	0.8	7	9	9	NW 5	WSW 6	WSW 7
30	102.2	97.4	98.0	99.2	-0.7	-0.1	2.2	0.9	2.2	-1.1	75	84	87	82	1.4	1.0	1.0	1.1	9	10	10	SW 9	SW 9	SW 7
31	99.0	99.8	105.1	101.3	2.9	4.0	0.3	1.9	4.4	0.3	89	83	84	85	0.8	1.3	0.9	1.0	10	10 ●	10	SW 7	WSW 9	W 3
M	101.1	101.4	101.6	101.4	1.2	2.6	1.6	1.8	3.8	-0.5	87	83	88	86	0.9	1.2	0.8	1.0	8.3	8.7	7.4	5.6	6.4	[illegible].7

Szczecin - Dąbie

$H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 24\,m$

Listopad - Novembre 1965

DZIEŃ	WIDZIALNOŚĆ V	OPAD R	BURZA BŁYSKAWICA b	POGODA
1	7	5.1	•	•°$^{3^{05}}$ 4^{30} 10^{15} 13^{12-40} 15^{50} 18^{25} 19^{40} 20^{35} ⚲°23^{19-35}; par wiatru 14 m/sek 13^{15} 20^{42} ≫ 21^{25} (par 17 m/sek), par wiatru 14 m/sek 21^{25} 23^{04} ≫ 23^{40} (par 18 m/sek), par wiatru 14 m/sek 23^{40} – 24;
2	8	0.0	•	⚲°10^{25-30}; 11^{55} 14^{02}; 18^{45-47}; par wiatru 14 m/sek 0^{00} 7^{10} ≫ 19^{20} (par do 22 m/sek), par wiatru 12 m/sek 23^{30} 24
3	8	•	•	par wiatru 12 m/sek 0^{00} 7^{40}; 9^{00} 15^{30}
4	7	•	•	= 9^{40} 12^{30}; 17^{15} 18^{40}; ⌓° 2–5 ⌣° 6–7 ⌓° 20–24
5	5	•	•	= 1^{30} 4^{50} ≡¹–9^{10} ≡¹–11^{15} ≡°–11^{45} = –24; ⌓° 0^{00} – 14
6	5	0.0	•	•°8^{05} 11^{30} – 13^{45} 14^{35} 16^{25}; = 0^{00} – 24
7	7	•	•	= 0^{00} – 9^{30} 17^{30} – 24; ⌓° 17 – 24
8	6	0.0	•	•°1^{503}...40; = 0^{00} – 2^{50} ≡°–3^{45} = –7^{20} ≡°–8^{15} ≡°–8^{20} = –10^{15} 12^{40} 13^{30} ∞ –14^{20} = 15^{30} – 24; ⌓° 0^{00} – 12
9	1	0.3	•	•°18^{10} – 24; = 0^{00} – 6^{10} ≡°–7^{15} ≡²–8^{30} ≡¹–9^{40} ≡²–13^{45} ≡¹–14^{20} ≡²–22^{30} ≡¹–24
10	4	0.1	•	•°0^{00} – 4^{20} 11^{15} – 14^{45} 18^{30} – 20^{50}; ≡¹$0^{00}$ – 6^{15} ≡°–11^{05} = –21^{50} ≡°–23^{40} = – 24
11	8	•	•	= 0^{00} – 6^{30} ≡≡ –7^{40} = –11^{15}; ⌓° 20 – 22 ⌣° 23 – 24; ⊽ 20^{30} – 23^{30}
12	8	•	•	⌣° 0^{00} – 2 ⌣¹ 3 – 11 ⌓° 12 – 17 ⌣° 18 – 24
13	8	•	•	= 9^{15} – 10^{45}; ⌣° 0^{00} – 2 ⌣¹ 3 – 12 ⌣° 13 – 24
14	8	•	•	⌣° 0^{00} – 12
15	7	0.0	•	*° 7^{35} – 10^{15}...40; = 7^{20} – 10^{50}; 18^{30} – 23^{30}
16	6	0.0	•	*° 7^{30} – 8^{40}...10^{30} △° – 11^{15}; = 3^{30} 21^{30}; ⌣° 19 – 24
17	7	0.0	•	*° 23^{50} – 24; = 6^{15-35} ≡°–6^{50} = –12^{40}; 20^{30} – 24; ⌣° 0^{00} – 2 ⌣¹ 3 – 14 ⌣° 15 – 23
18	6	0.0	•	*° 0^{00} – 1^{50} 10^{02}...11^{15}; ≫ 10^{15} – 13^{40}; = 0^{00} – 24; ⊕ 9^{15-55}
19	6	0.0	•	*° 5^{50}...7^{30} – 10^{35}; = 0^{00} – 2^{10} 11^{35} – 24
20	6	3.3	•	*° 19^{40}...22^{30} – 24 = 0^{00} – 14^{30} 18^{30} – 24
21	4	12.2	5	*° 0^{00} – 9^{40} *¹ – 18^{50} *° – 21^{40} 22^{40} 24; ⚶¹ 16^{10} – 19 ⚶° – 20^{30} ⚶° – 22^{25}; par wiatru 13 m/sek 5^{30} – 8^{15}; = 0^{00} – 20^{30}
22	6	0.0	22	*° 0^{00} – 3^{25}; 8^{15}...9^{15}; 12^{30} 13^{40}; = 20^{30} – 24
23	7	•	22	= 0^{00} – 6^{30}; 9^{20} – 12^{45} 14^{10} 24
24	7	0.0	19	*° 15^{20} – 16^{35} 18^{15} – 19^{20} 21^{05-40}; ⚶° 10^{45} 17^{30} ⚶¹ – 18^{30} ⚶² 24; par wiatru do 17 m/sek 10^{30} 17^{40} ≫ 21^{40} (par 17 m/sek), par wiatru 14 m/sek 21^{40} 24; = 0^{00} – 7^{50}; 14^{45} – 24
25	6	0.0	17	⚶² 0^{00} – 1 ⚶° – 2^{10}; ≫ 21^{30} – 23^{30}, par wiatru 14 m/sek 23^{30} – 24; = 0^{00} – 23^{20}
26	6	2.6	15	*° 1^{10} – 2^{30} *° – 3^{35} •° 7^{30} 8^{30} *¹ – 9^{15} *° – 9^{55} *¹ – 10^{20} *° – 11^{30} •° – 13^{45}; par wiatru 14 m/sek 0^{00} – 2^{30} ≫ 11^{35} (par do 18 m/sek), par wiatru 14 m/sek 11^{35} – 13^{10}; = 11^{30} – 15^{40}
27	6	7.5	11	*° 13^{50} 14^{40} *¹ – 18^{45} *° – 19^{50} •° – 23^{30} 24; par wiatru 14 m/sek 13^{15} – 20^{30}; = 7^{40} – 24
28	7	2.9	5	•° 0^{00} – 1^{50}; 2^{10}...4^{45} *° 10^{15}...50 •° 16^{50} – 18^{10} *° 22^{35} – 24; = 0^{00} – 7^{30}
29	7	5.7	2	*° 0^{00}...10 – 10^{00} *° 10^{10-20} •° – 3^{30} *° 21^{30} – 24; par wiatru 14 m/sek 16^{30} – 17^{35} ≫ – 24 (par do 18 m/sek); = 13^{30} – 17^{30}
30	8	3.1	2	*° 0^{00} – 3^{30} •° – 7^{20}; ≫ 0^{00} – 8^{30} (par do 20 m/sek), par wiatru 14 m/sek 8^{30} – 11^{35}; 23^{20} – 24
31				
Σ	–	42.8	–	

Grudzień - Décembre

1	7	0.4	3	*° 3^{40} 4^{20} *¹ – 6^{20} *° 7^{35} •° – 8^{40} *° 9^{40}...10^{45}; ⚶¹ 14^{20} – 16^{20}; par wiatru 14 m/sek 0^{00} – 1^{10} ≫ – 5^{30} (par 17 m/sek), par wiatru 14 m/sek 5^{30} – 6^{30}; 13 m/sek 8^{45} – 11^{20}; = 15^{15} – 24
2	6	1.0	2	△° 11^{40} 13^{15} *° 23^{10} – 24; = 0^{00} – 1^{50} ≡°–4^{35} = –24
3	6	2.9	1	*° 0^{00} – 1^{50} *° – 3^{10} •° 8^{35} 9^{15-36} *° – 10^{25} •° – 10^{50}...11^{10}; = 0^{00} – 11^{50}; 12^{05} – 24
4	6	0.2	p2	•° 0^{20} – 2^{05}; 17^{40}...20^{35}; = 0^{00} – 24
5	6	8.6	p2	•° 12^{39} 13^{10} •¹ – 20^{20} •° – 20^{40}; par wiatru 14 m/sek 15^{15} – 18^{15} ≫ – 22^{25} (par do 19 m/sek) ≫ – 24 (par 24 m/sek); = 0^{00} – 20^{30}; ⌣° 1 – 11
6	8	0.4	•	•° 1^{10}...2^{25} ⊽° 7^{30-45}; 8^{12-15}; 8^{40-46}; 9^{13-17}; 9^{35-38} ⊽¹ 16^{10-15}; ≫ 0^{00-50} (par 24 m/sek) ≫ – 18^{30} (par 20 m/sek)
7	8	0.0	•	
8	6	0.2	•	•° 1^{20} – 2^{10} *° 11^{15}...50 *° 12^{05-40} •° – 13^{40} ⊽° 14^{20-30}; = 6^{20} – 8^{20}; 10^{32} – 15^{30}; 17^{30} – 19^{30}
9	4	12.4	•	*° 8^{20} 10^{30} *¹ – 10^{40} *² 10^{55} *¹ – 11^{30} *° – 11^{52} *¹ – 12^{05} *° – 12^{47} *¹ – 13^{20} *° – 15^{35} •° – 24; par wiatru do 14 m/sek 5^{40} 13^{45} ≫ – 24 (par do 19 m/sek); = 1^{30} 7^{20}; ⌣ 3^{30} – 5^{30}
10	8	1.8	•	•° 0^{00-15} •¹ – 2^{35} •² – 4^{20} ⊽° 8^{32-40} •° 13^{35} 14^{15} 14^{45} 17^{30} 19^{30} – 21^{15} – 22^{20} 23^{40} 24; ≫ 0^{00} 6^{15} (par do 22 m/sek), par wiatru do 17 m/sek 6^{15} – 11^{15} ≫ – 18^{40} (par 19 m/sek), par wiatru do 16 m/sek 18^{40} – 24
11	7	1.5	•	•° 0^{00} 1^{40} 10^{45} – 20^{30} – 24; par wiatru 14 m/sek 0^{00} 18^{15}
12	8	•	•	•° 0^{00} – 20
13	7	•	•	= 1^{30} – 11^{45}; 15^{40} – 24; ⌣° 1 – 24
14	7	•	•	= 0^{00} – 12^{30}; 20^{30} – 24; ⌣° 0^{00} – 24
15	5	0.9	•	•° 10^{15}...11^{20} •° – 11^{40} •° – 12^{05} •• °– 15^{40}; = 0^{00} – 14^{50} ≡°–15^{40} = –19^{50} ≡°–20^{35} = –24; ⌣° 0^{00} – 8
16	7	•	•	= 0^{00} – 12^{30}
17	6	2.2	•	*° 11^{40}...13^{15} – 14^{50} *¹ – 17^{15} *° – 22^{20}; = 11^{30} – 24
18	6	10.9	2	*° 6^{05} – 7^{35} •° – 8^{40} •¹ – 9^{40} •° – 12^{30}...14^{30} – 16^{40} •• °– 18^{35} •° – 24; = 0^{00} – 24
19	8	3.3	•	•° 0^{00} – 1^{30}...3^{40}; 5^{45}...11^{40}; 16^{40} – 17^{35}; 18^{15} – 21^{10}; par wiatru 14 m/sek 9^{45} – 18^{30}; = 0^{00} – 8^{30}
20	7	•	•	par wiatru 12 m/sek 3^{40} – 6^{45}; = 17^{30} – 24
21	6	•	•	= 0^{00} – 6^{50} ≡°–8^{10} = –24
22	6	0.0	•	△° 7^{30} – 8^{30} •° – 9^{10}; = 0^{00} – 24
23	6	0.0	•	par wiatru 14 m/sek 17^{30} – 18^{15} ≫ – 20^{30} (par 17 m/sek), par wiatru 14 m/sek 20^{30} – 21^{05} ≫ – 24 (par 17 m/sek); = 0^{00} – 21^{10}
24	6	0.0	•	*° 5^{40} – 6^{35}; ≫ 0^{00} – 6^{05} (par 17 m/sek), par wiatru do 14 m/sek 6^{05} – 8^{15}; = 4^{30} – 24
25	6	0.0	•	•° 6^{50}...11^{40}; 20^{10}...21^{30}; 22^{30} – 24; = 0^{00} – 24
26	7	•	•	•° 0^{00} – 2^{15}; = 0^{00} – 7^{30}; ⌣° 20 – 24
27	6	0.0	•	= 7^{45} – 24; ⌣° 0^{00} – 24
28	6	0.9	•	*° 3^{15-25}; 10^{30-45}; 11^{40}...13^{45}; = 0^{00} – 10^{35}; ⌣° 0^{00} – 3; 23 – 24
29	8	0.2	1	*° 1^{30}...3^{50}; 4^{10} – 5^{40} *° 11^{30-50}; 15^{20-30}; ⌣° 0^{00} – 1
30	6	0.3	1	*° 8^{15} – 10^{05} *¹ 10^{34} – 12^{05} *° – 12^{40} ⊽° 15^{03-09} *° 17^{35}...18^{40}; ⚶¹ 10^{45} 12^{05} ⚶° – 12^{40}; par wiatru 14 m/sek 7^{10} – 9^{55} ≫ – 12^{05} (par 16 m/sek), par wiatru 14 m/sek 12^{05} 20^{15}; = 12^{40} – 24
31	6	0.1	•	•° 9^{20}...11^{20}; 12^{50}...13^{10}; 14^{50}...15^{20}; 16^{40} – 17^{40}; = 0^{00} – 17^{50}
Σ	–	48.2	–	

Poznań – Ławica φ = 52°25' λ = 16°50' Styczeń – Janvier 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	91.4	92.1	91.2	91.6	3.8	5.4	2.6	3.6	5.7	2.4	93	94	86	91	0.5	0.6	1.1	0.7	10	9	9	SW 2	SW 4	SW 4
2	88.8	89.8	91.5	90.0	0.6	2.8	0.6	1.2	3.3	-0.2	98	86	96	93	0.1	1.1	0.3	0.5	8	9	8	SW 4	W 3	SW 5
3	94.4	96.9	100.3	97.2	0.2	1.4	-0.3	0.2	1.7	-0.4	98	85	94	92	0.1	1.0	0.4	0.5	10	10	10	SW 2	NNW 2	C 0
4	105.5	109.5	112.9	109.3	0.0	1.0	-1.5	-0.5	1.9	-2.3	90	79	89	86	0.6	1.4	0.6	0.9	9	2	0	N 5	N 5	NW 6
5	106.0	105.5	103.3	106.9	-0.5	2.0	0.6	0.7	2.6	-3.0	88	93	94	92	0.7	0.6	0.4	0.6	10 *	9	2	W 9	W 9	WNW 8
6	111.2	112.1	114.0	112.4	-0.8	0.2	-3.2	-1.8	1.1	-5.3	92	92	83	89	0.5	0.5	0.8	0.6	8	10	0	NW 6	NW 5	NNW 7
7	114.8	112.7	106.8	111.4	-5.9	-1.0	-3.5	-3.5	-0.8	-6.2	92	81	76	83	0.3	1.1	1.1	0.8	0	4	8	NW 5	W 3	S 5
8	98.5	93.5	89.1	93.7	0.6	2.6	5.1	3.4	5.2	-3.6	100	98	95	98	0.0	0.2	0.4	0.2	10 ≡	10	10 •	SW 5	SW 5	W 9
9	92.3	93.1	93.8	93.1	3.8	3.9	2.3	3.1	5.4	1.8	97	92	95	95	0.3	0.7	0.4	0.5	9	9	10 •	W 4	W 6	W 7
10	89.5	97.3	111.3	99.4	0.4	-0.4	-4.7	-2.4	2.7	-4.8	96	96	83	92	0.3	0.2	0.7	0.4	10 *	10	10	SE 2	NE 9	NE 5
11	113.0	111.1	108.1	110.7	-4.3	-0.8	-0.7	-1.6	-0.1	-5.8	84	83	85	84	0.7	1.0	0.9	0.9	10	5	9	SE 6	SE 6	SE 5
12	106.5	103.9	101.9	104.0	-1.9	3.0	-0.1	0.2	3.7	-2.0	87	72	84	81	0.7	2.1	1.0	1.3	9	6	6	SE 3	S 2	S 4
13	102.3	103.9	105.9	104.1	-2.2	1.9	0.8	0.3	2.2	-2.5	89	82	92	88	0.6	1.3	0.5	0.8	0	10	0	S 3	SSW 6	SSW 4
14	102.3	99.3	103.6	101.7	-1.9	1.4	1.3	0.5	2.0	-2.5	92	78	94	88	0.4	1.6	0.4	0.8	0	0	10	SE 5	S 7	SW 5
15	109.2	109.0	107.0	108.4	-1.4	3.4	-0.1	0.4	3.9	-1.6	91	70	84	82	0.5	2.4	1.0	1.3	0	0	8	SSW 5	S 7	S 4
16	104.2	105.4	102.9	104.2	-1.7	1.2	-0.5	-0.4	1.5	-1.8	90	85	86	87	0.6	1.1	0.9	0.9	10	9	0	S 3	SW 4	S 5
17	88.9	83.5	79.2	83.9	0.7	3.9	3.4	2.8	4.9	-1.1	94	80	97	90	0.4	1.6	0.3	0.8	9	8	10 •	S 10	S 12	S 4
18	81.0	81.3	79.3	80.5	1.8	3.6	2.0	2.4	4.5	1.3	89	80	87	85	0.8	1.6	0.9	1.1	4	6	10 • *	SW 6	SW 7	SW 9
19	80.9	82.3	84.9	82.8	1.0	3.7	-0.4	1.0	4.1	-0.9	85	68	90	81	1.0	2.6	0.6	1.4	9	8	8	SW 5	S 3	SE 1
20	86.2	84.9	82.4	84.5	-1.5	1.2	-0.2	-0.2	1.9	-1.9	96	79	94	90	0.3	1.4	0.4	0.7	10	10	10 *	S 1	E 4	NE 7
21	85.1	86.3	91.2	86.9	-0.8	0.0	0.0	-0.2	0.5	-1.0	93	90	94	92	0.4	0.6	0.4	0.5	10 *	10	10	N 3	NW 3	SW 3
22	95.8	96.2	99.1	96.4	-0.4	0.6	-0.1	0.0	1.3	-1.1	98	94	88	93	0.1	0.4	0.8	0.4	10 *	9	10	W 3	SW 2	SE 4
23	103.2	106.2	110.8	106.7	-0.6	2.0	-1.0	-0.2	2.5	-1.4	85	78	87	83	0.8	1.6	0.7	1.0	10	9	10	SE 3	SE 1	C 0
24	113.7	114.7	114.8	114.4	-1.3	0.4	-0.1	-0.3	1.2	-1.4	91	94	96	94	0.5	0.4	0.3	0.4	10	8 * ≡	10	S 1	C 0	C 0
25	111.4	108.6	105.8	108.6	-1.2	-0.5	-1.4	-1.1	0.3	-1.9	97	94	97	96	0.2	0.4	0.2	0.3	10 *	10 *	10 ≡	C 0	NW 3	C 0
26	103.5	102.0	102.1	102.5	-2.0	-0.5	0.0	-0.6	0.2	-2.1	94	92	94	93	0.4	0.5	0.4	0.4	10 *	10	10 *	E 3	E 2	SE 3
27	102.3	103.3	103.0	103.0	-0.9	-2.5	-1.3	-1.5	0.0	-4.2	93	91	88	91	0.4	0.5	0.6	0.5	10 *	10 △	10	ESE 3	ESE 5	ESE 4
28	102.3	102.8	101.7	102.3	-0.7	1.4	0.0	0.2	1.8	-1.7	93	92	96	94	0.4	0.6	0.2	0.4	10 *	10	10	SE 4	E 2	E 3
29	99.2	99.2	100.0	99.5	-1.7	0.0	-0.1	-0.5	0.4	-2.0	96	100	98	98	0.2	0.0	0.2	0.1	10 ≡	10 ≡	10	C 0	C 0	NW 2
30	99.0	97.0	97.1	97.7	-0.5	0.6	0.1	0.1	0.9	-0.6	98	94	100	97	0.2	0.4	0.0	0.2	10 *	10 *	10 * •	E 2	E 4	N 3
31	103.8	104.7	104.6	104.4	-3.0	-2.7	-3.5	-3.2	0.4	-5.2	95	95	94	95	0.3	0.2	0.3	0.3	10 ≡	8	10 ≡	NE 1	NE 1	C 0
M	99.4	99.6	100.2	99.7	-0.7	1.3	-0.1	0.1	2.2	-2.0	95	87	91	90	0.4	1.0	0.6	0.7	8.2	8.0	8.0	5.6	4.3	4.0

Luty – Février

1	105.3	106.5	110.6	107.3	-3.3	-1.1	-2.7	-2.4	-0.1	-6.7	95	85	91	90	0.3	0.9	0.5	0.6	10 *	7	10	W 4	NW 7	W 5
2	114.8	117.5	120.2	117.5	-4.1	-1.6	-8.3	-5.7	-0.8	-8.5	77	80	80	79	1.0	1.1	0.6	0.9	8	2	0	NW 7	NW 8	NW 4
3	116.9	114.4	113.3	114.9	-3.8	-2.0	-1.9	-2.4	-1.3	-9.7	94	87	94	92	0.3	0.7	0.3	0.4	10	6	10 *	W 5	W 5	W 4
4	114.6	115.2	114.4	114.7	-3.6	-0.3	-0.6	-1.3	0.4	-5.2	94	90	95	93	0.3	0.6	0.3	0.4	1	10	10 *	NW 6	NW 8	E 1
5	109.2	110.6	113.8	111.9	-3.3	-4.2	-13.3	-9.1	-0.3	-13.4	87	63	76	75	0.5	1.6	0.5	0.9	10 *	0	0	SE 3	SE 3	E 2
6	116.8	114.6	109.5	113.6	-11.1	-6.4	-3.6	-6.2	-3.6	-17.1	86	75	90	84	0.4	0.9	0.5	0.6	9	9 *	10 *	S 1	SW 5	SW 1
7	108.7	108.9	97.2	104.9	-4.3	-2.3	0.6	-1.4	0.8	-5.2	93	87	98	93	0.3	0.7	0.1	0.4	10 *	10 •	10	SE 1	SW 2	W 9
8	92.9	94.2	100.7	95.9	-4.0	-0.5	-2.5	-2.4	1.2	-4.0	82	76	82	80	0.8	1.4	0.9	1.0	2	4	10 *	NW 8	NW 10	N 5
9	107.7	111.5	113.1	110.8	-5.1	-4.3	-13.9	-9.3	-2.4	-14.0	90	70	87	82	0.4	1.3	0.3	0.7	10 *	3	4	N 5	N 7	SW 3
10	104.0	100.2	101.7	102.0	-5.0	-2.6	-0.4	-2.1	0.7	-14.6	73	91	90	85	1.1	0.3	0.6	0.7	10 *	10	4	SW 9	W 8	NW 7
11	106.8	108.9	110.7	108.8	-8.4	-0.5	-2.7	-3.6	1.4	-10.2	83	78	93	85	0.5	1.3	0.3	0.7	1	0	10	W 4	W 5	SW 1
12	108.7	107.7	105.9	107.4	0.4	1.8	0.8	1.0	2.1	-2.9	100	98	98	99	0.0	0.2	0.2	0.1	10 ≡	10 •	6	SW 3	W 5	SW 6
13	95.9	90.4	84.2	90.2	1.2	2.0	1.7	1.6	2.6	0.2	92	93	89	91	0.3	0.6	0.8	0.6	10	10 •	10 •	SW 9	SW 8	WSW 10
14	79.1	85.4	92.1	85.5	1.1	0.8	0.6	0.8	2.1	-0.3	77	83	90	84	1.3	1.0	0.6	1.0	6	9	10 *	WNW 10	W 9	W 7
15	97.6	97.9	100.1	98.3	-2.4	0.2	-4.6	-2.8	0.9	-4.6	83	79	93	86	0.8	1.3	0.3	0.8	3	9	7	W 8	W 8	NW 3
16	103.3	105.2	108.8	105.8	-6.5	-3.3	-3.5	-3.2	-2.2	-9.2	94	88	85	89	0.2	0.6	0.6	0.5	9 ≡	9	9	C 0	SW 1	E 3
17	110.2	109.1	110.8	110.0	-8.9	-2.3	-1.1	-3.4	-0.6	-9.8	86	89	93	89	0.4	0.6	0.4	0.5	9	10 *	9	N 6	N 9	NE 8
18	112.9	113.4	114.3	113.6	-2.7	-1.5	-2.4	-2.2	-0.7	-3.5	82	82	78	81	0.9	1.0	1.1	1.0	10	10	10	NE 8	NE 6	NE 5
19	116.0	115.8	117.9	116.6	-3.2	-2.3	-4.6	-4.2	-1.7	-5.6	90	85	84	86	0.4	0.8	0.7	0.6	10	9	10	N 4	NE 9	E 6
20	119.9	121.5	122.7	121.4	-4.3	-3.1	-3.3	-3.6	-2.8	-3.2	81	77	76	78	0.8	1.1	1.1	1.0	10	9 *	10	NE 3	E 9	E 4
21	119.1	116.3	110.6	115.3	-11.7	-2.9	-4.1	-3.7	-2.4	-13.6	89	75	82	82	0.3	1.2	0.8	0.8	1	10	10	C 0	NW 5	W 7
22	105.0	106.4	107.9	106.4	-2.5	0.7	-6.0	-3.4	1.3	-7.0	93	71	84	83	0.4	1.9	0.6	1.0	10 •	8	0	W 9	NE 6	NW 3
23	105.8	105.1	106.7	105.9	-3.3	-1.9	-3.2	-3.4	-0.7	-8.6	80	69	86	78	0.8	1.7	0.7	1.1	10	5	9 *	W 2	W 2	NNE 3
24	108.7	105.3	98.2	104.1	-14.0	-2.3	-4.9	-6.3	-2.1	-14.1	83	49	78	70	0.3	2.7	0.9	1.3	0	4	0	C 0	WSW 4	WSW 4
25	95.8	97.8	100.2	97.9	-4.3	-3.0	-4.9	-4.3	-1.3	-7.0	79	66	78	74	0.9	1.7	0.9	1.2	9 *	4	7	N 8	NW 8	W 8
26	100.4	96.2	87.8	94.8	-9.3	-2.6	-3.1	-4.6	-1.1	-9.9	88	73	93	85	0.4	1.4	0.4	0.7	6	10	10 *	SW 3	W 6	SW 8
27	78.4	83.3	94.3	85.4	-1.8	-4.0	-3.6	-4.2	-1.3	-3.8	96	73	77	83	0.2	1.1	0.9	0.7	9	6	0	SW 6	WNW 8	NW 12
28	101.6	102.4	99.4	101.1	-13.6	-3.8	-6.3	-7.3	-2.8	-13.9	84	42	55	60	0.4	2.7	1.7	1.6	0	0	8	W 3	SW 2	SE 5
29																								
30																								
31																								
M	105.6	105.8	106.1	105.8	-3.3	-1.9	-3.8	-3.7	-0.5	-8.2	87	78	86	84	0.5	1.2	0.6	0.8	7.2	6.9	7.2	5.0	6.2	5.2

Poznań - Ławica

$H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_w =$ 12,5 m anemometr M-47, 15 m anemometr Gawrona-Fuchsa

Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	0.0	•	•°1^35_2^40 3^20 4^25_6^40. = 0^00_12^05
2	6	•	•	•°5^40..6^05, = 5^30_24. ⌣°17 – 24
3	6	0.0	•	= 0^00_24. ⌣° 0^00_11
4	7	0.0	•	*°3^35 4^10 △5^45_6^15. = 0^00_9^30. ⌣°18 – 24
5	6	0.7	•	*°5^35_8^10 ◎–8^45 *°–9^10 *¹ 9^30 *°_10^05 •°–12^10 por. wiatru 14 m/sek 7^10_9^20 ≫9^35 10^10 por. wiatru 18 m/sek – 11^05 ≫–11^10 (por. 17 m/sek), por. wiatru 14 m/sek 11^15–35 ≫12^20 14^15
6	6	•	•	≫17^50_18^15. = 6^40_24. ⌣° 0^00_10. 20 – 24 [5.I.: = 14^20 13^40. ⌣0^00_5. 21 – 24
7	7	0.7	•	*°22^40_24. = 0^00_12^10. 21^20_24. ⌣° 0^00_12. 18 – 24
8	5	3.3	1	*°0^00_2^10 3^15_4^35 •°4^40_5^25. 8^35_10^40 •°14^07–23^45. = 0^00_5^30 =°–6^15 =¹–8^35 =¹–10^40 =¹–11^20 =°–17^40 = 12^10 – 24
9	6	4.1	•	•°0^00–40 •°2^03–40. 14^35_17^40 19^30_21^15 23^35. = 0^00 – 24
10	6	1.2	2	*°4^40_5^30 *¹–8^10 *²–9^05 *¹–9^20 *°–9^35 •°_11^30. = 0^00 – 24
11	6	•	2	= 0^00 – 24
12	6	•	2	= 0^00_12^30 ∞–15^40 = –24. ⌣ 23^15 – 24 ⌣ 23^25 – 24
13	6	0.0	2	•°15^20_16^40. = 0^00 – 24. ⌣ 0^00_1^00 ⌣ 0^00–30
14	6	0.0	2	•°18^40_20^35. = 0^00 – 24. ⌣ 22^20 – 23^40
15	7	•	1	= 0^00_10^20. 16^15 – 24. ⌣° 19^15 – 24
16	6	2.4	1	*°13^40_14^05. = 0^00 – 24. ⌣° 0^00_2^20
17	7	7.7	3	*°4^35–50 *¹–5^40 *°–6^10 •°8^15..35 10^40_11^12 15^08–30 17^33_20^15 •¹–20^40 •°–21^30 •¹–22^10 •°–24. ≫13^30_3^40 5^35_9^20 9^50_16^40 17^20 18^05. = 0^00_9^10
19	7	0.6	pł.	•°0^00–40 •°11^07–20 •°2^03–35 •°–21^10 •°–21^25. ≫18^50_20^17
19	6	•	•	= 9^10_12^30 ∞–15^15 = –24
20	5	1.0	•	*°18^35_20^15 *¹–20^40 *°–24. = 0^00_7^50 =°–10^30 = –24; ⌣°6 – 12; ⌣ 3^30_5^45 ⌣ 3^45_5^45 ⊕ 9^30_13^15
21	6	1.1	2	*°0^00_5^30..7^10 16^30_18^30 21^45 – 24. = 0^00 – 24
22	5	0.2	2	*°0^00..1^15_10^40. = 0^00–45 =¹–12^20 = –24
23	4	•	2	= 0^00 – 24
24	3	0.5	2	*°8^45_10^40 11^20–45 12^30_13^20 23^05 – 24. = 0^00_11^50 =°–14^40 = –24
25	4	0.5	2	*°0^00_18^35. = 0^00_19^40 =°–19^45 =¹–21^45 = –24
26	5	0.9	3	*°5^40_12^03, 19^20..21^15. = 0^00 – 24
27	4	2.7	4	*°4^35_7^35 *¹–9^10 *°–9^45 *¹ 11^05 *°–11^40..12^30 △12^35_14^30 *°–14^45. = 0^00 – 24
28	4	0.0	6	*°6^40_7^05. 8^10. = 0^00 – 24
29	3	0.6	4	*°16^02_17^20. = 0^00–10 =¹–11^0 =¹–24^5 = –4^15 =¹–6^10 =¹–7^20 =²–8^40 =¹–9^20 =°–10^10 =¹–11^20 =°–13^15 = –24
30	4	3.2	4	*°21^8–11^20..12^30_14^05 •°–24. = 0^00–13^40 =°–19^20 = –24
31	4	0.0	5	•°0^00–20. = 0^00–5^45 =°–7^20 =¹–8^15 =²–10^15 =¹–10^40 =°–12^30 = –16^10 =°–17^35 = –20^05 =°–20^20 =¹–21^15 =²–22^40 =¹–24
Σ	–	31.4	–	

Luty - Février

1	6	0.0	5	*°5^40_10^15. =¹0^00_1^15 =°–12^5 = –24^5 =°–3^20 = –18^10
2	8	0.0	5	*°7^03–07 7^43..8^10. ≫9^40_11^15
3	6	0.2	5	*°20^03_22^40. = 21^5_3^20 =°–4^45 = –5^15 =°–6^25 = –24. V°5^15_6^25
4	6	0.7	5	◎⌣°16^50_18^30 ◎¹–19^30 *°–19^45 ◎°–20^05 •°–20^20 *°–22^45. = 0^00 – 24. ∽°16^50_20^20
5	6	0.0	6	*°3^40_8^15. = 0^00–23^0 3^45_10^45 ∞–17^30 = –24
6	5	0.5	6	*°12^06_14^05, 14^20..16^10. 16^35_19^50 20^20..23^40. = 0^00_11^15 ∞–13^30 = –24
7	5	0.7	7	*°0^15_4^35 5^30_7^35 8^38_11^15 •°18^17_21^35 △°22^43_23^03 *°–24. ≫22^05 – 24. = 0^00_2^45 =°–5^35 = –24
8	7	0.9	7	*°0^00–20 •°–2^10 *°2^35 3^05 ⚥°14^06–40 20^20 – 24; ≫0^00–10 por. wiatru 18 m/sek 0^50_1^6 ≫–13^5 por. wiatru 19 m/sek 1^35–40 ≫–22^7 23^0 4^50_12^20 16^20. = 0^00_3^15; 22^20 – 24
9	8	0.1	9	⚥°0^00_2^10 *°–8^40 *¹–9^30 *°–10^10 12^15–35. = 0^00_10^40. ⌣ 20^45_21^35
10	5	0.6	10	*°6^45_7^30 8^15–40 *¹–9^10 *°–10^10 *¹–10^30 *°–12^40 14^35_17^15 por. wiatru 14 m/sek 7^40_14^10 ≫–15^45. = 0^00 – 24
11	7	0.0	11	= 16^40 – 24 [12.II: =°–17^20 =¹–17^45 =°–18^05 = –24
12	4	1.4	11	*°4^45_5^05 *°7^40_9^03 *°10^30_11^15..40 12^35_13^20 13^40_14^45 ••°–15^05 •°–16^45 ••°–16^35 •°–17^40 18^02–15 *°18^20–40. = 0^00_3^20 =°–3^35 =¹–7^05 =²–9^05 =°–8^17 = –11^40 =°–11^45 = –16^55
13	6	1.6	8	*°3^40_4^10 *°–4^20 •°–5^30 6^13–35 8^20 11^35 12^30 14^40 15^45 17^40 ⚥°18^20 19^15 20^40 21^10 •°22^40 23^35. ≫7^40_11^40 18^50_22^30 por. wiatru 14 m/sek 22^40 – 24. = 0^00 19^15
14	7	1.7	5	⚥°0^20–30 ⚥°0^45_1^10 ⚥¹–1^40 ⚥°3^40_4^25 *¹4^35_5^10 7^02–20 *°7^35_10^40. 14^15–22 15^10–25 15^50_16^05 20^45_22^05 por. wiatru 14 m/sek 0^00_4^30 ≫–9^15 por. wiatru 14 m/sek 9^20_10^10 10^50_16^30 ⌣18^40_20^30
15	7	1.2	4	⚥°11^40–48 14^10–15 ⚥¹–14^30 *°–14^33 ⚥¹ 14^44 *°15^10 ⚥¹16^02–08 16^15–20 *°20^05..35. por. wiatru 14 m/sek 10^50_11^05 ≫15^37–54. = 16^10 – 24
16	7	0.0	5	*°9^20_10^35 14^02..20 18^20_19^10. = 0^00–35 =°–3^10 = –5^15 =°–5^50 =¹–6^20 =°–8^10 =¹–9^10. V°5^15–40 V¹–9^10
17	5	1.0	4	*°11^40_20^20. = 0^00_20^30. ⌣ 5^30_6^20 ⌣ 5^45_6^40
18	6	0.0	7	= 6^30 – 24
19	6	0.0	7	*°2^45_3^30 22^45..24; = 0^00 – 24
20	6	0.0	7	*°0^00..1^10 4^15..5^05. 7^35..11^30 12^15..13^16. = 0^00 – 24
21	6	0.0	6	= 0^00_6^30 = = –7^05 = –7^20 = = –7^45 = –24
22	7	0.0	5	*°3^45_6^30 ◎°–7^25 *°7^30 *¹–8^15 *°–8^50 *¹–9^10 *°–10^50 *°13^40–50 14^15_15^05 17^50_18^15. = 0^00_10^50. ∽6^30_7^25
23	7	0.0	5	*°20^17_21^35 21^45_22^35. ⊕°10^15_11^30
24	8	0.3	5	*°23^20..24. = 6^20_10^30 23^30 – 24. ⌣°2 – 10
25	7	0.0	5	*°0^00..1^5–45 *¹–1^20 *°–5^40 *¹–6^10 *°–6^35 7^10 ⚶°3^50_7^28. ≫3^40_6^40 por. wiatru 14 m/sek 14^45_15^20. = 0^00_7^10
26	6	3.0	4	*°8^20–40 *¹–9^35 *°–10^10. 14^15_15^05 17^45 – 24. = 8^15 – 24
27	7	0.3	8	*°0^00_2^25 4^50 6^45 7^40 8^03 *¹–8^20 *°–9^10 ⚥°19^23–35 17^20 18^30 ⚥18^35 19^20. ⚶5^50_6^45 8^35_11^30 ⚶°–15^35 ⚶¹18^40_19^30 ⚶°–21^30 por. wiatru 14 m/sek 8^45_9^40 ≫–10^45 (por. do 19 m/sek)
28	8	0.0	9	
29				[27.II: por. wiatru 14 m/sek 10^45_16^40 por. wiatru 18 m/sek 18^35–45 ≫–23^30 (por. 18 m/sek 10^45_10^10). = 0^00_9^30; 19^30_20^40
30				
31				
Σ	–	14.2	–	

Poznań – Ławica φ = 52°25' λ = 16°50' Marzec – Mars 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	95.8	93.8	91.1	93.6	-5.1	1.6	-2.7	-2.2	2.2	-6.3	73	65	69	68	1.1	2.6	1.5	1.7	9	9	9	SE 2	C 0	E 3
2	85.8	84.2	82.5	84.2	-5.4	-3.0	-5.8	-4.0	-2.5	-5.6	90	84	94	89	0.4	0.8	0.3	0.5	10 *	10	10 *	NE 7	NE 8	NE 9
3	78.5	78.0	80.0	78.8	-3.2	-1.8	-2.2	-2.4	-1.3	-4.3	95	96	94	95	0.2	0.2	0.3	0.2	10 *	10 *	10 *	NE 10	NE 2	W 6
4	85.8	86.7	90.2	86.9	-4.6	-4.1	-3.7	-4.0	-2.0	-5.0	93	89	85	89	0.3	0.5	0.7	0.5	10 *	10 *	10 *	W 12	W 14	W 10
5	95.8	97.9	103.3	98.3	-4.1	-0.9	-2.0	-2.2	-0.1	-4.8	89	83	89	87	0.5	1.0	0.6	0.7	10 *	9	10	W 6	NW 4	N 3
6	107.5	109.2	113.7	110.1	-1.8	-1.0	-3.0	-2.2	-0.3	-3.3	86	79	73	79	0.8	1.2	1.3	1.1	10	10	9	NE 4	NE 8	NE 8
7	117.4	118.8	119.4	118.5	-11.7	-4.1	-9.9	-8.9	-2.8	-12.1	86	70	81	79	0.3	1.3	0.5	0.7	4	2	0	NE 6	E 4	E 4
8	117.5	115.9	114.7	116.0	-17.3	-6.3	-13.9	-12.8	-4.4	-21.4	85	70	87	81	0.2	1.1	0.3	0.5	2	0	0	E 1	NW 1	W 1
9	113.3	113.2	114.8	113.8	-16.9	-3.7	-1.9	-6.1	0.3	-20.2	90	83	79	84	0.2	0.8	1.1	0.7	10 ≡	10	9	SE 1	SW 3	NW 7
10	118.7	120.5	120.8	120.0	-7.3	-1.0	-7.0	-5.6	1.9	-7.8	90	79	85	85	0.3	1.2	0.3	0.7	10	6	0	W 2	SW 3	SW 1
11	121.4	121.4	118.8	120.5	-13.8	2.0	-3.5	-4.7	4.8	-13.9	83	56	78	72	0.3	3.1	1.0	1.5	0 ≡	0	0	C 0	SW 1	S 2
12	117.5	115.8	114.7	116.0	-10.2	4.6	-1.6	-2.2	6.6	-10.6	84	48	83	72	0.4	4.4	0.9	1.9	1 ≡	1	0	C 0	S 1	SE 1
13	114.5	114.1	113.6	114.1	-7.4	7.5	0.0	0.0	8.1	-7.7	90	49	82	74	0.3	5.3	1.1	2.2	0 ≡	0	0	E 1	SE 1	SE 1
14	112.5	111.0	109.8	111.1	-5.4	4.1	0.0	-0.3	7.1	-5.4	92	66	88	82	0.3	2.8	0.7	1.3	0	0	0	SE 1	SW 3	SE 2
15	109.0	108.7	107.1	108.3	-0.7	6.6	3.9	3.4	8.8	-2.3	89	64	80	78	0.6	3.5	1.6	1.9	2	8	6	S 2	S 3	S 3
16	102.9	101.5	102.9	102.4	3.4	6.5	2.8	3.9	7.0	2.5	86	73	96	85	1.1	2.6	0.3	1.3	6	9	10	S 4	SSW 6	SW 3
17	103.2	101.1	99.4	101.2	0.9	10.2	3.7	4.6	11.3	0.6	100	62	92	85	0.0	4.6	0.7	1.8	10 ≡	4	7	S 1	S 6	C 0
18	96.9	94.1	91.4	94.1	-1.3	11.2	6.5	5.7	12.1	-2.2	99	60	81	80	0.1	5.3	1.9	2.4	10 ≡	3	9	C 0	S 3	SE 2
19	91.2	95.2	101.3	95.9	6.3	7.7	3.9	5.4	10.7	3.2	73	79	90	81	2.5	2.2	0.8	1.8	9	10	10	S 6	SW 6	NW 6
20	106.1	106.0	105.0	105.7	-0.5	6.3	0.5	1.7	7.0	-1.2	94	50	94	79	0.4	4.7	0.3	1.8	2	6	10 *	SW 2	W 6	C 0
21	100.4	93.1	96.5	96.7	-0.2	4.8	0.4	1.4	5.6	-1.2	100	89	96	95	0.0	1.0	0.3	0.4	10 ≡	10 •	10	SE 2	SE 6	W 8
22	102.5	104.7	105.3	104.2	-1.9	3.9	-0.8	0.1	5.8	-3.4	87	45	81	71	0.7	4.5	1.1	2.1	8	1	0	W 6	WNW 7	N 1
23	102.0	97.1	91.8	97.0	-1.4	6.8	3.0	2.8	8.1	-2.5	78	43	69	63	1.2	5.6	2.4	3.1	1	2	0	SE 3	SSE 10	SE 7
24	89.3	89.6	91.2	90.0	3.4	11.4	7.2	7.3	13.9	1.5	93	69	90	84	0.5	4.2	1.1	1.9	10	9	10 •	S 2	SW 6	SW 3
25	95.1	99.6	102.8	99.2	4.0	4.3	3.1	3.6	7.4	2.7	93	77	83	84	0.5	1.9	1.3	1.2	10 •	10	8	W 12	W 10	SW 2
26	102.9	100.7	104.5	102.7	2.9	7.7	4.8	5.0	8.2	2.3	96	69	87	84	0.2	3.2	1.1	1.5	10 •	9	10	SW 3	S 5	E 6
27	114.6	118.2	121.0	117.9	0.4	8.4	3.7	4.0	10.2	-0.2	94	69	88	84	0.4	3.4	1.0	1.6	1	8	0	NE 5	E 1	S 2
28	120.2	119.4	118.5	119.4	4.5	7.2	7.6	6.7	8.4	1.5	79	83	97	86	1.8	1.8	0.3	1.3	10	10	10 • ≡	S 4	SSW 7	SSW 3
29	118.7	118.8	116.5	118.0	8.0	13.7	8.7	9.8	15.3	7.1	97	65	80	81	0.3	5.5	2.2	2.7	9	4	0	WNW 5	NW 7	W 4
30	110.6	110.0	117.5	112.7	6.2	11.8	1.9	5.4	12.9	1.6	94	48	89	77	0.6	7.2	0.8	2.9	1	7	0	W 6	NNW 10	N 3
31	116.3	114.5	116.9	115.9	1.1	9.2	2.0	3.6	10.8	-1.3	92	47	73	71	0.5	6.1	2.0	2.9	2	3	1	WNW 6	NW 6	N 4
M	105.2	104.9	105.7	105.3	-2.6	4.2	0.2	0.5	5.8	-3.9	89	68	85	81	0.5	3.0	1.0	1.5	6.4	6.1	5.4	3.9	5.1	3.8

Kwiecień – Avril

1	120.0	121.4	117.8	119.7	0.0	6.3	2.5	2.8	9.2	-2.2	92	59	80	70	0.5	5.7	1.4	2.5	0	2	0	N 5	NNE 8	W 1
2	113.2	115.2	114.2	114.2	2.1	9.4	4.8	5.3	11.8	0.2	82	54	82	73	1.3	5.4	1.5	2.7	4	7	0	NW 5	NW 5	NW 3
3	108.8	108.4	105.2	107.5	0.2	3.8	2.4	2.2	8.0	-1.5	98	77	87	87	0.1	1.9	1.0	1.0	0	8	0	SW 2	NW 7	C 0
4	102.8	101.0	100.9	101.6	1.0	13.6	6.4	6.8	15.1	-0.5	92	45	76	71	0.5	8.6	2.3	3.8	1	9	2	SW 2	WNW 5	N 5
5	105.5	107.3	107.6	106.8	0.4	12.4	7.2	6.8	15.6	-2.5	98	40	62	67	0.1	8.7	3.9	4.2	1	2	0	C 0	E 3	E 3
6	107.6	104.8	101.2	104.5	3.2	15.1	9.9	9.5	16.6	1.1	86	34	54	58	1.1	11.3	5.7	6.0	0	1	6	E 2	SE 5	SE 6
7	100.8	103.3	102.2	102.1	6.7	8.6	5.0	6.3	10.8	5.0	91	61	86	79	0.9	4.4	1.2	2.2	10 = •	10	6	NW 8	NW 7	S 3
8	102.1	101.8	103.0	102.3	3.6	10.7	4.2	5.7	11.4	1.4	93	58	77	76	0.5	5.4	1.8	2.6	6	9	2	E 4	ENE 5	E 9
9	101.9	101.7	103.3	102.3	3.3	8.7	6.1	6.0	10.6	2.2	86	65	69	73	1.0	3.9	2.9	2.6	9	10	10	E 9	E 11	E 8
10	104.6	104.2	104.3	104.4	2.5	7.0	5.4	5.1	8.6	2.2	65	56	68	63	2.6	4.4	2.9	3.3	10	10	9	E 6	E 5	SE 7
11	101.7	101.2	101.2	101.4	1.6	3.6	3.2	2.9	5.7	1.6	74	67	83	75	1.8	2.6	1.3	1.9	10	10	3	SE 5	SE 6	E 2
12	102.7	103.1	102.1	102.6	2.2	6.0	5.1	4.6	7.5	0.2	93	85	94	91	0.6	1.3	0.6	0.9	9	10 •	4	C 0	C 0	S 1
13	99.3	98.9	100.7	99.6	4.4	13.1	7.3	8.0	14.6	2.8	93	53	94	80	0.6	7.0	0.6	2.7	2	9	10	SE 4	S 6	E 3
14	104.6	106.9	109.2	106.9	5.7	10.3	6.1	7.0	11.4	3.1	94	67	86	82	0.6	4.1	1.3	2.0	7	9	2	W 3	NE 3	E 2
15	109.0	107.5	104.7	107.1	4.0	10.4	6.0	6.6	12.1	2.3	87	54	69	70	1.1	5.7	3.0	3.3	6	9	1	SE 2	SE 4	E 6
16	99.1	95.9	97.2	97.4	2.2	12.7	8.0	7.7	13.4	1.2	87	49	95	76	1.0	7.6	0.7	3.1	0	9	10	SE 5	SE 6	SSE 2
17	100.7	100.1	92.5	97.8	5.9	8.9	7.2	7.3	11.4	5.5	89	51	69	70	1.0	5.6	3.2	3.3	9	8	10	W 6	SW 6	SE 4
18	82.1	83.5	90.6	85.4	6.6	11.8	4.4	6.8	13.7	4.3	96	60	89	82	0.4	3.3	1.0	2.3	10 •	7	0	S 7	SW 8	SW 2
19	92.6	91.7	91.2	91.8	4.4	9.2	7.2	7.0	10.6	2.2	93	63	87	81	0.6	4.2	1.4	2.1	10	9	10	SW 2	S 3	NE 2
20	89.7	91.8	93.0	91.5	7.2	9.6	10.7	9.6	12.3	5.8	88	77	67	77	1.2	2.8	4.3	2.8	10	10	6 •	E 4	E 7	E 8
21	93.3	92.7	91.9	92.7	8.3	12.0	8.9	9.5	12.3	6.8	83	66	92	80	1.9	4.8	0.9	2.3	9	10	10 •	E 7	E 9	NE 6
22	89.6	89.9	90.6	90.0	8.7	11.1	7.9	8.9	11.9	7.7	92	77	66	78	0.9	3.1	3.6	2.5	10 • •	10	4	NE 7	NE 8	NE 6
23	88.8	88.9	88.5	88.7	5.9	6.6	6.3	6.4	8.7	5.7	92	96	79	89	0.7	0.4	2.0	1.0	10 •	10 •	10	N 8	N 3	NW 8
24	87.7	89.0	92.3	89.7	5.0	6.6	5.6	5.7	7.6	4.4	94	85	89	89	0.5	1.4	1.0	1.0	10 •	10 •	9	W 6	WNW 9	W 4
25	94.7	96.2	97.8	96.2	6.4	9.3	3.1	3.5	10.4	3.1	95	71	97	88	0.4	3.4	0.2	1.3	10 •	10 •	0	SW 3	SW 3	C 0
26	98.8	98.2	96.3	97.8	4.3	9.9	6.8	7.0	12.0	1.9	93	56	82	77	0.5	5.4	1.8	2.6	7	7	0	SW 2	W 6	NE 2
27	93.1	91.9	92.1	92.4	6.0	12.8	8.4	8.9	13.6	4.2	79	53	85	72	2.0	7.0	1.6	3.5	8	7	4	NE 3	ENE 7	E 4
28	91.3	90.2	90.8	90.8	6.6	12.6	7.8	8.7	13.0	6.4	96	69	94	86	0.4	4.6	0.6	1.9	10	10	9 •	ENE 9	E 8	SE 3
29	95.3	97.7	101.4	98.1	8.0	11.7	9.1	9.0	14.3	3.7	91	60	77	76	0.9	3.5	2.7	3.0	9	9	4	S 4	ESE 3	NE 3
30	104.3	103.3	107.2	105.7	6.3	13.8	9.0	9.3	13.1	2.7	94	33	83	77	0.3	7.2	2.0	3.2	1	8	3	N 1	SE 2	NW 3
31																								
M	99.3	99.7	99.7	99.6	4.4	9.9	6.4	6.8	11.6	2.8	90	61	81	77	0.9	3.0	1.9	2.6	6.6	8.3	4.8	4.4	3.7	4.0

Poznań - Ławica $H_s = 86m$ $H_b = 92{,}1\,m$ $h_w =$ 12,6 m anemometr M-47 / 15 m anemometr Chauvin - Arnoux **Marzec - Mars 1965**

DNI	WILGOTNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	6	0.2	8	*240 3 45 540 = 320 4 15 615 935 ∞ -2140 = -24
2	6	5.4	8	*235 1125 1145 1250 1340 1425 1720 *●0 -1845 △-1940 *0 -2010 *1 -2335 *0 -24; +0 1040 1430 1550 1715 +1 2050 -24; » 1540 1650; = 000 -24
3	4	12.6	10	*0 000-30 △-140 *0 -530 △-615 *1 -720 *0 -1620 1715 2345 *1 -24; +1 000 -400 +2 -730 +1 -1215 +0 2345 -24; » 340 930; = 000 -24
4	4	3.6	27	*1 000 -710 *0 -2240 *1 -24; +2 000 -1530 +1 -24; » 030 2235; = 000 -24
5	6	0.2	35	*1 000 -230 *0 -645 *1 -705 *0 -1040; 1420 -1520; +1 000 -2050 +0 -645
6	6	0.0	35	*0 945 1035; = 000 -24
7	7	•	35	= 000 -1140; 1715 -24
8	6	•	35	= 000 -1200 ∞ -1730 = -2210 = 0 -24; ⌴ 1 -10
9	5	0.0	34	*0 903 -1005...45; = 0 000 -720 = -2015
10	6	•	31	= 610 -1530; 1715 -2335 = = -24
11	6	•	30	= = 000 -145 = 1 -430 = 0 -730 = = -010 = -1030 ∞ -2015 = -24; V 1 250 -730
12	6	•	26	= 000 -510 = = -605 = 0 -840 = -930 ∞ -1845 = -24; ⌴ 0 2 -9
13	5	•	20	= 000 -550 = 0 -935 = -950 ∞ -2030 = -24
14	5	•	17	= 000 -645 = = -730 = -1030 ∞ -1830 = -24
15	6	0.5	16	● 0 2205 -2340; = 000 -1015 ∞ -1930 = -24
16	6	0.4	12	● 0 435 510 1320 -1440; 1605 -1730 45; = 000 -2145 = 0 -2340 = 1 -24
17	6	•	9	= 1 000-30 = 2 -840 = 1 -920 = -1430 ∞ -1630 = -2340 = 0 -24
18	6	•	pł.	= 000 -120 = -140 = 0 -330 = 1 -440 = 2 -630 = 2 -845 = 1 -905 = 0 -1015 = -1130 ∞ -1840 = -24
19	6	0.3	pł.	▽ 0 1640 -1830 ● 0 1903-35; = 000 -1430 1625 -24
20	8	1.6	pł.	● 0 1640 -1710 *0 -1745 *0 -1815 *0 -1830 *1 -1940 *2 -2110 2205; = 000 -510 = = -645 = 1730 2245 = 0 -2310 = 1 -2340 = 0 -24, ⌴ 0 4 -9
21	5	0.3	pł.	△ 735 840 ● 0 1206 -1420 1510 1740 ● 0 -1845; = 0 000-40 = -110 = 0 -130 = 1 -150 = 0 -240 = 1 -320 = 2 -345 = 0 -510 = 1 -715 = 0 -810 = -24
22	8	•	pł.	= 000 -845
23	7	0.0	•	» 950 1615; = 015 -730 ∞ -830; 1745 -2040 = 2245 -24; ⌴ 0 1 -3 ⌴ 2 4 -8
24	6	2.3	•	● 0 735 340 ▽ 0 1708-15 2040 2110; = 000 -1250 ∞ -1730 = -24
25	6	0.4	•	▽ 0 715 -335 526 -1045; » 550 1320 (por 16 m sek 1150 1310); = 000 -450 535 1330 1820 -24
26	6	2.1	•	● 0 335 610 ● 0 -705 ▽ 0 -850 1608-20 ● 0 1640 -2045; = 000 -1320 ∞ -1630 = -24
27	7	•	•	= 000 -1215 ∞ -1820 = -24; ⌴ 0 2 -8
28	6	3.9	•	● 0 935 -950 1607 -1940 ● 1 -2110 ● 0 -2145 ● 0 -2240 2345 -24; = 000 -1915 = 0 -2210 = -24; ⌴ 0 3 -8
29	6	•	•	● 0 000-30; = 000 -1230 ∞ -1830 = -24
30	7	•	•	» 945 -1835; = 000 -830 ∞ -930
31	7	•	•	» 1530 -1830; ⌴ 0 0 -9
Σ	-	33.8	-	

Kwiecień - Avril

DNI	WILGOTNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	8	•	•	⌴ 0 4 -8
2	7	•	•	⌴ 0 5 -7
3	6	•	•	= 130 -445 = = -540 ∞ 1330 -1830 = -24; ⌴ 0 3 -5 ⌴ 1 6 -8
4	7	•	•	= 000 -830 ∞ -1930 = -2230 ∞ -2340 = -24; ⌴ 0 2 -8; ⊕ 1315 -1440
5	7	•	•	= 000 -930 ∞ -1340; ⌴ 0 3 -8
6	7	0.0	•	= 430 -830 ∞ -1040; 1815 -24; ⌴ 0 5 -8
7	7	0.0	•	● 0 0630 -710; ∞ 000 -230 = -840 ∞ -945 = 1815 -24; ⊕ 1 1535 -1810
8	6	•	•	» 1845 1935; = 000 -840 ∞ -2030 = -2115; ⌓ 1 2 -8
9	6	•	•	» 615-40 710 1830 (por 18 m/sek 1325 -1440, por 16 m/sek 1440 1805), por wiatru 14 m/sek 1845 -2045; = 715 -1230 ∞ -24
10	7	•	•	∞ 000 -430 630 -1115; ⊕ 1130 -1410
11	7	•	•	= 1930 -24
12	6	0.2	•	● 0 910...40 -1035 1120 -1310 1505 1545 1610 1650 1805; = 000 -24; ⌴ 0 3 -7
13	6	15.7	•	▽ 0 1740 -1820 1845 -2035 2105-27 ● 1 -2235 ▽ 0 -2320; = 000 -930 ∞ -1730 = -24; ⌓ 0 -8; ⊕ 815 -1430
14	6	•	•	● 0 040 130; = 000 -830 ∞ -1310 = 1840 -24
15	6	•	•	= 000 -920 ∞ -1520 18 -2020; ⌓ 0 1 -2 ⌓ 0 3 -8; ⊕ 0 000 -210
16	6	0.9	•	▽ 0 1435-45 1520 -1605 ● 0 1615 -1935 2010 ●● 0 -2030 ● 0 -2050 ● 0 2110-30 ●● 0 -2330 ● 0 -24; = 420 -840 ∞ -1715 = -24
17	7	3.0	•	● 0 000 -140 ● 0 335 440 2240 -24; = 000 -915 ∞ 1930 -24
18	8	0.1	•	● 0 000 -330 515 -820 ▽ 0 1402-07 1435-45; por wiatru 14 m/sek 1210 1420 por wiatru 12 m/sek 1515 1630; ∞ 000-30 = -920; ⌓ 0 23 -24
19	7	9.6	•	▽ 0 1420 -1835 ● 0 -2040 2145 2235; = 420 -940 ∞ -1015 = 1830 -24; ⌓ 0 000 -9
20	6	0.0	•	● 0 000-05 ● 1 -040 ● 0 -520 1840 1910 ▽ 0 2035 -2130, » 2105-20 2325-40; = 000 -1430 ∞ -2030
21	7	1.1	•	● 0 2040 2130 ● -2345; » 930 -1010; = 2130 -24
22	6	0.7	•	● 0 235 -330 ● 1 -415 ● 0 -440 ●● 0 -510 ●● 0 -730 ● 1 -840 ● 0 -1017 ▽ 0 1220-30; = 000 -1330 ∞ -1516
23	6	2.7	•	● 0 440 810 835 930 ●● 0 -1040 ● 0 1105-10 ●● 0 -1220 ● 0 -1320 2240 -24; = 430 -1730 2250 -24
24	7	4.4	•	● 0 000 435 520 930 ● 1 -1115 ● 0 -1440 ▽ 1 1510-20 ● 0 1535 -1630 2020-45; » 845 -1010 por wiatru 14 m/sek 1120 1505 » 1510 1650; = 000 1240 1930 -24
25	6	0.6	•	● 0 330 440 530 710 ▽ 0 1235 -1415 ● 0 1530; = 000 -1130 ∞ -1315 = -1730 1830 -24; ⌓ 0 20 -24, ⊕ 1110 -1240
26	7	0.0	•	▽ 0 1235-39; = 000 -830; ⌴ 0 1 -3 ⌓ 1 4 -8
27	6	•	•	= 330 -730 ∞ -1610 = 1920 -24
28	6	14.9	•	● 0 1320-40 ▽ 1 1413-26 ▽ 0 -1433 ● 1 -1505 ● 0 -1540 1640 1708 ● 1 -1735 ● 0 1840 ● 1 -1910 ▽ 0 -19 ● 0 -2140, ⊠ SE 1422 -⊠ 1433 1440 1505 E; » 745 -1030, por wiatru do 14 m/sek 1035 1130
29	7	3.5	•	● 0 430 615 ▽ 0 1805-38 ● 1 -1850 ● 0 -1915; = 000 815 ∞ 1015 1930 = -24, ⌒ 1805 1900 **28.IV:** 1220-40 1433 1445 1640 1810; = 000 1230 ∞ -1330 = -24; ⌓ 1 -8
30	7	0.2	•	▽ 0 1010-35 1320 35 1420 1505 1530-20; = 000 410 = = -530 = -940, ⌓ 0 2 -4 ⌓ 1 5 -10
31				
Σ	-	37.6	-	

Poznań – Ławica φ = 52°25' λ = 16°50' Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	108.3	106.7	108.9	108.0	5.8	15.1	7.0	8.7	16.7	0.4	68	41	53	54	2.9	10.1	4.7	5.9	0	7	0	NW 3	N 8	E 6
2	111.2	109.8	108.1	109.7	5.0	10.8	6.8	7.4	12.7	0.1	55	43	67	55	3.9	7.5	3.3	4.9	7	6	0	C 0	NE 2	E 2
3	109.8	109.2	108.6	109.2	2.7	9.8	6.6	6.4	10.5	-0.1	74	34	46	51	1.9	8.0	5.3	5.1	0	1	0	E 6	E 5	E 5
4	106.9	102.5	96.8	102.1	5.1	13.7	11.1	10.2	15.9	-0.2	57	41	40	46	3.8	9.3	7.9	7.0	3	2	9	SE 7	SE 10	ESE 8
5	93.1	92.6	94.0	93.2	6.4	10.5	7.8	8.1	11.2	5.8	97	87	94	93	0.3	1.6	0.6	0.8	10 •	10	10	SE 3	E 6	E 3
6	95.6	98.0	101.1	98.2	7.4	9.2	7.6	8.0	9.3	7.3	99	91	97	96	0.2	1.1	0.3	0.5	10 •	10 •	9	E 1	N 1	C 0
7	103.7	103.7	102.6	103.3	7.9	11.8	9.4	9.6	14.0	6.8	93	59	84	79	0.7	5.6	1.9	2.7	9	9	10	WNW 4	WSW 3	SE 2
8	97.9	101.9	105.0	101.6	9.8	11.6	10.0	10.4	14.2	8.4	97	75	81	84	0.3	3.4	2.4	2.0	10 •	10	1	SW 2	NW 6	W 4
9	100.5	95.5	89.4	95.1	10.4	13.7	9.3	10.7	14.8	6.5	97	89	74	87	0.3	1.8	3.1	1.7	10 •	10 •	10 •	SSW 5	S 6	W 12
10	88.0	88.4	88.3	88.2	8.3	10.4	6.6	8.0	11.4	6.6	84	82	93	86	1.7	2.2	0.7	1.5	9	9	10 •	W 11	W 12	WSW 8
11	93.0	100.0	106.8	99.9	6.2	10.7	9.0	8.7	12.9	6.2	94	69	89	84	0.6	4.0	1.3	2.0	10 ••	10	3	N 8	NNE 8	NW 6
12	111.9	112.8	112.6	112.4	6.8	16.1	11.3	11.4	17.3	4.3	97	52	82	77	0.3	8.7	2.5	5.8	10 •	4	6	NNW 7	N 5	N 3
13	112.9	111.9	109.7	111.5	6.2	14.6	11.5	11.0	16.8	5.8	100	54	76	77	0.0	7.7	3.3	3.7	10 ≡	8	8	N 4	WNW 2	NW 3
14	106.6	104.8	103.5	105.0	10.4	13.1	10.1	10.9	13.8	9.9	96	77	91	88	0.5	3.5	1.2	1.7	10	9 •	8	W 3	NW 4	C 0
15	103.0	102.3	100.2	101.8	9.2	14.2	13.5	12.6	17.4	7.8	95	66	58	73	0.6	5.4	6.5	4.2	10	8	9	ENE 4	ESE 5	ESE 6
16	97.2	96.6	96.3	96.7	11.1	18.5	13.1	14.0	19.5	10.1	77	67	94	79	3.1	7.0	0.9	3.7	9	8	7	E 4	E 4	SE 1
17	97.0	95.1	91.3	94.5	11.9	20.4	18.3	17.2	22.2	9.3	94	57	77	76	0.8	10.3	4.8	5.3	9	7	10	SW 1	SW 5	S 5
18	92.4	94.4	93.9	93.6	14.9	19.2	15.3	16.2	20.3	14.5	85	59	78	74	2.5	9.1	3.9	5.2	7	9	9	W 8	W 8	S 2
19	91.4	92.3	100.9	94.9	12.4	8.8	5.9	8.2	15.4	5.8	98	96	88	94	0.4	0.4	1.2	0.7	10 •	10 •	8	SW 3	N 7	NW 2
20	106.5	107.9	111.1	108.5	6.0	10.0	6.3	7.2	11.8	2.8	76	46	73	65	2.3	6.7	2.5	3.8	5	8	3	W 4	WNW 8	NW 3
21	115.6	116.8	117.3	116.6	6.4	10.5	7.2	7.8	13.5	2.5	88	39	74	67	1.1	7.8	2.7	3.9	2	8	5	WSW 4	W 7	SW 2
22	118.4	116.2	114.0	116.2	8.8	15.0	10.8	11.4	16.5	1.6	64	36	59	53	4.0	10.9	5.4	6.8	1	2	1	SE 1	E 7	E 5
23	112.1	110.1	109.0	110.4	9.8	16.8	14.0	13.6	17.4	6.4	59	44	52	52	4.9	10.8	7.7	7.8	3	8	10	E 9	E 9	ESE 9
24	106.8	106.0	105.4	106.1	10.3	10.9	10.3	10.4	14.0	10.1	94	94	99	96	0.8	0.8	0.1	0.6	10 •	10 •	10	E 6	E 5	ENE 2
25	105.2	106.5	107.5	106.4	10.6	12.2	11.3	11.4	13.2	10.0	99	87	94	93	0.2	1.9	0.8	1.0	10	10	10	N 2	NW 3	N 2
26	106.9	106.0	104.6	105.8	10.6	11.9	11.3	11.3	13.3	10.3	95	93	93	93	0.7	1.2	1.0	1.0	10 •	10 •	10 •	C 0	SW 1	C 0
27	103.1	103.2	103.0	103.1	9.9	14.5	12.1	12.2	15.2	9.5	88	60	71	73	1.4	6.7	4.1	4.1	9 •	9	6	N 3	C 0	E 3
28	102.9	101.8	99.9	101.5	11.7	17.3	13.9	14.2	18.0	5.6	83	57	74	71	2.3	8.5	4.1	5.0	2	8	7	E 4	E 7	NE 6
29	96.6	95.9	98.7	97.1	11.5	16.3	11.7	12.8	17.3	9.9	73	63	48	61	3.6	6.9	7.1	5.9	10	10	6	NE 8	NE 7	NE 8
30	100.1	99.7	98.5	99.4	6.3	13.6	8.5	9.2	15.7	2.5	73	40	77	63	2.5	9.3	2.6	4.8	3	4	2	NE 6	W 4	W 1
31	99.3	99.9	99.5	99.6	11.3	15.9	13.9	13.8	18.1	4.4	65	45	56	55	4.7	10.0	7.1	7.3	1	8	8	E 1	E 6	E 7
M	103.0	102.9	102.8	102.9	8.7	13.5	10.4	10.8	15.2	6.2	84	63	75	74	1.7	6.1	3.3	3.7	7.1	7.8	6.6	4.3	5.5	4.0

Czerwiec – Juin

1	93.8	93.0	95.7	94.2	8.6	13.8	10.8	11.0	15.3	8.5	93	86	92	90	0.8	2.2	1.0	1.3	10 •	10 • K	10	NE 8	E 7	S 4
2	98.6	102.9	104.7	102.1	9.2	12.5	12.0	11.4	16.7	8.9	91	64	82	79	1.1	5.2	2.5	2.9	10 ••	10	8	NW 7	W 9	SW 2
3	106.4	107.2	107.4	107.0	10.3	17.5	12.6	13.2	19.6	6.0	81	56	77	71	2.4	8.8	3.4	4.9	4	8	0	SW 3	WNW 5	N 4
4	107.9	106.9	105.6	106.8	13.1	21.1	17.0	17.0	21.8	8.6	79	45	64	63	3.1	13.7	7.1	8.0	0	7	8	E 3	E 5	E 5
5	103.1	101.0	100.3	101.5	13.5	17.0	13.9	14.6	17.8	13.0	67	68	85	73	5.2	6.2	2.3	4.6	9	10 •	10	ENE 8	ENE 7	E 5
6	97.9	96.9	98.6	97.8	15.2	20.3	15.3	16.5	21.5	12.3	68	42	65	58	5.5	13.7	6.2	8.5	4	6	4	ENE 7	NE 11	NE 2
7	101.0	100.2	99.9	100.4	15.3	20.3	16.8	17.3	22.5	9.3	58	39	68	55	7.4	14.4	6.1	9.3	2	5	9	E 4	SW 2	NE 2
8	100.9	99.5	98.8	99.7	16.1	23.2	18.7	19.2	23.4	10.7	64	37	53	51	6.7	17.9	10.1	11.6	1	4	3	SE 5	ESE 7	E 8
9	97.8	96.5	96.6	97.0	15.5	21.8	18.3	18.5	22.5	12.5	75	57	72	68	4.4	11.3	5.8	7.2	1	8	8	E 8	E 10	E 7
10	98.0	99.2	99.5	98.9	15.0	15.9	15.8	15.6	19.6	14.5	87	88	79	85	2.2	2.1	3.7	2.7	10 •	9 •	7	E 5	ENE 6	E 5
11	98.2	97.9	100.4	98.8	16.5	20.6	14.0	16.3	21.6	11.2	76	51	91	73	4.6	11.8	1.5	6.0	5	9	9	NE 5	ENE10	NW 3
12	102.4	103.6	105.1	103.7	13.1	15.9	14.3	14.4	16.8	12.9	92	75	70	79	1.3	4.5	5.0	3.6	10 •	9	9	NW 8	NW 9	WNW 7
13	104.5	103.8	104.2	104.2	13.3	18.2	14.0	14.9	18.3	9.3	71	53	72	65	4.5	9.9	4.4	6.3	5	6	6	W 5	WNW 5	N 6
14	104.9	105.6	106.5	105.7	12.0	20.1	15.1	15.6	21.7	9.7	88	54	72	71	1.7	10.9	4.8	5.8	8	8	4	NW 6	NNW 5	N 5
15	108.5	107.6	105.9	107.3	15.8	22.2	16.5	17.8	23.8	8.0	47	39	65	50	9.4	16.4	6.6	10.8	0	2	2	E 3	SW 1	S 2
16	104.0	101.4	97.3	100.9	16.5	26.3	20.5	21.0	27.0	11.8	67	39	61	56	6.2	21.0	9.3	12.2	5	6	3	S 4	S 6	SSE 4
17	90.6	90.0	95.9	92.2	18.1	22.8	12.8	16.6	23.9	12.8	68	35	95	73	6.8	12.3	0.7	6.7	7	9	10	SSE 5	SSW 6	W 8
18	102.9	103.2	101.0	102.4	12.8	19.4	16.1	16.1	19.9	12.3	75	45	80	67	3.8	12.3	3.6	6.6	9	8	10 •	W 8	WSW 8	SW 6
19	98.6	100.5	105.1	101.4	16.3	21.6	16.8	17.9	22.2	15.0	92	47	63	67	1.5	13.6	7.0	7.4	9 •	6	6	SW 8	W 12	W 7
20	108.5	108.8	109.1	108.8	14.8	17.6	15.3	15.8	20.0	10.9	72	60	82	71	4.7	8.1	3.2	5.3	3	9	8	W 8	W 6	WNW 2
21	109.3	108.1	104.9	107.4	15.9	24.1	19.8	19.9	25.1	10.0	77	40	61	59	4.2	17.9	9.1	10.4	4	4	1	SW 1	C 0	SE 3
22	100.3	97.9	96.0	98.1	17.5	27.8	22.2	22.4	29.0	14.1	75	48	78	67	4.9	19.5	5.8	10.1	3	9	8	SE 3	S 7	S 3
23	98.9	101.6	104.3	101.6	17.7	20.2	16.9	17.9	22.2	16.6	88	59	78	75	2.4	9.7	4.2	5.4	9	8	1	SW 6	W 9	W 2
24	105.5	105.5	106.6	105.9	16.7	25.9	19.1	20.2	26.8	11.5	85	39	68	64	2.9	20.3	7.0	10.1	7	6	3	S 1	WSW 7	W 3
25	108.4	107.9	107.0	107.8	18.4	26.6	21.0	21.8	27.3	12.5	70	39	67	59	6.5	21.2	8.3	12.0	3	6	1	WNW 1	W 2	NNE 2
26	105.0	103.8	108.1	105.6	21.8	31.2	20.1	23.3	32.0	16.8	64	40	82	62	9.3	27.0	4.1	13.5	2	7	2	S 2	SW 8	NNW 2
27	110.7	110.3	109.9	110.3	16.5	16.7	13.9	15.2	20.1	13.9	53	66	92	70	8.9	6.4	1.3	5.5	9	10	8	SE 2	NE 2	SW 2
28	113.4	114.1	113.0	113.5	14.3	17.3	12.5	14.2	19.6	11.9	72	45	77	65	4.6	10.7	3.4	6.2	2	9	3	NW 6	WNW 8	W 2
29	108.4	109.5	110.3	109.3	14.3	20.8	13.8	15.7	23.1	9.4	70	45	69	61	5.0	13.3	4.9	7.8	9	6	0	WSW 8	W 8	NNW 3
30	110.0	107.1	101.0	106.0	14.5	22.8	19.3	19.0	23.4	7.0	68	41	72	60	5.3	16.3	6.2	9.3	0	2	2	WSW 3	SSW 5	S 2
31																								
M	103.3	103.0	103.3	103.2	15.0	20.7	16.2	17.0	22.2	11.4	74	52	74	67	4.6	12.6	5.0	7.4	5.3	7.2	5.4	5.0	6.4	3.9

Poznań – Ławica $H_s = 86$ m $H_b = 92.1$ m $h_w =$ 12.5 m anemometr M-47, 15 m anemometr Chauvin - Arnoux **Maj – Mai 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	≫ 14^{35}–16^{40}; ⌒ 1 – 3 ⌒ 4 – 6
2	8	•	•	⌒ 2 – 8
3	8	•	•	
4	8	5.1	•	● 23^{35}–24; ≫ 9^{40}–16^{45}, 19^{10}–20^{30}
5	6	0.6	•	● 0^{00} 20^{5}, 21^{5}–7^{30}; = 2^{20}–24
6	6	5.5	•	● 5^{05}...6^{40} ● – 7^{15}, ● – 9^{30} ● ● 9^{30} ● – 9^{35}, 9^{45}–10^{01} ● – 10^{08} ● – 11^{30}...17^{15-35}, 14^{15}–17^{35}, 18^{30} ● 18^{35}–19^{15}...40; = 0^{00}–4^{20} = – 4^{35} = – 6^{20} = – 6^{30} = –24; ⌒ 2 – 5
7	7	3.9	•	● 12^{02-06}, 13^{01-10}, 15^{10-50}, 16^{40}, 17^{10} ● 21^{35}–24; = 0^{00}–9^{20}, 19^{20}–24
8	6	1.7	•	● 0^{00}–9^{15}; = 0^{00}–13^{40} ∞ – 19^{30} = –24
9	6	27.2	•	● 9^{10} 10^{03}...10 11^{35} 13^{12} ● – 13^{20} ● – 16^{15} ● – 16^{35} ● – 17^{20} ● 19^{20} 10^{02-35} 20^{40}–24; ≫ 17^{20}–18^{20} (por. 18 m/sek 17^{25-32}) ≫ 19^{20}–24 (por. do 18 m sek); = 0^{00}–18^{30}
10	8	10.7	•	● 0^{00} 1^{35} 2^{35} 3^{05} ● – 3^{15} ● – 3^{35} 4^{02-40} 5^{45} 6^{10} 7^{33} 8^{05} 8^{32-44} 9^{05-10} 10^{32-38} 11^{06-30} 12^{18-36} ● 13^{45} 14^{02} ● 14^{21-35} ● – 15^{45} ● – 15^{27}, 15^{42} 17^{05} ● 17^{40} 21^{35}, 22^{04}–24; ≫ 0^{00} 21^{10}
11	7	0.2	•	● 0^{00-10} ● – 0^{40} ● – 1^{40} ● 20^{05-30} ● – 3^{45} ● ● 6^{10} ● – 6^{40} ● ● 7^{10} – 7^{10}...10^{35}; = 23^{0}–10^{40}
12	7	1.3	•	● 4^{40} 7^{30}, 8^{05} ● – 15^{32}, 15^{15} 19^{22-40}; = 3^{45} 4^{20} = – 9^{20} **10V** (por. do 17 m/sek), 24^{0} 3^{30} 5^{40} 6^{05} 6^{40} 8^{10}, 8^{12} 9^{15} 9^{42} 16^{45} (por. do 19 m/sek), por. wiatru 16 m/sek 19^{34-42}
13	6	1.8	•	= 5^{35-40} = 7^{15} = – 9^{30} ∞ – 13^{15} = 19^{40}–24; ⌒ 22 – 24
14	7	0.2	•	● 0^{15} 3^{25} 5^{05}, 7^{07-25}, 8^{20-35} 9^{08} ● 11^{33} 12^{02} ● 12^{10} 13^{10} ● 14^{03-35}, 15^{38} 16^{06}, 16^{45} 17^{10}; = 0^{00} 10^{15}; 10^{05}–24; ⌒ 0^{00}–1
15	6	0.1	•	● 21^{58}–22^{20}; = 0^{00}–5^{02} = 5^{05} = – 5^{15} = – 5^{40} = – 12^{30} ∞ – 24
16	6	14.7	•	● 14^{45}–15^{26} ● – 15^{35} ● – 15^{50}, 17^{30-40} ● – 18^{01} ● – 18^{10}, 19^{08-15} ● – 19^{22} ● – 20^{20}; (K) SW 14^{20} K 14^{45}–15^{43} (K) E
17	6	3.1	•	● 6^{20}...9^{05} 9^{45} 10^{03} 21^{10}–22^{40} 23^{15}; = 0^{00}–3^{10} = = – 3^{40} = – 10^{30} ∞ – 19^{40} = –24
18	7	5.6	•	● 1^{35}–2^{10}; = 0^{00}–6^{30} 22^{30}–24; ⌒ 21 – 24; ⊕ 12^{40}–14^{20}
19	6	11.2	•	● 2^{40}...3^{10}–4^{05}...25 – 5^{02} ● – 6^{10} ● – 7^{35} ● 10^{43}–11^{35} ● – 16^{50}; = 0^{00}–16^{30}, ⌒ 0^{00}–2
20	8	1.5	•	● 14^{45}–16^{35}
21	8	0.0	•	● 5^{15-25}, 9^{26-30}, ⌒ 1 – 3 ⌒ 4 – 5
22	8	•	•	= 3^{30}–3^{25} = = – 5^{10} = – 6^{35} ∞ – 8^{30} ⌒ 1 – 3 ⌒ zm. 4 – 5 ⌒ 6 – 8
23	8	0.0	•	● 21^{45}–24; ≫ 5^{30}–6^{40}, 7^{45}–10^{20}, por. wiatru 14 m/sek 10^{20}–17^{30} por. wiatru 13 m/sek 18^{40}–20^{35}
24	6	8.8	•	● 0^{30}–1^{40}, 5^{35} 7^{35} ● ● – 8^{40} ● – 9^{15} ● 10^{50}...14^{15} 15^{40} ● ● – 17^{10} – 18^{30} ● – 19^{45}; = 5^{20}–24
25	6	0.0	•	● 7^{30}–4^{30} ● – 6^{40}; = 0^{00}–24
26	6	7.3	•	● 0^{45} 1^{25} 6^{50}...7^{30}–13^{35} 14^{10} ● 18^{32}–20^{35} ● 20^{45}...22^{40}–24; = 0^{00}–14^{15}, 16^{20}–24
27	7	1.0	•	● 0^{00}–4^{30}...5^{40}, 6^{05}...30 – 7^{35}...8^{50} ● 14^{02}–15^{15}; = 0^{00}–11^{35}, 23^{30}–24
28	7	0.0	•	= 0^{00}–7^{30}; ⌒ 1 – 7 ⌒ 8 – 10; ⊕ 15^{00}–18^{15}
29	7	0.0	•	● 3^{30}...4^{25} ● 14^{27-35}; ≫ 11^{25}–12^{40}, 13^{45}–14^{10}, 14^{30}...20^{10}; = 3^{45}–7^{30}, ⊕ 15^{35}–16^{30}
30	8	•	•	⌒ 2 – 8
31	7	16.0	•	= 2^{45}–6^{15} ∞ – 8^{30}; ⌒ 1 – 6 ⌒ 7 – 9
Σ	–	117.5	–	

Czerwiec – Juin

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	7.0	•	● 2^{15}–6^{30} ● – 7^{15} ● 11^{45}–13^{20} ● – 13^{45} ● – 15^{20} ● ● 21^{40}–22^{30} ● 22^{35} ● 22^{40}–24; (K) SE 12^{20} K 12^{45}–14^{05} (K) NW 14^{15}; (K) SW 14^{10}–W – NW 14^{40}
2	7	0.0	•	● 0^{00}...30, 1^{35}–4^{30}, 4^{40}...5^{20} ● ● 6^{15}...7^{30} ● – 8^{10}, ≫ 8^{45}–9^{20}; = 0^{00}–11^{20}
3	7	•	•	= 2^{30}–3^{25} = = – 4^{10} = – 8^{50} ∞ – 20^{35} = –24; ⌒ 2 – 8
4	7	•	•	= 0^{00}–7^{40} ∞ – 24; ⌒ 3 – 7 ⌒ 8 – 9; ⊕ 17^{20}–18^{25}
5	7	2.9	•	● 12^{05}–13^{20}, 13^{30}...14^{15}–19^{40} ∞ 0^{00}–45 ...4^{30}, 14^{30}–24
6	7	•	•	≫ 7^{40}–10^{10} 12^{35}–13^{20}; = 0^{00}–5^{30}
7	7	•	•	∞ 19^{20}–21^{30} = –24
8	8	2.2	•	● 22^{20-30} por. wiatru 13 m/sek 13^{37} 14^{10} por. wiatru do 14 m/sek 16^{45}–18^{45}; = 0^{00}–6^{30} ∞ – 0^{40}, 19^{20}–24; ⌒ 1 – 7
9	7	0.4	•	● 0^{25-35}, 20^{5-30} ● – 3^{38} ● 4^{05} 7^{16}–3^{2} 17^{45-52} 23^{40}–24; ↖ SW 10^{6}, 23^{2} W; ≫ 11^{30}–15^{35}; ∞ 0^{00-30}, 7^{40}–24
10	6	1.1	•	● 0^{00-15} 2^{35}–3^{45}, 5^{45}–7^{15} ● 0^{40}...10^{10} ● 11^{02}–12^{02} 12^{35}–13^{05}; ∞ 0^{00-30} = – 14^{15}, 23^{40}–24
11	7	5.6	•	● 4^{40-45}, 11^{35-40}, 18^{50}–19^{40} ● – 20^{05} ● – 20^{20} ● 23^{50}–24; ≫ 12^{20}–17^{05}; = 0^{00}–7^{10}, 18^{20}–24; ⌒ 2 – 5
12	6	0.3	•	● 0^{00}...10, 6^{05}...7^{20}, 7^{43}...8^{45}–9^{15}...10^{27}; ≫ 0^{40}–1^{35}, 11^{45}–12^{15}, 15^{28-46}; = 0^{00}–12^{15} ∞ – 13^{30} = – 15^{15}
13	7	1.5	•	● 15^{05-20}, 16^{13-15} ● – 16^{25} ● – 16^{35}; (K) W 16^{03}–NW 16^{15}; = 2^{45}–5^{30} ∞ 15^{40}–16^{15} = – 17^{20}
14	7	0.6	•	● 3^{40}–4^{10}, 13^{30-15} ● 13^{45}–14^{01} ● 14^{05-08} ● – 14^{12} ● 14^{23-30}; = 2^{30}–7^{15}
15	7	•	•	∞ 6^{45}–8^{15} = 21^{40}–24; ⌒ 2 – 8
16	7	•	•	= 0^{00}–7^{15} ∞ – 24; ⊕ 11^{40}–13^{15}
17	7	8.4	•	● 15^{01}–20^{05} ● 20^{10-46}; ∞ 0^{00}–3^{45} = – 6^{15} ∞ – 11^{30} = 15^{30}–24; ⊖ 0^{40}–1^{20} ⊎ 2^{10}–3^{15}
18	7	5.3	•	● 16^{10}...17^{10} 18^{20}–20^{10} 20^{50}–24; ≫ 0^{15}–1^{35}; = 0^{00}–3^{30}, 21^{20}–24
19	7	0.2	•	● 0^{00}–1^{10} ● 2^{15-25} ● 0^{35}, 3^{40}, 7^{10-35}, 17^{35}–18^{02}, 19^{27-35}; ≫ 10^{35}–19^{40}; = 0^{00}–9^{15}
20	8	•	•	= 20^{30}–24; ⌒ 22 – 24
21	7	•	•	= 0^{00}–7^{15} ∞ – 8^{30}, 19^{30}–24; ⌒ 1 – 6 ⌒ 7 – 8; ⊕ 7^{40}–0^{30}
22	7	0.0	•	● 22^{36}–23^{15}; (K) S 22^{20}–K 22^{35}–24; = 0^{30}–7^{40} ∞ – 13^{30} = 20^{20}–24
23	7	0.0	•	● 15^{01-05}; (K) 0^{00}–NE 0^{15}; ≫ 9^{45}–10^{10}; = 20^{30}–24
24	7	•	•	= 0^{00}–3^{10} = = – 5^{15} = – 8^{15} ∞ – 20^{45} = –24; ⌒ 1 – 3 ⌒ 4 – 8; ⊕ 16^{40}–17^{10}
25	7	•	•	= 0^{00}–6^{45} ∞ – 8^{30}, 19^{30}–23^{40} = –24; ⌒ 3 – 8
26	7	0.3	•	● 15^{20-30}; (K) SW 14^{03}–SE – E 15^{40}; por. wiatru 14 m/sek 13^{35}–14^{02} = 0^{00}–6^{30} ∞ – 11^{40} = 20^{30}–24; ⌒ 4 – 8
27	7	0.1	•	● 8^{02-10}, 9^{50}–10^{03}; = 0^{00}–3^{30}, 20^{40}–24
28	8	•	•	= 0^{00}–5^{30}
29	7	•	•	≫ 14^{40}–17^{30}
30	8	11.6	•	= 2^{30}–4^{15} = 3^{40}–5^{20}; ⌒ 1 – 3 ⌒ 4 – 8
31				
Σ	–	45.5	–	

Poznań – Ławica φ = 52°25' λ = 16°50' Lipiec – Juillet 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	99.8	101.9	103.7	101.8	13.7	18.7	13.5	14.8	19.9	13.1	91	58	67	72	1.5	9.0	5.2	5.2	10	5	5	NW 3	W 8	N 4
2	103.4	101.0	99.0	101.1	12.7	17.9	15.0	15.2	19.1	6.5	67	36	57	53	4.9	13.0	7.2	8.4	4	6	9	NW 4	WNW 10	WSW 7
3	98.3	98.2	99.2	98.6	12.9	16.5	10.6	12.6	17.0	10.5	64	44	80	63	5.4	10.6	2.6	6.2	4	9	2	W 8	WSW 8	SW 4
4	99.3	98.4	98.5	98.7	11.5	17.1	11.4	12.8	18.6	3.6	75	42	76	64	3.5	11.4	3.3	6.1	3	7	3	W 5	W 7	C 0
5	99.0	99.2	100.3	99.5	11.1	14.4	13.8	13.3	18.1	6.4	77	55	55	62	3.1	7.3	7.2	5.9	7	8	8 •	W 3	W 6	NW 8
6	101.4	99.9	102.2	101.2	11.8	14.9	11.3	12.3	17.5	7.1	71	58	82	70	3.9	7.0	2.5	4.5	7	8	9 •	WSW 5	W 10	WNW 6
7	101.6	99.3	98.2	99.7	11.9	20.4	14.6	15.4	20.9	8.5	90	48	90	76	1.3	12.6	1.6	5.2	10	9	5	SW 4	SSW 8	SSW 3
8	95.5	91.5	91.1	92.7	13.4	18.1	13.3	14.5	20.4	8.9	93	77	86	85	1.1	4.9	2.1	2.7	10	10 •	7	NE 2	SW 7	W 7
9	95.5	97.7	100.5	97.9	12.0	14.9	10.5	12.0	16.9	8.9	77	59	87	74	3.2	6.9	1.6	3.9	9	8	3	W 8	WSW 8	SW 4
10	103.2	104.1	105.9	104.4	10.7	15.1	10.3	11.6	17.3	7.0	87	68	94	83	1.7	5.5	0.8	2.7	9	6	4	WSW 4	W 5	SW 3
11	108.5	108.4	106.9	107.9	11.3	18.0	15.1	14.9	19.8	8.5	90	49	78	72	1.3	10.5	3.9	5.2	8	8	4	W 4	W 5	S 3
12	103.2	100.9	101.7	101.9	17.4	20.5	16.5	17.7	21.0	13.0	72	66	94	77	5.5	8.1	1.2	4.9	9 •	10	5	SSW 7	SW 8	W 4
13	104.7	103.9	103.4	104.0	16.1	22.3	19.7	19.4	24.3	13.4	89	61	82	77	1.9	10.5	4.0	5.5	9	8	2	SW 3	SW 6	SE 3
14	104.0	104.2	104.5	104.2	20.0	31.4	24.9	25.3	32.0	16.4	82	41	69	64	4.2	27.2	9.7	13.7	4	4	9	S 1	SSW 5	SE 2
15	107.0	106.9	106.4	106.8	19.4	28.0	23.6	23.6	29.1	17.2	82	51	77	70	4.0	18.5	6.5	9.7	6	5	9 (K)	C 0	C 0	NW 6
16	106.0	104.9	106.1	105.7	18.3	25.5	19.9	20.9	25.7	16.4	94	62	91	82	1.2	12.2	2.0	5.1	9 •	6	9 • (K)	C 0	NE 4	N 3
17	104.2	103.4	103.5	103.7	17.0	19.1	18.5	18.3	21.3	16.9	96	88	83	89	0.8	2.5	3.5	2.3	10 •	10	10	N 6	NNE 5	NE 6
18	104.3	106.5	108.2	106.3	15.6	17.1	15.9	16.1	19.7	15.1	78	74	83	78	3.9	5.1	3.1	4.0	8	9	4	NE 8	ENE 9	N 4
19	109.7	109.5	109.4	109.5	15.3	24.1	19.8	19.8	25.1	11.8	75	39	59	58	4.4	18.3	9.5	10.7	2	4	2	ENE 4	E 8	E 3
20	109.5	107.9	104.2	107.2	17.2	24.1	20.5	20.6	25.0	13.9	67	42	60	56	6.5	17.3	9.7	11.2	1	2	2	SE 2	SE 5	E 5
21	101.1	98.7	97.0	98.9	16.9	22.1	16.9	18.2	24.8	15.9	73	73	96	81	5.2	7.3	0.8	4.4	3	4	8	E 4	ESE 5	SW 3
22	98.8	99.6	98.3	98.9	16.5	23.7	17.8	19.0	24.4	14.9	93	52	77	74	1.4	14.0	4.6	6.7	4	5	4	WSW 4	SW 5	S 2
23	96.3	97.1	97.9	97.2	17.4	16.7	14.3	15.7	21.1	13.7	84	88	93	88	3.2	2.4	1.1	2.2	8	9	2	SE 1	W 3	C 0
24	96.2	98.0	100.4	98.2	16.0	22.9	15.5	17.5	23.5	13.2	88	46	72	69	2.1	15.0	5.0	7.4	7	4	5	SW 7	WSW 8	SW 2
25	101.5	100.8	99.1	100.5	14.9	21.7	14.4	16.4	23.5	9.9	74	47	91	71	4.3	13.9	1.4	6.5	2	8	6	SW 2	SW 7	NE 2
26	101.0	99.4	98.9	99.8	14.5	21.2	16.5	17.2	22.7	11.6	82	43	64	63	2.9	14.4	6.8	8.0	2	7	10	WSW 5	W 9	W 6
27	99.9	101.1	100.6	100.5	12.5	14.6	12.3	12.9	18.3	12.0	81	63	93	79	2.7	6.2	1.0	3.3	10	9	7	W 6	W 8	SW 6
28	101.9	102.2	99.9	101.3	12.6	14.5	13.3	13.4	16.2	11.4	81	72	93	82	2.7	4.6	1.1	2.8	9	10 •	10 •	WSW 8	W 8	SW 5
29	96.0	93.8	89.6	93.1	14.1	19.9	15.0	16.0	21.3	12.7	87	66	83	79	2.2	7.9	2.9	4.3	10	8	10 •	SW 6	SW 8	SW 6
30	86.2	87.1	89.9	87.7	15.7	18.5	14.9	16.0	20.7	12.7	77	64	74	72	4.1	7.6	4.3	5.3	7	10 • K	9	SW 6	W 8	W 6
31	91.4	90.0	94.9	92.1	13.3	12.6	11.3	12.1	14.9	9.8	86	94	93	91	2.1	0.9	1.0	1.3	9	10 •	4	W 5	N 4	W 5
M	100.9	100.5	100.6	100.7	14.6	19.6	15.5	16.3	21.3	11.7	81	59	80	73	3.1	10.1	3.8	5.7	6.8	7.3	5.8	4.4	6.6	4.1

Sierpień – Août

1	99.0	100.0	99.9	99.6	11.3	17.9	10.8	12.7	19.3	9.8	88	47	87	74	1.7	10.8	1.7	4.7	7	6	5	W 6	SW 4	C 0
2	98.5	98.4	98.8	98.6	12.1	20.0	12.3	14.2	20.1	7.9	81	46	80	69	2.7	12.6	2.9	6.1	4	7	1	C 0	W 6	W 3
3	97.9	97.9	98.9	98.2	11.8	18.0	14.8	14.8	21.6	7.0	85	57	79	74	2.0	8.7	3.4	4.7	1	9 •	9	SW 2	W 10	SSW 3
4	101.2	103.3	106.2	103.6	14.4	16.5	13.5	14.5	19.6	11.4	91	82	81	85	1.4	3.5	3.0	2.6	10	9	2	W 5	W 7	W 3
5	108.9	109.1	108.2	108.7	13.0	20.7	17.0	16.9	23.3	8.2	81	58	80	73	2.8	10.2	3.9	5.6	9	6	2	SW 3	W 6	S 1
6	104.8	102.3	102.9	103.3	17.7	27.8	22.4	22.6	30.8	13.8	76	50	78	68	4.7	18.3	6.1	9.8	4	7	9 •	S 3	S 5	W 4
7	102.3	101.4	103.0	102.2	20.6	26.7	20.0	21.8	28.7	17.8	76	60	84	73	5.8	14.0	3.7	7.8	2	9	10 • K	SW 2	W 8	NW 4
8	105.0	103.8	104.9	104.6	16.8	21.9	18.9	19.1	22.0	16.4	93	76	70	80	1.0	6.4	6.5	4.6	9 •	9	9	NE 2	E 2	W 7
9	108.3	109.2	110.2	109.2	13.7	17.2	12.1	13.8	19.0	12.0	84	62	82	76	2.5	7.4	2.5	4.1	10	8	1	W 7	NW 5	N 3
10	111.3	111.3	111.3	111.4	12.4	18.1	13.8	14.5	19.3	6.8	92	59	73	75	1.2	8.6	4.2	4.7	4	7	9	NW 2	N 4	N 4
11	112.4	112.1	112.7	112.4	10.7	18.3	13.0	13.8	18.8	6.9	84	54	87	75	2.1	9.7	1.9	4.6	8	8	6	NW 3	NW 9	NNW 5
12	113.0	112.1	112.1	112.4	11.3	18.6	12.5	13.7	19.9	6.9	86	48	88	74	1.8	11.1	1.7	4.9	2	7	2	NW 4	NW 3	NE 3
13	112.2	111.5	110.9	111.3	10.4	17.0	11.5	12.6	18.0	6.0	86	55	81	74	1.8	8.8	2.7	4.4	4	9	2	NW 2	NE 8	NW 3
14	110.3	109.6	109.3	109.7	11.3	18.4	13.1	14.0	19.4	6.8	80	42	72	65	2.6	12.3	4.3	6.4	4	9	6	W 1	NW 5	N 4
15	110.6	110.6	110.6	110.6	11.3	16.4	13.4	13.6	18.2	9.2	88	60	86	78	1.7	7.4	2.1	3.7	9	8	6	WNW 5	NW 4	C 0
16	110.4	109.6	108.2	109.4	13.3	17.7	12.7	14.1	19.9	11.6	85	68	84	77	2.3	7.7	2.4	4.1	9	8	0	C 0	E 3	C 0
17	107.7	107.6	106.9	107.4	11.8	22.6	13.9	16.6	23.3	7.2	89	33	68	63	1.3	18.4	5.8	8.6	0	3	0	NE 1	S 2	E 2
18	107.9	108.2	108.6	108.2	13.3	24.5	16.9	17.9	23.5	9.9	82	35	73	63	2.8	19.9	5.2	9.3	0	2	0	SE 1	SSE 3	SE 1
19	111.0	111.6	111.4	111.3	13.9	26.4	17.3	18.8	26.8	10.4	87	31	79	66	2.2	23.7	4.2	10.0	2	2	1	C 0	NW 3	S 1
20	110.7	109.1	106.3	108.7	16.3	28.4	19.9	21.1	29.0	13.3	80	29	57	55	3.6	27.4	10.0	13.7	1	0	0	C 0	S 5	SE 3
21	103.4	102.0	98.9	101.4	16.0	23.7	20.2	20.0	25.9	13.8	76	53	68	66	4.4	13.8	7.7	8.6	7	4	5	S 2	SW 4	SE 2
22	96.3	94.3	92.3	94.4	17.9	28.4	23.3	23.3	29.4	16.3	73	29	39	47	5.6	27.4	17.3	16.8	2	6	2	SE 3	SSE 7	SSE 6
23	93.1	93.3	93.7	93.4	18.1	28.1	21.0	22.0	29.2	17.0	63	58	78	59	8.1	23.7	3.4	12.4	2	3	8	SSE 2	SSE 6	NW 6
24	97.0	98.3	97.1	97.3	16.9	19.1	18.4	18.2	21.0	16.3	97	83	91	91	0.6	3.4	1.9	2.0	10	10	10	NW 2	NW 3	NW 3
25	95.0	96.3	99.3	96.9	16.9	17.7	14.6	16.0	18.4	14.4	92	83	97	91	1.6	3.0	0.3	1.7	10 •	9	10 •	NW 4	W 3	W 3
26	103.7	104.0	103.8	103.8	10.3	13.6	12.6	12.8	16.9	10.0	87	50	88	73	1.6	8.9	1.7	4.1	7	9	6	W 6	WNW 6	W 1
27	102.2	101.1	101.3	101.6	10.4	16.0	10.7	12.0	18.3	7.6	91	53	84	77	1.1	8.2	2.1	3.8	10	9	0	NW 4	NW 8	W 3
28	103.0	104.3	103.7	104.4	11.2	14.7	12.2	12.6	18.9	9.9	91	72	83	83	1.2	4.7	2.2	2.7	2	9 •	8	W 3	NW 8	W 1
29	104.2	101.9	102.2	102.8	9.7	20.0	12.0	13.4	20.8	6.6	91	39	93	74	1.1	14.4	1.0	3.3	8	9	0	SSW 2	SW 6	W 2
30	103.3	104.3	105.2	104.3	10.9	13.7	10.3	11.9	18.0	9.9	96	83	81	80	0.3	6.6	2.4	3.2	9	9 •	2	W 4	W 3	NNW 2
31	103.0	103.6	101.3	103.3	8.2	18.0	13.6	13.4	19.3	3.0	97	49	74	73	0.3	10.3	4.0	4.9	0	9	4	S 2	SW 3	E 2
M	1[illegible].8	104.6	104.6	104.7	13.4	20.3	15.2	16.0	21.9	10.5	83	54	79	73	2.4	12.0	4.0	6.1	5.4	7.1	4.3	2.7	5.3	2.7

Poznań – Ławica $H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_w =$ 12,5 m anemometr M-47; 15 m anemometr Chauvin-Arnoux **Lipiec – Juillet 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ SNIEGU h	POGODA
1	7	0.1	•	● 3^42–55 ●' 4^10 ●° 6^20 7^10–20 (K)°W 2^13 – N 2^45 K W 3^40 3^50 4^44 E; = 2^20 11^30, ⌒° 23–24
2	8	0.0	•	●° 22^45 23^40; ≫ 12^50 – 14^05, por. wiatru 12 m/sek 14^20 15^30; = 2^30–50 = – 3^15 = – 4^40; ⌒° 0^00 – 3 ⌒' 4–9
3	8	0.3	•	●° 10^07–20, 16^25–30 ●' 16^35 ●° 16^40; ≫ 9^40 – 10^20; ⌒ 16^40–55
4	8	•	•	= 23^40 24; ⌒' 23–24
5	7	0.1	•	●° 8^03–06 12^28–31 14^01–03 15^10–15, 20^45 – 21^03; = 0^00 – 4^30; ⌒' 0^00 – 8
6	7	2.2	•	●° 8^13 9^05 9^46–50 ●' 10^01 ●° 10^07 11^10–42 12^10–28 13^01–07 14^42 15^01 16^02–13 ●' 20^08–15 ●° 20^27 ●' 20^50 ●° 21^15 por. wiatru 14 m/sek 11^15–33 ≫ 12^40 13^02 por. wiatru do 13 m/sek 13^32 14^35 por. 14 m/sek 14^45 15^13
7	6	1.5	•	● 4^35 5^40 ●° 14^06–10 ●' 14^14 ●° 14^20 ●' 14^28; ≫ 13^20–45; = 1^30 9^40 ∞ – 19^45 = – 22^35 = = – 24; ⌒° 22–23 [6.VII: ≫ 15^22–30 16^45 17^03 por. 14 m/sek 12^04–10, 20^10–20; ⌒° 1–8
8	7	7.2	•	●° 7^15–35 ●° 12^15...23, 12^35 13^45 – 17^20; = = 0^00 2^15 = ' 3^50 = ° 5^35 = – 10^30 ∞ – 12^30 = 13^40 19^20 22^40 24
9	7	1.7	•	●° 11^15–20 11^40–43 12^05–14 ●' 13^10–17 14^12–16 ●° 14^22 16^12–32 ●' 16^45 17^05–15, ≫ 9^40 12^10 13^10–20 13^30 – 17^12 por. wiatru 18 m/sek 16^35–42; = 0^00 3^30
10	7	0.8	•	● ° 7^02 ... 8^15 ●° 8^22 ●... 8^40 ●' 14^28–32 ●' – 14^38 ●° – 14^42 15^13–26 ●' – 15^36 ●° – 15^50 16^05–20 17^35–50 por. wiatru 12 m/sek 15^03–15 = 4^10 9^15 ∞ 11^10 14^30 18^30 24; ⊕ 9^40 10^10
11	7	0.0	•	● ° 10^45 – 19^05 23^35 24; = 0^00 8^40 ∞ – 10^10 15^15 20^30 = – 24
12	7	4.2	•	● ° 0^00–40 6^40 7^05 9^35 10^45 ●° 13^35 14^40 ● – 17^20 18^10–50; = 0^00 8^40 ∞ – 9^40 = – 11^50 ∞ – 12^40 = 14^05 19^20 20^20 24; por. wiatru 14 m/sek 13^03–40
13	6	•	•	= 0^00 3^45 = = – 4^40 = ° – 5^20 = – 10^30 ∞ – 13^10 = 20^15 – 24
14	7	1.8	•	●' 22^28–33 ●° 22^42 ●' 22^49 ●° 23^04 (K)° 23^12 K° 23^20 24; ≫ 22^20–25 (por. do 19 m/sek) ≫ – 22^35 (por. 24 m/sek) ≫ – 23^20 (por. 17 m/sek); = 0^00 8^30 ∞ – 22^15
15	7	15.3	•	●° 0^00 1^35 2^10 – 22^20 ●' 24; K° 0^00 NW 1^05 (K)° S 2^05 – K' 22^40 – 23^10 (K)' 24; = 1^30 – 6^20 ∞ 19^15 – 20^40 = – 24
16	7	5.8	•	●' 0^00–40 ●° – 1^30 6^35 7^10 7^40–50 ●° 20^02–15 ●° – 21^20 (K)° NE 1^40 (K)° ESE 3^45 SE-E 4^40 (K)° E 5^35 ESE-SE 6^35 (K)° S 17^45 K° 19^50 – 20^20 (K) SW 20^40 (K)° N 21^15 N-NW 21^10 = 0^00 0^15 2^05 2^30 22^45 24
17	5	0.9	•	●' 1^20–33 ●° 1^40 ●° 2^40 ●' 14^02–15 ●° – 4^20 ●° 15^12 6^40 ● ° – 9^45 ● ° – 11^10 12^15–40 ●° 18^35 19^10 (K) NE 1^10 – K° 1^25 – 1^35 (K) NW 2^35; = 0^00 24
18	8	0.0	•	●° 1^35 – 2^10 ● ° 13^08 ... 30; = 0^00 – 3^30
19	8	•	•	⌒° 4–8
20	8	•	•	⌒° 4–7
21	6	5.7	•	●° 9^46 – 10^05 17^01–09 17^15–22 17^35–47 18^03–36 ●' – 19^40 ●° – 20^35 (K)° SW 15^45 – S – K° 17^01 – 19^30 (K)° SW 20^05; ∞ 11^15 – 18^30 = – 24
22	7	•	•	= 0^00 – 10^15 20^30 24; ⌒° 22–24
23	6	10.2	•	● ° 10^02 – 12^35 ●' 19^20–42; = 0^00 – 13^30 20^40 – 24; ⌒' 1–6 ⌒° 7–8
24	8	•	•	●° 3^05–35; ≫ 9^10 – 10^15, por. wiatru 13 m/sek 10^28 11^40; 12^05 – 15^10 por. wiatru 14 m/sek 15^12 16^40; = 0^00 – 8^30
25	8	1.4	•	●' 20^03–15 ●° – 20^35; por. wiatru 14 m/sek 20^10–35; = 3^40 5^05 22^30 – 24; ⌒° 1–9
26	7	2.0	•	●° 17^40 – 18^02 18^10–20 ● ° 21^45 – 22^20 22^40 – 24, por. wiatru 14 m/sek 11^45 12^20 14^10–45 15^30 17^30; = 0^00 4^30; ⌒' 2–9
27	8	0.1	•	● ° 0^00 – 3^40 ●° 8^28–35 ● ° 10^40 – 20^10; = 12^20 – 24 [30.VII: por. wiatru 13 m/sek 11^10–12^15 por. 20 m/sek – 12^16 por. do 18 m/sek – 13^10 por. 13 m/sek 13^35–15^30; 16^20 – 19^20; ⌒° 3–8
28	7	2.8	•	●° 11^32 12^03 12^50 13^05 ● ° 14^48 17^30 ● ' – 17^45 ● ° – 19^05 ● ' – 19^40 ● ° – 21^10; por. wiatru do 14 m/sek 9^05–10 9^12–20 9^25 10^03 10^07–20 10^25 11^10; = 0^00 8^15 14^15 24
29	7	1.4	•	● ° 7^15 – 7^15 9^40 3^10 7^10 ... 18 9^20 ... 45 – 10^10 10^23 ... 40 11^15–35 ●° 15^18–24 ● ° 16^25 – 17^25 18^52 19^45 20^25 21^20; ≫ 13^45 – 14^08 14^50 15^45; = 0^00 – 10^30
30	6	5.6	•	●° 10^07–16 11^02–06 12^16–12 ●° 12^15 ●° 12^30 ●° 12^50 13^03 ●° 13^05 13^15–20 13^45 14^35 17^40 18^02 ●° 18^10 ●° – 18^20 K° SW 12^15–25 (K) NE 12^35 K° W 12^50–55 (K) NE 13^05; ≫ 8^20 – 10^20
31	5	9.0	•	● ° 10^35 – 11^05 ● ' – 13^30 ● ° – 14^15 ●° 17^45 18^35; = 3^30 – 8^40, 10^45 – 15^20 17^30 – 18^40 19^20 – 24
Σ	–	80.1	–	

Sierpień – Août

1	7	•	•	= 0^00 – 8^15; ⌒' 21–24
2	7	1.5	•	●° 14^01–17 15^05–10 15^47–50 ●▲' – 15^52 ●° 16^07; = 0^15 – 7^40 ∞ – 12^15; ⌒° 0^00 – 2 ⌒° 3–8 ⌒° 21–24
3	6	0.0	•	●° 12^46 ... 13^30 ≫ 12^35 – 13^05 por. 17 m/sek 12^40–44; = 1^15 – 8^30 ∞ – 20^40 = – 24; ⌒' 1–3 ⌒° 4–7 ⌒' 8–11 ⌒° 20–24
4	6	7.0	•	● ° 7^05–15 7^35–44 ●° 9^15–50 11^02–05 ●° – 11^10 ●° – 11^50; (K)° W 11^05 K° 11^10–15 (K)° E 11^20, por. 13 m/sek 13^40 14^30 15^15 17^40; = 0^00 13^30 ∞ – 15^30; ⌒° 0^00 2 ⌒' 3–5 ⌒° 6–7
5	6	•	•	= 4^20 11^40 ∞ – 13^30 = – 24; ⌒° 21–24
6	7	1.0	•	●° 10^42 11^01 ●° 20^40–46 ●° – 20^48 ●° 20^51 21^02; (K)° N 17^13 NE 17^35 (K)° SW 19^40 SE 20^37 ↖ NW 23^35 24; = 0^00 7^30 ∞ – 20^45 = – 24; ⌒° 0^00 2 ⌒' 3–8; ⊕ 14^20 – 15^30
7	7	1.6	•	●° 10^32 11^06 15^51 16^06 ●° 19^54 20^03 ●° 20^28–33 ●° – 21^15 22^02–15; ↖ NW 0^00 1^35 NE (K)° W 20^28 K° 20^35–40 (K)° E 21^06 (K)° SW 21^48 K° 22^00–05 (K)° NE 22^10; = 0^00 – 5^15;
8	6	0.3	•	●° 5^10 ... 35 ●° 5^42 7^15 ● ° 7^46 8^20 9^05 14^00–40 16^10–20; = 3^35 19^40 [7.VIII: ⌒' 2–5 ⌒° 6–9
9	7	•	•	●° 1^45 2^20
10	7	•	•	= 0^15 3^25 = = – 5^10 = – 7^20 ⌒° 0–2 ⌒' 3–8
11	8	1.7	•	●° 13^44 14^05 14^21 15^20 17^05–25 17^35 18^06; = 1^30 6^15; ⌒° 2–4 ⌒' 5–8
12	8	0.1	•	●' 15^10–13 ●° 15^22–35, por. wiatru 17 m/sek 14^50 15^15; = 1^10 – 4^10, 3^32 – 4^45 = 5^10 – 7^30; ⌒° 2–4 ⌒' 5–9 ⌒° 21–24
13	7	3.4	•	●° 10^37 11^02 ●' 13^01–12 ●° – 14^05 ●' 17^35–43; = 3^30 – 6^15; ⌒' 0^00 3 ⌒° 4–6 ⌒' 7–8
14	8	•	•	
15	8	1.4	•	●° 12^03–16 14^02–05 ●' – 14^15 ●° – 14^35 ●' 15^08–13 ●° – 15^39
16	7	•	•	= 4^15 – 8^30 ∞ – 9^40; ⌒° 2–9 ⌒' 20–24
17	8	•	•	= 1^20 – 3^30 = = – 5^15 = – 7^45 ∞ – 10^20; ⌒° 1–9 ⌒° 20–24
18	6	•	•	= 3^30 – 7^30 ∞ – 21^45 = – 24; ⌒° 0^00 2 ⌒' – 9 ⌒° 22–24
19	7	•	•	= 0^00 – 3^30 = = – 6^10 ∞ 8^30 – 19^40 = – 19^45 = = – 20^30 = – 24; ⌒° 0^00 4 ⌒' 5–7 ⌒° 8–9
20	6	•	•	= 0^00 – 7^30 ∞ – 24; ⌒° 4–9
21	6	•	•	∞ 0^00 – 2^20 = – 7^40 ∞ – 23^40 = – 24; ⌒° 2–7
22	7	•	•	= 0^00 – 7^20 ∞ – 24
23	7	2.8	•	●° 10^33–40 ●° 22^24–27 ●° – 22^32 23^16 24; (K) SW 10^27–28 SW; ∞ 0^00 – 20^30 = – 24
24	6	0.2	•	●° 0^00–40 ● ° – 2^05 6^15 ... 35 18^48 19^20; = 0^00 – 15^30 ∞ – 16^30 = – 24
25	6	5.5	•	●° 4^40 5^23 6^40 7^05 7^40 8^40 9^05 ... 20–50 11^05 ●° 13^17–30 ●° – 13^40 ● ° 14^45 15^03 ●' – 15^15 ●° – 17^30 18^42 20^25 ●' – 21^05 ●° – 21^30 22^40 23^38 24; = 0^00 – 24
26	8	•	•	●° 0^00 1^40, por. wiatru 13 m/sek 10^30–46; = 0^00 5^15 20^40 – 24; ⌒° 20–24; ⊕ 11^12 – 15^30
27	7	0.0	•	●° 16^03–08; = 0^00 – 9^40 23^48 24; ⌒° 0^00 3 ⌒' 4–9 ⌒° 19–24
28	8	0.0	•	●° 10^32 13^12; = 0^00 – 10^15 ∞ – 12^30 = 23^30 – 24; ⌒' 0^00 – 9
29	7	0.7	•	●° 15^15 – 16^05 17^03 18^30; = 0^00 4^05 = = – 5^30 = – 8^15 17^15 24; ⌒° 0–9; 22–24; ⊕ 11^30 – 14^40
30	7	0.0	•	●° 11^02 12^03 12^45 13^02; = 0^00 2^35 ●° – 2^50 = ' – 3^10 = ° – 4^40 = ° – 5^10 = – 9^30 22^20 24; ⌒' 1–3 ⌒° 4–7 ⌒° 8–10 ⌒' 20–24
31	7	•	•	= 0^00 – 4^00 = = – 5^30 = ° – 5^45 = ' – 6^20 = ° – 6^40 = – 9^15 ∞ – 20^30 = – 23^00 ∞ – 24; ⌒' 0^00 3 ⌒° 4–8 ⌒' 9–10
Σ	–	27.2	–	

Poznań - Ławica

$\varphi = 52°25'$ $\lambda = 16°50'$

Wrzesień - Septembre 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	99.0	100.9	102.7	100.9	12.9	21.2	16.4	16.7	22.1	12.5	78	44	91	71	3.3	14.0	1.7	6.3	9	8	10 •	SE 3	SW 2	NE 4
2	103.7	104.5	103.6	103.9	17.2	25.5	22.7	22.0	27.5	15.9	83	48	59	63	3.4	16.9	11.3	10.5	8	3	4	NNE 7	E 6	E 5
3	99.3	97.8	98.1	98.4	20.5	28.2	19.0	21.7	28.7	18.8	58	36	79	58	10.1	24.6	4.6	13.1	4	4	8	SE 6	SSE 8	E 3
4	97.9	98.9	98.2	98.3	15.0	20.3	15.9	16.8	21.0	14.8	94	61	90	82	0.9	9.2	1.8	4.0	10	9	9	NW 5	W 4	C 0
5	99.5	99.0	97.7	98.7	12.5	21.6	14.9	16.0	23.3	11.9	92	49	82	74	1.2	15.2	3.1	5.8	4	4	3	SW 2	SW 6	C 0
6	95.4	94.1	94.4	94.6	13.5	22.3	12.5	15.2	23.3	10.7	81	53	90	75	3.0	12.7	1.4	5.7	0	7	9	S 1	SW 4	SW 5
7	94.2	95.8	96.5	95.5	11.4	12.8	12.5	12.3	15.9	11.2	89	81	75	81	1.5	2.8	3.9	2.7	10	9	3	SW 7	WSW 9	SW 5
8	100.7	101.7	101.2	101.2	11.0	18.8	14.7	14.8	20.1	9.5	91	49	72	71	1.1	11.0	4.7	5.6	7	7	8	WSW 7	WSW 6	S 3
9	98.4	100.6	101.7	100.2	13.1	22.7	16.8	17.4	24.0	10.7	79	53	86	75	3.1	13.0	2.7	6.3	8	9	6	S 4	SW 4	WSW 2
10	96.2	98.5	101.8	98.8	16.6	16.7	12.0	14.3	19.9	11.8	81	76	91	83	3.7	4.6	1.2	3.2	8	9	8	SSE 3	WNW 8	W 2
11	98.4	102.4	105.3	101.4	11.9	13.8	9.3	11.1	13.8	9.3	93	81	95	90	1.0	3.0	0.6	1.5	10 •	9 •	2	NNW 9	W 5	SSW 2
12	102.9	102.0	100.5	101.8	7.3	17.4	11.6	12.0	18.7	6.7	96	52	79	76	0.4	9.3	2.8	4.2	10 ≡	7	6	S 1	SW 4	SW 3
13	100.1	100.4	100.7	100.4	9.4	16.8	11.6	12.4	17.4	8.2	92	62	90	81	1.0	7.3	1.3	3.2	0	8	9	SW 2	W 6	SW 3
14	102.5	104.2	107.3	104.7	8.7	16.9	10.3	11.6	18.1	7.1	94	57	92	81	0.6	8.2	0.9	3.2	9	9 •	5	SW 2	W 7	SW 3
15	109.7	111.6	114.5	111.9	11.3	17.5	10.0	12.2	17.8	10.0	90	61	88	80	1.3	7.9	1.5	3.6	8	8	2	W 5	WNW 7	NW 2
16	115.9	114.8	111.6	114.1	7.3	20.0	14.1	13.9	20.3	4.9	96	50	80	75	0.4	11.6	3.2	5.1	0 ≡	4	0	C 0	S 2	SE 3
17	109.4	108.7	107.4	108.5	11.1	23.2	15.4	16.3	24.3	10.4	90	54	89	78	1.3	15.2	1.9	5.5	2	3	1	S 2	W 3	S 1
18	104.4	101.6	100.7	102.2	13.5	24.2	18.6	18.7	24.8	12.8	90	51	76	72	1.6	14.9	5.1	7.2	0	0	6	SE 2	S 7	WSW 8
19	106.9	110.2	113.8	110.3	12.0	16.4	12.0	13.1	18.9	11.7	77	54	74	68	3.2	8.6	3.6	5.1	7	7	2	W 6	W 9	W 4
20	118.2	120.4	123.5	120.7	9.1	15.7	8.9	10.6	17.4	7.0	83	59	90	77	2.0	7.2	1.1	3.4	9	8	0	W 6	NW 7	WNW 3
21	123.9	123.2	119.5	122.2	5.9	17.0	9.0	10.2	17.4	4.1	95	53	86	78	0.5	9.2	1.6	3.8	7	10	3	SW 1	W 6	SW 3
22	113.5	113.1	109.2	112.6	6.9	20.4	10.8	12.2	21.4	5.5	91	44	84	73	0.8	13.5	2.2	5.5	6	3	0	SW 4	SW 4	SW 2
23	106.9	105.1	102.7	104.9	7.2	22.8	14.1	14.6	23.7	5.8	94	42	82	73	0.6	16.1	2.9	6.5	3	3	0	S 1	SSW 3	SE 2
24	103.1	102.9	102.2	102.7	9.8	23.9	15.7	16.3	24.7	9.0	95	38	65	66	0.6	18.3	6.2	8.4	0	0	0	SE 1	S 3	E 3
25	101.1	99.3	98.1	99.5	11.9	25.2	18.4	18.5	23.6	11.8	85	38	63	62	2.0	19.8	8.0	9.9	3	2	0	SE 4	SE 5	SE 3
26	93.0	92.8	93.9	93.9	14.1	24.8	18.4	18.9	25.0	13.5	76	34	61	57	3.9	20.5	8.4	10.9	0	2	0	SE 5	SE 8	SE 4
27	90.6	92.0	93.5	92.7	13.8	17.9	12.9	14.9	21.7	11.9	73	60	81	71	4.8	8.2	2.8	5.3	8	6	4	SE 5	SW 11	E 1
28	93.2	93.7	89.8	92.2	10.1	17.2	14.5	14.1	17.5	9.8	93	69	98	87	0.8	6.0	0.4	2.4	5	9	10	E 3	S 3	NW 4
29	94.4	97.1	100.7	97.4	11.3	12.8	10.1	11.1	15.6	10.0	93	83	87	88	1.0	2.6	1.6	1.7	10	10	2	W 2	WSW 5	SW 3
30	102.3	102.1	103.9	102.8	7.0	17.9	13.1	12.8	19.7	6.5	93	63	86	81	0.7	7.6	2.1	3.5	6	8	0	ESE 1	S 4	SE 2
31																								
M	102.6	103.0	103.2	102.9	11.5	19.7	13.9	14.8	21.0	10.1	87	55	82	75	2.0	11.2	3.2	5.5	5.7	6.2	4.0	3.6	5.6	2.9

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1	106.4	108.0	108.9	107.8	9.7	22.3	14.3	15.2	22.8	8.7	93	53	86	77	0.8	12.7	2.4	5.3	1	1	0	E 3	SE 3	E 3
2	107.3	105.3	106.3	106.3	10.5	21.0	16.5	16.1	21.1	10.4	92	56	78	75	1.0	10.9	4.3	5.4	0	2	10 •	E 6	ESE 8	ESE 3
3	109.7	111.5	112.4	111.2	12.4	17.3	11.4	13.1	19.0	11.0	94	69	91	85	0.9	6.2	1.2	2.8	10	3	3	NW 5	NW 2	NE 1
4	113.2	113.2	113.3	113.2	8.7	18.3	11.6	12.6	18.8	8.1	97	64	94	85	0.3	7.5	0.8	2.9	1 ≡	6	8	C 0	NE 2	E 2
5	114.0	115.2	114.9	114.7	9.1	11.2	10.0	10.1	13.2	8.9	96	90	87	91	0.5	1.3	1.6	1.1	10 ≡	10	9	SE 3	ENE 2	SE 2
6	114.1	113.3	111.4	112.9	9.0	13.4	9.1	10.2	15.4	8.3	95	68	91	85	0.7	5.0	1.1	2.3	10 ≡	5	0	SE 2	SSE 2	ESE 3
7	109.3	108.2	106.5	108.0	5.4	16.9	8.9	10.0	18.3	5.0	92	55	92	80	0.7	8.6	0.9	3.4	2	6	10	C 0	C 0	SW 2
8	105.5	107.4	109.1	107.3	7.7	10.6	10.0	9.6	12.2	5.3	94	82	88	88	0.6	2.3	1.5	1.5	10 ≡	10	6	NW 3	NW 5	N 4
9	110.2	109.4	108.6	109.4	4.2	11.7	5.5	6.7	12.5	2.9	90	54	81	75	0.8	6.2	1.7	2.9	8	9	2	N 3	N 5	N 4
10	108.1	107.5	107.6	107.7	3.0	10.7	6.9	6.9	11.3	2.7	90	62	87	80	0.8	4.9	1.3	2.3	6	9	9	NW 2	WNW 7	WNW 3
11	107.2	106.6	110.7	108.2	2.5	11.9	7.0	7.1	12.9	2.3	91	58	63	71	0.6	5.8	3.7	3.4	2	7	0	W 2	WNW 8	NE 5
12	116.5	118.1	118.2	117.6	-1.0	10.5	1.0	2.9	10.8	-1.7	95	39	90	75	0.3	7.8	0.7	2.9	0	4	1	C 0	S 2	W 1
13	116.7	114.7	112.3	114.6	-2.1	12.5	5.9	5.6	14.5	-2.1	94	45	80	75	0.3	8.0	1.9	3.4	6	8	2	C 0	SW 3	SW 4
14	111.5	111.0	110.0	110.8	1.4	14.8	5.9	7.0	15.6	1.3	92	54	89	78	0.6	7.7	1.0	3.1	0	4	0	SW 2	SSW 4	SE 1
15	108.9	107.5	106.0	107.5	1.6	13.9	9.8	9.3	17.9	-0.6	93	53	81	76	0.6	8.2	2.3	3.7	0	8	0	SSE 1	SSW 6	SW 3
16	104.2	103.8	109.9	106.6	10.6	9.5	9.0	9.5	12.1	8.9	79	92	90	87	2.8	1.0	1.1	1.6	10	10 •	4	SW 5	W 4	W 6
17	113.1	117.3	117.7	116.7	7.0	12.3	7.7	8.7	12.4	6.7	83	63	79	76	1.4	3.0	2.2	2.9	8	6	9	W 5	W 5	W 3
18	115.6	115.0	113.7	115.4	7.1	12.3	8.4	9.0	13.1	7.0	83	78	89	84	1.3	3.2	1.2	2.0	10	8	0	SW 2	W 6	NW 3
19	116.9	118.1	118.7	117.9	4.6	7.4	3.2	4.6	9.1	2.3	93	96	93	93	0.4	0.3	0.3	0.3	10 ≡	10	0	NW 2	NW 2	W 2
20	120.6	122.5	122.9	122.0	2.6	10.1	4.3	5.4	11.4	0.0	93	71	87	84	0.4	3.6	1.1	1.7	10	5	0	E 1	E 3	E 2
21	124.3	123.5	123.9	123.2	0.7	7.9	2.1	3.2	8.3	0.1	90	59	84	78	0.6	4.3	1.2	2.0	3	6	0	E 3	E 3	E 2
22	126.7	126.2	124.6	125.8	-3.0	7.3	-1.4	0.4	8.7	-3.3	90	53	83	77	0.3	4.6	0.8	2.0	0	0	0	C 0	E 2	C 0
23	122.1	120.6	119.5	120.7	-3.1	9.3	2.6	2.9	11.3	-3.3	93	68	91	84	0.4	3.9	0.7	1.7	6	3	0	NW 1	WNW 5	NW 3
24	119.6	120.3	120.0	120.0	6.2	9.3	1.5	4.6	9.9	1.1	88	67	91	82	1.2	3.8	0.6	1.9	10	9	0 ≡	SW 1	C 0	W 1
25	118.7	118.2	117.3	118.1	-3.2	8.9	6.0	4.4	9.2	-3.2	92	72	89	84	0.3	3.2	1.1	1.3	7 ≡	2	10	C 0	SW 1	NE 1
26	113.2	113.0	110.4	112.9	4.4	10.0	1.0	4.1	11.2	1.0	90	63	92	82	0.9	4.3	0.3	2.0	7	3	10 ≡	S 1	SSE 4	SW 2
27	108.8	108.4	107.0	108.1	1.3	4.6	3.0	3.0	6.2	0.4	94	93	93	93	0.4	0.4	0.4	0.4	10 ≡	10 ≡	0 ≡	W 3	SW 3	S 3
28	104.3	103.7	103.2	103.8	7.2	14.8	9.3	10.2	16.3	2.1	84	67	83	78	1.7	5.3	2.1	3.1	10	9	0	SE 4	SW 6	SW 3
29	101.2	98.5	104.4	101.4	7.2	18.2	8.1	10.4	18.9	6.3	91	58	89	79	0.9	8.8	1.2	3.6	0	1	2	S 3	SW 7	SW 7
30	107.9	107.6	103.9	106.5	4.3	11.4	4.9	6.4	11.3	4.3	87	61	84	77	1.1	3.3	1.4	2.6	0	6	3	SE 3	WSW 7	S 3
31	98.3	98.8	98.8	98.6	9.2	11.9	3.3	8.0	12.3	4.7	72	44	83	66	3.2	7.8	1.3	4.2	-6	6	2	SW 7	W 8	SW 8
M	112.2	112.1	112.1	112.1	4.7	12.4	6.8	7.7	13.3	3.3	91	63	87	81	0.9	3.4	1.4	2.6	3.6	6.0	3.3	2.4	4.1	3.1

Poznań – Ławica $H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_w =$ 125 m anemometr M-47 / 15 m anemometr Chauvin-Arnoux **Wrzesień – Septembre 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚNIEGU h	POGODA
1	7	5.0	•	●°17^46–21^20, 22^40–23^45; ∞ 0^00–6^15 = –8^40 ∞ –18^20 = –24; ⊕ 12^40–14^15
2	7	•	•	●'0^10–1^05 ●°–1^20, 2^15–50; = 0^00–9^30 ∞ –13^30, 17^20–24
3	7	9.2	•	por. wiatru 12 m/sek 10^15–20 ≫ 11^01–35; por. wiatru 14 m/sek 11^40–12^50 ≫ 13^15–40; ∞ 0^00–20^35 = –24
4	7	•	•	▽°0^40–2^30 ●°–4^30, 4^45–5^40; = 0^00–10^40 ∞ 11^45–17^30 = 18^30–24; ⌓' 21–24; ⊕ 12^35–14^20
5	7	•	•	= 0^00–9^30 ∞ –12^30 = 20^15–24; ⌓'0^00–2 ⌓°3–5 ⌓'6–9 ⌓°20–24
6	6	1.3	•	●°18^25–20^40; = 0^00–8^30 ∞ –16^30 = –17^30, 18^20–24; ⌓°0^00–3 ⌓'4–10
7	6	0.1	•	●°10^34...50–11^40, 11^45–12^20; = 0^00–10^30, 10^50–13^40 ∞ –19^40 = –24
8	7	•	•	= 0^00–10^15 ∞ –19^45 = –24; ⌓°1–3 ⌓'4–7 ⌓°8–10
9	8	0.2	•	●°17^45–18^05, 18^20–50, 19^35–47; = 0^00–7^10 ∞ 7^30–8^15 = 21^15–24; ⌓°3–9
10	6	25.1	•	▽10^56–11^01, por. wiatru 14 m/sek 10^54–11^02; = 0^00–9^40 ∞ –11^10 = –13^20, 19^40–24; ⌓°3–10, 19–24
11	7	0.4	•	●°2^08–30 ●'–3^35 ●°–4^40 ●'–6^05 ●°7^20–7^35 8^05–8^10–50, 8^55–9^10, 10^05–12^45 ●°–13^35 ●°13^45–14^10; = 0^00–8^45, 18^40–23^05 ≡°–24; ⌓°0^00–2
12	7	•	•	≡°0^00–15 = –2^10 ≡°–2^40 ≡'–4^55 ≡'–6^50 ≡°–7^10 = –9^45 ∞ –14^15, ⌓°21–24
13	7	•	•	= 4^30–9^40 ∞ –17^35 = –24; ⌓°0^00–3 ⌓'4–7 ⌓°8–11, 19–24
14	6	0.0	•	▽°12^47–53, 14^36–15^07; = 0^00–9^30 ∞ –14^45 = –24, ⌓°0^00–3 ⌓'4–9 ⌓°10–11, 20–24
15	7	•	•	= 0^00–9^15 ∞ 13^15–17^30 = –23^40 ≡²–24; ⌓°0^00–10, 20–24
16	7	•	•	≡²0^00–10 ≡°–1^30 ≡'–2^40 ≡²–4^35 ≡'–5^20 ≡²–5^40 ≡²–6^30 ≡'–7^20 = –9^40 ∞ –20^30 = –24; ⌓°0^00–2 ⌓'3–10, 20–24
17	6	•	•	= 0^00–9^20 ∞ –18^10 = –24; ⌓'0^00–4 ⌓²5–7 ⌓'8–9, 20–24
18	7	0.0	•	▽°21^28–22^05; < W 19^45–20^30 WNW; = 0^00–8^30 ∞ –19^30 = –21^40; ⌓'0^00–2 ⌓²3–9
19	8	•	•	por. wiatru 13 m/sek 9^20–11^40
20	8	•	•	⌓°2–9, 21–24
21	7	•	•	= 1^30–2^10 ≡ –3^45 = –9^40 ∞ –11^15 = 19^15–24; ⌓°0^00–3 ⌓'4–9; ⊕ 9^45–15^20
22	6	•	•	= 0^00–8^45 ∞ –18^30 = –24; ⌓°1–2 ⌓'3–9 ⌓°21–24
23	6	•	•	= 0^00–4^30 ≡ –6^15 ≡ –8^40 ∞ –20^30 = –24; ⌓°0^00–3 ⌓'4–7 ⌓°8–10, 21–24
24	6	•	•	= 0^00–4^30 ≡ 4^40–6^10 ∞ 9^30–24; ⌓°0^00–2 ⌓'3–10
25	6	•	•	= 0^00–8^35 ∞ –24
26	7	•	•	por. wiatru 14 m/sek 11^10–20 ≫ 11^50–12^20, por. wiatru 14 m/sek 14^10–16^05; ∞ 0^00–3^30 = –8^15 ∞ –24
27	7	0.0	•	▽°7^05–10 ●°8^06...42; por. wiatru 13 m/sek 9^50–11^40, por. wiatru 18 m/sek 11^40–50 ≫ 15^40, ∞ 0^00–13^0 = –8^30 ∞ –12^40
28	6	22.7	•	●°13^20–14^40–15^15...45–16^01 ●'–16^15 ●°–16^30 ●'–17^30 ●°–18^10–43 ●'–19^03 ●°–19^28 ●'–19^40 ▽²19^01–07 ●°–21^17 ●²20^05–45 ●°●°–23^30; = 5^20–10^15 ∞ –13^30 = –24;
29	6	•	•	●²2^35–3^30; = 0^00–15^30 ∞ –17^15 = –24; ⌓°19–23 [28.IX: ⌓'3–7 ⌓°8–9; ⊖ 8^15–10^20
30	6	•	•	= 0^00–9^15 ∞ –17^30 = –24; ⌓'0^00–4 ⌓²5–8 ⌓°9–11 ⌓'19–24
31				
Σ	–	54.0	–	

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1	7	•	•	= 0^00–10^40 ∞ –17^45 = –24; ⌓'0^00–3 ⌓²4–9 ⌓°10–11, 19–24
2	6	0.3	•	●°20^30–21^10...30 = 0^00–9^30 ∞ –18^20 = –24; ⌓°0^00–3 ⌓'4–8 ⌓°9–10
3	6	•	•	●°7^10–40; = 0^00–7^45 ≡°–8^35 = –12^40 ∞ –18^30 = –24, ⌓'20–24
4	6	•	•	= 0^00–3^10 ≡°–3^20 ≡²–8^25 ≡'–8^35 ≡°–9^20 = –11^40 ∞ –16^45 = –23^45 ≡°–24, ⌓°0^00–2 ⌓²3–11 ⌓'20–24
5	6	•	•	≡°0^00–20 ≡²2^40 ≡°–3^30 ≡²–4^15 ≡²–9^45 ≡°–10^50 = –24, ⌓²1–9 ⌓'10–12 ⌓°13–14, 18–24
6	4	0.0	•	●°8^35–9^30; = 0^00–8^15 ≡°–7^10 = –12^20 ∞ –17^15 = –24; ⌓°0^00–8, 20–24
7	6	•	•	= 0^00–25 ≡°–1^45 ≡'–3^35 = –10^40 ∞ –17^30 = –24, ⌓²19–24
8	6	0.0	•	●°8^40–9^15; = 0^00–1^20 ≡°–2^40 ≡²–5^10 ≡'–6^20 ≡²–8^45 ≡'–9^20 ≡°–10^10 = –24, ⌓²0^00–8
9	8	•	•	= 0^00–7^15; ⌓°1–9
10	8	•	•	⌓°2–10
11	7	•	•	= 4^30–5^40 ≡ ≡ –6^45 = –9^40 ∞ –11^30; ⌓°0^00–4 ⌓'5–10
12	8	•	•	= 5^30–45 ≡ –8^05 ≡ –8^15 = 16^45–17^40 = 18^15–24, ⌴²2–10 ⌓°19–24
13	7	•	•	= 0^00–5^50 ≡ ≡ –7^05 = –8^40 ∞ –12^30, 16^45–19^15 = –24, ⌓°0^00–1 ⌴'2–4 ⌴²5–9 ⌓°20–24; ⊕ 10^35–13^30
14	6	•	•	= 0^00–9^30 ∞ –17^30 = –17^45 ≡°–18^15 = –24, ⌓°0^00–2 ⌓'3–8 ⌓°9–11, 22–24
15	6	0.0	•	= 0^00–9^30 ∞ –17^30 = –24; ⌓°0^00–2 ⌴°3–8 ⌓°20–24; ⊕ 12^30–13^20
16	6	7.7	•	●°5^50...6^15 8^20–35, 10^15–11^10–17^10, 19^05–16; = 0^00–24, ⌓°0^00–3
17	7	•	•	= 0^00–7^20 23^45–24
18	7	•	•	= 0^00–8^35 20^40–24
19	5	•	•	≡°4^40–5^35 ≡'–6^20 ≡²–9^50 ≡'–10^15 ≡°–10^45 ≡°–12^20 = –19^35 = ≡ –22^20 ≡°–22^45 ≡²23^50 ≡'–24, ⌓°1–11, 20–24; ⊖ 0^40–3^50
20	6	•	•	≡'0^00–1^20 ≡²–4^40 ≡²–5^30 ≡°–5^50 ≡ –8^40 ≡°–9^05 = –12^30 ∞ –16^40 = –24, ⌓°0^00–2 ⌓'3–4 ⌓²5–11 ⌓'18–20 ⌓²21–24
21	7	•	•	= 0^00–9^30 ∞ –13^20, 16^35–17^45 = –24; ⌓²0^00–2 ⌴'3–5 ⌴²6–9 ⌓°20–24
22	6	•	•	= 0^00–9^20 ∞ –15^40 = –22^40 ≡'–23^45 = –24; ⌴°0^00–2 ⌴'3–4 ⌴²5–8 ⌴°9–11 ⌓°18–20 ⌴°21–23
23	7	•	•	= 0^00–25 ≡°–0^50 ≡'–1^15 ≡°–1^30 = –2^45 ≡'–2^50 ≡²–3^40 ≡°–5^35 ≡ ≡ –7^05 = –10^40 ∞ –16^30 = –21^20 ≡°–21^25 ≡'–21^30 ≡²–21^50 = –24, ⌴'0–2
24	6	•	•	= 0^00–9^40 ∞ –16^30 = –20^40 ≡°–22^45 ≡'–24, ⌓°0^00–10, 18–19 ⌴°20–24 [23.X: ⌴²3–9 ⌓°19–24
25	5	•	•	≡'0^00–15 ≡°–1^20 ≡'–6^15 ≡°–7^20 ≡²–9^25 ≡'–9^30 ≡°–10^40 = –24, ⌴°0^00–2 ⌴²3–10 ⌓°21–24
26	6	•	•	= 0^00–6^35 ≡ ≡ –7^35 ∞ 11^30–16^35 = –19^45 ≡'–20^10 ≡²–23^15 ≡'–23^45 ≡²24; = 0^00–6^35 ≡ ≡ –7^35 = 16^35–19^45, ⌓°0^00–10, 17–24
27	2	•	•	≡²0^00–11^40 ≡'–13^35 ≡'–14^10 ≡°–15^40 ≡²–16^50 ≡'–19^45 ≡²–21^15 ≡'–21^35 ≡°–23^45 = –24, ⌓²2–13 ⌓°14–18 ⌓'19–24
28	6	•	•	= 0^00–10^40 ∞ –16^30 = –24; ⌓'0^00–10, 19–24
29	6	1.2	•	▽°14^35–15^06 ●°–17^10; 17^15...40; ≫ 16^10–16; = 0^00–10^40 ∞ –15^20 = –24, ⌓'0^00–3 ⌓²4–10
30	7	•	•	= 0^00–5^10 8^15–11^30 ∞ –16^40 = –17^45; ⌓°18–24
31	7	2.6	•	▽°13^50–14^05 ▽'14^24–35 ▽°16^02–07, 17^20–45, por. wiatru 13 m/sek 9^20–14^45, por. wiatru 18 m/sek 17^20–35 por. wiatru 13 m/sek –17^45; ⌓°0^00–4, ⌒ 14^30–40
Σ	–	11.8	–	

Poznań – Ławica φ = 52°25' λ = 16°50' Listopad – Novembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	94.4	87.3	82.8	88.3	6.3	11.2	11.3	10.0	12.3	5.4	89	89	79	86	1.0	1.5	2.8	1.8	10 •	10	4	S 6	SW 8	SW 8
2	84.4	87.1	88.1	86.5	8.2	10.1	8.6	8.9	11.3	7.6	65	47	68	60	3.9	6.6	3.6	4.7	4	9	9 •	WSW 9	WSW 12	SW 9
3	94.6	96.4	98.7	96.6	4.8	8.6	3.8	5.2	8.9	3.7	79	59	83	74	1.8	4.6	1.3	2.6	3	8	0	WSW 8	WSW 9	W 6
4	104.8	108.7	112.5	108.7	1.3	5.3	3.4	3.4	6.8	0.8	91	74	83	83	0.6	2.3	1.5	1.5	9	9	0	WSW 5	W 7	W 4
5	116.7	118.5	120.4	118.5	1.9	3.1	3.7	3.1	3.8	-0.2	91	95	82	89	0.6	0.4	1.5	0.8	10 ≡	10 • ≡	10	W 3	W 5	W 5
6	119.7	118.5	115.1	117.8	3.3	5.5	5.3	4.8	5.9	3.0	85	81	89	85	1.2	1.7	1.0	1.3	10	10	10 •	W 6	SW 6	SW 2
7	111.0	110.0	110.9	110.6	4.0	7.5	3.4	4.8	8.6	3.0	94	83	91	89	0.6	1.8	0.7	1.0	10	9	2	C 0	C 0	C 0
8	112.5	113.1	113.1	112.9	1.4	7.3	1.9	3.1	7.8	-0.4	94	79	91	88	0.4	2.2	0.6	1.1	10 ≡	6	2 ≡	E 1	S 1	E 1
9	112.1	111.7	110.9	111.6	3.1	7.0	7.0	6.0	7.9	0.1	91	93	94	93	0.6	0.7	0.6	0.6	10 ≡	10 ≡	10 ≡	C 0	WNW 3	NW 2
10	109.6	109.0	107.2	108.6	5.6	6.9	6.8	6.5	7.2	5.2	94	92	91	92	0.6	0.7	0.9	0.7	10 ≡	10	10	NW 3	N 1	NE 1
11	103.5	102.4	100.9	102.2	2.7	4.7	2.0	2.8	6.8	1.9	89	74	66	76	0.8	2.1	2.5	1.8	9	10 •	10	E 7	E 7	E 8
12	100.2	100.8	102.1	101.0	-0.9	0.7	-1.6	-0.3	2.0	-1.7	81	69	75	75	1.1	2.0	1.3	1.5	9	8 *	9	ENE 8	NE 9	NE 7
13	102.7	103.5	104.2	103.5	-2.2	-2.2	-3.2	-2.7	-1.6	-3.2	72	74	79	75	1.5	1.3	1.0	1.3	10 *	10 *	10 *	E 8	E 10	E 9
14	104.8	105.3	105.9	105.3	-5.0	-2.7	-3.9	-3.9	-2.5	-5.2	78	65	75	73	0.9	1.8	1.1	1.3	9	9	10 *	ENE 7	E 4	E 4
15	106.3	108.5	112.2	109.0	-5.4	-4.6	-4.2	-4.6	-3.9	-6.6	85	76	70	77	0.6	1.0	1.3	1.0	10 *	10 *	10	NE 4	N 5	N 3
16	116.7	117.5	118.6	117.6	-5.7	-3.3	-10.3	-7.4	-3.2	-10.3	82	74	81	79	0.7	1.2	0.5	0.8	10 *	9	0	C 0	C 0	C 0
17	116.1	114.0	110.4	113.5	-12.1	-7.9	-9.4	-9.7	-7.9	-12.7	85	84	85	85	0.4	0.5	0.4	0.4	9 △	10	10 ≺ ≻	SE 1	SE 2	ESE 3
18	104.8	102.3	98.9	102.0	-13.0	-10.1	-10.0	-10.8	-9.4	-13.6	69	74	74	72	0.7	0.7	0.7	0.7	4	6	10 *	E 6	E 8	ESE 4
19	95.0	92.7	92.3	93.3	-9.4	-7.8	-6.9	-7.8	-6.6	-10.0	79	76	80	78	0.6	0.8	0.7	0.7	10 *	10 *	10	E 4	E 7	E 4
20	93.2	94.0	91.6	92.9	-7.2	-5.8	-5.5	-6.0	-5.2	-7.3	77	77	85	80	0.8	0.9	0.6	0.8	10	10	10	NE 4	ENE 3	E 7
21	83.2	78.0	78.1	79.8	-3.7	-2.2	-3.9	-3.4	-1.7	-5.5	92	91	85	89	0.4	0.5	0.7	0.5	10 •	10 *	10 *	E 8	E 9	N 7
22	90.2	96.5	102.9	96.5	-0.8	-0.9	-5.1	-3.0	-0.4	-5.8	91	89	83	88	0.5	0.6	0.7	0.6	10 *	9 *	8	NW 9	WNW 7	NW 7
23	107.9	110.0	110.3	109.4	-14.7	-7.8	-13.1	-12.2	-5.1	-15.2	78	67	80	75	0.4	1.1	0.4	0.6	0	6	0	W 3	WSW 2	S 2
24	107.1	103.8	99.9	103.6	-12.4	-2.5	-2.2	-4.3	-2.1	-13.2	81	61	68	70	0.4	2.0	1.7	1.4	0	8	10	SSE 2	SSE 5	SE 6
25	98.5	101.9	101.7	100.7	0.7	1.7	-1.0	0.1	1.9	-2.6	90	87	85	87	0.6	0.9	0.9	0.8	10 *	10 •	2	SW 6	SW 6	S 5
26	89.9	85.8	90.8	88.8	-0.2	2.9	1.4	1.4	3.9	-1.4	67	94	83	68	2.0	3.5	1.1	2.2	9	10	3	SSE 6	S 10	SW 5
27	89.7	80.8	69.7	80.1	-3.6	0.4	2.3	0.4	2.3	-4.8	87	89	93	90	0.6	0.7	0.5	0.6	8	10 *	10 •	SSE 4	ESE 4	S 5
28	73.1	75.7	81.3	76.7	1.6	1.3	1.7	1.6	2.8	0.8	87	85	83	85	0.9	1.0	1.1	1.0	10 • •	10 *	10 *	WSW 8	SE 6	SW 8
29	88.6	91.2	81.8	87.2	1.9	2.4	1.6	1.9	2.6	1.1	84	84	63	77	1.2	1.2	2.6	1.7	10	9	10	W 8	SW 4	SE 7
30	74.3	81.0	85.6	80.3	4.7	5.0	1.7	3.3	6.1	1.5	67	63	63	64	2.8	3.3	2.5	2.9	9	10	4	S 8	SW 5	SW 5
31																								
M	100.2	100.2	100.0	100.1	-1.5	1.1	-0.5	-0.4	2.0	-2.9	83	77	80	80	1.0	1.7	1.2	1.3	8.4	9.2	7.1	5.1	5.5	4.8

Grudzień – Décembre

1	79.1	81.8	88.9	83.3	0.2	1.9	1.2	1.1	2.8	0.1	92	91	90	91	0.5	0.6	0.7	0.6	10 *	10 •	10 •	S 7	SW 8	WSW 5
2	94.4	95.2	90.2	93.3	0.1	0.4	-0.1	0.1	1.8	-0.3	98	86	92	92	0.2	0.9	0.5	0.5	10	9	6	W 8	SW 2	S 4
3	83.6	84.0	85.4	84.3	0.9	2.7	1.3	1.6	2.8	-0.2	95	86	91	87	1.0	1.0	0.5	0.9	9	9 •	9	S 6	S 6	S 4
4	86.8	88.1	89.5	88.1	0.5	4.5	3.2	2.8	5.0	0.2	92	79	83	85	0.5	1.8	1.3	1.2	4	4	10 •	SW 3	SW 4	SW 5
5	91.9	87.9	73.5	84.4	-1.7	3.0	3.6	2.1	4.7	-2.0	91	84	88	88	0.5	1.2	0.9	0.9	6	9	10 •	S 2	SE 4	SSE 10
6	77.9	82.2	88.0	82.7	6.0	7.3	3.3	5.0	8.6	3.1	60	58	79	66	3.8	4.3	1.5	3.2	9	5	4	WSW 12	WSW 10	WSW 6
7	92.0	95.2	97.9	95.0	3.0	4.6	2.2	3.0	5.0	1.8	71	70	89	77	2.2	2.6	0.8	1.9	8	9	9	SW 8	SW 7	W 4
8	99.7	102.2	105.4	102.4	2.3	3.0	1.7	2.2	3.1	1.0	80	83	87	83	1.4	1.3	0.9	1.2	9	9	10	SW 5	WSW 4	W 7
9	103.3	97.3	84.2	94.9	0.3	3.3	3.5	2.6	4.0	-0.4	80	58	57	65	1.2	3.2	3.4	2.6	9	6	10	S 8	SSW 10	SSW 10
10	70.1	68.0	68.0	68.7	4.6	6.7	6.0	5.8	7.8	2.6	85	68	73	75	1.3	3.1	2.6	2.3	10	3	9	SSW 10	S 12	SSW 13
11	77.2	78.5	80.5	78.7	3.3	3.9	1.5	2.6	6.0	1.4	68	65	85	73	2.5	2.8	1.0	2.1	10	9	10 •	WSW 10	WSW 8	SW 8
12	88.7	91.5	95.4	91.9	0.5	0.4	-0.7	-0.1	1.6	-1.1	90	94	79	84	1.2	0.4	1.2	0.9	9	9 *	9	N 3	NW 4	NW 4
13	98.9	99.0	97.5	98.5	-3.5	-0.1	-2.1	-2.0	0.2	-6.0	88	71	85	81	0.6	1.3	0.7	1.0	9	5	6	W 2	W 1	E 5
14	107.2	111.8	114.5	111.2	-7.6	-2.1	-3.9	-4.4	-1.9	-7.6	84	70	87	80	0.5	1.5	0.6	0.9	6	3	9	W 3	NW 8	W 3
15	109.1	108.5	111.6	109.7	-0.5	1.7	-0.3	-0.2	1.8	-4.1	94	89	87	90	0.4	0.8	0.7	0.8	10	10 •	10	SW 5	NW 8	E 3
16	111.2	110.5	109.4	110.4	-5.6	-4.4	-6.3	-5.9	-0.8	-6.8	90	77	83	83	0.4	1.0	0.6	0.7	10	1	0	E 2	ESE 2	ESE 4
17	106.0	103.6	102.4	104.0	-0.1	-5.3	-3.5	-5.1	-3.4	-6.1	81	80	88	83	0.6	0.9	0.6	0.7	10 *	10 *	10 *	SE 4	SE 4	SE 5
18	99.9	95.8	97.8	97.8	0.4	3.0	8.1	4.9	8.1	-3.8	94	91	96	94	0.4	0.7	0.3	0.5	10	10 •	10 •	SE 2	S 5	SW 6
19	98.4	98.6	96.9	98.0	10.9	12.3	10.3	10.9	12.4	7.9	79	72	81	77	2.8	4.0	2.4	3.1	10	10	9	WSW 8	WSW 8	SW 7
20	103.0	105.3	103.9	104.1	3.7	4.8	1.3	2.8	10.7	1.0	78	76	91	82	1.0	2.0	0.6	1.5	4	8	10	W 7	SW 3	S 2
21	101.4	101.7	104.8	102.6	2.1	3.1	0.4	1.5	3.6	0.2	91	90	90	90	0.6	0.8	0.6	0.7	10 •	10	7	C 0	NW 2	NW 2
22	107.3	106.6	106.8	106.9	-0.6	1.6	-0.5	0.0	1.6	-1.1	92	76	94	87	0.4	1.7	0.4	0.8	10	9	9	W 3	S 2	SE 3
23	104.5	100.6	94.5	99.9	-2.2	0.8	-0.6	-0.6	0.9	-2.2	89	78	81	83	0.6	1.4	1.1	1.0	0	6	10	SE 5	SE 6	SE 7
24	87.0	85.0	81.2	84.4	-0.4	0.7	-0.1	0.0	1.1	-1.3	80	90	90	87	1.2	0.6	0.7	0.8	10	10 *	0	SE 7	SSE 3	SSE 3
25	75.3	73.2	73.1	73.9	-0.6	1.7	2.3	1.4	2.3	-2.4	95	87	80	87	0.3	0.9	1.4	0.9	9	9 •	10	SE 4	SSE 5	S 4
26	75.7	80.4	87.8	81.3	2.8	1.3	1.4	1.7	3.5	0.9	89	89	87	88	0.8	0.8	0.9	0.8	10	10 *	0	W 5	W 3	WSW 5
27	90.6	88.9	84.4	88.0	1.1	2.4	-0.2	0.8	2.5	-0.2	83	73	90	82	1.1	2.0	0.6	1.2	9	6	9	SW 5	SSW 4	S 1
28	83.3	88.4	93.8	88.5	0.2	-0.6	-1.6	-0.9	0.4	-1.6	94	79	92	88	0.4	1.2	0.4	0.7	10 *	10	0	N 4	W 8	SW 8
29	95.3	100.1	100.7	98.7	-0.6	0.2	0.8	0.3	1.4	-1.7	95	72	86	84	0.3	1.7	0.9	1.0	10 *	2	10 *	WSW 7	W 7	WSW 7
30	96.5	91.2	90.9	92.9	-1.8	0.7	1.1	0.3	1.1	-2.4	77	62	81	73	1.2	2.4	1.2	1.6	9	9	10 *	SSW 6	SW 7	SW 6
31	91.8	92.7	93.6	92.7	1.9	2.6	3.3	2.8	3.3	0.9	87	86	83	85	0.9	1.1	1.3	1.1	10	10	10	SW 5	SW 5	SW 5
M	93.1	93.3	93.3	93.2	0.4	2.1	1.1	1.2	3.3	-1.0	85	78	85	83	1.0	1.6	1.0	1.2	8.7	7.7	7.9	5.4	5.5	5.3

Poznań - Ławica $H_s = 86\ m$ $H_b = 92{,}1\ m$ $h_w =$ 12,5 m anemometr M-47; 15 m anemometr Chaux in-Arnoux **Listopad - Novembre 1965**

DNI	WIDZALNOŚĆ V	OPAD R	GRUBOŚĆ GO h	POGODA
1	6	5.8	.	● 3⁴⁵ 10¹⁵ ●● –10³⁵ ● 17⁴⁵ ● 15⁴⁰ 16¹⁵ ● 16⁴⁰ 17¹⁵ 17³⁰ 18⁰⁵ ● 21¹⁵–30 21⁵⁰ 22¹⁰. ≫ 23⁴⁵ 24. = 4²⁰ 14¹⁵ 15³⁰ 21¹⁰
2	8	1.4	.	▽ 3³⁰ 5⁰⁵ 21⁵⁰ 22⁴⁰. ≫ 0⁰⁰–30 por wiatru 14 m/sek 14⁵ 21⁰ 3⁵² 4³⁰ ≫ 5²⁰–30 7⁴⁰ 16³⁵ (por do 20 m/sek 10⁰² 15⁰⁵) ≫ 23¹⁰–35
3	8	.	.	≫ 3¹⁵ 6⁰⁵ por wiatru 13 m/sek 10²⁸ 12⁴⁰. ⌒ ⁰22–24. ⊕ 13³⁵ 15⁰⁵
4	6	.	.	= 2³⁰ 12⁴⁰ ∞ –18³⁰ = –19³⁰ 22³⁰ 24. ⌒ ⁰0⁰⁰ 2 ⌣ ⁰3–4 ⌣ ¹5–7 ⌣ ⁰8–9 ⌒ ¹8–22 ⌣ ⁰23–24
5	3	0.0	.	● 10³⁵ 13¹⁵. = 0⁰⁰ 5²⁰ = ¹–10⁴⁵ = ⁰–13⁰⁵ = –24. ⌣ ⁰0⁰⁰–3 ⌣ ¹4–5
6	6	0.1	.	● 10²⁰ 12¹⁰. 14⁰⁵–15 14³⁵ 21²⁰. = 0⁰⁰ 24
7	5	.	.	● ⁰11⁰ 4³⁵ 5²⁵ = 0⁰⁰ 18⁴⁰ = = –24. ⌒ ⁰19–24. ⊖ 21⁴⁰ 24
8	5	0.2	.	= = 0⁰⁰–45 = ⁰–0⁵⁰ = ²–2⁴⁰ = ²–9¹⁵ = ⁰–10²⁰ = 20⁴⁵ = ¹–21²⁰ = ⁰–22³⁰. ⌒ ⁰0⁰⁰ 2 ⌒ ¹3–12 18–22 ⌣ ⁰23–24
9	2	0.2	.	● ²2⁵⁴ 3¹³ 3⁴⁰ 4¹⁵ ● ⁰13³⁵ 15³⁰ 16¹⁵ 40 17⁴⁰ ● ¹18³⁰ ● ⁰10²⁰ 23⁴⁰ 24. = ¹0⁰⁰ 1³⁵ = –6⁴⁰ = ⁰–10¹⁰ = ¹–10³⁰ = ⁰–12⁵⁰ = ¹–13⁴⁰ = ²–14¹⁵ = ⁰–16²⁰ = ²–19⁴⁵ = ¹–20³⁵ = ²–21³⁵
10	5	.	.	● ⁰0⁰⁰ 4³⁰ 5⁴⁰ 6³⁰. = ²0⁰⁰ 24⁵ = ¹–4⁴⁰ = ⁰–5⁴⁵ = ¹–6³⁵ = ⁰–9⁴⁰ = –24 [9.XI: = ¹–23²⁰ = ²–24. ⌣ ⁰0⁰⁰–3
11	7	0.0	.	● ⁰10⁴⁵ 13²⁰. = 0⁰⁰ 11⁴⁰. ⊖ ⁰23⁰–6¹⁰
12	7	0.1	.	▽ ⁰12⁵⁰ 13⁰⁵ * ⁰22⁴⁰ 24. ⊖ 0³⁰ 3⁴⁰ 4³⁰ 6⁴⁰
13	6	0.1	.	* ⁰0⁰⁰ 1²⁰ 12²⁵ 12³⁰ 14⁰⁵ 14¹⁰ 16³⁰ 17⁴⁰ 23⁴⁰. ≫ 11²⁰ 14¹⁰. = 7²⁰ 16²⁵
14	6	1.3	.	* ⁰14⁰ 4²⁵ 20³⁵ 24. = 7¹⁰ 11⁴⁰ ∞ –18³⁰ = –24
15	6	0.3	1	* ⁰0⁰⁰ 14²⁰ 23⁴⁵ 24. = 0⁰⁰ 21³⁰. 23³⁰ 24
16	6	0.0	2	* ⁰0⁰⁰ 3¹⁰ 4⁴⁵ 5¹⁰ 6²⁰ 7³⁵. = 0⁰⁰ 3³⁰ 6³⁰ 24
17	5	0.1	2	△ 6⁴⁰ 7¹⁵ * ⁰–9³⁰ 10¹⁵ → 17³⁵ 21³⁵. = 0⁰⁰–45 = ⁰–21⁰ = –24
18	6	2.2	2	* ⁰20⁴⁰–24. = 0⁰⁰–6⁴⁵ ∞ –10³⁰ = –24
19	5	0.3	4	* ⁰0⁰⁰ 6³⁵ 7²⁰ 12³⁰–13⁴⁰ △ –15³⁰ * ⁰–19⁴⁵. = 0⁰⁰ 24
20	5	0.5	4	△ 5¹⁵ 16³⁵ * ¹–17¹⁰ * ⁰–19⁴⁰ * ¹–20¹⁵ * ⁰–20⁴⁵. = 0⁰⁰ 24
21	4	7.3	6	* ⁰0⁴⁰ 1³⁵ ⌒ ⁰5⁴⁵ 7³⁵ * ⁰–7⁴⁰ * ¹–10³⁰ △ –11⁴⁰ * ¹–13⁴⁵ * ⁰–15⁰⁵ 16³⁰–45 * ¹–19³⁵ * ⁰–21³⁰ 22⁴⁵. ⊕ ¹2⁴⁵ 3⁴⁰ ⊕ ⁰–8²⁰. ≫ 23³⁰ 3⁴⁰. = 0⁰⁰ 24. ⌒ 5⁴⁵–7³⁵
22	6	0.2	11	* ¹1³⁵ 2³⁰ * ⁰–3⁴⁵ * ¹–4³⁰ * ⁰6³⁵ … 55 –7⁴⁰ 9⁵⁰ 10⁰⁵ 13³⁰–14²⁵ 40 17⁵⁰ 20¹⁰. ⊕ ¹3⁵⁰ 7¹⁵ ⊕ ⁰–8²⁰. ≫ 3⁵⁰–4⁴⁰. 18⁰⁵–13. = 0⁰⁰ 22⁴⁵
23	6	.	12	= 7¹⁰–8⁴⁰ ∞ 12³⁰–14⁴⁰ = –24. ⌣ ²2–12 ⌣ ²20–24. ⊕ 14¹⁰–15²⁰
24	6	1.3	12	* ⁰21⁰–24. = 0⁰⁰ 11⁴⁰ ∞ –18³⁰ = –19⁴⁰ ∞ 22¹⁰ = –24. ⌣ ²1–9 ⌣ ⁰10–14
25	6	0.4	14	* ⁰0⁰⁰ 4³⁰ * ¹–6³⁰ * ⁰–7³⁵ △ 8⁴⁰–9¹⁵ * ⁰–9⁴⁰ * ¹–10¹⁰ * ⁰–10⁴⁰ ● ⁰12²⁰ 13⁴⁵. = 0⁰⁰ 24
26	6	0.5	9	* ⁰10⁵⁰–11¹⁰ * ⁰13⁴⁵ 14²⁰ * ¹–15⁰⁷ ● ⁰15³³ 16¹⁷. ≫ 12³⁵–14⁴⁰. = 0⁰⁰ 3³⁰ ∞ –14¹⁰ = –24
27	4	7.8	7	* ⁰11⁴⁰ 12⁰⁵–40 * ¹–13¹⁵ * ⁰–14¹⁰ △ –15⁰⁵ ● ⁰17¹⁵ 19¹⁰–35 ● ¹–20⁴⁰ ● ⁰–21⁴⁸ 23⁴⁵. = 0⁰⁰ 24. ⌣ ¹2–11
28	5	2.6	4	● ⁰3³⁵ 4³⁰. 6¹⁵ ● ⁰–8²⁰ * ⁰10⁰² 13²⁰ * ¹–14¹⁵ * ⁰–14⁴⁵ * ¹15⁴⁰ 16¹⁵ * ⁰16³⁵ 18²⁰ * ⁰20²⁰ 22³⁰ * ⁰–24. = 0⁰⁰ 5³⁰ 10²⁰–24
29	6	0.4	3	* ⁰0⁰⁰–10 * ⁰1¹⁵ 2³⁵ * ⁰–3²⁷ ● ⁰–4²⁰ 5³⁵ 6⁴⁰ 7⁰⁵…35 △ 7⁴⁰–50 ● ⁰9¹⁵–50. = 0⁰⁰ 10³⁰
30	7	0.4	3	* ⁰0²⁹–30 ● ⁰2⁴⁰–4³⁰ 5²⁸. ≫ 7⁵⁰–8¹⁰. = 0¹⁵ 1³⁰
31				
Σ	–	33.5	–	

Grudzień - Décembre

DNI	WIDZALNOŚĆ V	OPAD R	GRUBOŚĆ GO h	POGODA
1	6	8.7	1	* ⁰5⁵⁰ 6³⁰ * ¹–7⁴⁰ * ⁰–8⁴⁵ ● ⁰–21²⁰ * ⁰–24. ≫ 5⁵⁵…6⁴⁰ por wiatru 13 m/sek 6⁴⁰–7¹⁵ 8²⁰–10⁴⁰ 14²⁰–17⁴⁰. = 5⁴⁰–24
2	6	0.4	2	* ⁰0⁰⁰ 5²⁸ ● ⁰14²⁰–16⁰⁵. = 0⁰⁰ 24
3	6	0.6	3	* ¹1⁵⁰–4⁴⁵ ▽ ⁰10⁰²–08 ● ⁰10⁴⁹–11¹⁰ 11³⁵–50 ● ⁰12²⁰–16⁴⁰. = 0⁰⁰ 24
4	6	0.3	pł.	● ⁰20¹⁵ 21³⁵. = 0⁰⁰–24
5	6	3.2	pł.	● ⁰0³⁵–1⁴⁰ 17¹⁵ 18²⁵ 18³⁰ 21²⁰ ● ¹–21⁴⁵ ● ⁰–22³⁵ 23⁴⁰ = 0⁰⁰ 8⁰⁶ = ⁰8²⁰ = ¹–9²³ = –24. ≫ 19⁴⁵–24. ⌣ ⁰4–10
6	7	0.0	pł.	● ⁰11⁰³–08 11³³–45 14³⁰–37 18²⁰–35 22²⁰–30 ≫ 0⁰⁰ 2⁴⁰ 4²⁰ 16¹⁵ (por do 19 m/sek 9¹⁰ 10¹⁵ 10⁵⁰ 14⁴⁰) ≫ 18²⁰ 10¹⁵ (por 18 m/sek 18¹⁵–40) ≫ 22⁴⁰ 23¹⁰ = 0⁰⁰ 12⁵
7	7	1.1	pł.	● ¹20²⁰–30 ● ¹20³³ ● ¹20³⁷ ● ⁰–20⁴⁵ por wiatru 14 m/sek 20²⁹–33. = 23⁴⁵ 24. ⌣ ¹1–8. ⊖ 21¹⁰–40
8	6	1.3	.	● ⁰12⁰⁷…15 ● ¹13¹⁵–30 * ⁰–13³⁷ ● ⁰14²⁰–40 ● ¹15¹⁰–25 ● ⁰–15⁴⁰ 16³⁵–45. = 0⁰⁰–24. ⊖ 3⁴⁰–5¹⁵
9	6	6.8	.	● ⁰21³⁰ 24. ≫ 9⁵⁰ 24. = 0⁰⁰ 10³⁰ ∞ –17¹⁵. ⌣ ⁰1–2 ⌣ ²3–10. ⊖ ⁰4⁰⁰–7²⁰ ⊖ ¹19⁴⁰–21²⁰
10	7	0.2	.	● ⁰0⁰⁰–40 1³⁵–2³⁰ ● ¹2–3⁰⁵ ● ⁰–3⁴⁰ ● ⁰5³⁰ 6–6¹⁵ ● ⁰6⁵⁰ ● ⁰10²⁰–35 21¹⁵–50 23⁴⁰ 24. ⌒ S 6⁴⁵ SE 7¹⁰. ≫ 0⁰⁰ 22⁵⁰ (por do 25 m/sek 3¹⁰ 5⁰⁵ por do 19 m/sek 19¹⁰ 22²⁰). = 1⁴⁰ 6⁴⁰
11	8	0.4	.	▽ ⁰0⁰⁰–25 * ⁰17⁴⁵ 18³⁰ ● ⁰–18⁴⁰ ● ⁰19³⁰ ● ⁰19⁴⁵ 20¹⁵ ● ⁰–20³⁵ ● ⁰20⁴⁰ ● ⁰20⁵⁰ ● ⁰21⁵ ● ⁰–21³⁰ * ⁰21⁴⁰ * ¹22⁴⁵ = 21²⁰ 22⁴⁰ 23³⁰ 24. ≫ 0¹⁰ 8¹⁵ por wiatru do 14 m/sek 10⁰⁵ 15⁴⁵ 17⁴⁰ 19³⁵
12	6	0.8	.	● ⁰0⁰⁰…40 * ⁰7¹⁵–17 △ 7⁴⁰–8¹⁵ ● ⁰9⁴⁰ 9⁵⁰ * ⁰–9⁴⁰ * ⁰10¹⁵–50 * ¹11⁰³–50 * ⁰–12¹⁰ 12³⁵ 13⁰⁵. = 0⁰⁰ 7⁴⁵ 8³⁰–13³⁰
13	6	.	1	= 4¹⁰–12³⁰ ∞ –17⁴⁰ = –24 [11.XII: = 21²⁰ 22⁴⁰ 23³⁰–24
14	7	.	1	= 0⁰⁰ 10³⁰ 15⁴⁰ 24
15	5	0.5	1	△ 7⁴⁰–8³⁰ ● ⁰–9³⁵ ● ⁰10⁰²–05 * ⁰–10¹⁸ ● ⁰10⁴⁵ 11¹⁰ ● ⁰12⁰⁵ 13³⁵ ● ⁰–13²⁰ * ⁰–13⁴⁰ ● ⁰15³⁰ ● ⁰16³⁵ ● ⁰–16⁴⁰ = 0⁰⁰ 15³⁵ = ⁰–16⁵⁰ = –24
16	6	0.3	.	△ ⁰8²⁸–9⁰⁵. = 0⁰⁰ 24. ⌣ ⁰19–23
17	5	1.1	1	* ⁰5⁰² 10³⁰. 10⁴⁰ 13³⁰–19⁴⁵. 20²⁰ 23⁴⁰ = 0⁰⁰ 24. ⌣ ¹0–5 [18.XII: = ¹–10³⁵ = ⁰–20⁰⁵ = –24
18	4	12.6	2	● ⁰7⁴⁰ 8²⁰ ● ⁰9¹⁰ ● ⁰–9³⁰ ● ⁰10¹⁵ * ¹10³⁵ ● ⁰10⁴⁵ * ¹11³⁰ ● ⁰12⁰⁵ * ¹12⁴⁰ ● ¹13⁴⁰ ● ⁰13³⁰ * ¹–14⁴⁰ ● ⁰14⁴⁰. = 0⁰⁰ 15¹⁰ = ⁰–15⁴⁵ = ¹–15³⁵ = ²–16⁴⁵ = ¹–19⁴⁰
19	7	1.2	.	● ⁰0⁰⁰ 6³⁵ 15³⁵ 16⁴⁰. 17²⁰ 18²⁵ 19¹⁵ 21³⁵–50 22¹⁰–30 22⁴⁰ 23²⁰ 23³⁰–24. = 0⁰⁰ 7³⁰ 17¹⁰–24
20	7	0.8	.	● ⁰0⁰⁰…40. = 0⁰⁰–50 13²⁰–24. ⌣ ⁰20–23
21	5	1.6	.	● ⁰3⁴⁰ 10¹⁵ 10²²–50 = 0⁰⁰ 24. ⌒ ⁰20–22 ⌣ ⁰23–24
22	6	.	.	= 0⁰⁰ 24. ⌣ ⁰0⁰⁰–9. 19–24
23	6	.	.	= 0⁰⁰–24. ⌣ ⁰0⁰⁰–11. ⊕ ⁰11³⁰–12⁴⁰
24	5	2.5	.	* ⁰7⁰³–13¹⁰. = 0⁰⁰ 24
25	6	3.5	2	△ 7²⁰–9⁰² * ⁰–9⁰⁶ ● ⁰9¹⁵…35 10⁰⁸…20 10²⁵–35 ● ⁰–11⁰³ * ¹–11¹⁵ ● ⁰–11⁴⁰ 13²⁰ 17⁴⁵ 19³⁰ 21³⁵–24. = 0⁰⁰ 24
26	5	2.3	pł.	● ⁰0⁰⁰–30 0³⁵ 2³⁰–4³⁰ ●● ⁰–4⁴⁰ ● ⁰–5⁴⁵ 6¹⁵ ● ⁰11¹⁵ 12¹⁰ * ¹–13²⁰ ● ¹–13⁴⁰ * ⁰–15¹⁵ ● ⁰15³⁰–35 ● ⁰* –16²⁰. = 0⁰⁰–18¹⁵. ⌣ ⁰19–24
27	7	0.5	.	= 2¹⁵–7¹⁵. 8²⁰ 11⁴⁰. 15³⁰ 24. ⌣ ⁰0⁰⁰–2 ⌣ ¹3–11
28	6	1.0	1	* ⁰0⁴⁰–2²⁵ 3⁵⁰–11²⁰. = 0⁰⁰–24
29	8	0.5	2	* ⁰4⁴⁰ 6²⁰ * ¹–6⁴⁰ * ⁰–8⁰² * ¹20¹⁷–27 * ⁰–20⁴⁰ * ⁰20⁴⁵ 21⁵⁰. ≫ 7¹⁸ 10¹⁰. = 0⁰⁰ 9¹⁰ 16¹⁵–24
30	6	0.1	3	* ⁰15³⁵–16⁰⁵. 20⁴⁰ 21⁰⁵. ≫ 14²⁰–40. = 0⁰⁰–9³⁰ ∞ –14⁴⁵ = –24
31	6	.	2	● ⁰2⁴⁵ 3³⁰ 4⁴⁰. 5³⁰. = 0⁰⁰–24
Σ	–	52.3	–	

Warszawa – Bielany φ = 52°17' λ = 20°58' Styczeń – Janvier 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	92.6	92.6	92.6	92.6	3.0	3.1	2.1	2.6	4.4	1.8	86	81	85	84	1.1	1.4	1.0	1.2	10 •	10	5	S 6	SW 4	SSW 2
2	89.8	89.4	91.5	90.2	1.5	2.3	1.3	1.6	2.7	1.1	91	89	94	91	0.6	0.8	0.4	0.6	9	9	10	S 2	SW 1	C 0
3	94.2	96.1	98.4	96.2	-0.7	0.2	-0.7	-0.5	1.3	-1.1	100	94	100	98	0.0	0.4	0.0	0.1	10 ≡	9 ≡	10 ≡	C 0	C 0	NNW 1
4	101.8	105.3	108.3	105.1	-1.2	-0.6	-0.1	-0.5	0.4	-1.5	96	85	68	83	0.2	0.9	2.0	1.0	10	7	9	N 1	NNE 4	NW 2
5	102.8	99.3	102.7	101.6	-3.1	1.6	0.3	-0.2	1.9	-4.2	86	80	69	78	0.7	1.4	1.9	1.3	8	7	1	SW 5	W 7	W 5
6	105.0	106.2	106.4	105.9	-2.2	-0.9	-3.1	-2.3	0.5	-3.3	72	69	86	76	1.5	1.8	0.7	1.3	2	1	9	WNW 7	WNW 6	NW 5
7	109.0	109.3	107.8	108.7	-3.4	-1.7	-5.5	-4.0	-1.3	-5.5	88	82	87	86	0.6	1.0	0.5	0.7	2	9	0	NW 3	NW 4	WSW 3
8	100.4	94.8	87.8	94.3	-5.0	-0.1	1.9	-0.3	2.5	-7.0	71	94	93	86	1.2	0.4	0.5	0.7	9	10	10	S 2	SW 5	SW 6
9	89.3	91.1	91.8	90.7	3.6	3.7	1.3	2.5	4.3	1.1	90	82	94	89	0.8	1.3	0.4	0.9	10	10	10	W 5	W 2	WSW 2
10	91.4	95.2	109.1	98.6	0.0	-6.4	-11.2	-7.2	1.6	-11.6	98	86	79	88	0.1	0.5	0.5	0.4	10 *	10 △	3	C 0	NNE 6	NE 3
11	116.5	126.7	114.1	115.8	-13.6	-8.8	-9.9	-10.6	-8.2	-15.0	80	68	75	74	0.4	1.0	0.7	0.7	2	8	0	NNE 2	S 4	SE 5
12	109.8	108.9	107.1	108.6	-8.2	-3.8	-3.4	-4.7	-2.3	-10.3	78	71	79	76	0.7	1.3	1.0	1.0	9	9	0	SE 2	ESE 3	SSE 4
13	105.7	105.7	106.6	106.0	-6.3	-0.7	-0.8	-2.2	-0.1	-6.8	81	65	85	77	0.7	2.0	0.9	1.2	2	0	9	SSE 2	SSW 3	S 2
14	105.7	103.1	103.6	104.1	-2.4	-0.3	-0.6	-1.0	0.7	-2.7	89	73	77	80	0.5	1.6	1.3	1.1	2	2	8	S 3	SE 4	SSW 3
15	109.0	111.0	110.9	110.3	-0.2	2.4	-0.2	0.4	3.2	-0.8	90	72	84	82	0.6	2.1	1.0	1.2	7	3	3	SW 4	SW 2	SSE 2
16	106.4	106.4	105.8	106.2	-0.4	1.7	0.4	0.5	2.1	-1.8	88	78	92	86	0.7	1.5	0.5	0.9	10	10	10 *	SSE 2	SSW 2	SW 2
17	95.0	89.9	83.5	89.5	-0.9	2.3	3.7	2.2	4.2	-1.8	75	68	80	74	1.4	2.3	1.6	1.8	9	9	9	S 7	SSW 7	SSW 6
18	83.0	83.9	83.7	83.5	2.7	3.9	1.5	2.4	4.7	1.0	84	75	85	81	1.2	2.0	1.0	1.4	10	9	6	WSW 3	SSW 3	SW 3
19	83.0	84.1	86.8	84.6	0.5	3.1	-0.8	0.5	3.7	-1.5	82	69	92	81	1.1	2.3	0.5	1.3	9	2	0	SSW 2	C 0	C 0
20	88.0	85.9	81.0	85.0	-4.3	-2.2	-0.9	-2.1	-0.4	-4.7	94	91	93	93	0.3	0.5	0.4	0.4	10	10 *	10 *	NE 3	E 5	E 2
21	81.2	85.0	90.5	85.6	0.5	1.1	0.4	0.6	1.4	-1.1	98	90	98	95	0.1	0.6	0.1	0.3	10 *	10 *	10 •	ENE 3	ESE 3	C 0
22	94.6	97.2	101.4	97.7	0.1	0.7	-3.1	-1.4	1.0	-3.4	92	92	95	93	0.5	0.5	0.3	0.4	10 *	10 *	0 ≡	S 2	S 2	C 0
23	104.7	106.3	109.2	106.7	-5.9	-1.8	-0.5	-2.2	-0.4	-7.1	89	96	98	94	0.4	0.2	0.1	0.2	3	10 ≡	10 * ≡	C 0	NE 2	C 0
24	112.3	113.0	112.8	112.7	-1.1	-0.5	-0.3	-0.6	0.4	-1.5	95	92	100	96	0.3	0.5	0.0	0.3	10	10 *	10 *	NW 1	NNW 2	N 3
25	108.9	107.2	106.4	107.5	-1.0	-4.0	-3.0	-2.8	0.1	-4.2	99	91	99	96	0.1	0.4	0.0	0.2	10 •	10	10	E 2	E 2	SE 2
26	105.7	105.7	105.7	105.7	-1.9	-0.5	-2.1	-1.6	-0.1	-3.2	100	88	85	90	0.0	0.7	0.9	0.5	10	10	10	C 0	SE 3	SE 3
27	107.0	107.1	106.0	106.7	-3.4	-2.6	-1.2	-2.1	-1.2	-4.7	88	93	89	90	0.6	0.3	0.6	0.5	10	10	10	SE 5	SE 4	SE 7
28	105.8	106.1	104.8	105.6	-1.5	-0.3	-0.6	-0.8	0.0	-2.2	86	74	81	80	0.8	1.6	1.1	1.2	10	9	10	SE 6	SE 6	SE 6
29	101.5	100.2	98.9	100.2	0.7	1.7	1.4	1.3	2.4	-2.6	83	92	92	89	1.1	0.5	0.6	0.7	10	10 •	6	SE 5	SE 5	S 2
30	99.4	98.4	95.2	97.7	-0.1	0.9	2.2	1.3	2.5	-0.5	94	100	96	97	0.4	0.0	0.3	0.2	10	10 ≡	10	C 0	C 0	C 0
31	101.1	104.0	103.2	102.8	-1.6	-0.9	-2.8	-2.0	2.6	-3.4	94	85	91	90	0.3	0.8	0.5	0.5	9	9	10	C 0	C 0	C 0
M	100.0	100.2	100.4	100.2	-1.8	-0.2	-1.1	-1.0	1.1	-3.5	88	83	88	86	0.6	1.1	0.7	0.8	8.1	8.1	7.0	2.8	3.3	2.6

Luty – Février

1	102.5	102.8	105.1	103.5	-3.6	-2.4	-2.6	-2.8	-1.5	-5.2	94	85	77	85	0.3	0.8	1.2	0.8	10	10 *	7	W 2	W 3	W 3
2	108.2	110.0	114.7	111.0	-5.4	-2.8	-4.5	-4.3	-1.5	-5.5	80	77	79	79	0.8	1.1	0.9	0.9	7	3	1	WNW 5	WNW 7	WNW 3
3	113.2	109.6	109.4	110.7	-8.8	-2.0	-1.8	-3.6	-1.4	-9.6	83	89	86	86	0.5	0.6	0.8	0.6	9	10 *	9	WSW 3	W 5	WNW 3
4	109.5	107.6	112.6	109.9	-2.3	0.3	-8.3	-4.6	0.6	-8.4	93	92	80	88	0.4	0.5	0.6	0.5	10 *	10 *	9	W 3	NW 4	NNE 4
5	110.3	110.2	114.3	111.6	-12.2	-11.1	-17.8	-14.7	-8.2	-18.5	85	72	79	79	0.4	0.7	0.3	0.5	10 *	0	0	C 0	NNW 2	N 2
6	115.9	114.7	111.6	114.1	-20.1	-12.8	-11.2	-13.8	-10.6	-20.7	89	61	79	76	0.1	0.9	0.5	0.5	1	3	9	C 0	C 0	WSW 2
7	110.5	108.4	95.0	104.6	-16.1	-6.9	-5.3	-8.4	-3.1	-16.6	86	53	85	75	0.2	1.7	0.6	0.8	0	0	10 *	C 0	SW 3	SSW 6
8	83.7	86.0	94.1	87.9	-4.0	-3.9	-4.9	-4.4	-0.6	-5.8	87	78	90	85	0.6	1.0	0.4	0.7	9	10	10 *	NW 7	NNW 9	N 5
9	103.0	107.8	110.3	107.0	-8.4	-9.1	-12.4	-10.6	-4.8	-12.6	80	64	81	75	0.6	1.1	0.4	0.7	9	2	2	NNW 4	N 6	NW 2
10	103.9	96.1	97.2	99.1	-7.1	-5.1	-1.1	-3.6	-0.8	-13.7	82	90	89	87	0.6	0.4	0.6	0.5	10	10 *	7	W 6	W 10	NW 2
11	101.9	105.0	108.5	105.1	-6.7	-1.2	-5.6	-4.8	0.2	-7.1	83	70	87	80	0.6	1.7	0.5	0.9	3	4	0	WNW 4	NW 4	WNW 3
12	109.1	107.3	105.1	107.2	-3.7	-0.3	1.2	-0.4	1.6	-7.0	97	92	98	96	0.2	0.5	0.2	0.3	10 ≡	10	10	WSW 2	WSW 5	SW 3
13	98.1	92.8	86.6	92.5	1.0	1.5	1.3	1.3	2.6	-0.1	79	89	92	87	1.4	0.8	0.5	0.9	10	10 •	10 *	SW 5	SW 4	SW 5
14	81.2	79.3	89.3	83.3	1.9	0.5	0.8	1.0	2.6	-0.3	71	98	86	85	2.0	0.1	0.9	1.0	5	10 *	9	SW 8	SW 9	WNW 4
15	95.0	97.9	99.3	97.5	-1.2	-0.3	-3.4	-2.1	0.8	-3.4	91	86	83	87	0.5	0.9	0.8	0.7	10 *	10	7	W 3	W 3	C 0
16	101.7	104.1	106.2	104.0	-4.4	-3.3	-5.8	-4.8	-2.2	-6.3	86	79	97	87	0.6	1.0	0.1	0.6	10	9	10	C 0	C 0	N 4
17	103.2	103.4	107.3	104.6	-4.7	-1.5	-0.7	-1.9	0.5	-7.2	93	94	81	89	0.3	0.3	1.1	0.6	10 *	10	10	NNE 4	NE 5	NE 5
18	109.3	110.3	111.2	110.3	-5.0	-4.9	-5.6	-5.3	-0.3	-6.0	93	78	79	83	0.3	0.9	0.8	0.7	10	10	10	NE 5	NE 5	NNE 5
19	112.1	113.2	115.5	113.6	-6.8	-5.2	-4.9	-5.4	-3.6	-7.1	88	75	73	79	0.4	1.0	1.1	0.8	10	9	10	NE 5	NNE 6	NE 3
20	118.7	120.9	122.0	120.5	-6.2	-2.7	-5.8	-5.1	-1.8	-6.8	94	75	89	86	0.2	1.2	0.4	0.6	10	10	3	NE 5	E 5	C 0
21	117.0	113.5	106.7	112.4	-4.5	-2.6	-4.7	-4.1	-1.7	-7.0	93	77	88	86	0.3	1.2	0.5	0.7	10	10	10 *	C 0	W 3	W 5
22	98.9	102.1	103.3	101.4	-3.1	-2.8	-7.6	-5.3	-2.4	-7.7	95	54	67	72	0.3	2.3	1.1	1.2	10 *	1	0	WNW 3	N 4	WSW 2
23	103.0	102.1	104.2	103.1	-10.9	-3.0	-6.8	-6.9	-2.1	-11.7	90	70	72	77	0.3	1.5	1.0	0.9	9	6	8	WSW 3	W 4	N 1
24	106.1	104.1	96.9	102.4	-14.5	-10.5	-8.0	-10.2	-6.2	-17.4	83	87	72	81	0.3	0.4	0.9	0.5	1	1	4	W 1	WSW 3	SW 5
25	90.7	92.8	93.9	92.5	-4.3	-3.9	-7.8	-6.0	-3.4	-8.5	68	50	56	58	1.4	2.3	1.5	1.7	7	10	0	NW 5	WNW 3	W 4
26	97.1	97.7	91.2	95.9	-11.8	-4.7	-4.9	-6.6	-4.3	-11.9	78	74	88	80	0.5	1.1	0.5	0.7	1	8	10 *	WSW 4	SW 4	SSW 4
27	82.2	79.6	84.9	82.2	-3.9	-1.4	-6.3	-4.5	-1.2	-6.3	82	84	86	84	0.8	0.9	0.5	0.7	10 *	10 *	8 *	SW 4	SSW 5	SW 5
28	94.0	98.7	102.2	98.3	-8.9	-4.6	-8.9	-7.8	-3.7	-9.9	70	69	67	69	0.9	1.3	1.0	1.1	7	3	2	WNW 5	WNW 5	SW 2
29																								
30																								
31																								
M	102.9	102.8	103.5	103.1	-6.6	-3.8	-5.5	-5.4	-2.1	-8.9	85	77	82	81	0.6	1.0	0.7	0.8	7.8	7.3	6.6	3.4	4.5	3.3

Warszawa - Bielany $H_s = 98\,m$ $H_b = 99{,}5\,m$ $h_w = 16\,m$ Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GŁ h	POGODA
1	6	1.0	4	$\bullet^{0}$ na – a; = nc – np
2	5	.	pż.	$\bullet$ na; = na – p
3	3	.	pż.	$\equiv^{1-0}$ na – a $\equiv^{0}$ a – p $\equiv^{2}$ p – np
4	6	.	pż.	= np
5	7	0.6	pż.	$*^{0}$ a, $\dagger^{2}$ a, $\sqcup^{1}$ n – a
6	7	.	1	
7	7	0.0	1	$*^{0}$ a – p; $\sqcup^{0}$ n – a
8	6	2.9	1	$\bullet^{0}$ a, p – n; = a – p
9	7	2.7	pż.	
10	6	0.0	1	$\bullet^{0}$ n – 6^{02} $*^{0}$ – 12^{40} $*^{1}$ – p
11	6	.	2	= a – p; $\sqcup^{0}$ na
12	5	.	2	= a – p
13	6	.	2	= a – p
14	6	.	1	= na – p
15	6	.	1	= a – p
16	6	0.0	1	$*^{0}$ a z prz., p z prz.; = a – p
17	8	1.5	1	$*^{1}$ 7^{40} – 10^{25}; = p
18	6	.	.	$\bullet^{0}$ na; = na – np; $\sqcup^{0}$ p – np
19	6	.	.	= na – np; $\sqcup^{0}$ na – a, p – np
20	4	4.5	.	$*^{0}$ a – np; = na – a, p – n; $\sqcup^{2}$ na – a
21	5	1.5	4	$\bullet^{0}$ na – a $\bullet^{0}$ p – np; = na – p
22	6	0.6	3	$*^{0}$ na – a, p; = na – p $\equiv^{0-2}$ p – np; $\sqcup^{0}$ p – np
23	3	1.3	3	$*$ p – np; = na – a $\equiv^{0}$ a – p, p – np; $\sqcup^{2}$ na – a $\vee^{0}$ a – p
24	4	2.8	4	$*^{0-1}$ na, a – np; = na – p; $\vee^{0}$ na – p
25	5	0.0	6	$\bullet$ n – a, p – n; = na – np
26	6	.	4	= na – np
27	6	1.2	4	$*^{0-1}$ 12^{45} – 20^{15} $*^{0}$ 20^{40} – n; $\dagger$ p; = a – p
28	6	.	5	= p – n
29	6	0.3	5	$\bullet$ 6^{38} – p
30	3	2.0	4	$\bullet^{0}$ 8^{18} 6^{45} – p $\bullet^{0}$ p; = n – a $\equiv$ a – p
31	6	.	4	= a – p
Σ	-	22.9	-	

Luty - Février

1	6	0.0	1	$*^{0}$ 8^{25} ... 14^{20}; = na – a; $\sqcup^{0}$ na – a
2	8	0.0	2	$*^{0}$ 8^{40} ... 10^{35}, 14^{20} – 15^{10}; $\sqcup^{0}$ np
3	6	1.2	3	$*^{0}$ 8^{45} 16^{20}; $\sqcup^{0}$ na – p
4	6	0.9	5	$*$ na ... 13^{40}; = na – a
5	7	0.0	5	$*^{0}$ n – a
6	6	.	5	= $\sqcup$ n – a
7	5	2.6	5	$*^{1}$ p – np; $\dagger^{0}$ p – np; = na – p; $\sqcup^{1}$ na – a
8	8	0.3	10	$*^{2}$ na $*^{0}$ 14^{40} – np; $\dagger$ na – np; $\gg$ na
9	6	0.2	13	$*^{0}$ 7^{30} – 10^{00} $*^{0}$ 10^{20} – 11^{30}; = a – p, $\sqcup$ p – np
10	4	1.2	14	$*^{0-2}$ 9^{10} – 16^{10}, 18^{15} – 19^{40}; $\dagger$ a – p; $\gg$ a – p; = na – a, p – np
11	8	.	14	= p – np; $\sqcup^{0}$ na – a $\sqcup^{0-1}$ p – np
12	4	0.2	13	$*^{0}$ p; $\equiv^{0}$ na – a = a – np; $\sqcup^{2}$ na $\vee^{0}$ na
13	6	2.7	12	$\bullet^{0}$ $*$ 8^{50} – 11^{10} 11^{30} – np; = na – np
14	4	2.2	5	$\bullet$ na $\bullet^{0-2}$ 11^{10} – 14^{10} $*^{0}$ p
15	7	0.7	8	$*^{0}$ 5^{50} – 7^{20}, 11^{50} – 12^{10}, 15^{52} – 16^{00}, 16^{10-14} $\triangle$ – 16^{20} $\bullet^{0}$ $*$ – p; = n – a, p – np; $\backsim$ p – np
16	6	0.7	8	= n – p
17	6	1.2	9	$*^{0}$ n – p; = n – p
18	6	.	8	= na – np
19	7	.	8	= n – a
20	6	.	8	$\dagger$ a, = na – np; $\sqcup^{0}$ p – np
21	6	2.4	8	$*^{0}$ 21^{15} – n; $\dagger$ 21^{13-30}; = n – a
22	8	0.1	12	$*^{1}$ na – 8^{10}; = na
23	8	1.7	12	$*^{0}$ 9^{10} – 11^{15}, 13^{10} – 17^{20}; = na – a; $\sqcup^{0}$ na – a
24	6	0.2	14	= a – p; $\sqcup^{0}$ na
25	8	.	17	$*^{0}$ na; $\dagger$ na
26	7	1.5	14	$*^{0}$ 15^{05} p – np; = a – np; $\sqcup^{0}$ na
27	5	2.1	18	$*^{0}$ na – np, $\dagger$ a – p $\dagger$ np; = na – p
28	9	.	20	$\dagger$ na, $\sqcup^{0}$ np
29				
30				
31				
Σ	-	22.1	-	

Warszawa – Bielany φ = 52°17' λ = 20°58' Marzec – Mars 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N_w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_v I	II	III
1	99.9	96.9	93.2	96.7	-9.7	-7.1	-2.3	-4.1	-0.2	-10.2	56	58	85	66	1.3	2.2	0.8	1.4	9	9	10	SE 5	SE 2	SE 4
2	86.7	84.3	81.8	84.3	-2.5	2.1	1.5	0.6	2.3	-2.9	95	85	94	91	0.3	1.0	0.4	0.6	10 x	10	10	ESE 2	ESE 1	ESE 2
3	77.6	75.2	82.7	78.7	1.2	1.1	-1.5	-0.2	3.4	-1.7	96	92	68	85	0.3	0.5	1.8	0.9	10 •	10 x	0	E 1	WSW 5	SE 6
4	83.5	87.2	90.4	87.0	-3.6	-3.6	-4.6	-4.1	-1.4	-4.6	76	80	91	82	1.1	0.9	0.4	0.8	8	10 x	10 x	SW 8	SW 6	WSW 7
5	92.4	95.3	101.2	96.3	-4.7	-2.4	-3.1	-3.3	-1.8	-5.0	96	82	88	89	0.2	0.9	0.6	0.6	10 x	10 x	10	WSW 6	WSW 4	WNW 2
6	106.3	108.3	111.6	108.7	-3.9	-1.9	-3.9	-3.4	-1.7	-4.8	94	77	78	83	0.3	1.2	1.0	0.8	10	9	10	C 0	E 4	ENE 4
7	115.5	116.6	117.9	116.7	-10.8	-6.6	-10.0	-9.4	-3.8	-12.5	83	72	87	81	0.4	1.0	0.4	0.6	10	6	0	NNE 1	NNE 3	C 0
8	117.1	115.1	114.3	115.5	-16.1	-3.5	-6.5	-9.2	-2.6	-16.5	95	52	80	76	0.1	2.3	0.6	1.0	2	2	0	C 0	ESE 2	C 0
9	113.2	113.0	112.1	112.8	-11.0	-4.6	-3.1	-5.4	-2.8	-12.7	90	67	70	76	0.3	1.4	1.4	1.0	2	1	10 x	C 0	WSW 4	WNW 3
10	115.3	117.5	118.8	117.2	-4.5	0.6	-4.3	-3.1	1.2	-5.1	91	58	89	79	0.4	2.7	0.5	1.2	3	1	0	C 0	NW 4	WNW 2
11	119.2	120.0	118.9	119.4	-5.3	0.1	0.2	-1.2	1.5	-7.4	87	81	92	87	0.5	1.2	0.5	0.7	10	10	7	W 1	W 2	W 1
12	117.9	116.4	115.3	116.5	-7.5	4.5	1.7	0.1	5.9	-8.4	96	53	63	71	0.1	4.0	2.5	2.2	2	0	0	W 1	WSW 2	W 1
13	115.4	115.1	114.7	115.1	-5.3	5.3	1.1	0.6	6.6	-6.2	89	54	68	70	0.4	4.1	2.1	2.2	1	0	0	C 0	SW 2	S 1
14	114.2	113.1	111.7	113.0	-4.8	7.5	2.1	1.7	7.7	-5.0	93	45	75	71	0.3	5.7	1.8	2.6	0	0	0	C 0	S 2	C 0
15	110.1	110.1	108.9	109.7	-0.8	8.1	6.2	4.9	8.5	-1.1	95	51	67	71	0.3	5.2	3.1	2.9	0	2	3	S 2	S 2	S 2
16	106.1	103.6	102.5	104.1	3.5	8.7	5.8	6.0	9.6	3.3	85	64	74	74	1.2	4.0	2.4	2.5	10	8	9	SSW 1	SSW 3	SSW 3
17	103.2	103.0	100.1	102.1	2.8	4.8	3.4	3.6	6.2	2.7	100	100	97	99	0.0	0.0	0.3	0.1	10 ≡	10	10 ≡	WSW 3	SW 2	C 0
18	97.5	96.8	95.0	96.4	1.5	3.7	1.1	1.8	6.8	0.7	98	95	100	98	0.1	0.4	0.0	0.2	10 ≡	0	8	SW 2	ESE 5	ESE 1
19	93.6	94.9	98.9	95.8	2.3	11.1	5.2	6.0	12.6	0.9	89	59	89	79	0.8	5.4	0.9	2.4	8	8	7	SE 4	SSW 3	SW 2
20	104.0	105.4	104.5	104.6	1.9	6.1	2.6	3.3	7.2	1.7	89	49	74	71	0.8	4.8	2.0	2.5	7	6	0	NW 3	SW 3	W 1
21	111.3	108.7	91.2	103.7	0.3	3.0	5.3	3.5	5.3	0.3	96	88	91	92	0.2	0.9	0.8	0.6	10	10 •	9	NW 2	ESE 3	SSW 3
22	97.9	101.7	104.2	101.3	0.0	3.4	1.2	1.4	6.1	-0.7	76	52	68	65	1.5	3.8	2.2	2.5	9	1	0	NW 3	W 3	W 2
23	104.5	102.4	97.7	101.5	-1.8	5.8	2.0	2.0	6.4	-2.3	88	34	59	60	0.7	6.1	3.0	3.3	0	1	0	C 0	SE 6	SE 6
24	92.7	92.2	92.6	92.5	1.9	5.3	6.6	5.1	8.2	0.6	84	72	78	78	1.2	2.5	2.1	1.9	10 •	10	6	SE 3	SE 3	SE 2
25	93.0	96.7	101.5	97.1	6.0	4.7	2.5	3.9	7.9	2.5	92	87	82	87	0.8	1.1	1.3	1.1	10	10	0	SW 3	WSW 5	W 2
26	103.9	103.5	105.2	104.2	2.0	4.7	3.6	3.5	6.1	1.4	84	82	86	84	1.2	1.5	1.1	1.3	10	10	10	C 0	SW 1	SE 2
27	112.1	116.2	119.8	116.0	0.7	6.5	4.6	4.1	8.5	0.2	98	71	68	79	0.1	2.9	2.7	1.9	10 ≡	8	7	ENE 2	NE 3	NNE 1
28	121.0	120.2	118.8	120.0	2.2	8.9	7.5	6.5	10.4	2.1	87	53	63	68	1.0	5.4	3.9	3.4	9	9	10	C 0	SSW 2	SSW 3
29	116.1	116.5	114.3	115.6	5.4	7.9	7.6	7.1	10.1	5.2	95	90	94	93	0.5	1.0	0.6	0.7	10	10	5	S 2	NW 1	W 2
30	106.7	104.7	111.3	107.6	5.3	11.6	2.2	5.3	13.9	2.1	94	59	68	74	0.6	5.6	2.3	2.8	0	10	0	SW 3	WNW 7	NW 4
31	110.1	109.7	111.3	110.4	1.1	7.4	1.7	3.0	8.6	-0.7	79	44	78	67	1.4	5.8	1.5	2.9	4	9	2	WNW 4	NNW 4	WNW 4
M	105.1	105.2	105.2	105.2	-1.7	3.5	1.1	1.0	5.1	-2.7	89	68	79	79	0.6	2.8	1.5	1.6	6.9	6.5	4.9	2.0	3.2	2.4

Kwiecień – Avril

1	115.8	117.9	115.5	116.4	-2.0	2.8	2.7	1.6	5.1	-2.0	81	45	55	60	1.0	4.1	3.3	2.8	4	3	9	NNW 3	N 2	NNW 2
2	108.9	110.4	112.0	110.4	2.2	8.7	3.7	4.6	10.3	1.6	77	40	59	59	1.7	6.7	3.3	3.9	5	4	0	W 3	NW 5	N 2
3	109.8	105.5	103.3	106.2	0.3	8.4	3.8	4.1	10.3	-1.9	65	45	72	61	2.2	6.1	2.2	3.5	9	6	9	C 0	SW 2	NW 4
4	100.8	99.9	98.7	99.8	3.6	11.7	8.9	8.3	12.6	2.6	90	41	52	61	0.8	8.0	5.5	4.8	9	10	10	WSW 3	NW 5	C 0
5	105.6	106.7	108.2	106.2	0.7	8.8	7.1	5.9	10.7	0.6	100	68	70	79	0.0	3.6	3.1	2.2	10 ≡	9	4	N 2	NE 2	NE 1
6	108.9	107.8	105.3	107.3	3.0	10.4	5.9	6.3	12.2	1.6	88	44	61	64	0.9	7.0	3.6	3.8	0	7	0	SE 1	E 1	SE 5
7	99.8	99.7	101.2	100.2	2.0	12.1	7.2	7.1	12.5	1.3	85	56	74	72	1.1	6.2	2.7	3.3	9	9	9	SE 4	W 4	NW 3
8	101.1	101.2	102.6	101.6	3.6	9.7	5.7	5.2	10.6	3.1	90	59	82	77	0.8	4.9	1.5	2.4	4	8	0	W 2	NNW 3	NE 4
9	103.8	105.0	105.1	104.6	2.9	4.8	2.6	3.2	6.6	1.4	91	76	55	74	0.6	2.0	3.4	2.0	10	10	8	ENE 5	E 10	E 8
10	105.6	106.5	105.8	106.0	0.5	4.4	3.7	3.1	6.8	0.2	61	54	59	58	2.4	3.9	3.3	3.2	10	8	8	E 7	E 6	E 5
11	105.0	103.7	103.5	104.1	0.4	6.6	3.6	3.6	7.7	-0.7	65	53	67	62	2.2	4.6	2.6	3.1	4	4	10	E 6	ESE 10	SE 7
12	104.2	104.1	104.0	104.1	1.2	7.2	7.4	5.8	8.1	0.6	68	58	57	61	2.2	4.3	4.5	3.7	9	9	10	ESE 8	ESE 9	ESE 8
13	103.0	102.4	103.2	102.9	1.6	10.1	6.7	6.3	10.9	1.2	76	60	51	62	1.7	5.0	4.8	3.8	10	8	2	SSE 5	SE 4	SE 4
14	105.6	107.3	109.7	107.5	1.1	6.5	2.9	3.4	7.4	0.1	74	51	79	68	1.7	4.8	1.6	2.7	8	6	9	SE 6	E 4	C 0
15	109.8	109.4	106.4	108.5	2.7	4.7	4.7	4.2	6.7	2.1	86	71	82	80	1.0	2.4	1.5	1.6	10	9	9 •	E 1	ESE 1	C 0
16	102.9	99.9	99.2	100.7	3.3	11.0	9.8	8.5	13.9	2.0	90	50	79	73	0.7	6.6	2.5	3.3	6	2	10	ESE 3	ESE 5	SE 1
17	99.9	100.2	97.7	99.3	6.4	7.7	7.1	7.1	10.9	5.0	84	96	87	89	1.6	0.5	1.3	1.1	9	10 •	9	S 3	WSW 4	SSW 1
18	88.8	88.2	90.5	89.2	7.9	9.3	8.7	8.6	11.0	6.4	83	78	77	79	1.7	2.6	2.5	2.3	10	10 •	6	SSE 6	SSE 6	C 0
19	91.8	91.8	92.0	91.9	6.0	9.8	9.8	8.8	11.7	5.4	97	70	62	76	0.3	3.6	4.6	2.8	10 •	10	0	E 2	SE 3	SE 8
20	92.8	93.1	95.0	95.6	7.5	12.4	10.3	10.1	13.6	5.5	84	56	67	69	1.7	6.4	4.1	4.1	6	9	10	E 6	E 10	E 6
21	95.7	92.4	91.5	92.5	7.4	9.5	8.6	8.5	10.3	6.5	88	83	95	88	1.2	2.1	0.8	1.4	10	10	10	NE 4	E 4	E 5
22	88.1	87.4	85.7	87.1	9.1	7.1	5.6	6.8	9.5	5.5	74	74	94	81	3.1	2.6	0.6	2.1	8	10	10 •	NE 7	NE 10	NE 8
23	84.8	83.7	83.3	83.9	6.2	6.5	4.9	5.6	6.9	4.9	94	91	92	92	0.6	0.9	0.7	0.7	10	10	10	NE 6	N 3	W 3
24	84.9	87.7	91.1	87.9	4.3	6.1	5.6	5.4	7.5	3.1	93	88	91	91	0.5	1.1	0.9	0.8	10 •	10 •	10	WSW 3	SW 5	SW 3
25	95.2	97.0	98.1	96.8	6.1	10.7	7.9	8.2	12.4	5.0	89	70	86	82	1.0	3.9	1.4	2.1	10	9	10 •	SW 3	C 0	SW 3
26	98.6	98.4	98.2	98.4	6.0	6.1	5.6	5.8	10.1	4.2	94	94	88	92	0.6	0.6	1.1	0.8	9	10 •	2	SSW 2	W 3	C 0
27	94.4	92.9	94.1	93.8	4.3	9.0	7.3	7.0	9.9	2.3	97	90	90	92	0.3	1.1	1.0	0.8	10 •	10	0	ESE 1	C 0	SE 1
28	92.7	92.5	94.7	93.3	8.9	14.2	9.1	10.3	14.5	5.0	89	58	81	76	1.2	6.8	2.2	3.4	6	9	10 •	E 5	E 10	ESE 8
29	97.5	97.9	100.2	98.5	6.7	13.5	9.7	9.9	15.1	6.4	81	44	73	66	1.9	8.7	3.2	4.6	7	6	0	SSW 3	ENE 2	NE 1
30	102.1	102.2	102.6	102.3	7.9	14.1	11.0	11.0	15.1	7.4	87	39	46	57	1.3	9.8	7.0	6.0	9 •	8	8	NNE 1	N 8	NW 2
31																								
M	99.8	99.8	99.9	99.8	4.1	8.8	6.5	6.5	10.4	2.9	84	63	73	73	1.3	4.4	2.7	2.8	8.0	8.1	6.7	3.7	4.7	3.4

Warszawa - Bielany $H_s = 98\,m$ $H_b = 99{,}5\,m$ $h_w = 16\,m$ Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ LODU h	POGODA
1	7	1.5	19	$*^{0-1}$ p; = p − n; ⊕ a − p
2	6	3.0	20	$*^{1}$ na − a $\bullet^{0}$ np; = a − np
3	5	2.6	16	$\bullet^{0}$ na .. a ∇^{0-2} 10^{16} − 16^{20}; = na − a
4	6	1.9	15	$*^{0}$ a − p $*^{1}$ p − np; $+^{0}$ a $+^{1}$ p − np
5	5	0.2	15	$*^{0}$ na − p; $+^{0}$ na − a; = na − np
6	6	0.0	17	$*^{0}$ a; = na − np
7	7	•	17	= na − a; ⊔^{0} p − np
8	8	•	15	= na − a, p − np; ⊔^{1} na − a ⊔^{0} p − np
9	6	0.0	10	= na − a ∞ a − p; ⊔^{1} na − a
10	8	•	9	$*^{0}$ na
11	6	•	8	
12	6	•	7	$\equiv^{0-2}$ 6^{05-30} = − a ∞ a − np; ⊔^{2} na − a
13	5	•	6	= na − a ∞ a − p = p − np; ⊔^{0} na − a, p − np
14	5	•	5	= na − a ∞ a − p = p − np; ⊔^{2} na − a ⊔^{0} p − np
15	6	•	4	= na − np; ⊔^{0} na
16	6	0.5	2	$\bullet^{0}$ 20^{45} − np; = na − np
17	5	0.0	pł.	$\bullet^{0}$ na − 8^{10}; $\equiv^{0}$ na − 10^{10} = − 20^{10} $\equiv^{0}$ − np
18	4	•	pł.	$\equiv^{0}$ na − 8^{20} = − 17^{00} $\equiv^{0}$ − 17^{30} $\equiv^{1}$ − 19^{35} = − np
19	6	•	•	= na − np; ⊔^{0} na
20	8	•	•	= na − a
21	6	1.5	•	$\bullet^{0}$ 11^{10} − 13^{20}, 15^{15} p; = a − np
22	8	•	•	⌓^{0} p − np
23	8	0.0	•	
24	6	0.5	•	$\bullet^{0}$ 6^{10} − a
25	6	0.5	•	$\bullet^{0}$ na, a • 10^{47}
26	6	0.8	•	• n $*^{0}$ △ 6^{10-15} $*^{0}$ − 6^{20} $\bullet^{0}$ 16^{10} − 17^{40}, p; = na − np
27	6	•	•	≡ n − a = a − p
28	7	0.0	•	= na − a, ⊔^{0} na
29	6	0.2	•	• 5^{50} − a; = na − np
30	7	•	•	= ⌓^{1} n − a
31	9	0.4	•	$*^{0}$ ∇ p
Σ	-	13.6	-	

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1	9	•	•	
2	9	•	•	
3	7	•	•	= ⊔^{2} n − a
4	7	•	•	= n − a = ⌓^{0} p − np
5	6	•	•	≡ n − a = a − p
6	7	•	•	= na − a; ⌓^{1} na
7	6	0.9	•	$\bullet^{0}$ 12^{45} − 15^{25}; = na − a; ⌓^{0} na
8	7	•	•	= na − a; ⌓^{0} na
9	7	•	•	≫ a − p; = a
10	7	•	•	
11	7	•	•	≫ a − p
12	7	•	•	
13	6	0.0	•	∇^{0} a; ∞ na − p
14	6	•	•	∞ na − p = p − np
15	5	0.0	•	∇^{0} 15^{10-28} 20^{32-37}; = na − a ∞ a − p = p − np
16	7	0.2	•	∇^{0} 18^{15-40}; = na − a
17	5	0.5	•	$\bullet^{0}$ a $\bullet^{0}$ a − p $\bullet^{0}$ p; = na − p
18	5	0.4	•	$\bullet^{0}$ a − p ∇^{0} p; = na − p
19	6	1.4	•	$\bullet^{0}$ na − a, p; = na − p
20	8	•	•	≫ a − p
21	7	5.2	•	$\bullet^{0-1}$ 9^{15} − 10^{40} 17^{40} − 18^{45}, 19^{30} − np
22	7	1.6	•	$\bullet^{0}$ p − 21^{20}; ≫ a − p
23	6	9.6	•	• na, a ... n; = n − p
24	7	2.0	•	$\bullet^{0}$ n − p
25	7	2.5	•	$\bullet^{0}$ a ∇^{0} p; K^{0} WSW 17^{10-30} ENE; = a
26	6	0.4	•	$\bullet^{0}$ na, a − p
27	6	5.3	•	$\bullet^{0}$ na, 7^{44} − 8^{35} $\bullet^{1}$ − 9^{48} $\bullet^{0}$ − 11^{04}
28	6	11.8	•	∇^{0} a $\bullet^{0-2}$ p − np; ≫ a − p; = na − a ∞ a − p; ⌓^{1} na − a
29	8	0.0	•	$\bullet^{1-0}$ na; = na − a ⌓^{0} p − np
30	8	0.0	•	$\bullet^{0}$ 6^{34-38} ∇^{0} 11^{50-22}, p; = na − a; ⌓^{2} na − 6^{34}
31				
Σ	-	41.8	-	

Warszawa – Bielany φ = 52°17' λ = 20°58' Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N_w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_v I	II	III
1	103.9	103.1	104.7	103.9	4.4	11.9	5.7	6.9	13.5	2.6	69	34	55	53	2.6	9.1	4.2	5.3	0	5	0	NW 4	NW 6	NW 4
2	107.7	108.4	107.6	107.9	2.5	7.3	5.4	5.2	7.8	0.1	75	37	50	54	1.8	6.4	4.5	4.2	7	8	3	NNW 4	N 2	N 1
3	108.0	108.5	109.1	108.5	1.8	6.7	4.4	4.3	8.3	-0.9	85	40	57	60	1.2	5.8	3.6	3.5	6	9	1	N 1	NE 2	C 0
4	110.3	107.7	103.9	107.3	3.4	9.1	6.7	6.5	10.7	-1.0	57	33	46	45	3.4	7.8	5.3	5.5	0	1	3	ESE 3	SE 4	ESE 5
5	98.1	96.1	95.8	96.7	5.1	10.2	6.9	7.3	10.5	2.9	49	49	88	62	4.5	6.2	1.1	3.9	10	10 •	10 •	ESE 8	SE 4	SE 4
6	95.5	97.1	99.8	97.5	6.7	9.0	7.1	7.5	9.1	5.6	90	72	83	82	1.0	3.2	1.8	2.0	10 •	10	10	E 2	E 4	E 1
7	101.8	102.1	103.0	102.3	6.9	12.2	10.5	10.0	14.0	5.7	78	48	71	66	2.2	7.4	3.7	4.4	8	9 •	9	N 1	N 1	C 0
8	101.2	100.3	103.0	102.5	10.1	12.7	8.9	10.2	13.7	6.7	73	66	89	76	3.4	5.1	1.2	3.2	9	10 •	0	S 3	SSW 4	W 5
9	101.5	98.2	89.4	96.4	6.3	12.1	13.1	11.2	13.5	5.1	100	87	87	91	0.0	1.8	1.9	1.2	10 ≡	10 •	10 •	SW 1	SW 4	SSW 3
10	86.7	87.3	89.1	87.7	8.1	10.4	8.2	8.7	13.1	7.7	87	74	82	81	1.4	3.3	2.0	2.2	10 •	8	5	SW 5	WSW 5	SW 4
11	92.4	97.0	102.4	97.3	7.9	12.1	11.8	10.9	14.3	5.5	86	63	68	72	1.4	5.2	4.4	3.7	9	9	5	SSE 2	C 0	NNW 1
12	107.2	108.8	109.5	108.5	4.3	11.1	11.7	9.7	14.2	4.1	98	77	49	75	0.1	3.1	7.0	3.4	10	10	9	NW 4	NW 5	N 3
13	110.3	109.4	107.7	109.1	7.7	16.1	12.6	12.2	16.7	5.2	67	37	62	55	3.5	11.5	5.5	6.8	0	5	2	NW 3	NW 3	NW 2
14	104.8	102.9	101.6	103.1	9.6	14.6	12.0	12.0	16.2	6.6	79	58	80	72	2.6	7.0	2.8	4.1	4	9	3	C 0	W 3	WSW 2
15	101.0	101.1	100.6	100.9	8.6	12.4	10.0	10.2	15.0	8.4	92	64	48	68	1.0	5.2	6.4	4.2	9	8	2	N 4	NNW 4	N 3
16	100.3	99.0	96.7	98.7	7.4	14.6	12.4	11.7	15.4	4.8	61	38	62	54	4.0	10.4	5.5	6.6	8	10	10	E 3	ESE 4	E 4
17	95.3	96.0	93.7	95.1	12.3	19.1	18.6	17.2	20.6	10.1	92	58	63	71	1.2	9.3	8.0	6.2	1	7	10 •	WSW 2	W 4	SSW 2
18	90.6	93.7	94.9	93.1	17.3	18.6	16.8	17.4	20.1	14.6	78	69	75	74	4.3	6.6	4.8	5.2	8	10 •	9	WSW 5	WSW 5	SW 2
19	90.2	90.9	97.4	92.8	13.9	14.9	5.5	10.0	16.9	5.5	98	81	91	90	0.4	3.3	0.8	1.5	10	10	10 •	NW 2	NNW 1	NW 6
20	103.7	105.3	108.6	105.9	5.4	10.6	7.4	7.7	11.5	3.8	86	47	65	66	1.3	6.8	3.6	3.9	10	9	3	W 4	NW 2	W 2
21	113.6	113.1	116.2	115.0	6.3	10.1	8.6	8.4	12.2	3.3	82	54	64	67	1.7	5.7	4.1	3.8	0	9 •	1	WSW 2	W 6	W 1
22	117.9	116.9	114.8	116.5	8.6	13.2	10.6	10.8	15.2	5.8	55	35	57	49	5.1	9.8	5.5	6.8	1	8	3	C 0	ENE 2	NE 4
23	113.5	112.1	110.7	112.1	10.1	15.4	13.8	13.3	17.1	5.8	56	37	61	51	5.4	11.1	6.2	7.6	0	9	10	ENE 6	E 8	ESE 6
24	108.4	107.0	104.7	106.7	11.6	11.2	12.3	11.8	14.1	8.2	72	80	90	81	3.7	2.6	1.4	2.6	10	10 •	10	SE 8	SE 9	ESE 3
25	104.1	104.1	104.9	104.4	11.9	12.7	11.9	12.1	15.7	10.6	96	98	95	96	0.5	0.4	0.7	0.5	10	10 • K	10	C 0	C 0	C 0
26	105.0	105.1	104.1	104.7	10.5	11.8	12.4	11.8	13.6	10.3	96	88	90	91	0.5	1.6	1.4	1.2	10	10	10	C 0	NNW 1	C 0
27	102.2	102.2	102.3	102.2	10.5	14.9	11.9	12.3	15.7	8.9	90	69	87	82	1.3	5.2	1.8	2.8	10	9	2	SW 2	W 5	C 0
28	102.1	101.3	99.4	100.9	8.7	15.9	13.8	13.0	16.5	6.5	99	60	81	80	0.1	7.2	3.0	3.4	4 ≡	9	9	C 0	ENE 3	ENE 4
29	94.3	92.7	94.7	93.9	13.1	12.1	9.5	11.0	14.0	9.1	87	93	91	90	1.9	1.0	1.1	1.3	10	10 •	10 •	NE 4	NNE 6	E 2
30	95.0	96.6	98.2	96.6	7.7	10.1	9.4	9.2	14.2	5.2	80	72	64	72	2.1	3.5	4.3	3.3	3	9	0	N 6	WNW 4	C 0
31	100.8	101.7	101.5	101.3	9.0	14.3	12.4	12.0	16.3	4.0	72	38	59	56	3.2	10.1	5.9	6.4	5	4	3	C 0	E 1	ENE 3
M	102.2	102.2	102.3	102.2	8.3	12.5	10.4	10.4	14.2	5.8	80	60	71	70	2.2	5.9	3.7	3.9	6.5	8.5	5.9	2.9	3.3	2.5

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1	95.4	94.4	96.7	95.5	11.4	21.3	15.9	16.1	22.3	10.8	96	53	63	71	0.3	11.6	6.7	6.3	10	6	2	ESE 5	SW 5	SW 1
2	97.8	99.8	103.0	100.2	12.5	11.2	10.7	11.3	16.1	9.9	72	84	75	77	4.1	2.1	3.2	3.1	9	10	10	SW 4	SW 4	W 4
3	106.0	106.5	106.7	106.4	11.8	15.9	13.3	13.7	17.7	8.0	76	60	82	73	3.3	7.2	2.8	4.4	0	9	5	W 1	C 0	C 0
4	107.8	107.2	105.8	106.9	13.6	20.2	16.5	16.7	20.7	9.7	76	47	63	62	3.7	12.7	7.0	7.8	0	8	9	C 0	NE 3	NE 4
5	103.5	101.9	99.7	101.7	13.2	15.4	14.0	14.2	16.7	12.7	73	73	77	76	3.8	4.4	3.7	4.0	10	10 •	9	ENE 4	ENE 7	ENE 3
6	93.7	94.7	95.5	93.3	13.2	13.9	12.9	13.2	15.1	12.5	79	76	75	77	3.2	3.9	3.8	3.6	10	10	8	NE 7	NE 6	NE 6
7	96.4	97.4	99.7	97.8	12.8	17.5	14.4	14.8	19.2	10.6	66	46	62	58	5.1	10.9	6.3	7.4	2	7	1	N 5	N 5	N 2
8	102.9	102.7	101.0	102.2	14.1	20.6	16.2	16.8	21.3	8.6	66	35	55	52	5.4	15.6	8.2	9.7	1	2	0	N 3	N 5	N 3
9	100.0	98.2	98.2	98.8	14.1	20.1	16.2	16.6	21.3	11.6	83	57	74	71	2.7	10.1	4.7	5.8	9	9	10	E 7	E 8	E 6
10	98.4	99.2	98.0	98.5	13.1	13.3	14.3	14.2	17.5	12.7	92	87	95	91	1.3	2.3	0.7	1.4	10 •	10 •	10 •	ENE 4	ENE 5	ENE 2
11	93.8	93.7	94.7	94.1	13.6	15.0	13.1	13.7	15.2	12.7	91	90	93	91	1.5	1.6	1.1	1.4	10	10 •	9	NE 5	NE 5	NE 4
12	97.1	97.2	99.0	97.8	13.8	19.4	13.4	15.0	20.3	12.0	86	60	94	80	2.2	8.9	0.9	4.0	9	8	9 •	NNE 2	NNW 5	W 2
13	100.1	101.4	100.7	100.7	11.5	13.6	13.3	12.9	15.5	10.6	85	81	87	84	2.4	3.0	2.0	2.5	10	10	4	NNW 5	W 6	W 4
14	99.9	101.1	103.3	101.4	12.5	14.3	14.8	14.1	19.1	10.0	98	94	71	88	0.4	0.9	4.8	2.0	10 •	10 • K	3	WNW 3	W 1	NW 1
15	105.6	106.1	105.8	105.8	11.1	19.7	16.2	15.8	21.2	8.6	79	42	68	63	2.8	13.3	6.0	7.4	6	4	0	NW 1	N 1	C 0
16	105.8	104.1	100.4	103.4	16.4	22.3	20.0	19.7	23.9	11.0	69	30	51	50	5.8	18.8	11.4	12.0	3	8	2	C 0	S 1	C 0
17	96.2	93.9	95.4	95.2	17.4	24.9	19.1	20.1	25.7	14.4	72	35	68	58	5.7	20.6	7.0	11.1	0	0	9	SE 2	S 6	W 3
18	101.3	103.9	102.9	102.7	13.4	15.1	16.2	15.2	19.1	12.3	78	73	68	73	3.3	4.6	6.0	4.6	9	9	10	W 5	WSW 3	C 0
19	99.0	98.8	102.9	100.2	13.9	19.3	13.9	15.8	21.4	13.6	85	71	87	81	2.7	6.3	2.2	3.8	10 •	8	8	SW 6	W 8	W 1
20	106.3	106.6	107.3	106.7	14.4	18.5	15.6	16.0	20.3	12.0	72	52	72	65	4.6	10.2	5.0	6.6	3	7	9	W 6	W 8	WSW 1
21	108.8	108.8	106.8	108.1	14.8	19.2	17.3	17.2	22.2	10.8	73	57	66	66	4.1	9.6	6.8	6.8	0	9	1	WSW 3	C 0	C 0
22	103.4	101.3	98.0	100.9	17.3	23.9	24.6	23.2	27.7	13.0	63	49	54	56	7.0	17.1	14.3	12.8	1	3	8	SE 3	SE 4	SE 4
23	98.4	99.9	103.4	100.6	18.4	24.1	18.4	19.8	24.7	18.0	88	53	71	71	2.5	14.0	6.3	7.6	10 •	5	3	SW 1	SW 4	W 2
24	103.3	103.3	103.4	103.3	17.2	23.7	21.0	20.7	24.6	14.0	82	49	68	66	3.5	15.1	8.1	8.9	1	7	4	SW 3	WSW 4	C 0
25	106.9	107.3	107.7	107.3	19.3	24.1	21.7	21.8	26.2	16.9	72	47	60	60	6.3	15.9	10.4	10.9	1	8	2	C 0	W 2	NW 1
26	107.5	106.3	105.5	106.4	20.3	28.9	19.5	22.1	30.3	16.0	71	38	86	65	6.9	24.6	3.3	11.6	1	0	8	C 0	S 3	S 2
27	109.7	109.0	108.1	108.9	18.6	22.7	16.2	18.4	24.0	16.0	71	46	92	70	6.3	14.9	1.6	7.6	3	9	9	NW 3	C 0	NE 4
28	109.1	110.1	110.0	109.7	15.6	18.7	15.2	16.2	19.3	15.0	87	48	62	66	2.3	11.2	5.5	6.7	9	8	1	NNW 3	NW 3	NW 4
29	106.6	106.3	107.1	106.7	14.6	16.9	15.6	15.7	20.7	9.6	64	70	64	66	6.0	5.7	6.4	6.0	3	9	0	SW 5	W 4	WNW 2
30	108.6	107.5	102.5	106.2	13.2	19.2	18.3	17.2	22.7	9.0	74	48	65	62	4.0	11.6	7.3	7.6	0	0	0	W 4	WSW 3	C 0
31																								
M	102.4	102.4	102.4	102.4	14.7	19.2	16.3	16.6	21.1	12.1	78	58	72	69	3.8	10.3	5.5	6.5	5.4	7.1	5.4	3.3	4.0	2.3

Warszawa - Bielany $H_s = 98\,m$ $H_b = 99{,}5\,m$ $h_w = 16\,m$ Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	⌓⁰ na – a
2	8	•	•	
3	7	•	•	∞ a – p; ⌣⁰ na
4	8	•	•	⌣⁰ na
5	6	0.4	•	•⁰ a z poz., p z poz., p... np; ∞ na – a
6	7	0.1	•	•⁰ 6^{20-40}, a ▽⁰ p
7	7	0.0	•	•⁰ 12^{35-40}
8	6	1.6	•	•⁰ 11^{53}..12^{50}, = na – a ∞ a – p = p – np, ⌓⁰ na – a
9	6	3.0	•	•⁰ a – p, np; ≡⁰ na – 6^{50} = a, ll
10	8	2.5	•	•⁰ na, na – 7^{15} ▽⁰ a, p
11	8	•	•	⌓¹ p – np
12	7	•	•	= n – a
13	8	•	•	⌓⁰ n – a, p – np
14	8	8.3	•	▽¹ 9^{45}–10^{35} •² 10^{50}–11^{25}, = ⌓¹ n – a
15	7	•	•	⌓⁰ p – np
16	9	5.5	•	•¹ 22^{00}–23^{20}, ⌇ 21^{55}–22^{10}, ⌓⁰ p – np
17	6	3.3	•	•⁰ 20^{25}–21^{05}, = na ∞ a – p
18	7	4.0	•	•¹ na •⁰ 12^{25-40}
19	7	22.3	•	•⁰ na, 16^{00-10} •² 18^{20-25} •²▲⁰ – 16^{30} •² – 16^{40} •⁰ – 18^{20}, 20^{10-45}, ⌇ 16^{05}–18^{00}, ⟩ 17^{10-50}
20	8	0.1	•	•⁰ 12^{40-50}
21	7	0.0	•	•⁰ 12^{35-40}, ⌓¹ na ⌓⁰ p – np
22	7	•	•	⌓⁰ na
23	7	0.3	•	
24	7	0.7	•	•⁰ na, a, 12^{04}..p; = p – np
25	5	36.7	•	•⁰ na – 6^{25} ▽⁰⁻² 11^{40}–18^{00}, ⌇⁰ 11^{51}–13^{45}
26	5	1.1	•	▽⁰ np; = na – np
27	6	0.1	•	= na – np; ⌓⁰ p – np
28	7	2.6	•	•⁰ 11^{21-40}, 22^{20}–23^{50}; = na – a ≡²⁻⁰ 7^{06}, ⌓² na – a
29	6	19.3	•	•⁰ n •⁰⁻² a – np; = na – a
30	8	•	•	⌓ p – np
31	8	5.5	•	= n – a; ⌓¹ n – a ⌓⁰ p – np
Σ	–	117.4	–	

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1	9	0.2	•	•¹ na – 6^{10} ▽⁰ 11^{10}; = n – a; ⌓¹ p – np
2	9	0.6	•	•⁰ a •⁰ p z poz.; ⌓⁰ n – a
3	8	0.5	•	•⁰⁻¹ 11^{26-38} ▽⁰ 12^{25}, = ⌓¹ n – a, p – np
4	8	•	•	= ⌓² n – a
5	7	0.4	•	▽⁰ 10^{08-15} •⁰ 12^{10} – p, ⟩ a, por. wiatru p; ∞ n – a
6	9	0.0	•	•⁰ na ▽⁰ 12^{25-35}; ⟩ a, por. wiatru p
7	9	•	•	
8	9	•	•	∞ na – a; ⌓⁰ na
9	7	4.9	•	•⁰ np
10	7	8.6	•	•⁰ na – 12^{50}, 19^{10} – np
11	6	3.2	•	• na, 9^{40}..p
12	8	7.7	•	▽⁰ 13^{15}..p •⁰⁻¹ 17^{15}, 20^{45}; ⌇⁰ 18^{15}–19^{10}; ⌓² na – a
13	7	9.8	•	
14	7	34.0	•	•² 3^{30}–9^{27} ▽²⁻⁰ 10^{31}–12^{52}; ⌇⁰ 11^{21}–12^{45} N-S
15	8	•	•	
16	6	•	•	= na – a ∞ a – n; ⌓¹ na – a
17	8	0.7	•	∞ na – a
18	7	2.4	•	▽⁰ na; ∞ p – np
19	8	9.2	•	•⁰ na •⁰⁻¹ 6^{34} ▽²▲⁰ 17^{40-42} ▽² – 17^{44} ▽⁰⁻¹ 19^{01-16}; ⌇⁰ 17^{29-50} NW-SE
20	7	•	•	∞ n – a
21	6	•	•	∞ n – a = ⌓¹ p – np
22	7	0.0	•	= ⌓¹ n – a ∞ a – p ⌓⁰ p – np
23	9	0.0	•	•² 6^{15}..7^{50}
24	7	•	•	= ⌓¹ n – a ∞ a – p = p – np
25	8	•	•	= n – a; ⌓⁰ p – np
26	8	5.0	•	•⁰⁻¹ 18^{26-35}, (⌇) 18^{10}–19^{09}; ⊖ 18^{10-25}
27	9	5.8	•	•⁰ 13^{15} 17^{10-50} •¹⁻⁰ – 19^{15} •⁰ 19^{40-50} •¹ – 19^{53} •⁰ – 19^{58}
28	9	•	•	= na
29	7	0.1	•	•⁰ 9^{15-50}
30	8	•	•	∞ p; ⌓⁰ na
31				
Σ	–	91.0	–	

Warszawa - Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ *Lipiec — Juillet 1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D_v I	II	III
1	96.3	99.1	100.6	98.7	18.7	18.1	16.2	17.3	19.3	14.9	64	73	55	64	7.9	5.6	8.2	7.2	10	9	4	SSW 2	W 5	WNW 2
2	101.6	100.3	97.6	99.8	12.5	16.6	16.2	15.4	19.1	9.3	73	47	60	60	3.9	10.1	7.4	7.1	7	7	9	NW 1	W 3	W 2
3	96.6	97.0	96.6	96.7	13.4	15.6	12.8	13.6	17.2	12.5	73	49	83	68	4.2	9.1	2.6	5.3	5	9	7	WSW 7	WSW 5	SW 1
4	99.1	98.3	98.2	98.5	11.2	15.2	11.9	12.6	16.6	8.1	75	56	87	73	3.3	7.7	1.8	4.3	2	10 •	0	WSW 3	W 4	SSW 1
5	97.6	97.2	97.6	97.5	11.7	14.8	13.1	13.2	16.7	8.6	84	61	66	70	2.1	6.5	5.1	4.6	8	9	2	C 0	N 1	NW 3
6	100.2	99.6	100.4	100.1	10.7	16.2	11.5	12.5	17.2	6.9	79	42	84	68	2.8	10.7	2.2	5.2	2	9	9	W 6	W 8	W 2
7	101.9	101.7	99.0	100.9	12.7	16.1	13.0	13.7	19.3	8.8	80	63	94	79	2.9	6.9	0.9	3.6	9	10	10 •	WSW 4	SSW 5	C 0
8	97.4	95.1	88.8	93.8	15.4	21.4	16.2	17.3	24.7	12.7	84	64	95	80	2.8	9.2	1.4	4.5	5	9	10 •	S 2	SSE 3	WSW 2
9	94.3	96.8	99.7	96.9	15.2	15.4	11.3	12.8	16.9	11.0	71	54	88	71	4.5	8.0	1.7	4.7	6	10	10 •	WSW 4	W 8	WSW 3
10	102.4	103.2	104.7	103.4	12.1	15.9	12.3	13.2	17.4	8.8	76	60	78	71	3.3	7.3	3.2	4.6	2	10	7	W 2	W 3	WSW 1
11	106.9	107.3	108.0	107.4	11.0	16.2	14.5	14.0	18.6	8.4	87	62	73	74	1.6	7.0	4.5	4.4	0	10	1	WSW 1	WSW 4	C 0
12	106.8	103.7	101.4	104.0	14.9	22.4	17.0	17.8	23.3	10.9	63	47	91	67	6.2	14.4	1.8	7.5	9	9	10 •	S 3	S 3	SSW 3
13	104.5	104.2	104.9	104.5	15.5	20.7	19.2	18.6	23.4	14.6	94	61	74	76	1.1	9.6	5.8	5.5	10	9	1	C 0	SW 1	C 0
14	106.0	106.4	106.4	106.3	19.3	28.3	24.6	24.2	29.4	15.2	77	42	56	58	5.2	22.3	13.6	13.7	0	4	4	C 0	S 4	SE 2
15	107.4	107.2	106.3	107.0	22.0	29.1	23.4	24.5	29.7	18.4	72	47	63	61	7.5	21.2	10.6	13.1	1	2	8	SSE 2	SSE 3	C 0
16	105.1	103.8	103.3	104.1	22.1	28.6	22.6	24.0	29.7	17.0	73	42	74	63	7.1	22.8	7.0	12.3	2	4	3	C 0	NE 3	NNE 2
17	103.0	101.2	101.3	101.8	19.3	25.5	17.0	19.7	27.5	15.7	92	63	98	84	1.8	12.0	0.4	4.7	9	8	10	NE 3	NE 3	ENE 3
18	102.1	103.5	105.4	103.7	14.5	17.8	17.9	17.0	20.4	13.1	91	76	67	78	1.5	4.8	6.7	4.3	10	10	8	ENE 4	ENE 4	NNE 3
19	110.4	110.3	110.3	110.3	15.5	21.0	17.3	17.8	22.2	11.6	76	46	69	64	4.3	13.6	6.2	8.0	1	6	0	NE 3	NE 5	C 0
20	111.0	109.3	107.0	109.1	16.9	23.1	18.7	19.4	23.4	11.6	66	44	61	57	6.4	15.9	8.4	10.2	0	2	3	ESE 1	SSE 6	E 2
21	103.9	101.3	97.9	101.0	17.9	24.0	18.9	19.9	25.2	13.7	61	50	88	66	8.0	15.0	2.5	8.5	8	4	10 (K)	ESE 7	ESE 7	SSE 5
22	98.0	99.0	98.8	98.6	15.3	21.7	19.7	19.4	24.2	16.3	100	67	73	80	0.0	8.5	6.1	4.9	10 •	8	2	W 1	W 2	C 0
23	97.8	95.4	97.3	96.8	18.3	25.0	16.9	19.3	25.2	14.4	89	48	93	77	2.2	16.6	1.4	6.7	7	9	1	W 1	SE 4	W 4
24	97.8	97.4	99.4	98.2	17.1	23.8	18.5	19.5	24.0	14.2	82	61	68	70	3.5	11.6	6.8	7.3	0	8	5	SSE 2	SW 2	C 0
25	101.9	101.5	99.3	100.9	15.3	21.6	19.9	19.2	23.3	13.5	85	46	59	63	2.6	14.0	9.5	8.7	8	9	1	C 0	W 3	W 1
26	99.4	98.4	97.9	98.6	15.5	18.8	17.1	17.1	21.0	15.6	91	59	68	73	1.5	9.0	6.2	5.6	8	8	2	W 2	W 7	SW 3
27	97.5	98.8	99.9	98.7	13.5	14.0	12.7	13.2	17.1	12.6	87	64	77	76	2.0	5.8	3.4	3.7	9 •	8	1	WSW 3	W 7	W 2
28	99.6	100.2	99.6	99.8	13.1	15.8	13.4	13.9	18.1	12.0	83	57	90	77	2.6	7.6	1.6	3.9	9	8 •	10 •	SW 4	W 5	W 3
29	97.3	95.9	91.5	94.9	13.5	18.1	17.0	16.4	21.3	12.5	90	70	83	81	1.6	6.2	3.4	3.7	10	10	10 •	W 2	W 2	SW 3
30	89.1	86.4	89.0	88.2	16.1	20.8	13.7	16.1	21.1	13.5	79	57	85	74	3.8	10.6	2.3	5.6	9	5	8	SW 4	SW 9	SW 6
31	92.0	91.0	91.4	91.5	14.0	19.0	13.8	15.2	20.4	10.9	79	60	88	76	3.4	8.9	2.0	4.8	9	8	10 •	WSW 3	SW 5	WSW 4
M	100.8	100.3	100.0	100.4	15.3	20.0	16.4	17.0	21.7	12.4	80	56	77	71	3.6	10.9	4.7	6.4	6.0	7.8	5.7	2.5	4.3	2.0

Sierpień — Août

1	97.6	100.0	100.7	99.4	11.8	16.0	14.1	14.0	17.9	10.8	91	59	71	74	1.1	7.5	4.6	4.4	9	9	7	WNW 3	WSW 6	C 0
2	96.4	97.1	96.7	96.7	11.1	10.1	10.8	10.7	14.1	9.6	88	92	92	91	1.6	1.0	1.0	1.2	10 •	10 •	9	E 5	NNW 4	C 0
3	97.8	97.9	98.4	98.0	10.9	19.9	15.3	15.4	21.3	8.0	86	45	69	67	1.8	12.8	5.5	6.7	1	4	3	WSW 3	SW 4	SW 4
4	100.8	100.3	103.5	101.5	13.3	17.9	13.0	14.3	18.6	11.4	82	73	94	83	2.8	5.6	0.9	3.1	8	10	9	SW 4	W 3	W 3
5	107.3	108.3	108.4	108.0	13.4	18.9	15.9	16.0	21.4	11.9	87	60	81	76	2.0	8.6	3.5	4.7	1	9	1	WSW 2	W 3	C 0
6	108.2	105.5	102.7	105.5	16.8	26.3	23.3	22.4	28.3	11.0	79	52	67	66	4.1	16.5	9.4	10.0	4	5	9	SSW 2	SSW 3	S 3
7	103.7	102.1	100.9	102.2	22.1	28.0	24.6	24.8	30.4	19.5	72	53	60	62	7.5	17.8	12.3	12.5	8	9	4	WSW 3	SW 4	W 1
8	104.6	102.9	102.7	103.4	19.5	25.6	17.9	20.2	28.2	17.9	85	60	85	77	3.5	15.2	3.0	6.6	9	1	9	C 0	C 0	NNE 7
9	104.9	107.0	107.8	106.6	16.2	15.2	14.6	15.2	18.3	14.6	84	88	94	89	2.9	2.1	0.9	2.0	8	10	9	W 3	W 3	NNW 1
10	107.4	109.6	108.9	108.6	12.6	17.0	13.1	13.0	18.7	11.3	80	47	62	63	2.9	10.2	6.5	6.5	3	7	8	N 3	N 3	NNW 2
11	109.2	109.4	108.1	108.9	12.1	15.6	14.1	14.0	17.6	11.5	88	63	67	73	1.7	6.5	5.3	4.5	10 •	9	3	C 0	NNW 1	NW 2
12	108.8	108.4	108.3	108.6	11.8	15.8	12.4	13.1	18.7	10.3	88	77	86	84	1.6	4.1	2.0	2.6	10	6	9	N 4	NW 4	WNW 2
13	107.4	107.7	106.9	107.3	10.7	14.9	11.3	12.0	15.5	8.4	89	66	83	79	1.3	5.7	2.3	3.2	2	9	9	NW 4	NNW 3	WNW 4
14	107.1	106.5	105.8	106.5	10.5	13.5	12.3	12.2	14.8	9.3	95	77	89	87	0.7	3.5	1.5	1.9	10 •	9	10	W 4	W 5	WNW 2
15	107.6	108.4	109.0	108.3	11.7	16.1	12.8	13.4	18.1	11.1	91	58	88	79	1.1	7.7	1.8	3.5	9	8	8	NW 1	C 0	W 1
16	109.6	108.6	107.4	108.5	10.1	17.7	13.8	13.8	18.9	8.5	96	55	80	77	0.5	9.0	3.2	4.2	2	8	0	C 0	C 0	C 0
17	106.9	107.1	106.7	106.9	12.0	18.9	14.9	15.2	21.4	9.7	93	54	81	76	1.0	10.1	3.3	4.8	9	5	1	C 0	NW 2	C 0
18	108.0	108.6	108.9	108.5	13.8	22.0	15.9	16.9	23.4	10.4	84	46	77	69	2.5	14.3	4.2	7.0	2	6	1	C 0	C 0	C 0
19	111.2	111.3	111.5	111.3	15.6	25.1	20.4	20.4	25.7	11.5	68	36	50	51	5.7	20.5	12.0	12.7	1	3	0	W 1	S 1	SW 3
20	111.6	110.6	109.1	110.4	16.2	26.1	20.1	20.6	26.4	13.0	68	37	54	53	6.0	21.2	10.9	12.7	0	1	0	C 0	SSW 3	SE 2
21	106.0	103.8	101.4	103.7	15.8	26.3	22.1	21.6	27.5	15.2	79	46	49	58	3.7	18.3	13.7	12.0	6	2	4	SSE 3	S 4	SSE 3
22	100.7	99.4	97.1	99.1	17.6	26.3	21.6	21.8	27.9	14.9	77	33	60	57	4.5	22.6	10.3	12.3	2	7	0	S 3	E 6	SE 3
23	97.6	97.2	97.4	97.4	17.2	27.2	22.3	22.4	27.8	13.5	72	38	57	56	5.4	22.4	11.8	13.2	0	1	8	SE 7	NNE 8	SE 3
24	98.1	98.0	96.2	97.4	18.3	24.7	23.6	22.6	27.7	18.2	76	53	60	63	5.1	14.5	11.7	10.4	10	8	9	SE 2	ESE 3	SE 4
25	93.0	94.0	93.7	94.2	20.1	23.3	18.8	20.6	26.2	18.3	73	62	90	76	6.0	12.4	2.1	6.8	8	9	9	ESE 4	SSW 3	WSW 3
26	98.2	100.6	100.6	99.8	12.6	12.3	11.3	11.9	18.7	11.2	93	93	98	96	0.7	0.7	0.4	0.6	10 •	10	10 •	NW 3	NW 4	NW 4
27	96.2	96.4	99.0	97.2	9.3	10.6	10.3	10.3	11.3	9.1	96	96	96	96	0.3	0.3	0.3	0.3	10 •	10 •	10 •	WNW 7	NW 8	WNW 8
28	101.2	102.4	102.9	102.2	9.4	16.4	13.2	13.0	18.2	9.0	97	54	82	78	0.3	8.6	2.8	3.9	9	7	0	WSW 1	NW 2	W 3
29	103.2	103.3	101.4	102.6	10.0	18.1	14.2	14.1	19.3	8.5	96	59	76	77	0.5	8.6	3.9	4.3	1	3	2	W 2	C 0	C 0
30	101.0	102.7	103.9	102.3	12.4	16.8	12.2	13.4	18.0	11.6	90	66	87	81	1.4	6.4	1.3	3.2	10	7	0	W 3	NW 2	WNW 1
31	103.5	102.9	101.8	102.7	9.7	16.7	12.5	12.8	18.4	8.2	91	60	89	80	1.1	7.7	1.5	3.4	0	6	1	WNW 3	WNW 4	C 0
M	103.7	103.8	103.5	103.7	13.7	19.4	16.0	16.3	21.2	11.9	83	60	77	74	2.6	10.3	5.0	6.0	3.9	6.8	5.2	2.5	3.1	2.2

Warszawa - Bielany $H_s = 98\,m$ $H_b = 99.5\,m$ $h_w = 16\,m$ Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚCIEŃ LÓD h	POGODA
1	7	4.3	•	$\bullet^{0}\,7^{45}-8^{20}$ $\bullet^{1}-8^{35}$; $K^{0}\,8^{13-15}$; = na
2	7	•	•	$\frown^{0}$ na
3	7	0.0	•	$\bullet^{0}\,18^{05-12}$ 19^{18-24}
4	9	0.9	•	$\nabla^{0}\,12^{30-40}$, p; = p − np
5	7	0.9	•	$\nabla^{0}\,10^{50}-11^{20}$; = na − a; $\frown^{1}$ na − a
6	8	0.7	•	$\nabla^{0}\,12^{40-50}$; $15^{15}-16^{35}$ $20^{50}-21^{20}$; $\frown^{0}$ na
7	6	6.9	•	$\nabla^{0}\,17^{15-20}$ $\nabla^{1}\,18^{45}-20^{55}$; = na − a
8	7	1.6	•	$\bullet^{0}\,17^{15}$ 21^{10}; = na − a ∞ p = p − np
9	9	1.9	•	$\nabla^{0}\,17^{55}-18^{20}$ 20^{05} np
10	7	2.8	•	$\nabla^{0}\,12^{45-58}$ $14^{20}-16^{05}$; $K^{0}\,14^{04-25}$
11	7	0.0	•	$\nabla^{0}\,12^{25-35}$; = na − a, p − np; $\frown^{2}$ na $\frown^{0}$ a
12	7	3.2	•	$\bullet^{0-1}\,18^{20}-19^{15}$ $\bullet^{1}$ np; = n − a ∞ a − p
13	8	•	•	= $\frown^{1}$ p − np
14	9	•	•	= $\frown^{0}$ n − a
15	8	•	•	∞ n − a $\frown^{0}$ p − n
16	8	•	•	= $\frown^{0}$ n − a ∞ a − p
17	7	57.2	•	$\nabla^{2}\,15^{11}-17^{41}$ $\nabla^{1}-21^{46}$ $\nabla^{0}-22^{05}$; (K)$^{0}\,12^{17-48}$ $K^{0-2}\,15^{05}-17^{48}$ − (K) 20^{20} S−N; ∞ $\frown^{0}$ n − a
18	7	2.3	•	$\nabla^{1}\,3^{11}-4^{51}$ $\nabla^{0}\,5^{51}-6^{30}$, 7^{26-56}
19	8	•	•	= p − np; $\frown^{0}$ na − p, p − np
20	7	•	•	∞ na − a, p − np
21	8	24.2	•	$\nabla^{0}\,18^{57}-19^{15}$ $\nabla^{0-1}\,20^{41}-21^{58}$; (K) 20^{30} − $K^{0-1}\,20^{50}-22^{10}$
22	8	2.0	•	$\bullet^{0}\,5^{26}-8^{26}$; $\frown^{0}$ p − np
23	7	7.7	•	$\nabla^{0}\,13^{10}-14^{06}$ $\nabla^{1}\,14^{53}-15^{06}$; (K)$^{0}\,12^{55}$ − $K^{0-1}\,13^{05}-16^{40}$ S−N; = na − a, p − np; $\frown^{1-2}$ na − a; ⊕ a
24	7	•	•	= na − a; $\frown^{2}$ na − a
25	8	5.8	•	$\frown^{0}$ na − a, p − np
26	8	0.0	•	∇^{2} na; K na
27	7	0.5	•	$\nabla^{0}\,8^{20}$ − a; $\frown^{0}$ p − np
28	6	1.5	•	∇^{0} p $\bullet^{0}\,19^{36}$ − np
29	7	2.8	•	$\bullet^{0}$ na $\nabla^{0-1}\,19^{48}$ − np; = na − a
30	8	10.1	•	$\nabla^{2}\,13^{20-34}$ $\nabla^{0}\,15^{00}$ − p; $K^{0}\,13^{10-45}$ W−E $K^{0}\,14^{56}$ − 16^{20} W−E
31	7	1.1	•	$\nabla^{0}\,15^{03-09}$ 18^{40-57} ∇ p − np; (K) 18^{25-45} W−E
Σ	-	138.4	-	

Sierpień - Août

1	8	•	•	= p − np; $\frown^{0}$ p − np
2	6	12.5	•	$\bullet^{0}$ a − p
3	8	•	•	= $\frown^{2}$ n − a
4	8	3.2	•	$\bullet^{1}\,11^{06}$ $\bullet^{2-1}\,11^{07-17}$ $\bullet^{0}\,12^{57}$ $\bullet^{1}\,13^{21}$, 13^{29} $\bullet^{2-1}\,18^{27}$... 19^{27}; (K) 10^{41-58}
5	8	•	•	= $\frown^{2}$ n − a = $\frown^{1}$ p − np
6	8	•	•	= $\frown^{2}$ n − a
7	7	•	•	∞ a − p
8	8	•	•	
9	7	0.4	•	$\bullet^{0}\,15^{45}$... p; $\frown^{0}$ na − a
10	8	0.2	•	$\frown^{2}$ na − a
11	9	0.0	•	$\bullet^{0}$ na − a
12	7	6.4	•	$\nabla^{0}\,11^{15-25}$ 11^{55} − 12^{20} $\nabla^{1}\,15^{50}$ − 16^{40} $\bullet^{0}\,18^{50-55}$
13	9	6.0	•	$\nabla^{0}\,11^{14-25}$ $\nabla^{1}\,13^{06-15}$ 18^{20-56}; $\frown^{2}$ na − a
14	9	3.0	•	$\bullet^{0}\,6^{05}$ − 10^{10} ∇^{0} a...p
15	9	2.8	•	$\bullet^{1}\,18^{07}$ − 19^{30}
16	9	•	•	= $\frown^{1}$ n − a $\frown^{1}$ p − np
17	9	•	•	= $\frown^{1}$ n − a $\frown^{0}$ p − np
18	8	•	•	= $\frown^{1}$ n − a = $\frown^{1}$ p − np
19	7	•	•	= $\frown^{1}$ n − a ∞ a − p = $\frown^{0}$ p − np
20	7	•	•	= $\frown^{0}$ n − a ∞ a − p $\frown^{0}$ p − np
21	7	•	•	= n − a ∞ a − p
22	7	•	•	= na − a; $\frown^{0}$ na
23	7	•	•	
24	7	0.0	•	
25	7	20.8	•	• na • $^{0}\,13^{45}$...p; = na
26	7	39.2	•	$\bullet^{2}$ na $\bullet^{0-1}$ a − 11^{25} • p z prz. $\bullet^{1}\,16^{35}$ − np; = np
27	7	13.0	•	$\bullet^{1-0}$ na − np; = na − a
28	9	0.0	•	$\nabla^{0}\,13^{25-30}$; = na − a
29	8	•	•	= na − a; $\frown^{0}$ na
30	7	0.7	•	$\nabla^{0}\,13^{06-18}$; = na − a; $\frown^{0}$ np
31	8	•	•	= na; $\frown^{2}$ na $\frown^{0}$ np
Σ	-	108.2	-	

Warszawa – Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ *Wrzesień – Septembre* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	101.5	102.0	104.7	102.7	11.6	20.0	15.6	15.7	21.6	8.4	91	55	86	77	1.1	10.5	2.4	4.7	4	2	0	C 0	ESE 4	C 0
2	107.5	107.7	107.2	107.5	13.8	25.1	19.1	19.3	26.5	12.8	89	48	81	73	1.8	16.4	4.2	7.5	10	8	1	E 3	E 6	ESE 1
3	104.7	102.4	100.4	102.5	18.2	26.6	21.5	22.0	27.1	15.8	80	47	65	64	4.3	18.4	9.0	10.6	2	7	3	ESE 3	SE 7	SSE 3
4	99.1	98.1	95.1	97.4	17.7	22.3	16.9	18.4	24.8	16.0	84	78	98	87	3.2	5.8	0.4	3.1	9	9	10 •	SSE 2	WSW 4	WSW 2
5	99.0	100.1	98.5	99.3	12.8	18.9	15.2	15.5	20.5	12.0	92	62	88	81	1.2	8.2	2.1	3.8	9	7	0	SW 3	WSW 6	C 0
6	96.6	94.9	93.7	95.1	14.5	22.1	17.3	17.8	23.6	12.9	89	55	84	76	1.8	11.9	3.1	5.6	5	9	10	C 0	C 0	C 0
7	94.5	96.2	98.2	96.3	11.1	16.1	12.5	13.0	17.6	11.0	94	59	76	76	0.8	7.5	3.6	4.0	8	4	2	W 1	W 5	SW 1
8	100.9	102.7	103.5	102.4	10.3	16.5	13.7	13.6	18.0	9.4	88	64	75	76	1.4	6.8	3.9	4.0	2	5	9	SW 3	WSW 4	SW 1
9	101.6	101.8	102.6	102.0	12.8	22.5	17.1	17.4	24.3	9.2	78	54	87	73	3.3	12.6	2.6	6.2	6	8	4	SE 4	SW 5	C 0
10	100.6	98.9	100.5	100.0	15.6	23.7	17.5	18.6	24.9	14.8	87	50	88	75	2.3	14.7	2.4	6.5	1	8	9	SE 3	SE 6	W 2
11	96.0	98.6	101.9	98.8	15.9	16.2	11.9	14.0	18.5	11.8	89	80	94	88	2.0	3.6	0.8	2.1	9	9	10	SE 5	WSW 6	WSW 3
12	102.9	103.0	101.5	102.5	10.7	15.9	12.3	12.8	17.8	10.4	96	56	75	76	0.5	8.0	3.5	4.0	9	6	5	WSW 3	WSW 4	C 0
13	99.9	99.7	99.7	99.8	10.5	17.7	12.7	13.4	18.1	8.0	87	55	81	74	1.6	9.0	2.8	4.5	7	7	2	SW 1	W 2	W 2
14	101.8	102.9	105.2	103.3	10.3	16.7	13.0	13.2	18.1	9.5	91	58	78	76	1.1	8.0	3.3	4.1	9	9	9	SW 1	W 5	W 2
15	106.8	108.2	112.2	109.1	11.2	15.1	11.0	12.1	16.4	9.5	96	56	74	75	0.5	7.5	3.4	3.8	10	5	0	W 5	WNW 5	WNW 1
16	115.7	116.0	114.0	115.2	6.6	16.1	11.0	11.2	18.1	5.7	96	54	84	78	0.4	8.4	2.1	3.6	1	5	1	W 1	C 0	C 0
17	111.7	110.0	108.6	110.1	10.1	20.7	16.3	15.8	22.4	9.5	79	56	80	72	2.6	10.7	3.6	5.6	0	5	0	SSE 2	S 3	SSW 3
18	107.4	105.2	102.4	105.0	13.0	22.1	17.9	17.7	23.2	12.0	88	53	63	68	1.8	12.5	7.6	7.3	0	0	0	SSW 2	SE 6	S 4
19	104.6	108.6	111.8	108.3	14.7	14.3	12.0	13.2	17.9	11.7	80	71	77	76	3.3	4.8	3.2	3.8	9	10	9	W 3	W 4	WSW 3
20	114.2	116.4	119.8	116.8	8.1	15.5	11.1	11.4	15.7	6.8	89	61	90	80	1.2	6.9	1.3	3.1	8	9	0	W 3	W 3	W 3
21	122.0	121.8	118.4	120.7	6.1	15.2	10.1	10.4	15.7	5.0	97	58	86	80	0.3	7.3	1.8	3.1	7	8	0	W 2	W 3	WSW 2
22	115.6	112.2	108.2	112.0	8.7	18.3	13.2	13.4	19.6	8.2	90	49	74	71	1.0	10.6	4.0	5.2	9	0	0	WSW 2	WSW 6	SW 3
23	106.7	106.1	104.1	105.6	10.1	21.4	14.8	15.3	22.6	9.0	87	56	87	77	1.6	11.2	2.2	5.0	1	0	0	SW 3	SW 3	C 0
24	104.7	105.0	104.0	104.6	10.0	22.3	14.2	15.2	23.0	9.0	93	46	86	75	0.8	14.5	2.4	5.9	0	0	0	C 0	C 0	SSE 1
25	104.1	102.1	100.9	102.4	10.1	22.5	16.3	16.3	23.7	8.4	97	56	73	75	0.4	12.0	4.9	5.8	2	1	1	SSE 1	SE 3	SE 2
26	98.9	98.6	98.6	98.7	12.4	23.2	18.0	17.9	24.3	11.2	86	43	68	66	2.0	16.1	6.5	8.2	2	1	0	E 4	ESE 7	ESE 5
27	97.4	96.4	98.7	97.5	14.3	17.2	16.1	15.9	20.6	13.6	88	87	90	88	2.0	2.6	1.7	2.1	9 •	9 •	0	E 2	ESE 5	SSE 5
28	96.1	95.9	93.1	95.0	15.9	23.9	21.4	20.6	24.5	14.9	86	57	64	69	2.5	12.6	9.2	8.1	9	6	4	SSE 5	SSE 5	SSE 7
29	93.5	94.7	102.1	96.8	16.9	13.1	11.2	13.1	21.6	11.1	95	95	94	95	1.0	0.7	0.8	0.8	9 •	10 •	1	S 2	W 5	WSW 4
30	105.2	105.0	105.2	105.1	9.0	18.7	14.6	14.2	19.5	7.6	89	66	88	81	1.3	7.3	2.0	3.5	5	6	0	S 2	SE 4	S 1
31																								
M	103.7	103.7	103.8	103.7	12.1	19.3	14.8	15.2	21.0	10.5	89	60	81	77	1.6	9.6	3.4	4.9	5.7	5.8	3.0	2.3	4.1	2.0

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1	106.6	108.1	109.1	107.9	9.6	19.7	13.5	14.1	20.2	9.0	99	72	92	88	0.2	6.3	1.3	2.6	0 ≡	2	0	C 0	C 0	C 0
2	109.2	108.0	108.1	108.4	9.3	18.8	12.2	13.1	19.1	7.9	93	59	88	80	0.8	9.0	1.7	3.8	0	0	0	C 0	NE 6	E 3
3	108.7	109.8	111.5	110.0	10.7	16.6	13.7	13.7	17.1	10.6	94	76	95	88	0.9	4.6	0.7	2.1	6	9	10	E 5	ESE 4	C 0
4	112.3	112.3	111.9	112.2	11.6	12.9	9.6	10.9	14.1	9.5	99	92	99	97	0.1	1.3	0.2	0.5	10 ≡	10	10	C 0	NW 2	C 0
5	112.5	113.4	113.3	113.1	7.2	12.4	9.0	9.4	14.4	6.2	100	79	99	93	0.0	3.0	0.2	1.1	10 ≡	7 ≡	0	NW 1	C 0	W 2
6	113.7	113.8	112.3	113.3	5.4	10.4	7.0	7.4	11.4	4.5	100	99	100	100	0.0	0.2	0.0	0.1	10 ≡	10 ≡	10 ≡	C 0	C 0	W 2
7	110.3	109.2	106.2	108.6	3.9	15.2	8.9	9.2	15.7	3.4	100	56	92	83	0.0	7.7	0.9	2.9	9 ≡	2	4	C 0	S 1	C 0
8	103.3	103.7	106.0	104.3	5.9	11.3	9.8	9.2	12.5	5.5	100	79	83	87	0.0	2.8	2.0	1.6	10 ≡	10	3	SW 3	NW 4	NNW 3
9	106.1	105.4	104.8	105.4	5.7	10.5	6.2	7.2	11.1	5.0	94	64	85	81	0.6	4.6	1.5	2.2	9	9	8	NW 3	WNW 4	NW 2
10	103.8	103.7	103.3	103.6	4.3	9.1	6.8	6.8	10.1	4.1	90	67	91	83	0.8	3.8	0.9	1.8	9	9	1	C 0	NW 3	W 2
11	103.9	101.7	106.3	104.0	5.6	8.6	4.1	5.6	9.5	4.1	95	86	87	89	0.4	1.6	1.1	1.0	10	10	1	W 2	NW 6	WNW 2
12	112.9	115.2	115.7	114.6	1.1	8.1	3.4	4.0	8.7	0.4	94	57	81	77	0.4	4.7	1.5	2.2	9	8	1	NW 2	NNW 3	WSW 2
13	115.3	114.3	111.2	113.6	2.0	10.1	5.8	5.9	11.1	2.0	84	52	77	71	1.2	6.0	2.1	3.1	2	9	0	W 5	WSW 4	SW 2
14	110.0	110.9	110.8	110.6	3.6	12.2	7.3	7.6	13.6	3.6	90	66	96	84	0.8	4.8	0.4	2.0	4	5	0 ≡	WSW 4	WSW 3	C 0
15	109.9	109.2	106.9	108.7	2.5	14.2	10.1	9.2	15.3	0.5	95	50	67	71	0.4	8.1	4.1	4.2	2	0	2	SSW 2	SSW 2	SSW 2
16	104.7	103.0	105.6	104.4	7.6	16.3	8.4	10.2	16.5	7.5	72	49	97	73	2.9	9.4	0.3	4.2	8	8	10 •	SW 3	SW 4	WNW 3
17	109.5	113.0	114.7	112.4	6.9	11.6	5.6	7.4	12.2	5.5	91	58	88	79	0.8	5.7	1.1	2.5	5	4	0	W 4	WNW 5	WSW 4
18	113.7	112.7	112.5	113.0	5.3	9.6	8.9	8.2	9.7	3.6	91	79	92	87	0.8	2.6	0.9	1.4	8	9	10	SW 2	W 5	W 4
19	114.3	115.1	116.6	115.3	7.0	9.8	4.4	6.4	10.5	4.4	97	62	97	85	0.3	4.6	0.3	1.7	9	6	8	NW 1	NNW 5	NW 2
20	118.3	120.3	123.3	120.6	4.8	8.9	1.2	4.0	9.1	1.1	95	57	87	80	0.4	4.9	0.9	2.1	5	6	0	NW 2	NNE 4	NNE 1
21	124.7	126.0	125.7	125.5	-3.1	4.1	1.2	0.8	5.3	-3.2	95	61	77	78	0.5	3.2	1.5	1.7	2	5	5	C 0	E 2	C 0
22	126.1	124.9	122.4	124.5	-1.6	6.3	3.3	2.8	7.6	-2.5	89	59	74	74	0.6	3.9	1.9	2.1	2	0	9	NE 1	W 1	W 3
23	118.2	116.8	116.1	117.0	5.0	8.8	8.5	7.7	9.8	2.6	92	78	88	86	0.7	2.4	1.4	1.5	10	10	10	W 3	NNW 2	NW 1
24	117.4	118.4	117.8	117.9	4.3	6.9	6.3	6.0	9.1	3.5	100	78	91	90	0.0	2.2	0.8	1.0	10 ≡	6	0	NNW 2	C 0	NW 2
25	116.9	116.7	116.8	116.8	7.1	8.2	7.7	7.7	9.1	6.0	90	79	87	85	1.0	2.3	1.3	1.3	10	10	9	C 0	C 0	C 0
26	115.7	114.3	111.1	113.7	5.2	9.4	6.1	6.7	9.7	4.6	100	69	85	85	0.0	3.7	1.4	1.7	10 ≡	1	10	C 0	E 2	E 2
27	107.8	106.7	107.8	107.4	-0.1	7.7	1.9	2.8	8.3	-0.3	98	73	94	89	0.2	2.6	0.4	1.1	0 ≡	8	10	E 2	WSW 4	W 2
28	105.4	104.2	103.2	104.3	3.7	12.1	12.6	10.2	13.3	1.6	98	66	74	79	0.2	4.8	3.7	2.9	6	8	9	E 3	SW 4	SW 3
29	102.4	101.2	100.1	101.2	7.5	13.3	13.3	12.4	16.1	7.3	84	62	83	76	1.7	6.7	2.7	3.7	8	8	10	SW 4	ESW 4	W 6
30	106.4	107.3	106.6	106.8	3.0	8.3	6.1	6.4	13.3	4.7	92	72	82	82	0.7	3.2	1.7	1.9	2	3	0	W 4	WSW 6	SW 4
31	98.4	99.0	97.3	97.9	6.0	10.9	6.5	7.3	11.6	3.6	74	58	83	72	2.4	3.3	1.3	3.1	9	7	3	SSW 4	WSW 8	W 3
M	110.9	110.9	110.8	110.9	5.1	11.1	7.4	7.8	12.1	4.1	93	68	88	83	0.6	4.4	1.3	2.1	6.5	6.4	4.8	1.9	3.[illegible]	[illegible].1

Warszawa - Bielany $H_s = 98\,m$ $H_b = 99{,}5\,m$ $h_w = 15\,m$ Wrzesień - Septembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	POGODA
1	7	•	•	= na – a; ⌒² na
2	7	•	•	= na
3	7	•	•	= na; ⌒⁰ na
4	7	7.6	•	●⁰ 15¹⁵–17²⁵ ●²–17⁵⁵ ●⁰ – np; = na; ⌒⁰ na
5	7	0.0	•	●⁰ na – a; = na, np; ⌒¹ np
6	7	2.6	•	●⁰ np, ⌒² na – a
7	8	•	•	= na – a; ⌒¹ p – np
8	6	•	•	= na – a ∞ a – p = p – np; ⌒² na – a ⌒¹ p – np
9	8	•	•	= na – a, p – np; ⌒² na – a ⌒¹ p – np
10	7	6.3	•	●⁰ 15⁵⁰–55 ●¹–16⁰⁷ ●²–16⁰⁸ ●¹–16¹⁷ ●⁰–16²⁶; (K)⁰ 15⁵⁶–16⁰⁹ SW–NE K¹ 16⁰⁹ (K)⁰–16²⁵; = n – a, ⌒² n – a, ⌣ 20³⁰ – np
11	7	2.0	•	●¹ na, 7⁴⁵ 8³⁵–42 ●⁰–9⁴⁰ = n – a, p – np
12	8	•	•	●⁰ na; = na – a, p – np; ⌒² p – np
13	7	•	•	= n – a ∞ a – p; ⌒² n – a ⌒¹ p – np
14	7	2.1	•	●⁰ 12³³; = n – a ∞ a – p; ⌒⁰ n – a, p – np
15	9	•	•	● na; = n – a, ⌒⁰ p – np
16	8	•	•	= ⌒² n – a
17	7	•	•	= n – p, ⌒⁰ n – a ⌒¹ p – np
18	6	•	•	= n – a ∞ a – p; ⌒¹ n – a
19	7	0.0	•	●⁰ 12⁰⁰, p; ∞ n – a
20	8	0.0	•	●⁰ 15³⁰–40, ⌒⁰ na, np
21	8	•	•	= na – a; ⌒² na
22	7	•	•	= na, ⌒⁰ na
23	6	•	•	= na, ⌒⁰ na ⌒¹ np
24	6	•	•	= na ∞ a – p, ⌒² na ⌒¹ np
25	6	•	•	= na ∞ a – p, ⌒² na
26	7	0.0	•	= na, ⌒⁰ na
27	6	2.6	•	●⁰ na, 9⁴⁵ 11⁵⁰–12⁴⁰ ●²–⁰ 17³⁹–55; K² 17³⁸–18⁰⁵ SW–NE; = na – a
28	8	3.2	•	●⁰ na, 7¹⁵–30
29	5	27.1	•	●⁰ na – 6¹⁰ ●⁰–⁰ 8³²–17²⁸; = na – a, p – np
30	7	•	•	= na – a; ⌒² na – a, p – np
31				
Σ	–	53.5	–	

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1	7	•	•	= na – 6³⁰, ⌒⁰ na ⌒¹ p – np
2	8	•	•	= na – a, ⌒² na – a ⌒¹ p – np
3	7	•	•	= na – a, p – np, ⌒⁰ na – a, p – np
4	6	•	•	= n – a = a – n, ⌒¹ n – a ⌒² np
5	1	•	•	= n – a = a – n, p – np, ⌒² na ⌒⁰ a – p ⌒¹ np
6	3	•	•	= n – p = p – n; ⌒² n – a ⌒⁰ a – p, ⌣ p – np
7	8	•	•	= na = np, ⌒² na ⌒¹ np
8	6	•	•	= na = a; ⌒² na ⌒⁰ np
9	9	0.1	•	●⁰ 11¹⁰–14 p
10	9	0.1	•	●⁰ a ●⁰ 13³⁵–46
11	6	1.6	•	●⁰ 13⁵⁰–15²⁰ 16⁴⁰–45; = na; ⌒⁰ na
12	9	•	•	⌣⁰ na
13	8	•	•	
14	6	•	•	= na – p = ⁰10³⁰ – np
15	6	•	•	= ⁰ na – 6¹⁰ = – a, ⌣⁰ na
16	6	4.4	•	●⁰ 17⁴⁵ – np; = na – p
17	9	•	•	
18	7	0.5	•	●⁰ 20⁴²–55; = p – np
19	7	•	•	= na – a, p – np; ⌒² p – np
20	7	•	•	= na – a; ⌒² na – a, p – np
21	7	•	•	= na – a, p – np, ⌣² na – a ⌣⁰ p – np
22	7	•	•	= na – a; ⌣¹ na – a
23	6	0.1	•	= na – np
24	7	•	•	= n – a, ⌒⁰ n – a, p – np
25	7	0.0	•	∞ a – p
26	6	•	•	= ²⁻⁰ n – a = a – p
27	5	•	•	= n = 6²⁵ – a = a – p; ⌣¹ n – a
28	5	•	•	= n – p; ⌒¹ n – a
29	6	0.5	•	⁰¹ 10⁴²–47; = n – a
30	7	•	•	∞ a – p; ⌒⁰ n – a
31	7	0.5	•	⁰¹ 20⁰²–28
Σ	•	7.6	•	

Warszawa – Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ *Listopad – Novembre 1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.9	92.2	85.7	90.9	5.5	6.9	10.5	8.4	10.6	4.7	89	94	82	88	1.0	0.5	2.3	1.3	10	10 •	10	WSW 2	SSE 5	SW 6
2	85.1	86.1	88.3	85.8	10.8	11.1	7.5	9.2	12.2	7.2	73	51	60	61	3.6	6.4	4.2	4.7	9	4	3	SW 5	WSW 6	SW 6
3	92.6	94.9	96.4	94.6	6.2	9.2	6.3	7.0	9.5	4.8	70	54	72	65	2.8	5.4	2.6	3.6	10	4	10	WSW 7	W 6	SW 2
4	100.8	106.0	110.3	105.7	2.2	6.5	3.4	3.9	7.2	1.7	91	68	86	82	0.7	3.1	1.1	1.6	10	5	10	WSW 5	WSW 7	WSW 2
5	113.1	114.9	116.5	114.8	1.9	2.8	3.9	3.1	4.1	1.3	96	96	95	95	0.3	0.3	0.6	0.4	10	10	10	W 5	W 2	WSW 3
6	116.4	115.4	113.0	114.9	2.9	3.7	4.3	3.8	4.4	1.8	88	97	98	94	0.9	0.3	0.1	0.4	10	10 •	10 •	W 4	W 5	W 2
7	109.9	108.7	109.0	109.2	4.6	6.4	5.4	5.4	6.4	3.9	97	88	91	92	0.3	1.1	0.9	0.8	10	10	9	W 2	W 5	W 2
8	112.4	113.9	115.9	113.4	1.5	4.9	2.4	2.8	5.5	1.3	100	97	100	99	0.0	0.3	0.0	0.1	10 ≡	9 ≡	10 ≡	C 0	C 0	C 0
9	112.5	110.8	109.3	110.9	-1.1	4.0	2.3	1.9	5.4	-1.6	99	85	100	95	0.1	1.2	0.0	0.4	10 ≡	1	10 ≡	C 0	C 0	C 0
10	107.0	107.0	107.0	107.0	5.1	5.9	4.3	4.9	6.7	2.0	100	100	97	99	0.0	0.0	0.3	0.1	10 ≡	10 ≡	9	WNW 1	WNW 2	C 0
11	104.5	103.0	101.2	102.9	1.8	2.8	-0.3	1.0	4.5	-0.5	98	81	92	90	0.2	1.5	0.5	0.7	8	8	10	C 0	E 2	E 4
12	98.4	98.3	100.6	99.1	-1.7	-1.1	-2.1	-1.8	-0.2	-2.6	77	87	81	82	1.2	0.8	1.0	1.0	10	10 *	10 *	NW 6	NE 8	NE 6
13	102.5	103.2	104.2	103.3	-5.0	-3.9	-5.0	-4.7	-2.0	-5.8	83	78	76	79	0.7	1.0	1.0	0.9	10 *	9 *	10 *	ENE 5	NE 4	NE 4
14	105.7	104.2	104.8	104.2	-6.3	-5.3	-5.7	-5.8	-4.8	-6.6	83	82	90	85	0.6	0.7	0.4	0.6	10 *	10 *	10 *	ENE 4	ENE 8	ENE 2
15	105.2	106.2	109.4	106.9	-6.7	-6.0	-7.2	-6.8	-5.5	-8.7	99	92	96	96	0.0	0.3	0.1	0.1	10 *	10 *	10 *	NE 1	ENE 3	C 0
16	114.1	115.9	117.8	115.9	-8.3	-6.6	-10.9	-9.2	-6.2	-11.1	95	80	94	90	0.2	0.7	0.2	0.4	10 *	5	9	NE 1	NE 1	C 0
17	117.0	115.9	113.0	115.3	-10.1	-9.3	-10.7	-10.2	-8.7	-12.3	91	82	87	87	0.3	0.5	0.4	0.4	10	10	10 *	C 0	SW 2	E 4
18	109.0	106.2	102.1	105.8	-13.5	-11.0	-12.4	-12.3	-10.4	-15.1	92	80	81	84	0.2	0.5	0.4	0.4	10	6	10	E 3	E 4	E 5
19	96.5	94.3	91.3	94.0	-9.7	-6.8	-2.8	-5.5	-2.6	-12.8	91	91	95	92	0.3	0.3	0.2	0.3	10	10 *	10 *	ESE 5	ESE 3	C 0
20	91.2	92.9	92.7	92.3	-4.5	-4.3	-4.0	-4.2	-1.7	-4.7	93	94	91	93	0.3	0.3	0.4	0.3	10	10	10	C 0	C 0	C 0
21	87.1	80.9	74.2	80.7	-3.1	0.4	0.5	-0.4	0.9	-4.2	97	100	100	99	0.1	0.0	0.0	0.0	10	10 * ≡	10 • ≡	ENE 2	E 3	C 0
22	82.9	90.6	96.3	90.6	-5.5	-2.4	-5.3	-4.6	2.8	-5.9	87	89	93	90	0.5	0.5	0.3	0.4	10 *	10 *	2	W 3	W 3	W 2
23	103.6	107.1	109.7	106.8	-8.9	-8.4	-11.5	-10.1	-5.2	-11.8	86	77	86	83	0.4	0.7	0.4	0.5	9	2	2	W 4	W 4	W 2
24	111.2	109.2	106.8	109.1	-11.9	-8.4	-9.5	-9.8	-7.6	-13.8	86	89	91	89	0.4	0.3	0.3	0.3	10	3	9	S 1	S 3	SE 5
25	104.9	104.5	104.6	104.7	-6.4	-2.7	-1.8	-3.2	-1.6	-10.1	89	78	90	86	0.4	1.1	0.5	0.7	10	10	10	SSE 5	SE 6	SSE 3
26	99.0	93.4	91.8	94.7	-4.0	-1.5	0.5	-1.1	1.1	-4.7	80	68	79	76	0.9	1.8	1.3	1.3	7	8	10 *	SE 6	SSE 8	S 4
27	92.7	87.0	75.5	85.1	-1.7	0.0	2.1	0.6	2.3	-2.6	94	96	87	92	0.3	0.2	0.9	0.5	7	10 *	10	SW 1	ESE 5	SSE 5
28	74.4	76.3	81.9	77.5	2.7	1.7	0.6	1.4	3.8	0.4	91	89	94	91	0.6	0.8	0.4	0.6	10	10	10 *	S 2	WSW 3	SW 6
29	86.3	92.3	91.1	89.9	1.4	1.7	1.3	1.4	2.2	0.4	91	92	79	87	0.7	0.5	1.4	0.9	10 *	10	0	SW 7	W 2	SE 3
30	81.7	83.4	86.7	83.9	2.5	4.5	2.6	3.0	4.7	0.1	75	70	96	80	1.8	2.5	0.3	1.5	9	10	10 •	SE 6	SSE 5	SSW 1
M	100.4	100.5	100.2	100.4	-2.0	-0.2	-1.0	-1.0	1.3	-3.5	89	84	89	87	0.7	1.1	0.8	0.9	9.6	8.1	8.8	3.1	3.7	2.6

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DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.8	86.0	90.1	87.6	0.4	3.3	2.9	2.4	3.6	0.2	86	68	79	78	0.9	2.5	1.6	1.7	1	10	9	SW 4	SSW 7	SSW 7
2	93.2	95.4	95.0	94.5	1.4	1.1	1.3	1.3	3.6	0.5	98	92	91	94	0.2	0.5	0.6	0.4	10 •	10 • △	4	SW 5	W 5	WSW 1
3	88.1	88.0	87.7	87.9	0.0	1.6	1.5	1.2	2.1	-1.1	82	69	78	76	1.1	2.2	1.5	1.6	10	10	10	SSW 4	SSE 4	SSE 1
4	86.5	89.0	91.9	89.1	0.4	2.0	0.9	1.0	2.8	-0.5	100	91	92	94	0.0	0.7	0.5	0.4	10	9	0	WSW 1	WSW 2	SW 1
5	93.0	93.0	83.0	89.7	0.2	3.0	2.1	1.8	3.2	-1.7	88	88	75	84	0.7	0.9	1.8	1.1	10	8	10	SW 2	S 2	S 8
6	79.2	82.8	88.2	83.4	5.0	6.9	6.0	6.0	7.3	0.6	87	61	66	71	1.1	3.8	3.3	2.7	9	7	8	SW 3	SW 6	SW 8
7	93.4	96.1	98.5	96.0	3.1	4.3	3.3	3.5	6.5	2.5	78	69	78	75	1.7	2.6	1.7	2.0	6	8	9	SSW 5	WSW 8	WSW 3
8	99.5	100.7	103.6	101.3	2.0	3.0	1.4	2.0	3.6	0.9	82	81	92	85	1.3	1.5	0.6	1.1	6	10	10	SW 2	W 2	WNW 2
9	106.3	102.0	91.3	99.9	0.0	2.5	2.5	1.9	3.2	-0.7	86	65	58	70	0.9	2.6	3.1	2.2	3	8	10 *	SW 2	SW 2	SW 8
10	76.4	73.4	72.7	74.2	2.9	5.7	4.5	4.4	6.4	1.9	57	71	81	70	3.2	2.7	1.6	2.5	9	10	4	S 6	SSE 7	SSE 6
11	77.4	80.4	82.4	80.1	3.4	3.5	2.0	2.7	5.2	1.8	86	73	75	78	1.1	2.1	1.8	1.7	9	9	9	SW 3	WSW 4	SW 3
12	86.7	89.8	92.8	89.8	1.4	0.9	-0.1	0.5	2.3	-0.6	89	81	80	83	0.8	1.2	1.2	1.1	10	10	10	W 1	W 2	NW 1
13	95.8	97.7	98.2	97.2	-1.3	-0.8	-2.8	-1.9	0.5	-3.7	98	83	95	93	0.2	0.9	0.2	0.4	10 *	4	9	W 1	NNW 3	C 0
14	101.6	105.8	110.1	105.8	-2.9	-3.3	-4.9	-4.0	-2.4	-5.1	77	63	76	72	1.1	1.8	1.0	1.3	8	4	0	NW 2	NW 4	W 4
15	108.6	106.3	110.0	108.3	-4.3	-2.5	-5.0	-4.2	-2.0	-6.3	94	95	93	94	0.3	0.3	0.3	0.3	10 *	10	9	SW 3	SW 2	ENE 2
16	110.3	110.0	110.2	110.2	-8.9	-8.9	-12.3	-10.6	-4.7	-12.7	92	92	93	92	0.3	0.3	0.2	0.3	10	10	10 ≡	WSW 2	WSW 2	C 0
17	109.2	106.6	104.8	106.9	-14.6	-11.5	-6.0	-9.5	-5.7	-16.4	87	90	94	90	0.3	0.3	0.2	0.3	10	9	10 *	C 0	E 2	C 0
18	104.2	101.4	98.0	101.2	-3.4	0.8	2.4	0.6	2.6	-6.2	97	90	98	95	0.2	0.7	0.2	0.4	10	10	10 •	SE 3	SE 5	SSW 3
19	97.8	98.1	96.6	97.5	8.3	9.2	8.6	8.7	9.5	2.4	94	92	96	94	0.7	0.9	0.3	0.7	10 •	10 •	10 •	SW 6	SW 5	SW 7
20	101.3	104.2	104.3	103.3	4.6	4.9	2.2	3.5	9.6	2.0	84	81	91	85	1.4	1.7	0.7	1.3	9	4	0	W 4	W 3	SW 2
21	100.5	98.9	101.1	100.2	1.0	2.0	1.8	1.6	2.4	0.0	100	98	98	99	0.0	0.2	0.2	0.1	10	10 •	10 •	C 0	C 0	NNW 2
22	104.8	106.4	107.1	106.1	-0.1	0.3	-0.5	-0.2	2.2	-0.7	94	96	90	93	0.4	0.2	0.6	0.4	9	10	9	NW 1	NW 3	C 0
23	106.2	104.3	99.4	103.3	-1.4	-0.7	-3.1	-2.1	0.2	-3.4	94	83	84	88	0.3	0.9	0.8	0.7	9	10	0	C 0	NE 1	SE 3
24	92.7	89.9	86.1	89.6	-1.0	0.3	0.0	-0.2	0.6	-4.0	83	82	84	83	1.0	1.1	1.0	1.0	9	9	7	SSE 6	SSE 5	SE 4
25	81.7	79.0	78.2	79.6	-0.7	0.9	1.1	0.6	1.3	-1.1	83	73	83	81	0.9	1.6	1.1	1.2	9	9	9	SE 6	SE 4	SE 3
26	77.7	79.8	83.6	81.0	0.2	1.7	0.7	0.8	2.1	-0.4	86	89	96	90	0.9	0.8	0.2	0.6	10	10 •	10 *	SE 2	S 1	W 2
27	91.6	91.6	86.8	90.0	0.7	1.4	1.4	1.2	2.4	-0.1	94	83	78	85	0.4	1.1	1.9	1.1	10	9	10	W 2	SW 1	S 4
28	82.1	83.9	92.0	86.0	0.1	0.3	-1.1	-0.4	1.8	-1.3	98	98	87	94	0.2	0.1	0.8	0.4	10 * ≡	10 * ≡	10	C 0	C 0	W 2
29	95.5	97.1	99.5	97.4	-1.5	-0.7	-1.5	-1.3	-0.2	-2.0	84	95	88	88	0.9	0.4	0.7	0.7	10	10 *	10	SW 3	W 3	W 3
30	98.5	95.3	92.3	95.4	-1.8	-1.8	0.8	-0.3	1.1	-3.0	83	73	75	77	0.9	1.4	1.6	1.3	8	9	10	W 6	S 3	SW 4
31	92.8	93.0	93.1	93.0	1.7	2.4	2.1	2.1	2.7	0.8	89	86	91	89	0.8	1.1	0.6	0.8	10	10	10	SW 4	SW 3	ENE 2
M	94.2	94.4	94.3	94.4	-0.2	1.0	0.4	0.4	2.4	-1.9	88	82	85	85	0.8	1.3	1.0	1.0	8.8	8.9	7.9	2.9	3.3	3.2

Warszawa - Bielany $H_s = 98\,m$ $H_b = 99{,}5\,m$ $h_w = 16\,m$ *Listopad - Novembre* 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY SNIEGU h	POGODA
1	5	4.0	•	$\bullet^{0}10^{30}-19^{35}$; $=$ na $-$ p
2	9	0.5	•	$\bullet^{0}\,7^{35-50}$
3	9	0.0	•	$\bullet^{0}\,21^{05-15}$
4	7	•	•	$=$ na $-$ a; $\frown^{0}$ na
5	5	•	•	$=$ na $-$ p; $\frown^{0}$ na
6	5	1.0	•	$\bullet^{0-2}$ a $-$ np; $=$ na $-$ np
7	5	0.1	•	$=$ na $-$ p
8	3	•	•	$\bullet^{0}$ na; $\equiv^{1-0}$ na $-$ p $=$ p $\equiv^{0-2}$ p $-$ np
9	4	0.2	•	$\equiv^{2}$ na $-$ a $=$ a $-$ p $\equiv$ p $-$ np; $\frown^{2}$ na $-$ a
10	3	0.1	•	$\bullet^{0}$ na, a; $\equiv^{1}$ na $-$ p
11	6	•	•	$=$ na $-$ np
12	6	0.1	•	$*^{0}$ a $-$ np
13	7	0.0	•	$*^{0}$ na $-$ p
14	6	1.9	1	$*^{0}$ na $-$ np; $=$ na $-$ p
15	1	5.2	7	$*^{0}$ n $-$ n; $\equiv^{2}$ n $-$ p
16	7	0.2	13	$*^{0}$ n $-$ a; $=$ n $-$ a, p $-$ n; $\smile^{0}$ p $-$ np
17	6	0.1	12	$*^{0}$ n, 6^{42}... np
18	6	1.1	11	$=$ n $-$ p; $\smile^{0}$ n $-$ a
19	5	3.7	11	$*^{0}$ n, 7^{10} $-$ n; $=$ n $-$ p; $\smile^{0}$ n $-$ a
20	4	•	13	$=$ n $-$ np
21	2	8.8	12	$*$ a $\triangle$ a $-$ p $*^{0}$ p $-$ 13^{50} $\bullet^{0}$ $-$ n; $=$ n $-$ a $\equiv$ a $-$ p
22	5	1.1	13	$*^{0}$ na... p; $=$ na $-$ p
23	7	•	13	$\smile^{0}$ na $-$ np
24	5	•	12	$=$ na; $\smile^{1}$ na $-$ a $\vee^{0}$ a $-$ p $\smile^{0}$ p $-$ np
25	7	0.6	12	$*^{0}$ 13^{05} $-$ 16^{20}
26	7	0.1	12	$*^{0}$ 17^{15} $-$ np
27	5	2.8	12	$*^{0}$ a $-$ p $\bullet^{0}$ 20^{50} $-$ np; $=$ na $-$ p; $\smile^{0}$ na
28	6	0.2	6	$*^{0}$ 18^{50} $-$ np; $=$ na $-$ p
29	6	0.4	3	$*^{0}$ na $-$ a; $=$ a $-$ p
30	7	5.4	3	$\bullet^{0}$ na, 12^{50}, 13^{55} $-$ np
31				
Σ	-	37.6	-	

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1	8	1.2	•	$*^{0}$ a $\bullet^{0}$ p
2	5	1.6	•	$\bullet^{0}$ na $-$ a $\bullet\triangle^{0}$ a $-$ p $*^{0}$ p; $=$ na $-$ np; $\smile^{0}$ p $-$ np
3	6	6.0	•	$=$ na $-$ a ∞ a $-$ p $=$ p $-$ np; $\smile^{0}$ na $-$ a
4	5	•	5	$*^{1}$ na; $=$ na $-$ np; $\smile^{0}$ p $-$ np
5	6	7.0	3	$=$ na $-$ p; $\smile^{0}$ na $-$ a
6	7	0.9	pł.	$\bullet^{1}$ n $\bullet^{0}$ 0^{55-56} $\bullet^{0}$ 20^{45} $-$ 21^{10}, 22^{10-18}
7	7	•	•	
8	6	•	•	$=$ na $-$ np; $\smile^{0}$ na $-$ a
9	6	0.0	•	$*^{0}$ 20^{20-40}; $=$ na $-$ a ∞ a $-$ p; $\smile^{0}$ na $-$ a
10	7	0.0	•	$\bullet^{0}$ a $\bullet^{0}$ p
11	7	0.0	•	∞ a $-$ p
12	6	0.6	•	$\bullet^{0}$ na $\bullet$ a; $=$ a $-$ p
13	7	0.0	2	$*^{0}$ na... a; $\smile^{0}$ np
14	8	0.9	1	$*^{0}$ 8^{15} $-$ 10^{20}, 14^{20} $-$ 15^{10}
15	5	3.1	2	$*^{0-1}$ na $-$ a; $=$ na $-$ p
16	4	•	10	$=$ na $-$ a $\equiv^{0}$ p $-$ np; $\vee^{0}$ na $-$ a $\vee^{1}$ a $-$ np
17	4	0.1	6	$*^{0}$ p $-$ n; $=$ n $-$ n; $\vee^{2}$ n $-$ p
18	4	17.9	5	$\bullet^{0}$ 13^{55} $-$ np; $=$ na $-$ np; $\vee^{0}$ na $-$ a
19	5	4.3	•	$\bullet^{0}$ na $-$ 10^{55} $\bullet^{0}$ $-$ 13^{00} $\bullet^{0}$ 18^{05} $-$ np; $=$ a $-$ np
20	7	•	•	$\frown^{1}$ a $-$ p $\frown^{0}$ p $-$ np
21	4	4.5	•	$\bullet^{0}$ 8^{45}... np; $=$ na $-$ np; $\frown$ na $-$ a
22	6	0.0	•	$\triangle^{0}$ a $-$ 12^{42}; $=$ a $-$ p; $\smile^{0}$ n $-$ a
23	6	•	•	$=$ a $-$ p; $\frown^{0}$ a $-$ p $\smile^{0}$ p $-$ np
24	7	0.1	•	$\smile$ na $-$ a
25	6	0.0	•	$*^{0}$ na, p; $\equiv$ na $-$ p
26	6	5.9	•	$*^{0}$ na $\bullet^{0}$ 12^{25} $-$ p $\bullet^{0}$ p $-$ np; $=$ na $-$ p
27	6	4.4	1	$=$ a $-$ p; ∞ n $-$ a, p $-$ np
28	5	1.5	6	$*^{0-1}$ n $-$ 8^{31} $*$... p; $\equiv^{2}$ n $-$ p
29	6	0.2	7	$*^{0}$ 9^{55}... p; $=$ a $-$ p
30	6	0.0	7	$=$ a $-$ p
31	6	0.0	5	$\bullet^{0}$ na $\bullet^{0}\bullet^{0}$ a; $=$ p $-$ np
Σ	-	58.0	-	

DNI	CIŚNIENIE p = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	81.8	81.8	81.2	81.6	2.0	2.4	1.2	1.7	3.4	0.5	85	84	83	84	1.1	1.2	1.2	1.2	10 ●	10 ●	9	SW 7	SW 7	SSW 5
2	78.2	78.1	79.9	78.7	0.8	1.4	0.2	0.6	1.7	0.0	92	91	96	93	0.5	0.7	0.3	0.5	10	10	9	SSW 5	WSW 3	SW 2
3	82.4	84.4	86.4	84.4	-1.2	-0.3	0.1	-0.3	0.3	-1.4	99	98	96	98	0.1	0.2	0.3	0.2	10 ≡	10 ≡	10	SW 2	NNW 1	N 1
4	90.2	93.6	97.9	93.9	-1.2	0.0	-0.8	-0.7	0.5	-1.5	93	81	85	86	0.4	1.2	0.9	0.8	10	9	10	NNE 4	N 6	NW 6
5	93.4	90.7	94.3	92.8	-3.2	0.3	0.6	-0.4	0.9	-3.9	86	93	80	86	0.7	0.4	1.3	0.8	9	10 *	8	WSW10	W 10	WNW 9
6	96.4	97.3	97.2	97.0	-1.6	-1.3	-3.4	-2.4	0.7	-3.6	88	74	79	80	0.8	1.4	1.0	1.0	9	8	9	NW 8	NW 8	NW 9
7	98.8	99.2	96.6	98.2	-5.0	-2.8	-7.3	-5.6	-2.5	-7.8	83	82	85	83	0.7	0.9	0.5	0.7	10 *	9	0	NW 7	WNW 6	S 2
8	88.6	84.4	78.1	83.7	-4.8	0.3	2.1	-0.1	2.2	-7.8	86	92	95	91	0.6	0.5	0.4	0.5	10	10	10 ●	SW 5	SW 6	SW 8
9	79.8	81.0	81.7	80.8	3.6	3.6	0.8	2.2	4.4	0.7	95	91	96	94	0.4	0.7	0.3	0.5	10	10	10 ●	W 8	WNW 6	W 3
10	79.5	81.8	96.9	86.1	0.0	1.0	-6.8	-3.2	1.7	-6.9	90	90	75	85	0.6	0.7	0.9	0.7	10	10	8	S 1	N 4	NNE 4
11	103.1	102.2	99.5	101.6	-10.8	-4.8	-7.6	-7.7	-4.1	-11.4	76	75	79	77	0.6	1.0	0.7	0.8	1	8	0	SE 5	SE 6	SE 7
12	96.8	95.2	93.2	95.1	-5.1	-0.6	-2.4	-2.6	0.8	-8.1	78	74	76	76	0.9	1.5	1.2	1.2	0	9	0	SSE 6	S 7	SSE 5
13	93.1	93.6	94.9	93.9	-2.4	1.9	0.0	-0.1	2.4	-3.8	70	66	80	72	1.5	2.4	1.2	1.7	0	6	10	S 8	SSW 6	S 2
14	92.7	89.6	92.7	91.7	-2.8	0.4	0.0	-0.6	0.9	-3.5	82	70	82	78	0.9	1.9	1.1	1.3	2	1	9	S 5	S 6	SW 7
15	98.6	99.0	97.5	98.4	-1.0	3.0	-1.2	-0.1	3.7	-1.3	83	67	85	78	1.0	2.5	0.8	1.4	4	3	8	SW 7	SW 6	SE 3
16	93.9	94.7	94.0	94.2	0.3	1.4	-1.2	-0.2	1.6	-1.9	81	74	93	83	1.1	1.8	0.4	1.1	10 *	9	0	S 6	SW 5	SSW 6
17	82.5	77.9	71.4	77.3	0.6	2.9	3.3	2.5	3.3	-2.8	76	71	79	75	1.6	2.2	1.5	1.8	10	9	10	SSW10	SW 10	SSW10
18	72.9	72.6	71.5	72.3	1.7	4.0	0.6	1.7	4.4	0.4	81	67	79	76	1.3	2.6	1.4	1.8	10	8	0	SSW 7	SW 7	SSW 6
19	71.0	72.2	74.2	72.5	0.0	3.4	-0.8	0.4	4.4	-1.2	78	58	81	72	1.3	3.3	1.1	1.9	9	3	6	SSW 4	S 2	SSE 2
20	74.8	71.4	68.6	71.6	-1.5	-0.8	-1.1	-1.1	-0.3	-2.7	82	93	95	90	1.0	0.4	0.3	0.6	9	10 *	10 *	E 2	NE 6	ENE 5
21	69.7	73.9	79.4	74.3	-1.0	-0.3	-0.5	-0.6	0.0	-1.4	97	94	94	95	0.2	0.4	0.4	0.3	10 ≡	10	10	WNW 2	WNW 2	W 1
22	82.6	84.8	88.6	85.3	-0.6	0.7	-4.8	-2.4	1.7	-5.1	91	81	93	88	0.5	1.2	0.3	0.7	10 *	0	0 ≡	SW 5	SW 1	ESE 2
23	91.9	93.8	97.5	94.4	-5.6	-0.4	-3.2	-3.1	0.3	-6.3	90	86	93	90	0.4	0.8	0.3	0.5	0	10	5	ESE 3	SE 2	NNE 2
24	100.9	101.7	101.2	101.3	-3.4	-2.6	-1.6	-2.3	-1.6	-4.2	94	95	96	95	0.3	0.2	0.2	0.2	10 ≡	10	10 *	N 2	NW 2	NNW 1
25	96.8	94.8	93.8	95.1	-2.2	-1.0	-1.5	-1.6	-0.8	-2.8	96	89	92	92	0.2	0.7	0.4	0.4	10 *	10 *	10	NNW 2	WNW 3	SW 2
26	92.3	91.5	91.9	91.9	-2.1	-0.8	-3.2	-2.3	0.1	-3.5	89	81	88	86	0.5	1.1	0.6	0.7	10	10	2	SE 4	SE 5	SE 4
27	91.8	92.5	91.8	92.0	-3.8	-2.4	-2.0	-2.6	-1.6	-4.9	92	87	94	91	0.4	0.7	0.4	0.5	10	10 *	10 *	ESE 6	SE 6	SE 5
28	91.7	91.7	90.3	91.2	-0.6	0.2	1.0	0.4	1.1	-2.6	91	90	87	89	0.5	0.6	0.9	0.7	10	10	9	SE 6	SE 6	SE 6
29	87.7	87.0	87.8	87.5	2.2	2.9	-0.8	0.9	3.9	-1.5	80	79	96	85	1.5	1.6	0.3	1.1	9	8	0 ≡	S 5	SSE 5	C 0
30	87.1	85.1	83.8	85.3	0.2	2.2	2.2	1.7	3.4	-1.5	94	87	91	91	0.4	1.0	0.7	0.7	10	10	10	SE 3	SE 3	SW 3
31	89.3	91.6	90.8	90.6	-0.6	-1.1	-1.9	-1.4	2.3	-2.1	95	87	92	91	0.3	0.8	0.4	0.5	10	10	8	N 4	E 2	SE 3
M	88.1	88.0	88.5	88.2	-1.6	0.4	-1.3	-1.0	1.3	-3.4	87	82	88	86	0.7	1.2	0.7	0.9	8.1	8.4	6.8	5.1	5.0	4.2

Luty - Février

1	92.0	92.3	95.2	93.2	-3.8	-2.2	-2.2	-2.6	-1.6	-3.9	92	85	83	87	0.4	0.8	0.9	0.7	10 △	10 *	9	NW 5	NW 6	WNW 8
2	99.1	100.5	105.0	101.5	-6.0	-3.7	-4.1	-4.5	-2.1	-7.7	84	87	82	84	0.6	0.6	0.8	0.7	3	9 *	7	NW 6	NW 9	NW 7
3	102.6	100.3	99.1	100.7	-6.0	-2.6	-2.8	-3.8	-1.8	-10.5	92	85	91	89	0.3	0.8	0.5	0.5	10 *	9	10 *	SW 2	WNW 8	WNW 6
4	99.3	99.2	100.7	99.7	-2.6	-1.4	-8.8	-5.4	-0.4	-9.2	91	94	74	86	0.5	0.3	0.8	0.5	10 *	10 *	0	WNW 5	NW 7	NNE 5
5	97.2	97.1	100.9	98.4	-14.6	-10.7	-14.6	-13.6	-8.8	-19.2	83	70	83	79	0.3	0.8	0.3	0.5	0	0	0	ESE 3	E 5	N 4
6	103.7	101.8	98.6	101.4	-19.8	-10.0	-8.8	-11.8	-8.8	-21.0	89	74	77	80	0.1	0.7	0.7	0.5	2	9	10 *	S 1	WNW 4	SSW 4
7	97.1	96.0	84.9	92.7	-14.8	-5.6	-4.4	-7.3	-4.4	-15.3	82	62	79	74	0.3	1.5	0.9	0.9	0	0	10 *	SE 4	SSW 3	SW 8
8	74.8	76.8	83.2	78.3	-4.2	-2.8	-5.8	-4.6	-0.3	-6.0	82	82	87	84	0.8	0.9	0.5	0.7	4	8	9 *	NNW12	NW 12	N 10
9	91.9	96.2	99.8	96.0	-8.4	-8.8	-15.4	-12.0	-5.6	-15.5	86	71	91	83	0.4	0.9	0.2	0.5	10 *	9	1	N 6	N 7	W 1
10	93.4	87.7	87.5	89.5	-9.4	-5.2	-1.4	-4.4	-1.3	-16.6	95	90	92	92	0.2	0.4	0.4	0.3	9	10 *	10	SW 8	WSW10	WNW 6
11	92.3	94.5	97.4	94.7	-9.2	-1.4	-4.1	-4.7	-0.2	-10.4	88	74	84	82	0.4	1.4	0.7	0.8	0	1	0	WNW 5	NW 8	NW 5
12	97.5	96.1	94.6	96.1	-5.9	-0.2	0.9	-0.6	0.9	-6.2	92	86	96	91	0.4	0.8	0.2	0.5	10	10 △	10	SW 5	SW 7	W 5
13	86.9	81.8	75.4	81.4	0.2	1.2	1.4	1.0	2.2	-1.1	81	87	89	86	1.2	0.9	0.8	1.0	10	10	10 ●*	SW 8	SW 8	SW 12
14	71.0	71.4	80.0	74.1	1.0	0.4	0.0	0.4	1.9	-0.2	77	82	80	80	1.6	1.1	1.2	1.3	8	8	9	SW 12	WNW10	W 6
15	85.2	86.8	87.5	86.5	-2.0	-1.0	-3.2	-2.4	0.5	-4.3	83	77	86	82	0.9	1.3	0.7	1.0	9	5	10 *	W 6	WSW 5	SW 3
16	89.4	91.7	94.2	91.8	-5.4	-4.2	-6.3	-5.6	-2.3	-7.5	90	75	89	85	0.4	1.1	0.4	0.6	10	9	10	NNE 4	NNW 3	N 5
17	92.3	91.4	94.4	92.7	-6.6	-3.6	-0.8	-3.0	-0.2	-8.5	91	85	87	88	0.3	0.7	0.7	0.6	10 *	10 *	10 *	NNW 8	NNE 9	E 4
18	96.3	98.2	99.3	98.0	-4.2	-4.6	-6.0	-5.2	-0.7	-6.1	87	79	79	82	0.6	0.9	0.8	0.8	10 *	10	10	NE 9	NNE 9	NE 6
19	99.6	101.0	103.2	101.3	-4.8	-6.2	-5.9	-5.7	-4.5	-7.3	88	84	74	82	0.5	0.6	1.0	0.7	10	8	9	N 7	NNE 7	NE 7
20	105.8	107.8	108.9	107.5	-6.4	-4.0	-7.2	-6.2	-3.2	-8.1	81	75	82	79	0.7	1.1	0.6	0.8	10 *	10 *	0	E 6	ENE 4	E 2
21	104.9	102.5	96.8	101.4	-8.0	-4.6	-5.2	-5.8	-3.9	-10.6	87	86	80	84	0.4	0.6	0.8	0.6	10	10	10	C 0	NW 4	W 7
22	89.2	91.2	93.4	91.3	-4.0	-2.0	-9.0	-6.0	-1.8	-9.2	91	86	95	84	0.4	1.8	0.2	0.8	10 *	6	0	WNW 7	N 7	WNW 3
23	92.7	91.8	92.4	92.3	-10.9	-3.8	-6.4	-6.9	-2.8	-13.6	90	66	91	82	0.3	1.5	0.3	0.7	9	9	10 *	SSW 2	WNW 5	WNW 2
24	94.9	92.7	86.1	91.2	-15.4	-7.4	-9.8	-10.6	-5.1	-16.1	86	85	88	86	0.3	0.5	0.4	0.4	10 ≡	2	2	W 1	NW 2	SW 5
25	80.8	83.1	85.3	83.1	-3.3	-5.0	-10.0	-7.1	-3.3	-10.4	88	56	62	69	0.6	1.8	1.1	1.2	10 *	10	0	NW 7	NW 9	NW 5
26	87.6	85.8	78.5	84.0	-9.2	-5.5	-3.8	-5.8	-3.1	-13.0	88	80	62	77	0.4	0.8	1.7	1.0	9	10 *	10	W 5	SW 5	SW 9
27	70.6	69.5	76.8	72.3	-4.4	-4.0	-5.8	-5.0	-1.8	-6.5	89	84	77	83	0.5	0.7	0.9	0.7	10 *	10 *	9	SW 9	WNW10	W 9
28	86.3	89.4	90.2	88.6	-10.5	-5.6	-11.0	-9.5	-4.6	-11.2	87	64	66	72	0.4	1.4	0.9	0.9	2	2	0	W 8	WNW 8	ESE 4
29																								
30																								
31																								
M	92.0	92.0	92.5	92.2	-7.0	-4.1	-5.7	-5.6	-2.4	-9.6	87	78	82	82	0.5	1.0	0.7	0.7	7.7	7.8	6.6	5.8	6.8	5.6

Łódź-Lublinek

$H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 10\,m$ Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	6	1.0	pł.	●0 00... 1 10_5 08 6 07_8 35 12 32_13 40 = 0 00_24
2	5	0.0	pł.	●0 20_4 05 13 15_14 05 17 42_18 26; = 0 00_21 45 ≡0_23 30 ≡0_24
3	2	0.1	pł.	*0 22 40_24; ≡0 00_2 15 = _3 30 ≡0_4 15 ≡1_16 50 ≡0_17 40 = _24
4	6	.	1	*0 00_2 50; = 0 00_19 30
5	6	0.5	pł.	*0 8 35_9 05 *1_12 30 *0_13 15...35; +0 11 30_12 30; ≫6 30_14 40
6	8	0.0	2	*0 23 40_24; ≫7 35_8 30
7	7	0.2	2	*0 00_05 35_2 00 6 35_11 10 ⚥0 11 30_12 05
8	5	4.6	3	*0 5 05_6 32 8 10_20 *1_8 35 *0_8 50 ●0 16 20_24; = 6 30_9 45 ≡0_10 25 ≡1_11 10 ≡0_11 45 = _24
9	5	6.2	pł.	●0 00_3 40 4 20_5 35 16 45_21 00 *0_21 15 *0_22 40 ●0 23 50_24 = 0 00_24
10	5	0.1	.	●0 00_2 30 *0_3 30 *0 8 45...9 35_11 40 ●0_12 18 ●0 *0 13 01-30 ●0_13 43 *0 14 15_15 40; = 0 00_18 40
11	7	.	.	
12	6	.	.	= 7 10_24
13	6	.	.	= 0 00_24
14	6	0.0	.	*0 23 10_24; = 0 00_24
15	6	0.0	.	*0 0 00-10; = 0 00_24; ⌴0 4 30_10 30; ⊽20 50_23 30
16	6	0.0	.	*0 1 18_3 00...20 6 40_7 10 18 20 20 03; = 0 00_24
17	6	0.6	.	*0 7 00_8 20 *1_8 40 *0_9 10...42 ●0 13 36-45 14 10-45 23 44_24; ≫5 35_24 (por. 17 m/sek); = 0 00_19 30
18	7	.	.	●0 0 00...36; ≫0 00_2 45
19	7	.	.	= 5 30_12 10 16 45_24
20	5	1.0	.	*0 11 30_14 00 *1_14 50 *0_15 30 *1_15 15 *0_22 20 △0_24; = 0 00_24; ⌴0 2_11 30
21	5	0.0	3	△0 0 00_1 45; 16 43_17 40; = 0 00_5 40 ≡0_6 35 ≡1_9 20 ≡0_9 25 = _24
22	5	0.1	2	*0 2 45_10 35 11 40; = 0 00_18 50 ≡1_10 30 ≡2_22 25 ≡1_22 40 ≡0_24; V0 20 45_24
23	5	.	3	≡0 0 00_2 45 = _23 50 ≡0_24; V0 0 00_2 45
24	4	3.0	2	*0 17 50 18 05-35 *1_22 15 *0_24 ≡0 0 00_1 15 ≡1_1 30 ≡1_4 30 ≡0_5 30 ≡0_7 20 ≡1_7 40 ≡0_10 20 = _24
25	5	1.7	8	*0 0 00_8 15 *1_9 34 *0_13 40; = 0 00_24
26	5	1.0	11	*0 8 02_9 40 △0_11 40; = 0 00_22 40 ≡1_23 35 ≡0_24; V0 22 45_24
27	5	2.2	12	*0 0 15 1 40 8 45 10 40 12 20 13 47 17 45_23 35; +0 21 35_23 35; ≡0 00-10 = _24; V0 0 00-10
28	6	.	15	△0 0 40_1 30 *0_3 40; = 0 00_24
29	6	.	9	= 0 00_20 25 ≡1_21 15 ≡1_21 30 ≡0_22 40 = _24
30	4	0.2	4	●0 15 10; 19 00_22 35_24; = 0 00_24
31	5	0.0	pł.	●0 0 00-30; = 0 00-50 ≡0_21 15 = _24
Σ	-	22.5	-	Uwaga. Wartości ciśnienia powietrza w ciągu całego roku są za niskie przeciętnie o ok. 0,5 mb.

Luty - Février

1	5	0.4	pł.	△0 6 41_8 10 *0_8 16 *1_9 15 *0_10 01 *1_10 13 *0_11 40 12 10-49 *1_12 58 *0_14 38 16 10 ⚥0_16 40 X0 18 20-28 ⚥0 21 45_22 50 *0 23 00_24; = 0 00_18 15
2	6	0.1	4	*0 0 00 4 45 10 43 12 20 ⚥0-1_14 30 *0_15 20 15 41_16 27
3	6	0.7	6	*0 5 45_8 10 *1_8 45 *0_9 40 10 35 11 35 *1 14 25_15 15 *0_20 03 *1_20 21 *0_21 15 24; = 5 30_24
4	5	0.3	8	*0 0 00 1 45 6 15 9 10_12 13 *1_13 40 *0_15 43 17 28; = 0 00_17 40 23 30_24
5	6	0.0	10	*0 8 10_9 00; = 0 00_24; ⌴0 1 30_8 10
6	6	0.1	7	*0 18 45 20 20...24; = 0 00_24
7	5	2.2	8	*0 0 00_1 35 19 40_24; +0 23 45_24; = 0 00_24
8	8	0.4	18	*0 0 00_1 10 *1_4 15 *0_4 40 ⚥0 16 43 17 48 ⚥1_17 50 ⚥0_19 15 19 40_21 15 23 30_24 +0 0 00_1 10 +1_2 35 +1_3 40 +0_11 10 +1_13 50 +0_16 45 +1_24; ≫0 35_24; = 0 00_5 30
9	6	0.0	23	⚥0 0 00_2 15 2 45 3 00 3 35 4 30 *0 5 35_7 30 8 05 11 20 ⚥0 13 02_15 20; +1 0 00_1 00 +0_5 30; ≫0 00_1 30; ∞12 30_15 00 = 20 30_24 [8.II: por. 18 m/sek 3 25-40]
10	5	1.2	22	*0 5 45 6 30 10 08 13 00 *1_13 45 *0_20 40; +0 9 30_11 45; ≫9 20_17 10; = 0 00_3 30 5 30_24 V0 1 15_5 10
11	6	.	26	= 0 00_24; ⌴0 4 30_9
12	5	0.6	23	△0 10 35_11 05; 12 40_14 45 16 40_17 10 *0_20 15 21 35_22 05; = 0 00_24; ⌴0 1_8
13	6	4.8	12	*0 8 10_9 20 ●0_9 45 10 20_11 20 △0 12 10 13 40_15 15 ●0_24; ≫13 30_24; = 0 00_24
14	7	0.7	12	●0 0 00-10 *0_4 35 5 22...37 ⚥0 9 15-45 ⚥2 9 50 ⚥1_10 10 ⚥0_11 12 ≫0 00-20 4 30_16 10 (por. 16 m/sek 10 45_12 45); = 0 00_4 20
15	7	1.6	12	*0 0 40 1 00_6 30 ⚥0 11 50_12 12 19 45_20 15 ⚥1 20 26-32 ⚥0_21 00 ⚥1_21 40
16	7	0.2	14	*0 0 45 2 30_5 33 20 45_21 47; = 1 35_11 40 17 35_24
17	6	1.3	15	*0 5 30_21 45 20 35_24; +0 7 40_21 40; ≫7 50_9 50; = 0 00_24
18	6	0.1	16	*0 0 00_1 10 2 20_11 50; +0 7_18 10; = 0 00_24
19	6	0.3	17	△0 8 25-40 *0 10 38 21 45 24; +0 8 45_12 15; = 0 00_24
20	6	0.0	20	*0 0 00 2 10_9 45 10 50 11 42 13 35; = 0 00_24
21	5	1.3	20	△0 9 20_10 20 *0 21 40_24; = 0 00_24
22	7	1.1	22	*0 0 00_5 10 *1_6 12 *0_7 45 *1_8 28 *0_9 38 *1_9 50 *0_10 32 ⚥0 16 37_17 37; +0 6 10_11 35; = 0 00_11 15 20 15_21 40 ≡1_24; V0 21 40_24
23	7	0.6	26	*0 19 35 20 10 *1_21 05 *0_23 40; ≡1 0 00_4 45 = _12 30; V0 0 00_4 45; ⊕ 8 15_11 15 12 15_14 30
24	7	0.4	27	= 1 30_2 40 ≡1_3 45 ≡2_4 10 ≡1_4 30 ≡0_6 10 ≡1_9 30; V0 14 00_3 50 V1_9 30
25	8	0.1	28	*0 0 20 1 45_7 05 7 08...30_8 35 ⚥1 16 45-57 ⚥0_17 05; +0 7 10_8 50; ⊕ 11 50_12 15
26	6	0.2	28	*0 11 30...40_13 10...43; +1 17 15-45; ≫17 15-45; = 6 15_8 20; ⌴0 1 30_8 15
27	5	0.2	32	*0 1 25_8 35 9 20 *1_9 45 *0_11 47 ⚥0 12 06-18 ⚥1_13 40 21 40_22 15 *1_23 30 *0_24; +0 15_1 00 +1_6 30 +0_12 30 +1_13 20 +0_22 15 +2_24; ≫2 30_6 30
28	7	0.0	34	*0 0 00_1 32 ⚥0 9 45-49; +0 0 00_2 15 +0_6 15; ≫0 00_5 20 [27.II: 9 45_15 30, 21 20_24]
29				
30				
31				
Σ	-	18.9	-	

Łódź - Lublinek φ = 51°44' λ = 19°24' Marzec - Mars 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.0	82.9	80.1	83.0	-12.0	-1.3	-1.6	-4.1	0.4	-12.6	85	52	92	69	0.9	2.7	0.4	1.3	9	9	10 *	SE 6	SSE 8	SE 3
2	72.8	71.3	69.4	71.2	-1.2	1.6	1.1	0.6	2.1	-3.6	93	87	92	91	0.4	0.9	0.5	0.6	10 *	10	10	SE 5	SE 4	SE 3
3	65.0	67.0	70.8	67.6	1.0	-1.4	-2.2	-1.2	1.6	-2.5	94	78	70	81	0.4	1.2	1.6	1.1	10 •	10 *	9	ENE 4	SW 12	SW 12
4	73.5	76.6	79.7	76.6	-5.0	-4.8	-5.4	-5.2	-2.1	-5.9	90	93	92	92	0.4	0.3	0.3	0.3	10 *	10 *	10 *	SW 12	SW 13	SW 9
5	81.7	84.5	89.6	85.3	-4.9	-3.0	-5.2	-4.6	-2.6	-6.0	86	84	93	88	0.6	0.8	0.3	0.6	10 *	10 *	9	WSW 7	W 8	WNW 2
6	93.7	94.7	98.5	95.6	-4.8	-1.6	-3.4	-3.3	-0.9	-7.6	93	69	85	82	0.3	1.6	0.7	0.9	10	10	10	SW 2	ENE 5	NE 8
7	102.2	103.6	105.0	103.6	-9.7	-5.2	-7.4	-7.4	-3.3	-10.0	85	73	73	77	0.4	1.1	0.9	0.8	10	9	9	ENE 5	NE 5	E 4
8	103.5	102.0	101.2	102.2	-12.0	-2.0	-6.9	-7.0	-1.6	-12.2	78	54	77	70	0.5	2.5	0.8	1.3	0	0	0	ESE 3	SSE 5	SE 2
9	101.0	101.0	101.2	101.1	-12.8	-3.0	-3.1	-5.5	-1.6	-13.4	81	49	86	72	0.4	2.5	0.7	1.2	10 ≡	8	10 *	SSE 2	WSW 4	W 2
10	104.1	107.0	107.9	106.3	-5.1	-1.0	-5.5	-4.3	0.0	-5.6	90	67	85	81	0.4	1.9	0.6	1.0	8	7	0	NW 3	NW 4	WSW 2
11	108.5	108.6	106.9	108.0	-9.7	1.0	-2.2	-3.3	2.5	-10.0	91	57	75	74	0.3	2.9	1.3	1.5	3	0	0	SW 1	NW 3	S 3
12	105.5	103.9	102.9	104.1	-6.0	3.3	0.3	-0.5	6.3	-6.8	81	61	65	69	0.7	3.0	2.2	2.0	1	6	0	SE 4	SW 3	SSE 5
13	103.0	102.6	102.2	102.6	-5.2	4.9	1.0	0.4	6.4	-5.5	83	47	66	65	0.7	4.6	2.3	2.5	0	0	0	ESE 4	SSE 4	SSE 3
14	101.5	100.2	98.7	100.1	-3.5	6.0	2.2	1.7	7.0	-5.8	81	53	71	68	0.9	4.5	2.1	2.5	0	0	0	SE 3	S 6	SSE 4
15	98.4	98.0	97.0	97.8	-2.4	8.5	6.0	4.5	9.0	-2.7	93	52	69	71	0.3	5.3	3.0	2.9	2	4	9	SE 4	S 4	SE 2
16	93.9	91.9	91.3	92.4	4.2	7.7	4.8	5.4	8.7	2.8	82	72	90	81	1.4	2.9	0.8	1.7	9	8	10 •	S 3	S 8	SW 3
17	92.2	90.9	88.0	90.4	2.6	5.0	2.2	3.0	5.2	2.2	98	98	98	98	0.2	0.1	0.2	0.2	10 ≡	10 ≡	10 ≡	SW 1	S 2	SE 3
18	85.7	84.0	82.3	84.0	0.0	10.9	4.4	4.9	11.4	-0.6	98	61	76	78	0.1	5.0	2.1	2.4	9 ≡	0	6	ESE 1	SSE 4	SSE 3
19	81.6	83.9	87.6	84.4	2.4	11.5	5.8	6.4	11.8	2.0	84	55	86	75	1.2	6.1	1.3	2.9	2	4	10	SE 3	W 7	S 2
20	93.5	94.4	92.3	93.4	0.5	5.6	2.4	2.7	7.6	-0.4	92	59	73	75	0.5	3.7	2.0	2.1	9	9	9	W 1	NW 4	S 4
21	89.7	84.0	80.9	84.9	0.5	3.6	5.8	3.9	7.2	-0.4	90	91	88	90	0.6	0.7	1.1	0.8	10 *	10	10	SE 1	SE 8	WSW 5
22	87.9	91.0	93.0	90.6	-0.8	3.3	-0.8	0.2	5.8	-1.1	79	48	77	68	1.2	4.0	1.4	2.2	8	2	0	NW 6	NW 8	WSW 2
23	91.9	88.4	83.6	88.0	-1.2	6.0	1.8	2.1	7.0	-3.4	77	36	65	59	1.3	6.0	2.4	3.2	0	2	9	SE 3	S 10	SE 5
24	79.7	79.4	80.4	79.8	3.4	11.6	8.0	7.8	12.4	1.5	80	61	83	75	1.6	5.3	1.8	2.9	10	8	9	SSE 3	SSW 5	SW 5
25	82.9	87.1	90.8	86.9	6.2	3.2	1.0	2.8	8.0	0.8	89	91	85	88	1.0	0.7	1.0	0.9	10 •	10 •	0	W 5	W 10	SW 2
26	92.0	90.4	91.6	91.3	1.1	6.0	4.4	4.0	6.6	-0.1	94	70	89	84	0.4	2.9	1.0	1.4	9	9	10 •	SW 3	SSE 6	SE 4
27	99.7	104.3	108.8	104.3	2.6	7.3	3.0	4.0	8.1	2.0	91	69	90	83	0.7	3.2	0.8	1.6	10	8	0	NE 5	E 3	C 0
28	109.7	108.1	106.6	108.1	1.8	9.8	7.0	6.4	9.9	-0.2	91	49	71	70	0.7	6.2	2.9	3.3	9	9	10	S 2	SSW 6	SSW 3
29	105.0	105.7	103.2	104.6	6.6	8.0	6.4	6.8	10.6	5.8	98	93	92	94	0.1	0.7	0.7	0.5	10 •	10 •	0	NW 3	NW 3	SW 1
30	97.5	94.7	101.7	98.0	5.6	13.1	2.0	5.7	14.2	1.7	91	50	66	69	0.9	7.5	2.5	3.6	1	6	0	W 5	NW 12	N 9
31	100.9	99.8	100.8	100.5	1.0	6.4	2.0	2.8	8.0	-1.1	77	53	71	67	1.5	4.5	2.1	2.7	7	8	0	WNW 8	NW 9	NW 7
M	93.0	93.0	93.4	93.1	-1.8	3.9	0.9	1.0	5.3	-3.1	87	66	80	78	0.7	3.1	1.3	1.7	7.0	6.7	5.8	3.8	6.2	4.1

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1	104.8	106.9	104.7	105.5	-1.4	2.8	-0.1	0.3	4.5	-1.7	82	54	76	71	1.0	3.5	1.5	2.0	0	4	0	NNW 6	N 7	W 3
2	98.6	100.0	100.8	99.8	1.6	8.4	4.6	4.8	9.6	-0.6	78	52	62	64	1.6	5.3	3.3	3.4	2	6	0	WNW 6	N 8	NNE 4
3	97.2	93.5	93.0	94.6	1.2	10.0	1.2	3.4	11.2	0.4	83	49	81	71	1.2	6.3	1.3	2.9	1	0	0	SSW 3	WNW 7	NW 4
4	90.4	88.9	87.5	88.9	1.0	12.4	7.5	7.1	13.3	-1.1	96	44	73	71	0.3	8.1	2.8	3.7	0	8	9	SW 1	WNW 5	WSW 1
5	92.0	94.7	95.5	94.1	0.6	9.6	6.2	5.6	11.3	-1.1	96	69	82	82	0.3	3.8	1.7	1.9	0	2	0	NW 2	ENE 5	ENE 3
6	96.3	95.2	92.0	94.5	1.8	13.0	5.5	6.4	14.0	0.6	91	36	80	69	0.7	9.6	1.8	4.0	0	0	2	SE 2	SSE 5	SE 5
7	88.1	89.6	90.7	89.5	3.6	7.6	6.0	5.8	10.3	1.3	83	91	79	84	1.3	0.9	2.0	1.4	7	10 •	9	SSE 3	WNW 6	WNW 2
8	89.8	89.5	90.1	89.8	3.8	11.7	5.6	6.7	11.9	2.1	92	49	81	74	0.7	7.0	1.7	3.1	0	7	0	SE 2	ESE 4	W 3
9	89.6	89.2	90.7	89.8	3.4	9.4	4.8	5.6	9.8	2.4	90	54	62	69	0.8	5.4	3.2	3.1	10	10	10	E 4	E 10	E 6
10	91.7	92.4	92.7	92.3	1.4	4.0	2.6	2.6	5.4	1.2	69	66	65	67	2.2	2.8	2.6	2.5	9	10	10	ESE 7	ESE 7	SE 5
11	90.5	89.8	89.7	90.0	0.0	4.0	3.6	2.8	5.4	-0.8	80	59	73	71	1.2	3.3	2.1	2.2	10	10	9	SE 5	SE 8	SE 8
12	90.4	91.3	90.8	90.8	1.1	3.6	3.8	3.1	5.0	1.0	90	93	93	92	0.6	0.5	0.5	0.5	10 •	10 •	10 •	SE 6	SE 4	SE 5
13	89.2	89.4	89.7	89.4	2.4	6.2	6.9	5.6	8.3	2.3	96	85	90	90	0.3	1.5	1.0	0.9	10 •	10 •	9 •	SSE 3	SE 6	SE 4
14	92.0	94.3	96.5	94.3	2.0	6.9	5.2	4.8	7.6	1.9	80	67	66	71	1.5	3.3	3.0	2.6	10	10	9	SE 4	SSE 3	SE 5
15	97.0	96.6	94.2	95.9	1.5	6.2	3.2	3.5	6.8	-0.6	81	56	79	72	1.3	4.2	1.6	2.4	8	8	1	SE 2	SE 5	SE 3
16	89.3	86.7	86.9	87.6	1.4	11.7	7.4	7.0	13.8	0.1	91	50	87	76	0.7	6.8	1.3	2.9	0	4	10 •	SE 5	S 6	SSW 3
17	87.5	89.3	84.8	87.2	6.6	7.6	5.1	6.1	8.8	4.9	97	72	83	84	0.3	2.9	1.5	1.6	10 •	10	0	SW 3	W 5	SSE 5
18	75.6	75.0	79.2	76.6	6.1	9.6	6.8	7.3	12.0	4.3	77	69	82	76	2.1	3.8	1.8	2.6	10 •	10 •	0	S 9	S 6	N 2
19	80.3	79.4	78.4	79.4	4.4	7.8	8.0	7.0	9.2	2.7	97	89	92	93	0.3	1.2	0.9	0.8	10 •	10 •	10 •	N 3	NE 4	ENE 4
20	78.7	79.6	81.0	79.8	6.2	11.6	9.1	9.0	13.8	4.8	85	64	72	74	1.5	4.8	3.2	3.2	9	9	0	ESE 6	E 8	E 5
21	80.4	79.3	77.8	79.2	7.2	8.9	8.1	8.1	10.3	6.7	86	85	93	88	1.5	1.7	0.8	1.3	10	10	10 •	E 5	E 8	ENE 6
22	75.6	75.6	74.6	75.3	8.2	6.2	4.6	5.9	9.2	4.6	92	82	93	89	0.9	1.7	0.6	1.1	10 •	10	10 •	ENE 7	NE 9	NNE 7
23	72.5	73.4	74.0	73.3	5.2	6.0	5.2	5.4	7.4	4.6	90	92	95	92	0.8	0.8	0.4	0.7	10 •	10 •	10 •	NE 5	N 6	NW 5
24	75.4	77.2	80.9	77.8	3.8	5.5	5.0	4.8	7.3	3.2	93	89	89	90	0.5	1.0	1.0	0.8	10 •	9	8	WNW 7	W 8	WSW 4
25	84.1	85.6	86.5	85.4	6.2	10.0	5.2	6.6	10.5	4.0	91	62	97	83	0.9	4.7	0.2	1.9	9	10	0	SW 5	SW 5	S 1
26	87.3	87.2	85.8	86.8	3.3	9.1	7.4	6.8	11.3	3.0	97	67	75	80	0.2	3.8	2.6	2.2	10 •	9	4	NW 5	W 3	SE 2
27	82.5	80.7	80.9	81.4	4.8	9.2	7.6	7.3	10.8	3.5	92	79	89	87	0.7	2.4	1.2	1.4	10	9	0	NE 1	E 2	SE 5
28	79.2	78.8	81.4	79.8	6.7	10.0	6.8	7.6	12.9	5.2	93	97	94	95	0.7	0.3	0.6	0.5	9	10 • K	9	ESE 6	E 5	SE 4
29	85.0	85.8	88.2	86.3	6.0	13.6	8.3	9.0	15.4	2.7	85	40	75	67	1.5	9.3	2.8	4.5	0	5	0	SSW 4	SW 3	NNE 2
30	91.2	91.2	93.0	91.8	4.0	13.6	6.8	7.8	14.3	1.9	100	55	88	81	0.0	7.0	1.2	2.7	8	9	0	W 1	NW 8	NW 3
31																								
M	87.4	87.5	87.7	87.5	3.5	8.5	5.6	5.8	10.0	2.1	88	67	82	79	0.9	3.9	1.7	2.2	6.7	8.0	5.0	4.3	5.9	4.0

Łódź - Lublinek $H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 10\,m$ Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU s	POGODA
1	7	1.8	34	$*^{0}15^{20}$ 21^{10} 22^{10} 24; = 6^{30} 10^{30} 15^{30} – 24; ⊕ 7^{40} – 9^{15} 10^{30} – 11^{15}
2	5	1.9	35	$*^{0}0^{00}$ 21^{5} – 10^{46} $\bullet^{0}17^{45}$ – 20^{10} $\bullet^{0}21^{48}$ – 22^{35} 23^{20} – 24; = 0^{00} – 24
3	6	4.0	25	$\bullet^{0}0^{00}$ 0^{12} 6^{30} – 9^{29} $\bullet^{0}*$ – 10^{15} $*^{0}$ – 11^{38} 12^{15} 13^{40} 22^{47} 24; ≫ 11^{20} – 24; = 0^{00} – 21^{30} ⊕ 16^{15} – 45
4	4	0.9	23	$*^{0}0^{00}$ 3^{15} – 4^{15} $*^{1}$ – 9^{05} $*^{0}$ – 24; ⊹^{1} 3^{45} – 24; ≫ 0^{00} – 14^{45} 15^{45} – 19^{30} (por. 15 m/sek); 21^{20} – 24
5	5	0.1	29	$*^{0}0^{00}$ – 7^{40} $*^{1}$ – 8^{10} $*^{0}$ – 11^{40} 12^{05} 13^{45} 14^{20} – 18^{20}; ⊹^{0} 0^{00} – 1^{30} ⊹^{0} – 14^{20}; ≫ 0^{00} – 23^{30}; = 14^{00} – 24
6	6	•	28	= 0^{00} – 24
7	6	0.1	28	⌓^{0} 7^{35} – 10^{10}; = 0^{00} – 24
8	6	•	27	= 0^{00} – 13^{10}; 17^{20} – 24
9	6	0.0	24	$*^{0}19^{45}$ 20^{50} 21^{40} 24; = 0^{00} – 6^{40} ≡^{0} – 7^{20} ≡^{0} – 8^{40} = – 24; V^{0} 6^{40} – 8^{40}
10	7	•	24	$*^{0}0^{00}$ 3^{45}; = 0^{00} – 10^{15}; 20^{30} – 24
11	8	•	23	= 0^{00} – 11^{30}; 18^{40} – 24
12	5	•	23	= 0^{00} – 15^{30} ∞ – 18^{30} = – 24
13	6	•	15	= 0^{00} – 12^{30} ∞ – 16^{30} = – 24
14	6	•	11	= 0^{00} – 10^{15} ∞ – 17^{15} = – 24
15	6	•	pł.	= 0^{00} – 24; ⌣^{0} 2^{30} – 8^{15}; ⊽ 22^{30} – 24
16	6	1.0	pł.	$\bullet^{0}9^{43}$ 12^{12} 19^{40} 21^{20} – 24; = 0^{00} – 24; ⊽ 0^{00} – 20
17	2	•	pł.	$\bullet^{0}0^{00}$ – 1^{15} 2^{38}; = 0^{00} – 2^{50} ≡^{0} – 3^{30} ≡^{1} – 6^{20} ≡^{1} – 13^{10} ≡^{0} – 13^{20} = – 16^{20} ≡^{0} – 16^{40} ≡^{1} – 24
18	6	•	pł.	≡^{1} 0^{00} – 5^{50} ≡^{1} – 6^{20} ≡^{0} – 7^{40} = – 24
19	7	0.0	pł.	$\bullet^{0}21^{45}$ – 22^{05}; = 0^{00} – 12^{30} 18^{15} – 24; ⌣^{0} 4 – 7^{30}
20	7	0.0	•	= 0^{00} – 9^{20} 18^{30} – 24
21	5	1.6	•	$*^{0}6^{32}$ – 9^{15} $*^{1}$ – 10^{00} $*^{0}$ – 10^{07} $\bullet^{0}*$ – 10^{20} $\bullet^{0}$ 10^{40} 14^{46} 16^{45} 17^{40} – 19^{45} 21^{48} 23^{38}; ≫ 23^{25} – 24; = 0^{00} – 24
22	8	•	•	≫ 0^{00} – 1^{30}; = 0^{00} – 4^{30}
23	8	0.0	•	≫ 12^{30} – 13^{40}; ⌣^{0} 1 – 10
24	7	0.0	•	$\bullet^{0}$ 0^{43} 5^{36}; = 5^{20} – 12
25	6	0.5	•	⊽^{0} 0^{45} – 1^{05} $\bullet^{0}$ 6^{38} 7^{10} 8^{45} – 13^{05} ⊽^{0} – 13^{43}; ≫ 8^{45} – 15^{15}; = 5^{20} – 13^{00} 18^{30} – 24
26	6	3.8	•	$\bullet^{0}7^{50}$ 8^{34} ⊽^{0} 13^{12} – 36 $\bullet^{0}18^{40}$ – 24; = 0^{00} – 24; ⌣^{0} 5 – 6^{30}
27	6	•	•	$\bullet^{0}0^{00}$ – 1^{50} 7^{00} 8^{02}; = 0^{00} – 24; ⌓^{0} 21^{30} – 23 ⌓^{1} – 24
28	7	0.5	•	= 0^{00} – 10^{40}; 18^{40} – 24; ⌓^{1} 0^{00} – 1^{30} ⌣^{0} – 6^{20}
29	5	0.0	•	$\bullet^{0}3^{40}$ 5^{35} $\bullet^{0}$ – 9^{15}; 10^{32} – 11^{05} 14^{00}; = 0^{00} – 7^{15} ≡^{0} – 7^{45} = – 24
30	7	•	•	≫ 12^{25} – 16^{20} (por. 18 m/sek); = 0^{00} – 11^{30}; ⌓^{0} 2^{30} – 9
31	8	0.1	•	⊽ 14^{50} – 15^{05} ⊽^{0} 16^{20} – 30; 16^{46} – 58; 17^{45} – 57; ⌣^{0} 13^{0} – 7^{15}
Σ	–	16.2	–	

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1	8	•	•	⌣^{0} 2 – 8^{30}
2	8	•	•	
3	7	•	•	= 5^{30} – 9^{45} 15^{30} – 24; ⌣^{0} 3 – 8
4	7	•	•	= 0^{00} – 9^{30}; 18^{30} – 24; ⌣^{0} 3 – 6^{30}
5	6	•	•	= 0^{00} – 10^{30} ∞ – 12^{15} = – 24; ⌣^{0} 2 – 7^{15}
6	7	•	•	= 0^{00} – 8^{30}; ⌣^{0} 3 – 7^{10}
7	6	0.4	•	$\bullet^{0}12^{35}$ 14^{10}; = 3^{30} – 15^{30}; 18^{30} – 24; ⌓^{0} 3 – 9
8	7	•	•	= 0^{00} – 10^{30} ∞ – 11^{40}; ⊽ 22^{56} – 23^{20}
9	7	•	•	≫ 7^{48} – 18^{30} (por. 15 m/sek 10^{30} – 15^{30}); = 4^{30} – 10^{30}; ⊕ 8^{30} – 12^{15}
10	7	•	•	
11	7	0.2	•	
12	6	6.0	•	$\bullet^{0}0^{30}$ 1^{25} 6^{35} 12^{05} – 14^{40} 16^{38} 18^{05} 20^{30} $\bullet^{0}$ 22^{35}; = 5^{30} – 24
13	6	2.2	•	$\bullet^{0}0^{00}$ 2^{30} 4^{40} 7^{25} 9^{43} 11^{47} 13^{45} ⊽^{0} 18^{12} 19^{20} $\bullet^{0}$ 22^{15}; = 0^{00} – 24
14	6	•	•	= 0^{00} – 24
15	7	•	•	= 0^{00} – 8^{30}
16	7	0.4	•	⊽^{0} 14^{47} – 15^{13} $\bullet^{0}20^{35}$ – 22^{05} 22^{45} 23^{10}; = 3^{20} – 10^{30} 15^{00} – 24; ⌣^{0} 4 – 8
17	7	0.4	•	$\bullet^{0}4^{45}$ 5^{15} $\bullet^{0}$ – 7^{35} $\bullet$ – 8^{15} $\bullet^{0}$ – 11^{43}; = 0^{00} – 1^{20} ≡^{0} – 7^{45} = – 12^{30} 18^{30} – 24
18	7	1.3	•	$\bullet^{0}8^{15}$ – 7^{36} 8^{45} 10^{40} 12^{35} 14^{12} ⊽^{0} 15^{23} – 30 16^{05} – 22; = 0^{00} – 11^{30}; ⌓ 1^{10} – 3^{25}
19	6	3.0	•	$\bullet^{0}4^{45}$ 5^{15} – 13^{00} 45 20^{00} 22^{20}; = 5^{30} – 24
20	7	•	•	= 0^{00} – 9^{35}
21	6	0.4	•	$\bullet^{0}9^{45}$ 10^{40} ⊽^{0} 12^{45} – 13^{00} 13^{40} – 59 $\bullet^{0}20^{35}$ – 21^{20} 24; = 4^{30} – 24
22	6	2.3	•	$\bullet^{0}0^{00}$ 1^{10} – 2^{50} 5^{25} – 7^{32} ⊽^{0} 8^{45} – 9^{00} $\bullet^{0}12^{50}$ 13^{15} 17^{02} 21^{10} – 24; = 0^{00} – 11^{30} 17^{30} – 24
23	6	12.4	•	$\bullet^{0}0^{00}$ – 3^{25} 6^{20} 7^{05} 7^{40} 8^{12} 10^{25} – 18^{44} 20^{40} – 24; = 0^{00} – 24
24	7	4.8	•	$\bullet^{0}0^{00}$ – 8^{20} 10^{15} – 12^{30} ⊽^{0} – 12^{38} 12^{55} – 14^{22} ⊽^{1} – 14^{28} ⊽^{0} – 14^{43} 15^{00} – 16^{07} 16^{43} – 17^{14} 17^{25} – 35; = 0^{00} – 9^{00}
25	6	11.6	•	$\bullet^{0}4^{40}$ 5^{35} 10^{42} – 58 11^{40} – 46 12^{56} 13^{05} ⊽^{1} – 13^{10} ⊽^{0} – 13^{30} 13^{42} 14^{35} 14^{42} – 58 16^{38} 17^{05} ⊽^{1} – 17^{20} ⊽^{0} – 17^{37} 18^{05} – 25 $\bullet^{0}23^{50}$ 24; = 3^{30} 11^{00} 12^{30} 22^{40} ≡^{0} – 23^{50} = – 24
26	7	3.9	•	$\bullet^{0}0^{00}$ – 2^{40}; 3^{32} – 4^{25} $\bullet^{1}$ – 5^{00} $\bullet^{0}$ – 10^{05}; = 0^{00} – 10^{30}; 19^{30} – 24
27	6	•	•	= 0^{00} – 24; ⌓^{0} 3 – 8^{30}
28	6	16.1	•	⊽^{0} 12^{03} – 13^{06} 13^{26} – 55 ⊽^{1} – 14^{10} ⊽^{2} – 14^{15} ⊽^{1} – 14^{28} ⊽^{0} – 14^{44} 14^{48} – 16^{10} 16^{32} – 48 ⊽^{1} – 17^{05} ⊽^{0} 18^{02} 18^{25} – 36 ⊽ ⌓SE 12^{15} – 14^{45} NW; por. wiatru 12 m/sek 10^{30} – 12^{35} 15 m/sek 14^{15} –
29	8	•	•	= 0^{00} – 8^{30}; ⌓^{0} 19^{30} – 24 [28.IV. = 0^{00} – 24]
30	7	2.8	•	⊽^{1} 12^{47} – 50 ⊽▲^{1} – 12^{54} ⊽^{1} – 12^{55} ⊽^{0} – 13^{10} ⊽^{1} 14^{35} 15^{03} ⊽^{0} – 15^{25}; = 3^{15} – 9^{30}; ⌓^{0} 0^{00} – 2^{30} ⌓^{1} – 4 ⌓^{2} – 6^{45} ⌓^{1} – 7 ⌓^{0} – 8
31				
Σ	–	68.2	–	

Łódź – Lublinek φ = 51°44' λ = 19°24' Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	93.9	92.9	94.6	93.8	4.3	11.8	4.2	6.1	12.9	0.6	76	43	55	58	2.0	7.9	3.7	4.5	0	4	0	NW 3	NNW 8	N 4
2	96.8	96.8	95.7	96.4	1.2	6.3	4.8	4.4	8.4	-1.5	85	49	55	63	1.1	5.1	3.9	3.4	5	7	0	N 5	N 4	SE 3
3	96.1	96.1	96.7	96.3	2.8	7.0	4.2	4.6	8.6	-0.6	77	47	57	60	1.7	5.3	3.5	3.5	0	7	0	NE 3	NE 6	E 3
4	96.9	94.1	89.4	93.5	2.2	11.1	6.8	6.7	12.3	-0.9	78	32	53	54	1.6	8.9	4.7	5.1	0	2	5	SW 3	SE 9	SE 8
5	84.0	82.7	81.7	82.8	3.1	5.2	6.6	5.4	7.3	2.9	93	98	97	96	0.5	0.1	0.3	0.3	10 •	10 •	10	SE 6	SE 5	SE 4
6	83.1	85.1	88.5	85.[illegible]	6.0	7.3	7.0	7.0	9.1	5.7	100	94	94	96	0.0	0.6	0.6	0.4	10 •	10 •	10	ESE 2	WNW 1	E 1
7	90.7	91.4	91.8	91.3	7.3	11.2	7.5	8.4	12.2	5.4	77	64	79	73	2.4	4.8	2.2	3.1	7	9	2	NNE 3	NNW 5	SW 2
8	88.5	88.8	92.5	89.9	8.6	13.3	7.8	9.4	15.3	5.2	81	83	93	86	2.2	2.7	0.8	1.9	9	9	0	S 5	SW 7	WNW 3
9	90.1	86.8	79.0	85.3	8.8	11.6	8.8	9.5	13.8	4.6	96	93	95	95	0.4	1.0	0.6	0.7	10	10 •	10 •	SW 4	SW 6	WSW 7
10	77.6	77.7	78.4	77.9	7.8	6.8	7.1	7.2	11.3	6.4	83	86	93	87	1.8	1.5	0.8	1.4	10 •	9 •	9 •	WSW 9	WNW 8	WSW 5
11	79.7	85.4	91.5	85.5	6.8	9.9	8.4	8.4	12.0	5.9	88	68	89	82	1.2	3.9	1.2	2.1	10	10	9	S 3	ENE 2	NW 3
12	96.8	98.7	99.0	98.2	7.2	9.1	7.7	7.9	13.2	3.7	84	89	79	84	1.7	1.3	2.2	1.7	1	10	8	NNW 4	NW 5	NNW 3
13	99.3	98.6	96.9	98.3	9.0	15.2	9.8	11.0	16.4	4.1	71	39	72	61	3.4	10.6	3.4	5.8	5	6	8	N 2	NW 3	WNW 2
14	93.8	92.3	90.9	92.5	9.4	11.9	10.3	10.5	13.0	7.3	91	72	92	85	1.1	3.9	0.9	2.0	10 •	10	8	NW 4	WNW 4	WNW 6
15	90.2	89.9	88.8	89.6	9.6	13.1	10.8	11.1	15.9	7.1	93	67	63	74	0.8	5.0	4.8	3.5	10	9	6	NNW 3	NNE 6	E 5
16	86.9	86.1	84.4	85.8	9.0	15.8	13.2	12.8	17.3	7.1	66	58	82	69	4.0	7.4	2.8	4.7	10	9	9	SE 9	S 7	SSW 3
17	85.8	84.8	82.1	84.2	11.1	19.0	17.2	16.1	21.9	9.0	100	58	76	78	0.0	9.3	4.7	4.7	10 =	9	10	SW 3	SW 5	SE 4
18	81.2	84.2	83.7	83.0	16.6	16.6	14.3	15.4	19.0	14.2	79	74	90	81	4.1	5.0	1.6	3.6	8	9	10	W 6	WSW 6	S 4
19	79.5	78.8	87.3	81.9	13.6	15.0	6.4	10.4	15.4	6.3	94	83	88	88	0.9	2.9	1.1	1.6	10	10	9	WNW 3	NNE 4	NNW 3
20	93.3	95.0	98.1	95.5	5.6	9.8	5.4	6.6	10.5	3.8	88	48	83	73	1.1	6.3	1.6	3.0	8	10	2	NW 4	NW 7	SW 3
21	103.1	104.3	105.3	104.2	5.8	10.6	7.2	7.7	12.3	1.2	82	56	67	68	1.7	5.6	3.4	3.6	6	6	0	SW 2	NW 8	SW 2
22	106.5	104.2	101.6	104.1	9.4	13.7	11.0	11.3	14.8	1.5	54	38	52	48	5.4	9.8	6.3	7.2	2	8	2	SSW 4	SW 5	ENE 5
23	99.0	98.0	96.9	98.0	10.6	13.8	9.8	11.0	14.5	7.1	51	42	86	60	6.2	9.2	1.7	5.7	8	9	10 •	E 8	E 8	ESE 8
24	94.3	94.0	92.6	93.6	9.4	10.3	10.7	10.3	12.5	9.4	92	92	96	93	1.0	0.9	0.5	0.8	10 •	10 •	8	ESE 6	ESE 3	N 2
25	92.9	93.0	93.9	93.3	11.0	14.4	12.1	12.4	14.8	10.3	95	78	90	88	0.6	3.6	1.4	1.9	10	9	10	N 3	NW 3	N 6
26	94.0	94.0	92.9	93.6	11.0	12.2	10.4	11.0	13.6	10.2	92	90	93	92	1.0	1.4	0.8	1.1	9	10	10	WNW 3	NW 5	C 0
27	91.2	90.8	90.8	90.9	9.9	14.1	10.0	11.0	15.5	7.3	93	66	92	84	0.8	5.4	1.0	2.4	10	9	4	WSW 5	W 5	C 0
28	90.0	89.0	86.7	88.6	11.6	14.4	13.4	13.2	16.5	6.0	83	71	80	78	2.3	4.8	3.2	3.4	9 •	10 •	10 •	ENE 3	ESE 5	ENE 6
29	82.1	81.8	83.9	82.6	11.4	12.4	9.6	10.8	13.8	9.6	96	93	92	94	0.5	1.0	1.0	0.8	10	10	10	NE 6	NE 7	NE 5
30	85.2	86.6	87.1	86.3	6.8	10.8	8.6	8.7	12.8	5.0	82	61	70	71	1.8	5.1	3.3	3.4	6	7	0	NNW 2	NNW 8	C 0
31	88.6	88.9	87.7	88.4	9.1	15.6	13.8	13.1	17.3	2.6	70	41	61	57	3.6	10.4	6.2	6.7	5	5	9	SE 5	SE 6	E 5
M	90.7	90.7	90.7	90.7	8.3	11.9	9.2	9.6	13.7	5.4	84	67	79	77	1.8	4.9	2.4	3.0	7.4	8.5	6.4	4.2	5.5	4.0

Czerwiec – Juin

1	81.8	83.1	85.2	83.4	13.8	16.4	13.4	14.2	18.8	10.4	92	54	75	74	1.3	8.6	3.8	4.6	9	9	9	SE 5	WSW 8	SW 5
2	86.4	89.4	93.1	89.6	9.8	9.4	9.0	9.3	13.5	8.4	84	92	84	87	1.9	1.0	1.9	1.6	10	10 •	7	SW 8	WSW 7	W 2
3	94.7	95.4	95.2	95.1	8.9	18.8	13.6	13.7	19.5	6.1	92	43	72	69	0.9	12.4	4.4	5.9	7	5	0	SW 3	WNW 4	C 0
4	95.6	94.8	93.5	94.6	15.2	20.7	17.1	17.5	21.3	9.1	64	39	60	54	6.2	14.8	7.8	9.6	0	5	10	ESE 6	ESE 5	E 3
5	90.1	88.4	86.3	88.3	13.4	12.8	13.0	13.0	17.4	12.8	80	94	81	85	3.2	0.9	2.8	2.3	10 •	10 •	10	E 5	E 8	E 5
6	83.0	83.1	84.2	83.4	12.0	12.8	12.6	12.5	14.6	11.4	88	86	77	84	1.7	2.1	3.4	2.4	10	10 •	4	NE 7	NE 6	NNE 5
7	86.9	87.8	88.7	87.8	11.4	17.4	14.9	14.6	19.6	7.2	71	48	67	62	3.9	10.3	5.5	6.6	1	7	2	N 5	NW 6	SSE 3
8	90.7	89.3	88.1	89.4	14.1	21.2	16.2	16.9	21.7	8.9	70	38	57	55	4.8	15.7	7.9	9.5	0	3	2	ESE 3	SE 7	E 4
9	85.9	84.6	85.1	85.2	14.9	21.0	14.4	16.2	21.8	12.2	75	54	86	72	4.1	11.5	2.4	6.0	4	9	9	ESE 7	SE 7	ESE 7
10	85.3	86.1	85.9	85.8	14.4	16.0	14.2	14.7	17.9	13.8	89	84	87	87	1.8	2.9	2.2	2.3	10	9	8	ESE 4	E 6	NE 4
11	82.1	82.8	83.9	82.9	13.2	14.0	12.6	13.1	15.4	12.5	93	94	93	93	1.1	0.9	1.1	1.0	10 •	10 •	10 •	NE 4	N 5	N 8
12	87.2	88.5	90.3	88.7	11.9	14.4	14.0	13.6	17.1	11.6	96	90	83	90	0.5	1.6	2.7	1.6	10 •	9	10	N 5	WNW 8	NW 6
13	91.6	91.3	90.5	91.1	11.4	15.0	12.5	12.8	17.1	9.1	85	62	87	78	2.0	6.4	1.9	3.4	9	8	8	WNW 8	WNW 9	W 4
14	90.7	91.5	93.4	91.9	10.0	16.6	12.1	12.7	20.2	8.4	97	78	68	81	0.3	4.3	4.5	3.0	10 •	6	2	WNW 5	NNW 7	N 4
15	95.0	95.4	94.6	95.0	11.9	18.3	15.0	15.0	20.4	5.1	61	33	56	50	5.3	14.0	7.4	8.9	3	1	0	N 7	SW 5	C 0
16	94.3	92.1	88.3	91.6	14.4	23.2	18.4	18.6	24.4	6.9	59	38	57	51	6.6	17.5	9.1	11.1	3	9	8	SSE 3	SW 4	SSE 5
17	83.5	81.1	85.0	83.2	17.7	22.4	13.0	16.5	24.4	12.9	68	41	98	69	6.4	16.1	0.4	7.6	2	9 •	10 •	SSE 4	SSW 6	WSW 2
18	91.0	92.5	91.1	91.5	12.0	17.1	15.4	15.0	20.1	10.9	83	56	70	70	2.3	8.7	5.3	5.4	9	6	10	W 7	W 4	SSW 4
19	88.8	89.1	92.9	90.3	14.4	18.4	16.0	16.2	20.3	13.5	98	71	63	77	0.4	6.1	6.7	4.4	10 •	8	9	WSW 4	W 8	WNW 6
20	96.2	96.9	97.0	96.7	14.0	17.4	13.0	14.4	19.8	11.8	70	56	81	69	4.8	8.8	2.8	5.5	2	8	3	WNW 7	WNW 7	SW 4
21	97.7	96.9	94.2	96.3	14.8	21.2	17.8	17.9	22.9	9.4	80	44	62	62	3.3	14.2	7.8	8.4	2	8	3	SW 2	S 3	ESE 5
22	90.6	88.7	86.1	88.5	16.7	26.6	22.1	21.9	28.4	12.8	75	47	68	63	4.8	18.4	8.6	10.6	6	6	5	SE 6	SSW 7	SSW 3
23	88.0	90.1	92.9	90.3	17.3	21.4	15.8	17.6	22.4	15.8	89	59	83	77	2.2	10.4	3.0	5.2	9	9	3	SW 5	SW 7	WSW 3
24	94.5	93.8	94.4	94.2	17.2	24.2	20.0	20.4	25.1	11.9	79	48	66	64	4.1	15.7	8.0	9.3	6	7	9	SSW 3	WNW 7	S 2
25	95.8	96.4	96.2	96.1	18.0	24.2	21.4	21.2	25.7	14.5	76	35	56	56	4.8	19.7	11.2	11.9	6	5	3	WNW 1	NW 5	E 2
26	95.0	93.5	95.1	94.6	20.6	30.4	18.3	21.9	31.6	14.5	66	33	93	64	8.3	29.0	1.4	12.9	0	1	9	SE 2	WSW 5	SW 2
27	98.3	97.9	96.7	97.6	17.4	18.8	16.2	17.2	21.4	15.4	69	83	90	81	6.3	3.7	1.7	3.9	8	9 (K)	10	NE 3	NNE 3	N 4
28	99.0	100.4	99.9	99.8	14.9	17.3	11.8	14.0	18.3	11.8	88	50	80	73	2.0	9.9	2.8	4.9	9	9	1	N 5	NW 7	NW 2
29	96.4	96.9	97.2	96.8	14.1	17.5	14.0	14.9	19.9	7.6	69	68	78	72	4.9	6.4	3.6	5.0	1	9	1	WSW 5	NW 7	NW 3
30	98.1	96.0	90.8	95.0	13.4	21.0	19.4	18.3	23.9	7.1	75	46	55	59	3.8	13.4	10.1	9.1	0	0	2	WSW 1	NW 5	SSW 2
31																								
M	91.1	91.1	91.2	91.1	14.1	18.9	15.2	15.8	20.8	10.8	79	59	74	71	3.5	10.2	4.7	6.1	5.9	7.1	5.9	4.7	6.1	3.6

Łódź - Lublinek $H_s = 187\,m$ $H_b = 187.7\,m$ $h_w = 10\,m$ Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	.	= 4^30 – 6^30; ⌓ ^0 3 – 4 ⌣ ^0 – 6^30
2	8	.	.	⌣ ^0 3 – 6 ⌓ ^0 20^30 – 24
3	8	.	.	⌓ ^0 0^00 – 3^30 ⌣ ^0 – 6^45
4	8	1.4	.	⌣ ^0 4 – 6^30
5	5	3.5	.	● ^0 2^40 – 3^05, 5^15 – 13^50, 17^40; = 8^00 – 24
6	5	0.1	.	● ^0 1^45, 5^10, 6^03 ... 7^35, 12^40, 13^35, 16^30, 19^25; = 0^00 – 24
7	7	.	.	= 0^00 – 9^30, 21^30 – 24; ⌓ ^0 2 – 4 ⌓ ^1 – 6 ⌓ ^0 – 7^30, 20 – 24
8	6	1.1	.	● ^0 7^27 ... 40, 8^30 – 11^15 ▽ ^0 13^48, 14^05 ▽ ^1 – 14^15 ▽ ^0 – 14^40, 14^57, 15^10, K ^0 W 14^02 – 20 SE; = 0^00 – 16^00, 18^30 – 24, ⌓ ^0 0^00 – 1^30 ⌓ ^1 – 4 ⌓ ^0 – 7^27
9	5	7.5	.	● ^0 7^32 – 10^45, 11^30 ... 14^35, 15^30 – 20^05 ▽ ^2 – 20^10 ▽ ^1 – 20^45 ▽ ^0 – 21^15; = 0^00 – 20^45
10	7	7.3	.	▽ ^0 1^35, 2^15, 3^25, 4^02, 4^35 – 40, 5^18 – 35, 5^48 – 53, 6^05 – 12, 6^25, 7^15, 7^25 – 37, 8^46, 10^25, 11^05 – 20, 11^30 – 43, 12^05 – 15, 12^25, 13^01, 13^25 – 58, 14^18 – 40, 14^48, 15^08, 19^15, 19^10, 20^34 – 21^08, ≫ 19^10 – 19^30 (por. 8 m/sek)
11	7	0.3	.	● ^0 3^41 ... 6^28 ▽ ^0 15^15 – 19, 15^40 – 49
12	6	0.0	.	● ^0 10^25, 12^35, = 9^15 – 13^30
13	8	0.0	.	⌓ ^0 3^30 – 8^30, 20 – 24; ⌔ 20^30 – 24
14	7	0.0	.	● ^0 5^57 ... 9^10 ▽ ^0 14^52, 15^20; = 3^30 – 9^30, 20^30 – 24, ⌓ ^0 0^00 – 5^57, 21^30 – 24
15	7	0.0	.	= 0^00 – 2^50 ≡ ^1 – 4^25 ≡ ^0 – 4^50 ≡ – 12^00, ⌓ ^0 0^00 – 3 ⌓ ^1 – 7 ⌓ ^0 – 8^30, 23 – 24
16	7	0.4	.	● ^0 3^40 – 5^30 ▽ ^0 18^05 – 20^10; K ^0 W 18^40, 19^55, 20^00 – (K) 20^05 E; = 22^30 – 24, ⌓ ^0 0^00 – 3^40
17	7	5.6	.	▽ ^1 18^05 – 08 ▽ ^0 – 18^27 ▽ ^2 23^38 – 48 ▽ ^0 – 24; (K) W 23^25 K ^2 23^38 K ^0 23^48 – 24, = 0^00 – 4^10 ≡ ^0 – 4^20 ≡ ^1 – 6^35 ≡ ^0 – 7^10 – 11^30, 19^20 – 24; ⌓ ^0 1 – 3 ⌓ ^1 – 3^30 ⌓ ^2 – 7^30 ⌓ ^1 – 10
18	7	5.1	.	▽ ^0 0^00, 1^05 ● ^0 10^50, 11^25, 14^10, 16^38 ▽ ^0 22^40 – 44 ▽ ^1 – 22^48 ▽ ^0 – 24, K ^0 0^00, 1^10 (K) E 1^35 (K) W 22^40 K ^0 22^44 – 49 – (K) NE 23^35 = 0^00 – 7^30, 19^30 – 24, ⌓ ^0 20^30 – 24
19	7	10.3	.	▽ ^0 0^00 – 13, 3^15 – 28 ● ^0 4^46, 6^28 ▽ ^0 15^25, 16^00 ▽ ^2 – 16^27 ▽ ^1 – 16^37 ▽ ^0 – 17^00, 18^22, 19^20 ● ^0 – 20^35 (K) NW 15^15 – K ^0 15^25 – K ^0 16^00 K 16^25 – K ^0 16^30 – 35 (K) SE 16^45 = 0^00, 10^00, 15^15 – 16^30;
20	8	0.0	.	▽ ^0 20^15 – 20, ⊕ 10^38 – 16^10 [19.V. ≫ 15^15 – 18^40 (por. 18 m/sek)]
21	8	0.3	.	▽ ^0 9^25 – 36, 10^36 – 48; ⌣ ^0 3^30 – 5^30, ⌓ ^0 20^30 – 22 ⌓ ^1 – 24
22	7	.	.	= 3^30 – 7^30, ⌓ ^1 0^00 – 2 ⌓ ^2 – 3 ⌣ ^0 – 5^30
23	7	2.0	.	● ^0 18^12 ... 21^32; por wiatru 15 m/sek 9^10 – 13^02 ≫ 13^02 – 18^20 (por. 18 m/sek)
24	6	12.2	.	● ^0 5^35 – 7^26 ● ^1 – 7^45 ● ^0 – 14^41; = 7^00 – 24
25	6	0.5	.	● ^0 3^45, 4^20 – 6^35, 7^10 ... 9^25; = 0^00 – 16^30, 18^15 – 24
26	6	3.3	.	● ^0 1^40 – 2^15, 5^35, 9^45, 10^28 ▽ ^0 11^33 – 12^13, 12^19 – 26, 21^12 – 22^03; (K) NW 21^05 – 22^05 E; = 0^00 – 13^30, 20^30 – 24
27	7	.	.	= 0^00 – 11^30, 21^30 – 24; ⌓ ^0 19^45 – 22^30 ⌓ ^1 – 23^30 ⌓ ^2 – 24
28	6	5.8	.	● ^0 22^50 – 24; = 0^00 – 24, ⌓ ^2 0^00, 7 ⌓ ^1 – 8 ⌓ ^0 – 10
29	6	13.7	.	● ^0 0^00 ... 2^36, 3^35, 4^16 – 6^20 ● ^1 – 7^26 ● ^0 – 8^15 ● ^1 – 8^30 ● ^0 – 11^20 ● ^1 – 11^30 ● ^0 – 18^10 ● ^1 – 18^20 ● ^0 – 18^40 ... 20^50 – 21^32 ▽ ^0 23^38 – 25; = 0^00 – 24
30	8	.	.	= 0^00 – 4^20; ⌓ ^0 20 – 24
31	8	5.9	.	⌓ ^0 0^00 – 1 ⌓ ^1 – 6^30 ⌓ ^0 – 8
Σ	–	86.3	–	

Czerwiec - Juin

1	8	0.0	.	● ^0 0^35 – 1^25 ● ^1 – 2^10 ● ^0 – 3^15 ● ^1 – 4^12 ● ^0 – 5^32 6^07; ≫ 10^30 – 12^15 (por. 15 m/sek), 13^35 – 16^30 (por. 17 m/sek), = 2^30 – 7^30
2	6	0.3	.	● ^0 5^20 6^10, 7^10 – 8^50, 14^33
3	7	.	.	= 4^10 – 8^30, 19^30 – 24, ⌓ ^0 1 – 2 ⌓ ^1 – 3 ⌓ ^2 – 7 ⌓ ^1 – 8 ⌓ ^0 – 9^30, 20^30 – 24
4	7	0.7	.	● ^0 19^50 – 20^00, 22^10 – 24, = 0^00 – 7^30, ⌓ ^0 0^00 – 8, ⊕ 14^30 – 15^20
5	5	5.7	.	● ^0 0^00 – 2^35, 5^40, 7^30 – 8^40 ... 10^10 – 11^20 ● ^1 – 11^40 ● ^0 – 14^05 ● ^1 – 14^35 ● ^0 – 15^40 ● ^0 16^04 ... 17^10 – 18^30; = 19^00 – 24
6	7	1.3	.	● ^0 0^09 – 3^45, 4^35 – 6^35, 8^20, 9^40 – 15^15; = 0^00 – 3^30
7	8	.	.	⌓ ^0 21^30 – 24
8	8	.	.	⌓ ^0 0^00 – 7^30
9	7	5.9	.	▽ ^0 16^40 – 43 ▽ ^2 – 16^45 ▽ ^1 – 16^48 ▽ ^0 – 16^55, 17^10 – 23, 17^58, 18^23 ▽ ^1 – 18^36 ▽ ^2 – 18^52 ▽ ^2 – 18^43 ▽ ^0 19^10, 19^23 – 20^06, 20^15 – 25 ● ^0 22^40 – 24, ≫ 14^10 – 16^45 (por. 14 m/sek)
10	7	1.4	.	● ^0 0^00 – 45, 4^30 – 5^40
11	6	9.5	.	● ^0 2^15, 3^10 ● ^0 – 11^15, 12^15 – 14^20 ▽ ^1 – 14^30 ▽ ^0 – 14^40, 15^15 – 28, 16^28 – 17^50 ● ^0 18^02, 19^10 – 28 ● ^1 – 19^45 ● ^0 – 24
12	6	2.9	.	● ^0 0^00 – 4^18 ● ^1 – 4^42 ● ^0 – 5^32 ● ^1 – 0^01 ● ^0 – 7^35, 9^50, 10^24 ▽ ^0 11^43 – 50 ▽ ^1 12^22 – 38 ▽ ^0 17^10 – 17, 18^01 – 09, 18^16 – 21, 19^11 – 14 (K) NW 16^50 K ^0 17^10 – 17 (K) SE 17^35 – 19^00, 19^30, 19^50 – 24
13	8	0.0	.	= 0^00 – 10, 2^20, 7^30, 22^30 – 24, ⌓ ^0 20^30 – 23^30 ⌓ ^1 – 24
14	7	1.1	.	● ^0 6^20 – 9^40 ▽ ^0 16^45 – 58; = 0^00 – 10^20, ⌓ ^1 0^00 – 1 ⌓ ^2 – 6^20 ⌓ ^0 21^30 – 24
15	8	.	.	⌓ ^0 0^00 – 8, 20^30 – 24
16	7	.	.	= 2^30 – 7^30; ⌓ ^0 0^00 – 8
17	7	3.2	.	▽ ^0 10^38 – 56 ● ^0 17^34, 19^00 – 22^10 ... 50; ≫ 10^10 – 11^40
18	8	5.6	.	● ^0 0^40 – 1^45
19	7	2.0	.	● ^0 0^30, 1^20 – 2^45, 5^50 – 6^01 ● ^1 – 6^30 ● ^0 – 6^33 ● ^1 – 7^02 ● ^0 – 7^17 ... 40, 8^44, 11^15 ▽ ^0 14^35 – 42
20	8	.	.	⌓ ^0 20^30 – 24
21	7	.	.	= 1^30 – 9^00, ⌓ ^0 0^00 – 8^30
22	7	1.2	.	⌄ W 22^40 – 24; = 2^30 – 9^30, ⌓ ^0 1^30 – 8
23	7	0.0	.	▽ ^0 3^20 – 4^25 ● ^0 – 5^40 ▽ ^0 13^48 – 14^05; ⌄ W 0^00 – 1^15 ⌓ ^0 21^30 – 24
24	7	.	.	= 1^30 – 7^30, ⌓ ^0 0^00 – 8^30
25	7	.	.	= 2^10 – 7^30, ⌓ ^0 1 – 9
26	7	5.4	.	▽ ^0 16^44 ▽ ^1 – 17^15 ▽ ^0 18^02; (K) W 16^30 K ^0 16^44 – 17^55 – (K) 18^05 E, ≫ 16^20 – 50 (por. 18 m/sek), = 4^30 – 8^30, 19^30 – 24, ⌓ ^0 2 – 7^30
27	7	6.1	.	▽ ^1 0^01 – 03 ▽ ^0 – 0^27, 11^51, 12^18 ▽ ^1 – 12^22 ▽ ^0 – 12^40, 16^00 – 17^32; (K) W 11^50 K ^0 11^51 – 12^35 – (K) E 13^25 (K) SW 16^30 – K ^0 16^25 – 17^03 – (K) SE 19^02; = 0^00, 7^30, 18^30 – 24
28	8	.	.	= 0^00 – 7^30, ⌓ ^0 23 – 24
29	7	0.0	.	● ^0 9^40 – 10^32; ⌓ ^0 0^00 – 9^40, 21^30 – 24
30	8	.	.	= 21^30 – 24; ⌓ ^0 0^00 – 2 ⌓ ^1 – 3 ⌓ ^2 – 5 ⌓ ^1 – 6 ⌓ ^0 – 9
31				
Σ	–	52.3	–	

Łódź-Lublinek — φ = 51°44' — λ = 19°24' — Lipiec – Juillet 1965

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	87.1	89.4	90.6	89.0	18.4	15.2	13.6	15.2	19.7	13.3	75	93	82	83	5.3	1.2	2.8	3.1	10	10 •	8	W 8	NW 6	WNW 2
2	91.1	89.5	87.4	89.3	11.3	16.8	14.0	14.0	19.0	6.8	86	49	65	67	1.8	9.7	5.6	5.7	9	6	9	NW 3	WNW 4	W 4
3	86.5	86.8	87.2	86.8	12.2	13.8	10.4	11.7	15.9	10.3	81	61	92	78	2.6	6.2	1.0	3.3	10	9	3	W 4	W 7	SW 5
4	88.0	87.2	86.8	87.3	10.9	13.1	11.6	11.8	16.4	5.3	79	75	84	79	2.7	3.8	2.1	2.9	7	9	6	SW 3	SW 3	S 2
5	86.8	86.1	87.9	86.9	11.6	15.9	10.0	11.9	17.3	7.8	90	47	92	76	1.3	9.5	1.0	3.9	9	10	3	C 0	W 3	WSW 3
6	90.4	89.2	90.5	90.0	10.7	15.3	9.4	11.2	16.7	5.6	76	52	92	73	3.1	8.4	1.0	4.2	5	9	7	W 6	SW 10	SW 3
7	91.4	90.0	88.1	89.8	10.8	16.2	13.6	13.6	19.5	8.2	89	66	93	83	1.5	6.3	1.1	3.0	10	10	9	SW 4	SW 5	SE 4
8	85.4	81.8	80.1	82.4	14.4	22.6	13.4	16.0	23.5	10.0	87	54	94	78	2.2	12.5	0.9	5.2	9	9	9	SSE 4	S 5	W 3
9	84.5	87.1	89.7	87.1	12.0	15.8	12.1	13.0	16.6	10.4	76	47	71	65	3.3	9.4	4.1	5.6	6	7	4	W 9	WSW 9	WSW 5
10	92.0	92.3	93.6	92.6	10.6	13.4	11.4	11.7	16.4	6.6	84	75	85	81	2.1	3.8	2.0	2.6	9	10 •	7	SW 5	W 9	WSW 4
11	96.0	96.7	96.5	96.4	10.8	17.4	13.8	14.0	19.5	6.8	92	47	69	69	1.0	10.5	4.9	5.5	4	7	1	W 5	W 7	S 3
12	94.7	92.0	90.0	92.2	14.2	20.8	15.9	16.7	22.4	10.0	76	51	97	75	3.9	12.2	0.6	5.6	5	10	10 •	SSE 6	SSW 9	W 6
13	94.9	93.5	94.0	94.1	15.0	21.7	19.3	18.8	22.9	13.3	93	54	78	75	1.1	12.0	4.8	6.0	10	7	0	W 4	SW 4	SE 3
14	94.4	94.4	94.5	94.4	19.2	28.8	23.3	23.6	30.5	14.2	81	46	69	65	4.2	21.4	9.0	11.5	4	8	3	SE 4	SW 5	SSE 5
15	95.6	95.6	94.6	95.3	21.8	29.1	23.0	24.2	30.1	16.9	72	39	81	64	7.2	24.6	5.3	12.4	4	3	2	ESE 5	SSE 7	SW 2
16	93.8	92.6	92.1	92.8	22.0	27.9	22.2	23.6	28.9	17.1	69	41	80	63	8.1	22.3	5.4	11.9	0	2	4	SE 3	E 5	NE 6
17	91.1	90.2	90.3	90.5	20.3	21.0	17.5	19.1	24.4	17.5	83	71	95	83	3.9	7.3	1.0	4.1	4	9 • K	10	ESE 4	NW 9	ESE 4
18	89.8	91.9	94.3	92.0	14.5	15.0	16.1	15.4	19.0	14.0	99	93	69	87	0.2	1.1	5.6	2.3	10 •	10	7	NE 8	NE 9	NNE 6
19	97.1	97.7	98.1	97.6	17.3	21.8	17.2	18.4	22.9	12.9	70	45	70	62	6.0	14.3	5.8	8.7	3	4	1	E 3	E 5	E 4
20	98.6	97.1	94.4	96.7	15.8	22.2	18.2	18.6	23.9	11.1	68	42	69	60	5.7	15.5	6.4	9.2	1	2	3	SE 7	SE 8	ESE 6
21	90.9	88.6	86.3	88.6	15.6	24.6	17.1	18.6	25.4	13.4	83	56	94	78	3.0	13.6	1.2	5.9	5	8	9 •	SE 7	SSE 8	SE 4
22	88.1	89.0	87.8	88.3	16.8	22.2	19.6	19.6	24.5	15.4	93	54	69	72	1.4	12.4	7.1	7.0	9	5	2	W 6	W 8	C 0
23	86.0	85.4	87.0	86.1	17.9	16.8	14.2	15.8	23.2	14.0	78	95	93	89	4.4	1.0	1.1	2.2	9	10	1 • K	SE 3	SW 3	SSW 4
24	86.6	87.2	89.1	87.6	16.5	23.3	16.8	18.4	25.2	12.7	87	57	81	75	2.6	12.4	3.7	6.2	8	7	3	S 6	W 8	W 2
25	91.3	90.7	88.0	90.0	15.5	21.9	18.7	18.7	23.4	10.7	80	41	67	63	3.5	15.5	7.1	8.7	2	9	2	SW 4	WSW 8	SSE 4
26	89.5	89.5	87.9	89.0	15.4	19.8	15.2	16.4	21.4	12.3	83	51	70	68	3.0	11.4	5.1	6.5	8	8	6	WNW 6	W 8	SW 4
27	87.8	89.3	89.7	88.9	13.0	14.0	12.5	13.0	16.1	10.8	81	55	80	72	2.8	7.2	2.9	4.3	10	9	10	WSW 6	W 9	WSW 5
28	90.7	91.5	90.1	90.8	12.0	14.6	12.2	12.8	16.4	10.4	82	62	94	79	2.5	6.3	0.9	3.2	9	9	10	W 7	W 7	SW 3
29	86.9	85.3	81.1	84.4	13.2	19.1	15.4	15.8	22.9	11.8	83	62	72	72	2.6	8.3	5.0	5.3	9	9	9	SW 6	SW 7	SW 5
30	77.4	76.2	79.6	77.7	15.4	21.2	13.0	15.6	22.2	12.9	77	50	78	68	4.1	12.7	3.3	6.7	10	6	4	SW 7	SW 10	SW 7
31	81.1	79.6	81.4	80.7	13.4	19.4	12.6	14.5	20.7	10.9	82	58	95	78	2.8	9.3	0.7	4.3	9	9	10 •	SW 6	SW 7	WSW 2
M	89.9	89.5	89.3	89.6	14.8	19.4	15.3	16.2	21.5	11.4	82	58	81	74	3.2	10.4	3.5	5.7	7.0	7.7	5.5	5.1	6.8	3.9

Sierpień – Août

1	88.0	89.3	88.9	88.7	9.4	16.0	13.6	13.2	17.9	9.2	95	49	77	74	0.6	9.2	3.5	4.4	10	6	10	W 4	W 6	C 0
2	85.1	86.2	86.8	86.0	12.2	15.2	12.1	12.9	17.8	11.0	80	67	76	74	2.9	5.6	3.3	3.9	10	10	4	N 3	NNW 4	W 3
3	87.8	86.9	88.6	87.8	10.9	19.0	13.0	14.0	20.8	6.6	86	44	76	69	1.8	12.3	3.6	5.9	0	7	4	SW 3	W 5	S 2
4	90.1	91.3	93.8	91.7	13.4	15.3	11.3	12.8	17.7	10.6	85	90	91	89	2.3	1.7	1.2	1.7	9	10 • K	1	SW 6	SW 6	NW 4
5	97.5	97.4	97.4	97.4	11.4	20.6	16.6	16.3	21.9	7.6	88	57	77	74	1.7	10.3	4.4	5.5	4	7	0	WSW 2	W 6	C 0
6	96.4	94.1	93.6	94.7	16.0	27.4	24.1	22.9	29.3	11.4	86	47	63	65	2.5	19.5	11.2	11.1	1	8	9	SSE 5	SSW 8	SW 9
7	93.1	91.2	90.8	91.7	21.2	29.6	23.3	24.4	30.1	19.2	77	43	60	60	5.8	23.4	11.6	13.6	4	5	4	SW 4	SW 7	SW 1
8	93.7	91.0	91.7	92.1	18.2	28.3	20.0	21.6	30.0	15.2	89	43	87	73	2.3	21.9	3.1	9.1	6	2	6	NW 2	S 5	WNW 3
9	94.8	96.4	97.9	96.4	14.6	12.7	12.2	12.9	20.2	12.1	82	92	99	91	2.9	1.2	0.2	1.4	10	10 •	9	NW 6	NW 6	SW 2
10	99.2	99.3	98.4	99.0	12.0	17.5	13.7	14.2	18.6	8.4	76	43	76	65	3.3	11.4	3.7	6.1	6	7	10	NNE 5	N 5	N 4
11	98.7	99.2	98.5	98.8	11.9	15.6	12.4	13.1	18.0	11.0	95	63	86	81	0.7	6.5	2.0	3.1	10 •	8	8	NW 3	N 7	NNW 5
12	99.1	100.1	99.1	99.4	10.0	14.6	11.1	11.7	17.2	9.3	97	67	96	87	0.3	5.5	0.5	2.1	10	9	9	N 6	NW 7	NNW 2
13	99.4	99.0	98.6	99.0	9.3	14.3	10.2	11.0	16.5	6.3	99	67	87	84	0.1	5.3	1.6	2.4	8	8	8	NW 4	NW 5	NW 5
14	98.5	98.0	97.2	97.9	9.2	15.8	11.6	12.0	17.3	5.3	95	57	83	78	0.6	7.8	2.3	3.6	7	8	9	NW 3	NW 7	NE 3
15	97.8	98.7	99.0	98.5	11.6	14.4	11.4	12.2	17.5	9.9	90	70	95	85	1.3	5.0	0.7	2.3	10	9	2	NNW 5	N 4	C 0
16	98.9	98.5	97.2	98.2	10.2	17.1	14.4	14.0	19.6	5.9	97	56	69	74	0.3	8.5	5.1	4.6	9	9	0	C 0	WNW 2	C 0
17	96.7	96.8	96.5	96.7	10.8	20.9	16.4	16.1	22.4	6.7	89	40	63	64	1.5	14.9	7.9	8.1	0	4	0	C 0	SW 3	C 0
18	97.2	97.9	98.6	97.9	13.1	23.0	17.2	17.6	24.1	9.6	79	37	62	59	3.1	17.8	7.4	9.4	0	4	0	C 0	SE 5	C 0
19	100.6	100.6	101.0	100.7	13.2	24.6	18.5	18.7	25.9	10.1	85	34	58	59	2.3	20.3	8.9	10.5	1	3	0	ESE 3	S 4	ESE 3
20	101.0	99.9	98.0	99.6	14.4	25.5	18.0	19.0	26.5	12.1	76	30	71	59	3.9	22.8	5.9	10.9	0	0	0	SE 3	S 5	ESE 5
21	95.3	92.1	90.5	92.6	15.6	26.8	20.3	20.8	28.4	12.7	83	35	64	61	3.0	22.8	8.6	11.5	7	5	0	SE 4	S 9	C 0
22	89.5	87.2	85.6	87.4	18.4	28.1	21.0	22.1	28.9	14.3	65	28	57	50	7.4	27.2	10.7	15.1	0	2	0	SE 5	SSE 9	SE 7
23	85.4	85.4	86.0	85.6	16.0	26.9	22.8	22.1	28.2	14.2	76	37	65	59	4.4	22.3	9.6	12.1	4	5	7	SE 3	SSE 6	SSE 4
24	86.9	87.3	85.2	86.5	18.2	25.2	18.9	20.3	26.0	17.4	77	56	89	74	4.9	14.1	2.3	7.1	9	9	10	SE 3	SE 1	S 2
25	83.0	84.3	87.8	85.0	17.6	20.0	13.6	16.2	20.1	13.5	97	88	95	93	0.6	2.9	0.7	1.4	10	10 •	10 •	C 0	SSW 3	NW 5
26	90.2	91.9	91.7	91.3	10.8	13.6	11.6	11.9	14.4	10.6	95	70	93	86	0.7	4.7	1.0	2.1	10 •	10	10 •	NW 8	NNW 8	NW 3
27	89.1	89.0	90.4	89.5	10.6	12.8	10.4	11.0	13.2	10.2	95	78	97	90	0.7	3.3	0.3	1.4	10 •	10	10	NW 5	NW 5	C 0
28	91.7	92.7	94.0	92.8	8.9	17.4	10.7	11.9	18.4	6.6	96	57	86	80	0.5	8.6	1.8	3.6	2	5	0	C 0	WNW 5	WNW 1
29	94.4	93.0	91.4	92.9	9.0	18.2	13.6	13.6	19.4	6.1	96	48	73	72	0.5	10.8	4.2	5.2	2	9	10	SW 1	SW 5	SSW 3
30	92.3	93.3	94.5	93.4	10.8	15.3	11.8	12.4	17.5	9.3	99	68	81	83	0.2	5.7	2.6	2.8	10	8	2	WNW 3	WNW 4	S 2
31	94.4	93.3	91.5	93.1	8.2	18.0	12.7	12.9	18.5	5.8	97	51	77	75	0.3	10.0	3.4	4.6	0	4	0	WSW 2	NW 5	C 0
M	93.7	93.6	93.6	93.6	12.8	19.7	15.1	15.7	21.4	10.3	88	55	78	74	2.0	11.7	4.3	6.0	5.8	6.8	4.9	3.3	5.	2.5

Łódź - Lublinek — $H_s = 187\,m$ — $H_b = 187.7\,m$ — $h_w = 10\,m$ — Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	POGODA
1	6	2.7	•	⛆° 7^02-15 ⛆¹-7^25 ⛆°-8^13, 10^32-11^20 •°... 12^40 •¹... 13^01 •°... 14^17; = 0^00-14^30; ⌓° 22^30-24
2	8	•	•	= 2^30-6^30; ⌓° 0^00-1^30 ⌓¹-3 ⌓²-6 ⌓¹-7 ⌓°-8
3	7	•	•	
4	7	0.0	•	⛆° 12^25-30, 17^15-20; ⌓° 1^30-2 ⌓¹-8 ⌓°-8^30
5	7	0.0	•	⛆° 10^35-11^07, 17^20-38; = 1^30-8^30; ⌓° 21^00-24; ⊕ 12^25-13^05
6	8	4.2	•	⛆° 13^03-07, 14^45-15^10 ⛆¹ 15^45-57 ⛆°-16^05, 16^53-58, 17^12-20, 18^45-19^14; ≫ 11^15-13^45; ⌓° 0^00-8
7	6	3.5	•	⛆° 18^25-30 ⛆¹-18^35 ⛆°-19^20; (K) W 18^30-K° 18^35-19^20-(K) S 20^10; = 3^30-13^30, 19^00-24
8	7	6.6	•	⛆° 0^12-38, 16-22, 6^10-16, •° 9^03...35 ⛆° 13^45, 14^20, 14^50-15^06, 16^35-44, 16^48, 17^01, 17^04-08 ⛆° 17^35-40 ⛆°-17^50 ⛆¹-19^05 •°-20^35; (K) SW 14^02-K° 14^07-30-(K) NE 14^45; = 0^00-11^30
9	8	0.0	•	⛆° 10^20-26, 21^40-22^03
10	7	0.2	•	⛆° 10^06-34, 12^40-48; = 23^20-24; ⌓° 21-22 ⌓¹-24
11	7	•	•	= 0^00-9^25; ⌓¹ 0^00-2 ⌓²-7 ⌓¹-9 ⌓°-10
12	7	4.9	•	•° 11^25-40 ⛆° 16^17-18^20... 19^00-21^03 •¹-21^10 •°-21^30; ≫ 10^30-11^25, 12^20-15^30; = 3^30-8^30; ⌓° 1-8
13	7	•	•	= 2^30-4^30 ≡°-5^10 ≡°-5^40 = -8^30, 20^15-24; ⌓° 21^30-24
14	7	•	•	= 0^00-9^30; ⌓° 0^00-8
15	7	•	•	= 20^30-24
16	8	•	•	= 0^00-7^30
17	6	1.3	•	⛆° 12^09-19 ⛆¹-12^22 ⛆° 13^08 •° 18^40-19^25; (K) SW 10^45-K° 12^27-13^05-(K) 14^35 NE; = 2^30-13^15, 14^30-16^15, 20^30-24; ⌓° 1-8
18	7	5.6	•	•° 4^41-6^14 •°-8^45, 10^45-12^30; = 0^00-12^30
19	8	•	•	
20	8	•	•	⌓° 3^00-8^00
21	7	6.3	•	⛆° 16^32-18^12 ⛆¹-18^26 ⛆°-18^40 ⛆¹-18^46 ⛆°-19^08, 20^36-21^03; (K) SW 16^05-K° 16^35-18^40-(K) NE 19^05; = 19^30-24
22	8	•	•	•° 0^28...3^43; = 0^00-8^30
23	6	4.0	•	⛆° 12^10-13^10; (K) S 12^05-K° 12^10-13^10-(K) N 13^35; = 4^30-6^10, 21^30-24; ⌓° 0-6^30
24	7	0.0	•	⛆° 10^20-23; = 0^00-7^30; ⌓° 2-4 ⌓¹-5 ⌓²-7 ⌓¹-8 ⌓°-9
25	7	•	•	(K) W 22^10-24; = 3^30-7^30; ⌓° 1-2 ⌓¹-7 ⌓°-8
26	8	•	•	(K) W 0^00-2^40 NE; = 4^30-6^30; ⌓° 1^30-7^30
27	8	•	•	⌓° 1^30-5^30, 23-24
28	8	1.3	•	•° 17^50-19^05, 21^45 23^20-23^58...24; = 3^30-6^30, 17^30-24; ⌓° 0^00-6
29	7	0.1	•	•° 0^00...1^45 7^53...8^32 18^27...19^18 22^42...24; = 0^00-9^30
30	8	9.0	•	•° 0^00...1^50 ⛆¹ 14^50-52 ⛆°▲ 14^55 ⛆¹ 14^58 ⛆° 15^04, 15^40-46 ⛆¹ 15^48 ⛆°▲ 16^51 ⛆¹ 15^54 ⛆° 16^12; (K) W 15^35 K¹ 15^42-K° 15^55 16^05-(K) E 16^16; ≫ 11^20-15^10 (por. 18 m/sek)
31	7	12.9	•	⛆° 14^50-57, 16^53-56 ⛆² 16^57 ⛆°▲ 16^59 ⛆² 17^00 ⛆¹-17^12 ⛆° 18^10, 20^30-21^18, 21^50-22^06; (K) W 16^50-K¹ 16^53 17^45-(K)° SE 18^08
Σ	-	60.6	-	

Sierpień - Août

1	7	•	•	= 3^30-8^20
2	7	0.9	•	•° 7^45...9^45 ⛆° 14^12-17, 16^20-27; ⌓° 23-24
3	8	0.0	•	⛆° 13^35-41; = 1^30-7^30; ⌓° 0^00-2 ⌓¹-8^30 ⌓°-9
4	6	5.2	•	•° 7^07-35 ⛆° 10^45-49 ⛆° 11^10-22 ⛆° 12^40 13^42, 14^14-20 14^50-15^28, 23^51-54; (K) W 12^44-K° 12^45-13^15-(K) 13^25 E; (K) W 15^08-K° 15^10-20-(K) E 15^25; = 5^45-9^30;
5	7	•	•	= 6^20-7^30, 19^50-24; ⌓¹ 4-7 ⌓°-8, 20^30-24 [4.VIII: ⌓° 0^00-7^07]
6	7	0.3	•	⛆° 21^02-15, 21^45-22^00; ⌒ 20^25-57; = 0^00-9^30; ⌓° 0^00-2 ⌓¹-8^30 ⌓°-9
7	8	•	•	
8	8	•	•	= 22^30-24; ⌓° 2^30-7^20, 23^30-24
9	7	1.2	•	•° 0^22...10^10, 11^50...13^05-14^40, 17^40-18^00; = 0^00-7^30, 19^30-24; ⌓ 0^00-7^30
10	8	2.2	•	•° 22^28...23^20-24; = 0^00-4^00
11	7	0.0	•	•° 0^00-2^15, 3^20-5^50, 8^40; = 3^00-8^30; ⌓° 23^45-24
12	8	2.6	•	⛆° 18^40-58, 19^10-12 ⛆¹-19^20 ⛆°-19^30 ⛆¹-19^34 ⛆°-19^58; = 4^30-9^20; ⌓° 0^00-9
13	8	2.9	•	⛆° 12^07-18, 13^43-48 ⛆¹-13^50 ⛆°-13^59; = 1^30-3^40 ≡°-4^20 ≡°-5^40 = -7^15
14	8	0.1	•	⛆° 14^10-44, 15^01-05, 16^52-17^02, 23^50-24; ⌓° 1^30-9
15	7	2.4	•	⛆° 0^00-04, 11-29, 9^40-46, 10^04-20, 15^45-16^22, 17^00-35; = 21^45-23^25 ≡°-24
16	8	•	•	≡° 0^00-3^45 = -4^30 ≡°-5^35 = -9^30, 21^00-24; ⌓° 20^30-21 ⌓¹-24
17	8	•	•	= 0^00-7^30; ⌓¹ 0^00-1 ⌓²-6 ⌓¹-7 ⌓°-7^30
18	7	•	•	= 2^30-8^30; ⌓° 2-8^30
19	7	•	•	= 4^30-9^30 ∞-11^20, 13^15-20^30 = -24
20	7	•	•	= 0^00-7^00 ∞-8^40
21	6	•	•	= 3^40-8^00 ∞-13^00
22	7	•	•	
23	7	0.0	•	
24	7	2.8	•	•° 4^35...5^10, 16^01...19^42; = 8^30-10^20
25	6	19.3	•	•° 0^40...5^43 •° 9^25...50 •° 10^40 11^30, 12^00 13^15, 13^50-15^25 •¹-15^35 •°-16^20, 17^10-19^10 •¹-19^35 •°-20^35 •¹-21^40 •°-22^39 •¹-23^05 •°-24; = 0^30-24
26	8	9.9	•	•° 0^00-3^40 •¹-4^20 •°-5^15 •¹-5^39 •°-8^30, 9^40, 20^35-21^40, 22^50-24; = 0^00-8^30
27	7	6.0	•	•° 0^00-1^10 •¹-3^20 •°-10^35 ⛆° 13^40-17^05 •°-19^40
28	7	•	•	= 3^30-8^30; ⌓° 20^30-24
29	7	0.1	•	= 3^30-9^25; ⌓° 0^00-2 ⌓¹-9 ⌓°-11^15
30	6	3.4	•	•° 0^42...2^41 ⛆° 13^00-15 ⛆¹-13^27 ⛆°-13^44; (K) NW 13^15-K° 13^20-40-(K) W 13^45; = 2^41-13^45
31	7	•	•	= 3^30-9^30, 19^30-24; ⌓° 3^00-6^00 ⌓¹-8^30 ⌓°-10^30
Σ	-	59.5	-	

Łódź - Lublinek φ = 51°44' λ = 19°24' Wrzesień - Septembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	89.8	90.8	92.8	91.1	12.0	21.0	16.4	16.4	22.9	10.0	79	52	82	71	3.0	11.9	3.2	6.0	6	6	8	SE 4	SSE 6	ESE 1
2	84.8	96.2	95.8	95.6	16.3	22.6	19.4	19.4	25.8	14.8	76	54	64	65	4.3	12.5	8.2	8.3	7	8	6	ESE 6	SE 7	SE 6
3	92.8	90.8	89.6	91.1	17.6	27.1	20.8	21.6	27.6	15.7	76	43	69	63	4.7	20.3	7.6	10.9	4	8	8	SE 6	SSE 7	SE 3
4	87.9	88.4	88.8	88.4	17.0	17.3	12.7	14.9	20.9	12.3	83	91	96	90	3.4	1.8	0.5	1.9	10 •	10 •	10	SE 3	ESE 4	WNW 3
5	89.8	90.0	88.3	89.4	12.4	20.1	16.3	16.3	21.9	9.9	93	57	76	75	1.0	10.1	4.3	5.1	10	5	5	SW 4	WSW 7	C 0
6	85.9	84.2	84.6	84.9	13.4	21.4	13.4	15.4	22.4	11.4	94	51	91	79	0.9	12.4	1.4	4.9	9	7	10	SE 3	S 8	WSW 6
7	85.4	85.8	87.8	86.3	9.7	15.6	10.2	11.4	16.8	8.3	92	50	81	74	0.9	8.9	2.4	4.1	3	8	0	SW 5	W 7	SSW 2
8	91.5	92.7	92.8	92.3	10.1	17.8	11.9	12.9	18.4	8.2	91	50	82	74	1.2	10.3	2.5	4.7	5	8	7	WSW 2	WSW 6	ESE 5
9	90.7	91.2	91.8	91.2	13.0	23.0	17.5	17.8	24.4	9.1	81	50	84	72	2.8	14.1	3.2	6.7	1	8	9	ESE 3	SW 6	C 0
10	88.6	88.0	90.8	89.1	14.0	23.4	13.8	16.2	23.9	12.5	92	50	93	78	1.3	14.5	1.1	5.6	8	7	9	SE 5	SSW 9	NW 2
11	85.7	90.5	93.1	89.8	16.0	12.5	10.6	12.4	16.5	10.4	96	92	95	94	0.8	1.2	0.7	0.9	10 •	10 •	10	SSW 7	W 7	W 3
12	92.9	92.6	91.0	92.2	8.6	17.0	11.6	12.2	17.9	7.0	100	55	81	79	0.0	8.7	2.6	3.8	2	6	7	C 0	SW 5	SSE 3
13	89.9	89.7	90.5	90.0	8.2	15.8	9.9	11.0	17.3	6.6	93	70	91	85	0.8	5.3	1.1	2.4	7	5	5	WSW 2	SW 2	C 0
14	92.3	93.6	95.8	93.9	8.0	16.6	12.4	12.4	18.0	6.5	97	49	79	75	0.3	9.6	3.0	4.3	9	3	9	SW 3	SW 4	WSW 2
15	97.8	99.6	102.6	100.0	11.4	15.8	9.6	11.6	16.5	9.3	89	53	95	79	1.5	8.4	0.7	3.5	9	9	0	W 5	W 8	C 0
16	105.2	104.8	102.8	104.3	4.0	17.8	12.6	11.8	18.9	2.8	100	50	79	76	0.0	10.3	3.1	4.5	0 ≡	2	0	C 0	C 0	SE 4
17	100.3	99.2	97.9	99.1	10.6	21.6	15.4	15.8	22.8	8.4	87	52	81	73	1.6	12.5	3.4	5.8	0	2	0	S 4	SW 7	S 2
18	96.8	93.9	92.0	94.2	12.8	22.2	15.6	16.6	23.3	11.3	86	43	75	68	2.1	15.3	4.4	7.3	0	0	0	S 6	S 8	S 3
19	95.7	99.0	102.0	98.9	13.2	13.6	9.8	11.6	16.0	9.7	82	79	81	81	2.8	3.4	2.3	2.8	9	10	0	W 3	W 4	W 2
20	105.5	107.9	110.7	108.0	6.6	13.0	8.8	9.3	14.2	5.3	94	75	96	88	0.5	3.8	0.4	1.6	9	9	0	WNW 4	NW 7	C 0
21	112.1	111.8	109.0	111.0	3.8	15.3	9.1	9.3	16.1	2.3	100	59	89	83	0.0	7.2	1.3	2.8	8 ≡	9	0	C 0	WNW 5	C 0
22	105.3	102.8	99.1	102.4	6.5	18.6	11.4	12.0	19.9	5.3	97	44	76	72	0.3	11.9	3.3	5.2	9	3	0	WSW 3	W 6	SW 3
23	97.1	95.7	93.9	95.8	9.6	21.1	13.8	14.6	22.7	7.8	95	47	80	74	0.7	13.4	3.2	5.8	3	3	0	SSW 3	S 5	S 1
24	93.9	94.1	93.6	93.9	10.2	22.8	14.6	15.6	23.4	9.3	91	35	80	69	1.1	18.0	3.3	7.5	0	0	0	SE 3	SSW 6	SE 3
25	92.8	91.6	90.1	91.5	9.9	22.8	15.0	15.7	23.2	9.3	93	48	78	73	0.8	14.3	3.6	6.2	0	6	0	ESE 3	SE 5	ESE 4
26	87.6	86.3	86.6	86.8	11.0	22.5	16.6	16.7	23.9	10.6	92	48	70	70	1.0	14.2	5.7	7.0	0	0	4	SE 5	SE 7	SSE 7
27	84.2	84.3	86.3	84.9	15.3	21.1	15.0	16.6	21.4	14.8	84	50	72	69	2.8	12.6	4.7	6.7	9	9	9	SE 7	SSE 12	SE 3
28	84.6	84.9	80.9	83.5	15.0	21.8	19.4	18.9	22.2	14.3	82	53	72	69	3.1	12.1	6.2	7.1	8	10	10 •	SSE 5	S 9	SSE 8
29	83.9	86.5	91.9	87.4	11.7	11.1	10.2	10.8	19.4	10.0	96	95	92	94	0.5	0.7	0.9	0.7	10 •	10 •	0	WNW 4	W 3	SSW 4
30	93.4	93.5	94.3	93.7	7.4	17.9	12.9	12.8	19.2	6.7	91	58	89	79	0.9	8.5	1.6	3.7	8	6	0	ESE 3	SSE 8	SSE 3
31																								
M	93.1	93.3	93.6	93.3	11.2	19.0	13.6	14.4	20.6	9.3	90	57	82	76	1.5	10.6	3.0	5.0	5.8	6.2	4.2	3.7	6.2	2.8

Październik - Octobre

1	96.8	97.4	97.5	97.6	9.2	21.9	14.9	15.2	21.9	8.8	97	52	86	78	0.3	12.6	2.4	5.1	0	0	0	C 0	E 3	E 3
2	96.6	95.9	96.0	96.2	10.7	19.4	14.6	14.8	20.2	10.2	92	58	80	77	1.0	9.3	3.3	4.5	0	1	3	SE 4	ESE 8	ESE 6
3	97.8	99.7	101.4	99.6	10.8	13.9	12.6	12.5	14.8	10.6	100	99	92	97	0.0	0.2	1.2	0.5	10 ≡	10 •	2	SE 2	NW 4	C 0
4	102.0	101.8	101.5	101.8	10.8	14.3	10.0	11.3	15.4	6.3	99	86	100	95	0.2	2.4	0.0	0.9	10	9	0	NE 2	C 0	C 0
5	102.2	102.8	103.2	102.7	5.0	13.4	8.0	8.6	13.7	3.9	100	76	100	92	0.0	3.7	0.0	1.2	10 ≡	4	10 ≡	C 0	NE 3	NNW 2
6	102.8	102.4	101.2	102.1	5.8	13.6	9.0	9.4	15.4	5.3	100	70	92	87	0.0	4.7	1.0	1.9	10 ≡	5	0	C 0	S 1	ESE 3
7	98.9	97.7	95.9	97.5	4.2	16.0	9.2	9.6	17.4	3.6	98	58	96	84	0.1	7.7	0.4	2.7	0	0	8	C 0	SSE 6	C 0
8	94.1	94.8	96.6	95.2	5.6	8.9	7.6	7.4	10.2	4.8	98	96	97	97	0.2	0.5	0.3	0.3	10 ≡	10	9	C 0	NW 5	WNW 1
9	97.3	96.9	95.8	96.7	3.8	9.9	6.7	6.8	11.4	2.3	97	68	88	84	0.3	3.9	1.2	1.8	9	8	9 •	WNW 2	NW 4	NNE 3
10	95.4	95.1	95.1	95.2	2.5	9.2	6.6	6.2	10.6	1.3	98	57	82	79	0.1	4.9	1.7	2.2	9	9	5	C 0	NW 7	W 6
11	95.2	94.2	97.6	95.7	5.0	9.8	6.0	6.7	11.0	3.3	100	64	76	80	0.0	4.3	2.3	2.2	10	9	9	WNW 3	W 9	N 5
12	103.7	105.8	106.4	105.3	-2.9	8.4	1.3	2.1	8.5	-3.2	99	43	81	74	0.0	6.2	1.3	2.5	0 ≡	8	0	WNW 1	NW 4	C 0
13	105.5	103.7	101.9	103.7	-0.3	11.0	4.8	5.1	12.2	-0.9	80	37	82	66	1.2	8.3	1.5	3.7	4	10	10	C 0	WSW 4	SW 3
14	100.9	100.7	100.1	100.6	1.3	13.9	6.5	7.0	15.4	0.9	89	50	78	72	0.8	8.0	2.2	3.7	0	6	0	SW 1	WSW 3	SE 1
15	99.5	98.6	97.2	98.4	2.0	16.0	8.4	8.7	16.9	1.3	87	42	71	67	0.9	10.5	3.1	4.8	1	3	2	SE 4	SW 7	SSW 6
16	95.6	93.2	97.8	95.5	7.0	17.8	8.2	10.3	18.8	5.3	70	43	97	70	3.0	11.7	0.3	5.0	7	5	10	SW 5	SW 6	WNW 7
17	102.0	104.8	105.9	104.2	6.2	10.6	5.2	6.8	11.3	5.2	92	56	86	78	0.7	5.6	1.2	2.5	4	4	0	WNW 7	WNW 7	W 4
18	104.5	103.7	103.4	103.9	4.8	8.9	8.2	7.5	9.6	2.4	87	72	89	83	1.1	3.2	1.2	1.8	9	10	9	WSW 4	WSW 6	W 3
19	104.0	105.7	106.7	105.5	5.8	8.8	4.9	6.1	9.6	3.7	98	76	94	89	0.1	2.7	0.6	1.1	10 ≡	8	10	NW 3	WNW 4	WNW 5
20	107.7	109.5	111.3	109.5	5.3	8.8	3.0	5.0	9.8	2.8	100	55	84	80	0.0	5.0	1.2	2.1	10	5	0	NW 4	NNE 7	ENE 4
21	112.4	114.1	114.4	113.6	-1.5	4.0	-0.7	0.3	5.2	-1.7	88	66	81	78	0.7	2.8	1.1	1.5	2	8	0	ESE 4	SE 5	ESE 2
22	114.8	114.2	112.7	113.9	-3.8	6.6	-1.1	0.2	7.8	-4.7	98	55	94	82	0.1	4.3	0.3	1.6	0	0	0	ESE 2	NE 2	C 0
23	109.7	108.4	106.9	108.3	-1.2	6.7	6.6	4.7	7.3	-4.0	95	81	93	90	0.3	1.9	0.7	1.0	10	9	10	WSW 2	WNW 6	NW 3
24	107.3	108.2	107.9	107.8	5.9	9.3	2.0	4.8	10.5	1.6	97	69	91	86	0.3	3.7	0.7	1.6	10	5	0	N 2	N 3	C 0
25	107.2	106.8	106.3	106.8	4.0	8.2	6.6	6.4	8.3	-0.7	95	77	90	87	0.4	2.6	1.0	1.3	10	10	10	C 0	WNW 4	C 0
26	104.4	102.9	99.5	102.3	6.1	5.8	2.7	4.3	7.2	2.6	94	88	93	92	0.6	1.1	0.5	0.7	10	10	0	NNW 3	S 6	SE 2
27	97.5	97.3	97.4	97.4	-0.8	10.4	4.2	4.5	10.9	-1.2	94	71	95	87	0.4	3.6	0.4	1.5	0	3	0	SW 2	WNW 7	C 0
28	95.7	94.7	94.3	94.9	3.3	13.4	9.6	9.0	14.4	2.3	90	68	82	80	0.7	5.0	2.2	2.6	8	10	0	S 3	SW 7	SW 5
29	92.6	91.1	92.6	92.1	6.4	16.2	10.5	10.9	17.2	5.3	82	60	90	77	1.7	7.4	1.3	3.5	3	2	10	SSW 4	WSW 6	WNW 7
30	97.7	97.8	95.3	96.9	4.3	9.4	3.6	5.2	10.7	3.2	88	71	83	81	1.0	3.4	1.3	1.9	0	5	0	WSW 7	W 7	SW 4
31	89.3	88.8	88.3	88.8	4.9	10.1	6.2	6.8	11.4	2.1	81	50	75	69	1.7	6.2	2.4	3.4	9	7	9	SW 6	WNW 10	WSW 5
M	101.0	100.9	100.9	100.9	4.2	11.4	6.6	7.2	12.4	2.7	93	65	88	82	0.6	5.1	1.2	2.3	6.0	6.2	4.4	2.5	5.2	2.8

Łódź - Lublinek $H_s = 187m$ $H_b = 187.7m$ $h_w = 10m$ Wrzesień - Septembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	= 0^{00}–11^{20}, 18^{30}–23^{00}
2	7	•	•	
3	7	•	•	por. wiatru 12 m/sek 12^{40}–15^{45}
4	6	29.2	•	●^{0}7^{02}–13^{15}, 15^{08}–19^{02} ●^{1}–19^{35} ●^{0}–24; = 6^{30}–24
5	7	0.3	•	●^{0}0^{00}–1^{20}, 5^{40}...6^{35}; = 0^{00}–9^{30}
6	7	0.4	•	●▽^{0}5^{05}–40, 19^{01}–23 ●^{0}21^{10}–22^{45}, = 3^{30}–8^{30}, 20^{30}–24; ⌒^{0}2–5^{05}
7	8	•	•	= 0^{00}–9^{30}; ⌒^{0}20^{30}–22^{30} ⌒^{1}–24
8	7	•	•	= 18^{30}–24; ⌒^{1}0^{00}–8 ⌒^{0}19^{30}–21^{30} ⌒^{1}–24
9	7	•	•	= 0^{00}–11^{20}, 21^{30}–24; ⌒^{1}0^{00}–8 ⌒^{0}–9
10	7	7.5	•	●▽^{0}22^{45}–23^{10}, = 0^{00}–9^{30}, 17^{30}–24; ⌒^{0}2–8^{30}, 20^{30}–22^{45}; ⊎ 20^{30}–21^{15}
11	7	0.2	•	●▽^{0}0^{25}–13 ●▽^{1}–18 ●^{0}–140 ●^{0}5^{35}–7^{35} ●▽^{0}8^{02}–08, 8^{40}–50, 12^{40}–13^{00}, 13^{10}–14; (K) SW 048–K^{0}0^{50}–1^{25}–(K) NE 135, (K) W 225–NW 330; = 0^{00}–3^{30}, 4^{30}–9^{20}
12	7	•	•	= 1^{30}–3^{55} ≡^{0}–6^{35} ≡–11^{30} 19^{30}–24; ⌒^{0}1–2 ⌒^{1}–3 ⌒^{2}–7 ⌒^{1}–7^{30} ⌒^{0}–8, 18–20 ⌒^{1}–24; ▽ 20^{30}–24
13	7	0.0	•	●▽^{0}11^{00}–12; = 0^{00}–9^{30}, 18^{30}–24; ⌒^{1}0^{00}–8^{30} ⌒^{0}–9^{30}, 19^{30}–24; ▽ 0^{00}–3^{00}
14	7	•	•	= 0^{00}–11^{30}; ⌒^{0}0^{00}–13^{0} ⌒^{1}–7 ⌒^{0}–9
15	7	•	•	= 0^{30}–11^{30} 21^{30}–23^{40} ≡^{0}–24; ⌒^{0}1–9^{30}, 18^{50}–20 ⌒^{1}–21^{30} ⌒^{0}–24
16	7	•	•	≡^{0}0^{00}–1^{00} ≡^{1}–7^{00} ≡^{0}–7^{05} =–9^{30} ∞ 16^{30}–17^{30} =–24, ⌒^{2}0^{00}–8 ⌒^{1}–8^{30} ⌒^{0}–9, 22^{30}–24
17	6	•	•	= 0^{00}–11^{30} ∞–17^{30} =–24; ⌒^{0}0^{00}–9, 22^{30}–24
18	7	1.7	•	= 0^{00}–8^{30}; ⌒^{0}0^{00}–8
19	8	0.1	•	●▽^{0}10^{00}–10 ●^{0}8^{08}...26, 10^{40}...11^{05}, = 4^{15}–6^{30}
20	7	•	•	= 22^{30}–23^{30} ≡^{0}–24; ⌒^{0}1–8^{30} 19^{30}–21^{30} ⌒^{1}–23 ⌒^{0}–24
21	7	•	•	≡^{0}0^{00}–1^{00} ≡^{1}–1^{30} ≡^{2}–4^{30} ≡^{1}–7^{00} ≡^{0}–7^{15} =–9^{30}, ⌒^{2}0–7^{30} ⌒^{1}–8 ⌒^{0}–9, 20^{30}–24
22	7	•	•	= 1^{30}–9^{30}; ⌒^{0}0^{00}–1^{30} ⌒^{1}–3 ⌒^{2}–8 ⌒^{1}–9 ⌒^{0}–10^{30}, 19^{30}–24
23	7	•	•	= 1^{20}–10^{30}, 17^{30}–24; ⌒^{0}0^{00}–2 ⌒^{1}–8 ⌒^{0}–9
24	7	•	•	= 0^{00}–8^{15} ∞–10^{20} = 17^{30}–24; ⌒^{0}1^{30}–2 ⌒^{1}–7 ⌒^{0}–7^{30}, 23^{30}–24
25	7	•	•	= 0^{00}–9^{30}; ⌒^{0}0^{00}–2 ⌒^{1}–8 ⌒^{0}–9
26	7	0.0	•	= 4^{40}–9^{30}, ⌒^{0}1^{30}–6 ⌒^{1}–7 ⌒^{0}–7^{30}
27	7	0.0	•	●^{0}1^{35}–45, 5^{40}...6^{25}, 9^{31}...58, ≫ 12^{10}–14^{15} (por. 18 m/sek)
28	7	2.8	•	●^{0}13^{32}–14^{30}, 15^{35}, 16^{12}...17^{32} ●▽^{0}20^{40}–21^{08}, 21^{32}–23^{18}, = 15^{20}–24
29	5	13.4	•	●^{0}5^{42}–14^{50}; = 0^{00}–24
30	8	•	•	= 0^{00}–30, 5^{15}–8^{30}; ⌒^{0}2–4 ⌒^{1}–6 ⌒^{2}–7^{30} ⌒^{1}–8 ⌒^{0}–8^{30}, 19–20^{30} ⌒^{1}–24
31				
Σ	–	55.6	–	

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1	7	•	•	= 4^{30}–11^{30}; ⌒^{1}0^{00}–4^{30} ⌒^{2}–8^{30} ⌒^{1}–9^{30} ⌒^{0}–10^{30}
2	7	•	•	= 5^{30}–8^{30}; ⌒^{0}1^{30}–5^{30} ⌒^{1}–8 ⌒^{0}–9
3	4	0.3	•	●^{0}12^{33}–14^{07} ●^{1}–16^{20} ●^{0}–17^{15}; = 5^{15}–6^{35} ≡^{0}–6^{42} ≡^{1}–7^{25} ≡^{1}–8^{06} ≡^{0}–8^{13} =–22^{30} ≡^{0}–22^{40} ≡^{1}–24
4	6	0.3	•	≡^{1}0^{00}–4^{25} ≡^{0}–5^{50} =–21^{30} ≡^{0}–22^{00} ≡^{1}–23^{40} ≡^{2}–24, ⌒^{0}19^{30}–21 ⌒^{1}–21^{30} ⌒^{2}–24
5	6	0.2	•	≡^{2}0^{00}–7^{30} ≡^{1}–8^{40} =–20^{35} ≡^{1}–21^{05} ≡^{2}–24; ⌒^{2}0^{00}–9 ⌒^{1}–10 ⌒^{0}–10^{30}, 18^{30}–19 ⌒^{1}–20^{30} ⌒^{2}–24
6	7	•	•	≡^{2}0^{00}–5^{10} ≡^{2}–8^{50} ≡^{1}–10^{12} ≡^{0}–10^{50} =–12^{30}, 17^{40}–24, ⌒^{0}0^{00}–11^{15} ⌒^{1}–12^{30} ⌒^{0}–13^{30}, 20^{30}–24
7	7	•	•	= 0^{00}–2^{50} ≡^{1}–3^{50} ≡^{2}–6^{10} ≡^{1}–6^{20} ≡^{0}–6^{25} =–9^{30}, 17^{30}–24, ⌒^{0}0^{00}–2 ⌒^{1}–4 ⌒^{2}–8 ⌒^{1}–9 ⌒^{0}–10^{30}, 18^{30}–23^{30} ⌒^{1}–24, ▽ 21^{30}–24
8	4	0.1	•	●^{0}13^{30}–14^{25}; = 0^{00}–4^{45} ≡^{0}–5^{10} ≡^{1}–6^{10} ≡^{2}–7^{10} ≡^{1}–7^{30} ≡^{0}–7^{45} =–11^{10} ≡^{0}–12^{05} =–23^{30}; ⌒^{1}0^{00}–1^{30} ⌒^{2}–12^{30} ⌒^{1}–13^{10} ⌒^{0}18^{30}–20^{30} ⌒^{1}–24
9	7	0.0	•	●▽^{0}10^{33}–37 12^{20}–23 20^{33}–56; = 5^{15}–8^{30}; ⌒^{0}0^{00}–8 ⌒^{0}–10^{33}
10	8	•	•	⌒^{0}22^{45}–24; ▽ 1^{30}–2^{20}
11	7	0.2	•	●17^{41}–18^{06} ●^{0} 19^{25}; = 2^{30}–9^{30}; ⌒^{0}0^{00}–2 ⌒^{1}–3^{30} ⌒^{2}–8^{30} ⌒^{1}–10 ⌒^{0}–10^{30}
12	8	•	•	= 3^{30}–5^{50} ≡^{1}–6^{25} ≡^{2}–7^{10} ≡^{1}–7^{18} ≡^{0}–7^{35} =–9^{15}, 21^{30}–24; ⌣^{0}1–2 ⌣^{1}–8^{15}, ⊕ 13^{00}–14^{15}
13	7	•	•	= 0^{00}–9^{30}, 17^{10}–24; ⌣^{0}1^{10}–3 ⌣^{1}–8 ⌣^{0}–9 ⌒^{0}22^{10}–24; ⊕ 13^{00}–14^{15} ⌣ 20^{38}–22^{30}
14	6	•	•	= 0^{00}–9^{20} ∞–15^{30} = 17^{30}–24; ⌒^{0}0^{00}–4 ⌣^{0}–8 ⌒^{0}20^{20}–24
15	7	•	•	= 0^{00}–10^{30} ∞–11^{30} = 16^{30}–24; ⌒^{0}0^{00}–4^{30} ⌣^{0}–8
16	7	4.8	•	●^{0}16^{45}–17^{40} ●^{1}–18^{45} ●^{0}–20^{35}; ≫ 16^{30}–18^{40}; = 0^{00}–8^{30} ∞–9^{40} = 15^{40}–20^{20}
17	7	•	•	
18	7	•	•	
19	7	•	•	= 1^{30}–6^{15} ≡^{0}–7^{40} =–11^{15}, 18^{30}–24; ⌒^{0}18^{30}–24
20	8	•	•	= 0^{00}–6^{10} ≡^{2}–6^{20} ≡^{1}–6^{25} ≡^{0}–6^{35} =–10^{20}; ⌒^{0}0^{00}–9^{20}
21	7	•	•	= 5^{30}–12^{30}, 16^{30}–24; ⌣^{0}3–10
22	7	•	•	= 0^{00}–10^{30}, 16^{30}–24; ⌣^{0}2–9^{45} ⌒^{0}18^{30}–20^{30} ⌣^{0}–24
23	6	•	•	= 0^{00}–24; ⌣^{0}0^{00}–7
24	7	•	•	= 0^{00}–10^{30}, 17^{30}–24; ⌣^{0}22^{30}–24
25	6	•	•	= 0^{00}–24; ⌣^{0}0^{00}–4
26	6	•	•	= 0^{00}–13^{30}, 18^{30}–22^{45} ≡^{1}–23^{10} ≡^{2}–24
27	6	•	•	≡^{2}0^{00}–1^{25} ≡^{0}–2^{40} =–24; ⌣^{0}2–5 ⌣^{1}–7 ⌣^{0}–9^{15} ⌒^{0}17^{30}–20^{30} ⌒^{1}–24
28	6	•	•	= 0^{00}–22^{45}; ⌒^{1}0^{00}–3 ⌣^{0}–8 ⌒^{0}22^{45}–24
29	6	0.4	•	●▽^{0}19^{10}–20; = 5^{30}–11^{30} ∞–16^{30} =–21^{30}; ⌒^{0}0^{00}–7
30	7	•	•	= 7^{30}–12^{30}, 16^{20}–24
31	7	0.4	•	≫ 12^{15}–13^{25} (por. 16 m/sek), = 0^{00}–10^{15}
Σ	–	6.7	–	

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	87.4	81.4	76.3	81.7	4.8	7.8	11.0	8.6	11.3	4.7	95	97	79	90	0.4	0.3	2.7	1.1	10 •	10 •	10 •	SW 6	SW 7	SW 8
2	74.7	78.0	80.4	77.7	10.9	10.5	7.3	9.0	12.3	7.1	69	39	73	60	4.0	7.8	2.7	4.8	9	8	9	SW 9	WNW10	WSW 7
3	84.8	86.5	88.5	86.6	3.6	9.1	4.0	5.2	9.2	3.3	85	61	82	76	1.2	4.6	1.5	2.4	0	4	10 •	WSW 5	WSW 8	WSW 6
4	93.9	97.7	101.4	97.7	1.4	6.4	3.4	3.6	7.0	0.8	94	69	83	82	0.4	3.0	1.3	1.6	9	4	10	W 6	W 7	WSW 2
5	104.7	106.0	108.3	106.3	0.4	2.6	1.8	1.6	4.0	-1.4	98	100	98	99	0.1	0.0	0.2	0.1	10	10	10	W 2	W 5	WNW 2
6	108.3	107.4	104.1	106.6	1.7	3.8	4.4	3.6	4.7	0.8	94	87	89	90	0.4	1.1	1.0	0.8	10	10	10 ♦	WSW 4	SW 5	WSW 5
7	100.2	99.1	99.3	99.5	3.8	6.0	4.6	4.8	6.6	3.5	98	86	93	92	0.1	1.3	0.6	0.7	10 ≡	10	9	WNW 3	SW 3	NNW 2
8	101.6	102.0	102.3	102.0	-0.8	6.5	1.5	2.2	7.3	-1.1	100	78	96	91	0.0	2.2	0.3	0.8	6 ≡	3	0	ESE 2	SE 5	ESE 2
9	101.5	100.5	99.1	100.4	-0.8	2.3	4.6	2.7	4.9	-1.7	94	98	100	97	0.4	0.1	0.0	0.2	10	10 ≡	10 ♦ ≡	SSW 1	SW 2	C 0
10	97.9	97.3	96.1	97.1	3.0	5.4	5.2	4.7	6.0	2.6	100	98	97	98	0.0	0.2	0.2	0.1	10 ≡	10 ≡	4	W 2	NW 3	ENE 2
11	92.7	90.8	88.3	90.6	1.2	3.7	0.0	1.2	5.3	-0.2	98	75	88	87	0.2	2.0	0.7	1.0	9 ≡	9	10	E 2	E 3	NE 9
12	86.0	86.5	88.6	87.0	-1.8	-1.3	-1.6	-1.6	0.5	-3.7	86	80	82	83	0.8	1.1	1.0	1.0	10 *	9 *	10 *	ENE10	NE 10	NE 8
13	90.2	90.8	91.4	90.8	-3.9	-4.2	-4.9	-4.5	-1.4	-5.0	80	77	83	80	0.9	1.0	0.7	0.9	10 *	10 *	10 *	E 6	E 5	E 5
14	91.6	92.5	93.1	92.4	-5.8	-5.5	-5.6	-5.6	-4.6	-6.6	79	77	85	80	0.8	0.9	0.6	0.8	10 *	10 *	10 *	ENE 5	NE 7	NE 3
15	93.1	94.8	98.7	95.5	-6.4	-5.8	-9.2	-7.6	-4.6	-9.6	89	89	85	88	0.4	0.4	0.4	0.4	10 *	10 *	10 *	NE 2	NE 4	NNW 1
16	103.4	105.3	106.9	105.2	-9.7	-7.8	-11.2	-10.0	-6.9	-13.7	81	81	86	83	0.5	0.6	0.4	0.5	10 *	0	10	NW 1	NW 3	C 0
17	105.6	103.1	99.6	102.8	-10.0	-8.8	-12.2	-10.8	-6.3	-12.4	87	80	89	85	0.4	0.6	0.3	0.4	10	10 *	0	SSW 3	SE 3	SE 5
18	94.7	91.9	88.1	91.6	-16.2	-11.8	-10.4	-12.2	-10.4	-16.8	86	75	80	80	0.2	0.6	0.5	0.4	0	9	10 *	ESE 5	ESE 7	ESE 5
19	85.9	81.4	79.8	81.7	-8.4	-4.2	-0.6	-3.4	-0.4	-10.6	89	94	93	92	0.3	0.3	0.4	0.3	10	10 ⚠	10	ESE 4	ESE 4	SE 2
20	80.2	81.7	81.4	81.1	-2.4	-3.1	-3.9	-3.3	0.5	-4.4	98	93	96	96	0.1	0.4	0.2	0.2	10 ≡	10 ≡	10 ≡	N 2	NW 2	E 2
21	74.8	68.6	64.5	69.3	-0.9	1.0	2.2	1.1	2.4	-4.2	97	92	98	96	0.2	0.5	0.2	0.3	10	10 •	10 •	E 4	E 7	SW 6
22	75.3	82.9	89.6	82.6	-4.0	-1.2	-2.4	-2.5	2.3	-5.2	80	86	91	86	0.9	0.8	0.4	0.7	10 *	10 *	10 ⚠	NW 7	WNW 9	WNW 5
23	95.2	97.5	99.8	97.5	-10.6	-8.5	-12.8	-11.2	-1.0	-13.3	87	77	85	83	0.4	0.7	0.4	0.5	5	6	0	WNW 3	W 4	C 0
24	98.3	96.5	94.0	96.3	-12.4	-4.2	-8.0	-8.2	-3.6	-14.1	85	68	81	78	0.4	1.4	0.6	0.8	0	0	0	SE 2	S 4	SSE 8
25	92.4	92.7	93.5	92.9	-6.4	-2.4	-0.4	-2.4	0.4	-10.1	78	91	92	87	0.8	0.4	0.5	0.6	10	10 *	10	S 6	S 5	SW 3
26	85.5	81.1	81.4	82.7	-3.6	-0.6	1.8	-0.2	2.2	-5.4	74	70	78	74	1.3	1.8	1.6	1.6	8	9	10 *	SE 9	SSE 8	SSW 6
27	81.5	75.0	64.9	73.8	-3.2	0.6	2.1	0.4	2.6	-4.4	92	84	91	89	0.3	1.0	0.6	0.6	7	10 *	10 •	SSE 3	SE 5	SSE 7
28	67.1	70.9	73.5	70.5	3.2	2.3	0.9	1.8	3.9	0.0	86	68	92	82	1.1	2.3	0.5	1.3	10	7	10	SW 6	SW 8	WSW 7
29	78.4	82.4	76.8	79.2	0.2	0.9	0.2	0.4	1.9	-0.3	98	92	66	85	0.1	0.5	2.1	0.9	10 *	9	4	WSW 9	SW 6	SE 8
30	71.6	73.7	76.4	73.9	3.1	4.3	2.8	3.2	5.3	-0.2	74	77	70	74	1.9	1.9	2.2	2.0	10	10	10	SSE 9	S 5	WSW 4
31																								
M	89.9	89.9	89.5	89.8	-2.3	0.1	-0.8	-1.0	2.0	-4.1	88	81	87	85	0.6	1.3	0.8	0.9	8.4	8.2	8.2	4.6	5.5	4.3

Grudzień – Décembre

1	75.5	76.0	80.3	77.3	-0.1	2.6	2.4	1.8	3.2	-0.7	71	72	73	72	1.8	2.1	2.0	2.0	0	10	9	S 8	SW 10	SW 9
2	82.9	85.8	83.3	84.0	1.0	1.6	0.4	0.8	2.9	0.0	92	78	90	87	0.5	1.6	0.6	0.9	10 ⚹	7	0	SW 7	WSW 7	S 5
3	76.8	77.2	76.9	77.0	0.6	1.6	0.6	0.8	2.4	-0.7	67	76	90	78	2.1	1.7	0.6	1.5	10	10	10 *	S 8	SSW 7	SSW 7
4	77.4	79.0	81.4	79.3	0.4	1.8	-0.4	0.4	2.4	-0.6	94	89	92	92	0.4	0.8	0.5	0.6	10	8	0	SW 2	SW 5	SSW 4
5	82.3	80.6	68.5	77.1	1.5	3.0	1.2	1.7	3.8	-1.6	91	81	90	87	0.6	1.5	0.7	0.9	10	8	10 ⚹	SSW 4	S 5	S 10
6	72.2	74.6	79.5	75.4	5.4	7.1	5.0	5.6	7.3	1.2	83	52	69	68	1.6	4.8	2.7	3.0	8	3	8	SW 9	WSW 9	SW 9
7	83.8	86.6	88.6	86.3	2.4	4.5	2.5	3.0	5.1	1.0	80	73	79	77	1.5	2.3	1.5	1.8	4	7	10	WSW 6	SW 7	SW 5
8	89.3	91.4	94.1	91.6	1.2	2.8	0.8	1.4	2.9	0.3	85	77	90	84	1.1	1.7	0.7	1.2	10	10	6	SW 5	WSW 4	W 5
9	96.4	91.3	80.6	89.4	-0.7	2.4	1.6	1.2	2.9	-1.0	89	66	63	73	0.6	2.5	2.6	1.9	5	8	9	SW 5	SSW 9	SSW12
10	65.6	64.3	64.3	64.7	2.5	5.1	3.9	3.8	5.3	0.9	65	69	74	69	2.6	2.8	2.2	2.5	10	9	6	SSW10	SSW13	SW 10
11	70.8	72.3	73.7	72.3	3.2	2.8	1.0	2.0	4.4	0.8	78	67	79	75	1.7	2.5	1.4	1.9	9	8	8	WSW 5	WSW 8	SW 8
12	77.9	80.2	83.1	80.4	-1.0	0.8	-1.0	-0.6	1.7	-1.4	89	86	95	89	0.6	0.9	0.4	0.6	3	9	8	W 5	WNW 6	WNW 5
13	86.9	88.3	87.1	87.4	-2.0	-1.4	-3.5	-2.6	-0.3	-3.7	94	82	83	86	0.4	1.0	0.8	0.7	10	8	6	WNW 5	NW 3	SE 4
14	92.4	97.1	102.0	97.2	-3.6	-3.9	-6.6	-5.2	-2.6	-7.1	78	64	78	73	1.0	1.7	0.8	1.2	9	9	0	NW 5	WNW 9	WNW 7
15	98.1	95.5	99.0	97.5	-4.6	-0.8	-4.7	-3.7	0.1	-6.9	86	95	91	91	0.6	0.3	0.4	0.4	10 *	10 *	10	SW 7	WNW 5	NE 4
16	99.4	99.3	99.2	99.3	-8.4	-4.2	-12.8	-9.6	-4.1	-13.2	86	70	92	83	0.4	1.3	0.2	0.6	4	0	0	SSE 4	SSW 3	ESE 2
17	95.8	93.4	92.6	93.9	-9.0	-6.1	-3.6	-5.6	-3.0	-15.1	89	89	92	90	0.4	0.4	0.4	0.4	6	10 *	10 ⚠	SE 4	SE 4	SE 3
18	91.9	89.3	88.0	89.7	-0.2	1.7	5.3	3.0	5.5	-3.7	98	92	98	96	0.1	0.5	0.1	0.2	7	10 •	10 •	SE 4	S 6	SW 8
19	89.2	89.7	87.9	88.9	8.0	8.2	8.5	8.3	9.2	5.2	96	94	89	95	0.4	0.6	1.2	0.7	10 •	10 •	10 •	WSW 8	SW 9	SW 6
20	91.9	94.3	92.8	93.0	4.6	5.0	1.6	3.2	9.8	1.5	84	78	94	85	1.4	1.9	0.4	1.2	4	8	9	WNW 7	WNW 8	SE 3
21	88.3	88.0	91.2	89.2	2.4	2.1	0.4	1.3	3.0	0.0	96	96	98	97	0.3	0.3	0.1	0.2	10 •	10 •	10 *	SE 2	N 4	NW 2
22	94.4	95.4	95.5	95.1	-0.4	-0.6	-1.0	-0.8	1.4	-1.4	96	95	87	93	0.2	0.3	0.7	0.4	7	10	10	WNW 3	WNW 3	C 0
23	94.3	91.3	85.3	90.3	-1.7	-0.7	-1.8	-1.5	-0.5	-3.1	88	71	75	78	0.7	1.7	1.5	1.2	10	9	9	SE 2	SE 8	SSE12
24	79.5	76.6	73.1	76.4	-2.7	0.4	0.3	-0.4	1.2	-3.3	86	76	83	82	0.7	1.5	1.0	1.1	5	9	10	SE 7	SSE 9	SSE 7
25	67.7	65.8	65.1	66.2	-1.1	0.5	1.7	0.8	2.1	-1.5	85	78	80	81	0.9	1.4	1.4	1.2	10	10	9	SSE 7	S 8	S 7
26	65.4	68.5	76.0	70.0	1.8	2.1	0.2	1.1	2.6	-0.1	87	93	98	93	0.9	0.4	0.1	0.5	9	10 ♦	10 *	SSW 5	WSW 2	WNW 7
27	80.8	79.9	74.7	78.5	-1.0	1.0	0.6	0.5	1.2	-1.7	95	77	77	83	0.5	1.6	1.5	1.1	0	0	10	SW 5	SSW 6	S 7
28	70.5	74.3	82.5	75.8	-0.2	-0.1	-1.4	-0.8	0.9	-2.0	96	98	84	93	0.2	0.2	0.9	0.4	10 *	10 *	9	S 2	WNW 4	WNW 6
29	85.4	87.3	89.7	87.5	-1.7	-0.6	-0.9	-1.0	-0.5	-5.2	86	91	85	87	0.8	0.5	0.8	0.7	8	10 ⚠	9 *	SW 6	W 9	SW 6
30	87.8	82.5	81.5	83.9	-3.5	-0.9	0.2	-1.0	0.6	-5.8	81	75	77	78	0.9	1.4	1.4	1.2	8	9	10	SW 7	WSW 9	SW 9
31	81.9	82.5	83.2	82.5	1.2	2.0	1.6	1.6	2.4	0.0	89	85	89	88	0.8	1.1	0.8	0.9	10 •	9	10	SW 6	SW 7	SW 6
M	83.6	83.9	83.5	83.8	-0.2	1.3	0.1	0.3	2.4	-2.2	86	80	85	84	0.9	1.4	1.0	1.1	7.7	8.3	7.9	5.5	6.0	6.4

Łódź - Lublinek $H_s = 187 m$ $H_b = 187.7 m$ $h_w = 10 m$ Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ CUK	POGODA
1	6	1.3	•	•^{0} 6^{50} 6^{55} – 13^{10}, 18^{50} 19^{45} 20^{40} 22^{35}, = 6^{40} – 19^{30}
2	7	2.0	•	⚥^{0} 7^{12} – 50, ≫ 8^{45} – 10^{30} (por. 17 m/sek)
3	8	1.6	•	▽^{0} 0^{10} – 40 •^{0} 19^{45} 20^{15} – 22^{35}
4	7	•	•	= 5^{35} – 12^{30}
5	4	•	•	= 2^{30} – 7^{15} ≡^{1} – 10^{10} ≡^{0} – 11^{25} = – 13^{35} ≡^{0} – 16^{40} = 20^{45} ≡^{0} – 23^{30} = – 24, ⊔^{0} 2 – 8^{30}
6	6	0.1	•	•^{0} 9^{25} 10^{15} 10^{35} 11^{10} 15^{40} 19^{30} 23^{15} •^{1} – 24, = 0^{00} – 24
7	6	•	•	•^{1} 0^{00} 15 •^{0} – 3^{45}, = 0^{00} 5^{45} ≡^{0} – 7^{05} = – 24
8	6	•	•	= 0^{00} – 1^{45} ≡^{1} – 3^{30} ≡^{2} – 8^{30} ≡^{1} – 10^{05} ≡^{0} – 10^{10} = – 24, ⊔^{0} 4^{30} – 9^{30} ⊔^{0} 19^{30} – 21^{30} ⊔^{0} – 24
9	2	0.5	•	•^{0} 18^{35} – 22^{30}, = 0^{00} 7^{00} ≡^{1} – 7^{45} ≡^{0} – 10^{50} ≡^{1} – 13^{10} ≡^{0} – 13^{15} = – 14^{40} ≡^{0} – 15^{15} ≡^{1} – 17^{20} ≡^{2} – 21^{10}, ⊔^{0} 0^{00} 1^{50} ⊔^{1} – 3 ⊔^{2} – 8^{30} ⊔^{1} – 9 ⊔^{0} – 10
10	2	0.2	•	•^{0} 2^{20} – 5^{30} 16^{35} 18^{40} 19^{45} ≡^{0} 0^{00} 1^{10} ≡^{1} – 7^{30} ≡^{1} – 8^{15} ≡^{0} – 11^{40} ≡^{1} – 14^{50} = – 15^{02} ≡^{0} – 19^{15} = – 24
11	7	0.0	•	= 0^{00} – 5^{0} ≡^{0} – 7^{20} = – 12^{30} 17^{30} – 19^{30}
12	6	0.0		*^{0} 6^{40} 8^{03} – 12^{00} 24, por. wiatru 12 m/sek 0^{15} – 4^{40} ≫ 6^{35} – 19^{30}
13	6	0.1	•	*^{0} 0^{00} 5^{40} 6^{30} 8^{10} – 13^{16} 15^{00} – 40 17^{10} – 24
14	6	3.6	pł.	*^{0} 0^{00} – 24
15	5	3.4	7	*^{0} 0^{00} – 8^{10} *^{1} – 8^{35} *^{0} 13^{30} 14^{40} – 24
16	6	0.0	11	*^{0} 0^{00} – 8^{30} 9^{22}, = 9^{22} – 19^{35} ≡^{1} – 20^{40} = – 24, V^{0} 19^{35} – 20^{40}
17	6	0.0	11	*^{0} 7^{15} 13^{35}, = 0^{00} – 22^{30}
18	6	0.7	11	*^{0} 20^{40} – 24, = 6^{10} – 24
19	4	1.4	11	*^{0} 0^{00} – 1^{20} 2^{10} △^{0} 8^{20} – 9^{15} 10^{47} – 11^{57} *^{0} – 12^{20} △^{0} – 13^{30} *^{0} – 19^{10}, = 0^{00} – 24
20	3	0.0	10	△^{0} 17^{43} – 19^{15}, = 0^{00} – 1^{45} ≡^{0} – 10^{10} ≡^{1} – 11^{30} ≡^{0} – 18^{30} = – 19^{30} ≡^{1} – 24
21	4	8.0	10	•^{0} 0^{00} 10^{26} – 19^{25} 24, ≡^{1} 0^{00} – 3^{30} ≡^{0} – 5^{40} = – 24
22	6	0.9	7	•^{0} 0^{00} – 40 *^{0} 1^{30} – 3^{10} 6^{40} – 7^{30} *^{1} – 8^{15} *^{0} – 11^{10} 12^{00} – 15^{45} 15^{20} – 30 ⚥^{0} – 16^{15} *^{0} 18^{35} 19^{30} ⚹^{0} – 21^{10} *^{0} 21^{45} – 22^{30}, 23^{40} – 24, = 0^{00} – 13^{20}
23	7	•	8	*^{0} 0^{00} – 1^{15} – 2^{20}, = 15^{30} – 24, ⊕ 14^{10} – 15^{10}
24	5	•	8	= 0^{00} – 24
25	4	2.0	7	*^{0} 7^{30} – 8^{25} *^{1} – 10^{30} *^{0} 11^{35} *^{1} – 12^{00} *^{0} – 16^{40}, = 0^{00} – 2^{30} 14^{00} – 24
26	6	0.1	10	*^{0} 14^{22} – 35 *^{1} – 14^{43} *^{0} – 15^{04} *^{1} – 15^{15} *^{0} – 15^{20} 16^{20} – 17^{35} •^{0} p – 18^{30} *^{0} 20^{40} – 21^{30}, 22^{45} – 24, ⚥ 11^{40} – 12^{35}, ≫ 11^{40} 12^{35}, ⊔ 0^{00} – 18^{30}
27	5	3.2	8	*^{0} 0^{00} 1^{15} 11^{15} 13^{45} ⚥^{0} – 15^{38} •^{0} 16^{20} 19^{50} 20^{08} – 22^{44} 24, = 4^{30} – 24
28	7	1.2	3	•^{0} 0^{00} 1^{50} *^{0} 10^{10} – 35 ⚥^{0} – 11^{05} ⚥^{0} 14^{00} 04 14^{58} 15^{04} 15^{28} – 35 15^{45} – 16^{40} *^{0} – 17^{42} *^{1} – 18^{15} *^{0} – 19^{40}, ≫ 15^{40} – 18^{25} 20^{30} – 24, ⊔ 0^{00} – 7^{30}
29	7	1.0	2	*^{0} 0^{45} 1^{40} 2^{42} 3^{35} – 12^{10}, ≫ 0^{00} – 2^{0} 2^{15} – 5^{20}, = 16^{15} – 20^{30}
30	6	0.0	2	*^{0} 0^{43} 1^{28} •^{0} 10^{20} – 40, = 11^{15} – 15^{30}
31				
Σ	–	31.3	–	

Grudzień - Décembre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ CUK	POGODA
1	7	1.1	pł.	*^{0} 8^{25} – 30 9^{00} 11^{40} ≫ 9^{40} – 13^{40} (por. 13 m/sek)
2	7	0.5	pł.	•^{0} 7^{15} 2^{50} •^{0} 8^{40} •^{0} – 9^{20} •^{0} – 9^{40} ⊔ 17^{50} – 19^{30} 16^{30} – 24
3	6	4.6	pł.	*^{0} 3^{35} 5^{15} 7^{30} – 48 20^{30} 21^{00} – 15 *^{1} 23^{40} *^{0} 24, = 0^{00} – 24
4	6	0.2	5	*^{0} 0^{00} 1^{15} •^{0} 8^{40} – 9^{00} •^{0} – 9^{30} •^{0} – 10^{20}, = 0^{00} – 24
5	6	6.5	2	•^{0} 11^{50} – 21^{15} •^{1} – 22^{10} •^{0} – 23^{45} 24, ≫ 17^{35} – 24 (por. 15 m/sek) ⊔ 0^{00} – 17^{41}
6	8	0.1	•	•^{0} 0^{00} 3^{15} *^{0} 0^{00} – 3^{38} (por. 15 m/sek), por. wiatru 14 m/sek 13^{30} – 18^{15}
7	8	•	•	⚥^{0} 0^{43} – 1^{28}, ▽ 18^{30} – 19^{15} 21^{35} – 22^{30}
8	6	0.0	•	⚹ 21^{45} – 52, = 8^{30} – 24, ▽ 0^{20} – 2^{15}
9	6	•	•	≫ 15^{10} – 24 (por. 15 m/sek) 16^{30} – 17^{30}, por. 18 m/sek 17^{30} – 23^{40}, por. [illegible] 0^{00} – 15^{15}, ⊔ 5 – 11, ⊔ 19^{30} – 21^{00}
10	7	0.0	•	•^{0} 9^{17} 10^{40} ≫ 0^{00} – 2^{30} (por. 20 m/sek) 0^{00} – 1^{20}, por. [illegible]
11	7	0.0	•	⚥^{0} 1^{07} – 36 ⚥^{0} 6^{56} – 7^{04}
12	7	0.8	•	⚥^{0} 0^{50} – 1^{15} 1^{48} – 2^{02} 12^{50} – 13^{05} 13^{11} – 42 *^{0} – 15^{4} [illegible] – 1^{44}
13	7	•	•	*^{0} 0^{03} – 2^{52}, = 3^{30} – 8^{40} 15^{35} – 24
14	7	0.0	•	*^{0} 9^{05} – 30 – 10^{43} ⚥^{0} 11^{05} – 40 13^{00} – 16, ≫ 12^{35} – 14^{15} (por. [illegible] m/sek) [illegible] – 8^{30}
15	4	2.1	•	*^{0} 5^{40} – 7^{30} 9^{30} 9^{58} – 10^{27} *^{1} – 11^{20} *^{0} – 11^{30} *^{1} – 11^{45} *^{0} – 12^{30} *^{1} – 14^{40} *^{0} – 13^{20} *^{1} – 13^{26} *^{0} – 17^{25} ⚥^{0} – 19^{38}, = 5^{30} – 24
16	6	•	3	= 0^{00} – 18^{25} ≡^{0} – 19^{05} ≡^{1} – 19^{37} ≡^{0} – 19^{12} = – 24
17	5	1.7	3	*^{0} 9^{15} – 11^{15} *^{1} – 11^{35} *^{0} – 20^{15} △ – 22^{40}, = 0^{00} – 24
18	5	16.5	5	•^{0} 11^{15} – 20^{20} •^{1} – 23^{25} •^{0} – 24, = 0^{00} – 8^{10} ≡^{0} – 9^{15} = – 24
19	6	1.4	•	•^{0} 0^{00} – 7^{15} 10^{42} 11^{10} 14^{20} 17^{45} 18^{35} 19^{50} 21^{13} 23^{40} 24, = 0^{00} – 24
20	8	0.5	•	•^{0} 0^{00} – 3^{20}, = 0^{00} – 1^{00} 15^{30} – 24
21	5	4.8	•	•^{0} 1^{05} – 3^{40} 5^{00} – 12^{30} 13^{30} – 15^{20} ⚥^{0} – 17^{20} *^{0} – 19^{35} 21^{40}, = 0^{00} – 24
22	6	•	•	= 0^{00} – 24
23	7	•	•	≫ 18^{30} – 21^{20}, = 0^{00} – 1^{40}
24	6	0.0	•	*^{0} 16^{45} – 17^{23}, = 7^{30} – 24, ⊔ 5 – 12
25	5	•	•	= 0^{00} – 24
26	5	5.0	•	•^{0} 7^{40} 9^{02} – 10^{15} – 35 •^{0} 11^{22} – 12^{05} 13^{20} •^{0} 14^{42} 15^{10} – 15^{32} *^{0} – 17^{27} *^{1} – 19^{26} *^{0} – 21^{43}, = 0^{00} – 24
27	6	2.7	4	*^{0} 3^{46} 4^{42}, = 0^{00} – 24
28	4	1.5	7	*^{0} 3^{20} – 4^{25} *^{1} – 5^{45} *^{0} – 8^{20} 9^{20} – 14^{50} 15^{40}, = 0^{00} – 7^{40} ≡^{0} – 8^{20} ≡^{1} – 9^{15} ≡^{0} – 10^{50} = – 18^{30}
29	6	0.4	8	⚥^{0} 0^{07} – 20 ⚥^{1} – 0^{00} ⚥^{0} – 0^{30} ⚥^{1} – 0^{35} ⚥^{0} – 11^{30} *^{0} – 12^{20} △^{0} 12^{40} – 13^{35} *^{0} 19^{05} 21^{10} 23^{57} – 24
30	6	0.0	10	*^{0} 0^{00} – 2^{50}, ≫ 13^{30} – 15^{40}, = 7^{30} – 24
31	6	0.0	8	*^{0} 0^{16} 3^{35} •^{0} 6^{35} 8^{45}, = 0^{00} – 24
Σ	–	50.2	–	

Wrocław – Strachowice $\varphi = 51°06'$ $\lambda = 16°53'$ *Styczeń – Janvier 1965*

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	91.0	90.9	89.7	90.5	4.5	5.9	2.8	4.0	6.1	2.6	81	77	86	81	1.6	2.1	1.1	1.6	10	9	9	SW 7	SW 8	SSW 5
2	86.9	86.9	88.9	87.6	2.1	3.2	1.2	1.9	3.9	0.3	93	91	92	92	0.5	0.7	0.5	0.6	10	10 •	10	WSW 3	W 3	WNW 2
3	91.4	92.9	95.6	93.3	-0.4	1.6	1.0	0.8	2.1	-1.6	98	91	94	94	0.1	0.7	0.4	0.4	8	10	10	NW 2	NNW 2	N 2
4	100.0	104.3	109.3	104.5	0.2	1.0	0.3	0.4	1.3	-0.1	90	83	74	82	0.6	1.2	1.6	1.1	10	8	10	NW 2	NNW 3	NW 4
5	106.4	104.5	107.3	106.1	-0.4	0.4	1.6	0.8	1.8	-2.9	76	98	91	88	1.4	0.1	0.7	0.7	10	10	8	W 8	WNW12	WNW 6
6	108.0	108.5	108.9	108.5	0.8	1.6	0.0	0.6	1.8	-0.3	94	89	86	90	0.4	0.8	0.9	0.7	9	9	8	WNW 7	NW 4	N 4
7	111.5	109.8	104.8	108.7	-5.6	-2.2	-5.4	-4.6	0.1	-6.2	92	79	85	85	0.3	1.1	0.6	0.7	0	3	6	WNW 4	W 2	S 2
8	97.7	93.4	89.4	93.5	1.1	3.6	3.9	3.1	4.6	-5.8	89	81	90	87	0.7	1.5	0.8	1.0	10	8	10	SW 3	SW 7	WSW 5
9	90.6	91.0	93.0	91.5	4.9	4.1	2.6	3.6	5.7	1.1	89	93	89	90	1.0	0.6	0.8	0.8	10 •	10 •	10	W 9	W 4	W 9
10	86.0	90.2	106.1	94.1	0.4	1.7	-0.9	0.1	3.4	-1.1	98	92	87	92	0.1	0.5	0.7	0.4	10 ⁑	10 ⁑	10	S 3	NW 4	N 2
11	109.3	107.6	105.0	107.3	-1.2	1.9	1.3	0.8	2.4	-1.6	93	78	76	82	0.4	1.5	1.6	1.2	3	2	9	SE 7	SE 7	SSE 5
12	103.2	100.7	99.6	101.2	0.0	4.9	2.2	2.3	5.7	-1.1	88	61	63	71	0.7	3.4	2.7	2.3	9	7	0	SE 3	SSW 8	SSW 8
13	100.5	101.8	103.2	101.8	-1.0	2.5	0.6	0.7	3.4	-2.9	83	79	86	83	1.0	1.5	0.9	1.1	2	9	7	SW 3	SW 4	S 1
14	99.1	97.5	102.5	99.7	-1.5	2.4	2.2	1.3	2.9	-2.7	88	70	77	78	0.7	2.2	1.7	1.5	0	0	9	S 5	SW 6	SW 4
15	107.3	106.9	103.9	106.0	-0.4	4.8	0.3	1.2	5.4	-1.8	82	61	88	77	1.1	3.4	0.7	1.7	0	1	10	SW 5	SSW 5	SE 6
16	102.0	103.6	102.0	102.5	-0.4	2.4	-0.6	0.2	2.9	-1.0	90	73	88	84	0.6	2.0	0.7	1.1	10	10	0	SSW 3	WSW 6	S 6
17	90.2	85.1	77.9	84.4	2.7	6.4	4.6	4.6	7.7	-2.2	75	68	79	74	1.8	3.1	1.8	2.2	10 •	9	8	SSW10	SSW 9	SSE 8
18	80.9	80.6	79.4	80.3	3.3	5.5	2.6	3.5	6.8	2.3	74	65	74	71	1.9	3.1	2.0	2.3	10	6	8	WSW 8	WSW 8	SW 6
19	79.0	79.5	82.0	80.2	-1.4	2.2	-0.3	0.0	2.8	-2.5	91	71	88	83	0.5	2.1	0.8	1.1	7	8	8	SE 3	SE 2	S 5
20	82.3	79.9	77.1	79.8	-2.8	1.2	-0.4	-0.6	1.9	-3.8	95	79	88	87	0.2	1.4	0.7	0.8	10 ≡	2	10 ⁎	C 0	N 3	NNE 3
21	79.8	83.4	88.8	84.0	-0.7	0.0	-0.1	-0.2	0.3	-1.1	97	90	94	94	0.2	0.6	0.4	0.4	10	10	10	NW 3	WNW 3	W 3
22	90.7	92.5	95.2	92.8	-0.2	1.8	-0.4	0.2	2.4	-0.9	98	87	90	92	0.1	0.9	0.6	0.5	10 ⁎	8	8	WSW 2	SE 3	SE 3
23	99.0	101.7	106.5	102.4	-2.8	1.0	-2.5	-1.7	1.4	-5.6	91	77	91	86	0.5	1.5	0.5	0.8	5	1	3	ESE 2	SE 1	C 0
24	110.1	110.5	110.4	110.3	0.6	2.8	-0.2	0.8	2.8	-2.9	90	81	98	90	0.6	1.5	0.1	0.7	9	4	7	NW 2	NW 2	NW 1
25	106.8	104.6	102.3	104.6	-0.4	0.6	-0.5	-0.2	0.9	-3.1	100	90	92	94	0.0	0.6	0.5	0.4	10	10	10 ⁎	C 0	C 0	ESE 3
26	98.7	98.1	98.0	98.3	-1.1	2.6	-1.8	-0.5	3.6	-1.8	97	86	89	91	0.2	1.1	0.6	0.6	9	4	0	SE 3	SE 4	ESE 3
27	98.2	98.2	98.3	98.2	-0.2	0.3	0.0	0.0	0.8	-1.8	98	90	94	94	0.1	0.6	0.4	0.4	10	7	10	SE 6	SE 6	SSE 3
28	98.3	98.1	97.3	97.9	-0.4	2.7	-1.8	-0.3	2.8	-2.1	94	86	98	93	0.3	1.0	0.2	0.5	9	7	10 ≡	SE 4	SE 3	ESE 2
29	95.4	95.8	96.5	95.9	-1.4	1.0	0.6	0.2	1.8	-3.4	99	98	98	98	0.1	0.2	0.1	0.1	8	8	10	C 0	WNW 3	C 0
30	94.6	92.9	93.2	93.6	0.3	3.8	4.4	3.2	4.5	-0.5	98	88	84	90	0.1	0.9	1.4	0.8	10	10	10 •	ESE 2	SE 3	W 4
31	98.9	100.3	99.6	99.6	0.4	1.0	-0.7	0.0	4.4	-0.8	100	88	97	95	0.0	0.8	0.2	0.3	10 ≡	10	10 ⁎	NNW 3	E 2	NNE 3
M	96.6	96.5	97.2	96.8	0.0	2.3	0.5	0.8	3.2	-1.7	91	82	87	87	0.6	1.4	0.9	1.0	8.0	7.1	8.0	3.9	4.4	3.7

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1	102.7	103.3	107.2	104.4	-1.4	-1.0	-2.6	-1.9	-0.6	-2.7	90	81	83	85	0.5	1.1	0.9	0.8	10	9 ⁎	8	WSW 3	NW 4	NW 3
2	111.6	113.4	116.8	113.9	-2.2	-1.6	-4.4	-3.2	-1.1	-6.4	89	75	89	84	0.6	1.3	0.5	0.8	9 ⁎	9	2	NW 7	NW 8	NW 3
3	114.4	111.9	110.4	112.2	-2.8	-0.8	-2.6	-2.2	-0.4	-6.3	88	85	89	87	0.6	0.9	0.6	0.7	10	10	9	NW 5	W 4	WSW 3
4	110.7	111.5	110.3	110.8	-0.7	0.5	-0.4	-0.2	0.8	-2.6	91	80	96	89	0.5	1.2	0.2	0.6	10	8	10 ⁎	W 2	NW 4	NW 5
5	105.3	104.8	110.6	106.9	-6.2	-4.2	-11.4	-8.3	-0.3	-11.5	89	65	83	79	0.4	1.5	0.4	0.8	10 △	5	0	SE 5	ESE 5	NE 1
6	113.4	111.6	106.9	110.6	-14.2	-7.2	-5.8	-8.2	-5.4	-17.7	92	68	82	81	0.2	1.1	0.7	0.7	10	8	10 ⁎	C 0	SSE 3	SSE 2
7	104.8	105.0	96.9	102.2	-6.4	-4.3	0.6	-2.4	0.6	-6.7	86	72	94	84	0.5	1.2	0.4	0.7	10	9	10	SE 3	SSE 3	WNW 7
8	88.4	90.8	95.2	91.5	-2.1	-1.6	-2.6	-2.2	1.4	-2.6	81	75	83	80	1.0	1.3	0.9	1.1	9	9	9	NNW 4	NW 7	NNE 4
9	102.7	106.6	110.6	106.6	-6.0	-5.0	-15.0	-10.2	-2.3	-15.0	89	83	87	86	0.4	0.7	0.2	0.4	10 ⁎	10 ⁎	2	N 1	NNE 3	WSW 3
10	105.7	100.2	99.4	101.8	-10.4	-2.8	-0.6	-3.6	-0.6	-16.7	77	86	95	86	0.6	0.7	0.3	0.5	3	10 ⁎	10 ⁎	WSW 6	W 5	WNW 7
11	103.9	105.7	108.1	105.9	-5.6	0.6	-5.0	-3.8	1.1	-6.7	92	79	93	88	0.3	1.4	0.3	0.7	2	0	0	WNW 3	NW 5	W 3
12	106.8	106.6	104.8	106.1	0.1	2.2	1.2	1.2	2.3	-8.3	81	78	89	83	1.2	1.6	0.8	1.2	10	10	9	WSW 5	WSW 4	WSW 5
13	95.8	91.1	84.0	90.3	2.0	3.4	3.3	3.0	3.8	0.2	78	78	79	78	1.6	1.7	1.5	1.6	10 ⁑	9	5	SW 7	WSW10	SW 9
14	81.7	84.1	90.4	85.4	0.0	1.8	0.8	0.8	3.3	0.0	98	91	88	92	0.1	0.7	0.8	0.5	9	9 ⁎	9	W 7	WNW11	W 7
15	95.8	96.9	96.7	96.5	-1.8	0.4	-2.7	-1.7	1.5	-5.7	90	76	95	87	0.5	1.5	0.2	0.7	4	6	8	W 6	WNW 6	W 5
16	99.5	101.0	103.6	101.4	-4.6	-2.4	-6.0	-4.8	-1.9	-8.9	84	74	87	82	0.7	1.3	0.5	0.8	10	6	9	WNW 2	WSW 3	ENE 2
17	104.5	103.8	104.0	104.1	-5.0	-4.0	-2.5	-3.5	-2.3	-13.1	83	89	93	88	0.7	0.5	0.4	0.5	10	10 ⁎	10 ⁎	NW 3	NNW 5	N 3
18	106.7	108.1	109.4	108.1	-1.8	-2.8	-3.6	-3.0	-1.0	-5.7	86	86	85	86	0.8	0.7	0.7	0.7	10	10	10	NNE 5	N 3	N 3
19	110.6	110.6	112.2	111.1	-5.8	-3.2	-5.5	-5.0	-2.6	-6.1	89	81	77	82	0.4	0.9	0.9	0.7	10	10	10	NNE 5	N 4	NNE 2
20	113.8	115.7	117.0	115.5	-5.6	-4.4	-5.2	-5.1	-3.8	-6.4	92	67	78	79	0.3	1.4	0.9	0.9	10 ⁎	6	10	NNE 4	E 5	NE 2
21	114.6	112.7	108.0	111.8	-11.2	-5.4	-6.8	-7.6	-4.4	-11.3	90	77	85	84	0.3	0.9	0.5	0.6	2	9	10	NE 2	WSW 2	W 2
22	103.0	102.6	103.7	103.1	-4.6	-2.4	-3.3	-3.4	-0.7	-7.5	88	89	92	90	0.3	0.5	0.4	0.5	10	10	9	WNW 7	NW 4	NW 1
23	102.7	102.1	102.3	102.4	-6.8	-3.2	-4.1	-4.6	-2.5	-9.7	91	86	94	90	0.3	0.7	0.3	0.4	9	10 ⁎	10 ⁎	WNW 2	WNW 2	WSW 1
24	104.2	102.3	97.0	101.2	-5.1	-3.8	-9.0	-6.7	-0.1	-9.9	93	76	82	84	0.3	1.1	0.5	0.6	10	9	2	NNE 2	SSW 1	WSW 4
25	92.9	94.4	98.0	95.1	-2.0	-3.3	-9.0	-5.8	-1.3	-9.7	92	70	67	76	0.5	1.5	1.0	1.0	10 ⁎	9 ⁎	0	NW 7	NW 3	WNW 5
26	98.3	95.1	88.4	93.9	-6.4	-1.1	-2.8	-3.3	-0.8	-10.4	65	63	60	63	1.3	2.1	2.0	1.8	4	7	8	WNW 6	SW 7	SW 10
27	79.0	82.1	91.4	84.2	-1.8	-4.4	-4.2	-3.6	-1.3	-6.0	73	95	79	82	1.3	0.3	0.9	0.8	10 ⁎	10 ⁎	2	SW 8	W 8	NW 12
28	99.0	99.9	96.3	98.4	-11.4	-5.6	-7.5	-7.5	-2.5	-11.6	90	76	73	80	0.3	1.1	0.9	0.8	4	1	0	WNW 4	SSE 3	SE 6
29																								
30																								
31																								
M	102.6	102.6	102.8	102.7	-4.6	-2.3	-4.2	-3.8	-0.7	-8.0	87	79	85	84	0.6	1.1	0.7	0.8	8.4	8.1	6.8	4.3	4.[illegible]	4.3

Wrocław - Strachowice $H_s = 120\,m$ $H_b = 123{,}8\,m$ $h_w = 10\,m$ Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY h	POGODA
1	7	0.0	•	•°^{105} 3^{40} 23^{10}...46; = 15^{45}–24
2	5	0.0	•	•°8^{10}...20 11^{40}–13^{05}; = 0^{00}–24
3	5	0.0	•	△ 15^{35}–40; = 0^{00}–24; ⌴° 1–11
4	7	0.0	•	*°11^{30}–35; = 0^{00}–10^{35}, 11^{15}–12^{10}
5	6	0.2	•	*°0^{45} 10^{05} 10^{47}–11^{40} *¹–12^{20} *°15^{40} 16^{26} •° 18^{40}; ≫7^{15}–14^{15} (por. do 22 m/sek 8^{00}–13^{20}); = 10^{42}–14^{20} 15^{40}–22^{30}
6	7	0.3	•	*°14^{44} 15^{05}–17^{35} 18^{40}; = 13^{15}–22^{30}
7	8	0.4	1	*°23^{50}–24
8	7	1.5	1	*°0^{00}–2^{45} *°–3^{02} •°12^{40} 14^{05} 14^{26} 15^{30} 15^{45} 16^{10}–17^{32} 19^{35} 20^{10} 20^{32} 24; = 3^{30}–10^{05} 14^{25}–24
9	6	4.5	•	•°0^{00}...45 6^{45} 7^{20} 7^{30} 8^{10} 11^{40} 14^{30}–18^{10}; = 0^{00}–7^{10} 11^{50}–18^{15}; = 0^{00}–7^{10}
10	7	2.8	•	*°4^{10}–8^{20} 10^{05}–12 •°–10^{28} 11^{32} 12^{05} 12^{35} 13^{10}; = 5^{40}–8^{00} 14^{30}–24
11	7	•	•	= 0^{00}–4 5^{30}–6^{10} 16^{30}–20^{30}; ⌴° 18–24
12	8	•	•	≫14^{40} 16^{35} 18^{50} 20^{35}; ⌴° 0^{00}–11
13	6	•	•	= 9^{35}–10^{40} 12^{10}–14^{40} 16^{45}–24; ⌴° 3–10
14	7	•	•	≫13^{45}–15^{15}; = 0^{00}–10^{35} ∞ 14^{15}–16^{15} = –24; ⌴° 2–10
15	8	•	•	= 0^{00}–7^{30}; ⌴° 3–9; ⊽ 17^{40}–23^{20}
16	6	0.1	•	= 7^{20}–9^{40} 11^{30}–21^{30}; ⌴° 4^{30}–9 21–24
17	8	0.1	•	•°6^{15}–8^{20} 10^{50} 11^{15} 22^{10}...23; ≫6^{15} 14^{00} (por. do 19 m/sek 7^{35}–8^{36} 10^{14}–15 13^{02}–25); ⌴ 0^{00}–6^{15}
18	8	•	•	
19	8	•	•	= 16^{15}–40; ⌴° 5^{00}–10^{00} 22–24
20	6	0.5	•	*°15^{35}–16^{15} 17^{10} *¹–18^{40} *°–20^{30}...21^{35}; = 0^{40}–5^{30} = = –5^{50} = °–7^{40} = –13^{20} 15^{20}–24; ⌴° 0^{00}–12; ⊽ 0^{35}–4^{00} ⌣ –5^{30}
21	6	0.6	1	*°14^{35}–16^{28}; = 0^{00}–24
22	5	0.0	2	*°7^{40}–7^{35} 7^{45}–8^{15}...9^{40}; = 0^{00}–24; ⌴° 23–24
23	4	•	pł.	= 0^{00}–24; ⌴° 0^{00}–11 19–24; ① 13^{35}–14^{00}
24	6	•	pł.	= 0^{00}–24; ⌴° 0^{00}–10 22–24
25	5	0.2	pł.	*°8^{05}–9^{10} 20^{40}...23^{20}; = 0^{00}–17^{45} = °–18^{10} = –24; ⌴° 0^{00}–8
26	6	0.2	1	*°2^{05}–8^{35}; = 0^{00}–14^{15} 15^{20}–24; ⌴° 20–24
27	4	•	1	*°0^{40} 3^{40}; = 0^{00}–24; ⌴° 0–1
28	4	•	pł.	= 0^{00}–19^{25} = °–19^{32} = ¹ 20^{10} = ²–24; ⌴° 23–24
29	4	•	pł.	= ²0^{00}–3^{30} = ¹–5^{50} = °–9^{30} = –7^{15} = °–8^{20} = –24; ⌴° 0^{00}–11
30	4	0.2	•	•°5^{32} 16^{27} 19^{40}–22^{15}; = 0^{00}–8^{08} = °–9^{20} = –24
31	6	3.6	•	•°1^{40}...3^{15}–5^{30} •°13^{05}–14^{35} *°–16^{40} 17^{15}–23^{20}; = 0^{00}–5^{40} = °–7^{10} = –24
Σ	–	15.2	–	

Luty - Février

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY h	POGODA
1	7	0.0	3	*°2^{10}...9^{05} 9^{40}–10^{30} ⊽°11^{23} *°12^{45} 14^{02} 14^{53} 15^{20} 15^{27} 16^{18}; = 0^{00}–11^{45}
2	8	0.0	4	*°0^{20}...3^{40} 5^{40} 7^{05} 8^{05}–9^{05}...15 ⊽°–9^{35} 10^{10}–25; ✢ 10^{10}–13^{20}; = 9^{15}–10^{45}
3	7	0.2	4	
4	7	2.2	4	*°1^{40}–3^{35} 17^{40}...18^{30}–24; = 0^{30}–11^{20} 20^{20}–24
5	8	0.0	6	*°0^{00}–3^{20} △–10^{10}; = 0^{00}–10^{10} 17^{30}–24
6	6	0.5	6	*°19^{10}–22^{10} *¹–22^{35} *°–24; = 0^{00}–14^{30} 17^{30}–24
7	6	1.0	8	*°0^{00}–2^{15}; ≫22^{00}–24 (por. 20 m/sek 22^{12}–20); = 0^{00}–24
8	8	0.1	5	•°0^{40} 1^{50} •°2^{05} *¹ 2^{30} *°3^{00} *¹–3^{46} 4^{20}–5^{10} *°8^{30}...45 10^{35}–11^{10} ⊽°14^{15}–20 ⊽¹ 11^{40} ⊽°–12^{05} ⊽°–13^{30} 17^{02} ≫0^{00}–13^{0}; = 0^{00}–3^{30}
9	5	0.0	7	*°4^{10}–8^{30} 8^{30} *¹–9^{20} *°–10^{05}...20 11^{40} 12^{45} *¹–13^{10} *°13^{20}–30 ⊽¹ 14^{00}–20 = 5^{10}–6^{30} 8^{20} 10^{20} 12^{50} 14^{25} 19^{45}–24
10	6	0.8	9	*°11^{45}–12^{05} 12^{20} 13^{10} 13^{12} 15^{10} *°15^{20}–28 *°–16^{12} 19^{20}–21^{15}; ✢ 15^{15}–22^{30}; = 0^{00}–3^{30} 12^{25}–15^{05} 17^{15}–24
11	7	•	10	= 0^{00}–9^{45} 17^{10}–24
12	6	0.0	9	•°11^{40} 12^{05} •°10^{25}–43; = 0^{00}–24
13	7	0.1	2	*°5^{40} 6^{20} •°6^{35} 7^{10} 8^{05}–15 •°13^{03}–16 15^{50} 16^{15} 17^{45} 18^{10} ⊽°21^{35} 22^{05}; ≫10^{45} 11^{40} 12^{40} 13^{10} 13^{50} 16^{45} por. wiatru 17 m/sek 21^{35}–36; = 0^{00}–5^{35}
14	6	0.9	2	*°2^{40}...3^{05} ⊽°5^{35} 6^{30} 7^{32} 8^{05} ⊽°8^{17} *°8^{20}–40 ⊽°8^{45} 9^{15} *°9–11^{05} 11^{04} *°11^{14}–21 12^{31}–34 12^{50} 13^{02} ⊽¹–13^{05} ⊽¹ 13^{08} ⊽°13^{10} 13^{48} 14^{03} 14^{31}–35 15^{33}–36, por. wiatru 16 m/sek 22–23 ≫10^{15}–13^{50}
15	8	1.2	•	*°0^{00}–16 ⊽°16^{40}–45 ⊽² 17^{20} ⊽¹–18^{00} *°21^{05}–22 ⊽¹–21^{46} ⊽°–22^{02} ⊽¹–22^{23} ⊽°–22^{30} ⊽¹–22^{50} ⊽°–23^{03}
16	8	0.1	7	*¹7^{02}–10^{10} ⊽°14^{42}–15^{30} ⊽¹–16^{20} ⊽°–16^{30}; = 7^{10}–10^{20} 17^{35}–22^{40} = °–24; ⌴ 22^{40}–23^{30}
17	5	4.9	7	*°7^{25}–9^{10} 11^{05}–20^{01} *¹–20^{25} 21^{45}–22^{25} *°–24; = °0^{00}–15 = –6^{40} 11^{05}–24
18	6	0.0	11	*°0^{00}–5^{40} 9^{40} 10^{10} △10^{45}–11^{40}; = 0^{00}–15^{40} 17^{15}–24
19	6	0.9	10	*°9^{20}...10^{30}–11^{40}...12^{50} 15^{40}–17^{35}; = 0^{00}–24
20	6	0.0	12	*°2^{35}–8^{10} 0^{15}; = 0^{00}–24
21	6	0.0	12	*°8^{40} 10^{35}; = 0^{00}–3^{40} 6^{55}–7^{06} = °–7^{25} = –7^{35} = °–7^{37} = ¹–8^{30} = °–8^{45} = –24
22	5	0.3	10	*°2^{32}–3^{10} △8^{40}–9^{10} *°–17^{15} 13^{40} 14^{28} 19^{45}–20^{25} 21^{10}...30 23^{46} 24; = 0^{00}–15^{40} 16^{45}–24
23	6	0.7	12	*°0^{00} 1^{10} 12^{35}–14^{40} 16^{40} 19^{25}–20^{30} 23^{42}; = 0^{00}–9^{20} 12^{30}–24
24	7	0.0	10	*°9^{40} 10^{10}; = 0^{00}–1^{15} = °–2^{40} = ¹–4^{10} = °–4^{20} = –7^{10} 7^{45}–12^{35} 17^{15}–24
25	7	0.1	11	*°3^{35}–8^{30} *¹–9^{50} ⊽¹–11^{05} *°11^{42} 12^{15} ⊽¹–12^{35} ⊽°–13^{05}; ✢ 14^{5}–5^{40}; = 0^{00}–11^{15}
26	7	0.0	10	≫20^{20}–22^{30}
27	3	0.6	8	*°8^{40}–8^{05} ⊽°8^{42}–9^{05} 9^{15}–15 ⊽²12^{10}–17 12^{20}–30 △–12^{35} ⊽°–12^{40} ⊽²–13^{10} ⊽¹13^{35}–48 14^{52} 15^{10} 16^{03} 17^{30} *¹–18^{30} ⊽²–20^{40} 22^{35}–23^{15}; △18^{05}–10^{30} ✢°–13^{30} ⊥¹–13^{40} ⊥²–21^{40} ✢²–24;
28	8	•	9	✢°0^{00}–14^{0} [27 II: ≫7^{20}–11^{20} (por. 16 m/sek 10^{15}), por. wiatru 17 m/sek 12^{25} ≫14^{10}–17^{15} 18^{15}–21^{30} (por. do 19 m/sek); por. wiatru 16 m/sek 22^{02}–03
29				
30				
31				
Σ	–	14.6	–	

Wrocław – Strachowice φ = 51°06' λ = 16°53' Marzec – Mars 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	92.6	90.4	86.5	89.8	-9.0	0.6	-0.5	-2.4	0.9	-10.4	82	72	78	77	0.5	1.8	1.3	1.2	5	5	10	ESE 3	S 4	E 3
2	79.7	78.0	77.0	78.2	-0.2	1.0	-0.4	0.0	1.3	-1.0	96	90	98	95	0.2	0.7	0.1	0.3	10	10	10 ●	NNE 2	NNE 4	NNW 2
3	74.5	77.6	81.1	77.7	-3.6	-2.2	-3.2	-3.0	0.1	-4.1	92	83	92	89	0.4	0.9	0.3	0.5	10 *	10	10 *	WNW 6	WSW 7	WSW 12
4	86.0	87.8	90.0	87.9	-5.8	-3.6	-3.2	-4.0	-2.1	-5.8	87	76	57	73	0.5	1.1	2.1	1.2	10	10	10	W 10	W 10	WSW 6
5	92.2	94.7	98.8	95.2	-9.0	-0.9	-6.6	-5.8	-0.2	-9.5	82	71	91	81	0.5	1.6	0.3	0.8	8	3	3	WSW 3	WNW 4	C 0
6	101.9	103.2	106.9	104.0	-3.8	-0.8	-2.2	-2.2	-0.3	-10.9	80	81	85	82	0.9	1.1	0.8	0.9	10	10	10 *	ENE 2	NE 1	NE 1
7	110.7	112.6	113.9	112.4	-6.4	-5.0	-5.7	-5.7	-2.1	-7.8	81	68	74	74	0.7	1.3	1.0	1.0	10	8	10	NNE 3	N 3	N 2
8	112.6	111.6	110.9	111.7	-6.8	-4.6	-14.2	-10.0	-5.4	-14.2	75	64	87	75	0.9	1.5	0.3	0.9	10	1	0	NW 1	WNW 1	SW 1
9	110.8	110.5	111.1	110.8	-19.8	-2.8	-1.7	-6.5	0.9	-21.5	89	73	82	82	0.1	1.2	1.0	0.8	0	9	8	ESE 1	SE 1	WNW 6
10	115.0	116.5	117.3	116.3	-4.3	1.6	-5.7	-3.5	2.1	-7.2	89	62	79	77	0.5	2.7	0.8	1.3	9	0	0	W 2	WSW 2	SW 3
11	117.5	117.3	114.7	116.5	-12.2	0.5	-4.4	-5.1	1.4	-12.3	89	65	67	74	0.3	2.2	1.4	1.3	0	0	0	SE 1	SE 4	SE 2
12	113.7	111.7	110.6	112.0	-10.4	3.0	-2.2	-3.0	3.8	-11.4	87	62	79	76	0.4	2.9	1.1	1.5	0	0	1	C 0	SE 4	SE 3
13	110.3	110.1	109.8	110.1	-6.3	4.8	-0.7	-0.7	5.2	-6.8	89	67	83	80	0.4	2.9	1.0	1.4	0	0	0	SE 3	SE 3	SSE 2
14	108.4	107.7	106.8	107.6	-4.4	7.0	-0.7	0.3	7.9	-4.6	93	69	96	86	0.3	3.1	0.2	1.2	0	0	0	SE 2	SE 2	SSE 2
15	106.2	105.9	105.0	105.7	-0.3	8.3	3.6	3.8	10.0	-2.4	92	67	85	81	0.5	3.6	1.2	1.8	6	9	9	E 2	SE 2	C 0
16	101.2	99.4	100.8	100.5	2.6	11.4	4.4	5.7	12.6	2.0	93	58	98	83	0.6	5.6	0.2	2.1	10	9	10 ●	S 3	SW 6	WSW 4
17	100.7	98.0	96.4	98.4	1.8	12.8	5.8	6.6	13.3	0.9	98	56	86	80	0.2	6.5	1.3	2.7	0	2	10	SW 2	SW 5	WSW 3
18	93.3	90.6	89.4	91.1	0.8	13.4	6.3	6.7	14.5	-0.2	98	58	85	80	0.2	6.5	1.4	2.7	4	2	4	ESE 3	SSE 6	S 4
19	89.9	92.7	97.9	93.5	3.8	12.5	6.8	7.5	13.6	2.3	97	57	87	80	0.3	6.3	1.3	2.6	7	5	10	SW 3	WSW 6	WNW 6
20	102.8	102.8	101.2	102.3	1.0	8.0	6.0	5.2	9.6	0.5	92	47	83	74	0.5	5.6	1.6	2.6	5	2	10 ●	WNW 2	NNW 1	WNW 3
21	96.7	90.9	91.9	93.2	2.5	8.9	5.8	5.8	9.5	1.5	96	71	95	87	0.3	3.3	0.4	1.3	10 ●	10	10	ESE 5	SW 8	NW 8
22	98.6	100.9	101.8	100.4	-0.4	5.4	0.6	1.6	6.1	-0.7	92	47	63	67	0.5	4.8	2.4	2.6	8	5	0	NW 4	NNW 2	SSE 2
23	98.7	93.4	88.8	93.6	-1.4	6.9	4.4	3.6	8.7	-4.4	88	45	84	72	0.6	5.4	1.4	2.5	5	5	10	SE 4	SSE 9	SE 4
24	87.3	87.4	89.3	88.0	5.2	13.8	7.6	8.6	14.1	2.8	92	59	89	80	0.7	6.5	1.2	2.8	9	6	7	SSW 3	SW 6	WSW 4
25	94.0	97.5	100.1	97.2	5.6	7.0	3.3	4.8	8.8	3.1	83	73	93	83	1.6	2.7	0.5	1.6	10	8	8	WNW 9	WNW 9	WSW 3
26	100.6	96.9	98.7	98.7	3.4	7.8	3.6	4.6	8.4	1.5	95	65	95	85	0.4	3.7	0.4	1.5	9	10	9	SSW 3	S 6	W 3
27	109.0	113.9	117.1	113.3	4.0	6.8	3.4	4.4	9.0	3.0	97	80	95	91	0.2	2.0	0.4	0.9	10	8	0	NNW 3	NNW 5	SW 2
28	117.3	116.3	115.7	116.4	1.8	9.7	7.6	6.7	10.5	-0.7	98	63	99	87	0.2	4.4	0.1	1.6	9	10	10 ●	SE 2	SW 3	WSW 2
29	115.3	114.8	113.8	114.6	8.7	14.0	9.1	10.2	16.0	7.1	97	71	87	85	0.3	4.6	1.6	2.2	9	7	2	NW 4	NW 5	WNW 4
30	109.9	104.9	112.1	108.7	7.1	17.0	5.6	8.8	17.3	4.7	93	42	69	68	0.8	11.2	2.8	4.9	1	5	8	W 5	W 7	NNE 5
31	113.7	110.7	111.5	112.0	1.0	9.8	6.2	5.8	11.4	-1.2	90	49	54	64	0.7	6.2	4.3	3.7	1	6	2	WNW 5	NW 8	NNE 7
M	101.9	101.5	102.2	101.9	-1.8	5.6	1.2	1.6	6.7	-3.5	90	65	84	80	0.5	3.7	1.1	1.8	6.3	5.6	6.2	3.3	4.6	3.5

Kwiecień – Avril

1	115.1	116.6	115.2	115.6	1.3	6.4	0.8	2.4	7.6	-1.2	85	44	79	69	1.0	5.4	1.4	2.6	2	2	0	NW 2	N 5	WSW 2
2	110.8	110.7	110.8	110.8	3.2	11.6	3.1	5.2	12.8	-1.5	81	36	66	61	1.5	8.7	2.6	4.3	2	2	0	NW 7	NNW 6	W 1
3	106.7	103.4	102.4	104.2	1.2	15.6	7.2	7.8	17.1	-1.9	83	29	59	57	1.2	12.6	4.2	6.0	2	0	5	C 0	WNW 9	W 2
4	100.2	98.3	97.0	98.5	1.5	15.9	7.7	8.2	16.9	-0.5	89	35	71	65	0.8	11.8	3.1	5.2	6	2	7	WNW 1	NW 5	WNW 2
5	100.8	102.4	102.5	101.9	3.2	13.2	8.7	8.4	14.5	0.1	95	31	55	60	0.4	10.6	5.0	5.3	6	1	1	N 1	C 0	E 4
6	102.7	100.8	98.0	100.5	3.3	16.0	9.2	9.4	17.1	0.7	86	39	66	64	1.0	11.2	5.9	5.4	0	0	5	ESE 4	SE 8	SE 5
7	97.8	100.0	99.2	99.0	8.9	7.9	5.0	6.7	9.5	3.2	89	78	95	87	1.2	2.3	0.4	1.3	10	10	9	WNW 4	NW 4	NNW 2
8	98.1	96.8	96.0	97.0	1.1	12.8	9.6	8.3	14.0	-1.5	100	56	67	74	0.0	6.5	4.0	3.5	0 ≡	5	9	C 0	ESE 5	E 5
9	95.2	94.9	97.0	95.7	5.4	10.0	6.7	7.2	10.0	5.1	92	76	77	82	0.7	3.0	2.3	2.0	10 ●	10	10	E 5	E 6	E 7
10	98.7	99.7	99.8	99.4	3.9	5.7	4.7	4.8	7.0	3.8	80	73	74	76	1.6	2.6	2.1	2.1	10	10	10	ENE 4	E 5	ESE 5
11	97.1	96.5	96.2	96.6	1.7	4.6	5.8	4.5	7.4	1.5	78	71	80	76	1.5	2.5	1.8	1.9	10	10	8	SE 5	SE 6	NNE 1
12	98.5	99.7	98.8	99.0	3.0	6.3	5.3	5.0	7.7	2.0	95	84	97	93	0.4	1.5	0.3	0.7	9	10	9	WNW 2	WNW 2	SE 2
13	96.4	95.5	97.7	96.5	4.7	13.3	6.3	7.6	13.8	2.3	97	52	95	81	0.2	7.4	0.4	2.7	8	9	10 ●	SE 3	SE 6	NW 3
14	100.7	102.7	104.9	102.8	4.0	10.5	6.6	6.9	12.2	1.8	95	58	84	79	0.4	5.3	1.5	2.4	3	9	1	WNW 4	NW 5	N 2
15	104.6	103.1	100.4	102.7	2.8	10.8	6.2	6.5	12.0	-1.7	100	55	75	77	0.0	5.9	2.4	2.8	10 ≡	6	0	ESE 2	NNE 3	ESE 7
16	95.4	93.3	94.1	94.3	3.4	12.0	7.9	7.8	12.2	0.9	88	51	96	78	0.9	6.9	0.4	2.7	6	10	10	ESE 5	SSW 7	SSE 3
17	98.6	98.1	91.1	95.9	5.4	9.3	6.7	7.0	11.0	5.2	87	49	68	68	1.2	6.0	3.1	3.4	9	6	3	NNW 5	WNW 5	SSE 6
18	81.6	82.3	87.8	83.9	7.1	13.8	5.9	8.2	15.0	5.3	87	54	91	77	1.3	7.4	0.9	3.2	10 ●	5	10	S 3	W 7	W 4
19	88.9	88.0	86.9	87.9	6.0	8.0	6.2	6.6	8.3	4.5	95	80	97	91	0.5	2.1	0.3	1.0	10 ●	10	10 ●	SW 2	NW 1	NW 1
20	85.7	86.9	87.0	86.5	5.6	7.0	8.1	7.2	8.4	5.3	98	97	100	98	0.2	0.3	0.0	0.2	10 ●●	10 ●●	10 ●	NW 3	NW 2	NNE 2
21	87.0	87.0	86.3	86.8	8.1	9.9	7.4	8.2	10.0	7.3	90	83	96	90	1.1	2.1	0.5	1.2	10	10	10 ●	E 4	NNE 2	NNE 3
22	84.3	84.3	85.5	84.7	8.3	10.4	7.3	8.3	10.8	6.9	97	77	80	85	0.4	2.9	2.0	1.8	10	10	10	NNE 4	NE 5	N 3
23	84.3	85.2	86.5	85.3	5.4	6.5	6.3	6.1	7.9	5.1	92	88	94	91	0.7	1.2	0.5	0.8	10 ●	10 ●	8	NNW 5	NW 5	W 6
24	87.1	88.0	90.9	88.7	5.6	9.1	7.2	7.3	10.5	5.0	92	76	81	83	0.7	2.8	2.0	1.8	10 ●	9	9	W 7	WNW 10	W 5
25	93.0	93.7	95.0	93.9	7.6	8.0	6.5	7.2	9.7	4.8	79	87	73	80	2.2	1.3	2.6	2.0	6	10 ●	10 ●	SW 4	WNW 8	C 0
26	96.1	95.7	92.9	94.9	5.1	7.4	6.2	6.2	11.9	2.8	92	80	86	86	0.7	2.1	1.3	1.4	6	6	4	WSW 2	C 0	C 0
27	88.7	87.2	88.0	88.0	5.0	12.8	7.6	8.2	14.5	2.3	90	46	95	76	0.8	8.0	0.7	3.2	9	8	9	SE 5	SE 5	W 1
28	84.8	84.9	87.8	85.8	7.8	12.4	6.6	8.4	13.4	6.0	89	72	79	80	1.2	4.0	2.0	2.4	9	9	10	ENE 4	E 5	SSW 5
29	92.4	93.9	97.3	94.5	7.2	12.6	8.7	9.3	13.5	2.4	76	53	77	69	2.5	6.9	2.5	4.0	4	6	7	S 4	SW 5	W 3
30	100.6	101.4	103.3	101.8	8.2	14.4	9.0	10.2	15.5	5.9	71	56	90	72	3.2	7.1	1.1	3.8	7	4	10 ●	NNW 3	WNW 6	NW 3
31																								
M	95.7	95.7	95.9	95.8	4.8	10.5	6.7	7.2	11.7	2.7	89	62	81	77	1.0	5.3	1.8	2.7	7.1	7.0	7.1	3.5	4.9	3.2

Wrocław - Strachowice $H_s = 120\,m$ $H_b = 123{,}8\,m$ $h_w = 10\,m$ Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	0.6	9	
2	5	1.4	7	$*^{0}\,2^{15}\text{–}3^{30}\ 5^{20}\ \bullet^{0}\,16^{35}\ 18^{30}\ 21^{40}\ \backsim^{0}\text{–}24,\ =\ 0^{00}\text{–}24$
3	7	0.4	9	$\bullet^{0}\,0^{00}\text{–}3^{45}\ *^{1}\text{–}4^{35}\ *^{0}\ 5^{30}\ *^{1}\text{–}6^{20}\ *^{0}\text{–}6^{30}\ *^{1}\text{–}11^{15}\ *^{0}\text{–}11^{40}\ 16^{35}\ 19^{10}\text{–}24,\ +^{0\text{–}1}\ 19^{35}\text{–}24,\ \succ 17^{10}\text{–}24$ (por. 18 m/sek $22^{50\text{–}51}$), $=\ 0^{00}\text{–}12^{40}$
4	7	0.0	10	$*^{0}\,0^{00\text{–}10}\ *^{1}\,9^{00}\text{–}10^{30}\ *^{0}\text{–}12^{30},\ +^{0}\,9^{00\text{–}10}\ +^{1}\text{–}0^{40}\ +^{2}\text{–}4^{10}\ +^{0}\text{–}5^{30}\ +^{2}\text{–}12^{10}\ +^{1}\text{–}12^{40}\ +^{0}\text{–}13^{40},\ \succ 0^{00}\text{–}13^{45}$
5	6	•	10	$=\ 0^{35}\text{–}10^{20}\ \infty\text{–}17^{30}\ =\ 22^{38}\ =^{0}\text{–}22^{40}\ =^{1}\text{–}22^{50}\ =^{2}\ 22^{55}\ =^{1}\text{–}23^{05}\ =^{2}\text{–}23^{30}\ =^{1}\text{–}23^{40}\ =^{0}\text{–}24$
6	6	1.6	8	$*^{0}\,16^{02\text{–}40}\ *^{1}\text{–}20^{30}\ *^{0}\text{–}21^{20},\ =\ 0^{00\text{–}05}\ =^{1}\text{–}0^{07}\ =^{0}\text{–}0^{25}\ =^{1}\text{–}0^{38}\ =^{0}\text{–}0^{50}\ =\text{–}24$
7	7	0.0	12	$*^{0}\,22^{40}\text{–}23^{10},\ =\ 0^{00}\text{–}3^{30}$
8	6	0.0	11	$*^{0}\,8^{20}\ 9^{05},\ =\ 5^{35}\ 13^{10}\ \infty\text{–}16^{30}\ =\text{–}24$
9	4	•	10	$=\ 0^{00}\text{–}19^{30}$
10	8	•	8	$=\ 1^{30}\text{–}6^{30}$
11	7	•	6	$=\ 0^{00}\text{–}12^{40}\ 18^{20}\text{–}24$
12	6	•	5	$=\ 0^{00}\text{–}10^{00}\ \infty\text{–}18^{00}\ =\text{–}24$
13	6	•	3	$=\ 0^{00}\text{–}10^{30}\ \infty\text{–}17^{30}\ =\text{–}24$
14	6	•	pł.	$=\ 0^{00}\text{–}14^{30}\ \infty\ 15^{15}\text{–}16^{40}\ =\text{–}21^{35}\ =^{0}\text{–}22^{20}\ =\text{–}24,\ \sqcup^{0}\,21\text{–}24$
15	7	0.0	pł.	$\bullet^{0}\,12^{30\text{–}37},\ 22^{20\text{–}40},\ =\ 0^{00}\ 11^{20}\ 15^{45}\text{–}24,\ \sqcup^{0}\,0^{00}\text{–}8$
16	7	2.2	pł.	$\bullet^{0}\,5^{20\text{–}35}\ 6^{40}\text{–}7^{10}\ 14^{30}\ 15^{10}\ 17^{35}\ 18^{10}\text{–}22^{40},\ =\ 0^{00}\text{–}9^{15}\ 17^{30}\text{–}24,\ \oplus\ 9^{35}\text{–}14^{25}$
17	7	2.1	•	$\bullet^{0}\,22^{05}\text{–}23^{25},\ =\ 0^{00}\text{–}4^{40}\ =^{0}\text{–}4^{50}\ =^{1}\text{–}5^{15}\ =^{0}\text{–}5^{45}\ =\text{–}10^{40}\ 23^{30}\text{–}24$
18	7	•	•	$=\ 0^{00}\ 5^{35}\ =\ =\text{–}6^{40}\ =\text{–}7^{02}\ =^{0}\text{–}7^{05}\ =^{1}\text{–}7^{10}\ =^{2}\ 7^{45}\ =^{1}\text{–}8^{05}\ =^{0}\text{–}8^{09}\ =\text{–}12^{15}\ 18^{30}\text{–}24,\ \sqcup^{0}\,4\text{–}11$
19	8	•	•	$=\ 0^{00}\text{–}7^{30}$
20	8	0.5	•	$\bullet^{0}\,18^{35\text{–}40}\ 20^{40}\ 21^{05},\ =\ 23^{30}\text{–}24,\ \backsim^{0}\,6\text{–}9,\ Ci\ lot\ 10^{00}\text{–}11^{30}$
21	7	0.8	•	$\bullet^{0}\,3^{40}\ 4^{25}\ 5^{30}\text{–}7^{40}\ 8^{30}\ 15^{20}\ 16^{30}\text{–}18^{40},\ =\ 0^{00}\text{–}12^{40}\ 19^{30}\text{–}22^{30}$
22	8	•	•	$=\ 23^{30}\text{–}24,\ \sqcup^{0}\,22\text{–}24$
23	7	0.4	•	$\bullet^{0}\,22^{10}\text{–}24,\ =\ 0^{00}\text{–}4^{30},\ 9^{10}\text{–}10^{20},\ 22^{15}\text{–}24,\ \sqcup^{0}\,0^{00}\text{–}8^{30};\ \oplus\ 13^{30}\text{–}15^{20}$
24	8	0.0	•	$\bullet^{0}\,0^{00}\text{–}1^{20}\ 23^{40}\text{–}24,\ =\ 0^{00}\ 7^{40}\ 20^{30}\text{–}24$
25	7	0.4	•	$\bullet^{0}\,0^{00\text{–}25}\ \bullet^{0}\,9^{35\text{–}43},\ \succ 2^{45}\text{–}4^{15}\ 4^{45}\text{–}8^{15},\ 7^{00}\text{–}8^{40}$ (por. 18 m/sek $7^{40\text{–}41}$), $=\ 0^{00}\text{–}5^{35},\ 20^{30}\text{–}24$
26	7	1.0	•	$\bullet^{0}\,4^{40}\ 5^{20}\ \bullet^{0}\,13^{35}\ 14^{40}\ \bullet^{0}\,14^{45}\ 17^{20},\ =\ 0^{00}\text{–}8^{15},\ 23^{20}\text{–}24$
27	7	0.0	•	$\bullet^{0}\,7^{30}\ 8^{15}\ \bullet^{0}\,9^{20\text{–}35},\ =\ 0^{00}\ 12^{40}\ 18^{40}\text{–}24$
28	7	3.8	•	$\bullet^{0}\,14^{50}\ 15^{01}\ 17^{45}\ 19^{20}\ 22^{10}\ \bullet^{1}\text{–}24,\ =\ 0^{00}\ 8^{30},\ 18^{30}\ 24,\ \sqcup^{0}\,0^{00}\text{–}6^{00}$
29	7	•	•	$\bullet^{1}\,0^{00}\ 2^{40}\ 0^{00}\text{–}12^{20},\ 16^{05}\text{–}24$
30	7	0.0	•	$\bullet^{0}\,14^{43}\text{–}15^{01},\ =\ 0^{00}\ 10^{15}$
31	8	•	•	$\sqcup^{0}\,2\text{–}7$
Σ	–	15.2	–	

Kwiecień - Avril

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	8	•	•	$\sqcup^{0}\,5\text{–}7$
2	8	•	•	$\sqcup^{0}\,1\text{–}7$
3	7	•	•	$\sqcup^{0}\,2\text{–}7^{30}$
4	7	•	•	$\infty\ 9^{20}\text{–}11^{40}\ =\ 16^{30}\text{–}24,\ \sqcup^{0}\,2\text{–}7$
5	8	•	•	$=\ 0^{00}\text{–}9^{30},\ \backsim^{0}\,0^{00}\text{–}2^{30}\ \sqcup^{0}\text{–}6^{45}$
6	6	•	•	$=\ 7^{30}\text{–}10^{30}\ \infty\text{–}13^{30}\ =\text{–}24,\ \sqcup^{0}\,2\text{–}7$
7	7	2.4	•	$\bullet^{0}\,8^{15}\ 9^{10\text{–}40}\ 10^{02},\ =\ 0^{00}\ 10^{25}\ 12^{40}\text{–}24,\ \backsim^{0}\,2\text{–}8^{15}$
8	7	0.9	•	$=\ 0^{00}\ 3^{40}\ =^{0}\text{–}4^{15}\ =^{1}\text{–}5^{25}\ =^{2}\ 7^{05}\ =^{1}\text{–}7^{30}\ =^{0}\text{–}7^{35}\ =\text{–}11^{40}$
9	6	0.3	•	$\bullet^{0}\,4^{14}\ 5^{30}\text{–}6^{35}\ 7^{20}\text{–}8^{35}\ 9^{35},\ \succ 19^{05\text{–}40},\ =\ 4^{25}\text{–}24$
10	7	•	•	$=\ 0^{00}\text{–}4^{20}$
11	8	•	•	$=\ 19^{30}\text{–}24$
12	6	0.0	•	$\bullet^{0}\,8^{42}\ 9^{20}\ 12^{32}\ 15^{05}\ 15^{50}\ 16^{08},\ =\ 0^{00}\text{–}24;\ \backsim^{1}\,23\text{–}24$
13	8	1.6	•	$\bullet^{0}\,14^{05\text{–}10}\ 14^{43}\ 15^{10}\ 17^{45}\ 18^{08}\ 18^{48}\ 19^{10}\ \bullet^{0}\text{–}21^{05},\ =\ 0^{00}\text{–}8^{30}\ 20^{30}\text{–}24,\ \backsim^{2}\,0^{00}\text{–}8,\ 20^{30}\text{–}24$
14	7	0.0	•	$\bullet^{0}\,15^{45}\ 16^{35},\ =\ 0^{00}\text{–}5^{15}\ =^{0}\text{–}5^{35}\ =\text{–}10^{20},\ 20^{20}\text{–}24,\ \backsim^{0}\,22\text{–}24$
15	7	•	•	$=\ 0^{00}\text{–}1^{40}\ =^{0}\text{–}2^{20}\ =\text{–}3^{35}\ =^{0}\text{–}4^{30}\ =^{1}\text{–}4^{35}\ =^{2}\ 5^{20}\ =^{1}\text{–}5^{40}\ =^{0}\text{–}6^{00}\ =^{1}\text{–}6^{10}\ =^{2}\ 7^{45}\ =^{1}\text{–}8^{15}\ =^{0}\text{–}8^{20}\ =\text{–}9^{30}\ 22^{00}\text{–}24;\ \backsim^{0}\,0^{00}\text{–}4\ \sqcup^{0}\text{–}6$
16	7	1.0	•	$\bullet^{0}\,13^{40}\ 16^{05}\ 16^{15}\text{–}19^{20},\ =\ 0^{00}\text{–}10^{45}\ 16^{10}\text{–}24,\ \backsim^{0}\,1\text{–}9$
17	8	3.0	•	$\bullet^{0}\,0^{45}\ 1^{38}\ 3^{40}\ 6^{20},\ =\ 0^{00}\ 6^{00}$
18	8	2.5	•	$\bullet^{0}\,0^{50}\ 1^{10}\ 1^{20}\text{–}8^{20}\ \bullet^{0}\,15^{12\text{–}17}\ 15^{19\text{–}30}\ 16^{35}\text{–}17^{05}$
19	7	14.4	•	$\bullet^{0}\,5^{00}\ 7^{05}\ 9^{15}\ 11^{20\text{–}40}\ 13^{00}\ 17^{05}\text{–}24,\ =\ 5^{10}\text{–}10^{15}\ 18^{20}\text{–}24$
20	6	16.3	•	$\bullet^{0}\,7^{00}\ 8^{30}\ 5^{30}\text{–}7^{20}\ 8^{40}\ 9^{10}\ 10^{40}\ \bullet^{0}\,13^{00}\ 14^{35}\ \bullet^{0}\,17^{20\text{–}25}\ \bullet^{1}\text{–}19^{15}\ \bullet^{1}\,20^{20}\ \bullet^{0}\text{–}20^{50}\ 21^{15}\text{–}22^{30\text{–}40}\ R\ 17^{25}\ NE\text{–}18^{10}\ 18^{42}\ SW,\ =\ 0^{00}\ 7^{40},\ 12^{30}\text{–}24$
21	7	0.5	•	$\bullet^{0}\,3^{12}\text{–}28\ 5^{40}\text{–}6^{45}\ 10^{25}\ 21^{35},\ =\ 0^{00}\text{–}5^{45}\ 18^{20}\text{–}24$
22	7	1.0	•	$\bullet^{0}\,3^{35}\ 6^{45}\ 7^{40}\text{–}10^{10}\ 17^{45}\ 18^{10},\ =\ 0^{00}\ 11^{30}$
23	7	2.4	•	$\bullet^{0}\,6^{10}\ 10^{00}\ 13^{05}\ 15^{10\text{–}20}\ 17^{35}\text{–}18^{00}\text{–}20^{10},\ =\ 6^{20}\text{–}9^{00}$
24	7	0.0	•	$\bullet^{0}\,1^{45}\ 4^{10}\text{–}11^{30}\ 12^{15}\ 21^{44}\text{–}22^{10}\ \bullet^{0}\,18^{14\text{–}22},\ \succ 12^{05}\text{–}13^{40}$
25	5	2.8	•	$\bullet^{0}\,0^{45}\text{–}10^{05}\ \bullet^{0}\,11^{10}\ 12^{02\text{–}20}\ 12^{48}\text{–}13^{10}\ 13^{15\text{–}25}\ 19^{40}\ 23^{35},\ =\ 11^{10}\text{–}13^{20}$
26	7	0.1	•	$\bullet^{0}\,0^{45}\text{–}1^{20}\ 3^{25}\ \bullet^{0}\,12^{05\text{–}50}\ =\ 21^{20}\text{–}24$
27	7	0.0	•	$\bullet^{0}\,18^{45}\ 19^{10}\ 19^{40}\text{–}20^{45}\ 22^{10\text{–}35},\ =\ 0^{00}\text{–}10^{30}\ 19^{20}\text{–}24,\ \backsim^{0}\,2\text{–}9$
28	7	7.3	•	$\bullet^{0}\,9^{40}\ 11^{12}\ \bullet^{0}\,14^{05\text{–}07}\ \Delta^{1}\text{–}14^{13}\ \bullet^{1}\text{–}15^{06}\ \bullet^{0}\text{–}15^{16},\ =\ 0^{00}\text{–}12^{45}$
29	8	•	•	$=\ 3^{35}\text{–}4^{20}$
30	8	3.0	•	$\bullet^{0}\,13^{01\text{–}02}\ 16^{35\text{–}40}\ 16^{52}\ 17^{00}\ \bullet^{1}\text{–}17^{05}\ \bullet^{0}\,17^{07}\ 20^{45}\text{–}22^{10};\ K\ 15^{35}\ N\text{–}17^{00}\ 17^{12}\ E\ (K)\ SE\ 18^{00\text{–}30}\ S,\ =\ 4^{10}\text{–}6^{03}\ 23^{30}\text{–}24$
31				
Σ	–	59.5	–	

Wrocław – Strachowice φ = 51°06' λ = 16°53' Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	104.2	103.4	103.5	103.7	6.6	14.4	10.1	10.3	16.0	3.6	90	39	48	59	1.0	10.0	6.5	5.8	0	4	0	NW 3	W 4	NNE 3
2	106.8	105.4	103.8	105.3	4.0	11.1	5.8	6.7	12.0	-0.5	75	46	68	63	2.0	7.2	2.9	4.0	2	5	0	E 1	E 2	ESE 3
3	104.3	103.8	104.0	104.0	4.2	10.6	6.7	7.0	11.8	-1.3	75	45	54	58	2.0	7.1	4.5	4.5	0	2	0	ESE 2	NE 3	E 5
4	102.9	98.6	93.3	98.3	4.3	15.3	12.5	11.2	16.8	-0.9	68	40	59	56	2.7	10.5	6.0	6.4	3	4	10	SE 6	SE 10	SSE 5
5	89.7	89.0	90.2	89.6	10.1	14.4	10.6	11.4	15.6	8.7	96	69	94	86	0.5	5.1	0.8	2.1	10	10	10	SE 2	SSW 4	WSW 4
6	92.4	95.0	97.7	95.0	9.7	10.2	6.2	8.1	13.2	6.0	92	73	89	85	0.9	3.3	1.0	1.7	10	10	1	WNW 5	NW 6	NW 1
7	100.4	100.6	99.5	100.2	8.4	13.1	9.8	10.3	14.1	5.0	90	49	86	75	1.0	7.7	1.7	3.5	9	8	9	W 4	W 3	S 3
8	96.8	98.4	102.4	99.2	10.8	13.8	11.2	11.8	15.0	8.6	89	72	91	84	1.5	4.4	1.2	2.4	10 •	9	9	SW 3	W 8	W 4
9	99.0	94.5	90.5	94.7	11.0	16.4	10.2	12.0	16.7	7.1	91	70	68	76	1.1	5.6	3.9	3.5	10 •	10	7	SSW 4	WSW 4	WNW 12
10	88.9	88.4	89.2	88.8	8.6	10.6	7.1	8.4	11.8	6.7	82	67	90	80	2.0	4.3	1.0	2.4	10 •	7	10 •	W 8	WNW 9	WNW 7
11	89.2	94.9	102.3	95.5	6.9	7.8	9.4	8.4	9.7	6.3	91	94	87	91	0.8	0.6	1.6	1.0	10	10	9	NNW 2	NW 4	NW 3
12	108.1	109.7	108.5	108.8	5.2	9.6	10.6	9.0	15.5	4.7	95	87	81	88	0.4	1.6	2.4	1.5	10	10	9	NW 3	NW 4	NW 2
13	108.5	107.9	106.2	107.5	8.9	16.2	10.6	11.6	16.9	8.3	94	52	86	77	0.6	8.9	1.8	3.8	2	6	8	WNW 3	NNW 5	C 0
14	103.3	101.7	99.8	101.6	10.0	14.2	12.0	12.0	15.0	8.9	96	75	91	87	0.5	4.1	1.2	1.9	10	10	9	W 2	WNW 2	C 0
15	98.4	97.5	96.3	97.4	10.4	17.3	13.2	13.5	18.1	7.4	99	65	76	80	0.2	6.9	3.7	3.6	9	2	10	C 0	E 3	E 3
16	93.7	93.0	93.9	93.5	12.8	20.3	13.0	14.8	22.6	9.5	87	69	96	84	1.9	7.2	0.6	3.2	9	9 ⊼	7	ESE 1	N 3	C 0
17	94.2	92.3	89.3	91.9	14.6	22.8	17.6	18.2	24.1	10.9	89	52	82	74	1.9	13.3	3.6	6.2	9	6	10 • ⊼	WSW 3	WSW 4	S 4
18	90.6	92.2	91.9	91.6	17.1	19.1	14.7	16.4	19.6	14.1	85	67	91	81	3.0	7.4	1.5	4.0	7	10	10 •	SW 1	W 3	C 0
19	88.6	86.9	97.7	91.1	12.4	13.8	6.6	9.3	14.7	6.4	93	92	94	93	1.0	1.3	0.5	0.9	10	10 •	10	WNW 2	NNE 1	NW 3
20	103.2	105.1	108.3	105.5	7.1	10.3	4.7	6.7	11.5	4.4	84	48	90	74	1.6	6.4	0.8	2.9	7	10	1	WNW 3	W 6	WNW 2
21	112.8	113.3	113.6	113.2	6.3	11.6	7.5	8.2	12.7	1.4	79	42	77	66	2.0	7.8	2.4	4.1	3	5	1	W 4	NW 4	E 1
22	113.5	110.6	107.4	110.5	7.9	14.8	12.1	11.7	16.0	0.3	75	42	56	58	2.6	9.8	6.2	6.2	1	8	3	ESE 3	E 7	ENE 2
23	104.8	104.3	102.7	103.9	10.1	10.5	10.6	10.4	12.2	8.6	61	90	94	82	4.8	1.3	0.8	2.3	10	10 •	10	NE 3	NNE 2	E 4
24	101.3	100.7	101.2	101.1	10.6	13.8	12.4	12.3	15.0	10.1	99	88	94	94	0.2	2.0	0.9	1.0	10 ≡	10	9	E 2	NE 2	NNE 1
25	101.4	102.8	103.9	102.7	11.6	12.1	11.2	11.5	12.7	9.2	99	86	96	94	0.1	2.0	0.5	0.9	10 •	10	10	WNW 3	NW 4	NW 2
26	103.4	102.9	102.3	102.9	11.1	14.2	9.8	11.2	16.2	9.4	95	72	93	87	0.7	4.6	0.8	2.0	10	9	3	NW 1	WNW 6	W 3
27	100.3	100.0	99.2	99.8	10.3	11.8	9.3	10.2	14.7	7.5	90	88	95	91	1.3	1.6	0.6	1.2	10	10	4	WSW 2	NW 3	WSW 1
28	98.0	96.1	94.3	96.1	10.2	16.0	14.1	13.6	16.4	4.3	96	63	82	80	0.4	6.7	2.9	3.3	6 •	9 •	10 •	ENE 2	E 5	NE 2
29	90.4	89.8	93.1	91.1	11.2	12.3	11.3	11.5	14.1	10.9	97	96	94	96	0.3	0.5	0.8	0.5	10	10	10	NNE 4	NNE 5	NNE 4
30	96.0	96.4	95.6	96.0	5.5	11.8	8.2	8.4	13.8	4.2	84	63	82	76	1.4	5.0	2.0	2.8	10	7	1	NW 2	N 4	S 1
31	95.5	94.9	93.2	94.5	8.0	16.2	14.2	13.2	17.0	3.7	87	58	71	72	1.3	7.7	4.8	4.6	2	8	10	SE 5	SE 6	E 4
M	99.4	99.0	99.	99.2	9.2	13.8	10.4	11.0	15.2	6.2	88	66	82	79	1.3	5.5	2.3	3.0	7.4	8.0	6.8	2.9	4.4	2.9

Czerwiec – Juin

DNI	CIŚNIENIE I	II	III	Dies	TEMPERATURA I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE i POGODA I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU I	II	III
1	87.2	89.4	94.2	90.3	13.9	15.6	10.4	12.6	17.2	10.3	91	70	85	82	1.5	5.3	1.9	2.9	4	9	9	SE 5	S 7	WSW 3
2	97.1	101.1	102.3	100.2	8.5	12.6	10.2	10.4	15.0	7.8	92	68	88	83	0.9	4.7	1.4	2.3	10	9	1	W 7	NW 7	C 0
3	103.7	103.5	102.9	103.4	12.2	19.3	14.2	15.0	20.4	5.3	76	41	67	61	3.4	13.1	5.3	7.3	1	3	0	W 2	SE 3	NE 2
4	102.7	102.0	101.2	102.0	12.1	17.9	13.3	14.2	19.6	6.5	88	65	91	81	1.7	7.3	1.4	3.5	10	10	10 •	E 1	ESE 2	E 2
5	96.8	94.7	94.0	95.2	13.8	14.7	13.6	13.9	15.1	12.3	84	91	90	88	2.5	1.5	1.6	1.9	10 •	10	10	ENE 2	E 3	E 5
6	91.9	92.3	94.1	92.8	12.6	13.5	13.9	13.5	15.5	12.1	89	93	87	90	1.6	1.1	2.2	1.6	10	10 •	7	NNE 3	NW 2	NW 1
7	96.7	96.7	96.2	96.5	14.3	19.2	15.0	15.9	19.9	7.4	82	55	74	70	2.9	10.0	4.3	5.7	6	4	5	N 1	W 3	ESE 2
8	96.1	94.3	93.2	94.5	13.8	22.2	18.3	18.2	23.1	8.4	77	53	71	67	3.7	12.6	6.0	7.4	6	5	8	E 6	SE 7	S 3
9	92.5	92.2	91.0	91.9	13.4	18.1	14.4	15.1	20.9	12.8	96	73	92	87	0.6	5.6	1.3	2.5	10 •	7	10	ESE 3	ESE 3	ENE 2
	93.2	93.5	94.5	93.7	13.0	19.4	14.4	15.3	20.4	11.4	92	58	94	81	1.3	9.3	0.9	3.8	8	7	9	E 3	N 1	N 2
	93.1	92.9	96.1	94.0	14.2	18.0	14.0	15.0	18.6	11.6	88	66	89	81	2.0	6.9	1.8	3.6	9	10	10 •	N 2	NNE 4	NW 4
12	98.8	101.0	102.7	100.8	12.1	12.4	11.0	11.6	14.6	10.8	95	86	84	88	0.7	2.0	2.1	1.6	10 •	10	8	NW 4	WNW 6	WNW 5
	102.1	101.3	101.0	101.5	11.2	14.9	10.8	11.9	16.1	5.6	88	76	96	87	1.7	4.0	0.5	2.1	10	10	8	WSW 1	W 5	W 2
14	102.1	102.1	103.3	102.5	11.3	17.9	15.7	15.3	21.0	9.8	91	66	81	79	1.1	7.1	3.4	3.9	10	8	8	WNW 5	NW 5	NW 5
	103.9	103.6	102.5	103.3	14.2	20.9	15.2	16.4	21.8	9.8	86	48	88	74	2.4	12.7	2.1	5.7	2	1	1	NNW 1	NNE 2	SE 1
	101.0	99.2	94.8	98.3	15.2	25.0	15.4	17.8	25.1	9.9	86	48	84	73	2.5	16.6	2.8	7.3	3	6	5	SE 4	S 4	SSE 3
17	88.6	88.4	94.7	90.6	17.8	19.0	12.6	15.5	21.7	11.3	76	66	86	76	4.8	7.6	2.1	4.8	8	10	10 •	SE 5	WSW 8	WNW 9
18	101.0	101.0	99.3	100.4	13.4	19.4	17.2	16.8	20.7	9.6	72	48	69	63	4.4	11.7	6.0	7.4	2	6	10	WNW 5	WNW 4	WSW 3
19	98.7	99.7	103.6	100.7	17.2	20.2	13.8	16.2	21.6	13.6	73	66	79	73	4.9	8.1	3.4	5.5	10 ⊼	3	1	NW 3	WNW 6	W 4
	106.6	105.7	106.0	108.1	15.6	21.0	16.0	17.2	21.8	10.2	76	48	78	67	4.3	13.6	4.0	7.3	2	4	7	NW 3	WNW 6	C 0
	106.0	103.8	100.3	103.4	15.2	23.2	19.6	19.4	24.6	9.8	86	48	69	68	2.5	14.8	7.1	8.1	1	8	0	C 0	SSE 3	E 1
22	97.3	95.8	93.4	95.5	18.6	28.3	22.2	22.8	28.6	10.4	86	61	76	74	2.9	15.0	6.3	8.1	3	6	3	SE 3	SW 3	S 4
23	97.6	99.1	101.0	99.2	19.4	20.8	17.5	18.8	22.9	15.3	79	60	83	74	4.6	9.8	3.4	5.9	3	8	1	SSW 4	WNW 5	NNE 1
24	102.1	103.0	103.7	102.9	16.0	24.2	20.8	20.4	26.2	10.0	94	55	70	72	1.2	14.1	7.4	7.8	4	3	3	SW 1	NW 3	C 0
25	105.2	104.8	104.5	104.8	17.6	25.3	21.2	21.4	27.0	13.3	84	50	77	70	3.2	16.4	5.8	8.3	2	4	0	W 1	WSW 4	ENE 1
26	101.9	100.6	104.1	102.2	20.7	32.1	19.3	22.8	32.3	13.3	84	47	95	75	3.8	23.4	1.1	10.1	0	3	7	SE 3	S 5	WSW 2
27	105.9	104.2	106.3	105.5	18.8	23.0	17.2	19.0	23.6	17.2	87	81	84	84	2.7	5.3	3.2	3.7	9	6	8	ESE 4	NE 2	NW 2
28	109.3	110.3	110.3	110.0	14.8	18.1	13.4	14.9	19.2	13.3	83	45	78	69	2.9	11.9	3.3	5.9	4	8	2	NNW 4	NW 5	WSW 1
29	107.2	107.2	107.0	107.1	15.2	18.3	14.0	15.4	20.3	8.5	73	63	85	74	4.6	7.7	2.3	4.9	1	10	0	W 5	WNW 5	WSW 3
30	106.6	103.9	97.9	102.8	14.4	23.6	18.8	18.9	25.4	8.3	88	54	86	76	2.0	13.3	3.1	6.1	0	1	2	C 0	SW 2	SE 2
31																								
M	99.8	99.6	99.9	99.8	14.7	19.9	15.4	16.4	21.3	10.6	85	61	83	76	2.6	9.8	3.3	5.2	5.6	6.8	5.5	3.1	4.2	2.5

DNI	WYSOKOŚCI NOŚCI	OPAD R	GŁĘBOKOŚCI ŚNIEGU h	POGODA
1	8	.	.	= 0^00 3^20 = = – 4^20 = – 6^40
2	9	.	.	⌒ 0 1 – 4 ⌣ 0 – 6, Ci lat 9^40 – 10^20
3	8	.	.	= 3^20 – 8^30, ⌒ 0 0 – 4 ⌣ 0 – 6
4	7	3.0	.	• 0 23^35 – 24, ≫ 8^45 – 16^40, ⌒ 0 1 – 9
5	8	14.4	.	• 0 0^00 – 05, 1^10 – 4^00 … 5^00, • 1 10^18 – 35, • 0 – 11^05, • 13^20 – 14^10, • 0 – 15^09, • 17^40 – 18^05, • 0 21^42 – 22^20, = 2^00 – 7^20, ⊕ 8^30 – 9^20, 12^35 – 13^10
6	7	0.0	.	• 0 13^35 – 14^05, = 3^20 – 7^20, 19^30 – 24
7	8	0.5	.	= 0^00 – 7^30, ⌒ 0 21 – 24
8	7	1.7	.	• 0 3^03 – 5^15, 6^40 – 10^10, • 0 13^01 – 12, 15^15 – 22; = 19^15 – 24, ⌒ 0 0^02 – 13^03
9	8	6.7	.	• 2^40 – 9^15, 15^20 – 35, • 1 16^10 – 17^20, 18^05 – 20, • 0 – 18^25, • 2 – 18^40, • 0 – 19^05, ☾ 0 18^30 – 50, ≫ 18^20 – 55, 19^20 – 24; = 0^00 – 10^10, 16^40 – 18^50
10	8	10.5	.	• 0 0^00, 7^04 – 7^35, 8^05, 9^01 – 10, • 0 – 9^20, • 0 – 9^30, 11^01 – 07, • 1 – 11^15, • 0 – 11^17, 13^12 – 20, 13^50 – 14^01, 14^42 – 15^15, 19^02 – 21^10, • 1 – 22^15, • 0 22^40, 23^03; 23^38 – 24; ≫ 0^00 – 4^15 (por do 18 m/sek), por wiatru 17 m/sek 11^07 – 08
11	6	1.5	.	• 0 0^00 – 1^35, • 1 – 2^10, • 0 – 4^40, 5^10 … 25, • 0 11^16 – 12^12, 13^44 – 14^02, • 1 15^12 – 20, = 12^15 – 13^10 **10.V.** 18 m/sek 13^10 – 15^11
12	7	.	.	= 6^30 – 7^40, ⌒ 0 22 – 24
13	8	1.6	.	= 3^30 – 9^30, ⌒ 0 0^00 – 10, 20 – 24
14	7	.	.	• 0 2^40, 4^10, 5^30 … 6^40, = 1^30 – 10^25, 19^20 – 24; ⌒ 1 0^00 – 2^40, 20^30 – 24
15	7	.	.	= 0^00 – 2^10 = 0 – 6^15 = – 12^40, 19^05 – 24, ⌒ 1 0^00 – 12^30, 21 – 24
16	6	0.6	.	• 0 7^35 – 8^08, • 0 17^35 – 40, 18^05 – 19^05, ☾ WSW 12^15, 13^10 NNE, W 13^35 – 14^15 NNE, NW 15^50 – 19^10 NE, = 0^00 – 14^15, 19^15 – 21^40 = = – 22^10 = – 24, ⌒ 0 0^00 – 7^35
17	7	0.4	.	• 0 6^10 – 12, • 0 20^45 – 21^20; ☾ SW 20^55 – 21^25 – 21^40 E; = 0^00 – 6^30
18	8	4.0	.	• 1 13^01 – 12, • 0 20^25 – 36, 20^38 – 21^02, 23^15 – 26; = 21^15 – 23^15
19	6	19.9	.	• 0 1^35 – 42, 4^10 – 16, • 0 5^30 – 38, • 0 11^45, 12^07, 12^47, 13^02, • 1 – 13^20, • 0 – 13^35, • 0 – 14^10, • 0 – 14^37, • 1 – 15^10, • 0 – 15^50, 16^35 – 18^25, • 0 … 19^10, = 4^10 – 5^40
20	8	.	.	⌒ 0 20^30 – 23, ⌒ 1 – 24; ⊕ 10^40 – 14^15
21	8	.	.	= 21^35 – 24; ⌒ 1 0^00 – 4 ⌣ 0 – 6 ⌒ 1 23 – 24
22	8	.	.	= 0^00 – 3^10 = 0 – 3^50 = – 4^05 = = – 5^45 = – 7^20, ⌒ 1 0^00 – 4 ⌣ 0 – 6
23	6	7.8	.	• 0 12^05 – 20, • 1 – 12^35, • 0 – 13^15, 13^38 – 14^15 … 35, 14^45 – 15^10, 15^45 … 16^03, 17^05 – 10, 17^45, 18^10 – 25, 20^15 – 35, 21^15 – 22^05; = 18^40 – 24
24	6	4.9	.	• 0 2^15 – 35, 3^50, 5^20, = 0^00 – 6^50 = 0 – 8^35 = – 24, ⌒ 1 23 – 24
25	8	3.8	.	• 0 5^03 – 6^40, • 2 – 7^05, • 1 – 7^30, • 0 – 11^20, 11^30, 12^10, 15^45, 16^10; = 0^00 – 2^43 = 0 – 3^05 = 1 – 3^30 = 2 – 4^35 = 0 – 5^10 = – 9^30, ⌒ 1 0^00 – 5^03
26	7	0.0	.	• 0 10^05 – 15, 11^50 – 12^05, 14^50 – 15^02; ☾ SW 14^42 – 55 – 15^02 SE (☾) 0 SE 17^02 – 07 SE; = 1^30 – 8^10, 21^15 – 24; ⌒ 1 19 – 20 ⌒ 2 – 24
27	7	0.0	.	• 0 12^10 – 22, = 0^00 – 7^20 = 20^30 23^30 = – 24, ⌒ 2 0^00 – 12^10 ⌒ 0 20 – 24
28	7	20.4	.	• 0 21^35 – 23^40 … 24; = 0^00 – 2^25 = 0 – 2^30 = 1 – 3^30 = 0 – 5^30 = – 9^30, 18^40 – 24; ⌒ 1 0 – 9
29	6	24.9	.	• 1 0^00 – 05, • 0 0^10 – 2^15, • 1 – 2^25, • 0 … 2^40 – 3^15, • 2 – 4^40, • 1 – 5^40, • 0 – 6^10, • 1 – 6^45, • 2 7^10, • 1 – 8^30, • 0 – 20^30, • 1 – 21^20, • 0 – 22^15, = 0^00 – 23^40
30	8	.	.	
31	6	9.0	.	• 1 23^18 – 24, = 2^30 – 5^30 7^25 – 10^30 ∞ – 13^20 = 18^10 – 24; ⌒ 0 – 8
Σ	–	135.5	–	

Czerwiec - Juin

1	8	1.6	.	• 1 0^00 – 1^40, • … 3^35, • 0 9^42 – 10^05, = 0^00 – 7^15
2	8	0.1	.	• 0 0^40 – 1^15, 2^10 – 4^20, 5^20 – 6^10, 9^05 – 10^05, = 23^35 – 24; ⌒ 0 20 – 24
3	8	.	.	= 0^00 – 4^20, 23^30 – 24; ⌒ 0 0^00 – 11, 20 – 24
4	6	2.3	.	• 0 11^45 – 12^05, • 0 17^45 – 18^05, • 0 18^25 … 20^30 – 22^35; = 0^00 – 14^30, 20^05 – 24, ⌒ 0 0^00 – 8; ⊕ 14^40 – 15^30
5	6	0.4	.	• 0 1^35 – 3^10, 4^02 – 38 … 10^15; = 0^00 4^25, 9^20 – 24
6	6	5.8	.	• 0 3^45 … 4^05, 5^35 – 45, 7^00 – 14^06; = 0^00 – 6^15
7	8	.	.	= 2^20 – 3^30, ⌒ 0 19 – 20 ⌒ 1 – 24
8	7	2.8	.	(☾) SW 19^05 – ☾ 19^20 – 20^00 – (☾) NW 20^35; = 3^15 – 10^30, ⌒ 2 0^00 – 9
9	8	9.7	.	• 0 2^50 – 3^05, 5^45 – 6^10, 6^25 – 40, • 1 – 7^10, • 0 8^05 – 35, 10^20, 11^05, • 1 17^23 – 40, • 0 – 18^05, 19^38, 20^08; (☾) 17^05 E – ☾ 0 17^10 – 18^10 W; = 6^20 – 11^10, 20^25 – 24
10	8	0.1	.	• 0 14^58 – 15^15, 17^50 – 18^01; (☾) NE 14^45 – ☾ 14^55 – 15^15 – (☾) 15^30 W; = 0^00 – 8^30, ⌒ 1 21 – 24
11	8	5.5	.	• 0 13^04 – 08, 14^04 – 26, 18^08 – 30, 18^47 – 51, • 0 19^03 … 21^40, 22^45, 23^05, ⌒ 2 0^00 – 11
12	7	0.8	.	• 0 5^10 – 15, 6^05 – 06, • 1 – 7^10, • 0 7^45 … 8^10, 8^50, 9^05, 9^40 – 10^05; = 20^25 – 24
13	7	5.2	.	• 0 13^35, 15^03, • 1 18^05 – 20, • 0 – 18^40, = 0^00 – 10^20, 13^10 – 15^40, ⌒ 1 – 10
14	8	2.7	.	• 0 7^45 – 8^05, • 1 18^32 – 45, • 0 18^58 – 19^05
15	8	.	.	= 2^20 – 3^35 = = – 4^50 = – 7^35, ⌒ 0 20 – 24
16	7	.	.	= 21^30 – 24, ⌒ 0 0^00 – 8, 21 – 24; ⊕ 11^40 – 12^30
17	8	2.7	.	• 0 13^45 – 14^50, • 0 14^58 … 16^35, • 0 20^05 – 20, • 0 20^50 – 21^15; = 0^00 – 3^40, ⌒ 0 0^00 – 9
18	8	0.0	.	• 0 23^28 … 40
19	8	2.4	.	• 0 6^50 – 7^05, 7^20 – 8^10, • 0 8^35 … 10^10; ☾ 0 W 6^50 – E 7^10; = 23^30 – 24, ⌒ 0 20^30 – 24
20	8	.	.	= 0^00 – 3^15, ⌒ 0 0^00 – 4, ⌒ 1 – 8, ⌒ 0 21 – 24
21	8	.	.	= 0^40 – 2^45 = 1 – 3^30 = 2 – 4^15 = 1 – 4^35 = = – 5^30 = – 8^30, 21^20 – 24, ⌒ 0 0^00 – 1, ⌒ 1 – 9, 22 – 24
22	8	11.0	.	• 1 22^43 – 23^30, • 0 – 24; (☾) SW 22^30 – ☾ 22^40 … 24; = 0^00 – 3^45 = 0 – 4^35 = = – 5^10 = – 7^15, ⌒ 1 0^00 – 9, 20 – 22^43
23	8	(0.0)	.	• 0 0^00 – 2^15, 9^30 – 35; ☾ 0 0^00 – 1^30 – (☾) E 2^52; = 21^15 – 24, ⌒ 1 20^30 – 24
24	8	.	.	= 0^00 – 2^40 = 0 – 3^25 = 1 – 3^40 = 2 – 4^20 = 1 – 4^38 = 0 – 4^50 = – 8^10, 21^30 – 24; ⌒ 1 0^00 – 8 ⌒ 0 21 – 24
25	8	.	.	= 0^00 – 7^30, 22^10 – 24, ⌒ 1 0^00 – 8, 22 – 24
26	8	1.8	.	• 0 14^04 – 08, • 1 – 14^20, • 0 – 14^24, 17^19 – 18^05, 22^00 – 10; ☾ 0 W 14^01 – E 14^35 (☾) S 16^50 – E 18^20 (☾) W 21^50 – E 22^10, ≫ 14^01 – 17; = 0^00 – 7^30, 19^30 – 24, ⌒ 1 0^00 – 9
27	7	0.1	.	• 0 8^50 – 9^50, 14^02 – 15; ☾ SE 9^02 – E 9^15, S 13^06 – 14^02 – NE 15^05; = 0^00 – 6^30, 20^40 – 24
28	8	.	.	= 0^00 – 4^10, ⌒ 0 21 – 24
29	8	.	.	= 21^40 – 24; ⌒ 1 0^00 – 8 ⌒ 0 22 – 24
30	8	0.0	.	= 0^00 – 2^35 = = – 4^30 = – 7^20; ⌒ 0 0^00 – 10, 21 – 24
31				
Σ	–	55.0	–	

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.6	99.6	99.6	98.6	18.1	14.5	15.1	15.7	20.2	14.2	91	87	93	90	1.9	2.2	1.2	1.8	10	10	6	W 4	NW 3	C 0
2	99.9	98.6	97.6	98.7	12.0	18.2	13.3	14.2	19.1	9.4	84	47	81	71	2.2	11.1	3.0	5.4	9	3	9	NW 1	NNW 6	W 3
3	96.1	96.2	97.4	96.6	13.3	14.6	10.6	12.3	17.0	10.4	79	66	76	74	3.2	5.7	3.1	4.0	10	10	5	WNW 4	WSW 4	W 2
4	96.6	96.2	95.3	96.0	12.2	14.4	11.0	12.2	17.0	6.1	71	69	94	78	4.2	5.1	0.8	3.4	7	7	4	WNW 2	SW 4	SW 1
5	95.4	95.4	98.1	96.3	11.8	15.5	10.4	12.0	17.0	9.3	76	55	92	74	3.3	7.9	1.0	4.1	8	8	6	NW 2	NW 6	W 2
6	100.1	99.5	100.5	100.0	12.2	13.6	11.5	12.2	16.5	6.5	73	74	78	75	3.8	4.0	3.0	3.6	3	9	2	W 4	W 4	W 3
7	100.0	98.0	95.5	97.8	12.8	20.2	14.8	15.6	22.8	8.3	84	63	86	78	2.4	8.9	2.4	4.6	10	9	7	SSW 2	SSW 6	E 1
8	92.0	89.2	89.5	90.2	17.2	17.7	14.5	16.0	19.8	9.6	80	81	87	83	3.9	3.8	2.2	3.3	10	10	9	S 5	NW 5	WSW 4
9	94.3	96.6	99.1	96.7	12.6	16.4	9.6	12.0	17.6	9.4	71	52	86	70	4.2	8.9	1.8	5.0	5	4	3	W 6	W 8	WSW 3
10	100.6	101.3	102.9	101.6	11.4	16.0	11.3	12.5	17.0	6.0	82	70	86	79	2.5	5.4	1.8	3.2	8	8	3	WSW 3	WSW 5	W 3
11	105.6	105.3	104.4	105.1	12.8	16.9	14.1	14.5	20.1	8.3	75	64	87	75	3.8	7.0	2.2	4.3	3	7	5	W 3	SSW 2	S 3
12	101.8	100.2	99.7	100.6	15.9	19.1	15.7	16.6	21.2	11.3	84	78	95	86	2.9	4.8	0.9	2.9	10	10 •	7	S 5	WSW 4	W 3
13	101.8	100.9	100.6	101.1	17.4	23.4	19.3	19.8	25.3	14.1	88	69	88	82	2.4	9.0	2.8	4.7	7	8	4	C 0	SW 2	SE 3
14	100.9	101.1	100.9	101.0	19.9	30.0	21.7	23.3	31.0	14.4	84	48	88	73	3.7	21.8	3.1	9.5	4	4	4	SE 2	SE 4	S 2
15	103.4	102.5	101.8	102.6	20.2	29.0	21.5	23.0	29.3	14.8	78	54	88	73	5.2	18.4	3.0	8.9	2	4	9	SSE 5	C 0	NW 4
16	101.3	100.2	99.8	100.4	18.9	26.2	17.6	20.1	26.4	15.6	85	63	95	81	3.3	12.6	1.0	5.6	2	9	10	ENE 1	ENE 2	N 2
17	99.1	98.3	97.7	98.4	18.5	20.6	17.5	18.5	23.6	16.9	98	92	98	96	0.4	2.0	0.4	0.9	10	10 •	10 • K	NNE 2	N 3	C 0
18	98.1	100.2	103.3	100.5	16.1	15.5	16.5	16.2	17.7	15.2	96	95	87	93	0.8	0.9	2.6	1.4	10 •	10 •	10 •	N 2	N 5	NNW 1
19	104.3	104.5	104.2	104.3	15.3	22.0	17.7	18.2	23.9	13.9	86	65	97	83	2.4	9.2	0.6	4.1	7	8	8	NNE 1	E 4	C 0
20	104.0	102.2	99.4	101.9	15.7	23.1	17.9	18.6	24.8	13.9	78	62	85	75	3.9	10.8	3.0	5.9	3	3	7	E 3	E 5	E 4
21	96.6	94.6	94.9	95.4	16.3	22.5	15.9	17.6	25.1	14.5	97	79	95	90	0.6	5.6	1.0	2.4	10 K	6	6	E 2	SE 5	W 2
22	96.7	96.5	95.1	96.1	17.7	22.6	17.5	18.8	24.6	12.9	79	60	83	74	4.2	11.0	3.4	6.2	0	6	2	W 5	W 2	ESE 1
23	92.7	95.1	94.8	94.2	15.9	16.8	16.8	16.6	22.2	13.6	94	84	88	89	1.2	3.1	2.3	2.2	10	9	2	ESE 2	W 4	SSW 1
24	94.7	95.6	97.9	96.1	17.4	24.2	15.7	18.2	24.6	12.8	82	42	76	67	3.6	17.6	4.3	8.5	9 •	3	1	SW 4	NW 6	W 1
25	99.1	98.3	95.6	97.7	15.9	23.9	17.5	18.7	24.6	10.1	78	57	79	71	4.0	12.8	4.2	7.0	3	8	3	WSW 2	S 2	SW 3
26	98.9	97.7	96.8	97.8	17.5	20.5	14.9	17.0	22.4	10.3	79	45	73	66	4.2	13.3	4.5	7.3	3	6	4	W 5	WSW 5	W 2
27	98.0	98.9	99.8	98.9	12.9	17.3	13.3	14.2	18.8	11.5	79	51	87	72	3.1	9.5	2.0	4.9	10	7	10	WNW 6	NW 5	WNW 6
28	100.8	101.0	98.2	100.0	12.3	14.0	14.1	13.6	16.0	11.0	90	79	79	83	1.4	3.4	3.4	2.7	10 •	10 •	10	W 5	W 6	SW 3
29	95.1	92.6	88.6	92.1	15.0	21.7	15.7	17.0	22.9	12.0	80	49	70	66	3.4	13.3	5.3	7.3	9	6	10	SW 4	WSW 7	SSW 5
30	85.6	95.1	89.2	86.6	16.2	19.7	13.9	15.9	21.8	13.1	74	57	82	71	4.7	9.8	2.9	5.8	9	9	3	SW 4	WSW 8	WSW 4
31	89.1	86.3	93.2	89.5	15.1	20.9	11.1	14.6	21.8	10.9	86	62	88	79	2.5	9.4	1.6	4.5	10	5	9	SW 2	SW 9	NW 5
M	98.0	97.7	97.8	97.8	15.4	19.7	15.1	16.3	21.7	11.6	83	65	86	78	3.0	8.7	2.4	4.7	7.1	7.3	6.0	3.2	4.5	2.5

Sierpień – Août

1	96.6	96.9	96.2	96.6	12.1	17.4	14.7	14.7	18.4	7.0	77	54	71	67	3.2	9.1	4.8	5.7	2	7	10	W 4	NW 2	ENE 2
2	94.3	95.7	96.3	95.4	11.5	16.0	10.7	12.2	18.6	9.3	91	62	90	81	1.2	7.0	1.3	3.2	10	6	1	WNW 3	N 3	WSW 2
3	95.3	95.2	96.5	95.7	10.9	19.4	12.3	13.7	20.7	6.3	91	53	86	77	1.1	10.6	2.0	4.6	2	9	2	ESE 2	W 8	WSW 3
4	99.3	101.0	103.6	101.3	14.4	18.9	12.6	14.6	20.4	10.2	90	53	91	78	1.6	10.3	1.4	4.4	10	5	4	W 6	WNW 8	WNW 1
5	106.0	105.7	105.0	105.6	14.1	22.1	17.2	17.6	24.0	10.1	90	53	84	76	1.6	12.5	3.2	5.8	1	5	0	WSW 3	WNW 4	SE 2
6	102.8	100.1	101.6	101.5	19.1	29.6	18.6	21.5	30.4	11.8	88	45	93	75	2.8	22.7	1.5	9.0	5	1	9	SSE 3	SW 7	SSE 4
7	100.0	98.7	98.4	99.0	21.0	29.3	22.9	24.0	31.0	18.2	90	61	74	75	2.5	15.9	7.3	8.6	8	4	2	SSE 2	WSW 3	NNW 3
8	100.9	98.8	101.6	100.4	19.2	27.2	19.4	21.3	27.8	15.7	93	55	69	72	1.5	16.2	7.0	8.2	3	8	7	WNW 2	SE 1	NW 3
9	105.6	105.6	106.6	105.9	12.3	14.5	14.1	13.8	19.6	11.8	92	79	94	88	1.2	3.4	0.9	1.8	10 • K	10	9	NW 1	NW 1	WSW 2
10	107.5	107.0	107.9	107.5	11.2	17.9	12.7	13.6	18.6	7.4	97	58	95	83	0.3	8.7	0.7	3.2	3	8	10 •	C 0	NNE 3	SW 2
11	108.3	108.4	108.6	108.4	11.9	16.7	12.3	13.3	18.6	10.6	89	49	85	74	1.5	9.7	2.2	4.5	8	5	6	NW 2	WNW 5	NW 2
12	109.1	108.7	108.0	108.6	11.3	18.0	13.2	13.9	19.4	8.8	89	55	85	76	1.5	9.2	2.3	4.3	3	7	7	C 0	NW 3	NW 2
13	108.3	108.2	107.1	107.9	10.7	17.8	10.7	12.5	18.9	8.3	95	52	87	78	0.7	9.8	1.7	4.1	2	6	2	W 1	NW 2	WNW 2
14	107.1	105.9	104.8	105.9	10.2	17.3	14.3	14.0	19.4	5.7	92	61	77	77	0.9	7.6	3.8	4.1	1	7	9	NW 2	WNW 2	N 1
15	106.5	106.9	106.5	106.6	10.9	16.1	10.7	12.1	16.7	9.1	94	66	96	85	0.8	6.1	0.5	2.5	8	9	3	C 0	NW 3	C 0
16	106.2	105.6	104.0	105.3	10.1	18.1	14.9	14.5	21.4	5.5	93	61	77	77	0.8	8.1	3.8	4.2	1	7	7	C 0	C 0	ENE 1
17	103.7	103.0	102.9	103.2	13.1	22.8	13.5	15.7	23.1	9.6	85	49	82	72	2.3	14.1	2.8	6.4	4	3	0	E 2	E 1	E 1
18	103.9	104.1	104.9	104.3	12.3	25.1	16.1	17.4	25.4	8.3	92	48	85	75	1.2	16.4	2.7	5.8	0	1	0	ESE 2	SSW 2	SSE 1
19	107.5	108.2	108.0	107.9	12.3	25.0	16.0	17.3	26.0	8.4	99	40	84	74	0.2	19.1	2.9	7.4	0	1	0	C 0	WNW 2	W 1
20	107.6	105.8	102.9	105.4	12.9	27.4	17.0	18.6	27.4	9.0	96	47	81	75	0.6	19.5	3.8	8.0	0	0	0	SE 1	SE 5	SSE 2
21	100.3	99.1	96.0	98.5	14.7	25.6	17.5	18.8	26.9	11.8	92	58	86	79	1.3	13.6	2.8	5.9	7	1	2	SSE 2	WSW 1	S 3
22	93.3	90.5	89.0	90.9	16.7	27.6	20.2	21.2	27.9	12.5	81	38	58	59	3.7	22.8	10.0	12.2	2	3	0	SE 2	S 9	SSE 7
23	89.7	89.6	91.4	90.2	17.7	27.9	20.2	21.5	28.3	13.5	73	47	81	67	5.5	20.1	4.6	10.1	5	4	9 •	SSE 4	S 6	WSW 2
24	93.3	94.9	93.3	93.8	16.3	17.0	16.7	16.7	20.3	16.3	100	94	97	97	0.0	1.2	0.6	0.6	10 =	10	10	NW 1	WNW 2	NNW 1
25	91.8	93.6	96.9	94.1	15.3	15.0	13.3	14.2	16.9	13.0	97	96	96	96	0.6	0.7	0.6	0.6	10 •	10 •	10 •	NNW 4	NW 4	W 3
26	101.1	101.2	100.5	100.9	10.2	14.7	11.3	11.9	15.3	9.5	91	54	91	79	1.1	7.7	1.2	3.3	4	9	3	NW 5	NW 5	W 2
27	99.2	98.5	98.6	98.8	10.8	14.8	10.3	11.6	17.6	8.0	89	65	90	81	1.5	5.9	1.3	2.9	9	7	0	NW 2	NW 4	W 1
28	100.0	101.0	102.7	101.2	11.7	17.1	10.1	12.2	18.4	7.6	95	56	90	80	0.6	8.5	1.3	3.5	9	3	0	NW 2	NW 3	WNW 2
29	101.6	99.4	99.4	100.1	10.9	19.7	14.1	14.7	20.3	7.0	91	50	94	78	1.1	11.5	0.4	4.5	6	9	10	W 1	WSW 5	NW 2
30	101.0	101.2	102.4	101.5	11.1	17.5	10.6	12.4	18.4	8.7	91	47	91	76	1.1	10.7	1.2	4.3	9	6	3	NW 2	NW 5	W 2
31	102.0	100.1	97.2	99.8	7.8	19.3	13.3	13.6	20.4	5.3	100	52	78	77	0.0	11.2	3.3	4.8	0	3	6	C 0	S 1	SE 3
M	101.6	101.2	101.3	101.4	13.1	20.4	14.6	15.7	21.8	9.8	91	57	85	78	1.4	11.3	2.7	5.1	4.9	5.6	4.5	2.0	3.3	2.1

Wrocław - Strachowice $H_s = 120\,m$ $H_b = 123.8\,m$ $h_w = 10\,m$ *Lipiec - Juillet 1965*

DNI	WIDZIALNOŚĆ	OPAD	GRUBOŚĆ LODU	P O G C D A
1	7	0.0	.	∇ 1255-510, 617-25, ● 1025-40, 1525-30, (K) W 455 E 525, = 230-330, 2120-24, ⌒ 000-455, 22-24
2	8	.	.	= 000-335, ⌒ 000-9
3	8	.	.	⌒ 23-24
4	8	2.4	.	● 1610-25, ● 1-1632, ● 1635-45, = 2030-24, ⌒ 000-3, ⌒ 1-9
5	8	0.9	.	● 548-602, ● 1602-08, 1745-1822, 2042-45, = 000-615
6	9	0.0	.	∇ 1050, 1103, 1115-25, 1225-45, ● 1-1250, ∇ 1303-08
7	8	.	.	= 2330-24, ⌒ 1-8, ⊕ 1130-1630
8	8	12.7	.	● 809-20, 037, ● 1301-35, 1405-18, ● 1-1505, ● 1525-45, = 000-630, ⌒ 000-800
9	8	0.0	.	● 305-13
10	7	5.5	.	● 725, 902-1022, ● 1225-30, 1328-41, ∇ 1-1330, ● 1540-1607, = 230-645, 2005-24, ⌒ 1-9, 21-24
11	8	0.0	.	∇ 005-25, = 000-630, ⌒ 20-24
12	7	5.5	.	● 640-50, 708-25, 1005-49, 1242-1325, 1445, 1510, 1545, 1608-1800, ● 1-1826, ⌒ 000-640
13	8	.	.	⌒ 000-8, ⌒ 21-23, ⌒ 1-24
14	8	0.1	.	⌒ 000-8, 2040-24
15	8	0.0	.	● 035-48, 1745-50, (K) SW 1540-S 1625, < 2140-2330 NE, ⌒ 000-35
16	7	13.0	.	∇ 1521-1617, 1628-50, ∇ 1745-53, ● 0-1844, (K) S 1432 W 1703, (K) S 1610 (K) S 1710, 1730 W 1800, (K) 1900, = 130-700, 1440-1635, 1915-24, ⌒ 0-2, ⌒ 1-10
17	6	27.0	.	● 245-347, ● 0-420, ● 0-440, 615, ● 1000-10, ● 1-1230, ● 1300, ● 1-1505, ● 0-1540, 1745-58, ● 1-1900, ● 0-1806, ● 1-1808, ● 1-1810, ● 0-1935, ● 1-1950, ● 0-2140, 2245-55, (K) N 1310 1330 NE 1420 (K) NE 1725 1820 SE 2055,
18	7	2.6	.	● 040-120, 200, ● 1-405, ● 0-445, 640-730, 1310, 2045, 2135-0000-730, 1930, 2145, 2230-24
19	8	10.5	.	∇ 1454-1514, 1732-44, ∇ 1-1745, ∇ 0-1805, (K) E 1745, 1750 W 1805, = 000-230, 2010-24
20	8	2.3	.	∇ 1825-32
21	7	0.0	.	● 600-25, 650-705, 746-812, 1602-07, ● 1845, 1915, (K) SW 515 (K) 2104 E 625 (K) W 650-705, (K) E 710, (K) WSW 1505 N 1530 E 1630, = 120-1035, ⌒ 1-1608
22	8	0.0	.	● 2042-2330, ⌒ 2-8, 20-2242
23	7	5.5	.	∇ 810-915, (K) W 805 E 900, = 415-920, ⌒ 2040-24
24	8	0.0	.	● 240-350, ∇ 610-15, 645-700, ⌒ 000-245, 20-24
25	8	0.3	.	∇ 1012-20, ∇ 2024-29, ⌒ 000-9, ⊕ 930-1400
26	8	.	.	⌒ 21-24
27	8	0.3	.	∇ 1750-1805, 2120-48, ⌒ 000-8
28	7	1.5	.	● 602-705-50, 1105, 1510, = 315-830, 1920-24
29	8	0.0	.	● 040, 135, 1545, 1605, 1540, 1704, > 1330, 1610, = 000-340
30	8	4.7	.	∇ 1516-32, ∇ 1731-54, 1838-35, ∇ 1438, 1725-29, ● 1-1734, ∇ 1738, > 025, 1230 poc: wiatru 15 m/sek, 1730-31, ⌒ 1643-46, 1649-53
31	8	5.0	.	∇ 910-20, 1350, 1415, 1450-55, ∇ 1510, ● 1-1512, ∇ 1548, ∇ 1-1622, 1620-30, (K) W 1435 (K) 1450, 1522 (K) 1535 E, (K) SW 1615-SE 1735
Σ	–	94.8	–	

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1	8	.	.	
2	8	0.3	.	● 105-37, ∇ 1525-35, 1750-1805
3	8	2.0	.	= 315-30, 420, = 645, ⌒ 1-4-9, 20-24, ⊕ 1100-1400
4	8	2.0	.	∇ 402-12, 1455-1502, 1618-34, = 1910-24, ⌒ 1-000-402
5	7	.	.	= 000-920, 2010-24, ⌒ 1-3-9, 20-24
6	8	7.0	.	∇ 1805-10, ∇ 1-1812, ∇ 2-1830, ● 1-1833, ∇ 1835, 1904-19, (K) W 1747, (K) 1805-15 (K) 1833-40 E, > 1805-17 (poc: 18 m/sek), = 000-330, ⌒ 000-9
7	8	.	.	● 035-103, ⌒ 19-24
8	8	0.6	.	= 400-30, = 520, = 710, ⌒ 2000-9
9	7	5.2	.	∇ 546-608, 630-725, ● 740-810, 815-45, ● 1-930, ● 1005, 1540-1615, (K) NW 625-SE 720, = 2020-24
10	8	1.1	.	● 2002-2115, 2030-2245, 24, = 000-345, = 0-405, = 1-410, = 0-425, = 745
11	8	.	.	● 000-10, 030-330, ⌒ 22-24
12	8	.	.	⌒ 000-5, ⌒ 1-8
13	8	0.0	.	∇ 1650-1703, = 130-435, = 0-145, 730, ⌒ 1-9, 20-24
14	9	0.2	.	∇ 2220-35, ⌒ 000-10, 20-2220
15	9	.	.	= 2330-24, ⌒ 1-21-24
16	9	.	.	= 000-20, 315-425, ⌒ 1-000-9
17	7	.	.	= 1925-24, ⌒ 0-9, 20-24
18	8	.	.	= 000-840, 1905-24, ⌒ 0-000-9, 18-24
19	7	.	.	= 030-140, = 1-150, = 2-220, = 1-235, = 0-245, = -315, = = -340, = -405, = -500, = 1-526, = -550, = -930, 1910-24, ⌒ 1-000-9, ⌒ 0-20-24
20	7	.	.	= 000-420, = -510, = -915, 1910-24, ⌒ 0-000-1, ⌒ 1-9, 21-24
21	7	.	.	= 000-945, ∞ 1010-1140, 1915-24, ⌒ 0-000-10, 20-24
22	8	.	.	= 000-230, ⌒ 0-000-5, ⌒ 1-9
23	8	0.0	.	● 2035-2220, = 2210-24
24	6	13.5	.	● 510-1110, ● 2215-2320-24, = 000-425, = 0-440, = 0-630, = 0-825, = -24, ⌒ 1-20-2215
25	5	11.2	.	● 1000-145, ● 2-236, ● 1-340, ● 0-405, ● 1-440, ● 0-510, ● 1-545, ● 0-1035, ● 1-1120, ● 0-1230, ● 1-1310, ● 0-1332, 1440-1540, 1615-2135, = 000-24
26	8	.	.	= 000-10, ⌒ 19-24
27	8	0.9	.	⌒ 1-000-9, ⌒ 20-24
28	8	.	.	∇ 350-405, = 415-820, ⌒ 0-000-350, 19-24
29	8	0.2	.	● 1740-1803, 1910-2015, = 1910-2340, = 0-24, ⌒ 0-000-8, ⊕ 1020-1510
30	8	.	.	∇ 548-602, = 0-000-240, = -510, ⌒ 0-20-24
31	8	.	.	= 130-840, 1910-24, ⌒ 0-000-9, 22-24, ⊕ 1445-1710
Σ	–	44.2	–	

Wrocław – Strachowice $\varphi = 51°06'$ $\lambda = 16°53'$ *Wrzesień – Septembre 1965*

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.0	96.6	97.4	96.7	11.5	20.4	16.3	16.1	20.4	10.6	94	60	95	85	0.9	9.7	1.0	3.9	9	4	10 •	C 0	ESE 1	ESE 3
2	98.7	99.4	98.9	99.0	16.7	26.0	20.5	20.9	26.7	15.7	85	45	59	62	3.3	18.5	9.9	10.6	7	5	6	SE 5	SE 10	SSE 7
3	95.4	94.8	94.8	95.0	18.7	25.8	19.7	21.0	25.9	17.1	65	58	86	70	7.5	14.0	3.2	8.2	7	8	10	SE 8	S 7	SE 3
4	94.8	95.8	95.8	95.5	14.9	18.8	14.2	15.5	19.9	14.2	97	67	91	85	0.5	7.1	1.5	3.0	10	10	9	NW 2	NW 1	S 2
5	96.3	95.8	94.0	95.4	12.4	23.0	14.5	16.1	23.9	11.0	90	50	88	76	1.4	14.1	2.0	5.8	2	6	1	W 1	S 1	S 2
6	92.2	91.9	92.9	92.3	10.9	17.8	10.3	12.3	18.9	8.8	99	78	95	91	0.1	4.4	0.6	1.7	4	9	6	ESE 1	NW 5	SSW 2
7	93.2	93.8	95.4	94.1	9.6	16.3	10.7	11.8	17.9	7.3	96	48	90	78	0.5	9.6	1.3	3.8	1	6	2	WSW 2	W 7	W 4
8	99.1	99.7	98.9	99.2	11.7	18.9	11.1	13.2	20.1	8.7	89	63	89	80	1.5	8.0	1.5	3.7	9	6	2	W 3	WNW 4	SSE 3
9	96.3	97.9	97.6	97.3	12.0	22.4	15.3	16.2	23.0	8.1	93	57	90	80	1.0	11.6	1.7	4.8	3	7	6	SSE 3	WNW 3	SE 2
10	95.0	96.3	97.8	95.7	14.8	16.5	13.7	14.7	18.7	12.8	91	80	94	88	1.5	3.9	0.9	2.1	9	10	8	SSE 4	NW 4	NNW 1
11	96.0	99.9	100.2	98.7	11.4	13.1	9.4	10.8	14.5	8.8	91	85	100	92	1.2	2.3	0.0	1.2	10	10	4	NNW 4	NW 3	C 0
12	100.4	98.9	98.1	99.1	6.9	19.1	9.3	11.2	19.7	3.5	100	51	97	83	0.0	10.9	0.3	3.7	0	4	4	C 0	W 4	C 0
13	97.7	97.6	98.0	97.8	9.8	15.5	10.7	11.7	16.6	7.8	96	64	92	84	0.5	6.4	1.0	2.6	7	9	6	NW 1	NW 5	C 0
14	99.4	101.8	104.8	102.0	9.8	16.9	12.3	12.8	18.0	9.1	99	62	92	84	0.1	7.3	1.2	2.9	9	3	10	C 0	NW 4	WSW 2
15	107.2	108.8	110.9	109.0	11.7	15.3	11.6	12.6	17.9	10.0	89	70	89	83	1.3	5.3	1.5	2.8	3	10	4	WNW 3	NW 3	WSW 1
16	112.0	109.0	108.6	109.9	6.6	21.9	11.9	13.1	22.6	4.1	100	51	87	79	0.0	13.0	1.8	4.9	2	1	0	SE 1	SSW 3	SSE 3
17	106.7	105.4	104.5	105.5	10.1	25.1	15.3	16.4	25.8	8.3	95	54	89	79	0.7	14.5	1.9	5.7	0	1	0	SE 3	SW 3	SSW 2
18	101.8	99.1	98.9	99.9	14.3	24.0	15.9	17.5	25.0	11.1	83	48	86	72	2.7	15.6	2.5	6.9	0	0	9	SSW 3	SSW 6	S 2
19	104.8	107.8	111.4	108.0	13.1	14.9	8.4	11.2	17.7	8.4	80	61	95	78	3.0	6.5	0.7	3.4	10	8	5	NW 3	WNW 6	WNW 2
20	115.3	117.0	119.6	117.3	7.4	13.7	11.3	10.9	14.5	5.3	99	70	83	84	0.2	4.7	2.3	2.4	8	8	8	NNW 3	N 4	NW 2
21	120.5	119.5	116.3	118.8	5.6	16.5	8.0	9.5	18.0	4.9	100	56	97	84	0.0	8.4	0.3	2.9	2	9	0	C 0	WNW 2	C 0
22	113.1	110.2	106.1	109.8	4.4	21.6	10.7	11.8	22.7	1.8	100	49	92	80	0.0	13.2	1.0	4.7	3	2	0	E 1	WSW 3	C 0
23	105.3	101.8	100.1	101.7	7.9	23.6	17.0	16.4	23.8	3.3	100	50	73	75	0.0	14.6	4.9	6.5	1	2	0	SE 1	WSW 4	SW 7
24	99.7	99.3	98.8	99.3	8.2	23.8	11.9	14.0	24.4	7.3	100	49	90	80	0.0	13.1	1.3	5.5	1	0	0	S 2	SSE 5	SSE 2
25	97.9	95.7	94.4	96.0	9.8	24.8	16.9	17.1	24.9	8.5	99	50	71	73	0.1	15.7	3.5	7.1	4	2	0	E 1	S 7	SSE 6
26	90.8	89.0	90.2	90.0	13.7	21.8	13.9	15.8	22.7	10.5	81	52	85	73	3.0	12.5	2.3	5.9	0	6	0	SE 6	S 10	SE 4
27	86.4	90.3	90.8	89.2	15.4	19.4	13.8	15.6	20.7	12.3	92	59	82	78	1.3	9.1	2.9	4.4	10 •	2	0	SE 6	WSW 6	ESE 3
28	90.2	90.1	87.3	89.2	13.3	17.0	13.0	14.1	18.4	9.8	86	91	95	91	2.1	1.8	0.7	1.5	9	10 •	10	SE 2	ENE 1	NW 7
29	92.3	94.8	97.9	95.0	10.3	14.9	8.8	10.7	16.7	8.7	96	69	92	86	0.3	5.2	0.9	2.2	10	7	0	NW 2	WNW 4	SE 1
30	98.5	98.4	100.2	99.0	6.8	20.1	12.1	12.8	21.0	5.9	99	58	91	83	0.2	9.7	1.2	3.7	3	4	0	SE 3	SE 6	S 3
31																								
M	99.6	99.9	100.0	99.8	11.0	19.6	13.0	14.2	20.7	8.8	93	60	88	80	1.2	9.8	1.9	4.3	5.2	5.6	4.0	2.5	4.4	2.3

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1	101.6	102.6	103.0	102.4	8.6	22.4	15.4	15.4	22.9	6.3	100	48	81	76	0.0	14.0	3.4	5.8	0	0	0	E 2	SSE 3	E 2
2	101.9	100.7	102.4	101.7	10.3	20.7	16.1	15.8	22.4	7.4	99	69	90	86	0.1	7.6	1.7	3.1	7	2	10	ESE 2	SE 4	NW 3
3	106.3	107.2	108.1	107.2	11.9	18.1	11.8	13.4	19.1	10.8	99	66	95	87	0.1	7.2	0.6	2.6	10 ≡	5	6	NW 3	NNW 2	C 0
4	108.5	108.1	108.2	108.3	8.7	17.5	12.3	12.7	18.9	6.8	100	75	89	88	0.0	4.9	1.5	2.1	5 ≡	6	0	C 0	SE 2	E 1
5	109.2	109.7	109.7	109.5	8.6	13.5	8.4	9.7	14.7	7.0	100	77	100	92	0.0	3.3	0.0	1.2	10 ≡	9	10	SE 3	SE 3	ENE 2
6	109.3	108.6	106.9	108.3	8.3	14.7	6.8	9.2	16.1	6.8	97	69	94	87	0.4	5.2	0.6	2.1	10	2	0	SSE 4	SE 2	SE 3
7	105.3	104.4	105.7	104.5	4.8	13.6	8.2	8.7	15.7	3.1	100	81	100	94	0.0	3.0	0.0	1.0	10 ≡	1	0 ≡	SE 2	E 1	C 0
8	102.9	103.5	105.6	104.0	3.2	10.9	9.2	8.1	11.8	2.3	100	94	95	96	0.0	0.8	0.6	0.5	2 ≡	10 •	10	C 0	NW 4	NW 1
9	105.6	105.3	104.5	105.1	6.6	10.9	7.7	8.2	11.9	6.3	91	63	89	82	0.8	4.6	1.2	2.2	9	8	9	NE 1	NE 2	NW 1
10	104.5	104.2	104.8	104.5	3.7	10.5	5.2	6.2	11.2	2.9	100	56	90	82	0.0	5.6	0.8	2.1	9 ≡	8	5	NW 3	NW 5	WNW 2
11	104.7	103.7	103.4	104.6	2.8	11.6	4.9	6.0	11.8	1.8	100	60	94	85	0.0	5.4	0.6	2.0	8	6	7	W 1	NW 6	NW 2
12	111.9	113.9	114.4	113.4	-1.4	9.6	-0.2	2.0	11.0	-1.8	98	58	94	83	0.1	5.1	0.4	1.9	1	4	0	C 0	W 1	C 0
13	113.2	111.4	109.7	111.4	-1.7	14.5	5.5	6.0	15.5	-3.6	98	44	78	73	0.1	9.2	1.9	3.7	1	6	7	ESE 1	W 3	W 2
14	108.8	107.9	106.7	107.8	-1.0	17.3	5.2	6.7	18.1	-1.6	100	41	86	76	0.0	11.9	1.2	4.4	2	2	1	ESE 1	S 3	SSE 2
15	106.2	104.9	104.3	105.1	0.0	19.9	7.3	8.6	20.2	-0.7	98	44	84	75	0.1	13.0	1.6	4.9	1	5	2	ESE 2	W 4	SE 2
16	102.1	101.4	107.7	103.7	7.0	18.1	6.3	9.5	19.0	6.3	81	53	99	78	1.9	9.7	0.2	3.9	7	5	0	SE 2	WNW 5	NW 3
17	112.5	114.5	114.9	114.0	6.6	8.7	6.6	7.1	9.2	6.3	90	72	78	80	1.0	3.1	2.1	2.1	9	10	10	NW 4	NW 4	NW 2
18	113.2	112.3	112.4	112.6	5.0	11.9	4.4	6.4	12.2	4.1	87	60	95	81	1.1	5.3	0.5	2.4	3	7	0	WSW 3	NW 2	WNW 2
19	112.9	114.4	115.2	114.2	4.4	7.4	6.2	6.0	8.9	3.1	100	91	98	96	0.0	0.9	0.2	0.4	3 ≡	10	10	NNW 1	NNW 2	NNW 1
20	116.1	117.0	118.3	117.1	4.3	9.9	3.0	5.1	10.3	2.1	98	76	98	91	0.1	3.0	0.2	1.1	9	8	0	C 0	C 0	E 2
21	119.3	119.6	121.0	120.0	-3.3	7.3	0.0	1.0	8.3	-4.9	97	63	88	83	0.1	3.7	0.7	1.5	2	4	0	E 1	SE 2	SE 4
22	121.9	121.2	120.4	121.2	-4.0	6.2	-2.6	-0.8	7.7	-4.7	96	66	100	87	0.2	3.3	0.0	1.2	2	0	0	ESE 2	SE 3	C 0
23	118.2	117.1	115.4	116.9	-5.2	7.9	1.3	1.3	10.1	-6.8	100	63	87	83	0.0	3.9	0.9	1.6	5	8	2	W 1	C 0	W 2
24	115.2	115.8	115.5	115.5	3.2	9.2	-1.3	2.4	9.8	-2.3	95	69	100	88	0.4	3.6	0.1	1.4	10	9	0 ≡	C 0	E 3	C 0
25	114.8	113.8	113.0	113.9	-2.4	7.4	1.2	1.8	9.4	-4.1	100	81	100	94	0.0	1.9	0.0	0.6	10 ≡	1	0 ≡	C 0	SE 3	SE 3
26	111.0	109.5	106.7	109.1	1.9	4.2	-1.4	0.8	5.4	-2.8	100	95	100	98	0.0	0.4	0.0	0.1	10 ≡	10	10 ≡	SSE 6	SSE 3	C 0
27	106.0	105.4	105.0	105.3	-3.7	14.9	4.6	5.1	15.5	-3.9	100	53	90	81	0.0	7.9	0.8	2.9	2 ≡	0	0	C 0	NW 3	WSW 1
28	103.2	102.0	101.7	102.3	0.9	17.1	7.8	8.4	18.4	-1.3	100	52	90	81	0.0	9.4	1.1	3.3	4	8	0	ESE 1	WSW 3	SW 1
29	99.3	97.4	102.9	99.9	9.4	19.0	8.9	11.6	19.4	5.3	83	56	83	73	1.7	9.8	1.7	4.4	2	4	0	WSW 4	WSW 9	NW 5
30	106.8	105.8	101.9	104.8	3.7	12.5	3.0	5.6	12.9	2.8	93	50	88	77	0.6	7.2	0.9	2.9	1	3	0	WNW 3	WNW 6	S 3
31	97.9	98.0	97.7	97.9	9.0	10.2	7.3	8.7	13.0	1.3	73	68	76	73	2.9	3.9	2.3	3.1	10	3	8	W 6	NW 7	WNW 8
M	108.7	108.4	108.6	108.6	3.6	12.8	5.8	7.0	13.9	1.8	96	63	91	84	0.4	5.7	0.9	2.3	5.6	5.3	5.3	1.9	3.4	2.0

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	7	3.0	•	•$^{0}15^{37...47}$, 17^{30}–18^{15}... 19^{12} •^{1}–$19^{35...40}$–22^{20}, = 0^{00}–11^{20}, 17^{30}–24; ⌓$^{0}0^{00}$–6 ⌓^{1}–8
2	8	•	•	≫12^{40}–13^{45}; = 0^{00}–10^{40}
3	8	4.0	•	•$^{0}18^{30}$... 19^{15}, 20^{03-35}, 22^{05-20}, 23^{10-45} •^{1}–24
4	8	•	•	•$^{1}0^{00-05}$ •^{0}–1^{50}; = 3^{30}–7^{15}, 19^{10}–24; ⌓^{0}20–24
5	8	•	•	= 0^{00}–2^{30}, 23^{30}–24; ⌓$^{0}0^{00}$–9, 20–24
6	6	4.1	•	•$^{0}13^{40}$... 14^{00-30} •^{1}–15^{20} •^{0}–15^{40}... 16^{10}; = 0^{00}–4^{30} = = –5^{25} = ^{0}–6^{20} = –15^{15}; ⌓$^{0}0^{00}$–6 ⌓^{1}–10
7	8	•	•	⌓$^{0}0^{00}$–5 ⌓^{1}–9, 19–24
8	0	•	•	= 2^{00}–4^{20}; ⌓$^{1}0^{00}$–9, 20–24
9	8	0.0	•	⚘$^{0}7^{43-48}$; = 18^{30}–24; ⌓$^{1}0^{00}$–7^{43} ⌓^{0}20–24
10	8	7.3	•	•$^{0}9^{35-45}$ 16^{12-22}, 23^{23}–24; = 0^{00}–9^{15}, 20^{20}–24; ⌓$^{0}0^{00}$–1 ⌓^{1}–9^{35} ⌓$^{0}20^{30}$–23^{23}
11	7	•	•	•$^{0}0^{00-05}$ ⚘^{0}–1^{10}, 1^{52}–2^{15}, 9^{00-15} •$^{0}4^{50}$–5^{10} •^{1}–5^{30} •^{0}–5^{40}, ⊽^{0}SW 0^{18}–SE 0^{35}; = 0^{00}–6^{15}, 19^{20}–20^{00} = = –21^{18} = ^{1}–23^{20} = ^{0}–23^{50} = –24; ⌓^{1}19–24
12	8	•	•	= 0^{00}–2^{30} = = –4^{00} = ^{0}–4^{40} = ^{1}–4^{48} = ^{2}–5^{30} = ^{1}–6^{20} = ^{0}–6^{25} = –8^{20}; ⌓$^{2}0^{00}$–10 ⌓^{1}20–24
13	8	•	•	= 1^{30}–5^{20} 19^{10}–24; ⌓$^{1}0^{00}$–9, 18–24
14	7	•	•	= 0^{00}–12^{20}, 22^{20}–24; ⌓$^{1}0^{00}$–11 ⌓^{0}20–24
15	7	•	•	= 0^{00}–9^{40}, 17^{40}–24; ⌓$^{0}0^{00}$–9, 20–24
16	7	•	•	= 0^{00-40} = ^{0}–0^{45} = ^{1}–5^{05} = ^{2}–5^{20} = ^{1}–5^{30} = ^{0}–6^{02} = ^{2}–6^{12} = ^{1}–6^{15} = ^{0}–6^{50} = –11^{30}, 19^{30}–24; ⌓$^{0}0^{00}$–4 ⌓^{1}–9 ⌓^{0}20–24
17	7	•	•	= 0^{00}–10^{30}; ⌓$^{0}0^{00}$–10, 20–24
18	7	0.7	•	⚘$^{0}21^{20-25}$, 21^{48}–22^{10}; ≫9^{15}–12^{10}; ⌓$^{0}0^{00}$–11
19	8	•	•	⚘$^{0}4^{40}$–5^{02}; ⌓^{0}18–24
20	8	•	•	⌓$^{0}0^{00}$–10, 20–24
21	8	•	•	= 5^{00}–8^{20}, 23^{30}–24; ⌓$^{1}0^{00}$–9, 20–24
22	8	•	•	= 0^{00}–3^{25} = ^{0}–3^{40} = ^{1}–3^{45} = ^{0}–6^{25} = –8^{30}, 22^{20}–24; ⌓$^{0}0^{00}$–3 ⌓^{1}–10 ⌓^{0}20–24
23	8	•	•	= 0^{00}–3^{45} = ^{0}–6^{30} = –8^{40}; ⌓$^{0}0^{00}$–11
24	8	•	•	= 5^{30}–9^{30}; ⌓^{0}3–4 ⌓^{1}–9 ⌓^{0}20–24
25	7	•	•	= 0^{00}–11^{30}; ⌓$^{1}0^{00}$–9
26	8	1.3	•	≫8^{15}–15^{20} (por. 17 m/sek 9^{30}–11^{30}); = 5^{20}–8^{30}
27	9	0.0	•	•$^{0}4^{10}$–7^{02}; ≫11^{20-40}; = 5^{20}–7^{10}
28	6	10.2	•	•$^{1}12^{07}$–14^{20} •$^{0}16^{25}$ 17^{05}, 19^{45}...52–20^{02}, 20^{11-22}, 21^{44}–22^{01} •^{1}–22^{45} •^{0}–23^{02} •^{1}–23^{06} •^{0}–23^{45} •^{1}–24; (K)$^{0}20^{18}$–E–20^{19}; = 20^{25}–24; ⌓^{0}1–9
29	7	0.0	•	•$^{1}0^{00-30}$ •^{0}–2^{10}...35, 7^{40}...10^{20}; = 0^{00}–11^{30}; ⌓^{0}19–24
30	8	•	•	= 3^{30}–9^{40}; ⌓$^{0}0^{00}$–12, 21–24
31				
Σ	–	30.6	–	

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1	7	•	•	= 0^{20}–1^{40} = ^{0}–3^{35} = ^{1}–4^{20} = ^{2}–5^{40} = ^{1}–6^{10} = ^{0}–6^{40} = –10^{25}, 19^{30}–24; ⌓$^{0}0^{00}$–10, 22–24
2	6	•	•	= 0^{00}–4^{35} = = –5^{15} = ^{1}–5^{25} = ^{2}–5^{32} = ^{1}–5^{36} = ^{0}–6^{40} = –9^{15} = ^{0}–10^{05} = –12^{30} ∞ –17^{30} = –24; ⌓$^{0}0^{00}$–10
3	7	•	•	= 0^{00}–6^{05} = ^{0}–7^{35} = –12^{30}, 18^{10}–23^{30} = ^{0}–24; ⌓^{0}19–24
4	6	•	•	= $^{0}0^{00}$–2^{40} = ^{0}–3^{15} = ^{0}–4^{30} = ^{0}–5^{10} = ^{0}–5^{30} = ^{1}–7^{00} = ^{2}–8^{10} = ^{1}–8^{15} = ^{0}–8^{25} = –24; ⌓$^{1}0^{00}$–11, 19–24
5	6	•	•	= 0^{00}–1^{40} = ^{0}–2^{05} = ^{1}–2^{35} = ^{2}–5^{25} = ^{1}–6^{10} = ^{0}–6^{25} = –6^{35} = ^{0}–8^{25} = –13^{15}, 16^{25}, 19^{10} = = –19^{30} = ^{1}–20^{10} = ^{0}–20^{40} = –24; ⌓$^{0}0^{00}$–11, 18–24
6	6	•	•	= 0^{00}–13^{20}, 16^{40}–24; ⌓$^{1}0^{00}$–11, 18–24
7	5	•	•	= 0^{00}–2^{40} = = –4^{45} = ^{0}–5^{10} = ^{1}–5^{20} = ^{2}–10^{05} = ^{1}–11^{10} = ^{0}–11^{15} = –17^{50} = ^{0}–18^{40} = ^{1}–20^{30} = ^{0}–21^{20} = ^{1}–24; ⌓$^{2}0^{00}$–12, 20–24
8	4	0.0	•	•$^{0}11^{40-50}$ •^{1}–12^{45} •^{0}–15^{30}...16^{45}, 17^{25}–19^{25}; = $^{0}0^{00}$–3^{35} = ^{2}–6^{20} = ^{1}–7^{30} = ^{0}–7^{40} = –15^{10} = ^{0}–16^{40} = –24; ⌓$^{2}0^{00}$–11^{40}
9	8	0.2	•	•$^{0}22^{35}$, 23^{15}; = 0^{00}–5^{00}; ⊕ 7^{40}–8^{30}
10	8	•	•	= 5^{00}–6^{25} = ^{0}–7^{08} = –9^{20}; ⌓^{0}23–24
11	8	•	•	⌓$^{0}0^{00}$–10
12	8	•	•	= 5^{20}–6^{35} = –10^{30}; ⌓^{0}2–6 ⌣^{0}–8, 20^{30}–24
13	8	•	•	= 0^{00-35} = ^{0}–2^{35} = –9^{15}, 18^{40}–24; ⌣$^{1}0^{00}$–9 ⌓^{0}21–24
14	8	•	•	= 0^{00}–0^{30}, 17^{30}–24; ⌓$^{0}0^{00}$–1 ⌣^{0}–9 ⌓^{0}20–24
15	7	•	•	= 0^{00}–3^{35} = –5^{20} = –9^{10}, 18^{30}–23^{30}; ⌓$^{0}0^{00}$–1 ⌣^{0}–9
16	8	3.0	•	•$^{0}15^{10}$–18^{20}; = 14^{20}–16^{25}, 23^{40}–24
17	8	•	•	= 0^{00}–1^{30}
18	8	•	•	= 19^{30}–24, ⌓$^{0}0^{00}$–9, 19^{30}–24
19	6	•	•	= 0^{00}–3^{25} = ^{0}–5^{10} = ^{1}–8^{40} = ^{0}–10^{30} = –13^{40}, 20^{10}–24; ⌓$^{0}0^{00}$–12
20	7	•	•	= 0^{00}–11^{20}; ⌓^{1}18–24
21	7	•	•	= 0^{00}–3^{45} = ^{0}–6^{45} = = –7^{20} = –12^{30}, 22^{30}–24; ⌓$^{1}0^{00}$–1 ⌣^{1}–9 ⌓^{0}–11 ⌣^{1}21–24
22	6	•	•	= 0^{00}–2^{45} = ^{0}–22^{10} = ^{1}–22^{30} = ^{2}–23^{15} = ^{1}–23^{25} = ^{0}–24; ⌣$^{1}0^{00}$–10, 18–24
23	5	•	•	= $^{0}0^{00}$–1^{40} = ^{1}–2^{00} = ^{2}–4^{35} = ^{2}–6^{15} = ^{1}–6^{45} = ^{0}–6^{50} = –24; ⌣$^{2}0^{00}$–11 ⌓^{0}21–24
24	7	•	•	= 0^{00}–9, 17^{30}–20^{20} = ^{0}–21^{40} = ^{1}–23^{35} = ^{2}–24; ⌓$^{0}0^{00}$–10^{30} ⌣^{0}18^{30}–24
25	6	•	•	= $^{2}0^{00}$–1^{45} = ^{2}–10^{35} = ^{1}–11^{30} = ^{0}–11^{40} = –17^{30} = = –18^{40} = ^{0}–18^{45} = ^{1}–19^{30} = ^{2}–20^{20} = ^{1}–20^{40} = ^{0}–21^{10} = –24; ⌣$^{0}0^{00}$–1 ⌣^{1}–10, 19–24
26	5	•	•	= 0^{00}–1^{45} = ^{0}–2^{15} = ^{1}–3^{10} = ^{1}–8^{40} = ^{0}–10^{30} = ^{0}–10^{40} = –16^{42} = ^{0}–17^{03} = ^{1}–18^{10} = ^{2}–19^{20} = ^{2}–24; ⌣$^{1}0^{00}$–2, 23–24
27	7	•	•	= $^{2}0^{00}$–1^{35} = ^{1}–2^{10} = ^{0}–2^{35} = –4^{45} = ^{0}–7^{40} = –12^{30}, 16^{05}–24; ⌣$^{1}0^{00}$–9 ⌓^{0}22–24
28	7	•	•	= 0^{00}–10^{30}, 21^{30}–24; ⌣$^{0}0^{00}$–8 ⌓^{0}22^{30}–24; ⊕ 11^{30}–14^{45}
29	8	0.0	•	•$^{0}18^{15-20}$; = 0^{00}–1^{30}; ⌓$^{0}0^{00}$–9
30	8	•	•	= 16^{15}–24; ⌓^{0}1–11, 22–24
31	8	0.8	•	•$^{0}9^{20-48}$; ≫10^{20}–12, 13^{35}–14^{20}; = 0^{00}–1^{20}; ⌓$^{0}0^{00}$–3
Σ	–	4.0	–	

Wrocław – Strachowice $\varphi = 51°06'$ $\lambda = 16°53'$ *Listopad – Novembre 1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	93.3	88.2	85.6	88.4	6.2	12.3	13.0	11.1	13.8	5.5	98	83	74	85	0.2	2.4	4.0	2.2	10 •	10	7	SSW 4	WSW 6	WSW 6
2	85.5	86.7	89.4	87.1	11.9	12.1	7.6	9.8	14.0	6.4	70	55	89	71	4.1	6.3	1.2	3.9	9	9	3	WNW13	NW 13	W 6
3	94.0	94.4	97.2	95.2	4.4	8.9	3.1	4.9	9.7	3.0	93	79	97	90	0.6	2.4	0.2	1.1	4	7	9	W 5	WNW 4	W 4
4	103.1	106.6	110.2	106.6	-0.2	6.0	0.8	1.8	6.9	-1.3	94	83	90	89	0.4	1.6	0.7	0.9	1	5	0	W 3	WNW 5	WNW 3
5	113.2	114.5	117.0	114.9	1.0	6.2	4.0	3.8	6.6	-2.7	94	89	93	92	0.4	1.0	0.5	0.6	1	9	9	WNW 2	NW 4	NW 2
6	117.2	116.1	112.0	115.1	3.1	5.9	0.4	2.4	7.2	-1.1	91	89	100	92	0.6	1.4	0.0	0.7	10	4	2 ≡	NW 4	NW 3	SSE 2
7	107.5	105.5	106.0	106.3	-4.4	8.6	-0.2	1.0	9.6	-4.9	98	74	98	90	0.1	2.9	0.1	1.0	0 ≡	0	7	C 0	SE 3	C 0
8	107.6	108.7	109.4	108.6	-2.6	7.3	1.3	1.8	9.2	-3.9	100	77	98	92	0.0	2.3	0.1	0.8	10 ≡	2	9	ENE 1	SW 2	C 0
9	108.6	108.1	107.1	107.9	4.0	9.4	8.6	7.6	9.6	1.3	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 ≡	10	C 0	NW 3	NW 1
10	105.3	104.5	102.3	104.0	7.4	7.8	6.8	7.2	8.8	6.6	100	96	97	98	0.0	0.5	0.3	0.3	10 ≡	10	10	ENE 1	ESE 1	C 0
11	98.0	95.9	94.0	96.0	4.6	5.6	2.2	3.6	6.8	2.1	92	67	77	79	0.7	2.9	1.7	1.8	10	10	10	E 4	E 4	ENE 2
12	93.5	94.8	96.2	94.8	-1.0	-0.4	-0.8	-0.8	2.4	-1.6	97	82	83	87	0.2	1.1	1.0	0.8	10 *	10 *	10	NE 4	NE 5	ENE 3
13	96.7	97.1	98.3	97.4	-1.5	-2.2	-3.2	-2.5	-0.6	-3.2	82	79	86	82	1.0	1.1	0.7	0.9	10	10 *	10 *	ESE 4	ENE 3	E 2
14	98.8	100.0	100.9	99.9	-4.1	-3.7	-5.2	-4.6	-3.1	-5.3	87	83	93	88	0.6	0.8	0.3	0.6	10	10 *	10 △	E 3	NE 3	NE 2
15	101.7	103.9	108.2	104.6	-6.0	-4.2	-5.0	-5.0	-3.5	-6.9	97	79	83	86	0.1	0.9	0.7	0.6	10 *	10	10 *	NNW 1	NW 3	NNW 2
16	112.2	113.4	114.1	113.2	-4.7	-3.8	-4.0	-4.1	-3.3	-6.3	86	87	94	89	0.6	0.6	0.3	0.5	10 *	10	10	NNW 4	NW 3	C 0
17	111.4	108.8	104.6	108.3	-5.8	-5.6	-9.7	-7.7	-3.4	-10.3	92	85	88	88	0.3	0.6	0.4	0.4	10	10	0	SE 4	SE 7	ESE 5
18	98.9	95.9	93.2	96.0	-10.2	-8.8	-7.2	-8.4	-7.2	-10.5	84	86	96	89	0.4	0.4	0.1	0.3	10	10	10 *	ESE 5	ESE 4	ESE 3
19	89.5	86.9	86.8	87.7	-5.2	-0.3	-1.4	-2.1	0.6	-7.4	95	92	92	93	0.2	0.5	0.4	0.4	10	10	6	ESE 3	SE 4	NNW 1
20	88.0	88.9	86.5	87.8	-3.4	-1.5	-1.2	-1.8	-0.6	-4.9	97	90	99	95	0.2	0.5	0.1	0.3	10	10	10 ≡	NNW 1	NE 1	ESE 4
21	78.2	73.0	74.4	75.2	0.4	0.9	1.2	0.9	3.6	-1.6	100	98	90	96	0.0	0.1	0.7	0.3	10 ≡	10 •	10 ⚹	SE 4	SE 4	WNW11
22	87.6	94.0	99.9	93.8	-1.6	0.0	-3.4	-2.1	1.2	-3.9	92	88	81	87	0.4	0.7	0.9	0.7	10 *	8	9	NW 7	NW 3	NW 4
23	104.7	106.3	107.5	106.2	-9.9	-5.2	-11.8	-9.7	-3.0	-12.3	94	78	93	88	0.2	0.9	0.2	0.4	4	7	0	NNW 3	NW 3	S 4
24	104.7	102.1	98.4	101.7	-11.8	-0.8	-5.5	-4.9	-0.6	-12.6	93	58	67	73	0.2	2.4	1.5	1.4	0	3	9	SSE 2	S 6	S 4
25	97.9	100.7	99.5	99.4	0.3	1.3	-4.4	-1.8	2.0	-5.2	80	85	89	85	1.2	1.0	0.5	0.9	10	10 *	0	WSW 6	W 5	S 5
26	88.4	86.0	89.1	87.8	0.8	2.6	1.3	1.5	3.8	-4.7	73	67	85	75	1.8	2.5	1.0	1.7	9	10	10	S 8	S 3	W 3
27	86.6	77.7	68.5	77.6	-2.0	1.4	5.2	2.4	5.7	-4.7	96	91	80	89	0.2	0.7	1.8	0.9	10	9	9	SSE 5	SE 6	SSW 7
28	73.0	76.3	82.0	77.1	2.3	2.2	2.5	2.4	5.7	2.0	82	77	77	79	1.3	1.7	1.7	1.6	10	10 *	9	W 5	WNW 7	W 6
29	88.3	89.3	79.7	85.8	2.4	4.4	2.1	2.8	5.5	0.5	75	63	73	70	1.8	3.1	1.9	2.3	9	3	10	W 5	WSW 5	S 8
30	74.1	79.9	83.8	79.3	7.6	5.8	1.4	4.0	8.5	1.2	61	59	72	64	4.0	3.7	1.9	3.2	8	10	10	WSW 8	WSW 7	WSW 3
31																								
M	96.9	96.8	96.7	96.8	-0.6	2.4	0.0	0.4	3.9	-2.9	90	80	88	86	0.7	1.6	0.8	1.0	8.2	8.2	7.6	4.0	4.3	3.4

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1	79.9	83.6	88.5	84.0	2.1	4.4	3.5	3.4	5.1	-1.2	73	68	73	71	1.9	2.7	2.1	2.2	7	9	10	WSW11	WSW11	WSW 7
2	92.3	93.2	88.4	91.3	1.9	3.0	0.0	1.2	4.2	-1.5	93	95	82	90	0.5	0.4	1.1	0.7	10 •	6	2	WNW 5	W 5	S 6
3	82.3	82.6	83.1	82.7	0.5	2.4	1.4	1.4	3.8	-0.8	84	87	94	88	1.0	1.0	0.4	0.8	3	10	9	WSW 6	SSW 5	WSW 2
4	84.7	86.0	88.1	86.3	1.8	5.9	0.6	2.2	6.4	-1.4	91	73	94	86	0.7	2.5	0.4	1.2	9	3	10	SW 3	WSW 5	SSE 3
5	89.5	85.6	75.2	83.4	1.4	6.2	4.0	3.9	6.4	0.4	94	69	92	85	0.4	3.0	0.6	1.3	4	8	10 •	SSW 3	SSE 6	SSW10
6	79.8	83.1	87.9	83.6	5.7	7.8	5.4	6.1	9.6	4.0	68	64	71	68	3.0	3.8	2.7	3.2	1	5	7	W 8	WSW12	W 8
7	91.8	94.5	96.2	94.2	-0.1	5.0	3.7	3.1	6.2	-0.6	96	72	73	80	0.3	2.4	2.2	1.6	8	10	10	C 0	WSW 7	WSW 4
8	98.3	99.9	104.1	100.8	2.6	3.7	0.0	1.6	4.2	-0.3	84	83	88	85	1.2	1.4	0.7	1.1	10	8	3	WSW 3	WNW 5	NW 4
9	103.1	97.9	86.9	96.0	-0.3	4.5	2.8	2.4	5.7	-2.6	88	53	52	64	0.7	4.0	3.6	2.8	9	5	10	SSW 5	WSW 8	SSE 5
10	72.1	68.9	69.2	70.1	3.2	6.7	5.7	5.3	7.4	1.8	68	63	67	67	2.5	3.4	3.1	3.0	10	6	4	SW 10	WSW10	WSW 9
11	77.4	78.8	81.0	79.1	1.8	4.7	2.2	2.7	5.9	-0.4	74	56	73	68	1.8	3.7	2.0	2.5	3	3	5	WNW 7	WNW 9	W 9
12	87.2	89.4	92.1	89.6	2.2	3.0	0.8	1.7	3.6	-0.2	82	84	98	88	1.3	1.2	0.2	0.9	10	9	10 △	NW 7	NW 7	NW 4
13	95.4	95.2	91.0	93.9	-1.0	0.2	0.0	-0.2	1.3	-2.1	89	90	100	93	0.7	0.6	0.0	0.4	9	9	10 *	E 2	SSE 3	ESE 6
14	103.6	108.1	112.0	107.9	-6.2	-3.0	-7.3	-6.0	0.5	-7.6	92	86	99	92	0.3	0.7	0.0	0.3	2	9	10 ≡	NW 3	NW 4	WSW 2
15	107.4	106.3	106.8	106.8	-4.0	1.8	1.1	0.0	1.9	-8.1	96	91	100	96	0.2	0.7	0.0	0.3	10	10	10 •	SE 1	NW 5	NW 2
16	105.9	105.4	104.6	105.3	-2.0	-3.6	-3.2	-3.0	1.5	-4.4	96	94	92	94	0.2	0.3	0.3	0.3	10	10	10	ESE 2	SE 3	C 0
17	101.3	99.3	99.1	99.9	-3.6	-1.4	0.5	-1.0	0.6	-4.6	97	92	100	96	0.2	0.4	0.0	0.2	10 ≡	10 *	10 ≡	SE 3	SE 2	SE 2
18	96.9	95.5	97.7	96.7	1.8	2.8	8.4	5.4	8.6	-0.3	91	100	96	96	0.7	0.0	0.4	0.4	10	10 •	10 •	S 4	S 3	WSW 5
19	98.7	98.8	97.0	98.2	9.8	11.3	9.9	10.2	11.7	8.2	86	78	77	80	1.7	3.0	2.8	2.5	10	9	8	WSW 6	WSW 7	WSW 7
20	101.6	102.4	99.8	101.3	5.8	5.8	4.0	4.9	10.7	2.6	80	80	97	86	1.8	1.8	0.2	1.3	8	8	10 •	NW 5	NNW 1	NE 1
21	99.9	97.7	100.6	98.1	3.6	2.3	1.3	2.2	4.4	0.4	98	96	100	98	0.1	0.3	0.0	0.1	10 •	10 •	10 •	NNE 1	N 2	NNW 2
22	103.7	103.3	102.9	103.3	1.0	2.6	-2.2	-0.2	2.9	-2.5	87	79	98	88	0.9	1.6	0.1	0.9	9	1	0	NNW 2	S 3	SE 3
23	100.8	97.2	90.3	96.1	-4.8	0.2	-2.2	-2.2	0.3	-4.9	98	83	91	91	0.1	1.1	0.5	0.6	0	1	0	SE 3	SSE 7	SE 5
24	84.6	82.7	78.7	82.0	0.1	0.4	-2.2	-1.0	0.7	-4.0	88	96	91	92	0.8	0.3	0.5	0.5	10 *	10	0	SSW 5	S 4	SSE 5
25	72.9	71.7	71.6	72.1	1.2	2.0	2.2	1.9	2.7	-3.6	85	87	86	86	1.1	0.9	1.1	1.0	5	9	6	SSW 8	SSW 7	SSW 6
26	73.7	76.7	86.8	79.1	2.9	3.4	1.3	2.3	4.1	0.4	91	95	89	92	0.0	0.4	0.8	0.6	9	10 •	9	WSW 5	NNW 8	WNW 6
27	89.0	86.6	81.2	85.6	0.8	2.2	0.6	1.0	2.8	-1.6	77	77	90	81	1.3	1.7	0.6	1.3	4	3	10	SW 5	S 4	SSE 2
28	79.8	86.4	92.9	86.4	0.4	0.7	0.2	0.4	1.4	-1.3	96	85	78	86	0.3	1.0	1.4	0.9	10 •	9	8	NW 3	NW 5	W 5
29	94.9	98.8	99.7	97.8	-0.2	1.2	-0.7	-0.1	1.7	-3.1	80	77	87	81	1.2	1.5	0.7	1.1	10 *	2	4	W 6	NW 7	W 5
30	95.4	90.3	90.1	91.9	-1.3	2.0	1.1	0.7	2.3	-3.0	76	56	79	70	1.3	3.1	1.4	1.9	9	9	9	SW 6	WSW 8	W 7
31	90.4	91.3	93.0	91.6	3.2	4.3	2.1	2.9	4.3	0.9	79	80	89	83	1.6	1.6	0.8	1.3	10	5	10	WSW 5	WNW 5	W 3
M	91.3	91.5	91.5	91.4	1.0	3.0	1.5	1.8	4.3	-1.3	86	80	87	84	1.0	1.6	1.0	1.2	7.7	7.3	7.5	4.6	5.7	4.7

Wrocław - Strachowice $H_s = 120\,m$ $H_b = 123{,}8\,m$ $h_m = 10\,m$ Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ	OPAD R	GŁUB. ŚNIEGU h	POGODA
1	8	0.8	•	$\bullet^{0}0^{45}\ldots5^{30}$–$8^{05}\ldots^{27}$, 19^{45}–20^{10}, $\gg 14^{25}$–^{45}
2	8	2.1	•	$\bullet^{0}0^{40}\ldots^{25}$ $\bullet^{0}19^{01-12}$ 19^{20-45} 23^{02-15}, $\gg 1^{30}$, 2^{40} 5^{10}, 8^{05} (por. 22 miesiąc 5^{30}, por. 26 miesiąc 6^{00}), 10^{05-20}, 11^{28}, 14^{40} (por. 21 miesiąc 11^{30}, por. 22 miesiąc 14^{26}) $\gg 19^{01-10}$ (por. 20 miesiąc 19^{03}), 19^{25-40} (por. 25 miesiąc 19^{31})
3	8	5.5	•	$\bullet^{0}8^{42}$–9^{10}, 9^{18-31} $\bullet^{0}15^{10}$, $16^{05}\ldots18^{25}$ $\bullet^{1}$–19^{40}; $= 17^{20}$–23^{10} | 2.XI: 23^{01-18}
4	9	•	•	$\sqcup^{0}20$–24
5	6	•	•	$=6^{05}$–24; $\sqcup^{0}0^{00}$–5 $\frown^{0}19$–24
6	6	•	•	$=0^{00}$–19^{30} $=$ $=$–20^{45} $=^{0}$–24; $\frown^{0}0^{00}$–7 $\sqcup^{0}19^{45}$–24
7	6	•	•	$=^{0}0^{00}$–4^{15} $=^{1}$–7^{15} $=^{2}$–8^{35} $=^{1}$–8^{40} $=^{1}$–8^{50} $=^{0}$–9^{08} $=$–24; $\sqcup^{0}0^{00}$–10 $\frown^{0}19$–23 $\sqcup^{0}$–24
8	6	0.3	•	$=0^{00}$–1^{10} $=^{0}$–2^{20} $=^{1}$–2^{35} $=^{2}4^{00}$ $=^{2}$–8^{30} $=^{2}$–9^{00} $=^{1}$–9^{15} $=^{0}$–9^{25} $=$–$13^{30}\infty$–16^{30} $=$–24; $\sqcup^{0}0^{00}$–10 $\frown^{0}20$–24
9	5	0.8	•	$\bullet^{0}3^{00-20}$ $\bullet^{0}4^{40}\ldots5^{30}$–$9^{40}$; $=0^{00}$–5^{10} $=^{1}$–5^{20} $=^{1}$–6^{20} $=^{1}$–9^{40}, 10^{35}–12^{03} $=^{0}$–12^{18} $=^{0}$–13^{30} $=$–21^{40} $=^{0}$–24, $\frown^{0}0^{00}$–3^{08}
10	5	•	•	$=^{0}0^{00}$–1^{30} $=^{1}$–7^{30} $=^{0}$–8^{10} $=^{0}$–8^{35} $=^{1}$–9^{00} $=^{0}$–9^{10} $=$–24; $\frown^{0}21$–24
11	7	2.6	•	$*^{0}23^{10}$–24; $=0^{00}$–11^{35}; $\frown^{0}0^{00}$–7
12	7	0.1	3	$*^{0}0^{00}$–7^{42}, 8^{05}–11^{35}, $12^{45}\ldots13^{10}$–16^{40}
13	7	0.2	2	$*^{0}7^{45}$–24
14	7	2.5	3	$*^{0}0^{00-35}$, 3^{50}–6^{10}, 7^{30}–19^{05} $\triangle$–21^{40} $\leftrightarrow$–22^{30} $*^{0}$–24; $=16^{30}$–24
15	6	0.3	10	$*^{0}0^{00}$–11^{25} $16^{40}\ldots22^{15}$–24; $=0^{00}$–24
16	6	0.1	10	$*^{0}0^{00}$–10^{35} $14^{50}\ldots15^{27}$; $=0^{00}$–2^{30}, 6^{15}–24
17	6	0.0	8	$*^{0}9^{50}$–10^{28}; $=0^{00}$–24
18	5	2.4	8	$*^{0}15^{40}$–16^{10}–17^{05} $*^{1}$–20^{35} $*^{0}$–21^{40}; $=0^{00}$–24
19	5	1.0	11	$*^{0}8^{50}$–10^{05} $*^{1}$–10^{45}; $=0^{00}$–9^{15} $=^{0}$–12^{08} $=$–15^{40} $=^{0}$–18^{50} $=$–21^{30} $=^{0}$–24
20	4	•	11	$=^{0}0^{00}$–2^{00} $=^{1}$–3^{00} $=^{0}$–5^{40} $=$–15^{45} $=^{0}$–17^{40} $=^{1}$–19^{45} $=^{1}$–24
21	4	3.4	9	$\bullet^{0}7^{45}\ldots9^{00}$–$10^{30}$ $\bullet^{0}$–13^{28} 16^{35}–20^{38} $*^{0}$–21^{20} $*^{0}23^{40}$–24; $\gg 20^{20}$–24; $=^{1}0^{00}$–1^{30} $=^{0}$–4^{30} $=^{1}$–7^{35} $=^{0}$–8^{20} $=$–22^{15}
22	7	0.1	4	$*^{0}0^{00}$–$1^{00}\ldots2^{10}$–4^{35} $*^{1}$–5^{28} $*^{0}$–9^{15} 9^{30}–11^{35}, 21^{35}–22^{45}; $\gg 0^{00}$–1^{20}
23	7	•	3	$=8^{15}$–11^{20}, 16^{40}–24
24	8	0.8	3	$*^{0}22^{10-30}$ $*^{1}$–23^{35} $*^{0}$–24; $=0^{00}$–10^{50}
25	6	0.0	5	$*^{0}0^{00-38}$ 4^{10}–5^{07} $\overset{*}{\bigtriangledown}{}^{0}10^{15-30}$ $*^{0}12^{32}$–13^{20}
26	8	0.0	4	$\bullet^{0}15^{40}$–16^{10} $18^{45}\ldots19^{40}$
27	6	1.1	2	$*^{0}9^{45}$–10^{20} $10^{26}\ldots11^{05}$ $\bullet^{0}17^{40}$–18^{10} $18^{15}\ldots30$–20^{40}; $=6^{40}$–20^{40}
28	7	1.1	•	$\overset{*}{\bigtriangledown}{}^{0}12^{33}$–$13^{02}$ 13^{15-27} $\overset{*}{\bigtriangledown}{}^{0}14^{02-13}$ $\overset{*}{\bigtriangledown}{}^{0}14^{27-30}$ $\bullet^{0}14^{32}$–14^{40}–15^{27} $*^{0}$–15^{29} $*^{0}$–15^{35} $*^{1}$–16^{07} $*^{0}$–16^{10} $\bullet^{0}$–$17^{15}\ldots29$, $22^{05}\ldots23^{15}$
29	8	0.0	•	$\bullet^{0}8^{20-35}$, $9^{20}\ldots40$
30	8	•	•	$\gg 5^{02}$–6^{24}
31				
Σ	–	25.2	–	

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1	8	0.0	•	$\gg 5^{40}$–15^{10}
2	7	1.5	•	$\bullet^{0}3^{45}\ldots6^{30}$–$7^{40}$ $\overset{*}{\bullet}{}^{0}$–$10^{00}$ $\overset{*}{\bullet}{}^{1}$–$10^{20}$ $\overset{*}{\bullet}{}^{0}$–$11^{10}$ $\bullet^{0}12^{05-30}$; $=16^{15}$–17^{10}
3	7	1.8	•	$\bigtriangleup 0^{45}$–1^{02} $*^{0}1^{20-35}$ $\bullet^{0}12^{20}$–14^{40}, $15^{10}\ldots35$–16^{10}; $\oplus$ 9^{50}–10^{40}
4	7	0.0	•	$\bullet^{0}4^{10-35}$; $=4^{30}$–5^{20}, 20^{30}–24; $\sqcup^{0}18$–20^{30}
5	8	4.6	•	$\bullet^{0}2^{45}\ldots3^{05}$, $17^{10}\ldots18^{15}$–20^{10} $\bullet^{1}$–21^{30} $\bullet^{0}$–22^{15}; $\gg 14^{30}$–21^{30}; $=4^{20}$–7^{30}
6	8	0.2	•	$\bullet^{0}23^{40}$–24; $\gg 8^{20}$–14^{15} 17^{40}–18^{20}
7	7	•	•	$\bullet^{0}0^{00}\ldots10$–$15\ldots24$, $0^{45}\ldots1^{08}$; $\sqcup^{0}5^{30}$–9; $\bigtriangledown^{0}17^{40}$–$19^{05}$, 20^{00}–24
8	7	0.0	•	$\bullet^{0}11^{45}\ldots12^{30}$ $\overset{*}{\bigtriangledown}{}^{0}13^{40}$–$14^{02}$; $\bigtriangledown$ 0^{00}–1^{00}
9	8	•	•	$\gg 22^{00}$–23^{40}; $=2^{10}$–7^{15}; $\sqcup$ 0^{00}–10; $\bigtriangledown$ 1^{45}–4^{30}
10	8	•	•	$\gg 0^{40}$–1^{25}, 4^{00}–7^{15}, 10^{05-15}, 10^{20-40}, 11^{32}–14^{40}
11	8	0.0	•	$*^{0}20^{20-38}$; $\gg 4^{50}$–5^{20} 20^{20-40}
12	8	1.7	•	$\bullet^{0}2^{42}$–3^{20} 9^{50}–10^{20} 15^{20}–16^{15} $\overset{*}{\bullet}{}^{1}$–$17^{10}$ $\triangle 20^{10}$–21^{20}; $=18^{30}$–24
13	7	3.1	pż.	$*^{0}17^{45}$–19^{25} $*^{1}$–21^{40} $*^{0}$–22^{25} $*^{1}$–24; $=0^{00}$–11^{30}, 14^{30}–24
14	7	•	5	$*^{1}0^{00}$–1^{25}; $=0^{00}$–12^{40} 16^{35}–20^{40} $=^{0}$–21^{30} $=^{1}$–24; $\vee$ 21^{30}–24
15	5	0.7	5	$*^{0}7^{35}$–45 $\bullet^{0}18^{10}$–$23^{40}\ldots24$; $=^{1}0^{00}$–30 $=^{0}$–0^{35} $=$–23^{45} $=^{0}$–24; $\vee$ 0^{00-35}
16	5	0.0	pż.	$\bullet^{0}0^{00}\ldots20$–$1^{15}$ $\bullet^{1}$–2^{30} $\bullet^{0}$–$2^{35}\ldots3^{35}$; $=^{0}0^{00-10}$ $=^{1}$–0^{45} $=^{0}$–1^{02} $=$–24
17	4	2.1	pż.	$*^{0}2^{10}$–5^{10} $*^{1}$–5^{25} $*^{0}12^{20\ldots25}$–14^{10} $*^{1}$–15^{40} $*^{0}$–17^{45} $\bullet^{0}18^{40}$ 19^{45} $\bigcirc$–20^{40}; $=0^{00}$–5^{10} $=^{0}$–7^{10} $=$–19^{15} $=^{0}$–21^{35} $=$–24
18	7	12.0	1	$\bullet^{0}7^{40}\ldots9^{15}$–$12^{15}$, 14^{35}–18^{30} $\bullet^{1}$–19^{10} $\bullet^{0}$–20^{05} $\bullet^{1}$–21^{30} $\bullet^{0}$–24; $=0^{00}$–12^{40}, 15^{40}–24
19	8	0.1	•	$\bullet^{0}0^{00}\ldots1^{35}$, 3^{30}–4^{25} $8^{20}\ldots45$ 9^{00-20}, 17^{30-40}; $=0^{00}$–1^{00}
20	8	1.8	•	$\bullet^{0}0^{40}\ldots3^{35}$, 4^{20}–5^{32}, $18^{10}\ldots23^{35}$; $=16^{15}$–24
21	6	3.5	•	$\bullet^{0}4^{24}\ldots5^{16}$ 6^{10}–13^{23} $\overset{*}{\bullet}{}^{0}$–$14^{10}$ $*^{0}$–14^{40} $\overset{*}{\bullet}{}^{0}$–$17^{35}$ $\bullet^{0}$–18^{40}, 20^{40}–21^{25}; $=0^{00}$–24
22	7	•	•	$=0^{00}$–7^{10}, 15^{35}–24; $\sqcup^{0}19$–24
23	5	0.0	•	$=0^{00}$–24; $\sqcup^{0}0^{00}$–24
24	6	0.8	1	$*^{0}6^{27}$–12^{10}; $=0^{00}$–22^{30}; $\sqcup^{0}0^{00}$–6^{27}
25	8	0.0	1	$\bullet^{0}10^{45}\ldots12^{10}$
26	6	3.6	•	$\bullet^{0}8^{40}\ldots9^{08}$, $10^{45}\ldots11^{35}$–12^{30} $\bullet^{1}$–13^{10} $*^{0}$–$14^{20}\ldots35$, 17^{03}–10
27	8	0.0	•	
28	8	0.0	•	$\bigcirc^{0}6^{40}$–8^{10} $\bullet^{0}\ldots9^{15}$ $\overset{*}{\bullet}{}^{0}$–$10^{20}$ $*^{0}\ldots11^{00}$; $=3^{30}$–10^{30}
29	8	0.0	•	$*^{0}5^{50}$–6^{15}, 6^{45}–7^{05} $\overset{*}{\bigtriangledown}{}^{0}8^{12-20}$; $\sqcup^{0}22$–24
30	8	•	•	$\sqcup^{0}0^{00}$–13
31	8	0.1	•	$\overset{*}{\bigtriangledown}{}^{0}9^{15}$–$10^{10}$ $\bullet^{0}23^{21}$–24; $=16^{20}$–17^{30}
Σ	–	37.6	–	

Jelenia Góra — φ = 50°54' — λ = 15°48' — Styczeń – Janvier 1965

DNI	CIŚNIENIE P = 900+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	64.0	64.1	62.7	63.6	5.6	5.6	4.3	5.0	6.4	4.0	71	72	79	74	2.7	2.5	1.8	2.3	10 ●	9	8	WSW 6	SW 4	SW 3
2	59.6	60.1	62.7	60.8	1.1	2.3	-0.4	0.6	4.7	-0.5	90	89	98	92	0.6	0.8	0.1	0.5	9 ●	9	10	NE 1	SE 1	C 0
3	64.7	66.2	68.8	66.6	-1.9	0.6	-0.2	-0.4	0.8	-2.5	98	86	92	92	0.1	0.9	0.5	0.5	7	10 *	9 *	ESE 1	NW 3	NW 3
4	74.0	78.0	83.5	78.5	-0.9	-1.0	-1.6	-1.3	0.0	-1.9	81	87	75	81	1.1	0.8	1.3	1.1	9	10 *	9	NE 1	N 4	NW 3
5	80.9	79.7	81.9	80.8	-0.3	-0.1	0.8	0.3	1.0	-5.9	72	98	96	89	1.7	0.2	0.3	0.7	10	10 *	10 *	W 8	W 7	WNW 5
6	81.8	82.0	82.5	82.1	0.1	0.3	-1.2	-0.5	1.0	-1.2	94	94	93	94	0.4	0.3	0.4	0.4	10 *	10 *	10 *	WNW 4	WNW 4	NW 2
7	84.7	82.1	77.2	81.3	-12.4	-8.5	-6.4	-8.4	-0.5	-15.0	89	86	89	88	0.3	0.4	0.4	0.4	0 ≡	8	10	C 0	C 0	C 0
8	71.3	65.8	64.1	67.1	-1.2	2.1	4.1	2.3	5.1	-6.7	95	87	80	87	0.3	0.9	1.6	0.9	10 *	10	10 ●	C 0	ENE 2	W 6
9	64.9	64.6	67.5	65.7	3.8	2.5	1.8	2.5	5.4	0.7	87	93	82	87	1.1	0.5	1.3	1.0	10	10 ●	4	W 2	NW 2	W 4
10	60.0	65.4	79.1	68.2	2.3	0.9	0.2	0.9	2.8	-0.1	84	94	94	91	1.2	0.4	0.4	0.7	10	10 ●	10	WNW 7	WNW 6	WNW 5
11	80.7	79.4	77.0	79.0	-3.2	2.5	0.5	0.1	3.8	-3.7	86	75	79	80	0.7	1.8	1.3	1.3	2	4	9	SE 2	C 0	SE 3
12	75.6	72.2	71.5	73.1	-0.2	3.5	-0.4	0.6	4.3	-0.7	76	60	76	71	1.4	3.1	1.4	2.0	9	6	1	E 4	ESE 5	SE 1
13	73.4	75.3	76.2	75.0	-3.2	2.0	-1.4	-1.0	2.1	-3.6	86	69	87	81	0.7	2.2	0.7	1.2	0	9	2	ESE 1	ESE 2	NE 3
14	71.1	69.9	76.4	72.5	-1.3	2.6	2.0	1.3	3.6	-2.8	76	62	71	70	1.3	2.9	2.1	2.1	1	4	9	E 4	SW 6	WSW 4
15	80.1	79.0	75.3	78.1	-4.7	4.8	0.7	0.4	5.6	-5.3	91	44	71	69	0.4	4.8	1.8	2.3	1	2	10	SE 1	WSW 3	NE 6
16	74.8	76.8	73.3	75.0	-2.0	1.6	2.1	1.0	2.4	-3.8	81	67	50	66	1.0	2.3	3.5	2.3	6	10	3	C 0	WSW 5	SW 9
17	62.9	58.5	50.6	57.3	2.5	5.7	4.2	4.2	8.5	0.9	72	71	75	73	2.1	2.7	2.0	2.3	10 ●	10	10 ●	SW 5	SSW 4	S 8
18	54.6	54.0	52.1	53.6	3.4	4.1	1.9	2.8	4.6	0.9	60	53	62	58	3.1	3.8	2.7	3.2	8	8	7	WSW 8	SSW 9	WSW 8
19	51.5	51.6	55.1	52.7	-3.8	0.9	-2.4	-1.9	2.2	-4.6	89	73	85	82	0.5	1.7	0.8	1.0	4	10	3	C 0	SE 9	SSE 2
20	55.3	52.7	50.0	52.7	-4.1	0.1	-1.4	-1.7	0.3	-5.7	96	86	92	91	0.2	0.9	0.4	0.5	10	9	10 *	C 0	NE 1	NE 3
21	53.2	56.6	62.0	57.3	-2.1	-1.3	-1.0	-1.4	-0.8	-3.1	92	90	89	90	0.4	0.5	0.7	0.5	10	10 △	10	NW 1	WNW 3	WNW 1
22	63.8	64.4	67.1	65.1	-1.5	1.7	0.1	0.1	2.3	-2.1	92	67	73	77	0.4	2.3	1.7	1.5	10 *	6	9	C 0	SE 3	ESE 3
23	72.2	74.5	80.0	75.6	-2.0	2.9	-0.6	-0.1	3.7	-3.6	87	57	92	79	0.7	3.2	0.4	1.4	10	7	10	C 0	C 0	SE 1
24	83.3	83.5	83.7	83.5	-2.9	1.5	-1.2	-1.0	1.5	-3.4	95	80	94	90	0.2	1.4	0.4	0.7	9	10	10	SE 1	NW 2	C 0
25	79.4	76.4	74.0	76.6	-3.7	0.6	-1.0	-1.3	0.9	-4.0	94	67	87	83	0.3	2.1	0.7	1.0	10	8	10 *	C 0	E 1	C 0
26	70.8	69.8	69.7	70.1	-3.1	1.2	-0.4	-0.7	2.3	-4.1	95	85	76	85	0.3	1.1	1.4	0.9	10	10	8	C 0	C 0	ESE 4
27	69.3	69.7	69.9	69.6	-1.2	1.4	-0.4	-0.2	1.7	-2.2	78	63	84	75	1.2	2.5	0.9	1.5	6	3	8	SE 4	SE 3	ESE 3
28	70.2	70.1	69.4	69.9	-4.6	3.1	-3.4	-2.1	3.4	-5.9	96	64	94	85	0.2	2.7	0.3	1.1	5	10	0 ≡	C 0	S 3	C 0
29	68.2	68.6	69.4	68.7	-2.1	2.8	-0.2	0.1	3.3	-5.5	100	70	96	89	0.0	2.2	0.2	0.8	10	9	10	SE 1	SE 1	SSE 1
30	66.8	65.4	67.1	66.4	-2.3	3.0	3.0	1.7	4.1	-2.9	100	83	84	89	0.0	1.3	1.2	0.8	10	10	10	C 0	C 0	C 0
31	72.1	72.3	72.7	72.4	-0.7	-0.4	-1.4	-1.0	3.1	-1.6	95	96	94	95	0.3	0.2	0.3	0.3	10 *	10 *	10 *	NW 1	ENE 3	ENE 1
M	69.5	69.3	70.1	69.6	-1.5	1.6	0.0	0.0	2.9	-3.1	87	76	84	82	0.8	1.7	1.1	1.2	7.6	8.4	8.0	2.0	3.1	3.0

Luty – Février

1	76.2	76.8	80.9	78.0	-2.6	-2.9	-3.5	-3.1	-1.2	-4.1	85	84	88	86	0.8	0.8	0.6	0.7	10	10 *	9	W 3	WNW 4	WNW 5
2	85.4	87.3	90.3	87.7	-3.6	-3.1	-3.7	-3.5	-2.7	-5.2	90	79	94	88	0.5	1.0	0.3	0.6	10 *	9 *	10	WNW 4	NW 7	NW 2
3	87.7	84.7	84.0	85.5	-6.7	-1.7	-7.4	-5.8	-1.7	-8.8	96	75	96	89	0.1	1.3	0.1	0.5	8	9	9	WNW 1	WNW 3	SE 1
4	84.3	85.7	84.5	84.8	-3.1	-1.9	-2.2	-2.4	-1.4	-8.8	97	79	94	90	0.1	1.1	0.3	0.5	10 ●	10	10 *	C 0	W 4	WNW 5
5	76.2	75.5	82.4	78.0	-2.2	-3.2	-19.0	-10.8	-1.2	-19.2	94	83	89	89	0.3	0.8	0.1	0.4	10 *	4	0 ≡	SE 1	ENE 5	C 0
6	85.6	83.4	79.5	82.8	-20.7	-8.2	-5.5	-10.0	-4.8	-25.4	82	89	85	85	0.2	0.3	0.6	0.4	8	10	10 *	C 0	C 0	SE 1
7	76.5	77.5	71.8	75.3	-4.2	0.2	0.3	-0.8	0.8	-5.7	94	90	83	89	0.3	0.6	1.0	0.6	10	10	10	C 0	C 0	W 6
8	63.5	65.9	69.0	66.1	-4.1	-4.1	-3.8	-4.0	1.1	-4.9	87	87	85	86	0.6	0.6	0.7	0.6	10 * ⚠	9 *	10 *	NW 10	WNW 6	NW 4
9	75.5	79.3	83.7	79.5	-6.0	-5.7	-19.2	-12.5	-3.5	-20.2	87	82	89	86	0.5	0.7	0.1	0.4	10 *	9 *	7	N 5	NNW 3	C 0
10	78.8	73.8	73.6	75.4	-24.2	-2.1	-1.0	-7.1	-0.7	-25.0	79	77	87	81	0.2	1.2	0.8	0.7	3	10 *	10 *	SE 1	W 6	W 6
11	77.9	79.7	81.6	79.7	-4.4	0.2	-12.6	-7.4	0.8	-12.7	91	64	96	84	0.4	2.2	0.1	0.9	7	0	0	WNW 2	WNW 3	C 0
12	80.4	80.0	77.7	79.4	-5.3	2.1	0.7	-0.4	2.3	-15.1	98	77	65	80	0.1	1.7	2.2	1.3	10	10	7	SSE 1	W 2	SW 4
13	69.1	64.1	57.6	63.6	2.4	3.3	2.7	2.8	3.5	-1.2	65	64	70	66	2.6	2.7	2.2	2.5	10	9	9 ●	SW 8	WSW 6	W 6
14	54.8	59.2	64.8	59.6	0.6	1.9	-0.6	0.3	2.8	-1.3	86	75	87	83	0.9	1.8	0.7	1.1	10 *	9 *	10	W 7	W 10	W 5
15	69.7	70.1	70.2	70.0	-2.3	-0.8	-5.4	-3.5	0.0	-5.9	83	56	77	72	0.9	2.6	0.9	1.5	8	6	9	W 5	W 6	W 5
16	72.5	73.8	73.8	74.0	-6.2	-3.4	-9.7	-7.2	-3.2	-11.3	86	76	98	87	0.5	1.1	0.1	0.6	9	9	9	NW 4	NW 3	C 0
17	78.0	78.5	77.9	78.1	-6.8	-5.4	-4.0	-5.0	-3.9	-9.7	91	82	89	87	0.3	0.7	0.5	0.5	10 *	10	10 *	WNW 3	WNW 5	WNW 2
18	80.0	81.7	82.4	81.4	-3.6	-4.4	-3.7	-3.8	-2.7	-4.7	87	96	90	91	0.6	0.2	0.5	0.4	10 *	10 △	10	NE 5	NNW 1	C 0
19	83.2	83.7	84.3	83.7	-3.9	-3.4	-3.8	-3.7	-3.3	-6.5	92	82	84	86	0.3	0.7	0.6	0.5	10 ●	10	9	NNE 2	NNE 3	NE 3
20	86.3	87.7	89.1	87.7	-7.4	-6.4	-6.7	-6.8	-5.4	-8.4	85	81	78	81	0.5	0.7	0.8	0.7	10 *	10 *	10	N 2	E 4	E 2
21	86.0	84.3	81.0	83.8	-7.3	-4.2	-5.4	-5.6	-2.1	-8.2	88	72	82	81	0.4	1.2	0.7	0.8	10	3	10	E 3	NE 1	W 4
22	77.1	76.4	76.8	76.8	-6.4	-4.2	-2.8	-4.0	-2.6	-6.7	89	89	91	90	0.4	0.5	0.5	0.5	10 *	10 *	10 *	W 5	W 4	W 3
23	75.3	74.4	74.7	74.8	-6.6	-3.2	-4.2	-4.6	-2.1	-7.0	97	88	94	93	0.1	0.6	0.3	0.3	10 *	10 *	10	C 0	NNW 1	C 0
24	73.8	73.7	70.3	73.3	-5.2	-1.0	-9.0	-6.0	-0.1	-9.3	88	63	89	80	0.5	2.1	0.4	1.0	10	8	6	ENE 3	NW 2	C 0
25	67.0	67.7	72.1	68.9	-3.0	-4.8	-19.6	-11.8	-2.2	-20.0	84	86	89	86	0.8	0.6	0.1	0.5	10 *	9 *	0	WNW 6	NNW 3	SE 2
26	71.7	67.4	60.8	66.6	-10.9	-2.2	-2.9	-4.7	-0.6	-21.6	83	39	45	56	0.4	3.2	2.7	2.1	9	9	1	ESE 1	W 4	SW 7
27	52.8	57.0	68.2	59.3	-3.4	-6.3	-5.9	-5.4	-2.3	-7.5	97	89	81	89	0.2	0.4	0.7	0.4	10 *	8	9	W 5	W 9	WNW 7
28	71.8	70.1	66.9	69.6	-11.1	-3.7	-7.6	-7.5	-0.8	-14.1	86	47	82	72	0.4	2.5	0.6	1.2	6	3	9	SE 1	ENE 4	NE 1
29																								
30																								
31																								
M	75.7	75.7	76.1	75.8	-6.1	-2.9	-6.0	-5.2	-1.3	-10.7	88	77	85	83	0.5	1.2	0.7	0.8	9.2	8.3	8.0	3.1	3.9	2.9

Jelenia Góra $H_s = 342\,m$ $H_b = 343{,}9\,m$ $h_w = 16\,m$ Styczeń - Janvier 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘB. ŚNIEGU h	POGODA
1	8	0.0	•	•0^00...2^45, 4^15...7^15
2	6	0.0	•	•0^40 8^15; = 3^00–24
3	6	0.3	•	*0^1140...13^20, 20^40–24; = 0^00–24
4	6	0.4	1	*0^00...6^10 ⚥1^15–25 *0^825 9^10 13^15; = 0^00 13^30
5	4	4.4	2	*0^900...40 10^20 12^15 *1–13^05 *0–14^35 △0–15^05 •0–16^40 *1–17^10 •0–18^30 *0–22^15; = 10^30–24
6	5	6.8	4	*0^030...1^40 *1...3^00–10^06 *0–12^15 *0–14^10 *0–15^40 *0–19^35 *0–20^45...21^15; = 0^00–21^30
7	6	0.0	10	= 5^30–6^10 ≡2–7^20 ≡2–9^35 ≡1–10^40 = –24; ⊕ 12^20–14^15
8	7	2.7	9	*0^635–7^15 •0–8^15 13^20–14^40, 17^20–24; = 0^00–8^25; 18^35–24
9	6	3.2	2	•0^00–5^15...6^35, 7^25–8^10 11^40...13^45 *0–14^50 *0–16^20 •0...20^00; = 0^00–24
10	5	2.6	pz.	*0^240...3^05, 4^30...6^10 •0^725–8^45 *0^942–10^35 •0–13^40 △14^35–17^38 *0–19^20; = 0^00–3^00, 4^30–24
11	7	•	pz.	= 0^00–6^30, ⊕ 9^15–13^10 ⌣20^40–21^50
12	7	•	pz.	
13	7	•	pz.	= 18^30–24
14	7	0.0	pz.	*0^1840...19^20; = 0^00–6^00; ⌣0^1–10
15	8	•	pz.	⌓17^45–18^35
16	7	0.0	pz.	
17	7	0.5	pz.	•0^610...7^45 ⚥0^1025–42 •0^1700...19^40, 20^25...24; ⚲3^15–5^45
18	8	0.0	•	•0^00...2^00 ⚥0^845 9^15
19	8	•	•	= 17^20–24; ⌣0^4–9
20	5	0.0	•	*0^1210...39 17^35–24; = 0^00–24; ⌓1–3
21	5	1.0	•	*0^000...3^15 ◎0^835–9^15 △10^45–16^30 *0–17^15...18^30 ◎0^2325–24; = 0^00–24
22	6	0.0	2	◎0^000...1^30 ⚥0–2^15 *1–3^30 *0–4^40 5^15–9^50; = 0^00–14^20, 22^40–24
23	6	•	1	*0^500–45; = 0^00–7^30, 11^30–12^30 ∞–16^30 = –24; ⊕ 11–15
24	5	0.0	1	*0^1035...11^40; = 0^00–24
25	7	0.2	pz.	*0^1345...15^20–21^30; = 0^00–12^20, 13^40–24
26	6	•	1	= 0^00–24
27	6	•	pz.	= 0^00–24
28	6	•	pz.	= 0^00–20^40 ≡0–21^35 = –24
29	5	•	pz.	= 0^00–4^5 ≡2–7^20 = –24
30	5	2.0	pz.	•0^1330...14^25 ⚥0^1649–17^10 •0^1735–18^40; = 0^00–14^30, 18^40–24
31	4	5.2	5	*0^310...35–5^15 *1–6^30 *0–13^15 *1–16^30 *0–22^40; = 0^00–24
Σ	-	29.3	-	

Luty - Février

1	5	1.5	9	⚥0^1004–35 ⚥1–11^10, 12^10–17 ⚥0–12^26 ⚥0–12^34 ⚥0–13^06 15^20–35; = 0^00–24
2	6	2.0	12	*0^015 2^30 6^05 7^30 ⚥0^745 8^50 9^05–20 10^45 11^10 ⚥1–11^51 ⚥0–12^00 ⚥0–13^03 ⚥1–13^10 ⚥2–13^21 ⚥0–13^40 14^46 17^30 *0...20^20, 21^40 22^30 *1...24; = 0^00 13^40, 14^30–24
3	6	0.3	15	*1^000–10 *0...1^20; = 0^00–24
4	6	4.7	9	△0^240–5^30 ◎1–7^45 ◎0–10^40 *0^1945 20^10 22^20 △0–23^10 *0–23^40 *1–24; = 0^00–24
5	5	1.6	16	*1^00–6^15 *0–7^30 *1–10^20 *0–11^15; = 0^00–14^30, 18^45–20^45 ≡0–24
6	6	2.1	15	*0^2010–24; ≡0^00–6^30 = –24
7	5	1.7	17	*0^000–6^20, 8^40–9^15 ⚥2245–24; por. wiatru do 15 m/sek 22^30–24; = 0^00–24
8	5	8.5	18	⚥0^00–1^15 ⚹0^205–3^45 ⚹1^625–7^30 ⚥0–11^10 ⚥1–12^32 ⚥0–20^30 *0–21^45 *1–23^25 *0–24; ⚲1^15–6^25; = 0^00–4^00, 6^20–24
9	5	1.8	29	*0^00–5^45 *1–6^15 *0^815 *1–9^30 *0–10^15 11^15 ⚥1^1130–12^20, 12^35–13^10 ⚥0–13^32 14^15 ⚥1^1430–15^15 ⚥0^1515–16^10; = 0^00–16^30, 18^45–19^45 = = –21^25 = –24
10	6	0.1	31	*0^1205 14^40 *1–15^25 *0–17^00, 22^45 ⚥0–23^10...24; = 0^00–2^40 = = –3^10 = –7^10, 12^20–24
11	7	•	28	*0^000...30 1^40, 3^00; = 0^00–12^15 ≡1–23^25 = –24
12	5	0.3	22	*0^745 8^10 *1–8^15 *0–10^15 13^20–35, 15^42–17^25...18^40; = 0^00–22^20
13	7	2.8	20	•0^1630...21^25 ⚥1–21^45 ⚥2–22^10 ⚥1–22^20 ⚥0–23^45; por. wiatru do 16 m/sek 21^20–22^10, 23^20–24
14	6	0.7	20	⚥0^235 3^10 3^45 4^40 5^45 6^15 ⚥1 7^20 ⚥0 7^30 7^42–55 ⚥1 8^00 ⚥0–8^05 9^00 ⚥0^912 10^17 ⚥1–10^25 ⚥0 12^10 12^30 13^00 13^32–45 14^05–20 15^05–45 18^00–20 ⚥0^1915 20^05 ⚥0–20^50 ⚥1–21^40 22^15;
15	7	0.6	16	⚥0^810–30 9^05–15 ⚥0^1025–35; = 0^00–7^00 **14.II:** por. wiatru do 16 m/sek 0^00 2^25; do 14 m/sek 5^40 6^20, 8^45–11^15 ⚲11^40–13^20; = 6^40–24
16	6	2.4	16	*0^310...6^40 7^15–8^20 ⚥1–8^50 ⚥0–9^30 ⚥1–10^06 ⚥0–12^38 ⚥1^1340 14^18 ⚥0^1418–36 15^03 16^10, 17^02–40; = 9^05–24
17	6	7.4	21	*1^020–1^25 *0^515 10^20 13^15–14^25 *1–17^20 *0–24; = 0^00–24
18	5	0.6	31	*0^000–8^00 △0–16^20 *0...18^10; = 0^00–24
19	5	1.8	30	◎0^635–7^20 △–8^25 *1–9^30 *0–10^25 11^25...12^30 13^20...17^15–20^42; = 0^00–24
20	6	1.5	31	*0^220...6^30 *1–9^05 *0–12^05...15^05 15^40...16^10–19^15; = 0^00–24
21	6	0.0	28	= 0^00–24
22	5	1.1	26	*0^710 3^45 5^50...7^10 △–10^30 *0–12^20 *1–14^30 *0^1720–24; = 0^00–24
23	5	2.5	28	*0^000...7^20–8^10 *1–8^40 *0...10^30–16^15 *1–17^45 *0–20^40, 22^35...23^30–24; = 0^00–24
24	7	0.4	28	*0^000...3^20 8^40...9^15 23^10...24; = 0^00–12^20, 13^30–24
25	5	1.6	28	*0^000...6^10–8^35 *1–10^20 *0–11^25 ⚥1–12^20 ⚥0^1235 13^15 13^40–14^20; = 0^00–15^15 22^45–23^30
26	8	0.2	30	*0^715...2^25; ⚹0^1540–19^45
27	6	2.0	30	*0^040 6^50 *1 7^15 ⚥2 7^35 ⚥1–0^740 8^15 ⚥0^910–20 11^08–20 ⚥0–11^35–12^35 16^40 18^20 ⚥0^2325–24; ⚹1^710–10^20 ⚹0–11^05 ⚹1–14^15 ⚹2–19^20 ⚹1–24; = 0^20–10^15
28	8	•	37	⚥0^000–15 0^35–1^30 ⚥1–2^10 ⚥0^335–35 ⚥1^420–40 ⚥0^540–6^30; ⚹1^000–4^15 ⚹0–6^30
29				
30				
31				
Σ	-	50.2	-	

Jelenia Góra. $\varphi = 50°54'$ $\lambda = 15°48'$ *Marzec – Mars* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	64.3	62.3	58.2	61.6	-10.4	1.8	-1.7	-3.0	2.9	-11.7	84	64	75	74	0.4	2.6	1.3	1.4	7	9	9	SE 1	NNE 1	ENE 2
2	51.4	50.5	50.2	50.7	-1.8	-1.3	-3.0	-2.3	-0.7	-3.1	94	97	93	95	0.3	0.2	0.4	0.3	10	10	10 * ●	E 3	WNW 1	C 0
3	48.9	50.8	56.2	52.0	-5.2	-3.3	-5.0	-4.6	-2.7	-5.6	93	76	88	86	0.3	1.1	0.5	0.6	10 *	10	10 *	W 2	W 5	W 8
4	59.9	61.3	63.6	61.6	-6.6	-4.0	-6.3	-5.8	-2.7	-7.0	75	50	70	65	0.9	2.3	1.1	1.4	10 *	10	8	W 6	W 7	N 1
5	65.3	67.8	71.7	68.3	-11.4	-2.1	-11.6	-9.2	0.3	-13.1	90	60	86	79	0.3	2.1	0.4	0.9	8	8	0	C 0	NNW 2	SSE 1
6	74.0	75.6	79.6	76.4	-5.0	-5.4	-3.7	-4.0	-2.7	-15.2	83	88	90	87	0.7	0.6	0.5	0.6	10	10 △	10 *	ESE 2	ESE 1	ENE 2
7	83.1	85.1	86.1	84.8	-6.3	-5.3	-8.3	-7.0	-3.6	-9.1	94	80	83	86	0.2	0.8	0.5	0.5	10	9	10	NE 4	N 2	C 0
8	84.5	83.2	83.0	83.6	-10.4	-5.3	-16.4	-12.1	-4.0	-16.6	87	65	95	82	0.4	1.4	0.1	0.6	10 *	0	0	C 0	NW 2	C 0
9	83.2	83.1	85.0	83.8	-22.0	-0.8	-5.6	-8.5	0.1	-24.9	88	67	95	83	0.1	1.9	0.2	0.7	9	6	0	SE 1	N 2	NNW 2
10	87.9	89.3	90.2	89.1	-7.0	-0.2	-7.5	-5.6	0.4	-14.6	93	61	87	80	0.2	2.3	0.4	1.0	9	8	0	SE 2	NW 2	C 0
11	89.9	88.6	87.4	88.6	-17.5	1.8	-8.4	-8.1	3.3	-18.3	90	41	83	71	0.2	4.2	0.5	1.6	2	0	0	C 0	NNW 1	C 0
12	86.4	83.7	83.0	84.4	-17.0	4.3	-5.4	-5.9	6.2	-17.9	90	51	90	77	0.2	4.1	0.4	1.6	0	0	0	C 0	C 0	SE 1
13	82.8	82.0	82.2	82.3	-13.7	6.6	-5.8	-3.7	8.5	-14.2	96	54	87	79	0.1	4.5	0.6	1.7	0	0	0	C 0	ENE 2	C 0
14	81.1	80.1	80.2	80.5	-11.9	6.2	-1.7	-2.3	10.6	-12.8	97	56	86	80	0.1	4.2	0.8	1.7	0	0	5	E 1	SE 2	SE 1
15	79.9	79.2	78.1	79.1	0.3	9.6	5.0	5.0	9.9	-3.3	88	57	72	72	0.7	5.2	2.4	2.8	10 ●	9	9	SE 1	C 0	SE 4
16	74.0	73.0	74.7	73.9	5.0	9.1	2.7	4.9	9.9	2.3	79	56	95	77	1.8	5.1	0.4	2.4	9	10	10 ●	E 3	SW 4	C 0
17	74.2	71.3	69.5	71.7	-1.8	8.9	1.9	2.7	11.3	-2.0	98	54	89	80	0.2	5.2	0.8	2.1	5	5	8	C 0	SW 5	SE 3
18	65.7	63.1	62.2	63.7	-3.1	12.9	7.9	6.4	13.9	-3.8	97	39	54	63	0.1	9.1	4.9	4.7	2 ≡	3	9	C 0	ESE 1	SSE 3
19	63.9	66.9	72.8	67.9	6.5	10.4	3.6	6.0	10.8	3.4	65	56	86	69	3.4	5.6	1.1	3.4	3	6	10	WSW 3	W 4	W 2
20	76.1	75.2	74.5	75.3	-0.8	7.4	4.0	3.6	9.2	-1.3	96	47	88	77	0.3	5.4	0.9	2.2	4	9	10	C 0	NW 3	NW 2
21	67.6	63.1	66.5	65.7	4.3	7.2	3.4	4.6	8.0	0.9	77	70	95	81	1.9	3.1	0.4	1.8	10	9	10 ●	ESE 3	SSW 5	NW 4
22	72.1	74.7	74.9	73.9	-2.0	3.2	-3.1	-1.2	3.8	-3.4	89	45	81	72	0.6	4.5	0.9	1.9	5	5	0	WNW 4	SE 1	C 0
23	68.7	63.6	61.3	64.5	-4.1	8.9	4.5	3.4	9.2	-6.6	87	41	77	68	0.6	6.8	1.9	3.1	7	8	10 ●	C 0	SE 5	SE 3
24	60.3	61.3	63.5	61.7	2.4	9.0	8.4	7.0	11.3	1.1	93	70	69	77	0.6	3.5	3.4	2.5	9	9	9	C 0	SW 3	WSW 3
25	68.8	71.1	74.4	71.4	3.5	6.4	2.6	3.8	8.5	1.9	78	60	93	77	1.7	3.8	0.6	2.0	10	10	9 ●	W 7	W 7	W 4
26	73.1	67.9	72.6	71.2	1.4	5.5	3.7	3.6	6.0	0.3	91	65	92	83	0.7	3.1	0.7	1.5	7	10	10 ●	S 1	SE 6	WNW 1
27	82.4	87.8	90.7	87.0	2.8	5.1	1.2	2.6	7.7	1.0	98	80	89	89	0.2	1.8	0.8	0.9	10 ≡	10	0	NW 4	W 2	ESE 1
28	89.7	89.6	89.8	89.7	0.7	7.7	7.8	6.0	7.9	-2.1	94	77	97	89	0.4	2.4	0.3	1.0	10	10	10 ●	C 0	C 0	WNW 2
29	90.0	89.3	88.6	89.3	7.2	13.4	6.4	8.4	13.7	6.2	97	62	89	83	0.3	5.8	1.0	2.4	10	7	0	C 0	WNW 4	C 0
30	84.0	80.1	86.2	83.4	0.5	14.8	4.4	6.0	15.4	-0.6	98	41	77	72	0.1	9.9	1.9	4.0	4 ≡	4	10	C 0	W 6	N 6
31	88.2	85.3	85.1	86.2	-1.5	7.8	5.9	4.5	9.9	-4.0	92	57	52	67	0.4	4.5	4.4	3.1	0	8	8	C 0	WNW 6	NNE 5
M	74.9	74.4	75.5	74.9	-4.0	4.6	-0.6	-0.2	5.9	-6.3	89	61	84	78	0.6	3.8	1.1	1.8	6.8	6.8	6.3	1.5	3.0	2.0

Kwiecień – Avril

1	89.1	90.0	89.1	89.4	0.1	6.9	-0.3	1.3	8.1	-2.8	82	51	84	72	1.2	4.9	1.0	2.4	3	6	0	WNW 2	NW 4	C 0
2	85.8	85.2	84.7	85.2	-2.1	11.3	2.0	3.3	12.6	-5.3	92	33	68	64	0.4	9.0	2.3	3.9	0	2	0	C 0	WNW 8	SSE 1
3	81.3	78.7	77.0	79.0	-1.7	14.9	4.5	5.6	15.3	-4.3	88	24	65	58	0.7	12.9	3.1	5.6	6	2	0	C 0	WNW 8	C 0
4	74.7	72.4	71.5	72.9	-1.4	15.6	6.4	6.8	16.2	-2.9	91	33	76	67	0.5	11.8	2.3	4.9	1	0	0	C 0	W 7	C 0
5	74.4	73.3	76.1	75.3	-0.3	13.5	4.4	5.5	14.3	-1.4	94	45	62	67	0.4	8.3	3.3	4.1	1	4	0	SE 1	NE 1	C 0
6	73.8	73.2	71.0	73.3	0.3	16.7	6.3	7.4	17.8	-2.3	88	32	82	67	0.7	13.0	1.7	5.1	0	1	0	C 0	N 2	SE 1
7	72.3	73.5	72.4	72.7	6.5	6.5	4.9	5.7	9.4	4.3	90	84	89	88	1.0	1.6	1.0	1.2	10 ●	10	10	WNW 5	NW 4	C 0
8	70.6	68.9	68.7	69.4	0.2	12.3	8.1	7.2	13.3	-1.0	98	54	70	74	0.1	6.5	3.3	3.3	0	7	7	C 0	E 5	C 0
9	67.2	67.9	69.4	68.2	5.2	6.0	5.8	5.7	8.2	4.7	94	94	85	91	0.5	0.6	1.4	0.8	10 ●	10	10	E 3	E 6	E 2
10	71.6	72.4	72.1	72.0	2.3	4.2	3.9	3.6	5.8	2.1	91	77	78	82	0.6	1.8	1.8	1.4	10 ●	10	10	ESE 2	E 4	E 3
11	68.7	67.7	69.6	68.7	1.6	11.0	5.4	5.8	12.6	-1.8	83	55	89	76	1.2	5.8	1.0	2.7	1	2	4	C 0	WNW 2	C 0
12	72.2	73.4	71.8	72.5	4.6	6.5	4.3	4.9	7.4	3.7	92	76	95	88	0.7	2.3	0.4	1.1	10 ●	10 ●	10	WNW 2	NW 2	C 0
13	68.7	68.1	72.1	69.6	2.1	12.2	3.9	5.5	12.7	-0.8	96	44	92	77	0.3	8.0	0.7	3.0	7	7	9	C 0	WSW 3	C 0
14	75.3	77.2	78.6	77.0	0.8	9.2	3.2	4.1	9.6	-1.7	96	65	91	84	0.3	4.1	0.7	1.7	10	7	9	C 0	WNW 4	C 0
15	77.9	75.7	73.0	75.3	-0.1	10.5	3.1	4.2	11.2	-1.0	98	45	86	76	0.2	6.9	1.0	2.7	7 ≡	7	1	C 0	SE 4	E 1
16	67.1	65.7	67.7	66.8	7.4	9.8	6.7	7.6	10.4	-0.4	70	57	91	73	3.1	3.2	0.9	3.1	9	10	10 ●	SE 1	S 6	C 0
17	72.9	70.9	62.7	68.8	3.5	8.4	8.2	7.1	10.2	2.9	81	53	50	61	1.4	5.1	5.4	4.0	9	9	10	W 4	WSW 3	SSW 4
18	53.9	56.7	61.7	57.4	7.8	11.8	2.8	6.3	12.9	2.4	72	49	93	71	3.0	7.0	0.6	3.5	10	7	0	SW 3	W 6	SSE 1
19	62.3	61.1	59.8	61.1	2.9	6.4	5.3	5.0	8.6	2.1	91	79	86	85	0.6	2.0	1.3	1.3	10	10	10	WNW 2	E 2	C 0
20	59.9	60.8	61.6	60.8	4.3	5.6	5.3	5.2	6.2	3.1	87	89	95	90	1.1	1.0	0.4	0.8	10	10 ●	10 ●	C 0	W 2	SW 3
21	60.7	60.7	60.3	60.6	3.9	7.1	7.1	6.8	7.6	4.0	97	94	94	95	0.3	0.6	0.6	0.5	10 ●	10 ●	10 ●	C 0	NE 2	WNW 4
22	58.6	58.4	59.8	58.9	6.6	7.9	5.7	6.5	8.1	5.3	96	96	83	92	0.4	0.4	1.6	0.8	10 ●	10 ●	10	WSW 3	C 0	NNE 2
23	59.2	60.0	62.2	60.3	4.0	5.3	4.3	4.3	6.0	3.8	93	84	92	90	0.5	1.4	0.7	0.9	10 ●	10 ●	10	WNW 3	WNW 5	WNW 4
24	62.0	62.4	63.3	63.3	4.4	8.4	4.6	5.5	9.3	3.7	89	66	89	81	1.0	3.7	1.0	1.9	9	10	0	W 6	W 6	C 0
25	66.6	68.0	68.6	67.7	4.9	3.6	4.1	4.7	8.0	2.1	87	81	90	86	1.1	1.7	0.8	1.2	10	10	10	C 0	WNW 3	SE 3
26	69.7	68.5	65.8	68.0	1.0	9.7	2.6	4.0	10.2	-1.3	92	54	93	80	0.3	3.3	0.4	2.1	1	9	0	C 0	W 3	SE 3
27	61.0	60.6	61.1	60.9	5.8	8.3	5.3	6.2	9.3	0.6	73	68	87	76	2.3	3.6	1.1	2.4	9	10 ●	4	SE 4	NNW 1	ENE 3
28	58.2	57.8	60.9	59.0	4.4	9.2	3.3	6.0	9.7	2.9	97	76	81	83	0.3	2.7	1.7	1.6	10	9 ●	10	C 0	NE 5	S 1
29	63.2	67.1	71.3	67.9	3.9	9.7	4.1	6.0	11.4	2.3	71	50	83	68	2.7	6.0	1.4	3.4	4	8	0	S 4	S 5	S 1
30	74.9	73.9	77.7	76.2	4.8	11.6	8.3	8.2	12.0	-0.2	86	60	77	74	1.2	3.4	2.6	3.1	9	8	9	C 0	W 3	ENE 3
31																								
M	69.3	69.1	69.5	69.3	3.1	9.4	4.8	5.3	10.3	0.8	88	62	83	78	1.0	3.0	1.3	2.3	6.9	7.3	5.8	1.6	3.9	1.3

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ h	POGODA
1	8	0.0	34	= 21^20_24
2	4	4.8	30	*0^40_3^10 ●1^45_16^30 ◎0–20^35 ●*0–21^30 *0–22^20_23^45 ◎0–24; ⊹0^40_7^10; = 0^00_24
3	6	2.6	32	◎0^00_3^30 *0–6^10 *1–9^35 *0–11^35 14^10_15^25 18^15_19^30–21^15 *1–22^30 *0–24; ⊹1^45_16^20 ⊹0–17^15 ⊹1–18^20 ⊹0–24; = 0^00_24
4	8	0.0	43	*0^00_8^20; ⊹2^00_6^30 ⊹0–19^35; = 0^00_8^35
5	6	.	42	= 5^10_24; ⊕ 8^40_11^20
6	5	1.7	40	△0^6^50_14^30 *0_15^45 *1–16^30 *0–24; = 0^00_24
7	5	0.0	42	*0^00_4^15 △0^8^30_12^15; = 0^00_24
8	6	0.1	40	*0^6^45_9^20; = 0^00_13^20; 17^35_24
9	5	0.1	37	*0^7^45_8^20_9^20_11^40 ⊛0^14^10–45; = 0^00_24; ⌴1–11, 23–24
10	7	.	35	*0^3^40_5^10; = 0^00_9^20, 17^40_24; ⌴1 0^00_4
11	6	.	35	= 0^00_14^30 17^15_24; ⌴0 1–2 ⌴2–8
12	6	.	33	= 0^00_10^30 ∞–18^30 =–24
13	6	.	31	= 0^00_24; ⌴0 6–8
14	7	0.0	29	= 0^00_12^15 21^40_24; ⌴0 2–10
15	7	0.0	24	●0^6^40_7^15; = 0^00_5^50
16	8	1.3	20	●0^16^45_18^15_20^45 24; = 19^30_24
17	8	.	15	●0^0^00_1^45; = 0^00_7^40, 21^30_24
18	8	.	7	= 0^00–45 =1–6^30 =2–7^15 =↖–10^10
19	8	0.5	pż.	⊛0^16^34_17^10; = 16^20_20^20
20	8	0.0	pż.	●0^2^45_5^10 ⊛0^18^45_19^10; = 1^35_9^45, 19^15_24
21	7	0.8	.	⊛0^13^35–15^15 ●0_17^20 18^30_20^10 ●_22^15 23^45_24; = 0^00_6^45, 18^30_23^40 =0_24
22	8	0.0	.	●0^0^00–30 *0–1^10 ⊛0^7^50_8^20; =0^00–35 =–5^50; ⌴0 20–24
23	8	1.4	.	●1^19^35–20^10 ●0_21^15; = 19^45–21^30; ⌴1 0^00_8
24	8	0.9	.	⊛0^21^15–22^05; = 21^20_24
25	7	0.2	.	⊛0^2^05–50 ●0^6^08_30 ⊛0^20^40_21^25; = 0^00_5^00, 16^40_21^25
26	7	3.8	.	●0^13^50_17^30_24; = 2^30_4^20, 19^20_24
27	6	.	.	●0^0^00_15 ●0–6^15; = 0^00_6^25 =0–6^40 =1–7^20 =–7^35 =–15^45 ∞–16^45 = 18^30_24
28	6	8.1	.	●0^8^40_9^20 ●●1^13^35_14^05 ●0_15^25 ●0_17^05_24; = 0^00_5^30, 12^20_24
29	7	0.1	.	●0^0^00_3^20_4^40 ●0^8^20_50; = 0^00_12^20 14^40_20^40 ==–21^10 =–24; ⌓0 22–24
30	7	..	.	= 0^00–50 ==–3^30 =2–4^40 =2–6^10 =1–7^45 =–12^25; ⌓0^00_3 ⌴1–6 ⌓1–7
31	8	..	.	= 2^20–8^45; ⌴1 3–5 ⌴2–7
Σ	–	26.5	–	

Kwiecień - Avril

1	8	.	.	
2	7	.	.	= 7^20–8^00 ∞–9^30; ⌴1 1–4 ⌴2–8
3	7	.	.	⌴0 2–4 ⌴1–8
4	6	.	.	= 1^30–9^15 ∞–19^45 =–24; ⌴0 2–8
5	7	.	.	= 0^00_10^05; ⌴0 5–8
6	7	0.0	.	= 1^20_7^30, 19^10_24; ⌴0 1–7
7	5	0.1	.	●0^5^15_6^00 ⊛0^6^45_7^15 ●0^7^30_10^15; = 0^00_24
8	7	3.1	.	●0^23^25_24; = 0^00_9^30 ∞–10^30 = 17^15_24
9	5	0.5	.	●0^0^00_6^20_12^15 ●1^15^25_16^20 ●0–19^15, 22^30_24; = 0^00_24
10	6	0.0	.	●0^0^00–40 6^40_7^10; = 0^00_24
11	7	1.1	.	= 0^00_10^35 16^50_24; ⌓0 6–9
12	6	3.0	.	●0^4^15_6^20_12^45 ⊛0–13^15 14^50_15^05, 15^45_16^10; = 0^00_19^30 19^30_22^50 =0–24; ⌔20^30_22^40
13	8	1.6	.	⊛0^14^53_15^22 ⊛1–15^40 ⊛0–15^47 ●0^17^30_18^40; =0^00_1^30 =1–2^45 =0–5^45 =–7^20, 15^15_23^40 =–24
14	6	0.0	.	=0^00_6^15 =–13^10, 19^30_24
15	7	.	.	= 0^00_3^30 =0–7^30 =–9^30 19^35_24; ⌔1–2 ⌴0 5–7
16	7	0.9	.	●0^13^47_15^45, 18^35_21^30_24; = 0^00_9^20; ⌴0 2–6 ⌓1–8
17	8	0.0	.	●0^0^00_5^15; = 5^15_7^20
18	8	2.2	.	●0^4^50_5^10 ⊛0^10^05–25 15^49_16^20; = 20^45_24
19	6	0.0	.	●0^3^45_6^15, 8^45_9^15; = 0^00_13^30, 19^45_24
20	6	8.6	.	●0^7^45_9^15_16^20 ●0^19^40_19^35 ●0–24; = 0^00_24
21	5	7.9	.	●0^0^00_4^15_5^35 ●1–6^25 ●0_12^10 ●0–15^38 ●1–16^20 ●0–17^35 ●0–18^20_20^40 21^40_24; = 0^00_24
22	5	8.2	.	●0^0^00_7^35 ●1–8^10 ●0–17^15 ●1–13^20 ●0–15^05 ●1–15^40 ●0_16^20, 19^20_20^10; = 0^00_24
23	5	2.8	.	●0^3^10_5^30–6^40_8^40 ⊛0^12^48_13^20 14^16_16^14 17^22–19^15 19^30_20^12; = 0^00_24
24	7	4.1	.	⊛0^4^20–40 ⊛1–5^10 ⊛0^5^25_6^00, 7^47_10^35 ⊛1^13^42–51 ⊛0–14^25 ●0–15^15; por wiatru do 15 m/sek 13^40; = 0^00_12^40, 13^50_15^30, 20^35_24
25	7	1.3	.	⊛0^0^00–40 ●0–2^45 ⊛0^9^20–35 11^05_12^10 ●0^17^40_20^35 21^10_22^20; = 0^00_8^30, 19^40_24
26	8	2.4	.	⊛0^14^50_15^22 16^20_17^15; = 0^00_3^45 =1–5^40 =0–6^30; ⌓1 6–8
27	7	2.5	.	●0^11^40_13^30–18^25; = 0^00–4^20, 13^30_24
28	6	6.4	.	●0^0^10_6^20, 8^40_10^25 ⊛0^12^42_13^10 ⊛1^13^29–34 ⊛0^13^40 ⊛1–13^55 ⊛0–14^40, 21^40_22^10 ●0_23^20; ⊠0^13^20_14^30 SE NW; = 0^00_13^40, 22^20–23^30
29	8	.	.	
30	7	0.0	.	⊛0^13^40_14^05, 14^50_15^07, 15^37–40; = 0^00_8^30, 20^30_24; ⌓1 2–4 ⌓2–7
31				
Σ	–	56.7	–	

Jelenia Góra — φ = 50°54' — λ = 15°48' — Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	78.8	78.1	77.2	78.0	5.2	13.6	6.3	7.8	14.4	1.5	92	40	84	72	0.7	9.3	1.5	3.8	6	5	9	C 0	WNW 3	SE 1
2	79.3	78.0	77.3	78.2	5.4	11.4	5.2	6.9	12.1	-1.7	47	41	64	51	4.8	3.0	3.1	5.3	0	1	0	ENE 3	ENE 3	ESE 2
3	77.0	76.7	76.4	76.7	2.2	10.6	4.8	5.6	11.3	-3.0	64	38	59	54	2.6	8.0	3.5	4.7	0	1	0	C 0	N 4	E 3
4	73.8	70.3	66.2	70.1	6.6	15.8	11.3	11.2	16.8	-1.1	59	37	67	54	3.9	11.2	4.4	6.5	5	8	8	C 0	SE 6	S 7
5	63.7	63.3	65.0	64.0	9.4	13.8	10.0	10.8	15.1	6.7	92	57	78	76	1.0	6.9	2.7	3.5	9	8	10	C 0	WSW 4	WSW 3
6	67.4	69.4	72.3	69.7	7.7	11.2	8.1	8.8	11.4	7.3	87	66	83	79	1.3	4.5	1.8	2.5	10 •	9	10	WNW 7	NW 5	WNW 3
7	75.0	74.3	73.1	74.1	6.9	10.2	9.0	8.8	12.4	6.4	80	72	73	75	2.0	3.4	3.1	2.8	9	9 •	9 •	W 3	ENE 3	WSW 1
8	70.6	73.5	77.4	73.8	10.0	10.7	9.7	10.0	11.3	6.5	82	84	88	85	2.2	2.1	1.4	1.9	10 •	10	10 •	WSW 1	W 7	WSW 3
9	73.0	68.8	66.3	69.4	10.4	15.2	8.6	10.7	15.6	6.0	91	67	70	76	1.1	5.6	3.3	3.3	10 •	10	9	SW 1	W 5	W 9
10	63.4	63.3	64.4	63.7	8.5	7.9	6.0	7.1	10.0	5.7	69	72	89	77	3.5	2.9	1.1	2.5	9	9	10 •	W 8	W 8	W 7
11	64.3	70.1	77.3	70.6	6.1	6.2	7.3	6.7	7.8	5.3	91	89	86	89	0.8	1.0	1.5	1.1	10 •	10 •	8	NW 7	NW 8	NNW 3
12	82.3	83.9	83.4	83.2	5.5	9.0	9.5	8.4	13.7	4.9	94	83	83	87	0.5	2.0	2.1	1.5	10	10	8	WNW 4	NW 1	WNW 2
13	83.1	82.3	80.9	82.1	7.3	14.6	9.8	10.4	15.9	4.6	94	58	88	80	0.6	7.0	1.4	3.0	5	5	10	C 0	NW 3	SE 1
14	77.6	75.6	73.3	75.5	9.5	14.7	12.4	12.2	17.5	7.7	96	73	87	85	0.5	4.5	1.9	2.3	10	9	9	C 0	WNW 3	C 0
15	71.5	70.3	69.1	70.3	10.0	19.1	12.6	13.6	19.3	6.7	99	55	87	80	0.2	10.0	1.9	4.0	3	9	8	C 0	NE 3	SE 1
16	68.1	67.4	68.5	68.0	11.8	20.2	11.9	14.0	20.3	6.9	97	55	93	82	0.3	10.8	1.0	4.0	9	5	10	C 0	WNW 5	C 0
17	68.4	66.8	63.8	66.3	13.7	21.0	16.4	16.9	22.5	9.6	86	45	83	71	2.2	13.7	3.0	6.3	6	6	9	C 0	WSW 4	C 0
18	65.2	66.6	65.5	65.8	16.5	16.8	13.2	14.9	19.3	12.8	74	70	84	76	5.0	5.7	2.5	4.4	9	10	10	WSW 4	WNW 3	ENE 1
19	62.2	61.5	72.4	65.4	11.0	10.9	4.8	7.9	13.4	4.6	96	95	94	95	0.5	0.6	0.6	0.6	10	10 •	10	SE 2	NW 3	WSW 3
20	77.5	79.1	82.3	79.6	4.6	8.0	2.6	4.4	9.7	1.2	81	60	91	77	1.7	4.2	0.7	2.2	9	7	0	W 4	W 6	SE 1
21	86.4	86.7	87.0	86.7	4.2	9.7	5.3	6.1	11.6	-1.2	85	47	84	72	1.2	6.3	1.4	3.0	4	8	2	C 0	NW 3	SE 1
22	86.0	83.2	80.5	83.2	5.7	13.3	10.5	10.0	14.5	-1.9	82	45	62	63	1.7	8.5	4.9	5.0	1	7	7	C 0	ESE 7	ESE 2
23	77.8	77.3	75.4	76.8	7.7	8.6	9.2	8.7	10.6	7.1	76	88	96	87	2.5	1.4	0.4	1.4	10	10 •	10 •	ESE 2	SE 2	ESE 4
24	74.6	74.2	75.4	74.7	10.6	13.2	10.6	11.2	14.2	8.9	95	90	99	95	0.7	1.6	0.2	0.8	9	10	9	SE 1	NW 2	C 0
25	75.8	77.5	78.5	77.3	10.8	10.3	9.8	10.2	11.4	9.6	97	96	97	97	0.4	0.5	0.3	0.4	10	10 •	10	WNW 3	WNW 3	C 0
26	77.8	77.2	76.7	77.2	9.4	12.0	8.3	9.5	13.6	6.9	96	79	93	89	0.5	3.0	0.8	1.4	10	9 • R	5	SE 2	W 4	SW 1
27	73.9	73.7	72.9	73.5	9.0	12.6	9.3	10.0	13.0	5.6	93	76	93	87	0.8	3.6	0.8	1.7	9	9	8	C 0	NNE 1	ESE 1
28	71.5	70.0	68.5	70.0	8.5	13.1	11.2	11.0	13.2	3.9	97	76	92	88	0.3	3.6	1.0	1.6	5	10	10 •	C 0	ENE 3	NE 3
29	64.8	64.7	67.9	65.8	10.1	10.7	9.9	10.2	12.0	9.7	93	95	91	93	0.8	0.7	1.1	0.9	10 •	10 •	10 •	NE 4	N 4	NE 4
30	70.3	70.1	69.1	69.8	5.5	11.0	6.5	7.4	12.9	2.7	75	51	84	70	2.2	6.4	1.6	3.4	3	5	1	WNW 2	NW 3	NE 2
31	67.8	67.6	66.1	67.2	7.2	13.0	12.1	11.1	15.3	0.8	81	68	77	75	2.0	4.8	3.2	3.3	2	10	9	C 0	ENE 3	E 4
M	73.2	73.0	73.2	73.1	8.3	12.5	9.1	9.7	13.9	4.4	85	67	84	79	1.6	5.2	1.9	2.9	7.2	8.0	7.7	1.9	3.9	2.4

Czerwiec – Juin

1	60.8	64.1	68.5	64.5	10.6	9.1	8.9	9.4	12.0	8.7	96	96	86	93	0.5	0.5	1.5	0.8	10 •	10 •	10	C 0	W 3	W 3
2	72.7	75.6	76.7	75.0	6.8	13.2	7.8	8.9	15.2	6.4	93	54	84	77	0.8	7.1	1.7	3.2	10 •	8	3	W 6	WSW 6	SE 1
3	77.9	76.7	76.5	77.0	8.2	18.6	14.9	14.2	19.3	1.2	85	39	50	58	1.7	15.1	8.4	7.7	2	5	6	C 0	E 1	E 4
4	76.3	75.3	74.6	75.4	9.9	16.3	11.6	12.4	16.5	6.5	91	63	87	80	1.1	6.9	1.8	3.3	10	10	10 •	C 0	ESE 4	E 4
5	70.9	68.9	67.5	69.1	11.5	12.3	12.6	12.2	12.8	11.2	91	96	96	94	1.2	0.3	0.5	0.7	10 •	10 •	10 •	E 2	C 0	C 0
6	66.1	67.1	68.9	67.4	11.4	12.3	10.9	11.4	13.4	10.1	96	92	99	96	0.5	1.2	0.1	0.6	10 •	10 •	6	NE 3	NE 2	C 0
7	71.2	70.3	70.1	70.5	9.3	17.5	11.2	12.3	18.5	6.3	99	59	90	83	0.1	8.2	1.3	3.2	8 ≡	8	5	C 0	E 3	SE 2
8	68.7	67.6	66.6	67.6	14.7	19.8	14.2	15.7	21.1	8.0	67	59	92	73	5.5	9.5	1.3	5.4	8	8 •	10	E 4	SSE 6	E 3
9	66.0	66.0	65.2	65.7	12.9	17.2	11.5	13.3	18.5	10.7	84	71	96	84	2.4	5.6	0.5	2.8	10 •	9	10	NE 3	NE 5	C 0
10	67.0	67.9	69.7	68.2	12.9	16.9	12.1	13.5	18.2	9.9	83	63	94	80	2.7	7.2	0.8	3.6	7	7	9 •	ENE 2	N 1	NW 2
11	68.9	68.7	71.8	69.8	13.2	15.3	12.8	13.5	17.0	10.1	92	84	96	91	1.3	2.8	0.5	1.5	8	9 •	10 •	WNW 5	NW 5	NW 3
12	75.2	76.5	77.4	76.4	8.6	11.6	10.2	10.2	13.0	8.2	93	78	77	83	0.8	2.9	2.8	2.2	10 •	10	9	NW 5	WNW 5	WSW 3
13	76.1	75.6	75.3	75.7	10.7	12.8	10.3	11.0	14.7	3.3	91	87	99	92	1.2	1.9	0.1	1.1	9	10	9 •	C 0	C 0	C 0
14	76.7	77.7	78.8	77.7	10.5	16.9	13.5	13.6	17.8	9.6	94	70	86	83	0.8	5.7	2.1	2.9	10	8	10	W 2	NW 3	WNW 3
15	78.8	77.4	76.3	77.3	11.2	20.4	12.8	14.3	21.1	8.0	96	58	92	82	0.3	10.1	1.2	3.9	5	6	1	C 0	NE 3	SE 1
16	74.8	72.8	68.5	72.0	15.8	23.9	17.6	18.7	24.6	7.5	82	45	55	61	3.2	16.1	9.0	9.4	1	5	3	C 0	E 2	SE 3
17	62.2	65.4	70.3	65.3	17.7	16.1	11.2	14.0	18.4	11.0	68	74	83	75	6.4	4.7	2.3	4.5	9	10 •	9	SW 4	SW 4	W 9
18	73.4	73.1	74.2	74.9	12.6	18.0	16.7	16.0	19.1	9.8	69	46	67	61	4.6	11.0	6.2	7.3	2	8	10	WNW 5	WSW 6	W 6
19	73.5	74.8	78.8	75.7	16.1	18.3	14.2	15.7	20.1	13.0	73	56	65	65	4.9	9.2	5.6	6.6	10 •	6	0	W 7	W 3	W 3
20	81.1	80.0	80.0	80.4	14.3	19.2	14.1	15.4	20.4	8.5	73	49	83	69	4.1	11.3	2.7	6.0	3	3	8	C 0	WNW 7	C 0
21	79.9	77.8	74.7	77.3	12.9	22.3	13.8	16.7	24.1	6.7	86	46	86	73	2.1	14.5	2.4	6.3	8	9	1	C 0	NE 2	C 0
22	70.9	70.8	68.6	69.9	17.9	26.4	19.3	20.8	27.3	8.6	84	49	86	73	3.2	17.4	3.3	8.0	3	8	9	C 0	WSW 6	C 0
23	72.2	73.8	75.8	73.9	17.6	19.2	13.7	16.0	21.0	12.9	73	69	94	77	3.3	7.7	0.9	4.7	8	9	1	W 4	NW 2	C 0
24	77.0	77.2	78.9	77.7	14.4	23.8	16.1	17.6	24.2	8.2	90	47	86	74	1.6	15.3	2.3	6.3	3	7	7	SSE 1	W 4	C 0
25	79.9	79.3	77.7	79.0	15.6	24.6	19.6	19.8	26.9	8.6	83	54	78	72	3.0	14.3	5.1	7.3	0	8	0	C 0	WNW 2	SE 1
26	76.4	77.3	79.7	77.9	19.9	24.4	20.0	21.1	31.3	11.0	81	56	89	73	4.3	13.6	2.7	6.9	0	9 (R)	10 • R	C 0	W 7	C 0
27	79.8	79.4	81.4	80.2	18.9	21.4	15.6	17.9	23.0	14.4	77	80	89	82	4.9	5.0	1.9	3.9	7	9	10	E 2	NW 3	C 0
28	84.7	85.5	84.5	84.9	15.0	16.5	12.7	13.7	17.5	12.4	80	52	76	69	3.0	9.0	3.6	5.2	8	6	0	NW 2	WNW 3	C 0
29	81.7	81.9	81.9	81.8	13.0	18.8	12.9	14.4	19.3	5.4	81	66	91	79	2.8	7.3	1.4	3.8	0	10	0	C 0	W 4	C 0
30	81.0	77.7	72.5	77.1	14.1	23.3	18.0	18.4	25.9	5.8	82	45	78	68	2.9	15.8	4.4	7.7	0	1	1	C 0	C 0	C 0
31																								
M	74.1	74.1	74.4	74.2	13.2	18.2	13.8	14.8	19.7	8.7	84	63	84	77	2.6	8.5	2.6	4.6	6.3	7.9	6.2	1.9	3.5	1.8

Jelenia Góra $H_G = 342\,m$ $H_b = 343{,}9\,m$ $h_w = 16\,m$ Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	.	= 0^00–9^15
2	8	.	.	⌴ 0 3–7
3	9	.	.	= 3^00–4^40; ⌴ 1 2–6
4	8	2.7	.	● 0 18^40 19^15 22^50 23^10–24; ⌴ 0 2–6
5	8	2.3	.	● 0 0^00–3^45 ⚉ 0 8^45–9^40, 10^49–11^10 ● 0 23^25–45, = 0^00–3^45
6	7	0.0	.	● 0 1^15–2^20, 4^20 7^25 ▽ ⚉ 0 9^30–10^05; = 1^20–12^20, 18^40–24
7	7	1.9	.	▽ ⚉ 0 11^34–42 ⚉ 0 ⚉ 0–11^47 ⚉ 0–11^55 12^42–13^03 17^40–50 19^50 20^10 20^45–21^05; = 0^00–7^25 22^20–24
8	6	6.7	.	● 0 3^15...45, 4^10 7^15–9^30 11^10 ▽ ⚉ 0 14^10–16 14^22–15^05 ⚉ 1–15^40 ⚉ 0–16^10, 20^35–21^12; = 0^00–3^10, 9^45–24
9	8	3.2	.	● 0 1^15 6^10–9^40 ⚉ 0 11^50–12^15 13^49 17^18 ⚉ 1–17^45 ⚉ 0–18^46 19^20–37 ⚟ 0 17^30–18^36 SW-E (⚟)0–19^15; = 0^00–2^20
10	8	18.8	.	⚉ 0 1^10–35 3^30–45 7^45–8^50 ⚉ 1–9^00 ⚉ 0–9^05 10^35–40 ⚉ 1 12^16–20 14^18–25 ⚉ 0–15^20 ⚉ 1–15^30 ⚉ 0–17^30, 17^50–18^30 19^15–20^00 ⚉ 1–21^10 ● 0 23^00–24, por wiatru do 15 m/sek, 14^40 8^15;
11	4	6.9	.	● 0 0^00–4^20 ▽ ⚉ 0 5^05–6^52 ⚉ 1–7^15 ● 0–10^25 ● 0 10^34–42, 11^30–50, 12^40 13^20, 13^35–14^15, 14^20–35, 14^45–15^38, por wiatru do 14 m/sek 2^30 3^10, = 0^00–24 10.V. 11^15–25 12^20–40 14^18–35 15^22–35, = 16^10–24
12	7	0.0	.	⚉ 0 18^13–20, = 0^00–9^45 21^15–24
13	7	2.4	.	⚉ 0 0^47–50 1^26–31, = 0^00–9^20, 20^40–24; ⌓ 0 2–4 ⌓ 1–6 ⌓ 2–9 ⌓ 1 19–24
14	6	0.0	.	● 0 2^40...3^15–5^45 ⚉ 0 9^40–10^05, 18^35–39; = 0^00–24; ⌓ 0 0^00–2^40
15	6	4.1	.	⚉ 0 16^20–38; = 0^00–10 = = –1^30 = 2^20 = = –5^30 = –9^30 ∞ –16^20 = 16^40–24; ⌓ 1 2–9
16	7	0.2	.	● 0 0^15–2^20 ⚉ 1 3^40–4^15 ⚉ 0 15^35–47 ● 0 17^40–18^10, = 0^00–4^30 = 0–6^40 = –12^45
17	8	0.5	.	⚉ 0 19^47–20^20 ⚉ 1–20^15 ⚉ 0–20^30, ⚟ 0 20^05–40 ⌓ 1 1–9
18	8	4.5	.	▽ ⚉ 0 13^20–30 ● 0 14^48 17^45 19^20...20^10; = 1^45–22^30
19	6	3.7	.	⚉ 0 0^45–1^10, 3^15–35 ● 0 5^10–6^50 ⚉ 0 8^40–9^15 ⚉ 1–10^10 ⚉ 0–10^45 ⚉ 1–13^30 ⚉ 2–14^10 ⚉ 1–14^40 ⚉ 0–15^40 ⚉ 1–16^30 ⚉ 0–17^15 ● 0 17^35 19^20, 23^15–24, = 0^00–24
20	8	0.0	.	● 0 0^00...2^45 ⚉ 0 13^45–38; = 0^00–7^30
21	8	0.0	.	= 2^20–7^35, 21^40–24; ⌴ 3 2–7 ⌓ 0 22–24
22	7	.	.	= 0^00–2^35 = = 0–2^50 = = 1–3^30 = = 2–4^45 = = 1–5^40, ⌓ 1 0^00–2 ⌴ 0–4 ⌴ 1–6
23	6	4.7	.	● 0 10^35–13^25 ● 1–14^20 ● 0–22^25 ● 0–24; = 11^20–24
24	6	19.3	.	● 0 0^00–4^40 ● 0 5^15...6^20 ⚉ 0 11^43–12^10, 13^36–16^16 ● 1–16^40 ● 0–17^10, ⚟ 0 13^15–16^10, = 0^00–24
25	5	8.4	.	● 1 3^05–6^30 ● 0–7^25 ● 1–11^20 ● 0–13^25 ● 0–14^40; = 0^00–24
26	6	4.7	.	⚉ 1 7^36–50 ⚉ 0 9^35 10^10 11^10–15 12^50 13^10 ⚉ 1 14^03–12 ⚉ 0–14^20 14^52 15^05, 15^45–50 ⚉ 1–15^55 ⚉ 0–16^35, ⚟ 0 13^01–17^00 S-W-E; = 0^00–10^15 12^50 13^40 14^45 15^20, 16^30–19^10, 21^15–24
27	7	.	.	= 0^00–3^00, 17^50–21^20 = = –24, ⌓ 2 21–24
28	6	15.3	.	● 0 13^40–21^15 24 = = 0^00–4^5 = = 1–1^35 = = 2–4^20 = = 1–4^45 = = 0–6^40 = –24; ⌓ 0 0^00–8
29	5	39.2	.	● 0 0^00...2^10–4^05 ● 1–20^20 ● 0–21^30; = 0^00–24
30	8	.	.	= 0^00–4^5, ⌓ 1 22–24
31	8	6.8	.	● 0 11^50...12^20, 21^50...23^10–24; = 1^40–3^00 = = –4^20 = –5^00, 19^40–24; ⌓ 1 0^00–3 ⌴ 0–6
Σ	–	184.3	–	

Czerwiec - Juin

1	5	4.5	.	● 0 0^00–13^40 22^40–24; = 0^00–18^30 23^40–24
2	8	0.5	.	● 0 0^00...15–40 ● 1–1^15 ● 0...5^20–8^40...9^25; = 0^00–9^30, 21^30–24, ⌓ 0 20–24
3	8	.	.	= 0^00–6^45 22^20–24; ⌓ 0 0^00–2 ⌓ 1–3 ⌓ 2–8
4	6	4.1	.	● 0 9^25...35, 13^50...16^05–21^45–24, = 0^00–2^10 = = –3^40 = = –12^15 ∞ –13^30 = –24, ⌓ 1 1–9^25
5	5	5.2	.	● 0 0^00...5^00–7^25 ● 1–8^05 ● 0...9^20, 10^20–18^15 ● 1–20^40 ● 0–24, = 0^00–24
6	5	1.2	.	● 0 0^00...10^15–14^15...15^40, = 0^00–18^30 = = 20^05–21^42 = = 1–23^30 = = 2–24; ⌓ 1 20^00–22^00 ⌓ 2–24
7	8	.	.	= = 2 0^00–2^20 = = 1–3^45 = = 0–4^50 = = 1–5^42 = = 0–7^02; ⌓ 2 0^00–9 ⌓ 0 21–24
8	8	2.9	.	⚉ 0 17^50–18^05 ⚉ 1 19^45–20^20 ⚉ 0–21^10, (⚟) S 19^15–⚟ 1 19^45–20^20 ⚟ 20^40, = 21^15–30 = = –23^45 = –24, ⌓ 0 0^00–6
9	8	6.4	.	● 0 6^10...10^15 ⚉ 0 18^48–19^03 ⚉ 2–19^08 ⚉ 1–19^35 ⚉ 0–19^42 ● 0 21^50–23^48, (⚟) 18^25–40 ⚟ 0–19^31 E-W, = 0^00–4^30
10	7	4.2	.	⚉ 0 14^10–30 ⚉ 1 20^15–45–21^06 ● 0 23^35...24, = 2^20–6^20
11	6	27.0	.	⚉ 0 0^00 5^00 ⚉ 0 9^52–10^10 11^00–45 ⚉ 1–2 12^00–05 ⚉ 1 12^25–40 12^50–58 ⚉ 0 13^06–15 ⚉ 2 14^35–40 ⚉ 0–15^02 ⚉ 1–2 15^55 19^45 ⚉ 0 20^00–10 ⚉ 1–2 20^50–22^00 ⚉ 0–1 23^15 ● 0...24; = 1^35–24
12	6	1.0	.	● 0 0^00...6^00 ● 0...7^15 ● 0...9^20, = 0^00–13^30 19^30–23^20 = = –24; ⌓ 1 22–24
13	5	10.0	.	● 0 8^20...9^10–10^40...11^20 ⚉ 1–0 15^27–58 ⚉ 2 16^01 ⚉ 1–16^06 ⚉ 0 16^12–20 ⚉ 1–16^45 ⚉ 0 17^42–18^15, 20^05–22^30, ⚟ 0 15^44–17^40 W-E; = = 0^00–5^35 = = –22^45 = = 0–24; ⌓ 1 0^00–8^20
14	7	0.4	.	⚉ 0 0^15–25 14^45 15^05 19^50 20^15 = = 0^00–2^30 = = –11^40 22^40–24
15	8	.	.	● 0 0^20...3^20; = 0^00–8^40...21^10–22^30 = = –24; ⌓ 0 20–24
16	7	.	.	= = 0^00–3^30 = = –4^15, ⌓ 0 0^00–1 ⌓ 2–8 ⌓ 1–9 ⌓ 2–10
17	7	1.1	.	⚉ 0 12^35 14^35 19^40–20^15 23^45–24
18	8	0.0	.	⚉ 0 0^00–10 ● 0 23^45–24
19	8	0.4	.	● 0 0^00...10 ⚉ 0 6^48 7^30 7^50–8^10 ● 0...10^02; = 22^20–24; ⌓ 0 22–24
20	8	.	.	= 0^00–4^00; ⌓ 0 0^00–8
21	7	.	.	= 1^50–2^48 = = = –5^45 = –8^40 21^30–23^45 = = 0–24; ⌓ 2 0–7 ⌓ 1–9 ⌓ 0 20–24
22	8	10.1	.	⚉ 21^05–15 ⚉ 2–21^30 ⚉ 1–21^45 ⚉ 0–22^15 22^50 23^30, ⚟ 1 21^05–23^30 W-E; = = 0^00–2^50; ⌓ 0 0^00–1 ⌓ 1–2 ⌓ 2–8
23	8	.	.	= = 20^40–21^30 = = –24; ⌓ 0 20–24
24	8	.	.	= = 0^00–1^30 = = 2–3^40 = = 0–4^15 = = –4^30 22^30–24; ⌓ 2 0–8 ⌓ 1–9 ⌓ 0–10, 20–23 ⌓ 1–24
25	8	.	.	= 0^00–5^30 22^35–24; ⌓ 1 0^00–2 ⌓ 2–8 ⌓ 0 21–23 ⌓ 2–24
26	8	3.6	.	⚉ 0 13^20–40 16^03–21 20^25–45 ⚉ 1–20^52 ⚉ 0–21^10; (⚟) 0 12^40–17^40 ⚟ 0 20^40–21^15, = = 0^00–4^30 = = –5^15, ⌓ 0 0^00–8
27	6	4.7	.	⚉ 1 7^30–35 ⚉ 2–8^07 ⚉ 1 15^15–17 ⚉ 1–18^30 ⚉ 2–19^25 ⚉ 1–19^35, = 0^00–19^30 21^30–24
28	8	.	.	= 0^00–7^30 21^30–24; ⌓ 0 20–21 ⌓ 1–23 ⌓ 2–24
29	7	.	.	= 0^00–3^50, 17^10–24; ⌓ 2 0^00–7 ⌓ 1–9 ⌓ 0 21–22 ⌓ 1–24
30	8	0.0	.	= 0^00–8^10, 21^10–24; ⌓ 0 0^00–8 ⌓ 0 22–24
31				
Σ	–	87.3	–	

Jelenia Góra — φ = 50°54' — λ = 15°48' — Lipiec – Juillet 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	71.3	74.3	74.4	73.3	17.7	13.3	13.8	14.6	18.8	13.0	89	94	91	91	2.2	0.9	1.5	1.5	10	10	10	NNW 1	NW 3	C 0
2	74.1	73.1	72.1	73.1	12.7	16.9	14.8	14.8	17.9	10.1	75	53	61	63	3.7	8.9	6.5	6.4	9	5	10	C 0	WNW 4	W 5
3	70.3	70.6	71.6	70.8	10.7	13.4	9.1	10.6	14.8	8.6	91	61	80	77	1.2	6.0	2.4	3.2	10	9	6	WNW 1	W 4	W 2
4	70.5	70.3	69.4	70.1	10.2	11.7	10.1	10.5	14.0	4.0	78	76	86	80	2.7	3.3	1.8	2.6	9	8	9	WNW 1	SSW 1	C 0
5	69.3	70.5	73.1	71.0	10.0	12.4	9.8	10.5	14.9	7.4	84	63	73	73	1.9	5.3	3.3	3.5	8	9	3	C 0	NW 3	NNW 3
6	74.3	74.0	75.2	74.5	10.7	11.2	10.7	10.8	14.6	6.3	56	83	74	71	5.7	2.3	3.4	3.8	10	10 •	3	WSW 4	WNW 6	WSW 3
7	73.6	71.5	70.1	71.7	13.3	19.5	13.6	15.0	21.5	10.3	68	49	83	67	5.0	11.5	2.7	6.4	9	9	3	SW 3	SSW 4	C 0
8	65.4	63.8	64.5	64.6	17.3	14.3	13.2	14.5	18.5	7.4	59	94	77	77	8.1	0.9	3.5	4.2	9	10 •	9	SSW 2	NNW 2	W 4
9	68.9	71.6	73.9	71.5	10.9	15.0	9.8	11.4	15.4	8.9	68	56	77	67	4.1	7.4	2.8	4.8	9	8	7	WNW 4	W 6	C 0
10	74.7	75.3	77.6	75.9	8.3	14.3	7.8	9.6	14.4	4.5	93	58	97	83	0.8	6.8	0.3	2.6	10 •	9	4	C 0	W 4	C 0
11	79.7	79.3	78.2	79.1	9.0	17.0	11.8	12.4	18.7	4.7	95	57	90	81	0.7	8.3	1.3	3.4	9	8	7	C 0	W 5	C 0
12	75.9	74.2	74.5	74.9	16.8	18.9	15.7	16.8	19.5	10.6	84	67	95	82	3.1	7.3	0.9	3.8	8	9	9	SW 3	SW 5	C 0
13	75.8	75.1	74.8	75.2	15.7	22.6	18.4	18.8	26.1	13.3	95	57	88	80	0.9	11.7	2.5	5.0	9	5	3	C 0	W 2	SSW 1
14	75.8	75.8	75.8	75.8	18.8	29.0	20.9	22.4	29.9	11.7	85	40	73	66	3.3	24.0	6.6	11.3	3	4	2	C 0	NE 1	C 0
15	78.4	77.7	77.5	77.9	19.4	23.8	18.8	20.2	25.4	13.7	76	68	92	79	5.4	9.6	1.7	5.6	9	9	9	C 0	N 1	C 0
16	75.4	75.3	74.8	75.2	17.8	17.4	17.2	17.4	23.1	13.0	90	90	97	92	2.0	2.1	0.6	1.6	6	9 (K)	9	C 0	SE 1	C 0
17	73.8	72.9	72.7	73.1	16.4	19.4	17.0	17.4	22.0	14.7	99	87	98	95	0.2	3.0	0.4	1.2	10 •	9 • K	10	C 0	NW 2	C 0
18	73.4	75.7	78.1	75.7	15.8	14.4	14.6	14.8	17.1	14.1	98	93	95	95	0.3	1.1	0.7	0.7	10 •	10 •	10	C 0	NW 2	NE 1
19	78.7	78.9	78.5	78.7	14.6	19.1	16.5	16.7	21.1	13.3	95	77	92	88	0.7	5.0	1.6	2.4	9	9	8	NW 1	E 2	C 0
20	77.5	75.7	72.9	75.4	15.7	22.0	17.0	17.9	22.6	13.8	82	72	90	81	3.2	7.5	2.0	4.2	8	7	1	E 1	E 3	ESE 1
21	69.9	68.5	69.9	69.4	18.5	21.4	15.6	17.8	22.4	14.4	83	70	98	84	3.5	7.6	0.4	3.8	8	9	10	ESE 2	SW 1	SE 1
22	71.6	71.3	69.2	70.7	14.1	21.6	15.4	16.6	22.9	9.2	92	51	89	77	1.3	12.7	1.9	5.3	1	7	8	C 0	WSW 2	C 0
23	67.9	69.7	69.3	69.0	14.0	18.3	12.9	14.5	21.2	10.4	97	78	89	88	0.6	4.6	1.6	2.3	10 • K	6	0	WNW 2	WSW 2	S 1
24	69.3	70.9	73.1	71.1	17.4	22.1	12.3	16.0	23.3	9.7	71	34	88	64	5.9	17.4	1.7	8.3	9	4	1	SSW 3	WSW 6	SSE 1
25	73.4	72.3	70.7	72.1	12.9	20.9	14.4	15.6	23.4	6.0	83	56	95	78	2.7	10.8	0.7	4.7	7	10	2	C 0	W 4	C 0
26	73.5	71.6	71.8	72.3	13.6	20.0	15.9	16.4	21.1	7.6	84	45	59	63	2.5	12.9	7.5	7.6	4	6	9 •	C 0	SW 3	WSW 2
27	73.4	73.4	74.7	73.8	10.6	15.7	11.0	12.1	17.0	8.8	84	60	91	78	2.1	7.1	1.1	3.4	10	9	10 •	WNW 3	NW 4	C 0
28	75.4	75.3	72.7	74.5	12.2	14.3	14.2	13.7	16.1	10.4	74	71	66	70	3.7	4.8	5.4	4.6	10	10 •	9	WNW 3	WSW 3	WSW 5
29	69.1	66.7	63.3	66.4	13.9	20.3	15.5	16.3	20.7	11.7	84	56	72	71	2.5	10.6	5.0	6.0	9	7	10	S 1	WSW 4	SSW 5
30	60.2	60.5	63.8	61.5	15.3	19.2	11.3	14.3	19.5	10.6	68	47	93	69	5.7	11.8	1.0	6.2	8	7	8	WSW 8	WSW 4	C 0
31	62.8	60.3	68.5	63.9	14.4	16.4	9.2	12.3	19.5	7.9	73	79	93	82	4.4	3.8	0.8	3.0	9	8 •	9	SW 3	WSW 2	WNW 2
M	72.4	72.1	72.5	72.3	14.2	17.9	13.8	14.9	19.9	10.0	82	66	85	78	2.9	7.6	2.4	4.3	8.4	8.0	6.7	1.5	3.1	1.2

Sierpień – Août

1	70.7	70.8	70.1	70.5	8.9	16.0	13.1	12.8	17.3	4.4	93	59	83	78	0.8	7.5	2.6	3.6	4	8	10	C 0	SE 1	C 0
2	69.6	70.6	71.5	70.6	9.1	16.7	8.6	10.8	17.6	6.8	97	51	93	80	0.4	9.2	0.8	3.5	3	8	0	C 0	NW 4	C 0
3	69.2	69.4	71.3	70.0	10.0	16.0	12.2	12.6	17.4	4.4	91	51	83	75	1.1	8.9	2.4	4.1	4	9	8	C 0	SSW 2	C 0
4	74.8	75.8	78.3	76.3	13.7	17.8	11.8	13.8	19.0	11.3	82	55	94	77	2.9	9.2	0.8	4.3	10	9	2	NW 3	NW 10	C 0
5	80.4	80.5	79.5	80.1	11.3	21.7	15.0	15.8	23.6	7.3	96	52	91	80	0.5	12.6	1.5	4.9	1	7	0	C 0	W 2	C 0
6	76.8	75.3	76.2	76.1	17.3	29.2	17.1	20.2	29.5	9.7	85	35	99	73	2.9	26.4	0.2	9.8	9	2	5	C 0	W 3	C 0
7	74.2	73.5	74.4	74.0	20.2	29.0	21.7	23.2	30.7	15.5	85	49	74	69	3.5	20.3	6.8	10.2	3	3	3	SSW 1	C 0	C 0
8	74.2	74.5	77.8	75.5	18.9	24.9	17.5	19.7	25.3	15.1	80	65	71	72	4.3	11.1	5.9	7.1	4	8	9	E 2	NW 3	WNW 3
9	79.9	80.0	81.0	80.3	10.8	12.6	10.1	10.9	17.8	9.7	97	88	99	95	0.4	1.7	0.2	0.8	10 •	10	6 ≡	W 2	SW 1	C 0
10	81.7	81.5	81.9	81.7	7.8	15.9	12.4	12.1	16.7	6.7	100	61	96	86	0.0	7.0	0.5	2.5	0 ≡	9	10	C 0	E 2	C 0
11	82.5	83.0	83.8	83.1	9.3	16.2	11.6	12.2	17.3	7.3	99	51	84	78	0.1	9.1	2.1	3.8	6	8	9	C 0	WNW 2	WNW 2
12	83.8	83.4	82.6	83.3	9.7	16.8	13.2	13.2	18.1	3.9	93	53	84	77	0.8	9.1	2.5	4.1	2	7	7	C 0	WNW 3	N 1
13	82.6	82.6	81.3	82.2	9.5	17.2	11.5	12.4	18.1	5.0	96	50	82	76	0.5	9.7	2.5	4.2	9	3	4	C 0	C 0	C 0
14	81.1	80.1	79.3	80.2	6.9	17.2	12.4	12.2	18.4	3.3	96	53	87	79	0.4	9.2	1.9	3.8	0	9	10	C 0	NW 1	C 0
15	81.0	80.9	80.7	80.9	9.3	15.8	10.6	11.6	17.8	4.1	93	58	91	81	0.8	7.4	1.2	3.1	0	9	8	C 0	NNE 2	C 0
16	80.1	79.2	78.0	79.1	7.0	17.3	11.8	12.0	18.7	2.3	93	53	89	78	0.7	9.3	1.3	3.8	1	9	8	C 0	NE 2	C 0
17	77.1	76.6	76.7	76.8	11.1	21.2	11.9	14.0	21.3	8.7	94	47	94	78	0.8	13.3	0.8	5.0	9	7	7	C 0	C 0	C 0
18	78.0	78.4	79.9	78.8	10.9	22.6	12.8	14.8	23.4	6.9	94	42	91	76	0.8	16.0	1.4	6.1	7	8	0	C 0	W 1	C 0
19	82.5	82.9	83.0	82.8	9.9	24.6	15.0	16.1	25.4	6.4	97	42	86	75	0.3	18.0	2.4	6.9	1	5	0	C 0	NE 1	C 0
20	81.8	79.4	77.3	79.5	11.4	25.9	14.2	16.4	26.9	7.7	93	41	86	74	0.7	19.7	2.4	7.6	0	5	0	C 0	SW 2	ENE 1
21	73.1	73.2	70.0	72.8	13.9	23.6	19.6	19.2	25.6	8.6	92	59	67	73	1.3	11.9	7.3	6.9	9	3	0	C 0	C 0	SE 3
22	66.0	63.5	61.5	63.7	20.9	26.3	22.0	22.8	27.0	17.1	56	39	33	49	10.3	20.8	12.4	14.7	6	3	0	SE 5	SE 6	SE 8
23	63.1	63.4	67.0	64.5	15.1	25.8	13.7	18.1	26.8	14.3	92	47	100	80	1.4	17.5	0.0	6.3	4	9	10 •	C 0	SE 3	W 1
24	68.3	69.1	67.9	68.4	14.6	17.0	14.3	15.0	17.3	14.1	98	88	100	93	0.4	2.4	0.0	0.9	10 •	10	10 •	C 0	C 0	C 0
25	67.5	68.7	72.0	69.4	13.9	14.1	13.1	13.6	14.4	11.8	100	95	89	85	0.0	0.7	1.6	0.8	10 •	10 •	10	WNW 2	C 0	W 3
26	73.8	73.3	73.3	73.5	9.7	14.7	8.4	10.3	15.3	8.2	88	33	96	79	1.4	7.8	0.4	3.2	10	9	0	WNW 2	W 3	C 0
27	73.9	72.5	73.1	73.2	7.2	15.1	8.5	9.8	16.8	4.9	100	56	94	83	0.0	7.7	0.6	2.5	10	8	2	C 0	NW 3	C 0
28	74.4	76.1	77.3	76.0	9.3	13.7	9.1	10.3	15.6	6.7	96	64	92	84	0.3	5.7	1.0	2.4	9 •	9	4	C 0	NW 2	C 0
29	75.4	73.4	74.4	74.4	6.0	17.0	12.9	12.2	18.2	3.4	95	48	91	78	0.3	10.0	1.4	4.0	4	10	8	C 0	WSW 3	WNW 2
30	73.7	73.7	77.3	76.2	9.3	15.2	7.9	10.1	16.6	6.3	100	54	95	82	0.0	8.0	0.7	2.9	7	8	0	C 0	WNW 1	C 0
31	76.1	72.8	70.4	73.1	4.9	17.2	14.2	12.6	18.3	2.1	98	49	72	73	0.2	10.0	4.6	4.9	0	9	10	C 0	ESE 1	C 0
M	75.[illegible]	75.6	75.8	75.8	11.2	19.2	13.2	14.2	20.4	7.9	93	55	87	78	1.3	10.9	2.3	4.8	5.2	7.5	5.2	0.5	2.1	[illegible].8

Jelenia Góra $H_s = 342\,m$ $H_b = 343.9\,m$ $h_w = 16\,m$ Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	0.6	•	●°4^05...15, 8^50...11^45 ●●°-12^30 ▽°14^35-40; = 0^00-3^20, 9^30-24; ⌒°0^00-4^05
2	8	0.0	•	= 0^00-2^20
3	7	0.0	•	●°5^10...7^15; = 2^30-11^25; ⌒¹22-24
4	5	1.6	•	▽°10^14-26 ▽¹11^02-30 ▽°-11^59; = 1^10-13^20, 21^30-24; ⌒¹0^00-8
5	7	0.2	•	▽°14^45-55 15^25-30 16^05-15; = 0^00-7^30; ⌒°1-9
6	7	0.2	•	●°7^45...8^10 ▽°12^25-13^10, 15^15-40
7	7	•	•	
8	6	11.8	•	●°7^48...8^10 11^54...12^00 ●¹-15^20 ●°...15^40 ▽°18^03-10 ▽¹-18^35 ▽°-18^45; = 12^40-15^40; ⌒°1-7; ⌒ 18^43-50
9	8	0.3	•	●°0^35...1^25 ▽°18^38-46; = 0^10-3^00
10	7	8.8	•	▽°6^28-7^45 13^15-25 14^55-15^05, 16^25-35 17^50-18^10 ▽¹-18^35 ▽°-18^40 ▽-18^45 ▽°0^25-0^50, 23^20; K°1^55-18^20-18^45 W-E; = 7^45-9^30 = = -24; ⌒°3-7; ⌒¹18^35-45
11	8	0.3	•	= = 0^00-1^40 = -7^15; ⌒°22^00-24
12	8	2.1	•	●°5^05...50 10^23-40, 21^40-22^05...23^35; ⌒°0^00-5^05
13	8	•	•	●°0^10...3^48; = 22^30-24
14	8	•	•	= 0^00-4^20; ⌒¹1-5 ⌒°-8
15	8	0.2	•	▽°13^25-58, K°13^34-17^30 S-E (K) 19^05-23^15
16	7	2.5	•	▽°12^14-25 ▽¹...12^34 ▽²-12^38 ▽°-12^42, (K) 9^48 NE K°11^24-12^40 SE-N (K)°14^30; = 0^35-3^10 = = -6^15 = -8^35, 19^30-24; ⌒¹1-8, 23-24
17	6	12.5	•	●°0^10...2^10 4^25-5^30 ●°-7^15 ●9^05-15 ▽°12^28-13^03 13^15-40, 17^50-18^05 ▽¹19^27-32 ▽°-20^00 ▽¹-20^15 ▽°-20^35 ▽¹21^52-22^00 ▽²-22^15 ▽°-22^40 ●°23^10-24; K°11^26-13^00 NW-SW; = 0^00-15^00, 17^40-24;
18	5	2.4	•	●°0^00-20...1^00, 3^50-4^05 ●¹-4^40 ●°0^00 ●°...9^45 ●●°10^30 ●°...11^20 ●●¹-12^15 ●°...14^40-15^30...18^35 ●°-19^25; = 0^00-24 [7.VII: ⌒°0^00-10]
19	8	•	•	= 0^00-9^30 20^40-24; ⌒¹4-5 ⌒²-7 ⌒¹21-23 ⌒²-24
20	7	0.0	•	▽°11^44-15^05, 15^50-16^05 18^45-19^10, K 14^35-16^25 S,E; = 0^00-7^20, 10^40-11^30 ∞ 13^10-20^00 = -24; ⌒²0^00-7 ⌒°20-24
21	6	5.1	•	▽°13^50-15^25 ▽¹16^10-35 ▽-17^05; (K) S 24^3-5^30, 13^32-15^10; = 0^00-13^20, 20^40-24
22	8	4.9	•	= 0^00-3^40 = °-5^35
23	7	2.1	•	▽°5^50-6^00 ▽¹-6^15 ▽°-6^45 ▽¹-7^01 ▽°7^06-30 ▽¹-7^40 ▽°-8^25, 10^36-11^10, 11^52-12^05; K°5^40-7^30 SW-NE; = 1^30-11^30; ⌒¹2-6, 22-24
24	8	•	•	▽°5^10-20 ▽°-5^25; ⌒¹0^00-4 ⌒°22-24; ⌒ 6^45-55
25	8	0.5	•	▽°17^40-18^03 18^22-28, 21^30-42; K°21^25-40 W-E; = 2^40-4^20 = 20^40-21^45; ⌒¹0^00-1 ⌒²-6 ⌒¹-8, 20-21 ⌒²-21^30
26	8	0.2	•	▽°20^48-58; = 1^20-5^25 23^40-24
27	7	2.6	•	●°5^20-30 ▽¹16^19-31 ●°16^35-17^15 ▽°20^20-34 ●°20^50-21^30, 22^15-23^10; = 0^00-2^00 = 16^30-17^30, 22^15-24 ⌒°1-3
28	7	0.2	•	▽°7^10-14 ●°9^25-10^15, 11^40-13^15; = 0^00-6^30
29	8	•	•	⟫ 23^30-24
30	8	1.1	•	▽°4^10-14 ▽¹14^16-25 ▽°17^55-18^05 ▽¹-18^10; K°17^56-18^30 SW-NE; ⟫ 0^00-3^30; = 22^35-24
31	7	15.9	•	▽°12^30-37, 12^52-13^03 ▽¹-21^47-14^04 ▽°-14^27-36, 15^01-05 ▽¹▲²-15^08 ▽¹15^12-16 ▽°16^17-20 ▽¹17^55-18^01 ▽²-18^05 ▽°-18^13 ●18^04-45...19^20, (K) NW 13^27 K°13^54-16^10 (K) 16^40 SE; = 0^00-3^40, 18^45-24
Σ	-	74.1	-	

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1	8	•	•	= 0^00-3^30 = = -4^20 = -4^40; ⌒¹2-4 ⌒²-8 ⌒¹-10 ⌒°-12, 22-24
2	7	0.0	•	▽°14^16-20; = 3^30-9^25 20^30-24; ⌒°0^00-2 ⌒¹-9, 21-24
3	8	0.0	•	= 0^00-7^30; ⌒²0^00-7
4	7	0.0	•	●°3^10-30 ▽°13^50-14^10 16^15-30; ⟫ 11^30-14^15; = 6^30-7^45, 19^45-24; ⌒°19-22 ⌒¹-24
5	7	•	•	= 0^00-9^30, 20^40-24; ⌒¹0^00-2 ⌒²-8 ⌒¹21-23 ⌒²-24
6	8	5.3	•	▽°17^19-35 ▽¹-17^47 ▽°17^53-18^18, 22^47-23^05, 23^50-24; (K) W 16^34 K°16^57-18^20 (K) 18^20 SE; = 0^00-4^20, ⌒²0^00-7
7	8	•	•	▽°0^00-10; ⌒¹2-7 ⌒°22-24
8	8	3.9	•	⌒°0^00-8, 22-24
9	6	2.2	•	●°0^10...2^10, 4^20-5^35 ▽¹-6^10, 6^42-58 ▽°-7^10, 7^20-8^35; = 4^10-20^40 = 19^45-20^40 = ¹-24; ⌒°0^00-10
10	8	0.0	•	= ¹0^00-3^30 = ²-4^15 = ²-6^45 = ¹-7^45 = -9^30, 21^30-23^50 = °-24; ⌒°20-24
11	8	•	•	= °0^00-6^45 = -8^35; ⌒°0^00-1 ⌒°-9
12	8	•	•	= 3^35-4^20 = = -4^40 = -8^20; ⌒²0-7
13	9	•	•	= ¹1^45-2^40 = ¹-4^30 = °-5^15 = -7^30, 23^30-24; ⌒°20-22 ⌒¹-24
14	8	•	•	= 0^00-6^30 = 23^35-24; ⌒¹0^00-9
15	8	0.0	•	▽°15^33-39; = 0^00-2^20 = -8^30 22^15-23^20 = 23^30-24; ⌒¹0-1 ⌒²-6; ⌒¹15^35-40 NE
16	8	•	•	= 0^00-4^10 = -2^45 = °-3^40 = ¹-5^25; ⌒°1-2 ⌒²-8
17	8	•	•	= 0^00-3^30 = 21^30-24; ⌒°1-9 ⌒¹22-24
18	8	•	•	= 0^00-2^20 = = -5^15 = -8^30 19^30-24; ⌒²0^00-8 ⌒°20-24
19	7	•	•	= 0^00-10^30, 19^10-24; ⌒°0^00-2 ⌒¹-3 ⌒²-8 ⌒¹23-24
20	7	•	•	= 0^00-10 = = -1^40 = -10^25, 21^30-24; ⌒¹0^00-2 ⌒²-8
21	6	•	•	= 0^00-8^30 ∞ -14^30; ⌒¹2-8 ⌒¹-9 ⌒°-10;
22	8	•	•	⟫ 22^15-24
23	7	26.7	•	▽°0-1 14^52-15^15 ▽¹16^08-14 ▽°-16^22 ▽²-18 ▽°-16^30 16^45-17^20 ▽°17^45-18^00 ▽°-18^15 21^30 ●°23^20-24; K S 16^10-16^18 N-17^05 NE 18^22-18^40-20^25; ⟫ 0^00-1^45; = 16^30-24
24	5	41.4	•	●°0^00...2^00, 4^50-5^40-6^45 ▽¹-7^10 ▽°-8^25, 14^20-15^25 ●°15^38...17^20-19^25 ●¹-20^46 ▽²-21^05 ●¹-23^30 ●°-24; = 0^00-24
25	5	8.6	•	●°0^00-11^30, 13^50-15^15, 18^20-19^15; = 0^00-24
26	8	•	•	= 0^00-9^00, 19^10-24; ⌒°20-24
27	7	7.6	•	= 0^00-3^15 = = -6^50 = -10^20, 19^46-24; ⌒¹0^00-3 ⌒²-8 ⌒°19-20 ⌒¹-24
28	8	0.0	•	▽°1^00-2^40 ▽°4^03-40 ▽°-5^36 ▽¹-5^55 6^40-7^05 ▽°-7^15; = 0^00-9^45, 23^30-24; ⌒¹0^00-1
29	8	2.0	•	●°16^20-35, 18^20-19^20; = 0^00-2^45 = °-4^40 = -6^20 16^30-23^30 = = -24; ⌒²1-9
30	8	•	•	▽°4^20-30; = = 0^00-2^20 = -7^35 ⌒¹0^00-4^20, 20-23 ⌒²-24
31	8	0.0	•	●°22^46...24; = = 0^00-4^15 = -8^30; ⌒²0^00-9 ⌒¹-10; ⌒°-11
Σ	-	97.7	-	

Jelenia Góra — φ = 50°54' — λ = 15°48' — *Wrzesień – Septembre 1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	69.0	70.2	70.7	70.0	9.7	18.0	14.7	14.3	18.8	7.6	99	57	94	83	0.1	8.9	0.9	3.3	9	9	10 •	C 0	C 0	E 3
2	71.3	72.2	71.1	71.5	17.5	23.8	21.8	21.2	24.6	14.5	71	41	50	54	5.9	17.3	13.1	12.1	7	9	8	E 5	ESE 8	ESE 7
3	67.7	69.0	68.8	68.5	19.6	23.6	15.2	18.4	24.4	14.9	60	55	97	71	9.2	13.1	0.6	7.6	9	9	10	SSE 7	SSW 3	C 0
4	69.6	69.9	70.5	70.0	13.1	19.2	12.3	14.2	19.5	12.1	99	48	90	79	0.2	11.4	1.4	4.3	9	10	8	C 0	C 0	C 0
5	70.5	69.9	68.3	69.6	9.7	19.9	11.7	13.2	21.7	7.2	96	57	96	83	0.4	9.9	0.3	3.6	2	9	0	C 0	C 0	C 0
6	66.4	67.2	66.7	66.8	8.5	10.9	9.3	9.5	14.1	5.8	100	96	99	98	0.0	0.5	0.1	0.2	9	10 •	8	C 0	C 0	C 0
7	67.0	68.1	69.8	68.3	10.5	14.7	12.7	12.6	16.1	7.8	77	55	73	68	2.9	7.5	3.9	4.8	7	6	9	W 1	WSW 3	SW 3
8	73.5	73.6	72.2	73.1	11.8	16.7	8.9	11.6	17.5	8.5	84	50	96	77	2.1	9.6	0.5	4.1	7	8	3	C 0	WSW 3	C 0
9	70.0	72.2	71.1	71.1	12.2	20.9	13.2	14.9	21.8	5.6	87	58	98	81	1.9	10.4	0.4	4.2	6	8	2	SSE 3	NW 1	C 0
10	66.7	71.2	71.5	69.6	13.9	13.9	12.2	13.0	17.0	11.8	93	85	95	91	1.1	2.3	0.7	1.4	10	10	10	WNW 3	WNW 2	C 0
11	71.5	73.8	74.3	73.2	9.8	12.6	7.9	9.6	13.8	7.3	97	81	99	92	0.3	2.7	0.1	1.0	10 •	10	9	WNW 2	NNW 2	SE 1
12	74.1	72.9	72.0	73.0	4.4	15.7	8.7	9.4	16.8	2.8	98	49	96	81	0.2	9.1	0.4	3.2	2 ≡	6	8	C 0	W 4	C 0
13	71.7	71.7	72.0	71.8	7.3	13.8	8.5	9.5	14.2	5.2	99	65	99	88	0.1	5.6	0.2	2.0	7	9	9	SE 1	WNW 2	C 0
14	74.2	76.3	79.6	76.7	7.3	14.9	9.3	10.2	16.1	5.2	97	64	96	86	0.3	6.0	0.5	2.3	10	8	10	C 0	C 0	C 0
15	82.1	83.3	85.3	83.6	9.1	16.4	8.0	10.4	17.2	7.3	96	56	97	83	0.5	8.1	0.3	3.0	5	6	0	C 0	NW 4	C 0
16	83.6	83.9	81.9	83.8	3.9	20.5	9.8	11.0	21.2	2.5	100	49	97	82	0.0	12.4	0.3	4.2	0 ≡	0	0	C 0	SE 1	C 0
17	80.7	79.5	78.7	79.6	8.2	23.6	11.9	13.9	24.0	5.8	100	53	99	84	0.0	13.5	0.1	4.5	6	2	0	C 0	WSW 1	C 0
18	75.0	72.7	74.6	74.1	15.0	23.4	15.6	17.4	23.7	10.1	72	54	84	70	4.7	13.3	2.8	6.9	0	1	10	E 2	SE 3	C 0
19	80.0	82.8	85.9	82.9	11.7	12.5	6.9	9.5	15.6	6.4	77	65	96	79	3.1	5.0	0.4	2.8	10	9	0	WNW 2	WNW 3	C 0
20	89.6	91.5	94.4	91.8	7.4	11.5	4.4	6.9	12.2	3.9	91	69	98	86	0.9	4.3	0.2	1.8	9	9	0	WNW 3	WNW 4	C 0
21	94.5	92.9	90.3	92.6	1.8	15.6	6.2	7.4	16.3	0.8	96	52	97	82	0.3	8.6	0.3	3.1	0 ≡	9	0	C 0	ENE 2	C 0
22	87.1	83.5	80.4	83.7	1.7	19.5	7.8	9.2	21.3	0.8	100	46	99	82	0.0	12.2	0.2	4.1	0 ≡	3	0	C 0	C 0	C 0
23	77.3	75.2	73.3	75.3	2.9	20.4	10.2	10.9	22.0	1.4	98	52	96	82	0.1	11.4	0.4	4.0	0 ≡	5	0	C 0	NE 1	C 0
24	72.6	72.4	71.7	72.2	10.5	20.6	16.7	16.1	21.2	4.3	84	54	69	69	2.1	11.0	5.9	6.3	0	2	0	SE 2	SE 7	ENE 4
25	70.1	68.8	66.8	68.6	15.1	21.2	16.8	17.5	21.4	12.4	69	65	74	69	5.3	8.8	5.0	6.4	6	7	0	ESE 3	SSE 4	SE 6
26	62.0	61.6	63.0	62.2	14.9	19.3	17.4	17.2	19.8	14.4	74	58	74	69	4.3	4.3	5.1	6.3	4	5	0	SE 6	SE 6	SSE 6
27	58.8	64.6	64.4	62.6	16.4	16.5	12.9	14.7	18.6	12.3	86	62	85	78	2.7	7.2	2.3	4.1	10 •	8	2	SE 4	WNW 6	S 1
28	64.4	63.5	63.4	63.8	8.6	15.2	10.1	11.0	15.4	6.3	99	84	99	94	0.2	2.8	0.2	1.1	9	10 •	10	C 0	E 2	WNW 2
29	67.2	68.2	70.8	68.7	8.0	14.8	6.2	8.8	15.4	5.8	99	66	95	87	0.1	5.7	0.5	2.1	10	6	0	C 0	WNW 5	NE 2
30	70.9	72.1	73.9	72.3	11.7	20.2	10.1	13.0	21.0	3.3	78	53	95	75	2.9	11.2	0.7	4.9	7	6	0	SE 7	SE 3	C 0
31																								
M	73.7	73.8	73.9	73.8	10.1	17.7	11.2	12.6	18.8	7.1	89	60	91	80	1.7	8.6	1.6	4.0	6.0	7.0	4.2	1.7	2.7	1.2

Październik – Octobre

1	74.9	76.2	76.9	76.0	6.0	21.8	11.5	12.7	22.1	3.7	98	58	96	84	0.2	10.9	0.5	3.9	1	2	0	C 0	ENE 4	C 0
2	75.0	74.3	77.7	75.7	9.8	21.3	14.9	15.2	21.5	6.2	97	61	91	83	0.3	9.7	1.5	3.8	9	6	10 •	C 0	SE 5	C 0
3	80.6	81.7	82.6	81.6	9.7	16.6	10.0	11.6	17.9	8.3	99	66	97	87	0.1	6.4	0.3	2.3	6	9	7	C 0	C 0	C 0
4	82.7	82.0	82.0	82.2	5.3	17.4	8.6	10.0	17.9	4.3	98	61	100	86	0.1	7.7	0.0	2.6	0 ≡	7	0 ≡	C 0	ESE 2	C 0
5	82.7	82.9	82.9	82.8	6.4	13.1	7.6	8.7	14.7	5.9	100	74	94	89	0.0	4.0	0.6	1.5	10 ≡	1	0	C 0	E 7	ENE 3
6	81.9	81.1	79.8	80.9	1.8	14.8	5.0	6.6	16.0	1.5	100	64	100	88	0.0	6.0	0.0	2.0	0 ≡	0	0 ≡	C 0	ENE 3	C 0
7	78.9	77.7	78.0	78.2	0.3	18.1	5.6	7.4	19.8	0.2	100	54	100	85	0.0	9.5	0.0	3.2	10 ≡	2	0 ≡	C 0	C 0	C 0
8	77.0	77.7	79.8	78.2	1.3	11.3	8.6	7.4	13.7	0.7	100	93	96	96	0.0	1.0	0.5	0.5	3 ≡	10	10	C 0	WNW 3	C 0
9	79.2	79.1	79.0	79.1	7.6	9.1	6.0	7.2	10.0	5.7	97	67	94	86	0.3	3.8	0.6	1.6	10	9	9	NNW 1	E 2	C 0
10	78.2	78.7	79.3	78.7	4.7	8.7	0.7	3.7	10.0	0.4	97	63	98	86	0.2	4.1	0.1	1.5	10	6	3	WNW 2	NW 3	C 0
11	78.9	77.7	79.8	78.8	-2.7	11.2	2.8	3.5	11.4	-3.1	100	60	98	86	0.0	5.3	0.2	1.8	10 ≡	1	4	C 0	W 3	C 0
12	84.6	86.7	87.6	86.3	2.1	9.2	-0.6	2.5	10.3	-0.7	96	56	98	83	0.3	5.1	0.1	1.8	2	4	0	C 0	NNE 1	C 0
13	86.5	85.1	83.7	85.1	-5.2	14.6	1.1	2.9	15.5	-5.9	100	35	96	77	0.0	10.8	0.2	3.7	1	4	5	C 0	W 1	C 0
14	82.4	81.2	80.5	81.4	-4.0	16.1	1.4	3.7	16.8	-4.2	99	39	98	79	0.1	11.2	0.2	3.8	3	2	4	C 0	E 4	C 0
15	79.3	78.8	78.1	78.8	-3.2	18.3	10.7	9.1	19.2	-3.9	99	45	73	72	0.0	12.0	3.2	5.1	3	4	8	C 0	SW 5	SE 3
16	76.0	76.3	82.8	78.4	6.2	13.4	6.0	7.9	16.3	5.4	89	69	98	85	1.0	4.8	0.2	2.0	7	10	10	C 0	WNW 6	C 0
17	87.2	88.9	88.5	88.2	3.7	6.4	3.3	3.7	8.0	3.0	94	87	80	87	0.6	1.3	1.8	1.2	9	10	10	W 3	WNW 4	WSW 3
18	87.2	85.9	86.8	86.6	3.7	11.4	1.2	4.4	12.0	0.4	92	63	96	84	0.7	5.0	0.3	2.0	10	4	0	C 0	NW 1	C 0
19	86.7	87.7	88.6	87.7	3.2	10.3	0.3	3.3	10.6	-0.3	98	63	100	87	0.2	4.7	0.0	1.6	9	7	5	C 0	NNW 1	C 0
20	89.3	90.5	90.9	90.2	1.3	7.8	3.1	4.9	8.7	-1.2	100	65	89	85	0.0	3.7	1.0	1.6	8	4	0	C 0	SSE 2	E 2
21	91.7	91.7	92.8	92.1	-4.6	7.6	-0.7	0.4	8.0	-3.4	98	58	90	82	0.1	4.3	0.6	1.7	0 ≡	9	0	C 0	E 4	C 0
22	93.7	92.9	93.1	93.2	-6.7	10.9	-3.0	-0.4	11.1	-7.0	94	41	100	78	0.2	7.7	0.0	2.6	0	0	0	C 0	W 4	C 0
23	91.7	90.0	89.1	90.3	-5.8	11.9	-0.6	1.2	13.3	-6.3	97	41	96	78	0.1	8.2	0.2	2.8	0	6	0	C 0	C 0	C 0
24	88.6	88.5	87.8	88.3	-4.8	9.3	1.5	1.9	9.6	-3.1	95	63	96	85	0.2	4.1	0.3	1.3	3	0	0	SE 1	ENE 4	C 0
25	86.9	85.6	85.3	86.0	-3.2	12.1	-1.3	1.0	12.9	-3.2	100	57	100	86	0.0	6.0	0.0	2.0	0 ≡	0	0 ≡	C 0	S 1	C 0
26	83.6	81.1	80.6	81.8	-3.4	13.8	-1.2	1.8	13.3	-3.7	100	44	100	81	0.0	9.6	0.0	3.2	0 ≡	2	0	C 0	NW 1	C 0
27	80.0	79.3	79.2	79.6	-4.3	13.4	1.0	3.2	16.2	-4.6	98	47	98	81	0.1	9.3	0.2	3.2	0	0	0	C 0	WNW 2	C 0
28	77.1	76.1	75.7	76.3	1.6	17.4	5.9	7.7	17.8	-1.1	96	51	97	81	0.3	9.8	0.3	3.3	8	9	0	E 1	W 3	C 0
29	73.7	71.9	77.8	74.3	3.7	13.9	8.2	9.0	18.2	1.3	100	62	81	81	0.0	6.8	2.1	3.0	4	4	4	C 0	SSW 5	W 3
30	81.2	79.2	74.4	78.3	0.6	11.6	0.3	3.3	11.7	-0.7	96	42	86	73	0.3	7.8	0.8	3.0	7	4	0	C 0	WSW 6	C 0
31	72.1	72.0	72.5	72.2	8.7	11.2	7.7	8.8	11.3	0.3	69	58	57	61	3.4	3.6	4.3	4.3	10	7	9	SW 7	W 9	WSW 4
M	82.2	81.9	82.4	82.2	1.2	13.2	4.2	5.7	14.1	-0.3	97	58	93	83	0.3	6.7	0.7	2.6	5.0	4.6	3.2	0.3	3.2	0.7

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ OCU h	POGODA
1	8	5.5	•	•$^{0}0^{00}$ 1^{45} 14^{20} 19^{20}–21^{35} 24; = 4^{15}–5^{15} = = –6^{30} = –8^{20} 14^{10}–24
2	8	•	•	•$^{0}0^{00}$ 1^{35}; ≫ 10^{40}–10^{10}; = 0^{00}–5^{20}; ⊕ 12^{45}–13^{10}
3	8	3.9	•	•^{0} 18$^{25-40}$ 18^{45}–19^{40} •^{0} 23^{40}–24; ≫ 7^{45}–10^{30} (por. do 20 m/sek); = 19^{15}–24
4	8	•	•	•$^{0}0^{00}$–1^{20} 2^{45}–4^{25}; = 9^{00}–8^{40} 20^{30}–24; ⌒^{0} 20–24
5	8	•	•	= 0^{00}–6^{45} = 20^{45}–21^{30} = –24; ⌒^{0} 0^{00}–2 ⌒^{1}–3 ⌒^{2}–8 22–24
6	5	8.2	•	▽^{0} 11^{50}–12^{20} ▽^{0} 12$^{30-50}$ ▽^{1}–13^{05} ▽^{0}–13^{45} ▽^{1}–14^{10} •^{0}–16^{15}; = 0^{00}–4^{10} = ^{1}–6^{25} = –17^{00} = 18^{20}–19^{10} = –21^{30} = = –22^{20} = –24; ⌒^{2} 0^{00}–9
7	8	•	•	= 0^{00}–5^{00}; ⌒^{1} 23–24
8	8	0.0	•	= 20^{30}–21^{45} = ^{0}–24; ⌒^{1} 0^{00}–7 ⌒^{0} 19–21 ⌒^{1}–24
9	8	•	•	= ^{0} 0^{00}–4^{40} = –5^{30} = 20^{45}–21^{20}; ⌒^{1} 0^{00}–7; 22–24
10	6	16.2	•	•^{0} 8^{45}–9^{10}, 9^{50}–10^{25} •^{0}–10^{55} •^{0} 16^{50}–17^{05} •^{1} ▽ 23^{25}–24; = 3^{40}–17^{30} 18^{40}–24; ⌒^{1} 0^{00}–5
11	6	3.5	•	•^{1} ▽ 0$^{00-50}$ •^{0}–1^{55} •^{1} ▽–2^{40} •^{0}–3^{10} •^{1}–4^{45} 5$^{00-50}$ 6$^{05-25}$ •^{1}–9^{40}; = 0^{00}–14^{45} = 18^{40}–19^{30} = = –20^{15} = –22^{45} = ^{0}–24; ⌒^{0} 19–24
12	8	0.2	•	•^{0} 16$^{18-50}$; = ^{0} 0^{00}–1^{40} = ^{1}–6^{35} = ^{0}–7^{25} = –7^{50}; ⌒^{2} 0^{00}–9
13	7	•	•	= 4^{20}–6^{35} = –8^{40} 9^{10}–11^{20} 18^{30}–22^{20} = = –23^{40} = –24; ⌒^{1} 1–4 ⌒^{2}–9 ⌒^{0} 20–23 ⌒^{2}–24
14	7	0.0	•	•^{0} 7^{20}–8^{45}; = 0^{00}–1^{30} = –3^{20} = = –4^{50} = –12^{15} 20^{45}–24; ⌒^{2} 0^{00}–7^{20} 22–24
15	7	0.0	•	= 0^{00}–11^{40} 17^{40}–21^{45} = ^{0}–24; ⌒^{2} 0^{00}–9 ⌒^{0} 19–20 ⌒^{1}–24
16	7	•	•	= ^{0} 0^{00}–1^{15} = ^{1}–7^{15} = ^{0}–7^{35} = –11^{10} 18^{40}–20^{25} = = –24; ⌒^{1} 0^{00}–10 20–24
17	8	•	•	= = 0^{00}–6^{25} = –7^{25} = ^{0} 22^{40}–23^{20}; ⌒^{1} 0^{00}–2 ⌒^{2}–9 ⌒^{1} 21–23 ⌒^{2}–24
18	8	7.1	•	•^{0} ▽ 19$^{16-21}$ •^{1} ▽ 20$^{08-50}$ •^{0} ▽ 21^{15}; ↖^{0} SW 19^{15}–20^{10} ↖^{1} S 20$^{10-45}$ E; = 18^{30}–24; ⌒^{2} 0^{00}–2
19	7	•	•	= 0^{00}–5; 20^{30}–21^{45} = ^{0}–24; ⌒^{0} 19–24
20	8	•	•	= ^{0} 0^{00}–3^{45} = –10^{45} 21^{15}–24; ⌒^{0} 0^{00}–1 ⌒^{1}–9; 21–23 ⌒^{1}–24
21	8	•	•	= 0$^{00-15}$ = ^{1}–6^{45} = ^{0}–8^{40} = 19^{10}–20^{20} = = –24; ⌒^{2} 0^{00}–9 ⌒^{1}–10 ⌒^{0}–12 ⌒^{1} 19–23 ⌒^{2}–24
22	8	•	•	= = 0$^{00-40}$ = ^{1}–3^{50} = ^{2}–5^{20} = ^{1}–6^{40} = ^{0}–7^{35} = –8^{10} = 17^{30}–20^{40} = –21^{30} = ^{0}–24; ⌒^{0} 0^{00}–9; 20–24
23	7	•	•	= ^{0} 0$^{00-20}$ = –6^{00} = = –7^{30} = –9^{30}; 21^{45}–24; ⌒^{0} 0^{00}–1 ⌒^{1}–4 ⌣^{0}–7 ⌒^{0} 20–24
24	7	•	•	= 0^{00}–7^{30} 19^{20}–24; ⌒^{2} 0^{00}–8 ⌒$^{1-0}$–9
25	8	•	•	= 0^{00}–5^{30}
26	7	0.1	•	≫ 8^{10}–9^{20} ≫ –12^{00}; = 22^{40}–24
27	8	0.0	•	•^{0} ▽ 5^{30}–6^{52} •^{1} ▽–7^{02} •^{0} ▽–7^{15} •^{0} 7^{25}–8^{40}; = 0^{00}–7^{15}; ⌒^{0} 22–24
28	7	5.2	•	•^{0} 11^{48}–13^{45} •^{1}–14^{05} •^{0}–14^{20}, 14^{30}–16^{50} 17^{05} •^{1}–17^{07} •^{0}–18^{30}–19^{15}; = 1^{48}–3^{50} = = –5^{20} = –5^{35} 19^{20}–24; ⌒^{0} 0^{00}–8
29	8	•	•	•^{0} 0^{20}–2^{20}; = 0^{00}–10^{20}; ⌒^{0} 19–23 ⌒^{1}–24
30	8	•	•	= 21^{40}–22 = = –24; ⌒^{1} 0^{00}–8; 22–24
31				
Σ	–	49.9	–	

Październik - Octobre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ OCU h	POGODA
1	8	•	•	= = 0^{00} 2^{10} = –8^{40} 22$^{20-35}$ = = –22^{40} = ^{0}–24; ⌒^{1} 0^{00}–8 ⌒^{0}–11; 20–22 ⌒^{1}–24
2	7	0.3	•	•^{0} 18^{10}–24; = ^{0} 0$^{00-40}$ = ^{1}–5^{05} = ^{0}–5^{35} = –10^{20} 14^{35}–24; ⌒^{2} 0^{00}–9
3	7	0.1	•	•^{0} 0^{00}–1^{45}; = 0^{00}–11^{40} 18^{30}–24; ⌒^{0} 20–21 ⌒^{1}–23 ⌒^{2}–24
4	7	•	•	= 0$^{00-20}$ = ^{0}–2^{20} = ^{1}–5^{25} = ^{2}–7^{45} = ^{1}–8^{20} = –12^{30} 15^{20}–19^{40} = = –20^{35} = ^{1}–22^{30} = ^{2}–23^{20} = ^{2}–24; ⌒^{2} 0^{00}–10; 19–24
5	7	•	•	= ^{2} 0^{00}–2^{20} = ^{1}–8^{40} = ^{1}–8^{58} = ^{0}–9^{35} = –11^{40} 18^{45}–24; ⌒^{2} 0^{00}–10
6	6	0.2	•	= 0^{00}–5^{40} = ^{1}–7^{45} = ^{0}–8^{40} = –10^{30} ∞ –17^{30} = –19^{45} = ^{0}–21^{30} = ^{1}–23^{15} = ^{2}–24; ⌒^{0} 1–5 ⌒^{1}–6 ⌒^{2}–9 ⌒^{1}–10 ⌒^{0}–12; 17–18 ⌒^{1}–19 ⌒^{2}–24
7	7	•	•	= ^{2} 0^{00}–7^{30} = ^{1}–8^{25} = –11^{45} = = 18^{45}–19^{25} = ^{1}–20^{35} = ^{2}–21^{48} = ^{2}–24; ⌒^{2} 0^{00}–9; 20–24
8	4	0.5	•	•^{0} 13^{05}–20^{50}; = ^{2} 0^{00}–6^{30} = ^{1}–7^{40} = –13^{10} = ^{0}–13^{30} = –15^{40} = ^{2}–18^{20} = –24; ⌒^{2} 0^{00}–9
9	7	•	•	= 0^{00}–11^{40}
10	8	•	•	= 5^{10}–9^{15} = 19^{20}–20^{25} = = –24; ⌒^{0} 20–21 ⌣^{0}–22 ⌣^{1}–24
11	7	•	•	= = 0^{00}–6^{40} = ^{0}–6^{50} = ^{1}–7^{15} = ^{1}–7^{40} = ^{0}–8^{35} = –12^{30} 16^{45}–24; ⌣^{0} 0^{00}–9 ⌒^{0} 19–21 ⌒^{1}–24
12	8	•	•	= 0^{00}–9^{10} 19^{40}–21^{20} = = –22^{30} = –23^{30} = = –24; ⌒^{1} 0^{00}–1 ⌒^{2}–9 ⌣^{0} 21–24
13	7	•	•	= = 0^{00}–1^{40} = –10^{15} = 17^{40}–18^{30} = –24; ⌣^{0} 0^{00}–1 ⌣^{1}–3 ⌣^{2}–8 ⌣^{0} 19–24
14	7	•	•	= 0^{00}–10^{20} = 17^{25}–18^{22} = –19^{30} = = –24; ⌣^{0} 0^{00}–2 ⌣^{1}–3 ⌣^{2}–8 ⌣^{0} 23–24
15	7	•	•	= = 0^{00}–5^{20} = –9^{30}; ⌣^{0} 0^{00}–2 ⌣^{1}–4 ⌣^{2}–8 ⌣^{0}–9
16	7	4.0	•	•^{0} 13^{40}–17^{10}; = 13^{30}–24
17	7	•	•	= 0^{00}–5^{10}
18	7	0.0	•	= 6^{30}–8^{45} 18^{30}–21^{40} = ^{0}–22^{45} = –24
19	7	•	•	•^{0} 2^{20}–3^{40}; = 0^{00}–11^{15} 17^{30}–20^{10} = = –24; ⌒^{2} 19–24
20	7	•	•	= = 0^{00}–2^{40} = ^{0}–3^{50} = ^{0}–5^{40} = –10^{40} 19^{50}–24; ⌒^{2} 0^{00}–9
21	7	•	•	= 0^{00}–3^{00} = = –7^{00} = = ^{2}–8^{00} = ^{2}–8^{15} = –9^{30} 19^{30}–24; ⌣^{1} 4–8
22	7	•	•	= 0^{00}–11^{20} 16^{15}–24; ⌣^{0} 1–3 ⌣^{1}–9; 22–24
23	6	•	•	= 0^{00}–11^{15} ∞ –18^{30} = –24; ⌣^{1} 0^{00}–2 ⌣^{2}–9 ⌣^{1}–10
24	6	•	•	= 0^{00}–14^{20} 18^{10}–24; ⌣^{0} 2–5 ⌣^{1}–9
25	6	•	•	= 0$^{00-40}$ = ^{1}–7^{45} = –20^{45} = ^{0}–22^{30} = ^{1}–23^{15} = ^{2}–24; ⌣^{0} 1–4 ⌣^{1}–10 ⌣^{0} 19–24
26	6	•	•	= ^{2} 0^{00}–6^{30} = ^{1}–7^{15} = ^{0}–7^{45} = –12^{40} ∞ –14^{40} = 15^{30}–21^{10} = = –24; ⌣^{0} 0^{00}–2 ⌣^{1}–9 = 21^{10}–24
27	6	•	•	= = 0^{00}–2^{25} = –12^{35} ∞ –13^{20} = –24; ⌣^{2} 0^{00}–9
28	8	•	•	= 0^{00}–4^{30} 8^{40}–10^{20} 17^{30}–24; ⌣^{0} 1–7
29	7	2.0	•	•^{0} 16$^{35-50}$ •^{1} ▽–17^{05} •^{0} ▽–18^{30}; = 0^{00}–7^{45}; ⌒^{1} 3–8 ⌒^{0}–10
30	8	•	•	≫ 23^{15}–24; = 19^{15}–23^{30}; ⌣^{0} 20–22
31	8	0.8	•	•^{0} ▽ 11$^{20-30}$; ≫ 0^{00}–2^{45};
Σ	–	7.9	–	

Jelenia Góra — φ = 50°54' — λ = 15°48' — Listopad – Novembre 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	65.7	61.7	58.6	62.0	6.9	11.7	12.9	11.0	14.3	4.5	90	74	63	76	1.0	3.6	5.6	3.4	10 •	9	7	NE 1	WSW 5	WSW 5
2	60.5	62.3	64.0	62.3	9.1	10.2	7.8	8.7	12.9	7.2	68	58	79	68	3.7	5.2	2.2	3.7	8 •	8	8	WSW 5	WSW 8	WSW 6
3	68.0	68.1	71.3	69.1	5.3	7.2	0.6	3.4	8.8	0.0	89	66	98	84	1.0	3.5	0.1	1.5	9 •	9	10	W 1	W 4	C 0
4	77.1	80.5	84.4	80.7	1.4	4.7	-2.7	0.2	5.1	-3.1	92	67	95	85	0.6	2.8	0.2	1.2	9	9	1	C 0	W 4	C 0
5	87.0	88.3	90.6	88.6	-1.9	6.1	0.3	1.2	6.4	-3.7	96	79	98	91	0.2	2.0	0.1	0.8	7	8	8	C 0	NW 2	C 0
6	91.0	89.2	84.9	88.4	-2.9	7.3	-2.1	0.0	7.9	-3.7	99	59	98	85	0.0	4.1	0.1	1.4	2	1	2	C 0	C 0	C 0
7	80.3	77.7	78.7	78.9	-5.1	12.1	0.8	2.2	12.2	-5.7	98	49	88	78	0.1	7.2	0.8	2.7	0	0	9	C 0	C 0	C 0
8	80.9	81.9	83.4	82.1	-5.9	8.5	-0.9	0.7	8.5	-4.6	96	57	98	84	0.2	4.7	0.1	1.7	3	1	8	C 0	NE 1	C 0
9	82.5	82.1	80.7	81.8	3.3	6.2	6.7	5.7	6.9	-1.0	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 ≡	10	C 0	C 0	C 0
10	78.7	77.6	74.9	77.1	5.1	7.0	6.3	6.2	7.9	4.9	100	97	98	98	0.0	0.3	0.1	0.1	10 ≡	10	10 •	C 0	C 0	C 0
11	70.0	68.4	66.6	68.3	4.4	3.4	0.9	2.4	6.3	0.1	98	81	78	86	0.2	1.5	1.4	1.0	10 •	10	10	E 5	E 2	E 2
12	66.5	67.6	68.9	67.7	-2.1	-2.4	-2.7	-2.5	1.0	-2.7	92	87	86	88	0.4	0.7	0.7	0.6	10 *	10 *	10 *	NE 4	ENE 1	E 4
13	68.7	69.3	70.4	69.5	-3.1	-3.5	-5.1	-4.2	-2.6	-5.1	86	90	98	91	0.7	0.5	0.1	0.4	10	10 *	10 *	E 2	ENE 2	ENE 2
14	70.9	72.0	72.9	71.9	-5.6	-5.4	-6.9	-6.2	-4.8	-7.0	95	90	96	94	0.2	0.4	0.1	0.2	10	10 *	10 *	ENE 3	E 2	C 0
15	74.0	76.9	81.7	77.5	-7.9	-5.5	-6.1	-6.4	-5.0	-8.3	96	80	86	87	0.1	0.8	0.5	0.5	10 *	9	10 *	C 0	NW 3	NW 2
16	85.6	86.2	86.1	86.0	-6.1	-5.0	-6.5	-6.0	-4.5	-7.0	89	88	97	91	0.4	0.5	0.1	0.3	10 *	10 *	10 *	WNW 4	WNW 3	C 0
17	81.6	78.7	73.6	78.0	-5.4	-5.9	-11.6	-8.1	-3.7	-11.6	85	78	100	88	0.6	1.0	0.0	0.5	10	1	0	E 5	SE 4	C 0
18	68.3	66.1	64.1	66.2	-10.2	-4.1	-6.8	-7.0	-3.7	-11.9	97	89	96	94	0.1	0.5	0.1	0.2	3	10 *	10 *	C 0	C 0	C 0
19	60.3	58.8	59.4	59.5	-5.8	1.3	1.3	-0.5	3.2	-8.7	97	87	96	93	0.1	0.9	0.2	0.4	10	10	8	C 0	ENE 1	C 0
20	60.5	60.6	57.5	59.5	-1.2	2.3	-2.4	-0.9	2.6	-4.6	100	87	98	95	0.0	0.9	0.1	0.3	10	10	3	C 0	C 0	C 0
21	49.2	45.2	49.9	48.1	2.7	3.7	-1.5	0.8	7.0	-4.6	82	90	88	87	1.3	0.8	0.7	0.9	10 •	10	10 *	SE 6	SSW 1	WNW10
22	62.5	67.8	73.5	67.9	-2.9	-2.1	-5.2	-3.8	-1.2	-5.5	95	87	90	91	0.2	0.6	0.4	0.4	10 *	10 *	10 *	W 5	NW 3	W 5
23	77.6	78.6	80.2	78.8	-14.2	-5.0	-14.2	-11.9	-4.8	-14.6	92	73	92	86	0.2	1.1	0.2	0.5	5	6	0	C 0	NW 2	C 0
24	76.5	72.7	69.7	73.0	-16.3	0.7	-1.4	-4.6	0.9	-17.2	95	37	70	67	0.1	4.0	1.7	1.9	0	8	10	C 0	WSW 1	C 0
25	71.3	73.8	70.6	71.9	0.9	1.7	-5.2	-2.0	1.7	-8.0	75	68	88	77	1.6	2.2	0.5	1.4	10	8	0	WSW 6	WSW 4	C 0
26	60.1	58.2	62.8	60.4	4.3	3.7	1.1	2.6	7.7	-5.2	58	75	85	73	3.5	2.0	1.0	2.2	8	10 •	9	S 4	SW 5	W 2
27	58.4	47.9	42.7	49.7	-2.8	1.3	5.1	2.2	5.8	-6.2	91	85	84	87	0.5	1.0	1.4	1.0	10	9	10	C 0	SE 7	W 4
28	47.0	49.9	56.4	51.1	1.5	0.5	1.4	1.2	6.0	0.0	69	90	81	80	2.1	0.6	1.3	1.3	6	10	10	WSW 7	W 7	WSW 6
29	62.7	60.8	50.4	58.0	1.1	2.2	2.3	2.0	3.9	-0.3	85	59	61	68	1.0	3.0	2.8	2.3	10 *	6	10	WSW 6	C 0	SSW10
30	47.4	53.1	56.5	52.3	8.1	4.9	0.2	3.4	9.3	-0.5	55	58	68	60	4.8	3.7	2.0	3.5	9	8	2	SE 10	SW 6	SSW 1
31																								
M	69.7	69.4	69.5	69.5	-1.4	2.3	-1.1	-0.3	3.9	-4.5	89	76	88	84	0.8	2.0	0.8	1.2	8.0	8.0	7.5	2.5	2.6	2.0

Grudzień – Décembre

1	52.6	57.6	62.2	57.5	1.9	2.7	1.9	2.1	2.9	-2.2	73	69	76	73	1.9	2.3	1.7	2.0	10	9 *	10 *	WSW 9	WSW 8	WSW 5
2	66.0	66.4	58.7	63.7	0.7	2.1	1.9	1.6	2.6	0.3	96	78	57	77	0.2	1.5	3.0	1.6	10 *	8	8	WSW 2	SW 2	S 7
3	55.9	55.1	56.4	55.8	-1.3	1.8	0.5	0.4	3.7	-1.6	89	78	84	84	0.6	1.6	1.0	1.1	9	10	9	SE 2	S 3	C 0
4	57.9	58.9	61.1	59.3	2.8	4.8	2.9	3.4	5.5	-0.3	81	61	83	75	1.5	3.4	1.3	2.1	10	3	10	C 0	SSW 4	NNW 2
5	62.0	56.4	47.0	55.1	0.9	5.4	6.6	4.9	7.1	-0.4	90	51	78	73	0.6	4.4	2.1	2.4	9	9	10 •	C 0	S 8	S 4
6	54.6	57.3	62.8	58.2	4.5	6.7	4.9	5.2	9.0	4.2	65	55	61	60	2.9	4.4	3.4	3.6	3	7	8	W 5	WSW 8	SW 3
7	65.3	68.1	69.9	67.8	3.2	4.4	3.6	3.7	5.7	1.9	64	55	67	62	2.8	3.8	2.6	3.1	8	10	10	WSW 5	WSW 3	WSW 6
8	71.6	73.6	77.8	74.3	2.6	2.4	1.5	2.0	3.7	-0.1	63	80	70	71	2.7	1.5	2.0	2.1	10	9	7	WSW 2	W 2	W 4
9	74.5	69.0	58.7	67.4	1.4	4.7	3.6	3.3	5.2	-3.6	72	44	60	59	1.9	4.7	3.1	3.2	9	7	9	SW 6	SW 6	SSE 6
10	44.4	42.0	43.4	43.3	2.8	6.0	5.1	4.8	6.7	0.8	79	58	67	68	1.6	3.9	2.9	2.8	10 •	5	9 •	S 6	SSW 6	WSW 5
11	51.8	52.6	55.4	53.3	1.9	2.7	0.9	1.6	5.3	-0.2	66	58	75	66	2.4	3.1	1.6	2.4	9	6	10	W 5	WSW 4	WSW 4
12	61.4	63.6	65.7	63.6	1.2	2.4	-1.9	0.0	2.5	-2.4	74	73	90	79	1.8	2.0	0.5	1.4	10	7	4	W 8	W 6	C 0
13	67.8	66.2	61.4	65.1	-0.5	1.9	0.2	0.4	2.1	-2.9	98	76	94	89	0.2	1.7	0.4	0.8	10 *	9	10 *	C 0	E 1	E 5
14	77.7	81.7	84.8	81.4	-4.9	-4.2	-14.6	-9.6	0.2	-15.0	86	91	87	88	0.6	0.4	0.3	0.4	9	1	0	WNW 2	C 0	C 0
15	81.2	80.5	80.4	80.7	-5.3	1.3	1.0	-0.4	1.5	-15.1	93	96	96	95	0.3	0.3	0.3	0.3	10	10 •	10	C 0	W 3	WNW 1
16	77.6	76.5	74.8	76.3	-0.7	0.2	-0.4	-0.3	1.2	-1.4	99	92	92	94	0.0	0.5	0.5	0.3	10	9	9 *	C 0	C 0	ENE 3
17	73.1	71.5	72.2	72.3	-3.1	-0.6	0.4	-0.7	1.6	-4.1	99	99	98	99	0.0	0.0	0.1	0.0	0 ≡	10 *	9 ≡	C 0	C 0	C 0
18	69.5	69.3	72.2	70.3	1.7	7.5	10.5	7.6	10.5	-0.1	94	84	81	86	0.4	1.7	2.4	1.5	10 •	10 •	10 •	C 0	SSW 4	WSW 7
19	72.9	72.9	71.7	72.5	9.9	11.2	10.7	10.6	12.3	8.6	76	71	67	71	3.0	3.9	4.3	3.7	10	9	3	WSW 7	WSW 4	W 5
20	75.9	75.2	71.5	74.2	5.1	5.0	3.4	4.2	11.0	2.4	67	75	97	80	2.9	2.2	0.3	1.8	10	9	10 •	W 3	C 0	WNW 2
21	69.2	71.5	73.8	71.5	3.2	0.2	0.3	1.0	3.8	0.0	100	100	98	99	0.0	0.0	0.1	0.0	10 •	10 *	10 *	WNW 2	WNW 2	C 0
22	76.9	75.8	75.3	76.0	-1.5	-0.6	-5.5	-3.3	1.3	-8.5	96	81	95	91	0.2	1.1	0.2	0.5	10	0	7 ≡	C 0	C 0	C 0
23	72.7	66.9	59.9	66.5	-9.7	-0.6	-1.2	-3.2	0.5	-10.9	91	81	68	80	0.3	1.1	1.8	1.1	10 ≡	6	6	C 0	ENE 5	SE 6
24	56.5	54.8	49.8	53.7	-0.4	4.4	0.7	1.4	4.4	-2.8	92	63	77	77	0.5	3.1	1.5	1.7	10	8	2	C 0	S 1	SSE 7
25	44.6	43.2	44.5	44.1	1.6	2.8	3.8	3.0	4.4	0.0	76	76	75	76	1.7	1.9	2.0	1.9	9	9	10	SE 3	SSE 4	SSW 4
26	46.9	53.2	60.9	53.7	2.0	0.3	0.5	0.8	4.6	0.0	91	96	89	92	0.7	0.2	0.7	0.5	10	10 *	7	SE 1	WNW 2	W 2
27	61.7	58.4	53.9	58.0	-5.6	2.4	1.2	-0.2	3.6	-6.2	95	60	77	77	0.2	3.0	1.5	1.6	3	3	10	C 0	C 0	C 0
28	53.9	60.5	66.6	60.3	0.6	-1.2	-2.0	-1.2	2.2	-2.9	90	76	77	81	0.6	1.3	1.3	1.1	10	6	0	W 6	WNW 4	W 3
29	69.2	72.7	73.2	71.7	-1.3	0.3	-0.8	-0.6	0.6	-7.7	74	72	77	74	1.4	1.7	1.3	1.5	7	5	9	W 6	W 8	WSW 2
30	66.4	62.0	63.2	63.9	-3.0	1.5	1.3	0.3	1.6	-4.8	66	52	76	65	1.7	3.3	1.6	2.2	6	9	9	SE 2	S 7	WSW 4
31	63.8	65.0	66.5	65.1	2.4	3.6	2.7	2.8	3.9	1.3	75	70	88	78	1.8	2.4	0.9	1.7	8	8	10 •	SW 3	WSW 3	WNW 2
M	64.4	64.5	64.4	64.4	0.4	2.6	1.4	1.4	4.2	-2.4	83	73	80	79	1.2	2.1	1.5	1.6	8.7	7.5	7.9	2.7	3.5	3.2

DNI	WIDZALNOŚĆ V	OPAD R	GRUBINE GU h	POGODA
1	8	0.2	•	•°0^40 3^30 6^20 7^40 8^50 ... 58 16^45 17^05 ≫ 15^40 – 16^10
2	8	0.5	•	•°6^05 7^05 ♀°17^23 – 18^10 19^25 – 40 20^48 – 21^06 21^25 22^10 22^20 – 40
3	7	5.8	•	♀°6^02 – 7^12 •°14^43 – 15^40 •¹ – 16^20 •° – 17^40 ✶° – 18^25 = 15^15 – 24
4	8	•	•	= 0^00 – 7^35 20^40 – 24
5	6	•	•	= 0^00 – 6^20 7^40 – 18^40 = = – 21^20 = – 24 ⌴° 0^00 9
6	6	•	•	= 0^00 – 5^15 = = – 6^50 = – 12^15 ∞ – 16^30 = – 24 ⌴° 5 – 10 20 – 23 ⌴¹ – 24
7	7	•	•	= 0^00 – 11^25 19^15 – 24 ⌴¹ 0^00 – 4 ⌴² – 10
8	7	0.3	•	= 0^00 – 11^40 16^30 – 24 ⌴° 1 – 10
9	2	0.1	•	•°6^15 – 7^20 9^30 – 12^40 = 0^00 – 6^15 = ¹ – 7^20 = ² – 11^50 = ¹ – 13^10 = ² – 19^40 = – 24
10	4	0.3	•	•¹9^35 – 10^20 •°13^20 – 14^35 20^15 22^45 23^15 – 24 = 0^00 – 14^0 = ¹ – 2^10 = ² – 3^30 = ¹ – 7^10 = ² – 7^30 = ¹ – 10^35 = – 24
11	6	2.3	•	•°0^00 – 8^35 ✶°17^40 19^20 ♀°21^40 – 22^32 = 0^00 – 13^30 17^20 – 24
12	6	0.3	5	♀°0^00 – 1^40 ✶°2^45 23^15 = 0^00 – 24
13	5	0.3	3	✶° 7^10 8^00 – 16^00 ... 21^30 = 0^00 – 4^20 7^00 – 24
14	5	3.2	3	✶° 7^10 9^15 – 21^45 24 = 0^00 – 24
15	5	0.5	7	✶°0^00 ... 2^30 – 6^15 11^20 14^15 – 18^25 19^40 – 24 = 0^00 – 24
16	5	0.3	8	✶°0^00 ... 16^15 19^40 21^15 = 0^00 – 24
17	6	•	8	= 0^00 – 4^40 6^20 – 24 ⌴° 20 – 24
18	5	5.3	6	✶°11^40 13^10 20^40 22^15 23^45 24 = 0^00 – 24 ⌴° 0^00 – 11
19	7	•	9	✶°0^00 14^5 = 0^00 – 9^45 15^20 – 24
20	6	0.1	7	•°9^15 10^15 13^40 15^45 = 0^00 – 21^40 = ¹ – 23^45 = – 24
21	7	2.7	5	•°6^40 8^10 – 10^40 15^35 16^10 17^50 19^20 ✶° – 24 ≫ 10^15 – 22^10 = 0^00 – 10^00 19^20 – 24
22	6	0.8	4	✶°0^00 2^10 ✶¹ 6^00 ✶° – 11^20 14^15 15^30 16^15 19^40 – 24 = 0^00 – 24
23	7	•	5	✶°0^00 2^40 = 0^00 – 10^45 16^45 – 24
24	8	0.3	4	= 0^00 – 10^20
25	8	0.0	4	✶°0^10 2^20 3^10 – 4^45 8^10 – 20 ✶¹ – 9^15 ✶° – 9^40 ♀°11^13 – 22 11^44 – 12^06 = 19^30 – 22^15
26	7	0.1	5	✶°14^20 12^18 •° ... 16^40 △ 18^45 – 19^20 = 18^50 – 21^20
27	6	1.9	4	✶°8^20 – 9^10 •°16^40 17^00 – 19^10 20^40 ≫ 13^45 – 14^20 = 5^40 6^20 7^30 – 24
28	7	2.4	pł.	•°0^15 ... 4^00 ♀°8^40 – 50 ♀° 9^20 9^35 10^45 11^40 13^25 ✶¹ 14^38 – 16^10 ✶° – 17^35 21^30 ... 22^20 por. wiatru do 13 m/sek 4^40 – 5^30 = 0^00 – 6^00 18^00 – 24
29	8	0.0	4	✶°6^40 7^20 ≫ 17^30 – 24 (por. 20 m/s) = 0^00 – 7^15
30	8	0.1	pł.	≫ 0^00 – 7^20 (por. 15 m/s)
31				
Σ	–	25.8	–	

Grudzień - Décembre

1	7	0.7	1	♀°3^20 – 4^40 ✶¹ – 5^10 ✶° – 6^30 7^20 – 35 ✶¹ 9^30 ✶° 10^10 ♀° 11^50 12^52 14^05 14^40 15^40 17^40 24 = 4^30 – 12^00 17^20 – 24
2	7	1.1	1	✶°0^00 4^00 – 5^40 ✶¹ – 6^10 ✶° – 10^30 11^15 por. wiatru do 14 m/sek 22^40 – 24 = 0^00 – 12^30
3	8	0.0	pł.	✶°3^20 4^38 ✕° 21^50 – 22^05 por. wiatru do 14 m/sek 0^00 – 2^20
4	8	0.0	pł.	•°16^40 17^15
5	7	1.4	pł.	•°2^10 ... 35 17^45 24 ≫ 23^50 – 24 = 3^30 – 8^10
6	8	0.4	•	•¹0^00 ... 15 •° 1^20 4^10 5^00 22^15 – 24 ≫ 0^00 – 15
7	8	•	•	•°0^00 2^15
8	7	0.0	•	✶°11^34 – 48
9	8	2.7	•	≫ 16^25 – 17^15 19^50 – 24 (por. do 18 m sek 22^42 – 24) = 2^45 – 5^15 ⌓ 4 – 6
10	7	0.0	1	•°3^10 – 4^05 •° – 4^40 ✶° – 5^40 •° – 8^20 9^10 •°14^25 – 30 16^05 – 15 •°17^40 18^10 19^45 22^20 ≫ 0^00 – 3^20 por. wiatru do 18 m/sek 0^00 – 4^15 por. wiatru do 13 m/sek 12^50 – 14^30 = 4^25 – 10^20
11	8	0.0	•	♀°11^30 – 40 12^15 – 25 14^50 – 15^10 19^40 – 20^05 por. wiatru do 12 m/sek 23^20 24 = 19^50 – 21^10
12	7	0.6	•	✶°0^38 – 45 ✶°3^40 5^15 ♀°8^10 – 30 8^40 – 9^10 10^42 11^20 por. wiatru do 12 m/sek 0^00 – 30 ≫ 14^0 – 25^0 = 3^30 – 5^40 23^30 24
13	6	5.2	1	✶°3^45 – 5^15 ✶° 7^20 14^40 17^10 19^25 ✶¹ – 20^20 ✶° – 22^15 ✶¹ – 24 = 0^00 – 13^20 14^40 – 24
14	6	•	7	✶¹0^00 – 1^30 ✶° – 2^20 5^15 = 0^00 – 15^25 = = – 17^30 = = – 22^20 = = – 24 ⌴° 10 – 24
15	4	0.5	6	△ 7^20 9^30 •°10^05 11^10 12^20 15^15 = = 0^00 – 42 = ° – 2^40 = – 24 ⌴° 0^00 – 6
16	5	0.0	3	✶°20^40 22^20 = 0^00 – 24
17	4	1.2	3	✶°9^20 – 18^40 = 0^00 – 5^35 = ¹ – 7^20 = ² – 9^20 = ° – 10^50 = – 15^50 = ° – 24
18	7	5.3	3	•°6^45 8^25 – 19^40 22^38 22^40 – 24 = °0^00 – 4^10 = – 4^50 19^35 – 24
19	8	0.9	•	•°0^00 2^40 3^50 – 5^20 = 0^00 – 6^20
20	7	0.8	•	♀¹22^8 – 35 •°15^40 18^10 19^15 – 30 21^30 •° 22^20 = 8^50 – 10^00 17^00 – 24 ⊕ 11^20 – 12^05
21	4	10.1	•	•°0^10 ... 3^00 4^15 7^40 – 9^40 ✶° – 10^10 ✶° – 12^15 ✶¹ – 14^20 ✶° – 16^40 ✶° – 17^45 ✶°18^20 19^30 ✶¹ – 21^15 ✶° – 24 = 0^00 – 24
22	6	•	11	✶°0^00 – 5^15 6^05 = 0^00 – 8^45 = ° ... 9^25 = ¹ – 10^35 = ° – 11^05 = – 15^40 = ° – 16^40 = ¹ – 18^35 = ° – 21^40 = – 24
23	8	0.0	8	≫ 22^40 – 24 = 0^00 – 5^45 = ° – 6^30 = ¹ – 7^40 = ² – 8^25 = ° – 9^30 = ° – 10^15 = – 12^20
24	8	0.1	7	✶°6^40 – 8^10 ≫ 0^00 – 2^30
25	8	0.2	5	✶°1^00 ... 3^15 ✕° 7^10 – 30
26	5	1.7	3	•°2^40 6^28 ♀°11^10 – 15 ✶¹ – 12^05 ♀° – 13^20 ✶° – 15^30 = 19^30 – 22
27	7	0.3	2	✶°22^45 – 24 = 22^15 – 24
28	7	0.0	3	✶°0^00 – 3^45 8^10 – 9^45 10^25 – 11^20 = 0^00 – 5^30 7^45 – 12^20
29	8	•	4	
30	8	•	2	
31	7	0.3	1	♀°8^42 – 9^10 •°9^30 ... 10^20 19^35 23^40 •° – 24 = 19^10 – 24
Σ	–	33.5	–	

DNI	CIŚNIENIE P= 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	122.9	123.0	121.9	122.6	-5.4	-5.4	-5.7	-5.6	-5.2	-4.5	97	97	97	97	0.2	0.2	0.2	0.2	10*≡	10 ≡	10≡	SSW20	SW 17	SW 8
2	119.8	119.7	120.6	120.0	-4.8	-4.8	-6.6	-5.7	-5.7	-6.8	95	95	94	95	0.2	0.2	0.2	0.2	10*≡	10*≡	10	SW 4	NW 4	NNW 6
3	121.2	122.8	123.9	122.6	-8.5	-8.6	-8.9	-8.7	-6.6	-9.0	95	92	89	92	0.2	0.3	0.4	0.3	8	10*≡	10*≡	NW 8	NNW 4	NW 12
4	126.3	129.6	135.0	130.3	-9.7	-9.6	-11.0	-10.3	-8.9	-11.2	91	91	90	91	0.3	0.3	0.3	0.3	10*≡	10*≡	10 ≡	NW 17	NW 18	NW 12
5	133.4	131.6	134.2	133.1	-9.8	-5.6	-6.2	-7.0	-5.5	-13.4	91	95	94	93	0.3	0.2	0.2	0.2	5	10*≡	10*≡	NW 15	NW 25	NW 20
6	135.3	136.4	135.0	135.6	-7.1	-7.0	-7.5	-7.3	-5.8	-7.6	93	93	93	93	0.2	0.2	0.2	0.2	10*≡	10*≡	10*≡	NW 14	NW 6	NW 12
7	135.8	135.7	135.4	135.0	-15.5	-11.0	-6.2	-9.7	-5.4	-15.7	81	73	94	85	0.3	0.7	0.2	0.4	0	6	10*≡	NW 10	NW 9	W 6
8	129.6	125.5	122.3	125.8	-3.0	-0.6	-2.8	-2.3	-0.4	-6.6	97	99	97	98	0.1	0.0	0.1	0.1	10*≡	10 ≡	10 ≡	WSW13	WSW20	WSW20
9	124.2	124.0	124.5	124.2	-3.4	-4.2	-6.4	-5.1	-2.1	-6.5	97	96	94	96	0.2	0.2	0.2	0.2	10*≡	10*≡	10*≡	WSW12	W 6	WNW12
10	117.6	121.5	133.2	124.1	-6.8	-6.2	-7.6	-7.0	-5.7	-7.9	94	94	93	94	0.2	0.2	0.2	0.2	10*≡	10 *	10*≡	WSW15	W 16	NNW12
11	136.1	137.1	136.9	136.7	-8.2	-4.2	-3.2	-4.7	-2.5	-8.9	87	91	97	92	0.4	0.4	0.1	0.3	6	10 ≡	8	NNW 3	WSW 8	W 6
12	135.4	132.0	130.7	132.7	-2.0	-4.0	-3.8	-3.4	2.2	-4.1	94	89	75	86	0.4	0.5	1.1	0.7	8	6	6	WSW 5	SSW12	SW 16
13	131.9	133.4	133.0	132.8	-2.6	-1.8	-4.2	-3.2	1.2	-4.2	93	94	91	93	0.3	0.3	0.4	0.3	4	9	5	NW 5	W 10	W 15
14	127.2	126.0	131.9	128.4	-6.4	-5.0	-7.0	-6.4	-3.9	-8.0	94	90	93	92	0.2	0.4	0.2	0.3	10 ≡	5	10 ≡	SW 20	SW 18	WSW20
15	133.2	133.4	130.8	133.8	-8.5	-6.8	-8.2	-7.9	-6.6	-9.0	92	88	92	91	0.3	0.4	0.2	0.3	2	3	10 ≡	W 16	SW 12	SW 18
16	131.6	132.0	129.4	131.0	-8.3	-7.6	-8.2	-8.1	-7.2	-9.1	92	93	92	92	0.2	0.2	0.2	0.2	9	10 ≡	10 ≡	WSW12	WSW10	WSW12
17	121.3	117.2	112.8	117.1	-8.0	-5.8	-4.5	-5.2	-3.2	-9.1	93	96	96	95	0.2	0.2	0.2	0.2	10*≡	10 ≡	10*≡	SW 25	SW 25	SW 16
18	113.9	112.6	111.7	112.7	-6.0	-6.6	-7.2	-6.8	-4.3	-7.3	94	94	93	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10*≡	SW 20	SW 20	SW 20
19	111.2	111.2	113.9	112.1	-8.4	-8.8	-9.0	-8.8	-7.2	-9.1	92	92	86	90	0.3	0.3	0.4	0.3	10*≡	10 ≡	7	SW 12	WSW12	NNW 2
20	114.2	111.3	109.0	111.5	-9.6	-8.8	-9.2	-9.2	-8.6	-9.9	91	92	92	92	0.3	0.3	0.3	0.3	9 *	10*≡	10*≡	N 4	N 6	N 7
21	111.2	114.7	119.3	115.1	-9.6	-9.2	-9.0	-9.2	-7.0	-10.0	91	92	92	92	0.3	0.3	0.3	0.3	10 ≡	10*≡	10 ≡	N 2	NNW 2	N 1
22	121.6	121.6	124.1	122.4	-9.0	-8.8	-7.8	-8.4	-7.8	-9.2	92	95	93	93	0.3	0.2	0.2	0.2	10 *	10*≡	10 ≡	W 1	SSW 5	SSW 8
23	128.8	131.6	135.6	132.0	-6.4	-4.0	-6.8	-6.0	-2.7	-7.8	91	96	94	94	0.3	0.2	0.2	0.2	10 *	8	10 ≡	SW 2	W 2	NNW 8
24	137.6	138.0	137.6	137.7	-8.8	-6.6	-9.3	-8.5	-6.4	-9.3	86	94	85	88	0.4	0.2	0.4	0.3	6	10 ≡	0	W 1	NW 3	NNW 2
25	134.5	132.2	130.3	132.3	-9.4	-7.8	-7.5	-8.0	-7.5	-9.7	85	87	93	88	0.4	0.4	0.2	0.3	9	10*≡	10*≡	NNW 3	SW 3	SW 4
26	127.9	126.2	126.2	126.8	-7.8	-7.8	-8.5	-8.2	-7.1	-8.5	93	93	92	93	0.2	0.2	0.3	0.2	10 ≡	10*≡	10 ≡	SW 4	SW 7	SW 6
27	125.3	126.4	125.8	125.8	-9.8	-7.7	-8.6	-8.7	-6.9	-9.8	91	93	92	92	0.3	0.2	0.3	0.3	10 ≡	6	10 ≡	SSW 8	S 5	SW 14
28	126.4	127.5	128.0	127.3	-6.4	-6.0	-5.8	-5.5	-3.7	-9.0	92	94	96	94	0.3	0.2	0.2	0.2	10 ≡	9	0	SW 12	WSW14	SW 12
29	128.1	127.8	127.9	127.9	-2.6	-1.9	-2.0	-2.1	-1.5	-4.6	93	85	77	85	0.3	0.8	1.3	0.8	9	6	0	SW 6	SW 8	SW 6
30	126.9	125.1	125.4	125.8	-0.8	-1.8	-2.2	-1.8	-0.2	-2.6	79	88	98	88	1.2	0.7	0.1	0.7	8	9	10 ≡	SW 8	SW 12	SW 14
31	128.6	129.4	128.5	128.8	-5.8	-5.8	-7.2	-5.5	-1.7	-7.3	96	96	93	95	0.2	0.2	0.2	0.2	10*≡	10*≡	10*≡	WNW 1	W 3	N 8
M	126.5	126.4	126.9	126.6	-7.0	-5.9	-6.6	-6.5	-4.5	-8.2	92	92	92	92	0.3	0.3	0.3	0.3	8.5	8.9	8.6	9.6	10.4	10.8

Luty – Février

1	129.9	129.8	133.1	130.9	-11.6	-11.2	-12.4	-11.9	-7.2	-12.6	89	90	93	91	0.3	0.3	0.2	0.3	10*≡	10*≡	10*≡	WSW15	NW 10	NW 6
2	135.3	135.7	139.7	136.9	-13.0	-13.4	-12.2	-12.7	-12.2	-14.5	88	88	89	88	0.3	0.3	0.3	0.3	10 ≡	10*≡	10*≡	NW 18	WNW25	WNW16
3	138.8	137.4	136.3	137.5	-12.0	-9.7	-11.6	-11.2	-9.6	-12.5	89	85	82	85	0.3	0.4	0.4	0.4	10*≡	9	3	WNW10	WNW 6	WNW 6
4	136.7	138.6	137.0	137.4	-9.6	-5.8	-8.8	-8.2	-5.1	-11.8	91	95	92	93	0.3	0.2	0.3	0.3	10 ≡	4	10 ≡	WNW 8	WNW 6	WNW14
5	131.5	130.0	132.0	131.2	-9.2	-7.2	-15.8	-12.0	-5.7	-15.9	92	93	76	87	0.3	0.2	0.4	0.3	10*≡	10*≡	4	WNW10	N 4	N 12
6	134.5	134.5	132.3	133.8	-16.6	-11.9	-10.6	-12.4	-10.6	-17.5	75	89	90	85	0.4	0.3	0.3	0.3	8	10*≡	10*≡	NNW10	NNW 9	NNW 8
7	130.9	131.7	126.7	129.8	-9.6	-7.0	-8.2	-8.2	-7.0	-11.1	91	91	92	91	0.3	0.3	0.2	0.3	10 ≡	9	10*≡	NNW 6	NNW 8	NNW20
8	114.4	118.1	120.6	117.7	-13.2	-13.2	-12.8	-13.0	-6.4	-13.7	88	88	88	88	0.3	0.3	0.3	0.3	10*≡	10*≡	10*≡	N 26	NW 20	NW 25
9	125.4	129.0	132.6	129.0	-14.8	-14.3	-15.6	-15.1	-12.8	-15.6	87	87	86	87	0.3	0.3	0.3	0.3	10*≡	10*≡	10*≡	N 20	N 18	N 18
10	130.4	127.7	127.7	128.6	-14.2	-10.0	-8.5	-10.3	-8.2	-16.3	79	91	92	87	0.4	0.3	0.3	0.3	6	10*≡	10*≡	W 14	WNW16	NW 18
11	130.2	133.5	135.9	133.2	-10.4	-7.8	-9.5	-9.3	-7.0	-10.7	90	84	85	86	0.3	0.5	0.4	0.4	2	1	0	NW 16	NW 8	NW 1
12	135.3	135.5	132.8	134.5	-7.2	-6.2	-7.6	-7.2	-5.9	-10.1	96	89	93	93	0.1	0.4	0.2	0.2	10 ≡	10 ≡	10*≡	W 8	WSW10	W 15
13	126.6	121.1	114.3	120.7	-7.6	-6.8	-6.4	-6.8	-6.1	-8.5	93	96	97	95	0.2	0.1	0.1	0.1	10*≡	10*≡	10*≡	WSW25	SW 30	SW 25
14	111.3	115.8	121.1	116.1	-8.2	-7.4	-7.4	-7.6	-6.4	-8.7	95	93	93	94	0.2	0.2	0.2	0.2	10*≡	10*≡	10*≡	SW 20	W 20	W 14
15	123.9	124.8	124.5	124.4	-9.8	-10.0	-11.2	-10.6	-7.4	-11.4	97	91	93	94	0.1	0.3	0.2	0.2	9	4	9	W 12	S 8	W 12
16	124.3	126.7	127.9	126.3	-13.6	-13.2	-12.6	-13.0	-11.2	-14.1	92	88	89	90	0.2	0.3	0.3	0.3	10*≡	10*≡	10*≡	W 12	W 10	W 8
17	128.6	128.1	128.4	128.4	-14.8	-13.8	-13.6	-14.0	-12.6	-15.3	87	88	88	88	0.3	0.3	0.3	0.3	10*≡	10*≡	10*≡	W 15	N 18	N 22
18	131.3	132.9	133.3	132.5	-12.0	-10.5	-11.7	-11.5	-10.2	-13.7	89	90	89	89	0.3	0.3	0.3	0.3	10*≡	10 ≡	10 ≡	N 16	N 17	N 17
19	133.1	134.0	134.1	133.7	-12.4	-12.8	-13.4	-13.0	-11.7	-14.1	89	88	88	88	0.3	0.3	0.3	0.3	10 ≡	9	10*≡	NNE17	ENE12	N 14
20	133.9	136.4	138.3	136.2	-16.4	-13.4	-11.6	-13.2	-11.6	-16.5	85	88	89	87	0.2	0.3	0.3	0.3	10 ≡	10 ≡	0	N 18	NNE16	ESE12
21	136.9	136.2	133.9	135.7	-10.7	-9.0	-9.2	-9.5	-7.4	-12.8	90	76	76	81	0.3	0.7	0.7	0.6	0	0	8	E 5	SE 5	N 4
22	129.4	128.8	129.9	129.4	-9.8	-11.1	-11.1	-10.8	-9.2	-12.0	85	90	90	88	0.4	0.3	0.3	0.3	9	10*≡	10*≡	N 10	NW 17	NW 10
23	127.7	128.2	128.5	128.1	-12.4	-11.8	-11.2	-11.6	-10.4	-12.7	89	89	90	89	0.3	0.3	0.3	0.3	10*≡	10*≡	10*≡	NW 15	W 4	NW 6
24	128.9	128.4	124.8	127.4	-12.2	-10.2	-11.6	-11.4	-8.0	-12.6	89	91	75	85	0.3	0.3	0.6	0.4	10*≡	9	8 *	WNW 6	W 1	W 6
25	120.5	121.4	123.4	121.8	-11.0	-10.2	-15.8	-13.2	-10.0	-15.9	90	91	86	89	0.3	0.3	0.3	0.3	10*≡	10*≡	0	W 20	W 20	WNW18
26	124.2	122.0	116.5	120.9	-15.4	-14.4	-13.8	-14.4	-13.8	-16.8	77	78	88	81	0.4	0.4	0.3	0.4	0	8	3	W 12	W 25	W 30
27	109.7	109.6	117.1	112.1	-12.0	-12.8	-14.6	-13.5	-11.8	-14.6	89	81	87	86	0.3	0.4	0.3	0.3	10*≡	8 *	10*≡	W 20	WNW22	NNW30
28	123.2	124.4	123.4	123.7	-17.0	-11.6	-12.8	-13.6	-11.3	-17.3	85	65	88	79	0.2	0.9	0.3	0.5	6	4	10 ≡	NW 12	SW 6	SW 8
29																								
30																								
31																								
M	128.1	128.6	128.8	128.5	-12.0	-10.6	-11.5	-11.4	-9.2	-13.5	88	88	88	88	0.3	0.3	0.3	0.3	8.6	8.4	8.0	14.1	13.2	14.1

Śnieżka — $H_s = 1603\,m$ — $H_b = 1610{,}6\,m$ — Styczeń – Janvier 1965

DNI	WIDZALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	0	4.6	45	*3.50 4.70 *-1 8.30 0.45 2.50 24; V 0.00 1.00 V-3.00 V-2 8.30 V-1 24; = 2 0.00 24; +-2 0.00 13.30 +-1 18.30 +-0 21.10 +-1 24; ≈ 0.00 13.30 > 18.30 21.10 24
2	0	3.2	49	*0.00 1.30 *-0 4.30 7.10 15.55 X-16.25 *-0 18.50 V 1.00 2.30 V 0.00 13.30 V 0.00 13.50 19.20 15.30 18.40 21.50 24; = 2 0.00 0.20 = -1.05 ▥ 9.40 11.05 = 2 1.40 ▥ -12.00 = 11.40 12.30 = 2 13.20 = -14.10 ▥ 13.30 14.10 = 2 -18.40 = -18.50
3	0	7.6	52	*2.40 15.30 24; V 0.00 2.30 8.15 24; = 2 0.00 3.20 = -8.15 ▥ 3.30 8.15 = 2 24; +-6.20 11.00 13.30 20.20 +-1 24; > 20.00 24 [2.: ▥ -21.40 = 10.30 21.40 = 2 24; +-1 0.00 5.15 +-0 -6.45 +-0 19.30 21.30
4	0	7.0	58	*0.00 13.30; V 0.00 23.30; = 2 0.00 23.30; +-1 0.00 4.15 +-2 -10.40 +-1 -23.10 +-0 -23.30; > 0.00 4.15 ≈ -10.40 > 24
5	0	21.0	62	*3.45 24; V 5.20 6.30 8.15 24; = 2 5.20 6.30 = 7.40 8.15 = 2 24; +-1 3.30 8.30 +-2 24; > 1.30 8.30 ≈ -24
6	0	13.0	72	*0.00 4.30 *-1 8.40 *-2 24; V 0.00 24; = 2 0.00 24; +-2 0.00 6.30 +-1 11.40 +-0 18.30 +-1 24; ≈ 0.00 8.30 > 11.40 18.30 24
7	8	1.6	80	*0.00 1.30 20.50 22.40 V 0.00 1.40 3.30 10.20 24; = 2 0.00 1.40 = -3.30 ▥ 9.40 13.10 = 2 17.40 24; +-1 0.00 7.30 +-0 15.30 23.50 24; > 0.00 7.30
8	0	2.3	82	*7.50 9.45; V 0.00 24; = 2 0.00 5.30 = -6.40 = 2 8.30 = -12.10 = 2 24; +-2 0.00 5.30 +-1 8.40 +-2 24; > 1.30 8.40 ≈ -24
9	0	9.3	85	*6.30 23.50; V 0.00 24; = 2 0.00 23.20 = -24; +-2 0.00 5.30 +-1 10.40 +-0 17.20 +-1 23.40 +-2 24; ≈ 0.00 5.30 > 10.40 17.20 23.40 ≈ -24
10	6	14.5	94	*3.40 6.30 *-1 9.15 *-0 0.40 10.20 23.45; V 0.00 23.55; = 2 0.00 140 = 2 9.15 = -10.20 = 2 10.50 = -14.20 = 2 23.10 = -23.55 +-2 0.00 7.30 +-1 20.10 +-2 22.20 +-2 22.40; ≈ 0.00 23.30 > -11.30 ≈ -20.10 > -22.20
11	0	.	105	V 0.00 14.40 14.40 19.20; = 1.40 2.00 ▥ 1.40 11.40 = 2 11.40 = -14.40 15.50 19.00 ▥ 15.50 19.20; > 14.20 17.40
12	9	.	105	▥ 15.50 24 = 15.20 21.30; +-0 10.20 13.30 +-1 22.00 +-0 24; > 10.00 14.20 ≈ -22.10 > 24
13	8	0.9	101	V 0 14.15 19.05; ▥ 0.00 14.25 = 6.20 7.40 12.25 13.45 = 2 19.05 = -24 ▥ 19.05 24; +-0 0.00-30; > 0.00-10 12.30 22.10 ≈ -24
14	9	2.0	98	V 1.15 3.30 V 2.45 15.50 24; = ▥ 0.00 1.15 = 2 7.45 = -11.20 ▥ 7.45 14.10 = 12.30 15.20 = 2 24; +-0 11.20 24; ≈ 0.00 24
15	8	0.9	96	V 0.00 3.40 20.15 24; = 2 0.00 3.40 = -12.25 ▥ 3.50 20.15 = 18.40 20.15 = 2 24; +-2 0.00 9.30 +-1 24; ≈ 0.00 7.30 > 18.30 ≈ -24; ⊕ 17.40 20.15
16	0	2.4	94	V 0.00 1.30 V 1.20 V 0 8.20 24; = 2 0.00 2.30 ▥ -8.30 = 7.30 8.20 = 2 24; +-1 0.00 2.30 +-0 -21.00 +-2 21.30 24; ≈ 0.00 2.30 > 24 ≈ -24
17	0	5.2	96	*0.45 9.45 X 12.45 *1 14.45 16.30 X 18.30 20.20 22.05 *1 23.45 V 0.00 14.30 V 24; = 2 0.00 24; +-2 0.00 24; ≈ 0.00 24
18	0	5.4	98	*4.35 6.45 *0 18.40 24; V 1 0.00 24; = 2 0.00 24; +-2 0.00 24; ≈ 0.00 24
19	0	1.2	100	*0.00 4.30 5.50 7.15 9.50; V 1 0.00 8.40 V 8 9.40 11.30 14.20 15.40 17.20; 18.20 19.20 22.40 24; = 2 0.00 8.00 = -8.30 = 2 9.40 11.30 14.20 15.40 16.20 = -17.40 18.30 19.20 ▥ 20.30 22.40 = -24; +-1 0.00 1.20 +-0 -13.30; > 0.00 13.30
20	0	4.3	102	*6.50 8.40 12.50 14.20 20.45 22.30; V 0.00 1.30 2.40 3.20 5.30 6.40 8.40 11.30 24; = 0.00 1.30 = 2 2.40 3.20 = 5.30 6.40 8.40 11.30 = 2 24
21	0	0.3	104	*3.50 18.45; V 0.00 24; = 2 0.00 24
22	0	0.7	105	*3.50 4.40 5.50 8.10 14.50; V 0.00 15.10 20.30 24; = 2 0.00 5.30 = -8.10 = 2 -15.10 = -15.30 18.40 20.20 = 2 24; +-0 16.30 24
23	8	0.2	105	*0.50 7.45; V 0.00 4.40 17.20 24; = 2 0.00 4.20 = -5.10 ▥ 8.40 17.20 = 13.30 14.40 15.20 17.20 = 2 24; +-0 0.00 4.30
24	0	0.0	106	V 0.00 4.30 11.20 14.20 16.50 17.50; = 2 0.00 2.30 = -4.30 8.20 11.40 = 2 14.20 = -16.40 = 2 17.50 = -18.30
25	0	1.0	104	*3.10 ..30 22.45; V 3.50 22.50; = 11.15 12.15 = 2 22.30 = -24
26	0	4.4	106	*1.20 10.50; V 3.30 24; = 0.00 3.30 = 2 24; +-0 9.30 11.40 +-0 16.30 +-0 -18.30, 22.20 24; > 23.40 24
27	7	2.5	111	V 0.00 10.15 13.30 14.05 14.45 24; = 2 0.00 10.15 = -13.30 ▥ 10.15 13.30 = 2 14.05 = -14.45 ▥ 14.05-45 = 2 24; +-0 0.00 9.30 +-0 18.30 24; > 0.00 6.40 18.30 24
28	7	0.1	108	V 0.00 2.30 V 1.30 V 1.20 15.40 23.30 24; = 2 0.00 10.20 = -15.40 ▥ 9.20 24 = 22.30 24; +-0 0.00 9.30; > 0.00 22.30 ≈ -24
29	8	.	108	V 0.00 4.40; = 0.00 4.40 ▥ 0.00 1.40 7.30 24; ≈ 0.00 4.40 > -5.30 23.05 24
30	8	0.7	106	*0 13.50 18.30; V 1 11.20 12.30 15.40 24; ▥ 0.00 10.40 = 2 12.30 ▥ -13.30 = 2 21.20 = -24; +-1 14.10 24; > 0.00 5.30 14.10 24
31	0	8.1	107	*4.55 7.30 *-1 8.20 *-0 9.40 12.30 24; V 0.00 7.20 12.30 24; = 0.00 1.30 = -1 7.20 = -12.30 = 2 24; +-1 0.00 1.10 22.40 24; > 0.00 1.10 22.40 24
Σ	-	124.2	-	

Luty – Février

DNI	WIDZALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	0	5.6	117	*0.00 21.40; V 0.00 22.30 24; = 2 0.00 22.30 = -24; +-1 0.00 5.30 +-2 6.20 +-1 -18.30 +-0 -21.30; > 0.00 5.30 ≈ 6.20 > 18.30
2	0	7.6	125	*0 7.45 24; V 0.00 ..10 1.30 3.30 24; = 0.00-10 1.30 3.30 = 2 24; +-1 0.20 5.10 +-2 24; > 0.25 5.10 ≈ -21.40 > 24
3	7	0.9	135	*0.00 9.30 16.55 17.40; V 0.00 9.30 15.30 16.40 17.40 = 2 0.00 9.30 = 15.30 16.40 = 2 17.40; +-2 0.00 4.00 +-1 8.40 +-1 24; > 0.00 8.40; ⊕ 12.30 13.10
4	8	9.6	135	*0.50 24; V 2.30 11.10 ..20 14.40 15.50 24; = 2 3.30 17.10 = -11.20 ▥ -14.40 = -16.50 = 2 24; +-0 0.00 8.40 9.30 11.10 17.40 -22.30 +-1 24; > 17.40 24
5	0	3.2	145	*0.00 3.30 *-7.40 *-0 12.20 13.30; V 0.00 13.40 16.40 17.50; = 2 0.00 13.10 = -13.20 = 2 -17.50 = -18.10; +-1 0.00 7.40 +-0 -8.30 +-0 16.30 20.20 +-1 24; > 0.00 7.40 18.30 24
6	0	10.2	147	*0.45 24; V 1.25 24; = 10.30 11.15 = 0 12.05 = 2 24; +-1 0.00 8.30 +-0 10.30 +-0 15.30 +-0 -21.20 +-0 24; > 0.00 8.30 21.10 24
7	8	28.1	152	*0.00 1.50 17.25 19.20 *-1 24; V 0.00 1.50 20.20 24; = 2 0.00 1.50 = -15.50 ▥ 14.00 15.20 = 2 15.50 16.40 = -17.20 19.00-50 = 2 22.00 = -24; +-0 0.00 15.30 +-1 19.20 +-2 24; > 0.00 2.30 14.20 17.10 ≈ -24 (por. 25)
8	0	15.9	178	*1.00 7.10 *-0 10.30 *-1 16.30 *-0 24; V 0.00 24; = 0.00-30 = 2 24; +-0 0.00 24; ≈ 0.00 24 (por. 40)
9	0	5.0	188	*0.00 20.30 21.50 V 0.00 21.65 = 2 0.00 21.40 = -22.20; +-0 0.00 21.50 +-1 -22.30 +-0 24; ≈ 0.00 22.30 > 24
10	0	11.5	189	*0.15 20.30 X 2.25 *1 22.40 23.05; V 11.10 24; ▥ 5.20 9.30 = 11.30 11.10 = 2 24; +-0 0.00 1.30 +-0 5.25 +-1 7.10 +-2 24; > 0.00 1.30 5.25 9.30 ≈ -24
11	8	.	195	V 0.00 6.15; = 2 0.00 6.15 = -7.30 ▥ 6.15 12.10; +-2 0.00 4.30 +-1 6.30; ≈ 0.00 7.30 > -8.30
12	0	2.6	180	*0.30 11.40 15.40 20.20 23.30; V 7.15 24; = 2 1.40 2.10 = -3.15 = 2 6.40 24; > 10.40 21.30 ≈ 24; +-0 15.30 21.30 +-2 24
13	0	8.3	185	*4.50 24; V 0.00 24; = 2 0.00 24; +-2 0.00 24; ≈ 0.00 24
14	0	12.9	195	*0.00 15.40 17.50 18.30 24; V 0.00 24; = 2 0.00 15.40 = -17.20 = 2 24; +-2 0.00 20.20 +-1 -23.40 +-2 24; ≈ 0.00 20.20 > -23.40 ≈ -24
15	7	1.8	205	*0.00 4.50 8.50 10.15 11.50 15.55 17.30; V 0.00 4.50 5.30 6.10 7.40 9.00 9.40 10.00 13.20 15.20 17.00 24; = 2 0.00 4.50 5.30 6.10 = -7.40 8.30 9.40 = 2 10.40 = -10.00 13.20 15.10 = 2 16.30 = -24; +-2 0.00 6.30 +-1 -10.30 +-0 -15.50 +-1 24; ≈ 0.00 6.30
16	0	5.7	210	*3.30 24; V 0.00 3.30 24; = 0.00 3.30 = 2 24; +-1 0.00-30 +-0 5.30 +-1 13.40 +-0 24; > 0.00-30 5.30 13.40 [15.II: > -8.10 15.50 24]
17	0	8.5	216	*0.00 24; V 0.00 24; = 0.00 24; +-0 0.00 2.40 +-1 -8.00 +-2 24; > 2.40 11.10 ≈ -24
18	0	7.5	220	*0.00 9.40; V 0.00 9.40 11.30 22.30 V 1 24; = 2 0.00 9.40 = -10.00 = 2 24; +-0 0.00 11.30 +-0 24; ≈ 0.00 8.30 > 12.25 ≈ -14.30 > 17.30 ≈ -24
19	8	6.1	220	*10.30 23.40 V 0.00 9.15 V 12.10 15.30 24; = 2 0.00 9.15 = -11.40 9.15 10.04 = 2 11.30 = -15.20 = 2 23.40 = -24; +-0 0.00 8.30 +-1 -24; ≈ 0.00 11.20 > 22.10 ≈ -24
20	0	0.0	225	V 0 14.10 8.25 12.30 18.10; = 0.00 4.10 = 2 8.25 = -12.30 = 2 18.10 ▥ -24; +-1 0.00 22.30 +-2 24; ≈ 0.00 13.30 > 22.30
21	8	.	220	▥ 0.00 24; +-0 0.00 8.30
22	0	6.4	200	*0 8.15 24; V 0 9.15 24; ▥ 0.00 9.25 = 7.40 9.25 = 2 24; +-0 7.20 8.30 +-1 -10.30 +-2 15.10 +-1 -24; > 1.20 10.30 ≈ -15.10 > 24
23	0	4.4	205	*0.00 20.40 21.50; V 0.00 24; = 2 0.00 24; +-1 0.00 11.30 +-0 -12.20; > 0.00 10.30
24	7	3.6	210	*0 5.50 9.05 11.55 1.40 13.50 14.40 19.45 21.30 V 0.00 9.05; 12.20 15.10 16.30 17.10 18.30 21.30 = 2 0.00 9.05 ▥ -12.20 = -15.10 16.30 17.10 ▥ -18.30 = -21.30; +-0 21.30 24
25	0	7.3	210	*0.25 ..30 15.50; V 0.30 3.40 5.25 17.20; = 0.30 3.40 ▥ -6.25 = 2 -6.30 = -17.20 = 2 23.40 24; +-0 0.00-10 +-2 24; ≈ 0.00 24
26	7	2.0	210	*0.50 5.30 6.40, 23.50 24; V 0.00-5.30 6.40, 22.20 23.40 24; = 2 0.00 5.30 = -6.40 ▥ -22.30 = -23.40 = 2 24; +-2 0.00 6.30 +-1 7.40 8.30 +-1 -10.30 +-2 24; ≈ 0.00 6.30 > 8.30 ≈ -24
27	7	12.9	210	*0.00 11.30 21.10 24; V 0.00 7.30 8.40 9.30 11.30 18.40 24; = 2 0.00 7.30 = -8.40 = 2 9.30 = -18.20 = 2 24; +-1 0.00 24; ≈ 0.00 24
28	8	0.3	215	*0.00 3.00 5.50 15.50 19.30 24; V 0.00 3.30 5.50 16.30 24; = 2 0.00 3.30 = -6.20 ▥ 5.50 16.30 = 2 24; +-2 0.00 6.10 +-1 -6.30 +-0 -8.40 +-1 -7.20 +-0 -8.10 ≈ 0.00 6.10 > -7.30
29				
30				
31				
Σ	-	185.9	-	

Śnieżka — φ = 50°44' — λ = 15°44' — Marzec – Mars 1965

DNI	CIŚNIENIE p = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	121.2	119.6	115.8	118.9	-11.2	-8.2	-8.2	-9.0	-8.2	-13.0	85	87	92	87	0.4	0.4	0.2	0.3	6	9	10✳≡	SW 7	SW 8	SW 10
2	111.1	111.1	110.3	110.8	-4.8	-1.4	-5.4	-5.2	-1.3	-9.8	95	99	97	97	0.2	0.1	0.2	0.2	10≡	9	10≡	S 10	SSW 6	SW 8
3	107.7	107.7	110.6	108.7	-4.8	-10.6	-13.4	-10.6	-5.4	-13.4	95	81	88	88	0.2	0.5	0.3	0.3	10✳≡	10✳≡	10✳≡	SW 6	SW 12	W 20
4	112.8	115.1	117.4	115.1	-15.2	-13.4	-14.3	-14.8	-13.4	-16.0	86	86	87	86	0.3	0.3	0.3	0.3	10	10	10	W 24	WSW20	WSW17
5	119.4	122.9	126.1	122.8	-14.0	-11.6	-11.8	-12.3	-9.6	-14.7	83	89	89	87	0.3	0.3	0.3	0.3	8	8	3	WNW 6	WNW 4	N 8
6	126.2	127.6	130.3	128.0	-13.4	-12.0	-11.9	-12.3	-11.4	-13.6	88	89	89	89	0.3	0.3	0.3	0.3	10≡	10≡	10✳≡	N 18	N 20	NNE18
7	132.9	135.0	136.5	134.8	-12.8	-12.6	-12.8	-12.8	-11.8	-14.3	88	81	46	72	0.3	0.4	1.2	0.6	10≡	8	0	NNE16	N 15	N 2
8	135.2	135.3	135.6	135.4	-11.6	-8.3	-12.0	-11.0	-6.6	-13.3	40	86	71	66	1.3	0.4	0.7	0.9	0	1	0	N 2	C 0	NW 4
9	135.0	136.2	136.3	135.8	-13.2	-9.4	-11.0	-11.2	-9.0	-14.5	76	91	90	86	0.5	0.3	0.3	0.4	3	10✳≡	10✳≡	WNW 8	WNW 4	W 14
10	139.0	140.8	142.5	140.8	-13.0	-7.2	-8.8	-9.4	-6.7	-13.3	88	93	59	80	0.3	0.2	1.3	0.6	8	6	0	WNW10	SSW 2	NW 3
11	142.5	143.2	142.3	142.7	-7.4	-4.0	-2.4	-4.0	-2.4	-9.5	68	50	50	49	1.1	2.3	3.6	2.3	0	0	0	C 0	SE 4	S 3
12	141.3	140.6	139.6	140.5	-2.2	0.4	0.6	-0.2	1.1	-3.5	28	35	27	30	3.7	4.1	4.7	4.2	0	0	0	SSE 3	S 6	S 7
13	138.8	139.1	138.9	138.9	1.4	0.6	-1.8	-0.4	2.0	-3.5	27	39	33	33	5.0	3.9	3.6	4.2	0	0	0	S 8	S 5	SSW10
14	138.0	138.5	138.4	138.3	-3.6	2.4	-1.1	-0.8	4.0	-4.3	45	34	91	57	2.6	4.8	0.8	2.7	0	0	4	SW 6	W 1	SW 8
15	138.5	139.0	136.8	138.1	-0.4	0.8	-2.0	-0.9	1.7	-2.1	96	74	98	89	0.2	1.7	0.1	0.7	9	7	10≡	WSW10	WSW 8	WNW16
16	132.7	130.2	132.9	131.9	-1.0	-1.3	-1.4	-1.3	-0.1	-3.7	99	99	99	99	0.1	0.1	0.1	0.1	10≡	10≡	10✳≡	WSW18	WSW22	NW 14
17	133.4	131.8	129.4	131.5	-2.8	-1.2	-2.4	-2.2	-1.1	-3.8	97	99	98	98	0.1	0.1	0.1	0.1	7	10≡	10≡	SW 6	WSW12	W 6
18	126.5	125.9	124.6	125.7	-4.0	-0.7	-2.2	-2.3	0.1	-4.4	91	81	98	90	0.4	1.1	0.1	0.5	8	4	6	WSW12	SW 14	SW 17
19	121.8	127.6	130.8	126.7	-2.9	-2.2	-3.4	-3.0	-0.6	-3.5	97	98	97	97	0.1	0.1	0.2	0.1	10≡	10≡	10≡	WSW22	WNW10	W 8
20	132.4	133.4	131.8	132.5	-6.8	-3.6	-3.8	-4.5	-3.0	-6.9	94	92	96	94	0.2	0.4	0.2	0.3	8	4	10≡	W 8	W 4	SW 12
21	126.3	123.0	124.8	124.7	-4.0	-1.6	-2.0	-2.4	-1.3	-5.2	96	98	98	97	0.2	0.1	0.1	0.1	10✳≡	10≡	10≡	WSW12	WSW20	W 14
22	126.5	130.3	130.6	129.1	-10.8	-8.2	-10.0	-9.8	-2.0	-11.1	90	92	91	91	0.3	0.2	0.3	0.3	8	4	1	WNW 1	NNW 2	NNW 1
23	127.0	124.0	120.1	123.7	-10.4	-3.4	-3.2	-5.0	-3.2	-11.0	90	90	97	92	0.3	0.5	0.1	0.3	6	8	10≡	SSW10	SSW14	SSW20
24	121.8	121.9	124.1	122.6	-1.0	-0.4	-1.0	-0.8	0.0	-3.2	95	100	99	98	0.3	0.0	0.1	0.1	8	9	10≡	WSW10	WSW15	WSW15
25	125.5	128.3	131.3	128.4	-5.0	-4.4	-5.0	-4.8	-0.7	-5.6	95	96	95	95	0.2	0.2	0.2	0.2	10≡	9	10≡	WSW15	WSW12	W 6
26	130.1	126.3	130.1	128.8	-6.6	-5.2	-4.2	-5.0	-3.9	-6.7	94	95	96	95	0.2	0.2	0.2	0.2	10≡	10✳≡	10✳≡	WSW 8	WSW20	WNW 8
27	137.9	142.1	146.1	142.0	-4.6	-4.0	-5.0	-4.6	-3.3	-5.6	96	96	85	92	0.2	0.2	0.6	0.3	10≡	10≡	3	WNW10	NW 8	SW 4
28	145.6	146.5	145.8	146.0	-5.8	0.1	0.6	-0.6	0.6	-5.7	94	100	100	98	0.3	0.0	0.0	0.1	10	10≡	10✳≡	WSW 6	NNW 6	NNW14
29	146.9	147.8	146.9	147.2	0.6	1.0	3.6	2.2	3.8	0.5	100	100	55	85	0.0	0.0	3.6	1.2	10≡●	10≡●	0	NNW16	NNW 3	NNW 6
30	143.3	140.2	139.2	140.9	2.0	3.2	-4.0	-0.7	4.2	-4.2	100	52	96	83	0.0	3.7	0.2	1.3	10≡	6	10≡	NNW14	NNW15	N 22
31	142.0	141.4	139.5	141.0	-7.0	-3.4	-4.8	-5.0	-3.0	-9.6	56	87	98	80	1.6	0.6	0.1	0.8	0	4	10≡	N 12	N 14	N 20
M	130.9	131.4	131.8	131.4	-6.3	-4.3	-5.2	-5.2	-2.9	-8.1	83	84	83	83	0.7	0.9	0.8	0.8	7.1	7.0	6.7	10.4	9.9	10.8

Kwiecień — Avril

1	141.2	143.1	143.6	142.6	-7.8	-6.0	-5.2	-6.0	-5.0	-8.4	93	94	72	86	0.2	0.2	1.1	0.5	9	8	0	N 18	N 20	N 16
2	141.3	142.2	141.7	141.7	-4.6	-0.6	-1.5	-2.0	0.2	-5.7	96	57	58	70	0.2	2.5	2.4	1.7	2	3	1	N 17	N 18	N 18
3	137.7	139.2	136.4	137.8	0.6	3.7	1.0	1.6	4.2	-2.5	29	31	50	37	4.6	5.5	3.3	4.5	6	3	5	N 20	NNW16	WNW20
4	133.6	134.2	133.1	133.6	0.2	3.8	2.1	2.0	4.4	-0.9	56	46	55	52	2.7	4.3	3.2	3.4	2	6	4	NW 16	NW 8	NW 12
5	133.1	136.1	136.0	135.1	-1.6	3.0	2.2	1.4	4.9	-1.6	96	62	67	73	0.2	2.9	2.4	1.8	8	3	0	NW 6	NW 2	W 4
6	136.0	136.1	133.9	135.3	1.4	4.6	2.6	2.8	6.3	0.4	61	58	69	63	2.7	3.6	2.3	2.9	0	2	0	SW 3	WSW 4	WSW 8
7	132.7	132.9	132.2	132.6	0.8	0.2	-1.0	-0.2	3.8	-1.1	96	98	93	96	0.3	0.1	0.4	0.3	10●≡	9	10✳	W 8	WNW 6	W 8
8	130.5	131.1	130.0	130.5	-0.7	1.8	-0.2	0.2	1.9	-1.6	85	86	100	90	0.9	1.0	0.0	0.6	4	9	10≡	W 4	WSW 4	S 15
9	128.0	128.4	128.5	128.3	0.0	1.4	-1.0	-0.2	1.4	-1.5	100	100	99	100	0.0	0.0	0.1	0.0	10✳≡	10≡	10≡	S 12	S 8	NE 6
10	129.4	130.7	130.6	130.2	0.2	-0.8	-0.6	-0.4	1.2	-2.1	96	89	76	87	0.3	0.6	1.5	0.8	8	7	2	ESE 8	ESE 8	S 2
11	128.6	128.3	130.2	129.0	-0.4	0.1	0.2	0.0	1.5	-1.5	78	96	98	91	1.3	0.3	0.1	0.6	2	8	9	WNW 8	N 6	N 8
12	131.0	131.6	131.5	131.4	-1.7	-2.4	-3.4	-2.7	0.2	-3.6	98	98	94	97	0.1	0.1	0.3	0.2	10✳≡	10✳≡	10	N 4	N 8	WNW 3
13	129.6	129.2	130.3	129.7	-2.4	-1.2	-4.5	-3.2	-0.9	-4.8	98	99	96	98	0.1	0.1	0.2	0.1	9	8 ✳	9	SW 8	SW 8	NNW 8
14	132.1	135.0	136.3	134.5	-4.0	-2.0	-3.6	-3.3	-1.9	-4.6	96	98	97	97	0.2	0.1	0.2	0.2	10≡	10✳≡	9	N 8	N 8	N 2
15	135.6	134.8	132.4	134.3	-4.9	-1.8	-2.8	-3.1	0.3	-5.2	90	88	95	91	0.4	0.7	0.2	0.4	3	9	8	W 1	SW 3	SW 8
16	126.7	125.9	128.4	127.0	-3.0	-1.8	-0.8	-1.6	-0.7	-3.3	97	98	99	98	0.1	0.1	0.0	0.1	10≡	10≡✳	10≡	SW 16	SW 16	SW 8
17	129.8	129.4	123.1	127.4	-4.7	-4.0	-3.2	-3.8	-0.7	-5.6	96	91	97	95	0.2	0.4	0.1	0.2	9✳≡	8	10≡	N 10	SW 12	SW 18
18	114.9	118.1	122.5	118.5	-2.0	-1.6	-3.2	-2.5	-0.7	-4.0	98	98	97	98	0.1	0.1	0.1	0.1	10	9	0	SW 18	SW 20	WNW 6
19	122.4	121.6	120.9	121.6	-4.2	-2.4	-3.2	-3.2	-0.8	-4.7	96	91	92	93	0.2	0.4	0.3	0.3	10✳≡	9	10	WSW 2	C 0	N 3
20	119.3	120.9	122.0	120.7	-3.8	-2.6	-1.0	-2.1	-0.3	-4.3	96	98	99	98	0.2	0.1	0.1	0.1	10≡	10≡	10✳≡	N 12	N 10	ENE12
21	121.6	121.5	120.7	121.3	-0.6	-0.2	0.1	-0.2	0.2	-1.5	99	100	100	100	0.0	0.0	0.0	0.0	10✳≡	10≡	10△≡	N 10	N 12	N 14
22	119.2	119.8	119.8	119.6	-0.4	-0.4	-2.2	-1.3	0.2	-2.3	100	100	98	99	0.0	0.0	0.1	0.0	10✳≡	10✳≡	10≡	N 14	WNW12	N 4
23	118.3	119.3	120.9	119.6	-4.2	-3.0	-3.0	-3.3	-1.9	-3.6	96	97	97	97	0.2	0.1	0.1	0.1	10✳≡	10≡	10 △	N 10	N 8	N 12
24	120.4	122.6	125.0	122.7	-4.0	-2.4	-2.6	-2.9	-1.9	-4.8	96	98	98	97	0.2	0.1	0.1	0.1	10✳≡	10✳≡	10✳≡	NW 15	NW 15	NW 14
25	125.1	126.4	127.2	126.2	-3.2	-1.7	-3.2	-2.8	-1.7	-3.5	97	98	97	97	0.1	0.1	0.1	0.1	10≡	10✳≡	10 ✳	NW 15	W 15	NW 7
26	128.1	128.5	125.3	127.3	-3.2	-2.7	-3.0	-3.3	-2.2	-3.6	95	97	97	96	0.2	0.1	0.1	0.1	2	9✳	10✳≡	NW 2	SW 4	SW 14
27	120.5	121.4	121.2	121.0	-4.0	-1.8	-2.3	-2.6	-1.7	-4.5	96	98	98	97	0.2	0.1	0.1	0.1	10≡	10✳≡	10✳≡	SW 12	S 10	S 10
28	119.2	119.8	121.3	120.1	-1.8	-0.8	-3.2	-2.2	-0.6	-3.4	98	99	97	98	0.1	0.0	0.1	0.1	10✳≡	10✳≡	10✳≡	SSE10	E 8	SW 8
29	124.0	126.1	130.1	126.7	-3.6	-2.4	-2.0	-2.5	-1.4	-4.2	97	98	98	98	0.2	0.1	0.1	0.1	10≡	10≡	10≡	SW 12	SW 14	SW 8
30	133.2	136.0	136.8	135.3	-2.6	-1.4	-0.6	-1.3	-0.3	-3.9	89	99	99	96	0.6	0.1	0.0	0.2	9	9	9✳	SE 2	SE 1	N 8
31																								
M	128.1	129.0	129.1	128.7	-2.4	-0.8	-1.6	-1.6	0.3	-3.5	90	89	89	89	0.6	0.8	0.6	0.7	7.8	8.3	7.5	10.0	9.[illegible]	9.5

Śnieżka — $H_s = 1603\ m$ — $H_b = 1610{,}6\ m$ — Marzec - Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	8	2.7	200	*0 00 1 40, 17 30 24, V0 00-05 1 10, 2 30, 16 20 24, =0 00-05 =1 10 2 30, 9 40 16 20 ▥ 8 10 15 30 =2 16 20 24, ⊹0 19 20 22 30 ⊹1-24, ⩥ 19 10 24
2	8	3.0	195	*0 00 2 50, V0 00 9 25 19 05-24, =0 00 9 25 ▥-19 05 =8 35 19 05 =2-24, ⊹0 00 10 30 ⊹0-11 30 ⩥ 0 00 10 30
3	0	5.4	198	*2 45 6 15 x1-15 30 *2-24, V0 00 24, =0 00 24, ⊹0 12 20 15 10 ⊹1-24, ⩥ 12 20 15 10 ⩝-24
4	7	0.0	200	*0 00 5 40 V0 00 1 30 19 10 20 30 =0 00 1 30 =-1 40 3 20 5 40 ▥ 10 20 14 30 =-15 15 ▥-16 45 =-18 30 =0 19 30 20 30 =-21 20, ⊹0 00 24, ⩝ 0 00 24
5	7	0.0	190	= 15 40 16 20 ▥-17 20, ⊹0 00 4 30 ⊹0-6 30, ⩝ 0 00 4 30 ⩥-5 30, ⊕ 9 30 14 40
6	0	12.2	190	*13 45 15 30 *0-24, V1 30 21 30 1-24, = 0 40 6 20 =2-24, ⊹2 6 20 24, ⩥ 1 40-6 20 ⩝-24
7	7	0.5	195	*0 00-3 45 V0 00 15 20 =0 00 11 10 =-16 20 ▥ 11 10 21 40, ⊹0 00 3 30 ⊹1-18 40, ⩝ 0 00-8 40 ⩥-19 30
8	8	.	195	▥ 5 10 24, = 15 15 16 30
9	0	6.6	185	*8 50 15 40-24, V0 30 24, ▥ 0 00 7 30 =2-13 40 =-14 30 =2-24, ⊹0 6 30-15 40 ⊹1-24, ⩥ 9 30 10 40 15 40 24
10	8	.	190	*0 00 6 40, V0 00 7 15, =0 00 6 40 =-7 15 ▥-11 30 =-17 20 ▥-24, ⊹0 00 6 30 ⊹0-7 30, ⩥ 0 00 7 05
11	9	.	180	▥ 0 00-13 30
12	9	.	170	▥ 3 20-24
13	8	.	160	▥ 0 00 11 30, 18 10-23 30 = 18 55 20 40, ⩥ 18 20 22 40
14	9	.	155	▥ 4 30-24
15	8	0.1	150	V0 19 30 21 10, 23 40 24, = 5 45 7 10, 18 10-25 =2-21 10 =-23 20 =2-24, ⩥ 4 30-8 20, 15 40 20 20 ⩝-24
16	0	1.7	140	*0 3 50 5 50 13 40 19 40 21 45 X 23 50 24, V0 00 1 30 3 40 24, =0 00 1 30 =-3 20 =2-24, ⊹0 13 40-24, ⩝ 0 00 17 30 ⩥-18 40 ⩝ 18 10 24
17	0	1.0	142	X4 00-30 *0 8 50 10 30 *2-20 40 21 40 22 20 V0 00 15 7 30 24, =0 00 15 ▥-7 30 =6 35 7 30 =2-9 25 =-11 40 =2-14 20 =-16 40 =2-24, ⊹0 00 4 30, ⩥ 0 00 1 30 10 40 19 30
18	7	0.7	145	V9 00 5 40 16 30 20 30 21 30 24, =0 00 4 40 =-5 40 18 30 19 10 =2-20 30 =-21 30 =2-24, ⊹0 5 40 11 30, ⩥ 2 10 19 30 ⩝-24, ⊕ 13 35 15 50
19	0	0.1	140	V0 00 24, =0 00 15 =-12 40 =2-24, ⩝ 0 00 2 40 ⩥-13 20 14 40 19 30
20	8	1.8	140	*0 15 50 20 45 V0 00 6 20 18 30 21 30 =0 00 4 40 =-6 00 =6 40 21 30 ▥-24, ⩥ 15 30 23 20
21	0	2.9	135	*3 40 5 20 11 40 13 50 15 30 V7 30 24, ▥ 0 00 1 30 =2-23 20 =-24, ⊹15 10 8 20 ⊹2-16 40 ⊹1-23 20 ⊹0-24, ⩥ 5 10 8 20 ⩝-16 40 ⩥-23 20
22	7	0.0	138	*0 15 55 17 45 V0 00 6 40 8 30 =0 00 1 30 =2-6 40 =-8 30 ▥ 6 40 24 =11 40 11 15; ⊹0 00 2 40
23	8	1.4	135	V0 15 30 24, ▥ 0 00 14 20 =-11 45 14 20 15 40 15 10 =2-24, ⩥ 1 30 18 10 ⩝-24, ⊕ 10 40 13 10
24	8	1.0	135	X0 20 05-12 21 04-08 21 50 22 03, V0 00 3 20 21 30 24, =0 00 3 20 =-15 10 =2-24, ⩝ 0 00 1 40 ⩥-8 30 12 30 24
25	7	2.2	130	*0 7 55 10 40 12 50 20 30 23 10-40, V0 00 11 15 21 20-23 10, =0 00 11 15 =-19 40 =2-23 10 =-24, ⊹0 8 30 15 20; ⩥ 0 00 15 10
26	0	6.6	125	*0 17 50 24, V0 30 7 01 8 20 24, =0 00 2 15 =2-7 01 =-7 05 ▥-8 20 =7 15 8 20 =2-24; ⩥ 2 30 5 30 9 40 11 30 ⩝-14 30 ⩥-17 30, ⊹2 13 40 14 20
27	0	0.2	130	*0 00 1 40, V0 00 13 02 =0 00 13 02 =-17 20 ▥ 15 20-18 30, ⩥ 4 40 8 20
28	0	20.2	125	*0 15 40 16 45 17 50 18 25 *0-24, V0 4 20 6 50 8 30 11 30, =1 40 3 20 =2-6 50 =-8 10 =2-24; ⩥ 18 30 21 30 ⩝-22 30 ⩥-24
29	0	0.9	110	*0 00 5 45, 7 30 10 40, =0 00 12 00, ⩥ 0 00-2 30 ⩝-7 15 ⩥-10 40
30	7	0.8	100	= 2 40-3 20 =2-9 05 15 45 16 40 =17 45 18 03 =2-24; ⩥ 2 40 15 15 ⩝-24
31	9	0.1	80	V0 00 2 30 20 30 22 20 24; =0 00 2 30 ▥ 8 15 14 30 =20 30 22 20 =-24; ⩝ 0 00 5 30 ⩥-17 30 ⩝-24
Σ	-	71.9	-	

Kwiecień - Avril

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ SNIEGU h	POGODA
1	8	0.0	75	V0 00 3 30 6 40 7 30 10 40 11 10 12 05; = 0 00 3 30 6 40 7 30 =2-10 40 =-11 10 =2-12 05 = 13 15-45; ⩝ 0 00 24
2	7	.	70	⊔ 13-9, ⩝ 0 00 2 30 ⩥-5 30 ⩝-24
3	8	.	68	⩝ 0 10-24
4	7	.	65	⩝ 0 00 8 30 ⩥-12 20 19 30 24
5	7	.	60	⊔ 0 4-9, = 5 40 9 10, ⩥ 0 00-20
6	7	.	50	⩥ 21 40-24
7	7	0.5	50	•0 8 50 7 10 *0-9 40 X0 10 60 *0 13 50 21 40, =2 5 40 10 50 =-13 20 ▥ 10 55 23 00 = 20 40-24; ⩥ 0 00 1 30
8	7	2.8	48	*0 22 50 24, ⊔ 0 10-7 30 21 40-24, = 0 00-1 40 2 30 6 20 13 15 15 40 =2-24, ⩥ 15 30 24
9	0	3.0	50	*0 00 5 40 *0-9 30 •0-12 45, V0 00 7 30 15 10 21 30, =0 00 22 10 ▥ 22 10-24, ⩥ 0 00-11 30
10	8	.	48	= 13 40-16 20 ▥ 0 00 24, ⩥ 7 40-11 20
11	8	2.4	48	▥ 0 00 13 10 = 12 15 13 30 =2-14 05 =-18 15 =22 10 23 30 =-24, ⩥ 4 40 6 20, ⊔ 18 50 20 30
12	0	4.6	49	*0 50 7 05 16 10 19 30, V0 30 17 20 18 40 23 30 24, = 0 00 3 10 =2-17 30 =-18 40 ▥-23 30 =2-24, ⊹0 7 30 13 20; ⩥ 7 10 12 20, ⊔ 19 30 22 30
13	7	1.0	52	X0 12 47 13 05 14 00-28 *4 40 15 20 *0-5, *5 35 16 30 17 05 *2-17 30 *0 10 15, V0 00 5 10 7 30 8 10 11 30 16 30 19 30 21 45 24, =0 00 5 10 =-7 30 8 10 11 30 12 15 13 30 14 30 15 10 =2-10 30 =-24 (X) 14 25 15 05, ⊹0 19 30 24
14	0	1.4	55	X0 1 55 13 08 15 04 16 45 V0 00 20 30 23 40 24, =0 00 24 =2-3 30 =-4 30 =2-20 30 ⊹0 00 20 ⩥ 0 00 20 ⊔ 21 10-24
15	7	0.1	57	*0 23 50 24, V0 20 3 30 23 30 24, V0 20 3 30 23 30 24, =2 13 30 =2-20 40 21 30 =2-24, ⩥ 22 00-24, ⊔ 0 00 1 30
16	0	8.1	57	*0 00 2 45 12 47 18 45, V0 00 24, =0 00 24, ⊹0 12 47 19 00, ⩥ 0 00-1 10, 2 40 5 20 ⩝-16 00 ⩥-19 30
17	8	6.3	60	*0 10-50 *1-5 40 23 00 24, V0 00 6 20 11 20 21 50 24, =0 00 6 20 =-6 40 ▥-19 30 =10 10 20 20 =2-24, ⊹0 1 20 6 30 ⊹1-10 40 ⊹2-15 30 ⊹1-24, ⩥ 6 20 8 40 10 10-18 20 ⩝-24
18	7	1.9	65	*0 00-1 00 8 40 10 50, V0 00 10 30 =0 00 10 30 =-15 20 =0 16 00 17 00 =-18 30, ⊹0 00 14 40 ⊹0-15 40, ⩝ 0 00 8 40 ⩥-10 20 ⩝-14 40 ⩥-16 20
19	7	0.6	67	*0 50 2 40 7 30 9 00 ⊹0-11 00, V3 40 11 55 =2 3 40 11 55 =-12 20 ▥-24 =-24
20	0	15.8	67	*0 3 50 11 40 13 50 16 20 17 40 18 00 21 30 24, V5 30 24, = 0 00 5 20 ▥ 0 00 5 10 =2 5 20 24, ⩥ 1 30-13 40 20 00 24
21	0	34.7	77	*0 00 1 40 6 50 8 40 ⊹0 17 40 18 05 •1-10 30 •2-20 15 ⊹0-22 30 ⊹1-23 25 ⊹0-24, V0 00 14 30 22 30 24, =0 00 24, ⩥ 0 00-30 4 20-24
22	0	33.2	75	⊹0 00 2 15 3 30 5 40 *11 50 8 00 ⊹0-9 40 *0-10 30 ⊹0-12 20 *0-15 40 ⊹0-17 50 *0 19 30 20 20, V0 00 24, =0 00 24, ⩥ 0 00 13 20
23	0	8.5	95	*3 30 10 30 11 45 ⊹0 14 00 24, V0 00 24, =0 00 24, ⊹0 3 30 11 30 ⊹0-13 30 ⊹1-24, ⩥ 0 00 11 30 13 30 24
24	0	5.6	100	⊹0 00 13 30 *4 30 6 00 16 40 17 45 24, V0 00 13 30 3 15 15 10 40 17 40 24, =0 00 13 30 =-3 15 =2 15 10 =-15 40 =2 17 40 24, ⊹0 00 24, ⩥ 0 00 24
25	0	2.8	105	*0 00 4 40 10 10 14 45 16 50 22 30 24, V0 00 6 30 13 30 20 30 22 15 23 30 =0 00 16 30 =17 25 18 30 =2 20 20 =-22 15 =2 23 30 =-24, ⊹0 00 6 30 ⊹0-17 00, 19 30 24, ⩥ 0 00 16 30
26	7	2.2	106	*0 00 1 30 X0 7 50 13 15 15 20 16 03 *1-17 45 *2-22 40, V4 45 5 10 8 30 40 9 10 13 40 14 15 15 30 24: = 0 00 1 30 4 45 5 10 ▥ 4 30 9 10 =0 30-40 9 10 13 40 14 15 15 30 =2-24, ⊹0 00 5 30 15 30-24 (X) 0 50 16 03
27	0	9.2	108	*0 7 50 14 00 *1-24, V0 00 2 00 22 30 24, =0 00 2 00 =-21 40 22 30 23 10 =2-24, ⊹0 00 24, ⩥ 0 00 18 10 20 40-24
28	0	7.6	115	*0 00 7 10 X0 11 55 13 10 *0 13 14 14 23 *0 20 45 24 (X) 0 51 13 15 14 25 NW, V0 00 24, =0 00 24, ⊹0 00 24, ⩥ 0 00 18 30 22 20 24, (X) 0 13 15 14 40
29	0	.	115	*0 00 4 40 V0 00 24, =0 00 24, ⊹0 00 1 30 ⊹1-5 50 ⊹1-24, ⩥ 0 00 1 30 ⩝-5 50 ⩥-18 10
30	7	0.3	110	*0 10 40 11 50 *1 18 30 15 20 20 30 21 10, V0 00-20 22 40 24, =0 00-20 =-1 15 9 10-10 30 =2-11 40 =-15 20 =2-17 10 =-17 40 =2-20 30 =-21 10 =2-24, ⊹0 00-30
31				
Σ	-	172.4	-	

Śnieżka — $\varphi = 50°44'$ — $\lambda = 15°44'$ — *Maj – Mai 1965*

DNI	CIŚNIENIE P = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	137.3	137.3	136.8	137.1	-0.8	-0.4	-0.1	-0.4	0.2	-1.7	99	90	98	96	0.0	0.6	0.2	0.3	10 ≡	6	10	WNW 6	N 12	N 10
2	136.7	137.7	135.7	136.7	-5.6	-0.2	-5.8	-2.8	0.3	-5.4	71	100	92	88	1.4	0.0	0.4	0.6	1	4	0	NNE 6	NNE 2	N 10
3	136.8	135.4	135.0	135.7	-4.6	-1.4	-2.9	-3.0	0.4	-4.7	69	64	77	70	1.3	2.0	1.1	1.5	0	1	0	NNE 2	NE 3	SE 3
4	133.7	132.1	128.1	131.3	-1.2	2.0	1.2	0.8	2.8	-3.3	66	68	100	78	1.9	2.3	0.0	1.4	5	7	10 • ≡	SW 9	WSW18	WSW20
5	126.5	125.8	126.7	126.3	1.0	1.4	0.3	0.8	2.4	0.2	100	96	100	99	0.0	0.3	0.0	0.1	10 ≡	8	10 * ≡	W 10	WNW 8	NW 14
6	126.8	128.4	131.5	128.9	-0.2	-0.8	-0.8	-0.6	1.4	-1.0	100	99	99	99	0.0	0.0	0.0	0.0	10 * ≡	10 ≡	10 ≡	NW 14	NNW18	NNW12
7	132.4	133.6	132.3	132.8	-2.8	0.4	-0.3	-0.8	0.4	-2.9	97	100	100	99	0.1	0.0	0.0	0.0	10 ≡	8	10 △ ≡	NW 15	W 6	SW 14
8	131.1	133.3	136.3	133.6	1.5	1.4	1.2	1.3	2.4	-0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 ≡	9 •	WSW16	WNW 8	NW 12
9	133.6	131.5	124.2	129.8	3.0	4.2	-1.6	1.0	4.8	-1.9	100	100	98	99	0.0	0.0	0.1	0.0	10 • ≡	10 • ≡	10 ≡	WSW18	WSW18	W 30
10	123.4	122.1	121.5	122.3	-2.0	-1.8	-2.2	-2.0	-1.5	-2.3	98	98	98	98	0.1	0.1	0.1	0.1	10 * ≡	9	10 * ≡	W 18	WNW16	NW 28
11	121.9	126.4	134.3	127.5	-1.8	-1.8	-1.0	-1.4	-0.9	-2.7	98	98	99	98	0.1	0.1	0.1	0.1	10 * ≡	10 * ≡	10 * ≡	NW 20	NW 20	WNW15
12	139.2	140.2	142.1	140.5	-1.2	0.3	1.6	0.6	1.6	-1.6	99	100	100	100	0.1	0.0	0.0	0.0	9	10 ≡	10 ≡	W 6	NW 9	NW 14
13	140.9	142.1	140.9	141.3	0.8	2.2	1.8	1.6	3.2	0.6	100	96	100	99	0.0	0.3	0.0	0.1	10 ≡	7	9	NNW14	NNW 8	NNW14
14	136.9	136.9	135.6	136.5	2.0	4.1	3.3	4.2	5.8	0.9	100	100	95	98	0.0	0.0	0.4	0.1	10 ≡	10 ≡	9	NNW14	NW 12	NNW10
15	134.2	134.4	133.0	133.9	5.0	8.5	8.8	7.8	9.3	4.6	100	77	39	72	0.0	2.6	6.8	3.1	10 ≡	9	8	NW 6	NW 3	WNW 8
16	131.2	132.6	132.1	132.0	7.0	9.3	6.8	7.3	10.2	5.6	89	74	94	86	1.1	3.1	0.6	1.6	8	8 (K)	6	W 16	W 10	W 14
17	131.7	131.6	128.0	130.4	5.8	9.2	7.6	7.6	9.9	5.0	97	58	96	84	0.3	4.9	0.4	1.9	9	7	8 • K	W 14	WSW16	NW 24
18	128.6	130.5	129.6	129.6	6.8	5.8	5.2	5.8	8.2	4.4	100	100	85	95	0.0	0.0	1.3	0.4	10 ● ≡	10 ● ≡	9	SSW18	SSW18	SSW12
19	126.4	124.4	128.3	126.4	4.8	4.0	-3.0	-0.3	8.3	-3.0	91	100	93	95	0.7	0.0	0.3	0.3	7	10 • ≡	10	W 8	WNW 4	N 18
20	133.2	136.8	138.7	136.2	-4.6	-3.6	-4.6	-4.4	-2.7	-3.0	96	97	96	96	0.2	0.2	0.2	0.2	10 △ ≡	9 *	4	NW 10	WNW 8	WNW 6
21	142.3	143.6	144.1	143.3	-4.8	-1.5	-1.7	-2.4	0.3	-3.6	88	90	90	89	0.5	0.6	0.6	0.6	4	8	6	W 8	NNW 2	SW 2
22	143.0	142.5	140.3	141.9	-2.0	2.8	1.0	0.7	4.2	-3.3	85	77	90	84	0.8	1.8	0.7	0.8	2	6	7	SE 8	ESE 6	E 8
23	136.3	136.0	135.7	136.0	1.8	1.0	4.0	2.7	4.0	0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 • ≡	10 • ≡	ESE25	SE 14	E 10
24	135.4	135.7	136.5	135.9	4.4	5.2	4.0	4.4	5.5	3.0	100	97	100	99	0.0	0.2	0.0	0.1	10 ● ≡	9	10 ≡	SW 2	N 4	N 3
25	135.7	137.0	137.8	136.8	3.8	5.6	2.8	3.2	4.0	2.8	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 ● ≡	10 ≡	WNW20	NW 14	NW 12
26	137.6	137.2	136.4	137.1	2.6	2.2	1.2	1.8	3.4	1.1	100	95	100	98	0.0	0.6	0.0	0.2	10 ● ≡	9	10 ≡	NW 10	NNW 8	WNW10
27	133.2	134.5	134.5	134.1	0.6	1.4	2.2	1.6	3.6	0.1	100	100	87	96	0.0	0.0	1.0	0.3	10 ● ≡	10 ≡	6	SW 16	WSW 6	W 3
28	132.4	131.7	129.9	131.3	1.8	2.6	4.2	3.2	4.2	1.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 • ≡	10 • ≡	E 8	NE 8	NE 14
29	126.4	126.1	127.6	126.7	3.0	3.0	1.8	2.4	4.2	1.7	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 • ≡	10 • ≡	N 12	N 14	N 25
30	128.9	130.0	129.7	129.5	-3.0	-0.8	-0.7	-1.3	1.9	-4.1	97	95	95	95	0.1	0.4	0.3	0.3	2	4	5	N 12	N 4	S 5
31	129.2	130.0	129.0	129.4	1.6	2.1	3.2	2.3	3.5	-1.2	77	98	100	92	1.6	0.1	0.0	0.6	8	10 ≡	10 • ≡	SW 4	S 6	S 3
M	133.0	133.5	133.3	133.3	0.8	2.1	1.3	1.4	3.4	-0.7	94	92	94	93	0.3	0.7	0.3	0.3	8.2	8.4	8.3	11.3	9.8	12.4

Czerwiec – Juin

1	124.2	126.2	128.6	126.3	4.2	3.0	0.2	1.9	4.4	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 • ≡	10 ● ≡	S 8	WSW10	WSW15
2	130.7	133.0	137.6	134.4	-1.0	-0.3	1.6	0.3	2.3	-2.0	99	100	82	94	0.1	0.0	1.2	0.4	10 ≡	10	4	W 20	NW 8	NW 4
3	138.1	138.8	138.4	138.4	2.0	7.4	5.2	5.0	9.6	1.0	66	62	98	75	2.4	3.9	0.1	2.1	1	8	10 ≡	W 1	NW 1	SE 8
4	138.0	137.7	135.5	137.1	4.8	4.4	4.0	4.3	5.3	3.5	97	100	100	99	0.3	0.0	0.0	0.1	10	10 ● ≡	10 • ≡	SE 6	SE 6	S 8
5	132.3	131.3	130.3	131.4	4.6	7.0	6.2	6.0	8.0	4.0	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 • ≡	10 • ≡	N 6	NE 5	N 8
6	128.2	129.0	131.5	129.6	4.2	4.2	4.0	4.1	6.2	3.8	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 • ≡	10 ≡	N 10	NNW10	N 10
7	133.3	133.6	132.9	133.3	3.8	5.6	5.2	5.0	5.8	2.6	91	97	85	91	0.7	0.3	1.3	0.8	7	9 •	2	N 8	SSW 4	SSW10
8	131.7	132.4	131.3	131.8	5.2	8.0	8.2	7.4	9.5	4.7	100	94	100	98	0.0	0.6	0.0	0.2	10 ≡	8	10(K) ≡	SW 18	S 10	S 12
9	129.2	130.0	129.0	129.4	4.6	6.8	5.0	5.4	8.5	2.6	100	97	100	99	0.0	0.3	0.0	0.1	10 • ≡	10 ≡	9	S 14	S 2	N 14
10	129.1	131.2	131.4	130.6	3.6	5.8	5.2	5.0	6.8	3.0	100	97	98	98	0.0	0.3	0.1	0.1	8	9	10 • ≡	N 3	N 4	N 6
11	129.7	130.8	133.0	131.2	5.6	6.1	5.4	5.6	6.8	5.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ≡	N 14	N 15	N 16
12	134.4	136.6	136.9	136.0	2.4	3.6	0.8	1.9	5.4	0.3	100	100	98	99	0.0	0.0	0.2	0.1	10 • ≡	10 ● ≡	9	N 16	N 12	NW 12
13	136.7	136.7	136.0	136.3	3.6	4.6	3.6	3.8	5.8	0.7	95	100	100	98	0.5	0.0	0.0	0.2	8	10 ≡	10 ≡	NW 12	NW 4	NW 8
14	135.7	138.6	139.1	137.8	2.4	4.8	3.2	4.4	6.4	1.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	NW 12	NW 14	NW 12
15	139.9	141.1	140.1	140.4	3.2	7.2	7.2	6.7	9.9	4.7	100	92	94	95	0.0	0.8	0.6	0.5	9	9	4	NNW 3	NNW 2	S 4
16	139.0	137.9	133.9	136.9	7.6	11.1	9.0	9.2	12.4	5.8	79	68	74	74	2.1	4.2	3.1	3.1	2	8	3	WNW14	SW 16	SW 20
17	125.9	127.4	130.3	127.9	7.4	4.2	2.0	3.9	9.0	1.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 • ≡	10 ● ≡	SW 22	SW 15	WNW25
18	135.5	136.3	136.8	136.2	1.2	5.4	6.8	5.0	7.0	0.3	91	77	100	89	0.7	2.1	0.0	0.9	5	9	10 ≡	NNW20	SW 8	SW 15
19	136.0	137.7	139.4	137.7	7.8	6.6	5.4	6.3	8.7	5.4	100	83	73	86	0.0	1.6	2.2	1.3	10 ● ≡	8	3	SW 14	W 16	WNW20
20	141.9	142.9	142.6	142.3	4.4	7.8	7.6	6.8	9.8	3.6	85	72	68	75	1.3	3.0	3.3	2.5	6	8	9	NNW10	SW 6	W 6
21	142.1	141.9	139.7	141.2	7.2	11.3	11.9	10.6	14.6	7.0	79	70	10	53	2.2	4.0	12.3	6.2	8	8	3	NW 4	W 3	S 8
22	136.6	136.8	135.6	136.3	11.2	13.0	13.7	12.9	16.0	9.6	90	92	100	94	1.4	1.3	0.0	0.9	3	9	10(K) ≡	SW 14	SW 12	SW 10
23	135.2	137.3	139.1	137.2	7.4	8.2	8.4	8.1	13.8	5.9	100	86	84	90	0.0	1.6	1.7	1.1	10 ≡	9	2	W 13	WSW12	W 8
24	139.7	142.3	142.8	141.7	9.6	11.3	11.1	10.8	13.8	8.0	77	74	71	74	2.7	3.3	3.7	3.3	6	8	4	W 16	W 14	W 14
25	143.1	143.9	143.3	143.3	8.8	12.9	14.7	12.8	16.2	8.1	80	72	60	71	2.2	4.2	6.7	4.4	2	8	0	W 12	SW 8	W 8
26	143.1	144.3	145.0	144.1	13.1	18.3	12.9	14.8	19.3	12.9	80	67	99	82	3.6	6.8	0.2	3.3	1	7	10(K) ≡	SW 6	SW 14	WNW 6
27	144.1	143.8	142.3	143.3	12.1	13.7	7.6	10.2	14.6	7.4	96	88	100	93	0.3	1.9	0.0	0.8	9	9	10 ● ≡	WSW10	SW 8	N 8
28	142.9	143.3	144.9	144.4	3.8	3.8	3.6	3.7	7.6	3.2	100	91	91	94	0.0	7.0	0.7	2.6	10 ≡	7	2	N 8	N 14	WNW12
29	142.6	144.1	143.4	143.4	5.4	8.6	6.6	6.8	9.8	2.8	88	96	100	93	1.1	0.3	0.0	0.3	4	10	9	N 15	N 6	NW 8
30	142.9	142.2	138.3	141.1	10.1	14.3	11.3	11.8	15.6	6.1	36	60	89	62	8.0	6.6	1.6	5.4	0	2	1	W 2	W 3	W 10
31																								
M	136.1	137.1	137.0	136.7	5.8	7.6	6.7	6.7	9.6	4.1	91	88	89	89	1.0	1.8	1.3	1.4	7.3	8.8	7.1	11.1	8.7	10.8

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ DU h	POGODA
1	8	•	98	V 0^00 8^20 ⌴ 0^22 – 24; ≡ 0^00 3^20 ≡ – 9^10; ≫ 9^30 21^30
2	9	•	95	⌴ 0^00 7; ≫ 18^30 24
3	8	•	90	≫ 0^00 14^0
4	8	3.1	88	• 16^30 .. 17^20 – 24; ≡ 16^40 – 24; ≫ 8^30 12^20 ⌫ – 24; ⊕ 11^20 13^40
5	8	3.5	78	• 0^00 1^50 ⌫ 15^15-22 17^20 18^00 ⌫ 18^10 ⌫ 18^30 ⌫ 20^00-30 ⌫ 20^40 ⌫ 21^30 ⌫ 20 ⌫ 23^10-25; ≡ 0^00 5^30 ≡ – 6^40 ≡ 17^15 ≡ – 13^10 ≡ 14^20 16^45 ≡ – 19^15 ≡ 24; (K) 15^10 16^10 (K) 17^50 .. 18^30 K 20^35 .. 21^50 K 23^10 .. 30.
6	0	0.3	75	△ 5^20-35 ⌫ 7^10 △ 16^15-55; V 18^30 13^30 .. 35 15^20 16^50 18^30 24; ≡ 0^00 13^30 ≡ – 15^30 ≡ 15^50 ≡ – 18^10 ≡ 24; ⌫ 0^00 8^30 ⌫ – 10^20 ≫ – 24 **5.V:** ⌫ 0^00 2^40 ≫ – 7^20 15^30 24
7	7	2.2	75	⌫ 10^05-45 △ 11^10 ⌫ 12^00 △ 13^40 14^0 △ 15^10 K 15^15 K 15^40 16^50 17^00 K 20^00; V 10^00 7^10 17^15 23^30 ≡ 0^00 7^10 ≡ – 10^00 10^15 12^20 14^45 15^10 17^05-15 ≡ 24; (S) 11^45 12^00 (S) 15^10 .. 25; ⌫ 16^15 22^30; ≫ 0^00 8^30 16^15 24
8	0	2.7	70	• 0^00 0^50 15^45 20^10 – 21^50; ≡ 0^00 16^30 ≡ – 17^10 ≡ – 20^10; ≡ – 24; ≫ 0^00 2^30 ⌫ – 7^15 ≫ 17^50 24
9	0	13.3	60	• 6^20-35 • 9^30 • 11^00 15^10 ⌫ 15^40 ▲ 17^20 15^40 ⌫ – 19^30; K NSW 15^35 18^40 ENE; V 19^30 24; ≡ 0^00-30 ≡ – 24; (S) 16^10 18^40; ≫ 0^00-30 ⌫ – 24
10	7	16.4	60	⌫ 0^00 2^40 ⌫ – 5^45 ⌫ 7^20 ⌫ 8^30 ⌫ 11^30 ⌫ 14^00-45 ⌫ 15^10 15^25 17^45 18^35 19^25 20^10 ⌫ 21^00 ⌫ 22^00 ⌫ 23^40 ⌫ 24; V 0^00 11^40 15^40 24; ≡ 0^00 11^40 ≡ – 15^30 ≡ – 24; (S) 18^45-50; 19^05-20; 19^35 20^10; 21^40-45; ⌫ 0^00 1^00 ⌫ – 5^30
11	0	37.4	70	⌫ 0^00 4^30 ⌫ – 5^20 ⌫ 7^40 ⌫ 8^30 17^40 18^20 19^30 22^40; V 0^00 24; ⌫ 0^00 24; ⌫ 0^00 18^30 ⌫ – 24; ⌫ 0^00 18^30 ≫ – 24 **10.V:** ⌫ 0^00 13^30 ≫ – 15^10 ⌫ – 24 (por. 35)
12	0	0.0	90	V 0^00 8^30; ≡ 0^00 6^40 ≡ – 7^30 ≡ – 24; ⌫ 0^00 4^00; ≫ 0^00 4^30 19^20 23^25 ⌫ – 24
13	7	5.8	80	≡ 0^00 8^40 ≡ – 10^30 ≡ 15^40 16^45 ≡ – 20^40 21^30 24; ⌫ 0^00 1^30 ≫ – 11^40 18^30 24
14	0	0.0	75	• 0^45 2^00 5^40 .. 6^50; ≡ 0^00 1^40 ≡ – 13^25 ≡ – 15^30 ≡ – 19^10 ≡ 18^00 19^10 ≡ – 20^30 ≡ 21^00 22^15 ≡ 21^30 24; ≫ 0^00 1^40 5^30 9^00 12^30 21^50
15	6	2.0	70	⌫ 15^20 16^35 ≡ – 19^00 21^30 ≡ 22^20 ≡ – 9^05 ≡ – 17^00 ≡ 9^40 12^00 13^20 16^30 ≡ 21^40 22^10 ≡ – 22^46 ≡ – 23^15 ≡ – 24; ⌫ WNW 20^10 – 21^40 NW; ≫ 22^00 – 24
16	6	2.2	50	• 0^15 2^15 ⌫ 7^40-55 ⌫ 8^20 ⌫ 15^15 ≡ 1^00 1^45 ≡ – 2^40 ≡ 3^00 ≡ 5^10 7^20 ≡ 8^15 – 5^30 7^20 ≡ 8^15-35 ≡ 8^15 14^15 ≡ 15^10 15^30 ≡ 22^25 24; (K) ⌫ NE 17^45 13^45; (K) ⌫ W 14^50 (K) ⌫ 15^30 (K) ⌫ 15^25 SE; (S) ⌫ 14^50 .. 16^10;
17	8	0.5	40	⌫ 19^40 20^30 ⌫ – 22^20; ≡ 0^00-30 ≡ 2^40 5^05 ≡ – 11^40 18^05-30 ≡ – 20^40 ≡ 21^05-20 ≡ – 24; K SW 19^45 21^45 NE; ≫ 0^00-30 3^30 8^20 ⌫ – 24 **16.V:** ≫ 0^00 5^40 ⌫ – 9^30 ≫ 13^30 18^40 24; ⊕ 13^45 15^35
18	0	4.4	35	⌫ 13^10 15^40 • 16^45 18^50 ⌫ 21^30 22^20 ≡ 1^00 14^20 ≡ – 17^00 19^40 20^20 ⌒ 14^40 15^15 ⌫ 0^00 20^20 ≫ – 21^40 ⌫ – 24; ⌫ 21^40 22^20
19	0	25.5	30	• 0^40 5^40 ⌫ 6^40-45 ⌫ 8^30 ⌫ – 8^50 ⌫ 10^25 ⌫ 11^20 ⌫ – 12^20 ⌫ 13^30 ⌫ – 13^20 ⌫ – 13^30 ⌫ – 15^30 ⌫ – 16^40 ⌫ 18^40 V 18^30 20^45; ≡ 3^20 5^30 m 7^20 8^35 ≡ – 8^35 ≡ – 10^20 ≡ – 11^35 ≡ – 12^30 ≡ – 13^25 ≡ – 20^25 ≡ – 20^45; ⌫ 17^30 22^40 (S) 11^20 12^10
20	7	0.6	25	△ 17^15-30 △ 18^20 ⌫ 19^30 ⌫ 11^37 – 16^20 17^30-40; V 2^20 9^30 12^40 15^20; ≡ 0^30 2^20 ≡ – 9^30 ≡ – 15^20 15^40 17^40 18^30 19^20; ⌫ 0^00-20 ≫ – 7^40 **10.V:** (S) 2^0 12^40 (S) 1^0 .. 13^20 14^10-35 ⌫ 0^00 20^20 ≫ – 3^30 14^15-40 ⌫ – 24
21	7	0.5	25	⌫ 0^45 9^42 ⌫ – 9^50 ⌫ 11^01 ⌫ 11^35 12^15-45 13^45-55 14^20-35 15^05 16^15 17^20-45; ≡ 4^40 5^20 8^30 11^20 18^20 20^20 22^50 24
22	8	0.2	25	≡ 12^30 23^40 24; ⌴ 1^2 – 12^00; ≫ 21^30 24
23	0	9.8	20	• 0^15 15^30 • 0^17^50 • 0^45 • 2^40 21^30 • 24; ≡ 0^00 1^30 ≡ – 24; ≫ 0^00 1^30 ⌫ – 5^30 ≫ – 15^30 19^10 – 21^50
24	7	11.4	pz.	• 0^00 5^30 • 1^45 ⌫ 13^00 .. 25 14^15-45 ⌫ – 15^40 • 16^45 ≡ 2^00 12^00 ≡ – 13^50 ≡ – 15^15 ≡ – 15^25 ≡ – 15^55 ≡ – 15^58 17^20 20^00 ≡ – 24; (K) ENE 13^35 SE 14^10 S 14^40 SE 14^45 (S) 11^10 .. 15^10
25	0	5.9	pz.	• 2^00 3^00 • 1^30 • 5^40 ⌫ 10^22 18^50 ≡ 0^00-15 ≡ – 3^00 ≡ – 24; ≫ 6^50 24
26	8	4.5	pz.	• 0^55 9^40 ⌫ 10^10 ⌫ 11^55 12^15 ⌫ 12^20 ⌫ 12^00 ⌫ 12^20 ⌫ 12^30 ⌫ 12^40-50 ⌫ 13^20 ⌫ 13^45 ⌫ 13^40 ⌫ 14^05 ⌫ 14^40 ⌫ 15^45 ⌫ 16^20-35 ⌫ 16^45 ⌫ 16^35-30 ▲ 18^50-42 ⌫ 16^45-50 ⌫ 19^00 .. 19; 19^40 20^30; ≡ 0^00 8^55 ≡ – 9^35
27	0	0.1	pz.	≡ 0^00 14^50 ≡ – 22^00 ≡ – 23^25 ≡ – 24; ⌫ 0^00 8^40 ≫ – 11^00 **26.V:** ≡ – 12^00 12^30 13^10 ≡ – 14^00 ≡ – 14^00 ≡ – 15^10 ≡ – 16^10 ≡ 16^35 ≡ – 16^50 ≡ 17^15 ≡ – 19^35
28	0	70.7	pz.	⌫ 12^40 15^10 ⌫ – 16^40 • 18^10 • 22^00 • 24; ≡ 0^00 3^30 ≡ – 3^40 ≡ – 5^20 ≡ – 24; ≫ 13^20 24 ≡ – 18^20 ≡ – 24; K E 11^55 N 12^00 NE 12^45 K W 13^12 N 14^20 NNW 14^45 W 15^40 K NNE 16^20 N 17^20 NW
29	0	92.6	pz.	• 0^00 2^15 • 2^40 • 2^35; V 23^15 – 24; ≡ 0^00 24; ≫ 0^00 14^40 ⌫ – 24 18^20 (S) 11^55 12^15 13^12 14^20 16^25 .. 30 (S) 16^20 17^00 (S) 17^40 19^10 ≫ 0^00 7^15 17^20 23^20 ⌫ – 24;
30	8	0.0	pz.	V 0^00 4^40; ≡ 0^00 4^40 ≡ – 5^20 m 4^40 11^30 ⌫ 0^00 6^30 ≫ – 10^30 < E 12^05-10 W 13^12 NNW 14^40 NE 15^25-30 NW; ⌒ 14^15-27
31	0	16.6	pz.	⌫ 11^15 12^15 • 13^50 .. 22^30 24; V 0^00 2^30; ≡ 0^30 2^30 11^10 13^30 ≡ – 14^30 ≡ – 24; (S) 11^40 .. 12^30
Σ	–	325.6	–	

Czerwiec – Juin

1	0	10.4	pz.	• 0^00 5^10 • – 9^20 • – 13^50; V 22^40 24; ≡ 0^00 24; ≫ 10^30 24
2	7	1.0	pz.	⌫ 0^50 .. 1^50 7^20 8^10; V 0^00 0^40; ≡ 0^00 0^40; ≫ 0^00 1^30 ⌫ – 9^30 ≫ – 12^00
3	8	•	pz.	≡ 20^40-50 ≡ – 24
4	0	15.2	pz.	• 14^50 15^30 24; ≡ 0^00 4^00 ≡ – 7^20 ≡ – 24; ≫ 0^40 4^30
5	0	12.1	pz.	• 0^00 1^40 5^30 .. 13^30 15^10 24; ≡ 0^00 13^55 ≡ – 15^05 ≡ – 24; ≫ 21^00 24
6	0	12.0	pz.	• 0^00 .. 14^40 15^10 .. 17^50; ≡ 0^00 22^30 ≡ – 24; ≫ 0^00 24
7	7	0.1	pz.	⌫ 0^0 11^55 13^40; ≡ 0^00 2^40 5^40 6^20 8^35 17^25 ≡ – 18^30 ≡ – 18^50 21^10 22^20 ≡ – 23^15 ≡ – 24; ≫ 0^00 6^20; 20^20 – 22^30 ⌫ – 24
8	7	11.4	pz.	⌫ 0^0 13^25-40 16^45 17^20 ▲ 18^20-25 ⌫ 0^0 18^25 21^00 ≡ 0^00-30 0^00-35 ≡ – 2^40 ≡ – 10^20 17^40 18^20 ≡ – 17^30 18^40 ≡ – 10^10 ≡ – 24; K S 16^20 N 17^55; K S 18^25-20^20 (K) S 20^10 N 21^55; ⌫ 0^00 9^40 ≫ – 10^40 17^20 – 24
9	0	11.5	pz.	• 0^00 6^40 ⌫ 8^30 • – 9^20 ⌫ 10^25 10^40; ≡ 0^00 2^40 ≡ – 3^30 4^40 5^20 ≡ 10^40 ≡ – 12^00 ≡ – 14^40 ≡ – 15^20 ≡ 19^40 ≡ – 21^00 ≡ – 24; K N 18^55 S 19^40 (K) S 20^50; (S) 6^40 8^30 18^05 21^50 ≫ 0^00 8^30 ⌫ – 6^40 ≫ – 9^10 21^00 24
10	7	8.4	pz.	⌫ 13^55 14^07 17^20 18^05 20^55 21^00; ≡ 0^00 4^0 ≡ – 11^40 ≡ 12^30 ≡ – 17^30 ≡ – 24; ≫ 0^00 1^30
11	0	50.5	pz.	⌫ 10^15-17 16^40 17^10 ⌫ 18^40 ⌫ 19^25 19^10 19^00 20^40 ⌫ 21^45 22^00 ⌫ – 23^30; ≡ 0^00 24; ≫ 5^30 14^30 ⌫ – 24
12	0	4.7	pz.	• 0^30 7^10 • – 9^40; ≡ 0^00 13^05 ≡ – 21^30 ≡ – 24; ⌫ 0^00 12^00 ≫ – 15^30 19^10 22^10 ⌫ – 24
13	0	5.2	pz.	⌫ 7^33-37; 9^40 10^45 15^30 16^10 ⌫ ▲ 16^50-53 ⌫ – 17^15; ≡ 0^00 6^25 ≡ – 7^30 ≡ – 24; ⌫ 0^00 6^10 ≫ – 8^10
14	0	0.2	pz.	⌫ 0^45 7^10; ≡ 0^00 17^05 ≡ – 19^30 ≡ – 23^30 ≡ – 23^30; ≫ 5^30 24
15	7	1.4	pz.	• 0^05 2^50 ▲ 7^50 11^02 ⌫ 11^55 .. 13^15 13^45 17^10 19^15-20; ≡ 0^00-35 ≡ 0^00 2^55 ≡ – 14^20 16^30 19^10 23^30 24; (K) ESE 9^00 – S 14^55; ≫ 0^00 1^30
16	7	0.1	pz.	≡ 0^00 1^30 ≡ – 3^00 ≡ 22^00 24; ≫ 3^00 4^40 5^30 17^00 ⌫ – 24
17	0	2.5	pz.	• 2^50 15^20 16^30 17^40 18^30 19^20; ≡ 0^00 2^00 ≡ – 24; ⌫ 0^00 9^30 ≫ – 21^00 ⌫ – 24
18	8	1.4	pz.	≡ 0^00 1^30 ≡ – 7^20 ≡ 15^30 24; ⌫ 0^00 7^20 ≫ 15^30 24
19	8	2.4	pz.	• 7^15 10^40; ≡ 0^00 8^50 ≡ – 10^40 ≡ 23^40 24; ≫ 0^00 5^10 ⌫ – 6^30 ≫ – 9^40 ⌫ – 14^20 ≫ – 17^40 ⌫ – 24
20	7	•	pz.	≡ 0^00 5^40 ≡ – 6^20; ⌫ 0^00 3^10 ≫ – 8^10
21	7	•	pz.	≫ 21^30 – 24
22	7	9.6	pz.	⌫ 17^00-30 ⌫ 22^00 23^40 m 4^40 7^00 ≡ – 8^40 13^30 19^00 ≡ – 24^40; (K) W 21^55 K 22^00-10 – (K) E 23^40; (S) 20^50 24; ≫ 0^00 24
23	8	•	pz.	≡ 0^00 8^30 ≡ – 10^0 < W 10^00-40; < E 10^00-40; ≫ 0^00 15^30 21^30 24
24	8	•	pz.	≡ 17^30 18^30; ≫ 0^00 2^40 ⌫ – 7^40 ≫ – 13^30 19^40 – 24
25	7	•	pz.	≫ 0^00 – 8^40
26	7	0.2	•	⌫ 17^00 .. 50 15^25 16^10 ≡ 15^35 .. 40 18^30 20^40 ≡ – 23^30 ≡ – 24; K NSW 15^35 16^10 (K) S 18^30 ESE 17^30; (K) NNW 20^20 22^30; ≫ 9^40 15^25 ⌫ – 17^30 ≫ – 18^20; (S) 1^0 20^40 21^10
27	7	0.1	•	⌫ 7^20-25 8^10 ⌫ 9^35 ≡ 0^00 7^10 ≡ 12^00 ≡ 13^40 15^10 ≡ – 17^40; ⌫ 4^40 12^10
28	7	•	•	≡ 0^00 2^30 3^40 10^30 ≡ – 17^00; ≫ 0^00 24
29	7	•	•	≡ 5^40 8^30 12^30 – 13^40 14^15 – 21^00; ≫ 0^00 11^10
30	8	0.1	•	m 1^30 – 4^10 ≡ 22^30 – 24; ≫ 21^00 – 24
31				
Σ	–	154.5	–	

Śnieżka — φ = 50°44' — λ = 15°44' — Lipiec – Juillet 1965

DNI	CIŚNIENIE P = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	155.4	156.5	156.2	156.0	9.9	9.7	5.8	7.8	11.9	5.7	85	100	97	94	1.9	0.0	0.3	0.7	9	10 ≡	9	W 16	W 10	W 10
2	155.4	155.3	154.0	154.9	5.2	6.2	4.0	4.4	7.8	3.0	91	81	93	88	0.7	1.8	0.3	1.0	10	8	10	N 4	NW 4	W 12
3	151.6	151.7	152.5	151.9	3.0	1.3	1.3	1.7	4.0	1.3	100	100	81	94	0.0	0.0	1.3	0.4	10 • ≡	10	6	WNW12	WNW 6	WNW13
4	151.4	151.4	151.2	151.3	1.0	1.2	1.6	1.4	2.5	0.2	83	96	90	90	1.2	0.3	0.7	0.7	9	8	8	WNW10	W 3	NW 4
5	150.6	151.4	153.0	151.7	0.4	2.4	1.1	1.2	3.2	0.2	100	93	79	91	0.0	0.6	1.4	0.7	10 * ≡	9	4	NW 4	NW 3	NW 12
6	153.2	154.4	155.4	154.3	-0.4	1.4	2.0	1.2	2.2	-0.6	100	100	96	99	0.0	0.0	0.3	0.1	10 *	10 • ≡	9	W 17	W 20	W 20
7	155.3	154.4	154.2	154.6	3.2	5.9	8.7	6.6	8.9	1.7	100	100	74	91	0.0	0.0	3.0	1.0	10 ♀ ≡	10 ≡	5	W 15	SW 17	SW 14
8	129.6	128.7	127.4	128.6	6.5	6.4	4.2	5.3	9.0	3.8	96	100	100	99	0.5	0.0	0.0	0.2	9 •	10 • ≡	10 ♀ ≡	SW 18	SW 8	SW 25
9	128.7	132.2	134.4	131.8	0.4	0.8	2.2	1.4	4.4	-0.1	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡	10 ≡	9	W 25	W 20	SW 17
10	134.2	135.9	137.4	135.8	1.0	1.6	2.2	1.8	3.3	0.5	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡	10 ≡	10	SW 15	WSW10	W 10
11	139.5	140.6	140.5	140.2	1.8	5.2	6.2	4.8	6.3	0.9	86	88	97	90	1.0	1.0	0.3	0.8	7	8	9	WNW10	SW 6	SW 10
12	138.5	136.5	136.8	137.3	7.2	8.2	9.4	8.6	10.1	6.0	97	100	100	99	0.3	0.0	0.0	0.1	9	10 • ≡	10 • ≡	W 20	SW 20	W 18
13	138.7	140.3	140.9	140.0	9.3	11.5	12.9	11.6	14.2	8.4	100	88	80	89	0.0	1.8	3.0	1.6	9	8	7	W 14	W 6	SW 9
14	141.9	143.3	142.6	142.6	14.1	17.3	15.1	15.4	18.6	11.9	71	65	82	73	4.7	6.9	3.2	4.9	5	6	1	SW 5	SW 6	SW 6
15	142.8	143.3	143.0	143.0	12.3	15.4	14.3	14.2	16.4	11.4	90	85	71	82	1.4	2.6	4.9	3.0	9	8	8 (K)	SSW10	NE 1	E 2
16	140.9	140.3	139.6	140.2	14.2	11.5	11.7	12.3	15.2	10.4	82	73	90	81	2.9	4.0	1.4	2.8	7	9 • K	9	NE 4	S 10	S 3
17	138.3	137.8	136.5	137.5	10.3	11.0	10.1	10.4	12.8	9.5	89	96	100	95	1.3	0.5	0.0	0.6	9	9 • K	10 ♀ ≡	N 2	C 0	N 9
18	136.2	137.4	139.8	137.8	9.4	7.6	7.6	8.0	10.6	7.2	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 • ≡	10 • ≡	N 9	WNW15	N 12
19	140.8	142.0	142.0	141.6	7.6	9.3	9.6	9.0	10.3	5.8	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ♀ ≡	N 12	NNE 2	SE 8
20	140.5	140.6	137.9	139.7	8.2	11.1	10.3	10.0	11.6	7.4	79	94	100	91	2.4	0.8	0.0	1.1	7	9	10 ≡	SE 11	S 6	WSW15
21	134.8	133.9	133.8	134.2	10.1	10.2	8.5	9.3	10.8	8.3	100	100	99	100	0.0	0.0	0.2	0.1	10 ♀ ≡	10 • K ≡	9	WSW12	WSW10	SW 9
22	134.3	133.3	134.4	134.7	6.5	8.4	9.9	8.7	10.7	5.8	91	90	80	87	0.9	1.1	2.5	1.5	3	8	7	SW 8	SW 8	SW 4
23	132.0	133.2	133.3	132.8	8.6	7.3	8.1	8.0	9.9	6.8	100	100	91	97	0.0	0.0	1.0	0.3	10 (K) ≡	10 ♀ ≡	2	WSW 4	W 8	W 8
24	132.9	134.4	136.3	134.6	7.6	9.6	8.4	8.3	11.2	7.3	90	73	69	78	1.1	3.0	3.4	2.5	8	7	1	WSW20	WSW16	W 10
25	136.2	136.7	134.8	135.9	6.2	8.6	9.4	8.4	10.6	5.6	73	93	93	88	2.4	0.9	0.6	1.3	8	10	8	WSW12	W 6	SW 20
26	135.1	134.8	135.1	135.0	4.2	7.8	4.6	5.3	9.8	4.0	91	72	93	85	0.7	3.0	0.6	1.4	8	8	10 • ≡	WSW17	SW 10	SW 8
27	133.2	134.9	135.7	134.6	3.4	3.7	4.1	3.8	5.5	1.6	100	100	98	99	0.0	0.0	0.2	0.1	10 • ≡	9	10 • ≡	WSW14	WSW17	WSW10
28	135.7	135.9	135.6	135.1	3.0	3.0	3.8	3.4	4.6	1.8	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	9	10 ≡	WSW14	WSW22	WSW30
29	132.1	130.5	127.6	130.1	5.2	7.2	6.8	6.5	7.4	3.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ♀ ≡	10 ♀ ≡	10 ♀ ≡	WSW16	SW 17	WSW20
30	123.6	124.9	126.9	125.1	5.3	5.4	5.2	5.3	6.9	3.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ♀ ≡	8	10 ≡	WSW25	WSW25	W 18
31	126.5	124.4	128.9	126.6	5.0	7.6	2.1	4.2	7.9	2.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ♀ ≡	10 ♀ ≡	W 12	SW 20	WNW18
M	134.8	135.3	135.4	135.2	6.1	7.2	6.8	6.7	9.0	4.7	93	93	92	93	0.8	0.9	0.9	0.9	8.9	9.1	8.1	12.3	10.7	12.4

Sierpień – Août

1	152.1	153.2	153.1	152.8	2.1	5.2	4.8	4.2	6.9	0.6	79	83	77	80	1.4	1.3	2.0	1.6	5	8	9	W 7	W 5	WNW 2
2	151.3	153.0	153.5	152.6	2.6	5.0	4.3	4.2	5.4	0.4	83	80	79	81	1.2	1.7	1.7	1.5	7	6	3	N 15	WNW12	NNW 7
3	152.1	151.5	153.3	152.3	3.4	4.6	4.7	4.4	5.4	3.0	91	70	100	87	0.7	2.6	0.0	1.1	9	9	10 ≡	WNW 9	SW 13	W 13
4	155.2	158.5	159.8	157.8	5.0	5.6	5.6	5.4	7.8	4.0	100	92	92	95	0.0	0.7	0.8	0.5	10 ♀ ≡	9 •	4	WNW20	W 11	WNW13
5	142.1	143.9	144.0	143.3	6.4	9.8	10.2	9.2	11.8	3.4	93	81	91	89	0.4	2.3	1.1	1.3	9	8	0	W 14	W 6	SW 7
6	141.9	142.4	141.9	142.1	11.8	15.7	14.5	14.1	17.9	10.0	70	76	68	71	4.1	4.3	5.4	4.6	6	3	8	SW 16	SW 12	SW 16
7	140.1	140.6	141.0	140.6	12.3	17.1	15.1	14.9	17.9	11.4	93	67	87	84	0.2	6.6	2.3	3.0	10 ♀ ≡	3	4	SW 16	SW 11	SW 7
8	139.9	140.3	140.9	140.4	13.3	13.9	11.7	13.2	16.6	11.7	54	91	100	82	8.0	1.5	0.0	3.2	2	9	10 ≡	NW 3	N 6	W 1
9	140.3	140.2	141.1	140.3	6.0	6.3	5.4	4.8	11.9	3.3	100	97	98	98	0.0	0.3	0.1	0.1	10 •	10 ♀ ≡	9	WNW 6	W 1	N 6
10	140.3	142.1	141.9	141.3	3.4	4.2	3.4	3.6	4.8	2.4	98	97	100	98	0.1	0.2	0.0	0.1	10 ♀ ≡	9	10 ≡	N 11	WNW 7	N 11
11	141.9	142.6	142.7	142.4	2.0	3.0	3.0	2.8	4.7	1.3	100	93	100	98	0.0	0.6	0.0	0.2	10 ≡	8	10 ♀ ≡	N 11	NW 6	N 6
12	142.3	144.0	143.0	143.2	2.6	4.8	4.2	4.0	5.8	1.6	100	83	100	93	0.0	1.3	0.0	0.4	9	8	10 ≡	N 8	N 8	N 9
13	141.6	143.1	142.3	142.4	2.6	4.2	4.0	3.7	6.3	1.3	100	72	91	88	0.0	2.3	0.7	1.0	10 ≡	4	9	WNW12	N 4	N 4
14	140.9	141.4	140.7	141.0	3.8	5.8	4.9	4.8	7.0	2.1	59	83	82	73	3.3	1.6	1.6	2.2	0	7	9	N 5	NNW 3	NNW 3
15	139.9	141.8	141.7	141.1	2.4	4.6	3.8	3.6	5.2	2.2	90	93	88	90	0.7	0.6	1.0	0.8	4	9	7	N 8	N 4	N 1
16	140.9	140.9	140.2	140.7	4.4	6.2	5.9	5.6	7.4	3.2	88	81	76	82	1.0	1.8	2.2	1.7	5	9	5	N 2	C 0	C 0
17	139.4	140.7	140.6	140.2	6.0	8.2	8.2	7.6	11.4	3.2	78	83	78	80	2.1	1.9	2.4	2.1	8	7	6	WNW 2	W 4	WNW 6
18	141.4	142.3	142.7	142.3	8.2	10.7	10.0	9.7	12.8	7.0	69	63	73	68	3.3	4.8	3.3	3.9	3	3	1	N 5	SW 4	NW 3
19	143.4	147.3	147.0	146.6	10.0	14.1	11.7	11.9	15.4	8.6	74	60	73	69	3.3	6.4	3.3	4.4	1	5	0	NNW 5	NNW 2	WNW 1
20	143.9	144.9	142.0	144.3	11.3	13.7	11.1	11.8	14.6	10.6	60	56	71	62	3.5	6.8	3.8	3.4	0	3	0	S 1	SW 4	WNW12
21	139.3	138.7	133.9	138.0	11.3	12.4	11.2	11.6	12.7	9.3	72	76	81	76	3.8	3.4	2.6	3.3	8	3	8	SW 6	SW 8	SW 16
22	132.6	129.0	128.3	130.0	9.4	12.9	10.9	11.0	14.6	9.3	93	64	91	83	0.6	3.4	1.2	2.4	4	6	9	SW 20	S 23	S 20
23	129.2	130.8	132.0	130.7	9.9	12.6	9.9	10.6	13.1	8.9	92	83	100	92	1.0	2.2	0.0	1.1	7	8	10 • ≡	S 12	SSW10	SW 5
24	132.1	133.4	132.4	132.6	9.2	9.8	8.2	8.8	9.9	8.1	100	100	100	100	0.0	0.0	0.0	0.0	10 • (K) ≡	10 • ≡	10 • ≡	C 0	SW 2	NW 3
25	130.3	131.6	133.3	131.8	6.6	3.0	4.6	3.2	8.2	3.8	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 •	10 ≡	NNW10	NW 8	W 17
26	134.8	136.0	136.0	135.6	0.3	2.2	1.8	1.6	4.6	0.2	100	83	100	94	0.0	1.2	0.0	0.4	10 ♀ ≡	7	10 ≡	SW 17	NW 7	NW 12
27	134.7	134.3	133.1	134.7	1.4	4.2	3.8	3.3	3.4	1.1	100	81	81	87	0.0	1.3	1.3	1.0	10 ≡	9	7	WNW12	NW 3	NNW 2
28	134.9	137.4	138.2	136.8	1.3	3.2	2.6	2.4	4.0	0.8	94	84	87	88	0.4	1.2	1.0	0.9	10 • ≡	9	3	WNW 5	WNW 5	WNW 6
29	136.7	136.2	136.0	136.3	1.6	4.9	3.0	4.1	6.1	1.4	96	80	100	92	0.3	1.8	0.0	0.7	8	9	10 ≡	W 6	NW 10	NW 8
30	136.2	137.1	138.0	137.1	3.3	3.2	3.2	3.0	3.0	2.2	63	87	73	82	1.1	1.0	2.1	1.4	6	7 •	0	NNW 9	W 12	W 13
31	137.1	135.7	133.3	135.4	2.8	7.0	3.2	3.0	7.3	2.3	80	69	100	83	1.3	3.1	0.0	1.3	0	8	10	W 7	NW 7	SSW12
M	137.9	138.3	138.5	138.3	5.8	7.8	6.8	6.8	9.3	4.8	87	81	88	85	1.4	2.3	1.3	1.7	6.8	7.3	6.8	9.0	7.0	7.9

DNI	WIELKOŚĆ DZIAŁU V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	1.0	•	•0 3⁵⁰ 4⁴⁵ 7¹⁰ 8³⁰ 10¹⁰ = 0⁰⁰ 3¹⁰ = ² 4²⁰ = -4³⁵ ▥ 4³⁰ 7²⁰ = -11³⁰ = ¹ 15²⁰ = -21⁴⁰ = ² 22³⁵ = -24, ≫ 0⁰⁰ 3³⁰ ≈ -9³⁰ ≫ -13³⁰, 15¹⁰ -22³⁰
2	8	0.9	•	= ⁰10⁰⁰ 4²⁰ = 7⁵⁰ 10²⁰ 21¹⁰ 24, ≫ 19²⁰ 24
3	7	1.1	•	•0 4⁴⁰ 6³⁰ 12⁴⁵; = 0⁰⁰ 12⁰ = ² 12³⁰ = -13⁰⁵, ≫ 0⁰⁰-20 ≈ -5²⁰ ≫ -9³⁰, 13³⁰ 24
4	7	1.2	•	•0 11²⁵-20 ✕0 11⁰⁵ 15⁴⁰ ⚥0 11²⁰ ✕¹ 11²⁷ ⚥0 11⁰² ✕¹ 12⁰⁰ ⚥¹ 12⁴⁶ ✕0 13²⁰-35 ⚥+13⁴⁰-50 ⚥0 13⁵⁵ 14¹⁰ ⚥² 14²⁵ ⚥¹ 14⁴⁰ 15²⁰-35 = ² 17⁰⁵ 18⁰⁵ = 23⁰ 23³⁰ ▥ 5³⁰ 9²⁰ = 9¹⁰ 10²⁰ = ² 10⁵⁰ = -17³⁵, ≫ 0⁰⁰ 7⁴⁰
5	7	1.7	•	✕0 6¹⁰-20 ✕¹ 6⁴⁵ ✕0 7²⁵ ... 45 ⚥0 8¹⁰ ... 36 ✕0 8⁴² ✕¹ 9⁰⁵-35 ✕0 10¹⁰-22 11³⁰-42 12⁰⁵-20 14⁰⁴-17 ✕¹ 14³⁶-45 ⚥0 15³⁵-41 ✕0 16⁰⁵-35 = 4¹⁰ 6⁰⁵ = ² 10⁵ = -18⁴⁰ = ² 15⁴⁰ 17⁰², 22¹⁰ 23³⁰ = -24, (☇) 0 15⁴⁵ 16³⁰.
6	0	2.2	•	✕0 6⁴⁰ 7³⁰ ✕¹ 8⁵⁰ ⚥0 12⁰⁴ 13¹⁰ 15¹⁵-30 ✓0 15³⁰ 16¹⁰ 18⁰⁵ 21⁰ = 0⁰⁰ 1⁴⁰ = ² 6¹⁰ = -7²⁵ = ¹ 9³⁰ = -9⁴⁰ = ² 16¹⁵ = -21²⁰ = ² 24, ≫ 0⁰⁰-25 ≈ -24 **5.VII: ≫ 18³⁰ 24**
7	0	0.6	•	⚥0 5⁵⁵ 6⁰⁵ •0 7²⁰ 10⁴⁵ = ² 0⁰⁰ 13³⁰ ≈ 0⁰⁰ 14⁰⁰ ≫ -7³⁰ ≈ -18³⁰ ≫ -22¹⁵ ≈ -24
8	0	17.6	•	•0 5⁴⁵ 7¹⁰ 8⁵⁰ ⚥0 11⁴⁵ 15³⁰ •0 17⁴⁰ 18⁵⁰ = 6¹⁰ 7³⁰ = ² 9²⁰ = -11³⁰ = ² 18⁴⁰ = -19²⁰ = ² 24, (☇) 0 7⁵⁰ 8¹⁰ 12³⁰ 14²⁰ ≈ 0⁰⁰ 14³⁰ ≫ -15⁰⁵ ≈ -20⁰⁰ ≫ -17³⁰ 14⁴⁰ 18⁵⁰ ≈ -23⁴⁰ ≫ -24
9	0	1.2	•	△0 10⁵⁰ 11¹⁵ ⚥0 11³⁰ 13⁴⁰-75 ✕¹ 19⁵⁵-57 = ² 0⁰⁰ 4²⁰ = -5⁴⁰ = ² 9⁴⁰ = -9¹⁰ = ² 19³⁰ = -15²⁰ 21⁴⁵ 21³⁰ ≫ 0⁰⁰ 3³⁰ ≈ -13³⁰ ≫ 21³⁰ ≫ -22⁴⁰ ≫ -24
10	0	4.7	•	⚥0 7¹⁰ 8¹⁵ ⚥² 8⁴⁰ 11⁴⁵ 12¹⁰ 15¹⁵-40 ⚥¹ 19⁵⁰ = 0⁰⁰ 5³⁰ = ² 13⁴⁰ = -18⁴⁵ = ² 18⁴⁰ = -19³⁰ 20²⁵ 23¹⁰ = ² 24, (☇) 0 WNW 18⁰⁵ ☇0 18⁵⁵ 19³⁰ E, ≫ 0⁰⁰ 10³⁰, 12¹⁰ 15⁴⁰ 18⁴⁰ 24
11	7	1.0	•	⚥0 7²⁵-35 14⁵⁵ 15⁰¹. = ² 0⁰⁰ 1³⁰ = -2⁰⁰ 7⁴⁰-50 = ² 11⁴⁵ 14³⁰ 18⁴⁰ = -19³⁰, 20¹⁰ 21³⁰ = ² 24, ≫ 0⁰⁰ 7³⁰, 10¹⁰ 11¹⁵, 16⁴⁰ 24
12	0	12.2	•	⚥0 5⁰⁵-17 •0 11⁴⁰ 12⁴⁰ •¹ 17¹⁵ •0 24, = ² 0⁰⁰ 3³⁰ = -4¹⁵ = ² 5¹⁰ = -10⁰⁵ = ² 24, ≫ 0⁰⁰ 3³⁰ ≈ -24
13	7	•	•	•0 0⁰⁰-10 ... 50, = ² 0⁰⁰ 10 = -3¹⁰ = ² 4⁴⁰ = -7¹⁰ = ² 7²⁰ = -10¹⁰, ≈ 0⁰⁰ 6²⁰ ≫ -10¹⁰
14	8	•	•	< WNW 21¹⁵⁵ - N 24, ≫ 23¹⁰-25 ≈ -24
15	7	•	•	= 0³⁰ 13³⁰ = ² 15³⁰ = -17⁴⁰ ▥ -18⁴⁵ = -19¹⁰ ▥ 19³⁰ = -19⁴⁵ = ² 20³⁰ ▥ -21⁴⁵ = ² 21²⁵ = -22³⁰ < N 0⁰⁰ N 1⁵⁰ < NW 2⁴⁰ WNW 4¹⁰ (K) NE 13⁴⁵ E 17³⁰ (K) ⁰ ENE 19³⁰ WNW 22⁴⁵ ≈ 0⁰⁰-10 ≫ -11⁵ 15³⁰ 7¹⁰
16	7	14.9	•	⚥0 9⁴⁵ 10⁰⁰ 11³⁵-50 ⚥¹ 12⁴⁰ ⚥0 15¹⁰ •0 17⁰⁵-15 = 0³⁰ 13³⁰ = ² 23³⁰ ▥ -5³⁰ = 7⁴⁰ 9⁴⁵ = ² 10⁰⁵ = -10⁴⁵ = ² 11¹⁰ = -11³⁰ = ² 12⁰⁵ = -13⁴⁰ ▥ 15⁴⁰ 17⁴⁰ = -19³⁰ 20⁴⁰ 22¹⁰ 23¹⁰-40 = ² 24, (K) ⁰ SW 7⁴⁵ (K) ¹ 9⁴⁵ 10⁴⁰ (K) 15 10¹⁰
17	7	37.7	•	•0 1⁵⁰ 4⁴⁰ 6³⁰ ⚥0 10⁵⁵ 11⁰⁷ ⚥¹ 11¹⁰ ⚥² 14⁴⁵ 17⁰⁵-25 = ² 0⁰⁰ 1⁵⁰ = -3³⁰ 7⁴⁰ 10¹⁰ = ² 12⁴⁵ = -13³⁰ = ² 24, (K) ⁰ SW 11⁵⁰ 12⁵⁰ W 14⁴⁵, (☇) ⁰ 18⁴⁵ ... 46
18	0	35.5	•	•0 0⁰⁰-08 ¹ 0²⁵ •0 0⁰ ¹ 0³³ ¹ 0³⁰ •¹ 1⁴⁵ 5⁴⁵-24, = ² 0⁰⁰ 24, ≫ 9⁴⁰ 24 **10.VII: (K) ⁰ 11⁵⁵ (K) ¹ 11⁵⁰, (K) ⁰ 12⁴⁰ 15¹⁰ (K) ⁰ 15⁴⁰ (☇) ⁰ 16⁴⁰ E, (☇) ⁰ 19⁵⁰ 20³⁰ (☇) ⁰ 14⁵⁰, ≫ 11⁵⁰ 14²⁰**
19	0	4.2	•	•0 0⁰⁰ 1⁴⁰ ⚥0 12¹⁵-48, = ² 0⁰⁰ 14³⁰ = -15⁴⁵ = ² 18⁵⁰ 19⁴⁵, 21, ≫ 0⁰⁰ 8¹⁵
20	7	10.9	•	⚥0 14⁵⁵ 15¹⁰ 15⁴⁰-15 17⁴⁰ 18³⁰ = ² 0⁰⁰ 3¹⁰ = -4⁴⁰ 8¹⁰-30 = ¹ 10²⁰ = -14⁵⁰ = ² 15⁴⁰ = -16²⁰ = ² 22⁴⁰ = 23⁴⁰ 24, (K) ⁰ ESE 14⁴⁰ (K) ⁰ 14⁵⁵ 15³⁰ (K) ⁰ 15³⁰ (K) ⁰ 17⁴⁰ 18³⁰ (K) ⁰ 20³⁰, ≫ 4³⁰ 7²⁰, 20²⁰ 24
21	0	8.3	•	⚥0 9⁴⁰ 10³⁰ 11⁴⁰ 12⁴⁵ 13⁴⁰ ⚥¹ 13⁴⁰ ⚥0 14⁴⁰ 15⁵⁰ 20¹⁴⁵, = 0⁰⁰ 1⁴⁰ = ² 13²⁰ = -14⁵⁰ 15¹⁰ = ¹ 17¹⁵ 18³⁰ 20¹⁰ = -21¹⁰ = ² 24, (K) ⁰ E 3⁴⁰ ENE 5³⁰, (K) ⁰ E 12⁴⁰ W 14²⁵, ≫ 0⁰⁰ 13³⁰, 22¹⁰ 24, (☇) ⁰ 12¹⁵, 14⁴⁰
22	8	7.1	•	= ² 0⁰⁰ 3³⁰ = -4¹⁰ 9¹⁰ 14¹⁰ 23²⁰ 24, ≫ 0⁰⁰ 6³⁰ 8⁴⁰ 12¹⁰
23	0	2.9	•	⚥0 5²³-27 ⚥² 5⁵⁰ ⚥¹ 6¹⁰ ⚥² 6¹⁵ ⚥0 6⁴⁵ 7¹⁵ 8¹⁴, = 0⁰⁰-30 = ² 1⁴⁰ = -4¹⁰ = ² 8¹⁰ 9⁴⁵ 10⁴⁰ = 13⁴⁰ 14¹⁰, (K) ⁰ NE 5¹⁰ NE 6⁴⁰ (K) ⁰ NE 7¹⁰, ≫ 14¹⁰ 15²⁰, (☇) 15¹⁵-20
24	8	0.0	•	⚥0 7³⁰ 20⁵ 7³⁰-35 = ² 23⁰ 6²⁰, 20⁴⁰-50 = ² 1⁴⁰ = -10³⁰, < SE 21⁴⁰ 24, ≫ 7²⁰ 8¹⁰ ≈ -15³⁰ ≫ -24, ∩ 6⁴⁵ 7⁰⁰
25	8	0.2	•	⚥0 17⁵⁵ 18²⁰, = ² 17⁴⁰ 20¹⁰ = -21¹⁵ = ² 23¹⁰ = -24, < SE 0⁰⁰-20 SE, (K) ⁰ W 18⁴⁰-50 E < ⁰ NE 21⁰⁰, 22⁴⁰, (☇) ⁰ 17⁴⁰ 18³⁵ ≫ 0⁰⁰ 3²⁰ ≈ -6¹⁰ ≫ -7⁴⁰, 10²⁰ 11¹⁵, 17¹⁵ 19³⁰ ≈ -23²⁰ ≫ -24
26	8	8.1	•	•0 19⁵⁵ 20²⁰ ⚥¹ 20²⁷ ⚥² 21⁴⁰ ⚥¹ 21²⁵ ⚥0 23¹⁵, = 0⁰⁰-30 6¹⁰ 7⁵⁰ = ² 20⁴⁵ 21⁴⁰ = 22⁴⁰ 24, ✕² 20²⁵ 21¹⁰, ≫ 0⁰⁰ 8²⁰ ≈ -7³⁰ ≫ -18²⁰, 22¹⁰ 24
27	7	11.1	•	•1 18⁵⁰ 19⁵⁰ ⚥0 19⁴⁰-45 15¹⁰-30 ⚥¹ 15⁴⁵ ⚥0 17³⁰ •0 21⁰⁰ 21⁰⁵ ... 45, 22²⁵ 23²⁵ ✕0 23¹⁰ •0 24, = 0⁰⁰ 1⁵⁰ = ² 5⁵⁵ = -9²⁵ 11³⁰ = ² 12⁰⁰ = -14²⁵ = ² 15³⁰ = -16¹⁰ = ² 18¹⁵ = -19²⁰ = ² 24, ≫ 0⁰⁰ 7²⁰ ≈ -5⁵⁰ ≫ 8¹⁰ ≈ -13³⁰
28	7	2.0	•	•0 0⁰⁰-02 5⁵⁰ 9²⁰ 10⁴⁰ 12⁵⁰, = 2⁰⁰ 12⁴⁰ = -13⁴⁰ = ² 15³⁰ = -16⁴⁰ = ² 24, ≈ 0⁰⁰ 5¹⁰ ≫ -9¹⁰ ≈ -24 **27.VII: ≫ 15⁴⁰ < 20³⁰ ≫ -21⁰⁰ ≈ -22⁵⁰ ≫ 23⁰⁵ ≈ -24, (☇) ⁰ 15⁴²-49 ✕ 23⁴⁵-52**
29	0	6.4	•	•0 8³⁵ 9⁵⁰ 14²⁵ 15⁴⁸ 18⁰⁵...50 19⁴²-46, = ² 0⁰⁰ 15¹² = -18⁴⁰ 19⁴⁵ = ² 24, ≈ 0⁰⁰ 7⁴⁰ ≫ -8³⁰ ≈ -24
30	7	2.1	•	•0 4²⁰ 6⁰² ⚥0 14⁴⁰-40 15⁵⁵-20 ⚥0 15²⁵ 16⁵⁰ 17¹⁰, = ² 0⁰⁰ 9⁴⁰ = -15³⁰ 14²⁰ 16³⁰ = ² 18²⁰ = -19⁴⁰ = ² 24, ≈ 0⁰⁰ 24, (☇) ⁰ 11⁵⁰-50 14¹⁰-40 (☇) ⁰ 15¹⁵-45, ∩ 15²⁵-40
31	0	12.6	•	•0 6⁴⁵ 9³⁰ 10¹⁵ •¹ 11⁴⁵ ⚥0 13⁴⁰ 14⁰⁰ ⚥¹ 14²⁵ ▲0 14⁴⁰-20 ⚥0 14³⁰-35 ⚥0 15²⁵ 28 ▲¹ 15³⁰ ⚥⚥0 ▲ 16¹⁰ = ² 0⁰⁰ 15³⁵ = -17⁰⁰ = ² 21⁰⁵ = -22¹⁰ ▥ -24, K¹ 14⁴⁵-30 K² N 15²⁰-25 (K) 15 16⁰⁰-45 NE, (☇) ⁰ 17⁴⁰ 14³⁵
Σ	-	209.4	-	**31.VII:** (☇) ⁰ 15¹⁷ 16³⁰ ≈ 0⁰⁰ 5⁴⁰ ≫ -8³⁰ ≈ -15¹⁵ ≫ -16¹⁵ ≈ -19³⁰ ≫ -20³⁰ ≈ -22¹⁵ ≫ -24, ∩ 15²⁵-30, 16⁴⁵-45

Sierpień – Août

1	7	(0.0)	•	✕0 7⁵⁰ 8²⁰, ▥ 0⁰⁰ 1¹⁵ = ² 2³⁰ = -3¹⁰ ▥ -5²⁰ = -11⁴⁰ 17³⁰ 22¹⁵ ▥ 20³⁰ 21¹⁰ = ² 22¹⁵ 24, ≫ 0⁰⁰ 2³⁰ 3¹⁰ 5⁴⁰
2	7	0.2	•	▲0 11⁰⁷-10 ⚥² 11⁵ 11³⁵-38 15⁵³ 17⁰⁴, = ² 0⁰⁰ 1³⁰ = -4⁴⁰ = ² 7²⁰ 8⁴⁰ = -11⁴⁰, ≫ 5³⁰ 9¹⁰, 12²⁰ 15¹⁰
3	8	1.2	•	•0 9⁴⁰ 12¹⁰ 14⁰⁵ 17¹⁰ 19⁵⁵ 24, = 9⁰⁵ 10³⁰ 15⁴⁰ 16⁴⁰ = ² 17³⁰ = -17⁴⁵ ▥ 17³⁰ 18¹⁰ = -18²⁵ = ² 24, ≫ 8³⁰ 13¹⁰ ≈ -15¹⁵ ≫ -24
4	7	0.0	•	•0 0⁰⁰ 5⁵⁰ ⚥0 12⁵⁵ 13⁰⁴ 18⁰³-05, = ² 0⁰⁰ 8¹⁰ = -9¹⁰ 13¹⁰ 14²⁰ 16³⁰ 17²⁰ = 22⁴⁰ 24, ≫ 0⁰⁰ 4³⁰ ≈ -10³⁰ ≫ -13⁰⁵ 16⁴⁰ 24
5	7	•	•	= 0⁰⁰ 2³⁰ = ² 4²⁰ 6¹⁰ = -8⁴⁵ = ² 9⁰⁰ ≫ 0⁰⁰ 8¹⁵
6	9	4.2	•	⚥0 10³⁷-45 ⚥¹ 15⁵⁰ ▲0 16⁵⁰-54 ▲¹ 17⁰¹ ⚥² 15⁵⁶ 17⁰¹ ⚥² 17⁰⁶, 17²⁷-30 17⁴⁰-50 21⁵⁰ 22⁰² (K) ⁰ W 15⁵² K¹ 16⁵⁵ 18⁰⁵ NE < ⁰ E 20⁰⁰ E 22³⁰, ≫ 3³⁰ 4³⁰ ≈ -9³⁰ ≫ 16³⁰, K¹ 19⁴⁰ ≈ -24, (☇) ⁰ 15³⁰ 17¹⁰, ▽ 20¹⁰⁴-15
7	8	•	•	⚥0 10³⁰-32, = 0⁴⁰ 1¹⁵ = ² 5³⁰ 23¹⁵, ≈ 0⁰⁰ 8³⁰ ≫ -15¹⁵, 17³⁰ 20¹⁰
8	7	9.7	•	▥ 1⁵⁰ 6³⁰ = 10⁴⁵ 14²⁰ 15⁴⁵ 18⁴⁰ = ² 22³⁰ = -23¹⁰ = ² 24
9	0	5.7	•	⚥0 4¹⁵ 6⁴⁰ •¹ 7²⁰ ⚥² 8⁴⁰ ⚥0 14⁵⁰ 15¹⁵ = ² 0⁰⁰ 1³⁰ = -3⁴⁰ = ² 6³⁰ = -7⁴⁰ = ² 8²⁰ ▥ -9⁴⁵ = 9⁰⁵-45 = ² 20⁵⁰ = -21³⁰ = ² 22³⁰ 23³⁰, (☇) ⁰ 5⁵⁰ 6⁴⁰ (☇) ⁰ 17⁵⁰ 8²⁰, ≫ 7⁴⁰ 8³⁰
10	7	0.0	•	⚥0 17⁴⁰-50, = ² 0⁰⁰ 10³⁰ = -15⁴⁰ = ² 24, ≫ 6²⁰ 8⁴⁰ 20⁵⁰ 24
11	7	0.5	•	= ² 0⁰⁰ 9⁰⁵ = -9⁴⁵ = ² 10⁰⁰ = -11³⁰ = ² 18¹⁰ 24, ≫ 0⁰⁰ 11²⁰
12	7	0.1	•	= ² 0⁰⁰ 3³⁰ = -12⁴⁰ = ² 20⁴⁵ 24, ≫ 7³⁰ 10⁴⁰
13	8	•	•	= ² 0⁰⁰ 8³⁰ = -9²⁰, ≫ 6⁵⁰ 9⁴⁰
14	8	•	•	= 0³⁰ 2²⁰, 22³⁰ 23³⁰ = ² 24
15	7	•	•	= ² 0⁰⁰ 4³⁰ = -5³⁰ = ² 6³⁰ = -9²⁰, 10³⁰ 13⁴⁰ = ² 14²⁰ = -20⁴⁰ ▥ 19³⁰ 22²⁰
16	8	•	•	= 6³⁰ 8⁰⁵ ▥ 5⁴⁰ 8³⁰
17	8	•	•	
18	7	•	•	
19	7	•	•	= 4³⁰ 10³⁰
20	7	•	•	≫ 20³⁰ 24
21	6	•	•	= 10¹⁵ 13³⁰ = ² 23³⁰ 24, ≫ 0⁰⁰ 4³⁰, 18¹⁵ 19³⁰ ≈ -24
22	7	•	•	= 0⁰⁰ 2¹⁰ 4⁴⁵ 7⁰⁵, 22³⁰ 23¹⁰ = ² 24, ≈ 0⁰⁰ 3³⁰ ≫ -6¹⁵ ≈ -24
23	7	27.7	•	⚥0 14³⁰-48 15⁵⁵ 16⁴⁵ 17⁰⁰-40, 17³⁰ 18¹⁰ ⚥¹ 18⁴⁰ ⚥0 19¹⁵ ⚥¹ 19⁵⁰ •0 21¹⁵ 21⁴⁵, 22⁵⁰ 24, (K) ⁰ 18¹⁵-45 = ² 0⁰⁰ 5⁴⁵ = 7⁴⁰ 9¹⁰ = ² 15³⁰ 21¹⁵ = 22³⁰ ▥ 21¹⁵ 24, (☇) ⁰ 18¹⁰...30 ≈ 0⁰⁰ 6²⁰ ≫ -7⁵⁰, 10⁴⁵, 13³⁰
24	0	39.3	•	•0 0⁰⁰ 1⁵⁰ •0 4⁴⁰ 5¹² •¹ 5¹⁵ •¹ 6⁰⁰ •¹ 6³⁰ •0 7⁰⁵ ⚥¹ 7¹³ •0 12⁵⁰ 13¹⁰ 13⁵³ 15³⁰, 20¹⁰ •¹ 20⁴⁵ •0 21¹⁵ •¹ 21³⁵ •0 24, ▥ 0⁰⁰ 2¹⁰ = ² 24, (K) ⁰ E 6³⁰ E 8¹⁰
25	7	15.9	•	•0 0⁰⁰ 2⁰⁵ •¹ 2⁴⁰ •0 10³⁰ •0 11⁰⁰ •0 ... 16⁴⁵ •0 17³⁰ 18¹⁰ •¹ 19⁵⁰, = ² 0⁰⁰ 1¹⁰ = -15⁰⁵ = ² 16¹⁰ 24, ≫ 5³⁰ 11³⁰, 14³⁰ 16³⁰, 18³⁰ 19²⁵ ≈ -24
26	7	•	•	= ² 0⁰⁰ 7⁰⁵ = -9⁴⁰ 15³⁰ 18⁴⁰ = ² 24, ≈ 0⁰⁰ 7⁴⁰ ≫ -11³⁰ 17⁴⁰ 24
27	7	4.1	•	= ² 0⁰⁰ 7⁴⁰ ≈ -10²⁰ ≫ 0⁰⁰ 8³⁰
28	7	1.0	•	⚥0 4³⁰ 5¹⁰ ⚥¹ 5⁴⁰ ⚥² 5⁴⁵ ⚥² 6⁴⁵ 7⁴⁵ = 24⁰ 3³⁰ = ² 4³⁰ 5⁴⁰ 6³⁰ 9⁰⁰ = -12⁴⁰ 13⁴⁰ 15²⁰ 18²⁰ 19⁴⁰, (☇) ⁰ 4³⁰ 5⁴⁵ 6⁴⁵ 7⁵⁰, ≫ 17⁴⁰ 20²⁰
29	8	1.2	•	•0 5³⁰ 13⁰⁰, ≈ 5³⁰ 8¹⁵, 14³⁵ 15⁰⁵ = ² 21⁴⁰ ≈ -24, ≫ 8³⁵ 13¹⁰
30	8	0.1	•	⚥0 4⁴⁵ 5²⁵ ▲0 5¹⁵-21 ⚥¹ 17²⁷-35 19⁵⁵ 13⁴⁰ 17³⁰-50, = ² 0⁰⁰ 1⁴⁰ = ² 5⁰⁵ ▥ 7¹⁵ 12⁴⁰, ≫ 5³⁰ 6³⁰, 11³⁰ 12³⁰, 15⁴⁰ 17²⁰, 18³⁰ 19
31	7	2.9	•	⚥0 22⁵³ 23³⁰ ⚥¹ 23⁴⁰, = 13⁴⁰ 20²⁰ = ² 0⁰⁰ 24, ≫ 0⁰⁰ 6¹⁰, ✕¹ 22⁵⁰ 23³⁵
Σ	-	192.4	-	

Śnieżka — φ = 50°44′ — λ = 15°44′ — Wrzesień – Septembre 1965

DNI	CIŚNIENIE P = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	132.1	133.7	133.7	133.2	4.8	7.5	9.2	7.7	9.3	3.7	74	85	100	86	2.2	1.6	0.0	1.3	9	9	10● ≡	SW 10	SW 1	SSW11
2	134.5	136.0	135.0	135.2	8.6	12.0	9.8	10.0	13.0	8.1	100	60	84	81	0.0	5.7	2.0	2.6	10 ≡	8	8	SW 18	SW 16	SW 24
3	129.8	134.8	133.4	132.7	9.0	11.0	11.7	10.8	12.1	8.4	100	99	100	100	0.0	0.1	0.0	0.0	10 ≡	10	10 ≡	S 30	SSW16	SSW15
4	133.0	134.3	133.8	133.7	6.6	8.4	6.1	6.8	11.7	5.4	81	76	84	80	1.8	2.7	1.5	2.0	9	9	9	N 7	W 3	SW 14
5	134.1	134.2	133.1	133.8	5.3	8.8	7.2	7.1	10.7	4.3	87	76	100	88	1.2	2.7	0.0	1.3	2	7	10 ≡	SW 7	SW 5	SSW 5
6	130.9	130.4	129.1	130.1	7.0	5.8	2.8	4.6	8.9	2.2	86	100	100	95	1.3	0.0	0.0	0.4	7	10● ≡	10 ≡	NNE 2	WSW 2	W 16
7	127.9	129.3	131.5	129.6	0.4	2.1	3.3	2.3	3.3	0.3	100	100	100	100	0.0	0.0	0.0	0.0	10● ≡	10● ≡	10● ≡	W 22	SW 18	SW 16
8	134.4	136.4	134.1	135.0	2.4	4.0	5.0	4.1	5.6	1.8	100	97	97	98	0.0	0.2	0.3	0.2	10● ≡	9	9	WSW15	W 10	SSW20
9	134.0	136.9	135.5	135.5	6.8	10.7	9.8	9.3	13.0	4.8	87	73	100	87	1.4	3.4	0.0	1.6	5	8	10● ≡	WSW20	WSW 6	SW 9
10	131.7	133.9	134.1	133.2	9.0	8.4	7.2	8.0	9.8	6.4	100	100	87	96	0.0	0.0	1.4	0.5	10● ≡	10 ≡	9	SW 15	SW 4	SW 8
11	132.3	134.7	135.3	134.1	2.4	2.4	2.8	2.6	8.2	1.9	100	100	83	94	0.0	0.0	1.2	0.4	10● ≡	10 ≡	6	WNW10	N 3	NW 3
12	134.7	134.4	133.7	134.3	1.2	3.2	2.6	2.4	4.6	0.9	96	84	93	91	0.3	1.2	0.6	0.7	10 ≡	8	9	W 4	SW 9	SW 9
13	132.6	133.6	133.7	133.3	1.4	2.0	2.4	2.0	4.0	1.0	91	96	96	94	0.7	0.3	0.3	0.4	2	9	9	W 6	WSW 3	W 7
14	134.4	137.6	139.9	137.3	2.2	3.4	3.2	3.0	4.9	1.4	90	93	97	93	0.7	0.5	0.3	0.5	9	9	9	W 4	WNW 3	WNW12
15	141.0	144.0	145.9	143.6	2.8	5.5	4.4	4.3	5.9	2.1	79	80	76	78	1.7	1.7	2.0	1.8	8	8	1	NW 14	NW 1	NNW 3
16	145.7	145.8	143.3	144.9	5.0	8.4	7.0	6.8	8.6	4.3	77	64	100	80	2.0	4.0	0.0	2.0	1	2	10● ≡	SW 2	SW 9	SW 18
17	143.2	143.9	142.6	143.2	8.2	10.5	9.6	9.5	11.8	5.9	94	81	100	92	0.6	2.5	0.0	1.0	8	6	10 ≡	W 9	WSW 7	S 15
18	139.1	138.1	136.9	138.0	6.4	10.2	8.0	8.2	11.2	6.2	100	78	100	93	0.0	2.7	0.0	0.9	9	2	10● K	WSW18	SW 12	SW 17
19	139.2	141.8	143.9	141.6	2.2	1.4	1.6	1.7	8.0	0.9	100	96	100	99	0.0	0.3	0.0	0.1	10 ≡	9	10 ≡	WNW 7	NNW12	NNW20
20	145.2	148.8	151.1	148.4	-1.4	0.4	1.0	0.2	1.6	-1.5	99	100	100	100	0.1	0.0	0.0	0.0	10 ≡	10● ≡	10● ≡	NNW20	NW 6	NNW 6
21	151.3	152.0	150.4	151.2	1.0	6.2	9.6	6.6	9.9	0.2	86	75	8	56	0.9	2.4	11.0	4.8	6	8	0	S 3	S 1	N 1
22	147.7	146.1	145.6	145.8	11.5	11.8	13.5	12.6	13.5	9.1	1	43	2	15	17.4	7.7	15.2	13.4	2	2	0	S 2	SSW 8	SSW 7
23	140.5	139.2	136.9	138.9	13.1	10.3	7.6	9.6	14.7	7.3	8	48	100	52	13.9	6.5	0.0	6.8	1	3	10● ≡	SSE 6	S 11	SSW13
24	133.1	133.7	134.5	133.1	6.0	8.2	8.0	7.6	9.7	5.2	89	90	97	92	1.1	1.1	0.3	0.8	4	8	9	SW 18	SW 16	SW 24
25	133.2	132.6	130.2	132.0	6.1	8.6	7.5	7.4	9.3	6.0	98	100	100	99	0.1	0.0	0.0	0.0	8	10 ≡	10● ≡	SW 18	SW 20	SW 30
26	124.7	127.1	128.8	126.9	5.6	7.2	9.2	7.8	9.5	5.4	100	100	100	100	0.0	0.0	0.0	0.0	10● ≡	10● ≡	10● ≡	SW 25	SW 16	SW 18
27	123.2	126.2	128.4	125.9	8.8	4.4	6.7	6.6	9.4	4.0	100	100	100	100	0.0	0.0	0.0	0.0	10● ≡	10● ≡	10● ≡	SW 18	SW 20	SW 15
28	128.5	127.7	126.1	127.4	7.2	6.4	7.4	7.1	9.1	5.6	77	100	100	92	2.4	0.0	0.0	0.8	9	10● ≡	10● ≡	SW 10	S 10	SW 12
29	128.5	130.8	132.0	130.4	1.0	2.3	2.3	2.0	7.4	0.9	98	100	100	99	0.1	0.0	0.0	0.0	9	9	10● ≡	WSW 6	WSW 8	WSW17
30	133.2	136.2	138.2	135.9	3.2	9.4	6.8	6.6	9.9	2.0	97	48	100	82	0.3	6.1	0.0	2.1	7	4	8	SW 17	SSW15	SSW10
31																								
M	133.2	136.5	136.3	136.0	5.1	6.7	6.4	6.2	9.0	3.8	86	85	90	87	1.7	1.8	1.2	1.6	7.5	7.9	8.5	12.0	9.0	13.2

Październik – Octobre

1	138.9	140.5	139.9	139.8	12.5	12.8	8.5	10.6	14.4	7.0	36	72	100	69	9.2	4.2	0.0	4.5	1	3	10● ≡	ESE14	C 0	SSE 7
2	138.0	138.7	140.4	139.0	8.0	8.8	7.8	8.1	9.1	7.4	100	100	100	100	0.0	0.0	0.0	0.0	10● ≡	10 ≡	10● ≡	SSW 7	WSW12	N 1
3	141.9	143.0	143.6	142.8	8.2	6.3	7.4	7.3	9.0	5.8	47	92	55	65	5.9	0.7	4.6	3.7	6	9	8	WSW 3	C 0	ENE 3
4	143.4	144.1	143.6	143.7	8.0	10.3	8.8	9.0	12.0	6.3	69	85	59	71	3.4	1.9	4.6	3.3	1	7	2	C 0	WSW 2	S 1
5	142.8	143.6	143.2	143.2	7.2	10.7	8.2	8.6	12.1	5.6	67	50	19	45	3.4	6.5	8.9	6.3	0	2	1	N 7	E 1	E 3
6	142.5	142.7	141.9	142.4	9.2	9.4	10.1	9.7	11.0	7.6	15	47	25	29	9.8	6.4	9.3	8.5	1	2	2	NNW 3	S 2	S 1
7	140.7	141.2	140.8	140.9	10.5	12.3	11.0	11.2	13.7	8.5	12	43	14	23	11.1	8.1	11.4	10.2	1	1	4	S 1	S 1	NNW 3
8	138.8	138.3	137.4	138.2	7.2	5.4	1.2	3.8	11.8	1.1	47	98	100	82	5.5	0.2	0.0	1.9	5	8	10● ≡	N 3	N 8	N 6
9	136.8	137.2	136.4	136.8	-1.0	-1.8	-1.6	-1.5	1.2	-1.9	99	98	98	98	0.1	0.1	0.1	0.1	10 ≡	10 ≡	10 ≡	N 7	NNW 8	N 14
10	134.9	136.6	137.1	136.2	-3.8	-1.2	-3.2	-2.8	0.5	-3.9	96	95	85	92	0.2	0.3	0.7	0.4	9	5	4	WNW10	NW 4	NW 8
11	136.5	137.0	137.2	136.9	-0.4	4.4	-1.0	0.5	4.4	-3.4	75	69	99	81	1.4	2.7	0.1	1.4	1	2	10 ≡	NW 6	WNW 1	NNW 7
12	140.3	144.5	144.5	143.2	-2.2	1.0	2.0	0.7	2.4	-2.7	98	82	40	73	0.1	1.2	3.3	1.6	10 ≡	3	0	NNW 7	NNW 1	N 4
13	144.9	144.4	143.3	144.2	4.2	5.3	5.9	5.3	6.8	0.4	49	46	31	42	4.2	4.9	6.4	5.2	1	1	6	WSW 2	SW 4	NW 9
14	142.3	143.0	141.9	142.4	8.2	8.8	8.0	8.2	9.3	4.4	23	23	7	18	8.4	8.8	10.0	9.1	4	3	3	W 5	WSW 4	WSW10
15	140.6	140.5	138.7	140.1	5.2	7.4	2.6	4.4	8.3	2.4	32	69	96	66	6.0	3.2	0.3	3.2	3	6	9	WSW10	SW 10	SW 18
16	137.4	137.3	139.5	138.1	4.6	3.2	-0.6	2.2	6.3	-1.9	97	83	99	94	0.3	1.3	0.0	0.3	9	9	10 ≡	SW 17	WSW17	WNW20
17	142.1	143.2	143.2	144.2	-3.8	1.4	3.1	1.0	3.9	-3.9	96	87	24	69	0.2	0.9	5.8	2.3	10 ≡	4	0	WNW17	SW 2	N 4
18	143.3	143.4	142.9	143.3	3.8	-0.6	-0.6	0.3	4.9	-2.0	33	96	83	71	3.3	0.2	1.0	2.2	0	6	0	NW 3	NW 4	N 8
19	143.3	143.1	143.2	144.3	-1.4	0.6	2.2	0.9	2.4	-2.7	99	79	34	71	0.1	1.4	4.8	2.1	8	6	0	E 6	N 2	N 12
20	144.9	146.3	146.0	145.8	1.0	2.0	-3.8	-1.2	3.3	-3.8	23	62	96	61	4.9	2.7	0.2	2.6	0	0	10 ≡	N 10	N 8	SE 10
21	146.1	147.2	147.9	147.1	-3.2	1.6	-0.1	-0.4	2.3	-3.6	33	38	4	23	3.2	4.2	3.8	4.4	1	6	1	E 10	S 1	SE 7
22	148.8	149.8	149.4	149.3	1.0	4.0	2.4	2.4	4.1	-0.3	11	38	35	28	3.9	3.0	4.7	3.2	0	0	0	SE 8	SSE 6	S 12
23	148.4	148.3	146.2	147.6	4.6	4.2	2.6	3.3	5.5	2.0	41	35	42	39	3.1	3.3	4.3	4.9	2	7	0	SE 4	NE 2	N 13
24	145.4	146.2	146.1	145.9	3.1	3.7	4.7	4.6	8.0	0.6	32	49	26	36	3.2	4.7	6.3	3.4	0	0	0	N 10	C 0	ENE 3
25	143.4	143.6	144.3	143.3	6.3	7.2	3.8	6.3	8.2	4.6	12	31	23	22	8.3	7.1	7.1	7.3	0	1	0	E 3	SSW 3	C 0
26	142.7	142.1	140.4	141.7	3.6	6.2	6.4	6.2	7.0	4.0	21	33	14	23	7.2	6.3	8.2	7.2	0	0	0	E 2	SW 6	W 6
27	139.7	140.1	140.6	140.1	4.0	6.0	5.3	5.6	7.4	3.6	43	54	61	60	2.9	4.3	3.6	3.6	1	0	0	NW 10	NW 9	W 10
28	137.3	138.0	137.3	137.3	4.0	6.8	4.4	4.9	7.2	4.0	93	88	98	87	0.4	3.1	0.2	1.2	8	9	8	SW 23	WSW18	SW 16
29	135.1	134.0	135.3	134.8	4.4	4.9	-1.0	1.8	5.3	-1.0	100	100	93	100	0.0	0.0	0.1	0.0	10● ≡	10● ≡	8	W 18	WSW20	NW 19
30	137.4	137.8	134.3	136.5	-3.4	-0.8	-0.6	-1.4	1.0	-3.6	97	66	81	81	0.2	1.9	1.1	1.1	4	7	2	NW 17	WNW10	W 18
31	130.8	131.4	130.3	130.8	-1.0	-1.4	-2.6	-1.9	-0.1	-3.0	99	94	95	96	0.1	0.3	0.2	0.2	10 ≡	6	9	W 24	NNW18	WSW18
M	141.0	141.7	141.3	141.3	3.6	4.9	3.4	3.8	6.5	1.1	59	67	59	62	3.8	3.2	3.7	3.6	4.1	4.6	4.4	8.7	6.0	8.8

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	POGODA
1	8	20.5	.	●0 00 11 0 24 30 5 ●0 50 14 05 ● 14 25 16 10 0 19 30 ● 20 ● 18 ● 19 30 ; 19 20 ● 0 21 30 22 45 = 2 17 00 30 5 = -3 40 ▥ 4 30 5 35 = -6 20 ▥ 0 10 12 15 = 2 19 40 24 ⟹ 0 00 3 20 ⟹ 7 10 20 30 22 10 ⟹ -24
2	7	.	.	= 2 00 4 10 = -5 05 = 2 6 05 = -10 20 ⟹ 0 00 24
3	7	6.4	.	● 10 27-45 ● 2 20 21 35 22 05 23 20-40 = 2 20 6 10 = 2 0 30 = 17 20 16 10 = 2 24 ⟹ 0 00 14 30 ⟹ 16 10 18 15 23 30 ⟹ -24
4	8	.	.	= 2 00 3 20 = 8 20 9 10 = 2 21 40 - 23 30 = -23 45 ⟹ 0 00 1 30 ⟹ 16 40 24
5	8	.	.	= 21 25 22 10 = -24 ⟹ 0 00 5 20
6	0	8.2	.	● 0 55 11 20 ● 0 11 40 ● 0 11 50 ● 12 50 13 10 ● 0 13 45 ● 14 20 0 16 40 ● 0 19 50 20 10 = 0 00-15 ▥ 4 50 8 20 = 2 15 40 ▥ -10 20 = 15 40 17 20 18 40 19 20 = 2 24 ⟹ 13 45 14 20 ⟹ 16 30 21 40 ⟹ -24
7	0	1.1	.	● 16 25 30 = 1 00 24 ⟹ 0 00 3 40 ⟹ -14 50 ⟹ 18 30 ⟹ 21 30 ⟹ 24
8	7	0.2	.	= 0 00 11 40 = 16 50 = 2 20 40 = -22 30 ⟹ 0 00 2 05 ⟹ 6 30 ⟹ 7 05 8 30 14 40 15 30 18 40 ⟹ -24
9	8	1.2	.	● 0 37 12 45 ▥ 6 30 14 45 = 16 15 18 25 = 2 24 ⟹ 0 00 1 20 ⟹ 12 40 ⟹ -24 ; ⌒ 8 10 9 50
10	0	24.4	.	● 6 05 8 05 ● 0 10 35 ● 10 40 0 23 30-40 0 24 = 2 00 18 40 = -22 30 ▥ 15 40 21 20 = 2 24 ⟹ N 23 40 24 ⟹ 0 00 3 30 ⟹ 8 40 21 20 24 ⟹ 23 40 24
11	0	5.2	.	● 0 00 30 0 3 20 0 1 40 ● 2 6 55 9 30 10 35 0 35-40 = 2 0 00 13 05 = -14 20 = 2 15 15 21 20 22 10 = -24 ⟹ 0 00 1 30 E ⟹ 0 00 1 40 4 30 8 20
12	8	.	.	= 0 00 2 30 = 2 6 20 7 40 = -17 20 = 2 22 40 24
13	7	.	.	= 2 0 00 4 15 = -7 20 ▥ 4 25 9 30 = 8 40 10 30 ; 12 40 14 30 = 16 50 24 ⟹ 18 20 4 40
14	7	0.0	.	● 0 7 40 8 50 = 0 00 6 30 7 50 23 20 = 2 24 ⟹ 10 20 24
15	7	.	.	= 0 00 1 40 = -6 10 ▥ 6 30 7 40 = 7 50 9 10 ⟹ 0 00 1 30 5 10 9 30
16	7	.	.	= 16 10 20 40 = 2 24 ⟹ 13 20 17 20 ⟹ -24 ⊕ 9 20 11 40
17	7	.	.	= 2 00-15 = -12 40 17 20 18 40 = 2 24 ⟹ 0 00-30 ⟹ 1 20 10 40 17 20 18 40 24
18	7	5.6	.	● 1 55 10 00 ● 0 10 45 ● 1 20 05 ● 0 20 40 ● 2 21 15 = 2 00 1 40 = 2 30 ▥ 5 20 = 3 40 0 10 ▥ 7 50 17 30 = 14 05 16 40 = 2 21 05 21 25 23 30 = 24 ⟹ 14 45 20 05 ⟹ 21 15 NE ; 0 50 21 15 ⟹ 0 00 4 10 ⟹ -8 30 ⟹ 17 50 ⟹ -18 30
19	7	0.3	.	● 2 05-20 = 0 00-40 = 2 45 10 05 = -16 40 = 2 17 30 = -18 40 = 2 24 ⟹ 0 00 7 15 23 20 6 15 8 30 11 40 ⟹ -17 00 ⟹ -18 40 ⟹ -24
20	0	0.4	.	V° 3 40 11 30 = 2 0 00 22 30 ⟹ 0 00 9 15 ⟹ -11 30
21	8	.	.	⌐ 12-9
22	9	.	.	
23	9	0.3	.	▥ 4 30 16 40 = -17 10 = 2 24 ⟹ 10 10 24
24	7	0.1	.	= 2 0 00-30 = -1 30 = 2 2 00 = -24 ⟹ 0 00 6 30 ⟹ -24
25	0	1.4	.	= 0 00-20 = 2 3 40 = -12 30 = 2 13 15 16 40 = -24 ⟹ 0 00 24
26	0	3.5	.	= 2 0 00 24 ⟹ 0 00 24
27	0	6.1	.	● 6 00-15 ● ∠ 7 25 ● 8 37 = 2 0 00 24 ; ⟨ 17 15 45 7 55 8 20 ⟹ 0 00 18 40 ⟹ -24
28	0	9.4	.	● 1 55 14 20 ● 1 16 30 ● 0 20 10-50 22 50 24 = 2 0 00 4 30 = -6 20 ▥ 8 20 11 45 = 11 40 12 10 = 2 21 30 = -23 10 = 2 24 ⟹ 0 00 7 30 12 20 15 20 ⟹ -18 30 ⟹ -20 10
29	8	0.8	.	● 0 00 1 50 = 1 40 2 40 = -5 10 6 30 10 30 = 2 11 15 = -16 05 = 2 24 ⟹ 17 15 18 30 ⟹ -24
30	8	.	.	= 0 00 2 30 ▥ -5 30 = 4 30 5 30 = 2 6 45 = -7 40 ▥ 6 45 24 = 16 40 21 20 ⟹ 0 00 2 10 ⟹ -4 30 ⟹ -11 30 ⟹ -22 30 ; ⊛ 6 45 7 10
31				
Σ	-	95.1	-	

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1	8	0.1	.	▥ 0 00 2 40 = 16 45 19 30 = 2 19 30 22 50 = -24 ⟹ 5 30 10 30 ; 22 10 24
2	0	2.2	.	● 17 40 18 20 19 50 20 50 21 30 = 0 00 1 30 = 2 24 ⟹ 0 00 4 30 9 40 12 30
3	7	.	.	= 0 00 1 40 = -4 20 ▥ -10 30 = 2 12 45 = -16 30 ▥ 20 10
4	7	.	.	⌒ 1 3-8 40 ; ▥ 4 30 24 = 9 30 13 40
5	8	.	.	⌒ 0 4 20 6 40 ; ▥ 0 00 24
6	8	.	.	▥ 0 00 14 40 ; ⊕ 11 10-20
7	8	.	.	▥ 4 20 24
8	8	2.5	.	▥ 0 00 13 30 = 11 10 16 20 = 2 24
9	0	0.7	.	⌒ 2 3 30 6 30 V° 24 = 2 0 00 24 ⟹ 7 40 11 20 18 30 24
10	8	0.1	.	V° 0 00 10 15 = 2 0 00 6 40 = -7 20 = 2 10 15 = -13 40 ▥ 10 20 11 40 16 30 18 40 = 18 10 20 20 ⟹ 0 00 3 40 ⟹ -6 40 ⟹ -7 10
11	8	1.0	.	V° 18 25 24 ; ▥ 5 20 11 50 13 15 14 05 = -16 30 ▥ 14 05 18 05 = 17 35 18 05 = 2 24 ⟹ 21 30 - 23 30
12	8	.	.	V° 0 00 7 30 = 2 0 00 7 30 = -8 10 ▥ 7 30 14 40 15 20 24 = 15 20 16 20
13	9	.	.	▥ 0 00 4 30 5 10 8 30 ; ⌒ 20 20-21 30 ⊽ -22 50
14	9	.	.	⟹ 17 40 24
15	8	.	.	= 17 46 23 30 ⟹ 0 00 17 40 ⟹ -24
16	7	3.3	.	● 13 07 15 50 ● 0 16 50 = 8 40 9 30 12 40 13 20 = 2 19 10 = -20 20 = 2 24 ⟹ 0 00 8 40 ⟹ -12 40 ⟹ -13 20 ⟹ 14 40 15 30 ⟹ -24
17	8	.	.	V° 0 00 8 40 = 2 0 00 7 10 = -8 40 ▥ 7 10 24 = 12 45 13 30 ⟹ 0 00 7 10 ⟹ -8 10
18	8	0.0	.	V° 15 52 18 20 ▥ 0 00 11 20 = -15 40 = 2 18 20 = -20 40 ▥ 19 40 20 20 = 2 21 20 24 ; ⊛ 9 30 10 15
19	8	.	.	V° 0 30 1 20 ; = 2 0 00 1 20 = -2 30 3 40 9 20 ▥ 6 10 24 = 13 40 14 20 15 40 16 20 ⟹ 20 40 24
20	9	0.0	.	V° 15 50 23 40 ; ▥ 0 00 16 20 = 15 20 16 40 = 2 23 40 = -24 ⟹ 0 00 1 30 6 20 10 10 20 30 24
21	9	.	.	= 0 00 2 20 ▥ 1 10 24 ; ⟹ 0 00 9 10
22	9	.	.	▥ 0 00 9 30 ⟹ 17 20 24
23	9	.	.	⟹ 0 00 4 10 20 15 24
24	8	.	.	▥ 0 00 24 ; ⟹ 0 00 7 30
25	9	.	.	
26	9	.	.	
27	9	.	.	▥ 3 40 17 00 ⟹ 10 9 30 14 50 17 30 20 10 23 10 ⟹ -24
28	8	0.0	.	= 3 40 7 15 = 2 8 10 = -12 20 ▥ 8 40 17 30 = 17 40 19 40 = 2 20 35 = -24 ⟹ 0 00 15 30 ⟹ -18 10 ⟹ -24
29	0	2.1	.	● 14 45 18 30 ● 1 17 45 ● 0 17 45 V° 10 50 24 = 0 00 1 20 = 2 7 35 = -9 15 = 2 13 10 = -14 10 = 2 18 50 = -24 ⟹ 0 00 17 30 ⟹ -19 45 ⟹ -24
30	9	0.2	.	V° 0 00 2 30 5 10 9 30 = 0 00 2 30 5 05 10 00 18 40 24 ⟹ 0 00 7 05 ⟹ -18 20 ⟹ -24
31	7	2.5	.	△° 16 55 18 05 ; V° 7 00 12 50 16 35 24 = 0 00 2 40 = 2 12 50 16 35 18 40 = -21 30 = 2 24 ⟹ 0 00 11 30 ⟹ -12 40 ⟹ -24
Σ	-	14.7	-	

Śnieżka — φ = 50°44' — λ = 15°44' — Listopad – Novembre 1965

DNI	CIŚNIENIE P = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	126.5	124.7	120.2	123.8	-0.2	1.2	2.6	1.6	3.0	-3.3	98	100	100	99	0.1	0.0	0.0	0.0	10 ✶ ≡	10 ● ≡	10 ● ≡	WSW18	SW 20	WSW35
2	120.6	120.9	122.5	121.3	0.4	-1.4	-1.4	-1.0	2.6	-1.6	100	99	99	99	0.0	0.1	0.1	0.1	10 ● ≡	10 ≡	10 ≡	W 22	WSW24	WSW20
3	127.0	127.4	128.3	127.6	-3.0	-2.8	-5.8	-4.4	-1.3	-5.8	97	97	95	96	0.1	0.1	0.2	0.1	10 ≡	10 ≡	5	WSW20	WSW15	NW 11
4	133.1	136.5	139.0	136.2	-6.8	-4.8	-5.6	-5.7	-4.4	-6.8	94	88	95	92	0.2	0.5	0.2	0.3	4	8	9	NW 8	NW 3	NW 6
5	141.3	143.5	145.3	143.4	-5.2	-3.0	-5.8	-5.0	-3.0	-6.4	95	97	77	90	0.2	0.1	0.9	0.4	9	10 ≡	0	NW 6	NNW 1	NNW 4
6	146.0	146.0	143.4	145.1	-2.4	2.2	5.0	2.4	5.3	-6.2	67	79	34	60	1.7	1.5	5.7	3.0	0	2	2	NW 9	NW 3	NNW 4
7	139.5	139.0	139.3	139.3	5.6	9.2	6.6	7.0	11.3	4.4	28	25	19	24	6.5	8.7	7.9	7.7	0	0	8	C 0	C 0	NNW 2
8	140.7	142.0	142.2	141.6	6.6	9.3	4.6	6.3	10.1	4.6	18	23	36	26	8.0	9.0	3.5	7.5	3	2	8	C 0	C 0	N 6
9	141.5	141.2	139.5	140.7	2.6	3.4	1.2	2.1	4.6	1.0	100	100	92	97	0.0	0.0	0.5	0.2	10 ● ≡	10 ● ≡	9	N 4	N 1	NE 1
10	137.4	136.4	133.4	135.7	0.4	0.1	-1.4	-0.6	1.2	-1.4	98	96	99	98	0.1	0.3	0.1	0.2	9	10 ≡	10 ≡	E 5	SSE 2	E 10
11	127.9	125.0	122.5	125.1	-2.6	-5.8	-8.6	-6.4	-1.0	-8.7	98	95	95	96	0.1	0.2	0.2	0.2	10 ≡	10 ✶ ≡	10 ✶ ≡	NE 14	NE 14	N 12
12	121.0	121.1	122.0	121.4	-10.5	-11.0	-11.7	-11.2	-8.6	-11.7	90	90	89	90	0.3	0.3	0.3	0.3	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	N 10	N 15	NNE 14
13	122.0	122.4	122.5	122.3	-12.2	-11.8	-13.4	-12.7	-11.7	-13.5	89	89	88	89	0.3	0.3	0.3	0.3	10 ✶ ≡	10 ≡	10 ≡	NE 14	NE 12	NE 10
14	123.4	124.6	125.5	124.5	-12.0	-11.1	-12.0	-11.8	-10.6	-13.7	89	90	89	89	0.3	0.3	0.3	0.3	10 ≡	10 ✶	10 ✶	NE 5	NE 2	C 0
15	125.9	128.1	130.7	128.2	-13.3	-11.8	-15.7	-14.1	-9.2	-15.8	88	93	91	91	0.3	0.2	0.2	0.2	4	9	10 ≡	N 1	N 2	NW 12
16	134.4	136.4	136.4	135.7	-15.0	-11.5	-12.6	-12.9	-11.4	-15.8	87	90	89	89	0.2	0.3	0.3	0.3	10 ≡	10 ✶ ≡	0	N 18	N 6	N 4
17	133.9	132.0	128.1	131.3	-10.6	-9.8	-7.2	-8.7	-6.4	-12.7	90	63	50	68	0.3	1.1	1.7	1.0	8	0	0	SE 4	S 6	S 8
18	124.1	122.8	120.6	122.5	-2.2	-4.2	-5.6	-4.4	-0.8	-10.0	96	96	95	96	0.2	0.2	0.2	0.2	8	-10 ✶	6	SW 4	S 7	W 12
19	118.4	117.7	119.7	118.6	-4.7	-3.0	-2.8	-3.3	-2.2	-5.7	96	97	95	96	0.2	0.1	0.2	0.2	10 ✶ ≡	10 ✶ ≡	0	SW 18	SW 22	SW 14
20	119.9	120.3	118.7	119.6	-2.8	-2.3	-2.8	-2.7	-2.0	-3.1	93	98	97	96	0.4	0.1	0.1	0.2	9 ✶	9	10 ≡	S 2	S 6	SW 8
21	111.2	107.0	108.0	108.7	-4.0	-1.8	-4.5	-3.7	-1.6	-4.5	96	98	96	97	0.2	0.1	0.2	0.2	10 ✶ ≡	10 ≡	10 ✶ ≡	SW 12	SW 22	W 18
22	116.2	122.0	124.3	120.8	-10.8	-9.8	-14.6	-12.4	-4.5	-14.7	90	91	91	91	0.3	0.3	0.2	0.3	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	NW 17	NW 12	N 12
23	127.3	129.8	131.7	129.6	-17.1	-13.8	-13.5	-14.5	-13.4	-17.4	85	88	88	87	0.2	0.3	0.3	0.3	5	7	0	N 10	NNW 8	WNW 12
24	130.0	125.9	124.2	126.7	-13.6	-13.0	-12.2	-12.8	-12.2	-14.3	88	61	89	79	0.3	0.9	0.3	0.5	2	8	10 ✶ ≡	WSW 15	SW 20	SW 24
25	126.3	128.7	126.9	127.3	-8.8	-8.4	-9.2	-8.9	-8.3	-12.2	92	89	92	91	0.3	0.3	0.3	0.3	10 ✶ ≡	9	10 ≡	W 16	W 10	SW 15
26	119.0	113.2	119.6	117.3	-7.6	-8.5	-7.2	-7.6	-6.3	-10.2	93	92	88	91	0.2	0.3	0.4	0.3	10 ✶ ≡	10 ≡	10	SW 25	SW 26	SW 14
27	116.2	106.8	104.3	109.1	-9.6	-6.6	-3.2	-5.6	-1.9	-10.7	85	94	97	92	0.4	0.2	0.1	0.2	10	10 ≡	10 ✶ ≡	SW 12	SW 25	SW 30
28	103.4	108.7	113.8	108.6	-7.6	-7.8	-7.8	-7.8	-2.7	-8.8	93	93	93	93	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	SW 35	SW 16	SW 16
29	119.3	118.0	109.4	115.6	-8.5	-8.1	-8.0	-8.2	-7.8	-9.4	92	92	93	92	0.3	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ≡	WSW 18	WSW 20	SW 30
30	107.1	111.3	114.8	111.1	-5.8	-6.1	-8.7	-6.8	-3.6	-9.0	96	94	92	94	0.2	0.2	0.3	0.2	10 ✶ ≡	10 ✶ ≡	10 ≡	SW 30	SW 22	W 17
31																								
M	126.0	126.0	125.9	126.0	-6.0	-5.1	-6.0	-5.8	-3.2	-8.1	87	87	85	86	0.7	0.9	0.9	0.8	8.0	8.5	7.9	12.4	11.4	12.7

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1	109.1	115.1	118.7	114.3	-8.4	-7.4	-7.2	-7.6	-7.0	-9.2	92	93	93	93	0.3	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	W 28	W 25	W 20
2	122.4	123.2	114.7	120.1	-7.2	-7.0	-8.4	-7.8	-7.0	-8.4	93	93	92	93	0.2	0.2	0.3	0.2	10 ✶ ≡	10 ✶ ≡	10 ≡	W 20	SW 15	SW 28
3	114.9	113.4	116.0	114.8	-6.6	-6.8	-5.8	-6.2	-5.8	-9.4	94	94	95	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	8	SW 14	SW 18	SW 10
4	117.1	117.8	120.3	118.4	-5.4	-5.8	-5.6	-5.6	-5.3	-5.8	95	95	95	95	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	SW 6	SW 10	W 4
5	120.2	113.7	108.7	114.2	-5.6	-5.8	-5.4	-5.6	-5.4	-6.1	95	95	95	95	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	W 15	SW 28	SW 28
6	112.9	115.9	121.0	116.6	-5.8	-4.8	-5.0	-4.6	-0.5	-5.5	96	95	95	95	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	SW 24	SW 25	SW 20
7	122.6	125.8	126.0	124.8	-5.8	-6.0	-6.0	-6.0	-4.7	-6.3	95	94	94	94	0.2	0.2	0.2	0.2	10 ≡	10 ≡	10 ≡	SW 25	SW 16	SW 26
8	127.7	129.5	132.0	129.7	-6.6	-7.2	-8.4	-7.6	-5.9	-8.5	94	93	92	93	0.2	0.2	0.3	0.2	10 ≡	10 ✶ ≡	9	SW 16	W 7	W 7
9	131.7	124.9	114.7	123.8	-8.6	-8.6	-8.8	-8.7	-8.3	-9.0	92	92	92	92	0.3	0.3	0.3	0.3	9	10 ≡	10 ≡	SW 12	SW 25	SW 30
10	103.5	104.3	103.1	103.6	-7.6	-5.7	-4.8	-5.7	-4.8	-9.5	93	95	95	94	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ≡	10 ≡	SW 30	SW 17	SW 25
11	109.4	110.6	112.9	111.0	-7.4	-8.0	-8.5	-8.1	-4.6	-8.7	93	93	92	93	0.2	0.2	0.3	0.2	10	10 ✶ ≡	10 ✶ ≡	W 15	W 20	W 16
12	118.1	119.6	122.3	120.0	-8.0	-8.2	-8.6	-8.4	-7.9	-8.7	93	92	92	92	0.2	0.2	0.3	0.2	10 ✶ ≡	8	9	WNW 16	NW 15	NW 6
13	124.7	124.1	119.8	122.9	-7.8	-7.4	-5.5	-6.6	-5.5	-8.9	93	93	95	94	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ≡	10 ✶ ≡	NW 6	SW 8	SSW 14
14	129.2	133.1	137.6	133.3	-8.1	-9.8	-10.0	-9.5	-5.1	-10.1	92	97	84	91	0.2	0.1	0.4	0.2	10 ≡	2	0	N 12	N 18	WNW 5
15	135.1	134.7	134.8	134.9	-7.8	-7.0	-6.8	-7.1	-6.7	-10.8	93	93	94	93	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	W 14	NW 16	NW 12
16	132.9	132.7	132.0	132.5	-6.4	-6.2	-5.4	-5.8	-5.3	-6.9	94	89	95	93	0.2	0.4	0.2	0.3	8	7	10 ✶	NW 5	WNW 3	W 4
17	129.6	128.2	129.3	129.0	-5.0	-3.8	-3.8	-4.1	-3.7	-6.5	95	96	96	96	0.2	0.2	0.2	0.2	8	10 ≡	10 ≡	W 5	W 12	WSW 12
18	128.5	129.6	132.2	130.1	-2.0	0.3	2.1	0.7	2.6	-4.6	98	100	100	99	0.1	0.0	0.0	0.0	10 ≡	10 ● ≡	10 ● ≡	SW 14	WSW 20	W 22
19	132.6	133.2	131.0	132.3	1.2	1.2	0.8	1.0	2.6	0.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	SW 25	WSW 20	WSW 26
20	132.9	133.4	130.9	132.4	-4.0	-1.0	0.0	-1.2	1.1	-4.0	84	21	100	68	0.7	4.5	0.0	1.7	10 ✕	10	10 ✶ ≡	WNW 12	SW 3	SW 12
21	128.8	128.6	128.8	128.7	0.3	-4.6	-6.8	-4.5	0.8	-7.0	100	96	94	97	0.0	0.2	0.2	0.1	10 ● ≡	10 ≡	10 ✶ ≡	SW 12	N 4	N 8
22	131.8	131.8	131.1	131.6	-8.0	-7.6	-7.6	-7.7	-6.7	-9.0	93	87	93	91	0.2	0.4	0.2	0.3	4	8	10 ≡	N 3	WSW 6	W 2
23	128.3	124.3	117.0	123.2	-9.6	-8.4	-10.0	-9.5	-7.5	-10.3	86	77	91	85	0.4	0.7	0.3	0.5	0	8	10 ≡	WSW 7	SW 20	SW 25
24	116.1	114.3	109.7	113.4	-7.0	-6.6	-7.0	-6.9	-3.7	-11.6	93	94	93	93	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	SW 10	WSW 15	W 24
25	105.6	103.3	106.1	105.7	-7.4	-6.6	-5.4	-6.2	-3.3	-8.1	93	88	95	92	0.2	0.4	0.2	0.3	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	W 22	WSW 16	WSW 16
26	107.8	110.3	117.6	112.0	-5.8	-8.4	-8.0	-6.8	-3.9	-8.4	97	93	93	93	0.2	0.2	0.2	0.2	10 ✶ ≡	10 ✶ ≡	10 ✶ ≡	WSW 15	WNW 15	NW 30
27	117.1	115.4	113.0	115.2	-9.0	-8.2	-7.4	-8.0	-7.4	-9.2	92	92	93	92	0.3	0.2	0.2	0.2	10 ≡	10 ≡	9	SW 18	SSW 20	SW 17
28	112.1	116.0	122.2	116.8	-6.2	-9.8	-11.0	-9.4	-3.2	-11.1	94	92	90	92	0.2	0.3	0.3	0.3	10 ≡	2	1	WSW 15	NW 16	NW 16
29	123.3	127.1	127.4	129.9	-11.0	-11.0	-10.2	-10.6	-9.4	-11.4	90	80	91	87	0.3	0.5	0.3	0.4	8	3	10 ≡	NW 18	NW 16	W 19
30	120.8	116.9	120.9	119.5	-11.6	-10.2	-6.8	-8.8	-5.9	-12.7	89	91	94	91	0.3	0.3	0.2	0.3	8	10 ≡	10 ≡	SW 25	SW 30	SW 20
31	120.4	122.0	123.9	122.1	-5.8	-6.0	-5.6	-5.8	-3.1	-7.3	93	94	93	93	0.2	0.2	0.2	0.2	10 ≡	10 ✶ ≡	10 ✶ ≡	SW 25	SW 18	W 12
M	121.5	121.8	121.8	121.7	-6.4	-6.4	-6.4	-6.4	-4.8	-8.1	93	90	94	92	0.2	0.4	0.2	0.3	9.2	9.0	9.2	15.6	16.0	16.3

DNI	WI. DZIAŁ-NOŚĆ v	OPAD R	GRUB. ŚNIEGU h	POGODA
1	0	4.9	•	*5^40 7^50; V0^00 7^50; ≡2^00 24; ≋0^00 24
2	0	2.1	•	•0^50 1^15 6^50 △0^45-55 △1-8^40 X0^30-40 17^40 18^15; V0^50 8^50, 11^30 13^30 16^50 24; =2^00 8^50 ==-11^50 ≡2-13^30 ==-16^10 ≡2-24; ≋0^00 24
3	0	6.2	•	*0^45 10^50; V0^00 10^30 22^30 24; ≡2^00 11^05 ==-11^45 ≡2 12^15 ==-12^30 ≡2 13^10 ==-10^30 21^00 23^30 ≡2 24; ≋0^00 3^30 ≫-6^40 ≋-9^30 ≫-14^50, 16^15 24; +0^15-24
4	8	0.0	6	V0^00 6^30 21^00 24; ≡2^00 21^15 ==-6^30 m 7^10 17^40 ==-18^40 20^30 21^10 ≡2 24; +0^00 4^30 +2 9^40; ≫0^00 4^30
5	0	0.0	5	V0^00-30, 1^00 2^00 6^10 11^30 17^00 19^20; ≡2^00-30, 1^30 2^00 ≡ 6^10-12^30 ≡2 15^30 ==-16^15 m-17^00 ==-19^20 m-20^30
6	9	•	3	m 1^50 24; ≫4^30 6^45
7	8	•	2	m 0^00 8^10; ⌀ 18^30 20^35
8	9	0.1	2	m 5^50 22^20 ≡ 22^15-40 ≡2-24; ≫21^20-24
9	0	0.2	1	≡2^00 14^10 ==-16^30 m-17^40 ==-19^10 m-20^30 ==-24; ≫0^00 2^20
10	0	1.9	pz.	⌐0^30 9^00 V15^10-24; ≡0^00 1^30, 6^40 11^20 m 7^40 11^10 ≡2 11^20-24; ≫20^30-24
11	0	25.8	pz.	*0^40-24; V0^00-24; ≡2^00-24; +1 13^30-24; ≫0^00 20^20 ≋-5^40 ≫-24
12	0	15.8	20	*0^00-24; V0^00-24; ≡2^00-24; +1 0^00-24; ≫0^00-24
13	0	5.7	30	*0^00-12^30, 22^50-24; V0^00-24; ≡2^00-24; +1 0^00-24; ≫0^00-24
14	7	2.8	33	*0^00 6^40 8^45 13^45 14^50 17^30 18^30-24; V0^00 12^10 ≡2^00 12^00 ==-13^30 m-15^50 ==-24 ≡23^30-24; +1 10^00 1^00 +0 7^50; ≫0^00-50
15	7	3.1	36	*0^00 2^30 6^50 →→8^10 11^20; V0^00 13^30-24; ≡0^00 8^30 ≡0^00 6^30 m 5^30 12^40 ==12^00 18^40 m 14^30 18^40 ≡2-24; +0 19^20-24; ≫18^40-24
16	0	1.3	32	*0^30 18^50; V0^00 20^30; ≡2^00 18^30 ==-20^30 m-24; +0 0^00-30 +1 10^30 +0-17^30 +1 18^30 +0 19^30 +0-21^30; ≫0^00-30 ≋-9^15 ≫-10^30 14^30 19^30
17	9	•	34	m 0^00 24 ≡ 23^20-30; ≫21^30 24; ⌀ 2^30 6^30
18	5	3.5	30	*0^15-20^15 V7^20-45 10^30-24; m 0^00 7^15 ≡ 1^30 3^20 5^40 7^20 ≡2 7^40 m-14^40 ≡ 10^30 14^40 ≡ 10^30 14^40 ≡2-20^15 ==-24 m-27; +0 17^15-13^30 +0-14^10 +1 18^30 +0-20^30 +1-24; ⌀ 4^00-40; ≫14^30-24
19	0	3.3	32	*0^45 14^30 16^50 V0^00 20^40; ≡2^00 5^15 m 0^00 5^15 ≡2-20^35 ==-22^10 m 20^50 23^30; +1 0^00 20^00 +0-22^20; ≫0^00 6^30 ≋-20^20 ≫-22^10
20	7	0.8	30	*5^50 11^15; V8^30 22^00; m 5^30 8^30 ==8^20-30 ≡2-11^10 ==-13^30 ≡2-22^00; ≫22^10-24
21	0	7.7	33	*5^40 11^50 15^20 20^50; V0^30 3^30 4^10 5^30 24; ≡0^30 3^30 4^10 5^30 ≡2 24; +1 6^50 22^30 +0-24; ≫0^00 8^50 ≋-22^30 ≫-24
22	0	5.0	36	*2^40-24; V0^00-24; ≡2^00-24; +0 0^00 1^50 +1-6^25 12^30 +1-14^10 +0-16^40 +1-24; ≫0^00 6^15 ≋-12^00 ≫-14^10 16^40-24
23	8	•	40	*0^00 1^40; V0^00 1^40; ≡2^00 1^40 m 5^30 11^30; +1 0^00 8^30 +0-11^30 +0 20^10 +0-21^30 +1-24; ≫0^00 11^30, 20^10-24
24	9	4.2	36	*0^15 21^10 *1-24; V7^30-24; ≡ 16^35 17^20 ≡2-24; +1 0^00 8^15 +2-24; ≫0^00 8^15 ≋-24
25	7	2.2	38	*0^00 2^20 *1-11^10; V0^00 11^10 15^30 16^10 18^40 21^15 23^30 ≡2 0^00 11^10 ==-15^30 ≡2-16^10 ==-18^40 ≡2-21^15 ==-23^30; +2 0^00 7^20 +1-16^10, 17^30-24; ≋0^00 1^20 ≫-16^10, 17^30 23^30 ≋-24
26	0	2.3	40	*0^50 18^50, 15^40 20^20-45; V0^00 3^20 10^05 11^30 20^30; ≡0^00 3^20 ≡2 10^05 ≡ 10^35 17^20 ≡2 21^20 ==-20^45; +1 0^00 4^00 +2 0^00 +0-23^30 +2-24; ≋0^00 20^10 ≫-24
27	0	15.5	40	*16^50-24; V8^00-24; ≡0^00 3^30 ≡2-4^40 ==-7^50 ≡2-24; +0 0^00 7^10 +0 7^30 +1-12^30 +2-24; ≫0^00 7^30 ≋-24
28	0	7.5	48	*0^00-24; V0^00-24; ≡2^00-24; +2 0^00 12^20 +1-15^30 +2-24; ≋0^00-24
29	0	4.4	50	*0^00 15^20; V0^00 16^10 40 17^10 19^30-24; ≡2^00 16^10 ==-16^40 ≡2 17^10 ==-19^30 ≡2-24; +2 0^00-24; ≋0^00-24
30	0	4.5	50	*5^30 9^50 10^00 15^50; V0^00 14^30 16^45-24; ≡2^00 14^30 ==-16^45 ≡2-24; +2 0^00 18^30 +1-22^30 +2-24; ≋0^00-24
31				
Σ	-	130.6	-	

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1	0	10.5	52	*3^45-24; V0^00-24; ≡2^00-24; +2 0^00-24; ≋0^00-24
2	0	5.2	60	*0^00 13^30 X0-14^40; V0^00-24; ≡2^00-24; +2 0^00 8^30 +1-15^30 +2-24; ≋0^00 8^30 ≫-15^30 ≋-24
3	0	6.6	62	*0^50-4^50 X27^55 23^20; V0^00 19^30 21^50-24; ≡2^00 19^30 ==-21^20 ≡2-24; +2 0^00 2^40 +1-8^50 +2 15^30 +1-24; ≋0^00 3^30 ≫-8^50 ≋-15^10 ≫-24
4	0	6.6	62	*0^40-24; V0^00-24; ≡2^00-24; +2 0^00 6^10 +0-15^30 +1-17^40 +0-22^20 +0-24; ≫0^00 6^10, 9^40 14^40 ≋-17^20 ≫-18^30
5	0	12.6	65	*0^00-24; V0^00-24; ≡2^00-24; +2 0^00 5^10 +1-8^20 +2-24; ≫5^10-8^20 ≋-24
6	0	3.8	75	*0^00-05 *1-0^20 *0-3^20 X0 14^55 16^50 *2-17^40; V0^00-24; ≡2^00-24; +2 0^00 21^20 +1-23^40 +2-24; ≋0^00 21^20 ≫-23^40 ≋-24
7	0	3.4	78	V0^00-24; ≡2^00-24; +2 0^00 1^30 +1-15^30 +2-24; ≋0^00-24
8	0	2.3	78	*0^50 13^10 *0 13^55 15^30 18^50 20^10; V0^00-24; ≡2^00 17^20 ==-17^25 ≡2 13^10 ==-13^40 ≡2 15^30 ==-18^40 ≡2 20^30 ==-21^20 ≡2-24; +2 0^00 5^20 +1-17^15 +0-14^40 +1-19^30 +0-24; ≋0^00 7^20 ≫-17^15, 14^40 19^30
9	0	0.3	79	V0^00 21^15 ≡2 0^00 2^40 ==-3^20 m 2^40 3^20 ≡2-4^50 ==-8^40 ≡2 13^10 ==-15^20 ≡2-21^15; +0 0^00 7^30 +1-24; ≫5^30 7^30 ≋-24
10	0	14.2	80	*6^45 7^40 9^50 X0-10^45 X1 14^45 15^15 *2 21^05-24; V3^30-24; ≡3^30-24; V15^15, (X)14 15^17...15; +2 0^00 10^30 +1-15^15 +2-24; ≋0^00-24
11	0	6.1	90	*0^00 5^50 9^20 11^30-24; V0^00-24; ≡2 0^00 5^10 ==-8^15 ≡2-24; +2 0^00 1^30 +1-8^30 +2-24; ≋0^00 2^30 ≫-8^30 ≋-24
12	7	2.1	95	*6^00-7^40; V0^00 14^30-24; ≡2 0^00-7^40 ==-24; +2 0^00 7^30 +1-18^40 +0-24; ≋0^00 7^30 ≫-18^10
13	0	7.0	90	*2^55 7^40 13^45 18^07 *1 10^45 *0 19^15 *1-19^45 *0 2^30 *1 22^15 *0-24; V4^00 19^20 7^40 17^15-24; ≡0^00 19^20 ≡2 7^40 ==-17^15 ≡2-24; ≫13^50-22^30; +2 0^00-8^30 11^30 13^50 +1-22^30 +2 23^10-24
14	8	4.7	95	*0^00 5^50; V0^00 10^30; ≡2 0^00 8^40 ==-10^30 m-15^30; +2 0^00 1^05 +1-14^20 +1-20^40 +0-21^20; ≫4^00 10^40 ≋-14^30 ≫-20^40
15	0	7.4	100	*3^50 5^20-23^15-24; V1^40-24; ≡2 1^40-24; +2 1^40 6^20 +2-20^20 +1-22^40 +0-23^20; ≫0^00 7^40 ≋-20^20 ≫-22^40
16	8	0.1	105	*0^00 1^40 18^55 21^40; V0^00 1^50 18^40 21^10; ≡2 0^00 1^50 ==-3^10 m 5^30 18^40 ≡2-20^50 ==-21^10
17	0	2.4	102	V8^40 6^40 9^30-24; ≡2^40 6^55 ==-9^20 ≡2-24; +0 0^30 8^20 +1-24; ≫8^30-24
18	0	15.9	102	•0^30 12^50 18^50 21^10 22^30 •1-24; V0^00 7^40; ≡2 0^00-24; +1 0^00 7^50; ≫0^00-1^10 ≋-5^20 ≫-8^40 ≋-24
19	0	12.0	85	•0^00-2^30 •0-16^40; ≡2 0^00 16^45 ==-19^20 ≡2-24; ≫0^00-24
20	9	1.7	60	•0^30 6^20 *0-7^30 8^45 14^45 15^30 22^50 •0 23^45-24; ∽0^40 6^20; V0^50 22^30; ≡2^00 6^10 ==-6^15 m-13^50 ≡2 15^40-24; ≋0^00 9^30 ≫-3^45 5^40 9^30 17^30-24
21	0	15.7	58	•0^00-1^50 *8^40 11^30 *0-24; V0^30-4^30 ∽0^30 4^30; V0^30-24; ≡2^00-24; +2 15^30-24; ≫0^00 8^45
22	7	0.0	70	*0^00 5^40 18^00 21^05; V0^00 6^15 12^00-24; ≡2^00 6^15 m 11^40 17^30 ==-15^40 m 14^00 15^40 ≡2-17^20 ==-18^40 ≡2-21^00 ==-24; +0 0^00 5^50
23	7	1.7	65	V0^00 5^40 9^40 11^00, 18^45 20^00-24; ≡2^00 5^40 m 8^40 20^00 ==9^40 11^30 18^45 20^00 ≡2-24; +0 8^30 9^50 +1-12^30 +2-24; ≫9^30 12^30 ≋-24
24	0	3.0	67	*6^10 8^40 9^00 13^30 14^10 18^40 19^30-24; V0^00-24; ≡2^00-24; +2 0^00 5^10 +1-7^40 +2-8^40 +1-9^00 +0-9^00 +1-16^40 +2-24; ≋0^00 5^10 ≫-7^40, 8^40 9^00 11^30 16^40 ≋-24
25	0	6.0	70	*0^00-2^50 4^40 5^20 13^40 15^50 18^40-24; V0^00-24; ≡2^00-24; +2 0^00 23^40 +1-24; ≋0^00 23^40 ≫-24
26	0	13.0	75	*0^00 1^40 8^30 9^40 20^30-24; V0^00 19^40-20^40-24; ≡2^00 19^40 ==-20^40 ≡2-24; +1 0^00 13^50 +2-24; ≫0^00 13^50 ≋-24
27	0	2.6	87	*0^00 7^15 21^45-24; V0^00 2^40 9^30 13^30 15^15 21^45-24; ≡2^00 2^40 ==-3^30 4^30 15^15 m-18^05 ≡2-24; +2 0^00 8^30 +1-24; ≋0^00 15^30 ≫-20^30 ≋-23^30 ≫-24
28	8	1.6	90	*0^00 5^20; V0^00 5^30 V1-11^10; ≡2^00 11^05 ==-12^05 m 11^30-24; ≡2 15^30-22^10; +1 0^00 10^30 +2-11^00 +1-24; ≫0^00 11^30 11^30 12^00 ≋-24
29	7	0.8	87	V4^00 6^20 15^30 16^20-24; ≡2 14^00 m 0^00 3^30 ≡2 4^00 6^20 ==-9^10 13^30 16^20 ≡2-24; +1 0^00 3^30 +2 6^30 +1-24; ≋0^00-24
30	0	3.6	85	V0^00 3^10 9^00 11^30 11^40-24; ≡2 0^00 3^10 ==-8^40 m-9^15 ≡2 11^30 ==-11^40 ≡2-24; +1 0^00 5^30 +2-24; ≋0^00-24
31	0	6.7	82	*8^50 13^46 15^50 23^30 *1-24; V0^00 18^30 V1-24; ≡2 0^00-24; +2 0^00 9^30 +1-24; ≋0^00 18^30 ≫-24
Σ	-	178.0	-	

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — *Styczeń – Janvier* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	94.6	83.7	83.1	83.8	0.2	2.0	1.0	1.0	2.3	-0.3	88	71	85	81	0.7	2.1	1.0	1.3	10	10 ⁑	10	WSW 3	WSW 8	WSW 5
2	79.3	77.7	78.9	78.6	0.2	0.4	0.2	0.2	1.3	-0.3	98	96	98	97	0.1	0.3	0.1	0.2	10 *	10 *	10 *	SW 5	SW 4	WSW 2
3	80.6	82.0	83.8	82.1	0.2	0.3	-0.3	0.0	0.5	-0.4	100	98	98	99	0.0	0.1	0.2	0.1	10 *	10 *	10 *	NE 2	NE 3	NE 5
4	85.1	88.0	93.5	88.9	-0.9	-0.5	-2.1	-1.4	0.0	-2.2	99	98	92	96	0.0	0.2	0.4	0.2	10 *	10 *	10	NE 6	NE 6	NE 8
5	94.1	89.3	91.4	91.6	-4.7	-2.1	-1.3	-2.4	-0.2	-6.6	83	96	84	88	0.7	0.2	0.9	0.6	0	10 *	0	WNW 5	W 12	WNW 8
6	92.7	94.1	93.1	93.3	-2.7	-1.2	-4.1	-3.0	0.0	-5.0	82	72	75	76	0.9	1.6	1.1	1.2	4	0	1	NW 7	NW 7	NW 8
7	95.2	96.3	95.8	95.8	-3.8	-2.9	-4.3	-3.8	-2.2	-5.0	92	86	94	91	0.4	0.7	0.3	0.5	10 *	10	10	NW 8	NW 7	NW 4
8	90.9	86.2	81.0	86.0	-9.6	-2.9	-2.5	-4.4	-1.2	-10.8	94	82	91	89	0.2	0.9	0.5	0.5	10	10	10 *	WSW 2	SW 8	SW 9
9	79.6	80.4	80.5	80.7	2.6	2.1	0.8	1.6	2.9	-2.9	95	95	96	95	0.6	0.4	0.3	0.4	10	10	10 •	NW 7	WSW 4	W 3
10	80.2	79.9	92.4	84.2	1.2	0.8	-6.5	-2.8	1.2	-6.8	89	88	86	88	0.8	0.8	0.5	0.7	3	10	10	WSW 4	SW 5	NE 6
11	103.5	104.2	103.5	103.7	-14.3	-9.7	-14.9	-13.4	-6.3	-15.0	91	78	96	88	0.2	0.6	0.1	0.3	0	3	0	E 2	ESE 2	SE 3
12	100.4	98.5	96.4	98.4	-13.9	-7.7	-8.7	-9.8	-5.9	-15.2	96	81	89	89	0.1	0.6	0.4	0.4	0	10	7	SE 2	ESE 3	SSE 2
13	95.2	95.9	97.2	96.1	-11.6	-2.1	-5.9	-6.4	-0.3	-12.0	93	75	94	87	0.2	1.5	0.2	0.6	0	0	0	SSE 2	S 2	SSW 4
14	95.4	93.4	94.2	94.3	-9.3	-0.7	-3.1	-4.0	0.6	-11.1	91	67	74	77	0.3	1.9	1.3	1.2	2	2	0	SSE 2	SSW 4	SSW 1
15	99.4	100.4	98.8	99.5	-1.9	1.2	-2.3	-1.3	2.8	-4.3	87	77	93	86	0.7	1.6	0.4	0.9	8	9	10	SW 3	WSW 2	ESE 3
16	95.7	96.0	96.2	96.0	-5.9	-2.9	-3.5	-4.0	-1.1	-6.2	87	68	81	79	0.5	1.5	0.9	1.0	9	4	10	SE 2	S 1	SW 3
17	89.4	83.1	77.4	83.3	-4.3	0.6	-0.3	-1.0	1.1	-6.0	82	70	82	78	0.8	1.9	1.1	1.3	6	9	10	SSW 5	SW 8	S 4
18	74.5	74.4	72.8	73.9	0.2	3.0	-0.5	0.6	3.3	-0.7	100	84	96	93	0.0	1.2	0.3	0.5	10 *	9	9	SW 6	SW 4	SW 3
19	71.6	72.6	74.3	72.8	-4.1	0.0	-3.1	-2.6	2.5	-4.6	96	73	95	88	0.2	1.7	0.3	0.7	0	0	1	WSW 3	SW 2	SSE 2
20	71.6	67.7	64.9	68.1	-2.8	-1.1	-0.1	-1.0	-0.1	-6.5	93	93	100	95	0.4	0.4	0.0	0.3	10	10	10 *	E 5	ESE 7	NE 3
21	67.1	71.7	78.6	72.5	0.4	0.3	-0.3	0.0	0.9	-0.5	98	96	100	98	0.1	0.2	0.0	0.1	10 •	10 ≏	10 ≏	NW 1	WSW 2	WSW 4
22	82.9	85.0	88.0	85.3	-1.7	0.8	-4.9	-2.7	1.6	-5.0	96	82	100	93	0.2	1.2	0.0	0.5	10	0	0 ≡	SW 2	SSW 2	E 1
23	90.2	91.6	95.2	92.3	-4.3	-1.1	-1.7	-2.2	-0.4	-8.9	98	99	98	98	0.1	0.1	0.1	0.1	10	10 *	10 *	NE 2	ENE 4	N 5
24	99.0	99.5	99.0	99.2	-1.1	-0.5	-0.9	-0.8	0.0	-1.9	97	96	99	97	0.2	0.3	0.0	0.2	10 *	10	10 • ≡	N 3	N 3	N 3
25	95.3	94.0	93.9	94.4	-1.3	-0.9	-1.7	-1.4	-0.3	-1.9	95	97	98	97	0.3	0.2	0.1	0.2	10 ≏	10 ≡	10	C 0	SW 1	WSW 2
26	93.1	92.4	92.6	92.7	-2.3	-0.3	-4.9	-3.2	-0.1	-4.9	98	86	98	94	0.1	0.9	0.1	0.4	10	10	3	SE 1	S 2	SE 2
27	93.3	93.1	92.8	93.1	-3.5	-1.9	-1.7	-2.2	-1.2	-5.8	99	92	92	94	0.0	0.4	0.4	0.3	10	10	9	SE 3	SSE 4	SSE 3
28	93.6	93.3	93.1	93.3	-3.3	-0.3	-1.6	-1.7	0.5	-3.5	95	86	90	90	0.3	0.9	0.5	0.6	10	7	10	SE 4	SE 2	SSE 2
29	91.3	89.5	88.3	89.7	-2.8	3.0	2.8	1.4	4.2	-3.5	93	76	82	84	0.4	1.9	1.3	1.2	10	10	10	SE 3	S 4	SW 1
30	87.0	85.4	84.2	85.5	0.4	5.3	1.9	2.4	5.7	-0.7	100	74	93	89	0.0	2.3	0.5	0.9	8	9	10	SE 2	SSE 5	SW 3
31	86.6	90.2	89.0	88.6	2.1	0.6	-1.1	0.1	2.3	-1.4	96	92	93	94	0.3	0.5	0.4	0.4	10 •	10 *	10 *	WNW 2	NE 2	NE 3
M	88.3	88.0	88.5	88.3	-3.3	-0.6	-2.4	-2.2	0.5	-5.2	94	85	92	90	0.3	0.9	0.4	0.5	7.4	7.8	7.4	5.4	4.1	5.6

Luty – Février

1	90.3	91.2	93.2	91.6	-2.4	-1.8	-3.3	-2.7	-0.7	-3.4	98	73	85	85	0.1	1.4	0.7	0.7	10 *	3	6	NNW 2	WNW 5	NW 3
2	95.4	97.4	101.4	98.1	-5.5	-2.7	-3.9	-3.5	-1.7	-5.8	85	75	92	84	0.7	1.2	0.4	0.8	10	9	9	NW 3	NW 3	NNW 4
3	101.7	99.2	96.6	99.2	-8.1	-5.9	-2.5	-4.8	-2.2	-10.7	84	92	93	90	0.3	0.3	0.4	0.4	1	10 *	10	NW 3	W 5	NW 5
4	96.7	95.6	97.5	96.6	-2.3	-0.6	-7.8	-4.6	0.0	-7.9	96	87	84	89	0.3	0.7	0.5	0.5	10	10 *	10	NW 5	W 3	NE 7
5	96.1	95.4	98.2	96.6	-13.5	-11.9	-13.3	-13.0	-7.6	-14.8	80	75	88	81	0.4	0.6	0.3	0.4	10	9 *	10	N 2	NNE 3	NNE 3
6	101.2	101.4	99.2	100.6	-20.5	-13.5	-17.2	-17.1	-11.7	-21.2	96	80	90	89	0.1	0.4	0.2	0.2	6	0	0	NNW 4	NNW 2	SW 2
7	97.7	96.5	87.5	93.9	-22.7	-14.9	-14.9	-16.8	-11.5	-23.7	96	91	78	88	0.0	0.2	0.4	0.2	8	0	2	C 0	WSW 2	WSW 6
8	65.7	70.0	77.7	71.1	-5.1	-4.7	-8.9	-6.9	-2.7	-16.9	98	93	92	94	0.1	0.3	0.3	0.2	10 *	10 *	10 *	NNW 9	N 9	NNE 7
9	87.7	92.1	97.9	92.6	-8.8	-6.9	-10.5	-9.2	-6.6	-10.7	92	77	84	84	0.3	0.8	0.4	0.5	10	4	10	NE 4	NNE 3	W 2
10	95.7	89.3	86.3	90.4	-14.1	-7.3	-4.1	-7.4	-3.8	-17.8	87	65	91	81	0.3	1.2	0.4	0.6	10	10	10	WSW 4	WSW 7	W 8
11	89.2	92.2	96.4	92.6	-4.7	-0.8	-4.9	-3.8	0.7	-6.3	88	71	88	82	0.5	1.7	0.5	0.9	0	4	0	WNW 3	W 5	NW 5
12	98.6	97.6	95.2	97.1	-6.5	0.2	-1.7	-2.4	1.7	-11.1	97	62	77	79	0.1	2.4	1.2	1.2	10	0	10	WSW 4	WSW 4	WSW 6
13	90.3	84.8	79.5	84.9	-4.1	-0.1	-2.1	-2.1	0.9	-5.1	91	71	85	82	0.4	1.8	0.9	1.0	8	10	10	WSW 6	SW 8	SW 5
14	74.6	73.6	79.9	76.0	-0.5	-0.7	-1.8	-1.2	2.9	-5.5	94	93	90	92	0.4	0.4	0.5	0.4	6	10 *	3	SW 8	SW 9	W 5
15	83.8	87.1	88.5	86.5	-2.3	0.2	-4.3	-2.7	0.5	-4.9	100	66	84	83	0.0	2.1	0.7	0.9	10	10	10	WSW 3	NW 5	SW 2
16	88.7	89.2	89.1	89.0	-9.0	-4.9	-4.1	-5.3	-3.6	-10.7	95	93	91	94	0.2	0.2	0.4	0.3	10 ▬	10	10 *	N 3	N 4	NNE 7
17	85.5	86.1	91.4	87.7	-5.5	-0.5	-1.9	-2.4	0.3	-5.7	97	100	87	95	0.1	0.0	0.7	0.3	10 *	10	10 *	NNE 8	NE 3	NE 5
18	92.6	93.9	95.1	93.9	-5.5	-4.7	-6.0	-5.6	-1.5	-6.2	97	91	94	94	0.1	0.4	0.2	0.2	10	10 *	10 *	NE 6	NE 7	N 7
19	95.3	97.1	99.9	97.5	-4.7	-5.5	-7.2	-6.2	-4.2	-7.2	98	87	90	92	0.1	0.3	0.3	0.3	10	10 *	10 *	NNE 5	NE 7	NE 6
20	103.4	106.1	106.7	105.4	-7.5	-3.7	-7.7	-6.6	-3.1	-8.3	93	76	87	85	0.2	1.1	0.4	0.6	10 *	8	2	NE 5	ENE 4	ENE 5
21	103.8	100.5	95.5	99.9	-6.9	-3.3	-3.1	-3.1	-2.6	-11.2	96	85	83	88	0.1	0.7	0.7	0.5	10	10	10	NNE 3	N 2	W 2
22	88.1	86.8	91.4	88.8	-3.7	-2.9	-8.8	-6.6	-2.4	-10.9	92	88	68	83	0.3	0.3	1.0	0.6	10 *	10 *	0	WNW 3	WNW 7	NW 3
23	91.8	90.9	90.7	91.1	-7.7	-4.1	-7.9	-6.9	-2.4	-13.7	93	73	84	84	0.2	1.1	0.3	0.6	10	10	6	WSW 2	WNW 4	WNW 4
24	93.7	92.6	86.6	91.0	-12.1	-3.3	-10.1	-9.4	-3.8	-13.6	96	62	94	84	0.1	1.3	0.2	0.6	0	0	0	WNW 4	SW 2	WSW 3
25	79.4	80.2	83.1	80.9	-4.7	-2.9	-8.9	-6.4	-2.0	-12.2	88	88	80	73	0.3	2.1	0.6	1.1	9	9	0	WSW10	NW 3	NW 3
26	86.1	86.8	81.3	84.8	-13.7	-6.0	-3.3	-7.8	-3.7	-14.7	88	68	88	74	0.3	1.3	1.3	1.0	0	4	10	WNW 3	WNW 3	NW 3
27	73.8	70.7	73.5	73.3	-6.1	-2.7	-6.1	-5.2	-2.0	-7.2	76	71	79	75	0.9	1.4	0.8	1.0	9	10	9	NW 4	NW 3	NW 3
28	83.4	87.2	91.7	87.4	-8.6	-3.3	-11.7	-9.3	-3.4	-11.9	74	70	75	73	0.8	1.2	0.6	0.9	3	2	0	WNW 9	NNW 7	WSW 4
29																								
30																								
31																								
M	90.4	90.4	91.2	90.7	-7.8	-4.4	-6.9	-6.5	-2.7	-10.6	92	78	85	85	0.3	1.0	0.6	0.6	7.9	7.2	6.7	4.7	4.8	4.8

Sandomierz $H_s = 202\,m$ $H_b = 200.3\,m$ $h_w =$ 20,6 m anemometr M-47 / 20,1 m wiatromierz Wilda **Styczeń - Janvier 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	1.7	13	•°12^{20-40} °22^{10} — 24, por wiatru 11 m/sek 12^{05} — 13^{45} = 0^{00} — 8^{20} 22^{10} — 24
2	5	3.2	15	•°0^{30} 1^{40} *° 4^{15} — 12^{20} ... 45 △° — 14^{10} *¹ — 14^{40} *° — 17^{40} △° 18^{42} — 20^{10} *° 21^{15} — 24, = 0^{00} — 24
3	5	10.4	18	*° 0^{00-35} 6^{05} — 17^{40} 20^{20} — 22^{20} 24, = 0^{00} — 24
4	6	1.1	25	*° 0^{00} 2^{20} — 9^{40} 10^{15} 12^{15} 13^{25}, por wiatru 12 m/sek 14^{30} — 18^{45}, = 0^{00} — 24
5	6	0.5	26	*° 11^{45} — 12^{10} 12^{15-38} 13^{10-22}, ⊹¹ 12^{35-40} ⊹° 13^{40} — 16^{30}, por wiatru 14 m/sek 11^{40-50} ≻ 17^{50} — 17^{00} (por do 19 m/sek) por wiatru 11 m/sek 20^{20} — 24, = 0^{00} — 7^{20}
6	7	0.0	22	por wiatru 10 m/sek 0^{00} — 8^{15}
7	7	0.4	22	⚹° 5^{40} — 6^{10} *¹ ⚹ 6^{15-20} *¹ — 6^{25} *° — 6^{40} *° 11^{35} ... 45 17^{05} ... 45 20^{40} ... 21^{25}, por wiatru 14 m/sek 0^{20} — 1^{10} 3^{20} — 6^{15}, = 20^{40} — 24
8	7	1.2	22	*° 20^{20} — 24, por wiatru 10 m/sek 11^{15} — 15^{30} 11 m/sek 17^{10} — 20^{20} = 0^{00} — 10^{45}
9	6	6.4	19	*° 0^{00} 3^{05} •° 3^{15-45} 4^{05} 5^{25} •° 7^{10} — 8^{35} 12^{48} 13^{15} — 16^{40} *° — 19^{30} •° — 21^{10} *° — 24, = 0^{00} — 13^{48} = ° — 13^{50} = ° — 18^{30} = ° — 19^{45} = 24
10	6	.	17	*° 0^{00} — 1^{10}, por wiatru 15 m/sek 17^{50} — 18^{20}, = 0^{00} — 24
11	7	.	17	= 0^{00} — 12^{15}
12	6	.	17	= 7^{40} — 24, ⊕ 9^{40} — 16^{40} ▽ 17^{00} — 21^{30}
13	6	.	16	= 0^{00} — 24
14	7	.	16	= 0^{00} — 12^{15}
15	6	.	15	= 0^{40} — 24, ▽ 16^{30} — 22^{15}, 23^{30} — 24
16	7	.	15	= 0^{00} — 12^{20}, ▽ 0^{00} — 1^{00}
17	7	7.1	15	◉ 17^{45} — 19^{45}, por wiatru 13 m/sek 10^{30} — 14^{20}, 12 m/sek 16^{15} — 17^{30}, 13 m/sek 18^{25} — 20^{15}; ∾ 17^{45} — 24
18	6	0.3	19	•° 0^{45} — 2^{20} *° 4^{10} — 5^{15} *¹ — 6^{10} *° — 6^{40} 7^{15} — ^{40}, por wiatru 13 m/sek 3^{30} — 4^{05}, = 0^{00} — 24; ∾ 0^{00} — ^{45}
19	7	.	19	= 0^{00} — 10^{30} 19^{40} — 24
20	6	5.0	18	*° 7^{20} — 11^{15} 12^{20} •° 16^{35} 17^{45} ◉ — 19^{10} △ 19^{35} *° — 20^{30} *¹ — 21^{40} *° — 24, por wiatru 13 m/sek 8^{30} — a ⚹ a — 10^{25} (por 16 m/sek), por wiatru 11 m/sek 12^{25} — 17^{30}, = 0^{00} — 24, ∾ 17^{45} — 19^{10} ▽ 20^{20} — 20
21	5	1.5	21	*° 0^{00} — 2^{40} •° 4^{40} — 5^{20} 6^{40} △ 9^{43} 10^{14} *° — 11^{15} △ — 13^{41} 15^{49} 17^{15} •° — 18^{45} ◉° — 20^{15} △ — 20^{40} *° — 22^{30} 24, = 0^{00} — 5^{40} = ° — 5^{45} — 8^{50} — — 24, ∾ 18^{45} — 20^{15}
22	6	.	22	*° 0^{00} — 10, = 0^{00} — 19^{15} = ¹ — 19^{45} = ° — 24, V° 19^{15} — 24
23	5	8.4	20	△ 8^{40} — 9^{30} *° — 10^{30} *¹ — 12^{15} *° — 14^{10} *¹ — 14^{45} *° — 24, = °0^{00} — 2^{40} = — 24, V° 0^{00} — 2^{40}
24	6	1.6	27	*° 0^{00} — 4^{40} 5^{20} — 8^{20} △° 16^{40} — 17^{20} ◉ °19^{40} — 24, = 0^{00} — 15^{50} = ° — 21^{40} = — 24, ∾ 18^{40} — 24
25	3	0.0	27	◉ 0^{00} — 5^{50} △° — 7^{15}, = 0^{00} — 9^{45} = ° — 14^{50} = — 24, ∾ 0^{00} — 5^{50}
26	6	.	27	= 0^{00} — 24
27	6	.	27	= 0^{00} — 24
28	6	0.0	27	*° 10^{15} — ^{30}, = 0^{00} — 24, ⊕ 12^{45} — 14^{10}
29	7	0.0	27	•° 8^{40} — 9^{45} ◉ — 10^{50}, = 0^{00} — 12^{10}, ∾ 9^{45} — 11^{00}
30	7	0.6	24	= 0^{00} — 6^{50} = ° — 9^{45} = — 12^{15}, 17^{30} — 24
31	6	10.2	21	•° 4^{40} — 5^{30} — 6^{10} ... 7^{25} — 8^{02} •° — 8^{20} *° ... 10^{20} — 13^{10}, 15^{05} — 24, = 0^{00} — 24
Σ	-	59.6	-	

Luty - Février

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	0.4	30	*° 0^{00} — 4^{30}, 4^{35} ... 6^{50} 7^{12} ... 11^{10} *° ⚹ 14^{35-42} *° 15^{45} 16^{40} 18^{40} 20^{30}, = 0^{00} — 12^{15} 19^{30} 24
2	7	.	32	*° 0^{10} 2^{40}, = 0^{00} — 8^{50}
3	6	1.9	30	*° 12^{08} — 40 — 14^{45} 15^{15} — 20^{15}, — 1^{30} — 6^{10} — 12^{09} — 24
4	7	2.1	30	*° 3^{40} — 6^{10} 11^{10} 14^{10-40} *¹ — 15^{05} *° — 15^{30} *¹ 15^{40} — 16^{30} *° — 17^{40} 19^{20} — 20^{20}, = 0^{00} — 9^{30}, 14^{40} — 23^{15}
5	7	0.0	33	*° 2^{45} — 3^{14} 7^{40} 10^{35} 12^{10} — 45 = 4^{30} — 11^{20} 17^{15} — 24
6	6	.	34	= 0^{00} — 24
7	6	1.4	30	*° 23^{40} — 24, = 0^{00} — 7^{45} = ¹ — 10^{20} = ° — 10^{40} = — 24, ⌣° 1 — 7^{45} V° — 14^{30}
8	5	9.1	33	*° 0^{00} 17^{45} *¹ — 18^{20} *° — 24, ⊹° 7^{45} — 8^{20} ⊹¹ — 20^{15} ⊹° — 24, por wiatru 12 m/sek 6^{40} — 8^{30}, 15 m/sek 8^{30} — 10^{20} 11^{10} — 12^{30}, 14 m/sek 14^{20} — 15^{40}, = 0^{00} — 24
9	7	0.1	38	*° 0^{00-30} 3^{30} 4^{40} — 5^{25} 6^{35} — 8^{35} 11^{20} *° ⚹ 13^{03-55} 17^{05} — ^{25} *° 18^{30} — 21^{20}, ⊹ 0^{00} — 6^{45}, = 0^{00} — 11^{40} 17^{30} — 24
10	7	0.4	38	*° 14^{40} — 15^{25} 16^{15} — 18^{40} 18^{50} — 20^{20}, ⊹° 20^{10} — 22^{20}, por wiatru 12 m/sek 15^{55} — 16^{20}, = 0^{00} — 12^{15} 14^{30} — 24, ⓣ 10^{40} — 12^{10}
11	7	.	35	= 0^{00} — 7^{30}
12	6	.	35	= 3^{10} — 13^{30} 20^{15} — 24, ▽ 1^{35} — 3^{10}
13	7	0.4	32	*° 15^{20} — 17^{15} por wiatru 11 m/sek 11^{30} — 13^{15} = 0^{00} — 9^{30} 15^{30} — 24
14	6	0.7	32	*° 0^{00} 1^{20} 4^{20} — 5^{15} *¹ 9^{30} — 10^{02} *° — 10^{35} ▽° 12^{04-18} *¹ ▽ — 12^{28} *° — 12^{33} *° 14^{36-38} *° — 14^{42} 15^{50} — 14^{15}, por wiatru 12 m/sek 0^{30} — 2^{10} 13 m/sek 3^{30} — 6^{10}, 14 m/sek 13^{30} — 15^{28}, = 0^{00} — 13^{30}
15	7	0.0	32	*° 2^{15} — 5^{30} 6^{15} — 8^{15-28}, = 3^{10} — 10^{30}, ▽ 21^{30} — 24
16	6	3.7	31	*° 17^{20} — 19^{30} — 24, = 2^{40} — 3^{45} = ° — 6^{15} = ¹ — 8^{40} = ° — 10^{50} = — 24, V° 7^{40} — 10^{50}, ▽ 0^{00} — 6^{20}
17	6	2.7	34	*° 0^{00} — 6^{15} *¹ — 7^{30} *° — 7^{50} *¹ — 9^{30} *° — 11^{30} 12^{15} 13^{05} — 14^{15} 15^{05} 19^{35} — 22^{45}, ⊹¹ 14^{15} — 9^{30} ⊹° — 10^{45}, = 0^{00} — 24
18	6	2.8	35	*° 6^{05} — 7^{30} *¹ — 9^{10} △° — 10^{30} *° — 21^{40} 22^{10}, = 0^{00} — 24
19	6	2.5	38	△ 7^{45} — 9^{25}, 9^{40} — 11^{45} *° ... 13^{30} △ 13^{40} — 14^{15} *° 14^{25} — 15^{10}, 15^{15} — 18^{40} *¹ — 19^{15} *° — 23^{10} ... 24, = 0^{00} — 24
20	6	0.2	41	*° 0^{00} — 2^{40} 3^{30} ... 5^{45} 6^{25} — 10^{20}, = 0^{00} — 12^{40} 18^{30} — 24
21	6	1.3	40	= 0^{00} — 24
22	5	1.2	41	*° 0^{10} — 9^{32} △° 9^{40} — 10^{02} *° — 12^{30} *¹ — 13^{05} *° — 13^{30}, ⊹° 10^{20} — 13^{40}, = 0^{00} — 20^{10}
23	7	.	42	= 2^{15} — 12^{30}, ⊕ 10^{30} — 14^{15}
24	6	0.0	40	= 1^{00} — 6^{45} = ° — 7^{50} = — 12^{40} 20^{15} — 24
25	7	0.7	40	*° 6^{36} — 47 7^{32-48} 8^{32} — 9^{20} *¹ — 10^{10} *° — 10^{20}, ⚹ 5^{20} — 7^{10}, = 0^{00} — 11^{20}
26	7	.	40	= 0^{00} — 6^{20}
27	7	0.6	39	*° 13^{17-30} *¹ — 15^{06} *° — 15^{40}, = 13^{17} — 15^{42}
28	7	.	41	⊹° 9^{25} — 14^{50}
29				
30				
31				
Σ	-	32.2	-	

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ *Marzec – Mars* 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	88.8	85.9	81.6	85.4	-15.7	-1.8	-2.9	-5.8	-0.5	-16.6	86	57	82	75	0.3	2.3	0.9	1.2	4	10	10	SE 5	SW 6	SSW 3
2	74.7	72.2	68.7	71.9	1.4	3.6	3.5	3.0	3.9	-3.5	72	72	83	76	1.9	2.2	1.3	1.8	10	10	9	S 4	SSW 5	S 4
3	64.3	67.8	74.1	68.7	1.4	3.2	-1.5	0.4	4.1	-1.6	96	88	72	85	0.3	0.9	1.6	0.9	10	10	0	SSE 3	WSW 4	WSW 6
4	76.7	78.3	81.5	78.8	-4.3	-1.3	-3.5	-3.2	-0.7	-5.1	72	72	81	75	1.2	1.6	0.9	1.2	0	4	10	WSW 8	SW 8	SW 3
5	82.8	83.9	88.8	85.2	-4.0	0.9	-2.9	-2.2	1.3	-5.0	82	62	75	73	0.8	2.5	1.2	1.5	1	5	3	SSW 1	W 4	NW 3
6	92.4	92.8	95.7	93.6	-9.5	-1.3	-4.3	-4.8	-0.7	-10.2	91	72	98	87	0.3	1.6	0.1	0.7	10 ≡	10	10 *	NE 1	NE 7	ENE 5
7	98.5	100.8	102.7	100.7	-4.9	-3.3	-5.3	-4.7	-2.9	-5.4	95	85	87	89	0.2	0.7	0.5	0.5	10 *	10 *	10	NE 5	NE 7	NE 5
8	102.0	100.7	100.4	101.0	-9.5	-2.9	-6.1	-6.2	-2.6	-9.8	82	64	86	77	0.5	1.7	0.5	0.9	9	8	10	ENE 4	NE 5	E 2
9	100.0	100.3	100.1	100.1	-7.1	-1.7	-6.3	-5.4	-0.8	-8.2	91	59	68	73	0.3	2.2	1.2	1.2	10	2	0	WSW 1	NNW 1	NW 2
10	101.7	104.9	106.8	104.5	-4.1	0.2	-3.9	-2.9	1.5	-7.0	94	68	73	78	0.3	2.0	1.2	1.2	8	3	0	NW 3	NW 4	NW 3
11	107.3	108.0	106.9	107.4	-12.3	1.4	-1.8	-3.6	3.3	-12.6	93	63	69	75	0.2	2.5	1.7	1.5	0	7	3	WSW 3	WSW 5	WSW 3
12	106.0	104.9	103.4	104.8	-8.5	1.8	-1.0	-2.2	3.8	-8.9	95	56	75	75	0.2	3.1	1.5	1.6	0	1	0	WSW 2	SW 2	SSE 2
13	103.2	103.1	102.6	103.0	-6.7	4.1	0.4	-0.4	5.4	-8.0	96	50	57	68	0.1	4.1	2.7	2.3	0	0	0	SSE 2	WSW 1	SSE 2
14	102.5	101.5	100.0	101.3	-6.5	6.7	2.6	1.4	9.1	-7.0	86	51	79	72	0.3	4.8	1.6	2.3	0	0	0	SSE 1	SE 2	SSW 1
15	99.4	99.0	98.6	99.0	-2.8	7.2	5.0	3.6	9.2	-3.4	98	59	72	76	0.1	4.2	2.4	2.2	0	0	10	SSE 2	WSW 3	SW 4
16	96.1	93.9	92.4	94.1	3.6	10.2	6.3	6.6	11.5	1.8	90	56	73	73	0.8	5.4	2.5	2.9	8	5	9	SSW 2	SW 2	SW 4
17	92.6	91.1	88.1	90.6	3.6	4.8	4.0	4.1	6.5	1.8	93	92	98	94	0.5	0.7	0.1	0.4	10 •	10 •	10 • ≡	W 3	SSW 1	S 1
18	85.9	85.6	85.7	85.1	0.2	3.0	4.7	3.2	9.3	-0.2	100	93	85	93	0.0	0.6	1.2	0.6	10 ≡	10 ≡	2	SW 3	SW 3	S 3
19	85.5	84.4	87.5	85.1	-1.1	7.8	6.2	4.8	11.0	-1.4	98	73	78	83	0.1	2.8	2.2	1.7	3	2	0	SE 2	SW 2	NW 1
20	91.6	95.8	93.3	92.9	2.7	5.6	1.8	3.0	6.5	0.9	98	66	94	86	0.1	3.1	0.4	1.2	10	10	0	NNE 3	N 2	SW 3
21	89.7	85.8	82.0	85.8	-0.9	7.3	4.8	4.0	9.0	-1.6	99	77	92	89	0.0	2.3	0.7	1.0	10 ≡	10	10 •	SW 2	SSE 2	SW 3
22	84.2	89.3	92.0	88.5	0.6	2.8	-0.6	0.6	5.1	-0.9	92	59	75	75	0.5	3.1	1.4	1.7	10	8	0	N 5	NW 6	N 2
23	92.6	89.9	85.0	89.2	-1.9	5.5	1.6	1.7	6.7	-4.0	94	44	71	70	0.3	5.0	2.1	2.5	0	0	0	ESE 1	SE 4	SE 6
24	81.6	81.2	82.3	81.7	1.5	8.0	4.5	4.6	9.0	0.5	87	68	97	84	0.9	3.4	0.3	1.5	10 •	10	10 •	SE 3	S 4	S 3
25	83.0	86.2	90.5	86.6	3.9	7.2	3.0	4.3	8.8	3.0	100	71	86	86	0.0	2.9	1.1	1.3	10 ≡	9	0	WSW 3	W 6	W 3
26	92.5	91.5	91.7	91.9	0.6	6.4	2.8	3.2	7.7	0.3	96	69	89	85	0.3	3.0	0.8	1.4	6	10	10	SW 2	SSW 3	ESE 3
27	96.6	101.2	106.7	101.5	2.0	4.1	3.8	3.4	5.4	1.3	96	93	87	92	0.3	0.6	1.1	0.7	10 •	10 •	10	NE 4	NE 6	E 3
28	109.0	108.7	107.4	108.4	2.0	9.4	5.9	5.8	10.4	1.6	93	55	68	72	0.6	5.3	3.0	3.0	9	4	9	N 2	SSW 1	SE 2
29	105.5	104.8	103.1	104.5	3.0	7.6	6.6	6.0	8.0	2.8	90	73	96	86	0.8	2.8	0.4	1.3	10	10	10	SSE 1	SW 3	NW 2
30	97.3	92.8	95.9	95.3	5.0	15.8	3.8	7.1	16.9	3.4	97	41	77	72	0.3	10.6	1.9	4.3	6 ≡	3	0	SW 3	W 9	N 7
31	98.3	96.8	96.5	97.2	0.9	4.2	2.2	2.4	7.1	-0.6	71	80	82	78	1.8	1.6	1.3	1.6	8	6	8	WNW 5	N 6	NNE 2
M	92.9	92.9	93.2	93.0	-2.2	4.1	1.1	1.0	5.6	-3.3	91	67	81	80	0.5	2.9	1.3	1.6	6.5	6.4	5.3	2.9	3.9	3.2

Kwiecień – Avril

1	100.9	103.9	103.1	102.6	-0.4	2.6	0.8	1.0	4.6	-1.3	92	55	76	74	0.5	3.4	1.6	1.8	8	7	4	NNW 5	N 7	NW 4
2	96.9	96.5	99.0	97.5	1.7	7.9	3.7	4.2	9.7	0.5	69	56	72	66	2.1	4.6	2.3	3.0	5	7	0	WNW 8	NNW 6	NW 5
3	97.4	94.1	89.8	93.8	1.0	8.4	5.2	5.0	11.5	-0.2	79	69	72	73	1.4	3.4	2.4	2.4	9	2	2	C 0	WSW 2	NNW 6
4	90.3	88.4	86.7	88.5	1.8	12.0	9.0	8.0	14.7	1.1	85	47	64	65	1.1	7.4	4.1	4.2	10	8	8	WSW 5	WNW 6	NE 2
5	89.0	93.1	95.9	92.7	4.0	9.6	3.7	5.2	10.7	2.6	90	65	87	81	0.8	4.2	1.1	2.0	0	1	0	N 4	ENE 6	SSE 2
6	96.8	96.1	93.0	95.5	-1.1	6.0	3.4	2.9	7.8	-1.5	100	69	83	84	0.0	3.0	1.3	1.4	10 ≡	2	0	C 0	SE 5	ESE 4
7	89.4	88.4	89.1	89.0	0.2	15.2	8.6	8.2	17.2	-0.7	96	46	93	78	0.3	9.3	0.8	3.5	10	4	10	SSE 3	SW 2	N 1
8	88.6	88.7	88.7	88.7	5.0	8.8	7.4	7.2	10.4	4.7	92	80	90	87	0.7	2.3	1.0	1.3	10 •	10	9	ENE 3	NE 2	NE 3
9	88.2	88.7	88.9	88.6	5.6	6.6	2.9	4.5	7.8	2.5	86	72	77	78	1.3	2.7	1.7	1.9	10	10	10	NE 5	E 9	ESE 8
10	89.7	91.4	92.2	91.1	1.2	2.4	1.0	1.4	3.3	0.8	81	72	77	77	1.3	2.1	1.5	1.6	10	10	9	E 8	ESE 7	ESE 7
11	90.6	90.3	91.5	90.8	-0.2	6.2	1.4	2.2	6.8	-0.7	76	60	76	71	1.4	3.8	1.7	2.3	10	4	9	SE 8	S 8	SE 7
12	91.0	91.8	92.1	91.6	0.3	5.3	3.6	3.2	8.3	-0.3	82	65	57	68	1.1	3.2	3.4	2.6	10	10	9	SE 6	SE 4	S 5
13	90.2	90.0	90.7	90.3	1.2	7.3	4.6	4.4	10.4	-0.2	89	69	62	73	0.8	3.2	3.3	2.4	8	8	6	SE 2	SE 5	SE 8
14	91.4	93.6	96.0	93.7	1.4	4.8	4.0	3.6	5.9	-0.2	79	67	77	74	1.4	2.9	1.9	2.1	10	10	10	SE 3	SE 3	E 3
15	96.1	95.7	93.8	95.2	3.2	7.0	5.2	5.2	8.7	2.4	76	61	77	71	1.9	3.8	2.0	2.6	10	7	10	ESE 5	ENE 5	ESE 3
16	89.4	87.4	87.1	88.0	3.1	14.4	8.2	8.5	14.7	0.4	91	44	74	70	0.6	9.2	2.9	4.2	2	4	2	ESE 4	SSW 3	S 2
17	87.9	87.7	86.2	87.3	4.0	13.4	7.3	8.0	14.3	2.3	92	56	87	78	0.6	6.8	1.3	2.9	2	7	10	SE 1	C 0	NNW 1
18	78.7	77.0	79.0	78.2	4.7	12.6	9.0	8.8	14.2	3.8	95	50	76	74	0.4	7.4	2.8	3.5	9	10	10	S 3	SW 7	SSW 2
19	78.7	78.0	78.0	78.2	6.5	13.6	10.0	10.0	15.7	6.5	88	51	62	67	1.2	7.6	4.7	4.5	10 •	6	8	ESE 3	S 3	SE 5
20	78.1	78.7	80.1	79.0	7.5	12.9	9.6	9.9	13.5	5.5	80	53	75	69	2.1	7.0	3.0	4.0	10	8	10	SSE 5	SE 7	SE 5
21	77.5	76.5	74.5	76.2	8.2	9.8	9.7	9.4	10.4	6.3	90	78	78	82	1.1	2.7	2.6	2.1	10	10	10	E 5	SE 7	ESE 8
22	69.9	68.3	70.3	69.5	6.6	6.0	5.6	6.0	10.0	5.5	88	83	95	89	1.1	1.6	0.4	1.0	10	10	10	ENE 9	NE 6	SW 3
23	71.4	71.0	73.1	71.8	5.3	6.8	5.0	5.5	9.2	4.8	92	78	94	88	0.7	2.2	0.5	1.1	10	10	10	SW 3	WSW 3	W 4
24	75.8	78.4	81.7	78.6	6.0	8.7	6.6	7.0	10.4	4.5	85	72	81	79	1.5	3.1	1.8	2.1	10	8	4	WSW 6	W 8	W 3
25	85.3	86.6	86.8	86.2	4.6	11.5	8.7	8.4	13.1	2.5	92	60	86	79	0.7	5.5	1.5	2.6	4	6	10 •	WSW 3	SW 6	SW 3
26	86.0	85.6	85.1	85.6	6.2	11.0	6.8	7.7	13.7	4.2	89	74	87	83	1.0	3.4	1.3	1.9	8	9	9	S 2	W 5	NNE 3
27	80.6	79.9	79.9	80.1	5.8	8.6	9.4	8.3	12.2	5.0	98	90	87	92	0.1	1.1	1.6	0.9	10 •	10 •	2	ESE 2	SW 2	SSE 2
28	78.5	78.8	82.0	79.8	8.6	12.0	9.6	10.0	13.5	6.3	93	82	80	85	0.8	2.5	2.4	1.9	9	10	10	SE 4	S 4	SW 3
29	85.4	84.8	85.9	85.4	7.0	14.6	9.6	10.2	15.2	4.0	81	38	74	64	1.9	10.4	3.2	5.2	0	3	0	SW 2	ENE 2	NE 3
30	88.1	89.1	90.3	89.2	8.1	11.4	8.0	8.9	15.2	6.7	89	70	78	79	1.2	4.1	2.4	2.6	9	4	6	NNW 6	NW 2	NW 6
31																								
M	86.6	86.6	87.0	86.7	3.9	9.2	6.3	6.4	11.1	2.6	87	64	78	76	1.0	4.5	2.1	2.5	8.1	7.2	6.9	4.0	4.7	4.0

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w =$ 20,6 anemometr M-47 / 20,1 wiatromierz Wilda **Marzec - Mars 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	0.5	40	
2	7	0.5	40	$*^{0}$ 1^{45} 2^{25} 8^{40} 9^{10} $\bullet^{0}$ 12^{42} 14^{40} – 15^{05} 15^{10-36} 16^{20} 17^{10} 18^{40} 19^{05} = 1^{30} – 6^{20}
3	6	3.8	35	$\bullet^{0}$ 7^{40} 8^{15} $\bullet^{1}$ – 9^{30} $\bullet^{0}$ – 10^{34} = 3^{15} – 13^{20}
4	7	.	32	por. wiatru 15 m/sek 10^{10} – 14^{30}
5	7	.	32	= 2^{20} – 11^{30} 23^{30} – 24 ⊕ 7^{45} – 9^{15}
6	6	6.4	31	$*^{0}$ 18^{30} – 24 = 0^{00} 6^{50} ≡^{1} – 8^{15} ≡^{0} – 9^{40} = – 24; ⊕ 12^{45} – 15^{10}
7	6	0.2	37	$*^{0}$ 0^{00} – 3^{30} 5^{20} 6^{10} 7^{25} – 8^{40} 8^{43} 9^{40} △^{0} 10^{40} – 11^{28} $*^{0}$ 14^{40} ⅄^{0} 15^{15} – 17^{10} $*^{0}$ – 18^{20} 18^{30} 20^{20} 21^{30} 22^{15}; = 0^{00} – 24
8	7	0.0	37	△^{0} 17^{35} – 18^{10} $*^{0}$ 21^{40} – 24; = 0^{00} – 11^{30} 19^{30} – 24
9	7	0.0	37	$*^{0}$ 0^{00-30} 0^{40} – 1^{20} 7^{15} 9^{35}; = 0^{00} – 10^{30}
10	7	0.0	36	$*^{0}$ 2^{40} 4^{50} 6^{35} 7^{15} 7^{20} 8^{15}; = 0^{00} – 12^{15}
11	7	.	35	
12	7	.	31	= 4^{30} – 12^{20} 23^{15} – 24
13	7	.	30	= 0^{00} – 11^{15}; ⌣^{1} 2 – 4 ⌣^{0} 5 – 10
14	7	.	29	= 0^{30} – 11^{20}
15	7	.	29	= 1^{30} – 10^{30}
16	7	0.0	22	⊕ 13^{45} – 15^{15}
17	5	7.0	19	$\bullet^{0}$ 5^{45} 7^{15} 7^{40-46} 8^{05} 10^{10} 11^{35} 12^{15} – 17^{15} 21^{30} – 24; = 1^{15} – 15^{10} ≡^{0} – 15^{27} ≡^{1} – 15^{45} ≡^{2} – 24
18	5	.	14	≡^{0} 0^{00} – 11^{30} ≡^{1} – 11^{45} ≡^{0} – 12^{50} = – 24
19	6	0.0	12	= 0^{00} – 7^{40} ≡^{0} – 7^{45} ≡^{1} – 8^{30} ≡^{2} – 9^{17} ≡^{1} – 10^{10} ≡^{0} – 10^{20} = – 13^{35} 19^{40} – 24
20	6	0.3	9	$\bullet^{0}$ 6^{20} 7^{20} $\bullet^{0}$ 7^{30} 8^{15} $\bullet^{0}$ 8^{40} 9^{40}; = 0^{00} – 14^{30} 19^{40} – 24
21	7	3.1	pż.	$\bullet^{0}$ 6^{04} – 25 19^{10} 21^{30} – 24; = 0^{00} – 2^{45} ≡^{1} – 7^{40} ≡^{0} – 7^{50} = – 12^{10} 19^{20} – 24
22	7	0.0	pż.	$\bullet^{0}$ 0^{00} – 1^{45} $*^{0}$ 8^{48} 9^{10}; = 0^{00} – 10^{15}
23	7	0.0	pż.	⌣^{0} 2 – 9
24	7	4.2	pż.	$\bullet^{0}$ 6^{20} 7^{15} 15^{35} 17^{30} – 24; = 5^{30} – 11^{30} 16^{15} – 24
25	7	1.4	pż.	$\bullet^{0}$ 0^{00} – 4^{15} 6^{45-50} 7^{05} – 8^{45}; = 0^{00} – 4^{45} ≡^{1} – 6^{15} ≡^{2} – 7^{15} ≡^{0} – 7^{40} = – 12^{10}
26	7	0.5	pż.	= 0^{00} – 11^{15}; ⌣^{0} 2^{00} – 6^{30}
27	6	5.0	pż.	$\bullet^{0}$ 3^{55} 6^{05} – 7^{20} 10^{15} – 12^{25} 12^{30} 15^{20} $\bullet^{0}$ 16^{30} – 17^{10} 23^{10} – 24; = 0^{30} – 24
28	7	.	.	$\bullet^{0}$ 0^{00} – 45; = 0^{00} – 10^{30}
29	7	0.5	.	$\bullet^{0}$ 13^{45} 14^{15} – 16^{35} 17^{25} – 18^{05}; = 3^{30} – 9^{45} 13^{30} – 15^{30} ≡^{1} – 15^{50} ≡^{1} – 19^{30} ≡^{0} – 19^{45} = – 24
30	7	.	.	por. wiatru do 14 m/sek 12^{20} – 24; = 0^{00} – 4^{45} ≡^{1} – 5^{30} ≡^{0} – 6^{45} = – 9^{30}
31	7	1.1	.	⅄^{0} 12^{25-35} 13^{05-12} 14^{40-50} ⛈^{0} 16^{40-50} ⛈^{0} 19^{25-31} ⅄^{1} 20^{40} – 21^{10}; por. wiatru 13 m/sek 9^{20} 10^{40} 11^{10} – 12^{30}; = 20^{20} 24
Σ	–	34.5	–	

Kwiecień - Avril

1	7	.	.	= 0^{00} – 5^{30}
2	8	.	.	por. wiatru 11 m/sek 4^{30} – 7^{10}
3	7	.	.	= 22^{30} – 24
4	7	0.3	.	= 0^{00} – 9^{30} ⊕ 16^{10} – 17^{40}
5	7	.	.	$\bullet^{0}$ 3^{07-30}; = 0^{00} – 4^{40}
6	7	.	.	= 1^{15} – 6^{02} ≡^{1} – 8^{20} ≡^{0} – 8^{50} = – 12^{15} 23^{30} – 24; ⌣^{0} 1 – 6
7	7	3.8	.	⛈^{0} 17^{40} – 18^{03} 18^{10-30} 19^{30} – 20^{10}; = 0^{00} 12^{30} 17^{40} – 24; ⌣^{0} 1 – 3 ⌣^{1} 4 – 7
8	6	1.2	.	⛈^{0} 3^{20-32} $\bullet^{0}$ 5^{40} 6^{15} – 7^{40} $\bullet^{0}$ – 8^{20}; = 0^{00} – 14^{40} 18^{30} – 24
9	7	.	.	por. wiatru 14 m/sek 13^{40} – 16^{30} ≋ 17^{10} – 18^{20} 19^{25-40}; por. wiatru 13 m/sek 20^{45} – 23^{30}; = 0^{00} – 12^{15}
10	7	.	.	por. wiatru 14 m/sek 1^{30} – 4^{20}; = 0^{45} – 1^{30}
11	7	.	.	por. wiatru 14 m/sek 1^{15} – 2^{40}
12	7	.	.	
13	7	.	.	$\bullet^{0}$ 11^{47-53}; ⌓ 20^{45} – 24
14	7	.	.	⌓ 0^{00-30}
15	7	.	.	
16	7	0.2	.	⛈^{0} 13^{55} – 14^{23}; ⌣^{0} 3 – 6^{30}
17	7	.	.	= 4^{40} – 8^{30}
18	7	0.9	.	$\bullet^{0}$ 13^{45} 14^{10} 15^{05} 17^{05}; = 2^{10} – 8^{30} 16^{30} – 17^{05}; ⊕ 8^{50} – 10^{15}
19	7	1.3	.	$\bullet^{0}$ 0^{20-30} 0^{35-50} 1^{40} 2^{15} 3^{15} – 31 5^{10} 6^{20} – 9^{25}; = 0^{30} – 11^{30}
20	7	0.0	.	⛈^{0} 12^{25-30}; por. wiatru 13 m/sek 10^{30} – 11^{45}; = 23^{30} – 24
21	6	2.9	.	$\bullet^{0}$ 6^{45} 8^{03} 16^{30} 17^{17}; = 0^{00} – 24
22	7	2.0	.	$\bullet^{0}$ 1^{35} 3^{10} – 4^{40} 5^{45} 7^{05} – 20 ⛈^{0} 11^{35-45} 12^{55} 13^{16} 13^{22-41} 15^{52} 16^{15} $\bullet^{0}$ 16^{20} 17^{39} 21^{20} – 22^{40}; por. wiatru 14 m/sek 5^{30} 9^{30}; = 0^{00} – 5^{45}; 16^{30} – 24
23	7	2.7	.	⛈^{0} 15^{45} – 16^{10} 17^{30} 19^{10} $\bullet^{0}$ – 20^{20} 21^{38} 23^{40}; = 0^{00} – 7^{40} 18^{10} – 24
24	7	0.0	.	⛈^{0} 10^{17-42} 11^{50} – 12^{10} 13^{33-41} 17^{06-16}; = 0^{00} – 8^{30}
25	7	1.0	.	⛈^{0} 17^{24-36} ⛈^{1} – 17^{28} ▲^{0} 17^{25-27} ⛈^{0} 17^{28-29} 20^{20-41}; = 0^{00} – 8^{20}
26	7	5.6	.	⛈^{0} 10^{08-12} ⛈^{1} 10^{55} – 11^{08} ⛈^{0} – 11^{28} 13^{45} – 14^{10} $\bullet^{0}$ 14^{15} 15^{12} 16^{40} 17^{15} 23^{38} – 24; K^{0}S $11^{02-10-18}$ N; = 1^{30} – 9^{15} 22^{30} – 24
27	6	5.6	.	$\bullet^{0}$ 0^{00} 3^{10} – 11^{40} ⛈^{0} 12^{30} 13^{05} 21^{45} – 22^{10}; = 0^{00} – 14^{30}
28	7	3.7	.	⛈^{0} 11^{16-47} 12^{12-20} 12^{30-42} 13^{51} 14^{06} ⛈^{1} – 14^{10} ⛈^{0} – 14^{25}
29	7	.	.	
30	7	1.9	.	⛈^{0} 10^{23-28} ⛈^{1} 10^{45-50} ⛈^{0} – 11^{10} 11^{40-50} ⛈^{1} – 11^{55} ⛈^{0} – 12^{10}; K^{0} W 10^{45} – 11^{10} – (K) SE 11^{30}
31				
Σ	–	33.1	–	

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ *Maj – Mai* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N_w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_w I	II	III
1	90.9	90.7	90.2	90.6	6.2	12.7	7.2	8.3	13.8	3.5	57	31	62	50	4.1	10.1	3.9	6.0	0	5	0	NW 6	NNW 7	NW 4
2	93.4	94.3	94.3	94.0	1.4	7.0	4.0	4.1	8.3	−0.1	81	51	66	66	1.3	4.9	2.8	3.0	2	8	4	N 6	NNE 5	N 2
3	93.8	94.4	95.5	94.6	1.9	6.8	3.2	3.8	9.0	−0.8	76	54	66	65	1.7	4.5	2.6	2.9	4	9	0	NNW 4	ENE 6	NE 2
4	96.7	95.2	91.5	94.5	2.8	9.6	5.0	5.6	10.9	−1.7	70	39	60	56	2.2	7.4	3.5	4.4	0	1	0	ENE 1	ESE 5	ESE 4
5	85.3	84.2	82.5	84.0	4.0	6.7	5.7	5.5	8.9	1.3	70	82	97	83	2.4	1.7	0.3	1.5	10	10 •	10 •	SE 4	S 3	SE 4
6	81.4	82.9	85.9	83.4	6.4	10.1	7.8	8.0	11.5	5.2	97	76	91	88	0.3	3.0	0.9	1.4	10	10	10	ENE 3	NE 2	NNE 1
7	88.5	89.9	91.1	89.8	7.0	10.5	7.2	8.0	11.9	6.0	87	69	81	79	1.3	4.0	2.0	2.4	10	10	0	NNW 4	NNW 3	C 0
8	90.0	88.9	90.8	89.9	3.0	16.8	12.6	11.2	17.0	1.1	100	42	77	73	0.0	11.1	3.4	4.8	10 ≡	6	9	SW 3	SW 3	NW 3
9	91.0	87.9	80.2	86.4	8.1	15.0	12.2	11.9	15.8	5.0	94	67	90	84	0.6	5.5	1.4	2.5	8	10	10	WSW 3	WNW 5	SW 3
10	78.9	78.3	79.3	78.8	9.2	9.9	6.2	7.9	12.8	6.1	72	76	94	81	3.2	3.0	0.6	2.3	8	8	6	W 7	W 9	WSW 5
11	80.0	83.4	88.6	84.0	7.1	11.6	9.0	9.2	12.9	4.7	90	61	95	81	1.0	5.3	0.8	2.4	10	9	10 •	SW 2	SE 2	SW 1
12	92.7	94.6	95.7	94.3	9.3	16.8	9.9	11.5	17.7	7.5	85	48	89	74	1.7	9.9	1.3	4.3	2	4	0	N 6	NNE 6	N 4
13	95.8	95.9	95.2	95.6	7.8	16.0	10.6	11.2	18.2	7.1	75	48	64	62	2.7	9.6	4.6	5.6	9	3	0	NNW 6	N 6	NNW 3
14	92.6	90.5	89.7	90.9	10.0	17.9	12.0	13.0	18.5	6.8	76	38	75	63	3.0	12.7	3.5	6.4	5	7	9	N 3	NE 1	NW 2
15	88.2	87.4	88.0	87.9	12.0	16.0	11.6	12.8	17.7	9.5	84	58	75	72	2.2	7.7	3.4	4.4	9	8	1	NW 2	NW 4	ENE 4
16	87.1	86.6	85.4	86.4	8.0	15.0	13.4	12.4	15.7	6.7	71	58	86	72	3.1	7.1	2.1	4.1	10	10	10	ESE 3	SSE 5	SSE 3
17	85.2	85.2	84.0	84.8	12.2	20.4	17.2	16.8	22.7	10.8	98	54	78	77	0.3	11.0	4.3	5.2	10 ≡	8	1	WSW 4	SW 3	SW 3
18	81.2	83.5	83.8	82.8	17.4	22.4	17.6	18.8	25.2	13.4	83	52	80	72	3.4	13.0	4.0	6.8	4	6	2	SW 6	W 7	ESE 2
19	78.5	77.6	82.5	79.5	16.2	26.3	13.2	17.2	27.8	12.9	82	43	83	69	3.2	19.5	2.6	8.4	4	8	3	SW 2	SW 5	NNW 6
20	92.0	95.2	98.4	95.2	3.0	6.2	5.2	4.9	13.4	2.6	93	78	95	89	0.6	2.2	0.4	1.1	10 •	10	4	NNE 3	C 0	WSW 3
21	102.8	103.5	104.2	103.5	5.2	12.2	8.2	8.4	14.6	1.0	90	47	70	69	0.8	7.6	3.3	3.9	0	4	3	SW 1	S 1	N 2
22	103.3	102.8	100.1	102.7	9.4	16.1	11.4	12.1	19.1	3.3	65	41	63	56	4.1	10.7	5.0	6.6	6	7	5	ENE 3	SE 3	NE 3
23	98.4	96.9	96.2	97.2	10.8	10.8	9.4	10.1	12.8	9.2	72	84	96	84	3.7	2.2	0.5	2.1	10	10 •	10 •	SE 6	E 10	E 7
24	93.9	93.0	92.3	93.1	9.8	14.8	12.8	12.6	16.9	9.1	90	82	94	89	1.3	3.1	0.9	1.8	10	8	8	ESE 5	SE 4	S 2
25	92.0	91.4	92.2	91.9	11.6	17.4	12.4	13.4	18.3	10.4	100	67	96	88	0.0	6.6	0.5	2.4	10 ≡	9	10	SSW 2	WSW 5	WSW 2
26	92.5	93.0	92.4	92.6	11.2	14.9	12.6	12.8	16.6	10.9	96	72	94	87	0.5	4.7	0.9	2.0	10	10	8	NW 2	W 3	SW 3
27	92.1	90.9	90.0	91.0	8.6	17.6	14.5	13.8	20.1	7.2	100	48	82	77	0.0	10.4	2.9	4.4	10 ≡	4	10 •	SW 2	SW 5	E 1
28	88.3	86.9	84.2	86.5	12.0	16.8	14.6	14.5	18.9	10.9	91	79	94	88	1.2	4.1	0.9	2.1	10 •	9	10	ENE 2	ENE 5	ENE 3
29	80.1	78.5	79.3	79.3	14.2	17.9	12.2	14.1	18.6	12.0	92	71	94	86	1.3	5.9	0.9	2.7	10	9	10	SE 1	SW 2	NNE 3
30	81.3	83.6	86.3	83.7	8.2	15.0	8.4	10.0	15.4	7.5	97	58	74	76	0.3	7.1	2.8	3.4	10 •	4	0	NNW 6	NW 5	NW 2
31	88.1	88.5	87.3	88.0	8.8	16.8	14.0	13.4	18.5	3.3	80	56	90	75	2.3	8.4	1.6	4.1	8	10	10	E 2	ESE 5	SE 2
M	89.6	89.5	89.6	89.6	8.5	14.3	10.4	10.9	16.1	6.2	84	59	82	75	1.7	7.2	2.2	3.7	7.4	7.5	5.6	3.5	4.2	2.9

Czerwiec – Juin

1	82.9	83.2	85.8	84.0	14.2	23.6	15.6	17.2	23.8	12.6	94	38	72	68	0.9	17.9	5.0	7.9	10	5	6	S 4	SW 7	SW 1
2	88.2	90.2	93.3	90.6	12.2	13.7	10.3	11.6	16.2	10.3	76	60	80	72	3.4	6.4	2.5	4.1	7	9	8	W 4	W 6	W 4
3	94.6	95.1	94.5	94.7	11.3	19.3	14.2	14.9	21.0	6.7	73	44	67	61	3.6	13.0	5.3	7.3	0	4	8	WSW 5	W 3	SW 1
4	94.9	93.8	92.2	93.6	14.8	22.2	16.6	17.6	22.6	8.3	72	37	67	59	4.7	16.8	6.3	9.3	1	10	10 •	E 2	SE 4	E 5
5	89.1	86.1	83.7	86.3	13.4	15.3	13.4	13.9	17.0	12.9	96	87	94	92	0.6	2.3	0.9	1.3	10 •	10	10 •	SE 3	E 5	E 3
6	79.3	78.7	79.6	79.2	12.4	13.4	11.0	12.0	13.9	10.9	99	94	99	97	0.2	0.9	0.1	0.4	10	10 •	10 •	NE 5	NNE 6	NNE 6
7	83.6	86.2	88.1	86.0	10.4	16.2	12.4	12.8	19.8	9.6	88	65	75	76	1.4	6.5	3.5	5.8	10	7	0	NNW 5	NW 3	C 0
8	90.5	89.9	88.2	89.5	13.7	22.0	15.0	16.4	22.6	7.5	82	39	65	62	2.9	16.0	5.9	8.3	0	6	3	C 0	SE 4	E 4
9	85.9	84.4	84.7	85.0	14.8	19.8	14.0	15.6	22.8	11.1	84	68	97	83	2.7	7.3	0.6	3.5	4	9	9	SE 5	SE 5	NNE 5
10	84.4	84.5	82.3	83.8	14.8	19.0	14.8	15.8	20.5	13.0	90	61	90	80	1.6	8.7	1.6	4.0	4	5	9	SSE 2	ENE 5	NE 3
11	78.8	79.1	79.8	79.2	13.4	16.6	12.2	13.6	17.5	11.9	94	73	96	88	0.9	5.2	0.5	2.2	9	10	8	ESE 3	S 2	NE 2
12	83.5	85.0	87.3	85.3	12.8	17.1	13.8	14.4	20.2	10.9	94	75	92	87	0.9	4.9	1.3	2.4	10	7	6	NNE 4	N 4	NW 4
13	89.6	90.3	89.3	89.7	12.8	15.4	12.5	13.3	16.4	11.6	78	57	80	72	3.3	7.6	2.9	4.6	4	9	3	NW 6	WNW 7	W 4
14	88.6	89.1	89.8	89.2	13.1	15.4	13.2	13.7	16.0	8.0	86	71	96	84	2.1	5.1	0.6	2.6	8	9	10	NW 5	N 7	N 4
15	92.3	94.0	93.6	93.3	10.8	17.8	14.5	14.4	20.6	10.1	87	70	75	77	1.7	6.1	4.1	4.0	10	9	4	NNW 6	ENE 2	W 2
16	94.2	93.2	89.7	92.4	15.2	22.6	18.4	18.6	24.3	9.8	80	42	68	63	3.5	15.8	6.8	8.7	2	3	2	WSW 1	SW 2	S 3
17	85.8	83.3	84.0	84.4	16.6	23.8	16.4	18.3	25.1	11.3	75	41	79	65	4.8	17.3	3.8	8.6	0	3	3	S 2	SSW 6	W 4
18	89.9	92.4	92.9	91.7	14.0	17.8	14.6	15.2	19.9	12.9	79	60	77	72	3.4	8.2	3.8	5.1	9	9	9	NNW 5	WNW 4	SW 2
19	90.7	90.1	92.0	90.9	14.3	17.0	17.2	16.4	22.0	12.2	82	41	66	63	2.9	11.6	6.7	7.1	9	10 •	8	SW 4	NW 6	WNW 7
20	95.3	96.2	96.2	96.0	15.2	20.8	16.4	17.2	22.2	11.1	76	48	63	62	4.3	12.7	7.9	8.3	0	7	9	W 4	NW 7	NW 3
21	97.5	96.9	94.6	96.3	16.4	23.2	16.8	18.3	23.9	11.1	73	42	71	62	5.1	16.3	5.5	9.0	0	4	3	WSW 1	SW 2	E 3
22	92.0	90.3	87.9	90.1	16.0	27.7	21.8	21.8	28.6	10.1	84	48	72	68	2.9	19.2	7.4	9.8	3	4	3	SE 2	SW 1	S 3
23	87.6	90.2	91.6	89.8	19.6	24.0	19.2	20.5	25.9	16.5	87	57	66	70	3.0	12.9	7.5	7.8	10	5	0	SW 3	SW 2	SW 3
24	94.2	94.1	94.3	94.2	19.3	26.2	20.6	21.7	27.8	13.3	73	49	64	62	6.0	17.3	8.7	10.7	1	4	3	C 0	WNW 4	NNW 2
25	95.4	95.3	95.9	95.6	20.0	27.7	20.4	22.1	28.1	15.3	68	44	66	59	7.4	20.7	8.1	12.1	2	4	0	WSW 3	WNW 3	NE 3
26	95.6	94.4	96.2	95.4	20.1	30.3	18.6	21.9	31.9	14.6	75	45	95	72	5.8	23.5	1.0	10.1	0	1	10 • K	SE 2	SSW 2	NW 9
27	96.6	96.7	94.6	96.0	20.0	26.2	20.9	22.0	27.3	17.1	87	56	84	76	3.1	14.9	4.0	7.3	0	0	10 • K	N 5	NE 3	NNW 3
28	95.4	97.9	98.4	97.2	15.2	15.4	12.8	14.0	21.0	12.8	99	99	92	97	0.2	0.2	1.2	0.5	10	10 •	5	N 5	N 3	NW 2
29	97.2	95.3	96.6	96.4	14.4	20.2	15.0	16.2	21.7	9.2	77	56	77	70	3.8	10.4	3.8	6.0	3	7	0	NW 4	WNW 6	WNW 3
30	97.5	96.1	92.0	95.2	15.1	22.6	17.9	18.4	24.6	11.4	68	49	70	62	3.3	13.9	6.1	8.5	0	1	0	NNW 2	W 4	SSW 1
31																								
M	90.4	90.4	90.3	90.4	14.9	20.4	15.7	16.7	22.2	11.5	82	57	78	72	3.1	11.3	4.1	6.2	4.9	6.4	5.6	3.5	4.2	3.3

Sandomierz $H_s = 202\,m$ $H_b = 200.3\,m$ $h_w =$ 20.6 m anemometr M-47 / 20.1 m wodromierz Wilda **Maj - Mai 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘB. ŚNIEGU h	POGODA
1	7	•	•	
2	7	•	•	= 2^30 – 6^30, ⌣° 2 – 6
3	7	0.0	•	⁂° 7^16 – 25, 7^28 – 32, 12^44 – 45, 12^46 – 49; ⌣° 3 – 6
4	7	•	•	⌣° 1 – 7
5	6	5.2	•	•° 9^12 … 10^30 – 11^35 … 16^15 – 19^35, 24; = 12^10 – 24
6	7	•	•	•° 0^00 … 2^15; = 0^00 – 12^20, 18^30 – 24
7	7	•	•	= 0^00 – 9^30, 21^15 – 24; ⌒° 20^30 – 21 ⌒¹ 22 – 24
8	7	•	•	= 0^00 – 5^10 ≡¹ – 8^15 ≡° – 8^45 = – 10^15; ⌒¹ 0^00 – 5^10
9	7	4.1	•	⁂° 11^09 – 11, 12^10 – 22, 13^38 – 14^15, 15^40 – 46, 16^09 – 10 ⁂¹ – 16^17 •° … 17^30, 17^35 18^20, 18^30 … 19^15, 22^35 … 23^10 – 24; = 1^00 – 7^30, 17^30 – 24; ⌒° 3 – 8
10	7	2.1	•	•° 0^00 – 40 ⁂° 10^23 – 40, 12^08 – 23, 19^15 – 35; (K)° SE 14^07 – K° 14^20 – 35 NE; por. wiatru 10 m/sek 14^10 – 7^15, 14 m/sek 7^40 – 8^15, 9^45 – 10^45; = 0^00 – 3^30
11	7	2.5	•	⁂° 10^20 – 11^20, 13^53 – 14^05, 15^18 – 16^20, 18^43 – 55 •° 19^15 – 22^30; = 1^30 – 8^30, 19^30 – 24
12	7	•	•	= 0^00 – 7^30, ⌒° 21 – 24
13	7	•	•	⌒° 0^00 – 4
14	7	•	•	
15	7	•	•	⁂° 10^25 – 29; ⌒° 4 – 8, 22 – 24
16	7	1.1	•	•° 22^23 – 23^40, 24; = 22^30 – 24, ⌒° 0^00 – 6
17	7	0.8	•	•° 0^00 … 17; = 0^00 – 4^50 ≡¹ – 5^30 ≡° – 7^20 = – 8^40
18	7	0.2	•	⁂¹ 7^15 – 25 ⁂° – 7^45 17^08 – 13; = 1^00 – 6^20 22^30 – 24; ⌒° 20 – 24
19	7	2.8	•	⁂° 17^40 – 43 ⁂¹ 17^54 ⁂° – 18^03 ⁂¹ 18^47 – 48 ⁂° 23^05 – 30 (K)° SW 17^34 – 17^50 18^15 NE; por. wiatru 13 m/sek 13^46 – 14^15 ⁂ 15^45 – 18^20 (por. do 20 m/sek), por. wiatru 13 m/sek 19^30 – 20^10 21^20 – 22^30;
20	7	1.6	•	•° 4^07 … 6^30 – 7^35, 7^45 – 8^15 12^15 ⁂° 14^41 – 15^26 •° 15^40 – 17^45; = 0^00 – 12^00, 16^30 – 24 [19.V: = 0^00 – 6^15; ⌒° 0^00 – 2 ⌒¹ 3 – 4 ⌒² 5 – 8
21	7	•	•	= 0^00 – 4^45 ≡¹ – 5^10 ≡° – 5^40 = – 7^30; ⌒° 22 – 24
22	7	•	•	⌒¹ 0^00 – 5 ⌒° 6 – 9
23	7	10.8	•	•° 10^07 … 12^45, 16^52 18^05 – 23^35; por. wiatru 16 m/sek 7^32 – 8^40 ⁂ – 14^16, por. wiatru 13 m/sek 14^16 – 15^40; = 17^30 – 24
24	6	5.4	•	•° 6^10 … 7^20 8^25 … 10^10 – 40 15^05 … 20 – 25 •¹ – 15^35 •° – 15^45 16^10 … 30; = 0^00 – 12^35, 20^15 – 24
25	7	6.4	•	•° 1^40 – 2^35 ⁂° 13^24 – 27, 15^10 – 15 ⁂¹ – 15^29 ⁂² – 15^38 – 15^45 17^04 ⁂² – 17^19 ⁂¹ – 17^44 ⁂° – 17^56 ⁂¹ – 18^04 ⁂² – 18^12 (K)° SW 14^50 – N – NE 15^24 (K)° SW 15^20 – N 15^45 (K)° SW 15^47 – NE 17^50;
26	7	•	•	= 0^00 – 9^45 [25.V: = 0^00 – 3^45 ≡² – 4^15 ≡¹ – 4^30 ≡° – 5^20 ≡¹ – 6^45 ≡° – 7^05 = – 9^40; 22^30 – 24
27	7	1.5	•	•° 20^12 … 22^30 – 23^35; = 1^00 – 4^15 ≡° – 2^30 ≡¹ – 7^15 ≡° – 7^45 = – 10^30, 20^30 – 24; ⊕ 10^45 – 12^10
28	6	1.4	•	•° 5^40 … 7^20 – 8^05 … 15, 10^45 … 11^05; = 0^00 – 14^10, 20^30 – 24
29	7	5.3	•	•° 10 … 35, 3^15 – 4^45 ⁂° 11^16 – 45, 13^20 – 55, 14^15 – 35, 15^40 – 16^05, 16^40 – 17^10; = 0^00 – 8^45, 20^30 – 24
30	7	0.1	•	•° 2^40 … 3^05 – 7^05 … 14; = 0^00 – 7^30, ⌒° 20 – 24
31	7	6.4	•	⁂° 18^20 – 19^35, 23^10 – 21; = 22^30 – 24; ⌒° 0^00 – 2 ⌒¹ 3 – 4 ⌒² 5 – 6 ⌒¹ 7 – 9; ⊕ 10^30 – 11^45
Σ	–	55.7	–	

Czerwiec - Juin

1	7	0.5	•	⁂° 0^00 – 1^30 •° – 2^10 •¹ – 2^45; = 0^00 – 8^30, ⌒° 22 – 24
2	7	•	•	⁂° 0^05 – 17, por. wiatru 14 m/sek 16^05 – 17^30, ⌒° 21 – 23
3	7	•	•	⌒¹ 0^00 – 8 ⌒° 20 – 24
4	7	2.1	•	•° 17^50 … 18^22 20^30 … 45; ⌒° 0^00 – 2 ⌒¹ 3 – 7 ⌒° 8 – 9; ⊕ 10^45 – 15^10
5	6	4.4	•	•° 0^00 1^45 •¹ 2^10 – 3^20 •° – 3^40 5^10 – 7^05 7^25 … 40 – 9^28 12^50 … 16^25 17^46 – 24; = 2^30 – 24
6	6	1.0	•	•° 0^00 … 2^40, 10^20 … 11^10 12^25 14^20 16^35 17^10 – 18^15 … 35 •° – 20^45, 21^20 – 46 •¹ 21^46 – 22^10 •° – 23^20 … 24; = 0^00 – 24
7	7	•	•	•° 0^00 – 50 •° 1^00 … 3^15; = 0^00 – 9^30; ⌒° 20 – 24
8	7	•	•	= 4^10 – 6^30, ⌒° 0^00 – 2 ⌒¹ 3 – 4 ⌒² 5 – 7 ⌒° 8 – 9
9	7	5.6	•	⁂° 16^27 – 30 ⁂¹ – 16^53 ⁂° – 18^15; (K)° N 16^43 – 16^55 – 17^30 NE
10	7	11.5	•	⁂° 11^40 – 45 ⁂¹ 18^48 – 54 ⁂° – 19^05 •° 21^48 – 22^15, 22^25 – 23^05 •¹ – 23^48 •° – 24; = 0^30 – 5^10, 22^15 – 24
11	7	5.2	•	•° 0^00 – 3^05 ⁂° 13^30 – 14^20 •° – 18^15 ⁂° 21^50 – 22^20; = 0^00 – 5^30, 16^30 – 19^10, 20^30 – 24
12	7	0.4	•	⁂° 6^44 – 50 •° 8^40 – 9^20 ⁂° 23^10 – 30 •° 23^35, 24; = 0^00 – 10^30, 21^20 – 24
13	7	•	•	•° 0^00 … 1^20; = 0^00 – 5^30
14	7	6.1	•	⁂° 13^45 – 14^05, 14^15 – 16^10 •° – 17^15 ⁂° 18^01 – 43 •° 19^05 – 20^12; = 2^30 – 6^15, 2^40 – 24; ⌒° 1 – 9
15	7	•	•	= 0^00 – 9^30, ⌒° 20 – 24
16	7	•	•	= 1^15 – 4^30, ⌒° 0^00 – 3 ⌒¹ 4 – 9 ⌒° 20 – 24
17	7	0.0	•	⌒° 0^00 – 6^30, 23 – 24
18	7	0.0	•	⁂° 5^02 – 07; ⌒° 0^00 – 5
19	6	1.7	•	•° 1^50 … 2^03 ⁂° 11^35 – 50 ⁂¹ – 11^58 ⁂° – 12^05, 12^30 – 13^05 •° 14^20 … 35; (K)° NW 11^40 – 11^50 – 12^25 SE < ° S 22^16 – 23^30 SW; = 10^40 – 11^30
20	7	•	•	
21	7	•	•	
22	7	•	•	
23	7	•	•	⌒° 4 – 7, 22 – 24
24	7	•	•	⌒° 0^00 – 7
25	7	•	•	⌒° 2 – 5
26	7	4.0	•	⁂° 20^25 – 29 ⁂¹ – 21^07 ⁂° – 21^35; (K)° NW 20^05 – K° 20^15 – 30 – (K)° SE 21^40; por. wiatru 18 m/sek 19^30 – 20^03, 14 m/sek 20^25 – 37; = 21^30 – 24; ⌒° 1 – 8; S 19^35 – 50
27	7	9.2	•	⁂° 20^05 – 23^15, 23^35 – 24; (K)° W 20^05 – K° 20^34 – 45 – (K)° E 23^45; = 0^00 – 2^30
28	6	11.4	•	⁂° 0^00 – 07 0^45 – 1^08 2^35 – 3^15 •° – 6^05, 7^15 – 12^40 13^30 – 14^02 ⁂¹ – 14^16 ⁂° – 14^43, 15^58 – 16^16; = 1^30 – 18^30
29	7	•	•	⌒° 22 – 24
30	7	•	•	⌒° 0^00 – 9, 20 – 24
31				
Σ	–	60.9	–	

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — *Lipiec – Juillet* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	88.2	87.7	89.3	88.4	17.0	23.2	16.2	18.2	24.9	13.7	85	65	93	81	3.0	10.0	1.4	4.8	2	10	10	SW 4	NW 5	NW 1
2	89.4	88.4	87.2	88.3	13.4	16.0	13.8	14.2	18.7	13.0	95	75	94	88	0.7	4.5	0.9	2.0	10 •	10	1	NNE 1	WSW 1	WNW 2
3	86.9	86.6	86.9	86.8	13.0	16.6	10.8	12.8	17.4	10.4	83	67	96	82	2.6	6.3	0.5	3.1	9	10	10 •	WSW 4	NW 2	WNW 3
4	88.3	87.4	86.3	87.3	11.6	16.4	11.4	12.7	18.4	7.5	90	56	95	80	1.3	8.2	0.7	3.4	3	10	10	W 3	SW 2	C 0
5	85.4	84.1	85.9	85.1	11.2	15.2	11.0	12.1	15.5	8.5	92	63	96	84	1.0	6.3	0.5	2.6	9	10 •	4	NNE 3	N 2	SW 3
6	90.0	90.3	91.0	90.4	11.4	15.4	10.9	12.2	17.5	7.5	79	50	87	72	2.8	8.7	1.6	4.4	2	7	9	NW 3	W 8	W 4
7	92.7	91.4	88.9	91.0	11.0	18.8	15.4	15.2	20.3	7.5	86	54	78	73	1.8	10.1	3.9	5.3	8	8	3	SW 4	NW 4	SW 2
8	87.4	83.7	79.7	83.6	15.0	24.2	17.0	18.3	25.2	7.5	80	43	91	71	3.4	17.4	1.8	7.5	9	2	10 •	SSW 4	SW 7	W 4
9	83.7	87.2	89.6	86.8	14.4	15.9	12.1	13.6	18.2	7.5	86	67	75	76	2.4	6.0	3.5	4.0	7	8	1	NW 3	WNW 5	W 3
10	92.0	92.0	93.3	92.4	11.3	17.8	11.0	12.8	19.2	7.0	84	52	92	76	2.2	9.8	1.0	4.3	3	7	4	W 3	WSW 4	C 0
11	95.6	95.9	96.3	95.9	11.3	17.1	12.6	13.4	19.0	6.7	91	57	86	78	1.2	8.3	2.1	3.9	0	8	0	NW 3	W 3	SW 2
12	96.2	93.8	92.5	93.8	11.2	21.6	18.6	17.5	22.5	7.0	91	49	60	67	1.2	13.2	8.3	7.6	6	2	10	SW 2	SSW 5	SW 1
13	92.1	92.5	93.2	92.6	17.2	23.3	18.8	19.5	23.2	14.6	91	55	76	74	1.8	12.8	5.1	6.6	10	5	0	NW 1	NNW 1	WNW 3
14	95.2	95.5	95.2	95.3	17.9	27.0	22.0	22.2	28.7	13.9	91	48	68	69	1.8	18.5	8.3	9.5	1	1	1	C 0	S 1	SE 2
15	96.2	95.6	94.1	95.3	19.8	28.0	21.3	22.6	29.0	15.8	79	47	72	66	4.9	20.1	7.3	10.7	0	1	1	C 0	ESE 3	ESE 2
16	92.6	91.3	90.6	91.5	20.4	26.0	22.2	22.7	29.2	15.3	74	63	73	70	6.3	12.5	7.4	8.7	0	3	3	NNE 2	NNE 2	NE 2
17	89.9	88.1	88.5	88.8	20.6	27.6	17.0	20.6	29.4	17.0	86	51	99	79	3.3	18.0	0.2	7.2	0	3	7	SSE 1	SSE 2	SE 1
18	86.9	87.3	91.0	88.4	17.0	22.2	16.2	17.9	23.4	15.9	99	74	97	90	0.2	6.9	0.6	2.6	10 •	9	9	E 2	NE 6	NE 4
19	94.9	96.8	97.5	96.4	17.0	22.2	15.2	17.4	22.8	15.2	86	52	78	72	2.8	15.0	3.9	6.6	5	4	0	NNE 5	SE 5	NNE 4
20	97.7	96.5	94.1	96.1	16.0	22.6	16.4	17.8	23.4	11.4	72	44	74	63	5.1	15.4	4.7	8.4	0	1	2	SE 5	ESE 6	SE 4
21	91.3	89.4	87.3	89.3	15.4	23.8	18.6	19.1	25.2	12.7	80	64	80	75	3.5	10.7	4.3	6.2	3	7	8	SE 5	SSE 5	SW 2
22	87.5	88.2	87.3	87.7	16.2	24.0	18.6	19.4	25.6	15.4	99	60	81	80	0.2	12.0	4.1	5.4	10 •	4	6	WSW 4	W 4	SW 2
23	85.5	84.3	85.3	85.0	17.2	24.2	18.0	19.4	25.9	14.3	91	66	89	82	1.8	10.2	2.2	4.7	4	7	9	E 2	S 3	W 3
24	88.5	88.2	88.8	88.5	15.4	22.3	20.7	19.8	25.9	12.4	92	62	70	75	1.3	10.3	7.4	6.3	2	9	6	SW 2	WSW 6	W 6
25	90.6	90.4	87.9	89.6	17.3	24.2	20.6	20.7	26.2	15.6	82	49	81	71	3.5	15.5	4.6	7.9	9	5	9	WSW 1	SW 2	SW 2
26	88.0	89.4	88.2	88.5	17.0	18.9	15.3	16.6	21.0	14.9	98	71	89	86	0.4	6.3	1.9	2.9	10	10	10	SW 2	W 3	SW 4
27	86.8	87.5	89.9	88.1	15.4	17.8	12.6	14.1	18.8	11.4	94	61	71	75	0.9	8.0	4.2	4.4	10	10	2	NW 2	W 6	W 3
28	90.7	91.2	90.5	90.8	13.6	15.3	13.2	13.8	17.7	10.8	81	67	84	77	3.0	5.8	2.5	3.8	6	9	10	WNW 4	W 8	WSW 4
29	88.0	86.0	82.0	85.3	13.8	20.9	19.2	18.3	23.5	11.4	88	50	73	70	2.0	12.3	6.0	6.8	10	8	10	WSW 3	WSW 4	NW 2
30	79.2	78.7	80.7	79.5	15.8	16.8	14.4	15.4	20.8	14.4	93	84	77	85	1.3	3.1	3.8	2.7	5	10	8	SW 2	WSW 6	W 4
31	82.0	81.5	81.2	81.6	12.0	17.2	14.8	14.7	18.8	10.4	94	71	91	85	0.8	5.6	1.3	2.6	10	10	8	WSW 3	SW 3	NW 3
M	89.7	89.3	89.0	89.3	15.0	20.7	16.0	16.9	22.5	11.8	87	59	83	76	2.2	10.5	3.4	5.4	5.6	6.7	5.8	2.7	4.0	2.9

Sierpień – Août

1	87.1	88.7	88.0	87.9	11.8	18.3	13.8	14.4	19.8	10.3	84	52	79	72	2.1	10.1	3.4	5.2	7 •	5 •	10	NW 3	NW 3	NNE 3
2	77.3	80.6	85.8	81.2	10.6	9.6	9.3	9.7	14.0	9.2	95	95	97	95	0.7	0.8	0.3	0.6	10	10	8	NE 12	NNW 8	WNW 3
3	87.1	87.2	89.0	87.8	9.9	19.4	12.0	13.3	20.4	7.5	97	50	91	79	0.3	11.2	1.2	4.2	0	4	8	W 4	WSW 5	SW 3
4	90.3	90.7	92.3	91.2	12.4	16.6	13.0	13.8	18.9	10.4	95	80	92	89	0.7	3.9	1.3	2.0	9	10	2	WSW 4	W 6	W 3
5	96.8	97.7	97.2	97.2	12.7	19.4	16.2	16.1	21.7	9.8	88	54	79	74	1.8	10.3	3.8	5.3	0	6	0	WSW 2	W 1	W 3
6	97.4	96.4	94.6	96.1	13.6	23.4	20.4	20.0	27.4	11.7	97	53	79	76	0.6	13.3	5.1	7.0	0	0	2	SW 3	SSW 6	SW 3
7	94.7	93.1	91.4	93.1	18.4	27.8	21.4	22.2	29.3	18.1	87	58	73	73	2.7	15.5	6.5	8.2	10	1	0	WSW 2	SW 4	SW 3
8	92.6	91.1	89.7	91.1	19.2	29.2	23.0	23.6	30.0	16.1	82	47	68	66	4.0	21.5	9.1	11.5	0	0	0	WSW 2	SW 2	SW 2
9	92.1	93.0	95.6	93.6	17.6	23.2	14.8	17.6	23.9	14.7	92	63	88	81	1.6	10.4	2.0	4.7	8	9	10	E 7	WNW 5	N 4
10	96.3	96.5	95.8	96.2	14.4	17.2	14.7	15.2	19.0	13.1	88	79	72	80	2.0	4.1	4.7	3.6	10	10	10	NE 3	NE 5	NNE 4
11	95.3	96.5	95.9	95.9	11.2	12.2	11.6	11.6	15.0	10.8	97	96	96	96	0.3	0.5	0.3	0.4	10 •	10 •	10	NNE 4	NE 5	NW 3
12	95.1	95.8	95.8	95.6	11.8	16.4	11.2	12.6	18.1	10.6	94	71	91	85	0.8	5.4	1.2	2.5	10	6	8	E 3	NNW 6	NW 3
13	95.6	95.6	95.6	95.6	10.6	15.1	10.0	11.4	16.8	9.1	94	68	89	84	0.8	5.3	1.3	2.3	4	6	4	NW 5	NW 6	W 3
14	95.9	96.0	94.7	95.5	10.6	14.4	11.9	12.2	16.0	8.4	88	67	94	83	1.5	3.5	0.8	2.6	9	9	10	NW 3	NW 3	WNW 1
15	95.1	96.0	96.8	96.0	11.6	16.0	11.0	12.4	17.7	10.3	96	74	96	89	0.3	4.7	0.3	1.9	10	9	3	NW 1	N 5	NW 1
16	97.0	96.5	95.2	96.2	11.4	18.4	12.8	13.8	19.9	8.2	96	54	85	78	0.3	9.8	2.3	4.2	2	6	5	NNE 1	NNE 1	NW 2
17	94.9	95.0	94.7	94.9	11.6	19.6	13.6	14.6	22.4	8.7	95	53	80	76	0.6	10.7	3.2	4.8	0	4	0	C 0	C 0	SSE 1
18	95.8	96.8	97.2	96.6	12.8	23.1	14.8	16.4	23.8	8.9	87	38	77	67	1.9	17.4	3.8	7.7	0	2	0	C 0	C 0	NE 1
19	99.6	100.3	99.7	99.9	12.4	24.0	15.6	16.9	25.2	10.4	96	40	70	69	0.3	17.8	3.3	7.9	4	3	0	E 1	SSE 1	S 2
20	100.4	99.4	97.1	99.0	13.4	24.8	17.0	18.0	25.3	10.3	92	47	74	71	1.3	16.7	3.1	7.7	0	4	0	C 0	SSE 2	SE 3
21	95.6	93.7	91.3	93.3	13.6	23.8	19.0	19.4	26.0	12.1	92	49	71	71	1.3	16.8	6.4	8.2	2	3	0	C 0	SW 1	SW 2
22	90.5	88.7	86.9	88.7	14.4	26.1	17.9	19.1	26.5	13.5	88	46	77	70	2.0	18.1	4.6	8.2	1	2	0	SE 2	S 4	SSE 2
23	86.6	86.5	87.4	86.8	14.2	25.8	19.9	20.0	26.4	12.0	90	48	66	68	1.6	17.3	7.9	8.9	0	0	1	ESE 3	SSW 2	SW 2
24	86.8	86.9	84.9	86.2	15.2	24.6	20.7	20.3	25.5	14.5	90	56	84	77	1.7	13.6	4.0	6.4	9	8	10	ESE 3	S 2	ESE 2
25	82.2	83.7	84.7	83.3	18.3	20.2	17.2	18.2	21.2	16.9	90	89	93	91	2.0	2.7	1.4	3.0	9	10	10	ESE 2	S 2	SW 3
26	85.4	87.3	86.5	86.4	11.9	12.0	10.2	11.1	17.4	9.9	97	91	99	96	0.3	1.2	0.1	0.5	10 •	10 •	10 •	NNW 7	NNW 8	NW 8
27	83.0	85.0	89.0	85.7	9.4	11.1	9.6	9.9	11.4	8.9	99	81	97	92	0.2	2.4	0.4	1.0	10 •	10	10 •	NNW 8	NW 7	W 3
28	90.0	90.9	92.2	91.0	9.8	17.1	12.0	12.7	18.2	9.0	100	63	89	84	0.0	7.3	1.5	2.9	10 ≡	9	9	SW 2	WSW 4	SW 4
29	92.1	91.8	90.6	91.5	10.7	18.4	12.4	13.5	19.6	10.3	97	56	85	79	0.4	9.4	2.2	4.0	5	7	7	W 1	WNW 2	NW 2
30	89.3	90.5	92.3	90.7	10.8	17.4	11.0	12.6	19.4	9.9	96	62	84	81	0.5	7.5	2.1	3.4	9	3	0	WSW 2	NW 4	NW 4
31	91.7	91.3	89.9	91.0	11.2	17.8	10.9	12.7	19.2	8.8	82	57	87	75	2.5	8.9	1.6	4.3	0	7	0	NW 2	WNW 3	C 0
M	91.9	92.2	92.2	92.1	12.8	19.6	14.5	15.4	21.1	11.1	92	62	84	79	1.2	9.8	3.0	4.7	5.4	6.0	4.7	3.0	3.6	2.7

Sandomierz $H_s = 202$ m $H_b = 200.3$ m $h_w = 20.6$ m anemometr M-47, 20.1 m wodomierz Wilda Lipiec – Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	1.9	•	▽° 13^15–43 13^49–15^08, = 3^15–8^15 21^30–24; ⌒° 0^00–9
2	7	1.2	•	•° 3^16 4^30 5^32–7^15...47, 7^52 9^12; = 0^00–12^15, 20^30–24
3	7	3.3	•	•°▽ 14^18–15^05 •°–16^20 19^48–20^15 21^10; = 0^00–7^30, 15^05–24
4	7	2.3	•	▽°• 13^10–14^20 15^05–15 •°16^25 17^10–18^30; = 0^00–8^30, 18^30–24
5	7	1.3	•	•° 11^02...12^48 14^32 16^08–17^05...25; = 0^00–11^15 21^00–24
6	7	1.4	•	•°▽ 18^03–07 •¹–18^12 •°▽ 18^20 18^28–48 19^10–12 •¹▽ 19^13 •°–19^20, 22^40–52; K°SW 18^15–20 (K)° 18^40 E, (K)°SW 18^50 S–19^15 E, por. wiatru 13 m/sek 11^20–12^20; = 0^00–6^30, 20^10–24
7	7	-	•	= 0^00–6^15; ⌒° 21–24
8	7	13.4	•	•°▽ 19^17–35 •¹▽ 19^40 20^00 •°▽ 20^20 •¹–20^45 •°–21^20 •¹–21^40 •°▽ 22^10 •¹–22^50 •°23^42–24; por. wiatru 13 m/sek 12^15–15^40; ⌒° 0^00–1 ⌒¹ 2–9
9	7	-	•	•° 1^30...2^40 3^20–4^20; = 0^00–7^30; ⌒° 20–24
10	7	3.6	•	•°▽ 12^02–10 13^15–22 13^30–45 •¹–13^50 •°▽ 14^07 16^20–57 •¹–16^42 •°▽ 16^50 •¹–16^55 •°▽ 17^20 •¹–17^25 •°–17^45 (K)N 18^10–NE 17^25; = 16^20–17^30 21^15–24; ⌒° 0^00–9
11	7	-	•	= 0^00–7^40 22^15–24; ⌒° 20–24
12	7	5.4	•	•°▽ 20^35–21^30 •¹▽ 21^45 •°▽ 23^30 •° 24; = 0^00–8^30, 21^30–24; ⌒° 0^00–2 ⌒¹ 3–4 ⌒² 5–7
13	7	-	•	•° 0^00–2^10; = 0^00–8^45; ⌒° 21–24
14	7	-	•	= 0^30–8^30; ⌒° 0^00–2 ⌒¹ 3–9
15	7	-	•	⌒° 0^00–9, 22–24
16	7	-	•	⌒° 0^00–2 ⌒¹ 3–6 ⌒° 7–9 **17.VII:** por. wiatru 14 m/sek 14^40–15^30; = 18^40–24; ⌒° 0^00–4 ⌒¹ 5–8
17	7	45.2	•	•°▽ 14^17–18 •²▽ 15^08–15^29 •°–15^39 •¹▽ –16^07 ▲° 15^42–47 •°▽ 16^07–43 •¹▽ 16^52 •°▽ –17^12 •¹▽ –17^25 •°▽ –18^15 (K)°NE 14^40 K¹ 14^42 15^25 (K)¹SW–16^20 (K)°NE 16^25 K¹ 16^40 (K)E 18^05;
18	7	46.9	•	•° 3^20 7^15 •°▽ 14^40–50 •¹–15^01 •°▽ –15^04 •°▽ 15^08 •²–15^40 •°▽ –15^48 •¹▽ 15^51 •²▽ 15^55 •¹▽ –16^27 •°▽ 17^06 •²▽ 17^20–26 •¹▽ –18^05 •°–1▽ 18^13 •²–2▽ 18^19 •°–1▽ 18^36 •°2^46 22^07 K¹ NE 15^28 K¹ 15^30–47 SW 16^50;
19	7	0.0	•	•° 3^36...46; = 0^00–5^15 **18.VII:** = 0^00–8^30, 18^30–24
20	7	-	•	⌒° 2–4 ⌒¹ 5–6 ⌒° 7–9
21	7	4.1	•	⌒° 21–24
22	7	0.0	•	•° 2^40–6^45 7^15; = 21^15–9^30; ⌒° 0^00–2^40, 22–24
23	7	0.2	•	▽¹ 14^30–36; (K)° S 14^29–K° 14^40–50 (K)° 15^20; ⌒° 0^00–3 ⌒¹ 4–8
24	7	-	•	= 2^30–7^30
25	7	1.1	•	•°▽ 20^45–21^20; ⌒° 3–9
26	7	0.2	•	•¹▽ 10^48–52 12^55–13^03 13^50–14^07 14^31–45 •° 15^25...30; = 0^00–10^30
27	7	0.0	•	▽°• 5^55–6^04 •¹▽ 10^40–46; por. wiatru 12 m/sek 15^10–16^20; = 0^00–9^30
28	7	0.0	•	•° 18^40...19^00; por. wiatru do 13 m/sek 11^30–50, 13^20–45 13^50–14^20, 14^40–15^20; = 23^30–24
29	7	3.6	•	= 0^00–7^30
30	7	0.3	•	•°▽ 1^10–2^20 3^05–4^10 •¹▽–4^30 •°▽–4^40 10^52 11^38 18^30–40 18^46–54 18^56 19^04 (K)N–NNE 18^45–K° 18^50–58 (K)SSE 19^15; por. wiatru 13 m/sek 13^30 14^10 14^25–50
31	7	0.9	•	•°▽ 20^45–56 •° 21^20–22^25; = 0^30–9^30 21^20–24 **30.VII:** = 3^10–10^15
Σ	-	136.5	-	

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1	7	33.7	•	= 0^00–6^15
2	6	16.8	•	•° 0^10...30 46 •¹–5^52 •°–6^15 6^30 7^05 •¹–7^40 •°–8^15 •¹–9^05 •°–10^30 13^30 14^30 16^40 •°▽ 20^42–47 20^49–51; por. wiatru do 14 m/sek 2^10–6^12 ≫–7^00 (por. 18 m/sek) por. wiatru 14 m/sek 7^20–30 12 m/sek
3	7	3.4	•	▽°• 13^48–51 13^54 14^02 15^20–24 15^36–40 15^48 16^23 ▽¹ 16^28–30 •°▽–16^37 •¹▽–16^42 •°▽–16^46; = 0^00–8^30, 23^30–24 **2.VIII:** 7^30–10^20, 14 m/sek 13^30–14^10; = 0^30–24
4	6	0.1	•	▽°• 9^50–10^36 11^26–46; = 0^00–14^30, 20^30–24; ⌒° 21–24
5	7	-	•	= 0^00–6^45 21^20–24; ⌒° 0^00–3 ⌒¹ 4–9 ⌒° 20–24
6	7	-	•	= 0^00–10^15; ⌒° 0^00–2 ⌒¹ 3–8
7	7	-	•	
8	7	-	•	⌒° 3–7
9	7	-	•	= 3^30–5^40
10	7	7.8	•	
11	6	12.6	•	•°▽ 0^16–30 •° 1^18–2^30 4^05–9^10 •¹–9^30 •°–14^30 •°▽ 15^05–50 16^05–10 •¹–16^30; = 1^15–24
12	7	5.0	•	•° 3^15...5^10 •°▽ 16^32–17^05 17^11–30 17^39–18^05 19^10–20^20; = 0^00–10^30
13	7	1.6	•	•°▽ 0^10–3^40 13^55–14^02 14^49–15^03 17^06–15
14	7	1.3	•	▽°• 15^40–16^20 18^30–19^18 21^51–22^15; = 18^30–24
15	7	0.4	•	•° 1^05–3^15 •°▽ 5^08–6^04 9^20–31 11^35–45; = 0^00–10^15
16	7	-	•	= 0^00–6^30; ⌒° 0–8, 20–24
17	7	-	•	⌒¹ 1–3 ⌒² 4–6 ⌒¹ 7–9 ⌒° 20–24
18	7	-	•	⌒° 0^00–2 ⌒¹ 3–9 ⌒° 22–24
19	7	-	•	⌒° 0^00–3 ⌒¹ –7 ⌒° –9, 22–24
20	7	-	•	⌒° 0^00–3 ⌒¹ 4–9 ⌒° 20–24
21	7	-	•	= 1^30–8^00; ⌒° 0^00–2 ⌒¹ 3–9
22	7	-	•	= 1^30–7^30; ⌒° 0^00–8, 22–24
23	7	-	•	⌒° 0^00–2 ⌒¹ 3–7 ⌒° 8–9
24	7	0.7	•	•° 2^28...35; = 0^00–7^30; ⌒° 0^00–9
25	7	16.7	•	•° 0^16...30 2^05 4^40 11^40...12^15 14^05...20 •°▽–15^15 •° 21^55 22^20 22^30...46; = 2^30–5^30
26	6	50.4	•	•° 0^10...30 3^30 •¹ 3^53 •°–6^03 •¹–7^12 •°–9^15 10^28 14^20 •¹ 17^20–42 •°–18^05 18^20 19^05 •¹–19^25 •°–19^50 •¹–20^45 •°–21^34 22^08 23^04 •¹–24; por. wiatru 12 m/sek 21^12–22^30 ≫–22^45
27	6	3.6	•	•¹ 0^00–06 •° 0^20 2^30–3^20 •¹–4^35 •°–4^50 6^00–40 7^10–8^10...20 11^06 12^15 14^45 16^40–17^25 18^30–20^40; ≫ 1^50–5^15; = 0^00–24
28	7	0.3	•	▽°• 13^40–46 14^23–40 15^16–28; = 0^00–5^40 ≡°–6^30 —10^30, 20^10–24 **26.VIII:** por. 13 m/sek 22^45–24; = 0^30–24
29	7	-	•	= 0^00–8^40, 21^30–24; ⌒° 20–24
30	7	0.0	•	▽°• 15^10–17, 15^28–35; = 0^00–11^30; ⌒° 0^00–2 ⌒¹ 3–9
31	7	-	•	= 21^15–24; ⌒° 1–8, 20–24
Σ	-	154.6	-	

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ *Wrzesień – Septembre 1965*

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	89.2	90.2	93.0	90.8	10.6	20.0	15.0	15.2	20.6	8.8	96	64	80	80	0.5	8.4	3.4	4.1	8	8	1	SE 1	SW 2	SSW 2
2	95.3	96.6	96.0	96.0	13.2	23.6	17.8	18.1	25.4	11.4	93	58	87	79	1.1	12.3	2.6	5.3	3	9	2	ESE 5	SSE 3	SE 4
3	93.9	92.3	90.5	92.2	14.4	24.9	18.9	19.3	25.7	13.4	97	49	74	73	0.6	16.1	5.5	7.4	0	8	8	SE 4	S 6	S 3
4	87.1	87.0	87.4	87.2	15.4	22.8	14.2	16.6	23.3	13.7	88	55	94	79	2.1	12.3	0.9	5.1	7	9	10	SE 1	S 2	SW 6
5	89.9	88.7	87.4	88.7	11.3	21.5	16.0	16.2	22.5	10.5	100	57	82	80	0.0	10.8	3.3	4.7	1	2	0	SW 2	SW 3	S 4
6	86.1	84.2	82.8	84.4	12.5	22.6	15.6	16.6	23.6	10.6	95	62	92	83	0.7	10.4	1.3	4.1	1	7	10 •	SE 3	SW 5	SSE 1
7	84.0	85.5	88.1	85.9	11.0	15.8	10.5	12.0	17.9	10.4	97	64	90	84	0.3	6.4	1.3	2.7	10	8	0	WSW 2	W 4	WSW 3
8	90.3	92.0	92.6	91.6	11.4	15.9	12.4	13.0	18.6	9.7	98	81	92	90	0.4	3.5	1.2	1.7	9	6	10	W 3	NW 4	SW 2
9	91.2	91.1	91.5	91.3	11.5	22.6	17.0	17.0	24.1	9.4	94	61	89	81	0.9	10.6	2.2	4.6	2	4	1	S 2	SW 5	S 1
10	89.8	88.9	89.2	89.3	13.4	23.0	17.8	18.0	25.2	11.4	95	59	82	79	0.7	11.7	3.6	5.3	2	9	2	SSE 2	SSE 4	SE 2
11	86.7	87.5	89.5	87.9	15.2	18.6	12.4	14.6	24.0	12.1	88	82	96	89	2.1	3.9	0.5	2.2	9	9	10 •	SSE 3	WNW 7	N 2
12	90.8	91.6	90.3	90.9	11.4	15.4	11.6	12.5	17.8	10.6	96	72	91	86	0.5	5.0	1.1	2.2	3	8	0	NNE 1	NW 1	SSW 1
13	88.2	87.5	88.1	87.9	8.6	18.0	9.8	11.6	19.2	6.8	100	57	93	83	0.0	8.7	0.8	3.2	1	2	1	E 2	SE 2	SW 1
14	90.6	91.9	94.8	92.4	10.0	16.4	10.9	12.0	17.2	9.4	97	71	97	88	0.3	5.4	0.3	2.0	10	8	2	SW 3	SW 4	WSW 3
15	96.5	97.4	100.6	98.2	10.1	15.2	11.2	11.9	16.8	8.9	99	71	82	84	0.2	5.0	2.5	2.6	9	8	0	WSW 3	WNW 5	NNW 4
16	103.6	104.2	102.8	103.5	8.0	17.6	11.5	12.2	18.4	6.8	96	59	77	77	0.4	8.2	3.2	3.9	0	1	0	N 3	C 0	ESE 3
17	101.0	99.7	98.4	99.7	6.6	19.9	14.0	13.6	21.0	5.0	98	62	83	81	0.1	8.7	2.7	3.8	0	0	0	SSE 1	SSE 2	SW 4
18	97.4	94.9	92.9	95.1	9.8	21.4	14.6	15.1	22.4	8.4	96	58	79	78	0.5	10.6	3.4	4.8	0	0	0	SW 2	S 2	SSW 3
19	93.7	96.8	100.4	97.0	13.1	12.3	11.1	11.9	15.5	9.9	87	96	96	93	1.9	0.5	0.5	1.0	9	10 •	10 •	WSW 4	N 4	W 2
20	103.2	104.9	107.9	105.3	9.6	15.8	12.0	12.4	16.8	9.2	93	58	84	78	0.8	7.4	2.2	3.5	9	7	10	N 4	NW 2	NNW 2
21	109.7	110.1	107.4	109.1	7.8	17.2	11.2	11.8	18.2	6.9	99	53	84	79	0.2	9.2	2.1	3.8	0	5	0	N 1	N 3	NW 2
22	104.5	101.8	98.2	101.5	6.4	17.4	11.8	11.8	19.0	5.8	95	60	89	81	0.4	8.1	1.5	3.3	3	4	0	SW 3	SW 5	WSW 4
23	96.6	95.5	93.6	95.2	8.1	20.8	14.0	14.2	22.3	7.5	100	51	83	78	0.0	12.0	2.7	4.9	10 ≡	0	0	WSW 4	WSW 3	SW 2
24	93.4	93.0	92.6	93.0	8.8	21.6	15.1	15.2	23.2	7.5	100	54	82	79	0.0	11.9	3.2	5.0	0 ≡	0	0	SSE 3	S 2	SSE 2
25	91.6	91.0	89.4	90.7	10.4	23.0	16.0	16.4	24.7	9.3	100	56	82	79	0.0	12.5	3.3	5.3	4	2	0	SE 2	SW 3	SE 3
26	87.9	87.4	87.6	87.6	10.2	23.0	14.4	15.5	23.2	9.5	99	52	92	81	0.1	13.5	1.3	5.0	2	0	0	SE 3	SSE 4	SE 3
27	86.2	85.6	87.0	86.3	14.2	20.4	15.0	16.2	21.5	13.4	92	70	94	85	1.3	7.3	0.9	3.2	9	6	0	SE 3	SSW 7	SE 5
28	85.7	85.8	83.8	85.1	12.9	24.6	19.6	19.2	25.2	11.9	99	62	77	79	0.2	11.9	5.3	5.8	6	4	10	SE 2	SW 6	S 2
29	81.8	83.6	92.5	86.0	17.8	13.6	9.0	12.4	20.0	8.7	76	99	99	91	4.8	0.2	0.2	1.7	9 •	10	0	SSE 3	WSW 4	SW 3
30	94.0	93.8	93.5	93.8	7.6	19.4	13.0	13.2	19.7	6.2	99	64	92	85	0.1	8.0	1.3	3.1	6	6	0	S 2	SW 6	SSE 2
31																								
M	92.7	92.7	93.0	92.8	11.0	19.5	13.8	14.5	21.1	9.4	95	64	87	82	0.7	8.7	2.1	3.8	4.7	5.3	2.9	2.6	3.7	2.7

Październik – Octobre

1	94.9	95.6	95.6	95.4	8.0	21.0	14.7	14.6	21.9	7.5	100	68	96	88	0.0	8.1	0.7	2.9	0 ≡	0	0	NE 1	SE 1	E 3
2	95.3	94.1	94.2	94.5	11.4	21.2	14.0	15.2	21.7	10.4	95	68	85	83	0.7	8.2	2.3	3.7	0	0	0	E 5	SSE 5	E 5
3	96.3	98.2	99.3	97.9	10.4	13.5	12.4	12.2	14.9	9.3	96	95	100	97	0.3	0.7	0.0	0.4	10	10	0	SE 1	ESE 2	SE 2
4	99.6	99.6	98.5	99.2	10.5	16.4	14.0	13.7	16.8	10.4	97	87	94	93	0.3	2.5	0.9	1.2	10	8	10	ESE 2	NE 2	NNE 1
5	98.9	99.7	100.9	99.8	11.1	15.8	8.2	10.8	16.9	7.9	97	72	96	88	0.3	5.0	0.5	1.9	9	8	0	NE 3	E 4	N 3
6	101.5	100.5	99.6	100.5	6.8	14.1	7.4	8.9	15.4	6.5	99	74	96	90	0.2	4.3	0.5	1.7	0 ≡	4	0	NE 1	NNE 2	ESE 1
7	97.8	96.9	95.1	96.6	2.9	12.6	7.6	7.7	14.6	2.5	100	69	99	89	0.0	4.6	0.1	1.6	0	0	0	SE 2	S 1	SW 3
8	92.3	91.4	92.9	92.2	6.6	15.1	10.0	10.4	16.0	5.4	100	76	88	88	0.0	4.1	1.5	1.9	10 ≡	10	10	SW 4	WSW 6	NW 5
9	93.7	93.1	91.9	92.9	4.2	10.1	7.4	7.3	12.0	3.9	98	75	87	87	0.1	3.2	1.3	1.5	4	9	9	NW 3	NE 5	NNE 5
10	91.2	91.9	92.2	91.8	4.4	8.8	6.4	6.5	9.6	4.1	98	67	81	82	0.2	3.7	1.9	1.9	10	9	6	NW 5	NNW 6	W 3
11	92.7	91.5	92.9	92.4	6.4	10.1	5.8	7.0	10.7	5.1	89	73	88	83	1.0	3.4	1.1	1.8	8	9	10	W 3	W 7	NE 7
12	100.9	103.5	104.8	103.1	-0.1	7.4	4.4	4.0	9.0	-0.5	96	62	80	79	0.2	3.9	1.7	1.9	0	2	8	NNW 3	NE 4	WNW 3
13	104.4	103.4	101.0	102.9	-0.9	10.0	4.6	4.6	10.8	-1.0	96	50	79	75	0.2	6.1	1.8	2.7	4	8	1	W 3	SW 3	SW 3
14	98.4	100.1	100.0	99.5	1.0	12.8	6.0	6.4	14.5	0.6	94	52	85	77	0.4	7.1	1.5	3.0	2	7	0	SW 4	SW 6	WSW 4
15	99.8	99.1	97.3	98.7	1.2	14.4	6.8	7.3	15.9	0.7	96	47	77	73	0.3	8.7	2.3	3.8	1	0	0	S 2	SW 4	SW 4
16	96.2	93.4	92.8	94.1	2.5	15.4	11.8	10.4	17.3	2.3	89	43	68	67	0.8	10.0	4.4	5.1	2	2	10	WSW 3	SW 6	NW 5
17	98.6	102.1	104.3	101.7	7.2	12.0	5.7	7.6	12.4	5.4	90	59	85	78	1.1	5.7	1.5	2.8	9	6	0	WNW 6	NW 3	WNW 3
18	103.3	102.1	101.4	102.3	0.4	9.0	6.4	5.6	10.2	-0.4	98	64	81	81	0.1	4.1	1.9	2.0	9	8	4	WSW 3	WSW 4	W 4
19	102.0	102.7	103.5	102.7	6.5	10.6	4.2	6.4	11.8	4.0	94	62	92	83	0.6	4.9	0.6	2.0	10	6	0	NW 3	N 1	NW 4
20	104.3	106.5	109.0	106.6	5.4	8.9	4.4	5.8	9.8	2.8	98	58	82	79	0.2	4.8	1.5	2.2	9	8	10	NNW 4	NE 3	ENE 3
21	111.2	112.4	112.8	112.1	1.2	3.2	-0.3	1.0	4.8	-0.9	85	69	90	81	1.1	2.4	0.6	1.4	10	10	0	SE 1	SE 2	E 2
22	113.0	112.3	110.2	111.8	-3.1	6.6	1.0	1.4	8.1	-3.5	97	61	83	80	0.1	3.8	1.2	1.7	0	0	0	NE 2	SSE 1	NNW 4
23	106.2	104.7	103.2	104.7	2.4	6.8	6.0	5.3	7.7	-1.4	82	84	88	85	1.3	1.6	1.2	1.4	10	10	10	W 4	NW 4	NW 4
24	103.8	104.7	104.6	104.4	5.7	10.7	3.2	5.7	11.4	3.0	97	61	97	85	0.3	5.1	0.3	1.9	9	1	0	NW 3	N 5	N 4
25	104.6	104.5	104.2	104.4	5.2	6.6	5.8	5.8	6.9	2.1	94	88	97	93	0.5	1.1	0.3	0.6	10	10	10 •	N 1	NW 2	C 0
26	103.1	102.2	99.3	101.5	5.2	6.6	3.0	4.4	7.0	2.9	97	82	98	92	0.2	1.7	0.2	0.7	10	10	0	C 0	S 1	SE 2
27	97.0	96.3	96.0	96.4	-2.0	9.2	4.7	4.2	10.0	-2.8	98	74	97	90	0.1	3.0	0.2	1.1	10 ≡	1	0	WSW 3	SW 5	WSW 5
28	95.9	94.3	94.2	94.8	0.6	11.3	7.8	6.9	12.9	0.3	100	65	79	81	0.0	4.7	2.2	2.3	10 ≡	10	9	WSW 5	SW 5	WSW 5
29	93.2	91.7	90.3	91.7	4.8	15.0	8.4	9.2	15.9	4.7	90	50	79	73	0.8	8.5	2.2	3.8	2	3	2	WSW 5	WSW 6	WSW 5
30	96.0	95.8	95.3	95.7	5.5	10.9	3.6	5.9	11.5	3.5	89	58	90	79	1.0	5.5	0.8	2.4	1	5	0	W 5	NW 5	WSW 2
31	90.2	89.4	87.5	89.0	1.8	8.4	6.0	5.6	8.7	0.5	94	71	86	84	0.4	3.1	1.3	1.6	9	10	10	WSW 4	W 5	WSW 4
M	99.2	99.2	98.9	99.1	4.3	11.4	6.8	7.3	12.5	3.1	95	67	88	83	0.4	4.6	1.2	2.1	6.4	5.[illegible]	[illegible].8	3.0	5.7	3.4

Sandomierz $H_s = 202\,m$ $H_p = 200{,}3\,m$ $h_w =$ 20,8 m anemometr M-47 / 20,1 m wiatromierz Wilda **Wrzesień - Septembre 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	= 0^00–8^30 23^30–24; ⌒ 0^00–2 ⌒ 1 3–9 ⌒ 0 20–22 ⌒ 1 23–24
2	7	•	•	= 0^00–7^40 22^40–24; ⌒ 1 0^00–2 ⌒ 2 3–7 ⌒ 1–9
3	7	•	•	= 1^00–7^40; ⌒ 0 1–4 ⌒ 1 5–10 ⌒ 0 22–24
4	7	1.0	•	▽ 0^47–11^05 • 0 14^40–15^10, 15^20–16^12; 16^15–22, 16^40–17^10, 17^15–18^40; por. wiatru 14 m/sek 18^50–19^15; = 16^15–24; ⌒ 0 0^00–4 ⌒ 1 5–9 ⌒ 0 19–22 ⌒ 1 23–24
5	7	•	•	= 0^00–8^40; ⌒ 1 0^00–4 ⌒ 1 5–7 ⌒ 1 8–10 ⌒ 0 22–24
6	7	2.5	•	• 0 16^15...35 19^45 20^40–21^30 22^30–24; = 20^15–24; ⌒ 0 0^00–3 ⌒ 2 4–7 ⌒ 1 8–9; ⊕ 12^45–13^10
7	7	1.7	•	• 0 0^00–3^30, 2^35–3^45; = 0^00–9^30; ⌒ 0 19–20 ⌒ 1 21–24
8	7	1.2	•	• 0 3^15...40–4^08 ▽ 0 12^01–17; = 0^30–10^30 21^40–24; ⌒ 1 0^00–3^15; ▽ 20^30–24
9	7	•	•	= 0^00–8^40; ⌒ 0 1–3 ⌒ 2 4–10; ▽ 0^00–1^00, 23^30–24
10	7	•	•	= 0^30–9^15; ⌒ 1 1–2 ⌒ 2 3–9 ⌒ 0 19–21 ⌒ 1 22–24; ▽ 0^00–15 ⊕ 11^40–13^10
11	7	15.7	•	▽ 0 12^47–13^02 ▽ 1–13^07 ▽ 2–13^10 ▽ 1–13^15 ▽ 0–13^20 ▽ 1–13^24 ▽ 0–13^40 ▽ 1 18^30–21^30 • 0 24, por. wiatru 12 m/sek 10^05–11^45; = 3^30–6^15, 21^30–24; ⌒ 1 0^00–4 ⌒ 2 5–9
12	7	•	•	• 0 0^00–4^30, = 0^00–10^30, 21^15–24; ⌒ 0 22–24
13	7	•	•	= 0^00–9^30 20^40–24; ⌒ 0 0^00–2 ⌒ 1 3–4 ⌒ 2 5–8 ⌒ 1 9–10 ⌒ 0 18–23
14	7	12.0	•	• 0 9^05...12 ▽ 0 13^40–43 13^45–58 ▽ 1–14^03 ▽ 2–14^04 ▽ 1–14^05 ▽ 0–14^12 ▽ 1–14^20 ▽ 0–14^48; K 0 W 13^42–14^10 E 14^35; = 0^00–11^30 17^30–24; ⌒ 1 0–3 ⌒ 2 4–9^05
15	7	•	•	= 0^00–11^30, 23^15–24; ⌒ 0 18–20 ⌒ 2 21–24
16	7	•	•	= 0^00–9^30; ⌒ 2 0^00–10^00 ⌒ 0 20–22 ⌒ 1 23–24
17	7	•	•	⌒ 1 0^00–1 ⌒ 2 2–8 ⌒ 1 9–10 ⌒ 0 22–24
18	7	•	•	= 0^00–9^15; ⌒ 1 0^00–3 ⌒ 2 8 ⌒ 1 9–10 ⌒ 0 19–21 ⌒ 1 22–24
19	6	5.8	•	• 0 10^45 12^00–23 • 1–12^30 • 0–12^45 13^05–14^10, 19^45–21^35, 23^40–24; = 2^30–24; ⌒ 1 0^00–10
20	7	•	•	• 0 0^00–1^40 2^10; = 0^00–9^30
21	7	•	•	= 0^30–4^10; ⌒ 2 3–9, 19–24
22	7	•	•	⌒ 0 0^00–3^00 ⌒ 2 4–9 ⌒ 0 19–21 ⌒ 1 22–24
23	7	•	•	= 0^30–4^45 ≡ 1–6^45 ≡ 1–7^20 ≡ 0–7^45 = –9^30 21^40–24; ⌒ 1 0^00–2 ⌒ 2 3–4^45 ⌒ 0 18–24
24	7	•	•	= 0^00–4^40 ≡ 2 4^45–5^40 ≡ 0–6^40 = –10^30 23^30–24; ⌒ 0 0^00–1 ⌒ 2 2–3^45 ⌒ 0 20–22 ⌒ 1 23–24
25	7	•	•	= 0^00–10^30; ⌒ 1 0^00–2 ⌒ 2 3–10 ⌒ 0 17–24
26	7	0.8	•	= 1^30–9^50; ⌒ 0 0^00–1 ⌒ 2 2–10^00
27	7	1.9	•	• 0 2^45...3^10 ▽ 0 4^40–5^25 • 0 6^35–48, 8^02–10^10; = 6^15–11^30
28	7	0.0	•	⌒ 0 1–4 ⌒ 1 5–9
29	6	14.6	•	▽ 0 6^28–40 7^01–15 9^03–14 ▽ 1–9^24 ▽ 0 10^05 • 0–11^10 • 1–12^10 • 0–12^40 ▽ 0 14^50–15^10, 15^16–20 ▽ 1–15^23 • 0–15^34 ▽ 0 16^02–17; = 10^05–13^30, 19^15–24
30	7	•	•	= 0^00–9^30, 21^30–24; ⌒ 0 18–19 ⌒ 1 20–22 ⌒ 2 23–24
31				
Σ	–	55.2	–	

Październik - Octobre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	•	•	= 0^00–5^40 ≡ 0–6^10 ≡ 1–6^30 ≡ 0–7^35 = –10^30, 20^30–24; ⌒ 2 0^00–5^40 ⌒ 0 19–21 ⌒ 1 22–24
2	7	•	•	= 0^00–9^40; ⌒ 1 0^00–5 ⌒ 2 6–7 ⌒ 1 8–9 ⌒ 0 19–24
3	5	0.1	•	• 0 7^15–45 9^20–40 ≡ 1 7^20–9^20 ≡ 0–9^45 ≡ 0–11^25 = –21^45 ≡ 1–24; ⌒ 1 2–7 ⌒ 0 18–19 ⌒ 1 20–21^45
4	6	0.0	•	• 0 23^10...24; ≡ 1 0^00–2^20 ≡ 0 2^40–5^45 = –24
5	7	•	•	• 0 0^00...1^20; = 0^00–10^30; ⌒ 0 18–24
6	7	•	•	≡ 1 2^45–9^25 ≡ 0–9^45 = –12^30; ⌒ 1 2–9 ⌒ 0 19–20 ⌒ 1 21–24
7	6	•	•	= 2^15–13^30, 20^20–24; ⌒ 1 0^00–3 ⌒ 2 4–11 ⌒ 0 18–24
8	6	•	•	= 0^00–1^45 ≡ 1–5^30 ≡ 2–8^25 ≡ 1–9^15 ≡ 0–9^40 = –24, ⌒ 2 1–14^5 ⌒ 0 21–24, ⊕ 9^40–13^30
9	7	0.0	•	▽ 0 13^40–43 13^47–50 16^04–10; = 0^00–9^15; ⌒ 0 0^00–10, 19–24
10	7	0.0	•	• 0 6^15–17 ▽ 0 18^38–39 • 0 23^45–24; = 3^30–7^15; ⌒ 0 0^00–6^15
11	7	1.5	•	• 0 18^05...10^10–20^03 21^03...17; por. wiatru 13 m/sek 19^55–21^03; = 3^30–6^30
12	7	•	•	= 4^30–6^15; ⌣ 0 3–5 ⌣ 1 6–10
13	7	•	•	⌣ 0 5–9; ⊕ 12^45–13^45
14	7	•	•	= 1^30–8^30, 21^45–24; ⌒ 0 2–10, 21–24
15	7	•	•	= 0^00–11^30; ⌒ 0 0^00–4 ⌣ 1–8 ⌒ 0 19–24
16	7	0.5	•	• 0 23^10–24; = 4^30–6^30, 23^30–24; ⌒ 0 0^00–4 ⌣ 0–7
17	7	(0.0)	•	• 0 0^00–1^20, 7^15–18; = 0^00–5^30; ⌒ 0 21–24
18	7	0.6	•	= 3^15–9^15; ⌒ 0 0^00–3
19	7	•	•	• 0 0^52–12; = 0^30–11^30, 21^15–24; ⌒ 0 17–24
20	7	•	•	= 0^00–10^30; ⌒ 1 0^00–9
21	7	•	•	
22	7	•	•	= 20^45–24
23	6	•	•	= 0^00–24
24	7	•	•	= 0^00–9^30, 23^30–24; ⌒ 0 20–24
25	6	0.2	•	• 0 9^40...11^15, 12^40–16^10–18^30 19^48–23^40; = 0^00–24; ⌒ 0 0^00–9
26	6	•	•	= 0^00–23^40 ≡ 1–24, ⌒ 0 19–23^40
27	6	•	•	≡ 1 0^00–40 ≡ 0–5^00 ≡ 1 5^40–8^45 = –24; ⌣ 0 0–4 ⌣ 1 5–10
28	6	•	•	= 0^00–5^45 ≡ 0–7^50 = –13^30; ⌣ 0 4–8
29	7	0.0	•	▽ 0 21^50–22^05; = 3^30–9^30 21^55–24
30	7	•	•	= 0^00–3^20, 23^30–24; ⌒ 0 20–24
31	6	2.4	•	• 0 17^15–18^32 21^20...45; = 0^00–12^40, 19^30–24; ⌒ 0 0^00–2 ⌣ 0–9
Σ	–	5.3	–	

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — *Listopad – Novembre 1965*

Dni	Ciśnienie P=900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	87.2	89.0	76.4	82.2	5.2	8.3	8.6	7.7	8.8	3.5	89	75	88	84	0.9	2.8	1.4	1.7	10	10 •	10 •	SW 5	WSW 5	SW 6
2	76.5	78.3	81.4	78.7	9.0	9.8	5.8	7.6	15.6	5.5	85	81	88	84	2.0	2.5	1.1	1.8	8	10 •	2	WSW 4	WSW 6	SW 4
3	84.5	86.1	84.9	85.2	5.6	9.6	6.8	7.2	10.9	5.0	75	65	77	72	2.2	4.2	2.3	2.9	1	8	9	WSW 6	WSW 5	SSW 5
4	92.5	96.4	99.4	96.1	2.6	6.6	3.4	4.0	7.5	2.3	91	66	86	81	0.7	3.2	1.1	1.7	2	2	8	WSW 5	WSW 5	WSW 4
5	102.8	103.1	105.0	105.6	0.4	6.2	3.4	3.4	6.6	-0.6	94	78	95	88	0.4	2.2	0.5	1.0	8	2	9	W 2	WSW 5	SW 5
6	105.7	105.2	102.8	104.6	2.1	4.2	5.8	3.5	4.8	1.4	89	80	90	85	0.8	1.6	0.8	1.1	7	10	10	W 6	WSW 6	WSW 4
7	98.7	97.2	97.2	97.7	2.6	6.0	5.4	3.8	6.9	2.2	95	85	95	90	0.6	1.6	0.5	0.9	10	10	8	W 5	WSW 5	W 5
8	99.9	101.2	101.5	100.8	0.6	7.2	1.2	2.6	8.1	-0.4	96	62	94	84	0.3	3.9	0.4	1.5	7	2	0	W 5	WSW 1	WSW 2
9	100.4	99.1	97.2	98.9	-5.3	-1.1	-0.5	-1.2	1.5	-5.4	99	99	100	99	0.0	0.1	0.0	0.0	10 ≡	10 ≡	10 ≡	SW 2	SSW 5	WSW 2
10	95.4	94.7	95.5	94.5	3.6	4.7	4.7	4.4	5.2	-0.4	100	98	100	99	0.0	0.1	0.0	0.0	10 ♦≡	10 ≡	10 ≡	WSW 2	SW 5	WSW 5
11	90.0	87.1	85.5	86.8	1.1	5.5	-1.5	0.5	5.0	-1.5	90	57	97	81	0.6	5.4	0.2	1.4	10	10	10 *	W 5	W 8	WSW 10
12	79.5	80.3	85.5	81.1	-2.3	-1.8	-1.8	-1.9	-1.0	-2.6	96	96	92	95	0.5	0.2	0.4	0.5	10 *	10 *	10	WSW 9	W 7	WSW 6
13	85.6	85.8	87.4	86.5	-5.6	-5.5	-5.1	-4.5	-1.5	-5.2	92	92	90	91	0.4	0.4	0.4	0.4	10	10 *	10	W 8	W 8	WSW 7
14	87.5	88.2	89.9	88.5	-6.3	-5.7	-6.5	-6.2	-4.9	-6.5	91	82	97	90	0.5	0.7	0.1	0.4	10	10 *	10 *	WSW 6	WSW 5	W 2
15	90.7	92.3	95.8	92.9	-7.6	-5.2	-6.1	-6.2	-4.6	-8.2	99	85	86	90	0.0	0.6	0.5	0.4	10 *	9	10	C 0	C 0	SW 4
16	99.5	101.3	104.0	101.6	-8.1	-7.5	-11.5	-9.6	-5.9	-11.9	95	84	97	92	0.2	0.5	0.1	0.3	10 *	9	9	WSW 5	WSW 5	WSW 2
17	103.9	102.0	98.5	101.4	-10.1	-8.6	-15.8	-11.6	-7.7	-14.0	87	77	96	87	0.4	0.7	0.1	0.4	10 *	2	0	C 0	WSW 5	WSW 5
18	94.4	91.2	86.9	90.8	-16.5	-10.9	-10.0	-11.8	-9.8	-16.8	95	85	94	91	0.1	0.4	0.2	0.2	5	10	10 *	SE 5	SE 6	WSW 6
19	85.0	81.4	79.3	81.2	-5.9	-2.3	-1.5	-2.8	-1.1	-10.2	92	89	99	95	0.3	0.6	0.1	0.3	10	10	9	SE 4	WSW 1	W 5
20	78.4	78.8	79.0	78.7	-5.7	-0.3	0.2	-1.4	0.7	-6.0	92	100	98	97	0.3	0.0	0.1	0.1	10	10 ♦	10 ♦≡	SSW 1	SE 1	W 2
21	73.0	67.6	63.2	67.9	0.4	2.6	3.4	2.4	3.7	-0.2	100	98	98	99	0.0	0.2	0.1	0.1	10	10 •	10	SE 5	S 4	SW 5
22	71.7	80.0	86.6	79.4	-0.9	-1.0	-1.3	-1.1	3.7	-1.8	85	79	88	84	0.8	1.2	0.6	0.9	10	10	8	WSW 12	W 6	WSW 4
23	91.3	94.2	96.9	94.1	-5.9	-5.7	-6.8	-5.3	-0.9	-7.1	80	73	85	79	0.9	1.2	0.5	0.9	10	4	9	W 7	W 5	W 5
24	97.8	97.5	95.1	96.7	-9.5	-8.6	-6.8	-7.9	-6.4	-11.0	98	89	96	94	0.1	0.4	0.1	0.2	10 ≡	10	10	C 0	S 1	SSW 3
25	95.7	93.9	94.1	93.9	-4.5	-1.7	-2.5	-2.8	-1.2	-7.1	88	73	91	84	0.5	1.5	0.5	0.8	10	5	10 *	SSE 3	SSE 5	S 5
26	89.5	83.1	82.3	84.9	-5.3	-0.1	-1.6	-2.2	1.3	-5.8	87	69	80	79	0.5	1.9	1.1	1.2	6	7	5	SSE 5	S 6	SW 5
27	81.9	75.6	65.8	74.4	-0.5	1.0	3.2	1.7	3.4	-2.1	90	92	86	89	0.6	0.5	1.1	0.7	10	10 *	10	SSW 2	S 4	SSW 5
28	64.0	66.6	73.0	67.9	3.3	1.9	1.2	1.9	4.8	1.0	95	89	89	91	0.4	0.8	0.8	0.7	10	10	10	SW 4	WSW 4	SW 5
29	79.4	83.2	80.9	81.2	1.4	1.6	0.2	0.8	2.2	0.0	78	81	77	79	1.6	1.3	1.4	1.4	8	7	3	WSW 7	WSW 8	S 5
30	72.6	74.1	74.7	73.8	2.6	3.6	2.2	2.6	5.7	-0.1	72	91	96	86	2.1	0.7	0.3	1.0	8	10	10 •	SW 5	SSW 4	WSW 4
31																								
M	88.4	88.3	88.0	88.2	-1.8	0.5	-0.8	-0.7	2.0	-3.4	90	82	91	88	0.6	1.3	0.6	0.8	8.6	8.2	8.2	4.1	4.3	4.2

Grudzień – Décembre

Dni	Ciśnienie P=900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	77.2	78.1	82.6	79.3	0.2	4.5	2.2	2.3	4.8	-0.1	94	57	68	73	0.4	3.6	2.3	2.1	2	0	9	SW 3	WSW 8	SW 5
2	85.0	85.6	84.7	85.1	0.8	1.8	-0.5	0.4	2.5	-0.5	75	78	90	81	1.6	1.6	0.6	1.3	9	10	8	SW 5	WSW 5	SW 5
3	78.4	77.3	76.2	77.3	-1.7	0.4	-1.6	-1.1	0.7	-3.0	84	74	98	85	0.9	1.7	0.1	0.9	6	10	10	SW 2	SSW 3	SSW 4
4	76.6	78.7	82.2	79.2	-0.1	1.0	-2.3	-0.9	1.6	-3.0	98	81	95	91	0.2	1.3	0.4	0.6	8	7	2	WSW 5	SW 2	SW 3
5	83.4	83.6	76.4	81.1	1.0	2.8	1.2	1.6	3.5	-3.0	87	76	77	80	0.9	1.9	1.5	1.4	10	4	10	SW 4	SW 3	WSW 6
6	71.8	75.9	80.7	76.1	2.6	4.5	3.4	3.5	6.1	0.6	86	82	76	81	1.1	1.3	1.9	1.5	10 •	3	2	WSW 7	SW 6	WSW 5
7	84.0	86.9	88.4	86.4	1.8	4.0	2.7	2.8	4.7	1.0	82	80	88	85	1.3	1.6	0.9	1.3	8	9	10	SW 2	WSW 4	WSW 4
8	89.3	90.2	92.8	90.8	1.0	1.4	0.4	0.8	2.9	0.0	92	94	88	91	0.5	0.4	0.8	0.6	10	10	0	WSW 4	SW 3	W 3
9	97.1	94.0	85.0	92.0	-2.2	2.0	0.2	0.0	2.9	-2.7	94	71	72	79	0.3	2.1	1.7	1.4	3	6	0	SW 3	SSW 3	SW 6
10	68.7	65.5	63.6	65.9	2.6	5.8	4.6	4.4	6.4	-0.5	79	77	89	82	1.6	2.1	1.0	1.6	9	10 •	10	SW 6	SW 5	WSW 5
11	66.8	69.7	72.6	69.7	1.8	2.4	0.5	1.3	4.8	0.3	85	86	79	83	1.1	1.1	1.3	1.2	8	10	10	W 3	W 2	WSW 4
12	75.2	78.0	81.0	78.1	-0.5	1.2	0.4	0.4	1.5	-2.0	90	74	92	85	0.6	1.8	0.5	1.0	10	8	10 *	W 3	WSW 3	W 3
13	84.1	85.8	85.8	85.2	-1.7	-0.9	-3.9	-2.6	0.7	-4.7	96	81	94	90	0.2	1.1	0.3	0.5	10	9	0	W 3	W 3	S 2
14	86.8	93.1	98.9	92.9	-2.6	-3.1	-4.5	-3.7	-2.3	-5.4	91	72	74	79	0.5	1.3	1.1	1.0	10	10 *	10	NE 4	NNE 5	W 1
15	98.4	94.3	96.3	96.2	-8.1	-4.3	-5.7	-6.0	-1.8	-9.0	92	94	97	94	0.2	0.3	0.1	0.2	6	10 *	10	SW 4	SW 5	NE 4
16	97.8	97.2	97.9	97.6	-8.5	-6.1	-11.5	-9.4	-5.0	-11.7	89	76	97	87	0.3	0.9	0.1	0.4	8	1	3	E 1	SW 2	SE 1
17	95.7	93.9	92.4	94.0	-13.9	-7.5	-5.1	-7.8	-4.8	-15.4	96	95	98	96	0.1	0.2	0.1	0.1	9	10 *	10 *	ESE 3	ESE 3	SE 1
18	93.1	91.8	90.1	91.7	-1.7	0.4	1.6	0.5	1.8	-5.2	96	92	100	96	0.2	0.5	0.0	0.2	10	10	10 •	S 2	S 4	SW 7
19	90.2	91.4	89.6	90.4	4.0	5.4	4.4	4.6	6.0	1.5	100	98	92	97	0.0	0.2	0.7	0.3	10 ≡	10	10	WSW 6	SW 4	SW 5
20	90.0	93.5	92.8	92.1	5.3	4.2	3.6	4.2	7.1	3.6	94	82	95	90	0.6	1.4	0.4	0.8	10	10	10	W 5	W 3	SE 1
21	87.8	86.3	87.0	87.0	3.0	4.0	2.8	3.2	4.5	2.5	100	98	98	99	0.0	0.1	0.2	0.1	10	10	10	SE 2	SW 2	W 3
22	90.9	92.2	93.1	92.1	0.5	0.4	-0.3	0.1	3.0	-0.4	100	92	96	96	0.0	0.5	0.3	0.3	10 *	9	10	W 5	WSW 3	NE 3
23	92.4	90.4	86.1	89.6	-1.0	-1.6	-3.3	-2.3	0.0	-3.5	79	74	93	82	1.2	1.4	0.4	1.0	10	9	10	E 6	E 3	SE 2
24	80.6	77.6	74.2	77.5	-1.9	0.1	-0.9	-0.9	0.7	-3.3	98	88	94	93	0.1	0.8	0.3	0.4	10	10	9	SE 2	SSW 4	SSE 3
25	69.8	67.4	66.9	68.0	-2.3	2.0	-1.8	-1.0	2.3	-4.0	93	71	96	87	0.4	2.1	0.3	0.9	2	4	8	SSE 3	S 3	SE 3
26	66.9	68.6	72.1	69.2	-2.2	-0.1	1.8	0.3	2.3	-2.3	100	94	89	94	0.0	0.4	0.8	0.4	10 m	9	10	SSE 3	S 2	W 3
27	81.2	81.5	76.3	79.7	-0.5	2.5	-0.1	0.4	3.7	-1.3	94	67	82	81	0.4	2.4	1.1	1.3	4	0	6	SW 3	SW 3	S 3
28	69.3	72.0	82.0	74.3	0.8	2.4	-0.5	0.6	2.7	-0.7	96	93	70	86	0.3	0.6	1.8	0.9	10 ♦	9	10	SW 3	W 3	WSW 3
29	86.0	87.1	90.4	87.8	-1.1	0.4	-1.9	-1.1	0.9	-2.2	79	70	83	77	1.2	1.9	0.9	1.3	10	3	7	W 3	W 8	W 3
30	89.3	83.2	82.6	85.7	-3.9	1.0	1.1	-0.2	2.3	-3.0	83	53	64	68	0.7	3.0	2.4	2.0	0	5	10	SW 3	SW 6	SW 7
31	83.0	83.3	83.8	83.4	0.6	2.2	1.2	1.3	3.2	0.2	81	78	92	84	1.3	1.6	0.3	1.1	10	8	10	SW 6	W 4	WSW 3
M	83.5	83.7	84.0	83.7	-0.9	1.1	-0.4	-0.2	2.3	-2.6	90	81	88	86	0.6	1.3	0.8	0.9	8.1	7.5	7.9	5.7	5.8	3.7

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w = 206\,m$ anemometr M-47 / $201\,m$ wiatromierz Wildt **Listopad - Novembre 1965**

DNI	WIDZIALNOŚĆ	OPAD R	GŁUB. ŚNIEGU h	POGODA
1	7	2.5	•	•°12^{05} 13^{10}–14^{35}, 19^{40} 20^{45} 21^{25} 22^{20}. = 0^{00} 10^{30} 12^{45}–24
2	7	1.0	•	⚲°11^{30}–40 11^{55}, 12^{02} 12^{28}–45 12^{50} 13^{07}. = 0^{00}–6^{20}
3	7	1.6	•	•°21^{15}...22–48 22^{10}...23^{12}; por. wiatru 14 m/sek 4^{05}–45
4	7	•	•	= 0^{00}–5^{30} 17^{30}–24; ⊕ 19^{05}–24
5	7	•	•	= 0^{00}–11^{30}; = 17^{15}–24; ⌣°5–9; ⊕ 0^{00}–10^{00}
6	7	•	•	= 0^{00}–8^{30} 18^{30}–24
7	6	•	•	= 0^{00}–13^{15} 17^{40}–24
8	7	•	•	= 0^{00}–11^{15}, 16^{15}–24; ⌣°4–9, 19–24
9	1	0.2	•	•°22^{30}–23^{40} 24; = 0^{00}–3^{40} ≡°–3^{45} ≡¹–5^{15} ≡¹–6^{20} ≡²–19^{35} ≡¹–24; ⌣°0^{00}–2 ⌣¹3–22^{30}
10	3	0.1	•	•°0^{00}...15 6^{10}–7^{45} 9^{20}–10^{15} 17^{20}...35–19^{45}; ≡¹$0^{00}$–3^{30} ≡°–5^{40} ≡¹–7^{30} ≡°–12^{45} = –15^{30} ≡°–23^{45} = –24
11	7	9.6	•	*16^{45} 17^{30}–20^{15} *¹–22^{20} *°–24, por. wiatru 12 m/sek 12^{30} 20^{20} ≫–24 (por. 14 m/sek); = 0^{00}–10^{40}, 17^{20}–24; ⌣ 3^{45}–4^{30}
12	5	3.8	15	*°0^{00}–10 *¹–2^{35} *°–14^{30} △°–15^{40} ≫0^{00}–2^{40} por. wiatru 14 m/sek 3^{15}–40; = 0^{00}–24
13	6	1.7	15	*°11^{35}–19^{30}...20^{20}; = 0^{00}–24
14	6	2.0	15	*°8^{45} 12^{20}–24; = 0^{00}–24
15	6	0.7	15	*°0^{00}–5^{25} 7^{25}–9^{30} 12^{20} 12^{40} 13^{20} 15^{15} 20^{20}; = 0^{00}–24
16	6	0.7	15	*°4^{20}...8^{20} △°–9^{35} *¹$17^{40}$...19^{20}; = 0^{00}–24
17	7	0.1	15	*°0^{20} 4^{30}–5^{15} 7^{05}–9^{20}; = 0^{00}–12^{00} 17^{30}–24
18	6	0.9	15	*°19^{02} 20^{05}–21^{25}...22^{10}; = 0^{00}–24
19	6	•	14	= 0^{00}–24
20	5	4.9	12	⌣°12^{45}–13^{40} •°–14^{50} •°–18^{40}...19^{30}–23^{35}; = 0^{00}–16^{50} ≡°–24; ∽ 12^{45}–14^{50}
21	5	4.1	10	•°0^{33}–15^{25}, 16^{35} 17^{15}–18^{40}; ≡°0^{00}–1^{15} ≡¹–3^{25} ≡°–4^{45} = –7^{40} ≡°–9^{45} = –24
22	7	0.0	5	•°14^{40} 3^{20} ⚹°15^{20}–28 15^{54}–16^{06}; por. wiatru 15 m/sek 6^{15}–25 ≫–9^{35} por. wiatru 15 m/sek 9^{40}–10^{15}; = 0^{00}–6^{15}
23	7	0.0	5	*°3^{40} 4^{15}, 6^{25} 7^{20}; = 3^{30}–7^{15}
24	5	•	4	△°5^{45}–6^{55}; = 4^{15}–6^{30} ≡¹–9^{15} ≡²–11^{45} = –24
25	7	0.3	4	*°18^{30} 21^{20}; = 0^{00}–8^{30} 18^{15}–24
26	7	0.2	4	*°23^{20}...24; = 0^{00}–9^{30}, 23^{30}–24
27	6	0.9	4	*°0^{00} 1^{15} 11^{45} 12^{10} *¹–12^{30} *²–12^{45} *¹–13^{05} *°–13^{15} •°21^{44}–22^{15}; = 0^{00}–24
28	6	2.2	3	•°3^{30}–5^{45} 7^{15}–10^{15} 10^{30} 12^{20} *°18^{20}–30 19^{35}...20^{03}; = 0^{00}–13^{20}, 19^{20}–24
29	7	0.0	pł.	*°9^{35}–10^{30} 11^{05}; por. wiatru 5^{30}–6^{10} = 0^{00}–5^{30}
30	7	2.5	pł.	•°11^{43}...12^{05}–44 13^{25}...38 14^{17}...28 16^{45} 17^{10}–21^{40} •°22^{35}–24; = 16^{45}–24
31				
Σ	–	39.8	–	

Grudzień - Décembre

DNI	WIDZIALNOŚĆ	OPAD R	GŁUB. ŚNIEGU h	POGODA
1	7	•	pł.	•°0^{00}...20 *°3^{40} 4^{15}; por. wiatru 12 m/sek 12^{15}–14^{20}; = 0^{00}–9^{30}
2	7	•	pł.	= 22^{30}–24
3	7	4.1	pł.	*°17^{05}–21^{40} *¹–22^{26} *°–24; = 0^{00}–6^{30}, 17^{30}–24
4	7	•	6	*°0^{00}–20...3^{20}; = 0^{00}–11^{40}, 17^{50}–24
5	7	1.1	6	•*°23^{38}–24; = 0^{00}–7^{15}, 23^{38}–24
6	7	0.8	4	•*°0^{00}–2^{20} •°–5^{10}, 6^{10}–7^{38} ⚲°10^{15}–23, 10^{27}–34, 10^{36}–40 △°⚲°–10^{44} •°–10^{51}; = 0^{00}–8^{15}
7	7	•	3	= 21^{30}–24
8	6	•	pł.	= 0^{00}–24; ⊕ 9^{30}–10^{30}
9	7	•	pł.	= 0^{00}–12^{15}; ⊕ 11^{35}–12^{20} ⌓ 22^{40}–24
10	7	0.2	pł.	•°12^{28} 13^{15}, 13^{50} 14^{05}–35 16^{40}; = 15^{30}–24; ⌓ 0^{00}–10
11	6	•	pł.	= 0^{00}–24; ⌣°23–24; ⊕ 20^{23}–22^{30}
12	7	0.4	pł.	△ 20^{02}–45; = 0^{00}–10^{30} 20^{15}–24; ⌣°0^{00}–10^{30}
13	7	0.0	1	*°0^{40} 1^{20}, 3^{50}–5^{05} 8^{45} 9^{10} 10^{05} 11^{25}; = 0^{00}–9^{30} 21^{40}–24
14	6	0.2	1	*°10^{40} 11^{15} 12^{20} 15^{30}; = 0^{00}–24; ⌓ 1^{00}–45
15	5	4.3	2	*°7^{45} 11^{35}–12^{15} *¹–14^{05} *°–14^{25} *¹–15^{30} *°–18^{25}...45; = 0^{00}–24
16	7	•	6	= 0^{00}–11^{30} 19^{30}–24; ⌣°21–22 ⌣¹23–24
17	6	3.3	6	*°10^{38} 11^{10}, 11^{35} 13^{30}–14^{30} 14^{40} 15^{20} 17^{35}–23^{40}; = 0^{00}–24; ⌣¹$0^{00}$–6
18	6	15.5	8	•°13^{55} 16^{15}–17^{45} •°–18^{30} •°–19^{45} •¹–20^{20} •°–22^{30} •¹–23^{15} •°–24; = 0^{00}–24
19	5	0.7	3	•°0^{00}–6^{15}...35 9^{05}–35 13^{15}–25 13^{35} 14^{10}; ≡°0^{50}–7^{15} ≡¹–9^{45} ≡¹–11^{10} ≡°–11^{45} = –24
20	7	•	•	•°4^{40}–5^{20} 5^{45}–6^{25}; = 0^{00}–10^{30} 16^{25}–24
21	5	1.8	•	•°11^{10}–17 11^{31}–12^{10} 12^{25}...37 14^{28}–15^{15} 15^{48}...16^{20} △°23^{40}–24; = 0^{00}–24
22	6	0.7	1	△°0^{00} 1^{30} *°–2^{15} 7^{25}–9^{35}, 10^{10}–20; = 0^{00}–24
23	7	•	pł.	= 0^{00}–3^{30}
24	7	•	pł.	= 16^{20}–24
25	7	•	pł.	= 0^{00}–9^{30}, 20^{15}–24; ⌣°21–24
26	6	1.2	pł.	•°18^{06}...48 *°21^{12}–24; = 0^{00}–3^{20} ≡¹–7^{40} ≡°–9^{30} = –24; ⌣°0^{00}–9
27	7	3.6	•	*°0^{00}–1^{17}; = 0^{00}–10^{30}
28	6	0.0	1	*°1^{35}–4^{20} *°–6^{10} •°8^{20}; = 14^{5}–20^{15}
29	7	0.0	1	*°14^{17}–26 14^{50}–15^{08} *°15^{10} 16^{15}; ⌓ 19^{30}–21^{30}
30	7	•	1	
31	7	•	pł.	= 16^{16}–24
Σ	–	37.9	–	

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Styczeń – Janvier 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	82.0	81.7	80.4	81.4	5.3	5.6	2.1	3.8	7.0	1.9	48	56	91	65	4.6	4.0	0.6	3.1	9	10	10 •	SW 4	C 0	C 0
2	76.4	75.5	77.1	76.5	0.8	1.5	0.8	1.0	2.2	0.4	98	100	96	98	0.2	0.0	0.3	0.2	10 • ≡	10 * ≡	10 * ≡	C 0	C 0	SW 1
3	79.0	79.9	80.5	79.8	0.9	0.6	0.5	0.6	1.0	0.2	96	98	90	95	0.2	0.1	0.6	0.3	10 *	10 * ≡	10 *	WSW 1	N 1	NNE 1
4	83.2	86.6	93.1	87.6	-0.5	0.0	-1.6	-0.9	0.6	-1.8	96	100	82	93	0.3	0.0	1.0	0.4	10 *	10 *	3	N 5	N 5	W 2
5	94.3	90.7	92.8	92.6	-2.8	0.0	0.3	-0.6	0.4	-4.6	77	65	95	78	1.1	2.1	0.4	1.2	5	10 *	8	SW 5	SSW 6	SW 5
6	93.8	94.4	93.3	93.8	0.4	0.5	-0.7	-0.1	1.3	-0.9	79	85	85	82	1.3	1.0	0.9	1.1	8	8	9	WSW 5	WSW 2	NNW 6
7	95.5	96.3	94.6	95.5	-4.3	-4.4	-6.1	-6.2	-0.7	-8.2	70	84	75	76	1.3	0.7	0.8	0.9	7	10	4	W 5	WSW 4	C 0
8	88.2	84.7	79.2	84.0	-7.8	-0.6	2.4	-0.9	2.7	-11.8	87	81	89	86	0.4	1.1	0.8	0.8	10	9	10	C 0	SW 1	SW 5
9	79.4	79.4	80.2	79.7	4.4	3.5	0.9	2.4	4.5	0.8	84	91	98	91	1.4	0.6	0.1	0.7	10	10 •	10 •	WSW 1	WSW 5	SW 1
10	77.6	76.3	90.7	81.5	0.9	1.5	-0.9	0.2	2.2	-1.0	79	94	94	89	1.4	0.4	0.5	0.7	9	10 *	10	SW 1	WSW 5	NW 5
11	99.4	99.0	97.5	98.6	-5.7	-5.1	-8.6	-7.0	-0.8	-8.7	92	88	89	90	0.3	0.5	0.4	0.4	10	1	1	NW 5	NW 2	NW 1
12	95.6	93.4	91.2	93.4	-9.7	-2.9	-3.5	-4.9	-0.4	-10.8	94	82	85	87	0.2	0.9	0.7	0.6	8	9	3	C 0	C 0	C 0
13	91.0	92.0	93.5	92.2	-7.6	0.1	-3.6	-5.7	0.9	-7.8	84	75	90	83	0.5	1.6	0.5	0.9	4 ≡	0 ≡	0 ≡	C 0	C 0	C 0
14	90.7	88.5	91.2	90.1	-6.7	1.1	1.3	-0.8	5.9	-7.4	96	83	77	85	0.1	1.1	1.5	0.9	4 ≡	4	9	C 0	NW 1	W 2
15	96.9	96.4	94.0	95.8	1.1	3.0	-1.5	0.3	3.9	-1.7	81	77	89	82	1.2	1.7	0.6	1.2	9	9	9	C 0	C 0	C 0
16	91.9	92.8	92.8	92.5	-2.3	1.4	0.7	0.1	1.8	-5.4	91	81	81	84	0.5	1.3	1.2	1.0	7 ≡	9 ≡	4	C 0	N 1	SW 1
17	84.1	79.7	73.3	79.0	-3.7	5.9	4.7	2.9	7.8	-4.3	90	50	64	68	0.5	4.7	3.1	2.8	9	10	10	C 0	C 0	S 1
18	72.4	72.1	70.6	71.7	2.3	4.7	2.0	2.8	5.7	1.4	91	76	71	79	0.6	2.0	2.1	1.6	9	10	4	SW 1	SW 1	SW 1
19	68.9	69.0	70.9	69.6	-3.1	2.4	-1.6	-1.0	3.2	-3.8	93	68	86	82	0.4	2.4	0.7	1.2	3 ≡	9	9	C 0	SW 1	ESE 1
20	67.2	65.7	63.1	64.7	-1.1	-0.7	-1.1	-1.0	-0.7	-3.9	85	97	99	94	0.9	0.2	0.1	0.4	10	10 *	10 ≡	NE 4	ENE 4	ENE 1
21	66.5	70.5	76.7	71.2	-0.7	-0.1	-0.1	-0.2	0.3	-1.5	97	98	94	96	0.2	0.2	0.4	0.3	10 ≡	10 ≡	10	NW 1	WNW 2	SW 1
22	79.8	82.0	84.5	82.1	-1.1	2.1	-3.1	-1.3	2.2	-3.4	93	68	77	79	0.4	2.3	1.1	1.3	10	10	0	C 0	SW 2	C 0
23	87.1	89.0	92.7	89.6	-3.4	-0.9	0.2	-1.0	0.4	-5.4	92	93	90	92	0.4	0.4	0.6	0.5	10 ≡	10 * ≡	10 * ≡	C 0	C 0	C 0
24	96.6	96.9	96.7	96.7	-0.1	1.5	-0.1	0.3	1.7	-0.5	94	87	94	92	0.4	0.9	0.4	0.6	10 ≡	10	10	C 0	NW 2	WNW 1
25	93.4	91.5	90.8	91.9	-1.3	-0.2	-0.6	-0.7	0.3	-1.6	95	88	87	90	0.3	0.7	0.7	0.6	10 ≡	10 ≡	10	WNW 2	WNW 1	C 0
26	89.2	88.2	88.0	88.5	-5.5	0.0	-3.9	-3.3	0.6	-5.7	97	84	92	91	0.1	0.9	0.4	0.5	10 ≡	7	6	C 0	WSW 1	C 0
27	87.4	88.0	87.2	87.5	-6.7	-2.5	-1.6	-3.1	-0.5	-7.0	96	87	98	94	0.1	0.7	0.1	0.3	10	10	8	ESE 1	NNE 1	C 0
28	88.4	88.3	87.6	88.1	-5.9	1.4	2.3	0.0	3.1	-6.1	97	78	86	87	0.1	1.6	1.0	0.9	3 ≡	9	8	SSE 2	NE 3	NE 2
29	85.7	84.3	84.5	84.8	0.5	5.7	2.2	2.6	8.3	-0.9	94	71	93	86	0.3	2.7	0.6	1.2	10	9	10 ≡	C 0	NE 2	C 0
30	82.9	81.9	82.0	82.3	0.1	4.5	2.4	2.4	4.6	-1.1	98	79	91	89	0.2	1.8	0.7	0.9	8 ≡	7	10 ≡	C 0	C 0	C 0
31	85.2	86.5	85.1	85.6	2.7	1.3	-0.2	0.9	3.8	-0.3	98	94	92	95	0.1	0.4	0.5	0.3	10 ≡	10 * ≡	10 * ≡	C 0	C 0	NNE 2
M	85.5	85.1	85.7	85.4	-2.0	1.0	-0.6	-0.6	2.4	-3.5	89	82	86	86	0.6	1.3	0.8	0.9	8.5	8.7	7.6	1.1	1.5	1.1

Luty – Février

1	89.1	89.8	92.6	90.5	-0.5	-0.7	-2.6	-1.6	0.0	-2.7	100	83	79	87	0.0	1.0	1.1	0.7	10	10 *	10	NNW 2	SW 2	SSW 1
2	95.4	97.1	100.9	97.8	-2.8	-2.5	-2.9	-2.8	-1.9	-4.1	80	80	75	78	1.0	1.0	1.2	1.1	10 *	10 * ≡	9	SSW 2	WSW 5	W 3
3	100.6	98.1	96.9	98.5	-7.2	-2.1	-2.7	-3.7	-1.5	-7.4	96	87	89	91	0.1	0.6	0.6	0.4	10	10 *	10	W 4	W 3	W 3
4	95.6	96.0	95.1	95.6	-2.9	-0.6	-2.7	-2.2	-0.5	-3.6	93	93	93	93	0.3	0.4	0.3	0.3	10	10 *	10	W 2	WSW 4	W 4
5	92.5	92.0	95.6	93.4	-11.5	-10.1	-14.6	-12.7	-2.7	-15.6	93	74	83	83	0.2	0.7	0.3	0.4	10 *	2	0	C 0	NNE 2	NNE 1
6	99.7	98.7	95.8	98.1	-17.5	-11.0	-15.4	-14.8	-9.5	-17.8	85	76	86	82	0.2	0.6	0.3	0.4	10 ≡	0	2	C 0	W 2	C 0
7	93.7	93.2	86.4	91.1	-22.5	-11.6	-10.7	-13.9	-8.3	-22.6	88	79	83	83	0.1	0.5	0.4	0.3	10 ≡	0	8	C 0	W 1	C 0
8	68.8	72.8	77.2	72.9	-2.4	-2.9	-5.1	-3.9	-0.4	-10.7	89	75	68	77	0.5	1.2	1.3	1.0	10 * ≡	8	10 *	NNW 10	WSW 8	WNW 3
9	86.9	90.3	96.3	91.2	-7.2	-6.0	-9.0	-7.8	-4.8	-9.1	88	81	67	79	0.4	0.7	1.0	0.7	10 *	9	10 *	N 2	NNW 2	NW 1
10	94.4	88.8	87.1	90.1	-15.2	-4.9	-3.5	-6.8	-2.4	-15.6	91	49	88	76	0.2	2.1	0.6	1.0	8	9	10 *	W 1	SW 2	WSW 5
11	90.0	91.8	93.4	91.7	-2.4	1.5	-0.7	-0.6	1.8	-3.7	85	69	69	74	0.8	2.1	1.8	1.6	10	2	9	SW 1	WSW 5	WSW 5
12	96.0	95.4	93.8	95.1	-7.6	2.6	1.3	-0.5	4.1	-8.4	87	57	76	73	0.4	3.2	1.6	1.7	2 ≡	2	10 *	C 0	SW 3	WSW 2
13	87.4	82.7	77.0	82.4	0.3	3.3	2.8	2.3	3.6	0.1	90	64	72	73	0.6	2.7	2.1	1.8	6	10	10 •	SW 3	SSW 4	SW 3
14	73.4	73.0	78.6	75.0	2.0	5.0	0.7	2.1	5.3	0.3	68	54	94	72	2.3	4.0	0.4	2.2	8	7	9	SSW 3	WSW 9	W 5
15	83.3	85.1	85.8	84.7	-0.5	0.1	-3.3	-2.8	1.1	-3.4	88	72	73	78	0.7	1.8	1.0	1.2	10 *	3	8	SW 5	SSW 4	C 0
16	86.3	86.8	87.6	86.9	-8.9	-1.6	-3.7	-4.3	-1.2	-9.6	98	73	83	83	0.1	1.4	0.7	0.7	10 ≡	10	10	WNW 1	WNW 1	WNW 3
17	86.5	86.1	87.8	86.8	-3.3	-4.3	-4.3	-4.6	-3.5	-3.9	87	94	96	92	0.3	0.3	0.2	0.3	10 * ≡	10 * ≡	10 * ≡	NW 4	W 3	SSW 2
18	90.3	91.7	94.2	92.1	-3.4	-3.7	-3.3	-4.4	-1.8	-3.3	97	99	98	98	0.2	0.1	0.1	0.1	10	10 *	10 *	NE 2	NNE 3	N 3
19	94.4	94.3	96.7	95.1	-6.3	-2.9	-6.1	-3.4	-2.3	-6.7	94	93	86	91	0.2	0.3	0.3	0.3	10 *	10 *	10	NW 3	NW 2	NNE 1
20	99.3	101.6	102.1	101.0	-7.3	-3.3	-3.3	-3.8	-3.1	-7.8	90	72	80	81	0.3	1.1	0.8	0.7	10 *	9	10	NE 3	NE 3	NE 4
21	99.9	97.8	94.2	97.3	-8.0	-4.3	-3.7	-3.9	-4.3	-8.4	98	82	87	89	0.1	0.8	0.3	0.5	10 * ≡	10	10	NE 3	NE 1	W 2
22	88.4	87.0	90.0	88.5	-3.4	-3.4	-6.3	-3.4	-2.0	-8.0	90	88	81	86	0.4	0.6	0.7	0.6	10	10 * ≡	10	SW 6	SW 7	WSW 2
23	89.8	88.9	89.2	89.3	-4.9	-3.2	-6.3	-3.3	-2.3	-7.0	95	86	94	92	0.2	0.7	0.2	0.4	10 * ≡	10 * ≡	7	SW 3	W 2	C 0
24	91.4	89.6	85.2	88.7	-9.8	-3.0	-6.7	-6.6	-2.3	-11.8	81	73	88	81	0.3	1.3	0.4	0.7	10 * ≡	7	8	C 0	W 1	S 2
25	79.8	78.4	83.7	80.6	-2.9	-0.3	-6.9	-4.2	0.1	-9.2	86	80	61	75	0.7	1.2	1.4	1.1	10 *	10	10	WSW 4	WSW 7	WSW 3
26	86.8	84.9	79.8	83.8	-10.4	-2.1	-4.3	-3.4	-0.8	-17.3	80	68	58	69	0.5	1.6	1.9	1.3	9	2	9	SSW 2	W 4	SSW 2
27	71.4	68.8	73.4	71.9	-2.9	-0.2	-6.3	-3.9	-0.1	-6.3	66	61	81	69	1.6	2.3	0.7	1.3	10	10	10 *	SSW 4	SW 6	SSW 4
28	84.9	87.6	87.6	86.7	-7.4	-4.2	-12.3	-9.0	-3.1	-12.4	76	47	70	64	0.8	2.4	0.7	1.3	9 *	7	0	SW 4	W 3	WSW 1
29																								
30																								
31																								
M	89.1	88.9	89.5	89.2	-6.5	-2.8	-5.4	-5.0	-1.6	-8.7	88	73	81	81	0.5	1.3	0.8	0.9	9.4	7.3	8.3	2.6	3.3	2.3

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$ *Styczeń – Janvier 1965*

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	4	5.6	7	• 17^{00} – n; = II, III
2	3	4.7	4	•° na •! *°II *° *° 15^{30} – III; ≡° I, II, III
3	3	8.9	5	*° △ *° na – I *$^{0-1}$ a, II *° p, III; = I ≡° II, III
4	5	0.5	11	*$^{0-1}$ na, I *° a – 15^{30}; = I, II
5	5	0.4	11	*° 11^{00} – II *^{1} – 16^{00}; ≫ a; = I, II, III
6	6	•	12	= I
7	4	•	12	= III; ⌣° III
8	4	1.6	11	*° 8^{30} – 9^{00} •° ok. 19^{00} III; = I, II; ⌣° I
9	4	7.5	7	•° II *$^{1-0}$ p •° III – np; = I, II, III
10	4	3.5	5	*$^{0-1}$ ok. 8^{00} – a * 11^{30} – ok. 15^{00}; = II
11	4	•	5	= II; ∽ na ⌣^{1} III ∽ p
12	4	•	4	= I, II, III; ⌣^{1} I ⌣° III
13	3	•	4	≡ I, II, III; ⌣^{1} I
14	4	•	4	≡ I = II; ⌣^{1} I
15	4	•	4	= I = II, III; ⊕ II; ψ III
16	3	•	4	≡° I, II = III; ⌣° I
17	6	8.7	4	•$^{0-1}$ 17^{15} – 45; = II; ⌣^{1} I
18	6	•	2	= I, ψ III
19	5	•	2	≡° I = II; ⌣° I, III
20	6	4.0	2	* 7^{10} *° 7^{20} II – ok. 15^{00}; = I ≡^{1} III
21	3	•	6	≡° I, II = III
22	5	•	6	= I, II, III
23	3	1.2	5	*^{1} ok. 10^{30} – p * – III; ≡° I, II, III
24	4	2.3	6	* a * p; ≡° I = II, III
25	3	•	10	* n; ≡° I, II = III
26	4	•	10	≡^{1} I ≡° ok. 8^{30} = ok. 9^{30}, II, III, ⌣° I, III
27	4	(0.0)	8	*° a; = I, II, III
28	5	•	8	≡° I = II; ⌣° I
29	9	•	5	= I ≡° III
30	4	1.0	3	≡° I = II ≡° III; ⌣° I
31	3	14.1	2	•° n •! *° a *$^{0-1}$ a, II *° III – n; ≡° I, II, III
Σ	–	64.0	–	Uwaga. Wartości ciśnienia powietrza w ciągu całego roku są za niskie przeciętnie o ok. 0,5 mb.

Luty – Février

1	5	0.9	16	* n *° 12^{40} II *$^{1-2}$ 14^{20} – 16^{15}; = I, II
2	3	1.6	17	* n *° I *^{2} 7^{40} – 55 *$^{1-0}$ 8^{30} *^{2} II *° 14^{30}; = I ≡° II
3	4	0.3	18	* a * II *^{1} p z prz.; = I, II, III
4	4	1.4	15	* n *° a z prz.; II *$^{0-1}$ p – 20^{35}; = I, II
5	6	0.0	14	*° na, ok. 6^{30} – a; = I, ⌣° I
6	4	•	14	≡ I = II, III; ⌣° I, III
7	4	2.4	12	≡° I = II, III
8	6	2.9	18	*^{1} na, I, * a *° p z prz. – np * n; ⊹ na, I, a, II; ≫ na, a; ≡° I
9	5	0.2	23	*$^{1-0}$ na *° na – 9^{30}, 13^{55} III; = II
10	5	0.6	20	*° n *$^{1-0}$ ok. 17^{00} III; = I, II, III; ⌣° I
11	4	•	20	*° n; = I, II, III, ⊖ III
12	4	0.0	18	*° ok. 20^{30} – np * n; ≡° I = II
13	6	0.0	17	• III; = I
14	8	4.3	12	*^{2} 7^{55} – 8^{30} *$^{0-2}$ p z prz. *° • p
15	6	0.0	13	* △ na *^{1} I *° △ a; = I, III; ⌣° III
16	4	2.4	12	*° 9^{30} – 10^{00}, p z prz.; ≡° I = II; ⌣° I
17	3	7.8	17	*^{1} na – a *^{2} – p *° III; ≡° I, II, III
18	4	2.5	26	*^{1} na – a *^{2} a *^{1} II, p z prz., III; = I, II
19	5	2.3	28	*° I – a *^{1} – p * do ok. 15^{00}; = II, III
20	6	0.2	31	*$^{0-2}$ na z prz. *° I, a; = I
21	5	1.3	28	*° na, I – ok. 9^{00}; ≡° I = II, III
22	3	1.4	28	*$^{1-2}$ 8^{30} – 11^{15} *^{2} ok. 12^{00} – ok. 14^{00}; ⊹ na, a; = I ≡° II = III
23	3	1.6	29	*$^{0-1}$ na, I *^{1} a, II *^{2} – ok. 14^{00}; ≡° I, II = III
24	4	0.4	29	*$^{0-1}$ na, I; ≡° I = II; ⌣° I
25	4	1.6	25	* na, I, a *^{2} ok. 13^{00} – 14^{00}; ⊹ a; = I, II
26	7	•	29	= I
27	6	1.6	24	*^{2} 13^{07} – 40, 16^{30} – 50 *° 17^{00} – n; ⊹ 13^{07} – 40, 16^{30} – 50; = III
28	6	0.0	28	*° na, I; ≡ I; ⊕ II
29				
30				
31				
Σ	–	37.7	–	

Kraków, Obserw. Ast. UJ $\varphi = 50°04'$ $\lambda = 19°58'$ *Marzec – Mars* 1965

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	83.2	80.3	76.4	80.0	-10.8	3.7	-0.3	-1.9	4.1	-15.9	66	46	76	63	0.9	4.3	1.5	2.2	10	10	7	SW 1	SSE 3	ESE 3
2	68.7	66.9	64.2	66.6	1.5	3.9	3.3	3.0	5.1	-0.9	80	69	83	77	1.4	2.6	1.3	1.8	9	9	5	ESE 2	E 2	C 0
3	62.3	66.5	71.6	66.8	2.2	2.8	-0.3	1.1	3.6	-0.5	100	64	68	77	0.0	2.7	1.9	1.5	10 ≡ •	7	6	C 0	WSW 4	SW 4
4	75.5	76.9	79.1	77.2	-3.1	-0.9	-2.6	-2.3	-0.3	-3.6	72	50	85	69	1.3	2.9	0.8	1.7	8	10	10	SW 6	SW 10	SW 1
5	80.0	81.7	86.3	82.7	-3.7	1.7	-1.7	-1.4	2.3	-4.5	76	44	73	64	1.1	3.9	1.5	2.2	8 ≡	10	0	SW 2	WNW 3	NW 1
6	88.0	88.1	91.6	89.2	-4.4	-2.6	-2.7	-3.1	-1.6	-5.4	84	87	86	86	0.7	0.7	0.7	0.7	10	10 * ≡	10	NE 4	NE 6	NE 3
7	94.7	96.7	98.6	96.7	-3.9	-3.3	-4.1	-3.8	-2.7	-4.4	96	97	91	95	0.2	0.1	0.4	0.2	10	10	10	NE 2	NE 4	NE 2
8	98.1	97.3	97.2	97.5	-5.5	-3.9	-6.0	-5.4	-3.3	-6.4	87	82	84	84	0.5	0.8	0.6	0.6	10 ⚹	10 ⚹	10	NNE 2	NNE 2	C 0
9	97.5	96.8	98.0	97.4	-7.1	-0.7	-5.6	-4.8	0.6	-7.7	96	71	64	77	0.1	1.7	1.4	1.1	10 ≡	0	7	C 0	S 2	W 1
10	100.5	102.6	104.6	102.6	-2.6	0.3	-3.9	-2.5	1.7	-5.9	87	71	78	79	0.7	1.8	1.0	1.2	10 *	8	0 ≡	WSW 1	NW 2	C 0
11	105.7	105.3	103.7	104.9	-9.2	1.7	-3.4	-3.6	2.2	-10.4	98	58	81	79	0.1	2.9	0.9	1.3	0 ≡	0	3	C 0	C 0	C 0
12	103.0	100.5	99.6	101.0	-9.3	3.7	-0.6	-1.7	4.8	-9.8	91	54	74	73	0.3	3.7	1.3	1.8	0 ≡	3	2	NW 1	NW 1	C 0
13	99.2	98.8	99.1	99.0	-6.4	3.6	-0.5	-1.0	5.3	-7.4	94	65	74	78	0.2	2.8	1.6	1.5	10 ≡	0	5	C 0	NW 1	C 0
14	98.4	96.6	95.8	96.9	-4.3	6.4	1.0	1.0	8.0	-5.0	91	63	83	79	0.4	3.5	1.2	1.7	0	0	3	C 0	NW 1	C 0
15	95.8	95.3	94.9	95.3	-2.1	7.6	2.7	2.7	10.1	-3.0	85	68	79	77	0.7	3.3	1.3	1.8	4 ≡	9 ≡	2 ≡	C 0	C 0	C 0
16	92.2	89.8	89.7	90.6	1.1	11.7	5.4	5.9	11.8	-0.8	96	69	84	83	0.2	4.2	1.4	1.9	9 ≡	9	10	C 0	NW 1	C 0
17	89.3	87.9	85.3	87.5	4.7	5.3	3.0	4.0	6.1	2.8	98	98	100	99	0.1	0.1	0.0	0.1	10 ≡	10 ≡	10 ≡	NW 1	C 0	C 0
18	83.2	81.4	80.5	81.7	-1.3	11.7	4.1	4.6	12.8	-1.6	100	61	82	81	0.1	3.3	1.3	2.3	10 ≡	0	5	C 0	N 2	SE 1
19	80.0	81.1	85.3	82.1	0.5	14.0	6.3	6.8	14.3	-0.7	94	55	84	78	0.3	7.2	1.3	3.0	2	0	3	C 0	WSW 3	W 1
20	89.6	90.8	90.0	90.1	4.4	5.6	2.5	3.8	7.0	2.2	90	74	91	85	0.9	2.4	0.6	1.3	10	10	6	W 1	W 1	W 1
21	86.4	81.4	79.4	82.4	-0.1	12.8	6.6	6.5	13.0	-0.7	100	45	97	81	0.0	8.2	0.3	2.8	10 ≡	7	10 •	C 0	SE 2	SW 1
22	83.9	87.6	89.2	86.9	0.5	2.6	0.5	1.0	7.2	-0.2	100	72	69	80	0.0	2.1	1.9	1.3	10 * ≡	7	2	NW 3	NW 4	C 0
23	88.5	84.2	79.9	84.2	-1.8	5.8	3.5	2.8	8.0	-3.6	90	47	65	67	0.5	4.9	2.7	2.7	0	1	9	C 0	ESE 4	ENE 2
24	77.7	77.6	78.8	78.0	3.9	9.5	7.1	6.9	9.7	2.8	88	69	88	82	1.0	3.7	1.2	2.0	10 •	10	10	ENE 1	SE 2	C 0
25	81.6	83.3	88.2	85.0	7.4	7.5	3.3	6.4	9.2	4.0	83	70	80	78	1.8	3.1	1.8	2.2	10	9	8	WSW 3	WNW 2	W 1
26	89.8	87.1	87.1	88.0	3.3	9.1	5.3	5.8	11.0	3.1	97	55	92	81	0.2	5.3	0.7	2.1	10	6	10 •	C 0	WSW 3	SW 2
27	93.2	98.6	103.9	98.6	3.6	5.1	4.9	4.6	5.6	3.1	97	86	86	90	0.3	1.3	1.3	1.0	10 •	10	10	NW 3	NNE 3	N 1
28	105.9	105.2	103.6	104.9	3.1	8.8	6.9	6.4	10.7	2.9	88	63	74	75	0.9	4.2	2.5	2.5	10	7	9	N 1	NE 2	NE 1
29	102.4	101.7	100.7	101.6	6.4	9.9	9.3	8.7	11.3	5.4	82	93	93	89	1.7	1.1	0.8	1.2	10 • ≡	10 •	10	NE 1	SW 1	WNW 1
30	96.3	91.9	95.5	94.6	8.1	15.8	6.4	9.2	17.4	6.2	87	55	69	70	1.4	8.1	3.0	4.2	8	9	9	SW 3	WSW 5	NNW 5
31	98.8	95.4	95.4	96.5	0.7	6.9	4.1	4.0	9.0	0.1	79	59	75	71	1.3	4.1	2.0	2.5	6	10 •	9	SW 3	WNW 5	WNW 6
M	90.0	89.6	90.1	89.9	-0.8	5.4	1.8	2.0	6.6	-2.1	89	66	81	79	0.6	3.3	1.3	1.7	7.9	7.1	6.8	1.3	2.6	1.3

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1	99.9	102.1	101.8	101.3	-0.2	3.5	2.3	2.0	5.0	-0.6	88	49	63	67	0.7	4.0	2.7	2.5	7	7	2	NW 4	NW 4	NW 1
2	97.4	95.4	96.8	96.5	1.9	11.5	7.5	7.1	11.9	0.1	62	34	63	53	2.7	9.1	3.9	5.2	8	5	8	SW 3	WNW 7	NW 1
3	94.5	90.6	89.3	91.3	3.5	13.1	9.3	8.8	16.2	1.3	86	33	53	57	1.0	10.1	3.5	5.9	3 ≡	0	0	NW 1	WSW 5	WNW 1
4	88.2	86.5	84.7	86.5	3.6	15.1	10.1	9.7	16.0	1.9	83	33	61	59	1.3	11.5	4.8	5.9	0	3	9	SW 1	WSW 3	W 2
5	87.5	89.4	91.3	89.4	5.7	12.7	6.7	8.0	13.9	3.5	80	33	72	62	1.9	9.8	2.7	4.8	0	1	0	SW 1	NNE 3	NE 4
6	92.3	91.2	88.8	90.8	1.1	10.1	5.8	5.7	10.6	-0.9	96	56	73	75	0.2	5.4	2.3	2.7	0	0	0	ENE 2	NE 3	ENE 1
7	86.1	85.5	86.8	86.1	1.9	15.7	8.9	8.8	16.7	0.4	98	47	88	48	0.1	9.4	1.4	3.6	9	9	10	C 0	WSW 4	C 0
8	85.3	85.2	84.7	85.1	7.2	7.7	9.0	8.2	9.1	6.5	91	90	88	90	0.9	1.0	1.4	1.1	10	10	10	NNW 1	NNE 3	NE 3
9	83.3	82.6	83.2	83.0	6.9	7.7	3.5	5.4	9.0	3.4	84	79	88	84	1.6	2.2	0.9	1.6	10	10	10 •	NE 4	ENE 8	NE 14
10	84.5	86.5	87.0	86.0	1.9	2.9	1.3	1.8	3.6	1.3	85	74	76	78	1.0	1.9	1.6	1.5	10	10	10	ENE 10	NE 9	ENE 8
11	85.3	85.5	85.6	85.5	0.3	4.1	4.3	3.2	5.4	0.2	82	74	82	79	1.1	2.2	1.3	1.6	10	10	10	ENE 6	ENE 3	ENE 3
12	86.8	87.3	87.7	87.3	1.8	3.1	5.9	4.7	6.2	1.6	96	97	95	96	0.3	0.3	0.3	0.4	10 •	10	10 •	NE 2	NE 3	NE 1
13	85.8	85.0	85.5	85.4	2.7	10.7	7.3	7.0	10.8	2.5	95	70	90	85	0.4	3.9	1.0	1.8	10 •	10	10 •	NE 2	NE 2	S 1
14	87.3	89.7	91.8	89.6	2.9	8.3	6.0	5.8	8.8	2.3	88	74	76	79	0.2	2.9	2.3	1.8	9	10	5	NE 1	ENE 1	NE 2
15	92.3	92.3	89.8	91.3	2.9	4.5	4.9	4.3	6.0	2.1	88	73	73	78	0.9	2.3	2.4	1.9	9	10	8	NE 1	NE 3	ENE 2
16	85.9	83.4	83.2	84.2	-0.8	11.8	9.1	7.3	13.6	-1.3	100	59	77	79	0.0	3.6	2.7	2.8	5 ≡	9	7	C 0	N 3	SW 1
17	85.2	86.3	83.5	85.0	6.7	8.3	7.1	7.3	9.7	4.0	81	79	88	83	1.9	2.3	1.2	1.8	6	10	10	C 0	WNW 2	C 0
18	73.6	74.1	73.8	73.2	6.4	12.3	8.9	9.2	13.6	4.6	83	47	82	71	1.4	7.7	2.0	3.7	10	10	3	C 0	S 3	C 0
19	73.9	74.6	73.2	74.6	6.3	12.0	9.1	9.2	13.4	3.7	99	66	88	84	0.2	4.8	1.4	2.1	10 •	10	10	C 0	SW 1	ENE 1
20	73.8	73.3	73.1	74.1	6.9	14.3	8.9	9.8	14.5	3.9	90	63	93	82	1.0	6.0	0.8	2.6	10	10	8	NE 3	ENE 6	E 3
21	73.9	72.4	70.4	72.2	7.5	10.7	9.0	9.0	12.1	7.2	93	82	93	90	0.8	2.3	0.7	1.3	10	10	10 •	NE 3	NE 4	NNE 4
22	68.4	68.9	69.5	68.9	8.1	7.3	6.5	7.1	9.0	6.3	90	83	83	86	1.1	1.7	1.3	1.4	10 •	10	10	NNE 3	N 4	C 0
23	70.1	70.2	73.2	71.2	5.5	6.4	6.2	6.1	7.8	4.9	89	84	91	88	1.0	1.6	0.9	1.2	10 •	10 •	10 •	SW 2	SW 4	W 4
24	73.0	77.1	80.1	77.4	6.3	9.7	6.9	7.4	10.9	3.1	84	63	83	78	1.3	4.1	1.4	2.3	10	7	10	SW 4	SW 3	SW 2
25	82.7	83.4	83.7	83.3	6.2	12.7	7.2	8.3	13.9	3.2	82	57	90	76	1.7	6.3	1.1	3.0	10 •	9	4	C 0	SSW 3	SW 1
26	83.5	84.8	82.1	83.3	6.8	7.2	6.9	7.0	9.3	3.7	88	77	81	82	1.2	2.4	1.8	1.8	10 •	10	10	WSW 3	WSW 2	SE 1
27	77.7	76.4	73.8	76.6	6.3	12.1	10.8	10.0	13.9	3.6	89	53	68	70	1.0	6.6	4.2	3.9	9	3	6	SE 1	E 1	NE 2
28	74.0	73.2	79.6	75.6	6.6	13.1	7.9	8.9	14.3	3.4	88	63	68	74	1.1	3.3	3.3	3.2	10	10	3	ENE 2	ESE 4	C 0
29	81.6	81.3	84.4	82.3	7.1	14.7	7.3	9.1	15.4	3.8	69	43	87	66	3.2	9.4	1.3	4.6	2	8	8	C 0	NE 3	SW 3
30	86.9	87.7	89.6	88.1	6.3	11.1	8.1	8.4	14.2	6.0	90	67	87	81	1.0	4.3	1.4	2.2	10	10	9	W 3	NW 3	WNW 3
31																								
M	85	83.4	83.8	83.6	4.6	9.9	7.1	7.2	11.2	3.2	87	64	80	77	1.1	4.9	2.0	2.7	7.9	8.1	7.4	2.1	3.7	2.3

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$ Marzec – Mars 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU k	POGODA
1	7	.	26	=1; ⌣°1
2	8	5.2	25	•°12^00-30, p
3	5	1.8	17	•^1-2 na •²1; ≡°1; ⊕ II
4	7	.	15	⚲ a; = III
5	5	.	14	≡°1 = II
6	3	7.7	11	*¹ok. 10^30 – p; ⚶ ok. 10^30 – p; = I ≡° II = III
7	5	0.6	22	*° a z prz.; p z prz.; = I, II, III
8	6	0.4	20	⚹ na, I, II
9	4	0.0	20	≡° na – I ≡° ok. 9^00 = ok. 11^00 – II, III
10	7	0.2	18	*° na, I *¹7^35 – 8^00; = I ≡° III, ⌣° III
11	6	.	16	≡°1 = III; ⌣¹1
12	4	.	15	≡°1 = II, III, ⌣¹1
13	5	.	10	≡²1 = II, III
14	5	.	6	= I, II, III; ⌣¹1
15	3	.	4	≡°1, II, III, ⌣¹1; ⊕ I; ∿ I
16	5	0.0	3	≡°1 = II, III; ⌣°1
17	3	0.0	3	• n, a; ≡¹1 ≡° II ≡² p, III
18	6	.	3	≡² na, I = ok. 9^00; ⚲ III
19	6	0.1	pz.	= I, III; ⌣¹1; ∿ I
20	5	0.0	pz.	⚲ na, = I, II, III
21	7	6.5	.	•¹ok. 17^30 – n; ≡°1 = II
22	7	2.4	1	•¹ na *²–1 *° ok. –11^00; ≡°1
23	8	0.3	.	= I; ⌣°1
24	7	0.2	.	• n, I, a • ok. 15^00 – 18^00; = I
25	6	4.9	.	•° na •^0-1 7^15 – 10^30; = I, III
26	7	4.6	.	•° na •^0-1 ok. 17^45 – 19^00 •°... III; = I
27	5	1.1	.	•• na •°1 •° ok. 8^00 •° – II; = I, II, III
28	7	0.7	.	= I
29	4	1.9	.	• na •¹6^30 – I... p • p; ≡°1 = II, III
30	5	.	.	⚲ p; = I, II
31	7	0.5	.	•° 12^35 ⚲ ok. 15^00 – 16^05; = I
Σ	–	39.1	–	

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1	8	.	.	⚹ na
2	7	.	.	= I; ⊕ II
3	6	.	.	≡°1
4	7	.	.	= I; ⌒°1, ⊕ II
5	7	.	.	= I; ⌒°1
6	7	.	.	= I; ⌣°1
7	5	4.3	.	•°14^56 – 15^12, p; = I, II
8	5	0.1	.	•¹ n •p; = I, II, III
9	5	0.0	.	• ok. 20 – np; ⚲ p; = I, II, III
10	7	.	.	⚲ na, a, p
11	7	7.9	.	
12	4	1.3	.	•¹ na •°1, a z prz., p... III – np; = I, II, III
13	5	2.6	.	•°6^30 – I •¹13^46... p •° – III; = I, II; ⚲ III
14	3	.	.	= I, II
15	7	.	.	= I
16	5	0.3	.	•°12^15 – II, 15^10 – ok. 16^00; ≡²1 = II; ⌣°1
17	6	0.0	.	= I, ⌒²1
18	8	1.3	.	⌒¹1
19	6	2.2	.	•° ok. 4^00 – I •¹18^05-30 •°... 20^05; = I
20	7	1.3	.	•¹12^55 •° p... 20^30; ⚹ 12^58 (⚹) 13^05 – 14^35; = I; ⌒°1
21	5	1.4	.	•° p z prz. •¹20^15 – III; = I, II, III
22	7	1.6	.	•° ok. 5^00... a, 16^50 – 17^05 •¹ p... np
23	6	3.9	.	•° na, I, a z prz., p z prz. •¹21^30 – 22^00 •¹ – np; = I
24	7	2.0	.	•¹ na •¹13^46 – 14^20 •° 16^00 ... 19^00
25	7	0.7	.	•° 6^20 – a; = III; ⌒° III
26	5	2.5	.	•¹3^20 – na •^0-1 7^40 •° 8^50 – ok. 10^00 • p; = I, II
27	6	.	.	= I
28	8	0.3	.	•° a z prz. •¹14^06 – 15^00; = I; ⌒²1
29	7	0.3	.	= I; ⌒°1, III; ⊕ II, a
30	6	8.1	.	•° a •° ok. 14^00 •¹17^35 – 19^20
31				
Σ	–	36.9	.	

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Maj – Mai 1965

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	90.2	89.3	89.0	89.5	7.3	13.3	9.7	10.0	14.9	5.4	79	31	53	54	2.2	10.6	5.6	6.1	3	6	0	WSW 2	NW 6	WNW 3
2	92.9	92.1	91.6	92.2	2.5	9.0	5.3	5.5	9.7	1.6	65	41	59	55	2.6	6.8	3.7	4.4	2	10	2	NW 2	NW 2	NW 1
3	90.9	90.7	91.9	91.2	3.9	8.9	5.5	6.0	11.0	-0.7	61	36	56	51	3.2	7.3	3.9	4.8	0	8	0	C 0	NNW 2	NW 2
4	93.1	90.3	85.6	89.7	2.3	11.5	7.9	7.4	13.5	-1.5	75	32	58	54	1.9	9.2	4.5	5.2	0	0	3	NE 2	ENE 4	NE 3
5	81.3	79.5	78.4	79.7	7.7	10.1	9.9	9.4	10.8	5.5	91	86	89	89	0.9	1.8	1.3	1.3	10 •	10 •	10 •	ENE 1	C 0	C 0
6	78.3	80.3	83.9	80.8	9.6	10.8	9.7	10.0	11.8	8.9	97	87	88	91	0.4	1.7	1.4	1.2	10 • ≡	10	10	C 0	NW 3	WNW 2
7	86.8	87.7	88.8	87.8	8.5	11.2	8.3	9.1	13.2	8.2	88	75	90	84	1.4	3.6	1.1	2.0	10	9	0	WNW 2	W 3	C 0
8	86.9	86.6	89.4	87.6	7.1	15.5	11.6	11.4	16.1	3.4	90	58	88	79	1.0	7.4	1.6	3.3	10 ≡	10	10	C 0	SW 4	WSW 2
9	88.5	85.2	77.0	83.6	12.2	15.9	13.9	14.0	16.9	9.4	79	61	71	70	3.0	7.0	4.6	4.9	3	10	10	W 2	WSW 4	SSW 2
10	78.0	76.3	78.1	77.5	10.1	13.4	7.5	9.6	13.9	6.8	66	52	87	68	4.3	7.4	1.4	4.4	3	10	10	SW 7	SW 8	SW 4
11	77.4	80.1	87.5	81.7	7.1	10.3	7.5	8.1	12.3	6.8	83	67	96	82	1.8	4.1	0.5	2.1	10	9	10 •	SW 4	WSW 2	SE 6
12	91.4	93.2	94.7	93.1	8.7	15.9	10.7	11.5	16.2	6.8	90	53	81	75	1.0	8.5	2.5	4.0	10	6	7	SW 1	NW 5	NW 1
13	94.6	93.9	92.8	93.8	9.9	16.1	11.9	12.4	16.9	8.0	63	37	64	55	4.5	11.5	5.0	7.0	1	7	3	W 1	NNW 3	C 0
14	91.3	89.9	87.8	89.7	11.2	13.3	11.5	11.9	16.4	7.4	71	73	89	78	3.9	4.2	1.5	3.2	9	10 •	10 •	NNW 2	WSW 2	C 0
15	86.6	86.0	85.0	85.9	11.1	15.7	12.8	13.1	17.8	10.0	88	57	77	74	1.6	7.6	3.4	4.2	8	10	8	W 1	WNW 1	C 0
16	83.4	83.4	82.4	83.1	10.1	14.3	15.5	13.8	17.8	9.2	97	90	90	92	0.4	1.6	1.7	1.2	10 •	10	10 •	N 1	NNE 1	C 0
17	83.4	82.3	80.8	82.2	13.5	23.1	17.3	17.8	24.3	10.2	85	46	74	68	2.3	15.1	5.1	7.5	3	3	3	C 0	W 3	C 0
18	80.1	81.2	81.0	80.8	19.5	23.6	18.5	20.0	25.1	13.5	66	46	76	63	7.3	15.8	5.1	9.4	3	5	5	SW 2	W 3	C 0
19	76.1	73.4	81.9	77.1	17.7	27.1	11.9	17.2	28.0	11.8	78	39	90	69	4.4	22.0	1.3	9.2	8	7	10 •	C 0	S 3	NW 5
20	90.4	93.0	95.9	93.1	3.1	6.9	5.3	5.2	11.9	2.6	93	75	98	89	0.5	2.4	0.1	1.0	10 •	10	5	NNW 2	E 1	C 0
21	100.1	100.4	100.9	100.5	7.2	11.9	9.2	9.4	13.4	4.2	83	50	76	70	1.8	6.9	2.7	3.8	6	3	3	NW 1	NW 1	NW 1
22	101.1	98.1	94.7	98.0	8.1	15.5	11.9	11.8	16.5	3.4	79	50	73	67	2.3	8.9	3.8	5.0	5	5	8	NW 1	ESE 6	E 2
23	91.8	91.5	90.1	91.1	11.3	11.9	11.4	11.5	12.3	10.8	82	84	90	85	2.5	2.1	1.4	2.0	10	10 •	10	ENE 8	ENE 6	NE 6
24	89.1	89.2	89.4	89.2	10.2	13.3	12.5	12.1	17.1	10.0	100	91	95	95	0.0	1.4	0.7	0.7	10 •	10	10	ENE 1	NE 1	C 0
25	88.8	89.7	90.8	89.8	13.0	16.3	12.1	13.4	17.0	9.2	92	68	91	84	1.3	6.0	1.2	2.8	10	10 •	10	NW 1	W 5	W 2
26	90.8	91.0	90.4	90.7	11.1	15.5	11.9	12.6	17.7	10.7	95	69	90	85	0.7	5.5	1.3	2.3	10 •	8	7	SW 2	W 4	WNW 1
27	89.3	87.6	87.3	88.1	10.3	18.0	14.7	14.4	19.0	9.4	90	42	70	67	1.3	11.9	5.0	6.1	2	9	10 •	NW 1	W 2	W 1
28	84.9	83.0	80.5	82.8	13.3	16.2	15.5	15.1	17.4	11.7	95	78	83	85	0.7	4.0	3.0	2.6	10	10	10	NE 3	NE 2	ENE 2
29	77.1	76.7	78.4	77.4	13.2	18.1	11.9	13.8	18.8	11.7	94	64	90	83	0.9	7.5	1.3	3.2	10	10 K	10 •	ENE 1	N 1	W 1
30	81.0	82.3	84.1	82.5	8.6	12.8	8.3	9.5	13.9	8.1	94	68	87	83	0.6	4.7	1.4	2.2	10	8	1	N 1	NNW 5	C 0
31	84.4	84.4	81.8	83.5	8.1	13.6	14.1	13.0	16.4	5.8	90	66	87	81	1.1	6.0	2.2	3.1	9	10	10	C 0	NE 2	ENE 3
M	87.1	86.7	86.8	86.9	9.6	14.5	11.2	11.6	16.1	7.3	84	60	81	75	2.0	7.1	2.6	3.9	6.9	8.2	6.9	1.7	3.1	1.6

Czerwiec – Juin

1	78.1	80.8	83.9	80.9	17.5	20.0	15.3	17.0	21.7	11.3	73	46	64	61	5.3	12.7	6.3	8.1	1	4	5	C 0	W 4	WSW 3
2	84.8	88.0	91.1	88.0	11.9	15.5	10.5	12.1	16.4	10.5	70	51	73	65	4.1	8.7	3.2	5.3	7	6	3	SW 3	WNW 10	C 0
3	92.4	91.9	91.4	91.9	11.1	19.7	14.9	15.2	20.1	5.5	64	35	70	56	4.8	14.8	5.0	8.2	4	4	9	W 1	NW 2	N 1
4	91.1	89.8	87.9	89.6	14.6	19.4	14.9	16.0	19.7	10.0	75	53	90	73	4.1	10.6	1.6	5.4	9	10	9 •	N 1	ENE 4	C 0
5	83.4	81.1	79.6	81.4	14.1	17.1	14.7	15.2	17.9	13.3	95	84	96	92	0.7	3.2	0.7	1.3	10	10	10 •	NE 2	NE 3	ENE 3
6	76.5	76.7	78.8	77.3	13.1	14.0	12.4	13.0	14.8	12.2	98	92	94	95	0.4	1.3	0.9	0.9	10 •	10 •	10	NE 2	ENE 3	N 2
7	83.0	84.6	85.5	84.4	12.2	17.0	13.0	13.8	18.8	11.0	79	58	85	74	3.0	8.1	2.3	4.5	10	8	0	N 1	NNW 2	C 0
8	86.3	84.2	83.2	84.6	13.7	22.0	17.3	17.6	23.0	8.9	75	54	76	68	3.9	12.2	4.7	6.9	8	5	6	NNE 4	ENE 6	ENE 3
9	81.6	78.6	80.2	80.1	15.7	20.3	12.1	15.0	22.1	12.1	83	65	95	82	2.6	8.2	0.7	3.8	8	9	6	E 2	ENE 7	C 0
10	80.6	80.1	80.0	80.2	12.6	20.2	14.3	15.4	21.0	8.3	87	54	91	77	1.9	11.0	1.5	4.8	9	5	10 •	N 1	ESE 1	C 0
11	73.9	76.4	76.7	76.3	14.7	18.3	13.9	15.2	18.7	13.1	89	62	91	81	1.8	7.9	1.5	3.7	10	8	10 •	NNE 2	NNE 2	NW 6
12	82.6	84.5	88.0	85.0	13.4	16.3	13.5	14.2	17.4	11.7	84	72	87	81	2.5	5.3	2.0	3.3	10	9	10	NNW 4	NW 5	WSW 4
13	89.4	89.0	88.0	88.8	11.5	15.5	13.9	13.7	17.6	10.6	82	58	85	75	2.3	7.4	2.3	4.1	10	10	10	WSW 4	W 4	ESE 4
14	87.8	88.2	89.7	88.6	11.9	14.3	13.1	13.1	16.7	11.1	90	72	98	87	1.3	4.6	0.4	2.1	9	10	10	W 3	WNW 5	NNE 1
15	91.1	90.9	91.2	91.1	12.3	19.7	14.3	15.2	21.3	8.3	83	44	76	68	2.4	12.9	3.9	6.4	3	2	0	NW 2	NNW 1	C 0
16	91.2	89.8	83.9	89.0	14.1	23.6	17.7	18.3	24.3	7.8	68	42	81	64	5.1	17.0	3.8	8.6	1	4	3	C 0	NE 1	NE 1
17	81.3	78.7	83.1	81.1	17.1	24.3	15.6	17.2	23.8	11.1	73	41	90	68	3.3	8.1	1.6	3.0	0	9	10 •	NE 2	ENE 2	SW 1
18	89.2	90.4	90.2	89.9	12.1	17.3	15.3	15.1	19.4	11.4	87	51	73	70	1.8	9.5	4.8	5.4	9	9	10	WSW 3	W 2	C 0
19	87.8	88.3	91.1	89.1	18.3	23.3	18.5	19.6	24.5	13.8	68	51	70	63	6.8	14.0	6.5	9.1	8	10 •	8	SW 1	WNW 8	W 2
20	94.4	94.0	93.6	94.0	16.2	19.9	16.6	17.3	20.1	11.1	67	53	77	66	6.2	10.8	4.4	7.1	3	7	9	WSW 4	SW 2	C 0
21	94.5	92.9	90.8	92.7	17.3	23.0	18.3	19.4	23.3	12.8	69	48	71	63	6.2	14.5	6.1	8.9	0	9	7	WNW 1	NNE 1	ENE 2
22	88.1	86.4	83.9	86.1	18.9	27.8	22.3	22.8	29.4	13.2	74	47	83	68	3.7	19.7	4.7	10.0	2	2	8	ENE 1	C 0	C 0
23	87.5	87.8	89.2	88.2	17.9	24.3	20.1	20.6	26.1	16.7	86	53	73	71	2.8	13.7	6.4	7.6	9	3	6	WSW 3	WSW 3	WNW 1
24	90.9	91.1	91.6	91.2	19.2	26.3	20.8	21.8	28.0	13.3	78	43	78	66	4.8	19.7	3.6	10.0	7	4	8	W 1	SW 3	C 0
25	93.2	92.8	93.2	93.1	18.9	26.9	20.9	21.9	27.9	13.0	84	40	76	67	3.3	21.2	6.0	10.2	3	1	3	SW 2	SW 4	C 0
26	91.7	90.3	93.3	91.8	20.4	31.0	23.1	24.4	32.8	13.4	76	48	63	63	3.9	23.4	9.9	13.1	1	1	9	C 0	ESE 1	NNW 3
27	93.9	91.3	92.9	92.8	21.1	27.4	17.8	21.0	28.6	16.7	79	34	97	77	3.4	16.0	0.6	7.3	4	1	10 • K	0 0	E 3	C 0
28	94.7	97.1	96.9	96.2	13.3	13.9	13.7	14.2	18.3	13.2	91	83	90	89	1.3	2.3	1.6	1.8	10 •	10 •	10	NNW 2	NNW 1	WSW 3
29	93.3	93.3	94.9	94.6	18.3	21.1	17.1	18.9	21.9	8.8	83	51	72	69	2.2	12.2	3.4	6.6	4	6	4	SSW 2	WSW 3	C 0
30	94.9	93.1	89.4	92.9	13.8	23.4	18.9	19.2	25.6	11.0	77	42	83	67	4.1	16.7	3.7	8.3	0	0	1	NNW 1	NE 1	0 0
31																								
M	87.8	87.4	87.8	87.7	15.2	20.8	16.1	17.0	22.1	11.7	80	53	82	72	3.6	11.6	3.6	6.3	6.0	6.2	7.3	1.8	3.3	1.3

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$ Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	•	•	$= I$; $\frown^{2}$ II
2	7	•	•	$\frown^{0}$ I
3	8	•	•	$= I$; $\smile^{0}$ II
4	8	2.1	•	$\smile^{0}$ I
5	6	6.6	•	• ^{0}ok. 2^{40} – a • $^{1}8^{30}$ – p • ... III • ^{1}ok. 23^{00} • ... np; = I, III
6	4	2.5	•	• na z prz. • ^{0}I • $^{1}7^{50}$ • $^{0}8^{20}$ ... a, p z prz.; $\equiv^{0}$ I = II
7	7	1.1	•	• ^{0}ok. 1^{10} • $^{2}14^{10-30}$ ▲ 14^{20-31}; = I
8	7	0.0	•	• p; = I; $\smile^{0}$ I
9	7	7.9	•	• 12^{20-35} p • $^{2}21^{02-22^{30}}$; = I
10	7	10.5	•	▲ 17^{44-45} • $^{2}14^{20}$ • $^{0}14^{55}$ • $^{2}16^{30}$ • $^{0}16^{40}$ • $^{2}17^{29}$ • $^{0}17^{55}$; K NE 16^{34-50}, NW 17^{21-24}
11	7	26.2	•	• $^{2-1}16^{45}$ • $^{0}19^{30}$ • $^{2}20^{25}$ • ^{0}ok. 22^{00} – n; K NE 17^{02-37}; = III
12	7	•	•	
13	8	•	•	$\frown^{0}$ I, III
14	5	0.5	•	• II, p • ^{0}ok. 16^{00}...III; = I, II, III; $\frown^{2}$ I
15	6	14.4	•	= I; $\frown^{1}$ II
16	4	2.9	•	• $^{2-0}$ok. 3^{00} – I ... ok. 10^{30} • ^{0}ok. 18^{30} – np • $^{2}21^{20}$ • ^{0}n z prz.; = I, II, III
17	7	•	•	= I; $\frown^{1}$ III; ∿ III; ⊕ p
18	7	•	•	$\frown^{2}$ I, III
19	8	25.2	•	• $^{0}17^{02}$ • $^{2}18^{46-55}$ • $^{2-1}19^{50}$ – n; K SW 16^{53} – SE 17^{20} – S 17^{29} – E – 17^{47}; ≫ 15^{30} – 17^{00}; = I; $\frown^{2}$ I
20	8	2.4	•	• ^{0}I
21	7	•	•	= I; $\frown^{0}$ III
22	7	0.0	•	= I; $\frown^{2}$ I
23	7	3.9	•	• na • $^{0}11^{00}$ – p • $^{1}13^{15}$ 19^{45}
24	4	6.5	•	• $^{2}5^{40}$ • $^{0}6^{20}$ – a • $^{2}7^{40}$ • $^{0}8^{10}$ • $^{2}8^{55}$ • $^{0}9^{15}$ • $^{0-2}16^{00}$ – 17^{30}; = I, II, III
25	4	1.6	•	• $^{0}12^{50}$ – ok. 13^{00} • $^{2}17^{11-14}$ • ^{0}... ok. 19^{00}; = I, II
26	7	1.5	•	• I • $^{2}16^{45}$ • $^{0}17^{05-20}$; = I
27	7	1.5	•	• 20^{30} – np • $^{0-2}21^{30}$ – ok. 24; = I; $\frown^{1}$ I
28	6	3.8	•	• $^{0}14^{30}$ – 15^{00} • $^{2}22^{00}$ – 23^{10}; K SW 22^{40} 22^{47} – 23^{01} E – E 23^{08}; = I, III
29	5	14.2	•	• $^{0}12^{22}$ • $^{2}12^{47}$ • $^{0}13^{30}$ • $^{2}14^{30}$ 17^{10-30} • $^{0}20^{20}$ • $^{2}20^{30}$ • $^{1}21^{20}$; K W 11^{30}, K S 12^{31} – SE 13^{28}, K 14^{36} – S 15^{54}; = I, II, III
30	6	0.1	•	• ^{0}ok. 1^{00} – 8^{20} • na; $\frown^{2}$ III
31	6	1.7	•	• a, p • $^{0}20^{55}$ • $^{2-1}21^{50}$ – 24; = I; $\frown^{0}$ I
Σ	–	156.9	–	

Czerwiec - Juin

1	8	•	•	• $^{2-1}0^{00}$ – ok. 0^{30}
2	7	•	•	≫ a; $\frown^{1}$ III
3	7	•	•	$\frown^{2}$ I; ψ III
4	7	1.6	•	• $^{0}15^{10}$ ... III – 24; = I; $\frown^{2}$ I
5	6	5.1	•	• $^{0}0^{00}$ – ok. 3^{30} • $^{1}16^{25}$ • $^{0}17^{10}$ • $^{2-1}19^{55}$ – n; = I, III
6	7	11.6	•	• I • $^{2}7^{40}$ • $^{0}8^{30}$ • $^{1}9^{50}$ • ok. 11^{00}, II • $^{2}17^{10}$ – 19^{40}; = I
7	7	•	•	• ^{0}ok. 0^{00} – ok. 3^{00}; $\frown^{2}$ III; ∿ III
8	7	0.0	•	• p; $\frown^{0}$ I; ⊕ ok. 12^{30} – II ψ III
9	4	8.8	•	• $^{2}13^{02}$ • $^{0}13^{20}$ • $^{1}14^{35}$ – 15^{20} • $^{2}19^{00-10}$; K S 12^{58} – SW 13^{00} – NW 13^{13} – N 13^{50}; = II; $\frown^{2}$ I; ψ III; ∿ I
10	8	24.3	•	• $^{0}18^{50}$ – 19^{05}; 22^{30-40}; K E 18^{35} – E 18^{40} – N 19^{10}; = I
11	8	24.6	•	• $^{2}1^{20}$ • $^{0}3^{00-40}$ • $^{1}14^{20}$ • $^{2}17^{00}$ • ^{1}ok. 20^{00} – np • $^{2}21^{05}$ – ok. 23^{30}
12	7	1.4	•	• $^{1}14^{20}$
13	6	11.4	•	= I, III
14	6	6.0	•	• $^{2}0^{50}$ • ^{0}ok. 6^{00} • $^{2}7^{06-30}$ • $^{0}14^{45}$ • $^{2}15^{25}$ – 18^{50}; = I, III
15	7	•	•	= I; $\frown^{2}$ III
16	8	•	•	= I; $\frown^{2}$ I, III; ∿ III
17	8	12.1	•	• ok. 13^{00} • $^{1}18^{00}$ – 24; $\frown^{2}$ I
18	7	•	•	• $^{1}0^{00}$ – ok. 5^{00}; = I; ∿ III
19	8	1.8	•	• $^{1}12^{40}$ – ok. 14^{00}; $\frown^{0}$ I
20	7	•	•	$\frown^{0}$ I
21	7	•	•	$\frown^{0}$ I, III
22	7	1.3	•	= I; $\frown^{1}$ I $\frown^{2}$ III; ⊕ a; ∿ III
23	7	•	•	• $^{1}4^{20}$ – ok. 5^{00}; (K) 4^{30} – 5^{00}; $\frown^{0}$ III
24	7	•	•	= I; $\frown^{0}$ I $\frown^{1}$ III; ∿ II, III
25	6	•	•	= I; $\frown^{2}$ I $\frown^{0}$ III
26	7	0.0	•	• $^{0}20^{20}$; K E 19^{50} – ENE 20^{00} – SE i S 20^{25} – S 20^{55}; = I; $\frown^{0}$ I
27	7	28.7	•	▲ 18^{45-52} • $^{2}18^{50}$ • $^{0}19^{15}$ • $^{2}20^{10}$ • ^{0}III • $^{2}22^{15}$; K N 17^{10} – NNW 18^{00} – N, W, NE, S 18^{40}, K S 19^{50} – SE 20^{50} K 22^{20} – 23^{12}; = I; $\frown^{2}$ I
28	7	9.3	•	• $^{0}1^{30}$ – 2^{40}, ok. 5^{00} • $^{2}6^{10}$ – a • $^{0}6^{55}$ • $^{1}7^{30}$ – 16^{30}; = I
29	7	•	•	= I; $\frown^{1}$ III; ∿ III
30	7	•	•	= II; $\frown^{2}$ I $\frown^{1}$ III; ∿ III
31				
Σ	–	148.0	–	

Kraków, Obserw. Astr. UJ — $\varphi = 50°04'$ — $\lambda = 19°58'$ — *Lipiec – Juillet* 1965

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	85.2	86.0	87.7	86.3	19.0	22.3	17.2	18.9	24.9	15.3	79	64	77	75	4.6	9.7	4.5	6.3	6	10	10	C 0	W 5	NNW 1
2	86.9	87.0	86.0	86.6	14.3	15.3	13.5	14.2	17.4	13.3	95	87	88	90	0.7	2.3	1.8	1.6	10	10	5	NNW 1	N 1	SW 2
3	84.8	85.9	85.9	84.9	13.8	17.4	11.1	13.4	19.4	11.1	82	72	90	81	2.9	5.7	1.3	3.3	10	10 •	10	SSW 1	W 1	SSW 3
4	85.8	84.5	83.9	84.7	11.4	15.4	11.7	12.0	16.0	7.6	88	73	95	85	1.7	4.2	0.6	2.2	8	10 •	10	C 0	WSW 1	C 0
5	83.1	82.3	85.3	83.6	11.5	14.5	12.7	12.8	15.4	10.9	95	73	73	80	1.0	4.3	3.9	3.1	10 •	10	6	WSW 1	WSW 1	W 2
6	89.2	88.5	88.9	88.9	12.0	16.2	13.9	14.0	17.6	7.4	75	58	64	66	3.3	7.7	3.7	5.6	5	8	5	W 3	SW 4	SW 3
7	90.3	88.0	86.1	88.1	13.1	21.2	15.9	16.5	22.5	9.0	79	46	82	69	3.1	13.6	3.3	6.7	10	9	3	C 0	SW 3	C 0
8	83.5	78.3	81.0	80.9	16.3	25.8	13.9	17.5	27.3	11.2	79	44	91	71	3.8	18.6	1.5	8.0	7	6	10 •	C 0	E 3	SSW 2
9	82.8	86.0	88.3	85.7	14.3	13.7	13.5	13.8	18.2	11.1	79	75	67	74	3.4	3.9	5.2	4.2	10 •	6	4	W 3	WNW 4	C 0
10	89.6	89.2	91.6	90.1	12.6	17.4	12.3	13.6	19.1	7.4	72	52	88	71	4.1	9.7	1.7	5.2	7	9	9	W 1	SSW 3	WNW 1
11	93.8	94.1	93.8	93.9	11.8	16.9	13.2	13.8	19.0	8.2	85	63	85	78	2.0	7.2	2.3	3.8	10	9	8	WNW 2	NW 4	C 0
12	92.9	90.4	89.2	90.8	13.8	23.1	17.8	18.1	23.9	8.3	79	53	83	72	3.4	13.3	3.4	6.7	2	9	10 •	C 0	SW 3	C 0
13	90.2	90.0	91.0	90.4	17.7	22.0	18.5	19.2	24.9	13.3	89	70	91	83	2.2	7.9	1.9	4.0	10 •	9	0	WSW 1	C 0	C 0
14	91.4	91.9	91.3	91.5	18.4	28.2	21.7	22.3	28.9	13.1	83	46	81	70	3.3	20.7	3.1	9.8	3	1	0	C 0	ESE 4	E 2
15	91.9	91.9	90.8	91.3	18.9	27.8	21.2	22.3	28.8	14.3	84	47	78	70	3.3	19.9	3.6	9.7	0	0	0	E 1	E 4	C 0
16	89.5	88.1	87.3	88.3	19.1	27.2	21.0	22.1	27.3	14.4	79	53	85	72	4.6	16.9	3.9	8.5	0	3	2	E 1	NE 4	C 0
17	86.8	84.6	85.1	85.3	18.7	22.6	19.3	20.0	27.4	17.3	91	79	92	87	1.9	3.6	1.8	3.1	7	8 •	9	C 0	SSW 1	C 0
18	83.7	84.6	87.9	85.4	17.3	19.7	17.3	18.0	20.0	16.6	97	82	90	90	0.6	4.0	2.0	2.2	10 •	10 •	9	C 0	C 0	NNE 2
19	91.1	92.2	93.1	92.1	16.7	21.0	17.3	18.1	23.3	15.8	92	71	74	79	1.6	7.3	3.1	4.7	9	8	3	NNE 3	NE 3	NE 3
20	92.9	91.5	89.3	91.2	15.6	23.4	19.2	19.4	24.8	12.3	77	56	74	69	4.1	12.7	3.8	7.3	4	4	6	NE 3	ENE 3	NNE 3
21	86.3	84.8	83.8	85.0	15.5	23.2	19.4	19.4	24.4	13.6	88	73	78	80	2.1	7.6	4.8	4.8	7	8	9	C 0	E 3	S 1
22	85.7	83.3	84.2	83.1	17.0	24.6	20.0	20.4	26.0	13.9	79	46	72	66	4.1	16.5	6.6	9.1	3	2	4	W 2	WSW 3	C 0
23	81.9	82.3	84.8	83.1	18.4	19.6	16.0	17.3	22.8	13.3	76	78	94	83	3.1	3.1	1.2	3.8	8	10	0	WNW 1	W 2	C 0
24	83.9	83.8	86.8	86.2	17.0	26.6	20.0	20.9	27.8	11.4	80	43	79	68	3.9	19.1	3.0	9.3	8	4	4	C 0	W 4	C 0
25	88.2	86.8	85.1	86.7	18.9	23.6	20.8	21.0	26.9	17.0	74	69	83	73	3.5	9.0	4.3	6.3	9	6	3	C 0	SE 2	C 0
26	86.4	87.8	86.5	86.9	18.4	17.4	15.7	16.8	20.8	15.5	85	81	71	79	3.1	3.8	3.2	4.0	10	10	10	WSW 1	WSW 3	SSW 1
27	85.7	87.3	87.9	87.0	14.9	15.0	14.9	14.9	18.8	12.9	84	82	82	83	2.7	3.1	3.1	3.0	10	9	5	WSW 3	WSW 3	SW 3
28	89.5	89.3	88.3	89.1	13.8	16.7	12.8	14.0	17.1	12.4	84	65	96	82	2.5	6.6	0.5	3.2	8	9	9	WSW 2	WSW 3	C 0
29	85.5	83.3	80.1	83.0	14.9	23.2	18.7	18.9	23.2	10.5	73	47	74	63	4.1	15.2	5.8	8.3	1	8	10	W 1	SSW 4	C 0
30	76.6	77.3	78.9	77.6	17.7	16.8	15.9	16.6	21.8	13.2	73	73	73	74	3.1	4.8	4.9	4.9	9	10 •	2	SW 1	SW 6	SW 3
31	79.7	78.4	79.9	79.3	14.0	18.1	16.9	16.3	20.0	10.6	83	71	72	73	2.7	6.0	3.3	4.7	10	10	9 •	C 0	SSE 2	WSW 3
M	87.0	86.5	86.8	86.8	15.7	20.4	16.6	17.3	22.5	12.4	83	64	81	76	3.1	9.4	3.6	5.4	7.2	7.6	5.9	1.1	2.9	1.1

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DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.1	86.1	84.3	85.5	11.7	18.7	15.7	15.4	20.1	11.4	83	56	79	73	2.3	9.6	3.7	5.2	8	9	10	WNW 2	WNW 3	E 2
2	80.6	83.9	85.4	83.3	10.1	11.3	12.1	11.4	15.9	9.6	99	89	88	92	0.2	1.3	1.7	1.1	10 •	10 •	10	NW 3	NW 1	SW 1
3	85.3	84.7	85.9	85.3	12.9	18.9	14.9	15.4	21.8	8.7	73	48	79	67	3.8	11.3	3.4	6.2	0	10	10	SW 1	WSW 1	C 0
4	89.4	89.9	91.1	90.1	13.5	18.1	15.7	15.8	21.4	10.6	84	78	73	79	2.5	4.7	4.4	3.9	9	8	10	SW 1	SW 2	C 0
5	93.2	94.9	94.5	94.9	13.9	21.8	16.6	17.2	23.7	10.4	89	52	91	77	1.8	12.5	1.8	5.4	9	8	6	SW 1	SSW 2	C 0
6	94.3	92.4	91.8	92.8	16.0	29.0	22.0	22.2	30.3	11.4	83	43	70	63	3.1	22.7	7.9	11.2	0	6	10	C 0	S 3	C 0
7	91.6	89.3	89.2	90.0	18.9	31.2	21.8	23.4	33.1	17.7	88	40	67	63	2.5	27.0	8.7	12.7	10	0	0	C 0	WNW 1	C 0
8	89.9	87.2	87.7	88.3	18.9	28.6	24.0	23.9	31.4	14.0	73	43	61	60	5.3	22.3	11.6	13.1	2	0	0	C 0	ESE 3	C 0
9	93.0	92.2	93.2	92.8	17.7	18.0	14.7	16.3	24.0	14.6	73	69	80	73	5.1	6.3	3.3	4.9	10	10	10	W 1	NNW 4	NNW 4
10	93.4	93.6	93.3	93.3	14.3	16.1	12.6	13.9	16.5	12.4	89	77	89	83	1.8	4.2	1.6	2.3	10	10	10	NNW 1	NNE 2	NNE 1
11	93.7	94.6	94.4	94.2	11.3	13.2	12.1	12.2	14.1	11.0	93	87	93	92	0.7	2.0	0.7	1.1	10 •	10 •	10	NNW 1	NNW 2	C 0
12	94.0	94.6	94.2	94.3	12.1	16.3	14.3	14.3	18.7	10.1	87	57	72	72	1.8	8.2	4.6	4.9	10	8	9	NW 3	NW 4	NW 1
13	93.9	93.0	93.8	94.2	11.9	16.6	13.4	13.8	18.2	11.2	85	51	78	71	2.0	9.2	3.3	4.8	10	9	9	NW 1	NW 2	C 0
14	94.3	93.4	92.4	93.4	11.8	17.7	13.3	14.1	18.2	10.7	85	54	87	75	2.0	9.3	2.0	4.4	8	9	10	W 1	W 1	C 0
15	93.0	93.2	92.8	93.0	12.7	17.3	11.3	13.2	17.9	11.3	91	60	89	80	1.4	7.8	1.3	3.6	10	9	9	C 0	NNW 1	C 0
16	93.6	92.8	92.1	92.8	11.9	18.3	13.8	14.3	19.7	10.3	89	57	86	77	1.3	9.1	2.2	4.3	9	7	9	C 0	NE 2	C 0
17	91.8	91.5	91.8	91.7	11.8	20.7	13.9	15.1	21.5	10.0	89	52	81	74	1.5	11.7	3.0	5.4	10	3	2	C 0	NE 1	E 1
18	93.1	93.1	94.8	93.7	12.3	22.2	15.3	16.3	22.8	7.9	83	49	84	72	2.4	13.8	2.8	6.3	2	4	6	C 0	E 1	C 0
19	96.4	96.4	96.4	96.4	12.3	23.9	16.0	17.0	24.5	12.0	88	53	86	76	1.7	13.9	2.5	6.0	2	4	5	C 0	E 1	C 0
20	96.7	95.2	93.1	93.0	14.1	24.5	16.2	17.8	23.0	10.0	82	46	84	71	2.9	16.5	2.9	7.4	0	0	4	E 1	ENE 2	C 0
21	92.0	89.3	87.8	89.7	15.5	27.6	19.0	20.3	27.8	11.5	89	35	73	66	1.9	24.1	6.0	10.7	8	5	4	C 0	SSW 2	C 0
22	86.2	83.6	82.5	84.1	15.9	27.7	17.8	19.8	28.9	12.4	81	41	76	66	3.5	21.8	5.0	10.1	3	3	0	C 0	E 4	C 0
23	81.9	82.1	83.2	82.4	15.4	24.8	19.7	19.9	26.4	11.6	88	58	80	73	2.1	13.3	4.7	6.7	10	10	9	C 0	E 2	C 0
24	82.8	81.6	81.2	81.9	17.7	26.6	19.2	20.7	27.1	16.6	88	59	93	80	2.4	14.2	1.3	6.0	10	10	10	E 1	ENE 1	C 0
25	79.3	80.1	84.1	81.2	18.1	20.4	14.7	17.0	23.3	14.5	98	86	93	92	0.3	3.4	1.1	1.7	10 •	10	10 •	C 0	W 1	SW 2
26	85.7	87.3	87.7	86.9	13.1	12.7	10.7	11.8	14.8	10.1	93	88	86	89	1.1	1.8	1.8	1.6	10 •	10 •	10 •	WSW 3	W 2	ENE 2
27	85.4	85.8	87.4	86.2	10.3	12.3	12.3	12.0	14.1	10.0	91	88	83	87	1.1	1.7	2.4	1.7	10 •	10 •	9	SW 1	WSW 1	WSW 2
28	87.7	88.3	90.7	89.0	10.3	13.0	12.3	12.3	18.3	9.9	99	67	83	83	0.2	5.3	2.4	2.7	7	7	9	C 0	N 1	NW 2
29	90.6	89.1	87.8	89.2	9.3	19.3	11.2	12.8	19.8	7.3	93	53	94	80	0.8	10.4	0.8	4.0	3	8	3	NW 1	SSE 2	C 0
30	88.1	89.0	90.9	89.3	12.7	18.0	10.7	13.0	18.7	10.4	94	59	99	84	0.9	8.4	0.2	3.2	10	8 •	6	SSW 1	W 2	C 0
31	90.8	88.6	86.8	88.7	9.1	18.7	12.3	13.2	20.2	8.3	97	51	88	79	0.4	10.6	1.7	4.2	3	4	4	W 1	W 1	C 0
M	90.0	89.6	89.8	89.8	13.3	20.2	15.2	16.0	21.8	11.2	88	60	83	77	2.0	10.9	3.3	5.4	7.2	7.1	7.2	0.8	1.9	0.6

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219.8\,m$ $h_w = 10\,m$ Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁUBOKOŚĆ h	POGODA
1	5	1.7	.	$\bullet^{1}11^{45}$ $\bullet$ II; = I, II; ⌓ ^{0}I; ▬ II, III
2	5	0.4	.	$\bullet$ 15^{05-45}; = I, II
3	5	2.0	.	$\bullet^{0}11^{50}$ – II, 16^{50} $\bullet^{1}18^{08-40}$; = II, III
4	5	3.9	.	$\bullet^{1}11^{30}$ $\bullet^{2}11^{45}$ $\bullet^{1}$ok. 12^{00} – 13^{30}, 15^{00} – 16^{40}; = I, II; ⌓ ^{0}I
5	4	0.9	.	$\bullet$ na. I $\bullet^{0}$ok. 8^{00} $\bullet^{1}15^{50}$ – 16^{40}; = I, II
6	7	0.0	.	
7	7	.	.	
8	8	5.1	.	$\bullet^{0}17^{10}$ $\bullet^{2}17^{50}$ – 19^{00}, 20^{05} – n; ↳ SSW 20^{48}, SSE 20^{55} – 21^{50}; ⌓ ^{1}I; ⊕ I
9	7	1.8	.	$\bullet$ I, 8^{30} $\bullet^{2}11^{55}$ – 12^{10}
10	7	0.7	.	$\bullet^{0}17^{20}$ – 18^{05}; ⌓ ^{1}I
11	6	.	.	= I
12	8	1.4	.	$\bullet^{0}$ok. 20^{00} – ok. 24; = I; ⌓ ^{0}I; ▬ II; ⊕ a, II
13	6	0.0	.	$\bullet$ 6^{30-45}; = I, III; ⌓ III
14	7	.	.	= I; ⌓ ^{1}I, II
15	7	.	.	= I; ⌓ ^{1}I ⌓ ^{0}III
16	7	2.6	.	= I; ⌓ ^{2}I ⌓ ^{0}III; ⊕ p
17	6	4.7	.	$\bullet^{2}12^{20}$ $\bullet^{1}12^{40}$ – II; (R) 0^{30}; R 5^{50-30} R SW 11^{15-30}; = I
18	6	3.9	.	$\bullet^{2}3^{00}$ $\bullet^{0}4^{50}$ – I, 7^{25} ... II $\bullet^{2}13^{06-35}$ $\bullet^{1}17^{17}$ $\bullet^{2}$ ... III; = I
19	7	2.0	.	= I
20	7	.	.	⌓ ^{0}I
21	7	1.9	.	$\bullet^{0}13^{30-53}$; ⌓ ^{2}I
22	8	.	.	$\bullet^{0}2^{05}$ – ok. 4^{00}; ⌓ ^{0}I ⌓ ^{1}III
23	7	0.2	.	$\bullet^{0}11^{03}$ ... 12^{30}; = I, III; ⌓ ^{1}I, III
24	7	.	.	= I; ⌓ ^{1}I ⌓ ^{0}II
25	6	0.2	.	$\bullet^{0}11^{45}$ – 12^{20}; ⌓ ^{0}I
26	7	3.0	.	$\bullet^{0}7^{00}$ $\bullet^{0}9^{20}$ $\bullet^{1}9^{30}$ $\bullet^{0}10^{10}$ – ok. 11^{00}; = I
27	6	0.1	.	$\bullet^{0}9^{45}$ – ok. 10^{30}
28	6	4.2	.	$\bullet^{2}14^{20}$ $\bullet^{2}15^{10}$ – ok. 18^{15}; = III
29	8	1.0	.	⊕ ok. 19^{30} – 20^{00} $\bullet^{0}$ ... 24; ⌓ ^{2}I
30	7	4.3	.	$\bullet^{0}0^{00}$ ... 2^{40} $\bullet^{2}9^{22}$ – ok. 10^{00} $\bullet^{0}$II; ⌓ ^{0}III
31	7	0.0	.	$\bullet^{0}20^{25}$ – III
Σ	–	46.0	–	

Sierpień - Août

1	7	39.5	.	$\bullet^{0}21^{00}$ $\bullet^{2}21^{30}$
2	7	7.7	.	$\bullet^{1}5^{05}$ $\bullet^{2}5^{50}$ I $\bullet^{1}11^{00}$ $\bullet^{0}$II; R S ok. 3^{00-30}
3	8	0.6	.	$\bullet^{1}12^{12-25}$ $\bullet^{2}15^{30-50}$ $\bullet$ 16^{05}, ok. 20^{00}; = I; ⌓ ^{2}I
4	5	5.1	.	$\bullet^{1}10^{50}$ $\bullet^{0}11^{30-50}$ $\bullet^{2}13^{50}$ – 14^{00} $\bullet^{1}21^{06-35}$; = II; ⌓ ^{2}I
5	7	.	.	= I; ⌓ ^{2}I, III; ⊕ II
6	8	.	.	= I; ⌓ ^{2}I, III; ⊕ II
7	8	.	.	= I; ⌓ ^{2}I
8	7	.	.	= I; ⌓ ^{1}I
9	7	.	.	
10	7	12.7	.	$\bullet^{2}16^{30-55}$ $\bullet^{1}18^{25-50}$ 19^{25-40}
11	9	11.5	.	$\bullet^{2}$ok. 10^{0} – ok. 3^{00} $\bullet^{1}6^{05}$ $\bullet^{2}$I $\bullet^{1}9^{50}$ ... 12^{30} $\bullet^{0}12^{40-50}$ $\bullet^{1}16^{45-55}$ $\bullet^{0}$ 19^{30}; = I, II, III
12	8	0.2	.	$\bullet^{0}5^{20-35}$ $\bullet$ ok. 17^{00}
13	7	0.0	.	$\bullet$ ok. 18^{00}; = I; ⌓ ^{1}I, III; ▬ I
14	5	.	.	= I, II; ⌓ ^{2}I ⌓ ^{1}III
15	7	.	.	= I; ⌓ ^{2}I, III
16	6	.	.	= I; ⌓ ^{2}I, III; ▬ I
17	8	.	.	= I; ⌓ ^{2}I, III; ▬ I
18	7	.	.	= I; ⌓ ^{2}I, III; ▬ I, II
19	6	.	.	= I; ⌓ ^{2}I, III; ▬ I; ⊕ I, a
20	7	.	.	= I; ⌓ ^{2}I, III
21	7	.	.	= I; ⌓ ^{2}I, III; ▬ II
22	7	.	.	= I; ⌓ ^{2}I
23	7	0.2	.	$\bullet$ ok. 14^{00-10}; ⌓ ^{2}I
24	7	4.0	.	$\bullet^{0}$ok. 4^{10-30} $\bullet$ ok. 14^{00} $\bullet^{0}21^{00}$ $\bullet^{1}22^{20}$; = III; ⌓ ^{1}III
25	6	38.5	.	$\bullet^{0}1^{00}$ – 3^{10} ... I – 8^{20} 10^{30-40} 11^{10-20} $\bullet^{2}16^{50}$ $\bullet^{1}21^{00}$ – 24; = I, III
26	5	17.4	.	$\bullet^{1}0^{00}$ – I $\bullet^{0}$II. $\bullet^{2}15^{00}$ $\bullet^{1}17^{00}$ – 20^{30} $\bullet$ III $\bullet^{1}22^{00}$ $\bullet^{0}23^{50}$; = I, II
27	4	1.6	.	$\bullet^{0}3^{00}$ – I ... a $\bullet^{0}8^{20}$ – 9^{00} $\bullet^{0}$II – 13^{15}; = I, II, III
28	7	.	.	$\bullet^{0}2^{50}$ – 3^{50}; = I; ⌓ ^{1}III
29	7	1.5	.	= I; ⌓ ^{2}III
30	7	1.3	.	$\bullet^{1}4^{50}$ $\bullet^{0}5^{10}$ $\bullet^{1}5^{20-40}$ $\bullet^{0}12^{45-55}$ $\bullet^{1}14^{15-35}$, 17^{45} – 18^{00}; R N 14^{05} – NE 14^{30}; = I, II, III; ▬ II
31	7	0.2	.	= I; ⌓ ^{2}I, III; ▬ II
Σ	–	142.0	–	

Kraków, Obserw. Astr. UJ — $\varphi = 50°04'$ — $\lambda = 19°58'$ — *Wrzesień – Septembre 1965*

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	85.5	85.9	89.0	86.8	12.0	21.3	15.2	15.9	22.7	10.1	91	62	88	80	1.2	9.5	2.1	4.3	10	8	4	C 0 E 5	ESE 1
2	89.4	90.3	91.8	90.5	16.2	26.4	20.7	21.0	27.4	14.3	82	44	68	65	5.2	19.4	7.8	10.1	10	4	9	E 1 E 5	ESE 3
3	88.6	87.2	86.6	87.5	17.3	27.9	18.6	20.6	28.8	14.4	82	46	83	70	3.5	20.3	3.7	9.5	9	8	6	C 0 E 2	C 0
4	83.7	84.4	86.1	84.7	16.3	18.1	13.9	15.6	18.8	13.2	89	96	93	93	2.1	0.9	0.7	1.2	10	10 •	10	C 0 C 0	WSW 2
5	86.6	85.9	84.3	85.6	9.9	21.4	16.5	16.1	22.6	8.6	100	61	82	81	0.0	10.0	3.5	4.5	8 ≡	1	4	C 0 E 5	C 0
6	82.3	81.2	81.7	81.7	13.7	21.0	14.8	16.1	22.7	10.9	86	61	92	80	2.2	9.7	1.3	4.4	9	10	10 •	C 0 S 2	W 2
7	82.9	84.1	85.6	84.2	10.5	16.5	13.5	13.5	17.7	8.6	90	57	82	76	1.3	8.2	2.8	4.1	6	8	9	WSW 1 WSW 1	W 1
8	88.7	89.3	89.7	89.2	12.3	19.7	13.3	14.6	20.2	11.9	93	52	90	78	1.0	10.9	1.6	4.5	10 •	7	7	W 2 SW 4	C 0
9	87.2	87.3	87.3	87.3	12.1	23.6	16.8	17.8	26.7	9.1	83	49	93	75	2.3	16.7	1.4	6.8	2	7	8	SW 1 WSW 3	C 0
10	85.0	84.8	86.2	85.3	13.3	23.6	16.3	17.4	24.7	11.3	95	56	95	82	0.7	12.7	1.0	4.8	9	10 •	7	C 0 S 4	C 0
11	83.3	87.3	88.1	86.3	15.5	16.5	12.6	14.3	18.2	12.4	98	78	98	91	0.4	4.3	0.4	1.7	9	10	10 •	C 0 W 5	C 0
12	88.5	88.9	87.0	88.1	11.0	17.6	11.5	12.9	18.2	10.2	96	58	93	82	0.3	8.4	1.0	3.3	3	4	7	W 1 NW 1	C 0
13	85.3	84.7	86.3	85.5	8.3	17.7	11.6	12.3	19.1	7.4	99	55	91	82	0.2	9.0	1.1	3.4	2	10 K	9	C 0 NNE 5	C 0
14	88.2	89.3	92.8	90.1	9.0	19.5	11.2	12.7	19.5	7.2	99	48	96	81	0.2	11.8	0.5	4.2	9	8	8	C 0 SW 1	C 0
15	93.1	96.1	98.8	96.7	11.0	16.5	10.5	12.1	17.5	9.1	95	70	92	86	0.6	5.7	1.0	2.4	9	10	0	C 0 SW 3	C 0
16	100.4	100.3	98.5	99.8	10.0	18.3	11.1	12.6	18.6	7.4	97	61	94	84	0.3	8.3	0.8	3.1	5	4	0	C 0 WNW 1	C 0
17	97.3	95.6	95.3	96.1	7.9	22.5	14.3	14.8	23.8	6.5	97	51	91	80	0.2	13.2	1.5	5.0	0	1	0	C 0 W 1	C 0
18	93.5	90.7	90.1	91.4	9.3	23.2	16.8	16.5	23.5	6.3	100	49	67	72	0.0	14.6	6.3	7.0	0	0	2	C 0 C 0	S 1
19	91.2	93.6	98.6	93.1	13.7	12.7	10.7	12.0	18.4	10.3	93	93	96	94	1.1	1.1	0.3	0.9	10	10 •	10 •	C 0 WNW 1	C 0
20	101.6	102.8	106.1	103.3	8.8	14.1	11.2	11.3	16.5	8.6	100	69	90	86	0.0	4.9	1.3	2.1	6	9	9	C 0 SSW 1	C 0
21	107.0	106.8	105.0	106.3	10.6	16.5	9.4	11.3	17.8	9.2	90	57	97	81	1.3	8.2	0.3	3.3	2	6	3	C 0 W 2	C 0
22	101.5	99.1	96.0	98.9	5.9	19.2	11.9	12.2	20.5	4.7	98	52	93	82	0.2	10.5	0.7	3.8	2	4	3	C 0 W 1	C 0
23	93.8	92.3	90.4	92.2	7.3	21.8	12.9	13.7	23.0	6.0	100	54	93	82	0.0	11.9	1.1	4.3	2	0	2	C 0 SW 1	C 0
24	90.3	89.8	89.0	89.7	7.7	21.6	13.4	14.0	23.3	6.9	98	49	92	80	0.1	13.0	1.3	4.8	0	0	0	C 0 SE 1	C 0
25	88.2	86.6	85.4	86.7	7.1	23.0	12.7	14.4	24.0	4.2	100	54	89	81	0.0	12.9	1.8	4.9	10 ≡	4	2	C 0 E 3	C 0
26	83.6	82.2	82.5	82.8	10.2	23.9	16.8	16.9	24.4	10.1	97	44	81	74	0.3	16.5	3.7	6.8	2	4	10	C 0 E 3	C 0
27	80.4	80.8	82.7	81.3	16.2	24.2	17.7	19.0	24.6	14.6	82	36	63	60	3.2	19.3	7.4	10.0	10 •	2	9	ESE 2 SSE 4	SE 1
28	82.1	81.5	78.1	80.6	14.5	21.2	20.9	19.4	23.5	12.0	89	74	63	75	1.8	6.5	9.0	5.8	10	9	9	C 0 S 1	ESE 5
29	78.5	82.9	89.1	83.5	13.5	12.1	8.4	11.1	21.0	7.1	98	96	100	98	0.4	0.3	0.0	0.3	10 •	10 •	3	C 0 WNW 4	C 0
30	89.3	89.1	90.1	89.6	7.1	20.6	12.1	13.0	22.0	5.9	99	51	93	82	0.2	11.8	0.7	4.2	4	9	2	C 0 ESE 1	C 0
31																								
M	89.3	89.4	89.9	89.5	11.3	20.1	13.9	14.8	21.7	9.3	94	59	88	80	1.0	10.4	2.2	4.5	6.3	6.2	5.7	0.3	2.3	0.5

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1	91.0	91.3	91.4	91.2	8.1	20.6	14.5	14.4	21.1	7.3	99	63	89	84	0.2	8.9	1.8	3.6	0	0	0	C 0 E 4	NE 1
2	90.9	89.4	90.2	90.2	9.3	20.3	14.3	14.6	21.5	9.2	100	71	98	90	0.0	6.8	0.4	2.4	10 ≡	0	0	C 0 E 3	C 0
3	93.6	94.8	95.5	94.6	13.8	17.2	15.4	15.4	17.2	11.3	97	83	92	91	0.6	3.4	1.3	1.8	10 ≡	10	10	N 1 N 1	N 1
4	95.6	96.1	95.4	95.7	14.8	15.7	14.8	15.0	16.2	14.6	97	91	94	94	0.3	1.5	0.9	1.0	10	10 •	10	N 1 N 1	C 0
5	95.8	96.5	97.2	96.5	13.3	14.7	11.0	12.5	14.9	9.7	95	75	92	87	0.7	4.1	1.0	1.9	10	9	9	N 2 NE 2	NNE 4
6	97.3	96.4	95.9	96.5	9.6	14.5	7.7	9.9	14.8	7.6	95	72	98	88	0.7	4.6	0.1	1.8	10	6	0 ≡	NE 1 ENE 3	NE 1
7	94.3	95.5	92.8	93.5	4.5	14.7	9.3	9.4	16.8	4.3	100	73	100	91	0.0	4.5	0.0	1.5	10 ≡	0	3	C 0 NE 1	C 0
8	91.0	90.0	91.5	90.8	7.9	16.7	11.9	12.1	17.6	6.6	100	65	88	84	0.0	6.6	1.7	2.8	10 ≡	4	10	C 0 WNW 4	WNW 4
9	91.7	91.0	90.8	91.2	9.3	11.3	8.6	9.4	12.2	8.4	93	58	76	76	0.8	5.6	2.8	3.1	10	9	10	NW 1 NNE 1	NW 1
10	90.1	90.9	92.1	91.0	6.5	9.7	7.7	7.9	10.3	6.3	84	58	73	72	1.6	5.0	2.8	3.1	10	9	10	C 0 WNW 3	NW 1
11	91.7	90.6	91.7	91.3	6.9	11.5	9.3	9.2	12.5	6.6	81	60	74	72	1.8	5.5	3.1	3.5	10	10	10	WSW 2 W 3	W 3
12	98.4	101.0	102.3	100.6	1.9	7.5	1.0	2.8	9.4	0.8	94	49	96	80	0.4	5.3	0.3	2.0	2	2	2	C 0 NNE 2	C 0
13	102.2	100.2	98.8	100.4	-1.7	13.5	6.2	6.0	14.4	-2.2	96	33	80	70	0.2	10.4	1.9	4.2	0	3	4	C 0 NE 2	C 0
14	98.4	97.1	96.3	97.3	0.2	16.2	4.7	6.4	17.0	-0.7	98	36	95	76	0.1	11.7	0.4	4.1	0 ≡	1	2	C 0 WSW 2	C 0
15	96.1	95.3	94.4	95.3	-0.9	16.1	5.3	6.4	18.4	-1.4	100	46	98	81	0.0	9.9	0.1	3.3	3 ≡	2	3	C 0 C 0	C 0
16	93.1	90.5	93.2	92.3	0.5	16.6	11.4	10.0	19.1	0.3	100	42	80	74	0.0	10.9	2.7	4.5	7 ≡	8	10 •	C 0 C 0	WNW 4
17	98.6	101.0	102.6	100.7	8.1	10.0	3.6	6.3	11.4	3.4	85	60	97	81	1.6	5.0	0.3	2.3	9	10	5	W 3 WSW 4	C 0
18	101.5	100.1	99.4	100.3	1.3	8.9	3.9	4.5	10.2	-0.1	94	68	95	86	0.4	3.6	0.4	1.5	9 ≡	4	5	C 0 SW 1	W 1
19	99.9	100.8	101.6	100.8	4.4	9.4	2.7	4.8	10.8	2.5	93	76	100	90	0.6	2.8	0.0	1.1	10	7	0 ≡	W 1 C 0	C 0
20	102.8	103.7	105.2	103.9	4.0	8.3	3.6	4.9	9.1	0.4	93	81	90	88	0.3	2.2	0.8	1.2	10	9 ≡	7	WNW 1 WNW 1	C 0
21	106.6	107.5	108.1	107.4	-1.1	4.1	0.5	1.0	5.2	-1.3	99	75	86	87	0.1	2.0	0.8	1.0	9 ≡	9	2	C 0 E 3	ENE 1
22	108.7	109.1	107.6	108.3	-4.3	3.5	-0.1	0.2	7.4	-4.8	96	66	98	87	0.2	3.0	0.2	1.1	2 ≡	0	0 ≡	C 0 E 1	C 0
23	105.5	102.9	101.8	103.4	-1.7	7.7	5.3	4.2	8.1	-2.7	98	68	86	84	0.1	3.4	1.3	1.6	5 ≡	10 ≡	10	C 0 SW 2	C 0
24	101.5	102.4	102.1	102.0	4.9	11.3	2.2	3.2	11.6	2.0	90	67	100	86	0.9	4.6	0.0	1.8	10	8	2 ≡	SW 1 SW 1	C 0
25	102.2	101.6	101.3	101.7	-2.1	7.5	4.7	3.7	8.8	-2.6	98	73	92	88	0.1	2.8	0.7	1.2	10 ≡	0	9	C 0 W 1	C 0
26	99.0	97.9	95.7	97.5	4.5	8.9	2.1	4.4	9.8	1.9	89	72	98	86	0.9	3.2	0.1	1.4	10	0	2	NE 1 NE 1	C 0
27	94.6	93.8	94.2	94.2	-1.7	12.8	4.5	5.0	14.2	-1.8	100	53	98	84	0.0	7.0	0.1	2.4	4 ≡	0	0	C 0 W 2	C 0
28	93.3	91.8	91.2	92.1	-0.6	16.1	9.1	8.4	17.9	-1.1	100	52	84	79	0.0	8.7	1.9	3.5	3 ≡	9	8	C 0 SW 2	C 0
29	90.8	88.9	88.5	89.4	2.1	19.1	11.8	11.2	19.4	1.9	100	48	78	75	0.0	11.4	3.0	4.8	10 ≡	2	15 •	C 0 SW 1	C 0
30	95.0	94.9	92.8	94.2	6.6	11.8	2.7	6.0	12.8	2.6	88	50	95	78	1.1	6.9	0.4	2.8	8	6	0 ≡	W 1 WSW 3	C 0
31	87.8	87.5	86.8	87.4	0.9	10.1	7.5	6.5	11.0	-0.8	90	73	84	82	0.6	3.4	1.7	1.9	8 ≡	10 •	10 •	W 1 SW 3	SW 3
M	96.7	96.4	96.4	96.5	4.2	12.5	7.0	7.7	13.6	2.8	95	63	90	83	0.5	5.6	1.1	2.4	7.4	5.4	5.3	0.5	1.9	0.9

Kraków, Obserw. Astr. UJ $H_s = 206 m$ $H_b = 219.8 m$ $h_w = 10 m$ Wrzesień - Septembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	7	•	•	$\bullet^{0}5^{40-50}$; $=I$
2	8	•	•	$\frown^{2}I$, ▬ I
3	7	•	•	$=I$; $\frown^{2}I$, III
4	4	15.8	•	$\bullet^{0}7^{10}-8^{00}$ $\bullet^{1}9^{20}-11^{30}$ $\bullet^{0}12^{05-45}$ $\bullet^{1}14^{10}-15^{20}$ $\bullet^{2}16^{05}-17^{20}$ $\bullet^{1}-18^{00}$ $\bullet^{0}p-np$; $=I,II$; $\frown^{2}I$
5	7	•	•	$\bullet^{0}na$; $\equiv^{1}I$; $\frown^{2}III$
6	8	11.6	•	$\bullet^{1}17^{20}$ $\bullet^{2}18^{20}$ $\bullet^{1}20^{40}-23^{00}$; $=I$; $\frown^{2}I$; ▬ II
7	8	2.6	•	$\bullet^{0}ok.\ 5^{00}$, $ok.\ 20^{30}$
8	8	•	•	$\bullet^{2}0^{50}-1^{20}$ $\bullet^{0}1^{30-50}$, 3^{20-30} $\bullet^{2}6^{30-45}$; ▬ I, II
9	8	•	•	$\frown^{2}I$, III; ▬ II; ⊕ III
10	8	1.0	•	$\bullet^{0}12^{30}$, I $\bullet^{1}12^{45-50}$; $=I$; $\frown^{2}I$ $\frown^{0}III$
11	6	8.4	•	$\bullet^{2}9^{30-50}$ 10^{05-20} $\bullet^{0}19^{20}-ok.\ 22^{00}$; $=I$, III; ▬ I
12	6	•	•	$=I$, III; $\frown^{2}III$
13	6	2.0	•	$\bullet^{2}12^{45}$ $\bullet^{0}13^{00}$; ↖ NW 11^{58} NNE 13^{24}; $=I$; $\frown^{2}III$
14	7	3.1	•	$\bullet^{1}16^{25-40}$ $\bullet^{2}18^{35-45}$; $=I$, III; $\frown^{2}I$
15	6	•	•	$=I$, III; $\frown^{1}III$
16	5	•	•	$\equiv^{0}na$ $=I$, II, III; $\frown^{2}I$, III
17	7	•	•	$\equiv^{0}na$ $=I$, III; $\frown^{2}I$ $\frown^{1}III$
18	7	•	•	$\equiv^{0}na$; $=I$; $\frown^{2}I$
19	5	11.4	•	$\bullet^{0-2}7^{30}-8^{25}$ $\bullet^{2}9^{40}$ $\bullet^{1-0}16^{30}$, $18^{50}-24$; $=I$, II
20	6	•	•	$\bullet^{0-1}0^{00}-ok.\ 1^{00}$; $=I$
21	7	•	•	$=I$ $=III$; $\frown^{0}I$
22	7	•	•	$=I$, III; $\frown^{2}I$, III; ▬ II
23	7	•	•	$\equiv^{0}na$ $=I$, III; $\frown^{2}I$, III
24	7	•	•	$\equiv^{0}na$ $=I$; $\frown^{2}I$
25	7	•	•	$\equiv^{2}na-ok.\ 19^{00}$; $\frown^{2}III$
26	8	0.0	•	$=I$; $\frown^{2}I$ $\frown^{1}III$
27	8	0.5	•	$\bullet^{1}6^{25}-7^{10}$
28	8	9.0	•	$\frown^{2}I$; ▬ I
29	5	19.9	•	$\bullet^{1-2}14^{0}-a$ $\bullet^{0}10^{10}$ $\bullet^{2}12^{10}-14^{00}$; $=I,II$
30	8	•	•	$=I$; $\frown^{2}I$, III
31				
Σ	-	85.1		

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1	8	•	•	$=I$ $=III$; $\frown^{2}I$
2	7	•	•	$\equiv^{2}na$, I $\equiv^{1}7^{20}-ok.\ 8^{30}$ $=III$; $\frown^{2}I$ $\frown^{1}III$; ▬ II
3	4	•	•	$\equiv^{0}I$ $=II$, III; $\frown^{2}I$ $\frown^{1}III$
4	4	0.4	•	$\bullet^{0}II$ $\bullet^{0}ok.\ 20^{00}$; $=I,II,III$; $\frown^{2}I$
5	7	•	•	$=I$; $\frown^{0}III$
6	7	0.2	•	$=I$ $\equiv^{0}III$; $\frown^{2}III$; ▬ I
7	5	•	•	$\equiv^{2}I$ $=II$ $=III$; $\frown^{2}I$, III
8	5	0.0	•	$\bullet ok.\ 20^{00}-III$; $\equiv^{0}I$ $=II$, III; $\frown^{2}I$; ⊕ II
9	8	•	•	$=I$
10	8	•	•	
11	7	•	•	▬ I, II
12	7	•	•	$\frown$ zm. na $\frown^{1}I$ $\smile^{0}III$; ▬ I
13	7	•	•	$=I$, II $\smile^{2}I$ $\frown^{0}III$; ▬ I
14	7	•	•	$\equiv I$ $=III$; $\smile^{0}I$ $\frown^{2}III$; ▬ I
15	5	•	•	$\equiv^{0}I$ $=II$ $=III$; $\smile^{2}I$ $\frown^{2}III$
16	5	0.5	•	$\bullet^{0}III$, $\equiv^{0}I$ $=II$; $\smile^{1}I$
17	7	•	•	$=I$
18	4	•	•	$\equiv^{0}I$ $=II$, III; $\smile^{0}I$ $\frown^{2}III$; ▬ II
19	5	0.1	•	$=I$, II $\equiv III$; $\smile^{2}I$ $\frown^{1}III$
20	5	•	•	$\bullet^{0}na$; $\equiv^{0}I$ $=II$; ▬ I
21	7	•	•	$\equiv^{1}I$; $\smile^{1}I$
22	4	•	•	$\equiv^{0}I$ $=II$ $\equiv^{0}III$; $\smile^{2}I$ $\smile^{0}III$; ▬ II
23	5	•	•	$\equiv^{0}I$, II $=III$; $\smile^{2}I$ $\frown^{1}III$
24	5	•	•	$=I$, II $\equiv^{0}III$, $\frown^{2}III$
25	7	•	•	$\equiv^{0}na-ok.\ 10^{00}$; $\smile^{2}I$
26	6	•	•	$=I$, III; $\smile^{0}III$; ▬ I
27	5	•	•	$\equiv^{1}I$ $=II$, III; $\smile^{0}I$
28	5	•	•	$\equiv^{1}I$ $=II$; $\smile^{0}I$ $\frown^{0}III$
29	5	0.3	•	$\bullet^{0}III$, n; $\equiv^{2}I$ $=II$, III; $\smile^{0}I$
30	6	•	•	$=I$ $\equiv^{0}III$
31	6	0.5	•	$\bullet^{0}12^{25-45}$, p z prz.; $\equiv^{0}I$; $\smile^{1}I$
Σ	-	2.0	-	

Kraków, Obserw. Ast. UJ — $\varphi = 50°04'$ — $\lambda = 19°58'$ — *Listopad – Novembre 1965*

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność wzgl. U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N_w I	II	III	Kierunek i prędkość wiatru D_v I	II	III
1	85.4	80.9	76.0	80.8	6.1	11.2	12.9	10.8	15.2	5.5	80	73	70	74	1.8	3.6	4.4	3.5	9	10	10 •	SW 3	SW 3	SW 2
2	75.1	76.7	80.4	77.4	13.5	14.7	7.7	10.9	14.9	7.5	59	51	82	64	6.3	8.2	1.9	5.5	6	10	9	SW 4	SW 6	SW 2
3	83.1	83.2	82.7	83.0	7.6	12.9	8.9	9.6	13.3	7.1	73	46	76	65	2.8	8.1	2.8	4.6	2	6	8 •	SW 1	SW 3	S 1
4	90.6	94.0	97.9	94.2	4.1	7.5	5.2	4.5	9.8	2.9	90	66	90	82	0.8	3.5	0.8	1.7	10	9	7	W 2	WSW 1	W 1
5	100.9	101.7	103.8	102.1	0.6	5.3	4.8	3.9	6.0	0.2	100	80	78	86	0.0	1.8	1.9	1.2	10 ≡	10 ≡	10	C 0	SW 2	SW 1
6	104.5	103.6	100.9	103.0	3.6	4.9	2.9	3.6	6.2	2.5	80	73	91	81	1.6	2.4	0.6	1.5	10	10	3	C 0	W 2	WSW 1
7	96.2	95.6	94.7	94.8	-0.7	8.9	1.4	2.8	10.4	-1.4	99	52	96	82	0.0	5.5	0.3	1.9	7 ≡	2	3	C 0	C 0	C 0
8	96.9	97.2	97.7	97.3	-1.3	6.3	-0.3	1.1	6.3	-1.8	98	78	100	92	0.2	2.1	0.0	0.8	5 ≡	0 ≡	0 ≡	C 0	C 0	C 0
9	97.6	96.4	94.9	96.3	-1.1	4.3	4.5	3.0	5.3	-1.6	99	82	92	91	0.1	1.5	0.7	0.8	10 ≡	0 ≡	10	C 0	WSW 1	C 0
10	92.9	92.0	90.4	91.8	4.5	5.5	5.3	5.2	5.8	4.1	92	95	98	95	0.7	0.4	0.1	0.4	10 ≡	10 ≡	10 ≡	WSW 1	C 0	C 0
11	85.4	81.7	79.0	82.0	4.5	3.3	-0.1	1.9	5.4	-0.2	73	88	100	87	2.5	0.9	0.0	1.1	10	10 •	10 *	ENE 5	NE 5	NE 5
12	76.7	78.5	80.7	78.6	-1.4	-1.3	-1.5	-1.4	-0.1	-1.8	97	88	96	94	0.2	0.6	0.2	0.3	10 *	10	10	NNE 2	N 2	C 0
13	81.9	82.3	83.4	82.5	-3.5	-3.0	-3.9	-3.6	-1.3	-4.1	85	95	89	90	0.7	0.3	0.5	0.5	10 ●	10 ☆	10	NNE 3	NNE 3	NNE 2
14	84.0	85.2	87.0	85.4	-5.4	-5.1	-5.7	-5.5	-3.9	-5.8	95	85	92	91	0.2	0.6	0.3	0.4	10 ☆	10	10 *	NE 2	NE 2	NNE 1
15	88.4	90.3	94.1	90.9	-6.1	-4.3	-5.1	-5.2	-4.2	-7.2	97	79	68	81	0.1	0.9	1.3	0.8	10 ≡	6	10 *	NNE 1	C 0	W 2
16	98.2	99.4	101.2	99.6	-6.8	-4.8	-6.8	-6.3	-4.4	-7.6	94	71	83	83	0.2	1.2	0.6	0.7	10 ≡	10 *	10	W 1	NW 4	NW 1
17	100.4	96.9	93.3	96.9	-8.2	-6.5	-12.4	-9.9	-6.4	-12.6	89	81	85	85	0.3	0.7	0.4	0.5	10 *	7	10	NE 1	NNE 1	C 0
18	88.0	84.5	82.7	85.1	-15.8	-8.3	-7.8	-9.9	-7.4	-16.1	91	78	81	83	0.2	0.7	0.6	0.5	9 ≡	7	10 ≡	C 0	NE 2	NE 1
19	79.6	77.8	76.4	77.9	-5.9	-0.9	-2.3	-2.8	-0.7	-8.2	81	81	93	85	0.7	1.1	0.4	0.7	10 ≡	9 • ≡	9 ≡	C 0	NE 1	C 0
20	75.8	76.1	76.2	76.0	-1.7	0.7	0.3	0.0	1.4	-5.9	98	92	100	97	0.1	0.3	0.0	0.2	10	10 •	10	C 0	C 0	C 0
21	68.3	63.5	62.0	64.6	0.5	2.6	3.3	3.5	5.6	-0.6	100	100	84	95	0.0	0.0	1.4	0.5	10	10	8	NE 1	NE 1	SW 2
22	73.6	80.4	83.3	79.8	-0.7	-0.4	-0.2	-0.4	6.2	-1.3	95	96	92	94	0.3	0.2	0.5	0.3	10	10	10	WSW 4	WSW 3	WSW 1
23	90.6	92.1	95.1	92.6	-4.5	-4.5	-5.6	-5.0	-0.1	-5.9	58	84	82	75	1.9	0.7	0.7	1.1	10	9	9	NW 1	NW 2	C 0
24	94.4	92.8	91.2	92.8	-9.9	-5.1	-8.1	-7.3	-2.7	-10.1	88	70	92	83	0.4	1.4	0.2	0.7	7 ≡	0	0	C 0	NE 1	C 0
25	90.0	90.5	90.9	90.5	-10.2	-5.9	-3.4	-5.2	-2.1	-11.2	91	89	88	89	0.3	0.5	0.6	0.5	2 ≡	10 ≡	9	C 0	C 0	C 0
26	83.1	78.8	78.7	80.2	-3.1	6.6	3.7	2.7	7.3	-5.9	79	40	77	65	1.0	5.8	1.9	2.9	10	8	10	NE 1	S 2	SW 2
27	77.6	69.9	61.1	69.5	1.1	1.3	8.5	4.8	9.6	0.4	92	94	74	87	0.5	0.4	2.9	1.3	10	9	10	ESE 3	E 1	C 0
28	63.5	66.5	72.8	67.6	6.1	5.1	2.3	4.0	9.4	1.8	73	55	77	68	2.5	4.0	1.7	2.7	10	6	3	SW 2	SSW 4	SW 3
29	78.8	80.5	74.5	77.9	1.1	3.2	0.3	1.7	5.2	-0.2	83	57	71	70	1.1	3.8	1.8	2.2	9	0	9	SSW 1	SSW 4	E 4
30	67.3	69.3	72.5	69.8	5.2	7.3	2.9	4.6	10.2	0.0	75	84	93	84	2.2	1.6	0.5	1.4	9	10 •	10 •	C 0	SSW 1	C 0
31																								
M	85.6	85.2	85.2	85.3	-0.9	2.2	0.4	0.5	3.9	-2.6	87	77	86	83	1.0	2.1	1.0	1.4	8.8	7.6	8.2	1.3	1.9	1.1

Grudzień – Décembre

Dni	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	74.6	76.1	80.3	77.0	1.6	4.8	3.7	3.4	5.7	1.1	69	59	65	64	2.2	3.5	2.8	2.8	1	8	8	SW 2	WSW 8	SW 2
2	82.1	83.0	81.4	82.2	2.4	4.2	0.0	1.6	4.8	-0.2	72	69	78	73	2.1	2.5	1.3	2.0	3	6	1	SW 4	SW 5	C 0
3	74.3	73.4	73.1	73.6	0.0	4.1	0.1	1.1	4.1	-2.0	84	50	96	77	0.9	4.1	0.3	1.8	10	10	10 *	C 0	ESE 1	SW 2
4	73.1	76.3	79.2	76.9	0.0	3.7	-0.1	0.9	5.3	-1.3	88	77	96	87	0.7	1.9	0.3	1.0	10 ≡	8	10	C 0	SW 2	C 0
5	80.1	78.7	71.8	76.9	1.3	3.7	4.3	4.0	6.9	-0.2	77	79	63	73	1.3	2.0	3.1	2.2	3	9	10 •	C 0	SSW 1	SSE 3
6	70.0	73.1	79.2	74.8	7.7	9.1	3.5	7.0	9.6	2.3	79	56	72	69	2.2	3.1	2.5	3.3	10 •	9	2	SW 7	SW 3	SSW 4
7	81.9	83.8	85.8	83.8	5.3	8.0	5.9	6.3	8.0	3.9	69	59	71	66	2.8	4.4	2.7	3.3	10	9	9	SW 1	SW 3	SW 2
8	86.9	87.7	91.2	88.6	1.8	4.1	2.7	2.8	5.9	1.4	83	64	82	76	1.2	2.9	1.3	1.8	10 ≡	10 •	8	C 0	WSW 1	WSW 2
9	94.2	90.2	81.3	88.6	-0.9	3.1	-0.7	0.7	5.4	-1.5	87	51	79	72	0.7	4.3	1.2	2.1	3 ≡	1	1	C 0	S 3	C 0
10	63.1	62.7	62.0	63.3	3.1	8.5	6.3	6.6	8.8	-1.8	66	65	66	66	3.0	3.9	3.2	3.4	8	10	9	S 1	SSW 6	SW 4
11	63.3	68.2	70.8	68.1	4.3	4.3	1.7	3.0	6.3	1.3	74	55	78	69	2.2	3.7	1.3	2.3	10	9	9	WSW 1	W 1	C 0
12	74.5	76.7	79.9	77.0	1.5	1.9	1.3	1.5	2.1	0.7	80	85	89	85	1.4	1.0	0.8	1.1	10 ●	10 *	10 •	WSW 2	SW 2	WSW 1
13	83.0	83.6	81.9	82.8	0.3	1.3	-1.1	-0.1	1.6	-1.4	79	79	93	84	1.3	1.4	0.3	1.0	10	10	10	WSW 1	W 2	N 1
14	83.0	92.0	98.8	91.9	-1.3	-3.1	-4.7	-3.3	-0.8	-4.8	92	79	81	84	0.4	1.0	0.8	0.7	10	9	9	N 3	WNW 3	W 1
15	96.3	93.4	93.6	94.4	-3.7	-1.7	0.3	-1.6	0.7	-7.4	84	84	88	85	0.6	0.9	0.7	0.7	9 ≡	10 *	10	C 0	SW 1	WSW 1
16	93.8	93.8	93.9	93.8	-4.9	-3.1	-3.7	-3.4	0.9	-3.9	76	75	72	74	1.0	1.0	1.1	1.0	10 ≡	10	10	NNE 2	NNE 1	NNE 1
17	91.2	89.3	89.0	89.8	-3.3	-2.3	-0.7	-2.3	-0.3	-6.2	72	85	93	84	1.1	0.8	0.3	0.7	10 * ≡	10	10	NNE 1	C 0	C 0
18	89.1	87.3	88.7	88.4	-3.7	1.1	4.7	1.7	4.8	-4.3	83	79	94	85	0.8	1.4	0.3	0.9	10 ≡	10	10	C 0	C 0	C 0
19	89.3	90.3	88.0	89.3	6.4	9.6	7.7	7.8	9.6	4.3	97	78	83	86	0.3	2.7	1.8	1.6	10 •	10	8	C 0	SSW 2	SW 2
20	88.8	90.6	88.2	89.2	8.3	7.6	4.9	6.4	11.3	4.6	89	82	92	88	1.3	1.9	0.7	1.3	10 ●	10	10	C 0	C 0	C 0
21	84.8	83.3	83.5	84.6	3.3	8.1	4.0	4.8	8.3	2.6	97	72	87	85	0.2	3.0	1.1	1.4	10 ≡	8	10 •	C 0	NNW 1	NNW 3
22	89.8	90.5	90.3	90.2	0.6	1.6	0.6	0.8	4.0	0.5	92	80	90	87	0.5	1.4	0.6	0.8	10 *	10	10 ●	NNW 1	NW 2	NW 1
23	89.0	86.2	81.5	85.6	-0.3	-0.6	-1.0	-0.7	0.8	-1.2	92	97	97	95	0.5	0.2	0.2	0.3	10	10	10	NE 2	E 2	NNE 3
24	76.2	74.0	71.4	73.9	-4.7	0.1	1.0	-0.6	1.1	-3.3	93	86	87	89	0.3	0.9	0.9	0.7	1	8	10	C 0	C 0	NE 1
25	66.2	62.9	63.4	64.2	-0.6	4.0	-0.7	0.3	5.4	-2.9	93	62	87	81	0.4	3.0	0.7	1.4	6	8	3	C 0	SE 2	C 0
26	64.0	66.3	74.9	68.5	-1.9	6.9	1.5	2.0	7.2	-2.4	96	61	89	82	0.2	3.8	0.8	1.6	8	9	8 *	C 0	C 0	W 3
27	81.0	78.0	71.3	76.8	-0.7	2.2	-0.4	0.2	3.3	-4.1	81	64	82	76	1.1	2.6	1.1	1.6	2	8	5	C 0	C 0	SSE 1
28	68.1	72.2	80.7	73.7	1.3	3.1	0.1	1.2	3.6	-0.6	96	91	84	90	0.3	0.6	1.0	0.6	10 • ≡	10 ●	3	C 0	WSW 2	W 3
29	83.3	86.2	89.0	86.2	-3.3	0.9	-1.6	-1.4	0.9	-4.7	81	69	78	76	0.9	2.0	1.2	1.4	9	3 *	4	C 0	W 2	SW 2
30	86.2	82.2	81.0	83.1	-3.7	1.9	3.3	0.7	4.7	-6.2	72	60	61	64	1.1	2.8	3.0	2.3	10	4	10	C 0	C 0	SW 4
31	82.2	80.9	82.2	81.8	1.6	4.3	1.3	2.2	5.4	0.8	83	73	81	78	1.2	2.4	1.3	1.6	10	10 •	9	C 0	SW 2	SW 1
M	81.0	81.2	81.6	81.3	0.5	3.3	1.4	1.6	4.7	-1.3	83	72	83	79	1.1	2.4	1.3	1.6	8.3	8.6	7.9	0.9	1.9	1.6

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$ Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU	POGODA
1	8	1.1	•	$\bullet^{0}$ na. 10^{00-45} $\bullet$ p – 20^{00} $\bullet^{0}20^{30}-21^{45}$
2	8	0.9	•	$\bullet^{2}14^{45}-15^{10}$; ≫ na. a ≫ p
3	8	3.4	•	$\bullet^{0}$ III. 20^{50} $\bullet^{1}21^{10}$ – n; ▟▟ I, II
4	6	•	•	= I, III
5	3	•	•	$\equiv^{0}$ I II = III; ⌴ ^{1}I
6	5	•	•	= I, II, III; ▟▟ I, II
7	5	•	•	≡ I = II, III; ⌴ ^{2}I ⌴ ^{0}III
8	3	•	•	$\equiv^{0}$ I, II $\equiv^{1}$ III; ⌴ ^{2}I ⌴ ^{0}III
9	3	•	•	$\equiv^{2}$ I $\equiv^{0}$ II = III; ⌴ ^{0}I
10	3	0.0	•	$\equiv^{0}$ I, II, III
11	6	11.5	•	• na $\bullet^{0}12^{20}-13^{15}$ $*^{0}$ – ok. 15^{00} $*^{0}$ – n; = III
12	7	10.7	6	$*^{0}$ na – a $*^{1}$ a z prz. $\overset{*}{\nabla}{}^{0}$ p
13	6	0.2	5	• na. I △ ^{0} a z prz. II $*^{0}$ ◡ p z prz.; ◡ p; = I
14	5	2.0	5	△ ^{0} na I, a $*^{0}$ ok. 18^{30} – p. III; = I, II
15	4	0.1	7	$*^{0}$ p... np; $\equiv^{0}$ I, a – ok. 9^{15} = II, III; ▟▟ II
16	4	0.2	7	$*^{0}$ na $*^{1-2}$ ok. $10^{30}-11^{30}$ * II, p $*^{0}$ ok. 21^{00-30}; $\equiv^{0}$ I = II
17	5	0.0	8	$*^{0}6^{00}$ ok. 10^{00}; = I, II, III; ⌴ ^{0}III
18	4	1.5	8	$*^{1}16^{00-30}$; $\equiv^{0}$ I = II, III; ⌴ ^{0}I
19	4	•	7	$*^{0}$ n; = I, II $\equiv^{0}$ III; ⌴ ^{0}III
20	1	7.5	7	• 8^{00} $\bullet^{0}11^{00}$ $\bullet^{0}$ • * a – p * 17^{00-40} • ok. 19^{00}; $\equiv^{1}$ I $\equiv^{2}$ II, III
21	4	8.9	5	$\bullet^{0-1}$ $7^{40}-13^{40}$ $\bullet^{0}14^{20}$ – p; = I, II
22	4	0.1	3	⚹ n $*^{0}7^{30}-9^{30}$ * p; = I, II
23	6	•	3	= I; ⌴ ^{0}III
24	7	•	3	$\equiv^{0}$ I; ⌴ ^{1}I ⌴ ^{0}III
25	3	0.0	3	$*^{0}13^{30}-14^{05}$; $\equiv^{0}$ I $\equiv^{0}$ II = III; ⌴ ^{2}I ⌴ ^{0}II; ▟▟ I
26	8	•	3	= I
27	5	1.2	2	$*^{0}9^{45}-10^{20}$; = I, II
28	8	•	pż.	≫ p
29	8	0.3	pż.	$*^{1-2}9^{10}-10^{30}$; ⊹ $9^{10}-10^{30}$; ▟▟ I
30	4	4.3	•	$\bullet^{1}$ ok. 14^{00}... p $\bullet^{0-1}$ – np; = II; ▟▟ I
31				
Σ	-	53.7	-	

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1	8	•	•	▟▟ I
2	8	•	•	⌴ ^{0}III; ▟▟ I
3	5	7.8	•	$\bullet^{0}14^{15}$ $\overset{*}{*}$ 14^{30} $\bullet^{0}19^{00}$ $\overset{*}{*}$ III; = I, II, III; ⌴ ^{0}I; ▟▟ I
4	4	•	5	$\equiv^{0}$ I = II, III
5	7	3.0	4	$\bullet^{0}20^{45}$ – np; = I; ⊕ a, II, p
6	8	•	pż.	• I; ⌣ p; ▟▟ III
7	8	•	•	⌣ III
8	4	0.0	•	• 12^{05} $\bullet^{0}$ II • p; $\equiv^{0}$ I = II
9	7	•	•	$\equiv^{0}$ na. – a; ⌴ ^{0}I, III
10	8	(0.0)	•	$\bullet^{0}$ ok. 12^{00} – a; ⌴ ^{0}I
11	5	•	•	= I, II; ⌣ III; ▟▟ II
12	4	1.2	•	• I $*^{0}$ ok. 9^{15} – a $\overset{*}{*}{}^{0}$△ a z prz. $*^{0}$ II... p $*^{0}$ 20^{15} – n; = II, III
13	4	4.5	•	= I, II
14	6	0.5	8	$*^{2}$ n $*^{0}$ a, p... 19^{30}
15	4	0.7	7	$*^{0}$ ok. 9^{45} II; $*^{1}$ ok. 14^{30}... III; $\equiv^{0}$ I = II
16	5	0.8	6	$\equiv^{0}$ I = II, III
17	4	1.4	6	$*^{0}$ n – ok. 9^{00} * a; $\equiv^{0}$ I = II, III
18	4	8.9	7	• a $\bullet^{1}$ ok. 15^{00} – np; $\equiv^{2}$ I = II, III
19	6	1.2	pż.	$\bullet^{1-0}$ na $\bullet^{0}$ I, 12^{40-44}; = I
20	4	0.0	•	$\bullet^{0}$ n $\bullet^{1}$ I, 14^{15} – p; = I, II, III
21	4	2.8	•	$\bullet^{0}$ ok. 19^{30} – np; $\equiv^{0}$ I = II
22	5	0.7	•	$\overset{*}{*}{}^{0}$ na $*^{0}$ ok. 11^{00} ◡△ ok. 19^{15} – III; = I, II
23	7	•	•	
24	5	0.0	•	$*^{0}$ p z prz.; = II, III; ⌴ ^{1}I
25	9	•	•	
26	6	1.0	•	• $\overset{*}{*}$ III; = I, II
27	8	6.8	•	= I
28	4	1.1	•	$\bullet^{0-1}$ na $\bullet^{1}$ I • $\bullet^{0-1}$ a, II $\bullet^{0}$ • $*^{0}$△ p – ok. 16^{20}; $\equiv^{0}$ I = II
29	4	0.0	•	$*^{0}$ II; = I, II; ⌴ ^{2}I ⌴ ^{1}II ⌴ ^{2}III; ⌣ III
30	4	•	•	= I, II; ⌴ ^{2}I; ▟▟ I
31	5	0.0	•	• II, = I, II, III
Σ	-	42.1	-	

Przemyśl — φ = 49°48' — λ = 22°46' — *Styczeń – Janvier* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	82.7	81.4	80.4	81.5	3.7	5.4	3.5	4.0	5.5	2.7	62	44	57	54	3.1	5.0	3.4	3.8	9	9	6	SW 7	WSW 8	WSW 3
2	75.9	74.3	75.4	75.2	3.6	3.6	0.7	2.2	3.9	0.6	65	72	94	77	2.8	2.2	0.4	1.8	8	10	10 *	W 7	SW 2	SE 1
3	76.7	77.4	78.3	77.5	0.3	0.4	0.2	0.3	0.8	0.0	98	98	98	98	0.1	0.1	0.1	0.1	10 *	10 * ≡	10	C 0	E 2	NE 3
4	79.4	81.4	86.6	82.5	-1.3	0.2	-2.3	-1.4	0.3	-2.6	99	98	96	98	0.1	0.1	0.3	0.2	10 *	10 *	10 *	E 1	NNE 5	N 6
5	90.2	86.1	87.4	87.9	-5.1	-1.0	-0.3	-1.2	0.3	-4.9	77	65	88	77	1.1	2.0	0.8	1.3	9	8	6	NW 5	W 9	W 7
6	88.3	89.2	88.4	88.6	-0.7	-1.3	-3.8	-2.4	0.0	-4.1	75	74	76	74	1.5	1.4	1.1	1.3	8	8	2	NW 8	NW 8	NW 7
7	89.5	90.6	91.7	90.6	-4.3	-5.9	-4.6	-4.4	-5.5	-5.1	79	85	86	83	0.9	0.7	0.6	0.7	10	9 *	10 *	N 8	NW 7	W 4
8	88.0	83.9	79.4	83.8	-8.0	-1.1	-1.6	-3.1	-1.0	-9.1	87	57	78	74	0.4	2.4	1.2	1.3	9	8	10	WSW 2	W 7	W 7
9	77.3	77.4	77.1	77.3	-1.0	0.6	-0.6	-0.4	0.7	-2.0	89	77	93	86	0.7	1.5	0.4	0.9	10 △	10	10 *	W 10	W 7	W 5
10	77.2	76.2	85.2	79.5	1.4	2.6	0.0	1.0	3.0	-1.5	85	72	98	85	1.0	2.1	0.1	1.1	8	10	10 *	W 5	SE 2	N 5
11	98.6	99.6	99.6	99.3	-15.2	-11.7	-16.4	-14.4	0.0	-16.4	92	89	90	90	0.2	0.3	0.2	0.2	2	0	0	N 4	E 1	ESE 1
12	97.0	95.3	94.1	95.5	-16.0	-9.0	-10.9	-11.7	-8.3	-18.2	91	76	87	85	0.2	0.7	0.4	0.4	0	6	10	C 0	ESE 3	ENE 2
13	92.7	92.6	94.0	93.1	-11.5	-5.9	-6.1	-7.4	-4.8	-12.3	86	66	81	78	0.4	1.3	0.7	0.8	0	0	0	NE 1	E 2	WSW 3
14	92.6	91.0	90.9	91.5	-7.3	-0.4	-1.3	-2.6	3.4	-9.4	85	53	58	65	0.5	2.8	2.3	1.9	0	1	0	SE 1	N 2	W 5
15	95.7	96.6	94.3	95.5	0.5	3.1	0.0	0.9	3.1	-8.9	75	66	84	75	1.6	2.6	0.9	1.7	10	0	9	W 3	C 0	E 2
16	92.7	92.4	92.7	92.6	-10.2	-5.1	-9.8	-8.7	-4.3	-11.0	91	75	91	86	0.3	1.0	0.3	0.5	1	4	0	SE 3	E 1	SW 2
17	88.1	83.0	76.2	82.4	-1.9	2.1	4.0	2.0	4.0	-9.8	71	57	59	62	1.5	3.0	3.3	2.6	3	9	9	SW 10	SW 9	WSW 7
18	71.9	71.9	69.5	71.1	4.2	4.1	2.1	3.1	5.8	0.0	71	71	82	75	2.4	2.4	1.3	2.0	10	10	10	WSW 7	W 1	W 3
19	68.4	69.4	70.3	69.4	-0.8	2.4	-3.3	-1.2	3.1	-3.5	94	68	92	85	0.4	2.4	0.4	1.1	1	2	0	WNW 3	WNW 1	ESE 2
20	65.5	63.2	59.3	62.7	-2.7	-0.3	0.3	-0.6	0.3	-6.0	93	92	98	94	0.3	0.5	0.1	0.3	10 *	10	10	E 10	ESE 6	ENE 5
21	63.2	68.2	75.4	68.9	-0.2	0.1	0.1	0.0	0.6	-0.5	100	98	96	98	0.0	0.2	0.3	0.2	10	10 ●	10	C 0	SW 5	WNW 1
22	80.1	81.5	83.7	81.8	-1.9	-1.2	-3.3	-3.4	0.4	-5.6	90	82	98	90	0.5	1.0	0.1	0.5	10	9	0	C 0	SE 1	W 1
23	85.3	86.0	89.8	87.0	-2.7	-0.4	0.1	-0.7	0.3	-5.8	97	94	98	96	0.1	0.3	0.2	0.2	10 △	10	10 ≡	C 0	N 2	C 0
24	93.9	94.3	93.8	94.0	-0.7	0.3	-0.1	-0.2	0.4	-0.7	99	93	96	96	0.0	0.4	0.3	0.2	10 ● ≡	10 ≡	10 ●	WSW 1	WNW 2	E 3
25	91.0	90.0	89.9	90.3	-1.3	-0.7	-0.9	-1.0	0.0	-2.1	99	97	99	98	0.1	0.2	0.0	0.1	10 ●	10 ●	10	ESE 1	NW 2	C 0
26	88.9	88.8	88.6	88.8	-1.8	-0.7	-2.1	-1.7	-0.6	-2.4	96	91	94	94	0.2	0.5	0.3	0.3	10	9	10	SE 1	E 3	SE 3
27	89.0	89.3	90.0	89.4	-5.0	-1.7	-1.6	-2.0	-1.1	-3.4	95	90	90	82	0.3	0.6	0.5	0.5	10	10	10	ESE 4	SE 5	S 1
28	91.1	91.1	90.6	90.9	-3.1	-0.1	-2.3	-2.0	0.5	-3.1	93	82	87	87	0.4	1.1	0.7	0.7	10	7	10	ESE 3	S 4	SSE 4
29	88.7	87.2	85.6	87.2	-4.1	5.2	5.1	2.8	6.1	-5.3	94	64	75	78	0.3	3.1	2.2	1.9	9	9	9	E 1	SSW 3	S 2
30	83.9	82.7	81.1	82.6	5.4	8.7	6.1	6.6	8.8	4.3	81	68	82	77	1.7	3.6	1.7	2.3	4	9	10	SW 4	SW 4	W 4
31	82.3	85.2	84.1	83.9	5.2	1.4	-0.2	1.6	6.9	-0.5	89	98	100	96	0.9	0.2	0.0	0.4	10 ●	10 *	10 *	WNW 2	NW 3	E 2
M	84.7	84.4	84.6	84.6	-2.5	-0.1	-1.7	-1.5	1.1	-4.7	87	78	87	84	0.8	1.5	0.8	1.0	7.5	7.6	7.5	3.6	3.7	3.3

Luty – Février

1	85.2	86.5	88.6	86.8	-2.1	-1.1	-3.1	-2.4	-0.2	-5.8	98	91	90	93	0.1	0.5	0.3	0.4	10 *	9 *	10	NW 3	NW 2	NW 2
2	90.6	92.2	96.3	93.0	-3.4	-3.3	-4.2	-3.8	-3.0	-4.8	90	81	94	88	0.5	0.9	0.3	0.6	9	9 *	10 *	NW 7	NNW 7	NW 5
3	97.1	95.4	92.5	95.0	-4.9	-3.9	-2.5	-3.4	-2.5	-6.1	88	82	84	85	0.5	0.8	0.8	0.7	9	2	10 *	NW 3	W 5	NW 5
4	91.5	91.4	91.0	91.3	-2.7	-1.1	-7.9	-4.9	-1.0	-8.1	86	85	84	85	0.7	0.9	0.5	0.7	10 *	9 *	10 *	NW 5	WNW 7	NE 10
5	91.0	89.6	92.0	90.9	-14.4	-11.8	-14.3	-13.7	-7.9	-15.1	83	75	79	79	0.3	0.6	0.4	0.4	10	5	10	W 1	N 4	N 2
6	95.1	95.2	94.4	94.9	-17.1	-13.5	-15.4	-15.4	-12.8	-17.2	85	76	86	82	0.2	0.5	0.3	0.3	10	7 *	10 *	NW 4	NW 4	WSW 2
7	92.8	92.0	84.5	89.8	-21.1	-13.5	-17.3	-17.3	-12.9	-21.8	89	80	85	85	0.1	0.4	0.2	0.2	3	0	4	W 2	E 1	NW 3
8	64.4	65.0	71.3	66.9	-7.1	-4.7	-8.1	-7.0	-4.5	-20.3	91	88	87	89	0.3	0.5	0.4	0.4	10 *	10 *	10 *	W 8	W 6	NNW 8
9	81.8	86.8	92.3	87.0	-10.3	-7.7	-9.7	-9.4	-7.0	-10.6	91	84	81	85	0.3	0.5	0.5	0.4	10 *	8	10 *	NNW 7	N 3	NW 5
10	92.5	87.3	83.1	87.6	-14.5	-5.9	-6.4	-8.3	-3.8	-14.6	87	56	89	77	0.3	1.7	0.4	0.8	0	8	10 *	WNW 4	SW 6	W 8
11	84.8	87.7	92.1	88.2	-5.1	-0.6	-4.9	-3.9	-0.2	-6.8	88	68	86	81	0.5	1.9	0.6	1.0	8	3	0	W 4	NW 7	W 4
12	94.3	93.7	92.0	93.3	-4.5	1.3	-3.5	-2.6	2.6	-8.0	91	57	67	72	0.4	2.9	1.5	1.6	9	1	2	W 3	W 4	WNW 3
13	87.7	83.5	77.3	82.8	-2.0	1.0	-0.5	-0.5	1.0	-3.7	75	66	76	72	1.4	2.3	1.4	1.7	9	8	9	W 4	WSW 9	WSW 10
14	73.9	72.9	77.5	74.8	-1.6	2.4	-0.2	0.1	2.6	-2.1	75	61	98	78	1.3	2.9	0.1	1.4	4	0	10 *	WSW 8	SW 8	W 4
15	80.1	83.3	84.6	82.7	-0.9	-0.3	-3.0	-1.8	0.2	-3.5	87	74	86	82	0.7	1.6	0.7	1.0	8	10	9	WNW 2	NW 4	C 0
16	83.6	82.7	81.5	82.6	-6.3	-2.7	-3.1	-3.8	-2.5	-7.1	97	91	97	95	0.1	0.5	0.1	0.2	10 *	10 *	10 *	W 1	N 6	N 6
17	79.0	81.1	84.6	81.6	-4.5	-3.9	-2.7	-3.4	-2.7	-4.5	93	87	97	92	0.3	0.6	0.1	0.3	10 *	10	10 △	W 5	W 2	NNE 4
18	86.2	87.1	88.5	87.3	-4.4	-3.3	-4.3	-4.1	-2.5	-4.7	93	88	91	91	0.3	0.6	0.4	0.4	10 *	10 *	10 *	NE 6	NNE 6	N 7
19	89.4	90.6	93.3	91.1	-4.3	-4.1	-6.5	-5.4	-3.5	-6.7	98	89	91	93	0.1	0.5	0.3	0.3	10 ●	10	10 *	N 3	NE 6	NE 6
20	97.6	99.8	100.7	99.4	-7.9	-5.4	-10.8	-8.7	-4.4	-11.0	87	85	94	89	0.4	0.6	0.2	0.4	10	10	0	E 4	ESE 6	ENE 5
21	97.5	95.1	90.7	94.4	-6.4	-3.2	-4.2	-4.5	-2.8	-11.5	94	86	84	88	0.2	0.7	0.7	0.5	10	10	10	E 2	NE 2	NW 3
22	84.0	81.8	86.8	84.2	-6.2	-4.0	-9.4	-7.2	-3.3	-9.6	89	82	79	83	0.4	0.8	0.6	0.6	10 *	10 *	0	WNW 7	WNW 8	WNW 5
23	87.6	86.9	86.5	87.0	-8.8	-3.5	-7.0	-6.6	-3.4	-13.5	92	78	88	86	0.3	1.0	0.4	0.6	10	10	0	W 2	W 3	W 4
24	88.5	88.4	83.6	86.8	-9.3	-4.0	-9.6	-8.1	-3.4	-11.2	91	59	82	77	0.3	1.9	0.5	0.9	2	3	0	W 3	WSW 3	WSW 2
25	77.4	76.1	78.9	77.3	-4.4	-2.1	-7.2	-5.2	-1.1	-11.0	74	67	71	77	1.1	0.6	1.0	0.9	9	10 *	4	W 4	WNW 7	W 4
26	82.8	83.2	80.2	82.1	-12.7	-3.0	-5.8	-7.3	-3.2	-12.7	81	56	64	67	0.4	1.8	1.4	1.2	6	3	0	WNW 5	W 3	SW 3
27	72.8	68.6	72.1	71.2	-6.1	-1.9	-3.7	-4.8	-1.1	-6.5	73	60	77	70	1.0	2.1	0.9	1.3	8	10	9 *	W 3	SW 10	W 3
28	78.4	83.3	88.1	83.3	-7.5	-3.3	-10.1	-8.3	-4.7	-10.3	84	52	65	67	0.5	1.9	1.0	1.1	5	1	0	W 9	NW 10	WNW 3
29																								
30																								
31																								
M	86.0	86.0	86.6	86.2	-7.2	-4.0	-6.7	-6.2	-3.1	-9.6	88	76	84	83	0.5	1.2	0.6	0.8	8.2	7.1	6.7	4.2	5.4	4.6

Przemyśl $H_s = 237\,m$ $H_b = 238{,}9\,m$ $h_w = 18{,}2\,m$ *Styczeń - Janvier* 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	11	⤳ 0^00–6^20 (por. 18 m/sek), 11^20–13^30
2	7	0.9	9	✱° 19^10–24; = 10^30–24
3	5	6.9	10	✱° 0^00–17^45 ✱● 21^10–23^40; = 0^00–9^40 ≡° –15^50 ≡¹ –17^45 ≡° 18^30 – 24
4	5	6.7	15	✱° 2^15–21^40; ⸸° 17^45–24; = 0^00–24
5	7	0.2	20	✱° 12^40–15^40; ⸸° 0^00–7^25 10^25–15^40; = 0^00–13^0
6	8	0.1	21	⚥° 9^50–12^20 23^40–24; ⸸° 3^45–24
7	7	0.0	20	⚥° 0^00–15 ✱° –2^20 4^40–5^10 ✱¹ 8^05–35 ✱° 8^50 15^50 20^20–21^10 22^25; ⸸° 0^00–16^45; = 15^50–22^25
8	8	0.0	21	✱° 21^50–24
9	7	3.3	22	✱° 0^00–50 △° 6^20–7^10 8^50–9^10 ✱° 13^20–14^20–24; ⸸° 3^50–8^40; ⤳ 6^25–7^30
10	6	2.3	25	✱° 0^00–3^40 ●° –4^10 ✱° 13^10–10^20 20^20–21^40 22^40–23^10; = 10^10–15^40 ≡° –17^25 = –24
11	6	0.1	20	✱° 5^30–6^20 7^40–8^40; = 0^00–1^15 7^45–24; ⊔¹ 22–24
12	5	.	20	= 0^00–24; ⊔° 0^00–10; ⊕ ¹12^10–14^20 ◸° 16^40–22^50
13	6	.	20	= 0^00–24
14	7	.	19	= 6^40–9^40, 23^20–24
15	7	.	17	= 0^00–14^0, 13^50–24
16	5	.	17	= 0^00–24
17	7	.	16	⤳ 6^20–40, 21^10–24, por. miedzy do 23 m/sek 20^20–24; = 0^00–3^50
18	7	0.4	13	✱° 23^40–24; ⤳ 0^00–3^10 (por. do 22 m/sek); = 15^35–18^20
19	7	0.8	11	✱° 0^00–20; = 0^10–2^30 15^20–21^40 23^10–24; ⊔° 21–24; ◸ 2–4
20	7	5.3	16	✱° 4^25–5^50 ✱¹ –7^40 ✱° –8^05 △° –8^45 ✱¹ –9^10 ✱° –9^38 ●° 16^50–17^05 ✱° –20^15; ⸸° 5^50–9^40; ⤳ 5^40–7^10; = 0^00–9^40 16^02–25 ≡° –20^20 = –24; ⊔° 0^00–7; ◸ 1–3
21	6	0.3	21	●° 8^40–10^45 11^45–13^50 ✱● ° –14^15 ●° –15^35 16^40–17^20 19^40–20^10; = 0^00–21^00
22	6	0.3	19	= 1^00–24
23	4	0.4	17	△° 5^35–7^00 ◠° 7^40–8^50 ◠° –10^45 ●° 23^10–24; = 0^00–13^50 ≡° –16^45 ≡¹ –17^50 ≡² –18^45 ≡¹ –23^10 ≡° –24
24	3	1.2	17	●° 0^00–1^45 ◠° –10^01 ◠° △ –10^10 ◠° –10^20 ✱° –10^35 ✱¹ –11^01 ✱° –11^15 ●° 14^36–16^40 ◠° –24; ≡° 0^00–17^45 = –24
25	5	1.1	19	◠° 0^00–7^40 ◠¹ –8^35 ◠° –9^35 11^40–13^45 △° –14^40 ◠° 17^45–18^25 ◠¹ –19^10 ◠° –20^25 ✱° 21^45–23^10; = 0^00–7^40 ≡° 9^35 = –17^45 ≡° –20^25 = –24
26	3	.	19	✱° 0^20–3^20; = 0^00–24
27	6	.	19	= 0^00–24
28	6	.	19	= 0^00–24
29	7	0.0	19	●° 13^20–30; = 0^00–11^20
30	8	0.0	16	●° 13^20–30
31	5	21.6	13	●° 6^20–45, 7^40–10^35, 11^40–12^25 ✱● ° –13^40 ✱° –14^15 ✱¹ –15^45 ✱° –24; = 7^20–16^35 ≡° –19^20 = –24
Σ	-	51.9	-	

Luty - Février

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	6	0.7	26	✱° 0^00–2^45 ✱¹ –5^10 ✱° –7^20 8^10–10^20 40–13^11 13^20–14^10 21^50–24; = 0^00–14^10 17^40–24
2	7	0.4	27	✱° 0^00–52 7^10–8^25 ✱¹ –9^00 ✱° –9^35 ⚥° 9^45–12^35 ✱¹ –13^10 ⚥° –14^02 ⚥¹ –14^15 ⚥° –14^40 15^40–17^25 20^20–23^10; ⸸° 11^45–17^40; = 0^00–2^30
3	8	2.4	24	⚥° 12^20–22^2 4^25–5^10 6^50–7^15 8^45–9^10 ✱° 14^45–16^20–22^40; = 14^40–22^35
4	6	0.9	28	✱° 2^40–8^25 11^20–12^15 13^10–19^20 20^15–21^10; ⸸° 10^45–22^35; ⤳ 20^15–21^30
5	7	0.2	30	✱° 3^40–6^10 ↔ 8^15–9^05 ⚥° 13^18–30 13^35–14^15 15^09–15 15^50–16^40 ✱° 19^50–20^15 21^30–22^45; = 4^50–11^20 17^40–24
6	6	0.2	31	✱° 5^30–6^10 7^05–14^10 15^50–16^20 19^40–21^20 23^05–24; ⸸° 4^05–6^45; = 0^00–24
7	6	1.4	30	✱° 0^00–2^40; = 0^00–24; ⊔° 4–9
8	3	4.6	32	✱° 1^40–3^10–10^40 ✱¹ –16^40 ✱° –18^25 ✱¹ –20^20 ✱° –24; ⸸¹ 5^40–24; ⤳ 8^45–11^30 (por. 16 m/sek 8^51), 14^50–24; = 0^00–30 8^40–24
9	6	0.2	42	✱° 0^00–10^40 14^03–15^01 ✱¹ –15^30 ✱° –16^10 ✱¹ –16^36 ✱° –16^42 19^50–22^40; ⸸¹ 0^00–6^50; ⤳ 0^00–4^10; = 0^00–16^40 17^45–24
10	8	1.7	44	✱° 19^40–24; ⸸° 16^40–24; ⤳ 16^25–24; = 0^00–2^50 6^50–9^20 19^40–24
11	8	.	45	✱° 0^00–3^40 4^45–5^10; ⸸° 0^00–3^40; = 0^00–11^25
12	6	.	43	= 5^30–13^30
13	7	.	37	⤳ 11^40–14^10 20^20–22^10 (por. 16 m/sek 20^45, por. 18 m/sek 20^50)
14	7	2.2	33	✱° 17^40–18^15 19^20–20^10 ✱¹ –21^20 ✱° –22^25; ⤳ 10^30–12^10 (por. 17 m/sek 10^42); = 22^10–23^10
15	7	0.6	34	✱¹ 9^30–10^15 ✱° –11^40; = 4^40–6^45 7^30–12^20 18^40–24; ◸ 21–24
16	5	4.6	35	✱° 4^35–17^45 18^05–24; ⸸° 17^50–24; = 0^00–24; ◸ 0^00–2
17	7	4.4	44	✱° 0^00–9^35 9^50–10^15 11^02–20–12^12 17^45–18^05 △° 20^20–21^40 ✱° –24; ⸸° 0^00–7^40 21^40–24; = 0^00–10^45 15^30–24
18	6	6.7	51	✱° 0^00–24; ⸸° 0^00–24; = 0^00–24
19	5	3.6	58	✱° 0^00–3^40 △° –4^35 ◠° 4^40–6^45 △° –8^15 ✱° –10^35 △° –12^10 13^05–15^30 ✱° –24; ⸸° 0^00–5^45 17^50–22^45; = 0^00–24
20	6	.	61	✱° 0^00–40 1^40–4^15; = 0^00–24
21	5	1.1	59	△° 8^40–11^20; ⸸° 22^50–24; = 0^00–24
22	5	1.9	60	✱° 3^20–6^10 7^20–8^20 ✱¹ –17^45 ✱° –13^20 ✱¹ –14^30 ✱° –15^35 ✱¹ –16^05 ✱° –16^10; ⸸° 0^00–19^35; = 0^00–16^10
23	6	1.7	61	✱° 2^20–3^10 13^10–30 ✱¹ –13^45 ✱² –14^10 ✱° –15^40 16^20–18^15 23^40–24; = 2^30–3^10 6^50–8^10 11^40–24; ⊕ 8^40–11^20
24	7	.	62	✱° 0^00–5^15; = 0^00–11^40 18^20–24
25	6	2.5	59	✱° 7^42–13^14 14^10–15^00 ✱¹ –15^16 ✱° –15^20 ✱¹ –15^25 ✱² –16^05 ✱¹ –16^14 ✱² –16^30 ✱° –16^50 ✱² –17^00 ✱¹ –17^04 ✱° –18^18; ⸸° 8^40–12^45 15^50–16^45; = 0^00–5^20 6^40–19^20
26	7	.	60	= 6^20–8^15
27	8	0.4	58	✱° 20^20–23^20; ⸸° 2^40–4^45 20^00–24; ⤳ 0^00–4^43 8^50–14^10
28	8	0.0	59	✱° 2^35–5^15 6^10–20 7^25–50 8^05–45 ⚥° 9^10–10^20; ⸸° 0^00–3^30 ⸸¹ –13^50 ⸸° –15^50; ⤳ 3^30 12^20
29				
30				
31				
Σ	-	42.4	-	

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ *Marzec – Mars 1965*

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE N_{ok} I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_{cr} I	II	III
1	86.2	83.5	78.9	82.9	-7.7	1.7	0.5	-1.2	2.3	-17.2	70	54	81	68	1.0	3.2	1.1	1.8	9	10	4	E 1	SW 7	SW 8
2	73.1	70.1	67.2	70.1	2.1	7.1	3.5	4.0	8.1	-0.4	71	59	93	74	2.0	4.2	0.5	2.2	8	8	10 •	SE 2	S 4	NNE 2
3	62.1	65.2	68.9	65.4	4.7	7.9	4.1	5.2	8.6	1.8	84	59	67	70	1.3	4.3	2.7	2.8	8	2	0	SW 4	SW 15	NNW 5
4	73.9	73.4	78.6	76.0	-2.3	1.0	-1.1	-0.9	4.1	-3.1	85	70	71	75	0.8	2.0	1.7	1.5	8	8 ⚹	10	W 2	W 3	WSW 6
5	79.5	80.3	84.0	81.[illegible]	-2.4	4.6	1.1	1.1	5.1	-3.0	74	54	64	64	1.3	3.9	2.3	2.5	4	9	10	NW 2	WSW 6	NW 3
6	87.3	87.3	89.5	88.0	-3.1	-0.1	-2.7	-2.2	1.1	-3.3	84	80	97	87	0.8	1.2	0.1	0.7	9	10	10 ⚹	ENE 1	ESE 7	E 7
7	92.4	94.7	96.2	94.4	-3.9	-3.2	-3.8	-3.7	-2.6	-4.2	92	92	89	91	0.4	0.4	0.5	0.4	10	10 △	10	NE 5	NE 4	ENE 3
8	95.6	95.1	94.9	95.2	-6.4	-4.1	-4.3	-4.8	-3.1	-7.0	91	82	94	89	0.3	0.8	0.3	0.5	10	10	10 △	NE 5	ESE 4	ENE 2
9	95.3	95.5	95.8	95.5	-5.0	-1.9	-5.6	-4.5	-0.7	-5.9	93	69	87	83	0.3	1.7	0.3	0.8	10 △	8	0	NW 1	N 1	WNW 2
10	96.8	99.5	102.1	99.3	-6.3	-1.7	-5.3	-4.6	-0.7	-9.8	89	82	82	84	0.4	1.0	0.7	0.7	10 ⚹	4	0	WNW 3	WNW 3	W 5
11	103.0	103.5	102.8	103.1	-9.1	1.2	-3.4	-3.7	2.6	-10.4	88	61	76	75	0.4	2.6	1.1	1.4	0	0	0	W 5	W 2	WNW 2
12	101.8	100.2	99.5	100.5	-8.5	3.0	-1.9	-2.3	3.5	-11.1	92	58	79	76	0.3	3.2	1.1	1.5	2	1	0	W 1	E 5	C 0
13	99.3	99.1	98.9	99.1	-9.5	3.8	-1.0	-1.9	4.5	-10.1	98	46	68	71	0.1	4.3	1.8	2.1	1	2	0	W 2	E 5	C 0
14	98.9	97.6	96.9	97.8	-5.5	8.8	3.5	2.6	10.4	-6.3	92	49	76	72	0.3	5.7	1.8	2.6	0	0	0	C 0	C 0	E 2
15	96.0	95.5	95.1	95.5	-2.7	12.3	6.6	5.7	12.5	-3.1	89	46	62	66	0.6	7.8	3.6	4.0	3	2	9	W 2	SW 8	SW 3
16	93.6	90.9	89.6	91.4	4.7	12.9	6.9	7.8	13.6	4.5	78	58	68	61	1.9	9.3	3.1	4.8	5	2	6	C 0	SW 9	S 1
17	88.5	87.2	84.6	86.8	2.4	6.7	4.9	4.7	7.0	1.6	93	75	81	83	0.6	2.4	1.7	1.6	10	10	10	WSW 2	E 1	N 2
18	82.0	81.4	80.9	81.4	2.1	10.1	3.2	4.6	10.6	1.4	100	73	97	90	0.0	3.4	0.3	1.2	7 ≡	3	0	W 2	NE 2	E 1
19	80.7	80.7	83.7	81.7	-1.9	13.5	3.1	4.4	14.2	-2.7	96	48	93	79	0.2	8.1	0.5	2.9	0	3	1	E 1	W 4	C 0
20	86.7	89.1	89.6	88.5	0.9	3.8	2.8	2.6	4.0	0.5	98	93	89	93	0.1	0.5	0.8	0.5	10	10	10	C 0	N 2	C 0
21	86.3	83.2	79.2	82.9	1.7	11.9	8.1	7.4	12.8	0.8	92	48	76	72	0.5	7.2	2.5	3.4	1	7	10 •	WSW 1	SW 4	W 4
22	79.0	84.6	87.8	83.8	6.5	0.0	-1.5	0.9	8.1	-1.7	87	98	96	94	1.3	0.1	0.2	0.5	10	10 ⚹	0	W 2	NW 3	W 2
23	88.6	86.0	82.1	85.6	-5.3	4.0	2.0	0.7	4.6	-6.1	93	64	78	78	0.3	2.9	1.6	1.6	0 ≡	2	0	WSW 1	SE 4	S 3
24	79.2	78.1	78.8	78.7	0.8	7.6	2.9	3.6	8.1	0.6	86	72	89	82	0.9	2.9	0.8	1.5	10	6	10	SE 4	E 5	C 0
25	79.8	83.1	86.9	83.3	3.1	6.6	3.3	4.1	8.4	1.9	98	81	90	90	0.1	1.8	0.7	0.9	10 ≡	9	0	C 0	W 7	W 2
26	88.4	88.1	88.0	88.2	1.7	1.9	2.4	2.1	3.8	-0.1	96	96	98	97	0.3	0.3	0.2	0.3	10	10 ⚸	10	W 2	C 0	ESE 2
27	91.2	95.4	100.6	95.7	2.1	3.9	4.0	3.5	4.5	1.8	100	98	95	98	0.0	0.2	0.4	0.2	10 • ≡	10 •	10	E 3	NE 3	NNE 5
28	103.9	103.8	103.0	103.6	2.3	8.7	4.2	4.8	9.3	2.0	91	56	77	75	0.6	4.9	1.8	2.4	9	4	0	N 1	E 5	E 1
29	101.3	100.5	98.8	100.2	0.2	8.4	6.4	5.4	8.9	-1.3	90	53	72	72	0.6	5.1	2.7	2.8	10	10	10	W 2	E 2	C 0
30	93.4	89.1	90.0	90.8	6.2	15.7	7.3	9.1	16.3	5.0	97	59	73	76	0.3	7.2	2.7	3.4	8	4	8	W 4	W 7	N 8
31	93.7	91.4	91.0	92.0	0.3	4.0	1.9	2.0	7.3	-0.6	69	75	87	77	1.9	2.0	0.9	1.6	1	8	10	WNW 8	NNW 8	NW 8
M	89.0	88.9	89.2	89.0	-1.2	5.2	1.7	1.8	6.4	-2.8	89	67	82	79	0.6	3.4	1.3	1.8	6.5	6.2	5.4	2.2	4.3	2.9

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DNI	CIŚNIENIE I	II	III	Dies	TEMPERATURA I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. I	II	III	Dies	NIEDOSYT WILGOTNOŚCI I	II	III	Dies	ZACHMURZENIE I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU I	II	III
1	94.2	97.6	98.4	96.7	0.0	1.5	0.0	0.4	2.5	-0.6	96	72	84	84	0.2	1.9	1.0	1.0	9	8	8	NNW 7	N 7	W 5
2	93.0	91.0	93.1	92.4	1.4	7.1	5.5	4.9	7.7	-0.6	79	60	63	67	1.4	4.0	3.3	2.9	9	10	2	W 5	N 8	N 7
3	93.0	90.3	86.2	89.8	0.7	7.5	4.6	4.4	9.6	-0.2	69	54	84	69	2.0	4.8	1.4	2.7	3	9	0	W 1	W 4	C 0
4	86.5	85.4	82.9	84.9	1.9	9.3	7.7	6.6	11.6	1.7	80	59	73	71	1.4	4.8	2.8	3.0	10	9	9	NW 7	WNW 6	W 1
5	84.0	87.8	91.9	87.9	5.0	5.7	3.5	4.4	8.8	3.5	97	82	90	90	0.3	1.7	0.8	0.9	0	10	9	N 1	NE 5	E 1
6	92.4	91.9	89.1	91.1	0.3	5.9	3.3	3.2	7.5	-0.2	88	73	83	81	0.7	2.5	1.3	1.5	10	5	0	SE 2	E 6	E 3
7	86.1	84.7	84.9	85.2	0.4	15.5	10.6	9.3	16.6	-1.3	96	45	70	70	0.3	9.7	3.8	4.6	0	9	10	C 0	W 7	W 5
8	84.4	83.7	84.0	84.0	6.8	12.3	8.3	8.9	13.9	6.1	94	74	89	86	0.6	3.7	1.3	1.9	10 •	10	10	SW 1	E 1	ENE 3
9	83.5	83.8	83.9	83.7	6.3	6.3	1.7	4.0	8.3	1.7	86	81	92	86	1.2	1.8	0.5	1.2	10	10	10	ESE 7	E 10	E 12
10	84.3	85.9	87.2	85.8	0.6	1.3	0.1	0.5	1.8	-0.1	84	81	78	81	1.0	1.3	1.4	1.2	10	10	10	ESE 10	SE 8	SE 10
11	86.7	87.1	87.6	87.1	-0.9	2.4	0.5	0.6	2.9	-1.8	79	73	80	77	1.2	2.0	1.2	1.5	9	10	10	SE 10	SE 10	ESE 9
12	87.5	87.3	88.2	87.7	-0.1	8.3	2.2	3.2	8.6	-0.4	86	60	78	75	0.9	4.5	1.6	2.3	10	3	9	SE 5	ESE 6	SE 6
13	86.5	86.2	86.9	86.5	1.6	7.0	3.2	3.8	9.3	0.9	89	70	71	77	0.8	3.0	2.2	2.0	10	5	9	SE 3	SE 7	SE 7
14	86.8	88.8	90.7	88.8	1.0	4.9	4.1	3.5	6.3	0.6	87	76	80	81	0.9	2.1	1.6	1.5	10	10	10	SE 6	E 7	SE 6
15	90.9	91.0	89.5	90.3	2.3	4.7	4.3	4.0	5.9	1.9	86	74	80	80	1.0	2.1	1.6	1.6	10	10	10	ESE 5	ESE 4	ESE 4
16	85.7	84.0	83.4	84.4	2.6	13.1	7.9	7.9	13.4	0.9	91	56	76	74	0.7	6.7	2.3	3.3	8	9	9	SSE 3	SE 3	SE 6
17	83.9	83.6	81.8	83.1	3.5	12.7	7.8	8.0	13.1	2.4	95	58	78	77	0.4	6.2	2.4	3.0	5	2	0	C 0	E 3	ENE 2
18	73.9	74.2	75.4	75.2	5.5	15.5	10.7	10.6	16.7	1.5	83	36	69	63	1.5	11.3	4.0	5.6	1	9	10	C 0	SW 6	W 2
19	75.2	74.0	74.7	74.6	6.3	13.6	8.7	9.3	14.9	5.4	76	45	80	67	2.2	8.6	2.2	4.3	9	8	0	SE 3	SE 7	ESE 8
20	74.4	74.9	75.2	74.8	7.0	10.5	9.6	9.2	10.8	5.8	85	70	82	79	1.4	3.8	2.2	2.5	10	10	10	SE 3	SE 8	ESE 5
21	73.2	71.8	69.3	71.4	8.7	9.3	8.3	8.6	9.8	7.9	89	83	93	89	1.2	1.7	0.8	1.2	10	10	10	ESE 5	ESE 7	E 8
22	64.3	66.4	69.1	66.7	5.1	6.4	6.2	6.0	8.6	4.7	90	91	88	90	0.9	0.9	1.2	1.0	10 •	10 •	10	W 8	SW 3	C 0
23	68.0	68.0	70.8	68.9	4.9	9.3	6.7	6.9	10.0	4.3	97	64	78	80	0.3	4.3	2.2	2.3	10	9	10 •	W 1	WSW 6	W 7
24	74.1	76.0	78.9	76.3	6.8	9.8	7.1	7.7	10.7	5.0	77	63	80	73	2.3	4.5	2.1	3.0	9	9	1	SSW 2	W 6	WNW 2
25	82.2	82.7	83.2	82.7	5.1	13.7	9.0	9.2	15.3	2.8	89	46	67	67	1.0	8.4	3.8	4.4	0	5	0	W 1	SW 4	E 1
26	82.9	81.0	81.0	81.6	7.2	15.3	7.3	9.3	16.3	2.3	83	48	96	76	1.8	9.0	0.4	3.7	2	8	4	ESE 1	SE 3	E 2
27	77.1	75.7	75.8	76.2	6.6	12.7	9.4	9.3	13.3	5.3	98	67	89	85	0.1	4.9	1.3	2.1	10 •	6	0	SW 3	E 3	E 3
28	75.1	75.4	78.7	76.4	7.4	11.3	8.8	9.1	13.0	5.2	94	84	82	87	0.6	2.2	2.0	1.6	8	10 •	8	E 2	SE 5	SW 2
29	81.0	80.5	81.0	80.8	6.1	14.7	10.5	10.4	15.3	2.8	91	57	56	68	0.8	7.2	5.6	4.5	2	6	0	SW 2	E 3	NE 3
30	82.9	84.6	85.9	84.5	7.0	10.9	7.0	8.0	11.5	4.4	96	63	84	81	0.4	4.7	1.6	2.2	10 •	7	1	WNW 7	SW 3	NW 3
31																								
M	82.5	82.3	82.8	82.7	3.9	9.3	6.2	6.4	10.3	2.4	88	66	80	78	1.0	4.3	2.0	2.3	7.5	8.2	6.3	3.8	3.7	4.3

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	8	.	55	≫ 11^{40}–14^{10}, 19^{20}–20^{40}
2	8	6.1	55	● ° 10^{35-45}, 19^{40}–21^{45}, 23^{35}–24, ≫ 13^{20}–15^{30}
3	8	6.7	46	● ° 0^{00}–2^{20} * ° 23^{35}–24; ≫ 7^{15}, 16^{10}; = 14^{00}–20^{20}, 22^{30}–24
4	7	0.0	46	* ° 0^{00-10} * ¹ –1^{40} * ° –3^{35}, 12^{00-12}, 12^{25}–13^{15}; = 0^{00}–9^{20}
5	7	.	45	= 5^{30}–9^{20}
6	6	5.6	57	* ° 15^{50}–24; ⊥ * ° 19^{45}–24; = 5^{10}–24
7	6	0.2	42	* ° 0^{00}–2^{40} △ ° 7^{40}–18^{15}; ⊥ * ° 0^{00}–1^{50}; = 0^{00}–24
8	7	0.5	42	* ° 7^{40}–12^{20}, 13^{16-38}, 14^{00-21}, 15^{14}–17^{18} △ ° 19^{35}–21^{20}; = 0^{00}–12^{10}, 15^{40}–24
9	7	0.3	45	△ ° 6^{15}–7^{40} * ° –9^{45}; = 0^{00}–12^{10}, 13^{40}–15^{10}, 17^{20}–24
10	6	0.0	42	* ° 3^{40}–5^{45}, 6^{20-40}, 8^{10}–9^{10} ⊛ ° 12^{05-13}, 13^{21-28}; = 0^{00}–15^{20}; ⌴ ¹ 1–6
11	7	.	42	= 0^{00}–11^{50}
12	6	.	41	= 5^{30}–24
13	7	.	40	= 0^{00}–12^{10} ∞ –14^{40} = 16^{40}–24; ⌴ ¹ 2–7
14	7	.	39	= 0^{00}–4^{20}, 5^{30}–11^{40}; ⌴ ° 2–7
15	8	.	35	≫ 11^{00-30}; = 5^{15}–9^{20}; ⌴ ° 3–7
16	8	0.0	30	≫ 12^{24}–14^{20}; = 6^{10}–8^{40}
17	6	1.6	21	● ° 6^{58}–7^{10}, 8^{00}–9^{20}, 10^{25}–11^{10}, 12^{45}–15^{10}–16^{15}, 17^{35}–19^{10}, 22^{46}–24; = 6^{20}–24
18	6	.	18	● ° 0^{00}–2^{20}; = 0^{00}–5^{40} ≡ ° –6^{30} ≡ ¹ –8^{15} ≡ ° –8^{50} = –24
19	7	.	14	= 0^{00}–12^{15}, 16^{50}–24; ⌴ ° 1–7
20	5	0.4	pł.	● ° 8^{40}–10^{35}; = 0^{00}–24
21	7	0.4	pł.	● ° 19^{45}–21^{10}, 22^{15}; = 0^{00}–5^{40} 7^{36}–9^{10}; ⊕ ¹ 8^{30}–10^{40}
22	3	2.7	pł.	● ° 8^{25-40} * ° –9^{45} ● ° –10^{10} * ° –10^{50} * ¹ –11^{20} * ° –12^{20} * ² –12^{50} * ¹ –13^{01} * ² –13^{15} * ¹ –13^{40} * ° –13^{55}; ≫ 8^{45}–11^{10}; = 5^{20}–14^{30}; ⌴ ° 23–24
23	8	.	pł.	= 3^{40}–4^{45} ≡ ° –8^{25} = –9^{35}; ⌴ ° 0^{00}–4 ⌴ ¹ 5–8
24	7	2.7	pł.	● ° 22^{20}–24; = 5^{40}–7^{30}, 17^{20}–24
25	6	1.0	.	● ° 0^{00}–6^{15}, 7^{40}–8^{20}, 9^{03}, 11^{27}–12^{06} ⊛ ° 15^{30-34}; = 0^{00}–6^{25} ≡ ° –8^{38} = –10^{26}, 11^{20}–12^{45}, 18^{08-35}, 19^{10}–24
26	4	7.7	.	● ° 4^{45}–6^{10}, 8^{15}–9^{10} * ¹ –9^{35} * ° –11^{05} * ² –11^{15} * ¹ –11^{30} * ° –11^{40} * ° 12^{10}–13^{15} ● ° –14^{05}, 22^{40}–23^{20}; = 0^{00}–24; ⌴ ° 2–4
27	5	3.4	.	● ° 2^{25}–3^{10}, 5^{10}–13^{25} ● ° 17^{35}–18^{45} ● ° –19^{50}; = 0^{00}–1^{45} ≡ ° –4^{40} ≡ ¹ –8^{50} = –24
28	7	.	.	= 0^{00}–9^{20}
29	7	0.3	.	= 4^{25}–9^{40}; ⌴ ° 2–6
30	7	.	.	● ° 2^{15}–4^{20}; = 2^{20}–12^{20}
31	8	4.2	.	△ ° 9^{35-45} * ⊛ ° 11^{25-40}, 14^{01-10} △ ¹ 14^{45-54} △ ° 15^{04-10} △ ² 16^{01-13} △ ° 16^{16-20} △ ² 17^{12-21} ⊛ ° 18^{14-25}, 19^{33}–20^{15}, 21^{05}–22^{40} ⊛ ° 23^{10-45}
Σ	–	44.4	–	

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1	8	0.0	2	△ ¹ 0^{20-24} △ ° –1^{20} ⊛ ° 3^{40}–4^{00}, 9^{35-40}, 10^{25-35}, 11^{02-15}, 11^{25-30}, 14^{00-10}
2	7	.	1	* ° 4^{20}–5^{15}
3	8	.	.	
4	6	2.0	.	= 2^{40}–12^{45}, 17^{50}–24
5	6	.	.	● ° 0^{10}–1^{45} ● ¹ 4^{02-40}; = 0^{00}–7^{40} ∞ 11^{30}–12^{20} = –21^{40}
6	7	.	.	= 4^{20}–5^{25}
7	7	0.1	.	= 0^{40}–9^{40}; ⌴ ° 1–7
8	6	0.3	.	● ° 8^{30}–7^{20} ⊛ ° 16^{10}–18^{05}; = 1^{40}–24
9	7	0.0	.	≫ 9^{30}–24 (por. do 18 m/sek 13^{45}–18^{35}); = 0^{00}–9^{20}, 14^{30}–24
10	8	.	.	△ ° 3^{50}–4^{15}; ≫ 0^{02}–24; = 0^{00}–5^{30}
11	7	.	.	≫ 0^{00}–22^{00} (por. 17 m/sek 6^{40})
12	8	0.0	.	≫ 16^{30}–18^{10}
13	7	.	.	● ° 3^{45}–6^{20}
14	7	.	.	= 7^{20}–10^{40}
15	7	.	.	
16	7	0.4	.	⊛ ° 12^{25-35}, 13^{43}, 14^{15}; = 3^{40}–10^{20}
17	7	.	.	= 4^{30}–9^{15}, 23^{30}–24; ⌓ ¹ 2–7 ⌓ ° 22–24
18	8	.	.	≫ 11^{20}–12^{10}; = 0^{00}–7^{35}; ⌓ ¹ 0^{00}–1 ⌓ ² 2–7; ⊕ ° 12^{10}–16^{10}
19	7	.	.	
20	8	0.1	.	● ° 7^{15}–8^{10}; = 18^{40}–19^{30}
21	7	17.4	.	● ° 16^{00}–18^{05}, 21^{40}–23^{30} ● ¹ –24; = 23^{20}–24
22	8	8.5	.	● ¹ 0^{00}–1^{15} ● ° –7^{40}, 8^{10}–15^{16}; = 0^{00}–6^{10}
23	8	0.2	.	● ° 2^{40}–5^{10}, 6^{15} ⊛ ° 12^{50-55}, 13^{16-24}, 14^{25-31}, 15^{55}–16^{02}, 20^{25}–21^{10}
24	8	1.6	.	⊛ ° 8^{35-53} ⊛ ¹ 0^{10-25} ⊛ ° 9^{30}–10^{03}, 14^{27-35}
25	7	0.0	.	⊛ ° 16^{32-35}; K ° N 16^{25}–17^{10} NE; ⌓ ¹ 2–8
26	8	13.2	.	⊛ ° 10^{42-48}, 11^{05-10}, 11^{50-54}, 12^{46}–13^{04}, 13^{17-22}, 13^{41}–14^{20}, 14^{22}–15^{02}, 15^{42}–16^{22}; K ° 13^{26}–15^{04}, 16^{01-40}; = 2^{30}–7^{20}, 17^{35}–18^{20} ≡ ° 23^{40}–24; ⌓ ° 1–7
27	8	2.9	.	⊛ ° 1^{35-45} ● ° 2^{50}–6^{10} ● ¹ –6^{45} ● ° –7^{30}, 8^{05} ⊛ ° 11^{20-30}, 14^{10}–15^{10}, 15^{25}–16^{05}, 16^{50-55}, 17^{22-33}; ≡ ° 0^{00}–1^{45} = –8^{10}
28	6	1.6	.	● ° 10^{30}–11^{25}, 12^{15-30} ● ¹ –13^{00} ⊛ ° 13^{30-35}; = 3^{20}–11^{30}, 12^{20}–13^{10}
29	8	0.7	.	= 4^{20}–7^{30}; ⌓ ² 2–7
30	8	8.8	.	● ° 2^{40}–3^{20} ● ° –7^{05} ● ¹ –7^{10} ● ° –7^{48} ⊛ ² 10^{17-20} ▲ ⊛ ² –10^{27} ⊛ ² –10^{30} ⊛ ° –11^{00}, 11^{16-35}, 13^{05-45}, 15^{12}–16^{06}; K ° 10^{40}–(K) 11^{35}–12^{05} (K) ° 14^{22} K ° 15^{10-25}, ≫ [illegible]
31				[30.IV. = 2^{30}–4^{40}, 8^{10}–10^{05}
Σ	»	97.8	.	

Przemyśl — φ = 49°48' — λ = 22°46' — Maj – Mai 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	86.0	86.0	85.5	85.8	6.9	11.7	8.9	9.1	12.3	5.3	75	33	44	51	2.4	9.2	6.3	6.0	0	5	0	NW 5	NW 8	NW 5
2	88.2	89.3	90.0	89.2	2.4	6.7	4.0	4.3	8.9	1.7	77	54	50	60	1.7	4.5	4.0	3.4	2	8	9	NW 4	NNE 5	N 3
3	89.0	89.3	90.6	89.6	1.1	4.1	2.9	2.8	7.3	-2.0	79	66	62	69	1.4	2.8	2.8	2.3	6	8	1	WSW 3	N 6	NE 3
4	92.4	91.2	88.0	90.5	0.7	7.5	4.7	4.4	9.1	-2.2	80	41	67	63	1.3	6.1	2.8	3.4	0	2	0	WSW 2	E 2	SE 2
5	83.2	82.2	78.8	81.4	4.3	5.8	6.4	5.7	7.3	-0.1	76	92	97	88	2.0	0.7	0.3	1.0	5	10 •	10 •	C 0	S 2	SE 3
6	76.9	78.6	81.3	78.9	5.8	9.7	9.0	8.4	10.1	4.4	98	87	89	91	0.1	1.6	1.3	1.0	10 =	10 •	10	C 0	N 3	NNW 3
7	84.0	85.3	87.0	85.4	7.5	10.7	6.9	8.0	11.6	6.4	83	62	84	76	1.8	4.9	1.6	2.8	8	8	1	N 3	NW 5	NW 2
8	86.5	85.6	86.8	86.3	3.6	14.9	12.4	10.8	16.1	0.8	100	43	74	72	0.0	9.6	3.7	4.4	0	2	10	SW 2	E 5	NW 3
9	87.3	84.5	78.2	83.3	10.8	17.0	13.7	13.8	17.5	9.4	80	58	72	70	2.6	8.1	4.4	5.0	3	9	10	WSW 3	W 5	C 0
10	76.6	76.0	76.2	76.3	9.5	12.5	7.9	9.4	14.9	7.4	70	59	90	73	3.6	6.0	1.0	3.5	10	4	9	WNW 4	W 5	WSW 3
11	76.9	79.4	83.4	79.9	7.5	9.6	7.6	8.1	10.9	5.7	87	75	93	85	1.4	3.0	0.7	1.7	10	8	5	C 0	SE 2	N 3
12	86.3	88.7	89.3	88.1	8.9	14.8	13.2	12.5	15.3	7.2	85	52	62	66	1.7	8.0	5.8	5.2	10	10	10	NE 1	E 3	N 7
13	89.9	90.4	90.0	90.1	9.1	13.0	11.8	11.4	15.4	8.9	88	71	67	75	1.4	4.3	4.5	3.4	10	10	8	NNE 5	NNW 4	N 4
14	88.1	86.4	85.2	86.6	8.9	14.6	11.2	11.5	16.4	5.0	75	43	74	64	2.9	9.4	5.4	5.2	0	9	9	W 4	N 4	NW 1
15	84.3	83.4	83.8	83.8	10.7	14.7	11.2	12.0	16.2	7.7	86	65	85	79	1.8	5.8	2.0	3.2	9	8	8	W 2	W 5	C 0
16	83.3	83.2	81.9	82.8	8.9	13.0	12.2	11.6	15.7	5.8	96	89	95	93	0.5	1.6	0.7	0.9	10	10 •	9	E 1	ESE 2	E 1
17	82.0	81.9	81.5	81.8	14.4	20.9	17.9	17.8	23.3	10.2	88	54	65	69	2.0	11.4	7.3	6.9	3	8	1	W 3	W 6	SSE 2
18	78.5	80.5	80.6	79.9	20.9	25.5	15.7	19.4	26.2	15.5	59	51	95	68	10.2	16.0	0.9	9.0	8	8	1	SW 7	W 6	SW 1
19	75.8	76.2	77.4	76.5	19.3	24.8	19.5	20.8	27.8	10.9	67	36	49	51	7.4	19.9	11.6	13.0	5	9	4	WSW 8	SW 7	NW 4
20	85.4	90.4	94.8	90.2	6.8	3.9	3.6	4.5	19.5	3.3	94	92	98	95	0.6	0.7	0.1	0.5	10 •	10 •	0	N 6	NNW 5	W 2
21	98.9	99.1	99.8	99.3	3.6	11.7	9.1	8.4	13.1	0.8	98	46	61	68	0.1	7.4	4.6	4.0	4	4	2	SW 2	NE 2	C 0
22	100.1	98.1	94.7	97.6	5.3	13.5	10.6	10.0	14.3	2.7	95	65	91	83	0.4	5.7	1.2	2.4	7	10	10 •	C 0	SE 7	E 7
23	91.9	91.2	92.0	91.7	10.3	14.0	10.9	11.5	14.3	9.1	85	71	83	80	1.9	4.6	2.2	2.9	10	10	10	E 8	E 8	SE 10
24	89.8	89.8	89.0	89.5	11.0	14.3	13.9	13.3	17.6	9.0	80	84	89	84	2.6	2.5	1.8	2.3	9	9	4	SE 5	ESE 4	SSW 1
25	88.4	87.7	88.4	88.2	12.5	17.5	12.1	13.6	18.5	9.8	93	65	96	85	1.0	7.0	0.5	2.8	5	9	10	WSW 1	SW 1	SW 1
26	88.4	88.9	88.9	88.7	11.9	16.3	11.8	13.0	16.9	11.3	93	74	91	86	1.0	4.7	1.1	2.3	10	9	1	WNW 3	W 5	W 1
27	88.5	87.1	85.5	87.0	11.3	17.5	15.8	15.1	19.4	7.8	90	61	70	74	1.3	7.9	5.3	4.8	2 ≡	7	10	C 0	E 2	NE 3
28	83.5	82.2	79.6	81.8	12.7	19.5	16.1	16.1	20.9	10.9	89	67	86	81	1.6	7.5	2.5	3.9	10	9	10	E 1	S 1	NE 1
29	76.7	75.7	75.8	76.1	13.8	19.7	16.5	16.6	21.3	12.8	94	51	57	67	0.9	11.1	8.2	6.7	9	6	10	C 0	WSW 9	W 6
30	75.8	79.8	82.1	79.2	9.3	11.9	9.9	10.2	16.5	8.4	95	67	74	79	0.6	4.6	3.1	2.8	10 •	8	0	NW 7	NW 4	C 0
31	84.3	84.0	83.4	83.9	7.1	17.5	14.4	13.4	18.6	2.9	94	61	91	82	0.6	7.7	1.4	3.2	9	8	10 •	ESE 1	ESE 3	SE 3
M	85.4	85.6	85.5	85.5	8.9	13.8	11.0	11.2	15.9	6.3	86	62	78	75	1.9	6.6	3.1	3.9	6.6	7.9	6.2	2.9	4.3	2.7

Czerwiec – Juin

1	81.1	81.9	82.6	81.9	15.3	21.5	16.2	17.3	22.7	12.3	86	53	68	69	2.4	12.0	6.0	6.8	9	10	1	SW 4	SW 4	SW 2
2	84.6	85.3	89.6	86.5	15.7	17.9	10.5	13.6	18.4	10.3	72	62	88	74	5.0	7.8	1.5	4.8	0	7	10 •	NW 2	N 5	NNW 5
3	91.2	91.6	90.6	91.1	11.2	18.2	14.6	14.6	19.3	6.7	79	44	69	64	2.8	11.6	5.2	6.5	1	3	10	WNW 4	C 0	C 0
4	90.7	89.3	87.4	89.1	14.3	22.0	16.4	17.3	22.3	8.5	75	49	82	68	4.5	13.6	3.2	7.1	1	10	5	E 2	ESE 8	E 4
5	85.2	81.7	78.6	81.8	13.0	15.4	15.4	14.8	16.8	12.8	99	90	99	96	0.2	1.7	0.2	0.7	10 • R	10	10	E 3	SE 3	ENE 3
6	74.8	75.7	74.1	74.2	14.4	15.7	13.5	14.3	16.6	13.5	99	96	99	98	0.2	0.7	0.2	0.4	10 =	10 •	10 •	NNE 3	NNE 5	NW 3
7	78.8	82.7	84.5	82.0	10.3	13.2	12.2	12.0	16.3	9.9	95	74	86	85	0.6	4.0	2.0	2.2	10 •	10	0	NNW 3	NW 3	WNW 3
8	86.7	86.0	84.2	85.6	12.5	19.6	16.1	16.1	20.9	6.3	81	45	72	66	2.7	12.5	3.1	6.8	1	3	6	WNW 1	E 2	SE 2
9	82.2	80.1	81.5	81.3	13.7	19.6	13.5	15.1	20.6	10.2	83	68	95	82	2.7	7.3	0.7	3.6	8	8	8	ESE 4	SE 8	E 1
10	80.8	79.7	76.5	79.0	12.1	19.4	14.3	15.0	20.4	10.0	98	62	99	86	0.3	8.6	0.2	3.0	4 ≡	9	10 •	C 0	SE 2	E 7
11	75.1	75.4	75.5	75.3	11.1	14.9	11.3	12.2	15.6	9.9	95	71	95	87	0.7	4.8	0.7	2.1	9	10	10 •	SE 1	SE 3	SE 2
12	77.6	80.3	82.6	80.2	11.5	15.0	13.6	13.4	18.2	10.4	97	78	94	90	0.4	3.6	0.9	1.6	10 •	9	9	N 5	NW 5	W 4
13	85.2	86.2	85.8	85.7	12.3	15.5	11.5	12.7	16.7	11.5	82	65	79	75	2.5	6.2	2.8	3.8	10	4	2	NW 6	NW 8	W 3
14	84.7	84.7	85.4	84.9	13.0	16.4	12.9	13.8	17.2	9.3	86	65	88	79	2.1	7.9	1.8	3.9	9	9	10	W 4	W 3	NW 1
15	87.0	89.0	89.2	88.4	13.3	15.9	13.4	14.0	17.4	12.2	95	78	86	86	0.7	4.0	2.1	2.3	10	9	2	NW 3	NW 4	NW 3
16	89.9	89.4	86.7	88.7	13.6	21.1	17.5	17.4	23.1	8.8	83	49	74	69	2.7	12.8	3.1	6.9	0	3	1	W 1	N 1	SW 2
17	83.4	80.8	80.2	81.3	16.9	23.4	17.4	18.8	24.0	9.9	72	37	76	62	5.3	18.2	4.8	9.4	2	4	2	S 3	S 7	W 1
18	85.0	88.8	89.7	87.8	14.5	16.1	13.3	14.3	18.3	12.1	87	68	87	81	2.2	5.8	2.0	3.3	9	9	2	NW 4	N 3	W 2
19	88.4	86.7	88.8	88.0	15.9	22.8	15.9	17.6	24.1	10.5	72	51	90	71	5.1	13.5	1.8	6.8	8	9	1	W 4	SW 7	WNW 2
20	92.4	92.3	92.6	92.4	15.3	20.5	13.5	16.7	21.3	12.1	79	50	79	69	3.7	12.0	3.7	6.5	0	4	9	WNW 5	W 5	W 1
21	93.4	93.1	90.8	92.4	15.3	21.4	18.2	18.3	22.5	13.3	78	48	69	65	3.9	13.2	6.6	7.9	6	3	9	WSW 1	NE 3	N 1
22	88.7	87.0	85.0	86.9	17.9	26.9	22.1	22.2	28.1	13.1	76	43	60	60	5.0	20.2	10.7	12.0	4	6	1	SE 1	SSW 2	WNW 1
23	85.2	86.4	87.5	86.4	21.8	21.2	19.0	20.2	26.4	15.4	74	81	87	81	6.8	4.8	3.0	4.9	2	9	2	SW 2	NW 4	WNW 1
24	90.1	89.9	90.4	90.1	16.7	23.6	19.9	20.5	26.7	13.3	94	53	79	73	1.2	13.4	4.9	7.2	2	3	2	C 0	NW 3	W 2
25	91.2	91.0	91.7	91.3	19.3	27.4	19.3	21.4	27.7	13.3	77	43	78	66	5.0	20.8	3.1	10.3	0	2	1	W 1	NNW 4	WNW 1
26	91.9	90.8	90.6	91.1	18.1	28.9	24.2	23.8	29.9	13.5	80	42	69	62	4.1	23.0	10.6	12.6	0	1	2	W 1	S 1	C 0
27	92.2	92.0	89.9	91.4	20.7	26.4	22.6	23.1	27.8	16.8	81	57	76	71	4.6	14.8	6.3	8.6	1	1	6	W 2	NE 2	NE 1
28	90.4	91.4	93.2	91.7	18.1	14.9	12.4	14.4	22.6	11.8	96	94	95	95	0.9	0.9	0.7	0.8	9	10 •	10 •	W 2	NNW 7	NNW 4
29	92.6	91.5	92.8	92.3	12.3	18.4	15.1	15.3	20.0	11.6	78	91	87	78	3.2	10.3	2.3	5.3	7	3	6	NW 2	NW 4	W 2
30	93.3	92.0	89.1	91.5	13.4	22.3	17.6	18.2	23.8	11.0	80	53	74	69	3.3	12.7	3.3	7.2	0	1	0	WNW 4	WNW 3	SW 2
31																								
M	86.3	86.4	86.2	86.4	14.9	19.9	15.9	16.6	21.5	11.4	84	61	82	76	2.8	10.2	3.5	5.5	5.1	6.4	3.2	2.7	4.0	2.2

DNI	WIDZALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	•	•	
2	8	0.0	•	▲° 14^10–14
3	8	0.0	•	⚹° 9^43–50 11^07–50, ⌴° 4–6
4	8	•	•	⌴° 3–7
5	6	8.9	•	•° 8^18, 9^10–10^42 11^02–17^09, 18^36–21^40; = 12^40–17^36, 22^10–24; ⌴° 3–5
6	6	1.5	•	•° 10^15–12^50, 13^05, 17^25; = 0^00–5^50 ≡°–8^20 =–24
7	7	•	•	= 0^00–9^20, ⌒¹ 23–24
8	8	•	•	= 0^40–3^40 ≡°–6^20 =–8^26; ⌒² 0^00–8
9	6	4.2	•	•° 18^05...20; = 4^20–8^10 ∞ 11^40–16^25; ⌒° 20–23
10	8	7.1	•	⚲° 11^45–12^01 14^26–36 ⚲¹ 16^40 17^10 ⚲° 18^25–50 ⚲¹–19^02 ⚲°–19^15, 22^50–23^25 •¹–24; (K)°W 14^15–50 E
11	7	0.1	•	•° 0^00–10 •°–2^25, 8^13...28, 8^39...44, 9^07...38, 11^14...25
12	7	2.6	•	⚲° 13^10–45, 14^35–15^15 •° 23^36, 24; = 6^10–9^20
13	7	0.3	•	•° 0^00...10–6^20 ⚲° 16^38–17^10; = 3^10–6^40
14	8	•	•	
15	7	0.3	•	⚲° 10^40–11^03, 13^45–55, 15^50–16^10; = 3^20–12^15, 19^36–24; ⌒° 2–8
16	6	0.2	•	•° 7^45–8^40 •¹ 9^15–10^10 •° 10^20...12^30 •° 12^40...13^25 •° 13^35–14^20; = 0^00–24
17	7	•	•	•° 1^20–2^25; = 0^00–7^20
18	8	14.6	•	⚲° 16^50–17^15 ⚲¹–18^10 ⚲°–18^25; (K)°W 15^47–K° 16^50–K¹ 17^15–18^30 E; = 17^20–22^40 ≡¹–24
19	8	1.8	•	⚲° 21^47–22^40; (K) 21^35–K° 21^47–22^15; ⚹ 8^40–12^20, 13^20–17^30; ≡¹ 0^00–3^40 =–4^25
20	6	3.4	•	•° 5^25–6^15 •² –7^10 •°–8^16, 8^48–10^10 •° 11^38–13^24, 14^07–15^08, 15^20–16^12, 16^28–18^14; = 5^30–8^30
21	7	•	•	= 2^10–3^20 ≡°–5^40 =–9^45, 19^40–21^10, ⌒° 20–24
22	7	5.1	•	•° 17^15–19^35, 21^50–24; = 2^40–3^20, 4^30–5^10, 6^18–9^40, 17^10–24, ⌒° 0^00–3 ⌒¹ 4–5 ⌒° 6–7; ⊕° 5^30–6^10
23	8	1.5	•	•° 0^00–1^15 •¹ 2^20–3^30 •°–4^45 13^40–14^10 16^20, 16^40...18^15, 21^15–45; ⚹ 10^10–40, 20^25–24; = 0^00–5^50
24	7	0.4	•	•° 1^00–40, 5^40...50, 9^25...10^10 ⚲° 19^30–46
25	8	6.2	•	⚲° 12^50–13^10, 19^25–45 ⚲¹ 15^30–37, 15^50–16^35 •° 18^30–20^15; (K) 12^17–K° 12^50–13^35 K° 15^50–16^35; = 0^20–2^35, 4^20–6^12, 17^50–24
26	7	0.0	•	•¹ 9^10–20; = 0^00–10^20 19^30–24
27	7	1.2	•	•° 20^36–21^01 •¹–21^10; ⌒ 22^48–23^05; = 0^00–4^45 ≡°–6^35 =–8^40, 23^10–24
28	6	0.7	•	= 0^00–13^30 ∞–17^40 =–24
29	8	2.5	•	•° 2^35–4^40, 10^45 11^02 ⚲° 11^48–55; ⚹ 15^40–17^35; = 0^00–7^10
30	8	0.3	•	•° 4^40...5^25–6^10 •¹–7^15 •°–8^05, 8^20...9^10; ⌒° 23–24
31	8	2.0	•	•° 15^35...16^10–17^40, 19^40...21^30, 22^15...23^25 ⚲¹ 23^50–24; ≡° 3^40–5^45 =–6^50, 19^20–24; ⌒° 0–2 ⌒² 3–7 ⌒¹ 8–9
Σ	–	64.9	–	

Czerwiec - Juin

DNI	WIDZALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8		•	⚲¹ 0^00–20 ⚲°–1^03, 1^35–2^10, 6^15–22; = 0^00–5^20; ⌒¹ 22–24
2	8	1.2	•	⚲° 16^03–35 •° 18^40–20^45; = 21^35...24; ⌒¹ 0^00–8
3	8	•	•	= 0^00–2^35, ⌒° 22–24
4	8	13.6	•	•° 17^03–12 17^41–18^03; ⌒ 22^50–24; = 19^30–24; ⌒° 0^00–8; ⊕° 11^08–12^12
5	6	10.9	•	⚲° 0^10 1^25 ⚲¹–3^45 •° 4^20–40 •¹–5^50 •°–6^20 ⚲° –6^25 ⚲¹–6^50 •¹–8^25 •°–9^10 10^15 11^10 15^30 16^25 17^10 •¹–17^35 •° 18^05 19^26; K° 1^40–3^35 6^20–35; ⌒ 0^10–3^40; = 0^00–24
6	5	1.6	•	•° 4^45–5^20 •° 11^45–14^45 •° 18^35–20^10 •¹–24; = 0^00–3^40 ≡¹–7^30 ≡°–10^45 =–24
7	7	•	•	•¹ 0^00–50 •°–1^15 •°–3^20 •¹–6^40; = 0^00–7^30, ⌒° 21–24
8	8	•	•	⌒¹ 1–8 ⌒° 21–24, ⊕ 10^10–11^20
9	8	9.9	•	⚲° 9^10–20 14^01–05 ⚲¹ 14^40–15^15 ⚲°–15^55; (K)°W 13^48 K¹ 14^40–K° 15^10–41 E; ⚹ 14^40–15^00; = 1^40–2^35, 23^40–24, ⌒° 0^00–8
10	8	29.2	•	⚲¹ 15^42 16^00, 16^42 19^10 •¹ 21^40 •°–22^10 •¹–22^45 •° 23^05 •¹–23^08 •°–23^15; K° 15^43–16^00, K¹ 16^47 K° 17^20–18^15; = 0^00–1^40 ≡°–2^30 ≡¹–3^10 ≡¹–4^20 ≡°–6^45 =–7^30
11	8	12.0	•	•° 19^45–24; = 21^10–24
12	7	10.6	•	•° 0^00–2^10, 3^20–9^20, 9^40–10^15 ⚲° 13^10–15 ⚲² 17^30–40 ⚲¹–18^05 ⚲°–18^10, 19^45–20^10, K¹ N 17^30–18^20 S; = 0^00–2^20
13	8	•	•	
14	7	1.0	•	⚲° 19^50–20^02 •° 21^40...22^15–24; = 3^30–8^15, 23^20–24; ⌒¹ 2–8
15	7	0.2	•	•° 0^00–30...1^35–3^15 ⚲° 16^05–40; = 0^00–12^15; ⌒° 21–24
16	8	•	•	⌒¹ 0^00–8 ⌒° 20–24
17	8	•	•	⌒¹ 1–5 ⌒° 6–8, 21–24
18	7	•	•	= 7^20–10^10; ⌒¹ 1–4 ⌒° 5–8, 22–24
19	8	4.7	•	⚲¹ 15^30–16^05 ⚲°–16^40 23^20–30 ⚲¹–23^35 ⚲°–23^45; (K)°NW 14^44–K° 15^30–K¹ 15^35–K° 16^10–30 SE; ⌒° 0^00–8
20	7	•	•	= 3^20–7^40
21	8	•	•	= 2^20–6^45; ⌒° 1–7, 22–24
22	7	•	•	= 2^20–8^40; ⌒° 0^00–7, 22–24
23	8	•	•	= 2^30–3^10; ⌒° 0^00–7, 21–24
24	8	•	•	= 1^40–8^10; ⌒° 0^00–2 ⌒² 3–5 ⌒° 6–8, 23–24
25	7	•	•	⌒° 0^00–7 ⌒¹ 22–24
26	7	0.0	•	⚲° 23^02–15; K° 23^03–(K) 23^20–24; ⚹ 21^50–23^10; = 0^40–8^20; ⌒¹ 1–5 ⌒¹–7
27	7	8.7	•	(K) 0^00–30 K° W 23^30–24 SE; = 2^40–6^45
28	6	16.2	•	⚲¹ 0^00–35 ⚲° 2^30–50 ⚲¹–3^00 ⚲°–4^10 •° 7^15...35 ⚲¹ 10^07–15 ⚲° 10^35 11^13 11^25 12^10 •° 12^25 13^40–21^35, 22^50–23^15; K° 0^00–K¹ 0^05–K° 0^40–2^35; ⚹ 9^50–12^10; = 6^10–24
29	8	•	•	= 0^00–30 19^50–24, ⌒° 20–24
30	7	•	•	= 0^00–6^20; ⌒° 0^00–2 ⌒¹–7 ⌒°–8, 21–24; = 0^40–6^20
31				
Σ	–	119.8	–	

Przemyśl — $\varphi = 49°48'$ — $\lambda = 22°46'$ — *Lipiec – Juillet 1965*

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	85.3	84.2	85.3	84.9	19.8	25.4	17.9	20.2	26.1	12.9	69	54	98	74	7.1	14.9	0.4	7.5	2	6	10	SW 5	WSW 5	W 2
2	84.9	83.6	83.8	84.1	14.7	14.8	13.7	14.2	17.9	13.7	97	96	97	97	0.5	0.7	0.6	0.6	10 •	10 •	9	E 4	ENE 4	W 1
3	83.3	82.7	82.8	82.9	14.7	19.3	13.7	15.4	19.8	11.3	80	63	98	80	3.3	8.2	0.4	4.0	5	6	10 •	WNW 2	E 2	W 1
4	84.8	83.2	82.0	83.3	12.0	17.1	12.0	13.3	17.5	9.3	86	61	99	82	2.0	7.6	0.2	3.3	1	9	10 •≡	WNW 3	NE 1	E 2
5	80.7	79.7	81.6	80.7	11.7	12.1	9.9	10.9	12.5	9.9	93	94	89	92	1.0	0.8	1.3	1.0	10	10 •	10	NE 1	N 4	NW 3
6	86.2	87.0	87.8	87.0	12.2	14.9	12.0	12.8	17.0	8.3	80	60	72	71	2.9	6.7	4.0	4.5	1	9	2	W 5	WNW 3	W 2
7	90.0	88.3	86.3	88.2	13.1	20.3	16.0	16.4	20.9	8.0	74	49	70	64	4.0	12.1	5.4	7.2	3	5	2	WSW 2	SW 6	SW 3
8	84.9	82.6	76.6	81.4	18.3	24.3	19.8	20.6	25.0	13.4	56	36	60	51	9.2	19.6	9.3	12.7	5	1	8	SW 6	SSW 7	S 5
9	80.0	83.8	86.6	83.5	13.1	14.7	11.3	12.8	21.7	11.2	98	73	83	85	0.4	4.5	2.3	2.4	8 •	9	0	WNW 2	NW 2	WSW 2
10	88.4	88.1	89.3	88.6	12.3	18.7	12.8	14.2	19.6	8.0	82	51	84	72	2.5	10.6	2.4	5.2	0	7	10 •	WNW 1	SW 1	WSW 2
11	90.9	91.6	92.5	91.7	12.0	16.0	12.7	13.4	17.9	10.0	86	61	80	76	2.0	7.2	2.9	4.0	1	8	0	C 0	N 5	WNW 2
12	92.6	90.7	88.7	90.7	10.8	20.0	16.8	16.1	21.5	7.2	92	50	72	71	1.0	11.8	3.3	6.0	0	5	8	SW 2	C 0	C 0
13	88.4	88.7	89.5	88.9	17.2	21.9	18.9	19.2	23.8	14.9	87	64	83	78	2.6	9.6	3.7	5.3	9	8	0	WNW 3	W 3	WNW 2
14	91.4	91.3	91.6	91.4	14.3	25.4	20.1	20.0	26.2	12.2	99	53	74	75	0.2	15.3	6.2	7.2	0	1	0	SW 1	SSE 3	C 0
15	91.9	91.3	90.0	91.1	16.1	25.6	20.2	20.3	26.5	11.8	89	49	79	72	1.9	16.7	5.0	7.9	0	1	0	WSW 1	ESE 6	C 0
16	88.5	87.0	86.4	87.3	15.9	26.5	22.3	21.8	28.2	12.8	95	54	80	76	1.0	16.0	5.4	7.5	0	3	0	S 1	SE 3	C 0
17	86.3	84.8	84.7	85.3	19.6	27.8	17.6	20.6	28.9	15.9	90	53	97	80	2.4	17.6	0.6	6.9	3	3	10 • K	W 1	SE 5	W 2
18	83.5	82.7	85.3	83.8	17.3	22.3	17.7	18.8	23.2	14.6	97	74	95	89	0.6	6.9	1.0	2.8	8	9 •	9	S 1	SE 3	N 5
19	89.5	91.5	92.4	91.1	15.6	20.4	15.3	16.6	21.4	15.0	96	60	80	79	0.7	9.5	3.5	4.6	10 •	4	1	E 5	E 7	ENE 2
20	93.2	92.3	90.2	91.9	15.0	21.5	16.0	17.1	22.4	11.2	78	53	77	69	3.6	12.0	4.2	6.6	0	4	1	SE 4	SE 6	E 3
21	88.0	86.3	84.1	86.1	15.2	23.8	17.7	18.6	24.5	13.2	85	61	80	75	2.6	11.6	4.0	6.1	8	8	6	SE 2	S 3	C 0
22	84.2	85.1	84.1	84.5	16.6	20.7	17.9	18.3	24.3	15.4	95	79	88	87	1.0	5.1	2.4	2.8	10	8	1	W 3	NW 3	C 0
23	82.4	81.4	83.3	82.4	16.7	17.7	18.3	17.8	24.7	13.1	94	89	96	93	1.2	2.2	0.8	1.4	1	10 • K	10 •	E 3	W 3	NW 3
24	85.5	85.1	84.8	85.1	16.7	25.7	20.4	20.8	27.1	12.8	94	57	83	78	1.2	14.2	4.0	6.5	0	4	1	C 0	W 5	C 0
25	87.0	85.9	84.4	85.8	20.1	24.4	17.6	19.9	25.5	16.4	83	74	96	84	3.9	8.0	0.8	4.2	2	9 (K)	8 •	WNW 2	NE 5	SSE 3
26	84.3	85.9	85.7	85.3	18.7	19.0	14.8	16.8	20.7	14.5	92	88	98	93	1.7	2.6	0.3	1.5	8	10 •	10 •	W 4	NW 5	WSW 1
27	83.2	84.5	86.7	84.8	13.4	16.7	13.1	14.1	16.9	11.9	95	86	88	90	0.7	2.7	1.8	1.7	10	10	0	WSW 2	W 5	NW 1
28	87.5	87.5	87.0	87.3	13.5	18.2	14.2	15.0	19.0	10.6	86	63	80	76	2.1	7.7	3.2	4.3	7	9 •	10	W 5	WNW 5	WNW 2
29	85.1	83.5	79.8	82.8	14.2	21.0	17.8	17.7	22.5	11.8	86	60	76	74	2.4	9.9	5.0	5.8	7	4	3	W 1	SW 4	SW 4
30	76.7	76.2	78.0	77.0	16.1	20.3	14.9	16.6	22.2	14.8	89	71	88	83	1.9	6.8	2.0	3.6	10	10 •	0	WSW 3	SW 7	W 3
31	79.7	78.9	78.2	78.9	14.3	16.9	14.5	15.0	17.3	12.8	94	80	91	88	0.9	3.8	1.5	2.1	10	10	2	S 1	SSE 2	WNW 3
M	86.1	85.7	85.5	85.8	15.2	20.4	16.1	17.0	22.0	12.2	88	65	85	79	2.2	9.1	2.9	4.7	4.8	6.8	4.9	2.4	3.9	1.9

Sierpień – Août

DNI	CIŚNIENIE P=900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	83.0	85.0	85.8	83.9	13.7	16.1	15.4	15.2	18.5	13.4	91	74	89	85	1.5	4.7	1.9	2.7	10	8	10 •	WNW 2	N 1	NE 2
2	69.8	75.1	82.1	75.7	14.1	10.9	9.5	11.0	16.9	9.2	97	95	93	95	0.6	0.6	0.8	0.7	10	10 •	3	ENE 3	NW 4	W 3
3	83.8	83.9	85.6	84.4	12.0	19.0	12.7	14.1	20.6	8.2	82	56	87	75	2.5	9.6	1.9	4.7	4	8	10 •	NW 2	WNW 3	W 1
4	87.8	87.7	88.8	88.1	13.5	19.3	13.4	14.9	19.9	11.2	85	65	95	82	2.3	7.8	0.7	3.6	4	8	2	WSW 2	SW 4	WNW 3
5	92.5	94.0	93.8	93.4	14.4	19.5	15.3	16.1	20.9	12.6	90	55	78	74	1.6	10.3	3.9	5.3	4	4	0	WNW 3	NW 3	W 2
6	94.2	93.3	91.6	93.0	17.1	26.1	20.0	20.8	27.0	12.4	79	51	74	68	4.1	16.6	6.0	8.9	0	1	1	W 2	WSW 6	WSW 3
7	91.8	91.2	89.2	90.7	22.3	28.6	22.7	24.1	29.0	19.6	65	48	60	58	9.5	20.5	11.1	13.7	6	2	0	WSW 5	SW 7	W 2
8	89.7	87.9	86.6	88.1	18.7	29.7	21.3	22.8	30.7	13.4	79	43	71	64	4.6	24.0	7.3	12.0	0	0	0	C 0	S 3	SW 1
9	87.4	88.0	89.5	88.3	19.5	23.3	19.6	20.5	23.5	16.2	82	73	79	79	4.1	7.2	4.7	5.3	0	8	10	W 2	WNW 5	WNW 3
10	91.3	91.1	90.3	90.9	14.7	17.0	16.2	16.0	19.6	14.3	94	82	86	87	0.9	3.6	2.5	2.3	10	10	10	NNE 1	NE 5	NNE 3
11	88.5	89.9	91.4	89.9	13.1	11.5	9.5	10.9	16.2	9.1	96	99	97	97	0.6	0.2	0.3	0.4	10 •	10 •	10 •	NE 5	NNE 7	NW 2
12	89.8	90.6	91.2	90.5	11.6	11.5	10.6	11.1	14.3	9.1	95	94	97	95	0.6	0.9	0.4	0.6	10 •	10 •	8	W 3	NE 6	WNW 4
13	90.8	91.1	91.7	91.2	10.7	13.1	10.6	11.2	15.6	9.2	92	69	90	84	1.0	4.6	1.3	2.3	9	6	6	NW 4	NW 7	WNW 3
14	91.7	91.7	90.8	91.4	10.2	13.1	12.5	12.6	16.2	9.2	92	56	88	79	0.9	7.7	1.7	3.4	10	8	10	WNW 4	W 3	W 2
15	91.0	91.8	92.2	91.7	10.6	13.1	11.1	12.0	15.9	10.3	97	75	95	89	0.4	4.3	0.7	1.8	9 •	8	4	W 2	C 0	W 1
16	92.5	92.0	91.2	91.9	9.3	17.3	10.9	12.1	18.9	7.4	100	58	91	83	0.0	8.3	1.1	3.1	4 ≡	7	0	W 1	E 2	W 2
17	90.8	90.6	90.5	90.6	8.1	19.8	11.6	12.8	21.2	6.2	99	49	91	80	0.2	11.7	1.1	4.3	0	3	0	WSW 2	NE 2	W 2
18	91.7	92.3	92.9	92.3	10.3	21.2	12.9	14.3	22.2	6.5	92	50	92	78	0.9	12.3	1.3	4.9	0	3	0	W 3	S 1	WSW 1
19	95.1	95.6	95.9	95.5	10.9	22.4	14.1	15.4	23.3	8.2	97	50	91	79	0.3	13.4	1.3	5.1	1	3	0	WSW 2	E 2	W 1
20	96.1	95.1	93.3	94.9	10.7	23.5	16.9	17.0	24.3	8.7	97	46	82	75	0.4	15.7	3.3	6.3	0 ≡	2	0	WSW 2	SE 7	SE 1
21	92.4	90.4	88.6	90.3	12.8	23.3	16.3	17.7	26.1	9.1	99	41	81	74	0.2	19.4	3.4	7.7	0	3	0	C 0	SW 4	C 0
22	87.2	85.8	84.0	85.7	13.7	26.3	16.8	18.4	26.7	10.1	92	41	83	72	1.3	20.2	3.3	8.3	3	3	0	E 1	S 3	N 2
23	83.7	83.7	84.4	83.9	13.4	23.9	18.1	18.9	26.3	11.3	91	43	79	72	1.4	18.2	4.3	8.0	0	3	0	C 0	S 3	C 0
24	84.3	83.5	81.3	83.0	14.5	26.0	21.1	20.7	27.2	12.8	91	55	78	73	1.3	13.0	3.6	7.4	8	7	10	E 1	ESE 5	ESE 2
25	79.8	79.9	80.4	80.0	17.3	20.0	16.3	17.3	21.4	16.2	93	90	93	93	1.0	2.4	1.3	1.6	10	10 •	10	C 0	C 0	WNW 1
26	80.9	81.2	80.6	80.9	12.8	12.9	10.6	11.7	16.3	10.3	92	94	93	94	1.2	0.9	0.7	0.9	10	10 •	10 •	WNW 6	WNW 5	NW 6
27	78.9	82.0	83.3	82.1	9.9	9.9	10.0	10.0	10.6	9.2	93	96	93	93	0.8	0.3	0.7	0.7	10 •	10 •	9	NW 6	WNW 5	W 3
28	86.1	86.9	88.1	87.0	10.6	16.0	11.3	12.4	16.6	9.3	96	69	91	83	0.3	3.6	1.2	2.4	10 •	8	10	WNW 2	NNE 1	W 2
29	88.4	88.0	86.9	87.8	10.1	13.0	11.3	12.0	17.6	6.9	93	78	94	89	0.7	3.6	0.9	1.7	2	9	0	WNW 2	NW 1	W 2
30	85.9	87.2	87.7	86.9	10.1	12.3	11.7	11.3	16.8	8.3	93	94	84	90	0.8	0.9	2.1	1.3	9	10	6	W 3	W 4	W 3
31	87.7	87.4	86.7	87.3	9.3	16.6	10.6	11.8	18.1	7.8	91	52	94	79	1.1	9.1	0.8	3.7	1	4	1	W 4	NW 5	W 3
M	87.9	88.2	88.3	88.1	12.9	18.9	14.2	15.0	20.6	10.6	91	66	87	81	1.3	9.0	2.3	4.3	5.3	6.3	4.3	2.4	3.7	2.1

Przemyśl — $H_s = 237\,m$ — $H_b = 238{,}9\,m$ — $h_w = 18{,}2\,m$ — Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GUŁ	POGODA
1	7	14.6	•	⚲°15-40 16^00 16^45 18^40 ⚲²-18^50 ⚲¹-19^30 ⚲°-20^05 °20^45 21^15 •¹-21^30 •°-21^40 K°NW 15^28-16^10 NE K¹S 19^35-K°19^10-35 = 17^40-24, ⌓°0-1 ⌓¹-7
2	5	20.2	•	•°5^05-15 •¹-5^35 •°-7^20 •¹-7^35 •°-8^20 9^25-45 •¹-10^15 •°-10^30 •¹-12^00 •°-13^10 •¹-13^30 •°-14^20, = 0^00-17^20 19^45-24
3	7	5.2	•	•°16^45 17^15-50 •¹-18^00 •°-19^10 •¹-19^15 •°-19^20 •¹-19^30 •°-21^10, = 0^00-9^35 15^30-24
4	7	16.7	•	•°13^20-40 14^00-15^50 16^25-18^10 •¹-19^15 •°-21^20; = 0^00-10^40, 14^50-19^45 ≡°-21^40 = -24
5	6	9.6	•	•°8^35-14^40 •¹-15^15 •°-15^25 •¹-15^35 •°-18^10, = 0^00-24
6	7	•	•	= 0^00-8^15; ⌓°23-24
7	7	•	•	⌓°0^00-8, 20-24
8	8	35.2	•	⚲°23^01-06; ⚲ 12^45-16^40; ⌓°0^00-6
9	7	•	•	⚲°0^18-29 0^45-1^00 •°-6^30; ⌓°21-24
10	8	0.0	•	⚲°20^20-35; K°18^50-20^25; ⌓°0^00-8, ⊕°15^35-16^20
11	7	•	•	= 3^40-8^15; ⌓°20-24
12	8	0.7	•	= 0^10-8^30, ⌓°0^00-2 ⌓²3-7 ⌓¹-8
13	8	•	•	•°1^50-2^30 3^40; = 3^30-24; ⌓°20-23 ⌓¹-24
14	7	•	•	= 0^00-8^15, ⌓¹0^00-2 ⌓²-6 ⌓°-7, 20-24
15	8	•	•	= 1^30-7^50; ⌓°0^00-1 ⌓¹-2 ⌓²-7 ⌓¹-8 ⌓°-9, 22-24
16	8	•	•	= 0^10-8^30 22^40-24, ⌓°0^00 1 ⌓¹-3 ⌓²-7 ⌓°20-24
17	7	37.4	•	⚲²15^15-18▲⚲°⚲²-15^22 ⚲¹-15^50 ⚲°-16^00 ⚲¹-16^07 ⚲°-16^15, 17^45-19^35 ⚲¹-20^20 ⚲°-21^40 22^05-25 ⚲¹-22^40 ⚲°-23^35 (K)°W 14^10 K¹15^15-K²15^18 K¹15^22 K°16^10-20 (K)N 16^20 K¹17^45 K¹18^00
18	8	9.3	•	•°2^45, 3^30 ⚲°12^15-30 ⚲²13^25-32 ⚲¹-13^45 ⚲°-14^35 ⚲¹20^33-37 ⚲°-20^40, (K)S 13^05 K°13^25 14^25, = 0^00 9^10
19	8	0.0	•	•°6^15-7^10; ⌓°21-24 [17.VII: K°18^30 23^30, ⚲15^15-25, = 0^00 9^40 19^20-24, ⌓°0^00 4 ⌓¹-8
20	8	•	•	⚲10^30-17^25; ⌓°0^00-8, 21-24
21	7	11.8	•	⚲¹16^50 17^00 ⚲°-17^02 23^20-30 (K) 13^15-35 19^02-35 < 20^20-21^20, ⌓°0^00-8 ⌓¹21-24
22	7	0.2	•	⚲°0^06-10^7 ⚲¹-13^8 ⚲°-22^5 ⚲¹3^32 4^01 •¹-4^40 •°-5^45 12^19-25; K°0^22 1^30; ⌓°21-24
23	7	16.6	•	⚲¹12^02-25 ⚲°-12^47 13^45 14^00 19^50 20^01 ⚲¹-20^04 ⚲²-20^10 ⚲¹-20^20 ⚲²-20^35 ⚲°-21^30; (K) 10^01-21 (K)°SW 11^45 K¹12^02 K°12^20-47 (K) NW 13^04, = 3^30-7^30 21^20-24, ⌓°0^00-1
24	8	0.0	•	⚲°18^34-45; K°W 16^48 19^15 SE; = 0^00 7^40 23^50-24, ⌓°21-24 [23.VII: ⌓¹-3 ⌓²-7 ⌓°-8
25	7	28.0	•	⚲¹12^32-37 ⚲°-13^02 ⚲¹-13^10 ⚲°-13^15 ⚲¹13^32-47 ⚲²-13^50 ⚲¹-15^15 ⚲°-15^45 ⚲¹-16^20 ⚲°-17^40 20^25-21^06 (K)W 11^20 K°12^32 K¹12^45 K°13^12 K¹13^25 K°15^10-17^20, = 0^00-7^30 = 22^40-23^45 = °-24;
26	6	8.0	•	•°10^35 11^10 11^50 12^30 14^40-50 15^42 16^03 •¹-16^25 •°-16^35 17^15-35 18^05-13 •¹-18^45 •°-19^20 19^35-20^40 21^45 23^32-24, = 0^00-46 = -3^25 12^10-24 [25.VII: ⌓°0^00 4 ⌓¹-8
27	7	8.2	•	•°0^00-40 8^35 10^50 ⚲¹13^10-14 ⚲²-13^30 ▲°13^15-17 (K) NW 12^50 K²13^15-35 (K) 13^55 SE; = 0^00-2^30 7^10-12^15 13^35-15^20 18^20-24
28	7	0.6	•	•°3^45-4^10 ⚲°12^05-42 12^45-48 13^34-46 14^06-13 ⚲¹-14^17 ⚲°-14^24; = 0^00 7^35 22^45-24
29	8	2.8	•	= 0^00-7^15; ⌓°20-24
30	8	3.4	•	•°3^02-06 •¹-3^09 •°-4^40 5^06-25 ⚲°10^52-11^02 12^25-13^15 •¹-14^10 •°-15^20, ⌓°0^00-3, 22-24
31	7	3.7	•	•°9^25-10^10 •¹-11^35 •°12^45-13^15; ⌓°0^00-8, 21-24
Σ	-	210.2	-	

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1	8	25.1	•	•°19^34-20^06 20^25-21^20 23^01-24; = 6^20 7^30; ⌓°0-9
2	6	1.0	•	•°0^00-03 0^05-40 ⚲°1^00-2^38 ⚲¹3^00-04 ⚲°-3^10 ⚲¹-3^35 ⚲°-4^05 •°11^20 14^20, K°0^48-K¹3^03-K°3^10-4^25, = 6^45-10^30 11^30-14^30; ⌓°22-24
3	8	2.0	•	⚲°15^35-16^04 17^02-18^02 •°20^25 21^10, K°15^48-16^04 (K)°17^30; ⌓¹0^00-8
4	7	3.8	•	⚲°14^40-45 ⚲¹-14^58 ⚲°-15^10 ⚲¹-15^28 ⚲°-15^15 16^45-55 18^35-43 (K) NW 14^32 K°14^40 K¹14^50 K°14^58 15^15 (K)°15^40 NE, K°S 19^26-20^25 NW, = 0^40 1^30 5^20 7^30 21^45-24
5	8	•	•	= 0^00 9^20; ⌓°21-24
6	7	•	•	= 3^30-7^40; ⌓°0^00-8^00
7	8	•	•	⌓°20-24
8	7	•	•	⌓°0^00-3 ⌓¹-7 ⌓°-8, 21-24
9	7	•	•	= 5^30-11^20; ⌓°0^00-7
10	7	1.2	•	= 0^00-8^20; ⌓°0^00-8
11	6	29.1	•	•°3^40-4^10 •°-6^40 7^20-25 •¹-7^40 •°-10^15 •¹-11^40 •°-13^30 •¹-15^10 •°-21^25 22^35-24; = 7^10-24
12	6	12.3	•	•°0^00-40 1^15-8^08 8^15-0^03 •¹0^10 •°-0^21 0^46 10^06 •¹10^25-32 ⚲°12^26-28 ⚲¹-12^44 ⚲°12^46-54 ⚲¹-12^59 ⚲°-13^22 14^02-22 14^30-58 17^16-24 17^30-40 •°18^14-19^18; = 0^00-10^40
13	8	0.4	•	⚲°2^55 3^20 •¹-4^10 •°-5^15 ⚲°12^45-50; = 3^15-6^00; ⌓°20-24
14	8	2.0	•	⚲°5^00-20; ⌓°0^00-2 ⌓¹-5
15	8	4.7	•	•°5^25-5^05 •¹-6^15 •°-7^10 ⚲°12^25-28 10^31-30 ⚲¹-10^43 ⚲²-10^46 11^38-46 11^48-12^06 12^21-13^10 ⚲¹-13^21 ⚲°-13^25 ⚲¹-13^34 ⚲°-13^40, K°NW 12^48-13^25; = 5^40-7^30 22^40-24
16	8	•	•	= 0^00-50 ≡ -7^40 = -8^15; ⌓°20-24
17	8	•	•	= 1^30-2^35 7^30-9^20; ⌓°0^00-2 ⌓¹-3 ⌓²-7 ⌓¹-8 ⌓°-10, 19-24
18	8	•	•	= 4^30-9^10 22^20-24; ⌓¹0^00-4 ⌓²-8 ⌓¹-9 ⌓°19-21 ⌓¹-24
19	7	•	•	= 0^00-8^30 21^45-24; ⌓¹0^00-2 ⌓²-9 ⌓°20-24
20	7	•	•	= 0^00-3^40 ≡ °5^40-7^15 = -10^30; ⌓°0^00-2 ⌓¹-3 ⌓²-8 ⌓¹-9 ⌓°-11, 18-24
21	7	•	•	= 0^30-7^25 21^10-24; ⌓¹0^00-3 ⌓²-8 ⌓°-9, 20-23 ⌓¹-24; = 0^30-7^25 21^10-24
22	7	0.0	•	⚲°13^05-10 15^50-16^03 (K) 13^35-40 (K) SE 14^25-15^35; = 0^00-8^30; ⌓¹0^00-3 ⌓²-9 ⌓°-10, 20-24
23	8	•	•	= 0^10-9^15; ⌓°0-2 ⌓¹-3 ⌓²-8 ⌓¹-9 ⌓°-10, 22-24
24	7	0.6	•	= 4^00-7^40; ⌓¹0^00-8 ⌓°-9
25	6	9.9	•	•°2^44-55 3^15-4^00 4^25 5^10 7^40 8^10 8^45 10^30 12^25-40 ⚲°17^00-25 18^25-55 20^36-50 •°22^00-20, (K) S 18^16 K°18^25-55 (K) 19^15, = 6^10-14^25
26	7	40.6	•	•°0^50 1^10 1^45 4^03 5^20-40 9^05-10^10 •¹-10^25 •°-10^45 12^20-40 13^35 14^02 •¹-14^10 •²-14^25 •¹-15^50 ⚲°-17^15 ⚲°-17^40 °18^00 19^05 •¹-19^25 •°-21^10, K¹15^50 K°16^40 17^30
27	6	22.5	•	•°0^15 1^40 •°-2^40 •¹-3^10 •°-4^45 5^22 8^40 •¹-9^00 •°-9^25 •¹-9^36 •°-9^40 •¹-10^20 •°-15^21, = 20^10-24
28	7	3.6	•	•°4^40-5^20 6^15 7^20 ⚲°11^50 12^02 13^40-43 ⚲¹-14^00 ⚲°-14^15, = 0^00-10^30 23^40-24; ⌓°22-24
29	7	•	•	= 0^00-12^10 18^20-24; ⌓°0^00-2 ⌓²-9 ⌓¹-10 ⌓°-11, 21-24
30	6	0.8	•	•°11^02-12^06 •°12^50-13^12 ⚲°18^05-18, = 0^00-8^40 11^40-15^36; ⌓°0^00-9
31	7	•	•	= 4^15-8^25 20^10-24; ⌓°1-2 ⌓¹-4 ⌓²-8 ⌓°-9, 20-24
Σ	-	139.6	-	

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ *Wrzesień – Septembre* 1965

DNI	CIŚNIENIE P = 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU Dv I	II	III
1	85.9	87.1	89.6	87.5	12.7	18.5	16.2	15.9	20.9	9.2	88	60	76	75	1.8	8.5	4.4	4.9	8	10	0	WSW 1	S 4	S 1
2	92.0	92.8	92.6	92.5	13.3	24.7	18.3	18.6	25.8	11.7	86	58	86	77	2.1	13.0	2.8	6.0	3	8	0	E 2	ESE 3	SSE 3
3	90.7	89.7	88.1	89.5	13.8	26.2	17.6	18.8	26.6	10.9	93	45	77	72	1.1	18.8	4.5	8.1	9	8	2	E 1	S 4	SW 2
4	84.2	83.2	84.3	83.9	16.7	26.0	18.9	20.1	26.4	12.2	78	56	73	69	4.2	14.8	5.9	8.3	7	5	6	ESE 2	ESE 2	SW 5
5	86.3	85.8	84.6	85.6	11.9	21.6	15.8	16.3	22.5	9.6	94	56	76	75	0.8	11.3	4.3	5.5	0	5	0	NW 1	SW 6	SSW 2
6	83.2	81.3	79.6	81.4	13.1	22.4	15.7	16.7	24.8	10.8	92	53	98	81	1.3	12.6	0.4	4.8	3	9	10	C 0	WSW 3	E 2
7	80.7	81.8	84.9	82.5	11.4	17.7	12.4	13.5	18.9	11.1	98	59	87	81	0.4	8.2	1.9	3.5	10 •	3	1	W 3	WNW 4	WNW 2
8	86.6	88.6	89.4	88.2	11.6	17.7	12.5	13.6	18.9	10.3	96	65	95	85	0.5	7.0	0.7	2.7	9	6	10	W 3	NNW 3	C 0
9	88.4	87.9	88.2	88.2	12.4	22.9	16.9	17.3	23.5	9.2	96	59	78	78	0.5	11.4	4.2	5.4	0	3	0	WSW 1	SW 5	WSW 3
10	87.5	86.2	86.4	86.7	13.0	24.1	17.7	18.1	25.6	11.0	93	56	81	77	1.1	13.2	3.8	6.0	1	8	1	E 1	SW 3	C 0
11	84.4	84.1	85.4	84.6	18.6	24.5	13.4	17.5	26.2	13.2	69	52	96	72	6.6	14.8	0.6	7.3	7	7	10 •	SE 4	SSW 7	N 3
12	86.2	87.6	86.5	86.8	12.2	14.1	9.5	11.3	15.1	9.4	93	77	97	89	1.0	3.7	0.3	1.7	10	9	0	C 0	NNW 3	C 0
13	84.4	83.4	84.1	84.0	7.2	14.8	11.3	11.2	16.4	5.8	100	83	96	93	0.0	2.9	0.5	1.1	10 ≡	9	6	C 0	NE 2	WNW 2
14	87.1	88.8	91.0	89.0	7.5	13.9	11.3	11.0	15.2	6.0	99	85	90	91	0.2	2.3	1.3	1.3	7 ≡	10 •	6	SW 1	SE 1	W 3
15	93.0	94.0	96.2	94.4	10.6	15.1	11.7	12.3	17.2	8.9	88	70	94	84	1.5	5.1	0.8	2.5	9	10	8	NW 3	WNW 4	WNW 3
16	98.8	99.7	99.1	99.2	7.0	15.3	8.0	9.6	16.3	6.4	98	64	96	86	0.1	6.3	0.4	2.3	2 ≡	2	0	W 2	N 2	C 0
17	97.3	96.4	95.1	96.3	3.5	20.3	12.7	12.3	22.5	1.4	100	48	76	75	0.0	12.3	3.6	5.3	0 ≡	0	0	WSW 1	E 1	SW 3
18	94.1	91.9	90.5	92.2	11.1	22.4	14.4	15.6	22.8	9.8	86	49	76	70	1.8	13.8	3.9	6.5	0	0	0	S 1	S 5	SW 2
19	89.7	90.9	95.4	92.0	15.9	19.9	12.2	15.0	21.4	11.9	69	67	86	74	5.6	7.5	2.0	5.0	6	9	10	W 5	N 3	NW 5
20	97.8	99.8	102.6	100.1	11.4	13.9	12.3	12.5	14.6	10.8	85	72	80	79	2.0	4.4	2.9	3.1	10	10	10	N 6	N 3	NNW 5
21	104.9	105.0	102.9	104.3	10.3	14.2	8.9	10.3	16.2	8.4	96	71	90	86	0.5	4.8	1.1	2.1	9	4	0	C 0	NW 1	W 2
22	100.3	97.7	94.7	97.6	5.9	18.6	11.5	11.9	19.4	4.3	94	55	85	78	0.6	9.6	2.0	4.1	2	5	0	W 3	NW 2	WNW 2
23	92.9	91.9	90.2	91.7	11.1	20.9	12.1	14.0	22.1	8.8	86	57	96	80	1.8	10.6	0.5	4.3	0	0	0	NW 4	W 2	W 2
24	89.8	89.5	89.2	89.5	6.6	22.1	13.5	13.9	22.8	4.8	97	55	95	82	0.3	12.1	0.7	4.4	0	1	0	W 1	E 1	C 0
25	88.4	87.4	85.7	87.2	7.7	22.3	16.0	15.5	23.5	6.3	100	56	78	78	0.0	11.7	4.0	5.2	0 ≡	1	0	WSW 2	SE 3	N 2
26	85.0	84.5	84.7	84.7	10.3	23.9	14.4	15.8	24.3	8.5	97	44	90	77	0.3	16.5	1.6	6.1	2	1	0	NNE 1	S 3	C 0
27	84.2	84.2	84.8	84.4	13.1	19.5	16.4	16.4	21.5	11.8	93	70	80	81	1.1	6.9	3.6	3.9	10 •	9	0	SE 2	S 6	S 6
28	83.6	83.8	82.0	83.1	16.6	25.3	17.2	19.1	25.6	13.8	82	51	90	74	3.5	15.7	2.0	7.1	8	5	9	S 8	SSW 5	SE 2
29	79.6	82.1	89.6	83.8	17.2	14.4	11.7	13.8	21.9	11.3	79	90	90	86	4.1	1.6	1.3	2.3	9	10	9	S 3	S 5	W 2
30	91.0	90.4	89.7	90.4	8.5	21.3	11.4	13.2	22.3	7.0	97	42	94	78	0.3	14.8	0.9	5.3	6	7	0	SSW 2	SSW 8	C 0
31																								
M	89.3	89.2	89.6	89.4	11.4	20.0	13.7	14.7	21.4	9.2	91	61	87	80	1.5	9.9	2.2	4.5	5.2	5.8	3.3	2.1	3.5	2.1

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1	90.8	91.0	91.4	91.1	8.9	21.1	13.2	14.1	21.4	7.4	99	56	95	83	0.2	11.1	0.7	4.0	0	0	0	W 3	WSW 3	W 1
2	90.6	89.5	89.9	90.0	8.1	20.9	14.7	14.6	21.4	7.7	99	59	90	83	0.2	10.2	1.6	4.0	0 ≡	0	0	E 1	SE 4	C 0
3	92.4	94.0	94.7	93.7	9.8	15.1	11.5	12.0	18.3	7.8	100	89	99	96	0.0	1.9	0.2	0.7	10 ≡	9	0	C 0	C 0	C 0
4	94.8	94.6	93.6	94.3	10.3	14.3	14.5	13.4	15.2	8.6	100	98	91	96	0.0	0.4	1.5	0.6	10 ≡	10	10	SE 1	E 2	C 0
5	93.0	94.3	95.2	94.2	12.7	14.7	10.2	12.0	15.7	10.0	100	64	88	84	0.0	6.0	1.4	2.5	10 •	6	10	N 3	NNE 5	NE 4
6	95.6	96.0	95.1	95.6	7.2	9.7	6.7	7.6	12.0	6.4	100	92	97	96	0.0	0.9	0.3	0.4	10 ≡	10	1	NE 1	E 1	W 1
7	93.5	93.1	91.2	92.6	4.9	8.7	5.8	6.5	12.0	3.0	100	93	100	98	0.0	0.7	0.0	0.2	10 ≡	9	10 ≡	SSW 2	E 1	W 3
8	88.9	87.6	87.7	88.1	7.7	16.0	12.0	11.9	16.3	5.0	91	63	84	79	0.9	6.7	2.2	3.3	8	10	10	W 2	WNW 5	NNW 5
9	88.9	88.2	87.3	88.1	7.5	9.9	6.4	7.6	12.0	5.9	86	62	92	80	1.5	4.6	0.7	2.3	6	9	10	NE 3	N 7	W 3
10	86.0	87.2	88.4	87.2	5.1	7.3	6.3	6.2	8.1	4.9	89	73	84	82	1.0	2.7	1.5	1.7	10	9	10	WNW 5	NW 4	W 2
11	88.8	87.9	87.5	88.1	6.6	9.4	8.2	8.1	10.3	4.5	88	88	79	85	1.1	1.4	2.3	1.6	10	9	10 •	W 4	W 7	WNW 6
12	95.6	97.9	100.1	97.9	0.5	6.4	3.4	3.4	8.2	0.0	94	58	83	78	0.3	4.1	1.3	1.9	1	6	9	N 2	NNE 5	WNW 3
13	100.3	99.6	97.5	99.1	0.9	10.1	5.8	5.6	11.6	0.3	88	48	64	67	0.7	6.5	3.3	3.5	9	2	6	WNW 3	WNW 3	WNW 2
14	96.6	96.3	96.5	96.4	4.1	14.1	6.8	8.0	14.3	2.6	72	41	84	66	2.3	9.5	1.6	4.5	2	4	2	WNW 3	WSW 5	W 2
15	96.1	95.1	94.1	95.1	3.6	17.5	9.3	9.9	17.9	3.4	86	44	48	59	1.1	11.2	6.1	6.1	1	1	0	C 0	SW 4	W 3
16	92.7	90.0	88.7	90.3	3.6	19.9	13.0	12.4	20.4	2.8	85	31	59	58	1.3	16.0	6.2	7.8	2	3	2	SW 2	WSW 4	W 3
17	94.6	97.1	99.9	97.2	7.9	10.0	4.8	6.9	13.0	4.7	86	61	89	79	1.4	4.8	1.0	2.4	9	7	0	W 3	NW 7	W 4
18	99.2	97.9	97.4	98.2	1.8	8.8	3.0	4.2	9.9	0.9	95	63	93	83	0.6	4.2	0.6	1.8	0	3	0	W 2	WNW 5	W 3
19	97.1	98.0	98.6	97.9	5.6	8.7	5.5	6.3	9.9	2.9	94	84	88	89	0.6	1.8	1.1	1.2	10	10	4	WNW 4	W 3	W 3
20	99.7	101.1	103.4	101.4	3.8	7.2	4.3	5.0	7.9	2.7	98	69	81	83	0.1	3.2	1.6	1.6	10 •	8	10	W 3	N 4	NE 2
21	105.7	106.6	107.4	106.6	0.0	3.9	1.4	1.7	4.3	-1.1	94	64	78	79	0.4	2.9	1.6	1.6	10	10	0	C 0	E 3	SE 3
22	108.0	107.5	105.2	106.9	-0.9	1.8	-0.9	-0.2	4.9	-3.1	99	83	94	93	0.0	1.1	0.3	0.3	10 ≡	4	0	S 3	S 1	WSW 1
23	101.4	99.8	98.4	99.9	-1.2	4.1	5.6	3.3	5.6	-2.3	93	83	89	89	0.4	1.2	1.0	0.9	8	10	10	WNW 4	W 3	W 3
24	98.4	99.3	99.6	99.1	3.6	9.1	3.8	3.6	9.7	3.8	94	69	88	82	0.6	4.1	0.9	1.9	9	3	0	NNW 4	N 3	W 3
25	99.7	99.9	99.7	99.8	3.1	3.7	3.1	4.8	6.2	1.8	97	92	94	94	0.2	0.8	0.6	0.3	10	10	10 •	W 3	WNW 3	C 0
26	98.5	97.8	95.4	97.2	4.7	7.3	1.8	3.9	9.9	1.7	93	79	100	91	0.4	2.2	0.0	0.9	10	7	0	C 0	S 2	WNW 1
27	93.3	92.8	92.7	92.9	1.0	12.4	6.2	6.4	12.9	-1.3	96	51	73	74	0.3	7.0	2.4	3.2	3	3	0	SW 2	NW 3	NW 3
28	92.3	91.2	90.7	91.4	3.0	15.4	10.1	10.2	15.7	3.7	79	48	62	63	1.8	9.2	4.7	5.2	2	10	8	NW 4	W 3	W 3
29	90.1	88.3	87.7	88.8	9.4	17.4	11.9	12.6	17.9	8.7	67	44	67	59	3.8	11.2	4.6	6.3	8	3	0	W 3	SW 6	W 3
30	92.1	92.6	92.3	92.3	3.9	10.9	3.2	6.3	11.9	2.7	87	53	90	77	1.3	6.1	0.8	2.7	8	2	0	WNW 2	WNW 6	W 1
31	87.2	85.9	84.5	85.9	6.4	12.4	8.1	8.8	13.3	-0.7	79	53	82	71	2.0	6.7	2.0	3.6	2	9	10 •	W 4	WSW 7	SW 3
M	94.9	94.8	94.6	94.8	5.2	11.3	7.2	7.7	12.3	3.4	91	66	84	80	0.8	3.2	1.7	2.6	6.7	6.4	4.6	2.3	4.0	2.3

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$H_s = 237\,m$ $H_b = 238{,}9\,m$ $h_w = 18{,}2\,m$

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU	POGODA
1	7	0.0	•	•°13^{05-10}; = 0^{00}–8^{10}, ⌒¹$0^{00}$ 2 ⌒²–8 ⌒¹–9 ⌒°–10, 20–24
2	8	•	•	= 3^{30}–7^{35}, 22^{20}–24; ⌒¹$0^{00}$–8 ⌒°–9, 19–22 ⌒¹–24
3	7	•	•	= 0^{00}–9^{30}, ⌒¹$0^{00}$–2 ⌒²–8 ⌒¹ 9 ⌒° 10, 20–24
4	7	0.0	•	•°16^{40}; 17^{25}; = 0^{50}–4^{40}; ⌒°0^{00} 2 ⌒¹–3 ⌒²–8 ⌒¹–9 ⌒° 22–24
5	8	•	•	= 4^{40}–8^{40}; ⌒°0^{00}–3 ⌒¹–8 ⌒°–9, 22–24
6	8	10.8	•	•°14^{10}–16^{40}, 17^{20-40}, 18^{15}–20^{15}; = 20^{15}–24; ⌒°0^{00}–4 ⌒¹–5 ⌒²–9
7	8	4.4	•	•°14^{0}–4^{10} •¹–8^{05} •°–8^{15}; = 0^{00}–10^{20}; ⌒° 20–24
8	7	0.1	•	⚲•°3^{25-40}, 4^{40}–5^{10} 5^{20-30} ⚲•¹–5^{45} ⚲•°–6^{10}, 7^{40-50}, 20^{50} 21^{01}; = 0^{40}–3^{10}, 22^{40} 24; ⌒°0^{00} 2 ⌒¹–3 ⌒° 19–20
9	8	•	•	= 0^{00}–5^{30}; ⌒° 18–23 ⌒¹–24
10	8	•	•	= 2^{30}–9^{20}; ⌒¹$0^{00}$–3 ⌒²–8 ⌒¹–9 ⌒° 20–24
11	8	28.0	•	•°18^{45}–20^{16} •¹–21^{05} •°–21^{15} •¹–22^{10} •°–23^{05}, 23^{10}–24; ⚲ 10^{15}.. 11^{10}; = 17^{20}–24; ⌒°0^{00}–3 ⌒¹–8 ⌒°–9
12	7	•	•	•°0^{00-06} 0^{10}–1^{40} 3^{20}–4^{05}; = 0^{00} 5^{20} 20^{15}–22^{40} ≡°–24; ⌒¹ 20–21 ⌒²–24
13	6	0.1	•	⚲•°15^{50}–16^{12}; ≡°0^{02} 2^{20} ≡¹–4^{40} ≡²–7^{15} ≡¹–7^{35} ≡°–9^{30} ≡°–9^{45} ≡–13^{30}, 20^{20} 24; ⌒²$0^{00}$ 9 ⌒¹–11 ⌒°–12, 21–24
14	6	0.0	•	•°11^{10-16}, 11^{45} 13^{20}; = 0^{00} 3^{40} ≡°–4^{10} ≡¹–5^{30} ≡°–7^{40} ≡–13^{20} 22^{30} 24; ⌒°0–3 ⌒¹–4 ⌒²–8 ⌒¹–9 ⌒°–10, 22–24
15	6	0.6	•	⚲°15^{35}–16^{10}, 17^{15-35}; = 0^{00}–24; ⌒°0^{00}–3 ⌒¹–7 ⌒°–10, 21–22 ⌒¹–24
16	7	•	•	= 0^{00}–6^{25} ≡°–7^{45} ≡–9^{15}, 21^{20}–24; ⌒¹$0^{00}$–2 ⌒²–8 ⌒°–10, 19–21 ⌒¹–24
17	8	•	•	= 0^{00}–2^{45} ≡°–7^{30} ≡–10^{30}; ⌒¹$0^{00}$ 2 ⌒²–8 ⌒¹–10 ⌒°–11, 19–24
18	7	•	•	= 4^{30}–9^{45}; ⌒°0^{00}–9
19	7	•	•	⚲ 14^{10}, 15^{30}; = 23^{20}–24
20	7	•	•	= 0^{00}–5^{20}
21	8	•	•	⌒°0^{00}–3 ⌒¹–8 ⌒°–9, 20–24
22	8	•	•	= 1^{30}–8^{35}; ⌒°0^{00} 2 ⌒¹–8 ⌒°–9 ⌒¹20–24
23	7	•	•	⌒¹$0^{00}$–8 ⌒°–9, 18–20 ⌒¹–21 ⌒²–24
24	7	•	•	= 0^{00}–9^{40}, 20^{20}–24; ⌒²$0^{00}$–9 ⌒°19–22 ⌒²–24
25	7	•	•	= 0^{00-45} ≡°–8^{45} ≡–11^{10}; ⌒²$0^{00}$–9 ⌒°19–24
26	8	0.0	•	= 0^{30}–8^{36}; ⌒°0^{00}–3 ⌒¹–8 ⌒°–9, 19–24
27	7	0.8	•	•°5^{35}..^{50}, 6^{20}..^{45} 8^{40}–9^{20}; = 2^{30}–12^{10}; ⌒°0^{00} 2 ⌒¹–5 ⌒° 22–24
28	8	•	•	⌒°0^{00}–8, 21–24
29	7	2.0	•	⚲°10^{40}–11^{02}, 11^{35}–12^{15}; = 7^{40}–8^{20}; ⌒°0^{00}–7, 21–24
30	8	•	•	⌒°0^{00}–3 ⌒¹–5 ⌒²–9 ⌒° 19–24
31				
Σ	-	46.8	-	

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1	8	•	•	= 3^{30}–5^{20}, 21^{10}–24; ⌒°0^{00} 2 ⌒¹–3 ⌒²–8 ⌒¹–10 ⌒°18–21 ⌒¹–24
2	7	•	•	= 0^{00}–5^{45} ≡¹–6^{20} ≡°–7^{45} ≡–10^{30}; ⌒¹$0^{00}$ 2 ⌒²–10 ⌒¹20–24
3	4	•	•	= 0^{20}–3^{45} ≡°–4^{20} ≡¹–10^{50} ≡–20^{40} ≡°–21^{15} ≡¹–24; ⌒¹$0^{00}$–1 ⌒²–10 ⌒¹–12 ⌒°–13, 18–20 ⌒¹–24
4	5	0.4	•	•°7^{45}–8^{20}; ≡¹$0^{00}$ 1^{20} ≡°–1^{45} ≡–4^{40} ≡°–5^{30} ≡¹–6^{10} ≡²–9^{40} ≡¹–10^{20} ≡°–10^{50} ≡–24; ⌒¹$0^{00}$–4 ⌒²–9 ⌒¹–13 ⌒° 19–24
5	7	0.0	•	•°3^{20}–4^{25}, 5^{55}–6^{40} •°–7^{15}; = 0^{00}–10^{30}, 20^{10}–24; ⌒°0^{00}–3, 22–24
6	5	0.0	•	= 0^{00}–4^{40} ≡¹–6^{15} ≡²–9^{40} ≡¹–10^{30} ≡°–11^{50} ≡–14^{20} 16^{40}–21^{50} ≡°–24; ⌒°0^{00}–2 ⌒¹–3 ⌒²–7 ⌒¹–11 ⌒°18–20 ⌒¹–22 ⌒²–24
7	5	•	•	•°4^{10}–5^{45}; ≡°0^{00-40} ≡¹–5^{30} ≡²–10^{30} ≡¹–11^{40} ≡°–12^{25} ≡–19^{40} ≡°–24; ⌒²$0^{00}$–11 ⌒¹–12 ⌒°–13, 18–20 ⌒¹–24
8	7	0.0	•	•°22^{50}–23^{15}; ≡°0^{00} 1^{35} ≡–4^{20}, 16^{35} 24; ⌒¹$0^{00}$–9 ⌒°–10; ⊕°11^{40}–13^{48}
9	8	0.0	•	⚲°15^{40}..16^{10}; ≡°0^{00}–5^{15}; ⌒°20–22 ⌒¹–24
10	7	0.2	•	⚲°10^{15-35}, 10^{45}–11^{05}; ⌒¹$0^{00}$–2 ⌒°–6
11	7	1.8	•	⚲°19^{55}–20^{20} •°..21^{30}–22^{45}; = 5^{30}–8^{50}; ⌒°0–7
12	8	•	•	⌒°22–24
13	8	•	•	⌒°0^{00}–6; ⊔°3^{50}–4^{00}
14	7	•	•	⌒°4–8
15	8	•	•	
16	7	0.5	•	= 7^{35}–9^{45}; ⌒°5–9
17	8	•	•	•°1^{30}–2^{10}; ⌒°20–22 ⌒¹–24
18	7	•	•	= 4^{20}–10^{40}, 16^{30}–24; ⌒¹$0^{00}$ 2 ⌒²–4 ⊔³5–7 ⌒° 19–24
19	6	0.0	•	= 0^{00}–24; ⌒°0^{00}–7, 21–24
20	7	0.1	•	•°5^{40}–7^{45}; = 0^{00}–11^{36}; ⌒¹$0^{00}$–5 ⌒°23–24
21	7	•	•	= 3^{25}–9^{30}; ⌒°0^{00}–9 ⊔°23–24
22	6	•	•	= 3^{20}–5^{40} ≡¹–9^{45} ≡°–10^{40} ≡–24; ⊔°0^{00}–10, 20–24
23	6	•	•	= 0^{00}–24; ⊔°0^{00}–8
24	7	0.0	•	= 0^{00}–9^{20}
25	5	0.0	•	•°3^{30}–5^{10} •°7^{35}, 8^{40} •°–12^{20}, 19^{40}..20^{10}–21^{10}; = 2^{00}–17^{30}, 19^{35}–24
26	8	•	•	= 0^{00}–9^{20}, 17^{30}–22^{45} ≡°..23^{50} ≡–24; ⌒¹20–22 ⌒¹zm–24
27	6	•	•	= 0^{00}–9^{30} ∞–17^{50} ≡–24; ⌒¹zm 0^{00}–7 ⌒°22–24
28	7	•	•	= 0^{00}–9^{45}; ⌒°0^{00}–9; ⊕°12^{10}–14^{05}
29	7	0.5	•	= 6^{20}–8^{35}
30	7	•	•	•°1^{20}–2^{45} 3^{10-40}; = 1^{20}–5^{15} 17^{40}–24
31	7	0.5	•	•°16^{40}–17^{20}, 19^{40}..20^{15} 21^{40}–22^{35}; = 0^{00}–5^{50} 15^{50}–16^{40} 19^{40}–22^{30}; ⊔°2–6
Σ	-	3.8	-	

Przemyśl $\varphi = 49°48'$ $\lambda = 22°46'$ *Listopad – Novembre 1965*

DNI	CIŚNIENIE P= 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	84.6	81.1	74.7	80.1	6.4	10.5	12.0	10.2	12.0	5.2	79	62	63	68	2.0	4.9	5.2	4.0	10	10 •	9	W 4	WSW 7	SW 7
2	74.6	75.5	79.1	76.4	10.5	15.4	9.3	11.1	16.0	8.2	80	55	70	68	2.6	7.9	3.5	4.7	5	5	5	NW 2	WSW 7	WNW 3
3	82.2	82.6	82.4	82.4	8.1	13.3	7.8	9.2	13.5	6.5	64	45	73	61	3.8	8.5	2.8	5.0	5	2	9	W 3	W 6	C 0
4	88.1	91.8	95.1	91.7	4.9	7.4	1.5	3.8	10.1	1.2	90	63	91	81	0.9	3.8	0.6	1.8	10	6	10	NW 2	WSW 4	W 2
5	98.0	98.8	100.3	99.0	1.1	5.4	1.7	2.5	6.5	0.8	92	74	94	87	0.5	2.4	0.4	1.1	7	8	2	W 3	W 5	WNW 3
6	101.6	100.9	99.1	100.5	2.4	5.1	4.2	4.0	5.5	1.5	89	70	82	80	0.8	2.6	1.4	1.6	9	9	10	W 3	WNW 6	WNW 3
7	94.4	92.8	92.2	93.1	3.5	8.5	3.8	4.9	8.7	1.9	81	59	80	73	1.4	4.6	1.6	2.5	10	9	9	W 4	W 4	WNW 2
8	95.1	96.1	96.8	96.0	-0.2	6.3	-1.5	0.8	6.9	-1.5	94	78	93	88	0.4	2.1	0.4	1.0	10	1	0	WSW 2	E 1	C 0
9	96.0	94.9	93.1	94.7	-4.2	6.7	1.4	1.3	6.7	-4.6	96	69	78	81	0.2	3.0	1.6	1.6	10 ≡	2	0	W 2	ENE 2	W 5
10	91.2	90.4	89.1	90.2	4.1	6.0	5.2	5.1	6.3	0.5	90	85	92	89	0.8	1.5	0.7	1.0	10	10	10	W 3	WNW 3	NE 3
11	84.9	81.8	77.0	81.2	3.0	0.1	-0.6	0.5	5.9	-0.7	90	98	97	95	0.8	0.2	0.2	0.4	10	10 *	10 *	ENE 5	E 7	E 10
12	73.2	74.4	78.0	75.2	-1.1	-0.3	-1.0	-0.8	-0.2	-1.3	99	96	97	97	0.1	0.3	0.2	0.2	10 *	10	10	E 6	E 1	WNW 2
13	79.5	79.4	81.1	80.0	-1.7	-2.2	-4.3	-3.1	-0.9	-4.4	98	96	96	97	0.1	0.2	0.2	0.2	10 •	10 *	10 *	E 5	ENE 5	NE 4
14	81.3	82.1	84.5	82.6	-5.8	-6.0	-6.5	-6.2	-4.3	-6.8	95	94	94	94	0.2	0.2	0.2	0.2	10	10 *	10 *	ENE 5	NNE 4	W 1
15	85.9	88.3	91.5	88.6	-8.5	-4.9	-7.6	-7.2	-4.4	-9.2	92	83	90	88	0.3	0.7	0.3	0.4	10	5 *	10	WSW 1	NW 2	WNW 1
16	94.7	95.9	98.6	96.4	-7.5	-6.7	-9.9	-8.5	-6.6	-10.0	90	80	81	84	0.3	0.7	0.5	0.5	10 *	9	5	WNW 3	NW 3	NW 3
17	99.4	97.7	94.6	97.2	-12.7	-9.6	-15.5	-13.3	-8.7	-15.6	88	85	91	88	0.3	0.4	0.2	0.3	10 *	0	0	C 0	E 3	C 0
18	90.7	87.1	82.7	86.8	-20.9	-11.6	-8.3	-12.3	-8.2	-21.0	89	82	86	86	0.1	0.4	0.4	0.3	2	10	10	C 0	SE 5	SE 4
19	78.5	78.8	76.7	78.0	-5.9	-1.9	-4.0	-4.0	-1.0	-8.5	92	83	94	90	0.3	0.9	0.3	0.5	9	10	0	SE 2	ESE 1	C 0
20	74.5	74.9	74.6	74.7	-4.9	0.0	0.1	-1.2	0.4	-7.3	95	92	98	95	0.2	0.5	0.2	0.3	9	9	10 •	C 0	E 1	C 0
21	70.6	65.0	60.9	65.5	1.9	3.8	3.4	3.1	6.0	-0.5	89	93	100	94	0.8	0.5	0.0	0.4	9	10 •	10 •	S 1	ESE 1	W 4
22	67.9	75.6	82.6	75.4	1.9	0.1	-0.4	0.3	6.3	-0.6	78	73	80	77	1.5	1.7	1.2	1.5	10	9	10	WNW 7	W 8	WNW 2
23	85.7	88.6	91.5	88.6	-1.8	-3.7	-5.5	-4.1	-0.2	-5.7	79	87	82	83	1.1	0.6	0.7	0.8	10	10 *	10	NNE 4	N 7	N 2
24	92.9	92.6	90.8	92.1	-7.7	-5.9	-5.6	-6.2	-5.3	-8.0	93	87	87	89	0.2	0.5	0.5	0.4	10	10	10	NW 2	C 0	SE 4
25	89.5	89.8	90.5	89.9	-4.3	-2.3	-5.7	-3.5	-1.7	-6.1	89	83	87	86	0.5	0.9	0.6	0.7	10	1	10	SSE 2	SE 3	C 0
26	87.7	82.7	79.7	83.4	-5.0	1.4	-0.6	-1.2	1.8	-5.7	78	55	68	67	0.9	3.1	1.9	2.0	0	7	10	S 2	SSW 8	SW 4
27	78.7	73.5	64.5	72.2	1.2	3.3	7.1	4.7	7.3	-0.6	79	74	67	73	1.4	1.9	3.3	2.2	7	9	9	W 1	SSE 3	S 5
28	62.1	63.6	71.1	65.6	4.5	2.1	2.3	2.8	8.1	1.2	93	87	75	85	0.5	0.9	1.8	1.1	10 •	10	10	WSW 2	W 5	W 4
29	77.4	80.7	79.8	79.3	1.0	3.7	1.2	1.8	4.0	0.3	72	60	64	65	1.9	3.2	2.4	2.5	2	6	0	SW 5	WSW 3	SSW 5
30	71.2	71.7	70.5	71.1	6.1	6.7	6.2	6.3	8.9	0.8	56	68	80	68	4.2	3.1	1.9	3.1	8	10	10	SW 9	SW 5	WSW 1
31																								
M	84.4	84.3	84.1	84.3	-1.1	1.7	-0.3	0.0	3.3	-3.0	86	77	84	82	1.0	2.1	1.2	1.4	8.4	7.5	7.5	3.0	4.0	2.8

Grudzień – Décembre

DNI	CIŚNIENIE I	II	III	Dies	TEMPERATURA I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N.w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D.v I	II	III
1	74.6	76.5	80.5	77.2	0.7	4.5	2.7	2.6	6.2	0.4	92	60	60	71	0.5	3.3	2.9	2.2	9	1	0	W 2	SW 7	WSW 7
2	82.7	82.6	82.4	82.6	0.5	5.3	0.2	1.6	5.8	-0.6	67	53	76	65	2.1	4.2	1.5	2.6	2	0	0	SW 5	W 5	S 1
3	76.3	74.7	73.9	75.0	-0.4	3.4	0.5	1.0	4.0	-2.3	66	47	88	67	2.0	4.1	0.7	2.3	0	9	10 *	S 1	WSW 7	S 2
4	73.2	75.9	79.4	76.2	1.8	4.9	0.7	2.0	5.4	0.4	73	58	77	69	2.0	3.7	1.5	2.4	9	4	5	W 3	W 4	W 3
5	80.6	81.1	76.3	79.3	2.6	5.9	3.5	3.9	6.3	-0.6	74	58	60	64	2.0	3.9	3.1	3.0	2	1	5	W 5	WSW 7	SW 6
6	69.2	74.5	79.1	74.3	6.2	5.3	5.3	5.5	6.6	1.9	75	75	72	74	2.4	2.2	2.5	2.4	9	10	8	SW 12	WSW 7	SW 5
7	81.5	83.8	85.0	83.4	6.1	8.1	5.8	6.4	8.3	4.7	64	58	68	63	3.3	4.5	2.9	3.6	10	10	10	WSW 9	SW 5	W 3
8	85.4	85.7	88.9	86.7	3.6	3.7	0.9	2.3	5.8	0.4	86	85	98	90	1.1	1.2	0.1	0.8	10	10 •	10	NW 3	W 2	WNW 4
9	93.3	91.4	83.5	89.4	-0.5	2.8	1.1	1.1	3.6	-1.6	79	69	66	71	1.2	2.4	2.2	1.9	3	8	2	NW 2	S 2	SW 5
10	68.0	64.6	61.9	64.8	6.1	9.7	7.7	7.8	10.4	0.9	69	75	90	78	2.9	2.9	1.0	2.3	8	10	10 •	S 8	WSW 9	S 3
11	63.5	65.6	69.1	66.1	5.5	2.7	0.8	2.4	7.7	0.6	91	93	96	93	0.8	0.5	0.3	0.5	10	10 •	10	WSW 1	NNW 5	WNW 2
12	71.3	73.1	77.1	73.8	0.6	0.4	-0.2	0.2	1.0	-0.3	81	80	94	85	1.3	1.3	0.4	1.0	10	10 *	2	WNW 3	NNW 6	WNW 3
13	79.7	81.4	82.2	81.1	0.5	0.1	-1.9	-0.8	1.3	-2.5	90	78	87	85	0.6	1.4	0.7	0.9	10 *	9 *	9	W 2	NW 4	C 0
14	80.8	86.8	94.1	87.2	-2.6	-2.7	-5.9	-4.3	-1.4	-6.1	95	84	79	86	0.2	0.8	0.8	0.6	10 *	9	9 *	E 3	N 6	NW 5
15	94.6	91.4	90.3	92.1	-7.9	-5.0	-5.9	-4.7	-2.6	-9.0	87	66	87	80	0.4	1.7	0.6	0.9	3	10	10 *	W 4	WSW 5	WNW 6
16	92.5	92.4	93.1	92.7	-6.1	-6.3	-12.5	-9.4	-3.9	-12.6	92	83	89	88	0.3	0.6	0.3	0.4	10	9	0	N 2	ENE 2	W 1
17	92.2	90.4	88.9	90.5	-12.9	-8.4	-3.9	-7.3	-3.7	-14.4	88	83	94	88	0.3	0.5	0.3	0.4	3	10	10 *	NE 1	ENE 2	E 1
18	89.7	89.3	88.3	89.1	0.1	0.9	4.1	2.3	4.3	-4.1	83	83	77	81	1.1	1.1	1.9	1.4	10	10	10 •	W 1	SE 1	W 8
19	87.6	88.5	87.2	87.8	4.3	6.3	7.0	6.2	7.0	3.3	95	86	75	85	0.5	1.2	2.4	1.4	10	10	9	W 6	W 7	WSW 5
20	87.1	89.7	78.8	85.2	7.9	6.1	5.0	6.0	8.3	4.7	72	86	97	85	2.9	1.3	0.3	1.5	9	10 •	10	W 4	W 4	NE 1
21	84.4	82.4	82.5	83.1	3.6	10.2	6.1	6.5	11.3	2.6	98	68	89	85	0.1	3.9	1.0	1.7	10	9	10	C 0	W 5	W 6
22	84.9	86.9	87.4	86.4	1.1	0.5	-0.1	0.4	6.1	-0.2	92	96	94	94	0.5	0.2	0.4	0.4	10 *	10 *	10	NNW 5	NNW 4	N 3
23	87.0	85.3	82.9	85.1	-1.1	-1.1	-2.2	-1.6	0.0	-2.9	83	79	89	84	1.0	1.2	0.6	0.9	10	8	10	NE 5	SE 3	SSE 3
24	77.6	75.0	71.5	74.7	-1.6	-0.5	-1.3	-1.2	-0.2	-2.6	90	88	93	90	0.5	0.7	0.4	0.5	10	9	0	SE 1	S 2	ESE 1
25	67.8	65.2	64.5	65.8	-1.5	1.7	-2.4	-1.2	2.9	-3.5	88	72	93	84	0.7	1.9	0.3	1.0	8	8	10	E 1	C 0	SSE 2
26	64.2	65.6	69.9	66.6	-3.3	-0.4	2.0	0.1	2.3	-3.5	92	88	89	90	0.4	0.7	0.8	0.6	10	10	10	SSE 2	E 1	W 4
27	78.1	78.6	73.8	76.8	0.3	4.2	0.6	1.4	4.6	-0.6	82	47	67	65	1.1	4.3	2.1	2.3	6	0	0	W 3	SW 4	ESE 4
28	66.3	68.6	78.1	71.1	3.7	4.7	1.2	2.7	5.5	0.2	90	89	77	85	0.8	0.9	1.3	1.1	10 •	10	10 *	SW 2	W 2	NW 6
29	82.3	84.1	87.6	84.7	-1.2	0.3	-0.8	-0.6	1.2	-2.1	72	73	79	75	1.6	1.6	1.2	1.5	9	6	9	SW 1	W 3	W 2
30	86.1	83.7	80.3	83.4	-2.5	4.0	2.0	1.4	4.2	-3.2	65	33	58	52	1.8	3.4	3.0	3.4	0	1	10	W 3	SW 6	W 7
31	79.8	79.6	80.4	79.9	1.4	3.5	1.3	2.0	4.0	0.0	74	73	80	76	1.8	1.9	1.4	1.7	10	9	10	W 4	SW 3	WNW 2
M	80.1	80.5	80.6	80.4	0.5	2.5	0.8	1.2	3.9	-1.7	82	73	82	79	1.2	2.1	1.3	1.3	7.7	7.7	7.4	3.4	4.2	3.7

Przemyśl

$H_s = 237\,m$ $H_b = 238{,}9\,m$ $h_w = 18{,}2\,m$

Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	1.5	.	•°12²² 13⁰⁴ 13²⁰ 14⁰⁰ 21³⁰ ⁴⁰ 22⁰³ 23⁴⁰ ≫ 12¹⁵ 13⁰⁵ 19⁴⁵ 20²⁰
2	7	0.6	.	•°14³⁰⁻³⁵ 15⁵⁵ 16¹⁰ 17³⁰ ³⁸ 18⁵⁵ 19⁰⁴ ≫ 14⁴⁰ 16³⁰ (por. 18 m/sek 15⁵⁴, 20 m/sek 16⁰⁵). ⌒°14³⁵⁻⁴⁰
3	8	0.0	.	
4	7	.	.	•°3⁴⁵ 5¹⁵ = 3³⁰ 5²⁵ ⌒°22 24, ⊕°19 20
5	7	.	.	= 4⁴⁰ 9¹², ⌒°0⁰⁰ 5 ⌒°2m 8 ⌒°21 24
6	7	.	.	= 6⁴⁰ 8³⁰, 13²⁰ 24; ⌒°0⁰⁰ 8
7	7	.	.	= 0⁰⁰ 9⁴⁰ 17²⁰ 24
8	6	.	.	= 0⁰⁰ 22⁴⁰ =°- 23³⁰ =¹ 24, ⌣°6 7, 20 24
9	6	.	.	=¹0⁰⁰ 4⁴⁰ =¹- 6¹⁰ =²- 6³⁰ =¹ 6⁴⁰ =°- 9⁴⁵ = 24, ⌣¹0⁰⁰ 10
10	6	0.5	.	•°22¹⁰ 24; = 0⁰⁰ 13⁰ 6²⁰ 23⁴⁰ =° 24
11	4	26.6	.	•°0⁰⁰ 14⁵ •¹ 20⁰ •° 4³⁵ 5⁴⁵ 6¹⁰ 8⁴⁰ 9²⁰ •°- 11³⁰ ⁴⁰°- 10⁴⁰ ×° 11⁴⁰ ×¹ 24, +¹22⁴⁵ 24, ≫ 17¹⁵ 24, =°0⁰⁰ 10⁰ =¹- 15⁰ =°- 23⁴⁰ = 24
12	5	1.4	26	×¹0⁰⁰ 3³⁰ ×°- 8¹⁰ △° 10²⁰ ×° 11³⁰ 12²⁰ △°21⁴⁵ 22⁴⁰, +¹0⁰⁰ 3¹⁵ +°- 6²⁵, ≫ 0⁰⁰ 3¹⁰, = 0⁰⁰ 24
13	4	5.2	22	⌒⌣ 4³⁵ 8³⁵ △°- 8⁴⁰ ×°- 24, = 0⁰⁰ 24, ∩ 4⁴⁰ 8³⁵
14	4	5.8	25	×°0⁰⁰⁻³⁰ △°8⁰⁵ 11⁵⁰ ×¹- 13³⁵ ×°- 21⁴⁰, = 0⁰⁰ 24
15	6	0.0	27	△°0²⁰ 1²⁰ ×°- 3²⁰ 8⁰⁵ 12⁵⁵, = 0⁰⁰ 24
16	6	0.7	28	×°0²⁰ 13⁰ 11¹⁵ 13³⁵ 17³⁰ 20²⁰, 21⁴⁰ 23¹⁵, = 0⁰⁰ 24
17	6	0.0	29	×°14⁰ 23⁰ 5⁴⁵ 6¹⁵ 8⁴⁵, = 0⁰⁰ 13⁵⁴ 14⁴⁰ 24
18	6	1.2	29	×°1⁷⁰ 20¹⁸, = 0⁰⁰ 24
19	6	0.0	25	= 0⁰⁰ 24
20	5	2.0	20	⌒⌣°6³⁵ 9⁴⁵ •°11³⁵ 12¹⁰ 13⁴⁵ 14²⁰ 17⁴⁰ 23²⁰, = 0⁰⁰⁻⁵⁰ =°- 3³⁰ = 15⁴⁵ =°- 17⁵⁰ = 24, ∩ 6³⁵ 11³⁰
21	6	9.1	16	•°8⁴⁰ 12⁴⁸, 13³⁸ 15⁴⁵, 16²⁰, 18¹⁰ 20¹⁰ •°- 21⁴⁰, = 0⁰⁰ 8³⁰, 9⁴⁵ 22²⁰
22	7	0.0	7	•°5⁴⁰ 6¹⁵ ×°8⁴⁰ 9²⁰
23	6	0.7	6	△°2⁴⁵ 3⁰⁶ ×° 7²⁵ 13¹⁵
24	6	0.0	7	△°10⁴⁰ 11³⁵, = 6¹⁰ 13²⁰
25	6	.	7	= 0⁴⁰ 24
26	8	0.0	7	= 0⁰⁰ 13⁰
27	7	2.7	6	×°2⁴⁰ 3¹⁰, ≫ 20⁴⁰ 24, ∞ 7⁴⁰ 12⁴⁰
28	6	11.6	3	•°10⁰ 3⁰ 2⁴⁰ 3²⁵ 7⁴⁰ •¹- 9³⁵ •°- 10⁵⁰ ×°- 11²⁰ •°11³⁰ 12²⁵, ≫ 0⁰⁰ 2³⁰
29	7	.	pł.	
30	8	3.7	pł.	•°11⁴⁵ 12²⁰, 19⁴⁵ 20¹⁰ 23⁴⁰ 24; ≫ 2³⁰ 7¹⁰
31				
Σ		73.3		

Grudzień - Décembre

1	8	.	pł.	•°0⁰⁰ ¹⁰ 2⁴⁵ ×°- 3⁴⁰ ×°- 4⁴³ 5¹⁰, ≫ 19¹⁵ 20²⁰
2	8	.	.	= 8²⁰ 9³⁵
3	8	0.0	.	×°10²⁰ 21⁰⁵; ⌣°1 8
4	8	.	.	⌣°23 24
5	7	0.0	.	≫ 11⁰⁰ 12¹⁰, 20³⁰ 24; ⌣°0⁰⁰ 9; ⊕ 20²⁰ 21⁴⁰
6	8	0.9	.	•°3⁴⁵ 4¹⁰, 6⁴⁸ 8²⁰, 10²⁰ 11¹⁵, ≫ 0⁰⁰ 6⁴⁵ ≫ 7¹⁵ ≫ 11²⁰ (por. do 26 m/sek)
7	8	.	.	
8	6	7.1	.	•°11⁰⁰ 12⁰⁵ 15⁴⁶ ×°- 16⁴⁰ ×°- 19²⁵, = 6⁴⁰ 24
9	7	.	pł.	≫ 22⁴⁰ 23²⁰, = 0⁰⁰ 10²⁰
10	8	0.6	.	•°17³⁵ 18¹⁵ 20¹⁰ 22²⁰, ≫ 7²⁰ 9²⁵
11	6	4.6	.	•°4⁴⁰ 6²⁵, 7⁴⁰ 8¹⁰ 14⁴⁰ ×°- 15³⁵ ×°- 18⁰⁵, = 18⁵⁰ 24
12	6	0.6	.	×°10¹⁰ 14¹⁵, = 0⁰⁰ 14²⁵
13	6	3.1	1	×°5¹⁰ 6²⁰ ×¹- 6⁴⁰ ×°- 6⁵⁰ 8⁰⁵ 9³⁰ 12¹⁵⁻³⁵ = 3⁴⁰ 14³⁰
14	6	2.9	6	×°2⁴⁰ 5¹⁵ ×¹- 6⁴⁰ ×°- 7⁵⁰ ×¹- 8¹⁵ ×° 12¹⁵, 13⁰²⁻⁰⁸, 13¹⁵ 15²⁰ 16⁴⁰ 18²⁵ 20²⁰ 21¹⁰; = 3⁰⁰ 13⁷⁰ 14⁰⁵ 19²⁰
15	7	3.5	8	×°13⁰⁵ 14¹⁵ 23⁴⁰, = 15³⁰ 24
16	7	.	12	= 0⁰⁰ 12¹⁰ 13⁴⁰ 24
17	6	1.6	12	×°9²⁴ 10¹⁵, 10²⁸ 11⁰⁴ 18³⁸ 24; = 0⁰⁰ 24
18	6	6.0	11	×°0⁰⁰ 2²⁵ •°16⁴⁵ 17⁴⁰ 19¹² ²⁵ 20²⁰ 21⁰⁵ 24, = 0⁰⁰ 3⁴⁰ 5³⁰ 13⁴⁰
19	7	.	3	•°0⁰⁰ 6³⁶
20	6	2.2	.	•°9²⁰ 10²⁴ 11¹⁶ 15⁰³⁻²⁶ 15³⁰ 16⁰⁶ 17³⁸, = 10²⁰ 24
21	7	0.7	.	•°22¹⁵ 24, = 0⁰⁰ 10²⁰ 22¹⁰ 24
22	4	3.3	.	•°0⁰⁰ 10⁰ ⁴⁰ 3³⁶ ×°4⁴⁵ 16²⁰ 16³⁰ 18¹⁵ 22⁴⁵ 24, = 0⁰⁰ 24
23	8	.	1	×°0⁰⁰ 2²⁰, = 0⁰⁰ 3¹⁵
24	5	0.2	pł.	×°9²⁵ 11⁴⁵, = 1⁴⁰ 24
25	7	.	1	= 0⁰⁰ 6¹⁰ 7⁰⁵ ⁴⁰ 15³⁰ 24
26	6	0.1	.	•°20¹⁰ 21²⁰ ×°22⁵⁰ 24; ≫ 21⁰⁵ 23⁰⁰, = 0⁰⁰ 24
27	7	1.0	pł.	×°0⁰⁰ 4³⁵, = 0⁰⁰ 4⁴⁰
28	6	2.5	.	×°0³⁵ 1⁴⁰ •°5³⁵ 12¹⁵ •°14¹⁰ 16⁰⁵ ×°10⁴⁵ 21¹⁰, = 12²⁰ 17¹⁰
29	7	.	.	= 7²⁵ 12²⁰
30	7	0.2	.	×°21⁴⁰ 24
31	7	.	.	×° 0⁰⁰ 1⁴⁰
Σ	-	41.1	-	

Zakopane $\varphi = 49°18'$ $\lambda = 19°57'$ *Styczeń — Janvier* 1965

DNI	CIŚNIENIE P=800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	114.1	112.1	110.3	112.2	-5.1	0.5	-1.6	-2.0	9.5	-6.6	87	70	86	81	0.6	1.9	0.7	1.1	7	9	9	SW 1	E 1	C 0
2	105.6	104.5	104.9	105.0	-2.4	-0.1	-1.0	-1.1	0.0	-5.1	96	86	95	92	0.2	0.9	0.3	0.5	10 *	9	10 △	C 0	C 0	C 0
3	106.2	106.5	107.6	106.8	-2.3	-1.7	-3.0	-2.5	-1.0	-3.2	93	92	93	93	0.4	0.4	0.4	0.4	10	10 *	10	C 0	C 0	NE 2
4	109.8	113.1	119.2	114.0	-4.0	-3.9	-5.1	-4.5	-3.0	-5.5	94	89	90	91	0.3	0.5	0.4	0.4	10 *	10 △	10 △	C 0	C 0	NE 2
5	122.8	120.5	121.4	121.6	-7.9	-5.8	-5.3	-4.6	-2.9	-10.4	78	71	85	78	0.7	1.3	0.7	0.9	8	10	5 *	SW 1	W 5	W 4
6	121.8	121.9	119.7	121.1	-3.3	-3.4	-4.8	-4.1	-3.0	-5.0	81	69	88	79	0.9	1.5	0.5	1.0	9	4	10 *	WSW 2	W 5	SW 1
7	121.9	122.3	120.7	121.6	-8.5	-7.1	-16.1	-12.0	-4.8	-16.5	77	72	86	78	0.7	1.0	0.2	0.6	10 *	6	0	C 0	SW 1	SW 1
8	116.4	114.3	109.7	113.5	-7.2	-4.2	-2.9	-4.3	-0.6	-18.4	85	87	93	88	0.5	0.6	0.3	0.5	10 △	10 *	10	C 0	C 0	C 0
9	109.4	108.0	109.4	108.9	1.3	2.9	-0.7	0.7	3.5	-3.0	83	84	93	87	1.2	1.2	0.4	0.9	10	10 ●	10 *	WSW 4	C 0	W 3
10	106.7	105.6	117.6	110.0	-3.3	-0.5	-2.9	-2.4	0.8	-4.3	90	88	88	89	0.5	0.7	0.5	0.6	9	10 *	10 *	C 0	W 2	NE 2
11	124.6	124.8	125.2	124.9	-6.1	-3.9	-11.2	-8.1	-1.9	-12.8	94	70	90	85	0.2	1.3	0.3	0.6	10	2	0	C 0	E 1	C 0
12	123.6	122.1	120.4	122.0	-10.3	-2.7	-10.3	-8.4	-1.8	-13.1	91	73	91	85	0.3	1.3	0.3	0.6	6	6	0	C 0	ENE 1	C 0
13	120.0	120.8	121.7	120.8	-13.1	-2.9	-10.2	-9.1	-1.0	-14.0	84	73	91	83	0.4	1.3	0.3	0.7	0	3	2	C 0	NE 1	C 0
14	119.3	117.5	121.1	119.3	-12.7	-2.1	-3.8	-5.6	2.9	-13.4	85	74	87	82	0.4	1.3	0.6	0.8	0	6	4	C 0	NE 2	SW 1
15	124.9	124.4	121.6	123.6	-1.6	-0.2	-4.0	-2.4	0.4	-6.7	84	84	91	86	0.9	1.0	0.4	0.8	10	9	8	C 0	ENE 1	C 0
16	120.0	121.1	121.4	120.8	-6.6	-1.2	-4.3	-4.1	2.5	-8.4	88	54	79	74	0.4	2.6	0.9	1.3	7	8	7	C 0	ENE 1	NE 1
17	114.7	110.6	105.0	110.1	-9.5	1.6	-2.4	-3.2	6.6	-12.8	91	67	87	82	0.3	2.3	0.7	1.1	9	9	10	NE 1	NE 3	SW 2
18	103.0	102.0	100.2	101.7	0.8	1.0	-1.3	-0.2	7.6	-3.1	70	75	74	73	1.9	1.7	1.3	1.7	8	10	7	SW 4	WNW 3	C 0
19	98.4	97.9	98.6	98.3	-10.9	-1.2	-8.4	-7.2	0.1	-12.1	87	68	80	78	0.4	1.8	0.6	0.9	0	9	8	C 0	ENE 2	C 0
20	93.7	91.5	91.6	92.3	-8.4	-5.1	-8.4	-7.6	-4.7	-11.2	86	88	89	88	0.4	0.5	0.3	0.4	10 *	10 *	6	C 0	C 0	C 0
21	95.0	99.1	105.0	99.7	-7.6	-4.2	-4.1	-5.0	-4.0	-12.7	90	84	87	87	0.3	0.7	0.6	0.5	9	10 △	10	C 0	C 0	N 1
22	108.5	110.2	112.6	110.4	-5.1	-1.6	-9.0	-6.2	-1.5	-10.4	80	63	89	77	0.8	2.0	0.4	1.1	10	3	4	C 0	ESE 1	C 0
23	114.3	115.7	119.9	116.6	-4.7	-1.5	-2.6	-2.8	-0.8	-9.2	83	90	91	88	0.7	0.3	0.5	0.6	10	10 *	10	C 0	C 0	C 0
24	124.1	123.7	123.5	123.8	-3.7	-1.9	-4.1	-3.4	-1.3	-4.4	90	81	94	88	0.5	1.0	0.3	0.6	10	10	10	C 0	NE 1	C 0
25	119.8	118.6	118.1	118.8	-4.7	-1.8	-3.5	-3.4	-1.7	-5.1	88	81	90	86	0.5	1.0	0.3	0.7	10	10 △	3	C 0	ENE 1	C 0
26	116.6	116.2	115.7	116.2	-9.3	-1.9	-9.7	-7.6	-0.5	-11.6	91	67	91	83	0.3	1.8	0.3	0.8	7	4	4	C 0	ENE 1	C 0
27	114.5	114.7	115.2	114.8	-6.5	0.0	-1.5	-2.4	2.3	-9.9	89	73	82	81	0.4	1.7	1.0	1.0	10	8	3	C 0	NE 2	NE 2
28	116.3	117.1	117.0	116.8	3.9	4.6	5.0	4.6	5.7	-2.2	63	61	59	61	3.0	3.3	3.6	3.3	7	9	7	SW 5	SW 5	WSW 4
29	115.3	114.1	114.8	114.7	5.3	6.7	2.7	4.4	7.3	1.6	56	55	83	65	3.9	4.4	1.2	3.2	10	7	7	SW 4	SW 7	SW 1
30	112.4	111.5	112.5	112.1	1.2	4.4	0.3	1.6	6.9	-2.0	89	77	92	86	0.8	2.0	0.5	1.1	9	9	9	NE 3	NE 2	SW 1
31	113.1	114.1	111.9	113.0	4.7	1.6	0.5	1.8	8.2	0.3	77	98	98	91	1.9	0.2	0.1	0.7	10	10 ●	10● ≡	W 1	ENE 1	C 0
M	113.8	113.4	114.0	113.7	-4.8	-1.1	-4.2	-3.6	1.0	-6.0	85	76	87	83	0.8	1.4	0.6	0.9	8.2	8.1	6.9	0.8	1.6	0.9

Luty — Février

1	115.4	116.4	119.0	116.9	-3.1	-4.5	-6.6	-5.2	1.3	-6.8	86	76	75	79	0.7	1.0	0.9	0.9	10	9	10 *	C 0	W 2	WNW 3
2	121.9	123.0	127.3	124.1	-7.3	-7.7	-8.3	-8.0	-6.6	-9.2	85	84	83	84	0.5	0.5	0.5	0.5	10 *	10 *	10 *	SW 3	W 4	NW 1
3	126.7	124.9	124.0	125.2	-12.5	-6.8	-7.2	-8.4	-6.4	-13.2	81	75	82	79	0.4	0.9	0.6	0.6	6	10 *	10 *	W 1	WNW 3	W 2
4	122.8	123.0	121.2	122.3	-7.1	-5.2	-5.6	-5.9	-4.8	-8.3	85	83	92	82	0.5	0.7	0.3	0.5	10 *	9 *	10 *	W 2	SW 2	SW 2
5	116.9	115.6	119.0	117.2	-17.9	-9.7	-20.4	-17.1	-5.6	-21.9	84	60	82	75	0.2	1.2	0.2	0.5	0	0	0	C 0	NW 1	SE 2
6	122.4	121.8	120.2	121.5	-18.3	-12.1	-20.6	-17.9	-11.3	-25.6	84	63	89	79	0.2	0.9	0.1	0.4	10	1	0	NE 1	NE 2	C 0
7	117.6	117.4	113.4	116.1	-21.9	-9.0	-13.5	-14.5	-8.7	-23.3	81	52	68	67	0.2	1.5	0.7	0.8	0	0	2	C 0	ENE 1	SW 2
8	96.8	100.7	103.5	100.3	-5.6	-8.1	-8.5	-7.7	-5.0	-13.7	95	81	89	88	0.2	0.6	0.3	0.4	10 *	9 *	10 *	W 5	NW 3	ENE 1
9	111.6	115.4	121.0	116.0	-11.7	-9.3	-12.8	-11.7	-8.2	-13.1	75	75	77	76	0.6	0.7	0.5	0.6	10 *	9	10	E 1	C 0	0 0
10	120.0	116.4	115.0	117.1	-20.3	-5.7	-7.5	-10.2	-3.8	-22.4	89	50	84	74	0.1	2.0	0.5	0.9	0	4	10 *	C 0	WSW 4	SW 4
11	116.7	119.5	122.8	119.7	-5.7	-4.3	-6.6	-5.8	-3.3	-7.9	87	60	83	77	0.5	1.8	0.6	1.0	10 *	9	9 *	W 1	NE 1	WSW 1
12	123.7	123.1	122.0	122.9	-11.7	-0.7	-3.8	-5.0	1.5	-13.1	82	50	80	71	0.4	2.9	0.9	1.4	2	4	10	C 0	SE 1	SW 1
13	116.9	111.8	106.5	111.7	-2.5	1.9	0.0	-0.2	2.2	-4.8	76	68	73	72	1.3	2.2	1.7	1.7	9	8	8	SSW 1	SSW 6	NE 3
14	103.6	104.2	107.9	105.2	-1.5	0.1	-1.1	-0.9	0.9	-1.9	68	64	77	70	1.8	2.3	1.3	1.8	8	7	8	SW 5	WSW 6	W 4
15	110.7	113.0	113.0	112.2	-3.3	-4.3	-9.7	-6.8	-1.0	-11.6	78	62	78	73	1.0	1.6	0.6	1.1	10 *	9	9	W 4	NW 2	SW 1
16	112.3	112.5	113.5	112.8	-13.2	-5.4	-7.7	-8.5	-5.1	-13.4	84	72	90	82	0.4	1.1	0.3	0.6	9	9	10 *	C 0	ENE 2	NE 1
17	112.3	112.5	114.2	113.0	-9.3	-8.1	-8.5	-8.6	-7.7	-9.8	88	78	86	84	0.4	0.7	0.4	0.5	10 *	10 *	10 *	C 0	C 0	C 0
18	115.3	116.6	118.0	116.6	-7.2	-6.6	-8.6	-7.8	-6.6	-9.0	90	83	86	86	0.3	0.6	0.4	0.4	10 *	10 *	10 *	C 0	ENE 1	E 1
19	119.3	119.4	120.5	119.7	-10.3	-6.9	-8.6	-8.6	-6.7	-10.4	87	75	89	84	0.4	0.9	0.4	0.6	10 *	7 *	9 *	E 1	E 1	ENE 2
20	122.6	124.7	126.3	124.5	-14.9	-7.8	-10.7	-11.0	-7.3	-17.0	82	73	87	81	0.3	0.9	0.4	0.5	3 *	1	10 *	C 0	E 3	NE 2
21	124.0	122.2	119.7	122.0	-13.3	-7.1	-10.8	-10.5	-6.2	-14.0	88	72	90	83	0.3	1.0	0.3	0.5	10 *	0	10	C 0	C 0	E 2
22	114.8	114.6	116.8	115.4	-11.3	-7.2	-11.3	-10.3	-6.5	-17.7	86	77	79	81	0.4	0.8	0.5	0.6	10	10 *	4	C 0	W 4	C 0
23	116.0	115.1	115.1	115.4	-8.7	-6.0	-7.6	-7.5	-5.4	-13.8	83	69	87	80	0.5	1.2	0.4	0.7	10	10	10 *	SW 1	WSW 2	SW 1
24	116.4	115.4	112.6	114.8	-12.0	-6.2	-13.3	-12.2	-5.1	-15.9	82	68	86	79	0.4	1.2	0.3	0.6	9	1	0	C 0	E 2	C 0
25	109.2	107.0	110.5	108.9	-7.9	-4.1	-11.3	-8.6	-3.3	-19.0	73	72	76	74	0.9	1.2	0.6	0.9	10 *	6	3	SW 3	W 4	NW 3
26	112.8	112.5	107.6	111.0	-12.3	-6.7	-9.7	-9.6	-4.4	-14.8	78	57	66	67	0.5	1.6	1.0	1.0	9	1	8	SW 1	SW 4	SW 2
27	100.3	98.1	103.7	100.7	-10.7	-4.7	-11.1	-9.4	-2.6	-12.5	80	61	83	75	0.5	1.6	0.4	0.8	7	10	9 *	SW 2	WNW 8	WSW 3
28	111.2	113.7	114.8	113.2	-11.8	-8.0	-17.5	-13.7	-6.2	-18.3	78	47	85	70	0.5	1.8	0.2	0.8	8 *	0	0	W 3	W 4	C 0
29																								
30																								
31																								
M	115.4	115.4	116.0	115.6	-10.5	-6.1	-9.7	-9.0	-4.7	-13.7	83	68	82	78	0.5	1.3	0.5	0.8	7.9	6.2	7.5	1.2	2.6	1.6

Zakopane — Styczeń - Janvier 1965

$H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘB. ŚNIEGU h	POGODA
1	7	3.2	20	por. wiatru 20 m/sek $2^{15}-3^{30}$; $= 18^{30}-24$
2	6	4.9	22	$*^{0}\,4^{25}\,6^{08}$ $*^{1}\,7^{12}$ $*^{0}-7^{40}$ $*^{1}-8^{05}$ $*^{0}-8^{45}$ $\triangle^{0}\,18^{30}-21^{10}$ $*^{0}\,21^{10}-24$; $= 0^{00}-24$
3	6	7.2	31	$*^{0}\,0^{00}\,1^{22}$ $8^{44}\,9^{35}$ $\triangle^{0}-10^{15}$ $*^{0}-14^{22}$ $\bullet\,16^{45}\,18^{10}$ $\triangle^{0}\,20^{45}\,24$; $= 0^{00}\,15^{20}$, $16^{30}-24$
4	7	5.5	38	$\triangle^{0}\,0^{00}\,1^{40}$ $*^{0}-12^{10}$ $\triangle^{0}-14^{25}$ $*^{1}-18^{12}$ $*^{0}-19^{40}$ $\triangle^{0}-24$; $= 20^{15}-24$
5	8	1.6	42	$*^{0}\,0^{00}-6^{15}$, $13^{15}-19^{15}$ $\overset{*}{\nabla}{}^{0}\,19^{25}-28$ $\overset{*}{\nabla}{}^{1}-19^{35}$ $\overset{*}{\nabla}{}^{0}-20^{48}$, $21^{10}-25$ $\overset{*}{\nabla}{}^{1}-21^{42}$ $\overset{*}{\nabla}{}^{0}-22^{18}$; por. wiatru 12 m/sek $15^{35}-18^{40}$; $\uparrow^{0}\,15^{35}\,18^{40}$; $= 0^{00}-50$
6	9	2.6	46	$*^{0}\,19^{40}\,20^{10}$ $*^{2}-21^{25}$ $*^{0}-22^{05}$ $22^{25}\,24$; $= 20^{10}-24$
7	9	0.2	52	$*^{0}\,0^{00}-20$ $\overset{*}{\nabla}{}^{1}\,1^{06}-18$ $\overset{*}{\nabla}{}^{0}-1^{36}$ $\overset{*}{\nabla}{}^{1}\,1^{54}-2^{07}$ $\overset{*}{\nabla}{}^{2}-2^{15}$ $\overset{*}{\nabla}{}^{0}-2^{25}$ $2^{43}\,3^{15}$ $*^{0}-11^{28}$ $\overset{*}{\nabla}{}^{0}\,12^{23-33}$; $= 0^{00}-10$, $7^{30}\,9^{30}$; $\sqcup^{0}\,17-21$ $\sqcup^{1}-24$
8	6	1.0	48	$\triangle^{0}\,6^{05}\,7^{40}$ $*^{0}-9^{43}$; 10^{09} $12^{15}-13^{08}$ $\triangle^{1}\,20^{07-23}$; $= 10^{30}\,13^{30}$ $16^{15}-22^{30}$; $\sqcup^{1}\,0^{00}-6$
9	7	4.3	42	$\bullet^{0}\,0^{34}\,13^{15}-15^{18}$ $\triangle^{0}\,18^{22}\,19^{40}$ $*^{0}-20^{05}$ $*^{1}-21^{52}$ $*^{0}-23^{45}$ $\triangle-24$
10	6	4.9	45	$\triangle^{0}\,0^{00-10}$ $\overset{*}{\nabla}{}^{0}-0^{16}$ $\overset{*}{\nabla}{}^{2}-0^{35}$ $\overset{*}{\nabla}{}^{0}-0^{43}$ $*^{0}\,9^{43}\,10^{10}$; $10^{20}\,11^{50}$ $*^{1}-12^{15}$ $*^{0}-14^{30}$ $*^{1}-15^{05}$ $*^{0}-16^{10}$; $= 21^{40}\,24$
11	9	•	49	$= 0^{00}\,10^{15}$; $\sqcup^{0}\,18-22$ $\sqcup^{1}-24$
12	8	•	46	$\sqcup^{1}\,0^{00}-10$ $\sqcup^{0}\,18-24$
13	9	•	46	$\sqcup^{0}\,0^{00}-3$ $\sqcup^{1}-9$ $\sqcup^{0}\,18-24$
14	8	•	45	$= 18^{30}\,24$; $\sqcup^{0}\,0^{00}\,11$
15	6	•	42	$= 0^{00-30}$; $8^{15}-11^{30}$; $12^{15}\,16^{20}$; $19^{30}\,24$
16	8	•	40	$= 0^{00-30}$ $17^{30}\,18^{20}$; $\sqcup^{0}\,22-24$
17	9	2.1	39	$\bullet^{0}\,22^{30}\,24$; $\gg 23^{15}\,24$ (por. 17 m/sek); $\sqcup^{0}\,0^{00}-9$; $\nabla^{1}\,3^{40}\,5^{30}$
18	9	•	36	$\bullet^{0}\,0^{00-10}$ $\gg 0^{00}-1^{10}$ (por. 17 m/sek)
19	8	0.0	35	$\sqcup^{0}\,23-24$; $\nabla^{0}\,23^{30}\,24$
20	7	1.1	35	$*^{0}\,6^{32-45}$ $*^{1}-7^{10}$ $*^{0}-10^{17}$ 10^{27-30}; $10^{40}\,11^{10}-13^{38}$; $= 6^{50}\,12^{20}$; $\sqcup^{0}\,0^{00}\,6$, $18-24$; $\nabla^{0}\,0^{00}\,2^{30}$ $\vee^{1}-3^{15}$
21	6	0.0	38	$\triangle^{0}\,12^{15}\,15^{10}$; $= 8^{45}-15^{30}$; $\sqcup^{0}\,0-9$
22	8	•	35	$= 9^{45}-11^{15}$ $21^{30}\,24$; $\sqcup^{0}\,21-24$
23	6	3.0	35	$*^{0}\,9^{36}-20^{35}$ 21^{40}; $22^{05}-24$; $= 0^{00-30}$ $9^{30}\,24$; $\sqcup^{0}\,0^{00}-9$
24	7	1.1	39	$*^{0}\,0^{00}-6^{15}$ $7^{20}\,11^{45}$ $\triangle^{0}\,15^{08}\,17^{14}$ $*^{0}\,18^{07}\,19^{25}$ $21^{22}\,24$; $= 0^{00}\,11^{30}$ $15^{10}-24$
25	7	0.1	42	$*^{0}\,0^{00}-6^{27}$ $\triangle\,12^{15}\,18^{10}$; $= 0^{00}\,6^{30}$ $7^{30}-12^{10}$; $\sqcup^{0}\,22-24$
26	7	•	42	$\sqcup^{0}\,0^{00}-8$, $18-24$
27	7	0.0	40	$*^{0}\,7^{06}-9^{10}$; $\sqcup^{0}\,0^{00}-9$
28	9	•	39	por. wiatru 12 m/sek $7^{00}-8^{30}$, 10 m/sek $12^{10}-13^{15}$
29	9	0.0	34	$\nabla^{0}\,18^{44}-19^{10}$
30	8	0.0	27	$\bullet^{0}\,22^{52}\,23^{20}$; $= 17^{40}-23^{10}$; $\sqcup^{0}\,0-6$
31	4	9.2	25	$\bullet^{0}\,7^{38}-8^{53}$; $9^{22}\,10^{18}-24$; $= 8^{20}\,10^{50}$ $\equiv^{0}-11^{45}$ $= -15^{40}$ $\equiv^{0}-23^{45}$ $= -24$
Σ	-	52.0	-	

Luty - Février

1	8	2.6	22	$\bullet^{0}\,0^{00-10}$ $*^{0}-0^{20}$ $*^{0}-0^{40}$ $*^{1}-2^{15}$ $*^{0}-3^{40}$ $\triangle^{0}\,7^{10}-8^{20}$ $*^{0}-12^{15}$ $\overset{*}{\nabla}{}^{0}\,13^{22}\,17^{10}$; $18^{25}\,20^{30}$ $*^{0}-24$; $= 0^{00}\,12^{20}$
2	5	5.9	34	$*^{0}\,0^{00}\,8^{40}$ $*^{1}-9^{50}$ $\overset{*}{\nabla}{}^{2}-10^{01}$ $\overset{*}{\nabla}{}^{2}-10^{07}$ $*^{0}-10^{30}$ $\overset{*}{\nabla}{}^{1}\,10^{52}$ $*^{0}-11^{41}$ $\overset{*}{\nabla}{}^{1}-11^{46}$ $*^{0}-11^{54}$; 12^{22-45} $\overset{*}{\nabla}{}^{2}-13^{10}$ $\overset{*}{\nabla}{}^{0}-14^{02}$; $14^{25}\,15^{18}$ $\overset{*}{\nabla}{}^{1}-15^{42}$; 16^{18-35} $\overset{*}{\nabla}{}^{0}-17^{17}$; 17^{30-45} $\overset{*}{\nabla}{}^{1}-18^{10}$ $\overset{*}{\nabla}{}^{0}-18^{35}$ $\overset{*}{\nabla}{}^{1}\,18^{45}\,19^{10}$
3	7	0.6	48	$*^{0}\,0^{00}\,3^{44}\,5^{15}$ $\overset{*}{\nabla}{}^{0}\,8^{12}-9^{43}$; $12^{23}\,16^{41}$; $17^{17}\,18^{10}$ $*^{0}-21^{45}$ [2.II: $\overset{*}{\nabla}{}^{0}-19^{33}$ $\overset{*}{\nabla}{}^{1}-20^{10}$ $*^{0}-24$
4	6	7.4	45	$*^{0}\,6^{03}\,7^{10}$ $*^{1}-8^{15}$ $*^{0}-12^{25}$ $\overset{*}{\nabla}{}^{1}-12^{45}$ $\overset{*}{\nabla}{}^{0}-13^{05}$ $\overset{*}{\nabla}{}^{1}\,13^{30}\,16^{10}$ $*^{1}-18^{15}$ $*^{2}-19^{25}$ $*^{1}-20^{10}$ $*^{2}-21^{35}$ $*^{1}-24$; $= 7^{30}\,24$
5	9	•	56	$*^{0}\,0^{00-10}$ $*^{0}-1^{40}$; $= 0^{00-15}$; $\sqcup^{0}\,18-22$ $\sqcup^{1}-24$
6	7	0.2	50	$\triangle^{0}\,7^{10}\,10^{35}$; $= 8^{15}-12^{15}$; $\sqcup^{1}\,0^{00}\,11$; $\sqcup^{0}\,17-24$
7	9	1.6	49	$*^{0}\,21^{45}\,24$; $\sqcup^{0}\,0^{00}\,11$ [8.II: $\overset{*}{\nabla}{}^{2}-22^{25}$ $\overset{*}{\nabla}{}^{1}-22^{40}$ $\overset{*}{\nabla}{}^{0}\,24$; $\uparrow^{0}\,8^{45}\,9^{50}$; $= 4^{15}-11^{50}$
8	6	11.0	48	$*^{0}\,0^{00-30}$; 0^{35} $*^{1}\,0^{40}$ $*^{0}\,10^{15}$ $*^{1}-11^{15}$ $*^{2}-11^{27}$ $*^{1}-11^{50}$ $\overset{*}{\nabla}{}^{0}-12^{10}$ $\overset{*}{\nabla}{}^{1}-12^{20}$ $\overset{*}{\nabla}{}^{2}-12^{35}$ $\overset{*}{\nabla}{}^{1}-14^{20}$ $\overset{*}{\nabla}{}^{2}-14^{50}$ $\overset{*}{\nabla}{}^{0}-15^{30}$ $\overset{*}{\nabla}{}^{1}-16^{10}$ $\overset{*}{\nabla}{}^{2}-16^{25}$ $\overset{*}{\nabla}{}^{1}\,16^{40}$ $\overset{*}{\nabla}{}^{0}\,18^{18}$ $*^{1}-20^{10}$ $*^{2}-21^{32}$ $\overset{*}{\nabla}{}^{1}-22^{18}$
9	8	0.3	66	$\overset{*}{\nabla}{}^{0}\,0^{00-12}$ $\overset{*}{\nabla}{}^{1}-0^{25}$ $\overset{*}{\nabla}{}^{2}-0^{55}$ $\overset{*}{\nabla}{}^{1}-1^{10}$ $*^{1}-1^{40}$ $*^{0}-7^{15}$ $\triangle^{0}-8^{10}$ $*^{0}-9^{15}$ $\overset{*}{\nabla}{}^{0}\,13^{35-42}$; $15^{35}\,16^{10}$ $*^{0}\,18^{20}$; 20^{35}; 21^{05}; 22^{20}
10	9	1.0	60	$*^{0}\,18^{40}$; $20^{15}\,24$; $\sqcup^{0}\,0-1$ $\sqcup^{1}-10$
11	8	0.6	67	$*^{0}\,0^{00}\,7^{14}$ $\overset{*}{\nabla}{}^{0}\,7^{52}\,8^{10}$ $\overset{*}{\nabla}{}^{1}-8^{20}$ $\overset{*}{\nabla}{}^{0}-10^{42}$ $\overset{*}{\nabla}{}^{1}-10^{50}$ $\overset{*}{\nabla}{}^{0}-10^{53}$; $12^{47}\,16^{45}$ $*^{0}-23^{35}$
12	9	•	55	$*^{0}\,21^{42}\,24$; $\sqcup^{0}\,4-9$
13	9	•	53	$*^{0}\,0^{00}\,1^{45}$; $\vee^{0}\,18^{20}\,19^{30}$; $20^{25}-22^{30}$
14	9	0.1	45	$\overset{*}{\nabla}{}^{0}\,15^{32}\,16^{03}$; $17^{48}\,18^{07}$; 23^{15-28}
15	8	0.7	44	$\overset{*}{\nabla}{}^{0}\,6^{18}\,7^{00}$ $\overset{*}{\nabla}{}^{1}-7^{35}$ $\overset{*}{\nabla}{}^{0}-8^{22}$ $\overset{*}{\nabla}{}^{1}-9^{40}$ $\overset{*}{\nabla}{}^{0}-11^{40}$; $\sqcup^{0}\,21-24$; $\nabla^{1}\,20^{15}\,24$
16	7	6.2	42	$\overset{*}{\nabla}{}^{0}\,11^{50}\,16^{40}$ $*^{0}-24$; $\sqcup^{0}\,0-8$; $\nabla^{1}\,0^{00}\,4^{30}$
17	6	7.2	62	$*^{0}\,0^{00}\,2^{45}$ $*^{1}-9^{40}$ $*^{0}-11^{25}$ $*^{1}-11^{45}$ $*^{0}-15^{20}$ $*^{1}-17^{10}$ $*^{0}-21^{45}$; $= 21^{15}\,24$
18	6	12.6	73	$\triangle^{0}\,0^{15}\,1^{30}$ $*^{0}-8^{02}$ $*^{1}-10^{35}$ $*^{0}-14^{40}$ $*^{1}-24$; $= 0^{00}\,24$
19	8	4.3	80	$*^{1}\,0^{00-30}$ $*^{2}-7^{38}$ $*^{1}-8^{50}$ $\overset{*}{\nabla}{}^{0}-11^{10}$ $*^{0}\,12^{20}$; $15^{30}-17^{25}$ $*^{1}-18^{40}$ $*^{0}-20^{01}$ $*^{1}-24$; $= 0^{00}-8^{30}$; $22^{30}\,24$
20	7	0.0	88	$*^{1}\,0^{00}-3^{12}$ $*^{0}-9^{33}$ $9^{35}\,10^{15}$ $20^{18}-23^{10}$; $= 0^{00}-11^{30}$; $16^{30}\,24$
21	7	0.0	84	$*^{0}\,6^{25}\,9^{18}$; $= 0^{00}\,10^{05}$ $20^{20}\,22^{15}$; $\sqcup^{0}\,20-24$
22	5	2.2	78	$*^{0}\,6^{45}$; 7^{35} $*^{1}-8^{05}$ $*^{0}-12^{25}$ $*^{1}-13^{45}$ $*^{0}-14^{35}$ $*^{1}-17^{15}$ $*^{0}-19^{10}$; $= 0^{00}-1^{40}$; $2^{15}\,4^{50}$; $11^{30}\,19^{15}$; $\sqcup^{0}\,0^{00}\,2$
23	7	1.5	80	$*^{0}\,3^{35}\,5^{00}$; $7^{45}-8^{40}$ $\overset{*}{\nabla}{}^{0}-10^{20}$ $\overset{*}{\nabla}{}^{1}-10^{38}$ $\overset{*}{\nabla}{}^{0}-11^{35}$ $*^{0}\,12^{10-38}$; $13^{38}\,15^{10}-16^{10}$ $*^{1}-17^{20}$ $*^{0}-24$; $= 15^{30}\,24$
24	8	0.0	78	$*^{0}\,0^{00}-3^{35}$; $= 0^{00}-8^{20}$; $\sqcup^{0}\,21-24$
25	8	4.9	68	$\overset{*}{\nabla}{}^{0}\,4^{10-45}$ $*^{0}\,6^{15}-7^{50}$ $\overset{*}{\nabla}{}^{0}\,14^{11}-15^{32}$ $\overset{*}{\nabla}{}^{1}-16^{20}$ $\overset{*}{\nabla}{}^{0}-16^{27}$ $\overset{*}{\nabla}{}^{1}\,17^{10-20}$ $\overset{*}{\nabla}{}^{2}-19^{30}$ $\overset{*}{\nabla}{}^{1}-20^{10}$; $22^{45}\,23^{20}$; $= 17^{15}-20^{10}$; $\sqcup^{0}\,0^{00}\,4$
26	9	0.0	80	$*^{0}\,7^{35}$; $8^{00}\,6^{15}$ $\overset{*}{\nabla}{}^{0}\,7^{20-35}$
27	8	3.0	76	$\overset{*}{\nabla}{}^{0}\,13^{25-30}$ $\overset{*}{\nabla}{}^{1}-13^{40}$ $\overset{*}{\nabla}{}^{0}-13^{45}$; 16^{20-22} $\overset{*}{\nabla}{}^{1}-16^{32}$ $\overset{*}{\nabla}{}^{0}-16^{35}$; $16^{42}\,17^{10}$ $\overset{*}{\nabla}{}^{2}-17^{40}$ $\overset{*}{\nabla}{}^{0}-18^{06}$; $19^{42}\,20^{10}$; $20^{33}\,21^{25}$ $\overset{*}{\nabla}{}^{1}-23^{25}$ $\overset{*}{\nabla}{}^{2}\,24$; $\uparrow^{0}\,9^{50}\,13^{45}$ $\uparrow^{+1}\,17^{15-50}$ $\uparrow^{1}\,23^{25}\,24$
28	9	0.0	78	$\overset{*}{\nabla}{}^{2}\,0^{00}\,1^{40}$ $\overset{*}{\nabla}{}^{1}-2^{25}$ $\overset{*}{\nabla}{}^{0}-3^{15}$ $\overset{*}{\nabla}{}^{1}-3^{35}$ $\overset{*}{\nabla}{}^{0}-5^{10}$ $\overset{*}{\nabla}{}^{1}-5^{50}$ $\overset{*}{\nabla}{}^{0}-7^{18}$; $\uparrow^{1}\,10^{00-30}$ $\uparrow^{2}-14^{0}$ $\uparrow^{1}-20^{25}$ $\uparrow^{0}-23^{45}$; $\sqcup^{0}\,21-24$
29				
30				
31				
Σ	-	73.9	-	

Zakopane $\varphi = 49°18'$ $\lambda = 19°57'$ *Marzec – Mars* 1965

Dni	Ciśnienie P=800 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	109.9	108.7	105.3	108.0	-5.5	-0.9	-4.1	-5.1	2.0	-18.5	52	63	87	67	2.3	2.1	0.6	1.7	7	10	10	SW 6	WSW 8	NE 4
2	98.4	96.8	94.3	96.5	3.8	6.5	5.5	5.3	7.2	-4.4	62	62	79	68	3.0	3.5	1.9	2.8	9	7	8	SSW 5	S 5	SE 1
3	92.4	96.3	100.2	96.3	1.7	2.9	-2.5	-0.1	5.5	-2.5	86	50	63	66	0.9	3.7	1.9	2.2	10 •	4	10	S 2	SW 8	C 0
4	103.9	105.2	107.0	105.4	-8.9	-2.9	-5.9	-5.9	-2.3	-9.5	70	47	74	64	0.9	2.6	1.0	1.5	1	9	7	NE 1	W 6	NE 1
5	107.7	109.0	112.9	109.9	-9.5	2.5	-1.6	-2.6	4.1	-13.2	82	60	84	75	0.5	2.8	0.9	1.4	7	4	10 *	C 0	W 7	C 0
6	112.8	112.8	116.9	114.2	-4.9	-0.7	-2.3	-2.6	1.4	-5.5	86	91	96	91	0.6	0.5	0.3	0.5	10	10 *	10	C 0	C 0	C 0
7	119.8	121.6	123.4	121.6	-5.5	-4.9	-7.0	-6.1	-2.3	-7.0	92	93	91	92	0.3	0.3	0.3	0.3	10	10 △	10 △	SE 1	ENE 1	NE 2
8	122.4	121.9	122.6	122.3	-8.0	-5.3	-7.7	-7.2	-4.9	-8.4	90	80	84	85	0.3	0.8	0.5	0.5	10 *	10 *	10 *	ENE 1	NE 2	C 0
9	122.8	123.0	124.9	123.6	-8.5	-4.0	-10.6	-8.4	-5.7	-11.5	85	75	87	82	0.5	1.1	0.4	0.7	10 *	9	9	C 0	ENE 1	C 0
10	126.1	128.5	130.7	128.4	-7.2	-5.0	-0.5	-6.8	-2.6	-12.7	82	62	85	76	0.6	1.9	0.5	1.0	10 *	5	3	SE 1	NE 2	C 0
11	131.0	131.0	130.2	130.7	-14.1	0.2	-9.0	-8.0	1.0	-16.9	79	48	86	71	0.4	3.3	0.4	1.4	0	0	0	C 0	ENE 1	S 1
12	129.6	127.8	127.6	128.3	-13.3	2.7	-6.2	-5.8	3.8	-14.3	84	45	84	71	0.4	4.1	0.6	1.7	0	1	5	C 0	E 1	C 0
13	126.9	126.6	127.6	127.0	-10.0	3.4	-4.1	-3.7	4.1	-11.5	91	48	80	73	0.3	4.1	0.9	1.8	1	0	1	C 0	ENE 1	C 0
14	126.4	125.4	125.6	125.8	-9.2	6.0	-2.7	-2.2	7.9	-10.1	88	45	81	71	0.4	5.2	0.9	2.2	1	1	0	C 0	NE 2	SW 1
15	125.5	125.2	125.3	125.3	-5.7	7.5	-0.3	0.8	8.5	-6.8	80	46	90	72	0.9	5.7	0.7	2.4	7	5	0	C 0	NE 1	C 0
16	122.7	119.9	120.0	120.9	-2.5	9.9	2.1	2.9	10.2	-5.5	89	40	85	71	0.6	7.2	1.1	3.0	7	8	9	C 0	SSE 4	C 0
17	118.6	116.6	114.9	116.7	1.3	4.0	1.8	2.2	4.3	0.1	96	89	94	93	0.2	0.8	0.4	0.5	10 •	10 •	9	C 0	E 1	SE 1
18	113.0	112.0	111.2	112.1	-2.8	6.6	-0.5	0.7	7.5	-5.2	91	53	88	77	0.5	4.5	0.8	1.9	2	1	1	C 0	ENE 2	C 0
19	110.8	112.1	113.5	112.8	-3.5	10.0	3.0	3.1	10.2	-4.4	90	45	84	73	0.5	6.7	1.2	2.8	8	3	10	C 0	ENE 1	SW 1
20	118.0	119.1	118.9	118.7	2.0	1.4	-0.2	0.8	3.2	-0.4	94	96	96	95	0.4	0.3	0.2	0.3	10 •	10 •	9	C 0	C 0	C 0
21	116.0	111.9	109.7	112.5	-2.9	7.2	5.9	4.0	8.5	-5.6	95	58	69	74	0.2	4.3	2.9	2.5	9	8	10 •	C 0	SSW 7	W 3
22	110.7	115.1	117.2	114.3	1.6	-2.8	-7.1	-5.8	5.9	-7.2	98	93	91	94	0.2	0.4	0.3	0.3	10 *	10	3	NE 2	NE 2	SW 1
23	115.2	112.6	109.3	112.4	-9.5	1.9	0.0	-1.9	5.3	-11.6	85	56	70	70	0.4	3.1	1.8	1.8	0	4	2	C 0	NE 1	SE 2
24	107.7	108.1	109.9	108.6	0.8	3.5	1.3	1.7	4.0	-1.2	85	79	98	87	1.1	1.6	0.1	0.9	10	10 •	10 •	C 0	E 1	C 0
25	112.6	113.2	117.5	113.1	2.7	4.1	0.8	2.1	5.2	0.4	91	60	85	79	0.6	3.2	1.1	1.6	10 •	6	6	W 2	W 6	C 0
26	118.3	116.3	116.0	116.9	0.8	6.5	0.7	2.2	6.7	0.0	90	38	98	75	0.7	6.1	0.1	2.3	9	7	10	SE 1	NW 3	W 1
27	120.8	123.4	131.0	125.7	0.4	0.3	0.0	0.2	1.1	-0.5	98	94	96	96	0.1	0.3	0.2	0.2	10 *	10 *	10 △	C 0	WNW 1	C 0
28	132.7	132.5	132.0	132.4	-0.8	4.2	1.6	1.6	5.4	-1.2	95	65	90	83	0.3	2.8	0.7	1.3	10	5	7	C 0	C 0	SE 1
29	130.6	130.8	130.4	130.6	2.1	4.7	3.8	3.6	5.6	0.5	91	95	98	95	0.6	0.4	0.1	0.4	10 •	10 •	10	C 0	SW 1	C 0
30	126.9	123.5	123.4	124.6	3.7	11.1	4.3	5.8	12.5	2.8	98	63	80	80	0.2	4.9	1.7	2.3	10	7	10	C 0	SW 3	N 3
31	125.9	123.5	123.4	124.8	-5.3	1.3	-0.2	-0.6	4.3	-4.1	90	70	86	82	0.5	2.0	0.8	1.1	1	8	9	S 1	WSW 3	NE 1
M	117.9	117.9	118.5	118.1	-5.6	2.7	-1.6	-1.0	4.2	-6.1	87	65	86	79	0.6	2.9	0.8	1.4	7.1	6.5	7.0	0.7	2.6	0.8

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1	126.1	128.3	129.1	127.8	-4.7	-1.8	-4.0	-5.6	-0.2	-6.0	79	57	84	73	0.9	2.3	0.7	1.3	9 *	9	6	NNW 3	SW 1	SW 2
2	126.6	124.8	126.2	125.9	-2.3	5.9	3.4	2.6	7.3	-6.1	74	48	71	64	1.4	4.8	2.3	2.8	6	7	8	SW 3	WSW 4	S 1
3	123.6	121.7	119.9	121.7	1.8	9.1	3.4	4.4	11.3	0.1	74	29	56	53	1.9	8.2	3.4	4.5	2	0	0	C 0	WSW 2	C 0
4	118.1	117.5	115.9	117.2	2.1	10.3	4.1	5.2	11.9	-0.5	63	30	58	50	2.6	8.7	3.4	4.9	8	8	7	W 1	W 4	S 1
5	116.3	118.8	120.4	118.5	3.3	8.8	-0.1	3.0	9.5	-0.1	73	30	84	63	1.8	7.8	1.0	3.5	8	3	0	SW 1	NE 2	SW 1
6	120.9	119.7	118.1	119.6	-0.1	11.2	1.9	3.7	12.5	-3.3	74	38	83	65	1.6	8.3	1.2	3.7	1	1	0	C 0	WSW 1	C 0
7	116.7	116.2	116.9	116.6	1.0	13.9	4.8	6.1	14.9	-1.1	89	34	91	71	0.8	10.5	0.7	4.0	4	7	9	C 0	WSW 2	SW 1
8	115.0	114.1	113.7	114.3	3.7	10.0	5.1	6.0	10.8	2.0	97	68	92	86	0.3	4.0	0.7	1.7	8	6	10	C 0	ENE 3	C 0
9	111.8	110.3	110.4	110.8	4.0	5.8	1.0	3.0	6.3	1.0	98	94	98	97	0.1	0.6	0.2	0.3	10	10	10 •	C 0	NE 2	NE 3
10	111.1	112.6	113.5	112.4	-1.6	-1.6	-2.7	-2.2	1.0	-3.0	96	91	97	95	0.2	0.4	0.1	0.2	10 *	10 *	10	NE 3	NE 3	NE 3
11	112.2	112.6	113.8	112.9	-1.6	4.4	3.3	2.4	5.1	-3.2	94	85	95	91	0.3	1.3	0.4	0.7	8 *	10	10	NE 1	NNE 1	SW 1
12	115.5	116.0	116.3	115.9	2.7	5.0	3.7	3.8	5.7	2.3	98	87	95	93	0.1	1.1	0.4	0.5	10 •	10	10 •	C 0	C 0	C 0
13	114.7	114.0	114.8	114.5	3.5	5.9	3.3	4.0	6.3	2.7	95	80	93	90	0.4	1.9	0.4	0.9	10 •	10	10 •	C 0	E 1	C 0
14	115.5	118.0	120.0	117.8	2.9	3.0	2.9	2.9	4.7	1.7	95	95	93	94	0.4	0.4	0.5	0.4	10 •	10 •	10	C 0	E 1	C 0
15	119.8	118.6	117.6	118.7	0.5	6.3	1.9	2.6	7.2	0.1	90	66	90	82	0.6	3.2	0.7	1.5	9	5	10	NE 2	E 1	NE 1
16	114.9	113.4	113.6	114.0	0.7	9.5	2.7	3.9	10.3	-2.2	88	55	75	73	0.8	5.3	1.8	2.6	4	7	4	C 0	SE 5	SSE 1
17	115.1	115.2	112.5	114.3	0.6	7.7	4.0	4.1	8.5	-1.6	84	69	95	83	1.0	3.3	0.4	1.6	7	8	10	C 0	N 4	NE 1
18	105.8	105.0	106.9	105.9	2.3	8.1	3.9	4.6	9.2	0.9	95	56	84	78	0.4	4.8	1.3	2.2	10	10	9	C 0	NE 1	C 0
19	105.2	104.5	102.8	104.2	3.7	7.6	5.1	5.4	9.7	2.5	92	77	92	87	0.7	2.4	0.7	1.3	10	10 •	10	C 0	C 0	C 0
20	102.2	103.5	104.8	103.5	4.4	8.1	4.2	5.2	10.2	2.6	95	82	89	89	0.5	2.0	0.8	1.1	9	10 •	4	SW 1	NE 2	SE 1
21	102.9	101.1	99.5	101.2	3.3	9.0	5.1	5.6	10.0	1.2	87	72	97	85	0.9	3.3	0.3	1.5	8	8	10 •	C 0	ENE 3	ENE 3
22	98.0	98.7	100.5	99.1	0.8	1.9	1.8	1.6	5.1	0.8	96	94	91	94	0.3	0.4	0.7	0.5	10 *	10 *	10 •	SW 2	SW 1	SW 3
23	100.7	101.6	104.2	102.2	1.3	4.1	2.3	2.5	4.7	0.7	92	74	88	85	0.5	2.1	0.8	1.1	10 *	7	10	W 1	WNW 3	SW 2
24	105.7	108.0	110.6	108.1	2.4	4.7	2.3	2.9	6.8	1.1	83	66	76	73	1.2	2.8	1.7	1.9	9	9	7	SW 1	W 3	W 1
25	113.1	114.0	114.3	113.8	4.1	8.8	4.0	5.2	10.4	-1.0	70	50	83	68	2.5	5.7	1.4	3.2	9	8	4	C 0	W 3	W 1
26	112.8	113.2	112.0	112.7	4.6	3.9	0.3	2.4	7.0	0.4	78	89	98	88	1.8	0.9	0.1	0.9	10 •	10 •	10 *	C 0	NE 1	C 0
27	107.5	106.5	106.5	106.8	-1.5	9.2	3.3	3.6	10.4	-2.6	100	43	82	75	0.0	6.5	1.3	2.6	3	8	7	C 0	SSW 2	C 0
28	103.6	104.5	110.1	106.1	4.3	8.0	1.1	3.6	9.4	-0.1	95	64	83	81	0.4	3.9	1.1	1.8	10 •	7 •	0	C 0	SSE 3	S 1
29	111.3	111.3	114.2	112.3	3.5	9.4	4.4	5.4	10.0	-2.2	64	40	88	64	2.7	7.0	1.0	3.6	9	8	10	C 0	NE 2	SW 2
30	116.7	117.4	120.0	118.0	3.8	8.7	4.1	5.2	9.7	2.8	86	57	89	77	1.1	4.8	0.9	2.3	9	7	10 •	C 0	C 0	NW 3
31																								
M	112.6	112.7	113.3	112.9	1.8	6.8	2.7	3.5	8.2	-0.3	87	64	86	79	0.9	4.0	1.0	2.0	8.0	7.8	7.5	0.6	2.2	1.1

Zakopane — $H_s = 844\,m$ — $H_b = 838{,}2\,m$ — $h_w = 17{,}7\,m$ — Marzec – Mars 1965

DNI	WILGOTNOŚĆ V	OPAD R	GRUBOŚĆ PŁYWU h	POGODA
1	8	0.1	75	*°10^50–12^30, por. wiatru 12 m/sek 10^30–11^30, 14 m/sek 13^30–14^30, do 12 m/sek 23^20–24; ⊥°6^50–7^45, 9^45–14^50; ⊔°0^00–3
2	9	1.0	67	por. wiatru do 14 m/sek 0^40–55 ≫–1^30 (por. 17 m/sek), por. wiatru do 12 m/sek 1^30–3^30 ≫–3^50 (por. 17 m/sek), por. wiatru do 12 m/sek 3^50–4^30, 5^05–13^15
3	9	0.0	50	•°3^45–4^20–5^25, 6^38–7^18 ⚲°9^35–10^20 ⚲°14^20–33
4	9	•	46	⊔°4–9
5	9	0.0	45	*°7^50–8^05, 10^32–21^15
6	5	2.7	43	*°7^35–8^10–11^16 *¹–13^25 *°–14^40 △°15^35–19^10; = 5^30–24
7	7	2.4	43	△°9^30–11^38, 12^10–17^20, 18^30–24; = 0^00–7^20 ≡°–9^50 = –11^30, 21^30–24; V^p 7^20–9^50
8	5	2.3	46	△°0^00–6^15 *°–24; = 0^00–24
9	6	0.1	48	*°0^00–3^30, 6^10–8^40, 11^07–12^15, 13^04–14; = 0^00–7^30, 8^50–16^30
10	7	0.3	49	*°3^20–6^30 *²–6^45 *¹–6^55 *°–7^20 ⚲°7^35–9^18
11	9	•	46	⊔°0^00–3 ⊔¹–8 ⊔°20–24
12	8	•	45	⊔°0^00–8, 22–24
13	9	•	44	⊔°0^00–8, 21–24
14	9	•	43	⊔°0^00–9
15	9	•	39	⊔°0^00–7, 21–24
16	9	0.8	37	⊔°0^00–8
17	6	4.8	30	•°6^05–15 •¹–7^10 •°–10^53, 11^07, 11^52, 12^12–19^35; = 8^20–17^30 ≡¹–18^50 = –20^15
18	9	•	26	⊔°0^00–8
19	9	0.0	24	⊔°2–7
20	5	2.4	20	•°5^42–7^15 •*°–7^46 *°–8^10 •°–13^50 *°–14^06 •°–15^20 *°–15^45 •°–16^50 •°–17^18; = 5^20–22^30
21	9	0.2	17	•°20^05, 21^15; ⊔°1–8
22	6	1.4	15	•°0^40, 1^25 *°6^35–7^50 △°–8^05 *°–10^45; = 6^30–15^30
23	9	•	14	⊔°0–7
24	7	7.5	12	•°12^07–13^10, 13^20–16^55 *°–17^15 •°–22^38; = 7^15–9^40, 15^30–20^30
25	8	1.7	10	⚲°6^05–28 ⚲¹–7^12 ⚲°–7^20
26	9	4.7	8	•°0^25–2^30 *°–3^40 *°7^50–18^15 •°–19^42 *°–20^15 △°21^32–22^10 •°–23^15 *°–23^35 •°–24; = 3^30–6^10, 23^20–24
27	6	14.1	8	•°0^00–30 *°–1^45 •°–3^05 *°–3^30 *°–4^40 •°–5^26 *°–5^37 *°–6^35 *¹–7^17 *°–8^20 *¹–9^18 *²–9^42 *°–9^48 *¹–11^20 *°–15^10 △¹–15^20 △°–24; = 0^00–24
28	8	0.0	12	△°0^00–1^50; = 0^00–8^35
29	6	4.5	8	•°6^25–44–8^40 •°12^05–15^15 •¹–17^44 •°–19^40 •°–20^15; = 12^40–24
30	8	0.0	5	•°1^45–2^15, 2^20–5^50 ⚹°23^07–12 ⚲°–23^17; = 0^00–5^30, 6^20–7^30
31	8	6.9	pł.	*°⚲12^50–13^08, 13^20–14^16 *¹–14^30 *°–14^55, 15^05–25 *¹–15^43 *°–16^27, 16^45–17^15 *¹–18^07 *°–18^25 *¹–19^10 *°–20^35 *¹⚲22^23–23^18 *°–24
Σ	–	57.9	–	

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1	8	0.2	10	*°⚲0^00–14 *¹⚲0^32–45 *°–0^52 *°⚲1^41–2^35 *¹–3^15 *°–3^40, 4^35–6^45 *¹–7^18 *°–9^42, 10^54–12^10, 13^08–30
2	9	•	4	
3	9	•	pł.	
4	8	•	pł.	⊔°4–8
5	9	•	•	⊔°21–24
6	9	•	•	⊔°0^00–7, 22–24
7	8	1.5	•	= 19^30–24; ⊔°0^00–8
8	7	0.0	•	•°1^48–2^07 •°–2^22 •¹–2^40 •°–3^38 ⚲°12^02–10; = 0^00–4^30, 9^20–12^30, 17^30–24
9	6	1.0	•	•°7^54–8^12, 11^02–12^15 •°17^10–22^40; = 0^00–24
10	6	0.3	1	△°3^35–6^25 *°–13^35–14^45 △°15^48–19^50; = 0^00–4^2 ≡°–4^45 = –24
11	6	0.3	1	*°6^15–7^40 •°14^18–15^25, 21^36–24; = 0^00–9^30, 11^30–15^30, 18^30–24
12	6	2.2	•	•°0^00–25 •°4^40–6^15 •°–7^25 •°–11^45, 18^35–20^20–22^17; = 0^00–24
13	7	1.9	•	•°0^18–2^35, 3^10–5^40, 6^25–7^20–8^40, 9^10–10^35 ⚲°10^50–11^20, 13^55–15^20 •°17^05–18^20, 18^30–21^33; = 0^00–10^30, 18^40–21^15
14	6	4.7	•	•°3^42–6^30–7^25 *°–7^30 •°–10^25 ⚲°12^12–29 △¹–12^36 ⚲°–13^25, 14^17–22, 15^02–44, 16^18–35 ⚹¹16^48–17^10 *°–17^22, 17^28–19^00 •°20^45–21^25; = 6^15–19^30, 18^20–24
15	8	0.0	•	⚲°16^42–56; = 0^00–3^0, 3^50–7^40
16	8	•	•	⊔°3–6
17	8	0.7	•	⚲°13^29–15^45; = 18^40–24; ⊔°0–7; ⊕¹6^30–7^20
18	9	0.2	•	= 0^00–1^20
19	7	4.2	•	•°0^50–1^50–3^35, 8^10–10^22, 11^42, 13^17 ⚲°15^15–16^06 ⚲¹–16^13 ⚲°–16^20 •°19^43–20^17, 21^05–22^45
20	7	1.5	•	⚲°10^28–11^06, 11^32–51 ⚲¹–12^11 ⚲°–12^15, 12^32–13^12
21	8	17.3	•	⚲°9^03–10^17, 14^15–22 ⚲¹–14^35 ⚲°–15^18 ⚲¹–16^06 ⚲°–16^47, 17^20–18^35 •°20^10–35 •¹–22^15 •°–24; = 20^10–24
22	6	14.4	•	•°0^00–1^25 ••°–1^35 •°–5^18 *°–5^40 *°–6^08 *¹–7^35 *¹–10^35 •°–12^38 *°–13^20 •°–18^17–20^35–21^10–45 *°–24; = 0^00–15^30
23	8	1.4	•	*°0^00–30 •°–1^48 *°6^10–8^43 ⚲°9^12–45, 10^35–40 *°–11^05, 11^38–45 ⚲°13^42–14^40 *¹–14^48 *°–15^05 ⚲°15^38–16^10, 16^52–17^45
24	8	0.2	•	⚲°7^33–8^20 ⚲°11^24–32 *°–12^05 ⚲°14^07–25
25	9	0.4	•	⊔°0–6
26	7	14.3	•	⚲°1^22–2^38, 6^26–35 ⚲¹–7^03 ⚲°–7^18, 8^25–9^14 ⚲¹–9^35 ⚲°–11^43, 12^04–14^10 •°14^15–48 *°–16^15 *°–16^40 *¹–17^10 *°–22^25 *°–24; = 15^30–24
27	9	0.9	2	*°0^00–20; = 0^00–3^40 ≡°4^50–5^45 ≡¹–6^30
28	8	2.4	•	•°5^31–6^20–7^22 ⚲°7^26–44, 9^14–24 •°11^44–12^10 ⚲°12^35–48, 13^47–14^42, por. wiatru 14 m/sek 15^10–25; ⊔°3–5, 23–24
29	9	0.6	•	⚲°15^11–22, 19^35–20^15, 20^48–21^25; ⊔°0^00–5
30	8	1.7	•	⚲°13^55–15^20, 16^32–17^22, 20^15–50
31				
Σ	–	72.3	–	

Zakopane $\varphi = 49°18'$ $\lambda = 19°57'$ *Maj – Mai* 1965

DNI	CIŚNIENIE P= 800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	119.7	119.7	118.9	119.4	3.5	6.5	4.2	4.6	9.3	2.0	91	64	72	76	0.6	3.5	2.3	2.1	10 •	10 •	8	SW 2	WSW 5	SW 2
2	120.1	120.0	120.0	120.0	1.5	5.2	−0.3	1.5	6.3	−0.7	55	27	80	54	3.0	6.4	1.3	3.6	8	8	7	W 2	NE 3	C 0
3	118.8	118.7	120.2	119.2	−0.7	5.4	−0.8	0.8	6.4	−4.7	75	39	75	63	1.4	5.5	1.5	2.8	0	2	0	NE 1	NE 5	NE 1
4	121.1	119.0	116.0	118.7	−0.2	8.9	4.0	4.2	12.2	−5.4	65	38	63	55	2.1	7.1	2.9	4.0	0	1	9	ENE 2	ENE 2	E 1
5	111.7	110.0	109.2	110.3	4.8	5.5	5.1	5.1	6.2	2.0	77	90	92	86	1.9	0.9	0.7	1.2	10	10 •	10 •	E 2	NE 2	SW 1
6	108.8	111.0	114.4	111.4	4.1	5.7	5.4	5.2	6.0	4.0	97	94	95	95	0.3	0.6	0.5	0.5	10 •	10 •	10 •	W 1	E 1	C 0
7	116.9	118.0	119.1	118.0	4.7	6.0	2.2	3.8	6.6	2.2	83	75	93	84	1.4	2.3	0.6	1.4	9	10	0	SW 1	NE 1	NE 1
8	117.4	117.5	120.8	118.6	4.2	10.4	7.1	7.2	10.7	−0.2	86	64	94	81	1.1	4.6	0.6	2.1	10	10	10 •	C 0	NW 2	SW 1
9	120.0	117.2	109.8	115.7	6.9	12.4	9.1	9.4	13.1	5.5	89	62	80	77	1.0	5.4	2.4	2.9	7	10	10	SW 2	W 2	SW 1
10	109.8	108.5	108.9	109.1	5.4	8.4	4.3	5.6	11.7	3.2	72	56	80	69	2.6	4.8	1.7	3.0	5	7	9	NW 4	W 5	WNW 3
11	107.2	110.1	116.1	111.1	3.3	4.8	1.6	2.8	5.4	0.7	86	80	96	87	1.1	1.7	0.3	1.0	7	10 •	10 •	W 2	N 1	SW 2
12	120.3	122.7	124.8	122.6	3.0	7.7	4.6	5.0	9.3	1.6	96	87	93	92	0.3	1.4	0.6	0.8	10 •	10	10	C 0	NW 2	NNE 4
13	124.3	124.1	123.7	124.0	6.6	10.7	6.9	7.8	11.6	4.3	57	38	76	57	4.1	8.0	2.3	4.8	3	1	4	SE 1	NE 3	NW 1
14	120.7	119.4	118.4	119.3	5.9	10.3	7.4	7.8	10.8	2.6	78	55	84	72	2.0	5.5	1.7	3.1	10	10	10	C 0	N 3	C 0
15	116.9	116.5	116.4	116.6	7.3	13.2	8.1	9.2	14.5	6.1	92	50	84	75	0.8	7.5	1.7	3.3	7	9	6	SW 1	NNW 3	W 1
16	114.4	124.5	115.1	114.7	9.4	15.7	10.7	11.6	17.1	6.9	90	62	80	77	1.2	6.8	2.7	3.6	10	9	10	C 0	WSW 5	SW 2
17	115.4	115.4	114.2	115.0	13.0	18.8	14.9	15.4	20.2	7.6	71	47	65	61	4.3	11.5	5.8	7.2	8	7	9	SW 3	W 5	C 0
18	114.0	113.8	113.8	113.9	17.6	21.6	14.1	16.8	22.4	13.8	52	44	68	55	9.6	14.4	5.1	9.7	5	2	1	W 5	S 5	C 0
19	109.4	107.1	112.4	109.6	19.7	21.4	12.0	16.3	22.1	11.4	42	31	74	49	13.3	17.5	3.7	11.5	5	9	8 K	S 5	SSW 12	NW 4
20	118.0	121.6	125.4	121.7	0.6	1.1	1.2	1.0	12.0	−0.2	92	92	92	92	0.5	0.5	0.5	0.5	10 *	10 *	4	NNE 3	NE 1	C 0
21	128.6	129.1	129.9	129.2	3.0	8.4	4.8	5.2	8.9	−2.0	72	54	79	68	2.1	5.1	1.8	3.0	8	9	6	C 0	NE 1	C 0
22	129.0	126.6	125.6	126.4	4.0	11.2	8.0	7.8	12.1	−1.5	63	58	85	69	2.9	5.7	1.5	3.4	9	9	9	NE 1	ENE 3	NE 2
23	120.2	119.3	119.4	119.6	7.4	11.0	10.3	9.8	13.8	6.2	93	94	97	95	0.8	0.8	0.3	0.6	10	9	10	C 0	ENE 3	C 0
24	119.3	119.8	120.7	119.9	9.0	13.6	9.3	10.3	15.4	7.5	97	61	92	83	0.3	6.0	1.0	2.4	9 •	9 •	10	C 0	W 2	SE 1
25	120.8	120.9	121.4	121.0	9.4	13.1	8.7	10.0	13.6	6.2	86	60	93	80	1.6	6.1	0.8	2.8	9	10 •	10 •	C 0	NW 3	W 1
26	121.5	121.6	121.6	121.6	8.3	13.9	8.3	9.7	15.3	7.5	85	62	88	78	1.6	6.1	1.3	3.0	10	6	4	C 0	WNW 5	C 0
27	119.8	118.7	117.9	118.8	10.5	14.0	9.5	10.9	14.6	2.5	64	52	89	68	4.7	7.7	1.3	4.6	6	8	10	C 0	NE 2	SW 1
28	115.0	113.7	112.0	113.6	9.2	12.4	9.8	10.3	14.4	8.3	93	87	83	88	0.8	1.9	2.1	1.6	10	10 •	10 •	NNE 2	NE 1	E 2
29	108.5	108.3	108.7	108.5	9.9	15.3	9.0	10.8	15.6	7.8	90	50	84	75	1.2	8.6	1.9	3.9	9	5	9	C 0	SW 3	C 0
30	110.9	112.8	114.2	112.6	4.9	7.2	6.1	6.1	9.8	4.3	92	75	89	85	0.7	2.6	1.0	1.4	10 •	10	9	E 1	W 2	NE 2
31	114.2	115.0	112.1	113.8	5.8	10.6	9.1	8.6	11.6	1.2	92	80	96	89	0.7	2.7	0.5	1.3	10	10 •	8	C 0	E 1	SW 1
M	117.2	117.1	117.4	117.2	6.5	10.7	6.9	7.8	12.2	3.6	80	62	84	75	2.3	5.5	1.7	3.2	7.9	8.1	7.7	1.5	2.8	1.1

Czerwiec – Juin

1	108.6	113.1	116.0	112.6	14.4	16.4	10.8	13.1	17.0	7.7	39	40	80	53	10.1	11.2	2.7	8.0	1	2	8	S 14	SSW 10	NE 1
2	117.3	118.7	122.4	119.5	9.5	12.7	7.1	9.1	14.4	3.3	66	52	85	68	4.1	7.1	1.5	4.2	1	6	4	SW 2	WNW 6	SW 2
3	123.3	122.9	123.0	123.1	9.0	15.2	10.6	11.4	16.4	1.3	56	41	89	62	5.1	10.2	1.4	5.6	1	8	10 •	SSE 1	ENE 2	C 0
4	121.3	120.9	118.5	120.2	10.1	13.5	10.7	11.2	14.1	5.7	84	70	93	82	2.0	4.7	0.9	2.5	10	10 •	10 •	C 0	NE 1	C 0
5	114.4	112.0	110.4	112.3	10.7	14.6	12.2	12.4	14.7	8.4	96	83	98	92	0.5	2.8	0.3	1.2	10 •	10	9	S 1	NE 1	C 0
6	107.8	107.1	110.1	108.3	12.0	13.9	9.8	11.4	16.4	9.4	94	91	96	94	0.8	1.5	0.5	0.9	9	10	10 •	C 0	NE 3	NE 1
7	114.1	115.8	117.1	115.7	7.4	12.1	9.0	9.4	12.9	7.1	96	64	90	83	0.5	5.0	1.2	2.2	10 •	7	4	C 0	NE 1	C 0
8	117.4	116.3	115.2	116.3	9.9	18.5	12.6	13.4	19.4	4.4	87	52	80	73	1.7	10.0	3.0	4.9	8	5	9	NE 1	SE 2	SE 1
9	112.4	110.5	111.6	111.5	12.5	11.4	10.5	11.2	16.5	9.6	77	77	85	73	3.5	3.2	4.5	3.7	6	10	3	SE 1	E 1	SE 4
10	111.4	111.7	111.2	111.4	9.5	14.4	9.4	10.7	15.4	6.1	88	54	92	78	1.5	7.7	1.0	3.4	10	8	10 •	C 0	N 3	NE 2
11	106.1	107.8	108.4	107.4	8.4	11.6	9.9	10.0	13.1	6.8	96	80	93	90	0.4	2.7	0.8	1.3	10 •	10	10 •	C 0	ESE 1	SW 2
12	113.6	116.2	119.9	116.6	8.2	10.3	8.4	8.8	10.7	7.8	94	89	97	93	0.6	1.3	0.3	0.7	10 •	10 •	10 •	S 1	NE 2	W 3
13	120.6	119.7	119.3	119.9	7.2	14.7	9.7	10.3	15.7	6.5	92	61	93	82	0.8	6.6	0.8	2.7	10	5	9	S 1	NW 3	C 0
14	118.5	119.7	120.7	119.6	9.0	8.5	9.1	8.9	10.9	6.5	89	85	96	90	1.3	1.7	0.3	1.2	8	10	10 •	NW 2	NW 2	NW 1
15	122.1	122.4	122.6	122.4	10.5	15.8	8.7	10.9	16.4	6.1	68	51	87	69	4.1	8.8	1.4	4.8	1	5	0	SE 1	NE 2	SE 1
16	122.6	121.4	118.8	120.9	12.0	19.0	12.4	14.0	20.4	3.0	66	43	75	61	4.7	12.6	3.6	7.0	0	4	2	NE 1	E 3	ENE 1
17	113.0	111.3	114.3	112.9	16.6	19.1	9.7	13.8	20.6	7.9	44	49	95	63	10.5	11.4	0.6	7.5	2	7	10 •	NE 1	SE 6	SE 2
18	120.3	121.6	122.5	121.5	7.7	11.5	10.1	9.8	14.7	7.3	92	72	84	83	0.8	3.9	2.0	2.2	10	10	9	C 0	ESE 2	C 0
19	121.1	121.2	124.0	122.1	15.0	19.0	11.8	14.4	20.0	7.7	65	46	76	62	5.8	11.9	3.3	7.0	8	7	2	NE 2	SW 5	SSW 2
20	126.1	125.8	125.8	125.9	12.1	17.6	12.5	13.7	19.1	7.4	65	46	78	63	4.9	10.8	3.3	6.3	7	7	5	C 0	NW 2	C 0
21	125.5	124.9	122.7	124.4	13.6	20.2	14.1	15.5	21.5	6.9	74	46	82	67	4.1	13.0	3.0	6.7	2	7	8	C 0	E 2	C 0
22	120.8	120.0	118.1	119.6	15.4	23.3	15.5	17.4	24.5	7.9	76	50	80	69	4.3	14.2	3.6	7.4	1	6	1	W 1	S 2	S 1
23	119.0	121.0	122.4	120.8	15.6	20.8	13.9	16.0	22.6	10.3	89	51	79	73	2.0	12.1	3.5	5.9	7	5	6	SE 1	W 5	ESE 1
24	123.5	124.1	125.1	124.2	18.0	23.0	16.0	18.2	24.0	9.0	66	54	77	66	6.8	12.9	4.5	8.0	4	6	1	C 0	NW 4	SW 1
25	125.7	126.1	126.3	126.0	18.6	23.5	16.1	18.6	25.0	12.5	75	43	77	65	5.3	16.5	4.3	8.7	6	2	2	SE 2	NW 2	S 2
26	125.1	124.5	126.5	125.4	19.7	27.7	20.2	22.0	28.8	10.2	70	33	71	58	6.9	25.0	6.9	12.9	1	2	10 (K)	E 2	SW 3	NW 3
27	126.4	125.4	125.3	125.7	17.4	24.6	16.1	18.6	26.5	11.9	86	51	94	77	2.9	15.0	1.2	6.4	8	4	10 (K)	ENE 1	NE 2	C 0
28	124.9	128.2	127.8	127.0	14.2	10.0	8.4	10.2	16.1	8.2	92	93	94	93	1.4	0.9	0.6	1.0	10 •	10 •	10 •	W 2	C 0	C 0
29	126.6	125.7	126.9	126.4	9.6	17.3	11.6	12.5	19.2	6.6	69	53	91	71	3.8	9.2	1.2	4.7	7	1	4	C 0	NW 4	C 0
30	126.1	124.8	122.0	124.3	11.8	20.5	14.4	15.3	23.1	5.1	70	55	82	69	4.0	10.7	3.0	5.9	0	1	1	C 0	E 3	C 0
31																								
M	119.2	119.4	119.8	119.5	12.2	16.7	11.7	13.1	18.3	7.3	77	59	86	74	3.5	8.8	2.2	4.8	5.9	6.5	6.6	1.3	2.8	1.0

Zakopane

$H_s = 844\,m$ $H_b = 838.2\,m$ $h_w = 17.7\,m$

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	7	2.8	•	▽°6⁴⁰–45 △°–6⁴⁸ ▽°–7¹² ✱°–7²⁵ ▽°–7²⁶, 11²²–24 •¹–11²⁵ ▽°–11³⁴, 12²⁵–50 •¹–12⁵¹ •°–13⁰⁰ •¹–13⁰¹ ▽°–13⁰³ •¹–13¹¹ ▽°–13¹³
2	9	•	•	⌴¹–6; ⊕¹ 9¹⁵–11³⁰
3	9	•	•	⌴¹–8, 23–24
4	9	0.2	•	⌴°0⁰⁰–7
5	7	13.9	•	•°0³⁰..2⁰⁰–3⁴⁰, 9⁵⁶..10⁴² •°11³⁴–12¹² •°12²¹, 13³², 14²⁹..16¹⁷, 19⁰⁷..³⁰, 19⁵⁰–21²⁰, 22⁴⁵–24
6	7	38.7	•	•°0²⁰–3²⁰ •¹–10²⁰ •²–11³⁶ •¹–11⁵² •°–12⁰⁰ •²–12⁰⁰ •°–12³⁰ •¹–12³³ •°–13³⁶ •¹–13⁵⁵ •²–13⁵⁸ •°–14²⁸ •²–14⁴⁰ •°–14⁵⁴ •¹–15²⁰ •°–15⁴³ •²–16¹¹ •¹–16²⁷ •°–16⁴⁷ •²–17²⁰ •¹–17⁴⁵ •²–17⁵⁸ •¹–18³² •°–20⁰² 20²⁵–49 •¹–21⁰²
7	7	0.4	•	•°0⁰⁰–40 ▽°7⁵⁶ 8¹², 8⁵⁵–9⁰² 9¹⁸–20 •°9⁵⁹..10¹⁰, 10²⁰–11⁰⁵, 11¹⁷–50, 12⁴⁷, 13³⁵ 15³², 16³⁰.. = 0⁰⁰–4³⁰ [6.V: •°–21²⁷ •¹23¹²–33 •°–24; = 8³⁰–9³⁰, 13⁴⁵–24
8	9	1.1	•	•°18²¹–09 ▽°20⁰⁸–44 21²⁰–25 •²–21³⁰ •°–21⁴⁷, ⌴°0–5
9	8	7.8	•	•18⁵⁰..19²⁰–42 •¹–19⁵¹ •°–20⁰⁷ ▽°21³¹–38 •¹–21³⁹ •²–21⁵⁹ •¹–22²³ •²–22²⁸ •°–22³² •²–22⁴⁴ •¹–22⁵⁶ •°–23⁰⁹ •²–23¹⁰ •¹–23²¹ ▽°–24; K°2¹⁴⁵..2²⁵⁰ S–N
10	9	5.4	•	▽°0⁰⁰–38 4²³–32, 7⁵²–8¹⁰, 11¹²–24, 11⁵²..12¹⁰, 15¹⁴–16 •¹–15⁴⁹ •°–15⁵⁰, 21⁵²..22⁰² •°22³⁹–48 •¹–23⁰⁵ •°–23¹⁹ •¹–23⁵⁶ •°–24; ⌒°15⁴⁰–55
11	9	33.5	•	▽°0⁰⁰–12 •°–0²⁰ 9⁵⁸..10⁰⁹ •¹×1¹⁰–45 ✱°×–10⁵⁴ •°–11⁰⁴ •²–11²⁰ 12³⁵ 14⁰⁸ •¹14⁵² 15⁰³ •²–15²⁰ •°×₁–15²⁷ •°–15³⁰, 15⁵⁰–56 •°×₂–16¹⁵ •¹–16⁰⁶ •²–16²³ •¹–16⁴⁸ •°–17³³ ✱°–18⁰⁵ •°–21¹⁰ ✱°–21²⁴ •°–23¹⁰
12	8	1.1	•	•°0⁰⁰–15, 4³⁵–7¹¹ •²–7¹⁵ •°–10⁴⁵ •°12⁴¹–13¹²; = 7¹⁵–11³⁰ [11.V: •°–23³⁵ •°–24
13	9	•	•	•°1¹⁰–25⁵
14	8	1.4	•	•°21²⁰–46 •°22⁰²–17 •¹–22⁴⁶ •°–23²⁵; ⌒¹3–6
15	8	1.1	•	= 4³⁰–7⁰⁰
16	8	1.4	•	•°1⁰¹..18 •²20³–05 •°–20⁵ •²20³⁹–42 •°–3¹⁵, 7⁰⁸–8⁵⁰ •²–9⁰⁰ •°–9¹⁵, 15²⁴–16³⁰ •°21²⁵–50, 22³⁰..38 K°7²⁴–8⁴⁵ SE–SW, 15²⁰ 16⁴⁵ SW–W; = 5³⁰–10³⁰
17	9	•	•	⌒°3–8
18	9	•	•	
19	9	16.5	•	•°20⁵³–21¹⁰ •°23²⁰–35 •°–24, (K)°W 19⁵² K°20³⁰ 21²⁵ E, par wiatru do 14 m/sek 10¹⁵ 12³⁰ >–13⁴⁵ (par do 20 m/sek) par wiatru do 14 m/sek 15⁴⁵ 18¹⁰; ≡°22⁴⁸ 23⁰³ ≡²–23⁴² = –24
20	5	4.1	•	•°0⁰⁰–20 •¹–10² •²–15 •°–14⁸ •²–21⁷ •°–24⁰ •¹–30⁵ •°–31³ •°–40² •¹–44⁵ •°–53³ ✱°–6¹⁰ ✱°–9²¹..40 ✱¹–10⁰⁸ ✱°–10¹⁰..55, 11¹² ✱¹–11¹⁹ ✱°..11⁴⁴ ✱¹–12⁴⁵ ✱°–15²⁵..18, K°19² K¹14⁸ K°22²–45 W–E;
21	8	•	•	⌴°0⁰⁰–7 [20.V: = 0⁰⁰–1²⁰, 5³⁰–12⁵⁰, ⌴°20–24
22	8	0.6	•	⌒°0–2 ⌴°–5
23	6	10.5	•	•²5⁴²–6⁰¹ •°–7²⁰ •°0⁴⁶..11⁰³ 12⁰⁷ ▽°15¹⁵–17 •¹–15³² •¹–15⁴⁵ ▽°–16⁴⁰ •¹–17²⁸ •°–17⁵⁸ •¹–18¹⁴ •°–19¹⁰, = 4–13³⁰
24	8	3.2	•	▽°0¹²–39 •¹–15³ •°–18⁰ •°20²⁶–36 •°–20⁵ 20⁵–52 •¹–5⁰¹ •°–6⁰⁵ 6³⁰ 7⁴⁵ •¹–7⁵² •°–8⁴⁸ 9⁰⁰–42 •¹–9⁵¹ •°–10²⁵ 12³⁸ 13¹⁰ 17³⁵ 18⁰⁹ •²–18¹⁸ •°–19³⁵, = 6¹⁵–8³⁰
25	7	3.5	•	•°12³⁶–55, 13³⁸ 14¹⁸ •¹14⁵⁶ 15¹⁰ 15⁵⁸ 16⁰¹ •¹–16⁰⁸ •²–16¹⁴ •¹–16¹⁹ •°–16³² •²–16⁴² •°–16⁵⁴ •¹–17¹⁸ •²–17³⁰ •¹–17³³ •°–17⁵¹ •¹–17⁵⁸ •°–18³² •°18⁵³ 19¹⁷, 19³⁶..21¹²
26	8	3.1	•	•²16²⁵–43 •°–17¹⁵
27	9	0.3	•	▽°15³⁸–45, 16³⁰–40 17²² 18²²
28	7	5.6	•	•°0⁰⁶..1¹⁵, 9²⁰..11¹⁵ •°12²²–46 •¹–12⁵⁵ •°–13¹² 19²⁹–50 •¹–19⁵⁷ •²–20¹⁷ •¹–20⁴⁵ •°–21³⁵, (K)°W 19²⁰ K 19²⁸–20²⁵ SE; = 3³⁰–9³⁰
29	8	6.5	•	•°2⁰²⁰–3¹⁵ 7¹⁰–30 17³³–35 18⁵⁶ 19⁰⁷ 22⁴⁴–23²⁰
30	8	1.6	•	•°1¹⁸–3⁰¹, 3³¹–40 •²–3⁴³ •°–5¹⁵ •¹–6⁴⁵ •°–9⁰³, = 5³⁰–9³⁰, 21³⁰–24
31	8	10.6	•	•°10²⁸–12³⁰ •°..13¹⁵–14⁴⁰..15⁰⁵–16²² •°21⁰²–12, 21³⁷–22⁴⁸ •¹–22⁵⁰ •°–23⁰⁵, 23²⁸–36 •²–23⁵⁶ •°–24, = 0⁰⁰–4³⁰, ⌒°1–7
Σ	–	154.9	–	

Czerwiec - Juin

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	9	0.4	•	▽°0⁰⁰–21 •°–1³⁸ 1⁵⁵–2¹⁰ 19²¹–35 21⁰³–14 •¹–21¹⁹ •°–21²⁹ 21⁴³–22⁰⁷, >2¹⁵ 7²⁵ (par do 20 m/sek) >–10³⁰ (par do 30 m/sek) >..12²⁵ (par 17 m/sek)
2	9	•	•	
3	9	0.3	•	•°18²⁸..27 18⁴²–51..19²⁸ 19³⁵–20⁰⁵ 21⁰⁷, ⌒°1–3 ⌴°4–5
4	7	11.8	•	•°7⁵⁵ 8⁰¹ 13³² 17⁰¹ 19¹⁵ 19¹⁰..40 19⁵⁵ 17²⁸ •²20⁴⁶ 21⁰¹ •°20¹⁰⁵ 21²⁰–28 •¹–21³⁴ •²–22⁰³ •°–23²⁰, K°21³⁵ K¹22²⁵ K°22²⁰ 23¹⁰ SW–SE; = 13⁴⁰ 15³⁵, ⌒°0–1 ⌒¹2–7
5	7	5.8	•	•°10⁴⁵–55 •°11⁰⁸ •¹–12⁵ •°12⁴⁰ •¹12⁵¹–140 •°–20⁸ •¹–20⁵⁸ •²–21⁰⁸ •°–3⁴⁰ •¹–4¹⁴ •°–6⁰¹ 6²⁰ 8¹⁰ 14⁰³..23 14²⁵ 15⁴⁵ •¹–15⁵⁵ •°16⁰² •¹16⁰⁷ •°17⁰⁸ •¹17¹⁸ •°18²⁸ •¹19²⁵ •°19⁰⁰ 19⁵⁵ 20⁰⁸ K°0⁴⁵ 2⁴⁰ S–W; = 17³⁰–24
6	7	11.5	•	•°21⁰³–07 •¹–21⁰⁹ •°–12¹⁰ •¹–12¹⁴ 12¹⁹ •¹–12²⁰ •¹–12¹² •²–12²⁸ •¹–12⁰⁶ •°–12³⁴ 12⁴⁴–46, 13⁰⁷–32 13⁴¹ 14⁰² 14¹⁸–26 •¹–14⁴⁴ •°–15¹⁹ •¹–15²¹ •°–15³⁰ 36, 17⁴⁵ 18⁰² •¹–19¹⁵ •²20¹⁰ •°–22²⁵ •°–24, = 1⁰⁰–5³⁰ 13³¹ 15⁵³ •°–16⁴⁴
7	8	0.1	•	•°0⁰⁰–06 •°–1⁵⁰ •°–2²⁰ 3⁰¹ 6²⁵ •°–7⁰⁸, = 0⁰⁰–7³⁰ [6.VI: = –24
8	8	0.5	•	⌒°1–8
9	9	4.8	•	•²12⁵–26 •¹–13³⁰ •°–13⁰ 13⁰⁸–51 •²–13⁵⁶ •¹–14⁰² •°–14³² •²–14⁵⁹ •°–15³⁰ 16⁰⁵–07 •²–16⁰⁸ •°–16⁰⁹ •°–16¹⁵ •²–16¹⁶, K°11²⁰ 12¹⁵ W–E
10	9	59.7	•	▽°6⁴⁴ 8¹³ 11¹⁴–31 •²–11³⁰ •°–11⁴⁰ 13²⁸–34 14²⁰–31 14⁴²–52 15²⁶–32 •¹–15⁵⁰ •°–16⁵⁵ 16⁵⁴–07 •°16²⁰ 25 •°17⁵⁵ 18⁰⁵ 19²⁷–30 19³⁸–52 •¹–19⁵⁷ •°–20¹⁰ •¹–20¹⁸ •²–23²⁰ •°–24
11	8	48.6	•	•°10²⁴ 12² •°4⁵⁸ •¹–5⁰⁸ •°7¹⁵..32 •°9⁴⁸ 10⁰², 10¹⁰–17 10³⁷–50 11²¹–26 •²–11³⁷ •¹–11⁴⁰ •°–12⁰¹ 12¹⁷–37 •°21 16²⁵–38 •²–16⁴⁷ •°–18⁰⁶ •¹–18⁴² •²–18⁴⁵ •°–23⁰¹ •²–24, = 18²⁰–24
12	7	17.6	•	•°10⁰⁰–30 •¹–3 3⁴ 4⁰² 5⁵⁷ •²–5⁵⁹ •°–6⁰⁵ •°7⁰²–12 •°–7²⁸ •°7⁴⁵ •°10⁰⁶..40 9⁵² 11⁰⁵ •²–11⁰⁷ •°–11⁴⁵ 11²⁸ 13⁰⁵ 15²⁰..32 •²–13⁵⁷ •°–14 •°–14⁰² •²–14³ •°–15³⁵ •°–15⁵⁰ •°–17¹⁰ •¹–17²⁰ •°..18³⁵ •°–23¹⁰ •°–24;
13	8	4.5	•	•°0⁰¹..09 10²..16 20²..35 •°17⁵⁰–53 •°17⁵⁹ •°–18⁰¹ •°–18⁰⁶ •°–18⁴⁰, = 0⁰⁰–7¹⁵ 20²⁵–24 [12.VI: = 0⁰⁰–8³⁰ 14³⁰–24
14	7	16.1	•	•°2⁰²⁵ 3⁰⁰ •²–3¹² •°–3²⁰ •²–3²⁸ •°–3⁵⁰ 6⁰⁹–11, 8⁴⁴–56 9¹⁵–20 •°–9²⁵ •°–9⁵² •²–10⁰⁴ 10⁴³ 11⁰⁵ •°20⁵–09 13⁵⁷ 14⁰³ •¹–14³⁰ •°–14⁴⁰ 15¹²–38 •°15²⁰ 17¹⁸ •°–20²⁵ •²–20⁴⁸ •°–22¹⁰, K°9³⁵ 10¹⁰ S–SE;
15	9	•	•	= 0⁰⁰–3⁰; ⌒²1–24 [14.VI: = 0⁰⁰–3³⁰ 17²⁰–24
16	9	•	•	⌒°0–6, 20–24
17	9	36.2	•	▽°14³⁰–17⁰⁷ •¹–18⁴⁵ •°–19¹² •¹–24; ⌒°0⁰⁰–6
18	8	0.5	•	•°1⁰⁰ 2⁵⁰ •°–3²⁰ •¹–5²³ •°–6⁴⁰ 7¹¹–8⁰⁰ 21²⁵; = 4³⁰–8³⁰
19	9	4.8	•	▽°13⁵¹–55 •²–13⁵⁶ •¹–14⁰¹ •²–14⁰³ •¹–14²⁰ •²–14²⁹ •¹–14³¹ •²–14⁴⁰ •°–15¹¹ 16⁴³–46 •¹–16⁵² •°–16⁵⁸; par wiatru do 14 m/sek 12²⁵ 14⁵⁰; ⌒¹16⁵⁵–58
20	8	•	•	⌒°20–24
21	8	•	•	⌒°0⁰⁰–9, 21–22 ⌒¹23–24
22	8	4.1	•	⌒¹0⁰⁰–8 ⌒°21–24
23	9	•	•	▽°3⁴²–50 •¹–3⁵⁵ •²–4²⁵ •°–4²⁸ •°–4⁴⁰; K°3⁴⁵ 4⁴⁰ W–E; ⌒°0⁰⁰–1 ⌒¹2–3 ⌒°20–22 ⌒¹23–24
24	8	•	•	⌒¹0⁰⁰–7 ⌒°22–24
25	9	•	•	⌒°0⁰⁰–1 ⌒¹2–6 ⌒°21–24
26	9	0.2	•	▽°22²¹–42; (K)°16⁴⁵ 17³⁵ SW–E (K)°20⁰² 21⁴⁵ S–N; ⌒¹0⁰⁰–7
27	8	20.3	•	•²17⁵⁵ 18²¹ 20¹⁰–23 •°–20³³ •²21¹⁸–32 •°–21⁴² •¹–22¹⁵ •²22⁴¹ •¹–22⁴⁵ •°–23⁰³, (K)°S 16²⁴ K°17⁵⁸ K°18⁰⁴–10 K°18¹⁵–30 (K)°N 19⁰² (K)°W 18⁴⁵ K°21¹⁵ K°22³⁵ 23⁴⁰ E
28	6	35.1	•	▽°0–2 8³⁵–9¹⁷ •°0–2 19⁰⁴ •°0–1 21³⁵ •°20⁰³..50, = 9¹⁵–13¹⁰
29	9	•	•	⌒°19–20 ⌒¹21–22 ⌒²23–24
30	9	•	•	⌒²0⁰⁰–7 ⌒°20–24
31				
Σ	–	282.9	–	

Zakopane — φ = 49°18' — λ = 19°57' — Lipiec — Juillet 1965

DNI	CIŚNIENIE P = 800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	118.5	118.3	119.0	118.6	14.3	21.8	14.0	16.0	24.1	7.5	82	55	94	77	3.0	11.9	1.0	5.3	7	9	7	E 1	E 5	C 0
2	117.2	117.1	117.6	117.3	12.4	12.0	9.9	11.0	14.1	9.7	98	95	96	96	0.4	0.7	0.5	0.5	10 •	10 •	2	C 0	NE 2	S 1
3	116.6	115.2	116.7	116.2	11.9	15.7	10.7	12.2	17.7	6.3	76	59	87	74	3.4	7.3	1.7	4.1	6	8	10	W 2	W 4	W 5
4	116.5	115.4	114.0	115.3	7.8	9.5	9.2	8.9	11.0	2.8	79	92	97	89	2.3	1.0	0.3	1.2	9	10 •	10	NE 1	W 2	C 0
5	113.0	112.7	116.4	114.0	7.9	8.2	7.1	7.6	10.2	7.1	97	95	94	95	0.2	0.8	0.6	0.5	10 •	10 •	10	NNE 1	NE 1	C 0
6	120.4	121.0	121.5	121.0	8.4	11.6	8.7	9.4	13.3	4.7	72	49	74	65	5.0	6.9	2.9	4.3	2	5	9	WSW 5	WSW 4	WNW 2
7	121.7	120.2	119.0	120.3	10.7	16.5	14.5	14.0	18.5	4.9	62	51	54	56	5.0	9.3	7.7	7.3	3	6	8	C 0	WNW 5	SW 4
8	116.0	112.6	112.5	113.7	15.4	18.4	11.7	14.3	19.9	6.1	57	45	94	65	7.6	12.0	0.9	6.8	9	7	10 R	NNE 4	SW 8	W 3
9	114.1	117.2	119.7	117.0	10.9	13.1	6.7	9.4	13.9	6.6	76	55	89	73	3.1	6.7	1.1	3.6	7	8 •	3	SW 2	WNW 5	SW 1
10	120.6	120.0	122.3	121.0	9.7	14.3	9.1	10.6	15.1	2.5	69	55	88	71	3.8	7.3	1.5	4.2	3	7	9	SSW 1	SW 2	NNE 1
11	123.7	124.8	125.5	124.7	9.1	12.7	7.7	9.3	14.2	5.5	81	62	87	77	2.3	5.5	1.4	3.1	5	8	0	SSE 1	NNW 1	C 0
12	124.4	122.8	122.2	123.1	10.7	19.4	14.9	15.0	19.6	3.3	76	55	71	67	3.1	10.6	4.8	6.2	8	7	10	C 0	SE 5	SSW 1
13	122.0	122.5	123.7	122.7	15.5	19.5	14.0	15.8	21.8	12.2	88	65	94	82	2.2	7.8	1.0	3.7	10	8	2	C 0	WNW 4	ESE 1
14	124.6	125.0	124.8	124.8	16.7	24.6	16.2	18.4	25.5	9.4	79	46	81	69	4.1	16.6	3.5	8.1	1	5	1	NE 1	NE 2	C 0
15	125.4	124.4	123.7	124.5	18.0	25.6	15.7	18.8	26.1	10.9	76	44	82	67	5.0	18.3	3.3	8.9	1	3	3	C 0	ENE 2	C 0
16	121.6	121.3	120.9	121.3	19.3	17.6	16.2	17.3	24.5	11.0	73	80	89	81	6.0	3.9	2.0	4.0	0	9	8	C 0	W 2	ESE 1
17	119.8	118.2	117.6	118.3	16.8	20.1	13.3	15.9	21.9	11.6	80	72	94	82	4.0	6.6	1.0	3.9	1	9	8	C 0	NE 2	C 0
18	116.2	117.3	119.8	117.8	14.3	14.6	13.7	14.1	18.1	9.8	85	82	94	87	2.4	3.0	1.0	2.1	7	10 •	10	SW 1	C 0	C 0
19	122.0	123.2	124.0	123.1	12.4	16.9	14.3	14.5	17.4	11.3	98	79	91	89	0.4	4.1	1.5	2.0	10 •	9	7	C 0	NE 5	NE 1
20	123.7	123.3	121.5	122.8	13.4	15.6	12.8	13.6	18.4	9.6	94	85	98	92	0.9	2.7	0.4	1.3	9	9 •	8	ESE 1	C 0	C 0
21	118.9	117.9	116.8	117.9	14.5	19.3	15.1	16.0	20.9	11.3	92	58	88	79	1.4	9.3	2.2	4.4	8	8	10 •	C 0	SW 3	SE 1
22	118.3	118.6	117.3	118.1	14.1	19.0	14.2	15.4	21.0	12.3	92	55	83	77	1.4	9.9	2.8	4.7	5	6	5	SW 1	WNW 4	ENE 1
23	114.7	115.1	118.2	116.0	13.4	19.3	12.2	14.3	21.0	8.2	81	74	86	80	3.1	5.8	2.1	3.7	9	9	1	NE 1	C 0	C 0
24	119.0	119.2	120.6	119.6	13.2	22.1	14.6	16.1	24.3	6.6	78	55	75	69	3.4	12.1	4.2	6.6	4	4	1	C 0	WNW 3	SE 1
25	120.5	119.7	118.9	119.7	15.6	21.0	17.0	17.6	22.5	11.8	83	72	85	80	3.1	7.1	3.1	4.4	9	9	2	C 0	NE 2	SW 1
26	119.4	120.3	118.3	119.3	14.1	13.3	9.8	11.8	17.0	9.3	90	89	91	90	1.7	1.7	1.2	1.5	10 •	10 •	10 •	C 0	NE 1	C 0
27	117.8	119.1	120.3	119.1	9.9	12.7	8.6	10.0	15.0	8.4	93	70	85	83	0.8	4.4	1.8	2.3	10	9	4	SSE 1	WSW 4	WSW 1
28	121.0	121.3	119.9	120.8	9.9	12.6	11.2	11.2	14.8	8.4	78	61	68	69	2.7	5.7	4.3	4.2	10 •	8	8	WSW 4	W 5	W 4
29	117.5	116.2	113.1	115.6	13.3	19.0	17.2	16.7	21.4	8.6	70	44	45	53	4.6	12.4	10.7	9.2	2	5	9	E 1	N 4	S 8
30	110.3	111.5	112.9	111.6	15.7	13.0	10.9	12.6	18.5	10.8	61	86	80	76	6.9	2.2	2.6	3.9	8	10 •	5	SW 3	C 0	C 0
31	113.0	111.1	113.0	112.4	10.5	13.0	11.4	11.6	15.3	8.7	86	89	73	83	1.8	1.7	3.7	2.4	10 •	10	6	C 0	N 1	S 3
M	119.0	118.8	119.1	119.0	12.9	16.5	12.3	13.5	18.6	8.3	81	67	84	77	3.0	7.0	2.5	4.2	6.5	7.9	6.3	1.0	2.6	1.3

Sierpień — Août

1	115.9	116.7	114.1	115.6	11.4	14.0	10.6	11.6	15.1	10.3	91	76	97	88	1.3	4.0	0.4	1.9	9	9	10 •	ENE 2	NE 1	C 0
2	110.4	115.0	117.2	114.2	7.0	5.4	6.3	6.2	10.6	4.5	96	92	90	93	0.4	0.8	0.9	0.7	10 •	10 •	9	NE 4	NW 2	SSW 1
3	116.9	116.6	118.1	117.2	9.5	14.6	10.1	11.1	16.2	4.4	79	48	80	69	2.6	8.6	2.5	4.6	0	9	7	C 0	ENE 3	C 0
4	120.6	122.1	123.7	122.1	10.9	14.2	11.0	11.8	17.0	8.4	81	64	81	75	2.5	5.8	2.5	3.6	8	8	10	SW 1	SW 4	SW 4
5	126.6	126.9	127.3	126.9	12.5	17.4	10.6	12.8	18.7	10.2	75	48	93	72	3.6	10.6	0.9	5.0	8	7	3	ESE 2	NW 4	C 0
6	126.9	126.4	126.4	126.6	13.0	23.7	15.2	16.8	23.4	7.1	81	57	81	73	2.9	12.7	3.4	6.3	0	1	4	C 0	WSW 2	SE 1
7	123.4	123.9	122.6	124.0	14.0	27.8	18.9	19.9	28.4	9.8	85	32	54	57	2.4	23.4	10.0	12.6	3	0	0	C 0	S 5	C 0
8	122.9	120.6	122.1	121.9	15.1	26.6	15.9	18.4	27.7	9.9	71	27	70	56	4.9	25.5	5.4	11.6	0	0	3	C 0	WSW 7	S 2
9	122.7	123.4	124.0	123.4	15.1	14.5	13.2	14.0	18.3	11.5	94	89	96	93	1.1	1.9	0.6	1.2	9	10 •	10 •	C 0	NE 2	C 0
10	123.6	123.6	123.0	123.4	10.7	12.3	11.0	11.2	13.3	10.3	97	91	94	94	0.4	1.3	0.8	0.8	10 •	10 •	10	C 0	ENE 2	E 2
11	123.2	124.2	124.8	124.1	8.0	8.7	7.7	8.0	11.0	7.6	96	94	94	95	0.4	0.6	0.6	0.5	10 •	10 •	10 •	E 2	NE 1	C 0
12	124.2	125.6	125.5	125.1	8.2	9.0	7.9	8.2	13.2	7.2	91	89	94	91	1.0	1.3	0.6	1.0	10	9	7	C 0	NE 1	C 0
13	124.3	125.5	125.3	125.0	8.3	11.5	7.3	8.6	12.1	7.2	88	60	88	79	1.3	5.3	1.2	2.7	9	9	3	W 2	SW 2	SE 3
14	124.7	124.5	123.6	124.3	9.3	13.9	9.1	10.4	15.2	6.1	73	53	86	71	3.0	7.9	1.7	4.2	2	7	9	SW 1	NE 2	SE 2
15	123.8	124.0	124.5	124.1	8.6	13.7	10.5	10.8	14.8	7.8	89	63	88	80	1.3	5.9	1.5	2.9	10	5	10	C 0	E 1	C 0
16	124.1	123.8	123.2	123.7	8.5	12.4	9.5	10.0	14.7	6.7	87	68	93	83	1.4	4.6	0.9	2.3	7	9	7	C 0	E 1	C 0
17	122.5	122.7	123.5	122.9	8.6	16.0	8.0	10.2	17.0	4.9	87	56	94	79	1.3	8.1	0.6	3.4	7	8	1	C 0	E 1	C 0
18	124.0	124.8	126.4	125.1	8.6	19.0	9.5	11.6	20.2	5.1	90	41	92	74	1.2	13.0	1.0	5.1	0	2	0	C 0	NNE 2	SE 1
19	128.2	128.6	128.8	128.5	9.4	20.4	10.4	12.6	20.9	5.8	97	40	91	76	0.3	14.5	1.2	5.3	1	3	0	C 0	NE 1	C 0
20	128.3	127.1	126.0	127.1	9.5	19.7	12.1	13.4	20.9	6.7	90	53	84	75	1.2	11.2	2.2	4.9	2	3	0	C 0	NE 2	C 0
21	124.6	122.9	120.9	122.8	11.7	20.8	17.6	16.9	22.0	7.2	82	43	50	58	2.3	14.2	9.9	8.9	1	4	0	SSE 1	SSE 3	S 6
22	118.4	116.7	115.0	116.7	18.1	20.9	18.4	19.0	21.4	16.7	44	36	42	41	11.8	15.9	12.3	13.3	1	1	0	S 7	S 10	S 3
23	114.7	115.9	116.7	115.8	18.2	20.3	19.0	19.1	22.5	16.2	52	47	54	51	10.0	12.6	10.1	10.9	3	8	10	SE 2	SSE 3	W 2
24	115.3	115.3	113.3	114.7	17.3	21.7	15.7	17.6	23.9	15.4	68	53	97	73	6.3	12.4	0.6	6.4	9	10 •	10 •	SW 1	SW 6	SW 2
25	111.8	112.7	113.6	113.4	15.8	17.1	11.2	13.8	18.2	11.1	73	74	94	80	3.1	3.1	0.8	3.7	10 •	10 •	10 •	S 1	SW 2	W 4
26	116.8	118.5	118.0	117.8	9.2	6.9	3.9	7.0	11.3	5.8	93	92	93	93	0.8	0.7	0.3	0.7	10 •	10 •	10 •	NW 2	E 3	SE 2
27	116.2	116.9	118.3	117.2	5.6	8.3	7.3	7.2	9.3	3.1	97	86	92	92	0.3	1.6	0.8	0.9	10 •	10 •	10	NW 2	WSW 1	SW 2
28	118.9	119.3	121.3	120.0	6.3	11.6	8.3	8.8	13.6	3.2	96	62	87	82	0.3	3.1	1.3	2.3	10 •	8	9	W 1	NE 3	C 0
29	121.0	120.4	119.7	120.4	6.3	12.6	7.0	8.3	13.7	4.7	93	69	86	83	0.7	4.3	1.3	2.2	6	8	4	C 0	N 1	SW 2
30	119.0	120.3	122.2	120.6	10.0	13.1	6.1	8.8	15.3	3.1	83	60	92	79	1.8	6.1	0.7	2.9	9	3	1	SW 1	W 3	C 0
31	121.2	119.7	118.6	119.8	6.0	13.3	8.1	9.4	16.3	3.3	90	44	90	73	1.0	9.8	1.1	4.0	4	3	4	C 0	SW 2	C 0
M	121.2	121.3	121.6	121.4	10.7	15.6	11.0	12.1	17.4	8.0	84	61	84	76	2.4	8.3	2.3	4.4	6.1	6.6	5.8	1.0	2.7	1.[illegible]

Zakopane — $H_s = 844\,m$ — $H_b = 838{,}2\,m$ — $h_w = 17{,}7\,m$ — Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBIENIE GU h	POGODA
1	8	12.5	•	♀1401-03 ♀0-1400 ♀1 1648-52 ♀2-1712 ♀1-1721 ♀0-1755; K°1652-1745 NW-NE; ⌒1 0000-8
2	6	7.1	•	♀1 142-240 ♀0-341 ♀2-340 ♀0-358 ●0 551-628 ●1-750 ●0-905 ●0...1035; 1146-1232 ●1-1345 ●0-1510 ●1-1605 ●0-1725; K°1751-215; = 320-1940; ⌒°22-24
3	8	0.4	•	♀0 1503-06 1924-2006; ⌒°0-1 ⌒1 2-8, 22-24 | 4.VII: = 1330, 24, ⌒1 0000-3 ⌒2 4-7
4	7	9.2	•	●1 0927-31 ♀0-959 ●0 1025-52 ●1 1055 ●0-1105 ●1...1128 ♀0 1155-1200 ♀2-1201 ♀0-1220 ●1-1243 ♀0-1315 ●0-1406 ●1-1502 ●0-1515; 1650-1715 1810 ●0 1845 1915 2023 2202 2902 24;
5	6	18.2	•	●0 0000-50 ●1-135 ●0 218 320 ●0 614-20 ●1-715 ●0-940 ●1-1023 ●2 1033 ●1-1040 ●0-1058 ●1-1147 ●0-1437 ●1-1441 ●0-1501 ●1-1516 ●0-1530 ♀0 1530-38 ●0 1922-24 ♀1-1926 ●0-2000; = 0000 830; 20-24
6	8	0.6	•	♀0 1515-1608 1652 1718 1728 1826; = 0000 515; ⌒°21-24
7	9	•	•	⌒°0000 1 ⌒1 2-8 ⌒°23-24; ⌣°2010-2120
8	9	19.1	•	♀0 1602-08 1733-54 ♀1-1801 ♀0 1827 ●1-1835 ♀2-0 2020 ♀0 2101-02 ♀2 2102-37 ♀1 2216 ♀0 2230 ♀1-2243 ♀0-2310; K°1825-2050 NW K°2119 2220 W; ⇘ 025 1130 (por. 17 miesiąc); ⌒°0000 9; ∞°12-13
9	8	0.1	•	♀0 1111-14 1116-18 1230-51 1316-18 1956-59 1444-46 1531-32; ⌒°21-24
10	9	0.0	•	♀0 1055 1107, 1526-28 ♀1 1922-26; ⌒°0-8
11	8	0.2	•	♀1 1701-08; ⌒°2-8
12	9	0.9	•	●0 1831-36 2110 2206 2316-28 ●1-2340 ●0...24; ⌒1 3-8
13	9	0.0	•	●0 0000...45 ●2 1212-16 ●0-2220 ●1-925 ●0-2245 742-48; ⌒°19-21 ⌒1 22-24
14	9	•	•	⌒1 0000-2 ⌒2 10 ⌒°20-24
15	9	•	•	⌒1 0000-3 ⌒1 4-5 ⌒2 6-8 ⌒°20-24; ⌫°2130-2215 W
16	9	0.6	•	♀1 1111-43 ♀2-1148 ●0-1203; (K)°SW 1042 1238 E; ⌒°0000 8
17	8	10.7	•	♀0 0552 101 ♀0-1920 ♀1-1934 ♀0 2029 ♀0-2049-50 ♀1-0555 ♀2-1001 ♀1-0 1013 ♀2-1015 ♀2-0 1055 ♀1 1150-53 ♀2-0 1332 1420 ♀0 1516; (K)°0552-1415 W-E K°0855 0945 N-E K°E 1320 1750
18	7	2.4	•	♀0 0957-59 1008 1128 ♀1-1134 ♀0 1218 ●0 1307 1321...34 1402...15 1506 1521-1602; = 940 1015; ⌒1 3-5
19	8	0.5	•	♀0 5 32-38 ♀1-553 ♀2-602 ♀0-622 ♀1-632 ♀2-705...15 1201-25 1435-42; = 630 730; ⌒°22-24
20	8	10.8	•	●0 1030-28 1048-50 ♀2-1059 ♀0-1112 ♀1-2 1123-49 ♀2-1223 ♀1 1207 ♀2-1 1344 ♀0 1350 ♀0-1 1405 ♀1 1530-55 ♀2 1604 ♀1-1645 ♀0-1705 ♀1 1747 1813 2352-24; = 2330 24, ⌒1 0000 2 ⌒3-9
21	9	8.9	•	♀0 0000 111 1340-43 ♀1-1348 ♀2-1348 ♀1-2 1404 1433 1501 ♀0 2040 24, (K)°1355-1445 SW-NW; = 0000 230
22	9	•	•	♀0-1 0000 132 ♀2-136 ♀0-1 252 ♀2-305 ♀1-1318 ♀3 1345-48 ♀2-3 32 ♀2-0 410; ⌒°20-23 ⌒1-24
23	8	0.3	•	●0 915 1012-21 ♀1 1027-30 ♀0-1033; 1056 1105; ⌒1 0-4 ⌒2 5-9, 20-24
24	9	•	•	⌒1 0000-8 ⌒°20-24
25	8	0.0	•	⌒°0000-7, 20-23 ⌒1-24
26	8	5.1	•	●0 554 710 742 835 ●1 902 ●0-944 ♀1-2 958 ♀2 1003 ♀0-1054 1240 ♀0 1302-13 ●0 1358 1413 1510-12 1541-43 1725 1810 1920 1958 2110 2147 2207; ⌒1 0000 6
27	8	0.6	•	●0 0446 501 ●1-510 ●0-818 ♀0 932-56 1004-12 1111-22 1207-15
28	7	0.0	•	●0 652 710
29	9	0.8	•	⌒°4-9
30	8	4.2	•	●0 0105-39 ●1-0140 ●0-0446 155 210 2228-35 ♀0 0956 1010 ●0-1 1405 ♀0 1604-07 1618-45 ♀1-1648 ♀0-1653 1702-08; ⌒°1646-63
31	7	4.7	•	♀0 415-19 ●0 603...13-801 ●1-845 ●0-915; 952 1014 ●1-1019 ●0-1032; 1058 1115; 2303-21; = 930 1215
Σ	-	117.7	-	

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1	8	67.9	•	●0 1722 1827 ♀1-1935 ♀2-1940 ♀1-2001 ●0-1 2152 ●2 2201 ●1-2213 ●2 2302 ●1-2308 ●2-24; = 610 700 1840 24
2	6	24.4	•	●2 0000-16 ●1-0222 ●2-035 ●1-053 ●2 126 ●1-158 ♀2-500 ●2-1033 ●1 1110 ●0-1127 ●1-1136 ●0-1306; K°1522 430; = 000 1330, ⌒1 21-22 ⌒2 23-24
3	8	0.0	•	●0 1342-46 1422 1602; ⌒2 0000 9
4	8	0.5	•	♀1 817-23 ♀0 942-53 958 1010 ♀1 1500-02 ♀0-1510
5	8	•	•	⌒°20-22 ⌒1-24
6	9	•	•	⌒1 0000 1 ⌒2-8 ⌒°20-22 ⌒1-24
7	9	•	•	⌒1 0000 9
8	9	•	•	⌒°0000 4 ⌒2-9 ⌒°21-23 ⌒2-24
9	6	1.8	•	●0 1225 1306 1830 1950 2001 2225; = 740-24; ⌒2 0000 8
10	6	14.7	•	●0 0105-30 ●1-212 ●0-725 935 1212 1315 ●0 1552 1610 ♀0-1735 ♀1-1740 ♀0-1815 ♀2 1938 ♀0-1918 ●0 2102 2238 ●0-24; = 000 24
11	6	16.3	•	●0 0000 135 ●1-150 ●0-240 ●1-253 ●0-316 ●1-345 ●0-417 ●2-525 ●1-550 ●0-605 ●1-710 ●0-843 ●1-907 ●0-1105 ●1-1111 ●2-1116 ●0-1355 ●0 1930 ●1-1965 ●0-24; = 000 1830 1930 24
12	7	11.1	•	●0 0000-30 ●2 048 ●0-115 ●2 204-20 ●0-310 350 455 ●2-700 935 ●0 1010-25 ♀0 1053-59 ●0-1112 1122-30 1139-45 ♀2-1153 ♀0-1202 1205-31 1245 1318 ♀0 1353 1402 ♀0 1435-45 1554-57 1652 1710 2340-52 ♀2-2357
13	8	0.7	•	♀0 000-10 0105-30 ♀1-0445 ♀0-0515 215-50 830-45; = 000 330; ⌒°21-24 | 12.VIII.: = 24; = 000 930; ⌒°21-2340
14	9	•	•	♀0 015-45
15	9	0.2	•	●0 045 710 ♀0 1022 1705 1520-23 ♀1-1525 ♀0-1538
16	7	•	•	= 1815-24; ⌒°21-24
17	8	•	•	= 0040-45; ⌒°0000 1 ⌒1-10, 19-23 ⌒2-24
18	9	•	•	⌒2 0000 9 ⌒1 19-23 ⌒2-24
19	8	•	•	= 2210-24; ⌒2 0-9 ⌒°20-24
20	6	•	•	= 0000-50 ∞ 815 2040; ⌒1 0000 10 ⌒°19-24
21	8	•	•	= 0000 240; ⌒°0000 3 ⌒1-10
22	9	•	•	por. miesiąc 14 miesiąc 930 1215 ⇘-1446 (por. 17 miesiąc), por. miesiąc 12 miesiąc 1445 1530
23	9	0.0	•	
24	8	4.5	•	●0 002...10 1235 1310 ●2-1319 ●0-1340 1545 1605 1925 2040 ♀1-2047 ♀2-2050 ♀0-2108 ♀2-2111 ♀0-2130 ●0 2227 2328 ♀1-2328 ♀0-2359; = 1815-24
25	8	38.0	•	●0 130 215 638 710 940 1002 ♀0 1013-37 1036-38 ●0 1235...30 ♀0 1838-46 ♀2-1935 ♀1 1945 ♀2-2050 ♀1-2110 ●1-2318 ●0-24; = 000 615 2110-24
26	6	48.1	•	●0 000-30 ●2-102 ●0-130 ●1-1040 ●2 1045 ●1-1305 ●2-1315 ●0-1353 ●1-1701 ●0-1753 ●1-1835 ●0-1940 ●1-2110 ●0-2240 ●1-24; = 000 24
27	6	5.0	•	●0 006-22 ●0-412 ●1-422 ●0-430 ●1-450 ●0-706 ●1-714 ●0-722 ●1-738 ●0-855 1016-22 1148 1205-40 ●1-1302 ●0-1325 1408 ●2 1420 ●0-1515 1632-40; = 000 640 840 1115 1215 1515 1815-24
28	8	0.4	•	●0 440 511 ●1-519 ●0-538 ●1-557 ●0-720; = 000-45 545 715; ⌒°22-24
29	8	0.1	•	♀0 1502 1408 1535-46; ⌒°0000 9
30	9	0.4	•	●0 750 928 ♀0 1607-22 1702-17; ⌒°20-24
31	8	•	•	⌒1 0000-9, 20-24
Σ	-	253.9	-	

Zakopane — $\varphi = 49°18'$ — $\lambda = 19°57'$ — *Wrzesień – Septembre* 1965

DNI	CIŚNIENIE P=800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	116.8	118.7	120.5	118.7	11.9	15.7	15.7	14.8	16.9	6.2	77	65	64	69	3.2	6.3	6.4	5.3	5	7	6	SW 1	SSW 7	ENE 1
2	121.5	123.1	123.9	122.8	15.6	22.3	20.0	19.5	22.7	10.7	62	34	44	47	6.8	17.8	13.2	12.6	8	7	9	SSW 4	SSW 6	S 8
3	119.9	120.5	120.6	120.3	18.9	24.1	18.9	20.2	25.1	16.1	48	38	53	46	11.3	18.6	10.1	13.3	9	8	8	S 6	SSW 4	SW 6
4	116.1	116.0	118.2	116.8	17.7	15.4	8.3	12.4	20.4	8.2	64	92	94	83	7.1	1.4	0.7	3.1	9	10 •	1	WSW 2	NE 2	C 0
5	118.2	117.7	116.7	117.5	7.3	16.4	11.0	11.4	18.4	4.7	94	47	84	75	0.6	9.9	2.2	4.2	5	4	2	C 0	SSW 6	NNE 2
6	114.1	114.2	112.9	113.7	12.1	15.5	12.4	13.1	19.1	8.5	74	69	94	79	3.7	5.5	0.9	3.4	9	10 •	10 •	ENE 3	SE 2	C 0
7	114.5	115.3	117.4	115.7	6.7	14.4	11.7	11.1	15.3	5.8	92	51	65	69	0.8	8.1	4.9	4.6	4	3	8	C 0	W 6	SE 3
8	120.2	121.5	121.8	121.2	9.5	15.3	9.2	10.8	16.7	8.4	87	52	86	75	1.6	8.4	1.6	3.9	8	2	6	WSW 2	WNW 4	C 0
9	119.8	120.8	120.1	120.2	8.5	20.7	14.7	14.6	22.3	5.0	89	54	66	70	1.3	11.3	5.6	6.1	1	6	7	C 0	ENE 1	SW 1
10	117.2	118.5	118.9	118.2	16.7	17.8	18.1	17.7	20.4	10.5	64	62	56	61	6.9	7.7	9.1	7.9	9	8	5	WSW 3	S 5	S 7
11	115.8	117.9	119.0	117.6	17.9	17.7	9.5	13.6	21.6	9.4	63	72	95	77	7.5	5.7	0.7	4.6	8	8	10 •	SE 2	WNW 2	C 0
12	119.1	119.1	117.6	118.6	8.0	12.8	8.7	9.6	14.1	7.6	93	62	91	82	0.7	5.6	0.9	2.4	10	7	9	C 0	C 0	C 0
13	116.1	115.9	117.5	116.5	5.8	12.9	6.8	8.1	14.2	3.1	94	63	97	85	0.6	5.6	0.3	2.2	5	8	4	C 0	ENE 1	SE 1
14	119.2	121.1	124.5	121.6	5.8	9.0	6.0	6.7	10.2	3.0	98	80	92	90	0.1	2.4	0.8	1.1	9	10	4	C 0	C 0	SE 2
15	126.1	127.4	130.0	127.8	6.4	12.9	6.7	8.2	13.4	3.8	88	62	94	81	1.2	5.7	0.6	2.5	7	7	7	SSW 3	W 2	SW 1
16	130.4	130.5	129.8	130.2	4.7	15.2	6.3	8.1	15.8	3.2	98	56	95	83	0.1	7.7	0.4	2.7	1	1	0	C 0	NE 3	SW 1
17	128.6	127.8	127.5	128.0	4.3	18.0	8.4	9.8	18.8	2.3	97	60	97	85	0.3	8.2	0.3	2.9	0	2	0	C 0	ESE 1	E 1
18	125.1	123.4	122.6	123.7	6.1	19.7	10.4	11.6	19.9	3.2	100	42	79	74	0.0	13.2	2.6	5.3	10 ≡	1	0	C 0	NE 3	NNE 1
19	122.6	126.3	128.8	125.9	8.0	9.0	6.3	7.4	14.1	5.6	94	93	97	95	0.6	0.8	0.2	0.5	7	10 •	10 •	C 0	W 1	C 0
20	130.5	132.0	135.3	132.6	5.9	7.8	6.3	6.6	8.6	5.5	98	91	97	95	0.2	1.0	0.2	0.5	10 •	10 •	10	C 0	NE 2	C 0
21	136.0	136.4	134.7	135.7	6.5	10.8	2.9	5.8	11.1	2.8	96	62	96	85	0.5	5.0	0.2	1.9	10 •	9	0	C 0	NNE 3	E 1
22	131.7	130.0	128.0	129.9	3.4	17.0	6.3	8.2	18.9	0.5	95	54	97	82	0.4	9.1	0.2	3.2	5	1	0	C 0	E 2	ESE 1
23	125.7	124.3	122.6	124.2	4.4	18.5	7.5	9.5	19.6	2.1	91	57	94	81	0.8	9.2	0.6	3.5	2	0	0	ESE 1	NE 1	S 1
24	121.8	121.5	121.5	121.6	4.3	18.0	7.3	9.2	19.2	2.4	95	52	96	81	0.4	9.7	0.4	3.5	0	0	1	C 0	E 2	C 0
25	120.3	118.9	117.7	119.0	4.0	19.6	10.0	10.9	21.1	2.2	93	48	78	73	0.5	12.0	2.8	5.1	1	9	3	C 0	NE 2	NE 1
26	114.1	114.6	115.2	114.6	15.6	18.7	16.2	16.7	19.7	9.6	51	44	49	48	8.7	12.2	9.4	10.1	2	3	7	SE 5	S 5	SSE 6
27	112.9	114.2	115.2	114.1	14.6	17.1	16.0	15.9	18.0	14.3	78	44	56	59	3.7	11.0	8.1	7.6	9 •	2	2	ESE 3	S 10	S 5
28	114.9	114.5	110.4	113.3	16.8	20.2	20.1	19.3	20.6	15.3	58	48	48	51	8.1	12.4	12.3	10.9	6	8	5	SSW 5	SSW 4	SSW10
29	110.5	115.3	120.9	115.6	13.2	9.8	3.5	7.5	20.4	3.4	96	85	98	93	0.6	1.8	0.1	0.8	10 •	10 •	0	C 0	WNW 4	C 0
30	119.9	121.1	122.5	121.2	12.3	18.0	6.8	11.0	18.7	2.2	49	39	94	61	7.3	12.5	0.6	6.8	8	7	1	SSW 5	E 3	E 1
31																								
M	120.7	121.3	121.7	121.2	9.8	16.0	10.4	11.6	17.8	6.2	83	59	81	74	2.9	8.2	3.2	4.8	6.2	5.9	4.5	1.5	3.1	2.0

Październik – Octobre

1	122.7	122.9	123.5	123.0	5.3	19.3	11.0	11.6	20.1	3.7	97	57	92	82	0.3	9.6	1.0	3.6	1	0	0	ESE 1	ENE 1	C 0
2	122.3	121.6	123.1	122.3	7.0	21.1	10.1	12.1	21.5	5.4	98	56	91	82	0.1	11.0	1.2	4.1	0	1	0	C 0	E 1	C 0
3	125.0	125.8	126.9	125.9	6.7	16.0	13.0	12.2	17.1	5.4	99	78	95	91	0.1	4.1	0.7	1.6	2	7	10	C 0	ENE 2	C 0
4	126.7	126.5	126.0	126.4	8.9	17.5	10.0	11.6	18.6	7.3	97	74	97	89	0.3	5.3	0.3	2.0	9	4	10	C 0	E 1	C 0
5	125.1	125.8	126.6	125.8	11.4	10.8	7.7	9.4	11.6	7.5	100	97	84	94	0.0	0.4	1.7	0.7	10 ≡	10	4	C 0	NE 1	E 1
6	126.7	126.0	125.7	126.1	0.5	11.6	2.5	4.3	13.0	0.0	98	62	98	86	0.1	5.1	0.1	1.8	8	5	0	C 0	ENE 3	C 0
7	124.3	123.9	124.0	124.1	1.4	14.7	4.6	6.3	15.5	-0.2	98	67	95	87	0.2	5.5	0.4	2.0	0	1	7	C 0	ENE 2	E 1
8	122.2	120.5	121.4	121.4	1.2	15.9	9.3	8.9	16.7	0.3	92	50	93	78	0.5	9.1	0.8	3.5	9	8	10	C 0	C 0	NE 1
9	120.6	120.0	120.0	120.2	5.2	5.1	3.9	4.5	9.3	3.4	97	90	89	92	0.2	0.9	0.9	0.7	10	10	10	C 0	C 0	ENE 1
10	118.7	119.8	121.9	120.1	3.1	2.6	-0.2	1.3	4.2	-0.4	85	73	92	83	1.1	2.0	0.5	1.2	10	9	1	C 0	NE 2	C 0
11	121.7	120.4	121.5	121.2	2.2	9.7	4.4	5.2	10.0	-1.6	88	50	85	74	0.9	5.9	1.3	2.7	9	4	8	C 0	WNW 4	ESE 1
12	125.7	128.1	130.5	128.1	1.4	4.3	-3.1	-0.1	5.6	-3.4	81	56	93	77	1.3	3.7	0.4	1.8	8	1	0	NE 2	NE 1	C 0
13	130.1	129.6	129.0	129.6	-4.4	10.4	0.4	1.7	11.1	-5.8	81	30	84	65	0.8	8.7	1.0	3.5	0	1	7	C 0	E 2	C 0
14	127.7	127.6	127.7	127.7	-2.9	11.7	0.5	2.4	12.8	-3.6	99	44	90	78	0.0	7.6	0.6	2.7	8	1	0	C 0	ENE 1	C 0
15	126.8	126.6	126.4	126.6	-2.9	13.8	0.6	3.0	14.6	-4.0	91	37	88	72	0.4	10.0	0.8	3.7	4	1	3	C 0	ESE 1	C 0
16	124.1	121.8	123.6	123.2	-2.2	15.6	9.2	8.0	15.9	-3.5	87	35	63	62	0.7	11.4	4.3	5.5	3	8	10	C 0	SE 3	SE 1
17	128.0	130.2	130.9	129.7	3.6	5.3	-1.5	1.5	9.2	-1.5	91	72	98	87	0.7	2.5	0.1	1.1	9	8	0	C 0	NW 1	C 0
18	129.0	128.0	128.8	128.6	-5.3	7.8	-0.4	0.4	9.5	-5.6	93	70	98	87	0.3	3.2	0.1	1.2	3	0	0	C 0	NE 1	E 1
19	129.0	129.0	130.2	129.4	-0.7	7.0	2.8	3.0	8.2	-3.5	95	65	90	83	0.3	3.5	0.7	1.5	10	10	9	SE 1	ENE 1	E 1
20	130.5	131.3	133.0	131.6	-1.0	5.0	-2.2	-0.1	5.3	-2.3	92	62	93	82	0.5	3.3	0.4	1.4	8	8	7	ENE 1	NE 1	C 0
21	133.1	133.1	134.7	133.8	-6.7	3.9	-4.6	-3.0	4.7	-6.8	88	60	91	80	0.4	3.3	0.4	1.4	2	0	0	C 0	NE 2	C 0
22	135.4	135.6	135.3	135.4	-7.5	7.2	-3.3	-1.7	7.9	-8.2	87	35	92	71	0.4	6.7	0.4	2.5	0	0	0	C 0	ENE 2	C 0
23	133.0	131.4	130.1	131.3	-3.2	9.9	0.3	1.8	10.6	-3.1	79	29	84	64	1.0	8.6	1.0	3.5	6	8	3	C 0	E 1	C 0
24	129.8	129.9	131.1	130.3	-0.5	6.9	-1.7	0.8	7.6	-2.7	94	63	96	84	0.4	3.6	0.2	1.4	10	0	0	C 0	C 0	C 0
25	129.8	129.2	129.3	129.4	-1.9	11.7	-1.1	1.9	12.1	-3.8	94	26	83	68	0.3	10.2	0.9	3.8	1	0	0	C 0	NE 2	C 0
26	127.7	126.7	125.9	126.8	-2.1	12.5	-0.4	2.4	13.5	-3.0	86	41	82	70	0.7	8.6	1.1	3.3	0	0	0	C 0	E 1	SW 1
27	124.2	124.0	125.0	124.4	-3.4	12.4	2.6	3.6	13.2	-4.3	83	27	78	63	0.8	10.6	1.6	4.3	1	0	0	S 1	SSW 3	SE 2
28	124.6	123.1	123.2	123.6	0.9	15.9	3.5	6.0	16.1	-0.6	68	34	86	63	2.1	11.9	1.1	5.0	7	9	8	C 0	SW 2	C 0
29	122.5	120.5	120.3	121.1	-0.5	16.4	6.7	7.3	16.9	-1.0	98	39	82	73	0.1	11.3	1.8	4.4	3	9	6	C 0	W 5	C 0
30	124.7	124.3	122.6	123.9	3.9	7.5	-1.5	2.1	10.7	-1.3	93	55	93	80	0.6	4.7	0.4	1.9	10	2	1	C 0	WSW 3	C 0
31	119.1	118.2	117.7	118.3	-2.0	9.1	4.0	3.8	10.1	-3.9	81	62	89	77	1.0	4.5	0.8	2.1	7	9	10 •	C 0	W 6	WNW 3
M	125.2	125.9	126.3	126.1	0.5	10.9	2.8	4.2	12.0	-1.4	91	55	89	78	0.5	6.3	0.9	2.6	5.4	4.3	4.0	0.2	1.8	0.5

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	8	.	.	⌓ 1 00–7
2	9	.	.	por. wiatru 12 m/sek 9 30–11 15, do 14 m/sek 20 15–24
3	9	.	.	por. wiatru 14 m/sek 3 30–4 30, 7 15–10 30
4	6	12.0	.	● 0 8 12–18 ● 3 0 43–45 ● 1 0 52 ● 0 8 0–10 03 ● 1 0 56–11 00 ● 2–0 12 20 ● 0–1 12 38–58 ● 2 13 02 ● 0–1 14 02 ● 2 14 10 ● 0–1 15 30 ● 2 15 44 ● 0 16 40; 17 15...25; = 10 30–16 30; ⌓ 0 23–24; ⌒ 0 9 58–10 02; 17 20–22
5	9	.	.	⌓ 0 00–8, 20–24
6	8	6.1	.	● 0 9 32–10 03, 10 17–26, 10 58–11 23, 12 24–43 15 48–16 08, 16 18–27, 16 34, 17 42, 18 38–55, 19 27–36 ● 0 19 42...20 24 ● 2–20 45 ● 1–21 26 ● 2–21 48 ● 0–22 01; = 20 30–22 30, ⌓ 0 00–6, ⌒ 0 10 58–59
7	9	0.9	.	
8	9	0.0	.	● 0 8 16–22 ● 1–1 28 ● 0–1 53, 3 28–31 ● 1–3 32 ● 0–3 42 ● 1–3 43 ● 0–4 28, 7 06–10, ⌓ 0 20–24
9	9	.	.	⌓ 0–1 ⌓ 1–8 ⌓ 0 20–24
10	9	0.4	.	por. wiatru 12 m/sek 15 30–16 15, 20 15–21 20, ⌓ 0 00–8
11	9	27.9	.	● 0 3 07–15, 4 18–23, 5 11–16, 5 36–48 ● 0 10 36–42 ● 2–10 48 ● 1–0 11 02 ● 0 14 38 15 10 ● 2–15 17 ● 0–1 15 13 ● 2–15 25 ● 1–15 32 ● 2–15 35 ● 1–19 01 ● 2–19 30 ● 1–21 04 ● 0–22 15, 22 35–23 07; = 17 30–24
12	7	.	.	● 0 1 44–1 15 ● 0 1 42–2 40; = 0 00–10 20, ⌓ 0 22–24
13	8	6.4	.	● 0 10 37–58, 13 18–20, 13 34–37, 16 06–07 ● 2–16 16 ● 0–16 28, 16 44–58, 17 16–36 ▲ 0–17 37 ● 2–18 04 ● 0–18 37; = 20 15–21 40; ⌓ 1 00–3 ⌓ 2–8, ⌒ 0 16 16–17
14	6	1.6	.	● 0 7 48...8 00–12 22; = 8 15–15 30, ⌓ 0 23–24
15	8	.	.	⌓ 0 00–2 ⌓ 1–5 ⌓ 0–8 ⌓ 0 20–24
16	7	.	.	⌓ 0 00–4 ⌓ 2–9, 20–24
17	9	.	.	⌓ 2 00–8 ⌓ 1 20–24
18	9	.	.	= 0 6 20–25 = 1–6 30 = 2–8 35 = –9 15, ⌓ 0 19–23 ⌓ 1–24
19	6	24.2	.	● 2–1 11 16–46 ● 2–11 57 ● 1–12 22 ● 0–13 27 ● 1–14 20 ● 0–15 10, 15 25–49 ● 1–16 02 ● 2–16 05 ● 0–2 24; = 12 30–24, ⌓ 1 0–3 ⌓ 2–8
20	6	0.7	.	● 1 00–2 32 ● 0–4 20, 8 35, 12 01, 13 07 ● 0 22 10...25; = 0 00–5 30 12 20–15 30
21	8	0.0	.	● 0 6 15...7 15; = 6 30–7 30; ⌓ 0 19–22 ⌓ 2–24; = 6 30–7 30
22	9	0.2	.	⌣ 0 00–3 ⌣ 1–7 ⌓ 0 19–20 ⌓ 1–24
23	9	0.1	.	⌓ 1 00–3 ⌓ 2–5 ⌓ 0–8 ⌓ 0 19–21 ⌓ 1–24
24	8	.	.	⌓ 1 00–4 ⌣ 0–7 ⌓ 0 20–24
25	9	.	.	⌓ 1 00–4 ⌣ 0–5 ⌣ 2–8 ⌓ 0 19–23
26	9	0.5	.	● 0 19 44–48, por. wiatru do 12 m/sek 6 30–21 15
27	9	0.0	.	● 0 3 45–4 12, 5 07–53, 6 12–7 02, por. wiatru do 14 m/sek 7 20–8 30 ⊳–9 20 ⊳–10 40 ⊳–14 30 por. wiatru do 14 m/sek ... 24
28	9	9.2	.	por. wiatru 14 m/sek 0 00–18 ⊳–4 30 (por. 20 m/sek), por. wiatru 14 m/sek 4 30–7 20–8 40–12 15 13 05–15 30 por. wiatru 17 m/sek 15 30–16 25, do 12 m/sek 16 25–22 15
29	7	14.2	.	● 0 1 33–2 25, 3 11–19 ● 2–0 21 ● 1–3 38 ● 0–3 50 ● 2–3 52 ● 0–1 8 20 ● 0–1 8 51 ● 2–8 58 ● 0–1 9 07 ● 1–0 9 16 ● 2–9 28 ● 1–0 9 55 11 12–14 06; = 5 30–7 10, 8 40–9 10, ⌒ 20–23 ⌣ 0–24
30	9	.	.	por. wiatru do 12 m/sek 6 20–11 15; ⌣ 0 00–4 ⌓ 0 19–20 ⌓ 1–23 ⌓ 2–24
31				
Σ	–	104.4	–	

Październik - Octobre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	9	.	.	⌓ 2 00–8 ⌓ 0 18–22 ⌓ 1–24
2	9	.	.	⌓ 1 00–1 ⌓ 2–8, 20–24
3	7	3.2	.	● 2 15 56–16 02 ● 0–16 23 ● 2–16 25 ● 1–16 31 ● 2–16 38 ● 0–16 54 ● 2 17 01 ● 0–17 15; ☒ 0 16 08–☒ 1 16 29–☒ 0 17 10–30 S-N; = 9 50–10 50, 17 30–24, ⌓ 2 00–9
4	8	0.0	.	● 0 5 40 6 25; = 0 00 3 40 = 0–4 50 = 20 15–24; ⌓ 0 19–24
5	4	2.7	.	● 0 6 42–8 30 ● 2–8 30 ● 1–8 50 ● 3–9 15 ● 0 10 50–11 20, 15 02–16 25; = 0 00–5 50 = 0–6 15 = 2–7 35 = 0–8 45 = –21 30; ⌓ 0 00–6
6	9	.	.	⌓ 2 0–4 ⌣ 1–8 ⌓ 0 19–20 ⌓ 1–22 ⌣ 0–24
7	8	.	.	⌣ 1 1–8 ⌓ 0 19–20 ⌓ 1–22 ⌣ 0 22–24, ⊖ 1 20 15–22 10, 23 15–24
8	9	1.4	.	= 18 30–24; ⌣ 0 00–3 ⌣ 1–4 ⌣ 2–8 ⌓ 0 19–24, ⊖ 0 00 21 10 ⊕ 1 6 25–9 15
9	6	0.8	.	● 0 00–52 ● 1–1 03 ● 0–4 15 5 32–6 8, 7 15–20 ● 1–7 28 ● 2–8 10 12 45, 13 20 ● 0 22 25–32 ● 1–22 34 ● 0–22 40; = 0 50–4 45 = –14 30, 18 40–22 30
10	8	0.2	.	● 0 0 10–16, 3 28–29 ⊼ 1–8 37 ● 0 9 17–23, 9 41–50 ● 0 ⊼ 0–10 04, 10 57–11 07; ⌓ 0 20–21 ⌣ 0–24, ⊖ 1 21 30–23 20
11	9	0.8	.	⌣ 0 00–1
12	9	.	.	● 0 0 13–3 51; = 0 15–6 10; ⌣ 0 19–21 ⌣ 1–24
13	8	.	.	⌣ 2 00–9 ⌣ 0 20–24
14	9	.	.	⌣ 0 00–3 ⌣ 2–8 ⌣ 0 18–22 ⌣ 1–24
15	9	.	.	⌣ 1 00–4 ⌣ 2–8 ⌣ 0 20–22 ⌣ 1–24
16	9	1.5	.	● 0 22 20–30 ● 1–22 41 ● 0–24, ⌣ 2 00–8
17	8	.	.	● 0 00–1 05 ● 0–1 17, 2 45–58, ⌣ 0 20–24
18	8	.	.	= 17 35–18 10, = 17 35–18 10; ⌣ 2 00–9 ⌣ 0 19–24
19	8	.	.	= 19–20 30; ⌣ 1 00–9 ⌣ 0 23–24
20	8	.	.	= 5 45–9 30, 22–24; ⌣ 0 00–9 ⌣ 1 21–24
21	9	.	.	⌣ 1 00–3 ⌣ 2–10, 20–24
22	8	.	.	⌣ 2 00–11 ⌣ 0 19–24
23	9	.	.	⌣ 0 00–1 ⌣ 1–9 ⌣ 0 20–24, ⊕ 1 9 40–13 15
24	8	.	.	= 3 30–9 30; ⌣ 0 00–8, 20–24
25	9	.	.	⌣ 0 00–9 ⌣ 1 20–24
26	8	.	.	⌣ 2 00–9 ⌣ 0 20–24
27	9	.	.	⌣ 0 00–1 ⌣ 1–11, 19–24
28	9	.	.	⌣ 0 00–1 ⌣ 1–8; ⊕ 0 12 15–13 10
29	9	2.5	.	● 1 21 32–22 12 ● 1 22 36–48 ● 0–24, ⌣ 0 2–8
30	8	.	.	● 0 00–1 50 ● 0 3 27–4 20; = 9 30–6 30; ⌣ 1 20–24
31	9	3.7	.	● 0 17 47...18 10–29 25; ⌣ 1 00–9
Σ	–	16.6	–	

Zakopane — $\varphi = 49°18'$ — $\lambda = 19°57'$ — *Listopad — Novembre 1965*

DNI	CIŚNIENIE P = 800 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	116.2	111.1	109.1	112.1	2.3	11.7	13.1	10.0	14.4	-1.4	85	51	40	59	1.1	6.7	9.1	5.6	10	9	8	W 2	WSW 8	WSW 8
2	107.9	110.0	113.2	110.4	10.5	9.5	7.2	8.5	13.1	7.0	55	58	53	55	5.5	5.0	4.9	5.1	7	9	8	WSW 6	W 7	WSW 6
3	114.7	113.9	113.2	113.9	3.5	9.2	9.0	7.7	9.8	3.3	65	47	57	56	2.9	6.2	5.0	4.7	1	7	8	W 2	NNW 4	SW 6
4	119.3	122.5	125.7	122.5	1.0	1.7	1.3	1.3	9.0	0.5	100	96	85	93	0.0	0.3	1.2	0.5	10 ● ≡	10 ≡	10	NE 1	E 1	C 0
5	128.1	129.3	132.9	129.8	-0.4	2.1	-0.6	0.1	2.4	-0.8	86	72	77	78	0.8	1.9	1.3	1.3	10	8	8	ENE 1	NE 1	C 0
6	132.2	131.1	128.8	130.7	-4.5	6.2	-1.6	-0.4	7.1	-5.1	88	56	80	75	0.5	4.1	1.1	1.9	0	2	1	S 1	E 2	C 0
7	125.0	122.6	123.7	123.8	-5.5	9.3	-1.7	0.6	9.6	-4.0	81	33	78	64	0.9	7.8	1.2	3.3	8	1	0	C 0	ENE 2	C 0
8	124.7	125.6	126.8	125.7	-5.5	9.3	-2.2	0.4	10.5	-4.9	78	44	79	67	1.0	6.7	1.1	2.9	6	7	0	E 2	NE 1	C 0
9	125.8	125.2	124.1	125.0	-5.0	10.1	-1.0	1.3	10.7	-5.7	77	42	89	69	1.1	7.1	0.6	2.9	2	0	6	C 0	NE 1	C 0
10	121.9	120.6	117.9	120.1	-5.5	5.3	1.1	1.0	6.2	-4.5	95	81	96	91	0.3	1.7	0.2	0.7	1	9	10	C 0	NE 2	C 0
11	111.8	107.9	104.9	108.2	1.1	0.5	-5.0	-1.1	1.3	-5.1	94	96	95	95	0.4	0.2	0.5	0.5	10 ✱	10 ✳	10 ✳	E 2	NE 5	NE 1
12	103.3	105.3	107.9	105.5	-4.3	-4.1	-5.6	-4.9	-5.0	-6.0	94	82	95	90	0.3	0.8	0.2	0.4	10 △	10 △	10 △	C 0	C 0	C 0
13	108.3	108.2	109.1	108.5	-5.6	-4.6	-6.2	-5.6	-4.3	-6.5	95	91	92	95	0.2	0.4	0.3	0.3	10	10 ✳	10	ENE 2	NE 1	NE 2
14	109.3	110.4	112.1	110.6	-7.1	-6.9	-8.1	-7.6	-6.2	-8.4	91	91	90	91	0.3	0.3	0.3	0.3	10 ≡	10	10 ⛆	E 1	NE 3	C 0
15	114.0	115.9	119.4	116.4	-12.7	-5.6	-8.2	-8.7	-5.1	-13.0	73	77	87	79	0.6	0.9	0.4	0.6	8	3	8 ✳	C 0	SSE 2	WNW 2
16	123.9	124.7	125.8	124.8	-10.7	-8.8	-10.5	-10.1	-8.2	-11.0	87	71	87	82	0.4	0.9	0.4	0.6	9 ✳	10	4 ✳	NE 1	W 5	C 0
17	124.7	121.9	118.3	121.6	-13.8	-7.7	-14.2	-12.5	-7.3	-15.9	79	73	87	80	0.4	0.9	0.3	0.5	10 ✳	1	2	C 0	C 0	C 0
18	113.4	110.3	108.8	110.8	-13.5	-5.5	-7.9	-8.7	-5.2	-15.4	84	75	90	83	0.4	1.0	0.3	0.6	8	10	5	C 0	NE 1	C 0
19	107.5	106.8	105.8	106.7	-6.0	2.8	-5.5	-2.6	3.5	-9.9	92	75	99	89	0.3	1.9	0.0	0.7	2	7	10 ≡	C 0	ESE 1	NNE 1
20	104.3	104.7	105.1	104.7	-2.2	1.9	0.2	0.0	1.9	-5.1	98	98	100	99	0.1	0.1	0.0	0.1	9	10 ●	7	C 0	C 0	C 0
21	97.8	93.6	94.7	95.4	5.2	4.0	4.7	4.6	6.8	-1.9	75	92	69	79	2.1	0.6	2.6	1.8	10 ●	9	9	SW 5	NE 5	WSW 6
22	101.5	108.3	112.5	107.4	-1.0	-2.5	-4.3	-3.0	5.1	-4.6	89	76	77	81	0.7	1.3	1.0	1.0	10	6	10	WNW 5	WNW 5	NW 1
23	115.8	117.6	120.1	117.8	-7.1	-9.4	-10.0	-9.1	-4.3	-10.2	91	82	84	86	0.3	0.5	0.4	0.4	10 ✳	10 ✳	10 ✳	NE 1	NE 5	NE 1
24	120.2	118.2	117.3	118.6	-17.7	-4.8	-14.1	-12.7	-4.7	-18.3	84	59	79	74	0.2	1.7	0.4	0.8	1	0	0	C 0	SSE 1	E 1
25	117.3	117.7	118.8	117.9	-12.3	-2.6	-9.8	-8.6	-2.3	-16.5	78	81	88	82	0.5	1.0	0.4	0.6	3	10	2	C 0	W 4	C 0
26	112.7	108.8	108.8	110.1	-8.6	1.7	-5.5	-3.5	3.3	-13.4	92	61	88	80	0.3	2.7	0.6	1.2	10	6	10	W 1	SE 5	SE 1
27	106.6	98.6	92.3	99.2	-5.4	4.9	6.4	3.6	7.3	-4.1	92	74	74	80	0.4	2.3	2.5	1.7	8	9	6 ●	C 0	SSW 8	SSW 14
28	93.7	97.1	103.2	98.0	1.0	-1.1	-1.5	-0.8	7.4	-1.6	96	77	80	84	0.3	1.3	1.1	0.9	10 ●	8	4 ✳	WSW 2	WSW 6	WSW 6
29	108.8	110.6	102.5	107.3	-2.1	0.6	2.3	0.8	2.5	-2.4	83	57	62	67	0.9	2.8	2.7	2.1	8	1	10 ✳	NW 3	WSW 2	WNW 7
30	98.2	99.9	102.2	100.1	7.7	6.4	-0.9	3.1	8.4	-1.1	51	57	98	69	5.1	4.1	0.1	3.1	9	8	10	SW 7	SSW 5	C 0
31																								
M	113.6	113.3	113.5	113.4	-3.8	1.1	-2.4	-1.9	3.0	-6.1	84	71	82	79	0.9	2.4	1.3	1.5	7.3	7.0	6.9	1.4	2.9	2.1

Grudzień — Décembre

DNI	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	105.0	107.2	110.5	107.6	-3.5	-0.9	-0.6	-1.4	-0.3	-5.7	74	73	70	72	1.2	1.5	1.8	1.5	0	4 ✳	9	SW 6	SSW 8	SW 5
2	111.8	112.3	110.2	111.4	-3.3	0.7	-9.0	-5.2	0.7	-9.5	70	66	92	76	1.3	2.2	0.3	1.3	2	1	0	SSW 1	WNW 4	C 0
3	103.3	103.0	102.5	102.9	0.8	-1.6	-4.3	-2.4	1.6	-10.2	56	63	94	71	2.9	2.0	0.3	1.7	10	10	10 ✳	NE 3	E 1	C 0
4	104.3	106.1	108.6	106.4	-1.4	0.2	-3.7	-2.2	0.9	-6.4	88	87	90	88	0.6	0.9	0.5	0.7	8	8	10	SSW 1	NE 1	C 0
5	109.9	109.0	102.6	107.2	-5.6	1.9	4.4	1.3	6.3	-6.4	90	64	53	69	0.4	2.3	4.0	2.3	1	10	9	SW 1	SW 6	SW 7
6	102.4	106.8	110.6	106.6	5.1	2.7	3.4	3.6	9.4	2.1	79	75	58	71	1.9	1.8	3.3	2.3	10 ●	5	4	SW 4	WNW 4	WNW 3
7	112.1	113.8	115.7	113.9	2.7	5.1	1.7	2.8	5.2	-0.6	64	51	82	66	2.6	1.3	1.2	1.7	9	10	9	SW 2	WSW 5	S 1
8	116.1	116.1	119.9	117.4	-0.7	-0.6	-1.6	-1.1	1.8	-1.9	99	91	88	93	0.0	0.5	0.6	0.4	10 ✳	10 ✳	9	C 0	W 1	SW 1
9	122.6	118.3	111.6	117.5	-8.4	-1.3	-9.5	-7.2	-0.2	-10.1	86	72	88	82	0.4	1.6	0.4	0.8	7	2	0	C 0	NE 1	C 0
10	95.6	94.3	94.2	94.0	6.3	4.3	0.1	2.8	7.0	-10.8	52	80	94	75	4.5	1.7	0.4	2.2	9	10 ●	9	S 10	NE 2	C 0
11	96.1	97.8	100.9	98.3	0.3	-2.3	-3.9	-2.4	1.0	-4.3	92	93	85	92	0.5	0.1	0.7	0.4	10	10 ✳	7	NW 2	W 3	WSW 1
12	103.9	105.8	108.8	106.2	-3.1	-2.6	-2.9	-2.9	-2.3	-6.6	90	87	93	90	0.5	0.7	0.3	0.5	10 ✳	10 ✳	10 ✳	WNW 1	W 3	SW 2
13	111.5	112.0	109.9	111.1	-3.3	-1.3	-5.0	-4.2	-0.4	-7.7	90	70	83	81	0.4	1.7	0.7	0.9	10	5	10	C 0	SW 2	SW 1
14	111.3	118.6	124.4	118.1	-3.7	-7.2	-9.8	-7.6	-3.4	-10.3	92	82	81	85	0.4	0.6	0.5	0.5	10 ✳	7 ✳	9 ✳	NE 2	NNE 2	C 0
15	122.9	121.4	120.5	121.6	-6.8	-3.7	-2.7	-4.0	-2.5	-17.4	75	90	91	85	0.9	0.3	0.5	0.6	10	10 ✳	10 ✳	SSE 2	W 3	NNW 2
16	119.4	118.8	119.2	119.1	-5.8	-3.9	-7.2	-6.0	-2.6	-11.0	89	68	88	82	0.4	1.4	0.4	0.7	4	7	8	NW 1	S 3	C 0
17	118.2	117.4	117.3	117.6	-6.5	-3.7	-5.9	-4.5	-3.5	-8.2	89	87	94	90	0.4	0.6	0.3	0.4	9	10	10	C 0	C 0	NE 1
18	117.9	118.2	120.3	118.8	-5.0	-0.4	4.9	1.1	4.9	-6.7	93	90	95	93	0.3	0.6	0.5	0.5	9	10	10 ●	C 0	C 0	WNW 3
19	121.0	120.5	119.3	120.3	3.3	6.5	6.9	6.4	8.1	4.5	94	82	76	84	0.6	1.8	2.3	1.6	10	9	3	WSW 3	S 3	WSW 4
20	119.3	119.6	117.7	118.9	8.3	5.6	0.3	3.7	10.3	0.0	71	76	94	80	3.2	2.1	0.3	1.9	10	9	3	W 2	NE 1	C 0
21	114.3	113.0	113.8	113.7	0.7	2.6	1.6	1.6	3.4	-0.5	98	93	98	96	0.1	0.6	0.2	0.3	9	10	10	C 0	C 0	W 1
22	116.9	117.0	117.3	117.1	-1.9	-2.4	-4.0	-3.1	2.2	-4.2	96	89	91	92	0.2	0.3	0.4	0.4	10 ⛆	10 ✳	10	NE 1	NE 2	C 0
23	115.4	112.8	108.6	112.3	-5.1	-4.3	-5.5	-5.2	-4.0	-5.7	88	84	90	87	0.5	0.7	0.4	0.5	10	10	10	E 2	E 1	NW 1
24	104.3	102.4	100.2	102.3	-9.7	-2.9	-7.0	-6.6	-2.4	-10.1	88	73	91	84	0.4	1.3	0.3	0.7	7	7	10	S 1	C 0	C 0
25	95.2	93.9	93.9	94.3	-6.3	-1.9	-6.5	-5.3	-0.9	-11.8	89	81	91	87	0.4	1.0	0.3	0.6	8	3	6	NE 2	ENE 3	C 0
26	94.8	97.0	104.4	98.7	-2.1	2.2	-2.3	-1.1	3.0	-8.1	89	69	83	80	0.5	2.2	0.9	1.2	9	4	10 ⛆	S 1	C 0	NNW 3
27	108.7	106.6	100.4	105.2	-9.2	-2.8	2.9	-1.6	3.2	-11.1	85	71	58	71	0.4	1.3	3.1	1.7	0	3	5	WSW 1	C 0	ESE 4
28	98.1	102.2	108.8	103.0	0.3	1.3	-2.0	-0.6	3.3	-2.2	94	73	70	80	0.3	1.7	1.6	1.2	10	10	9	C 0	WNW 5	W 4
29	112.2	114.6	117.3	114.8	-9.5	-3.4	-7.6	-7.0	-2.0	-10.4	91	69	57	72	0.3	1.5	1.5	1.1	4	4	2	C 0	NW 5	WSW 3
30	114.6	111.2	110.5	112.1	-12.8	-2.5	-1.4	-4.3	3.4	-13.2	81	63	74	73	0.4	1.9	1.4	1.2	3	3	9	C 0	C 0	ENE 2
31	110.4	109.9	111.6	110.6	-2.6	1.7	-1.0	-0.7	2.6	-3.3	87	70	81	79	0.7	2.0	1.1	1.3	10	8	7	C 0	WNW 5	WNW 3
M	109.9	110.2	110.7	110.3	-2.9	-0.5	-2.4	-2.0	1.8	-6.7	84	77	83	81	0.9	1.3	1.0	1.1	7.7	7.5	7.6	1.6	2.4	1.7

Zakopane

$H_s = 844\,m$ $H_b = 838{,}2\,m$ $h_w = 17{,}7\,m$

Listopad - Novembre 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	POGODA
1	9	0.1	.	•0 9^28 10^10 ∇0 20^42 21^21, 21^30-37, 21^52 22^17, por: wiatru do 14 m/sek 20^20 21^10
2	9	0.2	.	∇0 7^26-30, 7^30-50
3	9	0.0	.	•0 17^38, 18^06
4	5	0.0	.	•0 6^25-7^45, = 4^10-15 ≡1-11^40 ≡0-13^45 = -20^15
5	8	.	.	⌴0 23-24
6	7	.	.	⌴0 0^00-1 ⌴1-9 ⌴0 18-24
7	9	.	.	⌴0 0^00-1 ⌴1-10 ⌴0 19-24
8	8	.	.	⌴0 0^00-10, 19-22 ⌴1-24
9	9	.	.	⌴1 0^00-9 ⌴0 18-24
10	7	0.5	.	= 9^15-11^30 15^20-21^20; ⌴0 0-1 ⌴1-9; ▽0 18^25-21^15
11	6	8.6	.	•0 4^42-5^40 *0 10^10-18 *0-6^32 *0-7^15 *0-9^00 *0-11^18 *1-12^13 *0-16^25 *1-17^30 *0-21^25; = 6^15-24
12	6	1.0	5	△0 0^15-4^40 6^14-17^40, 20^12-22^15; = 0^00-3^30, 7^30-24
13	6	0.7	5	*0 10^45-16^22; = 0^00-24
14	6	0.7	5	△0 16^35-21^20 *1-24; = 0^00-6^50 ≡0-11^50 = -24; V0 7^30-11^50
15	6	0.1	6	*0 0^00-4^40, 8^05-25, 15^40-17^10, 20^05-24; = 0^00-5^30, 8^10-13^15, 20^15-24
16	7	0.3	5	*0 0^00-7^15 △0-10^15 *0-10^52 11^04-12^25 13^12-16^20 17^12, 20^03-24; = 0^00-11^30, 15^30-20^15, 22^20-24
17	8	0.0	6	*0 0^00-2^33, 3^30-9^20; = 0^00-9^30, 22^30-24
18	6	0.0	6	*0 12^43-14^10, 14^52-15^15; = 0^00-7^30, 10^15-24
19	7	.	6	= 16^40-18^40 ≡0-19^30 ≡1-20^01 ≡2-24; ⌴1 0-9 V0 18^40-24
20	5	4.5	6	⌓0 7^44-8^17 *0-8^48 •0-9^14 •0-9^26 •0-10^12 •0-13^20 •0-14^05 •1-15^52 •0-17^28 *0-17^36 ∇0-18^20 *0-19^05 •0-19^25 ≡0 20^00-3^40 = -15^45 ≡0-15^50 ≡1-16^08 ≡2-16^20 ≡1-16^42 ≡0-17^25 = -21^40 ≡1-24;
21	7	8.7	3	•0 5^20-12^22 13^38-14^10 •1-14^44 •0-16^20 ∇0 21^42-22^17, ≡1 0^00-2^35 ≡2-3^00 ≡0-3^45 = -6^15-15^20-18^15
22	8	1.8	1	*0 4^40-32
23	6	0.8	4	△0 0^50-2^20 *0-3^25 *2-4^13 *0-7^11 *1-9^15 *0-10^20 *1-10^45 *0-15^10-14^25-15^55, 18^35-22^45; = 2^30-15^30, 18^30-20
24	9	.	8	⌴0 1-11, 20-21 ⌴1-24
25	8	0.0	4	*0 12^55-13^25; ⌴1 0^00-10 ⌴0 20-24
26	9	0.0	4	⌴0 0^00-8
27	8	1.6	4	*0 0^12-25 7^25 9^20 •0-10^15 •0-11^40 •0 14^02-31 17^35 18^12 •0 20^05-20^25 •0 21^18 ∇1-21^26 •0-21^40 ∇1-22^03 •0-22^10 ∇0-22^20, por: wiatru do 14 m/sek 10^25-11^15 ≫ 12^40-13^35 (por: do 22 m/sek), por: wiatru do 17 m/sek 13^35-17^10
28	9	0.8	pł.	*0 5^32-7^04 *1-7^27 *1-8^55 ∇0 9^20-27 *1-9^36 ∇0-10^20, 20^25-21^30, ≫ 0^00-15 (por: do 14 m/sek); = 7^20-8^25
29	9	0.0	1	∇0 10^05-25 7^42-8^07 22^10-24, por: wiatru do 18 m/sek 20^40-21^10 ≫ 22^15 (por: 17 m/sek) ≫ -23^45 (por: do 24 m/sek), por: wiatru do 17 m/sek 23^45-24; ⌓0 22^32-45
30	9	9.6	pł.	*0 5^20-3^25 •0 7^13-8^05 •0 8^25-8^35, 9^20 •1 9^27 ∇1-9^44 •1 10^09 •0 10^22-10^50-11^16 *0 11^52-15^18 *1 15^25 •0-17^10 *1-19^15 *0-24, por: wiatru do 17 m/sek 0^00-2^20 ≫ -4^40 (por: 17 m/sek), por: wiatru do 14 m/sek 4^40-13^15;
31				**30.XI:** = 15^15-16^50 ≡0-18^45 = -24
Σ	-	40.0	-	

Grudzień - Décembre

1	8	0.1	4	△0 0^45-1^22 *0 8^25-9^15, 10^40-17^35 ∇1-18^25 *1-19^05 *0-19^30-21^10 ∇0 22^18-32; = 18^25-20
2	9	.	4	⌴0 7^8-24
3	8	2.5	4	*0 15^25-16^15-17^45 *1-18^20 *0-22^38; = 17^30-24, ⌴1 0^00-3
4	7	0.1	8	*0 11^52-12^08 *1-12^15 *0-12^25; = 0^00-5^30, 12^05-30, 18^15-23^20
5	8	0.4	8	•0 23^48-24; por: wiatru do 14 m/sek 19^15-24; ⌴0 0^00-3 ⌴2-9
6	8	0.0	pł.	•0 0^00-2^40, 5^35-7^45, 8^45-9^05 *0 11^30-46 △0 12^52-13^17; por: wiatru do 14 m/sek 0^00-6^15
7	9	0.5	pł.	
8	6	3.5	2	*0 4^02-6^12 *1-7^42 *0-13^25 *1-15^15 *0-18^45; = 6^30-18^15
9	7	.	7	⌴0 18-24
10	8	0.5	3	•0 9^52-11^12 •0-13^22 14^18-15^35-17^08, por: wiatru do 17 m/sek 14^20-6^10 ≫ -8^20 (por: do 26 m/sek); = 20^20-24
11	6	2.1	pł.	*0 5^55-9^20-11^30 *1-13^12 *0-14^23, 15^10-28; = 0^00-3^15, 6^25-14^15; ⌴0 0^00-3 ⌴1-6
12	5	3.7	4	*0 0^07-19 *1-7^12 *0-7^20 7^42-8^12 *1-2 11^10 *1-0 11^52 ∇0 12^26-51 ∇0-13^12 ∇0-13^25-14^18, 14^33-51 ∇2-15^03 ∇0-15^12 ∇0-1 15^28-17^20 ∇0 19^10-22^25 *0 23^30-24; = 8^20-17^15, 23^30-24
13	8	7.8	10	*0 0^00-1^20 8^18-35-9^15 20^43-21^18 *1-22^30 *0-23^12; = 0^00-1^30, 8^20-9^15, 18^22-24; ⌴0 18-21
14	7	2.0	16	*0 0^48-1^25 *1-3^15 *0-5^10 *1-7^35 *1-11^42 *1-11^55 *0-12^20 *1-12^36 ∇0-13^09 ∇1-14^12 ∇0-16^04 *0 17^52-22^17; = 1^00-12^30, 20^20-24
15	7	2.7	21	*0 10^32-11^15-14^10-15^17-24; = 0^00-3^40, 10^40-11^30, 15^10-24, ⌴1 0^00-5
16	8	0.3	25	*0 0^00-2^37, 13^18-32-14^15-28; = 0^00-5^40
17	6	2.1	24	*0 9^03-28 14^43-17^02 *1-19^06 *0-19^15-19^25-20^10; = 6^30-24
18	6	5.9	26	*0 0^42-1^22 11^56-12^15 •0 14^05-24; = 0^00-1^30, 6^10-9^15, 11^30-18^15, 20^05-24; ⌴0 2-8
19	9	.	8	•0 0^00-20, 2^25-6^12; = 0^00-6^20
20	7	.	pł.	= 13^15-19^15; ⌴0 19-24
21	6	1.7	pł.	•0 15^02-16^15 •0-17^08 •1-18^25 •0-19^05-23^22-24; = 5^30-22^45 ≡0-23^15 ≡1-24; ⌴0 0^00-7
22	6	5.3	1	•0 0^00-15 •1-1^32 △0-6^10 △1-7^35 △0-8^34 △0-8^36 △1-8^52 ∇1 △0-8^55 ∇1-9^10 *1-11^38 *0-14^48 △0-17^00 *0-19^15-21^15-23^22; = 1^00-10 ≡0-21^5 = -24
23	8	0.0	10	*0 7^22-10^23; = 0^00-10^50
24	7	0.3	6	*0 14^42-15^30 △0-19^40; = 0^30-5^20, 14^15-21^12 ≡0-21^20 ≡2-22^33 = 22^50-24; ⌴1-9 V0 21^12-22^33
25	8	.	7	= 0^00-10; ⌴0 0-11, 18-24
26	8	1.6	6	*0 16^20-18^15 △1 18^20-30 *0 18^35-19^15 ∇1 19^05-20 ∇0 19^25-20^35 △0 20^40-21^10, 21^15-22^20; = 18^15-24; ⌴0 0^00-9
27	9	0.1	8	*0 0^25-1^35 ∇0 22^42-23^07, 23^38-24; = 0^00-6^10; ⌴0 6-10
28	8	0.0	4	∇0 0^00-15, 1^17-23 ∇0 10^54-11^05, 11^25-12^15
29	8	.	4	⌴0 3-10, 22-24
30	8	.	3	= 9^15-11^25; ⌴0 0^00-11
31	9	0.0	2	= 3^30-8^30
Σ	-	45.2	-	

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Styczeń – Janvier 1965

DNI	CIŚNIENIE p = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	90.7	89.7	87.9	89.4	-3.3	-1.7	-3.6	-3.0	-0.9	-6.9	54	79	94	76	2.2	1.1	0.3	1.2	6	9	9	SW 18	SSW14	S 9
2	82.6	82.3	82.1	82.3	-4.7	-4.9	-5.3	-5.0	-3.4	-6.7	98	98	98	98	0.1	0.1	0.1	0.1	10 ✳ ≡	9	10 ✳ ≡	W 3	WSW 3	S 3
3	81.8	82.0	82.5	82.1	-7.5	-6.4	-7.9	-7.4	-5.3	-9.2	96	97	96	96	0.1	0.1	0.1	0.1	10 ✳ ≡	10 ✳ ≡	10 ✳	E 1	S 1	ESE 1
4	83.1	85.6	89.6	86.1	-10.0	-9.9	-12.6	-11.3	-7.9	-12.9	94	94	92	93	0.2	0.2	0.2	0.2	10 ✳ ≡	10△ ≡	10 ✳ ≡	NNE 9	NNE10	NNE12
5	92.5	93.1	93.5	93.0	-15.6	-10.4	-10.6	-11.8	-8.2	-16.1	95	94	94	94	0.1	0.2	0.2	0.2	0	10 ≡	10 ✳ ≡	N 10	NW 13	N 16
6	93.3	93.5	91.6	92.8	-12.1	-13.5	-12.7	-12.8	-10.6	-14.7	93	92	92	92	0.2	0.2	0.2	0.2	10 ≡	7	10 ✳ ≡	N 14	NNW10	N 8
7	90.8	92.0	92.1	91.6	-17.5	-15.7	-13.2	-14.9	-12.7	-18.2	95	100	60	85	0.1	0.0	0.9	0.3	10 ✳ ≡	3	3	N 10	NNE 6	NNW 4
8	90.5	89.6	87.0	89.0	-8.0	-5.9	-2.3	-4.6	-2.2	-13.5	98	97	98	98	0.1	0.1	0.1	0.1	10 ✳ ≡	10△ ≡	10 ✳	WSW 5	NW 8	W 13
9	86.1	85.6	84.3	85.3	-3.4	-4.2	-8.3	-6.0	-1.6	-8.6	97	96	95	96	0.2	0.2	0.2	0.2	10 ≡	10 △	10 ✳ △ ≡	WNW14	WSW14	WNW16
10	82.7	81.5	89.8	84.7	-9.5	-8.3	-10.5	-9.7	-8.1	-11.8	91	95	94	93	0.3	0.2	0.2	0.2	9	10 ✳ △ ≡	10 ✳ △ ≡	WSW12	WNW15	NNW10
11	95.9	97.6	98.9	97.5	-12.5	-8.0	-4.0	-7.1	-3.7	-12.9	92	39	46	59	0.2	2.0	2.5	1.6	5	3	0	NNE 7	NW 3	W 2
12	98.6	97.8	95.7	97.4	-4.1	0.3	-5.7	-3.8	0.4	-6.0	52	33	64	50	2.2	4.2	1.4	2.6	7	8	1	S 7	S 6	SSE17
13	95.5	95.9	96.1	95.8	-2.0	-2.8	-3.8	-3.1	-1.4	-6.4	9	24	35	23	4.8	3.8	3.0	3.9	1	1	4	SSE10	SSE 9	SSE 7
14	93.8	92.4	95.8	94.0	-8.1	-5.6	-4.9	-5.9	-3.3	-8.8	92	97	98	96	0.2	0.1	0.1	0.1	3	10 ≡	9	SSE11	SSE13	S 9
15	97.7	98.1	96.0	97.3	-7.2	-5.6	-5.6	-6.0	-4.7	-8.3	96	95	97	96	0.1	0.2	0.1	0.1	9 ✳	9	10 ≡	SSW 3	SSE 4	SSE 8
16	94.5	95.0	94.6	94.7	-8.0	-5.5	-9.0	-7.9	-4.4	-10.5	33	23	89	48	2.2	3.1	0.4	1.9	7	7	8	S 10	SSE 6	S 11
17	89.3	86.9	83.8	86.7	-7.9	-5.9	-2.4	-4.6	-2.2	-9.0	90	94	98	94	0.3	0.2	0.1	0.2	9	10	10 ✳ ≡	S 22	SSW20	S 17
18	79.7	79.1	77.2	78.7	-7.7	-8.5	-10.3	-9.2	-2.3	-10.7	96	95	94	95	0.1	0.2	0.2	0.2	9	10	9 ✳	W 7	SSW 6	SW 5
19	75.1	75.0	75.4	75.2	-12.0	-7.6	-8.7	-9.2	-7.4	-12.7	82	54	37	58	0.4	1.6	2.0	1.3	2	8	10	S 4	SSE 1	ESE 3
20	69.4	68.7	68.7	68.9	-9.5	-7.7	-6.5	-7.6	-6.4	-11.4	91	96	79	89	0.3	0.1	0.8	0.4	10 ✳	10 ✳	8	NE 3	ESE 3	SE 3
21	71.3	74.8	79.2	75.1	-6.1	-6.8	-8.2	-7.3	-3.7	-10.7	68	86	60	71	1.2	0.5	1.3	1.0	3	5	1	SSE 2	SE 4	S 7
22	81.9	84.2	87.7	84.6	-10.4	-7.8	-6.7	-7.9	-6.0	-13.6	78	51	51	60	0.6	1.7	1.8	1.4	2	3	7	SSE 9	S 10	SE 2
23	88.8	90.2	93.4	90.8	-6.5	-3.2	-5.3	-5.1	-2.6	-8.3	97	95	98	97	0.1	0.2	0.1	0.1	10 ✳	10 ✳	10 ≡	NNE 3	C 0	NE 1
24	96.2	96.4	96.0	96.2	-7.6	-5.6	-3.6	-5.1	-3.0	-8.3	96	97	89	94	0.1	0.1	0.5	0.2	10 ≡	9	10 ✳	NNE 4	ENE 4	C 0
25	92.8	91.7	90.9	91.8	-6.4	-7.6	-11.0	-9.0	-3.6	-12.4	97	96	77	90	0.1	0.1	0.6	0.3	10 ≡	10 ≡	0	SSE 1	S 2	SW 5
26	90.0	89.9	90.3	90.1	-8.8	-8.9	-7.0	-7.9	-7.0	-12.2	92	95	53	80	0.3	0.2	1.7	0.7	4	9	4	S 4	SSE 4	SW 2
27	88.7	89.8	90.8	89.8	-8.4	-7.4	-6.1	-7.0	-6.1	-11.3	95	96	97	96	0.2	0.1	0.1	0.1	10 ✳	10 ✳ ≡	10 ≡	SE 8	ESE 9	SSE10
28	91.4	92.1	92.6	92.0	-5.6	-4.7	-4.4	-4.8	-3.0	-7.4	97	98	98	98	0.1	0.1	0.1	0.1	10 ≡	10 ≡	10 ≡	SSE17	SSE13	SSE19
29	90.6	91.0	91.3	91.0	-4.2	-4.0	-3.9	-4.0	-3.5	-4.7	96	96	96	96	0.2	0.2	0.2	0.2	10 ≡	10 ✳ △ ≡	10 ✳ △ ≡	SSE19	SSE21	SSE13
30	89.0	88.4	90.2	89.2	-3.2	-3.6	-2.5	-3.0	-1.7	-4.0	97	97	86	93	0.1	0.2	0.7	0.3	10 ≡	10 ≡	9	SSE16	S 16	SSW13
31	91.2	91.3	89.4	90.6	-0.9	-0.9	-0.8	-0.8	0.3	-2.5	99	99	99	99	0.0	0.0	0.0	0.0	10 △	10 ✳ ≡	10	SW 10	SSW 7	SW 12
M	88.2	88.4	88.9	88.5	-7.7	-6.4	-6.7	-6.9	-4.4	-10.0	86	84	82	84	0.6	0.7	0.7	0.7	7.6	8.4	7.8	8.8	8.2	8.3

Luty – Février

1	88.7	88.5	89.4	88.9	-10.3	-12.0	-15.0	-13.0	-0.8	-15.3	94	89	87	90	0.2	0.3	0.2	0.2	10 ✳ △ ≡	2	10 ✳ ≡	NNW 4	SW 5	NW 5
2	91.1	92.2	95.9	93.1	-16.0	-16.5	-17.0	-16.6	-15.0	-17.7	86	90	90	89	0.2	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	NNW15	NNW11	N 11
3	94.8	94.5	94.5	94.5	-19.2	-15.7	-15.0	-16.2	-14.5	-19.4	95	86	87	89	0.1	0.3	0.2	0.2	1	9 ✳ △	10 ✳ ≡	NNW 9	NNW 6	N 4
4	92.9	93.6	92.1	92.9	-14.7	-12.3	-13.6	-13.6	-12.3	-15.2	87	93	92	91	0.3	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	NNW 6	N 7	NNW11
5	86.6	85.5	85.7	85.9	-20.0	-17.5	-21.7	-20.2	-13.6	-21.8	83	74	81	79	0.2	0.4	0.2	0.3	1	1	0	N 12	N 6	N 12
6	87.8	89.0	87.8	88.2	-23.0	-20.6	-21.6	-21.7	-20.1	-23.6	88	82	89	86	0.1	0.2	0.1	0.1	10 ≡	4	0	N 12	NNW 9	NNE11
7	86.3	87.5	84.6	86.1	-20.1	-16.9	-17.7	-18.1	-15.8	-21.9	71	55	52	59	0.4	0.7	0.7	0.6	0	0	4	NNE 9	NE 6	NNW 6
8	71.7	72.4	75.5	73.2	-12.8	-17.6	-16.4	-15.8	-11.0	-18.1	88	84	90	87	0.3	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	NNW16	NNW14	NNW12
9	80.2	84.5	88.3	84.3	-21.1	-18.7	-20.3	-20.1	-16.4	-22.7	96	89	89	91	0.0	0.1	0.1	0.1	10 ✳ ≡	10 ✳ ≡	10 ✳	N 14	N 12	N 11
10	89.8	88.9	87.1	88.6	-15.9	-13.5	-12.2	-13.4	-10.7	-20.8	49	43	89	60	0.9	1.2	0.3	0.8	0	3	10 ✳ ≡	NNE 7	WSW11	NW 11
11	87.9	90.0	93.4	90.4	-14.4	-14.5	-14.2	-14.3	-12.2	-15.6	91	91	87	90	0.2	0.2	0.3	0.2	10 ✳ ≡	10 ✳	10 ✳ ≡	NNW11	N 10	NNW10
12	95.1	95.5	94.9	95.2	-13.8	-10.6	-10.0	-11.1	-9.3	-14.5	88	41	91	73	0.3	1.5	0.3	0.7	6	5	10 ✳ ≡	SSE 2	SW 2	NW 3
13	90.1	87.1	82.5	86.6	-11.8	-10.2	-9.9	-10.4	-9.6	-12.1	93	91	94	93	0.2	0.3	0.2	0.2	10 ✳ ≡	9	10 ≡	SSW 5	S 13	SSW17
14	79.1	79.7	82.7	80.5	-10.9	-9.9	-10.2	-10.3	-9.7	-11.7	90	94	91	92	0.3	0.2	0.3	0.3	10 ✳ ≡	9 ✳	9 ✳ ≡	SSW 9	SW 13	WSW 8
15	84.0	85.2	85.5	84.9	-12.5	-12.9	-14.9	-13.8	-10.2	-16.2	92	88	56	79	0.2	0.3	0.8	0.4	10 ✳	9	9	WSW 5	SW 3	NW 3
16	83.0	83.8	83.7	83.8	-16.3	-14.7	-16.4	-16.0	-14.3	-16.9	67	96	95	86	0.6	0.1	0.1	0.3	10	10 ✳ ≡	10 ✳ ≡	NNE 6	NNW 8	N 12
17	82.9	83.3	85.5	83.9	-14.6	-14.3	-12.2	-13.3	-11.8	-17.0	91	91	93	92	0.2	0.2	0.2	0.2	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	N 14	NNE 9	NNE11
18	86.2	87.6	88.3	87.4	-12.2	-13.0	-13.5	-13.0	-10.8	-15.4	93	92	88	91	0.2	0.2	0.3	0.2	10 ✳ ≡	10 ✳ △ ≡	10 ✳ △ ≡	NNE12	NNE12	NNE15
19	88.9	89.6	90.3	89.6	-14.3	-14.2	-14.8	-14.5	-12.1	-17.2	87	87	91	88	0.3	0.3	0.2	0.3	10 ✳ △ ≡	10 ✳ ≡	10 ✳ ≡	NNE14	NW 7	N 11
20	91.2	95.6	96.6	94.5	-15.4	-7.6	-11.6	-11.6	-6.8	-18.1	91	85	86	87	0.2	0.5	0.4	0.4	2	1	1	ENE 3	C 0	ESE 3
21	94.9	94.5	91.4	93.6	-11.3	-5.8	-11.0	-9.8	-4.7	-12.2	83	80	70	78	0.4	0.8	0.8	0.7	1	1	1	ENE 2	N 3	NNE 4
22	87.0	85.8	86.3	86.4	-12.0	-16.1	-18.0	-16.0	-10.5	-18.1	83	91	90	89	0.4	0.2	0.2	0.3	10 ✳ ≡	10 ✳ ≡	10 ✳ ≡	NW 7	NW 8	NNW 8
23	87.0	86.6	86.4	86.7	-16.6	-15.6	-16.1	-16.1	-15.4	-19.4	90	95	91	92	0.2	0.1	0.2	0.2	10 ✳	10 ✳ ≡	10 ✳ ≡	NNW 9	WNW 4	NW 7
24	86.9	87.0	85.1	86.3	-17.4	-14.4	-12.8	-14.4	-12.6	-19.2	69	71	47	62	0.5	0.6	1.2	0.8	0	1	1	NE 2	SW 4	SW 5
25	81.1	80.5	80.1	80.6	-17.3	-13.9	-20.2	-17.9	-11.3	-20.3	90	92	89	90	0.2	0.2	0.1	0.2	6	9 ✳	10 ✳ ≡	WNW 8	NW 10	NNW 9
26	81.5	83.3	80.7	81.8	-20.9	-18.1	-16.6	-18.0	-16.3	-21.8	89	90	66	82	0.1	0.2	0.6	0.3	10 ✳ △ ≡	3	9	NW 10	W 7	SSE12
27	74.6	72.8	74.9	74.1	-16.7	-15.0	-19.8	-17.8	-14.5	-20.1	90	91	83	88	0.2	0.2	0.2	0.2	9	10	7 ✳	SSE12	WSW13	W 14
28	80.6	83.9	85.9	83.5	-21.6	-18.2	-16.5	-18.2	-15.7	-22.2	96	47	17	53	0.0	0.8	1.4	0.7	10 ≡	0	1	NW 10	NW 11	S 13
29																								
30																								
31																								
M	86.2	86.7	87.0	86.6	-15.8	-14.3	-15.3	-15.2	-12.1	-18.0	86	82	81	83	0.3	0.4	0.4	0.4	7.4	6.6	7.6	8.8	8.0	9.2

Kasprowy Wierch $H_s = 1991\,m$ $H_b = 1988{,}8\,m$ $h_w = 15{,}4\,m$ **Styczeń – Janvier 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	9	2.8	115	⩧ 20^30–24; ⇘ 0^00–8^00 (por. 34) ≫–19^00 (por. 26); ✢^0-1 11^15–16^30; () 0^00–24
2	8	4.4	118	*^0-1 4^35 8^40 △^0–11^10, 12^05 14^58 20^10 *^0-1–24; V^0-1 0^30 8^25 V^0 12^50–24; ⩧ 0^00-30 ≡^2 2^30 ⩧–3^10 ≡^2–8^25 ⩧ 12^50 13^10 ≡^2–24; () 0^00-30 [3.I: ≡^2–24
3	2	4.6	122	*^0-1 0^00 4^10 *^0 7^05 △^0 8^30 ⩝^0–9^15 *^0–10^30 *^1–12^15 *^0 14^15 △^1 15^15 16^30 *^0 19^50–24; V^0 0^00 a, 13^30 16^20 18^40 19^45 21^30–24; ≡^2 0^00 9^40 ⩧–10^30 ≡^0–11^30 ≡^1–13^30 ≡^2–16^20 ⩧–17^30 (m) 16^20 18^40 ≡^2–19^45 (m) ⩧–21^30
4	0	15.0	125	*^0 0^00 8^30 △^0–14^30 * △^0-1 22^30 △^0–23^30 * △^0–24; V^0 0^00 na V^0-1–24; ≡^2 0^00–24; ≫ 7^45–24, ✢^0-1 1^30–24 [5.I: ✢^0-1 0^00 10^30 ✢^1-2–24; () 6^30 11^30
5	0	6.5	140	* △^0 0^00 1^30 △–3^30 *^0–5^30 △^0 13^50 15^40 ⩝^2 20^05 22^25 ⩝^1-0 22^40 ⩝^0–24; V^0-1 0^00 5^30 11^10–24; ≡^2 0^00 5^30 (m)–11^10 ⩧–11^30 ≡^2–24; ≫ 0^00 10^40 (por. 19) ⇘ ... 12^00 (por. 26) ≫–17^30 (por. 25) ⇘–22^00 (por. 26) ≫–24 (por. 20)
6	8	12.0	142	⩝^0 0^00-30 * △^0 18^50 20^05 *^1-2 21^30 △^0–23^40 *^1–24; V^1 0^00 12 V^1 13^20 17^45–24; ≡^2 0^00 8^40 ⩧–9^40 ≡^2–12^00 ⩧–13^20 17^45 18^30 ≡^2–24; ≫ 0^00 19^40 (por. 24), 22^30–24 (por. 17); ✢^1 0^00 12^10 ✢^0–15^40 ✢^1-2–24; ⊗ 12^00 13^20; () 15^10 17^30
7	7	5.8	158	*^1 0^00 1^10 △^0–2^30 *^0-1 3^50 11^30; V^0 0^00 11^30; ≡^2 0^00 11^30 ⩧–14^30; ≫ 0^00–9^15 (por. 19); ✢^1-2 0^00 2^05 ✢^0-1–12^00
8	0	4.2	158	*^0 5^45 10^30 △^0–13^40 *^0 19^30–24; V^0 6^30 7^15 8^20 13^30 17^30 18^45 21^20–24; ⩧–4^40 6^30 ≡^0–7^15 8^20 13^30 ⩧–15^10 ≡^2 17^30 18^45 ⩧–21^20 ≡^2–24, ≫ 15^30 22^30 (por. 23) ⇘–24 (por. 29); ✢^0-2 9^30–24
9	6	8.0	161	*^0 0^00 3^30 △^0 4^30 6^10, 9^30 15^30 * △^0–17^40 △^0–18^30 * △^0–23^40 ⩝^1–24; ≡^2 0^00 10^40 ⩧–12^50 ≡^2–15^10 ⩧–18^30 ≡^2–24; ⇘ 0^00 4^30 (por. 31) ≫–20^20 (por. 25) ⇘–23^30 (por. 26) ≫–24 (por. 17); ✢^1-2 ... 19^00 ✢^0–17^00 ✢^1-2–24
10	0	19.1	164	⩝^1 0^00-30 * ⩝^0 1^30 2^40 3^30 △^0 7^15 8^50 * △^0–17^30 * ⩝^0-1 22^40 * △^0–24; V^1 0^00 3^30 V^0 7^10–24; ≡^2 0^00 2^30 ⩧–3^30, 7^10 12^30 ≡^2–24; ≫ 0^00-30 (por. 17) ⇘ ... 6^15 (por. 25) ≫–10^30 (por. 28) ⇘–11^40 (por. 20) ≫–24 (por. 22), ✢^1-2 0^00 ...
11	9	•	178	* △^0 0^00 1^50; V^0 0^00 5^50; ≡^2 0^00 5^30 ⩧–5^50 (m)–9^30; ≫ 0^00 1^30 (por. 15); ✢^1-2 0^00 1^50 ✢^0–7^10 ✢^0–8^30; () 6^30–24
12	9	•	176	⩧ 13^35 14^30, ≫ 16^00 18^15 ⇘–23^40 (por. 22) ≫–24; ✢^0 16^00 18^15 ✢^0-1–24; ⊕ 9^00 12^00; () 0^00–24
13	9	•	172	≫ 0^00 10^00, ✢^1 0^00 5^30 ✢^0–11^30, 12^10 14^30, ⌓^0 17^30 18^45; () 0^00 21^30
14	0	0.0	165	V^0 5^30 7^30, 8^30 20^50; ⩧ 5^30 7^30, 8^30 9^20 ≡^2–20^30 ⩧–20^50; ≫ 5^15 15^30 (por. 29) ⇘–20^10 (por. 25); ✢^0-1 6^00 12^40 ✢^1-2 18^10 ✢^0–21^20, 22^20 24
15	9	0.3	160	*^0 6^30 7^20, 9^55 12^30; V^0 1^40 7^10, 13^55 22^00; ⩧ 1^40 7^10 ≡^2 13^52 15^25 ⩧–16^15 ≡^2–21^30 ⩧–22^15; ≫ 21^40–24 (por. 23); ✢^0 0^00 1^20, 20^00–24; ⊕ 11^15–12^15; ⌣^2 22^00–24, () 7^30–8^30
16	9	•	158	⩧ 17^30 19^30; ≫ 0^00 7^00 (por. 17), 18^40–24; ✢^0-1 0^00 7^00; ⌣^0 0^00 4^00, 20^30 22^30; () 8^30 14^30, 20^30–24 [17.I: ✢^0-2 0^30–24; () 0^00–5^30
17	8	1.8	159	△^0 18^15 19^30 *^0 20^35 21^30 △^0–24; V^0-1 9^50 16^35 17^40–24; ⩧ 7^30 9^50 ≡^2–11^50 ⩧–12^50 ≡^2–13^20 ⩧–14^45 ≡^2–15^15 ⩧–16^35 17^40 18^15 ≡^2–19^30 ⩧–20^15 ≡^2–24; ≫ 0^00 2^10 (por. 22) ⇘–19^15 (por. 40) ≫–21^30 (por. 24) ⇘–24 ...
18	5	0.4	155	△^0 0^00 3^30 7^50 8^05 * △^0 14^50 19^20 *^0 22^00 23^20; V^1 0^00 5^30 7^15 8^30 11^15 19^15; ≡^2 0^00 5^30 ⩧–7^50 ≡^2–8^05 ⩧–8^30, 11^15-30 ≡^2–12^20 ⩧–15^30 ≡^2 18^30 ⩧–19^15; ⇘ 0^00 3^30 (por. 45) ≫ ... 6^00 (por. 20), 8^50 9^15; ✢^2 ...
19	9	0.0	154	⩧ 13^30 14^40, ≫ 0^40 3^30 7^05 8^30; ✢^0 0^40 3^30 7^05 10^15; ⊕^0 8^30–12^00 ⌓^1 23^30–24; () 3^40–24 [18.I: ✢^0 ... 8^40; () 9^30 11^15
20	5	2.2	152	*^0-1 6^30 11^30 ⩝^0-1 13^30, V^0 7^40 11^30, (m) 4^30 6^00 ⩧–7^10 ≡^2 8^30 ⩧–8^50 ≡^2–11^30 ⩧–13^30 (m)–19^30 ⩧ 16^40 17^30 (m) 23^30–24; ⌓^2 0^00 3^30, 23^30–24 ⌣^0 2^40 4^30 ⊕ 16^10 17^20; () 0^30 5^00, 14^30 16^30, 23^30–24
21	9	•	154	V^0 15^10 ... 16^10, 23^40–24; (m) 1^00 12^15 (m)–24 ⩧ 15^10 ... 16^10, 23^40–24; ⌓^0 0^00 1^50 ⌣^1 23^40–24, ⊗^0 15^00 ... 50; () 0^00–24
22	9	0.5	148	V^0 0^00-30; ⩧ 0^00-30 (m)–10^30; ≫ 7^05 15^10; ✢^0 7^30 16^20; ⌣^1 0^00-30; () 0^00–24
23	6	3.0	147	*^0 3^50 16^20, 17^45 18^20, 21^50–24; V^0 17^30–24; (m) 9^15 10^30 ≡^0–11^15 (m)–17^30 ≡^2–24; () 0^00–3^30
24	8	1.0	150	*^0 0^00-45 ⩝^0 7^30 9^30 *^0–10^10 * △^0–11^40 *^0 14^40 15^10, 20^15–24; V^0 0^00 10^10, 15^30 16^20, 23^30–24; ≡^2 0^00 10^10 (m)–24 ⩧ 15^30 16^20, 23^30–24; ⊕^0 12^15 13^15
25	0	•	152	*^0 0^00 6^30; V^0 0^00 16^30, (m) 0^00 4^30 ⩧ 0^00 5^30 ≡^2 16^20 ⩧–18^30 (m) 16^30–24 ⩧–20^30
26	8	0.0	151	V^0 12^30 15^05, 15^45 16^10; (m) 0^00 1^30 ⩧ 11^40 15^05, 15^45 16^10
27	1	7.5	150	*^0-1 5^50 16^45 ⩝^0 22^50 23^20; V^0 7^30 ρ V^1–24; ⩧ 7^30 8^30 ≡^2–24; ≫ 7^20 11^35 (por. 22), 17^30–24 (por. 19); ✢^0-1 6^10–24
28	0	•	152	⩝^1 4^50 5^15, V^1 0^00–24; ≡^2 0^00 9^05 ⩧–9^15 ≡^2–24; ≫ 0^00 6^20 (por. 20) ⇘–11^00 (por. 26) ≫–15^30 (por. 19) ⇘–24 (por. 33); ✢^1 0^00 6^20 ✢^2–24
29	0	8.1	145	⩝^0 10^40 11^30 * ⩝^0 12^50 ⩝^0–14^30 △^0 16^15 18^30 * △^0–23^30 △^0–24; V^1 0^00 9^00 V^0-1–24; ≡^2 0^00 8^15 ⩧–8^30 ≡^2–24, ⇘ 0^00 19^50 (por. 35) ≫–21^50 (por. 19) ⇘ ... 24 (por. 23); ✢^2 0^00 19^30 ✢^1-0 24
30	0	4.0	147	△^0 0^00-30 6^45 11^15 * △^0 21^50–24; V^1 0^00 13^15 V^0 13^40 22^40 23^10; ≡^2 0^00 13^15 ⩧–13^40, 22^40 23^10; ≫ 0^00 4^30 (por. 22) ⇘–12^50 (por. 32) ≫–14^30 (por. 26), 19^30–24 (por. 25); ✢^1-0 0^00 3^30 ✢^1-2 13^30 ✢^0–15^10; () 16^15 22^30
31	1	5.1	144	△^0 0^00 ... 40 4^50 5^10, 6^30 8^30 *^0 9^50 15^40 ⩝^0–16^15 *^0–19^45, 22^15–24; V^0 5^50 6^15 8^40–24; ⩧ 5^50 6^15 ≡^2 8^40 9^05 ⩧–10^30 ≡^2 19^45 ⩧–22^15 ≡^2–24; ≫ 0^00 6^10 (por. 24), 20^10–24 (por. 23); ✢^0 7^30 8^30, 20^00–24
Σ	–	114.1	–	

Luty – Février

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	6	10.1	147	*^0 0^00 3^45 ⩝^0 6^10 9^15 *^1–10^40 *^0–11^50, 13^40 18^20 *^1–18^40 *^0–16^40 *^1–24; V^0 0^00 na V^1–11^50 V^0 27^40–24; ≡^2 0^00 11^50 ⩧–13^40 ≡^2–17^35, 18^20–24; ≫ 0^00-15, 23^00–24; ✢^0 0^00 3^00 ✢^0 20^00 22^40 ✢^1–24
2	0	17.7	170	*^1 0^00 3^00 *^0–24; V^0 0^00 5^40, 17^30–24; ≡^2 0^00–24; ≫ 0^00 22^30 (por. 19); ✢^1 0^00–24
3	5	6.2	190	*^0 0^00 6^15 * △^0 8^50 10^30 12^20 13^10 *^0-1–24; V^0 0^00 6^25, 7^10 10^25, 10^50–24; ≡^2 0^00 6^25 ⩧–7^10 ≡^2–10^15 ⩧–10^25, 10^50 11^30 ≡^2–12^02 ⩧–12^50 ≡^2–24; ≫ 7^30 10^20 (por. 16); ✢^1-0 0^00 11^15 ✢^0 13^45–14^30
4	0	15.0	204	*^0 0^00 6^10 *^0-1–24; V^0 0^00 a V^1–24; ≡^2 0^00–24; ≫ 0^00–24; ✢^0 0^30 6^10 ✢^0-1 9^30, 15^40 22^00 ✢^1-2–24
5	9	•	220	*^0 0^00 3^20; V^0 0^00 4^15; ≡^2 0^00 4^15; ≫ 0^00 10^40, 15^15–24 (por. 21); ✢^1-2 0^00 5^00 ✢^0–10^40, 16^50 19^00 ✢^1–24; () 10^30 23^30
6	8	0.9	220	*^0 8^50 11^40; V^0 6^10 12^15; ⩧ 3^50 4^15 ≡^2–9^30 ≡^1–11^30 ⩧–12^50; ≫ 0^00 5^00 (por. 22), 6^30 7^50 8^30 10^50, 13^30 ... 24; ✢^1-2 0^00 1^00 ✢^2–8^30 ✢^1-0 24
7	9	1.5	215	*^0 21^50–24; V^0 21^40–24; ⩧ 21^40-50 ≡^2–23^30 ⩧–24; ≫ 0^00 3^30, 21^40 23^40; ✢^0 0^00 6^50, 21^50 23^45, zielony promień 16^40 (niebiesko-zielony); () 7^15 21^50
8	0	22.7	212	*^0 0^00 7^30 *^1–20^00 *^0–24; V^0 0^00–24; ⩧ 0^00-20 ≡^2–24; ≫ 0^30 3^10 (por. 21) ⇘–7^10 (por. 31) ≫–24 (por. 26); ✢^0 0^30 2^10 ✢^1-2 24 [9.II: ⌣ 22^50 23^20
9	1	7.6	225	*^0 0^00 9^50 11^30 13^50 19^40, 20^20 22^50; V^0 0^00 12^45 V^1 13^50 V^0–24; ≡^2 0^00 9^50 ≡^0–11^45 ≡^2–19^40 ⩧–21^20 ≡^2–22^50 ⩧–23^50; ≫ 0^00 11^30 (por. 17), 12^20 13^50, 14^40 15^40, 16^50 17^20, 19^50 21^40; ✢^1-2 0^00 12^50 ✢^0–20^20 ✢^1–22^50
10	9	8.9	230	*^0 18^50 21^30–24; V^0 0^00-50, 17^30–24; ≡^2 17^30–24; ≫ 0^50 4^50, 12^30 16^30 (por. 25) ⇘–18^30 (por. 25) ≫ ... 24 (por. 16); ✢^0 12^30 13^30 ✢^1-2 19^00 ✢^1-2 24; ⊕^0 11^15 12^15, ⊘ 13^45 14^10; () 4^50 16^30
11	7	5.4	236	*^0 0^00–24; V^0-1 0^00 23^20; ≡^2 0^00 11^40 ⩧–13^20 ≡^2–22^30 ⩧–23^20; ≫ 0^00 ... 8^30 (por. 16), 12^20 ... 23^20; ✢^0-1 0^00–24
12	9	0.7	240	*^0 0^00 2^40, 18^50–24; V^0 19^20–24; ≡^2 19^20–24; ✢^0 0^00 2^40; () 6^15 17^00
13	7	9.4	235	*^0 0^00 4^15, 6^05 7^30, 8^50 11^30 △^0 15^30 19^30 *^0 22^30 23^30; V^0 0^00 5^20, 6^30–24; ≡^2 0^00 5^20 ⩧–6^30 ≡^2–7^30 ⩧ ... 13^30 ≡^2–24; ≫ 7^30 18^15 (por. 23) ⇘–21^45 (por. 27) ≫–22^10 (por. 18) ⇘–24 (por. 24); ✢^1 7^30 24
14	4	4.1	240	*^0 0^30 10^30 ⩝^0 ... 24; V^0 0^00 10^15, 10^45 11^30, 19^30 21^40; ≡^2 0^00 10^15 ⩧–10^45 ≡^0–11^30 ⩧–16^30 ≡^2–21^40 ⩧–24; ⇘ 0^00-30 ≫–4^30 (por. 18), 7^30 12^40 (por. 23) ⇘–13^20 (por. 33) ≫–17^30 (por. 33), 18^10 19^05 (por. 23); ✢^1-2 0^30 17^30 ✢^1-0 23^30
15	7	1.0	245	⩝^0 0^00 2^30 ⩝^1–4^30 ⩝^0–5^40 ⩝^1-0 11^50; V^0 1^30 6^20 7^15 11^40; ⩧ 0^00 1^30 ≡^2–6^20 ⩧–7^15 ≡^2–10^20 ⩧–11^40 (m)–20^00; ⌓^1 18^30–24; () 23^30–24
16	1	7.7	243	⩝^0 10^05 15^30 ⩝^1–17^15 *^0–24; V^0 10^30–24; ⩧ 8^45 10^30 ≡^2–24; ≫ 15^40–24 (por. 16); ✢^0 11^30–24; ⌓^1-2 0^00 4^30 ⊕ 8^30-45, ⊗^0-1 8^45 ... 10^30; () 0^00–8^45
17	1	10.7	250	*^0 0^00 15^00 *^0-1–24; V^0 0^00–24; ≡^2 0^00–24; ≫ 0^00 12^30, 13^30 22^30 (por. 17); ✢^0 0^00 2^00 ✢^1–24
18	0	5.5	265	*^0-1 0^00 8^30 △^0–9^40 * △^0–24; V^0-1 0^00–24; ≡^2 0^00–24, ≫ 3^20 22^40 (por. 21) ⇘–24 (por. 22); ✢^1 0^00–24
19	0	2.6	271	* △^0 0^00 9^30 *^0 ... 16^30 17^03–24; V^0 0^00–24; ≡^2 0^00 15^45 ⩧–18^30 ≡^2–24; ⇘ 0^00 4^30 (por. 22) ≫–10^30 (por. 18), 16^30–24; ✢^1 0^00 8^30 ✢^0–10^30 ✢^0-1 16^30–24
20	8	•	271	*^0 0^00 4^30 5^15; V^0 0^00 5^15; ≡^2 0^00 4^30 ⩧–5^15 (m) 16^00–24; ≫ 0^00-45; ✢^0-1 0^00 5^30
21	9	0.0	265	(m) 0^00 1^00 (m)–9^30, 16^30–24; () 8^30–24
22	0	7.8	261	*^0-1 6^25 21^30, 22^40–24; (m) 0^00 6^30 ≡^2–9^50 ⩧–10^30 ≡^2–21^30, 22^40–24; ≫ 16^15–20^00 (por. 17); ✢^0 12^30–15^30 ✢^1-0 ... 21^00; () 0^00–4^30
23	1	1.9	266	*^0 0^00 13^45 *^1 16^50 19^30 *^0–24; V^0 0^00 1^15, 3^30 13^30, 16^15–24; ≡^2 0^00-30 ⩧–1^15 ≡^2–6^20 ⩧–8^30 ≡^2–13^30 ⩧–16^15 ≡^2–24; ✢^0-1 1^20 ... 8^00
24	9	•	268	*^0 0^00 2^20; V^0 0^00 2^15; ≡^2 0^00 2^15 ⩧–3^30 (m)–6^00 (m)–9^30; ✢^0 14^45 19^05, 19^40 20^15, 21^40–24; () 9^30–24
25	7	5.3	260	*^0 7^30 9^30 * △^0–11^30 ⩝^0–17^30 *^0-1 21^30; ⩧ 6^35-50 ≡^2–7^10 ⩧–17^30 ≡^2–24; ≫ 5^40–24 (por. 20); ✢^0-1 0^00–24; () 0^00–6^20
26	8	0.4	268	*^0 3^30 4^50 * △^0 6^20 7^30; V^0 0^00 7^30, 23^30–24; ≡^2 0^00 7^30 ⩧–8^30, 22^30 23^30 ≡^2–24; ≫ 0^00–24 (por. 23); ✢^1-2 0^00 8^30 ✢^0-1–23^00 ✢^1-2–24; () 15^30–23^30
27	7	4.5	262	⩝^0 16^15 18^15, 20^10–24; V^0 0^00 6^50, 16^25 20^15, 22^30–24; ≡^2 0^00 6^10 ⩧ ... 13^35 ≡^2 16^25 20^15 ⩧–22^30 ≡^2–24; ≫ 0^00-50 (por. 23) ⇘–3^00 (por. 23) ≫–19^20 (por. 30), 20^10 22^10 ⇘–22^45 (por. 30) ≫–24 (por. 25); ✢^1-2 0^00 10^15, 20^50–24
28	9	•	250	⩝^0-1 0^00 6^20; V^0 0^00 7^10, 23^40–24; ≡^2 0^00 7^10 ⩧–8^30 ≡^2 23^40–24; ≫ 0^00 1^30 ⇘–4^30 (por. 26) ≫–7^30 (por. 22), 8^30 13^15 (por. 25), 19^30–24 (por. 22); ✢^1-2 0^00 7^30 ✢^0-1 16^30, 21^05–24; () 10^30 22^30
29				
30				
31				
Σ	–	155.4	–	

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Marzec – Mars 1965

DNI	CIŚNIENIE p = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	83.4	82.4	81.8	82.5	-15.3	-11.0	-8.0	-10.6	-7.4	-17.2	86	93	96	92	0.3	0.2	0.1	0.2	8	10*△≡	10*△≡	SSE21	SSE20	SSE16
2	75.2	75.4	73.9	74.8	-5.6	-3.2	-3.0	-3.7	-2.4	-8.0	97	97	99	98	0.1	0.1	0.0	0.1	10 ≡	10△≡	10*△≡	S 20	S 16	ESE12
3	71.2	73.5	75.9	73.5	-5.2	-8.2	-10.3	-8.5	-1.8	-10.4	98	98	97	98	0.1	0.1	0.1	0.1	10 * ≡	10 * ≡	9	S 14	SSW18	SE 7
4	77.1	78.5	80.2	78.6	-15.2	-14.3	-14.8	-14.8	-10.3	-16.4	82	91	91	88	0.3	0.2	0.2	0.2	1	9	9	S 11	S 12	S 16
5	81.9	84.5	87.1	84.5	-11.3	-8.4	-7.7	-8.8	-7.4	-14.9	90	92	93	92	0.3	0.3	0.2	0.3	9	8	10*△≡	SSW15	S 8	S 8
6	87.3	87.9	90.8	88.7	-6.2	-5.1	-8.1	-6.9	-4.8	-8.4	94	95	92	94	0.2	0.2	0.2	0.2	10*△≡	10*≡	10 ≡	ESE 9	SSE 6	S 4
7	92.1	93.8	94.2	93.4	-10.3	-5.0	-11.0	-9.3	-4.4	-11.2	94	100	93	96	0.2	0.0	0.2	0.1	9	10 ≡	10 ≡	C 0	S 1	NE 7
8	93.1	92.7	92.9	92.9	-10.3	-8.7	-13.3	-11.4	-7.0	-13.4	94	95	80	90	0.2	0.2	0.4	0.3	10 *	10*△	8 *	NNE 3	NE 1	NE 3
9	93.1	94.0	94.6	93.9	-12.7	-8.5	-16.1	-15.4	-7.2	-16.3	92	83	67	81	0.2	0.5	0.6	0.4	10 * ≡	10 ≡	0	N 3	NNE 2	NNE 4
10	95.3	98.6	101.4	98.4	-15.1	-12.2	-11.6	-12.6	-8.7	-17.0	91	82	37	70	0.2	0.4	1.6	0.7	10 * ≡	1	0	N 8	NE 7	N 5
11	102.3	103.6	103.6	103.2	-9.1	-6.5	-5.0	-6.4	-4.9	-12.2	14	36	11	20	2.6	2.4	3.7	2.9	0	0	0	NNW 3	SSW 3	SW 5
12	102.6	102.0	101.2	101.9	-4.9	-4.1	-5.7	-4.1	-3.6	-5.4	8	32	11	17	3.9	3.1	4.2	3.7	0	0	6	SSW 6	S 6	S 6
13	99.8	100.6	100.8	100.4	-2.7	-5.5	-6.1	-5.1	-1.9	-8.5	9	57	38	35	4.6	1.7	2.4	2.9	2	1	0	SE 4	S 10	ESE 5
14	99.1	100.1	100.3	99.8	-7.1	-6.0	-7.0	-6.8	-5.3	-9.6	96	100	91	96	0.1	0.0	0.3	0.1	8	7	0	S 18	SSE15	S 15
15	101.2	101.6	101.5	101.4	-3.2	-2.7	-3.7	-3.3	-2.1	-7.0	54	93	92	80	2.2	0.4	0.4	1.0	8	7	3	SSW 5	SSE 9	S 8
16	99.2	97.5	96.9	97.9	-3.7	-2.8	-2.7	-3.0	-2.4	-4.6	97	95	82	91	0.2	0.2	0.9	0.4	9	9	9	SE 10	S 13	S 6
17	94.6	93.2	91.4	93.1	-2.7	-2.6	-4.8	-3.7	-1.5	-5.0	97	98	91	95	0.1	0.1	0.4	0.2	10*△≡	10*≡	10	S 3	SSW 1	SW 1
18	89.5	89.4	88.7	89.2	-5.6	-4.1	-2.4	-3.6	-0.3	-7.0	64	91	34	63	1.4	0.4	3.4	1.7	2	5	1	SW 2	SSE 7	S 5
19	87.9	90.7	92.8	90.5	-4.2	-1.1	-2.3	-2.6	0.5	-4.9	94	87	100	94	0.3	0.8	0.0	0.4	5	5	9	SSE12	SSE 5	WNW 2
20	93.5	94.3	94.1	94.0	-4.3	-3.2	-6.1	-4.9	-2.3	-6.2	98	99	97	98	0.1	0.0	0.1	0.1	10 * ≡	10△≡	2	C 0	SSW 2	WSW 7
21	91.5	88.3	86.7	88.8	-5.1	-4.7	-2.9	-3.9	-2.7	-6.1	63	96	97	85	1.5	0.2	0.1	0.6	10	9	10*△≡	S 12	SSW18	S 16
22	87.4	88.9	89.7	88.7	-4.2	-6.1	-13.1	-9.1	-2.2	-13.7	96	97	46	80	0.2	0.1	1.2	0.5	9	10 ≡	1	W 5	W 5	NE 6
23	89.7	89.2	86.2	88.4	-4.4	-5.8	-5.6	-5.4	-3.8	-13.1	14	59	95	56	3.8	1.6	0.2	1.9	0	4	6	WSW 2	S 10	SSE15
24	85.2	85.5	86.4	85.7	-4.4	-2.8	-5.6	-5.6	-2.4	-6.1	98	97	97	97	0.1	0.1	0.2	0.1	10*△≡	10*△≡	10△≡	S 9	SSE 6	N 4
25	88.6	91.3	92.9	90.9	-4.1	-5.8	-6.3	-5.6	-3.0	-6.9	96	97	91	95	0.2	0.1	0.3	0.2	10*△≡	9	9	NW 8	WSW 7	SSE 6
26	93.1	92.2	91.5	92.3	-6.6	-6.1	-5.9	-6.1	-5.3	-6.9	94	94	97	95	0.2	0.2	0.1	0.2	10*≡	6	10*△≡	NW 3	S 8	SSE 8
27	94.8	98.3	102.4	98.5	-6.6	-5.9	-7.4	-6.8	-5.1	-7.8	97	97	96	97	0.1	0.1	0.1	0.1	10*△≡	10*△≡	10△≡	N 3	N 6	N 9
28	104.8	105.9	105.9	105.5	-8.1	-5.1	-5.4	-5.5	-2.9	-8.5	95	74	65	78	0.2	1.2	1.4	0.9	7	3	9	NE 4	SW 2	N 5
29	104.8	105.3	104.6	104.9	-3.6	-1.7	-2.1	-2.4	-1.3	-6.3	99	98	98	98	0.1	0.1	0.1	0.1	10△≡	10 ● ≡	10 ● ≡	N 5	N 8	N 10
30	102.2	100.8	97.8	100.3	-1.2	-0.3	-3.8	-2.3	-0.1	-3.8	99	100	99	99	0.1	0.0	0.1	0.1	10 ≡	9	10 ≡	N 8	N 4	N 8
31	97.1	97.7	95.6	96.8	-11.7	-9.1	-8.8	-9.6	-3.8	-13.7	61	95	95	84	1.0	0.2	0.2	0.5	2	10*≡	10*≡	N 12	N 8	N 12
M	92.2	92.8	93.0	92.7	-6.9	-5.6	-6.9	-6.6	-3.8	-9.6	79	88	80	82	0.8	0.5	0.8	0.7	7.4	7.5	6.8	7.7	7.8	7.7

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1	96.1	99.0	100.1	98.4	-13.8	-10.4	-11.9	-12.0	-8.8	-14.1	96	94	93	94	0.1	0.2	0.2	0.2	10 * ≡	10*≡	10 ≡	N 11	NNE 9	N 9
2	98.9	99.2	99.7	99.3	-9.5	-6.2	-5.8	-6.8	-5.3	-14.0	94	89	100	94	0.2	0.4	0.0	0.2	10 ≡	6	10 ≡	N 7	NNW10	NNW11
3	97.8	98.0	98.4	97.4	-6.7	-3.8	-5.0	-4.1	-1.4	-8.0	91	53	70	71	0.3	2.2	1.5	1.3	2	1	2	NNE 7	NW 10	NNW12
4	94.3	94.7	94.0	94.3	-4.8	-1.6	-1.2	-2.2	-0.4	-6.0	83	63	65	70	0.7	2.0	2.0	1.6	8	5	8	N 7	N 5	WNW 7
5	92.4	93.3	96.2	94.6	-4.7	-2.3	-3.2	-3.4	-0.9	-7.2	98	63	63	73	0.1	1.8	1.8	1.2	10 ≡	1	1	N 7	NNE 2	SW 5
6	96.5	97.1	95.8	96.5	-4.2	-0.8	-1.6	-2.0	0.6	-5.0	70	64	77	70	1.3	2.0	1.2	1.5	2	1	0	NNW 5	SSW 2	SSW 7
7	94.6	95.3	94.7	94.9	-0.8	1.1	-0.5	-0.2	1.5	-2.1	95	73	100	89	0.3	1.8	0.0	0.7	4	9	10 ≡	S 8	SSW 8	SSW 6
8	92.8	92.8	92.3	92.6	-0.9	-0.7	-0.4	-0.6	0.9	-1.5	99	99	100	99	0.0	0.0	0.0	0.0	9	10	10	SSW 7	SSE 8	SSE 5
9	90.3	88.9	87.5	88.9	-0.1	1.0	1.0	0.7	2.2	-1.0	100	94	73	89	0.0	0.4	1.9	0.8	10	10	10	SE 3	NNE 5	S 3
10	86.5	87.3	88.1	87.3	-3.0	-1.9	-2.0	-2.2	1.1	-4.9	99	94	98	97	0.0	0.3	0.1	0.1	10	10	9	NNE 5	SE 1	SE 3
11	88.6	90.0	91.1	89.9	-1.5	-0.2	-1.1	-1.0	0.0	-2.7	99	100	99	99	0.1	0.0	0.1	0.1	9 *	10	7	SE 5	SE 3	SE 3
12	91.8	92.8	92.9	92.5	-3.7	-2.8	-3.0	-3.1	-1.1	-4.0	99	100	99	99	0.1	0.0	0.0	0.0	10	10 ≡	10*≡	SSE 3	SW 4	C 0
13	91.0	90.6	90.8	90.8	-3.9	-3.6	-4.0	-3.9	-2.8	-4.7	99	99	99	99	0.1	0.1	0.1	0.1	10 * ≡	10△≡	10 ≡	S 1	SSW 4	C 0
14	91.4	93.9	94.9	93.4	-3.8	-2.7	-4.7	-4.0	-2.5	-5.0	99	100	98	99	0.1	0.0	0.1	0.1	10*△≡	10△≡	10△≡	N 4	N 3	N 4
15	94.1	94.5	93.5	94.0	-7.6	-2.9	-4.5	-4.9	-2.6	-9.6	96	95	98	96	0.1	0.2	0.1	0.1	4	7	10 ≡	NNE 3	SSW 4	S 5
16	91.3	91.2	90.8	91.1	-5.2	-3.1	-5.0	-4.6	-2.8	-5.8	98	97	93	96	0.1	0.1	0.3	0.2	5	9 ✱	5	S 5	SSE 5	SSE 1
17	91.4	92.4	89.7	91.2	-4.2	-0.7	-2.8	-2.6	-0.6	-5.6	89	97	100	95	0.5	0.2	0.0	0.2	10	8	10 ≡	S 1	N 1	S 7
18	83.6	83.5	85.2	84.1	-5.4	-4.7	-3.2	-4.1	-2.7	-6.1	77	98	97	91	0.9	0.1	0.1	0.4	10	10*≡	10	S 11	S 14	C 0
19	83.3	83.4	82.3	83.0	-3.3	-1.2	-2.4	-2.3	-0.6	-4.8	99	99	98	99	0.0	0.1	0.1	0.1	10*≡	10 *	10*≡	S 7	S 4	SSE 6
20	81.5	82.5	83.4	82.5	-2.1	-1.1	-3.3	-2.4	-0.8	-3.6	100	99	97	99	0.0	0.1	0.1	0.1	10 *	10*✱≡	6	SE 11	S 7	SSE 8
21	82.0	81.2	78.7	80.6	-2.7	-0.2	-2.1	-1.8	0.5	-4.2	97	96	100	98	0.1	0.2	0.0	0.1	9 *	8	10 ● ≡	NE 4	NNE 1	N 6
22	76.5	77.1	78.4	77.3	-3.6	-3.0	-5.2	-4.8	-1.9	-5.6	99	98	98	98	0.1	0.1	0.1	0.1	10 * ≡	10*△≡	10△≡	N 3	SW 4	C 0
23	78.3	79.3	81.6	79.7	-6.3	-5.6	-5.9	-5.9	-5.1	-6.8	97	100	97	98	0.1	0.0	0.1	0.1	10△≡	9 *	10 ≡	WNW 6	W 6	WNW 7
24	82.6	84.8	87.7	85.0	-6.1	-5.3	-6.0	-5.9	-4.2	-7.1	97	97	92	95	0.1	0.1	0.3	0.2	9 △	9 *	5	WSW 7	W 7	W 7
25	89.5	91.1	91.3	90.7	-4.9	-3.5	-3.8	-4.0	-2.8	-6.6	90	99	99	96	0.4	0.0	0.1	0.2	9	6	3	SSW 5	S 11	SSW 9
26	89.5	89.9	88.3	89.2	-3.5	-2.3	-5.7	-4.3	-2.3	-5.9	99	98	97	98	0.0	0.1	0.1	0.1	10 * ≡	10△≡	10△≡	SSW11	S 7	NW 1
27	84.5	84.9	85.1	84.8	-5.9	-2.2	-3.6	-3.8	-1.3	-6.6	97	94	97	96	0.1	0.3	0.2	0.2	3	7	3	NNW 1	SSE 4	SSE 3
28	82.4	82.9	86.7	84.0	-2.4	-4.1	-6.0	-4.6	-2.2	-6.2	100	98	97	98	0.0	0.1	0.1	0.1	10*△≡	9 ✱	3	SE 6	S 11	S 10
29	88.3	89.2	91.0	89.5	-4.1	-1.1	-3.1	-2.8	-0.1	-6.9	96	85	99	93	0.2	0.9	0.0	0.4	8	8	10✱≡	S 1	NNE 1	N 5
30	92.5	94.2	95.4	94.0	-4.1	-3.1	-5.6	-5.6	-2.5	-5.2	98	99	99	99	0.1	0.0	0.1	0.1	9	8	10 ≡	N 5	N 4	N 4
31																								
M	89.1	89.9	90.1	89.7	-4.4	-2.7	-3.6	-3.6	-1.6	-5.9	95	91	93	93	0.2	0.3	0.4	0.4	8.3	8.0	7.7	5.6	5.4	5.1

Kasprowy Wierch $H_s = 1991\ m$ $H_b = 1988{,}8\ m$ $h_w = 15{,}4\ m$ **Marzec – Mars 1965**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	1	6.6	240	[illegible]
2	0	26.1	245	[illegible]
3	1	5.1	250	[illegible]
4	8	1.0	255	[illegible]
5	8	3.2	252	[illegible]
6	0	6.2	255	[illegible]
7	1	0.4	240	[illegible]
8	5	2.3	240	[illegible]
9	0	0.8	241	[illegible]; zielony promień 17.37 (zielono-niebieski); () 16.50–23.40
10	9	0.5	259	[illegible]; zielony promień 17.35 (fioletowy); () 11.30–24
11	9	•	240	zielony promień 17.40 (niebieski); () 0.00–24
12	9	•	255	[illegible]; () 0.00–17.00
13	9	•	255	[illegible]; zielony promień 17.39 (niebieski); () 5.40–22.30
14	8	0.3	251	[illegible]
15	9	•	225	[illegible]
16	8	2.5	225	[illegible]
17	1	9.8	225	[illegible]
18	9	•	252	[illegible]; () 8.30–9.30
19	8	0.4	250	[illegible]
20	0	1.6	228	[illegible]
21	8	6.4	229	[illegible]
22	0	0.4	252	[illegible]; () 16.30–24
23	9	5.0	253	[illegible]; () 0.00–14.30
24	0	14.0	255	[illegible]
25	8	2.9	247	[illegible]
26	8	7.5	248	[illegible]
27	0	26.0	255	[illegible]
28	9	0.0	272	[illegible]; () 10.00–11.30, 12.10–15.30
29	0	13.4	270	[illegible]
30	7	0.6	257	[illegible]
31	0	18.4	245	[illegible]; () 4.30–9.30
Σ	–	161.2	–	

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	POGODA
1	0	3.3	265	[illegible]
2	7	1.2	267	[illegible]
3	8	•	260	[illegible]
4	7	•	255	[illegible]
5	8	•	247	[illegible]
6	8	•	241	
7	8	0.7	253	[illegible]
8	6	1.6	227	[illegible]
9	7	0.6	222	[illegible]
10	7	0.2	220	[illegible]
11	5	0.5	215	[illegible]
12	0	2.1	209	[illegible]
13	0	5.9	210	[illegible]
14	0	8.0	212	[illegible]
15	8	0.1	214	[illegible]; () 5.30–12.30
16	7	0.1	212	[illegible]
17	7	1.7	212	[illegible]
18	1	3.0	210	[illegible]
19	5	20.8	210	[illegible]
20	1	7.2	225	[illegible]
21	8	18.1	227	[illegible]
22	0	25.7	255	[illegible]
23	7	1.5	248	[illegible]
24	8	0.8	249	[illegible]
25	8	7.7	246	[illegible]
26	0	14.2	248	[illegible]
27	8	1.8	255	[illegible]
28	7	14.0	252	[illegible]
29	9	2.5	260	[illegible]
30	7	2.5	258	[illegible]
31				
Σ	–	143.8	–	

Kasprowy Wierch $\varphi = 49°14'$ $\lambda = 19°59'$ *Maj – Mai 1965*

Dni	Ciśnienie P = 700 +				Temperatura T						Wilgotność wzgl. U				Niedosyt wilgotności Δ				Zachmurzenie i pogoda N,w			Kierunek i prędkość wiatru D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.2	95.8	95.1	95.4	-4.2	-3.9	-4.6	-4.3	-3.4	-6.5	98	96	98	97	0.1	0.2	0.1	0.1	10 * △̽ ≡	10 △̽ ≡	9	N 5	NNW 7	S 7
2	94.1	95.3	94.3	94.6	-9.6	-5.5	-8.4	-8.0	-4.4	<u>-10.4</u>	63	67	95	75	1.1	1.3	0.2	0.9	7	8	7	N 8	N 5	NNE 3
3	92.1	93.7	94.5	93.4	-8.3	-5.2	-8.7	-7.7	-4.7	-9.1	50	70	92	64	2.0	1.2	0.3	1.2	0	3	0	NNE 6	NNW 3	NNE 3
4	94.9	96.1	93.8	94.9	-6.4	-2.2	-2.2	-3.2	-0.4	-10.0	<u>21</u>	64	62	49	3.0	1.9	2.0	2.3	0	1	7	N 3	S 4	S 7
5	89.4	87.6	87.4	88.1	-4.0	-2.8	-1.5	-2.4	-1.3	-4.8	96	100	99	98	0.2	0.0	0.1	0.1	10	10 * △ ≡	10 △ ≡	SSE 12	SSW 8	N 4
6	86.8	88.4	90.7	88.6	-2.2	-1.3	-2.0	-1.9	-0.8	-2.8	100	99	98	99	0.0	0.1	0.1	0.1	10 * ≡	10 △ ≡	10 △ ≡	N 5	N 7	N 9
7	92.4	94.3	95.6	94.1	-4.0	-1.6	-4.3	-3.6	-1.5	-4.4	99	98	96	98	0.1	0.1	0.2	0.1	10 ≡	10 ≡	1	N 8	NNW 4	N 3
8	94.7	95.4	97.8	96.0	-2.4	0.1	-0.8	-1.0	0.1	-4.8	100	96	99	98	0.0	0.3	0.0	0.1	10	10	10 △ ≡	WSW 3	WSW 3	N 5
9	97.5	96.4	90.2	94.7	-1.2	0.6	1.3	0.5	1.7	-1.5	99	100	100	100	0.1	0.0	0.0	0.0	10 ≡	10 ●	9	NW 4	WSW 6	S 15
10	87.2	86.8	86.0	86.7	-4.9	-3.6	-4.9	-4.6	1.3	-5.2	98	99	98	98	0.1	0.1	0.1	0.1	8	8	10	NW 11	WSW 8	W 9
11	<u>84.3</u>	87.0	91.6	87.6	-4.6	-2.4	-3.9	-3.7	-0.7	-5.7	98	100	99	99	0.1	0.0	0.1	0.1	10 * △ ≡	10 * ≡	10 * ≡	SSW 3	N 3	NNW 7
12	95.3	98.3	99.4	97.7	-2.7	-1.0	-2.2	-2.0	-0.5	-4.6	100	99	100	100	0.0	0.1	0.0	0.0	10 △̽ ≡	10 △̽ ≡	10 ≡	NNW 10	N 16	N 9
13	99.1	100.4	100.0	99.8	-5.8	-1.8	-1.7	-2.8	-0.7	-5.9	100	98	98	99	0.0	0.1	0.1	0.1	7	5	10	NNE 12	N 8	N 11
14	97.0	96.7	95.5	96.4	-2.4	-1.0	-0.8	-1.2	-0.5	-2.8	100	99	99	99	0.0	0.1	0.0	0.0	10 ≡	9 *	10 ≡	N 6	N 5	N 6
15	94.3	95.5	95.9	95.2	-0.5	0.5	1.8	0.9	2.0	-1.1	100	100	98	99	0.0	0.0	0.2	0.1	10 ≡	9	8	N 6	WNW 4	NW 3
16	94.6	95.2	95.3	95.0	3.7	3.8	3.3	3.5	5.0	1.8	95	100	86	94	0.4	0.0	1.1	0.5	9	9	10 ●	WSW 7	WNW 9	WSW 7
17	95.5	97.1	96.2	96.3	3.5	6.5	5.8	5.4	7.6	2.5	88	71	88	82	0.8	2.8	1.1	1.6	8	8	9	WNW 5	W 6	S 10
18	95.8	96.2	95.7	95.9	7.1	7.8	6.3	6.9	<u>8.9</u>	5.2	70	81	87	79	3.1	2.0	1.2	2.1	6	7	4	W 12	SSW 8	S 8
19	91.3	90.1	92.6	91.3	7.1	7.7	5.2	6.3	8.6	4.9	71	66	88	75	2.9	3.6	1.0	2.5	5	8	7	S 20	SSW 18	SSW 11
20	92.8	95.6	99.5	96.0	-5.4	-5.8	-6.3	-6.0	5.5	-7.2	98	97	97	97	0.1	0.1	0.1	0.1	10 ≡	10 △ ≡	6	SW 1	N 6	N 5
21	102.4	104.2	<u>104.9</u>	103.8	-6.0	-2.4	-3.3	-3.8	-1.4	-7.4	94	96	97	96	0.2	0.2	0.1	0.2	8	8	8	NNE 2	C 0	ENE 1
22	104.5	104.0	101.8	103.4	0.9	1.2	4.7	2.9	5.5	-3.9	26	80	87	64	<u>4.8</u>	1.3	1.0	2.4	9	9	9 ●	C 0	S 2	SE 5
23	99.0	98.7	98.8	98.8	5.0	3.9	3.3	3.9	6.1	2.6	96	94	100	97	0.3	0.5	0.0	0.3	10 ●	9	9	SE 6	SE 8	SE 5
24	98.1	98.6	99.0	98.6	2.5	2.0	2.0	2.1	3.3	0.9	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	9	10 ≡	S 6	S 10	SSW 11
25	99.2	99.9	99.6	99.6	1.0	2.3	1.6	1.6	2.5	0.7	98	94	100	97	0.2	0.4	0.0	0.2	9	10	10 ● ≡	WSW 6	WSW 6	NW 9
26	99.2	100.3	99.9	99.8	0.8	2.5	0.9	1.3	3.7	-0.1	100	89	96	95	0.0	0.8	0.2	0.3	9	9	6	NE 4	NW 7	W 9
27	98.1	98.4	96.8	97.8	0.2	3.5	2.1	2.0	4.4	-0.3	83	67	96	82	1.1	2.6	0.3	1.3	8	10	10 ●	SW 3	SW 5	SE 4
28	94.6	93.9	91.8	93.4	2.5	2.6	0.5	1.5	5.0	0.4	100	100	98	99	0.0	0.0	0.1	0.0	10 ≡	10 ●	10 *̇	S 6	SSE 5	S 9
29	88.4	88.6	88.7	88.6	1.4	1.5	0.3	0.9	2.4	-0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10	10	S 11	SSE 12	S 9
30	88.2	90.4	91.9	90.2	-2.3	-2.6	-1.1	-1.8	0.3	-3.0	98	100	99	99	0.1	0.0	0.1	0.1	10 △ ≡	10 ≡	10 ≡	N 6	NE 4	SSW 7
31	92.5	94.0	92.4	93.0	-0.3	1.0	3.7	2.0	3.9	-1.7	98	100	100	99	0.2	0.0	0.0	0.1	9	10 ● ≡	10 ≡	S 9	SE 7	SE 9
M	94.5	95.3	95.2	95.0	-1.3	0.1	-0.4	-0.5	1.9	-2.7	88	91	95	91	0.7	0.6	0.3	0.5	8.5	8.7	8.4	6.6	6.6	7.1

Czerwiec – Juin

Dni	Ciśnienie P = 700 +				Temperatura T						Wilgotność wzgl. U				Niedosyt wilgotności Δ				Zachmurzenie i pogoda N,w			Kierunek i prędkość wiatru D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	90.2	92.2	95.3	92.6	2.5	3.7	2.1	2.6	5.0	2.0	80	77	100	86	1.5	1.8	0.0	1.1	4	9	9	SE 16	SSW 20	S 9
2	95.3	97.7	99.1	97.4	0.5	3.3	-1.5	0.2	4.4	-1.5	92	77	99	89	0.5	1.7	0.1	0.8	1	6	8	SSE 11	NNE 3	W 8
3	100.4	101.7	101.3	101.1	-0.2	4.2	1.8	1.9	5.4	<u>-2.5</u>	75	73	98	82	1.5	2.2	0.2	1.3	1	9	10 ● ≡	N 1	N 2	SSE 5
4	100.2	100.2	99.1	99.8	3.8	4.1	5.2	4.6	6.6	0.9	76	100	100	92	1.9	0.0	0.0	0.6	9	10 ●	10 ●	SSE 3	S 6	SSE 6
5	95.9	93.4	91.9	93.7	7.9	7.0	5.5	6.5	10.0	4.0	64	97	100	87	3.8	0.3	0.0	1.4	10	10	9	S 4	SE 3	SE 5
6	89.3	89.0	90.0	89.4	5.7	6.9	3.3	4.8	7.1	3.1	98	100	100	99	0.2	0.0	0.0	0.1	9	9 ●	10 ● ≡	NE 3	N 1	N 4
7	92.0	94.5	95.8	94.1	0.7	3.0	2.7	2.3	4.2	0.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	N 7	N 2	S 9
8	96.6	97.3	96.6	96.8	3.1	5.1	4.3	4.2	7.0	1.7	100	95	100	98	0.0	0.5	0.0	0.2	10 ≡	6	9	SSE 11	SSW 10	SSE 5
9	93.0	90.6	90.8	91.5	3.9	2.1	0.9	2.0	6.3	0.8	89	100	96	95	0.9	0.0	0.2	0.4	5	10	7	ESE 4	SE 10	SE 9
10	90.8	91.8	90.2	90.9	0.4	2.6	1.5	1.5	4.4	-0.4	100	96	100	99	0.0	0.3	0.0	0.1	10 * ≡	9	10 *̇ ≡	SSW 4	S 7	NNE 11
11	<u>85.8</u>	87.8	88.1	87.2	1.0	1.3	2.6	1.9	2.7	-0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 *̇ ≡	10 ● ≡	N 8	N 9	N 13
12	91.7	94.6	97.2	94.5	0.8	2.0	1.5	1.4	2.7	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ● ≡	10 ● ≡	10 ● ≡	NNE 14	N 10	NNW 10
13	97.5	98.6	97.9	98.0	-0.3	4.0	2.3	2.1	4.8	-1.1	100	67	98	88	0.0	2.6	0.1	0.9	9	6	10	NW 4	WNW 7	WSW 7
14	96.5	97.3	97.6	97.1	0.3	0.1	2.6	1.4	2.6	-0.7	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ● ≡	N 7	NNW 7	N 16
15	100.0	101.2	101.1	100.8	0.2	5.0	2.8	2.7	6.4	-1.6	67	81	92	80	2.1	1.6	0.6	1.4	3	8	1	N 12	N 5	NNE 6
16	101.5	102.2	99.9	101.2	4.3	8.4	5.4	5.9	10.6	1.7	51	72	95	73	4.1	3.2	0.5	2.6	0	6	5	C 0	C 0	SSE 6
17	94.0	93.6	93.5	93.7	3.7	7.2	3.7	4.6	8.9	3.5	84	83	100	89	1.3	1.8	0.0	1.0	2	9	10 ● ≡	SSW 18	SW 12	S 7
18	97.3	100.0	101.5	99.6	0.1	3.6	2.8	2.3	5.3	-0.1	100	100	96	99	0.0	0.0	0.3	0.1	10 △ ≡	10 ≡	9	N 9	WSW 1	W 4
19	101.3	102.1	103.1	102.2	6.4	8.0	4.6	5.9	9.4	2.6	78	67	75	73	2.1	3.6	2.2	2.6	8	8	4	WSW 7	WSW 13	WNW 11
20	104.0	105.3	105.2	104.8	2.0	6.7	5.5	4.9	9.7	1.2	100	69	82	84	0.0	3.0	1.6	1.5	9	8	6	NW 6	W 6	WSW 1
21	104.9	105.5	103.9	104.8	5.5	9.5	7.9	7.7	11.3	4.0	72	69	91	77	2.4	3.6	0.9	2.3	1	9	9	NNE 4	W 2	S 7
22	101.8	102.8	101.3	102.0	7.5	11.9	9.6	9.6	14.9	6.6	94	71	100	88	0.7	4.0	0.0	1.6	3	7	9	S 10	SW 7	S 10
23	101.0	102.5	103.8	102.4	8.6	11.3	8.7	9.3	13.4	7.7	100	84	74	86	0.0	2.3	3.0	1.8	10	8	2	SSW 10	SW 2	NW 5
24	104.5	106.2	106.8	105.8	8.8	13.6	10.5	10.8	14.7	7.3	87	57	77	74	1.5	6.6	2.9	3.7	8	8	2	W 4	NW 5	WSW 5
25	106.9	107.9	108.0	107.6	9.3	14.0	11.5	11.6	16.4	9.2	94	54	77	75	0.7	7.4	3.2	3.8	9	5	4	NW 4	W 5	SSW 3
26	107.6	108.4	<u>108.6</u>	108.2	12.2	17.1	13.5	14.1	<u>19.9</u>	10.8	81	56	86	74	2.7	8.6	2.1	4.5	4	4	10 (K)	WNW 4	C 0	NW 3
27	108.4	108.4	107.1	108.0	13.7	14.3	10.4	12.2	16.1	9.4	49	78	86	71	8.1	3.7	1.6	4.5	8	8	10 (K)	C 0	N 2	NE 4
28	104.9	105.1	104.3	104.8	8.2	1.5	0.9	2.9	11.8	0.2	100	100	100	100	0.0	0.0	0.0	0.0	10	10 ● ≡	10 ● ≡	W 3	N 12	N 15
29	103.6	105.2	105.9	104.9	-0.1	8.5	4.9	4.6	10.2	-1.0	96	61	100	86	0.3	4.2	0.0	1.5	8	1	10 ≡	NNE 7	N 7	N 5
30	105.4	105.9	103.6	105.0	9.1	12.3	8.3	9.5	14.0	3.3	<u>26</u>	74	97	66	<u>8.7</u>	3.8	0.4	4.3	0	1	4	C 0	NW 3	S 11
31																								
M	98.7	99.6	99.6	99.3	4.3	6.8	4.9	5.2	8.9	2.4	85	82	94	87	1.5	2.2	0.7	1.5	6.7	7.8	7.9	6.5	6.0	7.3

Kasprowy Wierch $H_s = 1991$ m $H_b = 1988{,}8$ m $h_w = 15{,}4$ m — Maj - Mai 1965

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	0	6.1	260	[snow, snow shower, hail, thunderstorm, thunder, fog, drifting snow and blowing snow entries; times 5:50 to 24]
2	9	•	265	V 0:30 3:35; [fog] 0:30–40 … 20:30, 22:30; [drifting snow] 0 … 9:30; [solar halo] 7:30 11:30; () 3:20 15:30
3	9	•	260	[fog] 7:30 8:30; () 4:30 15:30
4	9	1.0	255	[snow] 23:45 24; [wind] 23:25 24 (por. 14); () 5:30 16:00
5	0	22.9	250	[snow, snow pellets, glaze and fog entries; times 0:00 to 24]; [wind] 0:00 12:10 (por. 21); [drifting snow] 7:00 14:30
6	0	55.8	264	[snow pellets, snow and glaze entries; times 0:00 to 24]; [fog] 0:00 24; [blowing snow] 4:30 5:10
7	0	1.2	285	[snow pellets] 0:00 1:30, 8:30 9:30, 11:10 12:15, 15:45 16:50; V 0:00 12:00, 17:30 19:40; [fog] 0:00 19:40 –20:10 [9.V: (por. 23), 19:30 23:30 (por. 24); [drifting snow] 23:20 24; [blowing snow] 19:40 20:15, 21:20–23:05]
8	6	2.5	280	[snow-shower, snow pellet, rime and fog entries; times 13:30 to 24]
9	8	7.9	281	[snow, rain and snow-shower entries; times 11:00 to 24]; [wind] 17:10 18:30
10	8	3.7	275	[snow-shower and fog entries; times 0:00 to 24]; [wind] 0:30 9:30 (por. 18), 15:40 20:30 (por. 19)
11	0	15.5	278	[snow-shower, snow pellet and fog entries; times 0:00 to 24]; [drifting snow] 0:20 1:30; [blowing snow] 16:40 17:30 [10.V: [drifting snow] 0:00 23:30]
12	0	11.9	284	[snow-shower entries 0:00 to 19:30]; V 10:00 … 24; [fog] 0:00 24; [wind entries] (por. 16), (por. 23), (por. 16), (por. 24); [drifting snow] 8:30 11:30
13	8	•	287	[snow shower] 1:20 3:30; V 0:00 3:30, 19:45 21:40; [fog] 0:00 3:30, 19:45 21:40; [wind] 0:00 1:30 (por. 20), … 7:50 (por. 18), 17:40 24; () 5:30 7:30
14	7	5.6	282	[snow shower] 12:25–45, 13:30 14:20; [snow pellets] 21:30 24; V 3:30 9:40, 17:30 24; [fog] 3:30–50 … 13:10–15 … 24; [wind] 0:00 1:15
15	7	0.2	285	[snow pellets] 0:00–30, 1:30 2:20; V 0:00 8:30; [fog] 0:00 11:15, 16:45 18:30
16	6	5.2	270	[rain-shower, hail and thunderstorm entries, 0:45 to 23:45]; (R) 7:15–30 NE, (R) NNE 14:25, NE 15:12, N 15:30, NW 15:50 16:00, R 16:10–22–30 E; [fog] 4:40 5:15, 7:10–25
17	8	•	260	[fog] 23:20–40 … 24; [wind] 0:00–30, 18:30 19:40, 20:05 24 (por. 23); [solar halo] 6:30 7:20, 12:30 17:30; () 3:30 5:30 [16.V: 11:03–30 [fog] 16:05–15; [wind] 9:15 11:45 (por. 15), 23:40 24]
18	8	•	245	[fog] 0:00 1:10 … 3:30; [wind] 0:00 7:30 (por. 25), 16:20 19:30, 21:10 22:10 (por. 23) … 24 (por. 29); [corona] 19:05–20; () 6:10 8:30
19	9	5.7	228	[rain shower] 16:55; [lightning] 19:45 20:15 WNW–N; [dew] na; [fog] 21:30 24; [wind] 0:00–40 (por. 28) –3:10 (por. 24) –19:15 (por. 50) –21:00 (por. 25); [rainbow] 18:00–10; () 16:30 10:00
20	0	4.2	200	[rain-shower, hail, snow-shower and snow entries, 0:54 to 15:47]; (R) 1:54 NE–E–R 2:31 2:33 3:00 E–S; V 6:00 15:10, 17:50 19:05, 21:30 22:30; [fog] 0:00 11:30
21	8	•	202	[dew] 20:00 24; [fog] 8:30–50, 10:20–50, 19:05–15 [20.V: [fog] –12:20 … –15:10 … –16:40, 17:04…50 … –18:30 … –19:05, 21:30 22:30; [wind] 2:08–15; [blowing snow] 1:50 4:00]
22	8	2.5	197	[rain] 20:20…45; [dew] 0:00 1:30; (m) 19:30 24; () 8:30 11:20
23	8	18.1	182	[rain and rain-shower entries, 5:10 to 24]; (R) 17:47 S; (m) 0:00 24; [fog] 4:20 6:20 9:45 10:05 … 23:15; [blowing snow] 17:00 18:30, 23:40 24
24	8	7.2	135	[rain-shower and snow-shower entries, 0:00 to 20:02]; (m) 0:00 na; [fog] 3:30 5:15 … –24; [wind] 9:10 13:30 (por. 18), 20:00 22:20
25	8	6.2	118	[rain-shower and rain entries, 12:45 to 24]; [fog] 0:00 4:30, 7:30 8:40 … 15:10–30 … 24 [24.V: [rainbow] 8:25–30; [blowing snow] 0:00 3:30, 9:45 10:30]
26	7	1.4	107	[rain and rain-shower entries, 0:00 to 17:10]; [lightning] 22:05 23:15 ESE; [fog and mist entries, 0:00 to 20:10]; [wind] 21:10…45
27	8	3.0	100	[rain shower] 16:50 19:10, 20:35 23:15; [fog] 18:15 19:25 … –22:30 … 24; [solar halo] 4:30 6:15 [28.V: 17:30 18:05 19:25 24; [wind] 20:00–20, 21:15 22:00 (por. 17); [blowing snow] 19:30–20:50]
28	6	8.7	95	[rain-shower and rain entries, 0:30 to 22:10]; (R) S 19:05, R S 19:37 NE 19:56 20:15; [lightning] NE 22:27, N 22:52 24; [fog and mist entries, 0:00 to 16:03…45]
29	7	8.6	90	[rain-shower and snow-shower entries, 3:30 to 23:15]; [fog] 0:00–20 … 18:40
30	0	1.4	88	[snow] 1:10 5:10; [snow pellets] 1:30; V 4:40 13:20, 20:30 24; [fog] 2:45 3:15 … 15:30 … 24; [wind] 22:10 24 [29.V: [fog] 18:50 … 23:10; [wind] 2:40 8:30 (por. 20), 11:40 19:50 (por. 23)]
31	1	12.9	87	[rain-shower and snow-shower entries, 10:50 to 22:25] 24; V 0:00 3:30, 4:40 5:20; [fog] 0:00 3:30 4:40 5:20 … 7:20 8:30 … 10:20 21:30 … 23:20 … 24; [wind] 0:00 3:30, 21:05 24 (por. 35)
Σ	–	217.4	–	

Czerwiec - Juin

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	9	2.4	80	[rain-shower entries, 7:00 to 22:20]; [fog] 0:00 2:30 … 3:15 6:30, 19:25–40 … 20:10 … 22:50 … 23:30 … 24; [wind] 0:00 1:30 (por. 40) –4:30 (por. 36) –6:30 (por. 32) –17:15 (por. 57) 21:30 (por. 28)
2	8	•	78	[fog] 0:00 1:30; (m) 3:30 4:30; [fog] 19:02–30; [wind] 0:00 4:15 (por. 19) –6:10 (por. 25) –7:10 (por. 15) [1.VI: 23:15 24 (por. 18); () 8:30 10:30]
3	9	1.0	77	[rain shower] 17:50 18:05, 18:40 19:30; [rain] 20:50; [fog] 19:45 22:30 … 23:20; () 3:30 13:30
4	7	18.5	75	[rain and rain-shower entries, 7:45 to 23:05]; R 21:22 22:15 23:00 N–NW, E (R) 23:30 N; [fog and mist entries, 9:00 to 22:00]; [blowing snow] 19:40 23:00
5	8	7.4	65	[rain-shower and rain entries, 0:31 to 19:05]; (R) 0:32 5:45 E–S; [fog and mist entries, 0:30 to 24]; [wind] 1:15–30; [blowing snow] 1:30 6:00
6	7	18.7	55	[rain and rain-shower entries, 0:15 to 24]; [fog] 0:00 2:30 (m) –4:30 (m) –7:30 … –24; [blowing snow] 13:15 14:20
7	0	1.1	48	[rain] 0:00 5:15, 8:30; [fog] 0:00 9:10 … 24; [wind] 23:10 24 [9.VI: 11:30 13:00 (por. 16), 14:20 15:30 (por. 20), 15:55 18:30 (por. 18), 20:25 22:00 (por. 19) –22:30 (por. 23) –24 (por. 20); 4:10 6:00; [rainbow] 18:00…20; () 5:00 8:30]
8	8	5.8	45	[rain shower] 7:15–25, 23:23 24; [fog] 0:00 1:40 … 8:30 9:30, 18:45 21:30; [lightning] 21:45 22:15 SW; [wind] 0:00 2:30, 3:30 13:40 (por. 18) [9.VI: [blowing snow] 10:30 1:15]
9	8	10.5	pł.	[rain-shower and hail entries, 0:00 to 12:55]; (R) 11:05, (R) 11:25, (R) 11:45 12:55 –N; [fog] 0:30 3:30 … 24; [wind] 0:30 6:10 (por. 30)
10	8	66.9	pł.	[rain-shower and snow entries, 6:07 to 24]; R 11:28 12:30 SSE; [fog and mist entries, 0:00 to 16:40–50]
11	0	48.5	11	[snow and rain entries, 0:00 to 24]; [fog] 0:00 24; [wind] 0:00 1:05, 6:50 7:10, 11:50 12:00 (por. 14), 16:45 18:50 22:40 (por. 23) –23:10 (por. 22) –24 (por. 22)
12	0	59.7	7	[snow, rain and snow pellet entries, 0:00 to 24]; [fog] 0:00 24; [wind] 0:00 23:30 (por. 22) [10.VI: [fog] –17:10 … –17:50, 18:50 19:15 … 24; [wind] 0:00 2:10 (por. 22), 19:40 20:05, 20:30 24 (por. 19); [blowing snow] 16:40 17:30, 20:50 21:30]
13	8	7.0	pł.	[rain] 0:00 3:15; [rain shower] 17:40 18:45; [fog] 0:00 6:25 –7:15, 8:55 9:02 … 17:10 19:15 … –21:30 … –22:30 … –23:15 … 24
14	0	22.6	pł.	[hail, rain-shower and rain entries, 2:55 to 24]; (R) NNE 3:26, (R) SE 9:33, R 9:32, R 10:30 E–NE; [fog] 0:00–30 … –3:05 … 13:45 … –14:05
15	8	•	pł.	[rain] 0:00–10, 2:30; [fog] 0:00 3:10 … –3:40, 11:05 12:20; [wind] 0:00 10:30 (por. 16); () 3:30 7:30 [14.VI: [fog] 24; [wind] 3:45 4:00, 17:40 19:30 –19:50 –20:30 –22:40 (por. 27) –24 (por. 25); [blowing snow] 3:10–35]
16	8	•	pł.	0:30 4:30; [wind] 21:15 24; () 3:30 10:00
17	8	46.1	pł.	[rain shower] 13:37 16:15, 16:45 17:10; [rain] 24; [fog] 13:40 14:50 … 15:15 … –17:20 … 18:20 … –19:45 … 24; [wind] 0:00 6:00 (por. 30) … 10:35 (por. 30) –11:45 (por. 23), 12:00 17:20 (por. 22), 18:30 20:15 (por. 19)
18	0	0.8	pł.	[rain, snow and snow pellet entries, 0:00 to 9:05]; [fog] 0:00–30 … –1:15 … 10:35 … –10:45, 11:10–40 … 13:15 … –15:10 … 16:20 … –16:45; [wind] 3:35 4:40
19	8	2.5	pł.	[rain shower] 13:57 15:10, 15:30 16:15; [fog] 23:40–24; [wind] 2:40 5:45 (por. 18), 9:20 14:10 (por. 23) … 19:30 (por. 31) –23:30 (por. 22); [rainbow] 16:55 17:10; () 15:30 20:30
20	8	•	pł.	[fog] 0:00–30, 3:30 5:20 … 6:10…40; [lightning] 22:40–23:30 SW
21	8	•	pł.	[dew] 3:30–5:00, 22:30–24
22	8	5.1	pł.	[dew] 0:00 5:30; [fog] 1:40 2:15, 5:30 6:25, 19:00 22:40 … 24; [wind] 1:00–30, 5:00 8:30, 19:30 24; 18:30 19:30; () 7:20 8:40
23	9	•	pł.	[rain shower] 3:45 4:40; R SW 3:45 N–NE–(R) E 5:40; [dew] 22:30 24; [fog] 0:00–50 … –4:30, 5:05–30 … 6:35 … –6:55, 7:30 9:40; [wind] 0:00 3:30, 4:50 7:10 (por. 17); () 4:30 5:30, 13:00 16:00; [blowing snow] 13:45 5:15
24	8	•	pł.	[lightning] 23:45 W, SW–24; [dew] 0:00 4:30
25	8	•	pł.	[lightning] 0:00 W, SW – 2:30
26	8	•	pł.	(R) 19:45 21:45 SW–SE, NE; [fog] 21:20 22:30; [wind] 22:45 23:10 (por. 16); [blowing snow] 16:40 17:15
27	9	39.1	pł.	[rain-shower and hail entries, 9:53 to 22:05]; (R) 13:08 S–E 13:20 –NE 13:45; (R) SE 15:37, R E 16:23 –(R) E 16:40 NE 17:10 NW 17:55 W 19:53 NW
28	0	29.8	pł.	[rain-shower, rain, snow and snow pellet entries, 6:56 to 24]; [fog] 5:15 6:05 … 6:53 … 13:50 … –14:20 … 24; [wind] 7:25 8:50, 11:40 24 (por. 22); [blowing snow] 13:20 17:10
29	9	•	pł.	[rain] 0:00 1:20; [fog] 0:00 4:45 … –5:30, 6:30 7:15, 15:15 16:00 … 19:15 … –19:40 … 23:40 … –24; [wind] 0:00 4:15, 5:45 6:15; 5:30 6:00; () 5:30 14:15
30	8	•	pł.	[dew] 20:30 24; [fog] 0:00 1:40 (m) 2:30 6:00 … 20:20–23:30; [wind] 19:30–24; () 3:30–12:30
31				[27.VI: N–20:30 SW, S, N, W, R 21:15 R 21:21 R E, N 21:55 (R) E 23:30; [fog] 13:05–10, 19:27–30 … 19:50 … –20:03; [wind] 21:20 22:30 (por. 16); [rainbow] 17:30–37; () 8:30 10:20; [blowing snow] 13:02–10, 16:15 17:05, 21:15–50, 22:05]
Σ	–	375.5	–	

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Lipiec – Juillet 1965

DNI	CIŚNIENIE P = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	100.6	101.5	100.8	101.0	8.5	11.7	8.6	9.4	14.2	6.6	69	78	86	78	3.5	3.0	1.7	2.7	7	10 •	9	SSE 11	WSW 2	W 2
2	98.1	97.5	97.3	97.6	7.1	7.1	3.0	5.0	9.3	2.8	100	100	98	99	0.0	0.0	0.2	0.1	10 • ≡	10 ₉ ≡	4	WNW 5	C 0	WNW 4
3	96.1	96.3	96.0	96.1	2.6	4.6	3.3	3.4	5.8	1.1	84	91	100	92	1.3	0.7	0.0	0.7	6	9	9	WSW 5	S 7	W 12
4	95.3	94.7	93.7	94.6	2.8	4.3	4.6	4.1	5.4	0.2	79	100	100	93	1.5	0.0	0.0	0.5	9	10 • ≡	10 ≡	WSW 15	SW 10	SW 5
5	92.1	91.3	93.8	92.4	2.6	0.4	-0.4	0.6	4.8	-1.0	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 * ≡	10 ≡	W 3	W 6	W 10
6	97.3	98.6	99.4	98.4	-2.4	0.1	-0.1	-0.6	1.9	-2.4	100	85	96	94	0.0	1.0	0.3	0.4	7	9	9	NW 6	NW 7	WNW 15
7	99.8	99.8	99.6	99.7	0.6	4.7	4.7	3.7	5.9	-0.4	79	89	93	87	1.4	0.9	0.6	1.0	2	9	9	SW 7	SSW 14	SSE 15
8	97.8	93.8	92.7	94.8	6.1	6.8	5.5	6.0	8.8	3.6	62	86	100	83	3.5	1.4	0.0	1.6	9	8	10 • K ≡	SE 15	SSE 18	W 8
9	93.4	96.0	98.0	95.8	1.2	2.9	0.8	1.4	6.2	0.5	98	78	73	83	0.2	2.1	1.8	1.4	6	7	5	WSW 7	W 8	WNW 6
10	98.4	99.2	100.1	99.2	0.2	2.3	0.6	0.9	3.6	-1.3	71	89	100	87	1.8	0.8	0.0	0.9	4	10 * ⚹	10 ⚹ ≡	WSW 2	C 0	NW 5
11	100.8	102.5	103.5	102.3	0.5	2.5	1.7	1.6	4.5	-0.4	100	89	86	92	0.0	0.8	0.9	0.6	10 ≡	10	1	NNE 4	NNW 1	NW 1
12	103.1	103.4	103.0	103.2	3.2	9.4	7.8	7.0	9.9	1.4	87	70	81	79	1.0	3.4	2.0	2.1	7	9	10 •	W 1	N 3	WSW 7
13	102.7	103.6	104.7	103.7	7.2	8.3	9.1	8.4	11.5	6.5	100	97	97	98	0.0	0.4	0.4	0.3	10 ≡	9	4	NNW 4	WNW 5	WSW 4
14	105.7	107.3	107.2	106.7	9.7	14.2	12.2	12.1	15.2	7.3	66	64	74	68	4.0	5.8	3.8	4.5	1	6	1	N 8	N 1	SSW 3
15	107.2	107.2	106.3	106.9	11.3	15.5	12.7	13.0	16.7	9.7	87	63	63	71	1.8	6.6	5.4	4.6	1	4	5	N 4	N 5	N 3
16	104.3	104.2	103.4	104.0	12.3	11.9	11.4	11.8	14.1	8.2	73	87	61	74	3.9	1.8	5.2	3.6	1	9 • (K)	9	N 4	NNE 3	SE 5
17	102.1	101.0	99.5	100.9	10.6	12.1	8.1	9.7	12.7	7.1	95	78	84	86	0.7	3.0	1.8	1.8	2	9 (K)	8	SSE 3	SW 1	NNE 5
18	97.0	97.8	100.1	98.3	6.5	6.5	6.6	6.6	8.8	5.7	100	97	100	99	0.0	0.4	0.0	0.1	8	10 •	10 ≡	C 0	WSW 4	NNE 5
19	101.9	103.5	104.2	103.2	6.6	8.2	7.3	7.4	9.1	5.6	100	100	97	99	0.0	0.0	0.3	0.1	10 ₉ ≡	10 • ≡	9	NE 4	NNW 2	SSE 6
20	104.0	104.4	102.8	103.7	7.3	9.2	7.5	7.9	9.8	6.6	100	100	100	100	0.0	0.0	0.0	0.0	10	10	6	S 3	C 0	SSE 6
21	100.7	99.7	98.4	99.6	7.4	8.8	7.6	7.8	9.1	6.5	100	91	100	97	0.0	1.0	0.0	0.3	10	9 •	10	SSE 9	SE 11	SSW 5
22	98.9	100.3	99.1	99.4	6.0	9.3	8.1	7.9	11.5	5.6	100	87	100	96	0.0	1.5	0.0	0.5	8 •	9	10 • ≡	W 2	C 0	SSW 5
23	96.6	96.7	98.7	97.3	7.8	7.7	6.3	7.0	9.3	6.1	97	100	84	94	0.4	0.0	1.5	0.6	9	10 • ≡	1	SE 9	SSE 8	W 7
24	100.1	101.9	102.6	101.5	9.4	10.8	10.6	10.4	12.7	6.3	62	83	73	73	4.4	2.3	3.4	3.4	5	8	1	WSW 8	SW 11	WSW 8
25	102.7	102.5	101.0	102.1	10.3	11.7	9.6	10.3	13.5	9.2	72	73	100	82	3.5	3.7	0.0	2.4	8	9	10 ≡	SSW 8	SW 7	NW 2
26	100.9	100.3	98.4	99.9	9.1	5.9	3.7	5.6	11.3	2.5	65	100	76	80	4.1	0.0	2.0	2.0	10 •	10 • ≡	10 •	WSW 8	WNW 4	NW 6
27	96.5	98.0	99.6	98.0	2.0	2.4	2.7	2.4	4.4	1.3	100	100	89	96	0.0	0.0	0.8	0.3	10 • ≡	10 •	3	N 6	W 3	W 8
28	99.3	100.4	99.1	99.6	1.3	2.3	3.1	2.4	3.8	1.0	100	96	82	93	0.0	0.3	1.5	0.6	10 ≡	9	9	WNW 9	SW 4	WSW 9
29	97.2	98.0	95.9	97.0	3.6	8.3	6.8	6.4	10.2	2.0	91	76	71	79	0.7	2.7	2.9	2.1	3	7	9	S 7	SSW 4	SSW 13
30	91.7	92.5	93.1	92.4	3.5	4.4	3.7	4.3	7.1	3.5	85	100	85	90	1.3	0.0	1.2	0.8	9	10 • ≡	7	S 14	SSW 9	WSW 11
31	93.4	92.2	94.1	93.2	3.1	3.3	6.6	5.4	7.6	2.6	89	100	51	80	0.8	0.0	4.7	1.8	10 *	10 ≡	7	C 0	SSE 10	W 11
M	99.2	99.6	99.6	99.5	5.5	7.1	5.9	6.1	9.0	3.7	87	89	87	88	1.3	1.4	1.4	1.4	7.2	9.0	7.3	6.0	5.4	6.6

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1	95.5	96.7	94.3	95.5	3.4	6.1	4.5	4.6	8.1	3.0	98	97	100	98	0.1	0.3	0.0	0.1	9	10	10 • ≡	SSW 5	N 4	NE 3
2	87.8	91.3	95.1	91.4	-0.2	-2.2	-0.7	-1.0	4.6	-2.7	100	100	99	100	0.0	0.0	0.0	0.0	10 * ≡	10 * △ ≡	9	N 16	N 9	NW 8
3	95.5	96.4	97.2	96.4	0.3	3.2	1.8	1.8	3.6	-1.6	87	89	100	92	0.8	0.8	0.0	0.5	1	9	8	SW 7	SSE 6	SW 7
4	99.4	101.3	102.5	101.1	2.4	3.5	3.7	3.3	5.4	1.7	98	94	85	92	0.2	0.4	1.2	0.6	9	9	8	W 10	WSW 6	WNW 12
5	104.6	106.2	106.7	105.8	2.4	7.7	6.7	5.9	8.9	2.0	96	70	90	85	0.3	3.2	1.0	1.5	9	8	4	NNW 8	NNW 7	W 4
6	107.4	108.7	108.7	108.3	10.5	13.6	14.3	13.2	15.0	6.3	46	61	52	53	6.8	6.1	7.9	6.9	0	4	7	SSW 6	SSW 7	WSW 9
7	108.1	107.8	106.8	107.6	13.2	16.0	13.4	14.0	16.9	12.2	43	50	42	45	8.6	9.0	9.0	8.9	6	1	0	S 8	SSE 11	SSE 14
8	105.2	104.4	104.6	104.7	10.6	13.3	13.7	13.4	17.2	10.2	59	36	43	46	5.3	11.3	9.0	8.5	0	0	1	SSE 11	SSW 12	WSW 4
9	103.9	104.0	104.1	104.0	10.0	11.7	10.8	10.8	13.3	9.3	84	96	95	92	2.0	0.3	0.8	1.1	2	8	7	SSW 5	SSW 4	W 1
10	103.1	103.0	102.0	102.7	10.7	10.3	6.9	8.8	13.3	4.9	63	93	97	86	4.6	0.7	0.3	1.9	3	10 ≡	10	SSW 3	S 3	S 2
11	100.3	100.9	101.1	100.8	1.2	1.2	0.3	0.8	7.6	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	10 * ≡	10 * ≡	N 7	N 11	N 12
12	100.2	102.4	102.8	101.8	0.1	0.1	1.2	0.6	1.5	-0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ⚹ ≡	10 ≡	N 14	N 10	N 9
13	101.3	102.6	102.5	102.1	0.2	-0.4	-0.1	-0.1	1.3	-1.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	9	10 ≡	N 8	N 5	N 7
14	101.6	102.3	101.8	101.9	-0.6	3.2	2.0	1.6	4.8	-0.8	99	94	87	93	0.0	0.4	0.9	0.4	9	8	9	N 5	N 3	W 3
15	101.2	102.3	102.4	102.0	1.0	2.3	2.1	1.9	4.9	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 * ≡	8	8	N 4	NNW 1	NNW 1
16	101.7	102.2	102.0	102.0	1.2	2.9	2.9	2.3	4.6	0.7	96	100	94	97	0.3	0.0	0.4	0.2	8	10 ≡	5	E 3	SSE 2	SW 2
17	101.1	102.1	102.4	101.9	2.4	5.0	4.0	3.8	7.2	1.9	85	93	91	90	1.1	0.6	0.7	0.8	8	9	1	S 3	NNW 2	SW 4
18	102.7	104.7	105.9	104.4	3.5	7.3	6.1	5.8	9.8	2.8	81	78	82	80	1.5	2.3	1.6	1.8	0	6	0	W 2	N 2	NW 1
19	107.3	108.6	108.6	108.2	3.3	9.3	6.6	7.0	11.3	4.3	86	65	77	76	1.2	4.0	2.2	2.3	1	6	4	N 3	NNW 2	W 3
20	107.7	107.6	106.6	107.3	6.4	9.5	7.4	7.7	11.5	5.4	73	81	93	84	2.4	2.3	0.5	1.7	3	8	4	NNE 1	N 1	E 6
21	104.9	104.4	102.5	103.9	6.2	8.6	7.5	7.4	10.8	5.3	90	72	92	85	0.9	3.2	0.8	1.6	4	8	6	SSW 9	SW 7	SSE 9
22	99.5	98.7	97.5	98.6	7.2	9.2	7.3	7.8	10.3	6.6	73	66	79	73	2.8	3.9	2.1	2.9	5	2	2	SSE 13	S 16	SSE 14
23	97.2	98.4	99.1	98.2	7.5	8.7	9.3	8.7	11.2	6.6	89	80	87	85	1.2	2.2	1.5	1.6	3	9	10	SSE 11	S 13	SSE 16
24	97.6	98.3	96.0	97.3	10.0	10.4	9.2	9.7	12.5	8.9	78	87	100	88	2.7	1.7	0.0	1.5	8	10 •	10 •	SSE 14	SSE 7	SSE 9
25	93.7	94.4	95.3	94.3	6.7	7.2	5.5	6.2	9.4	5.3	100	100	100	100	0.0	0.0	0.0	0.0	10 •	10 • ≡	10 • ≡	SSW 11	S 6	NNW 5
26	95.0	95.2	94.5	94.9	2.0	-0.9	-1.6	-0.5	5.5	-2.0	100	99	98	99	0.0	0.0	0.1	0.0	10 • ≡	10 * ≡	10 * ≡	N 13	N 10	N 13
27	93.6	94.7	96.6	95.0	-1.3	-0.8	-0.3	-0.7	0.0	-2.2	99	99	100	99	0.1	0.0	0.0	0.0	10 * ≡	10 * ≡	10 ≡	N 10	N 3	WNW 5
28	96.6	98.1	99.3	98.0	-0.9	0.7	0.3	0.1	1.5	-1.3	99	98	100	99	0.0	0.1	0.0	0.0	10 * ≡	10 ≡	10 ≡	NNW 5	N 2	NE 2
29	99.0	99.1	98.5	98.9	0.7	0.9	1.3	1.0	2.4	-0.4	82	96	71	83	1.2	0.3	1.9	1.1	4	9 ⚹ △	3	C 0	S 5	W 4
30	97.8	99.1	100.0	99.0	1.9	1.6	0.2	1.0	3.1	0.2	98	100	96	98	0.1	0.0	0.3	0.1	9	9	3	WSW 5	N 4	NNE 2
31	99.0	99.1	97.8	98.6	-0.3	3.6	3.0	2.3	5.1	-0.5	100	76	92	89	0.0	1.9	0.6	0.8	9	7	4	N 1	SW 4	SSW 10
M	100.3	101.1	101.1	100.8	4.0	5.7	4.8	4.8	7.9	2.8	87	86	89	87	1.4	1.8	1.4	1.5	6.5	8.0	6.5	7.0	6.0	6.5

Kasprowy Wierch — $H_s = 1991\,m$ — $H_b = 1988{,}8\,m$ — $h_w = 15{,}4\,m$ — Lipiec - Juillet 1965

DNI	WIDZIALNOŚĆ	OPAD	GRUBA ŚNIEGU	POGODA
1	8	10.9	pz.	[illegible]
2	0	6.2	pz.	[illegible]
3	8	0.7	pz.	[illegible]
4	0	17.1	pz.	[illegible]
5	0	22.0	pz.	[illegible]
6	8	0.6	ʒ	[illegible]
7	8	.	pz.	[illegible]
8	8	24.6	pz.	[illegible]
9	8	0.0	pz.	[illegible] **10.VII:** [illegible]
10	8	4.2	.	[illegible]
11	7	0.2	.	[illegible]
12	8	5.9	.	[illegible]
13	8	0.0	.	[illegible]
14	9	.	.	[illegible]
15	7	.	.	[illegible] **17.VII:** [illegible]
16	8	25.8	.	[illegible]
17	8	20.7	.	[illegible]
18	8	5.5	.	[illegible]
19	0	10.3	.	[illegible]
20	6	10.5	.	[illegible]
21	8	15.2	.	[illegible]
22	9	.	.	[illegible] **20.VII:** [illegible]
23	0	0.9	.	[illegible]
24	8	0.0	.	[illegible] **21.VII:** [illegible]
25	8	0.0	.	[illegible]
26	0	9.2	.	[illegible]
27	7	1.7	.	[illegible]
28	8	0.0	.	[illegible]
29	9	4.0	.	[illegible]
30	1	8.9	.	[illegible]
31	0	8.0	.	[illegible]
Σ	-	211.1	-	

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1	6	53.3	.	[illegible]
2	0	54.4	.	[illegible]
3	8	0.2	19	[illegible] **2.VIII:** [illegible]
4	7	0.6	10	[illegible]
5	7	-	pz.	[illegible]
6	9	.	pz.	[illegible]
7	9	.	pz.	[illegible]
8	9	.	.	[illegible]
9	8	.	.	[illegible]
10	0	10.0	.	[illegible]
11	0	29.0	.	[illegible]
12	0	16.7	.	[illegible]
13	7	1.5	2	[illegible]
14	8	0.0	pz.	[illegible]
15	7	5.8	.	[illegible]
16	0	0.0	.	[illegible]
17	8	.	.	[illegible]
18	8	.	.	[illegible]
19	8	.	.	[illegible]
20	7	.	.	[illegible]
21	8	.	.	[illegible]
22	8	.	.	[illegible]
23	8	0.0	.	[illegible]
24	8	8.8	.	[illegible]
25	0	31.0	.	[illegible]
26	0	67.6	.	[illegible] **24.VIII:** [illegible]
27	0	6.7	24	[illegible]
28	0	3.3	26	[illegible]
29	8	0.5	20	[illegible]
30	7	0.6	19	[illegible]
31	8	1.6	17	[illegible]
Σ	-	289.6	-	

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Wrzesień – Septembre 1965

DNI	CIŚNIENIE P = 700+ I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	96.5	98.4	100.7	98.5	4.0	5.2	6.1	5.4	6.3	2.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10	S 11	S 15	SSE14
2	103.0	103.8	104.5	103.8	8.4	12.1	8.9	9.6	12.5	6.1	67	51	80	66	3.6	6.8	2.4	4.3	9	6	9	SSE 7	SSE14	SSE16
3	100.8	102.2	102.4	101.8	9.9	11.7	9.1	10.0	13.1	7.7	60	60	83	68	4.8	5.5	2.2	4.2	8	9	8	SSE20	SSE14	ESE 8
4	98.2	97.2	97.5	97.6	8.9	7.7	3.0	5.6	10.6	2.6	95	100	91	95	0.5	0.0	0.7	0.4	10	10 • ≡	1	SSW10	S 11	S 12
5	97.5	98.1	96.9	97.5	2.6	5.2	4.7	4.3	6.2	2.1	100	85	100	95	0.0	1.3	0.0	0.4	9	8	9	S 9	S 8	SSE12
6	95.2	94.5	93.7	94.5	4.9	5.6	5.5	5.4	6.1	4.4	100	100	100	100	0.0	0.0	0.0	0.0	10	10 •♦ ≡	10 • ≡	S 12	SSE 8	C 0
7	93.3	94.9	96.5	94.9	0.8	3.7	2.0	2.1	5.6	0.2	73	89	98	87	1.8	0.9	0.2	1.0	3	8	10 •	W 5	SSW 6	SW 10
8	98.0	100.6	101.2	99.9	0.9	3.5	3.2	2.7	5.2	0.8	100	87	91	93	0.0	1.0	0.7	0.6	9	8	7	W 12	SW 5	S 8
9	99.9	102.4	100.9	101.1	4.9	8.2	5.9	6.2	9.8	3.0	100	89	98	96	0.0	1.2	0.2	0.5	9	4	8	S 14	SW 9	S 13
10	97.9	99.2	99.6	98.9	6.6	7.3	7.5	7.2	7.9	5.4	100	100	100	100	0.0	0.0	0.0	0.0	9	10 • ≡	9	SSE16	SSW18	S 16
11	96.6	98.7	97.6	97.6	7.5	8.3	1.3	4.6	8.8	1.3	100	94	100	98	0.0	0.7	0.0	0.2	9	8	10 ✱	SW 21	SSW12	WSW 5
12	97.0	97.9	96.8	97.2	0.6	3.0	1.4	1.6	4.3	0.1	96	100	100	99	0.3	0.0	0.0	0.1	2	9	9	NNE 2	W 1	SSW 4
13	94.6	95.1	96.1	95.3	0.6	3.1	1.0	1.4	3.5	0.2	100	89	94	94	0.0	0.8	0.4	0.4	10	8	1	NNE 5	NW 4	SW 2
14	96.9	98.6	101.9	99.1	0.1	-0.4	0.6	0.2	1.7	-1.2	88	100	100	96	0.8	0.0	0.0	0.3	9	10 ✱ ≡	10 ≡	S 5	SSE 9	N 5
15	103.4	105.0	106.3	104.9	1.2	2.1	1.0	1.3	2.7	0.1	82	88	100	90	1.2	0.8	0.0	0.7	7	9	10 ≡	SW 5	WNW 6	N 8
16	107.2	108.2	108.1	108.0	1.7	7.5	7.7	6.2	8.3	-0.4	53	78	36	56	3.2	2.3	6.8	4.1	1	2	2	N 4	C 0	SW 3
17	106.9	107.6	107.0	107.2	6.1	9.0	7.7	7.6	10.4	5.9	21	70	50	47	7.4	3.4	5.3	5.4	0	1	0	S 6	SSW 4	SSW 6
18	104.2	103.6	103.2	103.7	5.1	6.5	5.1	5.4	8.3	3.5	50	81	89	73	4.4	1.8	0.9	2.4	0	2	2	SE 12	SSW13	S 13
19	102.8	103.6	104.3	103.6	5.5	2.1	-1.2	1.3	6.7	-1.3	100	100	99	100	0.0	0.0	0.1	0.0	8	10 • ≡	10 △ ≡	SSE10	N 6	N 7
20	105.5	107.3	109.9	107.6	-1.8	-0.8	-0.8	-1.0	-0.2	-2.1	98	99	99	99	0.1	0.0	0.0	0.0	10 ✱△ ≡	10 ♦ ≡	10 ♦ ≡	N 9	NNE 6	N 9
21	110.7	111.9	111.2	111.3	-0.6	1.3	6.5	3.4	7.1	-2.0	99	100	19	73	0.0	0.0	7.4	2.5	10 ♦ ≡	10 ≡	1	NNE 8	S 2	ENE 2
22	109.4	109.6	107.4	108.8	10.0	10.1	9.4	9.7	11.8	4.9	41	44	16	34	7.3	7.1	9.9	8.1	5	8	7	C 0	S 4	S 8
23	105.4	105.2	103.4	104.7	10.1	12.4	10.1	10.7	13.7	7.8	25	45	22	31	9.4	7.9	9.7	9.0	1	1	0	ENE 2	S 3	SSE 6
24	101.6	102.6	102.1	102.1	9.2	10.8	7.7	8.8	11.9	6.1	15	28	21	21	9.8	9.3	8.3	9.1	0	0	0	SE 7	SSW 7	SSE 7
25	100.7	100.6	98.5	99.9	6.6	11.0	6.5	7.6	11.9	4.8	70	47	58	58	2.8	6.9	4.0	4.6	1	7	6	SE 8	S 6	SE 10
26	95.1	95.0	95.3	95.1	4.3	6.5	5.3	5.4	7.1	3.8	98	83	88	90	0.1	1.7	1.1	1.0	9	7	9	S 18	SSE16	SE 17
27	93.5	94.1	95.5	94.4	5.4	4.8	5.1	5.1	7.4	4.2	100	90	98	96	0.0	0.9	0.2	0.4	10 • ≡	8	9	SSW15	S 20	S 17
28	94.9	95.5	91.2	93.9	6.1	8.2	8.9	8.0	9.2	5.1	98	87	91	92	0.1	1.5	1.0	0.9	9	9	9	S 23	S 13	S 23
29	92.8	93.6	98.8	94.7	5.7	0.6	0.9	2.0	9.4	-0.2	100	100	63	88	0.0	0.0	2.4	0.8	10 •	10 ✱	0	SSE11	SSW13	SSE10
30	98.2	100.9	102.1	100.4	1.3	5.6	4.4	3.9	6.3	0.5	94	79	82	85	0.4	1.9	1.6	1.3	8	7	6	SSE19	S 13	S 10
31																								
M	99.9	100.9	101.0	100.6	4.6	6.1	4.8	5.1	7.8	2.5	81	82	79	81	1.9	2.1	2.2	2.1	6.8	7.3	6.4	10.2	8.8	9.4

Październik – Octobre

1	102.6	104.1	104.1	103.6	9.3	10.8	9.5	9.8	12.4	3.5	53	71	62	62	5.5	3.8	4.5	4.6	1	0	0	S 8	S 7	SE 4
2	102.8	103.5	104.2	103.5	9.7	12.5	9.3	10.2	13.8	7.4	55	60	61	59	5.4	5.8	4.4	5.2	0	1	1	SSW 9	S 7	S 6
3	104.8	105.9	106.5	105.7	8.8	11.0	7.5	8.7	11.4	7.4	49	59	89	66	5.7	5.2	1.2	4.0	4	7	1	S 5	WSW 7	SE 6
4	106.7	106.8	105.9	106.5	6.4	8.9	7.6	7.6	10.4	6.1	90	88	92	90	0.9	1.3	0.8	1.0	9	8	6	SW 5	SSW 6	S 5
5	104.3	104.3	103.8	104.1	6.2	6.9	3.7	5.1	7.9	2.4	100	100	50	83	0.0	0.0	4.0	1.3	9	10 ≡	0	WSW 3	NNE 2	NNE 4
6	103.1	103.7	103.7	103.5	5.1	7.1	5.3	5.2	7.4	2.5	52	78	36	49	5.2	2.3	5.7	4.4	4	6	1	W 6	ENE 1	C 0
7	102.7	103.3	103.3	103.1	4.9	8.9	6.2	6.6	9.8	3.9	9	37	27	24	7.9	7.2	6.9	7.3	1	1	6	NNE 2	ESE 1	SW 2
8	101.4	100.7	99.2	100.4	6.3	9.0	2.4	5.0	9.6	2.2	14	35	100	50	8.2	7.6	0.0	5.3	9	7	10 ≡	WSW 4	WSW 4	NNE 5
9	96.6	96.2	95.0	95.9	-1.5	-2.2	-4.4	-3.1	2.9	-4.9	99	100	98	99	0.1	0.0	0.1	0.1	10 ≡	10 ≡	10 ≡	N 4	N 4	N 11
10	95.4	94.7	96.3	94.8	-5.6	-5.7	-6.0	-5.8	-4.4	-6.5	97	97	94	96	0.2	0.1	0.2	0.2	10 ⅄ ≡	10 ⅄ ≡	2	NNW12	N 1	N 9
11	97.1	97.3	97.4	97.3	-5.1	-1.4	-3.3	-3.3	-0.9	-6.5	98	94	99	97	0.1	0.3	0.0	0.1	8	3	10 ≡	N 3	W 1	NNW 7
12	98.6	101.8	103.7	101.4	-6.6	-6.0	-5.3	-5.8	-3.1	-7.8	97	92	40	76	0.1	0.3	2.4	0.9	10 ≡	1	0	N 7	NNE 5	NNE 6
13	104.6	105.9	105.7	105.4	-1.0	2.9	1.1	1.0	4.5	-5.6	36	45	58	46	3.7	4.1	2.8	3.5	0	2	9	NE 6	C 0	W 1
14	104.7	105.5	105.7	105.3	3.9	6.6	5.4	5.3	7.9	1.1	36	40	5	27	5.4	5.8	8.5	6.6	6	2	1	WSW 5	C 0	WSW 5
15	105.2	105.4	105.2	105.3	4.8	6.9	7.9	6.9	8.4	4.3	28	32	23	28	6.1	6.7	8.2	7.0	5	3	3	S 5	SSW 7	SW 3
16	102.2	101.7	101.5	101.8	5.4	7.1	2.1	4.2	8.8	2.0	26	35	88	50	6.6	6.6	0.8	4.7	3	7	9	S 12	S 12	WNW 7
17	102.3	104.6	106.4	104.4	-4.0	-3.7	1.8	-1.0	2.1	-4.7	99	99	11	70	0.1	0.1	6.2	2.1	10 ≡	10 ≡	0	N 11	NNE 3	NNE 4
18	105.3	104.9	104.1	104.8	2.5	4.5	0.1	1.8	4.8	-0.2	9	38	41	29	6.6	5.1	3.7	5.1	2	1	2	SW 5	W 3	NW 5
19	103.4	104.3	104.4	104.0	-1.1	-0.8	-2.0	-1.5	0.9	-4.5	53	95	22	57	2.6	0.3	4.0	2.3	3	10 ≡	7	S 3	N 1	N 7
20	104.4	105.3	105.5	105.1	-3.3	-2.8	-8.2	-5.6	-1.0	-8.2	37	97	92	75	3.0	0.1	0.2	1.1	1	10 ≡	4	NNE 7	NE 1	NE 3
21	105.3	106.7	107.7	106.6	-4.4	-1.3	-2.3	-2.6	0.0	-8.2	14	68	26	36	3.8	1.8	3.8	3.1	1	1	1	NE 6	SW 3	C 0
22	108.8	109.8	109.6	109.4	-2.5	0.2	0.1	-0.5	0.9	-3.3	26	45	59	43	3.8	3.4	2.6	3.3	0	0	0	N 2	ENE 2	NNE 6
23	108.1	107.6	105.5	107.1	-1.0	1.9	-1.3	-0.4	2.9	-1.4	60	31	63	51	2.3	4.9	2.0	3.1	8	9	7	NNE 6	NNE 5	N 7
24	104.5	105.8	106.4	105.6	0.1	3.8	0.8	1.4	4.6	-2.2	47	44	48	46	3.3	4.3	3.4	3.7	1	1	0	NNE 6	NE 4	NE 6
25	106.0	106.4	105.6	106.0	-0.2	3.4	0.2	0.9	4.0	-0.4	58	50	61	56	2.5	4.0	2.4	3.0	1	1	0	NNE 5	C 0	NNW 4
26	104.6	104.8	103.4	104.3	0.7	5.0	3.1	3.0	6.1	-0.2	53	44	28	42	3.0	4.8	5.4	4.4	0	0	0	NW 1	W 1	SW 6
27	101.2	101.9	102.4	101.8	2.0	2.4	2.4	2.3	4.4	0.4	33	29	23	28	4.8	5.2	5.6	5.2	2	1	1	WSW 3	WSW 5	NW 4
28	102.4	102.6	102.1	102.4	2.7	5.1	3.0	4.4	6.1	1.3	43	54	61	53	4.0	4.0	3.4	3.8	7	9	8	NW 5	SSW 4	WSW12
29	100.9	100.7	99.9	100.5	3.9	6.0	3.9	4.4	7.0	2.7	40	56	69	55	4.9	4.1	2.5	3.8	7	8	9	S 7	WSW 6	W 6
30	100.0	100.4	99.3	99.9	-3.7	-0.3	0.9	-0.6	4.2	-5.9	99	37	18	51	0.1	3.7	5.4	3.1	10 ≡	3	6	N 2	SW 6	SSW 8
31	97.0	96.2	94.0	95.7	2.8	0.1	-3.4	-1.0	4.1	-3.4	12	76	99	62	6.6	1.6	0.0	2.7	9	9	10 ✱	WSW11	W 11	W 11
M	102.7	103.3	103.1	103.0	1.4	3.4	1.6	2.0	5.1	-0.9	52	62	56	57	3.6	3.4	3.3	3.4	4.9	4.9	3.9	5.7	3.9	[illegible]

Kasprowy Wierch — $H_s = 1991\,m$ — $H_b = 1988{,}8\,m$ — $h_w = 15{,}4\,m$ — Wrzesień – Septembre 1965

DNI	WIDZIALNOŚĆ	OPAD	GRUBOŚĆ LODU	POGODA
1	0	2.5	12	•0240 4.45 •0 0.00 11.55 •0 12.25 12.55 14.15 •0 16.20, = 0.00 16.20 = -16.45 = 2 17.05 = -17.45 = 2 19.40 20.30 = -21.40, ⛷ 0.00 5.15 (por. 19). 6.15 7.10 (por. 17), 12.15 24 (por. 28)
2	9	•	p2.	⛷ 0.00 10.15 (por. 38) ⛷ -15.30 (por. 42) ⛷ -19.15 (por. 40) ⛷ -21.45 (por. 40) ⛷ -22.00 (por. 29) ⛷ -22.30 (por. 42) ⛷ -24 (por. 31)
3	9	•	•	⛷ 0.00-05 (por. 30) ⛷ -1.00 (por. 30) ⛷ -3.30 (por. 32) ⛷ -4.30 (por. 44) ⛷ -6.15 (por. 33) ⛷ -11.10 (por. 43) ⛷ -12.45 (por. 32) ⛷ -13.15 (por. 30) ⛷ -18.30 (por. 28), 22.35 24 (por. 30), ⊕ 0 10.00 12.15 ◡ 0 19.00-20.10, () 10.30-18.30
4	0	28.1	•	▽ 0 9.25 10.00, 10.30-45 ▽ 0-1 15.30 •0-1 17.30, = 8.05 10.20 = 2 18.15, ⛷ 0.00 24.00 (por. 23), 4.30 5.50 (por. 21), 6.35 13.10 (por. 25), 15.30 21.30, () 18.30 24
5	9	•	•	= 6.05-45 = 2 7.05 = -7.30 = 2 8.10 = -10.20, 17.40 18.30 = 2 19.01 = -22.30, ⛷ 19.45 24.15 (por. 18), 15.10 24 (por. 23); () 0.00 3.30
6	0	11.5	•	▽ 0.30 9.00 •0 -12.45 ▽ 0 15.40 18.10 ▽ 0-2 20.05 22.05, = 0.30-50 7.53-40 = 0 9.00 12.40 = -13.45 16.10-50 = 2 -24, ⛷ 0.00 1.30 (por. 26) ⛷ -3.10 (por. 26) ⛷ -12.15 (por. 26), 14.40 15.00 (por. 18); () 6.50 8.30
7	8	2.0	•	•0 10.50 21.30, 23.30 24, = 1.00 20.00 = 10.45 11.30 17.55 18.30 = 2 19.30 = -21.30 = 2 22.40, = 23.15 = 2 24, ⛷ 20.15 24 (por. 19), () 9.30 10.45
8	8	•	•	•0 1.00-30 7.30-50 ▽ 1.40-40, ◠ 0 21.00 24, = 2 1.00 1.40 = 5.30 8.50 23.15 24, ⛷ 0.00-30, 1.35 9.45 (por. 20), 21.25 24, () 17.30 18.30
9	9	•	•	◠ 0 0.00-30, = (0.00-30 = 2 3.40 = -4.15 = 2 5.50 = -10.00, 17.20 19.30 = 2 19.45 = -20.30, ⛷ 0.00 3.45 (por. 20) ⛷ -4.30 (por. 22) ⛷ -6.00 (por. 20) ⛷ -6.15 (por. 20) ⛷ -7.30 (por. 20) ⛷ -8.00 (por. 20) ⛷ -11.00 (por. 20), 18.40 24 (por. 33);
10	0	2.0	•	▽ 0 12.25 13.05 13.45 14.10, = 5.30 10.00 = 2 13.40 = -22.40, ⛷ 0.00 4.40 (por. 27) ⛷ -19.30 (por. 33) ⛷ -18.30 (por. 27) ⛷ -24 (por. 33) [9.IX: () 7.30 8.30
11	8	25.7	•	▽ 0 2.30 3.00 4.35 5.30 ▽ 0-2 10.05 11.10 ▽ 0 14.25 15.00 ▽ 0-1 17.00 •0-1 18.40 •0 20.10 ✳ 0 21.45 •0 22.40 23.35, = 0.30 3.30 = 2 4.30 = -11.40 = 2 11.00 = -12.05 14.30 18.30 = 2 20.15 = -20.45 = 2 24, ⛷ (0.00 11.00 (por. 45) ⛷ -15.40 (por. 30)
12	6	1.2	•	•0 3.20 5.00 ▽ 17.45 18.15 ▲ 2 19.30 ▽ 0 -18.30, = 2 0.00 5.15 = -5.40 = 2 7.10 8.40 = -15.40 = 2 16.05 = -19.20 = 2 20.05 = -20.45 m -21.30, ⛆ 16.15 7.10
13	8	0.7	•	▽ 0 17.30 19.05 19.52 20.00 21.35-40 15.05-15 ▽ 1-15.30 ▽ 0 16.30-40 ▽ 0 17.30 18.30, ◡ 2-na.-6.45, 22.30 24, = 6.05-45, 7.00-50 = 2 11.50 = -12.05 = 2 13.40 = -15.30 = 2 17.45 18.05 19.30 = 23.30 24, ⛷ 0 16.30 17.10
14	0	3.1	•	✳ 0 7.20 8.30 ✳ 0-1 17.50 ✳ △ 0 -19.30 △ 0 -20.00 ✳ 0 -15.20, ◡ 0-1 0.00 7.30 ⋁ 0 11.00 14.15, = 0.00 3.30 = 2 4.30 7.45 8.10 = -8.30 9.40 10.50 = 2 15.25 = -15.35 = 2 16.35 = -17.55 18.05-30 = 2 -21.30 = -23.15, ⛆ 0 16.45-48, () 3.00-30
15	8	•	•	◡ 0-1 0.00 7.30, = 1.00-30 = 2 16.45 -18.40 = -19.10 = 2 24, ◡ 1.00 21.15
16	8	•	•	◡ 0 3.30 8.30, = 2 0.00-30 = -1.40
17	9	•	•	= 1.00 15.10 17.10-40, () 6.30 14.20, 17.40 24
18	9	•	•	(m) na.-0.30 = 18.30 19.30 22.30 23.15, ⛷ 0.15 10.40 (por. 22) ⛷ -11.15 (por. 24) ⛷ -24 (por. 25); () 0.00 14.30
19	0	25.4	•	•0 10.40 11.00 ▽ 1-12.45 ▽ 1-13.10 ▽ 1 -14.20 ▽ 0-15.40 ▽ 1-16.30 △ 0-18.40 ◠ 0 -19.45 ✳ 1-20.20 △ 0-23.40 △ 1-2 24, ⋁ 17.30 19.40 ⋁ ◠ 0-19.45 ⋁ 2 24, = 6.05 10.15 = 2 24, ⛷ 0.00 2.15 6.30-8.10
20	0	1.8	6	△ 1-2 0.00 7.15 ✳ △ 1-2 8.30 △ 0 -9.15 •0 17.40 13.50 ◠ 0 20.15 22.10 ⋁ 0 22.15 23.30 19.30 20.15 ◠ 0 22.10 ⋁ 2 24, = 0.00 9.30 = -9.40 = 2 17.17 = -17.30 = 2 24, ⛷ 17.30 18.30
21	0	0.0	6	◠ 0 6.25 7.30 ⋁ 0 0.00 6.25 ◡ 0 -7.30, = 2 0.00 8.00 = -8.05 = 2 15.35 = m -16.45 = 2 17.00 = -17.35 m 17.20 18.30; () 15.35 16.45 17.20 24
22	9	•	5	() 0.00 24
23	9	•	p2.	() 0.00 15.30, 23.40 24
24	9	•	•	() 0.00 24
25	9	•	•	⛷ 9.00 10.50 (por. 18), 19.45 24 (por. 20); () 0.00 8.30 [26.IX: ⛷ 24 (por. 26)
26	9	2.5	•	▽ 14.50 15.05 16.25 17.10 18.10-20 19.45 20.05 21.55 22.05, = 5.30 6.05 6.30 7.10 22.30-45 = 2 24, ⛷ 0.00-30 (por. 20) ⛷ -2.15 (por. 20) ⛷ -3.45 (por. 25) ⛷ -4.00 (por. 30) ⛷ -5.40 (por. 26) ⛷ -12.50 (por. 41) ⛷ -15.40 (por. 24) ⛷ -23.30 (por. 44)
27	9	1.9	•	•0 4.40 6.10 ▽ 1-6.45 ▽ 2 7.10 23.45 24, = 0.00 2.30 = 3.55 10.10-25 = 2 7.15 = -8.40 = 2 10.00 = -21.30 = 2 -22.45 = -24, ⛷ 0.00-40 (por. 27) ⛷ -1.30 (por. 25) ⛷ -5.00 (por. 37) ⛷ -6.05 (por. 44) ⛷ -7.10 (por. 27) ⛷ -24 (por. 48);
28	9	20.5	•	▽ 0 0.00-10 8.50 9.05 14.00 15.05, = 0.00 = 2 1.30 = -5.30 16.25 20.30 = 23.40 24, ⛷ 0.00 1.05 (por. 43) ⛷ -12.40 (por. 29) ⛷ -15.10 (por. 45) ⛷ -15.25 (por. 25) ⛷ -15.50 (por. 42) ⛷ -17.00 (por. 35) ⛷ -24 (por. 28);
29	8	20.6	•	▽ 0 0.00-30 ▽ 0-1 3.35 21.30 23.30 7.47 ▲ 2 7.52 ▽ 1-8.45 ✳ 1-9.17 ▽ 0-9.35 ✳ 0-1 11.10 13.15, = 2 0.00 2.30 = -4.30 = 2 6.15 = -8.40 = 2 -9.15 = -9.30 = 2 10.40 12.30 = -12.50 = 2 -16.15 = -17.30 ⛷ 0.00 3.00 (por. 37) ⛷ -5.15 (por. 18),
30	9	•	•	= 2 1.20 5.15 = -6.15, 17.45 18.10, ⛷ 0.00 2.15 (por. 25) ⛷ -11.05 (por. 35) ⛷ -14.15 (por. 26), 14.20 10.30 (por. 16), 20.30 24, ⊕ 0 9.30 11.00, () 5.15 24 [27.IX: () 18.30 21.50 [28.IX: () 5.30 16.10
31				[29.IX: 6.20-45 (por. 17), 7.40 9.10 (por. 25) ⛷ -11.00 (por. 30) ⛷ -11.45 (por. 20), 19.45 24 (por. 20); ◠ 0 9.45-50, ⛆ 0 10.30 13.00, () 9.15 10.40
Σ	-	149.1	-	

Październik – Octobre

1	9	•	•	⛷ 0.00 3.20; () 0.00 24
2	9	•	•	() 0.00 24
3	9	0.8	•	▲ 0 15.37-40; (K) 0 SSE-SW 15.02- K 0 16.15-45 (K) 0 16.45 SW-W-17.30; (m) 7.20 8.30 m -12.00 (m) -19.00 m -24 = 16.45 17.30; () 0.00 14.00
4	8	0.0	•	▽ 0 6.10-15 7.10-15, ◠ 0 20.00 24, = 2 17.40 19.20 = 21.30 22.30 m 0.00 5.00 (m) 16.30 17.40, 21.30 24, () 5.30 7.00 8.30 11.30
5	0	1.0	•	•0 9.30 10.15 •0 11.10 •0 14.15 15.10, ◠ 1-2 0.00 8.40, (m) 0.00 6.30 = -8.40 = 2 10.15 = -11.45 m -12.15 = -12.30 = 2 -16.50 = m -24; () 17.05 24
6	9	•	•	m 0.00 3.30 11.00 12.45 = -14.15, ⊕ 0 7.30 11.00, ⛆ 2 11.30 12.45 ⛆ 0 13.45, () 0.00 24
7	9	•	•	◡ 1 21.00 23.50, () 0.00 24
8	9	1.9	•	•0 23.30 24, = 15.40 17.45 = 2 24, ⊕ 1-0 6.20-30, () 0.00 14.30
9	0	1.4	•	•0 0.00 3.30 ◠ 0 7.30 8.15 ◡ 2 8.30 △ 0 10.30 15.50 16.10 ▽ 1-0 22.30 23.30, ◠ 0 7.30 8.30 ⋁ 0-1 4.30 24, = 2 0.00 24, ⛷ 16.20 24
10	0	1.5	1	▽ 0-1 0.15-45 ▽ 0 1.35 2.05 6.25-45 7.45 8.10 9.40 10.10 12.20 13.10, ⋁ 1-0 0.00 p... 20.10, 23.20 24, = 2 0.00 14.40 = -15.20 = 2 20.10 = -20.30 = 2 23.20 24, ⛷ 0.00 12.00
11	9	3.5	3	⋁ 0 0.00 5.15 ⋁ 0 19.40 -24, = 2 0.00 5.15 17.10-35 = 18.30 19.40 = 2 24, () 9.30 15.30
12	9	•	4	△ 1-2 0.30 2.40 ◠ △ 0 -4.30, ⋁ 0 0.00 2.40 ◡ -4.30 ⋁ 2 -7.30 ⋁ 2 -9.15 10.10-40, = 2 0.00 9.15 = -10.10 = 2 -10.40 = -11.45 14.30 15.10 m 9.15 10.10 10.40 13.30; () 12.10 -24
13	9	•	2	⊕ 0 15.15 16.00; () 0.00 24
14	9	•	p2.	◡ 0 0.30 -5.00; () 0.00 24
15	9	•	p2.	⛷ 13.35 15.20; ◡ 0 0.30 -3.00; () 0.00 24
16	9	2.6	p2.	✳ 0 22.30 -24; = 21.30-40 = 2 -24; ⛷ 4.30 15.10 (por. 20); () 0.00 21.30
17	0	•	•	✳ 0 0.00-15 •0 ◡ 3.30 ◠ 0 5.15 3.30 ⋁ 2 6.15 ⋁ 2 -12.45, = 2 0.00 11.20 = -11.30 = 2 -12.45 = -13.15 m -18.00, ⛷ 6.30 8.30, ⛆ 2 12.45 13.20, () 12.45 -24
18	9	•	•	(m) 17.15 19.00, () 0.00 24
19	0	•	•	◡ 0-1 5.10 8.30 (m) 4.30 10.30 = 11.00 (m) -11.45 = 12.15 = 2 13.05 = -13.15 = 2 15.30 m -15.15 = 2 17.01 = -17.15 m -20.00 (m) -24, () 0.00 10.45 15.30 16.15 17.15 24
20	1	•	•	⋁ 0 16.45 20.15; (m) 0.00 6.00 m -10.40 = -11.30 = 2 -20.15 = -22.30, () 0.00 11.30
21	9	•	•	() 6.00 -24
22	9	•	•	() 0.00 24; zalewy promieni 16.20
23	9	•	•	⛷ 15.15 18.30, ⊕ 0 9.30 14.30; () 0.00 24
24	9	•	•	m 4.00 6.00 (m) -11.30; () 0.00 24
25	9	•	•	◡ 2 3.00 24; () 0.00 24
26	9	•	•	◡ 0 0.00-8.00; () 0.00 24
27	9	•	•	() 0.00 24
28	9	•	•	⛷ 20.30 23.30 (por. 16); ⊕ 0 12.20 13.30; () 0.00 24
29	9	2.1	•	▽ 0 7.45 22.05 23.40 24, = 2 22.30 24, ⛷ 0.40 9.30, ⊕ 0 13.30 14.30, () 0.00 14.30
30	9	•	•	▽ 0 0.00-30 ▽ 2 1.15 ◠ 0 3.30 4.30, ⋁ 0 7.40 9.30 ◡ 2 -4.30 ⋁ 2 -7.35, = 2 0.00 7.35 = -8.35 m 9.30 12.00, ⛆ 2 7.35 8.50, () 9.30 24
31	8	1.3	•	▽ 0 16.40 -18.30 ✳ 2 -24, ⋁ 0 21.00 24, = 17.30 23.30 = 2 24, ⛷ 4.50 7.15 (por. 22), 7.40 13.00 (por. 24), 13.15-30 14.02 24 (por. 28), ⛆ 0 23.15 24, () 0.00 10.00
Σ	-	16.1	-	

Kasprowy Wierch — $\varphi = 49°14'$ — $\lambda = 19°59'$ — *Listopad – Novembre 1965*

DNI	CIŚNIENIE P = 700 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE I POGODA N_w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D_v I	II	III
1	92.7	91.1	89.3	91.0	-4.0	1.6	2.1	0.4	5.5	-6.6	99	96	72	89	0.1	0.3	2.0	0.8	10	9	9	WNW11	WSW16	SSW17
2	87.8	88.7	90.6	89.0	0.5	-0.8	-2.8	-1.5	2.6	-2.8	92	85	84	87	0.5	0.9	0.8	0.7	9	9	8	WSW16	WSW10	WSW12
3	91.0	92.2	91.6	91.6	-2.2	-1.9	-1.7	-1.9	-1.0	-4.4	57	85	98	80	2.2	0.8	0.1	1.0	1	7	10*≡	W 15	SSE 6	S 10
4	94.8	97.5	99.8	97.4	-3.2	-2.4	-2.3	-2.6	-1.7	-4.4	90	100	65	85	0.5	0.0	1.8	0.8	9	10 ≡	9	WSW 7	SSW 4	SW 5
5	101.1	102.7	103.8	102.5	-5.7	-5.3	-5.6	-5.0	-2.0	-7.2	35	56	40	44	2.6	2.1	2.4	2.4	9	7	0	NNE 4	NNE 3	NNE 7
6	105.0	106.2	104.9	105.4	-4.9	0.6	2.6	0.2	2.7	-6.4	49	23	21	31	2.1	4.9	5.8	4.3	0	1	1	N 7	N 3	NW 5
7	102.0	100.6	100.4	101.0	2.3	3.5	2.5	2.7	6.1	1.6	15	26	11	17	6.1	5.8	6.5	6.3	6	1	1	WSW 2	SSW 4	W 2
8	101.7	103.2	103.6	102.8	4.9	5.2	5.1	5.1	7.5	1.3	0	12	7	6	8.6	7.8	8.1	8.2	7	7	1	NNW 3	SW 1	SW 3
9	103.1	102.8	101.0	102.3	4.5	5.5	3.2	4.1	7.3	2.9	0	19	20	13	8.2	7.3	6.1	7.2	3	1	5	W 1	SSW 2	SSW 4
10	98.0	97.1	94.5	96.5	-0.3	0.6	-0.4	-0.1	3.5	-2.1	41	70	71	61	3.5	1.9	1.7	2.4	1	5	10	SSE 3	SW 2	C 0
11	88.8	85.2	81.1	85.0	-1.9	-2.4	-4.7	-3.4	0.1	-4.7	100	100	98	99	0.0	0.0	0.1	0.0	10 *≡	10 *	10*≡	NE 2	NE 3	S 3
12	79.1	79.6	81.1	79.9	-6.4	-8.3	-9.6	-8.5	-4.3	-9.8	97	98	94	96	0.1	0.1	0.2	0.1	10△≡	10△≡	8	SSE 7	SW 6	NNE 1
13	82.0	82.3	83.5	82.6	-8.6	-6.1	-5.8	-6.6	-5.5	-10.9	95	97	95	96	0.2	0.1	0.2	0.2	9	10*△	9	S 3	SSE 7	SSW 2
14	83.2	84.1	85.1	84.1	-6.8	-5.6	-8.7	-7.4	-3.4	-8.8	91	97	98	95	0.3	0.1	0.1	0.2	9	7	10*≡	NNE 4	SSE 4	S 6
15	85.8	87.7	89.6	87.7	-12.4	-12.4	-15.2	-13.8	-8.6	-15.6	96	96	91	94	0.1	0.1	0.2	0.1	10 ≡	5	5	SSW 2	WSW 8	WSW 4
16	91.9	93.1	94.2	93.1	-19.5	-17.3	-16.3	-17.4	-14.8	-20.0	95	95	95	95	0.1	0.1	0.1	0.1	10*≡	10△≡	0	W 7	NNW 7	N 6
17	94.1	93.2	90.4	92.6	-14.2	-8.6	-10.0	-10.7	-7.8	-16.7	79	86	41	69	0.4	0.4	1.7	0.8	3	1	3	WNW 5	SSW 3	S 8
18	87.3	86.1	84.2	85.9	-8.2	-2.8	-5.0	-5.2	-2.7	-12.0	95	100	98	98	0.2	0.0	0.1	0.1	9	10*≡	10 ≡	SSW 6	S 9	SSW10
19	85.0	84.7	84.3	84.7	-4.7	-3.4	-4.3	-4.2	-3.1	-5.6	88	97	91	92	0.5	0.2	0.4	0.4	4	9	2	SSW 3	SSW 9	SSE13
20	82.5	82.7	82.8	82.7	-2.8	-2.0	-3.8	-3.1	-1.0	-5.2	100	98	96	98	0.0	0.1	0.2	0.1	10*△≡	10△≡	10 ≡	SSE12	S 3	S 6
21	76.9	74.0	73.9	74.9	-2.8	-1.5	-4.0	-3.1	-1.0	-5.3	97	99	96	97	0.1	0.1	0.2	0.1	10*△≡	10*△≡	10*△≡	SSE15	SSW17	SSW 9
22	77.1	82.8	85.4	81.8	-7.5	-9.6	-9.6	-9.1	-3.7	-10.2	96	98	91	95	0.1	0.1	0.3	0.2	10	8	2	WSW13	NW 2	S 4
23	86.1	87.1	89.1	87.4	-16.7	-16.8	-16.2	-16.5	-9.5	-17.7	95	95	48	79	0.1	0.1	0.9	0.4	10 *≡	10*△	10	N 7	N 8	W 9
24	90.6	90.5	89.7	90.3	-15.0	-12.8	-13.0	-13.4	-12.0	-16.7	31	36	31	33	1.3	1.5	1.6	1.5	5	1	1	NNE 7	NE 5	ENE 1
25	89.5	90.9	91.5	90.6	-13.0	-10.8	-12.3	-12.1	-10.4	-13.9	84	97	85	89	0.4	0.1	0.4	0.3	2	10 *	0	WSW 5	W 8	SSW 3
26	87.8	85.6	84.8	86.1	-12.6	-9.1	-7.4	-9.1	-6.3	-13.3	89	95	96	93	0.3	0.2	0.1	0.2	8	10 ≡	10 ≡	S 17	SSE18	SSW11
27	83.5	75.8	70.4	76.6	-6.0	-4.6	-3.1	-4.2	-2.8	-7.4	97	96	99	97	0.1	0.2	0.0	0.1	10*≡	10*△≡	10△≡	SSW13	S 17	S 19
28	72.3	73.5	78.7	74.8	-5.9	-10.4	-10.6	-9.4	-2.5	-11.1	97	97	97	97	0.1	0.1	0.1	0.1	10*△≡	9	10*≡	W 8	SW 6	W 7
29	82.7	85.2	78.0	82.0	-11.5	-11.5	-8.6	-10.0	-8.2	-12.1	97	93	92	94	0.1	0.2	0.3	0.2	8 *	9	10*△≡	SSW 9	SSW14	SSE30
30	78.5	78.6	78.4	78.5	-4.4	-4.7	-6.8	-5.7	-3.0	-8.7	98	98	96	97	0.1	0.1	0.1	0.1	10*△≡	10*△≡	10*≡	SSE22	SE 18	SSE 3
31																								
M	88.7	88.8	88.5	88.7	-6.3	-5.1	-5.7	-5.7	-2.7	-8.5	76	81	74	77	1.3	1.2	1.4	1.3	7.4	7.5	6.5	7.9	7.4	7.3

Grudzień – Décembre

1	80.3	81.8	84.8	82.3	-12.2	-10.7	-10.2	-10.8	-6.5	-12.4	96	94	94	95	0.1	0.2	0.2	0.2	1	10*≡	10*△≡	S 12	S 15	SSW14
2	86.0	86.8	84.9	85.9	-10.6	-10.0	-11.6	-11.0	-9.7	-11.9	94	97	89	93	0.2	0.1	0.3	0.2	10*△≡	10 ≡	0	S 12	S 8	SSE11
3	80.6	78.9	77.9	79.1	-10.3	-10.0	-9.6	-9.9	-5.8	-12.2	71	94	94	86	0.8	0.2	0.2	0.4	9	10 ≡	9*△	S 17	SSW18	SW 11
4	80.5	82.4	83.9	82.3	-8.5	-7.6	-8.1	-8.1	-7.2	-9.6	95	99	98	97	0.2	0.0	0.1	0.1	9	10*≡	10*≡	WSW 8	SSW 6	SSW15
5	85.7	84.3	80.5	83.5	-8.5	-8.1	-7.6	-8.0	-7.2	-9.3	98	95	96	96	0.1	0.2	0.1	0.1	10 ≡	10≡	10	S 14	S 17	SSE25
6	80.7	83.5	86.5	83.6	-4.0	-5.6	-7.1	-6.0	-1.2	-7.9	99	97	91	96	0.1	0.1	0.3	0.2	10*△≡	9△	6	SSW14	WSW 9	SSW16
7	88.5	90.4	90.9	89.9	-6.7	-5.8	-6.8	-6.5	-5.1	-7.9	91	85	96	91	0.3	0.6	0.1	0.3	9	9	10 *	SSW13	WSW12	S 9
8	90.6	90.4	93.3	91.4	-7.2	-8.3	-10.3	-9.0	-6.6	-10.3	96	98	97	97	0.1	0.1	0.1	0.1	10*≡	10*≡	10*≡	SSW 3	N 5	NW 6
9	95.3	93.0	88.3	92.2	-11.6	-8.9	-10.1	-10.2	-7.3	-12.5	65	73	91	76	0.9	0.8	0.3	0.7	9	4	2	C 0	SSE17	S 16
10	73.1	72.4	72.6	72.7	-5.6	-4.2	-6.0	-5.4	-3.8	-10.6	95	98	97	97	0.2	0.1	0.1	0.1	10 ≡	10*△≡	9	SSE30	SSW22	S 11
11	73.4	74.2	76.0	74.5	-7.6	-9.3	-11.9	-10.2	-6.0	-12.2	99	95	95	96	0.0	0.2	0.2	0.1	10*≡	10*△≡	10 ≡	WSW 1	NNW 4	NNW 6
12	77.9	79.9	82.8	80.2	-10.9	-10.4	-11.2	-10.9	-9.7	-12.7	94	94	97	95	0.2	0.2	0.1	0.2	10*△≡	10*≡	10*≡	N 12	N 10	NNW 7
13	84.7	86.0	84.7	85.1	-12.5	-10.8	-10.7	-11.2	-9.7	-12.5	96	94	94	95	0.1	0.2	0.2	0.2	10 ≡	9	10 *	NNW 4	W 5	S 10
14	83.9	87.8	92.3	88.0	-9.9	-14.7	-18.2	-15.2	-5.5	-18.6	94	100	95	96	0.2	0.0	0.1	0.1	10△≡	10*≡	9	NNW 9	N 15	N 14
15	95.2	93.9	92.9	94.0	-12.9	-10.3	-10.0	-10.8	-9.3	-18.6	88	94	94	92	0.3	0.2	0.2	0.2	10	10*△≡	10*△≡	NW 7	WNW10	NNW 8
16	91.2	90.7	91.3	91.1	-12.6	-13.6	-13.8	-13.4	-9.8	-14.2	92	100	96	96	0.2	0.0	0.1	0.1	8	10 ≡	0	N 4	N 6	WNW 5
17	91.6	91.9	91.8	91.8	-8.4	-6.1	-5.7	-6.5	-4.0	-14.1	95	97	97	96	0.2	0.1	0.1	0.1	9	8	10 ≡	WSW10	WSW16	WSW 8
18	93.2	94.1	97.0	94.8	-6.5	-2.3	-0.3	-2.4	0.6	-7.3	97	100	100	99	0.1	0.0	0.0	0.0	8	10*△	10*△≡	SSW 7	WSW11	W 8
19	98.2	98.9	98.7	98.6	1.7	2.2	5.4	3.7	5.7	-0.3	100	88	36	75	0.0	0.9	5.8	2.2	9 •	9	5	W 12	W 17	W 17
20	97.5	96.4	95.5	96.3	1.8	0.1	0.6	0.8	6.2	-1.1	80	98	92	90	1.5	0.2	0.5	0.7	9	9	8	WSW17	WSW11	WSW 6
21	91.0	90.1	90.3	90.5	-2.5	-2.8	-4.1	-3.4	1.0	-4.2	100	100	98	99	0.0	0.0	0.1	0.0	10*≡	10 ≡	9	SSW10	SE 2	SSE 1
22	90.3	90.1	89.5	90.0	-9.1	-9.8	-12.0	-10.7	-2.9	-12.3	95	94	95	94	0.2	0.2	0.2	0.2	10△≡	10*△≡	9	N 4	NNE 6	NNE 7
23	87.7	86.6	83.1	85.8	-11.3	-8.1	-11.4	-10.6	-7.1	-12.9	93	95	97	95	0.2	0.2	0.1	0.2	7 *	1	10 ≡	NE 5	S 6	SSE 8
24	78.5	78.3	76.6	77.8	-12.8	-9.3	-9.5	-10.3	-8.5	-13.0	92	98	94	95	0.2	0.1	0.2	0.2	5	7	8	S 13	S 7	SSW 7
25	73.0	72.4	72.9	72.8	-8.8	-6.9	-6.5	-7.2	-5.8	-11.9	95	96	94	95	0.2	0.1	0.2	0.2	10	5	9	SSE17	S 8	SSW 3
26	73.4	75.4	79.1	76.0	-6.0	-4.9	-10.2	-7.8	-4.7	-10.4	97	93	97	96	0.1	0.3	0.1	0.2	8	4	10*≡	WSW 6	SW 7	NNW 5
27	83.3	81.7	77.7	80.9	-11.1	-9.0	-6.2	-8.1	-6.0	-12.9	76	95	97	89	0.6	0.2	0.1	0.3	0	9	10 ≡	SW 8	S 16	S 18
28	76.2	78.7	82.8	79.2	-4.6	-6.7	-10.9	-8.3	-3.8	-11.0	98	96	94	96	0.1	0.1	0.2	0.1	10 *	10△≡	2	W 9	WSW 9	W 10
29	84.9	87.2	90.2	87.4	-14.6	-12.9	-13.8	-13.8	-10.7	-15.0	83	81	51	72	0.3	0.4	1.0	0.6	8	5	3	NNW 2	W 9	NNW 9
30	88.5	86.2	86.4	87.0	-11.0	-10.1	-8.1	-9.3	-7.3	-14.6	39	72	92	68	1.6	0.8	0.2	0.9	2	5	10 *	SSW19	S 17	SSE13
31	85.9	85.7	86.0	85.9	-7.6	-8.4	-10.0	-9.0	-6.8	-10.5	93	92	91	92	0.2	0.3	0.3	0.3	10	8	9	WSW 7	WSW 8	W 5
M	85.2	85.5	85.8	85.5	-8.5	-7.8	-8.6	-8.4	-5.3	-11.1	90	94	91	92	0.3	0.2	0.4	0.3	8.4	8.4	8.0	9.9	10.6	9.9

Kasprowy Wierch H_s = 1991 m H_b = 1988,8 m h_w = 15,4 m *Listopad - Novembre 1965*

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	8	0.2	2	*^0 0^00–2^15, 3^40–5^15 △^0 8^10–9^23 *△^0–10^15 *▽^0 10^50–11^15 •^0 21^15–23^30. V^0 0^00–3^30, 5^30–6^15, 6^35–8^30; ≡^2 0^00–3^30 ≡–5^30, 6^15, 6^35–8^30, 12^30–13^30. ⋙ 0^00–2^00 (por. 18), 5^15–12^30 (por. 23) ⇶–24 (por. 37); ⊹^0 0^00–1^30, 5^15–11^30.
2	8	0.0	2	*△^0 7^10–8^15 *▽^0 10^45–56, 14^03, 15^50–55; ≡ 7^30–8^30; ⇶ 0^00–7^30 (por. 37) ⋙–10^40 (por. 27), 11^10–13^40 (por. 26) ⇶–17^10 (por. 35) ⋙–24 (por. 30) **[1.XI:** () 15^30–20^50
3	9	0.9	pł.	*▽^{1-0} 16^40–19^35, 20^15–25 *▽^1–20^35 *▽^0 21^15, 23^10–25. V^0 16^30–24; ≡ 15^45–16^30 ≡^2–21^45 ≡–24; ⋙ 0^00–9^15 (por. 27), 17^50–19^30 (por. 18), 20^20–22^05 (por. 18); () 11^30–15^30
4	0	•	1	V^0 0^00–40, 8^05–15, 8^45–9^20, 12^15–15^05, 16^05...30; ≡ 0^00–40 ▥ 3^30–8^05 ≡–8^15 ≡^2–9^00 ≡–9^20 ▥–11^20 ≡–12^15 ≡^2–13^00 ≡–13^05 ≡^2–13^30 ≡–15^05 ▥–16^05 ≡–16^30 ▥–24; ⊕^0 15^18–25 ⊽^0 17^30–20^15; () 15^30–24
5	9	•	1	▥ 0^00–23^30; () 0^00–24
6	9	•	1	() 0^00–24
7	9	•	pł.	⌣^1 23^30–24; () 0^00–24
8	9	•	pł.	⌣^1 0^00–15; () 0^00–24
9	9	•	pł.	⊽^0 18^45–19^30; () 0^00–24
10	9	2.6	pł.	(▥) 3^30–6^30 ▥–13^00 ≡ 7^45–9^45, 12^58, 14^30 ≡^2–16^15 ▥–22^00; ⊽^2 17^30–19^30, ⌾^2 11^30–12^45; () 0^00–9^00
11	6	8.2	5	*^{0-1} 1^10–21^30 *^0 22^40–23^15. V^0 3^15–8^30, 12^05–24; ≡^2 3^15–8^30 ≡ 12^05–18^50 ≡^1–20^50 ≡^2–24
12	0	0.8	17	△^0 1^35–16^30. V^0 0^00–5^00 V^1–9^10 V^0–18^45, 21^45–24; ≡^2 0^00–18^30 ≡–18^45, 21^45–24; ⊹^0 3^30–13^30; ⌣^0 22^50–24
13	6	0.7	17	*^0 9^30–11^30 *△^0–16^45, V^0 0^00–2^20; ≡ 0^00–2^20 ▥–10^30 ≡ 16^10–19^30 (▥)–24, ⌣^0 0^00–2^20 ⊽^1–6^10
14	9	1.1	19	*^0 19^10–22^20. V^0 14^30–24, (▥) 0^00–4^30 ▥–14^30 ≡ 12^30–14^30 ≡^2–24; ⌣^0 1^30–3^30 ⊕^0 7^30–11^00; ⌾^2 11^30–12^15; () 7^30–14^30
15	8	0.8	18	*▽^{0-1} 8^50–10^15 *^0 17^45–18^25; V^0 0^00 na V^1–6^45 V^0 8^30–11^40, 14^50–24; ≡^2 0^00–6^45 ≡–12^30, 14^50–15^45 ≡^2–16^05 ≡–16^20 ≡^2–18^25 ≡–24
16	0	1.0	19	*^0 2^45–4^15–8^10 *△^0–11^30 △^0–19^15. V^{0-1} 0^00–20^15; ≡ 0^00–4^10 ≡^2–6^50 ≡–12^30 ≡^2–13^30 ≡–15^40 ≡^2–20^15 ▥–21^30 (▥)–24
17	9	•	19	(▥) 0^00–9^30 ▥ 12^30–24; () 6^00–24
18	1	1.9	19	*^0 12^25–18^10. V^{0-1} 1^15–5^30, 9^40 p V^2 p–22^15. ▥ 0^00–1^15 ≡^2–5^30 ≡–6^15, 9^40 ≡^2–22^15 ≡–22^30; ⋙ 0^30–2^30, 14^10–22^15; ⊹^0 0^30–5^30, 14^00–22^00; () 0^00–1^15, 5^30–9^40
19	9	3.6	17	V^0 14^30–16^15, 18^55–19^15, 23^30–24; ≡ 10^25, 11^10, 11^35...50, 12^05, 16^15, 18^55, 19^15, 22^45, 23^30 ≡^2 24; ⋙ 12^45–14^00 (por. 15), 16^10–24 (por. 24); ⊹^0 16^10–17^30, 20^00–24; ⊘^1 13^50; ⊽^0 4^30–6^00; () 8^30–12^20, 15^30–23^30
20	0	12.3	19	△^{0-1} 1^40–3^30 *△^{0-1} 11^30 △^{1-0} 20^05. V^{0-1} 0^00–24; ≡^2 0^00–30 ≡–1^15 ≡^2–14^40 ≡–18^30 ≡^2–22^30 ≡–24; ⋙ 0^00–2^00 (por. 19), 5^30–8^30 (por. 17); ⊹^0 0^00–11^40, 21^40–24
21	0	26.5	25	△^0 5^55–6^10 *△^0–18^10, 20^30–24; V^{0-1} 0^00–18^10, 19^30–24; ≡ 0^00–1^15 ≡^2–18^10, 19^30–24; ⋙ 2^15–8^30 (por. 26) ⇶–14^10 (por. 31) ⋙ 17^20–18^30 (por. 18), 22^30–24 (por. 16); ⊹^{0-1} 0^00–24
22	8	1.9	43	*△^0 0^00–30, 1^30–4^30 △^0 7^30–8^30 *▽^0–9^10 V^{0-1} 0^00–30, 1^30–4^30, 8^30–12^05, 23^20–24; ≡^2 0^00–30, 1^30–4^30 ≡–7^10 ≡^2–9^10 ≡–10^30 ≡^2–12^05 ≡–13^30 ▥–23^20 ≡ 15^40–16^30 ≡^2–24; ⋙ 0^00–1^40 (por. 18), 3^15–7^40 (por. 21);
23	9	0.4	46	*▽^1 3^05–5^30 *▽^0–9^05 *^0–12^30 *△^0–14^10 *^0 15^30–17^30. V^0 0^00 na V^1–9^30; ≡^2 0^00–9^05 ≡–12^10; ⋙ 9^50–10^10, 13^30–15^30; ⊹^{0-1} 17^30–18^10 ⊹^0–24; () 9^30–20^30 **[22.XI:** ⊹^{0-1} 0^00–8^30 ⌾^1 13^30–15^40
24	9	•	47	⊹^0 0^00–2^30; () 4^30–24
25	7	0.2	47	*▽^0 3^05–9^40, 10^25...13^15 *▽^{0-1} 14^30; ⊔^0 19^00–24; ≡ 11^30–14^45; ⋙ 23^45–24; () 0^00–6^45
26	0	4.5	45	*△^{0-1} 23^30–24; ⊔^0 0^00–2^00 V^0 7^40 a V^1 a–22^30, 23^30–24; ≡ 7^00–40 ≡^2 22^30 ≡–23^30; ⋙ 0^00–2^30 ⇶–10^05 ⋙–11^00 ⇶–18^20 (por. 25) ⋙–24; ⊹^{0-1} 2^00–24
27	0	23.6	47	*△^{0-1} 0^00–30, 6^20–8^45 △^0–10^30 *△^0–17^30 △^{0-1} 21^00 *△^{0-1}–24; V^0 1^00–24; ≡^2 0^00–24; ⋙ 0^00–1^30, 5^30–12^15 (por. 32) ⇶–24 (por. 35); ⊹^{0-1} 0^00–12^00 ⊹^{1-2} 24
28	7	3.7	60	*△^{0-1} 0^00–2^15 *^{1-0} 5^30 *△^{0-1} 9^30 △^0–10^15 *▽^0 13^30–15^10 *▽^{0-1} 16^15–20^50, 21^50–24. V^{1-0} 0^00–10^05, 11^45–24; ≡^2 0^00–3^05 ≡–5^10 ≡^2–7^40 ≡–10^05, 11^45–17^15 ≡^2–24; ⇶ 0^00–1^30 (por. 20) ⋙ 15^30–17^40 (por. 23), 18^40–19^15 (por. 19);
29	7	1.5	61	*▽^{0-1} 0^00–7^10 *△^0 20^30–24; V^{0-1} 0^00–9^30, 11^20–13^30, 20^30–24; ≡^2 0^00–6^20 ≡–9^30, 11^20–13^30 ≡^2–24; ⋙ 7^30–13^15 (por. 16) ⇶–14^30 (por. 22) ⋙–15^20 ⇶–24 (por. 53); ⊹^{0-1} 0^00–2^40, 3^50–11^30 ⊹^{0-2} 24;
30	0	11.4	55	*△^0 0^00–8^30 *△^{1-0} 16^30 *^1–18^50 *^0–23^30 *△^0–24. V^0 0^00–24; ≡^2 0^00–24; ⇶ 0^00–13^30 (por. 47) ⋙–14^15 (por. 16); ⊹^{1-2} 0^00–13^30 ⊹^{1-0} 16^30 **[28.XI:** ⊹^1 0^00–1^30 ⊹^0 3^05–9^30, 12^45–24
31				**[29.XI:** () 10^30–12^20, 12^30–16^30
Σ	–	107.6	–	

Grudzień - Décembre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	P O G O D A
1	0	2.6	60	*△^0 0^00–1^10 △^0 ...3^30 *▽^{0-1} 8^10–13^15 *△^0 16^50–24. V^0 0^00–5^20, 8^30–24; ≡^2 0^00–5^20 ≡ 7^45–8^30 ≡^2–10^40 ≡–12^10 ≡^2–14^45 ≡–16^30 ≡^2–24; ⋙ 6^00–7^35 ⇶–8^30 ⋙–9^15 (por. 19) ⇶–10^35 (por. 23) ⋙–12^45 (por. 22) ⇶–14^40 (por. 25) ⋙–24 (por. 24).
2	1	0.6	58	*△^0 0^00–2^10, 4^45–5^20, 6^20–10^05 *^0 11^20–12^10. V^0 0^00–14^10; ≡^2 0^00–2^20 ≡–3^15 ≡^2–10^05 ≡–11^20 ≡^2–14^05 ≡ 14^10–15^20, 21^30–22^15, 23^20–24; ⋙ 0^00–10^15 (por. 22), 19^25–22^30 ⇶–24 (por. 30); ⊹^{0-1} 0^00–12^00, 22^30–24; ⌾ 14^10...15^10
3	0	2.5	56	*^0 9^40–10^30 *△^0 13^30–19^45, 20^30–24. V^{0-1} 10^40–19^30, 20^20–24; ≡ 0^00–2^15 ≡^2 10^40–19^30 ≡–20^50 ≡^2–21^40 ≡–22^30 ≡^2–24; ⇶ 0^00–7^45 (por. 40) ⋙–11^30 (por. 22) ⇶–16^30 (por. 24) ⋙–23^20 (por. 20); ⊹^{1-2} 0^00–24
4	1	2.7	59	*△^0 0^00–3^30 *^0 7^20–9^30 *▽^{1-0} 11^40–13^15, 17^25–24. V^1 0^00–2^30 V^0 11^45, 13^30–19^30–24; ≡^2 0^00–1^30 ≡–2^30, 10^40–11^45 ≡^2–13^25 ≡–16^30, 17^20–19^30 ≡^2–24; ⋙ 19^26–24 (por. 21); ⊹^{0-1} 0^00–7^30, 19^20–24 **[1.XII:** ⊹^0 3^30–12^45 ⊹–14^40 ⊹^{1-0} 24
5	0	2.8	56	*▽^0 0^00–1^20 *△^0 21^15–24. V^0 0^00 na V^1 a V^2 a–10^15 V^0 14^30 V^0 15^15–24; ≡^2 0^00–13^45 ≡–14^30, 15^15–21^50 ≡^2–24; ⋙ 0^00–1^25 (por. 26) ⇶–24 (por. 51); ⊹^1 0^00–12^20 ⊹^2–24; () 14^30–16^45
6	8	0.4	50	*△^2 0^00–7^20, 8^30–10^50 △^2–12^50. V^0 0^00–4^30 V^1 10^30 V^0 12^50; ≡^2 0^00–10^30 ≡–12^50 ⇶ 0^00–8^05 (por. 33) ⋙–8^40 (por. 22), 10^00–13^50 (por. 22) ⇶...15^30 (por. 29) ⋙–16^05 (por. 25) ⇶ ...21^20 (por. 26) ⋙–24 (por. 22); ⊹^2 0^00–6^10 ⊹^1–9^30 ⊹^{0-1} 24
7	9	2.7	45	*^0 1^40–15^30–24. V^1 10^40–11^30, 15^30–24; ≡ 10^40–11^30, 15^30–16^20 ≡^2–20^20 ≡–22^30 ≡^2–24; ⋙ 0^00–16^10 (por. 29); ⊹^{0-1} 0^00–8^30, 19^40–22^30, ⊽^0 2^30–5^15; () 7^30–10^40, 11^30–15^30
8	0	9.2	48	*^0 0^00–5^30 *^{0-1} 21^05. V^{0-1} 0^00–30, 3^30–21^05, 23^35–24; ≡^2 0^00–30, 3^30–21^05 ≡–22^30 ≡^2 23^35–24
9	9	•	58	V^0 0^00–45, 22^45–24; ≡^2 0^00–15 ≡–2^30, 22^45–24; ⋙ 8^30–10^45 ⇶–24 (por. 36); ⊹^0 7^30–8^30 ⊹^1–24; ⊽^2 4^20–6^45; () 8^30–23^30
10	0	(6.1)	50	△^0 6^50–11^30 *△^0–18^50; V^{0-1} 0^00–20^50; ≡ 0^00–15 ≡^2–1^40 ≡–4^30 ≡^2–19^30 ≡–20^50; ⇶ 0^00–17^30 (por. 52) ⋙–18^40 (por. 17), 19^00–22^15; ⊹^1 0^00–1^30 ⊹^2 17^30 ⊹^{1-0} 22^15; ⌣^1 20^15–21^30 ⊽^0 21^30–22^00
11	0	4.9	51	*^0 6^15–7^30 *△^0–12^10 *△^{0-1} 17^30, 19^30–20^15; V^0 3^30–24; ≡^2 3^30–24
12	0	10.2	58	*△^{0-1} 4^30–9^00 *^1–11^30 *^{1-2} 18^00 *^0–22^15, 23^30–24; V^{0-1} 0^00–22^15, 23^30–24; ≡^2 0^00–22^15 ≡–23^30 ≡^2–24; ⋙ 6^10–12^45; ⊹^0 0^30–22^00
13	8	1.9	65	*^0 0^00–1^20 *▽^0 8^15–35, 8^50–9^05 *^{0-1} 20^20–22^30. V^1 0^00–9^30 V^0 12^10–30, 19^35–24; ≡^2 0^00–3^20 ≡–4^15 ≡^2 5^30–9^15 ≡–9^30, 12^10–30, 19^35–21^10 ≡^2–24; ⋙ 18^40–24 (por. 22); ⊹^0 19^10–24
14	0	15.9	64	*^{0-1} 0^45–8^15 △^{1-2} 8^50 *△^1–8^30 *△^0–12^15 *▽^{1-0} 18^30 *^0–20^20. V^{0-1} 0^00–21^15; ≡^2 0^00–20^30 ≡–21^15; ⋙ 0^00–30 ⇶–3^20 (por. 23) ⋙–4^40 (por. 20), 7^10–12^40 ⇶–14^30 ⋙–24; ⊹^1 0^00–3^50 ⊹^0–6^15 ⊹^{1-0} 24. ⤧^{0-1} 1^50–2^10
15	0	6.7	68	*△^0 8^40–19^30 *△^{0-1} 24. V^{0-1} 10^30–24; ≡^2 10^30–24; ⋙ 0^00...3^00, 8^30–12^50, 16^30–20^10; ⊹^0 0^00–4^30, 8^30–22^30; ⌣^0 2^30–3^30 ⊽^0 4^15–5^50
16	1	0.4	76	*△^{0-1} 0^00–6^20 *^0 13^05–15^40, 18^20–20^15. V^{0-1} 0^00–6^45, 12^30–23^15; ≡^2 0^00–6^25 ≡–6^45, 12^20–35 ≡^2–13^45 ≡–15^50 ≡^2 17^30–20^00 ≡–20^30, 21^30–22^30 ≡^2–23^15; ⊹^0 2^30–5^30; () 7^00–12^20
17	8	2.2	74	*^0 3^40–5^15, 6^45–7^20, 10^15–12^10 *△^{0-1} 14^10–19^15. V^0 13^45–19^45, 20^10–24; ≡ 8^30–9^15, 13^45–16^20 ≡^2–19^15 ≡–19^45, 20^10–20 ≡^2–24; ⋙ 6^00–8^15 (por. 18), 9^30–12^25 (por. 19) ⇶–12^45 (por. 23) ⋙–20^10 (por. 23); ⊹^0 6^00–24
18	5	7.0	75	⟶^0 10^50–11^30 △^0–12^10 *△^0–22^30 •^0–23^40; V^0 0^00–1^35, 8^05–18^00 V^{1-0} 22^30; ≡^2 0^00–45 ≡–1^35, 8^05–9^10 ≡^2–11^20 ≡–13^30 ≡^2–24; ⋙ 9^00–18^00 (por. 22), 22^50–24 (por. 19); ⊹^0 0^00–1^20 ⊹^{0-1} 11^20–19^30
19	9	1.8	68	•^{1-0} 1^30–3^00 •^{0-1} 5^30 •^0 6^40 •^0 7^50–11^15 •^0 13^30–14^20, 15^45–16^30; ≡^2 0^00–5^30 ≡–6^15, 6^50–7^15 ≡^2–11^15; ⋙ 0^00–10^30 (por. 24) ⇶ 12^20–45 (por. 30) ⋙–13^10 (por. 23) ⇶–21^10 (por. 41) ⋙–22^30 (por. 27) ⇶–24 (por. 31); () 11^30–15^30, 18^30–24
20	8	0.4	62	V^0 14^20–18^30; ≡ 10^20–13^30 ≡^2 13^50–18^25 ≡–19^30, 22^20–23^30; ⇶ 0^00–6^50 ⋙–8^40 (por. 23), 10^30...15^15; () 0^00–9^30
21	0	2.2	58	*^0 3^40–7^15 △^0 8^30–9^20, 10^40–11^15, 16^45–18^30. V^0 0^40–24; ≡^2 0^40–9^40 ≡–10^30 ≡^2–12^50, 13^15–19^50 ≡–22^10 ≡^2–24; ⋙ 2^45–7^40 (por. 18), 8^10–10^20 (por. 22); ⊹^0 6^00–7^40, 8^30–9^20
22	0	5.9	59	△^0 3^45–6^05 *▽^0 11^30 *△^0 20^20. V^0 0^00–20^30; ≡^2 0^00–20^30; ⊹^0 21^30–24
23	9	0.0	67	*^0 0^20–4^30, 6^15–7^20. V^{0-1} 1^30–2^30, 16^20–23^30; ≡^2 1^30–2^30 ▥ 7^20–16^20 ≡ 13^30–50, 14^15, 16^20 ≡^2–19^30 ≡–20^15 ≡^2–23^30 ≡–24; ⊹^0 0^00–6^30; ⌾^0 8^30–11^00
24	9	2.3	64	*^0 14^52, 16^10–19^30. V^0 1^40–2^30, 9^15–11^30, 12^30–21^30; ≡ 0^00–1^40 ≡^2–2^30 ≡–8^20, 9^15–11^30, 12^30–17^10 ≡^2–18^40 ≡–21^30; ⋙ 4^30–11^10, 23^40–24; ⊹^0 4^30–5^30, ⊹^1–9^40 ⊹^0–11^15, 23^45–24
25	9	0.1	64	V^0 4^40–10^25; ≡ 4^40–10^25 ▥–16^30 ≡ 14^40–15^30, 18^40–20^20; ⋙ 0^00–3^35 ⇶–6^45 (por. 30) ⋙–11^30 (por. 19); ⊹^0 0^00–3^30 ⊹^1–6^45 ⊹^0–12^30; () 9^30–24
26	9	4.5	62	*^0 3^45–4^10 *▽^0 15^15–17^30 *▽^{1-0} *▽^0 18^15–22^40. V^2 2^30–4^20, 13^35 np V^1 np–24; ≡^2 2^30–4^20, 13^35–15^15 ≡–16^30 ≡^2–17^20 ≡–18^15 ≡^2–24; ⋙ 17^00–18^10, 22^45–24 (por. 17); ⊹^{0-1} 22^45–24; () 0^00–2^30, 4^20–13^30
27	7	5.3	65	*▽^0 0^40–1^20, 2^15–25 *▽^1 22^45–23^15 *▽^0–24; V^1 0^00–2^30 V^0 13^40–14^10, 16^20–20^10 V^1–24; ≡^2 0^00–2^30 ≡–4^15, 13^40–14^10, 16^20–40 ≡^2–24; ⋙ 0^00–40, 9^30–12^20 (por. 23) ⇶–24 (por. 50); ⊹^0 0^00...2^25, 8^00–9^40 ⊹^1–12^30
28	1	1.5	68	*▽^0 0^00–20 *^{1-0} 0^20–9^30 △^0 20^10; V^{1-0} 0^00–20^10; ≡^2 0^00–6^20 ≡–10^30 ≡^2–13^30 ≡–14^10 ≡^2–15^40 ≡–18^30 ≡^2–19^45 ≡–20^10 ▥–23^30 ⇶ 0^00–2^30 (por. 31) ⋙–5^30 (por. 28), 6^50–7^15, 13^10–21^15 (por. 20); ⊹^1 0^00–5^30
29	9	•	68	▥ na–np. ⋙ 13^00–16^30, 20^45–24 (por. 19); ⊹^{0-1} 13^00–24; () 6^30–24 **[27.XII:** ⊹^2 19^30 ⊹^3–22^45 ⊹^2–24; () 8^30–10^30; ⤧^0 22^45–24 **[28.XII:** ⊹^{1-0} 21^30
30	9	0.8	63	*^{0-1} 18^40–21^30 *△^0–22^45 △^0–24. V^0 20^15–24; ≡ 18^45–19^30 ≡^2–20^30 ≡–22^45 ≡^2–23^40 ≡–24; ⋙ 0^00–5^00 (por. 20) ⇶–19^30 (por. 39) ⋙–21^15; ⊹^0 0^00–3^30 ⊹^{1-2} 19^30 ⊹^{1-0} 24; () 0^00–16^30
31	8	0.0	61	△^0 0^00–30, 1^40–2^40, 7^30–9^10. V^0 0^00–2^45, 7^15–10^40, 18^40–19^30; ≡ 0^00–2^45, 6^15–7^15 ≡^{0-2} 9^30 ≡–10^40, 18^40–19^30; ⋙ 4^15–40, 4^45–5^30; ⊹^0 2^40–5^30
Σ	–	101.6	–	

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1965

TABLICA II

WYNIKI MIESIĘCZNE I ROCZNE SPOSTRZEŻEŃ METEOROLOGICZNYCH

RÉSULTATS MENSUELS ET ANNUELS
DES OBSERVATIONS MÉTÉOROLOGIQUES

Rozewie — φ = 54°50′ — λ = 18°20′ — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	1.8	−1.9	4.8	1, 17	−9.1	11	−0.2	0.9	0.2	0.3	5.2	5.4	5.2	5.3	85	81	83	83	0.9	1.3	1.1	1.1	7.4	7.2	7.0	7.2
II	—	—	—	—	0.2	−4.2	3.2	13	−10.8	6	−2.0	−0.9	−1.8	−1.6	4.4	4.5	4.3	4.4	81	78	80	80	1.0	1.3	1.1	1.1	8.1	7.2	7.2	7.5
III	—	—	—	—	4.1	−2.3	11.9	29	−12.4	8	−0.7	2.9	0.6	0.8	5.2	5.8	5.4	5.5	86	76	83	82	0.8	1.9	1.1	1.3	5.8	5.9	5.2	5.6
IV	—	—	—	—	6.8	1.9	10.8	18	−2.5	3	3.6	5.7	4.2	4.4	7.0	7.4	7.1	7.2	88	80	85	84	0.9	1.9	1.3	1.4	7.3	6.8	6.1	6.7
V	—	—	—	—	10.1	4.3	17.0	17	0.9	31	7.2	9.0	6.4	7.2	8.5	8.9	8.4	8.6	83	77	86	82	1.7	2.7	1.4	1.9	5.1	4.4	4.5	4.7
VI	—	—	—	—	16.6	10.2	27.2	26	5.4	4	13.3	15.3	12.7	13.5	12.6	12.8	12.1	12.5	82	75	82	80	2.9	5.3	2.8	3.7	5.7	4.4	4.8	5.0
VII	—	—	—	—	16.9	11.4	23.7	15	7.7	6	14.0	15.4	13.2	14.0	13.9	13.9	13.6	13.8	87	79	89	85	2.1	3.7	1.7	2.5	6.4	7.1	6.1	6.5
VIII	—	—	—	—	18.1	11.5	27.8	6	8.1	31	14.0	17.1	14.1	14.8	13.9	14.5	13.7	14.0	87	75	85	82	2.2	5.4	2.6	3.4	5.3	5.6	4.7	5.2
IX	—	—	—	—	17.6	11.3	25.2	18	7.8	16	12.7	16.4	13.5	14.0	13.0	14.0	13.5	13.5	88	75	87	83	1.8	4.9	2.1	2.9	5.1	4.8	3.7	4.5
X	—	—	—	—	12.2	7.3	16.6	1	2.8	22	9.1	11.6	9.3	9.8	9.9	10.6	9.8	10.1	85	77	83	82	1.7	3.2	2.0	2.3	7.1	6.5	3.8	5.8
XI	—	—	—	—	3.1	−1.5	11.4	1, 2	−13.5	18	0.6	1.5	0.7	0.9	5.7	6.0	5.9	5.9	84	83	86	84	1.1	1.3	0.9	1.1	7.9	8.0	6.8	7.6
XII	—	—	—	—	2.4	−1.5	10.4	19	−10.9	17	0.4	1.3	0.7	0.8	5.5	5.8	5.7	5.7	85	85	87	86	0.9	1.0	0.8	0.9	8.5	7.8	7.5	7.9
Rok	—	—	—	—	9.2	3.9	27.8	6.VIII	−13.5	18.XI	6.0	8.0	6.2	6.6	8.7	9.1	8.7	8.8	85	78	85	83	1.5	2.8	1.6	2.0	6.6	6.3	5.6	6.2

Łeba — φ = 54°46′ — λ = 17°34′

I	—	—	—	—	2.2	−2.1	5.7	17	−11.3	11	−0.2	1.4	0.2	0.4	5.2	5.5	5.2	5.3	85	81	84	83	0.9	1.3	1.0	1.1	8.5	8.0	7.2	7.9
II	—	—	—	—	0.8	−4.2	4.1	11	−11.4	17	−1.7	0.0	−1.5	−1.2	4.4	4.5	4.2	4.4	80	72	75	76	1.1	1.7	1.4	1.4	8.8	8.0	7.2	8.0
III	—	—	—	—	4.8	−2.6	10.6	18	−13.1	8	−1.2	3.6	0.4	0.8	5.0	5.6	5.4	5.3	85	71	82	79	0.8	2.5	1.1	1.5	6.7	6.6	5.4	6.2
IV	—	—	—	—	8.8	2.3	15.6	6	−1.8	5	4.1	7.2	4.7	5.2	7.2	7.5	7.3	7.3	87	74	85	82	1.1	2.9	1.4	1.8	7.7	7.7	6.6	7.3
V	—	—	—	—	10.8	3.9	17.4	17	−2.7	2	7.4	9.4	6.9	7.7	8.6	8.6	8.6	8.6	83	73	85	80	1.8	3.3	1.5	2.2	5.7	5.5	5.0	5.4
VI	—	—	—	—	18.1	9.8	30.5	26	3.8	15	13.2	16.5	13.0	13.9	12.6	12.5	12.7	12.6	83	68	85	79	2.9	7.4	2.5	4.3	5.8	5.4	4.6	5.3
VII	—	—	—	—	17.6	11.4	25.1	20	6.6	5	13.8	15.9	13.9	14.4	14.0	13.7	14.0	13.9	88	76	88	84	2.0	4.6	2.0	2.9	7.2	7.6	6.6	7.1
VIII	—	—	—	—	18.9	10.7	29.1	23	5.9	18	13.8	17.8	13.7	14.8	13.8	14.2	14.0	14.0	87	71	89	82	2.1	6.6	1.8	3.5	6.1	6.3	4.3	5.6
IX	—	—	—	—	18.5	10.4	25.6	3, 18	4.6	16	12.3	17.7	13.1	14.0	13.2	14.8	14.0	14.0	92	74	92	86	1.2	5.8	1.2	2.7	5.6	5.6	4.2	5.1
X	—	—	—	—	12.6	6.1	17.0	1	−0.5	20	8.0	11.8	8.8	9.4	9.7	10.9	9.7	10.1	89	79	85	84	1.3	3.0	1.8	2.0	7.2	7.8	4.9	6.6
XI	—	—	—	—	3.2	−2.4	11.5	1, 2	−15.4	18	0.1	1.8	0.5	0.7	5.4	6.0	5.8	5.7	82	80	84	82	1.2	1.4	1.0	1.2	8.2	8.4	6.5	7.7
XII	—	—	—	—	2.4	−1.3	9.6	19	−11.3	17	0.3	1.4	0.7	0.8	5.5	5.7	5.7	5.6	85	83	86	85	0.9	1.1	0.9	1.0	8.4	8.9	8.3	8.5
Rok	—	—	—	—	9.9	3.5	30.5	26.VI	−15.4	18.XI	5.8	8.7	6.2	6.7	8.7	9.1	8.9	8.9	86	75	85	82	1.4	3.5	1.5	2.1	7.2	7.2	5.9	6.8

Puck — φ = 54°43′ — λ = 18°25′

I	—	—	—	—	2.4	−1.5	6.0	1	−9.6	11	0.0	1.1	0.6	0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.9	8.0	7.8
II	—	—	—	—	−0.3	−4.4	4.3	13	−9.8	6	−2.5	−1.1	−2.0	−1.9	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.4	9.0	8.8
III	—	—	—	—	4.5	−2.5	12.7	29	−13.8	9	−0.2	2.9	1.1	1.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	7.9	2.4	10.8	16, 26	−3.0	3	4.3	6.4	5.2	5.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	11.4	5.1	18.4	17	−0.8	2	8.2	9.8	7.9	8.4	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.9	6.3	5.5
VI	—	—	—	—	18.5	10.9	28.1	17, 26	5.8	15	14.2	16.9	14.3	14.9	—	—	—	—	—	—	—	—	—	—	—	—	6.0	5.3	6.1	5.8
VII	—	—	—	—	18.2	11.6	23.2	13	7.9	11	14.5	16.1	14.1	14.7	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.8	7.5	7.5
VIII	—	—	—	—	19.2	11.1	28.3	6	7.5	17	14.2	17.3	15.0	15.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	18.4	11.1	25.1	18	7.9	16	13.0	16.7	14.2	14.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.8	6.7	16.4	1	2.1	21	8.4	11.7	9.5	9.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	3.5	−1.7	12.3	2	−13.5	18	0.2	1.4	1.0	0.9	—	—	—	—	—	—	—	—	—	—	—	—	9.1	9.3	8.1	8.8
XII	—	—	—	—	3.0	−1.4	11.5	19	−10.3	17	0.3	1.2	0.5	0.6	—	—	—	—	—	—	—	—	—	—	—	—	9.0	9.1	8.5	8.9
Rok	—	—	—	—	10.0	4.0	28.3	6.VIII	−13.8	9. III	6.2	8.4	6.8	7.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Hel — φ = 54°36′ — λ = 18°49′

I	1009.6	1026.4	985.3	1008.9	2.2	−1.2	5.4	1	−8.0	11	0.4	1.2	0.7	0.7	5.6	5.6	5.5	5.6	88	83	86	86	0.8	1.2	0.9	1.0	8.6	8.4	7.9	8.3
II	1014.2	1036.4	981.5	1014.5	0.4	−4.1	4.0	13	−9.7	17	−1.8	−0.4	−1.9	−1.5	4.6	4.8	4.4	4.6	85	80	82	82	0.8	1.2	1.0	1.0	8.6	7.5	7.9	8.0
III	1015.5	1032.4	989.4	1015.8	3.5	−2.3	10.7	29	−8.7	8	−0.5	2.7	0.5	0.8	5.4	5.7	5.7	5.6	90	76	89	85	0.6	1.9	0.7	1.1	6.2	6.5	6.0	6.2
IV	1011.7	1031.9	992.9	1012.0	7.8	2.2	12.1	28	−3.0	3	3.8	6.7	4.2	4.7	7.2	7.6	7.4	7.4	89	77	89	85	0.8	2.4	0.9	1.4	8.2	7.7	7.0	7.6
V	1014.3	1030.5	988.6	1014.6	12.0	4.6	17.0	27	−0.4	31	7.5	10.7	6.7	7.9	8.7	8.6	8.6	8.6	83	67	87	79	1.7	4.4	1.3	2.5	5.6	5.3	5.2	5.4
VI	1013.3	1021.5	1000.8	1013.6	18.1	10.1	26.0	26	1.8	4	13.0	17.0	12.6	13.8	13.0	12.9	12.7	12.9	86	67	86	80	2.1	6.9	2.0	3.7	6.0	4.8	5.3	5.4
VII	1009.3	1023.0	992.0	1009.6	18.4	12.2	23.2	15	9.2	5	14.4	16.9	14.0	14.8	14.1	14.0	14.0	14.0	85	73	87	82	2.5	5.5	2.1	3.4	6.5	7.5	6.8	6.9
VIII	1014.0	1022.3	1004.3	1014.3	19.3	11.6	26.5	22	7.0	18	14.1	18.0	14.0	15.0	14.6	14.5	14.2	14.4	90	70	88	83	1.6	6.5	1.9	3.3	6.1	6.5	4.9	5.8
IX	1012.6	1031.7	1000.9	1012.9	17.9	11.8	21.4	10, 18	9.4	25	13.2	16.8	13.8	14.4	13.8	14.6	14.2	14.2	91	76	89	85	1.4	4.7	1.7	2.6	6.0	5.4	4.3	5.2
X	1021.0	1036.3	1001.9	1021.3	12.6	7.2	16.6	7	1.9	26	9.2	11.9	9.3	9.9	10.4	10.7	10.2	10.4	89	77	86	84	1.3	3.3	1.7	2.1	8.0	7.7	4.7	6.8
XI	1010.1	1028.9	979.3	1010.4	3.4	−0.4	11.6	2	−8.4	18	0.8	1.8	1.4	1.4	5.9	6.2	6.2	6.1	87	85	85	86	0.9	1.1	0.9	1.0	9.1	8.7	7.2	8.3
XII	1001.4	1022.5	972.8	1001.7	2.9	−0.3	8.2	19	−7.8	18	1.1	1.8	1.3	1.4	5.9	5.9	6.0	5.9	87	84	87	86	0.8	1.1	0.9	0.9	8.9	8.0	8.9	8.6
Rok	1012.2	1036.4	972.8	1012.5	9.9	4.3	26.5	22.VIII	−9.7	17. II	6.3	8.8	6.4	7.0	9.1	9.3	9.1	9.2	88	76	87	84	1.3	3.4	1.3	2.0	7.3	7.0	6.3	6.9

Rozewie

$H_s = 54\,m$ $h_w = 19\,m$ **1965**

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v v>10	v>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	5	10.7	8	5.4	5	6.0	8.5	4.1	19	4.4	31	5.3	11.5	5.9	3	6.5	2	5.3	29	4.8	8	·	5	24	·	8	2	2	12	19	11	·	6	14	·
II	18.5	7.8	17	6.9	0.5	5.0	1.5	6.3	6	2.9	8	3.7	13.5	6.7	18	7.4	1	6.5	45	8.0	27	1	12	26	·	11	5	·	14	23	14	·	2	25	·
III	2.5	4.0	12.5	6.0	7.5	5.2	7	3.9	11.5	3.4	24	3.4	20	6.1	7	6.2	1	4.7	21	10.0	3	2	7	22	·	5	1	4	9	11	4	1	7	15	·
IV	5	2.7	18.5	4.2	13.5	4.4	13	6.2	18.5	4.2	6.5	2.8	9.5	5.3	4.5	4.2	1	4.4	35	11.6	21	·	·	7	·	2	1	1	12	14	7	1	9	·	·
V	10.5	3.0	23.5	3.7	11.5	4.1	7.5	6.2	1.5	5.3	4	2.4	12.5	5.1	12	4.0	10	3.7	39	8.0	9	·	·	·	·	·	·	9	4	11	9	·	9	·	1
VI	2	3.0	14.5	3.6	10	3.4	6	4.0	10.5	3.8	7	3.3	24	6.0	14	6.3	2	4.6	87	26.9	22	·	·	·	2	4	2	5	4	11	10	3	5	·	3
VII	3	2.7	7.5	5.1	8.5	3.1	4.5	2.2	5.5	2.6	25.5	4.1	27.5	6.0	8	5.9	3	4.5	172	21.0	15	·	·	·	·	3	·	3	10	25	24	7	3	·	5
VIII	12.5	3.6	1	4.0	2	1.5	6	3.9	10	4.3	16.5	2.3	21	3.0	13	4.8	11	3.0	122	51.8	24	·	·	·	3	·	·	2	7	14	13	3	3	·	4
IX	4.5	3.9	3.5	4.3	6	4.0	11.5	3.8	14	3.9	19	5.6	20.5	5.9	7	6.0	4	4.7	104	38.5	4	·	·	·	1	5	1	9	5	14	11	4	2	·	4
X	15	5.0	5.5	3.1	5	4.6	0.5	5.0	4	2.9	20.5	4.9	21	5.5	14.5	5.9	7	4.6	30	8.8	31	·	·	·	·	5	1	3	4	7	5	·	4	·	·
XI	3.5	4.9	14.5	6.4	12	5.5	6	6.6	13.5	8.9	18	6.2	15.5	6.2	6	6.2	1	6.5	71	8.6	3	1	10	18	·	11	3	1	13	22	14	·	·	18	·
XII	2.5	5.0	3	2.3	·	·	3.5	8.4	16	6.4	36.5	6.1	24.5	6.1	7	5.3	·	6.0	71	13.7	19	1	2	23	·	9	2	1	19	22	12	2	4	13	·
Rok	84.5	4.7	129	4.6	81.5	3.9	75.5	5.0	130	4.4	216.5	4.2	221	5.6	114	5.7	43	4.9	826	51.8	24. VIII	5	36	120	6	63	18	40	113	193	134	21	54	85	17

Łeba

$H_s = 2\,m$ $h_w = 21{,}5\,m$

I	3	3.2	6	3.6	8	5.1	13	2.9	22.5	4.2	28.5	4.2	2.5	4.4	9.5	5.7	·	4.2	46	9.4	8	1	3	24	·	1	·	1	18	21	13	·	3	12	·
II	12.5	6.1	16	6.2	4	4.5	3	2.5	3	4.5	13	4.5	6.5	3.8	25	4.8	1	5.0	41	6.1	27	1	8	24	·	10	·	·	17	23	12	·	3	26	·
III	2.5	2.8	17	4.4	8.5	4.1	3.5	2.7	15	2.4	24.5	2.5	9.5	3.0	10.5	3.1	2	3.1	24	9.2	3	2	5	22	·	1	·	4	11	15	8	·	4	16	·
IV	5.5	3.3	15	3.3	14.5	4.4	14	4.0	13.5	2.8	5.5	2.8	13.5	2.7	7.5	1.5	1	3.2	33	7.2	26	·	·	4	·	·	·	3	13	17	8	·	8	·	·
V	8	2.2	30.5	3.1	12.5	3.6	8.5	4.5	2.5	1.6	9.5	1.9	12.5	2.8	9	2.9	·	3.0	55	14.4	9	·	·	3	·	·	·	6	8	11	10	1	8	·	·
VI	3	3.3	15.5	3.0	7.5	3.7	3	3.8	9.5	5.2	13.5	3.9	26.5	4.1	11.5	3.0	·	3.8	50	16.6	22	·	·	·	4	6	·	4	5	10	9	3	6	·	5
VII	1.5	2.0	10	4.2	7.5	2.7	5.5	2.1	5.5	3.2	35.5	4.3	23	4.4	3.5	2.4	1	3.9	215	47.3	12	·	·	·	1	·	·	3	15	26	23	5	3	·	6
VIII	11	2.4	7	1.6	2	1.5	6	3.8	12	2.7	12	2.8	19.5	2.4	20.5	2.8	3	2.5	46	9.8	27	·	·	·	4	·	·	5	7	15	8	·	4	·	2
IX	2	3.0	1	2.0	14.5	2.7	11.5	3.6	16.5	3.1	24	4.4	12.5	3.5	6	2.8	2	3.4	97	16.2	6	·	·	·	2	2	·	7	6	17	14	3	3	·	5
X	15.5	3.3	3.5	3.0	4	3.2	3.5	2.1	12	2.6	21	4.4	13	3.8	17.5	3.4	3	3.4	40	17.2	29	·	·	1	·	1	·	1	8	9	6	2	8	·	·
XI	4	5.5	4.5	5.7	14.5	3.8	14.5	3.4	19.5	4.3	18.5	4.9	7	5.0	7.5	3.6	·	4.3	75	16.6	3	3	10	18	·	5	1	1	17	24	14	2	2	19	1
XII	2.5	4.4	2.5	2.8	·	·	9	4.5	20.5	4.2	37	4.4	14.5	4.4	7	3.6	·	4.3	106	24.4	18	2	3	21	·	1	1	·	18	24	17	2	2	12	·
Rok	71	3.5	128.5	3.6	97.5	3.3	95	3.3	152	3.4	242.5	3.8	160.5	3.7	135	3.3	13	3.7	828	47.3	12. VII	9	29	117	11	27	2	35	143	212	142	18	54	85	19

Puck

$H_s = 1\,m$ $h_w = 14\,m$

I	·	·	5	3.6	4	4.5	9	4.4	2	3.5	17	5.5	7	4.0	9	7.7	40	2.9	25	6.2	4	·	1	21	·	3	·	2	19	12	8	·	2	16	·
II	7	9.4	21	7.8	3	6.0	1	5.0	·	·	11	3.7	12	6.1	14	7.5	15	5.6	40	5.5	7	·	14	25	·	12	·	·	21	19	12	·	·	28	·
III	2	7.0	12	5.8	6	7.7	6	3.2	·	·	9	3.6	17	4.9	3	6.7	38	3.1	21	9.0	3	2	6	23	·	4	·	—	—	11	6	·	2	21	·
IV	6	4.8	12	7.2	14	6.5	27	5.1	·	·	4	2.0	10	3.5	4	5.5	13	4.6	48	14.0	21	·	·	3	·	4	·	—	—	13	9	1	2	·	·
V	7	6.0	27	4.6	11	8.5	10	6.5	·	·	1	3.0	18	4.7	6	6.3	13	4.8	31	7.0	10	·	·	1	·	8	·	8	10	11	9	·	4	·	·
VI	4	4.2	10	6.2	12	5.2	11	5.0	1	7.0	7	4.0	26	6.9	6	4.2	13	4.8	96	29.2	22	·	·	·	4	7	1	4	8	11	8	4	2	·	3
VII	·	·	11	5.3	7	3.6	5	3.4	·	·	32	5.9	24	6.2	·	·	14	4.7	161	19.2	15	·	·	·	·	7	1	3	15	24	22	7	·	·	6
VIII	4	5.5	5	4.6	4	3.2	9	4.9	·	·	5	4.2	26	3.9	9	4.9	31	2.9	117	32.0	24	·	·	·	4	1	1	—	—	15	12	4	·	·	4
IX	·	·	3	3.0	8	5.2	15	5.5	·	·	25	4.6	11	4.9	3	8.7	25	3.7	105[2]	33.0	4	·	·	·	1	3	1	—	—	10	10	4	2	·	1
X	6	7.3	2	3.0	5	4.6	2	2.0	·	·	9	4.1	27	4.9	11	5.5	31	3.3	27	11.4	29	·	·	·	·	4	1	—	—	8	6	1	5	·	·
XI	2	8.0	9	5.3	12	7.5	7	4.1	6	11.3	11	6.5	19	3.8	3	3.0	21	4.5	66	13.3	3	2	10	19	·	7	1	·	23	18	13	1	2	17	·
XII	·	·	1	2.0	·	·	15	8.1	1	4.0	36	6.9	21	4.4	3	7.3	16	5.3	89	30.8	6	1	3	20	·	10	1	·	22	16	10	3	1	12	·
Rok	38	4.4	118	4.9	86	5.2	117	4.8	10	2.2	167	4.5	218	4.8	71	5.6	270	4.2	826[1]	33.0	4. IX	5	34	112	9	70	7	—	—	168	125	25	22	94	14

Hel

$H_s = 1\,m$ $H_b = 26\,m$ $h_w = 24\,m$

I	2.5	4.2	7	4.1	5.5	5.2	11.5	4.7	24.5	6.4	18	6.4	11.5	5.6	8.5	5.8	4	5.5	27	4.5	21	·	5	22	·	13	·	·	19	18	8	·	2	12	·
II	14	6.5	11	6.8	4	4.5	4.5	3.0	6	4.8	7.5	6.6	15.5	5.7	19.5	5.5	2	5.6	39	5.9	27	·	10	26	·	10	·	·	15	21	15	·	·	26	·
III	3.5	5.1	12.5	6.0	8	3.9	9.5	3.2	24.5	3.2	11.5	2.4	13.5	5.1	6	4.4	4	3.8	24	8.5	3	·	6	21	·	3	·	5	11	12	7	·	5	19	·
IV	8.5	3.9	15	5.8	9	5.5	19	3.8	13.5	3.7	2	3.5	9.5	3.1	6.5	3.2	8	3.8	45	13.5	21	·	·	6	·	5	·	1	16	16	13	1	3	·	·
V	16	4.6	18	4.4	12.5	4.4	6	5.1	2.5	4.2	1	1.5	14.5	3.9	11.5	4.0	11	3.8	33	11.9	17	·	·	2	·	3	·	5	6	11	8	1	4	·	1
VI	6.5	4.6	18	4.8	8	2.8	5.5	3.0	10	3.8	4	3.1	20	5.0	12	4.1	6	3.9	62	22.8	22	·	·	·	1	6	·	6	8	12	9	2	3	·	4
VII	3.5	5.0	12	6.0	7	3.4	5.5	3.0	7	4.8	25.5	5.8	27.5	6.4	3	6.0	2	5.4	110	19.5	23	·	·	·	·	11	·	3	11	24	21	4	1	·	10
VIII	9	2.8	2.5	2.8	4	2.1	10	3.8	7	4.1	7	3.9	22.5	4.5	20	4.4	11	3.5	77	20.8	27	·	·	·	2	1	·	4	10	13	11	4	2	·	3
IX	1.5	2.0	6	3.8	12.5	3.8	9.5	3.6	19	4.0	17.5	5.7	17.5	4.8	5.5	4.9	1	4.4	108	56.1	4	·	·	·	·	8	·	7	7	11	10	3	·	·	2
X	8.5	4.6	4.5	2.3	4.5	4.8	1.5	4.3	10.5	3.7	13	6.3	25	5.7	19.5	5.0	6	4.7	18	8.3	29	·	·	·	·	5	·	1	9	8	3	·	1	·	·
XI	3.5	3.0	7.6	6.0	18	5.7	6	7.2	14	7.5	12	8.1	19.5	6.7	6.5	4.2	3	6.3	46	8.5	22	·	10	17	·	16	·	·	18	21	10	·	4	14	·
XII	2	2.2	1	2.0	·	·	4.5	8.6	24.5	7.1	30	7.1	24.5	6.7	6.5	4.7	·	6.5	38	10.9	29	·	3	13	·	11	1	·	20	15	9	1	1	7	·
Rok	79	4.0	115	4.6	93	3.8	93	4.4	163	4.8	149	5.0	221	5.2	124	4.7	58	4.8	627	56.1	4. IX	·	34	107	3	92	1	32	150	182	124	16	26	78	20

Uwaga. Kierunki i prędkości wiatru – wg anemometru Chauvin Arnoux.

Ustka — φ = 54°35' — λ = 16°52' — 1965

MIESIĄC	CIŚNIENIE p: P_m	Max	Min	$P_{o.m}$	TEMPERATURA T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	1008.5	1025.7	983.8	1009.6	2.5	−1.3	5.9	17	−10.2	11	0.1	1.6	0.6	0.7	5.5	5.9	5.6	5.7	88	85	87	87	0.8	1.0	0.8	0.9	7.5	8.1	7.1	7.6
II	1014.9	1035.3	982.0	1016.0	0.8	−3.7	4.3	13	−10.6	17	−1.6	0.0	−1.4	−1.1	4.5	5.0	4.5	4.7	82	81	79	81	1.0	1.1	1.1	1.1	7.7	7.9	7.3	7.6
III	1014.9	1031.2	991.0	1016.0	4.7	−1.8	11.6	29,30	−12.7	8	−0.8	3.3	0.9	1.1	5.3	5.9	5.6	5.6	88	75	83	82	0.7	2.1	1.1	1.3	6.8	6.7	5.2	6.2
IV	1010.5	1031.9	988.6	1011.5	9.6	2.6	15.9	6	−2.4	5	4.2	7.7	5.3	5.6	7.3	7.6	7.4	7.4	88	73	83	81	1.1	3.2	1.7	2.0	7.4	7.9	6.3	7.2
V	1013.6	1028.9	991.6	1014.6	11.0	4.4	17.3	17	−2.0	3	7.3	9.3	7.4	7.9	8.7	8.9	8.6	8.7	85	76	82	81	1.6	3.0	1.9	2.2	5.5	5.4	5.0	5.3
VI	1012.9	1022.4	997.5	1013.9	17.7	10.1	30.1	26	4.0	4	13.2	16.2	13.0	13.8	12.4	12.6	12.5	12.5	82	71	83	79	3.0	6.9	2.7	4.2	4.7	6.3	4.7	5.2
VII	1008.5	1021.7	990.6	1009.5	17.3	11.4	25.3	20	7.2	5	13.7	15.5	14.1	14.4	13.9	13.6	14.0	13.8	88	77	87	84	1.9	4.4	2.2	2.8	7.1	6.8	5.7	6.5
VIII	1013.6	1022.7	1002.6	1014.6	16.6	11.2	28.1	22	6.6	17	13.8	17.4	14.1	14.8	13.8	14.3	14.0	14.0	87	73	87	82	2.1	6.0	2.1	3.4	6.5	6.4	4.3	5.7
IX	1011.5	1031.4	998.6	1012.5	18.3	10.6	27.3	3	6.4	16	12.0	17.4	13.3	14.0	12.8	13.8	13.7	13.4	91	71	89	84	1.3	6.5	1.8	3.2	6.1	6.4	4.2	5.6
X	1020.7	1035.6	1001.2	1021.7	12.4	6.5	17.9	2	0.4	20	7.8	11.6	9.2	9.4	9.5	10.8	9.9	10.1	89	79	85	84	1.3	3.0	1.8	2.0	7.2	7.1	3.9	6.1
XI	1009.0	1028.4	977.8	1010.1	3.2	−1.9	11.8	1	−12.8	18	0.3	2.1	0.7	1.0	5.7	6.1	5.9	5.9	86	80	85	84	1.0	1.4	1.0	1.1	7.9	8.1	6.6	7.5
XII	1000.1	1022.5	970.4	1001.2	2.9	−0.5	11.0	19	−7.0	17	0.8	1.6	1.3	1.2	5.7	5.9	6.1	5.9	86	84	89	86	0.9	1.0	0.7	0.9	8.3	8.8	8.9	8.7
Rok	1011.6	1035.6	970.4	1012.6	9.9	4.0	30.1	26.VI	−12.8	18.XI	5.9	8.6	6.5	6.9	8.8	9.2	9.0	9.0	87	77	85	83	1.4	3.3	1.6	2.1	6.9	7.2	5.8	6.6

Lębork — φ = 54°33' — λ = 17°45'

I	—	—	—	—	2.4	−1.7	6.3	17	−11.8	11	−0.3	1.4	0.5	0.5	5.4	5.6	5.5	5.5	89	82	85	85	0.7	1.2	0.9	0.9	8.3	8.3	7.8	8.1
II	—	—	—	—	0.2	−6.6	4.5	11	−16.3	24	−3.8	−0.7	−3.2	−2.7	4.2	4.7	4.2	4.4	86	80	85	84	0.6	1.1	0.7	0.8	8.2	8.1	8.1	8.1
III	—	—	—	—	5.4	−3.7	11.6	15	−19.2	8	−1.7	4.3	0.6	1.0	5.2	5.9	5.6	5.6	90	70	84	81	0.6	2.8	1.0	1.5	6.5	6.8	5.9	6.4
IV	—	—	—	—	10.6	2.4	15.7	6	−3.4	1	4.2	9.4	5.7	6.2	7.3	7.6	7.4	7.4	87	65	81	78	1.3	4.4	1.9	2.5	7.9	8.0	6.8	7.6
V	—	—	—	—	13.4	3.6	19.0	28	−4.6	3	7.4	12.4	7.7	8.8	8.6	8.3	8.5	8.5	83	58	80	74	1.8	6.3	2.2	3.4	6.0	6.8	5.5	6.1
VI	—	—	—	—	20.2	9.3	30.4	26	2.5	5	14.0	18.9	14.2	15.3	13.2	13.0	12.7	13.0	83	60	78	74	3.0	9.9	3.8	5.6	6.4	7.1	5.0	6.2
VII	—	—	—	—	19.0	11.0	26.4	15	5.6	5	13.8	17.2	14.2	14.8	14.0	13.7	14.0	13.9	88	70	86	81	2.0	6.6	2.5	3.7	6.9	8.0	6.1	7.0
VIII	—	—	—	—	19.9	9.9	29.1	23	4.4	17	12.8	18.6	13.6	14.6	13.4	13.9	13.8	13.7	91	66	89	82	1.6	8.2	2.1	4.0	6.8	7.8	5.4	6.7
IX	—	—	—	—	19.5	10.2	26.9	3	2.5	16	12.1	18.4	13.3	14.3	12.7	14.1	13.5	13.4	90	67	88	82	1.6	7.6	1.9	3.7	6.2	6.1	4.6	5.6
X	—	—	—	—	13.0	4.7	20.3	1	−0.4	19,20	6.6	12.4	7.6	8.6	9.3	10.7	9.5	9.8	93	74	90	86	0.7	3.9	1.1	1.9	7.6	8.3	5.2	7.0
XI	—	—	—	—	2.5	−3.1	11.8	1	−16.3	18	−0.8	1.3	−0.2	0.0	5.4	6.0	5.7	5.7	87	83	87	86	0.8	1.2	0.8	0.9	8.3	8.7	7.4	8.1
XII	—	—	—	—	2.7	−1.5	11.6	19	−16.4	17	0.4	1.7	0.9	1.0	5.6	5.8	5.7	5.7	86	83	86	85	0.9	1.2	0.9	1.0	8.6	9.2	9.3	9.0
Rok	—	—	—	—	10.7	2.9	30.4	26.VI	−19.2	8.III	5.4	9.6	6.2	6.8	8.7	9.1	8.8	8.9	88	72	85	82	1.3	4.5	1.6	2.5	7.3	7.8	6.4	7.2

Gdynia — φ = 54°31' — λ = 18°34'

I	1007.9	1024.6	983.7	1009.7	2.6	−1.6	6.3	17	−8.4	11	0.3	1.2	0.6	0.7	5.2	5.4	5.3	5.3	83	79	82	81	1.1	1.4	1.2	1.2	8.1	8.2	7.3	7.9
II	1012.9	1034.2	980.5	1014.7	0.8	−3.8	4.8	13	−9.3	6	−2.1	−0.6	−1.9	−1.6	4.2	4.4	4.1	4.2	78	74	76	76	1.1	1.5	1.3	1.3	8.1	8.2	7.9	8.1
III	1013.7	1030.2	988.4	1015.5	4.7	−1.3	14.0	29	−10.0	8	−0.1	2.8	1.1	1.2	5.1	5.5	5.4	5.3	82	72	79	78	1.1	2.2	1.4	1.6	6.2	6.7	5.8	6.2
IV	1010.1	1029.5	991.1	1011.9	7.6	2.9	11.0	30	−1.2	5	3.9	6.0	4.9	4.9	6.9	7.1	7.2	7.1	85	76	82	81	1.2	2.3	1.6	1.7	8.8	8.0	6.7	7.8
V	1012.7	1028.3	987.4	1014.4	11.4	5.8	18.4	17	1.0	2	8.2	9.6	7.9	8.4	8.5	8.3	8.6	8.5	77	69	80	75	2.5	3.9	2.2	2.9	5.6	6.3	6.5	6.1
VI	1011.8	1020.2	998.4	1013.5	18.2	11.4	26.6	26	6.7	4	13.8	16.2	14.3	14.6	12.3	12.4	12.5	12.4	78	69	76	74	3.7	6.3	3.9	4.6	6.5	6.2	5.5	6.1
VII	1007.8	1021.4	990.3	1009.4	18.5	12.6	22.8	22	9.3	6	14.3	16.8	14.7	15.1	13.3	13.2	13.8	13.4	81	69	82	77	3.1	6.1	3.0	4.1	6.5	7.6	7.2	7.1
VII	1012.6	1020.8	1003.0	1014.2	19.3	12.4	27.4	6	9.3	16	14.3	17.6	14.9	15.4	13.7	13.6	14.0	13.8	84	68	82	78	2.7	6.8	3.1	4.2	6.1	7.2	4.6	6.0
IX	1011.1	1029.5	999.6	1012.8	18.5	12.2	23.2	18	9.6	12	13.2	16.9	14.4	14.7	13.0	13.6	13.6	13.4	85	71	82	79	2.3	5.8	2.9	3.7	6.2	5.7	4.0	5.3
X	1019.5	1034.3	1000.7	1021.2	13.2	7.6	17.2	7	3.2	26	8.9	12.3	9.7	10.2	9.7	10.1	9.8	9.9	84	70	81	78	1.8	4.4	2.3	2.8	7.3	7.0	4.9	6.4
XI	1008.5	1026.9	976.6	1010.2	3.7	−1.1	12.4	1	−11.7	18	0.5	1.6	1.2	1.1	5.5	5.7	5.7	5.6	81	79	81	80	1.3	1.7	1.4	1.5	8.7	8.6	7.2	8.2
XII	999.9	1020.9	971.5	1001.7	3.4	−0.5	10.8	19	−10.4	18	0.9	1.8	1.4	1.4	5.5	5.6	5.6	5.6	83	78	81	81	1.2	1.5	1.3	1.3	9.0	8.1	7.7	8.3
Rok	1010.7	1034.3	971.5	1012.4	10.2	4.7	27.4	6.VIII	−11.7	18.XI	6.3	8.5	6.9	7.2	8.6	8.7	8.8	8.7	82	73	80	78	1.9	3.7	2.1	2.6	7.3	7.3	6.3	7.0

Słupsk — φ = 54°28' — λ = 17°01'

I	—	—	—	—	2.5	−0.7	6.4	17	−11.8	11	−0.3	1.4	0.3	0.4	5.4	5.7	5.5	5.5	89	84	88	87	0.7	1.1	0.8	0.9	7.2	6.9	7.2	7.1
II	—	—	—	—	0.9	−6.3	4.3	11,13	−13.7	17	−3.1	−0.1	−3.0	−2.3	4.4	5.1	4.3	4.6	88	83	85	85	0.6	1.0	0.7	0.8	7.5	7.5	7.2	7.4
III	—	—	—	—	5.7	−3.5	12.0	29	−19.8	8	−2.0	4.3	0.4	0.8	5.1	6.1	5.7	5.6	90	74	87	84	0.6	2.5	0.9	1.3	6.7	6.7	5.3	6.2
IV	—	—	—	—	10.9	2.7	16.1	6	−2.3	5	4.3	9.9	5.9	6.5	7.3	7.4	7.6	7.4	87	62	82	77	1.1	5.1	1.9	2.7	7.1	7.2	6.6	7.0
V	—	—	—	—	13.6	4.2	19.6	28	−2.8	3	7.7	12.4	7.8	8.9	8.8	8.9	8.7	8.8	82	62	81	75	1.9	5.8	2.1	3.3	5.8	6.2	4.6	5.5
VI	—	—	—	—	20.5	9.9	30.4	26	3.1	4	14.4	19.1	13.9	15.3	12.6	12.7	12.9	12.7	77	58	81	72	4.0	10.1	3.2	5.8	4.9	6.6	4.1	5.2
VII	—	—	—	—	18.8	10.8	26.1	14,15	5.4	5	13.7	17.1	13.7	14.6	14.2	13.9	14.3	14.1	90	71	90	84	1.6	6.1	1.6	3.1	7.3	7.4	5.9	6.9
VIII	—	—	—	—	20.3	9.9	28.5	23	4.9	17	13.0	18.8	13.2	14.6	13.6	14.3	14.2	14.0	91	65	93	83	1.6	8.3	1.2	3.7	6.1	7.0	3.7	5.6
IX	—	—	—	—	19.6	9.8	27.5	3	3.8	16	11.6	18.2	12.6	13.7	12.4	13.6	13.3	13.1	91	66	91	83	1.3	7.9	1.4	3.5	5.0	6.4	4.2	5.2
X	—	—	—	—	13.3	4.0	20.5	1	−1.8	12	5.9	12.3	7.1	8.1	9.0	10.6	9.3	9.6	94	73	92	86	0.6	4.0	0.9	1.8	7.5	6.5	5.0	6.3
XI	—	—	—	—	3.0	−2.6	12.1	1	−13.7	24	−0.9	1.8	0.0	0.2	5.5	6.2	5.8	5.8	90	84	88	87	0.6	1.1	0.7	0.8	8.4	8.0	7.2	7.9
XII	—	—	—	—	2.8	−1.0	11.4	19	−10.6	17	0.3	1.5	0.9	0.9	5.7	6.1	6.0	5.9	88	87	90	88	0.8	0.9	0.6	0.8	8.1	9.0	9.3	9.1
Rok	—	—	—	—	11.0	3.1	30.4	26.VI	−19.8	8.III	5.4	9.7	6.1	6.8	8.7	9.2	9.0	9.0	88	72	87	82	1.3	4.5	1.3	2.4	6.9	7.1	5.9	6.6

Ustka

$H_s = 6\,m$ $H_b = 8{,}1\,m$ $h_w =$ 17 m wiatromierz Wilda, 19,8 m anemometr

1965

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◔	◕	Opad R ≥0,1	≥5,0	≥10,0	≡	⊠	K (K)
I	6	3.8	1.5	2.3	12	3.1	15	3.0	27	4.9	18.5	5.3	3	8.0	5	5.8	5	4.2	43	6.7	8	1	2	21	·	2	1	1	15	23	15	·	3	15	·
II	14.5	6.1	17	6.3	5.5	3.1	7	3.1	6	2.0	11	5.5	4	6.0	19	6.0	·	5.3	51	7.7	27	1	7	23	·	8	·	·	13	21	14	·	3	28	·
III	3	2.8	13.5	4.9	7.5	3.0	6.5	2.5	26.5	2.9	10.5	3.9	17.5	4.8	3	3.2	5	3.5	39	22.7	3	1	4	21	·	4	·	6	11	13	8	1	7	17	·
IV	6.5	2.8	15.5	3.7	15	3.7	14.5	4.7	14	3.6	3	5.3	10.5	4.5	9	3.7	2	3.8	15	4.5	23	·	·	1	·	·	·	1	13	14	5	·	9	·	·
V	6.5	2.9	33.5	4.2	8	3.6	8.5	4.2	3.5	5.1	6	2.3	15	5.1	6	5.3	6	3.9	67	24.0	9	·	·	3	·	·	·	8	9	15	12	2	6	·	·
VI	4	3.2	18	4.1	3	1.7	7	3.9	7	5.1	4	3.5	32.5	5.8	9.5	4.2	5	4.4	53	22.7	18	·	·	·	4	2	·	4	6	9	8	1	3	·	3
VII	1	2.0	7	6.9	9	3.6	6	3.0	5.5	2.3	29.5	4.3	28	6.8	2	6.0	5	4.8	180	26.4	12	·	·	·	2	5	·	2	13	23	19	7	4	·	4
VIII	7.5	3.6	3.5	1.1	2	3.5	5	2.5	8	2.1	13	2.7	16	5.5	18	3.6	20	2.8	46	13.4	8	·	·	·	4	·	·	3	6	13	11	1	3	·	1
IX	2.5	1.8	0.5	1.0	7.5	2.9	13.5	3.3	15	3.4	20.5	3.5	15	4.5	9.5	5.3	6	3.5	99	28.7	6	·	·	·	2	1	·	4	6	16	13	3	·	·	3
X	9.5	3.4	6	2.9	2.5	2.0	4	3.0	14.5	2.3	16	3.6	15.5	5.2	12	3.6	13	3.0	32	11.7	29	·	·	·	·	·	·	3	5	9	5	1	5	·	·
XI	5	4.6	6.5	4.0	9.5	2.5	18.5	3.5	15	4.7	19	5.3	12	7.0	3.5	5.1	1	4.6	101	21.9	3	3	11	18	·	6	·	·	14	22	13	3	1	18	·
XII	3.5	4.9	·	·	1	4.0	12	5.0	14	4.2	42.5	5.8	11.5	5.6	7.5	4.7	1	5.2	103	13.3	9	·	2	17	·	4	·	·	22	24	19	5	2	14	·
Rok	69.5	3.5	122.5	3.4	82.5	3.1	117.5	3.5	156	3.6	193.5	4.2	180.5	5.7	104	4.7	69	4.1	829	28.7	6.IX	6	26	104	12	32	1	32	133	202	142	24	46	92	11

Uwaga. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru indukcyjnego Fuess.

Lębork

$H_s = 18\,m$ $h_w =$ 12 m wiatromierz Wilda, 13,5 m anemometr M-47

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◔	◕	Opad R ≥0,1	≥5,0	≥10,0	≡	⊠	K (K)
I	1	2.0	5.5	2.4	13.5	2.4	5	1.6	15.5	4.4	24.5	3.8	7.5	3.3	5.5	4.2	15	2.8	30	6.0	8	1	5	22	·	·	·	1	20	24	8	·	4	12	·
II	8	4.4	9	3.4	7	2.4	3	1.0	2	4.2	16	3.1	16.5	3.2	12.5	3.4	10	2.8	47	11.8	27	6	13	25	·	·	·	·	16	23	11	1	3	27	·
III	6	1.8	10	3.0	17	2.3	7.5	2.3	8.5	2.4	20	2.9	10	3.4	4	2.5	10	2.4	24	10.0	3	4	6	24	·	·	·	4	10	16	6	1	·	17	·
IV	3.5	3.3	13.5	3.3	17	3.9	15.5	3.0	9	2.9	7	3.1	10.5	2.9	4	2.2	10	2.9	33	8.7	23	·	·	6	·	·	·	·	15	12	8	·	2	·	·
V	4	2.5	17.5	3.1	19	3.2	7.5	3.2	1.5	2.3	4	2.8	16.5	3.8	8	3.4	15	2.7	50	11.4	7	·	·	4	·	·	·	4	11	13	9	1	4	·	1
VI	2	2.5	6.5	2.9	12	2.6	3.5	2.6	7.5	4.2	13.5	2.8	24.5	3.8	6.5	2.3	14	2.7	63	21.1	22	·	·	·	5	·	·	4	9	10	10	1	2	·	5
VII	1.5	1.0	6.5	1.5	8	2.5	7.5	2.2	2.5	2.4	32	3.2	24	3.6	1	3.0	10	2.6	191	34.5	15	·	·	·	3	·	·	3	12	26	25	5	·	·	6
VIII	6	2.1	2	1.0	7	1.0	3	3.3	4	3.2	18.5	1.4	20	1.6	10.5	1.6	22	1.3	89	22.1	24	·	·	·	5	·	·	1	11	14	11	3	3	·	4
IX	0.5	3.0	3	2.3	11.5	1.9	9	2.6	14	3.7	20	3.2	17.5	2.9	4.5	3.4	10	2.6	71	14.5	4	·	·	·	2	·	·	4	8	15	12	3	1	·	2
X	3	3.3	2.5	1.8	5.5	1.5	1.5	3.7	3	2.7	24	3.2	20	3.0	13.5	2.4	20	2.2	24	8.1	29	·	·	3	·	·	·	1	11	11	5	·	9	·	·
XI	2	5.0	7.5	2.4	17	1.9	5	4.2	10.5	4.1	20.5	5.0	14.5	3.1	2	2.0	11	3.1	74	15.2	2	4	11	20	·	·	·	1	20	21	12	2	4	19	·
XII	·	·	·	·	7	2.3	6	4.7	18	3.2	36	4.3	19	2.9	4	4.0	3	3.7	83	13.7	19	2	5	16	·	1	·	·	25	22	14	3	1	16	·
Rok	37.5	2.6	83.5	2.3	141.5	2.3	74	2.9	96	3.3	236	3.2	200.5	3.2	76	2.9	150	2.6	779	34.5	15.VII	17	40	120	15	1	·	23	168	207	131	20	33	91	18

Uwaga. Kierunki i prędkości wiatru w VIII – wg wiatromierza Wilda, w pozostałych miesiącach – wg anemometru M-47.

Gdynia

$H_s = 2\,m$ $H_b = 14{,}5\,m$ $h_w =$ 12,5 m wiatromierz Wilda, 25 m anemograf Dinesa

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◔	◕	Opad R ≥0,1	≥5,0	≥10,0	≡	⊠	K (K)
I	2	3.8	5.5	6.6	3.5	7.6	9	8.0	24	5.8	22.5	5.8	14	5.5	11.5	5.4	1	5.9	36	6.7	17	·	2	23	·	13	·	1	17	18	11	·	4	13	·
II	9.5	7.4	11.5	7.9	3.5	4.1	1	9.0	7	3.6	8.5	5.8	22	5.4	21	6.2	·	6.0	53	7.4	27	·	10	25	·	8	·	·	16	20	14	·	1	27	·
III	5.5	5.7	10	7.0	5	7.0	15	5.4	15.5	5.2	14	4.9	16.5	5.1	8.5	5.3	3	5.3	22	9.5	3	·	6	18	·	5	·	4	9	11	6	·	2	17	·
IV	5.5	5.2	10	5.6	12	5.8	21.5	5.5	15	4.9	4	3.0	9.5	4.8	7.5	4.8	5	4.9	60	13.8	21	·	·	3	·	2	·	·	16	16	11	1	4	·	·
V	23.5	5.7	14.5	5.3	9.5	5.6	10.5	6.5	6	3.8	3.5	5.1	13	5.6	11.5	4.7	1	5.4	38	15.3	17	·	·	·	·	4	·	3	9	11	9	1	3	·	1
VI	8.5	4.2	8.5	5.9	8	5.6	9.5	5.1	10.5	6.3	5.5	4.3	23	5.3	14.5	4.8	2	5.1	65	18.8	22	·	·	·	1	5	·	4	9	12	10	3	2	·	2
VII	7	5.6	5	6.4	5.5	5.4	5	5.3	9	4.5	32	4.9	23.5	5.0	3	3.3	3	4.8	109	23.5	23	·	·	·	·	3	·	2	12	24	19	3	2	·	7
VIII	6	5.2	·	·	6.5	4.5	6.5	5.1	11	4.5	9	3.9	29.5	3.9	16.5	3.5	8	3.8	111	28.1	24	·	·	·	2	2	·	3	10	17	13	4	·	·	3
IX	2	3.5	3	3.3	6	5.2	14	4.9	17	4.9	24.5	4.7	19	4.7	4.5	5.6	·	4.8	88	34.3	4	·	·	·	·	1	·	7	9	15	9	2	2	·	·
X	2.5	4.2	3.5	4.0	0.5	4.0	5	4.7	7	3.9	18.5	4.1	37.5	4.1	15.5	5.2	3	4.2	13	4.2	3	·	·	·	·	1	·	1	7	11	6	·	·	·	·
XI	2	6.2	2.5	8.8	11.5	9.1	11	9.1	18.5	6.5	16.5	5.6	20	4.2	7	4.2	1	6.2	49	7.1	21	2	9	16	·	8	1	1	18	24	13	·	5	15	·
XII	·	·	·	·	·	·	10	8.6	18.5	7.2	41	6.1	19.5	4.5	4	4.8	·	6.2	39	9.2	29	1	2	12	·	7	·	·	19	15	10	·	2	7	·
Rok	74	4.7	74	5.1	71.5	5.3	118	6.4	159	5.1	199.5	4.8	247	4.8	125	4.8	27	5.2	683	34.3	4.IX	3	29	96	3	59	1	26	151	194	131	14	27	79	13

Uwaga. Obserwacji nad wiatrem w terminach klimatologicznych dokonywano za pomocą wiatromierza Wilda, w czasie między terminami – wg anemografu Dinesa.

Słupsk

$H_s = 16\,m$ $h_w = 17\,m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	≥15	◔	◕	Opad R ≥0,1	≥5,0	≥10,0	≡	⊠	K (K)
I	3.5	4.6	6.5	2.3	1.5	2.0	4.5	1.4	26	3.4	13.5	3.0	4	3.8	4.5	4.2	29	2.2	46	9.8	8	1	2	22	·	2	1	2	15	20	11	·	3	18	·
II	15	2.9	3.5	2.6	1	2.0	1	1.0	3.5	2.9	15	2.7	9.5	2.2	9.5	3.3	26	1.9	72	13.5	8	6	10	26	·	·	·	·	10	22	16	1	1	28	·
III	6.5	2.0	7.5	2.9	0.5	2.0	2	2.5	17.5	1.4	21.5	2.0	4.5	3.7	3	1.7	30	1.4	37	17.4	3	4	3	23	·	·	·	7	13	15	10	1	2	17	·
IV	6	1.7	14	2.1	8	2.1	21.5	2.5	4	1.8	14	2.5	2.5	2.4	3	2.3	17	1.8	29	9.7	23	·	·	3	·	·	·	3	15	13	8	·	2	·	·
V	19	1.9	18.5	3.0	10	2.9	2	2.0	1	3.0	9.5	2.2	7.5	5.5	2.5	2.2	23	2.1	100	31.5	9	·	·	3	·	1	1[3]	5	11	14	11	2	·	·	·
VI	6.5	1.8	10.5	1.8	6.5	2.4	4	3.5	9	2.2	18.5	3.1	13.5	3.8	3.5	2.0	18	2.2	62	22.6	1	·	·	·	5	3	3	5	4	10	8	1	·	·	3
VII	6	2.1	5	2.3	2	2.0	·	·	13.5	1.7	40	2.9	3.5	1.7	·	·	23	1.9	279	71.7	15	·	·	·	4	1	·	3	10	24	23	8	·	·	6
VIII	4	1.8	·	·	·	·	3	3.7	4.5	2.0	11.5	1.9	12	2.5	5	2.2	55	1.0	63	16.4	8	·	·	·	5	·	·	3	3	13	11	2	1	·	2
IX	·	·	3	2.0	3.5	2.6	7.5	2.7	9	2.2	15.5	3.1	4.5	3.2	·	·	47	1.3	109	19.1	6	·	·	·	2	·	·	6	7	17	16	3	·	·	3
X	3.5	2.4	2	2.5	·	·	4	1.5	7.5	1.9	15.5	2.5	4.5	2.8	3	3.5	53	1.0	29	11.5	29	·	·	4	·	·	·	2	6	13	5	1	7	·	·
XI	1.5	3.0	10.5	2.3	4.5	2.3	5	4.3	17.5	3.0	20	3.8	1	2.0	2	4.0	28	2.2	99	29.7	2	4	10	19	·	3	2	1	18	23	13	3	1	12	·
XII	1	3.0	1	2.0	·	·	3.5	2.4	37.5	3.5	30	3.8	3.5	1.4	2.5	2.6	14	2.9	126	28.9	28	1	3	18	·	5	1	·	25	22	15	5	1	15	1
Rok	72.5	2.3	82	2.2	32.5	1.7	58	2.3	150.5	2.4	224.5	2.8	70.5	2.9	38.5	2.3	361	1.8	1051	71.7	15.VII	16	28	118	16	15	8[2]	37	137	206	147	27	18	90	15

Dartowo — φ = 54°27' — λ = 16°23' — 1965

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	2.6	–1.4	6.4	17	–7.9	11	0.4	1.4	0.7	0.8	5.5	5.7	5.5	5.6	86	84	85	85	0.9	1.1	1.0	1.0	8.5	8.2	7.2	8.0
II	–	–	–	–	0.5	–3.7	3.2	13	–11.6	17	–1.3	–0.2	–1.4	–1.1	4.7	5.0	4.5	4.7	83	83	79	82	0.9	1.0	1.1	1.0	8.2	8.2	7.3	7.9
III	–	–	–	–	3.4	–2.4	10.0	18	–13.4	8	–1.1	2.2	0.3	0.4	5.2	5.7	5.4	5.4	87	78	83	83	0.7	1.7	1.0	1.1	7.0	6.2	4.6	5.9
IV	–	–	–	–	9.1	2.4	14.8	6	–2.7	5	4.2	7.4	5.1	5.4	7.3	7.4	7.4	7.4	88	74	84	82	1.0	3.2	1.5	1.9	7.9	7.3	7.6	7.6
V	–	–	–	–	10.6	4.3	15.4	17	–1.3	3	7.0	9.1	7.4	7.7	8.4	8.6	8.4	8.5	83	76	78	79	1.7	3.0	2.3	2.3	5.9	5.4	6.2	5.8
VI	–	–	–	–	17.8	10.3	29.7	26	3.3	4	13.2	15.6	13.2	13.8	12.2	12.8	12.4	12.5	80	73	81	78	3.3	5.4	3.1	3.9	5.1	6.4	6.0	5.8
VII	–	–	–	–	16.6	11.7	25.7	20	6.5	5	13.8	15.2	14.4	14.4	13.7	13.5	14.0	13.7	86	79	85	83	2.2	4.0	2.5	2.9	7.8	7.3	6.7	7.3
VIII	–	–	–	–	18.7	10.9	27.7	22	7.0	17, 29	13.8	17.0	14.2	14.8	13.8	14.3	14.0	14.0	87	75	86	83	2.1	5.5	2.2	3.3	6.5	6.0	4.5	5.7
IX	–	–	–	–	17.9	10.3	26.7	3	4.4	15	12.3	17.0	13.6	14.1	12.6	13.9	13.2	13.2	87	73	85	82	1.9	6.0	2.4	3.4	7.0	6.5	5.3	6.3
X	–	–	–	–	12.2	5.8	19.3	1	–0.7	26	8.1	11.4	9.0	9.4	10.0	11.0	10.3	10.4	91	81	89	87	1.0	2.6	1.3	1.6	8.6	7.7	5.1	7.1
XI	–	–	–	–	3.0	–1.7	11.4	1	–13.0	18	0.5	2.0	0.8	1.0	5.9	6.4	6.1	6.1	86	84	86	85	0.9	1.2	0.9	1.0	9.1	8.5	7.0	8.2
XII	–	–	–	–	2.7	–0.5	11.8	19	–6.4	17	1.2	1.6	1.3	1.4	5.9	6.2	6.1	6.1	87	88	91	88	0.9	0.8	0.6	0.8	9.5	9.3	8.9	9.2
Rok	–	–	–	–	9.6	3.8	29.7	26, VI	–13.4	8, III	6.0	8.3	6.6	6.9	8.8	9.2	8.9	9.0	86	79	84	83	1.5	3.0	1.7	2.1	7.6	7.2	6.4	7.1

Gdańsk - Nowy Port — φ = 54°24' — λ = 18°40'

I	–	–	–	–	1.9	–2.1	5.6	1	–11.8	11	–0.5	0.8	–0.1	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	7.4	7.2
II	–	–	–	–	0.4	–4.5	4.5	13	–12.6	6	–2.8	–1.0	–2.5	–2.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	7.2	7.4
III	–	–	–	–	4.3	–2.7	12.0	29	–19.5	8	–1.6	3.0	0.6	0.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.2	5.1	5.4
IV	–	–	–	–	8.3	2.6	11.4	16,26,28	–1.5	6, 11	3.5	7.0	5.0	5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	7.0	7.2
V	–	–	–	–	11.8	5.8	19.4	17	–0.2	4	8.1	10.2	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.2	5.4	5.2
VI	–	–	–	–	18.9	11.3	29.7	26	5.7	4	14.0	17.6	14.3	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.5	4.7	5.2
VII	–	–	–	–	19.3	12.1	25.0	21	8.1	6	14.5	17.7	14.3	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	6.1	6.5
VIII	–	–	–	–	20.1	11.6	29.4	22	7.9	2	13.7	18.8	14.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.2	4.8	5.3
IX	–	–	–	–	19.2	10.6	24.5	3	7.2	16	11.9	18.1	13.4	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.4	4.2	5.1
X	–	–	–	–	13.0	6.2	17.5	7	0.6	21, 26	7.7	12.2	8.9	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.2	6.3	6.4
XI	–	–	–	–	2.5	–2.3	11.8	1, 2	–14.7	24	–0.6	0.8	–0.2	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.5	6.3	7.4
XII	–	–	–	–	2.7	–1.2	11.2	19	–13.5	18	0.2	1.4	0.6	0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	7.1	7.6
Rok	–	–	–	–	10.2	4.0	29.7	26.VI	–19.5	8. III	5.7	8.9	6.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.4	6.0	6.3

Gdańsk - Wrzeszcz — φ = 54°23' — λ = 18°36'

I	1008.6	1025.4	984.6	1010.2	1.9	–2.2	5.8	1, 17	–11.2	11	–0.4	0.8	–0.1	0.0	5.2	5.4	5.3	5.3	87	82	85	85	0.8	1.2	0.9	1.0	7.6	7.8	7.3	7.6
II	1013.5	1035.3	980.6	1015.1	0.0	–6.5	4.2	13	–12.0	6, 26	–3.0	–1.1	–2.8	–2.4	4.2	4.6	4.2	4.3	84	79	83	82	0.8	1.1	0.8	0.9	8.0	7.9	7.4	7.8
III	1014.5	1031.5	988.1	1016.1	4.8	–2.7	11.9	29	–18.9	8	–1.3	3.5	0.8	1.0	5.0	5.5	5.5	5.3	85	69	81	78	0.9	2.6	1.3	1.6	5.5	6.1	5.6	5.7
IV	1010.6	1030.7	991.5	1012.1	9.3	2.4	14.1	6	–1.8	5	3.9	7.6	5.4	5.6	6.9	7.1	7.2	7.1	84	68	80	77	1.3	3.6	1.9	2.3	8.2	8.1	7.0	7.8
V	1013.3	1029.3	987.6	1014.8	12.4	5.5	19.3	17	–0.3	2	8.3	10.8	8.0	8.8	8.4	7.9	8.5	8.3	75	61	78	71	2.7	5.2	2.4	3.4	5.6	6.9	5.9	5.8
VI	1012.5	1021.4	998.8	1014.0	19.7	11.2	30.1	26	5.4	5	14.4	18.3	14.5	15.4	12.4	12.2	12.7	12.4	76	60	76	71	4.2	9.6	4.0	5.9	6.2	5.9	5.7	5.9
VII	1008.6	1022.2	991.2	1010.1	19.4	12.1	25.5	21	8.4	6	14.5	17.8	14.6	15.4	13.4	13.0	13.8	13.4	80	63	82	75	3.2	7.7	3.0	4.6	6.3	7.7	6.4	6.8
VIII	1013.3	1021.3	1003.6	1014.8	20.3	11.8	29.4	23	8.9	17,31	13.9	18.6	14.5	15.4	13.6	13.6	14.0	13.7	85	65	84	78	2.4	8.6	2.9	4.6	5.9	7.4	5.3	6.2
IX	1011.8	1030.8	1000.7	1013.3	19.6	10.6	27.0	3	7.3	24	12.0	18.4	13.8	14.5	12.5	13.6	13.4	13.2	89	65	84	79	1.6	7.9	2.6	4.0	6.0	5.8	4.1	5.3
X	1020.3	1035.4	1001.3	1021.8	13.3	6.6	17.6	7	1.7	26	7.8	12.4	8.8	9.4	9.5	10.3	9.8	9.9	88	71	85	81	1.2	4.3	1.7	2.4	7.2	7.0	5.3	6.5
XI	1009.3	1028.1	978.4	1010.8	2.3	–2.6	12.2	1	–13.1	24	–0.7	0.8	0.0	0.0	5.3	5.7	5.6	5.5	85	81	84	83	1.0	1.3	1.1	1.1	8.2	8.2	6.4	7.6
XII	1000.5	1021.8	971.8	1002.1	2.7	–1.2	11.3	19	–12.6	18	0.4	1.5	0.8	0.9	5.5	5.6	5.7	5.6	86	81	85	84	0.9	1.3	1.0	1.1	8.4	8.4	7.7	8.2
Rok	1011.4	1035.4	971.8	1012.9	10.5	3.8	30.1	26.VI	–18.9	8. III	5.8	9.1	6.5	7.0	8.5	8.7	8.8	8.7	84	70	82	79	1.8	4.5	2.0	2.8	6.9	7.2	6.2	6.8

Kamienica Królewska — φ = 54°23' — λ = 17°54'

I	–	–	–	–	0.8	–	4.9	1	–	–	–1.5	0.0	–1.4	–1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	7.7	8.0
II	–	–	–	–	–0.9	–9.0	3.4	11	–18.0	24	–4.9	–1.6	–5.5	–4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.4	8.3	8.5
III	–	–	–	–	3.4	–4.4	9.9	29	–16.5	8	–2.5	2.2	–1.2	–0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.8	6.6	6.8
IV	–	–	–	–	9.4	1.9	14.9	28	–3.9	1	3.9	8.2	4.4	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	6.9	7.2
V	–	–	–	–	12.6	3.4	18.7	28	–4.1	2	7.2	11.7	6.1	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.0	6.3	6.6
VI	–	–	–	–	19.8	9.2	29.0	26	1.9	4	14.1	19.0	12.5	14.5	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.3	6.0	5.9
VII	–	–	–	–	18.2	10.1	27.8	14	5.3	19	13.6	16.8	12.7	13.9	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	7.2	7.4
VIII	–	–	–	–	19.3	9.5	27.8	23	4.5	13	13.7	18.2	12.3	14.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.0	4.7	6.0
IX	–	–	–	–	18.6	9.2	25.4	3	4.3	16	12.1	17.9	12.0	13.5	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.0	4.0	5.4
X	–	–	–	–	12.1	3.8	18.2	1	–1.0	22	6.7	11.5	6.5	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.9	5.7	6.8
XI	–	–	–	–	1.1	–3.9	10.3	2	–15.2	18	–1.8	0.0	–1.5	–1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.4	7.7	8.3
XII	–	–	–	–	1.3	–3.1	9.3	19	–14.1	16	–0.9	0.2	–0.6	–0.5	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.9	8.6	8.9
Rok	–	–	–	–	9.6	–	29.0	26.VI	–	–	5.0	8.7	4.7	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	6.6	7.1

Darłowo — $H_s = 3m$ — $h_w = 23m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%, V=0) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V >10	>15	☾	●	Opad R >0.1	>5.0	>10.0	≡	⊠	⊠
I	6.5	4.7	4.5	4.8	8.5	4.5	15.5	2.0	27	4.0	19	5.9	6.5	6.8	5.5	7.5	·	4.6	49	7.9	8	·	1	20	·	2	·	1	19	19	14	·	1	—	·
II	14	9.8	15	7.9	10	4.8	3	2.3	2	4.0	11	5.9	11.5	7.2	17.5	7.6	·	7.1	28	4.1	13	2	12	23	·	7	3	·	14	20	13	·	3	—	·
III	5	4.9	9.5	6.7	10.5	4.1	11	3.2	18.5	3.5	20	4.2	15	5.3	3.5	6.0	·	4.5	19	6.2	3	2	10	21	·	4	·	8	12	13	6	·	6	—	·
IV	6	5.2	8.5	5.7	19	4.7	14	3.6	12	4.0	7.5	3.4	18	4.0	5	4.0	·	4.3	32	8.9	13	·	·	4	·	1	·	1	17	12	6	·	7	—	1
V	8.5	5.2	18.5	6.7	19.5	3.7	10.5	4.4	3	2.8	10	3.2	17	5.0	6	5.2	·	4.8	40[2]	9.3	10	·	·	1	·	2	·	8	11	11	9	·	7	—	·
VI	4.5	4.4	14.5	5.7	10	3.2	6	3.8	2.5	3.7	7.5	5.5	32	6.0	8	4.8	·	5.1	30	10.8	18	·	·	·	4	5	·	5	6	10	7	1	2	—	2
VII	1	3.0	9.5	8.8	8	3.7	6	2.8	5	2.9	25	6.7	34	7.4	4.5	5.9	·	6.4	177	33.4	21	·	·	·	1	10	·	3	14	23	19	6	2	—	4
VIII	7	4.9	4	2.5	3	2.5	12	2.6	9.5	3.0	16.5	4.3	26	4.5	15	4.2	·	3.9	48	11.5	8	·	·	·	4	·	·	3	6	11	9	1	5	—	1
IX	1.5	2.7	0.5	4.0	9	3.9	17	4.0	19.5	3.5	20	5.4	14.5	6.9	8	4.8	·	4.7	98	17.3	3	·	·	·	2	3	·	3	13	16	16	3	·	—	2
X	6	5.3	8	3.9	5.5	2.9	7	2.4	13	3.3	21.5	5.0	19.5	6.1	11.5	6.4	1	4.7	21	14.8	29	·	·	2	·	4	·	1	10	6	2	1	8	—	·
XI	6	8.9	2.5	4.8	17.5	3.9	18	3.4	15.5	4.9	12.5	8.4	12	9.7	4	5.0	2	5.7	56	11.6	3	3	10	19	·	11	·	·	20	21	14	1	1	—	·
XII	3	5.5	·	·	2	1.0	13.5	4.9	24	5.1	26.5	7.4	13.5	7.8	10.5	5.9	·	6.1	91	15.5	18	·	2	20	·	6	1	·	25	21	19	3	1	—	1
Rok	69	5.4	95	5.1	122.5	3.6	133.5	3.3	156.5	3.7	197	5.4	219.5	6.4	99	5.6	3	5.2	689	33.4	21.VII	7	35	110	11	55	4	33	167	183	134	16	43	—	11

Gdańsk - Nowy Port — $H_s = 7m$ — $h_w = 13m$

I	3.5	4.4	5	5.2	4.5	3.2	14.5	2.2	21	4.9	17	2.9	12	4.7	6.5	5.4	9	3.5	24	4.8	6	1	7	25	·	6	3	3	14	15	10	·	4	19	·
II	11	7.3	12	7.5	3	5.0	5.5	2.3	5.5	3.2	7.5	5.9	25.5	4.9	11	6.1	3	5.4	26	7.2	27	2	12	26	·	14	8	·	12	20	9	·	1[2]	19	·
III	5	5.2	13.5	4.4	4	3.2	15	3.0	11.5	2.6	12	3.2	17	4.9	4	3.8	11	3.3	16	6.1	3	2	6	20	·	3	1	6	9	10	4	·	7	15	·
IV	9	3.7	13.5	3.4	10	3.2	18	3.1	14	2.2	2	3.0	6	2.3	7.5	4.1	10	2.8	36	11.3	21	·	·	5	·	·	·	1	11	14	8	1	4	·	·
V	23.5	4.7	18	3.1	10	4.1	4.5	4.3	2.5	1.8	3	3.7	14	3.9	6.5	3.5	11	3.4	29	8.3	7	·	·	1	·	2	·	9	9	12	7	·	4[2]	·	2
VI	9	3.1	13	3.4	6.5	3.2	2.5	3.4	11	3.3	6	3.1	19	4.7	10	3.8	13	3.1	68	34.0	22	·	·	·	4	4	1	6	6	12	7	2	·	·	3
VII	1.5	3.7	10	4.6	5	1.8	3.5	2.0	7.5	2.5	26	4.5	21	3.6	4.5	4.1	14	3.2	89	18.2	23	·	·	·	·	2	1	2	11	22	14	3	2	·	7
VIII	8.5	2.9	3	2.5	2	1.2	5.5	4.3	5	3.4	8.5	3.2	18.5	2.9	16	3.3	26	2.2	82	15.5	27	·	·	·	5	1	1	5	7	16	13	4	2	·	5
IX	2.5	2.6	4	2.2	6.5	2.5	7	3.6	12.5	3.0	22.5	3.0	17.5	3.1	1.5	3.7	16	2.4	99	44.2	4	·	·	·	·	4	1	5	7	14	8	2	3	·	1
X	7	4.7	2.5	2.2	3	3.3	5	2.6	10	2.5	10	4.6	22	3.7	16.5	5.5	17	3.3	10	4.5	29	·	·	·	·	3	1	2	9	6	3	·	7	·	·
XI	·	·	1	14.0	11	5.6	18.5	3.8	15.5	3.5	13	6.7	18	4.6	5	8.4	8	4.6	52	13.6	21	5	11	19	·	5	4	1	13	21	11	2	4	16	·
XII	2	3.0	·	·	·	·	9.5	2.6	22	3.8	25	4.3	27.5	4.2	2	6.0	5	3.7	26	7.1	14	2	5	17	·	4	2	·	12	16	6	·	·	12	·
Rok	82.5	3.8	95.5	4.4	65.5	3.0	109	3.1	138	3.1	152.5	4.0	218	4.0	91	4.7	143	3.4	557	44.2	4.IX	12	41	113	9	48	23	40	120	178	100	14	38[2]	81	18

Gdańsk - Wrzeszcz — $H_s = 13m$ — $H_b = 12{,}4m$ — $h_w = 15{,}5m$

I	4	7.9	7.5	4.3	1.5	3.3	10.5	2.7	23	4.4	22	6.0	7	5.7	7.5	4.9	10	4.4	29	4.9	21	1	8	26	·	7	·	1	17	21	11	·	3	21	·
II	10.5	8.6	18.5	7.1	0.5	6.0	2	1.5	6	1.5	15	5.8	12.5	6.8	17	6.6	2	6.2	37	7.0	27	3	14	26	·	9	·	·	14	20	13	·	·	27	·
III	5	5.5	16	6.1	2	2.2	9.5	3.0	18.5	2.8	16	4.6	14.5	6.2	5.5	4.9	6	4.3	27	10.7	3	3	7	21	·	4	·	6	9	10	5	1	1	17	·
IV	6.5	6.2	16	4.7	10	4.3	15	4.2	16	3.5	7	3.6	5.5	5.2	6	4.8	8	4.0	50	13.8	21	·	·	5	·	1	·	2	17	15	11	1	4	·	·
V	18	6.3	30	4.8	7.5	4.1	6	3.4	4	4.9	7.5	4.3	10	6.0	5	4.5	5	4.7	38	11.6	7	·	·	1	·	2	·	6	10	12	9	1	3	·	1
VI	13.5	4.4	16	5.1	6	3.3	4	4.9	8	4.6	10	4.6	19	5.8	8.5	5.0	5	4.6	88	47.8	22	·	·	·	4	2	·	3	8	12	7	2	1	·	2
VII	5	5.5	11.5	5.7	2.5	2.2	4	3.5	8.5	3.9	32.5	5.6	18	6.6	4	5.5	7	5.0	112	21.7	15	·	·	·	1	1	·	2	11	24	19	4	·	·	6
VIII	9.5	4.4	9.5	3.2	1.5	4.3	5	3.2	8.5	4.5	14.5	3.6	16	3.3	16.5	3.6	12	3.2	106	18.1	27	·	·	·	5	1	1	1	9	16	13	6	1	·	5
IX	3	4.3	4	2.6	4	3.1	7.5	2.5	15.5	3.4	28.5	4.6	9.5	4.4	3	5.5	15	3.3	84	38.8	4	·	·	·	1	·	·	3	8	14	9	2	3	·	1
X	9.5	6.9	5.5	3.0	2	3.5	3	1.7	9.5	2.8	19	4.6	19	4.3	13.5	4.6	12	3.8	14	4.2	29	·	·	·	·	3	·	1	8	10	6	·	3	·	·
XI	4	6.4	2	7.5	6.5	5.4	12	3.0	23.5	3.8	20.5	6.3	13	5.8	5.5	3.3	3	4.7	59	13.1	2	5	12	20	·	3	·	·	13	26	12	2	2	18	·
XII	1	3.5	·	·	·	·	9	5.8	25	4.8	36.5	6.8	16.5	5.6	5	5.6	·	5.9	40	10.8	29	2	3	19	·	5	·	·	18	18	9	1	·	14	·
Rok	89.5	5.8	136.5	4.5	44	3.5	87.5	3.3	166	3.7	229	5.0	160.5	5.5	97	4.9	85	4.5	684	47.8	22.VI	14	44	118	11	38	1	25	142	198	124	20	21	97	15

Uwaga. Kierunki i prędkości wiatru — wg anemometru Chauvin Arnoux.

Kamienica Królewska — $H_s = 160m$ — $h_w = 13{,}4m$

I	5	2.6	4.5	3.7	3.5	2.7	8	4.1	38.5	5.9	6	5.8	8.5	4.1	5	2.5	14	4.1	30	6.2	9	—	11	—	·	4	1	·	16	13	8	·	6	21	·
II	18	2.6	1	1.0	18	3.5	·	·	17.5	3.1	7.5	4.7	12	4.1	6	2.5	4	3.1	78	14.3	27	12	19	27	·	3	·	·	16	22	16	2	2	28	·
III	7.5	3.3	8.5	4.1	7	4.4	3.5	1.6	41.5	3.6	7	4.6	11.5	3.2	2.5	5.0	4	3.5	32	13.3	3	3	9	25	·	1	·	4	14	11	5	1	2	19	·
IV	8	3.4	5	6.6	11	3.7	10	4.6	37	5.3	7	5.3	5.5	2.8	2.5	2.6	4	4.5	47	13.6	23	·	·	9	·	5	1	1	13	13	8	1	5	·	·
V	10.5	3.4	13	3.2	13	3.8	11	6.9	12	5.1	4	4.0	18	3.3	2.5	2.6	9	3.7	58	12.9	17	·	·	4	·	4	·	4	12	15	9	3	4	·	1
VI	10	2.2	8.5	4.0	10	3.1	2	5.0	16.5	5.7	14	5.3	17.5	3.4	6.5	2.7	5	3.8	84	23.2	22	·	·	·	4	2	·	4	8	11	8	4	2	·	1
VII	0.5	1.0	4	2.8	9	4.1	5	5.9	10.5	4.7	30	5.5	19.5	4.9	0.5	1.0	14	4.1	179	21.3	15	·	·	·	2	8	·	3	14	26	22	6	2	·	5
VIII	13	1.9	1	1.0	·	·	1	5.5	14.5	5.7	14.5	4.7	18	2.7	11	2.8	20	2.8	118	21.8	4	·	·	·	4	5	·	3	8	12	12	4	4	·	3
IX	5	2.8	·	·	3	2.3	10	4.7	27	4.6	26	3.6	13	3.0	3	5.0	3	3.8	78	16.4	12	·	·	·	1	1	·	5	4	14	13	3	7	·	1
X	18.5	2.0	3	2.0	2.5	2.0	1.5	2.7	25	3.3	10	5.4	15	2.4	3.5	2.1	14	2.5	19	4.2	29	·	·	5	·	1	·	1	10	12	6	·	16	·	·
XI	2	2.0	2	2.0	4	1.8	11	2.5	27	6.2	12	5.2	17	3.4	1	1.0	14	3.7	59	9.8	2	5	14	22	·	6	1	·	19	19	13	·	10	17	·
XII	3	2.3	·	·	5	2.2	3	4.5	40	7.0	21	6.3	15	2.6	·	·	6	5.2	88	20.4	29	4	7	26	·	10	2	·	24	16	10	3	3	17	·
Rok	101	2.5	50.5	2.5	86	2.8	66	4.0	307	5.0	159	5.0	170.5	3.3	44	2.5	111	3.7	870	23.2	22.VI	—	60	—	11	50	5	25	158	184	130	27	63	102	11

Krynica Morska — φ = 54°23′ — λ = 19°27′ — 1965

Miesiąc	Ciśnienie p: p_m	Max	Min	$p_{o.m}$	Temperatura t: Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	1.4	−2.6	4.8	9	−13.2	31	−1.0	0.2	−0.6	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	6.3	7.0
II	–	–	–	–	−0.5	−6.8	4.0	10	−15.3	6	−4.2	−2.0	−3.4	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	6.4	7.1
III	–	–	–	–	7.5	−4.3	10.0	29	−24.5	8	−2.8	1.2	−0.6	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.5	5.5	5.6
IV	–	–	–	–	8.8	3.0	15.3	28	−1.6	3, 6	4.6	7.7	5.3	5.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.2	7.6	7.2
V	–	–	–	–	11.7	5.2	18.7	18	2.4	2	8.3	10.2	7.4	8.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.1	11.1	28.0	26	5.5	4, 8	14.3	17.9	13.7	14.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	19.9	12.5	26.2	15	8.4	6	14.9	18.4	15.1	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.4	6.2	5.5
VIII	–	–	–	–	19.6	12.3	27.1	23	8.6	10	14.4	18.4	14.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.3	5.1	5.3
IX	–	–	–	–	18.8	11.6	25.6	3	8.1	16	13.0	17.6	13.6	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.2	4.2	4.3
X	–	–	–	–	12.3	6.6	18.3	1	1.9	21	8.0	11.4	8.8	9.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.9	5.3	6.3
XI	–	–	–	–	1.8	−3.0	10.8	2	−13.4	24	−1.3	0.2	−0.9	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.1	7.0	7.4
XII	–	–	–	–	2.1	−1.6	8.4	19	−11.6	18	−0.2	0.5	0.3	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.3	8.1	8.2
Rok	–	–	–	–	9.8	3.7	28.0	26. VI	−24.5	8. III	5.7	8.5	6.1	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Czarna Dąbrówka — φ = 54°21′ — λ = 17°34′

I	–	–	–	–	1.1	−2.6	5.2	17	−11.9	11	−1.2	0.3	−0.8	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.8	7.8	8.1
II	–	–	–	–	−1.0	−9.6	2.9	13	−21.2	24	−5.2	−1.6	−5.6	−4.5	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.4	7.8	8.1
III	–	–	–	–	3.9	−5.0	11.1	29	−22.2	8	−3.2	2.9	−1.1	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.3	5.6	6.4
IV	–	–	–	–	9.3	2.0	15.0	22	−3.1	5	3.6	8.4	4.7	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	6.5	7.1
V	–	–	–	–	12.8	3.4	20.0	28	−4.1	3	7.2	11.7	6.7	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.0	5.5	6.3
VI	–	–	–	–	19.6	9.0	28.4	26	3.0	4	13.6	18.3	13.1	14.5	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.4	5.7	5.8
VII	–	–	–	–	18.0	10.4	27.0	14	5.3	2	13.3	16.3	13.1	13.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.0	7.0	7.4
VIII	–	–	–	–	19.0	9.3	27.1	23	4.4	17	12.6	17.7	12.6	13.9	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	4.7	6.1
IX	–	–	–	–	18.4	9.5	25.9	3	3.0	16	11.3	17.4	12.4	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.3	4.3	5.2
X	–	–	–	–	12.1	3.8	19.2	1	−2.4	12	5.7	11.5	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.0	4.8	6.6
XI	–	–	–	–	1.5	−3.9	10.7	1	−17.1	23	−2.0	0.4	−1.3	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.4	6.7	8.0
XII	–	–	–	–	1.6	−2.5	9.9	19	−16.6	16	−0.7	0.4	−0.1	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	9.7	8.9	9.8	9.5
Rok	–	–	–	–	9.7	2.0	28.4	26. VI	−22.2	8. III	4.6	8.6	5.0	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	6.4	7.1

Świbno — φ = 54°20′ — λ = 18°56′

I	–	–	–	–	1.3	−3.7	5.4	9	−15.2	11	−1.6	0.6	−0.8	−0.6	5.0	5.4	5.1	5.2	89	84	87	87	0.7	1.0	0.8	0.8	7.9	8.2	7.6	7.9
II	–	–	–	–	−0.2	−6.4	3.0	13	−15.0	6	−3.5	−1.5	−2.8	−2.6	4.2	4.4	4.2	4.3	86	79	82	82	0.6	1.1	0.9	0.9	8.5	7.7	7.1	7.8
III	–	–	–	–	2.9	−4.1	11.8	29	−22.4	8	−2.8	1.4	−0.3	−0.5	4.8	5.4	5.3	5.2	89	78	85	84	0.6	1.7	0.9	1.1	6.7	6.4	5.5	6.2
IV	–	–	–	–	8.8	2.7	15.8	28	−2.0	3	4.1	7.4	5.2	5.5	7.0	7.3	7.3	7.2	84	71	82	79	1.3	3.2	1.7	2.1	8.4	7.9	6.8	7.7
V	–	–	–	–	11.6	5.3	18.9	17	−1.2	4	8.2	10.1	8.1	8.6	8.9	9.0	9.0	9.0	81	72	82	78	2.0	3.5	2.0	2.5	6.0	5.8	6.3	6.0
VI	–	–	–	–	18.6	11.1	27.6	26	4.5	8	14.0	17.4	14.2	15.0	13.6	13.6	14.0	13.7	84	69	85	79	2.5	7.0	2.4	4.0	6.5	5.4	5.5	5.8
VII	–	–	–	–	18.9	11.5	24.1	21	6.3	2	14.4	17.6	14.6	15.3	14.2	13.9	14.5	14.2	86	69	87	81	2.4	6.5	2.3	3.7	6.9	8.0	7.2	7.4
VIII	–	–	–	–	19.4	10.8	27.6	22	6.7	2, 10	13.4	18.0	14.5	15.1	14.7	15.1	15.4	15.1	95	74	92	87	0.8	6.0	1.3	2.7	6.9	7.5	5.7	6.7
IX	–	–	–	–	18.8	10.0	26.0	3	4.6	16	11.7	17.7	13.1	13.9	13.3	15.5	14.2	14.3	95	76	94	88	0.7	5.2	1.0	2.3	6.5	5.8	3.9	5.4
X	–	–	–	–	12.3	5.2	16.7	7	−0.7	26	7.0	11.6	8.3	8.8	9.6	11.4	10.1	10.4	94	83	90	89	0.7	2.4	1.1	1.4	8.5	7.3	5.2	7.0
XI	–	–	–	–	1.9	−3.5	11.0	1, 2	−16.6	24	−1.4	0.5	−0.7	−0.6	5.4	6.0	5.8	5.7	89	86	90	88	0.6	0.9	0.5	0.7	8.5	8.1	7.1	7.9
XII	–	–	–	–	1.9	−2.5	9.2	19	−18.5	17	−0.4	0.8	−0.1	0.0	5.5	5.7	5.5	5.6	89	86	88	88	0.7	1.0	0.7	0.8	8.6	8.7	6.4	7.9
Rok	–	–	–	–	9.7	3.0	27.6	26.VI, 22.VIII	−22.4	8. III	5.3	8.5	6.1	6.5	8.8	9.4	9.2	9.1	88	77	87	84	1.1	3.3	1.3	1.9	7.5	7.2	6.2	7.0

Kartuzy — φ = 54°20′ — λ = 18°12′

I	–	–	–	–	0.4	−3.5	4.2	1	−13.6	11	−2.2	−0.7	−1.7	−1.6	4.9	5.2	5.0	5.0	92	88	91	90	0.4	0.7	0.5	0.5	9.2	8.2	7.9	8.4
II	–	–	–	–	−1.7	−7.5	2.3	13	−15.4	6	−5.0	−2.7	−4.8	−4.3	3.9	4.5	4.0	4.1	90	88	90	89	0.4	0.6	0.4	0.5	8.1	7.6	6.7	7.5
III	–	–	–	–	3.7	−3.8	9.6	29	−15.2	8	−2.6	2.3	−0.7	−0.4	4.7	5.5	5.1	5.1	88	75	84	82	0.6	2.1	0.9	1.2	7.1	6.4	6.6	6.7
IV	–	–	–	–	8.6	1.5	13.9	28	−3.0	5	3.0	7.0	4.3	4.6	6.7	7.3	6.8	6.9	88	73	81	81	1.0	3.0	1.6	1.9	7.6	8.0	6.5	7.4
V	–	–	–	–	12.3	3.9	17.9	17	−1.2	3	6.8	10.8	6.9	7.8	7.8	7.6	8.0	7.8	78	58	79	72	2.2	5.7	2.1	3.3	5.9	6.5	4.6	5.7
VI	–	–	–	–	19.1	9.7	29.0	26	4.8	8	13.3	17.8	13.5	14.5	12.0	11.5	11.8	11.8	78	58	76	71	3.5	9.6	3.9	5.7	5.2	6.5	5.0	5.6
VII	–	–	–	–	18.0	10.5	27.4	15	6.4	5	12.8	16.2	12.9	13.7	13.0	13.0	13.3	13.1	87	70	89	82	2.0	6.0	1.8	3.3	7.4	7.8	7.9	7.7
VIII	–	–	–	–	18.8	10.1	26.9	22, 23	6.4	16	12.7	17.2	13.0	14.0	13.2	12.8	13.1	13.0	89	66	88	81	1.7	7.5	2.2	3.8	7.1	7.0	5.1	6.4
IX	–	–	–	–	18.3	9.4	26.0	3	5.5	16	10.8	17.0	12.0	13.0	12.1	13.7	12.8	12.9	93	72	90	85	0.9	6.1	1.4	2.8	7.4	6.5	4.0	6.0
X	–	–	–	–	11.5	4.9	18.3	1	0.0	21	6.5	10.6	7.0	7.8	9.1	10.0	9.0	9.4	92	77	89	86	0.7	3.0	1.1	1.6	8.5	7.7	5.4	7.2
XI	–	–	–	–	0.8	−4.2	9.9	1, 2	−15.2	18	−2.3	−0.6	−1.8	−1.6	5.1	5.5	5.3	5.3	91	87	90	89	0.5	0.8	0.5	0.6	9.6	8.9	7.6	8.7
XII	–	–	–	–	1.0	−2.9	8.9	19	−12.8	17	−1.3	−0.3	−0.9	−0.8	5.2	5.4	5.3	5.3	90	88	90	89	0.5	0.7	0.6	0.6	9.5	9.5	8.8	9.3
Rok	–	–	–	–	9.2	2.3	29.0	26 VI	−15.4	6. II	4.4	7.9	5.0	5.6	8.1	8.5	8.3	8.3	88	75	86	83	1.2	3.8	1.4	2.1	7.7	7.6	6.3	7.2

Krynica Morska $H_s = 4\,m$ $h_w = 11\,m$ 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	24	5.9	30	1	7	25	·	—	—	4	15	16	8	·	4	20	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39	8.7	22	5	15	26	·	—	—	1	13	19	12	·	·	28	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	19	9.2	3	4	8	22	·	—	—	9	11	8	6	·	4	24	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	30	14.0	21	·	·	4	·	—	—	2	15	8	4	1	2	·	1
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	22	6.0	17	·	·	·	·	—	—	—	—	11	7	·	4²	·	·
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	70	14.7	1	·	·	·	3	—	—	—	—	10	10	3	1	·	4
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	98	16.8	16	·	·	·	5	—	—	7	6	20	18	3	·	·	3
VIII	15	5.3	1	8.0	·	·	5.5	4.8	8	3.9	20.5	3.8	18.5	4.4	14.5	5.2	10	4.1	87	33.4	27	·	·	·	3	1	·	8	9	15	12	2	2	·	2
IX	3.5	3.4	4	3.4	2.5	2.6	15.5	3.4	12	3.7	23	5.2	14.5	5.6	6	7.0	9	4.1	143	64.8	4	·	·	·	1	2	1	11	6	8	7	5	1	·	·
X	7.5	4.1	4.5	3.7	4.5	3.9	2	4.8	8	2.8	28	6.1	13.5	6.3	19	7.0	6	5.2	28	9.4	16	·	·	·	·	4	·	7	13	9	6	·	9	·	·
XI	3	8.0	10.5	6.4	12	4.1	18.5	6.1	8	5.4	14.5	8.0	12	9.6	7.5	8.3	4	6.6	48	12.3	21	6	11	18	·	7	3	2	17	14	9	2	3	16	·
XII	0.5	7.0	·	·	·	·	9	5.7	16.5	6.5	36.5	6.3	19.5	5.8	6	6.2	5	5.8	27	14.3	18	2	5	23	·	3	1	·	17	9	6	1	3	16	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	635	64.8	4. IX	18	46	118	12	—	—	—	—	147	105	17	33²	104	10

Czarna Dąbrówka $H_s = 120\,m$ $h_w = 12\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	2	3.2	·	·	7	2.6	31.5	3.6	24	4.7	17.5	4.4	3.5	9.3	7.5	3.7	·	4.2	32	6.4	8	1	10	26	·	4	1	1	19	21	10	·	1	16	·
II	15	4.3	9	3.4	4	2.8	4.5	2.9	4.5	2.3	9.5	5.7	22	4.0	15.5	4.1	·	4.0	54	5.8	-7, 28	11	18	27	·	2	·	·	14	23	16	·	1	28	·
III	7	2.8	5.5	3.9	10.5	2.5	11	3.6	24.5	3.6	15.5	3.0	16	4.0	3	4.8	·	3.4	32	15.1	3	5	8	25	·	·	·	7	13	15	6	1	4	22	·
IV	10.5	2.9	1.5	3.0	19.5	3.1	26.5	5.0	11.5	4.2	6.5	3.4	12	4.5	2	2.2	·	4.0	46	13.1	26	·	·	7	·	1	·	2	14	13	7	2	2	·	1
V	12	2.6	7	3.4	21	3.0	16	4.8	2	4.0	8	3.4	19.5	4.2	7.5	2.9	·	3.6	67	16.9	7	·	·	4	·	2	1	5	13	15	11	3	4	·	·
VI	6.5	2.8	3.5	2.1	15.5	3.2	6.5	4.5	7.5	5.1	7	3.4	32.5	4.2	11	2.0	·	3.6	65	18.3	1	·	·	·	3	3	·	3	8	12	9	2	2	·	4
VII	1	2.0	5	2.2	7.5	1.9	10.5	3.2	9.5	3.1	40.5	3.2	17.5	4.3	1.5	5.7	·	3.3	180	30.4	15	·	·	·	2	·	·	3	13	25	24	4	3	·	6
VIII	4	2.2	0.5	2.0	0.5	2.0	7	4.9	11	3.9	18.5	2.6	24.5	2.5	26	2.1	1	2.7	83	19.1	8	·	·	·	4	1	·	3	7	17	11	3	2	·	5
IX	1.5	1.7	·	·	5.5	3.5	17.5	4.0	15.5	4.2	31.5	3.6	16	3.0	2.5	2.6	·	3.6	89	18.8	4	·	·	·	1	2	·	7	7	15	13	3	2	·	2
X	12.5	1.9	·	·	1.5	2.3	5.5	2.6	21	3.0	23	3.5	21.5	2.7	8	2.5	·	2.8	19	6.7	2	·	·	4	·	·	·	2	10	12	4	·	6	·	·
XI	2	4.0	3	2.0	10.5	2.3	23.5	4.0	16	5.2	19.5	4.6	15.5	3.6	·	·	·	4.0	53	9.2	21	5	13	21	·	3	·	1	18	22	14	·	1	18	·
XII	·	·	·	·	·	·	19.5	4.9	24	5.2	33	4.9	13.5	3.5	3	3.7	·	4.8	83	12.3	18	3	7	22	·	4	1	·	29	26	15	2	1	19	·
Rok	74	2.5	35	1.8	103	2.4	179.5	4.0	171	4.0	230	3.8	214	4.2	87.5	3.0	1	3.7	803	30.4	15. VII	25	56	136	10	22	3	34	165	216	140	20	29	103	18

Świbno $H_s = 3\,m$ $h_w =$ 10 m I–VII, 15.5 m VIII–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	1	2.0	5.5	5.2	14	3.8	12	4.9	21	4.3	13.5	3.3	3.5	3.4	14.5	6.0	8	4.0	28	4.3	21	2	9	27	·	3	·	1	19	13	10	·	1	23	·
II	7.5	9.1	12.5	7.2	6.5	4.7	4	3.6	8	4.6	8	5.4	12.5	4.4	21	6.6	4	5.7	38	7.1	22	4	13	26	·	9	·	·	14	16	12	·	·	28	·
III	8	4.1	11.5	6.6	10.5	3.3	18.5	3.6	14.5	3.0	6.5	3.4	11.5	4.0	6	5.4	6	3.8	22	6.3	3	3	8	22	·	1	·	2	11	10	7	·	6	19	·
IV	8	5.1	16	5.6	12	6.4	24.5	6.1	3.5	5.7	1	3.0	7	3.6	9	4.7	9	5.0	46	11.4	21	·	·	5	·	5	·	1	17	15	9	1	4	·	·
V	22	6.1	15	5.6	11	6.0	6	6.5	2	2.0	3	3.3	10	4.8	12	5.1	12	4.8	33	11.4	10	·	·	1	·	8	·	5	11	7	7	1	2	·	·
VI	11.5	3.6	23.5	5.9	3	6.0	6.5	7.4	7.5	5.3	7	4.1	14	4.0	12	3.9	5	4.6	71	18.5	22	·	·	·	3	5	1	4	9	10	9	3	·	·	4
VII	3	8.0	14	6.7	5	4.2	5	5.4	7.5	4.1	23.5	4.6	22	4.6	4	4.2	9	4.6	107	27.0	15	·	·	·	·	4	·	2	15	20	16	3	·	·	6
VIII	8	3.6	5.5	2.5	4	3.5	5.5	5.0	6.5	3.5	6.5	3.5	21.5	3.1	11.5	3.4	24	2.5	82	21.5	27	·	·	·	4	·	·	3	14	16	15	1	2	·	3
IX	1.5	4.3	11	4.7	7.5	6.2	6.5	4.8	14.5	4.3	17.5	3.9	10.5	3.8	2	6.0	19	3.5	125	53.9	4	·	·	·	1	1	·	6	9	12	11	3	2	·	1
X	7	6.2	3.5	3.3	2.5	4.6	1.5	2.3	12	3.2	17	4.2	12.5	3.6	15	4.6	22	3.2	19	5.5	18	·	·	3	·	1	·	2	12	5	5	·	10	·	·
XI	1	6.0	3	6.3	17	5.5	11.5	5.2	16	4.2	18.5	6.4	12	3.2	5	3.4	6	4.7	24	5.9	1	7	12	21	·	5	·	2	16	17	7	·	2	15	·
XII	1.5	2.3	·	·	·	·	11	8.1	29	5.3	25	4.6	14	2.8	2.5	7.8	10	4.5	29	8.5	29	2	6	25	·	6	·	·	16	11	7	·	2	13	·
Rok	80	5.0	121	5.0	93	4.5	112.5	5.2	142	4.1	147	4.1	151	3.8	114.5	5.1	134	4.2	624	53.9	4. IX	18	48	130	8	48	1	28	163	152	115	12	31	98	14

Kartuzy $H_s = 220\,m$ $h_w = 10\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	·	·	5	3.4	2	2.0	1	3.0	·	·	51	2.5	6	1.7	13	3.6	16	2.2	33	5.6	9	1	12	28	·	·	·	1	20	15	11	·	12	23	·
II	4	2.5	14	3.1	·	·	·	·	2	2.0	17	3.5	9	3.0	27	3.6	11	2.9	63	12.0	27	5	21	27	·	·	·	·	14	20	17	2	4	28	·
III	·	·	9	3.9	5	2.2	2	5.0	2	3.0	45	2.1	9	3.0	12	3.8	9	2.5	30	11.5	3	3	9	25	·	·	·	4	11	9	7	1	10	21	·
IV	3.5	3.9	12	3.0	3.5	4.4	2.5	2.6	16.5	2.4	30.5	1.6	10	3.4	7.5	2.6	4	2.4	47	12.3	23	·	·	9	·	·	·	2	16	13	10	2	4	·	·
V	10.5	2.6	14	3.5	8	2.6	5	3.0	7.5	3.5	17	2.1	17.5	3.2	10.5	3.4	3	2.9	54	19.3	17	·	·	3	·	·	·	6	8	10	9	1	3	·	1
VI	4	2.5	6	3.0	2	4.0	1	1.0	7	3.3	23	3.3	24	2.6	15	3.4	8	2.8	76	19.8	1	·	·	·	4	·	·	4	6	12	7	4	1	·	3
VII	6	3.0	3	3.7	·	·	1	1.0	1	3.0	64	2.8	5	4.2	9	3.2	4	2.8	111	22.8	15	·	·	·	2	·	·	1	17	22	20	3	3	·	5
VIII	1	1.0	·	·	·	·	·	·	1	3.0	24.5	1.4	34.5	2.2	12	1.7	20	1.5	100	26.6	24	·	·	·	4	·	·	1	9	17	17	3	1	·	4
IX	·	·	2	1.0	2	2.0	2	2.0	1	1.0	44.5	2.0	12.5	2.0	7	3.3	19	1.7	69	20.7	4	·	·	·	1	·	·	3	8	13	11	3	2	·	1
X	·	·	1	1.0	·	·	1	1.0	·	·	35	2.3	6	1.3	32	2.4	18	1.8	20	2.2	3	·	·	·	·	·	·	1	13	7	5	·	8	·	·
XI	·	·	4	2.0	·	·	9	1.0	1	1.0	47	3.5	4	1.5	10	1.8	15	2.3	62	13.2	21	6	13	22	·	2	·	·	22	20	13	1	2	18	·
XII	·	·	·	·	·	·	·	·	3	3.0	71	3.4	8	2.5	9	1.9	2	3.1	76	15.7	29	3	10	26	·	1	·	·	24	13	11	2	2	21	·
Rok	29	1.3	70	2.3	22.5	1.4	24.5	1.6	42	2.1	469.5	2.5	145.5	2.6	164	2.9	128	2.4	741	26.6	24.VIII	18	65	140	11	3	·	23	168	171	138	22	52	111	14

Tolkmicko — φ = 54°19' — λ = 19°32' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.0	-2.6	5.6	1	-13.5	11	-0.8	0.6	-0.4	-0.2	4.8	5.1	4.8	4.9	81	78	80	80	1.1	1.4	1.2	1.2	8.9	8.1	8.4	8.5
II	–	–	–	–	-0.4	-6.9	3.3	13	-15.8	6	-4.4	-2.3	-3.9	-3.6	3.7	4.1	3.8	3.9	81	77	80	79	0.8	1.2	0.9	1.0	7.4	6.8	8.6	7.7
III	–	–	–	–	4.3	-4.3	11.6	29	-25.4	8	-2.9	2.2	0.4	0.0	4.5	5.3	5.0	4.9	83	71	76	77	0.9	2.3	1.6	1.6	6.0	5.7	5.8	5.8
IV	–	–	–	–	9.7	2.9	17.2	28	-2.6	6	4.4	7.7	5.5	5.8	6.8	7.2	6.7	6.9	79	69	74	74	1.7	3.6	2.5	2.6	7.9	7.5	7.1	7.5
V	–	–	–	–	13.0	5.3	18.6	18	1.0	4	8.4	10.8	8.2	8.9	8.7	8.6	8.4	8.6	78	66	76	73	2.4	4.6	2.7	3.2	5.9	5.5	5.6	5.7
VI	–	–	–	–	20.0	11.4	29.6	26	5.0	4	14.5	18.4	14.8	15.6	13.0	12.6	13.0	12.9	79	61	77	72	3.8	9.3	4.1	5.7	5.8	4.4	5.8	5.3
VII	–	–	–	–	19.9	12.3	25.5	20	8.1	2	14.8	18.0	15.0	15.7	14.2	13.9	14.0	14.0	83	67	82	77	2.9	7.1	3.3	4.4	5.9	6.7	6.4	6.3
VIII	–	–	–	–	20.1	12.1	28.9	23	7.9	17	14.3	18.4	15.0	15.7	14.3	14.5	14.2	14.3	87	69	83	80	2.2	7.4	3.2	4.3	6.1	6.3	5.9	6.1
IX	–	–	–	–	20.0	11.5	27.8	3	6.8	16	12.7	18.2	14.4	14.9	13.1	14.0	13.9	13.7	88	67	84	80	1.9	7.5	2.7	4.0	5.2	5.9	5.3	5.5
X	–	–	–	–	12.7	6.2	17.8	1	1.0	21	7.7	11.3	8.7	9.1	9.3	10.4	9.5	9.7	88	76	84	83	1.4	3.2	1.8	2.1	7.5	6.7	6.9	7.0
XI	–	–	–	–	2.2	-3.0	11.6	1	-13.4	18	-1.4	0.7	-0.9	-0.6	5.1	5.2	5.3	5.2	85	75	84	81	0.9	1.6	1.0	1.2	7.7	7.5	8.4	7.9
XII	–	–	–	–	3.0	-1.3	10.5	19	-11.9	18	0.3	1.3	0.7	0.8	5.4	5.5	5.4	5.4	85	81	82	83	0.9	1.3	1.2	1.1	8.6	7.8	8.7	8.4
Rok	–	–	–	–	10.5	3.6	29.6	26.VI	-25.4	8.III	5.6	8.8	6.5	6.8	8.6	8.9	8.7	8.7	83	71	80	78	1.7	4.2	2.2	2.7	6.9	6.6	6.9	6.8

Gołdap — φ = 54°19' — λ = 22°19'

I	–	–	–	–	-0.4	-4.9	3.5	18	-14.2	10, 11	-2.7	-1.8	-2.8	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-3.0	-12.5	2.1	14	-28.7	6	-8.7	-4.7	-7.5	-7.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.5	-6.2	8.8	28	-26.3	1	-4.2	1.5	-2.1	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	9.5	1.5	16.4	28	-4.9	3	3.3	8.3	4.8	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.5	7.4	7.9
V	–	–	–	–	13.3	3.3	18.6	18	-5.9	4	7.4	11.9	7.6	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.8	5.5	6.6
VI	–	–	–	–	19.9	9.5	26.6	26	2.2	8	14.3	18.2	13.7	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.6	6.0	6.5
VII	–	–	–	–	19.6	10.3	28.4	15	4.1	5	14.6	18.0	13.6	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	7.3	6.2	6.3
VIII	–	–	–	–	19.3	10.0	26.3	22, 25	3.6	31	13.0	17.9	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	5.7	6.3
IX	–	–	–	–	19.2	9.5	25.8	4	4.5	21	11.8	18.1	12.8	13.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.0	2.8	5.1
X	–	–	–	–	10.8	4.2	17.4	1	-3.9	21	5.8	9.9	6.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.0	7.1	7.9
XI	–	–	–	–	-0.3	-4.8	10.0	2	-19.0	24	-3.3	-1.2	-2.7	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.6	8.5	8.6
XII	–	–	–	–	1.0	-3.6	7.3	19, 20	-16.8	15	-1.0	-0.4	-1.2	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	9.2	8.8	9.0
Rok	–	–	–	–	9.3	1.4	28.4	15.VII	-28.7	6.II	4.2	8.0	4.7	5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Hopowo — φ = 54°16' — λ = 18°14'

I	–	–	–	–	0.0	-4.1	3.7	18	-12.8	11	-2.7	-0.8	-1.6	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	7.7	8.1
II	–	–	–	–	-1.8	-8.3	2.1	13	-16.2	26	-5.9	-2.7	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	6.5	7.4
III	–	–	–	–	2.7	-4.3	9.4	29	-14.2	8	-2.8	1.5	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.4	5.2	6.1
IV	–	–	–	–	8.1	0.8	13.1	6	-3.1	5	2.5*	7.1	2.8*	3.8*	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.9	6.9	7.4
V	–	–	–	–	11.7	3.6	17.0	17	-2.5	2	6.6	11.1	5.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.4	5.0	5.8
VI	–	–	–	–	18.1	9.2	28.1	26	3.3	1, 4	13.0	17.6	12.4	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	5.1	5.7
VII	–	–	–	–	16.9	10.3	26.5	14	6.2	5	12.7	16.5	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.4	6.8	7.1
VIII	–	–	–	–	19.0	10.0	27.0	22	5.9	16	12.5	18.1	12.5	13.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	5.5	6.3
IX	–	–	–	–	18.2	9.2	26.3	3	5.9	16	10.9	17.1	11.8	12.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.1	4.1	5.5
X	–	–	–	–	11.8	4.2	17.9	1	-1.4	26	6.0	11.1	6.8	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	5.6	6.8
XI	–	–	–	–	0.8	-4.5	10.6	1	-15.2	18	-2.9	-0.3	-2.1	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	7.4	8.1
XII	–	–	–	–	0.8	-3.3	9.3	19	-12.7	18	-1.7	-0.3	-1.3	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.8	8.5	8.8
Rok	–	–	–	–	8.9	1.9	28.1	26.VI	-16.2	26.II	4.0	8.0	4.5	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.3	6.2	6.9

Bartoszyce — φ = 54°15' — λ = 20°48'

I	–	–	–	–	0.8	-3.8	4.7	1	-12.6	11	-1.7	-0.4	-1.5	-1.3	4.9	5.2	4.9	5.0	88	85	86	86	0.6	0.9	0.7	0.7	8.0	7.2	7.6	7.6
II	–	–	–	–	-2.0	-11.4	3.0	13	-27.0	5	-7.0	-3.8	-6.7	-6.0	3.3	3.7	3.4	3.5	84	78	84	82	0.6	1.0	0.6	0.7	8.0	6.2	6.9	7.0
III	–	–	–	–	3.5	-6.3	9.6	28	-26.7	9	-4.4	1.7	-1.6	-1.5	4.4	5.2	4.9	4.8	89	72	83	81	0.5	2.1	1.0	1.2	6.3	5.2	5.2	5.6
IV	–	–	–	–	9.9	1.6	17.2	28	-3.3	3	3.5	8.6	5.1	5.6	6.7	7.1	6.9	6.9	84	64	78	75	1.3	4.3	2.1	2.6	7.5	7.3	6.7	7.2
V	–	–	–	–	13.7	3.5	18.6	18, 29	-4.1	4	7.5	12.5	8.0	9.0	9.6	8.1	8.5	8.4	81	55	77	71	2.0	6.7	2.4	3.7	6.4	6.6	5.2	6.1
VI	–	–	–	–	20.3	9.1	28.6	26	1.6	8	14.2	18.4	14.4	15.4	13.2	12.7	13.2	13.0	81	62	80	74	3.1	9.0	3.5	5.2	5.2	5.6	5.5	5.4
VII	–	–	–	–	19.8	10.8	29.2	14	5.1	5	14.2	18.3	14.2	15.2	13.6	13.2	14.1	13.6	83	62	86	77	2.8	8.3	2.4	4.5	6.0	7.0	6.1	6.4
VIII	–	–	–	–	20.5	9.6	27.7	22, 23	4.9	2	12.7	18.6	13.5	14.6	13.6	14.1	14.1	13.9	92	66	91	83	1.4	8.2	1.7	3.8	6.5	6.5	5.6	6.2
IX	–	–	–	–	20.0	8.4	27.0	3	4.2	16, 24, 25	11.0	18.3	12.7	13.7	12.4	14.6	13.5	13.5	93	70	90	84	1.0	6.9	1.6	3.2	5.9	5.6	4.0	5.2
X	–	–	–	–	12.3	4.2	19.2	1	-3.2	21	5.9	11.1	7.4	8.0	8.9	10.2	9.4	9.5	94	77	89	87	0.6	3.2	1.1	1.6	7.6	7.3	6.0	7.0
XI	–	–	–	–	0.6	-5.0	10.3	2	-23.4	24	-2.9	-0.6	-1.9	-1.8	4.9	5.3	5.2	5.1	86	83	88	86	0.7	1.2	0.6	0.8	7.9	7.9	7.5	7.8
XII	–	–	–	–	2.3	-2.6	10.2	19, 20	-17.5	17	-0.3	0.8	-0.2	0.0	5.4	5.6	5.5	5.5	87	85	86	86	0.8	1.0	0.8	0.9	8.7	8.5	7.2	8.1
Rok	–	–	–	–	10.1	1.5	29.2	14.VII	-27.0	5.II	4.4	8.6	5.3	5.9	8.3	8.8	8.6	8.6	87	72	85	81	1.3	4.4	1.5	2.4	7.0	6.7	6.1	6.6

Tolkmicko $H_s = 1\ m$ $h_w = 19\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v v>10	v>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4	6.5	3.5	3.6	5	4.2	22	4.7	14.5	4.8	25.5	6.5	0.5	12.0	7	7.9	11	5.0	36	11.5	8	2	6	23	·	10	·	·	19	22	11	1	·	20	·
II	2.5	8.0	21.5	5.0	4.5	2.1	2.5	4.6	3.5	4.1	22.5	6.2	9	4.1	14	8.4	4	5.4	57	9.2	22	5	14	26	·	12	·	·	15	21	17	·	·	28	·
III	1	6.0	8	6.2	8.5	2.9	14	4.8	8.5	3.1	37	3.8	3	3.7	6	5.0	7	3.8	33	11.4	3	4	9	21	·	2	·	6	10	13	7	1	1	17	·
IV	6	3.7	6	4.8	15	5.1	27	5.3	6	4.8	8	4.0	10	3.2	5	3.8	7	4.2	49	17.5	21	·	-	4	·	5	·	3	15	15	8	1	3	·	1
V	12	5.0	12	5.8	13.5	3.9	10.5	5.9	2	3.5	10	4.6	9	4.7	16	4.8	8	4.5	21	5.3	9	·	·	·	·	7	·	5	10	12	6	·	4	·	·
VI	5.5	3.5	15	3.7	10.5	5.2	10	6.0	8.5	5.9	21.5	5.9	12.5	6.1	6.5	4.1	·	5.2	88	26.9	22	·	·	·	3	9	·	3	8	14	12	3	1	·	4
VII	1.5	1.0	9.5	5.7	3.5	6.6	12	4.0	1.5	4.3	46	6.7	13	5.3	1	2.0	5	5.5	139	29.9	14	·	·	·	1	8	·	2	8	22	18	4	·	·	8
VIII	4.5	5.2	2	3.5	·	·	6.5	8.7	2	2.8	29	3.0	18.5	3.2	15.5	6.7	15	3.8	120	42.5	27	·	·	·	5	4	·	3	10	17	15	2	·	·	3
IX	·	·	2	4.0	1.5	4.7	25	4.5	12	5.1	31	5.7	6.5	5.6	5	6.4	7	4.8	142	63.6	4	·	-	·	1	6	·	4	6	12	8	5	·	·	1
X	7	7.7	5	2.6	1	6.0	8.5	3.2	3.5	3.3	36	5.3	10	5.0	12	5.2	10	4.5	29	7.5	16	·	-	·	·	6	·	2	10	11	6	·	2	·	·
XI	1.5	6.0	7	5.9	18.5	3.5	8	6.8	10	8.0	31.5	6.3	4.5	5.4	5	3.0	4	5.4	49	15.5	21	5	12	20	·	12	·	·	15	18	11	1	1	16	·
XII	·	·	·	·	·	·	11	5.5	22	5.7	52	6.4	3	3.8	4	7.2	1	6.0	38	16.3	18	2	4	20	·	10	·	·	19	21	6	1	1	15	·
Rok	45.5	4.4	91.5	4.2	81.5	3.7	157	5.3	94	5.0	350	5.4	99.5	5.2	97	5.4	79	4.8	801	63.6	4. IX	18	45	114	10	91	-	28	145	198	125	19	13	96	17

Gołdap $H_s = 150\ m$ $h_w = $ 15,5 m I - VII; 11,2 m VIII - XII

I	2	1.5	3.5	2.0	12.5	3.0	19	2.9	13	3.5	15.5	4.1	5	6.0	4.5	4.4	18	2.8	47	8.2	8	5	15	29	·	2	·	—	—	15	10	·	5	18	·
II	13	2.9	5	1.2	4	2.8	1	2.0	5	3.0	19.5	3.6	8.5	3.4	13	2.8	15	2.5	45	6.2	27	15	23	28	·	3	·	—	—	19	12	·	1	28	·
III	2	1.5	4	1.8	7.5	2.9	11.5	3.4	7	1.7	11	1.8	17.5	2.0	6.5	2.0	26	1.6	16	4.9	3	7	9	24	·	·	·	—	—	10	5	·	8	22	·
IV	3	2.3	9.5	3.6	19.5	4.1	25	3.5	11	2.7	3	1.0	6.5	2.0	3.5	2.6	9	2.9	26	8.8	23	·	·	10	·	1	·	1	20	7	5	·	4	·	1
V	11	2.6	9	2.1	12	2.3	6	3.3	7	2.7	4.5	2.7	8.5	2.8	13	2.1	22	1.9	53	16.8	19	·	-	6	·	·	·	1	9	12	7	2	1	·	1
VI	4	1.8	5	2.2	9	2.8	7	2.1	7	3.0	14	2.1	14.5	2.6	11.5	2.3	18	1.9	69	20.7	19	·	-	·	2	·	·	1	12	11	11	3	2	·	2
VII	1.5	3.3	5.5	4.0	7	2.0	5	2.0	12.5	1.8	33	3.1	13.5	2.7	2	3.0	13	2.3	134	29.5	22	·	-	·	3	·	-	1	9	20	19	3	2	·	4
VIII	2	3.0	0.5	2.0	3.5	1.1	8.5	3.2	4.5	3.4	14	3.4	19	2.4	20	2.8	21	2.2	65	14.6	9	·	-	·	5	·	·	3	14	12	9	2	7	·	2
IX	·	·	2	1.0	7.5	2.5	15.5	4.0	9	3.6	25	2.8	14.5	4.4	3.5	4.6	13	2.9	38	22.9	29	·	·	·	2	2	·	1	4	11	5	1	7	·	3
X	2	3.5	3	2.0	1	3.0	4	4.8	1	8.0	15.5	3.2	31.5	3.1	17	2.4	18	2.5	19	8.3	16	·	·	4	·	·	·	·	14	8	6	·	10	·	·
XI	1	1.0	15.5	2.1	13.5	2.9	8	6.0	5	4.0	17.5	3.4	15	3.0	4.5	2.2	10	2.8	39	7.2	1	6	16	20	·	1	·	·	15	16	8	·	5	18	·
XII	·	·	·	·	3	2.7	9	5.9	10	4.0	39.5	5.5	19	3.2	3.5	2.3	9	4.2	26	7.3	5	4	11	25	·	2	1	1	23	15	11	·	1	23	·
Rok	41.5	2.0	62.5	2.0	100	2.7	119.5	3.6	92	3.4	212	3.1	173	3.1	102.5	2.8	192	2.5	577	29.5	22. VII	37	74	146	12	11	1	—	—	156	108	11	53	109	13

Hopowo $H_s = 220\ m$ $h_w = 11\ m$

I	0.5	5.0	6.5	2.3	2.5	2.4	5.5	5.5	21	6.3	15.5	4.6	6	4.7	7.5	4.6	28	3.5	38	4.9	9	3	16	28	·	2	·	·	17	20	13	·	9	24	·
II	8.5	3.8	10.5	4.5	0.5	3.0	0.5	3.0	1	5.0	12	4.8	13.5	4.0	12.5	4.3	25	3.0	55	13.6	27	6	21	28	·	·	·	·	13	23	15	1	4	28	·
III	3.5	3.6	10	4.4	3.5	3.9	6	4.2	15	3.8	22	3.3	10.5	3.7	7.5	4.0	15	3.2	25	5.5	21	3	9	25	·	·	·	4	10	14	7	·	12	24	·
IV	3	3.0	11	4.0	6.5	4.2	17	5.0	11.5	4.4	6.5	3.4	6	3.4	8.5	3.8	20	3.2	51	13.2	23	·	·	10	·	·	·	·	14	13	9	2	6	·	1
V	8	4.1	19	4.1	6	3.9	9	4.5	4.5	4.9	4	3.2	7	4.6	13.5	4.6	22	3.3	42	17.7	7	·	·	5	·	·	·	4	8	11	8	1	4	·	1
VI	4	3.6	12.5	3.9	3.5	3.7	4	4.1	5	5.8	14	4.5	14.5	3.8	11.5	3.6	21	3.1	72	27.3	1	·	·	·	1	1	·	3	6	11	7	3	1	·	5
VII	1	4.0	9	3.3	3.5	3.0	3	3.2	6.5	3.8	35	4.3	15.5	4.5	7.5	4.5	12	3.6	117	21.5	15	·	·	·	2	·	·	2	10	24	17	3	4	·	7
VIII	2.5	3.4	·	·	·	·	2.5	6.6	7	5.5	8.5	3.8	11	3.2	15.5	2.9	46	1.9	108	43.3	24	·	·	·	4	·	·	1	8	17	15	3	5	·	5
IX	1	4.0	2	3.0	2	3.5	5.5	3.5	16	5.9	23.5	4.6	8	3.6	3	4.2	29	3.1	78	22.4	4	·	·	·	1	2	·	5	5	14	12	4	5	·	3
X	3	3.5	2	2.0	1.5	3.0	1	3.5	7	4.4	18.5	4.6	10.5	3.3	10.5	3.9	39	2.3	28	12.9	3	·	·	1	·	·	·	1	12	7	6	1	14	·	·
XI	2.5	2.0	2	5.2	5.5	3.6	8.5	4.6	9.5	5.3	21	5.9	9	3.9	4	3.6	28	3.3	46	7.9	1	7	14	21	·	3	1	2	20	24	14	·	9	17	·
XII	·	·	·	·	·	·	8	6.6	21	6.3	32.5	6.3	9.5	3.9	3	4.2	19	4.7	67	15.4	28	3	10	28	·	5	2	·	23	20	13	2	5	22	·
Rok	37.5	3.3	84.5	3.1	35	2.8	70.5	4.5	125	5.1	213	4.4	121	3.9	104.5	4.0	304	3.2	727	43.3	24. VIII	22	70	146	8	13	3	22	146	198	136	20	78	115	22

Bartoszyce $H_s = 60\ m$ $h_w = 11\ m$

I	3	1.7	6	2.6	16.5	2.9	7	2.6	18.5	3.5	20.5	2.7	11	5.5	3.5	3.1	7	3.0	26	6.0	8	2	9	26	·	1	·	·	17	17	7	·	·	9	·
II	11	4.0	6	3.7	4	2.2	·	·	5	5.1	18	4.2	13	4.5	11	2.7	16	3.1	29	4.5	13	15	18	27	·	2	·	1	11	21	10	·	3	28	·
III	9.5	3.3	9.5	2.5	3.5	2.9	6.5	2.2	17	2.4	18	2.8	6.5	2.3	2.5	5.6	20	2.1	28	11.4	21	7	8	26	·	·	·	5	10	11	5	1	5	18	·
IV	9.5	3.4	11	3.4	15.5	3.2	20.5	2.9	14.5	2.9	4	2.6	4.5	2.8	5.5	2.4	5	2.9	28	9.3	21	·	·	11	·	·	·	2	15	13	5	·	3	·	2
V	15.5	2.5	9	2.9	10.5	3.5	7.5	2.3	7.5	2.6	4.5	3.7	14	3.6	19.5	2.5	5	2.8	37	10.0	25	·	·	3	·	·	·	3	9	12	9	1	1	·	·
VI	11	2.8	8	3.0	7	3.4	4	3.1	10	3.6	9.5	3.6	27.5	3.3	11	2.3	2	3.1	53	14.3	19	·	·	·	3	·	·	4	8	11	10	2	·	·	4
VII	6.5	3.0	5.5	3.1	7	1.9	4.5	1.9	18.5	3.0	32	3.0	12.5	3.7	2.5	2.6	4	2.8	111	24.2	16	·	·	·	2	·	·	1	8	19	16	4	1	·	7
VIII	4.5	2.1	·	·	5.5	1.5	9	2.2	6	1.8	10.5	2.1	20	1.9	15.5	2.1	22	1.5	88	26.8	25	·	·	·	7	·	·	2	9	15	9	4	·	·	4
IX	0.5	1.0	3.5	1.4	9.5	2.0	10.5	2.1	14.5	2.5	22	4.8	9.5	2.8	5	2.6	15	2.1	56	25.8	29	·	·	·	1	·	·	5	6	12	8	1	4	·	·
X	0.5	2.0	5.5	1.6	1.5	1.3	0.5	2.0	4	1.9	33	2.6	13	2.2	20	2.2	15	1.9	30	9.8	16	·	·	4	·	·	·	1	12	8	6	·	7	·	·
XI	4	1.9	18.5	2.4	5.5	3.1	9	2.9	9.5	2.9	21.5	4.2	9	3.8	3	2.5	10	2.8	39	9.1	21	8	14	21	·	·	·	1	17	17	10	·	·	16	·
XII	·	·	·	·	1	7.0	14.5	2.7	19	3.2	48	4.0	8.5	2.2	·	·	2	3.4	34	10.8	18	4	4	23	·	1	·	1	17	20	10	1	·	12	·
Rok	75.5	2.3	82.5	2.2	87	2.5	93.5	2.2	144	3.0	241.5	3.4	149	3.2	99	2.6	123	2.6	559	26.8	25. VIII	36	53	141	13	4	·	26	139	176	105	14	24	83	17

Koszalin — φ = 54°12′ — λ = 16°10′ — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1005.4	1022.3	980.6	1009.7	2.4	−1.8	6.4	17	−10.1	31	−0.1	1.5	0.3	0.5	5.4	5.7	5.4	5.5	89	83	86	86	0.7	1.2	0.9	0.9	8.1	7.6	7.5	7.7
II	1012.2	1031.3	981.2	1016.5	0.5	−6.0	3.6	13	−15.8	17	−2.7	−0.4	−2.5	−2.0	4.2	4.6	4.1	4.3	81	76	79	79	0.9	1.4	1.1	1.1	8.8	7.9	7.5	8.1
III	1011.8	1027.8	987.9	1016.1	4.5	−2.5	12.3	29	−14.8	8	−1.1	3.1	0.8	0.9	5.2	5.9	5.6	5.6	88	76	83	82	0.7	2.0	1.1	1.3	6.7	6.7	4.9	6.1
IV	1006.9	1028.6	984.9	1011.1	10.5	2.7	16.1	6, 22	−3.0	5	4.2	9.0	5.7	6.2	7.3	7.5	7.4	7.4	87	66	80	78	1.1	4.3	1.9	2.4	8.0	8.0	6.9	7.6
V	1010.1	1025.2	988.8	1014.2	13.0	4.3	19.1	17	−1.6	3	7.7	11.3	7.9	8.7	8.6	8.7	8.4	8.6	82	65	78	75	1.9	4.9	2.4	3.1	6.8	7.1	5.9	6.6
VI	1009.8	1020.1	994.1	1013.9	20.0	9.8	29.5	26	2.0	4	13.9	18.2	13.8	14.9	12.3	12.4	12.3	12.3	77	60	78	72	3.8	9.1	3.8	5.6	6.1	6.9	5.4	6.1
VII	1005.7	1018.3	987.7	1009.8	18.6	10.9	25.4	21	5.8	2	13.5	16.8	13.6	14.4	13.6	13.2	13.6	13.5	87	69	87	81	2.1	6.3	2.3	3.6	7.1	7.7	6.3	7.0
VIII	1010.8	1020.0	998.8	1014.9	19.2	9.9	27.9	22	5.7	17	13.0	17.9	13.0	14.2	13.5	13.6	13.4	13.5	90	66	89	82	1.7	7.3	1.9	3.6	6.4	6.9	4.9	6.1
IX	1008.5	1029.1	995.4	1012.6	18.9	10.5	26.6	3	6.8	12	11.8	17.7	13.0	13.9	12.3	13.5	13.0	12.9	89	68	86	81	1.6	7.2	2.3	3.7	6.8	6.9	5.4	6.4
X	1018.0	1033.6	999.7	1022.2	12.8	4.9	20.5	1	−0.3	26	6.5	12.0	7.8	8.5	9.3	10.5	9.5	9.8	93	74	88	85	0.7	3.7	1.3	1.9	7.9	7.1	4.7	6.6
XI	1006.0	1025.5	974.7	1010.3	2.6	−2.5	11.9	1	−11.9	24	−0.7	1.6	−0.2	0.1	5.6	6.1	5.6	5.8	90	82	86	86	0.6	1.2	0.8	0.9	8.4	8.4	6.2	7.7
XII	997.3	1019.3	968.0	1001.5	2.5	−1.2	10.9	19	−7.5	16	0.4	1.2	0.7	0.8	5.8	5.9	5.9	5.9	89	87	90	89	0.7	0.9	0.6	0.7	9.0	9.0	8.8	8.9
Rok	1008.5	1033.6	968.0	1012.7	10.5	3.2	29.5	26.VI	−15.8	17. II	5.5	9.2	6.2	6.8	8.6	9.0	8.7	8.8	87	73	84	81	1.4	4.1	1.7	2.4	7.5	7.5	6.2	7.1

Kołobrzeg — φ = 54°11′ — λ = 15°35′

I	1009.1	1026.7	989.0	1009.9	3.1	−1.3	7.6	17	−7.7	31	0.3	1.9	0.6	0.8	5.5	5.8	5.6	5.6	87	83	86	85	0.8	1.2	0.9	1.0	8.3	8.3	7.4	8.0
II	1016.3	1034.8	989.0	1017.1	1.3	−3.7	5.1	13	−12.9	17	−1.7	0.1	−1.3	−1.0	4.5	4.8	4.3	4.5	81	76	76	78	1.0	1.4	1.3	1.2	8.1	8.2	7.6	8.0
III	1015.5	1031.8	994.2	1016.3	4.8	−2.0	12.9	29	−14.2	8	−0.7	3.1	0.7	1.0	5.3	5.8	5.6	5.6	87	75	84	82	0.7	2.0	1.0	1.2	6.9	6.4	5.6	6.3
IV	1010.5	1032.6	990.2	1011.2	9.7	2.7	16.4	6	−2.6	5	4.0	7.8	5.3	5.6	7.2	7.3	7.3	7.3	88	71	82	80	1.0	3.4	1.7	2.0	7.9	8.2	6.8	7.6
V	1013.8	1028.5	993.2	1014.5	11.3	5.3	18.9	17	−1.8	3	7.7	9.7	7.9	8.3	8.7	9.2	8.8	8.9	82	76	83	80	1.9	3.0	1.9	2.3	6.5	6.1	6.2	6.3
VI	1013.4	1023.9	997.9	1014.1	18.1	10.6	29.1	26	3.4	4	13.6	16.4	13.7	14.4	12.4	12.5	12.5	12.5	80	68	80	76	3.4	7.1	3.4	4.6	6.0	5.9	5.9	5.9
VII	1009.3	1021.8	992.3	1010.0	17.9	11.3	25.0	21	8.1	4	13.8	16.2	14.3	14.6	13.4	13.3	13.6	13.4	85	73	83	80	2.4	5.3	2.9	3.5	7.3	7.7	6.9	7.3
VIII	1014.3	1023.8	1001.6	1015.0	18.9	10.6	28.1	22	5.4	14	13.9	17.4	13.8	14.7	13.7	14.3	13.7	13.9	86	72	87	82	2.3	5.9	2.3	3.5	5.8	6.6	5.4	5.9
IX	1011.8	1032.6	998.1	1012.5	19.0	10.3	25.7	3	6.7	6	12.1	18.0	13.2	14.1	12.5	13.3	13.2	13.0	89	65	87	80	1.7	7.8	2.1	3.9	6.7	7.1	6.0	6.6
X	1021.7	1037.3	1003.0	1022.4	13.2	5.4	18.8	2	0.0	20	7.3	12.1	8.4	9.0	9.4	10.6	9.6	9.9	90	75	86	84	1.1	3.7	1.7	2.2	7.5	7.2	5.8	6.8
XI	1009.9	1028.9	982.2	1010.7	3.3	−2.0	12.3	1	−11.0	18	−0.2	2.1	0.2	0.6	5.6	6.0	5.7	5.8	85	78	84	82	0.8	1.5	0.9	1.1	8.6	7.8	7.3	7.9
XII	1001.0	1023.1	976.0	1001.8	3.3	−0.7	11.6	19	−6.9	17	0.9	1.8	1.2	1.3	5.8	6.1	6.0	6.0	87	85	88	87	0.9	1.0	0.8	0.9	9.0	9.0	8.8	8.9
Rok	1012.2	1037.3	976.0	1012.9	10.5	3.9	29.1	26.VI	−14.2	8. III	5.9	8.9	6.5	7.0	8.7	9.1	8.8	8.9	86	75	84	82	1.5	3.6	1.7	2.3	7.4	7.4	6.6	7.1

Kmiecin — φ = 54°11′ — λ = 19°10′

I	—	—	—	—	1.3	−4.0	4.5	1,9,17,18	−17.1	11	−1.8	0.3	−1.3	−1.0	4.8	5.3	4.9	5.0	87	84	87	86	0.7	1.0	0.7	0.8	8.0	7.6	8.1	7.9
II	—	—	—	—	−1.2	−8.5	2.0	13	−19.6	5	−5.2	−2.4	−4.6	−4.2	3.7	4.3	3.9	4.0	84	81	85	83	0.6	1.0	0.6	0.7	8.1	7.6	8.5	8.1
III	—	—	—	—	2.6	−6.1	11.5	29	−26.6	8	−3.9	1.6	−1.4	−1.3	4.5	5.3	5.0	4.9	86	75	86	82	0.6	1.9	0.8	1.1	5.5	6.3	6.1	6.0
IV	—	—	—	—	9.8	2.3	16.6	28	−3.3	3	4.4	8.6	4.8	5.6	6.9	7.0	7.1	7.0	81	63	80	75	1.7	4.5	1.9	2.7	8.1	6.9	7.1	7.4
V	—	—	—	—	13.3	4.0	19.8	18	−2.8	4	8.3	12.1	7.2	8.7	8.5	8.1	8.4	8.3	76	58	81	72	2.6	6.1	2.0	3.6	6.4	5.2	6.2	5.9
VI	—	—	—	—	20.1	9.3	28.4	26	3.0	8	14.5	19.0	13.4	15.1	13.1	12.7	13.2	13.0	79	59	85	74	3.6	9.9	2.5	5.3	5.5	4.8	4.9	5.1
VII	—	—	—	—	20.1	10.7	28.4	15	5.2	5	14.5	18.6	13.7	15.1	14.0	13.8	13.9	13.9	84	64	88	79	2.7	8.1	2.0	4.3	5.7	5.8	6.6	6.0
VIII	—	—	—	—	20.1	10.1	29.0	23	5.2	17	13.4	19.1	13.7	15.0	13.3	13.8	13.8	13.7	88	63	88	80	1.9	9.0	2.1	4.3	6.5	5.5	6.1	6.0
IX	—	—	—	—	19.5	9.5	27.6	3	3.2	16	11.9	18.6	12.9	14.1	12.6	14.4	13.3	13.4	90	67	89	82	1.9	7.4	1.7	3.7	5.7	5.8	5.1	5.5
X	—	—	—	—	12.2	4.4	18.2	1	−0.9	21	6.2	11.7	7.4	8.2	8.9	10.6	9.4	9.6	92	76	90	86	0.7	3.4	1.0	1.7	7.3	6.5	5.5	6.4
XI	—	—	—	—	1.5	−4.0	11.0	1, 2	−16.0	24	−1.7	0.3	−1.6	−1.2	5.4	5.9	5.4	5.6	88	85	90	88	0.6	0.9	0.6	0.7	8.3	7.1	6.1	7.2
XII	—	—	—	—	1.7	−2.6	9.1	19	−19.0	17	−0.7	0.5	−0.2	−0.2	5.4	5.8	5.5	5.6	90	88	89	89	0.6	0.8	0.7	0.7	7.9	7.5	7.8	7.7
Rok	—	—	—	—	10.1	2.1	29.0	23.VIII	−26.6	8. III	5.0	9.0	5.3	6.2	8.4	8.9	8.6	8.6	85	72	86	81	1.5	4.5	1.4	2.5	6.9	6.4	6.5	6.6

Żelisławki — φ = 54°10′ — λ = 18°39′

I	—	—	—	—	0.9	−3.9	4.8	1	−13.6	11	−1.7	−0.1	−1.2	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.6	6.8	6.9
II	—	—	—	—	−0.8	−8.4	2.6	13	−17.4	6	−4.6	−2.3	−4.4	−3.9	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.4	6.4	6.9
III	—	—	—	—	3.4	−4.6	10.3	29	−20.2	8	−2.6	2.0	−0.5	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	5.1	4.8	5.7	5.2
IV	—	—	—	—	9.4	2.0	14.4	28	−2.8	6	3.5	8.0	4.7	5.2	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.5	6.3	7.1
V	—	—	—	—	13.2	4.4	18.7	13	−0.9	4	7.9	11.8	7.3	8.6	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.7	5.3	5.1
VI	—	—	—	—	20.0	10.3	28.8	26	5.2	4	14.3	18.9	13.7	15.2	—	—	—	—	—	—	—	—	—	—	—	—	4.8	4.3	3.9	4.3
VII	—	—	—	—	19.5	11.0	28.5	14	6.2	2	14.0	17.9	13.7	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.6	6.4	6.2
VIII	—	—	—	—	19.9	10.3	28.4	6, 23	6.7	16	13.5	18.7	13.7	14.9	—	—	—	—	—	—	—	—	—	—	—	—	5.1	6.1	4.6	5.3
IX	—	—	—	—	19.2	9.6	27.0	3	5.3	16	11.2	18.1	12.9	13.8	—	—	—	—	—	—	—	—	—	—	—	—	5.0	4.3	3.4	4.2
X	—	—	—	—	12.4	4.8	19.1	1	0.0	21	6.6	11.8	7.6	8.4	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.1	4.5	5.8
XI	—	—	—	—	1.3	−4.1	10.7	1, 2	−15.7	24	−2.1	−0.1	−1.3	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.3	6.8	6.9	7.3
XII	—	—	—	—	1.9	−2.3	10.3	19	−13.2	17	−0.5	0.5	0.0	0.0	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.0	7.4	8.2
Rok	—	—	—	—	10.0	2.4	28.8	26. VI	−20.2	8. III	5.0	8.8	5.5	6.2	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.0	5.6	6.0

Koszalin — $H_s = 33\,m$ — $H_b = 33{,}9\,m$ — $h_w = 15\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10	Max<0°	Min<0°	Max>25°	Wiatr v >10	>15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	6	2.7	4	5.0	3	2.0	17.5	3.9	25	6.2	22.5	5.2	5.5	6.7	4.5	5.4	5	4.8	38	8.1	8	1	3	22	·	2	1	1	18	18	14	·	5	12	·
II	15.5	6.0	11.5	6.8	3.5	1.6	4	2.9	7	3.1	16.5	5.5	12	5.2	11	5.0	3	5.0	21	4.9	15	5	11	26	·	7	2	·	15	19	8	·	5	27	·
III	9.5	4.4	11.5	5.0	3	2.0	16	3.9	23	4.2	15.5	4.3	11.5	5.6	2	3.5	1	4.3	16	4.6	3	2	7	21	·	3	·	5	11	14	7	·	7	17	·
IV	8.5	4.0	10.5	4.0	9	4.4	21.5	5.0	15	4.9	3.5	5.3	8.5	5.2	10.5	4.4	3	4.5	35	8.3	13	·	·	3	·	2	·	1	14	12	9	·	5	·	1
V	17.5	4.1	16.5	3.3	8.5	3.0	17	5.2	5	3.6	8.5	4.2	8.5	4.7	10.5	4.6	1	4.1	66	20.7	9	·	·	1	·	5	·	3	13	16	7	3	9	·	2
VI	10	4.6	13.5	3.2	4	2.2	9	4.1	10	4.8	13.5	4.6	15.5	6.2	13.5	5.3	1	4.6	31	8.6	18	·	·	·	3	3	·	4	8	10	6	·	2	·	4
VII	3	3.0	10	3.8	1	2.0	11	4.2	11.5	4.0	36	5.4	12.5	5.6	7	5.6	1	4.8	138	16.6	12	·	·	·	2	3	·	3	12	23	23	3	4	·	10
VIII	12	2.7	3	1.0	0.5	1.0	13	3.4	15.5	2.6	19	3.4	12.5	2.6	10.5	5.2	7	2.9	81	14.9	8	·	·	·	4	2	·	1	7	13	10	4	5	·	6
IX	1.5	3.0	0.5	3.0	2.5	4.2	23.5	4.1	20.5	4.2	24	5.2	11.5	5.1	4	2.5	2	4.3	119	26.9	18	·	·	·	1	4	·	3	8	17	14	4	4	·	3
X	5	2.6	6.5	1.5	2.5	1.6	9	2.9	18.5	3.1	25.5	4.6	8.5	3.8	10.5	3.8	7	3.2	19	9.8	2	·	·	1	·	1	·	·	6	7	4	·	13	·	·
XI	3	3.7	8	2.6	7	2.4	13	4.6	18.5	5.0	26	6.6	5	5.0	2.5	5.4	7	4.6	43	8.6	1	5	10	18	·	3	1	·	16	18	12	·	4	10	·
XII	3	4.2	1	3.0	·	·	14	4.9	22.5	5.6	35	7.1	11	6.2	4.5	4.1	2	5.9	90	17.0	18	·	3	18	·	7	1	·	26	20	16	3	2	14	·
Rok	94.5	3.8	96.5	3.5	44.5	2.2	168.5	4.1	192	4.3	245.5	5.1	122.5	5.2	91	4.6	40	4.4	697	26.9	18. IX	13	34	110	10	42	5	21	154	187	130	17	65	80	26

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47

Kołobrzeg — $H_s = 3\,m$ — $H_b = 5{,}4\,m$ — $h_w =$ 13 m wiatromierz Wilda, 20 m anemometr Fuess

I	5.5	2.9	6	5.2	6.5	4.1	15	3.0	21	4.6	22	4.8	5	4.3	5	3.8	7	3.9	42	7.1	8	·	2	19	·	3	·	·	17	19	14	·	5	9	·
II	16	5.7	15.5	5.8	3	3.7	2	3.0	4	3.6	15.5	4.6	13	5.4	12	4.8	3	4.9	29	4.2	13	2	6	23	·	4	·	·	16	22	10	·	4	27	·
III	5	5.4	13	5.2	4.5	4.2	6.5	3.5	25.5	2.5	16.5	3.3	15.5	3.7	4.5	3.9	2	3.6	34	17.9	3	1	4	21	·	1	·	5	11	14	6	1	5	16	·
IV	2.5	4.4	21.5	5.0	8.5	5.0	17	5.1	8	3.8	8	2.9	15.5	3.3	6	3.8	3	4.2	31	7.2	26	·	·	3	·	·	·	1	15	15	10	·	7	·	1
V	8	4.8	31	5.0	8.5	3.8	8.5	4.8	4.5	3.0	4.5	3.6	18.5	4.1	5.5	4.1	4	4.2	58	18.9	9	·	·	1	·	2	·	3	12	14	8	2	6	·	·
VI	4	2.5	23	4.5	4.5	2.7	5.5	2.9	5	4.7	12	4.0	24.5	4.5	4.5	3.6	7	3.8	21	5.9	18	·	·	·	3	1	·	3	6	9	6	·	1	·	4
VII	2	2.8	15	5.3	3.5	4.1	3.5	3.1	8.5	3.8	33	4.5	23	5.7	2.5	3.8	2	4.6	105	16.1	12	·	·	·	·	1	·	1	13	22	21	4	4	·	3
VIII	12	2.5	3.5	3.4	4.5	2.3	5	2.5	9	2.7	17.5	2.7	18.5	3.9	5	3.8	18	2.5	63	20.8	23	·	·	·	2	·	·	3	8	15	10	1	3	·	5
IX	3	2.0	4	5.0	11	4.0	13	3.7	14.5	2.8	22	4.1	13.5	4.7	1	7.0	8	3.5	84	24.4	3	·	·	·	2	1	·	2	11	14	12	4	2	·	3
X	9	2.7	4	3.8	5	3.4	7.5	1.7	14	3.2	24.5	3.8	13	3.4	4	2.9	12	2.8	12	7.5	29	·	·	·	·	·	·	·	9	6	3	·	8	·	·
XI	2.5	5.4	9.5	4.8	17.5	3.5	12.5	4.3	16	3.6	23.5	5.4	1	1.0	3.5	4.4	4	4.2	52	12.1	21	1	8	16	·	4	·	·	17	19	13	1	4	10	·
XII	2.5	4.2	0.5	3.0	4.5	2.4	19	4.4	20	4.8	31	5.7	8.5	5.3	7	3.6	·	4.8	79	13.0	18	·	1	17	·	3	·	·	26	21	14	3	3	17	·
Rok	72	3.8	146.5	4.7	81.5	3.6	115	3.5	150	3.6	230	4.1	169.5	4.1	60.5	4.1	70	3.9	610	24.4	3. IX	4	21	100	7	20	·	18	161	190	127	16	32	79	16

Uwaga. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru indukcyjnego Fuess.

Kmiecin — $H_s = 0\,m$ — $h_w = 8\,m$

I	1	9.0	5	4.1	5.5	3.7	19	3.1	23.5	4.4	16.5	3.8	4.5	2.7	12	5.2	6	3.8	29	6.9	8	4	7	29	·	4	·	·	18	16	9	·	2	15	–
II	4.5	9.1	18	5.9	2.5	1.4	2	4.0	7.5	6.1	11.5	5.7	18.5	3.7	16.5	7.0	3	5.4	22	3.6	7, 23	7	18	26	·	10	·	·	14	13	10	·	3	28	–
III	7	5.8	13	4.9	3.5	3.9	10.5	4.0	18	3.8	17	3.1	11.5	3.2	5.5	5.6	7	3.8	20	7.2	3	6	9	23	·	4	·	5	12	12	7	·	4	19	–
IV	9.5	5.2	11	4.9	12.5	5.8	25	5.0	12.5	5.0	3	3.5	5.5	3.1	7	4.2	4	4.7	39	7.6	21	·	·	9	·	4	·	·	14	13	9	·	2	·	–
V	23	5.8	18	3.9	6.5	5.0	8.5	5.6	3.5	3.4	6.5	3.8	12	4.3	7	4.3	8	4.3	31	11.5	10	·	·	4	·	4	·	2	9	11	6	1	3	·	–
VI	11.5	3.7	15.5	4.2	6	4.0	6	4.8	7.5	5.1	9.5	3.7	20.5	4.0	8.5	3.8	5	3.9	65	18.8	1	·	·	·	3	2	·	7	7	13	11	1	·	·	–
VII	5	4.1	10	3.8	4.5	3.0	5	4.0	7.5	2.9	32.5	3.5	22	4.6	4.5	5.3	2	3.8	103	24.3	15	·	·	·	2	·	·	2	5	20	16	3	·	·	–
VIII	14.5	3.4	6.5	1.5	1.5	4.0	6.5	3.4	7	4.7	12.5	2.6	15.5	3.2	13	3.6	16	2.7	83	21.2	27	·	·	·	5	·	·	·	11	16	12	2	4	·	–
IX	1.5	4.0	6	2.9	4	5.5	20	4.0	17	4.1	22.5	4.2	10.5	2.8	6.5	4.3	2	3.8	123	56.0	4	·	·	·	1	·	·	5	5	11	8	3	·	·	–
X	8	3.4	5	2.6	1.5	4.3	4	3.4	11.5	3.9	21	4.0	18.5	3.5	15.5	4.6	8	3.5	22	6.4	16	·	·	3	·	1	·	2	11	8	8	·	9	·	–
XI	2	3.5	12.5	4.1	8	3.2	12.5	5.1	16.5	4.9	18.5	4.1	8.5	3.1	3.5	2.9	8	3.8	30	10.4	1	6	13	19	·	3	1	·	10	13	6	1	2	16	–
XII	0.5	1.0	0.5	1.0	1.5	4.3	14	5.6	21.5	5.9	31	4.9	11	3.7	4	3.5	9	4.5	31	11.0	18	4	5	23	·	3	·	·	16	11	6	1	2	8	–
Rok	88	4.8	121	3.6	57.5	4.0	133	4.3	153.5	4.5	202	3.9	158.5	3.5	103.5	4.5	78	4.0	598	56.0	4. IX	27	52	136	11	35	1	23	132	157	108	12	31	86	–

Żelisławki — $H_s = 68\,m$ — $h_w = 12\,m$

I	1	1.0	2	3.5	2	2.0	6	2.5	16.5	5.1	25.5	4.7	10.5	5.2	10.5	7.0	19	3.9	31	6.9	21	3	10	27	·	3	·	2	15	14	9	·	2	19	–
II	4.5	6.0	10	3.4	4	4.4	1	1.0	3.5	1.0	15.5	6.1	14	7.8	24.5	8.3	7	5.8	40	12.7	8	8	17	27	·	13	2	2	12	18	11	1	·	28	–
III	9	2.6	6.5	3.2	6	2.3	1.5	2.7	13	4.2	27	4.2	14.5	6.9	4.5	7.1	11	3.9	37	15.0	3	5	9	24	·	4	1	8	10	10	6	1	3	20	–
IV	6.5	3.5	7	2.3	16	3.8	16	3.0	10	3.0	5	5.6	9.5	3.6	5	6.1	15	3.0	44	9.8	23	·	·	9	·	1	·	4	16	13	7	·	3	·	–
V	21.5	3.4	11.5	2.5	12	3.0	7.5	2.9	2.5	3.0	7	2.4	16	5.2	3	3.2	12	3.0	29	9.6	9	·	·	3	·	1	·	9	9	9	6	·	2	·	–
VI	7.5	2.3	10.5	2.2	9.5	2.4	2	4.8	5	2.7	9	5.4	22.5	5.7	9	5.4	15	3.5	56	20.5	22	·	·	·	3	4	·	10	7	7	7	2	·	·	–
VII	7	2.4	5	3.1	3.5	1.9	3.5	2.1	4	2.6	33.5	4.6	24.5	5.8	3	5.2	9	4.0	129	43.9	15	·	·	·	2	4	·	4	9	17	14	5	·	·	–
VIII	3.5	3.1	0.5	2.0	0.5	2.0	1	1.0	7	2.0	16	3.1	23	3.8	20.5	2.8	21	2.4	70	13.9	25	·	·	·	5	·	·	6	10	13	11	2	2	·	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	81	31.8	4	·	·	·	1	–	–	11	8	14	9	2	1	·	–
X	9.5	3.8	5	1.1	1.5	2.3	·	·	4.5	2.2	14	4.0	28	4.1	14.5	5.6	16	3.3	11	4.3	16	·	·	·	·	2	·	3	7	7	4	·	6	·	–
XI	1.5	3.7	6.5	2.3	12	2.5	2.5	2.2	18	3.6	14.5	6.1	16	5.2	4	4.6	15	3.5	44	22.2	21	7	13	21	·	2	·	1	15	14	7	1	2	15	–
XII	0.5	4.0	·	·	·	·	2.5	3.2	28	4.1	31.5	4.2	17.5	5.3	4	6.6	9	4.0	28	7.2	14	2	6	24	·	5	·	2	17	12	11	·	·	14	–
Rok	–	–	–	–	–	–	–	–	–	–	–	·	–	–	–	–	–	–	600	43.9	15. VII	25	55	135	11	–	–	62	135	148	102	14	21	96	–

Elbląg — φ = 54°10' — λ = 19°26' — 1965

MIESIĄC	CIŚNIENIE p: P_m	Max	Min	$P_{o.m}$	TEMPERATURA T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	1005.7	1022.4	982.5	1011.2	1.3	-3.2	4.8	18	-14.4	11	-1.1	0.1	-1.1	-0.8	5.1	5.4	5.0	5.2	88	85	86	86	0.7	0.9	0.8	0.8	8.4	8.5	7.5	8.1
II	1009.3	1030.4	978.7	1014.9	-1.0	-8.0	2.5	12	-18.9	6	-5.5	-2.6	-4.3	-4.2	3.6	4.1	3.9	3.9	85	78	84	82	0.6	1.1	0.7	0.8	8.6	7.6	8.6	8.3
III	1010.7	1026.7	983.3	1016.2	3.6	-3.9	12.0	29	-20.0	7	-2.4	2.0	0.1	0.0	4.7	5.1	5.2	5.0	86	70	81	79	0.8	2.3	1.2	1.4	6.7	6.3	5.5	6.2
IV	1006.7	1026.4	989.0	1012.1	9.8	2.8	17.2	28	-3.6	6	4.2	8.2	5.7	6.0	6.8	7.1	7.1	7.0	80	66	76	74	1.7	4.0	2.3	2.7	8.4	8.0	7.0	7.8
V	1009.1	1024.6	984.9	1014.4	13.4	5.0	19.5	18	-0.7	3	8.2	11.8	8.3	9.2	8.3	7.9	8.2	8.1	75	56	74	68	2.7	6.3	2.9	4.0	6.6	7.0	6.7	6.8
VI	1008.6	1017.0	996.6	1013.8	20.4	11.0	28.7	26	4.8	4	14.4	19.0	14.6	15.6	12.6	11.9	12.8	12.4	77	56	76	70	4.0	10.7	4.2	6.3	6.4	6.3	5.5	6.1
VII	1005.0	1017.7	988.8	1010.2	20.0	12.0	29.2	14	6.4	6	14.3	18.4	14.7	15.5	13.8	13.3	13.8	13.6	83	63	82	76	2.8	8.4	3.2	4.8	6.8	7.9	7.3	7.3
VIII	1009.4	1017.2	999.5	1014.6	19.9	10.9	27.9	23	5.8	31	13.5	18.7	14.3	15.2	14.2	15.2	14.4	14.6	91	70	88	83	1.6	7.1	2.3	3.7	7.7	7.7	6.6	7.3
IX	1008.4	1026.7	997.8	1013.6	19.6	10.7	27.3	3	4.0	16	12.3	18.1	14.0	14.6	12.8	13.9	13.4	13.4	88	68	84	80	1.8	7.3	2.8	4.0	6.7	6.3	5.6	6.2
X	1016.6	1032.3	999.1	1022.0	11.9	5.0	19.5	1	-0.6	21	6.4	11.0	7.9	8.3	9.1	10.2	9.7	9.7	93	77	90	87	0.7	3.2	1.1	1.7	8.3	8.1	6.5	7.6
XI	1005.8	1024.2	976.4	1011.3	1.3	-3.6	11.1	2	-13.7	24	-1.9	0.0	-1.3	-1.1	5.1	5.4	5.4	5.3	87	82	87	85	0.7	1.2	0.7	0.9	8.4	8.4	7.2	8.0
XII	997.6	1017.6	971.3	1003.0	1.9	-2.2	9.5	19	-13.6	17	-0.5	0.6	-0.1	0.0	5.5	5.7	5.5	5.6	90	87	88	88	0.6	0.9	0.8	0.8	8.9	8.7	9.1	8.9
Rok	1007.7	1032.3	971.3	1013.1	10.2	3.0	29.2	14.VII	-20.0	7. III	5.2	8.8	6.1	6.6	8.5	8.8	8.7	8.7	85	72	83	80	1.6	4.4	1.9	2.6	7.7	7.6	6.9	7.4

Kościerzyna — φ = 54°08' — λ = 17°58'

I	–	–	–	–	0.7	-3.6	5.0	1	-13.6	11	-1.7	-0.3	-1.4	-1.2	5.1	5.4	5.1	5.2	93	88	92	91	0.4	0.7	0.5	0.5	8.9	8.2	7.0	8.0
II	–	–	–	–	-1.0	-8.3	3.2	11	-16.9	6	-4.9	-1.9	-4.8	-4.1	4.0	4.4	4.0	4.1	91	81	89	87	0.4	1.0	0.4	0.6	8.3	8.0	6.4	7.6
III	–	–	–	–	3.5	-5.1	10.9	29	-23.5	8	-3.5	2.1	-0.7	-0.7	4.7	5.4	5.2	5.1	91	75	85	84	0.4	2.0	0.9	1.1	7.9	6.5	5.3	6.6
IV	–	–	–	–	9.0	1.9	14.6	30	-3.3	5	3.4	7.7	4.8	5.2	6.9	7.0	7.1	7.0	88	68	82	79	1.0	3.8	1.6	2.1	8.3	8.4	6.0	7.6
V	–	–	–	–	12.9	4.0	18.1	17	-2.9	3	7.5	11.4	7.3	8.4	8.2	7.6	8.1	8.0	78	57	78	71	2.3	6.2	2.3	3.6	6.5	7.2	5.4	6.4
VI	–	–	–	–	19.7	9.7	29.1	26	4.1	4	13.9	18.4	13.8	15.0	12.1	11.7	12.3	12.0	76	56	77	70	3.9	10.2	3.7	5.9	6.1	6.5	5.6	6.1
VII	–	–	–	–	18.3	10.6	28.2	14	5.4	5	13.3	17.1	13.3	14.2	13.2	12.9	13.6	13.2	86	67	88	80	2.2	7.1	1.9	3.7	7.4	8.5	6.9	7.6
VIII	–	–	–	–	19.3	9.6	27.1	22, 23	5.5	17	12.7	17.9	13.2	14.2	13.4	13.1	13.3	13.3	90	65	88	81	1.5	8.1	2.2	3.9	6.6	8.0	4.0	6.2
IX	–	–	–	–	18.5	9.2	26.4	3	3.1	16	11.0	17.3	12.5	13.3	12.3	13.3	13.0	12.9	93	68	89	83	1.0	6.9	1.8	3.2	7.7	6.5	4.4	6.2
X	–	–	–	–	12.0	4.1	18.5	1	-1.3	22	5.7	11.4	6.9	7.7	9.0	10.1	9.3	9.5	96	75	92	88	0.4	3.6	0.8	1.6	8.8	7.6	6.2	7.5
XI	–	–	–	–	1.1	-4.1	10.4	1	-15.7	24	-2.2	-0.1	-1.5	-1.3	5.0	5.5	5.4	5.3	89	84	89	87	0.6	1.0	0.6	0.7	8.9	8.3	5.8	7.7
XII	–	–	–	–	1.6	-2.9	10.0	19	-17.0	17	-1.0	0.1	-0.3	-0.4	5.4	5.5	5.5	5.5	91	87	89	89	0.5	0.8	0.7	0.7	9.6	9.6	8.7	9.3
Rok	–	–	–	–	9.6	2.1	29.1	26.VI	-23.5	8. III	4.5	8.4	5.3	5.9	8.3	8.5	8.5	8.4	88	73	86	82	1.2	4.3	1.4	2.3	7.9	7.8	6.0	7.2

Lidzbark Warmiński — φ = 54°08' — λ = 20°36'

I	–	–	–	–	0.5	-3.8	4.4	1	-14.2	11	-2.0	-0.7	-1.8	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	6.5	7.8
II	–	–	–	–	-2.5	-10.1	2.0	13	-26.4	6	-7.2	-4.0	-6.4	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.6	7.6	7.5
III	–	–	–	–	2.8	-5.1	9.3	28	-24.3	8	-3.3	1.5	-1.2	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.3	6.0	6.4
IV	–	–	–	–	9.5	1.7	16.8	28	-3.8	6	3.1	8.1	4.8	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.2	6.9	7.6
V	–	–	–	–	13.6	3.5	18.7	18	-3.2	3	7.3	12.2	7.5	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.3	5.4	6.0
VI	–	–	–	–	20.0	9.9	28.3	26	3.8	8	13.9	18.6	14.0	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	4.9	5.4
VII	–	–	–	–	19.7	11.0	28.6	14, 15	6.3	5, 6	14.0	18.1	14.1	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.7	6.5	6.7
VIII	–	–	–	–	20.2	10.2	27.7	22	4.6	17	12.7	18.7	14.0	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	6.3	7.2
IX	–	–	–	–	19.5	9.5	27.2	3	4.4	1	11.4	18.2	13.2	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.9	3.9	5.7
X	–	–	–	–	11.5	4.4	18.4	1	-2.5	21	5.7	10.8	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.9	6.0	7.2
XI	–	–	–	–	0.1	-4.7	10.4	2	-17.8	16	-2.8	-0.9	-2.1	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.8	7.8	8.4
XII	–	–	–	–	1.4	-2.7	9.3	20	-15.5	17	-0.7	0.1	-0.4	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.6	9.2	8.7	9.2
Rok	–	–	–	–	9.7	2.0	28.6	14,15.VII	-26.4	6. II	4.3	8.4	5.2	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.4	7.1

Orneta — φ = 54°07' — λ = 20°07'

I	–	–	–	–	0.8	-3.6	4.7	18	-15.6	11	-1.8	0.0	-1.6	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-2.2	-9.9	2.0	13	-25.1	6	-6.8	-3.1	-5.9	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.4	-4.9	10.7	29	-22.9	8	-2.8	2.6	-0.7	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.4	7.8	7.3
IV	–	–	–	–	9.3	2.1	16.3	28	-3.1	6	3.5	8.7	5.2	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.4	8.2	8.0
V	–	–	–	–	13.8	3.7	19.8	18	-3.4	4	7.3	13.0	7.8	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.8	6.9	6.4
VI	–	–	–	–	20.3	9.7	29.0	22	1.0	5	13.5	19.7	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	3.9	6.4	5.1
VII	–	–	–	–	20.0	11.1	29.7	15	5.4	5	14.1	18.9	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.9	6.9	5.8
VIII	–	–	–	–	20.0	9.7	28.2	22	3.5	17	12.6	18.6	14.0	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.1	9.6	(28.0)	3	4.4	1	11.5	18.8	13.4	14.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.5	6.4	5.5
X	–	–	–	–	11.9	4.0	18.9	1	-3.0	21	6.1	11.4	7.2	8.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.3	7.5	7.8
XI	–	–	–	–	0.7	-4.6	11.0	2	-19.6	24	-2.7	-0.2	-1.7	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.6	9.2	9.0	9.3
XII	–	–	–	–	1.7	-2.0	10.6	19, 20	-13.1	16	-0.4	0.4	-0.2	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.4	9.3	9.4
Rok	–	–	–	–	10.0	2.1	29.7	15.VII	-25.1	6. II	4.5	9.1	5.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Elbląg

$H_s = 38\,m$ $H_b = 42{,}8\,m$ $h_w =$ 20 m wiatromierz Wilda; 13,5 m anemometr Chauvin Arnaux; 20 m anemometr M-47

1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊟	K (K)
I	2.5	5.0	4.5	3.9	9.5	4.8	23.5	3.9	22	4.3	13.5	4.1	4	3.1	8.5	6.3	5	4.1	38	10.9	8	3	7	27	·	4	·	·	17	20	9	1	3	23	·
II	12.5	8.2	6.5	4.1	3.5	3.1	6	2.0	9	4.9	11	4.9	13.5	4.4	10	5.4	10	4.4	39	6.7	2	7	16	26	·	9	·	2	20	20	13	·	·	28	·
III	13.5	6.5	1	3.0	10.5	5.8	20.5	3.5	16.5	4.4	6.5	3.4	5.5	4.2	4	4.0	15	3.8	25	6.3	3	3	9	22	·	4	·	5	12	16	6	·	4	18	·
IV	7.5	6.6	4	6.0	15.5	8.0	14	6.8	21	6.2	4	4.5	4.5	2.1	6.5	3.8	13	5.3	50	9.7	21	·	·	7	·	10	·	·	18	14	10	·	3	·	·
V	26	6.4	12	6.4	10	6.4	10.5	6.2	9.5	4.1	8	3.8	7.5	3.7	4.5	4.6	5	5.3	37	13.8	9	·	·	1	·	7	·	2	15	12	7	1	5	·	·
VI	9	4.2	6.5	6.1	13.5	6.1	9	5.4	12.5	5.8	6.5	4.3	13.5	3.6	12.5	4.0	7	4.5	102	24.2	1	·	·	·	3	6	·	3	8	13	11	4	3	·	4
VII	4	2.0	9.5	5.6	4.5	3.2	4	5.4	16	3.6	27.5	4.4	19	5.0	5.5	3.0	3	4.2	100	23.6	23	·	·	·	3	2	·	1	13	18	18	2	1	·	7
VIII	22	3.6	3.5	2.4	4.5	3.3	6	5.8	20	3.5	4.5	3.3	7.5	3.8	16	3.7	9	3.3	95	26.0	27	·	·	·	5	·	·	1	16	14	11	3	4	·	3
IX	3	2.7	1	5.0	7	7.2	18.5	5.1	22.5	3.9	18.5	4.5	10	4.2	4.5	3.7	5	4.3	159	71.4	4	·	·	·	1	3	·	4	9	12	9	5	·	·	2
X	9	5.1	5.5	3.8	3.5	3.6	6	3.5	13.5	3.0	14	4.5	12	3.5	9.5	3.6	20	3.0	31	6.7	16	·	·	1	·	2	·	2	16	10	7	·	14	·	·
XI	4	4.8	10	5.6	14.5	4.7	10	6.2	15.5	5.4	16.5	5.5	9	5.3	2.5	2.8	8	4.8	36	13.4	1	7	12	19	·	11	·	·	16	20	9	1	3	16	·
XII	0.5	3.0	·	·	·	·	8	3.9	26.5	4.8	31	4.1	14	2.6	5	3.1	8	3.6	57	21.4	18	4	6	23	·	5	·	·	24	20	10	1	6	14	·
Rok	113.5	4.8	66	4.3	96.5	4.7	136	4.8	204.5	4.5	161.5	4.3	120	3.8	89	4.0	108	4.2	769	71.4	4. IX	24	50	126	12	63	·	20	184	189	120	18	46	99	16

Uwaga. Kierunki i prędkości wiatru: I – wg wiatromierza Wilda, II–XI – wg anemometru Chauvin Arnaux, XII – wg anemometru M-47.

Kościerzyna

$H_s = 180\,m$ $h_w = 13\,m$

I	2	1.0	10	2.8	12.5	1.8	7.5	2.1	23	4.8	16.5	3.5	6	3.8	10.5	3.5	5	3.2	26	5.5	9	1	12	28	·	2	·	·	18	15	9	·	6	14	·
II	12	5.6	11	4.6	·	·	3	1.7	3.5	2.9	15	4.2	17.5	3.0	17	3.5	5	3.7	50	7.9	27	9	18	27	·	2	1	·	14	21	17	·	1	28	·
III	9	3.6	14	4.9	2.5	4.0	6.5	2.5	22	2.4	9	2.3	13.5	3.6	11.5	2.5	5	3.0	24	8.6	3	5	9	25	·	3	·	5	13	13	6	·	9	21	·
IV	5.5	3.4	21	6.6	13.5	4.2	17	3.1	14.5	2.9	1.5	1.0	9	3.3	6	2.6	2	4.0	27	7.6	23	·	·	7	·	2	·	2	13	13	10	·	2	·	1
V	11	3.2	30	4.6	11.5	5.0	5.5	3.7	5	3.0	3.5	3.3	14.5	3.5	8	2.6	4	3.7	44	13.1	7	·	·	5	·	3	·	4	12	13	9	2	·	·	1
VI	5	2.2	19	5.4	8.5	3.5	2.5	3.4	11.5	4.7	9.5	3.4	21.5	3.7	10.5	2.6	2	3.8	55	25.7	22	·	·	·	4	2	1	4	9	11	9	1	·	·	5
VII	3	3.3	11	4.5	5.5	1.7	4.5	2.3	14	3.9	32.5	3.8	16	3.3	3.5	1.9	3	3.4	109	20.8	15	·	·	·	2	2	·	2	15	22	21	3	1	·	8
VIII	12.5	1.6	9	1.3	4	2.0	5.5	3.0	9.5	3.3	12.5	1.6	13.5	1.9	10.5	1.9	16	1.7	76	22.4	6	·	·	·	4	·	·	2	6	12	9	2	1	·	6
IX	0.5	1.0	6	5.3	10.5	3.4	3	3.2	24	3.8	22.5	2.6	7.5	1.8	4	2.5	12	2.8	60	11.6	6	·	·	·	1	1	·	3	10	14	10	2	2	·	2
X	7.5	1.7	11	1.7	4.5	1.9	1	1.0	9	2.1	24	2.8	16.5	2.1	11.5	2.1	8	2.0	17	6.1	29	·	·	4	·	·	·	1	16	8	4	·	7	·	·
XI	3	1.8	6.5	5.5	18	3.5	7	4.0	10.5	2.8	18.5	6.1	12.5	2.4	6	2.0	8	3.5	35	8.1	1	6	12	22	·	4	·	1	13	20	11	·	2	13	·
XII	0.5	3.0	1	1.0	1	1.0	8	4.8	20	4.8	40	5.2	11.5	2.3	4	1.2	7	4.0	44	8.5	18	4	8	23	·	3	1	·	25	23	13	·	3	20	·
Rok	71.5	2.6	149.5	4.0	92	2.7	71	2.9	166.5	3.4	205	3.3	159.5	2.9	103	2.4	77	3.2	567	25.7	22.VI	25	59	141	11	24	3	24	164	185	128	10	34	96	23

Lidzbark Warmiński

$H_s = 90\,m$ $h_w = 13\,m$

I	2.5	2.2	4.5	4.2	11	3.2	9.5	3.6	19.5	5.1	19.5	4.3	5.5	4.0	7	6.3	14	3.7	24	7.3	8	3	9	27	·	2	·	·	14	13	4	·	2	19	·
II	10	4.2	8	4.2	1.5	4.3	1.5	3.0	4	4.9	14.5	5.2	19.5	4.2	7	3.9	18	3.5	25	3.6	13	12	18	27	·	2	·	1	13	19	9	·	·	28	·
III	7.5	3.5	10	2.6	1	5.0	14	4.0	13.5	3.9	18	3.0	15	3.3	5	2.9	9	3.1	27	12.0	3	5	9	24	·	1	·	3	13	11	7	1	5	19	·
IV	8.5	4.2	8	3.9	16.5	5.7	14	5.4	13	5.0	8.5	3.1	7.5	3.0	5	2.7	9	4.1	43	13.6	21	·	·	10	·	2	·	2	16	11	8	1	3	·	2
V	14	3.7	13	3.0	12	4.8	5.5	4.5	2	3.8	10	4.0	7.5	4.3	10	3.2	19	3.1	47	10.0	16	·	·	3	·	2	·	4	9	11	7	1	1	·	1
VI	6.5	3.4	13.5	3.4	5.5	1.6	2	5.8	10	3.7	7	4.3	25	4.1	9.5	3.8	11	3.3	71	19.4	22	·	·	·	3	4	1	2	8	13	9	2	1	·	4
VII	3	1.2	5.5	2.6	4	2.8	3	2.7	5	2.9	24	4.7	24	4.4	5.5	2.9	19	3.1	105	16.5	8	·	·	·	2	1	·	·	11	15	16	4	2	·	7
VIII	6	2.1	2	1.5	3	3.8	10	4.8	9.5	4.6	3.5	2.7	17	2.9	21	2.7	21	2.5	119	50.5	25	·	·	·	7	1	·	1	15	12	9	3	1	·	4
IX	2.5	3.0	4	2.8	1.5	3.0	8.5	3.2	19.5	3.6	22	3.4	15.5	4.0	5.5	3.3	11	3.1	63	23.5	29	·	·	·	1	·	·	3	7	10	9	2	1	·	1
X	6	3.0	3	2.5	1	2.5	0.5	4.0	2.5	3.0	22.5	4.2	28	3.2	11.5	3.3	18	2.8	24	8.7	16	·	·	4	·	·	·	2	14	10	6	·	7	·	·
XI	5.5	2.8	16.5	3.7	4.5	3.4	9.5	5.5	9.5	5.7	18	5.7	14.5	4.0	3	2.8	9	4.1	39	11.5	1	8	15	20	·	2	·	1	19	18	9	1	2	17	·
XII	·	·	1	3.0	·	·	9.5	5.8	17	5.7	38.5	5.0	23	3.6	2	2.8	2	4.7	33	11.0	18	3	8	27	·	4	·	·	23	14	9	1	·	17	·
Rok	72	2.8	89	3.1	61.5	3.3	87.5	4.4	125	4.3	206	4.1	202	3.8	92	3.4	160	3.4	620	50.5	25.VIII	31	59	142	13	21	1	19	162	161	102	16	25	100	19

Orneta

$H_s = 70\,m$ $h_w = 14\,m$

I	1.5	1.7	8	1.5	20	1.8	14	2.1	26	2.3	10	4.9	6	2.5	7.5	4.6	·	2.6	32	7.8	27	2	8	28	·	1	1	—	—	17	7	·	—	14	—
II	16	2.8	11.5	2.0	1	2.0	2	1.0	8.5	4.9	7.5	3.7	26	3.0	11.5	4.1	·	3.2	29	4.8	10	13	19	27	·	3	2	—	—	20	9	·	—	28	—
III	5	2.0	9	2.2	11	1.5	10.5	2.0	25.5	1.5	11	1.4	14	3.6	7	2.0	·	2.0	30	10.2	3	5	10	24	·	1	·	—	—	11	7	1	—	19	—
IV	10	2.8	11	1.4	26	2.9	18.5	2.8	9	2.1	3.5	3.0	8	2.5	4	1.5	·	2.5	34	16.2	21	·	·	9	·	·	·	—	—	12	7	1	—	·	—
V	11.5	3.4	11	1.4	20	2.2	3	2.3	7.5	1.4	5.5	3.5	7	2.0	23.5	2.9	4	2.4	35	8.1	9	·	·	3	·	1	·	—	—	12	6	·	—	·	—
VI	3	1.3	17	2.1	11.5	2.5	3	1.7	8	2.0	11	3.4	23	2.7	13.5	2.0	·	2.4	47	11.2	1	·	·	·	3	1	·	—	—	11	8	1	—	·	—
VII	3	2.0	8.5	1.2	9.5	1.5	6	1.8	22.5	2.9	18.5	2.6	17	2.6	8	1.1	·	2.2	81	10.8	23	·	·	·	2	·	·	—	—	17	15	3	—	·	—
VIII	9.5	1.3	·	·	3	1.0	13	2.7	5	1.4	15	1.9	25	1.8	22.5	1.4	·	1.8	102	40.6	27	·	·	·	6	·	·	—	—	14	8	4	—	·	—
IX	5	1.4	4	2.0	18	1.4	17	2.1	12	2.2	15	2.7	13	2.2	5	4.2	1	2.2	73	23.8	4	·	·	·	1	1	·	—	—	8	8	3	—	·	—
X	6	1.0	9	1.9	6	1.5	·	·	23	2.5	9	3.1	23	2.7	17	1.5	·	2.2	19	5.5	16	·	·	4	·	·	·	—	—	7	5	·	—	·	—
XI	7	1.6	6	2.0	12	1.8	15	3.5	12	3.6	22	4.0	13	2.3	2	1.0	1	2.9	39	10.2	1	8	15	20	·	2	·	—	—	17	9	1	—	15	—
XII	·	·	·	·	3	1.3	14	2.6	28.5	3.6	33.5	3.9	14	2.7	·	·	·	3.3	40	14.2	18	4	6	19	·	3	·	—	—	14	10	1	—	—	—
Rok	77.5	1.8	95	1.5	141	1.8	116	2.0	187.5	2.5	161.5	3.2	189	2.6	121.5	2.2	6	2.5	561	40.6	27.VIII	32	58	134	12	13	3	—	—	160	99	15	—	—	—

Kętrzyn I — φ = 54°06' — λ = 21°21' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	-4.3	4.4	1	-13.0	11	-2.3	-1.0	-2.1	-1.9	4.7	4.8	4.6	4.7	87	82	86	85	0.6	1.0	0.7	0.8	8.5	7.4	6.5	7.5
II	–	–	–	–	-2.3	-10.2	2.0	13, 14	-26.1	6	-7.0	-4.4	-6.2	-6.0	3.3	3.7	3.5	3.5	84	79	85	83	0.6	0.9	0.5	0.7	7.1	6.7	6.8	6.9
III	–	–	–	–	3.2	-4.7	10.0	28	-18.1	7, 8, 9	-3.1	1.7	-0.9	-0.8	4.6	5.2	4.9	4.9	87	73	81	80	0.6	2.0	1.1	1.2	6.1	5.5	5.3	5.6
IV	–	–	–	–	10.2	1.7	17.1	28	-4.1	3	3.4	8.2	5.2	5.5	6.6	6.8	6.9	6.8	84	62	77	74	1.3	4.4	2.1	2.6	7.5	7.6	7.4	7.5
V	–	–	–	–	13.8	4.0	19.5	18	-3.7	4	7.4	12.0	8.2	9.0	8.7	8.3	8.5	8.5	83	59	77	73	1.7	5.9	2.6	3.4	6.3	6.9	5.4	6.2
VI	–	–	–	–	20.4	10.2	28.3	26	3.6	8	14.1	18.4	14.8	15.5	13.2	13.0	13.1	13.1	82	63	78	74	3.2	8.6	4.0	5.3	5.3	6.0	6.1	5.5
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kętrzyn II — φ = 54°05' — λ = 21°22'

I	998.9	1015.9	978.1	1011.2	0.3	-4.1	4.4	1	-12.6	11	-2.3	-1.0	-2.1	-1.9	4.7	4.8	4.6	4.7	87	82	86	85	0.6	1.0	0.7	0.8	8.7	7.4	6.5	7.5
II	1001.5	1023.7	975.5	1014.0	-2.4	-10.2	2.0	13	-26.5	6	-7.1	-4.5	-6.1	-6.0	3.3	3.6	3.6	3.5	85	78	85	83	0.6	0.9	0.5	0.7	7.0	6.8	7.0	6.9
III	1004.1	1020.7	977.6	1016.4	3.2	-4.7	9.9	28	-18.3	7	-3.1	1.6	-0.9	-0.8	4.6	5.2	4.8	4.9	88	73	81	81	0.6	2.0	1.2	1.3	6.1	5.4	5.4	5.6
IV	1000.5	1017.0	982.1	1012.5	10.0	1.7	16.9	28	-3.9	3	3.3	8.2	5.2	5.5	6.7	6.9	6.9	6.8	84	59	76	73	1.3	4.3	2.2	2.5	7.6	7.9	7.0	7.5
V	1002.3	1018.3	980.6	1014.2	13.5	3.9	19.2	18	-4.6	4	7.3	11.9	8.3	9.0	8.6	7.9	8.4	8.3	82	59	75	72	1.8	6.0	2.8	3.5	6.4	7.2	5.2	6.3
VI	1002.0	1009.2	993.0	1013.6	20.3	10.3	28.4	26	3.3	8	14.1	18.3	14.8	15.5	13.3	12.9	13.2	13.1	82	63	78	74	3.1	8.6	4.0	5.2	5.4	5.9	5.0	5.4
VII	998.8	1011.6	983.3	1010.4	20.1	10.7	29.7	15	6.5	6	14.3	18.4	14.3	15.3	14.1	14.1	14.1	14.1	86	67	86	80	2.4	7.6	2.5	4.2	5.8	7.3	5.8	6.3
VIII	1002.9	1011.2	993.5	1014.5	20.0	10.3	26.6	22	6.2	2	12.9	17.9	14.2	14.8	13.7	14.7	14.2	14.2	91	72	87	83	1.7	6.6	2.4	3.6	6.3	6.8	5.4	6.2
IX	1002.5	1019.8	991.1	1014.1	19.6	9.7	26.4	3	4.9	16	11.5	18.1	13.4	14.1	13.0	15.0	14.0	14.0	94	72	90	85	0.8	6.1	1.6	2.8	5.4	5.8	2.9	4.7
X	1009.4	1025.3	992.5	1021.4	11.6	4.6	17.6	1	-1.9	21	6.1	10.7	7.3	7.8	8.9	10.0	9.3	9.4	93	77	90	87	0.7	3.1	1.1	1.6	7.2	7.7	6.1	7.0
XI	999.6	1017.7	971.4	1011.9	0.5	-4.5	11.1	2	-17.0	17	-2.6	-0.9	-1.9	-1.8	4.9	5.2	5.2	5.1	88	83	89	87	0.7	1.1	0.6	0.9	8.3	7.9	7.2	7.8
XII	991.7	1009.6	968.7	1003.8	1.5	-2.8	9.3	20	-14.6	17	-0.6	0.2	-0.6	-0.4	5.2	5.4	5.3	5.3	88	86	88	87	0.7	0.9	0.7	0.8	8.2	8.5	7.5	8.1
Rok	1001.2	1025.3	968.7	1013.2	9.8	2.1	29.7	15.VII	-26.5	6.II	4.5	8.2	5.5	5.9	8.4	8.8	8.6	8.6	87	73	84	81	1.2	4.0	1.7	2.3	6.9	7.0	5.9	6.6

Suwałki — φ = 54°06' — λ = 22°57'

I	990.5	1007.1	970.6	1012.0	-1.0	-5.1	2.9	1	-13.8	10	-3.3	-2.4	-3.3	-3.1	4.4	4.4	4.3	4.4	87	84	87	86	0.6	0.8	0.6	0.7	8.9	8.6	7.5	8.3
II	991.8	1014.7	967.9	1013.6	-3.8	-12.0	1.0	13	-28.0	6	-9.4	-5.7	-7.5	-7.5	2.9	3.3	3.2	3.1	85	79	84	83	0.4	0.8	0.5	0.6	8.7	7.6	6.8	7.7
III	995.5	1012.4	969.7	1017.0	2.0	-6.0	8.0	28	-26.0	9	-4.6	0.8	-2.2	-2.0	4.1	4.7	4.5	4.4	85	71	82	79	0.8	2.0	1.0	1.3	7.5	6.7	6.1	6.8
IV	992.7	1006.9	972.9	1013.5	9.3	1.3	16.4	27	-4.9	3	2.9	8.0	4.6	5.0	6.0	5.7	6.0	5.9	76	53	69	66	1.8	5.4	2.6	3.3	7.5	8.1	5.7	7.1
V	993.6	1010.4	973.7	1014.2	13.1	3.8	19.5	18	-3.5	4	7.1	11.8	8.0	8.7	7.9	7.5	8.1	7.8	76	54	73	68	2.4	6.6	2.9	4.0	6.8	8.2	5.2	6.7
VI	993.6	1000.1	985.3	1013.7	19.6	10.4	26.4	26	2.7	8	14.0	18.4	14.2	15.2	12.5	11.3	12.6	12.1	78	55	77	70	3.6	10.2	3.8	5.9	6.1	7.6	5.9	6.5
VII	990.7	1003.6	975.3	1010.7	20.2	10.4	28.3	15	4.6	5	14.2	18.6	14.4	15.4	13.1	12.0	13.0	12.7	80	56	79	72	3.3	9.9	3.7	5.6	6.3	8.1	6.8	7.1
VIII	994.4	1003.2	983.6	1010.4	20.0	10.0	27.6	25	5.3	2	12.8	18.5	13.3	14.5	13.0	12.2	13.2	12.8	87	59	86	77	2.0	9.9	2.4	4.8	6.6	7.3	4.9	6.3
IX	994.7	1010.6	983.4	1014.9	19.8	8.9	26.6	4	3.0	21	11.0	18.8	12.7	13.8	12.0	12.9	12.5	12.5	91	59	84	78	1.2	9.3	2.5	4.3	6.6	6.8	3.7	5.7
X	1000.3	1015.8	984.1	1021.1	10.9	3.7	17.7	1	-3.8	21	5.5	10.2	6.8	7.3	8.1	8.6	8.3	8.3	88	69	82	80	1.1	4.1	1.8	2.3	8.3	7.8	6.7	7.6
XI	990.9	1007.8	963.7	1012.3	-0.6	-5.3	10.2	2	-19.7	24	-3.4	-1.4	-3.0	-2.7	4.5	4.7	4.6	4.6	85	79	85	83	0.8	1.4	0.8	1.0	9.3	9.2	8.5	9.0
XII	983.3	999.0	962.3	1004.5	0.5	-3.9	5.6	20	-14.9	17	-1.7	-0.8	-1.4	-1.3	4.8	5.0	4.8	4.9	87	85	85	86	0.7	0.9	0.9	0.8	8.9	8.9	8.6	8.8
Rok	992.7	1015.8	962.3	1013.5	9.2	1.4	28.3	15.VII	-28.0	6.II	3.8	7.9	4.7	5.3	7.8	7.7	7.9	7.8	84	67	81	77	1.6	5.1	2.0	2.9	7.6	7.9	6.4	7.3

Sejny — φ = 54°06' — λ = 23°21'

I	–	–	–	–	-1.0	-5.4	2.7	1	-14.1	10	-3.4	-2.5	-3.5	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.4	6.5	7.2
II	–	–	–	–	-3.6	-13.2	1.1	13, 14	-32.1	6	-9.5	-5.5	-8.4	-8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	5.1	6.4
III	–	–	–	–	2.4	-6.8	8.6	28	-28.1	1, 9	-5.0	1.2	-2.7	-2.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	4.9	5.9	5.9
IV	–	–	–	–	9.2	1.2	16.2	27	-5.6	3	2.9	7.8	4.8	5.1	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.9	5.5	5.9
V	–	–	–	–	13.2	3.4	18.7	18	-5.1	4	7.0	11.6	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.6	5.6	5.9
VI	–	–	–	–	20.1	10.0	27.3	26	4.3	4	13.9	18.6	13.6	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.4	5.6	5.4
VII	–	–	–	–	20.6	9.5	31.2	16	4.1	5	14.2	18.8	14.3	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.3	6.7	5.9
VIII	–	–	–	–	20.3	9.0	27.8	25	2.5	31	12.6	19.0	12.9	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.2	4.8	5.1
IX	–	–	–	–	20.0	7.8	26.3	4	0.9	21	10.5	18.8	11.8	13.2	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.6	2.8	3.9
X	–	–	–	–	11.3	3.1	18.4	1	-6.1	21	5.2	10.3	6.5	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	5.8	6.4
XI	–	–	–	–	-0.4	-5.7	11.0	2	-19.1	24	-3.4	-1.2	-3.1	-2.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.2	7.0	7.4
XII	–	–	–	–	0.7	-3.7	6.2	20	-12.1	18	-1.5	-0.5	-1.4	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	6.9	7.4
Rok	–	–	–	–	9.4	0.8	31.2	16.VII	-32.1	6.II	3.6	8.0	4.4	5.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.1	5.7	6.1

Kętrzyn I

$H_s = 110\,m$ $h_w = 11\,m$ 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	2.5	2	3.0	9	3.2	19	3.1	25	3.8	11	4.9	4	3.8	9	4.2	12	3.2	25	5.8	8	3	11	28	·	3	·	2	16	11	7	·	5	17	·
II	7	3.6	8	3.6	2	3.5	·	·	9	3.4	18	5.1	17	5.5	9	3.9	14	3.7	13	2.2	13	12	20	27	·	1	·	3	12	12	4	·	1	28	·
III	2	3.0	5	4.4	8	2.2	18	3.5	21	3.5	9	3.1	16	3.9	4	5.0	10	3.2	16	6.4	21	5	9	23	·	·	·	6	13	9	4	·	6	21	·
IV	3	5.0	6	3.7	15	4.1	22.5	4.3	8.5	4.3	4	2.8	6	4.0	9	2.4	16	3.2	17	7.0	21	·	·	9	·	·	·	2	17	7	4	·	2	·	·
V	6	2.5	4	4.0	14	4.0	8	4.0	5	3.0	5	4.1	8	4.6	14	4.4	29	2.7	59	11.0	19	·	·	3	·	·	·	3	9	14	11	2	2	·	1
VI	2	3.5	4	3.2	10	4.4	7	2.3	5	4.4	10	3.5	14.5	4.4	5.5	4.0	32	2.5	49	16.1	19	·	·	·	3	·	·	4	9	12	9	1	1	·	3
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

ROZKŁAD WIATRU (n_D, v_{mD}); OPAD R; LICZBA DNI (r)

Kętrzyn II

$H_s = 108\,m$ $H_b = 97.2\,m$ $h_w = 10.5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	3	2.7	4	2.8	9.5	3.6	21.5	4.0	23.5	4.6	13.5	5.2	5	4.2	9	5.3	4	4.2	25	6.0	8	3	11	28	·	3	·	2	16	13	7	·	5	17	·
II	9	4.0	10	3.4	2	3.5	2	1.0	9.5	3.6	19.5	5.2	15.5	5.5	9.5	4.3	7	4.1	12	2.0	13, 27	12	20	27	·	3	·	2	12	15	4	·	3	28	·
III	4	2.0	7	3.4	7	3.1	19.5	3.8	21.5	3.3	9.5	3.4	15.5	4.1	5	6.7	4	3.5	16	6.2	21	5	9	24	·	2	·	6	13	10	3	·	7	21	·
IV	3.5	4.6	5	4.4	18	4.6	23.5	4.7	9.5	3.7	4.5	3.3	5.5	3.8	11.5	3.3	9	3.8	17	6.6	21	·	·	9	·	1	·	2	17	8	4	·	4	·	·
V	9	2.5	5.5	3.3	15	4.4	7.5	3.1	7	2.7	6.5	5.1	7.5	4.6	15	4.4	20	3.0	58	10.4	24	·	·	3	·	1	·	2	9	14	11	1	2	·	1
VI	3	2.7	3.5	2.4	11	4.3	8	3.1	4	4.0	12	3.4	14	4.3	8.5	3.4	26	2.6	54	18.6	19	·	·	·	3	1	·	4	9	12	9	1	1	·	3
VII	1	2.0	8.5	2.4	7	2.1	2.5	4.4	15	2.9	26.5	4.6	12.5	4.9	3	4.3	17	3.1	133	29.4	15	·	·	·	2	3	·	1	9	20	15	6	·	·	8
VIII	6	2.8	0.5	2.0	1.5	2.0	9.5	2.8	11	3.0	7	2.8	16.5	2.9	24	2.9	17	2.3	89	20.7	27	·	·	·	8	·	·	3	10	14	9	4	·	·	2
IX	·	·	·	·	7	1.9	21	2.4	14.5	3.0	22	3.4	18	4.1	2.5	3.4	5	2.9	84	46.5	29	·	·	·	1	·	·	8	6	12	11	2	2	·	3
X	2	2.5	1	3.0	·	·	3.5	2.3	8.5	2.5	13	3.3	21.5	7.8	25.5	3.0	18	2.6	24	8.9	16	·	·	2	·	·	·	1	14	10	7	·	8	·	·
XI	2.5	3.6	9.5	3.0	12.5	2.8	11	4.3	17	4.2	11.5	5.1	17	5.8	9	2.9	·	4.2	27	9.1	1	7	15	22	·	1	·	1	19	18	9	·	4	17	·
XII	·	·	·	·	·	·	8	4.4	20	4.9	39	4.9	18.5	4.6	6.5	3.2	1	4.6	29	10.2	18	3	7	23	·	2	1	·	16	20	7	1	2	17	·
Rok	43	2.4	54.5	2.5	90.5	2.7	137.5	3.4	161	3.5	184.5	4.1	167	4.7	129	3.9	128	3.4	568	46.5	29.IX	30	62	138	14	17	1	32	150	166	96	15	38	100	17

Uwaga. Kierunki i prędkości wiatru — wg anemometru M-47.

Suwałki

$H_s = 165\,m$ $H_b = 169.6\,m$ $h_w = 13\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2.5	3.4	5	3.8	16	4.9	17	4.8	23.5	4.9	15	4.2	10	5.6	4	6.0	·	4.8	43	8.0	8	3	14	28	·	3	·	1	20	17	12	·	12	16	·
II	9.5	5.6	7	6.6	4	2.8	3	2.0	5.5	6.3	25.5	4.4	13	3.9	14.5	4.6	2	4.5	28	4.3	27	15	23	27	·	2	·	1	15	20	9	·	5	28	·
III	5.5	3.6	5	2.8	7	3.5	13.5	3.7	13.5	4.0	27	3.8	11.5	4.0	3	6.8	7	3.5	27	7.3	3	7	9	23	·	1	·	2	16	16	7	·	8	23	·
IV	2	5.2	9.5	5.1	23	6.2	36	5.6	5	4.1	3.5	3.1	3.5	4.0	5.5	5.4	2	5.3	27	14.3	23	·	·	14	·	10	·	3	15	9	5	1	·	1	1
V	9.5	3.4	10.5	2.8	16	4.2	11.5	3.1	2.5	3.6	12.5	4.0	9.5	3.6	16	3.8	5	3.4	84	25.5	19	·	·	3	·	3	·	2	10	16	12	3	1	·	1
VI	6.5	2.7	10.5	3.4	12	5.4	12.5	3.7	10	4.0	14.5	4.4	12	4.0	10	3.3	2	3.9	73	20.0	13	·	·	·	1	4	·	·	9	13	11	2	1	·	5
VII	2	3.0	8	4.6	5.5	2.7	11.5	3.1	15	3.9	34	4.9	9.5	3.9	1.5	2.0	6	3.9	95	16.7	12	·	·	·	4	3	1	·	11	19	12	4	2	·	7
VIII	1	6.0	2	1.0	2.5	3.8	17.5	3.9	4.5	3.7	26.5	3.0	13.5	3.3	19.5	2.7	6	3.0	68	25.0	27	·	·	·	5	2	·	2	8	13	7	2	5	·	4
IX	0.5	1.0	3	1.8	10	3.8	22	3.7	20	4.2	17	4.5	10	3.2	2.5	2.4	5	3.6	31	10.5	29	·	·	·	2	7	·	4	6	11	6	1	5	·	2
X	1	3.5	5	3.3	2	4.2	2.5	3.8	8	4.4	33.5	3.6	19	3.4	16	3.2	6	3.3	24	9.3	16	·	·	3	·	·	·	·	15	8	5	·	4	·	·
XI	3	3.0	15	4.5	8.5	4.4	16	5.8	8	5.8	24	4.4	10.5	3.2	3	3.3	2	4.5	46	9.2	21	7	16	21	·	7	·	·	23	18	10	·	4	18	·
XII	0.5	1.0	·	·	1.5	6.0	21	5.3	22.5	5.9	36.5	4.7	9	2.7	1	2.0	1	4.9	45	12.6	19	4	14	28	·	7	1	·	25	21	11	1	3	31	·
Rok	43.5	3.4	80.5	3.3	108	4.3	184	4.0	138	4.6	269.5	4.1	131	3.7	96.5	3.8	44	4.0	591	25.5	19.V	36	76	147	12	49	2	15	173	181	107	14	50	117	20

Uwaga. Kierunki i prędkości wiatru — wg anemometru M-47.

Sejny

$H_s = 130\,m$ $h_w = 12.7\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	1	6.0	4	6.8	9	5.7	12.5	6.7	20.5	5.3	18	4.7	4	9.0	5	8.4	19	4.7	29	6.4	30	5	13	28	·	3	·	3	16	—	6	·	4	15	·
II	6	3.5	9	7.2	4	6.9	·	·	6	5.3	17	6.2	9	5.6	14	4.4	19	4.3	22	3.8	27	16	23	27	·	3	·	2	9	—	7	·	1	28	·
III	5.5	6.2	0.5	6.0	1	3.0	9.5	5.0	14.5	4.5	16.5	4.5	9.5	4.2	5	5.5	31	3.2	23	4.8	3	9	8	25	·	1	·	3	11	—	8	·	4	22	·
IV	7	6.0	2.5	6.6	17.5	7.9	24.5	6.9	24.5	6.2	2	4.2	1.5	3.3	4.5	5.1	6	6.1	18	10.5	23	·	·	13	·	8	·	4	7	—	4	1	·	·	1
V	17	4.5	5.5	3.7	12.5	5.9	4.5	4.3	4.5	5.7	7	5.8	7	4.9	8	5.1	27	3.6	92	29.4	19	·	·	5	·	·	·	3	8	—	11	3	1	·	1
VI	7.5	4.1	5	5.4	10	5.2	4.5	5.7	8.5	4.6	8.5	4.8	17.5	4.3	6.5	5.1	22	3.6	60	22.0	13	·	·	·	2	2	·	3	6	—	7	3	2	·	4
VII	3	3.7	6.5	4.9	0.5	6.0	2	3.2	14	4.4	33	5.0	8.5	3.7	0.5	3.0	25	3.3	79	15.5	31	·	·	·	3	·	·	2	6	—	13	2	2	·	5
VIII	4	3.4	2	4.0	·	·	5	4.0	11.5	4.1	16	4.5	17	3.7	12.5	3.0	25	2.8	51	17.6	2	·	·	·	6	-	·	5	6	—	6	2	3	·	3
IX	·	·	·	·	0.5	6.0	10.5	5.8	17.5	5.0	26.5	4.4	5	4.3	1	6.0	29	3.3	23	6.1	13	·	·	·	2	4	·	8	3	—	7	·	8	·	·
X	3.5	6.0	2.5	3.8	1.5	4.3	2	5.5	6.5	5.4	22.5	4.9	5	3.8	19.5	4.7	30	3.3	21	8.2	16	·	·	4	·	·	·	·	7	—	5	·	3	·	·
XI	1	6.0	7	5.7	8.5	4.9	11.5	5.5	11	5.4	18.5	6.3	11	3.7	1.5	5.0	18	4.3	34	10.5	21	7	16	22	·	1	1	·	10	—	8	1	1	12	·
XII	·	·	0.5	3.0	4.5	6.6	6.5	6.8	18	5.9	34	5.6	11	4.3	1.5	5.0	17	4.6	37	9.8	19	4	8	29	·	3	·	1	15	—	8	·	·	25	·
Rok	55.5	4.1	45	4.8	70.5	5.2	93	5.0	157	5.2	220.5	5.1	106	4.6	79.5	5.0	268	3.9	489	29.4	19.V	41	68	153	13	25	1	34	104	—	90	12	29	102	14

Tczew — φ = 54°05' — λ = 18°48' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{c.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	1.3	−2.9	5.4	1	−13.5	11	−1.3	0.4	−0.9	−0.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−0.4	−6.3	3.3	13	−15.2	6	−4.1	−1.5	−3.3	−3.0	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.5	7.3	7.3
III	—	—	—	—	3.9	−3.8	12.5	29	−21.0	8	−2.3	2.8	0.3	0.3	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.0	5.7	5.4
IV	—	—	—	—	10.1	2.7	15.3	28	−1.4	3	4.4	9.0	5.8	6.2	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.2	6.3	7.1
V	—	—	—	—	14.2	5.4	19.5	18	−1.2	4	8.6	12.4	8.6	9.6	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.0	5.9	5.5
VI	—	—	—	—	20.8	11.1	29.8	26	6.4	5	14.8	19.5	14.6	15.9	—	—	—	—	—	—	—	—	—	—	—	—	4.6	4.9	4.4	4.6
VII	—	—	—	—	20.5	11.8	29.5	14	7.7	5	15.1	19.3	14.9	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.0	5.6	5.7
VIII	—	—	—	—	20.9	11.5	28.9	22, 23	7.8	2	14.3	19.1	15.4	16.0	—	—	—	—	—	—	—	—	—	—	—	—	4.3	6.0	4.4	4.9
IX	—	—	—	—	20.0	10.1	26.5	3	5.3	16	12.0	18.8	13.9	14.6	—	—	—	—	—	—	—	—	—	—	—	—	4.1	5.1	2.7	4.0
X	—	—	—	—	12.9	5.5	21.5	1	−0.2	21	7.3	12.1	8.4	9.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	1.6	−3.0	11.3	2	−16.6	24	−1.5	0.3	−1.0	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.1	6.0	6.2
XII	—	—	—	—	2.5	−1.5	11.6	19	−15.1	17	0.2	1.2	0.6	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.3	7.7	7.7
Rok	—	—	—	—	10.7	3.4	29.8	26.VI	−21.0	8.III	5.6	9.4	6.4	7.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Rosnowo — φ = 54°04' — λ = 16°18'

I	—	—	—	—	2.1	−2.2	6.8	17	−9.2	11	−0.7	1.2	0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.3	7.3	7.5
II	—	—	—	—	0.0	−7.3	3.1	13	−15.9	24	−4.1	−1.0	−3.7	−3.1	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.6	6.5	7.4
III	—	—	—	—	4.6	−4.4	12.9	29	−21.5	8	−2.7	3.6	−0.6	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.7	4.1	5.3
IV	—	—	—	—	10.5	2.2	16.0	22	−3.7	5	4.2	9.4	5.5	6.2	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.0	5.0	6.4
V	—	—	—	—	13.6	4.2	19.9	17	−2.5	3	7.7	12.4	8.3	9.2	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.1	4.8	5.5
VI	—	—	—	—	20.8	9.4	29.8	26	3.6	4	14.2	19.1	14.1	15.4	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.0	4.1	4.9
VII	—	—	—	—	19.1	10.3	28.1	14	5.4	2	13.9	17.5	13.6	14.6	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.0	5.8	6.5
VIII	—	—	—	—	19.8	8.9	28.1	22	4.0	14	12.9	18.5	12.6	14.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.1	9.5	26.4	3	3.0	16	11.4	18.3	12.5	13.7	—	—	—	—	—	—	—	—	—	—	—	—	4.6	4.8	4.8	4.7
X	—	—	—	—	13.1	3.4	20.6	1	−2.6	12	5.8	12.3	6.4	7.7	—	—	—	—	—	—	—	—	—	—	—	—	7.4	5.6	3.1	5.4
XI	—	—	—	—	2.7	−3.2	12.1	1	−12.9	24	−1.4	1.5	−0.6	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.5	5.4	6.9
XII	—	—	—	—	2.8	−1.6	11.2	19	−12.8	17	0.0	1.1	0.4	0.5	—	—	—	—	—	—	—	—	—	—	—	—	9.1	9.2	8.5	8.9
Rok	—	—	—	—	10.7	2.4	29.8	26.VI	−21.5	8.III	5.1	9.5	5.7	6.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Stare Pole — φ = 54°04' — λ = 19°73'

I	—	—	—	—	1.3	−3.5	4.9	1	−18.7	11	−1.4	0.4	−1.2	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	9.2	8.2	7.1	8.2
II	—	—	—	—	−1.2	−8.8	2.5	13	−20.6	6	−5.5	−2.7	−4.9	−4.5	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.9	8.5	7.8
III	—	—	—	—	3.7	−5.4	12.3	29	−26.6	8	−3.3	2.0	−0.9	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.5	6.0	5.8
IV	—	—	—	—	10.0	2.3	16.3	28	−3.5	3	4.1	8.7	5.1	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.8	6.3	7.3
V	—	—	—	—	13.7	4.2	19.7	18	−4.0	4	8.2	12.3	7.6	8.9	—	—	—	—	—	—	—	—	—	—	—	—	6.0	5.7	5.3	5.7
VI	—	—	—	—	20.5	10.1	29.2	26	3.9	4	14.4	19.4	13.9	15.4	—	—	—	—	—	—	—	—	—	—	—	—	5.4	4.8	5.0	5.1
VII	—	—	—	—	20.3	11.2	29.3	14	6.3	2, 6	14.3	18.8	14.5	15.5	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.3	6.4	6.5
VIII	—	—	—	—	20.4	10.6	28.8	23	5.4	17	13.3	19.3	14.0	15.2	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.5	5.7	6.1
IX	—	—	—	—	19.6	10.0	27.3	3	5.0	16	11.8	18.4	13.3	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.4	5.8	5.7
X	—	—	—	—	12.3	4.5	18.9	1	−1.1	21	6.1	11.6	7.7	8.3	—	—	—	—	—	—	—	—	—	—	—	—	9.1	6.6	7.7	7.8
XI	—	—	—	—	1.6	−4.0	11.2	2	−15.6	20	−1.8	0.3	−1.4	−1.1	—	—	—	—	—	—	—	—	—	—	—	—	9.7	6.2	7.5	7.8
XII	—	—	—	—	2.1	−2.3	10.1	19	−15.6	17	−0.2	0.9	0.2	0.3	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.4	8.4	8.7
Rok	—	—	—	—	10.4	2.4	29.3	14.VII	−26.6	8.III	5.0	9.1	5.7	6.4	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.6	6.6	6.9

Giżycko — φ = 54°03' — λ = 21°46'

I	—	—	—	—	−0.4	−4.4	4.0	1	−12.1	11	−2.7	−1.6	−2.6	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.6	6.5	7.6
II	—	—	—	—	−3.0	−11.1	1.5	13, 14	−27.2	6	−8.0	−4.8	−6.6	−6.5	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.7	6.6	6.9
III	—	—	—	—	2.3	−5.0	8.9	28	−18.2	8, 9	−3.6	1.3	−1.2	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.3	5.9	5.9
IV	—	—	—	—	9.4	1.8	16.4	28	−3.3	3	3.4	8.0	4.8	5.2	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.4	6.1	6.7
V	—	—	—	—	13.0	4.4	17.6	28	−2.1	4	7.4	11.8	8.1	8.8	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.6	5.1	5.6
VI	—	—	—	—	19.6	10.7	26.9	26	5.0	8	13.9	17.9	14.8	15.4	—	—	—	—	—	—	—	—	—	—	—	—	4.9	6.0	5.0	5.3
VII	—	—	—	—	19.5	11.4	28.7	15	7.5	5, 6	14.1	18.3	14.4	15.3	—	—	—	—	—	—	—	—	—	—	—	—	5.0	7.2	5.8	6.0
VIII	—	—	—	—	19.5	11.1	26.8	22	7.9	31	13.2	17.8	14.3	14.9	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.7	4.7	5.7
IX	—	—	—	—	19.2	10.2	26.2	3	6.7	16	11.9	18.1	13.7	14.4	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.0	3.4	5.1
X	—	—	—	—	11.2	5.0	16.9	1	−1.3	21	6.2	10.5	7.5	7.9	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.7	5.5	6.9
XI	—	—	—	—	0.1	−4.3	10.1	2	−14.8	19	−2.7	−0.9	−2.0	−1.9	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.2	6.9	8.0
XII	—	—	—	—	1.2	−2.7	7.8	19, 20	−15.7	17	−0.8	−0.2	−0.7	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.7	7.5	8.4
Rok	—	—	—	—	9.3	2.3	28.7	15.VII	−27.2	6, 11	4.4	8.0	5.4	5.8	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.0	5.8	6.5

Tczew — $H_s = 10\,m$ — $h_w = 16\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%, V=D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	v≥15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	3	3.5	7.5	3.9	1.5	1.3	9.5	2.5	17.5	2.1	17	3.0	8.5	2.4	14.5	3.8	14	2.4	21	4.8	21	2	9	25	·	1	·	—	—	19	8	·	5	21	·
II	4.5	6.2	14	3.8	3.5	1.3	3.5	1.0	0.5	2.0	13.5	3.1	17	2.8	21.5	4.4	6	3.2	22	4.6	8	3	14	26	·	3	1	·	12	15	7	·	·	28^2	·
III	6.5	5.0	9.5	4.6	2.5	2.8	4.5	2.3	21.5	1.5	13	1.8	14	2.1	7.5	2.6	14	2.1	28	13.3	3	5	9	24	·	2	1	8	11	10	5	1	4	18	·
IV	5	4.6	11.5	4.3	12.5	5.8	20.5	2.9	10	2.6	3.5	1.6	3	2.0	14	2.5	10	3.1	48	9.1	13	·	·	4	·	2	2	1	13	14	11	·	3	·	·
V	2.5	5.1	17	4.2	8	6.6	6	3.5	7	4.1	6.5	1.8	12.5	2.8	8	4.3	3	4.1	24	6.7	9	·	·	1	·	5	2	10	11	10	6	·	1	·	·
VI	8	4.4	7.5	3.1	7	4.4	5	2.7	6	2.9	10.5	3.4	16.5	3.3	20.5	2.5	9	2.9	51	17.1	1	·	·	·	4	·	·	7	7	11	9	1	·	·	1
VII	5	2.6	7	4.3	1	3.0	7.5	2.3	9.5	2.6	31.5	3.0	12	3.4	12.5	2.8	7	2.8	96	33.4	15	·	·	·	3	1	·	4	4	20	13	2	1	·	4
VIII	13	1.9	3	1.0	2	1.0	5	1.1	9.5	1.7	9.5	2.2	12	2.0	21	2.7	18	1.6	83	16.1	4	·	·	·	6	·	·	8	9	18	11	4	3	·	5
IX	3	2.7	1	2.0	4.5	1.4	7	3.9	16.5	1.8	25.5	3.0	5	2.5	5.5	3.2	22	2.0	96	42.0	4	·	·	·	1	·	·	11	4	12	9	2	5	·	1
X	6.5	3.5	4.5	1.3	3	2.5	3.5	2.4	7	1.7	19.5	2.1	16	2.1	15	3.1	18	1.9	16	5.2	16	·	·	1	·	·	·	—	—	11	6	·	5	·	·
XI	1	8.0	4.5	2.6	20.5	2.3	9.5	4.9	12	2.2	21.5	3.4	13.5	3.0	3.5	3.0	4	2.9	40	20.4	21	7	12	16	·	1	·	2	9	14	6	1	4	15	·
XII	·	·	·	·	·	·	7.5	4.0	12.5	3.8	43.5	3.7	18	2.5	5.5	3.4	6	3.2	24	8.8	14	3	5	19	·	3	1	1	16	15	6	·	3	13^2	·
Rok	80.5	4.0	87	2.8	66	2.7	89	2.8	129.5	2.4	215	2.7	148	2.6	149	3.2	131	2.7	549	42.0	4.IX	20	49	116	14	18	7	—	—	169	97	11	34	95^5	1'

Rosnowo — $H_s = 62\,m$ — $h_w = 12\,m$

I	1	2.0	1	2.0	5	2.0	11.5	2.7	20.5	3.4	14.5	3.7	2.5	3.2	1	1.0	36	1.9	46	8.8	8	·	4	23	·	1	·	2	18	18	13	·	2	12	·
II	8	4.9	7	2.7	·	·	1	2.0	2.5	1.6	12	4.1	18.5	4.2	8	4.0	27	2.7	38	9.1	13	7	15	26	·	·	·	1	14	20	13	·	4	28	·
III	3.5	6.3	4.5	3.8	4.5	2.7	6	2.7	6.5	1.5	5.5	2.8	7	4.1	3.5	2.9	52	1.4	34	15.7	3	5	7	25	·	·	·	8	7	16	9	1	5	20	·
IV	2	3.0	10	2.7	18	4.1	11	3.8	5	2.5	5	3.6	7	2.6	7	2.7	25	2.4	27	5.1	25	·	·	4	·	·	·	3	10	12	7	·	3	·	·
V	9	3.0	6.5	2.1	16	3.4	5	6.8	3	2.0	3.5	3.1	4.5	3.6	7.5	3.8	38	2.0	80	33.3	9	·	·	4	·	1	·	9	11	17	12	2	1	·	·
VI	2.5	2.4	6	2.1	10	3.4	6	3.2	5.5	2.5	10.5	4.0	16	4.8	6.5	2.9	27	2.5	40	9.2	22	·	·	·	4	2	·	7	6	9	8	·	·	·	2
VII	·	·	8	3.6	2.5	2.2	4.5	3.7	5.5	2.7	43.5	3.9	6.5	4.5	0.5	2.0	22	2.9	171	18.9	30	·	·	·	3	1	·	3	9	23	19	7	2	·	9
VIII	3.5	1.9	·	·	2	3.5	2	2.5	·	·	5	3.4	14	2.6	3.5	3.0	63	0.9	74	17.5	8	·	·	·	5	·	·	—	—	13	11	3	3	·	2
IX	·	·	·	·	11.5	3.6	10	2.2	5.5	2.7	18.5	2.4	12.5	2.7	·	·	32	1.7	86	16.2	4	·	·	·	2	1	·	7	7	14	13	2	·	·	3
X	1	2.5	·	·	3	1.7	4	2.5	5	1.9	12	3.5	9	2.9	2	2.2	57	1.1	14	7.1	29	·	·	6	·	·	·	2	5	9	3	·	8	·	·
XI	3	2.0	5	3.2	7	2.7	10.5	4.3	4.5	4.7	24	5.0	·	·	·	·	36	2.5	49	12.2	21	5	10	19	·	1	·	2	14	17	13	1	1	10	·
XII	1	1.0	·	·	3	1.3	14	5.2	20.5	3.8	32	4.5	7.5	3.8	2	1.5	13	3.5	86	18.9	18	2	4	21	·	1	·	·	25	22	19	2	·	18	·
Rok	34.5	2.4	48	1.8	82.5	2.6	85.5	3.5	84	2.4	186	3.7	105	3.2	41.5	2.2	428	2.1	745	33.3	9.V	19	40	128	14	8	·	—	—	190	140	18	29	88	16

Stare Pole — $H_s = 3\,m$ — $h_w = 11{,}5\,m$

I	4	4.8	6	4.7	11.5	3.9	13.5	3.6	16	4.2	26	5.5	8.5	6.2	6.5	7.7	1	4.9	29	5.0	21	4	8	26	·	4	2	1	17	21	9	·	4	16	—
II	4.5	8.7	14	6.2	4.5	1.6	3.5	1.7	3	4.0	21.5	6.6	23.5	5.7	9.5	6.8	·	5.9	27	5.7	23	7	17	26	·	10	2	2	16	19	12	·	2	28	—
III	6	4.8	10	3.3	3	2.7	6.5	2.5	24.5	2.2	17	3.4	13.5	3.5	4.5	5.1	8	2.9	22	6.6	3	6	9	22	·	·	·	8	12	11	5	·	8	17	—
IV	10	5.8	9	5.7	19	4.9	20	3.6	8.5	2.3	5.5	2.7	8	2.8	4	6.2	6	4.0	33	5.8	21	·	·	8	·	2	·	2	13	12	10	·	5	·	—
V	23	5.3	18	3.9	8.5	4.5	7	6.7	5.5	2.7	8	5.4	11.5	2.9	5.5	4.5	6	4.2	30	7.6	10	·	·	4	·	2	·	4	11	9	7	·	2	·	—
VI	13	3.6	12.5	3.4	8	3.6	7	3.4	9	2.7	15	3.8	16.5	4.1	9	2.8	·	3.5	58	15.5	1	·	·	·	3	·	·	4	8	11	10	2	1	·	—
VII	7	4.5	8	3.6	7.5	2.7	5	2.5	26	4.4	26	5.9	9	5.6	2.5	4.8	2	4.6	78	14.2	16	·	·	·	3	2	·	2	8	22	19	1	1	·	—
VIII	8.5	2.2	5.5	2.1	2	2.2	7.5	2.3	12.5	2.7	12	2.7	18	2.4	18	3.7	9	2.5	74	22.7	27	·	·	·	5	·	·	3	12	17	10	2	3	·	—
IX	3	3.3	9	3.9	15.5	3.0	12.5	3.2	26	4.2	16.5	5.2	5	4.2	2.5	6.4	·	4.0	114	43.7	4	·	·	·	1	·	·	5	8	13	8	4	2	·	—
X	9	3.5	6.5	2.2	·	·	4	3.1	38.5	3.3	13.5	3.1	7.5	5.0	6	2.8	8	3.0	25	6.8	3	·	·	1	·	1	·	1	15	16	7	·	10	·	—
XI	4.5	4.0	11.5	3.2	7	3.3	13.5	4.6	22	3.4	16	4.4	3.5	4.9	2	3.0	10	3.4	29	8.9	21	8	11	19	·	1	·	·	15	22	7	·	3	15	—
XII	·	·	·	·	1.5	4.0	16	4.6	35.5	3.4	27.5	3.4	7	3.2	0.5	4.0	5	3.4	30	11.6	18	3	5	23	·	4	2	·	23	20	6	1	1	14	—
Rok	92.5	4.2	110	3.5	88	3.0	116	3.5	227	3.3	204.5	4.3	131.5	4.2	70.5	4.8	55	3.9	549	43.7	4.IX	28	50	129	12	26	6	32	158	193	110	10	42	90	—

Giżycko — $H_s = 132\,m$ — $h_w = 13\,m$

I	5	3.2	6	2.7	5	5.0	43	5.2	6	4.2	11	4.7	3	1.3	9	5.9	5	4.5	29	7.0	8	3	14	29	·	3	·	2	16	13	10	·	·	16	·
II	11	2.9	12	5.3	·	·	9	2.3	8	4.4	10	3.9	7	5.6	21	5.4	6	4.1	19	3.7	3	14	24	27	·	2	·	2	10	17	8	·	2	28	·
III	2	4.5	9	2.1	3	3.0	36	2.8	7	2.6	12	2.4	13	2.5	6	7.0	5	2.8	12	4.0	3	5	9	23	·	1	·	4	13	11	4	·	3	20	·
IV	1	3.0	9	4.1	22	6.1	33	5.1	11	2.5	1	1.0	2	1.5	8	3.6	3	4.5	13	5.5	23	·	·	10	·	3	·	3	13	7	5	·	·	·	1
V	8	2.6	14	2.9	14	4.0	14	3.2	6	2.0	6	4.0	5	3.6	19	3.2	7	3.0	63	14.5	19	·	·	3	·	·	·	4	8	13	11	2	·	·	1
VI	5	2.2	4	3.2	12	3.6	15	2.5	7	3.4	12	3.7	14	2.2	18	3.3	3	2.9	51	13.0	19	·	·	·	1	·	·	3	8	12	10	1	·	·	2
VII	·	·	7	3.6	3	1.0	12	2.0	10	3.2	34	4.4	6	4.2	3	1.3	18	2.8	91	17.0	12	·	·	·	3	·	·	1	7	21	16	5	·	·	5
VIII	10	2.6	1	1.0	4	1.8	18	2.4	4	3.5	15	2.7	12	2.3	18	3.3	11	2.4	60	22.5	26	·	·	·	6	·	·	4	6	15	8	2	·	·	2
IX	·	·	·	·	7	3.3	26	2.8	18	3.2	21	4.1	8	2.0	3	2.7	7	2.9	62	39.0	29	·	·	·	1	·	·	5	5	14	10	1	2	·	1
X	11	2.5	1	1.0	1	6.0	6	3.8	7	2.1	26	3.6	10	3.9	23	3.9	8	3.2	29	10.0	16	·	·	2	·	·	·	3	14	8	7	1	2	·	·
XI	4	3.0	5	3.8	15	3.7	19	7.3	7	3.3	16	6.7	10	3.9	10	4.8	4	4.9	25	6.8	1	6	16	21	·	4	·	·	18	17	8	·	·	16	·
XII	·	·	·	·	·	·	23	4.8	21	5.6	29	4.6	13	3.3	6	3.3	1	4.5	32	11.3	18	2	8	23	·	3	1	·	16	17	9	1	1	18	·
Rok	57	2.2	68	2.5	86	3.1	254	3.7	112	3.3	193	3.8	103	3.0	144	4.0	78	3.5	486	39.0	29.IX	30	71	138	11	16	1	31	134	165	107	13	10	98	12

Olecko

φ = 54°03′ λ = 22°30′

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																				
	P_m	Max	Min	P_{um}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	989.2	1005.3	970.0	1011.8	−0.9	−4.9	3.0	1	−12.9	10	−3.0	−2.1	−3.1	−2.8	4.6	4.6	4.5	4.6	89	86	89	88	0.5	0.7	0.5	0.6	9.3	8.4	8.2	8.6
II	990.7	1012.9	966.6	1013.6	−3.4	−11.4	0.9	12, 13, 14	−25.5	6	−8.6	−5.4	−7.0	−7.0	3.1	3.6	3.4	3.4	87	83	86	85	0.4	0.7	0.5	0.5	8.7	7.6	7.7	8.0
III	994.0	1010.4	968.0	1016.6	1.5	−5.2	8.0	28	−21.6	1	−4.1	0.8	−1.4	−1.5	4.4	4.9	4.7	4.7	89	73	81	81	0.6	1.8	1.1	1.2	7.2	6.3	6.1	6.5
IV	991.0	1005.5	972.1	1012.9	9.0	1.9	15.9	27	−3.7	3	3.2	7.9	4.9	5.2	6.3	6.1	6.5	6.3	80	57	73	70	1.6	4.9	2.4	3.0	7.9	7.7	6.6	7.4
V	992.3	1008.4	971.4	1013.9	12.8	4.5	19.0	18	−1.8	4	7.1	11.7	8.4	8.9	8.3	8.0	8.3	8.2	80	58	74	71	2.0	6.0	2.9	3.6	7.4	7.9	6.8	7.4
VI	992.6	999.9	984.9	1013.7	19.4	10.5	26.0	26	3.3	8	13.7	18.1	14.6	15.2	12.6	12.1	12.7	12.5	80	59	77	72	3.3	9.0	4.2	5.5	6.5	6.5	6.9	6.6
VII	989.7	1001.9	975.0	1010.8	19.9	10.9	28.0	15	5.6	5	13.9	18.0	14.4	15.2	13.1	12.4	13.1	12.9	82	60	79	74	3.0	8.8	3.6	5.1	7.0	7.9	7.3	7.4
VIII	993.2	1002.0	982.4	1014.5	19.5	10.3	26.7	25	6.4	31	12.6	18.0	13.7	14.5	13.1	12.8	13.2	13.0	89	63	84	79	1.7	8.5	2.8	4.3	6.5	6.6	5.6	6.2
IX	993.6	1009.5	982.5	1014.9	19.5	9.2	25.8	3	4.3	21	10.8	17.9	12.9	13.6	12.3	13.2	12.9	12.8	94	65	86	82	0.9	7.7	2.4	3.7	6.8	6.4	5.6	6.3
X	999.3	1014.6	983.2	1021.2	10.8	3.9	17.8	1	−2.7	21	5.3	9.9	7.0	7.3	8.7	9.1	8.8	8.9	95	75	87	86	0.4	3.4	1.3	1.7	8.7	7.9	8.2	8.3
XI	989.9	1006.3	963.6	1012.5	−0.5	−4.9	9.8	2	−18.6	24	−3.4	−1.5	−2.9	−2.7	4.8	4.9	4.8	4.8	90	83	90	88	0.6	1.1	0.5	0.7	9.3	9.0	9.2	9.2
XII	982.3	998.4	961.3	1004.4	0.6	−3.8	6.3	20	−14.6	17	−1.7	−1.0	−1.5	−1.4	4.9	5.1	5.1	5.0	90	88	90	89	0.5	0.7	0.6	0.6	9.1	8.8	9.3	9.1
Rok	991.5	1014.6	961.3	1013.4	9.0	1.8	28.0	15.VII	−25.5	6. II	3.8	7.7	5.0	5.4	8.0	8.1	8.2	8.1	87	71	83	80	1.3	4.4	1.9	2.5	7.9	7.6	7.3	7.6

Malbork

φ = 54°02′ λ = 19°02′

I	–	–	–	–	1.4	−3.5	5.4	1	−13.4	11	−1.3	0.4	−1.0	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.5	6.2	6.6
II	–	–	–	–	−0.7	−7.9	3.3	13	−20.6	6	−4.9	−2.2	−4.4	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	7.2	7.3
III	–	–	–	–	3.7	−4.9	12.0	29	−25.7	8	−3.0	2.1	−0.7	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.0	4.9	5.1
IV	–	–	–	–	10.2	2.5	15.9	28	−2.5	3	4.1	8.7	5.7	6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.5	5.9	7.2
V	–	–	–	–	13.7	4.8	20.1	18	−2.6	4	8.2	12.8	8.3	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.2	6.5	6.4
VI	–	–	–	–	20.8	10.7	29.7	26	5.3	8	14.4	19.8	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.5	5.4	5.7
VII	–	–	–	–	20.4	11.7	30.1	14	6.7	5	14.4	19.0	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.5	6.8	6.8
VIII	–	–	–	–	20.7	10.8	29.1	22	5.3	16	13.4	19.5	14.0	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.2	5.0	6.3
IX	–	–	–	–	19.7	9.8	27.3	3	4.9	16	11.9	18.7	13.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.0	3.6	5.5
X	–	–	–	–	12.6	5.0	19.6	1	−0.7	21	6.2	11.7	7.6	8.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.9	4.6	6.7
XI	–	–	–	–	2.0	−4.0	11.4	2	−16.6	24	−1.9	0.1	−1.4	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.8	7.4	8.0
XII	–	–	–	–	2.4	−2.1	10.1	19	−17.7	17, 18	−0.1	1.0	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.5	7.9	8.3
Rok	–	–	–	–	10.6	2.7	30.1	14.VII	−25.7	9. III	5.1	9.3	5.9	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	6.0	6.7

Dziwnów

φ = 54°01′ λ = 14°44′

I	1008.2	1027.4	982.8	1009.1	2.9	−0.8	7.1	17	−5.6	31	0.6	1.6	0.8	1.0	5.7	6.0	5.8	5.9	88	86	89	88	0.8	1.0	0.7	0.8	8.1	8.2	6.1	7.5
II	1016.4	1034.5	986.8	1017.3	0.9	−2.7	5.2	13	−9.0	28	−1.2	−0.5	−0.7	−0.7	4.9	5.0	5.0	5.0	85	83	84	84	0.8	1.0	0.9	0.9	7.4	7.6	5.9	7.0
III	1015.1	1031.4	994.2	1016.0	4.4	−1.9	13.1	29	−13.7	8	−1.0	2.9	1.2	1.1	5.2	5.9	5.7	5.6	88	77	82	82	0.7	1.9	1.2	1.3	6.2	5.6	3.8	5.2
IV	1009.7	1032.5	985.1	1010.5	9.2	3.5	16.5	6	−1.6	5	4.6	7.5	5.8	5.9	7.4	7.4	7.4	7.4	86	73	81	80	1.2	3.2	1.9	2.1	7.6	7.5	5.3	6.8
V	1013.3	1027.8	993.3	1014.1	11.7	6.4	17.3	17	0.7	3	8.4	10.1	8.9	9.0	9.1	9.4	9.5	9.3	82	76	83	80	1.9	3.1	2.0	2.3	5.7	5.3	5.9	5.6
VI	1013.0	1024.0	995.9	1013.8	18.2	11.7	29.3	26	7.2	4	13.8	16.4	14.3	14.7	13.3	13.5	13.6	13.5	84	73	83	80	2.7	4.8	3.0	3.5	4.8	4.7	5.6	5.0
VII	1008.9	1020.9	990.4	1009.7	17.5	12.2	25.8	21	9.2	11	13.8	16.0	14.3	14.6	13.7	13.7	14.1	13.8	86	76	86	83	2.3	4.8	2.3	3.1	6.8	7.3	6.4	6.8
VIII	1014.1	1024.2	999.8	1014.9	19.0	12.8	27.6	22	9.1	31	14.4	17.4	15.2	15.6	14.4	14.3	14.2	14.3	87	72	82	80	2.1	5.8	3.3	3.7	5.0	5.3	4.4	4.9
IX	1011.3	1032.8	995.7	1012.1	19.0	11.5	25.7	3	7.8	30	12.5	17.9	13.9	14.6	13.4	14.1	14.0	13.8	92	70	86	83	1.2	6.8	2.0	3.3	6.4	5.7	4.2	5.4
X	1021.6	1037.1	1003.4	1022.4	12.7	6.6	19.6	2	1.5	26	8.0	11.7	9.3	9.6	10.0	10.7	10.3	10.3	92	77	87	85	1.0	3.2	1.6	1.9	7.6	5.9	3.9	5.8
XI	1009.0	1029.1	976.4	1009.9	3.2	−1.4	11.8	1	−11.1	18	0.2	2.2	0.6	0.9	5.9	6.0	5.9	5.9	88	78	86	84	0.7	1.5	0.9	1.0	8.0	7.1	5.8	7.0
XII	1000.2	1022.7	968.1	1001.1	3.2	−0.4	11.1	19	−4.2	17	1.1	1.8	1.2	1.3	6.1	6.3	6.2	6.2	90	89	91	90	0.6	0.8	0.6	0.7	8.8	9.0	7.5	8.5
Rok	1011.7	1037.1	968.1	1012.5	10.2	4.8	28.3	26.VI	−13.7	8. III	6.3	8.8	7.1	7.3	9.1	9.4	9.3	9.3	87	78	85	83	1.3	3.2	1.7	2.1	6.9	6.6	5.4	6.3

Piaszczyna

φ = 54°01′ λ = 17°10′

I	–	–	–	–	1.4	−3.3	5.9	1	−14.1	11	−1.4	−0.2	−1.1	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−0.7	−8.9	3.1	7, 12, 13	−19.7	24	−5.1	−2.2	−4.5	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.5	−5.3	11.7	29	−23.2	8	−3.3	2.2	−0.7	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.1	1.9	16.3	22	−4.0	5	3.5	8.4	5.5	5.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	13.3	4.0	19.9	17, 28	−3.5	3	7.1	11.5	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.2	9.4	29.3	26	5.0	4, 15	13.3	18.4	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	18.5	10.1	28.9	14	5.5	5, 6	12.7	16.7	13.2	14.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	19.1	7.9	26.3	6,20,22,23	3.0	13,18,31	11.2	17.8	13.2	13.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.8	8.5	26.3	3	3.5	16	10.1	17.4	12.7	13.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.3	3.7	19.8	1	−1.5	20	5.7	11.4	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.5	−4.1	10.2	2	−15.1	18	−2.2	0.1	−1.4	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.2	−2.4	10.2	19	−15.5	16	−0.5	0.4	0.1	0.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.0	1.8	29.3	26.VI	−23.2	8. III	4.3	8.5	5.5	6.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Olecko

$H_s = 181\,m$ $H_b = 177{,}7\,m$ $h_w = 13\,m$ **1965**

MIESIĄC	ROZKŁAD WIATRU (%D, %wD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<-10	Max<0	Min<0	Min>25	Wiatr V V≥10	V≥15	◐	●	Opad R R≥0.1	R≥10	R≥100	≡	⊠	K
I	·	·	4.5	3.1	13	3.7	19	5.1	17	6.4	16.5	5.4	7	6.3	16	5.2	·	5.2	29	5.9	8	3	15	29	·	3	1	·	21	18	9	·	5	18	·
II	15	4.5	11.5	4.7	3.5	2.9	2	3.0	7.5	4.7	14.5	6.0	17.5	5.8	12.5	6.0	·	5.2	14	2.8	27	14	23	27	·	5	1	1	17	20	4	·	1	28	·
III	3	3.0	8	3.5	8	3.6	18	3.4	18.5	4.2	16	2.5	17	4.9	4.5	8.7	·	3.9	19	4.7	3	6	9	22	·	3	·	5	15	13	6	·	8	25	·
IV	3.5	4.0	9.5	4.5	20.5	5.0	31	5.4	12	3.8	2.5	3.2	7	4.1	4	6.2	·	4.8	27	9.7	23	·	·	10	·	1	·	2	14	9	7	·	2	·	1
V	12.5	4.0	9	2.1	16.5	3.6	12	2.9	8.5	3.3	7.5	5.3	12	3.7	15	4.8	·	3.7	72	24.9	19	·	·	3	·	·	·	2	16	15	9	2	2	·	1
VI	10.5	3.0	7	4.1	12	4.0	5.5	4.2	9.5	4.1	11.5	3.9	22.5	3.9	11.5	2.7	·	3.7	71	17.6	23	·	·	·	1	·	·	3	11	12	11	2	·	·	2
VII	1	4.0	10	3.7	1.5	2.7	6	3.2	15	4.8	37.5	3.7	19	4.1	2	3.0	1	3.8	85	14.4	12	·	·	·	3	·	·	·	15	20	14	3	·	·	8
VIII	2	2.5	·	·	1	5.0	18	3.6	6	4.3	13.5	3.3	27.5	3.5	23	3.3	2	3.4	50	10.5	27	·	·	·	5	·	·	4	11	12	8	1	1	·	3
IX	·	·	·	·	7	2.7	24	3.4	16	2.9	28.5	3.2	13	4.8	1.5	1.3	·	3.3	49	22.8	29	·	·	·	2	·	·	2	9	14	9	1	2	·	3
X	2.5	2.8	3	2.7	3	3.7	4.5	4.0	6	2.8	25	4.0	22.5	4.0	23.5	3.9	3	3.7	22	10.9	16	·	·	2	·	·	·	·	21	8	4	1	6	·	·
XI	1	2.0	22	4.3	5	3.4	12.5	5.4	10.5	4.0	21	5.3	12.5	3.4	5.5	4.1	·	4.4	46	11.8	1	7	16	21	·	2	1	·	25	22	11	1	2	16	·
XII	·	·	·	·	0.5	4.0	17	4.5	28	6.1	32	4.3	12.5	3.9	1	5.0	2	4.8	42	14.3	19	4	13	27	·	4	·	·	26	21	8	1	2	25	·
Rok	51	2.5	84.5	2.7	91.5	3.7	169.5	4.0	154.5	4.3	226	4.2	190	4.4	120	4.5	8	4.2	526	24.9	19. V	34	76	141	11	18	3	19	201	184	100	12	31	112	18

Malbork

$H_s = 20\,m$ $h_w = 11\,m$

I	3	5.2	6	4.1	15	3.1	14.5	6.6	26	6.8	14	6.5	3.5	3.3	8	7.1	3	5.6	36	8.4	21	4	8	25	·	7	1	1	12	19	11	·	1	21	·
II	5.5	5.2	12.5	6.2	7	4.0	7	4.6	10.5	6.3	10.5	5.2	15.5	4.5	13.5	7.9	2	5.5	33	8.2	27	8	18	26	·	7	·	·	11	18	9	·	2	28	·
III	3	4.3	18	3.5	5	3.7	11.5	4.7	23.5	3.7	13.5	4.1	11.5	4.5	2	6.0	5	3.8	35	14.5	3	5	7	21	·	3	·	8	10	10	6	1	3	18	·
IV	9.5	5.4	10.5	5.5	15.5	5.1	24	4.9	5.5	3.2	7	3.3	5	3.2	5	4.4	8	4.3	32	5.9	21	·	·	7	·	1	·	1	14	11	10	·	3	·	·
V	20	5.0	19	4.4	11	4.9	11.5	6.3	2	5.0	9	4.2	10.5	6.0	8	4.4	2	4.9	27	7.6	10	·	·	3	·	7	·	2	13	10	7	·	1	·	·
VI	14	3.5	10.5	4.6	10.5	4.4	4	5.8	9.5	7.7	6.5	5.2	14.5	4.9	18.5	4.8	2	4.8	57	17.4	1	·	·	·	3	8	1	4	9	11	9	2	·	·	4
VII	6.5	3.2	9	5.1	3	2.7	6.5	3.8	4.5	5.6	24.5	5.8	29.5	5.4	7.5	3.9	·	5.0	90	19.8	15	·	·	·	2	6	·	2	10	22	18	2	1	·	6
VIII	14.5	3.7	2	1.8	·	·	6	4.7	10	5.6	12.5	2.9	13	4.3	25	3.4	10	3.4	75	19.6	27	·	·	·	5	4	·	3	11	17	11	3	5	·	1
IX	1	4.5	1	4.0	5.5	4.4	5.5	5.9	19	4.8	27.5	4.0	14	4.6	10.5	4.4	6	4.2	118	61.5	4	·	·	·	1	4	·	5	6	12	7	3	3	·	·
X	11.5	3.5	4.5	2.7	2	4.0	8	1.8	6	4.0	17	5.2	20.5	4.2	17.5	4.5	6	3.8	20	5.9	16	·	·	1	·	2	·	1	10	8	6	·	8	·	·
XI	1.5	7.3	9.5	4.0	14	4.3	7.5	8.1	13.5	8.9	25.5	4.7	12	7.0	6.5	5.1	·	5.8	39	22.2	21	8	11	19	·	8	4	·	16	16	7	1	3	15	·
XII	·	·	·	·	·	·	3.5	9.1	24.5	9.5	4.2	6.1	16	4.4	6	7.3	1	6.8	27	7.7	18	4	5	20	·	11	3	·	19	16	7	·	2	10	·
Rok	90	4.2	102.5	3.8	88.5	3.4	111.5	5.5	154.5	5.9	209.5	4.8	165.5	4.7	128	5.3	45	4.8	589	61.5	4. IX	29	49	122	11	68	9	27	141	170	108	12	32	92	11

Dziwnów

$H_s = 7\,m$ $H_p = 7{,}1\,m$ $h_w = 18\,m$

I	2.5	4.4	5.5	6.4	7.5	3.6	20	3.2	30.5	4.7	10	5.0	10	4.6	5	6.9	2	4.4	31	5.0	8	·	1	19	·	2	·	·	15	17	10	·	2	7	·
II	17.5	9.1	11.5	7.1	3.5	3.6	1	2.0	6.5	3.5	13	5.2	13	6.7	16	8.9	2	6.9	19	5.3	23	·	8	23	·	13	2	1	11	14	5	·	1	18	·
III	5	5.1	9.5	7.4	6.5	4.1	11	3.4	31.5	3.4	11	3.8	12.5	5.2	4	8.5	2	4.4	17	7.3	24	1	5	21	·	4	·	6	7	9	5	·	4	17	·
IV	3.5	6.4	19.5	6.1	10	4.4	16	3.5	9.5	4.1	6.5	3.9	11.5	5.2	5.5	4.8	8	4.4	32	6.8	19	·	·	2	·	3	·	1	12	15	10	·	2	·	·
V	6.5	4.9	26	6.7	12.5	4.0	9.5	3.8	3	3.1	4.5	3.9	14	4.2	11	8.0	6	5.0	55	18.0	10	·	·	·	·	9	1	7	11	14	8	2	2	·	1
VI	5	4.0	22.5	5.6	6	3.2	3	3.8	8.5	4.5	9	4.2	16	6.3	14	5.4	6	4.8	18	7.8	18	·	·	·	3	5	·	6	7	6	4	·	·	·	3
VII	2	5.5	10	8.7	6	4.0	1	2.0	12	3.8	30	5.4	24.5	7.3	4.5	7.4	3	5.9	121	21.2	21	·	·	·	1	13	·	2	13	22	18	4	4	·	5
VIII	8	4.4	7.5	2.4	4	2.2	6.5	2.8	13	3.5	11.5	4.0	19.5	4.2	12	5.2	11	3.4	55	15.3	23	·	·	·	1	1	·	4	5	11	8	2	2	·	4
IX	1	4.0	1.5	3.7	5.5	5.1	12	3.5	27	3.8	22	5.0	10.5	6.5	3.5	6.7	7	4.3	72	20.5	10	·	·	·	1	4	1	7	7	13	10	4	2	·	5
X	8	4.1	6	2.9	8	3.5	10	2.8	19	3.9	13.5	5.7	11	6.0	11.5	6.7	6	4.3	13	6.6	29	·	·	·	·	4	2	1	1	7	2	·	8	·	·
XI	1.5	9.7	2	10.0	16	4.5	20.5	4.0	16	4.0	20.5	6.8	9.5	7.8	3	8.2	1	5.5	36	10.2	1	1	9	16	·	6	3	2	12	14	7	1	2	11	·
XII	1.5	4.7	·	·	2	4.0	14	4.2	27.5	5.5	28	7.1	15	7.6	3	5.0	2	6.0	65	18.1	9	·	2	18	·	9	·	·	21	22	14	1	3	10	·
Rok	62	5.5	121.5	5.6	87.5	3.8	124.5	3.2	204	4.0	179.5	5.0	167	6.0	93	6.8	56	4.9	534	21.2	21. VII	2	25	99	6	73	9	37	122	164	101	14	32	63	18

Piaszczyna

$H_s = 175\,m$ $h_w = 12\,m$

I	2.5	3.4	1	4.0	5	3.4	22	3.7	11	4.0	23	3.8	10	3.6	18.5	3.2	·	3.6	85[2]	19.2	17	2	8	25	·	·	·	—	—	14	13	3	—	21	—
II	10.5	2.7	11.5	4.1	1	5.0	4	3.0	·	·	11	4.2	18	4.3	28	3.6	·	3.8	66	18.0	12	13	19	27	·	·	·	—	—	17	14	1	—	28	—
III	3	5.3	12	4.2	6	3.8	11	3.5	7	2.8	25	2.8	13	3.3	16	3.1	·	3.3	58	28.0	3	7	9	23	·	·	·	—	—	9	7	2	—	24	—
IV	6	3.8	3	3.0	22	3.6	23.5	4.4	7.5	4.4	2	2.5	6	3.3	20	3.2	·	3.7	21	6.6	23	·	·	7	·	·	·	—	—	7	5	·	—	·	—
V	13.5	3.5	7	3.6	21	3.8	15.5	4.6	5	3.0	1.5	3.3	14	3.1	15.5	3.8	·	3.7	113	45.2	9	·	·	2	·	1	·	—	—	16	14	3	—	·	—
VI	2.5	3.4	5	2.4	14	3.7	10	4.4	6	4.4	7	3.7	15	4.5	25.5	4.1	·	4.0	83	22.2	1	·	·	·	3	·	·	—	—	9	9	4	—	·	—
VII	2.5	4.4	8.5	3.6	4	4.5	6	3.8	9.5	4.9	21.5	4.1	32	3.8	9	3.7	·	4.0	193	30.4	15	·	·	·	2	·	·	—	—	25	25	4	—	·	—
VIII	11.5	2.4	2	3.0	·	·	6.5	4.5	4	3.2	11.5	2.3	21	3.0	36.5	3.0	·	2.9	82	14.2	25	·	·	·	4	·	·	—	—	16	16	1	—	·	—
IX	0.5	4.0	1.5	3.3	7	4.4	24.5	4.1	6.5	3.6	16	3.9	17	3.7	17	3.0	·	3.0	86	16.2	10	·	·	·	1	·	·	—	—	13	13	2	—	·	—
X	1.4	2.6	0.5	3.0	5	5.0	3	2.0	4	4.0	22	3.9	11	4.0	33.5	3.6	·	3.6	18	7.2	29	·	·	3	·	·	·	—	—	4	4	·	—	·	—
XI	3	3.0	8.5	3.4	12	3.7	13	4.6	7.5	5.0	27.5	4.0	6	6.0	12.5	4.0	·	4.2	32	12.6	1	5	11	21	·	·	·	—	—	10	10	1	—	13	—
XII	4.5	3.9	7	3.1	·	·	10.5	4.7	18.5	4.7	31	4.6	9	5.7	12.5	4.8	·	4.6	68	22.5	18	2	4	20	·	1	1	—	—	15	14	2	—	21	—
Rok	79	3.5	67.5	3.4	97	3.4	149.5	3.9	86.5	3.7	199	3.6	172	4.0	244.5	3.6	·	3.8	905[2]	45.2	9. V	29	51	128	10	2	1	—	—	155	144	23	—	107	—

Miastko

φ = 54°00′ λ = 16°58′ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	-3.1	4.7	17	-11.3	11	-1.6	0.0	-1.1	-1.0	5.2	5.4	5.2	5.3	90	87	91	89	0.4	0.8	0.5	0.6	8.5	7.5	7.6	7.9
II	–	–	–	–	-0.8	-9.0	2.4	13	-20.0	17	-4.8	-1.8	-4.7	-4.0	4.0	4.5	4.0	4.2	90	83	89	87	0.4	0.9	0.4	0.6	7.9	7.1	7.0	7.3
III	–	–	–	–	3.7	-5.4	12.4	29	-24.8	8	-3.4	2.6	-1.2	-0.8	4.7	5.6	5.2	5.2	90	75	88	84	0.4	2.0	0.6	1.0	7.2	5.7	4.8	5.9
IV	–	–	–	–	10.0	2.0	15.4	30	-4.3	5	3.3	8.6	5.0	5.5	7.1	7.2	7.4	7.2	90	65	85	80	0.8	4.2	1.4	2.1	8.1	7.4	6.8	7.4
V	–	–	–	–	13.3	4.1	19.2	17	-4.3	3	7.2	11.8	7.9	8.7	8.3	8.0	8.5	8.3	81	58	79	73	2.0	6.1	2.2	3.4	6.0	6.5	5.6	6.0
VI	–	–	–	–	20.4	9.6	29.2	26	5.2	7	13.9	18.6	13.9	15.1	12.2	12.2	12.4	12.3	76	58	77	70	3.9	9.9	3.7	5.8	4.1	6.2	4.3	4.9
VII	–	–	–	–	18.7	10.4	28.9	14	5.3	5	13.1	16.9	13.3	14.2	13.2	13.1	13.8	13.4	86	68	89	81	2.1	6.7	1.8	3.5	5.0	6.7	6.5	6.1
VIII	–	–	–	–	19.5	9.2	27.4	22	5.3	12, 17, 29	12.3	18.4	12.9	14.1	13.1	13.3	13.6	13.3	91	63	91	82	1.4	8.5	1.5	3.8	5.0	5.7	3.7	4.8
IX	–	–	–	–	18.7	8.7	25.8	3	2.3	16	10.7	17.5	12.1	13.1	12.2	12.8	12.8	12.6	94	65	91	83	0.9	7.6	1.5	3.3	5.6	5.3	4.5	5.1
X	–	–	–	–	12.1	3.2	19.7	1	-4.1	12	5.1	11.4	6.2	7.2	8.5	10.1	8.9	9.2	94	74	93	87	0.6	3.6	0.7	1.6	7.5	5.8	3.9	5.7
XI	–	–	–	–	1.5	-4.2	10.7	1, 2	-16.3	24	-2.3	0.5	-1.6	-1.2	5.1	5.7	5.3	5.4	90	84	90	88	0.5	1.0	0.5	0.7	8.2	7.7	6.0	7.3
XII	–	–	–	–	1.5	-2.5	9.6	19	-15.2	17	-0.7	-0.1	-0.3	-0.4	5.6	5.5	5.7	5.6	94	87	92	91	0.4	0.8	0.5	0.6	9.9	9.1	9.8	9.6
Rok	–	–	–	–	10.0	1.9	29.2	26.VI	-24.8	8. III	4.4	8.7	5.2	5.9	8.3	8.6	8.6	8.5	89	72	88	83	1.2	4.3	1.3	2.3	6.9	6.7	5.9	6.5

Radostowo

φ = 53°59′ λ = 18°45′

I	–	–	–	–	1.2	-4.4	5.4	1	-15.0	11	-1.8	0.1	-1.6	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.4	7.5	7.8
II	–	–	–	–	-0.7	-8.8	2.6	12	-20.1	6	-4.9	-1.9	-4.5	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	7.8	8.0
III	–	–	–	–	2.8	-5.8	12.4	29	-26.2	8	-3.9	1.5	-1.5	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	7.0	7.3
IV	–	–	–	–	9.9	1.9	15.6	22	-3.0	3	3.9	8.4	5.1	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.2	7.5	8.2
V	–	–	–	–	13.8	4.0	20.1	18	-3.4	4	8.1	12.3	7.3	8.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.9	7.0
VI	–	–	–	–	20.5	9.3	29.1	26	3.5	8	14.4	19.2	13.4	15.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	6.4	6.5
VII	–	–	–	–	20.2	10.2	28.2	15	4.5	2	14.3	18.6	13.6	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.1	7.8	7.8
VIII	–	–	–	–	20.9	9.4	29.8	22	4.0	16	13.4	19.5	13.6	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	6.2	6.9
IX	–	–	–	–	19.8	8.5	28.1	3	3.4	16	11.0	18.5	12.1	13.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	5.2	6.3
X	–	–	–	–	12.7	3.7	19.0	1	-2.0	21	6.2	11.8	6.8	7.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.1	5.8	7.1
XI	–	–	–	–	1.6	-4.8	11.7	1	-21.8	24	-2.3	-0.2	-1.7	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	7.5	7.8
XII	–	–	–	–	2.1	-3.4	10.1	19	-20.6	17	-0.7	0.8	-0.4	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.6	8.1	8.6
Rok	–	–	–	–	10.4	1.6	29.8	22.VIII	-26.2	8. III	4.8	9.0	5.2	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.4	7.0	7.4

Międzyzdroje

φ = 53°56′ λ = 14°27′

I	–	–	–	–	2.7	-1.1	6.8	17	-6.7	7	0.4	1.8	0.8	1.0	5.9	6.1	6.0	6.0	93	88	91	91	0.5	0.9	0.6	0.7	8.1	7.9	6.9	7.6
II	–	–	–	–	0.8	-3.6	4.5	13	-13.2	28	-1.8	0.0	-1.1	-1.0	4.9	5.3	5.0	5.1	89	86	86	87	0.5	0.8	0.8	0.7	8.0	6.4	7.0	7.1
III	–	–	–	–	5.1	-2.4	11.9	24	-13.3	8	-0.8	3.6	1.2	1.3	5.3	6.0	5.9	5.7	89	75	85	83	0.7	2.2	1.0	1.3	6.6	6.0	5.7	6.1
IV	–	–	–	–	10.4	2.9	16.4	6	-4.2	5	4.8	8.7	5.9	6.3	7.7	7.9	7.8	7.8	88	72	83	81	1.0	3.5	1.7	2.1	7.0	5.4	5.6	6.0
V	–	–	–	–	14.0	5.7	20.0	17	0.1	3	8.9	12.6	8.9	9.8	9.3	9.4	9.4	9.4	81	65	82	76	2.2	5.4	2.1	3.2	5.8	4.7	4.8	5.1
VI	–	–	–	–	20.6	11.9	28.7	26	7.5	1	14.9	19.0	14.8	15.9	13.1	13.2	13.1	13.1	77	61	78	72	4.1	9.4	3.9	5.8	5.6	3.9	4.8	4.8
VII	–	–	–	–	18.9	11.4	25.9	21	7.8	7, 11	13.7	16.9	14.0	14.6	13.6	14.2	13.9	13.9	86	74	86	82	2.3	5.5	2.3	3.4	6.7	6.5	6.5	6.6
VIII	–	–	–	–	20.3	11.5	27.9	22	7.2	31	14.1	18.9	14.5	15.5	14.6	15.6	14.3	14.8	90	71	87	83	1.6	6.5	2.3	3.5	5.2	4.7	5.4	5.1
IX	–	–	–	–	19.3	10.9	25.6	3	7.9	30	12.3	18.1	13.2	14.2	13.1	14.3	13.4	13.6	92	69	88	83	1.3	6.9	1.9	3.4	6.8	6.2	4.6	5.9
X	–	–	–	–	13.5	5.9	23.0	1	-0.6	23	7.3	12.6	8.6	9.3	9.8	10.8	10.0	10.2	95	73	89	86	0.6	4.0	1.3	2.0	6.3	5.1	4.0	5.1
XI	–	–	–	–	3.0	-2.1	11.8	1	-11.9	18	-0.5	2.1	0.0	0.4	5.7	6.0	5.8	5.8	90	80	89	86	0.6	1.5	0.7	0.9	7.7	6.9	6.5	7.0
XII	–	–	–	–	3.1	-0.6	10.4	19	-3.9	17	0.9	2.0	1.1	1.3	6.0	6.3	6.1	6.1	91	88	91	90	0.6	0.8	0.6	0.7	8.0	8.5	8.1	8.2
Rok	–	–	–	–	11.0	4.2	28.7	26.VI	-13.3	8. III	6.2	9.7	6.8	7.4	9.1	9.6	9.2	9.3	86	75	86	83	1.3	4.0	1.6	2.3	6.8	6.0	5.8	6.2

Świnoujście

φ = 53°55′ λ = 14°14′

I	1008.7	1027.3	982.4	1009.4	3.1	-0.6	7.4	17	-6.0	31	0.7	2.0	1.1	1.2	5.8	6.1	5.9	5.9	90	86	89	88	0.7	1.0	0.8	0.8	7.9	8.4	6.9	7.7
II	1017.1	1034.5	986.3	1017.8	1.2	-3.5	5.4	13	-13.4	28	-1.8	-0.1	-0.8	-0.9	4.7	5.1	4.8	4.9	86	84	83	84	0.8	1.0	1.0	0.9	7.9	7.7	6.6	7.4
III	1015.6	1031.6	996.3	1016.3	5.3	-2.1	15.5	29	-12.9	8	-0.9	3.4	1.3	1.3	5.4	5.9	5.9	5.7	90	75	85	83	0.6	2.1	1.1	1.3	6.6	6.0	4.2	5.6
IV	1010.2	1032.2	986.6	1010.8	9.4	3.0	15.9	6	-2.4	5	4.7	7.6	5.7	5.9	7.7	7.8	7.8	7.8	90	77	85	84	0.9	2.7	1.5	1.7	7.3	7.2	5.8	6.8
V	1013.7	1027.9	997.1	1014.3	12.7	6.5	20.4	17	0.2	3	8.7	11.3	9.2	9.6	9.3	9.7	9.9	9.6	82	73	85	80	2.0	3.9	1.8	2.6	6.5	6.2	6.5	6.4
VI	1013.5	1024.1	996.7	1014.1	19.3	11.6	28.5	26	7.8	3	14.4	17.7	14.7	15.4	13.3	13.5	13.6	13.5	81	67	81	76	3.3	7.6	3.4	4.8	6.0	6.4	5.6	6.0
VII	1009.4	1021.2	991.5	1010.0	18.5	11.7	26.7	21	8.1	11	13.7	16.3	14.0	14.5	13.5	13.7	13.9	13.7	85	74	86	82	2.3	5.2	2.2	3.2	6.8	8.0	6.8	7.2
VIII	1014.3	1024.2	999.7	1014.9	19.5	11.6	27.1	22	8.1	1	13.8	18.0	14.9	15.4	14.2	13.8	13.8	13.9	89	67	81	79	1.7	7.0	3.4	4.0	6.1	6.2	5.5	5.9
IX	1011.4	1033.0	996.0	1012.0	19.0	11.4	24.8	3	8.2	30	12.7	17.8	13.8	14.5	13.0	13.5	13.3	13.3	89	67	84	80	1.8	7.2	2.7	3.9	6.4	6.0	4.6	5.7
X	1021.6	1036.8	1004.2	1022.2	13.3	5.9	20.7	1	0.3	22, 23	7.3	12.2	9.0	9.4	9.6	10.6	10.1	10.1	92	74	86	84	0.8	3.8	1.6	2.1	6.5	5.6	5.0	5.7
XI	1009.3	1029.8	977.4	1010.0	3.4	-1.7	12.6	1	-10.3	18	0.0	2.2	0.5	0.8	5.6	5.8	5.7	5.7	86	76	85	82	0.9	1.8	0.9	1.2	8.3	7.0	5.9	7.1
XII	1000.6	1022.9	969.1	1001.3	3.5	-0.4	11.0	19	-3.6	14	1.2	2.1	1.4	1.5	5.9	6.1	6.1	6.0	86	84	88	86	0.9	1.2	0.8	1.0	8.8	8.8	7.5	8.4
Rok	1012.1	1036.8	969.1	1012.7	10.7	4.4	28.5	26.VI	-13.4	28. II	6.2	9.2	7.1	7.4	9.0	9.3	9.2	9.2	87	75	85	82	1.4	3.7	1.8	2.3	7.1	7.0	5.9	6.7

Miastko

$H_s = 145\ m$ $h_w = 12\ m$ **1965**

ROZKŁAD WIATRU (n_D, v_{mD}) — OPAD R — LICZBA DNI (n): Temperatura T, Wiatr v, Opad R

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	◕	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊟	K (K)
I	1	2.0	2	2.5	4	1.8	2	2.5	27	2.5	10	3.8	19	1.7	4	2.0	24	1.8	48	7.0	17	1	9	26	·	1	·	1	17	20	12	·	3	19	·
II	11	2.3	2	2.0	2	2.0	·	·	3	2.3	14	2.5	17	2.1	20	2.4	15	1.9	51	7.5	14	10	20	27	·	·	·	1	13	21	14	·	2	28	·
III	9	2.7	2	2.0	5	1.8	3	1.7	20	1.8	10	2.2	15	1.8	4	2.5	25	1.5	37	17.8	3	6	8	24	·	·	·	6	9	13	7	1	5	22	·
IV	4	2.8	5	3.0	10	2.6	14	2.0	15	2.4	6	2.3	13	1.8	7	2.4	16	1.9	29	14.7	23	·	·	8	·	·	·	4	15	11	6	1	3	·	·
V	4	2.0	7	2.3	6	2.3	16	2.5	8	2.5	5	2.4	16	2.1	14	2.5	17	1.9	92	35.9	9	·	·	5	·	·	·	4	12	17	11	3	1	·	·
VI	2	2.5	2	4.0	5	3.0	10	2.7	10	2.3	11	2.5	30	2.2	12	2.8	8	2.3	71	22.2	22	·	·	·	4	·	·	5	5	11	7	3	·	·	3
VII	·	·	6	3.2	1	2.0	5	1.8	17	1.9	25	2.3	22	2.8	7	2.4	10	2.1	133	24.2	21	·	·	·	2	·	·	3	7	23	21	5	1	·	7
VIII	·	·	·	·	·	·	·	·	10	2.0	12	2.2	24	2.2	9	3.0	38	1.4	62	13.5	4	·	·	·	4	·	·	4	3	15	10	3	·	·	4
IX	1	2.0	·	·	1	3.0	13	2.7	24	2.1	13	2.2	14	2.4	5	2.2	19	1.8	76	19.7	10	·	·	·	1	·	·	7	6	14	13	2	2	·	5
X	1.5	1.7	·	·	·	·	2	2.0	12.5	2.0	15.5	2.3	25	2.2	6.5	2.7	30	1.5	18	5.2	29	·	·	7	·	·	·	2	5	8	6	·	12	·	·
XI	2	1.0	4	3.0	5	2.2	8.5	1.9	11.5	2.3	13.5	3.5	19.5	2.5	5	1.8	21	1.9	51	12.2	1	8	12	21	·	·	·	1	14	19	11	2	3	10	·
XII	1	3.0	1	2.0	·	·	10.5	2.8	22	3.0	15.5	4.3	21	2.5	5	2.6	17	2.5	82	20.6	18	2	6	23	·	·	·	·	28	20	16	2	·	18	·
Rok	36.5	1.8	31	2.0	39	1.7	84	1.9	180	2.3	150.5	2.7	235.5	2.2	98.5	2.4	240	1.9	750	35.9	9.V	27	55	141	11	1	·	38	134	192	134	22	32	97	19

Radostowo

$H_s = 40\ m$ $h_w = 15\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	◕	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊟	K (K)
I	3	4.8	5	5.0	4.5	4.1	10	4.5	15.5	6.5	29.5	5.7	7	3.4	7.5	3.9	11	4.6	29	6.0	21	4	8	28	·	—	—	·	12	19	10	·	—	22	·
II	6	7.9	15.5	5.8	0.5	1.0	2.5	3.4	5	5.9	16.5	6.5	25	4.5	11	5.4	2	5.4	24	7.0	14	9	16	28	·	—	—	·	15	17	7	·	—	28	·
III	10.5	5.0	11.5	6.2	1.5	4.3	6.5	3.4	16.5	4.0	19.5	3.6	15.5	4.6	6.5	3.7	5	4.1	27	8.4	3	10	9	23	·	—	—	1	15	12	9	·	—	19	·
IV	9	4.5	15.5	6.0	12	7.0	15.5	6.2	12	5.6	5	5.3	8.5	3.3	7.5	3.2	5	5.1	38	7.0	27	·	·	8	·	—	—	·	17	13	10	·	—	·	1
V	23.5	5.5	22	4.4	8.5	6.1	7	5.3	4	4.0	11	3.8	10	4.6	5	4.9	2	4.8	30	6.9	7	·	·	4	·	—	—	·	14	10	7	·	—	·	·
VI	14	4.2	12	5.2	7	4.4	4.5	4.8	6.5	6.6	13	6.1	19	3.8	10	3.4	4	4.5	57	25.0	1	·	·	·	3	—	—	1	8	10	7	1	—	·	1
VII	8.5	5.2	5	5.4	4	3.6	4	4.2	8	4.4	40.5	5.7	15.5	4.4	5.5	3.2	2	4.9	75	14.2	23	·	·	·	2	3	·	·	15	20	15	3	—	·	5
VIII	13	3.1	5	2.7	1.5	2.7	4	5.2	8	5.4	14.5	3.7	21	3.1	16	3.0	10	3.1	65	15.0	25	·	·	·	7	3	·	·	9	18	10	3	—	·	2
IX	4	3.4	5	3.7	3.5	5.9	7	4.1	16.5	4.2	28	4.1	10	4.3	5	3.1	11	3.6	101	41.2	4	·	·	·	1	2	·	2	7	13	9	3	—	·	·
X	5.5	4.6	10	3.6	3	3.7	4	2.8	9	3.3	26.5	4.6	15.5	3.2	15.5	2.8	4	3.5	23	7.5	18	·	·	4	·	·	·	·	7	18	4	·	—	·	·
XI	4	5.5	13.5	4.6	10	4.6	8	6.2	12.5	6.1	27.5	6.1	7.5	3.9	2	4.5	5	5.1	38	9.4	21	8	11	21	·	3	1	·	13	20	6	·	—	16	·
XII	·	·	·	·	·	·	7.5	6.7	23	7.0	40	7.0	14	4.8	3.5	3.4	5	6.1	25	5.6	14	4	6	24	·	7	3	·	19	20	8	·	—	9	·
Rok	101	4.5	120	4.4	56	4.0	80.5	4.7	136.5	5.2	271.5	5.2	168.5	4.0	95	3.7	66	4.6	532	41.2	4.IX	35	50	140	13	—	—	4	151	190	102	10	—	94	9

Międzyzdroje

$H_s = 10\ m$ $h_w = 14\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	◕	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊟	K (K)
I	4	1.2	5.5	1.7	16	1.5	22	2.5	15	3.7	10	2.8	9	2.2	6.5	2.7	5	2.3	38	7.5	25	·	2	21	·	·	·	1	16	14	13	·	7	6	—
II	24	3.6	9	2.4	5.5	1.5	7	2.1	4.5	2.4	10.5	3.1	8.5	5.7	13	3.5	2	3.2	42	12.0	28	1	7	24	·	3	1	·	11	21	15	1	1	14	—
III	12.5	2.8	13	2.3	9.5	2.2	14	1.8	11	1.9	7	1.8	8	2.6	8	2.4	10	2.0	44	19.7	3	2	6	22	·	1	·	3	8	10	9	1	4	15	—
IV	16	1.7	13	2.3	19.5	2.2	18	1.9	4.5	2.2	2.5	1.8	10.5	1.9	6	2.1	·	2.0	53	11.5	21	·	·	5	·	·	·	2	6	15	12	1	2	·	—
V	17	2.6	13	1.8	23.5	1.9	7.5	2.7	3.5	1.3	4.5	2.3	11	2.7	9	2.5	4	2.2	66	22.5	10	·	·	·	·	1	1	2	4	13	8	3	·	·	—
VI	11	2.1	14.5	2.5	17	1.9	8	1.9	4	2.2	3	2.0	15	4.1	13.5	3.0	4	2.5	31[2]	22.5	22	·	·	·	5	3	1	3	1	5[2]	3[2]	1[2]	·	·	—
VII	2.5	2.6	12	2.8	11	1.6	6.5	1.3	12	2.0	6	2.1	30.5	2.7	7.5	1.9	5	2.2	129	17.5	22	·	·	·	3	·	·	1	6	19	18	4	1	·	—
VIII	10	1.2	8.5	1.1	10.5	1.3	13	1.1	2.5	1.5	4	1.0	15	1.4	16.5	1.6	8	1.2	55	16.0	23	·	·	·	3	·	·	·	2	10	10	2	1	·	—
IX	3	1.0	2.5	1.0	18.5	3.0	22.5	2.1	10	1.9	2.5	2.4	18	2.7	7	2.6	6	2.2	93	19.9	10	·	·	·	1	·	·	2	5	13	11	4	·	·	—
X	5	2.0	8	1.5	18	2.0	8	1.8	15.5	2.3	7	1.9	11	3.2	11.5	2.6	9	2.0	16	6.2	29	·	·	1	·	·	·	1	1	5	4	·	6	·	—
XI	2.5	3.2	4	4.5	26.5	2.8	10	3.4	7.5	3.3	9	3.4	14.5	3.5	2	3.0	14	2.7	55	15.0	21	2	9	16	·	1	·	2	13	14	9	1	4	15	—
XII	2	2.5	·	·	11	2.3	20.5	3.0	15.5	3.4	19	3.4	18.5	3.1	5.5	2.8	1	3.0	65	17.9	9	·	1	18	·	·	·	·	18	20	11	3	4	9	—
Rok	109.5	2.2	103	2.0	186.5	2.0	157	2.1	110.5	2.3	85	2.3	169.5	3.0	106	2.6	68	2.3	687[2]	22.5	10.V, 22.VI	5	25	107	12	9	3	17	91	159	123	21	30	59	—

Świnoujście

$H_s = 6\ m$ $H_b = 5{,}4\ m$ $h_w =$ 9 m I–VIII, 11 m IX–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	◕	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊟	K (K)
I	5.5	3.2	7.5	5.8	9	1.9	11	2.1	24	3.9	22.5	3.5	9	3.1	4.5	2.6	·	3.4	35	6.4	21	·	2	18	·	2	·	1	17	16	12	·	4	7	·
II	9.5	10.6	12.5	6.5	7	3.3	3.5	1.9	4.5	2.4	12	3.4	15.5	3.1	18.5	5.4	1	4.9	30	7.0	28	1	7	24	·	10	2	·	11	20	8	·	1	26	·
III	6	5.5	9	5.2	4.5	3.0	9.5	2.1	16.5	1.9	11	2.0	17	2.7	7.5	3.3	12	2.6	17	4.6	4	1	5	21	·	2	·	6	10	13	5	·	6	16	·
IV	8	2.6	22	5.7	8.5	4.1	13.5	3.1	11.5	2.8	5.5	3.1	10.5	2.0	9.5	3.7	1	3.6	40	7.9	28	·	·	4	·	2	·	1	13	14	10	·	4	·	1
V	8	5.0	29.5	5.5	9	4.4	9	4.2	2.5	1.4	6	2.8	15	3.0	9	4.1	5	4.1	73	23.4	10	·	·	·	·	5	·	4	13	11	7	3	2	·	2
VI	9.5	3.6	18.5	5.5	7	2.1	6.5	2.1	5	2.6	9.5	3.7	20	3.2	10	3.6	4	3.5	22	8.5	18	·	·	·	4	·	·	2	7	5	4	·	·	·	3
VII	1.5	3.3	12	6.9	5	3.4	3	2.5	3.5	1.6	29.5	3.1	29.5	3.4	4	2.4	5	3.5	89	10.4	29	·	·	·	3	3	·	·	12	20	18	1	3	·	6
VIII	7.5	3.1	5.5	2.0	9	2.1	5.5	1.9	7	1.9	18.5	2.4	19	2.2	9	2.7	12	2.0	72	14.3	8	·	·	·	2	·	·	2	7	11	10	4	1	·	3
IX	3.5	2.1	4.5	5.2	2.5	4.4	17	2.9	14	2.1	26.5	2.7	14	3.0	4	2.8	4	2.7	71	16.4	7	·	·	·	·	·	·	5	8	15	11	3	·	·	2
X	4.5	4.8	4.5	4.0	14.5	2.1	3	2.0	16.5	2.0	20	3.3	19.5	2.5	4.5	3.4	6	2.6	15	7.6	29	·	·	·	·	·	·	2	3	5	3	·	9	·	·
XI	3.5	4.0	4	7.5	16	3.8	12.5	2.7	11.5	3.5	25.5	4.4	9	3.4	1	9.0	7	3.7	35	8.6	1	1	9	17	·	2	·	1	11	14	8	·	1	15	·
XII	2	3.0	1	4.0	2	3.8	14.5	3.8	15.5	3.9	32.5	4.1	22	3.4	3.5	4.0	-	3.8	62	14.2	9	·	1	19	·	1	·	·	22	20	14	2	2	10	·
Rok	69	4.2	130.5	5.3	94	3.2	108.5	2.6	132	2.5	219	3.2	200	2.9	85	3.9	57	3.4	561	23.4	10.V	3	24	103	9	27	2	24	134	164	110	13	33	74	17

Gryfice — φ = 53°55' — λ = 15°13' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{s.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.5	−1.7	8.0	17	−9.3	31	−0.3	1.5	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	6.1	7.6
II	–	–	–	–	0.8	−4.9	4.1	13, 14	−15.1	17	−3.0	−0.3	−2.2	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	6.9	7.7
III	–	–	–	–	4.7	−3.5	13.3	29	−17.7	8	−2.2	3.6	0.0	0.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.4	4.8	6.0
IV	–	–	–	–	11.2	2.5	17.0	6	−2.2	5	4.2	9.9	5.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	6.2	7.1
V	–	–	–	–	14.4	5.3	20.6	17	0.2	3	8.2	13.1	8.3	9.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.1	7.3	6.4
VI	–	–	–	–	21.0	10.5	29.3	26	3.8	4	14.2	19.5	14.0	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.9	6.5	5.9
VII	–	–	–	–	19.2	10.8	27.4	14	7.3	4, 7	13.3	17.7	13.4	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	7.8	7.3
VIII	–	–	–	–	20.1	10.7	27.6	20	6.7	31	12.7	19.0	13.3	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.3	5.3	5.7
IX	–	–	–	–	19.0	9.8	25.8	3	5.6	30	11.4	18.2	12.6	13.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.2	6.6	6.7
X	–	–	–	–	13.1	3.8	21.8	1	−1.9	22	6.1	12.2	6.9	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.7	5.5	6.6
XI	–	–	–	–	2.6	−2.6	11.8	1	−12.9	23	−1.1	1.6	−0.7	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.5	6.7	7.7
XII	–	–	–	–	2.8	−1.1	11.2	19	−6.1	16, 17	0.6	1.5	0.6	0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.1	9.0	8.3	8.6
Rok	–	–	–	–	11.0	3.3	29.3	26.VI	−17.7	8. III	5.3	9.8	6.0	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	6.5	7.0

Morąg — φ = 53°55' — λ = 19°56'

I	–	–	–	–	0.7	−4.4	4.4	1, 18	−19.2	11	−1.7	−0.4	−1.8	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.5	6.7	7.7
II	–	–	–	–	−1.9	−10.3	1.9	12	−24.7	6	−6.8	−3.4	−6.0	−5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.8	6.8	7.3
III	–	–	–	–	3.6	−5.9	10.4	29	−26.2	8	−4.2	2.2	−1.2	−1.1	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.9	5.5	5.7
IV	–	–	–	–	9.2	1.7	15.3	28	−2.9	3, 6	3.3	7.7	5.4	5.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.5	6.7	7.0
V	–	–	–	–	13.3	4.0	18.8	18	−3.1	4	7.4	12.0	8.2	9.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.5	5.4	5.8
VI	–	–	–	–	20.4	10.2	28.8	26	4.6	8	14.1	18.9	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.7	4.4	5.1
VII	–	–	–	–	20.1	10.9	29.3	15	5.2	2	13.9	18.2	14.5	15.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.7	6.5	6.9
VIII	–	–	–	–	20.5	10.0	27.6	6	4.7	16, 31	12.6	18.8	13.9	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	4.6	6.1
IX	–	–	–	–	19.5	9.2	27.4	3	4.2	16	11.2	18.0	13.3	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.9	2.6	4.7
X	–	–	–	–	11.6	3.7	19.6	1	−3.3	21	5.3	10.6	7.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.3	5.0	6.5
XI	–	–	–	–	0.7	−4.7	10.8	2	−22.2	24	−2.5	−0.4	−1.8	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.5	7.9	8.6
XII	–	–	–	–	1.4	−2.7	8.9	19, 20	−16.5	17	−0.9	0.2	−0.4	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	7.4	8.0
Rok	–	–	–	–	9.9	1.8	29.3	15.VII	−26.2	8. III	4.3	8.5	5.5	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	5.8	6.6

Wirty — φ = 53°44' — λ = 18°23'

I	–	–	–	–	1.0	−3.9	5.1	17	−16.6	11	−1.8	−0.3	−1.5	−1.3	5.0	5.4	5.0	5.1	92	89	90	90	0.4	0.7	0.6	0.6	8.3	7.4	6.7	7.5
II	–	–	–	–	−1.2	−8.6	2.8	11	−17.6	6	−5.5	−2.5	−4.8	−4.4	3.8	4.5	4.0	4.1	91	86	89	89	0.4	0.7	0.4	0.5	8.1	7.0	6.7	7.3
III	–	–	–	–	4.2	−5.0	12.3	29	−25.2	8	−3.0	2.4	−0.6	−0.4	4.7	5.6	5.3	5.2	89	76	86	84	0.6	2.0	0.8	1.1	5.7	5.9	6.3	6.0
IV	–	–	–	–	9.4	1.9	14.3	6, 22, 30	−2.9	3, 6	3.6	7.9	5.0	5.4	7.0	7.6	7.4	7.3	87	71	84	81	1.0	3.3	1.4	1.9	7.4	7.9	5.8	7.0
V	–	–	–	–	13.6	4.1	19.8	17	−1.9	3	7.7	11.8	7.8	8.8	8.7	8.3	8.8	8.6	81	61	82	75	2.0	5.9	2.0	3.3	5.8	5.9	5.0	5.6
VI	–	–	–	–	20.4	9.7	29.7	26	4.8	4	14.3	16.9	13.5	15.0	12.9	12.8	12.5	12.7	79	60	80	73	3.7	9.7	3.1	5.5	5.2	5.3	3.8	4.8
VII	–	–	–	–	19.5	10.6	30.2	14	5.6	2	13.7	18.0	13.6	14.7	13.7	13.1	13.8	13.5	86	64	88	79	2.2	8.1	2.0	4.1	5.8	7.1	6.7	6.5
VIII	–	–	–	–	20.3	9.6	28.2	6, 22	5.3	17	13.4	18.7	13.2	14.6	13.9	13.7	13.5	13.7	90	65	89	81	1.7	8.6	2.0	4.1	5.7	6.5	3.8	5.3
IX	–	–	–	–	19.3	9.0	26.7	3	2.6	16	11.0	17.8	12.7	13.6	12.7	14.0	13.7	13.5	95	69	92	85	0.6	6.9	1.2	2.9	5.7	5.7	4.9	5.4
X	–	–	–	–	12.4	3.8	18.5	1	−1.4	22	5.5	11.5	6.4	7.4	8.9	10.5	9.1	9.5	96	77	93	89	0.4	3.3	0.6	1.4	6.7	6.1	3.9	5.6
XI	–	–	–	–	1.0	−4.5	10.8	2	−16.1	24	−2.6	−0.2	−1.7	−1.6	5.1	5.5	5.4	5.3	91	85	91	89	0.5	1.0	0.5	0.7	9.6	7.1	7.0	7.9
XII	–	–	–	–	1.8	−2.8	10.3	19	−17.1	17	−0.9	0.6	−0.2	−0.2	5.3	5.5	5.6	5.5	90	85	91	89	0.5	1.0	0.6	0.7	9.2	9.1	8.6	9.0
Rok	–	–	–	–	10.1	2.0	30.2	14.VII	−25.2	8. III	4.6	8.7	5.3	6.0	8.5	8.9	8.7	8.7	89	74	88	84	1.2	4.3	1.3	2.3	6.9	6.8	5.8	6.5

Jazy — φ = 53°53' — λ = 23°22'

I	–	–	–	–	−0.8	−5.7	3.2	18	−14.5	10, 11	−3.2	−1.9	−3.3	−2.9	4.6	4.7	4.5	4.6	90	86	90	89	0.4	0.7	0.5	0.5	9.1	8.4	8.2	8.6
II	–	–	–	–	−3.5	−12.1	1.8	17	−28.5	6	−8.8	−4.7	−7.7	−7.2	3.3	3.8	3.4	3.5	93	84	93	90	0.2	0.7	0.3	0.4	9.1	7.7	7.7	8.2
III	–	–	–	–	2.8	−6.4	8.4	16, 28	−26.3	1	−4.1	2.3	−2.3	−1.6	4.5	4.9	4.7	4.7	91	67	86	81	0.5	2.6	0.8	1.3	7.4	6.3	7.3	7.0
IV	–	–	–	–	9.6	0.7	17.4	27	−8.6	3	3.6	8.4	4.6	5.3	6.4	6.3	6.2	6.3	79	57	72	69	1.8	5.0	2.5	3.1	6.4	6.3	7.5	6.7
V	–	–	–	–	13.7	2.5	20.6	18	−6.4	4	7.7	12.0	6.8	8.3	8.7	8.0	8.6	8.4	81	57	84	74	2.0	6.3	1.6	3.3	5.6	7.0	7.0	6.5
VI	–	–	–	–	20.4	9.0	27.5	26	1.7	8	15.0	18.9	13.8	15.4	13.8	12.3	13.2	13.1	81	57	84	74	3.3	10.0	2.8	5.4	5.3	5.4	6.1	5.6
VII	–	–	–	–	21.1	9.6	30.0	16	4.0	12	15.2	19.4	14.4	15.8	14.6	13.4	13.8	13.9	84	60	84	76	2.9	9.7	2.8	5.1	4.5	5.9	6.0	5.5
VIII	–	–	–	–	20.8	9.5	29.2	25	4.0	2, 31	13.5	19.2	13.6	15.0	13.5	12.8	14.0	13.4	88	59	89	79	2.1	10.2	2.0	4.8	5.2	5.9	4.5	5.2
IX	–	–	–	–	20.8	7.9	28.1	4	1.4	24	10.7	19.4	12.3	13.7	12.5	12.8	13.0	12.8	96	57	90	81	0.6	10.3	1.7	4.2	4.9	4.4	3.2	4.2
X	–	–	–	–	11.3	2.6	18.1	1	−6.0	21	5.1	10.3	6.6	7.2	8.5	9.1	8.8	8.8	95	73	90	86	0.5	3.7	1.1	1.8	8.4	7.6	7.0	7.7
XI	–	–	–	–	0.0	−5.6	11.3	2	−18.7	24	−3.2	−1.0	−2.6	−2.4	5.1	5.0	5.0	5.0	93	83	92	89	0.4	1.2	0.4	0.7	8.8	8.7	8.5	8.7
XII	–	–	–	–	1.1	−3.8	7.8	20	−13.9	17	−1.5	−0.1	−0.9	−0.8	5.3	5.6	5.3	5.4	95	91	92	93	0.3	0.6	0.5	0.5	8.2	8.7	8.7	8.5
Rok	–	–	–	–	9.8	0.7	30.0	16.VII	−28.5	6. II	4.2	8.5	4.6	5.5	8.4	8.2	8.4	8.3	89	69	87	82	1.2	5.1	1.4	2.6	6.9	6.9	6.8	6.9

Gryfice $H_s = 40\ m$ $h_w = 14\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V>10	V>15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	1.0	1	1.0	7	2.6	5	2.0	3	3.3	22	2.8	21	3.7	3	2.3	29	2.0	40	8.1	8	·	3	23	·	2	1	2	15	17	13	·	4	7	·
II	10	6.3	8.5	7.2	8	3.2	·	·	0.5	3.0	4.5	2.8	20	4.5	14.5	6.7	18	4.2	42	8.8	14	3	8	24	·	9	3	·	15	21	12	·	4	21	·
III	1	2.5	4	7.0	11	3.7	2	1.5	2	1.0	9	1.9	14.5	3.7	8.5	5.5	41	2.1	46	24.3	3	3	6	22	·	3	·	4	9	15	8	1	5	18	·
IV	3.5	4.0	7	4.2	14	4.8	4.5	2.1	6.5	1.9	7	3.0	12	3.7	10.5	3.8	25	2.7	39	7.1	23	·	·	3	·	1	·	1	12	16	10	·	3	·	1
V	6.5	3.2	13.5	3.3	12.5	3.2	4.5	2.3	3	4.3	·	·	18.5	5.7	8.5	5.2	26	3.0	75	20.7	9	·	·	·	·	3	2	3	14	13	10	2	1	·	2
VI	2	2.5	8	2.7	6.5	3.5	4.5	3.0	1	2.0	6	3.5	17.5	5.8	15.5	3.8	29	2.7	31	8.9	22	·	·	·	4	2	1	5	12	8	6	·	·	·	4
VII	·	·	5	2.8	8	3.2	1	2.0	·	·	9	2.7	34	5.5	6	4.9	30	3.0	128	14.0	22	·	·	·	5	2	·	3	16	21	19	4	2	·	7
VIII	5	3.4	6.5	2.4	·	·	1	1.0	·	·	3.5	2.4	20	3.4	14	3.1	43	1.6	64	21.7	23	·	·	·	3	·	·	2	8	12	8	2	5	·	4
IX	·	·	·	·	4.5	4.2	3	5.0	2.5	4.0	10.5	2.4	26.5	3.7	7	8.0	36	2.5	122	31.2	9	·	·	·	1	3	·	1	11	13	12	5	4	·	6
X	3	2.7	3.5	2.6	1	5.0	·	·	·	·	7	3.7	28	3.4	8.5	4.1	42	1.9	15	6.4	29	·	·	5	·	3	·	1	7	6	3	·	10	·	1
XI	2	8.5	·	·	21.5	3.0	7.5	2.7	2	3.6	6.5	3.9	30	5.2	2.5	7.4	18	3.4	40	10.0	21	5	11	19	·	7	1	2	16	19	8	1	5	10	·
XII	2	1.0	·	·	2	1.8	3	2.2	5	3.7	20	4.4	36	5.3	4	5.6	21	3.6	78	19.9	9	·	4	22	·	3	1	·	22	23	16	2	5	7	·
Rok	37	2.9	57	2.8	96	3.2	36	2.0	25.5	2.2	105	2.8	278	4.5	102.5	5.0	356	2.7	720	31.2	9. IX	11	32	118	13	38	9	24	157	184	125	17	48	63	25

Morąg $H_s = 113\ m$ $h_w = 12{,}5\ m$

I	2	2.0	3.5	2.4	10.5	2.0	11	2.2	13	3.6	20	3.3	7	3.2	7	2.6	19	2.3	42	16.8	8	3	10	28	·	2	1	·	15	20	10	1	3	22	·
II	8.5	1.9	8	2.2	1.5	3.7	2	3.5	7	2.4	14.5	2.9	18	3.3	9.5	2.9	15	2.3	47	8.5	7	14	19	27	·	2	2	1	13	23	16	·	2	28	·
III	8.5	2.6	6	2.2	3	3.3	9	2.4	12.5	1.9	14	1.7	7.5	2.6	7.5	3.3	25	1.7	35	11.7	3	7	9	24	·	2	2	7	11	14	8	1	9	20	·
IV	7	2.1	8.5	3.6	17.5	3.9	19.5	3.5	7.5	2.6	7	2.0	7	2.0	10	2.0	6	2.8	41	7.1	21	·	·	10	·	2	·	3	13	16	12	·	2	·	1
V	15	2.8	13.5	3.2	12.5	4.2	5	3.5	5	1.4	8	2.8	7.5	3.3	12.5	3.2	14	2.7	42	12.1	9	·	·	3	·	·	·	5	11	13	9	1	1	·	·
VI	9.5	2.8	11	2.5	10	3.1	5.5	4.5	5.5	4.5	11	3.6	17.5	2.9	15	2.4	5	2.9	56	12.7	19	·	·	·	4	1	1	4	7	15	10	2	·	·	2
VII	3.5	3.0	6.5	2.5	5.5	1.5	4.5	2.2	12	2.7	30	3.5	16.5	3.4	2.5	2.6	12	2.6	84	11.5	8	·	·	·	2	·	·	2	17	23	20	2	1	·	5
VIII	3.5	1.3	1	1.0	1	3.5	7	2.9	6.5	3.5	11	3.1	13.5	2.2	18.5	1.9	31	1.6	106	30.0	27	·	·	·	7	1	1	3	12	18	11	4	1	·	3
IX	·	·	3	1.8	9.5	2.3	10.5	3.0	15.5	3.7	18	4.0	10	3.0	3.5	2.4	20	2.5	90	30.8	4	·	·	·	1	·	·	7	4	13	10	2	2	·	1
X	2	2.8	1.5	2.3	2.5	1.8	4	1.2	5.5	3.5	19.5	3.2	14	2.6	11	2.1	33	1.7	26	6.0	16	·	·	5	·	·	·	3	10	10	8	·	6	·	·
XI	7.5	3.3	16	2.8	8	2.8	10.5	6.0	7	3.9	14.5	3.7	12.5	4.6	6	3.2	8	3.5	50	11.7	1	8	14	22	·	4	1	1	21	20	11	2	3	16	·
XII	·	·	·	·	3	3.0	10	4.4	19	4.2	31.5	4.3	11.5	3.3	2	4.5	16	3.4	54	20.1	18	4	9	26	·	3	2	1	20	20	9	1	2	20	·
Rok	67	2.0	78.5	2.2	84.5	2.9	98.5	3.3	116	3.2	199	3.2	142.5	3.0	105	2.8	204	2.5	673	30.8	4. IX	36	61	145	14	17	10	37	154	205	134	16	32	106	12

Wirty $H_s = 121\ m$ $h_w = 13\ m$

I	2	3.5	4	1.5	7	1.3	13	1.6	19	2.1	18	1.8	7	2.3	5	2.0	18	1.6	27	5.7	30	2	12	28	·	·	·	2	17	14	9	·	—	21	·
II	12	2.6	7	1.6	3	1.0	1	1.0	4	1.5	10	1.7	31	2.5	6	3.5	10	2.0	40	15.5	8	9	17	27	·	·	·	1	15	17	9	1	—	28	·
III	7	1.9	13	2.8	1	5.0	7	2.1	7	1.3	22	1.4	17	2.1	2	2.5	17	1.6	28	9.2	3	4	9	24	·	·	·	7	12	10	6	·	—	23	·
IV	5	1.6	10	2.3	19	2.5	16	1.9	3	1.0	6	2.0	12	1.8	3	2.0	16	1.7	48	10.4	25	·	·	8	·	·	·	3	12	14	12	1	—	·	1
V	12	2.0	18	1.8	9	2.2	7	2.7	2	2.0	11	2.3	8	1.8	6	2.2	20	1.6	39	10.2	9	·	·	5	·	·	·	8	9	11	7	1	—	·	·
VI	6	1.1	10	2.1	9.5	2.6	4.5	2.3	5.5	2.2	13.5	1.7	25	2.6	2	2.5	14	1.9	64	22.7	1	·	·	·	5	·	·	8	5	8	7	2	—	·	1
VII	9	2.4	2	1.2	3.5	1.6	1.5	2.3	14	2.2	29	2.2	18	3.0	·	·	16	2.0	107	17.6	12	·	·	·	2	·	·	3	10	20	16	4	—	·	7
VIII	2	1.0	2	1.0	1.5	2.7	4	1.9	7.5	1.8	13.5	1.7	18.5	1.8	4	1.8	40	1.0	54	21.5	24	·	·	·	7	·	·	3	7	13	9	1	—	·	2
IX	2	2.5	3	2.7	8	2.2	3	1.7	15	1.4	20	2.2	5	1.9	2	3.0	32	1.3	67	16.8	10	·	·	·	1	·	·	8	10	13	11	2	—	·	1
X	4	2.2	2	1.0	3.5	1.4	1.5	1.3	11	1.7	20	2.4	12	1.9	6	2.5	33	1.3	11	2.2	30,31	·	·	5	·	·	·	5	7	13	6	·	—	·	·
XI	3.5	2.4	8	1.8	14.5	2.1	7.5	2.1	10	1.8	24	2.8	5.5	2.4	1	2.0	16	1.9	27	14.8	21	8	13	22	·	·	·	·	16	21	6	1	—	15	·
XII	·	·	·	·	1	2.0	14	2.5	16.5	3.4	36.5	2.7	9	1.7	1	1.0	15	2.2	26	7.3	5	3	7	24	·	·	·	·	22	17	10	·	—	17	·
Rok	64.5	1.9	79	1.6	80.5	2.2	80	2.0	114.5	1.9	223.5	2.1	168	2.2	38	2.1	247	1.7	538	22.7	1.VI	26	58	143	15	·	·	48	142	171	108	13	—	104	12

Jazy $H_s = 120\ m$ $h_w = 15\ m$

I	1.5	4.7	2	2.8	6	3.0	14	3.5	11.5	3.3	12.5	3.1	4	7.5	5.5	7.9	36	2.5	—	—	—	5	15	29	·	4	·	·	23	—	—	—	5	31	—
II	11.5	3.6	6.5	2.6	·	·	·	·	3.5	3.6	15.5	3.4	7.5	3.9	9.5	3.9	30	2.3	—	—	—	14	23	28	·	·	·	·	15	—	—	—	·	28	—
III	3	4.7	2	2.5	·	·	6.5	2.8	10	2.6	9.5	2.9	9.5	3.6	3.5	4.0	49	1.5	48	14.2	3	5	8	25	·	·	·	2	12	15	11	1	4	31	—
IV	2.5	1.8	11.5	3.6	10	4.2	17.5	3.7	5.5	2.4	2.5	2.2	0.5	2.0	7	3.1	33	2.2	25	15.8	23	·	·	13	·	·	·	3	12	7	3	1	·	·	—
V	4	3.4	6.5	2.8	3.5	4.0	4	3.5	2.5	3.6	4	3.4	4	4.0	5.5	3.9	59	1.3	105	31.3	19	·	·	8	·	·	·	2	11	12	12	3	2	·	—
VI	3.5	3.3	3	2.5	4.5	3.4	6	3.6	6.5	3.8	7.5	4.0	9.5	3.7	7.5	2.8	42	1.9	70	18.6	13	·	·	·	2	·	·	3	7	11	9	2	1	·	—
VII	2	4.2	3	3.0	2	1.8	3.5	2.4	5.5	2.5	20	3.6	9.5	3.6	1.5	4.0	46	1.7	74	24.0	31	·	·	·	4	·	·	2	5	16	10	3	·	·	—
VIII	2.5	2.6	0.5	2.0	1	2.0	5.5	3.0	4	2.9	8.5	2.3	7.5	1.9	9.5	2.3	54	1.0	38	16.7	2	·	·	·	7	·	·	8	9	10	9	1	2	·	—
IX	·	·	0.5	2.0	3	2.5	10.5	2.7	10	2.8	7	3.3	10.5	3.1	1.5	2.0	47	1.4	27	7.0	29	·	·	·	2	·	·	9	2	9	7	·	2	·	—
X	2.5	3.2	1.5	2.7	4	3.1	1.5	4.0	6	2.8	9.5	3.2	19.5	3.6	8.5	4.1	40	2.0	18	7.8	16	·	·	6	·	·	·	·	18	7	5	·	2	·	—
XI	1	2.0	3	1.8	0.5	2.0	10	4.0	9	4.6	9.5	4.6	9.5	3.8	5.5	3.0	42	2.1	56	12.9	21	6	16	22	·	·	·	·	20	16	9	2	·	16	—
XII	0.5	3.0	·	·	6.5	3.5	8.5	4.6	18	4.9	17.5	4.2	9.5	3.4	2.5	3.0	30	2.9	42	14.2	19	3	10	29	·	1	·	1	20	18	8	1	·	31	—
Rok	34.5	3.0	40	2.4	41	2.5	87.5	3.2	92	3.3	123.5	3.4	101	3.7	67.5	3.7	508	1.9	—	31.3	19.V	33	72	160	15	5	·	30	154	—	—	—	18	137	—

Biskupiec — φ = 53°52′ — λ = 20°57′ — 1965

Miesiąc	Ciśnienie p: P_m	Max	Min	$P_{o.m}$	Temperatura T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	—	—	—	—	−0.2	−4.8	3.7	1	−15.1	11	−2.6	−1.1	−2.5	−2.2	4.6	4.9	4.6	4.7	86	84	87	86	0.7	0.9	0.6	0.7	—	—	—	—
II	—	—	—	—	−2.7	−11.1	1.6	13	−26.9	6	−7.7	−4.0	−6.5	−6.2	3.1	3.7	3.4	3.4	83	77	84	81	0.5	1.0	0.6	0.7	—	—	—	—
III	—	—	—	—	3.1	−5.7	9.1	28	−24.1	8	−4.0	2.1	−1.6	−1.3	4.4	5.2	4.9	4.8	86	72	84	81	0.6	2.2	0.8	1.2	—	—	—	—
IV	—	—	—	—	9.6	1.3	16.2	28	−4.5	3	3.3	8.3	5.0	5.4	6.6	6.6	6.8	6.7	83	61	78	74	1.3	4.5	2.1	2.6	—	—	—	—
V	—	—	—	—	13.4	3.3	18.6	18	−2.3	3	7.4	12.4	7.5	8.7	8.5	8.0	8.4	8.3	80	55	79	71	2.0	6.6	2.2	3.6	—	—	—	—
VI	—	—	—	—	20.7	9.8	28.6	26	2.4	8	14.1	18.8	14.1	15.3	12.8	12.0	12.8	12.5	79	56	79	71	3.4	10.2	3.7	5.8	—	—	—	—
VII	—	—	—	—	20.2	10.3	30.0	15	3.9	5	14.6	18.7	14.0	15.3	13.7	13.2	13.7	13.5	82	62	85	76	3.1	8.9	2.5	4.8	—	—	—	—
VIII	—	—	—	—	20.1	9.5	28.1	22	4.0	17	12.8	19.0	13.5	14.7	13.3	14.1	13.7	13.7	90	65	87	81	1.7	8.7	2.3	4.2	—	—	—	—
IX	—	—	—	—	19.8	8.9	26.9	3	3.8	1	11.3	18.8	12.8	13.9	12.4	13.8	13.3	13.2	92	64	88	81	1.1	8.4	1.9	3.8	—	—	—	—
X	—	—	—	—	11.5	3.6	19.3	1	−4.4	21	5.4	10.9	7.1	7.6	8.5	9.7	9.2	9.1	92	73	89	85	0.7	3.7	1.1	1.8	—	—	—	—
XI	—	—	—	—	0.2	−5.1	10.0	2	−21.7	24	−3.1	−1.0	−2.2	−2.1	4.6	5.0	5.0	4.9	85	81	86	84	0.8	1.2	0.7	0.9	—	—	—	—
XII	—	—	—	—	0.8	−3.4	8.2	19, 20	−16.2	17	−1.1	−0.2	−0.9	−0.8	5.0	5.2	5.2	5.1	86	84	87	86	0.8	0.9	0.7	0.8	—	—	—	—
Rok	—	—	—	—	9.7	1.4	30.0	15. VII	−26.9	6. II	4.2	8.6	5.0	5.7	8.1	8.4	8.4	8.3	85	70	84	80	1.4	4.8	1.6	2.6	—	—	—	—

Augustów — φ = 53°50′ — λ = 22°58′

I	—	—	—	—	−0.6	−5.2	2.7	9, 18	−14.2	10, 11	−3.4	−2.0	−3.3	−3.0	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.5	8.2	8.5
II	—	—	—	—	−3.7	−13.1	1.9	17	−28.8	6	−9.6	−5.4	−8.0	−7.8	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.6	6.1	7.1
III	—	—	—	—	2.0	−6.0	7.7	28	−25.5	9	−4.3	0.9	−1.9	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.1	5.8	5.9	6.3
IV	—	—	—	—	9.4	2.8	16.2	27, 28	−4.4	3	3.4	8.2	4.5	5.2	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.5	6.4	7.2
V	—	—	—	—	13.3	3.4	20.2	18	−3.5	4	7.3	12.1	7.7	8.7	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.4	6.0	6.6
VI	—	—	—	—	19.8	9.9	26.2	26	2.1	15	14.0	18.8	14.2	15.3	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.0	6.4	6.6
VII	—	—	—	—	20.3	9.9	29.8	16	4.1	11	14.2	18.8	14.1	15.3	—	—	—	—	—	—	—	—	—	—	—	—	5.6	7.2	6.8	6.5
VIII	—	—	—	—	20.4	—	28.1	25	—	—	13.2	19.2	13.9	15.0	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.6	5.9	6.2
IX	—	—	—	—	20.2	—	27.1	4	—	—	11.2	19.0	12.6	13.8	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.5	4.4	5.8
X	—	—	—	—	11.2	2.6	18.2	1	−4.9	21	5.5	10.4	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.6	5.3	7.1
XI	—	—	—	—	−0.4	−5.6	10.7	2	−19.5	24	−3.4	−1.1	−3.2	−2.7	—	—	—	—	—	—	—	—	—	—	—	—	9.4	9.3	8.5	9.1
XII	—	—	—	—	0.5	−4.1	5.7	20	−15.0	15, 16	−1.7	−0.5	−1.5	−1.3	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.8	8.8	8.7
Rok	—	—	—	—	9.4	—	29.8	16. VII	−28.8	6. II	3.9	8.2	4.6	5.3	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.5	6.6	7.2

Mikołajki — φ = 53°47′ — λ = 21°35′

I	994.6	1011.1	974.5	1011.1	−0.1	−4.3	3.9	18	−13.4	11	−2.5	−1.2	−2.3	−2.1	4.9	5.0	4.8	4.9	91	87	91	90	0.4	0.7	0.5	0.5	8.6	7.7	7.0	7.8
II	996.7	1018.1	972.0	1013.6	−2.6	−10.0	1.5	13	−27.2	6	−7.6	−4.5	−6.0	−6.0	3.4	3.6	3.7	3.6	89	80	90	86	0.4	0.9	0.4	0.6	8.2	7.1	7.1	7.5
III	999.5	1015.9	972.8	1016.0	3.2	−5.4	8.8	28	−23.7	8	−3.8	1.9	−1.0	−1.0	4.6	5.3	5.1	5.0	91	74	86	84	0.5	2.0	0.9	1.1	6.5	5.5	6.0	6.0
IV	995.9	1012.1	977.2	1012.1	9.3	1.8	15.4	28	−3.8	3	3.1	7.8	4.8	5.1	6.8	7.1	7.2	7.0	88	66	82	79	1.0	3.8	1.6	2.1	7.8	8.1	6.9	7.6
V	997.8	1013.2	977.0	1013.7	13.2	4.6	19.8	18	−1.7	4	7.3	11.9	8.4	9.0	8.7	8.2	8.7	8.5	83	58	77	73	1.7	5.9	2.5	3.4	6.5	7.2	5.6	6.4
VI	997.6	1004.4	989.3	1013.2	19.9	11.0	27.4	26	3.9	8	14.1	18.2	14.9	15.5	13.2	12.6	13.1	13.0	82	62	77	74	3.0	8.8	4.2	5.3	5.5	6.9	6.0	6.1
VII	994.8	1007.3	979.1	1010.3	20.1	11.6	28.9	15	6.8	5	14.5	18.6	14.8	15.7	13.9	12.9	14.1	13.6	83	60	83	75	2.8	9.1	3.0	5.0	5.8	7.7	6.2	6.6
VIII	998.5	1006.8	989.1	1014.2	19.8	11.2	26.8	25	7.9	31	13.0	18.2	14.2	14.9	13.5	13.6	14.1	13.7	90	66	86	81	2.0	8.1	2.5	4.2	6.1	6.4	4.6	5.7
IX	998.4	1015.3	986.6	1014.1	19.5	10.2	26.5	3	6.5	21	11.6	18.1	13.5	14.2	12.9	13.7	13.7	13.4	94	66	87	82	0.9	7.4	2.0	3.4	5.7	6.1	3.4	5.1
X	1005.0	1020.8	988.6	1021.1	11.5	4.8	19.1	1	−1.5	21	6.1	10.7	7.6	8.0	8.9	9.6	9.3	9.3	93	74	88	85	0.7	3.5	1.3	1.8	7.0	7.5	6.1	6.9
XI	995.0	1012.5	967.3	1011.5	0.5	−4.1	10.3	2	−18.2	24	−2.7	−0.7	−1.7	−1.7	5.1	5.2	5.2	5.2	91	84	90	88	0.5	1.2	0.6	0.8	8.7	8.5	8.4	8.5
XII	987.5	1004.7	964.5	1003.8	1.4	−2.6	8.4	20	−16.2	17	−0.7	0.0	−0.6	−0.5	5.3	5.4	5.4	5.4	91	86	90	89	0.6	0.9	0.6	0.7	9.0	8.7	7.8	8.5
Rok	996.8	1020.8	964.5	1012.9	9.6	2.4	28.9	15. VII	−27.2	6. II	4.4	8.2	5.6	6.0	8.4	8.5	8.7	8.5	89	72	86	82	1.2	4.4	1.7	2.4	7.1	7.3	6.3	6.9

Resko — φ = 53°46′ — λ = 15°25′

I	1003.2	1020.5	978.9	1010.2	2.5	−1.7	7.4	17	−9.1	31	−0.2	1.5	0.1	0.4	5.5	5.7	5.7	5.6	91	84	91	89	0.6	1.1	0.6	0.8	8.1	8.2	6.8	7.7
II	1010.4	1028.2	981.3	1017.6	0.3	−5.8	4.0	11	−17.5	17	−3.9	−0.5	−2.7	−2.4	4.2	4.8	4.5	4.5	88	80	87	85	0.6	1.2	0.6	0.8	8.9	8.1	7.3	8.1
III	1009.6	1024.9	987.4	1016.7	4.9	−3.6	14.2	29	−18.0	8	−2.4	3.6	0.2	0.4	4.9	5.8	5.6	5.4	89	72	86	82	0.6	2.4	0.9	1.3	6.7	6.3	4.2	5.7
IV	1004.4	1025.9	982.5	1011.3	11.3	2.4	16.3	30	−3.5	5	4.2	9.8	5.9	6.4	7.5	7.4	7.6	7.5	89	62	82	78	0.9	5.0	1.8	2.6	7.6	8.2	6.1	7.3
V	1007.5	1022.3	990.9	1014.4	14.5	5.1	19.8	28	−1.5	3	7.9	13.3	9.0	9.8	9.1	9.0	9.5	9.2	85	60	82	76	1.6	6.5	2.2	3.4	6.4	6.7	6.5	6.5
VI	1007.5	1017.9	992.5	1014.2	21.0	10.0	28.8	26	2.5	4	14.1	19.4	14.6	15.7	12.8	12.8	13.1	12.9	79	57	79	72	3.5	10.4	3.8	5.9	6.1	7.4	5.0	6.2
VII	1003.8	1015.1	986.8	1010.5	19.4	10.5	29.3	14	6.7	5	13.3	17.8	13.9	14.7	13.5	13.6	14.0	13.7	88	67	87	81	1.9	7.4	2.0	3.8	7.2	7.9	6.6	7.2
VIII	1008.5	1017.5	995.3	1015.3	20.3	9.7	28.0	22	4.8	16	12.5	18.9	13.4	14.6	13.6	14.2	13.8	13.9	94	65	90	83	1.0	8.0	1.8	3.6	6.1	7.0	4.8	6.0
IX	1006.2	1027.0	991.5	1013.0	19.1	10.0	25.5	3	5.6	23	11.3	18.1	12.8	13.8	12.5	13.8	13.3	13.2	93	67	90	83	1.1	7.4	1.6	3.4	6.6	6.2	5.4	6.1
X	1016.9	1031.2	999.3	1022.9	13.4	3.3	21.8	1	−3.6	12	5.3	12.3	6.3	7.6	8.8	10.5	9.0	9.4	96	73	93	87	0.4	4.1	0.8	1.8	7.1	6.6	2.8	5.5
XI	1003.7	1023.5	972.6	1010.7	2.5	−3.1	11.8	1, 2	−12.3	18	−1.3	1.6	−0.8	−0.3	5.4	5.8	5.5	5.6	90	78	88	85	0.6	1.5	0.7	0.9	8.0	7.4	5.6	7.0
XII	995.5	1017.0	965.7	1002.5	2.8	−1.0	11.2	19	−7.0	16, 17	0.5	1.4	0.8	0.9	5.8	6.1	6.0	6.0	90	87	90	89	0.7	0.9	0.7	0.8	9.0	8.9	7.6	8.5
Rok	1006.4	1031.2	965.7	1013.4	11.0	3.0	29.3	14. VII	−18.0	8. III	5.1	9.8	6.1	6.8	8.6	9.1	9.0	8.9	89	71	87	82	1.1	4.7	1.5	2.4	7.3	7.4	5.7	6.9

Biskupiec $H_s = 160 m$ $h_w = 14 m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	OPAD R			LICZBA DNI (n) Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◔	◕	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	3	1.3	5	2.0	7	2.4	18	3.4	9	3.4	27	3.7	11	3.2	12	3.3	1	3.2	32	7.6	8	3	13	29	·	1	·	—	—	15	11	·	8	18	·
II	12	2.6	12	2.9	2	1.5	3	1.7	1	1.0	15	4.4	16	3.6	22	2.5	1	3.0	44	6.1	7	13	23	27	·	·	·	—	—	18	15	·	2	28	·
III	3	1.7	13	1.8	5	2.4	9	3.0	8	2.5	17	2.6	19	2.6	8	4.1	11	2.3	25	8.9	3	6	9	24	·	·	·	—	—	10	8	·	8	21	·
IV	7	3.7	17	2.9	15	4.6	21	4.0	6	2.3	8	2.8	3	1.7	10	3.0	3	3.3	34	9.7	21	·	·	11	·	·	·	—	—	10	6	·	5	·	1
V	10	3.4	13	2.2	14	4.1	10	2.5	1	2.0	9	3.8	6	2.8	26	2.8	4	2.9	56	12.1	19	·	·	3	·	·	·	—	—	11	9	2	4	·	·
VI	8	2.0	7	2.7	12	4.2	3	4.0	6	4.3	11	3.6	12	3.7	28	3.0	3	3.2	61	13.7	19	·	·	·	3	·	·	—	—	12	11	3	·	·	3
VII	1	1.0	9	2.2	4	3.0	5	2.8	3	2.0	32	4.2	24	3.4	9	1.6	6	3.0	82	14.2	23	·	·	·	2	·	·	—	—	18	14	3	2	·	8
VIII	6	2.3	2	1.0	5	2.4	5	4.0	6	2.3	8	3.1	23	1.9	29	2.0	9	2.0	120	28.2	27	·	·	·	8	·	·	—	—	12	11	5	4	·	2
IX	·	·	2	2.5	14	2.9	6	3.2	8	2.6	22	3.3	16	2.8	6	1.7	16	2.4	71	29.4	29	·	·	·	2	·	·	—	—	12	8	3	7	·	1
X	9	2.0	5	2.6	·	·	1	1.0	1	1.0	18	3.2	20	2.2	24	2.2	15	2.0	24	6.6	16	·	·	6	·	·	·	—	—	7	6	·	10	·	·
XI	6	1.5	16	2.1	5	4.2	9	4.1	5	2.8	18	5.4	17	3.1	7	2.3	7	3.1	39	12.1	21	7	15	21	·	1	·	—	—	18	10	1	4	16	·
XII	2	1.0	·	·	·	·	12	3.0	9	4.4	36	4.9	28	2.6	3	3.0	3	3.6	42	10.9	18	3	9	26	·	1	·	—	—	20	11	1	5	19	·
Rok	67	1.9	101	2.1	83	2.6	102	3.1	63	2.6	221	3.8	195	2.8	184	2.6	79	2.8	630	29.4	29. IX	32	69	147	15	3	·	—	—	163	120	18	59	102	16

Augustów $H_s = 130 m$ $h_w = 12,5 m$

I	8	1.0	2.5	3.2	18	3.7	29.5	3.3	16	4.4	7.5	4.2	3	8.0	5.5	5.2	3	3.6	33	6.8	29	5	12	28	·	5	1	1	21	—	8	·	—	24	·
II	17	3.7	5	1.6	3	2.2	6.5	2.0	14.5	6.0	14	3.3	12.5	3.4	7.5	3.3	4	3.5	8	2.6	27	19	23	27	·	1	·	2	11	—	3	·	—	28	·
III	7.5	1.3	1.5	1.3	9	2.4	15.5	2.8	20.5	2.4	13	2.8	7	2.2	8	4.1	11	2.3	31	5.9	4	8	9	25	·	1	1	7	16	—	8	·	—	25	·
IV	7	2.7	10	4.5	34	4.4	18	4.3	6	2.8	5.5	3.8	2	1.5	5.5	3.6	2	3.9	26	13.3	23	·	·	13	·	1	1	1	16	—	5	1	·	1	1
V	15	2.0	8.5	2.1	18	4.0	5.5	1.5	5	3.6	8	1.9	14.5	2.0	13.5	2.9	5	2.5	58	20.8	29	·	·	6	·	·	·	1	11	—	10	·	2	·	1
VI	5.5	2.5	10	3.2	13.5	4.3	4	3.8	15.5	2.9	8	4.6	23.5	2.9	8	3.3	2	3.3	48	20.0	13	·	·	·	1	1	·	1	11	—	10	1	·	·	2
VII	4	5.0	9	3.8	4	1.5	6.5	3.2	26	4.2	34	4.9	5.5	2.9	3	4.0	1	4.2	83	19.6	31	·	·	·	4	1	·	·	10	—	12	2	·	·	4
VIII	1.5	5.7	1	4.0	10.5	1.9	8.5	3.0	4	3.5	18.5	2.7	26	2.5	17	2.8	6	2.5	37	9.0	26	·	·	·	6	·	·	2	9	—	8	·	2	·	3
IX	·	·	·	·	13	2.6	17	3.5	18.5	2.8	19	3.5	11.5	3.2	·	·	11	2.7	19	13.0	29	·	·	·	2	·	·	2	9	—	4	1	3	·	1
X	6	1.8	1	1.0	2	3.0	2	1.0	13	2.5	17.5	3.2	27	2.7	17.5	2.9	7	2.5	14	7.4	16	·	·	3	·	·	·	2	14	—	3	·	3	·	·
XI	2	3.5	20.5	3.1	8.5	7.7	4.5	6.6	15.5	3.2	21.5	4.9	9	3.1	3.5	2.3	5	4.0	53	13.7	21	8	16	22	·	3	1	·	24	—	8	2	3	16	·
XII	·	·	·	·	5	4.2	17.5	4.2	38	4.1	11.5	3.6	15	2.5	3	2.0	3	3.6	34	10.0	19	4	13	27	·	4	1	·	23	—	8	1	3	24	·
Rok	73.5	2.4	69	2.3	138.5	3.5	135	3.3	192.5	3.5	178	3.6	156.5	3.1	92	3.0	60	3.2	444	20.8	29. V	44	73	151	13	17	5	19	175	—	87	8	—	118	12

Mikołajki $H_s = 127 m$ $H_b = 131,1 m$ h_w = 12 m wiatromierz Wilda, 15,3 m anemometr M-47

I	3.5	3.9	3	2.5	8	3.4	17.5	5.2	18.5	5.1	17.5	5.6	9	5.2	9	5.0	7	4.5	26	5.0	8	3	13	29	·	4	·	1	18	16	9	·	6	17	·
II	9	5.7	9	4.7	3.5	3.9	1	2.5	5.5	3.9	13	5.1	21	4.1	18	4.1	4	4.2	21	2.7	3, 7, 10	11	23	26	·	2	·	1	13	15	8	·	3	28	·
III	4.5	5.7	4.5	2.7	6	2.8	13	3.9	15.5	4.0	16.5	3.9	15.5	3.3	9.5	4.9	8	3.5	19	6.4	3	5	8	23	·	1	·	5	14	11	6	·	10	19	·
IV	1	2.5	6	3.9	18.5	5.1	24.5	6.1	16	4.8	7	4.0	4	3.2	10	4.0	3	4.8	37	13.6	21	·	·	9	·	7	·	1	16	11	5	1	5	·	2
V	11.5	4.0	8.5	2.6	13	4.1	12.5	5.2	3	3.7	9	3.5	9	3.1	18.5	4.0	8	3.5	68	14.9	19	·	·	2	·	2	·	3	13	13	10	3	6	·	1
VI	6	4.5	8	4.9	11	4.1	8	5.2	8	5.1	11.5	4.2	12	3.6	21.5	4.2	4	4.2	42	16.3	1	·	·	·	1	6	·	2	9	15	7	1	4	·	4
VII	1	2.0	5.5	4.5	3.5	3.0	10	3.2	14	4.6	29	4.2	21	4.6	5	4.4	4	4.0	90	23.8	22	·	·	·	3	3	·	·	9	16	11	3	2	·	13
VIII	6.5	4.4	1	3.5	2	3.8	11	4.2	9	5.3	10.5	3.5	15.5	3.9	27.5	3.7	10	3.6	74	24.2	26	·	·	·	7	5	·	5	6	11	10	3	2	·	5
IX	·	·	1	2.0	6	3.4	18	3.4	17	4.9	23	4.0	16	3.8	5	4.0	4	3.8	72	42.7	29	·	·	·	1	9	·	6	6	13	9	1	2	·	3
X	6	2.8	3.5	2.1	2	3.8	3.5	3.9	4	3.4	26.5	3.7	20.5	3.5	23	4.3	4	3.5	15	8.9	16	·	·	2	·	8	·	3	12	6	3	·	11	·	·
XI	5	3.8	12.5	3.0	8.5	4.3	11	7.5	10	6.4	20	4.7	19.5	4.7	3.5	4.1	·	4.9	34	10.6	21	6	15	22	·	19	2	·	18	15	8	1	7	16	·
XII	·	·	·	·	0.5	1.0	11	5.8	17	5.9	39.5	5.2	17	3.8	6	4.1	2	4.9	35	8.0	19	2	7	25	·	17	2	·	22	20	10	·	3	20	·
Rok	54	3.3	62.5	3.0	82.5	3.6	141	4.7	137.5	4.8	223	4.3	180	3.9	156.5	4.2	58	4.1	533	42.7	29. IX	27	66	138	12	83	4	27	156	162	96	13	61	100	28

Resko $H_s = 55 m$ $H_b = 56,2 m$ $h_w = 11,9 m$

I	3.5	1.4	4.5	2.8	7	3.1	14.5	2.8	19.5	4.3	19.5	4.3	11	2.6	7.5	2.1	6	3.2	42	8.0	8	·	3	20	·	·	·	1	17	16	12	·	6	12	·
II	8.5	4.8	9	4.0	2	4.5	3.5	2.9	5	2.1	16.5	3.5	16	3.6	16.5	3.7	7	3.4	36	6.7	13	5	10	25	·	1	·	·	16	18	10	·	6	28	·
III	6	3.9	10.5	3.6	3	3.3	14.5	2.2	20.5	2.5	11	2.5	10.5	3.1	7	4.1	10	2.6	49	22.2	3	4	5	22	·	·	·	5	9	13	10	1	6	20	·
IV	6	2.7	13	3.2	12.5	4.0	21	4.5	9	2.9	7	3.7	6.5	2.7	8	3.4	7	3.3	33	7.4	23	·	·	5	·	·	·	2	15	16	10	·	6	·	1
V	10.5	3.9	12	2.5	13	2.9	17	4.0	2.5	3.2	7	2.6	9.5	2.9	13.5	3.9	8	3.0	73	20.4	9	·	·	3	·	3	·	5	14	16	12	2	1	·	3
VI	6.5	3.3	9	2.6	7	2.3	9.5	2.9	10.5	2.8	14.5	3.4	16	3.7	9	2.7	8	2.8	42	9.6	11	·	·	·	4	·	·	1	8	10	7	·	1	·	5
VII	3.5	2.6	6.5	2.5	7	2.7	6.5	3.5	9.5	2.5	35	3.5	17	3.9	1	1.0	7	3.0	107	23.1	14	·	·	·	3	·	·	·	11	20	19	2	3	·	10
VIII	4	3.1	2.5	1.4	3.5	1.3	8.5	1.6	8.5	1.8	17.5	2.6	12	2.3	9.5	3.1	27	1.6	64	24.0	23	·	·	·	3	·	·	1	7	12	11	2	5	·	5
IX	0.5	1.0	2	1.0	11.5	3.1	13.5	3.7	14	2.9	24	3.0	9.5	2.8	3	3.0	12	2.7	104	16.8	3	·	·	·	1	·	·	3	9	12	12	6	·	·	5
X	3	2.0	3.5	1.6	8.5	1.9	9	2.1	8.5	2.9	22.5	2.9	11	2.6	3	3.7	24	1.9	11	4.0	29	·	·	7	·	·	·	2	1	5	4	·	13	·	·
XI	1	1.5	9.5	2.8	11	3.6	15	4.1	9	4.1	26.5	4.0	5.5	3.7	3.5	2.4	9	3.3	49	15.0	21	6	10	19	·	·	·	2	13	18	10	2	4	11	·
XII	2	2.0	1	1.0	2.5	2.8	18.5	5.2	11.5	4.1	37.5	4.4	16.5	3.8	2.5	2.8	1	4.2	74	17.4	9	·	4	22	·	·	·	1	21	22	15	2	4	15	·
Rok	55	2.7	83	2.4	88.5	3.0	151	3.3	128	3.0	238.5	3.4	141	3.1	84	3.0	126	2.9	684	24.0	23. VIII	15	32	123	11	4	·	23	141	178	132	17	55	86	29

Uwaga. Kierunki i prędkości wiatru — wg anemometru M-47.

Świdwin — φ = 53°46' — λ = 15°46' — 1965

MIESIĄC	CIŚNIENIE p: P_m	Max	Min	$P_{o.m}$	TEMPERATURA T: Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	–	–	–	–	2.1	−2.7	7.1	17	−9.1	31	−0.7	0.9	−0.6	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.7	7.5	7.8
II	–	–	–	–	−0.3	−6.8	3.3	13	−17.5	17	−4.4	−1.4	−3.5	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.4	7.2	7.5
III	–	–	–	–	4.2	−4.3	13.0	29	−20.6	8	−2.4	2.9	−0.2	0.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.1	4.2	5.7
IV	–	–	–	–	11.0	2.3	15.8	6,22,30	−4.3	5	4.2	9.3	5.5	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	6.5	7.2
V	–	–	–	–	14.0	4.9	19.6	28	−3.0	3	8.0	12.6	8.5	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	6.4	6.7
VI	–	–	–	–	20.7	9.6	28.9	26	2.6	4	14.1	19.3	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.0	4.9	5.9
VII	–	–	–	–	18.9	10.1	29.4	14	6.4	2, 4	13.6	17.5	13.5	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	6.5	6.7
VIII	–	–	–	–	19.9	9.7	28.0	22	4.9	14	13.2	18.4	13.0	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.9	4.4	5.2
IX	–	–	–	–	18.9	9.6	25.6	3	5.3	23	11.6	17.6	12.7	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.5	5.3	5.6
X	–	–	–	–	12.9	3.4	22.1	1	−3.2	22	5.5	11.9	6.3	7.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.3	−3.3	11.2	1, 2	−13.2	24	−1.7	1.0	−1.2	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.2	−1.8	10.6	19	−10.3	17	−0.1	0.9	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.8	8.5	8.5
Rok	–	–	–	–	10.5	2.6	29.4	14.VII	−20.6	8. III	5.1	9.2	5.7	6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Połczyn-Zdrój — φ = 53°46' — λ = 16°06'

I	–	–	–	–	1.9	−2.3	6.4	17	−10.9	31	−0.6	1.1	0.0	0.1	5.3	5.7	5.5	5.5	90	86	89	88	0.6	1.0	0.7	0.8	–	–	–	–
II	–	–	–	–	−0.2	−6.4	3.5	13	−15.9	17	−4.0	−0.9	−3.3	−2.9	4.1	4.5	4.2	4.3	85	76	83	81	0.6	1.3	0.8	0.9	–	–	–	–
III	–	–	–	–	4.3	−3.7	13.7	29	−18.9	8	−2.2	3.5	0.1	0.4	5.1	5.9	5.5	5.5	90	73	84	82	0.5	2.2	1.0	1.2	–	–	–	–
IV	–	–	–	–	10.4	2.1	15.6	30	−3.9	5	4.4	9.4	5.8	6.4	7.4	7.2	7.6	7.4	87	63	83	78	1.1	4.8	1.7	2.5	–	–	–	–
V	–	–	–	–	13.9	4.7	19.0	17, 28	−3.4	3	8.2	12.7	8.6	9.5	9.1	9.0	9.3	9.1	82	62	82	75	2.0	6.0	2.1	3.4	–	–	–	–
VI	–	–	–	–	20.5	9.8	29.6	26	5.1	15	14.5	19.4	14.4	15.7	12.2	12.1	12.9	12.4	74	54	78	69	4.5	11.3	3.8	6.5	–	–	–	–
VII	–	–	–	–	18.9	10.4	29.8	14	6.7	6	13.8	17.5	13.8	14.7	13.4	13.2	13.7	13.4	83	66	86	78	2.6	7.5	2.2	4.1	–	–	–	–
VIII	–	–	–	–	20.0	10.0	27.5	22	5.1	14	13.6	18.9	13.3	14.8	13.5	13.4	13.7	13.5	86	61	89	79	2.2	9.0	1.8	4.3	–	–	–	–
IX	–	–	–	–	18.8	9.5	25.6	3	4.7	16	11.6	18.1	12.9	13.9	12.3	12.7	12.9	12.6	89	62	86	79	1.5	8.6	2.2	4.1	–	–	–	–
X	–	–	–	–	12.9	3.7	20.7	1	−2.8	22	6.2	12.1	6.9	8.0	9.3	10.0	9.0	9.5	92	70	89	84	0.8	4.4	1.2	2.1	–	–	–	–
XI	–	–	–	–	1.8	−3.3	11.4	1, 2	−12.2	24	−1.4	1.1	−1.1	−0.6	5.2	5.9	5.4	5.5	87	83	88	86	0.7	1.2	0.7	0.9	–	–	–	–
XII	–	–	–	–	2.3	−1.4	10.2	19	−9.3	16	0.3	1.1	0.4	0.6	5.7	5.9	5.8	5.8	89	87	89	88	0.7	0.9	0.6	0.7	–	–	–	–
Rok	–	–	–	–	10.5	2.8	29.8	14.VII	−18.9	8. III	5.4	9.5	6.0	6.7	8.6	8.8	8.8	8.7	86	70	86	81	1.5	4.8	1.6	2.6	–	–	–	–

Olsztyn-Dajtki — φ = 53°46' — λ = 20°25'

I	993.7	1010.1	973.5	1010.9	0.5	−4.3	4.5	1	−18.8	11	−1.9	−0.5	−1.9	−1.6	5.0	5.1	4.9	5.0	91	85	90	89	0.5	0.9	0.6	0.7	8.5	7.7	6.9	7.7
II	996.9	1017.5	969.9	1014.3	−2.3	−9.4	1.6	13, 14	−24.6	6	−6.6	−3.7	−5.8	−5.5	3.6	3.9	3.8	3.8	90	81	90	87	0.4	0.8	0.4	0.5	7.9	6.5	7.4	7.3
III	998.9	1014.8	972.3	1016.0	3.5	−5.0	9.4	17	−22.9	8	−3.4	2.5	−1.0	−0.7	4.7	5.2	5.2	5.0	91	69	86	82	0.4	2.5	0.8	1.2	6.3	5.8	5.4	5.8
IV	995.2	1012.7	977.5	1012.0	9.4	1.6	15.0	28	−4.2	3	3.4	8.0	5.4	5.6	7.0	7.0	7.0	7.0	87	66	77	77	1.0	3.9	2.1	2.3	7.6	8.3	7.0	7.6
V	997.2	1012.7	975.5	1013.9	13.3	3.6	19.2	18	−4.8	4	7.4	12.0	8.0	8.8	8.8	8.3	8.8	8.6	84	59	80	74	1.7	6.0	2.2	3.3	6.6	7.0	5.3	6.3
VI	997.2	1004.9	987.6	1013.4	20.3	10.2	29.1	26	2.8	8	14.0	18.7	14.8	15.6	13.0	12.3	12.9	12.7	81	59	77	72	3.2	9.8	4.2	5.7	5.4	6.0	4.9	5.4
VII	994.1	1006.5	978.6	1010.4	20.1	10.9	29.3	15	6.2	5	14.2	18.2	14.5	15.4	14.2	13.6	14.3	14.0	86	65	85	79	2.3	8.0	2.6	4.3	5.7	7.5	5.0	6.1
VIII	998.1	1006.0	988.3	1014.5	20.1	10.0	28.4	22	4.1	31	12.9	18.7	13.9	14.8	13.7	13.7	13.9	13.8	92	65	87	81	1.4	8.8	2.4	4.2	6.2	6.7	5.0	6.0
IX	997.5	1015.1	987.0	1013.9	19.7	9.4	28.6	3	4.3	16	11.4	18.4	13.4	14.2	12.9	14.2	13.9	13.7	95	67	89	84	0.7	7.5	1.7	3.3	4.8	5.5	3.6	4.6
X	1004.7	1020.3	988.2	1021.4	11.6	4.2	19.8	1	−4.1	21	5.7	10.8	7.3	7.8	8.9	10.1	9.7	9.6	95	77	93	88	0.4	3.2	0.8	1.5	6.5	7.3	6.4	6.7
XI	994.2	1012.1	966.0	1011.4	0.5	−4.3	10.5	2	−16.5	17	−2.4	−0.6	−1.8	−1.6	5.2	5.3	5.3	5.3	93	86	90	90	0.4	1.0	0.6	0.7	8.4	8.0	7.8	8.1
XII	986.7	1005.1	962.8	1003.7	1.4	−2.4	9.5	19	−14.7	17	−0.5	0.3	−0.3	−0.2	5.5	5.5	5.5	5.5	91	86	90	89	0.6	0.9	0.7	0.7	8.7	8.1	8.1	8.3
Rok	996.2	1020.3	962.8	1013.0	9.8	2.0	29.3	15.VII	−24.6	6. II	4.6	8.6	5.5	6.0	8.5	8.7	8.8	8.7	90	72	86	83	1.1	4.4	1.6	2.4	6.9	7.0	6.1	6.7

Kwidzyń — φ = 53°44' — λ = 18°55'

I	–	–	–	–	–	−3.9	–	–	−16.1	11	−1.2	0.9	−1.2	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.8	6.9	8.5	8.1
II	–	–	–	–	–	−8.6	–	–	−21.7	6	−5.1	−1.3	−4.9	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.9	8.1	7.6
III	–	–	–	–	–	−5.6	–	–	−26.7	8	−3.3	3.3	−1.4	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	7.7	7.1
IV	–	–	–	–	–	2.6	–	–	−3.1	6	4.4	10.2[1]	5.5	6.4[1]	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.3	7.9	7.3
V	–	–	–	–	–	4.6	–	–	−1.4	3	8.3	14.0[1]	7.8	9.5[1]	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.7	7.0	6.5
VI	–	–	–	–	–	9.6	–	–	3.0	15	14.5	20.9[1]	14.4	16.0[1]	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.0	5.8	5.4
VII	–	–	–	–	–	10.2	–	–	5.7	2, 6	14.9	20.4[1]	14.1	15.9[1]	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	7.3	6.3
VIII	–	–	–	–	–	9.6	–	–	4.7	3	14.0	20.6[1]	14.5	15.9[1]	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.7	6.8	6.1
IX	–	–	–	–	–	9.5	–	–	1.6	16	12.1	20.1[1]	13.5	14.8[1]	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.2	6.4	5.9
X	–	–	–	–	–	3.6	–	–	−1.8	22	6.0	12.7[1]	6.7	8.0[1]	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	7.8	7.3
XI	–	–	–	–	–	−3.6	–	–	−20.3	24	−1.6	1.3	−1.2	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.1	8.2	7.8
XII	–	–	–	–	–	−2.3	–	–	−18.4	17	−0.4	1.9	−0.3	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.2	9.3	8.8
Rok	–	–	–	–	–	2.1	–	–	−26.7	8. III	5.2	10.4[1]	5.6	6.7[1]	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	7.6	7.0

Świdwin — $H_s = 94\,m$ — $h_w = 12{,}4\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<-21°	Max>25°	Wiatr v >10	>15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K
I	2	3.0	2	2.0	2	2.5	14	2.3	11.5	5.1	24.5	5.0	5.5	4.1	4.5	3.9	27	2.9	36	7.9	8	·	4	26	·	1	1	1	17	13	10	·	4	7	·
II	7.5	7.9	9	3.7	·	·	11	4.0	1	2.0	16	4.4	11.5	3.3	10	4.2	18	3.5	20	3.1	13	5	16	28	·	3	1	1	14	15	8	·	4	28	·
III	9.5	1.8	9	1.9	2	5.0	6.5	4.2	3	3.8	10.5	4.6	5	1.7	10.5	2.4	37	1.8	23	5.8	3	6	9	22	·	1	·	7	9	10	7	·	·	16	·
IV	2	4.0	7	4.6	19	4.2	13.5	4.2	2.5	5.8	7	3.6	9.5	2.9	8.5	4.2	21	3.0	35	8.5	13	·	·	5	·	·	·	3	12	13	9	·	1	·	1
V	6.5	2.7	12.5	3.6	10	3.4	15	3.4	3	2.7	8.5	2.6	6	4.5	13.5	3.9	18	2.8	85	29.6	9	·	·	1	·	·	·	3	14	17	13	2	·	·	3
VI	3	2.3	8	4.5	14	3.2	6.5	3.0	2.5	4.8	21	3.8	6.5	4.2	7.5	4.1	21	2.9	32	9.7	18	·	·	·	3	·	·	2	9	8	6	·	·	·	2
VII	·	·	9	6.4	2	2.5	5	3.4	2.5	2.6	40.5	5.0	11	6.2	3	3.3	20	4.0	111	18.1	8	·	·	·	3	2	1	3	12	21	20	3	·	·	8
VIII	4	2.8	3	2.3	2	2.5	2	2.5	5	2.8	15	3.5	6	3.3	2	5.0	54	1.3	61	16.0	8	·	·	·	3	·	·	5	6	11	9	2	·	·	2
IX	1	7.0	3	4.0	5	3.2	10.5	2.4	7	3.5	21.5	3.6	7	2.4	5	3.4	30	2.2	70	21.5	3	·	·	·	1	·	·	5	11	12	11	1	·	·	2
X	1	2.0	1	1.0	2	4.5	5	2.2	5	3.6	14.5	2.7	6.5	4.7	4	4.5	54	1.4	13	4.7	29	·	·	3.6	·	·	·	—	—	5	5	·	2	·	1
XI	0.5	2.0	2.5	4.2	13.5	2.8	12	4.2	9	4.6	21	5.3	1	4.0	3.5	5.1	27	3.0	46	10.2	21	5	12	20	·	2	·	—	—	12	9	2	2	10	·
XII	·	·	1	2.0	1	2.0	15.5	3.8	15	4.4	30	5.3	10.5	4.1	·	·	20	3.6	58	17.6	18	1	4	22	·	2	1	2	23	16	12	2	1	11	·
Rok	37	3.0	67	3.4	72.5	3.0	116.5	3.3	67	3.8	230	4.1	86	3.8	72	3.7	347	2.7	590	29.6	9.V	17	45	130	10	11	4	—	—	153	119	12	14	72	19

Połczyn-Zdrój — $H_s = 50\,m$ — $h_w = 11{,}2\,m$

I	1	1.0	1	2.0	5	1.4	16	1.2	16	2.0	22.5	2.5	18.5	2.0	3	1.0	10	1.7	45	8.8	25	1	4	22	·	1	·	—	—	—	12	·	·	13	—
II	9	1.3	5	1.8	3	1.3	1	1.0	2	2.0	11.5	2.0	29	1.9	12.5	1.5	11	1.5	29	6.2	26	7	18	27	·	·	·	—	—	—	10	·	1	28	—
III	6	1.2	3.5	1.3	5.5	1.4	2	1.0	11	1.8	23.5	1.1	22	1.4	6.5	1.3	13	1.2	50	28.0	3	4	8	21	·	·	·	—	—	—	6	1	6	19	—
IV	1	1.0	3.5	1.4	16	2.5	8.5	1.9	15	2.0	9	1.6	16.5	1.3	7.5	1.1	13	1.5	34	8.6	28	·	·	5	·	·	·	—	—	—	6	·	3	·	—
V	9.5	1.1	4.5	1.3	16	1.8	9.5	1.5	4.5	3.6	2	2.0	25	1.4	12	1.0	10	1.4	91	32.9	9	·	·	2	·	·	·	—	—	—	13	2	·	·	—
VI	4.5	1.0	5	1.4	13	1.5	2	1.0	9.5	1.7	13	1.2	27	1.3	8	1.0	8	1.2	37	14.0	1	·	·	·	3	·	·	—	—	—	5	2	·	·	—
VII	2	2.2	5	3.2	9	2.5	1	1.0	4	2.4	33	3.0	27.5	2.0	2.5	1.4	9	2.3	134	21.8	14	·	·	·	2	·	·	—	—	—	17	4	2	·	—
VIII	6	1.0	1	1.0	·	·	1	2.0	6	1.7	12.5	1.1	35	1.2	6.5	1.2	25	0.9	56	21.0	8	·	·	·	5	·	·	—	—	—	8	2	2	·	—
IX	1	1.0	·	·	7.5	2.1	6.5	2.2	9.5	1.0	26	1.3	23.5	1.2	1	1.0	16	1.1	95	20.8	3	·	·	·	1	·	·	—	—	—	13	3	—	·	—
X	4	1.0	2	1.0	7	1.4	2	2.0	6	1.0	23	1.7	20.5	1.0	4.5	1.0	24	1.0	12	6.5	30	·	·	5	·	·	·	—	—	—	4	·	6	·	—
XI	2	1.0	·	·	18	1.2	3	1.3	15	1.7	20	2.4	16	1.5	1	1.0	15	1.4	48	15.7	22	6	12	20	·	·	·	—	—	—	9	2	1	10	—
XII	·	·	·	·	·	·	7.5	2.3	18.5	1.7	32.5	2.2	29.5	1.5	1	1.0	4	1.8	64	23.5	9	·	3	23	·	1	·	—	—	—	11	2	·	18	—
Rok	46	1.1	30.5	1.2	100	1.4	59	1.5	117	1.9	228.5	1.8	290	1.5	66	1.1	158	1.4	695	32.9	9.V	18	45	125	11	2	·	—	—	—	114	18	—	88	—

Olsztyn-Dajtki — $H_s = 133\,m$ — $H_b = 135{,}4\,m$ — $h_w = 12\,m$

I	5	2.4	6	3.5	13.5	3.1	10	3.7	14.5	4.1	26.5	4.0	7.5	5.1	8	5.4	2	3.9	31	9.4	8	3	10	27	·	2	·	·	15	19	8	·	5	23	·
II	13	5.0	9.5	3.5	1.5	4.3	1	2.0	4	3.4	15	4.7	27.5	4.7	9.5	4.9	3	4.4	38	4.6	25	10	22	27	·	3	·	1	12	22	14	·	2	28	·
III	4.5	3.7	8	3.3	4.5	3.8	8	3.8	17	3.6	19	2.7	17.5	3.9	6.5	6.4	8	3.4	29	10.4	3	4	9	24	·	3	·	6	12	14	7	1	8	21	·
IV	6.5	3.5	6	4.2	23.5	5.1	15.5	4.0	11	3.5	8.5	2.8	5.5	3.9	9.5	4.1	4	3.9	36	8.7	21	·	·	10	·	1	·	2	13	12	13	·	3	·	1
V	15.5	3.3	10.5	3.5	18.5	3.8	3.5	5.0	5.5	3.5	11	4.0	10	3.8	12.5	3.5	6	3.5	46	9.7	19	·	·	4	·	4	·	[illegible]	[illegible]	[illegible]	[illegible]	·	3	·	1
VI	10.5	3.2	10.5	3.3	10.5	4.1	1	6.0	8.5	2.4	10.5	3.4	23	4.0	10.5	4.6	5	3.5	82	36.4	22	·	·	·	3	1	·	4	8	15	11	2	3	·	4
VII	4	3.5	10.5	2.2	4.5	1.6	2.5	1.8	8.5	2.2	37.5	3.1	20	3.4	4.5	1.8	1	2.8	85	13.5	16	·	·	·	2	·	·	2	7	19	14	3	1	·	8
VIII	1.5	1.0	·	·	5	1.0	4	3.8	9.5	2.4	5	3.1	29.5	3.4	21.5	3.1	17	2.5	132	40.0	26	·	·	·	8	·	·	3	12	15	12	3	7	·	4
IX	·	·	0.5	3.0	14.5	2.7	5	2.2	14.5	2.2	21.5	3.3	14.5	4.0	4.5	4.1	15	2.6	75	32.4	29	·	·	·	1	·	·	9	5	12	9	3	8	·	1
X	5	2.3	3	2.2	3.5	3.4	1	2.0	1.5	3.0	21	3.9	25.5	3.7	15.5	3.9	17	2.9	20	6.1	16	·	·	6	·	1	·	2	12	9	5	·	4	·	·
XI	5.5	2.8	17.5	4.4	9.5	4.2	3.5	4.7	14.5	4.4	17.5	5.0	16.5	4.5	2.5	2.8	3	4.2	36	11.1	1	7	14	22	·	·	·	2	21	17	11	1	7	16	·
XII	·	·	·	·	0.5	3.0	14	4.9	15	4.5	34	4.6	26	4.7	2.5	3.4	1	4.5	50	15.9	18	4	10	24	·	2	·	1	20	13	10	2	5	19	·
Rok	71	2.6	82	2.8	109.5	3.3	69	3.7	124	3.3	227	3.7	223	4.1	107.5	4.0	82	3.5	661	40.0	26.VIII	28	65	144	14	17	·	38	155	189	120	15	71	107	19

Kwidzyń — $H_s = 15\,m$ — $h_w = 13\,m$

I	2	1.2	1	1.5	3.5	3.3	7.5	2.9	29	3.8	26	3.9	5	4.8	2	1.5	17	3.0	34	6.3	21	3	—	26	—	2	·	·	16	—	11	·	1	18	—
II	12	2.7	7	2.3	0.5	1.0	2	1.2	14.5	3.4	16.5	5.0	8	2.8	5.5	4.0	18	2.7	47	—	—	8	—	27	—	2	·	·	13	—	9	2	1	28	—
III	11	3.1	5	2.8	2	1.0	4	2.8	21.5	2.2	19.5	1.9	3	1.3	3	1.0	23	1.7	60	18.3	4	8	—	21	—	·	·	1	13	—	7	2	3	18	—
IV	5.5	1.7	6	3.1	9.5	4.3	14.5	3.1	19.5	2.5	17.5	2.5	2	2.2	2.5	1.6	13	2.4	51	6.8	12	·	—	5	—	·	·	·	16	—	13	·	1	1	—
V	16.5	2.2	12.5	1.8	7	2.6	12.5	2.1	10.5	1.9	9.5	2.6	3.5	4.0	3	3.0	18	1.8	50	13.3	9	·	—	5	—	·	·	·	7	—	9	1	·	·	—
VI	8.5	2.2	4.5	1.9	1.5	1.0	8.5	2.6	15.5	2.3	17.5	2.3	9	3.2	6	2.2	21	1.8	80	18.5	26	·	—	·	—	1	·	·	5	—	9	4	·	·	—
VII	1.5	3.3	2.5	2.8	0.5	2.0	3.5	1.9	24	2.5	40	3.2	2	2.2	1	1.5	18	2.3	92	15.2	12	·	—	·	—	2	1	·	5	—	13	3	·	·	—
VIII	1.5	1.7	·	·	·	·	4.5	2.3	15.5	1.6	25.5	1.7	8	1.4	3	1.7	35	1.1	108	21.1	25	·	—	·	—	·	·	·	8	—	13	5	1	·	—
IX	2	1.8	·	·	3	2.3	9.5	1.7	29.5	1.6	22	2.0	·	·	3	1.8	21	1.4	201[2]	68.1	4	·	—	·	—	·	·	·	7	—	8	6	3	·	—
X	5	4.0	2.5	1.2	·	·	1	2.0	19.5	1.7	24	1.7	5.5	1.6	1.5	3.3	34	1.2	36	18.5	16	·	—	1	—	·	·	·	9	—	3	2	8	·	—
XI	3	1.8	6.5	2.2	7.5	1.7	9	4.6	16.5	2.8	24	4.0	·	·	0.5	1.0	23	2.4	37	11.8	1	7	—	17	—	2	·	·	14	—	11	1	4	14	—
XII	·	·	·	·	3	2.0	15	2.6	29	3.6	31	4.0	5	2.2	·	·	10	3.1	31	6.7	14	3	—	19	—	3	1	·	22	—	8	·	2	4	—
Rok	66.5	2.1	48.5	1.6	38	1.8	91.5	2.5	244.5	2.5	273	2.9	51	2.1	31	1.9	251	2.1	827[2]	68.1	4.IX	29	—	121	—	12	2	1	135	—	114	26	24	82	—

Prabuty — φ = 53°44' — λ = 19°13' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia t	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.9	−3.9	4.8	1	−16.7	11	−1.6	−0.1	−1.7	−1.3	4.8	5.1	4.8	4.9	87	83	87	86	0.7	1.1	0.7	0.8	8.6	7.9	6.6	7.7
II	–	–	–	–	−1.5	−9.4	2.5	11	−22.0	6	−6.1	−3.1	−5.5	−5.0	3.5	3.9	3.6	3.7	85	78	83	82	0.6	1.1	0.7	0.8	7.2	6.0	6.8	6.7
III	–	–	–	–	3.1	−3.3	12.8	29	−24.5	8	−3.5	1.4	−0.7	−0.9	4.5	5.1	5.0	4.9	86	74	82	81	0.7	1.9	1.1	1.2	6.2	5.7	5.4	5.8
IV	–	–	–	–	9.7	2.2	14.4	22, 30	−2.5	3	3.8	6.1	5.3	5.6	6.9	7.5	7.0	7.1	83	70	79	77	1.3	3.5	2.0	2.3	7.3	7.6	5.3	6.7
V	–	–	–	–	13.7	4.7	19.0	17	−1.7	4	8.2	12.2	7.8	9.0	8.5	8.3	8.6	8.5	76	58	80	71	2.5	6.2	2.2	3.6	6.3	6.6	4.4	5.8
VI	–	–	–	–	21.0	10.4	29.2	26	5.5	8	14.5	19.4	14.5	15.7	12.6	11.9	12.8	12.4	77	54	77	69	4.1	11.2	3.9	6.4	5.7	5.7	4.3	5.2
VII	–	–	–	–	20.4	11.2	29.5	14	6.3	5	14.6	18.5	14.2	15.4	13.5	13.1	13.8	13.5	81	62	84	76	3.3	8.8	2.7	4.9	5.9	7.4	5.5	6.3
VIII	–	–	–	–	20.5	10.4	28.4	22	4.6	16	13.3	19.1	13.8	15.0	13.7	13.7	13.4	13.6	89	63	85	79	1.8	9.0	2.8	4.5	5.9	6.7	3.8	5.5
IX	–	–	–	–	19.6	9.8	26.4	3	3.5	16	11.9	18.1	13.3	14.2	12.6	13.4	13.1	13.0	89	64	85	79	1.6	7.9	2.4	4.0	5.7	4.9	2.6	4.4
X	–	–	–	–	12.1	4.1	19.4	1	−1.5	21	5.7	10.9	7.1	7.7	8.6	9.9	9.2	9.2	92	75	90	86	0.7	3.3	1.0	1.7	7.1	6.6	3.7	5.8
XI	–	–	–	–	0.8	−4.2	10.6	2	−16.6	24	−2.6	−0.5	−1.7	−1.6	5.0	5.2	5.2	5.1	89	82	87	86	0.5	1.2	0.7	0.8	7.9	7.6	6.4	7.3
XII	–	–	–	–	1.4	−2.5	10.0	19	−19.0	17	−0.8	0.2	−0.5	−0.4	5.2	5.3	5.3	5.3	88	84	86	86	0.8	1.1	0.9	0.9	7.8	8.3	5.9	7.3
Rok	–	–	–	–	10.1	2.5	29.5	4.VII	−24.5	8. III	4.8	8.7	5.5	6.1	8.3	8.5	8.5	8.4	85	71	84	80	1.6	4.7	1.8	2.7	6.8	6.8	5.1	6.2

Szczecinek — φ = 53°43' — λ = 16°41'

I	992.6	1008.3	969.8	1010.4	1.6	−2.6	5.9	1	−10.0	31	−1.1	0.5	−0.5	−0.4	5.2	5.4	5.3	5.3	91	85	89	88	0.5	1.0	0.6	0.7	8.6	8.1	7.4	8.0
II	998.5	1017.0	969.1	1016.8	−0.7	−8.0	3.2	13	−18.3	17	−4.8	−1.7	−4.3	−3.8	3.9	4.2	4.0	4.0	87	77	86	83	0.5	1.2	0.6	0.8	7.9	7.8	7.0	7.6
III	998.5	1013.8	973.4	1016.5	4.4	−5.3	13.5	29	−25.8	8	−3.6	3.1	−0.4	−0.3	4.7	5.4	5.2	5.1	89	70	83	81	0.6	2.5	1.0	1.4	7.2	6.3	5.0	6.2
IV	993.8	1014.6	974.1	1011.2	10.4	2.6	15.8	30	−4.9	5	3.6	9.1	5.7	6.0	7.1	7.1	7.3	7.2	89	62	80	77	0.9	4.7	2.0	2.5	8.0	8.3	6.4	7.6
V	997.0	1011.9	977.0	1014.3	13.8	5.1	19.8	17	−1.8	3	7.7	12.3	8.7	9.4	8.7	8.4	8.7	8.6	81	59	76	72	2.0	6.0	2.8	3.6	7.4	7.3	6.1	6.9
VI	997.1	1007.1	982.7	1014.0	20.4	10.3	28.3	26	5.0	4	14.0	18.9	14.5	15.5	12.3	12.4	12.5	12.4	76	57	76	70	4.0	10.1	4.2	6.1	5.9	7.2	5.8	6.3
VII	993.4	1004.9	976.8	1010.4	18.9	11.2	29.0	14	7.6	5	13.4	17.5	14.1	14.8	13.4	12.9	13.7	13.3	86	65	84	78	2.2	7.6	2.6	4.1	6.9	7.9	6.7	7.2
VIII	998.1	1006.5	987.2	1015.2	19.8	10.3	27.3	22	6.3	2	12.7	18.6	13.7	14.7	13.2	13.2	13.6	13.3	89	62	85	79	1.7	8.7	2.4	4.3	6.0	7.2	4.3	5.8
IX	997.3	1016.1	983.6	1014.4	19.0	9.6	26.2	3	2.6	16	11.1	17.7	13.1	13.8	12.1	13.0	12.9	12.7	91	65	85	80	1.3	7.7	2.3	3.8	6.7	6.8	5.0	6.2
X	1005.3	1020.3	988.4	1022.9	12.7	3.6	20.6	1	−3.8	22	5.5	11.7	6.3	7.4	8.8	10.3	8.9	9.3	95	74	91	87	0.5	3.7	0.9	1.7	7.5	6.8	3.7	6.0
XI	993.4	1011.8	963.2	1011.2	1.5	−3.6	11.1	1	−13.6	24	−2.0	0.6	−1.3	−1.0	5.1	5.6	5.2	5.3	89	81	86	85	0.6	1.1	0.8	0.8	7.9	8.1	6.6	7.5
XII	985.3	1006.6	956.8	1003.1	2.0	−1.8	9.9	19	−13.4	17	−0.2	0.8	0.1	0.2	5.5	5.6	5.6	5.6	89	84	89	87	0.7	1.0	0.7	0.8	9.7	8.6	8.6	9.0
Rok	995.9	1020.3	956.8	1013.5	10.3	2.6	29.0	14.VII	−25.8	8. III	4.7	9.1	5.8	6.4	8.3	8.6	8.6	8.5	88	70	84	81	1.3	4.6	1.7	2.5	7.5	7.5	6.0	7.0

Śliwice — φ = 53°43' — λ = 18°11'

I	–	–	–	–	1.1	−3.7	4.8	17	−16.1	11	−1.8	0.3	−1.5	−1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.4	7.6	7.7
II	–	–	–	–	−0.7	−8.4	3.8	11	−17.0	25	−5.4	−1.6	−5.0	−4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.9	5.9	7.3
III	–	–	–	–	4.3	−5.5	12.3	29	−24.5	8	−3.9	3.2	−1.2	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.2	5.8	6.4
IV	–	–	–	–	9.9	1.9	15.1	6	−3.3	6	3.9	8.6	5.2	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.0	7.0	7.6
V	–	–	–	–	14.1	4.3	20.2	17	−3.1	4	8.4	12.8	8.3	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	5.7	6.3
VI	–	–	–	–	21.4	10.0	30.8	26	5.1	4	14.4	20.0	14.6	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.4	5.0	5.6
VII	–	–	–	–	20.3	10.9	30.5	14	5.8	2	14.1	19.1	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.4	6.8	6.9
VIII	–	–	–	–	21.1	10.0	29.8	23	5.0	2	12.7	19.8	13.9	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.4	5.0	6.1
IX	–	–	–	–	19.8	8.9	28.1	3	2.3	16	10.7	18.6	12.7	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.3	4.0	5.3
X	–	–	–	–	12.7	3.7	19.5	1	−3.1	21	5.2	12.1	6.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.8	3.4	6.1
XI	–	–	–	–	1.2	−4.5	10.8	2	−19.6	24	−2.7	0.2	−1.8	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.7	7.0	7.8
XII	–	–	–	–	1.7	−2.4	9.7	19, 20	−18.6	17	−0.7	0.6	0.1	0.0	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.1	8.5	9.0
Rok	–	–	–	–	10.6	2.1	30.8	26.VI	−24.5	8. III	4.6	9.5	5.5	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.3	6.0	6.8

Chojnice — φ = 53°42' — λ = 17°33'

I	988.4	1004.5	966.3	1010.5	0.7	−3.6	4.4	17	−11.4	10	−1.8	−0.6	−1.5	−1.4	5.1	5.3	5.1	5.2	94	89	92	92	0.3	0.7	0.4	0.5	8.1	8.0	6.0	8.0
II	993.5	1012.5	963.6	1016.1	−1.7	−8.6	1.9	15	−14.5	24	−5.6	−2.7	−5.0	−4.6	3.8	4.2	3.8	3.9	91	83	87	87	0.3	0.8	0.5	0.5	7.8	7.9	6.5	7.4
III	994.1	1009.4	968.0	1016.4	2.8	−5.0	11.4	29	−21.2	8	−3.6	1.3	−1.1	−1.1	4.7	5.4	5.1	5.1	92	79	87	86	0.4	1.5	0.8	0.9	7.5	6.4	5.7	6.5
IV	989.7	1009.5	970.9	1011.4	9.2	2.4	15.0	30	−3.9	5	3.3	8.0	5.2	5.4	7.3	7.4	7.3	7.3	92	70	82	81	0.6	3.5	1.7	1.9	7.9	8.6	6.6	7.7
V	992.8	1008.0	972.9	1014.3	13.6	4.5	19.4	28	−3.0	3	7.1	12.2	8.1	8.9	8.6	8.5	8.6	8.6	84	61	78	74	1.7	6.0	2.5	3.4	6.8	7.7	6.3	6.9
VI	992.8	1002.2	979.8	1013.9	20.2	9.6	28.3	26	4.6	4	13.4	18.7	14.1	15.1	12.4	12.6	12.4	12.5	80	59	77	72	3.1	9.5	3.9	5.5	6.2	7.8	6.0	6.7
VII	989.4	1001.1	973.3	1010.4	18.9	10.1	28.4	14	4.8	2	12.8	17.5	13.3	14.2	13.3	12.8	13.7	13.3	89	64	89	81	1.7	7.7	1.8	3.7	6.5	8.2	7.0	7.2
VIII	993.9	1001.7	984.1	1015.0	19.6	9.6	27.5	23	5.6	31	12.1	18.2	13.8	14.2	13.2	13.2	13.3	13.2	93	63	87	81	1.1	8.3	2.3	3.9	6.3	7.9	4.0	6.1
IX	992.2	1011.5	980.3	1013.4	18.7	9.0	26.3	3	3.9	16	10.2	17.6	12.6	13.2	11.9	13.3	13.0	12.7	95	66	89	83	0.7	7.2	1.7	3.2	7.1	6.8	4.6	6.2
X	1000.7	1015.3	984.0	1022.5	12.1	3.5	20.1	1	−1.5	22	5.1	11.1	6.1	7.1	8.6	10.3	8.9	9.3	97	77	93	89	0.3	3.2	0.6	1.4	8.1	7.7	3.4	6.4
XI	988.9	1006.9	959.8	1011.2	0.7	−4.4	10.3	1	−16.4	24	−2.8	−0.2	−2.0	−1.8	5.1	5.7	5.3	5.4	93	87	91	90	0.4	0.8	0.5	0.6	8.7	8.2	7.0	8.0
XII	981.1	1001.5	953.9	1003.1	1.1	−2.9	9.7	19	−13.9	17	−1.1	−0.3	−0.8	−0.8	5.4	5.5	5.6	5.5	93	90	93	92	0.4	0.6	0.4	0.5	9.3	8.8	9.4	9.2
Rok	991.5	1015.3	953.9	1013.1	9.7	2.0	26.[illegible]	14.VII	−21.2	8. III	4.1	8.4	5.2	5.7	8.3	8.7	8.5	8.5	91	74	87	84	0.9	4.2	1.4	2.2	7.5	7.8	6.2	7.2

Prabuty $H_s = 98$ m $h_w = 12$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	3.0	8	3.5	·	·	18	3.3	27	5.3	19	3.8	5	3.4	4	7.5	10	3.8	26	5.0	8	2	11	28	·	2	1	·	15	19	9	·	4	18	·
II	6	5.7	13	4.2	2	2.5	1	3.0	9	3.3	28	4.6	16	3.5	3	4.0	6	3.9	40	12.5	27	8	18	26	·	3	·	3	13	21	11	1	3	28	·
III	7	6.7	6	3.7	5	3.0	2.5	3.2	35.5	2.8	21	3.0	11	2.5	1	2.0	4	3.0	35	7.2	21	5	9	22	·	2	·	7	12	13	9	·	3	18	·
IV	6	5.7	3	9.0	18	6.7	14	5.5	25	5.0	9	2.4	7	3.0	2	2.5	6	4.8	34	6.0	19	·	·	8	·	7	1	4	12	14	10	·	1	·	·
V	19	4.6	9	3.6	14	5.5	12	4.8	8	2.0	18	3.2	5	3.6	2	3.0	6	3.8	59	15.7	9	·	·	4	·	3	·	3	10	17	15	1	·	·	1
VI	8	4.2	8	5.0	8	4.4	6	4.5	16	5.0	25	3.1	11	3.8	3	3.7	5	3.9	48	18.1	1	·	·	·	4	1	·	4	7	10	6	2	·	·	4
VII	2	7.0	6	4.7	1	5.0	7	3.0	25.5	2.7	33.5	3.9	8	4.6	·	·	10	3.2	67	12.8	24	·	·	·	2	1	·	1	7	20	14	1	1	·	8
VIII	2	3.5	3	2.3	·	·	5	4.2	21	3.5	22	2.4	9	3.4	5	3.0	26	2.2	75	17.5	27	·	·	·	5	·	·	5	5	17	13	1	1	·	2
IX	·	·	2	2.5	3	4.7	11	3.5	30	3.3	25	3.6	2	5.0	2	4.5	15	2.9	108	46.8	4	·	·	·	1	1	·	8	3	9	8	3	3	·	2
X	2	2.5	1	2.0	4	3.0	2	2.0	24.5	1.9	36.5	3.6	2	1.5	4	3.2	17	2.3	26	7.3	3	·	·	3	·	·	·	3	8	10	5	·	8	·	·
XI	3	2.7	14	4.0	9	4.0	9	5.7	18.5	5.3	26.5	4.6	5	3.6	·	·	5	4.3	41	12.3	21	8	13	19	·	4	1	2	14	18	10	2	3	16	·
XII	·	·	1	2.0	·	·	11.5	7.1	31	4.7	44.5	4.5	1	5.0	·	·	4	4.7	38	12.2	18	4	7	23	·	5	·	·	16	15	8	1	2	—	·
Rok	57	3.8	74	3.9	64	3.2	99	4.2	271	3.7	308	3.6	82	3.6	26	2.8	114	3.6	597	46.8	4. IX	27	58	133	12	29	3	40	122	183	118	12	29	—	17

Szczecinek $H_s = 137$ m $H_b = 142{,}6$ m $h_w = 18$ m

I	3.5	3.4	5	3.3	6.5	3.1	12	3.2	23	5.5	22	5.1	11	3.8	6	2.5	4	4.1	41	7.1	25	·	9	26	·	1	·	·	18	16	11	·	4	16	·
II	6.5	3.5	10	5.2	3	5.2	2.5	3.4	7.5	4.2	17	4.3	21.5	4.7	13	5.7	3	4.5	27	4.5	13	8	20	27	·	4	·	·	13	21	10	·	7	28	·
III	3.5	6.6	9	4.7	6.5	2.6	9	4.2	21	3.1	20	3.4	9.5	3.4	7.5	5.5	7	3.5	30	14.7	3	7	9	23	·	1	·	5	10	15	6	1	9	22	·
IV	5	4.4	7	5.2	20.5	5.0	14	4.6	16.5	4.2	7	4.4	8	4.0	8	4.6	4	4.4	38	23.2	13	·	·	4	·	·	·	2	17	10	8	1	6	·	1
V	7.5	4.8	13.5	4.1	15	4.4	11.5	4.3	7	5.1	11.5	4.2	12.5	4.0	11.5	4.1	3	4.2	73	35.4	9	·	·	2	·	·	·	3	15	17	13	1	1	·	1
VI	3	4.5	14	5.2	7	4.5	4.5	4.6	15	4.7	13.5	4.6	17	5.2	12	4.5	4	4.6	79	28.3	22	·	·	·	4	·	·	2	7	10	7	3	1	·	4
VII	1.5	5.3	8	6.1	4.5	2.7	6.5	3.0	11	3.6	43.5	4.8	14	5.2	2	5.2	2	4.5	86	11.8	14	·	·	·	2	·	·	2	13	21	16	1	3	·	8
VIII	4	4.1	2.5	1.8	1	1.0	7.5	2.1	13	3.8	21	3.4	18	3.2	12	3.4	14	2.8	32	7.2	25	·	·	·	4	·	·	1	5	12	9	·	5	·	3
IX	·	·	2	4.8	8	3.2	14.5	4.2	22.5	3.5	24.5	4.4	7	3.5	3.5	4.1	8	3.6	80	20.0	6	·	·	·	1	·	·	2	10	14	8	3	6	·	4
X	1.5	3.7	6	1.7	6	2.8	6	3.2	17.5	3.2	18	4.6	17	3.0	9	3.2	12	2.9	23	13.4	2	·	·	7	·	·	·	1	4	6	3	1	15	·	1
XI	0.5	9.0	13.5	3.4	10	4.4	9.5	5.1	16	4.7	23	5.3	7.5	3.4	3	3.3	7	4.2	36	9.7	1	7	12	20	·	1	·	1	14	17	10	·	7	15	·
XII	0.5	4.0	·	·	0.5	4.0	13	5.8	23	6.2	37	5.7	10	5.0	4	2.6	5	5.3	55	12.4	18	2	5	21	·	2	·	·	25	23	11	2	7	18	·
Rok	37	4.4	90.5	3.8	88.5	3.6	110.5	4.0	193	4.3	258	4.5	153	4.0	91.5	4.1	73	4.0	600	35.4	9. V	24	55	130	11	9	·	19	151	182	112	13	71	99	22

Uwaga. Kierunki i prędkości wiatru – wg anemetru M – 47.

Śliwice $H_s = 115$ m $h_w = 11$ m

I	2.5	1.4	9	2.7	3	2.0	20.5	1.8	13	2.3	29.5	2.4	6	5.2	8.5	2.2	1	2.4	26	5.5	8	3	10	28	·	1	·	·	19	12	8	·	4	7	·
II	8	2.9	17.5	4.1	3.5	2.1	5	1.0	6.5	1.6	20	3.2	14	3.5	7.5	3.5	2	3.1	43	12.4	8	8	17	27	·	·	·	·	13	17	11	1	·	28	·
III	2	3.5	11.5	2.9	2.5	1.4	13.5	1.8	16	1.8	21.5	2.2	10	2.9	7	2.1	9	2.0	46	15.0	3	7	9	23	·	·	·	4	10	10	9	1	6	19	·
IV	4	2.5	8	3.6	14.5	2.7	29	2.2	5.5	1.8	13	1.9	7	2.0	4	2.8	5	2.2	44	9.3	25	·	·	9	·	·	·	2	16	14	9	·	2	·	·
V	9.5	2.3	15	3.3	19.5	2.5	13	2.6	8.5	1.8	8.5	2.4	9.5	3.5	6.5	2.3	3	2.5	51	15.0	9	·	·	5	·	3	·	1	11	10	10	1	·	·	·
VI	3	1.7	14	2.6	13	2.6	5.5	2.9	11.5	2.4	21	2.5	16	3.8	6	3.0	·	2.8	55	16.9	1	·	·	·	5	2	·	2	7	8	7	2	·	·	3
VII	4	2.5	7.5	2.9	3.5	2.3	8	1.9	10	2.2	47.5	3.3	10.5	3.6	1	3.0	1	3.0	136	—	—	·	·	·	3	1	·	2	9	20	16	4	·	·	11
VIII	1	2.0	2	1.0	1	1.0	8	2.8	6	1.6	31	1.7	19.5	2.2	12.5	2.4	10	1.8	71	25.7	24	·	·	·	7	·	·	·	8	13	8	3	1	·	2
IX	·	·	3	2.3	5	1.2	19	1.9	16.5	2.2	28.5	2.3	4	2.2	5	2.6	9	1.9	78	25.4	6	·	·	·	1	·	·	5	5	10	8	3	6	·	2
X	3	1.3	7	1.6	5	1.6	9	1.0	9	1.3	29	2.0	12.5	1.9	7.5	2.1	11	1.5	13	6.0	16	·	·	4	·	1	·	2	5	6	3	·	10	·	·
XI	1	1.0	20	2.5	10	1.9	12.5	3.4	14.5	3.6	25	3.3	4	3.5	1	4.0	2	2.9	49	13.6	21	7	13	21	·	4	·	1	18	14	9	2	3	15	·
XII	1	1.0	3	1.0	·	·	10.5	3.8	19	3.6	47.5	4.3	8	2.4	1	5.0	3	3.7	35	9.2	5	3	7	24	·	3	·	·	23	15	9	·	4	14	·
Rok	39	1.8	117.5	2.5	80.5	1.8	153.5	2.3	138	2.2	322	2.6	121	3.1	67.5	2.9	56	2.5	646	—	—	28	56	141	16	15	·	19	144	143	107	17	36	83	18

Chojnice $H_s = 172$ m $H_b = 177{,}2$ m $h_w =$ 14,2 m anemometr I-VI, IX-XII; 12,5 m wiatromierz Wilda

I	7	2.5	6	3.2	9	3.0	13	3.3	16.5	4.2	22.5	5.3	11	5.7	8	3.9	1	4.1	27	4.7	30	3	12	27	·	2	·	1	19	19	10	·	9	22	·
II	9	4.6	9	4.8	2.5	2.8	3	1.7	5.5	1.8	14.5	5.0	21.5	5.2	18	6.3	1	4.7	17	2.6	13	13	21	27	·	7	·	·	12	21	7	·	4	28	·
III	6.5	3.1	9	4.2	7	2.8	10	2.5	14	2.1	18	2.4	15	4.2	10.5	3.5	5	2.9	39	15.5	3	5	11	24	·	1	·	5	13	15	7	1	13	25	·
IV	4.5	3.3	9.5	3.9	22	3.6	24.5	3.3	5	4.2	5.5	4.3	9.5	4.4	7.5	4.2	2	3.7	31	5.7	23	·	·	6	·	2	·	·	16	15	11	·	6	·	1
V	9	3.3	15.5	3.2	18.5	3.3	11.5	3.9	9	3.3	5	3.5	11	4.7	16.5	4.3	3	3.6	51	21.3	9	·	·	3	·	2	·	3	15	17	10	1	3	·	·
VI	7	2.5	9.5	3.4	11.5	2.7	7	3.3	8.5	4.2	7.5	3.1	21	4.5	15	3.4	3	3.4	53	12.3	22	·	·	·	2	2	·	2	12	12	8	2	·	·	3
VII	3	3.5	8.5	3.4	3	3.7	5	3.2	4.5	3.2	23.5	4.9	31.5	4.7	4	3.5	10	3.8	123	28.0	15	·	·	·	2	1	·	2	11	20	17	4	1	·	7
VIII	5.5	1.7	·	·	4.5	2.2	5	3.7	3.5	3.9	9	2.7	19.5	2.4	19	2.6	27	1.8	56	14.6	24	·	·	·	4	·	·	1	9	14	11	2	3	·	3
IX	2.5	4.8	5.5	3.3	4	3.8	10.5	3.9	14	3.0	13	3.3	24.5	4.7	10	3.2	6	3.5	60	11.2	6	·	·	·	1	1	·	4	10	14	8	1	5	·	1
X	15	2.5	7	2.1	7	2.5	5	2.0	4	2.0	16.5	3.3	24.5	5.1	12	3.1	4	3.2	21	5.4	16	·	·	3	·	1	·	2	9	11	5	·	15	·	·
XI	2.5	6.4	4	3.1	22	3.1	10.5	3.9	9	5.1	10.5	5.4	24	7.0	7.5	4.3	·	4.8	40	13.0	21	7	13	22	·	5	1	1	15	19	8	1	6	16	·
XII	1	4.0	2	2.2	1	2.5	5.5	6.0	13.5	5.4	21	7.3	38.5	7.1	8.5	3.1	1	6.3	35	6.8	18	3	8	24	·	11	1	·	26	20	10	·	10	19	·
Rok	72.5	3.5	85.5	3.1	112	3.0	108.5	3.5	100	3.5	164.5	4.2	251.5	5.0	132.5	3.9	63	3.8	553	28.0	16.VII	31	66	136	9	35	2	21	167	197	112	12	75	110	15

Uwaga. Kierunki i prędkości wiatru: VII – VIII – wg wiatromierza Wilda, w pozostałych miesiącach – wg anemometru M – 47.

Ostróda — φ = 53°42' — λ = 19°58' — 1965

MIESIĄC	CIŚNIENIE p: P_m	Max	Min	$P_{o.m}$	TEMPERATURA T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	—	—	—	—	0.8	−4.1	4.4	1	−17.9	11	−1.9	−0.5	−1.9	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.2	7.1	7.6
II	—	—	—	—	−2.2	−9.8	1.4	12, 13	−23.2	6	−7.0	−3.5	−5.8	−5.5	—	—	—	—	—	—	—	—	—	—	—	—	7.1	5.6	6.5	6.4
III	—	—	—	—	3.1	−5.4	8.2	15, 19, 29	−23.4	8	−3.9	2.1	−1.3	−1.1	—	—	—	—	—	—	—	—	—	—	—	—	5.5	4.8	5.8	5.4
IV	—	—	—	—	9.1	2.0	14.8	30	−2.5	1, 3	3.2	8.0	5.3	5.4	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.8	6.6	6.7
V	—	—	—	—	13.6	4.4	20.3	18	−3.0	4	7.5	12.3	8.4	9.2	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.6	4.9	5.4
VI	—	—	—	—	20.5	10.5	29.0	26	5.3	8	14.2	19.0	14.8	15.7	—	—	—	—	—	—	—	—	—	—	—	—	5.4	4.9	5.6	5.3
VII	—	—	—	—	20.4	11.2	29.8	15	5.9	2	14.2	18.6	14.8	15.6	—	—	—	—	—	—	—	—	—	—	—	—	4.9	5.8	5.0	5.2
VIII	—	—	—	—	20.2	10.5	27.3	22	6.1	17	13.1	18.8	14.2	15.1	—	—	—	—	—	—	—	—	—	—	—	—	6.3	7.1	5.2	6.2
IX	—	—	—	—	19.6	9.8	26.8	3	4.9	16	11.5	18.3	13.4	14.2	—	—	—	—	—	—	—	—	—	—	—	—	4.7	4.3	3.2	4.1
X	—	—	—	—	11.5	4.6	19.8	1	−2.0	21	5.6	10.6	7.6	7.8	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.2	5.9	6.3
XI	—	—	—	—	0.5	−4.3	10.8	2	−18.4	24	−2.5	−0.7	−2.1	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.7	7.2	7.7
XII	—	—	—	—	1.4	−2.4	9.2	19, 20	−14.8	17	−0.8	0.2	−0.3	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.7	7.5	7.8
Rok	—	—	—	—	9.9	2.2	29.8	15, VII	−23.4	8. III	4.4	8.6	5.6	6.0	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.1	5.9	6.2

Trzebież — φ = 53°40' — λ = 14°31'

MIESIĄC	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	2.9	−1.5	8.9	17	−9.6	31	0.3	1.8	0.8	0.9	5.8	6.0	5.8	5.9	91	86	90	89	0.5	1.0	0.7	0.7	8.2	8.6	7.1	8.0
II	—	—	—	—	0.9	−4.8	5.3	13	−15.2	28	−2.6	−0.4	−1.3	−1.4	4.6	5.0	4.8	4.8	88	83	84	85	0.6	1.0	0.9	0.8	8.1	8.3	6.5	7.6
III	—	—	—	—	5.2	−3.3	15.3	29	−18.3	8	−1.6	3.2	1.0	0.9	5.3	6.1	5.8	5.7	91	77	85	84	0.6	2.0	1.1	1.2	6.5	5.8	4.1	5.5
IV	—	—	—	—	11.1	2.8	15.5	6	−3.0	5	4.8	9.1	6.6	6.8	7.8	7.8	7.9	7.8	89	69	81	80	1.0	3.9	2.0	2.3	8.1	8.2	5.9	7.4
V	—	—	—	—	14.5	5.7	20.4	17	0.1	3	8.8	13.0	10.1	10.5	9.6	10.2	10.4	10.1	83	68	83	78	1.9	4.9	2.2	3.0	5.5	6.3	6.1	6.0
VI	—	—	—	—	20.6	10.5	28.6	26	5.7	3	14.6	18.9	15.4	16.1	13.0	13.8	13.6	13.5	77	63	77	72	3.8	8.6	4.1	5.5	4.5	5.8	4.6	5.0
VII	—	—	—	—	19.3	10.6	25.2	13	5.9	11	13.7	17.2	14.0	14.7	13.5	14.3	13.8	13.9	85	73	85	81	2.3	5.6	2.4	3.4	7.3	7.9	6.0	7.1
VIII	—	—	—	—	20.0	9.9	27.4	22	5.6	13	13.0	18.3	15.0	15.3	13.9	14.7	14.1	14.2	91	70	82	81	1.3	6.6	3.2	3.7	5.3	5.4	4.4	5.0
IX	—	—	—	—	19.2	9.8	25.4	3	5.6	30	11.8	18.1	13.1	14.0	12.6	13.8	13.1	13.2	91	67	87	82	1.4	7.3	2.1	3.6	6.1	6.2	4.2	5.5
X	—	—	—	—	13.2	3.7	21.4	1	−3.4	23	6.0	11.8	7.8	8.4	9.0	10.7	9.6	9.8	94	77	89	87	0.6	3.4	1.2	1.7	6.6	5.2	3.7	5.2
XI	—	—	—	—	3.1	−2.3	13.1	1	−10.9	23	−0.4	2.0	0.1	0.4	5.7	5.8	5.8	5.8	90	78	88	85	0.6	1.6	0.7	1.0	7.2	7.4	6.2	6.9
XII	—	—	—	—	3.6	−0.9	11.4	19	−6.0	13	1.1	2.2	1.3	1.5	5.8	6.3	6.0	6.0	86	86	88	87	0.9	1.1	0.8	0.9	8.5	8.9	7.5	8.3
Rok	—	—	—	—	11.1	3.4	28.6	26. VI	−18.3	8. III	5.8	9.6	7.0	7.4	8.9	9.5	9.2	9.2	88	75	85	83	1.3	3.9	1.8	2.3	6.8	7.0	5.5	6.4

Nowogard — φ = 53°40' — λ = 15°07'

MIESIĄC	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	—	−2.2	—	—	−13.9	31	−0.5	1.4	0.0	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.3	7.6	8.2
II	—	—	—	—	0.4	−5.6	4.2	13	−16.6	28	−3.8	−0.8	−2.7	−2.5	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.0	7.6	8.1
III	—	—	—	—	4.5	−4.1	14.7	29	−17.3	8	−2.4	3.0	−0.4	0.0	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.2	5.4	6.1
IV	—	—	—	—	11.2	2.3	16.2	6	−4.0	5	4.4	9.8	6.0	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.7	5.9	7.1
V	—	—	—	—	14.7	5.3	20.5	17	−1.5	3	8.4	13.5	9.3	10.1	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.2	6.5	6.5
VI	—	—	—	—	21.3	9.9	28.7	26	4.0	4	14.9	19.8	14.8	16.1	—	—	—	—	—	—	—	—	—	—	—	—	5.0	6.1	5.5	5.5
VII	—	—	—	—	19.6	10.6	29.2	14	7.0	5, 10	13.8	18.3	13.7	14.9	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.7	6.6	6.7
VIII	—	—	—	—	20.8	10.0	28.7	22	5.0	31	13.5	19.6	13.9	15.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.2	5.0	5.7
IX	—	—	—	—	19.4	9.7	26.2	3	5.5	30	11.5	18.8	12.6	13.9	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.8	4.6	5.5
X	—	—	—	—	13.2	3.5	21.7	1	−3.0	22	5.5	12.2	6.6	7.7	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.7	3.1	5.1
XI	—	—	—	—	2.5	−3.0	12.2	1	−13.3	23	−1.2	1.4	−0.9	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.5	6.4	7.0
XII	—	—	—	—	2.7	−1.1	11.2	19	−6.6	13	0.6	1.3	0.8	0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.3	8.1	8.3
Rok	—	—	—	—	—	2.9	29.2	14. VII	−17.3	8. III	5.4	9.9	6.1	6.9	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.8	6.0	6.6

Biebrza — φ = 53°39' — λ = 22°36'

MIESIĄC	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.4	−5.1	3.5	18	−14.5	11	−3.0	−1.7	−2.8	−2.6	4.8	5.0	4.8	4.9	93	90	92	92	0.3	0.5	0.4	0.4	9.0	7.2	7.3	7.8
II	—	—	—	—	−3.2	−13.1	2.0	17	−30.7	6	−9.1	−5.2	−7.8	−7.5	3.2	3.8	3.4	3.5	91	87	91	90	0.3	0.6	0.3	0.4	7.2	6.0	5.8	6.3
III	—	—	—	—	2.7	−6.5	9.3	28	−27.7	9	−4.5	1.5	−1.9	−1.7	4.6	5.4	5.1	5.0	92	77	90	86	0.4	1.7	0.6	0.9	6.5	5.2	5.8	5.8
IV	—	—	—	—	10.1	1.1	16.8	28	−5.8	3	3.4	8.6	4.8	5.4	6.8	6.5	6.6	6.6	85	58	77	73	1.2	5.1	2.1	2.8	6.9	7.0	6.6	6.8
V	—	—	—	—	13.5	2.8	20.7	18	−6.4	4	7.5	12.0	7.4	8.6	8.6	8.3	8.6	8.5	81	58	81	73	2.0	5.9	1.9	3.3	5.8	6.9	5.4	6.0
VI	—	—	—	—	20.1	8.9	27.2	26	−0.9	8	14.0	18.5	13.9	15.1	13.1	12.8	13.1	13.0	82	61	82	75	3.1	8.9	3.1	5.0	5.4	5.9	4.9	5.4
VII	—	—	—	—	20.6	9.1	28.9	16	1.7	5	14.5	19.2	14.3	15.6	13.6	12.8	13.5	13.3	82	57	82	74	3.0	10.0	3.2	5.4	4.4	6.4	6.2	5.7
VIII	—	—	—	—	20.4	8.9	27.4	7	2.3	31	12.7	18.7	13.0	14.4	13.3	13.3	13.5	13.4	90	63	89	81	1.6	9.0	1.9	4.2	5.4	5.7	4.3	5.1
IX	—	—	—	—	20.1	7.2	26.2	3	−0.4	21	10.4	19.1	11.9	13.3	12.0	12.7	12.4	12.4	94	58	88	80	0.9	9.9	1.9	4.2	5.0	4.4	3.3	4.2
X	—	—	—	—	11.2	2.0	18.6	1	−8.1	21	4.7	10.3	6.0	6.8	8.2	9.3	8.6	8.7	94	74	90	86	0.5	3.5	1.0	1.7	8.0	7.2	5.2	6.8
XI	—	—	—	—	−0.1	−5.6	11.0	2	−20.3	24	−3.4	−0.9	−2.8	−2.5	4.8	5.2	4.9	5.0	91	85	91	89	0.5	1.1	0.5	0.7	8.8	8.7	7.6	8.4
XII	—	—	—	—	0.9	−3.6	7.3	20	−15.5	17	−1.4	−0.2	−1.2	−1.0	5.2	5.5	5.2	5.3	93	90	91	91	0.4	0.7	0.6	0.6	9.3	8.1	7.7	8.4
Rok	—	—	—	—	9.7	0.5	28.9	16. VII	−30.7	6. II	3.8	8.3	4.6	5.3	8.2	8.4	8.3	8.3	89	72	87	83	1.2	4.7	1.5	2.5	6.8	6.6	5.8	6.4

Ostróda

$H_s = 106$ m $h_w = 10$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	·	·	1	2.0	9.5	3.3	20.5	3.2	13	4.0	26.5	3.6	15	3.6	2.5	3.8	5	3.3	25	5.6	8	2	11	28	·	·	·	·	15	16	7	·	2	—	·
II	4.5	3.2	14.5	2.6	1	2.5	·	·	2.5	2.6	23	3.7	18.5	4.4	7	3.6	13	3.0	26	3.2	25	13	25	27	·	·	·	1	10	19	10	·	·	28	·
III	·	·	9	2.0	7	2.9	17.5	2.9	8	2.8	20.5	2.6	13	3.0	4	3.8	14	2.3	36	14.0	3	6	10	24	·	·	·	6	9	9	8	1	4	20	·
IV	0.5	2.0	3	4.3	21.5	3.9	29	4.0	6	3.0	9.5	2.8	5.5	2.1	10	2.8	5	3.3	34	6.4	19	·	·	7	·	·	·	3	14	12	8	·	1	·	1
V	3	3.0	7	2.9	13.5	2.7	12.5	2.8	6	3.5	14.5	2.9	8	3.4	23.5	3.2	5	2.9	32	7.8	19	·	·	2	·	·	·	5	7	12	9	·	2	·	·
VI	2.5	3.0	5	2.6	12	3.2	13	3.9	5	4.6	15	4.1	17.5	3.7	15	3.5	5	3.4	47	16.4	22	·	·	·	3	·	·	2	7	14	8	1	·	·	1
VII	·	·	3	2.0	4.5	3.7	9.5	2.2	6	2.5	40.5	3.5	18	3.8	1.5	2.0	10	2.9	95	14.6	16	·	·	·	2	·	·	3	4	15	14	2	1	·	8
VIII	1	2.0	·	·	1	2.0	15	3.3	3.5	2.4	17	2.7	28	2.7	8.5	2.9	19	2.2	90	17.6	27	·	·	·	8	·	·	·	6	19	14	3	3	·	2
IX	·	·	2	4.5	3	3.5	18.5	3.2	12	3.0	21	3.6	20	3.2	2.5	2.2	11	2.9	73	28.4	29	·	·	·	1	·	·	9	3	10	10	2	1	·	·
X	1	2.0	4	2.0	4	2.8	2	2.0	5	2.9	26	3.2	27	2.8	10	3.0	14	2.5	40	12.4	18	·	·	3	·	·	·	1	7	9	9	1	9	·	·
XI	·	·	9	2.7	11.5	2.5	16.5	4.1	7	3.0	26	3.6	11	3.9	6	2.0	3	3.2	42	12.4	1	7	15	20	·	·	·	1	15	18	11	1	4	—	·
XII	·	·	·	·	·	·	15	3.6	22	4.2	28.5	4.2	21.5	3.7	·	·	6	3.7	50	20.4	18	3	8	23	·	·	·	·	17	17	14	1	3	—	·
Rok	12.5	1.3	57.5	2.3	88.5	2.8	169	2.9	96	3.2	268	3.4	203	3.4	90.5	2.7	110	3.0	590	28.4	29.IX	31	69	134	14	·	·	31	114	170	122	12	30	—	12

Trzebież

$H_s = 1$ m $h_w = 18$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4	4.4	10.5	4.0	1	2.5	11	4.8	13	4.3	26.5	6.5	10.5	6.3	5.5	3.2	11	4.6	29	5.9	8	·	1	24	·	6	1	2	17	17	9	·	3	7	—
II	12	8.7	12	7.4	6	5.0	3.5	6.0	2.5	2.0	7	6.2	12	5.2	23	5.9	6	5.8	26	4.2	13	3	7	24	·	10	2	1	14	20	9	·	5	20	—
III	5	7.5	9.5	7.3	5.5	4.7	10.5	3.7	13.5	3.6	14	4.1	11.5	4.0	8.5	6.2	15	4.1	19	4.6	3	3	6	22	·	4	1	7	10	11	6	·	5	17	—
IV	9.5	7.5	12	6.5	12	5.5	19.5	5.9	10	5.4	1.5	6.0	11	5.0	9.5	4.8	5	5.5	54	10.3	25	·	·	3	·	6	·	1	13	16	12	1	3	·	—
V	16.5	6.7	11.5	6.6	6.5	5.6	18	5.1	7.5	5.5	5	4.8	5.5	6.5	17.5	6.1	5	5.6	81	30.0	10	·	·	·	·	6	2	7	13	17	11	2	·	·	—
VI	17	6.8	11	5.5	5.5	4.8	9.5	3.7	8.5	3.4	13	5.3	10.5	6.1	13	7.1	2	5.5	24	14.0	18	·	·	·	4	7	·	8	7	6	4	1	·	·	—
VII	5	6.3	9.5	6.9	0.5	2.0	6.5	5.0	5	2.9	31	5.8	24.5	6.1	9	7.1	2	5.8	73	15.0	12	·	·	·	2	8	·	3	11	21	15	1	2	·	—
VIII	12.5	5.2	7	4.6	·	·	10	2.9	8.5	3.4	14.5	4.3	11	4.6	19.5	4.2	10	3.8	46	10.0	23	·	·	·	3	1	·	5	4	12	8	1	2	·	—
IX	5.5	2.5	1.5	7.3	1	10.0	13	6.4	18	5.2	23.5	5.2	14.5	5.2	6	6.6	7	5.0	61	20.8	10	·	·	·	1	7	·	6	6	13	9	2	·	·	—
X	2	6.0	8.5	4.4	2	3.5	7	3.6	11	3.5	19.5	5.6	15.5	6.3	12.5	4.7	15	4.2	19	9.2	31	·	·	4	·	2	·	3	4	7	5	·	13	·	—
XI	2	7.8	6	5.9	16	6.0	6	7.3	13.5	5.7	19.5	7.8	15.5	7.3	3.5	7.3	8	6.2	30	6.0	29	3	9	16	·	9	1	3	14	15	6	·	4	14	—
XII	2	4.0	·	·	·	·	7	6.7	17	7.0	38	7.2	20	6.3	7	5.4	2	6.6	57	13.6	9	·	3	19	·	9	1	1	19	19	12	2	·	6	—
Rok	93	6.1	99	5.5	56	4.1	121.5	5.1	128	4.3	213	5.7	162	5.7	134.5	5.7	88	5.2	519	30.0	10.V	9	26	112	10	75	8	47	132	174	106	10	37	64	—

Nowogard

$H_s = 60$ m $h_w = 11$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	1.0	3	1.0	3	2.3	5.5	2.8	35.5	6.2	11	4.9	9	3.4	3	3.7	21	3.7	54	9.4	8	1	—	26	·	8	2	·	18	15	14	·	4	7	·
II	11	3.7	9	3.6	6	2.7	3	2.7	6	6.3	8	1.6	21	3.1	5	3.2	15	2.7	47	6.5	28	4	9	26	·	3	1	·	15	18	15	·	1	28	·
III	6	5.2	5	4.2	5	3.2	6	2.0	32	1.8	2	1.5	15	1.6	4	4.5	18	1.9	40	19.3	3	3	6	23	·	1	·	7	10	13	8	1	4	19	·
IV	12	1.9	1	1.0	16	2.6	9	2.9	28.5	3.5	1.5	1.7	12	2.7	4	2.2	6	2.6	43	8.7	19	·	·	3	·	·	·	2	12	16	11	·	·	·	1
V	23	2.5	6.5	1.3	2	2.0	12.5	3.3	16.5	4.6	2	3.8	13	2.4	7.5	3.3	10	2.7	81	19.8	9	·	·	1	·	3	1	4	11	16	12	3	·	·	3
VI	11.5	2.1	8.5	3.6	6	1.8	5	1.8	15.5	2.8	8.5	4.5	15	2.9	8	2.6	12	2.5	44	9.3	18	·	·	·	5	·	·	7	8	9	7	·	·	·	5
VII	3	3.0	6	2.3	3	1.0	5	3.4	23	2.1	22	3.7	24	3.4	·	·	7	2.7	122	28.1	14	·	·	·	4	·	·	3	12	21	20	2	1	·	7
VIII	10	1.6	·	·	2	1.0	2	3.0	22.5	1.5	4.5	1.4	16	1.8	5	1.8	31	1.1	51	12.7	8	·	·	·	4	·	·	3	5	8	7	2	2	·	1
IX	2.5	1.0	·	·	3	5.7	7	2.8	39.5	3.1	12.5	3.2	6	2.2	1.5	1.7	18	2.4	127	32.4	6	·	·	·	1	1	·	6	5	11	11	4	1	·	4
X	9.5	1.4	·	·	3	1.0	3.5	1.3	30.5	2.4	7	3.4	5	1.0	2.5	1.6	32	1.4	18	7.0	29	·	·	5	·	·	·	4	3	5	4	·	9	·	1
XI	·	·	·	·	20	1.6	9	2.1	29.5	6.1	9.5	4.7	4	3.8	2	2.0	16	3.3	55	13.0	1	4	10	19	·	5	1	3	13	16	12	1	6	10	·
XII	·	·	·	·	3	1.0	10	4.3	31	7.4	17	5.5	21	3.2	5	1.8	6	4.8	100	22.0	18	·	3	21	·	9	3	2	21	21	20	3	1	8	·
Rok	90.5	2.0	39	1.4	72	2.2	77.5	2.7	310	4.0	105.5	3.3	161	2.6	47.5	2.4	192	2.6	782	32.4	6.IX	12	—	124	14	30	8	41	133	169	141	16	29	72	22

Biebrza

$H_s = 117$ m $h_w = 13$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5	2.6	4	3.8	9	5.3	17.5	3.9	22	4.5	13	5.8	4	8.8	6.5	8.8	12	4.4	27	5.1	30	5	12	29	·	3	·	2	20	13	8	·	4	17	·
II	10.5	4.3	13	5.8	2	7.0	2	1.5	6.5	3.3	17	5.2	17	4.9	8	4.7	8	4.4	9	3.5	7	18	23	26	·	2	·	3	11	15	2	·	·	28	·
III	3	4.7	3.5	3.3	6.5	4.2	8.5	3.7	18.5	3.6	19	2.6	13.5	4.6	4.5	6.3	16	3.1	29	7.3	20	8	7	26	·	·	·	5	12	12	7	·	3	20	·
IV	4	5.8	4.5	6.3	23	8.2	27	5.2	11	3.6	6	3.0	3	3.0	6.5	4.4	5	5.3	28	11.4	26	·	·	14	·	5	·	4	15	7	6	1	1	·	1
V	12	3.8	11	3.0	11	5.1	9	3.8	7	2.3	8.5	4.2	10.5	3.3	9	3.6	15	3.1	78	25.7	19	·	·	7	·	1	·	5	11	15	11	2	1	·	1
VI	8	3.4	5	4.4	15.5	4.4	5.5	3.5	8	3.9	13.5	4.1	15	4.8	7.5	3.7	12	3.6	50	17.8	13	·	·	1	2	1	·	3	6	11	10	1	·	·	2
VII	1.5	1.7	6	4.7	4.5	4.1	7	3.1	16.5	2.8	33	4.4	14.5	4.4	·	·	10	3.5	94	26.0	31	·	·	·	4	·	·	3	8	13	11	2	1	·	5
VIII	5	3.2	2	3.0	1.5	1.0	6.5	4.0	10.5	3.6	8	3.2	17	2.9	15.5	3.1	27	2.3	56	11.9	27	·	·	·	4	·	·	6	7	12	8	2	1	·	2
IX	0.5	5.0	·	·	3	3.3	11	3.7	25	3.7	20	3.3	16	3.7	2.5	2.2	14	3.0	39	26.0	29	·	·	1	2	·	·	7	3	10	6	1	1	·	·
X	6	2.2	2	4.0	3	4.7	2	4.5	6	2.7	20.5	3.8	23	3.3	16.5	3.4	14	2.9	14	5.8	16	·	·	6	·	·	·	3	12	9	5	·	3	·	·
XI	1	3.0	8.5	4.6	17	3.4	6.5	5.2	14.5	4.6	16.5	3.1	18.5	3.5	3.5	4.1	4	4.0	32	7.6	30	7	16	23	·	1	·	·	21	14	7	·	·	16	·
XII	·	·	·	·	·	·	10.5	3.9	19.5	4.2	40	4.6	16	3.2	1	6.0	6	3.9	32	7.5	19	4	10	28	·	2	·	·	20	14	[illegible]	·	·	24	·
Rok	56.5	3.3	59.5	3.6	96	4.2	113	3.8	163	3.6	215	4.1	168	4.2	81	4.2	143	3.6	488	26.0	31.VII, 29.IX	40	68	161	12	15	·	41	146	145	90	9	15	105	11

Pisz — φ = 53°38' — λ = 21°48' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.1	−4.8	3.4	18	−17.2	11	−3.0	−1.3	−2.7	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.4	8.3	8.6
II	—	—	—	—	−2.6	−11.2	1.7	15	−29.7	6	−8.2	−4.2	−6.7	−6.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.1	8.2	7.8
III	—	—	—	—	3.9	−5.4	9.7	28	−25.7	9	−3.5	2.8	−1.2	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.1	5.9	7.3	6.8
IV	—	—	—	—	10.3	1.7	17.6	28	−4.6	3	3.6	8.7	5.2	5.7	—	—	—	—	—	—	—	—	—	—	—	—	7.5	8.6	8.6	8.2
V	—	—	—	—	14.0	3.6	21.1	18	−6.6	4	7.5	12.6	8.5	9.3	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.4	7.0	7.1
VI	—	—	—	—	20.9	9.6	29.9	26	0.4	8	14.4	19.2	14.7	15.8	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.3	6.6	6.5
VII	—	—	—	—	21.5	10.3	31.9	15	3.2	11	14.4	19.8	14.6	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.2	7.0	6.2
VIII	—	—	—	—	21.0	9.7	28.2	22	4.3	31	12.7	19.4	13.5	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.8	5.5	6.0
IX	—	—	—	—	20.9	8.3	27.7	3	2.4	21	11.1	19.6	12.6	14.0	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.9	5.2	5.9
X	—	—	—	—	12.1	3.1	20.6	1	−5.5	21	5.3	11.1	6.6	7.4	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.5	7.3	7.8
XI	—	—	—	—	0.4	−5.0	10.6	2	−21.2	24	−3.1	−0.5	−2.6	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.8	8.8	9.0
XII	—	—	—	—	1.2	−3.2	8.1	19	−17.5	17	−1.2	0.1	−0.9	−0.7	—	—	—	—	—	—	—	—	—	—	—	—	9.1	9.0	9.2	9.1
Rok	—	—	—	—	10.3	1.4	31.9	15.VII	−29.7	6.II	4.2	8.9	5.1	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.3	7.4	7.4

Różanystok — φ = 53°38' — λ = 23°24'

I	—	—	—	—	−0.8	−5.4	2.6	18	−14.5	11	−3.5	−2.4	−3.3	−3.1	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.6	6.7	7.6
II	—	—	—	—	−3.9	−12.0	1.1	14	−25.5	6	−8.8	−6.2	−7.9	−7.7	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.7	5.0	6.6
III	—	—	—	—	2.1	−5.3	8.1	28	−23.0	8	−3.7	0.8	−1.6	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	7.2	5.3	5.1	5.9
IV	—	—	—	—	9.3	1.3	16.7	27	−4.8	3	2.8	8.0	4.8	5.1	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.8	5.9	5.8
V	—	—	—	—	13.2	3.6	20.1	18	−3.3	4	6.9	11.5	8.1	8.6	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.6	5.7	6.0
VI	—	—	—	—	19.9	10.4	27.0	26	3.2	8	13.5	18.1	14.5	15.2	—	—	—	—	—	—	—	—	—	—	—	—	5.1	5.5	4.6	5.1
VII	—	—	—	—	20.8	10.9	29.5	16	6.4	11	14.3	19.0	15.1	15.9	—	—	—	—	—	—	—	—	—	—	—	—	4.1	6.6	6.3	5.7
VIII	—	—	—	—	20.4	10.5	27.4	25	4.6	31	12.7	19.0	14.2	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.3	4.5	5.1
IX	—	—	—	—	20.4	9.1	26.9	4	3.6	21	10.9	19.2	13.0	14.0	—	—	—	—	—	—	—	—	—	—	—	—	4.8	4.7	3.3	4.3
X	—	—	—	—	11.0	3.6	19.0	1	−2.1	21	5.0	10.0	6.5	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.0	5.9	6.9
XI	—	—	—	—	−0.4	−5.1	11.0	2	−16.5	17, 19	−3.2	−1.5	−2.9	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.7	8.1	8.1
XII	—	—	—	—	0.7	−3.6	6.7	20	−11.8	17, 18	−1.7	−0.7	−1.2	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	7.9	8.0	8.2	8.0
Rok	—	—	—	—	9.4	1.5	29.5	16.VII	−25.5	6.II	3.8	7.9	4.9	5.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.4	5.8	6.3

Szczytno — φ = 53°34' — λ = 27°02'

I	—	—	—	—	0.0	−5.2	3.6	9, 18	−22.7	11	−3.0	−1.1	−2.7	−2.4	4.7	4.8	4.5	4.7	90	83	87	87	0.5	0.9	0.7	0.7	9.1	8.4	6.7	8.1
II	—	—	—	—	−2.6	−11.5	1.4	13	−29.4	6	−7.6	−4.0	−6.8	−6.3	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.5	6.5	6.8
III	—	—	—	—	3.7	−6.2	9.2	28	−26.3	8	−3.7	2.8	−1.9	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.5	5.8	6.0
IV	—	—	—	—	9.8	1.1	16.2	28	−5.4	3	3.7	8.6	4.5	5.3	6.7	6.8	6.6	6.7	82	61	76	73	1.5	4.6	2.1	2.7	7.3	7.4	5.7	6.8
V	—	—	—	—	13.7	3.1	19.8	18	−6.3	4	8.0	12.7	6.7	8.5	8.7	8.2	8.3	8.4	78	56	82	72	2.3	6.7	1.8	3.6	6.3	6.6	4.2	5.7
VI	—	—	—	—	20.6	9.0	29.0	26	1.5	8	14.9	19.2	13.4	15.2	12.8	12.1	12.6	12.5	76	56	81	71	4.3	10.7	3.1	6.0	4.9	5.4	5.3	5.2
VII	—	—	—	—	20.7	9.3	30.3	15	1.8	5	14.7	19.3	13.5	15.2	13.7	13.2	13.4	13.4	81	60	86	76	3.4	9.8	2.4	5.2	4.3	6.6	5.4	5.4
VIII	—	—	—	—	21.0	9.2	28.5	22	2.8	31	13.8	19.5	14.6	15.6	14.0	14.0	13.9	14.0	88	63	84	78	2.1	9.7	3.3	5.0	6.1	6.4	4.6	5.7
IX	—	—	—	—	20.0	7.5	28.5	3	2.8	16, 21	10.2	18.8	12.1	13.3	11.7	13.7	12.9	12.8	92	63	90	82	1.0	8.6	1.6	3.7	5.6	5.1	3.5	4.7
X	—	—	—	—	11.6	2.4	20.3	1	−6.1	21	4.6	10.8	6.2	7.0	7.9	10.1	8.9	8.7	86	77	92	85	1.0	3.2	0.7	1.6	6.6	5.6	5.7	6.0
XI	—	—	—	—	−0.3	−5.4	10.2	2	−24.0	24	−3.1	−1.0	−2.8	−2.4	4.6	5.1	4.8	4.8	87	83	86	85	0.6	1.0	0.7	0.8	8.2	7.4	6.6	7.4
XII	—	—	—	—	1.0	−3.3	8.6	20	−18.5	17	−1.1	−0.5	−1.2	−1.0	5.1	5.3	5.2	5.2	88	87	89	88	0.7	0.7	0.6	0.7	9.0	7.7	6.9	7.9
Rok	—	—	—	—	9.9	0.8	30.3	15.VII	−29.4	6.II	4.3	8.8	4.6	5.6	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.6	5.6	6.3

Szczuczyn — φ = 53°34' — λ = 22°17'

I	—	—	—	—	−0.4	−4.8	3.5	9	−13.1	11	−2.7	−1.5	−2.6	−2.4	4.7	4.8	4.7	4.7	90	86	90	89	0.5	0.7	0.5	0.6	8.7	7.7	6.9	7.8
II	—	—	—	—	−3.1	−12.3	1.4	17	−30.0	6	−8.6	−4.8	−7.1	−6.9	3.3	3.7	3.5	3.5	88	81	88	86	0.4	0.8	0.4	0.5	7.2	7.4	6.3	7.0
III	—	—	—	—	2.3	−5.7	8.7	30	−26.1	9	−4.0	1.4	−1.7	−1.5	4.4	5.2	4.9	4.8	89	77	85	84	0.6	1.8	0.8	1.1	7.8	6.0	5.5	6.4
IV	—	—	—	—	9.8	1.6	17.0	30	−3.9	3	3.5	8.5	4.9	5.4	6.8	6.8	7.0	6.9	84	61	79	75	1.3	4.7	1.9	2.6	7.9	8.0	7.0	7.6
V	—	—	—	—	13.5	3.6	20.6	18	−4.3	4	7.4	12.1	8.1	8.9	8.7	8.8	8.8	8.8	82	59	77	73	1.8	5.9	2.2	3.3	7.0	7.8	5.9	6.9
VI	—	—	—	—	20.3	9.5	27.1	26	1.6	8	14.2	18.8	14.6	15.6	13.2	12.8	13.2	13.1	81	60	79	73	3.1	9.3	3.6	5.3	6.1	7.1	6.4	6.5
VII	—	—	—	—	20.7	9.9	30.8	16	4.4	5, 11	14.6	19.3	14.4	15.7	13.6	12.7	13.8	13.4	81	57	84	74	3.2	10.3	2.8	5.4	5.8	7.8	6.9	6.8
VIII	—	—	—	—	20.2	9.7	27.1	7	4.0	17	12.8	18.9	13.3	14.6	13.4	13.0	13.5	13.3	90	60	88	79	1.5	9.6	2.1	4.4	6.5	6.6	4.8	6.0
IX	—	—	—	—	20.0	7.9	26.4	3	1.9	21	10.5	18.9	12.1	13.4	12.2	13.2	12.7	12.7	95	61	89	82	0.7	9.0	1.7	3.8	6.5	5.9	3.4	5.3
X	—	—	—	—	11.1	3.4	19.3	1	−5.4	21	5.0	10.1	6.6	7.1	8.3	9.4	8.9	8.9	93	75	89	86	0.6	3.2	1.1	1.6	8.3	7.8	5.8	7.3
XI	—	—	—	—	−0.1	−5.6	10.5	1	−22.6	24	−3.5	−1.0	−2.8	−2.5	4.8	5.1	4.9	4.9	90	85	90	88	0.5	1.1	0.6	0.7	8.7	9.0	8.2	8.6
XII	—	—	—	—	0.9	−3.1	7.6	20	−15.6	17	−1.4	−0.5	−0.9	−0.9	5.2	5.2	5.2	5.2	91	87	89	89	0.5	0.8	0.6	0.6	9.5	8.6	8.4	8.8
Rok	—	—	—	—	9.6	1.2	30.8	16.VII	−30.0	6.II	4.0	8.4	4.9	5.6	8.2	8.4	8.4	8.3	88	71	86	82	1.2	4.8	1.5	2.5	7.5	7.5	6.3	7.1

Pisz $H_s = 118\ m$ $h_w = 14\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v V≥10	V≥15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	12	2.5	5	1.6	18	1.9	12	2.2	26	2.1	8	2.8	9	3.4	3	2.7	·	2.3	48	8.3	23	3	13	27	·	·	·	·	21	18	12	·	—	24	·
II	18	2.7	13	2.9	5	2.0	4	1.5	5	1.6	5	4.4	28	3.4	6	2.5	·	2.9	35	6.4	7	13	22	26	·	·	·	1	17	19	12	·	—	28	·
III	6	1.7	6	1.7	17	1.4	9	1.9	27	2.0	2	1.6	19	1.6	6	3.8	1	1.8	29	6.3	20	7	8	22	·	·	·	1	13	15	6	·	—	21	·
IV	12	1.8	1	1.0	34	3.0	17	2.9	15	2.8	1	2.0	4	2.5	6	1.7	·	2.6	35	14.0	27	·	·	11	·	·	·	·	19	10	6	1	—	·	1
V	29	2.0	13	1.3	25	1.9	4	2.0	9	1.8	1	3.0	7	2.7	5	2.2	·	1.9	76	23.7	19	·	·	5	·	·	·	2	13	12	7	3	—	·	1
VI	20	1.9	13	2.2	12	2.4	6	1.3	7	2.3	4	1.5	16	2.1	11	1.5	1	2.0	43	11.5	12	·	·	·	3	·	·	3	11	11	8	1	—	·	1
VII	8	1.2	11	1.9	13.5	1.2	3.5	1.6	8	1.5	10.5	2.7	37.5	2.2	1	1.0	·	1.9	85	17.5	22	·	·	·	6	·	·	3	10	14	12	3	—	·	7
VIII	27.5	1.8	6.5	1.0	4	1.6	13	1.6	5.5	1.9	4.5	1.9	15.5	1.8	12.5	1.6	4	1.6	74	24.0	26	·	·	·	9	·	·	4	8	11	10	3	—	·	4
IX	2.5	1.6	0.5	2.0	13	1.3	12.5	1.8	14.5	1.8	10.5	1.8	30.5	1.9	1	1.0	5	1.6	50	29.8	29	·	·	·	4	·	·	2	5	10	7	1	—	·	1
X	24.5	1.5	1	1.0	2.5	1.4	3.5	1.9	2	1.0	1.5	1.7	45	2.1	10	1.4	3	1.8	15	8.2	16	·	·	5	·	·	·	·	17	8	3	·	—	·	·
XI	5	1.4	4	1.2	17.5	2.2	6.5	2.7	15	2.1	5	2.7	24	2.8	5	1.2	8	2.1	49	9.6	21	7	15	22	·	·	·	·	21	13	11	·	—	16	·
XII	3.5	1.1	·	·	1	1.0	8.5	2.3	22	2.4	9.5	1.9	37	2.4	10.5	1.1	1	2.1	49	9.6	3	3	9	24	·	·	·	·	26	20	13	·	—	25	·
Rok	168	1.8	74	1.5	162.5	1.8	99.5	2.0	156	1.9	62.5	2.3	272.5	2.4	77	1.8	23	2.0	588	29.8	29.IX	33	67	142	22	·	·	16	181	161	107	12	—	114	15

Różanystok $H_s = 160\ m$ $h_w = 12\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8	6.2	7	3.6	14.5	4.2	6	5.0	22.5	5.6	16	6.7	3	6.2	6	12.0	10	5.3	21	5.4	20	3	16	29	·	5	2	2	15	—	5	·	6	16	·
II	15	5.3	10	5.2	1	4.0	·	·	8	4.8	17.5	8.5	21.5	6.2	6	5.3	5	5.8	14	3.2	24	17	23	28	·	8	1	3	9	—	4	·	2	28	·
III	4.5	3.6	2.5	3.2	2	4.0	14	4.1	21.5	4.3	14.5	5.4	11	5.5	7	5.3	16	3.9	30	5.9	2	5	9	24	·	1	1	4	12	—	7	·	6	22	·
IV	3.5	6.7	15.5	4.1	17	3.7	26.5	4.3	14.5	3.2	1.5	5.0	1	3.0	6.5	4.8	4	3.9	14	7.8	23	·	·	13	·	1	·	6	9	—	4	·	·	1	·
V	18	5.4	10.5	3.9	7.5	2.9	3.5	2.3	10	3.2	7	4.5	9	3.4	9.5	4.5	18	3.3	79	24.6	29	·	·	3	·	1	·	5	10	—	12	2	1	·	2
VI	11.5	3.7	11.5	3.1	6	3.7	2	4.0	14	3.8	8	5.4	12	4.2	14	4.1	11	3.5	50	21.8	13	·	·	·	1	1	·	7	5	—	9	1	·	·	2
VII	8	2.2	9	2.0	1.5	2.7	3	1.7	8	3.1	28.5	4.4	24.5	5.6	5.5	5.0	5	3.9	89	19.4	31	·	·	·	3	3	·	2	8	—	12	4	·	·	4
VIII	19.5	3.4	0.5	3.0	1	1.0	5	3.2	17	3.3	4	2.2	20	4.4	18	3.6	8	3.3	55	25.0	2	·	·	·	5	3	·	7	7	—	9	2	1	·	2
IX	·	·	9	3.7	3.5	2.7	11.5	3.2	22	3.3	12	4.1	21	5.3	4	3.2	7	3.6	29	15.8	29	·	·	·	2	2	1	8	3	—	7	1	1	·	2
X	10	4.2	1	2.0	·	·	1	2.0	6	3.7	17	5.2	27.5	3.9	14.5	4.3	16	3.5	18	8.5	16	·	·	5	·	·	·	2	12	—	5	·	4	·	·
XI	3	4.7	15	3.1	8	3.6	6	5.6	9	3.5	10.5	6.6	17.5	5.6	7	3.8	14	3.9	44	11.0	21	6	16	21	·	2	·	·	18	—	9	1	5	16	·
XII	·	·	·	·	1	2.0	8	3.7	25.5	5.1	28	7.5	20.5	5.3	5	3.0	5	5.3	30	11.2	19	4	12	28	·	4	1	·	18	—	7	1	1	24	·
Rok	101	3.8	91.5	3.1	63	2.9	86.5	3.3	178	3.9	164.5	5.5	188.5	4.9	103	4.9	119	4.1	472	25.0	2.VIII	35	76	151	11	31	6	46	126	—	90	12	27	107	12

Szczytno $H_s = 144\ m$ $h_w = 15.3\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5.5	1.8	3.5	3.7	5	2.2	17.5	2.5	12.5	2.6	29	3.1	9	2.9	8	5.3	3	2.9	40	8.1	8	3	12	28	·	3	3	·	19	16	11	·	20	24	—
II	6.5	4.1	16.5	3.4	2.5	2.8	1	4.0	2	3.5	12	7.3	23	4.0	13.5	3.1	7	3.9	24	4.0	7, 27	13	23	27	·	7	3	2	12	17	10	·	7	28	—
III	5	7.2	4.5	2.6	1.5	2.0	8	2.4	11	2.9	13.5	4.4	17	2.8	10.5	3.1	22	2.6	26	5.7	3, 20	7	8	24	·	4	1	6	13	13	7	·	13	22	—
IV	6	4.5	10.5	4.3	15.5	3.7	22.5	4.2	9	2.6	7.5	2.3	8	2.3	7	2.1	4	3.3	42	13.4	27	·	·	13	·	4	2	3	14	11	9	1	12	·	—
V	10.5	2.9	13	4.3	9	3.8	9.5	4.0	6.5	2.9	12	4.3	4.5	4.0	13	3.2	13	3.2	43	14.0	19	·	·	4	·	4	3	5	10	15	11	1	10	·	—
VI	6	4.4	7	4.6	11.5	3.7	3	6.3	3	3.3	10	4.9	18.5	3.7	23	3.3	8	3.6	55	16.5	1	·	·	·	3	2	·	5	6	12	10	1	1	·	—
VII	1	5.0	4	4.5	3	2.7	7	3.0	6	3.5	23	4.0	30	4.9	9	4.0	10	3.7	60	13.8	23	·	·	·	5	·	·	3	6	13	9	2	1	·	—
VIII	3	2.0	1	2.0	·	·	4.5	3.8	10.5	3.0	5.5	3.5	16.5	3.7	34	2.9	18	2.5	108	43.6	26	·	·	·	10	·	·	7	12	10	8	3	1	·	—
IX	2.5	3.6	·	·	1	4.0	13	3.3	14.5	3.0	14.5	3.6	17.5	3.0	13	3.0	14	2.7	84	32.2	30	·	·	·	2	·	·	5	6	—	—	3	5	·	—
X	7	2.5	6	1.8	4	2.5	1	3.0	3	2.7	12.5	2.6	23.5	3.0	14	3.1	22	2.1	16	9.4	16	·	·	7	·	·	·	6	9	6	4	·	5	·	—
XI	6	2.6	14.5	1.9	7.5	2.7	9	3.9	5	4.6	12.5	4.2	18	4.6	6.5	2.6	11	3.0	50	11.7	21	7	15	22	·	2	·	1	16	17	10	1	2	16	—
XII	·	·	·	·	·	·	4	3.2	22	4.9	30	5.0	16.5	3.8	3.5	2.6	17	3.7	39	13.6	18	4	9	26	·	4	1	2	19	—	—	1	1	22[2]	—
Rok	59	3.4	80.5	2.8	60.5	2.5	100	3.6	107	3.3	182	4.1	202	3.6	155	3.2	149	3.1	587	43.6	26.VIII	34	67	151	20	30	13	45	142	—	—	13	78	112[2]	—

Szczuczyn $H_s = 130\ m$ $h_w = 15\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5	4.3	7	3.1	11.5	3.7	16.5	5.6	19.5	4.8	14.5	7.2	6.5	5.2	7.5	7.1	5	5.0	35	6.8	30	3	11	28	·	6	2	1	17	18	9	·	7	17	·
II	12.5	4.8	10	4.8	1.5	5.0	3.5	1.9	6	5.4	12	9.0	22	5.9	12.5	5.4	4	5.5	26	4.4	7	15	23	26	·	7	4	1	12	21	11	·	7	28	·
III	3	3.0	5	2.3	6	2.5	8.5	4.4	22	3.4	12.5	4.3	14	4.3	7	6.4	15	3.3	35	7.9	20	7	8	24	·	4	1	4	15	16	7	·	11	26	·
IV	6	4.7	2	7.8	25	7.8	25.5	6.9	13	3.8	4	4.4	2.5	3.4	7	3.4	5	5.7	22	8.5	23	·	·	12	·	12	3	2	18	10	5	·	3	·	1
V	9.5	3.7	8.5	3.0	16	4.7	5.5	4.2	3.5	3.7	6	5.7	10.5	3.8	17.5	3.7	16	3.3	79	23.2	19	·	·	4	·	4	·	2	15	15	11	3	5	·	2
VI	7.5	4.1	8	4.2	10	5.6	5	6.1	11.5	3.8	11	4.7	19	4.6	9	3.8	9	4.1	62	23.5	13	·	·	·	1	4	·	1	10	11	8	2	·	·	1
VII	2	3.0	4	4.4	6	2.7	8	3.0	9.5	3.9	35	5.2	14	5.7	1.5	4.0	13	3.9	107	28.7	22	·	·	·	3	7	3	·	10	15	11	3	1	·	7
VIII	10	4.0	1.5	1.7	1	1.0	7.5	5.4	8	3.5	15	3.0	20.5	3.5	11.5	3.7	18	2.9	55	19.1	26	·	·	·	6	1	·	4	9	11	8	1	1	·	5
IX	·	·	·	·	1	2.5	12.5	4.3	19.5	3.5	17.5	5.1	19.5	5.0	2	3.0	18	3.5	62	33.2	29	·	·	·	2	5	2	6	5	12	7	2	6	·	3
X	9	2.8	1	2.5	2	4.2	2.5	5.2	6	3.7	28	4.8	20.5	4.3	15	3.5	9	3.7	14	5.9	16	·	·	4	·	1	1	·	13	9	4	·	8	·	·
XI	2.5	2.4	10	3.9	13.5	4.6	11.5	7.8	10	6.0	19.5	6.8	14.5	5.4	4.5	3.8	4	5.4	39	9.8	21	7	16	21	·	9	3	·	21	15	8	·	8	16	·
XII	1	2.0	·	·	0.5	3.0	11	6.2	23	6.6	32	8.0	12	4.7	9.5	2.9	4	6.0	39	7.9	18	2	10	25	·	10	4	·	23	24	9	·	6	25	·
Rok	68	3.2	57	3.1	94	3.9	117.5	5.1	161.5	4.3	207	5.7	175.5	4.6	104.5	4.2	120	4.4	575	33.2	29. IX	34	68	144	12	70	23	21	168	177	98	11	63	112	19

Kamień Kraj.

φ = 53°32' λ = 17°32'

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																		
	p_m	Max	Min	$p_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.9	−3.0	4.0	1, 18	−10.1	11	−1.5	0.0	−1.3	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.6	6.2	7.5
II	–	–	–	–	−1.1	−8.5	3.4	11	−17.9	24	−5.5	−2.0	−4.7	−4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.0	7.9	7.8
III	–	–	–	–	3.1	−6.2	11.7	29	−26.0	8	−4.6	2.3	−1.6	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.2	5.6	6.6
IV	–	–	–	–	9.0	2.4	14.9	30	−3.3	5	3.6	7.9	5.1	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	7.1	7.6
V	–	–	–	–	13.7	4.8	19.9	17	−1.6	4	8.1	12.2	9.3	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.6	6.2
VI	–	–	–	–	20.6	9.7	29.4	26	5.6	15	14.0	18.8	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.7	5.4	5.4
VII	–	–	–	–	19.7	10.5	29.4	14	5.5	5	14.0	17.8	14.0	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.1	7.3	7.0
VIII	–	–	–	–	20.3	9.2	27.8	23	4.9	2	12.9	18.6	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.4	5.1	5.7
IX	–	–	–	–	19.1	8.7	26.9	3	1.5	16	10.7	17.8	12.8	13.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.4	3.9	5.3
X	–	–	–	–	12.5	3.1	19.9	1	−4.0	22	5.3	11.4	6.2	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.4	3.0	5.6
XI	–	–	–	–	0.9	−4.2	8.3	2	−20.2	24	−2.4	0.0	−1.9	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.6	7.5	8.1
XII	–	–	–	–	1.6	−1.9	10.4	19	−13.2	17	−0.5	0.5	−0.3	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.8	8.8	8.6	9.1
Rok	–	–	–	–	10.0	2.0	29.4	26.VI, 14.VII	−26.0	8. III	4.5	8.8	5.6	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	6.1	6.8

Grudziądz

φ = 53°30' λ = 18°46'

I	–	–	–	–	1.9	−2.4	5.4	1	−12.2	11	−0.9	0.7	−0.7	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.3	8.3	8.6
II	–	–	–	–	−0.4	−7.1	3.3	11	−16.5	6	−5.1	−1.6	−4.2	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.7	7.9	8.1
III	–	–	–	–	4.3	−3.9	12.1	29	−21.2	8	−2.8	2.7	−0.2	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.9	7.0	7.4
IV	–	–	–	–	10.5	3.3	15.8	30	−1.5	6	4.2	8.9	6.5	6.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	8.4	8.1
V	–	–	–	–	14.6	5.8	20.7	17	−0.3	3	8.3	13.3	9.4	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.7	6.8	6.7
VI	–	–	–	–	22.0	11.6	31.3	26	6.7	15	14.9	20.4	16.1	16.9	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	4.5	4.9
VII	–	–	–	–	21.7	12.1	31.1	14	7.4	2	14.8	20.0	16.0	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.9	5.8	6.0
VIII	–	–	–	–	21.5	11.2	29.7	22	7.1	16, 31	13.7	20.2	15.4	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.2	4.9	5.5
IX	–	–	–	–	20.5	10.7	28.3	3	4.7	16	11.7	19.2	14.2	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.3	5.1	5.4
X	–	–	–	–	13.0	4.5	20.9	1	−2.0	22	5.5	11.9	7.5	8.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.8	6.7	6.6
XI	–	–	–	–	1.4	−3.6	11.4	1	−17.2	24	−1.9	0.1	−1.2	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.8	7.8	8.0
XII	–	–	–	–	2.3	−1.6	10.4	19	−17.2	17	−0.1	1.2	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	9.0	8.4
Rok	–	–	–	–	11.1	3.4	31.3	26.VI	−21.2	8. III	5.2	9.8	6.6	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	6.8	7.0

Szczecin - Niebuszewo

φ = 53°28' λ = 14°33'

I	–	–	–	–	2.7	−1.2	8.0	17	−9.0	31	0.1	1.6	0.5	0.7	5.8	5.9	5.7	5.8	93	86	90	90	0.5	1.0	0.7	0.7	8.7	9.0	7.3	8.3
II	–	–	–	–	0.4	−5.0	4.5	13	−16.4	28	−2.9	−0.7	−2.2	−2.0	4.4	4.8	4.5	4.6	88	81	86	85	0.6	1.1	0.7	0.8	7.4	8.0	7.8	7.7
III	–	–	–	–	4.9	−2.9	14.5	29	−14.7	8	−1.2	3.4	1.0	1.0	5.3	5.9	5.8	5.7	90	73	84	82	0.6	2.2	1.1	1.3	6.5	6.5	4.1	5.7
IV	–	–	–	–	11.5	3.3	16.4	6	−2.9	5	5.1	9.6	6.5	6.9	7.7	7.6	7.8	7.7	87	65	80	77	1.2	4.5	2.0	2.6	7.4	8.4	5.8	7.2
V	–	–	–	–	14.9	6.2	20.0	17	0.6	3	9.0	13.4	9.8	10.5	9.0	9.1	9.6	9.2	78	60	79	72	2.6	6.6	2.6	3.9	6.3	6.9	6.1	6.4
VI	–	–	–	–	21.3	10.8	28.3	26	6.0	3	15.0	19.6	15.1	16.2	12.5	11.8	12.5	12.3	72	53	73	66	4.8	11.5	5.0	7.1	4.7	6.2	4.8	5.2
VII	–	–	–	–	19.5	11.0	29.2	14	6.9	4	13.5	17.7	13.8	14.7	13.2	13.3	13.5	13.3	84	66	84	78	2.5	7.5	2.5	4.2	7.3	7.5	6.4	7.1
VIII	–	–	–	–	20.3	10.5	27.5	22	6.8	31	13.4	18.6	14.3	15.2	13.5	13.3	13.5	13.4	87	62	82	77	2.0	8.5	3.1	4.5	5.6	6.5	4.7	5.6
IX	–	–	–	–	19.1	10.3	25.1	3	6.2	21	12.0	17.8	13.2	14.0	12.6	12.8	13.0	12.8	89	63	85	79	1.6	7.9	2.3	3.9	6.5	6.8	4.5	5.9
X	–	–	–	–	13.1	5.0	21.9	1	−0.6	25	6.3	11.9	7.7	8.4	9.2	10.0	9.5	9.6	94	72	89	85	0.7	4.1	1.2	2.0	7.3	6.5	3.5	5.8
XI	–	–	–	–	2.6	−2.4	12.3	1	−10.8	23	−0.8	1.5	−0.3	0.0	5.5	5.8	5.5	5.6	89	79	86	85	0.6	1.5	0.9	1.0	8.8	7.9	5.8	7.5
XII	–	–	–	–	3.4	−0.9	11.6	19	−5.9	13	0.7	2.0	1.1	1.2	5.8	6.1	6.0	6.0	88	85	89	87	0.8	1.1	0.8	0.9	9.1	9.0	7.6	8.6
Rok	–	–	–	–	11.1	3.7	29.2	14.VII	−16.4	28. II	5.8	9.7	6.7	7.2	8.7	8.9	8.9	8.8	87	70	84	80	1.5	4.8	1.9	2.7	7.1	7.4	5.7	6.7

Szczecin - Dąbie

φ = 53°24' λ = 14°37'

I	1009.0	1027.1	983.9	1009.9	3.2	−1.5	9.4	17	−8.2	31	0.4	2.1	0.7	1.0	5.9	6.1	5.9	6.0	93	86	90	90	0.5	1.1	0.7	0.8	8.2	8.5	7.1	7.9
II	1017.0	1033.7	987.7	1017.9	0.9	−4.7	4.8	13	−14.1	17	−3.1	−0.6	−1.6	−1.7	4.5	4.9	4.7	4.7	88	82	85	85	0.6	1.1	0.8	0.8	7.8	8.4	7.7	8.0
III	1015.6	1031.9	993.5	1016.5	5.3	−3.5	15.0	29	−22.7	8	−2.2	3.7	0.7	0.7	5.1	6.1	5.7	5.6	90	75	85	83	0.6	2.2	1.0	1.3	6.5	6.4	4.1	5.7
IV	1009.9	1032.6	986.9	1010.8	12.1	2.8	16.8	6	−4.1	5	4.5	10.1	6.8	7.0	7.6	7.6	7.9	7.7	89	63	80	77	0.9	5.0	2.1	2.7	7.2	8.3	5.8	7.1
V	1013.5	1028.2	997.5	1014.3	15.5	6.2	21.5	17	−0.2	3	8.7	14.0	10.4	10.9	9.3	9.7	10.0	9.7	82	61	79	74	2.1	6.5	2.8	3.8	6.3	6.9	6.7	6.6
VI	1013.4	1024.8	997.4	1014.2	21.7	11.1	27.8	26	4.0	4	14.9	20.1	16.1	16.8	13.1	13.4	13.6	13.4	76	57	76	70	4.1	10.6	4.8	6.5	5.2	6.5	5.2	5.6
VII	1009.9	1021.1	992.7	1010.7	20.0	11.6	30.1	14	7.6	4	13.6	18.3	14.8	15.4	13.6	14.1	14.2	14.0	87	67	83	79	2.1	7.5	2.8	4.1	7.6	7.6	6.6	7.3
VIII	1014.5	1024.1	999.5	1015.3	20.7	10.8	26.2	22	5.5	29	13.0	19.3	14.8	15.5	13.8	14.2	14.3	14.1	91	63	84	79	1.4	8.6	2.7	4.2	6.1	6.7	5.1	6.0
IX	1011.8	1033.8	995.2	1012.6	19.6	10.2	25.8	3	5.3	23	11.7	18.5	13.5	14.3	12.5	13.5	13.2	13.1	90	64	85	80	1.5	8.1	2.4	4.0	6.7	6.6	5.0	6.1
X	1022.1	1037.0	1005.7	1022.9	13.5	3.3	22.4	1	−4.5	23	5.3	12.1	7.0	7.8	8.7	10.5	9.3	9.5	95	74	91	87	0.5	3.9	1.0	1.8	7.1	6.5	4.6	6.1
XI	1009.6	1030.8	977.4	1010.5	3.0	−2.2	12.4	1, 2	−11.2	23	−0.4	2.1	0.1	0.5	5.5	6.0	5.7	5.7	88	80	86	85	0.8	1.5	0.9	1.1	7.8	7.8	6.5	7.4
XII	1001.4	1023.7	970.1	1002.3	3.8	−0.5	12.0	19	−6.9	13	1.2	2.6	1.6	1.8	5.9	6.2	6.2	6.1	87	83	88	86	0.9	1.2	0.8	1.0	8.3	8.7	7.4	8.1
Rok	1012.3	1037.0	970.1	1013.1	11.6	3.6	30.1	14.VII	−22.7	8. III	5.6	10.2	7.1	7.5	8.8	9.4	9.2	9.1	88	71	84	81	1.3	4.8	1.9	2.7	7.1	7.4	6.0	6.8

Kamień Kraj. $H_s = 124\,m$ $h_w = 12{,}8\,m$ 1965

Miesiąc	Rozkład wiatru (%D,VmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<0°	Max<0°	Min<0°	Max>25°	Wiatr V 10≤V<15	V≥15	◔	◕	Opad R 0,1≤R<1,0	1,0≤R<10,0	R≥10,0	≡	⊠	K
I	7	1.7	6	2.2	13	2.0	8	2.1	7.5	3.1	16	2.6	11	2.5	9.5	1.9	15	1.9	25	5.3	25	1	8	26	·	·	·	·	16	16	9	·	—	6	·
II	10	2.0	11	2.7	·	·	3	1.0	1	1.0	5	3.8	29	3.0	20	3.6	5	2.7	16	2.5	13	9	20	27	·	·	·	·	16	18	7	·	—	28	·
III	9	1.9	11	4.8	5	1.4	1.5	2.0	7.5	1.2	3.5	1.0	20	2.0	4.5	2.7	31	1.5	40	13.9	3	9	9	26	·	·	·	3	13	12	10	1	—	22	·
IV	9	1.1	12.5	3.1	18.5	3.3	10	2.6	7	2.4	5	2.8	6	1.7	6	3.3	16	2.2	30	5.4	13	·	·	7	·	·	·	3	17	13	10	·	2	·	·
V	11	2.5	19	2.6	19.5	3.3	3.5	4.7	2	1.5	2	4.0	11	3.0	13	2.7	12	2.5	76	45.7	9	·	·	3	·	1	·	5	11	13	11	1	—	·	·
VI	10	2.4	15.5	3.5	5	2.8	3.5	4.0	10	3.4	3.5	3.0	20.5	2.9	10	3.8	12	2.8	54	18.9	22	·	·	·	3	·	·	2	6	9	9	2	·	·	1
VII	1	6.0	11	4.4	4	4.1	5	3.5	8	3.1	9.5	3.8	37	4.7	6.5	4.8	11	3.8	122	33.2	15	·	·	·	3	·	·	2	11	20	17	3	—	·	6
VIII	12	2.5	3	1.0	·	·	6	2.2	7	2.7	3.5	3.4	17	2.0	14.5	2.5	30	1.6	45	15.9	25	·	·	·	5	·	·	1	7	12	8	2	2	·	3
IX	1	3.0	3	4.5	12.5	2.8	6.5	3.3	7.5	2.1	9.5	3.9	21.5	2.9	5.5	2.8	23	2.3	59	10.8	1	·	·	·	1	·	·	7	5	10	8	2	2	·	1
X	9	2.1	3.5	1.7	5	3.0	0.5	2.0	8.5	3.0	8	4.2	19.5	2.9	11	2.7	28	2.0	14	5.4	16	·	·	6	·	1	·	5	7	9	4	·	13	·	1
XI	3	3.7	19	4.4	8	4.9	3	5.0	11	3.7	11.5	5.7	20.5	4.8	3	3.3	11	4.0	34	7.8	21	6	12	22	·	4	·	1	17	15	7	·	4	9	·
XII	·	·	1	3.0	2.5	3.0	7.5	4.5	19	5.9	24.5	5.4	23.5	3.7	10	1.7	5	4.2	36	8.8	9	1	7	23	·	3	·	·	25	15	6	·	4^2	5	·
Rok	82	2.4	115.5	3.2	93	2.6	58	3.1	96	2.8	101.5	3.6	236.5	3.0	113.5	3.0	199	2.6	551	45.7	9.V	26	56	140	12	9	·	29	151	162	106	11	—	70	12

Grudziądz $H_s = 40\,m$ $h_w = 12{,}5\,m$

I	4	3.0	6.5	2.9	11.5	3.4	21.5	4.6	2.1	3.9	20	3.6	4	4.6	4.5	3.6	·	3.8	42	11.4^2	5	2	4	26	·	3	1	·	24	17	10	1	·	18	·
II	4	4.9	9	4.3	8.5	4.4	7	2.2	14.5	3.7	26.5	4.5	9.5	4.6	5	4.6	·	4.2	17	2.7	27	4	16	26	·	2	·	·	16	17	7	·	·	26	·
III	3	4.3	4	3.4	10	2.8	17.5	2.6	28	2.2	23.5	2.7	4	3.5	3	3.7	·	2.7	50	16.4	3	3	8	21	·	·	·	·	15	14	8	1	4	16	·
IV	4	2.7	4	3.1	21	4.3	32	3.5	8.5	2.7	11.5	2.8	4.5	2.9	3.5	2.3	1	3.4	30	7.2	13	·	·	3	·	1	·	·	19	13	7	·	·	·	·
V	5.5	2.5	9	2.9	24	2.8	18.5	2.9	12	2.6	12	3.2	5.5	6.5	5.5	4.3	1	3.1	68	18.6	9	·	·	1	·	1	·	1	14	13	11	2	2	·	1
VI	3	3.7	4.5	2.7	18.5	3.2	13	2.8	13.5	2.4	24	3.5	6.5	3.8	7	4.0	·	3.2	65	23.0	1	·	·	·	6	·	·	7	7	9	8	3	·	·	4
VII	2	1.0	·	·	5.5	2.1	9	1.7	21.5	2.5	32.5	2.7	13.5	3.5	3	1.7	1	2.5	39^2	—	—	·	·	·	7	·	·	2	8	17	13	·	·	·	4
VIII	3	1.3	1.5	2.0	4.5	1.9	12.5	2.2	15	1.7	31.5	1.9	14.5	1.7	7.5	1.5	3	1.8	76	10.3	24	·	·	·	8	4	·	3	6	14	13	1	1	·	·
IX	·	·	·	·	5.5	3.6	24	3.3	28.5	2.8	25	3.5	5.5	4.4	1.5	4.3	·	3.3	100	46.9	4	·	·	·	1	4	·	6	10	9	7	3	8	·	2
X	4	2.0	2	1.5	11.5	3.0	11	1.9	23	2.5	28	2.8	6.5	3.5	6	4.2	1	2.7	21	10.0	16	·	·	2	·	·	·	3	12	5	3	1	23	·	1
XI	2.5	1.4	8.5	2.2	19	2.8	14.5	3.0	21	2.8	21	5.0	3	5.2	0.5	3.0	·	3.3	38	16.9	21	8	11	17	·	2	1	2	16	11	6	1	2	15	·
XII	0.5	5.0	·	·	2.5	2.6	12.5	3.0	35.5	3.1	32.5	4.3	3.5	4.9	1	3.5	·	3.6	29	9.9	18	3	4	20	·	1	·	·	18	13	7	·	1	13	·
Rok	35.5	2.6	49	2.1	142	3.1	193	2.8	242	2.7	298	3.4	80.5	4.1	48	3.4	7	3.1	575^2	46.9	4. IX	20	43	116	22	18	2	24	165	152	100	13	41	88	12

Szczecin - Niebuszewo $H_s = 69\,m$ $h_w = 10\,m$

I	5.5	2.0	8	2.9	12	2.2	10	3.6	12.5	4.4	20.5	5.1	12.5	3.0	6	2.6	6	3.3	41	8.4	8	·	3	20	·	2	·	·	21	16	11	·	8	8	·
II	15.5	4.7	11.5	3.5	1.5	4.7	2.5	2.8	2.5	2.6	12.5	4.2	22	2.9	14	4.1	2	3.7	29	5.2	26	2	11	26	·	4	·	1	12	21	11	·	5	28	·
III	8	5.2	14	3.4	4.5	2.2	8.5	2.3	8.5	2.6	17	2.9	17	3.1	8.5	3.5	7	2.9	25	9.4	3	1	6	20	·	·	·	7	10	11	6	·	8	18	·
IV	6	3.8	24.5	3.4	12	3.5	13.5	3.9	6	4.8	11.5	4.3	9	2.7	6.5	3.1	1	3.6	46	10.3	20	·	·	2	·	·	·	2	13	18	13	1	·	·	3
V	14.5	3.1	10.5	3.6	17	3.6	8	3.8	3	2.0	10.5	3.0	12	3.6	15.5	3.4	2	3.3	107	44.3	10	·	·	·	·	·	·	4	15	17	11	3	1	·	5
VI	9	3.7	14	3.4	4.5	3.2	6.5	2.9	10.5	4.1	12.5	4.4	17.5	3.9	9.5	3.5	6	3.5	21	8.5	18	·	·	·	4	·	·	5	5	5	4	·	·	·	3
VII	5	3.5	6	4.1	8	2.1	2	2.0	6	3.4	38.5	4.2	19.5	4.1	4	2.1	4	3.6	117	20.2	14	·	·	·	2	·	·	·	12	21	14	6	1	·	5
VIII	10	3.0	10.5	1.9	4	2.4	3.5	3.3	10	2.0	17.5	2.8	16	2.5	13.5	2.1	8	2.3	49	18.8	8	·	·	·	3	·	·	2	7	12	5	2	3	·	2
IX	2	3.0	3	4.0	9.5	3.1	13.5	3.2	18.5	3.6	22.5	3.0	12	3.0	2	1.5	7	2.9	74	16.6	10	·	·	·	1	1	·	3	9	13	9	3	1	·	2
X	4.5	2.0	8.5	1.9	13	2.2	4.5	2.1	10	2.2	11.5	3.0	15	3.7	8	2.0	16	2.1	18	9.9	31	·	·	2	·	·	·	2	4	5	5	·	12	·	·
XI	3	4.2	14.5	3.1	14.5	3.9	6.5	6.2	8	5.7	20	5.0	9.5	4.2	3	3.7	11	3.9	32	7.3	21	2	11	18	·	3	·	1	14	14	8	·	5	10	·
XII	2.5	1.0	2.5	1.0	5.5	4.3	13.5	4.2	14	4.6	38.5	5.2	14	3.0	2.5	2.6	·	4.3	52	13.1	18	·	3	22	·	7	2	·	23	17	9	2	3	8	·
Rok	85.5	3.3	127.5	3.0	106	3.1	92.5	3.4	109.5	3.5	233	3.9	176	3.3	93	2.8	72	3.3	611	44.3	10.V	5	34	110	10	17	2	27	145	170	106	17	47	72	20

Szczecin - Dąbie $H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 24\,m$

I	9	2.4	7.5	3.2	10.5	2.7	12	4.5	4.5	4.0	40	5.6	5.5	3.8	3	4.2	1	4.4	38	7.1	8	·	1	21	·	6	·	·	19	15	11	·	6	8	·
II	9.5	5.8	12	5.5	3.5	4.3	4	5.2	·	·	22	5.1	19	4.2	10	4.6	4	4.7	26	6.5	13	3	11	24	·	6	·	1	16	18	8	·	9	26	·
III	5	7.1	13	4.8	6	3.7	11	3.4	3.5	4.3	36.5	4.1	6.5	4.7	4.5	5.7	7	4.0	29	10.2	3	4	6	20	·	1	·	8	10	13	7	1	9	16	·
IV	6	4.9	11	3.5	18	5.0	14.5	4.7	8.5	6.6	14.5	4.2	8	4.4	6.5	3.2	3	4.5	52	10.4	19	·	·	4	·	·	·	1	14	18	13	2	4	·	3
V	14	4.4	13.5	3.7	15	3.7	13.5	5.7	3.5	6.0	6.5	3.5	13.5	4.3	9.5	4.9	4	4.2	102	30.1	10	·	·	2	·	4	·	2	14	15	12	3	3	·	3
VI	8	4.0	14.5	3.8	7	4.8	4	5.0	5	5.7	20	4.8	14	4.0	9.5	3.8	8	4.0	24	8.8	18	·	·	·	4	·	·	2	7	7	5	·	3	·	3
VII	3	3.8	8	5.1	4.5	3.1	3.5	6.3	2.5	3.8	49	4.7	16.5	5.3	3	4.3	3	4.6	97	16.8	12	·	·	·	3	3	·	·	10	21	16	2	1	·	5
VIII	8	3.2	7	2.2	4	2.1	8	3.5	1.5	2.0	31.5	3.2	16	2.5	5	3.6	12	2.6	35	13.8	8	·	·	·	3	·	·	3	7	10	6	2	6	·	1
IX	1	2.5	2.5	2.0	9	3.7	14	5.4	8	5.2	42	3.8	8	4.1	1.5	2.3	4	3.9	63	16.6	9	·	·	·	1	2	·	4	7	11	9	3	7	·	2
X	0.5	2.0	6	2.2	10.5	2.8	12	3.2	1.5	2.7	29.5	4.2	11.5	3.0	5.5	2.5	16	2.8	12	7.3	3.1	·	·	5	·	·	·	2	5	6	4	·	20	·	·
XI	0.5	5.0	9.5	4.2	17	4.6	8.5	6.1	8.5	7.1	35	5.6	8.5	4.4	1.5	5.0	1	5.2	43	12.2	21	3	11	15	·	8	·	·	13	10	8	1	5	10	·
XII	0.5	2.0	0.5	4.0	4.5	4.1	11	6.6	7.5	6.5	50	6.4	15	4.9	4	4.1	·	5.9	48	12.4	9	·	2	18	·	8	2	·	21	18	9	2	3	6	·
Rok	65	3.9	105	3.7	109.5	3.7	116	5.0	54.5	4.5	376.5	4.6	142	4.1	63.5	4.0	63	4.2	569	30.1	10.V	10	51	109	11	38	2	23	143	162	108	16	76	66	17

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Jabłonowo Pom. φ = 53°24' λ = 19°10' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.9	-3.7	4.7	18	-14.6	11	-1.9	0.0	-1.2	-1.1	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.6	8.2	8.2
II	—	—	—	—	-2.0	-9.6	1.9	14	-21.7	6	-6.5	-3.3	-4.9	-4.9	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.2	7.6	7.5
III	—	—	—	—	3.0	-5.1	10.0	29	-26.7	8	-3.4	1.6	-0.4	-0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.3	7.0	7.2
IV	—	—	—	—	9.8	2.3	15.3	30	-2.3	3	3.7	8.3	5.9	6.0	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.5	7.8	7.6
V	—	—	—	—	13.6	4.6	18.9	18	-2.5	3	7.6	12.0	9.2	9.5	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.5	7.5	7.4
VI	—	—	—	—	20.6	10.2	28.6	26	6.3	8	14.0	19.6	15.2	16.0	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.7	6.6	6.5
VII	—	—	—	—	20.4	10.7	29.1	14	5.3	6	13.8	19.2	15.0	15.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	20.5	10.2	28.4	22	5.6	16	13.1	19.5	14.8	15.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.7	9.5	26.9	3	3.5	16	11.1	18.2	13.6	14.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.1	3.8	21.1	1	-2.8	21	5.0	11.3	7.7	7.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	1.3	-4.0	11.4	1	-18.7	24	-2.8	-0.4	-0.7	-1.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	1.9	-2.4	9.2	19	-18.5	17	-1.1	0.5	0.4	0.0	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.5	9.3	8.9
Rok	—	—	—	—	10.2	2.2	29.1	14.VII	-26.7	8.III	4.4	8.9	6.2	6.4	—	—	—	—	—	—	—	—	—	—	—		—	—	—	—

Wierzchowo φ = 53°27' λ = 16°06'

I	—	—	—	—	1.8	—	5.8	1	—	—	-0.9	0.9	-0.1	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.0	7.5	7.7
II	—	—	—	—	-0.6	—	3.6	14	—	—	-4.7	-1.5	-4.0	-3.6	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.9	5.9	6.6
III	—	—	—	—	3.5	—	13.5	29	—	—	-3.0	3.0	-0.7	-0.4	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.1	5.1	5.6
IV	—	—	—	—	10.1	1.9	15.1	6, 30	-3.8	5	4.4	9.4	4.9	5.9	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.7	6.0	6.3
V	—	—	—	—	13.8	5.0	19.7	17	-1.8	3	8.1	12.7	8.5	9.4	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.3	6.1	6.2
VI	—	—	—	—	20.3	9.7	27.6	26	4.8	1, 3	14.5	19.0	14.0	15.4	—	—	—	—	—	—	—	—	—	—	—	—	4.6	5.8	4.9	5.1
VII	—	—	—	—	18.9	10.3	29.1	14	3.1	5	13.6	17.6	13.9	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.2	6.7	6.2
VIII	—	—	—	—	20.2	9.0	27.1	22	3.5	14	13.3	18.8	13.1	14.6	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.3	3.5	4.8
IX	—	—	—	—	19.0	8.5	26.1	3	4.1	16	11.3	18.1	12.2	13.4	—	—	—	—	—	—	—	—	—	—	—	—	5.6	5.5	4.6	5.2
X	—	—	—	—	12.4	2.5	20.7	1	-4.5	22	4.8	11.7	5.5	6.9	—	—	—	—	—	—	—	—	—	—	—	—	7.0	5.9	4.4	5.8
XI	—	—	—	—	1.1	-4.0	13.5	2	-15.4	23, 24	-2.1	0.4	-1.8	-1.3	—	—	—	—	—	—	—	—	—	—	—	—	8.4	6.9	6.2	7.2
XII	—	—	—	—	2.2	-2.0	10.4	19	-9.9	17	-0.5	0.7	0.2	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.3	8.1	8.3
Rok	—	—	—	—	10.2	—	29.1	14.VII	—	—	4.9	9.2	5.5	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.4	5.8	6.3

Jastrowie φ = 53°25' λ = 16°48'

I	—	—	—	—	1.9	-2.9	6.3	17	-10.0	11	-1.1	1.0	-0.8	-0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.1	8.1	8.3
II	—	—	—	—	-0.8	-8.6	2.7	13	-18.0	24	-5.7	-1.9	-4.7	-4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.8	6.7	7.0
III	—	—	—	—	4.2	-5.4	14.1	29	-23.5	8	-2.2	3.5	-0.9	-0.1	—	—	—	—	—	—	—	—	—	—	—	—	6.8	5.7	6.3	6.3
IV	—	—	—	—	10.7	1.9	16.0	6	-4.2	5	4.4	10.2	5.3	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.0	7.3	6.7
V	—	—	—	—	14.2	4.8	20.4	17	-2.1	3	7.9	13.6	8.4	9.6	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.1	7.0	6.4
VI	—	—	—	—	21.3	9.7	29.4	26	3.7	3	13.6	20.3	14.0	15.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	19.8	10.1	30.5	14	5.0	2	13.9	19.4	13.8	15.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	20.7	9.3	28.4	22	4.1	29	13.2	20.2	13.2	15.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.6	8.7	27.4	3	3.7	16, 21	11.7	18.9	12.2	13.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.8	2.7	20.8	1	-4.5	12	5.6	12.4	5.8	7.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	1.7	-4.3	10.8	2	-19.8	24	-2.0	1.1	-1.4	-0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.9	7.4	7.4
XII	—	—	—	—	2.4	-2.0	11.8	19	-10.3	17	-0.1	1.5	0.3	0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.8	8.8	8.4
Rok	—	—	—	—	10.7	2.0	30.5	14.VII	-23.5	8.III	4.9	10.0	5.4	6.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Uwaga. W dniu 23.XI.1965 przeniesiono stację o ok. 500 m w kierunku E.

Kołno φ = 53°25' λ = 21°56'

I	—	—	—	—	-0.3	-4.6	3.4	9, 18	-16.0	11	-2.7	-1.4	-2.2	-2.1	—	—	—	—	—	—	—	—	—	—	—	—	9.3	8.1	7.2	8.2
II	—	—	—	—	-2.8	-11.9	1.3	17	-29.2	6	-8.5	-4.4	-6.9	-6.7	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.1	6.0	6.7
III	—	—	—	—	3.0	-5.2	9.8	30	-21.2	9	-3.2	2.3	-1.1	-0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.3	5.6	5.7	6.2
IV	—	—	—	—	9.8	2.2	15.8	28	-2.6	3	3.7	8.7	5.3	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.1	8.1	6.5	7.2
V	—	—	—	—	13.7	4.0	20.9	18	-4.1	4	7.7	12.6	8.1	9.1	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.3	6.3	6.5
VI	—	—	—	—	20.5	10.6	28.0	26	3.7	8	14.7	19.4	14.7	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.4	5.5	5.8
VII	—	—	—	—	20.9	10.4	29.8	15, 16	4.1	5	14.7	19.6	14.6	15.9	—	—	—	—	—	—	—	—	—	—	—	—	4.5	7.0	6.9	6.1
VIII	—	—	—	—	20.8	10.3	28.0	7	4.9	17	13.3	19.6	14.0	15.2	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.9	4.5	5.5
IX	—	—	—	—	20.3	9.1	27.2	3	2.9	21	11.1	19.2	13.0	14.1	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.8	3.9	5.0
X	—	—	—	—	11.2	3.2	19.6	1	-4.0	21	5.1	10.6	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.2	5.0	6.6
XI	—	—	—	—	0.3	-4.6	10.4	2	-20.1	17	-2.7	-0.6	-2.0	-1.8	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.5	7.5	8.2
XII	—	—	—	—	1.1	-3.1	9.2	20	-16.8	17	-0.9	0.1	-0.6	-0.5	—	—	—	—	—	—	—	—	—	—	—	—	9.5	9.8	8.4	9.2
Rok	—	—	—	—	9.9	1.7	29.8	15, 16.VII	-29.2	6.II	4.4	8.8	5.3	6.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.2	6.1	6.8

Jabłonowo Pom. — $H_s = 97\,m$ — $h_w = 13\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (=D, V=D) N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	OPAD R Suma	Max	Date	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	≥15	◐	●	Opad R ≥0.1	≥5.0	≥10.0	≡	⊠	⊠
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n																		
I	10	2.1	5	1.4	9	1.8	18	2.2	14	2.1	8	2.1	21	1.7	8	2.0	·	2.0	36	6.8	8	2	11	28	·	·	·	·	19	15	12	·	6	—	—
II	18	2.3	9	2.0	2	2.0	1	2.0	2	1.5	3	2.3	13	2.1	7	3.1	29	1.5	33	5.4	2	11	21	26	·	·	·	·	9	21	12	·	5	28	—
III	6	1.8	7	1.9	13	1.9	10	2.3	15	2.0	·	·	12	2.2	9	1.7	21	1.5	51	18.2	4	6	10	23	·	·	·	·	15	16	9	2	19	18	—
IV	11	2.8	13	2.8	16	2.6	19	3.7	19	2.9	·	·	9	2.8	1	2.0	2	2.9	31	6.8	23	·	·	6	·	·	·	·	14	12	10	·	4	·	—
V	10	2.9	14	2.3	29	2.3	11	3.0	8	3.4	1	9.0	5	6.2	9	4.0	6	2.8	69	13.2	19	·	·	2	·	2	·	·	14	15	11	2	2	·	—
VI	7	1.7	14	2.1	21	2.0	4	2.2	11	2.7	1	5.0	13	2.2	13	2.5	6	2.1	42	13.2	13	·	·	·	4	·	·	·	8	12	9	1	·	·	—
VII	·	·	2	2.5	6	1.5	2	1.5	8	1.4	4	2.2	30	2.4	25	2.1	16	1.8	80	13.7	17	·	·	·	3	·	·	—	—	18	17	1	·	·	—
VIII	·	·	21	2.1	4	2.0	6	2.3	7	2.7	4	2.2	9	2.0	22	2.1	20	1.7	70	11.2	26	·	·	·	7	·	·	—	—	16	15	1	2	·	—
IX	9	1.3	3	2.7	7	1.7	13	2.1	18	1.8	2	2.5	16	2.1	9	2.4	13	1.7	93	49.2	4	·	·	·	1	·	·	—	—	12	11	3	8	·	—
X	19	1.8	10	1.8	4	1.2	1	1.0	7	1.6	5	1.8	16	1.8	12	2.1	19	1.4	21	7.2	16	·	·	3	·	·	·	—	—	12	3	·	17	·	—
XI	8	2.0	18	2.1	6	2.0	20	4.1	3	6.0	7	3.3	5	4.8	22	3.4	1	3.2	58	16.5	21	7	12	18	·	3	·	—	—	24	16	1	5	16	—
XII	8	2.2	·	·	·	·	15	4.4	9	4.0	9	3.7	28	3.8	23	3.3	1	3.6	53	12.5	18	3	7	20	·	2	·	·	22	28	14	1	5	16	—
Rok	106	1.7	116	2.0	117	1.8	120	2.6	121	2.7	44	2.8	177	2.8	160	2.6	134	2.2	637	49.2	4. IX	29	61	126	15	7	·	—	—	201	139	12	73	—	—

Wierzchowo — $H_s = 140\,m$ — $h_w = 13\,m$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	29	8.0	17	—	10	—	—	—	—	1	16	14	8	·	2	9	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	18	4.0	26	—	20	—	—	—	—	1	12	12	7	·	·	28	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	35	15.0	3	—	8	—	—	—	—	6	9	8	6	1	4	20	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	26	6.1	24	·	·	8	—	—	—	2	11	10	7	·	·	·	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	69	30.5	9	·	·	3	—	—	—	4	10	13	11	1	·	·	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	53	16.5	11	·	·	·	3	—	—	4	3	7	7	3	·	·	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	56	9.5	23	·	·	·	2	—	—	1	5	18	17	·	·	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39	14.5	23	·	·	·	6	—	—	4	4	9	9	1	3	·	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	87	23.0	7	·	·	·	1	—	—	3	3	10	9	4	·	·	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	16	5.4	31	·	·	7	·	—	—	2	5	4	4	·	9	·	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	6	13	20	·	—	—	1	11	—	—	—	4	10	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	75	19.2	9	·	5	23	·	—	—	1	23	20	9	3	7	10^2	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	30.5	9. V	—	56	—	12	—	—	30	112	—	—	—	29	77^2	—

Jastrowie — $H_s = 120\,m$ — $h_w = 13\,m$

I	4.5	2.8	10.5	2.2	12	2.5	13	2.4	7	2.6	20.5	3.2	14	3.2	5.5	3.1	6	2.6	43	7.4	25	·	7	26	·	·	·	·	18	14	10	·	5	6	—
II	13.5	4.1	16.5	3.7	1.5	3.7	1	4.0	·	·	8.5	6.3	33.5	4.5	9.5	4.8	·	4.5	29	5.3	28	14	18	28	·	·	·	·	9	15	11	·	2	28	—
III	10	3.2	8	3.2	3	5.7	5	2.6	2	2.8	21	2.2	14	3.6	18	3.2	12	2.7	52	17.2	3	6	9	25	·	·	·	·	9	11	9	1	7	22	—
IV	8.5	3.2	16.5	3.2	13.5	3.4	13.5	3.2	7.5	3.0	6	2.8	8	3.2	13.5	3.2	3	3.1	45	8.2	13	·	·	9	·	·	·	1	8	14	9	·	2	·	—
V	2.7	3.4	20.5	3.0	3	2.2	9	2.7	2	8.5	2	5.8	9	4.5	14.5	3.7	6	3.3	75	25.0	9	·	·	5	·	1	·	1	10	15	13	1	·	·	—
VI	15.5	3.0	20.5	2.9	5	3.9	1	1.0	4	2.4	11	2.6	11.5	3.7	12.5	3.5	9	2.8	48	13.0	1	·	·	·	4	·	·	—	—	8	5	2	·	·	—
VII	6.5	3.2	11	2.9	·	·	5	2.8	1.5	3.8	31.5	3.3	25	3.6	8.5	3.0	4	3.2	91	10.5	14	·	·	·	2	·	·	—	—	21	14	1	·	·	—
VIII	12.5	2.3	6	1.7	·	·	2	3.5	8	2.1	15	2.2	14.5	2.7	20	2.6	15	2.0	39	8.9	25	·	·	·	5	·	·	—	—	14	10	·	·	·	—
IX	7.5	3.1	5	3.2	6	2.7	6	2.7	6.5	2.2	32	3.2	10.5	3.9	0.5	3.0	16	2.6	78	23.8	10	·	·	·	1	·	·	—	—	11	10	2	4	·	—
X	28.5	3.1	7.5	2.8	6	3.2	1	3.5	·	·	11	4.1	15.5	3.3	8.5	3.7	15	2.8	22	9.8	16	·	·	8	·	·	·	—	—	7	4	·	6	·	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	65	15.6	21	5	12	20	·	—	—	·	13	10	8	1	2	10	—
XII	5	2.0	2	3.0	6	4.0	15.5	3.1	3.0	4.6	17.5	6.0	10	3.1	1	2.0	6	3.9	72	11.7	31	1	5	25	·	2	1	·	19	15	12	2	3	5	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	659	25.0	9. V	26	51	146	12	—	—	—	—	155	115	10	31	71	—

Kołno — $H_s = 128\,m$ — $h_w = 16.5\,m$

I	6	5.2	14	5.1	6	3.8	13	4.6	2.6	5.3	13	6.6	4	3.5	4	10.2	7	5.0	35	5.8	8	3	11	27	·	6	1	5	20	15	13	·	6	23	—
II	15.5	7.6	11	7.5	·	·	3	3.3	5	7.5	12.5	7.8	15	5.2	8	6.1	14	5.6	43	8.9	10	14	23	27	·	10	1	3	13	14	11	·	3	28	—
III	8	5.1	7	2.1	2.5	1.8	5	2.8	14	5.3	16	3.9	13.5	4.7	4	14.5	23	3.6	21	6.0	4	5	7	24	·	4	2	6	14	12	6	·	11	22	—
IV	8	5.6	7.5	4.3	19.5	7.0	22.5	6.4	17	6.1	5	4.4	2.5	3.2	8	8.2	·	6.2	39	12.4	27	·	·	10	·	7	3	3	15	8	7	1	4	·	—
V	20	5.0	11	3.9	13.5	5.0	2.5	3.6	9.5	3.5	7.5	4.9	8.5	6.9	6.5	7.2	14	4.2	73	24.3	19	·	·	3	·	6	1	3	13	14	10	2	2	·	—
VI	15	4.9	7.5	5.0	9.5	5.9	10	6.4	4	7.8	14	4.5	11	6.6	12	5.8	7	5.2	43	19.1	13	·	·	·	4	5	·	7	9	12	7	2	·	·	—
VII	2	3.2	8.5	6.4	2	2.5	10	4.0	9	4.9	33.5	7.0	9.5	7.7	12.5	4.4	6	5.5	107	33.3	31	·	·	·	4	10	·	5	11	14	11	3	2	·	—
VIII	19	3.9	1	2.0	·	·	·	·	10.5	4.1	18.5	4.6	13	3.8	15	4.3	16	3.4	74	26.7	26	·	·	·	8	1	·	4	8	12	8	2	5	·	—
IX	·	·	1.5	2.0	1.5	2.0	10.5	5.5	13	3.9	19.5	5.8	20	4.8	3	1.7	21	3.6	50	24.0	29	·	·	·	3	4	1	8	7	9	7	1	7	·	—
X	7.5	3.7	0.5	2.0	1.5	4.3	4.5	2.6	7	3.6	12	5.8	19.5	4.9	9.5	4.4	31	3.0	17	8.5	16	·	·	4	·	1	·	3	13	8	4	·	14	·	—
XI	4	6.9	13.5	5.8	6.5	3.6	10	7.4	11	6.2	15	9.0	12.5	6.9	4.5	3.8	13	5.7	42	8.5	30	7	14	20	·	9	2	·	18	19	10	·	10	18	—
XII	1	12.0	·	·	·	·	10.5	6.3	20.5	5.6	31	5.9	11	4.4	6	3.7	13	4.8	45	9.1	18	3	9	26	·	5	·	·	26	20	11	·	4	23	—
Rok	106	5.3	83	3.8	62.5	3.0	101.5	4.4	146.5	5.3	197.5	5.8	140	5.2	93	6.2	165	4.6	589	33.3	31. VII	32	64	141	19	68	11	47	167	157	105	11	68	114	—

Sokółka — φ = 53°24' — λ = 23°30' — 1965

Miesiąc	Ciśnienie p: P_m	Max	Min	$P_{o.m}$	Temperatura T: Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	−0.8	−5.6	2.7	18	−15.1	11	−3.8	−2.3	−3.5	−3.3	4.4	4.7	4.5	4.5	91	87	90	89	0.4	0.6	0.4	0.5	8.7	8.0	7.7	8.1
II	–	–	–	–	−3.7	−11.5	1.3	14	−25.5	6	−8.5	−5.6	−7.8	−7.4	3.2	3.4	3.3	3.3	92	80	90	87	0.3	0.8	0.4	0.5	8.4	6.9	5.8	7.0
III	–	–	–	–	2.8	−4.8	9.5	16	−20.8	1	−3.4	1.6	−1.3	−1.1	4.7	5.1	4.8	4.9	91	72	83	82	0.5	2.1	0.9	1.2	7.0	6.1	4.8	6.0
IV	–	–	–	–	9.8	1.1	16.6	27	−5.2	3	3.0	8.3	4.7	5.2	6.4	6.4	6.9	6.6	82	57	78	72	1.4	5.0	1.9	2.8	6.8	6.7	6.1	6.5
V	–	–	–	–	13.5	3.9	21.1	18	−3.1	4	7.2	11.9	8.5	9.0	8.7	8.7	9.0	8.8	83	63	80	75	1.6	5.4	2.2	3.1	6.1	7.5	5.5	6.4
VI	–	–	–	–	20.1	10.6	27.6	26	2.9	8	14.0	18.2	14.8	15.5	13.2	13.0	13.7	13.3	82	64	81	76	3.0	8.3	3.4	4.9	6.1	7.3	6.7	6.7
VII	–	–	–	–	21.2	11.1	28.9	16	5.9	5	14.6	19.3	15.3	16.1	13.7	12.9	13.5	13.4	82	58	78	73	3.2	10.1	4.2	5.8	3.3	6.8	5.7	5.3
VIII	–	–	–	–	21.0	10.1	27.6	7	5.3	31	12.9	19.5	14.0	15.1	13.1	13.8	13.9	13.6	88	61	87	79	2.0	9.7	2.4	4.7	5.6	5.7	5.0	5.4
IX	–	–	–	–	20.7	9.0	27.2	4	3.2	21	11.1	19.2	12.8	14.0	12.1	12.8	12.8	12.6	91	58	85	78	1.3	10.0	2.4	4.6	4.7	4.9	3.0	4.2
X	–	–	–	–	11.2	2.8	19.4	1	−5.1	21	4.6	10.1	6.1	6.7	8.1	9.1	8.5	8.6	94	73	89	85	0.5	3.5	1.1	1.7	8.5	7.2	5.5	7.1
XI	–	–	–	–	−0.3	−4.9	10.9	2	−16.9	19	−3.2	−1.4	−2.9	−2.6	4.9	5.0	4.9	4.9	92	84	91	87	0.4	1.1	0.5	0.7	8.9	8.4	7.8	8.4
XII	–	–	–	–	0.7	−3.6	7.1	20	−12.9	18	−1.8	−0.3	−1.2	−1.1	5.1	5.4	5.2	5.3	94	90	91	92	0.4	0.6	0.5	0.5	7.7	8.4	7.8	8.0
Rok	–	–	–	–	9.7	1.5	28.9	16.VII	−25.5	6, 11	3.9	8.2	5.0	5.5	8.1	8.4	8.4	8.3	88	71	85	81	1.2	4.8	1.7	2.6	6.8	7.0	6.0	6.6

Zawodzie — φ = 53°23' — λ = 21°24'

I	–	–	–	–	0.2	−4.9	4.7	9	−19.9	11	−2.8	−1.0	−2.4	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	7.7	8.0
II	–	–	–	–	−2.4	−10.9	1.9	17	−29.1	6	−7.8	−4.0	−6.2	−6.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.8	−5.6	10.6	30	−25.1	9	−3.3	2.6	−1.0	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.0	1.7	16.1	29	−5.3	3	4.0	8.7	5.9	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	7.9	7.3
V	–	–	–	–	14.1	3.5	20.4	18	−2.3	3	8.0	12.8	8.4	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.7	5.1	5.7
VI	–	–	–	–	20.7	9.7	29.4	26	1.7	8	14.4	19.3	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.3	5.2	4.9
VII	–	–	–	–	20.7	9.7	30.6	15	3.7	5	14.0	19.4	14.4	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.0	5.8	5.8	5.2
VIII	–	–	–	–	20.5	9.3	27.3	25	4.2	17, 18	12.6	19.1	14.0	14.9	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.7	5.1	5.2
IX	–	–	–	–	20.4	8.2	27.8	3	2.1	21	11.0	19.2	13.9	14.5	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.5	3.8	4.4
X	–	–	–	–	11.7	3.4	19.4	1	−5.4	21	5.1	10.9	7.4	7.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.5	6.1	6.3
XI	–	–	–	–	−0.2	−4.5	10.4	2	−19.9	24	−2.8	−0.7	−1.9	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.6	9.0	9.0
XII	–	–	–	–	1.8	−2.8	10.4	20	−18.1	17	−0.5	0.8	−0.3	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	7.6	8.3
Rok	–	–	–	–	10.1	1.4	30.6	15.VII	−29.1	6, 11	4.3	8.9	5.6	6.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Nidzica — φ = 53°22' — λ = 20°25'

I	–	–	–	–	−0.2	−4.8	4.3	18	−18.4	11	−2.5	−1.0	−2.5	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.7	7.2	8.0
II	–	–	–	–	−2.6	−11.2	1.5	14	−27.2	6	−7.7	−4.2	−7.0	−6.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.9	6.5	7.3
III	–	–	–	–	2.9	−6.5	8.8	27, 28	−24.5	8	−4.2	1.6	−1.9	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.8	5.5	6.1
IV	–	–	–	–	9.4	1.5	14.9	30	−3.8	3	3.3	7.5	5.1	5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.4	6.8	7.7
V	–	–	–	–	13.6	3.8	19.3	18	−4.2	4	7.4	12.0	8.1	8.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.3	6.3	6.7
VI	–	–	–	–	20.6	9.8	28.4	26	4.2	8	14.1	19.1	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.7	6.1	6.2
VII	–	–	–	–	20.6	9.8	29.4	15	1.8	5	14.3	18.8	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.4	5.9	6.4
VIII	–	–	–	–	20.3	9.5	27.3	22	3.0	31	13.0	18.6	13.8	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.1	5.1	6.0
IX	–	–	–	–	19.8	8.2	26.9	3	0.8	16	10.8	18.2	12.5	13.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.7	4.3	5.2
X	–	–	–	–	11.7	3.0	20.9	1	−5.7	21	4.7	10.5	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	5.3	6.7
XI	–	–	–	–	0.3	−5.2	10.4	2	−21.8	24	−3.1	−0.9	−2.6	−2.3	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.4	8.1	8.6
XII	–	–	–	–	0.6	−3.6	8.2	19	−21.8	17	−1.6	−0.6	−1.4	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.3	8.4	8.5
Rok	–	–	–	–	9.8	1.2	29.4	15.VII	−27.2	6, 11	4.0	8.3	4.9	5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	6.3	6.9

Lipki — φ = 53°21' — λ = 14°58'

I	–	–	–	–	2.4	−1.2	8.4	17	−8.6	31	0.1	1.7	0.3	0.6	5.6	5.9	5.6	5.7	90	85	88	88	0.6	1.1	0.7	0.8	9.5	8.7	7.3	8.5
II	–	–	–	–	0.3	−5.5	4.0	13	−20.4	28	−3.7	−0.9	−2.2	−2.2	4.2	4.8	4.6	4.5	87	83	87	86	0.6	1.0	0.7	0.8	8.1	7.9	7.9	8.0
III	–	–	–	–	3.8	−4.6	13.2	29	−19.3	8	−2.9	2.5	−0.6	−0.4	4.9	5.9	5.5	5.4	90	78	89	86	0.5	1.7	0.6	0.9	6.5	6.4	5.5	6.1
IV	–	–	–	–	11.4	2.5	16.0	6	−4.3	5	4.4	9.6	6.1	6.6	7.8	7.7	8.0	7.8	92	65	85	81	0.7	4.4	1.5	2.2	7.6	8.2	7.7	7.8
V	–	–	–	–	15.0	5.8	20.6	17	0.3	3	8.6	13.5	9.9	10.5	9.4	9.0	9.9	9.4	83	59	80	74	1.8	6.7	2.5	3.7	6.0	6.7	7.0	6.6
VI	–	–	–	–	21.3	10.5	27.9	26	4.5	4	14.6	19.6	14.9	16.0	13.0	12.6	13.4	13.0	78	56	79	71	3.8	10.8	3.8	6.1	4.5	5.7	5.2	5.1
VII	–	–	–	–	19.7	10.9	29.2	14	6.2	5	13.5	17.8	14.2	14.9	13.7	14.3	14.1	14.0	88	78	86	81	2.0	6.7	2.3	3.7	7.1	7.8	7.5	7.5
VIII	–	–	–	–	20.6	9.9	27.9	22	4.8	13	13.0	18.8	14.3	15.1	14.0	13.6	14.2	13.9	93	63	87	81	1.1	8.6	2.3	4.0	5.1	6.9	6.0	6.0
IX	–	–	–	–	19.2	9.6	25.1	3	5.3	30	11.5	17.9	12.9	13.8	12.4	13.6	13.1	13.0	91	67	88	82	1.3	7.3	2.1	3.6	6.2	5.8	5.8	5.9
X	–	–	–	–	13.0	3.4	22.4	1	−3.3	23	5.0	11.8	6.6	7.5	8.6	10.2	9.2	9.3	96	74	92	87	0.4	3.9	0.9	1.7	6.2	5.7	5.3	5.7
XI	–	–	–	–	2.6	−2.9	12.3	1, 2	−17.2	23	−1.3	1.3	−0.6	−0.3	5.5	6.0	5.6	5.7	92	83	90	88	0.4	1.2	0.6	0.7	7.8	7.7	7.4	7.6
XII	–	–	–	–	3.2	−0.9	11.8	19	−6.4	14	0.6	1.8	0.9	1.0	5.9	6.2	6.1	6.1	91	89	93	91	0.6	0.9	0.5	0.7	9.8	8.6	8.5	9.0
Rok	–	–	–	–	11.0	3.1	29.2	14.VII	−20.4	28, 11	5.3	9.6	6.4	6.9	8.8	9.2	9.1	9.0	89	73	87	83	1.2	4.5	1.5	2.4	7.0	7.2	6.8	7.0

Sokółka — $H_s = 180$ m — $h_w = 13$ m — 1965

MIESIĄC	ROZKŁAD WIATRU (n,v) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	V ≥15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K
I	7.5	4.1	4	4.0	13	7.2	25.5	4.2	22	5.2	4.5	4.7	4	13.0	2.5	9.4	10	4.9	40	9.3	30	5	17	28	·	7	1	2	20	17	7	·	6	31	·
II	18.5	4.2	9.5	5.0	0.5	5.0	2	4.0	7	6.6	16	5.5	16	5.2	4.5	6.3	10	4.5	43	10.1	7	13	23	28	·	3	·	2	14	23	10	1	1	28	·
III	6	3.8	6.5	1.9	13	4.9	12	3.5	19.5	4.1	9.5	4.6	12.5	4.7	1	5.0	13	3.5	32	7.2	2	4	9	24	·	2	2	5	10	17	9	·	5	28	·
IV	6	4.7	9	5.1	30.5	6.9	27	6.4	9	3.7	1.5	4.7	2.5	3.2	3.5	4.1	1	5.8	16	8.7	23	·	·	12	·	7	1	4	10	7	4	·	2	·	1
V	21	3.8	7.5	2.7	16.5	5.1	6.5	3.5	9.5	4.0	6.5	3.8	5.5	3.9	7	4.3	13	3.5	108	45.3	29	·	·	3	·	2	1	4	13	16	11	2	3	·	2
VI	6.5	2.2	7	4.9	17	3.4	5	1.4	10	3.2	9.5	3.8	16.5	3.6	6.5	3.6	12	2.9	85	39.0	13	·	·	·	1	·	·	1	13	13	11	2	·	·	1
VII	2.5	3.6	4.5	3.8	4.5	2.7	8.5	2.1	19	2.4	25	4.2	11	4.3	2	2.0	16	2.8	76	14.9	30	·	·	·	3	2	·	3	4	14	12	3	·	·	2
VIII	10.5	3.5	0.5	6.0	7	4.0	12.5	4.2	9.5	3.4	8.5	4.4	20.5	3.9	7	3.6	17	3.2	63	25.5	2	·	·	·	7	·	·	5	7	11	8	2	·	·	4
IX	1	3.0	·	·	10.5	4.4	19	4.6	19.5	4.3	12	5.2	7.5	3.9	1.5	3.7	19	3.5	34	9.2	29	·	·	·	2	2	·	7	2	8	7	·	2	·	3
X	10	2.4	·	·	5.5	5.5	0.5	6.0	22	3.1	19	3.8	17	5.0	4	2.9	15	3.2	14	6.8	16	·	·	6	·	·	·	2	15	8	3	·	10	·	·
XI	4	4.0	16.5	4.5	11	5.2	9	6.9	14	5.5	18.5	5.9	10	4.3	1	4.0	6	4.9	47	9.4	21	6	16	22	·	4	·	1	19	22	10	·	5	18	·
XII	·	·	1.5	5.7	5.5	5.4	9.5	6.3	34	6.0	19.5	5.9	16	3.6	·	·	7	5.1	36	7.9	19	4	10	27	·	4	·	·	18	21	8	·	3	31	·
Rok	93.5	3.3	66.5	3.6	134.5	5.0	137	4.4	195	4.3	150	4.7	139	4.9	40.5	4.1	139	4.0	594	45.3	29.V	32	75	150	13	33	5	36	145	177	100	10	37	136	13

Zawodzie — $H_s = 122$ m — $h_w =$ 12 m I–VIII, 13,3 m IX–XII

I	2	1.5	4.5	4.0	12	2.9	10.5	2.7	24	2.3	13	2.7	7.5	8.3	6.5	5.4	13	2.9	48	11.0	30	3	10	27	-	2	1	1	20	11	10	1	–	22	–
II	17	4.0	6	3.7	·	·	·	·	5.5	7.4	15.5	5.1	18	3.9	8	4.6	14	3.8	31	7.1	7	13	21	26	·	5	·	–	–	12	10	·	–	28	–
III	5.5	1.8	11.5	2.4	8.5	2.2	9.5	2.4	11	5.2	8	2.3	16.5	3.7	3.5	9.1	19	2.7	36	8.0	20	6	7	24	·	3	·	–	–	12	8	·	–	22	–
IV	6	3.1	15	4.5	18.5	4.8	18	4.4	7	3.9	4.5	4.4	4	1.8	7	4.6	10	3.8	67	13.0	23	·	·	11	·	3	1	2	14	11	10	1	–	·	–
V	7	2.8	14	3.9	13	3.7	4.5	5.0	2	2.5	5	3.3	8.5	3.8	23	4.4	16	3.2	71	22.0	9	·	·	6	·	2	·	7	10	11	9	2	–	·	–
VI	10.5	2.7	9	4.7	12	4.8	2	6.0	3	3.0	16	4.8	15	3.9	11.5	4.6	11	3.7	42	12.0	1	·	·	·	3	3	1	6	5	12	8	1	–	·	–
VII	1	2.0	3	2.0	3	1.7	3	3.2	12	2.1	33.5	5.2	15.5	3.8	·	·	19	3.1	83	20.8	31	·	·	·	4	4	2	5?	6?	17	11	2	–	·	–
VIII	6	2.4	3	1.7	1.5	1.7	3	2.7	4	3.0	17.5	4.0	23	2.7	17	4.0	18	2.6	95	49.0	26	·	·	·	8	·	·	7	7	13	7	2	–	·	–
IX	9.5	3.2	16	4.4	26	5.5	9	1.3	4	4.0	6	5.2	·	·	1.5	2.3	18	3.4	55	38.0	29	·	·	·	1	4	2	11	4	9	7	1	–	·	–
X	6.5	2.0	9	3.1	6.5	3.3	·	·	5	3.8	9.5	4.1	22	3.7	16.5	3.3	18	2.7	14	6.5	16	·	·	6	·	2	·	4	11	6	4	·	–	·	–
XI	3.5	2.4	8	2.4	12.5	3.9	12.5	4.2	8.5	2.6	14	7.3	15.5	3.3	3.5	2.4	12	3.5	44	13.3	21	7	15	19	·	2	1	·	25	17	7	1	–	16	–
XII	·	·	·	·	1	1.0	14	4.0	17	7.0	33.5	5.5	16.5	4.2	2	3.0	9	4.7	43	12.0	18	4	5	20	·	7	3	·	19	15	14	1	–	15	–
Rok	74.5	2.3	99	3.1	114.5	3.0	86	3.0	103	3.9	176	4.5	162	3.6	100	4.0	177	3.3	629	49.0	26.VIII	33	58	139	16	37	11	–	–	146	105	12	–	103	–

Nidzica — $H_s = 170$ m — $h_w = 13$ m

I	7	1.7	5	3.0	6	1.8	12	3.8	14.5	3.7	24.5	5.3	0.5	8.0	9.5	4.9	14	3.4	54	13.5	30	3	13	29	·	1	1	·	18	15	11	1	9	22	·
II	12.5	4.6	9.5	3.9	0.5	2.0	1	3.0	2	4.0	22.5	5.4	2.5	2.8	21.5	4.7	12	4.0	43	4.4	7, 13	12	24	27	·	2	·	·	10	22	18	·	3	28	·
III	6	2.7	3	2.3	2	3.5	8	2.6	13.5	4.1	10	4.4	11.5	3.8	9	5.0	30	2.6	33	10.4	3	9	9	25	·	2	·	3	12	13	9	1	10	23	·
IV	9	4.6	13.5	3.9	12	4.4	25	4.2	5	5.2	9	3.3	1	6.0	8.5	3.2	7	3.8	56	8.2	23	·	·	9	·	1	·	·	17	15	15	·	3	·	·
V	19	3.2	18.5	2.9	7.5	3.1	9	4.2	3	3.8	10.5	4.5	4.5	3.4	8	4.0	13	3.1	57	16.0	19	·	·	6	·	1	·	3	10	15	11	1	6	·	1
VI	7	4.2	7	3.5	6.5	3.8	6.5	4.1	10	3.6	8.5	6.5	14	5.5	22.5	4.2	8	4.1	50	9.7	22	·	·	·	3	2	·	·	7	14	13	·	·	·	4
VII	3	3.7	8	3.0	1	2.0	8.5	3.2	6.5	3.8	44	6.2	8.5	5.1	5.5	2.0	8	4.5	100	33.6	8	·	·	·	3	4	1	1	6	17	12	3	1	·	5
VIII	8	3.2	1	2.0	·	·	9.5	4.0	9	4.4	15	4.7	9	3.6	22.5	3.2	19	3.0	118	42.4	26	·	·	·	7	·	·	2	10	13	12	4	1	·	2
IX	·	·	2	2.0	4.5	4.3	15.5	3.6	13.5	3.9	22.5	4.7	5	4.2	6	4.3	21	3.2	80	29.4	4	·	·	·	1	2	2	6	5	10	9	2	3	·	1
X	6.5	2.2	1	4.0	6	2.2	5	2.8	2	2.0	23.5	4.4	9.5	3.9	19.5	3.7	20	2.8	26	9.2	17	·	·	6	·	·	·	1	11	8	7	·	12	·	·
XI	5	2.1	19	2.5	2.5	3.6	7.5	4.9	8.5	5.5	20	6.8	8.5	4.1	3	2.7	16	3.7	59	13.6	21	7	14	21	·	3	·	1	23	18	14	1	6	16	·
XII	·	·	·	·	·	·	8.5	5.2	13.5	4.5	40	6.0	7.5	4.1	7.5	4.4	16	4.4	67	16.0	18	4	10	25	·	4	1	1	20	20	17	1	4	24	·
Rok	83	2.7	87.5	2.8	48.5	2.6	116	3.8	101	4.0	250	5.2	82	4.5	143	3.9	184	3.6	743	42.4	26.VIII	35	70	148	14	22	5	18	149	180	148	14	58	113	13

Lipki — $H_s = 30$ m — $h_w = 10$ m

I	9.5	2.8	7	3.1	8.5	3.7	12.5	4.7	17	5.9	12.5	6.0	7.5	4.5	7.5	4.0	6	4.4	38	8.1	8	·	3	23	·	4	·	·	23	15	11	·	7	8	·
II	10	4.4	3.5	4.4	2.5	4.8	2.5	4.4	2.5	3.8	15	5.7	22.5	6.4	19.5	5.9	6	5.2	19	3.8	13, 26	4	10	24	·	7	2	·	15	12	5	·	2	20	·
III	9	6.1	5	4.6	9	3.6	14	3.4	13	2.7	7.5	3.9	9.5	5.8	9	6.0	17	3.6	14	5.3	21	8	8	22	·	3	·	8	15	7	4	·	7	17	·
IV	7	3.9	16.5	5.2	13	4.9	13	4.7	10	5.4	8	5.7	9	4.1	9.5	4.5	4	4.6	53	11.3	19	·	·	3	·	5	·	2	19	15	11	1	4	·	3
V	13.5	5.6	11	4.3	13.5	4.7	9.5	5.2	2.5	4.4	5.5	4.1	11	6.2	12.5	4.9	14	4.3	73	29.5	9	·	·	·	·	4	1	3	13	13	10	2	1	·	2
VI	8.5	4.8	10.5	4.0	6	3.8	7.5	4.4	8	4.8	13.5	5.7	13.5	5.1	12.5	4.3	10	4.2	70	22.5	26	·	·	·	4	2	·	6	5	8	8	3	·	·	5
VII	7.5	4.3	2	4.0	5	3.8	3.5	4.1	6.5	4.4	33.5	5.2	16	6.6	3	5.2	16	4.1	98	31.8	14	·	·	·	3	4	·	2	14	17	13	2	2	·	4
VIII	6.5	3.0	5	2.9	6.5	3.5	4.5	3.9	6	3.3	20.5	3.8	14.5	3.8	9.5	2.8	21	2.7	37	12.5	8	·	·	·	4	·	·	2	7	9	7	2	3	·	2
IX	2.5	2.8	2	3.8	11	5.5	14.5	3.7	14.5	5.1	23.5	4.3	10.5	4.2	1.5	3.7	10	3.9	90	36.7	9	·	·	·	1	4	·	4	8	9	8	3	1	·	1
X	6	2.6	3	3.2	11.5	2.7	8.5	3.1	12	3.5	10.5	5.0	8.5	4.1	7	3.7	26	2.5	19	12.1	31	·	·	5	·	1	·	4	8	6	4	1	11	·	1
XI	2	8.5	17	3.4	9	5.3	6.5	4.8	12.5	8.0	22	6.6	3	6.5	5	5.5	13	4.9	23	7.7	21	4	11	19	·	8	·	2	17	11	6	·	4	7	·
XII	1.5	2.3	1.5	3.0	6.5	3.8	13	6.1	15.5	6.4	35	7.3	11.5	6.3	5.5	5.4	3	6.1	52	14.3	9	·	3	23	·	10	1	·	24	19	12	2	1	5	·
Rok	83.5	4.3	84	3.8	101	4.2	109.5	4.4	120	4.8	212	5.3	137	5.2	102	4.7	146	4.2	586	36.7	9. IX	16	35	119	12	52	4	33	168	141	99	16	43	57	12

Wałcz

$\varphi = 53°17'$ $\lambda = 16°28'$ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	996.2	1011.9	973.7	1011.0	2.1	−2.1	6.7	17	−9.0	11	−0.6	1.1	−0.1	0.1	5.5	5.8	5.6	5.6	93	86	90	90	0.4	0.9	0.6	0.6	8.7	8.1	7.7	8.2
II	1002.2	1019.9	973.7	1017.2	−0.1	−6.7	3.0	13	−14.5	24	−4.5	−1.0	−3.2	−3.0	4.1	4.4	4.2	4.2	88	76	85	83	0.5	1.3	0.7	0.8	8.3	7.9	7.1	7.7
III	1001.9	1017.5	976.1	1016.7	4.8	−4.2	15.1	29	−23.3	8	−2.7	3.4	0.3	0.3	4.9	5.9	5.5	5.4	90	73	83	82	0.5	2.2	1.1	1.3	6.7	5.8	5.0	5.8
IV	996.9	1017.7	977.3	1011.4	11.3	2.5	15.8	6	−3.6	5	4.0	9.9	6.4	6.7	7.6	7.8	8.0	7.8	92	64	83	80	0.7	4.6	1.7	2.3	7.4	8.0	5.8	7.1
V	1000.0	1015.1	981.5	1014.3	14.9	5.3	20.9	17	−2.1	3	8.2	13.4	9.9	10.4	9.5	9.4	9.3	9.4	86	62	76	75	1.5	6.3	3.1	3.6	6.8	6.9	6.3	6.7
VI	1000.3	1010.7	986.1	1014.3	21.6	10.5	30.5	26	5.4	15	14.5	20.3	15.7	16.6	13.5	13.8	14.0	13.8	81	58	79	73	3.2	10.6	4.0	5.9	5.0	7.0	5.6	5.9
VII	997.0	1007.5	981.2	1011.0	20.0	11.1	30.7	14	6.1	5	14.1	18.5	14.9	15.6	14.3	14.4	14.6	14.4	88	68	85	80	2.0	7.6	2.7	4.1	6.6	8.0	6.0	6.9
VIII	1001.4	1009.8	989.7	1015.4	20.9	10.1	28.6	23	5.3	14	12.9	19.7	14.6	15.4	13.8	14.3	14.5	14.2	92	63	86	80	1.3	9.1	2.4	4.3	5.9	6.7	3.4	5.3
IX	999.4	1019.9	987.6	1013.5	19.7	9.7	26.3	3	4.4	16	11.4	18.6	13.4	14.2	12.6	14.1	13.7	13.5	93	67	89	83	1.0	7.7	1.8	3.5	6.6	6.5	4.3	5.8
X	1008.7	1023.6	993.0	1023.3	13.0	3.3	21.5	1	−4.3	22	5.0	12.2	6.5	7.6	8.6	10.3	9.2	9.4	95	72	93	87	0.4	4.1	0.8	1.8	7.0	6.4	2.8	5.4
XI	996.7	1016.2	966.5	1011.5	1.7	−3.1	12.5	1	−12.9	17	−1.4	0.9	−0.8	−0.5	5.3	5.9	5.5	5.6	90	84	87	87	0.6	1.1	0.8	0.8	9.0	7.8	6.9	7.9
XII	989.0	1010.3	961.5	1003.7	2.6	−1.4	11.7	19	−10.5	17	0.3	1.4	0.6	0.7	5.7	5.8	6.0	5.8	89	85	90	88	0.7	1.1	0.6	0.8	9.4	8.3	8.5	8.7
Rok	999.1	1023.6	961.5	1013.6	11.0	2.9	30.7	14.VII	−23.3	8.III	5.1	9.9	6.5	7.0	8.8	9.3	9.2	9.1	90	72	86	83	1.1	4.7	1.7	2.5	7.3	7.3	5.8	6.8

Lidzbark

$\varphi = 53°16'$ $\lambda = 19°50'$

I	–	–	–	–	0.9	−4.3	4.8	1	−16.5	11	−2.0	−0.5	−2.0	−1.6	5.1	5.3	5.1	5.2	94	88	93	92	0.3	0.7	0.3	0.4	9.7	7.7	7.9	8.4
II	–	–	–	–	−2.4	−10.1	1.9	14	−22.6	6	−7.0	−3.7	−5.9	−5.6	3.4	3.9	3.7	3.7	88	82	87	86	0.4	0.8	0.4	0.5	8.5	6.8	8.1	7.8
III	–	–	–	–	3.2	−5.8	9.2	16, 30	−25.5	8	−4.1	2.1	−1.3	−1.2	4.7	5.7	5.3	5.2	94	80	90	88	0.3	1.7	0.6	0.9	8.4	6.4	7.7	7.5
IV	–	–	–	–	9.3	1.7	14.9	30	−3.9	3	3.4	7.8	5.1	5.4	7.2	7.6	7.4	7.4	90	72	83	82	0.8	3.1	1.5	1.8	8.4	8.2	8.1	8.2
V	–	–	–	–	13.4	4.1	19.4	18	−3.8	4	7.8	12.0	8.5	9.2	8.9	8.7	9.0	8.9	83	62	79	75	1.8	5.5	2.4	3.2	6.3	6.9	6.7	6.6
VI	–	–	–	–	20.7	10.4	29.6	26	5.2	8	13.9	19.2	14.8	15.7	12.9	12.4	13.2	12.8	81	58	78	72	3.2	10.4	3.8	5.8	5.2	5.9	7.8	6.3
VII	–	–	–	–	20.5	10.3	29.8	15	3.1	10	14.4	18.8	14.8	15.7	13.5	13.2	13.9	13.5	81	61	82	75	3.2	9.2	3.3	5.2	6.4	6.4	8.0	6.9
VIII	–	–	–	–	20.4	10.1	27.2	22, 23	4.4	31	12.8	18.6	14.3	15.0	13.6	13.5	14.4	13.8	91	64	88	81	1.5	8.8	2.3	4.2	6.6	6.7	8.4	7.2
IX	–	–	–	–	19.4	8.9	26.6	3	2.1	16	11.0	18.2	12.6	13.6	12.6	13.4	13.3	13.1	95	65	90	83	0.7	7.9	1.6	3.4	7.0	4.9	4.6	5.5
X	–	–	–	–	11.7	3.5	19.4	1	−4.3	22	5.1	10.7	6.9	7.4	8.5	9.9	9.4	9.3	95	76	93	88	0.5	3.3	0.7	1.5	8.5	6.5	6.9	7.3
XI	–	–	–	–	0.2	−5.2	10.8	2	−22.0	24	−2.9	−0.9	−2.3	−2.1	5.0	5.2	5.2	5.1	92	85	92	90	0.5	0.9	0.4	0.6	9.7	8.0	9.0	8.9
XII	–	–	–	–	1.1	−3.0	9.7	19	−19.2	17	−1.0	0.1	−0.7	−0.6	5.4	5.5	5.5	5.5	92	87	90	90	0.5	0.8	0.6	0.6	9.9	8.7	9.2	9.3
Rok	–	–	–	–	9.9	1.7	29.8	15.VII	−25.5	8.III	4.3	8.5	5.4	5.9	8.4	8.7	8.8	8.6	90	73	87	83	1.1	4.4	1.5	2.3	7.9	6.9	7.7	7.5

Kisielnica

$\varphi = 53°15'$ $\lambda = 22°07'$

I	–	–	–	–	−0.1	−4.6	3.9	18	−16.0	11	−3.2	−1.8	−2.4	−2.4	4.7	5.0	4.8	4.8	93	90	91	91	0.3	0.5	0.4	0.4	8.2	7.8	7.1	7.7
II	–	–	–	–	−3.3	−12.2	1.9	12	−29.4	6	−9.1	−5.1	−7.6	−7.4	3.2	3.7	3.5	3.5	91	85	92	89	0.3	0.6	0.3	0.4	7.9	6.5	5.9	6.8
III	–	–	–	–	3.0	−5.1	10.6	30	−22.1	9	−3.7	1.9	−1.6	−1.2	4.7	5.5	5.2	5.1	93	78	91	87	0.3	1.7	0.5	0.8	6.4	5.1	4.9	5.5
IV	–	–	–	–	10.1	1.9	15.5	28	−3.6	3	3.5	8.7	5.1	5.6	7.3	7.5	7.5	7.4	91	66	84	80	0.7	4.1	1.4	2.1	6.8	8.3	6.4	7.2
V	–	–	–	–	13.6	4.3	21.0	18	−2.9	4	7.4	12.4	8.1	9.0	8.9	8.8	9.0	8.9	84	60	81	75	1.6	5.8	2.0	3.1	6.1	8.1	6.0	6.7
VI	–	–	–	–	20.4	10.4	27.0	26	3.7	8	14.2	19.0	14.6	15.6	13.1	13.0	13.2	13.1	80	60	80	73	3.2	9.3	3.5	5.3	5.5	6.6	5.8	6.0
VII	–	–	–	–	20.8	10.0	29.3	16	4.5	5, 11	14.8	19.5	14.5	15.8	13.9	13.2	13.6	13.6	82	58	82	74	3.2	10.0	3.1	5.4	4.3	6.9	6.4	5.9
VIII	–	–	–	–	20.6	9.6	28.3	7	4.5	17	13.2	19.1	13.3	14.7	13.5	14.1	13.2	13.6	89	65	86	80	1.9	8.9	2.4	4.4	5.3	6.8	4.1	5.4
IX	–	–	–	–	20.6	8.3	27.7	3	1.6	21	10.7	19.3	12.6	13.8	12.1	13.5	12.7	12.8	93	60	86	80	1.0	9.3	2.2	4.2	5.1	5.4	2.3	4.3
X	–	–	–	–	11.3	2.7	18.9	1	−4.6	21	4.4	10.3	6.1	6.7	8.0	9.6	8.5	8.7	93	75	89	86	0.6	3.2	1.1	1.6	6.6	7.8	4.6	6.3
XI	–	–	–	–	0.1	−5.1	10.9	2	−22.6	24	−3.0	−1.0	−2.5	−2.3	4.8	5.1	5.1	5.0	90	85	91	89	0.5	1.0	0.5	0.7	9.3	8.3	7.3	8.3
XII	–	–	–	–	0.9	−3.3	7.9	10	−16.1	16, 17	−1.4	−0.3	−0.8	−0.8	5.1	5.3	5.2	5.2	89	87	89	88	0.6	0.8	0.7	0.7	9.2	9.3	8.4	9.0
Rok	–	–	–	–	9.8	1.4	29.3	16.VII	−29.4	6.II	4.0	8.5	5.0	5.6	8.3	8.7	8.5	8.5	89	72	87	83	1.2	4.6	1.5	2.4	6.7	7.2	5.8	6.6

Kopna Góra

$\varphi = 53°15'$ $\lambda = 23°29'$

I	–	–	–	–	−0.8	−6.3	3.4	18	−20.2	11	−4.0	−2.3	−3.7	−3.4	4.6	4.9	4.6	4.7	96	91	94	94	0.2	0.4	0.3	0.3	8.6	8.1	7.2	8.0
II	–	–	–	–	−3.5	−11.8	2.2	14	−28.0	7	−9.3	−5.0	−8.0	−7.6	3.2	3.7	3.4	3.4	94	83	93	90	0.2	0.6	0.2	0.3	8.3	6.4	5.0	6.6
III	–	–	–	–	3.7	−6.1	10.6	30	−25.4	9	−4.2	2.8	−1.5	−1.1	4.6	5.1	5.0	4.9	92	68	88	83	0.4	2.6	0.7	1.2	7.3	5.5	5.3	6.0
IV	–	–	–	–	10.1	1.4	17.1	27	−7.4	3	3.6	8.7	5.0	5.6	6.6	6.2	6.9	6.6	82	56	77	72	1.6	5.4	2.1	3.0	6.5	5.9	6.1	6.2
V	–	–	–	–	13.6	2.8	20.6	18	−6.9	4	7.3	12.2	7.7	8.7	8.8	8.6	9.2	8.9	84	60	85	76	1.6	5.8	1.6	3.0	5.6	7.1	5.5	6.1
VI	–	–	–	–	20.2	9.7	27.6	26	0.9	8	14.2	18.2	14.1	15.2	13.6	13.4	13.6	13.5	84	66	85	78	2.8	8.0	2.7	4.5	5.5	7.1	4.6	5.7
VII	–	–	–	–	21.5	9.9	29.6	15	3.4	2	14.6	20.1	14.5	15.9	13.9	13.3	13.6	13.6	83	57	83	74	3.0	10.7	3.2	5.6	3.7	5.9	5.2	4.9
VIII	–	–	–	–	21.0	9.4	28.6	25	3.4	19	12.7	20.0	14.0	15.2	13.1	13.8	14.0	13.6	89	60	88	79	1.9	10.3	2.4	4.9	5.6	5.1	4.5	5.1
IX	–	–	–	–	20.9	7.6	28.0	4	1.0	17	10.3	19.7	12.4	13.7	11.9	13.4	12.7	12.6	93	59	87	80	1.4	10.2	2.2	4.6	4.1	4.5	3.5	4.0
X	–	–	–	–	11.2	2.2	22.3	1	−7.7	21	4.1	10.2	6.1	6.6	8.0	9.3	8.6	8.6	95	74	91	87	0.4	3.5	1.0	1.6	7.7	7.0	5.5	6.7
XI	–	–	–	–	−0.1	−4.9	10.8	2	−21.0	17	−3.2	−1.0	−2.9	−2.5	5.0	5.3	5.0	5.1	95	88	94	92	0.3	0.9	0.4	0.5	9.2	8.2	7.9	8.4
XII	–	–	–	–	0.6	−3.6	6.6	19	−15.5	16	−1.7	−0.1	−1.3	−1.1	5.3	5.6	5.3	5.4	95	90	93	93	0.3	0.6	0.4	0.4	8.6	8.5	8.2	8.5
Rok	–	–	–	–	9.9	0.9	29.6	15.VII	−28.0	7.II	3.7	8.6	4.7	5.4	8.2	8.6	8.5	8.4	90	71	88	83	1.2	4.9	1.4	2.5	6.7	6.6	5.7	6.3

Wałcz

$H_s = 111\,m$ $H_b = 117{,}6\,m$ $h_w = 23\,m$ **1965**

MIESIĄC	ROZKŁAD WIATRU *0,V=0 N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10	Max<0°	Max<0°	Max≥25°	Wiatr V ≥10	≥15	◐	◒	Opad R ≥0,1	≥1,0	≥10,0	≡	⊠	K (K)
I	4	1.2	10	1.8	14	1.3	6	1.7	18	3.1	12	3.2	20.5	2.3	6.5	1.2	2	2.2	43	5.9	25	·	6	26	·	·	·	1	20	19	11	·	2	13	·
II	9	2.3	9	2.8	4	2.1	2.5	2.4	4.5	1.6	9.5	3.3	24.5	2.4	21	2.6	·	2.5	33	5.5	26	7	13	27	·	·	·	·	14	16	12	·	1	28	·
III	4	2.5	9	2.0	10	1.6	16	1.4	12.5	1.3	7.5	2.0	17.5	2.3	11.5	2.5	5	1.8	64	24.8	3	6	6	22	·	·	·	6	11	14	12	1	2	21	·
IV	8	1.1	13	2.5	26	2.7	10	3.4	2.5	3.2	8.5	2.1	9	2.2	11	2.0	2	2.4	37	8.8	28	·	·	5	·	·	·	2	13	11	10	·	3	·	·
V	11.5	2.0	18	1.8	20	3.0	3	5.7	5.5	1.5	4.5	3.2	12	2.9	16.5	1.8	2	2.4	85	30.0	9	·	·	2	·	3	·	4	15	17	15	1	·	·	·
VI	9.5	1.6	10.5	2.2	19	1.9	6	1.8	1	1.0	9	2.4	21	2.8	14	2.1	·	2.2	54	13.1	18	·	·	·	4	·	·	2	6	9	8	2	·	·	5
VII	3	1.7	8	2.0	9	1.7	7	1.7	4	1.5	24	2.6	31.5	2.7	5.5	2.4	1	2.3	89	14.9	14	·	·	·	2	·	·	2	12	21	14	2	·	·	5
VIII	5	1.5	2	1.0	6.5	1.7	3.5	2.6	5.5	1.7	11.5	2.1	25	1.6	17	1.1	17	1.3	50	14.0	6	·	·	·	5	·	·	2	4	12	9	1	1	·	2
IX	·	·	3	2.0	16.5	2.8	5.5	2.4	4.5	2.8	17	2.0	25.5	2.0	8	2.5	10	2.0	80	20.3	10	·	·	·	1	·	·	3	7	10	10	3	·	·	3
X	6	1.0	6	1.3	9.5	1.9	1.5	3.0	5.5	2.2	13.5	2.4	16	2.5	14	2.1	21	1.6	19	8.8	16	·	·	6	·	1	·	3	3	4	4	·	9	·	·
XI	2	2.0	19.5	2.1	11.5	3.4	6	3.5	8.5	2.2	13.5	3.8	17.5	2.7	6.5	2.0	5	2.6	63	20.9	21	5	12	18	·	·	·	1	19	13	10	2	4	16	·
XII	·	·	1.5	1.3	10.5	2.3	12	3.1	10	2.8	28	4.1	25.5	2.7	4.5	1.9	1	3.1	78	20.1	9	1	4	21	·	·	·	·	25	21	13	2	·	19	·
Rok	62	1.4	109.5	1.9	156.5	2.2	79	2.7	82	2.1	158.5	2.8	245.5	2.4	136	2.0	66	2.2	695	30.0	9.V	19	41	127	12	4	·	26	149	167	128	14	22	97	15

Lidzbark

$H_s = 150\,m$ $h_w = 11{,}6\,m$

I	3.5	1.9	2	3.0	7	3.5	20	3.6	14.5	4.8	20	4.9	5	4.7	12	3.7	9	3.7	32	11.7	8	3	11	28	·	1	·	·	19	18	8	1	2	22	·
II	13	5.3	9	4.5	1	2.0	1	7.0	2.5	3.6	12	4.3	17.5	3.7	20	3.4	8	3.7	25	3.2	7	11	21	27	·	2	·	·	13	20	12	·	1	28	·
III	6.5	4.5	10	3.0	4	2.2	11.5	3.2	11	3.8	8.5	4.4	18.5	2.5	10	3.1	13	2.8	26	7.1	3	7	10	23	·	·	·	·	13	15	6	·	8	18	·
IV	8	3.7	13	4.5	10.5	6.5	26.5	6.3	4.5	6.4	10	3.2	6	2.2	9.5	3.7	2	4.8	66	10.4	23	·	·	11	·	7	·	·	19	18	14	1	·	·	1
V	10.5	3.4	16.5	3.1	9	3.9	14.5	5.3	2.5	5.2	9	4.1	9.5	3.6	12.5	3.6	9	3.5	59	16.1	19	·	·	6	·	3	·	3	12	17	10	2	1	·	1
VI	9	3.9	11	5.1	8	5.8	8.5	5.8	8	4.3	10.5	3.0	16.5	3.6	16.5	3.8	2	4.2	87	46.8	1	·	·	·	3	3	·	2	10	15	11	1	·	·	4
VII	1	3.5	4	3.4	2.5	4.4	13	3.8	7	4.1	36.5	4.0	16.5	4.6	5.5	3.4	7	3.7	65	14.4	8	·	·	·	3	·	·	1	10	17	12	2	·	·	7
VIII	5	2.6	2	2.5	1	4.0	8.5	5.4	8	5.1	11	3.9	14.5	2.7	31	2.8	12	3.0	94	19.5	26	·	·	·	8	1	·	·[3]	14[3]	18	14	3	1	·	6
IX	0.5	4.0	·	·	2.5	3.0	20.5	4.4	17	4.8	17	3.6	7	2.8	8.5	3.7	17	3.3	107	53.8	4	·	·	·	1	·	·	6	9	14	11	2	7	·	1
X	2	1.8	5	2.9	3	4.5	4	2.9	5.5	3.9	13	3.5	18	3.1	26.5	2.8	16	2.6	26	10.6	11	·	·	6	·	·	·	2	14	13	5	1	13	·	·
XI	1.5	2.7	18	4.2	5.5	4.5	11	4.7	6.5	5.2	20	6.5	7	3.9	7.5	3.6	13	4.1	41	13.0	8	7	14	22	·	2	·	·	22	21	12	1	8	16	·
XII	·	·	·	·	1	3.0	11	6.0	18	6.4	30	5.0	17	3.4	10	2.8	6	4.5	57	20.2	18	4	9	25	·	4	·	·	26	21	11	1	6	17	·
Rok	60.5	3.1	90.5	3.0	55	3.9	150	4.9	105	4.8	197.5	4.2	153	3.4	169.5	3.4	114	3.7	685	53.8	4.IX	32	65	148	15	23	·	14[3]	181[3]	207	126	15	47	101	20

Kisielnica

$H_s = 140\,m$ $h_w = 14\,m$

I	2	3.5	5.5	4.5	1	2.0	9	4.8	2	4.5	22	3.6	26.5	2.4	18	3.1	7	3.1	38	7.0	30	4	10	27	·	1	·	2	19	–	9	·	1	22	·
II	12	6.4	3.5	5.7	2	5.5	·	·	·	·	7	3.4	31.5	2.9	19	3.1	9	3.3	32	9.0	7	14	23	28	·	2	·	2	12	–	9	·	2	28	·
III	7	3.1	·	·	·	·	1	3.0	6	5.6	16.5	3.2	39.5	1.8	19	3.6	4	2.7	26	11.0	20	7	7	24	·	3	·	6	11	–	6	1	9	23	·
IV	5	5.9	7.5	6.3	10	8.0	10	6.4	7.5	4.8	13.5	2.4	20	2.1	16.5	3.8	·	4.4	38	14.7	27	·	·	11	·	4	1	3	14	–	6	1	1	·	2
V	4.5	4.2	1	7.0	4	7.0	5	7.6	·	·	5.5	3.1	29.5	1.8	38.5	3.3	5	3.1	80	22.8	19	·	·	3	·	3	·	4	15	–	15	2	·	·	2
VI	8.5	5.6	2	10.0	7	6.7	·	·	·	·	7	3.9	42	2.5	23.5	3.2	·	3.6	60	20.0	13	·	·	·	1	2	·	5	9	–	10	3	·	·	2
VII	6	7.3	·	·	·	·	·	·	·	·	10.5	4.3	66.5	2.5	7	2.1	3	2.9	106	26.0	31	·	·	·	3	2	·	5	9	–	14	3	2	·	6
VIII	1	6.0	·	·	·	·	·	·	2	7.0	6.5	3.1	59	2.0	24.5	3.1	·	2.5	48	17.5	26	·	·	·	8	·	·	8	8	–	6	1	3	·	2
IX	·	·	·	·	·	·	·	·	2	5.0	20.5	3.0	61.5	2.3	6	2.9	·	2.5	42	19.7	29	·	·	·	2	·	·	10	3	–	7	1	6	·	·
X	1	8.0	·	·	1	5.0	1	7.0	·	·	8.5	3.2	51	2.0	30.5	2.8	·	2.5	18	9.3	16	·	·	5	·	·	·	2	7	–	5	·	7	·	·
XI	1	8.0	13	6.0	4	4.5	3.5	5.0	4.5	9.2	13	4.5	36.5	3.3	11.5	3.1	3	4.2	41	7.5	1	6	15	20	·	4	·	·	20	–	10	·	5	16	·
XII	·	·	·	·	·	·	·	·	10.5	6.7	23	4.8	43.5	3.2	16	1.8	·	3.7	44	11.0	3	3	7	23	·	1	·	·	24	–	9	1	2	22	·
Rok	48	4.8	32.5	3.3	29	3.2	29.5	2.8	34.5	3.6	153.5	3.5	507	2.4	230	3.0	31	3.2	573	26.0	31.VII	34	62	141	14	22	1	47	151	–	106	13	38	111	14

Kopna Góra

$H_s = 160\,m$ $h_w = 15{,}4\,m$

I	·	·	·	·	1	6.0	7	3.0	48.5	2.6	13.5	3.1	3.5	4.9	0.5	5.0	19	2.3	49	12.1	20	6	15	30	·	·	·	2	19	15	10	2	5	31	·
II	6.5	3.2	1	7.0	4	5.5	8	4.0	22	2.3	16	3.1	1	5.0	0.5	3.0	25	2.2	52	11.4	7	13	23	26	·	·	·	3	10	17	11	1	·	28	·
III	·	·	·	·	0.5	4.0	4.5	3.3	30	2.1	11	3.3	3	6.0	·	·	44	1.4	33	6.9	17	6	7	24	·	·	·	6	12	16	2	·	7	26	·
IV	0.5	2.0	1.5	6.7	8	6.9	21.5	4.3	40.5	2.7	6.5	2.9	0.5	6.0	1	6.0	10	3.3	21	11.1	23	·	·	11	·	2	·	4	11	7	4	1	1	1	1
V	3.5	4.9	3	5.3	2.5	5.6	9	3.9	36	2.2	4.5	3.1	0.5	6.0	2	4.5	32	2.0	142	54.4	29	·	·	7	·	1	1	5	7	18	14	4	5	·	2
VI	2.5	2.8	·	·	4.5	4.9	16.5	3.5	17	2.6	17	3.0	7	2.6	4.5	1.8	21	2.3	124	38.8	13	·	·	·	3	·	·	6	9	16	14	4	·	·	3
VII	5	3.4	4	3.2	·	·	5	2.6	13.5	2.2	33.5	3.3	6	3.5	1	4.0	25	2.2	52	11.1	12	·	·	·	5	·	·	4	3	14	12	1	4	·	2
VIII	7.5	2.7	2	2.5	1	5.0	6.5	3.7	17	2.2	9	3.1	12.5	3.3	11.5	2.9	26	2.1	77	32.8	2	·	·	·	9	·	·	7	6	8	8	2	3	·	4
IX	·	·	·	·	2	2.5	16	3.2	18.5	2.6	20.5	2.5	6.5	3.2	1.5	2.7	26	2.0	35	9.4	29	·	·	·	3	1	·	6	4	8	6	·	7	·	2
X	6.5	2.7	1	5.5	4	5.6	·	·	7.5	2.7	25	3.5	9	4.7	10	2.4	30	2.3	15	6.4	16	·	·	7	·	1	·	4	12	6	4	·	10	·	·
XI	6	2.0	13.5	4.0	11.5	4.4	12	4.1	9.5	3.4	19.5	4.6	8	2.6	2	3.0	8	3.5	66	14.4	1	5	17	23	·	·	·	·	18	17	10	2	8	18	·
XII	1	2.0	1	4.0	3	3.7	9.5	3.8	25	3.1	28.5	3.5	9	3.0	4	1.8	12	2.8	48	9.1	19	4	11	26	·	·	·	·	20	18	14	·	4	27	·
Rok	39	2.1	27	3.2	42	4.5	115.5	3.3	285	2.6	204.5	3.2	66.5	4.2	38.5	3.1	277	2.4	714	54.4	29.V	34	73	154	20	5	1	47	131	160	115	17	54	131	14

Tykocin

φ = 53°12' λ = 22°47' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.5	−4.8	3.5	9	−14.1	11	−3.1	−1.8	−3.0	−2.7	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.8	6.7	7.7
II	—	—	—	—	−3.3	−11.0	2.5	14	−25.5	6	−8.7	−5.1	−7.0	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.7	5.5	6.6
III	—	—	—	—	2.7	−4.5	10.5	30	−20.9	8	−3.4	1.8	−0.8	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.3	5.8	4.9	5.7
IV	—	—	—	—	9.7	2.3	16.0	26,27,28	−2.8	3	3.3	8.2	5.2	5.5	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.8	6.0	6.5
V	—	—	—	—	13.3	4.7	20.5	18	−2.1	4	7.4	12.2	8.8	9.3	—	—	—	—	—	—	—	—	—	—	—	—	6.3	7.7	5.8	6.6
VI	—	—	—	—	20.2	11.2	26.7	26	3.2	8	14.3	18.7	15.1	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.7	5.3	5.9
VII	—	—	—	—	20.9	11.0	28.8	16	6.1	5	14.9	19.6	15.1	16.2	—	—	—	—	—	—	—	—	—	—	—	—	4.4	6.8	5.9	5.7
VIII	—	—	—	—	20.4	10.5	27.6	7	5.6	19	13.0	19.3	14.0	15.1	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.7	4.3	5.5
IX	—	—	—	—	20.7	9.2	26.7	3, 4	4.6	21	11.0	19.8	12.9	14.2	—	—	—	—	—	—	—	—	—	—	—	—	4.6	5.2	2.9	4.2
X	—	—	—	—	11.1	3.3	19.1	1	−4.4	21	4.6	10.2	6.7	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.9	5.3	6.9
XI	—	—	—	—	0.0	−4.5	10.8	2	−18.1	17	−3.1	−0.9	−2.4	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.9	7.8	8.5
XII	—	—	—	—	1.0	−2.8	8.8	20	−14.7	17	−1.3	−0.1	−0.8	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.2	7.8	8.1
Rok	—	—	—	—	9.7	2.0	28.8	16.VII	−25.5	6.II	4.1	8.5	5.3	5.8	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.1	5.7	6.5

Kończewice

φ = 53°11' λ = 18°33'

I	—	—	—	—	1.3	−2.7	4.8	9	−10.7	11	−1.1	0.5	−0.8	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.0	6.7	7.2
II	—	—	—	—	−2.1	−9.8	2.2	13	−19.1	24	−5.9	−2.9	−5.5	−5.0	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.8	5.1	6.4
III	—	—	—	—	3.1	−5.6	11.5	29	−25.6	8	−3.4	2.1	−0.7	−0.7	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.5	5.5	6.2
IV	—	—	—	—	9.5	2.6	15.1	30	−0.7	3	4.1	8.4	6.0	6.1	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.8	6.3	7.3
V	—	—	—	—	13.7	4.8	20.6	17	−2.8	3	8.1	12.4	8.9	9.6	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.9	5.9	6.6
VI	—	—	—	—	20.8	10.1	30.2	26	4.7	3	14.2	19.4	15.2	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.2	5.1	5.5
VII	—	—	—	—	20.8	10.9	30.2	14	5.0	5	14.1	19.2	14.8	15.7	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.4	6.1	6.6
VIII	—	—	—	—	21.1	10.3	28.6	22	5.8	2	13.3	19.7	14.9	15.7	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.7	5.1	5.8
IX	—	—	—	—	19.8	9.9	27.9	3	3.2	16	11.4	18.5	14.1	14.6	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.4	4.4	5.1
X	—	—	—	—	11.8	3.6	19.8	1	−2.2	22	5.0	11.3	6.7	7.4	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.0	1.6	4.7
XI	—	—	—	—	0.6	−4.3	11.3	2	−18.0	24	−2.3	−0.4	−1.7	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.6	6.4	7.5
XII	—	—	—	—	1.7	−2.3	10.0	19	−18.9	17	−0.5	0.8	0.0	0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.1	8.1	7.6	7.9
Rok	—	—	—	—	10.2	2.3	30.2	26.VI, 14.VII	−25.6	8.III	4.8	9.1	6.0	6.5													6.8	6.9	5.5	6.4

Wyrzysk

φ = 53°09' λ = 17°16'

I	—	—	—	—	2.0	−2.5	5.6	17	−10.8	31	−1.4	1.0	−0.5	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−0.4	−7.6	2.6	13, 14	−17.9	6	−5.9	−1.3	−3.9	−3.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	4.4	−4.5	14.1	29	−23.8	9	−3.2	3.5	−0.3	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	10.6	2.9	15.3	30	−2.2	5	4.4	10.0	5.7	6.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	14.6	5.5	21.1	17	−1.2	3	8.2	13.4	8.9	9.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	21.6	10.6	30.7	26	5.6	3	14.6	20.7	14.4	16.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	20.7	11.0	30.3	14	5.6	2	14.9	19.4	14.3	15.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	21.4	10.3	28.9	6	5.3	2	13.7	20.6	13.8	15.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	20.3	9.7	27.9	3	3.8	16	12.3	19.5	13.4	14.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.7	3.6	21.3	1	−3.7	22	5.0	12.2	6.3	7.4	—	—	—	—	—	—	—	—	—	—	—	—	5.5	4.6	2.7	4.3
XI	—	—	—	—	1.6	−3.4	11.3	1, 2	−16.3	24	−2.3	0.9	−1.3	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.7	7.3	7.7
XII	—	—	—	—	2.8	−1.1	10.5	19	−10.3	17	−0.1	1.8	0.8	0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.0	8.4	8.3
Rok	—	—	—	—	11.0	2.9	30.7	26.VI	−23.8	9.III	5.0	10.1	6.0	6.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Bydgoszcz, IMiUZ

φ = 53°08' λ = 18°01'

I	—	—	—	—	2.1	−2.4	5.9	17	−11.1	11	−0.9	1.0	−0.4	−0.2	5.3	5.4	5.3	5.3	91	81	88	87	0.5	1.3	0.7	0.8	7.9	7.4	6.2	7.2
II	—	—	—	—	−0.6	−7.0	2.9	13	−14.6	6	−5.1	−2.0	−3.9	−3.7	3.7	4.1	3.9	3.9	86	76	82	81	0.6	1.2	0.8	0.9	8.0	7.7	6.2	7.3
III	—	—	—	—	5.1	−4.1	12.9	29	−21.1	9	−2.8	3.2	0.2	0.2	4.9	5.5	5.4	5.3	90	70	83	81	0.6	2.6	1.1	1.4	8.5	6.7	5.0	6.7
IV	—	—	—	—	10.7	2.7	15.8	30	−1.7	6	3.7	8.8	6.2	6.2	7.1	7.2	7.7	7.3	88	63	80	77	1.0	4.4	1.9	2.4	8.2	8.3	5.9	7.5
V	—	—	—	—	14.8	5.3	21.1	17	−1.8	3	7.8	12.7	9.6	9.9	9.0	8.5	9.0	8.8	84	59	74	72	1.7	6.4	3.2	3.8	7.1	6.9	6.3	6.8
VI	—	—	—	—	21.8	10.9	31.7	26	4.7	3	14.1	20.0	16.1	16.6	12.5	11.7	12.9	12.4	78	51	70	66	3.8	12.3	5.6	7.2	4.7	6.9	4.9	5.5
VII	—	—	—	—	21.2	11.5	31.4	14	6.8	5	14.1	19.0	15.5	16.0	13.4	12.6	13.9	13.3	82	57	78	72	2.9	10.1	4.1	5.7	6.8	7.8	6.5	7.0
VIII	—	—	—	—	21.8	10.9	29.9	22	6.1	2	12.8	19.9	15.4	15.9	13.0	12.3	13.7	13.0	87	54	79	73	2.0	11.6	4.2	5.9	5.6	7.5	4.2	5.8
IX	—	—	—	—	20.5	9.7	28.9	3	3.2	16	10.9	18.9	14.0	14.4	12.2	12.6	13.4	12.7	92	59	84	78	1.0	9.8	2.8	4.5	6.5	6.1	3.4	5.3
X	—	—	—	—	12.6	3.3	20.9	1	−4.5	22	4.8	11.2	6.8	7.4	8.2	9.8	9.0	9.0	94	73	89	85	0.6	3.8	1.1	1.8	7.6	6.8	2.3	5.6
XI	—	—	—	—	1.5	−3.9	11.9	2	−19.6	24	−2.1	0.3	−1.5	−1.2	5.2	5.6	5.3	5.4	91	84	90	88	0.6	1.1	0.7	0.8	9.1	8.0	7.1	8.1
XII	—	—	—	—	2.8	−1.8	10.9	19	−15.0	17	−0.1	1.4	0.6	0.6	5.6	5.6	5.8	5.7	89	82	87	86	0.7	1.3	0.9	1.0	9.0	8.6	7.8	8.5
Rok	—	—	—	—	11.2	2.9	31.7	26.VI	−21.1	9.III	4.8	9.5	6.6	6.9	8.3	8.4	8.8	8.5	88	67	82	79	1.3	5.5	2.3	3.0	7.4	7.4	5.5	6.8

Tykocin — $H_s = 120$ m — $h_w = 14$ m — 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V ≥ 10	Wiatr V ≥ 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	1.5	1.7	6	2.8	9	4.2	32	4.5	9.5	4.5	11	4.1	7	4.6	5	7.4	12	3.9	33	9.2	30	3	12	27	·	3	·	2	17	14	6	·	3	21	·
II	11.5	2.3	10.5	4.1	3	3.2	2.5	1.8	9	3.3	17	4.4	12	3.7	2.5	4.2	11	3.1	27	9.5	7	11	23	26	·	2	·	2	11	18	7	·	2	28	·
III	1.5	3.7	5.5	1.7	4.5	2.3	24	3.7	13.5	2.6	8	3.2	11.5	2.9	5.5	4.3	19	2.5	28	5.4	17	4	7	25	·	·	·	6	11	14	9	·	4	19	·
IV	5.5	3.3	5	2.3	24.5	5.3	36	5.0	6	2.3	2	3.2	1.5	1.3	4.5	2.3	5	4.1	24	7.0	23	·	·	10	·	6	2	3	11	10	6	·	·	·	2
V	11.5	2.5	8.5	2.8	14	3.7	12.5	2.6	6	2.2	8.5	3.4	7.5	2.3	9.5	2.9	15	2.4	104	31.5	29	·	·	2	·	·	·	4	14	16	14	3	2	·	2
VI	7	3.1	8.5	3.5	11.5	4.0	10	3.4	7	2.9	10.5	3.6	13	3.5	8.5	2.5	14	2.8	75	22.9	13	·	·	·	1	1	·	2	9	14	9	2	1	·	4
VII	1	2.5	7	3.7	2	4.2	11	2.9	10	2.6	28	3.9	11.5	4.0	3.5	1.6	19	2.7	82	18.4	30	·	·	·	4	·	·	1	5	14	13	3	2	·	5
VIII	12.5	2.9	1.5	2.7	·	·	9.5	4.4	12.5	3.1	8	2.7	14.5	2.2	16.5	2.7	18	2.3	53	18.8	2	·	·	·	7	·	·	4	7	9	7	3	1	·	6
IX	·	·	·	·	1	3.0	24	3.2	19.5	2.6	16	2.9	20.5	3.4	2	2.0	7	2.8	25	11.6	29	·	·	·	3	3	1	8	2	10	5	1	3	·	3
X	7	1.4	3.5	1.6	2.5	3.2	2.5	4.4	8.5	2.8	14.5	3.1	19	2.7	19.5	2.6	16	2.2	19	6.8	16	·	·	4	·	·	·	3	14	9	4	·	9	·	·
XI	2.5	1.8	6	4.3	14	3.4	14	6.7	10.5	3.5	13	6.3	18	3.9	2	4.0	10	4.1	50	10.7	21	6	16	19	·	4	3	1	19	15	9	1	10	16	·
XII	·	·	·	·	·	·	17.5	4.3	18	3.9	29	4.3	14	3.4	6.5	1.7	8	3.5	45	8.7	18	3	9	22	·	2	1	·	19	20	12	·	2	21	·
Rok	61.5	2.1	62	2.5	86	3.0	195.5	3.9	130	3.0	165.5	3.8	150	3.2	90.5	3.2	154	3.0	565	31.5	29. V	27	67	135	15	21	7	36	139	163	101	13	39	105	22

Kończewice — $H_s = 94$ m — $h_w = 12$ m

I	8	2.4	8	3.5	11	3.5	6	4.7	9	3.3	14	4.4	20	5.3	11	6.1	6	4.1	22	5.4	30	1	7	26	·	3	·	·	15	16	8	·	6	6	·
II	8	3.9	15	5.7	·	·	0.5	2.0	1	2.5	8.5	4.9	23	7.3	23	6.8	5	5.8	15	3.3	7	11	22	27	·	10	·	1	8	22	4	·	4	28	·
III	5	4.7	16.5	5.1	8	2.6	10	3.5	5	2.0	12	4.1	14	5.1	10.5	5.2	12	3.7	46	16.8	4	6	10	22	·	5	·	6	12	13	7	1	12	18	·
IV	11.5	4.8	15.5	4.8	16.5	4.6	16.5	6.0	3	5.3	3	3.7	7	5.6	9	4.7	8	4.6	31	6.8	23	·	·	4	·	·	·	·	14	15	9	·	1	·	·
V	15	4.3	26.5	4.2	11	4.7	4	7.0	1	3.0	2	6.0	20	5.4	9.5	3.8	4	4.5	71	15.4	19	·	·	3	·	4	·	1	11	17	10	2	3	·	2
VI	9.5	3.3	11.5	4.4	7.5	3.3	3	4.0	7.5	3.5	7.5	5.0	17	4.7	17.5	5.2	9	3.9	81	26.7	1	·	·	·	3	1	·	3	7	11	7	3	1	·	4
VII	5	4.8	9	4.8	5	2.4	2	3.0	3	4.0	18	4.3	39	6.0	8	2.4	4	4.6	42	18.6	21	·	·	·	3	2	·	1	8	19	9	1	·	·	6
VIII	8	2.8	5.5	1.5	2	1.5	5	4.2	5	3.8	6	4.2	21	3.8	23.5	3.7	17	2.8	33	12.5	25	·	·	·	8	·	·	1	4	14	7	1	1	·	3
IX	2	2.5	1	2.0	8.5	3.4	15	3.7	7.5	3.5	17.5	4.4	21.5	4.6	6	5.2	11	3.6	89	31.2	10	·	·	·	1	·	·	7	4	11	7	3	5	·	2
X	7	2.0	9	2.2	3	1.7	5	1.6	2	1.5	7	3.4	25	4.6	15	2.7	20	2.5	14	9.5	16	·	·	2	·	1	·	4	3	5	4	·	13	·	·
XI	5	2.2	18	6.2	8	5.1	7	5.4	7	5.4	14.5	6.1	20.5	6.3	5	4.6	5	5.3	27	7.3	1	8	12	18	·	7	·	3	15	17	9	·	7	16	·
XII	1	2.0	·	·	2	2.0	9	5.2	6.5	6.8	26	7.8	27.5	6.6	12	3.8	9	5.7	37	9.7	18	2	6	19	·	8	·	·	14	18	8	·	9	10	·
Rok	85	3.3	135.5	3.7	82.5	2.9	83	4.2	57.5	3.7	136	4.9	255.5	5.4	150	4.5	110	4.3	508	31.2	10. IX	28	57	121	15	41	·	27	115	178	89	11	62	78	17

Wyrzysk — $H_s = 90$ m — $h_w = 12$ m

I	15	2.3	5	3.0	12	2.9	7	3.7	4	1.8	14	6.6	25	3.4	2	5.0	9	3.3	34	8.0	17	1	6	26	·	2	1	—	—	15	11	·	—	11	—
II	10	3.5	7	6.4	8	4.2	2	1.0	1	5.0	1	3.0	19	3.8	20	3.4	16	3.1	7?	1.5	26	8	13	27	·	1	·	—	—	10	3	·	—	28	—
III	5	4.2	15	3.8	4	3.8	5	2.4	15	2.5	4	2.5	4	2.0	7	2.7	34	1.9	40	10.0	4	6	8	21	·	·	·	—	—	10	9	1	—	17	—
IV	9	2.4	3	3.3	26	5.6	15	4.7	3	3.7	·	·	9	2.6	9	3.3	16	3.5	36	9.0	28	·	·	5	·	2	1	—	—	12	12	·	—	·	—
V	10	3.9	8	3.2	23	3.8	2	4.0	7	5.0	·	·	16	4.0	4	3.0	23	2.9	83	20.0	9	·	·	3	·	1	·	—	—	18	16	4	—	·	—
VI	10	3.2	7	4.1	7	4.1	·	·	5	3.6	3	3.7	14	4.2	13	4.0	31	2.6	35	10.0	17	·	·	·	5	·	·	—	—	9	8	1	—	·	—
VII	8	4.4	1	1.0	4	3.0	3	3.3	5	2.2	2	2.0	44	4.1	11	3.7	15	3.2	80	13.0	15	·	·	·	2	·	·	—	—	18	17	1	—	·	—
VIII	16	2.4	·	·	·	·	·	·	5	2.8	6	3.5	15	2.7	19	3.1	32	1.8	82	18.4	6	·	·	·	7	·	·	—	—	13	10	3	—	·	—
IX	2	4.5	·	·	3	3.3	7	2.9	16	3.8	10	4.0	16	3.5	9	3.2	27	2.5	59	18.5	10	·	·	·	1	1	·	—	—	10	8	2	—	·	—
X	4	1.8	3	3.3	6	2.3	8	2.0	5	2.4	3	2.7	20	3.4	7	2.3	37	1.6	23	9.6	16	·	·	7	·	·	·	12	6	4	4	·	—	·	—
XI	3	2.0	7	2.9	17	4.1	2	3.5	3	2.3	13	5.3	21	5.4	4	6.5	20	3.5	49	10.5	27	6	11	17	·	1	1	1	18	10	7	1	—	12	—
XII	5	2.4	·	·	4	1.5	·	·	12	4.8	23	5.6	30	4.4	9	2.8	10	3.9	64	10.5	18	1	3	21	·	4	·	1	20	19	14	2	—	8	—
Rok	97	3.1	56	2.6	114	3.2	51	2.3	81	3.3	79	3.2	233	3.6	114	3.6	270	2.9	592?	20.0	9. V	22	41	127	15	12	3	—	—	148	119	15	—	76	—

Bydgoszcz, IMiUZ — $H_s = 47$ m — $h_w = 10$ m

I	1	2.0	6	1.7	13	1.5	5	1.8	12	2.8	24	1.8	6	2.3	6	1.5	20	1.5	28	6.3	25	1	5	26	·	·	·	3	15	17	8	·	5	13	—
II	5	2.6	11	2.3	2	1.0	·	·	4	2.5	13	3.0	25	2.2	9	2.8	15	2.0	19	3.2	28	5	16	26	·	·	·	2	10	18	6	·	3	28	—
III	4	1.8	8	2.2	4	1.2	8	1.2	10	2.3	8	2.4	18	1.9	5	3.2	28	1.4	42	15.4	3	5	8	21	·	·	·	2	13	13	7	1	10	16	—
IV	1	1.0	14	2.9	17	2.3	13	2.1	3	2.3	2	2.5	11	1.8	9	1.8	20	1.7	33	7.9	21	·	·	6	·	·	·	1	15	13	8	·	3	·	—
V	4	3.0	20	2.2	18	2.5	4	3.8	·	·	7	2.4	16	2.8	6	1.3	18	2.0	75	10.9	9	·	·	3	·	·	·	3	15	19	13	1	1	·	—
VI	·	·	17	2.6	10	2.4	4	3.5	5	3.8	14	2.7	16	2.9	6	2.0	18	2.2	47	21.0	1	·	·	·	5	·	·	6	7	9	9	2	·	·	—
VII	·	·	9	2.7	5	2.4	3	2.0	4	2.8	30	3.0	18	2.8	1	1.0	23	2.1	40	7.0	23	·	·	·	4	·	·	2	14	18	13	·	·	·	—
VIII	1	2.0	1	1.0	1	1.0	6	2.2	5	3.2	10	2.6	23	1.7	12	1.6	34	1.3	53	17.3	25	·	·	·	9	·	·	2	5	12	7	1	2	·	—
IX	·	·	1	1.0	10	1.6	9	3.0	5	2.0	16	2.8	13	2.2	3	2.3	33	1.5	51	15.1	4	·	·	·	2	·	·	6	6	11	8	1	3	·	—
X	1	2.0	4	1.2	4	2.0	·	·	4	2.0	14	1.9	17	1.5	5	1.6	44	0.9	16	10.5	16	·	·	7	·	·	·	4	6	6	3	1	17	·	—
XI	2	1.0	16	2.1	8	1.8	12	2.7	3	1.0	15	3.3	16	1.7	1	2.0	17	1.8	40	11.9	21	6	11	20	·	1	·	1	17	14	7	2	7	16	—
XII	1	3.0	·	·	5	1.6	9	3.4	17	3.4	27	3.6	15	2.8	6	2.0	12	2.7	31	9.3	18	1	3	22	·	1	·	·	22	19	7	·	7	12	—
Rok	20	1.5	107	1.8	97	1.8	73	2.1	72	2.3	180	2.7	195	2.2	69	1.9	282	1.8	475	21.0	1. VI	18	43	131	20	2	·	32	145	169	96	9	58	85	—

Bydgoszcz

$\varphi = 53°07'$ $\lambda = 17°58'$

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1001.9	1017.2	980.9	1010.9	1.7	−3.6	5.4	1, 9	−13.8	31	−1.4	0.6	−1.0	−0.7	5.2	5.4	5.2	5.3	92	84	89	88	0.4	1.1	0.6	0.7	7.7	7.9	7.2	7.6
II	1006.8	1025.0	978.5	1016.1	−1.2	−9.1	2.4	13	−19.7	24	−6.0	−2.5	−4.7	−4.5	3.6	4.1	3.8	3.8	87	79	84	83	0.5	1.0	0.7	0.7	7.8	7.8	6.6	7.4
III	1007.0	1022.6	980.3	1016.1	4.3	−5.8	12.9	29	−25.4	9	−3.5	2.7	−1.2	−0.8	4.7	5.4	5.2	5.1	91	70	86	82	0.5	2.5	0.8	1.3	7.5	6.6	5.7	6.6
IV	1002.2	1022.5	985.0	1011.0	10.4	1.5	15.5	30	−3.6	5	3.6	8.9	5.2	5.7	7.1	6.9	7.3	7.1	88	60	81	76	0.9	4.7	1.7	2.4	8.1	7.9	6.1	7.4
V	1004.9	1020.2	986.4	1013.6	14.3	3.9	20.5	17	−4.1	3	7.9	12.8	8.9	9.6	9.0	8.6	8.7	8.8	82	59	75	72	1.9	6.5	2.9	3.8	7.4	7.2	6.4	7.0
VI	1005.0	1015.0	992.3	1013.6	21.4	9.7	31.7	26	2.8	3	14.2	19.7	14.9	15.9	12.3	12.1	12.5	12.3	76	54	74	68	4.2	11.5	4.6	6.8	5.6	6.9	5.5	6.0
VII	1002.0	1012.7	987.2	1010.5	20.9	10.4	31.1	14	3.7	2	14.2	19.0	14.5	15.6	13.5	12.6	13.6	13.2	82	57	82	74	2.9	10.1	3.3	5.4	6.9	8.0	6.4	7.1
VIII	1006.1	1014.2	996.1	1014.8	21.5	9.2	29.8	22	3.0	13	12.7	19.6	13.9	15.0	13.3	12.6	13.1	13.0	90	56	83	76	1.7	10.9	3.3	5.3	6.0	7.5	5.1	6.2
IX	1004.7	1024.6	992.1	1013.3	20.3	8.2	29.4	3	1.1	16	11.0	18.9	12.7	13.8	12.4	13.1	12.8	12.8	94	61	86	80	0.9	9.2	2.4	4.2	6.1	6.4	4.4	5.6
X	1013.6	1028.7	998.1	1022.5	12.4	1.6	20.5	1	−5.9	22	3.8	11.3	5.0	6.3	7.9	9.8	8.2	8.6	95	73	92	87	0.5	3.9	0.7	1.7	6.5	6.8	2.4	5.2
XI	1002.2	1020.2	973.2	1011.3	0.9	−4.8	11.5	2	−19.6	24	−2.4	0.1	−1.9	−1.5	5.0	5.5	5.1	5.2	89	82	87	86	0.6	1.2	0.7	0.8	8.9	8.2	7.9	8.3
XII	994.8	1014.8	968.8	1003.8	2.3	−2.6	11.1	19	−15.8	17	−0.2	1.2	0.1	0.3	5.4	5.5	5.5	5.5	88	81	87	85	0.8	1.3	0.9	1.0	9.3	8.3	8.3	8.6
Rok	1004.3	1028.7	968.8	1013.1	10.8	1.6	31.7	26, VI	−25.4	9. III	4.5	9.4	5.5	6.2	8.3	8.5	8.4	8.4	88	68	84	80	1.3	5.3	1.9	2.8	7.3	7.5	6.0	6.9

Mława

$\varphi = 53°07'$ $\lambda = 20°22'$

I	993.2	1009.2	974.4	1011.6	0.3	−4.4	4.3	18	−16.5	11	−2.4	−0.9	−2.2	−1.9	5.0	5.2	5.0	5.1	94	89	94	92	0.3	0.6	0.3	0.4	8.1	7.6	6.4	7.4
II	996.2	1015.4	971.1	1014.9	−2.5	−10.8	1.2	13, 14	−24.8	6	−7.8	−4.1	−6.9	−6.4	3.4	3.9	3.6	3.6	92	84	92	89	0.3	0.7	0.3	0.4	7.9	6.9	6.3	7.0
III	998.2	1014.3	970.0	1016.7	3.2	−5.3	10.1	30	−19.4	9	−3.7	1.9	−1.2	−1.0	4.8	5.5	5.2	5.2	95	77	89	87	0.3	1.8	0.7	0.9	6.4	6.4	5.7	6.2
IV	994.1	1011.7	976.8	1012.0	9.5	1.7	14.9	30	−3.2	3	3.2	7.7	5.3	5.4	7.2	7.7	7.5	7.5	91	73	83	82	0.7	3.0	1.5	1.7	7.6	8.4	6.5	7.5
V	996.2	1012.2	977.1	1013.8	13.8	4.1	19.9	18	−3.3	4	7.7	12.3	8.7	9.4	9.0	9.1	9.2	9.1	84	63	80	76	1.7	5.4	2.3	3.1	6.7	7.7	5.5	6.6
VI	996.3	1004.3	987.0	1013.5	21.0	10.5	29.9	26	6.1	30	14.2	19.4	15.1	16.0	13.3	12.8	13.5	13.2	82	58	78	73	3.0	10.3	3.9	5.7	5.7	7.2	5.6	6.2
VII	993.8	1005.2	979.0	1011.0	20.8	10.3	30.2	15	4.0	5	14.2	19.3	14.6	15.7	14.1	13.8	14.5	14.1	86	61	85	77	2.4	9.2	2.6	4.7	5.6	8.4	5.1	6.4
VIII	997.5	1005.1	987.4	1014.9	20.7	10.1	28.2	22	4.6	31	12.7	19.2	14.1	15.0	13.7	14.0	14.2	14.0	93	64	88	82	1.2	9.2	2.3	4.2	5.9	7.5	5.0	6.1
IX	997.2	1015.2	986.1	1014.6	19.9	8.9	27.4	3	1.8	16	10.6	18.3	12.5	13.5	12.6	14.2	13.5	13.4	97	67	92	85	0.4	7.4	1.2	3.0	5.5	5.8	2.9	4.7
X	1004.4	1019.5	988.9	1022.3	11.7	3.0	20.3	1	−5.3	21	4.2	10.7	6.3	6.9	8.3	10.0	9.2	9.2	98	77	95	90	0.2	3.2	0.5	1.3	7.5	6.9	4.5	6.3
XI	993.6	1011.3	966.7	1012.0	0.2	−5.2	10.1	2	−19.3	24	−3.1	−1.0	−2.6	−2.3	5.1	5.4	5.2	5.2	94	89	94	92	0.3	0.7	0.3	0.4	9.3	8.1	8.8	8.7
XII	986.7	1004.4	963.5	1004.4	0.9	−3.4	8.7	20	−20.1	17	−1.3	−0.3	−1.0	−0.9	5.4	5.6	5.4	5.5	94	90	92	92	0.3	0.6	0.5	0.5	8.3	8.2	8.4	8.3
Rok	995.6	1019.5	963.5	1013.5	10.0	1.6	30.2	15, VII	−24.8	6. II	4.0	8.5	5.2	5.7	8.5	8.9	8.8	8.7	92	74	88	85	0.9	4.3	1.4	2.2	7.0	7.4	5.9	6.8

Białystok

$\varphi = 53°07'$ $\lambda = 23°11'$

I	994.9	1011.8	976.1	1012.8	−0.6	−5.5	3.0	18	−14.9	11	−3.3	−2.1	−3.2	−3.0	4.6	4.8	4.5	4.6	91	87	90	89	0.4	0.6	0.5	0.5	8.7	8.5	7.9	8.4
II	996.1	1016.9	974.6	1014.3	−3.2	−11.2	2.7	14	−25.3	7	−8.7	−4.9	−7.3	−7.0	3.2	3.6	3.4	3.4	91	81	88	87	0.3	0.8	0.4	0.5	8.6	7.8	6.2	7.5
III	999.6	1016.2	971.7	1017.4	3.6	−6.0	11.0	30	−22.8	9	−3.8	2.6	−1.2	−0.9	4.6	5.2	5.0	4.9	91	70	85	82	0.5	2.4	0.9	1.3	7.5	6.7	5.8	6.7
IV	995.8	1010.0	976.4	1013.1	10.3	2.0	17.0	27	−5.1	3	3.4	9.0	5.5	5.8	6.7	6.6	7.0	6.8	84	58	76	73	1.3	5.2	2.2	2.9	7.5	7.7	7.0	7.4
V	997.1	1012.7	979.6	1014.2	14.2	4.1	21.5	18	−4.4	4	7.4	12.7	9.0	9.5	9.1	9.1	9.2	9.1	86	61	79	75	1.4	5.9	2.5	3.3	6.4	8.3	6.4	7.0
VI	997.2	1003.8	987.9	1013.9	20.7	10.7	28.9	26	2.7	8	14.2	19.1	15.2	15.9	13.5	13.7	13.9	13.7	83	63	80	75	2.9	8.9	3.6	5.1	6.0	7.7	6.6	6.8
VII	995.1	1006.7	981.5	1011.8	21.7	10.6	29.9	15	5.4	5	14.6	20.1	15.4	16.4	14.0	13.9	14.2	14.0	84	59	80	74	2.8	10.2	3.7	5.6	5.7	7.8	6.4	6.6
VIII	998.1	1006.4	986.9	1014.8	21.1	10.3	27.9	7	5.4	19	12.9	19.9	14.2	15.3	13.6	13.9	13.9	13.8	91	61	85	79	1.6	10.0	2.6	4.7	6.3	7.5	4.8	6.2
IX	999.0	1015.2	987.4	1015.9	21.1	8.6	27.3	4	2.3	21	10.5	20.0	12.9	14.1	12.3	14.0	13.3	13.2	95	60	89	81	0.7	10.0	2.0	4.2	5.2	5.9	3.6	4.9
X	1004.5	1020.3	989.6	1021.9	11.3	2.8	20.3	1	−5.8	21	4.3	10.4	6.5	6.9	7.9	9.3	8.7	8.6	93	73	89	85	0.6	3.7	1.2	1.8	7.8	8.3	6.3	7.5
XI	995.3	1011.3	968.9	1013.1	0.1	−4.8	11.1	2	−20.7	17	−2.9	−0.8	−2.6	−2.2	4.9	5.2	4.9	5.0	90	83	89	87	0.5	1.1	0.6	0.7	9.1	9.2	8.4	8.9
XII	988.6	1003.3	968.2	1006.2	0.9	−3.1	7.8	20	−13.9	17	−1.3	0.0	−0.8	−0.7	5.1	5.3	5.1	5.2	90	85	87	87	0.6	0.9	0.8	0.8	8.9	8.8	8.8	8.8
Rok	996.8	1020.3	968.2	1014.1	10.1	1.6	29.9	15, VII	−25.3	7. II	3.9	8.8	5.3	5.8	8.3	8.7	8.6	8.5	89	70	85	81	1.1	5.0	1.8	2.6	7.3	7.8	6.5	7.2

Przelewice

$\varphi = 53°06'$ $\lambda = 15°05'$

I	—	—	—	—	2.4	−1.5	7.5	17	−10.5	31	−0.3	1.3	0.3	0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.9	7.2	8.3
II	—	—	—	—	0.4	−5.8	3.7	13	−17.5	28	−3.9	−1.0	−2.6	−2.5	—	—	—	—	—	—	—	—	—	—	—	—	7.9	8.4	7.0	7.8
III	—	—	—	—	4.8	−3.8	13.6	29	−18.0	7	−2.1	3.4	−0.1	0.3	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.2	4.1	5.6
IV	—	—	—	—	11.5	2.7	16.5	6	−2.8	5	4.8	10.0	6.1	6.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.9	5.7	7.1
V	—	—	—	—	15.2	6.3	20.8	17	−0.4	3	9.1	14.0	9.6	10.6	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.4	6.9	7.1
VI	—	—	—	—	21.5	10.7	29.0	26	4.3	4	15.2	20.3	14.8	16.3	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.0	5.9	6.5
VII	—	—	—	—	19.9	10.9	30.6	14	6.5	5, 6	13.8	18.3	14.0	15.0	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.4	6.6	6.9
VIII	—	—	—	—	20.7	10.1	28.2	22	6.0	31	13.3	19.4	13.9	15.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.4	10.0	25.8	3	6.1	21	11.7	18.1	12.8	13.8	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.9	4.8	6.2
X	—	—	—	—	13.1	3.5	22.4	1	−1.9	23	5.3	11.9	6.7	7.6	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.1	3.9	5.7
XI	—	—	—	—	1.8	−2.8	12.1	1, 2	−14.1	23	−1.2	1.0	−0.9	−0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.7	6.8	8.0
XII	—	—	—	—	3.1	−0.6	11.7	19	−5.4	17	0.6	1.8	1.1	1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.7	9.3	7.8	8.6
Rok	—	—	—	—	11.2	3.3	30.6	14, VII	−18.0	7. III	5.5	9.9	6.3	7.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Uwaga: Dane za okres I–VI pochodzą z Terenu doradów PGR, a za okres VII–XII z nowego miejsca, odległego o 800 m w kierunku SE od poprzedniego (stację przeniesiono)

Bydgoszcz

$H_s = 70$ m $H_b = 72,1$ m $h_w = 11$ m **1965**

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7.5	3.0	5.5	3.5	13	3.2	9.5	3.5	11	5.4	26	5.2	10.5	4.7	8	3.6	2	4.2	21	5.4	25	2	6	28	·	4	·	·	16	17	6	·	7	14	·
II	7.5	4.8	11	5.0	3.5	3.4	2.5	2.2	3	3.5	17	5.1	26	5.9	11.5	6.3	2	5.2	19	5.2	7	12	17	27	·	7	·	·	12	21	6	·	3	28	·
III	4.5	5.1	11.5	3.2	12	2.2	5.5	4.2	11	4.0	20	4.0	16.5	5.3	6	3.5	6	3.7	39	15.4	3	6	10	23	·	4	·	2	13	13	8	1	11	19	1
IV	8	3.8	10	3.6	26	4.7	17	3.9	7.5	4.4	7.5	3.9	5	4.5	8	3.8	1	4.1	38	8.7	21	·	·	11	·	5	·	2	15	15	7	·	4	·	·
V	12	4.1	15.5	3.9	21.5	4.0	10.5	4.6	5	2.5	10	4.3	10.5	5.1	6	4.6	2	4.1	70	10.7	9	·	·	6	·	4	·	2	13	18	14	1	4	·	2
VI	6.5	2.6	11.5	3.9	13	4.0	5	4.0	12.5	4.6	12	5.0	17	5.2	9.5	5.3	3	4.3	60	20.7	1	·	·	·	5	4	·	2	9	9	9	2	·	·	4
VII	2.5	1.2	11	4.0	5	3.1	4	4.4	7	3.4	36.5	5.2	22.5	6.1	3.5	2.4	1	4.7	66	25.1	21	·	·	·	3	8	·	2	13	16	12	1	3	·	7
VIII	8	2.6	1	1.5	3.5	2.0	4.5	3.3	8	5.3	18.5	3.4	18	2.9	18.5	3.3	13	2.8	57	15.7	4	·	·	·	9	3	·	1	7	12	9	3	4	·	5
IX	1.5	4.0	0.5	4.0	13.5	2.0	10.5	4.2	16.5	3.7	21	4.1	15	3.8	3.5	4.9	8	3.3	50	10.5	4	·	·	·	2	2	·	3	5	10	8	1	5	·	2
X	3.5	1.4	4.5	1.6	5.5	2.4	4.5	2.4	5	1.9	18.5	3.5	23	3.8	8.5	2.5	20	2.4	15	9.0	16	·	·	11	·	1	·	4	4	5	3	·	18	·	1
XI	3	2.0	12	3.6	13	4.0	6	4.8	9.5	5.2	21.5	5.4	14.5	5.5	3.5	4.3	7	4.4	38	9.6	21	7	12	22	·	5	·	1	20	19	9	·	7	17	·
XII	2.5	3.6	1	1.0	3.5	1.7	9.5	4.8	15.5	5.3	33.5	6.2	20.5	5.1	3	4.0	4	5.0	34	11.4	18	1	5	23	·	5	·	·	22	19	8	1	6	12	·
Rok	67	3.2	95	3.2	133	3.1	89	3.9	111.5	4.1	242	4.6	199	4.8	89.5	4.0	69	4.0	507	25.1	21.VII	28	50	151	19	52	·	19	149	174	99	10	72	90	22

Uwaga. Prędkości i kierunki wiatru – wg anemometru M-47.

Mława

$H_s = 141$ m $H_b = 145,8$ m $h_w = 13,5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5.5	1.7	3	3.3	20.5	3.8	13	3.2	17.5	3.3	11.5	3.5	10.5	3.6	5.5	3.4	6	3.2	44	7.4	30	3	12	28	·	·	·	1	16	16	10	·	4	28	·
II	10	4.2	8	4.0	2.5	2.6	1.5	2.3	8	2.8	13	3.4	22	3.6	11	3.8	8	3.2	35	5.4	27	13	21	27	·	·	·	·	10	18	10	·	5	28	·
III	4	4.0	11	2.9	8	2.8	11.5	2.5	20.5	2.4	6.5	2.5	12.5	3.0	5	4.0	14	2.4	39	11.5	3	7	9	24	·	·	·	4	13	16	9	1	7	22	·
IV	5.5	3.2	10	4.8	21	4.9	19.5	4.3	11.5	3.2	5.5	2.5	6.5	2.0	7.5	2.7	3	3.7	48	8.2	23	·	·	8	·	2	·	2	15	16	11	·	3	·	·
V	15	3.2	11	2.5	19.5	4.3	9	3.1	5	2.2	7.5	4.6	8	3.6	13	3.7	5	3.3	58	16.5	19	·	·	3	·	1	·	3	14	15	9	2	2	·	1
VI	8.5	3.1	6.5	3.8	16.5	4.9	6.5	4.2	6	3.3	12	3.8	16.5	4.8	10.5	3.8	7	3.8	41	7.2	19	·	·	·	3	·	·	1	10	16	11	·	·	·	3
VII	3	2.7	9	3.5	8	3.1	7.5	4.0	9	3.3	32	4.5	16.5	5.0	1	1.0	7	3.8	87	22.8	8	·	·	·	4	·	·	·	9	18	13	3	3	·	9
VIII	7.5	2.5	1.5	1.3	5.5	2.3	15	2.9	3.5	3.1	12	2.9	20.5	3.3	14.5	3.5	13	2.6	90	34.6	26	·	·	·	9	·	·	4	11	16	11	3	2	·	3
IX	·	·	1	2.5	13	4.4	17.5	3.2	13.5	2.0	15.5	3.2	8	4.8	3.5	3.3	18	2.7	98	43.9	4	·	·	·	1	1	·	9	4	12	8	3	1	·	3
X	4.5	2.1	6	2.7	7	2.9	3.5	1.9	12	1.8	15.5	3.3	17	3.2	12.5	3.1	15	2.3	16	6.4	16	·	·	6	·	·	·	3	9	8	5	·	13	·	·
XI	7.5	2.5	13	4.6	12	4.8	15	4.8	4.5	2.2	16	5.1	16.5	3.7	2.5	3.2	3	4.1	53	13.6	21	7	14	22	·	·	·	·	22	16	10	1	8	16	·
XII	0.5	1.0	·	·	3.5	3.7	19.5	4.5	15.5	4.1	29	4.4	12.5	3.8	3.5	2.3	9	3.8	53	14.4	18	4	10	24	·	·	·	1	20	20	11	1	6	25	·
Rok	71.5	2.5	80	3.0	137	3.7	139	3.4	126.5	2.8	176	3.6	167	3.7	90	3.2	108	3.2	562	43.9	4.IX	34	66	142	17	4	·	28	153	187	118	14	54	119	19

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Białystok

$H_s = 139$ m $H_b = 140,8$ m $h_w = 11$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	2.9	4	3.8	8.5	3.8	18.5	4.7	23	4.7	11	3.6	4.5	5.8	6	5.9	13	3.8	42	9.7	20	4	13	28	·	3	·	2	22	14	8	·	11	31	·
II	11.5	4.7	8.5	5.5	2.5	2.6	1	3.0	8.5	5.1	16	5.1	20.5	3.4	8.5	4.2	7	4.1	41	12.2	7	13	23	27	·	1	·	·	15	19	11	1	7	28	·
III	4	3.8	2.5	1.4	3	2.8	15.5	4.0	19	4.2	12	3.4	11.5	3.8	6.5	5.3	19	3.1	27	5.9	17	4	7	25	·	·	·	4	16	13	8	·	8	23	·
IV	5.5	4.7	6	4.8	20.5	5.6	30.5	4.6	10.5	4.7	2.5	4.2	2.5	3.4	6	4.4	6	4.5	21	8.0	23	·	·	12	·	3	·	2	14	8	6	·	1	·	2
V	15	3.6	5.5	2.5	11.5	4.6	8.5	3.8	6.5	3.2	7.5	3.2	11.5	3.1	15	4.3	12	3.2	112	45.2	29	·	·	3	·	1	1	1	15	18	13	2	5	·	2
VI	8	3.5	7	5.4	11	5.1	6.5	4.2	8.5	2.9	11.5	3.9	15.5	4.3	12	3.7	10	3.7	68	24.6	13	·	·	·	5	2	·	·	11	13	12	2	·	·	3
VII	3.5	4.4	5.5	3.9	3	2.7	4.5	3.6	16	3.5	26.5	3.6	18	4.1	4	2.1	12	3.2	51	11.3	24	·	·	·	6	1	·	·	8	16	13	1	3	·	4
VIII	7.5	4.0	·	·	1.5	3.3	12.5	3.7	7.5	4.3	7.5	3.5	27.5	3.2	15	3.4	14	3.0	68	29.2	2	·	·	·	9	·	·	1	10	8	7	2	3	·	4
IX	·	·	·	·	4.5	3.6	15.5	3.8	21.5	4.2	19	3.6	12.5	4.1	4	4.2	13	3.3	26	11.3	29	·	·	·	4	1	1	3	4	8	4	1	2	·	3
X	5	2.6	1.5	2.0	3.5	2.9	2.5	5.2	7	3.0	14	3.2	23.5	3.6	18	3.6	18	2.7	13	6.9	16	·	·	5	·	·	·	2	17	7	3	·	10	·	·
XI	1.5	2.3	12.5	4.1	8	3.4	13.5	4.9	13.5	4.1	11	5.6	16.5	3.9	5.5	3.5	8	3.9	58	13.6	21	6	17	23	·	1	·	·	23	19	11	2	9	18	·
XII	·	·	·	·	0.5	6.0	7	5.4	39	3.7	27.5	3.9	2.5	4.4	1.5	4.7	15	3.3	45	7.5	19	3	8	25	·	1	·	·	23	19	13	·	3	25	·
Rok	66	3.0	53	2.8	78	3.9	136	4.2	180.5	4.0	166	3.9	166.5	3.9	102	4.1	147	3.5	572	45.2	29.V	30	68	148	24	14	2	15	178	162	109	11	62	125	18

Uwaga. Kierunki i prędkości wiatru – wg anemometru indukcyjnego.

Przelewice

$H_s = 60$ m $h_w =$ 10 m I–IV, 15 m V–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40	8.0	9	1	3	26	·	—	—	1	19	12	9	·	3	11	·
II	11	3.6	4	2.8	3	2.7	2	2.8	3	3.3	16.5	4.9	23	4.3	14.5	4.9	7	3.9	28	8.9	13	3	12	27	·	3	·	2	17	14	8	·	2	27	·
III	5	3.0	5.5	3.2	2	2.0	9.5	2.6	22	2.7	15	2.6	17.5	3.1	7.5	4.0	9	2.6	30	7.9	21	6	6	20	·	1	·	7	10	11	6	·	3	21	·
IV	9	2.5	7	2.6	12.5	3.9	18.5	3.8	11	4.2	7.5	3.7	9	3.0	10.5	2.5	5	3.2	66	12.4	28	·	·	3	·	·	·	4	16	20	13	2	·	·	2
V	9.5	3.1	7.5	2.7	20	3.1	12	4.2	5.5	2.5	6	3.5	14	3.5	14.5	2.7	4	3.1	96	25.5	9	·	·	1	·	1	·	1	15	15	9	3	·	·	2
VI	6	3.3	6.5	3.1	8.5	3.2	8.5	3.5	10.5	3.3	10	3.4	22.5	3.8	12.5	2.6	5	3.2	43	11.1	18	·	·	·	4	·	·	·	8	9	7	1	·	·	3
VII	2	2.0	5.5	2.9	3	2.0	7.5	3.1	9	2.5	41	3.4	19.5	3.8	3.5	2.0	2	3.2	35	38.9	17	·	·	·	3	·	·	·	11	17	13	2	1	·	4
VIII	3	2.3	1	1.0	1.5	1.0	6	2.8	10.5	2.7	22.5	2.4	18	2.4	16.5	2.2	14	2.0	34	14.4	23	·	·	·	4	·	·	—	—	12	5	1	·	·	·
IX	4	1.5	0.5	2.0	5	4.2	14	4.2	19	3.7	28	3.0	14.5	3.7	2	1.5	3	3.3	65	17.2	10	·	·	·	1	2	·	2	8	12	8	2	·	·	·
X	3	1.7	5	2.2	6.5	2.3	18	2.2	7	2.4	19.5	5.0	7.5	3.1	11.5	2.4	15	2.5	14	7.3	31	·	·	5	·	·	·	4	4	4	4	·	6	·	·
XI	1.5	4.7	9	2.8	15	3.2	12	4.5	13.5	5.4	24	5.1	8.5	4.6	2.5	3.8	4	4.2	27	7.0	21	5	12	16	·	3	·	·	17	13	7	·	3	14	·
XII	·	·	·	·	8.5	3.2	10	5.9	15.5	5.1	37	6.2	11.5	5.3	8.5	2.1	2	5.1	39	15.1	9	·	3	23	·	4	·	·	21	16	6	2	1	4	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	567	38.9	17.VII	15	36	121	12	—	—	—	—	155	95	13	19	77	11

Ostrołęka

φ = 53°05' λ = 21°34'

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień
I	999.3	1016.5	980.0	1011.5	0.5	−4.6	4.0	9	−18.4	11	−2.7	−1.0	−2.0	−1.9	4.7	5.0	4.9	4.9	91	86	90	89	0.4	0.8	0.5	0.6	7.9	7.9	6.6	7.5
II	1001.7	1021.5	978.2	1014.1	−2.1	−10.1	1.7	14, 17	−25.2	6	−7.4	−3.8	−6.2	−5.9	3.4	3.7	3.6	3.6	88	78	89	85	0.4	1.0	0.4	0.6	7.7	6.6	6.4	6.9
III	1004.1	1020.7	976.2	1016.2	4.4	−4.5	11.5	30	−21.9	9	−3.0	3.3	−0.6	−0.2	4.8	5.3	5.3	5.1	91	68	87	82	0.5	2.7	0.9	1.4	6.4	6.2	4.6	5.7
IV	999.8	1016.5	981.2	1011.7	10.6	2.2	15.7	30	−2.8	3	3.9	9.1	6.0	6.2	6.9	6.9	7.1	7.0	84	60	74	73	1.3	4.9	2.4	2.9	7.4	8.1	6.8	7.4
V	1001.7	1017.6	983.2	1013.4	14.4	4.6	21.3	18	−3.5	4	8.0	12.8	9.1	9.8	8.9	8.9	9.1	9.0	81	60	77	73	2.0	6.0	2.7	3.6	6.1	7.4	5.2	6.2
VI	1001.7	1009.2	993.5	1013.2	21.6	10.9	29.8	26	5.4	8	14.8	19.8	15.3	16.3	13.5	13.2	13.9	13.5	80	58	80	73	3.5	10.4	3.7	5.9	6.1	6.8	5.6	6.2
VII	999.6	1011.1	985.1	1011.1	21.4	10.9	30.8	16	5.5	5	14.6	19.8	15.3	16.2	14.0	13.3	14.2	13.8	83	58	81	74	2.9	10.4	3.4	5.6	5.2	7.6	5.2	6.0
VIII	1003.5	1011.4	994.3	1015.0	21.4	10.2	28.5	7	5.4	31	13.0	19.4	14.1	15.2	13.6	14.1	14.2	14.0	90	64	87	80	1.6	9.4	2.4	4.5	5.6	6.8	3.9	5.4
IX	1003.6	1021.2	992.4	1015.1	20.8	9.3	28.5	3	3.2	21	11.1	19.5	13.1	14.2	12.6	13.8	13.4	13.3	94	61	88	81	0.9	9.3	2.0	4.1	5.5	5.7	2.8	4.7
X	1010.4	1026.2	994.9	1022.3	11.9	2.7	19.3	1	−6.0	21	4.6	10.7	6.5	7.1	8.2	9.7	9.2	9.0	95	74	92	87	0.5	3.4	0.8	1.6	7.3	7.5	5.6	6.8
XI	1000.3	1017.6	972.9	1012.5	0.6	−4.2	10.5	2	−17.3	24	−2.6	−0.6	−1.8	−1.7	5.0	5.2	5.3	5.2	91	82	91	88	0.5	1.2	0.5	0.7	8.8	8.6	8.6	8.7
XII	993.5	1010.2	971.3	1005.5	1.6	−2.6	9.0	20	−16.6	17	−0.9	0.4	−0.3	−0.3	5.3	5.5	5.4	5.4	90	86	88	88	0.6	0.9	0.8	0.8	8.9	8.7	8.2	8.6
Rok	1001.6	1026.2	971.3	1013.5	10.6	2.1	30.8	16.VII	−25.2	6.II	4.4	9.1	5.7	6.2	8.4	8.7	8.8	8.6	88	70	85	81	1.3	5.0	1.7	2.7	6.9	7.3	5.8	6.7

Uwaga. W miesiącach I–VI wartości ciśnienia są za niskie przeciętnie o ok. 0,5 mb.

Rypin

φ = 53°04' λ = 19°24'

I	—	—	—	—	1.3	−3.5	5.1	1	−12.3	11	−1.3	0.2	−1.5	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	9.2	7.8	6.7	7.9
II	—	—	—	—	−2.0	−10.7	1.9	13, 14	−24.1	6	−6.9	−3.4	−6.3	−5.7	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.6	5.5	7.2
III	—	—	—	—	3.8	−5.6	10.4	24	−23.7	8	−3.8	2.5	−1.1	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.5	5.5	6.1
IV	—	—	—	—	9.9	2.1	15.5	30	−3.0	3	4.0	8.3	5.4	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.6	5.6	7.1
V	—	—	—	—	13.9	4.0	20.5	17	−2.6	3	8.0	12.5	8.6	9.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.8	5.9	6.8
VI	—	—	—	—	21.2	10.2	30.7	26	4.6	3, 15	14.2	19.6	14.8	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.8	5.0	5.8
VII	—	—	—	—	21.5	10.6	31.2	14	3.8	5	14.3	19.6	14.4	15.7	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.3	5.9	6.6
VIII	—	—	—	—	20.7	10.2	27.9	22	5.0	16	12.7	19.0	14.3	15.1	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.4	5.1	6.3
IX	—	—	—	—	20.1	9.5	27.1	3	1.8	16	11.4	18.5	13.1	14.0	—	—	—	—	—	—	—	—	—	—	—	—	6.1	6.0	4.1	5.4
X	—	—	—	—	12.1	3.1	20.3	1	−4.5	22	4.8	11.0	6.2	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.2	3.9	5.8
XI	—	—	—	—	0.9	−5.1	11.1	2	−19.7	24	−2.6	−0.6	−2.2	−1.9	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.1	8.7	8.4
XII	—	—	—	—	1.8	−2.7	10.0	19	−18.4	17	−0.9	0.3	−0.2	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.5	9.0	9.3	8.9
Rok	—	—	—	—	10.4	1.8	31.2	14.VII	−24.1	6.II	4.5	9.0	5.5	6.1	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.4	5.9	6.9

Toruń - Wrzosy

φ = 53°03' λ = 18°35'

I	1002.4	1018.1	982.2	1011.2	1.7	−3.0	5.4	9	−10.9	11	−1.1	0.7	−1.0	−0.6	5.3	5.4	5.2	5.3	91	83	90	88	0.5	1.2	0.5	0.7	8.3	7.8	6.7	7.6
II	1007.1	1026.0	979.4	1016.2	−1.4	−9.2	2.3	13	−21.2	6	−6.2	−2.6	−5.4	−4.9	3.6	4.1	3.7	3.8	89	80	87	85	0.4	1.0	0.5	0.6	8.0	8.0	6.2	7.4
III	1007.7	1023.5	979.8	1016.6	4.3	−5.6	12.5	29	−26.5	8	−3.7	2.5	−1.4	−1.0	4.8	5.5	5.3	5.2	92	72	89	84	0.4	2.3	0.6	1.1	7.3	6.3	5.1	6.2
IV	1002.9	1023.2	986.6	1011.5	10.3	2.0	15.7	30	−3.9	3	3.6	8.4	5.3	5.6	7.3	7.2	7.5	7.4	90	66	84	80	0.8	4.1	1.5	2.1	8.0	8.2	6.2	7.5
V	1005.6	1021.5	996.4	1014.2	14.4	4.6	21.3	17	−2.5	3	7.8	12.5	8.5	9.3	9.2	8.6	9.1	9.0	85	60	81	75	1.6	6.2	2.3	3.4	7.1	7.3	6.5	7.0
VI	1005.5	1015.1	993.5	1013.9	21.7	10.5	31.3	26	3.8	3	14.3	20.0	15.5	16.3	12.7	11.8	13.2	12.6	78	52	74	68	3.8	12.2	4.6	6.9	5.7	6.6	5.6	6.0
VII	1002.7	1013.7	987.6	1011.0	21.2	11.0	31.4	16	3.8	6	14.4	19.5	14.9	15.9	14.0	12.8	14.3	13.7	84	56	83	74	2.7	10.6	3.0	5.4	6.8	7.7	6.4	7.0
VIII	1006.8	1014.2	996.0	1015.2	21.5	10.0	29.7	6, 22	4.9	2	13.1	19.6	14.4	15.4	13.6	13.0	13.5	13.4	90	59	83	77	1.7	10.7	3.3	5.2	5.8	7.7	4.8	6.1
IX	1005.7	1025.7	992.8	1014.2	20.4	9.1	28.7	3	1.2	16	11.3	19.1	13.0	14.1	12.7	13.1	13.1	13.0	93	60	87	80	1.0	9.6	2.2	4.3	6.3	6.2	4.2	5.6
X	1014.3	1029.9	999.0	1023.0	12.4	2.6	20.5	1	−6.4	22	4.3	11.1	5.6	6.6	8.3	9.8	8.7	8.9	98	74	93	88	0.2	3.7	0.7	1.5	6.9	6.7	3.0	5.5
XI	1002.9	1021.8	973.8	1011.8	1.1	−5.0	11.1	1, 2	−22.8	24	−2.7	−0.1	−2.2	−1.8	5.0	5.4	5.1	5.2	90	83	88	87	0.5	1.1	0.6	0.7	9.1	8.5	7.6	8.4
XII	995.7	1015.6	969.6	1004.5	2.3	−2.6	11.1	19	−19.3	17	−0.6	0.9	−0.3	−0.1	5.4	5.6	5.6	5.5	89	83	89	87	0.7	1.2	0.8	0.8	9.1	8.7	8.6	8.8
Rok	1004.9	1029.9	969.6	1013.5	10.8	2.0	31.4	14.VII	−26.5	8.III	4.5	9.3	5.6	6.2	8.5	8.5	8.7	8.6	89	69	86	81	1.2	5.3	1.7	2.7	7.4	7.5	5.9	6.9

Przasnysz

φ = 53°01' λ = 20°53'

I	—	—	—	—	0.0	−4.7	3.4	9	−19.0	11	−2.7	−0.7	−2.3	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.6	7.9	8.0
II	—	—	—	—	−2.7	−10.1	1.3	14	−27.3	6	−7.3	−3.6	−6.4	−5.9	—	—	—	—	—	—	—	—	—	—	—	—	8.5	6.9	8.0	7.8
III	—	—	—	—	2.9	−4.8	10.7	30	−20.0	9	−3.2	2.2	−1.0	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.8	7.6	7.5
IV	—	—	—	—	9.2	1.9	14.7	28, 30	−2.5	3	3.9	8.0	5.1	5.5	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.5	7.7	7.3
V	—	—	—	—	13.7	4.9	20.3	18	−2.4	4	8.3	12.7	8.6	9.6	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.6	6.0	6.0
VI	—	—	—	—	20.7	10.7	27.8	26	5.4	8	14.5	19.7	14.6	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.4	4.3	5.0	4.9
VII	—	—	—	—	20.9	10.4	29.4	15	4.9	5	14.6	19.7	14.5	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.5	4.6	5.7	5.3
VIII	—	—	—	—	21.0	10.3	28.9	7	6.2	2	13.4	19.7	14.4	15.5	—	—	—	—	—	—	—	—	—	—	—	—	5.9	3.9	5.2	5.0
IX	—	—	—	—	20.2	8.7	27.7	3	3.5	16	11.3	20.0	12.7	14.2	—	—	—	—	—	—	—	—	—	—	—	—	6.8	4.8	5.6	5.7
X	—	—	—	—	11.6	3.3	19.7	1	−3.8	21	5.0	11.5	6.8	7.5	—	—	—	—	—	—	—	—	—	—	—	—	8.1	5.5	7.3	7.0
XI	—	—	—	—	0.1	−4.1	10.2	2	−18.0	24	−2.9	−0.2	−1.8	−1.7	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.6	9.0	9.0
XII	—	—	—	—	1.0	−3.0	8.7	19, 20	−17.2	17	−0.9	0.5	−0.8	−0.5	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.0	8.5	8.5
Rok	—	—	—	—	9.9	2.0	29.4	15.VII	−27.3	6.II	4.5	9.1	5.4	6.1	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.1	7.0	6.8

Ostrołęka $H_s = 95\ m$ $H_b = 96,3\ m$ $h_w = 13\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8	1.9	4.5	3.0	7	2.8	20.5	3.5	17.5	3.3	20	4.0	3.5	4.3	8	6.0	4	3.4	41	7.3	30	3	8	28	·	3	·	·	17	17	13	·	3	29	·
II	9.5	5.2	11	4.1	2.5	3.4	0.5	1.0	3.5	2.3	20	5.1	15	3.7	15	4.3	7	4.0	27	8.3	7	12	21	27	·	3	·	1	12	15	8	·	1	28	·
III	1	1.5	4	2.0	6.5	1.8	10.5	3.0	17.5	2.4	21	3.2	9	3.1	9.5	5.3	14	2.6	20	4.6	3	5	7	24	·	3	·	5	11	11	7	·	8	20	·
IV	8.5	3.1	4.5	4.0	16.5	4.8	28	4.3	10.5	3.5	9.5	2.8	1.5	3.3	7	4.5	4	3.8	42	8.7	21	·	·	9	·	2	·	1	15	13	9	·	1	·	2
V	12	3.9	11	2.4	5.5	4.5	12.5	3.5	3.5	2.9	14	3.5	3.5	3.3	7	3.5	24	2.5	48	18.5	19	·	·	2	·	2	·	4	11	14	8	1	1	·	1
VI	5.5	5.2	8	4.3	9	3.6	12	3.4	5	3.2	15	3.3	16.5	3.2	9	3.0	10	3.1	48	16.7	13	·	·	·	5	·	·	4	8	11	7	2	·	·	1
VII	1	2.5	7	3.5	2	3.0	11.5	2.6	13.5	3.4	37.5	4.6	7	4.0	2.5	1.6	11	3.4	105	22.3	31	·	·	·	5	1	·	2	7	16	13	4	1	·	5
VIII	6	3.2	1	1.5	1.5	1.3	14	3.6	7	2.4	11.5	2.7	14	2.7	17	2.8	21	2.2	91	26.2	26	·	·	·	9	·	·	5	7	13	9	3	3	·	5
IX	·	·	·	·	3	3.0	32	2.8	7.5	2.8	27.5	3.4	7	3.4	·	·	13	2.6	45	28.5	29	·	·	·	4	2	·	9	4	10	6	1	1	·	2
X	4	1.9	1.5	2.7	1.5	2.7	3	2.3	8	2.6	17.5	3.2	16.5	2.7	17	2.3	24	2.0	9	5.5	16	·	·	6	·	·	·	·	10	6	2	·	11	·	·
XI	2.5	2.0	14	3.5	7.5	3.4	13	4.5	8.5	3.0	26	4.1	8.5	3.1	2	4.5	8	3.4	46	11.0	21	7	15	20	·	1	·	·	21	16	11	1	8	16	·
XII	·	·	·	·	·	·	12.5	4.8	19	4.1	36	4.7	16.5	2.8	3	2.3	6	3.9	41	8.4	18	2	5	24	·	1	·	·	23	21	11	·	5	20	·
Rok	58	2.5	66.5	2.6	62.5	2.9	170	3.3	121	3.0	255.5	3.7	118.5	3.3	97	3.3	146	3.1	563	28.5	29. IX	29	56	140	23	18	·	31	146	163	104	12	43	113	16

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Rypin $H_s = 98\ m$ $h_w = 13,6\ m$

I	2	3.0	·	·	9	4.8	18.5	6.7	9	5.3	8.5	5.7	6.5	9.7	5.5	7.1	34	4.0	26	5.0	8	2	9	28	·	4	2	1	16	16	9	·	13	13	·
II	16	4.4	2	4.8	·	·	·	·	0.5	5.0	10.5	8.4	23	6.7	9	5.8	23	4.5	31	4.0	26	13	21	27	·	7	3	1	13	17	14	·	3	28	·
III	3	3.7	1	3.0	2.5	4.2	9	4.9	10	4.4	10.5	5.2	11.5	4.6	4.5	8.0	41	2.8	35	10.3	4	7	10	23	·	5	·	6	11	16	8	2	7	18	·
IV	2.5	6.4	7	9.4	13.5	9.4	13	6.5	3	5.2	5	4.2	17.5	5.4	5.5	5.9	23	5.1	32	6.1	23	·	·	6	·	7	6	1	12	14	10	·	2	·	·
V	7.5	3.5	4	4.9	11.5	7.1	5	5.1	3	4.7	8	9.0	6.5	5.5	12.5	4.6	35	3.6	48	14.8	19	·	·	6	·	4	2	2	14	17	12	1	2	·	2
VI	3.5	3.9	4.5	4.8	11.5	4.8	3.5	4.1	3	4.3	12	5.1	14	4.9	6	4.9	32	3.2	65	21.1	1	·	·	·	4	2	1	4	10	11	11	2	·	·	5
VII	3.5	3.3	0.5	3.0	7	4.5	2	4.5	5	4.2	22.5	6.2	21.5	5.4	1	4.5	30	3.6	74	14.5	21	·	·	·	5	4	·	2	9	17	13	1	·	·	10
VIII	·	·	0.5	7.0	0.5	7.0	6	4.0	3.5	3.9	7	4.4	24	4.0	5.5	3.1	46	2.0	52	12.8	4	·	·	·	7	·	·	·	10	14	11	2	3	·	2
IX	0.5	5.0	0.5	5.0	9.5	3.9	8.5	4.9	10.5	3.8	14.5	3.6	15.5	5.3	1.5	4.3	29	2.9	78	46.5	4	·	·	·	1	2	1	7	7	8	7	3	6	·	·
X	2	3.5	·	·	3	6.7	0.5	3.0	1.5	3.0	12	4.0	20	4.2	3	4.0	51	1.9	16	6.6	16	·	·	7	·	·	·	4	10	5	4	·	15	·	1
XI	1.5	3.7	8.5	4.4	8.5	5.0	8.5	8.5	8	6.9	22.5	6.4	5.5	3.5	1	4.0	26	4.2	24	8.2	21	7	12	23	·	6	2	2	21	13	4	·	6	16	·
XII	·	·	·	·	2.5	6.6	9	6.4	15	5.6	24	7.1	15.5	5.5	1	3.5	26	4.5	48	15.5	18	4	7	23	·	8	3	·	22	18	10	1	6	16	·
Rok	42	3.4	28.5	3.9	79	5.3	83.5	4.9	72	4.7	157	5.8	181	5.4	56	5.0	396	3.5	529	46.5	4. IX	33	59	143	17	49	20	30	155	166	113	12	63	91	20

Toruń - Wrzosy $H_s = 69\ m$ $H_b = 70,2\ m$ $h_w =$ 12 m wiatromierz Wilda, 13 m anemometr

I	3	2.7	5.5	3.4	8.5	3.1	14	3.5	15	3.4	20	3.2	13.5	3.3	10.5	3.0	3	3.2	20	5.3	30	1	8	28	·	1	·	·	16	14	4	·	5	14	·
II	9	4.0	9.5	4.7	4.5	3.0	3.5	1.3	2	3.5	16	3.6	28.5	3.9	9	4.3	2	3.7	22	5.3	7	11	19	26	·	5	·	·	12	19	7	·	2	28	·
III	7.5	4.2	8.5	3.4	4.5	2.1	19.5	2.4	12	2.7	10	2.9	16.5	3.3	9.5	3.8	5	2.9	43	17.9	3	6	9	22	·	2	·	5	12	12	9	1	8	19	·
IV	9.5	3.4	9	3.4	17.5	5.0	24.5	4.1	7.5	3.8	6.5	2.5	8.5	2.9	5	3.6	2	3.8	33	6.0	28	·	·	9	·	5	·	·	16	14	8	·	1	·	·
V	16	3.4	13.5	3.6	13	4.8	10	4.8	5	2.7	7	3.9	16.5	2.9	7	2.2	5	3.4	60	17.1	19	·	·	4	·	6	·	2	14	16	12	1	6	·	1
VI	9	3.3	9.5	3.9	9.5	4.5	9.5	3.8	7	3.6	14	2.5	15.5	3.2	12	3.4	4	3.3	56	25.6	22	·	·	·	6	5	·	2	9	9	8	2	·	·	5
VII	4.5	3.9	6	3.5	8	2.5	4.5	4.4	11	2.2	30.5	3.1	21	3.7	1.5	3.7	6	3.0	73	15.8	17	·	·	·	4	2	·	2	11	18	16	2	1	·	8
VIII	3.5	2.0	4	1.8	2.5	1.4	10	2.6	7	3.1	14.5	2.2	21	2.3	18.5	2.8	12	2.1	38	10.1	25	·	·	·	9	1	·	2	9	12	9	1	5	·	4
IX	1	5.0	0.5	3.0	10.5	3.1	18.5	3.0	11	2.3	18	2.0	14	2.8	3.5	2.7	13	2.3	78	22.5	4	·	·	·	2	·	·	7	9	11	8	3	4	·	3
X	3	2.0	3	2.0	6	2.5	8	1.9	3.5	1.6	16	2.8	23.5	2.8	10	2.7	20	2.0	12	9.7	16	·	·	9	·	2	1	5	7	7	2	·	17	·	·
XI	3.5	2.4	14	3.4	13	4.0	9.5	5.4	7	4.1	17	3.9	17	4.4	3	1.8	6	3.7	30	10.2	21	6	11	20	·	3	·	1	19	18	8	1	7	16	·
XII	0.5	1.0	2.5	2.2	3	1.5	9	3.8	15	4.4	30.5	4.5	25	3.7	2.5	2.4	5	3.7	33	8.7	18	2	6	22	·	6	·	·	25	15	9	·	9	15	·
Rok	70	3.1	85.5	3.2	100.5	3.1	140.5	3.4	103	3.1	200	3.1	220.5	3.3	92	3.0	83	3.1	498	25.6	22.VI	26	53	140	21	38	1	26	159	165	100	11	65	92	21

Uwaga. W I-VII, X-XII – kierunki i prędkości wiatru – wg anemometru M-47, w VIII kierunki w anemometru, prędkości wg wiatromierza Wilda, w IX kierunki i prędkości – wg wiatromierza Wilda.

Przasnysz $H_s = 120\ m$ $h_w = 14\ m$

I	2	1.5	2.5	3.2	4	3.0	16.5	1.6	15	1.8	20.5	3.2	8.5	5.3	·	·	24	2.0	31	7.4	30	3	14	29	·	1	·	2	21	—	8	·	1	22	·
II	12	3.8	8	3.0	3	1.0	·	·	0.5	3.0	10.5	4.7	24.5	4.1	14.5	3.6	11	3.3	17	2.9	10	14	23	27	·	1	·	1	13	—	6	·	2	28	·
III	4	4.0	5	1.0	3	2.0	7.5	1.9	2	3.2	9.5	5.3	18	1.6	10	1.8	34	1.6	11	3.1	4	6	8	22	·	1	·	·	14	—	5	·	7	19	·
IV	10	1.8	6	2.3	21	2.7	13	2.8	8	3.1	1	2.0	6.5	1.9	11.5	1.4	13	2.0	34	7.8	28	·	·	9	·	·	·	·	10	—	8	·	1	·	1
V	14	2.1	7.5	1.8	11.5	2.7	7.5	1.9	1.5	2.3	5.5	2.8	10.5	1.9	15	1.5	20	1.6	42	14.9	19	·	·	2	·	·	·	1	5	—	8	1	·	·	·
VI	9.5	1.9	5.5	3.5	7.5	3.1	·	·	5.5	2.1	7.5	2.6	18.5	3.1	15	1.7	21	1.9	43	7.5	19	·	·	·	3	·	·	3	2	—	10	·	·	·	3
VII	3.5	1.4	7.5	3.2	4	1.5	2	3.0	7.5	1.7	14	3.2	37	2.5	4.5	1.3	13	2.1	54	16.4	31	·	·	·	5	·	·	3	4	—	11	2	1	·	6
VIII	4	1.4	·	·	·	·	7	1.6	7	2.1	2	1.0	28	2.3	18	2.1	27	1.5	98	33.4	26	·	·	·	10	·	·	2	4	—	8	3	·	·	4
IX	·	·	·	·	3	2.0	9	3.7	15.5	2.0	13	2.2	26.5	2.2	5	1.0	18	1.8	62	29.1	29	·	·	·	2	·	·	2	4	—	8	2	4	·	2
X	7	1.9	3	1.0	6.5	1.9	4.5	1.9	4	1.2	3.5	2.4	29	2.5	20.5	2.0	15	1.8	7	5.2	16	·	·	6	·	·	·	·	8	—	2	·	10	·	·
XI	·	·	5.5	2.3	18.5	1.9	9	3.7	9.5	3.5	5.5	4.7	31	2.9	2	1.5	9	2.6	38	20.3	21	6	15	21	·	·	·	·	23	—	9	1	5	16	·
XII	·	·	·	·	·	·	8.5	2.6	17	2.8	22	3.8	37	2.5	3.5	1.9	5	2.7	40	10.3	18	4	6	25	·	·	·	·	21	—	11	1	1	13	·
Rok	66	1.6	50.5	1.8	82	1.8	84.5	2.1	93	2.4	114.5	3.2	275	2.7	119.5	1.6	210	2.1	477	33.4	26.VIII	33	66	141	20	3	·	14	129	—	94	10	32	98	16

Chodzież — φ = 52°59' — λ = 16°54' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	1.8	−2.5	5.6	1	−9.5	11	−1.1	0.9	−0.7	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.6	6.6	6.7
II	—	—	—	—	−0.3	−6.6	2.7	13	−15.9	6	−4.7	−1.3	−3.6	−3.3	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.5	6.8	7.1
III	—	—	—	—	5.3	−4.3	14.2	29	−21.5	8	−2.5	4.2	−0.4	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.1	5.4	4.3	5.6
IV	—	—	—	—	11.0	2.6	15.6	6	−2.4	5	4.4	10.1	5.7	6.5	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.7	5.3	7.0
V	—	—	—	—	14.8	5.3	20.5	17	−2.4	4	8.6	13.2	9.2	10.0	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.7	6.3	6.5
VI	—	—	—	—	22.0	10.6	31.7	26	6.2	4	15.0	20.5	15.4	16.6	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.7	5.9	5.7
VII	—	—	—	—	20.3	11.1	31.1	14	7.0	4	14.4	18.6	14.5	15.5	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.2	6.3	6.4
VIII	—	—	—	—	21.1	10.8	28.9	6	6.8	2, 31	13.7	19.5	14.4	15.5	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.6	4.5	5.2
IX	—	—	—	—	20.1	9.4	27.4	3	4.9	16	11.8	19.0	12.7	14.0	—	—	—	—	—	—	—	—	—	—	—	—	6.3	5.5	4.3	5.4
X	—	—	—	—	12.6	3.8	21.3	1	−3.7	22	4.9	11.8	6.4	7.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.2	3.9	5.6
XI	—	—	—	—	1.3	−3.5	11.3	1	−14.9	23	−2.0	0.5	−1.3	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.3	6.6	7.6
XII	—	—	—	—	2.5	−2.0	10.5	19	−12.6	17	0.0	1.3	0.2	0.4	—	—	—	—	—	—	—	—	—	—	—	—	9.2	7.3	7.4	8.0
Rok	—	—	—	—	11.0	2.9	31.7	26. VI	−21.5	8. III	5.2	9.9	6.0	6.8	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.7	5.7	6.4

Trzcińsko - Zdrój — φ = 52°58' — λ = 14°36'

I	—	—	—	—	2.7	−1.4	9.3	17	−6.7	31	0.3	1.9	0.6	0.8	—	—	—	—	—	—	—	—	—	—	—	—	9.5	8.8	6.8	8.3
II	—	—	—	—	0.3	—	4.5	13	—	—	−4.3	−1.0	−2.2	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.8	6.7	7.8
III	—	—	—	—	4.9	−5.1	14.8	29	−24.6	8	−2.8	3.8	−0.8	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.3	4.1	5.4
IV	—	—	—	—	11.6	2.8	16.7	6	−1.9	5	5.0	10.4	6.4	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.7	8.8	6.0	7.5
V	—	—	—	—	15.8	6.5	21.0	17	0.7	22	9.1	13.8	10.4	10.9	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.9	6.9	7.2
VI	—	—	—	—	21.7	10.6	27.7	26	3.8	4	14.8	19.6	15.5	16.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	20.0	11.0	30.3	14	5.4	5	14.3	18.6	14.4	15.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	21.0	9.5	28.1	22	4.6	13	13.9	19.7	13.9	15.4	—	—	—	—	—	—	—	—	—	—	—	—	4.9	7.4	4.6	5.6
IX	—	—	—	—	19.2	9.3	25.3	2	4.6	21	11.6	18.3	12.5	13.7	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.0	4.4	6.0
X	—	—	—	—	13.6	2.7	22.2	1	−4.3	23	4.7	12.5	6.0	7.3	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.5	2.8	5.0
XI	—	—	—	—	2.5	−2.9	12.9	1	−17.9	23	−0.9	1.5	−0.5	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	9.6	8.4	6.4	8.1
XII	—	—	—	—	3.7	−0.8	12.5	19	−6.2	13, 14	0.9	2.5	1.3	1.5	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.7	7.6	8.6
Rok	—	—	—	—	11.4	—	30.3	14.VII	—	—	5.6	10.1	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Wądołki Borowe — φ = 52°57' — λ = 22°13'

I	—	—	—	—	−0.4	−5.1	3.1	9	−17.0	11	−3.0	−1.8	−2.5	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	9.3	8.7	7.6	8.5
II	—	—	—	—	−3.4	−11.6	2.1	14	−26.2	6	−8.5	−4.9	−7.1	−6.9	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.0	6.2	7.1
III	—	—	—	—	2.9	−5.0	11.8	30	−23.8	9	−3.6	2.3	−1.2	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.0	4.8	6.3
IV	—	—	—	—	9.9	2.1	15.2	26	−3.3	3	3.9	8.7	5.1	5.7	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.3	6.0	7.5
V	—	—	—	—	13.5	4.5	20.7	18	−3.6	4	7.9	12.7	8.0	9.2	—	—	—	—	—	—	—	—	—	—	—	—	7.0	8.0	5.4	6.8
VI	—	—	—	—	20.2	10.4	27.2	26	3.2	8	14.4	19.0	14.3	15.5	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.3	6.6	7.0
VII	—	—	—	—	20.8	9.9	29.7	16	4.7	5	14.8	19.6	14.4	15.8	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.7	6.1	6.6
VIII	—	—	—	—	20.1	9.9	28.0	7	4.6	31	13.3	19.0	13.2	14.7	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.4	4.4	6.1
IX	—	—	—	—	20.5	8.4	27.2	3	0.3	21	11.3	19.8	12.6	14.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	11.1	2.0	18.8	1	−5.0	21	4.3	10.5	6.1	6.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.0	5.8	7.3
XI	—	—	—	—	−0.1	−5.0	10.7	2	−21.2	17	−2.7	−1.0	−2.4	−2.1	—	—	—	—	—	—	—	—	—	—	—	—	9.0	9.3	8.9	9.1
XII	—	—	—	—	0.9	−3.2	8.7	20	−15.9	17	−1.3	−0.1	−0.7	−0.7	—	—	—	—	—	—	—	—	—	—	—	—	9.5	9.1	8.8	9.1
Rok	—	—	—	—	9.7	1.4	29.7	16.VII	−26.2	6. II	4.2	8.6	5.0	5.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Krzyż — φ = 52°53' — λ = 16°01'

I	—	—	—	—	2.4	−2.6	7.5	17	−9.5	31	−0.8	1.7	−0.1	0.2	5.1	5.8	5.3	5.4	87	84	86	86	0.7	1.1	0.8	0.9	8.3	8.0	7.5	7.9
II	—	—	—	—	−0.3	−7.1	3.5	13	−17.8	28	−4.8	−1.2	−3.1	−3.0	3.7	4.7	4.1	4.2	82	82	82	82	0.8	1.0	0.8	0.9	7.7	7.5	7.4	7.5
III	—	—	—	—	5.2	−6.1	13.9	29	−26.6	8	−3.8	4.0	−1.2	−0.6	4.6	6.2	5.2	5.3	88	74	85	82	0.6	2.3	0.8	1.2	7.6	5.5	4.8	6.0
IV	—	—	—	—	11.4	1.9	16.6	6	−4.4	5	4.3	10.2	5.9	6.6	7.5	7.9	7.9	7.8	89	64	84	79	0.9	4.7	1.5	2.4	7.3	7.4	6.4	7.0
V	—	—	—	—	15.2	4.9	22.1	17	−2.1	4, 22	8.5	13.8	9.3	10.2	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.6	6.7	6.7
VI	—	—	—	—	21.8	9.7	29.2	26	4.5	4	14.6	20.4	15.1	16.3	13.1	12.7	14.0	13.3	78	54	81	71	3.8	11.8	3.4	6.3	4.9	6.6	6.1	5.9
VII	—	—	—	—	20.1	10.4	31.6	14	3.9	2	14.1	18.7	14.5	15.4	14.0	13.7	14.2	14.0	86	64	85	78	2.3	8.6	2.5	4.5	6.0	7.4	6.8	6.7
VIII	—	—	—	—	21.3	8.6	29.0	6	3.7	2, 17	12.4	19.7	13.5	14.8	13.2	13.5	13.6	13.4	91	60	87	79	1.5	9.9	2.3	4.6	5.2	6.6	3.7	5.2
IX	—	—	—	—	20.2	8.1	26.9	3	1.4	23	10.8	19.1	12.5	13.7	12.0	13.3	13.3	12.9	92	61	91	81	1.3	9.2	1.4	3.9	6.2	6.2	4.8	5.7
X	—	—	—	—	13.0	1.5	21.9	1	−5.8	22	3.7	12.0	4.9	6.4	8.0	10.0	8.4	8.8	96	71	94	87	0.3	4.4	0.6	1.8	6.6	6.1	1.8	4.8
XI	—	—	—	—	1.7	−4.1	12.1	1, 2	−21.8	24	−2.0	1.0	−1.5	−1.0	5.3	5.9	5.4	5.5	92	85	90	89	0.4	1.1	0.6	0.7	8.0	8.5	7.1	7.9
XII	—	—	—	—	3.2	−1.7	12.5	19	−8.4	16	0.2	2.1	0.7	0.9	5.7	6.0	5.9	5.9	89	83	89	87	0.7	1.3	0.7	0.9	8.5	8.3	7.7	8.2
Rok	—	—	—	—	11.3	2.0	31.6	14.VII	−26.6	8. III	4.8	10.1	5.9	6.7	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.1	5.9	6.6

Chodzież $H_s = 100$ m $h_w = 12$ m   1965

MIESIĄC	ROZKŁAD WIATRU n(D), Vm(D)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	●	Opad R			≡	⊠	☈
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15			R≥0.1	R≥1.0	R≥10.0			
I	1.5	2.0	5	2.5	12	1.6	8.5	1.6	19.5	1.6	21.5	2.3	3	2.5	3	1.7	19	1.5	48	6.6	17, 25	·	7	27	·	·	·	2	13	19	13	·	1	14	·
II	9.5	3.0	4	2.4	7.5	2.3	1.5	1.3	5.5	2.1	19	2.9	17.5	2.7	9.5	2.0	10	2.3	29	11.4	26	5	15	27	·	·	·	·	11	22	7	1	2	28	·
III	2.5	1.6	3.5	1.9	7.5	2.0	8	1.7	24	1.4	21	2.2	9.5	2.2	6	2.2	11	1.6	73	25.5	3	6	7	22	·	·	·	5	8	15	11	1	3	19	·
IV	5	1.5	4.5	2.3	21	3.0	14.5	2.0	15	1.5	13	1.7	7.5	2.5	4.5	2.7	5	2.0	37	10.5	28	·	·	5	·	·	·	1	12	13	8	1	5	·	·
V	7.5	1.7	4.5	3.1	22	2.6	10	2.2	8	1.8	8.5	1.5	6	2.8	6.5	1.7	20	1.7	97	23.9	9	·	·	3	·	·	·	4	12	21	14	4	·	·	1
VI	6	1.3	4.5	2.3	13.5	2.1	4.5	1.1	16.5	2.0	13.5	1.5	14.5	1.9	7	2.1	10	1.6	29	7.8	17	·	·	·	6	·	·	3	7	11	6	·	·	·	2
VII	3	2.0	3.5	2.0	2.5	2.4	6	2.3	6	2.0	43.5	2.2	9.5	2.4	4	2.6	15	1.9	111	23.7	21	·	·	·	3	·	·	1	8	21	18	3	1	·	5
VIII	2.5	1.6	1	1.0	·	·	1	1.0	13.5	1.7	16.5	1.4	16	1.7	7.5	1.5	35	1.0	42	10.6	12	·	·	·	6	·	·	4	5	15	11	1	2	·	3
IX	3	1.3	1	2.0	4	2.9	5	2.7	28.5	1.5	33.5	2.1	10	2.4	3	2.0	2	1.9	47	14.2	10	·	·	·	1	·	·	5	3	10	9	1	12	·	2
X	2	1.0	2.5	1.0	4	2.0	4.5	1.1	10.5	1.5	20.5	1.9	14	1.8	8	1.1	27	1.1	19	10.5	16	·	·	5	·	·	·	3	3	6	4	1	16	·	1
XI	1	2.0	7	2.0	14	2.0	4	2.2	13.5	1.9	15	2.1	13	2.0	3.5	1.7	19	1.6	54	17.2	21	6	13	20	·	·	·	1	16	17	12	1	5	16	·
XII	1	2.0	·	·	1	5.0	6	1.8	14	2.1	28.5	2.6	11.5	2.7	4	1.5	27	1.7	57	15.3	18	2	4	24	·	·	·	·	15	22	11	2	2	14	·
Rok	44.5	1.8	41	1.9	109	2.3	73.5	1.8	174.5	1.8	254	2.0	132	2.3	66.5	1.9	200	1.7	643	25.5	3. III	19	46	133	16	·	·	29	113	192	124	16	49	91	14

Trzcińsko - Zdrój $H_s = 60$ m $h_w = 11$ m

I	1	1.0	11	2.2	12.5	3.9	30.5	5.9	6	6.2	10.5	3.4	3.5	4.6	5	3.0	13	3.8	38	9.6	17	·	3	23	·	4	·	·	18	16	9	·	—	9	·
II	6	4.0	16	5.5	26	3.5	13	6.2	4	3.8	1	3.0	4	3.8	3	5.0	11	4.0	42	10.4	26	—	11	—	·	5	1	1	13	14	10	1	—	13[?]	·
III	4	5.2	5	6.3	14.5	3.3	21.5	3.3	4.5	3.8	2	4.5	7.5	3.7	9	3.6	25	2.8	47	16.4	1	8	6	22	·	1	·	8	10	12	9	1	—	20	·
IV	2	3.0	13.5	3.3	18.5	4.6	5	5.2	11	4.6	10	5.1	10	5.8	8	5.0	12	4.0	57	14.0	28	·	·	4	·	3	·	1	17	16	13	2	—	·	3
V	5.5	5.3	21	3.3	21.5	4.0	7	3.6	2	6.0	6	3.3	18.5	4.5	5.5	3.8	6	3.7	138	29.0	10	·	·	·	·	2	·	3	16	16	13	5	—	·	1
VI	4	4.2	12.5	3.1	20	5.4	15	4.1	3.5	3.1	2	3.0	9	4.0	10	3.4	14	3.5	53	8.6	1, 7	·	·	·	5	2	1	—	—	15	11	·	—	·	4
VII	3.5	4.4	5.5	2.2	48	4.9	15.5	4.3	·	·	2.5	5.0	3.5	3.3	4.5	3.4	10	4.0	111	29.0	21	·	·	·	4	3	1	—	—	17	15	4	—	·	7
VIII	3.5	3.0	13	2.2	28	3.1	21	2.9	1.5	1.7	3	3.7	·	·	1	10.0	22	2.3	46	20.9	6	·	·	·	4	1	·	2	7	11	7	1	—	·	1
IX	1	1.0	3	4.3	21.5	3.2	23.5	4.4	4	3.0	6.5	3.2	5.5	7.0	1	3.0	24	2.9	82	23.5	10	·	·	·	2	4	·	4	9	13	9	3	—	·	1
X	1.5	1.3	10.5	1.6	12	4.8	14	3.4	3	2.3	6.5	2.7	7.5	2.5	5	1.8	33	1.9	17	8.0	31	·	·	7	·	2	·	7	5	3	3	·	—	·	·
XI	3	2.0	2	1.0	24.5	6.5	11	6.4	5.5	7.0	7	5.1	10	4.7	13	3.6	14	4.5	36	10.8	21	2	11	18	·	7	·	·	17	15	9	1	—	10	·
XII	0.5	3.0	5	4.2	27	6.4	30.5	7.3	8	3.9	11.5	5.2	3.5	4.1	1	4.0	6	5.7	69	22.0	9	·	3	21	·	12	1	·	21	17	10	2	—	8	·
Rok	35.5	3.1	118	3.3	274	4.5	207.5	4.8	53	3.8	68.5	3.9	82.5	4.0	66	4.1	190	3.6	736	29.0	10.V, 21.VII	—	34	—	15	46	4	—	—	165	118	20	—	60[?]	17

Wądołki Borowe $H_s = 130$ m $h_w = 11{,}4$ m

I	4.5	3.3	9.5	4.1	15	5.3	10.5	4.5	21.5	4.1	11	5.0	6.5	6.3	6.5	5.1	8	4.3	27	6.8	30	3	11	29	·	2	·	1	21	21	7	·	5	23	·
II	10	4.6	8.5	6.3	2.5	4.4	0.5	3.0	8	5.0	19	6.0	15	5.1	9.5	5.4	11	4.7	14	4.2	7	13	23	27	·	2	·	1	10	15	6	·	4	28	·
III	6.5	4.1	1.5	3.0	5	4.0	14.5	4.1	19	3.3	9	4.4	10.5	4.6	10	3.8	17	3.2	19	6.5	17	7	8	25	·	1	·	7	12	13	7	·	4	21	·
IV	4.5	2.9	12.5	5.4	18	5.7	26	4.9	8.5	3.3	7	4.6	1	1.0	7.5	5.5	5	4.6	52	26.1	27	·	·	11	·	4	·	2	17	11	7	1	1	·	1
V	21.5	3.7	7.5	3.3	14	3.9	4	3.1	8	2.2	11	3.8	7	3.9	8	3.8	12	3.1	77	25.6	19	·	·	3	·	·	·	4	16	15	11	2	1	·	2
VI	9.5	3.3	8.5	5.5	11.5	5.1	10.5	2.9	6.5	3.5	11	4.6	13.5	5.6	8	3.9	11	3.9	69	26.0	14	·	·	·	3	·	·	1	11	11	8	3	·	·	2
VII	3	3.0	3.5	4.6	2.5	2.8	7	2.7	15.5	3.0	31.5	4.8	13.5	5.4	2.5	1.8	14	3.5	65	21.5	17	·	·	·	4	1	·	1	11	17	11	1	3	·	7
VIII	7.5	2.3	0.5	2.0	2.5	3.2	11	4.0	7	3.0	10.5	3.2	19.5	3.5	15.5	3.0	19	2.6	58	18.0	8	·	·	·	8	·	·	2	12	11	6	3	2	·	3
IX	·	·	·	·	8.5	2.9	25	3.4	14	3.8	20.5	4.0	11.5	4.8	1.5	1.7	9	3.3	28	18.2	29	·	·	·	2	1	·	—	—	6	4	1	3	·	·
X	4.5	2.6	1.5	1.7	3	4.0	2	2.2	11	3.4	17	3.4	23	4.1	14	3.0	17	2.8	9	5.0	16	·	·	7	·	·	·	1	14	7	2	·	8	·	·
XI	1.5	2.3	16.5	4.3	7	3.9	12	6.0	10	3.5	19.5	6.3	10	4.2	2.5	4.4	11	4.3	39	9.4	1	6	15	21	·	2	·	·	23	15	9	·	5	18	·
XII	0.5	2.0	·	·	2	2.5	14.5	4.7	20.5	5.4	31.5	5.3	15.5	4.8	1.5	2.7	7	4.6	35	7.8	18	2	8	25	·	3	·	·	26	15	9	·	7	19	·
Rok	73.5	2.8	70	3.4	91.5	4.0	137.5	3.8	149.5	3.6	198.5	4.6	146.5	4.4	87	3.7	141	3.7	492	26.1	27. IV	31	65	148	17	16	·	—	—	157	87	11	43	109	15

Krzyż $H_s = 31$ m $h_w = 10$ m

I	4.5	1.4	12.5	2.0	13	1.6	4	1.5	10.5	2.0	28.5	3.0	13.5	1.7	4.5	1.0	2	2.1	37	7.3	8	·	3	27	·	1	·	2	20	15	9	·	2	15	—
II	13	3.5	2	3.0	·	·	3	2.3	2	1.0	27.5	3.3	23.5	2.3	9	2.6	4	2.7	20	8.9	26	5	17	26	·	1	1	3	16	8	7	·	·	28	—
III	14	2.9	6	2.3	6	1.3	6	2.0	13	1.5	18	1.9	17	4.4	6	5.5	7	2.5	57	16.6	4	7	7	23	·	2	2	5	13	11	8	2	8	19	—
IV	10	4.4	7.5	8.2	21.5	4.5	9.5	4.2	8	3.0	12.5	3.7	14	3.9	4	3.5	3	4.2	47	13.6	28	·	·	8	·	4	2	3	14	12	9	2	1	·	—
V	22.5	2.5	6	4.0	23	5.0	·	·	4	4.0	3	3.7	26	4.2	6.5	3.8	2	3.8	100	27.3	9	·	·	5	·	2	·	4	14	14	10	3	·	·	—
VI	12	2.7	9	5.9	25	4.0	8.5	3.1	1.5	5.0	18.5	4.4	17	5.4	9	4.1	12	3.9	52	12.6	26	·	·	·	6	3	1	1	8	8	7	1	·	·	—
VII	6	2.2	5	3.0	9	3.0	1	5.0	9	2.1	37	3.5	21.5	3.1	0.5	3.0	4	3.0	147	24.3	9	·	·	·	4	·	·	1	10	22	17	7	·	·	—
VIII	1	7.0	1	1.0	5	1.0	2	1.0	13.5	1.4	25.5	1.7	32	2.2	4	2.0	9	1.7	49	20.2	23	·	·	·	5	·	·	3	3	12	10	1	1	·	—
IX	1	1.0	3	3.0	4.5	3.7	4.5	5.0	16	2.1	35.5	2.7	7.5	2.6	·	·	18	2.2	86	27.5	11	·	·	·	1	·	·	2	7	8	8	3	2	·	—
X	6.5	1.3	4	2.0	5.5	2.6	2	2.0	4	1.8	30	2.8	18	1.8	3	1.3	20	1.7	20	9.8	16	·	·	13	·	·	·	5	2	3	3	·	5	·	—
XI	6.5	4.4	14.5	4.5	11	3.8	2	1.0	12.5	2.8	31.5	4.0	10	1.6	·	·	2	3.5	49	12.5	27	6	12	20	·	1	·	·	13	14	10	2	2	9[?]	—
XII	·	·	3	3.0	3	1.0	10.5	2.1	16.5	1.9	44	3.2	15	2.7	·	·	1	2.7	60	16.0	18	·	4	22	·	1	·	1	19	16	8	3	1	6	—
Rok	97	2.8	73.5	3.5	104	2.6	53	2.4	110.5	2.4	311.5	3.2	215	3.0	46.5	2.2	84	2.8	724	27.5	11. IX	18	43	144	16	15	6	30	139	143	106	24	22	77[?]	—

Ciechocinek

$\varphi = 52°53'$ $\lambda = 18°48'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.0	−2.4	5.8	1	−10.6	11	−0.7	1.1	−0.6	−0.2	5.4	5.5	5.4	5.4	91	82	90	88	0.5	1.2	0.6	0.8	8.2	8.3	7.0	7.8
II	–	–	–	–	−0.6	−8.7	2.7	14	−18.1	6, 24	−5.8	−2.0	−4.7	−4.3	3.6	4.1	3.9	3.9	88	76	87	84	0.5	1.2	0.5	0.7	7.7	8.0	5.9	7.2
III	–	–	–	–	5.3	−4.9	12.5	30	−24.1	8	−3.2	3.1	−0.5	−0.3	4.9	5.7	5.6	5.4	92	73	90	85	0.4	2.4	0.7	1.2	6.7	6.9	5.3	6.3
IV	–	–	–	–	10.9	2.5	16.8	30	−1.7	3, 6	4.0	9.2	6.0	6.3	7.2	7.4	7.7	7.4	87	64	82	78	1.1	4.5	1.8	2.5	7.4	7.7	6.1	7.1
V	–	–	–	–	14.9	5.2	21.7	18	−2.2	3	8.3	13.4	9.3	10.1	9.4	9.4	9.2	9.3	84	61	80	75	1.8	6.2	2.5	3.5	6.7	7.1	6.0	6.6
VI	–	–	–	–	22.2	11.0	31.3	26	5.3	3	14.7	20.5	15.7	16.6	13.6	13.5	14.1	13.7	81	57	78	72	3.3	11.2	4.0	6.2	4.9	6.5	4.6	5.3
VII	–	–	–	–	22.4	11.6	30.9	14	6.1	2	15.0	20.8	15.4	16.6	14.5	14.4	14.8	14.6	83	58	83	75	2.9	10.9	3.1	5.6	5.3	7.2	4.6	5.7
VIII	–	–	–	–	22.0	10.9	29.4	22	5.9	31	13.4	20.6	15.0	16.0	13.9	14.2	14.5	14.2	90	60	85	78	1.7	10.8	2.9	5.1	5.3	6.5	4.2	5.3
IX	–	–	–	–	21.1	9.5	29.1	3	2.0	16	11.7	19.9	13.6	14.7	13.0	14.6	13.9	13.8	93	64	89	82	1.0	9.1	1.9	4.0	4.9	5.6	3.6	4.7
X	–	–	–	–	13.0	3.3	22.4	1	−4.5	22	4.7	12.0	6.3	7.3	8.4	10.3	9.2	9.3	96	73	94	88	0.4	4.1	0.6	1.7	7.2	6.0	3.3	5.5
XI	–	–	–	–	1.4	−4.2	11.8	2	−20.0	24	−2.2	0.3	−1.6	−1.3	5.3	5.7	5.4	5.5	93	85	90	89	0.4	1.0	0.6	0.7	9.6	8.1	8.0	8.6
XII	–	–	–	–	2.4	−2.2	10.6	19	−18.4	17	−0.1	1.3	0.3	0.4	5.7	5.7	5.8	5.7	91	83	89	88	0.6	1.2	0.8	0.9	8.1	8.5	8.2	8.3
Rok	–	–	–	–	11.4	2.6	31.3	26.VI	−24.1	8.III	5.0	10.0	6.2	6.8	8.7	9.2	9.1	9.0	89	70	86	82	1.2	5.3	1.7	2.7	6.8	7.2	5.6	6.5

Więcławice

$\varphi = 52°51'$ $\lambda = 18°19'$

I	–	–	–	–	1.2	−2.5	4.8	1	−10.2	11	−1.2	0.6	−0.7	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.0	7.1	7.4
II	–	–	–	–	−2.0	−9.5	1.9	13	−21.2	6	−6.3	−2.7	−5.3	−4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	7.0	7.2
III	–	–	–	–	3.4	−5.0	12.0	29	−24.7	8	−3.2	2.5	−0.6	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.5	7.2	7.2
IV	–	–	–	–	10.2	2.5	15.4	30	−1.0	11	4.6	9.3	5.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	7.2	7.1
V	–	–	–	–	14.3	5.4	20.9	17	−2.3	3	8.7	13.1	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	6.5	6.7
VI	–	–	–	–	21.7	10.9	31.3	26	6.2	15	15.6	20.5	15.5	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.7	5.3	5.6
VII	–	–	–	–	20.9	11.3	30.3	14	6.4	3	15.2	19.7	15.2	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.3	6.1	5.7
VIII	–	–	–	–	21.1	10.7	29.2	22	6.5	31	14.3	19.8	15.3	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.8	6.3	6.1
IX	–	–	–	–	20.2	9.5	27.9	3	3.9	16	12.9	19.2	13.3	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.0	5.9	5.7
X	–	–	–	–	12.4	3.5	21.7	1	−2.8	22, 23	5.4	11.8	7.1	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.5	6.3	6.3
XI	–	–	–	–	1.1	−4.7	10.9	2	−18.4	24	−2.6	0.1	−1.5	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	8.0	7.8
XII	–	–	–	–	2.2	−2.3	10.7	19	−19.2	17	−0.4	0.9	0.3	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	8.1	8.1
Rok	–	–	–	–	10.6	2.5	31.3	26.VI	−24.7	8.III	5.2	9.6	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.3	6.8	6.7

Szepietowo

$\varphi = 52°51'$ $\lambda = 22°33'$

I	–	–	–	–	−0.5	−5.2	3.1	18	−16.9	11	−3.3	−2.1	−2.8	−2.8	4.4	4.7	4.5	4.5	87	86	87	87	0.6	0.7	0.6	0.6	8.4	8.0	7.6	8.0
II	–	–	–	–	−3.6	−10.4	2.2	14	−23.2	6	−8.2	−5.2	−7.2	−7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.7	5.5	6.6
III	–	–	–	–	2.9	−4.4	11.3	30	−21.2	8	−3.3	2.0	−0.9	−0.8	4.7	5.3	5.0	5.0	90	74	83	82	0.4	2.0	0.9	1.1	7.4	6.2	6.0	6.5
IV	–	–	–	–	9.8	1.9	15.4	27	−3.4	3	3.2	8.5	5.3	5.6	6.9	6.7	7.1	6.9	88	60	78	75	0.9	4.7	1.9	2.5	6.8	7.4	5.9	6.7
V	–	–	–	–	13.3	4.5	20.2	18	−2.6	4	7.3	12.2	8.7	9.2	8.7	8.6	8.9	8.7	82	60	78	73	1.7	5.8	2.5	3.3	6.2	7.7	5.2	6.4
VI	–	–	–	–	19.8	10.9	27.7	26	4.7	8	13.8	18.5	14.8	15.5	13.2	12.8	13.9	13.3	83	62	82	76	2.7	9.0	3.2	5.0	6.1	7.3	6.4	6.6
VII	–	–	–	–	20.8	11.0	29.7	16	5.5	5	14.2	18.9	15.1	15.8	13.6	13.1	13.8	13.5	83	60	79	74	2.9	9.4	3.7	5.3	4.5	7.3	6.0	5.9
VIII	–	–	–	–	20.2	10.5	28.0	7	5.5	31	12.7	18.7	14.2	15.0	13.3	13.1	13.4	13.3	90	62	83	78	1.6	9.2	3.1	4.6	5.6	6.1	3.7	5.1
IX	–	–	–	–	20.4	9.0	27.2	3	3.1	21	10.6	19.4	13.2	14.1	12.1	12.7	13.1	12.6	93	56	85	78	1.0	10.4	2.4	4.6	5.0	4.9	4.0	4.6
X	–	–	–	–	11.2	2.7	19.9	1	−5.1	21	4.1	10.1	6.5	6.8	7.7	9.1	8.6	8.5	92	72	87	84	0.7	3.7	1.3	1.9	7.5	7.2	4.7	6.5
XI	–	–	–	–	0.1	−4.6	10.7	2	−18.2	17	−2.8	−1.2	−2.3	−2.2	4.8	5.1	5.0	5.0	88	86	90	88	0.6	1.0	0.6	0.7	8.9	8.7	8.0	8.5
XII	–	–	–	–	0.9	−2.9	8.2	20	−15.8	17	−1.4	−0.2	−0.8	−0.8	5.2	5.4	5.2	5.3	91	87	88	89	0.4	0.8	0.7	0.6	8.6	8.1	7.3	8.0
Rok	–	–	–	–	9.6	1.9	29.7	16.VII	−23.2	6.II	3.9	8.3	5.3	5.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.1	5.9	6.6

Głodowo

$\varphi = 52°50'$ $\lambda = 19°15'$

I	–	–	–	–	1.2	−3.3	4.7	1	−11.6	11	−1.2	0.4	−1.3	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	7.5	7.8
II	–	–	–	–	−2.0	−10.2	1.9	13	−23.8	6	−6.7	−3.3	−5.7	−5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	6.2	7.2
III	–	–	–	–	3.8	−5.0	11.2	30	−21.1	9	−2.9	2.7	−1.1	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.4	5.8	6.6
IV	–	–	–	–	9.7	2.2	15.1	30	−1.8	3	4.3	8.4	5.1	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.8	6.6	7.4
V	–	–	–	–	13.5	4.4	20.6	17	−2.3	3	8.4	12.3	8.2	9.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	5.2	6.5
VI	–	–	–	–	21.1	10.3	30.9	26	4.7	3	14.5	19.6	14.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.9	4.7	5.2
VII	–	–	–	–	20.8	10.9	29.7	14	4.9	5, 6, 11	15.2	19.2	14.3	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	5.7	6.4
VIII	–	–	–	–	20.8	10.1	28.5	7	4.7	31	14.0	19.5	13.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.1	4.7	5.5
IX	–	–	–	–	20.0	9.2	27.2	3	0.9	16	12.2	18.8	12.6	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.8	3.6	4.8
X	–	–	–	–	11.9	2.6	20.5	1	−4.8	22	4.9	11.2	5.8	6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.5	3.5	5.4
XI	–	–	–	–	0.8	−5.1	11.2	2	−22.4	24	−2.8	−0.5	−2.2	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	8.2	8.4
XII	–	–	–	–	1.7	−2.8	10.1	19	−20.8	17	−0.8	0.4	−0.3	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.6	8.5	8.4
Rok	–	–	–	–	10.3	1.9	30.9	26.VI	−23.8	6.II	4.9	9.1	5.3	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.9	5.9	6.6

Ciechocinek — $H_s = 44 m$ — $h_w = 16,7 m$ — 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Max<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	1.2	7	1.6	7	2.0	18.5	2.4	12.5	3.4	27	3.6	7	2.1	6.5	4.3	3	2.8	23	4.1	8, 30	1	2	27	·	2	·	1	18	18	9	·	1	10	·
II	9.5	3.8	10.5	3.1	1.5	2.7	1	2.0	2	3.0	18.5	3.3	15	2.8	17	3.4	9	2.9	24	5.1	26	10	13	26	·	1	·	1	14	20	9	·	2	28	·
III	1	2.0	9.5	2.5	4	1.8	10	2.4	16	1.8	20.5	2.1	14.5	2.1	10.5	2.7	7	2.0	41	19.4	3	6	6	22	·	·	·	5	13	16	9	1	5	17	·
IV	9	3.0	7	3.2	15	4.2	24.5	3.9	9	2.6	4.5	1.4	8.5	2.1	7.5	2.5	5	3.0	44	13.1	28	·	·	4	·	1	·	2	14	14	8	1	2	·	·
V	16.5	2.7	12	3.2	14.5	3.6	8.5	4.7	1.5	1.3	8	3.8	12.5	2.8	7.5	1.4	12	2.7	69	19.3	19	·	·	2	·	1	·	3	13	18	11	2	2	·	2
VI	8	3.1	9.5	4.0	5.5	5.6	5.5	4.5	7	3.9	13.5	2.2	16.5	2.5	14.5	2.4	10	2.8	54	16.0	26	·	·	·	6	3	1	6	8	14	7	1	·	·	3
VII	3.5	2.3	8	3.1	3	1.8	6	3.1	3	2.5	29	3.0	27.5	2.8	3	1.7	10	2.5	62	12.7	31	·	·	·	8	1	·	3	9	17	14	2	·	·	4
VIII	12	1.5	0.5	1.0	0.5	4.0	6.5	4.5	9	3.4	13.5	1.8	20	1.4	16	1.7	15	1.7	54	22.0	4	·	·	·	9	1	·	5	6	13	9	1	·	·	3
IX	1	1.0	0.5	1.0	5.5	2.1	19	3.0	10.5	2.8	13	2.3	23.5	1.9	5	2.1	12	2.0	47	18.0	28	·	·	·	3	1	·	8	6	12	6	1	2	·	·
X	7.5	1.3	5	1.2	7	1.6	1.5	2.0	12	1.5	13.5	2.0	20	1.8	10.5	1.4	16	1.3	16	11.4	16	·	·	5	·	1	·	5	7	8	3	1	13	·	·
XI	·	·	13.5	2.6	11.5	2.4	8	4.2	7.5	3.3	15.5	3.7	23	2.7	5	1.6	6	2.8	46	17.5	21	6	11	20	·	3	1	1	22	17	8	1	6	16	·
XII	·	·	4	1.0	1.5	1.0	6	4.0	14	4.1	32.5	5.1	28.5	2.3	3.5	2.0	3	3.5	49	13.5	18	2	4	19	·	4	2	·	19	19	10	1	4	14	·
Rok	72.5	1.8	87	2.3	76.5	2.7	115	3.4	104	2.8	209	2.9	216.5	2.3	106.5	2.3	108	2.5	529	22.0	4.VIII	25	36	125	26	19	4	40	149	186	103	12	37	85	12

Więcławice — $H_s = 90 m$ — $h_w = 22 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Max<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	1.5	3	1.7	14	2.4	10	1.6	4	1.6	24	1.7	19	2.3	12	2.6	5	1.9	17	3.2	16	1	8	26	·	·	·	·	15	14	8	·	9	10	·
II	7	2.3	7	2.3	5	3.6	1	2.0	·	·	9	2.1	37	3.0	16	2.2	2	2.6	7	2.0	26	14	24	27	·	·	·	·	7	14	2	·	5	28	·
III	2	2.5	22	2.0	4	2.5	3	2.7	3	3.3	10	1.5	17	2.4	9	3.2	23	1.7	22	12.5	3	7	9	20	·	·	·	·	7	11	6	1	13	19	·
IV	9	2.2	8	2.4	28	4.0	13	2.6	4	1.8	10	2.3	14	2.8	2	3.0	2	2.9	43	15.3	28	·	·	6	·	2	·	·	12	10	8	1	1	·	1
V	6	1.8	23	2.3	17	2.8	8	2.9	3	2.3	4	1.2	16	4.0	11	1.5	5	2.4	71	20.5	19	·	·	2	·	1	·	·	9	16	12	2	3	·	·
VI	13	1.8	7	2.7	17	3.4	3	1.3	5	3.2	9	2.0	28	2.5	5	2.2	3	2.4	37	9.5	22	·	·	·	5	·	·	3	5	10	7	·	·	·	4
VII	1	2.0	8	3.4	5	2.8	3	2.7	6	2.8	13	3.4	50	2.9	2	4.5	5	2.8	48	8.8	31	·	·	·	3	·	·	·	1	14	9	·	·	·	6
VIII	2	1.0	2	1.0	1	1.0	4	2.0	5	2.6	12	2.6	24	2.1	31	2.2	12	1.9	69	16.1	25	·	·	·	8	·	·	·	5	13	12	2	1	·	3
IX	1	3.0	·	·	12	3.1	9	1.6	15	1.8	23	2.5	20	2.0	4	3.0	6	2.1	59	19.5	10	·	·	·	2	·	·	1	4	10	10	1	1	·	2
X	4	1.2	1	1.0	6	1.7	7	1.6	1	1.0	9	1.7	26	2.3	16	2.1	23	1.5	14	11.5	16	·	·	7	·	·	·	·	6	5	2	1	11	·	·
XI	·	·	13	2.1	22	3.9	2	4.0	8	3.2	7	2.4	25	2.9	8	1.8	5	2.8	35	13.1	22	8	12	18	·	·	·	·	14	13	8	1	7	16	·
XII	9	2.4	·	·	1	1.0	7	3.6	5	2.8	27	3.3	30	3.5	6	2.2	8	2.9	27	9.4	18	2	3	22	·	·	·	·	18	10	5	·	4	11	·
Rok	56	1.8	94	1.7	132	2.7	70	2.4	59	2.2	157	2.2	306	2.7	122	2.5	99	2.3	449	20.5	19.V	32	56	128	18	3	·	4	103	140	89	9	55	84	16

Szepietowo — $H_s = 150 m$ — $h_w = 14 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Max<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6.5	4.5	3.5	3.1	2.5	2.0	18	5.6	31	3.4	15.5	4.7	5.5	7.4	7.5	6.7	3	4.5	36	6.5	30	3	13	28	·	5	·	1	20	14	9	·	6	29	·
II	20.5	3.6	5	3.8	7	3.3	·	·	3.5	2.6	14.5	5.5	20.5	4.9	13	5.7	·	4.5	25	5.8	7	11	23	26	·	7	·	2	11	14	9	·	2	28	·
III	6.5	3.5	8.5	1.5	5.5	2.5	9	3.4	21	2.9	14	2.7	18	3.3	8.5	4.2	2	2.9	18	6.5	17	4	8	24	·	·	·	5	15	10	5	·	5	21	·
IV	10.5	3.6	4	3.0	13.5	6.3	29	4.3	16.5	4.4	8.5	3.0	3	2.3	4	3.1	1	4.2	51	10.6	26	·	·	12	·	6	·	2	12	12	10	1	1	·	2
V	21	3.3	9.5	2.4	10.5	3.6	9.5	3.8	7	2.4	7.5	4.4	14.5	2.8	10.5	4.2	3	3.2	93	32.9	29	·	·	3	·	1	·	3	11	14	12	3	3	·	2
VI	13	3.0	6.5	3.5	13	3.6	4.5	2.7	7.5	3.5	12.5	3.8	21	3.8	10	2.4	2	3.3	71	22.0	13	·	·	·	2	1	·	2	11	12	9	2	·	·	2
VII	4.5	2.4	6	3.2	2	1.5	4.5	2.1	15.5	3.2	31	3.9	27.5	4.4	1	2.0	1	3.6	73	11.3	17	·	·	·	3	1	·	2	7	14	13	2	2	·	3
VIII	18.5	4.4	2	4.0	·	·	7.5	4.2	10	2.8	11.5	3.0	22.5	2.9	18	2.9	3	3.2	53	18.8	2	·	·	·	6	3	·	8	7	10	8	2	2	·	3
IX	·	·	1	2.0	0.5	5.0	16	4.8	24	3.5	22	3.1	17.5	4.3	[illegible]	2.2	·	3.6	28	16.4	29	·	·	·	2	2	·	5	2	7	5	1	2	·	2
X	17.5	2.1	2	1.5	4	2.2	3	3.7	12.5	3.3	12	3.8	23.5	4.3	14.5	2.3	4	3.1	11	4.4	16	·	·	5	·	·	·	2	7	5	4	·	9	·	·
XI	4.5	2.8	2.5	3.4	20	2.6	8.5	3.5	11.5	3.6	10.5	5.1	27	4.5	15	5.3	4	3.6	56	12.5	1	6	15	21	·	3	·	·	19	15	13	1	5	18	·
XII	·	·	·	·	1	3.0	11	3.9	22	4.3	30	4.0	23.5	3.4	5.5	2.8	·	3.8	45	12.8	19	2	9	24	·	1	·	·	18	17	13	1	1	17	·
Rok	123	2.8	50.5	2.6	79.5	3.0	120.5	3.5	182	3.3	189.5	3.9	224	4.0	103	3.7	23	3.6	560	32.9	29.V	26	68	143	13	30	·	32	140	144	110	13	38	113	14

Głodowo — $H_s = 129 m$ — $h_w = 10 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Max<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2.5	2.4	1	1.0	7.5	3.3	16	3.4	24.5	3.0	14.5	3.3	12	4.5	6	3.5	9	3.1	20	5.0	8	1	8	28	·	1	·	1	16	13	7	·	9	11	·
II	5.5	5.0	11.5	4.2	4	2.2	1	1.0	9	2.3	14	4.4	26	4.6	10	4.2	3	3.9	18	6.0	26	14	21	27	·	·	·	2	14	14	6	·	3	28	·
III	3.5	3.3	8	3.4	3	3.3	17.5	2.7	15	1.8	11.5	4.8	13	3.7	6.5	5.1	15	2.8	25	7.6	3	7	10	21	·	1	·	3	14	15	7	·	10	18	·
IV	2.5	2.2	7.5	6.0	16	6.6	25.5	4.5	9.5	2.8	5.5	2.7	12	3.1	9.5	3.5	2	4.3	29	6.5	28	·	·	7	·	1	·	1	15	12	8	·	2	·	2
V	14	2.9	6	3.0	17.5	4.3	14.5	4.3	4.5	1.7	8.5	3.9	15	4.0	6	2.5	7	3.3	89	19.8	31	·	·	4	·	·	·	2	13	19	12	3	4	·	1
VI	4.5	3.4	3	6.5	18	4.3	8	2.3	11	3.5	10	2.6	18.5	3.9	7	4.0	10	3.3	46	12.2	30	·	·	·	4	·	·	5	7	14	9	1	·	·	2
VII	0.5	4.0	6	3.3	6.5	3.4	9	2.8	14.5	2.1	29	3.5	20.5	4.8	2	3.5	5	3.3	105	21.4	16	·	·	·	3	·	·	2	9	18	15	3	·	·	5
VIII	2.5	2.6	1	2.0	4	1.9	13	3.7	11.5	2.2	8	2.4	19	3.2	14	3.1	20	2.3	54	12.7	25	·	·	·	8	·	·	6	5	15	10	1	1	·	1
IX	·	·	·	·	7	4.3	20	3.2	21	2.3	20.5	3.4	12	3.6	1.5	3.3	8	2.9	81	43.5	4	·	·	·	1	·	·	7	6	11	5	3	2	·	·
X	3.5	2.0	2.5	1.8	5.5	4.5	2.5	2.0	13.5	1.7	17	3.0	16	3.2	6.5	2.4	26	2.0	12	7.3	16	·	·	5	·	·	·	6	6	13	2	·	15	·	1
XI	1	1.0	6.5	2.9	20	4.3	12	4.3	7	3.2	26	4.5	9.5	3.5	1	4.0	7	3.7	23	7.0	1	7	12	22	·	1	·	2	21	18	8	·	11	16	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	53	15.4	18	3	9	23	·	—	—	·	18	18	10	1	4	16	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	555	43.5	4.IX	32	60	137	16	—	—	37	144	180	99	12	61	89	12

Inowrocław $\varphi = 52°48'$ $\lambda = 18°14'$ 1965

MIESIĄC	CIŚNIENIE P: P_m	Max	Min	$P_{o,m}$	TEMPERATURA T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	—	—	—	—	1.7	−2.2	5.1	1	−9.7	11	−1.1	1.1	−0.6	−0.3	5.2	5.3	5.3	5.3	90	80	89	86	0.6	1.4	0.6	0.9	8.1	7.2	7.3	7.5
II	—	—	—	—	−1.4	−9.0	2.3	13	−19.3	6	−6.0	−2.2	−4.8	−4.4	3.6	4.1	3.9	3.9	86	77	86	83	0.5	1.1	0.6	0.7	8.3	7.8	7.4	7.8
III	—	—	—	—	4.3	−4.3	12.7	29	−22.6	8	−2.6	3.5	−0.4	0.0	4.9	5.8	5.4	5.4	87	72	86	82	0.6	2.4	0.8	1.3	7.6	7.2	4.7	6.5
IV	—	—	—	—	10.6	2.5	15.2	30	−1.2	5	4.3	9.6	5.7	6.3	7.4	7.8	7.8	7.7	88	65	85	79	1.0	4.4	1.4	2.3	8.0	8.3	5.2	7.2
V	—	—	—	—	14.2	5.5	20.8	17	−1.0	3	8.2	13.1	9.2	9.9	9.7	9.6	9.7	9.7	87	64	81	77	1.4	5.8	2.2	3.1	6.9	7.4	6.2	6.8
VI	—	—	—	—	21.6	10.7	31.1	26	5.2	3	14.6	20.7	15.1	16.4	13.6	13.6	13.8	13.7	82	56	80	73	3.1	11.3	3.6	6.0	5.3	6.9	4.3	5.5
VII	—	—	—	—	21.2	11.6	30.3	14	6.5	2, 6	14.7	20.1	14.8	16.1	14.6	15.1	14.8	14.8	86	64	87	79	2.4	9.1	2.5	4.7	6.5	7.1	5.8	6.5
VIII	—	—	—	—	21.4	10.8	28.9	22	6.6	31	13.4	20.5	14.6	15.8	13.9	14.7	14.3	14.3	90	62	86	79	1.7	10.2	2.7	4.9	5.6	7.0	4.1	5.6
IX	—	—	—	—	20.4	10.1	28.5	3	5.0	16	12.1	19.6	13.7	14.8	12.9	13.9	13.6	13.5	91	62	86	80	1.4	9.5	2.4	4.4	5.5	6.1	3.9	5.2
X	—	—	—	—	12.6	3.7	21.5	1	−3.0	22	5.1	12.0	6.8	7.7	8.4	10.3	9.1	9.3	94	73	90	86	0.6	4.1	1.0	1.9	6.7	6.4	2.6	5.2
XI	—	—	—	—	1.3	−4.0	11.1	1	−17.7	24	−2.3	0.6	−1.4	−1.1	5.2	5.5	5.4	5.4	91	80	89	87	0.4	1.4	0.6	0.8	8.8	8.1	7.3	8.1
XII	—	—	—	—	2.2	−1.9	10.5	19	−15.3	17	−0.2	1.5	0.2	0.4	5.7	5.6	5.8	5.7	91	81	89	87	0.6	1.3	0.7	0.9	9.0	8.1	8.2	8.4
Rok	—	—	—	—	10.8	2.8	31.1	26.VI	−22.6	8. III	5.0	10.0	6.1	6.8	8.8	9.3	9.1	9.1	89	70	86	82	1.2	5.2	1.6	2.7	7.2	7.3	5.6	6.7

Bielsk Podlaski $\varphi = 52°47'$ $\lambda = 23°11'$

I	—	—	—	—	−0.2	−5.6	3.4	18	−15.5	11	−3.5	−2.0	−3.3	−3.0	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.6	7.4	8.3
II	—	—	—	—	−3.0	−11.1	2.6	14	−23.0	6	−8.6	−4.8	−7.5	−7.1	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.5	6.3	7.5
III	—	—	—	—	3.8	−4.3	13.3	30	−19.1	9	−3.2	2.5	−1.2	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.0	5.9	7.0
IV	—	—	—	—	10.6	1.8	17.2	27	−4.5	3	3.4	8.8	4.9	5.5	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.0	7.2	7.3
V	—	—	—	—	14.6	4.6	22.2	18	−2.9	4	7.6	12.9	8.8	9.5	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.6	6.4	6.7
VI	—	—	—	—	21.0	10.9	28.7	26	3.9	8	13.8	19.3	14.5	15.5	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.7	6.9	6.6
VII	—	—	—	—	22.1	10.9	30.3	16	6.0	5	14.5	20.3	15.0	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.4	7.1	6.0	6.2
VIII	—	—	—	—	21.3	10.5	28.3	7	5.7	31	13.3	19.7	13.8	15.2	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.2	5.0	6.1
IX	—	—	—	—	21.7	9.3	27.4	3	3.3	21	11.5	19.8	13.2	14.4	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.5	5.1	5.3
X	—	—	—	—	11.7	2.7	20.8	1	−6.4	21	4.3	10.4	6.1	6.7	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.5	5.8	7.3
XI	—	—	—	—	0.6	−4.5	11.6	2	−19.0	17	−2.9	−0.9	−2.6	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.7	8.2	8.8
XII	—	—	—	—	1.3	−3.0	8.3	20	−15.2	17	−1.6	−0.1	−0.7	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.9	8.6	8.6
Rok	—	—	—	—	10.5	1.8	30.3	16.VII	−23.0	6. II	4.0	8.8	5.1	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.4	6.6	7.1

Gorzów Wlkp. $\varphi = 52°44'$ $\lambda = 15°15'$

I	1003.0	1019.5	980.6	1010.5	2.7	−1.2	8.5	17	−5.9	7	−0.1	1.8	0.4	0.6	5.7	6.0	5.8	5.8	93	87	91	90	0.4	1.0	0.6	0.7	8.3	8.7	7.5	8.2
II	1010.4	1026.9	982.0	1018.1	0.1	−5.5	3.7	13	−13.8	28	−4.2	−1.5	−2.5	−2.7	4.1	4.4	4.5	4.3	87	79	85	84	0.5	1.1	0.7	0.8	8.0	8.4	7.1	7.8
III	1009.1	1025.0	983.9	1016.7	5.6	−3.4	15.0	29	−19.3	8	−2.7	3.8	1.3	0.9	5.0	5.8	5.7	5.5	91	71	81	81	0.4	2.6	1.3	1.4	6.5	6.4	4.3	5.7
IV	1003.1	1025.5	982.9	1010.6	11.8	3.3	17.3	6	−0.6	1	4.2	9.8	7.2	7.1	7.7	8.0	8.2	8.0	92	67	81	80	0.7	4.3	2.0	2.3	7.9	7.9	6.4	7.4
V	1006.6	1021.6	992.3	1013.9	15.6	6.5	22.0	17	−0.2	3	8.5	13.6	10.8	10.9	9.9	9.8	9.9	9.9	87	64	75	75	1.4	6.0	3.3	3.6	6.1	7.6	6.6	6.8
VI	1006.8	1018.5	992.6	1014.0	21.6	11.3	28.3	26	6.9	3	13.8	19.7	16.2	16.5	13.1	12.5	13.1	12.9	83	55	72	70	2.8	11.0	5.6	6.5	5.9	7.4	5.7	6.3
VII	1003.9	1014.0	988.4	1011.0	20.4	11.4	32.2	14	6.7	4	13.6	18.4	15.3	15.6	13.7	13.0	13.8	13.5	87	62	78	76	2.0	8.9	4.0	5.0	7.5	7.6	6.8	7.3
VIII	1008.2	1017.4	993.5	1015.4	21.1	10.4	28.5	6, 22	6.4	29	12.3	19.3	15.5	15.6	13.4	13.3	13.8	13.5	92	59	78	76	1.1	9.7	4.1	5.0	5.7	7.0	4.8	5.8
IX	1006.0	1027.6	992.5	1013.2	19.6	9.7	26.1	2	4.8	21	10.7	17.9	13.9	14.1	12.0	13.3	13.0	12.7	93	65	82	80	1.0	8.0	3.0	4.0	6.3	6.9	4.4	5.9
X	1015.8	1030.5	1001.2	1023.3	13.1	3.6	22.7	1	−2.7	23	4.5	11.6	7.6	7.8	8.3	9.7	9.6	9.2	96	70	89	85	0.4	4.4	1.1	2.0	5.4	6.1	4.2	5.2
XI	1003.5	1025.1	972.1	1011.0	2.4	−2.8	12.6	1	−15.4	23	−1.2	1.0	−0.5	−0.3	5.4	5.8	5.6	5.6	90	83	88	87	0.6	1.2	0.8	0.9	8.1	8.1	7.6	7.9
XII	996.0	1018.5	967.3	1003.5	3.6	−1.1	12.1	19	−7.0	14	0.6	2.0	1.3	1.3	5.9	6.1	6.2	6.1	91	85	91	89	0.6	1.1	0.6	0.8	8.9	8.6	8.2	8.6
Rok	1006.0	1030.5	967.3	1013.4	11.5	3.5	32.2	14.VII	−19.3	8. III	5.0	9.8	7.2	7.3	8.7	9.0	9.1	8.9	90	71	83	81	1.0	4.9	2.3	2.7	7.0	7.6	6.1	6.9

Pułtusk $\varphi = 52°42'$ $\lambda = 21°06'$

I	—	—	—	—	1.0	−4.1	4.3	9	−17.8	11	−2.4	−0.5	−1.5	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.2	7.6	8.1
II	—	—	—	—	−1.9	−9.3	2.8	14	−23.6	6	−7.0	−3.4	−5.6	−5.4	—	—	—	—	—	—	—	—	—	—	—	—	8.2	6.8	6.4	7.1
III	—	—	—	—	4.8	−4.3	12.5	30	−21.3	9	−3.1	3.5	−0.2	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.8	5.9	6.7
IV	—	—	—	—	10.9	2.5	15.4	28	−2.6	3	4.0	8.9	6.1	6.3	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.8	6.4	7.3
V	—	—	—	—	14.6	5.2	20.8	18	−2.2	4	8.1	13.0	9.4	10.0	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.5	5.9	6.7
VI	—	—	—	—	21.7	11.2	31.0	26	6.1	8	14.6	20.0	15.6	16.4	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.9	5.4	5.9
VII	—	—	—	—	22.2	11.0	31.0	16	5.4	11	14.5	20.4	15.6	16.5	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.4	5.6	6.3
VIII	—	—	—	—	22.1	10.6	30.5	7	6.0	16	12.9	19.9	14.8	15.6	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.5	5.5	5.9
IX	—	—	—	—	21.3	9.2	29.0	3	2.5	21	10.8	19.8	13.2	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.4	3.1	4.6
X	—	—	—	—	12.4	3.0	20.9	1	−5.4	22	4.5	11.3	6.1	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.9	5.4	6.5
XI	—	—	—	—	0.9	−4.0	11.3	2	−19.8	24	−2.2	−0.3	−1.5	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	9.8	8.9	8.9	9.2
XII	—	—	—	—	1.9	−2.5	9.5	19, 20	−17.3	17	−0.8	0.7	−0.3	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	9.0	9.1	8.2	8.8
Rok	—	—	—	—	11.0	2.4	31.0	26.VI, 16.VII	−23.6	6. II	4.5	9.4	6.0	6.5	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.4	6.2	6.9

Inowrocław $H_s = 90 m$ $h_w = 15 m$ 1965

MIESIĄC	ROZKŁAD WIATRU (D, V_D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6.5	2.3	8	1.9	9	2.3	19.5	3.1	9	4.1	15.5	5.2	13.5	3.1	12	2.7	·	3.2	29	7.1	25	·	6	26	·	2	·	2	18	16	7	·	3	12	·
II	11.5	3.8	10.5	3.5	6	2.1	5	1.8	1.5	2.3	18	4.5	18.5	3.8	13	3.1	·	3.5	32	7.2	8	10	19	27	·	2	·	·	16	16	9	·	1	28	·
III	3.5	4.3	14.5	2.9	9	2.3	26	2.7	5.5	2.5	14	3.2	11.5	3.5	9	2.3	·	2.9	44	18.8	3	5	8	20	·	1	·	1	13	12	7	2	3	19	·
IV	5	3.8	12.5	3.0	22.5	3.8	27.5	3.5	2.5	5.4	7.5	2.5	8	2.7	4.5	2.0	·	3.3	40	17.4	28	·	·	6	·	2	·	2	14	10	6	1	1	·	1
V	7.5	3.8	21.5	2.7	21	3.3	10.5	4.5	1.5	1.3	10	3.1	10	3.8	9	2.4	2	3.2	77	17.4	19	·	·	2	·	1	·	4	14	14	12	2	1	·	1
VI	8	2.8	7.5	2.7	15.5	3.2	12	3.5	6	3.5	16.5	3.3	13.5	3.0	11	2.6	·	3.1	37	10.2	30	·	·	·	5	·	·	3	7	13	10	1	·	·	3
VII	3.5	2.9	5.5	3.3	7	3.5	9.5	2.2	8	2.8	39	3.9	17	3.7	1.5	2.7	2	3.4	48	9.9	31	·	·	·	4	·	·	2	11	14	12	·	·	·	8
VIII	9.5	2.0	6	1.6	5.5	1.5	13.5	2.8	6.5	3.4	16.5	1.8	17.5	1.7	13	1.8	5	1.9	51	17.0	25	·	·	·	9	·	·	4	7	11	9	2	1	·	3
IX	1	1.5	·	·	5	2.9	32	2.8	10	3.2	17.5	3.1	16.5	2.4	7	2.0	1	2.7	63	22.3	10	·	·	·	2	·	·	5	7	11	9	2	2	·	2
X	5.5	1.4	7.5	1.3	17.5	2.0	14	1.7	7.5	2.3	15	3.1	15	2.5	11	2.3	·	2.2	12	7.9	16	·	·	6	·	·	·	7	7	5	3	·	10	·	·
XI	3	1.8	18	2.9	12	3.3	18.5	3.4	4	3.9	20.5	4.3	10.5	4.0	3.5	2.0	·	3.5	40	14.4	21	6	11	19	·	1	·	2	13	10	8	1	4	15	·
XII	1	3.0	4.5	1.4	2.5	1.8	20	3.0	12	4.8	34	4.4	14.5	3.3	4.5	1.7	·	3.6	35	10.7	18	2	4	21	·	1	·	·	18	14	8	1	5	11	·
Rok	65.5	2.8	116	2.3	132.5	2.7	208	2.9	74	3.3	224	3.5	165	3.1	99	2.3	10	3.0	508	22.3	10.IX	23	48	127	20	10	·	32	151	146	100	12	31	86	18

Bielsk Podlaski $H_s = 145 m$ $h_w = 12,5 m$

I	4.5	1.6	7.5	2.3	9.5	4.9	19	5.6	16	4.1	16	4.2	10.5	3.6	8	5.8	2	3.8	37	8.1	20	5	14	29	·	3	·	·	20	16	10	·	7	18	·
II	11	3.4	11	4.0	1	2.0	·	·	3.5	2.4	22	5.3	17.5	3.3	11	3.1	7	3.6	40	9.2	7	12	22	27	·	2	1	1	12	21	11	·	4	27	·
III	4	1.1	2.5	2.0	1	5.0	16	3.1	20	2.3	24	2.2	14	3.7	1.5	3.7	10	2.4	22	6.8	19	5	7	22	·	·	·	2	14	11	6	·	5	16	·
IV	4	2.2	8.5	2.8	23.5	3.4	20.5	5.4	14	3.8	7.5	3.1	1	2.0	8	2.8	3	3.6	40	10.6	27	·	·	10	·	3	1	1	11	14	10	1	1	·	2
V	13	2.2	4.5	1.8	11.5	2.4	4	3.0	6	2.3	12	3.4	13.5	2.2	21.5	2.8	7	2.4	121	58.2	29	·	·	3	·	1	1	·	12	18	13	2	2	·	2
VI	10	3.2	9	2.6	5.5	2.6	5.5	3.2	3.5	1.9	13	3.9	24.5	2.8	13	2.2	6	2.7	55	17.8	13	·	·	·	5	·	·	2	9	14	10	1	·	·	4
VII	1.5	1.3	4.5	4.4	3	2.7	2	4.0	14.5	3.0	24.5	3.3	26	3.4	3	2.7	14	2.8	48	8.9	23	·	·	·	7	·	·	2	8	13	11	·	1	·	4
VIII	4.5	2.9	·	·	3	2.0	4.5	4.1	6	3.3	15.5	2.6	35	1.8	13.5	2.8	11	2.1	61	38.5	2	·	·	·	9	·	·	1	7	10	5	2	1	·	2
IX	1.5	1.7	·	·	5	3.2	11	3.6	15.5	2.5	30	3.2	22.5	2.6	1.5	1.7	3	2.8	37	14.5	13	·	·	·	6	1	1	3	6	9	5	1	1	·	3
X	3.5	2.4	2.5	2.6	1.5	2.3	0.5	3.0	6	2.8	18	2.6	33.5	3.0	19.5	1.9	8	2.4	9	4.2	16	·	·	6	·	·	·	1	12	10	2	·	10	·	·
XI	5	1.8	11	3.2	4	3.9	10.5	4.5	8	3.9	18	4.7	19	3.6	5.5	2.3	9	3.4	59	16.8	1	5	14	23	·	1	·	1	21	19	12	1	8	16	·
XII	2	1.5	0.5	1.0	1.5	1.7	9	3.2	20.5	4.1	35.5	4.0	16.5	2.6	2.5	1.4	4	3.4	40	6.1	5	2	7	24	·	3	1	·	21	21	10	·	1	10	·
Rok	64.5	2.1	61.5	2.2	70	3.0	102.5	3.4	133.5	3.0	237	3.5	233.5	2.9	108.5	2.8	84	3.0	569	58.2	29.V	29	64	144	27	14	5	14	153	176	105	8	41	87	17

Gorzów Wlkp. $H_s = 65 m$ $H_b = 59,7 m$ $h_w = 12 m$

I	11.5	2.3	4.5	2.1	10	2.2	17	2.6	11	2.7	11	3.5	19.5	3.9	7.5	3.3	1	2.9	33	5.5	17	·	1	23	·	·	·	·	18	17	9	·	7	9	1
II	22	4.3	11	4.0	7.5	3.5	7	4.2	2	2.8	2.5	3.2	12.5	3.9	19.5	3.4	·	3.8	32	9.3	26	3	13	26	·	2	1	1	14	21	9	·	4	28	·
III	8	3.9	6.5	4.4	13.5	3.4	18	2.2	11	2.7	6	1.9	9	2.2	20	3.2	1	2.9	32	8.7	3	5	7	22	·	1	·	6	11	14	8	·	6	21	·
IV	18	3.0	7	3.5	10	3.8	21	4.2	9.5	3.8	6.5	3.9	7.5	4.9	8.5	2.6	2	3.6	53	12.0	28	·	·	4	·	1	·	2	18	19	11	2	2	·	2
V	21	3.3	11	3.7	10	5.2	6	4.1	3	4.7	2.5	4.6	14	3.8	24.5	2.9	1	3.6	91	19.5	9	·	·	1	·	1	·	3	14	21	12	4	1	·	1
VI	15.5	3.4	15	3.2	10.5	3.3	2	6.5	·	·	6	3.8	21.5	3.7	19.5	2.8	·	3.4	53	13.0	1	·	·	·	4	·	·	1	8	13	10	2	·	·	4
VII	5	2.3	5.5	3.8	11.5	2.3	4.5	3.8	5	3.0	2.5	3.2	38	4.0	18	3.2	3	3.3	113	16.1	21	·	·	·	3	1	·	·	11	24	15	5	2	·	4
VIII	23	2.6	5	1.3	5	1.6	5.5	3.3	1	2.5	3	3.2	25.5	2.1	22	2.1	3	2.2	39	18.7	23	·	·	·	5	·	·	2	6	16	7	1	1	·	·
IX	4.5	1.9	4	2.1	8.5	4.2	13.5	3.9	2.5	2.6	7	3.4	32.5	2.3	16.5	2.2	1	2.7	53	16.2	10	·	·	·	2	·	·	5	8	13	10	2	3	·	1
X	17.5	2.2	9.5	1.6	24	2.4	6.5	2.7	1	2.0	1	2.0	20.5	2.6	10	2.2	3	2.2	17	9.1	16	·	·	5	·	·	·	4	2	4	3	·	10	·	·
XI	5.5	3.4	5	2.7	29.5	3.7	4.5	4.4	4.5	6.2	1	4.5	28.5	4.3	7.5	2.3	4	3.7	35	8.9	27	5	11	18	·	1	·	·	16	15	8	·	4	13	·
XII	4	2.9	1	3.0	7	3.9	11.5	3.6	2.5	3.0	19	4.3	35.5	4.2	12.5	2.6	·	3.8	75	13.9	18	·	3	22	·	3	1	·	22	23	16	3	3	17	·
Rok	155.5	3.0	85	[illegible]	147	3.3	117	3.8	53	3.0	68	3.5	264.5	3.5	186	2.7	19	3.2	626	19.5	9.V	13	35	121	14	10	2	24	148	200	118	19	43	88	13

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Pułtusk $H_s = 80 m$ $h_w = 12 m$

I	1.5	4.0	13.5	2.8	11.5	2.8	9.5	3.7	9.5	4.4	10	4.7	5	7.0	11.5	6.1	21	3.3	44	8.0	30	2	8	29	·	3	1	·	20	14	12	·	2	30	·
II	13.5	5.6	10	5.0	1.5	2.0	1	1.0	1	4.5	9.5	7.5	22.5	5.4	13	5.6	12	4.6	30	6.6	13	10	21	26	·	5	1	·	13	16	10	·	3	28	·
III	3.5	3.1	4	2.8	5.5	3.6	6	2.0	2	6.8	7	6.5	9	4.2	22	3.9	34	2.5	20	5.6	3	4	6	22	·	5	·	2	14	10	7	·	4	19	·
IV	6.5	4.5	8.5	5.4	11	8.2	19	5.6	5.5	5.2	9.5	4.3	2.5	4.2	12.5	4.1	15	4.5	45	13.3	28	·	·	8	·	5	1	1	10	13	6	2	1	·	1
V	9	3.3	7	3.3	8	4.6	8	4.6	1.5	4.0	9.5	6.3	7.5	3.8	15.5	4.0	27	3.0	69	29.8	19	·	·	2	·	4	1	2	13	13	10	1	1	·	2
VI	8.5	7.2	10	4.7	7	4.4	4.5	3.9	4.5	5.1	13	5.2	22.5	4.4	9	4.8	11	4.3	84	33.5	13	·	·	·	5	5	1	1	9	12	9	3	·	·	4
VII	2.5	6.2	3	5.5	2.5	4.2	5	4.5	6.5	4.2	29.5	4.2	23.5	4.9	1.5	3.3	19	3.6	61	9.1	17	·	·	·	7	5	1	2	10	17	14	·	1	·	6
VIII	2	3.8	2	3.8	·	·	7.5	4.7	8.5	4.0	1.5	6.3	16.5	3.2	26	5.0	29	3.0	106	39.7	26	·	·	·	10	2	·	·	8	11	9	4	·	·	3
IX	·	·	·	·	0.5	4.0	10.5	5.3	13	4.1	15	3.7	19.5	3.6	3.5	2.6	25	2.8	64	40.0	29	·	·	·	7	1	·	7	4	9	8	2	·	·	3
X	11	3.5	0.5	3.0	3.5	2.3	2.5	3.6	1	1.0	3	3.3	15	4.3	24.5	3.3	32	2.3	6	4.9	16	·	·	5	·	·	·	2	9	4	1	·	8	·	·
XI	5	4.2	9.5	3.8	11.5	2.2	7.5	5.7	8.5	5.8	8	6.8	19	4.8	3	4.0	18	3.7	57	13.2	21	5	12	20	·	3	1	·	26	17	11	2	6	16	·
XII	·	·	·	·	·	·	11.5	4.7	13	5.5	30	4.8	19	3.6	2.5	5.0	17	3.8	62	13.8	18	2	5	24	·	2	·	·	23	21	11	1	[illegible]	16	·
Rok	63	3.8	68	3.3	62.5	3.2	92.5	4.1	74.5	4.6	145.5	5.3	181.5	4.5	144.5	4.3	263	3.5	648	40.0	29.IX	23	52	136	29	40	7	17	159	157	108	15	[illegible]	109	21

Białowieża

$\varphi = 52°42'$ $\lambda = 23°51'$ **1965**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	992.8	1009.7	975.5	1013.6	-0.8	-6.1	2.7	9	-20.2	11	-4.0	-2.0	-3.6	-3.3	4.4	4.5	4.4	4.4	92	83	89	88	0.4	0.8	0.5	0.6	8.6	8.5	8.4	8.5
II	993.4	1014.2	971.7	1014.5	-3.7	-11.1	1.9	14	-26.6	7	-8.7	-5.1	-7.4	-7.2	3.2	3.5	3.3	3.3	91	80	87	86	0.3	0.8	0.4	0.5	8.4	8.5	7.7	8.2
III	997.4	1014.2	970.7	1018.2	3.4	-5.4	11.6	30	-24.1	9	-4.0	2.5	-1.4	-1.1	4.7	5.3	5.2	5.1	93	71	89	84	0.4	2.3	0.6	1.1	7.8	6.9	5.8	6.8
IV	993.5	1006.8	974.0	1013.7	9.9	1.3	16.9	26	-6.2	3	3.0	8.7	4.5	5.2	6.4	6.4	6.6	6.5	83	57	76	72	1.4	5.2	2.1	2.9	7.2	6.7	5.9	6.6
V	994.3	1010.4	978.5	1014.2	14.0	3.8	23.8	19	-5.2	4	7.3	12.5	8.5	9.2	8.8	8.9	8.7	8.8	83	60	76	73	1.7	6.0	2.7	3.5	5.6	7.4	5.9	6.3
VI	994.6	1001.5	984.4	1014.0	20.0	10.0	27.6	26	1.5	8	13.9	18.3	14.4	15.2	13.3	13.5	13.4	13.4	84	65	82	77	2.8	8.1	3.2	4.7	5.9	6.9	5.9	6.2
VII	992.9	1004.4	980.2	1012.2	21.4	9.7	28.8	16	4.1	5	14.4	19.7	15.1	16.1	13.8	13.4	13.5	13.6	83	59	79	74	2.8	10.0	3.9	5.6	4.0	6.8	4.3	5.0
VIII	995.6	1004.1	982.7	1015.0	20.9	9.3	28.7	7	4.9	30	12.6	19.6	13.9	15.0	13.3	13.6	13.9	13.6	90	60	87	79	1.6	9.9	2.4	4.6	5.5	5.5	4.4	5.1
IX	997.0	1013.2	985.8	1016.5	20.7	8.2	27.9	4	2.3	17	10.2	19.4	12.3	13.8	11.8	13.1	13.1	12.7	93	58	88	80	0.9	10.0	1.9	4.3	4.4	4.6	3.9	4.3
X	1002.0	1018.2	987.7	1022.2	10.9	1.9	20.1	1	-7.8	21	3.7	9.7	6.0	6.4	7.5	8.9	8.3	8.2	93	73	88	85	0.6	3.5	1.2	1.8	8.6	7.1	5.8	7.2
XI	992.8	1008.7	967.8	1013.4	0.1	-4.9	11.0	2	-19.5	17	-3.0	-0.9	-2.6	-2.3	4.9	5.1	4.9	5.0	91	83	90	88	0.5	1.2	0.6	0.8	9.8	9.3	7.8	9.0
XII	986.8	1001.4	967.4	1007.3	0.9	-3.6	7.9	20	-14.5	17	-1.5	0.1	-0.9	-0.9	5.1	5.4	5.3	5.3	91	86	90	89	0.5	0.9	0.6	0.7	8.5	8.1	7.9	8.2
Rok	994.4	1018.2	967.4	1014.5	9.8	1.1	28.8	16.VII	-26.6	7.II	3.6	8.5	4.9	5.5	8.1	8.5	8.4	8.3	89	70	85	81	1.2	4.9	1.7	2.6	7.0	7.2	6.1	6.8

Łagiewniki

$\varphi = 52°40'$ $\lambda = 18°19'$

I	—	—	—	—	1.4	-2.5	5.5	1	-9.2	11	-1.2	0.6	-0.8	-0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.2	7.1	7.0
II	—	—	—	—	-1.7	—	2.2	14	—	—	-6.2	-3.1	-5.6	-5.1	—	—	—	—	—	—	—	—	—	—	—	—	7.1	5.8	6.9	6.6
III	—	—	—	—	4.3	-5.5	11.4	29, 30	-26.0	8	-3.5	2.9	-1.3	-0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.3	4.6	6.5	5.8
IV	—	—	—	—	10.4	2.4	17.5	4	-1.3	5	4.6	9.0	5.8	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.4	6.5	6.1
V	—	—	—	—	14.2	5.1	21.4	17	-1.3	3	8.8	12.8	9.1	10.0	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.4	6.2	6.0
VI	—	—	—	—	21.5	10.3	31.3	26	5.2	3	14.8	20.0	14.8	16.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.1	11.6	31.1	14	5.9	5	14.8	19.7	14.8	16.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	21.4	10.4	29.6	22	5.5	13	13.6	20.1	14.4	15.6	—	—	—	—	—	—	—	—	—	—	—	—	5.0	4.7	5.6	5.1
IX	—	—	—	—	20.3	9.7	28.9	3	3.0	16	11.6	19.3	13.5	14.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.4	3.0	21.0	1	-4.2	22	4.8	11.3	6.3	7.2	—	—	—	—	—	—	—	—	—	—	—	—	5.1	4.8	5.0	5.0
XI	—	—	—	—	1.3	—	12.0	2	—	—	-2.6	0.0	-1.7	-1.5	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.7	7.5	7.2
XII	—	—	—	—	2.3	-2.1	10.8	19	-17.0	17	-0.3	1.1	0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.1	7.4	7.4
Rok	—	—	—	—	10.7	—	31.3	26.VI	—	—	4.9	9.5	5.8	6.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Wieniec-Zdrój

$\varphi = 52°40'$ $\lambda = 19°00'$

I	—	—	—	—	1.6	-2.8	7.5	9	-11.1	11	-0.9	0.8	-0.8	-0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.4	6.5	7.3
II	—	—	—	—	-1.5	-9.5	2.2	13	-21.4	6	-6.7	-2.4	-5.7	-5.1	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.7	7.0	7.8
III	—	—	—	—	5.1	-5.0	12.2	30	-22.8	8	-3.1	4.0	-0.7	-0.1	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.0	5.8	6.6
IV	—	—	—	—	10.4	1.7	16.0	30	-3.6	3	4.2	9.0	5.0	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	8.2	5.6	7.1
V	—	—	—	—	14.2	4.3	21.7	17	-3.5	3	8.4	12.9	8.6	9.6	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.5	6.7	7.1
VI	—	—	—	—	22.3	10.4	31.5	26	4.7	16	14.8	20.8	15.2	16.5	—	—	—	—	—	—	—	—	—	—	—	—	4.7	7.1	5.8	5.9
VII	—	—	—	—	22.3	11.1	31.2	14, 15	4.7	2	15.1	20.1	14.6	16.1	—	—	—	—	—	—	—	—	—	—	—	—	5.6	7.8	5.8	6.4
VIII	—	—	—	—	22.0	9.8	30.2	23	3.9	31	13.3	20.5	14.6	15.8	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.8	4.4	6.1
IX	—	—	—	—	20.9	8.7	29.5	3	1.2	16	11.7	19.4	12.8	14.2	—	—	—	—	—	—	—	—	—	—	—	—	6.0	5.9	3.9	5.3
X	—	—	—	—	12.5	2.7	21.9	1	-5.7	22	4.6	11.6	5.9	7.0	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.3	3.7	5.6
XI	—	—	—	—	1.3	-4.7	11.6	2	-20.7	24	-2.8	0.5	-1.9	-1.5	—	—	—	—	—	—	—	—	—	—	—	—	9.7	8.6	8.2	8.8
XII	—	—	—	—	2.5	-2.1	10.4	19	-18.7	17	-0.5	1.3	0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.7	9.2	9.0
Rok	—	—	—	—	11.1	2.0	31.5	26.VI	-22.8	8.III	4.8	9.9	5.6	6.5	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.5	6.0	6.9

Nur

$\varphi = 52°40'$ $\lambda = 22°19'$

I	—	—	—	—	0.2	-5.2	4.0	8	-19.6	11	-3.2	-1.3	-2.5	-2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.0	7.1	7.9
II	—	—	—	—	-2.7	-10.3	3.0	14	-22.7	6	-7.4	-4.1	-6.6	-6.2	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.1	6.4	7.0
III	—	—	—	—	4.1	-4.4	12.6	30	-20.0	9	-2.7	2.9	-0.7	-0.3	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.0	5.5	6.0
IV	—	—	—	—	10.5	2.4	16.3	26	-2.4	3	3.9	9.1	5.6	6.0	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.5	6.4	6.9
V	—	—	—	—	14.2	5.0	21.2	18	-2.5	4	8.0	13.1	9.0	9.8	—	—	—	—	—	—	—	—	—	—	—	—	5.7	7.2	6.2	6.4
VI	—	—	—	—	20.6	11.3	28.7	26	4.3	8	14.4	19.5	15.0	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.2	6.0	5.8
VII	—	—	—	—	21.5	11.0	29.1	15	5.5	5	14.9	20.2	15.3	16.4	—	—	—	—	—	—	—	—	—	—	—	—	3.7	6.6	5.2	5.2
VIII	—	—	—	—	20.7	10.7	29.1	7	6.9	17,18,31	13.1	19.4	14.4	15.3	—	—	—	—	—	—	—	—	—	—	—	—	5.6	5.6	4.6	5.3
IX	—	—	—	—	21.1	9.2	27.6	3	3.0	21	11.0	20.3	13.2	14.4	—	—	—	—	—	—	—	—	—	—	—	—	4.9	4.6	2.6	4.0
X	—	—	—	—	11.7	2.7	20.2	1	-5.7	21	4.3	10.8	6.3	6.9	—	—	—	—	—	—	—	—	—	—	—	—	8.4	6.9	4.0	6.4
XI	—	—	—	—	0.5	-4.4	10.7	2	-17.5	17	-2.1	-0.6	-1.9	-1.6	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.4	8.3	8.6
XII	—	—	—	—	1.4	-2.7	8.7	20	-17.5	17	-1.1	0.4	-0.4	-0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.8	8.1	8.4
Rok	—	—	—	—	10.3	2.1	29.1	15.VII,7.VIII	-22.7	6.II	4.4	9.1	5.6	6.2	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.9	5.3	6.5

Białowieża

$H_s = 163\,m$ $H_b = 163{,}7\,m$ $h_w = 10{,}7\,m$ **1965**

MIESIĄC	ROZKŁAD WIATRU n=D, V=D N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V ≥10	V ≥15	◔	●	Opad R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	K (K)
I	6	5.2	4.5	1.8	5.5	3.9	25.5	3.5	14	3.8	13.5	4.0	2.5	5.2	8.5	8.5	13	3.7	48	11.2	20	5	14	29	·	10	·?	2	22	13	10	1	5	31	·
II	8	4.1	12.5	4.9	5.5	4.0	0.5	3.0	3.5	3.0	16.5	5.5	16	4.6	16.5	4.6	6	4.3	33	6.0	7	12	23	26	·	9	1	1	19	18	10	·	1	28	·
III	3.5	7.6	6.5	1.8	4	2.0	15.5	2.1	16.5	2.2	16.5	2.4	10.5	3.0	11	4.6	9	2.5	27	6.0	17	5	8	26	·	2	1	7	16	14	8	·	7	26	·
IV	6.5	5.9	2	2.2	19	8.9	31.5	5.6	11	5.0	5	3.3	0.5	5.0	4.5	3.6	10	5.3	28	8.7	23	·	·	13	·	11	3?	3	9	11	8	·	·	1	2
V	13	4.3	13.5	2.6	12.5	5.3	10.5	3.2	4.5	1.3	9.5	2.5	5	4.4	9.5	4.1	15	3.0	50	10.9	29	·	·	5	·	4	1?	5	11	16	10	1	2	·	4
VI	8	2.8	5	2.8	10.5	5.4	7	6.3	5	4.2	8.5	5.2	15	4.3	16	4.0	15	3.7	77	18.2	13	·	·	·	2	6	3?	3	9	15	13	2	1	·	4
VII	2	1.2	4	4.1	4.5	4.2	6	2.1	10	4.0	23	4.2	17	4.8	7.5	2.3	19	3.1	48	12.0	23	·	·	·	4	1?	·	3	5	14	10	1	3	·	4
VIII	11.5	4.0	1.5	7.0	4	3.0	10	3.0	8	4.2	9	3.7	10.5	3.1	19.5	3.3	19	2.8	56	29.3	2	·	·	·	9	2	1	7	6	10	8	1	2	·	5
IX	1	2.5	1.5	3.3	1	5.0	18	3.8	14.5	4.1	13	3.9	14	3.3	12	3.4	15	3.1	28	6.7	11	·	·	·	3	3?	1?	8	2	8	8	·	2	·	2
X	11.5	3.9	3	3.0	2.5	4.0	4.5	4.2	9.5	3.1	10	2.8	12.5	4.1	19.5	4.1	20	2.9	10	3.7	11	·	·	6	·	·	·	1	14	10	3	·	6?	·	·
XI	1.5	1.0	4.5	5.4	11.5	4.2	21.5	3.5	5.5	4.0	12.5	4.2	17	4.8	10	3.6	6	3.8	50	14.6	1	4	14	23	·	5?	1?	·	22	21	14	1	4	18	·
XII	5.5	1.5	2	2.0	0.5	3.0	14	3.1	13	3.5	32	3.9	14	4.1	7	4.1	5	3.4	38	8.6	5	3	11	27	·	4?	2?	1	20	18	9	·	2	29	·
Rok	78	3.7	60.5	3.4	81	4.4	164.5	3.6	115	3.5	168	3.8	134.5	4.2	141.5	4.2	152	3.5	493	29.3	2.VIII	29	70	157	18	57?	14?	41	155	168	111	7	35?	133	21

Łagiewniki

$H_s = 80\,m$ $h_w = 10\,m$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	29	5.0	25	·	7	27	·	—	—	·	10	16	11	·	5	—	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	26	5.2	26	—	22	—	·	—	—	1	5	15	10	·	·	—	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	42	16.3	3	7	10	20	·	—	—	1	4	14	11	1	6	—	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	38	13.2	28	·	·	7	·	—	—	·	6	10	10	1	1	—	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	94	18.2	19	·	·	4	·	—	—	1	7	16	14	4	·	—	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	25?	5.2	22	·	·	·	6	—	—	—	—	10	8	·	·	—	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	50	14.6	31	·	·	·	4	—	—	—	—	12	11	1	·	—	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	66	25.8	24	·	·	·	8	—	—	3	4	8	6	3	1	—	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	62	23.4	10	·	·	·	1	—	—	—	—	7	6	3	2	—	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	11	5.8	16	·	·	6	·	—	—	2	1	13	2	·	11	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40	12.6	22	—	12	—	·	—	—	·	9	16	6	1	6	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	23	10.0	18	2	3	22	·	—	—	·	10	11	5	1	6	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	506?	25.8	24.VIII	—	54	—	19	—	—	—	—	148	102	15	38	—	—

Wieniec - Zdrój

$H_s = 82\,m$ $h_w = 14\,m$

I	·	·	·	·	·	·	7	1.1	7	1.1	7	1.4	10	1.7	17	1.4	45	0.7	28	5.9	30	1	6	28	·	·	·	5	19	8	8	·	—	11	—
II	5	1.6	7	1.9	3	1.7	7	2.1	3	1.0	13	1.8	15	1.8	5	2.4	26	1.3	38	7.8	26	12	20	26	·	·	·	1	18	14	11	·	—	28	—
III	3	1.7	10	2.2	4	2.2	13	2.1	7	2.4	6	4.7	16	2.7	5	3.2	29	1.8	43	16.2	3	7	9	24	·	·	·	4	14	14	10	1	—	20?	—
IV	3	3.3	8	2.9	22	2.6	14	2.9	3	1.7	4	2.0	6	2.2	10	2.0	20	2.0	21?	3.2	19	·	·	9	·	·	·	1	14	14	8	·	—	·	—
V	2	2.5	12	2.1	17	1.9	4	2.5	·	·	3	2.7	14	2.6	14	1.9	27	1.5	86	21.4	19	·	·	5	·	·	·	4	16	14	13	3	—	·	—
VI	10	1.5	1	3.0	12	2.3	6	2.3	6	2.5	6	1.8	10	2.5	11	2.0	28	1.5	38	11.2	19	·	·	·	7	·	·	2	8	9	9	1	—	·	—
VII	2	1.5	4	1.8	4	2.5	6	1.8	4	3.0	31	2.0	7	3.3	2	1.0	33	1.4	60	12.1	31	·	·	·	8	·	·	1	10	15	13	1	—	·	—
VIII	1	1.0	·	·	·	·	5	2.6	3	2.7	12	2.2	12	1.5	15	1.5	45	0.9	43	8.9	24	·	·	·	8	·	·	1	8	13	10	·	—	·	—
IX	·	·	·	·	1	1.0	10	2.1	4	2.8	13	2.2	8	1.8	7	2.0	47	1.0	76	35.8	4	·	·	·	2	·	·	7	6	9	8	2	—	·	—
X	4	1.2	·	·	6	1.5	4	2.0	·	·	8	1.6	15	1.9	9	1.7	47	0.8	26	13.1	3	·	·	8	·	·	·	4	7	5	4	1	—	·	—
XI	2	1.5	8	1.8	12	2.8	5	2.2	2	2.5	12	3.2	17	2.2	5	1.8	27	1.7	37	13.8	21	7	11	20	·	·	·	·	24	10	9	1	—	16	—
XII	·	·	·	·	·	·	10	1.7	10	2.7	24	2.9	18	2.3	8	1.2	23	1.8	48	13.6	18	2	4	20	·	·	·	·	23	10	8	1	—	16	—
Rok	32	1.3	50	1.3	81	1.5	91	2.1	49	1.9	139	2.4	148	2.2	108	1.8	397	1.4	544?	35.8	4.IX	29	50	140	25	·	·	30	167	135	111	11	—	91	—

Nur

$H_s = 110\,m$ $h_w = 13\,m$

I	2.5	2.0	4.5	2.8	10	1.7	19	1.9	12	1.8	10	3.3	4.5	5.8	7.5	3.6	23	1.9	40	5.4	29	4	10	27	·	·	·	2	19	14	10	·	4	31	·
II	14.5	5.8	5	5.6	4.5	2.6	·	·	5.5	2.8	22.5	3.8	6	2.7	14	5.0	12	3.7	34	6.0	7	11	22	26	·	5	2	2	14	15	13	·	2	28	·
III	3	9.7	6	1.7	2.5	1.6	18	1.7	11.5	1.5	7	3.2	7	2.0	7	1.7	31	1.5	22	6.0	17	6	7	24	·	1	·	8	14	13	8	·	4	19	·
IV	3	5.8	5.5	4.1	31.5	3.7	19.5	2.4	7	1.8	3.5	1.3	2	3.0	8	4.7	10	2.9	35	8.3	23	·	·	6	·	5	1	3	15	11	9	·	·	·	2
V	16.5	3.5	14	3.2	12.5	2.3	10.5	1.9	5	2.2	8	2.0	5	1.8	9.5	3.9	12	2.4	90	34.2	29	·	·	1	·	3	·	5	13	13	12	2	1	·	3
VI	7	4.2	11.5	3.1	10	2.4	7	1.7	4	1.5	13.5	3.0	11	3.2	11	3.3	15	2.4	56	15.6	13	·	·	·	2	3	·	5	9	11	8	2	·	·	1
VII	3	1.3	6.5	3.0	4.5	1.6	7	1.1	11	1.8	32.5	2.8	6	2.8	1.5	1.0	21	1.8	80	25.2	17	·	·	·	5	1	·	5	6	17	14	1	·	·	2
VIII	9	2.2	1	3.0	·	·	12	1.8	3.5	2.1	4	2.0	11	2.1	24.5	2.8	28	1.6	54	17.6	2	·	·	·	9	1	·	6	7	10	7	2	·	·	2
IX	·	·	0.5	1.0	4.5	1.3	25	2.0	11.5	1.4	16.5	1.9	3	3.7	5	1.4	24	1.4	31	11.2	29	·	·	·	3	·	·	9	2	8	6	1	2	·	1
X	3.5	2.1	8	1.6	5	1.6	1	1.0	10	1.6	18.5	2.1	8	2.3	13	2.3	26	1.4	10	3.0	16	·	·	5	·	·	·	2	8	8	5	·	13	·	·
XI	·	·	12	2.7	8.5	1.4	11.5	1.9	7.5	2.6	18.5	2.9	5	1.2	2	2.0	25	1.7	59	11.3	1	6	13	19	·	·	·	·	21	20	13	1	5	18	·
XII	1	1.0	·	·	3	1.0	14	1.7	26	2.2	25.5	2.0	8.5	1.1	1	1.0	14	1.6	56	11.8	18	2	6	23	·	1	·	·	8	19	12	1	·	16	·
Rok	63	3.1	74.5	2.6	96.5	1.8	144.5	1.6	114.5	1.9	180	2.5	77	2.6	104	2.7	241	2.0	567	34.2	29.V	29	58	131	19	20	3	47	136	159	117	10	31	112	11

Poświętne — φ = 52°38' — λ = 20°23' — 1965

MIESIĄC	CIŚNIENIE p: P_m	Max	Min	$P_{o.m}$	TEMPERATURA T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	–	–	–	–	0.8	-3.8	4.8	18	-16.6	11	-1.9	-0.2	-1.5	-1.3	4.9	5.2	5.1	5.1	90	85	91	89	0.6	1.0	0.5	0.7	8.3	7.3	6.5	7.4
II	–	–	–	–	-2.3	-10.2	1.9	13, 14	-23.0	6	-7.0	-3.9	-6.1	-5.8	3.4	3.9	3.6	3.6	88	82	88	86	0.4	0.8	0.5	0.6	7.7	6.9	5.7	6.8
III	–	–	–	–	4.1	-4.8	11.6	30	-21.5	8	-3.3	2.7	-0.4	-0.4	4.8	5.6	5.4	5.3	91	73	86	83	0.5	2.2	0.9	1.2	5.8	6.2	4.9	5.6
IV	–	–	–	–	9.9	1.8	15.2	30	-2.7	3	3.6	8.3	5.5	5.7	7.1	7.8	7.6	7.5	88	71	83	81	1.0	3.3	1.5	1.9	6.5	7.7	5.0	6.4
V	–	–	–	–	14.0	4.5	20.4	17	-2.8	3	8.1	12.4	9.1	9.7	9.2	9.2	9.5	9.3	83	63	80	75	1.8	5.5	2.2	3.2	6.2	7.6	5.9	6.6
VI	–	–	–	–	21.0	10.3	29.4	26	5.5	4	14.3	19.3	14.9	15.8	13.5	13.5	13.8	13.6	82	61	81	75	3.0	9.4	3.4	5.3	4.6	5.4	4.9	5.0
VII	–	–	–	–	21.3	10.1	29.5	16	4.1	5	14.8	19.7	14.9	16.1	14.4	14.3	14.9	14.5	84	61	86	77	2.7	9.4	2.4	4.3	4.7	6.5	4.8	5.3
VIII	–	–	–	–	21.1	10.3	29.7	6, 7	4.9	31	13.2	19.4	14.3	15.3	13.8	14.2	14.3	14.1	90	65	87	81	1.7	9.2	2.4	4.1	5.0	5.6	4.3	5.0
IX	–	–	–	–	20.2	9.3	26.7	3	2.0	21	11.4	18.8	13.2	14.2	12.9	13.8	13.6	13.4	94	64	89	82	0.9	8.4	1.8	3.7	5.0	5.1	2.2	4.1
X	–	–	–	–	11.9	2.8	19.7	1	-5.5	22	4.5	10.7	6.5	7.0	8.1	9.8	9.1	9.0	94	75	92	87	0.5	3.4	0.9	1.6	5.2	5.3	3.3	4.6
XI	–	–	–	–	0.6	-5.0	11.1	2	-23.7	24	-2.5	-0.5	-2.1	-1.8	5.1	5.4	5.2	5.2	90	85	91	89	0.5	1.0	0.6	0.7	9.0	7.9	8.4	8.4
XII	–	–	–	–	1.9	-2.8	9.5	19, 20	-19.9	17	-0.4	0.7	-0.1	0.0	5.5	5.6	5.5	5.5	89	84	87	87	0.7	1.1	0.8	0.9	8.8	7.9	7.9	8.2
Rok	–	–	–	–	10.4	1.9	29.7	6,7.VIII	-23.7	24.XI	4.6	9.0	5.7	6.2	8.6	9.0	9.0	8.9	89	72	87	83	1.2	4.6	1.5	2.4	6.4	6.6	5.3	6.1

Przebędowo — φ = 52°35' — λ = 17°01'

I	–	–	–	–	2.0	-2.5	5.6	1	-11.7	31	-0.8	1.0	-0.1	0.0	5.5	5.7	5.8	5.7	95	87	94	92	0.3	0.9	0.4	0.5	7.3	7.0	7.4	7.2
II	–	–	–	–	-1.0	-9.4	2.6	13	-19.5	6	-5.7	-2.1	-4.4	-4.2	3.8	4.2	4.2	4.1	91	79	92	87	0.4	1.1	0.3	0.6	7.9	6.4	5.9	6.7
III	–	–	–	–	5.2	-4.7	14.5	29	-24.5	9	-2.9	3.7	0.3	0.4	5.0	5.8	5.8	5.5	91	71	87	83	0.4	2.6	0.9	1.3	6.7	5.7	5.8	6.1
IV	–	–	–	–	11.1	2.6	16.0	6, 30	-2.2	5	4.1	9.7	6.8	6.8	7.6	7.5	7.9	7.7	91	63	80	78	0.7	4.7	2.0	2.5	6.4	7.1	6.0	6.5
V	–	–	–	–	14.6	5.5	21.2	17	-0.4	3	8.4	13.2	10.4	10.6	10.1	10.6	10.3	10.3	89	70	82	80	1.1	4.8	2.8	2.9	–	–	–	–
VI	–	–	–	–	21.7	10.5	31.2	26	4.7	3	14.7	19.8	16.2	16.7	14.4	14.1	15.0	14.5	86	62	82	77	2.6	9.7	3.6	5.3	–	–	–	–
VII	–	–	–	–	20.8	10.9	31.0	14	5.2	2	14.6	18.8	15.2	16.0	14.4	14.1	14.9	14.5	85	65	85	78	2.4	8.3	2.8	4.5	–	–	–	–
VIII	–	–	–	–	21.7	9.6	30.2	6	4.2	14	13.1	19.9	15.3	15.9	13.6	12.7	13.9	13.4	90	56	81	76	1.8	11.3	3.9	5.7	–	–	–	–
IX	–	–	–	–	20.6	9.5	28.0	3	3.2	21	11.6	19.2	13.9	14.6	12.3	12.1	13.4	12.6	90	56	84	77	1.6	10.7	2.8	5.0	4.4	4.2	4.1	4.2
X	–	–	–	–	13.0	2.5	23.0	1	-4.9	22	4.3	12.1	6.8	7.5	8.3	9.7	9.3	9.1	97	69	93	86	0.3	4.8	0.9	2.0	6.0	4.5	4.4	5.0
XI	–	–	–	–	1.8	-3.5	12.2	2	-17.9	24	-1.8	0.7	-0.9	-0.7	5.4	5.9	5.6	5.6	94	85	91	90	0.4	1.1	0.6	0.7	8.5	7.6	7.1	7.7
XII	–	–	–	–	3.0	-1.3	11.8	19	-8.8	17	0.3	1.8	0.9	1.0	5.9	6.1	6.1	6.0	93	86	93	91	0.5	1.0	0.5	0.7	9.0	7.0	6.2	7.4
Rok	–	–	–	–	11.2	2.5	31.2	26.VI	-24.5	9. III	5.0	9.8	6.7	7.0	8.9	9.0	9.4	9.1	91	71	87	83	1.0	5.1	1.8	2.6	–	–	–	–

Wyszków — φ = 52°35' — λ = 21°27'

I	–	–	–	–	0.6	-4.7	4.1	18	-19.8	11	-2.6	-0.4	-1.7	-1.6	4.8	5.1	5.2	5.0	91	85	93	90	0.5	1.0	0.4	0.6	7.8	7.5	6.8	7.4
II	–	–	–	–	-2.2	-11.3	3.7	14	-22.3	6	-7.2	-3.2	-6.8	-6.0	3.5	3.9	3.6	3.7	90	78	90	86	0.4	1.1	0.3	0.6	7.7	6.6	6.0	6.8
III	–	–	–	–	5.0	-5.1	13.4	30	-18.7	9	-2.7	3.9	-0.7	0.0	5.0	5.6	5.3	5.3	90	68	88	82	0.5	2.8	0.8	1.4	6.9	6.4	5.3	6.2
IV	–	–	–	–	11.0	2.1	15.7	30	-3.0	3	4.5	10.1	5.8	6.6	7.2	7.4	7.5	7.4	83	60	80	74	1.4	5.2	1.9	2.8	7.5	7.5	6.3	7.1
V	–	–	–	–	14.7	4.5	22.2	18	-3.1	4	8.9	13.5	9.0	10.1	9.4	9.4	9.4	9.4	80	60	80	73	2.2	6.3	2.3	3.5	6.2	6.5	5.9	6.2
VI	–	–	–	–	21.3	10.5	31.6	26	5.5	8	14.9	19.7	14.4	15.8	14.0	13.9	14.2	14.0	82	62	86	77	3.2	9.7	2.4	5.1	4.4	6.0	5.2	5.2
VII	–	–	–	–	21.8	10.9	30.4	16	5.8	11	15.1	20.4	14.9	16.3	14.7	13.9	14.8	14.4	85	58	86	76	2.6	10.7	2.5	5.3	3.7	5.4	4.4	4.5
VIII	–	–	–	–	21.1	10.3	29.6	7	5.3	16	13.3	19.6	14.0	15.2	13.9	14.1	14.2	14.0	90	50	88	76	1.7	9.7	2.3	4.6	4.5	5.9	3.6	4.7
IX	–	–	–	–	20.7	8.6	27.2	3	2.3	21	11.1	19.4	12.9	14.1	12.6	14.1	13.6	13.4	95	63	91	83	0.8	9.0	1.6	3.8	3.7	3.6	1.7	3.0
X	–	–	–	–	12.1	2.5	21.0	1	-5.0	22	4.3	11.0	6.2	6.9	8.1	9.8	9.1	9.0	95	73	92	87	0.4	3.6	0.7	1.6	7.1	6.2	5.1	6.1
XI	–	–	–	–	0.4	-4.4	12.1	2	-17.5	24	-2.2	-0.5	-2.0	-1.7	5.1	5.4	5.3	5.3	91	86	91	89	0.5	0.9	0.5	0.6	9.2	8.2	8.4	8.6
XII	–	–	–	–	1.7	-3.0	9.0	20	-21.6	17	-1.0	0.6	-0.4	-0.3	5.4	5.7	5.6	5.6	92	87	92	90	0.5	0.9	0.5	0.6	8.8	8.2	8.2	8.4
Rok	–	–	–	–	10.7	1.7	31.6	26.VI	-22.3	6. II	4.7	9.5	5.5	6.3	8.6	9.0	9.0	8.9	89	69	88	82	1.2	5.1	1.4	2.6	6.5	6.5	5.6	6.2

Gorzyń — φ = 52°34' — λ = 15°54'

I	–	–	–	–	2.7	-1.3	8.1	17	-7.4	31	0.0	1.9	0.4	0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	7.4	7.7
II	–	–	–	–	-0.2	-6.0	3.9	13	-16.0	6	-4.2	-1.3	-2.8	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	7.5	7.4
III	–	–	–	–	5.5	-3.4	13.5	29	-21.6	8	-2.2	4.6	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.7	4.9	5.5
IV	–	–	–	–	11.4	3.2	16.4	6	-1.7	5	4.7	10.1	6.5	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.2	6.0	6.6
V	–	–	–	–	15.3	6.2	22.5	17	-0.6	3	9.2	14.2	9.8	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	6.2	6.5
VI	–	–	–	–	21.7	11.5	30.5	26	6.3	3	14.7	20.0	15.8	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.0	5.1	5.9
VII	–	–	–	–	20.7	11.8	32.1	14	6.3	2	14.6	18.8	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.3	6.4	6.8
VIII	–	–	–	–	21.5	10.8	29.8	6	6.1	2	13.6	20.0	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.8	3.4	4.6
IX	–	–	–	–	20.0	10.4	27.0	3	5.2	21	11.8	18.7	13.6	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.8	4.1	5.0
X	–	–	–	–	13.0	3.6	22.5	1	-4.9	23	5.0	12.0	7.3	7.9	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.5	2.9	4.4
XI	–	–	–	–	2.1	-2.3	12.7	1	-12.0	23	-0.9	1.4	-0.3	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.3	6.9	7.5
XII	–	–	–	–	3.5	-0.7	13.0	19	-7.7	13	0.8	2.3	1.6	1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.0	7.2	7.7
Rok	–	–	–	–	11.4	3.6	32.1	14.VII	-21.6	8. III	5.6	10.2	6.9	7.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.9	5.7	6.3

Poświętne

$H_s = 101$ m $h_w = 14$ m **1965**

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temperatura Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V ≥ 10	V > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K
I	6.5	1.8	1.5	5.3	20	2.2	14	2.6	7	5.7	21.5	4.0	10	4.7	10.5	5.1	2	3.5	31	6.8	30	3	9	27	·	·	·	1	17	14	8	·	7	19	·
II	14	5.3	10	5.1	1.5	9.3	1	1.0	1	3.0	18.5	4.9	22	5.6	13	4.6	3	5.0	15	3.5	13	12	22	27	·	6	1	·	10	17	6	·	3	28	·
III	4	6.8	14.5	1.9	5	1.8	11.5	2.6	9.5	3.1	13	4.4	24	2.7	4.5	5.8	7	2.9	18	5.1	4	8	8	20	·	3	·	7	12	14	7	·	7	18	·
IV	7.5	5.6	10	3.9	25.5	4.8	24	3.5	1.5	3.3	6.5	2.6	6	2.5	8	3.4	1	3.9	48	10.0	23	·	:	10	·	6	·	1	6	13	11	1	2	·	·
V	17.5	3.4	9.5	2.6	15.5	4.6	6.5	2.9	4	3.6	7	3.8	13	3.7	13	2.8	7	3.2	65	18.5	19	·	·	3	·	2	·	3	14	17	12	1	2	·	2
VI	9	4.0	12	4.8	9	3.5	4	2.4	4.5	4.0	10	3.6	23.5	3.6	10	3.4	8	3.4	35	10.4	13	·	·	·	4	2	·	4	7	13	10	1	·	·	5
VII	0.5	2.0	8.5	3.9	8.5	2.4	2	1.8	7	2.6	27	3.2	28.5	3.3	2	1.5	9	2.8	92	24.8	21	·	·	·	6	·	·	3	6	17	14	3	·	·	7
VIII	6	2.8	1	1.0	1.5	2.0	6	2.3	8.5	2.9	14	2.2	27.5	2.5	13.5	2.8	15	2.1	76	31.3	26	·	·	·	9	·	·	7	8	11	9	2	·	·	5
IX	·	·	·	·	9.5	1.9	11.5	2.7	19.5	2.8	16	2.1	15	3.7	2.5	1.8	16	2.2	62	26.6	4	·	·	·	2	1	·	9	3	13	7	2	·	·	2
X	7	1.8	4.5	1.9	7	2.1	5.5	1.2	4.5	1.4	13	2.6	24.5	3.3	16	2.1	11	2.1	9	5.1	16	·	·	5	·	·	·	7	5	7	2	·	14	·	·
XI	·	·	19.5	3.4	13	3.3	7.5	4.6	10.5	3.7	11.5	3.5	24	4.5	3	4.8	1	3.8	36	8.7	21	7	14	21	·	1	·	1	20	15	8	·	5	16	·
XII	1.5	1.0	1	2.0	1	2.0	12	3.3	15.5	4.1	34.5	4.6	16.5	3.7	10	2.1	1	3.7	41	14.8	18	2	6	23	·	4	·	·	17	19	10	1	3	13	·
Rok	73.5	2.9	92	3.0	117	3.3	105.5	2.6	93	3.4	192.5	3.5	234.5	3.6	106	3.4	81	3.2	528	31.3	26.VIII	32	59	136	21	25	1	43	125	170	104	11	43	94	21

Przebędowo

$H_s = 82$ m $h_w = 11$ m

I	6	5.0	8.5	2.5	9	1.7	15.5	2.6	14	4.1	17.5	5.1	7.5	4.8	10	4.0	5	3.5	38	8.9	17	1	3	27	·	1	·	1	16	16	8	·	5	20	·
II	17	4.9	6.5	4.1	5	4.4	2.5	5.4	6	4.7	23	5.4	16	6.4	5	5.4	3	5.1	12	3.2	14	13	18	28	·	4	·	3	12	12	6	·	3	28	·
III	18	3.6	·	·	2.5	2.6	4.5	3.2	21	3.1	11	4.5	17	5.8	5	5.8	14	3.5	24	7.8	3	6	8	22	·	1	1	6	14	10	8	·	7	18	·
IV	16	3.6	11.5	3.3	20.5	3.1	8	4.0	5	4.2	12	3.4	9.5	5.2	6.5	3.9	1	3.7	40	14.0	28	·	·	5	·	·	·	4	13	12	9	1	·	·	·
V	11	3.5	15	2.6	13	3.5	7	4.4	7	2.1	9	4.1	17.5	3.6	11.5	2.6	2	3.2	108	16.5	9	·	·	2	·	2	·	—	—	16	15	5	2	·	1
VI	13	3.3	11	2.9	4	3.5	8	4.4	4	3.5	14	4.6	13.5	3.9	8.5	2.6	14	3.1	41	22.1	17	·	·	·	4	·	·	—	—	6	5	1	·	·	1
VII	8	3.4	2.5	1.6	5.5	2.5	5	2.8	20	4.2	27	4.3	11	4.4	3	3.7	11	3.4	76	15.4	21	·	·	·	3	1	1	—	—	17	15	1	·	·	7
VIII	1	2.0	1	1.0	6	1.5	5	3.6	12	2.3	14	2.9	20	3.2	10	3.1	24	2.1	34	8.5	25	·	·	·	7	·	·	—	—	17	11	·	2	·	3
IX	·	·	1.5	1.3	9.5	2.5	11.5	2.8	22.5	3.3	18.5	3.9	12.5	5.0	2	3.0	12	3.0	43	14.0	10	·	·	·	3	2	·	7	3	7	7	2	1	·	·
X	10	1.5	6	1.9	6	1.4	5	2.0	12	3.2	13	4.2	17	3.0	7	2.0	17	2.2	12	8.6	16	·	·	9	·	·	·	7	9	3	3	·	11	·	·
XI	7	5.7	18	3.7	4.5	4.8	4	4.6	11.5	5.6	21.5	7.1	10	4.6	4.5	3.6	9	4.7	42	11.7	27	5	12	18	·	4	·	·	17	15	11	1	6	15	·
XII	1	3.0	1	1.0	5	2.4	12	4.9	22	5.8	34.5	6.8	7.5	3.6	2	4.5	8	5.1	56	13.9	18	·	3	20	·	7	·	1	14	17	10	1	1	9	·
Rok	108	3.3	82.5	2.2	90.5	2.8	88	3.7	157	3.8	215	4.7	159	4.5	75	3.7	120	3.6	526	22.1	17.VI	25	44	131	17	22	2	—	—	148	108	12	38	90	12

Wyszków

$H_s = 96$ m $h_w = 13$ m

I	3	2.0	10	2.1	15	2.3	7	2.1	12.5	1.6	9	2.1	8.5	4.9	3	3.7	25	1.8	37	7.0	20	3	9	28	·	·	·	2	18	17	11	·	2	21	·
II	11	3.3	11	3.9	·	·	·	·	4	3.0	15.5	2.8	25	3.6	16.5	4.5	1	3.5	38	6.9	7	15	22	28	·	·	·	2	13	19	10	·	1	28	·
III	4	2.2	9	1.8	10	2.2	8.5	2.3	16.5	2.0	7	1.9	14.5	1.9	10.5	4.6	13	2.0	16	3.2	3	7	6	25	·	·	·	6	14	10	6	·	4	17	·
IV	5	4.6	14	3.4	22	3.5	18	4.3	·	·	10	2.8	2	2.5	7	3.4	12	3.1	28	10.5	27	·	·	9	·	·	·	2	14	13	9	1	1	·	·
V	5.5	2.1	14	4.3	10	3.1	1.5	4.0	1.5	3.3	13	2.5	12	3.1	17.5	3.2	18	2.6	57	22.1	19	·	·	3	·	·	·	5	13	14	10	1	1	·	2
VI	7	2.7	8.5	2.1	6.5	4.9	6	3.3	5.5	2.4	7.5	2.5	17	2.5	11	2.7	21	2.1	81	19.0	13	·	·	·	5	·	·	10	9	13	10	3	·	·	5
VII	·	·	7	1.1	3	2.7	5	3.0	12	1.4	22.5	2.6	18.5	3.2	2	1.5	23	1.8	93	36.6	17	·	·	·	5	·	·	10	4	15	12	2	·	·	6
VIII	2	1.0	1	3.0	5	2.6	8.5	3.0	7.5	1.4	6.5	2.2	16.5	2.4	22	2.5	24	1.8	113	35.9	26	·	·	·	10	·	·	10	7	11	9	4	·	·	2
IX	·	·	1	1.0	9	2.0	10	2.2	8.5	1.6	12.5	2.2	20.5	2.3	2.5	2.4	26	1.5	45	30.2	29	·	·	·	4	·	·	12	·	10	6	1	·	·	1
X	7	1.1	3	1.7	5	1.4	2	1.5	11	1.2	11	2.2	12	2.4	17	2.3	25	1.4	9	3.2	16	·	·	6	·	·	·	3	9	9	4	·	11	·	1
XI	5	2.8	16	2.9	10	3.0	11	2.9	10	1.8	10	3.6	18	2.4	4	2.5	6	2.6	48	10.1	21	6	16	21	·	·	·	1	23	17	11	1	4	16	·
XII	2	2.0	·	·	4	2.8	13.5	2.7	15	1.8	24.5	2.3	10	2.4	10	2.5	14	2.0	64	10.9	18	2	7	28	·	·	·	·	21	19	15	1	·	10	·
Rok	51.5	2.0	94.5	2.3	99.5	2.5	91	2.6	104	1.8	149	2.5	174.5	2.8	123	3.0	208	2.2	629	36.6	17.VII	33	60	148	24	·	·	63	145	167	113	14	24	92	17

Gorzyń

$H_s = 60$ m $h_w = 15$ m

I	4	1.4	3.5	3.0	6	2.2	10	2.5	14.5	3.8	21.5	3.4	16	3.0	7.5	2.5	10	2.7	36	7.2	17	·	1	24	·	·	·	·	15	15	8	·	4	8	·
II	10	4.5	8	3.6	3.5	3.7	3	3.0	5	3.1	10	3.3	22	4.3	19.5	4.5	3	3.9	22	4.0	25, 26	5	15	26	·	3	·	1	12	18	10	·	·	28	·
III	6	3.4	6.5	3.5	4.5	2.1	7.5	2.7	14	2.8	12	2.6	13	2.5	14.5	2.6	15	2.3	39	16.1	3	5	7	21	·	·	·	7	12	12	9	1	3	18	·
IV	5.5	2.1	4.5	2.9	11	4.1	18.5	4.0	12.5	3.2	4	2.6	11.5	2.7	13.5	2.9	9	2.9	45	9.7	19	·	·	2	·	·	·	3	14	15	10	·	·	·	3
V	11.5	1.9	6.5	1.8	14	3.2	17	3.3	6	3.3	2	2.5	10.5	3.6	16.5	3.2	9	2.7	75	15.0	9	·	·	1	·	2	·	3	11	18	13	3	·	·	1
VI	7	2.1	4.5	2.7	10.5	2.6	8.5	3.2	5	4.4	5.5	4.2	15	3.5	22	3.0	12	2.7	51	12.9	8	·	·	·	4	·	·	2	8	11	8	2	·	·	4
VII	3	1.5	4	2.8	4	2.8	3.5	2.4	5.5	2.0	18.5	2.8	33	3.0	12.5	2.9	9	2.5	124	25.2	21	·	·	·	4	1	·	1	10	23	17	3	·	·	5
VIII	11.5	2.3	3	1.5	·	·	5.5	2.5	9.5	2.9	9	3.2	20	2.3	19.5	2.2	15	2.0	30	13.7	23	·	·	·	9	·	·	4	3	10	8	1	2	·	1
IX	1.5	2.7	0.5	2.0	1.5	5.3	8	5.2	12	2.9	20.5	3.1	23	2.3	13	2.0	10	2.6	51	19.0	3	·	·	·	2	1	·	4	2	10	8	2	1	·	2
X	·	·	3	1.3	6	2.0	8	1.9	4	3.0	14.5	2.2	26.5	2.1	4	1.8	27	1.5	23	16.5	16	·	·	6	·	·	·	8	1	4	3	1	7	·	·
XI	1.5	2.0	13.5	2.7	11.5	3.8	4	6.2	12	4.5	15.5	5.0	17.5	3.2	3.5	2.9	11	3.4	44	11.2	27	4	12	16	·	1	·	1	13	19	9	2	5	11	·
XII	·	·	1.5	2.7	3	2.3	10.5	3.6	20	4.4	33	4.2	18	3.7	2	2.5	5	3.7	59	12.0	18	·	4	19	·	2	·	·	15	25	15	1	·	8	
Rok	61.5	2.0	59	2.5	79.5	2.8	104	3.4	120	3.4	166	3.3	226	3.0	148	2.8	135	2.7	599	25.2	21.VII	14	39	115	19	10	·	34	116	180	118	16	22	73	16

Trzemeszno — φ = 52°34' — λ = 17°49' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.8	-2.5	5.6	1	-8.1	11	-1.0	1.1	-0.5	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	7.6	8.0
II	–	–	–	–	-1.2	-9.4	2.6	13	-22.0	6	-5.9	-2.5	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.9	7.4	7.5
III	–	–	–	–	5.2	-4.4	13.1	29	-23.3	9	-2.5	4.1	-0.3	0.2	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.0	5.8	6.1
IV	–	–	–	–	10.9	2.8	15.7	6	-2.1	5	4.9	9.9	5.9	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	4.6	6.9
V	–	–	–	–	14.4	5.8	21.3	17	-0.2	2, 3	9.1	13.1	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.9	7.5	7.4
VI	–	–	–	–	21.6	10.7	31.7	26	6.0	3	15.3	20.0	15.0	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.9	6.1	6.6
VII	–	–	–	–	21.3	11.6	30.8	14	6.2	2	15.2	19.3	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	7.3	7.4
VIII	–	–	–	–	21.6	10.6	29.0	6, 22	6.0	14, 17	14.6	19.9	14.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	7.2	5.3	5.9
IX	–	–	–	–	20.4	9.9	28.1	3	3.9	16	11.9	19.1	13.5	14.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.2	4.1	5.2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Gniezno — φ = 52°33' — λ = 17°36'

I	–	–	–	–	1.8	-2.6	5.8	1	-9.1	11	-1.1	0.9	-0.5	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	7.2	7.6
II	–	–	–	–	-1.0	-8.7	2.8	13	-21.0	6	-6.0	-2.5	-4.8	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	7.1	7.5
III	–	–	–	–	5.0	-4.3	13.7	29	-22.3	9	-2.9	3.7	-0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.7	4.9	5.7
IV	–	–	–	–	10.9	2.5	15.7	30	-1.5	5	4.2	9.4	5.9	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.4	4.7	6.4
V	–	–	–	–	14.5	5.7	21.5	17	-1.2	3	8.2	12.9	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	7.0	7.1
VI	–	–	–	–	21.5	10.7	31.8	26	6.3	3	14.2	20.1	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	7.0	5.5	5.8
VII	–	–	–	–	21.0	11.5	30.9	14	6.9	2	14.1	19.1	14.9	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	7.4	6.9
VIII	–	–	–	–	21.2	10.4	29.1	6	5.9	13	13.0	19.9	14.1	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.1	4.0	5.1
IX	–	–	–	–	20.5	9.8	27.7	3	4.4	16	11.5	19.0	13.2	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.0	3.8	5.0
X	–	–	–	–	12.6	3.3	21.8	1	-4.1	22	4.8	11.6	6.3	7.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.1	2.5	4.8
XI	–	–	–	–	1.6	-3.6	11.8	1	-15.5	17	-2.3	0.4	-1.1	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.6	8.0	8.3
XII	–	–	–	–	2.7	-1.5	11.3	19	-10.7	17	-0.1	1.5	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.4	7.5	8.3
Rok	–	–	–	–	11.0	2.8	31.8	26.VI	-22.3	9.III	4.8	9.7	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	5.8	6.5

Krzemień — φ = 52°33' — λ = 22°30'

I	–	–	–	–	0.2	-4.8	3.7	9	-19.2	11	-2.9	-1.1	-2.3	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-2.9	-11.0	2.1	13	-22.7	6, 10	-7.4	-4.3	-7.0	-6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.7	-4.4	13.0	30	-19.8	9	-2.7	2.8	-1.7	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.3	2.5	16.3	26	-2.2	3	4.0	8.8	5.2	5.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.0	4.4	21.8	18	-3.3	4	8.2	12.8	8.9	9.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.6	11.0	28.1	26	4.2	8	14.4	19.2	15.1	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	10.8	29.2	16	5.1	5	15.8	20.0	15.7	16.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.9	10.3	28.8	7	5.7	16	14.0	19.3	14.4	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.2	8.9	27.2	3	1.6	21	11.9	20.4	14.4	15.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	11.8	1.9	20.0	1	-6.5	21	4.6	11.0	6.1	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	0.6	-4.1	11.5	2	-18.1	17	-2.0	-0.8	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1.3	-2.9	9.6	19	-16.7	17	-1.1	0.3	-0.7	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.3	1.9	29.2	16.VI	-22.7	6.10.II	4.7	9.0	5.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Płock - Radziwie — φ = 52°32' — λ = 19°40'

I	1003.7	1020.2	984.8	1011.8	1.5	-2.9	5.5	18	-11.9	11	-1.2	0.7	-0.9	-0.6	5.2	5.6	5.3	5.4	91	86	91	89	0.5	1.0	0.5	0.7	8.4	8.2	7.2	7.9
II	1007.5	1026.1	982.7	1015.7	-1.7	-8.7	2.4	13	-20.5	6	-6.3	-3.0	-5.0	-4.8	3.5	4.1	3.8	3.8	87	81	86	85	0.5	0.9	0.6	0.7	8.2	7.6	7.1	7.6
III	1008.6	1024.9	979.7	1016.7	4.8	-3.9	12.9	30	-19.5	8	-2.6	3.4	0.2	0.3	5.1	5.9	5.6	5.5	92	74	86	84	0.4	2.2	0.9	1.2	6.9	7.2	5.5	6.5
IV	1003.4	1022.8	987.6	1011.3	10.4	2.7	15.4	30	-2.0	3	4.0	8.8	6.2	6.3	7.3	7.6	7.7	7.5	88	67	80	78	1.0	4.0	1.9	2.3	7.2	8.3	6.8	7.4
V	1006.0	1022.1	989.1	1013.8	14.3	5.6	21.7	17	-0.3	3	8.2	12.8	10.1	10.3	9.5	9.7	9.9	9.7	85	65	79	76	1.6	5.4	2.7	3.2	6.9	7.7	6.3	7.0
VI	1006.0	1015.0	995.6	1013.7	21.8	11.5	31.5	26	6.6	4	14.4	20.4	16.2	16.8	13.4	13.3	14.2	13.6	81	57	76	71	3.2	11.3	4.5	6.3	5.5	7.1	6.5	6.4
VII	1003.7	1014.6	988.8	1011.3	22.3	11.5	30.5	14, 15	5.7	5	14.9	20.3	15.7	16.7	14.4	14.1	14.9	14.5	84	58	82	75	2.8	10.5	3.3	5.5	6.8	8.2	5.9	7.0
VIII	1007.5	1015.0	996.7	1015.2	21.6	11.1	30.6	7	5.8	31	13.2	20.0	15.3	16.0	13.9	14.3	14.9	14.4	91	62	85	79	1.6	10.1	2.9	4.9	6.0	6.8	5.5	6.1
IX	1007.0	1026.4	994.7	1014.7	21.0	9.9	28.3	3	4.0	16	11.6	19.5	13.7	14.6	12.9	13.9	13.8	13.5	94	62	88	81	1.0	9.2	2.1	4.1	5.7	6.1	3.4	5.1
X	1015.0	1030.4	1000.5	1023.0	12.5	3.4	21.8	1	-4.4	22	4.6	11.4	6.9	7.4	8.3	9.9	9.4	9.2	96	72	93	87	0.4	4.0	0.8	1.7	7.5	6.8	3.8	6.0
XI	1004.1	1022.3	976.4	1012.2	1.3	-4.0	12.3	2	-20.2	24	-2.4	0.1	-1.2	-1.2	5.1	5.6	5.5	5.4	90	86	90	89	0.5	1.0	0.6	0.7	9.0	8.7	8.2	8.6
XII	997.5	1015.9	973.6	1005.6	2.7	-1.8	10.7	19	-17.5	17	0.0	1.6	0.4	0.6	5.6	5.9	5.8	5.8	89	85	89	88	0.7	1.1	0.8	0.9	8.3	8.5	8.4	8.4
Rok	1005.8	1030.4	973.6	1013.7	11.0	2.9	31.5	26.VI	-20.5	6.11	4.9	9.7	6.5	6.9	8.7	9.2	9.2	9.0	89	71	85	82	1.2	5.1	1.8	2.7	7.2	7.6	6.2	7.0

Trzemeszno — $H_s = 105\,m$ — $h_w = 15{,}4\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%, V=m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0,1	R≥1,0	R≥10,0	≡	⊠	K (K)
I	5.5	1.4	6.5	1.6	16	4.3	9	2.1	14.5	3.1	14	2.8	17	2.2	10.5	2.5	·	2.2	34	4.7	27, 30	·	6	28	·	1	·	·	19	16	11	·	4	13	·
II	7	2.0	12	2.0	5	1.4	3.5	1.0	2.5	1.4	10	4.2	25	3.3	19	3.6	·	2.9	17	5.4	26	12	20	27	·	·	·	1	16	15	5	·	2	28	·
III	5	1.7	16.5	1.8	6.5	1.3	10.5	1.9	14	1.2	7	1.5	23	3.5	10.5	2.3	·	2.1	37	17.0	3	7	9	21	·	1	·	4	13	13	6	1	7	19	·
IV	5	1.3	23.5	1.8	25	2.2	12	2.4	3	2.5	4	1.8	9.5	2.7	8	2.8	·	2.2	—	—	—	·	·	5	·	·	·	2	13	—	—	—	1	·	1
V	7.5	1.7	22	1.8	19	2.4	5.5	3.9	1.5	1.3	8	1.9	14	2.8	15.5	1.8	·	2.2	79	15.0	19	·	·	3	·	·	·	1	15	17	14	1	2	·	·
VI	3.5	1.3	12.5	2.1	15	1.8	2.5	3.2	10.5	2.0	9.5	1.8	22.5	2.6	14	2.6	·	2.2	59	18.9	1	·	·	·	5	·	·	·	8	12	8	2	·	·	4
VII	0.5	7.0	9.5	1.9	6.5	1.5	3	1.3	10.5	1.7	24	2.4	32.5	2.9	6.5	1.5	·	2.3	54	13.7	31	·	·	·	5	·	·	2	14	15	12	1	·	·	5
VIII	6.5	1.0	4	1.0	2	1.0	11.5	1.3	7.5	2.5	8.5	2.0	25	1.6	26	1.5	2	1.5	41	13.4	25	·	·	·	7	·	·	3	11	14	6	1	1	·	3
IX	1.5	1.7	0.5	1.0	8.5	1.5	16	1.7	11	1.3	15	2.3	27	1.6	9.5	1.7	1	1.7	43	19.4	6	·	·	·	3	·	·	6	6	8	7	2	9	·	1
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Gniezno — $H_s = 110\,m$ — $h_w = 10\,m$

I	8	1.9	10.5	2.0	12	1.7	4	1.6	7	3.6	20	3.0	14	2.5	10.5	1.6	7	2.2	36	5.0	25	·	5	27	·	1	1	1	17	16	14	·	9	16	·
II	8.5	3.2	11.5	4.8	3	1.8	0.5	1.0	0.5	1.0	13.5	4.2	22.5	2.1	17	2.5	7	3.3	24	6.2	26	10	17	27	·	5	·	1	15	17	8	·	4	28	·
III	4	1.2	15.5	3.3	6	1.5	5	1.9	9	1.6	9	3.8	16	3.4	12.5	2.2	16	2.2	36	16.8	3	6	9	22	·	3	·	6	11	14	6	1	4	17	1
IV	3	2.3	29.5	4.1	10	4.3	10.5	2.6	2	1.0	7.5	3.9	10	1.4	10.5	2.6	7	3.0	39	18.7	28	·	·	7	·	5	·	3	11	13	7	1	4	·	1
V	2.1	1.9	26	3.4	6	6.1	5	2.8	0.5	1.0	5	2.3	10.5	3.7	11	2.5	8	2.8	94	14.4	26	·	·	3	·	5	2	2	15	19	14	3	10	·	2
VI	9	1.7	20	4.8	2.5	6.6	3	1.0	5.5	2.8	5.5	2.5	17	4.1	12.5	1.8	15	2.8	42	11.8	30	·	·	·	5	3	·	5	9	14	6	1	·	·	4
VII	3	1.3	11	4.1	2.5	3.0	0.5	6.0	3	1.7	17	2.7	32.5	2.2	9.5	2.0	14	2.2	87	17.9	15	·	·	·	3	4	·	1	12	19	13	3	1	·	4
VIII	17.5	1.4	1.5	1.3	2	2.0	2.5	1.0	4.5	2.4	4.5	2.4	19.5	1.9	17	1.6	24	1.3	57	23.4	4	·	·	·	7	·	·	6	5	16	6	2	2	·	5
IX	3	4.3	6	1.8	6	2.1	6.5	3.0	9	1.7	13	2.5	25.5	2.4	5	1.4	16	1.9	52	20.7	10	·	·	·	1	·	·	4	3	9	7	2	1	·	·
X	6	1.6	13	1.5	6	2.2	2	1.0	0.5	2.0	14.5	2.0	15.5	2.6	7.5	2.1	28	1.4	15	7.9	16	·	·	6	·	1	·	6	5	4	3	·	12	·	·
XI	6	1.4	19.5	5.2	6	6.0	3.5	3.6	7.5	2.6	12	4.0	17	4.2	3.5	1.9	15	3.4	41	9.8	21	6	11	17	·	6	·	1	19	18	9	·	7	16	·
XII	0.5	6.0	3.5	1.6	4	1.4	9.5	2.7	10.5	3.9	32	4.1	19	2.7	5	1.9	9	2.9	49	13.3	18	1	3	21	·	3	·	·	19	22	10	1	3	11	·
Rok	89.5	2.4	162.5	3.2	66	3.2	52.5	2.4	59.5	2.1	153.5	3.1	219	2.8	121.5	2.1	166	2.4	572	23.4	4.VIII	23	45	130	16	36	3	36	141	181	105	14	57	88	17

Krzemień — $H_s = 111\,m$ — $h_w = 10\,m$

I	3	5.7	4	4.2	7	4.5	24.5	3.7	15	3.4	7.5	4.9	7.5	4.3	5.5	5.5	19	3.3	17	3.6	8	3	10	28	·	·	·	—	—	14	6	·	2	22	—
II	8.5	5.4	13.5	6.6	2.5	2.0	1.5	2.0	5	4.0	13	5.0	16	4.4	9	4.2	15	4.0	16	5.7	7	13	22	27	·	2	·	—	—	12	7	·	2	27	—
III	1	12.0	6	3.5	3	2.5	28	2.3	6	3.2	9	4.5	9.5	3.3	5.5	4.3	25	2.4	21	5.3	17	4	7	22	·	2	·	—	—	13	7	·	3	16	—
IV	9.5	3.1	2	7.5	26	6.9	23.5	4.1	8	4.4	9	2.7	3	5.0	2	3.2	7	4.5	40	12.1	26	·	·	5	·	5	·	—	—	13	10	1	1	·	—
V	7	3.6	9	2.9	19	4.6	9	2.5	4	3.2	5	4.2	5.5	3.3	12.5	3.4	22	2.7	77	25.5	29	·	·	1	·	3	1	—	—	14	11	3	1	·	—
VI	5	1.8	8	4.2	10.5	5.5	9.5	2.9	2.5	5.2	7	3.4	12.5	3.6	8	2.4	27	2.3	59	16.7	13	·	·	·	4	·	·	—	—	12	9	1	·	·	—
VII	0.5	3.0	3.5	3.6	3	2.7	7.5	3.9	13.5	3.5	18	3.6	16	3.8	1	3.0	30	2.9	93	36.5	17	·	·	·	5	·	·	—	—	16	13	3	1	·	—
VIII	5.5	4.2	·	·	3	3.0	5.5	3.4	8.5	3.1	9	2.6	13	3.5	14.5	3.1	34	2.1	63	20.1	2	·	·	·	8	1	1	—	—	11	8	2	·	·	—
IX	1.5	2.0	·	·	2.5	4.8	25	3.2	8	2.9	14	3.5	8.5	3.3	4.5	2.2	26	2.3	27	12.5	29	·	·	·	2	·	·	—	—	9	6	1	2	·	—
X	3	2.3	4	3.5	3	3.3	2	4.2	6.5	2.8	7.5	3.1	16	3.7	12	3.0	39	1.9	6	3.1	16	·	·	6	·	·	·	—	—	6	2	·	8	·	—
XI	3.5	1.9	11.5	5.3	10	3.5	11	4.4	5.5	3.7	9	5.7	23	4.1	5.5	3.9	11	3.7	33	8.1	1	4	12	20	·	·	·	—	—	23	7	·	7	18	—
XII	·	·	2	1.5	1	2.0	15.5	3.5	10.5	3.5	36.5	4.4	17	2.9	1.5	2.5	9	3.3	36	8.2	18	2	6	23	·	·	·	—	—	19	8	·	1	15	—
Rok	48	3.8	63.5	3.6	90.5	3.8	162.5	3.3	93	3.6	144.5	4.0	147.5	3.8	81.5	3.4	264	2.9	487	36.5	17.VII	26	57	132	19	13	2	—	—	162	94	11	28	98	—

Płock-Radziwie — $H_s = 63\,m$ — $H_b = 63{,}8\,m$ — h_w = 14 m wiatromierz Wilda, 10,8 m anemometr

I	3.5	3.6	2.5	3.8	20.5	3.1	13	3.0	17	3.9	13	4.2	15.5	3.7	6	2.7	2	3.5	23	4.3	8	1	6	27	·	2	·	·	18	16	7	·	11	13	·
II	10	5.4	6	4.0	4	2.5	2	2.2	6.5	4.8	18.5	4.8	27	4.5	7	3.9	3	4.3	29	4.7	7	10	19	26	·	1	·	1	15	17	11	·	4	28	·
III	2	4.2	6.5	2.7	25	2.4	16.5	2.8	4.5	4.0	12	5.0	13.5	3.8	5	5.5	8	3.1	28	3.7	3	6	7	22	·	1	·	4	13	14	8	·	11	18	·
IV	3.5	3.9	11	4.8	29.5	4.5	14	3.6	5.5	2.9	5	2.9	10	3.5	7.5	4.3	4	3.9	54	17.4	28	·	·	4	·	·	·	1	14	13	12	1	3	·	·
V	4.5	3.7	8.5	3.2	20.5	3.7	7.5	3.9	3.5	2.3	12	4.1	12.5	2.6	17	3.1	7	3.1	94	22.7	19	·	·	2	·	1	·	1	13	17	13	2	7	·	2
VI	5	3.0	12	3.4	12.5	4.2	10	3.4	4	3.9	14	4.4	16	3.9	9.5	3.3	7	3.5	75	23.0	12	·	·	·	5	3	·	2	8	15	12	2	2	·	4
VII	2.5	4.0	7	3.1	14	2.4	7.5	1.5	6.5	3.3	29.5	3.9	18	4.5	3	3.2	5	3.3	80	18.9	16	·	·	·	5	2	·	2	8	16	14	2	1	·	10
VIII	6	1.6	1	2.0	5	2.6	11.5	3.2	10.5	2.5	9	3.1	16	2.8	9	3.0	25	2.0	76	18.6	23	·	·	·	9	·	·	4	9	14	12	3	2	·	3
IX	·	·	·	·	13	2.2	17	3.0	14	2.2	17.5	3.0	8.5	3.0	2	2.5	18	2.2	90	53.6	4	·	·	·	2	·	·	5	4	11	9	2	3	·	2
X	1	1.0	1	3.0	11	2.2	10	1.2	4.5	2.0	12	3.9	27.5	2.8	10	2.9	16	2.2	9	4.6	16	·	·	5	·	·	·	2	7	6	4	·	16	·	·
XI	2	1.5	10.5	3.3	18.5	3.4	14.5	4.2	4.5	3.4	16.5	4.8	12.5	3.9	3	2.7	8	3.5	37	8.3	21	7	12	17	·	1	·	1	22	14	9	·	10	16	·
XII	1.5	1.7	1.5	1.0	6.5	2.8	15.5	4.2	14.5	6.1	29	5.2	21	4.1	1.5	2.0	2	4.3	46	14.7	18	2	5	19	·	4	·	·	20	20	10	1	2	13	·
Rok	41.5	2.8	67.5	2.9	180	3.0	139	3.0	95.5	3.4	188	4.1	198	3.5	80.5	3.2	105	3.2	651	53.6	4.IX	26	49	122	21	15	·	23	151	175	121	13	72	68	21

Uwaga. W VIII-IX kierunki wiatru - wg wiatromierza Wilda, prędkości - wg anemometru M-47, w pozostałych miesiącach kierunki i prędkości - wg anemometru M-47.

Przybroda

$\varphi = 52°31'$ $\lambda = 16°40'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max obs.	Data	Min obs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.7	−2.1	5.7	1	−9.5	31	−0.6	1.0	−0.1	0.0	5.2	5.5	5.4	5.4	89	83	88	87	0.6	1.1	0.7	0.8	7.7	7.4	7.7	7.6
II	–	–	–	–	−0.8	−7.6	2.6	13	−17.9	6	−4.8	−1.7	−3.6	−3.4	3.7	3.9	4.0	3.9	83	72	81	79	0.7	1.5	0.8	1.0	7.1	6.9	6.9	7.0
III	–	–	–	–	4.9	−4.2	13.9	29	−23.9	8	−2.4	4.0	0.4	0.6	4.8	5.7	5.4	5.3	84	67	81	77	0.8	2.9	1.3	1.7	5.9	5.4	5.0	5.4
IV	–	–	–	–	11.0	2.9	16.0	6	−1.8	5	4.9	10.0	6.5	7.0	7.7	7.4	7.9	7.7	87	61	81	76	1.1	5.1	1.9	2.7	6.7	6.6	4.6	6.0
V	–	–	–	–	14.5	6.0	21.5	17	−0.5	3	9.1	13.5	9.8	10.6	9.8	9.6	9.5	9.6	83	62	78	74	2.0	6.1	2.8	3.6	6.5	6.5	6.2	6.4
VI	–	–	–	–	21.3	10.8	30.8	26	5.2	3	15.3	19.6	15.2	16.3	13.0	12.7	13.4	13.0	75	57	77	70	4.6	10.5	4.1	6.4	4.4	6.0	5.6	5.3
VII	–	–	–	–	20.4	11.2	30.2	14	5.7	5	14.8	18.9	14.5	15.7	13.9	13.6	14.1	13.9	81	63	84	76	3.2	8.8	2.7	4.9	6.5	6.2	6.2	6.3
VIII	–	–	–	–	21.6	10.3	30.0	6	5.7	13, 31	14.3	20.1	14.8	16.0	13.5	12.6	13.3	13.1	82	54	79	72	3.2	11.7	3.9	6.3	4.6	5.3	3.6	4.5
IX	–	–	–	–	20.1	9.8	27.9	3	4.5	21	12.1	18.7	13.5	14.4	12.6	12.6	13.1	12.8	88	59	85	77	2.0	9.5	2.7	4.7	5.1	5.2	3.1	4.5
X	–	–	–	–	13.0	3.0	22.2	1	−3.8	22	5.0	12.0	6.5	7.5	8.4	9.8	9.0	9.1	93	70	91	85	0.6	4.7	0.9	2.1	4.7	5.5	3.1	4.4
XI	–	–	–	–	1.6	−3.5	12.6	2	−16.1	23	−1.8	0.7	−1.1	−0.8	5.2	5.8	5.3	5.4	88	84	87	86	0.7	1.1	0.8	0.9	8.3	8.1	6.7	7.7
XII	–	–	–	–	3.0	−1.2	11.8	19	−8.0	17	0.3	1.7	0.9	1.0	5.7	5.9	6.0	5.9	90	85	91	89	0.7	1.1	0.7	0.8	8.6	7.8	7.4	7.9
Rok	–	–	–	–	11.0	3.0	30.8	26. VI	−23.9	8. III	5.5	9.9	6.4	7.0	8.6	8.8	8.9	8.8	85	68	84	79	1.7	5.3	1.9	3.0	6.3	6.4	5.5	6.1

Wieliszew

$\varphi = 52°27'$ $\lambda = 20°58'$

I	–	–	–	–	1.0	−3.5	4.5	18	−16.1	11	−1.9	−0.2	−1.4	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−1.7	−8.4	2.3	14	−22.9	6	−6.4	−3.8	−5.6	−5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	4.5	−3.3	12.8	30	−16.4	8	−1.4	3.5	0.2	0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.0	2.8	15.0	30	−2.4	3	4.6	8.9	6.1	6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.2	5.2	20.8	17	−1.0	4	9.1	12.7	9.8	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	21.2	11.4	30.4	26	6.4	4	15.2	19.5	15.7	16.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.6	11.3	29.4	15, 16	5.5	11	16.0	20.2	15.6	16.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.4	10.8	31.4	7	7.0	3, 16	14.4	19.9	15.1	16.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.9	9.6	27.9	3	2.0	21	11.7	19.5	13.8	14.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.0	2.9	19.4	1	−5.5	22	5.0	11.3	6.8	7.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.6	−3.8	12.0	2	−16.1	24	−1.5	0.1	−1.2	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.6	−2.5	10.1	19	−17.5	17	0.0	0.9	0.0	0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.8	2.7	31.4	7. VIII	−22.9	6. II	5.4	9.4	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sulęcin

$\varphi = 52°26'$ $\lambda = 15°07'$

I	–	–	–	–	3.0	−1.1	8.6	17	−7.9	7	0.1	2.3	0.6	0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.3	7.6	8.2
II	–	–	–	–	−0.1	−7.0	3.9	13	−19.5	28	−4.7	−1.0	−2.8	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.2	7.6	8.0
III	–	–	–	–	5.9	−5.0	14.5	29	−25.2	8	−3.0	5.0	−1.0	0.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.5	5.5	6.1
IV	–	–	–	–	11.9	2.3	17.4	6	−3.1	5	4.8	10.7	6.1	6.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.5	5.3	6.4
V	–	–	–	–	15.7	6.3	22.4	17	−1.8	22	9.7	14.5	10.3	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.3	6.4	6.6
VI	–	–	–	–	21.9	9.8	29.8	26	3.6	3	14.8	20.5	14.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.6	5.6	5.7
VII	–	–	–	–	20.6	10.8	32.1	14	3.6	2	14.5	19.1	14.3	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.7	6.4	7.0
VIII	–	–	–	–	21.4	8.3	30.0	6	3.0	29	13.1	20.2	13.3	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.5	6.1	3.9	4.8
IX	–	–	–	–	19.6	8.5	26.0	2	2.4	21	11.3	18.7	11.9	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.1	3.9	5.2
X	–	–	–	–	13.9	1.9	22.5	1	−5.4	23	4.0	13.0	6.1	7.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.2	3.5	4.8
XI	–	–	–	–	2.6	−2.7	13.4	1	−17.7	23	−1.0	1.6	−0.2	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.1	8.1	8.2
XII	–	–	–	–	3.9	−0.7	12.7	19	−8.7	14	0.9	2.7	1.6	1.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.3	8.2	8.4
Rok	–	–	–	–	11.7	2.6	32.1	14. VII	−25.2	8. III	5.4	10.6	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.2	6.0	6.6

Poznań - Sołacz

$\varphi = 52°26'$ $\lambda = 16°54'$

I	–	–	–	–	2.4	−1.5	6.1	1	−5.8	11	−0.2	1.8	0.4	0.6	5.3	5.9	5.6	5.6	86	84	87	86	0.8	1.1	0.8	0.9	–	–	–	–
II	–	–	–	–	−0.5	−6.7	2.9	13	−16.4	6	−4.7	−1.3	−3.1	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	5.9	−3.4	14.6	29	−21.0	9	−2.1	4.9	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	11.3	3.6	16.1	6, 30	−1.7	5	5.1	10.3	7.3	7.5	7.7	7.6	8.0	7.8	86	61	78	75	1.2	5.1	2.3	2.9	–	–	–	–
V	–	–	–	–	15.0	6.5	22.0	17	0.1	3	9.2	13.8	10.8	11.2	10.1	10.0	9.8	10.0	85	64	75	75	1.7	6.0	3.4	3.7	–	–	–	–
VI	–	–	–	–	21.9	11.5	31.1	26	6.4	3	15.4	20.8	16.4	17.2	13.6	13.3	14.2	13.7	77	55	76	69	4.1	11.8	4.8	6.9	–	–	–	–
VII	–	–	–	–	21.0	12.1	31.2	14	6.8	5	14.9	19.6	15.7	16.5	14.3	14.1	14.8	14.4	83	62	82	76	2.8	9.4	3.5	5.2	–	–	–	–
VIII	–	–	–	–	21.9	11.0	31.1	6	6.7	14	13.8	20.4	15.5	16.3	13.6	13.2	14.2	13.7	86	56	81	74	2.4	11.6	3.9	6.0	–	–	–	–
IX	–	–	–	–	20.6	10.5	28.0	3	5.3	16	12.0	19.6	14.2	15.0	12.4	12.8	13.8	13.0	88	57	85	77	2.0	10.6	2.7	5.1	–	–	–	–
X	–	–	–	–	13.5	3.6	23.1	1	−3.6	23	5.2	12.6	7.1	8.0	8.5	10.0	9.3	9.3	93	68	90	83	0.7	5.1	1.1	2.3	–	–	–	–
XI	–	–	–	–	2.1	−2.6	13.0	2	−13.6	18	−1.1	1.3	−0.2	0.0	5.4	6.0	5.5	5.6	86	83	84	84	0.7	1.3	1.0	1.0	–	–	–	–
XII	–	–	–	–	3.4	−0.6	12.5	19	−8.0	17	0.8	2.4	1.6	1.6	5.7	6.0	6.0	5.9	85	82	86	84	1.0	1.4	1.0	1.1	–	–	–	–
Rok	–	–	–	–	11.5	3.7	31.2	14. VII	−21.0	9. III	5.7	10.5	7.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Przybroda $H_s = 88\ m$ $h_w = 10\ m$ 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr V≥10	Wiatr V>15	◔	●	Opad R≥0.1	Opad R≥1.0	Opad R≥10.0	≡	⊠	K
I	6	2.8	6.5	2.3	13	2.7	10.5	1.3	19	4.4	13.5	4.0	12	3.3	7.5	2.4	5	3.1	33	7.5	17	·	6	26	·	·	·	·	15	14	9	·	10	19	—
II	10	4.6	5	4.2	2	3.5	2	4.2	4	3.8	17	5.3	28	4.9	9	5.9	7	4.5	8	1.7	12,13,15	8	18	26	·	3	·	2	12	12	3	·	1	26	—
III	12	4.5	4	3.2	3.5	2.4	12.5	2.3	11	2.6	13.5	3.4	14.5	4.9	4	5.1	18	2.9	35	12.6	3	7	7	22	·	1	·	7	11	10	8	1	8	16	—
IV	7.5	3.3	18	4.8	16.5	3.8	9.5	2.9	6.5	4.0	6.5	3.3	10	4.4	11.5	3.6	4	3.7	45	11.6	13	·	·	4	·	·	·	5	10	12	8	2	·	·	—
V	11	3.6	17.5	3.4	10	3.6	3	3.5	2.5	2.4	8.5	3.5	14.5	3.8	15	3.0	11	3.0	77	13.7	9	·	·	1	·	1	·	3	12	17	15	3	4	·	—
VI	12	3.5	9.5	3.9	4	3.8	7	2.7	7	3.2	13.5	3.3	17.5	3.6	10.5	2.8	9	3.0	37	10.5	30	·	·	·	4	·	·	5	6	9	7	1	·	·	—
VII	9	2.5	2	3.0	7.5	3.4	1	2.0	11	3.3	37	3.8	14	3.5	3.5	2.1	8	3.1	108	36.6	21	·	·	·	3	·	·	1	7	19	17	2	·	·	—
VIII	2.5	1.8	1	2.0	3	1.7	6.5	2.6	6.5	2.5	12.5	2.6	25.5	3.1	10.5	2.3	25	1.9	14	3.5	13	·	·	·	8	·	·	7	3	9	5	·	·	·	—
IX	1.5	2.3	2.5	3.4	12	3.4	10.5	3.0	16	3.5	20.5	3.9	11.5	3.3	2.5	3.4	13	3.0	43	18.2	10	·	·	·	2	·	·	8	2	8	5	2	2	·	—
X	7	2.2	4.5	2.6	8	3.3	2	2.0	11.5	2.7	9.5	3.6	20	3.0	6.5	2.5	24	2.2	10	6.5	16	·	·	7	·	·	·	7	2	5	3	·	11	·	—
XI	10	3.6	16.5	5.2	3.5	4.4	8	3.4	10.5	5.2	20	5.7	7.5	3.8	4	3.6	10	4.2	35	10.9	2	6	12	18	·	1	·	2	17	10	7	1	7	15	—
XII	0.5	3.0	2	2.8	8	3.4	11	3.7	25	4.7	29	5.8	13	4.2	3.5	1.9	1	4.5	46	10.7	18	·	4	21	·	4	·	1	16	18	10	1	2	12	—
Rok	89	3.1	89	3.4	91	3.3	83.5	2.8	130.5	3.5	201	4.0	188	3.8	88	3.2	135	3.3	491	36.6	21.VII	21	47	125	17	10	·	48	113	143	97	13	45	88	—

Wieliszew $H_s = 78\ m$ $h_w = 13\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr V≥10	Wiatr V>15	◔	●	Opad R≥0.1	Opad R≥1.0	Opad R≥10.0	≡	⊠	K
I	4	3.2	2.5	2.4	3	3.2	14	3.5	19.5	3.7	16.5	5.2	4	5.8	2.5	3.6	27	2.9	26	3.9	8	3	7	28	·	3	·	—	—	14	9	·	—	17	·
II	7	9.5	8	7.9	1.5	10.0	2.5	7.8	5.5	5.9	20	4.7	17.5	4.6	6	10.7	16	5.2	40	4.9	3	8	18	28	·	6	2	—	—	14	11	·	—	28	·
III	2.5	5.8	7.5	4.2	3	3.3	10	3.6	10	4.4	16.5	4.4	7.5	4.0	4	4.6	32	2.8	16	3.9	4	3	7	20	·	1	·	—	—	11	6	·	—	16	·
IV	3.5	6.0	10	4.8	8	6.2	22.5	4.9	16	6.0	7.5	4.2	2	2.8	6.5	4.5	14	4.4	40	10.8	23	·	·	5	·	5	1	—	—	12	9	1	—	·	1
V	10.5	4.0	10	3.8	12.5	4.2	5.5	5.8	8	4.8	11	5.7	8.5	3.7	11	3.8	16	3.6	48	18.9	18	·	·	2	·	3	1	—	—	12	8	1	—	·	3
VI	4.5	3.9	3.5	4.7	7.5	4.6	7.5	4.7	12	3.8	21.5	4.6	13.5	4.2	4	3.1	16	3.0	89	15.7	13	·	·	·	4	1	·	—	—	14	12	5	—	·	4
VII	1	4.0	5	5.6	4	3.4	9.5	3.2	8.5	3.8	31	4.6	13	3.7	5	3.0	16	3.4	125	39.2	17	·	·	·	5	1	·	—	—	20	17	4	—	·	9
VIII	4.5	3.0	1.5	4.3	1	3.0	5.5	2.9	7	3.7	19.5	4.2	10	3.4	6	3.1	38	2.2	84	33.3	26	·	·	·	10	·	·	—	—	11	9	2	—	·	1
IX	·	·	·	·	3	2.8	10	2.5	20.5	3.5	18.5	4.4	3.5	3.1	2.5	1.6	32	2.2	49	26.8	29	·	·	·	3	·	·	—	—	9	7	1	—	·	2
X	2	1.5	1.5	2.3	1.5	2.0	4	2.8	7.5	2.7	17.5	3.4	10.5	3.8	4.5	2.3	44	1.6	7	4.3	16	·	·	6	·	·	·	—	—	5	2	·	—	·	·
XI	0.5	6.0	9.5	5.3	12	4.5	11.5	5.2	9.6	7.1	16.5	6.9	5	3.6	1.5	3.0	24	4.1	32	7.0	21	6	11	18	·	3	2	—	—	14	8	·	—	15	·
XII	0.5	3.0	1	2.5	3.5	2.7	9.5	4.5	24	5.1	26	5.1	5.5	4.5	2	3.5	21	3.7	60	14.9	18	2	5	24	·	3	1	—	—	16	10	1	—	11	·
Rok	40.5	4.2	60	4.0	60.5	4.2	112	4.3	148	4.5	222	4.8	100.5	3.9	55.5	3.9	296	3.3	616	39.2	17.VII	22	48	131	22	26	7	—	—	152	108	15	—	87	20

Sulęcin $H_s = 80\ m$ $h_w = 10{,}4\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr V≥10	Wiatr V>15	◔	●	Opad R≥0.1	Opad R≥1.0	Opad R≥10.0	≡	⊠	K
I	2.5	1.8	5	1.7	5	1.2	9	1.8	14.5	2.9	24.5	4.3	5.5	3.5	6	2.6	21	2.3	49	11.6	17	·	2	24	·	1	·	1	19	14	11	1	8	7	1
II	9.5	4.1	5	3.0	2.5	3.0	2.5	3.4	4	3.1	13	3.9	6	3.8	21.5	4.1	20	2.9	34	5.6	13	7	17	26	·	2	·	1	17	21	13	·	5	27	·
III	5.5	2.7	7	3.9	·	·	9.5	2.2	19	2.0	9.5	1.8	11.5	2.4	7	3.5	24	1.8	62	24.1	3	7	6	21	·	·	·	9	15	13	9	2	2	17	·
IV	7.5	2.2	6.5	2.7	10	4.3	10.5	3.6	9.5	2.6	9.5	2.4	5	3.8	7.5	3.1	24	2.3	45	6.6	17	·	·	9	·	1	·	5	12	16	13	·	·	·	·
V	7.5	3.1	9.5	2.9	11.5	5.3	8	3.6	3.5	3.9	6.5	3.0	11.5	3.1	12	5.0	23	2.9	91	21.1	9	·	·	2	·	2	1	3	11	15	10	3	·	·	2
VI	11	2.9	6	3.1	9	4.2	3.5	3.9	7	3.3	9.5	3.6	14.5	3.2	5.5	3.5	24	2.5	35	13.1	1	·	·	·	6	·	·	2	6	6	5	1	1	·	4
VII	3.5	3.0	5	2.4	2.5	2.6	5	3.0	6	2.8	27	3.3	17.5	3.0	6.5	3.2	20	2.4	178	52.9	21	·	·	·	5	·	·	·	9	20	17	5	2	·	5
VIII	4	2.2	1.5	2.3	1	1.0	3.5	3.7	8.5	2.3	12	2.0	11.5	2.2	7	2.7	44	1.2	21	8.6	23	·	·	·	7	·	·	4	6	8	6	·	·	·	·
IX	0.5	3.0	·	·	2	5.5	6.5	6.1	14.5	2.2	19	3.0	8.5	3.2	3	2.7	36	2.0	81	34.3	10	·	·	·	3	·	·	7	6	10	10	2	·	·	2
X	2	1.8	2.5	1.8	4.5	2.2	8	2.5	10.5	1.7	11	2.0	10.5	2.4	4	2.0	40	1.2	22	11.4	16	·	·	12	·	·	·	8	2	3	3	1	10	·	·
XI	2	3.0	10	2.4	17	3.1	6	3.4	13	5.7	15	3.7	10	3.7	2	3.0	15	3.1	49	12.1	27	3	12	16	·	2	·	·	17	12	12	1	3	11	·
XII	·	·	·	·	·	·	9.5	2.9	20	3.3	29.5	4.3	20.5	2.9	3.5	2.4	10	3.1	77	14.3	18	·	3	21	·	·	·	·	18	21	14	3	2	8	·
Rok	55.5	2.5	58	2.2	65	2.7	81.5	3.3	130	3.0	186	3.1	132.5	3.1	85.5	3.2	301	2.3	744	52.9	21.VII	17	40	[illegible]	[illegible]	[illegible]	[illegible]	40	[illegible]	159	123	19	33	70	[illegible]

Poznań - Sołacz $H_s = 71\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr V≥10	Wiatr V>15	◔	●	Opad R≥0.1	Opad R≥1.0	Opad R≥10.0	≡	⊠	K
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	38	7.5	17	·	2	25	·	—	—	—	—	18	11	·	—	—	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	14	2.6	12	5	18	26	·	—	—	—	—	18	6	·	—	—	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	34	12.4	3	5	5	20	·	—	—	—	—	15	8	1	—	—	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	45	9.1	19,28	·	·	3	·	—	—	—	—	15	10	·	—	·	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	93	13.8	31	·	·	·	·	—	—	—	—	19	14	5	—	·	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40	9.6	30	·	·	·	5	—	—	—	—	14	8	·	—	·	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	103	23.7	21	·	·	·	3	—	—	—	—	19	17	3	—	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	28	7.0	25	·	·	·	8	—	—	—	—	14	9	·	—	·	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	38	15.0	10	·	·	·	3	—	—	—	—	7	4	2	—	·	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	10	6.5	16	·	·	7	·	—	—	—	—	18	2	·	—	·	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	42	9.1	21	4	11	16	·	—	—	—	—	19	10	·	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	49	14.1	18	·	4	16	·	—	—	—	—	21	9	1	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	534	23.7	21.VII	14	40	113	19	—	—	—	—	197	108	12	—	—	—

Poznań-Ławica

φ = 52°25′ λ = 16°50′ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{s.m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	999.7	1014.8	979.2	1011.3	2.2	−2.0	5.7	1	−6.2	7	−0.7	1.3	−0.1	0.1	5.4	5.8	5.6	5.6	93	87	91	90	0.4	1.0	0.6	0.7	8.2	8.0	8.0	8.1
II	1005.8	1022.7	978.4	1017.7	−0.5	−8.2	2.6	13	−17.1	6	−5.3	−1.9	−3.8	−3.7	3.7	4.2	4.1	4.0	87	78	86	84	0.5	1.2	0.6	0.8	7.2	6.9	7.2	7.1
III	1005.3	1021.4	978.0	1017.0	5.8	−3.9	15.3	29	−21.4	8	−2.6	4.2	0.2	0.5	5.0	5.8	5.6	5.5	89	68	85	81	0.5	3.0	1.0	1.5	6.4	6.1	5.4	6.0
IV	999.6	1021.4	982.1	1011.0	11.6	2.8	16.6	6	−2.5	5	4.4	9.9	6.4	6.8	7.6	7.4	7.8	7.6	90	61	81	77	0.9	5.0	1.9	2.6	6.6	8.3	4.8	6.6
V	1002.9	1018.4	988.0	1014.1	15.2	6.2	22.2	17	−0.2	4	8.7	13.5	10.4	10.8	9.7	9.6	9.6	9.6	84	63	75	74	1.7	6.1	3.3	3.7	7.1	7.8	6.6	7.2
VI	1003.2	1014.1	990.0	1014.1	22.2	11.4	32.0	26	6.0	3	15.0	20.7	16.2	17.0	12.7	12.5	13.7	13.0	74	52	74	67	4.6	12.6	5.0	7.4	5.3	7.2	5.4	6.0
VII	1000.7	1009.7	986.2	1011.7	21.3	11.7	32.0	14	5.6	4	14.6	19.6	15.5	16.3	13.8	13.4	14.3	13.8	81	59	80	73	3.1	10.1	3.8	5.7	6.8	7.3	5.8	6.6
VIII	1004.7	1013.0	992.5	1015.7	21.9	10.5	30.8	6	5.0	31	13.4	20.3	15.2	16.0	13.2	12.6	13.7	13.2	85	54	79	73	2.4	12.0	4.0	6.1	5.4	7.1	4.3	5.6
IX	1002.9	1023.9	990.6	1013.9	21.0	10.1	28.7	3	4.1	21	11.5	19.7	13.9	14.8	11.9	12.4	13.0	12.4	87	55	82	75	2.0	11.2	3.2	5.5	5.7	6.2	4.0	5.3
X	1012.1	1026.7	998.3	1023.5	13.5	3.5	22.8	1	−3.5	23	4.7	12.4	6.8	7.7	8.0	9.4	8.7	8.7	91	65	87	81	0.9	5.4	1.4	2.6	5.5	6.0	3.3	5.0
XI	1000.1	1020.4	969.7	1011.7	2.0	−2.9	12.3	1	−15.2	23	−1.5	1.1	−0.5	−0.4	5.0	5.5	5.1	5.2	83	77	80	80	1.0	1.7	1.2	1.3	8.4	9.2	7.1	8.2
XII	993.2	1014.5	968.0	1004.6	3.3	−1.0	12.4	19	−8.1	17	0.4	2.1	1.1	1.2	5.4	5.7	5.8	5.6	85	78	85	83	1.0	1.6	1.0	1.2	8.7	7.7	7.9	8.1
Rok	1002.5	1026.7	968.0	1013.8	11.6	3.2	32.0	26.VI, 14.VII	−21.4	8.III	5.2	10.2	6.8	7.2	8.4	8.7	8.9	8.7	86	66	82	78	1.6	5.9	2.2	3.2	6.8	7.3	5.8	6.6

Nowy Dwór Mazowiecki

φ = 52°26′ λ = 20°43′

I	—	—	—	—	1.1	−3.7	5.0	18	−14.2	11	−2.0	0.1	−1.5	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	9.3	7.3	5.7	7.4
II	—	—	—	—	−2.1	−8.9	2.8	14	−20.4	6	−6.5	−3.5	−5.5	−5.2	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.4	6.0	6.8
III	—	—	—	—	5.1	−3.6	12.6	30	−16.5	8	−2.7	3.9	0.1	0.4	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.3	4.5	5.4
IV	—	—	—	—	10.3	2.9	15.4	29	−1.3	3	4.1	8.9	6.2	6.4	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.0	6.3	7.0
V	—	—	—	—	14.6	5.7	21.2	17	−1.0	4	8.2	12.9	10.1	10.3	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.5	6.2	6.1
VI	—	—	—	—	21.5	12.0	30.2	26	7.6	8	14.7	20.1	16.2	16.8	—	—	—	—	—	—	—	—	—	—	—	—	4.3	5.7	6.7	5.6
VII	—	—	—	—	21.8	12.1	30.4	16	7.4	6	14.9	20.6	15.9	16.8	—	—	—	—	—	—	—	—	—	—	—	—	4.7	6.8	7.6	6.4
VIII	—	—	—	—	21.8	11.4	30.7	7	8.2	3	13.3	20.3	15.5	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.4	6.3	6.7	6.1
IX	—	—	—	—	20.9	9.6	27.8	3	4.8	21	11.0	19.6	13.8	14.6	—	—	—	—	—	—	—	—	—	—	—	—	4.5	4.8	2.9	4.1
X	—	—	—	—	12.3	3.6	20.9	1	−4.1	22	4.6	11.5	6.8	7.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	4.8	3.9	5.7
XI	—	—	—	—	1.1	−3.6	12.0	2	−19.1	24	−2.1	0.1	−1.2	−1.1	—	—	—	—	—	—	—	—	—	—	—	—	9.8	7.7	7.9	8.5
XII	—	—	—	—	2.2	−2.0	10.5	19	−17.0	17	−0.2	1.1	0.3	0.4	—	—	—	—	—	—	—	—	—	—	—	—	9.5	8.0	7.3	8.3
Rok	—	—	—	—	10.9	3.0	30.7	7.VIII	−20.4	6.II	4.8	9.6	6.4	6.8	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.4	6.0	6.5

Siemiatycze

φ = 52°26′ λ = 22°52′

I	—	—	—	—	−0.4	−5.7	3.0	9	−20.1	11	−3.4	−1.9	−2.8	−2.7	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.4	6.8	7.4
II	—	—	—	—	−3.2	−11.1	2.3	14	−22.0	24	−8.1	−4.6	−7.2	−6.8	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.6	5.4	6.7
III	—	—	—	—	3.9	−4.0	13.4	30	−19.4	9	−2.3	2.8	−0.5	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	7.3	5.8	5.5	6.2
IV	—	—	—	—	10.3	2.2	15.5	26,27,30	−3.8	3	4.0	8.8	5.3	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.4	6.4	7.0
V	—	—	—	—	14.5	4.7	22.1	18	−1.9	4	8.3	13.2	8.7	9.7	—	—	—	—	—	—	—	—	—	—	—	—	5.6	7.3	5.7	6.2
VI	—	—	—	—	20.5	11.0	28.4	26	3.8	8	14.6	19.3	14.7	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.4	6.3	6.2
VII	—	—	—	—	21.4	10.6	29.0	16	5.8	12	15.7	20.1	15.2	16.6	—	—	—	—	—	—	—	—	—	—	—	—	3.4	7.2	4.4	5.0
VIII	—	—	—	—	20.7	10.6	28.6	7	6.4	31	13.5	19.3	14.5	15.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	20.8	9.1	27.2	3	2.6	21	11.3	19.9	13.9	14.8	—	—	—	—	—	—	—	—	—	—	—	—	3.8	5.5	3.2	4.2
X	—	—	—	—	11.5	2.4	20.4	1	−5.9	21, 22	3.8	10.4	6.3	6.7	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.2	4.6	6.3
XI	—	—	—	—	0.7	−4.3	11.6	2	−19.7	17	−2.4	−0.8	−2.3	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	9.6	8.9	8.3	8.9
XII	—	—	—	—	1.1	−3.1	8.4	20	−16.6	17	−1.4	−0.1	−0.7	−0.7	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.2	8.4	8.1
Rok	—	—	—	—	10.2	1.9	29.0	16.VII	−22.0	24.II	4.5	8.9	5.4	6.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Legionowo

φ = 52°24′ λ = 20°58′

I	999.6	1016.3	980.8	1012.8	1.1	−4.1	5.1	18	−16.9	11	−2.3	−0.3	−1.5	−1.4	4.7	5.1	5.0	4.9	89	84	89	87	0.6	1.0	0.6	0.7	8.2	7.8	7.2	7.7
II	1002.4	1021.4	979.0	1015.8	−2.3	−9.4	2.6	14	−23.1	6	−7.0	−3.6	−5.9	−5.6	3.4	3.8	3.6	3.6	88	77	87	84	0.4	1.0	0.5	0.6	8.2	7.9	6.5	7.5
III	1004.4	1021.0	975.6	1017.5	4.9	−3.7	13.3	30	−17.5	8	−2.4	3.5	0.4	0.5	5.1	5.5	5.4	5.3	92	68	83	81	0.4	2.7	1.1	1.4	7.3	6.9	4.9	6.4
IV	999.4	1017.2	982.8	1012.2	10.4	2.0	15.6	30	−3.5	3	3.8	8.9	5.8	6.1	7.0	7.3	7.3	7.2	85	64	78	76	1.1	4.3	2.1	2.5	7.8	8.0	6.3	7.4
V	1001.7	1017.8	985.7	1014.3	14.4	4.8	21.2	18	−2.5	4	8.4	12.7	9.8	10.2	9.1	8.8	9.3	9.1	80	59	74	71	2.2	6.2	3.1	3.8	6.2	7.9	6.5	6.9
VI	1001.9	1010.1	993.5	1014.2	21.3	11.3	30.4	26	6.4	8	14.8	19.5	16.1	16.6	13.1	12.7	13.5	13.1	77	58	73	69	4.0	10.6	5.1	6.6	5.5	6.9	6.6	6.3
VII	999.8	1010.6	985.9	1012.1	21.8	11.4	30.3	16	6.9	6	15.0	20.1	15.8	16.7	14.0	13.0	14.5	13.8	81	55	80	72	3.2	11.2	3.7	6.0	6.1	7.3	6.0	6.5
VIII	1003.3	1011.2	993.1	1015.6	21.8	10.9	30.9	7	7.0	16, 31	13.5	19.9	15.6	16.2	13.4	13.1	13.8	13.4	86	58	78	74	2.3	11.2	4.4	6.0	5.9	6.5	4.9	5.8
IX	1003.2	1021.8	992.5	1015.6	21.1	9.4	27.9	3	3.5	21	11.3	19.4	14.0	14.7	12.4	12.9	13.6	13.0	91	58	84	78	1.3	10.2	2.7	4.7	5.7	5.3	2.5	4.5
X	1010.2	1025.7	996.5	1023.0	12.2	3.1	19.6	1	−4.6	21, 22	4.5	11.3	6.9	7.4	8.0	9.1	9.1	8.7	93	68	89	83	0.6	4.5	1.2	2.1	7.5	6.5	4.7	6.2
XI	999.8	1016.9	973.1	1013.0	0.8	−4.0	12.2	2	−16.6	24	−2.0	−0.2	−1.5	−1.3	5.1	5.3	5.3	5.2	89	84	90	88	0.7	1.2	0.6	0.8	9.4	8.7	8.6	8.9
XII	993.7	1008.8	971.8	1006.6	2.2	−2.5	10.2	19	−18.1	17	−0.5	0.9	0.1	0.2	5.5	5.5	5.4	5.5	89	82	85	85	0.7	1.3	0.9	1.0	8.6	8.5	7.9	8.3
Rok	1001.6	1025.7	971.8	1014.4	10.8	2.4	30.9	7.VIII	−23.1	6.II	4.8	9.3	6.3	6.7	8.4	8.5	8.8	8.6	87	68	82	79	1.5	5.4	2.2	3.0	7.2	7.4	6.0	6.9

Poznań-Ławica

$H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_w =$ 12,5 m anemometr M-47; 15 m anemometr Chauvin-Arnoux **1965**

MIESIĄC	ROZKŁAD WIATRU °D,V=D N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Min<0°	Max<0°	Max≥25°	Wiatr V ≥10	≥15	◐	●	Opad R ≥0,1	≥1,0	≥10,0	≡	⊠	⊠
I	5	4.1	5	4.6	8.5	3.1	13.5	3.5	16.5	4.8	17.5	4.4	9.5	6.0	8.5	4.5	9	4.0	31	7.7	17	·	2	28	·	4	·	·	20	17	9	·	8	20	·
II	7	6.3	7.5	6.6	6.5	4.2	4	3.0	1	1.0	17	4.9	23.5	6.0	14.5	6.9	3	5.5	14	3.0	26	8	18	27	·	9	·	1	13	15	6	·	5	28	·
III	5.5	4.4	10	6.7	7	2.9	12.5	2.7	16	3.7	13.5	3.4	14.5	7.2	8	5.6	6	4.3	34	12.6	3	5	7	22	·	7	·	6	14	14	7	1	11	17	·
IV	5.5	4.7	8.5	5.6	23	5.7	16.5	4.2	6.5	3.8	9	3.8	7	4.7	9	6.1	5	4.7	58	15.7	13	·	·	4	·	6	·	2	10	14	8	2	·	·	1
V	12	4.3	7.5	5.9	25	5.0	8	4.8	3.5	4.4	8	3.0	13	6.7	10	4.0	6	4.6	118	17.2	9	·	·	2	·	6	·	2	15	21	17	5	4	·	1
VI	5	5.0	7.5	6.3	15.5	5.8	7	3.4	11.5	3.7	13.5	4.3	19	6.1	10	5.7	1	5.1	46	11.6	30	·	·	·	7	9	·	2	8	15	9	1	·	·	5
VII	5.5	4.3	6.5	4.8	5.5	5.3	5.5	2.8	5	3.5	26.5	5.4	28.5	6.3	5	5.8	5	5.0	80	15.3	15	·	·	·	4	9	1	1	6	22	16	2	2	·	5
VIII	4.5	3.9	4	3.5	4	2.2	7.5	2.9	12	3.0	8.5	3.2	24	4.6	21.5	4.3	7	3.6	27	7.0	4	·	·	·	8	1	·	4	3	13	9	·	2	·	4
IX	0.5	9.0	1.5	5.0	7	3.6	15.5	3.8	14	2.9	25	4.0	17.5	5.3	6	5.2	3	4.0	54	22.7	28	·	·	·	3	3	·	4	3	8	5	2	4	·	·
X	6	3.5	5.5	2.4	12	3.4	7	2.6	7.5	2.7	20.5	4.2	13.5	4.2	12	3.5	8	3.2	12	7.7	16	·	·	5	·	1	·	5	2	4	3	·	15	·	·
XI	4	4.0	6.5	5.2	21	6.0	7.5	4.0	9	5.1	16.5	6.3	13.5	5.8	5	5.2	7	5.1	34	7.8	27	5	12	18	·	8	·	·	17	22	8	·	5	16	·
XII	1	4.0	·	·	4	3.2	14	4.5	18	5.6	29	6.3	20	5.4	6	4.7	1	5.4	52	12.6	18	·	3	19	·	8	·	·	18	25	13	1	3	13	·
Rok	61.5	4.8	70	4.7	139	4.2	118.5	3.5	120.5	3.7	204.5	4.4	203.5	5.7	115.5	5.1	62	4.5	580	22.7	28.IX	18	42	125	22	71	1	27	129	190	110	14	59	94	16

Uwaga. Kierunki i prędkości wiatru w ciągu roku - częściowo wg anemometru Chauvin - Arnoux, częściowo wg anemometru M-47.

Nowy Dwór Mazowiecki

$H_s = 70\,m$ $h_w = 13\,m$

I	2	1.0	3	1.8	7	1.4	15.5	1.0	8	1.0	11	1.6	5	2.8	6.5	4.2	35	1.1	34	5.6	27	3	7	27	·	·	·	1	18	16	10	·	6	26	·
II	9.5	2.8	7.5	3.0	6	3.2	1	1.5	2	1.8	16	1.7	21	2.5	12	3.0	9	2.2	39	10.5	26	9	22	26	·	·	·	2	12	19	9	1	3	28	·
III	1	6.0	3	1.0	4.5	1.0	11.5	1.3	5.5	1.4	14.5	2.5	9.5	1.8	8.5	2.8	35	1.2	15	3.6	4	5	7	19	·	·	·	5	10	13	5	·	5	18	·
IV	4.5	2.3	4.5	1.6	17.5	2.5	24.5	2.3	3	1.7	6.5	1.3	7.5	1.9	8	2.2	14	1.8	46	11.3	28	·	·	5	·	·	·	1	15	13	11	1	2	·	1
V	7.5	2.5	6	2.3	10.5	2.0	9	1.7	2.5	1.8	6	2.1	12	2.0	7.5	2.4	32	1.4	69	22.0	19	·	·	2	·	·	·	5	15	15	10	1	1	·	1
VI	0.5	4.0	5	3.4	9.5	2.7	5.5	2.5	3	1.7	8	2.3	17	2.4	9.5	2.8	32	1.6	88	17.6	12	·	·	·	5	·	·	5	11	14	13	3	·	·	4
VII	·	·	3.5	1.6	8	1.6	5	1.4	12	1.4	24	2.2	9	2.2	4.5	1.8	27	1.3	82	23.8	17	·	·	·	6	·	·	3	10	18	16	1	·	·	7
VIII	3.5	1.3	1	2.0	3	1.7	8	1.7	6.5	1.4	12.5	1.2	18.5	1.9	15	3.3	25	1.4	63	28.7	26	·	·	·	10	·	·	2	8	11	6	2	1	·	1
IX	·	·	·	·	3.5	1.4	12.5	1.7	11.5	1.4	15.5	1.5	8	2.0	4	1.9	35	1.0	54	19.2	29	·	·	·	2	·	·	10	6	9	8	1	4	·	2
X	5	1.5	3	1.2	4.5	1.3	1.5	1.7	2.5	1.2	16	1.4	15.5	2.0	14	2.3	31	1.2	8	4.1	16	·	·	4	·	·	·	3	9	5	2	·	15	·	·
XI	1	1.0	5	2.0	16.5	1.9	14	1.3	7.5	1.3	14	2.2	15	2.7	3	2.0	14	1.6	40	8.8	21	7	11	17	·	·	·	·	21	17	10	·	5	16	·
XII	2	1.0	·	·	1.5	1.0	9.5	1.2	12.5	1.8	36.5	2.3	10.5	1.6	4.5	1.2	16	1.5	60	14.5	18	2	6	22	·	1	·	·	22	19	14	1	1	13	·
Rok	36.5	2.0	41.5	1.7	92	1.8	117.5	1.6	76.5	1.5	180.5	1.9	148.5	2.2	97	2.5	305	1.4	598	28.7	26.VIII	26	53	122	23	1	·	37	157	169	114	11	43	101	16

Siemiatycze

$H_s = 145\,m$ $h_w = 16\,m$

I	7	1.2	6	1.9	15	2.5	19.5	2.3	22	2.2	8.5	1.8	7.5	3.5	7.5	2.3	·	2.3	33	8.3	20	5	11	30	·	·	·	4	16	13	8	·	3	31	·
II	16	1.6	12.5	3.0	1	3.0	2	2.0	8.5	3.5	13	3.4	18.5	2.1	10.5	3.3	2	2.6	36	8.5	7	12	23	28	·	1	·	1	10	18	13	·	3	28	·
III	3	1.8	12	1.1	4.5	2.2	23	1.5	25	1.5	6.5	2.2	14.5	1.9	4.5	1.8	·	1.6	23	5.4	17	4	7	24	·	·	·	5	13	11	6	·	9	19	·
IV	4.5	1.7	5	7.0	26	3.2	31.5	2.7	6.5	2.5	4.5	1.7	2.5	1.8	9.5	2.7	·	2.9	44	10.4	21	·	·	11	·	1	·	3	13	11	9	1	1	·	2
V	15	1.7	7.5	2.7	18.5	3.0	5	3.1	3.5	2.1	8	2.4	14.5	2.1	21	2.0	·	2.3	55	24.6	28	·	·	2	·	—	—	6	11	14	10	1	1	·	2
VI	5.5	1.7	9	3.2	7.5	2.7	6	3.0	9	2.0	12	2.7	21	2.0	16	2.1	4	2.2	62	14.2	14	·	·	·	4	·	·	·	8	13	13	2	·	·	3
VII	2.5	1.0	8.5	1.4	5	1.6	6	1.7	17	2.0	24	2.2	25	2.4	4	1.2	1	2.0	147	67.4	17	·	·	·	4	—	—	4	5	16	13	4	1	·	2
VIII	4	1.2	2	2.0	5	1.9	2	2.8	12	1.5	11	1.8	24	1.8	26	2.0	7	1.7	73	23.8	2	·	·	·	9	·	·	—	—	12	8	3	1	·	1
IX	·	·	·	·	8.5	2.7	18.5	1.8	22	1.7	18	1.8	14	1.9	7	1.6	2	1.8	29	9.8	14	·	·	·	3	·	·	7	4	9	5	·	4	·	1
X	11	1.6	8.5	1.5	6.5	2.1	3	1.3	16.5	1.5	9.5	2.0	18	2.8	19	2.1	1	2.0	10	3.8	16	·	·	5	·	·	·	10	3	9	3	·	13	·	·
XI	3.5	2.1	13.5	2.6	11.5	2.2	14	2.9	4.5	1.9	14.5	4.0	28.5	2.0	6	2.0	2	2.5	55	15.4	1	4	11	20	·	1	·	·	22	22	12	1	8	18	·
XII	3	1.0	2	1.5	7.5	1.9	9	1.9	34	2.9	23	2.1	10.5	1.8	4	2.8	·	2.3	43	8.6	18	2	6	26	·	·	·	·	17	19	11	·	5	20	·
Rok	75	1.4	86.5	2.3	116.5	2.4	139.5	2.2	180.5	2.1	152.5	2.3	190.5	2.2	135	2.2	19	2.2	610	67.4	17.VII	27	58	146	20	—	—	—	—	167	111	12	49	116	11

Legionowo

$H_s = 93\,m$ $H_b = 103{,}7\,m$ $h_w = 10\,m$

I	3.5	2.6	8	3.1	12.5	3.3	17.5	3.3	12	3.8	19	4.5	10	5.6	4.5	6.1	6	3.7	20	4.1	20	3	9	27	·	2	·	·	18	14	9	·	7	19	·
II	12	5.1	10.5	5.3	1.5	7.0	2	2.0	5	4.6	20	5.4	26	5.5	5	5.7	2	5.2	20	3.8	3	9	23	27	·	5	·	·	14	15	8	·	1	28	·
III	1.5	3.0	7.5	4.1	11	3.5	12	3.0	17	3.0	21	4.3	12	4.3	6	4.8	5	3.6	10	2.6	3	5	7	23	·	2	·	4	13	11	5	·	4	16	·
IV	5.5	5.3	10.5	4.2	33	5.6	11	3.8	5.5	2.7	6.5	3.9	7.5	4.4	6.5	3.8	4	4.4	39	11.9	23	·	·	7	·	4	·	·	14	13	8	1	1	·	1
V	14.5	3.2	19.5	3.6	15.5	4.9	4.5	3.6	2	2.2	9	4.3	15	3.8	10	3.8	3	3.7	54	15.6	19	·	·	3	·	4	1	1	12	16	9	1	2	·	3
VI	11.5	3.4	12	4.8	13	5.0	1	3.0	9.5	4.3	14.5	4.7	20.5	4.6	4	4.9	4	4.3	83	16.3	12	·	·	·	4	2	·	2	11	16	11	3	·	·	4
VII	2.5	3.4	6	5.5	12	3.7	7.5	3.0	9.5	3.3	32.5	4.4	20	4.4	2	4.5	1	4.1	134	57.3	17	·	·	·	5	1	·	3	10	20	15	2	·	·	10
VIII	11	2.7	3.5	3.0	5.5	2.5	10.5	3.4	11	3.6	16.5	3.4	19.5	4.1	9.5	3.9	6	3.3	72	30.8	26	·	·	·	10	·	·	2	7	10	9	2	1	·	1
IX	·	·	2	1.8	8	2.9	25	3.3	13.5	3.6	19	4.2	18	4.0	0.5	3.0	4	3.4	46	23.5	29	·	·	·	4	1	·	8	2	9	8	1	2	·	4
X	7.5	2.4	3.5	2.9	8	3.2	5	2.4	7.5	3.2	12.5	4.2	27.5	4.5	9.5	2.9	12	3.1	6	4.6	16	·	·	6	·	1	1	2	6	5	2	·	14	·	·
XI	4	2.2	13	5.2	16	4.3	9	4.8	7	3.8	15	4.7	18.5	5.2	1.5	3.0	6	4.3	29	7.5	21	6	12	20	·	3	2	·	23	13	8	·	5	16	·
XII	2.5	2.0	2	2.8	3.5	3.3	13	4.1	16	5.0	37	5.3	15	4.7	3	2.2	1	4.6	59	18.0	18	2	6	24	·	2	1	·	20	16	11	1	2	11	·
Rok	75	2.8	98	3.9	139.5	4.1	118	3.3	115.5	3.6	232.5	4.4	209.5	4.6	62	4.0	54	4.0	572	57.3	17.VII	25	57	137	23	27	5	22	150	158	103	11	39	90	23

Stubice

φ = 52°21' λ = 14°36'

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1007.8	1024.3	986.4	1010.9	3.9	−0.9	10.7	17	−7.8	7	0.8	2.8	1.0	1.4	6.0	6.3	6.0	6.1	91	85	90	89	0.6	1.3	0.7	0.9	8.2	7.9	7.7	7.9
II	1015.5	1030.9	988.5	1018.6	0.9	−5.7	5.4	13	−17.7	24	−3.5	−0.8	−1.6	−1.9	4.4	4.6	4.7	4.6	90	80	86	85	0.5	1.2	0.8	0.8	7.9	8.0	7.6	7.8
III	1013.8	1029.8	990.1	1016.9	6.8	−3.9	15.2	29	−25.3	8	−2.1	5.0	1.1	1.3	5.2	6.1	5.9	5.7	90	69	84	81	0.6	3.1	1.2	1.6	6.3	6.1	5.2	5.9
IV	1007.6	1030.0	987.5	1010.6	12.4	3.1	18.5	6	−2.2	5	4.9	10.6	7.3	7.5	7.7	7.9	8.4	8.0	88	64	82	78	1.0	5.0	1.9	2.6	5.8	7.7	7.1	6.9
V	1010.9	1025.5	998.0	1013.9	16.5	6.9	23.2	17	−0.4	3	9.8	14.7	11.4	11.8	10.3	9.9	10.2	10.1	83	60	75	73	1.9	7.0	3.5	4.1	6.2	7.5	6.3	6.7
VI	1011.3	1023.7	996.9	1014.2	22.2	11.4	29.3	26	6.5	30	14.9	20.0	16.2	16.8	13.3	12.9	13.9	13.4	78	56	76	70	3.9	11.0	4.7	6.5	4.8	7.2	5.7	5.9
VII	1008.5	1017.3	993.9	1011.4	21.1	11.9	32.2	14	6.8	2	14.5	19.1	15.5	16.2	14.3	13.8	14.3	14.1	85	62	80	76	2.4	8.9	3.5	4.9	7.0	7.5	6.4	7.0
VIII	1012.6	1022.0	996.4	1015.5	21.9	9.7	30.2	22	4.5	16	12.7	20.1	14.9	15.6	13.4	13.8	14.0	13.7	91	58	82	77	1.5	10.3	3.4	5.1	4.6	6.8	4.8	5.4
IX	1010.2	1032.0	995.3	1013.2	20.0	9.3	26.9	2	4.2	30	11.1	18.6	13.0	13.9	12.3	13.4	13.0	12.9	92	63	87	81	1.2	8.5	2.2	4.0	5.4	6.4	3.9	5.2
X	1020.3	1034.2	1006.4	1023.3	14.0	2.6	23.4	1	−5.2	23	4.2	12.8	7.0	7.8	8.3	10.4	9.4	9.4	96	69	92	86	0.4	4.8	1.0	2.1	6.0	5.7	3.4	5.0
XI	1008.1	1029.8	977.1	1011.2	3.4	−1.9	14.0	1	−14.1	23	−0.3	2.1	0.6	0.8	5.7	6.0	5.9	5.9	88	80	87	85	0.7	1.6	0.9	1.1	7.8	7.8	8.1	7.9
XII	1000.9	1022.9	972.3	1003.9	4.9	0.1	13.6	19	−6.6	14	1.7	3.7	2.6	2.6	6.2	6.6	6.8	6.5	88	82	90	87	0.9	1.5	0.7	1.0	7.9	8.3	9.1	8.4
Rok	1010.6	1034.2	972.3	1013.6	12.3	3.6	32.2	14.VII	−25.3	8.III	5.7	10.7	7.4	7.8	8.9	9.3	9.4	9.2	88	69	84	80	1.3	5.4	2.0	2.9	6.5	7.2	6.3	6.7

Paproć

φ = 52°19' λ = 16°08'

I	—	—	—	—	3.0	−1.4	8.6	17	−6.5	7	0.1	2.3	0.5	0.8	5.6	6.1	5.9	5.9	91	85	91	89	0.6	1.2	0.5	0.8	8.1	7.6	7.7	7.8
II	—	—	—	—	0.3	−6.2	3.7	13	−15.8	6	−4.3	−0.9	−2.7	−2.6	4.0	4.6	4.5	4.4	85	79	88	84	0.6	1.2	0.6	0.8	7.6	6.9	7.8	7.4
III	—	—	—	—	6.4	−4.3	15.2	29	−23.7	8	−2.6	5.2	0.6	1.0	5.0	6.2	6.0	5.7	87	68	86	80	0.6	3.2	0.9	1.6	5.0	5.5	5.3	5.3
IV	—	—	—	—	12.1	3.1	18.3	6	−2.1	3	4.9	10.8	7.4	7.6	8.0	8.3	8.6	8.3	91	65	83	80	0.8	4.8	1.7	2.4	5.8	7.1	6.2	6.3
V	—	—	—	—	15.5	6.3	22.4	17	−0.2	2	9.5	14.1	11.2	11.5	10.3	10.4	10.5	10.4	86	65	78	76	1.7	6.1	3.1	3.6	5.6	7.0	6.0	6.2
VI	—	—	—	—	21.7	11.1	30.1	26	4.9	3	14.8	20.2	16.3	16.9	13.5	13.6	14.3	13.8	80	58	77	72	3.6	10.7	4.4	6.2	5.1	6.5	5.2	5.6
VII	—	—	—	—	20.3	11.0	30.7	14	4.5	5	14.1	18.6	15.3	15.8	14.3	14.5	14.7	14.5	88	67	83	79	2.1	7.6	3.0	4.2	6.2	7.1	5.9	6.4
VIII	—	—	—	—	21.1	8.9	29.7	6	3.4	31	12.4	19.7	15.2	15.6	13.5	14.2	14.1	13.9	93	61	81	78	1.2	9.4	3.6	4.7	4.3	5.9	4.7	5.0
IX	—	—	—	—	19.8	8.4	26.3	3	1.2	21	10.4	18.5	13.7	14.1	11.9	13.7	13.5	13.0	93	65	86	81	1.1	8.1	2.5	3.9	4.7	5.4	4.5	4.9
X	—	—	—	—	13.6	1.9	22.3	1	−6.4	23	3.6	12.3	7.0	7.5	7.9	10.1	9.3	9.1	96	70	90	85	0.4	4.7	1.2	2.1	5.1	4.8	3.1	4.3
XI	—	—	—	—	2.7	−3.2	12.8	1	−21.6	23	−1.6	1.4	−0.6	−0.4	5.4	6.1	5.6	5.7	90	86	89	88	0.6	1.2	0.7	0.8	8.1	7.8	7.3	7.7
XII	—	—	—	—	3.8	−2.0	12.8	19	−8.3	14	0.4	2.4	1.5	1.4	5.9	6.2	6.4	6.2	92	84	92	89	0.6	1.2	0.5	0.8	8.3	7.4	8.2	8.0
Rok	—	—	—	—	11.7	2.8	30.7	14.VII	−23.7	8.III	5.1	10.4	7.1	7.4	8.8	9.5	9.4	9.2	89	71	85	82	1.2	5.0	1.9	2.7	6.2	6.6	6.0	6.3

Ostrowy

φ = 52°18' λ = 19°10'

I	—	—	—	—	1.3	−3.0	4.9	18	−11.5	11	−1.5	0.3	−1.1	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.1	7.2	7.4
II	—	—	—	—	−2.1	−9.7	2.1	13	−22.0	6	−6.6	−3.5	−5.6	−5.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.8	7.2	7.6
III	—	—	—	—	4.4	−4.8	12.5	30	−22.2	8	−3.0	2.9	−0.3	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.6	5.5	6.7
IV	—	—	—	—	9.9	2.0	15.1	30	−2.3	3	3.5	8.4	5.1	5.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	13.6	4.8	21.3	17	−1.8	4	8.0	12.2	8.9	9.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	21.2	10.7	31.2	26	5.2	16	14.2	19.6	15.0	16.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.3	11.0	30.2	15	4.6	5	14.5	19.8	14.4	15.8	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.9	5.8	5.7
VIII	—	—	—	—	21.2	10.0	29.2	6	4.8	17	13.0	19.9	13.8	15.1	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.4	4.9	5.6
IX	—	—	—	—	20.4	8.7	28.8	3	2.1	16	11.2	19.0	12.7	13.9	—	—	—	—	—	—	—	—	—	—	—	—	5.6	5.4	2.7	4.6
X	—	—	—	—	12.2	2.7	20.6	1	−5.8	22	4.6	11.0	6.0	6.9	—	—	—	—	—	—	—	—	—	—	—	—	7.1	5.9	4.1	5.7
XI	—	—	—	—	1.3	—	11.6	2	—	—	−2.7	0.1	−1.5	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	9.8	8.0	8.8	8.9
XII	—	—	—	—	2.4	−2.5	9.7	19, 20	−21.2	17	−0.3	1.0	−0.2	0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.5	8.5	8.3
Rok	—	—	—	—	10.6	—	31.2	26.VI	—	—	4.6	9.2	5.6	6.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Słupca

φ = 52°17' λ = 17°52'

I	—	—	—	—	1.7	−2.6	5.2	1	−7.2	11	−1.2	0.9	−0.7	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.7	7.4	7.7
II	—	—	—	—	−1.3	−9.0	2.5	14	−19.8	6	−6.1	−2.6	−5.1	−4.7	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.6	7.2	7.6
III	—	—	—	—	5.3	−4.4	14.9	29	−20.3	9	−2.4	3.9	−0.8	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	5.9	5.6	6.2
IV	—	—	—	—	10.7	2.6	15.7	30	−1.1	1	4.7	9.6	5.7	6.4	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.5	5.3	6.7
V	—	—	—	—	14.3	5.9	21.4	17	−1.1	4	8.8	13.0	9.4	10.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.1	6.1	7.1
VI	—	—	—	—	21.5	10.8	32.0	26	6.3	3	14.9	20.1	14.5	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.9	4.7	5.7
VII	—	—	—	—	21.3	11.3	30.8	14	6.2	4	14.8	19.5	14.5	15.8	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.8	5.5	6.8
VIII	—	—	—	—	21.7	9.9	29.3	7	5.3	14	13.7	20.3	14.0	15.5	—	—	—	—	—	—	—	—	—	—	—	—	5.0	6.5	4.7	5.4
IX	—	—	—	—	20.5	9.2	28.2	3	3.0	16	11.6	19.2	12.8	14.1	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.8	3.5	4.9
X	—	—	—	—	12.8	2.6	22.1	1	−4.2	22	4.7	11.8	5.8	7.0	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.9	2.8	4.8
XI	—	—	—	—	1.5	−4.1	12.0	2	−17.5	24	−2.2	0.5	−1.6	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.5	7.8	8.3
XII	—	—	—	—	2.9	−1.4	11.0	19	−11.7	17	−0.2	1.6	0.6	0.6	—	—	—	—	—	—	—	—	—	—	—	—	9.2	8.3	7.3	8.3
Rok	—	—	—	—	11.1	2.6	32.0	26.VI	−20.3	9.III	5.1	9.8	5.8	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.2	5.7	6.6

Słubice $H_s = 21 m$ $H_b = 24,1 m$ $h_w = 17 m$ 1965

MIESIĄC	ROZKŁAD WIATRU: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8.5	2.2	7.5	1.6	5	1.8	5.5	1.5	23	3.2	27.5	4.2	7.5	3.4	3.5	2.1	5	2.9	43	7.3	17	·	·	22	·	3	·	·	16	17	11	·	7	6	1
II	14.5	4.2	5.5	3.5	4.5	2.6	0.5	1.0	7.5	3.3	15	4.4	22.5	4.4	12	4.8	2	4.0	27	5.5	13	2	10	24	·	6	·	1	17	21	10	·	7	25	·
III	7	4.4	7	2.8	2.5	3.0	9.5	2.7	18	2.2	21.5	2.7	13	4.4	6.5	4.7	8	2.9	43	14.9	3	7	5	21	·	3	·	8	11	12	8	1	4	17	·
IV	3.5	4.1	10	2.6	10.5	4.0	12.5	2.2	11.5	2.7	11	2.5	12.5	3.9	11.5	3.5	7	2.9	37	7.3	17	·	·	4	·	2	·	3	15	17	10	·	·	·	·
V	13.5	3.7	12.5	3.5	14.5	3.8	5.5	3.6	5	2.8	10	3.6	16	4.1	13	3.5	3	3.5	86	20.6	9	·	·	1	·	3	·	4	14	14	9	3	·	·	1
VI	7	3.5	11	3.4	12	3.5	6.5	1.8	5	1.6	18.5	3.1	16.5	4.2	9.5	3.7	4	3.2	35	12.1	1	·	·	·	7	3	·	2	7	11	7	1	·	·	3
VII	4.5	3.6	7.5	2.5	6	2.7	3.5	3.0	10.5	1.9	35	3.6	19	5.0	4	1.8	3	3.3	123	29.2	17	·	·	·	6	3	·	·	8	19	14	4	1	·	6
VIII	9.5	2.4	4	1.2	3.5	1.1	7	2.3	8.5	1.8	25	2.5	14	3.2	10.5	2.6	11	2.1	39	19.9	23	·	·	·	7	·	·	4	5	9	5	1	1	·	1
IX	·	·	1.5	2.0	6.5	2.6	11	2.3	16	2.1	27.5	3.4	13.5	3.9	3	3.0	11	2.6	87	33.0	10	·	·	·	2	1	·	5	5	14	9	2	1	·	3
X	3.5	2.0	0.5	2.0	11	2.5	4.5	2.3	11.5	2.7	19.5	3.4	7.5	3.1	10	2.0	25	2.0	14	8.1	16	·	·	10	·	1	·	5	4	5	2	·	12	·	·
XI	·	·	14	3.2	14	4.0	7	3.0	11.5	4.1	24.5	5.0	7.5	3.9	5.5	3.5	6	3.8	49	15.9	21	1	10	18	·	1	·	1	18	13	8	2	4	11	·
XII	1.5	1.7	1	2.0	5	2.8	14	2.9	18.5	4.2	32.5	5.3	16	4.8	1.5	1.7	3	4.2	68	17.5	9	·	1	15	·	5	·	·	20	19	12	2	5	8	·
Rok	73	2.6	82	2.5	95	2.9	87	2.4	146.5	2.7	267.5	3.6	165.5	4.0	90.5	3.1	88	3.1	651	33.0	10.IX	10	26	115	22	31	·	33	140	171	105	16	42	67	15

Uwaga. Kierunki i prędkości wiatru - wg anemometru M-47.

Paproć $H_s = 75 m$ $h_w = 11 m$

I	8	1.9	7	2.3	11.5	2.0	13.5	2.0	17	2.2	13.5	2.4	13	2.4	0.5	1.0	9	2.0	47	8.8	9	·	1	25	·	·	·	1	16	18	12	·	12	14	·
II	11	3.4	8	2.6	5	2.2	1	2.0	2	1.0	16	3.3	20.5	2.8	14.5	3.1	6	2.7	24	3.8	25	5	11	26	·	·	·	·	13	17	11	·	5	27	·
III	7	2.7	11	2.7	·	·	7	1.6	12	1.8	7	2.1	18	2.7	10	3.4	21	1.9	39	14.8	3	8	5	21	·	·	·	6	10	15	9	1	10	18	·
IV	10	2.3	12.5	3.3	25.5	2.8	4	1.2	8	2.4	7	2.3	12	2.3	9	2.1	2	2.5	42	13.0	19	·	·	5	·	·	·	6	10	17	10	1	3	·	2
V	12	2.2	11.5	2.8	23.5	3.0	1	2.0	1	2.0	10	2.9	16	2.7	14	2.5	4	2.6	100	14.1	26	·	·	1	·	·	·	2	9	22	17	3	6	·	2
VI	4	2.2	13.5	2.7	12.5	2.6	7	2.4	3	2.3	10	2.1	22	2.5	14	2.6	4	2.4	60	19.5	1	·	·	·	6	·	·	3	6	11	7	2	·	·	2
VII	6	2.7	3.5	2.6	9	2.3	0.5	1.0	10.5	2.0	32.5	2.3	21	2.7	5	1.9	5	2.3	119	49.8	16	·	·	·	3	·	·	·	7	22	16	2	1	·	5
VIII	4	2.0	2	1.0	2	2.0	5	1.6	4	1.2	6	2.5	23	2.0	20	1.8	27	1.3	29	16.1	23	·	·	·	6	·	·	·	3	11	5	1	8	·	2
IX	·	·	·	·	8.5	2.4	12.5	2.6	8	2.0	26	1.9	14	2.1	2	2.0	19	1.7	56	21.4	10	·	·	·	2	·	·	2	1	12	9	2	10	·	·
X	1.5	1.3	1	2.0	11.5	1.3	9.5	1.5	8	1.5	10	1.7	16	1.9	6.5	1.4	29	1.1	16	7.2	16	·	·	12	·	·	·	5	2	4	3	·	16	·	·
XI	1	2.0	17	2.6	12	2.6	7	2.7	10	2.3	20	2.7	8	3.4	12	1.8	3	2.5	40	9.4	21	5	10	19	·	·	·	·	17	18	10	·	11	16	·
XII	·	·	·	·	6	2.5	12	2.3	21	2.9	22.5	3.9	19.5	2.4	8	1.9	4	2.7	60	15.0	18	·	2	19	·	1	·	·	14	26	20	1	2	4	·
Rok	64.5	1.9	87	2.0	127	2.1	80	1.9	104.5	2.0	180.5	2.5	203	2.5	115.5	2.1	133	2.1	632	49.8	16.VII	18	29	128	17	1	·	25	108	193	129	13	84	79	13

Ostrowy $H_s = 120 m$ $h_w = 11 m$

I	8	2.0	4.5	3.2	8	3.5	6.5	4.4	19.5	3.5	19.5	4.4	11.5	4.3	5.5	3.7	10	3.4	25	5.4	30	1	6	27	·	·	·	·	13	14	7	·	5	14	·
II	14.5	4.4	5.5	3.4	2	3.5	·	·	1.5	5.0	16	4.7	28.5	5.4	11	4.4	5	4.5	18	2.5	7	12	20	28	·	2	·	·	15	17	9	·	3	28	·
III	2	2.2	8.5	2.0	2	1.5	7	3.0	13.5	2.7	16	3.3	23	3.3	8	3.6	13	2.6	25	6.4	3	6	7	23	·	·	·	1	13	12	7	·	2	17	·
IV	8	2.9	9.5	3.8	15.5	3.7	11	3.4	6	3.7	5.5	1.9	7	3.5	6.5	3.7	21	2.6	59	23.6	28	·	·	7	·	·	·	—	—	15	11	1	1	·	1
V	8.5	2.5	6.5	2.3	18	3.0	2.5	5.4	3	3.2	7	3.4	9.5	4.4	11	3.0	27	2.3	93	27.0	19	·	·	3	·	3	·	—	—	15	14	2	1	·	3
VI	9.5	2.3	12	2.8	10	2.3	2.5	3.6	6.5	3.2	6	3.9	20.5	3.0	9	2.6	14	2.4	55	14.3	26	·	·	·	6	2	·	—	—	13	10	2	·	·	3
VII	·	·	5.5	2.3	5.5	2.1	2.5	3.0	9.5	3.2	22.5	3.3	25	3.7	4.5	2.0	18	2.6	63	9.2	8	·	·	·	5	2	·	1	6	15	15	·	·	·	6
VIII	9	1.4	·	·	1	1.0	6.5	3.4	9	2.5	9.5	2.4	15	2.0	14	1.8	29	1.5	50	12.6	25	·	·	·	9	·	·	2	8	10	9	1	2	·	2
IX	·	·	·	·	4.5	3.7	13	3.2	12.5	3.5	19	2.9	22	3.0	4	1.8	15	2.6	68	45.8	4	·	·	·	2	·	·	8	3	6	5	1	1	·	·
X	8.5	1.8	5.5	1.2	11	2.6	3.5	2.4	6	3.0	17	3.4	10.5	3.6	8	2.3	23	2.1	10	6.2	16	·	·	7	·	·	·	6	11	3	3	·	9	·	·
XI	·	·	8	3.4	18.5	2.9	8	4.1	7.5	3.9	17	5.3	15.5	4.6	3.5	2.0	12	3.5	31	11.6	21	—	10	—	·	1	·	1	23	10	6	1	5	16	·
XII	·	·	1	1.6	1.5	1.7	8.5	4.4	22	5.8	26	4.9	23	4.0	3	5.0	8	4.3	51	18.0	18	2	5	22	·	5	2	1	19	13	11	1	4	5	·
Rok	68	1.6	66.5	2.2	97.5	2.6	71.5	3.4	116.5	3.6	181	3.6	211	3.7	88	3.0	195	2.9	548	45.8	4.IX	—	48	—	22	15	2	—	—	143	107	9	33	60	15

Słupca $H_s = 90 m$ $h_w = 11 m$

I	3	2.3	3.5	2.0	8	1.9	16.5	2.4	18.5	2.4	21	2.5	10.5	2.0	6	2.4	6	2.1	30	5.0	24	·	5	28	·	·	·	1	17	16	10	·	3	15	·
II	10	3.4	5	2.8	3	2.2	2	2.0	6.5	2.5	18.5	3.0	19	2.8	12	3.8	8	2.7	22	2.9	7	11	18	28	·	·	·	2	17	17	10	·	1	28	·
III	6	3.2	7	2.2	3	2.2	9.5	2.2	10.5	1.7	17	2.7	8.5	3.5	11.5	2.4	20	2.0	31	10.3	3	7	8	21	·	1	·	5	13	13	8	1	3	16	1
IV	5.5	2.5	8.5	2.3	14	3.1	28	2.3	7.5	1.7	7	1.9	10	2.2	5.5	2.1	4	2.2	26	10.0	28	·	·	6	·	·	·	2	12	11	7	1	1	·	1
V	6.5	2.8	7.5	2.4	11	2.9	12.5	3.6	4.5	1.8	7.5	2.4	10.5	2.0	16	2.0	17	2.1	99	19.4	19	·	·	2	·	·	·	2	14	20	16	3	·	·	1
VI	1	1.0	11	3.0	5.5	2.5	10.5	2.5	11.5	2.8	14	1.5	13.5	3.3	10	2.6	13	2.2	52	12.0	12	·	·	·	5	·	·	3	7	13	8	2	·	·	5
VII	2.5	1.4	6.5	2.5	4	2.1	5	2.1	15	1.8	31.5	2.1	17.5	2.8	3	1.7	8	2.0	45	13.0	28	·	·	·	4	·	·	3	9	16	11	1	·	·	8
VIII	2.5	1.0	1.5	1.0	·	·	7.5	1.8	13	1.6	18.5	1.4	20	1.8	18	1.5	12	1.4	28	12.1	25	·	·	·	7	·	·	4	5	7	5	1	·	·	·
IX	·	·	·	·	0.5	2.0	24	2.0	16.5	1.6	25	1.9	12	2.2	1	3.0	11	1.7	48	17.4	10	·	·	·	3	·	·	5	4	7	7	2	2	·	1
X	3	1.2	2.5	1.8	4	1.6	8	1.1	10	1.0	21	1.9	12.5	2.1	6	1.3	26	1.2	16	6.6	2	·	·	9	·	·	·	5	5	4	4	·	8	·	·
XI	3.5	2.1	13.5	2.4	7	2.3	11.5	2.1	10	2.1	23	3.2	6	1.5	4.5	3.0	11	2.2	37	8.0	21	6	11	20	·	1	·	1	19	13	10	·	4	16	·
XII	0.5	1.0	1.5	1.0	1	1.0	18	2.1	18.5	2.4	33	2.9	8.5	1.8	4	1.5	8	2.2	38	11.3	18	1	4	21	·	·	·	·	20	17	12	1	1	6	·
Rok	44	1.8	68	2.0	61	2.0	153	2.2	142	2.0	237	2.3	148.5	2.3	97.5	2.3	144	2.0	472	19.4	19.V	25	46	135	19	·	·	33	142	154	108	12	23	81	17

Warszawa - Bielany φ = 52°17' λ = 20°58' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1000.2	1016.7	981.0	1012.8	1.1	−3.5	4.7	18	−15.0	11	−1.8	−0.2	−1.1	−1.0	4.9	5.0	5.1	5.0	88	83	88	86	0.6	1.1	0.7	0.8	8.1	8.1	7.0	7.7
II	1003.1	1022.0	979.3	1015.9	−2.1	−6.9	2.6	13, 14	−20.7	6	−6.6	−3.8	−5.5	−5.4	3.4	3.7	3.5	3.5	85	77	82	81	0.6	1.0	0.7	0.8	7.8	7.3	6.6	7.2
III	1005.2	1021.0	975.8	1017.7	5.1	−2.7	13.9	30	−16.5	8	−1.7	3.5	1.1	1.0	5.1	5.4	5.4	5.3	89	68	79	79	0.6	2.8	1.5	1.6	6.9	6.5	4.9	6.1
IV	999.8	1017.9	983.3	1012.0	10.4	2.9	15.1	29, 30	−2.0	1	4.1	8.8	6.5	6.5	7.1	7.2	7.1	7.1	84	63	73	73	1.3	4.4	2.7	2.8	8.0	8.1	6.7	7.6
V	1002.2	1017.9	986.7	1014.2	14.2	5.8	20.6	17	−1.0	4	8.3	12.5	10.4	10.4	9.1	8.8	9.2	9.0	80	60	71	70	2.2	5.9	3.7	3.9	6.5	8.5	5.9	7.0
VI	1002.4	1010.1	993.7	1014.2	21.1	12.1	30.3	26	8.0	3	14.7	19.2	16.3	16.6	13.1	12.6	13.3	13.0	78	58	72	69	3.8	10.3	5.5	6.5	5.4	7.1	5.4	6.0
VII	1000.4	1011.0	986.4	1012.1	21.7	12.4	29.7	15, 16	6.9	6	15.3	20.0	16.4	17.0	14.0	13.2	14.4	13.9	80	56	77	71	3.6	10.9	4.7	6.4	6.0	7.8	5.7	6.5
VIII	1003.7	1011.6	993.0	1015.5	21.2	11.9	30.4	7	8.0	3	13.7	19.4	16.0	16.3	13.4	13.2	13.8	13.5	85	60	77	74	2.6	10.3	5.0	6.0	5.9	6.8	5.2	6.0
IX	1003.7	1022.0	993.1	1015.5	21.0	10.5	27.1	3	5.0	21	12.1	19.3	14.8	15.2	12.7	13.3	13.8	13.3	89	60	81	77	1.6	9.6	3.4	4.9	5.7	5.8	3.0	4.8
X	1010.9	1026.1	997.3	1023.1	12.1	4.1	20.2	1	−3.2	21	5.1	11.1	7.4	7.8	8.4	9.2	9.2	8.9	93	68	88	83	0.6	4.4	1.3	2.1	6.5	6.4	4.8	5.9
XI	1000.4	1017.8	974.2	1013.0	1.3	−3.5	12.2	2	−15.1	18	−2.0	−0.2	−1.0	−1.0	5.2	5.4	5.4	5.3	89	84	89	87	0.7	1.1	0.8	0.9	9.6	8.1	8.8	8.8
XII	994.4	1010.3	972.7	1006.8	2.4	−1.9	9.6	20	−16.4	17	−0.2	1.0	0.4	0.4	5.5	5.5	5.5	5.5	88	82	85	85	0.8	1.3	1.0	1.0	8.8	8.5	7.9	8.5
Rok	1002.2	1026.1	972.7	1014.4	10.8	3.3	30.4	7. VIII	−20.7	6. II	5.1	9.2	6.8	7.0	8.5	8.5	8.8	8.6	86	68	80	78	1.6	5.3	2.6	3.2	7.1	7.4	6.0	6.8

Warszawa, Inst. Geogr. UW φ = 52°14' λ = 21°01'

I	—	—	—	—	1.4	−2.7	4.7	17	−13.5	11	−1.4	−0.1	−0.7	−0.7	5.0	5.3	5.3	5.2	89	86	89	88	0.6	0.9	0.7	0.7	7.8	8.2	7.0	7.7
II	—	—	—	—	−1.9	−7.9	2.8	14	−18.4	6	−6.2	−3.3	−5.0	−4.9	3.5	4.0	3.8	3.8	87	81	85	84	0.5	0.8	0.6	0.6	7.5	7.4	7.1	7.3
III	—	—	—	—	5.1	−1.9	13.8	30	−13.4	8	−1.1	3.7	1.8	1.6	5.3	5.9	5.8	5.7	89	73	80	81	0.6	2.4	1.4	1.5	7.5	6.9	5.5	6.6
IV	—	—	—	—	10.4	3.4	15.0	29	−0.9	1	4.3	9.1	6.9	6.8	7.1	7.4	7.4	7.3	83	64	73	73	1.4	4.3	2.7	2.8	8.4	8.0	6.6	7.7
V	—	—	—	—	14.3	6.6	20.6	17	0.2	3, 4	8.7	12.9	10.9	10.8	9.3	9.3	9.6	9.4	80	62	72	71	2.2	5.8	3.6	3.9	6.4	8.5	6.6	7.2
VI	—	—	—	—	21.2	12.7	29.8	26	8.8	3	14.8	19.6	16.8	17.0	13.4	12.9	13.9	13.4	79	59	73	70	3.6	10.6	5.5	6.6	5.5	7.4	5.8	6.2
VII	—	—	—	—	21.8	13.1	29.6	16	8.7	6	15.3	20.3	17.0	17.4	14.1	13.8	14.7	14.2	80	58	76	71	3.5	10.7	5.1	6.4	5.5	7.3	5.5	6.1
VIII	—	—	—	—	21.2	12.4	30.8	7	8.6	13	13.8	19.5	16.4	16.5	13.7	14.4	14.4	14.2	86	64	77	76	2.3	9.2	4.9	5.5	5.8	6.9	5.0	5.9
IX	—	—	—	—	20.5	11.2	26.5	3	7.2	21	12.2	19.1	15.5	15.6	12.9	14.3	14.7	14.0	90	65	83	79	1.5	8.2	3.1	4.3	5.6	5.9	3.9	5.1
X	—	—	—	—	11.9	4.9	19.7	1, 2	−1.6	22	5.8	11.0	8.3	8.4	8.5	9.5	9.5	9.2	91	71	85	82	0.9	4.0	1.7	2.2	6.5	6.7	4.7	6.0
XI	—	—	—	—	1.6	−2.8	12.5	2	−14.0	18	−1.5	0.0	−0.5	−0.6	5.3	5.5	5.5	5.4	89	84	88	87	0.7	1.1	0.8	0.9	9.5	8.7	9.1	9.1
XII	—	—	—	—	2.9	−1.3	10.3	20	−15.4	17	0.3	1.3	0.8	0.8	5.6	5.7	5.6	5.6	87	82	85	85	0.9	1.3	1.0	1.1	8.3	9.1	8.3	8.6
Rok	—	—	—	—	10.9	4.0	30.8	7. VIII	−18.4	6. II	5.4	9.4	7.4	7.4	8.6	9.0	9.2	8.9	86	71	80	79	1.6	4.9	2.6	3.0	7.0	7.6	6.3	7.0

Warszawa, Obserw. Astr. UW φ = 52°13' λ = 21°02'

I	998.0	1015.1	977.8	1012.5	1.6	−3.3	5.1	18	−14.0	11	−1.7	0.1	−0.9	−0.8	5.1	5.3	5.2	5.2	91	85	90	89	0.5	1.0	0.6	0.7	—	—	—	—
II	1000.8	1019.4	977.6	1015.6	−1.6	−8.2	2.5	13, 14	−19.0	6	−6.3	−3.2	−4.9	−4.8	3.5	4.0	3.8	3.8	85	79	85	83	0.6	1.0	0.6	0.7	—	—	—	—
III	1002.8	1019.6	973.5	1017.2	5.7	−2.5	14.2	30	−14.5	8	−1.5	4.1	1.3	1.3	5.1	5.8	5.7	5.5	87	71	82	80	0.7	2.7	1.2	1.5	—	—	—	—
IV	997.8	1015.6	981.0	1011.9	10.8	3.0	16.8	30	−1.9	3	4.3	9.5	6.7	6.8	7.3	8.2	7.9	7.8	86	68	79	78	1.1	3.9	2.0	2.3	—	—	—	—
V	1000.2	1016.3	984.3	1014.2	14.8	6.4	21.1	17	−1.4	4	8.8	13.3	10.6	10.8	9.8	10.8	10.5	10.4	84	67	80	77	1.8	5.1	2.6	3.2	—	—	—	—
VI	1000.4	1008.4	991.8	1014.1	21.5	12.4	30.4	26	8.5	8	14.6	19.9	16.2	16.7	13.7	14.4	14.4	14.2	82	64	77	74	3.0	9.4	4.4	5.6	—	—	—	—
VII	998.0	1009.1	983.4	1011.6	22.1	12.7	30.1	16	8.5	6	15.0	20.4	16.4	17.0	14.6	14.7	15.1	14.8	84	61	81	75	2.7	10.1	3.8	5.5	4.8	7.2	5.5	5.8
VIII	1001.8	1009.9	991.3	1015.5	21.8	12.1	30.1	7	8.7	3	13.6	19.9	15.8	16.3	13.8	14.3	14.2	14.1	88	62	79	76	2.1	9.9	4.2	5.4	5.1	6.0	4.5	5.2
IX	1001.9	1020.1	991.2	1015.6	20.9	10.3	26.8	3	6.8	21	11.7	19.6	14.7	15.2	13.0	14.2	14.3	13.8	93	63	85	80	0.9	9.0	2.6	4.2	4.7	4.9	2.0	3.9
X	1008.8	1024.0	995.4	1023.0	12.4	4.5	21.4	1	−2.6	21	5.5	11.5	7.9	8.2	8.5	9.7	9.4	9.2	92	70	86	83	0.8	4.3	1.5	2.2	6.2	5.3	3.9	5.1
XI	998.3	1015.5	971.3	1012.8	1.8	−2.9	12.2	2	−14.5	18	−1.6	0.4	−0.7	−0.6	5.2	5.5	5.5	5.4	89	83	89	87	0.7	1.2	0.7	0.9	9.7	8.4	8.8	9.0
XII	992.6	1008.6	970.8	1006.9	2.8	−1.5	9.8	20	−16.5	17	0.1	1.3	0.7	0.7	5.5	5.7	5.5	5.6	86	83	85	85	0.9	1.2	1.0	1.0	8.4	9.0	7.9	8.4
Rok	1000.1	1024.0	970.8	1014.2	11.2	3.6	30.4	26. VI	−19.0	6. II	5.2	9.7	7.0	7.2	8.8	9.4	9.3	9.2	87	71	83	80	1.3	4.9	2.1	2.8	—	—	—	—

Warszawa, St. Pomp. Rzecz. φ = 52°13' λ = 21°03'

I	—	—	—	—	1.1	−3.3	4.8	18	−14.1	11	−1.7	−0.2	−1.2	−1.1	—	—	—	—	—	—	—	—	—	—	—	—	7.4	8.1	8.4	8.0
II	—	—	—	—	−2.0	−8.2	2.8	14	−19.8	6	−6.2	−3.4	−4.8	−4.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.7	8.1	7.6
III	—	—	—	—	5.3	−2.8	14.1	30	−14.1	8, 9	−1.8	3.6	1.1	1.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	11.1	2.8	15.1	30	−1.6	3	4.2	9.3	6.4	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.6	7.9	7.6
V	—	—	—	—	14.6	6.1	22.2	17	−1.1	4	8.7	12.9	10.5	10.6	—	—	—	—	—	—	—	—	—	—	—	—	5.7	7.5	6.7	6.6
VI	—	—	—	—	21.3	12.3	29.9	26	8.3	8	14.8	19.6	16.4	16.8	—	—	—	—	—	—	—	—	—	—	—	—	5.0	6.3	4.8	5.4
VII	—	—	—	—	22.0	12.4	29.6	14, 15, 16	7.8	5	15.2	20.4	16.6	17.2	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.3	5.8	5.6
VIII	—	—	—	—	21.4	11.8	30.7	7	8.1	16	13.6	19.7	15.5	16.1	—	—	—	—	—	—	—	—	—	—	—	—	4.9	5.6	5.4	5.3
IX	—	—	—	—	20.9	10.0	26.8	3	6.0	17	11.6	19.5	14.3	14.9	—	—	—	—	—	—	—	—	—	—	—	—	4.7	4.9	2.6	4.1
X	—	—	—	—	12.4	3.9	21.3	1	−4.4	22	5.1	11.3	7.5	7.8	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.0	5.5	5.9
XI	—	—	—	—	1.5	−3.1	13.3	3	−14.5	18	−1.9	0.1	−0.9	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	9.9	8.3	9.1	9.1
XII	—	—	—	—	2.5	−1.7	10.1	20	−17.3	17	0.0	1.2	0.4	0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.7	8.1	8.4
Rok	—	—	—	—	11.0	3.4	30.7	7. VIII	−19.8	6. II	5.1	9.5	6.8	7.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Warszawa - Bielany $H_s = 98$ m $H_b = 99,5$ m $h_w = 16$ m 1965

MIESIĄC	ROZKŁAD WIATRU (D, V_D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	2.6	5	3.1	6.5	2.8	17	4.2	16	3.2	14.5	3.5	6.5	4.7	7	3.3	17	2.9	23	4.5	20	3	8	27	·	·	·	·	19	13	10	·	4	23	·
II	9.5	4.1	9	4.7	1	5.0	·	·	1.5	5.0	17.5	4.4	23.5	3.8	13	4.2	9	3.7	22	2.7	13	8	21	28	·	2	·	·	14	18	10	·	1	28	·
III	2	2.2	3.5	2.4	6.5	2.3	14.5	3.4	9.5	2.1	17.5	3.4	17	2.6	9.5	3.2	13	2.5	14	3.0	2	4	7	18	·	·	·	7	14	12	5	·	4	16	·
IV	7	3.1	10.5	4.5	22.5	5.6	17	4.6	4	3.6	7.5	3.2	6.5	3.1	7	3.3	8	4.0	42	11.8	28	·	·	3	·	5	·	·	16	13	8	1	1	·	1
V	11.5	2.6	6	3.7	13.5	3.6	8.5	5.2	3	2.8	10.5	3.1	12	3.4	14	3.5	14	3.0	117	36.7	25	·	·	2	·	1	·	2	12	19	13	3	2	·	3
VI	6.5	3.2	12.5	4.7	8.5	5.3	4.5	3.4	4	3.0	11.5	3.6	20	3.7	8.5	2.6	14	3.2	91	34.0	14	·	·	·	4	2	·	2	9	16	10	1	·	·	4
VII	2	1.8	7.5	3.3	4	3.8	6.5	3.7	9	3.1	18.5	3.5	31	3.5	2.5	2.0	12	2.9	138	57.2	17	·	·	·	6	·	·	1	8	20	16	3	·	·	8
VIII	6	3.2	0.5	7.0	3.5	5.6	8.5	4.4	7	2.8	10.5	3.3	20.5	2.8	17.5	3.0	19	2.6	108	39.2	26	·	·	·	10	·	·	1	11	12	9	4	·	·	1
IX	·	·	·	·	7	3.9	16.5	4.1	10.5	2.8	17.5	2.9	24.5	3.1	1	3.0	13	2.8	54	27.1	29	·	·	·	2	·	·	6	4	8	8	1	·	·	2
X	4	2.8	3	3.2	3.5	3.4	0.5	4.0	7.5	2.3	15.5	3.5	20.5	3.4	17.5	2.7	21	2.4	8	4.4	16	·	·	3	·	·	·	4	8	8	2	·	11	·	·
XI	·	·	10	3.7	11.5	3.8	9.5	5.1	7.5	3.5	12.5	4.2	21	3.2	2	3.8	16	3.1	38	8.8	21	7	12	18	·	·	·	·	22	21	10	·	5	17	·
XII	1.5	2.3	1.5	1.3	1	2.0	11.5	4.0	12	4.4	30.5	3.8	18.5	2.9	6.5	2.2	10	3.1	58	17.9	18	2	5	20	·	·	·	·	20	17	11	1	2	13	·
Rok	54.5	2.3	69	3.5	88	3.9	114.5	3.8	91.5	3.2	184	3.5	221.5	3.4	106	3.1	166	3.0	713	57.2	17.VII	24	53	119	22	10	·	23	157	177	112	14	30	97	19

Warszawa, Inst. Geogr. UW $H_s = 108$ m $h_w = 20$ m

I	1	1.5	8	1.9	15.5	2.2	26.5	2.7	17	2.8	6	3.2	6	5.4	4	4.2	9	2.6	20	4.1	20	3	4	25	·	1	·	·	19	16	7	·	4	20	·
II	6	4.0	6.5	1.9	11	2.1	4	2.0	17.5	3.3	18	3.8	14.5	3.4	5.5	5.0	1	3.2	26	5.4	10	8	21	26	·	2	·	1	14	18	11	·	3	28	·
III	0.5	3.0	2.5	2.4	16.5	1.9	27	2.1	15	3.0	14.5	3.7	5	4.3	5	4.0	7	2.5	11	2.9	3	4	7	16	·	·	·	4	14	11	4	·	4	17	·
IV	2.5	1.8	10.5	3.7	31	3.3	20	2.7	8	2.5	5	3.3	7	2.6	3	2.7	3	2.9	33	9.8	28	·	·	3	·	·	·	·	15	12	8	·	2	·	·
V	6.5	1.9	8.5	2.5	20.5	2.4	16	3.0	7.5	2.3	8	2.8	6	3.0	11	3.2	9	2.4	74	17.0	29	·	·	·	·	·	·	1	14	15	11	3	1	·	3
VI	4.5	2.2	8	2.9	17.5	2.4	11.5	2.0	15	2.5	16	3.2	5	4.0	5.5	3.2	7	2.5	68	22.4	14	·	·	·	4	·	·	1	10	13	10	1	1	·	3
VII	1	3.0	9	2.6	10	3.2	18	2.6	28	2.9	21	4.2	2	5.0	·	·	4	3.1	141	68.0	17	·	·	·	6	·	·	2	4	19	16	2	·	·	7
VIII	4	4.0	6	1.8	10	2.4	26	2.1	13	2.7	10.5	2.9	8.5	3.2	7	4.1	8	2.4	97	39.5	26	·	·	·	9	·	·	1	9	12	9	3	·	·	·
IX	·	·	·	·	12	2.2	35.5	2.5	20.5	2.7	12.5	3.0	4.5	2.6	·	·	5	2.4	52	27.2	29	·	·	·	2	·	·	5	7	10	8	1	·	·	2
X	4.5	2.1	3	1.7	10	1.4	15.5	1.6	12	2.2	15.5	2.6	11	3.2	11.5	2.8	10	2.0	6	3.5	16	·	·	2	·	·	·	3	10	6	3	·	9	·	·
XI	·	·	7.5	3.1	19	2.6	18	3.2	10.5	2.6	21	2.9	7	2.9	·	·	7	2.6	32	7.1	21	6	11	18	·	·	·	·	24	14	8	·	9	16	·
XII	2	1.0	1	3.0	7.5	1.5	24.5	3.0	28	3.7	21	3.5	4	3.0	·	·	5	3.0	39	9.7	18	2	4	19	·	1	·	·	23	18	9	·	3	10	·
Rok	32.5	2.0	70.5	2.3	180.5	2.3	242.5	2.5	192	2.8	169	3.3	80.5	3.6	52.5	2.4	75	2.6	599	68.0	17.VII	23	47	109	21	4	·	18	163	164	104	10	36	91	15

Warszawa, Obserw. Astr. UW $H_s = 110$ m $H_b = 114,8$ m $h_w = 25$ m

I	4	1.5	5	1.4	8	1.8	9.5	1.9	12.5	2.3	19	2.5	18	1.8	6	4.4	11	1.9	33	5.3	20	3	4	26	·	·	·	—	—	16	11	·	7	26	—
II	8	3.5	13.5	2.6	3	2.3	·	·	6	4.2	16	3.8	14.5	4.1	21	3.9	2	3.5	33	5.8	7	8	21	26	·	1	·	—	—	18	12	·	1	28	—
III	4	3.5	7	2.3	2	2.5	11.5	1.9	21.5	2.3	13	3.8	15	3.7	11	3.5	8	2.7	16	3.9	3	4	5	16	·	1	·	—	—	11	6	·	6	16	—
IV	11	3.5	5.5	2.5	12	4.8	26	4.1	11	2.5	5	2.8	7	2.7	7.5	3.9	5	3.4	43	13.3	28	·	·	3	·	3	·	—	—	13	9	3	1	·	—
V	20.5	3.1	12	2.3	6	4.0	14	3.1	6.5	3.0	5.5	2.8	14	2.4	11.5	2.9	3	2.8	104	39.5	25	·	·	1	·	2	·	—	—	14	14	2	·	·	—
VI	9.5	1.6	10.5	2.7	14	2.9	5	3.0	5.5	2.7	10.5	3.3	14.5	3.7	13.5	3.9	7	2.8	76	22.3	14	·	·	·	5	·	·	—	—	13	11	1	·	·	—
VII	1	1.0	4	2.0	5.5	2.2	8.5	2.1	8.5	2.0	23	3.1	27.5	2.8	11	2.3	4	2.5	133	62.0	17	·	·	·	6	·	·	3	6	19	16	2	·	·	—
VIII	8.5	2.5	2	2.5	2	2.0	8	2.1	9	2.8	9	2.6	18.5	2.3	19	3.2	17	2.1	96	35.7	26	·	·	·	10	·	·	4	9	13	10	3	·	·	—
IX	·	·	·	·	·	·	14.5	1.9	18.5	1.7	18	1.8	16.5	2.4	10.5	2.5	12	1.7	52	26.3	29	·	·	·	2	·	·	10	3	10	8	1	·	·	—
X	13	2.3	2.5	2.0	1.5	1.3	10	1.8	6	1.2	12	3.7	20	4.4	21	3.0	7	2.8	7	3.6	16	·	·	2	·	1	·	6	5	5	3	·	7	·	—
XI	4	2.2	14	2.6	4.5	2.9	10.5	2.9	6.5	3.2	13	4.5	19	5.6	17.5	3.1	1	3.7	47	8.5	15	5	11	18	·	2	·	·	21	19	9	·	7	17	—
XII	5.5	2.5	1	1.0	·	·	6.5	2.3	24.5	3.5	35	4.4	6.5	3.2	13	2.8	1	3.5	56	15.8	18	2	4	19	·	3	1	·	19	17	12	1	3	12	—
Rok	89	2.3	77	2.0	58.5	2.2	124	2.3	136	2.6	179	3.3	191	3.3	162.5	3.3	78	2.8	696	62.0	17.VII	22	45	111	23	13	1	—	—	168	121	13	32	99	—

Warszawa, St. Pomp Rzecz. $H_s = 85$ m $h_w = 14$ m

I	6	1.9	4.5	2.9	6.5	2.7	20	2.6	12	2.6	19.5	2.4	9	3.9	6.5	5.5	9	2.6	27	4.7	20	3	4	26	·	1	·	·	21	15	11	·	5	26	·
II	15.5	3.8	6.5	4.1	3	3.0	2	1.0	3	1.5	15.5	3.2	22.5	4.2	11	3.3	5	3.3	25	4.5	7	7	22	26	·	·	·	1	15	18	9	·	1	28	·
III	2	2.8	1.5	1.3	4	1.8	14.5	3.0	15.5	1.8	15.5	2.7	25	3.0	6	3.5	9	2.4	14	4.7	3	4	6	17	·	·	·	—	—	12	5	·	4	17	·
IV	7	2.5	4.5	2.2	22.5	4.2	23	3.0	3	1.5	13	3.1	8.5	3.6	7.5	3.0	1	3.2	40	11.8	28	·	·	5	·	1	·	·	15	12	10	1	1	·	1
V	13.5	2.3	7.5	2.1	14.5	3.1	8.5	3.2	4.5	1.9	14	2.0	10	3.2	11.5	2.4	9	2.3	101	38.2	25	·	·	1	·	·	·	1	12	16	14	3	·	·	3
VI	7.5	1.3	12	2.5	10	3.4	5	2.4	1.5	3.0	11	2.1	23.5	2.3	13.5	1.6	6	2.1	69	21.1	14	·	·	·	6	·	·	6	8	13	11	1	·	·	2
VII	3	1.2	4.5	2.1	12	2.2	8.5	2.1	5	1.4	19.5	2.2	29	2.3	3.5	1.6	8	1.9	109	52.1	17	·	·	·	6	1	1	5	7	19	15	2	·	·	4
VIII	9	1.4	1.5	1.7	2.5	2.0	11.5	1.3	6	1.4	9.5	1.9	27.5	1.9	13.5	2.1	12	1.5	91	36.6	26	·	·	·	10	·	·	7	9	10	9	3	·	·	2
IX	·	·	·	·	2	1.6	20	2.2	8.5	1.6	19	1.8	22	2.2	4.5	2.0	14	1.7	57	34.0	29	·	·	·	3	·	·	7	1	10	8	1	·	·	2
X	7.5	1.9	1	1.5	3.5	2.1	6	2.0	4	1.1	13.5	1.8	24	3.0	15.5	2.7	18	1.9	7	3.8	16	·	·	3	·	·	·	5	11	5	3	·	8	·	·
XI	3	1.5	10.5	3.0	16	4.0	14.5	3.2	8	1.0	9	3.0	24.5	4.1	1.5	2.3	3	3.2	40	8.1	21	5	11	20	·	1	·	·	22	19	10	·	5	16	·
XII	2.5	1.4	3	2.3	5	1.5	12	2.0	13.5	2.8	30	2.8	15.5	2.8	6.5	2.4	5	2.4	59	12.9	18	2	4	21	·	1	·	·	20	18	10	1	·	14	·
Rok	76.5	1.8	67	2.1	101.5	2.6	145.5	2.3	84.5	1.8	189	2.4	241	3.0	101	2.7	99	2.4	639	52.1	17.VII	21	47	119	25	5	1	—	—	167	115	12	24	101	14

Warszawa - Okęcie φ = 52°09' λ = 20°59' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																				
	P_m	Max	Min	P_{sum}	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	998.8	1015.4	979.3	1012.4	1.0	−3.9	4.6	9	−13.6	11	−1.9	−0.4	−1.5	−1.3	4.9	5.2	5.1	5.1	90	87	90	89	0.5	0.8	0.6	0.6	7.6	8.1	6.9	7.5
II	1001.7	1020.3	978.1	1015.5	−2.1	−9.7	2.4	13, 14	−22.9	6	−7.1	−4.0	−5.9	−5.7	3.4	3.8	3.5	3.6	87	80	84	84	0.5	0.8	0.6	0.6	7.8	7.1	7.2	7.4
III	1003.5	1019.9	975.3	1017.0	4.9	−3.3	13.9	30	−14.8	9	−2.3	3.2	0.4	0.4	5.0	5.6	5.4	5.3	90	72	83	82	0.5	2.4	1.1	1.3	6.3	6.4	5.3	6.2
IV	998.2	1016.2	981.7	1011.4	10.6	2.4	15.7	29	−2.1	3	4.0	8.8	6.0	6.2	7.0	7.1	7.1	7.1	85	63	75	74	1.2	4.4	2.4	2.7	7.4	7.6	6.9	7.3
V	1000.8	1017.0	985.8	1013.8	14.2	5.1	20.5	17	−1.9	3	8.5	12.4	9.7	10.1	9.4	9.3	9.5	9.4	82	63	77	74	1.9	5.4	2.8	3.4	5.8	8.0	6.2	6.7
VI	1001.0	1009.4	991.9	1013.8	21.2	11.4	29.5	26	7.4	8, 15	14.6	19.3	15.5	16.2	13.4	13.3	13.7	13.5	80	61	77	73	3.3	9.7	4.2	5.7	5.3	6.6	5.4	5.8
VII	999.0	1009.4	985.1	1011.8	21.8	11.6	29.5	16	6.6	11	15.1	19.9	15.6	16.6	14.1	13.3	14.4	13.9	81	57	81	73	3.3	10.5	3.7	5.8	5.4	7.4	5.1	6.0
VIII	1002.4	1010.4	992.1	1015.2	21.4	10.7	30.6	7	6.0	31	13.3	19.5	15.0	15.7	13.6	13.4	13.9	13.6	88	60	81	76	2.0	10.3	3.7	5.3	5.3	6.4	5.2	5.6
IX	1002.4	1021.0	991.7	1015.2	21.0	9.2	26.8	2	3.7	21	11.4	19.2	13.7	14.5	12.5	13.6	13.5	13.2	92	61	85	79	1.2	9.2	2.5	4.3	6.0	5.6	3.6	5.1
X	1009.5	1024.7	995.7	1022.7	12.3	2.6	21.4	1	−5.0	22	4.5	11.3	6.4	7.2	8.1	9.2	8.9	8.7	94	68	90	84	0.5	4.5	1.0	2.0	6.2	6.4	4.5	5.7
XI	998.9	1016.3	972.1	1012.5	1.4	−3.6	12.3	2	−16.1	18	−2.1	−0.1	−1.1	−1.1	5.1	5.4	5.4	5.3	90	84	89	88	0.6	1.2	0.7	0.8	9.1	8.3	9.5	9.0
XII	992.9	1009.4	971.4	1006.3	2.5	−2.3	10.1	20	−18.6	17	−0.4	0.9	0.0	0.1	5.5	5.6	5.4	5.5	89	84	86	86	0.7	1.2	0.9	0.9	8.6	9.0	8.1	8.6
Rok	1000.8	1024.7	971.4	1014.0	10.8	2.5	30.6	7. VIII	−22.9	6. II	4.8	9.2	6.2	6.6	8.5	8.7	8.8	8.7	87	70	83	80	1.4	5.0	2.0	2.8	6.8	7.2	6.2	6.7

Jeziory φ = 52°16' λ = 16°48'

I	—	—	—	—	2.3	−2.2	6.4	1	−6.5	7	−0.6	1.6	−0.3	0.1	5.5	6.0	5.6	5.7	93	86	92	90	0.4	1.0	0.5	0.6	7.5	7.4	7.4	7.4
II	—	—	—	—	−0.4	−7.4	2.9	13	−16.7	6	−5.3	−1.3	−3.6	−3.4	3.8	4.2	4.2	4.1	90	74	88	84	0.4	1.5	0.5	0.8	7.3	6.3	6.8	6.8
III	—	—	—	—	6.2	−3.8	15.6	29	−19.5	8	−2.3	4.8	0.1	0.7	5.1	6.2	5.9	5.7	90	69	90	83	0.5	3.0	0.6	1.4	5.8	5.7	6.1	5.9
IV	—	—	—	—	11.4	2.7	16.9	4	−2.0	5	4.9	10.1	6.3	6.9	7.8	7.7	7.9	7.8	89	63	83	78	0.9	4.9	1.7	2.5	6.5	7.2	4.8	6.2
V	—	—	—	—	15.2	6.0	22.5	17	−0.7	2	9.3	13.8	9.9	10.7	10.0	10.2	9.8	10.0	84	65	79	76	1.8	5.9	2.7	3.5	6.6	7.0	5.6	6.4
VI	—	—	—	—	21.5	11.1	31.6	26	5.8	3	15.4	20.1	15.0	16.4	13.6	13.7	14.2	13.8	77	59	82	73	4.2	10.5	3.1	5.9	4.5	5.9	4.0	4.8
VII	—	—	—	—	20.7	11.7	30.1	14	5.4	5	14.8	18.9	14.9	15.9	14.2	14.3	15.1	14.5	84	66	87	79	2.8	8.3	2.3	4.5	5.7	6.4	5.4	5.8
VIII	—	—	—	—	21.7	10.1	29.7	6	5.5	31	13.5	20.5	14.2	15.6	13.9	14.0	14.1	14.0	89	58	86	78	1.8	10.8	2.5	5.0	3.8	6.0	3.6	4.5
IX	—	—	—	—	20.4	9.8	27.3	3	4.1	21	11.7	19.3	13.2	14.4	12.3	13.4	13.4	13.0	90	60	88	79	1.7	9.6	2.0	4.4	4.2	4.6	3.0	3.9
X	—	—	—	—	13.4	3.5	22.5	1	−3.5	23	4.7	12.6	6.6	7.6	8.4	10.1	9.3	9.3	94	69	92	85	0.5	4.9	0.8	2.1	5.0	4.2	2.7	4.0
XI	—	—	—	—	2.0	−3.1	12.9	2	−15.0	17	−1.6	0.9	−0.5	−0.4	5.3	6.0	5.6	5.6	90	85	89	88	0.6	1.1	0.8	0.8	8.3	8.9	7.3	8.2
XII	—	—	—	—	3.6	−1.2	11.9	19	−8.0	17	0.3	2.2	1.2	1.2	5.7	6.2	6.2	6.0	89	85	90	88	0.7	1.1	0.7	0.8	8.3	7.0	7.0	7.4
Rok	—	—	—	—	11.5	3.1	31.6	26. VI	−19.5	8. III	5.4	10.3	6.4	7.1	8.8	9.3	9.3	9.1	88	70	87	82	1.4	5.2	1.5	2.7	6.1	6.4	5.3	5.9

Świebodzin φ = 52°15' λ = 15°32'

I	—	—	—	—	3.1	−1.0	8.3	17	−5.4	7	0.3	2.2	0.6	0.9	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.6	7.3	7.5
II	—	—	—	—	0.4	−6.0	4.3	13	−15.6	6	−4.2	−1.0	−2.9	−2.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.0	7.2	7.7
III	—	—	—	—	6.7	−4.3	15.6	29	−20.6	8	−2.6	5.5	−0.2	0.6	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.4	4.5	5.5
IV	—	—	—	—	12.4	3.0	18.2	6	−1.0	5	5.0	10.8	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.5	5.3	6.0
V	—	—	—	—	16.5	6.5	23.3	17	0.5	2, 3	10.0	14.7	10.2	11.3	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.9	5.2	5.9
VI	—	—	—	—	22.7	10.9	30.3	26	6.2	3	15.2	20.6	15.1	16.5	—	—	—	—	—	—	—	—	—	—	—	—	5.0	6.7	5.6	5.8
VII	—	—	—	—	21.2	11.6	33.0	14	6.1	5	14.3	19.3	14.8	15.8	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.6	5.7	6.7
VIII	—	—	—	—	22.3	9.7	30.5	6	6.2	31	13.8	20.7	14.1	15.7	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.3	3.2	4.7
IX	—	—	—	—	20.3	8.8	26.8	2	3.7	21	11.4	19.1	12.3	13.8	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.8	4.3	5.5
X	—	—	—	—	14.1	2.9	23.5	1	−4.4	23	4.8	12.8	6.4	7.6	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.1	3.1	4.9
XI	—	—	—	—	3.0	−2.7	13.5	1	−14.5	23	−0.8	1.7	−0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.9	7.0	7.9
XII	—	—	—	—	4.5	−0.5	12.9	19	−8.9	14	1.1	3.1	1.9	2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.6	7.7	8.3
Rok	—	—	—	—	12.3	3.2	33.0	14. VII	−20.6	8. III	5.7	10.8	6.6	7.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.0	5.5	6.4

Zbąszyń φ = 52°15' λ = 15°56'

I	—	—	—	—	2.9	−0.9	8.4	17	−5.9	7	0.3	2.5	0.7	1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.1	8.4	7.9	8.1
II	—	—	—	—	0.2	−5.6	3.8	13	−15.0	6	−4.2	−0.7	−2.5	−2.5	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.9	8.5	8.1
III	—	—	—	—	6.1	−4.0	14.9	29	−20.1	8	−2.7	5.3	0.4	0.8	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.6	5.9	5.7
IV	—	—	—	—	12.2	3.3	17.7	6	−1.3	5	5.0	10.7	6.7	7.3	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.7	6.7	6.8
V	—	—	—	—	15.9	6.5	22.6	17	−1.0	2	9.6	14.3	10.5	11.2	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.4	6.7	6.7
VI	—	—	—	—	22.1	11.2	31.2	26	5.6	3	15.0	20.5	16.0	16.9	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.9	6.7	6.1
VII	—	—	—	—	21.0	12.0	31.9	14	6.0	5	14.6	19.1	15.6	16.2	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.6	7.2	6.9
VIII	—	—	—	—	21.9	10.2	29.9	6	6.0	13, 17	13.0	20.6	14.9	15.8	—	—	—	—	—	—	—	—	—	—	—	—	3.4	6.3	4.1	4.6
IX	—	—	—	—	20.2	9.1	27.0	2	2.9	21	11.1	18.8	13.0	14.0	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.4	4.4	5.1
X	—	—	—	—	13.7	2.8	23.3	1	−4.7	23	4.1	12.5	6.6	7.4	—	—	—	—	—	—	—	—	—	—	—	—	4.8	5.2	3.9	4.6
XI	—	—	—	—	2.7	−3.0	13.5	1	−16.1	23	−1.3	1.6	−0.5	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.2	7.7	8.1
XII	—	—	—	—	3.9	−0.6	12.6	19	−6.9	15	0.7	2.6	1.6	1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.1	8.7	8.4
Rok	—	—	—	—	11.9	3.4	31.9	14. VII	−20.1	8. III	5.4	10.6	6.9	7.4	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.1	6.5	6.5

Warszawa - Okęcie

$H_s = 106\ m$ $H_b = 106{,}9\ m$ $h_w = 10{,}8\ m$ **1965**

MIESIĄC	ROZKŁAD WIATRU n:V>n N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◷	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	3.5	5.7	2	4.2	12.5	4.2	21	4.2	11.5	3.7	17	5.7	9.5	6.1	10	5.6	6	4.5	18	3.3	8	3	7	27	·	3	·	·	17	17	6	·	8	17	·
II	12.5	6.6	6.5	5.6	2	5.8	1.5	2.0	4	5.8	19.5	5.9	31.5	6.0	5.5	7.7	1	6.0	10	2.0	13	10	22	27	·	5	·	1	14	21	3	·	2	28	·
III	1.5	3.0	5	5.0	12.5	3.7	24.5	2.9	13	3.0	12.5	5.5	14	5.6	7	6.9	3	4.1	10	2.0	2, 3	4	8	22	·	3	·	5	13	13	4	·	6	17	·
IV	3.5	4.9	12.5	5.4	31	5.6	16	4.3	3.5	3.3	7	5.3	8.5	5.3	6	5.5	2	5.0	41	15.4	28	·	·	5	·	2	·	·	11	13	8	1	1	·	2
V	8.5	5.1	9	4.6	16	5.0	9	3.4	4.5	2.7	10	4.4	17.5	4.6	16.5	4.8	2	4.4	78	16.4	25	·	·	3	·	·	·	2	11	16	12	4	4	·	4
VI	3.5	3.6	10.5	5.6	13.5	4.9	6	4.2	5.5	2.7	14	4.8	24	5.3	9	4.0	4	4.5	60	23.1	14	·	·	·	3	1	·	1	8	13	10	1	·	·	5
VII	2	2.0	5.5	5.5	10	3.4	7.5	3.6	10	3.8	27.5	4.7	26.5	5.3	2	3.2	2	4.4	111	60.3	17	·	·	·	6	1	·	1	5	19	17	1	1	·	9
VIII	3.5	4.9	1.5	2.7	5	3.1	14	3.5	7	3.6	13	3.7	24.5	4.6	15.5	4.4	9	3.6	92	39.2	26	·	·	·	10	·	·	2	7	11	9	3	1	·	2
IX	·	·	1	3.5	13	2.8	24	3.6	11.5	3.6	20.5	4.4	16	4.7	·	·	4	3.7	45	25.1	29	·	·	·	2	·	·	6	4	11	8	1	6	·	2
X	4	3.2	3.5	3.9	8.5	3.1	7.5	2.6	9.5	2.5	9.5	4.3	33.5	4.5	12	3.8	5	3.6	4	3.3	16	·	·	6	·	·	·	3	4	6	1	·	13	·	·
XI	2	3.5	14.5	6.1	11.5	4.8	13.5	4.9	6.5	3.7	12.5	6.2	25	5.3	0.5	2.0	4	5.0	26	6.5	21	6	11	18	·	1	·	·	23	19	7	·	10	17	·
XII	1.5	2.0	2	3.0	6.5	3.5	11.5	5.2	18	4.8	27.5	6.0	19	5.2	5	4.0	2	5.0	50	15.4	18	2	4	20	·	2	·	·	22	20	10	1	4	14	·
Rok	46	3.7	73.5	4.6	142	4.2	156	3.7	104.5	3.6	190.5	5.1	249.5	5.2	89	4.3	44	4.5	545	60.3	17. VII	25	52	128	21	18	·	21	139	179	95	12	56	93	24

Uwaga. Kierunki i prędkości wiatru - wg anemometru M-49.

Jeziory

$H_s = 84\ m$ $h_w = 15\ m$

I	4	1.0	5	1.0	6	1.7	27	1.1	3	1.0	35	1.3	7	1.1	5	1.6	1	1.2	47	9.2	17	·	3	28	·	·	·	1	17	16	14	·	11	20	·
II	4	1.8	11	1.5	3	2.0	6	1.3	·	·	25	1.8	18	1.3	15	2.0	2	1.6	26	7.5	8	8	16	26	·	·	·	2	13	22	5	·	2	28	·
III	2	1.0	14	1.7	2	2.5	10	1.5	1	1.0	40	1.1	10	1.4	13	1.5	1	1.3	54	25.0	3	5	6	22	·	·	·	9	13	12	8	2	11	21	·
IV	3	1.0	10	1.9	10	2.7	25	1.6	4	1.2	21	1.4	2	1.0	14	1.2	1	1.6	60	15.7	19	·	·	7	·	·	·	6	11	12	10	3	1	·	1
V	2	1.0	18	1.6	7	1.3	14	2.0	1	1.0	21	1.5	4	1.8	24	1.2	2	1.5	87	11.6	10	·	·	1	·	·	·	4	12	21	16	4	8	·	2
VI	1	1.0	11	1.9	5	1.4	12	1.4	2	1.0	35	1.3	10	1.5	11	1.2	3	1.3	68	11.4	30	·	·	·	5	·	·	7	6	15	12	1	1	·	4
VII	·	·	9	1.2	1	2.0	9	1.2	2	2.0	48	1.4	14	1.9	9	1.2	1	1.4	91	25.2	16	·	·	·	3	·	·	3	5	21	18	2	4	·	7
VIII	2	1.0	·	·	·	·	8	1.1	6	1.0	37	1.1	17	1.2	19	1.2	4	1.1	17	6.0	25	·	·	·	8	·	·	8	4	11	5	·	4	·	·
IX	·	·	2	1.5	2	2.0	11	1.6	12	1.1	25	1.2	13	1.6	·	·	25	1.0	46	16.8	10	·	·	·	2	·	·	7	2	6	5	2	3	·	·
X	2	1.0	6	1.0	3	1.3	14	1.1	1	1.0	43	1.1	6	1.7	7	1.0	11	1.0	10	6.1	16	·	·	6	·	·	·	10	2	3	3	·	14	·	·
XI	2	1.5	10	2.4	12	2.1	16	1.4	3	1.7	29	1.7	7	1.4	5	1.2	6	1.6	42	14.5	21	6	12	19	·	·	·	2	20	17	7	1	7	15	·
XII	1	1.0	1	1.0	1	1.0	16	1.5	4	1.8	56	1.7	7	1.6	7	1.0	·	1.5	44	8.9	18	·	2	18	·	·	·	1	15	22	14	·	7	8	·
Rok	23	0.9	97	1.4	52	1.7	168	1.4	39	1.2	415	1.4	115	1.5	129	1.2	57	1.3	592	25.2	16. VII	19	39	127	18	·	·	60	120	178	117	15	73	92	14

Świebodzin

$H_s = 78\ m$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39	9.6	17	·	1	22	·	—	—	2	17	15	10	·	2	9	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	23	4.0	27	3	14	26	·	—	—	2	16	17	12	·	3	26	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	43	18.4	3	8	6	21	·	—	—	8	11	11	8	1	5	17	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40	7.2	13	·	·	2	·	—	—	5	9	17	10	·	·	·	1
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	102	17.7	5	·	·	·	·	—	—	6	11	18	15	4	2	·	2
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	64	15.2	1	·	·	·	8	—	—	3	9	9	8	2	·	·	2
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	136	29.7	16	·	·	·	4	—	—	1	12	21	17	5	3	·	6
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	28	15.0	23	·	·	·	8	—	—	2	3	11	7	1	3	·	1
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	54	22.0	10	·	·	·	3	—	—	4	7	9	8	2	5	·	3
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	19	9.3	16	·	·	8	·	—	—	6	4	3	3	·	10	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	45	13.9	27	4	11	17	·	—	—	1	17	14	10	1	4	17	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	62	17.3	18	·	2	17	·	—	—	·	20	16	14	1	2	12?	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	655	29.7	16. VII	15	34	113	23	—	—	40	136	161	122	17	39	81?	15

Zbąszyń

$H_s = 57\ m$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	32	7.0	9	·	1	23	·	—	—	2	20	13	9	·	1	6	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	20	3.6	26	4	15	26	·	—	—	·	20	19	6	·	1	25	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	45	14.0	3	8	6	21	·	—	—	11	13	10	7	2	9	18	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	28	6.7	13	·	·	3	·	—	—	5	15	14	8	·	·	·	·
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	89	16.2	26	·	·	1	·	—	—	3	15	19	17	2	·	·	2
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39	14.2	30	·	·	·	6	—	—	3	10	9	5	2	·	·	5
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	104	42.8	16	·	·	·	4	—	—	2	13	18	15	2	·	·	8
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	28	13.0	23	·	·	·	8	—	—	3	2	10	7	1	·	·	2
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	52	16.9	10	·	·	·	3	—	—	5	7	9	9	2	2	·	1
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	12	6.3	31	·	·	8	·	—	—	7	4	2	2	·	10	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	42	10.1	27	5	11	17	·	—	—	1	18	12	9	1	4	14	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	42	10.7	18	·	3	19	·	—	—	·	18	22	13	1	·	6	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	533	42.8	16. VII	17	36	118	21	—	—	43	155	157	107	13	27	69	18

Kórnik

φ = 52°15′ λ = 17°06′ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.0	−2.5	6.6	1	−7.0	27	−0.8	1.1	−0.5	−0.2	5.5	5.7	5.5	5.6	94	86	93	91	0.3	1.0	0.4	0.6	7.9	7.4	6.9	7.4
II	–	–	–	–	−0.7	−7.4	3.4	13	−16.8	6	−5.4	−2.1	−4.0	−3.9	3.8	3.9	4.1	3.9	83	74	87	83	0.4	1.4	0.6	0.8	7.4	6.8	7.0	7.1
III	–	–	–	–	5.3	−4.0	14.8	29	−22.8	9	−3.2	3.8	−0.4	0.0	5.0	5.7	5.4	5.4	91	69	85	82	0.5	2.9	1.0	1.5	6.3	5.6	5.1	5.7
IV	–	–	–	–	11.1	2.9	15.8	6	−1.1	5	4.4	9.9	6.0	6.6	7.5	7.2	7.8	7.5	89	60	83	77	0.9	5.0	1.6	2.5	6.7	7.5	4.8	6.3
V	–	–	–	–	14.9	6.1	22.3	17	−1.0	3	8.6	13.3	9.7	10.3	9.8	9.7	9.4	9.6	86	63	77	75	1.5	5.9	2.9	3.4	6.8	7.1	6.7	6.9
VI	–	–	–	–	21.4	11.2	32.3	26	7.1	3	14.7	20.2	15.5	16.5	12.9	12.6	13.6	13.0	77	54	77	69	4.1	11.8	4.2	6.7	4.9	6.0	5.1	5.3
VII	–	–	–	–	20.9	11.7	30.7	14	5.6	5	14.4	18.8	15.3	16.0	13.7	13.5	14.6	13.9	82	63	82	76	2.9	8.8	3.2	5.0	6.4	6.3	7.0	6.6
VIII	–	–	–	–	21.8	10.3	30.4	6	1.5	17	13.4	20.3	15.1	16.0	13.4	12.3	13.9	13.2	87	55	81	74	2.2	12.4	3.7	6.1	3.8	4.9	3.6	4.1
IX	–	–	–	–	20.5	9.6	28.1	3	4.7	16	11.4	19.2	13.2	14.2	12.2	12.0	13.0	12.4	90	55	85	77	1.5	10.9	2.4	4.9	4.3	4.6	3.7	4.2
X	–	–	–	–	13.5	3.1	22.7	1	−4.0	23	4.5	12.0	6.5	7.4	8.1	9.5	9.1	8.9	93	67	91	84	0.7	5.0	0.9	2.2	5.3	4.4	2.9	4.2
XI	–	–	–	–	2.0	−3.7	13.4	1	−16.9	24	−1.9	0.7	−1.1	−0.8	5.2	5.6	5.3	5.4	90	81	86	86	0.6	1.4	0.9	1.0	8.4	9.0	7.1	8.2
XII	–	–	–	–	3.4	−1.4	12.5	19	−9.3	17	0.3	2.0	1.0	1.1	5.6	5.7	5.9	5.7	88	80	88	85	0.8	1.5	0.8	1.0	8.6	7.6	7.5	7.9
Rok	–	–	–	–	11.3	3.0	32.3	26.VI	−22.8	9.III	5.0	9.9	6.4	6.9	8.6	8.6	9.0	8.7	88	67	85	80	1.4	5.7	1.9	3.0	6.4	6.4	5.6	6.1

Sinołęka

φ = 52°13′ λ = 21°55′

I	–	–	–	–	0.1	−5.0	3.6	9	−17.8	11	−3.3	−1.5	−2.2	−2.3	4.4	4.8	4.7	4.6	88	86	88	87	0.5	0.7	0.6	0.6	7.5	8.2	6.5	7.4
II	–	–	–	–	−3.1	−10.2	2.2	14	−21.8	6	−7.6	−4.7	−6.8	−6.5	3.3	3.7	3.3	3.4	88	81	84	84	0.4	0.8	0.5	0.6	8.4	7.1	5.8	7.1
III	–	–	–	–	3.8	−4.3	12.3	30	−19.0	9	−3.2	2.2	−0.3	−0.4	4.8	5.6	5.3	5.2	90	76	84	83	0.5	1.8	0.9	1.1	7.7	6.4	5.8	6.6
IV	–	–	–	–	10.1	1.8	14.3	30	−2.5	3	3.2	8.7	5.3	5.6	7.0	7.1	7.2	7.1	88	63	79	77	0.9	4.4	1.9	2.4	8.2	7.9	6.2	7.4
V	–	–	–	–	13.7	4.8	20.8	18	−2.8	4	8.0	12.4	9.2	9.7	9.2	8.9	9.6	9.2	83	61	80	75	1.8	5.8	2.3	3.3	6.3	7.5	6.9	6.9
VI	–	–	–	–	20.4	10.9	29.0	26	5.2	8	14.3	18.6	14.9	15.7	13.6	13.7	13.8	13.7	83	65	81	76	2.9	8.3	3.3	4.8	5.7	6.7	5.9	6.1
VII	–	–	–	–	21.5	10.8	29.7	16	3.3	5	14.8	19.7	15.1	16.2	14.1	13.3	14.3	13.9	83	60	83	75	3.0	10.3	3.2	5.5	4.8	7.2	5.5	5.8
VIII	–	–	–	–	20.7	10.5	29.9	7	5.7	16	12.9	18.7	14.4	15.1	13.3	12.6	13.8	13.2	83	60	83	77	1.7	9.9	3.1	4.9	6.0	5.8	4.1	5.3
IX	–	–	–	–	20.7	9.0	27.4	3	4.0	21	10.7	19.2	13.6	14.3	12.2	12.8	13.5	12.8	93	58	86	79	1.0	10.0	2.4	4.5	4.4	5.5	2.5	4.1
X	–	–	–	–	11.7	3.2	20.2	1	−5.1	22	4.5	10.5	6.6	7.0	7.9	9.2	8.8	8.6	92	72	88	84	0.7	3.8	1.2	1.9	7.2	6.8	5.4	6.5
XI	–	–	–	–	0.5	−3.8	11.2	2	−18.8	17	−2.1	−0.9	−1.9	−1.7	5.0	5.2	5.1	5.1	88	86	88	87	0.7	1.0	0.7	0.8	9.3	9.1	9.1	9.2
XII	–	–	–	–	1.3	−2.9	9.0	20	−17.8	17	−1.1	0.1	−0.6	−0.6	5.2	5.4	5.2	5.3	89	85	87	87	0.7	1.0	0.8	0.8	8.9	9.1	7.4	8.5
Rok	–	–	–	–	10.1	2.1	29.9	7.VIII	−21.8	6.II	4.3	8.6	5.6	6.0	8.3	8.5	8.7	8.5	88	71	84	81	1.2	4.8	1.7	2.6	7.0	7.3	5.9	6.7

Pętkowo

φ = 52°12′ λ = 17°15

I	–	–	–	–	1.8	−2.0	6.4	1	−6.9	27	−0.7	1.2	−0.2	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	6.2	7.1
II	–	–	–	–	−0.9	−7.7	2.9	13	−15.6	6	−5.1	−2.2	−3.9	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	6.9	7.4
III	–	–	–	–	5.2	−4.0	14.7	29	−22.3	9	−2.6	4.0	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.2	5.1	5.6
IV	–	–	–	–	11.2	2.7	15.4	6	−1.1	3	5.0	10.1	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	4.9	6.4
V	–	–	–	–	14.6	6.0	21.9	17	−1.1	3	8.8	13.1	10.0	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.3	6.6	6.8
VI	–	–	–	–	21.3	10.5	31.2	26	5.7	3	15.0	19.8	15.4	16.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	6.3	5.9	5.6
VII	–	–	–	–	20.9	11.1	30.4	14	4.3	5	14.8	19.1	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.6	5.7	6.1
VIII	–	–	–	–	21.8	10.0	30.7	6	5.6	14, 31	13.6	20.1	15.4	16.1	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.4	4.5	4.8
IX	–	–	–	–	20.8	9.4	28.3	3	4.2	16, 21	11.5	19.3	14.1	14.8	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	3.2	4.5
X	–	–	–	–	13.4	2.8	23.2	1	−4.9	22	4.4	12.2	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.3	2.4	4.0
XI	–	–	–	–	1.9	−3.9	12.8	2	−18.5	23	−1.8	0.7	−1.0	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.1	7.1	8.0
XII	–	–	–	–	3.1	−1.3	12.1	19	−9.4	17	0.1	2.1	1.0	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.3	6.9	7.6
Rok	–	–	–	–	11.3	2.8	31.2	26.VI	−22.3	9.III	5.2	10.0	6.6	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	5.4	6.1

Koło

φ = 52°12′ λ = 18°38′

I	–	–	–	–	1.8	−2.7	5.3	9	−9.7	11	−1.2	1.1	−0.7	−0.4	5.3	5.7	5.3	5.4	93	86	91	90	0.4	1.0	0.5	0.6	7.8	8.0	7.2	7.7
II	–	–	–	–	−1.8	−9.0	2.7	13	−19.7	6	−6.5	−3.1	−5.3	−5.0	3.6	4.1	3.9	3.9	91	83	89	88	0.3	0.8	0.4	0.5	8.4	8.0	7.1	7.8
III	–	–	–	–	5.6	−3.5	13.3	29	−20.0	9	−2.5	4.0	0.3	0.5	5.2	6.0	5.8	5.7	92	72	87	83	0.4	2.6	0.9	1.3	7.0	6.2	5.1	6.1
IV	–	–	–	–	10.8	2.8	15.7	30	−1.1	5	4.1	9.3	5.8	6.2	7.3	7.8	7.8	7.6	88	67	83	79	1.0	4.1	1.6	2.2	7.4	7.6	4.4	6.5
V	–	–	–	–	14.5	5.8	22.0	17	−0.7	3	8.5	12.9	9.6	10.2	9.7	9.7	9.7	9.7	85	66	80	77	1.6	5.4	2.5	3.2	6.9	8.1	6.0	7.0
VI	–	–	–	–	21.7	11.0	32.4	26	6.8	7, 15	14.5	20.0	15.6	16.4	13.4	13.3	14.2	13.6	81	58	79	73	3.3	10.7	3.8	5.9	5.5	6.4	6.1	6.0
VII	–	–	–	–	21.6	11.7	31.4	14	6.9	4	14.5	20.0	15.2	16.2	14.4	14.5	14.6	14.5	86	61	83	77	2.4	9.6	3.0	5.0	6.6	7.4	5.7	6.6
VIII	–	–	–	–	22.1	10.6	30.6	7	5.8	17	13.0	20.5	14.9	15.8	13.4	13.2	14.2	13.6	89	56	83	76	1.8	12.0	3.1	5.6	5.6	6.7	4.3	5.5
IX	–	–	–	–	21.1	9.3	29.9	3	2.8	16	11.0	19.5	13.3	14.3	12.3	13.3	13.3	13.0	92	59	87	79	1.2	10.1	2.2	4.5	5.3	5.6	3.2	4.7
X	–	–	–	–	12.7	2.9	22.1	1	−5.6	22	4.3	11.7	6.3	7.2	8.1	9.9	9.0	9.0	96	71	92	86	0.4	4.2	0.8	1.8	6.1	6.0	3.5	5.2
XI	–	–	–	–	1.8	−3.8	12.3	2	−16.1	17	−2.3	0.5	−0.9	−0.9	5.1	5.6	5.4	5.4	92	84	88	88	0.5	1.2	0.8	0.8	8.6	8.2	7.6	8.1
XII	–	–	–	–	2.8	−1.6	10.6	19	−16.4	17	0.2	1.7	0.3	0.6	5.6	5.8	5.7	5.7	88	82	88	86	0.8	1.3	0.8	1.0	8.4	8.1	8.0	8.2
Rok	–	–	–	–	11.2	2.8	32.4	25.VI	−20.0	9.III	4.8	9.8	6.2	6.8	8.6	9.1	9.1	8.9	89	70	86	82	1.2	5.2	1.7	2.7	7.0	7.2	5.7	6.6

Kórnik $H_s = 77\,m$ $h_w = 16\,m$ 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4	4.0	4.5	2.1	4	2.8	16.5	2.9	11.5	3.9	20.5	3.2	16	3.8	6	3.3	10	3.0	32	7.0	17	·	3	28	·	2	·	2	16	16	9	·	4	19	·
II	11	5.4	6	6.1	4	4.2	2	3.0	1	6.5	20.5	5.3	21	3.4	10.5	5.9	8	4.4	13	3.0	26	8	17	27	·	3	·	2	13	18	4	·	1	28	·
III	10	3.8	4	4.8	2.5	2.0	12	2.4	12.5	2.1	10.5	2.8	19.5	4.1	6	3.8	16	2.7	33	12.7	3	6	7	21	·	·	·	9	12	12	7	1	5	17²	·
IV	5.5	3.2	5	6.3	19	5.8	17	3.0	5	4.7	11	4.0	8	3.6	5.5	3.9	14	3.6	41	10.7	28	·	·	2	·	2	·	5	12	15	9	1	1	·	1
V	8	3.8	5.5	4.8	17	4.2	11.5	3.8	3.5	1.9	10.5	3.0	11.5	2.6	11.5	3.6	14	3.0	93	18.0	10	·	·	2	·	2	1	4	14	19	15	4	2	·	1
VI	3.5	3.4	10.5	4.6	9.5	3.6	11	2.2	2	3.0	19	3.1	14.5	4.0	7	3.0	13	2.9	52	9.1	9	·	·	·	6	·	·	5	8	14	8	·	·	·	4
VII	4	4.1	4	3.8	5.5	2.4	4.5	1.8	8.5	2.3	34.5	3.4	21.5	3.6	4.5	2.9	6	3.0	130	32.3	15	·	·	·	4	·	·	2	10	19	14	2	·	·	7
VIII	·	·	1	1.0	1	3.0	8	1.8	14.5	3.0	14.5	2.4	15.5	2.8	2.5	3.4	36	1.6	24	10.1	4	·	·	·	8	·	·	8	1	11	5	1	1	·	1
IX	0.5	8.0	·	·	5.5	3.7	10.5	3.7	10	2.9	14.5	3.3	21.5	3.4	0.5	8.0	27	2.4	38	20.7	10	·	·	·	4	2	·	7	2	10	6	1	1	·	·
X	2.5	2.6	5	2.0	15	2.3	4	1.8	4.5	3.0	10.5	3.6	14	2.7	7.5	2.3	30	1.8	12	5.2	16	·	·	8	·	·	·	9	3	4	3	·	9	·	·
XI	3	2.0	15.5	3.6	9	4.2	8.5	4.3	6	4.7	23	4.7	6.5	6.0	3.5	2.7	15	3.5	28	6.5	27	6	12	18	·	3	·	·	18	15	8	·	8	16	·
XII	·	·	1	2.0	4.5	2.4	12.5	3.5	13.5	5.0	36	4.3	12.5	4.2	2	1.0	11	3.6	57	11.5	18	·	4	19	·	2	·	·	15	22	14	2	1	9	·
Rok	52	3.4	62	3.4	96.5	3.4	118	2.8	92.5	3.6	225	3.6	182	3.6	67	3.6	200	3.0	553	32.3	15.VII	20	43	125	22	16	1	53	124	175	102	12	33	89²	14

Sinołęka $H_s = 160\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6.5	2.1	6	2.2	5	2.2	20.5	2.9	18.5	3.0	12.5	2.2	8.5	4.2	5.5	6.8	10	2.7	28	5.5	23	3	10	27	·	2	·	2	17	14	8	·	5	29	·
II	14.5	3.8	6.5	3.7	2	2.0	·	·	5	4.4	10	4.6	24	3.7	15	4.4	7	3.7	14	3.6	13	11	23	28	·	3	·	2	14	15	5	·	1	28	·
III	1	2.5	8.5	2.1	3.5	1.7	13	2.6	17	1.9	11.5	2.8	12.5	2.6	10	4.6	16	2.2	21	5.5	17	5	8	24	·	1	·	4	16	13	7	·	6	18	·
IV	7	2.6	5	3.4	24	5.2	27.5	3.9	5.5	2.2	7	2.1	5	2.3	6	4.2	3	3.7	41	11.9	23	·	·	10	·	1	·	·	12	11	6	2	1	·	·
V	12.5	2.4	11.5	1.6	16.5	3.0	4.5	4.0	3.5	2.6	8	2.6	12	2.1	13.5	3.7	11	2.4	92	30.4	29	·	·	3	·	·	·	2	11	13	10	3	·	·	3
VI	10	1.9	9	2.9	10	3.2	8	2.8	2.5	3.2	10.5	2.6	19	3.0	15	2.3	6	2.5	45	9.8	14	·	·	·	5	·	·	2	10	10	8	·	·	·	1
VII	·	·	8	2.2	3.5	3.1	5	1.8	10.5	2.1	19	2.3	26	2.7	6	2.7	15	2.0	136	87.3	17	·	·	·	5	1	1	3	6	14	13	1	·	·	3
VIII	6.5	3.5	1	3.0	2	2.0	16.5	2.5	3	2.2	4.5	1.8	14.5	2.4	25	3.4	20	2.2	95	33.2	26	·	·	·	8	·	·	6	9	11	8	4	·	·	3
IX	·	·	·	·	3	1.3	23	2.2	11.5	2.1	14.5	2.1	14.5	2.4	7.5	1.9	16	1.8	21	10.7	29	·	·	·	4	·	·	9	2	8	5	1	·	·	·
X	6.5	2.2	2.5	1.6	5.5	1.9	2.5	3.0	10	1.9	9	2.7	21.5	2.9	19.5	2.8	16	2.1	5	3.1	16	·	·	5	·	·	·	3	8	4	2	·	8	·	·
XI	2	1.5	11.5	3.9	7.5	2.5	15	2.8	8.5	3.4	12	3.6	19	3.3	5.5	1.6	9	2.8	36	7.2	30	6	12	20	·	·	·	·	25	16	8	·	7	17	·
XII	2.5	1.2	·	·	2	2.0	13.5	2.7	23	3.6	19.5	3.1	23	2.5	5.5	2.4	4	2.8	68	27.4	18	2	7	23	·	2	·	·	18	19	11	1	·	14	·
Rok	69	2.0	69.5	2.2	84.5	2.5	149	2.6	118.5	2.7	138	2.7	199.5	2.8	134	3.4	133	2.6	602	87.3	17.VII	27	60	140	22	10	1	33	148	148	91	12	28	106	10

Pętkowo $H_s = 86\,m$ $h_w = 17.5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8.5	3.0	4.5	4.1	22.5	3.1	9.5	4.2	8.5	6.1	21	4.0	8	6.2	10.5	3.5	·	4.0	22	5.8	16	·	6	26	·	2	2	2	13	13	6	·	—	9	·
II	10	3.8	11.5	6.2	1	3.0	5	2.6	·	·	10.5	5.8	25	5.2	20	6.0	1	6.2	11	2.3	27	9	19	26	·	4	2	2	15	15	4	·	—	28	·
III	4	4.0	8.5	5.5	10	2.6	14.5	2.9	6	2.7	12	3.2	15.5	7.5	22.5	4.6	·	4.3	23	8.5	3	6	8	21	·	5	1	6	13	11	5	·	—	16	·
IV	6	4.3	26	6.4	13	5.2	8	5.8	4	6.8	6.5	4.0	16	3.8	11.5	5.3	·	5.3	36	10.5	28	·	·	5	·	3	3	4	12	13	9	1	—	·	2
V	12	3.2	25	5.2	10.5	8.0	2	6.0	1	2.0	5.5	3.7	16	6.1	20	3.7	1	4.9	99	19.9	19	·	·	2	·	4	3	2	13	18	15	4	—	·	1
VI	3.5	3.9	19.5	6.1	4.5	5.2	6	3.5	5	6.2	9	6.0	20.5	4.7	20	4.4	2	5.0	44	13.3	1	·	·	·	5	4	2	5	8	9	7	1	—	·	3
VII	4	4.0	4.5	5.9	6.5	5.8	4	4.2	6.5	4.3	25.5	4.8	29.5	5.1	10.5	4.3	2	4.7	124	39.5	15	·	·	·	3	3	·	3	9	20	16	4	—	·	7
VIII	9	2.7	3	3.7	·	·	11	4.6	5	2.6	12	4.3	16	3.3	34	3.5	3	3.5	36	11.0	4	·	·	·	8	·	·	5	4	13	8	1	—	·	·
IX	·	·	2.5	3.8	9	5.2	10.5	3.6	12	5.1	23.5	4.0	27	3.9	5.5	4.3	·	4.2	34	21.2	10	·	·	·	4	3	·	7	2	5	5	1	—	·	·
X	2.5	2.6	16	2.7	9.5	2.8	2.5	4.2	2.5	4.2	12.5	4.2	18	4.0	22.5	2.9	7	3.1	9	4.3	16	·	·	7	·	·	·	9	5	4	3	·	—	·	·
XI	1.5	1.7	29.5	6.5	2	3.5	4.5	6.3	5.5	7.0	16.5	7.9	16.5	5.0	12	2.8	2	5.7	26	5.9	27	6	12	19	·	5	1	1	17	11	8	·	—	14	·
XII	·	·	8.5	3.7	3	4.8	9	4.3	8.5	8.2	34.5	6.8	18	5.3	8.5	2.9	3	5.5	33	13.7	18	·	3	19	·	5	4	·	16	13	8	1	—	4	·
Rok	61	2.8	158	5.0	91.5	4.1	86.5	4.4	64.5	4.6	189	4.9	226	5.0	197.5	4.0	21	4.6	497	39.5	15.VII	21	48	125	20	38	18	46	127	145	94	13	—	71	13

Koło $H_s = 95\,m$ $h_w = 14.4\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7.5	2.3	4	3.0	12	2.2	11.5	2.7	14	3.1	14	4.0	10.5	3.9	4.5	2.8	15	2.7	28	4.1	30	·	6	27	·	2	·	2	18	15	9	·	6	14	·
II	10.5	4.1	3	3.8	4	2.5	1	1.0	3.5	3.4	12	5.0	31.5	4.3	10.5	4.5	8	3.8	30	5.1	7	12	22	27	·	2	·	1	16	19	10	·	7	28	·
III	4.5	2.7	9	3.2	6.5	1.9	11.5	2.3	5	1.6	13	4.3	16.5	3.5	7	3.4	20	2.4	26	7.1	3	6	6	19	·	1	1	5	12	12	7	·	7	17	·
IV	8	3.6	11	3.8	27	3.3	5.5	3.0	7	1.7	4.5	1.9	11.5	3.7	5.5	3.2	10	2.9	62	27.0	28	·	·	4	·	1	·	1	10	14	8	2	2	·	1
V	15	2.9	11.5	2.9	16.5	3.8	2.5	1.4	·	·	13.5	3.5	10	3.2	11	2.3	13	2.7	76	17.5	19	·	·	2	·	3	·	1	13	18	13	2	5	·	1
VI	10	2.7	8	3.0	12.5	3.4	3.5	1.4	7	4.1	8	3.0	20	3.6	6	3.1	15	2.7	42	9.1	11	·	·	·	5	1	1	3	9	17	10	·	·	·	4
VII	5	3.4	4	2.4	9.5	2.9	3	1.7	7.5	1.6	26	3.3	24.5	4.2	4.5	2.3	9	2.9	119	30.5	21	·	·	·	5	3	·	2	9	18	15	3	1	·	13
VIII	2.5	1.8	0.5	1.0	5	1.5	7.5	2.4	6	2.0	10	2.8	20	3.3	11.5	2.4	30	1.8	29	10.3	24	·	·	·	10	·	·	4	7	9	5	1	4	·	2
IX	1	2.0	1	3.0	14	2.1	15.5	2.3	10	2.4	11	3.0	21	2.9	1.5	3.0	15	2.2	65	21.4	28	·	·	·	4	·	·	6	3	10	6	2	2	·	2
X	2	2.5	4	2.4	5	2.3	2.5	1.4	3	1.7	11	3.3	24	3.0	8.5	1.8	33	1.7	14	7.1	16	·	·	7	·	·	·	6	6	5	3	·	11	·	·
XI	5	1.9	12	3.6	14	3.7	6	4.5	4	3.8	17.5	4.1	18.5	4.1	4	1.9	9	3.3	35	9.0	21	6	10	18	·	1	·	1	20	12	8	·	6	16	·
XII	1.5	2.3	·	·	9.5	1.8	14	2.8	13.5	4.7	25.5	5.3	18	4.9	6	2.9	5	3.9	43	13.1	18	2	3	18	·	4	·	·	18	18	12	1	4	9	·
Rok	72.5	2.7	68	2.7	135.5	2.6	84	2.2	80.5	2.5	166	3.6	226	3.7	80.5	2.8	182	2.8	569	30.5	21.VII	26	47	122	24	18	2	32	141	167	106	11	55	84	23

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Niepokalanów

φ = 52°12′ λ = 20°25′

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m.}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.3	-4.0	5.5	18	-14.2	11	-1.8	0.3	-1.6	-1.2	4.9	5.2	5.0	5.0	89	82	90	87	0.6	1.2	0.5	0.8	7.5	6.8	6.6	7.0
II	–	–	–	–	-2.0	-10.2	2.6	14	-22.7	6	-7.1	-3.5	-6.0	-5.6	3.4	3.7	3.6	3.6	88	76	88	84	0.4	1.1	0.5	0.7	7.2	6.6	6.4	6.7
III	–	–	–	–	5.6	-3.8	14.7	30	-17.8	8	-2.3	4.0	0.0	0.4	5.0	5.6	5.4	5.3	90	67	85	81	0.6	3.0	1.0	1.5	5.9	5.7	4.5	5.4
IV	–	–	–	–	10.6	2.0	16.2	29	-2.8	3	4.2	9.1	5.7	6.2	7.2	7.6	7.4	7.4	85	66	80	77	1.2	4.2	1.8	2.4	6.4	6.7	6.0	6.4
V	–	–	–	–	14.4	4.8	21.5	17	-2.5	3	8.6	12.6	9.2	9.9	9.4	9.5	9.8	9.6	81	64	82	76	2.1	5.4	2.1	3.2	5.4	7.6	5.1	6.0
VI	–	–	–	–	21.6	10.9	31.0	26	5.7	15	14.8	19.8	15.1	16.2	13.6	13.9	14.1	13.9	81	61	81	74	3.3	9.8	3.2	5.4	4.6	6.2	4.5	5.1
VII	–	–	–	–	22.1	11.2	30.8	15	6.0	2	15.2	20.4	15.2	16.5	14.6	14.5	14.9	14.7	83	60	85	76	2.9	10.2	2.7	5.3	4.7	6.0	4.8	5.2
VIII	–	–	–	–	21.7	10.5	30.9	7	5.2	16	13.4	20.0	14.3	15.5	13.8	13.7	14.1	13.9	89	60	86	78	1.9	10.8	2.6	5.1	4.9	5.0	4.4	4.8
IX	–	–	–	–	21.4	9.0	27.8	3	3.2	16, 21	11.3	19.7	12.9	14.2	12.7	13.9	13.4	13.3	93	61	89	81	1.0	9.6	1.8	4.1	5.0	4.3	2.8	4.0
X	–	–	–	–	12.7	2.5	21.8	1	-5.7	22	4.3	11.4	6.6	7.2	7.9	9.3	8.9	8.7	93	68	90	84	0.6	4.6	1.1	2.1	5.6	5.5	3.9	5.0
XI	–	–	–	–	1.5	-4.7	12.5	2	-19.2	16	-2.4	0.3	-1.4	-1.2	5.0	5.4	5.3	5.2	89	82	89	87	0.7	1.3	0.7	0.9	8.2	7.7	8.5	8.1
XII	–	–	–	–	2.7	-2.3	10.5	19	-19.7	17	-0.1	1.4	0.2	0.4	5.5	5.5	5.3	5.4	87	81	84	84	0.9	1.4	1.1	1.1	8.2	7.3	8.2	7.9
Rok	–	–	–	–	11.1	2.2	31.0	26.VI	-22.7	6.II	4.8	9.6	5.8	6.5	8.6	9.0	8.9	8.8	87	69	86	81	1.4	5.2	1.6	2.7	6.1	6.3	5.5	6.0

Łosice

φ = 52°12′ λ = 22°43′

I	–	–	–	–	-0.4	-5.5	3.1	9	-19.3	11	-3.3	-1.7	-2.5	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.3	7.5	8.1
II	–	–	–	–	-3.6	-10.9	1.4	14	-22.6	6	-7.8	-4.6	-7.2	-6.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.1	6.0	7.1
III	–	–	–	–	3.4	-4.1	13.2	30	-17.2	9	-2.3	2.5	-0.3	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.6	5.7	6.6
IV	–	–	–	–	10.0	2.1	14.8	26	-2.5	3	3.7	8.9	5.4	5.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.8	7.5	8.0
V	–	–	–	–	14.1	4.8	21.9	19	-2.8	4	8.3	13.1	9.0	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.0	6.8
VI	–	–	–	–	20.3	11.1	27.8	26	5.0	8	14.3	19.0	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.1	6.7	6.7
VII	–	–	–	–	21.5	10.8	29.5	17	5.8	5	15.5	20.0	14.8	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	7.7	6.3	6.3
VIII	–	–	–	–	20.7	10.6	28.1	7	6.3	31	13.1	19.0	14.1	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.0	5.0	5.9
IX	–	–	–	–	20.8	9.2	27.0	3	2.6	21	11.4	19.8	13.4	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.4	3.1	4.8
X	–	–	–	–	11.2	2.7	19.8	1	-5.5	21	4.2	10.4	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.0	4.6	6.1
XI	–	–	–	–	0.4	-4.4	11.2	2	-19.7	17	-2.4	-1.0	-2.3	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	9.7	9.5	8.3	9.2
XII	–	–	–	–	0.9	-3.2	7.1	19	-17.7	17	-1.7	-0.1	-1.0	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.4	7.3	8.0
Rok	–	–	–	–	9.9	1.9	29.5	17.VII	-22.6	6.II	4.4	8.8	5.3	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	6.2	7.0

Siedlce

φ = 52°11′ λ = 22°16′

I	994.0	1010.5	974.6	1012.8	0.3	-4.9	3.6	9	-19.5	11	-3.2	-1.4	-2.0	-2.2	4.4	4.8	4.7	4.6	87	85	85	86	0.6	0.8	0.8	0.7	7.9	8.5	6.9	7.8
II	995.9	1014.5	973.3	1015.0	-2.9	-11.2	2.2	14	-21.9	24	-7.9	-4.7	-7.2	-6.8	3.2	3.6	3.2	3.3	85	80	81	82	0.5	0.8	0.6	0.6	8.0	7.3	6.2	7.2
III	998.7	1015.3	971.2	1017.5	4.1	-4.3	13.3	30	-19.6	9	-2.8	2.6	-0.2	-0.2	4.7	5.4	5.1	5.1	87	71	81	80	0.6	2.3	1.2	1.4	7.4	6.7	5.8	6.6
IV	993.9	1009.9	976.3	1012.2	10.8	2.2	15.1	19	-2.6	3	3.6	9.3	5.5	6.0	6.8	7.0	7.2	7.0	83	59	77	73	1.3	5.0	2.0	2.8	8.8	8.1	7.0	8.0
V	995.8	1012.0	981.0	1013.9	14.4	4.5	21.7	19	-3.4	4	8.1	12.9	9.2	9.8	9.1	9.0	9.6	9.2	82	59	81	74	1.9	6.3	2.2	3.5	6.5	7.5	6.7	6.9
VI	996.2	1003.5	986.9	1013.9	20.6	10.6	28.7	26	4.2	8	14.3	19.1	15.0	15.8	13.1	13.0	13.6	13.2	80	60	80	73	3.4	9.7	3.6	5.6	5.6	6.7	6.0	6.1
VII	994.4	1005.3	981.7	1012.0	21.9	10.4	29.5	16	4.4	5	14.9	20.3	15.4	16.5	14.1	13.3	13.9	13.8	82	56	79	72	3.2	11.2	3.9	6.1	5.1	7.5	5.4	6.0
VIII	997.6	1005.7	987.6	1015.4	20.7	9.9	29.0	7	4.8	31	12.9	19.1	14.1	15.0	13.4	13.5	13.9	13.6	89	62	85	79	1.7	9.5	2.7	4.6	5.8	6.0	4.1	5.3
IX	998.1	1015.5	986.3	1016.0	21.0	8.7	27.4	3	1.7	21	10.9	19.7	13.4	14.4	12.1	13.0	13.1	12.7	92	57	85	78	1.2	10.4	2.6	4.7	5.6	5.8	3.0	4.8
X	1004.3	1019.7	990.6	1022.8	11.7	2.3	20.3	1	-6.1	21	4.1	10.7	6.2	6.8	7.8	9.1	8.5	8.5	93	70	88	84	0.6	4.2	1.2	2.0	6.7	6.8	5.1	6.2
XI	994.2	1010.6	968.3	1013.0	0.7	-4.4	11.2	2	-21.5	17	-2.0	-0.6	-1.8	-1.6	5.0	5.2	5.1	5.1	88	84	87	86	0.7	1.1	0.7	0.8	9.1	9.3	8.9	9.1
XII	988.5	1003.6	968.0	1007.1	1.4	-2.8	8.6	20	-17.6	17	-1.0	0.4	-0.4	-0.4	5.0	5.3	5.1	5.1	86	83	84	84	0.8	1.2	1.0	1.0	8.0	8.6	7.5	8.0
Rok	996.0	1019.7	968.0	1014.3	10.4	1.8	29.5	16.VII	-21.9	24.II	4.3	9.0	5.6	6.1	8.2	8.5	8.6	8.4	86	69	83	79	1.4	5.2	1.9	2.8	7.0	7.4	6.0	6.8

Kęguty

φ = 52°10′ λ = 20°51′

I	–	–	–	–	0.9	-4.1	4.6	18	-13.9	11	-1.9	-0.2	-1.5	-1.3	5.1	5.5	5.3	5.3	95	93	95	94	0.3	0.6	0.3	0.4	8.2	7.8	7.2	7.7
II	–	–	–	–	-2.2	-10.5	2.6	13, 14	-24.0	5, 6	-7.2	-3.5	-6.0	-5.7	3.5	4.0	3.8	3.8	92	83	91	89	0.3	0.7	0.3	0.4	7.7	7.4	6.7	7.3
III	–	–	–	–	4.8	-3.7	13.2	30	-16.4	8, 9	-2.3	3.4	0.1	0.3	5.1	6.0	5.6	5.6	93	75	89	86	0.4	2.2	0.8	1.1	6.6	6.5	5.7	6.3
IV	–	–	–	–	10.4	2.1	15.5	29	-3.2	3	4.0	9.0	5.6	6.0	7.4	7.9	7.9	7.7	89	69	86	81	0.9	3.8	1.3	2.0	7.5	7.4	7.4	7.4
V	–	–	–	–	14.1	4.8	20.7	17	-2.9	4	8.3	12.7	9.3	9.9	9.6	9.8	10.3	9.9	85	65	85	78	1.6	5.2	1.7	2.9	6.1	8.2	6.8	7.0
VI	–	–	–	–	21.0	11.3	29.4	26	6.5	3	14.4	19.5	15.0	16.0	13.8	13.7	14.7	14.1	83	62	85	77	2.8	9.6	2.5	5.0	4.9	7.1	5.6	5.9
VII	–	–	–	–	21.7	11.2	29.9	16	5.4	11	15.0	20.1	15.0	16.3	14.5	14.1	15.4	14.7	83	60	89	77	2.8	10.1	1.9	4.9	5.3	7.4	5.0	5.9
VIII	–	–	–	–	21.3	10.3	29.9	7	4.7	16	13.2	19.7	14.1	15.3	13.8	13.8	14.3	14.0	90	61	89	80	1.7	10.3	2.3	4.8	5.4	6.8	5.2	5.8
IX	–	–	–	–	20.9	9.5	28.4	2	4.5	21	11.4	19.3	13.4	14.4	12.6	13.8	13.8	13.4	93	62	89	81	1.0	9.1	1.8	4.0	5.3	5.5	2.4	4.4
X	–	–	–	–	12.3	2.9	21.8	1	-5.2	22	4.6	11.4	6.6	7.3	8.1	9.5	9.0	8.9	93	70	90	84	0.6	4.3	1.0	2.0	5.8	5.9	4.4	5.4
XI	–	–	–	–	1.3	-4.1	12.2	2	-17.5	24	-2.1	-0.1	-1.2	-1.2	5.2	5.5	5.6	5.4	92	87	94	91	0.5	1.0	0.5	0.7	9.2	7.8	9.1	8.7
XII	–	–	–	–	2.2	-2.4	9.8	20	-21.0	17	-0.2	1.0	0.2	0.3	5.6	5.7	5.5	5.6	89	85	87	87	0.7	1.1	0.9	0.9	8.9	8.8	8.3	8.7
Rok	–	–	–	–	10.7	2.3	29.9	16.VII, 7.VIII	-24.0	5, 6. II	4.8	9.4	5.9	6.5	8.7	9.1	9.3	9.0	90	73	89	84	1.1	4.8	1.3	2.4	6.7	7.2	6.2	6.7

Niepokalanów $H_s = 92$ m $h_w = 24{,}5$ m 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5.5	4.2	9.5	3.2	8	3.2	18.5	3.3	3.5	2.1	9.5	5.6	22	4.5	15.5	4.6	1	4.0	24	3.9	20	1	10	27	·	1	·	2	14	15	9	·	6	22	·
II	14	5.3	8.5	6.4	3.5	3.9	3	1.8	0.5	1.0	6.5	5.2	19.5	6.2	28.5	5.4	·	5.5	34	3.5	7	14	20	27	·	2	·	1	9	19	13	·	2	28	·
III	9.5	4.5	9.5	4.3	9	2.4	20.5	2.1	5.5	4.1	10.5	5.7	9	5.8	17.5	5.1	2	4.0	17	6.0	3	5	6	21	·	2	·	6	8	13	6	·	4	16	·
IV	10	4.4	5.5	4.4	17.5	5.2	24.5	5.1	5.5	5.5	3	5.5	7.5	5.2	13.5	4.7	3	4.8	54	19.7	28	·	·	9	·	1	·	2	9	15	11	1	·	·	1
V	20	4.4	7.5	4.1	11.5	4.0	12.5	4.8	1	5.0	6.5	3.3	10	4.1	18	4.0	6	3.9	75	16.7	19	·	·	3	·	·	·	4	10	17	11	3	2	·	4
VI	8	5.6	5.5	5.6	9	6.0	8	6.2	1.5	4.0	8.5	5.4	27	5.4	16.5	4.7	6	5.0	55	12.4	10	·	·	·	5	1	·	4	6	14	10	1	·	·	3
VII	5.5	4.6	7	3.9	4.5	3.9	2.5	5.0	4	5.0	22	5.0	37.5	4.6	6	3.1	4	4.4	104	36.5	17	·	·	·	6	·	·	6	6	17	14	2	1	·	9
VIII	1	2.0	1.5	1.0	6.5	3.5	5	3.9	5.5	2.9	6	3.9	32	4.8	20.5	3.4	15	3.3	49	21.1	26	·	·	·	9	·	·	8	3	12	8	2	1	·	1
IX	·	·	1	3.0	6	3.5	14	2.7	8	4.4	14.5	3.8	19.5	4.3	16	3.9	11	3.3	47	16.4	29	·	·	·	2	2	·	8	2	8	7	2	2	·	2
X	6	3.8	2.5	3.6	7	3.0	7.5	2.0	1	1.0	10.5	5.3	11.5	4.6	38	3.6	9	3.4	4	3.2	16	·	·	6	·	·	·	9	4	4	1	·	12	·	·
XI	5.5	3.7	14	4.4	9.5	4.4	12.5	4.4	9	4.4	6.5	5.7	21	5.4	11	3.7	1	4.6	37	9.2	21	7	11	20	·	1	·	1	19	16	10	·	11	16	·
XII	4.5	3.3	1	2.0	6	2.7	13	4.2	3.5	4.6	23	5.7	30	5.3	12	4.1	·	4.8	49	15.9	18	2	5	21	·	4	·	·	17	19	13	1	3	12	·
Rok	89.5	3.8	73	3.8	98	3.8	141.5	3.8	48.5	3.7	127	5.0	246.5	5.0	213	4.2	58	4.2	549	36.5	17. VII	29	52	134	22	14	·	51	107	169	113	12	44	94	20

Łosice $H_s = 153$ m $h_w = 14$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7	2.9	2	4.5	7	4.1	21	6.1	29	4.6	11.5	3.8	7	5.8	5.5	4.5	3	4.6	22	4.6	17	4	14	29	·	3	·	2	19	16	7	·	3	31	·
II	12	5.1	2.5	7.0	6	5.7	1	1.0	9.5	4.8	23	6.2	25.5	4.1	3.5	5.0	1	5.1	18	3.6	7	12	24	28	·	4	1	1	13	16	8	·	1	28	·
III	6	3.8	·	·	6	3.5	8.5	5.6	34.5	4.4	25	3.5	6.5	4.4	6.5	5.6	·	4.2	16	4.3	21	4	7	23	·	2	·	5	14	9	5	·	4	20	·
IV	1.5	4.0	3	7.2	19	8.6	27.5	7.4	11.5	4.3	16	4.3	5.5	3.2	5	2.9	1	6.1	38	10.0	26	·	·	11	·	10	·	1	20	10	6	1	·	·	2
V	5	5.4	3.5	2.4	9	7.8	15	4.3	7.5	4.2	19	3.2	18	2.5	14	5.6	2	4.1	81	31.1	25	·	·	2	·	3	1	1	10	14	13	2	·	·	3
VI	2.5	5.4	3	4.7	7.5	7.1	11	5.1	8.5	3.5	30.5	3.4	18.5	3.1	6.5	3.4	2	3.9	64	15.2	14	·	·	·	4	1	·	2	12	10	10	1	·	·	3
VII	·	·	1	3.0	5.5	4.1	6	4.4	21	3.5	47	4.2	9.5	3.2	·	·	3	3.8	107	66.1	17	·	·	·	4	·	·	2	11	13	10	2	·	·	7
VIII	2	7.0	·	·	·	·	6	4.3	16	4.6	34.5	2.7	29.5	2.6	4	3.4	1	3.2	69	28.9	2	·	·	·	8	·	·	2	6	11	9	2	·	·	2
IX	·	·	·	·	0.5	9.0	16	6.8	34	3.7	32.5	3.5	6	3.3	·	·	1	4.1	19	7.7	6	·	·	·	3	1	·	4	3	10	3	·	1	·	1
X	1	1.0	1	3.0	0.5	9.0	4.5	5.2	20.5	2.9	24.5	3.3	26	3.2	6	3.8	9	3.0	7	2.6	16	·	·	3	·	·	·	4	10	5	3	·	10	·	·
XI	3	2.0	11.5	4.5	11	4.6	12	7.0	10.5	4.4	22	5.0	13	3.5	3	1.3	4	4.4	26	4.9	1	4	12	21	·	3	·	·	25	19	8	·	5	18	·
XII	3	1.0	0.5	1.0	3.5	1.0	14	5.4	31.5	4.9	21.5	4.4	12.5	2.0	2.5	1.8	4	3.9	33	6.6	18	2	8	28	·	1	·	·	19	23	7	·	·	19	·
Rok	43	3.1	28	3.1	75.5	5.4	142.5	5.2	234	4.2	307	4.0	177.5	3.4	56.5	3.1	31	4.2	500	66.1	17. VII	26	65	145	19	28	2	24	162	156	89	8	24	116	18

Siedlce $H_s = 146$ m $H_b = 149.1$ m $h_w = 12$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	3.5	6	3.1	13	2.8	19.5	3.7	19	5.0	12.5	5.7	5.5	5.6	6.5	6.8	5	4.2	36	7.8	17	3	10	27	·	5	·	2	18	14	9	·	4	31	·
II	13	4.9	7.5	5.1	3.5	5.3	·	·	7.5	6.3	16.5	6.3	26	5.1	8	5.2	2	5.3	20	4.0	8	14	23	28	·	7	·	1	14	17	7	·	3	28	·
III	3.5	4.6	4.5	3.0	9	2.1	16	3.2	23	3.6	13.5	3.9	12.5	4.1	6	5.8	5	3.5	28	5.8	19	7	8	22	·	2	·	5	13	12	8	·	7	19	·
IV	6	4.3	5	3.9	26.5	4.6	30	3.5	7	5.0	5.5	5.9	5	3.2	4	3.5	1	4.1	48	15.7	23	·	·	11	·	1	·	·	19	10	7	1	2	·	2
V	16.5	3.3	5	2.3	17	3.2	5.5	2.5	2.5	4.6	12	3.7	12	3.2	11.5	3.2	11	2.9	73	17.3	25	·	·	2	·	3	1	1	10	15	9	4	1	·	2
VI	11	3.0	7.5	4.0	10.5	3.7	3.5	2.3	10	3.8	8.5	5.1	21	3.9	6	3.8	12	3.3	45	12.9	6	·	·	·	5	1	·	2	9	10	9	1	2	·	2
VII	0.5	5.0	7	3.2	6	1.8	6.5	2.3	21	3.7	21.5	4.1	18	4.7	2.5	4.0	10	3.3	88	64.1	17	·	·	·	6	7	·	3	6	14	10	1	3	·	6
VIII	9	4.2	1	3.0	2	1.5	10.5	3.0	9	2.9	11.5	3.1	21.5	3.6	13.5	4.0	15	2.9	78	20.8	26	·	·	·	8	2	·	5	9	12	10	2	·	·	2
IX	0.5	2.0	·	·	3.5	1.6	22.5	2.5	22	2.8	18.5	4.2	13	3.2	2	3.0	8	2.8	19	9.1	29	·	·	·	2	2	·	6	4	7	4	·	3	·	·
X	9.5	2.0	3	1.0	5	1.8	4	1.6	11	3.9	13	4.0	25	3.6	9.5	3.2	13	2.7	6	3.4	16	·	·	4	·	·	·	3	9	7	2	·	14	·	·
XI	2	1.8	10.5	4.2	11	2.9	14.5	4.0	9.5	3.9	15	5.4	18.5	4.6	3	3.3	6	3.9	39	7.0	30	5	12	20	·	2	·	·	24	21	10	·	8	16	·
XII	3	2.3	1.5	2.0	3	1.7	13.5	4.1	30	5.3	24.5	5.1	10	4.7	3.5	3.4	4	4.5	36	6.6	18	2	6	23	·	3	·	·	20	17	10	·	4	16	·
Rok	80.5	3.4	58.5	2.9	110	2.8	146	2.7	171.5	4.2	172.5	4.7	188	4.1	76	4.1	92	3.6	516	64.1	17.VII	31	59	137	21	35	1	28	155	156	95	9	51	110	14

Uwaga. Kierunki i prędkości wiatru – wg anemometru M - 47.

Reguły $H_s = 98$ m $h_w = 14{,}5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	3.1	2.5	3.2	5.5	1.8	17.5	2.7	11.5	3.0	15.5	3.0	6	4.2	10	3.7	20	2.4	29	5.3	24	3	8	28	·	·	·	1	16	14	11	·	3	16	·
II	13	4.3	10.5	3.4	3	2.2	1.5	2.0	1.5	2.3	16	5.6	26.5	3.5	10	4.4	2	4.0	28	4.3	7	9	22	28	·	·	·	·	13	16	11	·	1	28	·
III	1.5	4.7	5	3.5	11	2.9	15	2.6	10.5	2.6	9.5	4.9	17	2.9	9.5	3.4	14	2.7	13	5.9	4	5	7	20	·	·	·	6	16	8	4	·	4	16	·
IV	8.5	2.6	9.5	2.6	16	4.1	21.5	2.6	2.5	3.6	4.5	4.1	9	2.3	7.5	3.1	11	2.7	32	11.0	28	·	·	5	·	·	·	·	12	11	6	1	2	·	·
V	11.5	2.3	11.5	2.4	12.5	3.2	6.5	2.9	1	1.0	11	2.6	14	2.5	16	2.5	9	2.3	53	12.8	25	·	·	3	·	·	·	1	13	13	11	2	2	·	2
VI	10.5	2.7	7.5	3.7	10.5	3.4	6.5	3.5	5	2.7	11.5	3.3	21	3.1	13.5	2.6	4	3.0	75	30.3	14	·	·	·	3	·	·	1	10	13	11	2	·	·	4
VII	2.5	3.6	4.5	3.0	7.5	2.7	7.5	2.4	8.5	2.8	25.5	3.0	28	3.0	5	2.3	4	2.8	126	33.5	17	·	·	·	5	·	·	2	7	17	17	4	·	·	6
VIII	11.5	1.7	2	2.2	3	2.2	13	3.2	5	3.0	7	2.6	20	2.6	18.5	2.5	13	2.2	107	44.6	26	·	·	·	11	·	·	2	10	14	10	4	1	·	1
IX	0.5	1.0	0.5	1.0	6.5	2.8	26	2.7	10.5	2.8	10.5	2.9	19	3.3	5.5	2.5	11	2.5	61	24.9	29	·	·	·	3	·	·	6	4	10	9	2	6	·	·
X	12.5	1.5	2	2.0	5	2.7	9	2.1	5.5	2.3	12.5	3.2	23.5	2.7	10	2.6	13	2.1	7	3.8	16	·	·	4	·	·	·	5	8	6	1	·	13	·	·
XI	3	1.8	12.5	3.1	12.5	3.0	14	4.6	7	3.3	10	5.0	25.5	3.9	0.5	5.0	5	3.6	38	8.2	21	7	11	21	·	·	·	·	23	19	10	·	6	16	·
XII	2	2.0	1.5	2.3	5	3.1	12	3.7	13	5.4	26	4.5	24	3.9	6.5	2.2	3	3.9	57	18.7	18	2	5	23	·	3	1	·	22	19	12	1	2	10	·
Rok	81.5	2.6	69.5	2.7	98	2.8	150	2.9	81.5	2.9	169.5	3.7	233.5	3.2	112.5	3.1	109	2.8	626	44.6	26.VIII	26	53	132	22	3	1	24	156	162	113	16	40	86	13

Brwinów

$\varphi = 52°08'$ $\lambda = 20°43'$ **1965**

Miesiąc	Ciśnienie p: p_m	Max	Min	$p_{m.m}$	Temperatura t: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	999.7	1016.1	980.5	1012.2	1.2	−3.4	5.3	19	−14.6	11	−1.9	−0.1	−1.2	−1.1	4.8	5.1	5.1	5.0	87	83	88	86	0.7	1.1	0.6	0.8	7.8	7.3	6.4	7.2
II	1003.0	1020.7	978.8	1015.7	−2.5	−9.4	2.5	13, 14	−24.1	6	−7.1	−3.9	−5.6	−5.6	3.3	3.8	3.6	3.6	86	79	86	84	0.5	0.9	0.6	0.7	7.7	6.8	5.6	6.7
III	1004.6	1021.5	975.5	1017.0	5.4	−3.1	13.7	30	−16.1	8	−2.1	3.7	0.8	0.8	5.0	5.7	5.6	5.4	88	70	84	81	0.6	2.7	1.1	1.5	6.3	6.5	5.0	5.9
IV	999.4	1017.7	983.0	1011.5	10.7	2.4	15.4	29, 30	−3.1	3	4.1	9.0	6.1	6.3	7.3	7.9	7.7	7.6	87	69	80	79	1.1	3.8	1.9	2.3	7.0	7.3	6.0	6.8
V	1002.0	1018.2	985.6	1013.9	14.3	5.2	21.0	17	−2.0	4	8.5	12.5	9.7	10.1	9.5	9.9	9.9	9.8	83	67	80	77	1.9	4.9	2.4	3.1	5.6	5.1	5.6	6.4
VI	1002.3	1010.4	992.9	1014.0	21.4	11.3	29.6	26	6.4	15	14.6	19.4	15.3	16.2	13.7	13.9	14.4	14.0	82	63	82	76	3.0	9.2	3.1	5.1	4.8	6.1	5.2	5.4
VII	1000.1	1010.7	986.1	1011.8	21.8	11.5	29.8	16	6.8	5	15.4	20.0	15.3	16.5	14.4	13.9	14.9	14.4	81	59	85	75	3.3	10.2	2.8	5.4	5.4	6.5	4.7	5.5
VIII	1003.8	1012.4	992.4	1015.5	21.4	10.9	30.3	7	6.1	16	13.6	19.7	14.8	15.7	13.7	13.2	13.8	13.6	88	59	83	77	2.1	10.8	3.7	5.5	5.5	5.9	5.5	5.6
IX	1003.6	1022.6	992.4	1015.3	21.1	10.0	26.8	2	4.3	21	11.8	19.4	13.9	14.8	13.0	14.1	13.9	13.7	92	63	87	81	1.2	8.9	2.3	4.1	5.0	5.2	2.2	4.1
X	1010.9	1025.9	996.7	1023.1	12.4	3.0	21.9	1	−5.6	22	4.7	11.2	6.6	7.3	8.3	9.7	9.1	9.0	94	71	91	85	0.5	4.0	0.9	1.8	5.7	5.7	4.4	5.3
XI	1000.3	1019.1	972.8	1012.7	1.6	−3.5	12.6	2	−16.2	24	−2.0	0.1	−1.0	−1.0	5.2	5.4	5.5	5.4	90	83	89	87	0.5	1.2	0.7	0.8	8.6	7.9	8.3	8.2
XII	994.2	1011.2	971.9	1006.5	2.8	−2.1	10.4	20	−18.7	17	0.0	1.3	0.3	0.5	5.6	5.6	5.4	5.5	88	82	86	85	0.8	1.3	1.0	1.0	8.0	8.2	7.4	7.9
Rok	1000.9	1025.9	971.9	1014.1	11.0	2.7	30.3	7. VIII	−24.1	6. II	5.0	9.4	6.2	6.7	8.6	9.0	9.1	8.9	87	71	85	81	1.4	4.9	1.8	2.7	6.4	6.8	5.5	6.2

Wielichowo

$\varphi = 52°07'$ $\lambda = 16°21'$

I	—	—	—	—	2.9	−1.1	8.2	17	−5.8	7	0.0	2.2	0.6	0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	8.1	7.0	7.6
II	—	—	—	—	0.1	−5.9	4.2	14	−14.4	28	−4.2	−1.0	−2.7	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.0	7.2	7.4
III	—	—	—	—	6.3	−4.2	15.7	29	−23.1	9	−2.5	4.8	0.3	0.7	—	—	—	—	—	—	—	—	—	—	—	—	6.6	5.6	4.6	5.6
IV	—	—	—	—	12.2	3.0	17.0	30	−2.1	3	5.0	11.0	7.0	7.5	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.4	5.2	6.2
V	—	—	—	—	15.8	6.6	23.4	17	−0.5	2	9.7	14.2	10.4	11.2	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.2	6.4	6.7
VI	—	—	—	—	21.8	11.1	31.4	26	5.7	3, 30	15.2	20.5	15.7	16.8	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.7	6.2	6.3
VII	—	—	—	—	21.0	11.2	30.4	14	3.7	5	15.1	19.3	15.3	16.2	—	—	—	—	—	—	—	—	—	—	—	—	6.7	8.0	7.4	7.4
VIII	—	—	—	—	21.9	10.1	31.7	6	5.7	13, 17	13.6	20.7	14.6	15.9	—	—	—	—	—	—	—	—	—	—	—	—	4.2	6.0	3.3	4.5
IX	—	—	—	—	20.3	8.7	26.4	3	2.7	21	11.2	19.2	12.8	14.0	—	—	—	—	—	—	—	—	—	—	—	—	4.0	5.6	3.2	4.3
X	—	—	—	—	13.7	2.5	22.9	1	−5.9	23	4.1	12.7	6.3	7.4	—	—	—	—	—	—	—	—	—	—	—	—	4.8	4.9	2.5	4.1
XI	—	—	—	—	2.9	−2.7	14.0	2	−15.5	23, 24	−1.2	1.9	−0.1	0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.8	6.6	7.5
XII	—	—	—	—	4.3	−0.5	13.4	19	−6.4	13	1.1	3.1	2.0	2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.8	7.8	8.1
Rok	—	—	—	—	11.9	3.2	31.7	6. VIII	−23.1	9. III	5.6	10.7	6.8	7.5	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.8	5.6	6.3

Łowicz

$\varphi = 52°07'$ $\lambda = 19°56'$

I	—	—	—	—	1.5	−3.2	5.1	18	−13.2	11	[illegible]	[illegible]	−1.2	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.9	7.0	7.8
II	—	—	—	—	−2.1	−9.5	2.7	13	−20.0	6	−6.6	−3.[illegible]	−5.8	−5.4	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.7	6.8	7.5
III	—	—	—	—	5.5	−3.2	13.7	30	−16.1	8	−1.5	4.1	0.7	1.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.9	6.0	6.6
IV	—	—	—	—	10.2	2.3	15.4	30	−1.5	1	4.3	8.8	5.5	6.0	—	—	—	—	—	—	—	—	—	—	—	—	6.9	8.4	7.4	7.6
V	—	—	—	—	14.1	5.7	21.4	17	−1.1	4	8.7	12.5	9.6	10.1	—	—	—	—	—	—	—	—	—	—	—	—	6.7	8.1	6.3	7.0
VI	—	—	—	—	21.4	11.2	30.5	26	6.3	15	14.9	19.8	15.2	16.3	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.8	6.0	6.1
VII	—	—	—	—	21.7	11.7	30.5	14	6.9	6	15.7	20.3	15.1	16.6	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.0	6.1	6.6
VIII	—	—	—	—	21.8	10.8	31.3	7	5.4	16	13.3	20.1	14.8	15.8	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.3	5.5	6.1
IX	—	—	—	—	21.0	9.6	28.1	3	3.4	16	11.8	19.5	13.3	14.5	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.9	4.8	5.6
X	—	—	—	—	12.2	3.3	21.7	1	−5.5	22	4.7	10.9	6.6	7.2	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.6	5.8	6.3
XI	—	—	—	—	1.6	−4.0	12.8	2	−18.2	24	−2.4	0.4	−1.3	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.0	8.1	8.4
XII	—	—	—	—	2.9	−1.7	11.0	19	−18.3	17	0.3	1.8	0.4	0.7	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.2	8.8	8.7
Rok	—	—	—	—	11.0	2.8	31.3	7. VIII	−20.0	6. II	5.1	9.6	6.1	6.7	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.3	6.6	7.0

Świder

$\varphi = 52°07'$ $\lambda = 21°15'$

I	—	—	—	—	1.0	−4.1	4.6	18	−17.2	11	−2.0	0.2	−1.4	−1.2	4.7	5.1	4.8	4.9	86	81	85	84	0.7	1.2	0.8	0.9	8.5	8.5	6.3	7.8
II	—	—	—	—	−1.8	−11.0	3.4	14	−23.8	6	−7.3	−2.9	−6.5	−5.8	3.1	3.5	3.2	3.3	81	68	80	76	0.7	1.5	0.7	1.0	7.8	6.8	6.6	7.1
III	—	—	—	—	5.5	−4.0	14.6	30	−18.0	8	−2.2	4.2	0.0	0.5	4.8	5.4	5.1	5.1	85	64	80	76	0.8	3.1	1.2	1.7	7.9	7.3	5.0	6.7
IV	—	—	—	—	11.2	2.0	16.0	29	−4.6	3	4.4	10.0	6.0	6.6	7.0	7.3	7.2	7.2	82	60	76	73	1.5	5.2	2.2	3.0	8.7	7.6	7.2	7.9
V	—	—	—	—	15.0	4.6	22.1	18	−5.1	4	9.0	13.7	9.4	10.4	9.2	9.0	9.4	9.2	78	57	78	71	2.5	7.0	2.7	4.1	6.2	8.5	6.3	7.0
VI	—	—	—	—	21.6	10.5	30.8	26	5.3	8	15.0	20.3	15.1	16.4	13.3	13.1	13.8	13.4	77	57	80	71	4.0	11.5	3.6	6.4	5.3	6.9	5.9	6.0
VII	—	—	—	—	22.6	10.8	30.7	16	4.6	11	15.5	20.8	14.9	16.5	14.3	13.6	14.7	14.2	80	56	85	74	3.5	11.8	2.6	6.0	6.0	8.0	5.1	6.4
VIII	—	—	—	—	21.8	10.5	31.0	7	5.0	29	13.3	20.5	14.3	15.6	13.8	13.6	13.8	13.7	90	58	85	78	1.8	11.7	3.1	5.5	6.3	6.4	5.1	5.9
IX	—	—	—	—	21.6	8.8	27.8	2, 3	1.7	21	11.4	20.2	13.1	14.4	12.6	13.8	13.6	13.3	92	59	89	80	1.2	10.5	1.9	4.5	6.6	5.5	3.4	5.2
X	—	—	—	—	12.6	2.1	21.9	1	−6.9	22	4.1	11.9	6.0	7.0	7.8	9.3	8.8	8.5	92	66	91	83	0.6	5.0	0.9	2.2	7.7	6.3	5.2	6.4
XI	—	—	—	—	1.3	−3.8	12.0	2	−15.6	24	−1.6	0.3	−1.0	−0.8	5.0	5.3	5.3	5.2	86	80	86	84	0.8	1.4	0.8	1.0	9.3	9.3	8.7	9.1
XII	—	—	—	—	2.1	−2.7	9.8	20	−16.5	17	−0.3	1.2	0.0	0.2	5.3	5.4	5.2	5.3	86	80	84	83	0.8	1.4	1.1	1.1	8.3	9.0	8.2	8.5
Rok	—	—	—	—	11.2	2.0	31.0	7. VIII	−23.8	6. II	4.9	10.0	5.8	6.6	8.4	8.7	8.7	8.6	85	66	83	78	1.6	5.9	1.8	3.1	7.4	7.5	5.1	7.0

Brwinów $H_s = 96\ m$ $H_b = 98{,}0\ m$ $h_w = 11\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU %D, V m/D: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8	3.1	·	·	10	3.6	13	5.3	13	5.1	22	4.1	12.5	4.8	5.5	4.1	9	4.0	26	5.8	24	3	10	27	·	3	1	3	16	12	10	·	2	13	—
II	14	4.2	8.5	2.8	3	4.3	1	1.0	1	2.0	19	6.1	27.5	3.5	5	3.7	5	3.9	18	2.8	10, 21	9	24	27	·	2	·	2	10	14	8	·	·	28	—
III	3	5.5	1	1.0	5	2.0	15.5	3.0	14	2.9	15.5	5.5	15	3.0	5	5.9	19	2.9	13	4.0	3	4	7	19	·	2	1	5	10	10	5	·	3	15	—
IV	10	3.7	6	7.0	16.5	5.8	20.5	5.4	3	2.3	7	4.0	12	3.7	5	4.8	10	4.3	46	15.6	28	·	·	5	·	6	1	2	11	14	10	1	1	·	—
V	4	6.0	7	4.9	12	5.5	9	3.2	1	4.0	8.5	3.5	19	4.0	19.5	3.3	13	3.5	79	15.2	16	·	·	3	·	3	·	3	13	17	12	4	1	·	—
VI	3.5	3.0	10	2.9	14	3.2	4	5.2	2.5	3.8	13.5	3.9	26.5	3.1	10	4.0	6	3.2	88	29.1	14	·	·	·	3	1	·	7	7	13	12	3	·	·	—
VII	5	1.8	2	4.0	10	4.1	9	3.3	6	4.0	19	4.7	30.5	4.6	1.5	3.7	10	3.8	78	20.0	17	·	·	·	6	·	·	3	9	18	15	2	·	·	—
VIII	7.5	3.7	0.5	2.0	2.5	4.4	12.5	4.6	10	5.2	12.5	4.1	21	4.0	9.5	4.6	17	3.5	86	43.5	26	·	·	·	10	1	·	5	9	10	8	3	1	·	—
IX	·	·	·	·	7	2.9	27	3.7	10.5	3.2	20	3.0	15	2.8	0.5	2.0	10	2.8	49	16.9	29	·	·	·	2	·	·	8	3	12	8	2	·	·	—
X	2.5	1.8	2	2.0	4	2.8	6.5	3.2	7.5	2.5	11.5	3.0	29.5	3.8	7.5	2.9	22	2.5	9	5.1	16	·	·	6	·	·	·	5	7	5	2	·	6	·	—
XI	2	2.0	11.5	3.0	12.5	3.4	13	4.2	6	3.0	10.5	5.1	17	4.9	4.5	3.0	13	3.4	32	8.0	21	7	11	18	·	1	·	·	19	18	9	·	7	14	—
XII	1	1.0	·	·	3.5	2.6	8	5.1	19	5.8	28	4.1	19.5	3.1	4	3.5	10	3.8	47	15.0	18	2	5	22	·	2	·	1	16	19	12	1	1	8	—
Rok	60.5	3.0	48.5	2.5	100	3.7	139	3.9	93.5	3.6	187	4.3	245	3.8	77.5	3.8	144	3.5	571	43.5	26.VIII	25	57	127	21	21	3	44	130	162	111	16	22	78	—

Wielichowo $H_s = 65\ m$ $h_w = 10\ m$

I	5.5	2.1	10	2.1	11	2.5	9	1.5	10.5	2.8	15.5	3.3	9.5	2.4	3	2.3	19	2.0	28	7.0	17	·	1	26	·	·	·	1	16	13	7	·	—	11	·
II	9.5	3.3	8	3.5	5	1.9	1.5	2.0	1.5	2.3	20	4.6	23	3.2	10.5	3.1	5	3.3	13	3.6	17	6	15	26	·	1	1	2	16	16	3	·	—	23	·
III	10	2.6	6	3.5	2	2.2	6.5	1.8	6.5	1.8	14	2.5	13	3.3	9	2.8	26	1.9	26	10.2	3	7	6	21	·	·	·	6	9	11	8	1	—	18	·
IV	8	2.1	14.5	3.3	17.5	3.4	7.5	2.5	4	2.4	6.5	3.8	9	3.8	14	1.9	9	2.7	31	9.4	19	·	·	4	·	·	·	4	12	14	8	·	—	·	·
V	8.5	2.8	14.5	3.2	12	3.3	6	3.1	1	3.0	10.5	2.6	13	3.2	15.5	2.2	12	2.5	83	11.8	10	·	·	2	·	·	·	1	12	22	17	2	—	·	3
VI	11	1.8	15	2.6	5.5	2.5	2	2.2	1.5	3.7	14	3.1	17	2.4	8	2.1	16	2.1	57	15.1	1	·	·	·	6	·	·	4	9	13	9	1	—	·	5
VII	6.5	2.7	9	2.4	4.5	2.6	0.5	4.0	6	3.5	35.5	2.3	16	3.0	3	2.8	12	2.3	140	72.7	16	·	·	·	3	·	·	·	12	19	16	2	—	·	4
VIII	10.5	1.3	3	1.2	1	1.5	5.5	2.1	4	2.9	12	1.9	25.5	2.0	13.5	1.4	18	1.5	19	5.0	23	·	·	·	8	·	·	5	3	10	6	·	—	·	·
IX	1.5	1.7	0.5	2.0	7	2.6	5	2.5	5	2.7	19.5	2.2	17	2.0	1.5	1.7	29	1.5	31	14.9	10	·	·	·	2	·	·	6	2	6	5	1	—	·	1
X	5.5	1.4	15.5	1.7	12.5	1.3	2	1.8	5	1.8	17	2.1	9.5	2.3	4	1.4	22	1.4	10	4.7	16	·	·	13	·	·	·	13	2	3	3	·	—	·	·
XI	3.5	2.0	23	3.7	4	2.8	4.5	3.0	7.5	3.3	22.5	3.1	11.5	2.7	2.5	2.2	11	2.7	33	8.7	1	5	11	20	·	·	·	2	15	16	7	·	—	15	·
XII	2	1.5	4.5	2.9	5.5	3.6	9	3.3	16.5	4.1	33	5.4	14	4.1	3.5	2.3	5	4.1	46	13.6	18	·	2	17	·	2	·	1	15	24	12	1	—	4	·
Rok	82	2.1	123.5	2.7	87.5	2.5	63	2.5	69	2.9	220	3.1	178	2.9	88	2.2	184	2.3	517	72.7	16.VII	18	35	129	19	3	1	45	123	167	101	8	—	71	13

Łowicz $H_s = 95\ m$ $h_w = 14\ m$

I	7	1.4	7.5	1.5	4.5	1.6	18.5	2.2	12.5	4.5	17.5	2.1	12	3.6	8.5	2.8	5	2.5	19	3.8	9	2	6	26	·	3	1	·	19	13	7	·	3	10	·
II	14.5	4.1	6.5	2.5	2	2.5	1	1.0	3	3.7	14	4.9	23.5	2.7	9.5	2.9	10	3.0	22	3.2	16	11	20	26	·	2	·	·	12	21	8	·	2	28	·
III	4.5	3.3	5.5	1.2	7.5	1.5	11.5	2.0	14.5	1.9	14	4.4	13	3.3	10.5	2.3	12	2.3	9	4.3	3	4	6	19	·	1	1	2	11	9	2	·	3	14	·
IV	11	2.3	5	1.9	20.5	3.2	18.5	2.6	9	2.3	3	1.3	10	2.0	8	2.4	5	2.4	58	18.6	28	·	·	7	·	·	·	3	16	16	12	1	·	·	3
V	16	2.6	9.5	1.8	13	1.9	11	2.9	2	2.0	9	3.3	15	2.3	11.5	1.7	6	2.2	57	11.6	19	·	·	2	·	1	·	2	15	14	10	1	1	·	4
VI	15.5	2.3	9.5	2.1	9	2.4	4	2.8	7.5	2.9	9.5	3.0	19	2.6	12	1.7	4	2.3	68	11.6	27	·	·	·	5	1	1	2	9	12	10	3	·	·	2
VII	1.5	1.0	2	2.5	11	1.9	4	2.5	9	2.0	20	2.3	31.5	2.2	7	1.6	7	2.0	105	35.0	21	·	·	·	6	·	·	2	10	13	11	3	1	·	7
VIII	5	1.0	9.5	1.5	6	1.5	4	2.6	7	1.8	11.5	1.7	18	1.4	14	1.6	18	1.3	50	13.0	26	·	·	·	10	·	·	1	9	11	8	3	5	·	2
IX	·	·	·	·	6	1.2	17	2.3	14.5	2.4	17.5	2.1	18	1.8	5	1.8	12	1.8	71	41.3	4	·	·	·	2	·	·	4	5	7	4	2	4	·	·
X	5	1.2	5	1.2	8	1.4	4	1.2	7	2.1	18	1.9	16.5	2.3	11.5	1.9	18	1.5	5	3.3	16	·	·	6	·	·	·	4	13	3	2	·	11	·	·
XI	·	·	12	1.8	14	2.0	4.5	2.7	11.5	3.5	13	2.7	22	2.2	·	·	13	2.0	20	5.3	15	7	10	19	·	·	·	1	20	18	5	·	8	13	·
XII	0.5	1.0	1.5	1.0	5	1.0	7	2.0	19	4.1	30	4.4	18	2.2	6	1.7	6	3.0	36	14.6	18	2	6	18	·	4	1	·	22	13	7	1	3	5	·
Rok	80.5	1.7	73.5	1.6	106.5	1.8	105	2.2	116.5	2.8	177	2.8	216.5	2.4	103.5	1.9	116	2.2	520	41.3	4.IX	26	48	123	23	12	4	21	161	150	86	14	41	70	18

Świder $H_s = 94\ m$ $h_w = 16{,}9\ m$

I	6	1.9	3.5	2.6	9	2.3	23	2.7	17.5	2.2	9.5	2.6	6.5	3.4	5	2.5	14	2.1	29	6.2	20	3	6	27	·	·	·	1	17	16	10	·	5	29	·
II	16	2.9	4.5	2.2	1.5	3.0	1.5	1.0	12	2.2	21	2.8	16.5	2.6	3	4.0	9	2.4	38	6.9	7	12	22	27	·	·	·	1	12	20	12	·	·	28	1
III	3.5	1.9	6.5	1.7	7	1.6	23.5	1.9	16.5	2.1	11.5	2.8	8.5	2.7	5	3.6	11	1.9	17	3.8	3	4	6	24	·	·	·	3	15	13	7	·	7	19	·
IV	5.5	1.9	17.5	3.4	14.5	3.5	18	2.6	8	2.4	5.5	2.5	6	2.1	6	2.3	9	2.5	45	17.7	28	·	·	5	·	·	·	·	15	12	5	2	2	·	2
V	7.5	2.1	10	2.6	9.5	2.7	7	2.5	7.5	2.1	9.5	2.6	9	2.3	16	2.2	17	1.9	88	26.8	29	·	·	4	·	·	·	2	15	14	12	3	3	·	5
VI	7	2.4	13	2.9	6	3.2	7	2.9	6.5	3.7	15	3.2	13	2.9	5.5	2.2	17	2.4	73	23.0	14	·	·	·	7	·	·	2	9	15	12	1	·	·	4
VII	4	1.6	6.5	2.8	5.5	2.6	7	3.0	19.5	2.3	29.5	3.2	5	3.2	1	1.0	15	2.3	107	61.8	17	·	·	·	8	·	·	3	9	17	15	1	·	·	6
VIII	2.5	3.6	1	1.0	3	1.7	13.5	3.1	10	2.8	13	2.3	11.5	2.3	12.5	3.4	26	2.0	114	46.0	26	·	·	·	10	·	·	2	8	12	10	3	·	·	2
IX	·	·	1.5	1.0	7	1.7	27	2.6	12.5	2.4	12.5	2.7	7.5	2.1	·	·	22	1.8	64	35.4	29	·	·	·	6	·	·	6	7	10	6	2	1	·	·
X	8	1.1	2.5	1.8	3	2.0	8	1.4	10.5	1.9	14.5	2.6	17.5	1.9	7	1.6	22	1.4	8	5.2	16	·	·	7	·	·	·	3	10	5	2	·	11	·	·
XI	8	1.8	11	1.9	6	2.1	15.5	2.7	10.5	2.2	16.5	3.0	8.5	2.2	·	·	14	2.0	44	7.9	21	6	11	22	·	·	·	·	24	21	10	·	4	18	·
XII	1.5	1.3	2	1.2	3.5	1.7	19.5	3.0	23.5	2.9	22	2.5	7.5	2.0	1.5	1.3	12	2.2	61	14.9	18	2	7	26	·	·	·	·	22	19	11	1	2	14	·
Rok	68.5	1.9	79.5	2.1	75.5	2.3	170.5	2.4	154.5	2.4	180	2.7	116	2.5	62.5	2.0	188	2.1	688	61.8	17.VII	27	52	146	31	·	·	23	163	174	112	13	35	108	20

Uwaga. Kierunki i prędkości wiatru – wg anemografu Fuess.

Śrem — φ = 52°05' — λ = 17°01' — 1965

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	2.1	-1.9	6.5	1	-5.8	7	-0.5	1.3	-0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.5	7.5	7.6
II	–	–	–	–	-0.8	-7.5	3.1	13	-15.9	6	-4.9	-1.9	-3.7	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.8	7.4	7.4
III	–	–	–	–	6.0	-3.7	15.5	29	-20.1	9	-2.5	4.4	0.2	0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.7	5.3	6.1
IV	–	–	–	–	11.5	3.0	16.3	6	-1.2	5	4.4	10.2	6.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	5.8	6.8
V	–	–	–	–	15.2	6.3	22.6	17	-0.5	3	8.8	13.6	10.1	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.6	7.0	7.1
VI	–	–	–	–	21.7	11.2	31.9	26	6.0	3	14.8	20.1	15.7	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.5	6.0	5.9
VII	–	–	–	–	21.2	11.5	30.6	14	5.1	5	14.3	19.2	15.3	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	6.6	7.1
VIII	–	–	–	–	22.0	10.0	30.5	6	5.6	13, 14	13.1	20.2	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.5	3.6	5.0
IX	–	–	–	–	20.8	9.5	28.1	3	4.4	21	11.3	19.1	13.2	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	3.0	4.8
X	–	–	–	–	13.7	2.8	23.2	1	-4.6	23	4.1	12.4	6.3	7.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.0	3.3	4.7
XI	–	–	–	–	2.1	-3.3	12.9	1	-16.1	23	-1.8	1.0	-0.8	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.4	7.3	8.1
XII	–	–	–	–	3.4	-1.0	12.2	19	-7.7	17	0.3	2.2	1.3	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.4	7.8	7.8
Rok	–	–	–	–	11.6	3.1	31.9	26.VI	-20.1	9.III	5.1	10.2	6.6	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	5.9	6.5

Topola - Błonie — φ = 52°05' — λ = 19°11'

Miesiąc	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.4	-3.0	5.0	18	-10.7	11	-1.2	0.8	-0.8	-0.5	5.3	5.6	5.4	5.4	93	86	92	90	0.4	0.9	0.5	0.6	8.4	8.2	6.4	7.7
II	–	–	–	–	-2.2	-10.4	2.4	13	-19.2	6	-6.5	-3.5	-5.9	-5.4	3.5	4.0	3.6	3.7	88	83	87	86	0.5	0.8	0.5	0.6	7.7	7.6	6.5	7.3
III	–	–	–	–	4.9	-4.0	12.6	30	-17.4	9	-2.2	3.6	0.5	0.6	5.3	6.2	5.8	5.8	93	76	87	85	0.4	2.1	0.9	1.1	6.6	6.3	5.1	6.0
IV	–	–	–	–	10.1	2.7	15.2	30	-1.0	11	4.1	9.1	6.0	6.3	7.6	8.1	8.0	7.9	91	71	84	82	0.7	3.6	1.5	1.9	7.3	7.6	5.4	6.8
V	–	–	–	–	13.8	5.9	22.1	17	-0.9	3	8.6	12.8	9.8	10.2	9.8	10.0	10.1	10.0	86	67	82	78	1.6	5.0	2.2	2.9	6.4	7.6	6.1	6.7
VI	–	–	–	–	20.8	11.0	31.5	26	5.7	3	14.4	19.5	15.7	16.4	13.6	13.6	14.1	13.8	83	61	79	74	3.0	9.7	4.0	5.6	5.4	6.2	5.4	5.7
VII	–	–	–	–	21.3	11.1	30.3	14	6.0	5	14.5	19.7	15.1	16.1	14.5	14.3	14.6	14.5	87	61	84	77	2.2	9.4	2.8	4.8	6.4	7.2	5.1	6.2
VIII	–	–	–	–	21.5	9.9	30.9	7	5.5	14	13.0	20.3	14.8	15.7	13.7	13.2	14.3	13.7	91	57	84	77	1.6	11.5	3.0	5.4	5.5	6.0	5.8	5.8
IX	–	–	–	–	20.8	9.2	28.3	3	2.9	21	11.2	19.4	13.3	14.3	12.6	13.1	13.2	13.0	93	59	86	79	1.0	10.0	2.3	4.4	5.7	5.1	2.9	4.6
X	–	–	–	–	12.2	2.4	21.1	1	-4.7	22	4.2	11.2	6.2	7.0	8.1	9.4	8.9	8.8	95	70	91	85	0.4	4.3	0.8	1.8	6.3	6.5	4.9	5.9
XI	–	–	–	–	1.5	-4.7	12.2	2	-18.8	17	-2.7	0.5	-1.2	-1.2	5.0	5.7	5.3	5.3	89	84	87	87	0.5	1.2	0.8	0.8	8.6	8.1	8.5	8.4
XII	–	–	–	–	2.6	-2.1	10.2	19	-19.7	17	-0.2	1.4	0.3	0.4	5.5	5.7	5.7	5.6	88	83	89	87	0.7	1.2	0.7	0.8	8.4	7.9	7.6	8.0
Rok	–	–	–	–	10.7	2.3	31.5	26.VI	-19.7	17.XII	4.8	9.6	6.2	6.7	8.7	9.1	9.1	9.0	90	72	86	83	1.1	5.0	1.7	2.6	6.9	7.0	5.8	6.6

Terespol — φ = 52°05' — λ = 23°37'

Miesiąc	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	996.4	1013.6	976.9	1013.6	-0.1	-5.6	3.4	9	-17.5	11	-3.2	-1.5	-2.8	-2.6	4.6	4.8	4.6	4.7	90	84	89	88	0.5	0.8	0.5	0.6	8.5	8.5	7.4	8.1
II	997.2	1016.6	974.7	1014.6	-3.3	-10.3	2.6	14	-22.6	7	-7.7	-4.7	-6.6	-6.4	3.3	3.6	3.4	3.4	89	80	84	84	0.4	0.8	0.6	0.6	7.7	7.5	7.2	7.5
III	1000.9	1017.6	974.2	1017.9	4.3	-3.6	14.3	30	-16.9	9	-2.2	3.2	0.1	0.3	4.9	5.7	5.3	5.3	89	73	83	82	0.6	2.3	1.1	1.3	7.6	6.7	5.5	6.6
IV	996.2	1010.0	977.6	1012.8	10.4	2.5	17.1	26	-3.1	3	3.6	8.8	5.6	5.9	6.6	6.6	7.2	6.8	81	58	76	72	1.5	5.0	2.1	2.9	8.1	7.5	6.1	7.2
V	997.4	1013.3	983.2	1013.8	15.2	5.7	26.0	19	-2.7	4	8.4	13.8	10.1	10.6	9.2	9.2	9.8	9.4	81	56	77	71	2.1	7.2	2.9	4.1	6.8	7.9	6.7	7.1
VI	997.8	1004.5	987.8	1013.8	20.7	11.8	28.6	26	5.4	8	14.5	19.2	15.7	16.3	13.6	13.7	14.2	13.8	82	63	79	75	3.1	9.1	4.0	5.4	6.1	6.7	7.4	6.7
VII	996.3	1007.4	984.2	1012.3	22.3	11.6	29.8	16	7.0	5	15.2	20.6	16.0	17.0	14.2	13.4	14.4	14.0	82	55	78	72	3.3	11.3	4.2	6.3	4.3	7.6	6.3	6.1
VIII	998.9	1007.7	984.8	1014.9	21.2	10.8	28.5	7	6.5	16	13.2	19.9	14.6	15.6	13.7	14.4	14.5	14.2	89	62	86	79	1.8	9.7	2.4	4.6	5.8	6.0	4.1	5.3
IX	1000.4	1016.5	989.9	1016.5	21.3	9.1	27.3	4	4.7	17	11.1	20.4	13.6	14.7	12.6	14.5	14.1	13.7	94	60	89	81	0.9	10.0	1.7	4.2	4.6	5.6	4.4	4.9
X	1005.8	1021.6	992.5	1022.5	11.5	2.5	20.0	1	-5.5	21	3.9	10.4	6.4	6.8	7.7	9.2	8.5	8.5	94	72	88	85	0.5	3.8	1.3	1.9	7.1	6.8	5.2	6.4
XI	996.4	1012.1	970.6	1013.5	0.7	-4.4	12.2	2	-20.0	17	-2.3	-0.6	-2.1	-1.8	5.0	5.3	5.0	5.1	89	84	88	87	0.6	1.1	0.7	0.8	9.9	8.7	7.9	8.8
XII	990.7	1005.3	970.8	1007.6	1.5	-2.4	7.3	19, 20	-15.6	17	-1.0	0.7	-0.2	-0.2	5.2	5.5	5.2	5.3	88	83	85	85	0.7	1.2	0.9	0.9	9.2	8.5	8.0	8.6
Rok	997.8	1021.6	970.6	1014.5	10.5	2.3	29.8	16.VII	-22.6	7.II	4.5	9.2	5.9	6.4	8.4	8.8	8.8	8.7	87	69	84	80	1.3	5.2	1.9	2.8	7.1	7.3	6.4	6.9

Młochów — φ = 52°03' — λ = 20°47'

Miesiąc	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	-4.0	4.5	18, 19	-15.6	11	-2.3	-0.4	-1.6	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-2.4	-9.6	3.9	13	-22.8	6	-7.0	-4.2	-5.9	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	4.8	-3.3	13.1	30	-16.5	8	-1.8	3.4	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.1	2.0	14.7	29	-2.9	3	3.8	8.6	5.5	5.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	13.6	5.1	20.8	17	-2.3	4	8.5	12.1	9.1	9.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.8	11.1	30.0	26	7.4	15	14.5	18.9	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	12.0	29.2	16	7.2	4, 6	15.3	19.8	14.7	16.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.1	11.0	29.9	7	6.4	16	13.6	19.4	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.7	9.8	26.9	2	4.8	16	11.7	19.2	13.9	14.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.1	3.4	21.1	1	-4.5	22	5.0	11.1	7.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.3	-3.8	11.8	2	-17.0	18	-2.3	-0.1	-1.2	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.1	-2.2	9.5	20	-17.7	17	-0.3	0.9	0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.5	2.6	30.0	26.VI	-22.8	6.II	4.9	9.1	6.0	6.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Śrem $H_s = 85$ m $h_w = 10$ m   1965

MIESIĄC	ROZKŁAD WIATRU (D, V, D) N n	N v	NE n	NE v	F n	F v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Max<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5.5	2.5	4	2.5	15	2.1	7	2.3	19	3.8	9	4.4	14	3.5	2.5	2.6	17	2.6	30	5.5	17	·	3	26	·	·	·	2	15	16	10	·	3	20	·
II	11.5	3.5	10.5	3.6	2	3.8	2	1.5	6	3.5	16	5.6	20	5.7	9	4.4	7	4.2	9	2.9	17	7	18	28	·	3	·	2	15	16	2	·	2	26	·
III	7	2.9	8.5	3.2	4	2.9	6	2.4	9	1.7	12	3.4	10	5.3	8.5	3.8	28	2.3	26	10.7	3	5	6	20	·	·	·	6	12	12	6	1	5	15	·
IV	12	1.9	15	3.9	12.5	3.5	9.5	2.3	7	2.6	8.5	3.3	7	4.8	7.5	3.5	11	2.8	43	11.2	19	·	·	3	·	·	·	5	15	14	12	1	·	·	1
V	14	2.3	21.5	2.7	9.5	3.7	2	3.2	5	2.7	8	3.1	10	5.4	10	2.9	13	2.7	86	16.1	19	·	·	1	·	2	·	2	15	21	16	3	1	·	2
VI	3	4.0	19.5	3.3	3	4.0	7	2.0	10.5	3.0	7.5	3.7	13	4.6	8.5	3.3	18	2.8	43	13.9	1	·	·	·	5	·	·	5	7	13	8	1	·	·	3
VII	7	2.2	9	3.0	3	3.5	2.5	1.6	12.5	2.8	26.5	4.0	16.5	4.3	3	3.8	13	3.0	133	47.7	15	·	·	·	3	1	·	1	11	18	12	3	·	·	5
VIII	9.5	1.5	1.5	1.0	0.5	3.0	6.5	3.5	7.5	2.3	7	2.8	15.5	3.5	9	2.0	36	1.6	11	4.6	25	·	·	·	8	·	·	5	4	11	3	·	1	·	2
IX	0.5	3.0	1	3.5	7	2.2	9	2.8	14.5	2.0	14	3.4	12	3.5	3	1.5	29	1.9	29	18.9	10	·	·	·	3	·	·	6	4	6	5	1	2	·	·
X	3.5	1.9	7	1.6	7	2.2	3	1.7	9.5	2.4	9	3.2	14	3.4	6	2.1	34	1.6	9	5.2	16	·	·	8	·	·	·	7	6	3	3	·	8	·	·
XI	0.5	3.0	23	3.0	6	2.8	3.5	3.6	7	4.1	20.5	4.3	7.5	5.3	3	2.0	19	2.9	29	6.2	21	5	11	19	·	1	·	2	21	16	8	·	8	15	·
XII	1.5	2.7	6.5	2.5	5.5	2.8	8	3.6	23	5.1	25.5	4.9	13	5.1	2	4.0	8	4.1	36	9.3	18	·	3	19	·	1	·	·	17	20	10	·	1	8	·
Rok	75.5	2.6	127	2.8	75	3.0	66	2.5	130.5	3.0	163.5	3.8	152.5	4.5	72	3.0	233	2.7	484	47.7	15.VII	17	41	124	19	8	·	43	142	166	95	10	31	84	13

Topola – Błonie $H_s = 109$ m $h_w = 12$ m

I	6	2.6	6.5	2.4	13.5	2.4	8	3.9	16	4.7	17.5	4.7	9	3.6	7.5	4.7	9	3.5	20	3.6	8	1	8	28	·	4	·	2	16	14	6	·	4	7	·
II	9	4.9	11.5	5.7	2	4.0	1	1.0	4.5	5.2	17.5	6.4	20	5.3	13.5	6.3	5	5.3	14	2.4	15	17	20	28	·	4	2	3	13	15	6	·	8	28	·
III	3.5	3.9	15	3.8	6.5	4.1	5.5	2.7	10.5	2.6	17	5.5	9.5	3.9	5.5	5.5	20	3.2	33	19.3	4	6	7	21	·	4	·	5	12	12	4	1	3	16	·
IV	6.5	3.6	14	3.8	22	4.5	14.5	3.6	6	2.4	5	3.7	6.5	4.9	8.5	3.5	7	3.6	46	8.6	23	·	·	4	·	1	·	3	13	13	11	·	2	·	1
V	10.5	4.0	13.5	3.9	15.5	4.1	3	4.8	1	4.0	10	4.8	9.5	3.5	12	3.2	18	3.2	89	22.2	19	·	·	2	·	2	1	3	13	18	14	2	2	·	2
VI	8.5	4.3	10.5	4.3	12	4.2	3	3.8	7	4.8	11	4.2	14	3.9	8	3.9	16	3.4	56	20.4	26	·	·	·	3	1	1	5	10	15	12	1	·	·	4
VII	1	3.5	6.5	4.5	7.5	3.0	3.5	3.7	9.5	2.5	28.5	4.3	22.5	3.9	4	2.9	10	3.4	58	13.0	17	·	·	·	4	1	·	2	8	18	12	1	·	·	8
VIII	5.5	1.4	3	3.0	1	2.0	6	3.0	10	3.2	10.5	2.9	18	3.1	11	2.9	28	2.0	45	10.7	25	·	·	·	9	·	·	5	9	14	11	1	3	·	2
IX	1.5	4.0	4	2.6	9.5	2.6	9	2.9	14.5	3.4	17	4.7	11	3.7	1.5	3.3	22	2.7	58	37.7	4	·	·	·	2	·	·	7	4	6	4	1	3	·	·
X	5.5	2.0	4.5	3.0	8.5	1.7	4.5	1.9	3.5	1.7	16.5	3.8	11.5	3.7	12.5	3.6	26	2.2	5	3.5	16	·	·	7	·	·	·	5	12	4	2	·	10	·	·
XI	2.5	1.8	16	5.3	11.5	3.7	9	4.1	7.5	3.3	23	5.8	10.5	5.0	5	3.2	5	4.4	25	7.2	21	6	10	22	·	3	·	2	21	13	8	·	7	14	·
XII	0.5	3.0	2	2.8	4.5	1.8	9.5	3.8	20.5	5.4	35	6.2	8	4.1	9	4.2	4	4.8	40	15.9	18	2	4	20	·	6	·	1	19	13	9	1	2	7	·
Rok	60.5	3.2	107	3.8	114	3.2	76.5	3.3	110.5	3.6	208.5	4.8	150	4.0	98	3.9	170	3.5	489	37.7	4.IX	32	49	132	18	26	4	43	150	155	99	8	44	72	17

Terespol $H_s = 133$ m $H_b = 135{,}0$ m $h_w = 14{,}4$ m

I	4	3.1	5	3.7	18	3.8	20	3.0	15	3.8	11	3.9	8.5	5.4	8.5	5.2	3	3.8	39	10.5	17	5	13	29	·	1	·	2	19	16	10	1	8	31	·
II	12.5	4.7	7.5	5.1	1.5	1.0	0.5	1.0	5.5	4.5	21.5	4.9	21	4.1	13	4.6	1	4.5	26	5.2	16	11	23	28	·	·	·	1	13	22	9	·	1	28	·
III	2.5	4.0	10	2.6	5.5	2.5	27.5	3.0	9.5	2.5	13	4.0	10.5	3.1	8.5	5.7	6	3.1	24	6.7	2	3	6	22	·	·	·	5	13	12	7	·	2	17	·
IV	6.5	4.5	13	5.3	23.5	4.4	21.5	4.6	10.5	3.6	5.5	3.5	3	4.0	5.5	5.4	1	4.4	43	11.5	21	·	·	9	·	·	·	1	15	11	7	2	1	·	2
V	13.5	3.8	8.5	2.9	16	4.6	3	2.8	6.5	1.9	7	5.2	7	3.1	23.5	3.8	8	3.4	63	27.7	29	·	·	3	1	·	·	·	12	14	9	1	·	·	4
VI	10	2.5	12.5	4.5	9	4.9	5.5	4.5	2.5	4.0	2.5	4.2	18.5	3.5	21.5	3.4	8	3.5	125	30.6	14	·	·	·	6	1	1	2	12	14	10	4	·	·	2
VII	2	1.2	9	3.4	5.5	2.5	5	2.2	9.5	2.8	20	3.2	24.5	3.3	11.5	3.1	6	2.9	129	53.5	17	·	·	·	6	1	1	1	8	18	10	3	1	·	4
VIII	7	3.9	1	1.0	5	2.8	10	3.6	11.5	2.9	11	3.2	24	3.2	15.5	3.4	8	3.0	63	27.6	2	·	·	·	10	·	·	7	5	12	9	1	·	·	2
IX	·	·	·	·	11	2.6	31.5	3.6	17	3.2	15.5	3.4	9	3.0	5	2.2	1	3.2	29	12.6	11	·	·	·	4	·	·	3	4	7	5	1	·	·	1
X	4	2.9	3.5	3.3	2	4.2	4	2.9	15	2.8	15.5	3.5	21	3.8	21	3.3	7	3.1	5	2.5	11	·	·	5	·	·	·	3	11	6	2	·	10	·	·
XI	1	2.0	14	5.4	8.5	3.2	16	4.5	5.5	3.9	18	4.5	19	4.6	3	1.7	5	4.1	44	7.0	21	4	12	21	·	·	·	·	24	17	11	·	5	18	·
XII	2	3.0	2	2.5	5.5	3.8	10.5	4.1	30	4.9	27.5	4.3	8.5	4.8	6	3.0	1	4.3	26	6.0	18	2	5	26	·	·	·	·	21	13	8	·	1	12	·
Rok	65	3.0	86	3.3	111	3.4	155	3.3	138	3.4	168	4.0	174.5	3.8	142.5	3.7	55	3.6	616	53.5	17.VII	25	59	143	27	3	2	25	157	162	97	13	29	106	15

Uwaga. Kierunki i prędkości wiatru – wg anemometru M – 47.

Młochów $H_s = 141$ $h_w = 12{,}5$ m

I	5.5	5.5	2.5	5.2	5	2.8	17	3.6	14	3.6	20.5	5.2	8.5	5.9	9	5.1	11	4.0	29	6.3	20	4	13	27	·	2	·	–	–	12	10	·	4	21	·
II	9.5	5.5	6	3.2	·	·	1	3.0	4	4.1	16	4.7	23	6.0	13.5	6.8	11	4.7	15	3.1	17	9	24	27	·	2	1	–	–	14	6	·	1^{2}	28	·
III	·	·	5.5	4.9	4.5	2.4	15	2.8	16.5	2.7	21	5.1	13.5	4.7	6	7.0	11	3.6	13	3.0	2	4	8	20	·	2	·	–	–	10	4	·	3	16	·
IV	3	4.0	8	4.5	23	5.7	19	4.5	7	2.8	8.5	4.0	6.5	3.8	8	5.3	7	4.3	64	22.7	28	·	·	8	·	·	·	–	–	14	9	2	1	·	1
V	3.5	3.6	12	3.2	12	3.3	8.5	3.9	5.5	4.1	13.5	4.6	14	3.5	16	4.7	8	3.6	83	19.6	29	·	·	3	·	2	·	–	–	15	13	3	·	·	4
VI	5	3.3	10	4.2	11	4.7	4.5	3.6	6	3.0	14	4.0	18.5	5.2	17	3.6	4	4.0	96	24.0	14	·	·	·	3	1	·	–	–	12	11	3	·	·	4
VII	1	3.0	7.5	3.0	8.5	2.2	3	2.5	6.5	3.2	27	3.9	31.5	3.7	5	2.7	3	3.3	75	20.5	21	·	·	·	4	·	·	–	–	17	14	2	1	·	3
VIII	5.5	3.5	1.5	3.3	4.5	4.3	7.5	2.8	10	3.1	14.5	3.8	22.5	3.9	18	4.4	9	3.4	86	43.5	26	·	·	·	9	·	·	–	–	9	8	3	·	·	1
IX	0.5	7.0	·	·	10	3.3	15	3.8	14	4.1	23.5	4.2	17.5	3.7	2.5	4.0	7	3.6	46	22.2	29	·	·	·	2	1	·	–	–	11	9	1	·	·	2
X	6.5	2.7	7	1.6	4	2.1	6.5	2.2	2.5	3.0	23	4.8	20.5	5.4	20	3.7	3	3.8	9	5.0	16	·	·	4	·	1	·	–	–	6	2	·	6	·	·
XI	1	1.5	13.5	5.5	6.5	3.8	14	4.3	8	4.2	18	5.7	19.5	5.2	3.5	4.1	6	4.6	40	8.3	21	5	12	21	·	1	·	–	–	18	11	·	4	17	·
XII	1	3.5	2	3.0	2	4.0	14	3.6	14	4.9	34	6.3	18.5	3.9	4.5	3.4	3	4.7	46	13.5	18	2	7	21	·	3	1	–	–	12	10	1	2	11	·
Rok	42	3.6	75.5	3.5	91	3.2	125	3.4	108	3.6	233.5	4.7	214	4.6	123	4.6	83	4.0	602	43.5	26.VIII	24	64	131	18	15	2	–	–	150	107	15	22^{2}	93	15

Trzebiechów

φ = 52°01' λ = 15°44'

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.3	−0.8	8.7	17	−6.2	7	0.4	2.4	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.4	−5.4	4.3	14	−14.3	28	−3.9	−1.1	−1.9	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	6.8	−4.1	15.4	29	−20.9	8	−2.4	5.2	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	12.6	3.1	18.2	6	−1.7	1	5.2	10.7	8.0	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.2	6.5	23.8	17	0.2	22	9.8	14.7	11.4	11.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	22.6	10.9	32.2	26	5.7	3	14.9	20.9	16.2	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.3	11.6	32.6	14	5.7	4	14.9	19.6	15.6	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.5	10.1	31.6	6	6.0	13	13.2	20.9	15.7	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.6	8.6	27.3	2	3.1	21	11.2	19.5	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.8	2.7	23.2	1	−5.8	23	4.3	12.9	7.5	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3.6	−2.3	14.4	2	−14.6	23	−1.0	1.7	0.5	0.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	4.6	−0.3	13.7	19	−6.4	14	1.1	3.2	2.2	2.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.4	3.4	32.6	14.VII	−20.9	8.III	5.6	10.9	7.6	7.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biała Podlaska

φ = 52°01' λ = 23°08'

I	–	–	–	–	0.2	−5.9	3.6	9	−19.5	11	−3.5	−1.7	−2.9	−2.8	4.5	4.6	4.5	4.5	91	83	87	87	0.4	0.9	0.6	0.6	8.3	8.2	6.8	7.8
II	–	–	–	–	−3.1	−11.0	2.4	14	−24.0	7	−7.8	−4.5	−6.7	−6.4	3.2	3.5	3.3	3.3	88	77	82	82	0.4	1.0	0.6	0.7	7.9	7.7	6.0	7.2
III	–	–	–	–	4.4	−4.1	14.2	30	−17.6	1	−2.4	3.3	−0.3	0.1	4.9	5.6	5.3	5.3	91	71	85	82	0.5	2.4	0.9	1.3	7.3	6.6	5.0	6.3
IV	–	–	–	–	10.6	1.9	15.8	26	−3.7	3	3.6	9.1	5.2	5.8	7.0	7.1	7.4	7.2	87	62	81	77	1.1	4.6	1.6	2.4	8.3	7.4	5.3	7.0
V	–	–	–	–	14.9	5.2	24.7	19	−2.2	4	8.2	13.8	9.8	10.4	9.3	9.1	9.7	9.4	83	57	78	73	1.9	7.1	2.6	3.9	7.4	7.9	6.0	7.1
VI	–	–	–	–	20.9	11.0	28.9	26	3.7	8	14.6	19.3	15.5	16.2	13.6	13.3	14.2	13.7	82	61	80	74	3.2	9.8	3.7	5.6	6.1	6.6	7.2	6.6
VII	–	–	–	–	22.1	10.7	30.2	16	5.9	5, 12	15.3	20.6	15.6	16.8	14.4	13.4	14.5	14.1	82	56	81	73	3.3	11.4	3.6	6.1	4.7	7.1	6.0	5.9
VIII	–	–	–	–	21.0	10.2	29.3	8	5.7	30	13.1	19.6	14.3	15.3	13.4	13.8	14.5	13.9	88	61	88	79	1.9	9.8	2.2	4.6	5.3	6.3	3.9	5.2
IX	–	–	–	–	21.3	8.2	27.5	3	2.7	17, 21	10.7	20.4	13.2	14.4	12.3	13.6	13.5	13.1	94	57	88	80	0.8	10.8	2.0	4.5	4.7	4.9	2.9	4.2
X	–	–	–	–	11.8	2.3	21.1	1	−5.7	21	3.6	10.5	6.5	6.8	7.6	9.1	8.8	8.5	95	71	89	85	0.5	4.1	1.1	1.9	6.9	6.7	5.6	6.4
XI	–	–	–	–	0.8	−4.5	12.2	2	−20.0	17	−2.3	−0.6	−2.1	−1.8	5.2	5.3	5.2	5.2	93	87	92	91	0.4	1.0	0.5	0.6	9.7	9.1	7.9	8.9
XII	–	–	–	–	1.5	−2.8	7.8	19	−17.0	17	−1.0	0.6	−0.3	−0.2	5.4	5.6	5.3	5.4	92	86	88	89	0.5	0.9	0.8	0.7	9.2	8.6	7.7	8.5
Rok	–	–	–	–	10.5	1.8	30.2	16.VII	−24.0	7. II	4.3	9.2	5.6	6.2	8.4	8.7	8.8	8.6	89	69	85	81	1.2	5.3	1.7	2.7	7.2	7.3	5.9	6.8

Skierniewice

φ = 51°58' λ = 20°10'

I	996.2	1012.0	976.1	1012.6	1.2	−4.1	5.1	18	−14.9	23	−2.1	0.0	−1.4	−1.2	4.9	5.3	4.9	5.0	90	86	85	87	0.5	0.9	0.8	0.7	8.5	7.3	6.8	7.5
II	999.6	1017.4	975.4	1016.3	−2.1	−9.4	2.8	13	−20.0	6	−6.9	−3.8	−5.8	−5.6	3.4	3.8	3.4	3.5	89	79	81	83	0.4	0.9	0.7	0.7	8.5	6.7	7.2	7.5
III	1001.0	1017.0	973.3	1017.3	5.2	−3.2	13.8	30	−16.5	8	−1.6	3.8	0.3	0.7	5.2	5.7	5.4	5.4	89	69	82	80	0.6	2.7	1.1	1.5	6.3	5.5	4.7	5.5
IV	995.7	1016.2	980.2	1011.6	9.9	2.2	14.9	29	−2.5	15	3.9	8.6	5.1	5.7	7.3	7.7	7.5	7.5	88	69	84	80	0.9	3.7	1.4	2.0	6.9	7.9	5.0	6.6
V	998.4	1014.5	984.1	1014.1	13.7	5.3	20.5	17	−2.6	4	8.7	12.2	8.9	9.7	9.5	9.5	9.9	9.6	82	66	85	78	2.0	5.0	1.8	2.9	6.9	7.9	6.1	7.0
VI	998.7	1007.3	988.7	1014.1	21.0	11.1	29.8	26	6.5	15	14.8	19.4	15.0	16.0	13.6	13.3	13.8	13.6	80	60	80	73	3.4	9.9	3.5	5.6	5.1	6.3	5.9	5.8
VII	996.7	1006.5	982.9	1012.1	21.5	11.3	29.8	14	6.4	4	15.4	20.0	15.1	16.4	14.3	13.7	14.7	14.2	81	58	84	74	3.4	10.4	2.8	5.5	6.3	8.0	6.6	7.0
VIII	1000.2	1007.6	989.1	1015.6	21.4	10.5	30.8	7	5.1	16	13.5	19.9	14.5	15.6	13.7	13.0	13.8	13.5	88	58	84	77	2.2	11.3	3.2	5.6	5.7	6.4	5.0	5.7
IX	1000.1	1018.1	988.5	1015.6	20.8	9.6	27.3	3	3.5	16	11.9	19.4	13.4	14.5	12.8	13.0	13.3	13.0	91	59	86	79	1.3	10.1	2.4	4.6	5.1	4.8	3.5	4.5
X	1007.3	1022.3	994.3	1023.3	12.0	3.1	22.1	1	−5.1	22	4.8	10.9	6.6	7.2	8.7	9.3	9.0	8.8	92	71	90	84	0.6	4.1	1.1	1.9	6.1	6.2	5.5	5.9
XI	996.3	1013.9	970.3	1012.7	1.9	−4.2	12.6	2	−19.2	18	−2.4	0.1	−1.1	−1.1	5.0	5.4	5.3	5.2	88	85	87	87	0.7	1.2	0.8	0.9	8.4	8.1	7.4	7.9
XII	990.4	1007.5	968.4	1006.6	2.7	−1.0	10.5	20	−17.4	16	0.0	1.3	0.3	0.5	5.5	5.7	5.5	5.6	88	84	85	86	0.8	1.2	0.9	1.0	7.6	7.9	8.2	7.9
Rok	998.4	1022.3	968.4	1014.3	10.8	2.6	30.8	7.VIII	−20.0	6. II	5.0	9.3	5.9	6.5	8.6	8.8	8.9	8.8	87	70	84	80	1.4	5.1	1.7	2.7	6.8	6.9	6.0	6.6

Zielona Góra

φ = 51°56' λ = 15°30'

I	990.0	1005.8	970.2	1011.7	2.8	−1.2	7.9	17	−6.0	7	0.0	1.7	0.4	0.6	5.7	5.8	5.8	5.8	93	84	91	89	0.5	1.2	0.6	0.8	8.2	8.5	8.4	8.4
II	996.6	1011.5	970.8	1018.9	−0.5	−5.7	3.6	14	−12.4	6	−4.3	−2.1	−3.0	−3.1	4.3	4.3	4.6	4.4	93	81	90	88	0.3	1.0	0.4	0.6	8.8	8.2	8.6	8.5
III	995.5	1011.0	969.8	1017.2	6.2	−1.9	14.8	29	−15.3	8	−1.0	4.8	1.5	1.7	5.3	5.6	5.5	5.5	88	65	78	77	0.8	3.5	1.6	2.0	7.1	6.6	5.4	6.4
IV	989.7	1011.5	971.9	1010.9	11.7	3.5	17.8	6	0.1	1	4.6	9.8	7.1	7.2	7.2	7.4	7.6	7.4	85	63	76	75	1.3	5.0	2.6	3.0	8.0	8.2	6.6	7.6
V	993.3	1007.4	981.0	1014.3	15.6	6.9	23.3	17	0.1	3	8.9	13.7	10.6	11.0	9.6	9.3	9.6	9.5	82	60	74	72	1.9	6.7	3.3	4.0	6.8	8.2	7.2	7.4
VI	993.9	1005.7	981.2	1014.5	21.7	11.8	31.4	26	6.7	2	14.4	19.3	16.3	16.6	12.6	12.2	13.0	12.6	77	55	71	68	4.0	10.7	5.9	6.9	5.9	8.2	6.1	6.7
VII	991.5	999.8	977.7	1012.1	20.7	12.2	32.4	14	7.2	4	14.0	18.2	15.8	16.0	13.4	13.9	13.8	13.7	83	66	76	75	2.8	7.8	4.5	5.0	7.6	8.3	7.7	7.9
VIII	995.4	1003.8	981.0	1016.1	21.6	11.6	30.4	6	7.6	13	13.5	19.8	15.8	16.2	12.7	12.5	12.6	12.6	81	55	71	69	3.0	11.2	5.7	6.6	5.2	7.1	4.8	5.7
IX	993.3	1014.2	978.5	1014.1	19.8	10.4	26.4	2	6.6	20	11.7	18.1	13.9	14.4	12.0	12.4	12.8	12.4	87	61	81	76	1.9	8.9	3.3	4.7	4.9	7.4	3.8	5.4
X	1002.3	1015.4	989.6	1023.6	13.3	4.9	22.3	1	−2.3	22	5.9	11.9	8.3	8.6	8.6	9.7	9.2	9.2	90	69	82	80	1.0	4.8	2.1	2.6	6.1	6.8	4.6	5.8
XI	990.1	1011.2	960.6	1011.9	2.8	−2.6	13.8	1	−12.4	23	−1.0	1.2	−0.3	−0.1	5.4	5.6	5.4	5.5	90	80	86	85	0.6	1.6	1.0	1.1	8.2	8.6	7.1	8.0
XII	983.8	1005.0	958.4	1005.3	4.1	−0.6	12.7	19	−6.5	14	0.7	2.4	1.8	1.7	5.7	6.0	6.2	6.0	88	82	88	86	0.8	1.4	1.0	1.1	8.4	8.7	9.2	8.8
Rok	993.0	1015.4	958.4	1014.3	11.6	4.1	32.4	14.VII	−15.3	8.III	5.6	9.9	7.4	7.6	8.5	8.7	8.8	8.7	86	68	80	78	1.6	5.3	2.7	3.2	7.1	7.9	6.6	7.2

Trzebiechów — $H_s = 55\ m$ — $h_w = 10{,}4\ m$ — 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5	2.0	6	1.2	5.5	1.6	12.5	1.4	14	2.9	17	2.4	17	2.9	·	·	16	1.9	33	6.7	9	·	·	24	·	2	·	—	—	14	9	·	3	2	—
II	8	2.1	6	2.2	6.5	1.5	2.5	2.0	1.5	1.0	11	4.0	24.5	4.2	18	5.0	6	3.4	31	4.3	10	3	13	26	·	2	·	—	—	19	11	·	2	18	—
III	6.5	1.9	7.5	1.9	3.5	2.0	8.5	1.6	7	1.3	11	2.0	25	3.1	6	3.5	18	1.9	82	31.0	3	9	5	21	·	1	·	—	—	15	8	3	7	16	—
IV	5	2.0	6.5	3.2	13.5	2.6	12.5	2.0	3	1.7	7.5	1.9	19.5	3.1	9.5	3.4	13	2.2	32	4.0	13	·	·	3	·	·	·	—	—	16	12	·	·	1	—
V	10.5	1.8	6	3.2	17	1.8	2.5	2.2	1	2.0	7.5	2.1	21	3.0	10.5	3.1	17	2.0	73	12.2	10	·	·	·	·	2	·	—	—	18	14	1	·	·	—
VI	4.5	1.7	11.5	1.6	9	1.9	7	1.9	2.5	2.4	10.5	2.9	19.5	3.4	8.5	3.2	17	2.1	39	11.6	1	·	·	·	7	·	·	—	—	13	7	1	·	·	—
VII	5.5	1.7	7	1.9	4.5	1.4	1.5	2.0	3	1.2	19.5	2.4	38.5	3.5	4.5	2.8	9	2.5	122	51.8	16	·	·	·	7	·	·	—	—	20	16	3	·	·	—
VIII	2.5	1.0	2.5	1.4	3.5	1.3	7	2.1	4.5	1.6	10.5	1.5	22	2.3	10.5	2.6	30	1.4	26	7.7	24	·	·	·	8	·	·	—	—	10	6	·	1	·	—
IX	·	·	1.5	1.0	4.5	1.9	13	2.0	10.5	2.4	12	2.1	20.5	2.0	4	3.1	24	1.5	43	16.0	3	·	·	·	3	·	·	—	—	9	7	2	3	·	—
X	1	1.0	1	1.0	12	1.2	5.5	1.0	2	1.2	10	1.6	24.5	3.2	1	1.0	36	1.3	13	5.4	16	·	·	12	·	1	·	—	—	3	3	·	9	·	—
XI	1	1.0	20	2.3	13	2.0	6.5	1.9	3.5	2.0	12.5	3.1	21	4.1	3.5	2.7	9	2.5	34	8.6	27	3	10	18	·	1	·	—	—	15	9	·	6	12	—
XII	1	1.0	·	·	5	1.5	8	1.3	13.5	2.7	26.5	2.7	26.5	2.8	2.5	1.0	10	2.2	56	10.8	18	·	2	20	·	1	·	—	—	22	16	1	2	1	—
Rok	50.5	1.4	75.5	1.7	97.5	1.7	87	1.8	66	1.9	155.5	2.4	279.5	3.1	78.5	2.6	205	2.1	584	51.8	16.VII	15	30	124	25	10	·	—	—	174	118	11	33	49	—

ROZKŁAD WIATRU: n=D, v=D; OPAD R; LICZBA DNI (n): Temperatura T, Wiatr V, Opad R

Biała Podlaska — $H_s = 145\ m$ — $h_w = 12\ m$

I	4.5	2.4	5	3.9	11.5	4.5	17	5.1	17.5	4.3	10	5.1	6	10.2	5.5	9.6	16	4.4	43	12.4	17	4	10	28	·	4	2	3	17	19	12	1	6	31	—
II	15.5	4.6	9	5.7	1	7.0	·	·	4.5	6.9	15	6.4	20.5	6.5	9.5	4.6	9	5.2	26	5.8	7	14	23	28	·	4	2	2	14	19	11	·	1	28	—
III	3.5	6.1	9	3.1	4	3.8	13	4.3	13	3.7	13	5.4	10.5	4.7	6	6.8	21	3.5	22	6.2	17	3	6	25	·	3	2	5	13	12	6	·	5	15	—
IV	4.5	4.3	9	6.6	24.5	8.7	25	6.2	4	4.0	5.5	4.3	0.5	3.0	5	7.0	12	5.8	59	21.8	22	·	·	12	·	13	4	1	15	11	8	2	1	·	—
V	13.5	2.7	8	3.5	12.5	6.9	3	4.3	3.5	3.3	8.5	4.2	8.5	5.5	12.5	5.4	23	3.5	62	15.0	29	·	·	4	·	6	1	1	12	14	12	2	1	·	—
VI	5	4.5	6.5	5.2	11.5	6.4	5.5	5.2	5	5.6	6	5.5	24	5.6	5.5	4.5	21	4.2	59	12.9	14	·	·	·	6	6	2	1	12	10	10	2	·	·	—
VII	1	2.5	5.5	3.8	3	3.3	8.5	4.8	9.5	4.3	17.5	4.4	19	5.2	3	3.3	26	3.2	105	28.1	17	·	·	·	6	7	2	1	8	16	14	4	1?	·	—
VIII	6	5.3	0.5	2.0	2.5	5.0	9	4.8	7.5	3.9	5	4.8	19.5	4.9	15	4.4	28	3.3	90	41.8	2	·	·	·	8	3	2	6	8	10	9	3	1	·	—
IX	0.5	3.0	·	·	5	4.4	20	4.8	11.5	5.1	15	4.0	11	4.0	3	2.7	24	3.2	33	15.5	29	·	·	·	4	3	1	7	3	6	4	1	·	·	—
X	4	3.1	3	2.7	3	3.3	1.5	7.7	5	2.5	14.5	4.6	23.5	4.4	14.5	4.1	24	3.1	6	3.0	11	·	·	5	·	2	1	3	12	6	2	·	5	·	—
XI	0.5	3.0	14	5.8	9.5	4.3	12.5	5.2	4	4.9	12.5	6.6	19.5	5.6	0.5	2.0	17	4.5	52	6.7	27	4	11	22	·	4	2	·	23	23	13	·	5	18	—
XII	2	1.0	2	2.5	3.5	4.0	11	4.3	19	6.0	30	5.0	16	3.9	3.5	3.9	6	4.4	38	7.7	18	2	5	23	·	2	·	·	21	18	11	·	1	9	—
Rok	60.5	3.5	71.5	3.7	91.5	5.1	126	4.7	104	4.5	152.5	5.0	178.5	5.3	83.5	4.9	227	4.0	595	41.8	2.VIII	27	55	147	24	57	21	30	158	164	112	15	27?	101	—

Skierniewice — $H_s = 128\ m$ — $H_b = 129{,}5\ m$ — $h_w = 8{,}3\ m$

I	3	2.7	5	2.8	8.5	4.6	8	4.4	24	4.1	13.5	3.6	10.5	4.3	6.5	4.4	14	3.4	14	3.6	21	3	8	27	·	·	·	3	17	11	5	·	3	16	—
II	13.5	5.1	6	4.1	1.5	2.7	·	·	7.5	4.1	12	5.4	29	4.3	9.5	3.3	5	4.1	12	1.9	23	12	23	27	·	1	·	1	13	17	6	·	3	28	—
III	4	5.1	7	3.0	5.5	3.7	5	3.9	24	3.0	12	4.7	9.5	4.9	6	4.3	20	3.0	10	4.1	3	4	6	19	·	1	·	6	10	9	4	·	3	12	—
IV	5.5	3.1	8.5	4.6	24	6.3	10.5	4.0	7	4.0	5.5	3.0	9	2.8	10	3.2	10	3.9	64	14.9	28	·	·	5	·	3	·	2	12	18	12	2	1	·	—
V	12	3.2	7.5	3.6	15.5	4.9	8	3.8	3.5	3.4	8	3.1	16	2.5	15.5	3.4	7	3.2	78	19.9	19	·	·	2	·	·	·	2	14	13	11	2	1	·	—
VI	7.5	2.7	5	4.0	11.5	4.5	5	3.3	6.5	2.7	11	3.4	23.5	3.3	10	2.2	10	2.9	63	12.4	14	·	·	·	5	·	·	4	8	14	11	2	·	·	—
VII	4	3.2	4.5	4.9	8.5	3.4	5.5	2.8	10	3.2	24	3.5	26	3.7	1.5	2.7	9	3.2	101	38.8	17	·	·	·	4	·	·	·	13	16	13	3	·	·	—
VIII	4	1.6	2.5	1.6	5	4.2	9.5	3.2	7	3.1	6	3.8	20.5	2.6	17.5	3.2	21	2.3	48	16.6	26	·	·	·	9	·	·	2	8	13	7	2	·	·	—
IX	0.5	3.0	0.5	3.0	7	3.0	13.5	3.8	21.5	2.7	18	3.2	18	3.3	·	·	11	2.8	69	26.7	4	·	·	·	2	·	·	8	2	11	8	2	5?	·	—
X	8.5	2.1	2	1.8	4.5	3.3	3	2.3	7.5	3.1	16	3.5	22	3.0	9.5	3.5	20	2.4	6	3.1	16	·	·	6	·	·	·	2	11	4	2	·	12	·	—
XI	4	1.2	13	4.5	10.5	4.0	9	5.7	10.5	4.7	14	5.0	15	4.7	3	2.5	11	3.9	26	8.0	21	7	11	20	·	1	·	1	16	12	9	·	3	16	—
XII	2.5	2.8	2	2.5	5.5	3.9	7.5	3.8	28.5	5.3	15	4.5	21.5	4.0	5.5	2.5	5	4.1	42	15.0	18	2	4	21	·	4	·	·	14	12	8	1	2	11	—
Rok	69	3.0	63.5	3.4	107.5	4.0	84.5	3.4	157.5	3.6	155	3.9	220.5	3.6	94.5	2.9	143	3.3	533	38.8	17.VII	28	52	127	20	10	·	31	138	150	96	14	33?	83	—

Zielona Góra — $H_s = 180\ m$ — $H_b = 173{,}8\ m$ — $h_w =$ 16,3 m wiatromierz Wilda, 12,8 m anemometr

I	8	2.2	7.5	1.5	8	2.2	12	2.6	16	3.3	19	3.6	16.5	3.5	6	2.9	·	2.9	33	7.0	9	·	1	25	·	·	·	1	21	15	9	·	13	13	·
II	13.5	2.8	6	2.7	6.5	2.5	2	3.2	3	2.7	11	4.5	22	4.0	20	3.4	·	3.5	30	4.2	17	2	17	27	·	·	·	·	20	25	10	·	7	28	·
III	6.5	2.5	9	3.3	3.5	2.3	8.5	3.1	18	2.7	14	3.1	16	3.8	14.5	2.9	3	2.9	45	19.2	3	3	7	18	·	·	·	6	16	14	8	2	7	16	·
IV	6	2.0	5.5	2.9	13	3.2	14.5	2.9	11	2.7	6	3.6	17	3.1	15	2.5	2	2.8	39	9.1	9	·	·	·	·	1	·	1	17	19	11	·	3	·	·
V	9.5	2.4	9.5	3.1	14.5	3.5	10	3.6	2.5	2.8	10	2.6	19.5	3.8	15.5	2.9	2	3.1	81	18.5	10	·	·	·	·	1	·	1	14	19	13	2	4	·	3
VI	8	2.4	11	2.5	10	2.8	7.5	2.8	5.5	2.3	14	3.6	21	3.0	10	2.7	3	2.8	53	12.4	1	·	·	·	6	·	·	1	10	14	9	2	1	·	6
VII	4	2.1	7	2.2	5	2.9	6	2.5	5.5	2.2	29	3.8	28	3.8	7.5	2.7	1	3.2	126	38.9	16	·	·	·	4	·	·	·	19	21	16	4	2	·	9
VIII	8	1.6	3.5	1.4	7.5	1.8	7.5	2.5	8.5	2.8	11.5	2.7	24.5	2.7	19	1.6	3	2.2	26	13.6	24	·	·	·	8	·	·	3	5	10	3	1	4	·	·
IX	1.5	1.3	0.5	3.0	2.5	3.2	16.5	3.2	15	2.4	27.5	2.8	17.5	2.5	7	2.1	2	2.6	60	23.6	10	·	·	·	2	·	·	3	5	9	8	2	·	·	3
X	6.5	1.4	3.5	2.0	18	2.6	14	2.3	8	2.6	18	3.2	12	3.4	12	1.8	1	2.5	16	6.4	31	·	·	2	·	·	·	6	7	8	3	·	11	·	·
XI	1.5	1.3	15.5	2.5	14.5	3.2	5.5	3.5	12.5	3.6	14.5	4.9	18.5	3.8	6.5	2.0	1	3.4	40	10.2	27	5	12	16	·	1	·	·	19	20	10	1	10	17	·
XII	1	1.5	1	2.0	6.5	3.1	14	2.9	18	4.1	28.5	5.3	19.5	5.1	4.5	2.0	·	4.2	54	10.4	18	·	2	20	·	·	·	·	22	24	18	1	11	15	·
Rok	74	2.0	79.5	2.4	109.5	2.8	118	2.9	123.5	2.8	203	3.6	232	3.5	137.5	2.5	18	3.0	603	38.9	16.VII	10	39	108	20	3	·	22	175	198	118	15	73	89	21

Uwaga. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru Fuess.

Pleszew

φ = 51°54' λ = 17°47' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.0	−2.3	5.5	1, 17	−7.1	27	−0.7	1.4	−0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.9	7.9	8.1
II	–	–	–	–	−1.0	−7.7	3.1	13	−16.9	6	−5.4	−2.3	−4.3	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.4	6.9	7.7
III	–	–	–	–	6.4	−2.9	15.5	29	−17.7	9	−1.5	5.1	1.0	1.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.2	6.0	6.0
IV	–	–	–	–	11.3	3.0	15.9	6	−0.3	5	4.7	10.3	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	6.2	6.7
V	–	–	–	–	15.0	6.1	23.4	17	−0.9	3	8.9	13.4	9.9	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	7.5	7.4
VI	–	–	–	–	21.8	11.0	33.1	26	7.2	3	14.6	20.0	15.3	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.6	5.7	5.8
VII	–	–	–	–	21.7	11.8	31.9	14	6.8	2	14.8	19.9	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.6	4.4	6.2
VIII	–	–	–	–	22.3	10.4	31.0	6	5.4	17	13.2	20.7	14.4	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.4	4.2	5.0
IX	–	–	–	–	21.2	9.5	29.3	3	4.0	16	11.3	19.6	13.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.5	4.0	5.1
X	–	–	–	–	13.6	3.3	22.3	1	−4.4	22	4.5	12.3	6.3	7.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	4.8	4.2	5.1
XI	–	–	–	–	2.2	−3.5	12.5	2	−16.9	17	−1.8	0.8	−1.0	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.3	7.5	9.0	8.6
XII	–	–	–	–	3.5	−0.9	11.3	19	−9.9	17	0.4	2.2	1.0	1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.0	8.5	8.6
Rok	–	–	–	–	11.7	3.2	33.1	26.VI	−17.7	9. III	5.2	10.3	6.4	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.9	6.2	6.7

Leszno-Strzyżewice

φ = 51°50' λ = 16°32'

I	999.9	1015.0	979.9	1011.5	2.9	−1.3	6.9	1	−5.7	7	−0.1	2.0	0.4	0.7	5.6	5.8	5.7	5.7	92	82	89	88	0.5	1.3	0.7	0.8	8.5	8.0	7.9	8.1
II	1006.1	1021.6	980.1	1018.0	−0.2	−6.7	4.1	14	−13.9	6	−4.8	−1.8	−3.5	−3.4	3.9	4.0	4.1	4.0	88	74	84	82	0.5	1.4	0.7	0.9	8.7	7.4	7.0	7.7
III	1005.3	1021.3	978.3	1017.0	6.5	−4.7	16.3	29	−24.0	9	−2.7	4.6	−0.6	0.2	5.0	5.8	5.6	5.5	90	67	88	82	0.5	3.3	0.7	1.5	6.9	5.7	5.3	6.0
IV	999.3	1021.0	982.6	1010.7	12.0	2.6	17.1	6	−1.8	2	4.4	10.4	6.5	7.0	7.5	7.4	6.0	7.6	89	60	82	77	1.0	5.4	1.8	2.7	7.7	8.0	7.2	7.6
V	1002.6	1017.6	989.7	1013.8	15.5	6.7	24.0	17	−1.5	2	9.3	13.8	10.0	10.8	10.1	10.1	10.2	10.1	84	64	82	77	1.7	5.9	2.3	3.3	7.4	7.7	6.8	7.3
VI	1003.1	1014.3	990.5	1014.1	21.8	10.8	32.5	26	5.0	3	14.5	19.7	15.5	16.3	13.5	13.8	14.4	13.9	82	61	82	75	3.2	9.8	3.5	5.5	6.6	7.5	6.0	6.7
VII	1000.8	1008.8	987.0	1011.8	21.4	11.2	30.5	14	4.5	5	14.5	19.3	14.8	15.8	14.2	14.5	14.7	14.5	85	64	86	78	2.5	8.5	2.5	4.5	7.2	7.5	6.5	7.1
VIII	1004.7	1013.0	991.7	1015.7	22.0	9.4	31.1	6	5.0	14, 31	12.8	20.3	14.2	15.4	13.6	13.0	13.8	13.5	91	55	84	77	1.5	11.5	2.9	5.3	5.2	6.2	5.1	5.5
IX	1003.0	1023.9	989.2	1014.0	20.6	8.5	27.5	2	2.0	21	10.7	19.0	12.7	13.8	12.0	13.0	12.9	12.6	92	60	87	80	1.2	9.5	2.2	4.3	5.1	7.2	4.3	5.5
X	1012.1	1025.9	999.1	1023.6	13.8	1.8	23.2	1	−5.7	23	3.4	12.2	5.8	6.8	7.8	9.6	8.8	8.7	95	67	92	85	0.4	5.1	0.8	2.1	5.9	6.7	4.8	5.8
XI	1000.1	1020.8	970.5	1011.7	3.0	−2.9	14.1	1	−15.9	23	−1.4	1.7	−0.3	−0.1	5.3	5.7	5.4	5.5	89	77	85	84	0.6	1.8	1.0	1.1	8.4	8.9	7.6	8.3
XII	993.9	1014.8	969.5	1005.3	4.4	−0.8	12.5	19	−7.7	14	0.6	2.7	1.6	1.6	5.6	6.0	6.1	5.9	87	80	87	85	0.9	1.6	1.0	1.2	8.2	8.0	8.7	8.3
Rok	1002.6	1025.9	969.5	1014.0	12.0	2.8	32.5	26.VI	−24.0	9. III	5.1	10.3	6.4	7.0	8.7	9.1	9.1	9.0	89	68	86	81	1.2	5.4	1.7	2.8	7.2	7.4	6.4	7.0

Belsk

φ = 51°50' λ = 20°48'

I	–	–	–	–	0.5	−4.8	4.0	18	−20.0	11	−2.1	−0.6	−1.9	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.4	7.3	7.9
II	–	–	–	–	−2.7	−10.2	1.9	13	−22.7	5	−7.5	−4.2	−6.2	−6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.6	7.0	7.4
III	–	–	–	–	4.5	−4.2	14.6	30	−19.3	8	−2.3	3.1	−0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	5.4	6.2
IV	–	–	–	–	9.8	0.9	14.7	29	−4.6	3	3.6	8.4	4.9	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	6.8	7.9
V	–	–	–	–	13.5	4.3	20.9	17	−5.8	4	8.3	12.1	8.4	9.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	8.5	6.5	7.1
VI	–	–	–	–	20.4	10.2	29.3	26	4.7	8	14.2	18.9	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.7	5.0	5.7
VII	–	–	–	–	21.2	10.2	28.4	16	5.3	11, 12	15.0	19.5	13.9	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.3	4.7	5.9
VIII	–	–	–	–	20.7	10.2	29.7	7	4.0	16	13.2	19.1	13.2	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.7	5.6	5.8
IX	–	–	–	–	20.4	8.4	25.7	3	3.6	16	11.4	18.9	12.3	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	4.3	5.7
X	–	–	–	–	11.8	2.7	20.7	1	−6.3	22	4.1	10.8	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.5	5.3	5.9
XI	–	–	–	–	1.2	−4.4	11.5	2	−17.7	24	−2.5	−0.3	−1.5	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.4	8.7	8.8
XII	–	–	–	–	2.0	−3.0	11.0	20	−17.5	17	−0.7	0.6	−0.4	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.8	7.9	8.4
Rok	–	–	–	–	10.3	1.7	28.7	7.VIII	−22.7	5. II	4.6	8.9	5.2	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.5	6.2	6.9

Wschowa

φ = 51°49' λ = 16°19'

I	–	–	–	–	2.7	−1.2	7.1	1, 17	−5.7	7	0.0	2.0	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.4	6.9	7.3
II	–	–	–	–	−0.3	−6.6	3.9	14	−14.4	28	−4.7	−1.8	−3.4	−3.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.6	6.9	7.1
III	–	–	–	–	6.2	−3.4	15.6	29	−18.2	8	−1.8	5.0	0.7	1.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.2	5.1	6.0
IV	–	–	–	–	11.8	2.9	17.3	6	−1.3	1	4.7	10.5	6.5	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	5.7	6.3
V	–	–	–	–	15.3	6.4	23.2	17	0.2	3	9.3	13.7	10.0	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	6.1	6.4
VI	–	–	–	–	21.4	11.1	31.5	26	6.3	3	14.9	19.6	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.5	5.1	5.5
VII	–	–	–	–	20.9	11.3	30.1	14	5.4	5	14.9	18.9	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.0	5.8	6.3
VIII	–	–	–	–	21.5	9.7	30.0	6	4.2	13	13.7	20.3	14.3	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.5	3.9	4.5
IX	–	–	–	–	20.1	9.5	27.1	2	3.6	21	11.7	18.6	13.4	14.3	–	–	–	–	–	–	–	–	–	–	–	–	3.7	6.1	3.1	4.3
X	–	–	–	–	13.5	2.6	23.2	1	−4.8	23	4.3	12.3	6.6	7.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.3	3.1	4.6
XI	–	–	–	–	2.8	−2.9	13.6	2	−15.2	23	−1.2	1.5	−0.5	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	7.4	7.8
XII	–	–	–	–	4.2	−0.6	12.5	19	−6.9	14	0.6	2.5	1.7	1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.5	7.7	7.8
Rok	–	–	–	–	11.7	3.2	31.5	26.VI	−18.2	8. III	5.5	10.2	6.7	7.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.7	5.6	6.2

Pleszew

H_s = 120 m h_w = 11,6 m

ROZKŁAD WIATRU (n D, V m/s) · OPAD R · LICZBA DNI (n): Temperatura T, Wiatr V, Opad R

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K
I	2	1.5	8	1.1	14.5	1.0	19.5	1.0	21.5	2.1	16.5	1.9	11	2.1	·	·	·	1.6	32	5.6	10	·	3	26	·	·	·		19	16	9	·	—	18	—
II	13	2.3	6	2.0	5	1.4	3	1.0	3	1.3	21	2.8	26	2.5	6	3.8	1	2.4	18	3.5	13	8	18	26	·		·	2	15	21	6	·	—	28	—
III	3.5	1.9	11	1.9	4	1.0	24.5	1.4	12.5	1.6	19	2.8	10.5	2.2	6	2.0	2	1.8	20	4.2	3	4	7	19	·	·	·	5	12	15	5	·	—	15	—
IV	10.5	1.8	11.5	1.7	25.5	1.9	12.5	1.5	2.5	1.0	6	1.6	19	2.0	2.5	1.8	·	1.8	36	7.4	23	·	·	1	·	·	·	4	13	11	7	·	—	·	—
V	10.5	1.3	17.5	1.5	15	1.8	8.5	2.1	4	1.8	11	2.3	12	2.2	8.5	1.6	6	1.7	113	18.4	19	·	·	2	·	·	·	2	17	23	17	3	—	·	—
VI	5.5	2.1	8.5	1.9	13.5	1.9	10	1.4	12	1.3	15.5	1.7	18	2.9	4	2.2	3	1.9	65	16.0	22	·	·	·	6	1	1	5	11	16	13	1	—	·	—
VII	3	1.3	4	1.8	11	1.5	4	1.0	19	1.7	27	1.9	17	2.4	5	1.4	3	1.8	111	25.7	21	·	·	·	5	·		3	10	19	15	4	—	·	—
VIII	6.5	1.3	2.5	1.4	4	1.0	14	1.4	8	1.1	14	1.7	18	1.9	17	1.2	9	1.3	35	15.0	25	·	·	·	9	·	·	5	4	12	5	1	—	·	—
IX	0.5	1.0	·	·	7	1.3	28.5	1.3	15	1.2	25	1.6	10.5	1.6	1.5	1.7	2	1.4	35	12.5	10	·	·	·	3	·	·	5	5	8	7	1	—	·	—
X	7	1.6	4.5	1.0	21	1.0	5.5	1.1	9	1.3	15.5	1.9	20	2.0	7.5	1.7	3	1.5	9	6.9	16	·	·	7	·	1	·	8	8	4	2	·	—	·	—
XI	3	1.7	13.5	2.0	16	1.4	7	2.3	11	2.0	18	2.8	10.5	2.5	8	1.2	3	2.0	34	7.7	21	6	10	19	·	·		·	21	17	8	·	—	15	—
XII		·	1.5	1.0	8.5	1.1	11.5	2.0	23	2.1	31	2.9	12	2.1	5.5	1.8	·	2.2	44	13.6	18	·	3	17	·	·	·	·	20	19	10	1	—	3	—
Rok	65	1.5	68.5	1.4	145	1.4	148.5	1.5	140.5	1.5	219.5	2.2	184.5	2.2	71.5	1.7	32	1.8	552	25.7	21.VII	18	41	117	23	2	1	39	155	181	104	11	—	79	—

Leszno - Strzyżewice

H_s = 91 m H_b = 92,4 m h_w = 14,2 m wiatromierz Wilda; 11,3 m anemometr

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K
I	8.5	4.5	5	3.6	13.5	2.6	13.5	3.1	16	3.9	15.5	4.7	15	5.4	4	4.1	2	3.9	22	4.4	9	·	1	27	·	2	·	·	19	14	7	·	3	10	
II	8.5	6.5	8.5	5.1	3	3.0	5	3.4	2	2.5	16.5	4.9	26.5	5.2	13	6.1	1	5.1	12	1.9	27	8	15	26	·	8	·	1	16	23	4	·	3	22	
III	9	4.2	9.5	5.1	3	1.8	9.5	3.5	17.5	2.6	14	3.8	15.5	5.4	7	5.7	8	3.7	33	14.2	3	8	7	21	·	5	·	5	12	12	9	1	9	17	
IV	4.5	4.7	11	4.7	16	4.4	13	3.9	7	3.9	10	3.7	13.5	4.7	14	4.0	1	4.2	34	7.9	13	·	·	7	·	1	1	3	18	12	8	·	·	·	2
V	10	4.8	11.5	4.2	13.5	4.1	9.5	3.8	5.5	2.7	15	3.6	15	5.2	13	3.8	·	4.1	92	12.0	19	·	·	1	·	3	·	1	15	22	18	2	4	·	5
VI	3.5	5.7	10	4.9	12	4.2	5.5	2.9	10.5	3.1	14.5	4.4	20	3.6	7	4.2	7	3.7	74	20.9	1	·	·	·	6	1	·	2	7	15	8	3	·	·	8
VII	5.5	3.8	6	5.2	6	4.8	5	3.3	9	3.5	35	4.2	22	4.6	2.5	4.4	2	4.2	193	76.9	16	·	·		3	7	·	·	10	19	12	5	3	·	9
VIII	8	2.9	4	2.2	2	2.0	10.5	3.7	7.5	3.3	10	3.8	28.5	3.3	17.5	2.8	5	3.0	21	8.2	23	·	·		8	2	·	4	5	8	5	·	2	·	1
IX	0.5	1.0	·	·	9	3.8	17.5	3.6	12	3.5	16	3.8	23	3.4	5	3.9	7	3.3	36	14.5	10	·	·		2	3	·	2	5	7	5	2	5	·	
X	5	2.7	5	2.8	15	2.9	7.5	2.5	3.5	2.1	17	3.7	19.5	3.5	7.5	3.0	13	2.7	9	4.4	16	·		11	·	1	·	4	7	4	3	·	10	·	
XI	1.5	5.7	16.5	4.7	14.5	3.8	8	4.3	8.5	4.9	17.5	5.9	16.5	4.5	4	4.0	3	4.6	28	7.8	27	4	10	20	·	4	·	1	21	19	8	·	6	15	
XII	4	3.4	1	5.5	7.5	3.5	11.5	4.2	19.5	4.9	30.5	6.0	15	5.9	4	4.2	·	5.1	40	11.2	18	·	2	20	·	5		·	16	25	10	1	1	7	
Rok	68.5	4.2	88	4.0	115	3.4	116	3.5	118.5	3.4	211.5	4.4	230	4.6	98.5	4.2	49	4.0	594	76.9	16.VII	20	35	133	19	42	1	23	151	180	97	14	46	71	25

Uwaga. Kierunki wiatru - wg wiatromierza Wilda, prędkości - wg anemometru Fuess

Belsk

H_s = 180 m h_w = 10 m I–IV; 15,8 m V–XII

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K
I	2	4.5	4.5	3.1	8	3.2	22.5	3.1	21	3.2	8	4.4	6.5	6.3	4.5	3.2	16	3.0	28	5.0	8	4	12	27	·	·		·	19	16	8	·	6	26	
II	6	6.1	7	3.9	1.5	5.7	2.5	2.8	11	5.1	27	4.8	17	5.4	3	5.3	9	4.4	14	3.9	7	11	24	28	·	3	·	2	15	14	5	·	2	28	
III	·	·	7.5	3.4	4	3.0	26.5	2.7	20.5	3.0	12.5	4.5	6	5.7	3	5.7	13	3.0	8	2.9	3	4	7	23	·	2	·	4	11	8	3	·	4	18	
IV	2.5	5.0	7	5.2	21.5	6.1	19	2.9	12	2.6	7	3.6	7.5	4.5	4.5	3.2	9	3.8	39	10.9	28	·	·	12	·	1		·	15	12	9	1	1	·	1
V	5	3.6	9	4.0	12	5.6	7.5	3.3	3	2.7	14	3.4	17	2.5	13.5	3.7	12	3.2	70	16.5	29	·	·	5		1	·	1	13	16	15	2	1		4
VI	4	3.1	12	4.3	8.5	6.1	4.5	5.8	7	1.8	17.5	4.2	21.5	3.2	6	3.6	9	3.5	80	22.5	12	·	·	·	3	·	·	2	10	13	11	3	·		1
VII	2	3.8	3	5.7	4.5	4.4	7.5	4.3	2	2.5	36.5	3.8	18.5	4.0	3	2.8	16	3.3	75	23.5	21	·	·	·	4	1	·	2	4	14	12	1		·	6
VIII	1	5.5	·	·	1	4.0	8.5	4.4	8.5	2.8	15	3.1	26	2.5	13	4.1	20	2.5	88	37.2	26	·	·	·	8	·	·	4	6	15	8	3	·	·	1
IX	1	1.0	1	3.0	1.5	2.3	13.5	5.2	15	3.5	26.5	3.3	10	3.7	4.5	3.3	17	3.0	52	29.5	29	·	·		2	1		4	9	10	6	1	1	·	
X	4	2.0	1.5	2.3	3	4.3	2	2.5	4.5	2.6	21.5	4.2	30	2.8	8.5	2.7	18	2.6	6	4.0	16	·	·	4	·	·	·	5	11	5	2	·	9		
XI	4	4.2	9.5	4.9	9	4.9	8	5.4	11	4.1	18.5	4.1	16.5	3.4	1.5	3.0	12	3.7	31	7.0	21	7	10	21	·	·	·	·	20	17	9	·	7	18	
XII	0.5	3.0	4.5	2.9	2	3.0	16	4.9	16.5	5.4	29	4.3	13.5	2.6	7	3.4	4	4.0	44	15.3	18	2	6	24	·	2	1	·	19	16	9	1	4	11	
Rok	32	3.5	66.5	3.6	76.5	4.4	138	3.9	132	3.3	233	4.0	190	3.9	72	3.7	155	3.3	535	37.2	26.VIII	28	69	144	17	11	1	24	152	156	97	12	35	101	13

Wschowa

H_s = 106 m h_w = 12,4 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	V ≥ 10	V ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K
I	5.5	3.3	6	3.2	11.5	2.8	13	3.2	12	3.1	14.5	4.3	13.5	4.9	5	3.2	12	3.1	21	5.8	9	·	1	25	·	1	·	1	15	16	5		4	5	
II	8.5	4.0	7.5	3.3	3.5	3.0	3.5	2.3	2	2.0	13.5	5.3	22	5.2	18.5	4.8	5	4.2	18	3.7	17	8	16	26	·	4	1	2	13	23	6		1	20	
III	8.5	3.2	6.5	3.6	5	1.6	16	2.9	9.5	2.3	8.5	4.1	18.5	4.9	11.5	4.1	8	3.2	29	7.8	3	4	7	20	·	1	·	2	10	14	7	·	·	15	
IV	6	2.6	10.5	3.7	15.5	3.3	13.5	3.0	4	2.8	6.5	3.4	14	3.9	15	3.8	5	3.2	34	6.4	19	·	·	4	·	1		5	11	17	9	·	·	·	
V	9.5	3.7	7.5	2.1	16.5	3.4	6.5	3.2	2.5	2.8	7.5	4.3	20.5	4.3	14.5	3.3	8	3.3	97	14.0	19	·	·	·	·	1		1	11	22	16	4			3
VI	6.5	2.8	9.5	4.8	8	3.6	10.5	2.0	8.5	2.2	14.5	4.3	12.5	4.4	15	3.5	5	3.4	49	12.9	1	·	·	·	6	2	1	2	6	14	10	1	·	·	4
VII	8	2.5	5	2.3	4.5	2.4	5	2.2	9.5	2.6	27.5	4.0	27	4.4	4.5	4.2	2	3.5	100	45.7	16	·	·	·	3	2	1	·	7	19	14	2			5
VIII	7	2.4			3.5	1.7	10	2.8	10	2.0	11	2.7	22	3.4	13.5	3.3	16	2.4	23	5.5	24		·		8	·		4	3	12	6		·		
IX	1	1.0			4	3.0	16	3.7	18.5	2.3	17.5	3.1	20.5	3.4	3.5	4.0	9	2.8	29	10.9	10				2			5	1	8	6	1	1	·	·
X	2	3.0	3.5	2.0	20.5	2.3	6.5	2.5	10	2.7	15.5	2.6	17	3.5	14	2.8	4	2.6	9	3.6	16			9				7	4	4	3		6		1
XI	2.5	2.8	14	3.8	15	3.9	8.5	3.7	6	2.6	13	3.7	22.5	5.1	5.5	3.4	3	3.9	35	9.4	18	4	11	20		1	1	1	17	16	7		6	14	
XII	3.5	3.0	1.5	3.0	6.5	2.8	11.5	2.9	11.5	3.8	28.5	4.3	23.5	4.7	6.5	3.5		3.9	40	9.6	18		2	20		4	2		15	20	10			2	
Rok	68.5	2.9	71.5	2.6	114	2.8	120.5	2.9	104	2.6	178	3.8	233.5	4.3	127	3.7	78	3.3	483	45.7	16.VII	16	37	124	19	17	6	30	113	185	99	8	18	56	13

Strzelna

φ = 51°49' λ = 19°54'

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.n}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień
I	–	–	–	–	0.8	−4.1	4.0	9	−14.8	11	−2.4	0.1	−1.8	−1.5	4.9	5.2	5.0	5.0	92	84	91	89	0.3	1.0	0.5	0.6	7.8	8.1	5.9	7.3
II	–	–	–	–	−2.6	−9.9	1.9	13	−23.9	6	−7.3	−3.9	−6.1	−5.8	3.3	3.6	3.6	3.5	87	77	87	84	0.4	1.0	0.5	0.6	7.5	7.1	6.2	6.9
III	–	–	–	–	5.2	−4.3	14.1	30	−16.8	1	−2.6	3.8	−0.1	0.2	4.9	5.5	5.4	5.3	90	67	86	81	0.5	2.9	1.0	1.5	6.5	6.2	4.2	5.6
IV	–	–	–	–	9.8	1.3	15.2	30	−3.8	3, 15	3.2	8.3	5.1	5.4	7.1	7.3	7.4	7.3	90	68	82	80	0.8	3.8	1.5	2.0	7.5	7.1	5.1	6.6
V	–	–	–	–	13.4	4.6	20.7	17	−4.3	4	8.2	12.0	8.5	9.3	9.2	9.3	9.5	9.3	82	66	83	77	1.9	4.9	1.9	2.9	6.4	8.0	5.5	6.6
VI	–	–	–	–	20.4	10.0	30.4	26	5.1	16	14.1	18.9	14.4	15.4	13.2	13.0	13.4	13.2	82	61	82	75	3.1	9.5	3.1	5.2	4.6	6.1	5.2	5.3
VII	–	–	–	–	21.0	10.6	29.5	14	5.1	2, 11	14.8	19.5	14.3	15.7	14.2	13.8	14.5	14.2	83	61	88	77	2.9	9.5	2.0	4.8	5.9	6.8	3.8	5.5
VIII	–	–	–	–	20.7	9.5	29.9	7	4.4	16	12.7	19.5	13.2	14.6	13.3	12.9	13.5	13.2	90	59	88	79	1.7	10.9	2.3	5.0	4.9	5.2	3.9	4.7
IX	–	–	–	–	20.4	8.2	27.2	3	1.8	16	10.6	19.2	12.0	13.4	12.0	13.4	12.6	12.7	93	61	90	81	1.0	9.3	1.7	4.0	5.1	5.0	3.2	4.4
X	–	–	–	–	11.9	2.1	22.2	1	−6.9	22	3.9	11.3	5.6	6.6	7.9	9.2	8.6	8.6	95	68	92	85	0.4	4.6	0.8	1.9	6.1	5.5	3.8	5.1
XI	–	–	–	–	1.6	−4.5	12.3	2	−18.1	18	−2.7	0.1	−1.5	−1.4	5.0	5.4	5.4	5.3	92	85	90	89	0.5	1.1	0.6	0.7	8.5	7.8	6.9	7.7
XII	–	–	–	–	2.0	−2.7	9.4	20	−18.1	17	−0.5	1.0	−0.3	0.0	5.5	5.5	5.5	5.5	91	82	87	87	0.5	1.2	0.7	0.8	7.2	7.7	6.3	7.1
Rok	–	–	–	–	10.4	1.7	30.4	26.VI	−23.9	6, 11	4.3	9.2	5.3	6.0	8.4	8.7	8.7	8.6	89	70	87	82	1.2	5.0	1.4	2.5	6.5	6.7	5.0	6.1

Żelechów

φ = 51°49' λ = 21°54'

I	–	–	–	–	0.2	−4.9	2.7	9, 18	−16.9	11	−2.8	−1.0	−2.3	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−3.4	−11.6	1.6	4, 14	−23.0	24	−8.0	−5.0	−7.7	−7.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.9	−4.6	13.7	30	−19.1	9	−3.0	2.7	−0.4	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.4	2.1	15.1	7	−2.3	3	3.6	9.1	5.6	6.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.2	4.9	21.9	19	−3.4	4	8.2	12.8	9.3	9.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.6	10.6	29.9	26	4.9	8	14.3	19.3	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.2	10.5	30.2	16	4.6	12	15.4	20.6	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.1	10.1	29.8	7	4.0	16	13.1	19.6	14.1	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.2	8.6	26.4	2, 3	1.9	21	11.0	19.9	13.4	14.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	11.7	2.3	20.9	1	−6.5	22	3.8	10.8	5.7	6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	4.0	5.1	4.7
XI	–	–	–	–	0.8	−4.4	11.6	2	−20.6	17	−2.1	−0.6	−1.7	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	9.6	6.9	7.8	8.1
	–	–	–	–	1.3	−3.0	8.3	20	−15.6	17	−1.0	0.3	−0.7	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	6.1	7.3
Rok	–	–	–	–	10.4	1.7	30.2	16.VII	−23.0	24.II	4.4	9.0	5.4	6.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Radzyń Podl.

φ = 51°48' λ = 22°38'

I	–	–	–	–	0.1	−5.5	3.4	30	−20.9	11	−3.3	−1.3	−2.7	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	6.9	7.7
II	–	–	–	–	−3.2	−11.1	1.8	14	−22.9	7	−8.1	−4.6	−7.6	−7.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	6.3	7.2
III	–	–	–	–	4.7	−4.0	14.7	30	−16.7	9	−2.3	3.5	−0.5	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	5.8	5.7	6.5
IV	–	–	–	–	10.6	2.2	16.4	7	−2.8	3	3.8	9.5	5.3	6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	6.3	7.4
V	–	–	–	–	14.6	5.2	24.8	19	−3.0	4	8.5	13.5	9.0	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.8	6.6	7.0
VI	–	–	–	–	20.5	10.6	28.8	26	4.2	8	14.5	19.3	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.8	6.1	6.2
VII	–	–	–	–	22.0	10.5	29.7	17	5.0	5	15.6	20.8	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	7.0	5.6	5.7
VIII	–	–	–	–	21.0	10.1	29.2	7	5.6	31	13.2	19.5	14.0	15.2	–	–	–	–	–	–	–	–	–	–	–	–	4.4	6.1	4.1	4.9
IX	–	–	–	–	21.2	8.5	26.9	3	2.6	21	10.9	20.0	13.1	14.3	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.7	3.1	4.1
X	–	–	–	–	11.8	2.7	20.4	1	−5.8	22	3.5	11.0	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	5.6	6.0
XI	–	–	–	–	0.7	−4.2	12.6	2	−19.6	17	−2.1	−0.4	−2.0	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.9	9.0	8.4	9.1
XII	–	–	–	–	1.4	−2.7	7.2	19	−16.5	17	−1.0	0.7	−0.6	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.0	6.8	8.3
Rok	–	–	–	–	10.4	1.8	29.7	17.VII	−22.9	7, 11	4.4	9.3	5.3	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	6.3	6.7

Puczniew

φ = 51°47' λ = 19°05'

I	–	–	–	–	1.6	−2.7	4.8	18, 29	−9.9	11	−1.1	1.2	−0.7	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.6	7.2	7.7
II	–	–	–	–	−2.1	−9.0	2.4	13	−18.4	6	−6.5	−3.4	−5.1	−5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	6.9	7.3
III	–	–	–	–	5.5	−3.0	13.9	30	−16.3	8	−1.6	4.5	1.0	1.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	5.5	5.8
IV	–	–	–	–	10.2	2.5	14.5	30	−1.1	16	4.3	9.2	5.9	6.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	5.2	6.1
V	–	–	–	–	13.7	5.9	22.0	17	−2.0	3, 4	8.9	12.6	9.5	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.0	6.0	6.5
VI	–	–	–	–	20.6	10.9	31.0	26	5.4	16	14.8	19.4	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.3	5.2	5.2
VII	–	–	–	–	21.0	11.5	30.0	14, 15	6.4	11	15.2	19.6	15.2	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.6	4.2	5.1
VIII	–	–	–	–	21.5	10.2	30.8	7	4.4	17	13.7	20.2	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.2	5.0	5.1
IX	–	–	–	–	20.8	10.0	27.8	3	2.8	21	12.2	19.8	13.9	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.0	3.8	4.1
X	–	–	–	–	12.3	3.2	21.5	1	−4.1	22	4.8	11.8	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.9	4.8	5.0
XI	–	–	–	–	2.1	−3.8	12.4	2	−18.3	18	−1.9	0.8	−0.6	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	8.0	8.1
XII	–	–	–	–	2.8	−1.4	10.5	19, 20	−15.8	16, 17	0.4	2.1	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	7.1	7.4
Rok	–	–	–	–	10.8	2.9	31.0	26.VI	−18.4	6, 11	5.3	9.8	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.2	5.7	6.1

Strzelna $H_s = 194\,m$ $h_w = 18\,m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD}																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	●	Opad R			≡	⊠	K (K)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15			R≥0.1	R≥1.0	R≥10.0			
I	13	1.9	1	2.0	12.5	2.0	8.5	2.2	16	3.6	8	4.0	8	5.5	2	4.5	24	2.3	24	6.5	24	1	10	27	·	2	·	3	17	13	7	·	10	19	·
II	13.5	3.3	5	2.0	1	2.0	·	·	1	6.0	13	6.2	22	3.5	16.5	4.5	12	3.5	30	4.6	17	11	24	28	·	3	1	3	12	18	13	·	3	28	·
III	·	·	4	3.2	5	2.2	8	2.1	14	3.1	6	7.5	6	5.3	8	2.0	42	1.9	16	7.6	3	5	7	23	·	1	1	7	10	11	4	·	6	17	·
IV	11	2.4	8	3.2	25	3.2	9	2.7	2	1.0	3	1.7	5	2.6	4	4.2	23	2.1	69	13.3	23	·	·	7	·	·	·	4	14	15	13	2	2	·	3
V	15	1.7	11	2.2	16	2.7	·	·	3	2.3	6	2.3	8	2.9	10	2.3	24	1.7	128	23.8	19	·	·	6	·	1	1	3	13	14	12	5	3	·	3
VI	10	2.8	10	2.5	12	2.5	6	2.2	7	2.0	7	3.1	10	2.7	9	2.6	19	2.0	75	12.7	14	·	·	·	4	1	1	6	8	15	13	1	1	·	1
VII	2	2.5	8	2.4	10	2.2	5	1.6	17	2.4	18	3.5	13	2.8	3	1.3	17	2.1	100	39.4	21	·	·	·	3	1	1	6	7	15	14	3	2	·	5
VIII	17	1.8	·	·	5	1.4	12	3.0	8	2.2	4	2.2	4	2.0	11	2.8	32	1.5	65	25.1	25	·	·	·	9	·	·	9	6	12	8	2	1	·	2
IX	·	·	·	·	14	1.9	16.5	2.3	17	2.6	11.5	2.7	4	1.8	3	1.7	24	1.7	84	44.2	4	·	·	·	2	·	·	7	3	11	7	2	3	·	1
X	16	2.1	9	1.4	4	1.2	7	2.3	6	2.0	8	2.9	7	2.6	5	2.8	31	1.4	6	4.9	16	·	·	9	·	·	·	7	10	3	1	·	12	·	·
XI	5	1.6	11	3.6	5	2.4	11	2.6	7	2.9	19	4.5	8	2.8	2	1.0	22	2.4	35	10.2	21	7	11	21	·	1	1	2	17	17	11	1	7	17	·
XII	2	1.0	·	·	6	2.0	9	2.8	26.5	4.7	25.5	3.3	8	1.6	5	2.2	11	2.9	51	18.0	18	2	7	22	·	2	2	·	13	14	12	1	2	10	
Rok	104.5	1.8	67	1.9	115.5	2.1	92	2.0	124.5	2.9	129	3.7	103	3.0	78.5	2.7	281	2.1	683	44.2	4.IX	26	59	143	18	12	8	57	130	158	115	17	52	91	15

Żelechów $H_s = 175\,m$ $h_w = 14{,}5\,m$

I	8.5	3.1	8.5	4.4	7.5	3.3	10.5	5.1	14.5	5.7	17	4.4	9	7.7	9.5	8.5	8	4.8	37	6.8	1	3	10	27	·	4	3	—	—	—	—	—	—	28	·
II	15.5	5.2	6	7.2	1	5.0	·	·	3.5	4.9	12	6.5	29.5	5.4	12.5	6.8	4	5.6	—	—	—	14	22	28	·	7	1	—	—	—	—	—	6	28	·
III	4.5	5.7	5.5	3.5	4.5	4.0	7.5	5.2	11	5.6	20.5	4.5	22.5	3.6	9	4.6	8	4.0	23	11.6	2	9	8	21	·	6	·	—	—	—	—	—	11	19	·
IV	7	4.9	10	5.2	21	7.1	22	5.7	2	2.5	11	5.1	10	3.8	2	3.0	5	5.2	50	19.8	28	·	·	10	·	6	1	—	—	7	6	2	4	·	1
V	15	3.7	8.5	4.0	9	5.2	9	3.0	1.5	3.0	9.5	4.1	11	4.6	21.5	3.9	8	3.7	41	15.5	25	·	·	3	·	4	1	—	—	12	6	2	3	·	3
VI	6	3.8	7	4.6	9	6.6	5	5.0	4	3.5	7	4.6	30	4.3	15	3.0	7	4.0	70	15.4	14	·	·	·	5	2	·	—	—	13	10	2	—	·	4
VII	4	1.5	6	4.3	1	4.0	5	5.4	4.5	4.8	24.5	4.9	28.5	4.2	12.5	3.0	7	3.9	52	11.6	17	·	·	·	6	1	·	—	—	14	12	1	·	·	6
VIII	6	4.1	2	3.5	·	·	9	3.6	9	4.3	4	4.0	18	4.2	29	4.4	16	3.5	92	28.2	26	·	·	·	9	1	·	—	—	13	6	3	3	·	3
IX	1.5	1.3	2	3.0	1	4.0	19	4.2	10.5	5.4	14.5	3.4	23	3.6	9.5	2.0	9	3.3	42?	18.0?	10	·	·	·	5	1	·	—	—	9	6	2	5	·	1
X	6	2.8	4.5	3.1	2	5.0	2	3.0	6	4.3	8.5	5.1	24	3.9	23	4.1	17	3.2	5	2.5	16	·	·	6	·	·	·	5	6	4	3	·	12	·	·
XI	4	3.8	10	4.2	9.5	4.5	8	5.9	9.5	5.9	7	6.8	28.5	5.2	6.5	4.5	7	4.8	43	6.8	30	6	12	21	·	7	·	·	19	14	9	·	10	17	·
XII	3	1.6	2	2.0	4	2.5	6	6.8	23.5	6.0	26.5	4.5	23	5.3	3	3.2	2	4.8	60	13.2	18	2	7	30	·	9	·	1	17	18	11	2	3	13	·
Rok	81	3.5	72	4.1	69.5	4.3	103	4.4	99.5	4.7	162	4.8	257	4.6	153	4.2	98	4.2	—	28.2	26.VIII	34	59	146	25	48	6	—	—	—	—	—	—	105	18

Radzyń Podl. $H_s = 151\,m$ $h_w = 13\,m$

I	5.5	5.5	14	3.9	4	2.8	16	3.8	6	3.7	15	4.2	8	4.3	11.5	6.7	13	3.8	27	8.2	17	4	13	28	·	4	·	2	17	16	10	·	6	30	·
II	12.5	6.0	8	7.0	2	4.0	·	·	3	5.7	9.5	4.9	19.5	3.8	19.5	5.1	10	4.5	29	5.7	7	14	24	28	·	3	·	1	12	20	11	·	3	27	·
III	1.5	10.0	8	4.7	7	2.5	9	3.6	5	3.6	18	2.8	10	2.4	15.5	5.7	19	3.0	15	4.7	17	5	6	24	·	2	·	5	15	8	5	·	7	16	·
IV	7.5	5.2	7	4.7	21	6.2	22.5	4.7	7.5	4.9	4.5	3.8	9	2.6	3	5.7	8	4.5	38	9.6	23	·	·	12	·	6	·	1	13	10	6	·	1	·	4
V	11	3.5	10.5	3.3	13	5.3	2	2.0	2	2.5	3	2.3	10	3.3	19.5	3.9	22	2.9	46	13.2	29	·	·	2	·	1	·	1	12	15	10	1	·	·	5
VI	6.5	3.7	14	4.7	8	5.4	4	3.5	3	4.0	6	4.8	12	3.2	21.5	3.6	15	3.4	56	12.9	14	·	·	·	6	·	·	3	11	14	10	1	·	·	4
VII	2	1.5	8	4.2	7	3.1	·	·	5	3.2	21	2.8	16	3.5	13	3.4	21	2.5	128	87.5	17	·	·	·	6	1	·	5	7	19	13	1	1	·	6
VIII	15.5	3.8	2.5	3.4	1	3.0	7.5	2.9	8.5	2.8	3	3.7	6	3.0	23	3.8	26	2.5	72	21.0	2	·	·	·	8	1	·	7	5	12	11	3	·	·	2
IX	·	·	·	·	4	2.5	19	2.8	16.5	2.9	5.5	2.7	14	2.6	10	2.7	21	2.1	32	10.1	5	·	·	·	4	·	·	8	1	9	7	1	4	·	3
X	11.5	3.4	7	2.9	7	3.1	2	2.0	2	3.0	12	2.5	13	2.2	25.5	3.5	13	2.6	8	2.5	16	·	·	6	·	·	·	3	8	8	3	·	11	·	·
XI	0.5	3.0	15.5	6.8	8.5	4.6	6	4.3	8	3.6	9	3.2	23	3.7	9.5	3.3	10	3.9	42	5.2	27	4	12	21	·	2	·	·	23	22	15	·	5	19	·
XII	7	3.4	1	3.0	4	2.2	9	3.3	3	3.7	40.5	3.5	16	2.8	4.5	3.1	8	3.0	41	8.4	18	2	7	24	·	·	·	·	17	18	12	·	2	11	·
Rok	81	4.1	95.5	4.0	86.5	3.7	97	2.7	69.5	3.6	147	3.4	156.5	3.1	176	4.2	186	3.2	534	87.5	17.VII	29	62	145	24	20	·	36	141	171	113	7	40	103	24

Pucznieẇ $H_s = 142\,m$ $h_w = 10\,m$

I	2.5	3.0	8.5	2.8	2.5	3.8	11.5	3.2	11.5	2.3	22	3.1	7	4.9	7.5	6.7	20	2.8	17	4.4	8	·	5	27	·	1	1	·	19	9	4	·	—	12	·
II	10.5	6.7	6.5	6.1	5	5.0	1	3.0	2	2.8	10.5	4.7	20.5	4.9	19	5.5	9	4.7	10?	2.0	13	10	23	28	·	1	·	2	13	14	4	·	—	27	·
III	3	5.0	6	3.5	7	4.9	7	4.9	16	2.5	10.5	6.5	14	5.2	10.5	4.0	19	3.5	13?	3.7	3	4	6	20	·	2	·	6	9	9	5	·	—	13	·
IV	10.5	4.8	13.5	5.1	15	5.9	13	4.1	4.5	3.7	5	3.8	10	4.5	9.5	4.3	9	4.2	47	14.1	23	·	·	8	·	1	·	5	12	13	7	2	—	·	3
V	11	3.4	8	3.5	13	4.5	7.5	4.9	1.5	3.0	9.5	2.5	12.5	4.6	13	3.4	17	3.1	119	29.2	24	·	·	3	·	2	·	1	11	17	13	5	—	·	2
VI	8	4.2	9.5	3.2	12.5	4.8	1.5	3.3	5	4.6	8.5	3.5	19.5	4.2	11.5	3.7	14	3.4	60	11.0	27	·	·	·	2	·	·	6	10	13	9	2	—	·	2
VII	3	2.3	7.5	4.3	6.5	3.8	4	4.0	5.5	2.1	16	3.6	32.5	4.0	8	3.7	10	3.3	34?	6.0	8	·	·	·	4	·	·	3	4	11	10	·	—	·	11
VIII	7	3.0	1	3.0	1.5	1.7	5	3.9	7.5	3.3	6	4.5	10	3.1	21	3.2	34	2.1	45	10.9	25	·	·	·	9	·	·	5	8	13	10	1	—	·	2
IX	1	1.0	·	·	4	3.5	11.5	3.4	18	2.7	15.5	2.7	15	3.4	6	3.7	19	2.4	66	36.2	4	·	·	·	2	·	·	10	3	6	5	3	—	·	·
X	6.5	2.7	5	2.4	7	2.6	1.5	4.3	2.5	2.2	13	2.8	19.5	4.3	13	3.5	25	2.4	5	4.2	16	·	·	7	·	·	·	9	5	3	1	·	—	·	·
XI	3.5	1.9	11	4.6	13	4.6	6.5	3.5	8	4.1	11.5	4.1	20	5.1	6.5	3.5	10	3.8	26	7.0	21	5	10	19	·	·	·	1	19	14	9	·	—	14	·
XII	2	4.5	0.5	3.0	2	1.0	5.5	2.5	17	4.3	26	4.3	20.5	5.4	10.5	3.9	9	3.9	43	14.2	18	2	3	16	·	3	·	·	14	13	10	1	—	—	·
Rok	68.5	3.5	77	3.5	89	3.8	75.5	3.8	99	3.1	154	3.8	201	4.5	136	4.1	195	3.3	485?	36.2	4.IX	21	47	128	17	10	1	48	127	135	87	14	—	—	20

Warka — φ = 51°47' — λ = 21°12' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o,m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	–	−4.3	–	–	−15.3	11	−2.2	0.1	−1.6	−1.3	4.7	5.2	4.9	4.9	87	84	88	86	0.6	1.0	0.7	0.8	7.7	8.1	6.7	7.5
II	–	–	–	–	–	−10.1	–	–	−25.7	24	−7.3	−3.7	−6.2	−5.8	3.2	3.7	3.4	3.4	85	76	82	81	0.5	1.1	0.7	0.8	7.4	7.0	6.6	7.0
III	–	–	–	–	5.3	−3.8	14.8	30	−16.6	9	−2.5	4.0	0.3	0.5	4.9	5.7	5.4	5.3	88	69	82	80	0.6	2.8	1.1	1.5	6.7	6.3	5.4	6.1
IV	–	–	–	–	10.7	2.2	15.8	29	−2.4	3	4.0	9.1	6.1	6.3	7.2	7.6	7.5	7.4	86	65	78	76	1.1	4.1	2.0	2.4	8.1	8.0	6.6	7.6
V	–	–	–	–	14.8	5.2	21.6	17, 18	−2.7	4	8.5	13.5	9.7	10.4	9.6	9.9	10.2	9.9	84	63	83	77	1.7	5.9	2.1	3.2	5.4	7.7	6.6	6.5
VI	–	–	–	–	21.6	11.4	31.4	26	7.2	16	14.5	20.0	15.1	16.2	13.9	13.8	14.1	13.9	84	61	82	76	2.8	10.3	3.2	5.4	5.5	6.9	6.3	6.2
VII	–	–	–	–	22.5	10.8	30.5	16	4.2	5	15.3	20.9	15.3	16.7	14.6	14.3	14.9	14.6	83	58	85	75	3.0	11.2	2.7	5.6	4.2	7.1	4.9	5.4
VIII	–	–	–	–	21.8	10.5	30.7	7	5.8	16	13.1	20.0	14.6	15.6	13.8	13.8	14.1	13.9	91	61	84	79	1.6	10.8	3.0	5.1	5.4	6.9	5.3	5.9
IX	–	–	–	–	21.8	8.9	27.1	3	2.4	21	11.0	20.3	13.6	14.6	12.4	13.6	13.6	13.2	93	58	87	79	1.1	10.7	2.2	4.7	4.4	5.1	2.5	4.0
X	–	–	–	–	12.9	2.6	22.4	1	−6.4	22	4.3	11.8	6.5	7.3	8.0	9.5	9.0	8.8	93	68	90	84	0.6	4.7	1.0	2.1	6.8	5.9	4.2	5.6
XI	–	–	–	–	1.7	−3.8	12.2	2	−17.2	18	−1.8	0.5	−1.0	−0.8	5.2	5.5	5.4	5.4	89	83	88	87	0.6	1.3	0.7	0.9	9.3	8.3	8.5	8.7
XII	–	–	–	–	2.4	−2.6	9.0	20	−18.1	17	−0.4	1.2	−0.1	0.2	5.3	5.5	5.2	5.3	87	80	84	84	0.8	1.4	1.0	1.1	8.0	8.8	6.5	7.9
Rok	–	–	–	–	–	2.2	31.4	26.VI	−25.7	24.II	4.7	9.8	6.0	6.6	8.6	9.0	9.0	8.9	88	69	84	80	1.2	5.4	1.7	2.8	6.6	7.2	5.8	6.5

Wisznice — φ = 51°47' — λ = 23°13'

I	–	–	–	–	−0.3	−5.9	3.9	30	−20.5	11	−3.5	−1.6	−3.4	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.2	7.9
II	–	–	–	–	−3.4	−11.5	1.8	14	−23.4	7	−7.8	−4.7	−7.7	−7.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	6.8	7.5
III	–	–	–	–	4.3	−4.2	14.4	30	−17.2	1	−1.4	3.3	−1.2	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.1	5.9	6.4
IV	–	–	–	–	10.7	2.1	17.3	26	−2.9	3	5.2[2]	9.0	4.5	5.8[2]	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.6	6.5	7.3
V	–	–	–	–	15.0	5.0	25.0	19	−3.8	4	10.0[2]	13.7	8.2	10.0[2]	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.7	6.2	6.8
VI	–	–	–	–	20.8	10.9	29.1	26	4.1	8	15.4[1]	19.2	14.2	15.8[2]	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	5.8	6.4
VII	–	–	–	–	22.3	10.7	29.8	17	5.0	5	16.7[2]	20.8	14.9	16.8[2]	–	–	–	–	–	–	–	–	–	–	–	–	5.2	7.1	5.8	6.0
VIII	–	–	–	–	21.1	10.2	29.5	8	5.8	16	14.6[2]	19.6	13.7	15.4[1]	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.4	4.4	5.1
IX	–	–	–	–	21.6	8.7	28.3	2	2.9	21	13.2[2]	20.4	12.7	14.8[2]	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.9	2.6	4.0
X	–	–	–	–	12.0	2.2	20.7	1	−5.5	22	5.8[2]	10.9	5.5	6.9[2]	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.5	5.4	6.5
XI	–	–	–	–	1.0	−4.2	12.3	2	−20.4	17	−1.8	−0.4	−1.9	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	9.4	9.2	8.4	9.3
XII	–	–	–	–	1.6	−2.6	7.1	20	−17.4	17	−0.8	0.6	−0.6	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.6	6.2	8.0
Rok	–	–	–	–	10.6	1.8	29.8	17. VII	−23.4	7. II	5.5[2]	9.2	4.9	6.1[2]	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	6.0	6.8

Kalisz — φ = 51°44' — λ = 18°05'

I	993.4	1007.9	974.2	1011.5	1.6	−2.8	4.4	9	−7.4	27	−1.3	0.9	−0.7	−0.4	5.2	5.5	5.3	5.3	93	85	90	89	0.4	1.0	0.6	0.7	8.1	8.3	6.8	7.7
II	998.5	1014.3	974.6	1017.0	−1.4	−7.8	3.0	13	−15.8	6	−5.7	−2.8	−4.6	−4.4	3.7	3.8	3.8	3.8	90	76	84	83	0.4	1.2	0.7	0.8	7.8	7.5	6.5	7.3
III	998.4	1014.3	969.6	1016.5	5.9	−2.8	14.3	29	−16.0	9	−1.7	4.4	1.0	1.2	5.4	5.9	6.0	5.8	93	67	86	82	0.4	3.0	0.9	1.4	6.4	6.2	5.0	5.9
IV	992.8	1013.4	978.3	1010.4	10.8	2.7	14.8	6, 29	−0.7	16	4.5	9.6	6.3	6.7	7.6	7.8	8.0	7.8	89	66	84	80	0.9	4.3	1.6	2.3	6.9	7.3	5.8	6.7
V	996.0	1011.4	982.7	1013.5	14.3	6.1	22.3	17	−1.1	4	8.6	12.9	9.7	10.2	10.0	10.3	10.0	10.1	87	69	81	79	1.4	4.9	2.3	2.9	7.1	8.0	6.2	7.1
VI	996.5	1006.8	984.7	1013.6	20.9	11.1	31.9	26	6.9	3	14.4	19.5	15.3	16.1	13.6	13.4	14.1	13.7	82	60	81	74	3.0	9.9	3.6	5.5	5.5	6.5	6.1	6.0
VII	994.5	1002.7	980.7	1011.5	21.5	11.6	31.0	14	6.2	4	14.8	19.8	14.9	16.1	14.2	14.1	14.5	14.3	83	61	85	76	2.9	9.7	2.7	5.1	7.1	7.1	5.0	6.4
VIII	998.1	1005.4	987.8	1015.2	22.1	10.4	31.2	7	6.4	3, 17, 31	13.1	20.6	14.8	15.8	13.4	12.8	13.7	13.3	88	54	81	74	2.0	12.5	3.5	6.0	4.9	6.4	4.6	5.3
IX	997.0	1016.7	984.3	1014.3	20.8	9.4	29.0	3	3.7	16	11.1	19.5	13.6	14.4	12.2	12.8	13.3	12.8	91	57	85	78	1.4	10.5	2.6	4.8	5.6	6.0	3.3	5.0
X	1005.4	1019.4	992.6	1023.2	13.2	3.1	21.7	1	−4.2	22	4.1	12.2	6.9	7.5	8.1	9.6	9.1	8.9	96	67	89	84	0.4	5.1	1.1	2.2	5.5	5.4	3.5	4.8
XI	993.6	1013.4	965.0	1011.7	2.2	−3.6	12.3	2	−16.6	18	−1.9	0.9	−0.8	−0.6	5.3	5.7	5.5	5.5	92	84	89	88	0.5	1.3	0.7	0.8	8.2	8.2	7.7	8.0
XII	987.8	1007.4	964.5	1005.8	2.9	−1.3	10.3	19	−10.7	17	0.3	2.0	0.7	0.9	5.7	5.8	5.7	5.7	89	82	88	86	0.7	1.4	0.9	1.0	8.2	7.9	7.0	7.7
Rok	996.0	1019.4	964.5	1013.7	11.2	3.0	31.9	26.VI	−16.6	18.XI	5.0	10.0	6.4	7.0	8.7	9.0	9.1	8.9	89	69	85	81	1.2	5.4	1.8	2.8	6.8	7.1	5.6	6.5

Uwaga: W stosunku do Roczników za poprzednie lata wartość H_b poprawiono z 143,1 na 144,5 m – wg niwelacji kontrolnej z dnia 17.III.1967 r. H_b = 144,487 m. Wartości ciśnienia powietrza są za niskie przeciętnie o ok. 0,5 mb.

Łódź - Lublinek — φ = 51°44' — λ = 19°24'

I	988.2	1003.1	968.6	1011.7	1.3	−3.4	4.4	9, 18, 19	−11.4	11	−1.6	0.4	−1.3	−1.0	4.8	5.2	4.9	5.0	87	82	88	86	0.7	1.2	0.7	0.9	8.1	8.4	6.8	7.8
II	992.2	1008.3	969.5	1016.2	−2.4	−9.8	2.2	13	−21.0	6	−7.0	−4.1	−5.7	−5.6	3.3	3.6	3.4	3.4	87	78	82	82	0.5	1.0	0.7	0.7	7.7	7.6	6.6	7.3
III	993.1	1009.7	965.0	1016.5	5.3	−3.1	14.2	30	−13.4	9	−1.8	3.9	0.9	1.0	5.0	5.5	5.4	5.3	87	66	80	78	0.7	3.1	1.3	1.7	7.0	6.7	5.8	6.5
IV	987.5	1006.9	972.5	1010.4	10.0	2.1	15.4	29	−1.7	1	3.5	8.5	5.6	5.8	7.0	7.4	7.5	7.3	88	67	82	79	0.9	3.9	1.7	2.2	6.7	8.0	5.0	6.6
V	990.7	1006.5	977.6	1013.3	13.7	5.4	21.9	17	−1.5	2	8.3	11.9	9.2	9.6	9.3	9.4	9.5	9.4	84	67	79	77	1.8	4.9	2.4	3.0	7.4	8.5	6.4	7.4
VI	991.1	1000.4	981.1	1013.3	20.8	10.8	31.6	26	5.1	15	14.1	18.9	15.2	15.8	12.8	12.3	12.9	12.7	79	59	74	71	3.5	10.2	4.7	6.1	5.9	7.1	5.9	6.3
VII	989.6	998.6	976.2	1011.8	21.5	11.4	30.5	14	5.3	4	14.8	19.4	15.3	16.2	13.9	12.9	14.3	13.7	82	58	81	74	3.2	10.4	3.5	5.7	7.0	7.7	5.5	6.7
VIII	993.6	1001.0	983.0	1015.9	21.4	10.3	30.1	7	5.3	14	12.8	19.7	15.1	15.7	13.1	12.3	13.5	13.0	88	55	78	74	2.0	11.7	4.3	6.0	5.8	6.8	4.9	5.8
IX	993.3	1012.1	980.9	1015.7	20.6	9.3	27.6	3	2.3	21	11.2	19.0	13.6	14.4	12.1	12.2	12.8	12.4	90	57	82	76	1.5	10.6	3.0	5.0	5.8	6.2	4.2	5.4
X	1000.9	1014.8	988.3	1024.0	12.4	2.7	21.9	1	−4.7	22	4.2	11.4	6.6	7.2	7.9	8.9	8.8	8.5	93	65	88	82	0.6	5.1	1.2	2.3	6.0	6.2	4.4	5.5
XI	989.6	1008.3	969.9	1013.3	2.0	−4.1	12.3	2	−16.8	18	−2.3	0.1	−0.8	−1.0	4.9	5.3	5.4	5.2	88	81	87	85	0.6	1.3	0.8	0.9	8.4	8.2	8.2	8.3
XII	983.8	1002.0	965.1	1007.1	2.4	−2.2	9.8	20	−15.1	17	−0.2	1.3	0.1	0.3	5.3	5.5	5.4	5.4	86	80	85	84	0.9	1.4	1.0	1.1	7.7	8.3	7.9	8.0
Rok	991.2	1014.8	965.0	1014.1	10.8	2.4	31.6	26.VI	−21.0	6.II	4.7	9.2	6.2	6.6	8.3	8.4	8.6	8.4	87	66	82	79	1.4	5.4	2.1	3.0	7.0	7.5	6.0	6.8

Uwaga: Ciśnienie powietrza jest za niskie przeciętnie o ok. 0,5 mb.

Warka $H_s = 120$ m $h_w = 13$ m   1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD}: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	⊕	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	3	2.3	3	3.3	3	2.7	17	2.6	8	2.4	17	3.0	7	3.9	7	5.1	28	2.2	27	5.2	20	3	—	26	·	·	·	4	21	15	10	·	2	27	·
II	12.5	2.7	7	3.6	2.5	2.4	·	·	1.5	2.7	14.5	4.5	21.5	4.0	14.5	5.2	10	3.5	23	5.8	17	13	—	27	·	1	·	2	12	18	11	·	·	28	·
III	1	4.0	4.5	2.2	3	1.7	17	2.0	6	1.3	14	2.6	10.5	2.8	13	3.7	24	1.9	13	5.6	3	6	6	20	·	·	·	5	12	9	5	·	3	17	·
IV	4.5	3.8	3	5.3	16.5	4.3	26.5	3.8	4	2.0	6	2.7	7	4.0	7.5	3.5	15	3.2	38	15.0	28	·	·	8	·	1	·	1	17	11	8	1	1	·	1
V	3.5	2.0	8.5	2.4	12.5	3.5	6	3.0	2.5	2.8	7	2.7	13	2.5	22	2.9	18	2.3	71	17.8	29	·	·	3	·	1	·	5	13	16	12	1	2	·	3
VI	9.5	1.8	9	2.4	8.5	3.2	3.5	4.3	4.5	2.2	6	3.0	24.5	2.8	13.5	2.8	11	2.4	56	12.5	10	·	·	·	7	1	·	3	11	15	10	1	·	·	4
VII	1	3.0	5	2.6	3.5	2.0	6	2.5	4	2.0	24	2.0	25.5	3.3	7	1.7	17	2.0	70	29.5	17	·	·	·	7	1	1	4	4	15	13	1	2	·	4
VIII	4	2.2	0.5	2.0	0.5	2.0	6	1.8	8	2.0	6	2.0	21	2.6	22	3.7	25	2.0	103	40.0	26	·	·	·	10	1	·	4	11	14	11	3	1	·	·
IX	·	·	·	·	·	·	13.5	2.4	12.5	1.8	12	2.6	18	2.2	7	1.7	27	1.5	26	20.0	29	·	·	·	4	·	·	9	3	7	3	1	·	·	1
X	3	1.7	·	·	6	2.2	2	2.5	2	1.5	13.5	2.0	16.5	3.2	25	2.3	25	1.7	6	4.1	16	·	·	7	·	·	·	5	9	5	2	·	8	·	·
XI	·	·	13	3.1	3.5	3.1	13	3.2	6.5	2.0	12	3.9	21.5	3.2	0.5	2.0	20	2.5	39	5.5	12	6	10	19	·	·	·	·	22	19	10	·	7	19	·
XII	0.5	2.0	0.5	2.0	1.5	1.3	12.5	2.2	14	2.6	31.5	2.8	14.5	2.9	6	3.2	12	2.3	48	12.2	18	2	4	24	·	·	·	·	16	19	9	1	1	14	·
Rok	42.5	2.1	54	2.4	61	2.4	123	2.5	73.5	2.1	163.5	2.8	200.5	3.1	145	3.2	232	2.3	520	40.0	26.VIII	30	—	134	28	6	1	42	151	163	104	9	27	105	13

Wisznice $H_s = 152$ m $h_w = 13$ m

I	4.5	2.8	7	1.9	14	2.3	18.5	2.9	15	2.6	13	3.7	8	2.2	3	5.7	10	3.0	37	11.8	17	4	13	26	·	2	·	1	19	15	9	1	3	31	·
II	8	2.0	13	2.8	2	1.5	·	·	3	3.7	21.5	3.9	24	3.3	7.5	2.0	5	2.9	29	4.6	21	14	23	28	·	1	·	1	14	21	9	·	1	28	·
III	4	6.0	6	1.5	2	1.5	15.5	1.7	19	1.4	18.5	2.4	9	2.2	5	3.8	14	1.9	14	3.1	21	4	7	25	·	1	·	4	11	12	6	·	3	18	·
IV	4.5	3.7	4	1.5	29.5	4.2	26.5	4.0	7	2.9	8.5	3.0	1.5	2.0	4.5	4.3	4	3.6	43	14.3	22	·	·	12	·	·	·	·	12	11	10	1	·	·	3
V	13.5	2.4	9	1.9	10	4.6	5	2.4	10	1.6	10	3.8	9	3.1	12.5	3.6	14	2.5	73	19.7	28	·	·	2	·	1	·	1	11	17	11	2	1	·	3
VI	6	2.7	10	3.6	7	4.6	6	3.0	6.5	4.0	7.5	3.0	24.5	4.4	6.5	3.6	16	3.1	94	18.9	11	·	·	·	6	2	·	5	12	12	11	4	·	·	2
VII	1.5	2.0	4	2.0	7	2.0	7	3.0	15	2.9	29	3.2	11	3.9	1.5	1.3	17	2.5	97	44.6	17	·	·	·	7	1	·	5	10	17	14	1	·	·	5
VIII	6.5	4.1	2.5	4.2	2	1.0	8	2.4	8	2.0	8.5	2.6	19	2.4	11.5	2.5	27	1.8	75	27.8	2	·	·	·	9	·	·	7	6	10	8	3	1	·	1
IX	·	·	·	·	1.5	2.7	22.5	2.4	19	2.3	16.5	2.6	7.5	3.5	6	1.3	17	2.0	40	16.5	11	·	·	·	5	·	·	8	2	7	5	2	·	·	·
X	7.5	2.4	5	1.8	5	2.8	4	2.8	5.5	1.8	15.5	3.3	24	3.4	12.5	2.3	14	2.4	4	1.9	16	·	·	5	·	·	·	3	10	5	2	·	5	·	·
XI	·	·	13	3.2	10	2.6	7	2.6	8	2.8	11.5	5.9	25.5	5.1	·	·	15	3.4	46	5.8	15	4	12	21	·	4	·	·	24	19	14	·	2	17	·
XII	2	1.5	1	2.0	2	3.5	12	2.9	15.5	4.3	39	3.8	11.5	2.4	4	2.2	6	3.2	38	8.7	18	2	5	24	·	·	·	·	16	17	11	·	1	9	·
Rok	58	2.5	74.5	2.2	92	2.7	132	2.5	131.5	2.7	199	3.4	174.5	3.6	74.5	2.7	159	2.7	590	44.6	17.VII	28	60	143	27	12	·	35	147	163	110	14	17	103	14

Kalisz $H_s = 140$ m $H_b = 144{,}5$ m $h_w = 15$ m

I	5	2.2	6.5	2.4	8	2.0	10	2.0	24.5	2.7	13	4.1	13.5	4.0	4.5	2.4	8	2.6	15	2.0	6, 26	·	5	27	·	·	·	1	18	13	7	·	5	19	·
II	11.5	2.8	6	3.6	2	1.5	1.5	1.3	3.5	2.3	11	4.6	23	4.0	19.5	4.1	6	3.4	11	2.4	7	9	21	28	·	1	·	1	14	18	2	·	·	28	·
III	3	3.3	11	3.3	2	2.8	11	2.5	15	1.8	10.5	4.2	18.5	3.1	8	3.3	14	2.5	10	2.2	3	5	6	17	·	·	·	5	10	12	5	·	3	16	·
IV	7	2.6	12.5	3.7	15	3.5	15.5	2.1	5.5	2.5	4	2.8	15	3.1	12.5	2.6	3	2.8	31	5.5	23	·	·	3	·	·	·	4	14	14	10	·	1	·	1
V	9.5	2.5	14	2.8	12	3.5	6.5	2.7	2.5	1.6	9.5	3.0	18	3.4	14	2.0	7	2.6	102	20.5	29	·	·	2	·	·	·	1	15	21	13	3	6	·	4
VI	8	2.1	12	3.8	7	3.1	2.5	3.8	9.5	2.5	13	3.2	24	3.2	7	2.8	7	2.8	49	7.3	27	·	·	·	5	1	·	2	10	15	9	·	·	·	5
VII	2.5	2.0	7.5	2.3	6	1.6	3	2.2	11	2.0	27.5	3.1	25	3.3	4.5	1.9	6	2.5	50	17.3	21	·	·	·	4	1	·	1	9	16	8	1	1	·	8
VIII	4	1.5	1	1.0	2	1.5	6.5	2.4	14	3.0	9.5	1.9	16.5	2.5	20.5	2.1	19	1.8	42	13.8	24	·	·	·	8	·	·	4	4	10	6	2	1	·	1
IX	·	·	·	·	6	2.2	16.5	2.7	19.5	2.1	14	3.2	23.5	2.0	1.5	2.7	9	2.2	44	18.7	28	·	·	·	3	·	·	5	5	8	7	1	2	·	3
X	5.5	1.7	5.5	2.2	12	2.0	7	1.3	8.5	1.9	13	2.1	21.5	3.4	9	1.9	11	2.0	5	4.8	16	·	·	8	·	·	·	9	5	2	1	·	9	·	·
XI	3.5	2.0	13.5	4.0	11	3.3	5.5	4.0	11	3.7	16.5	4.5	13	4.5	7	2.4	9	3.4	20	4.6	15	5	10	19	·	1	·	3	21	14	7	·	7	16	·
XII	1	2.0	0.5	3.6	2.5	1.8	12	2.4	22	3.9	30.5	4.5	14	3.5	7.5	2.1	3	3.5	34	12.1	18	1	3	20	·	4	·	·	18	16	10	1	2	9	·
Rok	60.5	2.1	90	2.7	85.5	2.4	97.5	2.4	146.5	2.5	172	3.4	225.5	3.3	115.5	2.5	102	2.7	413	20.5	29.V	20	45	124	20	8	·	36	143	159	85	8	38	88	22

Łódź - Lublinek $H_s = 187$ m $H_b = 187{,}7$ m $h_w = 10$ m

I	8	3.0	3	4.5	4	3.0	19.5	4.5	16.5	5.0	22.5	5.6	8	5.3	10.5	5.3	1	4.8	23	6.2	9	1	6	27	·	4	·	·	18	15	8	·	11	14	·
II	11	6.8	6	6.8	5.5	4.1	2	3.8	2.5	2.2	16.5	6.8	17	5.8	22.5	6.5	1	6.1	19	4.8	13	13	24	28	·	9	·	3	14	23	7	·	3	27	·
III	1	9.0	4.5	5.6	5	3.6	24	3.8	17	4.4	18	5.4	10.5	5.0	12	5.6	1	4.7	16	4.0	3	3	6	23	·	8	·	4	15	12	6	·	4	14	·
IV	7	5.1	8	4.8	14	5.8	26	4.6	8	4.6	7.5	3.3	10	4.4	9.5	4.9	·	4.7	68	16.1	28	·	·	6	·	1	·	5	13	16	11	3	2	·	1
V	12.5	4.6	8.5	4.9	10.5	4.8	12.5	5.5	5	4.5	14.5	4.2	8.5	4.9	18	4.5	3	4.6	86	13.7	29	·	·	3	·	3	·	1	17	19	14	3	2	·	6
VI	9.5	5.3	6	4.7	10.5	4.9	10.5	5.0	7	3.6	17	4.4	14	5.2	13.5	5.6	2	4.8	52	9.5	11	·	·	·	4	4	·	3	10	15	13	·	·	·	3
VII	0.5	6.0	3.5	7.4	6	4.4	14	5.0	8	4.9	28	5.2	26.5	5.9	4.5	5.3	2	5.3	61	12.9	31	·	·	·	5	3	·	·	10	14	12	1	1	·	8
VIII	9	4.8	1.5	3.7	1.5	3.7	11.5	4.2	10.5	4.6	13.5	4.1	9	3.9	22.5	4.6	14	3.7	60	19.5	25	·	·	·	9	·	·	6	8	15	11	1	3	·	2
IX	·	·	·	·	4	3.6	24.5	4.8	16.5	5.6	15.5	4.4	15.5	4.5	4	4.2	10	4.2	56	29.2	4	·	·	·	2	1	·	5	5	9	5	2	5	·	1
X	5	3.5	4.5	3.1	5.5	3.7	9.5	3.5	4.5	4.0	15	4.6	16	5.1	16	4.4	17	3.5	7	4.8	16	·	·	7	·	2	·	5	8	8	1	·	11	·	·
XI	2	1.8	8.5	6.1	13	4.4	14	5.1	8	5.3	18.5	5.5	14	5.0	9	3.7	3	4.8	31	8.0	21	7	9	22	·	5	·	1	20	18	11	·	9	16	·
XII	1	4.0	1	4.0	0.5	2.0	13	4.7	18	7.0	35.5	7.0	14	6.1	9	4.9	1	6.2	50	16.5	18	2	6	21	·	8	·	1	19	17	11	1	3	10	·
Rok	66.5	4.5	55	4.6	80	4.0	181	4.5	121.5	4.6	222	5.0	163	5.1	151	5.0	55	4.8	529	29.2	4.IX	26	51	137	20	48	·	34	157	181	110	11	54	81	21

Uwaga: Kierunki i prędkości wiatru – wg anemometru M-47.

Łódź-Ruda Pabianicka — φ = 51°42' — λ = 19°27' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.3	-3.8	4.4	18	-11.3	11	-1.8	0.5	-1.6	-1.1	4.9	5.4	5.0	5.1	91	84	91	89	0.5	1.0	0.5	0.7	9.5	8.4	7.8	8.6
II	–	–	–	–	-2.2	-10.5	2.0	13	-22.8	6	-7.4	-3.6	-5.9	-5.7	3.4	3.7	3.6	3.6	91	77	86	85	0.4	1.0	0.5	0.6	8.7	7.8	6.8	7.8
III	–	–	–	–	5.9	-4.3	15.2	30	-17.2	9	-2.3	4.6	0.1	0.6	5.0	5.6	5.5	5.4	90	65	95	80	0.6	3.4	1.0	1.7	7.0	6.8	5.8	6.5
IV	–	–	–	–	10.6	1.7	15.5	29	-2.3	3	3.8	9.0	5.5	6.0	7.1	7.5	7.6	7.4	87	66	83	79	1.0	4.2	1.5	2.2	6.9	8.2	5.3	6.8
V	–	–	–	–	14.2	5.1	22.4	17	-2.5	4	8.5	12.4	8.9	9.7	9.5	9.8	9.8	9.7	83	67	93	78	1.9	4.9	1.9	2.9	7.4	8.8	6.5	7.6
VI	–	–	–	–	21.3	10.3	32.8	26	4.5	16	14.3	19.4	14.6	15.7	13.5	13.6	13.8	13.6	82	62	82	75	3.0	9.6	3.0	5.2	5.6	7.3	6.2	6.4
VII	–	–	–	–	21.8	10.9	31.1	14	5.2	4	14.9	19.7	14.7	16.0	14.3	14.1	14.6	14.3	83	61	86	77	3.0	9.8	2.4	5.1	7.0	7.5	5.7	6.6
VIII	–	–	–	–	21.6	9.7	31.2	7	4.7	31	12.8	19.9	13.8	15.1	13.4	13.3	13.8	13.5	90	58	86	78	1.8	11.2	2.5	5.2	5.6	7.1	4.9	5.9
IX	–	–	–	–	20.6	8.7	27.3	3	2.0	21	11.0	19.1	12.5	13.8	12.2	13.3	12.9	12.8	92	61	89	81	1.2	9.4	1.8	4.1	6.1	6.0	4.2	5.4
X	–	–	–	–	12.6	2.1	22.2	1	-5.5	22	4.0	11.5	6.0	6.9	8.0	9.3	8.7	8.7	95	67	91	84	0.4	4.8	0.9	2.0	7.0	6.0	4.6	5.9
XI	–	–	–	–	1.9	-4.3	12.3	2	-17.9	24	-2.3	0.2	-1.0	-1.0	5.0	5.5	5.5	5.3	91	84	89	88	0.6	1.1	0.7	0.8	9.3	8.7	8.3	8.8
XII	–	–	–	–	2.4	-2.5	9.9	20	-17.1	17	-0.3	1.4	0.1	0.3	5.5	5.7	5.5	5.6	90	82	86	86	0.7	1.2	0.9	0.9	9.1	8.5	8.3	8.6
Rok	–	–	–	–	11.0	1.9	32.8	26.VI	-22.8	6.II	4.6	9.5	5.6	6.3	8.5	8.9	8.9	8.8	89	70	86	82	1.3	5.1	1.5	2.6	7.4	7.6	6.2	7.1

Smolice — φ = 51°42' — λ = 17°11'

I	–	–	–	–	2.3	-2.0	6.1	17	-5.3	7	-0.7	1.5	-0.2	0.1	5.6	5.9	5.7	5.7	96	87	94	92	0.2	0.9	0.3	0.5	8.1	7.7	6.7	7.5
II	–	–	–	–	-0.8	-6.9	3.0	13, 14	-14.7	10	-4.8	-2.1	-4.0	-3.7	4.0	4.3	4.3	4.2	92	81	90	88	0.3	1.0	0.4	0.6	8.6	7.6	5.7	7.3
III	–	–	–	–	6.1	-3.6	15.6	29	-21.1	9	-1.9	5.0	0.3	0.9	5.3	6.2	5.9	5.8	91	69	89	83	0.5	3.1	0.8	1.5	7.0	6.0	4.9	6.0
IV	–	–	–	–	11.7	2.9	16.7	6	-1.0	3	5.0	10.6	6.4	7.1	7.9	8.2	8.4	8.2	90	65	87	81	0.9	4.8	1.3	2.3	7.2	7.0	5.3	6.5
V	–	–	–	–	15.0	6.2	22.4	17	-1.1	7	9.2	13.4	9.5	10.4	10.4	10.3	10.1	10.3	87	67	84	79	1.5	5.3	1.9	2.9	6.8	7.4	6.9	7.0
VI	–	–	–	–	21.0	11.0	30.3	26	5.7	3	15.1	19.6	14.9	16.1	13.8	14.0	14.3	14.0	80	62	84	75	3.6	9.4	2.9	5.3	5.2	6.7	5.4	5.8
VII	–	–	–	–	21.2	11.2	33.1	14	5.4	5, 10	14.9	19.6	15.0	16.1	14.6	15.5	14.9	15.0	85	67	86	79	2.6	7.9	2.5	4.3	7.1	6.9	6.3	6.8
VIII	–	–	–	–	22.3	9.8	30.2	6	4.0	14	13.8	20.3	15.2	16.1	13.4	13.1	14.3	13.6	84	55	82	74	2.7	11.8	3.4	6.0	4.6	5.7	4.3	4.9
IX	–	–	–	–	20.7	9.2	28.7	2	2.5	21	11.7	19.4	13.3	14.4	12.9	13.4	14.2	13.5	93	60	92	82	1.2	9.7	1.4	4.1	5.2	5.5	3.5	4.7
X	–	–	–	–	13.9	2.8	22.9	1	-5.2	23	4.3	12.7	6.2	7.4	8.2	10.0	9.2	9.1	94	67	94	85	0.6	5.2	0.6	2.1	5.6	5.3	4.0	5.0
XI	–	–	–	–	3.1	-3.2	13.8	2	-14.1	18, 23, 24	-1.6	2.0	-0.6	-0.2	5.3	5.9	5.5	5.6	90	79	88	86	0.5	1.7	0.8	1.0	8.2	8.4	8.0	8.2
XII	–	–	–	–	3.6	-0.9	11.6	19	-6.5	16	0.6	2.6	1.3	1.4	5.8	6.0	6.1	6.0	89	80	90	86	0.7	1.5	0.8	1.0	8.3	7.0	7.8	7.7
Rok	–	–	–	–	11.7	3.0	33.1	14.VII	-21.1	9.III	5.5	10.4	6.4	7.2	8.9	9.4	9.4	9.2	89	70	88	82	1.3	5.2	1.4	2.6	6.8	6.8	5.7	6.4

Głogów — φ = 51°39' — λ = 16°06'

I	–	–	–	–	3.1	-0.8	8.8	17	-5.2	7	0.4	2.3	1.0	1.2	5.8	6.3	6.0	6.0	91	87	90	89	0.6	1.0	0.6	0.7	7.7	7.8	7.5	7.7
II	–	–	–	–	-0.4	-6.1	3.7	13	-13.5	6	-4.1	-1.6	-2.9	-2.9	4.0	4.4	4.4	4.3	87	81	87	85	0.6	1.0	0.6	0.7	8.2	6.9	7.3	7.5
III	–	–	–	–	6.3	-2.6	15.3	29	-15.4	8	-1.4	5.4	1.3	1.6	5.3	6.5	6.2	6.2	87	70	87	81	0.7	3.0	0.9	1.5	6.6	6.0	4.8	5.8
IV	–	–	–	–	11.8	3.5	17.1	6	0.8	1, 5, 6	4.7	10.6	7.0	7.3	7.9	8.3	8.5	8.2	91	66	85	81	0.8	4.7	1.6	2.4	7.3	7.2	5.2	6.6
V	–	–	–	–	15.5	6.7	24.0	17	0.6	3	9.5	14.2	10.4	11.1	10.6	10.9	10.8	10.8	88	67	84	80	1.4	5.7	2.0	3.0	6.6	7.5	6.6	6.9
VI	–	–	–	–	21.6	11.5	31.9	26	7.3	2	4.9	19.7	15.4	16.4	13.7	13.7	14.1	13.8	81	61	80	74	3.5	10.0	3.7	5.7	5.8	6.7	5.9	6.1
VII	–	–	–	–	20.9	11.9	29.6	14	7.3	5	4.9	19.2	15.0	16.0	14.2	14.4	14.1	14.2	82	65	81	76	3.0	8.2	3.3	4.8	7.0	7.5	7.1	7.2
VIII	–	–	–	–	21.6	10.7	30.1	6	6.7	16	3.6	20.5	14.6	15.8	13.5	13.3	12.9	13.2	86	55	78	73	2.3	11.5	4.1	6.0	5.2	6.0	3.9	5.0
IX	–	–	–	–	20.0	9.6	26.4	2, 3	4.8	16	1.8	18.9	13.2	14.3	12.2	12.9	11.7	12.3	87	60	84	77	1.9	9.5	2.6	4.7	5.0	6.2	3.2	4.8
X	–	–	–	–	13.4	3.0	23.0	1	-4.2	22	4.8	12.2	7.1	7.8	8.0	9.4	8.8	8.7	90	66	84	80	1.0	5.4	1.7	2.7	5.8	6.3	3.6	5.2
XI	–	–	–	–	3.1	-2.7	14.2	2	-12.6	24	-0.6	1.9	0.0	0.3	5.4	5.7	5.5	5.5	87	79	86	84	0.9	1.8	1.0	1.2	8.3	8.1	7.6	8.0
XII	–	–	–	–	4.4	-0.5	12.2	19	-5.8	14	1.3	3.0	2.1	2.1	6.0	6.4	6.4	6.3	88	83	89	87	0.9	1.4	0.9	1.1	7.8	7.4	8.0	7.7
Rok	–	–	–	–	11.8	3.7	31.9	26.VI	-15.4	8.III	5.8	10.5	7.0	7.6	8.9	9.4	9.1	9.1	87	70	85	81	1.5	5.3	1.9	2.9	6.8	7.0	5.9	6.6

Ostrów Wlkp. — φ = 51°39' — λ = 17°49'

I	–	–	–	–	2.5	-1.9	5.4	9, 15, 19	-5.4	7	-0.8	1.7	-0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	7.2	7.7
II	–	–	–	–	-0.7	-7.4	3.5	13	-16.1	6	-5.3	-1.9	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.9	6.1	7.0
III	–	–	–	–	7.0	-2.6	15.5	30	-17.7	9	-1.2	5.6	1.3	1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.0	5.5	5.9
IV	–	–	–	–	11.6	3.2	16.1	6	-0.5	5	4.8	10.5	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	5.9	6.3
V	–	–	–	–	15.2	6.2	22.8	17	-0.7	3	8.9	13.7	9.7	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.1	6.2	6.7
VI	–	–	–	–	21.7	11.1	33.3	26	6.7	4	14.9	20.2	15.3	16.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	6.0	4.8	5.1
VII	–	–	–	–	22.1	12.1	31.7	14	6.7	4	15.2	20.4	15.1	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.7	4.3	5.7
VIII	–	–	–	–	22.4	10.5	31.5	7	5.9	14, 17	13.8	21.0	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.2	4.0	4.5
IX	–	–	–	–	21.2	9.8	28.8	3	4.0	21	11.7	19.8	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.9	3.3	4.4
X	–	–	–	–	13.9	2.9	23.1	1	-5.0	22	4.4	12.9	6.2	7.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.1	2.9	4.1
XI	–	–	–	–	2.8	-3.3	13.0	2	-16.1	18	-1.5	1.4	-0.7	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	7.3	7.8
XII	–	–	–	–	3.7	-0.9	10.9	19	-9.3	17	0.5	2.4	1.0	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.9	8.1	7.7
Rok	–	–	–	–	12.0	3.3	33.3	26.VI	-17.7	9.III	5.4	10.6	6.5	7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.4	5.5	6.1

Łódź - Ruda Pabianicka $H_s = 181\ m$ $h_w = 18\ m$ 1965

ROZKŁAD WIATRU n_D, V_{mD} · OPAD R · LICZBA DNI (n): Temperatura T, Wiatr V, Opad R

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5.5	2.7	2	2.8	10	3.2	19	3.9	12.5	4.2	21.5	3.9	8.5	4.3	8	3.8	6	3.5	28	5.2	9	1	7	27	·	1	·	·	21	14	9	·	10	19	
II	9	4.3	3.5	4.3	6	3.8	2.5	2.8	1.5	2.0	17	5.9	29	4.3	11.5	4.5	4	4.3	37	5.7	7	12	23	28	·	2	·	2	16	24	16	·	2	28	
III	·	·	9	3.3	9.5	3.0	18	2.8	6.5	2.5	14.5	5.6	16.5	3.6	7	4.6	12	3.2	21	5.3	3	6	5	24	·	2	·	4	14	13	6	·	5	16	
IV	·	·	2.5	6.4	36.5	5.4	11	3.6	·	·	2	4.0	15.5	3.3	15.5	4.9	7	4.3	65	14.7	28	·	·	9	·	·	·	4	14	16	11	3	1	·	1
V	1	4.0	8	3.2	23.5	4.4	6	3.7	3.5	2.9	5	4.0	22.5	3.5	15.5	5.2	8	3.7	98	16.4	24	·	·	4	·	2	·	1	17	18	14	3	2	·	6
VI	6.5	3.3	7.5	3.1	13.5	4.0	8.5	4.4	5.5	3.1	7	3.3	19.5	3.3	12	3.2	10	3.1	59	9.6	26	·	·	·	5	2	·	3	11	15	13	·	·	·	2
VII	·	·	6	1.8	7	2.7	11	3.0	4	2.8	21	3.4	28.5	3.6	5.5	3.0	10	2.8	69	17.2	30	·	·	·	4	·	·	4	9	18	11	2	·	·	6
VIII	5	2.0	3	1.0	3	1.0	11	2.9	4	3.8	11.5	3.0	14	2.5	25.5	2.3	16	2.1	58	19.5	25	·	·	·	9	·	·	6	11	16	10	1	·	·	2
IX	·	·	·	·	2.5	2.6	25	2.9	12.5	2.5	13	3.4	15.5	2.9	7.5	1.9	14	2.4	59	30.3	4	·	·	·	2	·	·	5	6	9	5	2	2	·	·
X	6.5	2.0	4	1.9	13	2.0	6.5	2.2	2	2.8	15	2.3	16.5	3.0	17.5	1.9	12	2.0	7	4.4	16	·	·	9	·	·	·	4	10	10	1	·	11	·	·
XI	·	·	7.5	3.4	10.5	3.3	17.5	3.8	4.5	3.2	13	4.6	21	3.3	9	2.4	7	3.3	41	7.6	21	7	10	21	·	·	·	1	22	25	12	·	7	17	·
XII	2	1.5	1	3.0	3.5	1.3	12	3.7	12.5	4.2	36	5.2	14.5	3.9	10.5	3.0	1	4.1	54	16.6	18	2	6	20	·	2	·	·	20	17	12	1	2	11	·
Rok	35.5	1.6	54	2.8	138.5	3.1	148	3.3	69	2.8	176.5	4.0	221.5	3.5	145	3.4	107	3.2	596	30.3	4.IX	28	51	142	20	11	·	34	171	195	120	12	42	91	17

Smolice $H_s = 107\ m$ $h_w = 15\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6.5	2.9	4	2.8	6	2.7	4	2.5	14	2.9	21	2.8	12	3.1	6.5	2.0	19	2.2	18	3.3	8	·	1	28	·	·	·	1	15	15	7	·	7	14	·
II	5	3.0	9	3.3	5	4.2	1	2.0	2.5	2.4	12	4.1	21.5	4.1	20	3.0	8	3.2	14	2.8	13	7	16	27	·	1	·	1	14	17	4	·	3	22	·
III	9	3.2	7	3.0	1	4.0	4.5	3.8	0.5	2.0	16	2.8	17	3.4	12	3.5	26	2.3	37	13.2	3	6	8	19	·	·	·	5	11	16	8	1	6	16	·
IV	2.5	3.6	14	3.1	18	3.9	6.5	3.5	4.5	4.1	4.5	4.7	15.5	2.7	7.5	3.1	17	2.8	37	13.0	19	·	·	3	·	·	·	6	14	13	9	1	·	·	·
V	10	2.2	9.5	3.1	11.5	4.5	5.5	4.9	1	2.0	8.5	2.9	14.5	3.7	15.5	3.0	17	2.8	152	23.7	5	·	·	3	·	·	·	2	14	22	19	6	2	·	4
VI	9.5	2.6	6	3.4	6.5	2.7	5.5	3.6	2.5	2.4	14	2.9	20	2.8	5	2.0	21	2.2	90	23.8	13	·	·	·	4	1	1	4	9	15	14	2	·	·	6
VII	2	1.5	6	2.7	6	2.8	3	2.7	0.5	4.0	25	3.1	29	2.4	2.5	3.0	19	2.2	116	24.2	16	·	·	·	3	·	·	2	9	21	15	4	·	·	8
VIII	6	1.7	·	·	·	·	3	2.5	8	2.1	7.5	1.9	21.5	1.7	10	1.8	37	1.1	22	5.1	25	·	·	·	9	·	·	8	4	10	7	·	·	·	1
IX	1	6.0	1	5.0	5	4.6	9	3.2	7	2.6	19.5	2.1	22.5	2.2	1	2.0	24	1.9	30	13.8	10	·	·	·	3	·	·	6	3	7	5	1	·	·	·
X	1	3.0	3	2.3	10	2.9	8	2.0	4	1.8	14.5	2.6	18.5	2.2	7	2.4	27	1.7	6	4.8	16	·	·	8	·	·	·	8	6	4	2	·	8	·	·
XI	3	1.7	10.5	3.4	14.5	3.4	3.5	2.9	3.5	5.1	14.5	3.4	22	3.4	4.5	2.4	14	2.8	24	5.4	1	4	9	21	·	·	·	1	18	14	7	·	7	13	·
XII	3	2.3	1	2.0	7.5	2.3	6	3.2	15.5	2.9	31.5	4.4	18	3.2	4.5	2.0	6	3.2	39	12.8	18	·	2	20	·	3	·	·	15	16	9	1	1	7	·
Rok	58.5	2.8	71	2.8	91	3.2	59.5	3.1	63.5	2.9	188.5	3.1	232	2.9	96	2.5	235	2.4	585	24.2	16.VII	17	36	129	19	5	1	44	132	170	106	16	34	72	19

Głogów $H_s = 112\ m$ $h_w = 10\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	11	2.5	4	2.8	2	2.0	15.5	2.4	4	4.0	25.5	7.0	20.5	4.3	9.5	4.1	1	4.3	22	4.7	9	·	1	21	·	7	·	·	18	12	6	·	1	5	·
II	8	7.5	12.5	5.2	1.5	4.0	5	5.4	·	·	8	12.4	17.5	8.9	30.5	6.7	1	7.3	20	4.5	17	7	15	25	·	12	3	1	13	21	6	·	1	23	·
III	5	4.0	9	5.3	2	3.5	14	3.1	5	3.4	13	6.2	28	5.9	15	5.3	2	4.9	33	12.1	3	4	7	17	·	5	2	4	10	11	9	1	2	15	·
IV	8	3.6	10	5.2	10.5	4.0	8	4.9	4.5	2.6	5.5	4.6	21	4.7	22.5	4.0	·	4.3	35	6.3	13	·	·	·	·	1	·	2	11	16	13	·	1	·	1
V	5	3.6	12.5	4.6	8.5	4.6	5.5	4.5	1.5	9.0	9.5	7.9	14	5.0	33.5	4.3	3	4.7	89	16.8	19	·	·	·	·	5	3	3	12	20	15	3	·	·	2
VI	10	2.5	12.5	3.7	8	2.1	4	3.1	4.5	4.4	10.5	5.0	18.5	5.3	17	5.3	5	4.0	45	6.9	26	·	·	·	6	5	·	2	8	13	11	·	·	·	5
VII	5	3.6	7	3.7	5.5	3.2	1.5	4.3	5	3.4	21	6.5	34.5	6.6	12.5	4.3	1	5.4	101	36.4	16	·	·	·	4	7	·	·	10	15	14	3	·	·	6
VIII	7	2.9	5.5	2.1	6	2.5	6	6.8	3.5	3.9	9.5	3.5	19	4.6	35.5	3.5	1	3.7	41	11.5	23	·	·	·	8	2	·	2	3	12	8	2	·	·	1
IX	·	·	·	·	1	5.0	15	4.8	6.5	3.8	13.5	5.4	26.5	4.0	20.5	3.7	7	4.0	30	11.5	10	·	·	·	3	4	·	4	4	6	5	1	1	·	·
X	1	9.0	14	2.0	15	2.3	10	2.8	·	·	13.5	5.7	18	5.0	19.5	3.2	2	3.5	11	5.6	31	·	·	10	·	1	·	5	6	3	2	·	9	·	1
XI	·	·	20.5	5.5	6.5	3.8	3	5.3	9.5	8.4	17	7.9	17	8.6	14.5	3.8	2	6.3	26	7.0	27	4	11	18	·	10	1	·	17	11	7	·	3	13	·
XII	1	3.0	1.5	5.0	5.5	3.4	4	7.0	10	7.2	41	9.9	16.5	7.2	13.5	4.2	·	7.6	46	7.9	18	·	2	16	·	12	3	1	14	20	10	·	—	4	·
Rok	61	3.5	109	3.8	72	3.4	91.5	4.5	54	4.2	187.5	6.8	251	5.8	244	4.4	25	5.0	499	36.4	16.VII	15	36	107	21	71	12	24	126	160	106	10	—	60	16

Ostrów Wlkp. $H_s = 126\ m$ $h_w = 11\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	1.5	3.0	3	3.2	5.5	2.5	21	2.7	23	4.1	11.5	3.7	3.5	4.7	7	4.4	17	2.9	29	4.9	24	·	2	25	·	1	·	2	17	15	9	·	6	21	·
II	9	5.0	9	3.9	6	4.2	2	2.2	10.5	3.4	16.5	4.5	9	3.6	15	4.4	7	3.8	25	4.0	17	8	18	27	·	·	·	2	11	19	9	·	2	28	·
III	5	5.3	7.5	3.5	8	3.3	7	3.5	13.5	2.9	13.5	3.8	8.5	3.6	9	3.5	21	2.8	24	8.5	3	5	5	17	·	1	·	7	10	13	7	·	—	14	·
IV	4.5	3.3	13	3.8	19.5	4.5	13	3.7	6	3.1	7	3.2	4.5	3.6	5.5	3.8	17	3.1	31	6.2	24	·	·	3	·	·	·	8	15	12	9	·	·	·	2
V	10.5	3.5	13.5	3.5	12.5	4.7	7	3.6	4	3.4	11	2.9	6.5	6.1	7	3.8	21	3.0	114	21.9	29	·	·	1	·	1	·	5	14	21	15	4	—	·	5
VI	4	4.4	7	2.4	12.5	3.5	9	2.9	12.5	3.3	15.5	3.8	7.5	4.5	6	4.8	16	3.0	53	12.6	26	·	·	·	6	1	1	11	9	15	10	1	·	·	7
VII	1.5	3.7	3.5	2.6	6.5	2.8	9	2.8	16	3.6	26.5	3.9	12	4.6	6	3.6	12	3.2	59	19.4	21	·	·	·	7	·	·	6	8	20	11	1	·	·	10
VIII	4.5	3.0	4	2.4	1	2.0	10.5	3.1	12	4.2	13.5	3.0	7	3.0	9.5	3.4	31	2.2	48	20.9	24	·	·	·	9	1	·	8	5	10	5	2	1	·	2
IX	·	·	·	·	2.5	3.6	19	3.8	12.5	3.2	15	3.1	7	2.9	6	3.2	28	2.3	36	13.7	28	·	·	·	3	·	·	9	3	8	7	1	—	·	3
X	1.5	2.0	2	2.5	7.5	2.8	9.5	2.4	11.5	3.1	6	3.5	8	4.4	7	2.9	40	1.8	6	4.3	16	·	·	9	·	·	·	10	4	3	1	·	6	·	·
XI	1.5	2.0	8.5	4.2	17.5	3.6	7	4.4	11.5	4.4	15.5	4.7	8.5	4.7	7	4.9	13	3.7	34	6.2	21	5	10	20	·	·	·	3	19	17	9	·	6	16	·
XII	2	3.0	2.5	2.8	3	3.0	12.5	3.2	27.5	4.6	24.5	5.2	2.5	5.3	3.5	2.6	10	3.9	44	15.6	18	·	3	17	·	3	·	·	14	19	9	1	3	7	·
Rok	45.5	3.2	73.5	2.9	102	3.4	126.5	3.2	160.5	3.6	176	3.8	89.5	4.2	88.5	3.8	233	3.0	503	21.9	29.V	18	38	119	25	8	1	71	129	172	101	10	—	86	29

Żary

φ = 51°38' λ = 15°08' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.1	−0.9	7.7	17	−7.9	7	0.3	1.9	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.6	7.6	8.0
II	–	–	–	–	0.1	−5.8	3.5	13	−17.3	6	−4.0	−1.8	−2.7	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.4	8.8	8.4
III	–	–	–	–	6.4	−2.5	14.8	30	−20.5	8	−0.9	5.0	0.9	1.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	5.7	5.1	6.1
IV	–	–	–	–	11.6	2.7	18.5	6	−1.3	1	4.7	9.9	6.1	6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	6.0	6.9
V	–	–	–	–	15.7	6.6	23.7	17	0.6	3	9.6	13.8	10.0	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.8	6.3	6.6
VI	–	–	–	–	21.2	11.0	30.6	26	6.5	13	15.1	19.0	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.6	6.1	6.1
VII	–	–	–	–	20.5	11.9	31.3	14	6.8	4	14.6	18.4	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.5	7.6
VIII	–	–	–	–	21.4	10.3	30.1	6	5.6	14	13.6	20.0	14.0	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	4.3	5.4
IX	–	–	–	–	19.8	9.8	25.6	2	5.4	21	11.6	18.0	13.0	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.3	4.0	5.3
X	–	–	–	–	13.6	3.6	22.4	1	−2.7	22	5.0	12.2	6.9	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	4.4	3.0	5.0
XI	–	–	–	–	3.2	−2.4	14.1	1	−11.7	23	−0.4	1.9	−0.3	0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	7.2	8.1
XII	–	–	–	–	4.6	−0.3	12.7	19	−8.6	14	1.3	2.9	2.2	2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.2	8.5	8.5
Rok	–	–	–	–	11.8	3.7	31.3	14.VII	−20.5	8.III	5.9	10.1	6.7	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.9	6.2	6.8

Nowe Miasto n.P.

φ = 51°37' λ = 20°35'

I	–	–	–	–	1.1	−4.2	5.0	18	−14.6	11	−2.4	0.1	−1.7	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.5	7.2	7.5
II	–	–	–	–	−2.3	−9.8	2.5	13	−20.9	6	−7.4	−3.9	−6.2	−5.9	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.1	6.5	6.4
III	–	–	–	–	5.6	−3.3	15.3	30	−15.7	8	−2.1	4.2	0.8	0.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.4	4.6	5.4
IV	–	–	–	–	10.7	2.3	15.2	30	−1.5	15, 16	3.4	9.2	5.8	6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.0	6.8	6.9
V	–	–	–	–	14.3	5.7	21.9	17	−2.1	4	8.2	12.7	9.8	10.1	–	–	–	–	–	–	–	–	–	–	–	–	4.6	7.4	5.7	5.9
VI	–	–	–	–	21.3	11.5	31.7	26	6.7	15	14.1	19.6	15.4	16.1	–	–	–	–	–	–	–	–	–	–	–	–	4.1	5.6	6.1	5.3
VII	–	–	–	–	22.0	11.7	30.3	16	6.7	5	14.7	20.4	15.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	3.6	6.2	6.0	5.3
VIII	–	–	–	–	21.5	10.9	30.3	7, 8	6.0	16	12.8	19.8	14.7	15.5	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.4	3.8	4.5
IX	–	–	–	–	21.1	9.3	26.3	3	3.7	21	10.9	19.9	13.7	14.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.8	2.9	4.1
X	–	–	–	–	12.4	3.3	22.1	1	−4.8	22	4.5	11.4	6.5	7.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	4.2	5.3
XI	–	–	–	–	1.2	−3.6	12.6	2	−18.4	18	−2.2	0.3	−1.2	−1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.7	7.9	8.0
XII	–	–	–	–	2.6	−2.1	10.3	20	−17.4	17	−0.4	1.3	0.0	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	6.0	7.6
Rok	–	–	–	–	11.0	2.6	31.7	23.26.VI	−20.9	6.II	4.5	9.6	6.1	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.4	5.7	6.0

Sieradz

φ = 51°36' λ = 18°44'

I	–	–	–	–	1.6	−2.7	5.8	29	−7.9	11	−1.4	1.1	−0.9	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−2.0	−8.6	2.8	13	−18.0	6	−6.0	−3.0	−5.0	−4.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	6.1	−2.5	14.8	30	−14.0	9	−0.6	4.9	1.0	1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	11.0	2.9	15.4	30	−0.5	16	4.9	9.6	6.3	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.3	6.1	6.5
V	–	–	–	–	14.6	5.9	22.3	17	−1.8	2	9.0	13.2	9.4	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.7	6.7	6.9
VI	–	–	–	–	21.3	10.9	32.4	26	6.2	7	14.8	19.9	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.7	4.5	5.0
VII	–	–	–	–	21.5	11.5	30.4	14, 15	6.4	4	15.0	19.9	14.8	16.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.1	10.3	31.0	7	5.5	14	13.4	20.5	14.5	15.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.1	9.3	28.9	3	2.9	21	11.4	19.7	13.1	14.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.4	2.7	22.4	1	−5.2	22	4.4	12.2	6.3	7.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	2.5	−3.7	12.6	2	−15.6	18	−2.1	1.1	−1.0	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.8	−1.3	10.4	19	−12.9	17	0.3	1.9	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.3	2.9	32.4	26.VI	−18.0	6.II	5.3	10.1	6.2	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sobieszyn

φ = 51°36' λ = 22°10'

I	–	–	–	–	0.2	−4.7	3.1	19	−16.5	11	−2.7	−0.8	−1.8	−1.8	4.6	4.9	4.8	4.8	89	84	87	87	0.5	1.0	0.7	0.7	7.9	8.1	6.8	7.6
II	–	–	–	–	−3.4	−10.9	1.5	14	−22.0	7	−7.7	−4.7	−6.8	−6.5	3.2	3.5	3.3	3.3	85	78	84	82	0.5	0.9	0.5	0.6	8.1	8.0	6.2	7.4
III	–	–	–	–	4.3	−4.1	14.4	30	−16.9	1	−2.4	3.2	0.5	0.4	4.8	5.5	5.4	5.2	87	70	81	79	0.6	2.5	1.2	1.4	9.4	6.7	4.6	6.6
IV	–	–	–	–	10.3	1.9	15.9	7	−2.4	3	3.4	8.9	5.9	6.0	6.8	7.2	7.3	7.1	85	62	76	74	1.1	4.4	2.1	2.5	8.7	8.2	5.8	7.6
V	–	–	–	–	14.4	5.6	24.9	19	−1.8	4	7.9	13.0	9.8	10.2	9.6	9.5	10.2	9.8	87	62	83	77	1.4	5.9	2.2	3.2	6.8	8.4	6.7	7.3
VI	–	–	–	–	20.3	10.9	27.8	26	6.2	4	14.0	18.6	15.2	15.8	13.7	13.3	13.9	13.6	85	64	80	76	2.4	8.7	3.7	4.9	6.3	7.6	6.6	6.8
VII	–	–	–	–	21.6	11.1	28.3	16	5.6	5	14.9	19.9	15.4	16.4	14.8	13.8	14.6	14.4	87	59	83	76	2.4	10.1	3.3	5.3	6.2	7.8	6.4	6.8
VIII	–	–	–	–	20.7	10.2	28.9	8	5.0	16	12.8	19.0	14.5	15.2	13.6	13.4	14.1	13.7	92	62	85	80	1.4	9.4	2.8	4.5	6.4	6.6	4.5	5.8
IX	–	–	–	–	20.9	8.9	26.4	2	2.3	21	10.8	19.3	13.9	14.5	12.2	13.3	13.5	13.0	93	59	85	79	1.0	9.6	2.6	4.4	6.5	5.4	2.3	4.7
X	–	–	–	–	12.2	2.5	21.9	1	−6.5	22	4.1	11.1	6.5	7.0	7.8	8.9	8.7	8.5	93	66	88	82	0.6	4.7	1.3	2.2	7.0	6.5	3.9	5.8
XI	–	–	–	–	1.0	−4.1	11.9	2	−17.8	18	−1.9	−0.3	−1.4	−1.3	5.1	5.4	5.2	5.2	88	86	87	87	0.6	1.0	0.8	0.8	9.7	9.1	8.2	9.0
XII	–	–	–	–	1.5	−2.7	7.4	20	−17.4	17	−0.9	0.5	−0.4	−0.3	5.2	5.4	5.3	5.3	88	84	86	86	0.7	1.1	0.8	0.9	9.1	9.0	7.3	8.5
Rok	–	–	–	–	10.3	2.0	28.9	8.VIII	−22.0	7.II	4.4	9.0	5.9	6.3	8.4	8.7	8.9	8.7	88	70	84	81	1.1	4.9	1.8	2.6	7.6	7.6	5.9	7.0

Żary — $H_s = 162\,m$ — $h_w = 12{,}7\,m$ — 1965

Miesiąc	Rozkład wiatru (%) N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Opad R Suma	Max	Data	Liczba dni (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	3	3.0	3.5	2.6	13	1.7	11.5	1.5	25.5	3.3	14	4.0	4.5	5.4	2	6.5	16	2.5	46	8.6	17	·	1	22	·		·	1	16	15	11	·	3	8	·
II	7.5	4.3	6.5	2.4	5.5	2.5	5	1.7	7.5	1.8	17.5	5.2	15.5	5.5	11	5.7	8	3.8	31	4.1	4	3	16	26	·	3	·	·	17	24	10	·	2	25	·
III	4.5	3.2	7.5	2.5	8	2.5	10.5	2.2	22	2.9	19	3.9	6	5.3	3.5	4.6	12	2.8	42	13.2	2	4	7	19	·	·	·	4	10	13	8	2	2	16	·
IV	6	2.9	6	2.2	18.5	2.7	18.5	1.9	9.5	1.8	12.5	3.4	4	5.1	5	4.2	10	2.4	52	8.4	20	·	·	3	·	·	·	3	11	18	12	·	2	·	·
V	10	3.4	7.5	2.1	18	3.1	10	2.6	12.5	2.5	13	3.9	5	7.1	8	4.5	9	3.1	102	23.0	10	·	·	·	·	2	·	4	14	19	15	4	1	·	3
VI	3	3.0	6	2.2	16	2.4	8.5	1.6	14	2.4	13	3.7	9	3.7	6.5	4.3	14	2.4	67	12.5	11	·	·	·	5	·	·	2	6	17	11	2	·	·	4
VII	0.5	7.0	6	1.8	9.5	2.0	12	1.3	16.5	2.2	22	3.6	15	4.7	4.5	4.7	7	2.8	107	29.0	17	·	·	·	4	·	·	·	11	19	13	3	1	·	6
VIII	4.5	3.1	3.5	2.6	5.5	1.3	17	1.5	15.5	1.9	11	2.8	9.5	4.2	5.5	2.9	21	1.7	21	8.2	24	·	·	·	6	·	·	3	5	9	4	·	·	·	1
IX	·	·	0.5	2.0	6.5	2.0	19	2.1	25.5	2.2	15.5	3.5	6.5	4.6	5.5	3.5	11	2.4	55	23.1	10	·	·	·	1	·	·	5	6	10	7	2	2	·	3
X	1	2.5	0.5	1.0	17	2.2	15.5	4.5	22	2.4	14	3.5	4	2.9	2	2.8	17	2.0	17	6.2	31	·	·	8	·	·	·	2	5	5	3	·	10	·	·
XI		·	1.5	2.7	22.5	2.7	12.5	2.0	14	3.3	17	4.1	11	5.2	2.5	3.0	9	3.0	43	12.0	27	1	11	21	·	1	·	·	16	16	10	1	5	13	·
XII	0.5	3.0	0.5	3.0	3.5	2.3	14	1.8	26.5	2.9	31.5	4.9	9	6.1	1.5	4.3	6	3.5	69	14.7	18	·	·	20	·	·	·	·	19	26	15	1	2	4	·
Rok	40.5	3.0	49.5	2.3	143.5	2.3	154	1.8	211	2.5	200	3.9	99	4.9	57.5	4.2	140	2.7	652	29.0	17.VII	8	35	119	16	6	·	24	136	191	119	15	30	66	17

Nowe Miasto n. P. — $H_s = 155\,m$ — $h_w = 13{,}5\,m$

I	9.5	5.9	3.5	4.1	6	4.8	13.5	2.6	12.5	3.1	21.5	3.0	4.5	3.9	10	5.8	12	3.4	37	4.6	9	5	10	26	·	2	·	3	19	17	13	·	3	14	·
II	8	6.6	8	5.6	3.5	3.9	1.5	2.3	9.5	4.3	17.5	6.1	15.5	5.0	18.5	5.9	2	5.4	15	4.8	17	11	23	27	·	5	1	5	11	15	5	·	·	28	·
III	18	2.5	4.5	4.4	5.5	3.6	10	3.2	6	3.8	15.5	3.0	14	3.8	12.5	3.8	7	3.1	15	5.9	2	4	7	21	·	2	·	6	8	7	3	·	1	15	·
IV	2.5	2.6	8.5	5.4	25	4.9	14.5	5.3	7.5	4.6	12.5	3.6	5	5.2	12.5	3.7	2	4.5	49	11.2	28	·	·	6	·	2	1	3	12	16	11	1	1	·	1
V	10	4.2	10	3.7	12.5	3.6	10	4.2	10	3.0	7	2.9	10	3.4	20.5	3.5	3	3.5	111	19.2	16	·	·	3	·	·	·	4	8	13	11	5	·	·	4
VI	11.5	3.0	8	3.7	10.5	4.0	5	3.6	5	2.6	8.5	3.9	15	2.5	22.5	3.5	4	3.2	60	18.6	14	·	·	·	6	·	·	5	5	11	10	1	·	·	2
VII	1.5	1.0	6	4.8	8	2.8	10	2.9	2.5	2.2	25.5	2.8	21	3.1	15.5	2.7	3	2.8	99[2]	50.6[2]	30	·	·	·	8	1	·	3	4	13	12	1	1	·	5
VIII	9.5	4.3	1.5	1.0	2.5	3.8	10.5	3.0	16	1.9	9	3.1	12.5	1.6	21.5	3.7	10	2.6	82	27.0	26	·	·	·	10	1	·	9	7	15	13	3	1	·	·
IX	3	1.7		·	2	3.0	16.5	2.8	10.5	2.9	22	2.6	15.5	2.7	9.5	4.2	11	2.5	51	22.5	29			·	2	1	1	9	6	10	6	1	2	·	·
X	8.5	2.2	3.5	2.6	3	4.5	6.5	1.7	4.5	2.1	22.5	2.5	15.5	3.1	21	3.3	8	2.5	8	4.6	16	·	·	7	·	·	·	6	8	5	2	·	4	·	·
XI	4	2.4	7.5	6.3	9	4.9	11.5	4.0	8	3.1	18.5	3.3	17	3.6	6.5	4.5	8	3.6	39	6.5	21	7	10	18	·	·	·	1	20	19	11	·	6	13	·
XII	7	3.5	2.5	1.2	3.5	1.3	10	3.3	9.5	4.6	37	4.5	11.5	3.7	8	4.2	4	3.8	58	18.2	18	2	5	22	·	·	·	·	13	18	11	1	1	9	·
Rok	93	3.3	63.5	3.6	91	3.8	119.5	3.2	101.5	3.2	217	3.4	157	3.5	178.5	4.1	74	3.4	624[2]	50.6[2]	30.VII	29	55	130	26	14	3	54	121	159	108	13	20	79	12

Sieradz — $H_s = 137\,m$ — $h_w = 14\,m$

I	2	1.0	7	1.4	11	1.8	8	1.8	10	1.2	20	2.7	11	3.2	4	1.8	20	1.7	27	7.5	24	·	7	27	·	·	·	–	–	14	7	·	6	7	·
II	11	2.0	8.5	2.2	2	1.5	1	1.0	·	·	6	5.0	19	3.8	25.5	4.2	11	3.0	14	2.7	17	11	24	27	·	2	·	–	–	18	6	·	3	27	·
III	1	2.0	3	1.3	9	1.6	10	1.8	9	1.1	15	1.7	14	4.1	13	4.1	19	2.0	21	4.4	2	3	6	18	·	1	·	–	–	15	5	·	5	11	·
IV	7.5	2.3	12.5	2.6	12	2.4	13	1.6	5	1.8	5	1.8	16	2.7	8	2.1	11	2.0	38	11.8	25	·	·	4	·	·	·	–	–	14	7	1	2	·	·
V	24	1.5	7	2.3	8	2.2	1	2.0	3	1.3	1	1.0	20.5	2.6	13.5	2.0	15	1.7	80	11.6	9	·	·	3	·	1	·	–	–	20	17	1	3	·	7
VI	6.5	2.2	11.5	3.5	9.5	3.6	2	2.5	8	3.2	11.5	2.8	17.5	3.9	9.5	3.4	14	2.8	58	14.6	12	·	·	·	5	2	·	–	–	15	11	2	·	·	4
VII	3.5	2.3	8	2.6	2	2.5		·	7	2.0	13.5	3.9	36	3.6	7	3.0	16	2.7	66	13.1	17	·	·	·	5	·	·	–	–	19	10	2	·	·	8
VIII	6	2.3			1	2.0	8	4.0	8	2.6	8	2.4	25	3.0	11	2.9	26	2.1	58	32.2	24	·	·	·	9	1	·	–	–	10	7	1	·	·	2
IX	·	·		·	2	3.0	10	3.0	15	2.7	21	2.8	15	3.3	3	2.0	24	2.1	39	12.9	28	·	·	·	3	·	·	–	–	7	6	2	1	·	·
X	3	2.7	1	2.0	3	1.7	3.5	1.0	1.5	1.0	10	2.9	14	3.9	20	3.0	37	1.7	6	4.0	16	·	·	7	·	·	·	–	–	4	1	·	11	·	·
XI	3	2.7	6	2.2	11	2.1	5	2.0	10	1.7	9	4.0	16	4.3	7	2.4	23	2.1	34	7.8	21	5	10	19	·	1	·	–	–	19	9	·	6	13	·
XII	1	2.0			3	3.3	5	1.2	17.5	2.1	30.5	3.0	19	2.4	4	1.5	13	2.1	39	13.7	18	2	5	17	·	2	·	–	–	18	8	1	2	1	·
Rok	68.5	1.9	64.5	1.7	73.5	2.3	66.5	1.8	94	1.7	150.5	2.8	223	3.4	125.5	2.7	229	2.2	480	32.2	24.VIII	21	52	122	22	10		–	–	173	94	10	39	59	21

Sobieszyn — $H_s = 159\,m$ — $h_w = 13\,m$

I	8	1.8	6	2.5	12.5	3.0	13	2.8	8	1.8	22	4.0	8	7.2	4.5	3.6	11	3.0	28	5.6	17	3	11	27	·	3	·	3	17	20	7	·	–	31	
II	10.5	3.2	10	4.3	1.5	4.7	·	·	2	4.5	20.5	5.6	27	4.6	9.5	3.7	3	4.4	20	4.2	8	15	23	28		3	1	2	14	17	7	·	–	28	
III	3.5	2.0	5	2.9	11.5	2.6	9.5	1.7	8	1.9	22.5	3.8	14	2.7	6	2.8	13	2.4	22	5.5	21	5	7	22	·	1	·	2	11	12	6	·	–	18	
IV	6	3.5	10.5	5.2	34.5	4.5	14	3.2	3	2.0	8.5	4.1	5.5	3.5	4	2.8	4	3.9	56	16.2	23	·	·	10		3	·		14	11	8	2	–	·	2
V	10.5	2.3	13	2.3	12.5	3.1	6.5	1.3	4	3.5	10.5	3.0	13	3.3	14	2.1	9	2.4	59	15.0	29	·	·	3	·	1	·	1	14	15	11	1	–	·	4
VI	7	1.6	11	3.1	9.5	3.5	8.5	2.1	4.5	2.3	11	3.0	20.5	3.1	9	2.5	9	2.5	91	16.8	10	·	·	·	5	·	·	2	10	12	10	5	–		4
VII	1	2.0	6.5	2.5	6.5	2.7	3	3.8	7.5	1.5	33.5	3.2	16.5	3.1	0.5	2.0	18	2.3	64	15.7	18	·	·	·	5	·	·		12	15	13	1	–	·	5
VIII	9.5	2.8	2.5	1.4	8.5	1.5	7.5	2.7	3	2.3	14	2.3	28	2.8	12	3.9	8	2.5	111	29.8	27	·	·		6	1		5	9	11	8	4	–	·	2
IX		·	2	1.0	13.5	1.6	17	2.4	14.5	3.4	22.5	2.7	13	3.3	3.5	2.0	4	2.5	23	8.2	29	·	·	·	3	1		8	4	8	6		–		
X	6.5	1.8	7	1.8	3.5	2.1	3	2.0	4.5	1.9	19	3.1	23.5	3.0	15	3.2	11	2.4	3	1.2	16			6				4	8	8	2		–	·	
XI	2.5	1.4	14.5	3.3	9.5	4.2	10	3.6	8	3.3	19.5	4.6	16	5.8	5	1.6	5	3.8	41	4.9	12	6	11	19		6	1		23	24	13		–	17	
XII	2.5	1.6	2	2.0	7.5	2.2	8	3.0	15.5	5.1	43	4.4	10.5	3.7	3	1.8	1	3.9	44	12.6	18	2	7	23		2	2		20	21	12	1	–	17	
Rok	62.5	2.0	90	2.7	131	3.0	100	2.4	82.5	2.8	246.5	3.6	195.5	3.8	86	2.7	96	3.0	562	29.8	27.VIII	31	59	138	19	21	4	[illegible]	156	174	103	14		111	17

Szprotawa

φ = 51°34′ λ = 15°32′ 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.3	−1.1	8.9	17	−7.7	7	0.0	2.5	0.8	1.0	5.7	6.1	6.1	6.0	94	84	93	90	0.4	1.3	0.5	0.7	8.3	8.2	7.0	7.8
II	–	–	–	–	−0.3	−6.7	3.3	13	−18.3	6	−4.3	−1.3	−3.3	−3.0	4.2	4.4	4.5	4.4	91	78	91	87	0.4	1.2	0.4	0.7	9.1	7.7	7.5	8.1
III	–	–	–	–	6.8	−4.1	16.2	29	−19.7	9	−2.4	5.6	0.5	1.0	5.1	6.0	5.9	5.7	90	65	89	81	0.6	3.7	0.9	1.7	7.3	6.7	5.2	6.4
IV	–	–	–	–	12.0	2.7	18.9	6	−1.8	3	4.4	10.5	6.6	7.0	7.5	7.8	7.8	7.7	89	64	81	78	0.9	5.2	2.0	2.7	6.9	7.6	6.9	7.1
V	–	–	–	–	16.0	6.9	25.5	17	0.6	22	9.5	14.4	10.4	11.2	10.3	10.3	10.7	10.4	85	64	83	77	1.7	6.5	2.2	3.5	6.5	7.8	6.8	7.0
VI	–	–	–	–	21.9	11.0	32.0	26	4.5	3	14.6	20.2	15.4	16.4	13.9	13.8	14.6	14.1	84	60	83	76	2.9	10.5	3.3	5.6	5.3	7.5	6.8	6.5
VII	–	–	–	–	21.2	11.6	31.7	14	4.4	5	14.7	19.4	15.3	16.2	14.4	15.1	15.3	14.9	85	68	87	80	2.6	8.0	2.4	4.3	7.2	8.2	7.5	7.6
VIII	–	–	–	–	22.3	9.1	31.1	6	4.6	31	12.1	21.0	14.0	15.3	13.3	13.7	14.1	13.7	93	55	88	79	1.2	11.9	2.3	5.1	5.4	7.1	4.4	5.6
IX	–	–	–	–	20.1	8.1	25.8	2	2.3	21	10.2	18.9	12.2	13.4	11.8	12.9	12.8	12.5	94	60	91	82	1.0	9.3	1.7	4.0	3.8	6.1	4.3	4.7
X	–	–	–	–	14.0	2.3	23.2	1	−5.5	23	3.6	12.8	5.6	6.9	7.9	10.1	9.1	9.0	97	68	97	87	0.3	5.2	0.4	2.0	6.3	5.8	4.6	5.6
XI	–	–	–	–	3.5	−2.9	14.7	1	−15.1	24	−1.0	2.3	−0.5	0.1	5.5	6.0	5.7	5.7	91	79	92	87	0.6	1.8	0.6	1.0	8.5	8.1	8.2	8.3
XII	–	–	–	–	4.7	−0.3	12.9	13	−7.2	14	1.1	3.4	2.2	2.2	6.1	6.4	6.6	6.3	91	81	90	87	0.7	1.6	0.8	1.0	7.9	8.0	8.7	8.2
Rok	–	–	–	–	12.1	3.0	32.0	26.VI	−19.7	9.III	5.2	10.8	6.6	7.3	8.8	9.4	9.4	9.2	90	69	89	83	1.1	5.5	1.5	2.7	6.9	7.4	6.5	6.9

Włodawa

φ = 51°33′ λ = 23°33′

I	991.7	1008.2	971.3	1014.0	−0.4	−6.1	3.4	9, 30	−20.7	11	−3.8	−1.6	−3.2	−3.0	4.6	4.9	4.7	4.7	93	88	92	91	0.3	0.6	0.4	0.4	8.3	8.5	7.9	8.2
II	992.5	1010.6	970.0	1015.0	−3.8	−10.8	0.8	14	−23.6	7	−7.8	−4.9	−6.8	−6.6	3.3	3.6	3.4	3.4	91	81	86	86	0.3	0.8	0.5	0.5	8.2	7.6	8.1	8.0
III	996.2	1011.8	970.6	1018.5	4.2	−4.1	14.6	30	−17.1	1	−2.5	3.3	−0.2	0.1	4.9	5.7	5.4	5.3	92	72	85	83	0.4	2.3	0.9	1.2	7.3	6.7	6.0	6.7
IV	991.2	1005.3	973.4	1012.6	10.4	2.2	16.4	26	−2.9	3	3.5	8.8	5.5	5.8	7.3	7.4	7.8	7.5	89	65	84	79	0.8	4.2	1.4	2.1	8.2	7.7	6.9	7.6
V	992.8	1009.0	980.2	1014.0	15.2	5.7	26.7	19	−2.3	4	8.5	13.8	9.9	10.5	9.8	9.7	10.4	10.0	86	60	84	77	1.6	6.8	2.1	3.5	7.0	7.9	6.7	7.2
VI	993.4	1000.0	982.1	1014.3	20.7	11.4	28.3	26	5.9	8	14.7	19.0	15.7	16.3	13.9	13.8	14.6	14.1	83	64	81	76	3.0	8.9	3.5	5.1	5.7	6.6	7.3	6.5
VII	992.2	1002.4	980.6	1012.9	22.2	11.2	30.1	17	6.8	5	15.3	20.9	15.6	16.8	15.2	14.6	15.0	14.9	87	59	84	77	2.4	10.7	3.1	5.4	4.0	7.1	5.5	5.8
VIII	994.6	1003.6	978.5	1015.5	21.1	10.8	29.4	8	6.5	30	13.4	19.7	14.6	15.6	13.5	14.1	14.4	14.0	87	62	86	78	2.1	9.8	2.6	4.8	5.1	6.4	4.1	5.2
IX	996.2	1012.0	984.8	1017.2	21.1	9.0	27.2	3	4.4	17	11.0	20.3	13.4	14.5	12.2	13.9	13.6	13.2	92	59	88	80	1.2	10.4	2.0	4.5	4.9	5.9	2.9	4.6
X	1001.2	1016.3	989.0	1022.9	12.1	2.3	22.1	1	−4.9	22	3.8	11.2	6.3	6.9	7.5	8.6	8.2	8.1	91	64	85	80	0.7	5.3	1.5	2.5	5.7	6.9	4.9	5.8
XI	991.7	1007.1	966.7	1013.8	0.8	−3.9	13.5	2	−16.9	17	−1.9	−0.3	−1.6	−1.4	5.0	5.2	5.1	5.1	88	82	86	85	0.7	1.3	0.8	0.9	9.1	8.9	8.4	8.9
XII	986.8	1000.7	967.7	1008.7	1.9	−2.6	7.4	20	−17.2	17	−0.9	1.0	−0.2	0.0	5.1	5.4	5.1	5.2	86	80	83	83	0.8	1.4	1.0	1.1	8.2	7.8	8.0	8.0
Rok	993.4	1016.3	966.7	1015.0	10.5	2.1	30.1	17.VII	−23.6	7.II	4.4	9.3	5.8	6.3	8.5	8.9	9.0	8.8	89	70	85	81	1.2	5.2	1.6	2.7	6.9	7.4	6.4	6.9

Wińsko

φ = 51°28′ λ = 16°37′

I	–	–	–	–	2.7	−0.8	6.5	17	−6.2	7	0.2	1.9	1.0	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	7.8	7.8
II	–	–	–	–	−1.1	−6.2	4.1	13	−12.6	10	−4.4	−2.1	−3.5	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	7.6	8.0
III	–	–	–	–	6.3	−1.3	15.6	29, 30	−11.5	7	−0.3	5.4	2.6[2]	2.6[2]	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.2	5.1	5.6
IV	–	–	–	–	11.5	3.8	16.7	6	−0.5	1	5.0	10.4	7.6	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.8	6.5	6.8
V	–	–	–	–	15.0	7.0	22.5	16	−0.1	3	9.1	13.6	10.9	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	6.6	7.2
VI	–	–	–	–	21.4	11.9	32.2	26	7.2	13	14.5	19.5	16.4	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.6	5.7	6.1
VII	–	–	–	–	20.9	12.5	30.6	14	8.0	4, 6	14.8	19.3	16.2	16.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	5.9	6.7
VIII	–	–	–	–	21.5	11.5	30.3	6	7.4	1, 14	13.8	20.3	16.1[2]	16.6[2]	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.5	4.4	4.8
IX	–	–	–	–	19.8	10.9	26.4	2	6.0	20	12.7[2]	18.7	14.9[2]	15.3[2]	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.0	3.8	5.0
X	–	–	–	–	13.5	4.4	22.5	1	−4.2	22	5.6[2]	12.7	8.1[2]	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.1	3.3	4.9
XI	–	–	–	–	3.0	−2.2	13.7	2	−11.8	18	−0.6	1.8	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.5	8.0
XII	–	–	–	–	4.0	−0.5	12.3	19	−6.6	14	1.1	2.7	1.9	1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	7.9	7.9
Rok	–	–	–	–	11.5	4.2	32.2	26.VI	−12.6	10.II	6.0[2]	10.4	7.7[2]	8.0[2]	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	6.0	6.5

Grabownica

φ = 51°28′ λ = 17°27′

I	–	–	–	–	2.9	−1.9	5.5	15, 17	−6.1	29	−0.3	2.0	0.1	0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.7	7.0	7.4
II	–	–	–	–	−0.5	−7.8	3.9	13	−17.4	6	−4.9	−1.8	−4.3	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.7	6.4	7.0
III	–	–	–	–	7.0	−3.4	15.6	30	−18.8	9	−1.1	5.6	0.9	1.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.7	5.5	5.8
IV	–	–	–	–	11.7	2.4	16.2	6	−2.4	5	4.9	10.2	5.8	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.0	6.3	6.5
V	–	–	–	–	14.9	5.9	23.6	17	−2.2	3	9.2	13.4	9.1	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	5.9	6.6
VI	–	–	–	–	21.3	10.3	32.7	26	6.2	3	15.6	19.9	14.7	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.8	5.1	5.0
VII	–	–	–	–	21.8	11.8	30.9	14	6.8	4	15.4	19.8	15.3	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.8	5.7	6.3
VIII	–	–	–	–	22.1	9.9	31.4	7	4.9	14	14.0	20.1	14.4	15.7	–	–	–	–	–	–	–	–	–	–	–	–	3.9	5.4	4.9	4.7
IX	–	–	–	–	20.9	8.5	28.3	3	3.1	22	11.6	19.4	12.6	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.8	3.7	4.4
X	–	–	–	–	13.7	2.0	22.2	1, 2	−6.6	22	3.8	12.8	5.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.1	3.0	4.1
XI	–	–	–	–	3.0	−3.2	13.5	2	−14.5	18	−1.4	1.8	−0.5	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.1	7.6
XII	–	–	–	–	3.7	−0.8	11.7	20	−6.1	15	0.8	2.7	1.5	1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.6	7.4	7.9
Rok	–	–	–	–	11.9	2.8	32.7	26.VI	−18.8	9.III	5.6	10.5	6.3	7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.6	5.7	6.1

Szprotawa $H_s = 122$ m $h_w = 12{,}5$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	1.5	5	1.8	3	2.3	·	·	1	3.0	18.5	3.9	18	2.9	5.5	2.0	36	1.8	28	7.0	9	·	1	22	·	1	·	2	17	16	11	·	–	8	·
II	9.5	2.7	9	2.1	2.5	3.4	·	·	·	·	9	4.9	12	4.0	21	4.2	21	2.8	40	5.0	13	6	15	27	·	4	·	1	18	21	12	·	–	26	·
III	9	2.7	7	2.3	4	3.0	1	2.0	·	·	19	2.7	12	3.7	11	3.2	30	2.0	38	16.5	3	8	5	21	·	·	·	3	14	10	7	2	–	17	·
IV	12.5	1.8	13	2.2	13.5	2.8	2	3.0	·	·	10.5	3.0	9.5	2.7	14	2.5	15	2.1	42	9.8	20	·	·	6	·	·	·	3	14	17	14	·	–	·	1
V	18.5	1.7	19.5	2.6	7	3.4	0.5	3.0	1	2.0	6	3.6	10	2.6	15.5	2.0	15	2.0	94	19.9	10	·	·	·	1	1	1	3	16	19	13	4	–	·	3
VI	12.5	2.0	16.5	2.2	3	3.2	0.5	3.0	·	·	8.5	4.0	11.5	3.5	14.5	2.3	23	2.0	46	11.3	1	·	·	·	6	·	·	3	8	11	9	1	–	·	3
VII	5.5	1.8	2	1.8	3.5	1.6	0.5	3.0	·	·	14.5	3.1	24.5	4.3	17.5	2.4	25	2.3	105	29.0	16	·	·	·	5	·	·	·	15	17	12	3	–	·	4
VIII	9.5	1.6	5.5	1.7	3	2.3	4	2.5	1	1.0	3	2.0	9	2.8	14	1.8	44	1.1	57	22.9	24	·	·	·	9	·	·	3	6	11	6	2	–	·	1
IX	3.5	1.9	2.5	1.6	10	2.2	1	3.5	2	2.5	6.5	3.3	13.5	2.3	7	2.0	44	1.2	70	27.8	3	·	·	·	2	·	·	8	5	8	7	2	–	·	·
X	3.5	1.0	8	1.7	11.5	2.0	·	·	0.5	2.0	9	2.2	14	3.0	8.5	1.6	38	1.2	12	5.1	16	·	·	12	·	·	·	7	11	4	3	·	–	·	·
XI	1.5	2.3	14	2.9	13	2.5	1.5	3.3	2	2.8	19	4.7	13	3.8	6	2.3	20	2.6	29	8.4	27	3	10	21	·	2	·	·	20	14	8	·	–	16	·
XII	3	1.3	1	2.0	9	2.1	2	1.2	5.5	2.8	33	4.7	27	2.7	1.5	1.3	11	3.0	55	11.2	18	·	·	19	·	3	·	1	19	21	12	1	–	6	·
Rok	94.5	1.9	103	2.1	83	2.6	13	2.0	13	1.3	156.5	3.5	174	3.2	136	2.3	322	2.0	616	29.0	16.VII	17	31	128	23	11	1	34	163	169	114	15	–	73	12

Włodawa $H_s = 175$ m $H_b = 175{,}9$ m $h_w = 13$ m

I	5.5	2.6	6	2.4	14	3.3	26	3.2	15	3.6	12	4.5	8.5	5.5	6	5.9	·	3.7	53	15.3	17	5	14	28	·	2	·	2	22	17	9	2	4	31	·
II	10.5	4.4	8	5.0	2	5.8	0.5	3.0	9.5	5.3	18	5.9	23.5	6.2	11	3.7	1	5.2	32	6.0	16	13	24	28	·	2	·	1	18	22	11	·	1	28	·
III	1	1.0	9	3.5	8	3.1	28	3.3	15	3.0	11.5	3.7	12	4.5	7.5	5.9	1	3.6	30	11.0	17	4	6	24	·	1	·	4	12	11	7	1	5	17	·
IV	5	3.9	8	4.8	26.5	5.6	26.5	5.3	5.5	3.5	9	4.7	4	4.6	4.5	4.8	1	5.0	45	10.0	23	·	·	11	·	·	·	1	17	13	10	1	1	·	2
V	12	3.0	6	2.4	9	3.6	8.5	3.5	8	1.9	8.5	3.9	13	3.5	23	3.6	5	3.1	106	32.6	29	·	·	3	1	·	·	1	14	18	11	2	2	·	8
VI	7	2.3	4.5	3.4	10	2.4	6	4.2	5	4.0	9	3.7	19	4.6	17.5	3.4	12	3.1	78	15.5	11	·	·	·	5	·	·	1	10	12	9	4	1	·	2
VII	2.5	1.2	5	3.2	6.5	2.6	13.5	2.8	12	2.6	22.5	3.2	20	3.8	8	2.2	3	2.9	157	81.0	17	·	·	·	7	1	·	2	4	18	13	3	2	·	7
VIII	9.5	4.1	2	3.8	1.5	1.7	13	2.9	9	3.1	10	2.4	22	3.7	19	3.6	7	3.1	84	19.9	1	·	·	·	10	·	·	6	5	9	9	3	·	·	2
IX	1	2.5	·	·	1.5	3.0	32.5	2.6	14.5	3.2	13	2.7	10.5	3.2	10	2.7	7	2.6	25	10.2	6	·	·	·	5	·	·	6	1	8	4	1	·	·	1
X	5	3.7	5	2.7	3.5	3.1	5.5	1.7	7.5	2.3	17	3.3	20.5	4.5	22	4.1	7	3.3	4	2.0	11	·	·	7	·	1	·	5	9	6	2	·	10	·	·
XI	3.5	1.9	7.5	3.7	13	3.4	17.5	3.7	9	3.5	11.5	5.8	18	4.6	8	2.6	2	3.8	59	9.0	12	4	11	21	·	1	·	·	22	20	13	·	6	17	·
XII	3	3.0	2.5	2.4	1.5	2.7	14.5	3.4	18	5.1	32	4.5	16	4.0	4.5	4.6	1	4.2	26	7.6	18	2	6	25	·	·	·	·	19	14	7	·	2	8	·
Rok	65.5	2.8	63.5	3.1	97	3.4	192	3.3	128	3.4	174	4.0	187	4.4	141	3.9	47	3.6	699	81.0	17.VII	28	61	147	28	8	·	29	153	168	105	17	34	101	22

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Wińsko $H_s = 180$ m $h_w = 14{,}6$ m

I	6	2.5	2	2.0	3	2.3	17.5	2.4	15.5	4.7	15.5	3.7	16.5	3.0	6	3.0	11	2.9	16	4.4	9	·	1	23	·	1	·	1	19	12	5	·	–	5	·
II	11.5	3.4	5.5	2.7	3	2.0	3	2.7	2	2.5	18	4.1	23.5	5.1	14.5	5.5	3	4.1	20	3.0	17	6	21	27	·	2	·	2	16	17	6	·	–	27	·
III	5	2.2	9	3.3	2	2.5	16.5	2.4	10	2.8	20.5	3.5	22	4.0	3	4.0	5	3.1	27	8.7	3	2	7	16	·	1	·	6	9	8	6	·	–	15	·
IV	3.5	2.1	11.5	2.4	16	2.8	10	2.7	6	2.2	9	3.9	16.5	4.0	14.5	3.4	3	3.0	36	8.2	19	·	·	1	·	1	·	4	16	16	11	·	–	·	·
V	10	2.7	10.5	2.7	9.5	2.8	4.5	4.2	4	3.0	11	3.0	20	4.5	18.5	3.9	5	3.3	121	34.0	19	·	·	1	·	1	·	3	15	23	19	3	–	·	4
VI	6	2.3	10.5	2.7	9	2.1	7.5	2.9	9.5	1.9	12	3.5	21.5	4.5	7	4.4	7	3.0	56	8.3	1	·	·	·	6	2	·	2	11	17	14	·	–	·	7
VII	7.5	2.1	2.5	2.4	4	2.5	9	2.3	10	2.4	30.5	3.7	26	4.0	2.5	4.0	1	3.3	110	29.2	16	·	·	·	4	1	·	·	8	17	14	4	–	·	9
VIII	9.5	1.5	3	1.3	6	2.3	11.5	2.4	10.5	2.7	14	2.4	23.5	4.0	12	3.4	3	2.7	43	16.0	24	·	·	·	8	1	·	5	3	12	9	1	–	·	4
IX	·	·	·	·	5	2.4	20.5	3.1	23	2.8	21	2.6	17.5	4.0	2	4.0	1	3.0	26	13.7	10	·	·	·	2	·	·	6	5	8	5	1	2	·	·
X	4.5	2.0	2.5	2.0	21	1.8	7.5	2.6	10.5	2.7	18	3.1	19.5	3.8	4.5	2.0	5	2.6	6	4.0	16	·	·	5	·	·	·	8	6	4	2	·	12	·	·
XI	3	1.7	13	3.6	15.5	2.8	4	4.6	10	5.2	16.5	3.7	21	4.8	2	4.0	5	3.7	24	6.6	27	3	10	19	·	·	·	·	19	13	6	·	7	15	·
XII	3	2.3	·	·	4	2.0	11.5	3.3	20	4.4	28	4.6	24	5.3	2.5	2.4	·	4.3	35	6.8	18	·	2	18	·	2	·	·	15	18	10	·	4	7	·
Rok	69.5	2.1	70	2.1	98	2.4	123	3.0	131	3.1	214	3.5	251.5	4.2	89	3.7	49	3.2	520	34.0	19.V	11	41	110	20	12	·	37	142	165	107	9	–	69	24

Grabownica $H_s = 119$ m $h_w = 12$ m

I	5.5	2.4	4	2.6	·	·	5	3.1	9.5	3.1	17	2.5	9	3.1	5	1.9	38	1.6	19	5.0	9	·	1	27	·	·	·	2	17	13	9	·	–	8	·
II	8	3.6	5	4.4	1	4.0	1	3.0	0.5	3.0	13	3.2	17	3.1	17.5	3.6	21	2.6	13	3.2	14	8	17	27	·	·	·	1	13	12	5	·	–	20	·
III	5	3.8	7.5	3.7	1.5	4.7	3	4.3	11	2.9	14.5	3.1	10.5	4.4	6	3.1	34	2.2	23	4.5	26	6	5	20	·	·	·	5	10	12	8	·	–	13	·
IV	3.5	2.6	9.5	3.8	8	3.3	10	3.2	3.5	2.7	8	2.4	9	3.0	11.5	2.7	27	2.1	38	11.2	19	·	·	10	·	·	·	4	15	12	7	1	–	·	2
V	5.5	2.9	10	3.0	10	2.8	4	3.0	2	3.8	4.5	2.9	11	3.0	19	2.7	27	2.0	150	21.7	29	·	·	3	·	·	·	4	13	21	19	6	–	·	5
VI	3.5	3.9	7	2.6	7.5	2.5	5	3.6	4.5	3.3	9	2.6	16	2.8	10.5	3.1	27	2.0	93	15.3	26	·	·	·	5	·	·	8	6	15	13	4	–	·	4
VII	3	1.5	5	2.3	3	2.2	3.5	1.7	3.5	1.7	13.5	2.8	25.5	3.1	8	2.4	28	1.8	91	46.0	21	·	·	·	4	·	·	2	9	21	12	2	–		5
VIII	5	2.4	3	1.7	·	·	1	3.5	12.5	2.5	6	1.9	17	2.1	12.5	2.5	36	1.4	30	7.1	9	·	·	·	9	·	·	8	7	15	8	·	–	·	1
IX	·	·	·	·	1.5	3.0	4.5	4.1	10.5	3.3	17.5	2.1	13.5	1.9	6.5	1.8	36	1.5	31	10.0	10	·	·	·	2	·	·	10	4	10	6	1	–		2
X	5	2.1	3	2.7	3	2.3	8	2.2	0.5	5.0	11	2.0	9	2.6	7.5	2.1	46	1.2	5	3.0	16	·	·	11	·	·	·	12	4	3	2	·	–	·	·
XI	0.5	4.0	9.5	3.5	10	2.7	5.5	2.9	6.5	3.5	16.5	3.4	16	3.2	8.5	2.4	17	2.5	26	5.5	27	4	10	20	·	·	·	3	16	15	12	·	–	13	·
XII	3	2.5	1	3.0	1	3.0	6	2.8	17.5	3.3	29	3.4	18.5	3.4	6	2.7	11	2.8	40	15.0	18	·	1	17	·	·	·	·	17	15	9	1	–	1	·
Rok	47.5	2.6	64.5	2.8	46.5	2.5	56.5	3.1	82	3.2	159.5	2.7	172	3.0	118.5	2.6	348	2.0	559	46.0	21.VII	18	34	135	20	·	·	59	131	164	110	15	–	55	19

Nowa Wieś — φ = 51°27' — λ = 22°45' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.3	-4.5	4.3	30	-17.4	11	-2.8	-0.8	-2.0	-1.9	4.4	4.7	4.7	4.6	83	78	85	82	0.8	1.2	0.8	0.9	8.0	7.3	7.7	7.7
II	–	–	–	–	-3.5	-10.2	1.2	14	-21.6	7	-7.3	-4.8	-6.8	-6.4	3.1	3.2	3.0	3.1	80	71	74	75	0.7	1.2	0.9	0.9	8.2	7.5	7.0	7.6
III	–	–	–	–	4.4	-3.5	14.6	30	-18.7	1	-2.0	3.6	0.4	0.6	4.7	5.3	5.1	5.0	84	65	78	76	0.8	2.9	1.4	1.7	6.6	6.0	4.7	5.8
IV	–	–	–	–	10.4	2.2	16.2	7	-2.5	3	3.7	9.2	5.7	6.1	6.7	6.9	7.1	6.9	82	59	76	72	1.3	5.0	2.2	2.8	7.9	7.8	6.1	7.3
V	–	–	–	–	14.7	5.8	25.8	19	-2.5	4	8.4	13.2	9.9	10.4	9.4	9.8	9.9	9.4	82	58	79	73	1.9	6.8	2.6	3.8	6.9	8.2	6.7	7.3
VI	–	–	–	–	20.5	11.4	28.7	26	5.8	8	14.5	19.1	15.3	16.0	13.7	13.1	14.0	13.6	83	61	81	75	3.0	9.8	3.6	5.5	6.0	7.1	6.5	6.5
VII	–	–	–	–	21.9	11.4	29.2	17	5.8	5	15.5	20.5	15.8	16.9	14.6	13.0	14.4	14.0	82	54	80	72	3.3	11.7	3.9	6.3	4.5	7.6	5.8	6.0
VIII	–	–	–	–	20.8	10.7	29.6	8	6.6	16	13.5	19.5	14.4	15.4	13.3	13.4	13.6	13.4	86	60	82	76	2.3	10.2	3.2	5.2	5.3	6.1	3.6	5.0
IX	–	–	–	–	21.2	9.1	27.3	2, 3	4.6	17	11.4	20.0	13.6	14.7	12.2	14.0	13.5	13.2	90	60	86	79	1.5	10.0	2.4	4.6	4.4	5.3	2.2	4.0
X	–	–	–	–	12.2	2.5	22.0	1	-5.2	22	4.4	11.6	6.5	7.2	7.8	9.6	8.8	8.7	91	69	88	83	0.8	4.4	1.2	2.1	5.3	5.9	3.7	5.0
XI	–	–	–	–	1.1	-3.7	12.8	2	-18.1	18	-1.8	-0.2	-1.3	-1.2	5.1	5.3	5.2	5.2	87	81	84	84	0.7	1.2	0.8	0.9	9.3	9.1	7.8	8.7
XII	–	–	–	–	1.8	-2.4	7.9	20	-19.5	17	-0.6	1.1	0.0	0.1	5.1	5.3	5.1	5.2	83	78	82	81	1.0	1.5	1.1	1.2	8.6	8.2	6.9	7.9
Rok	–	–	–	–	10.5	2.4	29.6	8.VIII	-21.6	7. II	4.7	9.3	6.0	6.5	8.3	8.6	8.7	8.5	84	66	81	77	1.5	5.5	2.0	3.0	6.8	7.2	5.7	6.6

Ostrzeszów — φ = 51°26' — λ = 17°56'

I	–	–	–	–	1.9	-2.2	4.9	9	-7.6	7	-1.0	1.1	-0.7	-0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.3	8.1	8.6
II	–	–	–	–	-1.7	-8.3	2.7	13, 14	-18.9	6	-5.8	-3.0	-5.0	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	6.0	7.2
III	–	–	–	–	6.3	-2.3	15.7	30	-14.5	9	-0.5	4.9	1.3	1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	5.5	6.2
IV	–	–	–	–	10.9	2.6	15.2	6	-1.5	5	5.2	9.7	5.5	6.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.5	5.9	6.7
V	–	–	–	–	14.4	6.0	23.8	17	-2.7	2	9.2	12.9	9.2	10.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.8	6.9	7.4
VI	–	–	–	–	20.7	11.0	32.5	26	5.2	7	15.4	19.5	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	7.6	5.4	6.0
VII	–	–	–	–	21.6	12.1	30.9	14	7.6	4	15.3	20.0	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.6	5.9	6.7
VIII	–	–	–	–	21.8	10.4	31.8	7	4.9	14	14.3	20.2	14.6	15.9	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.9	5.0	5.6
IX	–	–	–	–	20.6	10.0	28.8	3	3.5	21	12.7	19.1	13.9	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.7	4.0	5.0
X	–	–	–	–	13.0	3.7	21.9	1	-4.6	22	5.5	12.1	6.9	7.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.6	3.2	4.4
XI	–	–	–	–	2.5	-3.1	12.6	2	-15.7	18	-1.5	1.1	-0.6	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.1	8.3	8.3
XII	–	–	–	–	3.1	-1.4	10.3	20	-9.1	17	0.2	1.7	0.8	0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.3	8.1	8.3
Rok	–	–	–	–	11.3	3.2	32.5	26.VI	-18.9	6. II	5.8	9.9	6.3	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	6.0	6.7

Zawołocze — φ = 51°26' — λ = 23°34'

I	–	–	–	–	-0.3	-6.1	4.8	30	-23.5	11	-3.8	-1.3	-3.2	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.1	8.0
II	–	–	–	–	-3.5	-11.1	1.3	14	-25.2	7	-8.3	-4.6	-7.0	-6.7	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.9	7.4	8.2
III	–	–	–	–	4.4	-4.9	15.6	30	-21.6	1	-3.2	3.5	-1.0	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	5.9	6.7
IV	–	–	–	–	10.8	1.9	16.6	26	-4.4	3	3.4	9.2	5.1	5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.6	6.7	7.6
V	–	–	–	–	15.8	5.7	27.5	19	-3.9	4	8.5	14.2	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.9	7.2	7.4
VI	–	–	–	–	21.2	11.3	29.5	26	4.5	8	14.7	19.7	15.0	16.1	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	6.3	6.0
VII	–	–	–	–	22.8	11.4	30.2	16	7.1	12	15.2	21.5	15.4	16.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.5	5.3	5.5
VIII	–	–	–	–	21.6	10.9	30.8	8	6.3	31	13.1	20.2	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.5	3.9	4.7
IX	–	–	–	–	21.4	8.7	28.2	3	3.8	17	10.6	20.6	12.6	14.1	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.5	1.4	3.3
X	–	–	–	–	12.5	2.2	22.8	1	-6.1	22	3.5	11.7	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.1	4.7	5.8
XI	–	–	–	–	1.0	-3.8	13.6	2	-15.4	17	-2.1	-0.2	-1.7	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.8	8.9	9.0
XII	–	–	–	–	2.0	-2.7	7.3	20	-19.9	17	-1.0	1.1	-0.2	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.2	8.7	8.7
Rok	–	–	–	–	10.8	2.0	30.8	8.VIII	-25.2	7. II	4.2	9.6	5.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.1	6.7

Piotrków Trybunalski — φ = 51°25' — λ = 19°42'

I	–	–	–	–	0.8	-3.9	3.9	18	-11.9	11	-2.2	-0.1	-1.6	-1.4	4.9	5.3	5.1	5.1	91	86	92	90	0.4	0.8	0.4	0.5	8.9	8.1	6.8	7.9
II	–	–	–	–	-2.5	-9.8	1.9	14	-19.5	6	-7.1	-4.1	-6.1	-5.8	3.4	3.7	3.5	3.5	88	80	86	85	0.4	0.9	0.5	0.6	9.0	7.5	6.6	7.7
III	–	–	–	–	5.4	-3.5	15.4	30	-14.2	8	-2.2	3.8	0.8	0.8	5.1	6.8	5.6	5.5	91	70	84	82	0.5	2.7	1.1	1.4	7.8	7.0	5.1	6.6
IV	–	–	–	–	10.3	2.0	15.9	30	-1.9	1, 15	3.6	8.9	5.5	5.9	7.2	7.8	7.8	7.6	89	70	85	81	0.8	3.8	1.4	2.0	7.4	8.1	5.9	7.1
V	–	–	–	–	14.3	5.9	22.9	17	-1.8	4	8.5	12.8	9.4	10.0	9.6	9.9	10.0	9.8	83	65	82	77	1.8	5.3	2.1	3.1	7.4	8.6	6.2	7.4
VI	–	–	–	–	21.0	10.9	31.9	26	5.7	3	14.5	19.3	15.0	16.0	13.3	14.1	13.6	13.7	80	65	79	75	3.4	9.0	3.7	5.4	6.1	7.7	6.7	6.8
VII	–	–	–	–	21.8	11.6	38.1	15	6.2	6	15.1	19.8	15.0	16.2	14.5	14.1	14.6	14.4	83	61	85	76	3.0	9.8	2.9	5.2	7.7	8.2	6.0	7.3
VIII	–	–	–	–	21.6	10.5	30.7	17	5.6	14	13.2	19.8	14.7	15.6	13.4	13.1	13.6	13.4	87	58	81	75	2.1	11.1	3.6	5.6	6.2	7.9	4.0	6.0
IX	–	–	–	–	20.8	9.3	27.6	3	3.6	16	11.3	19.1	13.7	14.4	12.5	14.0	13.8	13.4	93	64	88	82	1.1	8.7	2.1	4.0	6.1	6.8	4.4	5.8
X	–	–	–	–	12.6	2.8	21.9	1, 2	-5.5	22	4.5	11.7	6.6	7.4	8.3	9.8	9.0	9.0	85	70	90	82	0.4	4.4	1.0	1.9	6.9	6.7	3.9	5.8
XI	–	–	–	–	2.0	-3.8	12.4	2	-17.3	18	-2.3	0.5	-0.8	-0.8	5.1	5.7	5.6	5.5	91	85	89	88	0.5	1.1	0.6	0.7	8.8	8.8	8.7	8.8
XII	–	–	–	–	2.4	-2.4	9.1	19	-15.8	17	-0.2	1.3	0.1	0.3	5.6	5.6	5.6	5.6	91	85	89	87	0.5	1.2	0.7	0.8	8.9	8.1	7.3	8.0
Rok	–	–	–	–	10.9	2.5	31.9	26.VI	-19.5	6. II	4.7	9.4	6.0	6.5	8.6	9.1	9.0	8.9	88	71	86	82	1.2	4.0	1.7	2.5	7.6	7.8	6.0	7.1

Nowa Wieś $H_s = 179$ m $h_w = 16$ m 1965

MIESIĄC	ROZKŁAD WIATRU $\%D, V_mD$ N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7.5	2.2	2.5	1.4	9.5	3.3	21	3.3	13	3.7	15.5	3.4	11	4.0	5	8.4	8	3.3	31	10.2	17	4	10	26	·	2	·	3	17	15	9	1	[illegible]	[illegible]	—
II	11	3.9	7	3.6	2.5	5.4	0.5	5.0	5	3.9	17.5	3.9	24.5	4.4	13	5.1	3	4.1	23	4.9	7	14	23	28	·	1	·	1	15	19	9	·	3	28	—
III	1.5	4.3	6.5	3.5	4.5	3.0	18	2.2	14.5	2.6	13.5	3.3	12.5	4.0	6	4.3	16	2.6	19	6.3	17	3	7	21	·	·	·	6	10	9	6	·	4	18	—
IV	6	3.5	4.5	2.9	24.5	6.2	30	3.9	2	4.0	9.5	2.5	5	2.8	4.5	4.6	4	4.1	38	16.1	28	·	·	9	·	3	·	·	11	10	8	1	3	·	—
V	7.5	3.1	5.5	2.1	11	4.3	7.5	2.8	4.5	1.7	6	2.7	14.5	2.6	16.5	3.0	20	2.3	72	15.2	25	·	·	2	1	·	·	1	14	17	11	1	·	·	—
VI	4.5	2.3	6.5	2.8	10	3.8	6	3.4	6	2.5	6	3.2	23	3.5	17	2.6	11	2.7	98	17.1	14	·	·	·	5	·	·	2	13	11	9	4	·	·	—
VII	0.5	2.0	3.5	2.7	7	2.6	8	2.2	8	2.8	15	2.6	27.5	3.1	6.5	1.3	17	2.2	46	13.7	17	·	·	·	7	·	·	2	7	19	10	1	·	·	—
VIII	7	2.3	0.5	3.0	1.5	2.3	10.5	2.7	5.5	2.5	9.5	2.1	18.5	3.1	23	3.8	17	2.5	54	14.9	2	·	·	·	8	·	·	5	6	10	8	2	·	·	—
IX	·	·	·	·	2.5	2.6	19	2.6	19.5	2.5	15.5	2.6	11	2.9	9.5	2.2	13	2.2	33	12.7	11	·	·	·	5	·	·	7	2	6	4	1	1	·	—
X	4	2.8	4	2.0	6	2.5	3.5	2.3	6	2.0	11.5	3.1	22	3.4	20	2.9	16	2.4	5	1.5	11	·	·	6	·	·	·	6	4	5	3	·	5	·	—
XI	2	2.0	8.5	4.5	10	3.4	12	3.6	11	3.0	8	4.2	25	3.9	1.5	2.3	12	3.2	39	4.5	27	4	11	19	·	·	·	·	20	18	13	·	7	19	—
XII	3	2.7	1.5	2.3	2.5	3.0	12	3.2	14.5	3.6	33	4.2	17.5	3.7	3	4.3	6	3.5	34	11.9	18	2	6	20	·	·	·	·	17	15	7	1	1	9	—
Rok	54.5	2.6	50.5	2.6	91.5	3.5	148	3.1	109.5	2.9	160.5	3.2	212	3.4	125.5	3.7	143	2.9	492	17.1	14.VI	27	57	131	26	6	·	33	136	154	97	12	27	105	—

Ostrzeszów $H_s = 198$ m $h_w = 12$ m

I	5.5	2.5	3	3.0	0.5	5.0	15.5	2.5	17.5	2.2	13.5	3.7	6	4.8	4.5	3.0	27	2.1	33	5.8	8	·	5	27	·	2	·	·	21	11	8	·	4	20	·
II	8	3.2	6	2.8	5	2.4	3	1.3	2	2.0	11.5	3.5	24.5	4.0	14	3.9	10	3.0	24	4.0	17	8	21	28	·	1	·	2	15	19	9	·	1	28	·
III	2	5.0	8	3.2	4	3.0	7.5	3.2	17.5	2.1	14.5	3.8	14	3.6	8.5	3.1	17	2.6	23	5.9	26	4	6	18	·	·	·	5	14	11	8	·	4	15	·
IV	1.5	3.3	8.5	3.8	13	3.7	17	3.1	3	4.3	6	3.7	16.5	3.8	7.5	2.7	17	2.8	56	10.2	19, 23	·	·	4	·	·	·	4	12	14	10	2	1	·	4
V	7	3.0	5.5	2.4	10.5	5.1	10	4.0	-	-	10	2.3	10.5	3.0	15.5	2.7	15	2.7	165	26.1	9	·	·	3	·	1	·	2	18	22	20	6	1	·	4
VI	3	3.7	6.5	3.0	10.5	3.5	7	3.7	10.5	3.6	15.5	2.6	13	4.6	10	4.2	14	3.0	69	17.0	27	·	·	·	5	·	·	2	7	17	12	3	·	·	3
VII	1.5	2.0	3	2.3	2.5	2.2	9	2.8	7.5	2.5	24	3.4	21	3.3	4.5	2.8	20	2.4	64	28.0	21	·	·	·	4	·	·	2	13	17	13	1	·	·	7
VIII	6.5	1.7	1	1.0	0.5	3.0	5.5	3.0	12	2.8	7.5	2.1	19	2.1	16	3.1	25	1.8	54	16.8	25	·	·	·	8	·	·	3	5	12	7	3	1	·	1
IX	·	·	·	·	0.5	4.0	14.5	3.9	20	2.6	10.5	2.1	17.5	2.7	2	2.8	25	2.1	53	22.4	28	·	·	·	2	1	·	6	8	8	8	1	1	·	1
X	0.5	1.0	1.5	1.7	5.5	2.3	8.5	2.6	7	1.7	12	1.8	12	3.6	11	2.8	35	1.6	6	4.5	16	·	·	8	·	·	·	9	7	2	2	·	7	·	·
XI	0.5	1.0	6	5.2	8.5	4.6	14.5	3.3	10	4.2	13	4.3	19	3.2	2.5	3.4	16	3.2	30	5.8	27	4	10	18	·	5	·	1	20	13	11	·	9	15	·
XII	5	2.1	0.5	2.0	0.5	2.0	10.5	4.5	18	3.3	30.5	5.0	12.5	4.1	4.5	2.6	11	3.6	50	18.8	18	·	3	20	·	4	2	·	19	15	8	1	2	8	·
Rok	41	2.4	49.5	2.5	61.5	3.4	122.5	3.2	125	2.6	168.5	3.2	194.5	3.6	100.5	3.1	232	2.6	627	28.0	21.VII	16	45	126	19	14	2	36	159	161	116	17	31	86	20

Zawołocze $H_s = 165$ m $h_w = 12$ m

I	6	4.2	1	4.0	7.5	2.9	20	4.0	12.5	3.0	15	4.5	7.5	5.0	5.5	6.7	18	3.3	49	12.1	17	6	13	26	·	4	·	2	21	17	11	2	4	31	—
II	11.5	2.8	6	3.0	5	2.6	·	·	5.5	5.8	16.5	4.4	20.5	3.7	11	4.8	8	3.5	41	7.7	16	14	23	28	·	3	2	·	16	21	12	·	2	28	—
III	0.5	6.0	5.5	2.6	3.5	2.6	20	2.6	10	2.0	16.5	2.7	4.5	3.9	8.5	4.1	24	2.1	44	13.0	17	7	6	25	·	1	·	4	14	11	8	1	5	20	—
IV	3	3.0	5	2.6	22.5	4.4	31	4.4	3.5	2.9	6.5	3.8	7	2.9	3.5	4.1	8	3.6	58	15.4	23	·	·	10	·	1	·	·	13	12	9	2	·	·	—
V	8	2.6	2	2.0	8.5	3.8	11.5	3.0	3	1.7	15	3.6	12	3.2	19	3.1	14	2.6	99	28.4	29	·	·	3	1	1	·	·	14	18	14	3	1	·	—
VI	6.5	2.6	3.5	2.9	8.5	3.8	7	3.8	6	3.7	7	3.6	23.5	3.6	9	2.2	19	2.6	56	16.0	28	·	·	·	6	·	·	4	9	9	7	3	2	·	—
VII	·	·	1.5	1.3	6.5	2.3	7	3.0	10	2.9	22	3.6	24	3.3	1	3.0	21	2.5	120	55.7	17	·	·	·	10	1	·	6	7	16	11	3	·	·	—
VIII	6	2.6	1.5	6.0	·	·	11.5	2.8	3.5	2.3	10	2.6	22.5	2.9	12	2.6	26	2.0	74	22.4	2	·	·	·	10	·	·	7	6	9	8	2	·	·	—
IX	·	·	·	·	2.5	2.2	18.5	2.6	13.5	2.3	14.5	2.1	11.5	2.6	3.5	2.7	26	1.7	30	14.5	11	·	·	·	5	·	·	9	·	7	4	1	1	·	—
X	2	3.8	1.5	3.3	0.5	4.0	8.5	2.6	6	2.1	16	2.9	17.5	3.5	14	2.9	27	2.1	7	3.4	11	·	·	6	·	·	·	6	8	5	2	·	7	·	—
XI	1.5	1.3	7	4.4	10.5	3.3	12	4.4	6.5	3.5	14.5	5.4	15.5	4.7	1.5	2.0	21	3.3	69	11.2	21	4	12	22	·	3	·	·	23	18	15	1	3	17	—
XII	1.5	1.3	3	2.3	1.5	4.3	16	3.1	11	3.5	34	4.6	17.5	2.5	1.5	2.7	7	3.3	32	9.1	18	3	7	24	·	3	·	·	20	13	8	·	·	4	—
Rok	46.5	2.5	37.5	2.9	77	3.0	163	3.0	91	3.0	187.5	3.6	183.5	3.5	90	3.4	219	2.7	679	55.7	17.VII	34	61	144	32	17	2	38	151	156	109	18	25	100	—

Piotrków Trybunalski $H_s = 200$ m $h_w = 13{,}5$ m

I	3.5	2.4	4.5	3.7	4.5	3.2	14.5	2.4	14.5	5.0	20	3.6	10.5	3.7	10	2.5	11	3.0	29	5.1	24	1	10	27	·	1	1	1	16	15	10	·	—	28	·
II	15.5	4.5	7.5	4.6	3	3.3	0.5	2.0	2	1.8	15.5	4.2	18.5	3.4	19.5	3.0	2	3.7	17	3.8	7	11	23	28	·	2	1	2	14	19	4	·	—	28	·
III	2	4.0	6.5	4.1	3	1.7	9.5	3.1	14	2.6	17	3.9	22	2.5	11	3.5	8	2.8	29	6.8	26	4	6	21	·	1	·	2	12	11	7	·	—	15	·
IV	8	3.9	9.5	4.1	19	5.4	11.5	2.2	6	3.5	10	1.9	13	3.4	7	2.7	6	3.3	57	12.8	23	·	·	7	·	1	·	3	15	14	12	1	—	·	1
V	12.5	2.2	12.6	2.5	7	4.1	6.5	4.2	2.5	2.4	5.5	4.2	23	2.4	14.5	2.8	4	2.7	131	22.0	28	·	·	3	·	1	·	2	16	17	15	5	—	·	4
VI	12.5	3.4	10	5.3	4	5.5	7.5	3.1	8	3.5	5.5	4.3	22	2.7	16.5	2.9	4	3.3	75	13.1	14	·	·	·	4	1	·	2	13	15	12	3	—	·	4
VII	2	2.5	8.5	2.3	4.6	2.6	1	3.0	6.5	3.0	24.5	3.4	32.5	2.3	6.5	2.4	8	2.5	40	6.0	31	·	·	·	7	·	·	·	13	16	11	·	—	·	4
VIII	6.5	2.5	0.5	1.0	0.5	1.0	7.5	3.0	11	3.0	9	3.6	13.5	2.2	19.5	2.3	25	1.9	71	24.1	25	·	·	·	11	·	·	1	9	13	9	2	—	·	1
IX	·	·	2.5	2.6	4.5	2.3	18	3.4	18.5	2.8	11	3.3	22	2.2	8.5	2.1	5	2.6	79	42.1	4	·	·	·	2	·	·	4	8	8	7	2	—	·	2
X	12	1.6	10	1.8	9	2.1	4	2.5	8	2.1	15	3.3	11	3.3	15	2.4	9	2.2	6	4.1	16	·	·	6	·	·	·	4	9	4	1	·	—	·	·
XI	2	1.5	15.5	4.7	8	2.7	13	3.1	9.5	3.0	18.5	4.0	11.5	2.9	7	1.9	5	3.2	27	4.3	3	6	9	21	·	·	·	1	22	20	8	·	—	18	·
XII	1.5	5.7	4	2.5	3.5	1.9	14	3.4	21	5.6	28.5	4.7	12.5	3.9	4	3.2	4	4.2	57	21.8	18	2	6	21	·	3	1	·	17	18	10	1	—	13	·
Rok	83	2.8	91.5	3.3	70.5	3.0	107.5	3.0	120.5	3.2	180	3.7	212	2.9	139	2.6	91	3.0	618	42.1	4.IX	24	54	134	24	10	3	22	164	170	106	14	—	102	16

Radom 1965

$\varphi = 51°25'$ $\lambda = 21°07$

MIESIĄC	CIŚNIENIE P: P_m	Max	Min	$P_{o.m}$	TEMPERATURA T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	990.2	1005.9	968.8	1012.8	0.8	−4.0	4.1	1, 18	−13.9	11	−2.4	0.0	−1.8	−1.5	4.9	5.3	5.0	5.1	91	87	91	90	0.4	0.9	0.5	0.6	8.2	8.4	8.2	8.3
II	993.1	1010.0	970.9	1016.1	−2.7	−10.2	2.1	13, 14	−21.8	6	−7.3	−4.2	−6.7	−6.2	3.3	3.7	3.3	3.4	86	80	84	83	0.5	0.9	0.6	0.7	7.6	7.5	7.7	7.6
III	995.0	1011.6	966.3	1017.4	5.4	−3.0	15.7	30	−14.6	1	−1.6	4.1	0.9	1.1	5.2	5.9	5.7	5.6	90	71	84	82	0.6	2.7	1.1	1.5	7.7	6.4	7.3	7.1
IV	989.3	1006.7	973.0	1011.2	10.6	2.1	15.7	16	−1.0	1	4.0	8.9	6.2	6.3	7.2	7.5	7.5	7.4	87	66	79	77	1.1	4.1	2.1	2.4	9.1	8.2	8.3	8.5
V	992.1	1008.0	979.3	1013.7	14.7	5.6	27.5	19	−2.5	4	9.0	12.8	10.2	10.6	9.6	9.4	10.3	9.8	82	62	81	75	2.1	5.8	2.4	3.4	6.1	8.2	7.9	7.4
VI	992.6	1000.7	981.9	1013.8	20.9	11.2	30.2	26	7.1	3, 15	14.3	19.2	15.5	16.1	13.3	13.2	13.4	13.3	82	61	77	73	3.1	9.8	4.4	5.8	5.7	7.8	7.0	6.8
VII	991.1	1000.3	979.7	1012.2	21.6	11.4	29.0	14, 16	5.6	5	15.2	20.0	15.7	16.6	14.2	13.6	14.7	14.2	81	58	82	74	3.3	10.5	3.5	5.8	6.4	7.7	7.6	7.2
VIII	994.6	1002.3	985.0	1015.8	20.3	10.8	30.5	7	6.6	16	13.9	19.2	14.8	15.7	14.1	13.7	13.9	13.9	88	63	83	78	2.1	9.7	3.4	5.0	5.0	6.6	6.5	6.0
IX	994.8	1012.6	984.7	1016.0	21.0	9.7	25.7	2	5.4	16	11.5	19.5	14.1	14.8	12.5	13.6	13.6	13.2	91	60	83	78	1.3	9.6	2.8	4.6	5.8	5.6	3.5	5.0
X	1001.2	1015.5	988.6	1023.1	12.1	3.6	21.8	1	−5.7	22	4.9	11.0	6.8	7.4	8.2	9.2	8.9	8.8	92	68	88	83	0.7	4.6	1.2	2.2	6.9	6.2	3.5	5.5
XI	990.3	1008.1	964.7	1012.6	1.7	−3.6	12.8	2	−18.2	18	−2.1	0.3	−0.9	−0.9	5.1	5.4	5.4	5.3	90	82	88	87	0.6	1.3	0.7	0.9	8.8	8.9	7.9	8.5
XII	984.9	1001.3	964.4	1007.0	2.3	−2.8	9.5	20	−18.2	17	−0.7	1.1	−0.5	−0.2	5.4	5.5	5.2	5.4	88	82	87	86	0.7	1.3	0.8	0.9	8.0	8.2	7.6	7.9
Rok	992.4	1015.5	964.4	1014.3	10.7	2.6	30.5	7.VIII	−21.8	6. II	4.9	9.3	6.2	6.6	8.6	8.8	8.9	8.8	87	70	84	80	1.4	5.1	2.0	2.8	7.1	7.5	6.9	7.2

Puławy

$\varphi = 51°25'$ $\lambda = 21°58'$

I	—	—	—	—	0.8	−4.1	4.3	30	−14.8	11	−2.3	−0.2	−1.7	−1.5	4.6	5.0	4.8	4.8	87	82	87	85	0.6	1.1	0.7	0.8	7.9	8.3	7.6	7.9
II	—	—	—	—	−2.8	−10.4	2.3	14	−22.2	24	−7.5	−4.2	−6.5	−6.2	3.2	3.4	3.1	3.2	85	73	78	79	0.5	1.2	0.8	0.8	7.6	8.3	6.8	7.6
III	—	—	—	—	5.3	−3.5	15.7	30	−17.2	1	−1.9	3.8	0.8	0.9	5.0	5.5	5.4	5.3	88	67	79	78	0.6	2.9	1.3	1.6	7.4	6.9	4.4	6.2
IV	—	—	—	—	11.0	2.3	17.4	7	−2.1	3	4.0	9.2	6.3	6.4	6.9	6.9	7.3	7.0	83	59	75	72	1.4	5.0	2.4	2.9	8.8	8.3	6.5	7.9
V	—	—	—	—	15.0	5.8	26.3	19	−2.8	4	8.5	13.4	10.3	10.6	9.5	8.9	10.0	9.5	82	57	78	72	1.9	6.9	2.8	3.9	6.9	8.6	7.0	7.5
VI	—	—	—	—	21.2	11.3	29.8	26	6.4	8	14.6	19.5	16.0	16.5	13.6	13.0	13.9	13.5	81	59	76	72	3.2	10.4	4.5	6.0	6.4	7.9	6.1	6.8
VII	—	—	—	—	22.2	11.6	29.8	17	6.1	5	15.5	20.6	16.0	17.0	14.7	13.6	14.6	14.3	83	56	79	73	3.2	11.4	4.0	6.2	7.0	8.4	6.5	7.3
VIII	—	—	—	—	21.2	10.8	30.0	8	5.9	16	13.1	19.6	14.9	15.6	13.6	13.5	14.0	13.7	89	60	82	77	1.8	10.3	3.5	5.2	6.5	6.4	4.3	5.7
IX	—	—	—	—	21.4	9.6	27.1	2	3.9	16	11.9	20.0	13.9	14.9	12.4	13.2	13.4	13.0	89	57	84	77	1.9	10.6	2.8	5.1	6.0	6.6	2.6	5.1
X	—	—	—	—	12.5	3.0	22.3	1	−5.1	22	4.7	11.4	6.6	7.3	8.1	9.0	8.9	8.7	92	66	89	82	0.7	4.9	1.2	2.3	6.9	7.2	3.9	6.0
XI	—	—	—	—	1.8	−3.5	13.0	2	−18.8	18	−1.8	0.4	−1.1	−0.9	5.1	5.2	5.3	5.2	89	79	87	85	0.6	1.6	0.8	1.0	8.6	9.4	8.9	9.0
XII	—	—	—	—	2.2	−2.5	8.5	20	−17.8	17	−0.8	1.1	−0.3	−0.1	5.2	5.5	5.3	5.3	88	81	86	85	0.7	1.3	0.9	1.0	8.4	9.3	7.2	8.3
Rok	—	—	—	—	11.0	2.5	30.0	8.VIII	−22.2	24. II	4.8	9.6	6.3	6.8	8.5	8.6	8.8	8.6	86	66	82	78	1.4	5.6	2.1	3.0	7.4	8.0	6.0	7.1

Opoczno

$\varphi = 51°23'$ $\lambda = 20°16'$

I	—	—	—	—	1.0	−3.8	5.3	30	−12.2	11	−2.2	0.1	−1.6	−1.3	4.7	5.2	4.9	4.9	87	83	87	86	0.7	1.1	0.7	0.8	8.4	8.1	8.2	8.3
II	—	—	—	—	−2.6	−9.8	2.2	13, 14	−20.6	6	−6.9	−4.0	−6.7	−6.1	3.3	3.5	3.3	3.4	84	74	83	80	0.6	1.1	0.6	0.8	7.9	7.2	6.2	7.1
III	—	—	—	—	5.3	−3.3	15.3	30	−13.9	1	−2.2	4.2	0.2	0.6	4.9	5.8	5.6	5.4	88	69	85	81	0.6	2.8	0.9	1.4	6.1	6.0	5.3	5.8
IV	—	—	—	—	10.2	1.7	15.5	29	−3.2	15	3.4	8.7	5.3	5.7	7.1	7.8	7.7	7.5	89	70	85	81	0.8	3.7	1.4	2.0	8.0	7.6	5.8	7.1
V	—	—	—	—	13.9	5.1	21.8	17	−2.9	4	8.4	12.4	9.3	9.8	9.6	9.9	10.3	9.9	84	68	85	79	1.7	4.8	1.7	2.7	6.1	8.0	6.4	6.8
VI	—	—	—	—	20.8	10.3	31.7	26	4.7	3	14.1	19.1	14.4	15.4	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.4	4.9	5.5
VII	—	—	—	—	21.7	10.6	29.6	15	4.6	5	14.7	19.8	14.4	15.8	14.5	14.6	15.1	14.7	86	64	91	80	2.5	9.3	1.6	4.5	4.8	7.0	5.0	5.6
VIII	—	—	—	—	21.1	9.8	30.2	8	4.4	31	12.5	19.5	13.8	14.9	13.2	13.3	13.9	13.5	90	61	88	80	1.7	10.3	2.5	4.8	4.5	5.6	3.6	4.6
IX	—	—	—	—	20.8	8.6	26.7	3	3.0	21	10.8	19.4	13.4	14.2	12.4	14.4	13.8	13.5	94	65	89	83	1.0	8.5	1.9	3.8	4.2	5.0	4.0	4.4
X	—	—	—	—	12.6	2.0	21.5	1	−6.1	22	4.0	11.7	5.9	6.9	8.0	10.0	9.0	9.0	94	71	94	86	0.4	4.2	0.6	1.7	5.6	5.3	4.1	5.0
XI	—	—	—	—	2.0	−4.0	12.2	2	−20.2	18	−2.3	0.5	−1.2	−1.0	5.0	5.6	5.4	5.3	89	83	88	87	0.6	1.2	0.6	0.8	8.0	8.2	8.2	8.1
XII	—	—	—	—	2.4	−2.3	10.0	20	−17.5	17	−0.4	1.5	−0.2	0.2	5.3	5.5	5.4	5.4	86	80	86	84	0.9	1.4	0.9	1.1	7.7	7.4	7.3	7.5
Rok	—	—	—	—	10.8	2.1	31.7	26.VI	−20.6	6. II	4.5	9.4	5.6	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.8	5.8	6.3

Sulejów

$\varphi = 51°22'$ $\lambda = 19°53'$

I	—	—	—	—	0.9	−4.3	4.8	18	−11.6	11	−2.2	0.1	−1.7	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.5	7.0	7.6
II	—	—	—	—	−2.4	−10.1	2.4	13	−19.9	6	−7.0	−3.8	−6.1	−5.8	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.1	5.9	7.0
III	—	—	—	—	5.0	−3.9	15.1	30	−14.2	9	−2.4	3.9	−0.2	0.3	—	—	—	—	—	—	—	—	—	—	—	—	6.0	5.8	4.5	5.4
IV	—	—	—	—	10.2	1.8	15.2	29	−2.5	15	3.4	8.8	5.3	5.7	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.0	5.1	6.4
V	—	—	—	—	14.1	5.4	21.7	17	−2.5	4	8.4	12.6	9.4	10.0	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.4	6.1	6.6
VI	—	—	—	—	20.6	10.4	31.0	26	5.0	15	14.3	19.1	14.5	15.6	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.0	4.7	5.1
VII	—	—	—	—	21.6	11.3	29.5	15	6.3	5	15.0	19.8	14.6	16.0	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.7	4.6	5.8
VIII	—	—	—	—	21.3	10.1	30.8	7	5.0	31	12.9	19.8	14.1	15.2	—	—	—	—	—	—	—	—	—	—	—	—	4.9	5.6	4.2	4.9
IX	—	—	—	—	20.5	9.1	26.5	3	2.7	21	10.8	19.0	13.1	14.0	—	—	—	—	—	—	—	—	—	—	—	—	4.1	4.9	3.7	4.2
X	—	—	—	—	12.7	2.4	22.1	1	−6.0	22	4.0	11.9	6.0	7.0	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.0	3.9	4.8
XI	—	—	—	—	2.2	−3.8	12.6	2	−17.9	18	−2.3	0.4	−0.9	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.1	8.0	8.1
XII	—	—	—	—	2.7	−2.1	10.1	20	−15.9	17	−0.2	1.6	0.0	0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.6	6.2	7.3
Rok	—	—	—	—	10.8	2.2	31.0	26.VI	−19.9	6. II	4.6	9.4	5.7	6.4	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.6	5.3	6.1

Radom $H_s = 178$ m $H_b = 178{,}8$ m $h_w = 13$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V>15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4	3.8	3	3.0	0.5	6.0	23.5	3.2	5.5	4.3	25	2.9	8	3.8	7.5	4.5	16	2.8	31	4.8	20	3	10	26	·	1	·	2	22	18	11	·	6	23	·
II	5.5	5.6	5	5.0	2	4.5	·	·	4.5	4.2	27	4.3	14	3.4	14	6.3	12	4.0	22	6.0	17	13	23	28	·	2	·	1	14	22	7	·	1	28	·
III	3	3.2	5	2.9	3	2.7	13.5	3.0	17.5	3.4	6.5	3.6	11.5	3.9	6	4.7	27	2.5	22	7.2	3	2	7	20	·	·	·	2	14	10	4	·	6	16	·
IV	5	2.4	10	5.1	20	4.1	19	2.9	3	1.0	10	4.0	5.5	2.9	4.5	5.6	13	3.2	36	8.2	23	·	·	7	·	1	·	1	22	12	11	·	2	·	1
V	8.5	3.6	12	2.4	9	2.9	10	2.8	6	3.2	8	4.0	7	3.0	16.5	3.3	16	2.6	67	16.8	29	·	·	3	1	·	·	·	16	17	11	2	1	·	4
VI	6.5	3.6	6	2.6	8	3.0	8.5	3.7	2	2.8	9.5	3.7	17	3.5	12.5	2.9	20	2.6	76	16.5	27	·	·	·	5	·	·	1	12	13	11	2	·	·	2
VII	2.5	2.2	1.5	2.3	4	3.2	7	2.9	6	1.7	20	3.4	21	3.1	6	2.3	25	2.1	91	46.5	17	·	·	·	6	·	·	1	14	16	9	3	·	·	1
VIII	9.5	3.3	2	1.5	·	·	15	2.1	3.5	1.7	6.5	2.8	12	2.4	18.5	3.4	26	2.0	113	35.0	26	·	·	·	9	·	·	3	13	13	10	4	·	·	·
IX	·	·	·	·	3	1.7	31	2.7	7	2.0	13	2.2	11	1.6	5	2.2	20	1.8	27	15.6	29	·	·	·	2	·	·	6	5	8	6	1	3	·	1
X	8	2.2	3	2.0	5.5	1.9	4.5	1.4	4.5	1.8	20	2.7	10	3.0	18.5	2.3	19	1.9	9	3.2	11	·	·	4	·	·	·	6	8	9	3	·	8	·	·
XI	·	·	14	3.1	7	2.6	11	3.4	7.5	3.6	17	4.9	11.5	3.3	5	3.0	17	2.9	40	9.0	12	6	9	21	·	2	·	·	20	16	10	·	7	16	·
XII	2	1.5	·	·	2	2.5	18.5	2.7	20	4.4	23.5	3.4	11	3.3	5	3.2	11	3.0	47	13.6	18	2	6	24	·	1	·	1	16	11	9	1	1	15	·
Rok	54.5	2.6	61.5	2.5	64	2.9	161.5	2.6	87	2.8	186	3.5	139.5	3.1	119	3.6	222	2.6	581	46.5	17.VII	26	55	133	23	7	·	24	175	165	102	13	35	98	9

Puławy $H_s = 142$ m $h_w = 12$ m

I	8	2.3	5.5	2.5	7.5	2.5	13.5	3.0	29.5	2.4	7.5	2.0	4.5	3.4	11	5.8	6	2.8	31	4.6	20	2	8	27	·	4	1	2	18	13	9	·	6	31	·
II	12	3.5	5	3.6	2.5	4.6	2	2.5	7.5	3.3	12	2.5	13.5	3.7	22.5	4.2	7	3.3	28	6.2	7	14	23	28	·	2	1	3	15	21	8	·	2	28	·
III	2.5	5.0	5.5	2.8	4	1.9	12	2.2	24.5	1.8	11	2.6	6.5	4.4	9	4.1	18	2.2	22	6.1	21	5	6	20	·	1	·	4	11	16	6	·	8	17	·
IV	4.5	3.9	4	4.4	20.5	6.0	28	5.1	9.5	1.7	3.5	2.6	2.5	3.0	8.5	3.1	9	4.0	35	8.2	23	·	·	9	·	8	2	·	18	8	6	·	2	·	3
V	9.5	2.9	4.5	2.1	12	3.5	11.5	3.5	4.5	2.2	7	2.6	8.5	3.1	19.5	4.4	16	2.8	58	11.2	28	·	·	2	1	3	2	2	15	19	13	1	3	·	4
VI	6	2.8	5.5	2.9	10.5	3.5	7.5	3.5	5.5	3.4	6	2.9	14	2.8	16	3.6	17	2.6	62	15.3	14	·	·	·	6	1	1	2	12	12	10	2	·	·	4
VII	1.5	2.0	2.5	2.8	8	2.8	7.5	2.5	12.5	2.2	15.5	2.1	17	2.5	8.5	3.0	20	1.9	62	14.5	18	·	·	·	8	1	·	2	15	17	12	2	1	·	6
VIII	7.5	3.3	2.5	2.6	0.5	1.0	11.5	1.6	11	1.7	3.5	1.9	10.5	1.9	18	3.1	28	1.6	133	33.2	26	·	·	·	9	2	·	4	10	12	9	5	2	·	1
IX	·	·	·	·	0.5	1.0	19	2.1	19	2.0	5.5	1.9	12	2.0	7	2.1	27	1.4	21	9.4	29	·	·	·	4	1	·	6	5	9	4	·	2	·	·
X	7	2.3	0.5	3.0	4.5	2.1	6.5	1.2	11	1.4	2.5	1.2	8.5	1.8	28.5	2.2	24	1.4	9	2.8	11	·	·	6	·	·	·	4	7	11	3	·	5	·	·
XI	1.5	2.0	7	2.7	10	2.4	15	1.8	11.5	2.0	9	2.1	11	2.6	10	2.6	15	1.9	35	4.8	3	5	9	19	·	1	·	·	22	24	12	·	6	16	·
XII	2	1.2	1.5	2.3	1.5	2.0	11	2.4	26	2.6	22	2.5	9	1.7	9	2.7	11	2.1	38	12.8	18	2	4	26	·	3	2	1	21	18	9	1	1	10	·
Rok	62	2.6	44	2.6	82	2.8	145	2.6	172	2.2	105	2.2	117.5	2.7	169.5	3.4	198	2.3	534	33.2	26.VIII	26	50	137	28	27	9	30	169	180	101	11	38	102	18

Opoczno $H_s = 180$ m $h_w = 14{,}6$ m

I	7.5	4.9	6.5	3.4	3.5	3.0	13.5	2.8	23.5	3.7	15	4.1	11	5.0	8.5	4.3	4	3.7	27	4.6	24	2	9	25	·	6	·	1	23	13	10	·	·	20	·
II	11.5	6.0	7	4.8	0.5	2.0	1	2.0	9	4.5	16.5	5.9	20.5	5.7	13	7.3	5	5.4	12	2.3	17	13	24	28	·	7	1	2	14	20	5	·	2	28	·
III	5.5	5.0	8.5	4.2	3.5	3.1	13.5	2.7	16.5	2.6	16.5	4.7	9	4.4	6	5.2	14	3.3	20	7.4	3	5	7	21	·	5	·	4	12	10	7	·	–	15	·
IV	5.5	4.0	18	5.8	21	4.5	11.5	2.6	5	1.8	9.5	3.7	7.5	4.5	6	4.2	6	3.9	41	8.9	23	·	·	7	·	5	·	3	12	15	10	·	·	·	1
V	14	3.4	11.5	3.7	9.5	3.7	4	3.1	3	3.5	12	5.7	13	3.5	18	3.9	8	3.6	96	18.2	18	·	·	3	·	2	·	·	13	16	14	4	2	·	2
VI	9	4.4	13	5.1	7	3.2	5	4.2	3	4.8	13.5	3.5	22	3.7	9.5	3.4	8	3.6	85	19.2	14	·	·	·	4	3	·	6	7	15	13	2	·	·	3
VII	3.5	2.7	6.5	3.5	5	3.7	4	3.0	14.5	3.0	28	3.5	19	3.9	0.5	3.0	12	3.0	66	12.9	17	·	·	·	6	1	·	3	6	14	10	2	1	·	3
VIII	4.5	2.9	2.5	2.2	4	2.4	14	2.3	8	3.1	11	2.8	18	3.6	14	3.2	17	2.4	95	19.0	25	·	·	·	9	·	·	11	5	16	14	3	1	·	·
IX	·	·	1.5	1.7	3	2.4	24	2.8	18	3.4	12	3.1	17.5	3.0	4	5.8	10	2.8	69	24.5	4	·	·	·	2	1	·	7	4	10	6	2	3	·	·
X	7.5	3.2	5.5	2.5	2.5	2.2	6	2.1	11.5	2.2	14.5	3.7	15.5	4.1	11	3.1	19	2.5	6	3.3	16	·	·	8	·	·	·	9	8	6	2	·	7	·	·
XI	4.5	4.8	17	5.1	4.5	2.6	9.5	4.2	12	3.6	18.5	4.8	14	4.1	3	2.7	7	4.0	29	6.7	3	7	9	20	·	1	·	2	21	19	8	·	6	15	·
XII	2.5	2.8	2.5	2.8	2.5	3.8	14	3.2	25	4.5	26	5.5	12	5.6	6.5	3.5	2	4.5	58	15.9	18	2	6	22	·	4	·	1	13	16	10	1	·	10	·
Rok	75.5	3.7	100	3.7	66.5	3.0	120	2.9	149	3.4	193	4.2	179	4.3	100	4.1	112	3.6	604	24.5	4.IX	29	55	134	21	35	1	49	138	170	109	14	–	88	9

Sulejów $H_s = 186$ m $h_w = 14$ m

I	4	3.5	7.5	2.9	4.5	2.6	17	3.8	20	3.9	15	4.7	11.5	4.6	6.5	3.6	7	3.6	27	4.1	24	1	8	27	·	3	·	2	19	16	9	·	4	19	·
II	13	4.7	4.5	3.9	2.5	3.0	1	2.0	6.5	3.0	13	6.9	27.5	5.7	12	4.8	4	4.9	11	4.4	17	11	24	28	·	4	·	1	12	17	4	·	1	28	·
III	1.5	5.0	8	3.0	2	4.0	18.5	3.5	14	2.9	16	4.5	11	5.1	10	3.6	12	3.3	26	6.7	26	5	7	21	·	3	·	4	10	11	7	·	5	15	·
IV	6	3.3	9	4.5	20	4.3	15.5	3.1	5.5	2.7	7	3.9	11	3.8	7	3.3	9	3.3	49	11.3	23	·	·	7	·	·	·	5	10	15	12	1	·	·	1
V	8.5	2.6	11.5	3.3	8.5	3.5	9	4.3	3	3.8	8.5	4.3	13	3.4	16	3.0	15	2.9	117	16.2	18	·	·	3	·	4	1	4	11	18	16	5	2	·	4
VI	6	3.8	10.5	3.6	7.5	3.8	4	3.1	6.5	3.9	10.5	4.5	23	3.4	10	2.6	12	3.1	96	22.8	14	·	·	·	4	1	1	7	7	13	12	2	·	·	2
VII	3	3.0	5	3.6	5	2.6	5.5	3.6	8	2.9	27	3.6	24.5	3.7	5	2.2	10	3.0	44	8.8	21	·	·	·	6	1	·	1	6	14	9	·	·	·	7
VIII	5.5	2.8	2	1.6	1	1.0	10.5	3.4	10.5	4.1	6.5	3.6	13.5	3.3	15.5	3.3	28	2.3	87	34.6	25	·	·	·	9	·	·	8	9	15	12	2	·	·	2
IX	·	·	·	·	3.5	2.1	21.5	4.1	14	4.2	21	2.9	16	3.2	4	4.0	10	3.1	72	36.6	4	·	·	·	2	·	·	8	7	12	9	2	1	·	·
X	6.5	2.7	5.5	2.1	8	2.0	4	2.6	6	2.1	13.5	3.5	17.5	4.7	14	2.6	18	2.5	7	3.6	16	·	·	7	·	·	·	9	8	7	2	·	6	·	·
XI	1	2.0	12	5.5	8	2.9	15	4.4	6	3.5	11.5	6.3	20.5	4.6	6	2.7	10	4.0	30	5.2	3	5	8	19	·	1	·	2	21	22	8	·	5	16	·
XII	2.5	1.8	1	3.0	2	2.5	14	4.0	18	5.5	27.5	5.6	17.5	4.8	4.5	2.4	6	4.5	42	13.8	18	2	5	23	·	3	·	2	14	17	11	1	2	10	·
Rok	57.5	2.9	76.5	3.1	72.5	2.9	135.5	3.5	118	3.5	177	4.5	206.5	4.2	110.5	3.2	141	3.4	608	36.6	4.IX	24	52	135	21	20	2	53	134	177	111	13	26	88	16

Szczerców — φ = 51°20' — λ = 19°07' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																		
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.5	−3.6	6.2	29	−9.3	11	−1.6²	1.0²	−1.4	−0.8²	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.0	8.1	8.5
II	–	–	–	–	−1.8	−9.7	3.0	13	−19.7	6	−6.9	−2.7²	−5.8	−5.3²	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.1	7.3	7.7
III	–	–	–	–	6.4	−3.2	16.0	30	−14.9	9	−1.4	5.9²	0.5	1.4²	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	6.9	7.2
IV	–	–	–	–	11.1	2.4	15.5	29	−1.5	1	4.7	10.6²	5.1	6.4²	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	7.9	7.5
V	–	–	–	–	15.0	5.6	24.0	17	−2.2	3	9.5	14.6²	9.1	10.6²	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	6.3	6.8
VI	–	–	–	–	21.9	10.7	34.0	26	6.6	16	15.6²	21.0²	13.8	16.0²	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.1	5.2	5.0
VII	–	–	–	–	22.2	11.5	31.2	14	6.6	4	16.0²	21.3²	14.9	16.8²	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	5.6	6.6
VIII	–	–	–	–	22.6	10.2	31.8	7	5.1	17	14.3²	21.9²	14.1	16.1²	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	6.1	5.8
IX	–	–	–	–	21.3	9.4	29.0	3	3.4	21	12.0	21.0²	12.9	14.7²	–	–	–	–	–	–	–	–	–	–	–	–	6.1	4.9	5.7	5.6
X	–	–	–	–	13.6	2.1	23.0	1	−6.0	22	4.4	13.3²	5.4	7.1²	–	–	–	–	–	–	–	–	–	–	–	–	7.9	5.8	5.5	6.4
XI	–	–	–	–	2.6	−3.4	13.5	2	−17.0	18	−1.7	1.7²	−0.6	−0.3²	–	–	–	–	–	–	–	–	–	–	–	–	9.7	8.7	8.5	9.0
XII	–	–	–	–	3.1	−1.4	10.5	20	−13.5	16	0.3	2.2²	0.7	1.0²	–	–	–	–	–	–	–	–	–	–	–	–	9.6	8.4	9.1	9.0
Rok	–	–	–	–	11.6	2.6	34.0	26.VI	−19.7	6.II	5.4²	11.0²	5.7	7.0²	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.8	6.8	7.1

Oborniki Śl. — φ = 51°18' — λ = 16°55'

I	–	–	–	–	3.1	−1.1	6.5	18	−6.1	7	−0.3	1.9	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.0	7.0	6.6
II	–	–	–	–	−1.0	−7.3	3.7	13	−15.1	6	−5.1	−2.4	−4.3	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	7.4	7.7
III	–	–	–	–	6.9	−2.8	16.7	30	−16.9	9	−0.9	5.4	1.2	1.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	11.8	3.3	17.8	4	−1.9	1	5.3	10.6	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.6	5.4	6.1
V	–	–	–	–	15.1	6.4	23.9	17	−1.1	2	9.1	13.4	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	6.0	6.5
VI	–	–	–	–	21.4	11.2	31.5	26	4.7	3	14.8	19.4	14.8	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.4	4.5	5.6
VII	–	–	–	–	21.5	11.9	31.2	14	6.0	10	15.1	19.4	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.5	5.1	6.9
VIII	–	–	–	–	21.9	10.8	31.4	7	5.8	31	13.4	20.2	14.2	15.5	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.5	3.2	4.5
IX	–	–	–	–	20.6	9.7	27.4	2	4.4	22	11.8	18.9	13.2	14.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.1	3.5	4.5
X	–	–	–	–	14.0	3.5	22.9	1	−3.9	23	4.8	12.5	6.3	7.5	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.4	3.2	4.3
XI	–	–	–	–	3.9	−2.6	13.9	2	−11.4	24	−1.2	2.1	−0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	7.6	7.6
XII	–	–	–	–	4.2	−0.7	12.0	20	−6.1	14, 15	0.5	2.4	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	6.9	7.1
Rok	–	–	–	–	12.0	3.5	31.5	26.VI	−16.9	9, III	5.6	10.3	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Bolesławiec — φ = 51°16' — λ = 15°35'

I	–	–	–	–	3.4	−1.4	8.8	17	−8.5	7	0.0	2.2	0.7	0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.1	8.2	8.0
II	–	–	–	–	−0.6	−6.5	4.2	13	−18.7	6	−4.2	−2.2	−3.4	−3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	7.6	8.3
III	–	–	–	–	6.5	−2.9	16.5	30	−14.1	9	−1.2	4.9	0.7	1.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.7	5.9	6.4
IV	–	–	–	–	11.2	3.0	17.6	3	−1.2	1	4.8	9.4	6.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	5.8	6.9
V	–	–	–	–	15.0	6.7	23.1	17	0.0	3	9.2	13.4	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	6.3	7.0
VI	–	–	–	–	20.7	11.1	30.5	26	6.8	2, 4, 13	14.4	18.6	15.1	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.3	5.7	6.3
VII	–	–	–	–	20.9	12.2	31.6	14	7.2	10	15.0	19.0	15.1	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	6.1	7.0
VIII	–	–	–	–	21.3	10.3	30.6	6	5.6	14	13.5	19.8	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.8	4.6	5.7
IX	–	–	–	–	19.5	9.2	25.5	2	4.3	21	11.4	17.9	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.2	3.7	5.0
X	–	–	–	–	13.3	3.3	21.4	1	−4.1	23	4.7	12.2	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.8	4.1	4.6
XI	–	–	–	–	3.6	−2.3	14.5	1	−11.4	23	0.0	2.0	0.0	0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.7	7.3	8.2
XII	–	–	–	–	5.0	0.0	12.3	19	−6.7	14	1.5	3.0	2.4	2.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.4	8.8	8.5
Rok	–	–	–	–	11.6	3.6	31.6	14.VII	−18.7	6.II	5.8	10.0	6.8	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	6.2	6.8

Nałęczów — φ = 51°17' — λ = 22°13'

I	–	–	–	–	0.6	−4.6	4.7	30	−16.7	11	−2.9	−0.5	−2.3	−2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.6	7.5	7.7
II	–	–	–	–	−3.1	−11.6	1.4	14	−26.8	24	−8.3	−4.4	−7.6	−7.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.5	7.1	7.7
III	–	–	–	–	5.3	−4.1	16.5	30	−19.7	1	−2.4	3.9	−0.1	0.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	3.9	5.5
IV	–	–	–	–	11.3	2.1	16.8	7	−2.4	3	3.8	9.3	5.6	6.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.9	7.1	7.7
V	–	–	–	–	15.2	5.5	25.5	19	−4.0	4	8.9	13.5	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.5	6.9	7.1
VI	–	–	–	–	21.1	10.7	29.3	26	4.5	8	14.4	19.5	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.0	6.8	6.6
VII	–	–	–	–	22.1	10.6	29.9	16	5.0	5	15.7	20.5	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	7.0	6.4	6.2
VIII	–	–	–	–	21.1	10.1	30.3	8	3.7	16	12.8	19.6	13.7	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.4	4.1	4.9
IX	–	–	–	–	21.4	8.8	27.1	2	1.8	16	11.4	20.0	12.7	14.2	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.8	2.0	4.1
X	–	–	–	–	12.8	2.0	22.9	1	−6.2	22	4.0	11.8	5.8	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.9	3.3	5.0
XI	–	–	–	–	1.8	−4.2	13.0	2	−20.1	18	−2.2	0.5	−1.7	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.8	8.4	8.7
XII	–	–	–	–	2.1	−2.7	7.6	20	−21.0	17	−1.0	0.9	−0.6	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.5	7.3	7.9
Rok	–	–	–	–	11.0	1.9	30.3	8.VIII	−26.8	24.II	4.5	9.6	5.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.1	5.9	6.6

Szczerców $H_s = 160\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD}																		OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	◕	Opad R			≡	⊠	K (K)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15			R≥0.1	R≥1.0	R≥10.0			
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40	7.4	24	·	7	27	·	—	—	·	19	14	12	·	6	27	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	32	7.6	7	11	21	28	·	—	—	·	18	15	9	·	2	28	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	21	4.4	1	4	4	20	·	—	—	2	16	12	9	·	3	13	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	58	17.0	23	·	·	6	·	—	—	1	16	12	9	2	·	·	1
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	101	18.0	16	·	·	3	·	—	—	1	12	18	15	4	·	·	5
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	48	9.3	11	·	·	·	6	—	—	10	7	14	13	·	·	·	2
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	54	14.6	8	·	·	·	8	—	—	3	12	15	11	1	·	·	4
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	53	17.5	24	·	·	·	10	—	—	5	8	9	9	1	·	·	2
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	84	50.0	4	·	·	·	3	—	—	4	7	8	8	2	2	·	·
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	6	5.1	16	·	·	11	·	—	—	4	13	5	1	·	10	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	43	7.3	15	5	8	19	·	—	—	·	23	16	10	·	8	16	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	56	20.5	18	2	3	18	·	—	—	·	26	12	10	1	1	13	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	596	50.0	4.IX	22	43	132	27	—	—	30	177	150	116	11	32	97	14

Oborniki Śl. $H_s = 180\ m$ $h_w = 12{,}4\ m$

I	12	1.5	4	1.7	2	1.0	19	1.7	11.5	2.6	19.5	1.7	9.5	2.7	10.5	1.9	5	1.8	28	5.0	9	·	1	26	·	·	·	2	15	19	9	·	2	—	·
II	13	1.6	4	1.5	5	1.6	·	·	0.5	2.0	7.5	2.0	14	2.6	26	2.3	14	1.7	34	7.2	17	8	19	28	·	3	·	1	16	23	12	·	·	28	·
III	14.5	1.7	9.5	1.8	7.5	1.7	4.5	1.6	9.6	2.1	8.5	1.6	9.5	2.8	13.5	1.9	16	1.6	29	8.9	28	3	4	19	·	·	·	—	—	12	8	·	3	16	·
IV	8.5	2.0	10	1.8	7.5	2.7	7	2.2	5.5	3.1	7	1.7	12.5	2.0	16	2.0	16	1.7	70	17.2	19	·	·	3	·	·	·	6	14	17	14	2	—	·	2
V	15.5	2.4	11.5	2.0	5.5	1.4	2.5	1.6	1.5	2.0	4	2.5	11	1.9	19.5	1.9	22	1.5	196	28.7	28	·	·	1	·	1	1	5	14	23	20	9	2	·	4
VI	7	1.5	13	1.7	6.5	1.5	4	1.9	5.5	1.6	13	2.1	13	2.2	14	2.1	14	1.6	78	19.1	11	·	·	·	6	·	·	1	7	18	17	2	·	·	7
VII	6	1.9	6.5	1.5	4.5	2.2	1.5	2.0	6	1.5	21	1.7	24.5	2.1	9	2.1	14	1.6	85	12.8	17	·	·	·	4	·	·	·	9	17	14	3	·	·	7
VIII	10	1.8	4.5	1.6	4.5	1.3	4.5	2.7	10	2.2	9	1.4	10.5	2.0	21	1.7	19	1.5	40	9.3	24	·	·	·	8	·	·	6	3	17	9	·	·	·	2
IX	·	·	·	·	1.5	2.3	14	2.8	14	1.7	19.5	2.1	18	1.7	9	1.8	14	1.7	31	11.4	10	·	·	·	2	·	·	8	6	9	5	1	—	·	1
X	13	1.3	5.5	1.6	17	1.7	6	1.8	4	1.2	6	1.1	7	1.6	10.5	1.8	24	1.2	5	2.6	16	·	·	7	·	·	·	7	6	4	2	·	—	·	·
XI	5.5	1.5	9.5	1.5	11	3.9	6.5	2.1	4.5	2.3	10.5	1.9	11	2.1	16.5	1.8	15	1.8	29	5.6	27	3	9	21	·	1	·	3	19	16	10	·	2	15	·
XII	11.5	1.6	0.5	1.0	4	2.0	10	1.8	14	2.2	14	2.1	7.5	2.8	9.5	1.9	22	1.6	53	13.9	18	·	·	17	·	·	·	2	10	20	10	1	2	—	·
Rok	116.5	1.6	78.5	1.5	76.5	1.9	79.5	1.8	86.5	2.0	139.5	1.8	148	2.2	175	1.9	195	1.6	678	28.7	28.V	14	33	122	20	5	1	—	—	195	130	18	—	—	23

Bolesławiec $H_s = 208\ m$ $h_w = 12{,}6\ m$

I	2.5	2.6	3.5	1.6	4	1.0	3.5	1.0	3.5	2.4	16	2.6	18	2.6	4	1.0	38	1.3	30	7.8	9	·	·	24	·	·	·	2	20	13	9	·	5	6	·
II	17	2.4	6.5	2.8	5.5	1.4	4	2.0	·	·	13	3.3	14.5	3.2	17.5	2.6	6	2.5	43	5.6	17	5	21	27	·	·	·	1	19	23	13	·	·	26	·
III	7	1.9	8.5	2.3	3	1.3	3	1.3	4	1.2	12.5	1.5	18.5	2.9	11.5	1.9	25	1.5	28	8.2	2	4	6	19	·	·	·	4	11	13	6	·	2	16	·
IV	6.5	1.6	5.5	2.5	10	2.3	11.5	2.1	3	1.3	9.5	1.6	14	1.9	9	2.6	21	1.6	53	11.7	20	·	·	1	·	·	·	4	16	19	13	1	·	·	·
V	13	2.0	5.5	1.7	10	2.3	9.5	2.5	1	3.0	10.5	2.4	15	3.0	13.5	2.3	15	2.0	138	25.5	29	·	·	·	·	2	·	4	15	21	17	5	2	·	3
VI	9	1.9	10	1.8	3.5	1.3	5.5	2.6	2.5	1.4	7	1.6	18	2.9	12.5	2.7	22	1.7	90	30.2	11	·	·	·	6	·	·	4	11	16	12	2	·	·	7
VII	6	1.4	3	1.7	1.5	2.3	1.5	2.3	4	1.7	11	2.5	36.5	2.1	7.5	2.3	22	1.8	63	12.9	16	·	·	·	3	1	·	2	15	19	10	1	2	·	5
VIII	6.5	1.5	5.5	1.0	2	2.5	2	2.0	4	2.0	10	1.5	18.5	1.9	11.5	1.9	33	1.1	91	32.0	24	·	·	·	8	·	·	2	5	14	9	2	5	·	3
IX	0.5	1.0	4.5	1.4	8	2.4	4.5	4.0	2.5	3.4	8	1.4	22	1.8	12	1.5	28	1.4	78	25.8	3	·	·	·	2	·	·	5	7	9	7	4	1	·	2
X	7	1.6	8	2.0	14	2.6	3	3.3	2	1.0	7.5	2.3	16.5	2.4	6	2.3	29	1.6	8	5.0	16	·	·	7	·	·	·	8	8	5	2	·	8	·	·
XI	2.5	1.8	16	1.8	9	2.0	3	3.3	·	·	14.5	4.4	26.5	3.3	3.5	2.1	15	2.4	28	7.0	27	1	10	20	·	3	1	·	18	16	6	·	3	13	·
XII	0.5	3.0	·	·	8	1.2	3	1.7	5.5	3.3	24	3.3	23.5	3.1	4.5	2.1	24	2.1	53	8.5	18	·	·	15	·	2	·	·	20	23	13	·	4	2	·
Rok	78	1.9	76.5	1.7	78.5	1.9	54	2.3	32	1.7	143.5	2.4	241.5	2.6	113	2.1	278	1.8	703	32.0	24.VIII	10	37	113	19	8	1	36	165	191	117	15	32	63	20

Nałęczów $H_s = 166\ m$ $h_w = 15\ m$

I	6	2.7	·	·	9.5	3.2	14.5	2.3	22	3.8	11	3.8	8.5	5.7	4.5	7.2	17	3.1	41	9.6	17	2	9	27	·	3	·	3	18	18	11	·	5	31	·
II	7.5	3.3	8.5	2.4	1.5	4.0	·	·	4	7.8	9	6.2	20.5	4.6	17	4.7	16	3.7	37	6.9	8	14	23	28	·	1	·	1	16	21	13	·	2	28	·
III	2.5	3.2	4	2.1	4	2.1	6	2.6	26	2.2	11	3.5	8	3.2	7.5	3.2	24	2.0	21	6.8	21	7	6	21	·	·	·	4	8	9	7	·	4	17	·
IV	7	3.6	2	5.8	37	4.8	7.5	3.7	9.5	2.8	9.5	4.0	3	4.0	1.5	3.0	13	3.6	41	9.3	28	·	·	10	·	·	·	·	17	12	10	·	2	·	3
V	10	2.4	11.5	1.7	11.5	3.6	3.5	1.6	8	2.9	12.5	3.2	6.5	2.0	11.5	3.1	18	2.5	57	9.7	10	·	·	4	1	1	1	·	11	16	12	·	·	·	4
VI	5	1.4	11	2.3	12.5	2.2	3	3.2	10	2.8	7.5	3.3	16	2.5	9	2.7	16	2.1	76	16.1	9	·	·	·	6	·	·	2	10	14	13	1	·	·	2
VII	1.5	1.3	·	·	8.5	2.2	4	2.1	12.5	2.8	11.5	3.0	24.5	3.0	5.5	1.5	25	1.9	53	15.5	18	·	·	·	7	·	·	4	9	17	14	1	·	·	6
VIII	9.5	3.1	0.5	5.0	0.5	2.0	9.5	1.9	8.5	3.2	3.5	4.4	9.5	1.6	22.5	3.7	29	2.1	88	22.5	2	·	·	·	9	·	·	8	7	12	9	4	·	·	2
IX	·	·	·	·	1.5	2.3	18	2.4	21	3.1	12.5	3.2	4.5	4.3	8.5	1.9	24	2.1	51	25.6	29	·	·	·	3	·	·	6	2	7	4	2	1	·	3
X	8	2.0	3.5	1.3	3.5	1.9	1.5	1.3	9.5	1.6	11	2.9	14	2.9	13	2.3	29	1.6	11	3.7	11	·	·	8	·	·	·	6	8	7	5	·	4	·	·
XI	·	·	16	2.6	6	1.8	9	3.7	10.5	3.7	13.5	4.1	13.5	3.3	2.5	2.0	19	2.6	50	6.9	11	5	11	20	·	·	·	·	21	20	15	·	4	17	·
XII	3	1.3	1	1.0	1	3.0	8	3.1	30.5	4.0	24.5	3.4	10.5	2.7	4.5	2.3	10	3.0	31	10.7	18	2	3	23	·	·	·	2	18	14	7	1	2	6	·
Rok	60	2.0	58	2.0	97	2.8	84.5	2.3	172	3.4	137	3.8	139	3.7	107.5	3.1	240	2.5	557	25.6	29.IX	30	52	141	26	5	1	36	145	167	120	9	24	99	20

Motycz

$\varphi = 51°15'$ $\lambda = 22°25'$ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.2	−5.3	4.0	30	−18.2	11	−3.3	−1.1	−2.5	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−4.0	−11.0	0.6	14	−23.5	24	−8.2	−5.3	−7.4	−7.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	3.9	−3.2	14.6	30	−16.2	1	−1.7	3.1	0.3	0.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	9.9	2.1	15.4	7	−1.8	3	3.6	8.5	5.4	5.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	14.4	5.8	26.0	19	−2.4	4	8.7	13.1	9.4	10.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	20.2	10.9	28.4	26	5.2	8	14.5	18.8	14.7	15.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.4	11.1	28.0	16	5.9	12	15.6	19.8	15.2	16.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	20.3	10.3	29.2	8	4.5	16	13.3	18.7	13.5	14.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	20.6	9.1	26.3	2	3.8	21	11.9	19.2	13.2	14.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	11.8	2.6	21.6	1	−5.8	22	4.2	11.0	6.1	6.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	1.0	−4.4	12.3	2	−22.6	18	−2.0	−0.3	−1.9	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	1.6	−2.5	7.6	20	−19.7	17	−0.9	0.6	−0.5	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	10.1	2.1	29.2	8.VIII	−23.5	24.II	4.6	8.8	5.5	6.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Lublin

$\varphi = 51°14°$ $\lambda = 22°34'$

I	991.1	1007.5	968.8	1013.4	0.7	−4.6	5.7	30	−15.4	11	−2.6	−0.4	−1.9	−1.7	4.7	5.0	4.8	4.8	90	83	88	87	0.5	1.0	0.7	0.7	7.8	7.7	7.5	7.7
II	992.8	1010.2	968.5	1015.4	−3.1	−10.6	1.2	14	−24.6	24	−7.8	−4.4	−6.8	−6.4	3.3	3.5	3.3	3.4	89	77	84	83	0.4	1.0	0.6	0.7	8.5	7.9	7.5	8.0
III	995.8	1011.9	968.2	1018.1	5.2	−3.6	16.1	30	−21.7	1	−1.9	4.1	0.6	0.8	5.1	5.7	5.5	5.4	91	68	83	81	0.5	2.9	1.1	1.5	6.5	6.5	4.7	5.9
IV	990.2	1005.8	972.0	1011.9	11.1	2.3	16.8	18	−3.0	3	3.7	9.4	6.0	6.3	7.1	7.2	7.5	7.3	87	61	78	75	1.0	5.0	2.0	2.7	7.9	8.0	5.7	7.2
V	992.4	1008.6	980.6	1013.7	15.4	5.8	27.4	19	−3.8	4	8.8	13.7	10.3	10.8	9.7	9.4	10.5	9.9	83	59	81	74	1.9	6.9	2.4	3.7	7.1	8.0	6.4	7.2
VI	993.0	1000.0	981.6	1013.9	21.4	11.0	29.9	26	4.3	8	14.5	19.6	15.8	16.4	14.0	13.8	14.6	14.1	84	63	82	76	2.8	9.9	3.7	5.5	5.6	6.9	5.8	6.1
VII	991.8	1001.5	980.1	1012.7	22.4	11.1	29.8	17	5.3	5, 12	15.0	20.9	16.0	17.0	14.8	13.9	15.2	14.6	86	56	83	75	2.4	11.5	3.3	5.7	4.9	7.8	6.1	6.3
VIII	994.5	1003.0	980.6	1015.6	21.6	10.0	30.8	8	4.3	16	12.6	19.9	14.3	15.3	13.2	13.8	14.1	13.7	90	61	86	79	1.6	10.5	2.7	4.9	5.2	6.3	3.9	5.1
IX	995.5	1012.2	985.0	1016.7	21.8	7.9	28.2	2	1.3	17	10.3	20.5	13.1	14.2	11.9	13.6	13.5	13.0	93	57	88	79	1.0	11.1	1.9	4.7	4.8	5.6	2.1	4.2
X	1001.2	1016.1	989.2	1023.1	12.5	1.9	21.7	1	−6.1	22	4.0	11.7	5.7	6.8	7.8	8.8	8.5	8.4	94	63	90	82	0.5	5.4	1.0	2.3	5.8	5.6	3.9	5.1
XI	991.1	1007.5	965.8	1013.3	1.8	−3.9	13.4	2	−20.6	18	−1.8	0.3	−1.1	−0.9	5.2	5.5	5.4	5.4	92	83	88	88	0.5	1.2	0.7	0.8	8.8	8.9	8.3	8.8
XII	986.3	1000.8	966.7	1008.3	2.1	−2.2	7.6	20	−20.8	17	−0.6	1.3	0.1	0.2	5.3	5.5	5.3	5.4	87	80	85	84	0.8	1.4	1.0	1.1	8.7	8.1	7.7	8.2
Rok	993.0	1016.1	965.8	1014.7	11.1	2.1	30.8	8.VIII	−24.6	24.II	4.5	9.7	6.0	6.6	8.5	8.8	9.0	8.8	89	68	85	81	1.2	5.6	1.8	2.9	6.8	7.3	5.8	6.6

Felin

$\varphi = 51°14'$ $\lambda = 22°38'$

I	—	—	—	—	−0.3	−4.9	3.2	30	−17.0	11	−3.2	−1.4	−2.4	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.5	7.3	7.6
II	—	—	—	—	−4.0	−10.6	0.7	14	−21.7	7, 24	−7.9	−5.3	−7.2	−6.9	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.4	7.2	7.7
III	—	—	—	—	3.8	−3.6	14.9	30	−17.2	1	−2.2	2.6	0.0	0.1	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.3	4.5	5.8
IV	—	—	—	—	10.1	2.2	16.1	18	−2.0	3	3.4	8.5	5.6	5.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.8	6.0	7.3
V	—	—	—	—	14.5	5.9	25.3	19	−1.6	4	8.3	12.8	9.8	10.2	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.7	6.0	6.8
VI	—	—	—	—	20.1	11.2	28.0	26	7.8	3, 8	14.2	18.5	15.2	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.3	7.0	5.4	5.9
VII	—	—	—	—	21.2	11.2	28.3	16	5.9	5	14.9	19.7	15.3	16.3	—	—	—	—	—	—	—	—	—	—	—	—	4.8	7.2	5.8	5.9
VIII	—	—	—	—	20.3	10.4	28.7	8	4.7	16	12.9	18.8	14.3	15.1	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.0	3.7	5.0
IX	—	—	—	—	20.3	9.3	26.3	2	3.2	21	11.6	19.2	13.5	14.4	—	—	—	—	—	—	—	—	—	—	—	—	4.5	4.9	1.9	3.8
X	—	—	—	—	11.7	2.7	21.4	1	−5.5	22	4.3	10.8	6.4	7.0	—	—	—	—	—	—	—	—	—	—	—	—	5.6	5.0	3.3	4.6
XI	—	—	—	—	1.0	−4.3	13.1	2	−19.7	17	−2.3	−0.4	−1.5	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.9	8.6	8.7
XII	—	—	—	—	1.6	−2.5	7.3	20	−17.9	17	−1.0	0.6	−0.4	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.1	7.5	8.1
Rok	—	—	—	—	10.0	2.2	28.7	8.VIII	−21.7	7,24.II	4.4	8.7	5.7	6.1	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.0	5.6	6.5

Legnica

$\varphi = 51°13'$ $\lambda = 16°10'$

I	996.0	1011.5	975.5	1011.8	3.9	−0.7	9.0	17	−6.5	7	0.6	2.5	1.2	1.4	5.7	6.0	5.8	5.8	89	82	87	86	0.7	1.5	0.9	1.0	7.3	7.9	7.9	7.7
II	1002.5	1017.2	977.6	1018.5	0.0	−5.9	6.5	13	−17.6	6	−3.7	−1.9	−2.9	−2.8	4.1	4.1	4.3	4.2	86	77	84	82	0.7	1.3	0.8	0.9	8.5	7.5	7.1	7.7
III	1001.4	1017.3	974.7	1017.2	7.1	−2.7	17.4	30	−18.6	9	−1.1	5.7	1.6	2.0	5.3	6.1	6.0	5.8	87	64	82	78	0.8	3.8	1.3	2.0	7.0	6.4	6.1	6.5
IV	995.3	1016.6	979.1	1010.7	12.0	3.8	17.9	4	−0.7	8	5.0	10.5	7.3	7.5	7.7	8.2	8.2	8.0	88	66	80	78	1.1	4.7	2.1	2.6	7.5	7.6	7.0	7.4
V	998.8	1013.2	987.0	1014.0	15.7	7.4	24.4	17	−0.1	3	9.4	13.8	10.8	11.2	10.6	10.9	11.0	10.8	87	69	83	80	1.4	5.2	2.2	2.9	7.8	8.1	7.1	7.7
VI	999.3	1010.5	986.3	1014.3	21.6	11.5	32.6	26	5.9	3	14.7	19.8	15.7	16.5	14.3	14.3	14.9	14.5	85	63	83	77	2.6	9.5	3.3	5.1	6.1	7.5	5.8	6.5
VII	997.3	1005.0	984.6	1012.3	21.8	12.5	31.0	14	7.9	10	15.4	19.5	15.7	16.6	14.6	15.0	15.1	14.9	82	66	83	77	3.2	8.4	3.0	4.9	7.8	8.2	6.5	7.5
VIII	1000.9	1009.2	987.2	1015.9	22.3	10.5	31.7	6	4.7	16	13.3	20.7	15.2	16.1	13.5	13.2	14.2	13.6	88	55	82	75	2.0	12.1	3.3	5.8	4.5	6.1	4.2	4.9
IX	999.1	1020.2	984.8	1014.2	20.7	9.6	26.5	2, 3	3.4	21	11.2	19.4	13.3	14.3	12.2	13.3	13.3	12.9	91	59	86	79	1.4	9.7	2.3	4.5	5.2	6.0	3.6	4.9
X	1008.2	1021.5	996.7	1023.8	14.1	2.4	22.1	1	−5.5	23	3.9	12.7	6.1	7.2	7.9	10.0	8.9	8.9	95	67	91	84	0.5	5.2	0.9	2.2	6.0	6.0	3.6	5.2
XI	996.1	1017.3	966.8	1012.0	4.3	−1.9	15.5	1	−12.0	24	0.2	2.6	0.6	1.0	5.5	5.8	5.6	5.6	85	76	83	81	1.1	2.0	1.2	1.4	7.9	8.7	8.0	8.2
XII	990.4	1011.6	966.8	1006.1	5.4	0.2	14.0	19	−5.7	14	1.8	3.6	2.6	2.6	5.8	6.0	6.1	6.0	82	76	82	80	1.3	2.1	1.5	1.6	8.0	7.6	7.4	7.7
Rok	998.8	1021.5	966.8	1014.2	12.4	3.9	32.6	26.VI	−18.6	9.III	5.9	10.7	7.3	7.8	8.9	9.4	9.4	9.2	87	68	84	80	1.4	5.5	1.9	2.9	7.0	7.3	6.2	6.8

Motycz

$H_s = 213$ m $h_w = 14$ m **1965**

MIESIĄC	ROZKŁAD WIATRU #D,VmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	⊠
I	4.5	6.0	12.6	2.5	9.5	4.5	13	3.7	11	5.3	23	4.3	11	4.7	6.5	8.5	2	4.4	28	8.3	17	2	15	27	·	5	·	–	–	14	7	·	4	31	·
II	10	5.2	9	6.6	3	7.0	·	·	1.5	5.7	18	5.5	22.5	5.4	18	5.9	2	5.6	20	4.2	27	13	24	28	·	2	·	–	–	18	8	·	3	28	/
III	3.5	4.4	3.5	5.7	8	5.2	6.5	4.4	16.5	4.1	21	2.9	15	3.9	11	4.8	8	3.7	20	6.2	21	3	8	20	·	2	·	–	–	10	5	·	4	17	·
IV	7	4.9	3	5.8	20.5	8.1	28	6.3	4.5	4.2	9.5	4.3	5.5	5.1	5	4.6	7	5.6	45	9.4	17	·	·	10	·	8	·	–	–	10	8	·	3	·	1
V	10.5	4.8	7	3.3	10.5	5.8	12	4.5	3	5.0	7.5	3.7	18	4.3	18.5	3.8	6	4.1	55	20.8	29	·	·	2	1	4	·	–	–	16	10	1	·	·	6
VI	6.5	3.9	4.5	4.8	11.5	5.1	9	5.1	3	3.5	8.5	3.6	17.5	3.7	21.5	4.2	8	3.9	102	19.5	10	·	·	·	5	1	·	–	–	14	10	5	·	·	5
VII	2	2.5	2.5	2.4	8.5	3.9	7.5	3.7	9.5	2.8	14	3.8	30.5	3.8	8.5	4.5	10	3.3	60	16.3	18	·	·	·	4	·	·	–	–	19	10	2	·	·	6
VIII	8	4.7	2	7.0	·	·	9.5	3.8	7	2.9	18	3.3	18	3.1	22.5	5.0	8	3.6	78	22.2	2	·	·	·	6	1	·	–	–	12	8	3	·	·	6
IX	2	2.0	·	·	2.5	3.8	18.5	3.9	20.5	4.0	20.5	3.4	14	3.6	9	3.7	3	3.6	39	17.3	11	·	·	·	2	1	·	–	–	7	4	2	·	·	1
X	7.5	3.3	2.5	3.2	4.5	4.0	5.5	2.7	0.5	5.0	17.5	3.7	28.5	4.5	16.5	3.9	10	3.5	6	4.5	11	·	·	6	·	·	·	–	–	5	2	·	5	·	·
XI	5	2.8	7	6.4	9	6.0	16.5	3.8	9.5	4.8	16.5	4.6	17.5	4.7	6	3.0	3	4.4	30	3.4	12	6	11	22	·	4	·	–	–	19	10	·	5	18	2
XII	2	3.5	0.5	5.0	3	3.3	9.5	4.2	17	5.4	27.5	5.1	24.5	3.8	7	4.3	2	4.5	21	10.5	16	2	7	21	·	4	·	–	–	13	4	1	2	12	·
Rok	68.5	4.0	54	4.4	90.5	4.7	135.5	3.8	103.5	4.4	201.5	4.0	222.5	4.2	150	4.7	69	4.2	504	22.2	2.VIII	26	65	136	18	32	·	–	–	157	86	14	26	106	26

Lublin

$H_s = 171$ m $H_b = 176.7$ m $h_w = 10$ m

I	6.5	3.3	5.5	3.8	12.5	3.4	11.5	3.4	17.5	4.1	23	4.2	7	5.6	4.5	3.4	5	3.7	47	14.7	17	2	9	25	·	1	·	2	18	17	11	1	7	31	·
II	12.5	4.9	7	4.6	2.5	3.6	0.5	2.0	5.5	4.5	19	5.3	26	4.5	7	4.1	4	4.5	40	7.8	8	14	23	28	·	3	·	2	19	24	15	·	2	28	·
III	0.5	4.0	9.5	3.7	3	2.2	14	2.8	20	2.9	15	4.1	11.5	3.4	6.5	5.3	13	3.0	23	7.7	17	2	4	25	·	·	·	6	11	12	6	·	7	15	·
IV	3	3.7	7.5	3.8	3.2	5.2	19.5	3.6	4	3.0	9	4.4	7	3.1	7	5.4	1	4.3	48	13.3	28	·	·	8	·	·	·	·	11	13	8	2	4	·	1
V	10.5	2.9	10.5	3.9	11	4.0	6	3.2	6.5	3.5	13.5	4.5	11	3.5	21	3.5	3	3.6	50	9.7	29	·	·	3	1	1	1	1	14	18	12	·	2	·	6
VI	9.5	2.9	4.5	4.7	10	5.4	6.5	3.4	5	5.5	19.5	3.3	13.5	3.8	16.5	2.7	5	3.5	78	18.0	10	·	·	·	7	1	·	4	10	13	11	2	·	·	4
VII	1.5	2.3	5	2.2	6.5	3.3	5	3.1	13	2.8	30.5	3.4	9.5	3.1	6	1.5	16	2.5	63	23.9	18	·	·	·	9	·	·	2	7	17	12	1	3	·	6
VIII	7	3.9	1	7.0	1.5	2.7	7	2.7	10.5	2.3	13.5	3.0	22	3.3	9.5	3.4	21	2.4	86	27.2	2	·	·	·	9	·	·	5	8	11	9	3	1	·	1
IX	·	·	·	·	5	2.4	11	3.4	21	3.0	16.5	3.4	9	3.4	4.5	1.9	24	2.3	52	14.8	14	·	·	·	8	·	·	8	3	8	4	3	2	·	3
X	3.5	2.7	4.5	1.9	5	2.2	1	5.0	3	3.3	20	2.8	17.5	2.8	16.5	2.8	22	2.1	7	3.8	11	·	·	10	·	·	·	6	7	7	3	·	10	·	·
XI	3.5	2.7	13	4.5	9	2.6	12	3.2	14	3.7	16.5	4.1	15.5	3.9	4.5	1.4	2	3.5	53	8.6	11	4	10	19	·	·	·	·	22	23	14	·	7	19	1
XII	5	2.4	1	4.0	2.5	2.4	9	3.2	20	5.2	38.5	4.3	10	3.0	5	3.5	2	4.0	26	8.2	18	2	5	22	·	·	·	·	19	19	7	·	1	5	·
Rok	63	3.0	69	3.7	100.5	3.3	103	3.2	140	3.6	234.5	3.9	158.5	3.6	108.5	3.2	118	3.3	573	27.2	2.VIII	24	51	140	34	6	1	36	149	182	112	12	46	98	22

Felin

$H_s = 215$ m $h_w = 13$ m

I	9.5	3.9	3	5.3	5.5	4.8	19.5	5.1	18	6.2	19.5	5.2	6.5	5.6	7.5	7.5	4	5.2	25	9.3	17	2	13	28	·	6	·	3	18	13	4	·	6	31	–
II	12	5.8	9	6.3	1	6.0	·	·	5.5	9.0	16.5	7.7	21	5.0	17	4.6	2	5.8	52	7.8	27	15	25	28	·	4	1	2	16	20	13	·	4	28	–
III	1	4.5	7	4.9	2.5	4.2	12.5	3.7	19	6.0	21	4.2	11.5	4.1	8.5	6.0	10	4.0	19	6.9	17	6	7	20	·	2	·	5	9	10	5	·	7	16	–
IV	5.5	6.0	5.5	6.7	25	6.2	25.5	6.5	6	5.9	6.5	5.3	5.5	4.5	7.5	4.6	3	5.8	51	12.2	28	·	·	8	·	7	·	·	12	11	7	2	4	·	–
V	10	4.0	8.5	3.1	12	5.3	4	3.9	3.5	6.4	9.5	4.6	8	3.9	23.5	3.7	14	3.5	57	11.0	29	·	·	2	1	2	·	1	11	16	11	1	2	·	–
VI	7	3.4	7.5	5.0	9	4.9	8	2.6	7	4.7	5.5	4.1	23.5	3.9	14.5	3.4	8	3.6	88	19.7	10	·	·	·	4	1	·	2	11	13	12	3	1	·	–
VII	5.5	1.9	6.5	2.5	6.5	4.0	6	3.5	5	6.1	22.5	4.5	23.5	3.7	7.5	2.5	10	3.3	76	22.5	18	·	·	·	4	·	·	2	7	16	13	2	·	·	–
VIII	12	4.3	1.5	1.7	·	·	12	2.8	7	2.9	11	3.9	21	3.2	18.5	3.8	10	3.1	84	26.1	2	·	·	·	6	1	·	5	7	11	8	2	·	·	–
IX	·	·	·	·	1.5	3.0	24.5	3.9	20	3.6	19.5	4.4	10.5	2.8	10	2.9	4	3.5	52	17.6	11	·	·	·	2	1	·	8	2	6	4	4	2	·	–
X	9.5	3.6	3	3.2	3.5	4.1	3	5.0	5	4.2	20.5	4.0	20	4.0	20.5	3.0	8	3.4	4	1.8	18	·	·	5	·	·	·	9	5	5	1	·	4	·	–
XI	1.5	3.3	12	6.2	8.5	4.5	7.5	4.1	13	5.8	12.5	5.7	17	5.4	11	2.6	7	4.6	29	3.5	21	5	11	22	·	2	1	·	20	20	11	·	8	16	–
XII	4.5	3.0	0.5	5.0	2.5	4.0	9.5	5.2	18	7.5	32.5	6.6	18.5	3.8	6	3.8	1	5.6	19	7.3	18	2	7	21	·	7	1	·	17	17	5	·	2	6	–
Rok	78	3.6	64	4.2	77.5	4.2	132	3.9	127	5.6	197	5.0	186.5	4.2	152	4.0	81	4.3	556	26.1	2.VIII	30	63	134	17	33	3	37	135	158	94	14	40	97	–

Legnica

$H_s = 121$ m $H_b = 126.3$ m $h_w =$ 14.4 m I–VIII; 15 m IX–XII

I	3.5	1.1	2	2.0	1.5	2.0	14	2.6	12	2.7	21	2.9	16	2.8	10	2.6	13	2.3	17	5.1	9	·	·	21	·	·	·	·	17	11	6	·	3	2	·
II	3	2.8	5.5	2.9	5	2.4	3	3.2	·	·	16	3.2	25.5	3.7	24	4.0	2	3.4	29	5.4	17	4	17	26	·	1	·	1	16	23	8	·	·	26	·
III	6.5	3.9	3.5	3.6	3	3.0	5.5	3.7	7	2.6	19.5	2.2	22	3.2	11	3.0	15	2.5	26	8.8	3	5	6	18	·	1	·	4	13	13	5	·	2	14	·
IV	4.5	2.8	7.5	2.9	13.5	3.3	7.5	3.7	5.5	2.6	10	2.8	18.5	3.0	16	2.7	7	2.8	64	19.8	20	·	·	1	·	·	·	4	19	19	13	1	3	·	·
V	5	3.3	10.5	2.4	10.5	3.7	7.5	2.3	3.5	3.0	11	2.5	27	3.1	12	3.2	6	2.8	144	25.9	19	·	·	1	·	·	·	2	19	21	17	5	5	·	4
VI	3.5	2.9	6.5	2.2	4	1.4	9.5	2.5	3	1.7	11.5	2.5	23	3.6	14	3.5	15	2.4	58	10.4	9	·	·	·	6	·	·	3	12	17	13	1	·	·	8
VII	3	2.5	3	2.0	4	2.6	8	2.2	9.5	1.7	27	2.5	23.5	3.1	9	2.5	6	2.4	78	20.3	17	·	·	·	5	1	·	·	13	19	12	3	·	·	13
VIII	3.5	1.9	1.5	1.7	4.5	2.3	8.5	2.7	6	1.9	12.5	2.0	20.5	2.4	20	2.6	16	1.9	60	39.0	24	·	·	·	10	·	·	6	5	10	8	1	·	·	4
IX	1	2.0	1.5	2.0	4	2.6	15	3.9	13	2.9	13.5	2.2	19.5	3.3	7.5	3.8	15	2.6	38	15.9	10	·	·	·	3	·	·	4	3	9	7	1	2	·	2
X	1	2.0	5	1.3	10	2.2	10.5	3.0	7.5	1.3	8.5	2.5	18.5	3.0	10	3.4	22	1.9	4	3.1	16	·	·	11	·	1	·	5	8	3	1	·	13	·	·
XI	1.5	1.3	10	3.9	14.5	4.1	7	4.6	12	4.0	7	3.7	21	4.0	10	3.6	7	3.6	18	5.5	21	1	9	19	·	2	·	·	20	15	5	·	3	13	·
XII	1.5	3.0	2	2.5	5.5	4.0	9	3.7	19	3.6	18.5	3.7	29	4.6	7.5	4.0	1	3.9	38	9.3	21	·	·	15	·	1	·	·	15	21	8	·	2	3	·
Rok	37.5	2.5	58.5	2.4	80	2.8	105	3.2	98	2.3	176	2.7	264	3.3	151	3.2	125	2.7	574	39.0	24.VIII	10	32	112	24	7	·	29	160	181	103	12	33	58	31

Uwaga: Kierunki i prędkości wiatru - wg anemometru M-47

Wieluń — φ = 51°13' — λ = 18°35' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	p_m	Max	Min	$p_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	987.5	1001.6	967.2	1012.2	1.7	−3.3	6.0	29	−9.0	8	−1.3	1.2	−1.0	−0.5	5.3	6.9	5.3	5.5	95	89	93	92	0.3	0.8	0.4	0.5	8.8	8.2	7.5	8.2
II	992.2	1007.5	970.3	1017.5	−1.7	−8.5	2.9	13	−17.3	6	−6.0	−3.0	−5.2	−4.8	3.7	4.1	3.9	3.9	93	81	90	88	0.3	0.9	0.4	0.5	8.8	8.0	6.9	7.9
III	992.4	1008.5	963.5	1017.0	6.6	−2.3	16.1	30	−13.5	9	−1.0	5.4	1.4	1.8	5.7	6.4	6.2	6.1	94	70	88	84	0.4	3.2	0.8	1.5	6.6	6.7	5.5	6.3
IV	986.5	1006.4	972.2	1010.6	11.3	2.8	16.1	6	−1.3	16	4.6	10.0	6.1	6.7	7.8	8.4	8.4	8.2	91	70	89	83	1.0	4.1	1.1	2.1	7.0	7.9	6.7	7.2
V	989.9	1005.2	977.5	1013.9	15.0	6.2	23.8	17	−1.6	3	9.1	13.3	9.6	10.4	10.4	11.1	10.6	10.7	89	72	86	82	1.3	4.5	1.6	2.5	7.2	7.8	6.8	7.3
VI	990.5	1000.6	980.4	1013.9	21.2	10.9	33.0	26	6.3	4	14.6	19.7	14.7	15.9	13.9	14.0	14.1	14.0	83	63	84	77	3.0	9.8	2.9	5.2	5.7	6.9	5.9	6.2
VII	988.8	996.6	976.4	1012.2	21.9	11.7	31.2	14	7.2	4, 6	15.0	20.1	14.8	16.2	14.7	15.1	14.8	14.9	86	64	87	79	2.6	9.4	2.3	4.8	6.7	7.3	6.3	6.8
VIII	992.2	999.1	981.1	1015.6	22.1	10.6	31.2	7	6.5	17	13.4	20.5	14.4	15.7	13.6	13.4	13.8	13.6	88	57	84	76	2.0	11.9	3.0	5.6	4.9	6.1	5.6	5.5
IX	991.3	1011.0	977.9	1014.9	21.1	9.5	29.1	3	4.4	21	11.6	19.8	13.1	14.4	12.7	14.6	13.4	13.6	92	64	89	82	1.2	9.1	1.8	4.0	6.0	6.2	4.5	5.5
X	999.2	1012.9	987.8	1023.6	13.4	2.8	22.9	1	−6.6	22	4.4	12.5	6.2	7.3	8.2	9.9	8.9	9.0	93	68	90	84	0.6	5.0	1.0	2.2	6.4	5.2	4.8	5.5
XI	987.5	1007.1	960.3	1012.2	2.6	−3.6	13.1	2	−17.3	18	−1.8	1.3	−0.8	−0.5	5.2	5.7	5.4	5.4	91	82	89	87	0.6	1.4	0.7	0.9	8.5	8.3	8.1	8.3
XII	982.3	1001.5	960.7	1006.8	2.9	−1.5	10.2	20	−9.6	17	0.1	1.8	0.6	0.8	5.6	5.8	5.6	5.7	89	83	87	86	0.7	1.3	0.9	1.0	8.7	8.4	7.9	8.3
Rok	990.0	1012.9	960.3	1014.2	11.5	2.9	33.0	26.VI	−17.3	6.II, 18.XI	5.2	10.2	6.2	7.0	8.9	9.5	9.2	9.2	90	72	88	83	1.2	5.1	1.4	2.6	7.1	7.2	6.4	6.9

Siemianice — φ = 51°11' — λ = 18°09'

I	—	—	—	—	2.0	−2.6	6.6	29	−8.6	7	−1.0	1.4	−0.6	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.4	7.3	8.0
II	—	—	—	—	−1.8	−8.3	3.3	13	−16.8	6	−6.0	−3.2	−5.1	−4.8	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.6	6.7	7.6
III	—	—	—	—	6.4	−2.4	16.2	30	−15.7	9	−1.1	5.3	1.4	1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.2	6.0	6.5
IV	—	—	—	—	10.8	2.8	14.7	4	−1.9	15	4.6	9.6	6.4	6.8	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.2	6.8	6.9
V	—	—	—	—	14.4	6.1	23.6	17	−2.1	3	8.9	12.9	9.6	10.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.1	7.0	7.6
VI	—	—	—	—	20.5	10.8	31.7	26	5.8	3	14.4	19.2	15.0	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.3	5.9	6.0
VII	—	—	—	—	21.1	11.8	30.5	14	6.3	4	15.0	19.4	15.2	16.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.4	6.6	7.1
VIII	—	—	—	—	21.2	10.3	30.5	7	5.9	28	13.4	19.8	14.8	15.7	—	—	—	—	—	—	—	—	—	—	—	—	5.0	5.9	5.4	5.4
IX	—	—	—	—	20.4	9.2	28.3	3	3.7	21	11.9	19.1	13.3	14.4	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.1	4.2	5.3
X	—	—	—	—	13.1	2.9	21.6	2	−5.1	22	4.2	12.0	6.5	7.3	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.0	4.3	5.2
XI	—	—	—	—	2.7	−3.3	13.8	2	−15.6	18	−1.5	1.4	−0.6	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.2	7.5	8.0
XII	—	—	—	—	3.2	−1.2	11.0	19	−8.4	17	0.3	2.0	0.9	1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.5	7.2	8.2
Rok	—	—	—	—	11.2	3.0	31.7	26.VI	−16.8	6.II	5.3	9.9	6.4	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.1	6.2	6.8

Opole Lubelskie — φ = 51°09' — λ = 21°59'

I	—	—	—	—	0.9	−4.2	4.9	30	−14.5	11	−2.2	−0.1	−1.5	−1.3	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.7	7.1	7.8
II	—	—	—	—	−2.9	−11.0	2.3	12	−24.6	24	−7.6	−3.9	−6.8	−6.3	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.6	6.3	7.4
III	—	—	—	—	5.4	−3.0	16.3	30	−18.7	1	−0.9	4.6	0.8	1.3	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.7	5.0	5.7
IV	—	—	—	—	11.3	2.1	17.1	7	−2.8	3	4.7	9.8	6.0	6.6	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.3	6.0	6.7
V	—	—	—	—	15.6	6.0	27.4	19	−4.3	4	9.7	14.2	10.5	11.2	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.9	6.9	6.5
VI	—	—	—	—	21.5	11.3	30.5	26	6.4	8	15.2	20.0	15.9	16.8	—	—	—	—	—	—	—	—	—	—	—	—	5.4	6.4	5.9	5.9
VII	—	—	—	—	22.4	11.5	28.4	16, 17	5.4	11	16.3	20.7	16.3	17.4	—	—	—	—	—	—	—	—	—	—	—	—	5.1	6.7	5.9	5.9
VIII	—	—	—	—	21.1	10.6	30.9	8	5.2	31	13.9	20.0	14.7	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.6	4.9	5.5
IX	—	—	—	—	21.7	9.3	26.9	2, 3	2.0	16	12.6	20.2	13.9	15.2	—	—	—	—	—	—	—	—	—	—	—	—	4.2	4.8	2.4	3.8
X	—	—	—	—	12.9	2.7	22.7	1	−5.5	22	5.4	11.9	6.9	7.8	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.2	3.2	4.6
XI	—	—	—	—	2.1	−3.6	13.5	2	−17.8	18	−1.7	0.7	−1.0	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.8	9.1	8.8	8.9
XII	—	—	—	—	2.4	−2.5	8.5	19	−19.4	17	−0.6	1.4	−0.3	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.6	6.1	7.7
Rok	—	—	—	—	11.2	2.4	30.9	8.VIII	−24.6	24.II	5.4	10.0	6.3	7.0	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.8	5.7	6.4

Zgorzelec — φ = 51°08' — λ = 15°02'

I	986.4	1000.6	967.1	1011.5	2.9	−1.3	7.7	17	−7.3	7, 27	0.2	1.8	0.8	0.9	5.4	5.6	5.6	5.5	87	81	86	85	0.9	1.4	1.0	1.1	8.0	8.7	8.5	8.4
II	993.3	1007.9	969.4	1019.0	−0.4	−6.8	3.3	14	−17.7	6	−3.8	−2.4	−3.5	−3.3	4.2	4.1	4.1	4.1	88	79	85	84	0.6	1.1	0.7	0.8	9.0	8.5	7.9	8.5
III	991.8	1007.4	967.5	1017.0	5.7	−3.5	15.5	30	−16.5	9	−1.6	4.1	0.5	0.9	5.2	5.6	5.7	5.5	89	67	85	80	0.7	3.1	1.1	1.6	7.0	6.8	5.3	6.4
IV	985.6	1007.5	968.8	1010.7	11.6	2.7	18.4	6	−1.4	1	4.3	9.8	6.7	6.9	7.6	7.4	7.8	7.6	90	63	79	77	0.8	4.9	2.2	2.6	7.4	7.2	6.8	7.1
V	989.3	1003.8	978.0	1013.6	15.1	6.6	22.6	17	−0.2	3	9.2	13.3	10.3	10.8	10.2	10.1	10.6	10.3	85	67	83	78	1.7	5.5	2.2	3.1	6.8	7.7	6.5	7.0
VI	990.2	1002.4	977.9	1014.1	20.6	10.4	29.7	26	5.4	3	13.8	18.5	15.1	15.6	13.4	13.4	14.1	13.6	84	63	82	76	2.7	8.5	3.3	4.8	6.2	7.4	5.1	6.2
VII	988.1	995.4	975.5	1012.0	20.7	11.7	31.0	14	6.6	4	14.5	18.6	15.3	15.9	14.0	13.8	14.2	14.0	83	64	80	76	2.7	8.2	3.5	4.8	7.3	7.8	6.1	7.1
VIII	991.7	1000.3	975.7	1015.7	21.5	9.8	30.2	6	3.9	14	12.4	20.0	14.4	15.3	13.0	12.1	13.8	13.0	89	52	84	75	1.7	12.1	3.0	5.6	4.7	6.3	4.5	5.2
IX	989.6	1011.2	973.4	1013.7	19.2	9.2	26.9	2	2.9	30	11.1	17.6	12.8	13.6	11.8	12.0	12.5	12.1	89	60	84	78	1.7	8.5	2.6	4.3	5.6	6.3	4.0	5.3
X	998.7	1010.8	987.5	1023.7	13.4	2.8	21.7	1	−4.5	23	4.1	12.5	6.6	7.4	7.8	9.3	8.8	8.6	92	63	88	81	0.8	5.5	1.2	2.5	4.3	4.9	2.9	4.0
XI	986.2	1008.2	957.8	1011.4	3.5	−2.5	14.3	1	−11.8	23	−0.1	2.0	−0.1	0.4	5.3	5.5	5.3	5.4	86	77	84	82	1.1	1.8	1.2	1.4	8.6	8.4	7.1	8.0
XII	980.6	1001.5	956.3	1005.5	4.4	0.3	11.5	19	−5.0	14	1.6	2.8	2.4	2.3	6.0	6.0	6.2	6.1	86	80	84	83	1.0	1.6	1.2	1.3	8.0	8.0	8.2	8.1
Rok	989.3	1011.2	956.3	1014.0	11.5	3.3	31.0	14.VII	−17.7	6.II	5.5	9.9	6.8	7.2	8.7	8.8	8.1	8.9	87	68	84	80	1.4	5.2	1.9	2.8	6.9	7.3	6.1	6.8

Wieluń

$H_s = 195\,m$ $H_b = 198{,}4\,m$ $h_w = 10\,m$ **1965**

MIESIĄC	ROZKŁAD WIATRU °D,V,m/s N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◐	◕	Opad R R≥0,1	R≥1,0	R≥10,0	≡	⊠	R (K)
I	4.5	2.8	4	1.6	9.5	2.3	17.5	2.8	26.5	4.2	11	3.2	12	2.4	8	2.0	·	3.0	34	4.8	10	·	4	28	·	1	·	·	19	18	12	·	6	27	·
II	12.5	3.2	6.5	2.5	2	2.2	2	2.0	6	3.4	21.5	3.3	23	2.7	10.5	4.1	·	3.1	28	6.9	17	9	22	28	·	·	·	1	16	19	11	·	2	28	·
III	6	2.3	5	2.7	8	2.6	18.5	2.5	14.5	2.6	24.5	2.8	12	2.6	4.5	3.1	·	2.6	23	5.5	3	2	6	19	·	3	·	4	12	13	7	·	4	15	·
IV	7	2.9	16.5	3.2	19	3.7	10.5	2.6	6	3.0	12	2.1	10.5	3.0	7.5	2.4	1	2.9	52	10.0	23	·	·	3	·	·	·	3	15	14	12	1	1	·	3
V	9.5	2.2	11	2.6	7	2.8	8	2.5	2	2.0	17	2.4	20	2.0	13.5	2.0	5	2.2	86	14.8	19	·	·	3	·	1	·	2	15	23	16	1	4	·	5
VI	7	2.3	5.5	2.5	9	2.5	10.5	1.9	13.5	2.1	14.5	2.3	14.5	2.7	8.5	1.7	3	2.2	77	17.3	6	·	·	·	5	1	·	1	9	18	15	3	·	·	4
VII	5.5	2.5	3	2.3	8.5	2.5	6	1.6	13.5	2.0	31	2.2	19	2.1	1.5	1.7	5	2.0	49	8.8	31	·	·	·	5	1	·	1	10	14	9	·	2	·	7
VIII	2	1.2	3.5	1.3	3.5	1.9	14	2.4	13	2.0	17	1.3	23.5	2.1	10.5	2.0	6	1.8	46	17.2	25	·	·	·	9	·	·	5	7	11	6	1	2	·	3
IX	·	·	·	·	12	2.3	23.5	2.0	18	1.9	15.5	1.9	14.5	1.6	0.5	1.0	6	1.8	51	14.8	4	·	·	·	3	·	·	7	8	9	6	2	1	·	3
X	3.5	1.0	7.5	1.3	15	1.6	2.5	1.4	15.5	1.6	15	2.0	14	2.0	7	1.5	13	1.4	10	4.9	16	·	·	6	·	·	·	7	10	5	2	·	9	·	·
XI	3	1.8	13	3.3	9.5	2.2	9.5	3.6	13.5	3.4	17	3.4	14	2.2	2.5	1.2	8	2.7	43	5.8	3	3	8	21	·	·	·	1	23	20	10	·	7	18	·
XII	2.5	1.4	1	1.5	8	1.9	8.5	3.5	23.5	4.8	28	4.2	13	3.5	8.5	2.5	·	3.7	49	16.1	18	·	3	21	·	5	·	·	21	17	13	1	1	13	·
Rok	63	2.0	80.5	2.1	111	2.4	131	2.4	165.5	2.8	224	2.6	190	2.4	83	2.1	47	2.4	548	17.3	6. VI	14	43	129	22	12	·	32	165	181	119	9	39	101	25

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Siemianice

$H_s = 182\,m$ $h_w = 10\,m$

I	4	5.0	5	5.0	3	3.5	10	2.8	16	4.1	28	4.0	8.5	5.8	6.5	6.7	12	3.8	25	5.3	24	·	4	27	·	3	·	1	17	15	10	·	5	26	·
II	14	6.5	8	6.2	1	7.5	·	·	2.5	2.8	13.5	5.3	20.5	6.6	19.5	7.8	5	6.1	12	2.1	17	9	22	28	·	11	4	·	16	18	5	·	2	28	·
III	2	4.5	9	4.4	2	5.0	7.5	3.5	16	2.4	22.5	3.5	14.5	6.7	9.5	7.0	10	3.9	18	6.2	2	3	6	19	·	8		3	13	11	7	·	7	14	·
IV	8	4.7	9.5	6.3	11.5	6.6	12	4.1	4.5	3.4	8	3.5	12.5	5.4	11	5.8	13	4.4	50	18.8	23	·	·	3	·	4		5	17	14	8	1	1	·	3
V	11.5	3.4	10.5	5.0	10	5.5	3	5.2	3	3.7	8.5	4.1	15.5	6.3	17	5.0	14	4.2	146	19.7	19	·	·	3	·	4	2	2	20	23	19	7	3	·	7
VI	9	4.9	8	4.1	6.5	4.4	4.5	6.8	10	4.0	15	3.0	19	4.9	12	5.5	6	4.2	83	21.1	6	·	·	·	3	1		1	9	18	14	3	·	·	5
VII	3	5.0	2.5	5.8	5.5	4.1	4	5.2	3	2.7	22.5	3.5	35	5.0	8.5	4.4	9	4.0	72	26.2	17	·	·	·	5	2		1	10	18	11	1	1	·	5
VIII	6	3.3	1.5	3.3	·	·	6	3.8	9	2.9	11.5	3.1	16.5	4.0	24.5	4.6	18	3.1	63	19.3	25	·	·	·	9	·	·	4	6	15	8	2	·	·	2
IX	·	·	·	·	1.5	5.0	11.5	4.9	17	4.0	22	3.0	13.5	4.5	8.5	4.5	16	3.3	63	23.4	28	·	·	·	3	2	·	6	5	10	6	2	3	·	3
X	4	3.4	7	4.0	10	3.8	4	3.1	7.5	2.4	17	3.2	14	4.4	14.5	4.1	15	3.1	5	3.1	16	·	·	8	·	·	·	7	8	4	1	·	10	·	·
XI	2.5	3.8	10	8.6	11	5.4	5.5	3.5	15.5	3.1	17	4.4	16	7.0	10.5	4.9	2	5.1	38	6.4	3	4	8	20	·	5	2	1	18	20	10	·	7	17	·
XII	2.5	6.0	·	·	2.5	4.2	6	4.0	18.5	4.5	33	5.5	18	5.6	7.5	4.9	5	4.8	44	16.0	18	·	3	20	·	5	2	·	20	16	9	1	4	11	·
Rok	66.5	4.2	71	4.4	64.5	4.6	74	3.9	122.5	3.3	218.5	3.8	203.5	5.5	149.5	5.4	125	4.2	619	26.2	17. VII	16	43	128	20	45	10	31	159	182	108	17	43	96	25

Opole Lubelskie

$H_s = 149\,m$ $h_w = 12{,}5\,m$

I	8	4.0	2	3.5	7.5	3.5	10	3.7	26.5	4.5	7	6.1	6.5	4.6	8.5	6.0	17	3.9	41	9.8	17	2	6	26	·	5	·	3	17	16	10	·	2	17	—
II	7.5	2.8	15	5.0	·	·	·	·	6	10.5	7	8.0	5	4.8	26.5	4.8	17	4.3	39	7.2	7	15	23	28	·	7	·	3	14	20	14	·	2	28	—
III	3	6.3	12	3.5	2	4.0	2	2.5	14	5.1	6	3.5	4	3.2	15	3.7	35	2.5	22	5.2	21	4	6	19	·	3	·	4	11	13	6	·	1[2]	16	—
IV	12	3.3	6.5	5.1	27.5	5.0	13	4.3	2.5	2.4	3.5	5.1	6.5	2.2	7.5	3.2	11	3.6	41	9.0	28	·	·	8	·	4	·	1	10	13	10	·	1[2]	·	—
V	18	3.4	11	2.8	12	4.5	1	8.0	3	3.3	3	3.7	11.5	3.7	17.5	4.5	16	3.2	61	13.8	9	·	·	2	1	3	·	3	11	14	12	2	·	·	—
VI	11.5	3.4	7.5	4.5	4	7.0	6.5	3.7	3.5	6.3	1	3.0	4	6.0	33	3.8	19	3.3	77	15.0	27	·	·	·	7	3	·	3	9	12	10	2	·	·	—
VII	1.5	3.0	5	2.4	2	3.0	3.5	4.0	9	4.8	13	5.6	13.5	4.7	22.5	3.2	23	3.1	56	19.4	17	·	·	·	10	2	·	3	7	14	12	1	·	·	—
VIII	10.5	4.2	1.5	3.0	·	·	8	3.1	8.5	5.1	2.5	3.2	2	6.0	35	3.6	25	2.8	122	31.6	26	·	·	·	9	2	·	10	11	13	12	5	1	·	—
IX	1.5	2.0	·	·	·	·	10	3.5	21.5	3.6	7	2.4	10	2.4	14	2.9	26	2.2	41	16.6	29	·	·	·	6	1	·	8	2	8	5	2	2	·	—
X	9	2.1	6	1.8	6	3.3	·	·	7.5	1.3	4	2.6	11.5	1.8	26	2.5	23	1.7	7	2.5	11	·	·	5	·	·	·	10	6	8	3	·	6	·	—
XI	6	2.2	10	3.9	5.5	2.2	8.5	3.3	11.5	3.4	6.5	2.9	4.5	3.1	19.5	3.0	18	2.5	44	5.2	11	5	10	18	·	1	·	·	21	24	15	·	5	13	—
XII	3	2.0	1	1.0	1	1.0	8.5	2.7	28	4.8	16	2.7	13.5	2.4	9	3.2	13	2.9	37	12.0	18	2	4	20	·	4	·	·	14	18	8	1	1	5	—
Rok	91.5	3.2	77.5	3.0	67.5	2.8	71	3.2	141.5	4.6	76.5	4.1	92.5	3.7	234	3.9	243	3.0	588	31.6	26.VIII	28	49	126	33	35	·	48	133	173	117	13	21[2]	79	—

Zgorzelec

$H_s = 203\,m$ $H_b = 202{,}2\,m$ $h_w = 15\,m$

I	3	4.2	5.5	2.7	2	2.0	2	1.0	28.5	5.0	29.5	4.8	8.5	4.5	6	2.9	8	4.0	39	3.8	9	·	·	21	·	6	·	·	23	16	9	·	5	12	·
II	9.5	4.2	7	3.9	3	4.3	0.5	2.0	11.5	4.7	14.5	4.4	20.5	5.1	15.5	4.4	2	4.4	31	5.1	13	7	17	28	·	4	1	·	19	23	13	·	·	27	·
III	6	5.1	7	4.1	1.5	2.0	2.5	1.8	22.5	3.4	28	4.3	11	4.4	5.5	4.0	9	3.6	23	4.6	2	9	6	19	·	1	·	4	12	14	8	·	2	15	·
IV	6	3.2	10.5	4.3	10.5	3.4	2.5	2.0	18.5	3.3	13	4.0	10	5.0	10	4.0	9	3.4	72	11.6	28	·	·	5	·	2	·	1	16	18	16	1	1	·	1
V	5.5	4.4	13	4.1	8	3.9	·	·	11	3.5	16.5	3.2	17	4.6	12	3.7	10	3.5	139	20.3	29	·	·	1	·	2	·	2	13	21	17	6	·	·	3
VI	3	4.0	13	3.2	6	6.1	3.5	2.1	11.5	3.6	19.5	3.2	17.5	4.4	9	3.7	7	3.3	87	36.7	11	·	·	·	5	·	·	2	10	15	10	2	·	·	7
VII	7.5	2.5	3.5	3.0	5	3.3	1.5	1.7	18	3.9	23	3.8	26	3.8	3.5	3.0	5	3.4	64	10.4	31	·	·	·	3	3	·	·	12	17	11	1	·	·	9
VIII	3	2.2	2.5	2.8	2	1.2	1.5	3.3	20	2.2	19.5	2.4	17	3.4	6.5	2.5	21	2.0	34	13.3	24	·	·	·	7	1	·	4	4	12	9	1	·	·	2
IX	1	3.0	2	2.0	4	3.4	3.5	3.3	23	3.5	26	3.0	12.5	3.5	·	·	18	2.6	69	23.5	10	·	·	·	1	·	·	7	5	12	8	4	·	·	5
X	5	1.7	8.5	3.2	5	2.7	1.5	1.7	13.5	3.8	20.5	3.0	7.5	3.0	2.5	1.8	29	2.1	10	5.3	16	·	·	9	·	·	·	10	5	5	2	·	7	·	·
XI	4	2.8	13.5	3.5	4	2.2	3.5	3.3	27	4.6	17	4.6	7	4.8	3	2.8	11	3.6	25	5.4	21	4	9	22	·	·	·	·	17	16	8	·	1	15	
XII	0.5	3.0	2	2.0	3.5	1.9	0.5	1.0	38.5	5.7	30	4.6	9.5	3.5	3.5	2.1	5	4.4	66	14.9	18	·	·	13	·	5	2	·	17	24	14	1	1	10	
Rok	54	3.4	88	3.2	54.5	3.0	23	1.9	243.5	3.9	257	3.8	164	4.2	77	2.9	134	3.4	659	36.7	11. VI	20	32	118	16	24	3	30	153	193	125	16	17	79	27

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47

Szymanów — φ = 51°08′ — λ = 16°29′ — 1965

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	3.2	−0.7	7.1	17	−7.2	7	0.4	2.1	0.9	1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.6	7.9	8.0
II	–	–	–	–	−0.7	−7.0	4.3	13	−15.4	10	−4.5	−2.3	−4.0	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.4	6.9	7.5
III	–	–	–	–	6.1	−2.6	16.6	30	−17.9	9	−0.8	5.2	1.5	1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.9	6.0	6.1
IV	–	–	–	–	11.3	2.9	16.8	4	−0.4	8	5.3	10.2	6.4	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	7.7	7.4
V	–	–	–	–	14.9	6.8	24.2	17	−0.4	3	9.6	13.5	10.4	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	7.5	7.7
VI	–	–	–	–	20.9	10.8	32.2	26	6.9	3	14.9	19.4	14.8	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	5.9	6.1
VII	–	–	–	–	21.3	11.9	30.6	14	7.0	10	15.7	19.6	14.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.4	7.0	7.5
VIII	–	–	–	–	21.5	10.1	31.1	6	4.7	16	14.5	20.5	14.3	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.9	5.2	5.4
IX	–	–	–	–	20.1	9.6	26.0	2	3.9	22	12.5	19.1	13.1	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	4.8	5.4
X	–	–	–	–	13.5	2.9	21.6	1	−5.2	23	4.6	12.6	6.8	7.7	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.4	4.4	5.2
XI	–	–	–	–	3.6	−2.2	14.8	1	−11.0	23	−0.1	2.3	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	7.9	8.2
XII	–	–	–	–	4.5	−0.7	12.5	19	−10.4	15	1.4	3.0	2.0	2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.9	7.7	8.0
Rok	–	–	–	–	11.7	3.5	32.2	26.VI	−17.9	9.III	6.1	10.4	6.8	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	6.6	6.9

Wrocław-Strachowice — φ = 51°06′ — λ = 16°53′

Miesiąc	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	e_m I	II	III	Dies	U_m I	II	III	Dies	Δ_m I	II	III	Dies	N_m I	II	III	Dies
I	996.8	1011.5	977.1	1012.4	3.2	−1.7	7.7	17	−6.2	7	0.0	2.3	0.5	0.8	5.6	5.9	5.6	5.7	91	82	87	87	0.6	1.4	0.9	1.0	8.0	7.1	8.0	7.7
II	1002.7	1017.0	979.0	1018.5	−0.7	−8.0	3.8	13	−17.7	6	−4.6	−2.3	−4.2	−3.8	3.9	4.1	4.0	4.0	87	79	85	84	0.6	1.1	0.7	0.8	8.4	8.1	6.8	7.8
III	1001.9	1017.3	974.5	1017.4	6.7	−3.5	17.3	30	−21.5	9	−1.8	5.6	1.2	1.6	5.3	6.1	6.0	5.8	90	65	84	80	0.5	3.7	1.1	1.8	6.3	5.6	6.2	6.0
IV	995.8	1016.6	981.6	1010.9	11.7	2.7	17.1	3, 6	−1.9	3	4.8	10.5	6.7	7.2	7.7	7.6	8.0	7.8	89	62	81	77	1.0	5.3	1.8	2.7	7.1	7.0	7.1	7.1
V	999.2	1013.6	986.9	1014.2	15.2	6.2	24.1	17	−1.3	3	9.2	13.8	10.4	11.0	10.5	10.5	10.6	10.5	88	66	82	79	1.3	5.5	2.3	3.0	7.4	8.0	6.8	7.4
VI	999.8	1010.5	987.2	1014.5	21.3	10.6	32.5	26	5.3	3	14.7	19.9	15.4	16.4	14.3	14.3	14.6	14.4	85	61	83	76	2.6	9.8	3.3	5.2	5.6	6.8	5.5	6.0
VII	997.8	1005.6	985.1	1012.5	21.7	11.6	31.0	14	6.0	10	15.4	19.7	15.1	16.3	14.7	15.0	15.0	14.9	83	65	86	78	3.0	8.7	2.4	4.7	7.1	7.3	6.0	6.8
VIII	1001.4	1009.1	989.0	1016.1	21.8	9.8	31.0	7	5.3	31	13.1	20.4	14.6	15.7	13.9	13.7	14.2	13.9	91	57	85	78	1.4	11.3	2.7	5.1	4.9	5.6	4.5	5.0
IX	999.8	1020.5	986.4	1014.6	20.7	8.8	26.7	2	1.8	22	14.0	19.6	13.0	14.2	12.2	13.6	13.3	13.0	93	60	88	80	1.2	9.8	1.9	4.3	5.2	5.6	4.0	4.9
X	1008.6	1021.9	997.4	1023.9	13.9	1.8	22.9	1	−6.8	23	3.6	12.8	5.8	7.0	7.9	9.7	8.7	8.8	96	65	91	84	0.4	5.7	0.9	2.3	5.6	5.3	3.5	4.8
XI	996.8	1017.2	968.5	1012.4	3.9	−2.9	14.0	2	−12.6	24	−0.6	2.4	0.0	0.4	5.5	6.2	5.7	5.8	90	80	88	86	0.7	1.6	0.8	1.0	8.2	8.2	7.6	8.0
XII	991.4	1012.0	968.9	1006.8	4.3	−1.3	11.7	19	−8.1	15	1.0	3.0	1.5	1.8	5.7	6.1	6.0	5.9	86	80	87	84	1.0	1.6	1.0	1.2	7.7	7.3	7.5	7.5
Rok	999.3	1021.9	968.5	1014.4	12.0	2.8	32.5	26.VI	−21.5	9.III	5.5	10.6	6.7	7.4	8.9	9.4	9.3	9.2	89	68	86	81	1.2	5.5	1.6	2.8	6.8	6.8	6.1	6.6

Czarniecka Góra — φ = 51°08′ — λ = 20°31′

Miesiąc	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	e_m I	II	III	Dies	U_m I	II	III	Dies	Δ_m I	II	III	Dies	N_m I	II	III	Dies
I	–	–	–	–	0.9	−4.5	5.3	30	−16.3	11	−2.4	0.3	−1.7	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	6.7	7.0
II	–	–	–	–	−3.2	−12.7	1.1	12, 13, 15	−29.2	6	−8.0	−3.8	−7.9	−6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	6.4	6.7
III	–	–	–	–	5.1	−5.0	16.4	30	−21.2	1	−2.9	4.8	0.0	0.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.3	5.4	5.8
IV	–	–	–	–	9.2	0.7	14.1	7, 20	−3.5	6	3.1	8.8	4.7	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.6	4.8	5.9
V	–	–	–	–	13.7	4.5	22.4	19	−5.2	3	8.3	13.2	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.5	6.2	6.1
VI	–	–	–	–	20.5	9.7	31.5	26	2.8	3	14.2	19.6	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.3	5.8	5.3
VII	–	–	–	–	21.4	10.2	29.2	16	3.4	5, 11	14.8	20.1	14.5	16.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.5	6.1	5.3
VIII	–	–	–	–	19.9	9.0	30.6	8	2.0	31	12.2	19.3	13.5	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.5	4.7	5.2
IX	–	–	–	–	20.6	8.1	25.5	3	1.0	22	10.5	19.6	12.8	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.2	4.0	4.5
X	–	–	–	–	12.4	1.1	22.6	1	−6.6	22	3.6	11.9	5.0	6.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.6	4.0	4.8
XI	–	–	–	–	2.1	−4.3	11.5	2	−19.2	24	−2.4	0.7	−1.3	−1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.1	7.9	7.9
XII	–	–	–	–	2.3	−3.3	8.5	20	−19.8	17	−0.5	1.4	−0.5	0.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	5.5	6.3
Rok	–	–	–	–	10.4	1.1	31.5	26.VI	−29.2	6.II	4.2	9.7	5.2	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	5.6	5.9

Pszczela Wola — φ = 51°07′ — λ = 22°31′

Miesiąc	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	e_m I	II	III	Dies	U_m I	II	III	Dies	Δ_m I	II	III	Dies	N_m I	II	III	Dies
I	–	–	–	–	0.2	−5.1	5.3	30	−17.3	11	−2.8	−0.4	−2.2	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.1	6.9	7.2
II	–	–	–	–	−3.6	−11.0	0.6	14	−25.4	24	−8.0	−4.6	−7.1	−6.7	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.2	6.3	7.4
III	–	–	–	–	4.8	−3.8	15.5	30	−19.2	1	−1.9	4.1	−0.1	0.5	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.9	5.2	5.9
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	5.3	6.1
V	–	–	–	–	15.3	5.7	26.4	19	−3.7	4	9.1	14.1	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.4	5.8	6.6
VI	–	–	–	–	21.1	10.7	28.9	26	5.4	8, 9	14.6	20.0	14.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.5	6.0	6.1
VII	–	–	–	–	22.3	10.8	28.9	16	5.7	11	15.5	20.9	15.2	16.7	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.6	5.5	5.6
VIII	–	–	–	–	21.1	9.5	30.3	8	3.5	17	13.0	19.7	13.7	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.2	4.1	4.7
IX	–	–	–	–	21.7	–	27.9	2	–	–	11.0	20.7	12.8	14.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.5	2.1	22.4	1	−6.5	22	4.2	12.1	5.9	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.8	−4.1	13.8	2	−21.2	18	−1.9	0.7	−1.3	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.5	8.1
XII	–	–	–	–	2.0	−2.5	7.8	20	−19.3	17	−0.5	1.5	0.0	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.7	6.8	8.0
Rok	–	–	–	–	–	–	30.3	8.VIII	−25.4	24.II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Szymanów $H_s = 145\ m$ $h_w = 12\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD}: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V: V ≥ 10	V ≥ 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	6	3.5	1.5	2.7	6	2.5	12.5	3.3	15.5	4.4	24	3.7	20	3.6	6.5	2.2	1	3.5	13	4.5	9	·	1	24	·	1	·	·	16	13	5	·	1	5	·
II	11	3.4	3	3.2	5.5	1.4	4.5	3.2	0.5	3.0	8.5	2.9	25	4.9	22	4.7	4	3.8	16	3.8	17	7	20	27	·	1	·	2	16	20	5	·	1	27	·
III	8.5	4.0	7	3.0	3	2.8	9.5	2.5	11.5	2.3	21	3.3	22	4.3	8.5	3.7	2	3.3	24	6.0	16	4	7	17	·	·	·	5	13	15	9	·	1	14	·
IV	9.5	3.8	5	3.3	14.5	3.1	10.5	2.9	5.5	3.2	7.5	2.9	17.5	3.4	18	3.2	2	3.2	59	19.1	20	·	·	1	·	·	·	4	17	19	12	1	1	·	2
V	11	2.5	8.5	2.8	14	2.9	4.5	4.6	5	3.8	4.5	2.8	19.5	3.4	21	3.0	5	2.9	142	25.1	29	·	·	1	·	·	·	2	18	21	17	4	·	·	6
VI	6	2.0	7	2.4	6.5	3.0	11	1.8	5.5	3.1	9	2.2	22.5	3.1	14.5	3.3	8	2.5	52	11.0	22	·	·	·	6	·	·	5	12	15	12	1	·	·	5
VII	4	3.2	4.5	2.4	3	3.2	3.5	3.6	12	3.0	23	2.9	33	3.3	9	2.7	1	3.0	112	40.5	16	·	·	·	3	·	·	·	16	19	13	3	·	·	11
VIII	5	2.8	1	1.5	10	1.7	8.5	3.2	6.5	2.7	5	2.9	26	3.1	28	2.1	3	2.5	71	50.9	24	·	·	·	8	·	·	4	4	13	7	1	·	·	1
IX	0.5	1.0	1.5	2.3	8	2.8	15.5	4.8	12.5	2.7	18	2.5	22	3.1	5	3.0	7	2.9	36	16.6	10	·	·	·	3	·	·	5	4	7	6	2	·	·	2
X	3	1.0	2.5	1.8	19	2.1	15.5	2.3	7	2.5	12	2.8	16	2.8	13	2.5	5	2.3	4	4.0	16	·	·	8	·	·	·	10	6	2	1	·	8	·	·
XI	3.5	1.9	10	3.5	11	3.4	8	4.6	10.5	5.0	11.5	5.2	23	4.3	10.5	3.0	2	4.0	18	3.5	3, 21	3	11	20	·	1	·	·	19	19	5	·	4	16	·
XII	1	3.0	4	3.0	5	3.8	5.5	4.2	16	4.8	31.5	5.5	21	5.4	9	4.0	·	4.9	26	6.3	21	1	·	18	·	4	1	1	18	17	8	·	·	3	·
Rok	69	2.7	55.5	2.7	105.5	2.7	109	3.4	108	3.4	175.5	3.3	267.5	3.7	165	3.1	40	3.2	573	50.9	24.VIII	15	39	116	20	7	1	38	159	180	100	12	16	65	27

Wrocław - Strachowice $H_s = 120\ m$ $H_b = 123.8\ m$ $h_w = 10\ m$

I	6.5	2.8	1	3.0	3.5	2.3	20	3.9	11	4.8	16.5	5.6	14.5	5.3	14	3.3	6	4.0	15	4.5	9	·	·	27	·	4	·	·	18	14	4	·	6	6	·
II	9.5	3.3	7	2.6	2	4.2	5.5	4.0	2.5	2.4	11.5	5.7	22	4.8	23	5.1	1	4.4	15	4.9	17	8	20	26	·	6	·	2	15	16	4	·	4	27	·
III	7	3.4	5	2.7	4.5	2.7	18.5	2.9	7.5	4.1	16.5	4.1	17	5.2	14	4.6	3	3.8	15	3.8	28	6	5	20	·	3	·	4	10	12	6	·	5	13	·
IV	8.5	2.9	5	3.3	12.5	4.8	13	4.9	4	4.9	5	3.8	16	4.2	20	3.9	6	3.9	60	16.3	20	·	·	6	·	2	·	3	17	16	12	2	3	·	2
V	6.5	3.2	8.5	2.6	14	3.1	7.5	4.8	4.5	3.2	6	2.8	19.5	4.4	21.5	3.5	5	3.4	136	24.9	29	·	·	3	·	3	·	2	17	18	15	5	5	·	4
VI	6.5	2.0	5	2.2	11.5	2.7	13	3.3	6.5	4.3	7.5	3.0	17	4.0	18	4.2	5	3.3	55	11.0	22	·	·	·	6	1	·	3	9	17	12	1	3	·	8
VII	6	2.8	2	1.5	8	2.8	5.5	3.3	8	3.4	18	3.8	28.5	3.9	12	4.1	5	3.4	95	22.0	17	·	·	·	5	2	·	·	10	17	13	4	·	·	8
VIII	4	2.4	1.5	2.0	5	1.5	11	2.6	8.5	3.8	6.5	3.2	19.5	2.9	29	2.7	8	2.5	44	13.5	24	·	·	·	9	1	·	4	4	12	7	2	6	·	2
IX	2.5	3.2	0.5	1.0	4.5	1.4	21	3.9	15.5	3.9	7.5	3.6	11.5	3.5	18	3.2	9	3.1	31	10.2	28	·	·	·	3	4	·	5	4	7	6	1	6	·	2
X	2	1.5	2.5	1.6	10.5	1.7	19.5	2.7	4.5	3.8	3.5	3.4	13.5	3.3	22	3.5	15	2.4	4	3.0	16	·	·	12	·	1	·	6	4	3	1	·	17	·	·
XI	3	2.0	7.5	2.7	10.5	3.1	12.5	4.1	9.5	5.1	5.5	5.1	16	5.3	19.5	4.2	6	3.9	25	5.5	3	4	9	21	·	5	·	·	18	18	9	·	8	16	·
XII	3.5	2.6	1.5	1.0	2	3.0	12.5	3.3	13.5	4.7	18.5	6.4	22.5	6.4	17	4.8	2	5.0	38	12.0	18	·	·	23	·	6	·	1	15	15	10	1	4	5	·
Rok	65.5	2.7	47	2.2	88.5	2.8	159.5	3.6	95.5	4.0	122.5	4.2	217.5	4.4	228	3.9	71	3.6	533	24.9	29.V	18	34	138	23	38	·	30	141	165	99	16	67	67	26

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Czarniecka Góra $H_s = 256\ m$ $h_w = 14.5\ m$

I	3	3.0	2	1.0	10	3.4	10	2.6	19	2.6	19	3.1	10	2.6	9	2.2	11	2.4	64 ?	7.5	23	5	10	25	·	—	—	4	14	—	—	—	—	—	—
II	9	4.1	9	2.6	3	3.0	·	·	·	·	14	4.4	20	3.4	20	3.2	9	3.2	69 ?	9.5	16	14	24	28	·	—	—	2	10	—	—	—	—	—	—
III	10	3.3	5	2.2	6	2.7	6	4.0	23	2.5	11	3.4	16	2.3	2	6.0	14	2.4	34	14.4	3	5	7	25	·	—	—	3	7	—	—	—	—	—	—
IV	6	2.8	2	1.0	30	4.0	14	4.5	7	1.6	3	3.0	12	3.0	7	3.0	9	3.1	59	19.4	23	·	·	14	·	—	—	·	6	—	—	—	—	—	—
V	17	1.9	5	1.4	13	3.7	6	3.3	7	1.4	14	2.9	11	1.8	14	2.6	6	2.3	58	12.5	9	·	·	6	·	—	—	1	9	—	—	—	—	—	—
VI	7	2.0	1	7.0	19	4.5	9	4.3	4	2.8	9	3.1	18	3.3	15	3.1	8	3.2	99	14.4	11	·	·	·	5	—	—	2	5	—	—	—	—	—	—
VII	4	2.8	1	5.0	12	2.5	6	3.2	9	3.1	30	4.3	24	3.8	2	2.0	5	3.4	85	22.0	18	·	·	·	5	—	—	1	3	—	—	—	—	—	—
VIII	13	1.8	2	1.0	4	2.5	13	3.5	9	3.2	12	2.5	16	2.8	19	2.8	5	2.6	104	31.8	26	·	·	·	9	—	—	1	6	—	—	—	—	—	—
IX	·	·	·	·	3	4.0	16	3.8	22	3.5	14	3.9	14	2.4	13	2.2	8	3.0	61	23.7	29	·	·	·	1	—	—	3	3	—	—	—	—	—	—
X	11	1.8	2	1.5	11	2.5	·	·	9	1.3	18	3.0	18	3.4	15	2.6	9	2.3	7	2.4	16	·	·	14	·	—	—	3	5	—	—	—	—	—	—
XI	3	1.7	10	2.9	9	4.0	8	2.8	16	2.4	12	2.7	17	2.4	6	3.2	9	2.5	58	9.4	11	6	9	22	·	—	—	1	17	—	—	—	—	—	—
XII	4	1.2	1	2.0	2	2.5	4	2.0	22	3.0	26	3.6	17	3.2	7	2.3	10	2.7	71 ?	20.0	18	2	5	27	·	—	—	2	10	—	—	—	—	—	—
Rok	87	2.2	40	2.3	122	3.3	92	2.8	147	2.3	182	3.3	193	2.9	129	2.9	103	2.8	769 ?	31.8	26.VIII	32	55	161	20	—	—	23	95	—	—	—	—	—	—

Pszczela Wola $H_s = 195\ m$ $h_w = 18\ m$

I	1	1.0	5	2.6	0.5	2.0	12.5	2.3	16.5	2.0	21	2.4	11.5	3.4	2	1.0	23	1.8	35	9.4	17	3	12	26	·	·	·	5	18	12	10	·	—	31	—
II	7.5	2.1	7	2.6	·	·	0.5	4.0	8	3.1	8.5	3.6	27.5	2.4	8	2.0	17	2.1	—	—	—	15	24	28	·	·	·	1	12	—	—	—	—	28	—
III	1	1.0	6	1.8	1	2.0	6	1.3	19	1.9	11.5	2.0	8	2.1	2.5	3.4	38	1.2	21 ?	5.9	17	5	7	23	·	·	·	5	11	10	6	·	—	—	—
IV	3	1.3	12.5	3.7	25	2.8	8	2.5	8	1.5	6	1.3	9	1.6	7.5	2.2	11	2.0	35	10.5	26	—	—	—	—	·	·	2	7	9	7	1	—	·	—
V	3	2.7	2	1.0	13	2.2	1.5	2.3	7.5	1.8	5	2.0	25.5	1.7	7.5	1.8	28	1.3	62	14.5	29	·	·	2	1	·	·	3	11	14	12	2	—	·	—
VI	3	1.7	2	2.5	13	1.7	2	2.8	10	2.5	7	2.2	27	1.7	6	1.8	20	1.5	81	21.7	27	·	·	·	6	·	·	3	12	14	12	2	—	·	—
VII	1	2.0	4.5	1.9	5.5	1.7	4	2.2	10.5	2.0	21	1.8	30	2.0	1.5	1.0	15	1.6	50	10.9	17	·	·	·	8	·	·	4	4	16	10	2	—	·	—
VIII	5	2.2	·	·	3	3.0	1	1.5	16	2.6	6.5	2.5	21.5	2.5	15	2.8	25	1.9	75 ?	27.9	1	·	·	·	8	·	·	9	9	10	8	2	—	·	—
IX	0.5	1.0	·	·	1	3.0	4	3.6	29.5	2.5	11	2.1	16.5	2.1	2.5	1.0	25	1.7	28	15.4	11	·	·	·	8	·	·	—	—	4	4	1	—	·	—
X	2	2.2	0.5	2.0	1.5	1.3	1.5	1.7	5.5	1.3	11	2.5	17	2.2	6	2.4	48	1.0	5 ?	2.9	17	·	·	9	·	·	·	—	—	3	2	·	—	·	—
XI	·	·	10	2.6	4	2.9	9.5	2.3	6.5	2.5	12.5	3.0	15.5	2.5	·	·	32	1.7	31	4.6	11	5	10	21	·	·	·	·	18	18	13	·	—	17	—
XII	·	·	4	1.5	2	2.5	4.5	2.7	19	2.8	25.5	3.2	16	3.0	4	1.8	18	2.3	22 ?	8.9	17	2	5	22	·	·	·	·	19	11	8	·	—	—	—
Rok	27	1.4	53.5	1.8	69.5	2.1	55	2.4	156	2.2	146.5	2.4	225	2.3	62.5	1.8	300	1.7	—	27.9	1.VIII	—	—	—	—	·	·	—	—	—	—	—	—	—	—

Chełm Lubelski — φ = 51°07' — λ = 23°30' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	987.5	1004.0	965.6	1014.0	−0.4	−5.8	4.2	30	−20.5	11	−3.8	−1.6	−3.2	−3.0	4.4	4.8	4.5	4.6	90	86	89	88	0.4	0.7	0.5	0.5	7.5	8.1	6.2	7.3
II	988.4	1006.3	965.3	1015.4	−4.0	−10.7	0.4	14	−23.0	7	−7.9	−5.3	−7.2	−6.9	3.3	3.6	3.2	3.4	92	83	85	87	0.3	0.7	0.5	0.5	8.6	7.0	7.2	7.6
III	992.1	1008.6	966.2	1018.4	4.1	−3.8	15.4	30	−17.3	1	−2.5	2.8	−0.5	−0.2	4.9	5.6	5.1	5.2	90	74	83	82	0.5	2.2	1.0	1.2	6.5	6.9	4.9	6.1
IV	986.8	1001.0	969.1	1012.5	10.3	1.8	17.2	26	−3.4	3	3.4	8.7	5.1	5.6	6.9	6.8	7.1	6.9	86	60	79	75	1.1	4.8	1.9	2.6	8.1	7.6	5.1	6.9
V	988.6	1005.1	976.9	1014.0	15.4	6.1	27.5	19	−2.0	4	8.5	13.8	9.9	10.5	9.5	9.3	10.0	9.6	82	58	80	73	2.0	7.2	2.6	3.9	6.5	7.9	6.5	7.0
VI	989.3	996.4	977.3	1014.2	20.6	11.0	28.4	26	5.2	8	14.4	18.9	15.4	16.0	13.9	13.8	14.3	14.0	84	64	82	77	2.8	8.7	3.5	5.0	5.2	6.6	5.8	5.9
VII	988.2	998.1	977.1	1013.0	21.7	11.5	28.9	16	7.1	7, 10	15.5	20.5	15.6	16.8	15.1	14.7	15.1	15.0	85	61	85	77	2.8	10.0	3.1	5.3	4.9	7.0	5.3	5.7
VIII	990.7	999.4	972.7	1015.6	21.0	10.8	29.9	8	7.1	3	13.5	19.4	14.2	15.3	13.8	14.0	13.9	13.9	89	63	86	79	1.9	9.4	2.7	4.7	5.0	6.0	3.3	4.8
IX	992.3	1008.1	981.5	1017.3	21.1	9.1	27.7	3	4.8	16	11.7	19.9	13.3	14.6	12.6	13.9	13.4	13.3	91	61	87	80	1.4	10.0	2.2	4.5	4.2	5.5	2.1	3.9
X	997.6	1012.3	985.3	1023.4	12.1	2.2	21.8	1	−5.2	22	3.9	11.2	6.1	6.8	7.7	9.3	8.5	8.5	94	69	88	84	0.5	4.5	1.2	2.1	6.1	6.2	2.8	5.0
XI	987.6	1005.9	962.4	1013.9	1.1	−4.0	13.8	2	−17.1	17	−2.0	−0.4	−1.5	−1.4	5.1	5.5	5.2	5.3	91	87	88	89	0.5	0.9	0.6	0.7	9.4	8.6	8.1	8.7
XII	982.9	995.7	964.3	1009.0	1.9	−2.9	6.9	11	−17.9	17	−1.1	0.8	−0.7	−0.4	5.2	5.6	5.2	5.3	89	84	86	86	0.7	1.1	0.8	0.9	8.7	7.8	7.1	7.9
Rok	989.3	1012.3	962.4	1015.1	10.4	2.1	29.9	8.VIII	−23.0	7. II	4.5	9.0	5.5	6.1	8.5	8.9	8.8	8.7	89	71	85	82	1.2	5.0	1.7	2.6	6.7	7.1	5.4	6.4

Grabowiec — φ = 51°06' — λ = 21°23'

I	–	–	–	–	0.5	−4.7	4.1	31	−13.2	12	−2.7	−0.4	−2.3	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.6	7.6	8.2
II	–	–	–	–	−3.0	−11.0	2.2	12, 13	−23.1	7	−7.6	−4.0	−7.2	−6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.0	6.5	7.5
III	–	–	–	–	4.7	−3.7	15.4	30	−17.3	1	−2.1	4.1	−0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.7	6.8	7.0
IV	–	–	–	–	10.4	1.9	15.7	7	−1.2	6	3.8	8.9	5.2	5.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	6.1	7.8
V	–	–	–	–	14.5	5.4	26.5	19	−2.9	4	8.6	13.6	9.5	10.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.8	6.8	7.0
VI	–	–	–	–	20.6	10.7	29.4	26	6.0	8	14.5	19.6	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.9	6.5	6.4
VII	–	–	–	–	21.6	10.9	28.2	17	5.8	11	15.8	20.7	14.6	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.8	6.3	6.9
VIII	–	–	–	–	20.4	10.6	29.3	7	6.3	17	13.3	19.2	14.0	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.5	5.7	6.0
IX	–	–	–	–	20.8	8.8	25.9	2	4.2	16	11.3	19.8	13.0	14.3	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	4.3	5.2
X	–	–	–	–	12.2	2.8	21.9	1	−5.6	22	4.9	11.7	6.3	7.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.1	4.3	5.8
XI	–	–	–	–	1.8	−3.8	13.2	2	−22.0	18	−2.1	0.6	−1.0	−0.9	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.7	8.7	8.9
XII	–	–	–	–	2.2	−2.9	9.0	20	−19.0	17	−0.7	1.3	−0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.1	6.8	7.9
Rok	–	–	–	–	10.6	2.1	29.4	26.VI	−23.1	7. II	4.8	9.6	5.5	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	6.4	7.0

Namysłów — φ = 51°05' — λ = 17°43'

I	–	–	–	–	2.6	−2.0	5.7	29	−6.7	8	−0.7	1.9	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.3	7.9	8.4
II	–	–	–	–	−2.4	−9.0	1.6	13	−17.7	6	−5.8	−3.1	−5.8	−5.1	–	–	–	–	–	–	–	–	–	–	–	–	9.9	8.0	7.8	8.6
III	–	–	–	–	6.6	−3.0	17.5	30	−18.0	9	−1.3	5.6	1.1	1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	5.7	4.7	6.3
IV	–	–	–	–	11.9	3.2	16.8	6	−1.4	3	5.0	10.6	7.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	7.0	7.2
V	–	–	–	–	15.4	6.5	24.5	17	−1.3	3	9.5	13.7	10.4	11.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.2	7.6
VI	–	–	–	–	21.6	10.8	32.9	26	5.1	3	15.1	20.1	15.6	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.2	6.6	6.3
VII	–	–	–	–	21.9	11.9	31.3	14	5.7	4	15.6	20.3	15.8	16.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	8.6	7.9
VIII	–	–	–	–	21.8	10.0	30.5	6	4.9	14	13.1	20.2	14.8	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	5.6	5.6
IX	–	–	–	–	20.7	9.3	28.5	3	4.3	21	11.8	19.2	13.6	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.9	3.3	5.2
X	–	–	–	–	13.7	3.0	22.7	2	−4.5	23	4.3	12.7	6.4	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.1	3.9	5.5
XI	–	–	–	–	3.5	−2.9	14.4	1	−15.0	18	−1.1	2.0	−0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.7	9.0	7.7	8.8
XII	–	–	–	–	4.0	−0.9	11.6	19	−9.1	14	0.7	2.4	1.5	1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	7.6	8.3
Rok	–	–	–	–	11.8	3.1	32.9	26.VI	−18.0	9. III	5.5	10.5	6.7	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.0	6.5	7.1

Przedbórz — φ = 51°05' — λ = 19°53'

I	–	–	–	–	0.6	−4.1	4.7	18	−15.2	11	−2.5	−0.1	−1.7	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.2	7.8	8.5
II	–	–	–	–	−2.7	−9.8	2.0	13, 14	−21.6	6	−7.4	−4.1	−6.3	−6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.0	6.4	7.4
III	–	–	–	–	5.4	−3.1	16.3	30	−14.0	1	−1.8	4.5	0.9	1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.8	4.8	5.9
IV	–	–	–	–	10.3	1.7	14.9	20	−3.0	15	3.3	9.0	5.3	5.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.1	5.4	6.4
V	–	–	–	–	14.4	5.4	23.0	18	−3.6	4	8.3	12.9	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.5	5.4	6.1
VI	–	–	–	–	20.7	10.5	31.2	26	5.1	4	14.0	19.3	14.8	15.7	–	–	–	–	–	–	–	–	–	–	–	–	4.3	6.0	4.0	4.8
VII	–	–	–	–	21.4	11.0	29.4	14	5.0	5	14.6	20.0	14.9	16.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.0	4.8	5.4
VIII	–	–	–	–	20.8	10.2	30.2	8	5.7	14	12.6	19.6	14.5	15.3	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.9	4.1	5.0
IX	–	–	–	–	20.6	9.3	26.4	3	4.2	16	11.3	19.0	13.8	14.5	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.8	3.7	4.4
X	–	–	–	–	12.5	2.6	21.8	1	−6.2	22	4.3	11.8	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.3	3.3	4.7
XI	–	–	–	–	2.2	−3.6	12.0	2	−19.3	18	−2.3	0.7	−0.7	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.4	7.4	8.0
XII	–	–	–	–	2.6	−2.2	9.4	20	−14.5	16	−0.4	1.6	0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.8	7.4	8.0
Rok	–	–	–	–	10.7	2.3	31.2	26.VI	−21.6	6. II	4.5	9.5	6.0	6.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.4	6.2

Chełm Lubelski

$H_s = 208$ m $H_b = 209{,}6$ m $h_w =$ 12,5 m anemometr, 12,6 m wiatromierz Wilda

1965

MIESIĄC	ROZKŁAD WIATRU (%, V m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < 10°	Min < 0°	Min < 0°	Max ≥ 25°	Wiatr V V ≥ 10	V ≥ 15	◔	◕	Opad R R ≥ 0,1	R ≥ 1,0	R ≥ 10,0	≡	⊠	K
I	5.5	2.8	6	2.4	8.5	3.7	24	4.6	9	3.8	20.5	5.5	9	5.6	5.5	7.5	5	4.4	33	6.8	20	5	14	28	·	9	·	3	16	16	10	·	5	31	·
II	6	3.5	8.5	4.5	4	3.5	·	·	1	6.0	21	5.8	17	6.4	19.5	4.2	7	4.7	28	4.9	17	14	24	28	·	6	2	·	12	22	9	·	3	28	·
III	3.5	5.7	6	2.9	4	3.1	21.5	4.2	11.5	2.8	17.5	2.7	11.5	3.6	6.5	4.1	11	3.1	26	9.7	17	5	7	25	·	1	·	4	10	12	7	·	6	18	·
IV	5.5	4.8	3.5	3.9	24.5	5.2	34	5.1	5.5	4.0	4.5	4.7	4.5	5.1	5	5.3	3	4.8	39	15.9	28	·	·	12	·	6	·	·	11	12	8	1	3	·	·
V	8.5	2.6	7	2.3	8.5	3.6	10.5	3.5	5.5	2.1	13	3.9	15.5	3.5	14.5	3.0	10	2.8	92	44.1	28	·	·	3	1	1	·	1	11	19	13	2	1	·	5
VI	5.5	3.5	4	3.1	11.5	3.7	9.5	2.8	5.5	3.4	8.5	3.1	19.5	4.3	9	3.3	17	2.9	69	14.7	10	·	·	·	5	2	·	3	9	14	10	1	3	·	3
VII	5.5	1.9	4	2.4	10.5	2.7	11.5	3.0	9.5	3.5	14.5	3.5	23	3.7	4.5	2.4	10	2.8	93	54.7	17	·	·	·	5	1	·	1	5	17	10	2	·	·	4
VIII	4	2.6	5	2.8	3	3.7	7	3.4	1.5	3.7	13.5	2.4	19	3.4	15	2.4	25	2.1	70	18.3	1	·	·	·	9	·	·	8	6	9	8	2	·	·	5
IX	0.5	3.0	·	·	4	3.2	23	3.1	12	3.5	16	2.4	9	2.4	3.5	2.0	22	2.2	30	13.6	11	·	·	·	5	1	1	8	2	6	5	1	1	·	1
X	2	3.0	4	1.5	5.5	3.0	3.5	2.7	4.5	4.4	31.5	4.0	14	3.4	14	2.9	14	2.9	6	4.2	11	·	·	5	·	·	·	6	6	6	1	·	4	·	·
XI	3	5.3	11.5	5.0	13	4.4	17	4.7	5	5.3	16	6.6	17	5.3	4.5	2.2	3	4.9	48	10.0	21	4	12	22	·	7	2	·	21	19	14	1	7	17	·
XII	3	2.5	1.5	3.0	4	4.9	17	5.1	16	6.0	36	5.6	9.5	3.6	3	4.5	3	5.0	22	6.9	18	2	7	24	·	6	1	·	16	10	7	·	5	4	·
Rok	52.5	3.4	61	2.8	101	3.7	178.5	3.5	86.5	4.0	212.5	4.2	168.5	4.2	104.5	3.6	130	3.6	556	54.7	17. VII	30	64	147	25	40	6	34	125	162	102	10	38	98	18

Uwaga. Kierunki i prędkości wiatru: I-VII – wg anemometru M-47, VIII-XII – wg wiatromierza Wilda.

Grabowiec

$H_s = 210$ m $h_w =$ 15 m

I	7.5	3.9	1.5	3.0	1.5	3.7	11	3.3	28	3.8	13	2.8	11	5.1	10.5	4.0	9	3.4	25	4.6	23	3	14	29	·	·	·	·	18	14	9	·	3	26[2]	·
II	13	4.7	4	3.6	1	2.0	0.5	1.0	6.5	4.4	12	6.2	18.5	5.8	21.5	5.3	7	4.8	14	2.7	17	15	23	28	·	5	·	1	14	22	6	·	1	28	·
III	1.5	6.0	7	3.2	2.5	1.8	16.5	2.8	26	2.7	10.5	4.9	10	2.4	11	4.7	8	3.0	37[2]	22.7[2]	2	4	7	23	·	3	·	3	11	12	5	1	5	18	·
IV	3.5	3.4	4	3.4	19.5	3.5	21	3.0	11	2.9	7.5	2.6	6	3.4	11.5	3.0	6	2.9	31	6.3	23	·	·	9	·	·	·	·	16	14	10	·	3	·	2
V	6.5	3.0	6.5	2.8	9	2.9	8.5	3.0	6	2.2	12.5	3.6	12.5	3.1	23.5	3.3	8	2.8	63	13.4	9	·	·	3	1	1	·	·	13	15	10	1	2	·	3
VI	4.5	3.4	2	3.0	9.5	2.3	7	2.6	10.5	3.3	6	3.3	17	3.0	22.5	3.6	11	2.8	70	11.3	27	·	·	·	4	·	·	1	10	13	11	2	·	·	3
VII	4	1.6	3	1.7	5.5	2.3	7.5	2.3	11	2.7	24.5	2.6	25	2.7	5.5	2.1	7	2.3	48	14.4	10	·	·	·	6	·	·	1	9	14	10	2	·	·	4
VIII	3.5	4.9	·	·	·	·	5.5	3.5	14	3.3	9	1.8	20	2.5	22	4.1	19	2.6	129	38.8	26	·	·	·	7	1	·	2	11	15	12	5	·	·	·
IX	0.5	2.0	·	·	·	·	14	4.2	30	3.2	19.5	2.5	10.5	2.9	6.5	2.4	9	2.8	30	16.2	29	·	·	·	2	·	·	5	2	10	6	1	4	·	1
X	4.5	3.2	3.5	2.0	4.5	1.6	3	1.3	13	2.3	15	2.9	17.5	4.1	22	3.1	10	2.6	8	3.2	11	·	·	6	·	1	·	4	8	12	4	·	6	·	·
XI	3	1.2	13	3.5	4	2.9	8	3.9	17	4.8	13	4.7	16.5	3.6	6.5	2.7	9	3.4	29	6.3	11	6	12	22	·	4	·	·	22	19	10	·	3	18	·
XII	1.5	2.0	1	1.0	1	2.0	5.5	4.0	29	5.4	28.5	3.9	12.5	4.2	8	3.4	6	4.0	38	12.0	18	2	5	20	·	3	·	·	19	11	7	1	2	13	·
Rok	53.5	3.3	45.5	2.3	58	2.1	108	2.9	202	3.4	171	3.5	177	3.6	171	3.5	109	3.1	522	38.8	26. VIII	30	61	140	20	18	·	17	153	171	100	13	29	103	13

Namysłów

$H_s = 151$ m. $h_w =$ 12,6 m I–XI, 15,2 m XII

I	1	1.0	2.5	1.4	11.5	1.6	11.5	1.4	21.5	2.0	11.5	2.0	15.5	2.1	6	3.3	12	1.7	30	5.2	10	·	2	28	·	·	·	·	20	17	8	·	6	13	·
II	18	2.3	2	2.8	7.5	1.9	1	1.0	8	2.6	4	2.5	27	2.6	12.5	2.4	4	2.3	24	3.5	14, 17	12	23	28	·	·	·	·	20	20	7	·	1	28	·
III	3	1.7	6	2.3	15	2.0	8	1.6	15	1.3	7.5	1.3	26.5	2.1	8	2.4	4	1.8	24	6.9	2	5	7	20	·	·	·	·	9	14	8	·	3	15	·
IV	7	1.3	11.5	1.3	22.5	2.0	8	1.6	4.5	2.4	9.5	1.8	15.5	1.9	9.5	1.6	2	1.7	43	13.0	19	·	·	6	·	·	·	4	16	12	8	2	2	·	2
V	1	2.0	9.5	1.9	17.5	2.2	6.5	1.7	3.5	1.4	14	1.6	19	2.2	15	1.8	7	1.8	151	25.6	16	·	·	2	·	·	·	2	17	19	17	6	2	·	6
VI	4	2.8	6	1.7	13.5	2.2	12	1.8	5	1.8	10	2.4	20	2.8	10.5	2.0	9	1.9	99	22.8	10	·	·	·	7	1	·	2	10	18	12	4	·	·	6
VII	6.5	1.8	8.5	1.8	5.5	1.8	2.5	1.6	4	3.1	16.5	2.6	30	2.8	14.5	1.8	5	2.2	74	28.5	31	·	·	·	6	·	·	·	18	17	12	1	·	·	3
VIII	6.5	1.0	0.5	2.0	3	2.3	5	2.8	6	2.7	9.5	2.7	13	2.7	28.5	2.2	21	1.8	80	29.8	24	·	·	·	8	1	1	4	6	9	6	4	1	·	1
IX	8	1.0	4.5	1.0	8.5	1.8	12.5	2.3	14	2.3	12	2.4	10.5	2.5	15	1.5	5	1.8	83	49.1	28	·	·	·	3	·	·	6	6	10	7	2	1	·	2
X	23.5	1.1	15.5	1.4	5.5	1.5	5.5	1.4	3.5	1.3	4.5	2.6	18	2.5	13	1.8	4	1.6	3	2.3	16	·	·	8	·	·	·	4	10	3	1	·	7	·	·
XI	15	1.7	15.5	2.2	3	1.7	2.5	2.2	10.5	2.1	14.5	2.9	14	2.5	12	1.8	3	2.1	28	6.2	3	4	8	20	·	·	·	·	22	15	11	·	4	16	·
XII	0.5	2.0	1.5	1.0	3	1.5	5.5	2.2	27	3.0	31	2.6	17.5	2.6	8	1.5	2	2.5	53	16.2	18	·	·	17	·	·	·	·	21	18	15	1	·	6	·
Rok	94	1.6	83.5	1.7	116	1.9	80.5	1.8	122.5	2.2	144.5	2.3	226.5	2.4	149.5	2.0	78	1.9	692	49.1	28. IX	21	40	129	24	2	1	22	175	172	112	20	27	78	20

Przedbórz

$H_s = 235$ m $h_w = 13$ m

I	1	7.0	6	3.7	7	3.6	15	3.1	26	3.4	14	4.4	8.5	3.9	7.5	3.5	8	3.3	34	4.4	2	2	15	26	·	·	·	·	23	13	11	·	4	27	–
II	13	5.3	8.5	5.2	2.5	4.2	2	1.5	11	4.1	15	4.2	24.5	5.3	5.5	6.9	2	4.8	15	2.9	17	10	24	28	·	4	·	1	14	15	5	·	1	28	–
III	3	4.0	6	5.5	5	6.4	13	3.6	26	2.3	11	3.5	10	4.4	7	4.4	12	3.2	25	5.6	3	4	7	21	·	4	·	5	13	11	7	·	6	16	–
IV	4.5	3.7	12.5	5.7	15.5	6.1	20	3.3	9.5	2.6	6	3.3	9.5	3.7	2.5	5.8	10	3.8	52	9.7	23	·	·	6	·	4	·	4	13	14	12	·	·	·	–
V	9	3.3	14	4.1	10	4.8	11.5	3.1	9.5	2.6	11	5.0	11	3.1	9	4.1	8	3.5	96	27.8	24	·	·	4	·	1	·	3	13	16	14	3	1	·	–
VI	6	4.5	6	3.8	9.5	4.6	11	3.3	10.5	3.9	10	3.4	13	4.5	8	3.8	16	3.3	115	24.8	6	·	·	·	5	·	·	10	6	13	13	4	·	·	–
VII	1.5	4.3	2.5	4.6	7	3.3	12	4.2	22	3.3	24.5	4.2	13.5	3.6	1	5.0	9	3.4	62	14.5	21	·	·	·	7	1	·	2	5	15	11	1	1	·	–
VIII	6	3.8	1.5	3.7	2	3.5	15	3.5	20.5	3.7	6	3.8	16	3.9	12	4.2	14	3.2	83	20.3	25	·	·	·	9	2	·	9	7	15	12	3	·	1	–
IX	·	·	·	·	4.5	6.8	22.5	4.1	26.5	3.4	14.5	2.8	16.5	3.3	1.5	3.7	4	3.5	70	30.1	4	·	·	·	2	3	·	8	4	10	8	3	4	·	–
X	4	3.5	8	3.5	4.5	2.1	12.5	2.5	17.5	2.8	8.5	3.1	14.5	4.0	11.5	2.9	12	2.7	7	3.2	31	·	·	6	·	1	·	8	7	5	3	·	7	·	–
XI	2.5	3.6	12.5	6.2	10	5.7	10.5	4.1	18.5	2.9	12	4.5	12.5	3.8	3.5	2.1	8	3.9	32	5.8	28	4	10	23	·	1	·	2	17	14	13	·	5	18	–
XII	1.5	3.0	1.5	3.0	5.5	4.5	14.5	3.8	38	4.9	15.5	4.2	11.5	3.7	4	3.5	1	3.9	41	12.2	18	2	5	22	·	1	·	·	19	12	10	1	·	8	–
Rok	52	3.8	79	4.1	83	4.6	159.5	3.3	235.5	3.2	148	3.9	161	3.9	73	4.2	104	3.5	632	30.1	4. IX	22	61	136	23	22	·	52	141	153	119	15	29	97	–

Laskowice Oławskie

$\varphi = 51°03'$ $\lambda = 17°21'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	2.7	−1.9	6.2	17	−9.1	29	−0.4	2.0	0.1	0.4	5.4	5.7	5.5	5.5	90	81	88	86	0.6	1.4	0.8	0.9	8.2	8.4	7.9	8.2
II	—	—	—	—	−1.0	−8.1	3.7	13	−19.2	6	−4.8	−2.3	−4.5	−4.0	3.9	3.8	3.9	3.9	87	73	85	82	0.5	1.4	0.7	0.9	9.4	7.6	6.5	7.8
III	—	—	—	—	6.8	−3.1	16.7	30	−19.1	9	−1.6	5.6	1.5	1.8	5.3	5.9	6.0	5.7	90	63	84	79	0.6	3.9	1.2	1.9	7.2	5.9	6.2	6.4
IV	—	—	—	—	11.7	3.2	16.8	3, 6	−0.9	15	4.9	10.5	6.8	7.2	7.7	7.7	8.1	7.8	88	62	82	77	1.1	5.2	1.8	2.7	7.5	7.3	6.9	7.2
V	—	—	—	—	15.3	6.6	24.1	17	−2.9	3	9.3	13.7	10.4	11.0	10.4	10.6	10.5	10.5	87	68	82	79	1.5	5.4	2.3	3.1	7.8	8.2	6.3	7.4
VI	—	—	—	—	21.2	11.0	31.7	26	4.2	3	14.9	19.8	15.4	16.4	14.0	13.8	14.6	14.1	82	60	83	75	3.2	10.1	3.1	5.5	5.9	6.6	5.9	6.1
VII	—	—	—	—	21.6	12.0	30.4	14	7.7	10	15.4	20.0	15.5	16.6	14.7	14.5	15.3	14.8	83	62	86	77	3.0	9.7	2.6	5.1	7.6	7.4	6.4	7.1
VIII	—	—	—	—	21.9	10.2	30.9	6	4.9	14, 31	13.4	20.2	14.7	15.8	13.5	12.6	14.2	13.4	87	54	84	75	2.2	12.0	2.9	5.7	4.5	5.7	4.9	5.0
IX	—	—	—	—	20.7	9.1	27.7	2	3.2	22	11.5	19.0	13.2	14.2	12.2	12.7	13.1	12.7	90	59	86	78	1.6	9.8	2.4	4.6	5.6	6.2	3.4	5.1
X	—	—	—	—	13.7	2.4	22.3	1, 2	−6.9	23	3.7	12.4	6.4	7.2	7.9	9.5	8.9	8.8	95	65	89	83	0.5	5.5	1.1	2.4	6.8	5.9	4.6	5.8
XI	—	—	—	—	3.6	−2.8	14.7	1	−11.6	18	−0.8	2.1	−0.1	0.3	5.3	5.7	5.6	5.5	88	77	87	84	0.9	1.9	0.9	1.2	8.5	8.2	7.3	8.0
XII	—	—	—	—	4.1	−0.8	11.6	19	−8.8	14	1.1	2.7	1.6	1.8	5.6	5.9	5.8	5.8	84	79	84	82	1.2	1.7	1.2	1.4	9.2	8.4	7.6	8.4
Rok	—	—	—	—	11.9	3.2	31.7	26.VI	−19.2	6.II	5.6	10.5	6.8	7.4	8.8	9.0	9.3	9.0	88	67	85	80	1.4	5.7	1.8	3.0	7.4	7.2	6.2	6.9

Suchedniów

$\varphi = 51°02'$ $\lambda = 20°50'$

I	—	—	—	—	0.7	−5.7	4.9	30	−17.2	11	−3.2	−0.4	−2.3	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.6	7.1	8.0
II	—	—	—	—	−2.8	−12.8	1.9	12	−27.7	6	−9.1	−4.1	−8.4	−7.5	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.7	7.1	7.3
III	—	—	—	—	5.1	−5.2	16.1	30	−23.2	1	−2.7	3.9	−0.6	0.0	—	—	—	—	—	—	—	—	—	—	—	—	6.9	5.7	5.9	6.2
IV	—	—	—	—	9.9	0.0	15.7	7	−5.3	15	3.0	8.4	3.7	4.7	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.9	5.4	7.2
V	—	—	—	—	14.2	3.8	26.4	19	−6.4	4	7.9	12.9	8.5	9.4	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.8	6.5	6.9
VI	—	—	—	—	20.7	9.2	31.1	26	2.6	4	13.7	19.1	13.6	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	7.1	6.2	6.2
VII	—	—	—	—	21.4	9.6	28.9	16	2.9	5, 6	15.0	20.3	14.1	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.5	7.1	5.5	6.0
VIII	—	—	—	—	20.4	8.8	30.4	8	3.0	17	13.1	19.0	13.2	14.6	—	—	—	—	—	—	—	—	—	—	—	—	4.7	6.6	5.1	5.5
IX	—	—	—	—	20.7	7.4	26.2	2	0.9	16	10.9	18.9	12.5	13.7	—	—	—	—	—	—	—	—	—	—	—	—	3.8	5.2	3.9	4.3
X	—	—	—	—	12.2	1.0	21.9	1	−8.1	22	4.4	11.2	5.3	6.6	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.8	4.1	5.4
XI	—	—	—	—	2.2	−5.0	12.6	2	−24.1	18	−3.0	0.4	−1.6	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.4	8.2	8.3
XII	—	—	—	—	2.2	−3.2	8.8	20	−21.7	17	−1.0	1.2	−0.8	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.1	6.5	7.5
Rok	—	—	—	—	10.6	0.7	31.1	26.VI	−27.7	6.II	4.1	9.2	4.8	5.7	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.2	6.0	6.6

Krasnystaw

$\varphi = 50°59'$ $\lambda = 23°10'$

I	—	—	—	—	0.6	−5.6	7.1	1	−18.7	11	−3.2	−0.8	−2.6	−2.3	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.8	7.7	7.9
II	—	—	—	—	−3.5	−10.7	0.7	12	−23.8	7	−7.5	−4.7	−7.0	−6.6	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.7	7.7	7.9
III	—	—	—	—	4.7	−4.2	15.1	30	−19.2	1	−1.1	3.5	0.3	0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.0	5.8	6.6
IV	—	—	—	—	10.2	2.1	15.9	26	−2.3	3	5.1	8.9	5.3	6.2	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.1	6.0	7.1
V	—	—	—	—	15.3	5.8	26.4	19	−3.2	4	9.8	13.7	10.1	10.9	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.4	6.9	7.0
VI	—	—	—	—	20.9	10.8	32.2	26	5.5	8	15.0	19.4	14.9	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.2	5.6	5.8
VII	—	—	—	—	22.2	11.3	29.4	16	6.5	12	16.1	20.2	15.4	16.8	—	—	—	—	—	—	—	—	—	—	—	—	5.3	7.7	5.9	6.3
VIII	—	—	—	—	21.0	10.3	29.8	8	6.9	16	15.0	19.7	13.8	15.6	—	—	—	—	—	—	—	—	—	—	—	—	5.5	7.0	5.1	5.9
IX	—	—	—	—	21.2	9.0	27.8	3	3.8	17	11.9	19.7	13.5	14.6	—	—	—	—	—	—	—	—	—	—	—	—	4.7	4.2	1.6	3.5
X	—	—	—	—	12.2	2.2	22.0	1	−6.2	22	4.5	11.4	5.9	6.9	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.4	3.0	4.9
XI	—	—	—	—	1.7	−4.5	13.7	2	−23.4	18	−1.7	0.4	−1.3	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.8	7.8	8.6
XII	—	—	—	—	2.0	−2.2	6.9	11	−19.5	17	−0.3	1.1	−0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.1	8.1	8.3
Rok	—	—	—	—	10.7	2.0	32.2	26.VI	−23.8	7.II	5.3	9.4	5.7	6.5	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.0	5.9	6.6

Wojcieszów Górny

$\varphi = 50°57'$ $\lambda = 15°55'$

I	—	—	—	—	2.9	−2.5	8.1	17	−14.5	7	−0.9	1.4	0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.0	7.7	7.3
II	—	—	—	—	−1.2	−8.9	3.6	13	−20.9	6	−5.1	−2.8	−4.7	−4.3	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.2	7.2	7.7
III	—	—	—	—	5.7	−4.1	16.4	30	−17.7	9	−2.2	4.2	0.2	0.6	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.0	6.3	6.0
IV	—	—	—	—	10.7	1.9	17.9	6	−2.3	1	4.0	9.3	5.7	6.2	7.0	7.4	7.2	7.2	86	66	79	77	1.2	4.6	2.1	2.6	6.1	6.7	5.3	6.0
V	—	—	—	—	14.4	5.6	22.9	17	−1.5	3	8.3	12.7	9.1	9.8	9.4	10.1	10.0	9.8	84	69	85	79	1.8	5.0	1.7	2.8	7.1	7.2	6.9	7.1
VI	—	—	—	—	20.1	9.6	31.7	26	3.3	3	12.8	18.5	13.7	14.7	12.7	13.4	13.4	13.2	85	65	85	78	2.3	8.7	2.6	4.5	5.5	7.1	5.4	6.0
VII	—	—	—	—	19.9	11.1	30.1	14	6.1	10	13.7	17.8	14.1	14.9	13.3	14.0	13.6	13.6	83	69	83	78	2.6	6.9	2.8	4.1	7.6	7.8	5.7	7.0
VIII	—	—	—	—	20.4	9.3	30.6	7	4.1	16	11.5	19.0	13.1	14.2	12.3	12.8	13.3	12.8	90	58	87	78	1.6	10.1	2.1	4.6	4.7	6.6	4.4	5.2
IX	—	—	—	—	18.6	8.9	25.3	2	2.6	21	11.0	17.3	11.9	13.0	11.5	12.5	12.2	12.1	87	64	87	79	2.0	7.6	2.0	3.9	4.8	5.2	3.2	4.4
X	—	—	—	—	13.6	2.5	22.0	1	−3.4	23	4.2	12.4	5.4	6.8	7.7	9.0	8.2	8.3	90	61	89	80	0.9	5.8	1.1	2.6	2.9	3.5	2.8	3.1
XI	—	—	—	—	3.7	−2.8	14.1	1	−12.9	23	−0.5	2.0	−0.1	0.3	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.5	7.3	7.3
XII	—	—	—	—	4.2	−1.7	12.6	19	−11.0	15	0.8	2.5	1.6	1.6	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.5	6.7	6.8
Rok	—	—	—	—	11.1	2.4	31.7	26.VI	−20.9	6.II	4.8	9.5	5.8	6.5	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.5	5.8	6.2

Laskowice Oławskie

$H_s = 135$ m $h_w = 13,5$ m

MIESIĄC	ROZKŁAD WIATRU n(D), v(D) — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V: V ≥ 10	V > 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	4	3.5	6.5	3.2	2	2.2	20	3.6	19.5	4.2	11.5	4.6	8	5.1	8.5	3.0	13	3.4	19	4.6	9	·	1	27	·	3	·	·	19	14	5	·	7	10	·
II	13.5	4.5	5.5	3.6	2.5	3.2	2	2.0	7	4.1	13.5	3.9	15	3.9	22	6.1	3	4.4	15	2.8	17	9	20	26	·	3	·	1	16	15	6	·	1	27	·
III	4.5	4.2	7	2.9	4.5	5.6	13.5	3.1	13	2.7	12	3.1	12	5.0	14.5	4.7	12	3.3	25	4.9	2	5	5	20	·	4	·	2	9	14	9	·	4	13	·
IV	8.5	3.6	13	4.6	9.5	4.9	12	4.2	9	4.0	11	2.5	9	3.9	15	4.3	3	3.9	63	19.0	19	·	·	4	·	2	·	2	17	14	10	2	2	·	4
V	7	2.6	14	4.5	10	3.8	8	4.6	4	3.0	9	3.5	12	4.0	23	3.3	6	3.5	120	17.7	29	·	-	2	·	3	1	1	14	19	16	4	1	·	7
VI	9.5	4.5	9.5	3.3	8.5	3.5	10	4.3	11	3.4	9.5	3.4	13	4.0	12	3.7	7	3.5	83	24.7	27	·	-	·	5	5	·	4	9	19	13	3	·	·	5
VII	6.5	3.2	1.5	3.7	4	3.8	9.5	3.1	16.5	3.2	25.5	3.6	12.5	3.1	8	3.4	9	3.0	135	60.0	17	·	·	·	5	·	·	·	9	17	12	3	·	·	9
VIII	11.5	1.6	2.5	2.8	6.5	2.2	13.5	2.4	15	3.1	8	2.6	13.5	2.5	13.5	2.2	9	2.2	69	22.8	24	·	·	·	8	1	1	4	4	10	9	3	1	·	5
IX	1.5	2.0	0.5	1.0	3.5	2.3	33	2.9	24.5	2.6	8.5	1.7	8	1.8	4.5	2.0	6	2.3	40	16.3	28	·	·	·	2	3	·	5	3	10	5	1	2	·	2
X	9.5	1.5	7	1.6	16	2.2	14	1.8	10.5	1.6	7	2.6	13	2.6	10	2.5	6	1.9	3	2.0	16	·	·	12	·	2	·	4	11	4	1	·	8	·	·
XI	0.5	4.0	15	4.3	18	3.2	11.5	3.4	9.5	3.8	10.5	3.2	14	4.3	9	2.6	2	3.5	30	6.1	3	4	9	21	·	4	1	·	18	15	9	·	8	16	·
XII	2.5	2.2	1	3.0	4.5	4.7	17	3.7	24.5	4.8	22	4.8	13	4.1	6.5	2.8	2	4.2	49	13.2	18	·	·	18	·	6	2	·	20	20	12	1	3	6	·
Rok	79	3.1	83	3.2	89.5	3.5	164	3.3	164	3.4	148	3.3	143	3.7	146.5	3.4	78	3.3	651	60.0	17. VII	18	35	130	20	36	5	23	149	171	107	17	37	72	32

Suchedniów

$H_s = 278$ m $h_w = 15,4$ m

I	7	2.3	2.5	2.8	2.5	2.0	2.5	2.4	22.5	3.4	19	3.7	6	3.4	5	4.0	26	2.4	53	6.0	3	5	14	27	·	·	·	2	21	19	14	·	4	31	·
II	11	3.4	3	4.3	·	·	·	·	0.5	3.0	11.5	4.9	15.5	3.9	25.5	3.5	17	3.1	44	7.0	8	15	24	28	·	·	·	1	15	23	15	·	1	28	·
III	6	2.1	4.5	2.2	0.5	4.0	1.5	6.0	22.5	3.9	12	3.0	10.5	3.3	9.5	4.1	26	2.5	27	7.5	3	7	6	24	·	·	·	6	12	14	7	·	4	18	·
IV	2.5	5.0	12	3.5	13.5	4.8	10.5	4.4	3.5	2.4	1.5	3.3	10	3.0	7.5	3.9	29	2.6	41	9.5	23	·	·	17	·	·	·	3	12	13	10	·	·	·	2
V	9	2.8	1.5	3.3	8	4.2	7	2.4	4	3.6	14	3.7	8.5	3.9	13	3.4	28	2.4	93	30.0	25	·	·	7	1	1	1	·	12	17	13	3	1	·	1
VI	7	3.1	8.5	2.6	7	2.4	1	5.0	4.5	4.0	7	3.1	17.5	3.3	17.5	2.9	20	2.4	85	17.8	11	·	·	·	5	·	·	2	9	12	11	5	·	·	1
VII	2	1.2	3.5	2.1	4.5	3.7	0.5	4.0	7	4.3	18	3.4	24	3.9	9.5	3.3	24	2.6	57	25.6	17	·	·	·	7	·	·	2	6	12	9	1	1	·	3
VIII	3.5	3.9	1.5	2.0	·	·	8	4.5	8	3.4	6	3.2	12.5	2.1	21.5	2.9	32	2.0	120	30.0	26	·	·	·	8	·	·	4	11	16	11	5	·	·	·
IX	·	·	·	·	2	3.2	6	4.7	27	3.8	5	2.5	12	2.8	6	2.8	32	2.2	55	18.5	29	·	·	·	3	·	·	10	7	8	7	2	2	·	1
X	6.5	1.8	4.5	2.0	2.5	2.0	1	3.0	3.5	3.3	9	2.3	17	2.6	12	2.5	37	1.5	10	2.8	31	·	·	14	·	·	·	6	7	9	4	·	5	·	·
XI	2.5	3.2	9	3.2	4	1.9	6	3.7	12.5	4.0	10.5	4.7	21.5	3.8	4	2.4	20	2.9	41	8.8	11	7	10	23	·	·	·	2	21	19	14	·	3	18	·
XII	·	·	2.5	2.2	1.5	1.7	1.5	1.0	26.5	4.6	24	4.1	13.5	3.6	10.5	3.0	13	3.3	47	16.0	18	2	6	25	·	2	·	1	14	14	7	1	1	6	·
Rok	57	2.4	53	2.5	46	2.5	45.5	3.4	142	3.6	137.5	3.5	168.5	3.3	141.5	3.2	304	2.5	673	30.0	25.V 26.VIII	36	60	165	24	3	1	39	147	176	122	17	22	101	8

Krasnystaw

$H_s = 190$ m $h_w = 14,5$ m

I	5.5	3.2	1.5	1.7	14	3.1	15.5	3.2	23	3.2	10	4.4	8.5	6.5	2	7.0	13	3.2	30	5.7	3	4	12	27	·	2	1	2	23	17	7	·	8	31	—
II	12	3.7	5.5	2.1	3.5	4.7	·	·	8	6.3	14	4.6	18	4.9	13	4.2	10	3.9	25	6.2	16	13	24	28	·	3	1	·	15	19	8	·	4	28	—
III	1	9.0	10.5	2.3	1.5	5.0	12.5	2.2	26	1.8	10.5	2.0	10	4.0	7	4.7	14	2.2	25	8.7	24	5	5	26	·	·	·	2	11	13	6	·	13	17	—
IV	4.5	4.1	4.5	7.4	17.5	6.9	26.5	6.5	9	1.7	8.5	2.8	4.5	2.4	5	5.2	10	4.7	33	14.8	28	·	·	11	·	7	4	·	12	10	5	1	2	·	—
V	9.5	2.1	2.5	2.2	16	3.1	4.5	1.7	7.5	2.6	9	2.0	12	3.2	14	2.5	18	2.1	81	12.9	28	·	·	2	1	·	·	·	13	17	12	3	·	·	—
VI	6.5	1.5	3.5	3.3	13	3.0	3.5	5.4	8.5	2.5	4.5	2.7	26.5	3.1	10	2.8	14	2.5	67	17.6	10	·	·	·	6	·	·	7	12	13	9	3	1	·	—
VII	1	1.0	2.5	1.0	6.5	3.5	8.5	3.2	14.5	3.7	24.5	3.1	12.5	2.9	5	2.7	18	2.5	65	11.3	17	·	·	·	8	1	·	3	9	17	12	1	·	·	—
VIII	6	2.2	2	9.2	2.5	1.6	13	2.3	15.5	3.9	9	2.8	19.5	3.3	24.5	3.7	1	3.3	43	14.3	2	·	·	·	10	2	1	2	9	10	7	1	·	·	—
IX	2	1.0	0.5	2.0	5	1.9	13.5	2.3	23.5	1.7	17	2.9	9.5	3.5	5	2.0	14	2.0	37	17.5	11	·	·	·	5	1	1	9	·	9	5	2	3	·	—
X	5.5	2.3	1.5	2.7	5	2.4	3	2.7	9.5	2.5	15.5	2.8	20	3.4	11	2.4	22	2.1	5	2.8	11	·	·	5	·	·	·	8	8	9	1	·	12	·	—
XI	6.5	1.2	12.5	3.7	4.5	3.9	16.5	2.5	9	3.1	13.5	3.4	18.5	2.1	4	2.2	5	2.6	42	6.9	21	5	12	22	·	1	·	·	22	21	14	·	5	16	—
XII	3	2.0	2	2.5	1	2.0	9	2.8	26	4.2	30.5	4.0	11.5	3.0	2	2.0	8	3.3	20	7.3	18	2	5	21	·	4	·	·	20	13	6	·	2	5	—
Rok	63	2.8	49	3.3	90	3.4	126	2.9	180	3.1	166.5	3.1	171	3.5	102.5	3.4	147	2.9	473	17.6	10. VI	29	58	142	30	21	8	33	154	168	92	11	50	97	—

Wojcieszów Górny

$H_s = 358$ m $h_w = 23$ m

I	6	2.0	5	2.2	1	1.0	1	4.0	19.5	3.7	17.5	4.6	5	1.4	6	3.8	32	2.3	35	6.6	9	1	2	27	·	1	·	·	16	15	7	·	3	9	·
II	14	3.4	11	4.1	4	1.8	·	·	4	6.8	10	6.2	10	7.2	10	4.5	21	3.6	66	12.3	17	8	22	28	·	4	·	1	15	25	18	1	6	28	·
III	6	3.8	5	3.6	6	1.5	3.5	2.9	14.5	2.2	13	2.9	10	4.4	4	3.2	31	2.0	35	6.2	3	5	7	20	·	1	·	5	11	18	8	·	5	18	·
IV	11	2.6	7	2.1	10	2.4	1	2.0	4	3.8	14	3.4	2	2.5	10	4.8	31	2.1	67	15.6	22	·	·	5	·	·	·	7	14	18	14	1	8	·	1
V	12.5	3.3	5.5	2.4	4	1.5	5	2.0	10	4.8	7	3.7	6	6.2	10	3.7	33	2.3	214	48.3	29	·	·	2	·	2	·	3	15	21	19	6	6	·	3
VI	6	2.7	4	1.8	3	1.3	·	·	9	3.1	11	5.2	3	2.3	13	3.1	41	1.8	87	16.2	13	·	·	·	5	·	·	3	10	19	15	2	3	·	5
VII	7	1.7	3	2.3	·	·	3	2.3	20.5	3.8	9.5	5.4	4	3.8	10	3.5	36	2.2	79	15.3	8	·	·	·	3	1	·	1	11	23	13	3	1	·	9
VIII	9	1.9	4	2.2	1	1.0	2	4.0	9	4.8	4	3.0	·	·	14	3.9	50	1.6	88	35.8	24	·	·	·	6	1	·	2	2	13	9	2	2	·	5
IX	1	4.0	1	4.0	2	1.5	6.5	2.0	21.5	3.1	6	5.2	2	7.0	8	2.9	42	1.8	51	16.6	10	·	·	·	1	·	·	6	5	8	8	1	·	·	1
X	3	2.3	1	2.0	4	1.5	3	1.3	16	2.8	8	3.0	5	2.4	6	2.2	47	1.2	8	4.9	16	·	·	9	·	·	·	15	5	4	3	·	2	·	·
XI	3	1.3	5	2.2	5	1.2	2	1.5	14	4.8	16	6.4	4	3.0	7	3.1	34	2.5	39	8.2	11	2	8	21	·	4	2	2	16	19	9	·	5	17	·
XII	3	2.0	3	1.7	·	·	2	4.0	15.5	6.6	37.5	4.9	11	5.0	2	3.0	19	3.9	55	13.6	18	2	1	21	·	7	·	1	10	17	12	2	4	17	·
Rok	81.5	2.6	54.5	2.6	40	1.2	29	2.2	157.5	4.2	153.5	4.5	62	3.8	100	3.5	417	2.3	824	48.3	29. V	18	40	133	15	21	2	46	130	200	135	18	45	89	24

Opawa - Zwierzyniec φ = 50°57' λ = 17°18' 1965

Miesiąc	Ciśnienie p: P_m	Max	Min	$P_{o.m}$	Temperatura T: Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	3.1	-1.7	7.0	17	-6.8	29	0.0	2.1	0.3	0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.4	8.1	8.1
II	–	–	–	–	-0.8	-7.1	3.9	14	-17.7	6	-4.4	-2.2	-4.2	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.4	7.4	6.9	7.9
III	–	–	–	–	7.0	-2.7	17.1	30	-20.4	9	-1.3	5.8	1.4	1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.5	5.2	5.8
IV	–	–	–	–	12.0	3.7	17.0	3	0.4	1	5.1	10.8	7.1	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.9	7.0	7.1
V	–	–	–	–	15.6	6.8	24.4	17	-0.7	3	9.3	13.9	10.6	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	7.4	7.7
VI	–	–	–	–	21.4	11.8	32.4	26	7.7	3, 13	14.9	19.9	15.9	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.1	5.8	5.8
VII	–	–	–	–	21.8	12.7	31.0	14	7.1	4, 10	15.4	20.2	16.1	17.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	6.6	7.3
VIII	–	–	–	–	22.1	11.2	31.0	6	6.6	31	13.6	20.8	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.3	5.4	5.1
IX	–	–	–	–	21.1	10.0	27.7	2	4.9	22	11.8	19.7	13.7	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.3	3.3	4.5
X	–	–	–	–	14.3	3.5	23.3	1, 15	-4.1	23	4.5	13.1	7.0	7.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.9	4.3	4.9
XI	–	–	–	–	3.8	-2.2	14.6	1	-10.8	18	-0.3	2.4	0.2	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.3	7.2	8.0
XII	–	–	–	–	4.3	-0.4	11.9	19	-8.6	15	1.3	3.0	1.8	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.9	7.6	8.1
Rok	–	–	–	–	12.1	3.8	32.4	26.VI	-20.4	9. III	5.8	10.8	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	6.2	6.7

Bodzentyn φ = 50°57' λ = 20°57'

I	–	–	–	–	–	-5.1	–	–	-15.5	23	-2.7	-0.1	-2.3	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.1	6.2	7.4
II	–	–	–	–	-3.3	-12.4	1.6	13, 14	-24.9	7	-8.2	-4.4	-8.3	-7.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.8	5.8	6.5
III	–	–	–	–	4.7	-4.8	15.4	30	-18.8	1	-1.9	3.7	-0.4	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	4.6	6.0
IV	–	–	–	–	9.6	0.7	15.4	7	-3.5	15	2.7	8.6	4.6	5.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	6.2	7.4
V	–	–	–	–	14.3	4.4	26.5	19	-4.7	3	7.9	12.9	9.2	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.7	6.4	6.9
VI	–	–	–	–	20.3	10.0	30.2	26	3.6	4	14.2	19.2	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.0	6.1	5.8
VII	–	–	–	–	21.1	10.1	28.5	14	4.4	12	15.1	19.8	14.1	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	5.1	6.1
VIII	–	–	–	–	20.1	9.3	29.9	7	3.3	16	13.1	18.5	13.6	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.0	5.2	5.4
IX	–	–	–	–	20.6	8.4	25.5	2	2.7	25	12.1	18.9	13.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.3	3.2	4.3
X	–	–	–	–	11.8	1.6	20.4	1	-6.8	22	4.6	11.0	5.5	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.5	3.3	5.2
XI	–	–	–	–	2.1	-4.9	12.3	2	-23.4	17, 18	-2.7	1.0	-1.7	-1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.5	6.9	7.8
XII	–	–	–	–	2.1	-2.9	8.7	20	-21.1	17	-0.7	1.4	-0.6	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.5	6.0	7.7
Rok	–	–	–	–	–	1.2	30.2	26.VI	-24.9	7. II	4.5	9.2	5.1	6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	5.4	6.4

Silniczka φ = 50°55' λ = 19°46'

I	–	–	–	–	0.9	-5.5	4.9	18	-15.3	11	-2.5	-0.3	-2.1	-1.8	4.7	5.1	4.9	4.9	90	85	91	89	0.6	1.0	0.5	0.7	9.0	8.6	8.2	8.6
II	–	–	–	–	-2.5	-11.0	2.8	13	-24.7	6	-6.9	-3.9	-6.9	-6.2	3.4	3.7	3.3	3.5	87	79	86	84	0.5	1.0	0.6	0.7	7.9	7.3	6.6	7.3
III	–	–	–	–	5.6	-4.9	16.3	30	-17.4	1	-1.6	4.7	-0.8	0.4	5.0	5.3	5.2	5.2	87	61	86	78	0.7	3.7	0.8	1.7	7.6	6.3	6.3	6.7
IV	–	–	–	–	10.3	1.0	14.9	29	-3.9	15	3.7	9.1	4.5	5.4	7.0	7.5	7.3	7.3	87	66	86	80	1.0	4.3	1.2	2.2	7.9	8.0	6.0	7.3
V	–	–	–	–	14.4	4.6	22.4	17, 19	-5.1	3	8.6	13.0	8.9	9.8	9.6	10.0	10.2	9.9	84	66	87	79	1.8	5.4	1.5	2.9	7.0	8.1	6.6	7.2
VI	–	–	–	–	20.8	9.2	31.4	26	3.9	4	14.3	19.3	13.8	15.3	13.7	12.9	13.5	13.4	83	60	85	76	2.9	10.4	2.4	5.2	4.9	6.4	5.8	5.7
VII	–	–	–	–	21.6	10.2	29.6	14	3.8	5	14.6	20.0	13.9	15.6	14.1	13.9	14.1	14.0	84	60	88	77	2.8	10.4	2.2	5.1	6.9	7.4	5.3	6.5
VIII	–	–	–	–	20.9	8.7	30.7	7	3.3	31	12.6	19.6	13.2	14.6	13.1	13.0	13.4	13.2	89	59	88	79	1.7	10.9	2.1	4.9	5.4	6.5	5.8	5.9
IX	–	–	–	–	20.7	7.7	27.4	3	1.8	22	11.2	19.3	11.9	13.6	12.4	13.4	12.7	12.8	92	61	90	81	1.2	9.6	1.5	4.1	6.7	5.9	5.1	5.9
X	–	–	–	–	12.8	1.2	21.4	1	-6.9	22	4.8	12.1	5.6	7.0	8.4	9.6	8.5	8.8	94	67	90	84	0.5	5.1	1.0	2.2	5.5	5.2	4.5	5.1
XI	–	–	–	–	2.5	-4.5	12.5	2	-20.6	18	-2.2	0.5	-1.2	-1.0	5.0	5.6	5.4	5.3	89	82	89	87	0.7	1.3	0.7	0.9	7.7	7.7	8.1	7.8
XII	–	–	–	–	3.1	-2.5	9.7	20	-16.1	16	0.1	1.7	0.2	0.6	5.5	5.5	5.4	5.5	87	78	88	84	0.9	1.6	1.0	1.2	8.9	6.8	7.4	7.7
Rok	–	–	–	–	10.9	1.2	31.4	26.VI	-24.7	6. II	4.7	9.6	5.1	6.1	8.5	8.8	8.7	8.7	88	69	88	82	1.3	5.4	1.3	2.7	7.1	7.0	6.3	6.8

Kraśnik Lubelski φ = 50°55' λ = 22°12'

I	–	–	–	–	-0.2	-5.8	4.2	30	-18.1	11	-3.7	-1.5	-2.6	-2.6	4.3	4.7	4.5	4.5	88	85	87	87	0.5	0.8	0.6	0.6	7.8	8.0	7.3	7.7
II	–	–	–	–	-4.0	-11.2	0.1	17	-22.0	6	-8.2	-5.4	-7.5	-7.2	3.1	3.3	3.0	3.1	87	77	82	82	0.4	0.9	0.6	0.6	8.0	7.8	7.6	7.8
III	–	–	–	–	4.5	-3.6	15.1	30	-15.9	1	-2.1	3.4	0.3	0.5	4.9	5.3	5.4	5.2	88	68	83	80	0.6	2.7	1.1	1.5	6.8	7.1	4.5	6.1
IV	–	–	–	–	10.0	2.1	15.2	7, 18	-1.9	6	3.5	8.7	5.3	5.7	6.8	7.0	7.2	7.0	84	63	79	75	1.2	4.5	1.9	2.5	8.5	8.8	5.2	7.5
V	–	–	–	–	14.5	6.0	25.1	19	-1.6	4	8.2	12.9	9.8	10.2	9.4	9.4	10.0	9.6	83	62	80	75	1.8	6.1	2.4	3.4	7.1	8.4	6.3	7.2
VI	–	–	–	–	20.2	11.4	29.7	26	6.2	3	14.2	18.7	15.2	15.8	13.4	13.5	13.6	13.5	83	64	79	75	3.0	8.8	4.0	5.3	5.7	7.5	5.8	6.3
VII	–	–	–	–	21.2	11.6	27.7	14	6.8	4	15.0	19.8	15.3	16.4	14.5	14.2	14.5	14.4	85	62	82	76	2.8	9.4	3.3	5.2	6.0	7.5	6.7	6.7
VIII	–	–	–	–	20.0	11.1	28.7	8	6.0	3	13.2	18.5	14.6	15.2	13.0	13.5	13.6	13.3	86	64	82	78	2.4	8.8	3.4	4.9	5.9	7.1	4.0	5.7
IX	–	–	–	–	20.3	10.2	26.3	2	6.2	21	12.2	19.0	13.9	14.8	12.1	13.6	13.0	12.9	85	62	82	76	2.5	8.9	3.1	4.8	5.1	5.7	2.1	4.3
X	–	–	–	–	11.6	2.8	21.6	1	-3.6	22	4.3	10.8	6.3	6.9	7.8	8.7	8.2	8.2	92	66	84	81	0.7	4.7	1.6	2.3	6.7	5.6	3.7	5.3
XI	–	–	–	–	1.3	-4.0	12.7	2	-19.8	18	-2.1	-0.2	-1.3	-1.2	5.0	5.2	5.2	5.1	89	82	87	86	0.6	1.3	0.7	0.9	8.2	8.8	7.8	8.3
XII	–	–	–	–	1.4	-3.0	6.4	20	-14.8	17	-1.1	0.2	-0.8	-0.6	5.1	5.2	5.0	5.1	87	82	86	85	0.7	1.1	0.8	0.9	8.3	8.1	7.2	7.9
Rok	–	–	–	–	10.1	2.3	29.7	26.VI	-22.0	6. II	4.4	8.7	5.7	6.1	8.3	8.6	8.6	8.5	86	70	83	80	1.4	4.8	2.0	2.7	7.0	7.5	5.7	6.7

Oława-Zwierzyniec $H_s = 137\ m$ $h_w = 12{,}6\ m$ 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7	2.4	·	·	0.5	1.0	16.5	2.2	15.5	3.0	19.5	3.5	8.5	3.5	3.5	2.9	22	2.2	29	7.0	9	·	1	27	·	1	1	·	18	16	9	·	8	12	·
II	7.5	2.9	1	1.0	·	·	4.5	1.8	4.5	1.6	14	3.4	25	3.4	14.5	3.8	13	2.7	24	5.0	17	5	20	26	·	1	·	1	16	19	9	·	1	27	·
III	4.5	1.6	0.5	2.0	2	2.2	16	1.8	9	2.3	12.5	2.8	13.5	2.9	9	2.7	26	1.7	33	7.2	2	3	4	18	·	·	·	6	10	14	8	·	4	14	·
IV	6.5	1.9	4.5	2.0	8	1.8	16.5	2.4	4.5	2.0	8.5	2.6	15	3.8	11.5	2.7	15	2.2	63	17.3	19	·	·	·	·	1	·	4	17	12	11	2	1	·	3
V	4	2.2	5	2.2	4	2.5	9.5	2.9	3	2.3	9.5	2.5	15.5	3.4	19.5	2.2	23	2.0	124	20.4	29	·	·	1	·	·	·	2	18	20	16	4	·	·	5
VI	3.5	2.7	4	1.6	7	2.7	10	2.4	6.5	3.5	12	2.6	15	3.2	6	3.3	26	2.0	86	17.8	22	·	·	·	7	·	·	5	11	17	13	3	·	·	8
VII	3	2.3	·	·	2.5	1.4	14	1.8	7.5	2.5	24	2.9	14	2.5	5	1.9	23	1.8	143	57.6	17	·	·	·	5	1	·	2	14	19	12	3	2	·	8
VIII	6	1.8	·	·	2.5	3.2	14	2.7	5	3.8	6	1.6	12.5	3.2	14	2.7	33	1.8	55	13.9	24	·	·	·	8	·	·	4	6	12	10	2	4	·	5
IX	·	·	·	·	6	2.2	23	2.6	16	2.9	9	2.8	8.5	2.2	5.5	2.0	22	2.0	47	21.4	28	·	·	·	2	·	·	8	4	11	6	1	7	·	3
X	2.5	1.2	·	·	6	1.9	16.5	1.8	4.5	1.7	10	2.3	2	2.5	11.5	2.3	40	1.1	4	2.4	16	·	·	7	·	·	·	5	6	4	1	·	14	·	·
XI	4	2.1	7	2.2	4.5	1.4	24	1.9	7	2.7	11	2.5	14	2.8	7.5	2.5	11	2.0	36	6.8	3	2	8	18	·	·	·	2	21	16	10	·	5	17	·
XII	·	·	·	·	2.5	1.6	21	2.5	17.5	4.1	25	3.5	16	3.5	4	1.6	7	3.0	50	14.6	18	·	1	16	·	3	1	·	20	17	12	1	6	5	·
Rok	48.5	1.8	22	0.9	45.5	1.8	185.5	2.2	100.5	2.7	161	2.8	159.5	3.1	111.5	2.6	261	2.0	694	57.6	17.VII	10	34	113	22	7	2	39	161	177	117	16	52	75	32

Bodzentyn $H_s = 270\ m$ $h_w = 14{,}8\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2.5	2.0	0.5	1.0	3.5	2.9	6	3.0	4.5	3.6	26	3.1	18.5	3.7	7.5	3.3	24	2.4	39	8.2	17	3	—	26	·	1	·	3	18	10	9	·	5	20	·
II	10	4.4	9.5	5.2	1.5	3.0	·	·	·	·	11.5	7.9	23	4.7	16.5	4.0	12	4.3	16	3.8	14	15	24	28	·	3	2	5	13	13	6	·	·	28	·
III	2	3.2	9	4.1	4	3.9	3	4.0	5	3.4	20.5	3.8	24.5	4.0	10	5.3	15	3.4	21	8.3	21	8	7	23	·	1	·	7	13	9	4	·	4	16	·
IV	1.5	4.3	20.5	4.8	18.5	3.9	4	4.1	3.5	3.9	8.5	3.6	16.5	3.7	6	3.9	11	3.6	35	6.8	23	·	·	13	·	2	·	2	14	13	11	·	·	·	1
V	6	3.8	10	5.4	12	4.8	4	2.5	3.5	2.3	12	3.8	18.5	3.5	23	3.8	4	3.8	83	16.4	29	·	·	5	1	2	2	2	13	17	14	4	3	1	4
VI	3	3.8	11.5	3.3	12	3.5	2	5.8	4.5	3.7	10	4.6	26.5	3.8	16.5	3.3	4	3.5	100	16.9	11	·	·	·	4	2	1	2	7	13	12	7	2	·	3
VII	·	·	3.5	2.0	9.5	2.9	3	4.3	3.5	3.4	20.5	4.0	35.5	3.3	6.5	2.6	11	2.9	28	7.4	8	·	·	·	5	·	·	3	7	15	10	·	·	·	2
VIII	5.5	2.0	5	1.9	3	3.2	7.5	3.3	6.5	3.0	9	3.0	19.5	2.9	23	3.4	14	2.5	117	29.6	1	·	·	·	7	·	·	7	11	15	10	5	·	·	·
IX	·	·	0.5	5.0	3.5	4.0	10	4.1	15	4.0	20	3.4	22.5	3.3	6.5	3.2	12	3.1	50	16.5	29	·	·	·	1	·	·	8	4	9	7	2	3	·	1
X	2.5	3.2	3	3.0	5.5	3.0	2.5	3.8	1	3.5	12	4.1	27.5	3.9	16	2.9	23	2.7	10	5.4	31	·	·	10	·	·	·	7	6	6	3	·	8	·	·
XI	2	2.0	11.5	4.0	7	3.3	4.5	3.1	9	4.3	13.5	4.4	26.5	3.8	4	3.2	12	3.3	27	8.4	11	7	9	22	·	2	·	1	14	13	8	·	7	18	·
XII	2	3.2	9	2.6	1.5	3.0	3	3.3	12	4.0	30.5	4.5	21	4.0	11	3.1	3	3.8	40	10.6	18	2	9	24	·	2	·	·	16	11	8	2	1	11	·
Rok	37	2.7	93.5	3.5	81.5	3.4	49.5	3.4	68	3.3	194	4.2	280	3.7	146.5	3.5	145	3.3	566	29.6	1.VIII	35	—	151	18	15	5	47	136	144	102	20	33	94	11

Silniczka $H_s = 215\ m$ $h_w = 14\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	4.2	4	4.0	9.5	3.1	19.5	2.7	14	3.6	7.5	2.3	13	3.8	7	3.6	14	2.8	44	9.1	9	5	10	28	·	·	·	·	23	14	10	·	5	28	·
II	12.5	3.2	6.5	2.3	1	3.5	·	·	2.5	4.8	15	4.8	21.5	4.8	13	4.9	12	3.7	20	4.0	17	14	23	28	·	1	·	1	14	18	7	·	·	28	·
III	4	3.2	11.5	3.4	4	5.1	21	3.0	3	3.0	8.5	4.1	13	4.4	6	4.6	22	2.8	25	7.2	2	8	7	25	·	·	·	2	12	10	6	·	3	15	·
IV	7.5	2.5	1.5	3.0	25	4.8	13.5	4.4	3.5	3.1	5	4.0	5.5	4.2	8.5	2.9	20	3.1	49	8.5	23	·	·	12	·	1	·	3	13	14	12	·	·	·	3
V	10.5	3.6	10	3.4	8.5	5.4	6.5	2.7	7.5	2.6	12.5	4.0	14	3.2	12.5	3.6	11	3.2	99	17.1	24	·	·	6	·	1	·	1	14	21	15	4	·	·	3
VI	10	2.9	9.5	3.6	8	3.5	13.5	3.0	4	2.0	9.5	3.8	14.5	4.1	9	3.1	12	2.9	105	16.8	14	·	·	·	5	·	·	3	8	14	13	3	·	·	4
VII	2	1.0	4	2.5	10	2.6	9	3.2	12	1.9	13.5	3.8	16.5	3.8	1	2.0	19	2.5	55	16.6	17	·	·	·	7	1	·	3	11	15	9	2	1	·	4
VIII	5	2.6	2.5	2.2	4.5	2.3	12	2.5	7	1.9	5	2.8	12	2.3	17	2.9	28	1.8	95	22.2	25	·	·	·	9	·	·	3	12	16	12	3	·	·	2
IX	1	4.0	·	·	4.5	3.3	23.5	3.7	10.5	2.1	10.5	3.1	9.5	3.1	2.5	2.2	28	2.2	93	41.8	4	·	·	·	3	·	·	4	7	10	7	3	5	·	·
X	7.5	1.9	3	1.7	9	2.7	8	2.1	8.5	2.0	11.5	4.0	14.5	3.3	9	2.7	22	2.1	4	2.6	31	·	·	12	·	·	·	8	8	2	2	·	4	·	·
XI	1.5	5.0	13.5	3.9	7	2.3	12	2.9	6.5	3.2	14	3.6	12.5	3.4	8	2.2	15	2.7	31	6.9	3	6	10	23	·	·	·	·	17	16	9	·	6	16	·
XII	1	3.0	1	2.5	6.5	2.2	15.5	3.1	21	3.4	26	3.3	12	3.7	7	2.6	3	3.1	43	16.0	18	2	3	25	·	·	·	·	15	14	10	1	2	13	·
Rok	67	3.1	67	2.7	97.5	3.4	154	2.8	100	2.8	144.5	3.6	158.5	3.7	100.5	3.1	206	2.7	663	41.8	4.IX	35	53	159	24	4	·	28	154	164	112	16	26	100	16

Kraśnik Lubelski $H_s = 250\ m$ $h_w = 14{,}4\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	3.5	4.0	6	2.4	7	2.7	17	4.7	24.5	5.2	19	5.6	8.5	5.1	7.5	4.7	·	4.7	50	12.6	17	4	15	30	·	4	·	2	17	18	10	1	4	31	·
II	12	2.8	2.5	3.4	4.5	4.1	0.5	5.0	6.5	7.5	18.5	6.6	18.5	4.2	16	3.4	5	4.3	35	5.8	7	15	26	28	·	3	·	1	17	21	10	·	3	28	·
III	0.5	6.0	6	2.7	6	1.5	7	3.9	32	5.4	14	5.0	12.5	3.2	8	3.6	7	3.9	31	6.1	24	4	7	22	·	1	·	5	9	13	9	·	6	21	·
IV	4.5	2.9	3.5	2.4	20.5	5.7	23	4.7	12	4.2	8.5	4.9	8	3.6	6	3.9	4	4.3	47	10.6	26	·	·	10	·	1	·	·	14	14	9	1	2	·	3
V	7.5	2.8	6	1.2	13.5	4.4	7.5	3.9	9	3.3	15	4.0	13	3.5	17.5	2.9	4	3.2	73	12.1	29	·	·	3	1	1	·	1	14	19	14	2	·	·	3
VI	5	2.8	2	3.5	10	3.6	8	3.2	14	3.7	11	2.9	23.5	3.1	13.5	2.7	3	3.1	82	12.5	19	·	·	·	5	·	·	1	11	14	12	3	1	·	5
VII	0.5	4.0	4.5	2.4	6.5	2.2	7	2.6	16.5	3.8	24.5	4.6	19.5	3.4	7	2.6	7	3.3	47	12.9	17	·	·	·	4	·	·	3	12	18	8	2	·	·	5
VIII	5.5	3.6	0.5	1.0	0.5	1.0	5.5	3.1	19.5	4.0	15	3.2	20.5	3.0	20	2.8	6	3.0	128	50.6	26	·	·	·	6	·	·	6	11	14	10	3	·	·	2
IX	·	·	·	·	·	·	12	5.0	41	4.1	16.5	4.1	8.5	2.9	8	2.1	4	3.8	38	18.9	11	·	·	·	2	1	·	8	4	10	5	1	1	·	1
X	4	1.6	2.5	2.0	6	2.8	3	2.5	9.5	4.2	20.5	4.8	23	3.0	11.5	2.0	13	2.8	7	2.5	31	·	·	6	·	·	·	8	9	7	3	·	6	·	·
XI	-	·	7.5	3.2	5.5	6.0	10.5	4.2	19.5	5.7	17.5	5.0	15	3.8	9.5	2.2	5	4.1	38	4.3	12	5	12	23	·	2	·	·	19	21	15	·	4	15	·
XII	1	3.0	2.5	2.4	1	6.0	1.5	5.3	32	5.7	33.5	5.1	11	3.4	6.5	4.5	4	4.8	35	17.1	18	2	6	26	·	1	·	1	17	16	8	1	1	10	·
Rok	44	2.8	43.5	2.2	81	3.2	102.5	4.0	236	4.7	213.5	4.6	181.5	3.5	131	3.1	62	3.8	611	50.6	26.VIII	30	66	148	18	14	-	36	154	185	113	14	28	105	19

Świeradów-Zdrój

$\varphi = 50°54'$ $\lambda = 15°20'$ 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA t												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	p_m	Max	Min	$p_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.0	−2.8	4.1	8, 17	−10.9	7	−1.4	−0.1	−0.8	−0.8	4.9	5.4	5.1	5.1	88	88	89	88	0.7	0.7	0.6	0.7	8.2	8.5	8.1	8.3
II	–	–	–	–	−3.0	−8.1	1.1	12	−13.5	6	−5.8	−4.4	−5.7	−5.4	3.6	3.9	3.4	3.6	87	85	84	85	0.5	0.6	0.6	0.6	8.9	8.4	8.4	8.6
III	–	–	–	–	3.7	−3.1	13.5	30	−16.0	8	−1.5	2.5	−0.7	−0.1	4.8	6.0	4.9	5.2	83	79	80	81	1.0	1.8	1.3	1.4	7.1	6.7	6.1	6.6
IV	–	–	–	–	8.2	1.5	14.4	6	−2.1	1	3.9	7.4	3.8	4.7	6.6	6.8	6.7	6.7	83	68	84	78	1.5	3.7	1.5	2.2	7.5	7.3	6.6	7.1
V	–	–	–	–	12.0	5.3	20.7	17	−0.3	3	8.3	10.8	7.5	8.5	9.0	9.4	9.1	9.2	80	72	86	79	2.1	4.0	1.5	2.5	7.6	7.9	7.7	7.7
VI	–	–	–	–	17.7	9.3	29.8	26	4.6	13	13.5	16.2	12.1	13.5	12.8	13.8	12.3	13.0	83	74	87	81	3.2	5.4	2.2	3.6	6.5	6.3	5.6	6.1
VII	–	–	–	–	17.9	10.6	28.7	14	5.8	11	13.4	16.1	12.8	13.8	12.9	13.4	12.5	12.9	83	73	83	80	2.9	5.4	2.5	3.6	8.1	7.5	6.5	7.4
VIII	–	–	–	–	18.2	9.7	28.3	6	5.0	1	12.8	17.4	12.7	13.9	11.9	11.6	11.9	11.8	81	59	81	74	3.2	9.1	3.1	5.1	5.6	5.5	4.9	5.3
IX	–	–	–	–	16.8	9.3	23.2	2	3.9	21	11.4	15.6	11.9	12.7	11.0	11.3	11.6	11.3	81	64	82	76	2.7	6.9	2.5	4.0	6.4	4.9	4.6	5.3
X	–	–	–	–	12.3	3.9	20.0	1	−2.8	22	5.2	11.4	6.1	7.2	7.3	8.9	7.6	7.9	79	65	79	74	1.9	5.0	2.0	3.0	3.4	3.4	2.9	3.2
XI	–	–	–	–	2.1	−3.0	11.7	8	−12.5	23	−1.1	0.6	−1.0	−0.6	5.0	5.6	5.2	5.3	85	81	82	83	0.9	1.3	0.9	1.0	7.4	8.3	7.5	7.7
XII	–	–	–	–	2.1	−1.3	9.7	19	−8.1	14	−0.2	0.5	0.4	0.3	5.3	5.5	5.6	5.5	86	85	87	86	0.8	1.0	0.9	0.9	8.5	9.2	8.0	8.6
Rok	–	–	–	–	9.1	2.6	29.8	26. VI	−16.0	8. III	4.9	7.8	4.9	5.6	7.9	8.5	8.0	8.1	83	74	84	80	1.8	3.7	1.6	2.4	7.1	7.0	6.4	6.8

Jelenia Góra

$\varphi = 50°54'$ $\lambda = 15°48'$

I	969.6	984.7	950.0	1012.1	2.9	−3.1	8.5	17	−15.0	7	−1.5	1.6	0.0	0.0	4.8	5.2	5.1	5.0	87	76	84	82	0.8	1.7	1.1	1.2	7.6	8.4	8.0	8.0
II	975.8	990.3	952.8	1019.4	−1.3	−10.7	3.5	13	−25.4	6	−6.1	−2.9	−6.0	−5.2	3.6	3.8	3.5	3.6	88	77	85	83	0.5	1.2	0.7	0.8	9.2	8.3	8.0	8.5
III	974.9	990.7	948.9	1017.6	5.9	−6.3	15.4	30	−24.9	9	−4.0	4.6	−0.6	−0.2	4.5	5.3	5.2	5.0	89	61	84	78	0.6	3.8	1.1	1.8	6.8	6.8	6.3	6.6
IV	969.3	990.0	953.9	1010.9	10.5	0.8	17.8	6	−5.3	2	3.1	9.4	4.8	5.5	6.8	7.1	7.2	7.0	88	62	83	78	1.0	5.0	1.5	2.5	6.9	7.5	5.8	6.7
V	973.1	987.0	961.5	1014.3	13.9	4.4	22.5	17	−3.0	3	8.3	12.5	9.1	9.7	9.6	9.6	9.9	9.7	85	67	84	79	1.6	5.2	1.9	2.9	7.2	8.0	7.7	7.6
VI	974.2	985.5	960.8	1014.8	19.7	8.7	31.3	26	1.2	3	13.2	18.2	13.8	14.8	12.9	13.0	13.4	13.1	84	63	84	77	2.6	8.5	2.6	4.6	6.3	7.9	6.2	6.8
VII	972.3	979.7	960.2	1012.6	19.9	10.0	29.9	14	4.0	4	14.2	17.9	13.8	14.9	13.5	13.5	13.7	13.6	82	66	85	78	2.9	7.6	2.4	4.3	8.4	8.0	6.7	7.7
VIII	975.8	983.8	961.5	1016.4	20.4	7.9	30.7	7	2.1	31	11.2	19.2	13.2	14.2	12.5	12.2	13.3	12.7	93	55	87	78	1.3	10.9	2.3	4.8	5.2	2.5	5.2	6.0
IX	973.8	994.5	958.8	1014.6	18.8	7.1	24.6	2	0.8	21, 22	10.1	17.7	11.2	12.6	11.1	12.0	12.1	11.7	89	60	91	80	1.7	8.6	1.6	4.0	6.0	7.0	4.2	5.7
X	982.2	993.7	971.9	1024.3	14.1	−0.3	22.1	1	−7.0	22	1.2	13.2	4.2	5.7	6.8	9.0	8.0	7.9	97	58	93	83	0.3	6.7	0.7	2.6	5.0	4.6	3.2	4.3
XI	969.5	991.0	942.7	1012.0	3.9	−4.5	14.3	1	−17.2	24	−1.4	2.3	−1.1	−0.3	5.1	5.6	5.2	5.3	89	76	88	84	0.8	2.0	0.8	1.2	8.0	8.0	7.5	7.8
XII	964.4	984.8	943.2	1006.5	4.2	−2.4	12.3	19	−15.1	15	0.4	2.6	1.4	1.4	5.3	5.4	5.5	5.4	83	73	80	79	1.2	2.1	1.5	1.6	8.7	7.5	7.9	8.0
Rok	972.9	994.5	942.7	1014.5	11.1	1.0	31.3	26. VI	−25.4	6. II	4.1	9.7	5.3	6.1	8.0	8.5	8.5	8.3	88	66	86	80	1.3	5.3	1.5	2.7	7.1	7.5	6.4	7.0

Ślęża

$\varphi = 50°53'$ $\lambda = 16°43'$

I	–	–	–	–	0.5	−3.9	4.5	12, 17, 18	−9.7	7	−2.1	−1.3	−2.1	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.4	8.7	8.2
II	–	–	–	–	−4.1	−9.2	−0.5	13, 14	−16.2	6	−7.4	−6.1	−7.0	−6.9	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.0	8.0	8.3
III	–	–	–	–	2.7	−3.4	11.5	30	−11.8	8	−1.9	1.4	−1.0	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	7.0	6.7
IV	–	–	–	–	7.3	1.2	13.5	6	−4.6	11	2.7	5.7	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	7.2	7.5
V	–	–	–	–	11.3	4.4	21.0	17	−1.5	2	6.5	9.2	6.8	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	7.3	7.6
VI	–	–	–	–	17.3	9.6	28.6	26	4.1	2	12.3	15.3	12.0	12.9	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	6.8	7.0
VII	–	–	–	–	17.6	10.0	26.8	14	6.1	11	12.4	15.6	12.3	13.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.9	8.0	8.0
VIII	–	–	–	–	17.7	9.9	26.6	6, 7	5.3	1	11.9	16.0	12.3	13.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	4.8	5.4
IX	–	–	–	–	16.5	9.1	21.6	2	4.6	20	11.0	14.6	11.5	12.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.6	4.0	5.0
X	–	–	–	–	10.4	4.0	18.2	2	−2.9	22	5.9	9.1	6.0	6.8	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.6	4.4	4.3
XI	–	–	–	–	1.0	−4.0	11.5	8	−11.5	17	−1.9	−1.0	−2.0	−1.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.6	7.8	8.3
XII	–	–	–	–	−1.1	−3.3	7.3	20	−8.2	14, 15	−1.6	−1.1	−1.3	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	7.8	8.2
Rok	–	–	–	–	8.1	2.0	28.6	26. VI	−16.2	6. II	4.0	6.4	4.3	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.1	6.8	7.0

Olesno

$\varphi = 50°53'$ $\lambda = 18°25'$

I	–	–	–	–	1.7	−3.1	6.3	29	−11.5	7	−1.5	1.1	−1.2	−0.7	5.0	5.9	5.2	5.4	90	89	91	90	0.6	0.8	0.5	0.6	9.3	7.5	8.2	8.3
II	–	–	–	–	–	–	–	–	–	–	−6.5	−3.6	−6.1	−5.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	6.2	−2.9	15.7	30	−18.3	9	−1.5	5.3	1.1	1.5	5.3	5.8	6.0	5.7	88	64	87	80	0.6	3.7	0.9	1.7	8.5	6.5	8.3	7.8
IV	–	–	–	–	11.0	2.7	15.3	6	−1.6	2	4.3	9.8	6.1	6.6	7.6	8.3	8.2	8.0	90	70	86	82	0.8	4.0	1.3	2.0	7.0	7.0	6.2	6.7
V	–	–	–	–	14.5	5.9	23.3	17	−2.2	3	8.8	13.2	9.7	10.4	10.3	10.9	10.5	10.6	89	72	85	82	1.3	4.5	1.8	2.5	7.5	8.2	7.1	7.6
VI	–	–	–	–	21.0	10.5	32.6	26	6.4	7	14.7	19.4	14.8	15.9	13.7	13.7	14.1	13.8	82	62	83	76	3.3	9.8	3.1	5.4	5.2	6.4	6.2	5.9
VII	–	–	–	–	21.2	11.6	30.3	14	5.7	6	14.9	19.6	14.9	16.1	14.6	15.2	14.9	14.9	85	67	87	80	2.7	8.5	2.4	4.5	7.0	7.6	5.9	6.8
VIII	–	–	–	–	21.5	10.2	30.7	8	4.4	31	13.2	19.8	14.4	15.4	13.0	12.4	13.7	13.0	86	56	84	75	2.6	11.8	3.2	5.9	5.6	6.3	5.4	5.8
IX	–	–	–	–	20.7	9.4	28.5	3	3.0	20	11.2	19.2	13.5	14.4	11.9	12.7	13.0	12.5	89	58	84	77	1.7	10.3	2.9	5.0	5.4	5.6	4.2	5.1
X	–	–	–	–	13.4	2.7	23.1	2	−5.6	23	4.1	12.6	6.1	7.2	8.0	9.1	8.7	8.6	93	61	89	81	0.6	6.0	1.1	2.6	5.8	4.8	2.8	4.5
XI	–	–	–	–	2.8	−3.5	13.1	2	−16.0	18	−1.6	1.7	−0.8	−0.4	5.3	5.8	5.6	5.6	91	82	91	88	0.6	1.5	0.6	0.9	8.7	8.2	7.5	8.1
XII	–	–	–	–	2.9	−1.7	10.2	20	−10.2	15	0.2	1.8	0.5	0.8	5.7	5.9	5.6	5.7	88	84	87	86	0.8	1.2	0.9	1.0	8.9	8.8	7.9	8.5
Rok	–	–	–	–	–	–	32.6	26. VI	–	–	5.0	10.0	6.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Świeradów-Zdrój

$H_s = 549$ m $h_w = 13{,}5$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} – N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R – Suma	Max	Data	LICZBA DNI (n) – Temperatura T – Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V – V ≥ 10	V > 15	◔	◕	Opad R – R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	1	2.0	2	1.0	1.5	2.7	8.5	2.9	17.5	4.6	19.5	3.4	12.5	2.4	10.5	4.1	20	2.7	95	18.9	9	1	13	30	·	3	·	·	19	18	11	3	3	26	·
II	7.5	2.3	2	1.2	0.5	1.0	1	1.0	2.5	6.0	12.5	3.1	19	2.8	21	3.2	18	2.3	96	14.6	8	7	25	28	·	1	·	1	21	22	21	1	7	28	·
III	4	1.5	1	2.0	3	1.0	2	3.2	18.5	4.5	19.5	3.0	12.5	2.2	10.5	2.4	22	2.2	66	15.7	3	3	9	19	·	·	·	3	12	17	16	1	4	21	·
IV	0.5	2.0	0.5	2.0	4.5	2.0	7	1.6	12	2.5	19.5	2.3	20.5	1.6	13.5	1.7	12	1.8	120	19.9	22	·	·	4	·	·	·	1	13	19	17	4	5	1	1
V	4	1.8	6.5	1.4	4	3.8	3	1.8	3.5	2.0	22.5	2.2	17.5	2.6	10	2.2	22	1.7	317	57.4	29	·	·	1	·	·	·	1	19	21	21	9	2	·	6
VI	1	1.0	1.5	2.7	9	1.6	2.5	1.2	10	4.8	14	3.0	20.5	2.0	11.5	1.8	20	1.9	125	42.2	11	·	·	·	1	·	·	2	9	16	13	3	3	·	6
VII	2	2.0	0.5	1.0	2	1.5	3.5	1.9	13.5	2.4	34.5	2.2	14.5	2.4	3.5	2.4	19	1.8	170	27.9	17	·	·	·	1	1	·	·	12	22	21	6	2	·	11
VIII	2.5	1.0	·	·	·	·	1	2.0	19.5	3.3	22.5	1.8	8	1.3	13.5	1.2	26	1.5	127	66.2	24	·	·	·	2	1	·	3	6	12	8	4	1	·	2
IX	·	·	1	1.0	·	·	2	3.5	28	4.4	21.5	3.0	8.5	1.6	8	2.0	21	2.5	118	27.8	3	·	·	·	·	5	·	5	8	10	9	4	1	·	1
X	·	·	·	·	·	·	4	1.6	15	2.6	15	2.7	5	3.1	5	2.1	49	1.2	17	6.2	16	·	·	6	·	·	·	14	3	5	4	·	3	·	·
XI	1	2.0	3	2.0	8.5	1.9	5	4.8	16	4.3	23.5	3.7	6.5	2.5	2.5	2.6	24	2.5	82	12.5	21	1	10	22	·	3	·	2	19	21	17	2	3	20	·
XII	·	·	·	·	·	·	1.5	4.0	35.5	6.0	21.5	3.3	16	2.0	0.5	4.0	18	3.5	123	25.5	18	·	3	23	·	5	·	1	23	22	18	4	1	29	·
Rok	23.5	1.3	18	1.2	33	1.3	41	2.5	191.5	3.9	246	2.8	161	2.2	110	2.5	271	2.1	1456	66.2	24.VIII	12	60	133	4	19	·	33	164	205	176	41	35	125	27

Jelenia Góra

$H_s = 342$ m $H_b = 343{,}9$ m $h_w = 16$ m

I	1	4.0	7.5	2.4	8	2.7	17.5	2.4	4	4.8	9	5.6	12	5.1	12	2.9	22	2.7	29	6.8	6	1	2	27	·	1	·	·	19	12	8	·	3	11	·
II	5	2.7	6.5	2.8	5	3.1	7	1.1	0.5	1.0	3.5	6.3	27.5	4.9	16	4.0	13	3.3	50	8.5	8	10	21	28	·	2	·	·	19	25	17	·	3	28	·
III	8	2.6	3.5	2.9	7	2.0	16.5	2.3	2.5	2.6	4.5	3.9	14.5	4.7	10.5	2.7	26	2.2	27	8.1	28	10	6	23	·	·	·	4	14	14	7	·	5	18	·
IV	2	1.8	4.5	3.1	9.5	3.4	8.5	2.2	6.5	3.1	3.5	3.1	16	4.3	10.5	3.8	29	2.3	57	8.6	20	·	·	14	·	·	·	4	15	17	14	·	5	·	1
V	3	3.3	8.5	2.9	8	3.0	13	2.1	1	7.0	6	2.2	19.5	4.7	15	3.7	19	2.7	184	39.2	29	·	·	5	·	·	·	2	17	20	18	5	4	·	4
VI	1	1.0	6.5	2.9	10	2.8	6.5	2.1	1	3.5	4	4.6	18.5	4.8	11.5	3.7	31	2.4	87	27.0	11	·	·	·	4	·	·	1	12	17	14	3	7	·	5
VII	2.5	1.6	2	1.0	4	1.9	3.5	1.1	5.5	1.9	15	3.2	19.5	3.7	12	2.6	29	1.9	74	13.9	31	·	·	·	3	2	·	·	14	22	13	3	1	·	10
VIII	1.5	1.3	3	1.5	3	1.7	6.5	4.1	1	1.5	3.5	1.7	11.5	2.2	11	3.1	52	1.1	98	41.4	24	·	·	·	8	3	·	1	3	8	8	2	6	·	2
IX	0.5	2.0	3	2.0	6.5	3.7	15.5	4.3	3.5	3.6	3	2.7	9	2.8	8	2.9	41	1.8	50	16.2	10	·	·	·	·	3	1	4	9	9	7	1	15	·	1
X	1.5	1.0	2.5	3.0	8.5	3.3	4	2.8	2	2.2	4	5.2	11	3.9	6.5	2.2	53	1.4	8	4.0	16	·	·	16	·	2	·	7	5	7	2	·	13	·	·
XI	·	·	5.5	1.9	9.5	2.8	4	6.8	2.5	4.0	9	5.2	15	4.7	6.5	3.2	38	2.3	26	5.8	3	4	8	24	·	5	·	1	17	21	7	·	3	17	·
XII	0.5	2.0	1	4.0	3	3.3	6.5	3.5	10.5	5.1	16	4.6	27	4.4	4.5	2.1	24	3.1	34	10.1	21	3	·	21	·	7	·	·	17	18	8	1	5	19	·
Rok	26.5	1.9	54	2.5	82	2.8	109	2.9	40.5	3.4	81	4.0	201	4.2	124	3.1	377	2.3	724	41.4	24.VIII	28	37	158	15	25	1	24	161	190	123	15	70	93	23

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Ślęża

$H_s = 718$ m $h_w = 15$ m

I	3.5	3.1	·	·	0.5	3.0	16.5	3.5	14.5	3.8	7	5.1	18	4.7	23	4.8	10	3.8	30	7.4	31	·	15	30	·	6	2	·	19	15	7	·	18	31	·
II	12.5	2.6	1	1.0	·	·	6	4.7	1	2.0	0.5	2.0	9.5	8.2	42.5	5.0	11	4.2	40	6.5	7	12	28	28	·	6	2	·	17	21	11	·	21	28	1
III	21	5.8	·	·	·	·	5	3.1	6.5	3.2	12.5	2.8	11.5	4.0	22.5	5.0	14	3.8	44	8.1	6	4	10	23	·	6	1	4	13	13	10	·	14	19	·
IV	4	4.4	2	2.0	5	6.4	11.5	4.0	5.5	4.6	4.5	4.1	12.5	4.3	37	3.8	8	3.7	86	15.0	20	·	·	3	·	6	1	5	21	18	13	3	19	·	1
V	8.5	5.2	·	·	0.5	6.0	15	4.2	2.5	4.0	2	6.5	16.5	3.5	37	3.9	11	3.6	255	46.0	28	·	·	2	·	4	·	2	21	21	18	9	17	·	6
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	128	27.0	22	·	·	·	2	—	—	2	14	17	17	4	11	·	5
VII	3.5	3.1	·	·	4	5.0	7	3.7	2	3.0	1	4.0	20	3.7	43.5	3.0	12	2.9	92	16.0	8	·	·	·	2	3	·	1	19	22	16	3	6	·	7
VIII	2	3.0	1	1.0	4	1.5	11.5	4.6	6.5	5.9	2	2.0	17.5	3.1	35.5	3.7	13	3.1	89	37.0	24	·	·	·	2	2	1	3	3	14	12	2	9	·	2
IX	2	2.5	-	-	3	4.0	16	5.0	12	4.5	10	3.2	17	2.7	15	3.8	15	3.2	44	13.5	28	·	·	·	·	6	·	5	7	11	8	2	9	·	1
X	4	4.0	1.5	1.0	1.5	1.3	24.5	2.8	3	3.3	4.5	4.2	14	3.5	22	4.4	18	2.8	8	5.0	16	·	·	3	·	3	1	11	4	5	2	·	11	·	·
XI	1	2.0	3	3.3	11.5	4.9	7.5	2.8	7	3.1	14.5	3.3	15	4.3	26.5	3.6	5	3.5	53	9.6	11	3	12	24	·	4	·	1	21	20	12	·	20	20	·
XII	·	·	·	·	0.5	5.0	6	5.5	8.5	6.9	18.5	4.5	22	4.5	30.5	3.1	7	4.0	44	10.2	18	·	13	29	·	3	3	·	20	16	12	1	13	28	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	913	46.0	28.V	19	78	142	6	—	—	34	179	193	138	24	168	126	23

Olesno

$H_s = 238$ m $h_w = 16{,}6$ m

I	7	2.5	2.5	2.4	7	2.5	10	2.5	27.5	3.6	20.5	3.0	7.5	2.8	9	2.7	2	2.9	43	6.0	9	1	7	29	·	1	·	1	23	18	14	·	2?	31?	·
II	10	2.7	4	2.4	3	2.5	1.5	2.3	5.5	3.8	17.5	4.0	19	4.2	21.5	4.4	2	3.8	22	3.2	17	—	—	—	·	1	·	—	—	19	10	·	·	28	·
III	5	3.6	3	3.8	3.5	3.9	13	2.8	17	3.0	16	4.2	20.5	3.5	14	3.6	1	3.4	27	8.4	6	4	6	19	·	2	·	1	19	10	8	·	1?	18	·
IV	6	2.4	8.5	2.6	14	2.9	17.5	1.9	2.5	3.2	10.5	2.3	8.5	3.4	13.5	4.2	9	2.6	48	15.3	23	·	·	6	·	·	·	4	14	16	10	1	5	·	1
V	7.5	2.7	8	2.2	8.5	2.9	5	1.5	3.5	1.9	11	2.5	14	3.4	27.5	2.3	8	2.3	148	33.1	29	·	·	3	·	·	·	3	19	23	18	5	4	·	6
VI	5.5	3.5	8	2.8	7.5	2.8	11	1.7	8	1.9	13.5	2.4	18.5	3.2	12	3.5	6	2.6	101	16.2	10	·	·	·	6	1	·	3	8	18	13	4	1	·	3
VII	3	2.7	·	·	5	2.4	6	2.0	9	2.2	30.5	2.7	23.5	3.6	5	2.6	11	2.5	38	6.7	8	·	·	·	7	·	·	·	11	17	15	·	3	·	7
VIII	5	1.8	3	1.8	3.5	1.6	8	3.1	15	2.9	19.5	1.8	7	3.8	19	3.4	13	2.3	46	17.4	25	·	·	·	9	·	·	7	10	15	8	1	1	·	4
IX	·	·	·	·	2.5	1.4	20.5	2.3	19.5	2.8	17.5	2.9	12	3.0	10	2.8	8	2.4	36	8.7	10	·	·	·	2	·	·	8	6	10	6	·	3	·	1
X	4	1.8	6.5	1.5	13.5	2.0	11.5	1.3	6	1.8	19	2.4	14	2.5	10.5	3.1	8	2.0	4	1.9	16	·	·	7	·	·	·	10	6	4	2	·	9	·	·
XI	2	1.0	10	2.0	11	2.4	11.5	2.2	9.5	2.9	21.5	3.7	11	3.3	10.5	2.4	3	2.7	37	9.1	11	4	9	25	·	1	·	1	21	21	7	·	9	15	·
XII	1	1.5	·	·	2.5	1.6	7	2.4	19.5	3.6	36.5	3.8	14.5	3.7	11	2.6	1	3.4	58	15.7	18	1	3	21	·	3	·	·	22	19	14	1	2	13?	·
Rok	56	2.2	53.5	1.8	81.5	2.4	122.5	2.2	142.5	2.8	233.5	3.0	170	3.4	163.5	3.1	72	2.7	608	33.1	29.V	—	—	—	24	9	·	—	—	190	125	12	40?	105?	22

Cieplice Śl.-Zdrój — φ = 50°52′ — λ = 15°41′ — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA t											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.6	−2.9	8.3	1	−15.9	7	−1.5	1.8	0.1	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.3	8.8	8.4
II	–	–	–	–	−0.9	−9.0	4.4	13	−23.6	6	−5.6	−2.5	−4.7	−4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	9.0	8.2	8.7
III	–	–	–	–	6.2	−5.5	15.8	18, 30	−23.6	9	−3.2	5.0	−0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.2	6.8	7.0
IV	–	–	–	–	10.6	1.8	17.8	6	−3.6	2	4.1	9.4	5.5	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.8	7.5	7.4
V	–	–	–	–	14.2	5.5	21.9	17	−2.6	4	8.9	12.7	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.3	8.1	7.9
VI	–	–	–	–	20.0	8.8	31.8	26	1.7	3	13.4	18.3	13.5	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.3	7.0	7.4
VII	–	–	–	–	20.3	10.5	30.9	14	4.4	4	14.2	18.0	14.0	15.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.9	7.4	8.3
VIII	–	–	–	–	20.6	8.4	30.8	7	2.6	31	12.3	19.2	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.5	6.9	6.7
IX	–	–	–	–	18.9	7.1	24.8	2, 3, 18	0.4	21, 22	10.9	17.6	11.5	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.5	4.7	5.6
X	–	–	–	–	14.5	0.1	22.9	1	−6.6	22	1.7	13.3	4.7	6.1	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.7	3.5	4.1
XI	–	–	–	–	4.2	−3.8	14.6	1	−15.6	24	−1.3	2.5	−0.6	0.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.1	7.7	7.8
XII	–	–	–	–	4.7	−1.4	14.0	19	−14.6	14, 15	0.9	2.8	1.5	1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.4	8.2	8.0
Rok	–	–	–	–	11.4	1.6	31.8	26.VI	−23.6	6.II, 9.III	4.6	9.8	5.7	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.7	7.1	7.3

Słupia Nowa — φ = 50°52′ — λ = 21°05′

I	–	–	–	–	0.1	−4.2	3.9	31	−14.5	11	−2.8	−1.1	−1.7	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.3	7.3	8.0
II	–	–	–	–	−3.4	−9.8	1.6	13	−20.1	6	−8.0	−4.5	−6.5	−6.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	6.0	7.2
III	–	–	–	–	4.3	−2.7	15.6	30	−11.5	1	−0.2	3.2	0.7	1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.6	5.2	6.3
IV	–	–	–	–	9.4	2.0	14.9	7	−1.9	15	4.3	8.2	5.2	5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.2	6.2	7.7
V	–	–	–	–	13.9	5.5	25.7	19	−2.2	3	8.5	13.0	9.4	10.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.8	6.2	7.0
VI	–	–	–	–	20.1	11.3	29.9	26	7.8	3	14.8	19.1	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.1	6.8	6.1
VII	–	–	–	–	20.8	12.2	27.0	14, 16	6.6	5	15.5	19.8	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.0	5.5	6.3
VIII	–	–	–	–	19.8	11.0	28.9	7	7.2	29	14.2	18.7	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.3	5.1	5.6
IX	–	–	–	–	19.9	10.4	24.9	2	5.7	16, 21	13.2	18.8	14.1	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.7	4.0	4.5
X	–	–	–	–	11.5	4.0	20.5	1	−5.0	22	6.4	10.7	7.6	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.4	4.7	5.7
XI	–	–	–	–	1.7	−3.7	12.7	2	−18.3	18	−1.8	0.3	−0.9	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	8.3	8.2
XII	–	–	–	–	1.6	−2.7	7.7	20	−12.4	16	−0.8	0.7	−0.6	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.2	6.5	7.9
Rok	–	–	–	–	10.0	2.8	29.9	26.VI	−20.1	6.II	5.3	8.9	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.0	6.7

Świdnica — φ = 50°51′ — λ = 16°29′

I	–	–	–	–	3.4	−0.9	7.5	17	−7.3	7	0.4	2.3	1.2	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.5	7.9
II	–	–	–	–	−1.2	−7.3	3.5	14	−18.9	6	−4.4	−2.6	−3.8	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.1	7.3	7.8
III	–	–	–	–	5.9	−2.1	16.6	30	−17.2	9	0.0	5.0	1.4	2.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.6	5.9	6.0
IV	–	–	–	–	10.9	3.6	17.4	6	−0.4	1	5.5	9.6	6.5	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	6.9	7.2
V	–	–	–	–	14.4	6.8	23.4	17	−0.8	3	9.6	12.9	10.0	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.0	7.8	7.6
VI	–	–	–	–	20.4	11.4	31.5	26	7.7	7	15.2	19.0	14.7	15.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.6	6.4	6.3
VII	–	–	–	–	20.7	12.2	31.1	14	7.6	4	15.5	18.9	15.0	16.1	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.5	6.8	7.4
VIII	–	–	–	–	21.2	11.0	30.7	6	5.2	16	14.6	19.9	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.0	6.1	5.9
IX	–	–	–	–	19.8	9.9	26.1	3	4.0	22	12.8	18.5	13.4	14.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.4	4.5	5.1
X	–	–	–	–	13.6	3.9	21.6	1	−4.5	23	6.1	12.9	7.0	8.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.9	4.4	4.8
XI	–	–	–	–	4.0	−2.2	14.4	1	−9.9	17	−0.1	2.6	0.3	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.0	7.3	7.7
XII	–	–	–	–	4.6	−0.5	11.5	20	−12.5	15	1.7	3.1	2.1	2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	7.2	7.6
Rok	–	–	–	–	11.5	3.8	31.5	26.VI	−18.9	6.II	6.4	10.2	6.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.8	6.5	6.8

Kielce — φ = 50°51′ — λ = 20°37′

I	979.6	994.2	957.6	1013.5	0.5	−5.6	5.5	30	−22.1	11	−3.5	−0.5	−2.6	−2.3	4.4	5.0	4.7	4.7	89	85	90	88	0.5	0.9	0.5	0.6	7.6	8.5	7.0	7.7
II	982.4	997.7	960.5	1017.0	−2.7	−12.4	2.6	12	−26.6	7	−8.2	−3.9	−8.0	−7.0	3.2	3.6	3.1	3.3	88	76	85	83	0.4	1.1	0.5	0.7	7.9	7.7	6.5	7.4
III	984.2	1000.2	955.7	1017.9	5.2	−4.9	16.9	30	−18.7	1	−2.6	4.1	−0.6	0.1	4.9	5.2	5.2	5.1	89	64	84	79	0.5	3.3	1.0	1.6	7.7	6.1	5.5	6.4
IV	978.3	995.8	962.6	1011.2	10.3	1.1	15.7	29	−3.5	15	3.6	8.5	4.6	5.3	7.1	7.3	7.2	7.2	88	67	84	80	0.9	4.0	1.4	2.1	8.1	7.7	5.0	6.9
V	981.4	996.7	969.3	1013.8	14.8	4.7	27.5	19	−4.6	3	8.3	13.1	8.9	9.8	9.5	9.5	10.1	9.7	84	62	85	77	1.8	6.0	1.7	3.2	7.0	8.2	6.2	7.1
VI	982.2	990.5	970.9	1013.9	21.3	10.2	31.5	26	4.4	3	14.5	19.4	14.6	15.8	13.1	12.4	13.3	12.9	79	57	80	72	3.6	11.0	3.5	6.0	5.1	6.7	6.3	6.0
VII	981.1	988.7	970.0	1012.8	21.8	11.1	29.2	16	4.8	11	15.2	20.0	14.6	16.1	14.1	13.1	14.0	13.7	80	57	83	73	3.6	11.0	3.0	5.9	6.2	7.5	5.3	6.3
VIII	984.1	991.9	974.0	1016.1	20.4	9.6	30.9	7	3.7	31	12.8	19.1	13.5	14.7	13.1	12.5	13.2	12.9	88	59	85	77	1.9	10.7	2.8	5.1	5.0	6.5	4.6	5.4
IX	984.1	1001.5	973.7	1016.2	20.5	8.8	26.0	2, 3	3.2	22	11.2	18.9	13.1	14.1	12.2	13.1	13.1	12.8	91	61	87	80	1.4	9.3	2.3	4.3	5.8	6.5	4.4	5.6
X	990.6	1003.8	979.2	1023.7	12.3	1.3	21.8	1	−6.3	22	3.5	11.3	5.9	6.6	7.8	8.9	8.5	8.4	95	65	89	83	0.4	5.1	1.1	2.2	6.5	6.3	4.4	5.7
XI	979.3	997.7	954.9	1013.1	1.9	−4.1	12.5	2	−17.0	18	−2.5	0.5	−1.2	−1.1	4.9	5.4	5.4	5.2	90	81	90	87	0.6	1.3	0.6	0.8	8.7	8.4	8.2	8.4
XII	974.8	990.8	955.0	1008.2	2.3	−3.1	9.2	20	−17.8	16, 17	−0.5	1.3	−0.4	0.0	5.3	5.3	5.2	5.3	88	78	86	84	0.7	1.6	0.9	1.1	8.0	8.3	7.3	7.9
Rok	981.8	1003.8	954.9	1014.7	10.7	1.4	31.5	26.VI	−26.6	7.II	4.3	9.3	5.2	6.0	8.3	8.4	8.6	8.4	87	68	86	80	1.4	5.4	1.6	2.8	7.0	7.4	5.9	6.8

Cieplice Śl.-Zdrój $H_s = 345$ m $h_w = 13.6$ m   1965

MIESIĄC	ROZKŁAD WIATRU (n_D, V_{nD}) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6.5	3.2	5.5	3.4	4.5	1.7	3.5	1.9	12	6.8	11.5	5.0	8	4.3	6.5	3.5	35	2.7	30	6.0	5, 31	1	2	26	·	1	1	·	21	11	9	·	1	5	·
II	8	3.1	3	2.3	5	2.0	5.5	2.0	0.5	2.0	8	8.5	10	6.0	20	7.2	24	3.9	38	6.7	17	10	19	28	·	4	4	1	22	22	13	·	·	28	·
III	11	3.9	4	2.9	7	1.6	5.5	1.5	6.5	2.2	11.5	5.5	10	3.5	10.5	4.5	27	2.5	19	6.4	2	9	6	23	·	2	·	3	14	9	6	·	2	17	·
IV	5	3.5	7	2.8	11	2.6	5	2.6	7.5	2.9	4	3.5	4	3.5	13.5	5.5	33	2.3	38	8.1	22	·	·	11	·	2	·	2	19	14	11	·	2	·	2
V	8	3.6	5	2.6	12	3.0	3	2.5	5.5	2.5	10.5	4.3	7.5	5.6	16.5	5.8	25	3.0	141	28.4	29	·	·	5	·	4	1	2	19	20	16	5	·	·	3
VI	2	5.5	7	2.6	8	3.2	5.5	2.8	8	1.9	8.5	4.1	10	4.1	14	5.3	27	2.6	104	40.8	11	·	·	·	5	·	·	·	14	14	11	3	·	·	6
VII	4	2.8	3	2.0	1	4.0	7.5	1.5	9.5	1.6	21.5	5.7	14.5	5.0	7	4.6	25	3.0	72	16.0	17	·	·	·	2	5	1	·	19	16	14	2	·	·	8
VIII	3	2.7	7	2.0	4	1.0	11	3.3	15	2.8	9.5	3.4	8.5	5.4	11	4.5	24	2.5	128	48.9	24	·	·	·	8	1	1	2	8	8	8	3	·	·	3
IX	2	1.5	9.5	2.7	10	4.6	11	5.2	16.5	5.9	5.5	5.4	8	4.3	3.5	4.0	24	3.4	55	16.7	10	·	·	·	·	4	3	7	10	7	7	1	2	·	1
X	6.5	3.0	6	3.5	13.5	2.1	14	1.4	8	3.5	5.5	5.6	8.5	5.6	5	4.0	25	2.3	4	3.1	16	·	·	17	·	2	1	10	6	4	1	·	5	·	·
XI	2	2.0	9	3.6	11.5	2.2	4.5	4.2	11.5	4.4	15.5	8.7	9.5	5.6	6.5	5.2	20	3.9	28	4.3	11	6	7	20	·	8	3	1	17	16	8	·	2	17	·
XII	1	1.0	0.5	2.0	6.5	2.5	3.5	5.7	10.5	6.8	38	8.3	11.5	5.1	3.5	4.6	18	5.4	38	12.9	21	2	·	17	·	12	2	1	18	14	9	1	4	12	·
Rok	59	3.0	66.5	2.7	94	2.5	79.5	2.9	111	3.6	149.5	5.7	110	4.8	117.5	4.9	308	3.1	695	48.9	24. VIII	28	34	147	15	45	17	29	187	155	113	15	18	79	23

Słupia Nowa $H_s = 307$ m $h_w = 15$ m

I	10	3.4	·	·	1	4.0	3	4.0	30	5.1	22.5	5.1	12.5	3.6	10	3.7	4	4.3	62	16.3	17	2	16	30	·	2	·	1	19	19	10	1	5	31	·
II	12.5	2.6	1	2.0	·	·	·	·	5	7.2	13.5	6.3	15	4.8	32	4.9	5	4.6	23	3.4	7	10	25	28	·	4	·	3	13	20	10	·	·	28	·
III	8	3.7	3.5	2.0	1.5	2.0	1.5	3.0	30	4.6	16.5	3.9	11	2.8	14	3.6	7	3.5	30	9.5	21	1	7	20	·	1	·	5	13	14	8	·	2	18	·
IV	5	3.0	4	3.4	21	3.7	11	4.9	13	3.6	6.5	3.2	11	3.6	10.5	3.9	8	3.4	32	7.4	23	·	·	7	·	·	·	1	15	9	6	·	1	·	1
V	12.5	3.2	4	2.5	8.5	3.6	5	3.2	9.5	2.2	9	3.7	19.5	3.4	19	3.3	6	3.0	80	22.1	29	·	·	3	1	1	1	1	13	16	14	2	·	1	1
VI	8.5	2.6	2	2.0	6	3.0	6.5	3.0	7.5	3.6	11	2.8	17.5	2.7	19	3.3	12	2.6	94	17.5	11	·	·	·	4	·	·	1	8	13	12	3	3	·	3
VII	2.5	2.6	2	1.5	5.5	2.6	4.5	2.2	14	3.1	28.5	3.1	14.5	3.0	12.5	2.4	9	2.6	79	47.3	17	·	·	·	4	1	1	4	9	15	8	2	·	·	3
VIII	6	3.5	·	·	0.5	2.0	4.5	3.2	18	3.5	11.5	2.7	12	2.2	34.5	2.7	6	2.7	113	41.0	26	·	·	·	5	·	·	5	8	13	8	5	·	·	·
IX	·	·	·	·	·	·	4.5	4.9	42	3.8	19.5	3.2	11.5	2.9	4.5	2.3	8	3.2	33	14.2	29	·	·	·	·	·	·	11	4	12	7	1	·	·	1
X	7	2.3	·	·	2	2.0	4	2.5	11	3.0	13.5	4.0	16.5	3.1	21	2.9	18	2.5	8	4.0	31	·	·	5	·	·	·	6	8	8	2	·	4	·	·
XI	10	2.6	5	4.6	2	3.0	5	3.2	26	4.2	12.5	3.9	8	2.4	11.5	2.1	10	3.0	42	18.6	11	4	11	21	·	·	·	1	20	15	10	1	2	18	·
XII	4	2.5	1	1.0	1	2.0	2	2.5	32.5	5.1	30.5	4.0	13.5	3.8	7.5	3.5	1	4.1	31	5.4	5	2	6	26	·	1	·	·	17	16	10	·	·	19	·
Rok	86	2.7	22.5	1.6	49	2.3	51.5	3.0	238.5	4.1	195	3.8	162.5	3.2	196	3.2	94	3.3	627	47.3	17. VII	19	65	140	14	10	2	39	147	170	105	15	17	115	9

Świdnica $H_s = 230$ m $h_w = 14$ m

I	2.5	2.2	·	·	1	1.0	3.5	2.4	15	3.5	31.5	6.7	11	3.7	5.5	4.8	23	3.7	23	8.2	31	·	1	25	·	7	1	·	16	11	5	·	1	3	·
II	4	3.8	1	3.0	1	3.0	4	2.5	·	·	14	6.0	22.5	3.9	15.5	6.3	22	3.5	26	6.4	17	6	21	27	·	4	2	1	17	21	8	·	1	25	1
III	1.5	3.7	1	5.0	1.5	2.3	4.5	3.2	2	3.0	32	3.1	13	3.0	10.5	3.6	27	2.3	19	4.1	2	4	6	19	·	·	·	3	12	9	5	·	2	12	·
IV	2.5	2.6	3.5	2.4	11.5	2.2	4	1.5	3.5	1.6	16.5	2.7	16.5	3.5	12	3.1	20	2.1	72	9.6	20	·	·	1	·	·	·	2	15	18	13	·	1	·	1
V	3	3.3	6	2.1	9	2.5	3	3.0	2	1.5	14.5	2.9	21	4.5	10.5	3.2	24	2.4	168	37.2	29	·	·	2	·	2	·	2	17	21	18	5	1	·	4
VI	3.5	1.6	6.5	2.8	5	1.8	3	2.0	4.5	2.8	19	4.1	17.5	3.9	10	3.8	21	2.6	97	24.6	8	·	·	·	5	·	·	1	10	12	11	3	·	·	5
VII	2	3.0	2	2.0	3	1.3	4.5	2.3	11	3.4	14.5	4.5	15	2.9	12	3.0	29	2.2	69	20.1	8	·	·	·	3	1	·	·	13	16	11	2	2	·	5
VIII	5	2.2	8.5	1.3	4	3.2	6	3.1	4.5	2.0	16.5	3.2	11	2.6	7.5	3.6	30	1.8	72	33.3	24	·	·	·	8	·	·	1	4	12	8	2	·	·	1
IX	2	3.5	·	·	10	2.5	11.5	3.9	4	4.2	15.5	4.0	8.5	4.2	7.5	3.3	31	2.4	33	21.0	10	·	·	·	2	·	·	7	7	8	4	1	·	·	·
X	5	2.0	5.5	2.3	7.5	2.6	7	2.0	3	3.2	18	4.0	8	4.1	10	2.9	29	2.1	2	1.1	8	·	·	7	·	·	·	8	6	2	1	·	4	·	·
XI	2.5	2.8	7.5	2.8	10	2.9	3.5	3.3	4.5	5.4	20.5	5.5	5.5	4.7	14	4.1	22	3.2	33	7.8	3	·	9	19	·	2	·	2	18	17	9	·	3	13	·
XII	·	·	·	·	3	1.7	5.5	2.8	9	4.1	38	7.2	13	3.8	8.5	3.6	16	4.4	29	8.3	13	2	·	17	·	5	3	·	13	15	7	·	1	4	·
Rok	33.5	2.6	41.5	2.0	66.5	2.2	60	2.7	63	2.9	250.5	4.5	162.5	3.7	123.5	3.8	294	2.7	643	37.2	29. V	12	37	117	18	21	6	27	148	162	100	13	16	57	17

Kielce $H_s = 268$ m $H_b = 270.1$ m $h_w = $ 20.2 m I–VI, 20.8 m VII–XII

I	2	2.5	3.5	3.4	10	3.2	24.5	3.1	15.5	3.0	8.5	3.0	9	3.6	8	3.4	12	2.8	73	9.6	9	5	11	27	·	·	·	3	19	19	15	·	3	31	·
II	6	3.2	5	4.5	5.5	3.0	1	1.0	11.5	3.8	11.5	3.4	25.5	3.6	13	4.6	5	3.5	34	4.3	14	17	24	28	·	1	·	1	14	21	13	·	3	28	·
III	1	6.0	6	2.6	5	2.7	24.5	4.3	14.5	2.6	6	4.2	9	2.7	10	3.6	17	2.8	42	13.1	3	6	6	25	·	·	·	3	11	17	7	1	5	19	·
IV	2	5.5	2.5	4.0	27	4.6	24	2.9	4	2.1	4.5	2.4	9	2.3	7	4.4	10	3.2	31	7.6	30	·	·	11	·	·	·	2	11	15	11	·	·	·	1
V	7	2.8	4	1.8	16	4.2	8	2.5	10.5	2.4	12	3.6	7.5	1.9	16	3.6	12	2.7	109	15.0	29	·	·	5	1	2	·	·	14	18	15	4	2	·	5
VI	5.5	2.1	7	3.1	16	3.2	13.5	3.5	5	3.0	9	3.6	14.5	3.4	12.5	2.9	7	2.9	75	15.5	11	·	·	·	6	·	·	2	9	13	11	3	·	·	4
VII	2	4.5	5.5	3.1	9	3.4	6	3.8	10	3.2	18.5	3.1	22	3.2	7	2.1	13	2.7	41	19.0	17	·	·	·	7	·	·	3	9	14	7	1	1	·	3
VIII	4.5	3.9	1	1.0	3	2.7	12	3.8	16.5	3.5	5	2.1	16.5	2.9	13.5	4.0	21	2.6	103	25.1	26	·	·	·	6	·	·	6	7	15	10	4	1	·	·
IX	·	·	1	3.0	3	2.0	22.5	4.4	23.5	3.4	12	3.0	10	2.9	5	3.4	13	3.0	78	23.4	29	·	·	·	2	·	·	5	7	10	8	3	4	·	2
X	0.5	6.0	3.5	3.4	8	2.0	6.5	3.1	12	3.1	4	3.8	20.5	3.0	12	3.1	26	2.2	10	5.1	31	·	·	13	·	·	·	7	10	9	3	·	9	·	·
XI	·	·	9	5.3	8.5	3.9	11.5	4.1	15	3.8	8.5	5.6	14	2.9	8.5	2.9	15	3.3	37	5.2	3, 11	4	10	23	·	·	·	·	21	21	13	·	3	17	·
XII	1	2.0	3	2.0	5.5	2.1	9.5	3.2	26	3.6	25.5	4.1	16.5	3.3	5	3.2	1	3.4	53	15.5	18	2	5	25	·	·	·	·	16	18	9	2	·	20	·
Rok	31.5	3.2	51	3.1	116.5	3.1	163.5	3.3	164	3.1	125	3.5	174	3.0	117.5	3.4	152	2.9	686	25.1	26. VIII	34	56	157	22	3	·	32	148	190	122	18	31	115	15

Strzyżów

φ = 50°51′ λ = 24°02′ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.5	−6.0	3.0	1	−19.5	11	−3.8	−1.6	−3.3	−3.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−3.5	−11.7	1.8	14	−23.6	7	−8.1	−4.7	−7.4	−6.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	4.1	−4.4	14.7	30	−19.9	1	−2.4	3.1	−0.3	0.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	9.8	2.3	17.8	26	−3.4	3	3.9	8.4	5.3	5.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	15.9	6.4	27.4	19	−1.5	4	9.5	14.3	10.2	11.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	21.3	11.4	29.0	26	4.5	8	15.3	20.0	14.9	16.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	22.1	11.7	29.2	17	7.0	10	15.6	20.5	15.2	16.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	21.4	10.8	30.0	8	6.6	3, 29	13.8	20.0	14.1	15.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	21.2	8.7	27.4	3	2.4	17	11.2	20.3	13.0	14.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.2	1.5	22.3	1	−6.2	22	3.7	11.5	5.4	6.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	1.4	−4.0	14.5	2	−15.9	18	−1.9	0.3	−1.6	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	2.0	−2.7	6.0	10, 20	−18.9	17	−0.9	1.0	−0.7	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	10.6	2.0	30.0	8. VIII	−23.6	7. II	4.7	9.4	5.4	6.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Szklarska Poręba

φ = 50°50′ λ = 15°32′

I	—	—	—	—	1.9	−3.5	7.4	12	−14.9	7	−1.6	0.8	−0.6	−0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.7	8.1	8.5
II	—	—	—	—	−3.0	−9.5	1.1	12	−18.1	6	−6.2	−4.0	−5.8	−5.4	—	—	—	—	—	—	—	—	—	—	—	—	8.8	9.0	7.5	8.4
III	—	—	—	—	3.9	−5.3	13.5	30	−20.1	8	−2.5	3.2	−1.0	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.3	7.6	7.4
IV	—	—	—	—	8.2	0.7	15.7	6	−3.2	2	3.3	7.3	3.4	4.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.0	7.2	7.8
V	—	—	—	—	11.8	4.0	19.7	17	−3.1	3	7.9	10.6	6.9	8.1	—	—	—	—	—	—	—	—	—	—	—	—	7.6	8.0	8.1	7.9
VI	—	—	—	—	17.6	7.9	28.3	26	2.6	3	13.0	16.1	11.6	13.1	—	—	—	—	—	—	—	—	—	—	—	—	6.7	8.0	7.5	7.4
VII	—	—	—	—	17.5	9.5	29.3	14	4.2	4	13.0	15.7	12.6	13.5	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.6	8.3	8.4
VIII	—	—	—	—	17.9	8.0	27.6	7	2.6	14	12.1	16.4	11.7	13.0	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.8	6.1	6.2
IX	—	—	—	—	17.0	7.8	22.3	2	0.6	21	10.9	15.6	11.0	12.1	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.3	5.4	6.3
X	—	—	—	—	12.6	1.2	20.6	1	−5.7	22	3.5	11.7	4.8	6.2	—	—	—	—	—	—	—	—	—	—	—	—	4.5	4.4	4.7	4.5
XI	—	—	—	—	2.3	−4.6	12.6	7	−14.4	23	−1.6	1.0	−2.2	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.4	7.4	8.1
XII	—	—	—	—	2.0	−2.7	8.9	19	−12.2	14	−0.6	0.5	0.0	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.3	8.5	8.5
Rok	—	—	—	—	9.1	1.1	29.3	14. VII	−20.1	8. III	4.3	7.9	4.4	5.2	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.7	7.2	7.4

Lipowa

φ = 50°50′ λ = 21°27′

I	—	—	—	—	−0.2	−5.1	3.5	30	−14.6	11, 12	−3.1	−0.8	−2.7	−2.3	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.4	8.9	8.5
II	—	—	—	—	−3.4	−10.6	2.0	14	−23.6	7	−7.5	−4.1	−7.4	−6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.5	7.6	7.5
III	—	—	—	—	4.0	−3.8	16.2	30	−18.1	1	−1.8	3.3	0.0	0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	6.8	7.6	7.6
IV	—	—	—	—	10.1	2.1	16.5	7	−1.5	16	3.6	8.8	5.4	5.8	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.6	8.6	8.7
V	—	—	—	—	14.8	5.9	27.0	19	−3.0	4	8.6	13.6	9.7	10.4	—	—	—	—	—	—	—	—	—	—	—	—	7.3	8.1	8.0	7.8
VI	—	—	—	—	20.9	10.8	29.6	26	6.1	4, 8	14.4	19.6	14.8	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.4	6.1	5.9
VII	—	—	—	—	21.5	11.4	29.1	16	6.1	5	14.9	20.1	15.0	16.2	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.9	6.5	6.6
VIII	—	—	—	—	20.3	10.5	28.6	7	7.3	17, 18	12.8	18.8	13.7	14.8	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.2	6.9	6.4
IX	—	—	—	—	20.2	9.2	24.6	2	4.5	13	10.9	18.9	13.2	14.0	—	—	—	—	—	—	—	—	—	—	—	—	5.0	5.3	4.8	5.0
X	—	—	—	—	12.0	2.9	21.6	1	−5.8	22	4.7	11.1	6.7	7.3	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.0	6.5	6.6
XI	—	—	—	—	1.5	−3.9	12.6	2	−20.9	18	−2.2	0.3	−1.0	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.1	8.5	8.3
XII	—	—	—	—	1.8	−3.0	6.6	19	−16.4	17	−0.9	0.9	−0.8	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.5	8.6	8.6
Rok	—	—	—	—	10.3	2.2	29.6	26. VI	−23.6	7. II	4.5	9.2	5.6	6.2	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.2	7.4	7.3

Częstochowa

φ = 50°49′ λ = 19°06′

I	980.3	994.1	959.2	1013.1	1.5	−3.8	6.3	29	−11.3	8	−1.8	0.9	−1.3	−0.9	4.8	5.4	4.9	5.0	89	82	87	86	0.6	1.2	0.7	0.8	7.9	7.9	7.3	7.7
II	984.4	998.7	963.2	1018.0	−2.1	−9.5	2.4	13	−21.8	6	−7.1	−3.5	−5.9	−5.6	3.3	3.7	3.4	3.5	87	76	83	82	0.5	1.1	0.6	0.7	8.6	7.5	7.1	7.7
III	985.0	1001.4	956.1	1017.8	6.5	−2.6	16.6	30	−13.0	11	−1.3	5.5	1.1	1.6	5.3	5.7	5.7	5.6	89	62	82	78	0.6	3.8	1.2	1.9	7.2	5.5	4.2	5.6
IV	979.0	998.2	964.5	1011.0	11.1	2.7	15.2	20, 29	−1.5	2	4.0	9.3	6.2	6.4	7.2	7.8	7.9	7.6	88	67	82	79	1.0	4.2	1.7	2.3	7.0	7.5	6.4	7.0
V	982.6	997.2	971.0	1014.2	15.1	6.1	23.1	17	−1.7	3	8.7	13.3	9.9	10.4	9.8	10.7	10.2	10.1	85	66	82	78	1.7	5.4	2.2	3.1	6.2	8.5	5.8	6.8
VI	983.4	993.0	972.8	1014.3	21.3	10.7	31.8	26	6.2	3	13.7	19.3	15.2	15.8	13.4	14.0	14.0	13.8	84	63	81	76	2.5	9.3	3.5	5.1	4.8	6.8	5.8	5.8
VII	982.0	990.1	970.6	1012.9	21.6	11.6	30.2	14	4.6	5	14.5	19.7	15.3	16.2	14.3	14.3	14.9	14.5	86	62	85	78	2.4	9.5	2.9	4.9	7.2	7.5	5.4	6.7
VIII	985.3	992.2	974.1	1016.3	21.7	10.6	31.2	8	5.6	31	12.8	20.2	14.9	15.7	12.9	12.3	13.3	12.8	87	54	79	73	2.2	12.5	4.0	6.2	5.6	6.5	6.5	5.9
IX	984.5	1003.1	971.7	1015.6	20.9	9.6	28.1	3	4.6	22	11.4	19.3	13.7	14.5	12.2	12.9	13.1	12.7	90	59	84	78	1.6	10.1	2.9	4.9	5.5	5.3	4.8	5.2
X	992.0	1004.9	981.4	1024.1	13.5	3.1	22.4	2	−5.0	23	4.7	12.5	6.6	7.6	8.2	9.3	8.7	8.7	92	63	87	81	0.7	5.7	1.4	2.6	5.2	4.1	2.9	4.1
XI	980.2	1000.1	954.3	1012.9	3.0	−3.5	12.4	2	−15.3	18	−1.7	1.8	−0.6	−0.3	5.2	5.6	5.5	5.4	90	77	88	86	0.6	1.8	0.8	1.1	8.0	7.6	7.6	7.7
	975.6	993.6	955.2	1008.1	2.9	−1.8	8.8	20	−9.0	15	0.0	1.9	0.5	0.7	5.5	5.7	5.5	5.6	88	81	86	85	0.8	1.4	0.9	1.0	8.8	8.5	8.3	8.5
Rok	982.9	1004.9	954.3	1014.9	11.4	2.8	31.8	26. VI	−21.8	6. II	4.8	10.0	6.3	6.8	8.5	8.9	8.9	8.8	88	68	84	80	1.3	5.5	1.9	2.9	6.8	6.9	5.9	6.5

Strzyżów — $H_s = 185$ m — $h_w = 12{,}5$ m — 1965

MIESIĄC	ROZKŁAD WIATRU (n, V m/s) N n	N V	NE n	NE V	E n	E V	SE n	SE V	S n	S V	SW n	SW V	W n	W V	NW n	NW V	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	5.5	3.0	3	3.0	13.5	3.3	27.5	3.4	10	4.4	14	4.0	10	4.4	5.5	4.5	4	3.6	36	10.0	20	6	14	27	·	1	·	–	–	–	7	1	–	31	–
II	18	3.3	2	3.5	5	4.7	·	·	2	4.8	6.5	6.8	32	4.7	16.5	3.3	2	4.1	33	5.8	8	16	24	28	·	3	·	–	–	–	10	·	2	28	–
III	1.5	2.7	11	2.7	9	2.7	19.5	3.9	11	3.1	6.5	4.1	11	2.4	15.5	2.8	8	2.8	27	9.2	21	7	6	23	·	1	·	–	–	–	7	·	–	20²	–
IV	7	3.6	2	2.5	33	7.0	25	6.6	3.5	3.3	11.5	3.6	1.5	3.3	5.5	5.3	1	5.7	41	15.6	28	·	·	9	·	9	1	–	–	–	6	2	4	·	–
V	18	2.8	3	2.3	17	3.6	5.5	3.0	6.5	2.8	3.5	4.7	18.5	2.8	17	2.3	4	2.8	61	14.6	28	·	·	3	1	1	·	–	–	–	13	2	·	·	–
VI	7	1.7	1	2.0	16	3.4	9.5	4.4	3.5	5.3	5	2.8	16	3.2	22	2.3	10	2.7	75	16.7	28	·	·	·	6	·	·	–	–	–	11	2	·	·	–
VII	4	2.0	4	2.0	11	2.4	8.5	3.4	4.5	4.3	18	3.6	22	2.7	9	2.6	12	2.6	121	46.0	17	·	·	·	8	·	·	–	–	–	14	4	1	·	–
VIII	11.5	2.5	2	4.5	5.5	3.9	11	4.3	3.5	3.6	7	4.0	23.5	2.5	15	2.5	14	2.6	91	32.7	1	·	·	·	8	1	·	–	–	–	10	3	3	·	–
IX	1.5	1.7	1.5	1.7	12.5	2.4	15.5	3.2	9.5	4.9	8.5	4.3	15	2.5	15	2.8	11	2.7	44	20.0	11	·	·	·	4	1	1	–	–	–	5	2	6	·	–
X	13.5	2.9	2.5	2.8	8.5	2.8	2.5	2.4	3	2.3	9	3.0	27.5	2.5	21.5	3.0	5	2.6	7	5.2	11	·	·	10	·	·	·	–	–	–	1	·	6	·	–
XI	3	2.8	10.5	4.7	14.5	4.1	14	4.0	6.5	2.9	6.5	3.5	24	3.3	10	2.7	1	3.6	61	12.4	21	4	12	24	·	·	·	–	–	–	11	2	4	17	–
XII	4	2.8	1	3.0	4	2.2	11.5	3.8	18	4.6	16	4.2	25	3.3	8.5	2.4	5	3.4	26	8.6	18	3	7	25	·	1	·	–	–	–	4	·	4	3	–
Rok	94.5	2.6	43.5	2.9	149.5	3.5	150	3.5	81.5	3.9	112	4.0	226	3.1	161	3.0	77	3.3	622	46.0	17. VII	36	63	149	27	18	2	–	–	–	99	18	–	99²	–

Szklarska Poręba — $H_s = 640$ m — $h_w = 13{,}7$ m

	N n	N V	NE n	NE V	E n	E V	SE n	SE V	S n	S V	SW n	SW V	W n	W V	NW n	NW V	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	21	1.4	3	1.2	3.5	1.9	0.5	1.0	3.5	9.9	5.5	4.6	8	3.6	48	1.5	·	2.0	69	15.2	8	1	5	30	·	1	1	·	20	12	9	3	2	27	·
II	15	1.5	15.5	1.2	1.5	1.0	·	·	·	·	3	5.3	10	3.0	38	1.9	1	1.9	85	13.7	13	13	23	28	·	·	·	·	19	22	16	2	9	28	·
III	24	1.2	19	1.2	2	1.5	2	1.0	2	5.5	8	4.1	2	5.0	34	1.7	·	1.8	30	8.7	6	5	9	23	·	·	·	3	14	12	9	·	2	21	·
IV	19.5	1.2	30.5	1.1	2	1.0	4	2.0	0.5	4.0	6	3.2	3	3.3	24.5	1.6	·	1.5	126	23.2	17	·	·	12	·	·	·	1	21	17	17	4	6	·	·
V	22	1.5	24.5	1.0	1.5	1.0	2	5.0	·	·	1	6.0	8	5.2	33	2.2	1	2.0	302	55.8	29	·	·	5	·	1	·	2	20	20	19	8	2²	·	5
VI	17.5	2.2	29.5	1.2	1.5	2.3	·	·	1.5	4.0	3.5	2.9	4	4.1	31.5	2.6	1	2.1	134	71.3	11	·	·	·	1	·	·	2	14	16²	12²	2²	3	·	7
VII	14	1.3	14	1.1	·	·	2	4.0	5	6.4	14	4.3	11.5	3.0	32.5	2.4	·	2.7	123	15.1	17	·	·	·	1	1	·	·	20	26	20	4	1	·	9
VIII	21.5	1.2	6	1.0	1.5	2.0	4	3.4	4.5	8.0	7	3.6	9	1.7	39.5	1.7	·	2.1	99	43.3	24	·	·	·	2	1	·	·	7	9	7	4	1	·	3
IX	13	2.0	11.5	2.2	5.5	3.3	5	5.4	5.5	9.5	6	3.8	8	2.5	35.5	1.9	·	2.9	100	24.2	1	·	·	·	·	2	2	3	8	10	9	3	·	·	1
X	22.5	1.6	29.5	1.5	0.5	1.0	0.5	1.0	1	6.0	2	10.2	7	4.2	23	2.3	7	2.0	10	5.7	31	·	·	12	·	2	1	11	6	4	3	·	1	·	·
XI	11.5	1.0	31	1.0	·	·	1	6.0	4.5	5.8	12	7.7	9	4.3	20	3.0	1	2.9	95	28.2	28	5	11	25	·	4	·	2	20	21	17	2	8	19	·
XII	5.5	1.5	1.5	1.0	2	3.2	1	1.5	15	5.5	14	4.2	17.5	2.9	30.5	2.9	6	3.2	128	36.2	5	2	5	26	·	·	·	·	20	18	12	5	1	26	·
Rok	207	1.5	215.5	1.2	21.5	1.5	22	2.5	43	5.4	82	5.0	97	3.6	390	2.1	17	2.3	1301	71.3	11. VI	26	53	161	4	12	4	24	189	187²	150²	37²	36²	121	25

Lipowa — $H_s = 245$ m — $h_w = 16{,}5$ m

	N n	N V	NE n	NE V	E n	E V	SE n	SE V	S n	S V	SW n	SW V	W n	W V	NW n	NW V	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	8	3.0	3	2.7	3	5.0	7	4.4	3.0	4.9	10	2.8	13	6.3	8	6.1	11	4.1	28	4.6	20	3	17	31	·	5	2	1	23	15	11	·	19	31	·
II	9.5	5.5	5	4.8	·	·	·	·	9	5.9	11	4.1	16	5.4	26.5	5.8	7	5.0	34	4.0	27	14	23	28	·	11	4	1	15	19	12	·	9	28	·
III	6.5	5.7	3	3.3	3	3.0	9	4.6	28	3.5	8.5	5.5	10	5.5	10	4.4	15	3.7	12	2.2	6	8	7	21	·	9	3	·	14	11	5	·	16	16	·
IV	2.5	4.8	5	2.8	14.5	7.7	22.5	5.0	7	3.9	11	3.5	8	3.4	6.5	4.6	13	4.1	23	3.2	22	·	·	7	·	9	3	·	21	18	10	·	13	·	2
V	14.5	2.8	1	2.0	13	5.4	6.5	4.0	8.5	3.3	10	2.9	11	4.0	18.5	3.7	10	3.3	57	23.2	29	·	·	3	1	3	2	·	16	13	13	2	6	·	2
VI	11	4.5	2	3.5	5	4.2	8.5	5.6	9.5	3.4	1	4.0	18	4.1	19	4.1	16	3.5	79	14.5	9	·	·	·	5	9	2	3	8	11	11	4	3	·	2
VII	3	1.3	2	4.0	2	2.5	8	4.2	11	3.2	14	3.5	29.5	3.7	4.5	2.9	19	2.8	56	26.1	18	·	·	·	4	7	2	2	10	14	11	2	3	·	4
VIII	4.5	6.0	0.5	10.0	·	·	4	4.2	19	3.6	4	2.5	12.5	2.3	26.5	3.9	22	2.8	137	48.2	26	·	·	·	7	4	·	1	11	12	10	5	3	·	·
IX	1	4.0	·	·	·	·	4.5	4.7	35	3.4	10.5	2.5	9.5	2.1	5.5	2.5	24	2.3	45	25.2	29	·	·	·	·	3	·	6	8	8	4	2	10	·	1
X	2.5	3.2	2	2.0	4	1.8	·	·	14.5	2.6	10.5	3.0	7	2.7	18.5	2.9	34	1.7	2	1.2	11	·	·	6	·	·	·	2	13	3	1	·	14	·	1
XI	·	·	4	2.0	9	3.3	9	3.4	15.5	5.5	8.5	3.3	15	2.8	14	3.6	15	3.1	17	6.3	12	5	11	22	·	3	·	2	19	14	4	·	7	16	·
XII	1	4.0	2	1.0	·	·	6	5.7	20	5.2	28	3.2	20	2.8	7	2.9	9	3.3	25	4.1	6	2	5	25	·	5	1	·	22	15	11	·	1	6	·
Rok	64	3.7	29.5	3.2	53.5	2.7	85	3.8	207	4.0	127	3.4	169.5	3.8	164.5	4.0	195	3.3	515	48.2	26. VIII	32	63	143	17	68	19	18	180	153	103	15	104	97	12

Częstochowa — $H_s = 261$ m — $H_b = 262{,}7$ m — $h_w =$ 21,5 m wiatromierz Wilda; 23 m anemometr

	N n	N V	NE n	NE V	E n	E V	SE n	SE V	S n	S V	SW n	SW V	W n	W V	NW n	NW V	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	8	1.6	1	6.0	4	1.2	5	1.0	34	1.9	28	2.2	8	2.5	2	1.5	3	1.9	52	8.4	31	2	7	27	·	3	1	3	20	14	10	·	2	31	·
II	12.5	4.5	5.5	2.9	5	1.6	1	1.0	2	3.8	17	3.4	20.5	3.0	15.5	2.5	5	2.9	36	6.2	17	12	23	28	·	3	1	1	16	20	9	·	4	28	·
III	4.5	3.0	6.5	2.1	4	1.5	5.5	1.5	26.5	1.2	15.5	3.0	16	2.3	12.5	1.4	2	1.9	28	6.7	6	2	6	20	·	2	·	5	9	13	9	·	3	16	·
IV	7.5	2.7	8	2.6	15.5	2.4	14.5	1.2	14	2.3	6.5	3.2	13	2.2	9	1.4	2	2.1	55	8.8	12	·	·	5	·	3	·	3	15	18	12	·	1	·	2
V	13.5	1.6	5	2.2	11.5	2.5	7.5	1.4	6.5	2.1	19	2.8	17.5	1.8	12.5	1.4	·	2.0	93	16.7	29	·	·	3	·	4	1	2	13	21	16	3	1	·	3
VI	9	3.0	6	2.7	8	2.1	14	2.1	12.5	3.5	16.5	3.4	15	3.0	7	1.3	2	2.7	101	32.4	5	·	·	·	6	1	·	2	9	15	12	3	·	·	3
VII	6	2.0	3	2.0	7	1.7	4	1.6	22.5	2.6	40	2.9	6	3.1	4.5	2.1	·	2.6	46	8.4	18	·	·	·	5	3	·	1	10	16	15	·	1	·	4
VIII	6	2.2	3	2.2	5.5	1.8	10.5	2.6	23.5	2.4	16	2.8	12.5	2.1	15	2.7	1	2.4	47	11.7	24	·	·	·	9	1	·	4	10	15	12	2	1	·	1
IX	0.5	2.0	1	1.0	8.5	2.6	23	2.1	26.5	2.6	15.5	2.2	12.5	2.7	1.5	2.0	1	2.4	70	25.3	4	·	·	·	3	·	·	5	6	11	8	2	1	·	1
X	7	2.5	16	2.7	5.5	2.0	5	2.4	16	3.2	26.5	3.3	11.5	3.9	5.5	3.3	·	3.1	3	1.7	16	·	·	6	·	·	·	11	3	5	1	·	4	·	·
XI	5.5	3.1	9.5	3.3	8	1.2	10	2.1	19	2.4	20	5.1	9	2.1	4	2.0	5	2.8	39	11.2	11	4	10	21	·	4	·	2	18	17	10	1	4	18	·
XII	2	2.2	·	·	7.5	1.3	8	1.9	32.5	3.6	35	4.1	3	2.7	5	2.7	·	3.4	44	12.2	18	·	1	21	·	4	·	·	20	20	11	1	·	14	·
Rok	82	2.5	64.5	2.5	90	1.8	108	1.7	235.5	2.6	255.5	3.2	144.5	2.6	94	2.0	21	2.5	614	32.4	5. VI	20	47	131	23	28	3	39	149	185	125	12	22	107	14

Uwaga. Kierunki i prędkości wiatru: I–VI — wg wiatromierza Wilda, VII–XII — wg anemometru M-47

Szczawno-Zdrój

φ = 50°48′ λ = 16°16′ **1965**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	2.1	−1.9	5.2	17	−11.4	7	−0.7	0.7	0.1	0.0	5.1	5.4	5.3	5.3	88	83	85	85	0.7	1.1	0.9	0.9	9.3	8.9	8.8	9.0
II	—	—	—	—	−1.8	−8.2	2.4	13	−18.5	6	−5.2	−3.6	−4.9	−4.6	3.9	3.8	3.8	3.8	91	82	88	87	0.4	0.9	0.5	0.6	9.2	8.3	8.2	8.6
III	—	—	—	—	5.3	−2.4	15.5	30	−13.5	9	−0.4	3.8	0.8	1.2	5.2	5.4	5.3	5.3	83	66	79	76	1.1	3.2	1.5	1.9	7.5	7.1	7.8	7.5
IV	—	—	—	—	10.1	2.5	17.5	6	−1.0	1	4.8	8.5	5.6	6.1	7.0	7.3	7.0	7.1	81	68	77	75	1.7	4.0	2.2	2.6	7.3	7.5	8.1	7.6
V	—	—	—	—	13.6	6.0	22.1	17	−1.3	2	9.1	12.0	9.0	9.8	9.6	9.9	9.7	9.7	82	70	83	78	2.1	4.5	1.9	2.8	7.6	8.3	8.3	8.1
VI	—	—	—	—	19.6	10.3	30.9	26	5.7	3	14.6	17.9	13.8	15.0	12.9	12.9	13.0	12.9	78	64	82	75	4.1	8.3	3.1	5.2	7.2	8.4	7.3	7.6
VII	—	—	—	—	19.9	11.3	29.8	14	5.5	10	14.5	17.4	14.3	15.1	13.3	13.6	13.5	13.5	79	68	82	76	3.6	7.0	3.1	4.6	9.2	8.8	8.2	8.7
VIII	—	—	—	—	20.1	10.5	29.0	6	4.9	31	13.6	18.7	13.7	14.9	12.6	12.6	13.1	12.8	81	58	83	74	3.4	9.8	3.0	5.4	6.6	7.9	6.6	7.0
IX	—	—	—	—	18.6	9.8	25.0	2	5.0	21	12.6	17.0	13.0	13.9	12.0	12.0	12.4	12.1	82	62	82	75	2.8	7.8	2.9	4.5	6.8	7.4	4.5	6.2
X	—	—	—	—	13.3	3.8	21.2	2	−4.2	22	5.6	12.3	6.7	7.8	8.2	8.8	8.4	8.5	87	60	84	77	1.3	5.9	1.8	3.0	6.7	6.0	5.6	6.1
XI	—	—	—	—	3.3	−2.7	13.4	1	−9.9	23	−0.7	1.5	−0.3	0.0	5.3	5.4	5.3	5.3	87	77	86	83	0.8	1.8	1.0	1.2	8.8	8.6	8.5	8.6
XII	—	—	—	—	3.5	−1.2	10.5	19	−8.7	15	0.7	1.8	1.0	1.1	5.4	5.4	5.4	5.4	83	77	81	80	1.2	1.6	1.3	1.4	9.3	8.0	7.6	8.3
Rok	—	—	—	—	10.6	3.2	30.9	26.VI	−18.5	6.II	5.7	9.0	6.1	6.7	8.4	8.5	8.5	8.5	84	70	83	79	1.9	4.7	1.9	2.8	8.0	7.9	7.5	7.8

Bierutowice (Wang)

φ = 50°47′ λ = 15°44′

I	—	—	—	—	0.4	−4.3	7.2	12	−11.6	7	−2.2	−0.9	−2.0	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.7	8.2	7.9
II	—	—	—	—	−4.6	−10.2	0.3	12	−14.5	28	−7.8	−6.2	−7.6	−7.3	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.5	8.7	8.7
III	—	—	—	—	2.2	−5.2	11.1	30	−15.5	8	−1.8	1.1	−1.6	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.6	6.5	6.2
IV	—	—	—	—	6.4	−0.4	13.6	6	−4.0	1	2.7	5.0	2.3	3.1	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.0	7.0	7.1
V	—	—	—	—	9.9	2.9	17.7	17	−3.6	22	6.6	8.4	5.3	6.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.0	6.7	6.8
VI	—	—	—	—	16.3	8.0	27.3	26	2.8	2	12.0	14.3	11.3	12.2	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.2	5.9	6.1
VII	—	—	—	—	16.3	8.8	27.3	14, 15	4.3	4, 11	11.8	14.2	11.7	12.4	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.6	5.4	6.9
VIII	—	—	—	—	16.3	8.6	26.8	7	3.3	1	12.3	14.8	11.8	12.7	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.0	5.8	5.9
IX	—	—	—	—	15.1	7.6	22.3	3	2.8	21	10.7	13.3	10.4	11.2	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.5	4.4	5.3
X	—	—	—	—	10.2	2.9	18.3	1	−1.8	21	5.9	8.7	5.5	6.4	—	—	—	—	—	—	—	—	—	—	—	—	3.4	4.7	2.8	3.6
XI	—	—	—	—	0.4	−5.0	9.0	1, 8	−13.5	23	−2.5	−1.3	−2.9	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.2	6.8	7.8
XII	—	—	—	—	0.7	−3.8	7.5	19	−7.7	29	−2.3	−1.3	−1.8	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	9.3	8.9	6.9	8.4
Rok	—	—	—	—	7.5	0.8	27.3	26.VI, 4.5.VII	−15.5	8.III	3.8	5.8	3.5	4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.9	6.3	6.7

Karpacz

φ = 50°46′ λ = 15°45′

I	925.9	939.1	907.2	—	1.3	−3.7	7.1	12	−11.2	7	−1.9	−0.3	−1.5	−1.3	4.8	5.3	5.0	5.0	89	87	91	89	0.6	0.8	0.5	0.6	7.0	8.1	7.9	7.7
II	931.0	944.7	909.6	—	−3.4	−9.2	1.4	12	−14.5	6	−6.7	−5.2	−6.3	−6.1	3.5	3.6	3.5	3.5	93	85	90	89	0.3	0.6	0.4	0.4	8.6	8.8	7.1	8.2
III	930.9	946.3	905.7	—	3.0	−4.0	11.9	30	−15.5	8	−2.1	1.7	−1.3	−0.8	4.6	5.0	5.1	4.9	83	70	87	80	1.0	2.4	0.7	1.4	6.0	6.0	7.2	6.4
IV	926.2	945.6	912.0	—	7.5	1.0	13.5	6	−2.1	2	2.9	6.1	3.3	3.9	6.4	7.0	6.7	6.7	86	76	87	83	1.1	2.6	1.1	1.6	6.7	7.7	6.4	6.9
V	930.4	943.5	919.9	—	11.3	4.2	19.5	17	−1.6	3	7.2	9.6	6.7	7.6	8.6	8.9	8.9	8.8	83	75	90	83	1.8	3.3	1.0	2.0	7.1	7.9	7.4	7.5
VI	932.6	943.0	919.0	—	17.2	9.1	28.3	26	4.6	2	12.3	15.4	11.9	12.9	11.8	12.5	11.9	12.1	83	72	85	80	3.0	5.8	2.4	3.7	6.1	7.6	5.9	6.5
VII	931.0	937.9	918.9	—	17.2	9.9	28.1	14	4.7	11	12.4	15.1	12.4	13.1	12.3	12.9	12.3	12.5	84	75	85	81	2.5	4.7	2.4	3.2	8.3	7.7	6.4	7.5
VIII	934.4	941.7	920.8	—	17.0	9.4	26.8	7	4.4	1	12.0	15.7	12.1	13.0	11.3	11.7	11.8	11.6	80	65	84	76	3.2	6.9	2.6	4.2	4.9	6.8	4.8	5.5
IX	932.0	951.2	917.4	—	15.6	8.4	20.7	3	3.0	21	10.8	14.2	11.4	12.0	10.4	11.2	11.4	11.0	80	70	84	78	2.8	5.4	2.4	3.5	5.2	6.2	4.0	5.1
X	939.3	949.1	929.9	—	10.7	3.1	19.0	1	−2.5	21	5.1	9.8	5.7	6.6	7.1	8.3	7.3	7.6	78	67	77	74	2.0	4.2	2.1	2.8	3.6	4.5	3.2	3.8
XI	925.8	946.1	900.4	—	1.6	−3.7	10.9	1	−12.6	23	−1.7	−0.3	−1.5	−1.2	4.8	5.3	5.0	5.0	85	85	87	86	0.9	1.0	0.9	0.9	7.2	8.1	6.7	7.3
XII	921.0	939.1	901.0	—	1.8	−2.7	9.7	19	−8.4	14	−0.7	−0.1	−0.4	−0.4	5.2	5.2	5.2	5.2	88	84	86	86	0.7	1.0	0.8	0.8	8.7	7.7	7.5	8.0
Rok	930.0	949.1	900.4	—	8.4	1.8	28.3	26.VI	−15.5	8.III	4.1	6.8	4.4	4.9	7.6	8.1	7.8	7.8	84	76	86	82	1.7	3.2	1.4	2.1	6.6	7.3	6.2	6.7

Dobrogoszcz

φ = 50°46′ λ = 17°01′

I	—	—	—	—	2.7	−1.4	6.5	17	−7.0	7	0.1	2.1	0.4	0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.3	7.6	7.5
II	—	—	—	—	−1.5	−7.8	3.9	14	−19.6	6	−4.5	−2.6	−4.6	−4.1	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.1	7.0	7.6
III	—	—	—	—	6.1	−2.8	16.7	30	−18.5	9	−0.8	5.2	1.3	1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.9	7.8	7.4
IV	—	—	—	—	11.4	3.1	17.2	3	−1.5	2	5.0	10.4	6.6	7.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.0	7.7	7.3
V	—	—	—	—	14.7	6.9	23.1	17	−1.0	3	9.5	13.4	10.1	10.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.5	7.5	7.5
VI	—	—	—	—	20.6	10.9	31.0	26	5.3	13	14.9	19.4	15.0	16.1	—	—	—	—	—	—	—	—	—	—	—	—	5.4	6.0	5.0	5.5
VII	—	—	—	—	21.1	12.3	30.1	14	7.4	6	15.6	19.4	15.4	16.4	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.1	6.4	6.9
VIII	—	—	—	—	21.2	10.6	30.3	6	5.3	16	13.8	19.9	14.5	15.7	—	—	—	—	—	—	—	—	—	—	—	—	5.0	5.5	4.4	5.0
IX	—	—	—	—	20.0	10.0	27.3	2	4.1	30	12.4	18.8	13.2	14.4	—	—	—	—	—	—	—	—	—	—	—	—	4.6	5.8	3.8	4.7
X	—	—	—	—	13.5	3.7	21.5	2	−5.1	22	5.3	12.6	7.3	8.1	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.0	2.7	4.0
XI	—	—	—	—	3.8	−2.2	15.1	2	−11.1	17	0.1	2.5	0.3	0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.6	7.3	7.7
XII	—	—	—	—	4.3	−0.8	11.9	19	−13.2	15	1.5	3.1	1.6	2.0	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.3	6.5	7.1
Rok	—	—	—	—	11.5	3.5	31.0	26.VI	−19.6	6.II	6.1	10.4	6.8	7.5	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.6	6.1	6.5

Szczawno-Zdrój — $H_s = 415\,m$ — $h_w = 13\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (D,V=D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥19	≥15	◔	◕	Opad R ≥0.1	≥10	≥100	≡	⊠	K ⊠
I	14.5	1.9	4	2.4	·	·	0.5	5.0	6.5	10.0	25	7.8	16	4.2	26.5	1.9	·	4.5	31	8.4	31	1	5	27	·	7	1	·	24	14	7	·	·	12	·
II	22.5	1.8	4	2.0	1	5.0	·	·	1	2.0	7	9.1	12.5	6.0	34	3.4	2	3.7	53	13.5	17	6	21	28	·	5	·	·	20	25	15	1	1	28	·
III	16.5	2.5	6	2.9	·	·	0.5	2.0	5.5	5.5	21.5	5.4	12.5	5.0	29.5	2.1	1	3.6	33	7.3	6	4	8	18	·	1	·	·	15	13	8	·	2	15	·
IV	21.5	2.0	15	2.7	2.5	4.4	1.5	3.0	1	7.0	7.5	5.4	9.5	3.7	29.5	2.4	2	2.8	60	14.0	13	·	·	3	·	1	·	·	18	19	12	1	2	·	·
V	24.5	2.0	16.5	3.4	1.5	3.0	0.5	5.0	2	5.8	4.5	5.1	10.5	4.3	24	3.0	9	2.8	163	29.7	29	·	·	2	·	·	·	2	18	21	17	5	1	·	4
VI	14	1.8	18.5	2.0	0.5	4.0	1	5.0	0.5	10.0	5	6.3	10	5.6	26.5	3.2	14	2.8	71	11.6	27	·	·	·	3	1	·	1	14	14	12	2	1	·	5
VII	6.5	1.3	1.5	2.0	1	2.5	·	·	1	6.0	11.5	5.4	15.5	4.1	13	3.4	43	2.0	90	30.4	8	·	·	·	3	2	·	·	23	18	16	1	1	·	6
VIII	14	1.6	11	2.5	·	·	3	4.0	2.5	4.2	6.5	3.7	11.5	3.0	30.5	2.1	14	2.1	81	42.1	24	·	·	·	7	·	·	·	7	10	6	2	·	·	1
IX	4	1.1	4.5	2.2	4	3.9	9.5	3.8	6	4.2	23.5	3.8	13	3.2	22.5	1.9	3	2.9	32	14.3	10	·	·	·	·	·	·	·	8	8	5	1	·	·	1
X	9	2.1	13	2.1	6.5	2.1	1.5	1.7	4.5	4.0	20	3.3	10.5	2.7	16	2.7	12	2.4	7	4.8	16	·	·	7	·	·	·	2	10	4	3	·	3	·	·
XI	3	1.7	8	2.8	9	2.6	2	3.2	6.5	3.8	22.5	5.0	22.5	2.6	12.5	2.6	4	3.2	55	16.0	11	·	9	25	·	4	·	·	22	19	12	1	2	17	·
XII	2.5	2.0	6	2.1	3	1.7	1.5	2.3	6	2.8	42.5	5.6	21.5	4.1	8	2.9	2	4.2	39	9.7	21	·	1	21	·	7	1	·	20	15	9	·	1	13	·
Rok	152.5	1.8	108	2.4	29	2.4	21.5	3.3	43	5.4	197	5.5	165.5	4.0	272.5	2.6	106	3.1	715	42.1	24.VIII	11	44	131	13	28	2	5	199	180	122	14	14	85	17

Bierutowice (Wang) — $H_s = 860\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥19	≥15	◔	◕	Opad R ≥0.1	≥10	≥100	≡	⊠	K ⊠
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	89	14.1	17	1	15	29	·	–	–	·	17	17	16	3	12	31	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	113	15.1	13	14	27	28	·	–	–	·	24	26	23	3	11	28	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47	15.4	28	6	10	27	·	–	–	3	9	14	10	1	7	31	1
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	100	23.4	22	·	·	17	·	–	–	4	15	19	15	2	13	3	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	286	72.4	28	·	·	3	·	–	–	1	9	21	20	7	8	·	5
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	146	63.8	11	·	·	·	1	–	–	1	10	17	13	3	4	·	3
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	152	33.1	17	·	·	·	2	–	–	1	8	24	18	4	5	·	4
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	126	75.2	24	·	·	·	2	–	–	2	5	11	8	2	3	·	1
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	85	24.0	10	·	·	·	·	–	–	4	5	9	8	3	4	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	10	4.5	16	·	·	8	·	–	–	8	1	7	4	·	6	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	83	17.5	27	7	13	24	·	–	–	·	17	23	17	1	10	24	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	101	29.3	5	·	14	30	·	–	–	·	19	20	12	3	7	31	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1338	75.2	24.VIII	28	79	166	5	–	–	24	139	208	164	32	90	148	16

Karpacz — $H_s = 700\,m$ — $H_b = 708{,}0\,m$ — $h_w = 16\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥19	≥15	◔	◕	Opad R ≥0.1	≥10	≥100	≡	⊠	K ⊠
I	3	1.7	·	·	·	·	1.5	3.0	10	6.8	4.5	2.7	5	2.5	10	2.8	59	1.4	69	15.9	17	1	11	30	·	2	·	·	17	17	11	2	11	31	·
II	8.5	2.5	·	·	·	·	·	·	3.5	4.3	4.5	3.1	4.5	2.1	16	3.2	47	1.3	94	12.7	8	9	24	28	·	·	·	2	18	24	21	2	5	28	·
III	1.5	3.7	2	2.0	1	1.0	1	1.0	5	3.8	5	2.8	5.5	2.1	8	3.1	64	0.9	51	13.9	28	3	10	22	·	·	·	5	10	20	10	1	6	31	·
IV	1.5	1.3	1	2.0	·	·	·	·	5	4.8	3	4.0	1.5	2.3	11	2.0	67	0.7	144	24.5	22	·	·	6	·	·	·	4	15	18	17	5	11	4	1
V	5	1.5	1.5	2.0	·	·	1.5	4.0	3.5	3.7	1.5	2.3	8	1.8	15	2.9	57	1.0	294	66.4	28	·	·	3	·	·	·	4	18	23	17	7	9	·	4
VI	4	1.4	1	1.0	1	1.0	4	1.8	7	5.0	5.5	2.1	2.5	1.2	18	2.3	47	1.2	135	47.6	11	·	·	·	1	1	·	2	13	17	13	2	5	·	5
VII	5	1.4	·	·	·	·	1	4.0	12.5	3.3	14.5	4.0	8	2.0	7	1.8	45	1.5	156	40.3	17	·	·	·	1	·	·	·	15	26	20	5	8	·	8
VIII	6.5	2.1	·	·	0.5	1.0	3.5	2.3	12	5.8	2.5	1.5	4.5	1.3	10.5	1.9	48	1.4	137	61.2	24	·	·	·	2	2	·	2	3	11	10	3	6	·	3
IX	2	1.2	1	1.0	1	2.0	6	7.2	17.5	5.6	14.5	2.2	4	1.9	3	1.7	41	2.1	94	24.8	1	·	·	·	·	5	3	6	7	9	9	3	4	·	3
X	2	1.5	2	1.5	·	·	1	1.0	1	4.5	6	3.2	6	1.8	4	2.4	71	0.5	11	3.5	16	·	·	7	·	·	·	11	5	5	4	·	4	·	·
XI	3.5	1.7	0.5	1.0	1.5	1.7	1	9.0	13	9.3	8.5	4.3	5	2.9	2	3.0	55	2.2	95	18.1	27	4	11	24	·	7	1	1	15	22	14	2	6	23	·
XII	3	1.8	1	4.0	·	·	1	8.0	31	6.2	10	4.0	2	1.5	9	2.1	36	2.9	104	29.3	5	·	7	26	·	8	2	·	19	22	12	4	1	29	1
Rok	45.5	1.8	10	1.2	5	0.6	21.5	3.4	12.1	5.3	85	3.0	56.5	2.0	113.5	2.4	637	1.4	1384	66.4	28.V	17	63	148	4	25	6	37	155	214	158	36	76	146	25

Dabrogoszcz — $H_s = 175\,m$ — $h_w = 11{,}5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥19	≥15	◔	◕	Opad R ≥0.1	≥10	≥100	≡	⊠	K ⊠
I	5.5	1.9	7.5	1.0	0.5	1.0	7	2.3	17.5	3.6	33	6.0	6.5	3.2	15.5	4.1	·	4.1	30	9.2	9	·	1	23	·	8	1	2	15	13	8	·	2	9	–
II	13.5	3.1	9.5	1.6	3	2.2	1	1.5	3.5	3.9	12.5	7.2	12.5	5.8	27.5	4.3	1	4.3	20	7.5	17	7	22	26	·	7	1	1	14	16	6	·	2	26	–
III	3.5	4.3	1.5	2.0	1	1.0	4	2.4	23.5	2.6	19	4.0	8	4.2	21.5	3.7	11	3.0	25	5.9	6	5	7	18	·	1	·	·	13	13	7	·	2	15	–
IV	4	2.2	9	2.3	10	3.2	7	2.3	9.5	2.9	13	4.4	10	3.0	26.5	2.8	1	2.9	54	15.6	19	·	·	6	·	3	·	2	16	15	9	2	·	·	–
V	10	2.2	18	2.9	2	5.0	7	2.1	2.5	2.4	16.5	4.6	4.5	4.1	30.5	3.7	2	3.3	197	32.8	29	·	·	2	·	2	·	3	18	19	16	10	1	·	–
VI	10	2.3	10	1.8	4.5	1.7	7.5	2.5	8.5	4.2	12	5.3	13	2.8	20.5	3.7	4	3.1	93	20.2	22	·	·	·	6	1	·	4	7	16	13	4	·	·	–
VII	8	2.5	1.5	1.0	3.5	1.6	2.5	1.0	9	2.5	36	4.2	17.5	2.9	12	1.7	3	3.0	80	16.4	8	·	·	·	3	3	·	1	11	17	12	2	·	·	–
VIII	12.5	1.8	5.5	1.2	1	3.0	14	2.9	13.5	2.3	13	3.3	7.5	2.5	26	2.4	·	2.5	93	31.3	24	·	·	·	8	1	·	5	3	11	9	4	·	·	–
IX	·	·	·	·	·	·	10	4.8	21.5	3.1	28.5	3.4	6	1.8	23	1.8	1	2.9	57	20.8	28	·	·	·	2	2	·	7	6	10	7	2	·	·	–
X	6	2.2	·	·	9.5	1.4	21	1.5	9.5	2.2	18	4.6	4	5.9	25	2.0	·	2.5	3	2.1	16	·	·	6	·	1	·	10	2	3	1	·	6	·	–
XI	·	·	11.5	3.0	5	2.8	6	2.6	19	2.1	19.5	6.6	8.5	5.2	16.5	2.0	4	3.4	34	9.6	3	2	8	22	·	4	·	1	18	14	7	·	3	10	–
XII	0.5	3.0	3	3.3	·	·	3.5	3.0	17	5.2	44.5	6.3	7.5	5.1	17	3.5	·	5.3	24	6.7	18	2	·	17	·	6	2	·	12	10	7	·	1	4	–
Rok	73.5	2.1	77	1.7	40	1.9	90.5	2.4	154.5	3.1	265.5	5.0	105.5	3.9	261.5	3.0	27	3.4	710	32.8	29.V	16	38	120	19	39	4	36	134	157	102	24	17	64	–

Werbkowice

φ = 50°45′ λ = 23°46′ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.1	−6.2	5.4	30	−19.9	11	−3.9	−1.3	−3.2	−2.9	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.1	7.7	8.0
II	—	—	—	—	−4.0	−11.9	1.6	14	−24.4	7	−8.0	−5.3	−7.8	−7.2	—	—	—	—	—	—	—	—	—	—	—	—	9.2	7.3	6.9	7.8
III	—	—	—	—	4.4	−4.8	15.0	30	−19.3	1	−3.1	3.0	−0.4	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.7	5.5	7.1
IV	—	—	—	—	10.2	1.8	17.2	26	−3.4	1	3.5	8.3	5.0	5.4	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.6	6.7	7.9
V	—	—	—	—	16.1	5.8	28.1	19	−2.5	4	8.5	14.0	9.9	10.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.2	7.5	7.3
VI	—	—	—	—	21.3	10.8	28.7	26	5.1	8	14.3	19.7	15.2	16.1	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.3	6.5	6.2
VII	—	—	—	—	21.7	11.0	29.2	17	5.8	12	14.8	20.5	15.1	16.4	—	—	—	—	—	—	—	—	—	—	—	—	5.1	7.6	6.4	6.4
VIII	—	—	—	—	20.8	9.8	28.7	8	5.1	29	12.8	19.3	13.6	14.8	—	—	—	—	—	—	—	—	—	—	—	—	4.9	6.5	4.5	5.3
IX	—	—	—	—	20.9	7.5	27.2	4	0.4	17	9.6	19.7	12.8	13.7	—	—	—	—	—	—	—	—	—	—	—	—	4.8	4.7	2.0	3.8
X	—	—	—	—	12.2	1.0	22.2	1	−6.4	22	3.3	11.2	5.2	6.2	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.7	4.5	5.6
XI	—	—	—	—	1.4	−4.5	14.1	2	−22.0	17	−2.3	0.1	−1.9	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.7	8.7	8.8
XII	—	—	—	—	2.0	−2.6	8.0	10	−19.6	17	−1.2	0.9	−0.6	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.8	8.3	8.2
Rok	—	—	—	—	10.6	1.5	29.2	17. VII	−24.4	7. II	4.0	9.2	5.2	5.9	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.2	6.3	6.9

Śnieżka

φ = 50°44′ λ = 15°44′

I	826.6	838.0	809.0	—	−4.5	−8.2	2.2	12	−15.7	7	−7.0	−5.9	−6.6	−6.5	3.4	3.7	3.5	3.5	92	92	92	92	0.3	0.3	0.3	0.3	8.5	8.9	8.6	8.7
II	828.5	839.7	809.6	—	−9.2	−13.5	−5.1	4	−17.3	6, 28	−12.0	−10.6	−11.5	−11.4	2.2	2.4	2.3	2.3	88	88	88	88	0.3	0.3	0.3	0.3	8.6	8.4	8.0	8.3
III	831.4	847.8	807.7	—	−2.9	−8.1	4.2	30	−16.0	4	−6.3	−4.3	−5.2	−5.2	3.4	3.8	3.6	3.6	83	84	83	83	0.7	0.9	0.8	0.8	7.1	7.0	6.7	6.9
IV	828.7	843.6	814.9	—	0.3	−3.5	6.3	6	−8.4	1	−2.4	−0.8	−1.6	−1.6	4.6	5.0	4.8	4.8	90	89	89	89	0.6	0.8	0.6	0.7	7.8	8.3	7.5	7.9
V	833.3	844.1	821.5	—	3.4	−0.7	10.2	16	−5.6	21	0.8	2.1	1.3	1.4	6.3	6.6	6.4	6.4	94	92	94	93	0.3	0.7	0.5	0.5	8.2	8.4	8.3	8.3
VI	836.7	845.5	824.2	—	9.6	4.1	19.5	26	−2.0	2	5.8	7.6	6.7	6.7	8.5	9.2	8.8	8.8	91	88	89	89	1.0	1.8	1.3	1.4	7.3	8.8	7.1	7.7
VII	835.2	843.3	823.6	—*	9.0	4.7	18.6	14	−0.6	6	6.1	7.2	6.8	6.7	9.0	9.6	9.3	9.3	93	93	92	93	0.8	0.9	0.9	0.9	8.9	9.1	8.1	8.7
VIII	838.3	847.3	828.5	—	9.3	4.6	17.9	6, 7	0.2	26	5.8	7.8	6.8	6.8	8.1	8.7	8.8	8.5	87	81	88	85	1.4	2.3	1.3	1.7	6.8	7.3	6.8	7.0
IX	836.0	852.0	823.2	—	9.0	3.8	14.7	23	−1.5	20	5.1	6.7	6.4	6.2	7.5	8.3	8.6	8.1	86	85	90	87	1.7	1.8	1.2	1.6	7.5	7.9	8.5	8.0
X	841.3	849.8	830.3	—	6.5	1.1	14.4	1	−5.6	21	3.6	4.9	3.4	3.8	4.4	5.8	4.4	4.9	59	67	59	62	3.8	3.2	3.7	3.6	4.1	4.6	4.4	4.4
XI	826.0	846.0	803.4	—	−3.2	−6.1	11.3	7	−17.4	23	−6.0	−5.1	−6.0	−5.8	3.5	3.7	3.4	3.5	87	87	85	86	0.7	0.9	0.9	0.8	8.0	8.5	7.9	8.1
XII	821.7	837.6	803.1	—	−4.8	−8.1	2.6	18, 19	−12.7	30	−6.4	−6.4	−6.4	−6.4	3.6	3.5	3.7	3.6	93	90	94	92	0.2	0.4	0.2	0.3	9.2	9.0	9.2	9.1
Rok	832.0	852.0	803.1	—	1.9	−2.7	19.5	26. VI	−17.4	23. XI	−1.1	0.3	−0.5	−0.4	5.4	5.9	5.6	5.6	87	86	87	87	1.0	1.2	1.0	1.1	7.7	8.0	7.6	7.8

Zamość

φ = 50°42′ λ = 23°15′

I	987.0	1003.8	963.8	1013.9	0.1	−5.9	4.9	30	−19.1	11	−3.2	−1.1	−2.6	−2.4	4.3	4.7	4.3	4.4	84	80	84	83	0.8	1.1	0.8	0.9	8.0	8.0	7.6	7.9
II	988.1	1005.7	964.8	1015.6	−3.9	−11.5	0.9	14	−26.7	7	−7.9	−4.9	−7.5	−7.0	3.1	3.4	3.0	3.2	84	76	79	80	0.5	1.0	0.7	0.7	8.1	7.0	7.4	7.5
III	991.6	1007.2	964.2	1018.4	4.9	−4.3	15.6	30	−20.7	1	−2.5	3.6	0.2	0.4	4.7	5.5	5.2	5.1	85	69	81	78	0.7	2.7	1.2	1.5	6.9	6.5	5.5	6.3
IV	985.8	1000.2	967.3	1011.8	9.9	1.7	16.7	7	−2.4	7	3.7	8.2	4.8	5.4	6.9	6.9	7.2	7.0	84	64	81	76	1.3	4.3	1.7	2.4	7.8	7.8	5.4	7.0
V	988.0	1004.2	977.0	1013.8	15.3	5.6	27.1	19	−3.9	4	8.5	13.3	9.8	10.4	9.8	9.7	10.3	9.9	85	62	83	77	1.7	6.4	2.1	3.4	6.6	8.1	6.5	7.1
VI	988.7	995.9	976.3	1014.0	20.8	10.7	28.4	26	3.6	8	14.2	19.1	14.8	15.7	13.9	13.4	14.4	13.9	85	62	85	77	2.5	9.2	2.7	4.8	5.5	6.4	5.5	5.8
VII	987.9	997.3	977.4	1013.1	21.7	11.0	28.5	16	5.5	12	15.1	19.9	15.0	16.2	14.9	14.5	15.1	14.8	86	63	87	79	2.5	9.3	2.3	4.7	5.0	7.2	5.6	5.9
VIII	990.2	999.0	972.8	1015.6	20.6	10.0	29.8	8	4.4	16	12.7	18.9	13.5	14.6	13.5	13.7	13.5	13.6	92	64	87	81	1.4	9.1	2.3	4.3	5.4	6.3	3.5	5.1
IX	991.8	1007.9	980.3	1017.2	21.0	8.0	27.0	3, 4	3.0	17	10.8	19.5	12.1	13.6	12.1	13.4	13.0	12.8	93	60	91	81	1.1	9.9	1.4	4.1	4.8	5.3	2.5	4.2
X	997.1	1011.5	985.9	1023.4	12.1	1.5	21.4	1	−7.1	22	3.9	11.1	5.5	6.5	7.5	8.4	7.9	7.9	91	63	85	80	0.8	5.3	1.4	2.5	6.0	5.9	4.0	5.3
XI	986.9	1003.2	962.2	1013.7	1.8	−4.7	14.7	2	−25.4	18	−2.0	0.1	−1.6	−1.3	5.0	5.3	5.2	5.2	89	82	87	86	0.6	1.3	0.8	0.9	8.6	8.5	7.8	8.3
XII	982.4	996.5	963.4	1009.0	2.2	−2.7	8.1	10	−21.9	17	−0.9	1.2	−0.2	0.0	5.2	5.4	5.3	5.3	86	80	85	84	0.8	1.4	0.9	1.0	8.5	7.4	7.9	7.9
Rok	988.8	1011.5	962.2	1015.0	10.5	1.6	29.8	8.VIII	−26.7	7. II	4.4	9.1	5.3	6.0	8.4	8.7	8.7	8.6	87	69	85	80	1.2	5.1	1.5	2.6	6.8	7.0	5.8	6.5

Zdanów

φ = 50°43′ λ = 21°33′

I	—	—	—	—	−0.5	−6.0	3.7	30	−16.6	11, 12	−3.8	−1.5	−3.1	−2.9	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.1	7.2	7.4
II	—	—	—	—	−3.7	−11.4	1.6	14	−25.4	7	−8.2	−5.2	−7.3	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.0	6.6	6.9
III	—	—	—	—	4.0	−4.5	15.5	30	−17.2	1	−2.2	2.9	−0.4	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.1	5.8	6.6
IV	—	—	—	—	10.3	2.1	15.7	7	−1.8	6	3.5	8.5	5.2	5.6	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.7	6.4	7.3
V	—	—	—	—	15.0	5.8	26.0	19	−1.7	4	8.4	13.5	9.4	10.2	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.3	6.2	6.6
VI	—	—	—	—	20.7	10.8	30.4	26	6.1	3	14.3	19.4	14.3	15.6	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.0	5.2	5.2
VII	—	—	—	—	21.7	11.2	28.2	16	6.1	11	15.0	20.2	14.9	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.1	5.6	6.2
VIII	—	—	—	—	20.6	10.7	30.1	8	6.9	31	13.1	19.1	13.9	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.1	5.6	4.8	5.2
IX	—	—	—	—	20.6	9.1	26.0	3	4.7	17	11.0	19.1	13.1	14.1	—	—	—	—	—	—	—	—	—	—	—	—	4.1	5.1	2.6	3.9
X	—	—	—	—	12.0	3.0	21.2	1	−3.9	22	4.7	10.9	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.3	3.9	5.1
XI	—	—	—	—	1.2	−4.1	13.0	2	−18.1	18	−2.5	−0.1	−1.4	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.0	7.3	7.9
XII	—	—	—	—	1.3	−3.3	5.6	19, 20	−16.8	17	−1.4	0.4	−1.0	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.7	5.8	7.1
Rok	—	—	—	—	10.3	2.0	30.4	26. VI	−25.4	7. II	4.3	8.9	5.3	6.0	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.7	5.6	6.3

Werbkowice

$H_s = 204\ m$ $h_w = 14\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU °D,V=D N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Min<0°	Max<0°	Max>25°	Wiatr V ≥10	≥15	LICZBA DNI (n)			Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K (K)
I	4.5	3.1	1.5	2.3	6	2.7	19.5	2.6	13.5	2.3	26.5	5.8	5.5	4.2	3	6.7	13	3.4	33	9.0	20	6	13	28	·	5	·	3	21	16	8	·	5	31	·
II	9	4.1	7	3.1	3	3.3	0.5	3.0	3	4.2	20.5	5.6	19.5	5.7	17.5	4.4	4	4.6	30	9.4	16	16	24	28	·	4	·	1	15	14	8	·	2	28	·
III	5.5	2.6	8.5	1.8	3.5	2.1	15	2.2	22.5	2.1	14	2.8	10.5	3.3	10.5	4.4	3	2.5	33	8.6	17	6	7	25	·	2	·	2	14	15	9	·	12	19	·
IV	6.5	2.2	2	1.8	25.5	3.6	27	3.6	6	2.2	10	3.6	4.5	2.7	7.5	4.5	1	3.3	47	15.9	28	·	·	10	·	·	·	·	15	15	7	1	3	1	1
V	13.5	3.1	4	1.9	9.5	3.2	7.5	2.8	4	2.6	12.5	3.1	16.5	4.2	21.5	3.1	4	3.1	34	5.5	27	·	·	3	2	1	·	·	12	19	10	·	2	·	3
VI	7	2.1	2.5	2.2	13	2.7	4.5	1.6	8	1.9	8.5	3.5	21.5	2.9	18	2.6	7	2.4	80	19.4	28	·	·	·	6	·	·	1	11	12	9	3	1	·	2
VII	4	1.4	5	2.0	8.5	2.2	4.5	1.8	11	2.5	23.5	3.3	19	3.1	8.5	1.7	9	2.4	117	39.5	17	·	·	·	5	·	·	2	8	20	14	3	1	·	4
VIII	4.5	2.7	1.5	4.0	2	1.8	10	1.8	7	1.4	18.5	2.8	21	3.0	20.5	2.2	8	2.2	67	27.5	1	·	·	·	7	·	·	6	8	11	8	2	2	·	1
IX	1	4.0	·	·	7	2.7	16.5	2.0	26	2.3	11.5	3.7	10	2.9	9	2.3	9	2.3	30	17.3	11	·	·	·	5	1	1	9	1	9	5	1	4	·	·
X	7	2.6	2.5	1.8	7.5	1.9	3	2.2	9.5	1.9	17.5	3.8	20	4.1	20	3.4	6	3.0	7	6.0	11	·	·	12	·	·	·	5	10	8	1	·	7	·	·
XI	1.5	1.7	7.5	3.3	7	2.7	16	2.2	8.5	2.7	14	4.8	21	4.0	6.5	2.5	8	3.0	64	10.0	21	4	12	23	·	1	·	·	21	21	14	1	7	19	·
XII	3	3.2	0.5	2.0	1	3.5	10.5	2.5	16	3.2	38.5	4.2	15.5	3.6	5	4.1	3	3.5	23	8.5	18	2	6	22	·	·	·	·	19	15	8	·	3	3	·
Rok	67	2.7	42.5	2.2	93.5	2.7	134.5	2.4	135	2.4	215.5	3.9	184.5	3.6	147.5	3.5	75	3.0	565	39.5	17.VII	34	62	151	25	14	1	29	155	175	102	11	49	101	11

Śnieżka

$H_s = 1603\ m$ $H_b = 1610{,}6\ m$

I	10	4.8	·	·	·	·	·	·	3.5	9.0	39	12.4	19	9.3	21.5	10.1	·	10.3	124	21.0	5	3	29	31	·	24	16	·	23	27	20	3	31	31	·
II	19.5	15.2	1.5	15.0	2	8.5	1.5	7.3	1	8.0	6	17.8	28	13.7	24.5	12.9	·	13.8	186	28.1	7	26	28	28	·	26	20	1	18	25	23	6	27	28	·
III	15.5	12.2	1	17.0	·	·	2.5	5.4	9.5	7.5	25.5	11.4	24.5	11.6	12.5	7.7	2	10.3	72	20.2	28	11	22	30	·	26	17	5	15	22	14	2	28	31	·
IV	28	11.1	1.5	8.0	2.5	8.8	3.5	4.6	6.5	9.5	21	10.4	11	7.0	15	10.1	1	9.7	172	53.2	22	·	16	29	·	28	8	1	18	22	18	3	26	30	1
V	16.5	10.6	4.5	6.7	4	10.4	4	10.1	4.5	8.4	12	12.6	21.5	11.7	26	12.0	·	11.2	326	92.6	29	·	3	17	·	28	19	2	22	25	19	8	29	23	5
VI	21.5	10.0	1	5.0	·	·	3.5	7.1	9	8.1	19	12.6	19.5	10.8	16.5	9.3	·	10.2	155	50.5	11	·	·	1	·	29	14	1	13	22	16	7	28	·	5
VII	7	8.3	2.5	2.4	1	2.0	2.5	9.6	3.5	6.9	31.5	13.3	34.5	14.1	9.5	8.9	1	11.9	209	37.7	17	·	·	2	·	30	18	·	24	27	24	8	30	·	9
VIII	22.5	6.4	·	·	·	·	·	·	5	1.3	21	9.7	22	8.3	19.5	7.4	3	8.0	132	59.3	24	·	·	·	·	23	9	1	11	15	11	3	26	·	3
IX	6	7.1	0.5	2.0	·	·	0.5	6.0	12.5	10.8	46	13.6	16	9.2	8.5	8.3	·	11.4	95	24.4	10	·	·	1	·	27	21	1	18	18	12	2	28	·	2
X	20	6.9	1.5	2.3	4.5	5.6	6	7.5	11	3.3	14.5	11.2	14.5	12.2	16	8.8	5	7.8	15	3.3	16	·	1	14	·	20	9	7	6	10	6	·	20	·	·
XI	16	7.3	8.5	9.3	2	7.5	1.5	3.3	5.5	5.5	27.5	20.1	11	17.6	13	7.9	5	12.2	131	25.8	11	12	23	27	·	28	15	1	18	24	21	3	28	25	·
XII	5	9.0	·	·	·	·	·	·	1	17.0	44.5	18.7	29	14.6	13.5	12.7	·	16.0	178	15.9	18	7	27	30	·	29	26	·	26	30	27	7	31	31	1
Rok	187.5	9.1	22.5	5.6	16	3.6	25.5	5.1	72.5	7.9	307.5	13.6	250.5	11.7	196	9.7	17	11.1	1795	92.6	29.V	59	149	210	·	318	192	20	212	267	211	52	332	199	26

Zamość

$H_s = 212\ m$ $H_b = 213{,}2\ m$ $h_w = 13{,}1\ m$

I	2.5	6.8	2.5	4.8	13	4.5	20	4.8	13	4.8	24	5.4	8.5	7.9	2.5	8.6	7	5.0	31	7.4	17	4	13	27	·	6	·	3	20	18	8	·	6	31	·
II	7	6.6	4.5	6.9	6.5	3.8	·	·	2	10.0	20.5	7.1	26	6.3	12.5	4.9	5	5.9	12	1.5	17	17	25	28	·	8	·	1	15	19	6	·	4	28	·
III	2.5	5.2	6	4.1	12	4.0	8.5	3.8	16.5	2.8	13.5	4.2	10.5	4.7	6.5	6.2	17	3.3	23	5.8	17	6	6	24	·	2	·	3	11	11	6	·	5	16	·
IV	6.5	5.1	1.5	8.7	24.5	6.9	28	5.4	5.5	4.2	10	4.6	5.5	3.9	5.5	5.6	3	5.4	44	16.2	28	·	·	12	·	8	·	1	11	14	8	1	3	·	3
V	5.5	5.5	4.5	3.2	14.5	4.6	6.5	3.2	5.5	5.8	14.5	3.7	17.5	4.2	13.5	3.7	11	3.7	70	20.6	29	·	·	3	1	2	·	1	12	17	14	2	1	·	7
VI	4	4.1	1.5	4.3	14	4.4	9	3.8	7	3.9	7	3.6	23	4.9	15.5	4.5	9	3.9	65	16.3	10	·	·	·	6	1	·	3	9	14	9	2	2	·	4
VII	3	2.2	3	4.2	10.5	3.5	3.5	3.3	9.5	3.8	29	4.0	16.5	4.6	6	3.7	12	3.4	83	17.9	17	·	·	·	6	3	·	5	8	19	14	2	·	·	7
VIII	3.5	5.6	1	1.0	2	1.5	10.5	3.1	8.5	3.9	15	3.0	26.5	3.8	14	4.3	12	3.2	88	22.4	12	·	·	·	9	2	·	6	7	11	9	3	2	·	4
IX	1	2.5	·	·	3	2.8	23.5	3.0	18	3.4	14.5	3.3	8.5	3.9	11.5	3.0	10	2.9	35	18.4	11	·	·	·	5	1	·	9	1	6	5	1	3	·	·
X	8	4.8	2	2.5	5	2.4	5	3.8	4	3.1	17.5	4.2	22	4.6	17.5	4.0	12	3.6	4	1.6	31	·	·	9	·	2	·	8	8	6	2	·	9	·	·
XI	·	·	2.5	5.8	16.5	5.6	19.5	3.5	3.5	5.3	16.5	5.3	21.5	5.3	5	2.8	5	4.6	46	8.4	21	5	12	23	·	5	·	·	22	20	13	·	6	17	·
XII	1	2.0	3	4.3	2	3.8	13	4.1	8	6.2	40.5	6.3	14.5	4.9	7	4.6	4	5.2	26	8.3	18	2	7	22	·	4	·	·	18	16	7	·	5	8	·
Rok	44.5	4.2	32	4.2	123.5	4.0	147	3.5	101	4.8	222.5	4.6	200.5	4.9	117	4.7	107	4.2	527	22.4	12.VII	34	63	148	27	44	·	40	142	171	101	11	46	100	25

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Zdanów

$H_s = 236\ m$ $h_w = 15\ m$

I	7.5	3.5	3.5	3.6	2	2.0	13	3.2	9.5	4.3	8	3.4	7.5	8.0	11	4.5	31	2.8	46	11.7	3	5	20	31	·	2	1	3	20	11	8	1	6	31	·
II	14	4.6	5.5	2.6	·	·	·	·	4	7.1	13	5.3	18.5	5.8	15	5.1	14	4.3	18	4.2	16	17	26	28	·	5	1	5	14	15	7	·	4	28	·
III	14.5	4.0	4	5.9	1	4.0	4.5	4.0	4.5	3.1	5.5	5.4	7.5	4.5	7.5	5.9	50	2.2	25	4.4	7	7	7	23	·	3	1	4	14	10	8	·	12	21	·
IV	5.5	7.4	11	4.9	13.5	5.9	15	6.7	0.5	3.0	7	4.2	6	4.7	7.5	4.7	24	4.1	29	6.7	22	·	·	9	·	6	2	2	15	12	9	·	3	·	1
V	10	4.0	3	1.0	8	4.6	6.5	2.5	3	3.7	8.5	3.6	10.5	3.0	14.5	5.6	29	2.7	50	9.7	29	·	·	3	1	2	1	3	12	15	12	·	1	·	·
VI	7.5	4.2	6	3.8	7.5	2.7	4.5	3.1	3.5	5.7	1.5	1.7	19	4.2	14.5	3.6	26	2.7	68	13.0	27	·	·	·	5	2	1	5	7	12	10	2	·	·	4
VII	1	2.5	5	2.1	2	4.0	3.5	3.6	8.5	2.3	11	2.8	19.5	3.0	6.5	1.6	36	1.6	48	12.1	18	·	·	·	7	·	·	3	9	16	12	1	·	·	4
VIII	10	3.8	1	6.5	1	2.5	5	2.7	7.5	2.7	2	2.5	8.5	3.3	21	5.8	37	2.5	178	53.2	26	·	·	·	7	3	1	9	9	14	11	5	·	·	1
IX	2.5	1.6	·	·	0.5	1.0	12	3.1	19.5	3.6	4	2.8	6.5	3.5	8	2.0	37	1.8	52	21.0	29	·	·	·	4	·	·	11	4	9	7	2	5	·	1
X	12	2.4	1	2.5	4	2.4	6	2.8	4	2.2	6.5	4.6	18.5	4.3	13	2.7	28	2.3	5	3.5	31	·	·	6	·	1	·	8	9	5	2	·	8	·	·
XI	2	5.2	9	4.4	7.5	5.2	6.5	2.8	9	4.4	8.5	4.5	18	5.3	6.5	3.4	23	3.4	31	12.6	11	5	12	23	·	2	2	1	17	14	8	1	6	19	·
XII	3.5	3.9	1.5	1.7	·	·	7.5	3.2	24	4.0	18.5	3.8	18.5	3.5	3.5	2.6	16	3.0	33	12.2	18	2	6	26	·	3	·	2	13	12	8	1	2	16	·
Rok	84	3.9	50.5	3.2	47	2.9	84	3.1	97.5	3.8	94	3.7	158.5	4.4	128.5	4.0	351	2.8	583	53.2	26.VIII	36	71	149	24	29	10	56	143	145	102	13	47	115	11

Janów Lubelski

φ = 50°43′ λ = 22°25′ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.1	–6.1	5.9	30	–22.1	11	–3.8	–0.7	–3.2	–2.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–3.8	–11.4	1.7	12	–24.1	7	–8.5	–4.5	–7.4	–7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	5.1	–3.8	12.9	19	–18.1	1	–2.2	4.5	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.1	2.2	16.9	7, 18	–2.1	2	4.4	9.6	5.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.1	6.0	26.5	19	–2.1	3, 4	8.9	14.0	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.8	11.2	30.5	26	5.6	8	14.8	19.6	15.7	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.9	11.8	31.1	15	6.3	11	14.9	21.0	16.2	17.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.4	10.3	30.1	8	4.6	31	13.1	19.2	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.6	9.3	25.4	11	2.6	16	11.5	19.3	13.7	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	11.9	2.3	22.1	1	–3.1	22	4.1	11.5	6.3	7.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.5	–3.8	13.1	2	–17.2	18	–1.9	0.3	–1.3	–1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1.7	–2.8	6.1	10, 20	–16.9	16	–1.0	1.1	–0.7	–0.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.4	2.1	31.1	15.VII	–24.1	7. II	4.5	9.6	5.8	6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sokołowsko

φ = 50°41′ λ = 16°14′

I	–	–	–	–	0.0	–4.4	2.8	17	–17.2	7	–2.9	–0.9	–1.6	–1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	9.3	9.1	9.1
II	–	–	–	–	–3.4	–10.6	0.8	11	–20.3	10	–6.7	–4.5	–7.0	–6.3	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.8	7.6	8.5
III	–	–	–	–	3.2	–4.9	13.6	30	–20.6	9	–2.8	1.9	–1.5	–1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.5	6.8	7.2
IV	–	–	–	–	8.5	0.5	15.5	6	–4.6	2	2.9	7.2	3.4	4.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	7.8	7.6
V	–	–	–	–	12.3	4.4	19.7	17	–3.8	3	7.4	11.1	7.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.8	7.3	7.5
VI	–	–	–	–	18.2	8.2	28.8	26	1.1	3	12.4	16.8	12.0	13.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	6.3	6.5
VII	–	–	–	–	18.2	9.6	28.0	14	3.9	4	12.8	16.3	12.3	13.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.3	6.5	7.8
VIII	–	–	–	–	18.6	7.9	27.7	6	1.7	31	11.3	17.2	11.6	12.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.8	5.5	5.6
IX	–	–	–	–	16.8	7.8	22.7	2, 3	2.3	21	10.2	15.4	11.0	11.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.9	4.0	5.1
X	–	–	–	–	12.3	0.8	21.5	1	–7.1	22	2.7	11.6	3.8	5.5	–	–	–	–	–	–	–	–	–	–	–	–	5.0	3.9	3.2	4.0
XI	–	–	–	–	1.1	–4.3	10.2	1, 2	–14.7	24	–2.4	–0.1	–2.2	–1.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.3	7.8	8.1
XII	–	–	–	–	1.4	–3.2	7.7	19	–14.0	15	–0.8	0.1	–0.8	–0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.9	8.5	9.0
Rok	–	–	–	–	8.9	1.0	28.8	26.VI	–20.6	9. III	3.7	7.7	4.0	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	6.7	7.2

Grodków

φ = 50°41′ λ = 17°23′

I	–	–	–	–	3.1	–2.2	6.5	17	–9.6	7	–0.2	2.0	0.3	0.6	5.5	5.7	5.6	5.6	91	81	89	87	0.6	1.4	0.7	0.9	8.1	7.5	7.0	7.5
II	–	–	–	–	–1.2	–7.6	3.9	14	–18.8	6	–4.4	–2.3	–4.4	–3.9	4.1	4.2	4.1	4.1	91	81	90	87	0.4	1.0	0.5	0.6	8.8	7.4	7.2	7.8
III	–	–	–	–	6.5	–3.0	17.0	30	–20.0	9	–1.2	5.4	0.8	1.4	5.5	6.1	6.0	5.9	90	66	87	81	0.7	3.5	0.9	1.7	6.3	6.4	5.9	6.2
IV	–	–	–	–	11.4	3.6	16.8	3, 6	–0.2	6	5.5	10.5	6.7	7.4	7.9	7.4	8.3	7.9	87	60	84	77	1.2	5.5	1.6	2.8	7.3	7.2	6.8	7.1
V	–	–	–	–	15.1	7.0	23.6	17	–1.3	3	10.0	13.8	10.2	11.0	10.6	10.6	10.9	10.7	84	67	86	79	2.0	5.6	1.7	3.1	7.9	7.8	7.1	7.6
VI	–	–	–	–	20.9	11.2	31.6	26	4.7	3	15.2	19.8	14.8	16.2	14.4	14.7	14.6	14.6	83	63	86	77	3.1	9.5	2.5	5.0	4.8	6.3	5.1	5.4
VII	–	–	–	–	21.6	12.2	30.4	14	7.2	4, 10	15.9	20.1	15.0	16.5	14.8	15.4	15.3	15.2	81	65	88	78	3.4	9.0	2.1	4.8	7.9	7.8	6.1	7.3
VIII	–	–	–	–	21.6	10.9	30.6	7	5.2	31	14.2	20.4	14.6	16.0	13.8	13.4	14.2	13.8	85	56	85	75	2.7	11.5	2.8	5.7	5.5	5.5	5.5	5.5
IX	–	–	–	–	20.7	9.1	27.6	3	4.8	22	12.2	19.3	12.8	14.3	12.4	13.0	13.1	12.8	87	60	88	78	2.0	9.4	2.4	4.6	4.8	5.7	3.5	4.7
X	–	–	–	–	13.7	2.8	22.3	2	–5.2	22	4.7	12.8	6.3	7.5	8.2	9.8	8.9	9.0	93	66	90	83	0.7	5.5	1.0	2.4	6.2	4.3	3.5	4.7
XI	–	–	–	–	4.2	–2.4	15.3	1	–11.0	24	–0.5	2.6	0.4	0.7	5.4	5.9	5.7	5.7	90	79	88	86	0.8	1.9	1.0	1.2	8.4	7.8	7.2	7.8
XII	–	–	–	–	4.6	–0.9	12.3	19	–12.4	15	1.3	3.0	1.9	2.0	5.9	5.9	5.9	5.9	87	79	83	83	1.0	1.8	1.4	1.4	8.8	7.8	6.6	7.7
Rok	–	–	–	–	11.8	3.4	31.6	26.VI	–20.0	9. III	6.1	10.6	6.6	7.5	9.0	9.3	9.4	9.2	87	69	87	81	1.6	5.5	1.6	2.9	7.1	6.8	6.0	6.6

Sandomierz

φ = 50°41′ λ = 21°45′

I	988.3	1004.2	964.9	1013.5	0.5	–5.2	5.7	30	–15.2	12	–3.3	–0.6	–2.4	–2.2	4.7	5.0	4.8	4.8	94	85	92	90	0.3	0.9	0.4	0.5	7.4	7.8	7.4	7.5
II	990.7	1006.7	965.7	1016.3	–2.7	–10.6	2.9	14	–23.7	7	–7.8	–4.4	–6.9	–6.5	3.3	3.6	3.2	3.4	92	78	85	85	0.3	1.0	0.6	0.6	7.9	7.2	6.7	7.3
III	993.0	1009.0	964.3	1018.0	5.6	–3.3	16.9	30	–16.6	1	–2.2	4.1	1.1	1.0	5.1	5.6	5.5	5.4	91	67	81	80	0.5	2.9	1.3	1.6	6.5	6.4	5.3	6.1
IV	986.7	1003.9	968.3	1011.1	11.1	2.6	17.2	7	–1.5	6	3.9	9.2	6.3	6.4	7.2	7.5	7.6	7.4	87	64	78	76	1.0	4.5	2.1	2.5	8.1	7.2	6.9	7.4
V	989.6	1005.3	977.6	1013.6	16.1	6.2	27.8	19	–1.7	4	8.5	14.3	10.4	10.9	9.7	9.7	10.7	10.0	84	59	82	75	1.7	7.2	2.2	3.7	7.4	7.5	5.6	6.8
VI	990.4	998.4	978.7	1014.0	22.2	11.5	31.9	26	6.7	3	14.9	20.4	15.7	16.7	14.1	13.5	14.0	13.9	82	57	78	72	3.1	11.3	4.1	6.2	4.9	6.4	5.6	5.6
VII	989.3	997.7	978.7	1012.9	22.5	11.8	29.4	17	6.7	11	15.0	20.7	16.0	16.9	15.1	14.6	15.1	14.9	87	59	83	76	2.2	10.5	3.4	5.4	5.6	6.7	5.8	6.0
VIII	992.1	1000.4	977.3	1015.8	21.1	11.1	30.0	8	7.5	3	12.8	19.6	14.5	15.4	13.8	14.0	13.9	13.9	92	62	84	79	1.2	9.8	3.0	4.7	5.4	6.0	4.7	5.4
IX	992.8	1010.1	981.8	1016.6	21.1	9.4	25.7	3	5.0	17	11.0	19.5	13.8	14.5	12.7	14.4	13.8	13.6	95	64	87	82	0.7	8.7	2.1	3.8	4.7	5.3	2.9	4.3
X	999.1	1013.0	987.5	1023.7	12.5	3.1	21.9	1	–3.5	22	4.3	11.4	6.8	7.3	8.1	9.3	8.9	8.8	95	67	88	83	0.4	4.6	1.2	2.1	6.4	5.9	3.8	5.4
XI	988.2	1005.7	963.2	1013.3	2.0	–3.4	13.6	2	–16.8	18	–1.8	0.5	–0.8	–0.7	5.1	5.5	5.6	5.4	90	82	91	88	0.6	1.3	0.6	0.8	8.6	8.2	8.2	8.3
XII	983.7	998.9	963.6	1008.6	2.3	–2.6	7.1	20	–15.4	17	–0.9	1.1	–0.4	–0.2	5.3	5.4	5.3	5.3	90	81	88	86	0.6	1.3	0.8	0.9	8.1	7.5	7.9	7.8
Rok	990.3	1013.0	963.2	1014.5	11.2	2.6	31.9	26.VI	–23.7	7. II	4.5	9.6	6.2	6.6	8.7	9.0	9.0	8.9	90	69	85	81	1.0	5.3	1.8	2.7	6.8	6.8	5.9	6.5

Janów Lubelski

$H_s = 230\,m$ $h_w = 20{,}1\,m$ **1965**

MIESIĄC	ROZKŁAD WIATRU *D,V=D N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◐	◓	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	13	1.0	8	1.1	16	1.8	10	1.2	13	1.8	7	1.9	6	3.5	5	1.4	15	1.4	66	10.0	9	5	15	30	·	·	·	–	–	17	14	1	–	31	–
II	18	1.4	3	1.3	·	·	·	·	16	2.2	5	1.8	23	2.0	14	1.4	5	1.7	55[2]	10.0	19	15	27	28	·	·	·	–	–	18	13	1	–	28	–
III	16	1.1	3	1.0	7	1.0	8	1.1	23	1.0	13	2.2	9	1.1	2	1.5	12	1.1	65	10.5	3	6	7	23	·	·	·	–	–	13	11	2	–	–	–
IV	10	1.7	6	2.0	14	2.0	18	1.4	12	1.7	6	2.0	14	1.1	4	2.5	6	1.6	66	18.0	26	·	·	9	·	·	·	–	–	13	13	1	–	·	–
V	12	1.5	6	3.5	11	1.9	3	1.7	8	2.2	14	2.4	16	1.8	10	1.6	13	1.7	64	11.8	29	·	·	2	1	1	·	–	–	17	12	2	–	·	–
VI	8	1.1	8	1.9	9	2.2	2	2.0	6	1.8	8	2.4	31	2.1	4	1.0	14	1.6	83	16.7	28	·	·	·	6	1	·	–	–	15	12	2	–	·	–
VII	4	1.2	3	1.0	10	1.5	2	2.0	24	1.4	10	2.7	18	1.8	4	1.2	18	1.3	119	45.5	17	·	·	·	6	·	·	–	–	14	14	4	–	·	–
VIII	11	2.0	·	·	12	1.1	5	1.2	13	1.4	3	1.3	22	1.4	11	1.5	16	1.2	166	50.2	1	·	·	·	8	·	·	–	–	12	11	5	–	·	–
IX	2	1.0	14	2.0	9	1.6	15	2.5	15	1.4	1	2.0	11	1.3	3	2.0	20	1.4	60	16.5	11	·	·	·	3	1	·	–	–	8	7	4	–	·	–
X	4	1.0	7	1.3	4	1.0	1	1.0	7	1.4	12	1.6	24	1.5	12	1.7	22	1.1	13	3.7	24	·	·	9	·	·	·	–	–	7	5	·	–	·	–
XI	10	2.7	10	2.1	15	1.2	6	1.8	15	1.4	7	1.9	16	2.4	5	2.4	6	1.8	70	8.5	27	5	12	21	·	·	·	–	–	22	17	·	–	–	–
XII	3	1.0	·	·	16	1.3	7	1.4	33	1.7	10	1.8	16	1.1	4	1.5	4	1.4	60	20.0	18	2	7	26	·	·	·	–	–	17	16	1	–	–	–
Rok	111	1.4	68	1.4	123	1.4	77	1.4	185	1.6	96	2.0	206	1.8	78	1.6	151	1.4	887	50.2	1. VIII	33	68	148	24	3	·	–	–	173	145	23	–	–	–

Sokołowsko

$H_s = 570\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◐	◓	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	60	12.0	9	3	15	28	·	–	–	·	24	20	13	1	7	31	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	73	9.3	17	17	25	28	·	–	–	1	19	25	20	·	4	28	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	50	9.6	28	5	8	23	·	–	–	2	14	14	12	·	9	23	1
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	99	20.2	21	·	·	19	·	–	–	3	19	19	16	3	2	·	·
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	241	58.7	29	·	·	5	·	–	–	2	18	24	18	8	·	·	5
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	121	26.1	22	·	·	·	2	–	–	2	12	18	13	7	3	·	6
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	120	29.1	15	·	·	·	2	–	–	1	17	25	17	4	2	·	10
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	81	45.5	24	·	·	·	2	–	–	3	4	12	9	2	·	·	3
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41	16.2	10	·	·	·	·	–	–	8	8	10	8	1	2	·	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6	3.9	16	·	·	13	·	–	–	9	7	4	1	·	3	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	58	11.7	11	3	11	26	·	–	–	·	21	21	14	2	7	20	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	71	14.6	18	2	8	25	·	–	–	1	24	25	11	3	3	30	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1021	58.7	29. V	30	67	160	6	–	–	32	187	217	152	31	42	132	25

Grodków

$H_s = 176\,m$ $h_w = 13{,}6\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◐	◓	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8	1.6	5.5	1.2	14	1.7	4.5	3.6	7.5	5.2	18	3.4	6.5	3.3	8	1.9	21	2.1	35	8.9	31	·	2	27	·	1	·	1	15	15	9	·	6	15	·
II	12.5	2.9	8	1.4	2.5	1.4	·	·	1	2.0	11	5.3	10	4.0	3.0	3.2	9	2.9	28	8.9	17	7	21	26	·	1	·	1	17	17	7	·	1	27	·
III	15	2.2	4.5	1.4	2	2.0	7	2.7	3	1.7	15	2.9	6.5	2.1	24	1.7	16	1.8	32	8.9	6	5	4	18	·	·	·	4	12	8	7	·	6	15	·
IV	13.5	1.9	15.5	1.9	12	2.7	4.5	2.9	3.5	4.6	7.5	3.6	6.5	3.2	2.5	2.5	2	2.5	67	21.1	19	·	·	1	·	·	·	4	16	14	12	3	1	·	3
V	12.5	2.3	15.5	2.5	7.5	2.5	2.5	3.2	1	2.0	6.5	4.0	9	4.1	28.5	3.0	10	2.6	135	28.6	28	·	·	2	·	·	·	2	18	21	14	4	2	·	4
VI	14	1.8	10	1.2	8	2.2	6.5	3.2	3	4.7	9	2.2	7	3.1	21.5	3.0	11	2.2	80	19.2	22	·	·	·	5	·	·	8	9	16	10	3	2	·	3
VII	6	1.8	8	1.4	8	1.9	1	5.0	7	2.8	18.5	3.0	16.5	2.5	14	1.9	14	2.0	103	16.0	17	·	·	·	5	1	·	·	11	21	12	5	·	·	5
VIII	19	1.8	5	1.0	9.5	2.5	6.5	3.9	0.5	2.0	7	2.3	5.5	1.6	26	1.8	14	1.7	61	16.7	9	·	·	·	9	1	·	7	8	9	7	2	·	·	1
IX	4	2.2	1	1.0	27.5	2.6	9	5.3	1.5	2.3	7	3.1	3.5	2.1	14.5	2.0	22	2.1	63	45.5	28	·	·	·	2	3	·	8	7	11	6	1	·	·	2
X	9	1.8	9	1.4	7	1.7	3	2.3	4	2.0	15.5	2.8	1.5	2.0	14	1.5	30	1.3	3	2.0	16	·	·	8	·	·	·	8	6	6	1	·	9	·	·
XI	2.5	2.4	11.5	2.7	7	2.1	8	3.4	6.5	5.4	9	5.8	6	2.6	19.5	2.4	20	2.5	31	11.3	11	1	7	19	·	·	·	1	18	11[2]	6	1	7	14	·
XII	1	2.0	3	1.2	10.5	2.0	12.5	2.9	9.5	4.1	30	4.5	11.5	3.1	10	2.1	5	3.2	49	13.2	25	1	1	17	·	2	·	·	15	13	9	1	4	6	·
Rok	117	2.1	96.5	1.5	115.5	2.1	65	3.2	48	3.2	154	3.6	90	2.8	235	2.2	174	2.2	687	45.5	28. IX	14	35	118	21	9	·	44	152	162[2]	100	20	38	77	18

Sandomierz

$H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w =$ 20,6 m anemometr M-47; 20,1 m wiatromierz Wilda

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◐	◓	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	3.6	11.5	4.2	5	3.1	16	2.6	11.5	2.7	24	3.8	9.5	4.4	10	5.8	1	3.7	60	10.4	3	5	12	31	·	2	·	5	20	16	12	2	7	31	·
II	13	4.7	14	5.4	1	4.5	·	·	·	·	17.5	4.8	18.5	4.6	19	4.6	1	4.8	32	9.1	8	16	21	28	·	1	·	2	14	18	10	·	3	28	·
III	7.5	3.6	10	4.7	4	3.4	12	2.8	14	2.5	25.5	3.1	11	4.2	9	3.0	·	3.3	34	7.0	17	3	6	21	·	·	·	5	10	14	8	·	8	20	·
IV	6.5	4.2	9	3.8	11	5.4	23	4.8	10	3.6	12.5	3.4	7.5	4.9	7.5	4.8	3	4.2	33	5.6	26, 27	·	·	8	·	1	·	2	14	14	11	·	1	·	2
V	14	4.2	10.5	2.9	10.5	4.0	12	3.4	4.5	2.4	18.5	3.0	7.5	5.4	13.5	3.9	2	3.6	54	10.8	23	·	·	3	2	2	·	2	13	17	14	1	5	·	3
VI	10.5	4.5	7	4.1	8	3.9	9	3.4	7	2.8	14.5	2.7	14.5	4.0	16.5	4.8	3	3.7	61	11.5	10	·	·	·	7	·	·	1	7	13	11	2	·	·	4
VII	2.5	1.8	6	3.4	5.5	2.9	9	3.5	4.5	2.8	25.5	2.9	23	4.1	13	2.9	4	3.1	137	46.9	18	·	·	·	11	·	·	3	6	18	14	3	·	·	6
VIII	8.5	5.2	6	4.7	3.5	2.1	7.5	2.1	7	2.4	17.5	2.8	14	3.0	22	4.1	7	3.1	155	50.4	26	·	·	·	9	3	·	8	10	15	11	5	1	·	·
IX	7	2.6	0.5	1.0	2	3.0	21	2.7	18	2.6	25.5	3.5	9	3.6	6	3.0	1	3.0	55	15.7	11	·	·	·	4	·	·	8	5	10	9	3	2	·	1
X	8.5	3.1	11	3.0	7	3.3	9.5	1.7	4	1.8	18.5	4.3	17	4.2	15.5	3.8	2	3.4	5	2.4	31	·	·	7	·	·	·	6	9	6	2	·	8	·	·
XI	7	3.6	6	5.6	8.5	5.6	10	4.0	12	3.5	18.5	4.1	13	4.7	11	4.7	4	4.2	40	9.6	11	5	11	22	·	3	·	·	19	20	11	·	5	17	·
XII	3	4.0	3.5	4.4	4	3.2	10	2.2	9.5	2.9	38	4.2	22	4.1	3	4.3	·	3.8	38	15.5	18	2	4	23	·	·	·	·	19	14	8	1	2	16	·
Rok	92.5	3.8	95	3.9	70	3.7	139	2.8	102	2.5	256	3.6	166.5	4.3	146	4.1	28	3.7	704	50.4	26. VIII	31	54	143	33	12	·	42	146	175	121	17	42	112	16

Opole

$\varphi = 50°40'$ $\lambda = 17°58'$ **1965**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	990.8	1004.9	970.2	1013.1	2.3	−2.6	7.2	29	−10.2	8	−1.1	1.4	−0.5	−0.2	5.2	5.7	5.4	5.4	92	84	91	89	0.5	1.2	0.5	0.7	7.8	7.9	7.2	7.6
II	996.0	1009.9	975.1	1018.8	−1.4	−8.2	3.8	13, 14	−19.1	6	−5.9	−3.0	−5.1	−4.8	3.6	4.0	3.7	3.8	89	80	86	85	0.5	1.0	0.6	0.7	9.0	8.0	7.0	8.0
III	995.6	1011.5	968.3	1017.8	7.1	−2.5	17.2	30	−18.7	9	−1.5	6.1	1.8	2.0	5.4	6.3	6.1	5.9	90	65	83	79	0.6	3.8	1.2	1.9	7.3	6.1	5.1	6.2
IV	989.4	1009.3	976.4	1011.1	12.1	2.9	17.3	6	−2.1	16	4.6	10.7	6.5	7.1	7.7	7.8	8.1	7.9	89	62	83	78	0.9	5.4	1.7	2.7	7.7	7.2	6.3	7.1
V	992.8	1007.0	979.5	1014.2	15.5	6.4	24.9	17	−2.1	3	9.3	13.6	10.2	10.8	10.4	11.1	10.7	10.7	87	71	84	81	1.5	4.9	1.9	2.8	7.5	8.4	7.2	7.7
VI	993.4	1003.8	982.2	1014.5	21.5	10.8	32.2	26	5.0	3	14.9	19.8	15.4	16.4	14.6	16.0	15.3	15.3	86	70	87	81	2.6	8.1	2.5	4.4	6.2	7.2	6.4	6.6
VII	992.0	999.7	980.7	1013.0	22.0	12.3	30.4	15	4.8	5	15.3	20.1	15.6	16.6	15.0	16.8	16.0	15.9	86	71	89	82	2.6	7.6	2.1	4.1	7.2	7.7	6.3	7.1
VIII	995.3	1002.1	984.7	1016.4	22.2	10.6	31.2	8	5.8	31	13.4	20.7	15.3	16.2	13.3	13.2	13.8	13.4	86	55	79	73	2.5	12.3	3.9	6.2	5.6	5.7	5.6	5.6
IX	994.2	1013.8	982.0	1015.4	21.3	10.0	28.6	3	4.4	22	12.0	20.0	13.8	14.9	12.5	13.6	13.3	13.1	88	59	84	77	2.0	10.4	2.8	5.1	4.7	5.7	4.3	4.9
X	1002.2	1014.9	992.1	1024.1	14.2	2.5	23.2	2	−7.5	22	4.0	12.9	6.6	7.5	7.9	9.5	8.9	8.8	93	63	88	81	0.6	6.0	1.3	2.6	5.6	4.6	3.7	4.6
XI	990.7	1010.9	965.6	1013.0	3.6	−3.1	15.2	2	−12.6	18	−1.2	2.0	−0.1	0.2	5.2	5.8	5.6	5.5	89	80	88	86	0.8	1.8	0.8	1.1	8.1	7.6	7.5	7.7
XII	985.9	1005.1	966.4	1008.0	3.7	−1.2	12.0	19	−8.9	15	0.6	2.5	1.1	1.3	5.7	6.0	5.6	5.8	87	82	85	85	0.9	1.4	1.2	1.2	8.7	8.1	7.0	7.9
Rok	993.2	1014.9	965.6	1015.0	12.0	3.2	32.2	26.VI	−19.1	6.II	5.4	10.6	6.7	7.4	8.9	9.6	9.4	9.3	88	70	86	81	1.3	5.3	1.7	2.8	7.1	7.0	6.1	6.7

Lubliniec

$\varphi = 50°40'$ $\lambda = 18°41'$

I	—	—	—	—	1.8	−4.3	6.6	30	−15.4	7	−1.9	1.1	−1.1	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	6.8	7.2	7.4
II	—	—	—	—	−2.2	−10.1	2.4	14	−23.2	6	−7.6	−3.4	−6.4	−6.0	—	—	—	—	—	—	—	—	—	—	—	—	9.2	6.8	7.1	7.7
III	—	—	—	—	6.5	−3.3	16.8	30	−16.7	11	−1.3	5.7	0.7	1.4	—	—	—	—	—	—	—	—	—	—	—	—	7.7	5.1	5.7	6.2
IV	—	—	—	—	10.9	2.6	15.8	6	−3.2	2	4.4	9.8	5.8	6.4	—	—	—	—	—	—	—	—	—	—	—	—	7.6	6.3	6.5	6.8
V	—	—	—	—	15.0	6.0	23.5	17	−2.1	3	9.0	13.6	9.7	10.5	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.0	6.9	6.6
VI	—	—	—	—	21.3	10.4	33.3	26	5.4	3	14.9	20.0	14.9	16.2	—	—	—	—	—	—	—	—	—	—	—	—	4.7	4.8	6.5	5.3
VII	—	—	—	—	21.6	11.5	30.6	14	5.0	5	15.5	19.9	15.1	16.4	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.1	6.8	6.2
VIII	—	—	—	—	21.0	10.4	29.9	7	4.5	28	14.1	19.9	14.5	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.6	5.7	5.7
IX	—	—	—	—	20.7	9.3	27.9	3	3.2	20	11.7	19.4	13.6	14.6	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.9	4.8	5.0
X	—	—	—	—	13.6	2.7	22.3	1, 2	−5.9	22	4.3	12.8	6.0	7.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	5.8	5.0	6.2
XI	—	—	—	—	2.9	−3.5	11.8	2	−14.1	18	−1.8	1.7	−0.8	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	9.2	8.4	8.1	8.6
XII	—	—	—	—	2.8	−1.9	8.5	20	−9.5	14	−0.2	1.8	0.3	0.6	—	—	—	—	—	—	—	—	—	—	—	—	9.3	8.5	7.7	8.5
Rok	—	—	—	—	11.3	2.5	33.3	26.VI	−23.2	6.II	5.1	10.2	6.0	6.8	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.3	6.5	6.7

Ostroszowice

$\varphi = 50°39'$ $\lambda = 16°38'$

I	—	—	—	—	2.6	−2.0	7.1	17	−12.4	7	−0.7	1.3	0.3	0.3	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.1	8.6	8.3
II	—	—	—	—	−1.9	−8.3	2.6	14	−20.1	6	−5.4	−3.5	−4.8	−4.6	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.5	7.0	7.6
III	—	—	—	—	5.3	−2.7	15.7	30	−20.9	9	−0.8	4.1	0.9	1.3	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.4	6.3	6.5
IV	—	—	—	—	10.2	3.2	16.5	3	−2.1	2	4.8	8.7	5.9	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.4	8.1	7.5
V	—	—	—	—	13.7	6.3	22.0	17	−1.0	2	8.6	12.2	9.2	9.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.7	7.4	7.4
VI	—	—	—	—	19.9	10.7	31.6	26	5.7	13	14.5	18.5	13.9	15.2	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.9	5.8	6.2
VII	—	—	—	—	19.9	12.2	30.5	14	7.7	4	14.5	18.2	14.6	15.5	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.5	6.3	7.1
VIII	—	—	—	—	19.9	10.7	29.2	6	5.4	16	13.4	18.4	13.7	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.0	5.5	5.6
IX	—	—	—	—	18.9	10.2	24.5	3	5.5	21	12.4	17.5	13.4	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.2	5.3	3.7	4.7
X	—	—	—	—	13.2	3.7	21.7	2	−5.4	22	5.4	12.2	6.5	7.6	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.5	4.1	4.6
XI	—	—	—	—	3.5	−3.1	13.4	1	−11.4	17	−0.8	1.9	−0.3	0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.1	8.1	8.1
XII	—	—	—	—	3.5	−1.3	10.4	19	−14.0	14	0.8	1.9	0.9	1.1	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.3	6.4	7.4
Rok	—	—	—	—	10.7	3.3	31.6	26.VI	−20.9	9.III	5.6	9.3	6.2	6.8	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.9	6.4	6.7

Szczekociny

$\varphi = 50°38'$ $\lambda = 19°49'$

I	—	—	—	—	0.8	−5.1	5.6	1	−13.4	12	−2.8	−0.2	−2.0	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−3.0	−10.9	1.9	12	−22.6	7	−7.6	−3.8	−6.8	−6.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	4.5	−4.3	16.6	30	−16.1	1	−2.2	4.1	−0.5	0.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	9.1	1.6	14.5	4	−2.2	6	3.6	8.8	5.2	5.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	13.5	5.1	23.5	19	−4.0	4	8.7	12.9	9.3	10.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	—	10.0	—	—	5.2	4	14.3	19.4	14.3	15.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	—	10.8	—	—	4.5	5	15.1	19.8	14.1	15.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	20.4	9.6	30.3	7	4.5	17, 29	12.9	19.0	13.4	14.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	20.6	8.4	26.4	3	3.5	22	11.2	19.0	12.3	13.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.9	2.2	20.7	2	−6.3	22	4.9	12.1	6.0	7.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	2.7	−3.9	13.0	2	−20.7	18	−2.0	1.2	−0.9	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	3.1	−1.8	9.3	19, 20	−9.1	15	0.0	1.9	0.5	0.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	1.8	—	—	−22.6	7.II	4.7	9.5	5.4	6.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Opole

$H_s = 176\ m$ $H_b = 177{,}9\ m$ $h_w =$ 13,5 m wiatromierz Wilda; 15 m anemometr

1965

MIESIĄC	ROZKŁAD WIATRU (D,V=D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	V≥15	◔	◕	Opad R ≥5	≥10	≥10.0	≡	⊠	K (K)
I	4.5	4.3	·	·	4.5	1.9	11	4.2	30.5	5.0	12.5	5.9	15	5.3	12	3.7	3	4.5	43	6.8	31	2	2	28	·	4	·	1	17	17	11	·	7	23	·
II	14.5	6.7	4.5	5.2	2	2.5	2.5	2.6	6	4.6	9	3.7	25	6.0	14.5	6.1	6	5.1	26	3.4	17	8	20	27	·	2	1	·	15	23	13	·	2	28	·
III	4.5	2.6	3.5	4.1	0.5	2.0	7.5	2.3	26	1.9	9.5	2.9	19.5	2.3	8	3.1	14	2.1	22	9.1	6	3	5	19	·	·	·	4	10	11	5	·	8	15	·
IV	9	3.7	7.5	4.7	12	3.9	9.5	2.9	9.5	5.4	6	3.3	17.5	4.8	16	2.7	3	3.8	56	11.6	19	·	·	4	·	2	·	3	14	16	13	2	1	·	2
V	2	7.0	16	4.4	7	3.5	8.5	4.5	4.5	2.9	10.5	4.5	25.5	4.9	14	5.2	5	4.4	138	20.6	29	·	·	3	·	1	·	·	15	18	18	5	2	·	9
VI	6.5	4.5	7.5	4.2	8	3.4	8.5	3.8	12	4.7	12	3.9	19	4.7	14.5	5.7	2	4.4	72	18.6	10	·	·	·	6	2	·	1	11	17	13	1	2	·	6
VII	2	6.0	4.5	4.4	4	4.2	19	3.3	16.5	3.8	28	4.0	11.5	5.1	6.5	3.0	1	3.9	50	11.2	8	·	·	·	7	2	·	·	9	18	11	1	2	·	5
VIII	3	3.5	4	4.8	6.5	2.1	19	4.4	10.5	4.4	9.5	3.2	18	5.3	15.5	5.0	7	4.0	48	14.0	25	·	·	·	8	4	·	3	6	13	10	1	·	·	4
IX	0.5	4.0	·	·	5	2.5	36	4.2	18	4.1	8.5	3.9	12.5	4.4	3.5	5.1	6	3.8	43	14.1	28	·	·	·	3	4	·	8	4	10	8	1	2	·	2
X	2.5	1.6	7	1.4	7.5	1.6	9.5	1.5	8.5	1.8	10	3.8	14	3.6	6	2.2	28	1.7	-2	1.3	29	·	·	10	·	·	·	8	5	3	1	·	14	·	·
XI	4	2.2	7.5	3.5	2	2.2	10.5	3.1	9.5	3.4	12	2.8	14	1.9	2.5	2.6	28	1.9	29	5.3	21	3	9	22	·	3	·	2	19	16	8	·	8	16	·
XII	1	1.5	1.5	1.3	4.5	2.0	22	2.4	21.5	2.7	22	2.6	11.5	2.4	5	2.0	4	2.4	49	13.3	18	·	1	19	·	2	·	·	17	16	12	1	·	9	·
Rok	54	4.0	63.5	3.2	63.5	2.6	163.5	3.3	173	3.7	149.5	3.7	203	4.2	118	3.9	107	3.5	578	20.6	29. V	16	37	132	24	26	1	30	142	178	123	12	48	91	28

Uwaga. Kierunki i prędkości wiatru w ciągu roku – częściowo wg wiatromierza Wilda, częściowo wg anemometru. M-47

Lubliniec

$H_s = 256\ m$ $h_w = 12{,}5\ m$

I	11.5	2.2	2	2.0	·	·	9	1.4	13.5	1.7	29	2.4	12.5	2.3	13.5	1.6	2	2.0	45	8.9	31	2	7	30	·	·	·	·	16	16	9	·	5	31	—
II	15.5	3.2	3.5	1.9	2	1.0	·	·	·	·	11	2.3	17.5	2.5	27.5	2.0	7	2.2	33	5.4	14	15	23	28	·	1	·	·	15	23	11	·	4	28	—
III	11	2.3	5	2.4	1	2.0	6	1.4	7.5	1.7	20.5	2.0	23	2.1	17	1.7	2	1.9	33	6.4	6	4	5	20	·	·	·	1	9	16	11	·	4	16	—
IV	20.5	2.0	9	2.6	16	2.2	9	1.8	4.5	2.6	5	3.0	9.5	1.5	16.5	1.9	·	2.1	45	11.9	23	·	·	6	·	·	·	1	12	11	9	1	2	·	—
V	26.5	1.9	6.5	2.0	6.5	1.6	5	2.7	2	3.0	5	2.3	15	2.8	25.5	2.1	1	2.2	111	18.0	29	·	·	3	·	1	1	·	13	20	17	3	·	·	—
VI	17.5	1.9	7.5	2.6	8.5	1.6	3	1.2	1.5	4.0	13	3.0	14	2.5	25	2.3	·	2.3	82	15.8	11	·	·	·	6	·	·	1	8	14	10	4	·	·	—
VII	4.5	1.6	3.5	1.4	6.5	2.2	2	2.8	2	1.8	18.5	2.5	29	2.6	21	2.1	6	2.2	66	21.9	17	·	·	·	6	·	·	1	7	16	11	1	·	·	—
VIII	17.5	1.5	3.5	1.1	2	1.0	1.5	1.7	5.5	2.5	12.5	2.7	13.5	2.0	32	2.0	5	1.8	54	11.9	24	·	·	·	9	·	·	3	8	11	9	3	2^2	·	—
IX	5	1.6	3	1.0	1.5	1.0	7.5	1.9	15.5	2.2	14	2.0	17.5	1.8	21	1.5	5	1.7	43	13.1	4	·	·	·	2	·	·	2	1	8	7	1	1	·	—
X	15.5	1.7	7.5	1.1	12	1.5	4.5	1.2	1.5	1.3	14.5	1.6	10.5	1.7	22	1.6	5	1.5	4	2.1	16	·	·	7	·	·	·	·	6	4	2	·	10	·	—
XI	4.5	2.2	9.5	2.9	6.5	1.7	9	1.4	3.5	3.3	19	2.3	16.5	2.7	14.5	1.7	7	2.1	26	5.9	3	4	10	23	·	·	·	·	20	18	9	·	5	18	—
XII	3.5	2.0	3	1.3	·	·	·	·	4.5	2.8	45	3.1	24.5	2.7	9.5	1.7	3	2.6	56	17.5	18	·	4	21	·	·	·	·	21	17	13	1	·	11	—
Rok	153	2.0	63.5	1.9	62.5	1.3	56.5	1.5	61.5	2.2	207	2.4	203	2.3	245	1.8	43	2.0	598	21.9	17. VII	25	49	138	23	2	1	9	136	174	118	14	33^2	104	—

Ostraszowice

$H_s = 375\ m$ $h_w = 12{,}5\ m$

I	1.5	3.0	·	·	·	·	3	6.7	12	3.1	25	5.0	26	6.8	25.5	2.5	·	4.6	36	7.6	31	1	4	24	·	9	6	·	19	17	10	·	1	14	·
II	4.5	2.8	·	·	1.5	1.0	3.5	1.0	1	2.0	3	11.5	23.5	8.2	42	4.0	5	4.9	39	8.1	17	8	21	27	·	9	6	2	14	24	15	·	2	28	·
III	5.5	2.8	0.5	2.0	0.5	3.0	1.5	3.0	7	3.1	15	3.9	28.5	4.9	28.5	2.2	6	3.3	36	7.7	6	5	6	18	·	5	1	3	12	13	9	·	4	16	·
IV	8.5	2.4	2	1.0	3	1.7	5.5	1.5	4.5	1.7	12.5	4.2	21.5	3.7	31.5	2.1	1	2.7	81	15.2	20	·	·	3	·	3	1	3	19	17	15	2	·	·	1
V	2.5	2.8	2	2.5	6	1.0	1.5	3.0	6	3.5	6	4.4	21.5	3.7	39.5	2.6	8	2.7	227	55.5	29	·	·	3	·	1	·	2	16	25	20	8	·	·	5
VI	5.5	1.8	5	1.0	1	1.0	2	1.5	1.5	2.3	18.5	4.1	23.5	2.7	27	3.0	6	2.7	131	23.9	26	·	·	·	5	3	2	1	11	14	14	6	·	·	7
VII	4.5	1.0	1.5	1.0	·	·	·	·	2	2.5	19.5	3.7	45	3.5	15.5	2.1	5	2.9	84	12.8	18	·	·	·	3	1	1	·	13	21	16	2	·	·	8
VIII	4.5	1.1	·	·	·	·	0.5	1.0	6	2.8	16	4.0	24	3.3	37	2.1	5	2.6	70	17.9	6	·	·	·	6	3	·	3	5	12	7	4	·	·	3
IX	0.5	5.0	0.5	5.0	·	·	1.5	2.7	20	3.3	24	3.3	19	4.0	13.5	1.9	11	2.8	45	20.5	28	·	·	·	·	1	1	7	6	10	5	2	·	·	2
X	1.5	1.3	6	1.7	·	·	5	1.0	8	1.9	7	2.8	23	3.9	19.5	1.9	23	1.9	6	3.7	16	·	·	7	·	2	·	7	8	4	2	·	2	·	·
XI	1.5	1.3	8.5	1.7	1.5	1.0	2.5	2.0	10	4.0	11.5	6.7	24	5.0	18.5	1.7	12	3.2	65	23.9	27	2	9	23	·	7	5	1	18	17	10	3	4	15	·
XII	0.5	5.0	·	·	·	·	2.5	2.8	9.5	3.0	19.5	9.2	47	6.3	12	1.8	2	5.8	45	12.8	13	2	2	18	·	13	9	1	15	16	7	1	2	15	·
Rok	41	2.5	26	1.3	13.5	0.7	29	2.2	87.5	2.8	177.5	5.2	326.5	4.7	310	2.3	84	3.3	865	55.5	29. V	18	42	123	14	57	32	30	156	190	130	28	15	88	26

Szczekociny

$H_s = 262\ m$ $h_w = 14\ m$

I	3.5	5.1	4.5	3.1	2.5	3.0	15.5	3.0	7	3.8	17.5	5.3	8.5	5.4	8	3.9	26	3.0	46	8.2	31	5	12	28	·	2	·	—	—	15	11	·	·	27	·
II	11	5.6	2	4.5	2.5	2.2	3.5	2.4	2.5	6.0	13	9.0	19.5	5.1	15	5.4	15	4.7	27	6.1	14	15	23	28	·	5	·	—	—	21	14	·	·	28	·
III	4.5	7.1	5	4.7	4.5	4.0	16	3.3	6	3.3	5	7.9	10.5	4.6	6.5	3.8	35	2.8	23	4.5	26	8	5	21	·	3	·	—	—	16	7	·	4	18	·
IV	3	3.3	8.5	4.1	21	5.0	12.5	2.9	4	3.1	4	3.8	11.5	4.5	8.5	4.1	17	3.3	37	7.5	23	·	·	9	·	1	·	—	—	15	11	·	·	·	1
V	9	4.2	2.5	5.0	8	5.1	7.5	3.1	4	2.8	8	4.3	15.5	3.3	16.5	3.5	22	2.9	113	17.3	19	·	·	4	·	1	1	—	—	22	19	3	1	·	5
VI	6.5	3.5	4	4.4	9	3.2	6.5	4.2	3	5.5	9	5.1	11	3.3	14	2.9	27	2.6	163	35.0	6	·	·	·	—	1	·	—	—	14	14	6	·	·	6
VII	3	2.5	1.5	2.7	6	3.8	4	4.1	5	2.9	21	3.8	20.5	3.9	3	2.8	29	2.5	112	79.2	17	·	·	·	—	·	·	—	—	16	9	1	·	·	4
VIII	6.5	2.8	3.5	4.1	1.5	2.7	11.5	3.3	5.5	3.0	4.5	3.3	10.5	3.2	13.5	3.4	36	2.0	91	26.7	25	·	·	·	5	·	·	—	—	17	14	2	·	·	2
IX	0.5	2.0	0.5	2.0	5.5	3.0	22	3.5	9	3.2	6.5	3.4	7.5	3.5	6.5	3.1	32	2.1	77	22.8	4	·	·	·	2	·	·	—	—	10	7	3	4	·	2
X	4.5	3.2	4.5	3.3	4.5	2.6	3.5	2.4	3	3.8	16	4.5	11	3.4	8	3.5	38	2.1	4	2.3	31	·	·	8	·	·	·	—	—	4	1	·	4	·	·
XI	2.5	4.2	8.5	5.7	3	4.3	16	3.8	5.5	4.9	12.5	7.1	11	5.5	4	4.6	27	3.6	26	8.0	3	5	10	22	·	2	·	—	—	19	7	·	2	12	·
XII	3	5.0	·	·	1	3.0	12.5	3.4	12	5.8	37	6.6	11.5	5.0	6	4.8	10	5.0	31	11.9	18	·	6	22	·	6	·	—	—	13	8	1	·	7	·
Rok	57.5	4.0	45	3.6	69	3.5	131	3.3	66.5	4.0	154	5.3	148.5	4.2	109.5	3.8	314	3.0	750	79.2	17. VII	33	56	142	—	21	1	—	—	182	122	16	15	92	20

Skroniów

φ = 50°38′ λ = 20°16′

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																				
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	-6.1	4.3	17	-18.5	11	-3.8	-0.8	-2.7	-2.5	4.3	5.0	4.6	4.6	88	85	88	87	0.6	0.9	0.6	0.7	8.3	8.2	7.6	8.0
II	–	–	–	–	-3.1	-11.2	2.1	14	-24.0	7	-7.8	-4.3	-7.4	-6.7	3.0	3.5	3.1	3.2	83	76	82	80	0.6	1.0	0.6	0.7	8.4	7.3	6.7	7.5
III	–	–	–	–	4.3	-4.2	16.1	30	-16.2	1	-2.5	3.1	-0.4	0.0	4.8	5.4	5.2	5.1	87	69	82	79	0.6	2.6	1.0	1.4	7.9	6.4	5.3	6.5
IV	–	–	–	–	10.1	1.8	15.1	7	-2.1	15	3.5	9.0	5.1	5.7	7.1	7.4	7.3	7.3	89	66	83	79	0.9	4.4	1.6	2.3	8.6	8.1	6.5	7.7
V	–	–	–	–	14.7	5.4	26.7	19	-3.8	4	8.5	13.3	9.4	10.2	9.7	9.8	10.2	9.9	85	63	84	77	1.7	6.0	2.0	3.2	6.8	8.4	7.3	7.5
VI	–	–	–	–	20.9	10.3	30.5	26	5.5	3	14.2	19.5	14.5	15.7	13.3	13.0	13.9	13.4	81	59	83	74	3.1	10.4	2.9	5.5	5.1	6.1	7.1	6.1
VII	–	–	–	–	21.5	11.2	28.3	17	6.3	11	15.0	20.1	14.7	16.1	14.5	14.1	14.8	14.5	84	60	88	77	2.7	10.4	2.2	5.1	6.6	7.6	6.1	6.8
VIII	–	–	–	–	20.4	10.0	30.4	7	5.6	31	12.9	18.9	13.7	14.8	13.2	13.0	13.4	13.2	88	61	85	78	1.9	9.8	2.6	4.8	5.3	6.7	6.2	6.1
IX	–	–	–	–	20.3	8.8	25.8	3	4.9	23	10.8	18.9	12.9	13.9	12.3	13.2	13.1	12.9	93	61	88	81	1.0	9.1	2.0	4.0	5.0	5.8	5.1	5.3
X	–	–	–	–	12.2	2.5	20.9	2	-5.7	22	4.1	11.4	6.1	6.9	8.0	8.9	8.7	8.5	93	66	89	83	0.6	5.0	1.1	2.2	5.9	4.8	4.8	5.2
XI	–	–	–	–	2.0	-3.9	12.7	2	-17.1	18	-2.2	0.6	-1.0	-0.9	4.9	5.4	5.4	5.2	88	79	88	85	0.6	1.4	0.7	0.9	8.7	7.4	8.2	8.1
XII	–	–	–	–	2.5	-2.6	9.0	19, 20	-12.9	16	-0.5	1.4	0.0	0.2	5.3	5.4	5.3	5.3	86	79	85	83	0.8	1.5	0.9	1.1	8.2	8.0	7.9	8.0
Rok	–	–	–	–	10.5	1.8	30.5	26.VI	-24.0	7, 11	4.4	9.3	5.4	6.1	8.4	8.7	8.8	8.6	87	69	85	80	1.3	5.2	1.5	2.7	7.1	7.1	6.6	6.9

Staszów

φ = 50°34′ λ = 21°10′

I	–	–	–	–	0.7	-6.0	4.9	30	-15.1	11	-3.5	-0.5	-2.7	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.5	7.6
II	–	–	–	–	-2.5	-12.8	2.9	14	-29.2	7	-8.5	-4.2	-8.0	-7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.2	6.6	6.8
III	–	–	–	–	5.0	-5.6	16.7	30	-23.7	1	-3.4	3.5	-0.9	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.3	5.8	6.6
IV	–	–	–	–	10.7	1.4	16.5	7	-2.6	7	3.4	8.6	5.7	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.9	6.9	7.6
V	–	–	–	–	15.6	5.1	27.7	19	-4.8	4	8.4	14.0	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.8	6.2	6.8
VI	–	–	–	–	21.4	9.7	30.8	26	3.3	3	14.5	19.9	14.6	15.9	–	–	–	–	–	–	–	–	–	–	–	–	4.0	5.7	6.0	5.2
VII	–	–	–	–	21.9	10.4	29.0	15	3.9	10	14.9	20.2	15.3	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.8	5.5	5.9
VIII	–	–	–	–	20.9	9.3	30.2	7	4.1	3	12.6	19.4	13.8	14.9	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.8	4.6	5.1
IX	–	–	–	–	21.0	7.7	26.7	2	2.3	17, 22	10.5	19.3	12.7	13.8	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.5	3.0	3.8
X	–	–	–	–	12.6	0.4	21.2	1	-6.2	23	2.9	11.5	5.4	6.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.4	4.6	5.4
XI	–	–	–	–	2.2	-4.1	14.4	2	-18.5	18	-2.3	0.5	-0.8	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.4	8.3	8.3
XII	–	–	–	–	2.6	-3.0	7.6	20	-16.6	16	-0.7	1.4	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	7.5	7.7
Rok	–	–	–	–	11.0	1.0	30.8	26.VI	-29.2	7, 11	4.1	9.5	5.4	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	6.0	6.4

Paturzyn

φ = 50°34′ λ = 23°56′

I	–	–	–	–	-0.7	-6.3	3.3	1, 30	-19.3	11	-4.0	-1.2	-3.6	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	-4.7	-11.4	0.9	14	-21.8	7	-8.2	-5.2	-7.8	-7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.9	-3.6	14.7	30	-17.2	1	-2.2	3.0	-0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	9.3	2.0	16.6	26	-2.4	3	3.6	8.1	5.1	5.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.4	6.3	27.2	19	-1.6	4	8.8	13.9	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.9	11.2	28.4	26	6.3	3, 8	14.9	20.0	15.4	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.2	11.5	28.2	16, 17	7.3	7, 10	15.6	20.7	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.4	10.4	29.4	8	6.5	29	13.4	19.7	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.5	8.6	27.4	3, 4	4.4	17	10.9	19.8	13.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	11.6	2.4	21.2	1	-3.8	22	4.4	11.1	6.0	6.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.4	-4.3	14.3	2	-19.4	18	-2.2	0.5	-1.4	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1.5	-2.6	6.4	10	-17.4	17	-1.1	0.7	-0.7	-0.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.1	2.0	29.4	8.VIII	-21.8	7, 11	4.5	9.3	5.4	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Tarnobrzeg

φ = 50°34′ λ = 21°40′

I	–	–	–	–	1.1	-5.4	7.0	30	-15.3	12	-3.2	-0.7	-2.6	-2.2	4.6	5.1	4.7	4.8	92	84	90	89	0.4	1.0	0.5	0.6	8.3	7.7	7.5	7.8
II	–	–	–	–	-2.4	-10.7	3.7	14	-24.8	7	-7.8	-4.3	-6.9	-6.5	3.2	3.5	3.2	3.3	89	77	83	83	0.4	1.1	0.6	0.7	8.3	6.3	6.7	7.1
III	–	–	–	–	5.9	-4.0	17.5	30	-18.2	1	-2.5	4.1	0.8	0.8	4.9	5.5	5.5	5.3	89	66	82	79	0.6	3.1	1.2	1.6	7.8	6.6	4.8	6.4
IV	–	–	–	–	11.7	2.6	17.0	7	-1.5	6	4.3	9.4	6.4	6.6	7.1	7.4	7.4	7.3	84	63	75	74	1.3	4.7	2.4	2.8	8.1	8.2	6.7	7.7
V	–	–	–	–	16.3	6.2	27.8	19	-1.8	4	8.9	14.6	10.5	11.1	9.6	9.6	10.5	9.9	82	57	80	73	2.1	7.7	2.5	4.1	7.6	8.4	6.3	7.4
VI	–	–	–	–	22.5	11.6	32.0	26	6.3	8	14.9	20.5	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.3	5.4	5.6
VII	–	–	–	–	22.8	12.2	30.5	16	5.7	11	15.3	21.1	16.0	17.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	7.3	5.3	5.9
VIII	–	–	–	–	21.6	11.0	31.0	8	7.5	3, 31	13.2	19.7	14.8	15.6	13.8	13.2	14.1	13.7	90	59	83	77	1.6	10.9	3.4	5.3	5.5	6.3	5.1	5.6
IX	–	–	–	–	21.8	9.4	26.9	2	3.9	16	11.5	19.9	13.5	14.6	12.3	13.4	13.6	13.1	90	59	87	79	1.6	10.3	2.2	4.7	4.4	5.3	2.5	4.1
X	–	–	–	–	12.8	2.8	22.5	1	-4.3	22	4.1	11.4	6.6	7.2	8.0	9.7	9.0	8.9	95	70	89	85	0.5	4.3	1.1	2.0	6.0	5.7	4.6	5.4
XI	–	–	–	–	2.6	-3.3	15.2	2	-17.1	18	-1.7	0.8	-0.6	-0.5	5.1	5.8	5.6	5.5	89	84	90	88	0.7	1.1	0.7	0.8	8.5	7.9	8.0	8.1
XII	–	–	–	–	2.9	-2.3	7.5	10, 20	-14.6	17	-0.5	1.7	0.1	0.4	5.4	5.7	5.3	5.5	89	82	84	85	0.7	1.3	1.0	1.0	7.6	7.8	7.3	7.6
Rok	–	–	–	–	11.6	2.5	32.0	26.VI	-24.8	7, 11	4.7	9.9	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	5.8	6.5

Skroniów — $H_s = 256\ m$ — $h_w = 16{,}5\ m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%D, VmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	ℓ Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	8.5	3.6	3	3.7	14.5	2.6	12	2.6	4	4.5	14	4.2	10.5	6.2	13.5	4.7	13	3.4	52	9.1	2	6	13	29	·	1	·	2	19	17	11	·	5	31	·
II	11	6.1	7.5	4.6	1	4.5	·	·	·	·	7	8.2	27	5.9	21.5	6.3	9	5.5	16	2.5	14	16	25	28	·	6	2	2	12	18	7	·	2	28	·
III	3	5.3	7	4.4	5.5	2.4	16.5	3.0	5	2.4	4.5	5.8	14.5	4.1	10	5.1	27	2.8	33	7.5	3	5	6	23	·	2	·	3	12	15	6	·	5	18	·
IV	6	3.3	4	5.9	26.5	5.4	13	3.8	5	2.2	4.5	2.7	12	4.9	11	4.1	8	4.0	24	5.0	23	·	·	10	·	·	·	2	16	13	11	·	2	·	1
V	14	2.8	3.5	3.6	14	5.1	7	3.4	2.5	1.8	4	2.2	19	4.7	18	3.7	11	3.4	79	17.7	29	·	·	3	1	3	2	1	17	18	16	2	2	·	5
VI	3.5	4.4	5.5	3.2	15	3.8	5	3.2	2	3.0	5.5	3.9	17	3.8	20.5	3.7	16	3.0	103	40.2	27	·	·	·	6	2	1	2	10	13	12	3	·	·	3
VII	0.5	4.0	4.5	2.4	6.5	3.9	6.5	3.5	3	2.0	8.5	3.3	32	3.6	8.5	3.6	23	2.6	50	14.5	17	·	·	·	6	·	·	3	11	17	12	1	·	·	5
VIII	6.5	4.4	1.5	2.0	2.5	1.8	10.5	3.4	5	2.3	2	2.5	12.5	2.5	21.5	4.2	31	2.3	124	34.4	25	·	·	·	6	·	·	5	11	16	13	4	·	·	4
IX	2	1.0	1	2.0	2	2.8	24.5	2.9	7.5	3.3	5	3.5	12	2.5	10	3.4	26	2.1	78	22.6	29	·	·	·	2	·	·	4	5	11	7	4	3	·	2
X	6.5	2.3	3.5	1.9	4.5	2.2	7.5	2.5	1.5	1.7	6.5	3.4	22	3.7	18	3.5	23	2.3	4	2.2	31	·	·	9	·	·	·	9	10	3	1	·	7	·	·
XI	2.5	2.4	9.5	5.6	11.5	3.8	14	3.3	2	2.5	6	5.7	21.5	5.4	10	3.6	13	3.8	26	6.8	11	5	11	22	·	1	·	·	16	18	7	·	4	12	·
XII	3.5	3.1	·	·	5.5	2.4	14.5	2.5	13	2.8	20.5	5.3	21.5	5.3	10.5	5.3	4	4.0	32	8.9	18	2	3	24	·	2	·	1	19	14	6	·	·	13	·
Rok	67.5	3.6	50.5	3.3	109	3.4	131	2.8	50.5	2.4	88	4.2	221.5	4.4	173	4.3	204	3.3	621	40.2	27.VI	34	58	148	21	17	5	34	158	173	109	14	30	102	20

Staszów — $H_s = 193\ m$ — $h_w = 16{,}2\ m$

I	5.5	3.5	8.5	3.3	12.5	4.0	11	2.4	10	3.0	4	1.6	3.5	3.4	12	4.0	26	2.4	54	10.2	17	7	11	30	·	·	·	2	17	15	11	1	12	31	·
II	11.5	5.6	7.5	5.0	2	5.5	·	·	4	3.0	7	2.9	13.5	4.0	18.5	4.9	20	3.5	11	3.5	7	15	22	28	·	3	·	4	12	16	4	·	8	28	·
III	3	5.0	10	4.1	2	4.5	14	3.2	1.5	2.0	4.5	3.3	5	3.6	11	3.3	42	2.0	28	7.8	3	8	6	24	·	1	·	4	15	12	7	·	11	21	·
IV	3.5	7.3	11.5	3.7	23.5	6.4	8	4.0	2	2.5	3	3.0	7.5	3.5	6	4.1	25	3.5	31	3.9	22	·	·	11	·	4	·	1	16	13	11	·	2	·	1
V	7.5	4.6	8.5	3.8	16.5	4.0	3	3.3	4	2.2	3	3.0	13	3.7	11.5	3.2	26	2.6	63	10.8	29	·	·	5	1	1	·	3	14	16	14	1	4	·	5
VI	4	6.1	5	3.5	14	3.3	6	3.8	·	·	4	2.8	14	3.4	18	4.4	25	2.8	92	16.2	9	·	·	·	6	·	·	4	6	12	11	3	·	·	3
VII	·	·	4.5	2.2	7.5	4.3	7.5	2.5	4.5	2.8	11	2.6	20	2.7	9	3.3	29	2.0	47	8.4	18	·	·	·	9	·	·	4	7	18	14	·	3	·	6
VIII	7	4.4	·	·	3	3.0	9	3.7	5	2.8	3	2.7	3	2.0	26	4.2	37	2.3	108	26.0	1	·	·	·	6	1	·	11	9	14	13	3	3	·	2
IX	·	·	·	·	3	3.0	21.5	3.7	4.5	2.9	6	2.5	3	2.3	6	2.3	46	1.5	64	27.1	29	·	·	·	3	·	·	8	3	11	7	2	8	·	3
X	9	3.4	5	2.8	7	3.0	5	2.0	2.5	2.8	5.5	2.5	5	3.2	14	3.6	40	1.8	2	1.4	31	·	·	17	·	·	·	6	9	3	1	·	11	·	·
XI	1	2.0	11	5.5	9	2.2	15	3.3	6	3.0	4	4.5	13	3.2	17	2.7	14	2.9	29	6.7	11	5	10	20	·	1	·	1	19	17	10	·	8	10	·
XII	3	2.3	2	4.0	5	3.8	18	2.8	11	2.6	14	2.4	7	2.9	9	4.2	24	2.2	38	11.8	18	3	4	25	·	·	·	·	17	13	9	1	2	9	·
Rok	55	3.7	73.5	3.2	105	3.9	118	2.9	55	2.5	69	2.8	107.5	3.2	158	3.7	354	2.6	567	27.1	29. IX	38	53	160	25	11	·	48	144	160	112	11	72	95	20

Poturzyn — $H_s = 240\ m$ — $h_w = 14{,}7\ m$

I	9.5	6.6	3.5	3.3	8	3.6	22.5	3.2	10.5	3.1	15	3.1	6	3.5	8	9.3	10	3.8	33	7.8	20	4	14	28	·	3	1	–	–	10	10	·	–	31	–
II	16	4.2	6.5	6.4	5	4.6	2	4.0	5	4.4	14	4.5	11	4.7	18.5	7.2	6	4.9	29?	7.8	1	17	24	28	·	3	1	–	–	–	–	–	–	28	–
III	6.5	4.3	4.5	3.0	9	3.3	21.5	2.9	13	2.8	5.5	5.1	5	3.8	17	3.8	13	3.0	39?	9.0	18	3	7	21	·	2	·	–	–	–	–	–	–	20?	–
IV	9.5	5.6	4	5.5	21	7.4	25	6.5	10	6.1	4.5	6.6	3.5	4.7	5.5	6.3	7	5.9	55?	14.0	28	·	·	10	·	11	1	–	–	–	–	–	–	·	–
V	11	3.5	6.5	7.1	7.5	5.1	6	2.9	4.5	4.9	7	6.7	10.5	5.5	21	5.8	19	4.2	72?	19.5	25	·	·	3	2	7	1	–	–	–	–	–	–	·	–
VI	11.5	3.9	2.5	6.6	8	4.8	10.5	4.1	9.5	4.3	7	4.2	11.5	3.7	18.5	4.8	11	3.8	55?	12.0	10	·	·	·	5	4	·	–	–	–	–	–	–	·	–
VII	6.5	4.3	3	4.3	5	4.4	6.5	3.8	10	4.2	20.5	5.4	13.5	4.3	13	4.6	15	3.8	94	25.0	18	·	·	·	6	6	·	–	–	18?	13?	2?	–	·	–
VIII	8.5	6.0	·	·	0.5	4.0	8	5.1	11	4.2	12.5	5.6	14.5	4.9	18	5.4	20	4.1	96	41.0	1	·	·	·	7	6	·	–	–	9	9	2	–	·	–
IX	1.5	6.0	·	·	4	3.5	17	4.5	10.5	3.6	12.5	5.0	9	3.9	14.5	4.5	21	3.3	41	23.5	12	·	·	·	4	1	1	–	–	14	6	1	–	·	–
X	13	3.2	2	2.8	6.5	3.2	3.5	4.3	6.5	3.3	12.5	2.8	18	4.4	19	3.6	12	3.1	10	4.2	11	·	·	5	·	·	·	–	–	8	3	·	–	·	–
XI	5	3.3	14	4.5	7.5	5.2	15.5	3.0	2.5	3.6	12.5	4.6	18	3.9	9	2.7	6	3.6	37	13.0	21	6	12	23	·	1	·	–	–	18	7	1	–	6	–
XII	1	4.0	3	4.0	1	3.0	15.5	3.3	20.5	2.9	30.5	3.3	4	2.1	11.5	3.7	6	3.0	28	13.2	18	2	7	24	·	1	·	–	–	16	7	1	–	5	–
Rok	99.5	4.6	49.5	4.0	83	4.3	153.5	4.0	113.5	4.0	154	4.7	124.5	4.1	173.5	5.1	144	3.9	589?	41.0	1. VIII	32	64	142	24	45	5	–	–	–	–	–	–	90?	–

Tarnobrzeg — $H_s = 175\ m$ — $h_w = 15{,}2\ m$

I	7	4.1	4	3.4	13.5	2.6	14	5.4	13	3.6	21.5	4.4	10.5	6.4	5.5	6.3	4	4.2	60	12.6	31	5	6	31	·	5	2	1	19	18	11	1	11	31	·
II	18.5	5.0	7	4.0	·	·	·	·	3.5	10.9	12.5	7.1	26	5.8	16.5	5.0	·	5.7	24	5.0	8	15	20	28	·	7	5	2	12	19	7	·	8	28	·
III	6.5	4.5	10	2.6	·	·	8	5.4	17.5	2.7	16	3.4	17.5	4.7	9.5	3.9	8	3.4	35	7.0	17	5	5	22	·	4	2	3	9	16	7	·	11	20	·
IV	5	2.5	8	4.9	17.5	6.3	22	6.9	4	3.6	8.5	5.5	13	5.8	12	4.1	·	5.6	28	7.0	30	·	·	5	·	8	1?	1	17	12	8	·	·	·	1
V	9	4.9	6.5	4.2	9.5	4.2	14	3.9	4	6.6	12.5	5.3	14.5	5.2	15	4.5	8	4.3	54	11.1	29	·	·	2	1	6	2	1	15	15	13	1	2	·	5
VI	12.5	3.8	7	3.6	5.5	5.8	6	5.0	5.5	5.4	5	2.8	22	4.0	21.5	4.0	5	3.9	66	16.7	27	·	·	·	6	5	2	4	8	14	11	2	·	·	5
VII	6	1.5	3.5	3.1	3.5	5.1	6	5.2	11	3.2	20	3.9	28	4.7	8	3.6	7	3.7	70	19.4	18	·	·	·	11	4	3	4	7	17	15	1	·	·	5
VIII	11.5	3.4	4.5	3.3	7.5	2.1	5	4.8	11.5	4.5	8	2.9	15.5	3.6	15.5	5.5	14	3.3	142	39.8	26	·	·	·	9	4	1	8	12	14	9	5	·	·	3
IX	2	3.0	3	2.3	2	2.8	17.5	3.7	22.5	4.7	13	2.5	18	2.9	6	1.8	6	3.2	58	21.0	29	·	·	·	6	3	1	10	·	9	6	2	4	·	1
X	10	2.7	3.5	1.9	8.5	2.7	5	2.3	1.5	2.0	16	3.2	17.5	3.8	11	3.4	20	2.4	2	1.0	16	·	·	7	·	1	·	7	9	6	1	·	7	·	·
XI	1	1.0	10.5	5.9	6	5.0	15.5	3.6	6	8.3	13	4.1	21.5	5.0	9.5	3.8	7	4.4	45	13.5	11	4	10	19	·	7	2	1	15	23	12	1	3	12	·
XII	6	2.8	6	1.7	1.5	4.0	8	4.0	16.5	5.1	29.5	5.1	14.5	4.3	5	2.3	6	4.0	33	10.7	18	2	4	23	·	3	2	1	17	19	9	1	2	10	·
Rok	95	3.3	73.5	3.4	75	3.4	121	4.2	116.5	5.0	175.5	4.2	218.5	4.7	135	4.0	85	4.0	617	39.8	26. VIII	31	45	137	33	57	23	43	140	182	109	14	48	101	20

Biłgoraj — φ = 50°33' — λ = 22°43' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.3	—	5.6	30	—	—	−3.5	−0.4	−2.9	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.3	7.4	7.6
II	—	—	—	—	−3.2	—	1.8	12	—	—	−8.3	−3.9	−7.8	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	9.1	7.4	6.5	7.7
III	—	—	—	—	5.7	—	16.4	30	—	—	−2.7	4.8	0.3	0.7	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.0	6.2	6.6
IV	—	—	—	—	11.0	—	16.6	7, 18	—	—	4.2	9.8	5.5	6.2	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.3	6.9	7.6
V	—	—	—	—	15.7	5.5	27.0	19	−4.6	4	8.8	14.2	9.8	10.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.2	6.1	6.6
VI	—	—	—	—	21.8	10.8	30.0	25	4.1	8	14.9	20.8	15.3	16.6	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.6	5.2	5.4
VII	—	—	—	—	22.4	11.4	29.6	16	4.3	12	15.3	20.8	16.0	17.0	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.7	5.2	5.7
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	21.2	8.1	27.2	2	1.9	22	11.0	20.4	13.1	14.4	—	—	—	—	—	—	—	—	—	—	—	—	5.6	4.1	2.7	4.1
X	—	—	—	—	12.3	1.1	22.4	1	−4.6	23	3.2	11.5	5.3	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.7	4.7	3.6	5.0
XI	—	—	—	—	2.0	—	14.3	2	—	—	−1.7	0.6	−1.2	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.9	8.4	8.7
XII	—	—	—	—	2.1	—	6.7	11	—	—	−0.7	1.1	−0.5	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.9	7.8	8.0
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Nisko — φ = 50°31' — λ = 22°09'

I	—	—	—	—	0.8	−5.6	6.6	30	−16.4	11	−3.2	−0.6	−2.8	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.2	7.2	7.2
II	—	—	—	—	−2.3	−11.1	3.4	12	−25.8	7	−8.0	−3.7	−7.1	−6.5	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.2	6.6	7.3
III	—	—	—	—	6.3	−3.7	17.4	30	−16.9	1	−2.5	4.7	0.8	1.0	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.4	4.7	5.8
IV	—	—	—	—	11.6	2.7	17.1	7	−1.2	3	4.4	9.5	6.1	6.5	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.6	4.7	7.2
V	—	—	—	—	16.6	5.9	28.1	19	−4.3	4	9.0	14.6	10.1	11.1	—	—	—	—	—	—	—	—	—	—	—	—	6.9	8.5	6.2	7.2
VI	—	—	—	—	22.5	11.4	30.6	26	6.0	8	15.2	20.5	15.6	16.7	—	—	—	—	—	—	—	—	—	—	—	—	5.1	6.7	6.1	6.0
VII	—	—	—	—	23.1	11.9	30.4	16	5.7	11	15.5	20.8	15.7	16.9	—	—	—	—	—	—	—	—	—	—	—	—	5.0	7.4	5.6	6.0
VIII	—	—	—	—	21.7	10.8	30.2	8	5.7	31	13.1	19.9	14.2	15.4	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.4	4.4	5.7
IX	—	—	—	—	22.1	9.2	27.1	3	3.2	16	11.3	20.4	13.0	14.4	—	—	—	—	—	—	—	—	—	—	—	—	4.0	5.4	2.9	4.1
X	—	—	—	—	13.1	1.8	22.7	1	−5.6	22	3.6	11.8	6.1	6.9	—	—	—	—	—	—	—	—	—	—	—	—	5.6	5.9	4.1	5.2
XI	—	—	—	—	2.8	−3.3	15.4	2	−17.5	17	−1.5	1.0	−0.7	−0.5	—	—	—	—	—	—	—	—	—	—	—	—	9.2	8.4	7.6	8.4
XII	—	—	—	—	2.9	−2.5	7.4	10	−19.2	17	−0.2	1.8	−0.1	0.4	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.0	6.2	7.8
Rok	—	—	—	—	11.8	2.3	30.6	26.VI	−25.8	7. II	4.7	10.1	5.9	6.6	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.2	5.5	6.5

Korfantów — φ = 50°29' — λ = 17°36'

I	—	—	—	—	3.0	−2.7	7.2	29	−12.7	8	−0.6	2.0	−0.3	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.2	6.5	7.1	7.3
II	—	—	—	—	−1.5	−8.3	4.7	14	−17.8	6	−5.1	−2.7	−4.8	−4.4	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.5	7.2	7.7
III	—	—	—	—	6.5	−3.5	17.4	30	−21.0	9	−0.8	5.3	1.6	1.9	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.7	5.5	6.0
IV	—	—	—	—	11.5	3.5	17.2	3	0.2	2	5.5	10.4	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.4	6.2	6.8
V	—	—	—	—	15.3	6.7	24.0	17	−1.1	3	10.2	13.7	10.0	11.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.4	7.5	7.3
VI	—	—	—	—	21.0	11.1	32.1	26	5.9	3	15.2	19.5	15.5	16.4	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.3	5.9	5.8
VII	—	—	—	—	21.5	11.5	31.0	14	6.5	5	16.1	20.0	15.4	16.7	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.2	5.9	6.6
VIII	—	—	—	—	22.1	10.4	31.4	7	5.5	3	14.4	20.4	15.7	16.6	—	—	—	—	—	—	—	—	—	—	—	—	5.1	5.9	5.9	5.6
IX	—	—	—	—	20.7	9.0	27.8	3	3.1	22	12.3	19.5	14.2	15.0	—	—	—	—	—	—	—	—	—	—	—	—	4.5	5.3	4.5	4.8
X	—	—	—	—	14.1	2.4	23.4	3	−6.6	22	4.3	12.9	7.1	7.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	3.4	5.5	5.1
XI	—	—	—	—	3.9	−3.1	15.8	1	−11.5	24	−0.8	2.5	0.1	0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.3	7.0	7.6
XII	—	—	—	—	4.3	−1.0	12.3	19	−6.6	15	1.1	3.1	1.7	1.9	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.2	5.4	6.8
Rok	—	—	—	—	11.9	3.0	32.1	26.VI	−21.0	9. III	6.0	10.6	6.9	7.6	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.4	6.1	6.4

Zawiercie — φ = 50°29' — λ = 19°26'

I	—	—	—	—	1.8	−4.4	7.0	29	−11.7	7	−2.1	0.7	−1.4	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.2	6.8	7.8
II	—	—	—	—	−2.6	−11.2	2.1	14	−22.6	6	−8.2	−4.3	−7.0	−6.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	6.7	7.1	7.4
III	—	—	—	—	6.1	−3.8	16.5	30	−15.7	11	−1.4	4.9	−0.1	0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.9	5.9	4.0	5.6
IV	—	—	—	—	10.5	2.2	15.3	3	−2.4	2	4.1	8.8	5.1	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.3	5.9	6.8
V	—	—	—	—	14.9	5.3	25.6	19	−3.8	3	8.8	12.8	9.0	9.9	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.5	5.9	6.8
VI	—	—	—	—	20.8	9.8	31.6	26	4.4	15	14.7	19.0	14.1	15.5	—	—	—	—	—	—	—	—	—	—	—	—	5.4	6.6	5.3	5.8
VII	—	—	—	—	21.3	10.9	29.4	14	4.5	5	15.1	19.5	14.1	15.7	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.1	5.3	6.3
VIII	—	—	—	—	20.6	9.6	30.0	8	3.4	31	13.3	19.1	13.3	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.7	5.6	5.9
IX	—	—	—	—	20.8	8.6	27.5	3	3.3	20	11.7	18.8	12.7	14.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	5.6	4.3	5.0
X	—	—	—	—	12.9	2.0	21.0	1, 2	−6.1	23	4.3	11.9	5.6	6.8	—	—	—	—	—	—	—	—	—	—	—	—	5.9	4.2	4.4	4.8
XI	—	—	—	—	3.0	−3.7	12.3	2	−15.3	18	−1.9	1.4	−1.0	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.7	7.6	7.8
XII	—	—	—	—	3.2	−1.8	9.2	20	−8.7	15	−0.1	1.6	0.4	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.5	8.0	8.3
Rok	—	—	—	—	11.1	2.0	31.6	26.VI	−22.6	6. II	4.9	9.5	5.4	6.3	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.8	5.8	6.5

Biłgoraj

$H_s = 190\ m$ — $h_w = 19\ m$ — 1965

MIESIĄC	ROZKŁAD WIATRU $^{n}D, V_mD$ — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	2.0	4	1.8	9	1.6	23	2.5	18	2.6	4	5.2	5	5.8	2	2.5	22	2.1	51	8.9	17	—	11	—	·	3	·	3	20	15	12	·	5	31	—
II	13	2.5	6	1.7	·	·	1	2.0	10	3.6	8	2.9	16	3.1	11	3.0	19	2.2	34	5.9	7	—	23	—	·	·	·	1	17	17	11	·	2	28	—
III	1	1.0	8	2.4	5	1.2	22	1.9	8	1.4	7	2.6	5	2.2	7	3.6	30	1.4	37	8.5	17	—	3	—	·	·	·	2	11	12	9	·	5	—	—
IV	4	3.2	3	1.7	26	4.2	20	3.0	8	3.0	6	2.3	5	2.4	4	1.8	14	2.7	59	22.2	26	—	·	—	·	2	·	·	15	9	8	1	1	·	—
V	6	1.7	9	3.0	7	1.9	6	3.2	5	3.8	5	3.0	10	2.3	14	3.3	31	1.8	89	30.1	29	·	·	4	1	1	·	1	9	16	14	1	1	·	—
VI	4	2.0	7	2.3	5	2.4	10	3.3	4	3.0	3	2.3	19	2.9	11	2.6	27	1.9	80[2]	16.1	19	·	·	·	6	·	·	7	9	11	11	2	·	·	—
VII	·	·	4	2.0	1	2.0	10	2.3	14	1.7	11	2.4	19	2.4	3	1.0	31	1.4	68[2]	22.6	17	·	·	·	7	·	·	4	5	16	14	1	·	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	101	41.5	26	—	—	—	—	—	—	—	—	10	10	3	·	·	—
IX	·	·	·	·	6	1.3	24	2.3	14	2.4	2	1.0	4	1.5	6	2.2	34	1.3	49	18.8	6	·	·	·	4	·	·	8	3	7	7	2	3	·	—
X	3	1.0	1	2.0	7	1.1	4	1.2	3	1.3	4	1.2	14	1.9	9	2.1	48	0.8	8	4.9	31	·	·	14	·	·	·	7	7	6	3	·	6	·	—
XI	·	·	9	2.7	9	1.9	17	2.6	6	1.7	10	2.0	12	2.0	5	2.2	22	1.7	71	10.1	11	—	11	—	·	·	·	·	21	18	14	1	6	—	—
XII	6	1.7	·	·	1	2.0	24	2.2	14	2.6	19	2.4	10	2.9	6	1.7	13	2.0	40	13.0	18	—	8	—	·	1	·	·	19	17	10	1	3	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	687[2]	41.5	26.VIII	—	—	—	—	—	—	—	—	—	—	—	32	—	—

Nisko

$H_s = 164\ m$ — $h_w = 16\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	2	3.0	3	2.7	13	2.6	13.5	3.9	24.5	4.0	15	3.3	18.5	3.3	3.5	6.6	·	3.6	49	11.0	31	7	11	25	·	5	1	4	19	15	15	1	2	31	·
II	11.5	3.4	6.5	2.8	1	3.0	·	·	11	6.6	9	4.1	27	4.7	18	3.6	·	4.3	37	14.0	8	15	22	28	·	5	2	3	14	13	12	1	4	28	·
III	2	7.5	9	2.6	13	3.1	19	2.4	11	2.2	8	3.8	24	3.0	7	3.3	·	2.9	33	9.0	17	6	6	21	·	1	·	4	8	12	9	·	10	15	·
IV	5	3.0	2	12.5	36.5	5.3	11	5.6	9	2.3	10.5	3.0	7	3.4	8	2.9	1	4.4	42	8.0	7	·	·	5	·	5	2	2	14	16	12	·	2	·	2
V	11.5	2.2	2.5	1.0	22	3.8	3	3.3	6.5	4.1	9.5	2.2	18	2.9	20	4.2	·	3.3	66	20.5	29	·	·	3	2	3	2	1	13	19	11	1	5	·	4
VI	7	3.9	7	3.1	17	2.8	4	3.9	9	4.3	1	1.0	35	3.6	10	3.4	·	3.5	61	13.5	28	·	·	·	6	4	1	4	11	14	12	2	1	·	5
VII	5.5	1.2	3	2.0	16	2.4	3.5	1.6	15.5	3.4	10	3.2	29.5	2.7	8	1.5	2	2.5	214	87.1	18	·	·	·	13	·	·	3	5	20	16	6	1	·	6
VIII	7	2.7	10	1.4	7.5	1.9	7.5	2.7	11	2.1	7	2.7	28.5	3.1	14.5	3.7	·	2.7	167	52.0	26	·	·	·	9	1	·	8	11	12	8	5	2	·	·
IX	2	1.0	1	4.0	23	2.2	8.5	4.6	22.5	3.3	6	3.2	21	2.7	6	2.2	·	2.9	51	21.0	11	·	·	·	7	·	·	8	1	6	6	2	5	·	·
X	8	2.8	1	7.0	13	1.9	10	1.8	14	1.7	8	2.8	29.5	2.7	9.5	3.5	·	2.5	5	2.0	11	·	·	10	·	1	·	10	7	4	3	·	9	·	·
XI	1	1.0	9	3.9	11	5.5	16.5	2.0	9.5	3.6	9	4.1	30	2.6	4	1.8	·	3.3	43	8.8	21	5	11	20	·	3	1	·	20	16	12	·	5	10	1
XII	4	1.5	1	3.0	4	3.2	14	3.1	32.5	4.2	16.5	3.5	18	3.4	3	3.3	·	3.5	39	13.5	18	2	4	21	·	3	1	1	19	16	7	1	1	8	·
Rok	66.5	2.8	55	3.8	177	3.1	110.5	2.9	176	3.5	109.5	3.1	286	3.2	111.5	3.3	3	3.3	807	87.1	18.VII	35	54	133	37	31	10	48	142	163	123	19	47	92	18

Korfantów

$H_s = 200\ m$ — $h_w = 12,5\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	1	1.0	·	·	2	1.0	11.5	2.7	5.5	4.3	3	3.7	10.5	3.5	16.5	2.4	43	1.6	35	8.3	31	2	3	27	·	1	·	2	15	14	9	·	1	12	—
II	7	3.1	·	·	2	1.0	4	4.8	3	4.0	2	3.0	8	4.4	34	4.6	24	3.0	26	5.1	17	9	21	27	·	4	·	1	17	20	10	·	·	28	—
III	3	2.3	1	1.5	2	2.5	7.5	4.4	5	2.7	5	2.4	4	5.5	29.5	3.4	36	2.1	30	8.2	6	5	5	21	·	3	1	5	9	13	9	·	—	16	—
IV	8.5	3.0	5	2.7	5.5	4.5	9	3.8	7.5	4.8	0.5	4.0	10	4.4	26	3.5	18	3.0	68	18.3	19	·	·	·	·	·	·	5	14	16	11	2	5	·	—
V	8.5	3.4	3	4.2	3.5	3.3	7.5	4.4	2.5	2.4	6	3.1	11	4.3	30	3.8	21	2.9	127	17.8	19	·	·	2	·	2	·	1	16	19	15	5	5	·	—
VI	7	2.1	1	2.5	2.5	1.6	10.5	3.4	5.5	3.6	1	1.0	10.5	4.2	28	4.1	24	2.6	91	20.6	11	·	·	·	5	·	·	3	9	15	13	4	1	·	—
VII	4	3.1	5.5	3.0	·	·	4	7.0	1	14.0	9	5.4	22	4.6	26.5	3.5	21	3.4	80	16.0	15	·	·	·	5	2	2	1	8	19	14	3	·	·	—
VIII	7	3.0	·	·	·	·	3	8.3	7	8.0	5	3.6	8.5	3.9	31.5	2.9	31	2.6	50	19.1	24	·	·	·	8	3	2	5	7	8	6	2	1	·	—
IX	1	1.0	·	·	2.5	2.6	16	5.6	13.5	7.6	2	5.0	5	5.0	19	3.1	31	3.3	46	22.5	28	·	·	·	4	5	2	6	6	9	8	1	5	·	—
X	4	1.8	2	1.5	5	1.8	4	2.5	·	·	6	6.2	9	2.8	10	2.4	53	1.2	3	3.0	16	·	·	11	·	·	·	6	7	2	1	·	12	·	—
XI	2	2.0	5.5	3.2	5.5	3.4	10	3.2	2	9.5	9	9.8	13.5	6.1	13.5	2.6	29	3.3	23	7.4	11	2	9	21	·	4	3	·	15	11	6	·	5	14	—
XII	·	·	1	1.0	3	1.3	1	2.0	11.5	6.0	13	7.1	27	4.1	9.5	3.0	27	3.3	33	8.4	18	·	1	17	·	3	2	·	9	12	6	·	1	7	—
Rok	53	2.2	24	1.6	33.5	1.9	88	4.3	64	5.6	61.5	4.5	139	4.4	274	3.3	358	2.7	612	27.5	28.IX	18	39	126	22	27	12	35	132	158	108	17	—	77	—

Zawiercie

$H_s = 335\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	59	10.9	31	2	7	28	·	—	—	2	18	17	13	1	2	31	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	41	4.9	17	16	24	28	·	—	—	·	14	23	16	·	2	28	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	41	8.8	21	6	5	20	·	—	—	5	7	23	10	·	6	18	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	59	10.0	23	·	·	6	·	—	—	4	13	18	15	1	1	·	2
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	122	17.4	29	·	·	3	1	—	—	4	12	21	17	3	1	·	4
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	105	16.5	5	·	·	·	5	—	—	3	8	15	14	5	·	·	5
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	94	32.5	17	·	·	·	6	—	—	1	5	17	14	3	1	·	5
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	101	32.7	25	·	·	·	7	—	—	2	9	14	13	2	1	·	5
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	82	24.0	28	·	·	·	2	—	—	5	5	11	9	4	3	·	1
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2	2.2	16	·	·	10	·	—	—	9	9	3	1	·	6	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	38	8.0	11	4	10	23	·	—	—	1	18	22	10	·	4	14	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	41	11.3	18	·	2	24	·	—	—	·	18	20	13	1	·	11	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	785	32.7	25.VIII	28	48	142	21	—	—	36	136	204	145	20	27	102	22

Otmuchów

$\varphi = 50°28'$ $\lambda = 17°10'$ **1965**

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{0,m}$	Temperatura T: Max	Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	4.1	−1.8	8.4	17	−11.1	7	0.3	2.9	1.0	1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.3	7.4	7.9
II	–	–	–	–	−0.8	−9.3	4.7	14	−21.5	6	−4.8	−2.1	−4.6	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.5	7.0	8.1
III	–	–	–	–	6.9	−3.6	16.9	30	−24.1	9	−1.3	5.7	1.4	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	5.5	7.0
IV	–	–	–	–	11.8	3.3	18.1	3	−2.1	6	5.1	10.9	7.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.6	6.9	7.7
V	–	–	–	–	15.4	6.8	23.6	17	−1.7	3	9.9	14.0	10.4	11.2	10.2	10.5	10.8	10.5	82	65	84	77	2.2	5.9	2.1	3.4	8.4	8.1	7.7	8.1
VI	–	–	–	–	21.5	10.4	34.0	26	3.1	3	15.0	20.1	15.1	16.3	14.0	14.0	14.6	14.2	81	60	85	75	3.4	10.2	2.8	5.5	6.8	7.1	6.0	6.6
VII	–	–	–	–	21.8	11.9	31.5	14	6.2	4, 5	15.8	20.1	15.5	16.7	14.8	15.2	15.0	15.0	82	65	85	77	3.3	9.1	2.8	5.1	8.2	8.1	6.7	7.7
VIII	–	–	–	–	21.6	9.9	30.3	6, 7	4.0	31	13.7	20.0	14.7	15.8	13.6	13.5	14.4	13.8	87	59	86	77	2.5	10.9	2.8	5.4	5.7	6.8	5.1	5.9
IX	–	–	–	–	20.9	8.4	27.2	2	2.2	22	11.8	18.9	12.6	14.0	11.9	12.3	12.4	12.2	86	57	86	76	2.2	10.0	2.6	4.9	5.6	6.3	2.9	4.9
X	–	–	–	–	14.3	1.9	22.4	2	−5.4	23	4.1	12.8	5.7	7.1	7.9	9.1	8.6	8.5	93	61	90	81	0.7	6.2	1.1	2.7	7.3	4.9	4.3	5.5
XI	–	–	–	–	4.7	−3.1	15.6	1	−14.0	24	−0.3	2.8	0.2	0.7	5.3	5.7	5.3	5.4	85	74	85	81	1.0	2.2	1.2	1.5	8.3	7.4	7.9	7.9
XII	–	–	–	–	5.0	−1.2	12.6	19	−14.7	15	1.6	3.3	2.0	2.2	5.6	5.7	5.5	5.6	80	74	77	77	1.5	2.1	1.8	1.8	8.5	8.0	6.6	7.7
Rok	–	–	–	–	12.3	2.8	34.0	26. VI	−24.1	9. III	5.9	10.8	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.4	6.2	7.1

Kudowa-Zdrój

$\varphi = 50°27'$ $\lambda = 16°16'$

I	–	–	–	–	1.8	−3.1	4.9	29	−16.0	7	−1.7	0.7	−0.3	−0.4	5.0	5.3	5.5	5.3	91	81	91	88	0.5	1.2	0.6	0.8	8.4	8.3	8.9	8.5
II	–	–	–	–	−1.6	−10.0	2.4	14	−20.9	10	−6.8	−2.8	−5.7	−5.2	3.4	3.9	3.4	3.6	89	77	84	83	0.4	1.1	0.6	0.7	8.9	7.6	7.9	8.1
III	–	–	–	–	5.1	−4.4	11.9	30	−21.1	9	−2.8	3.8	−0.3	0.1	4.8	5.8	5.5	5.4	88	70	87	82	0.5	2.6	0.8	1.3	6.9	6.4	6.5	6.6
IV	–	–	–	–	10.5	1.7	17.4	6	−4.3	2	3.4	8.9	5.3	5.7	7.0	7.3	7.3	7.2	89	66	82	79	0.9	4.4	1.6	2.3	7.4	7.6	7.3	7.4
V	–	–	–	–	14.4	5.6	23.0	17	−2.3	3	8.6	12.8	9.1	9.9	9.8	9.9	9.8	9.8	82	67	84	78	1.6	5.2	2.0	2.9	6.5	8.0	7.1	7.2
VI	–	–	–	–	20.1	9.1	30.9	26	1.8	3	13.3	18.2	13.5	14.6	13.4	13.4	13.4	13.4	87	65	86	79	2.1	8.3	2.4	4.3	5.4	7.5	7.2	6.7
VII	–	–	–	–	19.9	11.0	29.9	14	5.6	10	14.3	18.0	14.0	15.1	14.4	14.7	14.7	14.6	88	71	91	83	2.2	6.7	1.6	3.5	7.1	7.9	7.6	7.5
VIII	–	–	–	–	20.4	9.3	29.7	6	3.4	31	12.0	19.1	13.5	14.5	12.8	12.7	13.3	12.9	91	58	85	78	1.7	10.3	2.8	4.9	4.7	6.1	5.1	5.3
IX	–	–	–	–	18.4	8.5	24.4	2	1.9	22	10.5	17.3	12.1	13.0	11.7	12.7	12.5	12.3	92	66	88	82	1.4	7.4	2.0	3.6	6.3	6.2	3.8	5.4
X	–	–	–	–	13.2	0.9	21.9	1	−5.7	22, 23	2.3	12.3	4.7	6.0	7.5	9.1	8.0	8.2	96	62	90	83	0.3	5.6	0.9	2.3	5.0	4.0	3.4	4.1
XI	–	–	–	–	2.8	−3.0	13.2	1	−15.8	24	−1.4	1.1	−0.7	−0.4	5.4	5.5	5.6	5.5	92	82	91	88	0.4	1.3	0.5	0.7	8.5	8.2	8.8	8.5
XII	–	–	–	–	3.4	−1.4	10.4	19	−14.3	15	0.5	1.9	0.9	1.0	5.7	5.7	5.9	5.8	89	80	88	86	0.7	1.4	0.8	1.0	8.6	8.3	8.4	8.4
Rok	–	–	–	–	10.7	2.0	30.9	26.VI	−21.1	9. III	4.4	9.3	5.5	6.2	8.4	8.8	8.7	8.6	90	70	87	82	1.1	4.6	1.4	2.4	7.0	7.2	6.8	7.0

Busko-Zdrój

$\varphi = 50°27'$ $\lambda = 20°43'$

I	–	–	–	–	0.7	−4.8	6.1	30	−14.8	11	−2.6	0.0	−2.1	−1.7	4.4	5.1	4.6	4.7	86	82	87	85	0.7	1.1	0.7	0.8	7.8	7.7	6.8	7.4
II	–	–	–	–	−2.7	−10.2	3.1	14	−22.4	7	−7.3	−3.7	−6.8	−6.2	3.3	3.9	3.3	3.5	88	81	87	85	0.4	0.9	0.5	0.6	7.8	7.3	6.2	7.1
III	–	–	–	–	5.0	−3.1	16.1	30	−12.6	1	−1.0	4.2	1.1	1.4	5.3	6.5	5.8	5.9	89	77	84	83	0.6	2.1	1.0	1.2	7.9	6.9	5.9	6.9
IV	–	–	–	–	10.5	2.2	16.3	7	−1.7	1	4.2	9.4	5.9	6.4	7.5	7.8	7.8	7.7	89	68	83	80	0.9	4.3	1.7	2.3	8.3	7.7	6.2	7.4
V	–	–	–	–	15.6	6.4	27.3	19	−1.2	2	9.7	14.3	10.5	11.2	10.3	10.8	11.0	10.7	83	65	84	77	2.1	6.1	2.0	3.4	5.9	7.7	7.2	6.9
VI	–	–	–	–	21.6	11.7	31.1	26	6.5	3	15.6	20.3	15.5	16.7	14.0	13.9	14.2	14.0	79	60	81	73	4.0	10.8	3.7	6.2	4.3	6.3	6.8	5.8
VII	–	–	–	–	22.0	12.3	28.1	14	6.7	6	15.9	20.6	15.9	17.1	15.8	16.8	16.5	16.4	86	69	89	81	2.6	8.2	2.0	4.3	7.3	7.2	6.5	7.0
VIII	–	–	–	–	20.9	11.1	30.1	7, 8	6.6	14	13.6	19.3	15.1	15.8	13.6	14.0	14.2	13.9	87	66	82	78	2.3	9.3	3.5	5.0	5.5	6.6	3.9	5.3
IX	–	–	–	–	20.7	9.9	26.0	3	5.4	22	12.4	19.4	14.1	15.0	12.8	14.3	13.8	13.6	89	64	86	79	1.9	8.8	2.5	4.4	4.9	5.6	3.9	4.8
X	–	–	–	–	12.6	3.3	21.2	1, 2	−2.8	22	4.7	11.8	7.1	7.7	8.1	9.2	8.9	8.7	90	65	85	80	0.8	5.1	1.5	2.5	7.1	5.4	4.2	5.6
XI	–	–	–	–	2.4	−3.4	14.2	2	−15.0	18	−1.9	1.1	−0.6	−0.5	4.9	5.4	5.3	5.2	86	77	87	83	0.8	1.7	0.8	1.1	8.8	7.5	7.7	8.0
XII	–	–	–	–	2.9	−2.0	9.1	20	−10.2	17	−0.2	1.9	0.2	0.5	5.3	5.4	5.3	5.3	85	75	84	81	0.9	1.8	1.0	1.2	8.4	7.1	6.5	7.3
Rok	–	–	–	–	11.0	2.8	31.1	26.VI	−22.4	7. II	5.3	9.9	6.3	7.0	8.8	9.4	9.2	9.1	86	71	85	81	1.5	5.0	1.7	2.7	7.0	6.9	6.0	6.6

Tomaszów Lub. I

$\varphi = 50°27'$ $\lambda = 23°25'$

I	–	–	–	–	−0.1	−6.5	7.3	30	−22.3	11	−4.1	−1.3	−3.3	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.9	8.2	8.2
II	–	–	–	–	−4.0	−11.0	1.7	14	−24.9	7	−8.2	−4.7	−7.7	−7.1	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.6	7.8	8.2
III	–	–	–	–	4.9	−4.3	16.7	30	−21.4	1	−2.7	3.7	−0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.3	7.2	7.0
IV	–	–	–	–	9.5	1.6	16.7	7	−3.0	3	3.3	7.9	4.7	5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.5	8.0
V	–	–	–	–	15.4	5.4	27.2	19	−2.9	4	8.9	13.4	9.5	10.3	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.0	7.5	7.5
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Otmuchów $H_s = 211\ m$ $h_w = 11\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7.5	1.7	2.5	1.0	4	1.4	2	1.5	2.5	1.8	9.5	2.2	15.5	2.2	18.5	1.8	31	1.2	30	8.1	31	1	·	25	·	·	·	·	18	14	10	·	5	9	·
II	12	2.0	8.5	1.0	·	·	·	·	·	·	1.5	2.3	12	2.8	37	2.7	13	2.0	24	4.7	17	12	18	27	·	1	·	2	19	17	10	·	1	27	·
III	5.5	1.7	6.5	1.5	3	1.7	·	·	5.5	1.2	8	1.3	10	1.8	32.5	1.5	22	1.2	27	5.8	2	6	4	20	·	·	·	1	11	10	7	·	4	16	·
IV	5.5	1.5	10	1.6	13	1.3	3.5	1.1	1.5	2.0	1.5	1.0	8.5	1.5	22.5	1.5	24	1.1	75	21.1	20	·	·	5	·	·	·	2	20	17	13	2	4	·	1
V	9.5	1.7	14	1.5	5	1.2	1.5	1.7	1	1.5	·	·	13.5	2.0	24.5	2.0	24	1.3	189	36.5	29	·	·	3	·	·	·	·	22	21	18	7	3	·	5
VI	6.5	1.9	8	1.4	6.5	1.2	3	2.3	2.5	1.8	4	1.8	11	2.0	23.5	2.1	25	1.4	109	20.2	22	·	·	·	7	·	·	2	12	16	13	5	1	·	4
VII	5.5	1.2	2	1.5	2	1.0	0.5	1.0	4.5	1.7	6	1.5	24.5	1.9	14	1.6	34	1.0	77	12.9	8	·	·	·	6	·	·	·	16	19	15	1	·	·	6
VIII	4.5	1.6	5	2.3	4	2.9	1	1.0	3	1.0	8.5	1.0	10.5	1.6	22.5	1.6	34	1.0	73	24.8	25	·	·	·	8	·	·	5	9	9	5	3	1	·	2
IX	4	2.1	4.5	3.1	3.5	3.9	3.5	3.0	5.5	2.3	10.5	1.3	9.5	2.3	11	1.8	38	1.3	51	34.4	28	·	·	·	2	·	·	6	6	8	5	1	8	·	1
X	10	1.4	2	1.2	9	1.4	1	1.5	·	·	5.5	2.6	8	3.1	9.5	3.1	48	1.1	3	2.3	16	·	·	12	·	·	·	5	10	3	1	·	26	·	·
XI	2	1.0	11.5	2.0	3.5	2.1	1.5	1.3	6.5	3.8	4.5	4.7	16	5.6	12.5	1.5	32	2.1	28	10.1	11	4	7	23	·	4	·	1	18	15	5	1	17	10	·
XII	3.5	1.6	1.5	1.0	2	2.5	3	1.3	7.5	2.4	11.5	2.5	26	3.0	20	2.4	18	2.0	32	10.7	13	2	·	15	·	·	·	·	17	13	6	1	4	5	·
Rok	76	1.6	76	1.6	55.5	1.7	20.5	1.3	40	1.6	71	1.8	165	2.5	248	2.0	343	1.4	718	36.5	29.V	25	29	130	23	5	·	24	178	162	108	21	74	67	19

Kudowa-Zdrój $H_s = 385\ m$ $h_w = 13{,}5\ m$

I	4.5	1.2	9	1.9	6	1.8	6	2.9	8	1.3	9	1.6	11.5	1.3	4	1.0	35	1.0	63	15.7	9	2	4	28	·	2	·	·	20	17	15	2	5	30	·
II	4.5	1.6	11	2.0	5	1.6	2	2.5	2	1.0	5.5	1.3	15.5	2.8	6.5	1.6	32	1.2	54	12.5	27	12	22	28	·	2	·	·	18	23	11	1	17	28	·
III	9.5	1.4	14	1.6	6	1.8	·	·	7	1.7	4	1.5	15.5	1.8	8	1.7	29	1.1	42	8.1	26	5	6	20	·	·	·	2	12	13	10	·	8	20	·
IV	5	2.0	23	1.7	3	3.7	2	1.5	2	1.5	1	2.0	13.5	2.0	15.5	1.4	25	1.3	76	13.0	17	·	·	9	·	·	·	1	17	18	13	2	4	·	·
V	14.5	1.2	19.5	1.9	5.5	3.5	2	2.2	2.5	2.2	1.5	1.7	21	2.0	12.5	2.0	14	1.7	163	43.2	29	·	·	3	·	·	·	1	12	21	18	5	8	·	4
VI	15.5	1.5	11.5	2.0	1	5.0	2	2.2	1.5	2.3	1	4.8	28	2.0	7.5	1.4	22	1.5	128	43.9	22	·	·	·	4	·	·	·	9	17	15	2	5	·	3
VII	16	1.3	4	1.5	·	·	1.5	6.0	6.5	2.4	3	2.5	16.5	2.2	19.5	1.4	26	1.3	143	35.8	21	·	·	·	4	·	·	1	14	24	17	3	·	·	5
VIII	13.5	1.1	10	2.0	3	4.3	2	3.2	1.5	4.0	1.5	1.7	8.5	1.9	7	1.6	46	1.0	76	21.5	24	·	·	·	6	1	1	2	4	9	7	3	3	·	·
IX	10	1.6	15.5	2.7	7	2.7	2	1.5	1	1.0	·	·	11	1.8	11.5	1.6	32	1.3	57	9.7	28	·	·	·	·	·	·	6	7	10	9	·	2	·	1
X	15	1.4	13	1.2	4	2.2	·	·	·	·	·	·	4.5	2.0	11.5	1.5	45	0.8	8	4.0	16	·	·	12	·	·	·	8	6	2	2	·	4²	·	·
XI	10	1.4	16.5	1.9	3	3.3	3.5	2.6	4.5	1.8	2	1.0	24.5	2.1	7	2.6	19	1.6	74	13.1	27	2	11	25	·	2	·	·	22	21	16	1	8	16	·
XII	6	1.7	12.5	1.4	6.5	2.3	0.5	4.0	7	2.3	7.5	2.0	35.5	2.0	3.5	1.9	14	1.7	70	17.5	5	2	1	20	·	3	·	1	22	19	13	1	·	12	
Rok	124	1.4	169.5	1.8	50	2.7	23.5	2.4	43.5	1.8	36	1.6	205.5	2.0	114	1.6	339	1.3	954	43.9	22.VI	23	44	145	14	10	1	22	163	194	146	20	64²	106	13

Busko-Zdrój $H_s = 225\ m$ $h_w = 14\ m$

I	7.5	5.2	7.5	4.9	14	2.5	18	1.8	14.5	4.1	9.5	3.8	9	2.9	10	4.2	3	3.3	74	12.6	31	3	12	31	·	2	·	·	17	20	15	1	6	31	·
II	9	4.4	9	2.8	2	1.0	·	·	4	3.0	14	6.1	13	4.5	32	3.5	1	4.0	36	4.3	17	12	24	28	·	5	·	4	15	21	14	·	4	28	
III	4	4.2	11	3.9	9.5	2.0	17	2.6	15.5	3.0	7	3.7	7	4.1	14	2.6	8	2.8	38	8.0	21	4	5	20	·	2	·	2	15	17	12	·	6	20	
IV	9.5	4.8	17	3.8	22	4.6	11	5.9	4	4.2	9	3.0	7	2.3	5.5	1.5	5	3.8	36	15.0	11	·	·	7	·	5	·	1	15	13	11	2	2	·	
V	11	2.9	11	3.7	10	4.1	13	2.5	6	2.0	11	2.8	14	2.5	13	2.7	4	2.8	76	16.0	29	·	·	3	1	2	1	3	13	17	13	3	1	·	5
VI	11	3.0	7	4.3	13	3.5	11	3.7	3	2.0	11	2.8	13	3.2	19	2.6	2	3.1	100	21.9	27	·	·	·	6	2	1	2	9	13	12	4	·	·	4
VII	2	2.0	5	4.2	10	3.1	6	3.7	12	3.5	24	2.2	23	2.7	7	2.0	4	2.7	72	36.0	17	·	·	·	8	3	1	3	11	16	13	1	·	·	7
VIII	12	4.0	5	1.4	4	1.0	17.5	2.1	10.5	3.4	6	2.5	15	1.9	18	2.3	5	2.3	74	18.0	26	·	·	·	7	1	·	4	8	15	11	2	1	·	2
IX	3	1.7	·	·	1	2.0	34	3.4	16	3.4	11	2.3	12	1.4	9	1.9	4	2.6	58	26.6	29	·	·	·	2	1	·	6	4	9	5	1	1	·	·
X	14	2.1	8	2.1	9	1.4	6	1.5	10	1.6	13	2.1	9.5	2.8	16.5	3.0	7	2.0	3	1.0	29	·	·	8	·	·	·	5	8	6	1	·	8	·	·
XI	2	2.0	11	3.9	10	2.3	14	3.6	9	3.4	14	2.6	14	3.1	9	2.3	7	2.8	43	16.0	11	4	10	21	·	3	1	1	16	17	11	1	3	11	·
XII	4	2.0	·	·	2	2.5	18	2.3	19	3.1	26	3.1	11	3.5	7	3.0	6	2.7	50	20.0	3	1	4	25	·	3	·	3	15	13	9	2	·	10	
Rok	89	3.2	91.5	2.9	106.5	2.5	165.5	2.8	123.5	3.1	155.5	3.1	147.5	2.9	160	2.6	56	2.9	660	36.0	17.VII	24	55	143	24	29	4	34	146	177	127	17	32	100	18

Tomaszów Lub. I $H_s = 273\ m$ $h_w = 13\ m$

I	3.5	3.1	6.5	2.1	14.5	2.3	14	3.4	11	4.0	25	3.8	7	4.9	6.5	3.8	5	3.3	39	9.3	31	6	13	27	·	·	·	3	21	15	10	·	—	31	·
II	10.5	3.4	6.5	3.4	1	7.0	·	·	4.5	5.3	21	5.2	20.5	3.5	15	2.9	5	3.7	29	5.5	16	17	24	28	·	1	·	·	18	18	11	·	—	28	·
III	2.5	2.4	14.5	2.7	5	4.0	12	2.2	10	3.2	11	3.1	14.5	2.6	12.5	3.4	11	2.5	32	7.6	3	3	6	25	·	2	·	2	14	12	10	·	—	19	·
IV	4.5	3.8	13	4.1	18.5	5.9	25.5	5.4	3.5	3.1	11	3.5	4.5	2.4	7.5	3.9	2	4.5	55	14.8	28	·	·	12	·	3	·	·	14	14	9	2	—	·	1
V	7.5	2.7	13	3.5	5.5	5.9	6	3.8	2.5	4.8	18	3.8	8.5	2.8	30	2.7	2	3.3	44	7.0	27	·	·	3	2	2	·	1	15	18	15	·	—	·	1
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Tomaszów Lub. II — φ = 50°27' — λ = 23°24' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.2	−7.0	7.0	30	−23.9	11	−4.3	−1.6	−3.6	−3.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.8	7.7	7.9
II	–	–	–	–	−4.3	−11.8	1.3	14	−27.8	7	−8.6	−5.2	−8.0	−7.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	6.9	6.5	7.4
III	–	–	–	–	4.5	−4.9	15.1	30	−23.6	1	−2.9	3.3	−0.3	0.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.6	6.6	6.4
IV	–	–	–	–	9.3	1.4	15.8	26	−2.4	7	3.2	7.6	4.9	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	6.4	6.9
V	–	–	–	–	15.0	5.2	27.2	19	−2.5	4	8.6	13.1	9.4	10.1	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.9	6.4	6.4
VI	–	–	–	–	20.6	10.5	27.4	26	3.9	8	14.6	19.2	14.5	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.7	5.9	6.1
VII	–	–	–	–	21.3	11.0	27.5	16	5.7	12	15.1	19.8	14.9	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.7	6.5	6.5
VIII	–	–	–	–	20.3	10.1	29.7	8	5.0	17	13.3	18.8	13.1	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.3	3.9	5.4
IX	–	–	–	–	20.4	7.4	27.7	4	0.8	17	10.8	19.3	11.9	13.5	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.9	2.1	4.0
X	–	–	–	–	11.7	2.0	21.9	1	−5.3	22	4.2	10.9	5.8	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.6	4.3	5.6
XI	–	–	–	–	1.6	−4.8	13.7	2	−23.0	17	−2.1	0.2	−1.9	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.0	8.2	8.6
XII	–	–	–	–	1.8	−2.7	8.4	10	−17.8	17	−0.9	0.8	−0.5	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.1	7.1	7.6
Rok	–	–	–	–	10.2	1.4	29.7	8. VIII	−27.8	7. II	4.2	8.8	5.0	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.0	6.6

Kłodzko — φ = 50°26' — λ = 16°39'

I	973.4	987.0	952.4	1012.0	1.8	−3.0	4.7	30	−17.0	7	−1.5	0.6	−0.2	−0.3	4.9	5.3	5.3	5.2	88	83	86	86	0.7	1.1	0.8	0.9	8.5	7.5	8.7	8.2
II	978.6	992.5	956.8	1018.9	−1.6	−10.2	3.3	14	−22.7	10	−6.8	−3.2	−5.4	−5.2	3.4	3.8	3.6	3.6	88	77	85	83	0.5	1.1	0.6	0.7	8.6	7.8	6.9	7.8
III	978.2	994.1	951.2	1017.6	5.1	−3.7	14.7	30	−19.6	9	−2.2	3.7	0.9	0.8	5.0	6.0	5.7	5.6	90	72	83	82	0.6	2.4	1.2	1.4	8.0	6.1	5.8	6.6
IV	972.2	992.0	959.1	1010.7	10.8	2.2	18.1	6	−3.3	2	3.4	9.3	6.2	6.3	7.2	7.9	7.7	7.6	91	69	81	80	0.7	4.1	1.8	2.2	7.8	7.4	8.3	7.8
V	975.9	989.5	963.0	1013.9	14.4	5.9	22.1	17	−1.9	3	8.2	12.9	9.8	10.2	9.7	10.2	10.2	10.0	87	68	82	79	1.4	5.0	2.2	2.9	7.5	7.9	7.5	7.6
VI	975.9	977.0	965.4	1013.2	20.2	9.6	32.0	26	2.6	3	12.7	18.5	14.3	15.0	13.0	13.6	13.7	13.4	88	65	84	79	2.0	8.5	2.8	4.4	5.9	7.3	5.8	6.3
VII	975.8	983.2	964.7	1013.1	20.5	11.4	29.1	14	5.8	4	14.1	18.9	14.5	15.5	14.1	14.9	14.3	14.4	86	68	85	80	2.3	7.5	2.5	4.1	8.1	8.0	6.8	7.6
VIII	979.1	986.3	966.4	1016.8	20.6	9.5	28.8	6	3.8	31	11.7	18.9	14.0	14.6	12.4	12.9	13.5	12.9	90	59	84	78	1.9	9.8	3.0	4.9	5.5	6.6	5.6	5.9
IX	977.5	997.6	963.5	1014.9	19.1	9.0	25.0	2	2.4	22	11.4	17.9	12.8	13.7	11.8	12.4	12.5	12.2	87	61	84	77	2.1	8.4	2.6	4.4	5.9	5.8	3.8	5.2
X	985.8	997.4	976.3	1023.3	13.5	1.7	22.0	2	−6.2	23	3.3	12.3	6.0	6.9	7.3	8.9	8.2	8.1	91	60	85	79	0.8	5.6	1.5	2.6	7.1	4.6	3.5	5.1
XI	973.5	995.0	947.2	1012.8	3.2	−3.0	14.2	1	−12.8	24	−1.2	1.5	−0.4	−0.1	4.9	5.4	5.1	5.1	84	76	83	81	1.0	1.8	1.1	1.3	8.2	7.7	8.1	8.0
XII	968.9	988.2	948.4	1007.9	3.3	−2.0	10.7	19	−16.7	15	0.5	1.8	0.8	1.0	5.3	5.4	5.3	5.3	81	77	80	79	1.2	1.7	1.4	1.4	9.3	7.6	7.9	8.3
Rok	976.2	997.6	947.2	1014.7	10.9	2.3	32.0	26. VI	−22.7	10. II	4.5	9.4	6.1	6.5	8.2	8.9	8.8	8.5	88	70	84	81	1.3	4.8	1.8	2.6	7.5	7.0	6.6	7.0

Świerklaniec — φ = 50°26' — λ = 18°57'

I	–	–	–	–	1.7	−4.4	6.8	29	−14.3	8	−1.8	0.8	−1.5	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.9	7.4	8.3
II	–	–	–	–	−2.3	−10.3	2.7	14	−24.9	6	−7.4	−3.6	−6.2	−5.8	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.5	7.0	7.9
III	–	–	–	–	5.9	−4.5	16.8	30	−19.9	11	−2.1	4.9	0.2	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	5.0	7.0
IV	–	–	–	–	10.7	2.2	15.4	4	−3.0	16	4.2	9.4	5.7	6.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.8	5.7	7.2
V	–	–	–	–	14.9	5.5	23.4	19	−3.9	3	8.8	13.2	9.6	10.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.9	6.4	7.3
VI	–	–	–	–	20.9	10.3	31.6	26	5.7	8	14.3	19.0	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.2	6.3	6.5
VII	–	–	–	–	21.1	11.7	30.1	15	5.2	5	15.1	19.5	14.9	16.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.0	5.9	7.2
VIII	–	–	–	–	20.8	10.2	30.0	8	5.0	31	13.2	19.6	14.1	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	6.1	6.4
IX	–	–	–	–	20.5	8.8	27.2	3	4.5	13	11.1	19.0	13.3	14.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.0	4.9	6.0
X	–	–	–	–	13.5	2.7	22.7	2	−6.4	22	4.7	12.4	6.4	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	5.5	4.3	5.9
XI	–	–	–	–	3.0	−4.2	12.4	2	−18.0	18	−1.7	1.8	−0.7	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.6	8.3	7.5	8.5
XII	–	–	–	–	3.0	−1.9	8.8	19, 20	−11.9	15	0.3	2.0	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.9	8.1	8.4
Rok	–	–	–	–	11.1	2.2	31.6	26. VI	−24.9	6. II	4.9	9.8	5.9	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.5	6.2	7.2

Duszniki-Zdrój — φ = 50°24' — λ = 16°24'

I	–	–	–	–	1.2	−3.5	4.7	29	−12.5	7	−2.2	0.2	−1.1	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.9	8.6	8.1
II	–	–	–	–	−2.9	−9.3	0.9	7	−17.6	6	−6.8	−3.8	−6.0	−5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.9	6.9	7.7
III	–	–	–	–	4.4	−4.1	12.6	30	−16.4	9	−2.4	3.4	−0.7	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.8	5.7	6.3
IV	–	–	–	–	8.9	1.4	16.1	6	−2.4	2	2.9	7.7	4.0	4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.6	7.5	7.5
V	–	–	–	–	12.7	5.0	21.0	17	−1.7	4	7.8	11.7	8.1	8.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.8	7.2	7.5
VI	–	–	–	–	18.6	8.8	30.4	26	3.1	3	12.2	17.1	12.7	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	5.5	6.2
VII	–	–	–	–	18.6	10.7	29.1	14	5.8	4, 5	13.3	17.0	13.3	14.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.8	6.7	7.4
VIII	–	–	–	–	18.8	9.1	28.0	6	4.3	16	11.8	17.7	12.4	13.6	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.6	5.4	5.6
IX	–	–	–	–	17.5	8.2	23.9	2	4.1	20	10.6	16.6	11.4	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.4	3.6	4.9
X	–	–	–	–	12.1	2.0	20.2	1	−4.3	22	4.0	11.2	5.0	6.3	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.5	3.2	4.4
XI	–	–	–	–	2.1	−3.7	12.0	2	−13.3	24	−1.9	0.8	−1.2	−0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.1	7.6	7.3
XII	–	–	–	–	2.1	−2.1	10.7	19	−10.4	14	−0.3	0.6	0.2	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	9.0	8.0	8.5
Rok	–	–	–	–	9.5	1.9	30.4	26. VI	−17.6	6. II	4.1	8.4	4.8	5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.3	6.8

Tomaszów Lub. II $H_s = 270$ m $h_w = 13$ m   1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V ≥10	Wiatr V >15	◔	●	Opad R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	K (K)
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	45	9.6	17	7	13	28	·	—	—	5	22	15	12	·	—	31	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	23	3.9	16	17	24	28	·	—	—	1	14	24	10	·	—	28	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	31	9.5	3	7	7	26	·	—	—	5	10	14	8	·	—	18	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	56	15.5	28	·	·	11	·	—	—	·	11	14	9	2	—	·	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	47	8.6	27	·	·	3	1	—	—	1	10	22	15	·	—	·	—
VI	10	3.4	6.5	4.3	5	3.2	7.5	3.5	6	3.5	7	3.6	14	4.3	20	3.2	14	3.1	90	17.9	9	·	·	·	6	·	·	2	10	15	10	3	—	·	—
VII	5	1.9	1	2.5	7.5	2.2	7.5	2.9	5.5	3.0	19	3.8	29	4.1	6.5	2.0	12	2.9	134	52.5	17	·	·	·	5	·	·	1	12	22	16	2	—	·	—
VIII	9.5	3.5	1.5	3.0	3	3.2	6.5	3.4	2	4.2	14	3.6	18.5	3.9	17	4.2	21	2.9	70	27.2	1	·	·	·	7	·	·	5	9	10	10	2	—	·	—
IX	1.5	4.0	0.5	2.0	0.5	2.0	5	2.7	18	3.6	20	3.5	13.5	4.1	9	3.5	22	2.7	35	17.5	11	·	·	·	4	2	1	9	1	9	7	1	—	·	—
X	11	3.3	3	2.3	5.5	3.0	4.5	3.0	1	2.0	17	4.7	21	5.0	17	4.6	13	3.6	7	2.5	31	·	·	8	·	·	·	5	10	8	2	·	—	·	—
XI	2.5	3.6	6	4.3	9.5	5.9	15.5	3.5	5	3.3	9.5	4.8	25	5.1	6	3.7	11	4.0	65	23.6	21	6	13	22	·	3	·	·	20	13	11	2	—	16	—
XII	5.5	4.0	4.5	4.2	·	·	26	4.5	14.5	4.2	17.5	4.3	17.5	5.1	1.5	4.0	6	4.2	50	12.9	18	2	8	23	·	1	·	1	17	13	10	1	—	3!	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	653	52.5	17. VII	39	65	149	23	—	—	35	146	179	120	13	—	96!	—

ROZKŁAD WIATRU (n, v) · OPAD R · LICZBA DNI (n)

Kłodzko $H_s = 316$ m $H_b = 317{,}3$ m $h_w = 15{,}4$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V ≥10	V >15	◔	●	R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	K (K)
I	6.5	2.2	5.5	1.9	0.5	3.0	1	1.0	30.5	4.9	16.5	4.7	4	4.0	3.5	3.0	25	3.0	37	9.3	9	2	3	27	·	1	·	·	19	15	9	·	·	28	·
II	12	2.8	10	3.0	1.5	2.3	·	·	7.5	3.3	5.5	3.9	8.5	5.0	11	3.8	28	2.4	23	4.7	17	13	21	28	·	1	·	1	16	22	7	·	1	28	·
III	5	2.2	9.5	2.7	1	2.0	·	·	12	4.0	15	3.4	4.5	3.8	7	2.4	39	1.8	32	6.2	21	5	6	20	·	·	·	2	12	12	8	·	7	16	·
IV	8	2.5	12	2.4	6	1.7	2.5	2.2	8.5	2.8	6.5	3.5	9.5	2.9	9	2.8	28	1.8	70	12.3	20	·	·	8	·	·	·	2	20	16	11	2	1	·	·
V	13	2.3	11.5	2.6	2.5	3.6	1.5	2.7	6.5	2.3	5	2.3	11	3.5	10	2.8	33	1.8	179	56.4	29	·	·	2	·	·	·	2	18	21	15	6	2	·	7
VI	13	2.1	6	1.3	1	2.0	4.5	2.7	13	3.3	7	2.7	10	3.7	9.5	2.5	26	1.9	87	20.2	22	·	·	·	5	·	·	1	8	17	14	2	4	·	7
VII	6	1.6	3.5	1.3	0.5	2.0	2	2.2	10	2.5	19	3.1	18.5	3.2	10.5	2.0	23	2.0	79	15.3	16	·	·	·	3	1	·	·	14	19	16	2	2	·	11
VIII	9	2.1	5.5	1.6	0.5	2.0	2.5	3.2	16	4.4	3.5	3.6	6	2.0	8	1.6	42	1.6	86	29.2	24	·	·	·	7	1	·	3	6	11	7	4	6	·	3
IX	1	1.0	·	·	0.5	2.0	12.5	3.0	25.5	4.5	8	3.5	5	2.6	3.5	1.9	34	2.2	36	21.0	28	·	·	·	·	1	·	6	6	9	5	1	5	·	3
X	7.5	1.5	6.5	1.7	1	3.0	0.5	2.0	14	2.7	4.5	3.8	3	2.5	7	1.4	49	1.1	3	2.2	16	·	·	14	·	·	·	4	7	3	1	·	12	·	·
XI	7	1.9	7.5	2.2	1	2.5	3	5.0	15	5.5	10.5	4.6	8	4.6	4	1.1	34	2.4	33	12.0	11	1	9	24	·	3	·	·	20	17	7	1	5	15	·
XII	1.5	1.7	1.5	1.0	·	·	8.5	3.6	29.5	4.6	20.5	4.5	12.5	4.2	1	4.0	18	3.5	31	9.9	13	3	3	20	·	6	·	·	20	16	5	·	3	11	·
Rok	89.5	2.0	79	1.8	16	2.2	38.5	2.3	187	3.7	121.5	3.6	100.5	3.5	84	2.4	379	2.1	696	56.4	29. V	24	42	143	15	14	·	21	166	178	105	18	48	98	31

Uwaga. Kierunki i prędkości wiatru - wg anemometru M-47.

Świerklaniec $H_s = 284$ m $h_w = 13{,}5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V ≥10	V >15	◔	●	R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	K (K)
I	7.5	2.9	1	1.5	0.5	1.0	8.5	1.7	14.5	2.3	28	3.9	15.5	3.1	11.5	1.8	6	2.7	54	10.1	31	2	6	29	·	1	·	·	18	15	12	1	1	31	·
II	8	3.6	7	3.1	1	5.0	·	·	0.5	1.0	12.5	6.8	29.5	3.8	24.5	3.8	1	4.2	32	7.2	17	10	23	28	·	2	·	·	16	23	11	·	3	28	·
III	10.5	2.3	2.5	3.8	2	3.0	10.5	1.5	9	1.7	20.5	3.2	17	3.4	14	2.8	7	2.5	46	12.8	6	8	5	22	·	1	·	·	11	19	11	1	7	20	·
IV	7	3.2	15.5	3.2	14	3.1	3.5	3.3	4	2.8	13	2.4	15	4.1	15	2.5	3	3.0	40	9.2	23	·	·	7	·	·	·	4	15	17	11	·	3	·	3
V	11.5	2.1	7	2.3	6	3.8	6	3.2	0.5	3.0	15	2.3	19	3.1	27	2.3	1	2.6	108	21.9	29	·	·	3	·	·	·	2	13	22	20	2	2	·	6
VI	7.5	1.8	10	2.4	7	1.6	2.5	1.6	2.5	4.4	9	3.7	26	2.8	23.5	2.9	2	2.6	92	19.5	11	·	·	·	5	·	·	1	9	14	14	2	·	·	7
VII	4	2.0	4	2.0	3.5	2.7	2.5	2.6	2.5	3.8	26	4.2	32	3.0	12.5	2.1	6	3.0	95	27.2	17	·	·	·	3	·	·	·	12	20	14	3	2	·	4
VIII	4	1.0	10	1.5	1.5	1.3	6.5	3.2	4	2.2	10.5	3.3	22.5	2.5	30	2.1	4	2.2	58	16.8	24	·	·	·	8	·	·	3	12	13	10	1	2	·	3
IX	1	2.5	1	3.0	2	2.0	12.5	2.8	15	2.8	22	2.4	14	2.6	17.5	1.7	5	2.3	70	21.2	4	·	·	·	2	·	·	5	10	12	10	3	11	·	·
X	12	1.4	13	2.1	6	2.3	0.5	2.0	·	·	13	4.3	26.5	3.2	14	2.1	9	2.4	4	1.6	16	·	·	8	·	·	·	5	10	4	2	·	15	·	·
XI	7	2.4	11.5	3.1	4	2.4	5.5	2.9	3.5	2.3	20	3.8	22	3.5	11.5	2.1	5	2.9	40	9.4	11	4	10	24	·	·	·	·	21	21	10	·	10	13	·
XII	3	1.7	2.5	2.2	2.5	3.0	2	2.8	7.5	4.5	42.5	4.7	21	3.1	12	2.4	·	3.8	47	10.5	18	1	2	21	·	2	·	·	18	19	11	1	1	10	·
Rok	83	2.2	85	2.5	50	2.6	60.5	2.3	63.5	2.6	232	3.8	259	3.2	213	2.4	49	2.8	686	27.2	17. VII	25	46	142	18	6	·	20	165	199	136	14	57	102	23

Duszniki-Zdrój $H_s = 540$ m $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V ≥10	V >15	◔	●	R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	K (K)
I	7	3.7	1.5	3.3	1	5.0	5.5	3.6	·	·	46	4.5	·	·	·	·	32	2.8	80	15.0	9	1	10	30	·	3	3	·	18	18	14	2	10	31	·
II	16.5	4.7	5	3.2	0.5	2.0	5	2.0	·	·	28	5.5	·	·	·	·	29	3.1	69	10.5	13	8	24	28	·	3	·	1	17	21	17	1	3	28	·
III	12	5.2	·	·	·	·	·	·	·	·	35.5	3.5	1.5	2.0	·	·	44	2.0	58	10.2	21	4	7	21	·	2	·	4	13	12	9	1	1	17	·
IV	15	2.8	2	3.0	·	·	1	4.0	·	·	48	2.5	2.5	2.0	7.5	2.3	14	2.2	97	17.0	17	·	·	5	·	·	·	5	20	18	17	3	9	·	·
V	22.5	3.2	14	2.9	0.5	2.0	7	3.7	1	4.0	33.5	2.5	2.5	3.6	2	2.5	10	2.6	260	53.5	29	·	·	4	·	·	·	2	18	24	20	9	6	·	6
VI	7	2.9	8.5	2.7	0.5	2.0	3	3.3	·	·	52	3.1	4	2.2	2	4.0	13	2.6	151	31.5	22	·	·	·	2	·	·	3	11	15	15	5	2	·	8
VII	7	2.3	·	·	·	·	9	3.1	5	4.8	27	3.7	4	2.5	·	·	41	1.9	122	27.5	16	·	·	·	2	·	·	1	18	23	20	3	1	·	10
VIII	12	2.3	5	2.0	·	·	·	·	·	·	42	3.0	·	·	·	·	34	1.8	91	24.0	24	·	·	·	4	·	·	3	10	10	7	5	1	·	3
IX	3	2.0	1	2.0	·	·	6	3.0	·	·	46	3.8	·	·	1	2.0	33	2.2	59	23.0	28	·	·	·	·	·	·	8	7	12	8	2	2	·	2
X	16	2.2	3	2.0	·	·	·	·	·	·	22	3.0	·	·	·	·	52	1.2	14	7.8	31	·	·	15	·	·	·	11	10	3	2	·	5	·	·
XI	6	5.0	8	3.2	·	·	·	·	·	·	34	4.9	·	·	·	·	42	2.5	80	18.0	27	4	10	26	·	2	·	6	20	16	13	1	8	19	·
XII	1	6.0	3	2.0	·	·	·	·	·	·	61	4.2	·	·	·	·	28	2.9	102	19.6	18	2	6	24	·	1	·	1	21	21	15	4	5	22	·
Rok	125	3.5	51	2.2	2.5	0.9	36.5	1.9	6	0.7	475	3.7	14.5	1.0	12.5	0.9	372	2.3	1183	53.5	29. V	19	57	153	8	11	3	45	183	193	157	36	53	117	29

Polanica-Zdrój

$\varphi = 50°24'$ $\lambda = 16°30'$ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.8	−2.9	6.8	17	−11.6	7	−1.2	1.1	−0.2	−0.1	5.1	5.4	5.4	5.3	89	81	89	86	0.6	1.4	0.7	0.9	8.0	7.6	8.7	8.1
II	–	–	–	–	−1.6	−8.5	2.5	14	−17.9	6	−6.2	−2.9	−5.1	−4.8	3.5	3.8	3.7	3.7	88	75	85	83	0.4	1.2	0.6	0.7	8.8	8.1	6.8	7.9
III	–	–	–	–	5.7	−3.8	14.3	30	−19.2	9	−2.2	4.2	0.4	0.7	5.1	5.9	5.8	5.6	91	69	88	83	0.5	2.9	0.8	1.4	7.2	6.3	6.3	6.6
IV	–	–	–	–	10.6	1.9	17.8	6	−3.7	2	3.7	9.0	5.6	6.0	7.2	7.9	7.7	7.6	90	70	84	81	0.8	3.8	1.5	2.0	8.0	7.4	7.8	7.7
V	–	–	–	–	14.3	5.7	23.1	17	−2.3	3	8.4	12.7	8.9	9.7	9.8	10.1	10.1	10.0	86	69	87	81	1.4	4.9	1.6	2.6	7.3	8.0	7.5	7.6
VI	–	–	–	–	20.4	9.5	31.9	26	2.7	3	13.3	18.4	13.7	14.8	13.1	13.1	13.4	13.2	84	64	85	78	2.4	8.8	2.6	4.6	6.4	6.9	5.4	6.2
VII	–	–	–	–	20.2	11.3	29.6	14	5.9	4	14.4	18.6	14.0	15.2	14.1	14.1	14.0	14.1	85	66	86	79	2.6	7.9	2.2	4.2	7.7	7.8	5.8	7.1
VIII	–	–	–	–	20.3	9.5	29.7	7	3.9	16	12.4	18.9	13.5	14.6	12.6	12.9	13.3	12.9	89	59	86	78	1.9	9.9	2.6	4.8	5.5	6.8	4.5	5.6
IX	–	–	–	–	19.0	8.6	25.2	3	2.8	22	11.3	17.8	12.0	13.3	11.8	12.6	12.5	12.3	88	62	88	79	2.0	8.1	1.9	4.0	5.9	5.6	3.5	5.0
X	–	–	–	–	13.2	1.5	21.5	2	−5.4	22	3.2	11.8	5.1	6.3	7.7	9.0	8.3	8.3	96	63	91	83	0.4	5.2	0.9	2.2	5.7	5.1	3.8	4.9
XI	–	–	–	–	3.3	−3.0	14.2	1	−13.5	24	−1.3	1.5	−0.6	−0.2	5.1	5.7	5.4	5.4	89	81	89	86	0.8	1.5	0.8	1.0	7.9	7.8	7.8	7.8
XII	–	–	–	–	2.7	−1.6	11.4	20	−11.6	15	0.4	2.1	1.1	1.2	5.6	5.8	5.7	5.7	88	81	85	85	0.8	1.4	1.1	1.1	8.5	7.9	7.2	7.9
Rok	–	–	–	–	11.0	2.4	31.9	26. VI	−19.2	9, III	4.7	9.4	5.7	6.4	8.4	8.9	8.8	8.7	89	70	87	82	1.2	4.8	1.4	2.5	7.2	7.1	6.3	6.9

Wolbrom

$\varphi = 50°23'$ $\lambda = 19°45'$

I	–	–	–	–	1.0	−5.4	6.1	29	−13.3	13	−2.6	0.0	−2.2	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	9.0	7.5	8.3
II	–	–	–	–	−3.2	−11.8	2.3	12	−27.0	6	−8.4	−4.3	−7.5	−6.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.5	7.4	8.0
III	–	–	–	–	4.9	−5.2	15.5	30	−17.9	1	−1.6	4.1	−0.9	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.7	5.7	6.7
IV	–	–	–	–	9.4	1.8	13.7	7	−2.1	1	3.8	8.6	4.8	5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.1	6.5	7.6
V	–	–	–	–	13.8	5.2	25.6	19	−4.2	3	8.7	12.6	8.9	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.4	6.5	7.3
VI	–	–	–	–	20.1	9.8	31.5	26	3.6	3	14.6	18.8	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.9	5.5	5.9
VII	–	–	–	–	20.3	10.8	27.2	14	5.6	11	15.3	19.4	14.0	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.2	5.5	6.5
VIII	–	–	–	–	19.6	9.2	29.7	7	4.7	18, 31	13.2	18.5	13.3	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.4	6.3	6.6
IX	–	–	–	–	19.8	7.7	26.3	3	1.7	22	11.9	18.4	12.4	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.7	5.1	5.4
X	–	–	–	–	12.0	2.2	19.7	1	−4.5	13	4.7	11.7	5.9	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	4.8	4.5	5.1
XI	–	–	–	–	2.6	−4.0	12.5	2	−14.9	24	−2.1	1.0	−1.2	−0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	8.1	8.0
XII	–	–	–	–	2.9	−1.8	9.1	20	−8.9	15	−0.1	1.7	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.2	8.3	8.0
Rok	–	–	–	–	10.3	1.5	31.5	26. VI	−27.0	6. II	4.8	9.2	5.2	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.3	6.4	7.0

Ząbkowice

$\varphi = 50°22'$ $\lambda = 19°17'$

I	–	–	–	–	1.8	−3.9	7.9	29	−11.6	7	−2.0	1.0	−1.0	−0.8	4.7	5.1	5.0	4.9	86	78	88	85	0.7	1.6	0.7	1.0	7.3	7.9	6.7	7.3
II	–	–	–	–	−2.6	−10.2	2.3	14	−24.1	6	−7.5	−3.8	−6.8	−6.2	3.2	3.5	3.2	3.3	87	75	83	82	0.5	1.2	0.6	0.8	8.7	6.0	7.7	7.5
III	–	–	–	–	6.2	−3.0	16.6	30	−14.9	11	−0.9	5.1	0.9	1.5	5.3	5.4	5.5	5.4	87	61	80	76	0.7	3.8	1.4	2.0	6.9	6.3	4.9	6.0
IV	–	–	–	–	10.6	2.3	15.6	3	−2.8	2	4.3	9.5	5.4	6.2	7.0	7.4	7.7	7.4	84	63	84	77	1.4	4.7	1.4	2.5	6.7	7.5	5.8	6.7
V	–	–	–	–	14.9	5.9	26.5	19	−1.8	3	9.0	13.3	9.5	10.3	9.8	10.1	10.2	10.0	83	66	84	78	1.9	5.7	1.9	3.2	7.2	8.4	5.9	7.2
VI	–	–	–	–	20.9	10.6	31.2	26	4.8	15	14.6	19.2	14.7	15.8	13.4	13.2	13.9	13.5	81	61	83	75	3.6	9.9	3.1	5.5	4.8	6.6	5.9	5.8
VII	–	–	–	–	21.1	11.9	29.8	14, 15	4.7	5	15.2	19.6	14.7	16.0	14.3	14.5	14.7	14.5	82	64	87	78	3.4	9.1	2.3	4.9	6.5	7.8	4.9	6.4
VIII	–	–	–	–	20.6	10.3	30.8	7	4.6	31	13.5	19.4	14.1	15.3	13.2	12.3	13.5	13.0	85	57	83	75	2.7	11.1	3.0	5.6	5.2	7.2	5.4	5.9
IX	–	–	–	–	20.5	9.6	28.2	3	5.0	13	12.1	19.0	13.4	14.5	12.1	12.2	13.0	12.4	85	57	85	76	2.3	10.4	2.6	5.1	4.6	5.5	3.9	4.7
X	–	–	–	–	13.1	2.5	22.1	2	−5.0	23	4.7	12.4	6.3	7.4	8.0	8.4	8.5	8.3	89	56	85	77	1.0	6.5	1.5	3.0	6.2	4.5	3.8	4.8
XI	–	–	–	–	3.0	−3.6	12.5	2	−15.0	18	−1.5	1.7	−0.6	−0.2	4.9	5.2	5.2	5.1	84	74	84	81	1.0	2.1	1.0	1.4	7.4	7.7	7.2	7.4
XII	–	–	–	–	3.2	−1.8	9.9	20	−11.1	15	0.0	2.1	0.7	0.9	5.3	5.4	5.3	5.3	84	75	82	80	1.0	1.9	1.3	1.4	7.8	8.3	7.7	7.9
Rok	–	–	–	–	11.1	2.6	31.2	26. VI	−24.1	6. II	5.1	9.9	5.9	6.7	8.4	8.6	8.8	8.6	85	66	84	78	1.7	5.7	1.7	3.0	6.6	7.0	5.8	6.5

Miechów

$\varphi = 50°22'$ $\lambda = 20°02'$

I	–	–	–	–	1.3	−5.1	5.9	30	−13.8	12	−2.9	0.3	−2.0	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.3	6.5	7.8
II	–	–	–	–	−3.0	−10.3	2.6	14	−23.5	7	−7.5	−4.1	−7.1	−6.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	6.8	7.7
III	–	–	–	–	5.1	−4.2	15.7	30	−19.4	1	−2.6	4.2	−0.2	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.3	4.6[3]	6.3[3]
IV	–	–	–	–	9.9	1.9	14.6	7	−1.7	1, 16	3.3	8.7	5.4	5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	4.8	7.2
V	–	–	–	–	14.5	5.5	26.7	19	−3.6	3	8.6	13.0	9.4	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	8.4	6.8	7.2
VI	–	–	–	–	20.7	9.7	30.5	26	3.4	3	14.4	19.4	14.5	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.5	6.7	6.1
VII	–	–	–	–	21.2	10.7	27.8	14	5.8	10, 11	14.8	19.7	14.5	15.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.7	6.1	7.0
VIII	–	–	–	–	20.4	9.4	30.1	7	4.9	31	12.4	19.1	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.7	6.1	6.2
IX	–	–	–	–	20.4	7.9	26.7	3	2.7	22	10.1	19.1	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.6	4.4	5.5
X	–	–	–	–	12.3	1.9	20.3	1, 2	−4.7	23	3.7	11.6	5.8	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.3	4.7	5.4
XI	–	–	–	–	2.6	−4.0	13.8	2	−17.9	18	−2.2	1.2	−1.2	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	7.5	7.9
XII	–	–	–	–	3.1	−1.5	9.4	20	−7.6	16	0.0	1.9	0.6	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.1	7.9	8.1
Rok	–	–	–	–	10.7	1.8	30.5	26. VI	−23.5	7. II	4.3	9.5	5.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	6.1	6.9

Polanica-Zdrój — H_s = 400 m — h_w = 11,3 m — 1965

MIESIĄC	ROZKŁAD WIATRU n(D), V(D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	☒	K (K)
I	7	2.0	2	1.0	2	2.5	1	2.0	9.5	2.6	10.5	2.6	10	2.9	8	2.4	43	1.3	50	14.3	18	1	2	27	·	·	·	·	17	14	11	1	12	31	·
II	15.5	2.8	6.5	2.3	1	2.0	1	2.0	1	2.0	5	3.6	12.5	2.9	14.5	2.1	27	1.8	36	4.9	17	8	20	28	·	·	·	1	16	18	14	·	7	28	·
III	6	2.3	4	3.0	1	3.0	2	2.5	6	3.0	3	4.0	10.5	3.2	13.5	2.4	47	1.4	39	11.2	21	4	5	20	·	·	·	3	14	13	9	1	11	18	·
IV	6	2.3	7	2.6	2	2.5	1	2.0	1	5.0	5	3.4	15.5	3.4	9.5	2.8	43	1.6	66	15.2	20	·	·	7	·	·	·	3	21	14	12	1	9	·	·
V	15	2.2	2	2.0	3	3.3	·	·	2.5	4.0	2.5	3.2	14	2.9	17	2.5	37	1.6	238	51.1	29	·	·	4	·	·	·	2	14	23	19	8	5	·	8
VI	10.5	2.4	·	·	·	·	·	·	0.5	4.0	12.5	4.2	9.5	3.1	22	2.2	35	1.8	116	18.2	22	·	·	·	5	1	·	3	12	17	14	5	3	·	8
VII	3	2.0	1	2.0	·	·	2	2.0	1	3.5	9.5	3.0	23.5	2.8	16	2.3	37	1.6	119	23.1	15	·	·	·	2	·	·	1	12	22	15	4	4	·	8
VIII	7.5	1.9	·	·	1	3.0	0.5	4.0	1.5	4.0	10	3.6	10.5	2.5	11	2.2	51	1.2	119	30.3	24	·	·	·	6	·	·	3	5	11	9	5	10	·	3
IX	5	1.6	·	·	2	3.5	6.5	3.5	5	4.0	11.5	3.2	13.5	2.7	8.5	1.8	38	1.6	38	18.8	28	·	·	·	1	·	·	6	6	9	8	1	6	·	1
X	9	2.1	2	2.0	2	2.0	1	2.0	·	·	2	3.0	8	2.6	12	2.4	57	0.9	10	4.3	16	·	·	13	·	·	·	8	8	3	3	·	21	·	·
XI	3	2.0	11	3.0	2	3.0	2.5	2.4	3.5	4.1	10.5	5.6	13	3.8	9.5	1.9	35	2.1	52	13.4	27	2	8	23	·	1	·	2	19	16	11	1	11	17	·
XII	1.5	1.7	0.5	1.0	2	3.0	3	2.7	9	3.8	23.5	4.8	16.5	2.7	10	2.4	27	2.5	61	15.9	5	2	1	22	·	1	·	1	19	19	12	2	6	19	·
Rok	89	2.1	36	1.6	18	2.3	20.5	2.1	40.5	3.3	105.5	3.7	157	3.0	151.5	2.3	477	1.6	944	51.1	29.V	17	36	144	14	3	·	33	163	179	137	29	105	113	28

Wolbrom — H_s = 373 m — h_w = 13,5 m

I	6.5	3.8	4.5	3.7	6.5	2.2	5	5.3	4	3.0	7.5	7.2	25	3.9	1	1.0	33	2.6	58	11.3	31	5	12	28	·	4	·	·	19	14	13	1	7	31	·
II	7.5	4.8	6.5	3.0	2	2.5	·	·	·	·	8	7.7	25	4.5	12	5.5	23	3.6	38	5.4	17	15	25	28	·	7	·	1	16	21	13	·	7	28	·
III	2.5	1.8	7	2.4	5.5	2.9	8	4.0	4.5	3.1	6	5.0	16	4.4	3.5	4.7	40	2.2	43	13.8	21	8	6	23	·	4	·	4	13	16	9	1	7	19	·
IV	2	3.8	4.5	2.2	31.5	3.8	1.5	3.0	5.5	3.2	1.5	7.3	13	3.5	6.5	2.9	24	2.6	40	6.5	23	·	·	7	·	2	·	1	16	16	14	·	5	·	1
V	9.5	3.0	3	1.3	12.5	4.2	3	3.3	1.5	2.0	14	3.4	14.5	3.7	9	3.1	26	2.5	122	33.0	29	·	·	3	1	4	1	2	14	23	19	2	5	·	2
VI	4.5	3.4	5	2.9	13.5	3.3	2.5	3.8	4.5	3.9	7.5	5.7	17	3.4	10.5	3.1	25	2.6	119	36.0	27	·	·	·	5	2	·	5	9	14	14	4	1	·	4
VII	3	1.7	0.5	2.0	6.5	2.8	2.5	2.2	2.5	3.2	20.5	3.7	19	3.2	2.5	3.2	36	2.0	75	25.7	17	·	·	·	4	1	1	2	8	23	15	1	2	·	4
VIII	6	2.1	2.5	2.4	6	1.8	7.5	2.4	4	3.1	9	2.7	9	2.3	14	2.4	35	1.5	99	26.0	1	·	·	·	4	·	·	3	12	16	12	2	4	·	2
IX	·	·	2	2.0	5	2.6	12	3.1	9.5	2.7	13	2.6	8.5	2.7	2	3.2	38	1.6	74	17.2	4	·	·	·	1	·	·	6	6	10	9	4	10	·	1
X	3	1.7	4.5	1.8	7	2.6	2	2.5	·	·	9	2.4	19.5	2.5	8	2.2	40	1.3	4	1.4	31	·	·	9	·	·	·	9	10	5	2	·	13	·	·
XI	1	3.0	6	5.2	5	2.3	9	3.7	5	2.9	11	4.6	12	3.9	3	1.0	38	2.1	30	6.2	21	4	10	25	·	2	·	2	20	20	11	·	6	13	·
XII	3.5	2.6	0.5	2.0	3	1.5	8	2.7	8.5	2.6	32.5	4.5	19	3.6	4	2.8	14	3.1	35	11.9	18	·	4	22	·	2	·	1	16	19	9	1	2	11	·
Rok	49	2.6	46.5	2.6	104	2.7	61	3.0	49.5	2.5	139.5	4.7	197.5	3.5	76	2.9	372	2.3	737	36.0	27. VI	32	57	145	15	28	2	36	159	197	140	16	69	102	14

Ząbkowice — H_s = 314 m — h_w = 14 m

I	9	2.4	1	4.0	17	2.2	6	2.2	3	2.7	26.5	2.5	8	3.1	8.5	1.9	14	2.1	54	11.4	31	2	7	29	·	·	·	2	16	14	13	1	1	30	·
II	13.5	3.7	4.5	3.6	7	2.0	2	6.0	0.5	2.0	17.5	4.5	12.5	3.3	13.5	4.3	13	3.2	36	6.4	17	12	24	28	·	3	·	1	14	22	12	·	4	28	·
III	15.5	2.2	6	4.0	6	2.2	7	1.8	7.5	2.4	12.5	3.6	17	2.4	7.5	2.1	14	2.2	46	9.2	21	5	6	21	·	1	1	3	11	15	9	·	5	16	·
IV	6	2.4	7	4.2	18.5	3.1	10	2.7	3.5	3.1	2	2.0	11	2.9	17	2.9	15	2.5	49	12.0	28	·	·	6	·	·	·	5	15	17	13	1	·	·	3
V	15.5	2.5	6	3.8	13	4.1	3.5	2.9	·	·	8	2.0	12	2.9	19	2.4	16	2.4	112	19.0	29	·	·	3	1	1	1	2	17	20	16	2	4	·	5
VI	13	2.2	5.5	1.8	7	3.0	6	3.7	2.5	1.6	5	2.7	19.5	3.0	13.5	2.3	18	2.1	101	14.8	10	·	·	·	5	·	·	4	11	14	13	4	·	·	2
VII	5	1.8	3	3.3	6.5	3.9	3.5	2.7	4.5	1.8	15.5	2.8	19.5	2.4	10.5	2.0	25	1.9	119	38.0	17	·	·	·	5	·	·	·	7	18	12	4	·	·	3
VIII	10	1.8	0.5	1.0	7	2.3	5.5	2.5	2.5	3.2	8	2.2	9.5	1.9	17	2.1	33	1.4	82	19.8	25	·	·	·	8	·	·	3	9	14	12	2	·	·	2
IX	4	1.8	·	·	10.5	2.3	9.5	2.8	3.5	1.7	20	2.4	6.5	1.9	7	2.0	27	1.6	89	21.0	28	·	·	·	2	·	·	7	5	12	10	4	5	·	1
X	10.5	1.8	7	2.0	11.5	2.6	0.5	1.0	1.5	1.0	8.5	2.3	19	2.0	5.5	2.4	29	1.5	2	1.1	16	·	·	7	·	·	·	8	6	2	2	·	8	·	·
XI	5	1.8	7	3.3	10	2.8	9	1.9	1.5	2.0	4.5	2.2	19	3.0	11	1.7	23	1.8	39	8.2	11	4	10	24	·	·	·	3	16	18	12	·	5	12	·
XII	4	1.8	·	·	7	2.1	7.5	1.3	3.5	2.1	20.5	3.0	24	3.2	8.5	2.1	18	2.1	44	9.9	18	1	2	23	·	·	·	1	19	19	10	·	-	7	·
Rok	111	2.2	47.5	2.6	121	2.7	70	2.6	34	2.0	148.5	2.7	179.5	2.7	138.5	2.4	245	2.1	773	38.0	17.VII	24	49	141	21	5	2	39	146	185	134	18	32	93	16

Miechów — H_s = 292 m — h_w = 16,4 m

I	7	5.0	5.5	4.3	12	2.8	10	2.7	5	2.8	13.5	3.1	11	5.3	12	4.3	17	3.1	43	10.7	31	5	11	27	·	3	·	1	16	13	10	1	4	31	·
II	10	5.2	6.5	3.9	3	3.7	·	·	1	2.0	7	5.3	21.5	4.9	26	5.1	9	4.3	15	2.6	17	14	25	28	·	1	·	1	17	17	6	·	1	28	·
III	4.5	6.3	6	3.8	7.5	2.9	8	2.6	6	2.2	2	6.0	10	4.5	14	3.3	35	2.3	33	6.9	21	5	6	22	·	1	·	4	13	17	9	·	5	21	·
IV	3.5	4.1	7.5	3.4	24.5	4.4	14.5	3.7	4	2.6	2	4.5	11.5	4.9	12.5	3.8	10	3.6	50	11.4	20	·	·	9	·	1	·	3	14	13	10	1	2	·	2
V	6	4.8	2.5	3.6	14	4.5	8	2.4	8.5	2.4	3	4.2	12.5	4.0	20.5	4.0	18	3.1	101	14.4	19	·	·	3	1	2	1	1	13	20	19	4	·	·	7
VI	7	4.1	6.5	4.0	11.5	3.5	5	2.9	7	2.7	3.5	4.7	13	3.4	20.5	4.0	16	3.0	128	45.7	27	·	·	·	5	·	·	4	11	14	12	3	·	·	3
VII	1.5	3.3	2	3.0	8	3.2	5.5	3.4	9	2.2	15	3.4	19	3.7	11	2.5	22	2.4	60	14.5	17	·	·	·	7	1	·	2	11	19	13	1	·	·	4
VIII	9.5	4.2	1.5	3.3	6	1.9	9	2.3	6	2.7	3.5	2.6	8	3.6	20.5	3.9	29	2.2	124	29.4	1	·	·	·	7	·	·	5	13	17	14	4	·	·	3
IX	4	2.4	·	·	4	1.9	18.5	3.0	8.5	3.0	6	3.6	9	2.8	8	3.2	32	1.9	82	20.0	4	·	·	·	2	·	·	3	5	10	7	4	5	·	2
X	4	3.8	5.5	2.9	10	2.5	7.5	2.1	1	2.5	6.5	4.4	14.5	3.7	14	3.6	30	2.2	3	0.7	8	·	·	13	·	·	·	9	11	8	·	·	5	·	·
XI	1	2.5	9	4.1	10	4.1	12.5	2.8	5	2.0	7.5	4.3	15	4.4	13	2.9	17	2.9	36	11.4	11	6	11	23	·	·	·	2	18	17	9	1	5	19	·
XII	4	5.0	1	3.0	4.5	2.4	12.5	2.4	12	2.8	19.5	4.6	22	4.3	8.5	4.2	9	3.4	32	9.3	3	·	4	22	·	·	·	·	17	13	7	·	·	11	·
Rok	62	4.2	53.5	3.3	115	3.2	111	2.5	73	2.5	89	4.2	167	4.1	180.5	3.7	244	2.9	707	45.7	27.VI	30	57	147	22	9	1	35	159	178	116	19	27	110	21

Tarnogród — φ = 50°22' — λ = 22°45' — 1965

Miesiąc	Ciśnienie p: P_m	Max	Min	$P_{o.m}$	Temperatura t: Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	–	–	–	–	–	–5.6	–	–	–20.9	11	–3.2	–0.3	–2.8	–2.3	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.5	7.7	8.5
II	–	–	–	–	–	–10.4	–	–	–25.4	7	–7.9	–4.2	–7.5	–6.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	7.5	7.9
III	–	–	–	–	–	–3.9	–	–	–19.4	1	–1.1	5.0	0.7	1.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.9	5.9	6.2
IV	–	–	–	–	–	2.3	–	–	–2.1	3	5.0	9.4	5.5	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.6	5.7	7.2
V	–	–	–	–	–	6.1	–	–	–3.1	4	9.9	14.2	9.9	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	11.1	–	–	5.4	8	16.0	20.3	15.5	16.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.1	6.2	5.7
VII	–	–	–	–	–	11.6	–	–	6.9	12	16.8	20.6	15.7	17.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	7.5	6.8	6.4
VIII	–	–	–	–	–	10.6	–	–	6.4	16,18,31	14.6	19.3	14.0	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.1	4.1	5.4
IX	–	–	–	–	–	8.8	–	–	4.4	22	12.8	20.0	13.0	14.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	2.9	–	–	–3.6	22	4.9	11.3	6.2	7.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.9	4.0	5.1
XI	–	–	–	–	–	–3.5	–	–	–17.9	18	–1.5	1.1	–1.1	–0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.9	8.0	8.4
XII	–	–	–	–	–	–2.5	–	–	–21.3	17	–0.3	1.5	–0.2	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	7.3	8.0
Rok	–	–	–	–	–	2.3	–	–	–25.4	7, 11	5.5	9.8	5.7	6.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lądek-Zdrój — φ = 50°21' — λ = 16°53'

I	–	–	–	–	2.1	–3.5	7.6	1	–12.7	5, 7	–1.8	0.3	–0.8	–0.8	4.8	5.1	5.1	5.0	89	81	88	86	0.6	1.2	0.7	0.8	9.7	8.3	9.0	9.0
II	–	–	–	–	–2.3	–10.0	2.5	14	–21.3	6	–7.3	–3.8	–6.1	–5.8	3.3	3.6	3.6	3.5	90	77	88	85	0.4	1.1	0.5	0.7	8.4	8.5	8.1	8.3
III	–	–	–	–	5.0	–3.6	14.9	30	–17.6	9	–2.0	3.2	0.3	0.4	5.0	5.4	5.6	5.3	90	68	86	81	0.6	2.7	0.9	1.4	7.9	7.1	7.0	7.3
IV	–	–	–	–	9.4	1.2	16.1	6	–4.4	2	2.7	8.2	4.6	5.0	6.9	7.1	7.4	7.1	93	68	87	83	0.5	4.0	1.2	1.9	7.9	8.0	8.6	8.2
V	–	–	–	–	13.3	4.9	20.8	17	–3.2	3	7.9	12.1	8.5	9.2	9.2	9.3	9.6	9.4	84	66	85	78	1.6	5.1	1.7	2.8	8.2	8.1	8.1	8.1
VI	–	–	–	–	19.2	9.2	30.8	26	2.6	3	12.8	17.5	13.3	14.2	13.1	12.7	13.1	13.0	87	65	85	79	2.0	8.2	2.6	4.3	7.0	8.2	6.9	7.4
VII	–	–	–	–	19.2	10.9	28.4	14	4.0	6	13.8	17.7	14.0	14.9	13.4	13.6	13.7	13.6	84	67	85	79	2.7	7.3	2.6	4.2	8.9	8.2	7.9	8.3
VIII	–	–	–	–	19.6	9.4	28.5	6	3.7	16	11.7	17.8	13.0	13.9	11.9	12.2	12.8	12.3	87	60	85	77	2.3	9.0	2.7	4.7	6.5	7.7	6.2	6.8
IX	–	–	–	–	18.0	9.4	24.2	2	3.7	22	11.4	16.7	12.3	13.2	11.4	11.9	12.2	11.8	84	64	85	78	2.5	7.5	2.5	4.2	7.3	6.5	4.2	6.0
X	–	–	–	–	12.9	2.1	22.3	2	–5.9	22	3.5	12.0	5.7	6.7	7.5	9.0	8.3	8.3	92	62	89	81	0.7	5.5	1.2	2.5	6.0	5.2	5.2	5.5
XI	–	–	–	–	3.1	–3.6	14.0	1	–14.3	24	–1.6	1.3	–0.8	–0.5	4.8	5.4	5.0	5.1	85	78	83	82	1.0	1.7	1.2	1.3	8.7	8.4	9.2	8.8
XII	–	–	–	–	3.0	–2.0	10.7	20	–12.3	15	0.3	1.6	0.5	0.7	5.2	5.3	5.3	5.3	81	77	82	80	1.2	1.6	1.3	1.4	9.2	9.5	8.8	9.2
Rok	–	–	–	–	10.2	2.0	30.8	26.VI	–21.3	6. II	4.3	8.7	5.4	6.0	8.0	8.4	8.5	8.3	87	69	86	81	1.3	4.6	1.6	2.5	8.0	7.8	7.4	7.7

Bytom — φ = 50°21' — λ = 18°55'

I	–	–	–	–	2.2	–2.5	7.9	29	–10.4	7	–0.9	1.4	0.0	0.1	5.2	5.4	5.3	5.3	89	80	87	85	0.6	1.4	0.8	0.9	8.2	7.8	7.6	7.9
II	–	–	–	–	–2.3	–8.9	3.4	14	–20.7	6	–6.6	–3.5	–5.4	–5.2	3.5	3.8	3.6	3.6	90	79	86	85	0.4	1.0	0.6	0.7	8.5	7.2	6.7	7.5
III	–	–	–	–	6.6	–1.8	17.0	30	–13.1	11	–0.3	5.3	2.3	2.4	5.6	5.8	6.1	5.8	88	64	81	79	0.7	3.6	1.4	1.9	7.7	6.3	5.0	6.3
IV	–	–	–	–	10.7	3.4	15.7	3	–0.9	1	4.8	9.6	6.5	6.8	7.5	7.8	7.9	7.7	86	66	81	78	1.2	4.4	1.9	2.5	6.9	7.4	5.7	6.7
V	–	–	–	–	15.1	6.7	23.4	19	–1.2	3	9.3	13.4	10.5	10.9	10.1	10.4	10.5	10.3	83	67	81	77	1.9	5.5	2.5	3.3	6.8	7.4	6.5	6.9
VI	–	–	–	–	21.4	11.3	32.1	26	5.9	3	14.9	19.3	15.4	16.2	13.6	13.6	14.3	13.8	80	62	81	74	3.6	9.6	3.6	5.6	5.3	6.5	6.0	5.9
VII	–	–	–	–	21.6	12.4	30.7	15	6.2	5	15.7	19.9	15.7	16.8	14.7	15.1	15.1	15.0	82	66	84	77	3.4	9.1	3.1	5.2	6.8	7.5	5.4	6.6
VIII	–	–	–	–	21.0	11.1	31.2	7	6.9	31	13.7	19.7	15.2	16.0	13.7	13.2	14.0	13.6	87	59	81	76	2.4	10.8	3.8	5.7	6.2	6.2	5.2	5.9
IX	–	–	–	–	21.1	10.1	28.2	3	4.7	22	12.3	19.4	14.6	15.2	12.9	13.1	13.6	13.2	89	60	82	77	1.8	10.0	3.4	5.1	5.7	5.4	4.3	5.1
X	–	–	–	–	13.4	4.0	23.1	2	–4.9	23	5.4	12.5	7.3	8.1	8.4	8.9	9.1	8.8	90	60	85	78	0.9	6.1	1.6	2.9	6.5	4.4	3.6	4.8
XI	–	–	–	–	3.6	–2.8	13.0	2	–13.3	18	–0.7	2.2	0.2	0.5	5.2	5.5	5.6	5.4	85	75	85	82	1.0	2.1	1.0	1.4	8.6	7.9	7.5	8.0
XII	–	–	–	–	3.6	–1.0	10.0	20	–7.8	15	1.0	2.5	1.3	1.5	5.6	5.7	5.7	5.7	84	77	83	81	1.1	1.8	1.2	1.4	7.8	8.0	7.1	7.6
Rok	–	–	–	–	11.5	3.5	32.1	26.VI	–20.7	6. II	5.7	10.1	7.0	7.4	8.8	9.0	9.2	9.0	86	68	83	79	1.6	5.4	2.1	3.0	7.1	6.8	5.9	6.6

Chorzelów — φ = 50°21' — λ = 21°27'

I	–	–	–	–	0.7	–5.5	5.1	30	–14.9	12	–2.9	0.1	–2.4	–1.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–2.6	–11.7	3.8	14	–27.8	7	–8.2	–4.5	–7.3	–6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	5.4	–4.3	16.7	30	–22.7	1	–2.4	4.2	0.8	0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	11.3	2.2	17.2	7	–3.2	6	4.0	9.5	6.1	6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.0	6.0	27.4	19	–3.6	4	8.9	14.4	10.4	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	22.0	11.2	31.6	26	5.5	3	14.6	20.4	15.9	16.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.4	12.0	29.5	17	6.9	6, 11	15.2	20.8	16.0	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.0	10.9	30.6	8	6.6	17	13.2	19.4	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.5	9.5	26.8	2	3.9	24	11.7	19.8	13.8	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.6	1.9	22.4	1	–5.5	22	3.7	11.6	6.7	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	2.7	–3.5	15.1	2	–16.6	18	–1.5	1.3	–0.5	–0.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.8	–2.3	7.2	10	–14.9	17	–0.4	1.9	0.3	0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.3	2.2	31.6	26.VI	–27.8	7. II	4.7	9.9	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Tarnogród — $H_s = 217\ m$ — $h_w = 15{,}9\ m$ — 1965

MIESIĄC	ROZKŁAD WIATRU (%D, V m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10	Max<0	Min<0	Max≥30	Wiatr V ≥10	≥15	◐	◕	Opad R ≥0,1	≥1,0	≥10,0	≡	⊠	K
I	5	2.6	1	2.0	5	1.6	13	1.5	15	2.3	16	2.7	11	2.6	4	3.8	24	1.8	42	14.8	20	4	—	25	—	·	·	2	24	10	6	2	—	31	—
II	14	1.6	7	1.9	4	1.5	·	·	5	2.8	16	3.2	15	1.9	12	2.2	11	1.9	30	9.8	10	12	—	28	—	·	·	2	16	14	9	·	—	28	—
III	4	2.5	5	1.6	4	1.5	8	1.9	20	1.4	17	2.0	7	2.0	7	2.3	21	1.4	25	7.6	17	3	—	24	—	·	·	6	13	8	7	·	—	15	—
IV	7	1.4	8	3.2	13	2.2	16	2.4	12	1.9	9	2.6	6	1.7	10	2.1	9	2.0	31	7.2	22	·	—	9	—	·	·	2	14	10	7	·	—	·	—
V	12	2.4	3	1.0	10	2.0	9	1.4	4	2.2	7	1.6	19	2.2	10	2.2	19	1.6	51	7.4	18	·	—	2	—	·	·	—	—	13	12	·	—	·	—
VI	4	1.8	4	1.2	5	2.2	7	1.1	7	1.6	5	2.4	22	1.7	16	1.8	20	1.3	67	13.6	28	·	—	·	—	·	·	8	11	11	8	2	—	·	—
VII	4	1.0	1	1.0	3	2.0	9	1.4	11	1.7	13	1.9	20	1.8	3	3.3	29	1.2	133	34.4	18	·	—	·	—	·	·	3	11	15	14	3	—	·	—
VIII	9	1.8	1	2.0	·	·	5	1.6	7	1.6	10	2.0	22	1.8	13	1.7	26	1.3	123	37.8	26	·	—	·	—	·	·	8	11	13	10	4	—	·	—
IX	1	1.0	·	·	1	1.0	11	1.5	22	1.7	11	2.2	5	1.2	9	1.9	30	1.1	40	16.4	11	·	—	·	—	·	·	—	—	8	7	2	—	·	—
X	6	2.0	3	1.7	4	1.0	1	1.0	7	1.4	13	1.6	23	1.4	8	2.6	28	1.1	6	3.1	31	·	—	7	—	·	·	9	7	10	2	·	—	·	—
XI	6	1.5	5	2.4	6	1.7	9	1.4	9	2.3	12	2.5	14	1.9	6	2.3	23	1.5	66	15.2	21	3	—	22	—	·	·	1	21	14	11	1	—	11	—
XII	2	1.5	3	1.7	·	·	8	1.2	23	2.4	33	2.5	6	1.7	5	2.0	13	1.9	50	13.6	18	2	—	23	—	1	·	1	21	18	10	1	—	7	—
Rok	74	1.8	41	1.6	55	1.4	96	1.4	142	1.9	161	2.3	170	1.8	103	2.4	253	1.5	664	37.8	26.VIII	24	—	140	—	1	·	—	—	144	103	15	—	92	—

Lądek-Zdrój — $H_s = 460\ m$ — $h_w = 11{,}2\ m$

I	8	1.3	7	1.2	1	1.0	9.5	2.7	24	2.9	25.5	2.6	2.5	2.0	1.5	1.0	14	2.0	59	12.0	9	3	5	28	·	1	·	·	22	17	12	2	·	31	·
II	11.5	1.2	15	1.1	1	1.0	0.5	1.0	3.5	2.7	22.5	2.5	6	3.2	5	2.8	19	1.5	62	10.7	17	10	24	28	·	1	·	1	20	22	17	1	·	28	·
III	5	1.6	9.5	1.7	1.5	1.3	1	1.0	15.5	2.5	31.5	2.1	5.5	2.6	3.5	1.6	20	1.6	43	10.2	28	3	6	21	·	·	·	4	18	13	10	1	·	20	·
IV	4	1.8	23	1.4	3.5	1.6	5	1.1	7.5	1.9	13.5	1.6	5	2.3	3.5	1.3	25	1.1	94	17.8	22	·	·	9	·	·	·	2	21	19	16	5	2	1	·
V	10.5	1.5	23	1.3	1.5	1.3	0.5	1.0	8.5	2.1	12.5	1.8	6	2.7	5.5	1.8	25	1.2	242	80.1	29	·	·	4	·	·	·	2	21	22	18	9	1	·	5
VI	4	1.6	17.5	1.0	3.5	1.0	2	2.0	5.5	3.0	19	2.3	7	1.5	4.5	1.6	27	1.2	129	22.4	9	·	·	·	4	1	1	1	13	19	14	4	3	·	7
VII	0.5	1.0	5.5	1.0	2	1.0	1	1.0	13	2.5	28	2.5	8	1.8	4	1.0	31	1.4	84	17.8	18	·	·	·	2	1	·	·	19	22	13	2	·	·	6
VIII	6	1.7	13.5	1.1	0.5	3.0	5.5	2.7	9.5	2.2	13	1.8	2.5	1.4	4.5	1.2	38	1.0	75	26.1	25	·	·	·	5	1	·	2	11	12	9	2	1	·	2
IX	2	1.2	2.5	1.2	4.5	1.9	10	2.6	25	2.3	21	2.1	4	1.9	2	1.0	19	1.7	84	35.6	10	·	·	·	·	1	1	5	8	9	7	2	·	·	3
X	8.5	1.3	16.5	1.2	·	·	2	2.8	11.5	2.1	9.5	2.1	6.5	2.5	2.5	1.2	36	1.1	10	6.8	16	·	·	10	·	·	·	7	10	5	3	·	·	·	·
XI	6.5	1.8	13.5	2.0	·	·	4.5	2.7	17	3.4	23.5	3.9	3	3.8	1	1.5	21	2.4	55	23.8	11	3	9	24	·	5	·	1	23	19	14	1	3	18	·
XII	3.5	1.0	4.5	1.2	·	·	3.5	3.1	24.5	3.5	39	3.7	4	4.4	2	1.5	12	2.9	35	9.9	13	2	3	23	·	7	·	·	24	14	6	·	·	20	·
Rok	70	1.4	151	1.3	19	1.1	45	2.0	165	2.6	258.5	2.4	60	2.5	39.5	1.5	287	1.6	972	80.1	29.V	21	47	147	11	18	2	25	210	193	139	29	10^2	118	23

Bytom — $H_s = 300\ m$ — $h_w = 16{,}3\ m$

I	5	2.2	1	1.0	3	1.7	7	1.6	13.5	2.1	28	2.1	8	1.8	8.5	2.6	19	1.6	61	12.5	31	1	4	25	·	—	—	·	16	14	12	2	—	31	·
II	13.5	3.2	4	3.8	1	3.0	5	2.6	4.5	2.3	16.5	3.8	18	2.9	13.5	3.3	8	2.9	36	6.5	7	8	22	28	·	—	—	·	14	20	12	·	—	28	·
III	6	2.5	6	3.0	4	3.0	8	2.3	13	2.4	17.5	2.9	8.5	3.0	8	4.1	22	2.2	50	11.5	21	2	5	18	·	—	—	·	8	18	8	2	—	17	·
IV	8	3.1	7.5	4.1	15	3.2	6.5	2.8	4	2.2	7	3.0	10	3.1	11	2.8	21	2.4	61	10.6	25	·	·	3	·	—	—	5	13	17	15	1	—	·	3
V	14	3.3	10.5	3.1	12.5	3.5	2	1.0	3	2.8	8	2.3	8	2.5	10	3.8	25	2.3	149	27.7	29	·	·	2	·	—	—	3	15	21	20	3	—	·	5
VI	6.5	2.4	10.5	2.8	6	4.0	3	2.0	·	·	18	3.5	10	3.2	11	3.9	25	2.4	106	20.6	11	·	·	·	6	—	—	2	7	14	13	5	—	·	6
VII	1.5	2.7	3.5	3.4	14	2.6	7	2.3	6.5	3.5	29	3.9	4.5	2.4	2	2.5	25	2.4	97	23.4	17	·	·	·	5	—	—	·	9	20	13	4	—	·	4
VIII	12.5	2.8	1	3.0	·	·	10.5	3.3	3.5	1.9	9	2.7	5.5	2.8	9	3.4	42	1.6	55	15.5	24	·	·	·	8	—	—	4	7	15	10	3	—	·	2
IX	·	·	·	·	10.5	3.4	20	3.1	8	2.9	8.5	3.8	4	2.9	7	3.4	32	2.1	69	18.2	4	·	·	·	2	—	—	4	6	11	10	3	—	·	·
X	2	3.0	8.5	2.9	14.5	2.8	1	2.0	4.5	3.0	16	3.5	16.5	3.0	3	2.3	27	2.1	4	2.3	29	·	·	5	·	—	—	8	6	2	2	·	—	·	·
XI	1.5	2.7	9.5	2.3	11	2.8	4	2.0	11	3.0	16	3.0	9.5	2.7	3.5	2.4	24	2.0	38	7.0	21	3	8	22	·	—	—	·	19	18	11	·	—	17	·
XII	1	2.0	1	5.0	5	2.2	4.5	1.4	30	2.9	23.5	3.4	11.5	2.9	7.5	1.9	9	2.6	58	13.5	18	·	·	18	·	—	—	1	14	18	10	1	—	9	·
Rok	71.5	2.5	63	2.9	96.5	2.7	78.5	2.2	101.5	2.4	197	3.2	114	2.8	94	3.0	279	2.2	784	27.7	29.V	14	39	121	21	—	—	27	134	188	136	24	—	102	20

Chorzelów — $H_s = 170\ m$ — $h_w = 16\ m$

I	4	5.4	10	2.2	7	3.1	12.5	2.2	25	3.4	7.5	2.7	11	4.0	6	3.2	10	2.8	73	15.1	9	8	12	27	·	·	·	—	—	17	13	2	5	31	·
II	10.5	5.0	12	4.4	0.5	5.0	1	5.0	12	4.4	10.5	3.0	23	4.0	10.5	3.3	4	3.9	35	5.4	17	16	24	28	·	1	·	—	—	20	11	·	3	28	·
III	7	3.8	9.5	3.5	1.5	6.0	7	2.9	21.5	2.9	12	2.2	10.5	2.9	6	3.8	18	2.5	44	7.0	21	6	5	21	·	1	·	—	—	17	9	·	7	18	·
IV	7	4.3	10.5	2.6	24	4.8	11.5	2.8	4.5	2.1	8	3.3	8	2.7	8.5	3.4	8	3.2	41	8.3	26	·	·	8	·	1	·	—	—	14	9	·	1	·	3
V	10.5	3.4	11	2.1	11.5	3.2	10.5	1.6	6	2.3	12	3.1	8.5	2.8	11	3.4	12	2.4	65	21.7	29	·	·	3	2	1	·	—	—	19	13	1	2	·	7
VI	5	4.7	6	3.3	9	2.7	4.5	1.7	9.5	3.2	5.5	2.2	22	3.2	16.5	2.8	12	2.6	82	14.0	28	·	·	·	6	1	·	—	—	13	13	4	1	·	6
VII	4	1.8	2	2.2	8	2.1	3	3.0	12.5	2.2	24.5	2.1	17	2.4	5	1.8	17	1.8	63	10.0	8	·	·	·	10	·	·	—	—	18	13	1	·	·	8
VIII	10	2.6	8	3.6	2.5	1.2	10.5	2.4	11.5	2.4	7	2.5	8.5	2.5	18	3.5	17	2.3	188	43.3	26	·	·	·	7	1	·	—	—	16	14	7	2	·	4
IX	0.5	1.0	1	2.0	1	1.5	16	2.7	25	2.8	11.5	1.8	10.5	2.2	3.5	2.6	21	1.9	55	20.5	11	·	·	·	7	1	·	—	—	9	8	2	5	·	1
X	11.5	2.4	3.5	2.3	4.5	2.0	3.5	1.4	10.5	1.9	8.5	1.8	15	3.2	5	2.3	31	1.5	4	1.5	31	·	·	13	·	·	·	—	—	7	2	·	6	·	·
XI	1.5	2.7	9.5	4.1	5.5	3.8	8	2.8	14	4.1	12.5	3.7	16.5	3.1	4.5	2.9	19	2.8	46	12.9	11	4	10	20	·	1	·	—	—	21	10	1	4	10	1
XII	5	2.7	4.5	1.9	1.5	2.3	5.5	1.4	36.5	3.5	19.5	2.6	8.5	2.2	4	3.9	8	2.7	49	13.4	18	2	4	22	·	1	·	—	—	17	12	1	1	7	·
Rok	76.5	3.3	87.5	2.8	76.5	3.1	93.5	2.6	188.5	2.9	139	2.6	158	2.9	96.5	3.1	177	2.5	745	43.3	26.VIII	36	55	142	32	9	·	—	—	188	127	19	37	94	30

Prudnik φ = 50°19' λ = 17°34' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	3.4	−3.1	7.7	12	−13.6	7, 8	−0.6	2.0	0.1	0.4	5.2	5.5	5.4	5.4	87	78	86	84	0.8	1.7	0.9	1.1	6.9	6.0	6.8	6.5
II	–	–	–	–	−1.4	−10.2	4.3	13	−20.6	6	−5.9	−3.1	−6.0	−5.2	3.4	3.8	3.4	3.5	84	79	84	82	0.7	1.1	0.7	0.8	7.6	7.2	6.3	7.0
III	–	–	–	–	6.2	−4.1	18.1	30	−19.9	9	−1.3	5.0	0.7	1.3	5.3	5.8	5.6	5.6	86	64	81	77	0.9	3.5	1.3	1.9	5.7	5.5	4.0	5.1
IV	–	–	–	–	10.8	2.6	17.1	4	−1.2	1	4.8	9.5	5.9	6.5	7.5	7.3	7.9	7.6	86	64	84	78	1.2	4.8	1.5	2.5	7.5	7.1	5.9	6.9
V	–	–	–	–	14.7	6.4	24.3	17	−1.2	3	9.5	13.5	9.9	10.7	10.1	10.4	10.6	10.4	83	67	86	79	2.0	5.5	1.8	3.1	6.8	7.3	7.7	7.1
VI	–	–	–	–	20.6	10.5	31.2	26	4.8	3	15.0	19.1	14.7	15.9	14.2	14.1	14.4	14.2	82	65	85	77	3.3	9.0	2.7	5.0	4.8	5.8	5.4	5.3
VII	–	–	–	–	21.1	11.8	29.6	14	4.0	5	15.3	19.2	15.2	16.2	14.7	15.3	14.6	14.9	84	69	84	79	2.9	7.7	3.1	4.6	6.8	8.0	5.8	6.9
VIII	–	–	–	–	21.0	10.4	31.0	7	4.8	16	13.7	19.7	14.5	15.6	13.5	13.8	14.3	13.9	87	61	86	78	2.6	10.3	2.7	5.2	4.5	4.9	5.4	4.9
IX	–	–	–	–	20.5	9.1	27.1	2	3.4	22	11.9	19.2	13.5	14.5	12.3	13.4	13.3	13.0	88	61	85	78	2.0	9.4	2.7	4.7	4.0	4.0	2.9	3.6
X	–	–	–	–	13.8	1.7	23.1	2	−6.9	22	3.5	13.0	5.4	6.8	7.9	9.9	8.8	8.9	95	65	94	85	0.4	5.7	0.7	2.3	4.0	3.8	3.3	3.7
XI	–	–	–	–	4.1	−3.0	15.7	1	−12.8	15	−1.0	2.6	0.2	0.5	5.3	6.1	5.7	5.7	89	81	89	86	0.8	1.8	0.9	1.2	8.3	6.4	7.1	7.3
XII	–	–	–	–	4.3	−1.8	12.7	19	−13.9	15	0.7	2.8	1.4	1.6	5.6	5.7	5.6	5.6	86	76	81	81	1.0	1.9	1.4	1.4	7.3	6.8	4.5	6.2
Rok	–	–	–	–	11.6	2.5	31.2	26. VI	−20.6	6. II	5.5	10.2	6.3	7.1	8.8	9.3	9.1	9.1	86	69	85	80	1.6	5.2	1.7	2.8	6.2	6.1	5.4	5.9

Sielec φ = 50°19' λ = 20°25'

I	–	–	–	–	0.8	−6.4	5.2	1	−15.9	12	−3.4	−0.4	−2.9	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−2.4	−11.0	3.2	14	−24.4	7	−7.1	−3.6	−7.1	−6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	5.2	−4.6	17.1	30	−21.6	1	−1.1	3.9	−0.6	0.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	11.2	2.1	17.0	7	−2.3	16	4.4	10.2	5.1	6.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.8	5.3	27.9	19	−3.7	3, 4	9.3	14.4	9.7	10.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	21.8	10.1	31.0	26	4.8	3	14.7	20.5	14.6	16.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.2	10.8	29.6	17	5.7	4, 10, 12	15.5	20.5	14.7	16.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.2	9.6	31.7	7	4.3	31	12.9	20.0	13.1	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.2	7.7	27.3	3	2.7	22	10.9	19.9	12.2	13.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.8	1.1	21.1	1	−6.1	22	3.5	12.1	5.3	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	2.4	−4.5	14.9	2	−20.4	18	−2.0	1.1	−1.2	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	3.4	−2.7	9.7	20	−13.9	17	−0.6	2.1	0.3	0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.3	1.5	31.7	7. VIII	−24.4	7. II	4.8	10.1	5.3	6.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Bystrzyca Kłodzka φ = 50°18' λ = 16°39'

I	–	–	–	–	1.7	−3.2	4.8	30	−13.5	5, 7	−1.8	0.4	−0.5	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.7	9.1	8.5
II	–	–	–	–	−1.7	−9.3	2.9	11, 14	−18.9	28	−6.5	−3.1	−5.2	−5.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.9	8.1	8.3
III	–	–	–	–	5.4	−3.1	15.5	30	−20.6	9	−1.4	3.8	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.9	7.0	6.4
IV	–	–	–	–	10.8	2.2	17.5	6	−3.7	2	4.0	9.4	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.1	7.3	7.1
V	–	–	–	–	14.5	5.6	23.4	17	−2.1	4	8.0	12.8	9.4	10.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.4	7.5	7.3
VI	–	–	–	–	20.2	9.6	32.3	26	1.8	3	13.8	18.7	14.0	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.4	5.7	5.9
VII	–	–	–	–	20.7	11.8	30.3	15	4.6	5	15.1	19.1	14.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	6.1	6.8
VIII	–	–	–	–	20.6	9.5	28.8	7	3.0	16	13.5	19.1	13.4	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.0	5.7	5.7
IX	–	–	–	–	19.0	9.6	25.3	3	2.4	22	12.1	17.8	12.7	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.9	4.0	4.9
X	–	–	–	–	13.4	1.9	22.3	2	−6.7	22	3.8	12.5	6.1	7.1	–	–	–	–	–	–	–	–	–	–	–	–	5.8	3.0	3.5	4.1
XI	–	–	–	–	3.2	−2.8	14.2	1	−12.2	24	−1.3	1.7	−0.4	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.5	7.7	6.0
XII	–	–	–	–	3.2	−2.1	10.4	19	−14.7	15	0.4	1.6	0.6	0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.9	7.5	8.2
Rok	–	–	–	–	10.9	2.5	32.3	26. VI	−20.6	9. III	5.0	9.5	5.9	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	6.6	6.8

Głuchołazy φ = 50°18' λ = 17°23'

I	–	–	–	–	3.2	−2.5	7.1	17	(−11.9)	7	−0.5	1.6	−0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	7.4	7.4
II	–	–	–	–	−1.8	−8.0	4.7	14	−18.4	6	−5.3	−3.1	−5.1	−4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	5.1	7.1
III	–	–	–	–	5.7	−2.6	16.2	30	(−18.8)	9	−0.3	4.6	1.2	1.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.7	5.5	5.9
IV	–	–	–	–	10.4	2.9	16.6	4	−0.5	2	5.2	9.1	5.6	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	6.6	7.2
V	–	–	–	–	13.8	6.3	23.5	17	−1.1	2	9.7	12.9	9.1	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	7.5	7.4
VI	–	–	–	–	20.3	11.0	30.7	26	5.8	3	15.4	19.0	14.0	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.6	5.2	5.4
VII	–	–	–	–	21.1	12.1	31.0	14	5.7	5	15.6	19.2	14.3	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.8	5.5	6.5
VIII	–	–	–	–	20.5	10.9	30.1	7	5.6	16	14.2	19.0	13.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.6	4.9	5.2
IX	–	–	–	–	19.9	9.8	26.9	3	5.6	22	12.9	18.7	12.9	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.5	3.0	4.0
X	–	–	–	–	12.9	3.4	23.5	2	−5.3	22	5.3	12.2	6.1	7.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.0	3.8	4.2
XI	–	–	–	–	4.0	−2.3	14.1	2	−10.1	24	−0.3	2.7	0.2	0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	6.9	7.0	7.5
XII	–	–	–	–	4.3	−1.5	11.9	19	−9.3	15	0.9	2.7	1.8	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.3	6.2	7.2
Rok	–	–	–	–	11.2	3.3	31.0	14. VII	(−18.8)	9. III	6.1	9.9	6.1	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.3	5.6	6.2

Prudnik $H_s = 265$ m $h_w = 14$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	3.0	·	·	·	·	13	1.4	15.5	2.2	10	2.4	9.5	4.3	14	2.5	29	1.7	39	9.1	3	2	2	28	·	·	·	2	12	15	10	·	—	31	·
II	6	2.7	3	1.7	·	·	2	1.0	·	·	6	5.0	24.5	4.1	18.5	4.6	24	2.8	35	9.3	17	13	20	26	·	·	·	2	12	15	12	·	—	28	·
III	2.5	2.6	0.5	1.0	3	2.3	9	2.3	10	2.4	2	2.0	27.5	3.6	9.5	2.5	29	2.0	29	10.3	6	8	5	19	·	·	·	7	3	10	7	1	—	18	·
IV	1	1.0	12	2.2	5	3.0	9	2.1	5.5	2.8	4.5	3.2	19	2.9	12	2.9	22	2.0	87	21.1	20	·	·	3	·	·	·	5	15	16	10	3	—	·	2
V	9	1.7	13	2.5	2	2.0	4	1.5	6.5	4.2	9.5	2.3	23.5	4.1	17.5	2.8	8	2.7	156	17.2	28	·	·	2	·	2	2	1	15	21	16	8	—	·	6
VI	8	2.4	7	2.4	4	3.0	7	2.3	8	2.9	3	2.0	29	2.9	14	3.4	10	2.5	100	23.6	11	·	·	·	7	1	·	8	10	17	14	3	—	·	5
VII	2	1.0	6	1.7	4	2.0	7	1.3	11	1.6	26	2.7	23	1.7	12	1.6	2	1.9	83	24.7	20	·	·	·	4	·	·	1	8	17	13	2	—	·	5
VIII	1	1.0	6	1.0	2	1.5	11	2.6	6	4.8	6	4.0	34	1.9	22	2.0	5	2.1	44	15.3	25	·	·	·	8	·	·	7	4	8	7	1	—	·	1
IX	3	1.7	4	1.5	2	2.0	15	2.5	20	4.6	11	2.5	20	2.3	10	2.6	5	2.7	38	18.1	28	·	·	·	2	2	·	13	3	8	6	1	—	·	2
X	7	1.7	1	1.0	7	1.9	6	2.2	·	·	6	2.7	17	2.2	12	1.5	37	1.2	3	1.4	16	·	·	12	·	·	·	15	4	5	1	·	—	·	·
XI	3	3.0	8	2.8	5	2.2	6	2.0	10	7.7	13	2.8	11	4.9	9	1.7	25	2.6	28	11.0	11	2	8	23	·	5	1	4	16	15	5	1	—	16	·
XII	·	·	1	3.0	4	2.0	3	1.7	14.5	6.6	20.5	4.1	26	3.6	7	2.1	17	3.3	36	9.4	13	2	1	19	·	7	1	3	9	14	6	·	—	15	·
Rok	44.5	1.8	61.5	1.7	38	1.8	92	1.9	107	3.3	117.5	3.0	264	3.2	157.5	2.5	213	2.3	678	24.7	20.VII	27	36	132	21	17	4	68	111	161	107	20	—	108	21

Sielec $H_s = 202$ m $h_w = 16,7$ m

I	3.5	5.3	7	3.9	18.5	2.9	·	·	1.5	5.3	4.5	3.8	11.5	6.2	0.5	3.0	46	2.1	67	9.7	30	8	11	28	·	2	1	—	—	16	13	·	10	28	·
II	5.5	1.9	2	3.8	0.5	2.0	·	·	0.5	4.0	13	4.7	24	5.1	17.5	4.0	21	3.3	29	5.2	16	14	23	28	·	2	·	—	—	13	8	·	7	28	·
III	5.5	3.5	9	2.8	6	3.9	6	2.7	1	2.5	6	4.5	8	5.9	5.5	1.3	46	1.8	42	9.6	26	6	4	24	·	2	·	—	—	10	7	·	8	17	·
IV	4.5	3.2	10	4.0	26.5	5.3	·	·	2	3.0	8	4.2	10.5	4.1	3.5	2.4	25	3.2	45	13.4	12	·	·	8	·	4	·	—	—	13	10	1	4	·	·
V	6	1.3	1.5	2.3	17.5	3.9	1	2.0	2	5.0	11	4.1	16.5	2.7	10.5	3.0	27	2.3	113	14.3	29	·	·	4	1	3	$2^{?}$	—	—	19	17	4	4	·	2
VI	1	1.0	4.5	2.8	17.5	3.7	2	4.0	1	3.0	7.5	4.2	20	3.5	6.5	2.2	30	2.3	107	20.5	27	·	·	·	8	·	·	—	—	13	12	4	·	·	2
VII	·	·	5	2.6	5	3.0	3	4.0	7	2.1	13	4.3	13.5	4.3	1.5	3.0	45	1.9	59	19.3	18	·	·	·	9	1	$1^{?}$	—	—	15	11	1	1	·	5
VIII	5.5	3.1	·	·	5.5	2.9	3.5	3.4	0.5	3.0	7	3.4	11.5	3.0	6.5	2.6	53	1.3	134	32.5	25	·	·	·	7	·	·	—	—	12	10	6	·	·	2
IX	·	·	4	2.8	12	3.7	4.5	2.3	5	2.3	6.5	3.8	10.5	2.9	1.5	2.3	46	1.5	85	26.4	29	·	·	·	4	·	·	—	—	10	8	3	6	·	·
X	6	2.2	2	1.8	6.5	2.5	1.5	1.0	·	·	6	3.6	15	4.2	4	2.6	52	1.4	8	5.3	11	·	·	17	·	1	·	—	—	5	2	·	13	·	·
XI	2.5	1.4	10	3.8	11.5	4.4	6.5	2.9	0.5	6.0	7	5.5	12.5	5.0	3.5	2.1	36	2.5	40	10.3	11	6	10	24	·	3	1	—	—	19	7	1	7	15	·
XII	0.5	1.0	3.5	1.1	6	2.2	7.5	2.3	4.5	2.6	16	5.4	16	4.9	5	2.9	34	2.4	35	8.9	4	1	2	24	·	1	·	—	—	13	9	·	2	8	·
Rok	40.5	2.0	58.5	2.6	133	3.4	35.5	2.0	25.5	3.2	105.5	4.3	169.5	4.3	66	2.6	461	2.2	764	32.5	25.VIII	35	50	157	29	19	$5^{?}$	—	—	158	114	20	62	96	11

Bystrzyca Kłodzka $H_s = 370$ m $h_w = 12,3$ m

I	14	3.8	·	·	·	·	3.5	4.0	40	3.7	7.5	4.9	3	5.7	3	3.2	22	3.0	49	12.8	17	4	6	27	·	1	·	·	23	19	11	1	1	30	·
II	21	4.7	2	2.8	·	·	3.5	4.3	12.5	5.0	5	9.4	2	5.0	7	3.4	31	3.1	34	5.3	13	9	23	27	·	2	1	·	17	23	15	·	1	28	·
III	14.5	3.5	1.5	4.0	·	·	4.5	3.6	29.5	3.8	5	3.9	2	5.5	3	2.5	33	2.4	31	5.1	2	3	5	18	·	·	·	4	12	13	9	·	3	17	·
IV	18	2.9	1	3.0	0.5	2.0	3.5	3.4	15	3.5	4	2.5	7	4.0	8	2.6	33	2.0	80	15.3	25	·	·	6	·	·	·	6	15	18	13	1	1	·	·
V	14.5	3.0	7.5	2.7	1	3.0	1.5	2.7	11	3.9	6	3.1	4.5	3.2	16	3.3	31	2.2	165	49.3	29	·	·	3	·	·	·	3	16	25	18	4	1	·	4
VI	11	4.5	0.5	5.0	·	·	1	2.0	24.5	4.0	5.5	3.5	6	3.4	9.5	3.1	32	2.5	121	24.3	9	·	·	·	7	·	·	5	9	15	12	5	1	·	6
VII	6.5	3.2	0.5	2.0	·	·	2	3.8	29	3.5	11.5	3.6	7.5	4.1	4	3.2	32	2.3	97	28.3	17	·	·	·	3	·	·	·	11	22	15	2	·	·	7
VIII	10.5	2.4	0.5	2.0	0.5	2.0	1.5	4.3	20	4.8	1.5	3.7	3.5	3.1	7	2.6	48	1.8	87	27.0	24	·	·	·	7	1	·	3	8	12	7	4	2	·	1
IX	3	1.8	·	·	·	·	4	6.0	47.5	4.6	1.5	6.0	2	2.5	1	2.5	31	2.9	54	29.4	28	·	·	·	1	·	·	6	6	11	7	2	1	·	3
X	16	2.5	4.5	3.2	·	·	2.5	4.8	14	4.0	3.5	3.1	1	2.0	13.5	2.8	38	1.9	7	2.6	16	·	·	10	·	·	·	7	4	5	2	·	7	·	·
XI	16	2.8	2	2.5	·	·	2.5	3.2	30	4.6	6	5.6	0.5	14.0	·	·	33	2.6	45	9.7	27	3	9	22	·	2	·	2	19	21	11	·	4	8	·
XII	2.5	2.8	·	·	·	·	5.5	4.0	41	4.5	13.5	5.8	5	5.2	1.5	3.3	24	3.5	69	22.4	5	3	2	21	·	1	·	1	20	19	12	1	·	20	·
Rok	147.5	3.2	20	2.3	2	0.6	35.5	3.8	314	4.2	70.5	4.6	44	4.8	73.5	2.7	388	2.5	839	49.3	29.V	22	45	134	18	7	1	37	160	203	132	20	22	103	21

Głuchołazy $H_s = 344$ m $h_w = 12,7$ m

I	4.5	1.4	0.5	2.0	1.5	2.0	6.5	1.8	12.5	1.8	19.5	2.1	8	1.7	18	1.4	22	1.3	47	8.2	3	2	2	27	·	·	·	·	14	12	11	·	2	19	·
II	7	2.1	3.5	1.3	1	1.0	1	1.0	5.5	3.7	6	3.8	19.5	2.6	27.5	2.3	13	2.1	54	12.2	17	6	23	26	·	3	·	2	9	19	13	1	2	28	·
III	7.5	2.7	1	1.5	2	4.0	3.5	2.0	17	2.3	22	1.3	12.5	1.5	20.5	2.0	7	1.8	39	13.0	6	3	7	19	·	1	·	4	9	10	6	1	1	17	·
IV	8	1.8	6.5	1.9	9	1.5	3.5	1.3	10.5	1.4	11	1.1	15.5	1.5	15	1.4	11	1.3	94	20.8	19	·	·	3	·	·	·	3	16	18	14	3	1	·	1
V	7	1.9	9	3.6	5.5	1.7	3.5	2.1	3.5	1.3	16	1.6	13	2.4	22.5	2.1	13	1.8	197	36.5	28	·	·	2	·	1	·	2	17	23	16	9	·	·	7
VI	4	2.4	4	2.0	2	3.0	9	1.7	12.5	2.5	12.5	1.7	14	1.5	21	2.2	11	1.8	133	42.7	11	·	·	·	6	1	·	6	7	16	15	4	·	·	4
VII	2	3.2	2	2.5	1	2.0	1.5	1.3	17	2.8	34.5	2.3	18	1.8	7	2.4	10	2.1	116	35.3	15	·	·	·	4	1	·	1	7	19	12	4	·	·	6
VIII	9	2.5	6	3.2	1	4.0	5	3.7	15	3.0	12.5	1.7	14.5	2.3	18	2.1	12	2.2	68	23.4	25	·	·	·	7	·	·	5	6	12	8	2	1	·	1
IX	4	3.9	2.5	2.8	1	9.0	8.5	4.6	35	3.5	11.5	2.0	12	1.9	12.5	1.8	3	2.9	46	19.2	28	·	·	·	2	2	·	9	2	10	8	1	·	·	1
X	9.5	2.0	9.5	1.9	3.5	3.6	6.5	1.5	16	1.6	8	2.0	7.5	1.6	11.5	2.1	21	1.5	4	2.2	16	·	·	6	·	·	·	12	5	5	2	·	2	·	·
XI	6.5	1.8	8	2.0	3	2.0	4	1.8	11.5	2.6	17.5	3.3	16.5	2.6	11	1.3	12	2.1	35	15.4	11	1	8	21	·	2	1	2	16	15	6	1	2	12	·
XII	·	·	·	·	0.5	4.0	3	3.7	16	4.7	36	2.6	12.5	1.6	4	1.8	21	2.2	29	11.0	21	·	1	16	·	4	2	·	12	12	7	1	2	12	·
Rok	69	2.1	52.5	2.1	31	3.2	55.5	2.2	172	2.6	207	2.1	163.5	1.9	188.5	1.9	156	1.9	862	42.7	11.VI	12	41	120	19	15	3	46	120	171	118	27	13	88	20

Gliwice — φ = 50°18′ — λ = 18°40′ — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.9	−3.2	6.9	29	−10.9	7	−1.5	1.2	−0.8	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.0	6.8	7.6
II	–	–	–	–	−2.0	−9.2	2.8	14	−21.7	6	−6.8	−3.2	−6.0	−5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.1	6.5	7.3
III	–	–	–	–	6.4	−2.1	16.7	30	−14.1	11	−0.9	5.3	1.6	1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.9	5.1	6.0
IV	–	–	–	–	11.1	3.3	15.8	3, 4	−1.5	2	4.5	10.0	6.4	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.1	5.7	6.7
V	–	–	–	–	15.0	6.8	23.0	17	−0.5	3	9.0	13.7	10.3	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	7.2	7.1
VI	–	–	–	–	21.2	11.2	31.7	26	5.8	3	14.4	19.4	15.1	16.0	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.3	5.9	5.7
VII	–	–	–	–	21.7	12.3	30.9	15	6.1	5	15.0	19.9	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.5	5.8	6.8
VIII	–	–	–	–	21.5	10.9	31.0	8	6.8	14, 31	13.2	19.9	14.9	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.9	5.5	5.5
IX	–	–	–	–	21.2	9.9	29.4	3	4.2	22	11.3	19.6	14.0	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.9	4.5	4.8
X	–	–	–	–	13.6	3.4	24.0	2	−6.0	22	4.8	12.9	6.7	7.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	3.8	3.7	4.4
XI	–	–	–	–	3.5	−3.0	13.0	1	−13.0	18	−1.1	2.3	−0.2	0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	7.0	7.6
XII	–	–	–	–	3.3	−1.3	10.0	20	−10.2	15	0.4	2.3	0.9	1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.1	7.6	8.0
Rok	–	–	–	–	11.5	3.2	31.7	26.VI	−21.7	6. II	5.2	10.3	6.5	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.6	5.9	6.4

Mielec — φ = 50°18′ — λ = 21°27′

I	992.2	1007.6	969.3	1013.7	1.1	−5.0	5.7	30	−15.1	12	−2.2	0.2	−2.0	−1.5	4.6	5.0	4.7	4.8	86	80	88	85	0.8	1.3	0.6	0.9	8.2	7.5	7.2	7.6
II	995.1	1009.7	971.8	1017.0	−3.0	−10.8	2.6	12	−27.7	7	−7.8	−4.6	−7.0	−6.6	3.3	3.7	3.3	3.4	90	80	86	85	0.4	0.9	0.5	0.6	9.2	7.5	6.6	7.8
III	996.7	1012.3	968.8	1018.0	6.0	−3.4	16.8	30	−19.7	1	−1.6	4.7	1.3	1.4	5.1	5.9	5.8	5.6	88	67	84	80	0.7	3.1	1.2	1.7	7.0	6.9	5.9	6.6
IV	990.5	1007.9	973.8	1011.3	11.5	2.6	17.1	7	−2.7	6	4.2	9.7	6.1	6.5	7.3	7.5	7.5	7.4	86	63	79	76	1.2	4.9	2.1	2.7	8.1	8.2	6.2	7.5
V	993.3	1009.2	981.5	1013.8	16.3	6.4	25.0	19	−4.3	4	9.2	14.5	10.4	11.1	9.8	9.7	10.7	10.1	82	58	81	74	2.3	7.4	2.3	4.0	6.6	8.0	6.3	7.0
VI	993.9	1002.1	982.2	1014.0	22.2	11.7	32.5	26	6.6	8	15.1	20.5	16.0	16.9	13.8	13.3	14.6	13.9	80	56	80	72	3.6	11.6	3.9	6.4	5.1	6.6	6.6	6.1
VII	992.9	1000.4	983.4	1013.0	22.6	12.4	30.0	16	7.3	6	15.7	20.8	16.6	17.4	14.8	14.0	15.0	14.6	82	58	79	73	3.2	11.4	3.6	6.1	5.7	6.7	6.0	6.1
VIII	995.8	1003.9	981.0	1016.1	21.4	11.1	31.1	8	5.9	17	13.6	19.6	15.4	16.0	13.6	12.9	13.7	13.4	85	58	79	74	2.6	11.0	4.2	5.9	5.5	6.1	5.3	5.6
IX	996.3	1013.8	984.6	1016.6	21.9	10.0	28.3	2	4.6	24	12.6	19.8	14.4	15.3	12.0	13.0	13.2	12.7	83	57	80	73	3.0	10.5	3.5	5.7	5.3	5.7	3.1	4.7
X	1003.1	1016.2	991.8	1024.1	12.8	2.2	22.4	1	−5.6	22	4.2	11.8	7.1	7.6	7.8	8.6	8.5	8.3	90	61	82	78	0.8	5.8	1.9	2.8	6.4	6.4	4.8	5.9
XI	992.1	1010.3	968.7	1013.4	2.8	−5.2	15.0	2	−15.6	18	−1.3	1.6	−0.2	0.0	5.0	5.4	5.3	5.2	85	75	84	81	1.0	2.0	1.1	1.4	8.5	8.1	7.6	8.1
XII	988.1	1003.2	968.8	1009.4	3.0	−1.7	8.0	6	−12.8	17	0.0	2.2	0.5	0.8	5.1	5.3	5.3	5.2	82	72	82	79	1.1	2.0	1.2	1.4	7.8	7.9	7.4	7.7
Rok	994.2	1016.2	968.7	1015.1	11.6	2.7	32.5	26.VI	−27.7	7. II	5.1	10.1	6.6	7.1	8.5	8.7	9.0	8.7	85	65	82	77	1.7	6.0	2.2	3.3	7.0	7.1	6.1	6.7

Spalona — φ = 50°17′ — λ = 16°33′

I	–	–	–	–	−1.3	−4.7	1.4	30	−11.0	7	−3.6	−2.9	−3.0	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.3	9.2	8.9
II	–	–	–	–	−4.6	−10.4	−0.8	12	−17.0	26	−7.8	−6.2	−8.0	−7.5	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.4	7.3	8.2
III	–	–	–	–	1.7	−3.9	11.2	30	−12.9	9	−2.4	−0.1	−1.4	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	6.5	6.8
IV	–	–	–	–	7.0	0.6	12.8	6	−3.1	1	2.6	5.3	3.1	3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	7.6	7.7
V	–	–	–	–	11.2	3.8	18.8	17	−2.0	3	6.4	9.5	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.2	8.5	8.1
VI	–	–	–	–	16.7	8.5	27.7	26	3.9	2	11.4	14.9	11.3	12.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.7	6.9
VII	–	–	–	–	16.6	9.4	25.8	15	4.8	5	11.9	14.8	11.9	12.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	7.1	7.8
VIII	–	–	–	–	16.6	9.1	25.4	7	5.2	16	11.5	14.9	11.7	12.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.0	5.7	5.6
IX	–	–	–	–	15.2	8.2	22.2	3	4.2	20	10.1	13.7	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.7	3.5	5.3
X	–	–	–	–	10.4	2.7	18.4	2	−3.9	22	4.6	9.0	5.0	5.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.0	4.4	4.9
XI	–	–	–	–	0.7	−4.1	10.8	8	−11.6	23	−2.6	−0.9	−2.4	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.2	8.1	8.0
XII	–	–	–	–	0.4	−3.7	7.7	19	−8.4	15	−2.2	−1.4	−1.5	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	8.8	9.1	8.3	8.7
Rok	–	–	–	–	7.6	1.3	27.7	26.VI	−17.0	26. II	3.3	5.9	3.6	4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	6.9	7.2

Olkusz — φ = 50°17′ — λ = 19°34′

I	–	–	–	–	1.5	−4.3	7.9	29	−10.6	8	−2.1	0.8	−1.8	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−3.4	−10.5	1.9	12	−25.5	6	−7.7	−4.4	−7.1	−6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	5.4	−3.8	15.9	30	−14.9	11	0.2	4.6	0.7	1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.0	2.0	15.0	4	−2.3	1	4.8	8.9	4.9	5.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.4	5.7	22.3	19	−3.8	3	9.3	12.9	9.0	10.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	20.5	10.2	31.0	26	5.0	3	15.7	19.2	14.1	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.5	11.7	28.6	14	5.8	5	16.2	19.3	14.8	16.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.1	10.5	30.2	7	6.4	18	14.2	18.8	14.1	15.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.4	9.1	27.6	3	3.0	22	12.8	19.0	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.7	2.8	21.1	1	−4.3	13	5.7	11.8	6.2	7.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	2.9	−4.2	12.9	2	−16.5	18	−1.5	1.4	−1.0	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	2.7	−1.7	9.4	19	−8.9	15	0.1	1.6	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	10.6	2.3	31.0	26.VI	−25.5	6. II	5.6	9.5	5.6	6.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Gliwice $H_s = 220$ m $h_w = 13$ m 1965

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V>15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	9.5	2.2	5.5	2.2	5.5	1.6	14	1.6	11.5	2.4	29.5	4.3	3.5	4.1	11	2.5	3	2.8	60	10.7	31	2	4	27	·	1	·	1	17	15	14	1	2	28	·
II	16	3.9	12	2.1	0.5	4.0	3.5	1.9	4	4.9	11.5	5.0	15.5	4.8	19	4.3	2	3.9	43	7.8	17	9	22	28	·	3	·	·	13	21	15	·	1	28	·
III	12.5	2.3	9.5	2.5	4.5	1.8	14	1.6	14.5	1.8	18.5	3.8	8.5	2.4	10	3.2	1	2.5	45	13.2	21	3	5	18	·	1	·	5	8	16	8	2	2	15	·
IV	16.5	2.4	8	2.9	21	3.4	10	2.2	7	4.6	6	2.9	14	4.0	6.5	3.9	1	3.2	50	8.1	20	·	·	3	·	·	·	5	15	18	12	·	3	·	3
V	24	2.9	6	2.2	12	3.2	7	3.2	4	2.6	13	3.8	10.5	2.4	12.5	3.2	4	2.9	131	18.8	17	·	·	2	·	1	1	2	15	22	19	4	1	·	6
VI	15	2.9	8	2.4	9.5	2.4	6	2.1	8	2.8	11	2.9	11.5	3.1	18	3.7	3	2.8	95	19.0	11	·	·	·	6	·	·	6	10	16	12	3	·	·	5
VII	7	1.9	6	1.8	7	1.3	7	2.3	13.5	2.5	30	3.4	15.5	2.6	5	2.2	2	2.5	80	14.4	8	·	·	·	7	1	·	1	11	17	15	3	2	·	3
VIII	19	2.6	7	1.4	4	1.9	8.5	2.4	8	5.1	11.5	3.0	12	2.1	15	3.1	8	2.5	33	10.2	10	·	·	·	8	·	·	6	10	11	7	1	·	·	2
IX	11.5	2.0	·	·	3	2.7	17.5	3.1	26.5	2.5	17.5	3.1	4	3.5	8	2.7	2	2.7	51	16.0	4	·	·	·	4	·	·	8	5	11	8	2	2	·	1
X	8	2.2	12	2.0	13.5	1.7	3.5	2.7	9.5	3.3	19	3.7	6	1.8	13.5	3.0	8	2.4	2	1.1	16, 29	·	·	7	·	·	·	10	7	2	2	·	6	·	·
XI	7.5	2.5	11	3.2	7	3.2	13.5	2.7	15	2.7	15	5.0	11.5	3.8	7.5	3.3	2	3.3	36	8.8	11	4	8	22	·	·	·	3	18	17	11	·	4	14	·
XII	4	3.0	2.5	2.2	3.5	3.4	7	2.6	16.5	4.1	42	5.4	10.5	3.4	7	4.4	·	4.4	43	7.6	18	1	1	19	·	2	·	·	16	17	10	·	·	9	·
Rok	150.5	2.6	87.5	2.1	91	2.6	111.5	2.4	138	3.3	224.5	3.9	123	3.2	133	3.3	36	3.0	669	19.0	11. VI	19	40	126	25	9	1	47	145	183	133	16	23	94	20

Mielec $H_s = 168$ m $H_b = 170.2$ m $h_w = 14.5$ m

I	10	4.8	4.5	2.6	7	3.9	12.5	3.8	30.5	4.7	10.5	3.6	8.5	6.1	3.5	2.9	6	4.0	73	14.9	31	6	9	26	·	3	·	1	17	17	12	2	5	31	·
II	14	5.4	6	3.8	1.5	3.0	0.5	2.0	14.5	5.1	14.5	4.1	22.5	5.0	7.5	4.7	3	4.6	35	5.6	18	15	24	28	·	·	·	·	15	18	10	·	2	28	·
III	8.5	3.5	7.5	4.3	3	5.0	6.5	3.7	26	4.1	10	3.2	8.5	4.1	4	3.6	19	3.1	51	7.4	17	4	5	20	·	·	·	5	14	16	12	·	4	16	·
IV	4.5	5.7	16	3.6	22	5.2	7.5	3.3	5.5	3.1	14.5	3.8	8	3.1	5	5.1	7	3.8	41	9.7	26	·	·	6	·	·	·	1	16	14	8	·	1	·	2
V	12.5	3.3	10	3.2	8.5	3.6	5.5	2.5	12	3.6	13	2.9	15.5	3.7	10	4.0	6	3.2	76	25.4	29	·	·	3	1	1	·	2	13	19	17	1	3	·	6
VI	5.5	4.9	6	3.7	9	3.4	8	2.9	11.5	3.9	14.5	2.8	13.5	3.9	10	4.0	12	3.1	86	17.4	27	·	·	·	7	·	·	·	7	12	11	4	1	·	5
VII	3.5	2.6	6.5	2.7	8.5	3.1	4.5	2.6	22.5	3.0	25	3.2	15.5	3.3	3	1.7	4	2.9	58	12.6	21	·	·	·	11	·	·	3	9	17	13	1	·	·	8
VIII	7.5	4.9	2	4.5	4.5	1.3	6	2.4	22.5	3.2	13	2.2	13.5	3.4	11	4.7	13	2.8	188	41.0	1	·	·	·	8	1	·	8	12	15	12	6	·	·	3
IX	1	2.0	·	·	1	3.0	21.5	3.3	35.5	3.8	10	2.7	7	3.3	4	2.8	10	3.0	48	20.4	11	·	·	·	7	·	·	6	3	7	7	2	4	·	1
X	7.5	2.3	7.5	1.7	4	2.1	2.5	1.4	20.5	2.5	15.5	2.5	15.5	3.6	5	3.2	15	2.2	2	1.4	31	·	·	12	·	·	·	5	10	4	1	·	7	·	·
XI	3	2.0	9.5	3.6	7.5	3.0	6	2.2	18	3.7	14.5	3.4	12.5	4.2	5	2.6	14	2.9	45	10.3	11	4	10	20	·	3	·	·	15	17	11	1	5	12	1
XII	1.5	1.0	1.5	2.3	4.5	1.4	3.5	3.0	40	4.3	22.5	3.2	9.5	3.6	4	3.1	6	3.3	44	14.9	18	1	4	21	·	2	·	1	18	16	11	1	·	8	·
Rok	79	3.5	77	3.0	81	3.2	84.5	2.8	259	3.8	177.5	3.1	150	3.9	72	3.5	115	3.2	747	41.0	1. VIII	30	52	136	34	10	·	32	149	172	125	18	32	95	26

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Spalona $H_s = 790$ m $h_w = 13.5$ m

I	5	6.6	3	5.7	1.5	4.3	14.5	4.2	29.5	7.5	19	8.2	6	9.2	4.5	4.6	10	6.1	67	12.3	17	1	25	31	·	7	·	·	24	21	14	1	14	31	·
II	3.5	8.1	20	6.6	1	7.0	3	4.3	6	4.3	20.5	7.8	11.5	6.7	7.5	5.9	11	6.0	43	6.3	13	14	28	28	·	5	2	1	18	23	17	·	10	28	·
III	4.5	5.7	12.5	6.4	6.5	4.8	7	5.6	23.5	6.2	17.5	7.4	9	6.0	2.5	3.0	10	5.6	42	7.8	21	4	10	21	·	3	·	3	13	16	12	·	8	28	·
IV	2.5	4.6	19.5	6.1	8	3.4	4.5	3.0	13.5	5.4	14.5	6.5	8.5	6.3	3	6.3	16	4.6	103[2]	15.8	21	·	·	7	·	·	·	5	22	18[2]	15[2]	3[2]	9	2	·
V	8	5.8	14	5.9	10	5.7	6	3.8	5.5	8.1	24	7.8	6	5.0	6.5	3.5	13	5.3	243	73.4	29	·	·	3	·	4	2	2	19	25	22	6	10	·	5
VI	3	6.3	10.5	5.9	5.5	4.5	7	4.9	13	6.2	23	7.6	12	7.4	4	7.5	12	5.7	170	31.6	9	·	·	·	1	6	2	2	14	18	14	7	7	·	6
VII	1	5.0	7.5	5.5	4.5	4.1	1.5	3.7	16.5	5.9	43.5	8.1	8.5	8.2	·	·	10	6.4	229	93.6	17	·	·	·	2	10	2	·	17	26	19	7	6	·	6
VIII	2	3.0	15	3.9	7	3.6	8.5	4.2	25.5	5.9	13.5	5.7	7	6.1	3.5	3.6	11	4.4	80	27.6	24	·	·	·	1	2	·	5	8	13	8	3	3	·	2
IX	2	4.0	1	9.0	5.5	6.1	9	7.8	37.5	6.4	25	7.0	3	4.3	3	3.7	4	6.2	58	24.3	28	·	·	·	·	7	1	5	7	15	8	1	2	·	2
X	3	5.0	16	4.3	13	4.0	10	4.8	14.5	7.3	16	8.2	6.5	7.2	·	·	14	5.1	16	7.3	31	·	·	4	·	6	1	6	6	8	4	·	9	·	·
XI	9	6.4	12	5.6	4.5	4.3	7	5.6	13	7.5	21	11.3	4	10.2	2.5	4.2	17	6.3	61	13.3	27	4	13	24	·	9	3	2	20	22	14	2	13	19	·
XII	1	3.0	·	·	4	6.8	7	6.6	14.5	8.4	42	10.8	11.5	10.7	4	4.8	9	8.5	138	37.2	5	·	16	28	·	13	7	·	22	24	18	3	10	31	·
Rok	44.5	5.3	131	5.4	71	4.9	85	4.9	212.5	6.6	279.5	8.0	93.5	7.3	41	3.9	137	5.8	1250	93.6	17. VII	23	92	146	4	72	20	31	190	225[2]	165[2]	33[2]	101	139	21

Olkusz $H_s = 360$ m $h_w = 16.5$ m

I	11.5	2.1	4	4.2	11	1.7	10	1.7	6.5	1.5	7	2.6	27	2.8	8	2.8	8	2.2	74	19.8	9	1	8	29	·	·	·	—	—	16	11	3	—	31	·
II	11	3.0	11	3.1	4	3.8	·	·	·	·	8	5.6	21	3.8	17	4.2	12	3.3	33	3.1	17	11	26	28	·	3	·	—	—	19	16	·	—	28	·
III	9	3.9	7.5	2.6	10.5	3.7	11.5	2.0	8	2.1	11.5	3.1	8	3.2	5	3.0	22	2.2	47	17.9	21	5	7	23	·	·	·	—	—	12	7	2	—	18	·
IV	10	3.0	4.5	3.0	24.5	5.6	10	2.1	2	3.0	·	·	14.5	3.2	6.5	1.2	18	2.9	43	8.0	23	·	·	6	·	2	1	—	—	15	12	·	—	·	2
V	8	2.9	3	2.7	12.5	3.1	8	3.2	1.5	1.0	12	3.8	12.5	2.9	13.5	2.9	22	2.3	128	24.4	29	·	·	3	·	·	·	—	—	21	20	2	—	·	5
VI	9.5	1.9	5.5	2.9	13	3.5	2	2.0	4	2.0	8	3.9	17.5	3.1	7.5	3.6	23	2.3	117	21.8	27	·	·	·	5	·	·	—	—	14	14	4	—	·	4
VII	4	1.8	2	1.5	11	1.8	3.5	1.6	2.5	2.6	19	2.5	23	2.3	5	2.2	23	1.7	79	29.0	17	·	·	·	4	·	·	—	—	20	14	1	—	·	·
VIII	9.5	2.5	9	1.7	7	1.6	6	2.0	5	1.7	7	2.1	11	2.1	11.5	2.3	27	1.4	103	32.2	26	·	·	·	7	·	·	—	—	15	11	2	—	·	·
IX	2.5	1.0	0.5	1.0	6	2.3	22	1.8	4.5	2.4	10.5	3.1	14	1.9	5	1.4	25	1.5	92	18.5	28	·	·	·	2	·	·	—	—	13	11	4	—	·	·
X	4	3.4	4.5	3.0	12	2.1	8	1.8	2	2.5	8.5	2.5	17	3.1	7	2.6	30	1.8	2	1.0	16	·	·	8	·	·	·	—	—	4	1	·	—	·	·
XI	4.5	2.6	10.5	3.9	8	4.2	4.5	1.6	3.5	2.6	19	4.6	12.5	2.4	6.5	1.6	21	2.5	45	10.6	11	4	10	24	·	2	·	—	—	17	12	1	—	10	1
XII	6	1.5	·	·	2.5	3.0	5.5	1.5	10.5	2.5	33.5	3.4	17.5	3.7	4.5	2.6	13	2.6	58	18.6	18	·	9	21	·	·	·	—	—	18	13	1	—	6	·
Rok	89.5	2.5	62	2.5	122	3.0	91	1.8	50	2.0	144	3.1	195.5	2.9	97	2.5	244	2.2	821	32.2	26.VIII	21	60	142	18	7	1	—	—	184	142	20	—	93	12

Borusowa

$\varphi = 50°17'$ $\lambda = 20°47'$

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	−5.6	5.4	30	−15.2	12	−3.0	−0.4	−2.2	−2.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	6.2	9.0	8.1
II	–	–	–	–	−2.0	−11.0	3.8	14	−24.9	7	−7.3	−4.0	−6.9	−6.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	6.2	8.2	7.6
III	–	–	–	–	5.2	−4.3	16.5	30	−19.0	1	−2.2	3.6	0.6	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	4.9	8.5	7.4
IV	–	–	–	–	11.2	2.5	17.1	7	−1.0	7, 6, 16	4.1	9.8	6.4	6.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.1	7.1	7.4
V	–	–	–	–	15.9	6.6	27.0	19	−1.1	4	9.2	14.3	11.0	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	7.9	7.0
VI	–	–	–	–	21.4	10.9	31.1	26	4.9	3	14.6	19.8	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.4	6.5	5.0
VII	–	–	–	–	21.6	11.0	27.9	16	6.4	10	15.0	20.0	15.7	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.2	6.5	5.8
VIII	–	–	–	–	20.9	10.2	30.7	8	4.6	31	12.9	19.6	14.8	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.8	6.7	5.5
IX	–	–	–	–	21.1	8.9	26.2	3	3.9	22	11.8	19.5	13.3	14.5	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.1	4.8	4.6
X	–	–	–	–	12.6	1.7	21.4	2	−5.0	23	3.2	11.3	6.5	6.9	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.7	6.5	6.4
XI	–	–	–	–	2.2	−3.8	14.7	2	−17.7	18	−2.1	1.1	−0.9	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	9.3	7.7	9.2	8.7
XII	–	–	–	–	3.0	−1.9	8.0	19	−11.3	17	−0.6	1.7	0.1	0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.4	9.2	9.0
Rok	–	–	–	–	11.2	2.1	31.1	26. VI	−24.9	7. II	4.6	9.7	6.2	6.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.0	7.5	6.9

Zakrzów

$\varphi = 50°16'$ $\lambda = 18°09'$

I	–	–	–	–	2.2	−2.8	6.4	29	−13.2	7	−1.5	1.3	−0.6	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	6.9	7.2
II	–	–	–	–	−1.3	−9.6	3.7	14	−20.9	6	−6.5	−2.9	−5.9	−5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.9	6.5	7.2
III	–	–	–	–	6.4	−3.0	16.5	30	−16.9	9	−1.2	5.4	1.1	1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.5	4.8	5.9
IV	–	–	–	–	11.4	2.7	16.2	4, 6	−2.3	16	4.9	10.2	6.3	6.9	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	5.7	7.0
V	–	–	–	–	15.3	6.8	23.6	17	−1.3	4	9.5	14.1	10.2	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.7	6.7	7.3
VI	–	–	–	–	21.3	10.9	32.5	26	4.4	3	15.1	20.0	14.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.7	5.2	5.7
VII	–	–	–	–	21.8	12.3	30.6	15	5.5	5	15.6	20.4	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.1	5.3	7.0
VIII	–	–	–	–	21.6	10.6	30.6	7, 8	4.8	31	13.5	20.2	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.9	4.9	5.4
IX	–	–	–	–	21.1	9.1	28.1	3	3.3	22	11.4	19.6	13.4	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.0	3.6	4.3
X	–	–	–	–	13.9	2.6	24.2	2	−7.1	23	4.7	12.8	6.2	7.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	4.1	3.3	4.8
XI	–	–	–	–	4.5	−2.9	14.5	2	−12.7	15	−1.0	2.6	0.0	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.1	6.7	7.5
XII	–	–	–	–	4.0	−1.6	9.9	19	−12.6	15	0.6	2.6	0.7	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.8	6.5	7.6
Rok	–	–	–	–	11.8	2.9	32.5	26. VI	−20.9	6. II	5.4	10.5	6.3	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	5.5	6.4

Długopole-Zdrój

$\varphi = 50°15'$ $\lambda = 16°38'$

I	–	–	–	–	1.3	−3.4	4.6	18, 30	−14.2	7	−1.9	−0.2	−0.5	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.0	9.2	8.7
II	–	–	–	–	−2.0	−9.7	2.5	14	−19.5	28	−6.7	−3.3	−5.6	−5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.1	7.3	8.0
III	–	–	–	–	4.8	−3.2	15.2	30	−20.4	9	−1.2	3.1	0.8	0.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.4	6.2	6.5
IV	–	–	–	–	10.4	2.1	16.8	4	−3.7	2	3.9	8.9	5.7	6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.0	6.7	6.9
V	–	–	–	–	14.2	5.8	22.4	17	−2.2	3	8.7	12.5	9.1	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	7.6	7.3
VI	–	–	–	–	19.9	9.7	31.4	26	2.0	3	13.8	18.1	13.8	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.2	5.4	5.8
VII	–	–	–	–	20.4	11.8	28.5	15	4.2	5	14.6	18.5	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.9	5.4	6.4
VIII	–	–	–	–	20.5	9.8	27.9	7	3.4	16	12.7	18.5	13.7	14.6	–	–	–	–	–	–	–	–	–	–	–	–	4.5	6.1	5.1	5.2
IX	–	–	–	–	18.5	10.2	25.2	3	3.2	20	12.2	16.8	12.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.1	3.5	4.7
X	–	–	–	–	12.9	2.2	22.0	1	−6.8	23	4.0	11.8	6.3	7.1	–	–	–	–	–	–	–	–	–	–	–	–	5.0	2.6	2.7	3.4
XI	–	–	–	–	3.1	−2.9	13.1	2	−12.5	15	−1.5	1.3	−0.6	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.6	7.8
XII	–	–	–	–	3.0	−2.5	9.0	19	−14.6	15	0.0	1.3	0.2	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	8.1	8.1
Rok	–	–	–	–	10.6	2.5	31.4	26. VI	−20.4	9. III	4.9	8.9	5.9	6.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	6.2	6.6

Leżajsk

$\varphi = 50°15'$ $\lambda = 22°26'$

I	–	–	–	–	0.9	−5.4	6.8	30	−16.9	12	−3.0	−0.9	−2.6	−2.3	4.5	4.9	4.6	4.7	87	83	87	86	0.6	1.0	0.6	0.7	7.9	7.9	7.4	7.7
II	–	–	–	–	−2.5	−10.1	2.3	12	−24.5	8	−7.5	−3.6	−6.9	−6.2	3.1	3.8	3.2	3.4	84	78	82	81	0.5	1.0	0.6	0.7	7.9	7.7	6.3	7.3
III	–	–	–	–	6.3	−3.0	17.5	30	−17.4	1	−1.9	4.7	1.0	1.2	4.8	6.2	5.6	5.5	86	72	84	81	0.7	2.7	1.1	1.5	6.5	6.7	6.1	6.4
IV	–	–	–	–	11.1	2.8	17.0	7	−0.9	6	4.3	9.4	6.1	6.5	7.3	8.2	7.7	7.7	85	70	80	78	1.2	3.9	1.9	2.3	8.0	8.2	5.3	7.2
V	–	–	–	–	16.3	6.5	27.2	19	−2.0	4	9.5	14.5	10.6	11.3	10.4	11.1	11.3	10.9	85	67	86	79	2.0	6.1	1.8	3.3	6.5	8.1	6.6	7.1
VI	–	–	–	–	22.3	11.9	30.0	26	6.1	8	15.1	20.4	16.3	17.0	14.5	14.5	14.7	14.6	84	62	79	75	3.0	10.1	4.2	5.8	5.4	6.7	7.7	6.6
VII	–	–	–	–	22.6	12.8	29.8	16	7.0	12	15.7	20.7	16.6	17.4	15.0	15.5	15.9	15.5	84	64	83	77	3.0	9.7	3.3	5.3	5.7	7.2	7.0	6.6
VIII	–	–	–	–	21.5	11.1	30.7	8	6.5	17	13.1	19.5	14.6	15.4	13.8	14.1	14.1	14.0	90	64	84	79	1.6	9.7	2.9	4.7	6.5	6.1	4.7	5.8
IX	–	–	–	–	21.7	9.6	26.9	3	4.2	22	11.6	19.7	13.4	14.5	12.7	14.2	13.5	13.5	92	62	87	80	1.2	9.3	2.0	4.2	4.1	5.5	2.0	3.9
X	–	–	–	–	12.8	3.2	23.4	1	−3.8	22	5.0	11.2	7.1	7.6	7.9	8.8	8.6	8.4	89	66	83	79	1.0	5.0	1.8	2.6	6.2	6.6	4.8	5.9
XI	–	–	–	–	3.3	−3.2	15.2	2	−18.8	18	−1.5	1.1	−0.6	−0.4	5.0	5.5	5.4	5.3	86	79	86	84	0.9	1.6	0.9	1.1	9.0	8.7	7.3	8.3
XII	–	–	–	–	3.1	−2.2	8.0	10	−18.8	17	0.0	1.7	0.0	0.4	5.3	5.7	5.5	5.5	83	81	87	84	1.1	1.4	0.8	1.1	8.1	7.7	7.1	7.6
Rok	–	–	–	–	11.6	2.8	30.7	8. VIII	−24.5	8. II	5.0	9.9	6.3	6.9	8.7	9.4	9.2	9.1	86	71	84	80	1.4	5.1	1.8	2.8	6.8	7.3	6.0	6.7

Borusowa — $H_s = 170\,m$ — $h_w = 14{,}1\,m$ — 1965

MIESIĄC	ROZKŁAD WIATRU #D,VmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Date	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	≥15	◔	●	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K ⊗
I	10	2.6	6	1.3	5.5	2.5	4.5	4.2	11	1.9	4	2.0	13	2.9	2	4.0	37	1.5	55	11.0	31	7	9	27	·	1	·	1	19	14	13	1	5	31	·
II	14	2.2	5.5	4.5	1.5	1.0	0.5	4.0	3.5	2.3	7	5.5	27	4.3	8	3.6	17	3.1	14	4.0	17	12	23	28	·	2	·	1	15	15	5	·	4	28	·
III	10.5	3.6	6	2.2	3.5	3.4	5.5	4.9	4	4.5	·	·	13	3.8	5.5	1.9	45	1.8	40	12.4	6	7	5	21	·	·	·	·	14	12	8	1	7	18	·
IV	10.5	3.2	13.5	3.0	19.5	5.1	1.5	3.3	2	5.8	·	·	16	4.2	7	3.3	20	3.1	35	9.6	12	·	·	4	·	4	·	2	14	11	8	·	2	·	1
V	13	2.7	9	2.8	13	2.7	2.5	1.8	6	2.8	2	3.0	15.5	3.3	13	3.1	19	2.3	80	18.4	11	·	·	2	1	1	·	1	14	17	16	2	1	·	5
VI	7	2.0	5	2.0	15.5	2.6	4	3.8	2.5	1.8	2	2.0	24.5	3.6	9.5	3.5	20	2.3	102	28.8	27	·	·	·	5	1	·	4	5	12	11	4	·	·	3
VII	2	2.5	4	2.2	10	2.0	1.5	5.7	7.5	2.2	9.5	2.2	25.5	3.5	2	2.0	31	1.8	61	9.9	5	·	·	·	6	·	·	3	7	15	13	·	·	·	3
VIII	11	2.7	·	·	5	1.4	4.5	2.7	9	3.1	2.5	3.0	21	2.9	8	3.1	32	1.8	124	38.5	1	·	·	·	6	·	·	5	8	11	10	4	·	·	1
IX	3	1.3	7	2.9	11	2.9	12	2.9	15	2.7	7	3.1	6.5	3.9	2.5	2.0	26	2.0	72	31.4	29	·	·	·	4	·	·	6	4	7	7	2	7	·	2
X	10.5	2.0	1.5	1.3	4.5	2.0	1	3.0	1.5	2.7	6	2.4	16.5	3.2	7.5	2.9	44	1.4	0	0.1	4	·	·	13	·	·	·	3	9	1	·	·	11	·	·
XI	1.5	1.3	7.5	2.9	11	2.8	2	5.5	6	2.2	12	3.4	15	4.2	8	2.6	27	2.3	34	9.5	21	5	11	23	·	1	·	·	23	12	6	·	4	10	·
XII	3	2.7	1	2.0	4	1.5	5	2.6	22	2.6	8	4.2	18.5	2.9	5.5	2.2	26	2.0	30	7.4	18	1	2	21	·	·	·	·	27	13	8	·	·	8	·
Rok	96	2.4	66	2.3	104	2.5	44.5	3.7	90	2.8	60	2.6	212	3.6	78.5	2.8	344	2.1	647	38.5	1. VIII	32	50	139	22	10	·	26	159	140	105	14	41	95	15

Zakrzów — $H_s = 217\,m$ — $h_w = 16{,}4\,m$

I	11	3.0	0.5	5.0	·	·	5	1.9	23.5	3.7	11.5	4.8	4	3.2	12.5	2.7	25	2.5	57	13.3	9	2	5	25	·	·	·	2	16	17	11	2	2	29	·
II	14	3.8	4	1.5	1	2.0	2	2.0	7.5	3.3	7.5	4.1	10	3.2	27	4.6	11	3.3	26	4.7	17	13	19	27	·	2	·	2	12	18	8	·	1	28	·
III	13.5	3.3	2	3.5	0.5	2.0	6.5	1.9	17.5	2.1	14.5	2.8	5	2.8	14.5	3.5	19	2.2	42	10.3	21	4	6	18	·	·	·	5	9	14	8	1	5	15	·
IV	10.5	3.2	6.5	2.3	11	3.5	9.5	1.7	14	2.4	3.5	3.4	6.5	3.2	22.5	3.5	6	2.8	72	16.8	19	·	·	5	·	·	·	5	14	17	11	2	4	·	1
V	13.5	3.1	4	3.0	7	3.9	4.5	2.4	8	2.9	6.5	5.0	14	2.2	24.5	3.5	11	2.8	121	15.7	17	·	·	2	·	3	2	1	16	23	18	4	1	·	6
VI	8	3.0	4	2.8	·	·	7.5	2.2	16	3.8	10	2.8	9	2.7	27.5	3.4	8	2.9	112	28.3	11	·	·	·	7	1	·	5	9	15	14	3	·	·	7
VII	7	2.3	·	·	5	2.4	2	2.0	20.5	3.4	15.5	2.8	14.5	2.8	15.5	2.8	13	2.5	53	9.5	1	·	·	·	7	·	·	2	11	20	14	·	1	·	5
VIII	17	2.6	1	3.0	0.5	3.0	3.5	4.1	15	3.9	7.5	2.1	9.5	2.9	27	3.0	12	2.7	43	16.4	24	·	·	·	8	1	·	4	6	8	7	1	2	·	1
IX	4	3.1	·	·	0.5	2.0	11.5	3.1	31	3.4	8	3.1	3	2.3	11	2.5	21	2.4	36	10.9	29	·	·	·	2	1	·	9	5	9	8	1	4	·	1
X	19	2.0	0.5	1.0	6.5	1.8	3	1.5	19.5	3.9	5.5	4.8	5	3.5	15	2.5	19	2.3	1	0.8	29	·	·	8	·	·	·	7	6	3	·	·	12	·	·
XI	5.5	2.7	5	3.4	8.5	2.8	4.5	2.3	22.5	3.2	9.5	3.5	7	4.8	13.5	2.6	14	2.7	27	10.1	11	4	7	22	·	·	·	2	16	14	7	1	4	10	·
XII	·	·	·	·	3	2.0	3.5	2.1	32.5	4.1	22	3.4	9	3.8	15	3.4	8	3.2	46	11.2	13	1	·	21	·	3	·	·	14	19	9	1	·	7	·
Rok	123	2.7	27.5	2.1	43.5	2.1	63	2.3	227.5	3.3	121.5	3.6	96.5	3.0	225.5	3.2	167	2.7	636	28.3	11. VI	24	37	128	24	11	2	44	134	177	115	16	36	89	21

Długopole-Zdrój — $H_s = 420\,m$ — $h_w = 20\,m$

I	10.5	3.4	·	·	0.5	3.0	10	4.0	43	4.0	7.5	4.4	·	·	3.5	1.7	18	3.1	49	13.4	17	3	9	28	·	·	·	·	21	18	12	1	–	31	·
II	25.5	4.7	4.5	2.0	2	2.5	4.5	3.9	14.5	3.0	3.5	3.3	2	4.0	4.5	3.6	23	2.7	41	7.0	13	10	21	28	·	·	·	1	17	23	14	·	–	28	·
III	16.5	3.8	6	2.3	·	·	9.5	3.3	38	3.3	5.5	2.6	·	·	3.5	3.9	14	2.8	38	6.9	21	4	7	18	·	·	·	3	12	17	11	·	–	18	·
IV	22.5	3.2	3.5	3.1	·	·	5.5	3.1	13	2.8	5	1.8	2.5	2.4	9	2.3	29	1.9	81	14.5	25	·	·	6	·	·	·	6	16	20	13	2	–	·	·
V	24.5	2.9	9	3.2	1	2.0	2.5	3.4	15.5	2.8	3	3.2	3	3.2	5.5	2.5	29	2.0	178	51.4	29	·	·	3	·	·	·	2	16	27	18	6	–	·	5
VI	17	2.8	5	1.6	2	1.2	7	2.9	32	2.5	7.5	2.1	4	2.0	2.5	4.0	13	2.1	112	18.2	22	·	·	·	5	·	·	4	10	15	13	3	–	·	6
VII	7.5	3.3	1.5	3.3	1	2.0	9.5	3.3	32	3.3	20.5	2.7	3	2.8	5	2.5	13	2.6	107	27.2	15	·	·	·	3	·	·	1	10	20	14	4	–	·	7
VIII	12	1.6	4.5	2.3	0.5	2.0	6.5	3.2	22	3.5	3	2.3	1	2.0	4.5	2.0	39	1.6	78	19.2	25	·	·	·	7	·	·	5	5	12	8	4	–	·	1
IX	2.5	2.6	2	3.2	1	3.0	10	4.6	45.5	3.8	4.5	3.6	0.5	3.0	1	2.5	23	2.8	68	38.3	28	·	·	·	1	·	·	6	7	11	7	2	–	·	2
X	22.5	2.5	3	3.2	2.5	1.2	4	3.8	16.5	3.3	6	3.5	·	·	2.5	2.4	36	1.8	12	6.7	31	·	·	11	·	·	·	10	1	4	3	·	–	·	·
XI	20.5	3.7	1.5	3.3	·	·	6.5	3.5	26.5	4.2	5	3.6	1	5.0	·	·	29	2.6	57	12.6	27	2	9	23	·	·	·	2	18	25	12	2	–	14	·
XII	7.5	2.3	0.5	1.0	1	3.0	9.5	3.1	47.5	3.9	5	3.3	3	2.8	2	2.0	17	2.8	85	27.9	5	3	5	21	·	1	·	·	19	21	14	2	–	20	·
Rok	189	3.1	40	2.4	11.5	1.7	85	3.5	347	3.4	76	3.0	20	2.3	43.5	2.4	283	2.4	906	51.4	29. V	22	51	138	16	1	·	40	152	213	139	26	–	111	21

Leżajsk — $H_s = 190\,m$ — $h_w = 15{,}7\,m$

I	3.5	1.3	1	1.0	6	4.3	16	3.2	10.5	5.2	21.5	4.3	16	4.5	3.5	3.3	15	3.4	43	12.8	31	7	7	26	·	2	·	3	21	18	11	1	5	31	·
II	7	2.6	6.5	2.2	1.5	3.0	·	·	3	8.5	16.5	6.3	34	4.7	9.5	2.6	6	4.2	39	8.7	8	12	21	28	·	4	·	2	14	20	12	·	4	28	·
III	5	3.9	11.5	1.9	2.5	2.6	19.5	2.6	12	2.5	8.5	3.5	12	3.1	6	3.1	16	2.3	49	9.4	17	2	2	21	·	1	·	5	12	15	12	·	16	18	·
IV	6	2.8	4	3.5	33.5	6.9	12.5	3.0	8.5	2.6	7.5	2.5	7	3.2	6	3.3	5	4.3	49	14.1	30	·	·	6	·	5	·	1	12	10	8	1	1	·	3
V	8	2.0	4	3.2	10	3.7	7	2.0	4	4.4	12.5	4.2	19.5	2.3	17	3.1	11	2.7	56	19.0	29	·	·	3	2	·	·	2	12	15	11	1	·	·	4
VI	4	2.1	5.5	2.4	15	3.1	2.5	2.6	9	2.9	6.5	4.1	33.5	3.0	9	2.8	5	2.8	87	15.4	10	·	·	·	6	2	·	1	12	11	10	3	1	·	5
VII	1	1.0	·	·	10	2.2	8	1.8	16.5	2.6	22	2.6	27	3.4	2.5	1.2	6	2.5	114	45.4	21	·	·	·	11	·	·	4	14	17	14	2	2	·	6
VIII	8.5	1.7	2	1.0	7	1.9	2.5	1.8	11	2.4	5.5	3.7	28	3.2	18.5	2.9	10	2.4	139	44.1	26	·	·	·	8	1	·	8	14	15	12	3	5	·	3
IX	3	2.3	·	·	15	2.8	10.5	1.7	14	2.1	14	2.4	11.5	2.6	5	2.8	17	1.9	48	19.2	11	·	·	·	6	·	·	11	4	8	6	2	8	·	1
X	9	1.8	1.5	2.3	3.5	2.4	1.5	1.0	2	6.0	25	5.0	21	4.0	7.5	3.2	22	2.9	7	3.5	31	·	·	7	·	1	·	6	10	7	2	·	12	·	·
XI	2	2.0	8.5	3.1	9.5	4.4	8	2.6	10	3.8	18	3.2	16	4.4	5	1.2	13	2.9	39[2]	8.4	30	3	9	20	·	2	·	1	20	18	11	·	7	16	·
XII	1	1.0	2	2.5	4	2.5	9	3.1	18	4.2	36.5	5.0	12.5	2.9	3	1.7	7	3.7	42	12.6	18	2	4	22	·	4	2	1	18	16	7	1	4	8	·
Rok	58	2.0	46.5	1.9	117.5	3.3	97	2.1	118.5	3.9	194	3.9	238	3.4	92.5	2.6	133	3.0	712[2]	45.4	21. VII	26	43	133	33	22	2	45	163	170	116	14	65	101	22

Katowice

φ = 50°14′ λ = 19°02′

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	978.1	991.3	956.0	1013.4	2.1	−3.7	7.3	29	−12.7	8	−1.6	1.2	−0.6	−0.4	4.9	5.3	5.2	5.1	89	80	88	86	0.6	1.4	0.7	0.9	8.0	8.7	7.3	8.0
II	982.1	995.0	962.1	1018.4	−2.4	−9.1	2.5	14	−22.0	6	−7.0	−3.7	−5.8	−5.6	3.3	3.7	3.5	3.6	86	79	84	83	0.5	1.0	0.6	0.7	7.9	7.4	7.6	7.6
III	982.6	998.7	954.7	1017.8	6.4	−2.5	16.4	30	−13.2	11	−1.2	4.9	1.7	1.8	5.4	5.8	5.8	5.7	91	65	81	79	0.5	3.4	1.3	1.7	7.0	6.9	4.9	6.3
IV	976.5	995.6	961.7	1011.0	10.7	2.4	15.4	3	−2.0	2	4.2	9.3	5.9	6.3	7.5	7.4	7.7	7.5	89	65	82	79	0.9	4.5	1.7	2.4	7.5	7.8	6.2	7.2
V	979.9	994.2	966.0	1014.0	15.0	5.7	26.2	19	−3.4	3	8.7	13.2	10.0	10.5	10.1	10.2	10.4	10.2	87	67	83	79	1.4	5.5	2.2	3.0	7.5	8.3	7.1	7.6
VI	981.2	990.6	969.4	1014.6	21.0	10.4	32.0	26	4.9	3	14.4	19.0	15.2	16.0	13.7	13.4	13.9	13.7	83	63	80	75	3.0	9.4	3.7	5.4	5.7	7.2	6.0	6.3
VII	980.0	987.1	970.1	1013.4	21.2	11.7	29.7	14	5.5	5	15.1	19.7	15.0	16.2	14.4	14.4	14.2	14.3	84	63	83	77	3.0	9.3	3.2	5.2	7.4	8.2	6.3	7.3
VIII	983.2	989.9	972.2	1016.8	20.9	10.4	30.5	8	5.2	31	12.9	19.4	14.4	15.3	13.1	12.2	13.2	12.8	88	56	80	75	2.1	11.3	3.6	5.7	6.3	6.9	6.1	6.4
IX	982.5	1000.2	970.3	1016.2	20.6	8.6	27.1	3	3.2	22	11.4	19.1	13.6	14.4	12.2	12.4	12.8	12.5	91	58	83	77	1.5	10.2	3.0	4.9	5.6	6.1	5.0	5.6
X	989.6	1001.8	980.2	1024.4	13.1	2.8	22.6	2	−6.4	22	4.6	12.3	6.6	7.5	8.3	8.4	8.8	8.5	93	58	87	79	0.6	6.3	1.3	2.7	6.1	4.8	4.1	5.0
XI	977.9	997.8	952.6	1013.2	3.3	−3.9	12.9	2	−16.1	18	−1.6	1.8	−0.3	−0.1	5.1	5.5	5.5	5.4	89	77	87	84	0.7	2.0	0.9	1.2	8.3	7.6	7.6	7.8
XII	973.8	991.5	953.7	1008.8	3.5	−1.9	10.1	20	−9.4	15	0.3	2.2	0.7	1.0	5.5	5.6	5.5	5.5	87	77	84	83	0.9	1.7	1.1	1.2	8.1	8.8	8.0	8.3
Rok	980.6	1001.8	952.6	1015.1	11.3	2.6	32.0	26.VI	−22.0	6. II	5.0	9.9	6.4	6.9	8.6	8.7	8.9	8.7	88	67	84	80	1.3	5.5	1.9	2.9	7.1	7.4	6.4	7.0

Kolbuszowa

φ = 50°14′ λ = 21°47′

I	–	–	–	–	0.7	−5.4	5.5	30	−17.3	11	−2.5	−0.2	−2.4	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.8	7.8	7.9
II	–	–	–	–	−3.0	−12.2	2.4	14	−29.2	7	−8.1	−4.5	−8.2	−7.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.8	7.2	8.0
III	–	–	–	–	5.8	−3.9	16.4	30	−20.4	1	−1.7	4.5	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.7	6.0	6.7
IV	–	–	–	–	10.9	2.4	16.9	7	−1.4	6	4.2	9.2	5.9	6.3	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.5	6.9	8.1
V	–	–	–	–	16.0	6.0	26.8	19	−3.8	4	9.2	14.1	9.9	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.2	6.9	7.4
VI	–	–	–	–	21.8	11.1	31.6	26	5.7	8	15.0	20.4	15.1	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.8	6.9	6.5
VII	–	–	–	–	22.0	11.6	28.8	16, 17	5.1	12	15.7	20.5	15.2	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.5	6.2	6.8
VIII	–	–	–	–	20.8	10.7	30.1	8	5.7	17	13.4	19.4	14.2	15.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.5	5.4	6.0
IX	–	–	–	–	21.2	8.9	26.2	28	3.5	22	12.3	19.8	13.1	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.5	3.2	4.7
X	–	–	–	–	12.4	1.9	23.1	1	−6.0	22	4.5	11.4	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	4.5	5.8
XI	–	–	–	–	2.9	−3.5	14.9	2	−18.4	18	−1.6	1.5	−0.6	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	7.2	8.1
XII	–	–	–	–	2.7	−2.3	6.5	10, 21	−16.5	16	−0.3	1.8	0.0	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.2	7.9
Rok	–	–	–	–	11.2	2.1	31.6	26.VI	−29.2	7. II	5.0	9.8	5.8	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	6.3	7.0

Głubczyce

φ = 50°12′ λ = 17°50′

I	–	–	–	–	2.5	−2.5	5.0	29, 30	−10.4	7, 8	−0.6	1.6	−0.2	0.2	5.6	5.7	5.6	5.6	94	83	92	90	0.4	1.2	0.5	0.7	6.4	6.2	7.0	6.5
II	–	–	–	–	−1.2	−8.9	5.0	14	−18.6	6	−5.9	−2.1	−5.5	−4.8	3.8	4.1	3.8	3.9	93	78	89	87	0.2	1.2	0.4	0.6	6.5	6.3	5.8	6.2
III	–	–	–	–	6.5	−2.3	18.3	30	−18.5	9	−0.5	5.5	1.3	1.9	5.7	6.4	6.3	6.1	90	68	88	82	0.6	3.2	0.8	1.5	6.3	5.4	5.5	5.7
IV	–	–	–	–	11.3	3.3	17.5	3	−2.0	2	5.1	10.0	6.5	7.0	7.8	7.7	8.2	7.9	88	65	85	79	1.1	4.8	1.5	2.5	7.2	7.0	7.0	7.1
V	–	–	–	–	14.5	7.0	22.7	17	−0.6	4	9.4	13.5	10.4	10.9	10.3	10.4	10.8	10.5	85	66	84	78	1.7	5.4	2.0	3.0	8.2	7.3	8.0	7.8
VI	–	–	–	–	20.3	11.1	30.9	26	5.6	3	14.8	19.1	15.2	16.1	14.0	13.5	14.2	13.9	82	63	82	76	3.1	9.4	3.3	5.3	5.0	6.1	4.8	5.3
VII	–	–	–	–	21.0	12.6	29.5	14, 15	5.9	5	15.4	19.5	15.6	16.5	14.7	14.8	14.8	14.8	83	65	82	77	3.0	8.6	3.2	4.9	7.1	7.5	6.4	7.0
VIII	–	–	–	–	20.8	11.2	28.9	8	6.3	31	13.9	19.7	14.8	15.8	13.4	12.1	13.5	13.0	84	54	80	73	2.7	11.7	3.7	6.0	7.1	6.9	5.6	6.5
IX	–	–	–	–	20.2	9.7	27.0	2	5.7	22	12.2	19.0	13.4	14.5	12.5	13.1	13.0	12.9	87	61	84	77	2.0	9.3	2.6	4.6	6.6	6.5	4.9	6.0
X	–	–	–	–	13.6	3.3	23.0	2	−6.1	22	5.1	12.6	7.1	8.0	8.3	9.3	9.1	8.9	91	63	86	80	0.8	5.8	1.5	2.7	7.4	5.7	5.1	6.1
XI	–	–	–	–	3.8	−2.6	14.7	2	−12.1	15	−0.6	2.6	0.3	0.6	5.3	5.7	5.7	5.6	87	77	86	83	0.3	2.1	1.0	1.3	8.7	7.8	7.9	8.1
XII	–	–	–	–	3.7	−1.5	11.5	19	−11.2	15	1.1	2.8	1.0	1.5	5.7	5.8	5.5	5.7	84	77	83	81	1.1	1.8	1.2	1.4	8.6	7.5	6.2	7.4
Rok	–	–	–	–	11.4	3.4	30.9	26.VI	−18.6	6. II	5.8	10.3	6.7	7.4	8.9	9.0	9.2	9.0	87	68	85	80	1.5	5.4	1.8	2.9	7.1	6.7	6.2	6.7

Uwaga. W dniu 27.IV.1965 r. stację przeniesiono z ul. Kochanowskiego 20 o ok. 1200 m w kierunku SSE na teren Technikum Rolniczego przy ul. Oświęcimskiej. Podane wyżej współrzędne geograficzne i wysokości dotyczą nowego miejsca.

Goszyce

φ = 50°11′ λ = 20°08′

I	–	–	–	–	1.4	−4.5	5.6	1	−12.5	12	−2.6	0.1	−1.7	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.4	6.1	7.3
II	–	–	–	–	−2.3	−9.5	3.7	14	−23.3	7	−7.3	−3.6	−6.5	−6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.4	7.1	6.9
III	–	–	–	–	5.5	−3.5	16.2	30	−18.5	1	−1.9	4.6	0.4	0.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.3	5.2	5.6
IV	–	–	–	–	10.5	2.4	16.0	7	−2.2	16	3.8	9.2	6.1	6.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.4	6.7	7.0
V	–	–	–	–	15.2	6.0	26.8	19	−2.7	4	9.0	13.7	10.3	10.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.1	6.4	6.5
VI	–	–	–	–	21.5	10.7	31.7	26	6.3	8	14.6	20.2	15.5	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.8	5.7	5.2
VII	–	–	–	–	21.8	11.9	28.1	14	6.9	6	15.5	19.9	15.9	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.3	5.3	6.4
VIII	–	–	–	–	21.1	10.5	32.2	7	7.2	18, 31	12.7	19.4	14.8	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.4	5.7	6.1
IX	–	–	–	–	20.7	8.8	28.2	3	4.5	17	10.9	19.2	13.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.9	2.3	3.7
X	–	–	–	–	12.6	2.9	20.8	2	−5.6	22	4.3	11.7	7.1	7.6	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.5	3.3	4.2
XI	–	–	–	–	3.0	−3.7	14.2	2	−18.8	18	−2.0	1.4	−0.9	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.1	6.8	6.7
XII	–	–	–	–	3.6	−1.8	10.1	20	−8.1	15	−0.1	2.3	0.7	0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.0	6.7	7.3
Rok	–	–	–	–	11.2	2.5	32.2	7.VIII	−23.3	7. II	4.7	9.8	6.3	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	5.6	6.1

Katowice $H_s = 284$ m $H_b = 283,8$ m $h_w = 20$ m 1965

Miesiąc	Rozkład wiatru n_D, V_{mD}: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R: Suma	Max	Data	Liczba dni (n): Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	◕	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	4.4	7	3.4	·	·	11	2.9	15	4.4	27	5.1	15.5	4.5	6.5	4.2	5	4.1	57	12.2	31	2	5	28	·	4	·	·	17	15	13	1	6	30	·
II	13	4.8	9.5	3.6	2.5	4.6	2.5	2.4	2	5.8	16.5	6.8	24.5	4.1	13.5	4.8	·	4.8	29	5.0	17	7	24	28	·	5	·	1	17	22	8	·	6	28	·
III	7.5	4.1	12.5	3.1	2	2.5	10.5	2.8	13.5	3.2	23.5	4.4	16	4.6	4.5	4.9	3	3.7	45	11.2	21	3	6	20	·	2	·	4	11	18	11	1	10	15	·
IV	7	3.1	6.5	3.7	23	4.2	10	3.5	9	3.3	8.5	4.2	14	4.2	8	4.1	4	3.7	47	8.3	23	·	·	6	·	1	·	4	14	18	13	·	2	·	2
V	9.5	3.8	10	3.6	12.5	4.1	7	3.8	5.5	3.0	19.5	4.3	16.5	3.7	8.5	4.2	4	3.7	104	16.2	19	·	·	3	1	2	·	·	17	21	17	3	2	·	4
VI	13	3.3	7.5	3.5	4.5	3.7	7.5	3.7	6	3.7	20.5	4.4	15.5	4.2	7.5	2.9	8	3.5	84	15.7	27	·	·	·	5	2	·	2	10	15	13	3	2	·	5
VII	6.5	2.7	2.5	1.8	4.5	3.7	9.5	3.2	6	3.2	37	4.5	16.5	3.9	5.5	3.5	5	3.7	100	35.0	17	·	·	·	5	2	·	2	12	20	15	3	2	·	6
VIII	10.5	3.2	4	2.1	3.5	2.9	11	4.0	3.5	4.6	20.5	3.5	15	3.6	14	3.5	11	3.1	57	13.1	24, 25	·	·	·	7	·	·	4	11	14	8	2	1	·	2
IX	6.5	2.5	0.5	1.0	1.5	2.7	19	3.9	15	4.2	24.5	4.3	7.5	4.5	4.5	3.1	11	3.5	61	14.6	19	·	·	·	2	1	·	4	8	13	9	4	8	·	1
X	6	2.8	10	2.6	14	2.8	2	3.0	·	·	25.5	4.8	15.5	3.9	7	3.0	13	3.1	1	0.9	16	·	·	8	·	·	·	9	10	1	·	·	9	·	·
XI	5.5	2.6	8	4.2	8	4.6	9	3.1	6.5	4.2	26	5.4	15	4.4	8	3.4	4	4.1	33	7.7	11	4	10	23	·	5	·	3	19	17	10	·	7	17	·
XII	4	3.2	0.5	1.0	2.5	3.2	8.5	3.2	11	5.2	47.5	6.5	14.5	4.8	4.5	4.4	·	5.4	41	8.1	18	·	3	21	·	8	·	·	18	19	11	·	·	12	·
Rok	95	3.4	78.5	2.8	78.5	3.2	107.5	3.3	93	3.7	296.5	4.8	186	4.2	92	3.8	68	3.9	659	35.0	17. VII	16	48	137	20	32	·	33	164	193	128	17	55	102	20

Uwaga. Kierunki i prędkości wiatru – wg anemometru M – 47.

Kolbuszowa $H_s = 208$ m $h_w = 16,1$ m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	3.9	5.5	3.5	4.5	7.7	8	4.4	21.5	4.4	21	4.8	13	4.8	5	3.9	10	4.1	58	11.5	31	7	11	28	·	4	1	1	21	16	10	2	—	31	·
II	12	3.6	6	3.0	1.5	3.7	·	·	3.5	10.1	12.5	5.9	26	4.8	12.5	4.8	10	4.3	51	10.7	8	14	25	28	·	3	1	1	16	19	13	1	—	28	·
III	4	3.1	11	3.7	3	3.5	4	3.2	16.5	5.0	15	2.9	14	3.2	4.5	4.1	21	2.9	33	7.8	17	6	5	19	·	3	·	3	13	15	9	·	—	19	·
IV	3.5	3.4	6	3.9	29.5	7.5	10.5	7.3	4	2.2	8	3.7	12.5	2.8	9	3.4	7	5.0	37	6.1	30	·	·	6	·	7	1	·	17	14	10	·	—	·	2
V	13.5	3.1	4	3.6	12	4.6	5.5	3.8	3.5	4.0	10.5	4.3	17	3.5	9	4.3	18	3.1	72	24.3	29	·	·	2	1	2	1	1	14	17	13	1	—	·	4
VI	6.5	3.4	3.5	3.3	6	4.0	10	2.1	5	3.6	7	3.4	25.5	3.5	14.5	3.8	12	2.9	108	19.0	10	·	·	·	6	1	1	·	9	12	11	5	—	·	3
VII	2	1.5	3	3.8	9	3.2	3.5	3.6	6	4.2	16	3.1	29	3.3	7.5	2.3	17	2.6	81	23.8	21	·	·	·	7	·	·	2	10	19	13	3	—	·	1
VIII	9	3.9	1	10.0	1	1.0	11	2.2	10.5	3.1	6.5	4.1	19.5	3.0	15.5	4.1	19	2.7	177	36.1	26	·	·	·	7	1	·	3	11	16	14	6	—	·	1
IX	3.5	3.0	0.5	2.0	·	·	14.5	2.5	23	3.7	12	3.8	6.5	2.2	8	2.8	22	2.4	53	30.0	11	·	·	·	4	1	·	6	3	7	6	2	—	·	3
X	6	3.4	1	2.0	8	2.6	3.5	1.9	3.5	2.4	18	3.0	18	3.1	9	2.2	26	2.0	5	2.3	31	·	·	11	·	·	·	4	9	5	2	·	—	·	·
XI	3	3.7	9.5	4.5	5.5	6.0	7	4.2	15	5.2	13.5	3.4	18.5	4.3	5	2.3	13	3.7	44	9.8	21	5	10	20	·	2	·	·	16	16	8	·	—	10	·
XII	2.5	2.6	3	2.0	1.5	3.7	7.5	2.2	23.5	5.4	38	4.1	13.5	3.9	3.5	3.4	·	4.1	44	17.0	18	3	4	22	·	3	2	·	18	17	12	1	—	7	·
Rok	70	3.2	54	3.8	81.5	4.0	85	3.1	135.5	4.4	178	3.9	213	3.5	103	3.4	175	3.3	763	36.1	26.VIII	35	55	136	25	27	7	21	157	173	121	21	—	95	14

Głubczyce $H_s = 280$ m $h_w = 12,9$ m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5	2.2	·	·	·	·	·	·	20	5.1	18	4.9	2	1.0	11	3.5	37	2.6	49	9.3	3	2	4	26	·	4	·	7	16	14	11	·	—	31	·
II	15	4.1	3.5	4.4	1	1.0	1	2.0	7.5	4.0	5.5	5.6	4.5	4.2	7	6.7	39	2.5	47	9.3	8, 17	12	18	28	·	2	·	3	9	17	11	·	—	28	·
III	9	3.0	·	·	·	·	1	1.0	12.5	3.8	7.5	3.5	7	3.7	1	2.0	55	1.4	35	10.5	6	3	4	17	·	·	·	5	10	10	6	1	—	18	·
IV	7	2.3	·	·	8	2.8	4	3.2	6.5	3.2	3	3.5	12.5	2.7	4	3.0	45	1.4	62	17.3	19	·	·	2	·	·	·	5	18	16	12	2	—	·	·
V	9	1.7	4	1.5	7	2.7	3.5	3.3	5.5	2.3	17	4.1	14	4.1	12	2.2	21	2.3	155	23.4	28	·	·	2	·	·	·	·	14	21	19	6	—	·	4
VI	3.5	3.6	2	2.0	1	1.0	5	3.0	14.5	4.2	10	5.7	15	3.2	12	3.9	27	2.7	140	46.5	11	·	·	·	5	2	·	5	7	16	14	4	—	·	7
VII	·	·	·	·	3	1.7	2.5	1.0	8	3.4	37	3.7	10	2.1	11.5	2.7	21	2.4	69	15.8	18	·	·	·	4	·	·	1	13	17	12	3	—	·	5
VIII	2.5	3.0	1	5.0	3.5	3.3	7.5	4.2	8	6.6	14.5	5.3	12.5	2.8	16.5	3.8	27	3.1	24	9.8	10	·	·	·	7	4	2	·	7	8	4	·	—	·	2
IX	·	·	0.5	1.0	1.5	2.3	14	6.5	22	6.6	16.5	5.4	9	2.6	4.5	4.3	22	4.1	35	11.2	4	·	·	·	2	4	1	2	5	9	7	1	—	·	·
X	9.5	2.9	2	3.5	4.5	3.7	6.5	4.1	5.5	4.5	19.5	5.5	4	2.5	14.5	2.7	27	2.8	1	0.4	8	·	·	7	·	·	·	1	7	3	·	·	—	·	·
XI	7.5	3.0	3	5.7	0.5	5.0	10.5	2.8	11.5	5.3	21.5	6.5	7	4.9	12.5	3.0	16	3.8	20	8.0	11	2	8	20	·	6	1	·	21	13	7	·	—	10	·
XII	·	·	1.5	3.0	2.5	4.6	3.5	5.7	10.5	6.0	47	7.1	9	3.4	10	3.5	9	5.4	17	5.6	13	1	1	22	·	8	2	1	11	9	5	·	—	7	·
Rok	68	2.2	17.5	2.2	32.5	2.3	59	3.1	132	4.6	217	5.1	106.5	3.1	116.5	3.4	346	2.9	654	46.5	11.VI	20	35	124	18	30	6	30	138	153	108	17	—	94	18

Goszyce $H_s = 260$ m $h_w = 14,5$ m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	3	3.0	5	2.6	11	2.0	5.5	2.6	9.5	2.7	12.5	3.0	14.5	2.6	9	2.7	23	2.0	55	13.2	31	4	10	26	·	1	·	1	13	13	10	2	3	31	·
II	10.5	1.9	7	2.6	3	4.3	·	·	6.5	2.4	8.5	4.3	24.5	3.8	11	4.5	13	2.9	22	5.9	17	11	23	27	·	2	·	2	12	18	6	·	1	28	·
III	·	·	7	1.6	16.5	2.5	17	1.9	5.5	2.0	2	2.0	11	3.4	7	4.9	27	1.8	34	8.1	6	4	5	21	·	1	·	7	10	14	10	·	2	20	·
IV	8	2.9	1.5	4.3	33.5	4.2	4	3.9	7	2.2	1	4.0	10.5	3.4	5.5	3.4	19	2.9	33	8.3	20	·	·	7	·	1	·	3	14	13	10	·	·	·	2
V	10.5	2.2	·	·	14	3.5	4.5	1.7	7.5	2.1	3.5	1.9	18	2.6	20	3.0	15	2.2	109	21.0	11	·	·	3	1	·	·	4	12	20	15	3	·	·	6
VI	6	3.1	6	3.2	11	3.1	4.5	2.4	11	2.5	6	1.9	15.5	3.0	18	2.7	12	2.4	105	21.3	6	·	·	·	7	·	·	7	9	12	10	3	1	·	3
VII	3.5	2.1	4.5	1.7	14	2.8	1	2.5	14	2.0	16	2.1	22.5	2.2	5.5	1.9	12	1.9	65	31.1	18	·	·	·	8	·	·	3	7	15	12	1	·	·	1
VIII	6.5	3.5	5	1.9	8	1.9	9.5	2.8	7.5	2.1	6.5	2.3	15.5	2.0	20.5	3.0	14	2.1	133	56.9	25	·	·	·	7	·	·	5	10	15	10	3	·	·	1
IX	·	·	2	2.5	4.5	3.1	11	4.1	21	2.3	8	2.8	13.5	2.6	7	1.9	23	2.0	81	19.6	29	·	·	·	3	·	·	9	2	12	7	3	6	·	1
X	5	2.2	5	1.8	17	2.2	·	·	3.5	2.0	9.5	2.3	15	2.7	6	2.5	32	1.5	3	1.9	8	·	·	8	·	·	·	10	7	4	1	·	4	·	·
XI	2.5	1.6	12.5	2.8	13.5	2.4	3	3.2	5	3.2	12	4.6	15.5	2.6	3	2.3	23	2.2	27	7.5	21	4	11	23	·	1	·	3	13	15	10	·	3	16	·
XII	2.5	4.0	·	·	8.5	2.6	9.5	2.2	15	3.7	21	3.6	11	2.9	4.5	3.8	21	2.5	28	8.2	3	·	2	21	·	·	·	2	15	14	6	·	·	7	·
Rok	58	2.2	55.5	2.1	154.5	2.9	69.5	2.3	113	2.4	106.5	2.9	187	2.8	117	3.0	234	2.2	695	56.9	25.VIII	23	51	136	26	6	·	56	124	165	107	15	20	102	14

Horyniec — φ = 50°11' — λ = 23°21' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	−6.8	10.1	30	−23.3	11	−3.9	−0.4	−3.4	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.1	7.5	8.0
II	–	–	–	–	−3.9	−12.9	1.8	14	−29.8	7	−8.7	−4.5	−8.9	−7.8	–	–	–	–	–	–	–	–	–	–	–	–	9.6	8.4	5.5	7.8
III	–	–	–	–	5.3	−5.0	15.6	30	−23.4	1	−2.8	4.1	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.3	6.3	6.7
IV	–	–	–	–	10.2	1.6	16.1	26	−2.7	3	3.9	8.6	4.8	5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.9	6.0	7.5
V	–	–	–	–	15.7	5.2	27.2	19	−4.6	4	9.2	14.0	9.5	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.4	7.4	7.7
VI	–	–	–	–	21.2	10.4	29.2	26	3.4	8	14.9	19.6	14.2	15.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.9	5.6	6.1
VII	–	–	–	–	21.8	10.5	28.4	16	4.5	12	15.5	20.4	14.7	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.7	5.8	6.4
VIII	–	–	–	–	20.7	9.0	29.3	8	3.9	31	13.1	19.1	12.9	14.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	4.9	6.1
IX	–	–	–	–	20.8	7.0	27.2	2	2.0	17, 22	11.2	19.5	11.9	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.2	2.4	4.6
X	–	–	–	–	12.1	0.0	22.7	1	−5.1	14	3.0	11.3	4.9	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.2	4.2	5.8
XI	–	–	–	–	2.3	−4.4	14.0	2	−20.0	18	−1.8	1.0	−1.6	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.5	7.5	8.4
XII	–	–	–	–	2.4	−3.3	9.7	10	−22.8	17	−0.5	1.5	−0.6	0.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	7.5	8.2
Rok	–	–	–	–	10.8	0.9	29.3	8, VIII	−29.8	7. II	4.4	9.5	4.9	5.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	5.9	7.0

Trzebinia — φ = 50°10' — λ = 19°28'

I	–	–	–	–	1.6	−3.6	8.1	29	−10.5	7, 8	−1.5	0.5	−0.8	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−2.9	−9.3	2.7	14	−21.0	6	−7.2	−4.0	−6.4	−6.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	6.0	−1.4	16.1	30	−10.6	11	0.7	4.9	1.7	2.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	10.5	2.7	15.3	3	−1.9	2	5.1	9.2	5.8	6.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.8	6.4	26.6	19	−1.6	3	9.8	13.2	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	21.0	10.7	32.2	26	4.5	3	15.5	19.3	14.6	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.3	12.4	29.6	14	5.7	6	15.7	19.6	15.5	16.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.1	11.2	30.8	7	6.6	3	15.0	19.5	14.8	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.0	10.2	28.2	3	5.1	22	13.7	19.2	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	13.1	3.5	21.1	2	−4.0	22	6.0	12.2	7.0	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	3.2	−3.1	13.8	2	−14.5	18	−0.9	1.7	−0.6	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	3.4	−1.5	10.3	20	−9.2	15	0.4	2.2	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.2	3.2	32.2	26. VI	−21.0	6. II	6.0	9.8	6.3	7.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biały Kościół — φ = 50°10' — λ = 19°50'

I	–	–	–	–	0.8	−3.9	6.8	29	−11.1	8	−2.4	−0.1	−1.8	−1.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.7	6.5	7.3
II	–	–	–	–	−3.4	−9.1	1.6	12	−19.6	6	−7.5	−4.7	−6.7	−6.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.2	7.6	7.6
III	–	–	–	–	4.7	−1.9	14.3	30	−10.2	1	−0.2	3.5	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.9	6.1	6.4
IV	–	–	–	–	9.3	2.3	14.9	7	−2.3	1	3.9	8.1	5.2	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.3	7.7	7.3
V	–	–	–	–	13.8	6.1	24.5	19	−1.1	2	8.7	12.6	9.2	9.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.2	6.9	6.8
VI	–	–	–	–	20.1	11.2	30.7	26	5.0	3	14.4	18.9	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.1	6.6	5.5
VII	–	–	–	–	20.3	12.2	26.8	14	6.8	6	14.9	19.0	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.3	6.6	6.3
VIII	–	–	–	–	19.8	11.1	30.3	7	7.4	31	13.5	18.3	14.1	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.9	5.5	5.7
IX	–	–	–	–	19.9	10.2	26.8	3	7.1	22	12.4	18.0	13.4	14.3	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.3	4.5	4.8
X	–	–	–	–	11.7	4.1	19.3	1, 2	−3.3	22	5.3	11.0	6.8	7.5	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.6	4.2	4.8
XI	–	–	–	–	2.1	−3.6	12.5	2	−14.9	18	−1.8	0.9	−1.0	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.4	7.5	7.7
XII	–	–	–	–	2.4	−2.1	8.5	19	−9.9	15	−0.6	1.4	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.6	7.8	8.4
Rok					10.1	3.0	30.7	26. VI	−19.6	6. II	5.0	8.9	5.8	6.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	6.5	6.5

Garlica Murowana — φ = 50°09' — λ = 19°56'

I	–	–	–	–	1.6	−4.5	6.8	29	−12.8	8	−2.5	0.4	−1.6	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	6.5	7.4
II	–	–	–	–	−2.8	−10.2	3.5	14	−23.3	6	−7.4	−4.0	−6.7	−6.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.2	6.8	7.7
III	–	–	–	–	5.5	−3.4	15.1	30	−16.9	1	−1.6	4.5	0.4	0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.4	5.3	6.5
IV	–	–	–	–	10.2	2.2	15.4	7	−1.3	1	3.8	9.1	5.6	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	6.2	7.0
V	–	–	–	–	14.8	6.1	26.9	19	−1.9	3	8.8	13.7	9.7	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	6.3	7.2
VI	–	–	–	–	20.8	10.5	30.6	26	3.5	3	14.6	19.7	14.6	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.9	6.0	5.8
VII	–	–	–	–	21.0	11.2	28.4	14	5.6	10	14.7	19.5	15.6	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.6	6.2	6.8
VIII	–	–	–	–	20.5	10.2	31.4	7	6.0	29	13.0	19.5	14.3	15.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.3	6.3	6.7
IX	–	–	–	–	20.2	8.1	26.4	3	3.6	22, 23	11.4	18.8	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.0	4.0	4.8
X	–	–	–	–	12.5	2.6	20.1	2	−3.9	22	4.1	11.7	6.2	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	4.9	4.5	5.3
XI	–	–	–	–	2.8	−3.6	13.9	2	−17.4	18	−2.0	1.3	−1.0	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.0	5.5	7.0
XII	–	–	–	–	3.5	−1.9	9.5	19	−10.3	15	−0.4	2.0	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.6	6.5	7.1
Rok	–	–	–	–	10.9	2.3	31.4	7. VIII	−23.3	6. II	4.7	9.7	5.9	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.7	5.8	6.6

Horyniec $H_s = 240\ m$ $h_w = 15\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2	2.0	2	2.0	13	1.8	13.5	2.7	13.5	2.4	6.5	5.1	10	6.0	2.5	3.4	30	2.2	53	14.3	31	7	11	30	·	1	·	4	21	13	11	1	1	31	—
II	4	2.1	9.5	2.2	3.5	2.0	·	·	4.5	4.7	9	4.6	26.5	3.9	7	4.2	20	2.8	30	3.6	8	18	24	28	·	1	·	·	13	22	12	·	3	28	—
III	0.5	6.0	3	2.5	8	2.8	12	2.4	9.5	2.5	4	2.2	13	2.8	5	3.2	38	1.6	41	9.1	26	9	4	24	·	·	·	2	12	16	10	·	7	27	—
IV	4.5	2.0	3.5	2.0	32.5	3.5	17.5	2.5	4.5	2.6	5.5	3.0	5.5	3.5	3.5	3.6	13	2.6	41	11.5	22	·	·	9	·	·	·	·	13	13	7	2	1	·	—
V	6.5	1.9	5	2.2	15.5	2.3	5	1.4	5	1.6	8.5	2.8	9.5	2.7	13	2.1	25	1.6	51	8.3	25	·	·	4	1	·	·	1	15	20	15	·	·	·	—
VI	4.5	1.2	·	·	10	1.7	5	2.8	4	3.5	5.5	1.9	17.5	2.5	8.5	2.7	35	1.4	118	36.4	15	·	·	·	6	·	·	2	8	15	13	4	1	·	—
VII	0.5	1.0	3.5	1.3	7.5	1.7	4	2.5	7	2.4	10.5	2.3	18.5	2.3	1.5	2.3	40	1.2	155	49.5	17	·	·	·	7	·	·	2	6	20	14	5	·	·	—
VIII	2.5	1.0	5	1.6	1	3.0	3.5	1.1	9	1.9	4.5	2.0	23	2.3	5.5	1.5	39	1.1	101	29.0	11	·	·	·	9	·	·	3	12	12	10	4	2	·	—
IX	0.5	1.0	·	·	1.5	1.3	14.5	1.4	10	2.2	4.5	1.3	9	2.0	2	1.8	47	0.8	45	22.5	11	·	·	·	5	·	·	6	2	7	6	2	3	·	—
X	2.5	1.2	4	1.2	6.5	1.0	1	1.0	1.5	1.0	1.5	2.3	20.5	2.7	5.5	1.6	50	0.9	8	4.8	31	·	·	17	·	·	·	4	8	7	2	·	6	·	—
XI	3	1.3	7	2.5	8	1.8	9	2.2	1	1.7	8.5	3.0	19	3.4	2.5	1.0	32	1.7	76	21.4	21	3	11	24	·	1	·	·	20	16	11	2	2	11	—
XII	5	1.0	·	·	2.5	1.6	18.5	1.6	12.5	1.4	17	1.9	11.5	2.0	3	1.0	23	1.2	48	12.8	18	3	7	24	·	·	·	1	20	21	14	1	·	6	—
Rok	36	1.8	42.5	1.5	109.5	2.0	103.5	1.8	82	2.3	85.5	2.7	183.5	3.0	59.5	2.4	392	1.6	767	49.5	17. VII	40	57	160	28	3	·	25	150	182	125	21	26	103	—

Trzebinia $H_s = 320\ m$ $h_w = 14{,}9\ m$

I	4	7.0	4	2.6	21	1.8	7	2.0	5	1.6	12.5	2.3	16.5	2.1	13	2.6	10	2.1	57	9.9	9, 31	2	8	27	·	1	1	—	—	15	11	·	—	31	·
II	9.5	2.8	6.5	2.7	5.5	2.3	1	2.0	·	·	12	4.8	28.5	2.5	18	2.9	3	2.9	27	4.3	17	10	24	28	·	2	·	—	—	22	9	·	—	28	·
III	7.5	2.9	8	2.3	15.5	2.7	7.5	2.5	0.5	1.0	13	4.8	9	3.6	10	2.5	22	2.4	28	8.2	21	1	5	18	·	4	1	—	—	$16^{?}$	8	·	—	14	·
IV	6.5	3.8	7.5	2.6	26	3.6	11	1.9	1	1.0	9	2.3	12	2.2	5	3.4	12	2.5	54	12.0	23	·	·	3	·	1	·	—	—	13	9	1	—	·	2
V	9	2.8	3.5	2.0	19	4.0	4	2.2	4	2.9	16.5	3.1	14.5	2.0	15.5	2.4	7	2.6	116	19.5	29	·	·	3	1	1	1	—	—	21	17	3	—	·	5
VI	9	1.8	7.5	1.7	14.5	2.5	5.5	1.8	2	1.0	14	2.6	14	2.3	15.5	2.9	8	2.1	150	41.2	27	·	·	·	6	·	·	—	—	14	13	4	—	·	3
VII	3	1.5	5	1.4	13.5	1.9	2	2.0	6.5	1.4	32	1.7	21.5	1.9	8.5	1.5	1	1.7	68	14.5	8	·	·	·	8	·	·	—	—	19	15	2	—	·	2
VIII	4.5	2.2	5.5	1.8	14	1.8	10	1.6	2	1.0	13.5	1.5	14.5	1.5	17	2.2	12	1.5	119	31.5	25	·	·	·	7	·	·	—	—	12	11	4	—	·	1
IX	2.5	1.8	2	1.5	17	2.0	15.5	1.8	9	2.1	16	2.0	11.5	2.2	6.5	1.8	10	1.8	95	24.4	28	·	·	·	3	·	·	—	—	12	10	3	—	·	1
X	5.5	1.4	9	1.7	17.5	2.0	4.5	1.8	·	·	12.5	1.6	14.5	1.7	10.5	3.2	19	1.5	1	0.8	16	·	·	5	·	1	·	—	—	1	·	·	—	·	·
XI	7	1.7	10.5	3.4	15	3.8	7	3.0	1.5	1.7	17	4.4	12	1.9	6	2.2	14	2.7	25	5.9	21	3	10	21	·	4	1	—	—	$17^{?}$	$8^{?}$	·	—	16	·
XII	4.5	1.9	0.5	2.0	9	1.9	9.5	1.7	4.5	4.2	34	3.4	13.5	2.4	7.5	1.9	10	2.4	45	13.4	18	·	3	21	·	3	·	—	—	$18^{?}$	10	1	—	7	·
Rok	72.5	2.6	69.5	2.1	187.5	2.5	84.5	2.0	36	1.5	202	2.9	182	2.2	133	2.5	128	2.2	785	41.2	27. VI	16	50	126	25	17	4	—	—	$180^{?}$	121	18	—	96	14

Biały Kościół $H_s = 400\ m$ $h_w = 18{,}5\ m$

I	·	·	·	·	13	1.0	15	1.2	2	1.0	8	1.0	35	2.1	5	1.0	15	1.3	75	13.6	17	1	11	28	·	·	·	3	13	16	12	4	3	31	·
II	4.5	1.9	4.5	1.3	2.5	1.2	·	·	·	·	6.5	3.5	39.5	1.6	19.5	1.7	7	1.7	44	7.3	17	8	24	28	·	·	·	2	16	24	13	·	1	28	·
III	·	·	·	·	9	1.6	8	1.0	9	1.0	11.5	1.5	8.5	2.8	10	1.8	37	1.0	32	8.7	27	1	5	17	·	·	·	6	12	11	7	·	4	18	·
IV	3	1.0	7	1.3	30.5	2.0	7	1.0	5.5	1.0	11	1.0	10	1.9	4	1.0	12	1.3	38	6.2	18	·	·	5	·	·	·	2	16	13	10	·	4	·	2
V	6.5	1.1	9.5	1.1	12	1.7	4	1.0	2	1.0	23	1.3	18	1.7	9	1.1	9	1.2	110	19.6	19	·	·	2	·	1	1	·	13	21	17	3	·	·	4
VI	3	1.0	5.5	1.2	16.5	1.6	5.5	1.0	5.5	1.0	17.5	1.5	16.5	1.5	15	1.5	5	1.4	164	66.0	27	·	·	·	5	2	2	3	10	13	12	6	·	·	3
VII	·	·	5.5	1.0	8	1.4	7.5	1.1	4.5	1.4	26	1.1	32.5	1.2	3	1.0	6	1.1	48	15.6	18	·	·	·	4	·	·	2	9	15	11	1	·	·	1
VIII	6	1.0	3	1.0	4	1.0	17	1.1	5	1.0	13	1.1	20	1.2	15	1.0	10	1.0	118	31.1	1	·	·	·	5	·	·	5	9	16	12	3	2	·	1
IX	·	·	·	·	3	1.3	13	1.2	8	1.0	10.5	1.2	17.5	1.1	2	1.0	36	0.7	73	17.6	4	·	·	·	1	·	·	7	4	12	8	4	1	·	1
X	4	1.0	6	1.2	16	1.0	1	1.0	2	1.0	7	1.0	23	1.3	8	1.1	26	0.8	0	0.0	16	·	·	3	·	·	·	11	7	·	·	·	7	·	·
XI	·	·	10.5	1.0	15.5	1.4	2	1.0	2	1.0	6	4.7	29.5	2.6	8.5	1.1	16	1.7	30	6.8	11	5	10	21	·	2	·	1	17	17	11	·	4	$16^{?}$	·
XII	2	2.0	·	·	5	1.6	12	1.3	3	1.7	52	1.9	15	2.0	3	1.0	1	1.8	36	9.8	18	·	6	23	·	·	·	·	21	17	11	·	·	10	·
Rok	29	0.8	51.5	0.8	135	1.4	92	1.0	48.5	1.0	192	1.7	205	1.8	102	1.2	190	1.2	768	65.0	27. VI	15	56	127	15	5	3	42	147	175	124	21	26	103	12

Garlica Murowana $H_s = 270\ m$ $h_w = 15{,}9\ m$

I	7.5	2.6	6	3.3	7	2.0	·	·	2	2.0	11	4.2	6.5	3.2	3	4.3	50	1.5	50	14.2	17	2	10	28	·	·	·	1	14	9	9	2	1	24	—
II	2	3.5	·	·	·	·	·	·	·	·	27.5	3.9	20	3.8	10.5	6.7	24	3.1	22	4.3	27	11	24	28	·	1	·	3	17	10	8	·	·	28	—
III	4.5	3.0	8.5	4.0	8.5	3.3	3.5	2.0	·	·	6.5	3.5	6	2.6	8.5	1.8	47	1.5	58	17.2	3	4	6	21	·	·	·	4	10	8	8	3	2	18	—
IV	4	3.5	14.5	3.0	25	4.9	9.5	2.5	·	·	6	4.2	10.5	3.6	7.5	3.1	13	3.2	33	8.0	13	·	·	6	·	·	·	2	16	12	10	·	1	·	—
V	9	5.2	4	3.5	10	3.2	3	1.5	2.5	3.0	9.5	3.0	13.5	3.7	6.5	2.8	35	2.2	126	25.6	19	·	·	3	1	·	·	1	11	15	14	4	1	·	—
VI	4	3.8	15	2.7	4	2.6	6	2.9	4	1.0	7	3.1	17	3.2	5	3.6	28	2.0	152	44.7	27	·	·	·	5	·	·	2	8	15	15	4	1	·	—
VII	3	2.0	2	1.5	10.5	2.3	2	3.0	4	2.4	11	2.5	25	2.6	2.5	2.0	33	1.6	56	8.1	17	·	·	·	7	·	·	1	11	18	16	·	·	·	—
VIII	8	3.1	4.5	2.2	4	2.8	3	2.3	1	2.0	2	1.0	9	2.8	10.5	2.4	51	1.2	117	28.2	1	·	·	·	6	·	·	3	14	12	12	4	1	·	—
IX	·	·	2	1.5	7.5	2.4	8.5	2.3	4	2.4	6.5	2.0	5.5	2.5	2	2.5	54	0.9	77	16.7	4	·	·	·	3	·	·	5	5	12	9	4	·	·	—
X	4	3.0	10	1.7	7	2.4	·	·	3	2.0	10	2.3	5	2.7	6	2.4	48	1.1	1	0.8	31	·	·	11	·	·	·	6	6	2	·	·	3	·	—
XI	1	3.0	12	3.7	3.5	4.9	4.5	2.4	2	2.5	13	2.8	11	4.3	5	3.8	38	2.0	22	8.2	20	4	11	20	·	·	·	1	13	10	7	·	3	10	—
XII	8	2.6	1.5	2.0	6	1.8	1.5	1.3	4	1.9	13	3.7	11.5	3.0	0.5	4.0	47	1.4	25	10.1	3	1	5	22	·	·	·	1	14	9	5	1	1	7	—
Rok	55	2.9	80	2.4	93	2.7	41.5	1.7	26.5	1.6	123	3.0	140.5	3.2	67.5	3.3	468	1.8	739	44.7	27. VI	22	56	139	22	1	·	30	139	132	113	22	14	87	—

Lubaczów — φ = 50°09' — λ = 23°08' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.3	-6.0	6.5	30	-20.2	11	-3.6	-0.9	-2.8	-2.5	4.6	5.0	4.9	4.8	92	84	92	89	0.3	0.9	0.4	0.5	8.4	8.0	7.6	8.0
II	—	—	—	—	-3.0	-13.1	1.9	14	-27.7	8	-8.4	-3.9	-8.4	-7.3	3.2	3.9	3.2	3.4	90	81	89	87	0.3	0.8	0.3	0.5	9.6	8.3	6.8	8.2
III	—	—	—	—	5.5	-4.7	16.4	30	-24.2	1	-2.9	4.3	0.4	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.0	7.1	7.4
IV	—	—	—	—	10.6	2.0	16.7	7	-4.0	11	4.1	9.0	5.3	5.9	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.3	5.6	7.5
V	—	—	—	—	15.9	5.8	27.0	19	-3.5	3	9.1	14.0	10.2	10.9	10.6	11.0	11.4	11.0	89	69	89	82	1.4	5.6	1.5	2.8	7.2	8.4	7.8	7.8
VI	—	—	—	—	21.6	11.1	29.4	26	4.6	8	14.7	19.9	15.3	16.3	15.0	15.0	15.8	15.3	89	65	90	81	1.9	8.9	1.8	4.2	6.6	7.7	7.4	7.2
VII	—	—	—	—	22.1	11.6	29.5	16	5.9	12	15.3	20.8	15.6	16.8	15.8	16.1	16.0	16.0	90	65	89	81	1.9	9.2	2.0	4.4	6.1	7.4	6.4	6.6
VIII	—	—	—	—	20.9	10.1	29.5	8	5.4	31	12.7	19.3	13.7	14.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.0	4.5	6.2
IX	—	—	—	—	21.2	7.9	26.4	3, 4, 11	2.2	22	10.5	19.8	12.5	13.8	12.4	14.8	13.7	13.6	96	64	93	84	0.6	8.9	1.1	3.5	5.5	5.9	2.7	4.7
X	—	—	—	—	12.6	1.1	23.2	1	-4.0	22	3.2	11.7	5.3	6.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.6	4.5	5.9
XI	—	—	—	—	2.7	-4.0	14.8	2	-21.7	18	-1.6	1.4	-1.4	-0.8	5.3	5.9	5.3	5.5	91	85	91	89	0.6	1.4	0.6	0.9	9.1	8.6	8.0	8.6
XII	—	—	—	—	2.8	-2.9	9.2	10, 11	-21.7	17	-0.4	1.8	-0.3	0.2	5.6	6.1	5.7	5.8	91	86	91	89	0.5	1.0	0.6	0.7	8.6	8.0	7.7	8.1
Rok	—	—	—	—	11.1	1.6	29.5	16.VII, 8.VIII	-27.7	8. II	4.4	9.8	5.4	6.2	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.6	6.3	7.2

Tychy — φ = 50°08' — λ = 18°59'

I	—	—	—	—	2.1	-4.2	8.8	29	-16.0	8	-2.1	0.9	-1.2	-0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.8	7.5	7.9
II	—	—	—	—	-1.9	-9.3	2.8	14	-21.1	6	-7.4	-3.3	-5.8	-5.6	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.3	7.9	8.0
III	—	—	—	—	6.6	-2.6	16.6	30	-15.9	11	-1.7	5.1	1.9	1.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.6	4.9	6.5
IV	—	—	—	—	11.0	2.3	16.0	4	-1.6	2	3.8	9.8	6.3	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.6	6.7	7.3
V	—	—	—	—	15.4	6.2	26.6	19	-1.6	3, 4	8.6	13.8	10.6	10.9	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.0	7.8	7.9
VI	—	—	—	—	21.5	10.6	32.2	26	5.0	3	13.9	19.5	15.6	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.5	5.4	5.8
VII	—	—	—	—	21.5	11.7	30.2	14, 15	5.9	5	14.6	19.9	15.6	16.4	—	—	—	—	—	—	—	—	—	—	—	—	7.0	8.1	5.1	6.7
VIII	—	—	—	—	21.4	10.1	31.2	8	5.9	3	12.3	19.9	14.5	15.3	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.5	6.4	6.5
IX	—	—	—	—	21.2	8.3	28.5	3	2.0	22	10.1	19.4	13.6	14.2	—	—	—	—	—	—	—	—	—	—	—	—	4.9	5.2	6.4	5.5
X	—	—	—	—	13.3	2.1	22.7	2	-5.5	22	3.5	12.3	6.0	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.5	3.8	4.0	5.1
XI	—	—	—	—	3.7	-3.5	13.5	2	-15.9	18	-1.7	2.1	-0.4	-0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.1	9.0	8.3
XII	—	—	—	—	3.6	-1.1	10.5	20	-8.6	15	0.3	2.4	1.0	1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.6	8.9	8.4
Rok	—	—	—	—	11.6	2.6	32.2	26. VI	-21.1	6. II	4.5	10.2	6.5	6.9	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.8	6.7	7.0

Rybnik — φ = 50°06' — λ = 18°33'

I	—	—	—	—	2.3	-2.9	7.2	29	-9.3	8	-1.2	1.4	-0.6	-0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.2	7.4	8.2
II	—	—	—	—	-1.8	-8.3	3.7	14	-18.9	10	-6.2	-2.9	-5.0	-4.8	—	—	—	—	—	—	—	—	—	—	—	—	9.2	7.6	7.9	8.2
III	—	—	—	—	6.9	-1.7	17.3	30	-12.8	1	-0.4	5.8	2.6	2.6	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.6	6.1	6.9
IV	—	—	—	—	11.2	3.1	17.6	5	-1.7	16	4.6	9.8	6.7	7.0	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.6	6.6	7.6
V	—	—	—	—	15.1	6.9	24.3	19	-1.0	3	9.2	13.7	11.0	11.2	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.8	8.4	8.1
VI	—	—	—	—	21.4	11.6	32.1	26	6.1	3	14.8	19.2	16.0	16.5	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.8	7.6	6.7
VII	—	—	—	—	21.5	12.7	30.7	15	7.2	5, 6	15.3	19.7	16.2	16.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.8	7.8	7.7
VIII	—	—	—	—	21.3	11.5	30.9	7	7.2	14, 17, 31	13.6	19.8	15.7	16.2	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.0	6.5	6.8
IX	—	—	—	—	20.9	10.1	28.2	3	4.8	22	12.2	19.3	14.4	15.1	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.0	5.4	5.8
X	—	—	—	—	13.4	4.0	23.8	2	-4.4	23	5.1	12.4	7.2	8.0	—	—	—	—	—	—	—	—	—	—	—	—	7.8	5.7	3.5	5.7
XI	—	—	—	—	3.8	-2.0	13.6	1	-12.5	18	-0.5	2.5	0.4	0.7	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.8	7.7	8.1
XII	—	—	—	—	3.6	-0.7	9.8	20	-7.8	15	0.9	2.8	1.2	1.5	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.4	7.9	8.5
Rok	—	—	—	—	11.6	3.7	32.1	26. VI	-18.9	10. II	5.6	10.3	7.2	7.6	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.3	6.9	7.4

Rzeszów - Jasionka — φ = 50°06' — λ = 22°03'

I	988.9	1004.5	965.0	1014.4	1.0	-5.6	5.9	30	-17.3	11, 12	-2.5	-0.5	-2.3	-1.9	4.5	4.9	4.6	4.7	86	81	86	84	0.8	1.2	0.7	0.9	7.5	8.1	7.7	7.8
II	990.9	1005.8	967.9	1016.9	-3.1	-12.9	1.0	12	-28.7	7	-8.0	-4.5	-8.4	-7.3	3.2	3.6	3.0	3.3	88	81	86	85	0.4	0.8	0.4	0.5	8.6	7.8	6.8	7.7
III	993.3	1008.8	964.7	1018.6	5.9	-3.9	16.3	30	-23.2	1	-1.6	4.8	0.6	1.1	5.2	5.9	5.7	5.6	90	68	86	81	0.5	3.1	1.0	1.5	7.2	6.5	6.4	6.7
IV	986.9	1003.2	969.3	1011.6	10.9	2.2	16.5	26	-1.2	6	3.9	9.3	5.9	6.2	7.4	7.6	7.7	7.6	90	64	81	78	0.8	4.5	1.8	2.4	7.9	8.6	6.8	7.8
V	989.8	1004.9	979.3	1014.1	15.9	5.8	26.5	19	-3.6	4	8.9	14.2	9.8	10.7	10.2	10.3	11.0	10.5	87	62	88	79	1.6	6.6	1.5	3.2	6.8	8.1	7.1	7.3
VI	990.6	998.0	978.5	1014.5	21.6	10.9	31.0	26	5.4	8	14.6	19.9	15.4	16.3	14.5	14.2	15.5	14.7	87	62	88	79	2.3	9.7	2.3	4.8	5.6	6.6	6.5	6.2
VII	989.8	997.1	979.5	1013.6	21.8	11.6	28.4	16, 17	5.3	12	15.2	20.0	15.7	16.6	15.6	15.4	16.0	15.7	89	66	89	81	2.0	8.8	2.1	4.3	5.4	7.0	5.6	6.0
VIII	992.4	1000.5	975.7	1016.3	20.8	10.8	29.1	8	5.7	17	13.0	19.3	14.1	15.1	14.0	14.0	14.6	14.2	93	64	90	82	1.2	9.3	1.8	4.1	5.9	6.3	5.3	5.8
IX	993.4	1009.6	982.8	1017.5	21.0	8.5	25.8	2	3.7	17, 30	11.8	19.7	12.8	14.3	12.6	13.7	13.6	13.3	91	60	91	81	1.5	9.7	1.5	4.2	4.8	5.4	2.9	4.4
X	999.4	1012.4	988.9	1024.3	11.9	1.8	21.4	1	-6.4	22	4.5	10.8	6.0	6.8	8.0	8.9	8.4	8.4	92	68	87	82	0.7	4.5	1.4	2.2	7.0	7.1	4.3	6.1
XI	988.7	1006.4	965.1	1014.0	3.0	-3.7	14.1	2	-21.0	18	-1.4	1.1	-0.5	-0.3	5.1	5.6	5.4	5.4	87	80	87	85	0.8	1.6	0.9	1.1	8.9	8.5	7.4	8.3
XII	984.7	999.6	965.3	1009.8	2.7	-2.5	7.4	21	-20.2	16	-0.1	1.6	0.1	0.4	5.3	5.5	5.5	5.4	86	79	87	84	0.9	1.5	0.9	1.1	8.6	8.2	7.4	8.1
Rok	990.7	1012.4	964.7	1015.5	11.1	1.9	31.0	26. VI	-28.7	7. II	4.9	9.6	5.8	6.5	8.8	9.1	9.2	9.0	89	70	87	82	1.4	5.1	1.4	2.5	7.0	7.4	6.2	6.9

Lubaczów $H_s = 214$ m $h_w = 16$ m 1965

MIESIĄC	ROZKŁAD WIATRU nD, VmD — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V: V ≥ 10	V ≥ 15	◔	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	5	1.8	5	1.6	4	2.2	27	2.6	13	1.3	13	1.2	14	2.8	6	6.3	6	2.2	51	17.0	31	7	12	27	·	·	·	3	22	15	11	1	2	31	·
II	8	1.9	12	1.7	4	1.5	1	1.0	·	·	5	4.2	28	3.0	19	2.4	7	2.3	38	7.6	16	17	22	28	·	1	·	·	16	17	12	·	1	28	·
III	2	2.5	6	1.3	10	1.5	19	1.8	12	1.8	12	1.3	18	1.7	11	2.0	3	1.6	47	9.5	3	8	4	21	·	·	·	1	16	15	11	·	·	18	·
IV	7	2.3	4	1.5	17	3.9	28	4.3	9	1.8	7	1.6	10	1.7	6	1.5	2	2.9	45	12.2	22	·	·	9	·	1	·	·	14	14	9	2	·	·	1
V	19	1.4	2	4.0	8	2.6	14	2.5	6	1.3	4	2.0	16	2.1	20	2.0	4	1.9	64	9.8	25	·	·	4	1	·	·	·	15	22	18	·	1	·	2
VI	6	1.2	3	1.3	7	1.4	7	1.9	7	2.4	6	1.2	25	1.9	24	2.0	5	1.7	75	14.2	28	·	·	·	6	·	·	·	8	17	13	3	1	·	4
VII	2	1.0	1	1.0	9	1.4	8	1.2	9	2.1	17	2.0	28	1.7	12	2.2	7	1.6	152	29.3	21	·	·	·	7	·	·	1	11	22	18	6	·	·	4
VIII	9	1.8	3	1.0	2	2.0	10	1.7	6	1.5	10	1.5	29	2.0	15	2.0	9	1.6	100	27.5	11	·	·	·	9	·	·	3	12	10	7	5	2	·	2
IX	·	·	1	1.0	4	1.0	14.5	1.8	16	1.6	13	1.7	16.5	1.5	12	1.6	13	1.4	46	25.3	11	·	·	·	5	·	·	6	1	9	7	1	1	·	·
X	4	2.2	4	1.8	5	1.2	11	1.3	4	1.5	9	1.7	25	1.9	16	2.3	15	1.5	10	6.0	31	·	·	15	·	·	·	3	7	8	3	·	2	·	·
XI	4	1.2	9.5	1.3	7.5	3.1	13	2.0	7	3.6	8	2.4	21	2.4	7	1.4	13	1.9	85	22.0	21	3	11	24	·	·	·	·	20	16	11	2	1	16	·
XII	3	1.7	3	1.3	0.5	2.0	16	2.2	11.5	2.5	31	1.9	14	1.6	8	1.8	6	1.8	50	7.9	18	3	5	23	·	·	·	·	19	22	15	·	·	8	·
Rok	69	1.6	53.5	1.6	78	2.0	168.5	2.0	100.5	1.8	135	1.9	244.5	2.0	156	2.3	90	1.9	763	29.3	21.VII	38	54	151	28	2	·	17	161	187	135	20	11?	101	13

Tychy $H_s = 280$ m $h_w = 16{,}3$ m

I	4	2.5	2	4.0	3	2.3	4	2.5	·	·	19.5	3.5	13.5	3.1	9	3.2	38	1.9	66	14.2	31	2	4	28	·	·	·	1	19	13	12	2	5	30	—
II	9	3.2	6	2.5	1	5.0	1	2.0	·	·	9	5.8	23	3.7	12	4.1	23	2.8	41	7.5	17	9	22	27	·	2	·	1	19	17	13	·	1	28	—
III	2	3.5	7	2.7	3	2.3	4	2.2	2	3.0	6.5	4.8	8.5	3.3	11	3.2	49	1.5	48	13.3	21	3	4	20	·	·	·	3	13	12	9	2	7	15	—
IV	3	2.7	12	2.9	9	4.1	5	2.6	3	2.7	4	3.0	12	3.4	8	3.2	34	2.0	47	7.9	23	·	·	7	·	·	·	3	18	16	12	·	4	·	—
V	5	2.4	6	2.7	7.5	3.2	4.5	3.8	1	3.0	8.5	2.9	11.5	3.0	12	3.3	37	1.8	104	20.0	19	·	·	3	1	·	·	·	13	18	18	2	·	·	—
VI	5	2.2	1	3.0	4	3.0	6	2.7	1	2.0	5	3.0	11	3.5	15	3.1	42	1.6	102	15.4	10	·	·	·	6	·	·	4	7	15	14	3	1	·	—
VII	3	2.3	·	·	4	2.8	3	2.7	1	2.0	13	3.8	22.5	2.8	4.5	2.4	42	1.5	71	10.8	8	·	·	·	6	·	·	2	11	17	13	1	1	·	—
VIII	2	2.0	1	2.0	4	2.0	4	2.5	3	2.7	6	2.8	8	2.4	16	2.9	49	1.2	61	17.6	24	·	·	·	8	·	·	2	11	9	9	3	·	·	—
IX	·	·	·	·	2	3.0	8	3.0	6	3.2	10	3.1	6	2.3	6	2.2	52	1.2	81	19.0	28	·	·	·	3	·	·	6	9	8	8	4	5	·	—
X	3	2.7	3	2.0	7	2.9	2	2.5	·	·	4	4.2	22	2.7	9	2.6	43	1.5	2	1.0	29	·	·	12	·	·	·	5	8	2	1	·	8	·	—
XI	·	·	8	2.9	4	3.0	1	3.0	3	3.7	9.5	4.2	15.5	3.6	6	2.5	43	1.8	35	13.7	11	4	8	23	·	·	·	·	21	9	9	1	8	16	—
XII	1.5	4.0	·	·	7	2.4	1	2.0	3	2.7	29.5	3.5	19.5	2.8	4.5	3.3	27	2.2	50	8.3	18	·	3	18	·	·	·	1	17	14	10	·	1	9	—
Rok	37.5	2.3	46	2.1	55.5	3.0	43.5	2.6	23	2.1	124.5	3.7	173	3.0	113	3.0	479	1.8	708	20.0	19.V	18	41	138	24	2	·	28	166	150	128	18	41	98	—

Rybnik $H_s = 243$ m $h_w =$ 17,2 m I–VI, 17 m VII–XII

I	7.5	1.9	·	·	4	1.5	3.5	1.0	8.5	2.8	24.5	3.1	12	1.8	2	1.0	31	1.6	68	12.9	31	·	5	28	·	·	·	·	17	16	16	2	·	31	·
II	10.5	2.8	4	2.5	1	2.0	2	1.5	4	10.0	24	5.0	18	1.8	9.5	3.4	11	3.2	38	5.0	17	6	22	27	·	4	3	·	19	14	14	·	2	28	·
III	5	1.6	4	2.9	·	·	3.5	1.6	5	3.4	25	3.9	7.5	3.3	5	2.5	38	1.9	34	11.8	21	3	4	19	·	2	1	4	13	12	7	1	3	15	·
IV	4	2.5	15	4.4	4.5	2.2	7.5	1.7	3	6.0	14	3.1	10.5	2.7	5.5	2.2	26	2.2	58	14.5	20	·	·	3	·	·	·	2	19	14	11	2	·	·	2
V	3	2.0	11	3.2	4.5	1.8	3.5	2.3	3	2.3	21	3.4	12	2.3	10	2.4	25	2.0	138	21.1	29	·	·	3	·	·	·	·	19	17	16	6	1	·	6
VI	4	2.8	7.5	2.0	3	2.3	4	2.0	6.5	3.8	19.5	4.9	9.5	2.2	10	3.0	26	2.3	117	22.8	11	·	·	·	6	3	2	1	9	14	14	5	·	·	4
VII	5	2.8	4	1.5	·	·	2	6.0	9.5	3.4	27	3.0	12	2.2	6.5	1.4	27	1.9	71	16.3	8	·	·	·	5	1	·	·	15	18	15	2	1	·	7
VIII	4	2.0	·	·	·	·	1	2.0	4.5	2.7	11	2.9	22.5	1.8	14	2.5	36	1.4	52	13.7	10	·	·	·	8	·	·	2	12	7	7	2	·	·	1
IX	·	·	·	·	·	·	3	2.3	10	3.6	27	3.5	8.5	1.7	9.5	1.4	32	1.8	58	19.9	29	·	·	·	2	2	·	3	6	8	8	3	1	·	·
X	5.5	1.1	8.5	1.5	·	·	·	·	3	1.3	20	2.0	5	2.0	10	1.7	41	1.0	2	1.8	29	·	·	5	·	·	·	4	7	1	1	·	10?	·	·
XI	8.5	1.8	5	2.8	1	3.0	1	1.0	1	1.0	35.5	2.4	4.5	1.0	6.5	1.2	27	1.5	34	14.0	11	3	8	18	·	·	·	1	19	11	4	2	2	15	·
XII	·	·	1	1.0	·	·	3	1.0	3.5	5.9	39	2.8	11.5	1.9	7	1.9	28	1.8	33	6.3	18	·	·	16	·	1	1	·	22	13	9	·	·	7	·
Rok	57	1.8	60	1.8	18	1.1	34	1.9	61.5	3.8	287.5	3.3	133.5	2.1	95.5	2.0	348	1.9	703	22.8	11.VI	12	39	119	21	13	7	17	177	145	122	25	20?	96	20

Rzeszów - Jasionka $H_s = 200$ m $H_b = 201{,}7$ m $h_w = 21$ m

I	8.5	4.1	3	2.8	16.5	5.4	2	3.5	22.5	6.4	18	4.9	10	5.8	8.5	5.2	4	5.1	46	13.4	31	7	9	27	·	8	·	2	19	19	11	1	5	31	·
II	11.5	4.7	3	4.0	1	4.0	·	·	9.5	8.4	12.5	4.9	27	5.7	13.5	5.5	6	5.2	30	6.8	8	18	24	28	·	5	·	1	14	20	12	·	1	28	·
III	4.5	4.0	13.5	3.4	14.5	3.2	2.5	3.2	18	4.7	17.5	3.9	11	3.7	6.5	5.4	5	3.7	42	8.8	17	5	5	20	·	3	·	5	14	16	12	·	3	14	·
IV	5	3.5	11	3.9	36	6.8	4	4.0	8.5	3.5	10	5.2	7.5	4.2	7	5.0	1	5.2	48	12.7	21	·	·	8	·	4	·	1	15	13	10	2	1	1	1
V	11.5	4.0	5.5	3.6	16.5	4.4	2.5	2.2	10	3.4	15	3.4	14	4.5	16	5.1	2	4.0	74	27.2	29	·	·	3	2	5	·	2	14	19	12	1	2	·	5
VI	3	2.8	3.5	3.3	19	3.4	4	1.6	7.5	5.7	13.5	2.6	23	4.0	15.5	4.7	1	3.7	108	27.0	27	·	·	·	6	2	·	1	9	13	11	4	2	·	6
VII	4.5	2.8	3.5	3.4	6	4.4	7.5	2.7	15.5	3.1	25	3.0	18	3.9	5	1.8	8	2.9	130	30.4	18	·	·	·	6	·	·	2	6	22	16	5	·	·	4
VIII	4	5.5	4.5	2.7	10.5	2.5	4.5	2.0	13.5	3.9	14.5	3.0	17	4.0	15.5	5.4	9	3.4	165	37.0	26	·	·	·	7	1	·	6	13	15	13	4	·	·	3
IX	·	·	5	3.2	15.5	2.6	10	2.4	23.5	4.1	11.5	2.8	7	4.5	4.5	4.6	13	2.9	49	17.6	11	·	·	·	2	2	·	8	2	8	5	3	4	·	·
X	7	3.4	6	1.5	10	2.4	1	2.0	7.5	5.1	23.5	3.8	21	4.2	10	3.2	7	3.3	9	3.2	31	·	·	12	·	·	·	4	9	8	3	·	8	·	·
XI	4.5	3.6	9.5	4.8	12	4.9	4.5	3.6	13.5	6.4	21	4.0	14.5	5.2	3.5	4.1	7	4.4	48	11.1	21	5	10	21	·	6	·	·	17	19	11	1	4	10	·
XII	1	4.0	2.5	2.0	8.5	3.4	2.5	3.6	39	6.7	23	5.2	10.5	4.8	6	5.4	·	5.5	34	13.5	18	3	4	22	·	8	·	·	20	18	9	1	3	9	·
Rok	65	3.5	70.5	3.2	166	4.0	45	2.6	188.5	5.1	205	3.9	180.5	4.5	111.5	4.6	63	4.1	783	37.0	26.VIII	38	52	141	23	44	·	32	152	190	125	22	33	93	19

Uwaga: Kierunki i prędkości wiatru — wg anemometru M-47.

Racibórz — φ = 50°05' — λ = 18°13' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max obs.	Data	Min obs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	989.3	1002.1	966.7	1013.5	2.8	−3.2	8.7	29	−14.6	7	−0.8	1.8	−0.4	0.0	5.0	5.3	5.2	5.2	86	77	87	83	0.8	1.7	0.8	1.1	7.9	7.6	7.2	7.6
II	994.0	1007.5	973.8	1018.7	−1.2	−8.9	4.2	14	−20.9	10	−6.2	−2.3	−5.3	−4.8	3.4	3.8	3.5	3.6	84	73	83	80	0.6	1.4	0.7	0.9	8.3	7.5	6.5	7.4
III	993.9	1010.1	964.7	1018.0	7.3	−2.3	17.8	30	−17.1	9	−1.2	6.1	2.0	2.2	5.4	5.8	6.0	5.7	89	60	81	77	0.6	4.2	1.4	2.1	6.9	5.8	5.2	6.0
IV	987.5	1007.1	973.1	1010.8	11.8	3.2	17.6	3	−2.2	2	4.8	10.3	6.8	7.2	7.7	7.5	7.9	7.7	88	62	79	76	1.0	5.2	2.1	2.8	8.4	7.4	5.9	7.2
V	990.9	1005.0	976.9	1014.1	15.9	7.0	24.0	17	−0.7	3, 4	9.3	14.6	11.0	11.4	10.4	10.5	11.1	10.7	86	63	83	77	1.6	6.5	2.3	3.5	7.4	7.7	7.1	7.4
VI	992.0	1001.9	981.0	1014.8	21.7	11.0	32.7	26	4.8	3	14.5	19.9	15.6	16.4	14.3	14.1	15.0	14.5	86	62	84	77	2.5	10.1	3.0	5.2	5.2	7.0	6.0	6.1
VII	990.6	998.3	980.8	1013.4	22.2	12.3	31.1	15	6.2	4	15.3	20.7	15.7	16.8	15.3	15.3	15.5	15.4	87	63	86	79	2.3	10.0	2.7	5.0	7.6	7.9	6.5	7.3
VIII	993.8	1000.8	983.2	1016.7	21.8	10.5	30.9	8	5.2	31	13.1	20.4	14.6	15.7	13.7	13.3	14.4	13.8	90	57	86	78	1.7	11.6	2.8	5.4	6.2	6.1	5.4	5.9
IX	993.0	1012.5	979.6	1016.0	21.3	9.0	28.3	2	4.3	30	11.4	19.8	13.5	14.6	12.4	13.7	13.4	13.2	91	60	87	79	1.4	10.0	2.4	4.6	5.3	5.6	4.0	5.0
X	1000.8	1013.3	991.7	1024.6	14.2	2.2	24.8	2	−5.5	23	4.3	13.2	5.9	7.3	8.0	9.1	8.6	8.6	93	59	88	80	0.7	6.8	1.2	2.9	6.5	4.6	3.2	4.8
XI	989.2	1009.2	962.8	1013.3	4.5	−2.7	14.5	1	−13.1	15	−0.5	3.1	0.5	0.9	5.3	5.7	5.5	5.5	86	73	84	81	1.0	2.5	1.3	1.6	8.0	7.2	7.0	7.4
XII	985.0	1003.8	964.6	1008.8	4.2	−1.3	10.6	20	−11.6	15	1.0	3.0	1.3	1.6	5.6	5.7	5.6	5.6	84	75	82	80	1.1	2.0	1.3	1.5	9.3	8.5	7.3	8.0
Rok	991.7	1013.3	962.8	1015.2	12.2	3.1	32.7	26.VI	−20.9	10. II	5.4	10.9	6.8	7.5	8.9	9.2	9.3	9.1	88	65	84	79	1.3	6.0	1.8	3.0	7.2	6.9	5.9	6.7

Bieruń Stary — φ = 50°05' — λ = 19°05'

I	983.7	996.9	961.1	1013.6	2.3	−4.7	8.8	29	−17.5	8	−1.9	1.6	−1.7	−0.9	4.9	5.4	5.1	5.1	91	79	91	87	0.6	1.5	0.5	0.9	8.0	8.3	6.5	7.6
II	987.8	1000.8	967.8	1018.4	−1.9	−9.9	3.4	14	−22.5	6	−7.4	−2.7	−6.2	−5.6	3.3	3.8	3.4	3.5	89	73	87	83	0.5	1.4	0.6	0.8	8.0	6.5	6.7	7.1
III	988.2	1004.3	960.4	1017.7	7.0	−3.4	16.8	30	−16.5	1	−1.4	6.0	0.5	1.4	5.6	5.5	5.8	5.6	94	59	88	80	0.3	4.4	0.8	1.8	6.7	5.6	5.5	5.9
IV	981.8	1001.1	966.7	1010.8	11.2	1.8	16.6	3, 4	−3.1	2	4.6	10.2	4.9	6.2	7.7	7.9	8.0	7.9	90	65	90	82	0.9	4.8	1.0	2.2	6.6	7.4	6.0	6.7
V	985.2	999.5	970.5	1013.8	15.6	5.8	27.2	19	−3.5	3	9.5	14.4	9.3	10.6	10.6	10.2	10.7	10.5	87	63	88	79	1.6	6.9	1.3	3.3	6.5	7.4	6.7	6.9
VI	986.3	995.9	974.4	1014.5	21.8	10.2	33.1	26	2.4	3	14.6	20.0	14.7	16.0	14.0	13.6	15.0	14.2	84	60	88	77	2.9	10.9	2.1	5.3	5.1	6.3	5.4	5.6
VII	985.1	992.5	975.1	1013.1	22.0	11.6	30.6	14	5.3	4	15.7	20.4	14.6	16.3	15.5	15.7	15.0	15.4	86	66	89	80	2.7	9.1	1.9	4.6	6.9	7.5	4.2	6.2
VIII	988.2	995.0	977.2	1016.5	21.5	9.7	31.6	8	5.0	3	13.0	20.5	13.5	15.1	13.9	13.5	14.1	13.8	92	57	90	80	1.3	11.6	1.7	4.9	5.3	6.1	5.2	5.5
IX	987.6	1005.8	975.9	1016.0	21.0	8.1	28.6	3	2.3	22	10.4	19.4	12.3	13.6	12.2	14.1	13.3	13.2	95	63	92	83	0.7	9.2	1.4	3.8	4.5	5.0	3.8	4.4
X	995.1	1007.6	985.7	1024.5	13.0	1.1	21.4	1, 2	−6.2	22	3.3	12.5	4.6	6.2	7.9	9.3	8.5	8.6	96	63	95	85	0.4	5.7	0.5	2.2	6.4	3.6	2.8	4.3
XI	983.4	1003.5	957.7	1013.2	3.8	−3.7	14.2	2	−15.4	18	−1.3	2.5	−0.7	0.0	5.0	5.6	5.4	5.3	86	76	88	83	1.0	2.2	1.0	1.4	8.0	6.4	7.0	7.1
XII	979.3	997.6	959.4	1008.9	3.8	−1.7	10.9	20	−8.6	15	0.4	2.8	0.9	1.2	5.5	5.7	5.5	5.6	86	76	85	82	1.0	1.9	1.1	1.3	7.7	8.0	6.9	7.5
Rok	986.0	1007.6	957.7	1015.1	11.8	2.1	33.1	26. VI	−22.5	6. II	5.0	10.6	5.6	6.7	8.8	9.2	9.2	9.1	90	67	89	82	1.2	5.8	1.2	2.7	6.6	6.5	5.6	6.2

Kraków - Balice — φ = 50°05' — λ = 19°48'

I	983.8	997.8	961.0	1013.5	1.6	−4.6	7.7	29	−15.7	8	−2.5	0.3	−1.5	−1.3	4.7	5.3	4.9	5.0	90	84	89	88	0.6	1.1	0.6	0.8	8.0	8.6	6.8	7.8
II	987.7	1000.8	966.8	1018.1	−2.4	−10.3	3.6	14	−23.4	7	−7.4	−3.6	−6.7	−6.1	3.2	3.7	3.3	3.4	87	77	84	83	0.5	1.1	0.6	0.7	8.1	7.1	7.3	7.5
III	988.5	1004.8	959.9	1018.2	5.6	−3.6	16.6	30	−18.3	1	−1.7	4.5	0.5	1.0	5.2	6.0	5.6	5.6	91	67	84	81	0.5	2.9	1.0	1.5	7.2	6.9	5.4	6.5
IV	982.0	1001.0	966.0	1011.0	10.7	2.5	15.8	3	−1.3	2	4.1	9.6	5.9	6.4	7.3	7.7	8.0	7.7	88	66	85	80	1.0	4.5	1.4	2.3	7.5	7.7	6.5	7.2
V	985.5	999.7	971.6	1014.1	15.3	6.1	27.5	19	−2.1	3	9.1	13.9	10.0	10.8	10.0	9.7	10.5	10.1	84	61	83	76	1.9	6.6	2.1	3.5	6.3	8.0	6.4	6.9
VI	986.4	996.1	974.0	1014.5	21.5	10.4	32.8	26	3.5	3	14.5	19.9	15.1	16.2	13.5	12.7	14.2	13.5	81	55	82	73	3.3	11.4	3.2	6.0	5.5	6.2	6.3	6.0
VII	985.4	993.1	975.4	1013.5	21.4	11.2	28.8	14	5.5	10	14.8	19.7	15.3	16.3	14.9	14.7	15.0	14.9	88	64	85	79	2.2	8.7	2.6	4.5	6.8	7.6	6.0	6.8
VIII	988.6	995.8	978.1	1016.9	20.9	9.9	31.6	7	5.5	3, 29	12.6	19.4	13.8	14.9	13.5	13.0	13.7	13.4	92	58	86	79	1.3	10.6	2.4	4.8	6.5	6.5	5.7	6.2
IX	988.2	1006.1	977.2	1016.5	20.7	8.3	28.0	3	3.3	22	10.6	19.2	12.9	13.9	12.2	12.8	13.2	12.7	94	59	88	80	0.9	10.0	2.0	4.3	5.3	5.7	4.6	5.2
X	995.3	1008.1	985.6	1024.5	13.0	1.8	21.2	1	−5.0	23	3.4	11.9	5.9	6.8	7.8	9.0	8.7	8.5	95	63	90	83	0.5	5.4	1.0	2.3	5.9	5.1	4.3	5.1
XI	984.0	1003.2	958.1	1013.6	3.2	−3.7	14.7	2	−16.5	18	−1.4	1.6	−0.8	−0.4	5.0	5.4	5.5	5.3	87	77	89	84	0.9	1.8	0.7	1.1	8.1	6.9	7.2	7.4
XII	979.7	997.3	959.9	1009.1	3.6	−2.4	9.6	20	−10.1	15	−0.2	2.5	0.8	1.0	5.3	5.7	5.5	5.5	87	77	85	83	0.9	1.7	1.0	1.2	7.9	8.7	7.3	8.0
Rok	986.3	1008.1	958.1	1015.3	11.3	2.1	32.8	26. VI	−23.4	7. II	4.7	9.9	5.9	6.6	8.6	8.8	9.0	8.8	89	67	86	81	1.2	5.5	1.6	2.8	6.9	7.1	6.2	6.7

Kraków - Chełm — φ = 50°04' — λ = 19°51'

I	–	–	–	–	2.0	−4.1	8.5	29	−13.6	8	−2.1	0.4	−1.0	−0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.9	7.1	8.2
II	–	–	–	–	−2.2	−9.6	4.0	14	−22.4	7	−7.4	−3.9	−6.2	−5.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.6	7.0	7.3
III	–	–	–	–	6.1	−3.3	16.3	30	−17.3	1	−1.7	4.6	0.9	1.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	5.9	6.9
IV	–	–	–	–	10.6	2.5	15.8	7	−1.0	1, 16, 29	4.1	9.4	6.0	6.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.2	7.6	8.0
V	–	–	–	–	15.5	6.5	27.3	19	−1.8	4	9.0	13.8	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.4	8.4	6.2	7.0
VI	–	–	–	–	21.3	10.7	31.1	26	3.2	3	14.4	19.8	14.8	16.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.6	5.4	5.3
VII	–	–	–	–	21.7	11.8	28.6	14	5.6	10	14.9	20.1	15.6	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	6.0	6.7
VIII	–	–	–	–	21.1	10.6	31.6	7	6.0	3	12.7	19.6	14.2	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	5.9	6.5
IX	–	–	–	–	20.9	8.7	28.6	3	3.4	22	10.7	19.1	13.4	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.9	4.6	5.5
X	–	–	–	–	12.7	2.1	20.4	1	−3.3	25	3.6	11.7	6.5	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	5.1	4.3	5.7
XI	–	–	–	–	3.4	−3.1	13.9	2	−15.6	18	−1.3	1.5	−0.3	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.9	7.8	7.8
XII	–	–	–	–	3.9	−1.6	10.7	20	−8.7	15	0.1	2.5	0.9	1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.9	7.6	8.3
Rok	–	–	–	–	11.4	2.6	31.6	7. VIII	−22.4	7. II	4.8	9.9	6.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	6.3	6.9

Racibórz

$H_s = 189\,m$ $H_b = 192{,}6\,m$ $h_w = 12{,}5\,m$ 1965

Miesiąc	Rozkład wiatru (%D,V=D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Liczba dni (n) Temperatura T Min<-10°	Max<0°	Max<0°	Max>25°	Wiatr V ≥10	V>15			Opad R ≥0,1	≥10	≥100			
I	13	1.7	0.5	1.0	1	2.0	9.5	1.8	21.5	2.4	20	2.1	3	2.7	8.5	2.0	16	1.7	66	13.8	9	2	3	26	·	·	·	2	14	17	14	1	1	31	·
II	14	2.6	3	1.8	1	2.0	7.5	1.6	6.5	2.6	7.5	3.9	6.5	2.7	28	3.5	10	2.6	29	4.3	8	11	19	27	·	·	·	1	13	19	10	·	·	28	·
III	7	3.7	·	·	1.5	1.0	11	1.7	12	2.2	15	2.2	3	2.7	22.5	2.2	21	1.8	36	9.4	21	4	4	17	·	·	·	4	11	15	6	·	3	15	·
IV	14	1.8	7	2.6	9	2.3	8.5	1.6	9	2.0	4.5	2.7	10	2.0	23	2.7	5	2.1	91	20.8	20	·	·	5	·	·	·	2	15	21	12	3	·	·	2
V	9.5	1.8	9.5	2.1	4	2.2	7.5	2.0	9.5	2.0	10.5	2.6	6	1.8	27.5	2.7	9	2.1	139	19.0	19	·	·	2	·	1	·	1	17	22	17	8	1	·	7
VI	9.5	1.8	2	1.2	3	1.3	11.5	1.7	10	2.4	12.5	2.2	4	1.5	26.5	2.2	11	1.7	129	26.2	27	·	·	·	8	·	·	2	9	15	13	5	1	·	6
VII	3	1.7	3	2.0	2.5	2.2	5	1.8	22	2.1	25	2.4	6	2.2	16.5	1.9	10	1.9	69	15.9	23	·	·	·	10	·	·	·	14	20	14	2	·	·	6
VIII	5	1.9	3	1.8	0.5	1.0	16	1.5	14.5	2.6	10.5	1.9	4	3.1	23.5	1.8	16	1.6	51	12.5	11	·	·	·	8	·	·	5	7	8	7	2	·	·	2
IX	2.5	2.0	·	·	·	·	18.5	2.2	27	2.1	9.5	2.0	4	2.1	10.5	1.8	18	1.7	52	13.9	10	·	·	·	3	·	·	6	5	9	9	2	4	·	·
X	11	1.9	6	1.2	3	2.3	6.5	2.3	11	2.5	10.5	2.3	4	1.8	9	2.3	32	1.4	1	0.4	8,29,31	·	·	12	·	·	·	4	4	4	·	·	7	·	·
XI	9.5	2.0	5.5	3.3	3.5	1.3	13	1.7	14	2.2	19.5	2.9	4	3.4	8	2.8	13	2.1	28	10.0	11	4	7	20	·	·	·	1	15	13	7	1	·	10	·
XII	2	2.8	2	1.5	2	1.0	5	1.8	31	2.4	23.5	3.0	6	2.6	11.5	1.7	10	2.1	53	12.4	13	1	·	18	·	2	·	1	18	14	8	1	·	10	·
Rok	100	2.1	41.5	1.5	31	1.6	119.5	1.8	188	2.3	168.5	2.5	60.5	2.4	215	2.3	171	1.9	744	26.2	27.VI	22	33	127	29	3	·	29	142	177	117	25	17	94	23

Bieruń Stary

$H_s = 236\,m$ $H_b = 239{,}0\,m$ $h_w = 30\,m$

I	4	2.8	2	2.5	7	1.7	·	·	·	·	19	4.2	15	2.5	2	2.0	44	1.6	61	12.6	31	2	6	27	·	·	·	2	17	14	13	2	–	27	·
II	11.5	3.1	5	2.4	3	2.3	·	·	·	·	12	5.2	19.5	3.6	12	3.8	21	2.8	41	8.3	17	13	23	27	·	3	·	3	12	20	14	·	–	28	·
III	5	1.6	6.5	2.1	6.5	1.6	1	3.0	1.5	1.7	10.5	5.0	14	3.2	9	3.1	39	1.8	42	11.5	6	3	3	22	·	2	·	5	12	18	10	2	–	16	·
IV	5	2.8	8.5	2.4	16	2.8	3.5	2.7	1	2.5	6	3.3	11.5	3.0	12.5	2.9	26	2.0	31	3.9	23	·	·	6	·	·	·	6	16	16	11	·	–	·	2
V	8.5	2.1	1.5	2.0	9.5	3.1	4	4.0	1.5	3.7	13	3.6	13.5	2.7	10.5	3.1	31	2.0	92	19.5	29	·	·	3	1	·	·	3	14	20	16	2	–	·	4
VI	7.5	2.6	4.5	1.8	8.5	3.0	3	2.2	2	1.5	11.5	4.5	12	2.5	21	3.2	20	2.3	123	35.1	27	·	·	·	8	1	·	3	10	14	13	3	–	·	4
VII	2.5	1.2	1	3.0	5.5	2.5	4.5	2.4	1	2.0	19	3.3	15.5	2.8	12	2.1	32	1.8	84	22.4	17	·	·	·	8	·	·	4	8	19	13	2	–	·	5
VIII	8.5	1.6	·	·	4	2.0	5	1.6	0.5	5.0	6	3.8	17	2.0	14	2.4	38	1.3	85	17.0	24	·	·	·	9	·	·	4	9	12	10	3	–	·	2
IX	1	2.0	1	2.0	6	2.3	8	2.4	7.5	3.0	11.5	2.4	9	1.7	4	1.8	42	1.2	84	13.6	19, 29	·	·	·	4	·	·	6	6	13	11	6	–	·	1
X	4.5	1.3	4	1.8	8.5	1.8	3.5	1.9	1	2.0	7.5	3.0	14	2.6	4	2.2	46	1.1	2	1.0	16	·	·	17	·	·	·	8	5	3	1	·	–	·	·
XI	4.5	1.9	3.5	2.7	6	2.7	2	1.5	0.5	2.0	21	4.3	10.5	3.0	5	1.8	37	1.9	35	12.0	11	4	9	20	·	·	·	1	16	15	9	1	–	15	·
XII	2	1.5	·	·	5	1.6	·	·	1.5	3.7	34	4.0	13.5	2.5	4	2.0	33	2.1	48	7.7	3	·	2	21	·	1	·	1	15	17	10	·	–	9	·
Rok	64.5	2.0	37.5	1.9	85.5	2.3	34.5	1.8	18	2.3	171	3.9	165	2.7	110	2.5	409	1.8	728	35.1	27.VI	22	43	143	30	7	·	46	140	181	131	21	–	95	18

Kraków - Balice

$H_s = 237\,m$ $H_b = 237{,}5\,m$ $h_w = 22\,m$

I	4	4.4	21.5	4.0	13.5	3.2	·	·	3	2.5	23.5	3.7	17.5	4.5	4	4.9	6	3.7	44	10.9	31	2	9	28	·	1	·	1	18	14	10	1	4	29	·
II	6.5	4.8	8.5	4.1	3.5	3.6	·	·	3	2.0	23.5	5.6	26	5.7	10	6.0	3	5.0	22	5.6	17	12	23	27	·	4	1	1	17	20	4	·	2	28	·
III	6	3.8	28	3.5	12	4.0	3	2.3	4	2.6	12	4.8	13.5	5.8	3.5	5.1	11	3.7	30	7.1	21	4	5	22	·	3	·	5	12	13	7	·	3	16	·
IV	5	3.6	27	4.9	23	5.2	1	1.0	0.5	2.0	8.5	5.4	16.5	5.0	4.5	4.1	4	4.6	28	4.9	23	·	·	6	·	4	·	3	15	15	11	·	·	·	1
V	6.5	4.2	16	4.3	11.5	5.3	3	2.0	2	5.0	18.5	4.4	23.5	4.9	7	3.9	5	4.3	116	27.0	19	·	·	3	1	3	1	1	13	21	17	4	1	·	6
VI	6.5	3.8	19	3.5	14.5	3.6	2.5	3.6	6	2.8	17	4.0	16.5	5.2	6	5.7	2	4.0	132	41.1	27	·	·	·	5	2	·	3	10	14	13	4	2	·	5
VII	2	2.0	13.5	3.3	10	3.8	1	4.0	7	2.9	23	3.9	25	4.8	3.5	3.6	8	3.6	54	13.1	17	·	·	·	6	1	·	2	10	21	11	1	1	·	3
VIII	6	4.5	19.5	2.9	6	3.3	2	2.8	1	1.5	16.5	3.6	21.5	3.5	10.5	4.1	10	3.1	91	21.5	1	·	·	·	8	·	·	3	12	15	10	3	3	·	2
IX	1.5	2.0	16.5	2.5	9	3.3	8.5	3.2	5.5	2.8	19	3.2	14	3.9	2	2.2	14	2.6	61	13.8	4	·	·	·	3	·	·	6	6	12	9	2	10	·	1
X	4	3.2	17	2.9	12.5	3.6	·	·	3	2.2	22	2.9	17	3.4	6.5	3.3	11	2.8	1	0.6	31	·	·	15	·	·	·	8	9	4	·	·	10	·	·
XI	3.5	2.7	23	5.1	10	4.1	1.5	3.3	3	3.5	23	4.8	21	4.8	2	5.5	3	4.5	33	8.3	21	4	11	21	·	5	·	2	16	19	8	·	8	15	·
XII	3	4.3	14	2.8	6.5	4.5	·	·	5	3.2	34	5.3	20.5	4.3	5	3.5	5	4.1	44	11.4	18	1	3	26	·	3	·	·	19	17	9	1	1	9	·
Rok	54.5	3.6	223.5	3.6	132	4.0	22.5	1.8	43	2.8	240.5	4.3	232.5	4.6	64.5	4.3	82	3.8	656	41.1	27.VI	23	51	148	23	26	2	35	157	185	109	16	45	97	18

Uwaga: Kierunki i prędkości wiatru – wg anemometru M-47.

Kraków - Chełm

$H_s = 225\,m$ $h_w = 17{,}5\,m$

I	2	5.0	2	5.0	11	3.2	3	2.7	1	3.0	11	3.7	24	4.5	·	·	39	2.3	47	12.2	31	2	8	27	·	·	·	·	21	12	9	1	·	25	·
II	5	3.2	2.5	3.0	6.5	5.3	·	·	·	·	3.5	5.0	38.5	5.7	8	5.1	20	4.0	16	4.8	17	10	23	28	·	2	·	2	17	14	6	·	·	28	·
III	3	4.7	1	3.0	10	3.4	6	2.8	·	·	2	2.5	19	5.5	5	4.8	47	2.2	30	7.6	21	4	5	22	·	1	·	4	16	11	8	·	3	15	·
IV	3	4.3	6.5	3.1	24	4.2	7.5	5.2	1	3.0	1.5	6.3	14	4.8	4.5	4.1	28	3.0	34	6.0	12	·	·	5	·	2	·	3	22	13	11	·	·	·	1
V	4	3.2	1	5.0	13.5	3.8	0.5	7.0	3	4.3	6	6.2	21	4.5	7	2.9	37	2.4	113	28.8	19	·	·	2	1	1	1	2	15	19	16	3	·	·	3
VI	4	2.5	1	2.0	10	2.8	4	2.2	1	7.0	4	3.8	22.5	4.3	10.5	4.6	33	2.4	132	44.5	27	·	·	·	6	2	·	7	8	15	13	4	·	·	6
VII	·	·	·	·	10	2.8	·	·	4	3.8	4.5	2.8	32	4.8	3.5	4.4	39	2.4	52	14.6	18	·	·	·	7	·	·	4	10	21	11	1	·	·	1
VIII	1	2.0	3	3.0	6	2.2	4	2.5	2	3.5	5	3.0	19	3.9	9	3.1	44	1.7	111	32.5	1	·	·	·	7	·	·	2	12	13	10	4	·	·	2
IX	1	2.0	0.5	1.0	5	1.7	5.5	2.0	5	2.8	2.5	2.2	17.5	3.5	3	4.3	50	1.3	75	14.1	29	·	·	·	2	·	·	3	6	12	10	3	8	·	1
X	1	3.0	1	3.0	12	2.0	1	5.0	1	3.0	5.5	2.9	22	3.4	4.5	3.6	45	1.5	0	0.2	29	·	·	13	·	·	·	5	11	1	·	·	7	·	·
XI	1	5.0	2	2.5	14.5	3.8	0.5	7.0	2	5.0	2	2.8	37	4.9	5	3.9	26	3.2	32	8.5	21	4	11	19	·	3	1	1	19	13	8	·	6	10	·
XII	2	5.0	·	·	6	2.7	2	2.0	3	1.7	13.5	4.0	34.5	4.8	3	4.0	29	2.9	32	8.3	3	·	2	21	·	·	·	·	23	15	7	·	1	8	·
Rok	27	3.3	20.5	2.6	128.5	3.2	34	3.2	23	3.1	61	3.8	301	4.6	63	3.7	437	2.4	674	44.5	27.VI	20	49	137	23	11	2	33	180	159	109	16	25	86	14

Kraków, Obserw. Astr. UJ

φ = 50°04' λ = 19°58' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	985.4	999.4	963.1	1013.1	2.4	−3.5	8.3	29	−11.8	8	−2.0	1.0	−0.6	−0.6	4.8	5.4	5.2	5.1	89	82	86	86	0.6	1.3	0.8	0.9	8.5	8.7	7.6	8.3
II	989.2	1002.1	968.8	1017.4	−1.6	−8.7	5.3	14	−22.6	7	−6.5	−2.8	−5.4	−5.0	3.5	3.8	3.4	3.6	88	75	81	81	0.5	1.3	0.8	0.9	9.4	7.5	8.5	8.5
III	989.9	1005.9	962.3	1017.4	6.6	−2.1	17.4	30	−15.9	1	−0.8	5.4	1.8	2.0	5.5	6.1	5.9	5.8	89	66	81	79	0.6	3.3	1.3	1.7	7.9	7.1	6.8	7.3
IV	983.6	1002.1	968.4	1010.4	11.2	3.2	16.7	7	−1.5	16	4.6	9.9	7.1	7.2	7.5	7.6	8.2	7.8	87	64	80	77	1.1	4.9	2.0	2.7	7.9	8.1	7.4	7.8
V	986.9	1001.1	973.4	1013.2	16.1	7.3	28.0	19	−1.5	4	9.6	14.5	11.2	11.6	10.3	10.0	11.0	10.4	84	60	81	75	2.0	7.1	2.6	3.9	6.9	8.2	6.9	7.3
VI	987.7	997.1	975.9	1013.7	22.1	11.7	32.8	26	5.5	3	15.2	20.8	16.1	17.0	13.9	13.4	15.0	14.1	80	55	82	72	3.6	11.6	3.6	6.3	6.0	6.2	7.3	6.5
VII	986.8	994.1	976.6	1012.7	22.5	12.4	28.9	14	7.4	6	15.7	20.4	16.6	17.3	14.9	15.4	15.5	15.3	83	64	81	76	3.1	9.4	3.6	5.4	7.2	7.6	5.9	6.9
VIII	989.8	996.7	979.3	1015.9	21.8	11.2	33.1	7	7.5	29	13.5	20.2	15.2	16.0	13.7	13.8	14.4	14.0	88	60	83	77	2.0	10.9	3.3	5.4	7.2	7.1	7.2	7.2
IX	989.5	1007.0	978.1	1015.7	21.7	9.3	28.8	3	4.7	22	11.3	20.1	13.9	14.8	12.7	13.8	14.0	13.5	94	59	88	80	1.0	10.4	2.2	4.5	6.3	6.2	5.7	6.1
X	996.5	1009.1	986.8	1023.5	13.6	2.8	21.5	2	−4.8	22	4.2	12.5	7.0	7.7	8.7	9.4	9.4	9.0	95	63	90	83	0.5	5.6	1.1	2.4	7.4	5.4	5.3	6.0
XI	985.3	1004.5	961.1	1013.0	3.9	−2.6	14.9	2	−16.1	18	−0.9	2.2	0.4	0.5	5.2	5.6	5.8	5.5	87	77	86	83	1.0	2.1	1.0	1.4	8.8	7.6	8.2	8.2
XII	981.3	998.8	962.0	1008.6	4.7	−1.3	11.3	20	−7.4	15	0.5	3.3	1.4	1.6	5.4	5.6	5.7	5.6	83	72	83	79	1.1	2.4	1.3	1.6	8.3	8.6	7.9	8.3
Rok	987.7	1009.1	961.1	1014.5	12.1	3.3	33.1	7. VIII	−22.6	7. II	5.4	10.6	7.1	7.6	8.8	9.2	9.5	9.2	87	66	84	79	1.4	5.9	2.0	3.1	7.6	7.4	7.1	7.4

Uwaga Wartości ciśnienia powietrza są za niskie przeciętnie o około 0.5 mb.

Kraków - Nowa Huta

φ = 50°04' λ = 20°05'

I	—	—	—	—	1.8	−4.1	6.3	29	−13.4	8	−2.1	0.6	−1.1	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.1	6.3	7.5
II	—	—	—	—	−2.1	−9.7	4.6	14	−25.6	7	−6.9	−3.6	−6.1	−5.7	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.9	7.3	7.4
III	—	—	—	—	6.1	−2.6	16.7	30	−15.0	1	−1.2	4.9	1.3	1.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.4	5.1	6.2
IV	—	—	—	—	11.0	2.8	16.4	7	−1.4	16	4.1	9.9	6.1	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.4	6.7	7.0
V	—	—	—	—	15.5	6.4	27.1	19	−2.9	4	9.0	14.3	10.4	11.0	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.4	6.2	6.5
VI	—	—	—	—	22.1	10.9	32.0	26	5.2	3	14.6	20.4	15.2	16.4	—	—	—	—	—	—	—	—	—	—	—	—	4.5	6.5	5.5	5.5
VII	—	—	—	—	21.9	11.8	29.0	14	6.3	4	15.2	20.0	15.5	16.6	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.7	4.8	6.1
VIII	—	—	—	—	21.4	10.4	31.1	7	6.5	18	12.8	19.9	14.3	15.3	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.2	5.5	6.1
IX	—	—	—	—	21.2	8.8	27.7	3	3.2	22	11.2	19.6	13.5	14.4	—	—	—	—	—	—	—	—	—	—	—	—	4.8	5.3	4.2	4.8
X	—	—	—	—	13.1	1.9	21.5	1	−5.3	22	3.4	11.9	6.3	7.0	—	—	—	—	—	—	—	—	—	—	—	—	6.2	4.9	3.5	4.9
XI	—	—	—	—	3.5	−3.4	14.9	2	−18.1	18	−1.2	1.6	−0.3	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.1	6.9	7.3
XII	—	—	—	—	4.1	−1.7	9.7	19	−8.4	15	0.2	3.0	1.2	1.4	—	—	—	—	—	—	—	—	—	—	—	—	7.3	8.5	7.5	7.8
Rok	—	—	—	—	11.6	2.6	32.0	26.VI	−25.6	7. II	4.9	10.2	6.4	7.0	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.8	5.8	6.4

Dębica

φ = 50°03' λ = 21°24'

I	—	—	—	—	1.0	−4.9	6.0	30	−18.3	12	−1.4	−0.2	−2.1	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.9	7.8	8.0
II	—	—	—	—	−2.8	−10.7	3.3	14	−26.9	7	−7.3	−4.0	−7.1	−6.4	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.5	7.4	7.9
III	—	—	—	—	6.3	−2.4	16.4	30	−19.1	1	−0.4	5.1	1.8	2.1	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.2	6.5	6.6
IV	—	—	—	—	11.1	2.8	17.0	7	−2.2	6	5.0	10.0	6.5	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.8	7.9	7.8
V	—	—	—	—	16.2	6.7	27.7	19	−3.4	4	9.4	14.6	10.7	11.4	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.3	7.2	7.1
VI	—	—	—	—	22.3	11.4	32.5	26	6.2	8	15.1	20.7	15.8	16.8	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.5	6.4	5.8
VII	—	—	—	—	22.4	12.7	28.9	16, 17	6.7	12	15.9	20.9	16.1	17.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.2	6.0	6.0
VIII	—	—	—	—	21.2	11.8	31.5	8	6.2	17	13.7	19.8	15.1	15.9	—	—	—	—	—	—	—	—	—	—	—	—	6.3	5.6	6.4	6.1
IX	—	—	—	—	21.5	10.3	27.7	2	4.1	22	12.7	20.0	14.3	15.3	—	—	—	—	—	—	—	—	—	—	—	—	4.7	4.4	3.4	4.2
X	—	—	—	—	12.7	3.3	20.8	1	−6.0	22	5.5	11.7	7.2	7.9	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.5	4.8	5.6
XI	—	—	—	—	3.6	−2.7	15.6	2	−17.2	18	−1.0	2.1	0.2	0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.9	8.0	8.2
XII	—	—	—	—	3.3	−1.2	8.2	6	−12.7	17	0.5	2.1	0.9	1.1	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.7	8.5	8.0
Rok	—	—	—	—	11.6	3.1	32.5	26.VI	−26.9	7. II	5.6	10.2	6.6	7.2	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.6	6.7	6.8

Tarnów

φ = 50°02' λ = 20°59'

I	987.3	1001.9	964.0	1013.5	1.6	−3.7	6.4	30	−11.8	11	−1.4	0.6	−1.1	−0.8	4.6	4.9	4.8	4.8	81	77	85	81	1.1	1.6	0.9	1.2	8.0	7.8	7.1	7.6
II	990.6	1004.9	967.1	1017.4	−2.6	−10.0	4.2	14	−24.4	7	−7.2	−3.9	−6.8	−6.2	3.3	3.5	3.2	3.3	86	75	81	81	0.5	1.2	0.7	0.8	8.8	7.6	7.6	8.0
III	991.9	1007.8	962.7	1017.9	6.1	−2.0	16.3	30	−12.8	1	0.0	4.9	1.9	2.2	5.3	5.8	5.8	5.6	83	66	79	76	1.1	3.4	1.6	2.0	6.7	6.9	5.3	6.3
IV	985.3	1003.4	968.6	1010.8	11.1	2.8	17.6	7	−0.6	1, 11	5.0	9.9	6.3	6.9	7.5	7.7	7.7	7.6	85	64	81	77	1.3	4.8	1.9	2.7	7.8	8.2	6.1	7.4
V	988.5	1003.4	976.3	1013.7	15.9	6.6	27.6	19	−3.2	4	9.4	14.2	10.6	11.2	10.1	10.2	10.9	10.4	84	62	82	76	2.1	6.7	2.2	3.7	6.6	8.2	6.7	7.2
VI	989.4	998.2	976.7	1014.2	21.7	11.4	31.5	26	6.0	3	15.1	20.5	15.4	16.6	14.1	14.0	14.7	14.3	82	59	83	75	3.4	10.9	3.1	5.8	4.8	6.8	6.1	5.9
VII	988.5	995.8	978.4	1013.3	21.9	12.3	28.3	16, 17	7.1	11	15.8	20.4	15.8	17.0	15.1	15.4	15.4	15.3	83	65	85	78	3.2	9.3	2.8	5.1	6.6	7.6	5.9	6.7
VIII	991.4	998.8	978.0	1016.2	20.7	11.2	30.4	8	6.8	31	13.7	19.2	14.9	15.7	13.7	13.4	13.9	13.7	87	62	82	77	2.3	9.7	3.5	5.2	5.8	6.7	5.2	5.9
IX	991.8	1009.0	980.4	1016.7	21.1	10.4	26.0	3	4.3	22	13.0	19.6	14.2	15.2	12.7	13.4	13.2	13.1	85	60	82	76	2.7	9.9	3.3	5.3	5.6	5.0	3.1	4.6
X	998.4	1011.2	988.1	1024.1	13.0	3.3	22.4	2	−5.1	22	5.0	12.1	7.2	7.9	8.1	8.9	8.9	8.6	89	62	85	79	1.0	5.6	1.7	2.8	5.5	6.1	4.3	5.3
XI	987.2	1006.2	963.4	1013.2	3.6	−2.5	15.4	2	−14.1	18	−0.8	2.2	0.4	0.6	5.1	5.3	5.5	5.3	85	72	83	80	1.0	2.3	1.2	1.5	8.1	7.6	7.8	7.8
XII	983.1	999.7	963.8	1009.0	3.8	−1.0	10.3	20	−9.6	7	0.8	2.6	1.1	1.4	5.2	5.3	5.3	5.3	78	71	79	76	1.5	2.2	1.5	1.7	7.4	8.1	7.5	7.7
Rok	989.4	1011.2	962.7	1015.0	11.5	3.2	31.5	26.VI	−24.4	7. II	5.7	10.2	6.7	7.3	8.7	9.0	9.1	8.9	84	66	82	77	1.8	5.6	2.0	3.1	6.8	7.2	6.1	6.7

Kraków, Obserw. Astr. UJ $H_s = 206$ m $H_b = 219{,}8$ m $h_w = 10$ m 1965

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	V ≥ 10	V > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
	ROZKŁAD WIATRU n, V = D																		OPAD R			LICZBA DNI (n): Temperatura T				Wiatr V				Opad R					
I	7	2.1	6.5	2.4	2	1.8	1.5	1.3	2	2.5	19.5	1.9	8	2.1	9.5	2.0	37	1.2	64	14.1	31	2	5	26	·	1	·	1	18	14	12	1	16	31	·
II	6.5	3.0	8	2.4	·	·	·	·	6	2.7	23	3.6	23.5	3.1	8	3.2	9	2.8	38	7.8	17	8	21	26	·	1	·	·	19	20	14	·	11	28	·
III	5	2.0	11.5	2.8	3.5	2.3	5	2.2	1.5	2.3	14	3.1	11.5	2.1	14	2.1	27	1.7	39	7.7	6	2	5	21	·	2	·	3	17	17	9	·	15	19	·
IV	5	3.1	28.5	3.6	8.5	3.6	2.5	1.6	2.5	2.2	15	2.5	7.5	3.1	8.5	2.5	12	2.7	37	7.9	11	·	·	3	·	2	·	3	18	18	13	·	2	·	1
V	6	1.8	11.5	2.8	6.5	2.9	1.5	6.0	1.5	2.7	11	3.5	17	2.3	20	2.2	18	2.1	137	26.2	11	·	·	2	2	1	·	1	16	21	19	5	2	·	5
VI	10.5	1.8	14	2.3	6.5	2.8	1	1.0	0.5	2.0	12.5	2.9	16	3.2	10	3.4	19	2.1	148	28.7	27	·	·	·	8	1	·	2	10	14	14	6	·	·	5
VII	3	1.5	6	3.1	7.5	2.5	2	2.5	5	2.1	18.5	2.7	18	2.3	4	2.2	29	1.7	46	5.1	8	·	·	·	9	·	·	2	10	21	15	·	·	·	2
VIII	5	1.8	4.5	1.6	10	1.7	1	2.5	3	2.2	10.5	1.4	11.5	1.4	13.5	2.0	34	1.1	142	39.5	1	·	·	·	7	·	·	2	16	15	11	5	·	·	2
IX	1.5	2.3	0.5	3.0	9.5	2.7	5	2.0	5	2.1	7.5	2.1	10.5	2.0	2.5	1.6	48	1.0	85	19.9	29	·	·	·	3	·	·	4	7	11	10	4	7	·	1
X	7.5	1.4	10.5	1.5	5	2.6	·	·	·	·	10	2.2	14	2.1	6	1.9	40	1.1	2-	0.5	16, 31	·	·	11	·	·	·	4	10	6	·	·	21	·	·
XI	4	2.0	16	1.9	3.5	2.7	0.5	3.0	4	2.0	19.5	2.5	8.5	1.6	4	2.0	30	1.4	54	11.5	11	4	11	20	·	2	1	1	21	16	10	2	12	16	·
XII	5.5	1.6	4.5	1.6	2	2.0	2.5	1.8	5	2.5	25.5	2.7	11	2.3	4	1.8	33	1.5	42	8.9	18	·	2	20	·	·	·	·	20	15	11	·	9	7	·
Rok	66.5	2.0	122	2.4	64.5	2.3	22.5	2.0	36	2.1	186.5	2.6	157	2.3	104	2.2	336	1.7	834	39.5	1. VIII	16	44	129	29	10	1	23	182	188	138	23	95	101	16

Kraków - Nowa Huta $H_s = 195$ m $h_w = 15{,}4$ m

I	3	6.5	2.5	2.4	19	2.6	5.5	2.2	3.5	2.4	3	2.3	26	3.1	6.5	3.3	24	2.2	37	9.7	31	2	6	27	·	·	·	2	17	12	9	·	1	23	–
II	6	5.2	3	5.0	7	3.4	1	1.0	0.5	1.0	7.5	3.7	37.5	4.4	11.5	4.0	10	3.7	27	8.2	17	12	23	28	·	·	·	1	15	17	7	·	3	28	–
III	6	3.5	6	4.5	16.5	2.0	5	3.1	4	1.9	1.5	3.3	18.5	3.2	6.5	2.6	29	2.0	25	5.5	21	1	5	22	·	·	·	6	13	11	8	·	3	11	–
IV	4	4.1	7.5	3.3	35	4.1	2	2.8	1.5	4.0	2	4.0	16	3.2	7	3.5	15	3.1	23	3.3	26	·	·	5	·	·	·	3	15	12	10	·	1	·	–
V	10	3.4	2.5	2.8	18	2.8	3	3.5	5	2.4	5	2.0	25	3.0	9.5	3.0	15	2.5	115	20.6	11	·	·	2	1	·	·	1	10	19	15	3	·	·	–
VI	5.5	4.1	2	3.0	17	2.9	9	2.0	1.5	3.7	4.5	2.8	25.5	3.8	6	3.1	19	2.5	151	60.1	27	·	·	·	9	·	·	4	9	13	11	4	·	·	–
VII	·	·	3	2.8	12	3.0	4.5	1.7	4	2.1	12.5	2.8	25	2.7	1	2.0	31	1.8	51	17.9	18	·	·	·	8	·	·	3	7	18	14	1	·	·	–
VIII	4.5	2.6	3.5	3.0	14	2.5	5	3.6	2.5	3.0	4	2.4	25	2.3	9.5	2.7	25	1.9	148	38.6	1	·	·	·	8	·	·	6	14	16	14	4	·	·	–
IX	0.5	3.0	·	·	18.5	2.4	11.5	2.9	4.5	3.2	8	2.0	14	2.3	6	2.2	27	1.7	74[2]	15.6	4	·	·	·	4	·	·	7	2	12	9	4	5	·	–
X	3.5	3.0	5.5	2.5	19.5	2.3	4	1.5	1	1.0	9	1.4	21	2.0	6.5	2.9	23	1.6	0	0.4	31	·	·	13	·	·	·	7	5	1	·	·	13	·	–
XI	1.5	1.3	5	5.0	26.5	2.6	2.5	1.4	3	3.2	8	2.6	23	3.4	2.5	1.8	18	2.4	41	7.5	21	4	11	23	·	·	·	2	14	12	8	·	7	10	–
XII	0.5	3.0	1	3.0	16.5	2.9	3.5	2.4	4.5	2.6	14.5	3.2	36.5	2.5	4	4.2	13	2.4	–	–	–	·	2	19	·	·	·	·	17	–	–	–	1	5	–
Rok	45	3.3	41.5	3.1	219.5	2.8	56.5	2.3	35.5	2.5	79.5	2.7	292	3.0	76.5	2.9	249	2.3	–	60.1	27. VI	19	47	139	30	·	·	42	138	–	–	–	34	77	–

Dębica $H_s = 205$ m $h_w = 16{,}2$ m

I	5.5	2.4	5	2.1	5.5	2.1	5.5	3.8	32	4.9	8	3.8	7.5	5.1	4	4.6	20	3.2	72	15.4	31	6	10	25	·	3	1	2	22	18	16	1	4	31	–
II	6.5	1.8	8.5	1.7	5.5	1.5	3	4.3	12	5.1	8	3.4	16	3.5	12.5	2.8	12	2.7	59	11.0	8	14	23	28	·	1	·	·	15	18	16	1	4	28	–
III	5	2.8	6	2.3	7	1.6	5.5	2.0	24.5	5.3	4.5	2.6	4	1.4	2.5	1.4	34	2.2	46	6.0	17, 24	4	5	17	·	3	·	5	11	17	12	·	6	15	–
IV	5	1.6	8.5	3.6	26	2.5	8	2.6	7	3.0	5	2.9	10	3.0	2.5	1.8	18	2.2	50	9.6	26	·	·	3	·	·	·	·	13	12	12	·	·	·	–
V	8	2.1	15	2.4	10.5	3.0	5.5	2.6	7.5	3.5	6	3.5	10	2.5	4.5	2.7	26	2.0	117	46.8	29	·	·	2	2	·	·	1	14	16	15	3	2	·	–
VI	4.5	2.4	5.5	1.9	9.5	2.0	9	3.1	7.5	4.3	5.5	2.2	11	2.4	8.5	2.9	29	1.8	178	54.6	10	·	·	·	7	·	·	3	7	14	13	6	1	·	–
VII	3.5	1.3	8	1.1	9.5	1.2	9	2.3	11	3.0	6	1.6	11.5	2.5	3.5	2.7	31	1.3	109	20.6	21	·	·	·	8	1	·	3	6	15	15	4	·	·	–
VIII	8	3.1	2.5	3.0	2	1.2	4.5	2.6	21	3.4	5.5	2.4	9.5	2.2	11	2.5	29	1.9	179	46.4	2	·	·	·	6	1	·	5	11	10	10	4	1	·	–
IX	2	1.5	5	1.4	1.5	1.3	15	2.6	31.5	3.8	5.5	2.5	3.5	1.7	·	·	26	2.2	56	37.4	11	·	·	·	4	1	1	8	3	8	3	2	2	·	–
X	7	1.9	3.5	1.4	4	1.5	6.5	3.0	10.5	3.4	8.5	2.9	8.5	2.9	4.5	1.4	40	1.5	6	2.8	31	·	·	6	·	·	·	4	6	3	2	·	9	·	–
XI	6.5	2.0	13	2.3	4	1.8	4	2.0	19	4.6	11	3.6	9.5	2.2	5	1.4	18	2.4	60	10.4	11	3	8	17	·	1	·	·	17	14	11	1	7	9	–
XII	2.5	1.0	2.5	1.6	3.5	1.4	9	3.3	42	3.8	4.5	3.8	8	2.4	7	2.3	14	2.7	37	8.4	18	1	2	14	·	1	1	·	17	15	10	·	·	7	–
Rok	64	2.0	83	2.1	88.5	1.8	84.5	2.8	225.5	4.0	78	2.9	109	2.6	65.5	2.2	297	2.2	969	54.6	10. VI	28	48	112	27	12	3	31	142	160	135	22	36	90	–

Tarnów $H_s = 209$ m $H_b = 209{,}1$ m $h_w = 13{,}6$ m

I	4	3.5	4.5	3.7	4.5	2.2	16	2.4	29.5	3.0	7	2.5	10	3.8	7.5	2.3	10	2.6	70	12.5	31	3	10	25	·	·	·	1	19	16	13	2	3	31	·
II	6.5	2.9	6	3.7	2.5	2.8	1.5	2.0	6.5	3.4	6	3.9	26	4.8	16	3.1	13	3.2	37	6.0	16	12	22	28	·	·	·	1	17	22	12	·	1	28	·
III	6	3.2	5	2.8	6	5.0	12.5	2.3	23	2.8	7	1.3	10	2.8	6.5	2.5	17	2.2	43	6.4	21	2	6	18	·	·	·	6	12	16	11	·	3	15	·
IV	3	2.2	8	2.8	28.5	4.5	11.5	3.2	6	2.5	4.5	1.9	12	3.8	8.5	3.2	8	3.2	28	7.4	26	·	·	5	·	·	·	1	17	13	11	·	·	·	3
V	10	2.7	4	3.0	13.5	4.2	10.5	2.1	4.5	2.8	5.5	2.5	17.5	2.2	10.5	2.8	17	2.3	94	28.4	29	·	·	3	1	·	·	1	12	19	17	2	1	·	4
VI	6.5	2.0	0.5	4.0	16	3.0	12.5	3.3	6	3.1	2.5	3.4	20.5	2.5	8.5	4.0	17	2.4	154	48.9	10	·	·	·	6	·	·	2	9	15	13	4	1	·	4
VII	1.5	1.0	1	1.0	4.5	2.7	10	1.6	4.5	3.2	7.5	1.2	19	3.0	12	2.0	33	1.5	132	40.0	18	·	·	·	8	·	·	3	11	19	18	4	·	·	6
VIII	5	3.5	1.5	3.3	2	1.5	10.5	2.6	12	2.4	4	3.0	11.5	2.4	21.5	2.7	25	1.9	151	29.4	1	·	·	·	6	·	·	6	12	15	10	5	·	·	2
IX	2.5	1.8	·	·	3	1.5	19.5	3.2	23.5	2.7	4	2.2	8	2.2	7.5	1.3	22	1.9	61	21.4	11	·	·	·	4	·	·	8	5	9	7	2	·	·	·
X	4	1.5	7.5	1.7	11.5	1.7	5	1.7	6	1.7	5	1.6	18	2.6	9	2.5	27	1.5	3	1.3	29	·	·	8	·	·	·	7	8	4	1	·	3	·	·
XI	2.5	2.0	7.5	3.5	10.5	3.5	6	3.7	12	4.3	9.5	2.7	11.5	4.0	12.5	3.0	18	2.8	41	12.4	21	2	9	21	·	·	·	·	17	15	8	1	3	10	·
XII	1	2.0	0.5	1.0	7.5	2.5	7	3.3	27	3.2	18.5	2.8	14.5	2.8	9	1.9	8	2.6	42	12.7	18	·	1	18	·	·	·	·	18	18	12	1	·	8	·
Rok	52.5	2.4	46	2.5	110	2.9	122.5	2.6	160.5	2.9	81	2.4	178.5	3.1	129	2.6	215	2.3	856	48.9	10. VI	19	48	126	25	·	·	36	157	181	133	21	15	92	19

Jakubowice

$\varphi = 50°01'$ $\lambda = 17°51'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.6	-3.7	5.1	29	-14.9	8	-1.3	0.6	-1.2	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.9	6.8	7.8
II	–	–	–	–	-1.9	-9.5	3.5	14	-21.3	6	-6.8	-3.0	-5.9	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	6.3	7.0
III	–	–	–	–	6.0	-2.5	17.5	30	-15.9	9	-0.5	4.8	1.4	1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.3	4.8	5.4
IV	–	–	–	–	10.9	2.9	17.3	3	-1.6	2	5.4	9.2	7.1	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.7	7.2
V	–	–	–	–	15.0	6.4	22.8	18	-1.6	4	9.9	13.3	11.1	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.7	7.2	7.5
VI	–	–	–	–	20.8	10.4	31.4	26	2.7	3	15.3	18.8	16.0	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.4	5.2	5.8
VII	–	–	–	–	21.5	11.7	30.8	14	5.7	6	15.9	20.0	15.7	16.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	5.5	6.8
VIII	–	–	–	–	21.2	9.8	29.6	8	5.1	31	14.4	19.6	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.2	4.6	5.1
IX	–	–	–	–	20.5	8.5	27.2	3	3.3	22	13.4	18.6	14.1	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.7	4.2	5.0
X	–	–	–	–	13.6	2.6	22.5	1	-6.7	22	5.3	12.5	7.1	8.0	–	–	–	–	–	–	–	–	–	–	–	–	4.9	3.4	3.5	3.9
XI	–	–	–	–	3.5	-3.0	13.7	2	-13.6	15	-1.0	2.3	0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.1	6.9	7.4
XII	–	–	–	–	3.7	-1.5	(11.1)	20	-13.3	15	0.4	2.5	1.2	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.1	6.6	7.8
Rok	–	–	–	–	11.4	2.7	31.4	26.VI	21.3	6. II	5.9	9.9	6.8	7.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	5.7	6.4

Ożańsk

$\varphi = 50°01'$ $\lambda = 22°35'$

I	–	–	–	–	0.8	-5.4	6.8	30	-16.6	12	-3.1	-1.5	-2.1	-2.2	4.6	4.8	4.8	4.7	89	85	88	87	0.6	0.8	0.6	0.7	7.7	7.0	7.3	7.3
II	–	–	–	–	-3.7	-10.3	0.0	15	-21.1	7	-7.7	-5.2	-7.3	-6.9	3.3	3.6	3.2	3.4	90	84	87	87	0.3	0.7	0.4	0.5	8.5	6.7	6.7	7.3
III	–	–	–	–	4.9	-2.6	15.5	30	-18.1	1	-0.7	3.7	1.2	1.4	5.5	6.2	5.9	5.9	90	75	86	84	0.6	2.2	1.0	1.3	6.4	5.5	5.5	5.8
IV	–	–	–	–	10.1	2.3	15.7	7	-1.5	9	3.8	8.5	5.6	5.9	7.5	8.1	7.9	7.9	91	73	85	83	0.7	3.3	1.4	1.8	7.7	7.0	7.0	7.2
V	–	–	–	–	15.2	6.4	26.1	19	-2.0	4	8.8	13.5	10.2	10.7	10.5	11.1	11.0	10.9	90	71	86	82	1.4	5.0	1.8	2.7	6.2	6.7	6.1	6.3
VI	–	–	–	–	21.0	11.4	28.7	26	5.4	3	14.7	19.4	15.7	16.4	15.0	15.2	15.4	15.2	89	68	85	81	1.9	7.8	2.9	4.2	4.9	6.0	5.4	5.4
VII	–	–	–	–	21.6	12.3	29.1	16	7.9	7	15.3	20.1	16.0	16.8	15.9	16.2	16.0	16.0	90	69	87	82	1.7	7.9	2.5	4.0	5.3	6.0	6.2	5.8
VIII	–	–	–	–	20.2	11.2	29.5	8	7.4	31	13.3	18.6	15.0	15.5	14.3	14.9	14.6	14.6	93	71	85	83	1.3	7.5	2.9	3.9	5.3	5.9	5.1	5.4
IX	–	–	–	–	20.8	9.8	25.5	3, 4	5.0	17	12.2	19.3	14.1	14.9	13.2	14.9	14.5	14.2	92	67	89	83	1.2	7.9	1.8	3.6	5.5	5.4	5.4	5.4
X	–	–	–	–	12.1	3.5	21.7	1	-3.5	22	5.2	10.5	6.9	7.4	8.6	9.5	9.0	9.0	94	74	89	86	0.6	3.7	1.2	1.8	6.6	6.2	4.6	5.8
XI	–	–	–	–	3.4	-3.4	14.3	2	-19.4	18	-1.5	0.6	-0.5	-0.5	5.4	5.9	5.6	5.6	93	88	90	90	0.5	1.1	0.9	0.8	8.3	7.5	6.6	7.5
XII	–	–	–	–	2.9	–	8.0	10, 21	-18.4	17	-0.2	1.3	0.0	0.3	5.7	5.9	5.8	5.8	92	87	92	90	0.5	0.9	0.5	0.6	7.8	6.9	7.4	7.4
Rok	–	–	–	–	10.8	–	29.5	8.VIII	-21.1	7. II	5.0	9.1	6.2	6.6	9.1	9.7	9.5	9.4	91	76	87	85	0.9	4.1	1.5	2.2	6.7	6.4	6.1	6.4

Jarosław

$\varphi = 50°01'$ $\lambda = 22°42'$

I	–	–	–	–	0.8	-5.2	8.3	30	-17.5	11, 12	-2.7	-0.7	-2.5	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	7.4	7.8
II	–	–	–	–	-3.0	-9.6	2.0	14	-22.9	7	-7.3	-4.1	-6.6	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	6.5	7.6
III	–	–	–	–	5.9	-3.2	15.9	30	-19.3	1	-2.0	4.3	1.4	1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	5.5	6.6
IV	–	–	–	–	10.6	2.8	16.4	7, 18	-1.0	11	4.1	9.3	6.1	6.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.5	6.9	7.9
V	–	–	–	–	15.9	6.9	27.2	19	-1.4	4	9.3	14.0	11.1	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.6	7.0	7.2
VI	–	–	–	–	21.6	12.1	29.3	26	7.0	8	15.1	19.9	16.7	17.1	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.0	5.8	5.5
VII	–	–	–	–	21.9	12.7	28.5	16	8.3	12	15.8	20.4	16.7	17.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	6.4	6.4
VIII	–	–	–	–	20.8	11.0	30.6	8	6.6	17	13.4	19.4	15.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.4	6.2	6.2
IX	–	–	–	–	21.2	9.1	26.4	3	4.2	17, 22	11.4	20.2	14.8	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.5	3.4	4.7
X	–	–	–	–	12.5	3.5	21.8	1	-3.4	22	5.0	11.5	7.6	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.5	5.1	6.1
XI	–	–	–	–	3.0	-2.8	15.1	2	-19.5	18	-1.1	1.9	-0.1	0.7	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.9	7.8	8.2
XII	–	–	–	–	2.8	-1.9	8.7	10	-17.4	17	0.1	1.9	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.5	8.2	8.0
Rok	–	–	–	–	11.2	3.0	30.6	8.VIII	-22.9	7. II	5.1	9.8	6.8	7.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	6.4	6.9

Pszczyna

$\varphi = 50°00'$ $\lambda = 18°55'$

I	–	–	–	–	2.0	-3.9	7.5	29	-14.1	8	-1.6	0.9	-1.2	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	6.3	7.3
II	–	–	–	–	-2.6	-9.0	3.5	14	-20.5	6	-6.6	-3.2	-6.3	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	6.6	7.1
III	–	–	–	–	6.4	-2.5	16.8	30	-14.7	11	-0.7	5.3	1.5	1.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.8	5.2	5.8
IV	–	–	–	–	11.0	2.5	16.4	3	-1.2	16	4.3	9.9	5.3	6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.4	5.7	6.3
V	–	–	–	–	15.3	6.4	25.8	19	-2.6	3	8.9	13.8	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.2	7.0	6.9
VI	–	–	–	–	21.1	11.1	31.5	26	4.6	3	14.5	19.1	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.8	5.7	5.3
VII	–	–	–	–	21.3	12.1	30.8	15	5.9	5	15.1	19.8	15.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.3	5.9	6.4
VIII	–	–	–	–	21.1	10.6	30.2	7, 8	6.3	18	13.4	18.6	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.9	4.4	5.1
IX	–	–	–	–	21.1	9.0	27.4	2, 3	2.9	22	11.4	19.3	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.6	3.9	4.3
X	–	–	–	–	13.3	3.0	22.0	2	-3.4	13	4.6	12.3	6.3	7.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	3.7	3.4	4.3
XI	–	–	–	–	3.6	-3.2	13.4	2	-15.1	18	-1.2	2.1	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.5	7.9	7.6
XII	–	–	–	–	3.4	-1.3	9.4	19	-19.1	15	0.5	2.2	0.8	1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	6.8	7.7
Rok	–	–	–	–	11.4	2.9	31.5	26.VI	-20.5	6. II	5.2	10.1	6.2	6.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	5.7	6.2

Jakubowice

$H_s = 319$ m $h_w = 14$ m 1963

MIESIĄC	ROZKŁAD WIATRU (%, V m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V ≥10	≥15	◐	◓	Opad R ≥1	≥10	≥100	≡	≋	K
I	11	4.5	·	·	·	·	3	2.3	11	3.2	37	4.2	4.5	3.2	11.5	2.9	15	3.2	59	15.0	3	3	7	28	·	1	·	2	20	17	12	2	5	31	–
II	21	4.9	3	3.0	·	·	2	3.0	1	5.0	11	5.5	5	2.2	21	7.7	20	4.2	37	8.5	18	13	22	28	·	5	1	1	11	23	10	·	5	28	–
III	15	3.8	4	2.0	1	1.0	·	·	12	3.0	26	3.4	6	4.0	11	3.9	18	2.8	34	9.3	6	4	4	17	·	·	·	6	9	11	6	·	3	16	–
IV	23	2.3	7	2.7	6	3.0	2	3.0	9	4.3	7	2.4	3	3.0	13	4.5	20	2.4	89	17.9	19	·	·	6	·	·	·	5	16	18	10	3	·	·	–
V	30	3.1	9	2.3	1	7.0	1	1.0	7.5	2.7	14.5	2.6	3	4.3	12	4.2	15	2.6	149	19.6	28	·	·	2	·	1	·	1	19	18	16	8	·	·	–
VI	11.5	2.1	5.5	1.7	2	3.0	4	4.0	10	3.6	13	2.8	9	2.6	24	4.5	11	2.9	122	29.2	11	·	·	·	5	1	·	4	7	14	13	5	·	·	–
VII	5	1.8	4	2.0	5	2.6	1	3.0	17	3.0	31	3.2	2	4.0	10	1.6	18	2.2	92	17.5	31	·	·	·	5	·	·	2	10	20	16	3	·	·	–
VIII	16.5	3.0	9	2.6	2	1.0	0.5	3.0	12.5	3.5	10	3.6	8	2.2	14.5	3.4	20	2.4	37	12.0	24	·	·	·	9	·	·	6	6	8	7	1	·	·	–
IX	7	3.3	4	2.5	1	3.0	5.5	4.5	32	3.4	13.5	3.4	3	3.7	6	2.7	18	2.7	59	27.4	4	·	·	·	2	1	·	8	5	8	7	1	·	·	–
X	16	2.9	3	1.7	4.5	2.3	1.5	1.7	17	2.5	11	3.2	4	2.5	3	2.0	33	1.7	8	7.0	8	·	·	7	·	·	·	11	6	3	1	·	3	·	–
XI	20	2.7	2	1.0	2	1.0	1	1.0	9	4.8	22	4.1	3	6.7	7	1.6	24	2.5	36	21.7	11	2	7	22	·	3	·	3	18	16	7	1	2	13	–
XII	4	2.0	2	2.0	2	3.0	1	5.0	13	6.2	47	4.1	6	3.3	11	3.2	7	3.8	32	14.5	13	1	·	20	·	2	·	1	17	12	6	1	1	9	–
Rok	180	3.0	52.5	2.0	26.5	2.2	22.5	2.6	151	3.8	243	3.5	56.5	3.5	144	3.5	219	2.8	754	29.2	11.VI	23	40	130	21	14	1	50	144	168	111	25	19	97	–

Ożańsk

$H_s = 250$ m $h_w = 20.5$ m

I	1.5	2.0	5.5	5.5	4	8.5	16	3.9	1.5	5.3	25.5	8.9	2	3.0	11	7.4	26	4.8	35	12.9	31	5	13	29	·	11	1	·	16	14	9	1	–	31	·
II	·	·	12	5.5	·	·	2	7.0	1.5	8.7	20.5	8.5	5	9.4	22	9.7	21	6.2	23	4.5	18	14	27	28	·	10	5	·	12	13	7	·	–	28	·
III	·	·	·	·	4	5.0	9	4.4	1	3.0	21	3.3	2.5	7.2	14.5	4.1	41	2.3	39	5.6	3	2	6	21	·	1	1	5	8	15	13	·	–	15	·
IV	3	6.0	3.5	3.7	2.5	7.6	39	8.1	3.5	6.3	13.5	4.5	·	·	5	3.2	20	5.1	58	15.0	22	·	·	8	·	8	3	·	12	12	8	3	–	·	3
V	6.5	2.8	5.5	2.5	4	8.5	12	4.3	0.5	4.0	16.5	4.6	1	2.0	20	4.2	27	3.0	47	14.0	29	·	·	2	1	2	·	·	7	16	13	1	–	·	3
VI	4	3.5	·	·	·	·	17	3.0	5.5	3.8	15.5	3.7	2	4.0	22	4.4	24	2.8	117	26.2	10	·	·	·	5	3	3	2	6	12	11	5	–	·	4
VII	1	2.0	2	4.0	2.5	2.8	11.5	3.4	2	3.0	22	4.0	3	3.3	25	4.3	24	2.9	156	34.7	18	·	·	·	7	2	1	3	3	22	16	4	–	·	9
VIII	1	4.0	9	4.9	·	·	5	4.0	5	4.4	25	3.5	2	6.0	21	5.1	25	3.2	127	37.5	26	·	·	·	7	3	1	7	7	13	12	3	–	·	4
IX	5	4.8	4	3.0	7	4.3	21	4.0	·	·	15	4.0	2	5.0	3	2.0	33	2.5	55	22.7	11	·	·	·	4	·	·	6	8	9	8	2	–	·	·
X	5	4.0	7	2.9	·	·	9	2.7	3	5.3	19	5.8	4	6.5	16	4.8	30	3.1	8	4.2	31	·	·	4	·	3	·	3	8	7	2	·	–	·	·
XI	·	·	7	4.3	3.5	3.1	12.5	4.6	2	4.0	18	6.0	5	8.2	11	4.0	31	3.3	45	16.5	21	3	8	19	·	6	1	1	14	11	7	1	–	16	·
XII	2	5.0	1	3.0	2	2.0	6	3.7	0.5	4.0	34.5	6.4	13	4.5	9	5.8	25	4.0	45	6.8	18	–	6	–	·	8	3	1	13	17	14	·	–	5	·
Rok	29	2.8	56.5	3.3	29.5	3.5	160	4.4	26	4.3	246	5.3	41.5	4.9	179.5	4.9	327	3.6	755	37.5	26.VIII	–	60	–	24	57	19	28	114	161	120	20	–	95	23

Jarosław

$H_s = 204$ m $h_w = 19$ m

I	6	3.7	·	·	4	4.8	22	4.7	6	3.0	17	6.1	20	3.0	11	6.5	7	4.3	47	19.2	31	7	12	26	·	3	·	3	21	16	9	1	7	31	·
II	10	4.1	7	3.1	2	3.0	1	6.0	·	·	9	8.6	32	6.0	20	4.6	3	5.2	39	5.8	18	12	24	28	·	6	·	1	13	15	14	·	·	28	·
III	4	3.0	6	3.0	11	2.3	13	3.8	14	2.1	11	2.2	15	2.7	9	5.2	10	2.6	43	9.6	2	3	4	21	·	1	·	3	12	14	13	·	9	17	·
IV	6	3.7	·	·	7.5	6.8	37.5	7.6	4	3.0	9	5.0	15	3.9	4	4.5	7	5.5	57	13.2	26	·	·	7	·	8	1	·	16	12	9	3	1	·	3
V	9.5	4.8	4.5	2.6	2.5	5.4	15.5	4.2	6	2.3	11	5.4	14.5	5.2	23.5	4.1	6	4.1	44	11.6	29	·	·	2	2	5	·	1	10	18	12	1	·	·	5
VI	6.5	5.6	·	·	9	3.4	17	4.4	2.5	3.8	9	5.7	10.5	4.5	22.5	5.2	13	4.1	118	23.3	28	·	·	·	6	3	·	2	6	14	11	4	·	·	6
VII	3	4.5	·	·	6.5	6.2	11.5	4.9	2.5	5.8	18.5	5.5	13.5	6.0	16.5	4.6	21	4.1	132	17.0	21	·	·	·	8	6	1	4	7	20	17	6	·	·	6
VIII	6	5.5	2	7.0	7.5	4.6	10	4.1	2	2.0	12	4.9	12.5	4.4	17	6.3	24	3.7	113	32.9	26	·	·	·	7	2	·	2	11	15	12	4	1	·	3
IX	4	4.4	·	·	5	4.8	19	3.9	10	5.0	14.5	3.0	13	3.7	9.5	3.6	15	3.2	48	24.1	11	·	·	·	5	3	1	7	1	9	6	2	4	·	·
X	12	5.4	2	4.0	2.5	4.0	4.5	3.1	2	3.0	11.5	6.6	18.5	6.1	17	5.2	23	4.1	7	3.5	31	·	·	8	·	3	·	3	7	9	2	·	9	·	·
XI	2.5	4.8	5	6.2	16	5.2	11.5	4.7	3.5	4.1	9	5.5	16	6.2	9.5	5.8	17	4.4	74	20.6	11	2	10	20	·	4	·	·	21	17	11	2	4	16	·
XII	4.5	6.1	2	5.0	4	4.8	9	5.2	9.5	7.4	30.5	6.7	15	6.1	9.5	4.4	9	5.5	47	7.2	13	1	4	21	·	9	2	1	20	20	15	·	1	6	·
Rok	74	4.6	28.5	2.6	77.5	4.6	171.5	4.7	62	3.5	162	5.4	195.5	4.8	169	5.0	155	4.2	769	32.9	26.VIII	25	54	133	28	53	5	27	145	179	131	23	36	98	23

Pszczyna

$H_s = 270$ m $h_w = 16.3$ m

I	2	3.5	6	2.2	·	·	19	1.1	10	1.5	39	2.3	4	2.2	1	2.0	12	1.7	78	19.5	9	2	6	28	·	·	·	·	14	14	13	2	12	29	·
II	·	·	9	1.3	3	1.0	1	3.0	·	·	41	2.5	8	2.4	19	2.3	3	2.2	49	9.2	17	9	23	28	·	·	·	3	13	19	14	·	6	28	·
III	1	1.0	18	1.4	1	3.0	7	1.1	1.5	1.3	37	1.9	8.5	2.2	13	1.3	6	1.6	41	11.4	21	3	5	21	·	·	·	5	7	14	9	1	12	16	·
IV	1.5	1.3	18	1.8	7	2.3	11	1.5	3	2.0	28.5	2.0	7	2.2	8	1.7	6	1.8	54	9.9	20	·	·	4	·	·	·	4	14	17	11	·	3	·	1
V	3	1.7	7	1.3	11	2.3	4	1.2	1	3.0	27	2.2	13	1.8	13	2.2	14	1.7	114	16.1	10	·	·	3	1	1	·	1	14	18	15	6	1	·	7
VI	2	2.0	3	1.0	·	·	12	1.5	4	1.2	34.5	2.4	8.5	2.1	12	2.6	14	1.8	167	39.7	10	·	·	·	5	·	·	3	7	14	13	7	2	·	6
VII	1	1.0	3	1.3	3.5	1.6	2.5	1.0	5	1.2	45	2.4	9.5	1.9	10.5	1.8	13	1.8	77	14.2	8	·	·	·	6	·	·	1	7	19	13	2	1		7
VIII	2	1.5	8	1.1	3	1.0	9	1.2	4	2.2	31	1.9	1.5	1.3	20.5	1.8	14	1.4	76^2	20.6	24	·	·	·	9	·	·	7	8	11	8	4	·	·	2
IX	1	2.0	·	·	·	·	18	1.2	19	2.1	31	2.0	4	1.5	2	2.0	15	1.5	70^2	15.2	18	·	·	·	2	·	·	7	4	11	8	4	4	·	·
X	5.5	1.2	7.5	1.4	2	3.0	11	1.4	5	1.7	34	1.7	9	1.3	13	1.2	6	1.4	4	1.7	29	·	·	7	·	·	·	10	6	4	2	·	8	·	·
XI	·	·	7	2.0	7	2.4	15	1.4	4	2.9	39	2.7	3	1.3	6	1.3	9	2.0	42	14.9	11	4	10	20	·	·	·	1	16	13	9	2	6	15	1
XII	1	2.0	4	1.5	3	2.0	5	1.4	5.5	2.0	65.5	3.2	2	2.5	5	1.8	2	2.7	52	13.0	18	·	3	23	·	2	·	1	16	15	10	1	4	7	·
Rok	20	1.4	90.5	1.4	40.5	1.6	114.5	1.4	62	1.8	452.5	2.3	78	1.9	123	1.8	114	1.8	824^2	39.7	10.VI	18	47	134	23	3	·	43	126	169	125	29	59	95	24

Czernichów — φ = 50°00' — λ = 19°41' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	2.2	−4.0	8.2	29	−16.6	8	−2.0	1.9	−1.1	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.9	8.0	8.1
II	—	—	—	—	−1.4	−9.8	5.2	14	−22.5	10	−7.0	−2.3	−6.0	−5.3	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.5	8.2	7.9
III	—	—	—	—	6.9	−2.7	17.2	30	−16.9	1	−0.9	6.4	1.8	2.3	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.5	5.8	5.8
IV	—	—	—	—	11.5	2.9	16.7	29	−1.0	16	4.7	11.0	6.4	7.1	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.2	7.4	7.2
V	—	—	—	—	15.8	6.4	27.9	19	−2.5	3	9.6	15.2	10.3	11.4	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.3	7.0	6.6
VI	—	—	—	—	22.2	11.0	32.9	26	3.5	3	15.4	21.6	15.5	17.0	—	—	—	—	—	—	—	—	—	—	—	—	4.6	5.3	6.8	5.6
VII	—	—	—	—	22.2	12.2	29.6	14	5.4	10	16.2	21.4	16.2	17.5	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.8	6.6	6.0
VIII	—	—	—	—	21.9	10.3	32.9	7	5.4	3	13.6	20.9	15.2	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.0	6.2	6.0
IX	—	—	—	—	21.7	8.8	29.2	3	3.3	22	11.3	20.8	14.0	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.5	4.9	5.2	5.2
X	—	—	—	—	13.4	1.9	21.4	2	−4.8	22	3.8	12.9	6.5	7.4	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.8	5.9	5.9
XI	—	—	—	—	4.1	−3.2	14.8	2	−15.2	18	−0.5	3.1	0.3	0.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.1	8.3	8.2
XII	—	—	—	—	4.5	−1.9	10.9	20	−10.8	15	0.5	3.9	1.5	1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.5	7.8	7.6
Rok	—	—	—	—	12.1	2.7	32.9	26.VI 7.VII	−22.5	10. II	5.4	11.4	6.7	7.6	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.5	6.9	6.7

Wieliczka — φ = 50°00' — λ = 20°03'

I	—	—	—	—	2.4	−4.3	9.1	29	−12.5	12	−2.3	1.1	−1.1	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−2.2	−8.9	4.2	12, 14	−24.4	7	−6.7	−3.6	−5.7	−5.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	6.3	−2.6	16.2	30	−15.7	1	−0.8	5.0	1.5	1.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	10.9	2.5	16.1	7	−2.3	6	4.0	9.5	6.1	6.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	15.5	6.6	27.1	19	−2.7	4	9.1	14.1	10.2	10.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	21.6	11.3	31.7	26	6.2	3	14.8	20.4	15.1	16.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.9	12.6	28.3	15	7.8	10	15.7	20.1	15.8	16.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	21.2	11.1	31.5	7	7.8	18, 29	13.2	19.9	14.8	15.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	21.4	9.5	28.1	3	5.3	30	11.5	19.6	14.1	14.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	13.3	2.8	22.3	2	−5.5	22	4.1	12.3	6.7	7.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	3.8	−2.8	14.3	2	−16.9	18	−1.1	1.8	0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	4.7	−0.8	11.3	20	−7.6	15	0.9	3.3	1.6	1.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	11.7	3.1	31.7	26.VI	−24.4	7. II	5.2	10.3	6.6	7.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Bochnia - Chodenice — φ = 49°59' — λ = 20°24'

I	—	—	—	—	2.0	−5.0	8.3	29	−15.1	8	−2.6	0.6	−1.4	−1.2	4.6	5.2	5.1	5.0	89	82	90	87	0.6	1.3	0.6	0.8	8.4	8.3	6.6	7.8
II	—	—	—	—	−2.4	−10.6	3.9	14	−28.4	7	−7.2	−3.6	−6.6	−6.0	3.4	3.7	3.4	3.5	89	78	86	84	0.4	1.1	0.5	0.7	7.9	7.6	7.9	7.8
III	—	—	—	—	6.0	−4.0	16.3	30	−21.5	1	−1.6	4.4	0.9	1.2	5.3	6.1	5.6	5.7	90	71	83	81	0.6	2.7	1.2	1.5	7.6	7.0	6.4	7.0
IV	—	—	—	—	11.3	2.0	16.9	7	−2.8	16	4.4	9.9	5.9	6.5	7.3	7.7	7.9	7.6	87	64	85	79	1.2	4.9	1.4	2.5	7.9	7.7	6.4	7.3
V	—	—	—	—	15.8	5.8	27.2	19	−4.6	4	9.7	14.4	9.8	10.9	10.1	10.4	10.7	10.4	82	63	86	77	2.4	6.5	1.8	3.6	6.5	8.6	7.1	7.4
VI	—	—	—	—	21.7	10.6	32.4	26	5.1	3	15.2	20.3	14.8	16.3	14.1	13.5	14.6	14.1	81	58	86	75	3.5	11.1	2.5	5.7	4.8	5.3	6.2	5.4
VII	—	—	—	—	22.1	11.6	28.8	14	6.4	10, 12	16.0	20.1	15.2	16.6	14.9	15.1	14.9	15.0	81	65	85	77	3.6	9.2	2.6	5.1	6.4	7.6	4.8	6.3
VIII	—	—	—	—	21.0	10.2	31.1	7	6.0	18	13.4	19.1	14.2	15.2	13.7	13.2	13.7	13.5	89	61	85	78	1.9	10.1	2.9	5.0	6.7	6.5	5.9	6.4
IX	—	—	—	—	21.4	8.5	27.8	3	3.1	22	12.0	19.6	13.7	14.8	12.4	13.3	13.1	12.9	89	59	84	77	2.0	10.0	3.0	5.0	5.5	5.3	5.1	5.3
X	—	—	—	—	13.2	1.6	21.8	2	−7.6	22	3.7	12.1	5.9	6.9	7.8	9.2	8.9	8.6	93	63	92	83	0.7	5.4	0.9	2.3	6.5	5.2	4.5	5.4
XI	—	—	—	—	3.7	−3.7	14.9	2	−21.1	18	−1.6	2.0	−0.5	−0.7	5.0	5.5	5.4	5.3	86	76	87	83	1.0	2.2	1.0	1.4	7.9	6.6	7.4	7.3
XII	—	—	—	—	4.5	−1.7	11.6	20	−7.8	15	0.4	3.3	1.4	1.6	5.2	5.7	5.5	5.5	82	73	81	79	1.2	2.2	1.4	1.6	7.6	8.1	7.4	7.7
Rok	—	—	—	—	11.7	2.1	32.4	26.VI	−28.4	7. II	5.2	10.2	6.1	6.9	8.6	9.0	9.1	8.9	86	68	86	80	1.6	5.6	1.6	2.9	7.0	7.0	6.3	6.8

Libertów — φ = 49°58' — λ = 19°53'

I	—	—	—	—	2.0	−3.8	8.0	29	−12.1	12	−2.1	0.7	−0.9	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.0	6.3	7.4
II	—	—	—	—	−3.0	−8.5	5.4	14	−19.2	6, 7	−7.3	−4.5	−5.4	−5.6	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.6	6.7	7.6
III	—	—	—	—	5.8	−1.0	15.3	30	−8.9	1	0.2	4.6	2.3	2.4	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.5	4.3	6.0
IV	—	—	—	—	10.0	2.7	15.2	7	−1.3	1, 6	4.1	8.7	6.4	6.4	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.3	6.0	6.8
V	—	—	—	—	14.6	6.8	26.0	19	−0.6	3	8.8	13.1	10.4	10.7	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.3	6.9	6.9
VI	—	—	—	—	20.7	11.6	31.1	26	7.2	10	14.1	19.1	15.7	16.2	—	—	—	—	—	—	—	—	—	—	—	—	4.8	5.3	5.4	5.2
VII	—	—	—	—	21.1	12.8	27.9	14	8.0	6	15.0	19.5	16.3	16.8	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.7	5.2	5.9
VIII	—	—	—	—	20.3	11.7	31.0	7	8.0	26	13.5	19.0	15.3	15.8	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.6	4.7	5.5
IX	—	—	—	—	20.5	11.0	28.0	3	7.2	22	12.8	18.7	14.7	15.2	—	—	—	—	—	—	—	—	—	—	—	—	4.5	4.7	2.3	3.8
X	—	—	—	—	12.3	4.0	20.4	2	−4.7	22	5.4	11.3	8.0	8.2	—	—	—	—	—	—	—	—	—	—	—	—	5.6	4.5	3.7	4.6
XI	—	—	—	—	3.4	−3.0	13.5	1, 2	−17.3	18	−1.5	1.9	0.3	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.9	6.1	6.8
XII	—	—	—	—	3.8	−1.1	10.5	19, 20	−7.7	15	0.5	2.6	1.2	1.4	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.8	6.1	6.9
Rok	—	—	—	—	11.0	3.6	31.1	26.VI	−19.2	6, 7. II	5.3	9.6	7.0	7.2	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.5	5.3	6.1

Czernichów $H_s = 218\ m$ $h_w = 17\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V V ≥ 10	V > 15	◔	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	·	·	13.5	3.0	17.5	3.1	·	·	·	·	9	3.0	44.5	3.6	8.5	3.3	·	3.3	68	23.2	3	2	3	24	·	3	·	·	16	12	11	2	11	29	1
II	3	5.0	6	6.3	3	5.0	·	·	·	·	3	7.0	42.5	5.6	26.5	5.3	·	5.6	53	9.3	27	13	20	26	·	3	·	·	16	19	11	·	7	28	·
III	1	5.0	27	4.7	13	4.1	3	2.3	·	·	8	4.7	29	4.5	12	5.0	·	4.5	39	8.2	26	5	3	22	·	1	·	1	8	13	7	·	5	15	·
IV	·	·	18	8.5	28	5.0	·	·	·	·	4.5	4.8	28.5	5.8	11	6.3	·	6.1	54	9.0	23	·	·	4	·	4	·	·	12	14	12	·	2	·	1
V	7	3.7	11	5.5	15	4.9	·	·	·	·	6.5	7.5	43.5	4.3	9	4.6	1	4.7	136	36.5	19	·	·	3	1	4	1	·	8	18	15	5	3	·	6
VI	2	4.0	6.5	3.7	19.5	3.4	7	2.6	·	·	6.5	4.3	39	4.3	9.5	4.4	·	3.9	136	28.0	27	·	·	·	7	1	·	2	5	14	14	5	1	·	6
VII	5	3.0	2.5	3.8	9.5	4.2	4	3.2	·	·	5	2.9	60	3.9	7	4.6	·	3.8	63	16.5	18	·	·	·	10	1	·	1	5	20	14	1	·	·	1
VIII	6	3.7	4	4.5	9	4.3	11	2.6	2	6.0	11	3.3	35.5	3.6	11.5	4.5	3	3.6	139	37.5	25	·	·	·	9	·	·	2	9	13	9	4	1	·	1
IX	3	3.3	3	2.7	19	2.6	1	2.0	9	2.3	6.5	2.5	44.5	2.9	4	4.5	·	2.8	99	22.5	19	·	·	·	3	·	·	5	5	12	8	4	8	·	1
X	9.5	4.1	8	4.1	22	3.1	·	·	1	2.0	·	·	42.5	3.2	10	4.4	·	3.4	2	1.5	29	·	·	13	·	·	·	1	4	5	1	·	22	·	·
XI	6	5.2	18.5	5.4	14.5	3.3	·	·	·	·	9	6.9	30	3.8	12	5.6	·	4.7	28	7.0	11	4	9	22	·	4	·	·	20	16	9	·	8	7	·
XII	6	3.7	3	5.0	13	4.0	·	·	·	·	16.5	3.9	42.5	4.0	12	5.7	·	4.2	75	15.0	18	1	2	20	·	1	·	·	14	14	11	3	3	7	·
Rok	48.5	3.4	121	4.8	183	3.9	26	1.1	12	0.9	85.5	4.2	482	4.1	133	4.8	4	4.2	892	37.5	25.VIII	25	37	134	30	22	1	12	122	170	122	24	71	86	17

Wieliczka $H_s = 225\ m$ $h_w = 20{,}4\ m$

I	2.5	3.2	15.5	1.6	4	1.0	2.5	1.2	14	3.1	28	2.2	12.5	2.6	3	2.2	11	2.0	60	11.8	3	3	9	27	·	1	·	—	—	15	11	1	6	30	1
II	5	3.8	11	2.1	1.5	1.7	·	·	3.5	3.7	29.5	3.5	21.5	3.1	9	2.5	3	3.0	37	6.3	17	7	22	26	·	·	·	—	—	20	11	·	5	28	1
III	6	2.1	12	2.2	6.5	1.9	7	1.9	7.5	1.7	26	1.5	11.5	1.6	7.5	2.2	9	1.6	45	8.7	6	1	5	20	·	·	·	—	—	18	11	·	9	16	-
IV	5.5	1.9	24.5	2.5	13	2.1	1	3.5	2.5	3.2	17	2.2	15.5	2.7	7	2.1	4	2.3	38	7.6	23	·	·	6	·	·	·	—	—	18	12	·	3	·	2
V	5	1.9	12.5	1.8	10.5	1.9	4	1.2	7.5	3.5	23	2.2	19.5	1.9	6	2.1	5	2.0	146	31.5	29	·	·	2	1	1	1	—	—	21	17	5	2	·	4
VI	5.5	1.5	11.5	1.7	8	1.4	1.5	1.3	10	2.8	18	2.2	20.5	2.4	11	1.9	4	2.0	165	35.6	27	·	·	·	7	·	·	—	—	15	15	6	·	·	7
VII	3.5	1.6	8.5	1.1	3.5	1.6	1.5	1.7	14	3.1	40.5	1.8	12	2.3	3.5	1.0	6	1.8	78	22.0	18	·	·	·	9	·	·	—	—	22	16	1	·	·	3
VIII	10	1.6	3.5	1.6	3.5	1.4	3.5	1.7	10.5	1.9	23.5	1.8	17.5	1.5	9	1.4	12	1.5	139	48.6	1	·	·	·	7	·	·	—	—	13	10	5	·	·	1
IX	3.5	1.6	10.5	1.2	5	1.8	4.5	2.1	15	1.5	25.5	1.3	16	1.6	5	1.2	5	1.4	79	17.1	4	·	·	·	3	·	·	—	—	13	8	4	2	·	-
X	8.5	1.5	18	1.4	6.5	1.6	·	·	1	4.0	28	1.4	20.5	1.5	3.5	2.1	7	1.4	6	2.7	4	·	·	8	·	·	·	—	—	6	1	·	7	·	·
XI	6	2.5	20	2.0	2	1.0	4	1.5	10	4.5	25	3.3	13	2.3	3	2.7	7	2.5	57	15.0	11	3	11	20	·	3	·	—	—	16	11	2	6	15	1
XII	5	2.3	5.5	1.4	4	1.6	4.5	2.3	22	5.5	34.5	2.7	15.5	2.1	2	2.0	·	3.0	40	9.0	3	·	1	18	·	3	·	—	—	15	9	·	2	8	-
Rok	66	2.1	153	1.7	68	1.6	34	1.5	117.5	3.2	318.5	2.2	195.5	2.1	69.5	2.0	73	2.0	890	48.6	1.VIII	14	48	127	27	6	1	—	—	192	132	24	42	97	20

Bochnia - Chodenice $H_s = 200\ m$ $h_w = 14{,}9\ m$

I	2.5	1.8	4.5	2.6	10.5	1.3	15	1.4	6.5	2.2	30	1.9	16	3.4	8	1.9	·	2.1	62	12.4	31	5	9	27	·	1	·	1	19	14	11	2	1	31	·
II	4	3.5	6	2.5	4	2.5	·	·	·	·	20.5	3.9	36.5	3.8	12	4.5	1	3.7	26	4.6	17	13	21	27	·	2	1	2	18	18	7	·	2	28	·
III	2.5	4.0	13	2.2	3.5	1.9	15	1.4	5.5	1.2	19.5	1.7	27.5	2.0	5.5	3.6	1	1.9	40	8.1	26	6	5	21	·	·	·	4	16	15	8	·	3	19	·
IV	0.5	4.0	9	2.8	24.5	2.4	11.5	2.3	3.5	1.4	14	3.0	18.5	3.5	8.5	3.4	·	2.8	26	8.0	19	·	·	8	·	2	·	2	14	11	7	·	1	·	3
V	2.5	6.8	5	2.6	13	2.0	4.5	1.4	4.5	1.4	18.5	2.8	27	2.4	18	2.6	·	2.5	93	17.2	11	·	·	4	1	3	1	2	15	20	16	2	3	·	4
VI	3.5	2.4	3.5	3.4	18.5	2.5	8	2.1	2	2.8	14	2.0	32.5	2.8	7	2.6	1	2.5	126	42.4	10	·	·	·	7	·	·	6	9	15	14	3	3	·	5
VII	0.5	1.0	2.5	1.6	5	1.6	8	1.6	9.5	2.0	35	2.0	25	2.3	5.5	1.3	2	1.9	59	14.1	8	·	·	·	7	·	·	4	7	18	14	1	1	·	7
VIII	1	3.5	1	2.0	7.5	1.3	13	1.2	7.5	1.9	21.5	1.7	21	2.1	19.5	1.5	1	1.7	151	49.1	1	·	·	·	7	·	·	5	13	14	11	4	·	·	2
IX	·	·	5	1.5	2	1.8	18	2.8	15.5	1.7	23	1.4	19.5	1.6	6	1.3	1	1.8	79	29.6	29	·	·	·	4	·	·	6	8	10	8	4	2	·	·
X	2	1.0	2.5	2.0	18	1.4	10.5	1.2	4.5	1.6	26	1.9	21	1.8	7.5	1.5	1	1.6	3	1.7	4	·	·	15	·	·	·	6	9	7	1	·	8	·	·
XI	0.5	1.0	13.5	2.3	7	1.6	14.5	1.6	6.5	1.8	17	4.6	27.5	2.7	3.5	2.7	·	2.7	39	10.2	20	4	10	20	·	3	·	2	15	15	6	1	2	11	·
XII	1	4.0	0.5	1.0	9	1.2	12	1.2	16	2.5	34.5	3.3	15.5	2.7	4.5	2.3	·	2.6	33	7.6	18	·	1	22	·	1	1	1	18	16	8	·	·	7	·
Rok	20.5	2.8	66	2.2	122.5	1.8	130	1.5	81.5	1.7	273.5	2.5	287.5	2.6	105.5	2.4	8	2.3	737	49.1	1.VIII	28	46	144	26	12	3	41	161	173	111	17	26	96	21

Libertów $H_s = 320\ m$ $h_w = 15{,}9\ m$

I	9	1.7	10.5	1.8	10	1.0	5.5	1.4	12	1.8	10.5	2.4	29.5	1.7	6	1.7	·	1.7	44	10.7	31	2	10	27	·	·	·	3	17	12	10	1	7	29	·
II	5.5	2.3	8	1.2	3.5	1.3	0.5	1.0	5.5	4.1	13	3.1	39.5	2.8	7.5	5.2	1	2.8	26	6.2	16	6	25	28	·	·	·	1	17	17	10	·	6	28	·
III	4	5.0	12.5	1.5	6.5	1.5	14.5	1.3	11.5	1.3	8.5	1.3	26.5	1.7	8	1.1	1	1.5	38	9.2	21	·	6	17	·	·	·	7	11	12	8	·	6	18	·
IV	8	1.6	23.5	1.6	18.5	1.8	1	2.0	6	1.5	6.5	2.6	20	2.2	6.5	2.8	·	1.9	35	9.8	23	·	·	5	·	1	·	4	16	12	9	·	3	·	1
V	6.5	1.9	11	1.2	13	1.7	2	1.0	9	3.3	7	1.9	34	1.7	9.5	1.2	1	1.8	104	23.3	19	·	·	2	1	1	1	5	13	18	14	3	1	·	5
VI	9	1.7	16	1.2	13	1.0	4.5	1.6	5.5	1.6	5	1.6	25.5	1.5	10.5	1.2	1	1.4	158	37.0	27	·	·	·	5	·	·	9	9	14	14	6	2	·	4
VII	6	1.0	6.5	1.8	9.5	1.0	1	1.0	14	3.0	14.5	1.4	36.5	1.5	5	1.0	·	1.6	47	11.8	18	·	·	·	8	1	·	3	7	20	14	1	·	·	2
VIII	10	1.5	3	1.0	15	1.0	4	1.2	13	1.4	6	1.3	34	1.4	7	1.7	1	1.3	136	40.6	1	·	·	·	6	·	·	7	10	9	7	6	·	·	1
IX	4	1.5	1	1.0	7	1.0	19.5	1.2	16	1.8	17	1.3	20	1.4	2.5	1.2	3	1.3	62	15.8	29	·	·	·	3	·	·	9	3	7	6	3	·	·	1
X	4.5	1.7	9.5	1.3	16.5	1.1	2	1.0	4	1.0	14.5	1.2	35	1.5	7	1.1	·	1.3	1	0.8	4	·	·	5	·	·	·	8	6	1	·	·	8	·	·
XI	6	2.0	10	1.2	10	1.3	15.5	2.0	7.5	2.7	13.5	4.4	24.5	1.4	3	1.0	·	2.1	27	9.2	20	3	10	20	·	·	·	3	14	11	6	·	3	10	·
XII	5	1.4	6.5	1.0	3.5	1.0	2	1.0	23	3.7	29	2.2	22	1.7	2	1.0	·	2.2	33	7.8	3	·	6	19	·	2	·	3	15	11	7	·	3	14	·
Rok	77.5	1.9	118	1.3	126	1.2	72	1.3	127	2.3	145	2.1	347	1.7	74.5	1.7	8	1.7	711	40.6	1.VIII	11	57	123	23	5	1	62	138	144	105	20	39	99	14

Jastrzębie-Zdrój

φ = 49°57′ λ = 18°34′

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnie				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max obs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	2.3	−4.8	7.0	29	−18.7	8	−1.5	1.6	−1.7	−0.8	5.1	5.7	5.1	5.3	92	84	93	90	0.5	1.2	0.4	0.7	7.7	7.2	7.4	7.4
II	—	—	—	—	−1.8	−9.9	3.7	14	−22.4	6	−6.7	−2.8	−6.1	−5.4	3.5	4.0	3.6	3.7	88	79	88	85	0.4	1.0	0.5	0.6	8.2	7.9	7.5	7.9
III	—	—	—	—	7.0	−2.7	17.3	30	−16.4	1	−1.1	6.2	1.2	1.9	5.5	6.3	6.0	5.9	90	66	87	81	0.6	3.7	1.0	1.8	6.0	5.9	5.5	5.8
IV	—	—	—	—	11.2	2.9	16.9	3, 4	−2.0	16	4.8	10.3	6.0	6.8	7.8	8.2	8.3	8.1	90	67	88	82	0.9	4.6	1.1	2.2	7.7	7.1	6.3	7.0
V	—	—	—	—	15.5	6.6	22.9	17, 18, 19	−1.6	3	9.5	14.2	10.1	11.0	10.8	10.9	11.1	10.9	88	67	88	81	1.4	5.8	1.5	2.9	7.1	6.6	7.2	7.0
VI	—	—	—	—	21.4	10.4	32.6	26	2.2	3	14.9	19.4	15.0	16.1	14.4	14.2	15.1	14.6	84	64	87	78	2.8	9.4	2.2	4.8	4.8	6.3	6.5	5.9
VII	—	—	—	—	21.9	11.7	30.6	15	6.0	4, 5	15.4	20.0	16.0	16.8	15.3	14.8	15.0	15.0	87	64	82	78	2.4	9.3	3.5	5.1	7.6	7.8	6.4	7.3
VIII	—	—	—	—	21.4	10.6	30.7	7, 8	5.5	28	13.5	20.1	15.0	15.9	14.1	14.4	14.8	14.4	90	62	85	79	1.7	10.1	2.8	4.9	5.3	4.7	3.8	4.6
IX	—	—	—	—	21.2	8.7	27.9	2	4.0	20	12.2	19.4	13.9	14.8	12.6	13.5	13.3	13.1	88	61	84	78	2.0	9.7	3.0	4.9	4.3	4.8	3.0	4.0
X	—	—	—	—	13.5	3.1	22.5	2	−3.7	23	4.8	12.5	7.1	7.9	—	—	—	—	—	—	—	—	—	—	—	—	6.4	4.8	3.6	4.9
XI	—	—	—	—	4.3	−2.4	14.4	1	−13.1	18	−0.5	2.5	0.5	0.8	5.6	5.8	5.7	5.7	90	78	85	84	0.7	2.0	1.1	1.3	8.6	7.2	7.4	7.7
XII	—	—	—	—	4.2	−0.9	12.1	20	−8.7	15	1.1	2.7	1.2	1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.0	7.1	8.0
Rok	—	—	—	—	11.8	2.8	32.6	26. VI	−22.4	6. II	5.5	10.5	6.5	7.2	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.5	6.0	6.5

Uwaga: W dniu 30.VI.1965 po 11 obserwacji klimatologicznej przeniesiono stację w kierunku SSW z terenu szkoły podstawowej przy ul. Włodzisławskiej na teren Szpitala Miejskiego przy ul. Zdrojowej. H_s = 262 m odnosi się do nowego miejsca. Stwierdzono, że H_s poprzedniego miejsca wynosiła 270 m (mylnie podawano 227 m).

Wadowice

φ = 49°53′ λ = 19°31′

I	—	—	—	—	3.2	−3.7	9.8	29	−13.2	8	−1.0	1.8	−0.7	−0.2	4.7	5.3	5.2	5.1	83	77	87	82	1.1	1.8	0.9	1.3	8.6	9.2	7.1	8.3
II	—	—	—	—	−2.0	−9.8	4.9	14	−22.8	10	−6.8	−3.2	−5.9	−5.4	3.2	3.5	3.3	3.3	83	73	81	79	0.7	1.4	0.8	1.0	9.3	7.4	7.7	8.1
III	—	—	—	—	6.8	−2.0	16.0	30	−13.1	1	0.2	5.4	1.6	2.2	5.5	5.8	6.0	5.8	84	63	82	76	1.4	3.7	1.2	2.1	7.1	7.1	6.4	6.9
IV	—	—	—	—	10.9	2.6	15.5	4	−1.9	2	4.8	9.5	6.3	6.7	7.2	7.7	8.0	7.6	83	67	83	78	1.5	4.4	1.7	2.5	7.2	7.6	6.6	7.1
V	—	—	—	—	15.4	6.2	27.4	19	−1.8	3	9.7	14.1	10.2	11.0	9.9	9.9	10.6	10.1	81	62	84	76	2.5	6.8	2.2	3.8	7.2	8.2	7.5	7.6
VI	—	—	—	—	21.6	10.6	31.4	26	3.6	3	14.9	19.8	14.7	16.0	14.0	14.1	14.8	14.3	82	62	87	77	3.2	9.8	2.3	5.1	6.1	6.5	7.3	6.6
VII	—	—	—	—	21.5	12.1	28.9	14	5.5	10	15.9	19.8	15.3	16.6	15.1	15.3	15.3	15.2	83	67	87	79	3.3	8.5	2.4	4.7	7.6	7.9	7.8	7.8
VIII	—	—	—	—	21.0	10.1	32.2	7	5.4	3	12.9	19.3	13.8	15.0	13.4	13.7	13.8	13.6	89	62	87	79	1.8	9.8	2.3	4.6	6.9	7.3	5.6	6.6
IX	—	—	—	—	21.1	9.0	28.5	2	4.0	22	11.8	19.1	12.7	14.1	12.7	13.6	13.2	13.2	91	62	90	81	1.4	9.2	1.7	4.1	6.2	6.3	5.1	5.9
X	—	—	—	—	13.2	1.8	21.8	2	−6.0	22	3.8	12.2	5.6	6.8	7.9	9.2	8.7	8.6	93	63	91	82	0.6	5.6	0.9	2.4	6.0	5.5	4.7	5.4
XI	—	—	—	—	4.3	−2.6	15.4	1	−15.5	18	−0.6	2.3	0.3	0.6	5.2	5.5	5.4	5.4	85	75	83	81	1.1	2.2	1.4	1.6	8.6	7.2	7.7	7.8
XII	—	—	—	—	4.8	−1.1	11.7	20	−11.8	15	1.0	3.1	1.6	1.8	5.4	5.5	5.5	5.5	82	72	79	78	1.4	2.3	1.6	1.8	8.5	8.5	7.4	8.1
Rok	—	—	—	—	11.8	2.8	32.2	7. VIII	−22.8	10. II	5.6	10.3	6.3	7.1	8.7	9.1	9.2	9.0	85	67	85	79	1.7	5.5	1.6	2.9	7.4	7.4	6.7	7.2

Żarnowa

φ = 49°52′ λ = 21°50′

I	—	—	—	—	0.9	−4.8	5.5	30	−19.6	12	−1.8	0.3	−2.0	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.5	7.7	7.8
II	—	—	—	—	−3.5	−10.8	0.5	12	−27.3	7	−8.0	−4.4	−7.2	−6.7	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.0	6.9	7.4
III	—	—	—	—	6.0	−2.5	15.8	30	−20.6	1	−0.5	4.7	1.8	2.0	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.2	5.9	6.5
IV	—	—	—	—	11.0	2.4	15.1	7	−2.5	6	4.3	9.7	6.2	6.6	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.9	6.8	7.8
V	—	—	—	—	15.7	6.0	25.4	19	−3.1	4	8.6	14.1	10.1	10.7	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.5	5.5	6.7
VI	—	—	—	—	21.9	10.6	31.8	26	4.7	3	14.7	19.9	14.5	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.4	5.3	5.8
VII	—	—	—	—	22.4	11.4	29.7	16	5.8	10	15.3	20.3	15.1	16.4	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.3	5.0	6.1
VIII	—	—	—	—	20.3	10.5	28.6	8	4.9	31	12.8	18.9	14.0	14.9	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.2	5.5	6.0
IX	—	—	—	—	20.7	9.2	27.1	2	3.0	17	12.4	19.5	13.1	14.5	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.8	2.7	4.2
X	—	—	—	—	12.4	2.8	23.6	2	−5.6	22	4.9	11.3	6.6	7.4	—	—	—	—	—	—	—	—	—	—	—	—	7.0	5.4	3.5	5.3
XI	—	—	—	—	3.4	−2.9	14.3	2	−18.5	18	−0.9	1.8	0.1	0.3	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.6	7.5	7.9
XII	—	—	—	—	2.6	−1.6	8.0	10	−9.0	15	0.1	1.5	0.5	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.5	6.9	7.5
Rok	—	—	—	—	11.2	2.5	31.8	26.VI	−27.3	7. II	5.2	9.8	6.1	6.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.8	5.8	6.6

Ochaby

φ = 49°51′ λ = 18°46′

I	—	—	—	—	2.5	−4.4	8.2	29	−13.7	8	−0.9	1.5	−1.1	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.3	7.0	7.9
II	—	—	—	—	−2.0	−10.0	3.5	14	−23.0	6	−6.8	−3.4	−5.8	−5.4	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.0	6.6	7.4
III	—	—	—	—	6.6	−1.9	16.3	30	−13.6	11	0.0	5.7	1.9	2.4	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.5	6.0	6.6
IV	—	—	—	—	10.6	2.7	16.2	3	−2.1	1	4.7	9.5	5.7	6.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.2	5.6	7.1
V	—	—	—	—	15.0	6.4	25.7	19	−2.1	3	9.4	13.6	10.0	10.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.8	7.5	7.6
VI	—	—	—	—	21.0	10.5	31.8	26	3.4	3	15.1	19.0	14.5	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.7	5.6	5.9
VII	—	—	—	—	21.4	12.2	29.9	14	6.3	5	16.1	19.9	15.5	16.8	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.8	6.1	7.1
VIII	—	—	—	—	20.8	10.6	30.8	8	5.8	28	14.0	19.4	14.2	15.4	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.6	5.6	6.0
IX	—	—	—	—	21.2	9.3	28.6	2	3.9	22	12.6	19.3	13.8	14.9	—	—	—	—	—	—	—	—	—	—	—	—	5.3	5.1	4.3	4.9
X	—	—	—	—	13.1	2.2	21.9	1, 2	−5.0	26	4.2	12.2	5.6	6.9	—	—	—	—	—	—	—	—	—	—	—	—	5.2	4.0	2.8	4.0
XI	—	—	—	—	4.0	−2.7	14.0	1, 2	−14.3	18	−0.6	2.4	0.2	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.0	6.9	7.5
XII	—	—	—	—	3.8	−1.1	9.5	19	−10.4	15	1.3	2.7	1.4	1.7	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.5	6.5	7.9
Rok	—	—	—	—	11.5	2.8	31.8	26.VI	−23.0	6. II	5.8	10.2	6.3	7.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.9	5.9	6.7

Jastrzębie - Zdrój

$H_s = 282$ m $h_w =$ 12,5 m I–VI; 16,5 m VII–XII **1965**

MIESIĄC	ROZKŁAD WIATRU nD, VmD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	◕	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5.5	1.2	12	1.1	7.5	1.2	1.5	1.7	4.5	1.4	16	2.4	20	1.8	13	1.2	13	1.4	87	14.4	9	3	3	28	·	·	·	2	15	17	14	3	—	31	·
II	8.5	1.5	14.5	1.6	1	2.0	1	1.0	2.5	1.6	11	3.0	14	2.5	27.5	1.5	4	1.8	42	8.0	17	11	22	26	·	·	·	1	16	17	12	·	—	28	·
III	3	1.3	14	1.5	4	2.1	3	1.5	4	1.1	12	2.5	17	2.0	24	1.0	12	1.4	44	9.3	6	5	4	22	·	·	·	5	7	16	11	·	—	16	·
IV	1.5	1.0	20.5	1.9	9	2.1	·	·	4.5	1.8	5	2.1	9	1.6	35.5	1.2	5	1.5	65	12.9	20	·	·	7	·	·	·	4	13	17	14	2	—	·	1
V	9	1.3	12.5	1.6	8.5	2.0	·	·	0.5	7.0	10.5	2.2	20	1.7	28	1.2	4	1.6	156	25.7	19	·	·	3	·	·	·	2	14	22	16	7	—	·	6
VI	9.5	1.1	12.5	1.1	2	1.8	2	1.0	2	1.0	11	3.4	12.5	2.6	22.5	1.2	16	1.4	143	24.6	11	·	·	·	7	·	·	4	9	15	15	7	—	·	5
VII	7	1.6	·	·	6	1.3	14	1.7	36.5	1.8	18.5	3.1	8.5	2.1	2.5	3.2	·	2.1	118	33.5	18	·	·	·	6	·	·	1	13	18	16	3	—	·	1
VIII	2	3.0	3	3.3	·	·	·	·	3.5	5.3	14	3.1	21.5	1.6	24	1.9	25	1.7	67	13.0	11	·	·	·	9	·	·	7	4	8	8	3	—	·	·
IX	0.5	1.0	·	·	·	·	0.5	1.0	12.5	2.3	40	1.7	17	1.8	8.5	1.5	11	1.6	66	19.8	19	·	·	·	3	·	·	8	4	12	8	3	—	·	·
X	7	1.9	3	3.0	18	1.7	2	1.0	5.5	1.4	16.5	2.0	16	2.2	15	1.7	11	1.7	9	2.4	31	·	·	9	·	·	·	7	6	6	4	·	—	·	·
XI	1	1.0	14	2.2	2	4.0	2	1.0	26	2.1	16	3.1	3	2.7	20	1.8	6	2.1	21	5.5	21	4	8	19	·	·	·	1	20	13	7	·	—	·	·
XII	·	·	1	3.0	8	2.1	4	2.2	37	2.5	26	3.7	6	2.5	11	2.7	·	2.8	39	6.0	22	·	1	18	·	·	·	·	20	15	10	·	—	—	·
Rok	54.5	1.3	107	1.7	66	1.7	30	1.0	139	2.4	195.5	2.7	164.5	2.1	231.5	1.7	107	1.8	857	33.5	18.VII	23	38	132	25	·	·	42	141	176	135	28	—	—	13

Wadowice

$H_s = 260$ m $h_w = 19{,}6$ m

I	1	1.0	6.5	1.0	13.5	1.2	9.5	1.3	10.5	1.8	13	3.2	17	2.5	11	1.2	11	1.6	72	16.2	31	2	3	26	·	·	·	1	20	14	12	3	—	23	·
II	2	1.0	2.5	1.2	4.5	1.3	7.5	1.0	3	1.3	20.5	3.9	30.5	2.2	8.5	3.3	5	2.4	39	6.8	8	12	23	26	·	1	·	·	20	18	12	·	—	28	·
III	6.5	1.4	7	1.0	9.5	1.8	12.5	1.1	13	1.2	11.5	2.0	18	2.5	13	1.2	2	1.6	41	10.8	21	2	5	17	·	·	·	5	16	15	8	1	—	16	·
IV	5	2.2	11	2.7	21.5	3.3	8	1.1	5	1.4	7	2.2	20.5	3.0	7	2.4	5	2.5	67	9.7	21	·	·	6	·	2	·	3	17	18	14	·	—	·	2
V	3.5	1.4	4.5	3.2	18.5	1.6	7.5	1.0	11.5	1.3	4.5	2.6	31	2.7	12	2.3	·	2.1	142	41.3	19	·	·	2	1	2	1	1	17	20	14	3	—	·	2
VI	6	1.0	4.5	1.0	9	1.6	7	1.0	7	1.0	11	1.4	22	1.8	9.5	1.2	14	1.2	163	31.4	27	·	·	·	5	·	·	1	9	15	13	5	—	·	5
VII	4.5	1.2	3	1.0	6	1.0	7	1.0	11.5	1.7	22	1.6	28	1.9	3	1.0	8	1.4	64	12.4	18	·	·	·	6	·	·	2	18	21	14	1	—	·	2
VIII	8.5	1.2	5	1.4	9	1.0	8	1.1	20	1.2	10.5	1.5	21	1.4	11	1.2	·	1.2	127	31.6	1	·	·	·	7	·	·	2	12	16	10	6	—	·	2
IX	1.5	1.3	4	1.5	8.5	1.4	22	1.1	21.5	1.5	11.5	1.2	14.5	1.4	5.5	1.2	1	1.3	89	26.8	19	·	·	·	3	1	·	3	8	9	8	4	—	·	·
X	5	1.1	5	1.5	13.5	1.6	17.5	1.0	13	1.0	9	2.6	13	2.2	13	1.7	4	1.5	6	2.5	29	·	·	15	·	·	·	6	10	6	3	·	—	·	·
XI	4.5	1.0	8.5	1.9	18.5	2.0	3	1.0	9	1.3	14	4.6	24	2.9	7.5	1.3	1	2.4	41	13.3	11	4	9	19	·	2	·	1	16	15	10	1	—	15	1
XII	2	1.0	·	·	8	1.4	4	1.5	13	2.8	33.5	3.7	25.5	2.3	7	1.6	·	2.7	45	10.5	13	1	1	18	·	3	·	·	20	18	9	1	—	7	·
Rok	50	1.2	61.5	1.4	140	1.6	113.5	1.1	138	1.5	168	2.5	265	2.2	108	1.6	51	1.8	896	41.3	19.V	21	41	129	22	11	1	25	183	185	127	25	—	89	14

Żarnowa

$H_s = 256$ m $h_w = 18{,}3$ m

I	15.5	2.3	3.5	2.7	4	1.0	6.5	1.7	46	5.2	4.5	4.8	5.5	3.5	1.5	5.0	6	3.7	56	13.1	31	4	10	26	·	3	2	2	19	18	13	1	1	31	·
II	19	2.6	2.5	3.8	·	·	1	1.0	14	5.5	3	4.3	13.5	2.3	24	2.5	7	2.9	61	12.9	8	12	25	28	·	1	·	1	14	21	17	1	2	28	·
III	26	3.0	·	·	8.5	1.4	8	2.9	30.5	4.3	6	1.8	2	4.0	7	1.6	5	3.1	60	10.2	17	3	4	16	·	4	2	4	12	16	13	1	3	13	·
IV	16.5	2.9	9.5	3.2	21.5	3.6	5	3.0	10.5	3.1	10.5	4.1	7	2.4	5.5	3.2	4	3.1	40	8.5	22	·	·	6	·	·	·	·	18	18	10	·	2	·	1
V	21.5	2.8	6.5	2.4	9	2.2	8	2.5	13	3.4	8	3.1	10.5	3.8	10.5	2.8	6	2.7	92	30.8	29	·	·	3	1	1	1	1	8	19	13	2	3	·	4
VI	17.5	2.3	4.5	2.9	6	1.0	7.5	4.6	9.5	4.4	2.5	2.6	11	4.1	16.5	2.5	15	2.5	146	33.2	10	·	·	·	6	2	1	3	7	14	12	6	1	·	5
VII	11.5	1.8	9	2.7	4.5	1.4	10.5	3.7	14	4.4	13	2.9	15	2.8	6.5	1.3	9	2.6	66	15.4	2	·	·	·	8	1	1	1	7	19	15	3	2	·	4
VIII	21.5	2.4	12.5	1.6	2	1.5	9	2.9	10	5.2	4.5	3.7	13	2.5	9.5	3.1	11	2.5	213	48.5	26	·	·	·	4	·	·	5	10	16	13	6	2	·	2
IX	7.5	1.4	1.5	1.0	2.5	1.0	20.5	2.9	29	5.3	6.5	4.5	4.5	1.9	7	3.1	11	3.2	49	19.6	11	·	·	·	3	·	·	8	3	7	6	2	5	·	·
X	17	3.0	7.5	1.5	10	1.6	6	1.8	22	2.4	2	4.0	9.5	3.0	6	3.0	13	2.1	6	2.0	11	·	·	8	·	·	·	5	8	6	2	·	5	·	·
XI	17	2.1	5.5	4.1	2	1.5	5	1.8	23.5	5.6	8	3.0	6.5	3.6	6.5	1.2	16	2.9	65	15.0	21	3	8	18	·	3	1	·	18	16	11	2	2	9	·
XII	11.5	2.2	2	2.5	4.5	1.2	9	3.1	44.5	5.6	8.5	3.2	4.5	1.4	6.5	1.6	2	3.9	42	14.0	18	·	5	22	·	3	3	1	18	16	10	1	·	7	·
Rok	202	2.4	64.5	2.4	74.5	1.4	96	2.7	266.5	4.6	77	3.5	102.5	2.9	107	2.6	105	2.9	916	48.5	26.VIII	22	52	127	22	18	11	31	142	186	135	25	28	88	16

Ochaby

$H_s = 270$ m $h_w = 18$ m

I	4.5	3.0	7	3.5	2	3.5	1.5	4.0	19	4.7	20.5	4.7	10.5	3.2	4	2.2	24	3.0	76	18.0	9	3	6	26	·	1	·	·	17	15	14	2	5	28	·
II	9	3.7	7	3.8	2.5	5.2	1.5	4.7	4	4.4	16.5	5.3	16.5	3.8	11	4.6	16	3.5	30	6.5	17	11	22	27	·	2	·	·	13	17	11	·	5	28	·
III	5	2.6	8.5	4.5	4.5	5.2	3	3.3	18.5	3.9	18.5	4.4	10	4.6	8	3.2	17	3.3	33	11.0	21	2	6	19	·	2	·	5	12	12	9	1	4	15	·
IV	9	3.2	13	4.5	5	5.5	1	1.0	11.5	3.9	11.5	4.0	11	3.4	6	3.2	22	2.9	75	9.6	24	·	·	4	·	2	·	2	14	16	15	·	4	·	2
V	6	4.2	12	4.0	8.5	4.6	1.5	3.3	7	4.3	14	4.5	9.5	3.9	7.5	3.7	27	3.0	166	33.3	29	·	·	3	1	3	·	1	16	17	16	6	·	·	7
VI	7	2.8	9.5	2.3	6	2.2	2.5	1.4	7	5.0	13	4.9	13.5	3.4	6.5	4.0	25	2.5	171	49.1	11	·	·	·	5	1	·	4	8	15	14	7	1	·	4
VII	1.5	1.7	5.5	2.1	5.5	3.5	3	1.5	12	3.3	19.5	4.8	14	5.2	2	2.2	30	2.7	106	24.7	16	·	·	·	5	·	·	1	11	20	17	4	1	·	7
VIII	8	2.9	11	2.5	4	2.5	2.5	4.0	13	4.0	9.5	3.6	6.5	2.7	8.5	2.9	30	2.1	86	22.5	25	·	·	·	7	·	·	4	10	15	8	4	2	·	3
IX	4	2.6	1.5	2.7	1.5	2.7	9.5	3.0	34	3.5	16	2.9	6	3.7	3.5	3.4	14	2.7	77	19.8	19	·	·	·	3	·	·	8	8	10	6	4	·	·	1
X	7	1.6	12.5	2.9	5.5	2.8	0.5	1.0	4.5	1.8	16	2.7	12.5	3.5	5.5	1.9	29	1.8	10	6.3	31	·	·	10	·	1	·	11	6	4	3	·	4	·	·
XI	4	2.9	9.5	3.6	12.5	2.4	1	1.0	10	6.0	29	5.2	5.5	3.2	5.5	3.2	13	3.6	34	13.2	21	3	9	22	·	7	·	2	18	11	8	1	6	12	1
XII	1.5	2.7	1.5	3.7	3	3.8	3.5	2.4	36.5	5.4	31	5.3	6.5	3.0	1.5	2.7	8	4.4	49	11.7	13	1	2	16	·	6	2	1	15	14	10	2	2	11	·
Rok	66.5	2.8	98.5	3.4	60.5	3.7	31	2.6	177	4.2	215	4.4	122	3.6	69.5	3.1	255	3.0	913	49.1	11.VI	20	45	127	21	25	2	39	148	166	131	31	34	94	25

Porąbka — φ = 49°49' — λ = 19°13' — 1965

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	—	—	—	—	3.1	−2.5	9.4	30	−11.5	8	−0.3	2.1	−0.2	0.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.3	5.9	7.1
II	—	—	—	—	−2.1	−9.4	4.4	14	−21.4	10	−7.3	−3.4	−5.8	−5.6	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.2	6.9	7.0
III	—	—	—	—	6.8	−1.7	15.9	30	−13.0	11	0.0	5.6	1.6	2.2	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.0	5.5	6.1
IV	—	—	—	—	10.5	2.6	15.5	4	−2.0	2	4.5	9.2	5.8	6.3	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.0	5.6	6.6
V	—	—	—	—	15.1	6.0	25.8	19	−3.0	2	9.2	13.8	9.4	10.4	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.7	6.2	6.4
VI	—	—	—	—	21.5	10.6	31.7	26	5.3	3	14.4	19.6	14.2	15.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.2	12.5	29.9	15	7.4	11	15.7	19.8	15.2	16.5	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.5	5.5	6.0
VIII	—	—	—	—	20.6	10.8	30.9	8	6.4	31	13.2	19.6	13.9	15.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	21.1	9.8	27.9	2	4.3	22	12.8	19.2	13.5	14.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	13.5	3.0	21.8	1, 2	−5.0	22	4.9	12.5	6.2	7.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	4.3	−2.6	14.0	1, 2	−14.1	18	−0.2	2.5	0.4	0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.3	6.8	7.0
XII	—	—	—	—	4.0	−1.1	11.9	20	−10.0	15	1.5	2.6	1.5	1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.5	6.7	7.2
Rok	—	—	—	—	11.6	3.2	31.7	26.VI	−21.4	10, 11	5.7	10.3	6.3	7.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Myślenice — φ = 49°49' — λ = 19°56

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	—	—	—	—	3.1	−2.9	10.9	30	−12.7	8	−1.1	2.3	−0.5	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.5	6.6	7.2
II	—	—	—	—	−2.0	−9.5	4.5	14	−26.5	7	−7.3	−3.1	−6.0	−5.6	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.0	7.8	7.4
III	—	—	—	—	7.0	−2.2	17.0	30	−13.9	11	0.2	6.0	1.5	2.3	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.1	6.2	6.4
IV	—	—	—	—	11.0	2.4	17.0	7	−1.7	2	4.6	10.0	5.9	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.2	6.6	7.1
V	—	—	—	—	15.5	6.0	27.1	19	−2.3	3	9.2	14.3	9.5	10.6	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.7	6.6	6.8
VI	—	—	—	—	21.9	10.5	31.5	26	4.3	3	14.1	20.9	14.3	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.1	5.3	6.2	5.5
VII	—	—	—	—	21.8	11.6	28.9	15	5.9	10, 11	15.5	19.8	14.8	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.2	4.7	5.9
VIII	—	—	—	—	20.6	10.4	31.3	8	5.4	31	12.8	19.3	13.6	14.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.9	5.6	6.3
IX	—	—	—	—	21.2	9.1	27.8	2	4.3	22	11.6	19.5	12.5	14.0	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.3	4.5	5.2
X	—	—	—	—	14.1	2.7	22.2	1	−4.6	22	4.5	13.4	6.2	7.6	—	—	—	—	—	—	—	—	—	—	—	—	6.1	4.8	4.1	5.0
XI	—	—	—	—	4.2	−3.0	14.4	2	−15.2	18	−0.9	2.7	−0.2	0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.1	7.3	7.4
XII	—	—	—	—	4.5	−1.1	11.0	20	−9.7	15	0.8	3.3	1.3	1.7	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.9	6.5	7.1
Rok	—	—	—	—	11.9	2.8	31.5	26.VI	−26.5	7, 11	5.3	10.7	6.1	7.0	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.7	6.1	6.5

Aleksandrowice — φ = 49°48' — λ = 19°00'

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	963.4	976.0	941.4	1013.1	2.5	−3.3	8.7	29	−13.0	8	−0.3	1.1	−0.5	0.0	4.8	5.1	4.9	4.9	80	78	82	80	1.4	1.7	1.2	1.4	8.5	8.9	7.5	8.3
II	967.3	980.6	948.6	1018.4	−2.8	−9.5	3.0	14	−20.9	6	−7.4	−4.3	−6.0	−5.9	3.2	3.5	3.3	3.3	87	78	83	83	0.5	1.0	0.7	0.7	8.5	7.3	7.4	7.7
III	968.1	984.1	941.0	1017.5	6.1	−1.1	15.8	30	−11.9	11	0.6	4.8	2.1	2.4	5.4	5.7	5.7	5.6	80	66	76	74	1.4	3.4	1.8	2.2	7.1	6.8	5.6	6.5
IV	962.1	980.4	947.2	1010.6	9.8	2.3	14.8	3, 4	−2.4	2	4.8	8.6	5.8	6.2	7.3	7.6	7.4	7.4	84	70	80	78	1.4	3.8	1.9	2.4	8.4	7.6	6.6	7.5
V	965.9	979.0	952.2	1013.9	14.0	5.5	24.6	19	−3.0	3	9.1	12.6	9.5	10.2	9.7	10.0	9.9	9.9	82	69	82	78	2.3	5.1	2.2	3.2	8.2	8.5	7.9	8.2
VI	967.2	976.7	955.3	1014.2	20.4	10.2	31.2	26	3.7	3	14.4	18.3	14.4	15.4	13.5	13.9	13.5	13.6	81	67	82	77	3.3	8.2	3.4	5.0	5.9	7.0	7.2	6.7
VII	966.2	973.5	956.6	1013.2	20.4	12.0	28.0	14	5.0	4	15.5	18.9	15.2	16.2	14.0	14.6	13.8	14.1	79	67	79	75	3.9	7.8	3.8	5.2	6.9	8.2	7.4	7.5
VIII	969.1	976.0	958.6	1016.5	19.6	10.5	29.4	8	5.0	31	13.5	18.4	14.0	15.0	12.7	12.4	12.2	12.4	83	61	77	74	3.3	9.6	4.3	5.7	5.7	7.0	5.6	6.1
IX	968.5	985.5	956.3	1015.8	20.2	9.8	26.3	3	4.6	22	13.1	18.2	13.9	14.8	11.8	12.6	11.8	12.1	78	62	75	72	3.7	8.8	4.5	5.7	6.1	6.0	4.6	5.6
X	975.1	986.5	966.2	1024.1	12.6	3.2	21.9	2	−4.3	23	5.4	11.8	6.9	7.8	7.9	9.2	8.2	8.4	85	65	79	76	1.5	5.2	2.1	2.9	5.2	4.8	4.2	4.7
XI	963.1	983.1	936.9	1012.8	4.0	−3.1	13.5	2	−12.9	17, 18	−0.7	1.9	0.1	0.4	4.9	5.4	5.2	5.2	83	76	82	80	1.2	2.1	1.4	1.6	8.1	7.0	7.6	7.6
XII	959.4	976.7	940.5	1008.6	3.7	−1.6	12.4	20	−11.8	15	1.0	2.1	1.2	1.4	5.2	5.3	5.2	5.2	79	73	77	76	1.5	2.0	1.6	1.7	8.1	8.6	7.7	8.1
Rok	966.3	986.5	936.9	1014.9	10.9	2.9	31.2	26.VI	−20.9	6, 11	5.8	9.4	6.4	7.0	8.4	8.8	8.4	8.5	82	69	80	77	2.1	4.9	2.4	3.1	7.2	7.3	6.6	7.0

Leskowiec — φ = 49°48' — λ = 19°27'

Miesiąc	Ciśnienie P: P_m	Max	Min	$P_{o.m}$	Temperatura T: — Max	— Min	Max abs.	Data	Min abs.	Data	Średnia: I	II	III	Dies	Średnia prężność pary e_m: I	II	III	Dies	Średnia wilgotność względna U_m: I	II	III	Dies	Średni niedosyt wilgotności Δ_m: I	II	III	Dies	Średnie zachmurzenie N_m: I	II	III	Dies
I	—	—	—	—	0.1	−4.2	4.7	30	−10.7	7, 8	−3.0	−1.8	−2.6	−2.5	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.6	7.3	8.1
II	—	—	—	—	−5.7	−11.1	−0.4	14	−19.8	6	−9.8	−7.2	−9.0	−8.8	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.0	8.3	8.3
III	—	—	—	—	3.1	−3.3	11.3	30	−11.4	1	−2.0	1.0	−0.8	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.0	7.2	7.3
IV	—	—	—	—	6.9	0.5	11.9	7	−6.1	1	2.0	5.0	2.8	3.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.2	7.3	7.8
V	—	—	—	—	11.8	3.9	23.1	19	−4.5	2	6.0	9.7	6.8	7.3	—	—	—	—	—	—	—	—	—	—	—	—	7.5	8.4	7.9	7.9
VI	—	—	—	—	17.3	9.4	28.1	26	5.0	13	11.9	15.1	12.1	12.8	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.9	6.5	6.5
VII	—	—	—	—	17.4	10.3	24.9	15	5.2	6	12.8	15.3	12.5	13.3	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.0	6.8	7.3
VIII	—	—	—	—	16.6	9.5	27.5	7	4.9	27	11.2	14.9	12.0	12.5	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.3	6.4	6.8
IX	—	—	—	—	17.2	9.1	23.5	2	4.7	20	11.1	14.7	12.1	12.5	—	—	—	—	—	—	—	—	—	—	—	—	6.1	6.5	5.6	6.1
X	—	—	—	—	10.5	3.5	20.4	2	−3.3	21, 22	5.3	8.9	5.6	6.4	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.1	4.7	5.2
XI	—	—	—	—	1.7	−4.1	10.7	7	−12.3	17	−2.5	−0.3	−1.9	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.4	7.8	7.8
XII	—	—	—	—	0.3	−4.3	6.9	21	−11.1	15	−2.5	−1.6	−2.4	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.1	7.2	7.5
Rok	—	—	—	—	8.1	1.6	28.1	26.VI	−19.8	6, 11	3.4	6.1	3.9	4.3	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.5	6.9	7.2

Porąbka — $H_s = 315\ m$ — $h_w = 17\ m$ — 1965

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	9	1.1	0.5	3.0	1	1.0	2.5	5.0	20.5	3.9	33.5	2.7	8.5	1.8	6.5	1.0	11	2.3	99	17.0	31	2	6	25	·	1	1	4	15	14	13	4	8	24	
II	21	1.7	0.5	4.0	·	·	0.5	7.0	10	4.3	29.5	2.6	9.5	1.6	12	1.7	1	2.3	53	6.4	16	9	22	27	·	1	·	3	16	17	12	·	1	28	
III	18	1.7	1.5	1.0	·	·	1	1.0	13.5	2.1	36.5	1.9	8	1.9	5.5	1.6	9	1.7	35	11.4	21	2	5	17	·	·	·	6	12	15	11	1	6	16	
IV	20.5	1.5	4.5	2.1	·	·	4.5	3.4	12.5	2.0	21	2.0	7.5	1.0	5.5	2.4	14	1.6	101	21.7	23	·	·	2	·	·	·	4	13	20	15	3	9	·	3
V	17.5	1.7	3	2.3	1	4.0	1	4.0	9.5	2.5	31	1.7	7	1.6	13	1.5	10	1.6	190	32.7	19	·	·	3	1	1	·	5	12	21	18	8	4	·	5
VI	17.5	1.4	1.5	1.0	1	1.0	0.5	3.0	10	3.0	27.5	2.0	5.5	1.4	9.5	1.1	17	1.5	224	55.4	11	·	·	·	7	1	·	—	—	13	13	6	2	·	8
VII	10	1.2	1	2.0	1	2.0	2	2.0	20	2.9	34	1.2	9.5	2.2	3.5	1.1	12	1.6	96	33.5	18	·	·	·	5	1	·	2	7	18	15	2	1	·	3
VIII	15	1.0	0.5	1.0	·	·	1.5	2.7	11.5	3.6	38.5	1.4	6.5	1.2	8.5	1.1	11	1.4	127	24.0	1	·	·	·	7	·	·	—	—	14	12	4	7	·	3
IX	6	1.0	1	1.0	2	1.0	4.5	1.7	25.5	2.2	40.5	2.0	1.5	1.3	3	1.0	6	1.8	99	33.1	19	·	·	·	2	2	·	—	—	11	8	4	3	·	1
X	12	1.0	2.5	1.6	·	·	1	2.0	10	2.0	42	1.9	2.5	1.0	10	1.0	13	1.4	22	11.2	31	·	·	8	·	·	·	—	—	7	5	1	10	·	·
XI	17	1.3	0.5	1.0	·	·	1	4.0	17.5	5.2	25	2.3	5.5	1.0	7.5	1.4	16	2.1	53	18.0	11	3	9	19	·	4	2	5	16	15	10	1	9	12	1
XII	5.5	1.0	·	·	·	·	2.5	5.0	34	4.1	35.5	2.1	3	1.0	9.5	1.7	3	2.7	68	18.2	18	·	2	16	·	5	2	1	14	15	13	2	1	12	·
Rok	169	1.3	17	1.7	6	0.8	22.5	3.4	194.5	3.2	394.5	2.0	74.5	1.4	94	1.4	123	1.8	1167	55.4	11.VI	16	44	117	22	16	5	—	—	180	145	36	61	92	24

Myślenice — $H_s = 295\ m$ — $h_w = 16{,}8\ m$ I–IX, $17{,}3\ m$ X–XII

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	1.7	·	·	·	·	1	2.0	12	5.1	32	3.2	7	2.3	0.5	3.0	36	2.1	76	19.1	31	2	6	25	·	2	1	2	14	14	12	3	2	21	·
II	6	1.8	·	·	·	·	·	·	12	4.5	28.5	3.8	9.5	2.5	3	2.0	25	2.4	66	8.3	8	9	22	27	·	2	·	3	14	20	16	·	2	28	·
III	10.5	1.5	0.5	2.0	·	·	1	2.0	18	2.4	30.5	3.0	8.5	2.2	3	1.8	21	1.9	36	5.9	27	2	4	18	·	·	·	6	13	16	13	·	6	15	·
IV	14	2.0	9.5	2.3	1.5	2.7	3	2.0	8.5	2.4	24.5	2.5	5.5	2.7	4.5	1.6	19	1.8	59	12.5	22	·	·	4	·	·	·	4	17	17	12	1	6	·	2
V	9	1.5	3	2.2	·	·	·	·	4	2.6	22.5	2.8	18	2.0	2.5	2.8	34	1.5	145	21.2	29	·	·	3	1	2	2	2	14	22	16	6	3	·	4
VI	8	1.5	2	2.5	1	2.0	·	·	8	2.7	22.5	2.1	7	1.3	1.5	1.7	40	1.1	215	51.1	10	·	·	·	7	·	·	4	6	15	14	7	2	·	5
VII	4	1.4	0.5	3.0	1	2.0	2	4.0	18.5	2.8	29.5	2.0	8	1.6	0.5	2.0	29	1.5	103	41.2	17	·	·	·	9	·	·	4	6	21	16	1	3	·	6
VIII	5.5	1.5	·	·	0.5	1.0	2	1.8	9.5	2.5	31.5	2.4	1.5	2.7	4.5	1.7	38	1.3	169	60.0	1	·	·	·	7	·	·	4	15	16	13	6	8	·	2
IX	3	1.7	·	·	1.5	2.3	1	3.0	7	2.9	38.5	2.6	5	2.5	·	·	34	1.6	77	14.3	11	·	·	·	3	1	1	6	6	11	8	4	4	·	·
X	4.5	2.4	6.5	2.0	6.5	1.8	3.5	1.9	6.5	1.6	34	2.8	9	2.6	1.5	2.0	21	1.9	9	2.5	11	·	·	9	·	·	·	8	10	6	5	·	14	·	·
XI	2	1.8	8	1.7	4	1.8	·	·	16.5	5.3	21.5	3.7	2	1.8	1	1.0	35	2.2	53	17.0	11	3	9	22	·	2	2	3	18	15	10	1	15	15	·
XII	·	·	·	·	1	2.0	1.5	3.3	29	3.3	30.5	5.1	7	2.8	1	2.0	23	3.0	52	10.1	18	·	2	18	·	5	1	2	14	17	11	1	3	8	·
Rok	71	1.6	30	1.3	17	1.3	15	1.7	149.5	3.2	346	3.0	88	2.2	23.5	1.8	355	1.9	1060	60.0	1.VIII	16	43	126	27	14	7	48	147	190	146	30	68	87	19

Aleksandrowice — $H_s = 398\ m$ — $H_b = 403{,}4\ m$ — $h_w = 20\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6.5	1.6	3.5	3.0	8	3.2	12	3.8	18	8.5	17	6.1	17	3.8	6	1.6	5	4.5	82	15.7	31	2	8	26	·	10	5	·	19	15	13	3	5	28	·
II	6	2.3	6.5	3.1	4	2.5	6.5	2.5	3.5	6.7	20	6.5	28	4.4	8.5	2.8	1	4.3	65	9.7	17	8	24	28	·	6	2	·	16	21	15	·	5	28	·
III	4.5	2.6	8	4.0	12.5	4.0	12	4.0	11.5	5.8	19.5	5.4	13	3.9	9	2.7	3	4.2	39	9.7	21	1	6	16	·	12	·	5	13	18	11	·	5	16	·
IV	5	3.1	15	4.2	16	3.6	6.5	3.0	7	6.1	13.5	4.4	18.5	3.7	5.5	2.1	3	3.7	95	15.2	20	·	·	6	·	3	·	1	17	19	15	3	6	1	1
V	2.5	2.2	5	3.7	17	3.3	9	2.3	8	6.8	19	4.4	17	3.1	13.5	2.0	2	3.5	146	32.0	19	·	·	4	·	8	·	1	20	20	16	5	2	1	4
VI	7.5	2.1	4.5	2.3	9	2.7	8	3.0	7.5	4.5	18	4.2	17.5	3.5	11	3.2	7	3.1	225	55.6	11	·	·	·	5	5	·	1	10	15	14	7	2	·	6
VII	4.5	1.9	5.5	2.5	6.5	2.7	11	2.6	9.5	5.3	22.5	5.1	21.5	4.0	7	2.1	5	3.6	85	27.0	18	·	·	·	3	5	·	1	13	23	14	3	5	·	4
VIII	7.5	2.0	4.5	1.6	14.5	2.6	12	3.6	10	4.4	18	3.5	13	2.7	8.5	2.5	5	2.9	135	40.8	25	·	·	·	4	5	·	4	10	14	11	4	·	·	2
IX	0.5	3.0	3.5	2.6	15	2.5	24	4.2	16	6.9	11	3.9	8	3.1	7	2.1	5	3.8	88	27.3	19	·	·	·	2	14	1	4	6	10	7	4	1	·	2
X	2.5	1.0	10	2.4	12	2.5	13.5	2.1	7	3.1	17.5	3.6	7.5	2.9	9	1.8	14	2.2	16	8.4	31	·	·	9	·	1	·	10	8	6	4	·	6	·	·
XI	5.5	1.9	7	4.4	12	3.1	6.5	3.2	8	13.1	16	7.5	14.5	4.3	7.5	2.8	13	4.5	53	14.4	1	3	9	20	·	11	3	1	19	15	11	2	9	15	1
XII	3	1.7	1.5	3.0	7	3.9	5.5	4.5	21	8.6	33	7.1	11.5	4.7	6.5	2.7	4	5.9	49	10.2	13	1	4	21	·	15	6	·	20	17	12	1	5	13	·
Rok	55.5	2.1	74.5	3.1	133.5	3.0	126.5	3.2	127	6.6	225	5.1	187	3.7	99	2.4	67	3.8	1078	55.6	11.VI	15	51	130	14	95	17	28	171	193	143	32	51	102	20

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Leskowiec — $H_s = 870\ m$ — $h_w = 16\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2.5	7.4	11.5	3.0	4.5	4.7	6.5	5.5	29.5	9.3	10	6.9	11	2.9	11.5	4.1	6	5.7	98	15.8	31	2	15	27	·	11	8	1	18	16	13	6	14	31	·
II	13	3.6	10.5	4.7	2.5	5.0	2	9.5	5.5	8.0	3.5	9.1	28	5.0	15	4.2	4	4.8	157	24.2	16	17	28	28	·	6	3	·	17	21	18	6	18	28	·
III	4	2.4	2.5	3.2	5	4.8	2	3.0	23	8.1	15	5.7	21.5	3.9	4	5.9	16	4.6	50	12.7	21	1	9	21	·	9	4	3	18	17	10	1	16	26	·
IV	7	3.1	6	3.0	22	4.8	2	3.0	9.5	5.1	3.5	4.9	20.5	3.3	8.5	4.6	11	3.6	99	27.3	22	·	·	9	·	3	·	·	17	19	17	4	16	2	1
V	4	2.9	5	3.9	16	4.9	1	6.0	12.5	8.6	3.5	4.3	24	3.7	16	5.1	11	4.4	193	49.3	19	·	·	5	·	6	2	1	17	21	18	5	17	1	3
VI	9	2.6	10	3.4	8	3.2	4	3.2	13.5	6.7	3.5	4.9	12.5	4.3	20.5	5.0	9	4.0	309	62.4	11	·	·	·	2	3	·	2	9	14	14	10	10	·	4
VII	3.5	1.7	5	2.4	19	2.9	8	4.9	19.5	6.7	8.5	4.6	10	4.1	11.5	2.9	8	3.8	101	19.0	18	·	·	·	·	3	·	2	12	22	17	2	14	·	2
VIII	12	1.9	6	3.3	5	4.6	4.5	4.2	16.5	7.4	2	4.5	18	4.6	17	2.6	12	3.7	202	41.9	1	·	·	·	2	5	·	2	11	14	10	6	10	·	1
IX	4	2.6	5	2.3	8.5	5.4	7.5	6.6	33	8.1	11	5.7	6	4.5	10	2.8	5	5.6	117	33.3	19	·	·	·	·	11	2	4	9	12	9	4	8	·	·
X	7	1.9	7.5	3.2	18	5.3	7.5	5.5	11.5	9.0	1	9.0	21.5	4.6	5	4.6	14	4.4	23	6.0	31	·	·	6	·	7	1	6	7	11	6	·	12	·	
XI	6.5	3.5	6	3.7	8	6.6	6	8.2	20	11.0	11	5.7	14	3.9	7.5	3.3	11	5.7	64	9.2	11	6	11	23	·	11	6	2	19	17	12	·	15	19	1
XII	2.5	4.8	5.5	4.4	3.5	2.3	6	6.9	30.5	11.3	11	9.1	21	4.5	7	5.3	6	7.1	97	14.8	13	2	13	27	·	16	6	·	16	20	18	3	16	30	
Rok	75	3.2	80.5	3.4	120	4.5	57	5.5	224.5	8.3	83.5	6.2	208	4.1	133.5	4.2	113	4.8	1510	62.4	11.VI	28	76	146	4	91	32	23	170	204	162	47	166	137	12

Uwaga. Prędkości wiatru oceniano wg skali Beauforta i wyrażano w m/s.

Dynów — φ = 49°48' — λ = 22°14' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{u.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień
I	—	—	—	—	1.0	−4.7	6.6	30	−20.1	12	−2.5	−0.1	−1.9	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.0	7.2	7.7
II	—	—	—	—	−3.6	−10.0	1.4	12	−25.0	7	−8.3	−4.6	−7.1	−6.8	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.2	7.4	7.7
III	—	—	—	—	6.1	−3.0	15.7	30	−20.7	1	−1.3	5.0	1.4	1.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.3	6.9	6.9
IV	—	—	—	—	11.0	2.3	15.9	26	−1.6	11	3.9	9.8	5.8	6.3	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.6	6.6	7.1
V	—	—	—	—	15.7	6.0	26.2	18	−3.1	4	8.8	14.1	10.3	10.9	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.7	7.0	7.2
VI	—	—	—	—	21.1	10.8	30.7	26	5.0	8	14.5	19.8	15.3	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.9	6.5	6.4
VII	—	—	—	—	21.9	12.0	28.7	16, 17	6.2	12	15.0	20.5	15.6	16.7	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.9	5.8	6.2
VIII	—	—	—	—	20.0	10.5	29.7	8	5.4	17	12.6	19.0	13.9	14.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.2	6.2	6.7
IX	—	—	—	—	20.8	8.8	25.2	3, 25	2.6	17	11.3	19.8	12.9	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.7	5.3	3.5	4.8
X	—	—	—	—	12.1	3.4	22.8	1	−5.1	22	5.1	11.3	6.7	7.4	—	—	—	—	—	—	—	—	—	—	—	—	7.6	5.5	5.1	6.1
XI	—	—	—	—	3.3	−2.8	14.8	2	−20.8	18	−1.2	1.9	0.0	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.6	7.2	7.7
XII	—	—	—	—	1.9	−1.9	8.2	21	−11.3	17	−0.5	1.4	0.0	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.1	8.1	7.7	8.0
Rok	—	—	—	—	10.9	2.6	30.7	26, VI	−25.0	7. II	4.8	9.8	6.1	6.7	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.9	6.4	6.9

Przemyśl — φ = 49°48' — λ = 22°46'

I	984.6	999.6	959.3	1014.6	1.1	−4.7	8.8	30	−18.2	12	−2.5	−0.1	−1.7	−1.5	4.6	4.8	4.9	4.8	87	78	87	84	0.8	1.5	0.8	1.0	7.5	7.6	7.5	7.5
II	986.2	1000.7	964.4	1016.8	−3.1	−9.6	2.6	12, 14	−21.8	7	−7.2	−4.0	−6.7	−6.2	3.3	3.5	3.3	3.4	88	76	84	83	0.5	1.2	0.6	0.8	8.2	7.1	6.7	7.3
III	989.0	1003.9	962.1	1018.8	6.4	−2.8	16.3	30	−17.2	1	−1.2	5.2	1.7	1.8	5.2	5.9	5.8	5.6	89	67	82	79	0.6	3.4	1.3	1.8	6.5	6.2	5.4	6.0
IV	982.7	998.4	964.5	1011.8	10.5	2.4	16.7	18	−1.8	11	3.9	9.3	6.2	6.4	7.2	7.6	7.6	7.5	88	66	80	78	1.0	4.5	2.0	2.5	7.5	8.2	6.3	7.3
V	985.5	1000.1	975.7	1014.2	15.9	6.3	27.8	19	−2.2	4	8.9	13.8	11.0	11.2	10.0	10.0	10.5	10.2	86	62	78	75	1.9	6.6	3.1	3.9	6.6	7.9	6.2	6.9
VI	986.4	993.4	973.7	1014.4	21.5	11.4	29.9	26	6.5	8	14.9	19.9	15.9	16.6	14.3	13.8	14.9	14.3	84	61	82	76	2.8	10.2	3.5	5.5	5.1	6.4	5.2	5.6
VII	985.8	993.2	976.2	1013.7	22.0	12.2	28.9	17	7.2	12	15.2	20.4	16.1	17.0	15.3	15.5	15.7	15.5	88	65	85	79	2.2	9.1	2.4	4.7	4.8	6.8	4.9	5.5
VIII	988.1	996.1	969.8	1016.5	20.6	10.6	30.7	8	6.2	17	12.9	18.9	14.2	15.0	13.7	14.0	14.2	14.0	91	66	87	81	1.5	9.0	2.5	4.3	5.3	6.5	4.5	5.4
IX	989.4	1005.0	979.6	1017.8	21.4	9.2	26.6	3	1.4	17	11.4	20.0	13.7	14.7	12.3	14.0	13.7	13.3	91	61	87	80	1.5	9.9	2.2	4.5	5.2	5.8	3.3	4.8
X	994.8	1008.0	984.5	1024.0	12.5	3.4	21.4	1, 2	−3.1	22	5.2	11.3	7.2	7.7	8.3	8.9	8.7	8.6	91	66	84	80	0.8	5.2	1.7	2.6	6.7	6.4	4.6	5.9
XI	984.3	1001.6	960.9	1014.1	3.3	−3.0	16.0	2	−21.0	18	−1.1	1.7	−0.3	0.0	5.2	5.5	5.3	5.3	86	77	84	82	1.0	2.1	1.2	1.4	8.4	7.5	7.5	7.8
XII	980.4	994.6	961.9	1010.0	3.9	−1.7	11.3	21	−14.4	17	0.5	2.5	0.8	1.2	5.3	5.4	5.4	5.4	82	73	82	79	1.2	2.1	1.3	1.5	7.7	7.7	7.4	7.6
Rok	986.4	1008.0	959.3	1015.5	11.3	2.8	30.7	8. VIII	−21.8	7. II	5.1	9.9	6.5	7.0	8.7	9.1	9.2	9.0	88	68	84	80	1.3	5.4	1.9	2.9	6.6	7.0	5.8	6.5

Międzybrodzie Bialskie — φ = 49°47' — λ = 19°12'

I	—	—	—	—	2.7	−3.1	8.7	29	−13.8	7	−0.6	1.4	−0.6	−0.1	4.8	5.2	4.9	5.0	83	78	84	82	1.1	1.7	1.1	1.3	8.5	8.5	7.5	8.2
II	—	—	—	—	−2.4	−10.5	4.5	14	−26.2	10	−7.9	−3.7	−6.0	−5.9	3.1	3.6	3.3	3.3	83	75	81	80	0.6	1.2	0.7	0.8	8.4	7.5	7.4	7.8
III	—	—	—	—	6.2	−2.2	15.4	30	−14.5	11	−0.4	4.8	1.6	1.9	5.3	5.6	5.6	5.5	84	65	78	76	1.0	3.4	1.5	2.0	7.0	6.9	4.8	6.2
IV	—	—	—	—	9.9	2.4	14.9	3	−2.2	2	4.1	8.4	5.9	6.1	7.4	7.5	7.7	7.5	90	69	83	81	0.9	3.8	1.6	2.1	7.6	7.4	5.7	6.9
V	—	—	—	—	14.5	6.1	25.5	19	−2.2	3	8.7	13.0	9.7	10.3	9.6	9.8	10.3	9.9	84	65	84	78	2.2	5.8	2.0	3.3	7.2	7.9	6.6	7.2
VI	—	—	—	—	20.4	10.1	31.0	26	3.8	3	13.9	18.6	14.6	15.4	13.0	13.1	13.8	13.3	82	62	84	76	3.1	9.2	3.0	5.1	5.4	6.3	6.6	6.1
VII	—	—	—	—	20.7	11.9	28.8	14	5.8	4	15.1	19.4	15.3	16.3	14.7	15.0	14.9	14.9	85	67	85	79	2.7	8.2	2.7	4.5	6.8	7.8	7.0	7.2
VIII	—	—	—	—	20.1	10.3	29.8	8	5.4	31	12.5	18.8	14.3	15.0	12.7	12.8	13.4	13.0	88	60	82	77	2.1	9.9	3.5	5.2	5.8	6.7	4.9	5.8
IX	—	—	—	—	20.4	9.3	26.7	2, 3	3.1	22	12.0	18.8	13.9	14.6	11.8	12.1	12.8	12.2	85	57	81	74	2.6	10.2	3.5	5.4	6.7	5.5	3.6	5.3
X	—	—	—	—	13.2	2.4	22.6	2	−5.8	22	4.1	12.1	6.0	7.0	7.7	9.3	8.6	8.5	90	65	89	81	0.9	5.5	1.2	2.5	7.0	4.4	3.4	4.9
XI	—	—	—	—	4.1	−2.9	13.7	2	−15.7	18	−0.6	2.1	0.1	0.4	5.3	5.5	5.5	5.4	86	75	86	82	0.9	2.0	1.1	1.3	8.4	7.0	7.2	7.5
XII	—	—	—	—	3.8	−1.5	10.5	20	−10.2	15	1.2	2.2	1.2	1.4	5.4	5.4	5.4	5.4	81	75	81	79	1.4	1.9	1.4	1.6	8.3	8.5	7.2	8.0
Rok	—	—	—	—	11.1	2.7	31.0	26.VI	−26.2	10. II	5.2	9.7	6.3	6.9	8.4	8.7	8.8	8.6	85	68	83	79	1.6	5.2	1.9	2.9	7.3	7.0	6.0	6.8

Ciężkowice — φ = 49°47' — λ = 20°58'

I	—	—	—	—	1.4	−5.5	6.5	30	−17.5	12	−2.5	0.3	−2.0	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.5	7.3	7.6
II	—	—	—	—	−2.5	−10.9	5.4	14	−27.6	7	−8.1	−3.7	−7.2	−6.6	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.8	7.2	7.7
III	—	—	—	—	6.4	−3.3	16.1	30	−20.5	1	−1.2	5.1	1.2	1.6	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.7	6.7	6.6
IV	—	—	—	—	11.3	2.2	17.3	7	−2.4	6	3.8	10.0	6.2	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.4	8.1	6.8	7.4
V	—	—	—	—	15.8	6.0	26.8	19	−2.8	3	8.3	14.1	10.3	10.8	—	—	—	—	—	—	—	—	—	—	—	—	6.7	8.3	7.1	7.4
VI	—	—	—	—	22.1	10.6	32.1	26	4.2	3	14.1	20.6	15.2	16.3	—	—	—	—	—	—	—	—	—	—	—	—	4.9	5.8	6.3	5.7
VII	—	—	—	—	22.2	11.2	28.9	16	5.4	10	14.5	20.4	15.4	16.4	—	—	—	—	—	—	—	—	—	—	—	—	6.3	7.3	5.4	6.3
VIII	—	—	—	—	20.6	10.3	31.3	8	6.4	31	12.4	19.2	14.1	15.0	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.4	6.1	6.3
IX	—	—	—	—	21.2	8.8	25.7	2, 11	2.5	22	11.2	19.8	13.2	14.4	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.1	3.7	4.8
X	—	—	—	—	13.1	2.2	24.8	2	−6.2	22	3.8	12.3	6.2	7.1	—	—	—	—	—	—	—	—	—	—	—	—	4.8	5.2	5.0	5.0
XI	—	—	—	—	3.9	−3.0	15.6	2	−17.6	18	−1.1	2.5	−0.2	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.3	7.6	7.5
XII	—	—	—	—	3.1	−2.1	8.2	10	−12.2	17	−0.4	2.1	0.1	0.5	—	—	—	—	—	—	—	—	—	—	—	—	7.7	8.0	7.6	7.8
Rok	—	—	—	—	11.6	2.2	32.1	26.VI	−27.6	7. II	4.6	10.2	6.0	6.7	—	—	—	—	—	—	—	—	—	—	—	—	6.7	7.0	6.4	6.7

Dynów

$H_s = 276\ m$ $h_w = 18{,}6\ m$ **1965**

MIESIĄC	ROZKŁAD WIATRU =0,V=0 N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥30°	Wiatr V V≥10	V≥15	◐	◓	Opad R n≥0,1	n≥1,0	n≥10,0	≡	⊠	K
I	4	1.5	2	1.0	4	3.5	·	·	34	7.8	6	3.7	3	4.3	8	4.0	32	3.9	61	25.1	31	3	12	27	·	11	4	1	16	17	10	2	2	30	·
II	12	1.2	4	1.2	2	2.5	·	·	1	6.0	22	4.9	5	2.2	22	2.5	16	2.4	60	8.3	9	12	25	28	·	3	2	1	15	21	16	·	·	28	·
III	7	2.3	8	1.1	3	1.3	1	1.0	24	6.0	8	1.6	·	·	7	2.9	35	2.2	68	11.9	17	4	5	20	·	5	3	4	13	16	13	1	5	18	·
IV	2	1.0	10	1.6	18	5.8	3	1.7	9	2.3	10	1.8	4	2.5	6	3.3	28	2.2	65	24.6	22	·	·	8	·	3	2	1	13	14	8	2	1	·	1
V	1	1.0	5	1.8	6	3.3	2	2.5	5	4.6	13	3.7	8	1.6	12	2.8	41	1.6	103	57.8	18	·	·	2	2	4	1	2	12	18	11	1	1	·	1
VI	4	1.0	2	1.0	5	2.4	3	4.3	7	2.6	9	2.6	9	2.7	12	2.1	39	1.3	153	36.8	10	·	·	·	6	1	·	1	9	14	10	8	2	·	5
VII	5	1.0	3	1.3	4	1.0	1	2.0	12	2.6	17	1.6	9	1.4	2	1.5	40	1.0	191	25.3	1	·	·	·	7	1	·	1	6	20	18	7	2	·	7
VIII	·	·	1	1.0	1	1.0	1	2.0	6	2.0	25	1.9	14	1.2	6	3.0	39	1.1	147	39.2	26	·	·	·	5	·	·	·	9	16	11	5	7	·	3
IX	1	1.0	·	·	·	·	4	1.8	16	2.9	14	2.4	2	2.0	7	1.7	46	1.2	61	28.4	11	·	·	·	2	·	·	3	1	5	4	2	7	·	·
X	4	1.0	1	2.0	2	1.0	1	1.0	4	3.5	24	2.0	4	1.2	10	1.6	43	1.0	7	2.4	11	·	·	7	·	·	·	1	10	8	3	·	8	·	·
XI	3	1.0	11	1.5	1	1.0	1	1.0	9	14.2	23	3.5	4	2.8	5	2.2	33	2.8	103	29.9	11	4	9	17	·	6	3	·	16	14	14	3	1	10	·
XII	2	1.0	3	1.0	1	1.0	·	·	14	5.6	48	4.9	2	1.0	8	1.4	15	3.6	35	5.4	18	2	7	22	·	7	4	·	19	18	13	·	1	5	·
Rok	45	1.1	50	1.2	47	2.0	17	1.4	141	5.0	219	2.9	64	1.9	105	2.4	407	2.0	1054	57.8	18.V	25	58	131	22	41	19	15	139	181	131	31	37	91	17

Przemyśl

$H_s = 237\ m$ $H_b = 238{,}9\ m$ $h_w = 18{,}2\ m$

I	7.5	4.3	3.5	2.9	14.5	2.7	11	2.5	4	2.6	13	4.5	22	4.8	9.5	4.7	8	3.5	52	21.6	31	4	7	26	·	5	·	5	18	17	8	1	7	31	·
II	9.5	4.9	6.5	5.6	4	2.9	0.5	6.0	·	·	7	6.6	33	4.4	22.5	4.9	1	4.8	42	6.7	18	13	24	28	·	8	·	1	15	21	13	·	·	28	·
III	7	3.4	7.5	3.4	16	2.8	4.5	3.7	3	2.7	10.5	6.1	24	3.2	8.5	3.8	12	3.1	44	7.7	26	4	4	20	·	6	·	6	11	16	10	·	4	19	·
IV	6.5	4.5	3	4.2	20	5.0	26.5	5.9	1	2.5	9	3.6	15	4.1	4	5.8	5	4.6	58	17.4	21	·	·	8	·	6	·	1	14	14	8	2	2	2	3
V	11.5	4.3	6	2.5	12	3.6	9.5	4.0	3	1.5	11	3.3	16.5	4.1	13.5	4.1	10	3.3	65	14.6	18	·	·	3	2	3	·	2	11	21	14	1	7	·	4
VI	7	3.7	3.5	3.0	8.5	3.2	11	3.0	8	2.9	22	2.4	21.5	3.7	3.5	3.4	5	2.9	120	29.2	10	·	·	·	6	3	·	4	6	13	12	6	2	·	8
VII	4.5	4.0	4	2.5	7	3.7	8	3.8	7	2.6	14.5	3.6	26	2.6	12	2.7	10	2.7	210	37.4	17	·	·	·	7	3	·	5	5	19	16	8	3	·	9
VIII	5	2.9	7.5	3.7	5.5	2.0	3	3.8	4	2.5	8	3.4	34.5	2.5	17.5	3.7	8	2.7	160	40.6	26	·	·	·	7	·	·	8	11	16	13	5	2	·	7
IX	8	3.2	1.5	1.7	7.5	1.5	7	2.4	14	4.2	13.5	3.3	17	2.5	10.5	3.0	11	2.6	47	28.0	11	·	·	·	6	2	·	9	6	8	4	2	6	·	·
X	7	4.4	5	3.0	5	1.6	3	2.7	3.5	2.0	8	3.5	39	3.3	13.5	4.1	9	3.0	4	1.8	11	·	·	5	·	·	·	4	10	7	1	·	8	·	·
XI	4	3.5	5	3.9	10	4.2	7	3.1	5	3.4	10	5.0	27.5	3.6	11.5	2.7	10	3.3	73	26.6	11	2	11	19	·	7	·	·	18	15	11	2	5	17	·
XII	5	4.2	4	2.2	6	1.8	5.5	2.2	8.5	2.8	16.5	5.5	34.5	4.1	10	4.0	3	3.8	41	7.1	8	2	5	19	·	6	1	1	17	18	11	·	·	10	·
Rok	82.5	3.9	57	3.2	116	2.9	96.5	3.5	61	2.5	143	4.2	310.5	3.6	136.5	3.9	92	3.4	916	40.6	26.VIII	25	51	128	28	49	1	46	142	185	121	27	46	107	31

Uwaga. Kierunki i prędkości wiatru – wg anemometru M-47.

Międzybrodzie Bialskie

$H_s = 320\ m$ $h_w = 10\ m$

I	9.5	4.4	2	2.5	0.5	9.0	26.5	5.8	23.5	8.0	0.5	3.0	2.5	5.6	9	5.6	19	4.9	69	13.2	9	2	4	26	·	5	–	2	21	15	12	2	·	26	·
II	21	4.8	3.5	4.8	·	·	7.5	5.9	8	9.2	3.5	3.9	5	3.0	16.5	6.0	19	4.3	34	5.0	17	11	22	28	·	5	–	·	17	21	13	·	·	28	·
III	17	3.5	2	3.5	1	3.0	10	4.8	22	6.3	·	·	6	5.3	5	4.2	30	3.3	35	8.8	21	3	6	18	·	5	–	6	12	16	10	·	2	15	·
IV	19	4.6	8	2.6	1	5.0	10	3.4	7	6.6	·	·	4	4.0	9	4.3	32	2.8	101	23.9	23	·	·	5	·	4	–	4	15	19	13	2	1	·	3
V	16.5	3.6	2.5	2.6	·	·	13	4.4	7	7.1	3	4.3	7	3.9	10	4.9	34	2.8	176	33.2	19	·	·	2	1	3	–	2	16	20	17	7	·	·	7
VI	15.5	4.4	10.5	3.9	·	·	9	3.6	12	5.8	1	5.0	7	4.1	7	5.4	28	3.1	211	65.9	11	·	·	·	5	4	–	3	9	15	13	5	2	·	8
VII	9	3.9	1	3.0	1.5	1.7	25.5	4.1	13	7.3	1	3.0	6	3.7	5	4.4	31	3.1	95	41.1	18	·	·	·	5	1	–	1	12	20	14	1	·	·	8
VIII	16.5	3.9	4	2.0	1	1.0	8	3.8	15	6.1	·	·	3.5	5.0	7	4.4	38	2.6	125	26.7	1	·	·	·	6	3	–	6	9	12	10	5	1	·	5
IX	4	3.0	3	2.3	2.5	2.6	22	4.7	26.5	5.4	·	·	4	3.5	2	2.0	26	3.2	106	35.5	19	·	·	·	2	5	–	5	7	12	9	4	4	·	1
X	17	3.2	7	2.9	·	·	18	4.5	7	2.1	·	·	5	5.4	6	4.0	33	2.4	20	10.0	31	·	·	8	·	·	–	7	8	13	4	1	7	·	·
XI	20.5	3.6	3	2.3	·	·	8	4.6	22	7.7	2	5.5	2	3.0	6.5	3.9	26	3.7	41	8.8	11	3	10	21	·	7	–	2	19	20	8	·	1	12	1
XII	9	3.4	2	2.5	1	1.0	41	6.4	22	8.4	2	7.5	1	6.0	8	3.9	7	5.8	56	20.1	18	1	1	19	·	8	–	·	18	18	11	2	·	14	·
Rok	174.5	3.9	48.5	2.8	8.5	1.9	198.5	4.7	185	6.7	13	2.7	53	4.4	91	4.4	323	3.5	1069	65.9	11.VI	20	43	127	19	50	–	38	163	201	134	29	18	95	31

Ciężkowice

$H_s = 280\ m$ $h_w = 15{,}9\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	73	16.1	31	6	9	26	·	–	–	3	18	16	14	1	5	31	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	79	12.1	8	13	22	28	·	–	–	1	13	23	19	1	3	28	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	81	9.0	17	4	5	22	·	–	–	6	12	15	12	·	4	20	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41	10.9	22	·	·	6	·	–	–	2	14	13	9	1	3	·	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	130	35.6	29	·	·	3	2	–	–	1	15	22	19	2	2	·	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	171	49.7	10	·	·	·	6	–	–	5	8	14	14	7	1	·	–
VII	4	1.1	5	1.2	7.5	1.1	7.5	1.9	8	1.6	5	1.1	5.5	1.9	12.5	1.9	38	0.9	135	32.6	17	·	·	·	12	·	·	3	5	21	16	5	1	·	–
VIII	8	2.9	6	1.6	5	1.0	13	1.4	6.5	1.5	0.5	1.0	2	2.0	23	2.7	29	1.4	162	34.6	26	·	·	·	8	1	·	5	11	15	13	6	3	·	–
IX	1.5	1.3	2.5	1.2	6	1.5	23.5	2.0	8	1.4	0.5	1.0	7	2.0	6	1.7	35	1.1	49	21.6	11	·	·	·	5	·	·	7	6	9	6	1	3	·	–
X	6	1.2	5	1.3	6.5	1.3	6	1.2	7	1.1	7	1.6	8	1.4	13.5	2.3	34	1.0	13	7.0	4	·	·	9	·	·	·	7	10	5	4	·	9	·	–
XI	7	1.6	3.5	2.1	4	1.5	12.5	2.0	12	4.6	3.5	2.4	10	2.3	10.5	2.7	27	1.8	46	15.4	11	3	10	20	·	1	·	1	13	13	10	1	2	10	–
XII	1.5	1.0	·	·	4.5	1.0	16	1.5	27.5	3.0	7	1.4	6.5	2.2	7	1.7	23	1.6	57	15.7	18	2	3	21	·	1	·	1	19	18	16	1	1	14	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1007	49.7	10.VI	28	49	134	33	–	–	42	144	184	151	26	37	103	–

Rożnów

$\varphi = 49°46'$ $\lambda = 20°41'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{0,m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	2.5	−3.8	8.1	30	−13.3	12	−1.7	1.0	−0.9	−0.6	4.5	5.0	4.9	4.8	82	76	84	81	1.0	1.7	1.0	1.2	8.2	7.8	7.9	8.0
II	—	—	—	—	−2.1	−10.0	6.1	14	−23.7	7	−7.3	−3.4	−6.8	−6.1	3.0	3.5	3.2	3.2	79	72	82	78	0.8	1.4	0.7	1.0	8.4	7.9	8.9	8.4
III	—	—	—	—	6.8	−2.4	15.9	30	−13.6	11	−0.4	5.2	1.5	2.0	5.1	6.1	5.9	5.7	83	70	83	79	1.1	3.3	1.2	1.9	7.2	6.7	6.4	6.8
IV	—	—	—	—	11.4	3.2	16.9	29	−1.2	1	4.9	9.5	6.2	6.7	7.3	7.4	7.7	7.5	84	63	80	76	1.4	4.8	1.9	2.7	8.4	8.0	7.1	7.8
V	—	—	—	—	16.0	6.5	27.2	19	−2.1	4	8.7	13.9	10.3	10.8	9.6	9.4	10.4	9.8	84	59	81	75	2.2	7.1	2.5	3.9	7.4	7.5	7.9	7.6
VI	—	—	—	—	21.7	11.7	31.7	26	6.4	3	14.8	20.0	15.4	16.4	13.2	13.4	14.2	13.6	78	58	81	72	3.9	10.8	3.7	6.1	5.0	5.6	6.2	5.6
VII	—	—	—	—	21.6	12.6	28.0	15	7.7	4	15.3	19.7	16.0	16.8	14.2	14.7	14.5	14.5	81	65	79	75	3.4	9.1	4.0	5.5	5.9	7.3	6.8	6.7
VIII	—	—	—	—	20.4	11.5	29.8	8	7.9	2	13.2	18.7	14.8	15.4	12.7	13.1	13.7	13.2	84	63	82	76	2.8	9.5	3.5	5.3	6.8	6.7	6.8	6.8
IX	—	—	—	—	20.2	10.6	26.4	3	4.4	22	13.1	18.9	14.3	15.2	12.0	13.2	13.2	12.8	81	61	81	74	3.5	9.2	3.5	5.4	5.5	5.1	4.7	5.1
X	—	—	—	—	12.5	4.1	22.3	1	−4.3	22	5.1	11.6	7.5	7.9	8.3	9.2	9.5	9.0	91	66	88	82	0.8	5.0	1.3	2.4	6.8	5.8	5.8	6.1
XI	—	—	—	—	3.9	−2.2	14.2	1	−11.9	25	−0.6	2.4	0.7	0.8	5.2	5.6	5.9	5.6	84	74	86	81	1.0	2.2	1.0	1.4	8.1	6.7	8.0	7.6
XII	—	—	—	—	3.8	−1.5	9.2	20	−8.7	15	0.1	2.3	0.9	1.0	5.1	5.4	5.4	5.3	80	74	82	79	1.3	2.0	1.3	1.5	7.6	7.8	7.1	7.5
Rok	—	—	—	—	11.6	3.4	31.7	26.VI	−23.7	7.II	5.4	10.0	6.7	7.2	8.4	8.8	9.0	8.7	83	67	82	77	1.9	5.5	2.1	3.2	7.1	6.9	7.0	7.0

Cieszyn-Bobrek

$\varphi = 49°45'$ $\lambda = 18°39'$

I	—	—	—	—	2.6	−3.5	8.1	29	−14.4	7	−0.2	1.6	−0.6	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.7	7.7	8.3
II	—	—	—	—	−1.8	−10.4	4.0	14	−25.5	10	−7.2	−2.9	−5.9	−5.5	3.3	3.8	3.4	3.5	85	76	84	82	0.6	1.2	0.7	0.8	8.8	7.2	7.8	7.9
III	—	—	—	—	7.3	−0.9	17.1	30	−14.5	11	0.5	6.0	2.3	2.8	5.5	5.9	6.0	5.8	83	63	79	75	1.2	4.1	1.6	2.3	6.9	6.9	6.2	6.7
IV	—	—	—	—	11.0	2.5	17.4	4	−3.9	2	4.4	9.6	5.7	6.4	7.5	7.6	7.8	7.6	88	66	85	80	1.0	4.6	1.4	2.3	8.0	7.6	6.8	7.5
V	—	—	—	—	15.3	6.1	25.7	19	−3.2	3	9.2	13.9	10.0	10.8	10.0	10.3	10.6	10.3	84	66	85	78	2.1	6.2	1.9	3.4	7.7	7.8	7.9	7.8
VI	—	—	—	—	21.6	10.5	32.4	26	4.3	3	14.9	19.4	14.8	16.0	13.9	14.1	14.5	14.2	82	65	85	77	3.4	9.7	2.7	5.3	5.0	6.8	6.5	6.1
VII	—	—	—	—	21.9	12.5	30.9	14	5.7	4	16.0	20.1	15.5	16.8	15.0	15.4	15.1	15.2	82	66	85	78	3.4	8.8	2.7	5.0	7.0	8.2	6.9	7.4
VIII	—	—	—	—	21.1	10.6	31.0	8	5.0	14	13.8	19.8	14.1	15.4	13.5	13.7	14.0	13.7	86	60	87	78	2.8	10.3	2.6	5.2	5.6	6.4	5.7	5.9
IX	—	—	—	—	21.2	10.3	27.6	3	3.6	22	13.1	19.5	13.5	14.9	12.8	13.5	12.9	13.1	85	61	84	77	2.7	9.7	3.0	5.1	5.2	5.7	5.2	5.4
X	—	—	—	—	13.6	2.6	25.2	2	−5.7	23	4.2	12.8	6.0	7.2	8.1	10.1	8.9	9.0	93	67	91	84	0.6	5.4	1.0	2.3	4.8	4.9	4.3	4.7
XI	—	—	—	—	4.6	−2.5	15.4	2	−14.6	18	−0.1	2.8	0.1	0.7	5.5	5.9	5.5	5.6	87	77	86	83	0.9	2.0	1.1	1.3	8.5	7.4	7.9	7.9
XII	—	—	—	—	4.2	−1.1	12.4	20	−10.8	15	1.3	2.6	1.4	1.7	5.7	5.7	5.6	5.7	83	77	82	81	1.3	1.8	1.3	1.5	8.1	8.5	7.5	8.0
Rok	—	—	—	—	11.9	3.1	32.4	26.VI	−25.5	10.II	5.8	10.4	6.4	7.2	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.2	6.7	7.0

Maków Podhalański

$\varphi = 49°44'$ $\lambda = 19°40'$

I	—	—	—	—	3.2	−4.9	9.6	30	−16.9	8	−2.3	2.6	−1.3	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.4	6.3	6.7
II	—	—	—	—	−1.9	−11.4	5.0	12	(−27.9)	7	−8.3	−2.3	−7.1	−6.2	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.8	7.6	7.3
III	—	—	—	—	7.0	−3.6	15.7	30	−17.4	1	−1.6	6.1	0.8	1.5	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.0	6.0	5.9
IV	—	—	—	—	10.9	1.8	17.4	3	−3.0	2	3.8	10.3	6.0	6.5	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.5	5.8	6.6
V	—	—	—	—	15.3	5.7	26.3	19	−2.8	3	8.7	14.3	9.6	10.6	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.5	6.8	6.3
VI	—	—	—	—	21.6	9.7	32.5	26	2.6	3	14.2	20.7	14.2	15.8	—	—	—	—	—	—	—	—	—	—	—	—	4.4	4.8	6.3	5.2
VII	—	—	—	—	21.4	10.8	29.6	14	4.6	10	14.5	20.1	14.5	15.9	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.5	5.9	6.4
VIII	—	—	—	—	20.7	9.6	32.7	7	4.1	31	11.9	19.9	13.5	14.7	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.0	6.5	5.7
IX	—	—	—	—	20.9	8.5	28.2	2	3.3	22	11.0	19.9	12.6	14.0	—	—	—	—	—	—	—	—	—	—	—	—	4.5	3.7	3.8	4.0
X	—	—	—	—	14.2	0.7	24.7	2	−6.4	22	2.7	13.7	4.8	6.5	—	—	—	—	—	—	—	—	—	—	—	—	4.1	2.8	4.2	3.7
XI	—	—	—	—	4.9	−4.0	13.7	1	−15.9	18	−1.0	3.9	−0.6	0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.6	7.3	7.2
XII	—	—	—	—	4.2	−3.4	11.3	20	−11.9	15	−0.4	3.3	0.3	0.9	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.2	6.5	6.9
Rok	—	—	—	—	11.9	1.6	32.7	7.VIII	(−27.9)	7.II	4.4	11.0	5.6	6.6	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.6	6.1	6.0

Biecz

$\varphi = 49°44'$ $\lambda = 21°15'$

I	—	—	—	—	0.8	−5.4	5.7	30	−17.8	12	−2.6	−0.2	−2.2	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.1	6.9	7.9
II	—	—	—	—	−3.2	−11.6	3.3	12	−27.7	7	−8.0	−4.2	−7.9	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.6	6.9	8.0
III	—	—	—	—	5.8	−3.4	15.8	30	−19.4	1	−1.3	4.4	1.4	1.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.1	6.3	7.0
IV	—	—	—	—	11.2	2.3	16.5	19	−2.1	6	4.1	9.8	6.2	6.6	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.2	6.2	7.8
V	—	—	—	—	15.4	5.9	26.2	19	−3.1	4	8.7	13.9	9.9	10.6	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.8	6.5	7.7
VI	—	—	—	—	21.5	10.4	30.7	26	3.8	3	14.5	20.1	14.7	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.2	6.4	5.9
VII	—	—	—	—	21.8	11.0	28.8	17	4.9	10	15.4	20.3	14.6	16.2	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.6	5.4	6.3
VIII	—	—	—	—	20.3	10.1	29.4	8	5.3	31	13.1	19.0	13.9	15.0	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.8	5.2	5.8
IX	—	—	—	—	20.7	8.4	25.7	2	2.2	22	11.6	19.4	12.8	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.4	2.1	4.4
X	—	—	—	—	12.7	1.9	23.7	2	−6.4	22	3.8	11.7	6.4	7.1	—	—	—	—	—	—	—	—	—	—	—	—	6.6	5.0	3.6	5.1
XI	—	—	—	—	3.4	−2.9	14.6	2	−16.8	18	−1.1	1.9	−0.1	0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.7	7.4	7.0	7.7
XII	—	—	—	—	2.6	−2.3	7.4	10	−13.8	17	−0.5	1.8	0.0	0.3	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.5	6.5	7.3
Rok	—	—	—	—	11.1	2.0	30.7	26.VI	−27.7	7.II	4.8	9.8	5.9	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.1	5.8	6.7

Rożnów $H_s = 300$ m $h_w = 20$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V>15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7	1.4	3.5	2.3	1	1.0	27.5	1.8	23.5	2.5	9	6.8	9	2.8	7.5	4.1	5	2.6	75	16.6	31	3	4	27	·	1	·	·	20	20	13	1	4	31	·
II	6.5	2.7	7.5	4.2	2.5	1.0	13.5	1.9	6.5	5.3	6.5	3.2	13.5	8.4	22.5	4.0	5	4.0	55	8.6	18	13	21	28	·	4	2	·	18	22	16	·	5	28	·
III	8.5	2.5	6	1.0	·	·	36	1.2	11	6.1	5	1.4	·	·	10.5	3.1	16	1.9	50	6.8	26	3	4	18	·	2	·	5	13	18	11	·	9	18	·
IV	9.5	2.5	4.5	1.7	10	1.6	27.5	1.5	11	2.5	1.5	2.0	7	3.0	6	4.8	13	1.9	37	9.1	26	·	·	3	·	2	1	·	17	14	8	·	4	·	1
V	5	2.9	·	·	9	1.4	30	1.9	16.5	1.3	2	3.8	3.5	2.9	22	2.9	6	2.0	127	41.7	29	·	·	2	2	1	1	1	15	21	17	3	6	·	3
VI	7.5	2.6	4	2.0	5.5	1.0	35.5	1.3	14	2.4	3	3.7	6.5	3.3	10	3.2	4	2.0	155	50.0	10	·	·	·	7	·	·	3	7	16	15	6	1	·	4
VII	3	5.3	2	1.5	3	1.0	28	1.2	24	1.8	9	4.6	8.5	2.1	3.5	2.7	12	1.8	104	44.2	17	·	·	·	6	2	1	1	8	20	17	3	2	·	5
VIII	3	2.3	1	1.0	4	1.5	33	1.3	20	2.2	5	2.0	6	2.5	17	4.3	4	2.1	151	45.4	1	·	·	·	7	1	1	4	13	16	15	4	4	·	1
IX	2	4.0	2	1.5	1	1.0	25	2.0	33	3.5	5.5	5.5	7.5	2.6	3	2.0	11	2.6	59	19.7	11	·	·	·	2	4	·	5	6	8	6	2	2	·	·
X	9	2.3	6	1.8	10	1.1	19	1.7	18.5	1.6	4	3.6	3.5	1.6	11	2.7	12	1.7	12	7.9	4	·	·	5	·	·	·	3	8	10	2	·	10	·	·
XI	5	2.0	4	1.2	8	1.5	16	1.5	26	3.6	9	6.5	9.5	3.9	6.5	3.2	6	2.9	50	20.3	11	3	10	19	·	4	1	1	14	17	10	1	4	10	·
XII	4.5	3.4	2.5	5.0	5	1.8	18	1.9	32	2.4	12.5	4.9	3.5	1.4	7	3.6	8	2.6	47	8.6	3	·	3	21	·	2	·	1	15	16	12	·	2	13	·
Rok	70.5	2.8	43	1.9	59	1.2	309	1.6	235	2.9	72	4.0	78	2.9	126.5	3.4	102	2.3	922	50.0	10.VI	22	42	123	24	23	7	24	154	198	142	20	53	100	14

Cieszyn – Bobrek $H_s = 300$ m $h_w = 14$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	4.5	2.0	6.5	2.0	3	1.3	7	3.9	29.5	3.6	12	2.3	8.5	1.3	9	1.3	13	2.3	74	15.1	9	3	6	27	·	·	·	·	19	17	13	2	—	29	·
II	2.5	3.0	14	2.5	2	1.0	1	3.0	3.5	3.3	15	4.4	14	2.4	14	2.4	13	2.5	65	9.0	17	11	22	27	·	1	·	·	15	20	15	·	—	28	·
III	6.5	1.8	11	2.5	0.5	4.0	8	3.1	19.5	3.3	17	3.1	6	2.7	13.5	1.4	11	2.3	29	8.5	21	1	4	16	·	·	·	5	11	16	9	·	—	15	·
IV	10	1.7	21.5	3.0	4	2.2	1.5	3.7	9.5	3.1	10	2.4	10	2.0	12.5	1.6	11	2.1	67	8.7	22	·	·	8	·	·	·	3	17	18	15	·	—	1	1
V	13.5	1.7	16	2.5	·	·	2.5	3.0	10	2.3	10	4.1	12	2.7	16	2.1	13	2.2	138	20.4	11	·	·	3	1	1	·	1	15	21	17	5	—	1	6
VI	7	1.7	11	2.1	1	2.0	3.5	2.9	8	3.8	15.5	2.9	12.5	2.4	14.5	2.0	17	2.0	184	47.3	11	·	·	·	7	·	·	2	7	17	14	6	—	·	6
VII	1.5	1.7	8.5	2.6	1	2.0	3	2.3	15.5	2.6	26.5	3.5	13	3.1	4	2.1	20	2.3	140	42.6	16	·	·	·	7	·	·	·	13	24	16	4	—	·	4
VIII	12	2.3	4.5	2.1	·	·	6	3.9	14	5.0	6.5	2.2	10	2.0	14	2.1	26	2.1	88	20.0	25	·	·	·	8	1	·	2	8	13	8	4	—	·	·
IX	2.5	1.6	2	2.5	0.5	1.0	19	3.5	18.5	3.7	16	4.2	4	2.2	7.5	1.5	20	2.6	90	26.0	19	·	·	·	3	·	·	6	6	11	9	4	—	·	·
X	9.5	1.4	11.5	2.3	·	·	2.5	2.2	7	2.1	12.5	2.9	6.5	2.6	6.5	1.3	37	1.3	14	8.5	31	·	·	11	1	·	·	8	6	6	4	·	—	·	·
XI	11	1.3	19	2.5	·	·	3	5.8	15	5.2	20	3.0	8.5	3.1	4.5	1.4	9	2.8	29	9.2	21	3	8	21	·	3	1	1	19	14	9	·	—	10	1
XII	4.5	1.2	4.5	1.6	0.5	2.0	9.5	4.0	33	3.5	27.5	2.9	8	2.8	3.5	1.3	2	2.9	64	11.8	18	1	1	19	·	·	·	·	18	19	11	2	—	13	·
Rok	90	1.8	130	2.4	12.5	1.3	66.5	3.4	183	3.5	188.5	3.2	113	2.4	119.5	1.7	192	2.3	982	47.3	11.VI	19	41	132	27	6	1	28	154	196	140	27	—	97	18

Maków Podhalański $H_s = 350$ m $h_w = 18$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	·	·	·	·	5	2.7	3	2.5	3	3.2	5	3.8	7	3.4	3	4.3	67	0.9	73	12.4	3	2	4	26	·	·	·	3	13	15	13	2	6	31	—
II	1	10.0	1	3.0	3	2.7	3	4.3	1	5.0	2	5.5	23	4.0	4	6.5	46	2.0	94	14.3	8	13	22	27	·	2	·	3	15	18	18?	1	3	28	—
III	·	·	2	6.0	6	3.2	7	2.0	10	3.6	1	2.0	3	3.7	4	4.2	60	1.2	29	4.7	21	3	4	22	·	·	·	8	11	13	10	·	10	19	—
IV	·	·	1	3.0	12	2.6	·	·	3	1.7	5	3.2	5	4.2	3	2.3	61	0.9	56	12.2	22	·	·	8	·	·	·	5	14	14	13	1	12?	·	—
V	1	4.0	2	4.0	3	2.7	3.5	2.9	6.5	2.8	4	3.2	10	4.1	3	3.3	60	1.2	142	27.0	19	·	·	2	1	1	1	2	10	22	20	5	7	·	—
VI	2	2.5	·	·	4	2.5	5	1.6	5.5	2.3	3.5	2.1	6	4.0	1	4.0	63	0.8	248	63.9	10	·	·	·	8	·	·	6	8	13	13	8	1	·	—
VII	·	·	·	·	3	3.3	6	1.8	1	6.0	5	2.2	3	3.3	·	·	75	0.5	113	28.6	18	·	·	·	7	·	·	3	11	18	15	2	4	·	—
VIII	1.5	2.7	3	1.7	7	3.6	3	3.0	4	4.5	1	4.0	6.5	4.5	9	3.5	58	1.4	151	44.0	1	·	·	·	8	·	·	7	11	12	10	6	11	·	—
IX	2	3.2	2	2.0	1	6.0	8.5	3.4	9.5	4.1	4	3.5	3	3.0	4	2.9	56	1.3	70	17.8	6	·	·	·	3	·	·	10	6	9	8	4	11?	·	—
X	2.5	4.0	3	2.0	6	1.8	·	·	·	·	·	·	1	3.0	9.5	2.9	71	0.6	9	5.9	31	·	·	17	·	1	·	12	5	5	3	·	—	·	—
XI	2.5	2.4	3	2.0	1	1.0	·	·	3	6.0	3.5	3.3	9.5	3.1	5.5	2.5	62	1.0	45	12.3	11	5	8	22	·	1	·	3	17	15	10	1	—	12	—
XII	1	2.0	·	·	2	1.5	·	·	3	2.0	3	4.3	16	3.0	2	3.5	66	0.8	54	11.8	3	1	2	25	·	·	·	3	15	14	13	1	3	15	—
Rok	13.5	2.6	17	2.0	53	2.8	39	1.8	49.5	3.4	37	3.5	93	3.6	48	3.3	745	1.0	1084	63.9	10.VI	24	40	149	27	5	1	65	136	168	146	31	—	105	—

Biecz $H_s = 260$ m $h_w = 16,1$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	6.2	1	4.0	1	3.0	·	·	10	3.1	41	5.5	5	4.0	20	4.6	9	4.4	47	12.0	31	8	14	29	·	6	1	2	20	17	10	1	2	31	·
II	7	4.3	6	4.3	·	·	·	·	·	·	11	6.3	13	4.5	39	5.3	8	4.6	44	6.3	8	14	23	28	·	4	·	1	17	19	15	·	·	28	·
III	9	3.3	7	3.9	3	4.3	·	·	12	5.6	19	4.6	8	3.9	16	4.6	19	3.5	52	9.5	27	4	5	21	·	3	·	5	16	17	12	·	6	18	·
IV	4	4.5	9	3.2	23	4.6	7	3.9	4	4.5	8	2.9	12	3.3	17	3.6	6	3.6	47	14.2	22	·	·	6	·	2	·	·	16	17	10	2	2	·	2
V	12	5.1	9	3.2	6	4.3	1	1.0	5	3.8	10	5.0	11	3.6	30	3.4	9	3.5	168	54.8	29	·	·	2	1	3	·	1	17	20	17	4	2	·	1
VI	5	3.2	4	2.2	4	2.5	6	3.2	12	3.8	4	5.2	7	3.4	32	4.3	16	3.2	156	35.0	10	·	·	·	6	2	·	6	11	14	13	7	·	·	3
VII	6	3.2	4	2.5	4	2.2	3	1.7	12	2.9	14	2.5	10	3.1	23	3.4	17	2.4	136	33.3	17	·	·	·	7	·	·	3	9	18	16	6	·	·	6
VIII	10	4.5	·	·	3	1.7	6	1.8	11	5.9	11	3.5	16	3.3	22	4.3	14	3.4	170	38.6	26	·	·	·	4	2	·	6	11	13	11	5	1	·	2
IX	2	5.0	2	3.0	2	1.5	3	1.3	34	4.7	9	3.2	5	3.2	6	4.0	27	2.8	43	24.2	11	·	·	·	3	·	·	9	4	6	5	1	2	·	·
X	5	3.4	7	3.4	11	3.0	·	·	1	5.0	15	4.2	3	3.0	22	4.2	29	2.6	11	6.5	4	·	·	12	·	·	·	9	9	4	3	·	3	·	·
XI	8	4.4	2	3.0	5	4.6	4	2.8	12	6.0	22	5.0	8	3.8	19	3.8	10	4.0	28?	13.0	11	3	11	19	·	4	1	·	15	12	7	1	2	9	·
XII	2	2.0	3	2.7	2	3.0	2	3.0	12	7.8	47	5.1	9	3.3	12	4.6	4	4.8	33	11.7	18	2	5	24	·	3	1	2	16	16	11	1	1	6	·
Rok	76	4.1	64	3.0	64	2.9	32	1.6	125	4.4	211	4.4	107	3.5	258	4.2	168	3.6	935	54.8	29.V	31	58	141	21	29	3	44	161	173	130	28	21	92	14

Jasło

$\varphi = 49°44'$ $\lambda = 21°28'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.6	−4.9	4.4	30	−16.6	12	−2.4	−0.3	−1.9	−1.6	4.4	4.8	4.7	4.6	85	80	86	84	0.8	1.2	0.7	0.9	7.5	7.3	6.5	7.1
II	—	—	—	—	−3.0	−11.0	1.0	12	−26.4	7	−7.8	−4.3	−7.3	−6.7	3.1	3.5	3.1	3.2	85	77	84	82	0.5	1.0	0.6	0.7	8.7	7.4	6.4	7.5
III	—	—	—	—	6.3	−2.7	16.8	30	−15.5	1	−0.9	4.8	2.1	2.0	5.4	6.0	6.0	5.8	88	68	81	79	0.7	3.1	1.4	1.7	7.4	6.3	5.8	6.5
IV	—	—	—	—	11.9	2.5	16.4	19	−1.9	6	4.2	10.5	6.9	7.1	7.4	7.9	8.1	7.8	89	63	81	78	0.9	5.1	2.0	2.7	7.9	7.2	6.3	7.1
V	—	—	—	—	16.1	6.6	25.6	19	−2.7	4	8.7	14.4	10.9	11.2	10.2	10.4	11.2	10.6	88	62	83	78	1.5	6.8	2.1	3.5	6.7	7.4	6.4	6.8
VI	—	—	—	—	22.2	11.7	31.3	26	5.4	3	14.7	20.7	16.2	17.0	14.8	15.3	15.8	15.3	88	63	85	79	2.2	10.0	3.0	5.1	4.8	5.3	5.6	5.2
VII	—	—	—	—	22.6	12.1	29.1	16	6.1	10	15.1	20.8	16.4	17.2	15.5	15.7	16.1	15.8	89	65	86	80	1.9	9.6	2.9	4.8	5.0	6.5	4.8	5.4
VIII	—	—	—	—	20.7	10.9	29.4	8	5.9	31	13.1	19.2	14.8	15.5	13.8	13.9	14.6	14.1	91	64	86	80	1.6	9.3	2.7	4.5	6.3	5.2	5.1	5.5
IX	—	—	—	—	20.7	9.8	25.6	2	2.7	22	11.7	19.3	13.8	14.6	12.4	14.2	13.9	13.5	89	64	88	80	1.9	8.6	2.2	4.2	4.6	4.2	1.7	3.5
X	—	—	—	—	12.6	2.7	23.9	2	−6.0	22	4.3	11.5	7.2	7.6	8.3	9.8	9.3	9.1	94	70	89	84	0.5	4.3	1.2	2.0	5.5	4.8	3.5	4.6
XI	—	—	—	—	3.4	−2.5	15.3	2	−13.0	17, 18	−0.8	2.2	0.1	0.4	5.5	5.8	5.7	5.7	90	79	89	86	0.6	1.8	0.8	1.1	7.6	6.8	6.2	6.9
XII	—	—	—	—	2.2	−1.8	6.5	10	−9.7	17	−0.4	1.4	0.3	0.4	5.4	5.7	5.6	5.6	90	83	87	87	0.6	1.2	0.8	0.9	6.6	6.9	6.3	6.6
Rok	—	—	—	—	11.4	2.8	31.3	26.VI	−26.4	7. II	5.0	10.0	6.6	7.0	8.8	9.4	9.5	9.2	89	70	85	81	1.1	5.2	1.7	2.7	6.6	6.3	5.4	6.1

Tęgoborze

$\varphi = 49°43'$ $\lambda = 20°39'$

I	—	—	—	—	2.4	−4.3	8.5	28	−14.5	8	−1.7	1.0	−1.3	−0.8	4.4	4.6	4.6	4.5	80	70	81	77	1.1	2.1	1.1	1.4	7.9	7.2	7.0	7.4
II	—	—	—	—	−1.6	−10.5	4.8	14	−24.2	10	−7.1	−2.7	−6.6	−5.8	3.1	3.0	3.1	3.1	82	59	78	73	0.8	2.1	0.9	1.3	8.9	8.0	7.7	8.2
III	—	—	—	—	6.7	−2.3	17.3	30	−15.5	1	−0.5	5.1	1.5	1.9	5.2	5.2	5.7	5.4	84	60	80	75	1.0	4.0	1.4	2.1	7.1	6.6	6.3	6.7
IV	—	—	—	—	11.3	3.4	17.9	7	−1.1	2	5.3	9.8	6.7	7.1	7.5	7.0	7.7	7.4	83	59	78	73	1.5	5.5	2.1	3.0	8.2	7.9	6.6	7.6
V	—	—	—	—	15.9	7.1	25.5	19	−0.5	3	9.2	14.3	10.6	11.2	9.7	9.5	10.4	9.9	82	58	79	73	2.3	7.4	2.7	4.1	6.8	7.5	6.5	6.9
VI	—	—	—	—	21.9	11.6	31.3	26	5.8	3	15.0	20.5	15.6	16.9	13.4	11.9	14.4	13.2	78	51	81	70	3.8	12.9	3.7	6.8	4.7	5.9	6.6	5.7
VII	—	—	—	—	22.0	12.6	28.3	14, 16	7.0	10	15.5	20.0	15.9	16.8	14.7	13.9	14.9	14.5	83	61	82	75	3.1	10.2	3.5	5.6	4.8	7.1	4.5	5.5
VIII	—	—	—	—	20.4	11.4	29.1	8	7.0	31	13.5	19.1	14.6	15.4	13.0	12.0	13.8	12.9	84	56	83	74	2.8	11.0	3.3	5.7	6.1	6.3	5.3	5.9
IX	—	—	—	—	20.6	10.6	25.3	11	4.7	22	13.2	19.3	14.2	15.2	12.6	11.2	13.3	12.4	83	51	81	72	3.0	11.4	3.3	5.9	5.5	5.1	3.6	4.7
X	—	—	—	—	13.5	4.4	24.3	2	−3.0	22	5.6	12.5	7.8	8.4	8.2	7.6	8.8	8.2	86	52	81	73	1.3	7.3	2.1	3.6	6.6	5.3	4.3	5.4
XI	—	—	—	—	4.4	−1.8	15.4	2	−11.7	15	0.0	3.0	0.9	1.2	5.1	4.8	5.4	5.1	80	63	79	74	1.4	3.2	1.7	2.1	8.0	6.9	6.8	7.2
XII	—	—	—	—	4.2	−1.8	8.7	6	−10.8	15	0.3	2.6	1.0	1.2	5.0	5.0	5.1	5.0	78	66	77	74	1.4	2.6	1.6	1.9	7.3	7.3	6.5	7.0
Rok	—	—	—	—	11.8	3.4	31.3	26.VI	−24.2	10. II	5.7	10.4	6.7	7.4	8.5	8.0	8.9	8.5	82	59	80	74	2.0	6.6	2.3	3.6	6.8	6.8	6.0	6.5

Limanowa

$\varphi = 49°42'$ $\lambda = 20°25'$

I	—	—	—	—	1.8	−6.2	6.3	30	−19.1	8	−2.5	0.8	−2.3	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.1	7.7	8.1
II	—	—	—	—	−2.6	−12.9	3.9	13	−28.8	7	−8.5	−3.9	−8.1	−7.2	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.0	8.3	8.3
III	—	—	—	—	5.7	−5.2	15.1	30	−19.5	1	−1.6	4.6	−0.7	0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.2	6.5	7.0
IV	—	—	—	—	10.7	1.2	16.0	7	−3.5	6	4.6	9.1	5.1	6.0	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.4	7.0	8.0
V	—	—	—	—	14.7	4.6	26.6	19	−5.3	3, 4	8.9	13.3	8.6	9.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.4	8.1	8.1
VI	—	—	—	—	21.3	8.8	31.4	26	1.1	3	14.9	19.9	13.3	15.4	—	—	—	—	—	—	—	—	—	—	—	—	5.9	6.7	7.3	6.6
VII	—	—	—	—	21.5	9.5	28.5	14	3.8	10	15.3	19.3	13.3	15.3	—	—	—	—	—	—	—	—	—	—	—	—	7.1	8.0	5.3	6.8
VIII	—	—	—	—	19.8	8.5	31.0	7	3.5	31	12.2	18.2	11.6	13.4	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.7	6.5	7.1
IX	—	—	—	—	20.6	7.2	26.1	3	0.6	22	11.2	19.1	10.7	12.9	—	—	—	—	—	—	—	—	—	—	—	—	6.3	5.7	5.3	5.8
X	—	—	—	—	13.1	0.0	23.6	2	−7.5	22	2.6	12.2	3.9	5.6	—	—	—	—	—	—	—	—	—	—	—	—	6.0	5.2	4.7	5.3
XI	—	—	—	—	4.1	−4.2	14.1	1	−15.9	18	−1.7	2.5	−0.9	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	8.6	7.1	7.1	7.6
XII	—	—	—	—	3.7	−4.0	9.9	19, 20	−16.7	15	−1.1	2.1	0.0	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.8	6.8	7.5
Rok	—	—	—	—	11.2	0.6	31.4	26.VI	−28.8	7. II	4.5	9.8	4.5	5.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.4	6.7	7.2

Żywiec - Sporysz

$\varphi = 49°41'$ $\lambda = 19°13'$

I	—	—	—	—	2.8	−4.5	8.9	29	−17.3	8	−1.7	1.7	−1.2	−0.6	4.8	5.2	4.9	5.0	85	76	85	82	0.8	1.8	0.9	1.2	8.4	8.8	7.1	8.1
II	—	—	—	—	−2.3	−11.2	3.7	14	−24.9	10	−8.3	−3.4	−7.0	−6.4	3.1	3.7	3.3	3.4	85	76	85	82	0.5	1.1	0.5	0.7	8.4	6.7	7.5	7.5
III	—	—	—	—	6.9	−2.9	16.1	30	−16.9	1	−1.1	5.6	1.2	1.7	5.3	5.7	5.5	5.5	87	64	82	78	0.7	3.8	1.2	1.9	6.9	6.7	6.3	6.6
IV	—	—	—	—	11.1	2.1	16.7	6	−2.2	2	4.0	9.8	5.7	6.3	7.3	7.5	7.7	7.5	89	64	84	79	0.9	4.9	1.5	2.4	7.9	7.5	6.7	7.4
V	—	—	—	—	15.2	5.9	26.5	19	−2.9	3	8.6	13.6	9.6	10.4	9.5	9.6	10.4	9.8	84	62	86	77	2.1	6.7	1.8	3.5	7.2	8.4	7.1	7.6
VI	—	—	—	—	21.8	10.0	32.0	26	5.6	16	13.5	19.6	14.7	15.6	13.0	13.4	14.2	13.5	84	61	84	76	2.7	10.4	2.9	5.3	5.5	6.7	6.7	6.3
VII	—	—	—	—	21.3	11.6	30.4	14, 15	5.3	11	15.1	19.8	15.2	16.3	14.6	14.7	14.7	14.7	84	65	85	78	2.8	9.1	2.8	4.9	6.9	7.8	6.7	7.1
VIII	—	—	—	—	20.8	9.3	31.0	8	4.3	31	12.3	19.4	13.4	14.6	12.7	12.7	13.4	12.9	88	58	87	78	2.1	10.9	2.3	5.1	5.5	6.5	5.1	5.7
IX	—	—	—	—	21.1	8.1	28.0	3	2.1	22	11.0	19.3	12.8	14.0	12.0	12.3	12.3	12.2	90	57	85	77	1.6	10.9	2.9	5.1	5.6	5.8	4.1	5.2
X	—	—	—	—	14.2	1.4	26.3	2	−6.6	22	3.6	13.2	5.7	7.0	7.5	9.0	8.3	8.3	90	58	87	78	0.9	6.9	1.4	3.1	4.2	4.3	3.7	3.9
XI	—	—	—	—	4.4	−3.1	12.9	2	−15.4	18	−0.9	2.7	−0.3	0.3	5.2	5.6	5.4	5.4	86	74	86	82	0.9	2.3	1.0	1.4	8.0	7.2	6.9	7.4
XII	—	—	—	—	3.5	−2.2	8.5	19, 20	−11.4	6	0.5	2.3	0.4	0.9	5.3	5.6	5.3	5.4	82	76	82	80	1.2	1.8	1.2	1.4	8.4	8.5	7.5	8.1
Rok	—	—	—	—	11.7	2.0	32.0	26.VI	−24.9	10. II	4.7	10.3	5.8	6.6	8.4	8.8	8.6	8.7	86	66	85	79	1.4	5.9	1.7	3.0	6.9	7.1	6.2	6.7

Jasło — $H_s = 240$ m — $h_w = 15.8$ m — 1965

MIESIĄC	ROZKŁAD WIATRU p_D, V_{mD}																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	◕	Opad R			≡	⊠	K (K)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15			R≥0.1	R≥1.0	R≥10.0			
I	5.5	2.2	·	·	5	2.0	·	·	33.5	7.5	7.5	2.8	9	4.2	11.5	3.4	21	4.0	56	13.1	31	6	10	27	·	4	·	4	16	16	11	2	2	31	·
II	3	3.8	·	·	·	·	·	·	11	8.5	2.5	2.6	17	4.9	29.5	3.5	21	3.5	63	11.6	8	13	23	28	·	1	·	1	17	22	15	1	1	28	·
III	12.5	2.7	1.5	3.3	1	3.0	·	·	24.5	4.9	4.5	4.0	3.5	4.0	10.5	3.2	35	2.5	41	7.0	17	4	4	20	·	2	·	5	14	16	11	·	4	16	·
IV	11.5	2.1	12	4.5	7	3.6	·	·	4	4.0	5.5	3.1	7.5	4.0	13.5	3.0	29	2.3	61	11.1	22	·	·	5	·	·	·	·	15	18	14	1	3	·	1
V	5	3.0	2	4.0	4	3.0	1	1.0	5	6.0	5	3.2	12.5	2.4	29.5	2.9	29	2.1	114	34.7	29	·	·	2	2	·	·	2	12	22	15	2	3	·	1
VI	5	1.8	6.5	2.5	1	2.0	·	·	11	4.4	5	3.0	14	2.7	22.5	3.0	26	2.2	140	31.7	10	·	·	·	7	1	·	6	8	16	12	6	·	·	4
VII	2.5	1.0	1.5	3.3	1.5	2.7	1	2.0	8	4.7	9	3.3	23.5	1.8	18	1.5	28	1.6	109	23.1	2	·	·	·	9	·	·	3	5	20	15	4	1	·	4
VIII	4	2.2	·	·	·	·	6	2.0	13	4.5	2	3.5	11.5	2.3	24.5	3.3	32	2.1	176	37.8	1	·	·	·	7	·	·	8	10	15	12	6	4	·	3
IX	1	1.0	·	·	·	·	6	3.2	38	4.2	0.5	3.0	7	2.2	6.5	2.6	31	2.4	46	26.8	11	·	·	·	2	·	·	10	1	8	5	1	4	·	·
X	5.5	1.7	2.5	1.8	2.5	2.6	3	1.7	18.5	4.2	2.5	2.8	11	3.1	14.5	2.7	33	2.0	16	11.2	4	·	·	9	·	·	·	9	8	5	3	1	3	·	·
XI	13.5	2.3	5.5	3.7	2	4.5	·	·	25.5	6.1	1	5.0	9	4.0	6.5	3.2	27	3.1	54	22.6	11	3	9	18	·	2	·	1	11	18	11	1	1	9	·
XII	1.5	1.7	0.5	3.0	2	2.5	1	3.0	57.5	5.7	2.5	2.6	6	2.8	8	3.0	14	4.1	35	8.9	15	·	4	21	·	3	·	4	15	18	9	·	1	6	·
Rok	70.5	2.1	32	2.2	26	2.2	18	1.1	249.5	5.4	47.5	3.2	131.5	3.2	195	2.9	325	2.7	901	37.8	1.VIII	26	50	130	27	13	·	53	132	194	133	25	27	90	13

Tęgoborze — $H_s = 272$ m — $h_w = 17.6$ m

I	·	·	·	·	1	1.0	5	1.8	17	4.4	2	4.5	4	2.0	4	2.2	60	1.2	75	17.5	31	3	6	27	·	·	·	2	17	15	14	2	·	31	·
II	3	1.3	·	·	·	·	2	3.0	6	5.2	5	3.2	10	2.1	5	4.4	53	1.2	73	10.0	18	14	19	28	·	1	·	·	17	19	17	1	·	28	·
III	1	1.0	·	·	1	2.0	3	2.3	13	5.5	·	·	3	2.7	1	4.0	71	1.0	56	8.0	24	2	3	19	·	2	1	4	14	14	12	·	4	·	·
IV	0.5	2.0	·	·	19	2.7	1	5.0	10	2.4	·	·	8	2.6	4.5	1.3	47	1.2	33	9.3	26	·	·	2	·	·	·	1	16	10	7	·	2	·	3
V	·	·	2	2.0	10	2.2	1	4.0	13	2.0	1	2.0	9	1.9	1	3.0	56	0.8	118	41.9	29	·	·	1	2	·	·	1	11	19	16	2	·	·	6
VI	1	1.0	1	2.0	·	·	·	·	20	2.0	1	2.0	4	1.8	1	1.0	62	0.6	158	47.1	10	·	·	·	6	·	·	4	8	16	14	6	·	·	4
VII	·	·	·	·	2	1.5	·	·	15	2.1	·	·	2	3.0	·	·	74	0.4	92	34.2	17	·	·	·	8	1	·	3	3	16	12	3	·	·	5
VIII	1	1.0	·	·	3	1.3	·	·	15	2.5	·	·	4	1.2	2	2.5	68	0.6	165	54.3	1	·	·	·	5	·	·	6	11	16	13	4	1	·	2
IX	·	·	·	·	3	1.7	2	4.0	34	3.0	·	·	1	1.0	·	·	50	1.3	65	21.5	11	·	·	·	2	·	·	7	5	8	6	2	2	·	·
X	·	·	·	·	3	1.3	·	·	19	1.5	1	1.0	2	1.0	1	1.0	67	0.4	17	10.0	4	·	·	4	·	·	·	6	9	6	3	1	4	·	·
XI	·	·	·	·	4	1.8	·	·	15	4.9	2	3.0	4	2.5	·	·	65	1.1	53	24.7	11	2	8	18	·	2	·	2	15	14	9	1	1	9	·
XII	·	·	·	·	·	·	1	4.0	35	2.6	2	4.0	·	·	·	·	55	1.1	35	6.7	18	1	2	22	·	2	·	2	15	13	12	·	·	8	·
Rok	6.5	0.5	3	0.3	46	1.3	15	2.0	212	3.2	14	1.6	51	1.8	19.5	1.6	728	0.9	940	54.3	1.VIII	22	38	121	23	8	1	38	141	166	135	22	14	76	20

Limanowa — $H_s = 440$ m — $h_w = 16$ m

I	2.5	2.0	2.5	2.4	13	3.8	26.5	3.5	4	2.5	8	2.5	9	4.2	22.5	3.4	5	3.2	63	16.1	31	9	9	29	·	·	·	1	20	16	12	1	2	31	·
II	1.5	3.7	·	·	1.5	3.0	6	2.4	4	1.8	4	5.9	21	5.3	39	4.4	7	4.0	59	7.4	18	16	23	28	·	3	1	·	19	21	18	·	·	28	·
III	4.5	2.8	1	2.0	4	3.2	21.5	3.0	8	2.7	12.5	2.7	14	3.4	19.5	3.1	8	2.7	38	6.1	27	6	5	23	·	1	·	5	13	16	10	·	3	23	·
IV	9.5	2.8	4.5	3.0	8.5	3.4	18	2.8	3	4.2	2.5	3.6	10.5	3.5	20.5	3.4	13	2.8	31	6.5	22	·	·	11	·	·	·	1	19	12	8	·	2	·	3
V	8.5	2.1	3	2.8	8	2.6	16.5	2.8	2	3.5	3.5	2.4	15.5	3.8	29	3.1	7	2.8	185	56.5	29	·	·	6	1	·	·	1	20	21	18	4	·	·	3
VI	7	2.3	4.5	2.2	4	2.8	14.5	2.7	5	4.0	4.5	3.1	15.5	3.7	28	3.1	7	2.8	214	58.6	10	·	·	·	6	·	·	1	10	15	15	8	·	·	7
VII	3.5	2.3	4	2.4	5	2.8	12	2.4	4	3.2	6	2.4	15.5	2.9	23	2.3	20	2.0	80	19.4	17	·	·	·	9	·	·	3	9	21	16	2	1	·	5
VIII	2.5	3.0	1	2.0	5	3.0	14.5	2.8	6.5	3.3	2.5	1.8	13	2.9	28	2.5	21	2.1	182	46.4	1	·	·	·	6	·	·	1	15	14	13	7	·	·	1
IX	5.5	1.5	1.5	2.3	7	2.8	24	3.3	14.5	2.7	7	2.0	6	2.9	15.5	2.6	9	2.5	71	23.5	11	·	·	·	3	·	·	5	6	9	8	3	·	·	·
X	8.5	2.1	1.5	1.7	4.5	2.4	12	2.1	4	1.5	8.5	1.9	10.5	3.0	23.5	2.3	20	1.8	15	4.0	9	·	·	18	·	·	·	7	7	7	5	·	6	·	·
XI	8	2.2	5	1.9	12	3.2	15.5	3.6	5	2.5	5	3.0	8	4.9	21.5	3.7	10	3.0	47	15.9	11	5	9	23	·	1	·	1	19	15	11	1	3	17	·
XII	1.5	2.0	2	2.0	11	3.5	23.5	3.7	8	4.5	4	4.1	18.5	4.1	20.5	3.0	4	3.4	46	9.9	18	1	3	25	·	1	·	·	15	17	10	·	·	24	·
Rok	63	2.4	30.5	2.1	83.5	3.0	204.5	2.9	67	3.0	68	3.0	157	3.7	290.5	3.1	131	2.8	1031	58.6	10.VI	37	49	163	25	6	1	26	172	184	144	26	17	123	19

Żywiec-Sporysz — $H_s = 360$ m — $h_w = 20.6$ m

I	0.5	1.0	1	1.0	3	1.2	6	1.1	7	2.3	18.5	2.9	4.5	3.3	5.5	1.8	47	1.2	62	11.3	3	2	4	25	·	·	·	2	19	16	12	2	2	31	·
II	4	1.9	3	2.5	2	1.0	·	·	3.5	3.6	12	2.8	7	1.6	13.5	2.0	39	1.2	80	12.4	8	11	22	28	·	1	1	2	15	18	16	1	·	28	·
III	1	1.0	3.5	1.1	6.5	1.2	5.5	1.4	7.5	1.7	15	2.2	6	1.7	9	1.2	39	0.9	33	7.4	21	3	5	20	·	·	·	5	17	18	9	·	3	17	·
IV	3	1.7	6.5	1.7	6.5	1.5	0.5	1.0	3	1.5	6	1.2	7	1.4	10.5	1.6	47	0.7	59	12.4	22	·	·	8	·	·	·	3	16	18	11	2	9	·	2
V	1.5	2.3	4	1.2	3	1.3	0.5	2.0	4.5	1.9	15	2.8	6.5	1.5	11	2.0	47	1.0	146	44.8	19	·	·	3	1	2	·	2	16	22	15	5	7	·	3
VI	3.5	1.9	·	·	·	·	·	·	3	2.0	5.5	1.9	5.5	1.8	16.5	2.0	56	0.7	201	48.2	11	·	·	·	8	1	·	5	10	15	14	7	2	·	7
VII	3	1.2	2	1.0	2.5	1.0	2	1.0	8	1.7	18	2.0	3	1.8	4.5	1.7	50	0.8	119	53.9	18	·	·	·	8	·	·	1	13	20	13	1	5	·	4
VIII	3	1.0	1.5	1.0	1.5	1.0	3.5	1.4	3.5	2.4	6	1.5	9.5	1.6	13.5	1.5	51	0.7	114	23.8	1	·	·	·	8	·	·	5	8	14	12	5	5	·	3
IX	·	·	0.5	1.0	3.5	1.3	10	1.8	7	2.1	13.5	2.0	2.5	1.8	2	1.2	51	0.8	122	46.4	19	·	·	·	2	·	·	7	4	10	8	5	5	·	1
X	1	1.0	5	1.3	11.5	1.1	5.5	1.0	3.5	1.6	11	2.6	5.5	1.8	5	1.6	45	0.8	12	7.4	31	·	·	12	2	·	·	13	5	5	3	·	11	·	·
XI	1	1.0	2.5	1.6	4.5	1.3	1.5	1.0	7.5	3.4	16.5	4.0	5	3.0	4.5	2.2	47	1.4	48	9.5	11	4	10	22	·	3	1	2	19	19	10	·	3	15	·
XII	3	1.3	0.5	2.0	·	·	2.5	1.2	13	2.6	32.5	2.6	8	2.0	3.5	2.6	30	1.6	57	12.1	13	1	1	22	·	2	1	·	20	19	12	1	1	15	·
Rok	24.5	1.3	30	1.3	44.5	1.0	37.5	1.1	71	2.2	169.5	2.4	70	1.9	99	1.8	549	1.0	1053	53.9	18.VII	21	42	140	29	9	3	47	162	194	135	29	53	105	20

Krosno — φ = 49°41' — λ = 21°45' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień	I	II	III	Dzień
I	—	—	—	—	0.4	−5.3	4.5	31	−15.7	12	−2.1	−0.6	−1.7	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.7	7.4	8.5
II	—	—	—	—	−3.7	−11.7	1.4	1	−27.2	7	−8.0	−4.7	−7.6	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.1	6.8	8.0
III	—	—	—	—	5.6	−2.5	15.7	30	−18.2	1	−0.2	4.3	2.1	2.1	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.6	6.2	6.8
IV	—	—	—	—	11.0	2.3	14.8	19	−3.3	6	4.6	9.8	6.7	7.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.9	7.1	7.8
V	—	—	—	—	15.2	5.9	25.2	19	−3.7	4	8.7	13.8	10.7	11.0	—	—	—	—	—	—	—	—	—	—	—	—	7.5	8.8	7.5	7.9
VI	—	—	—	—	21.2	10.7	30.1	26	3.1	4	14.8	19.8	15.3	16.3	—	—	—	—	—	—	—	—	—	—	—	—	5.5	7.1	7.1	6.6
VII	—	—	—	—	21.5	11.5	29.0	16	5.4	12	15.6	20.3	16.0	17.0	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.5	6.8	6.7
VIII	—	—	—	—	19.9	10.4	28.0	8	5.3	31	13.4	19.3	14.5	15.4	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.6	5.9	6.4
IX	—	—	—	—	19.8	9.5	26.5	2	1.5	22	12.6	19.2	14.4	15.2	—	—	—	—	—	—	—	—	—	—	—	—	5.3	5.2	4.1	4.9
X	—	—	—	—	12.1	3.1	24.6	2	−6.8	22	5.2	11.4	7.2	7.8	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.7	5.2	6.4
XI	—	—	—	—	2.7	—	15.1	2	—	—	−1.0	2.5	−1.0	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	9.8	9.1	8.2	9.0
XII	—	—	—	—	1.4	—	7.0	10	—	—	−1.2	1.2	−1.3	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	9.4	7.5	7.7	8.2
Rok	—	—	—	—	10.6	—	30.1	26.VI	−27.2	7. II	5.2	9.7	6.3	6.9	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.5	6.7	7.3

Bircza — φ = 49°41' — λ = 22°29'

I	—	—	—	—	1.3	−4.6	6.9	30	−20.0	12	−2.0	0.2	−1.5	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.6	7.5	7.7
II	—	—	—	—	−3.9	−10.8	1.5	12	−24.8	7	−7.9	−5.0	−7.5	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.1	7.3	7.9
III	—	—	—	—	5.9	−3.6	15.3	30	−18.3	1	−1.3	4.8	0.9	1.3	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.6	5.6	6.4
IV	—	—	—	—	10.3	1.4	15.5	26	−2.2	11	3.1	9.0	5.2	5.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.1	5.8	7.0
V	—	—	—	—	15.0	5.0	26.2	19	−4.8	4	8.4	13.3	9.8	10.3	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.3	6.6	6.8
VI	—	—	—	—	20.5	10.0	29.1	26	3.7	8	14.3	19.0	14.7	15.7	—	—	—	—	—	—	—	—	—	—	—	—	5.1	6.4	6.1	5.9
VII	—	—	—	—	21.0	11.2	27.5	16	4.5	12	14.9	19.5	15.4	16.3	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.8	6.2	6.1
VIII	—	—	—	—	19.5	9.5	28.7	8	3.9	17	12.3	18.2	13.2	14.2	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.3	5.1	5.8
IX	—	—	—	—	20.4	7.9	25.6	3	1.0	17	11.0	19.2	12.7	13.9	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.6	4.0	5.0
X	—	—	—	—	11.9	2.2	23.1	1	−6.6	22	4.4	10.9	6.0	6.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.4	4.3	5.4
XI	—	—	—	—	3.2	−3.6	14.4	2	−20.9	18	−1.1	1.4	−0.1	0.1	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.8	8.1	8.1
XII	—	—	—	—	3.2	−2.1	9.3	21	−10.7	16	0.2	1.9	0.5	0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.5	7.4	7.6
Rok	—	—	—	—	10.7	1.9	29.1	26.VI	−24.8	7. II	4.7	9.4	5.8	6.4	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.9	6.2	6.7

Mszana Dolna — φ = 49°40' — λ = 20°05'

I	—	—	—	—	2.6	−5.8	8.7	30	−17.2	8	−2.8	1.2	−2.0	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.6	7.1	7.7
II	—	—	—	—	−2.7	−12.4	2.4	14	−31.0	7	−8.7	−4.3	−7.4	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.5	7.7	8.0
III	—	—	—	—	6.3	−4.2	15.3	30	−18.8	11	−2.3	4.7	0.2	0.7	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.8	6.6	6.9
IV	—	—	—	—	11.2	1.8	17.3	7	−2.4	2	3.7	9.7	5.3	6.0	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.8	6.9	7.5
V	—	—	—	—	15.3	5.4	26.9	19	−4.2	3	8.6	13.8	9.1	10.2	—	—	—	—	—	—	—	—	—	—	—	—	7.0	8.3	7.3	7.5
VI	—	—	—	—	21.4	9.3	31.2	26	2.4	3	13.8	19.9	13.4	15.1	—	—	—	—	—	—	—	—	—	—	—	—	5.1	6.8	6.2	6.0
VII	—	—	—	—	21.2	10.3	28.6	14	5.3	6. 11	14.6	19.4	13.7	15.4	—	—	—	—	—	—	—	—	—	—	—	—	6.3	8.2	5.1	6.5
VIII	—	—	—	—	20.1	9.0	30.3	7	3.2	31	11.7	18.5	12.4	13.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.4	5.9	6.6
IX	—	—	—	—	20.8	7.6	28.4	3	1.6	22	10.7	19.0	11.8	13.3	—	—	—	—	—	—	—	—	—	—	—	—	5.0	5.8	4.4	5.1
X	—	—	—	—	14.2	0.7	25.9	2	−7.5	22	2.8	13.0	4.9	6.4	—	—	—	—	—	—	—	—	—	—	—	—	5.1	4.2	3.8	4.4
XI	—	—	—	—	4.4	−4.1	13.4	7	−18.2	18	−1.4	2.9	−1.0	−0.1	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.7	6.9	7.5
XII	—	—	—	—	3.6	−3.3	9.1	20	−13.8	15	−0.6	2.4	0.2	0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.7	8.1	7.3	7.7
Rok	—	—	—	—	11.5	1.2	31.2	26.VI	−31.0	7. II	4.2	10.0	5.0	6.0	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.2	6.3	6.8

Wisła — φ = 49°39' — λ = 18°52'

I	—	—	—	—	1.6	−3.9	6.7	29	−16.1	8	−1.5	0.7	−1.5	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.7	7.4	8.1
II	—	—	—	—	−3.3	−11.8	3.3	14	−24.9	10	−8.4	−3.9	−7.7	−6.9	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.3	7.4	7.6
III	—	—	—	—	5.6	−3.6	14.7	30	−17.4	11	−1.2	4.8	0.1	1.0	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.8	6.8	6.2
IV	—	—	—	—	10.1	1.6	16.7	6	−4.2	2	3.5	9.2	4.8	5.6	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.3	6.7	7.1
V	—	—	—	—	13.8	4.8	25.0	19	−3.1	3	8.4	13.2	8.3	9.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.4	7.4	7.4
VI	—	—	—	—	20.2	9.7	30.8	26	1.8	3	13.6	18.7	13.8	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.1	6.7	5.8	5.9
VII	—	—	—	—	20.3	11.1	29.2	14	5.5	10	14.8	18.8	14.1	15.4	—	—	—	—	—	—	—	—	—	—	—	—	6.0	8.3	7.4	7.2
VIII	—	—	—	—	19.4	9.6	29.6	7, 8	4.6	31	12.6	18.3	13.0	14.2	—	—	—	—	—	—	—	—	—	—	—	—	5.0	6.4	5.9	5.8
IX	—	—	—	—	19.8	8.1	27.7	3	2.2	22	11.3	18.5	12.4	13.6	—	—	—	—	—	—	—	—	—	—	—	—	4.9	5.3	4.3	4.8
X	—	—	—	—	13.0	1.3	24.5	2	−6.3	22	3.4	12.4	5.0	6.4	—	—	—	—	—	—	—	—	—	—	—	—	3.9	3.1	3.1	3.4
XI	—	—	—	—	3.9	−3.0	12.4	2	−13.2	18	−0.7	2.6	−0.9	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.9	7.3	7.8
XII	—	—	—	—	2.1	−2.3	6.8	21	−10.8	15	−0.4	1.4	−0.4	0.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.5	8.1	8.3
Rok	—	—	—	—	10.5	1.8	30.8	26.VI	−24.9	10. II	4.6	9.6	5.1	6.1	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.9	6.4	6.7

Krosno $H_s = 282$ m $h_w = 15$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	3.7	·	·	7	3.4	7	6.0	33	7.6	1	3.0	2	4.5	16	5.4	21	4.7	37	9.8	31	6	14	28	·	6	2	·	22	13	9	·	6	31	·
II	11	3.7	2	3.5	2	3.5	·	·	15.5	8.8	1.5	7.3	7.5	6.8	26.5	5.4	18	4.7	30	3.7	17	14	27	28	·	5	·	1	16	20	12	·	3	28	·
III	5	5.6	5.5	3.5	6.5	3.5	9.5	3.9	31	7.4	·	·	1	2.0	9.5	5.3	25	4.2	42	6.4	25	5	5	18	·	7	·	3	14	17	10	·	10	16	·
IV	8	4.0	6.5	3.5	24	4.9	8	3.1	11	5.5	4.5	4.2	2	5.5	8	4.6	18	3.6	56	22.7	22	·	·	5	·	·	·	·	15	22	11	1	2	·	1
V	6	3.7	7.5	3.6	4	4.5	14	3.1	12	5.8	3	2.0	2.5	3.6	21	3.0	23	2.8	87	30.7	18	·	·	3	1	1	·	1	20	21	16	1	5	·	2
VI	4.5	3.3	5	2.8	6	2.7	12.5	4.6	12.5	4.9	8	3.2	2	1.5	17.5	3.7	22	2.9	147	27.7	28	·	·	·	5	4	·	2	12	16	11	5	·	·	3
VII	1	3.0	3	2.7	14	2.4	10.5	3.2	27	5.7	3.5	4.6	5	2.6	12	2.3	17	3.1	167	21.6	1	·	·	·	7	3	·	3	12	20	17	8	2	·	5
VIII	1.5	5.3	1.5	2.7	3	2.7	14	3.4	15	6.9	2	3.0	1	4.0	32	3.9	23	3.3	193	44.6	26	·	·	·	2	3	·	3	15	15	10	5	1	·	1
IX	1	6.0	3.5	2.6	3	3.3	23	4.3	27	6.9	2	2.0	·	·	9.5	4.0	21	3.9	57	27.6	11	·	·	·	2	8	·	7	5	6	5	1	2	·	·
X	1	4.0	5.5	3.5	·	·	2.5	2.4	24.5	7.7	·	·	4	3.5	22.5	4.9	33	3.7	13	9.1	4	·	·	7	·	6	·	3	12	5	3	·	6	·	·
XI	2.5	6.8	5	5.6	2	4.5	10	3.6	31	8.1	1	2.0	2	2.5	17.5	4.3	19	4.7	45	10.1	11	—	10	—	·	8	·	·	23	17	13	1	4	9	·
XII	1	3.0	·	·	1	4.0	4	5.2	50.5	7.2	2.5	9.2	1	6.0	13	3.2	20	5.0	28	4.6	18	—	6	—	·	9	·	1	19	18	13	·	·	6	·
Rok	48.5	4.3	45	2.8	72.5	3.3	115	3.6	290	6.9	29	3.4	30	3.5	205	4.2	260	3.9	902	44.6	26.VIII	—	62	—	17	60	2	24	185	190	130	22	41	90	12

Bircza $H_s = 300$ m $h_w = 16$ m

I	4	3.5	1	1.0	4	4.8	6	2.1	9	3.8	25	4.5	11.5	5.1	3.5	5.3	29	2.9	52	17.8	31	3	12	28	·	4	·	3	21	13	11	1	4	31	—
II	8.5	3.1	1.5	3.0	5	4.4	·	·	1.5	9.7	16	6.6	26	4.7	16.5	3.0	9	4.1	49	10.0	16	13	24	28	·	5	·	·	17	20	13	1	1	28	—
III	2.5	2.2	6.5	2.6	10	3.0	4.5	2.7	11	3.8	14.5	4.0	11.5	2.6	5.5	4.6	27	2.4	60	19.0	17	5	4	22	·	·	·	5	12	14	9	2	3	19	—
IV	2.5	2.4	5.5	3.0	31	7.0	5.5	2.5	2	2.0	12	2.3	7	4.1	6.5	3.4	18	3.7	44	12.8	22	·	·	12	·	4	1	1	11	9	9	2	2	·	—
V	11	1.8	4.5	1.6	8	4.0	7	2.9	4	3.0	11	3.5	13.5	3.3	15	3.3	19	2.4	64	15.9	18	·	·	5	1	·	·	2	9	20	14	1	1	·	—
VI	2	2.5	1.5	3.0	10	3.2	8.5	2.7	5.5	3.4	8.5	3.4	11	3.1	20	2.3	23	2.1	139	29.4	10	·	·	·	5	·	·	4	7	13	12	8	·	·	—
VII	1	2.0	2.5	3.0	7	3.7	1.5	4.3	5	2.7	22.5	2.8	21.5	2.7	7	1.3	25	2.0	265	51.4	17	·	·	·	5	·	·	5	4	18	18	9	·	·	—
VIII	6.5	2.0	3	1.0	4	2.0	5	1.3	3	2.2	13.5	2.4	17	3.2	12	2.7	29	1.7	182	49.1	26	·	·	·	6	·	·	5	10	17	14	6	1	·	—
IX	1.5	1.7	1	1.0	2.5	3.4	9.5	3.1	14	3.3	10	2.8	10.5	2.6	8	2.4	33	1.8	59	32.9	11	·	·	·	2	·	·	9	5	12	4	2	3	·	—
X	13.5	1.7	2.5	2.8	6.5	2.5	2.5	1.2	·	·	18.5	3.3	19	3.1	10.5	2.6	20	2.1	17	7.7	4	·	·	9	·	·	·	5	9	15	5	·	6	·	—
XI	4	1.9	6	2.2	9	4.3	3	1.3	14	4.7	15	4.1	15	3.0	9	3.1	15	2.9	57	12.3	11	4	9	21	·	1	·	1	18	14	11	2	1	14	—
XII	3	2.7	1	1.0	2	3.5	2	1.5	10.5	4.4	38.5	3.4	14	2.2	7	1.7	15	2.6	38	6.0	8	2	5	25	·	1	·	1	18	16	12	·	·	9	—
Rok	60	2.3	36.5	2.1	99	3.8	55	2.1	79.5	3.6	205	3.6	177.5	3.3	120.5	3.0	262	2.6	1026	51.4	17.VII	27	54	150	19	15	1	41	141	181	132	34	22	101	—

Mszana Dolna $H_s = 410$ m $h_w = 16$ m

I	1.5	1.6	0.5	3.0	2	1.8	2.5	2.4	6.5	4.0	14.5	2.9	16	2.5	13.5	2.2	36	1.6	60	13.0	31	7	5	27	·	1	·	2	19	15	13	1	—	31	·
II	8.5	1.8	2	1.8	·	·	·	·	2	5.8	15	3.6	14.5	2.4	21	2.4	21	2.0	58	6.8	7	15	23	28	·	1	·	1	18	19	14	·	—	28	·
III	6.5	1.8	2	2.2	2	1.5	6	1.7	3.5	2.4	12	4.2	4.5	4.7	13.5	2.7	43	1.6	39	4.9	31	6	6	21	·	1	·	5	11	17	13	·	—	20	·
IV	8	3.2	6	3.7	5.5	3.5	2.5	3.4	0.5	3.0	2.5	3.2	6.5	3.6	22.5	2.5	36	1.8	44	13.7	22	·	·	9	·	·	·	2	17	14	9	1	—	1	1
V	7	2.2	6.5	2.3	3.5	2.6	·	·	0.5	4.0	5.5	4.1	7.5	3.1	23.5	2.2	39	1.5	157	24.0	6	·	·	3	1	1	1	2	18	23	18	6	—	·	3
VI	9	2.3	2	2.8	1.5	2.3	1	1.5	0.5	12.0	2.5	6.2	7	2.6	20.5	2.6	46	1.4	227	83.8	10	·	·	·	7	1	·	4	9	16	15	6	—	·	5
VII	7	1.5	1.5	2.7	0.5	4.0	0.5	4.0	0.5	3.0	5	3.2	14	2.2	13	2.1	51	1.0	98	21.3	8	·	·	·	6	·	·	2	9	20	17	2	—	·	4
VIII	8	2.1	·	·	2	2.5	3	2.2	1	1.5	3	4.2	10	2.0	14	2.1	52	1.0	177	58.6	1	·	·	·	6	·	·	4	15	16	12	6	—	·	·
IX	1.5	1.0	1.5	1.3	3	2.8	1.5	3.7	3	1.3	8	2.8	10.5	2.1	8	2.2	53	0.9	77	19.2	11	·	·	·	2	·	·	7	4	7	7	4	—	·	·
X	3	3.8	4.5	3.0	3	2.8	0.5	3.0	1	2.0	1	3.5	10	2.1	16	2.7	54	1.1	13	5.4	31	·	·	13	1	·	·	10	6	7	4	·	—	·	·
XI	7.5	1.8	1.5	2.7	1.5	2.7	2	2.0	1.5	1.7	10.5	4.2	13.5	4.3	12	2.5	40	1.8	42	11.4	11	5	9	24	·	1	·	3	19	14	7	1	—	10	·
XII	2.5	3.0	0.5	1.0	0.5	1.0	·	·	4	5.1	19	4.3	11.5	2.8	13	2.1	42	1.8	41	8.0	13	2	3	24	·	1	·	2	17	17	10	·	—	17	·
Rok	70	2.2	28.5	2.2	25	2.3	19.5	2.0	24.5	3.8	98.5	3.9	125.5	2.9	190.5	2.4	513	1.5	1033	83.8	10.VI	35	46	149	23	7	1	44	162	185	139	27	—	107	13

Wisła $H_s = 430$ m $h_w = 14.5$ m

I	0.5	2.0	·	·	3.5	1.3	40	2.6	18.5	2.8	0.5	2.0	15	2.4	15	2.4	·	2.5	78	13.6	9	4	8	27	·	·	·	2	20	17	11	1	1	31	·
II	1.5	1.3	1	1.5	4.5	1.6	16.5	2.1	2	3.2	0.5	2.0	28	2.9	30	2.7	·	2.6	73	9.3	8	16	24	28	·	1	·	3	17	19	14	·	·	28	·
III	0.5	2.0	·	·	4.5	1.6	36	2.3	15.5	2.3	1.5	2.7	17.5	2.3	17.5	2.3	·	2.3	41	8.9	29	3	5	22	·	·	·	6	13	16	12	·	5	16	·
IV	2.5	1.8	3	2.0	3.5	2.1	18	2.2	18.5	2.5	0.5	2.0	6.5	2.5	37.5	2.1	·	2.2	93	14.8	22	·	·	8	·	·	·	4	17	21	16	2	2	1	1
V	6	2.3	3	2.0	1	1.0	7	1.8	33	2.3	·	·	3.5	1.7	38.5	2.4	1	2.2	191	27.1	11	·	·	3	·	·	·	2	18	20	18	8	·	1	4
VI	9.5	1.9	3.5	1.3	5	1.4	5	1.8	26	2.6	·	·	1	3.0	40	2.4	·	2.3	311	83.3	11	·	·	·	5	·	·	3	9	16	16	8	·	·	5
VII	4	2.2	3.5	2.1	·	·	14	1.9	41	2.5	·	·	5	2.2	25.5	2.3	·	2.3	148	44.8	16	·	·	·	4	·	·	1	13	21	15	4	2	·	6
VIII	5	2.6	·	·	5	1.6	11	1.8	29	2.8	1	2.0	1.5	2.0	40.5	2.4	·	2.4	113	24.8	25	·	·	·	6	·	·	7	12	13	10	4	3	·	2
IX	4	1.8	·	·	4	1.2	17	2.1	46	2.6	·	·	1	2.0	18	2.3	·	2.3	86	30.7	19	·	·	·	2	·	·	7	6	12	8	3	·	·	1
X	6	2.2	·	·	9	1.2	13	1.5	23	2.3	·	·	1.5	2.3	40.5	2.1	·	2.0	31	22.1	31	·	·	11	·	·	·	13	4	7	4	1	1	·	·
XI	7	2.4	·	·	2	1.5	16	2.1	29	3.2	·	·	4	2.0	32	2.3	·	2.6	38	8.3	21	4	10	25	·	·	·	3	19	18	7	·	1	11	·
XII	2	2.0	·	·	·	·	19.5	2.8	50.5	3.0	·	·	1	2.0	20	2.2	·	2.8	68	20.3	18	1	6	24	·	·	·	1	23	20	15	1	2	16	
Rok	48.5	2.0	14	0.7	42	1.2	213	2.1	332	2.7	4	0.9	85.5	2.3	355	2.3	1	2.4	1271	83.3	11.VI	28	53	148	17	1	·	52	171	200	146	32	17	104	19

Lubań Wielki — φ = 49°39' — λ = 19°59' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{0,m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−1.6	−5.9	4.1	29	−12.4	8	−4.6	−3.2	−3.8	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.7	7.9	8.4
II	–	–	–	–	−2.0	−12.4	−0.3	1	−20.5	6	−10.8	−8.8	−10.4	−10.1	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.1	8.6	8.5
III	–	–	–	–	2.1	−4.7	9.9	19	−12.4	1	−3.2	0.3	−2.1	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	7.9	7.6
IV	–	–	–	–	5.9	−0.4	11.9	7	−7.1	1	1.0	4.2	1.7	2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	7.5	8.1
V	–	–	–	–	10.6	3.1	21.3	19	−3.9	2	4.7	8.6	5.6	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.3	7.8	7.8
VI	–	–	–	–	16.9	8.2	27.9	26	3.6	14	11.0	15.5	11.2	12.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.8	6.9	6.5
VII	–	–	–	–	16.7	9.2	26.9	14	4.0	6	11.5	14.4	11.7	12.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	8.1	6.2	7.1
VIII	–	–	–	–	15.4	8.4	25.9	8	3.8	2	10.0	13.6	10.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.4	6.4	6.9
IX	–	–	–	–	16.0	7.9	23.3	3	4.6	20	9.9	13.0	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.2	5.4	5.9
X	–	–	–	–	9.5	2.2	20.7	2	−4.1	21	3.8	7.6	4.5	5.1	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.0	5.2	5.1
XI	–	–	–	–	0.2	−5.4	9.5	9	−13.6	17, 24	−3.7	−1.9	−3.3	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.0	7.3	7.4
XII	–	–	–	–	−1.4	−6.0	4.9	20	−13.4	15	−3.9	−3.2	−4.0	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.1	7.5	7.8
Rok	–	–	–	–	6.9	0.4	27.9	26.VI	−20.5	6. II	2.1	5.1	2.7	3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.5	7.0	7.3

Zawoja — φ = 49°37' — λ = 19°31'

I	–	–	–	–	2.0	−5.0	9.0	1	−14.3	7	−1.6	0.1	−1.7	−1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.2	6.9	7.8
II	–	–	–	–	−4.5	−11.4	0.6	12, 13	−23.1	6	−9.1	−5.7	−8.3	−7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.4	7.6	7.6
III	–	–	–	–	4.4	−4.0	11.9	30	−13.5	1	−0.7	2.9	−0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	6.7	6.8
IV	–	–	–	–	8.2	0.5	14.8	7	−4.3	2	3.7	6.9	3.3	4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.8	6.7	7.3
V	–	–	–	–	12.4	3.9	23.3	19	−4.1	3	8.1	10.9	7.1	8.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	8.2	7.4	7.4
VI	–	–	–	–	18.5	8.7	29.0	26	2.1	3	13.6	17.3	12.0	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.5	7.2	7.0	6.6
VII	–	–	–	–	19.0	9.2	26.2	14	3.8	10	14.3	17.0	12.7	14.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.5	8.0	7.9
VIII	–	–	–	–	17.5	8.8	27.5	8	3.4	16	12.0	16.1	11.6	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.6	5.9	6.5
IX	–	–	–	–	18.4	8.3	25.2	2	3.1	22	12.2	16.4	11.9	13.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	5.1	6.2
X	–	–	–	–	12.5	0.9	23.0	2	−5.9	22	3.4	11.3	4.3	5.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.5	4.2	4.9
XI	–	–	–	–	3.1	−4.8	12.1	1	−15.6	17	−2.0	0.9	−1.5	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.5	7.2	7.6
XII	–	–	–	–	2.3	−4.1	9.7	20	−14.6	15	−0.5	0.6	−0.7	−0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.9	8.2	8.6
Rok	–	–	–	–	9.5	0.9	29.0	26.VI	−23.1	6. II	4.4	7.9	4.2	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	6.7	7.1

Nowy Sącz — φ = 49°37' — λ = 20°42'

I	977.3	990.5	954.4	1014.2	2.2	−5.6	8.4	30	−19.1	8	−2.5	0.9	−1.9	−1.4	4.4	4.8	4.6	4.6	85	74	85	81	0.9	1.9	0.9	1.2	8.1	8.2	7.2	7.8
II	980.3	992.7	958.2	1017.9	−1.9	−10.3	3.8	14	−25.8	7	−7.9	−3.4	−6.6	−6.1	3.0	3.3	3.1	3.1	83	68	79	77	0.6	1.6	0.9	1.0	8.4	7.8	7.6	7.9
III	981.7	997.4	953.3	1018.2	7.3	−2.8	16.4	30	−18.1	1	−1.1	5.0	1.9	1.9	5.0	5.7	5.9	5.5	84	65	81	77	1.0	3.6	1.4	2.0	6.9	6.9	6.4	6.7
IV	975.0	992.8	958.8	1010.7	11.8	2.5	17.7	7	−2.5	6	3.9	10.2	6.9	7.0	7.1	7.1	7.5	7.2	86	58	75	73	1.1	5.6	2.6	3.1	8.7	7.8	6.8	7.6
V	978.6	993.5	967.4	1013.8	16.0	6.3	27.3	19	−2.9	4	8.3	14.2	10.8	11.0	9.6	9.9	10.4	10.0	86	61	78	75	1.8	6.9	2.8	3.8	7.7	8.2	7.5	7.8
VI	979.7	988.4	966.6	1014.3	22.2	10.8	32.0	26	3.8	3	13.8	20.4	16.1	16.6	13.4	13.4	14.5	13.8	85	57	79	74	2.4	11.3	4.2	6.0	5.5	6.5	7.0	6.3
VII	979.0	986.0	970.3	1013.7	22.1	11.5	28.4	14, 15	5.6	10	14.1	20.2	15.9	16.5	14.4	14.6	15.4	14.8	89	62	84	78	1.9	9.0	3.0	4.0	6.5	7.9	6.0	6.8
VIII	981.9	989.6	967.1	1016.8	20.8	10.5	30.8	8	5.1	31	12.1	19.1	14.7	15.2	12.7	12.7	13.4	12.9	90	59	81	77	1.7	10.5	3.8	5.2	6.7	7.1	5.7	6.5
IX	981.9	998.8	970.3	1016.8	21.4	9.2	26.6	2, 3	2.9	22	11.3	19.7	13.8	14.6	11.5	12.5	12.9	12.3	86	56	82	75	2.5	11.0	3.2	5.6	6.0	5.9	4.3	5.4
X	988.5	1000.5	978.9	1024.7	13.7	1.7	24.1	2	−5.9	22	3.3	12.2	6.4	7.1	7.5	8.9	8.6	8.3	92	61	86	80	0.7	5.9	1.4	2.7	6.9	5.4	4.5	5.6
XI	977.0	995.9	953.5	1013.7	4.5	−3.3	14.0	2	−16.4	18	−1.1	2.8	0.0	0.4	5.0	5.2	5.1	5.1	84	68	81	78	1.1	2.8	1.4	1.8	8.0	7.3	7.1	7.5
XII	973.2	989.3	954.2	1009.6	4.2	−2.7	9.2	19	−13.9	15	−0.4	2.6	0.5	0.8	4.8	5.1	5.1	5.0	79	69	80	76	1.3	2.4	1.4	1.7	7.3	8.0	7.3	7.5
Rok	979.5	1000.5	953.3	1015.4	12.0	2.3	32.0	26.VI	−25.8	7. II	4.5	10.3	6.5	7.0	8.2	8.6	8.9	8.6	86	63	81	77	1.4	6.1	2.2	3.2	7.2	7.2	6.5	7.0

Istebna - Kubalanka — φ = 49°36' — λ = 18°54'

I	–	–	–	–	−1.1	−5.1	3.6	29	−12.3	7, 8	−3.7	−2.0	−3.2	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	7.9	8.3
II	–	–	–	–	−5.2	−11.0	−0.6	14	−19.2	6	−9.2	−6.4	−8.5	−8.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.0	7.9	7.7
III	–	–	–	–	3.6	−3.3	12.1	30	−10.9	1	−2.0	2.3	−0.6	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.6	6.0	6.6
IV	–	–	–	–	8.1	0.8	14.1	7	−4.9	2	2.3	6.7	3.2	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.8	6.6	7.0
V	–	–	–	–	11.7	4.3	22.4	19	−2.3	2	6.4	10.5	7.1	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.7	7.5	7.7
VI	–	–	–	–	18.2	9.5	29.4	26	3.8	3	11.9	16.3	12.7	13.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.9	6.0	5.6
VII	–	–	–	–	18.0	10.5	27.6	14	4.8	6	12.6	16.3	12.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.9	6.9	7.1
VIII	–	–	–	–	17.3	9.3	27.0	8	4.0	28	11.2	16.0	11.9	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	5.4	5.6
IX	–	–	–	–	17.5	8.8	24.7	2	5.3	20	11.0	15.5	11.8	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.1	4.5	5.0
X	–	–	–	–	11.2	3.1	22.0	2	−2.8	22	4.4	10.1	5.1	6.2	–	–	–	–	–	–	–	–	–	–	–	–	4.5	3.9	2.8	3.7
XI	–	–	–	–	1.5	−4.4	9.4	7	−12.2	17	−2.6	−0.3	−2.2	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.1	7.8	7.7
XII	–	–	–	–	−0.7	−4.3	4.3	20	−11.2	15	−2.7	−1.7	−2.6	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.6	8.5	8.8
Rok	–	–	–	–	8.3	1.5	29.4	26.VI	−19.2	6. II	3.3	6.9	4.0	4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.5	6.7

Luboń Wielki

$H_s = 1023\ m$ $h_w = 18{,}4\ m$ **1965**

MIESIĄC	ROZKŁAD WIATRU (%D.V=D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R ≥0.1	≥1.0	≥10.0	≡	⊠	K ⊠
I	7	2.4	4	3.5	1	4.0	6	2.3	6	2.8	48	5.9	5	2.2	12	4.0	4	4.4	69	12.8	31	2	25	29	·	4	·	·	19	16	12	2	—	31	·
II	17	3.3	2	2.0	3	2.0	2	2.0	2	4.5	25	5.6	13	3.0	20	4.5	·	4.2	92	9.2	8	22	28	28	·	3	·	·	21	19	17	·	—	28	·
III	10	3.2	10	3.1	1	2.0	6.5	2.2	11.5	3.8	39	4.8	5	2.4	9	3.9	1	3.8	42	5.2	27, 31	6	8	25	·	2	·	·	17	15	12	·	—	31	·
IV	13.5	3.5	10.5	4.4	14	3.6	7.5	2.5	9.5	3.3	19	4.2	4	3.2	12	4.2	·	3.8	55	17.9	22	·	2	14	·	·	·	·	19	14	11	1	—	12	3
V	13	4.2	14	2.9	7	3.4	9	3.2	5	2.8	25	5.1	7	3.3	13	4.1	·	3.9	166	30.4	6	·	·	6	·	2	·	1	16	25	18	6	17	1	4
VI	8.5	4.7	5.5	2.7	7	3.6	13	3.1	11	2.0	21	4.0	3	4.3	18	4.6	3	3.6	229	75.5	10	·	·	·	1	1	·	·	10	15	15	7	11	·	5
VII	2	2.0	6	2.0	9	2.6	8	2.0	9	2.2	46	4.1	3	3.3	7	4.9	3	3.3	122	20.8	8	·	·	·	1	2	·	·	10	22	20	4	13	·	8
VIII	12	3.0	5	2.4	4	3.2	14	2.1	8	2.0	25	3.5	3	4.3	15	4.3	7	2.9	170	56.2	1	·	·	·	2	1	·	1	14	15	14	6	11	·	1
IX	6	2.3	4	2.5	1	2.0	17.5	2.6	15.5	3.1	39	3.8	2	2.0	3	3.3	2	3.1	85	23.0	29	·	·	·	·	·	·	6	1	8	8	4	8	·	·
X	12	2.0	10	2.4	5	2.4	8	2.0	6	3.0	34	4.8	7	2.3	8	3.8	3	3.2	21	6.5	31	·	·	12	·	1	·	7	8	12	7	·	14	·	·
XI	3	2.0	9	3.1	5	2.8	5	2.8	7.5	2.5	41.5	5.8	4	3.0	10	2.0	5	3.9	49	13.3	11	8	14	24	·	4	·	·	16	15	12	1	14	19	·
XII	4	2.0	·	·	·	·	1	2.0	5	2.0	69	5.3	3	2.0	11	3.6	·	4.6	55	9.6	18	3	21	28	·	5	·	·	17	16	14	·	14	31	·
Rok	108	2.9	80	2.6	57	2.6	97.5	2.4	96	2.8	431.5	4.7	59	2.9	138	3.9	28	3.7	1155	75.5	10.VI	41	98	166	4	25	·	15	168	192	160	31	—	153	21

Zawoja

$H_s = 670\ m$ $h_w = 18\ m$

I	12	2.2	2	2.0	1.5	2.3	0.5	1.0	22	9.3	8.5	3.2	6.5	2.2	3	2.3	37	3.1	73	11.7	31	2	11	28	·	6	4	1	17	15	12	3	3	30	·
II	8.5	1.8	0.5	2.0	0.5	1.0	2.5	2.6	8.5	4.6	13.5	2.1	9	2.2	9	2.2	32	1.5	80	9.6	16	18	24	28	·	2	·	2	17	20	17	·	·	28	·
III	11	1.3	2	1.5	1	1.0	1	3.0	23.5	8.6	10.5	4.6	3.5	1.4	2.5	1.2	38	3.0	32	6.4	21	4	6	21	·	5	3	6	16	15	10	·	6	21	·
IV	12.5	2.1	4	1.6	·	·	2	1.0	11	3.4	3	4.0	7.5	2.2	5	1.2	45	1.2	96	16.2	22	·	·	10	·	·	·	3	17	19	14	4	8	·	1
V	8	2.0	1	1.0	·	·	0.5	2.0	15	3.0	9.5	2.2	7	1.8	4	1.9	48	1.1	155	22.0	6	·	·	6	·	1	·	2	15	24	16	6	2	·	·
VI	9	1.8	4	2.1	3.5	1.9	3	1.8	7.5	2.4	10	4.1	5	1.6	8	1.9	40	1.3	257	55.4	10	·	·	·	3	2	·	1	10	20	14	8	3	·	4
VII	7	1.3	1	2.0	·	·	·	·	10	4.6	20.5	2.3	5.5	2.0	3	2.3	46	1.3	121	31.2	18	·	·	·	2	2	·	·	15	21	18	3	9	·	4
VIII	12.5	2.3	2	1.5	0.5	1.0	3	4.8	12.5	6.3	7.5	4.2	6.5	1.7	3.5	1.9	45	1.9	188	60.8	1	·	·	·	3	4	·	3	13	21	14	7	5	·	2
IX	4	1.2	3.5	1.6	0.5	1.0	5	4.0	26	6.1	13.5	4.6	5.5	1.3	3	1.3	29	2.9	96	23.5	19	·	·	·	1	5	·	5	12	21	9	5	1	·	1
X	17.5	1.7	3	1.3	1	1.0	0.5	2.0	7.5	1.3	11	2.5	4.5	2.2	7	2.3	41	1.1	27	16.3	31	·	·	16	·	·	·	10	9	16	5	1	4	·	·
XI	11	1.6	1.5	1.7	·	·	·	·	16.5	9.2	14.5	4.9	5	3.0	2.5	1.0	39	2.9	57	9.5	11	5	10	27	·	7	3	2	19	19	12	·	7	17	·
XII	7.5	2.1	0.5	2.0	·	·	2.5	5.0	24.5	7.3	29	4.6	10	2.4	4	1.9	15	4.0	62	12.9	18	3	8	27	·	9	5	·	20	18	15	1	3	19	·
Rok	120.5	1.8	25	1.7	8.5	0.8	20.5	2.3	184.5	5.5	151	3.6	75.5	2.0	54.5	1.8	465	2.1	1244	60.8	1. VIII	32	59	163	9	43	15	35	180	229	156	38	51	115	12

Nowy Sącz

$H_s = 292\ m$ $H_p = 295{,}4\ m$ $h_w = 16{,}5\ m$

I	2.5	1.8	3	1.7	1	1.0	5.5	3.0	4	3.2	14	2.6	5	4.1	3	4.2	55	1.2	60	13.4	31	6	6	26	·	·	·	1	17	16	10	1	13	31	·
II	9.5	3.0	3	1.8	0.5	1.0	·	·	1.5	3.7	11	4.4	15.5	4.1	8	4.2	35	2.2	38	7.9	18	12	22	27	·	5	·	1	14	17	13	·	3	28	·
III	5.5	2.2	3.5	1.7	0.5	2.0	3.5	1.9	13.5	3.2	4	3.5	7	4.2	4.5	3.4	51	1.4	49	9.5	17	3	3	21	·	1	·	5	13	16	11	·	6	18	·
IV	8	2.2	11.5	2.6	10	1.8	6.5	2.0	3.5	2.9	6.5	3.5	6	4.7	5	3.8	33	1.8	31	11.4	22	·	·	4	·	3	·	1	15	11	7	1	2	·	2
V	9.5	2.7	3.5	1.7	2.5	3.0	5	2.0	3	3.5	3	4.7	8	2.9	17.5	2.5	41	1.5	87	14.9	29	·	·	2	1	2	·	·	18	23	16	3	5	·	7
VI	5.5	2.9	8	2.6	·	·	3.5	2.9	6.5	4.1	4.5	4.7	8.5	3.8	8.5	2.9	45	1.7	153	40.0	10	·	·	·	7	·	·	1	11	16	14	6	3	·	7
VII	6.5	2.5	1.5	3.7	1.5	3.7	3	1.8	6.5	3.1	11	3.1	7.5	4.2	3.5	2.0	52	1.3	132	33.7	17	·	·	·	9	1	1	3	11	21	19	3	7	·	7
VIII	3.5	2.4	5	2.0	·	·	1.5	2.3	6.5	2.7	4.5	2.9	5.5	2.7	14.5	3.3	52	1.2	145	44.8	25	·	·	·	8	·	·	5	14	17	13	3	2	·	2
IX	6	2.3	·	·	·	·	6	4.5	16	3.8	6	3.4	3	2.0	4	1.9	49	1.5	60	24.9	11	·	·	·	5	1	·	6	8	8	6	2	8	·	·
X	8.5	1.9	4.5	1.9	3	2.0	0.5	3.0	0.5	3.0	3.5	2.1	6.5	3.1	7	2.6	59	0.8	7	2.8	4	·	·	13	·	·	·	5	11	8	3	·	10	·	·
XI	9.5	1.7	3.5	2.6	2	1.5	2	2.0	7.5	4.8	9	4.4	7.5	3.9	8	3.2	41	1.8	38	19.5	11	3	9	21	·	3	·	2	17	15	7	1	5	10	·
XII	4.5	1.8	1.5	2.0	2	1.5	6.5	1.9	17	3.8	13.5	3.3	6.6	3.0	5.5	3.5	36	1.9	32	5.6	3	2	3	21	·	2	·	2	18	15	11	·	3	15	·
Rok	79	2.3	48.5	2.0	23	1.5	43.5	2.3	86	3.5	90.5	3.6	86.5	3.6	89	3.1	549	1.5	832	44.8	25.VIII	26	43	135	30	18	1	32	167	183	130	20	67	102	25

Istebna-Kubalonka

$H_s = 800\ m$ $h_w = 25{,}6\ m$

I	16.5	2.8	2	3.8	·	·	4.5	2.7	32	4.2	14.5	2.8	2	1.0	7.5	2.1	14	2.8	90	13.8	9	2	24	29	·	1	·	2	21	18	14	4	5	31	·
II	35.5	2.0	3.5	2.4	·	·	2.5	1.0	11	3.5	6.5	3.7	3	1.7	8	2.3	14	2.0	135	19.6	8	16	28	28	·	·	·	1	16	23	18	2	2	28	·
III	13.5	2.1	4.5	1.9	1.5	1.0	4	1.9	32	3.3	11	3.6	4	1.2	9.5	1.1	13	2.2	45	10.8	29	2	7	20	·	·	·	5	14	20	10	1	11	30	·
IV	14.5	2.1	10	2.0	3	1.0	4	1.8	15.5	2.4	7.5	2.0	3	1.3	10.5	2.4	22	1.6	102	16.0	23	·	·	7	·	·	·	4	17	19	17	3	10	1	2
V	15	1.9	11.5	2.5	1	2.0	5	1.6	20	3.9	6.5	2.5	1	2.5	14	2.3	19	2.1	205	36.6	19	·	·	4	·	·	1	1	18	19	17	8	8	1	6
VI	19	2.1	6	2.2	·	·	3.5	1.9	18	2.6	12	2.7	4.5	1.0	12	2.0	15	1.8	352	109.1	11	·	·	·	4	·	·	6	8	16	16	8	2	·	6
VII	5.5	2.1	4.5	1.7	·	·	8	1.4	22	3.1	15.5	2.9	7	1.7	5.5	1.2	25	1.8	180	40.3	16	·	·	·	3	1	·	2	11	24	19	6	8	·	7
VIII	15.5	2.5	8	1.1	·	·	3	3.3	18	4.2	7.5	3.3	2.5	1.6	7.5	1.9	31	1.9	153	37.9	25	·	·	·	2	1	·	6	9	14	12	5	9	·	1
IX	8.5	1.9	1.5	1.0	·	·	8.5	3.6	45.5	4.0	10	3.8	·	·	3	1.7	13	3.0	117	36.0	19	·	·	·	·	1	·	7	8	12	11	5	7	·	·
X	9.5	2.1	12.5	1.2	·	·	2	1.2	22.5	2.2	11	1.7	5	1.2	14.5	1.3	16	1.4	27	17.5	31	·	·	6	·	·	·	13	5	7	4	1	6	·	·
XI	13.5	2.0	11.5	2.0	1	3.0	2.5	3.0	26.5	3.5	15.5	3.1	2.5	2.6	8	1.2	9	2.4	62	13.0	21	5	12	27	·	3	·	2	20	20	13	1	5	18	·
XII	11	2.3	·	·		·	5.5	3.6	40.5	3.9	16.5	3.7	4.5	1.4	2	1.0	13	2.9	78	19.0	18	1	19	30	·	2	·	·	22	22	17	2	14	31	·
Rok	177.5	2.2	75.5	1.8	6.5	0.6	53	2.2	303.5	3.4	134	3.0	38	1.4	102	1.7	204	2.2	1546	109.1	11. VI	26	90	151	9	9	1	48	169	214	168	46	87	140	22

Istebna - Stecówka

φ = 49°35' λ = 18°57' 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.7	−5.2	4.1	28	−13.0	8	−3.4	−1.9	−2.8	−2.7	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.8	8.1	8.6
II	–	–	–	–	−5.6	−11.3	0.0	1	−21.4	6	−9.7	−7.2	−8.7	−8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.6	7.4	7.1
III	–	–	–	–	2.8	−3.4	10.5	30	−11.2	11	−1.8	1.4	−0.5	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.4	6.5	6.4
IV	–	–	–	–	7.6	0.4	13.4	7	−5.0	2	2.2	6.1	3.3	3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.2	7.3	7.4
V	–	–	–	–	11.2	4.2	20.9	19	−3.2	3	6.3	9.7	7.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	8.2	7.8
VI	–	–	–	–	17.6	9.2	28.8	26	3.5	3	11.8	15.9	12.6	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.4	6.0	6.0
VII	–	–	–	–	17.6	10.2	26.5	14	4.6	4, 6	12.6	15.8	12.9	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.4	6.8	7.0
VIII	–	–	–	–	16.8	9.2	26.1	8	4.4	16	11.2	14.8	11.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	4.9	4.8	5.2
IX	–	–	–	–	17.0	9.2	23.9	2	4.5	12	11.3	14.8	11.9	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.5	4.0	4.9
X	–	–	–	–	11.0	2.7	21.1	1	−3.0	21	4.5	8.9	5.2	6.2	–	–	–	–	–	–	–	–	–	–	–	–	4.8	3.6	2.5	3.6
XI	–	–	–	–	1.1	−4.6	8.3	3	−12.9	24	−2.6	−0.6	−2.2	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.8	7.1	7.9
XII	–	–	–	–	−0.8	−4.5	5.4	21	−12.2	15	−2.8	−1.9	−2.6	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.9	7.7	8.7
Rok	–	–	–	–	8.0	1.3	28.8	26. VI	−21.4	6. 11	3.3	6.4	4.0	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.7	6.4	6.7

Istebna - Zaolzie

φ = 49°34' λ = 18°56'

I	–	–	–	–	0.2	−9.0	5.8	28	−24.7	8	−4.6	−0.8	−4.5	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.9	7.6	7.6
II	–	–	–	–	−3.9	−15.6	0.3	14	−30.5	10	−11.1	−4.9	−10.4	−9.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.3	7.3	6.9
III	–	–	–	–	4.2	−6.9	13.0	30	−22.9	1	−3.9	2.8	−2.6	−1.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.1	6.5	6.3
IV	–	–	–	–	9.4	−0.5	16.4	6	−6.9	2	2.1	8.2	2.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.6	6.5	6.9
V	–	–	–	–	13.4	3.3	23.6	19	−5.7	3	7.5	11.8	6.8	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	7.0	7.1
VI	–	–	–	–	19.3	7.5	30.1	26	−1.5	3	13.1	17.6	11.9	13.6	–	–	–	–	–	–	–	–	–	–	–	–	4.4	6.1	5.4	5.3
VII	–	–	–	–	19.2	8.7	28.2	15	1.6	10	14.0	17.5	12.2	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.6	6.7	6.4
VIII	–	–	–	–	18.4	6.8	27.2	7	1.7	18	11.3	17.4	10.5	12.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	5.6	5.6
IX	–	–	–	–	18.5	6.2	25.5	2	−0.4	22	10.1	16.8	9.8	11.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.4	5.7	5.3
X	–	–	–	–	12.3	−2.4	23.0	2	−9.3	22	0.2	11.8	1.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	4.6	3.6	3.5	3.9
XI	–	–	–	–	2.5	−5.4	9.6	2	−18.7	18	−2.8	0.9	−2.5	−1.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	7.6	7.8
XII	–	–	–	–	0.5	−5.9	4.9	20	−17.3	15	−3.1	−0.5	−2.4	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.6	7.8	8.5
Rok	–	–	–	–	9.5	−1.1	30.1	26. VI	−30.5	10. 11	2.7	8.2	2.7	4.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	6.4	6.5

Rabka

φ = 49°37' λ = 19°58'

I	952.6	964.5	928.9	–	1.9	−5.3	8.4	29	−16.6	8	−2.8	0.9	−2.0	−1.5	4.4	4.7	4.6	4.6	86	71	86	81	0.7	2.0	0.8	1.2	8.6	8.3	7.0	8.0
II	955.4	967.3	935.0	–	−2.9	−11.8	2.3	12, 14	−24.9	7	−9.0	−4.2	−8.1	−7.4	2.9	3.2	2.9	3.0	85	69	82	79	0.5	1.4	0.6	0.8	8.7	7.1	7.9	7.9
III	956.9	972.4	929.7	–	6.2	−3.9	15.2	15	−16.6	11	−2.6	4.8	0.0	0.6	4.9	5.3	5.3	5.2	89	62	82	78	0.5	3.7	1.1	1.8	7.5	6.8	6.5	6.9
IV	950.9	968.6	935.2	–	10.3	1.7	18.2	7	−2.7	2	3.0	9.2	5.0	5.6	7.0	6.9	7.3	7.1	91	61	83	78	0.7	5.0	1.5	2.4	8.7	8.0	7.0	7.9
V	954.8	968.4	942.6	–	14.5	5.1	25.3	19	−3.9	3, 4	7.7	12.9	9.1	9.7	9.2	9.5	9.9	9.5	85	64	83	77	1.9	6.1	2.0	3.3	7.5	8.5	7.7	7.9
VI	956.2	955.1	943.1	–	20.8	9.1	30.6	26	2.0	5	12.7	19.1	13.9	14.9	13.1	12.2	13.4	12.9	88	56	84	76	1.8	10.7	2.8	5.1	6.0	7.2	7.2	6.8
VII	955.3	962.0	946.8	–	20.3	10.3	27.7	15	4.6	10	13.6	18.6	14.4	15.2	14.0	14.6	14.2	14.3	89	69	86	81	1.8	7.7	2.6	4.0	7.1	8.6	6.3	7.3
VIII	958.2	965.4	947.0	–	19.2	9.1	29.2	7, 8	3.3	31	11.1	17.9	12.7	13.6	12.3	12.5	12.8	12.5	92	63	86	80	1.2	9.1	2.3	4.2	6.3	7.4	5.7	6.5
IX	957.8	974.4	947.1	–	19.8	7.7	26.9	3	2.1	22	9.8	18.2	11.7	12.8	11.4	12.5	12.1	12.0	93	61	88	81	1.0	9.1	1.8	4.0	6.2	6.2	4.2	5.5
X	963.8	975.2	955.6	–	13.6	1.1	24.6	2	−6.9	22	2.8	12.3	5.0	6.3	7.1	9.1	8.1	8.1	90	62	89	80	0.7	5.8	1.1	2.5	5.3	4.6	3.8	4.6
XI	951.9	971.6	929.7	–	3.9	−4.0	12.4	2	−15.4	18	−1.9	2.1	−1.1	−0.5	4.8	5.0	5.0	4.9	85	68	84	79	0.9	2.6	1.0	1.5	8.2	7.4	7.1	7.6
XII	948.5	964.4	930.7	–	2.6	−3.4	8.2	20	−14.5	15	−1.3	1.2	−0.5	−0.3	4.8	5.0	5.1	5.0	83	74	84	80	1.0	1.8	1.0	1.3	8.1	8.3	6.9	7.8
Rok	955.2	975.2	928.9	–	10.8	1.3	30.6	26. VI	−24.9	7. 11	3.6	9.4	5.0	5.8	8.0	8.4	8.4	8.3	88	65	85	79	1.1	5.4	1.6	2.7	7.4	7.4	6.4	7.1

Brzezna

φ = 49°36' λ = 20°37'

I	–	–	–	–	2.2	−4.8	7.5	29	−17.3	8	−2.2	0.9	−1.5	−1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.2	6.3	7.2
II	–	–	–	–	−2.0	−10.2	4.1	14	−25.0	7	−7.5	−3.2	−6.5	−5.9	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.5	7.3	7.6
III	–	–	–	–	7.1	−2.9	16.7	19, 30	−15.5	1	−1.1	5.4	1.8	2.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.3	6.2	6.2
IV	–	–	–	–	11.9	2.4	18.2	7	−1.7	6	4.6	10.2	6.7	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.7	7.2	7.5
V	–	–	–	–	16.0	6.2	26.8	19	−2.8	4	8.9	14.3	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.1	6.2	7.3
VI	–	–	–	–	22.1	10.9	32.1	26	3.8	3	14.4	20.8	15.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.8	5.8	5.7
VII	–	–	–	–	22.2	11.4	29.3	15	5.5	10	14.9	20.2	15.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.3	3.8	5.6
VIII	–	–	–	–	20.8	10.6	30.5	8	5.3	31	12.8	19.4	14.3	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.3	4.8	5.7
IX	–	–	–	–	21.5	9.4	26.8	9	2.9	22	11.5	20.0	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.0	3.2	4.5
X	–	–	–	–	14.3	1.9	24.3	2	−5.9	22	3.6	12.6	6.4	7.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.5	3.9	4.5
XI	–	–	–	–	4.5	−3.3	14.6	2	−15.2	18	−1.0	2.9	0.0	0.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	6.2	6.6
XII	–	–	–	–	4.1	−2.8	9.9	19	−13.8	15	−0.1	2.7	0.5	0.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.6	5.5	6.4
Rok	–	–	–	–	12.1	2.4	32.1	26. VI	−25.0	7. 11	4.9	10.5	6.4	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	5.5	6.2

Istebna - Stecówka $H_s = 750 m$ $h_w = 12.5 m$ 1965

MIESIĄC	ROZKŁAD WIATRU $^{n}D, V_{m}D$																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	◕	Opad R			≡	⊠	K (K)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15			R≥0.1	R≥1.0	R≥10.0			
I	16	1.8	2	2.0	·	·	18	3.0	20.5	3.2	20.5	3.8	2	2.5	14	1.7	·	2.8	116	21.3	10	2	21	29	·	·	·	·	20	19	15	4	11	31	—
II	19	1.9	5.5	2.0	1	1.0	·	·	8	3.3	12	2.8	2	2.0	36.5	2.5	·	2.4	147	23.0	4	18	27	28	·	·	·	1	13	20	18	6	2²	28	—
III	15	1.6	·	·	1	5.0	2.5	2.6	34.5	2.8	14	3.0	6.5	2.2	18.5	1.4	1	2.3	42	8.4	29	1	7	24	·	·	·	5	15	16	11	·	8	30	—
IV	19.5	1.9	10.5	2.7	3	2.3	·	·	19	2.4	3	2.0	21	1.9	12	1.6	2	2.0	84	12.5	22	·	·	13	·	1	·	3	18	20	15	2	12	1	—
V	28.5	1.7	4	1.5	10	2.7	·	·	19.5	2.9	12.5	2.6	9	1.3	9.5	2.1	·	2.2	180	35.5	19	·	·	5	·	1	·	2	19	21	17	6	15	·	—
VI	21.5	1.4	3	1.5	3	1.0	3.5	1.7	15.5	3.4	10	2.9	10	1.9	7.5	1.5	16	1.7	280	76.3	11	·	·	·	3	1	·	5	10	16	15	7	6	·	—
VII	9	1.3	3	2.7	2	2.0	1.5	1.7	12	3.5	16	3.1	12.5	2.5	1	1.5	36	1.6	158	35.1	18	·	·	·	3	·	·	2	10	23	19	4	13	·	—
VIII	18.5	1.7	3.5	1.3	2.5	1.6	1.5	3.3	22.5	2.4	11	1.8	5.5	2.0	6	2.1	22	1.5	149	32.3	25	·	·	·	2	·	·	8	11	14	12	5	9	·	—
IX	7.5	1.4	1	2.0	5	4.0	3.5	5.4	46.5	3.9	12	2.3	1	2.0	2.5	1.4	11	3.0	109	40.0	19	·	·	·	·	2	·	8	7	11	10	4	8	·	—
X	19.5	1.4	3	1.8	5	1.6	2.5	1.8	20	1.8	6.5	2.0	1	1.0	4.5	1.3	31	1.1	24	14.9	31	·	·	10	·	·	·	13	6	6	5	1	5	·	—
XI	20	2.0	1	1.0	3	2.0	1.5	1.7	23.5	5.3	13	3.1	7	3.3	5	1.9	16	2.7	60	12.2	21	6	12	27	·	4	2	3	20	18	12	1	4	17	—
XII	8	1.9	2.5	1.8	2	4.0	1	2.0	57	3.4	9	2.1	4	1.2	8.5	2.1	1	2.8	88	16.0	18	1	21	30	·	·	·	·	24	24	16	3	11	31	—
Rok	202	1.7	39	1.7	37.5	2.3	35.5	1.9	298.5	3.2	139.5	2.6	81.5	2.0	125.5	1.8	136	2.2	1437	76.3	11.VI	28	88	166	8	9	2	50	173	208	165	43	104³	138	—

Istebna - Zaolzie $H_s = 580 m$ $h_w = 15.4 m$

I	10.5	2.7	2	3.0	5.5	1.3	3.5	2.6	12.5	2.2	11	2.5	2	1.8	2	2.5	44	1.2	87	14.3	10	12	16	29	·	·	·	3	14	15	15	4	13	31	·
II	17.5	2.4	6	2.8	2	1.5	1	4.0	7	2.4	5	2.9	6	2.9	7.5	2.6	32	1.6	112	13.6	4	19	27	28	·	·	·	1	14	20	20	3	12	28	·
III	13.5	1.8	2	2.5	2	1.0	1	2.0	17	2.6	11.5	2.7	6.5	2.2	5.5	3.3	34	1.5	41	7.1	21, 29	9	6	24	·	·	·	4	10	10	10	·	13	29	·
IV	12	2.6	6	2.2	7	2.7	·	·	8	2.6	8	2.4	5	2.0	3	3.7	41	1.4	79	12.8	23	·	·	17	·	·	·	4	15	15	15	2	16	1	2
V	18	2.1	10	1.8	4	1.8	0.5	4.0	6.5	3.8	7	2.9	4	3.2	3	2.0	40	1.4	187	37.3	19	·	·	7	·	1	·	2	16	18	18	8	17	·	4
VI	11.5	1.7	2.5	2.0	3	2.7	1	2.0	6	2.5	6	3.0	3.5	2.0	8.5	2.5	48	1.1	295	105.0	11	·	·	1	5	·	·	3	7	15	15	7	5	·	5
VII	6.5	1.7	3	2.0	2.5	2.8	1.5	2.0	7.5	2.4	12.5	2.7	12.5	2.3	4	2.0	43	1.2	177	24.5	17	·	·	·	3	·	·	1	7	18	18	6	9	·	4
VIII	14	2.0	1.5	3.3	4	2.8	3	2.0	6	2.2	10	3.1	7	2.3	4.5	3.0	43	1.3	132	27.6	24	·	·	·	2	·	·	4	5	12	12	4	14	·	1
IX	3	3.0	1	6.0	3	2.3	6	3.3	14	2.4	15	2.3	3	2.0	3	2.7	42	1.4	84	24.9	28	·	·	1	1	·	·	5	3	9	9	3	6	·	1
X	10	1.8	4	1.8	1	2.0	3	2.7	3	1.7	10	2.2	4	2.0	·	·	58	0.8	30	15.3	31	·	·	24	·	·	·	11	3	4	4	1	11	·	·
XI	7	1.7	8	2.4	4	2.5	1	4.0	8	3.1	8	2.8	7	2.9	2	2.0	45	1.3	52	10.3	21	6	9	27	·	·	·	2	20	13	13	1	11	17	·
XII	7	2.3	1	4.0	1	2.0	1	2.0	17	2.2	9	3.0	9	2.3	1	1.0	47	1.2	99	21.0	18	5	13	29	·	·	·	·	20	17	17	3	13	31	·
Rok	130.5	2.2	47	2.8	39	2.1	22.5	2.6	112.5	2.5	113	2.7	69.5	2.3	44	2.3	517	1.3	1375	105.0	11.VI	51	71	187	11	1	·	40	134	166	166	42	140	137	17

Rabka $H_s = 511 m$ $H_b = 500.8 m$ $h_w = 19 m$

I	2.5	2.6	5	3.1	1.5	1.3	1	1.0	17.5	2.7	21	3.8	13	2.9	4.5	1.4	27	2.1	64	16.1	31	3	9	28	·	1	1	1	19	17	10	1	·	31	·
II	4	2.5	9.5	2.0	0.5	1.0	0.5	2.0	5.5	3.8	17.5	5.4	15	2.5	7.5	5.3	24	2.7	72	7.1	8	16	22	28	·	6	2	·	16	19	16	·	·	28	·
III	2.5	1.8	7.5	3.5	2	1.5	8	1.9	14	1.7	21	3.4	6.5	3.5	8.5	2.7	23	2.0	39	5.7	24	5	6	20	·	3	·	6	16	18	12	·	3	23	·
IV	6.5	2.8	18.5	3.8	8	2.1	4	2.5	4	2.1	13.5	2.4	13.5	1.7	5	2.5	17	2.1	50	15.1	22	·	·	9	·	2	·	1	18	14	9	1	3	1	3
V	5	2.8	13	2.1	4.5	2.3	3	1.3	11	1.0	15	5.2	11	2.0	14.5	2.2	16	2.1	122	19.5	19	·	·	4	1	2	1	2	19	25	21	3	1	·	7
VI	6	2.7	7.5	2.6	4	1.9	6	1.1	5.5	1.8	16.5	4.0	14	2.2	9.5	3.3	22	2.1	242	85.5	10	·	·	·	5	4	2	2	10	15	14	8	1	·	6
VII	2	2.2	6.5	2.6	5.5	2.2	7	1.3	10.5	1.6	26.5	2.7	10	2.2	4	3.0	21	1.8	117	22.3	8	·	·	·	3	1	·	2	13	20	18	4	·	·	7
VIII	3.5	3.3	10	2.8	2	1.0	7.5	1.4	11.5	1.3	14.5	3.6	10	2.3	4	2.8	30	1.6	185	61.0	1	·	·	·	4	·	·	5	14	18	12	5	1	·	1
IX	3	2.2	3	1.3	1.5	1.3	4.5	1.0	16.5	2.2	23.5	3.3	13	2.1	4	2.0	21	1.9	70	21.1	11	·	·	·	2	·	·	6	7	8	6	4	1	·	·
X	6	2.2	4	3.2	4.5	2.3	5.5	1.8	5.5	1.4	15	2.7	17	1.6	7.5	2.5	28	1.5	11	3.0	31	·	·	10	·	1	·	11	9	9	4	·	4	·	·
XI	7.5	1.6	8	2.8	1	1.0	1.5	1.7	10	4.8	18.5	5.3	11	3.6	4.5	2.1	28	2.6	45	20.9	11	5	10	24	·	6	2	2	19	18	6	1	2	10	·
XII	1	1.5	1	3.0	1	1.0	1	1.0	13	3.5	37.5	3.4	11.5	2.5	9	1.8	18	2.4	49	11.0	3	1	7	25	·	5	2	1	20	17	10	1	·	25	·
Rok	49.5	2.4	93.5	2.7	36	1.6	48.5	1.5	124.5	2.3	240	3.8	145.5	2.4	82.5	2.6	275	2.1	1066	85.5	10.VI	30	54	148	15	31	10	39	180	198	138	28	16	118	24

Brzezna $H_s = 320 m$ $h_w = 16.9 m$

I	3.5	2.9	2.5	1.8	1	1.0	0.5	5.0	23.5	6.5	12.5	4.5	2.5	3.4	3	5.8	44	2.7	47	16.5	31	4	5	28	·	2	2	1	15	8	8	1	1	31	—
II	17.5	4.5	3.5	4.0	·	·	·	·	5	4.6	5	6.9	7.5	3.0	16.5	4.8	29	3.0	46	7.5	18	14	20	28	·	2	1	2	18	15	15	·	1	28	—
III	5.5	2.7	3.5	3.1	·	·	1	6.0	13.5	7.5	9.5	2.7	3	4.0	5	4.4	52	2.1	46	7.4	17	4	6	20	·	2	2	6	9	12	12	·	5	16	—
IV	7.5	4.9	14.5	3.8	0.5	3.0	4.5	3.1	7.5	4.6	3	3.0	5.5	4.2	4	3.5	43	2.1	32	15.5	22	·	·	5	·	·	·	1	16	8	8	1	3	·	—
V	16.5	4.2	11	3.0	·	·	1	3.5	3	5.5	3	4.8	3.5	2.3	10	3.6	45	2.0	91	15.8	29	·	·	2	1	2	·	1	12	17	16	2	1	·	—
VI	9.5	2.7	2.5	2.4	2	3.0	2.5	3.2	8	4.0	4	4.4	4	2.9	7.5	2.4	50	1.4	176	40.0	10	·	·	·	7	·	·	3	8	14	14	7	1	·	—
VII	4	3.0	4.5	3.1	1.5	3.7	·	·	8	5.6	2	3.5	6.5	2.6	4.5	6.6	62	1.4	137	23.1	18	·	·	·	9	1	1	2	5	18	18	5	·	·	—
VIII	10	3.0	4.5	2.0	0.5	2.0	2.5	2.2	8	4.9	4	2.6	1.5	2.0	8	3.1	54	1.3	144	45.9	1	·	·	·	6	1	·	7	10	11	11	4	1	·	—
IX	5.5	2.2	1	3.0	0.5	3.0	4.5	4.1	16.5	4.5	3.5	1.9	2	2.5	1.5	2.7	55	1.4	62	29.4	11	·	·	·	4	·	·	7	4	5	5	2	·	·	—
X	5	1.9	7.5	2.1	1.5	3.7	0.5	1.0	3.5	4.4	2	2.0	4.5	2.9	2.5	2.6	66	0.8	6	2.7	11	·	·	11	·	·	·	8	5	3	3	·	6	·	—
XI	8	2.2	6.5	3.2	·	·	1.5	2.3	13	7.7	8.5	5.5	1	3.0	5.5	2.1	45	2.3	34	22.0	11	5	9	22	·	5	3	3	13	6	6	1	2	10	—
XII	5.5	2.5	3	2.0	·	·	2.5	5.0	23	7.2	13.5	3.7	4	2.6	4.5	2.8	37	2.9	22	7.4	18	2	2	24	·	5	3	3	10	7	7	·	1	8	—
Rok	99	3.1	64.5	2.8	7.5	1.6	21	3.0	132.5	5.6	70.5	3.8	45.5	3.0	72.5	3.7	582	2.0	843	45.9	1.VIII	29	42	140	27	20	12	44	125	124	123	23	22	93	—

Płaszkowa — φ = 49°36' — λ = 20°53' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.2	−4.7	7.2	30	−12.8	8	−2.5	−0.7	−2.3	−2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	6.3	7.2
II	–	–	–	–	−3.8	−10.2	3.2	14	−21.9	7	−8.3	−5.5	−7.1	−7.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.2	7.6	8.2
III	–	–	–	–	5.3	−2.7	13.8	30	−11.6	11	−0.9	3.2	1.0	1.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	6.0	6.4
IV	–	–	–	–	9.4	2.0	13.9	7	−3.2	1	3.8	7.6	5.4	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	6.3	7.6
V	–	–	–	–	13.8	5.5	24.9	19	−2.6	3	7.9	11.9	9.0	9.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.7	7.5	7.9
VI	–	–	–	–	20.0	10.4	28.8	26	4.7	3	13.9	18.1	14.3	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.2	6.8	6.1
VII	–	–	–	–	20.2	11.4	28.5	16	6.0	10	14.6	18.0	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.7	5.7	6.6
VIII	–	–	–	–	18.6	10.2	28.9	8	4.9	11	12.6	17.1	13.8	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.8	5.8	6.4
IX	–	–	–	–	19.3	9.6	25.1	5	4.4	22	11.8	17.5	13.4	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.9	3.4	4.9
X	–	–	–	–	11.6	2.6	21.9	2	−5.0	22	4.1	10.1	6.1	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.5	4.4	5.3
XI	–	–	–	–	2.9	−4.2	13.3	2	−11.8	17, 25	−1.5	1.0	−0.8	−0.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.4	6.6	7.3
XII	–	–	–	–	2.8	−3.3	9.9	20	−10.4	15	−0.5	1.0	−0.4	−0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	6.9	7.3
Rok	–	–	–	–	10.1	2.2	28.9	8.VIII	−21.9	7. II	4.6	8.3	5.6	6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.2	6.1	6.7

Babia Góra — φ = 49°35' — λ = 19°31'

I	–	–	–	–	−1.9	−6.7	3.4	31	−14.3	7	−4.6	−3.4	−4.2	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.5	5.8	7.8
II	–	–	–	–	−7.7	−13.8	0.8	1	−19.9	5	−11.9	−9.6	−11.0	−10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	6.8	7.1
III	–	–	–	–	0.4	−5.8	7.4	30	−13.2	9	−3.7	−1.0	−3.2	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	6.3	6.6
IV	–	–	–	–	4.2	−1.4	10.3	7	−8.8	1	0.6	2.8	0.6	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	7.9	7.9
V	–	–	–	–	8.6	1.2	18.3	19	−5.8	3	3.8	6.3	3.9	4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.7	7.0	7.5
VI	–	–	–	–	15.1	6.4	25.5	26	1.5	3	10.3	13.3	9.5	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	6.5	6.4
VII	–	–	–	–	14.7	8.0	22.7	15	1.8	4	11.3	12.7	10.2	11.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	8.2	6.4	7.0
VIII	–	–	–	–	13.7	7.0	23.2	8	2.6	2	9.2	12.1	9.1	9.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.3	5.4	6.3
IX	–	–	–	–	13.7	6.7	20.7	2	2.6	22	9.2	11.9	9.2	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.1	3.8	5.1
X	–	–	–	–	8.8	−1.3	18.3	2	−5.5	21	3.6	7.3	3.2	4.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	4.3	3.4	4.6
XI	–	–	–	–	−1.1	−6.2	6.9	2	−15.2	17	−4.1	−3.0	−4.0	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	6.9	7.7
XII	–	–	–	–	−2.2	−6.6	5.8	19	−13.5	14	−4.2	−3.7	−4.3	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.0	8.0	8.8
Rok	–	–	–	–	5.5	−1.0	25.5	26.VI	−19.9	5. II	1.6	3.8	1.6	2.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	6.2	6.9

Kamienica — φ = 49°36' — λ = 20°21'

I	–	–	–	–	1.9	−7.0	7.8	29	−20.0	8	−3.9	0.7	−3.3	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	6.2	7.2
II	–	–	–	–	−2.2	−12.5	3.9	12	−28.4	7	−8.8	−3.9	−8.0	−7.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	6.2	7.2
III	–	–	–	–	6.4	−4.7	16.0	30	−20.1	11	−2.9	4.9	−0.7	0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	6.4	6.7
IV	–	–	–	–	11.0	1.3	18.1	7	−2.7	2, 6	3.6	9.2	5.2	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.8	6.5	7.4
V	–	–	–	–	15.1	4.7	25.8	19	−3.9	4	8.1	13.4	8.8	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.1	7.0	7.4
VI	–	–	–	–	21.1	8.8	30.7	26	1.0	3	14.1	19.4	13.3	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.3	6.9	6.1
VII	–	–	–	–	21.3	9.5	28.6	24	3.6	10	14.2	19.4	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.5	5.2	6.3
VIII	–	–	–	–	19.9	8.0	30.2	8	2.3	3, 31	11.5	18.2	12.1	13.5	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.6	6.2
IX	–	–	–	–	20.5	6.7	25.8	3	−0.1	22	10.0	18.7	11.2	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.2	4.2	5.0
X	–	–	–	–	13.8	−0.2	23.8	2	−7.4	22	1.8	12.3	4.4	5.7	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.3	4.0	4.5
XI	–	–	–	–	4.2	−4.6	14.8	1	−16.2	17	−2.0	2.3	−1.3	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	5.7	6.7
XII	–	–	–	–	3.5	−4.4	10.0	20	−15.5	15	−1.9	1.8	−0.7	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	6.3	6.8
Rok	–	–	–	–	11.4	0.5	30.7	26.VI	−28.4	7. II	3.6	9.7	4.6	5.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	5.8	6.4

Raba Wyżna — φ = 49°34' — λ = 19°53'

I	–	–	–	–	1.5	−5.1	7.9	29	−16.0	8	−2.9	0.2	−2.0	−1.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	7.0	7.3
II	–	–	–	–	−3.2	−11.5	1.5	14	−20.6	6, 7	−8.7	−4.6	−8.2	−7.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.8	6.5	7.2
III	–	–	–	–	5.7	−3.7	14.6	30	−15.6	11	−1.8	4.3	0.3	0.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.8	6.1	6.2
IV	–	–	–	–	10.3	1.8	17.2	7	−3.3	2	3.7	8.9	4.9	5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.8	7.0	7.5
V	–	–	–	–	14.5	5.1	24.5	19	−3.9	3	8.0	12.7	8.7	9.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.0	6.6	6.7
VI	–	–	–	–	20.3	9.3	30.0	26	3.1	3	13.8	18.8	13.3	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.7	6.2	5.7
VII	–	–	–	–	20.3	10.8	27.6	15	5.0	10	14.4	18.5	13.8	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.3	5.2	6.2
VIII	–	–	–	–	19.0	9.1	28.9	8	4.0	3	11.6	17.5	12.4	13.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.4	5.4	5.8
IX	–	–	–	–	19.6	8.0	27.0	3	4.5	30	11.0	18.1	11.8	13.2	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.1	4.2	4.6
X	–	–	–	–	13.5	1.7	23.6	2	−4.7	22	3.9	12.1	5.0	6.5	–	–	–	–	–	–	–	–	–	–	–	–	4.5	3.8	2.9	3.7
XI	–	–	–	–	3.3	−3.8	12.0	2	−13.2	24	−1.8	1.6	−1.1	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	6.0	6.6
XII	–	–	–	–	2.5	−3.4	9.1	20	−15.0	15	−0.9	1.0	−0.4	−0.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	6.9	7.3
Rok	–	–	–	–	10.6	1.6	30.0	26.VI	−20.6	6, 7. II	4.2	9.1	4.9	5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.4	5.8	6.2

Płaszkowa $H_s = 522$ m $h_w = 15.7$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V≥15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	4	2.2	1	2.0	10	2.5	6	2.7	19	5.1	10	3.1	14	4.9	2	2.5	27	2.7	56	10.0	31	3	12	29	·	3	1	3	13	17	10	1	2	31	·
II	10	3.2	2	1.5	1	1.0	2	4.0	6	4.3	13	5.5	41	5.0	3	2.3	6	4.2	53	10.1	18	12	24	28	·	9	·	1	18	19	14	1	1	28	·
III	9	2.2	·	·	8	2.8	6	6.5	16	4.5	8	2.9	12	3.7	5	1.8	29	2.5	51	8.9	24	1	6	20	·	3	·	6	10	16	12	·	8	21?	·
IV	4	2.2	13	3.5	18	3.1	9	3.6	9	1.9	13	3.2	13	4.3	2	5.5	9	3.0	43	13.5	22	·	·	5	·	·	·	·	15	13	8	1	4	1	3
V	4	3.0	12	2.2	6	3.3	5	2.8	9	2.4	16	3.8	20	2.5	10	2.9	11	2.5	108	15.4	29	·	·	3	·	1	·	1	17	23	19	3	1	·	2
VI	3	2.7	7	1.6	7	2.1	8	3.2	11	3.8	11	3.4	20	3.2	10	3.4	13	2.6	179	46.1	10	·	·	·	4	1	·	1	11	15	14	6	2	·	4
VII	5	1.4	8	1.8	3	2.0	4	2.2	10	4.3	25	3.5	16	2.9	2	2.5	20	2.4	157	29.8	18	·	·	·	4	·	·	3	8	23	18	5	4	·	9
VIII	5	1.8	5	2.2	5	2.6	8	4.0	12	3.7	17	2.8	26	3.0	7	3.1	8	2.8	177	38.5	1	·	·	·	3	·	·	4	13	15	13	6	3	·	1
IX	3	2.0	3	1.3	8	2.2	13	4.8	22	3.9	13	2.5	12	1.9	5	2.2	11	2.7	54	17.8	11	·	·	·	1	2	·	5	6	9	8	2	·	·	·
X	6	2.0	13	2.1	6	1.3	7	1.6	2	2.5	10	2.8	24	3.0	5	2.4	20	1.9	12	4.0	4	·	·	8	·	·	·	7	9	6	5	·	6	·	·
XI	7	1.4	9	2.2	2	3.5	12	5.2	8	8.6	15	4.3	15	3.3	4	2.8	18	3.3	39	17.4	11	5	10	22	·	6	2	2	16	15	9	1	5	10	·
XII	·	·	4	1.5	5	1.8	13	4.5	19	5.2	20	3.6	20	3.5	·	·	12	3.4	34	12.4	18	1	9	26	·	6	1	2	16	17	9	1	2	21	·
Rok	60	2.0	77	1.8	79	2.4	93	3.8	143	4.2	171	3.4	233	3.4	55	2.6	184	2.8	963	46.1	10.VI	22	61	141	12	31	4	35	152	188	139	27	38	112?	19

Babia Góra $H_s = 1180$ m $h_w = 17.5$ m

I	·	·	·	·	·	·	6.5	9.5	23	6.8	10.5	7.4	9	4.8	3	6.7	41	3.9	117	20.3	10	6	21	31	·	6	1	·	16	17	15	4	18	31	·
II	4	5.5	·	·	·	·	·	·	2	6.5	1.5	3.7	13.5	4.6	·	·	63	1.2	178	30.3	27	24	27	28	·	·	·	6	18	23	20	7	18	28	·
III	·	·	·	·	1	3.0	1	5.0	17	4.5	13.5	5.9	8.5	3.2	1	5.0	51	2.1	54	11.7	21	7	10	29	·	·	·	5	14	17	10	1	14	31	·
IV	4.5	3.4	·	·	3	2.0	2.5	3.0	10	2.7	5.5	3.0	5	3.0	1.5	3.0	58	1.0	109	22.2	22	·	3	20	·	·	·	2	20	20	13	4	14	30	·
V	7	3.6	1	3.5	1	4.0	3	3.7	6	2.8	7	3.5	6	3.8	1	3.0	61	1.2	184	27.3	19	·	·	11	·	·	·	2	16	23	20	8	17	17	3
VI	2.5	9.4	·	·	1	4.0	3.5	4.9	6	4.5	2.5	3.6	11.5	2.6	2	3.5	61	1.3	320	62.3	10	·	·	·	1	1	1	2	8	18	15	8	15	-	4
VII	3	2.3	·	·	1	2.0	1	6.0	14.5	4.1	1.5	2.7	20	3.6	3	3.3	49	1.7	153	28.2	18	·	·	·	·	1	·	·	12	21	18	4	14	-	3
VIII	2.5	1.6	·	·	·	·	4	3.5	14	6.0	3	4.2	7	2.1	5.5	3.6	57	1.6	215	51.6	1	·	·	·	·	2	·	3	10	18	15	7	15	·	1
IX	2	3.5	·	·	3	2.7	11	8.6	24	5.5	9	3.7	6	2.3	·	·	35	3.2	106	23.5	19	·	·	·	·	5	·	6	7	12	9	6	8	·	·
X	5.5	1.7	·	·	·	·	·	·	13.5	3.9	4.5	4.8	10	2.5	2.5	2.6	57	1.2	29	13.2	31	·	·	14	·	·	·	10	7	8	7	1	14	·	·
XI	·	·	·	·	5	5.4	1	9.0	10.5	3.9	10.5	6.6	12	3.6	1	5.0	50	2.2	90	18.3	11	8	13	25	·	3	·	3	19	19	16	3	16	21	·
XII	1.5	3.3	·	·	·	·	3.5	8.1	20	3.8	28.5	5.0	15	2.5	2.5	3.6	22	3.2	122	29.2	18	2	26	29	·	2	·	·	24	21	16	3	15	31	·
Rok	32.5	2.9	1	0.3	15	1.9	37	5.1	160.5	4.6	97.5	4.5	123.5	3.2	23	3.3	605	2.0	1677	62.3	10.VI	47	100	187	1	20	2	39	171	217	174	56	178	189	11

Kamienica $H_s = 460$ m $h_w = 21$ m

I	2	2.0	2	2.0	6.5	1.5	2.5	2.0	1	8.0	13.5	2.4	23.5	2.4	11	4.3	31	1.8	53	12.7	31	11	7	30	·	1	·	2	14	16	12	1	·	31	·
II	6	2.5	·	·	3.5	2.3	2.5	2.4	·	·	10	6.0	37.5	3.4	13.5	3.8	11	3.2	58	6.8	8	16	22	28	·	3	2	2	14	21	17	·	1	28	·
III	5	2.0	0.5	3.0	3	1.8	7.5	2.9	3.5	3.7	17.5	2.7	28.5	2.8	10.5	2.4	17	2.2	33	5.7	31	7	4	23	·	2	·	4	11	17	10	·	2	23	·
IV	2.5	4.4	2.5	2.2	16.5	2.8	6.5	2.8	5	2.4	10.5	2.1	24	2.8	7.5	4.7	15	2.4	37	9.4	21	·	·	9	·	1	·	1	15	17	9	·	5	1	2
V	1	2.5	3.5	1.9	6.5	2.5	4	2.0	1.5	4.3	8	3.3	39	2.6	9.5	2.9	20	2.1	110	11.7	11	·	·	6	2	·	·	1	14	21	17	5	3	·	5
VI	2.5	2.6	4	3.4	8.5	2.3	10	2.8	5.5	1.9	8	3.1	19.5	3.2	12	2.8	20	2.2	173	57.4	10	·	·	·	6	·	·	2	9	15	15	6	3	·	5
VII	1	1.0	·	·	6	2.1	7	4.1	4.5	2.0	19.5	4.3	22	2.9	7	3.5	26	2.4	83	15.4	8	·	·	·	7	3	1	2	7	20	15	3	3	·	7
VIII	1.5	2.7	0.5	2.0	6.5	2.8	6.5	3.5	4	2.5	14	2.3	29.5	2.4	8.5	2.2	22	1.9	133	49.3	1	·	·	·	6	·	·	2	12	14	10	3	3	·	1
IX	0.5	2.0	·	·	4	3.9	15.5	3.7	8	2.2	19.5	2.2	22	2.1	4.5	1.7	16	2.1	64	25.3	11, 29	·	·	1	2	·	·	6	4	8	6	2	5	·	·
X	4	3.0	2	3.0	4.5	1.9	5.5	2.1	4.5	1.7	14	1.7	20.5	2.9	7	2.6	31	1.6	15	3.8	9, 31	·	·	20	·	·	·	8	4	8	5	·	4	·	·
XI	5.5	2.5	2.5	1.6	2	2.5	6.5	2.6	2	5.2	19	6.0	18	2.7	8.5	1.5	26	2.5	37	16.0	11	6	10	25	·	3	2	3	14	15	9	1	2	11	·
XII	4	2.2	6.5	1.5	4.5	2.6	4	2.1	3	1.8	8.5	3.2	15.5	2.8	17	3.8	30	1.9	39	7.1	3	3	3	25	·	1	·	1	12	14	11	·	·	18	·
Rok	36.5	2.4	24	1.7	72	2.4	78	2.8	42.5	3.0	162	3.3	299.5	2.8	116.5	3.0	265	2.2	835	57.4	10.VI	43	46	167	23	14	5	34	130	186	136	21	31	112	20

Raba Wyżna $H_s = 600$ m $h_w = 16$ m

I	2	2.0	2	1.0	1	1.0	20	1.1	13	3.3	15	5.3	·	·	2	1.0	38	1.6	47	15.5	31	3	11	27	·	3	·	3	16	13	12	2	4	31	·
II	2	1.0	10	1.0	·	·	8	1.0	8	3.8	12	4.0	3	1.0	11	1.9	30	1.5	71	7.5	8	17	23	28	·	1	·	1	13	17	17	·	·	28	·
III	3	1.0	8	1.2	2	1.0	23	1.0	9	2.3	13	2.1	5	1.0	4	1.5	26	1.0	38	6.0	22, 26	4	6	20	·	·	·	6	12	14	10	·	2	18	·
IV	2	1.0	13	1.0	5	1.0	19	1.0	7	1.0	11	1.4	1	1.0	6	1.0	26	0.8	46	16.5	22	·	·	7	·	·	·	1	16	13	6	1	6	·	2
V	19	1.0	8	1.0	3	1.0	8	1.2	3	3.0	16	1.9	1	1.0	12	1.3	23	1.0	123	25.5	19	·	·	4	·	·	·	4	12	21	18	3	·	·	6
VI	14	1.0	4	1.0	4	1.0	17	1.0	6	1.7	9	1.9	3	1.7	9	1.2	24	0.9	230	73.3	10	·	·	·	5	·	·	4	7	15	15	8	·	·	4
VII	1	1.0	6	1.0	5	1.0	17	1.0	7	1.3	22	1.6	4	1.5	5	1.0	26	0.9	110	29.0	8	·	·	·	3	·	·	2	7	18	15	3	·	·	5
VIII	16	1.1	1	1.0	2	1.0	14	1.0	7	1.6	10	1.6	·	·	14	1.0	29	0.8	173	71.0	1	·	·	·	3	·	·	7	9	12	11	4	3	·	1
IX	3	1.0	2	1.0	1	1.0	28	1.0	12.5	1.2	10.5	1.4	1	1.0	4	1.0	28	0.8	80	22.5	11	·	·	·	2	·	·	8	6	7	6	3	1	·	·
X	6	1.0	11	1.0	10	1.0	34	1.1	2	2.0	4	3.0	2	1.0	6	1.0	18	0.9	9	2.5	4	·	·	11	·	·	·	13	6	7	4	·	1	·	·
XI	·	·	13	1.0	·	·	24	1.2	9	2.1	12	3.2	3	2.3	2	1.0	27	1.2	42	15.0	11	5	10	25	·	1	·	4	14	12	10	1	3	10	·
XII	4	1.5	2	1.0	·	·	15	1.3	13	2.7	30	4.0	·	·	2	2.0	27	2.0	50	9.0	3, 13	1	7	25	·	2	1	1	15	15	11	·	·	17	·
Rok	72	1.0	80	1.0	33	0.8	227	1.1	96.5	2.2	164.5	2.6	23	1.0	77	1.2	322	1.1	1019	73.3	10.VI	30	57	147	13	7	1	54	133	164	135	25	20	104	18

Iwonicz - Zdrój

φ = 49°34' λ = 21°48' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{a.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.3	−4.5	4.5	31	−12.7	11	−2.7	−0.8	−2.0	−1.9	4.4	4.7	4.7	4.6	86	81	87	85	0.7	1.2	0.7	0.9	7.6	8.3	7.1	7.7
II	—	—	—	—	−4.3	−10.3	0.5	1	−22.1	7	−8.5	−5.7	−7.7	−7.4	2.9	3.3	3.0	3.1	85	81	85	84	0.5	0.8	0.5	0.6	8.7	8.1	7.0	7.9
III	—	—	—	—	5.2	−2.1	15.2	30	−11.0	1	−0.3	3.9	1.0	1.4	5.5	6.1	5.9	5.8	87	75	87	83	0.8	2.4	0.9	1.4	6.9	6.3	5.9	6.4
IV	—	—	—	—	10.5	1.8	14.0	19, 26	−3.1	6	4.3	9.0	5.1	5.9	7.2	7.6	7.6	7.5	86	66	85	79	1.3	4.2	1.4	2.3	8.0	8.3	5.4	7.2
V	—	—	—	—	14.6	5.7	25.5	19	−3.6	4	8.5	12.7	9.5	10.0	10.0	10.3	10.6	10.3	88	69	87	81	1.4	5.0	1.6	2.7	7.0	8.3	6.8	7.4
VI	—	—	—	—	20.2	10.9	29.2	26	5.5	3	14.7	18.7	14.4	15.6	14.3	14.2	14.8	14.4	84	67	90	80	2.8	8.0	1.9	4.2	5.4	6.9	6.2	6.2
VII	—	—	—	—	20.8	11.5	25.7	16	5.8	10	15.0	19.2	15.1	16.1	15.0	15.5	15.3	15.3	87	71	89	82	2.4	7.3	2.2	4.0	5.1	6.6	6.2	6.0
VIII	—	—	—	—	18.9	10.7	27.7	8	6.6	31	13.1	17.5	13.3	14.3	13.6	13.7	13.7	13.7	90	70	90	83	1.9	7.1	2.1	3.7	6.2	6.6	5.3	6.0
IX	—	—	—	—	19.0	9.7	24.8	2	3.6	22	12.5	18.1	13.1	14.2	12.1	13.1	13.3	12.8	84	64	88	79	2.7	8.0	2.2	4.3	5.4	5.1	3.0	4.5
X	—	—	—	—	11.1	3.6	22.5	2	−5.1	22	5.1	10.2	6.3	7.0	8.1	8.8	8.6	8.5	88	69	88	82	1.0	4.1	1.3	2.1	6.8	6.2	4.2	5.7
XI	—	—	—	—	2.4	−2.7	13.0	2	−14.1	25	−1.0	1.0	−0.4	−0.2	5.3	5.5	5.4	5.4	89	81	88	86	0.7	1.5	0.9	1.0	8.4	7.9	7.1	7.8
XII	—	—	—	—	1.3	−2.5	6.5	10, 11	−10.9	15	−1.1	0.1	−0.7	−0.6	5.1	5.2	5.2	5.2	87	83	87	86	0.7	1.0	0.7	0.8	7.3	8.2	6.6	7.4
Rok	—	—	—	—	10.0	2.6	29.2	26.VI	−22.1	7. II	5.0	8.7	5.6	6.2	8.6	9.0	9.0	8.9	87	73	88	83	1.4	4.2	1.4	2.3	6.9	7.2	5.9	6.7

Sanok

φ = 49°34' λ = 22°12'

I	—	—	—	—	1.6	−5.5	5.9	29,30,31	−19.0	11, 12	−2.6	0.3	−1.6	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−3.5	−12.0	1.5	12	−24.8	7	−8.2	−4.9	−7.6	−7.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	6.6	−3.0	15.9	30	−17.5	1	−1.2	4.9	1.3	1.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	11.7	1.9	15.9	26	−3.0	6	3.8	9.7	5.8	6.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	15.7	5.7	26.9	19	−4.5	3, 4	8.4	13.8	10.1	10.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	21.6	10.6	30.5	26	4.5	3	13.8	19.6	14.9	15.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.9	11.6	28.9	16	5.9	7	14.6	20.2	15.7	16.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	20.2	10.0	29.1	8	5.1	31	12.1	18.6	13.3	14.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	20.7	8.7	26.7	2	3.5	22	11.0	19.5	12.7	14.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	12.5	1.8	24.5	2	−6.0	22	4.1	11.4	5.8	6.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	3.8	−3.1	14.3	2	−17.2	17, 18	−0.6	2.3	0.0	0.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	3.2	−1.9	8.5	11	−10.2	15	0.0	1.8	0.6	0.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	11.3	2.1	30.5	26.VI	−24.8	7. II	4.6	9.8	5.9	6.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Stańcowa

φ = 49°33' λ = 19°32'

I	—	—	—	—	−0.4	−5.2	3.6	31	−13.7	7	−3.5	−1.6	−3.3	−2.9	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.2	7.3	8.0
II	—	—	—	—	−5.4	−12.0	1.5	1	−21.4	6	−10.2	−6.7	−9.8	−9.1	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.3	7.2	7.1
III	—	—	—	—	3.0	−4.3	10.7	30	−12.8	11	−1.9	1.8	−1.5	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.5	6.6	6.8
IV	—	—	—	—	7.3	−0.2	14.0	7	−5.6	1, 2	2.0	6.3	1.7	2.9	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.3	7.0	7.4
V	—	—	—	—	11.6	3.3	21.5	19	−3.7	4	6.4	10.0	5.9	7.0	—	—	—	—	—	—	—	—	—	—	—	—	7.6	8.1	7.4	7.7
VI	—	—	—	—	17.6	8.1	28.2	26	1.9	3	11.9	16.1	10.9	12.4	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.9	6.2	6.3
VII	—	—	—	—	17.4	9.1	25.5	15	3.2	10	12.5	15.5	11.5	12.8	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.7	6.7	7.0
VIII	—	—	—	—	16.7	8.3	25.8	8	4.4	16	11.4	15.3	10.4	11.9	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.3	5.0	5.6
IX	—	—	—	—	17.2	7.8	23.6	2	2.9	22	11.2	15.3	10.5	11.9	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.8	4.6	5.4
X	—	—	—	—	11.8	1.7	21.7	2	−5.7	22	4.2	11.1	4.3	6.0	—	—	—	—	—	—	—	—	—	—	—	—	4.9	4.1	3.1	4.0
XI	—	—	—	—	1.5	−5.0	11.3	7	−13.7	24	−3.2	−0.1	−2.7	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.2	7.2	7.5
XII	—	—	—	—	−0.3	−5.5	4.7	20	−15.1	16	−2.9	−1.7	−3.0	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.5	7.9	8.3
Rok	—	—	—	—	8.2	0.5	28.2	26.VI	−21.4	6. II	3.2	6.8	2.9	4.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.9	6.4	6.8

Obidowa

φ = 49°33' λ = 19°58'

I	—	—	—	—	−1.0	−6.3	5.0	31	−14.0	8	−4.4	−2.5	−3.6	−3.5	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.1	7.5	8.1
II	—	—	—	—	−5.7	−11.5	−1.2	1	−20.5	6	−9.9	−7.3	−8.9	−8.8	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.4	8.1	8.1
III	—	—	—	—	2.9	−4.8	11.1	30	−17.1	1	−3.1	1.3	−1.0	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.1	6.9	7.4
IV	—	—	—	—	7.6	0.7	11.5	6	−5.7	1	1.9	6.1	3.3	3.7	—	—	—	—	—	—	—	—	—	—	—	—	9.2	8.1	6.5	7.9
V	—	—	—	—	11.9	4.3	23.3	19	−3.2	4	5.9	10.2	7.2	7.6	—	—	—	—	—	—	—	—	—	—	—	—	7.9	8.1	7.2	7.7
VI	—	—	—	—	17.8	9.1	27.3	26	4.0	3	11.5	16.3	12.6	13.2	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.9	7.3	6.7
VII	—	—	—	—	17.6	10.1	24.9	15	5.4	10	12.3	15.8	13.1	13.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.4	6.9	7.5
VIII	—	—	—	—	16.6	9.0	26.8	8	5.1	2	10.5	15.1	12.1	12.4	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.4	5.9	6.5
IX	—	—	—	—	17.5	7.5	24.5	3	2.6	30	10.2	15.7	11.5	12.2	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.0	4.6	5.6
X	—	—	—	—	10.9	1.9	21.3	2	−6.2	22	3.3	9.8	5.5	6.0	—	—	—	—	—	—	—	—	—	—	—	—	4.5	4.7	3.5	4.2
XI	—	—	—	—	1.3	−5.1	10.6	9	−13.6	24	−3.2	−0.5	−2.2	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.3	6.8	7.4	7.5
XII	—	—	—	—	−0.3	−5.2	6.9	20	−13.1	15	−2.9	−1.8	−2.7	−2.5	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.5	7.0	8.0
Rok	—	—	—	—	8.1	0.8	27.3	26.VI	−20.5	6. II	2.7	6.5	3.9	4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.3	6.6	7.1

Iwonicz - Zdrój

$H_s = 410$ m $h_w = 16,2$ m **1965**

MIESIĄC	ROZKŁAD WIATRU $n_0 V_{n0}$ N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	◕	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	1.5	2.7	1	2.0	1	2.0	1.5	9.3	35	6.7	10.5	3.7	1.5	1.7	9	1.8	32	3.4	48	11.1	31	2	14	29	·	3	1	2	19	14	8	1	6	31	·
II	6.5	1.4	1.5	1.3	·	·	·	·	18.5	5.8	8.5	2.5	7	2.8	17	1.9	25	2.4	66	9.6	16	12	27	28	·	5	·	2	16	17	13	·	4	28	·
III	4	1.0	5	1.0	0.5	1.0	·	·	27.5	5.2	11	1.7	1	2.0	7	2.6	37	2.1	46	9.1	27	3	5	18	·	4	·	5	12	14	12	·	10	17	·
IV	5.5	2.5	7.5	2.5	7.5	3.0	1	1.5	17.5	1.9	10	1.4	3.5	1.7	7.5	2.0	30	1.4	59	11.6	22	-	·	6	·	2	·	1	11	20	12	2	4	·	2
V	10	1.4	2.5	1.4	3	1.3	0.5	3.0	15.5	3.5	7	2.1	4.5	1.0	10	1.2	40	1.2	67	8.2	9, 27	·	·	2	1	1	1	1	15	21	13	·	2	·	4
VI	7.5	1.2	3	1.0	1.5	1.0	2.5	2.2	16.5	2.0	3	1.7	5	1.4	15	2.0	36	1.2	172	33.1	10	·	·	·	5	·	·	3	11	19	17	5	7	·	5
VII	3.5	1.1	1	1.5	4	1.4	·	·	22.5	3.1	10	1.4	2.5	1.0	5.5	1.3	44	1.1	148	23.7	2	·	·	·	6	1	·	3	6	20	18	7	3	·	5
VIII	9	1.0	·	·	·	·	·	·	19.5	3.0	6	1.7	6	1.2	11.5	1.4	41	1.1	208	43.5	26	·	·	·	2	·	·	5	13	14	12	6	8	·	3
IX	4	1.0	·	·	·	·	1	2.5	37	3.6	[illegible]	2.3	2.0	1.8	3.5	1.1	31	1.5	61	23.8	11	·	·	·	·	·	·	9	5	7	5	2	4	·	·
X	6.5	1.1	2.5	1.0	1.5	1.0	·	·	15	3.5	11.5	3.2	[illegible]	1.1	6.5	1.5	47	1.2	19	7.8	4	·	·	5	·	·	·	7	12	7	5	·	10	·	·
XI	7	1.2	3.5	2.7	0.5	1.0	·	·	27.5	6.5	13.5	2.0	2.5	1.2	5.5	1.7	30	2.7	72	24.3	11	2	11	19	·	6	1	1	18	16	12	1	4	11	·
XII	0.5	5.0	·	·	·	·	·	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	11	1.8	21	3.6	41	9.1	18	1	3	24	·	9	3	3	16	13	10	·	4	23	·
Rok	65.5	1.7	27.5	1.2	19.5	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	1.7	414	1.9	1009	43.5	26.VIII	20	65	151	14	37	6	42	154	182	137	24	66	110	19

Sanok

$H_s = 314$ m $h_w = 16$ m

I	1	4.0	·	·	6	4.0	8	5.2	[illegible]	3.1	1	3.0	12	4.0	6	11.2	33	4.4	53	16.7	31	15	5	26	·	11	4	—	—	18	10	1	2	31	—
II	5	5.4	2	3.0	4	4.0	4	4.5	9	9.3	·	·	31	6.4	8	3.8	21	4.5	40	7.2	16	14	24	28	·	8	·	—	—	17	12	·	1	28	—
III	1	4.0	4	3.9	6	2.8	3	14.3	18	7.4	1	5.0	8	5.4	5	7.0	47	3.2	39	9.0	3	4	4	19	·	7	2	—	—	13	11	·	·	16	—
IV	2	2.5	11	5.1	5	8.6	3	2.7	7	6.0	1	3.0	7	4.3	4	6.2	50	2.4	41	8.2	30	·	·	5	·	5	·	—	—	15	11	·	2	1	—
V	4	2.6	4	3.0	3	2.7	5	2.9	7	10.4	·	·	11.5	4.7	9.5	3.9	49	2.3	44	7.0	9	·	·	2	1	4	1	—	—	14	12	·	2	·	—
VI	·	·	·	·	2	5.0	4	3.3	7	6.7	1	10.0	18.5	4.8	6.5	4.2	51	2.2	129	24.0	10	·	·	·	5	4	·	—	—	15	12	6	2	·	—
VII	·	·	3	3.0	1	3.0	17	3.0	12	9.0	2	4.5	5	5.0	5	3.0	48	2.3	176	30.8	21	·	·	·	6	2	2	—	—	16	16	9	1	·	—
VIII	·	·	3	3.3	1	3.0	6	2.0	10	4.0	·	·	11	5.4	8	4.4	54	1.9	172	37.5	25	·	·	·	5	2	·	—	—	13	11	6	2	·	—
IX	·	·	·	·	2	4.4	18	3.0	13	4.8	·	·	5	5.8	2	3.0	52	1.6	51	36.0	11	·	·	·	2	·	·	—	—	6	5	1	3	·	—
X	1	3.0	2	2.5	2	4.0	3	3.0	10	4.5	·	·	9	3.7	4	3.5	62	1.5	15	8.6	4	·	·	12	·	1	·	—	—	6	4	·	5	·	—
XI	1	3.0	3	3.7	·	·	4	5.8	22	5.8	·	·	16	4.6	3	3.3	41	2.5	40?	15.2	11	3	7	19	·	6	2	—	—	12	9	2	1	11	—
XII	·	·	1	3.0	4	3.6	13	3.5	23	7.6	·	·	7	4.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	4	25	·	2	1	—	—	14	9	·	1	9	—
Rok	15	2.0	33	2.5	36	3.7	65	4.6	164	6.9	6	2.1	141	4.7	65	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	9	52	12	—	—	157	122	25	22	96	—

Stańkowa

$H_s = 850$ m $h_w = 18,5$ m

I	7	1.7	2	1.0	12	1.6	·	·	·	·	40	1.0	23	2.0	7	2.7	2	1.8	88	16.2	10	2	18	29	·	·	·	1	21	18	15	2	1	31	·
II	8	2.9	12	2.6	15	1.0	2	1.0	2	1.0	19	3.0	10	1.7	17	3.2	·	2.4	106	14.2	8	21	27	28	·	1	1	1	12	24	18	4	2	28	·
III	·	·	10	1.3	2	1.0	1	1.0	·	·	31	2.6	32	1.4	8	1.5	1	1.8	43	8.4	24	4	7	23	·	·	·	6	15	19	12	·	4	31	·
IV	12	2.8	18	1.4	7	1.1	8	1.0	·	·	19	2.1	17	1.6	8	1.2	1	1.7	98	18.8	13	·	·	11	·	·	·	2	14	22	16	3	5	7?	1
V	16	1.5	9	1.7	5	1.6	·	·	2	1.5	40	2.2	6	1.0	14	1.9	1	1.6	127	27.4	6	·	·	5	·	1	1	2	18	25	18	4	·	·	3
VI	22	1.4	3	1.5	1	2.0	3	1.0	·	·	28	2.5	16	1.3	15	2.1	2	1.8	280	70.5	10	·	·	·	2	1	·	2	9	18	15	7	·	·	6
VII	3	2.3	4	1.0	5	1.0	4	1.0	4	1.0	36	1.9	29	1.3	9	1.1	·	1.5	124	16.1	18	·	·	·	1	1	·	1	12	26	17	4	1	·	5
VIII	17	2.2	3	1.0	2	2.5	2	1.0	11	1.7	31	1.5	3	1.0	24	1.4	·	1.6	185	68.4	1	·	·	·	2	1	1	4	8	15	12	6	·	·	3
IX	2	1.0	·	·	·	·	3	1.3	1	4.0	61	2.1	13	1.7	10	1.4	·	1.9	84	21.8	19	·	·	·	·	·	·	7	5	9	7	4	·	·	1
X	10	1.5	17	1.1	9	1.3	2	1.5	·	·	25	1.5	15	2.5	7	1.2	5	1.1	18	8.3	31	·	·	13	·	·	·	11	4	8	4	·	4	·	·
XI	8	1.0	16	1.4	·	·	·	·	3	1.0	35	2.4	12	1.8	16	1.4	·	1.9	53	15.2	11	7	11	26	·	·	·	4	19	18	12	1	3	20	·
XII	11	2.4	·	·	1	1.0	·	·	·	·	42	2.0	20	1.4	19	1.6	·	1.9	[illegible]	21.9	13	4	13	28	·	·	·	·	20	26	16	3	1	31	·
Rok	124	1.7	100	1.1	58	1.2	25	0.7	23	0.8	408	2.2	196	1.6	149	1.7	12	1.8	[illegible]	70.5	10.VI	38	81	163	5	5	3	41	157	228	162	38	21	148?	19

Obidowa

$H_s = 800$ m $h_w = 20,5$ m

I	19	2.8	·	·	·	·	2	2.5	35	3.0	14	5.1	4	2.8	5	2.6	14	2.8	43	10.4	31	5	21	31	·	3	1	1	20	15	11	1	9	31	—
II	25	3.2	·	·	·	·	·	·	7.5	4.1	11.5	10.5	6	3.3	6	3.3	28	3.2	58	7.6	4	17	28	28	·	3	3	·	19	21	18	·	1	28	—
III	23	2.7	3	2.0	·	·	4	2.5	35	3.1	8	9.0	1	2.0	2	3.0	17	2.0	30	5.6	24	3	7	25	·	3	3	5	19	17	9	·	13	27	—
IV	26	2.5	5	2.6	5	3.4	3	3.0	22	2.7	6	3.4	1	2.0	5	3.0	17	2.2	29	5.1	26	·	1	8	·	·	·	1	19	17	8	·	11	1	—
V	32.5	2.6	2	2.0	5	2.4	4	2.2	24	3.0	7	2.6	1	2.0	2.5	2.0	15	2.2	105	20.5	6	·	·	5	·	·	·	3	17	23	17	4	9	1	—
VI	23.5	2.4	1.5	2.3	6	2.0	4.5	2.8	21	4.5	7.5	2.7	2	2.0	7	2.7	17	2.5	218	62.0	10	·	·	·	2	1	1	2	11	16	15	9	7	·	—
VII	11	2.3	1	2.0	6	2.0	4.5	2.0	27.5	3.5	18.5	3.4	4.5	2.7	2	2.0	19	2.4	108	20.4	21	·	·	·	·	1	1	2	14	25	17	2	7	·	—
VIII	25.5	2.6	·	·	7	2.1	7	2.1	19	2.7	6.5	2.9	4.5	2.0	6.5	2.0	17	2.1	144	49.4	1	·	·	·	2	·	·	5	14	15	10	5	8	·	—
IX	12	2.2	·	·	4	2.2	9.5	2.6	39.5	3.0	8	3.1	2	3.0	5	2.9	10	2.5	67	23.7	11	·	·	·	·	·	·	4	8	9	6	2	7	·	—
X	24	2.6	2	2.5	5	2.2	5.5	2.0	25	2.7	11.5	5.8	1	11.5	3	4.0	16	2.7	15	4.5	4	·	·	11	·	1	1	14	8	9	5	·	7	·	—
XI	22	2.5	1	2.0	2	2.0	3	2.3	26	3.6	12	7.2	2	4.0	2	2.0	29	2.8	25	7.4	11	8	12	27	·	4	3	2	18	16	7	·	7	16	—
XII	13	3.0	·	·	·	·	2	2.0	47.5	5.2	18.5	4.7	1	2.0	1	3.0	10	4.1	21	5.4	3	3	19	23	·	5	3	2	19	18	7	·	5	29	—
Rok	256.5	2.6	15.5	1.3	40	1.5	49	2.2	329	3.4	129	5.0	30	3.3	47	2.8	199	2.7	874	62.0	10.VI	35	88	153	4	21	16	41	186	201	130	23	91	133	—

Turbacz — φ = 49°33' — λ = 20°07' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−1.9	−7.2	2.9	29, 30	−14.2	7, 8	−5.4	−2.9	−4.8	−4.5	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.4	6.8	7.4
II	—	—	—	—	−7.9	−14.0	0.0	1	−20.9	6	−13.2	−9.4	−11.9	−11.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.1	7.7	7.7
III	—	—	—	—	1.5	−6.1	8.0	19, 30	−15.0	1	−3.8	−0.7	−3.3	−2.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.6	5.7	5.9
IV	—	—	—	—	4.0	−2.0	10.1	7	−9.2	1	−0.2	2.3	−0.1	0.5	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.7	6.6	6.9
V	—	—	—	—	8.6	1.3	20.6	19	−7.4	3	3.2	6.5	3.6	4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.6	6.6	6.8
VI	—	—	—	—	15.1	6.4	24.6	27	1.5	3	9.6	13.2	9.2	10.3	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.1	6.1	5.8
VII	—	—	—	—	14.8	7.8	22.6	15, 16	2.4	6	10.3	12.8	9.9	10.7	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.5	6.6	6.9
VIII	—	—	—	—	14.1	6.7	25.1	8	1.5	2	8.8	12.2	8.9	9.7	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.5	6.1	6.3
IX	—	—	—	—	14.4	6.3	20.3	3	3.0	19,20,30	8.6	12.3	8.5	9.5	—	—	—	—	—	—	—	—	—	—	—	—	5.2	5.2	4.0	4.8
X	—	—	—	—	9.1	1.1	19.7	2	−6.0	21	3.0	7.3	3.3	4.2	—	—	—	—	—	—	—	—	—	—	—	—	4.2	4.1	3.5	3.9
XI	—	—	—	—	−0.4	−6.9	9.8	8	−16.6	24	−4.4	−2.5	−4.3	−3.9	—	—	—	—	—	—	—	—	—	—	—	—	6.9	5.9	6.1	6.3
XII	—	—	—	—	−2.6	−7.3	4.7	21	−15.0	15	−5.1	−4.5	−5.1	−5.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.6	7.2	7.3
Rok	—	—	—	—	5.7	−1.2	25.1	8.VIII	−20.9	6.II	1.0	3.9	1.2	1.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.4	6.1	6.3

Łącko — φ = 49°33' — λ = 20°26'

I	—	—	—	—	2.5	−5.8	9.4	30	−17.6	8	−2.7	1.3	−2.1	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.5	7.2	7.2
II	—	—	—	—	−2.1	−10.8	4.4	13	−25.2	7	−7.9	−3.5	−7.1	−6.4	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.5	7.2	7.6
III	—	—	—	—	6.9	−3.2	15.9	30	−17.4	1	−1.1	5.6	1.2	1.7	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.1	6.3	6.5
IV	—	—	—	—	11.4	2.2	18.0	7	−2.4	6	3.9	10.0	6.3	6.6	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.6	6.5	7.2
V	—	—	—	—	15.5	5.7	27.1	19	−3.9	4	8.4	14.0	9.9	10.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.0	8.0	7.7
VI	—	—	—	—	21.4	9.7	30.3	26	3.9	3	13.8	19.8	14.6	15.7	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.2	6.3	5.7
VII	—	—	—	—	21.6	10.0	27.2	14, 15	4.3	7	14.2	19.7	14.7	15.8	—	—	—	—	—	—	—	—	—	—	—	—	5.4	7.3	5.6	6.1
VIII	—	—	—	—	20.5	9.4	30.3	7, 8	5.2	31	12.1	19.0	13.4	14.5	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.9	5.4	6.1
IX	—	—	—	—	20.8	8.3	26.7	3	3.6	30	10.9	19.5	12.2	13.7	—	—	—	—	—	—	—	—	—	—	—	—	4.9	4.8	3.9	4.5
X	—	—	—	—	13.6	0.9	23.2	2	−5.8	22	3.0	12.3	4.9	6.3	—	—	—	—	—	—	—	—	—	—	—	—	5.3	4.1	3.9	4.4
XI	—	—	—	—	4.3	−3.8	14.1	2	−17.5	18	−1.3	2.8	−0.8	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.1	5.6	6.8
XII	—	—	—	—	4.1	−3.4	11.0	20	−16.3	15	−0.8	2.5	0.6	0.7	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.2	6.1	6.8
Rok	—	—	—	—	11.7	1.6	30.3	26.VI.7.9.VIII	−25.2	7, 11	4.4	10.2	5.6	6.4	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.6	6.0	6.4

Stary Sącz — φ = 49°33' — λ = 20°39'

I	—	—	—	—	1.2	−5.2	6.5	30	−19.1	8	−2.1	0.4	−1.8	−1.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.1	6.8	7.2
II	—	—	—	—	−2.4	−11.1	4.7	14	−26.8	7	−7.9	−3.3	−6.6	−6.1	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.4	7.5	7.7
III	—	—	—	—	6.3	−2.1	15.9	19	−14.5	11	−0.2	5.5	1.4	2.0	—	—	—	—	—	—	—	—	—	—	—	—	6.7	5.6	6.1	6.1
IV	—	—	—	—	11.3	2.4	16.9	7	−2.1	6	5.0	10.3	5.9	6.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.6	5.2	6.3
V	—	—	—	—	15.4	5.8	26.2	19	−4.1	3	9.2	14.4	9.2	10.5	—	—	—	—	—	—	—	—	—	—	—	—	6.3	7.5	6.2	6.7
VI	—	—	—	—	21.7	10.3	31.3	26	2.6	3	15.0	20.9	14.0	16.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.7	11.0	28.0	15, 24	4.7	10	15.3	20.5	14.1	16.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	6.2	4.3	5.2
VIII	—	—	—	—	20.3	10.6	30.5	8	4.5	31	13.6	19.2	13.7	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.1	4.7	5.4
IX	—	—	—	—	20.8	10.0	26.6	11	3.4	22	13.6	19.5	13.7	15.1	—	—	—	—	—	—	—	—	—	—	—	—	4.5	4.6	3.6	4.2
X	—	—	—	—	13.0	1.9	22.9	2	−5.7	22	4.9	12.2	5.9	7.2	—	—	—	—	—	—	—	—	—	—	—	—	5.1	3.9	3.3	4.1
XI	—	—	—	—	3.9	−3.0	14.8	2	−16.9	17	−0.6	2.5	0.2	0.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	3.1	−2.4	8.8	6	−14.5	15	−0.2	2.1	0.1	0.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	11.4	2.4	31.3	26.VI	−26.8	7, 11	5.5	10.4	5.8	6.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Rymanów-Zdrój — φ = 49°33' — λ = 21°51'

I	—	—	—	—	0.3	−5.6	4.5	31	−15.5	11	−2.5	−0.8	−2.4	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.3	7.7	7.7
II	—	—	—	—	−4.3	−11.2	0.6	1	−25.7	7	−8.7	−5.9	−8.1	−7.7	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.4	7.3	7.7
III	—	—	—	—	5.1	−4.1	15.2	30	−17.6	1	−0.8	3.6	0.2	0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.4	5.8	5.8	6.0
IV	—	—	—	—	10.7	0.8	14.4	26	−4.6	6	4.0	9.1	4.4	5.5	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.0	5.4	6.6
V	—	—	—	—	14.4	4.4	25.5	19	−5.4	4	8.1	12.8	8.6	9.5	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.9	5.3	6.1
VI	—	—	—	—	20.1	9.2	29.5	26	2.3	3	14.3	18.9	13.5	15.0	—	—	—	—	—	—	—	—	—	—	—	—	5.1	5.7	6.1	5.6
VII	—	—	—	—	20.8	9.9	27.1	16	3.8	10	14.6	19.1	14.3	15.6	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.2	6.4	5.7
VIII	—	—	—	—	18.9	9.4	27.6	8	4.5	31	12.5	17.4	12.0	13.5	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.9	4.9	5.5
IX	—	—	—	—	19.5	8.1	25.6	2	1.1	22	11.8	18.2	12.0	13.5	—	—	—	—	—	—	—	—	—	—	—	—	4.4	4.5	3.2	4.0
X	—	—	—	—	11.9	1.8	23.1	2	−6.6	22	4.6	10.3	5.4	6.4	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.2	3.5	5.1
XI	—	—	—	—	2.7	−3.4	13.1	2	−13.6	17	−1.1	1.2	−0.4	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.6	6.8	7.0	7.1
XII	—	—	—	—	1.5	−3.3	6.5	10	−12.6	15	−1.1	0.3	−0.6	−0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.3	7.1	7.5
Rok	—	—	—	—	10.1	1.3	29.5	26.VI	−25.7	7, 11	4.6	8.7	4.9	5.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.3	5.8	6.2

Turbacz — $H_s = 1308$ m — $h_w = 18{,}6$ m — 1965

MIESIĄC	ROZKŁAD WIATRU (%, V=0) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0,1	≥1,0	≥10,0	≡	⊠	K (%)
I	11.5	5.1	7	6.3	3	2.0	5.5	5.2	16.5	5.5	14.5	4.8	11	5.3	12	5.6	12	4.5	104	21.8	10	4	21	31	·	2	·	2	16	16	14	4	17	31	·
II	16.5	4.5	5	3.6	1.5	3.7	0.5	1.0	3	6.2	10	4.4	12.5	3.8	29	5.9	6	4.5	156	18.8	17	25	27	28	·	8	·	2	17	20	20	5	20	28	·
III	12.5	4.7	1.5	3.7	1.5	5.3	6.5	5.1	12.5	5.0	17.5	6.0	9	3.4	10	5.2	22	3.8	75	15.6	31	9	8	29	·	5	·	5	10	17	13	1	17	31	·
IV	19	3.8	12	4.7	0.5	2.0	13.5	5.4	14.5	3.3	9	3.6	4.5	2.7	11	5.0	6	3.9	49	18.0	22	·	3	25	·	3	·	3	12	13	12	1	18	28	1
V	22.5	4.9	2	2.5	2.5	4.2	6.5	5.2	10.5	4.7	13	5.1	6.5	4.2	20.5	3.8	9	4.1	132	16.4	5	·	·	9	·	1	1	2	12	24	20	5	21	4	1
VI	18.5	4.9	1.5	3.0	3.5	4.1	13.5	4.6	8.5	6.1	10	4.3	7.5	4.1	20	4.6	7	4.3	294	66.8	10	·	·	·	·	8	6	2	7	16	14	9	12	·	6
VII	8	3.2	0.5	1.0	2	2.5	8	4.5	7	4.0	17	4.1	19	4.2	18.5	3.5	13	3.3	128	19.3	8	·	·	·	·	·	·	·	10	26	20	4	14	·	6
VIII	22.5	3.6	8.5	3.8	6	1.5	9	3.1	8.5	5.0	7.5	4.5	10.5	4.0	10.5	3.3	10	3.3	164	65.9	1	·	·	·	1	2	2	2	13	14	11	4	12	·	·
IX	5.5	3.2	1.5	3.0	2	1.0	19.5	3.4	21.5	6.3	15	4.5	9.5	4.2	7.5	3.1	8	4.0	89	27.1	11	·	·	·	·	5	·	7	8	11	6	4	11	·	·
X	18	4.3	6.5	2.1	6	2.2	5	2.4	2.5	3.6	17.5	6.1	12.5	5.0	15	5.1	10	4.0	28	7.3	31	·	·	14	·	2	1	12	5	10	7	·	14	·	·
XI	18.5	2.7	3.5	5.9	3.5	4.3	3.5	2.3	11	6.0	17	5.3	7	5.6	15	3.3	11	3.8	47	13.1	11	8	14	27	·	3	·	4	10	18	11	1	16	20	·
XII	10	4.0	·	·	·	·	2	3.0	14	6.7	34	6.3	15	2.8	9	4.1	9	4.6	80	11.3	18	4	24	30	·	6	·	1	15	22	15	2	15	31	·
Rok	183	4.1	49.5	3.2	32	2.7	93	3.8	130	5.2	182	4.9	124.5	4.1	178	4.4	123	4.0	1346	66.8	10. VI	50	97	193	1	45	10	42	135	207	163	40	187	173	14

Łącko — $H_s = 360$ m — $h_w = 17{,}6$ m

I	1	1.0	1	1.0	5.5	1.0	1.5	1.0	8.5	2.2	16	3.2	28.5	2.8	5	1.4	26	1.8	50	12.8	31	8	5	27	·	1	·	3	15	12	9	1	4	31	—
II	6.5	1.3	6	1.4	7.5	1.5	·	·	5.5	3.6	9	3.9	37	2.6	5.5	1.8	7	2.2	29	4.6	18	14	21	27	·	·	·	1	15	17	11	·	2	28	—
III	6	1.2	1.5	1.7	11	1.2	3	1.3	10.5	1.8	19.5	2.5	23.5	1.8	1	1.5	17	1.5	34	6.6	24	4	3	20	·	1	·	5	10	17	11	·	4	16	—
IV	7.5	1.9	10	2.0	19	1.6	7	1.4	7	1.9	7	1.7	21	2.1	3.5	2.3	8	1.7	37	12.4	22	·	·	6	·	·	·	1	14	14	8	1	3	·	—
V	15	1.8	9.5	1.4	13	1.4	1.5	2.0	6	1.8	7.5	2.3	26.5	1.6	7	1.7	7	1.5	118	28.7	29	·	·	3	1	·	·	1	17	21	16	3	3	·	—
VI	6.5	1.3	6	1.2	9	1.8	3	2.2	9	2.2	6	2.0	29.5	1.9	10	1.8	11	1.6	202	56.2	10	·	·	·	6	·	·	2	7	15	15	8	2	·	—
VII	1	1.0	·	·	7	1.4	4	2.5	9.5	1.2	14	1.5	29.5	1.5	5	1.2	23	1.1	119	17.3	8	·	·	·	7	·	·	2	8	17	17	5	3	·	—
VIII	3	1.0	2.5	1.4	7.5	1.3	5.5	2.0	11	1.5	11.5	1.5	34.5	1.5	8.5	1.4	9	1.3	103	44.8	1	·	·	·	6	·	·	6	11	13	11	2	1	·	—
IX	4	1.8	2	1.0	9.5	1.3	6	2.7	14	2.4	13	2.0	20.5	1.4	5	1.1	16	1.5	60	24.2	11	·	·	·	3	·	·	8	6	9	7	2	1	·	—
X	4.5	1.2	3	1.2	7	1.3	3	1.2	15.5	1.2	7.5	1.5	26	1.4	6.5	1.4	21	1.0	10	2.7	4	·	·	18	·	·	·	10	6	5	4	·	9	·	—
XI	6.5	1.7	7	1.2	6.5	1.5	3.5	1.9	7	3.0	17	2.2	17.5	1.5	10	1.6	15	1.5	35	20.0	11	5	9	25	·	·	·	2	15	15	5	1	4	10	—
XII	5	2.0	0.5	2.0	4	1.4	3	1.2	10	3.0	23	2.0	34.5	2.0	3	1.3	10	1.8	22	5.1	13	3	4	25	·	·	·	3	13	14	7	·	1	8	—
Rok	66.5	1.4	49	1.3	106.5	1.4	41	1.6	113.5	2.2	151	2.2	328.5	1.8	69	1.5	170	1.5	819	56.2	10. VI	34	42	151	23	2	·	44	137	169	121	23	37	93	—

Stary Sącz — $H_s = 320$ m — $h_w = 22$ m

I	7	2.1	·	·	·	·	15.5	10.7	35	9.4	1	2.0	3.5	5.0	2	4.2	29	5.8	53	15.9	31	6	8	27	·	12	8	2	15	11	11	2	—	31	·
II	13	3.2	·	·	·	·	3	9.3	10.5	11.7	3.5	5.4	14.5	4.0	9.5	3.9	30	3.6	34	8.1	18	13	22	28	·	6	2	1	15	17	8	·	—	28	·
III	5.5	1.8	·	·	·	·	5	9.9	22	10.0	2.5	6.4	3	3.0	3	4.0	52	3.4	46	7.5	17	4	5	17	·	8	3	6	12	14	12	·	—	12	·
IV	12	3.5	4.5	5.3	·	·	6	2.6	14	5.2	2	4.0	6.5	3.7	1	5.5	44	2.1	28	9.8	22	·	·	6	·	1	·	3	11	8	6	·	—	·	3
V	11	4.1	1	3.0	0.5	3.0	·	·	7	8.6	1	5.0	5	3.0	3.5	4.0	64	1.5	93	13.0	29	·	·	3	1	3	1	3	13	22	19	3	—	·	6
VI	7	2.4	·	·	·	·	4	5.0	17	6.6	2	3.8	7	2.4	6	2.8	47	2.1	166	45.5	10	·	·	·	7	3	1	—	—	15	14	6	—	·	5
VII	4.5	2.6	1	3.0	1.5	4.0	5	6.1	15	5.4	1	2.5	8	3.2	7	2.6	50	1.9	107	16.8	8	·	·	·	6	1	1	3	4	20	18	2	—	·	7
VIII	8.5	2.3	5	1.6	0.5	1.0	9	6.1	18	5.1	2	1.5	2	2.8	15	4.0	33	2.6	125	41.5	25	·	·	·	7	4	·	6	9	12	11	5	—	·	3
IX	1	3.0	1.5	2.7	0.5	4.0	17	4.7	38.5	4.2	1	2.5	2.5	3.6	3	3.7	25	3.1	52	18.0	11	·	·	·	3	1	·	9	5	6	5	3	—	·	·
X	14	2.0	1	2.5	2	2.0	9.5	4.2	16.5	4.6	0.5	4.0	2	5.0	9.5	3.2	38	2.1	7	1.9	11	·	·	12	·	2	·	11	5	8	3	·	—	·	·
XI	10	2.0	·	·	·	·	7.5	6.3	25	8.3	5	4.4	5	1.8	3.5	1.6	34	3.5	40	22.8	11	5	9	17	·	6	3	—	—	12	6	1	—	9	·
XII	3.5	2.1	·	·	·	·	10	5.4	52	7.4	0.5	2.0	1.5	2.0	3.5	3.6	22	4.9	17	6.0	13	3	6	23	·	11	8	—	—	11	4	·	—	13	·
Rok	97	2.6	14	1.5	5	1.2	91.5	5.9	270.5	7.2	22	3.6	60.5	3.3	66.5	3.6	468	3.0	773	45.5	10. VI	31	50	133	24	58	27	—	—	156	117	22	—	93	24

Rymanów-Zdrój — $H_s = 360$ m — $h_w = 18$ m

I	8.5	1.4	1.5	1.7	3	1.0	1.5	2.3	26.5	4.5	23	5.0	0.5	1.0	1.5	1.0	27	2.8	46	14.3	31	5	15	30	·	2	1	1	18	18	9	1	—	31	·
II	21	1.5	2	1.0	·	·	·	·	15	3.6	18	3.6	·	·	1	1.0	27	1.8	36	4.2	3	15	27	28	·	1	·	2	16	17	13	·	—	28	·
III	12.5	1.6	7	1.9	4	1.5	1	2.0	25	4.3	21	4.6	·	·	0.5	1.0	22	2.6	43	6.2	27	5	5	21	·	3	3	7	12	15	11	·	—	18	·
IV	9.5	2.1	18	3.1	0.5	1.0	2	1.0	15.5	2.1	11.5	2.0	·	·	·	·	33	1.5	54	13.0	20	·	·	10	·	·	·	2	11	16	12	2	—	1	2
V	17.5	1.9	13	2.0	·	·	2	1.0	14.5	3.0	10.5	3.6	1	1.0	1.5	1.0	33	1.6	70	9.6	9	·	·	6	1	·	·	4	10	21	16	·	—	·	5
VI	21	1.7	10	2.0	2	1.5	2	1.0	13.5	3.1	7.5	3.3	·	·	·	·	34	1.4	199	34.0	10	·	·	·	4	·	·	3	8	17	16	8	—	·	5
VII	5.5	1.4	3	2.0	0.5	1.0	7.5	1.2	21.5	2.7	15.5	2.4	·	·	0.5	1.0	39	1.3	162	19.3	4	·	·	·	6	1	·	3	4	18	17	8	—	·	9
VIII	16.5	1.6	10.5	1.2	3	1.0	0.5	1.0	11.5	2.7	14	2.4	·	·	·	·	37	1.2	208	46.7	26	·	·	·	2	·	·	7	11	14	13	7	—	·	3
IX	8	1.5	5.5	1.6	·	·	1	1.0	32.5	2.8	25.5	2.8	·	·	2.5	1.2	15	2.1	64	28.9	11	·	·	·	1	·	·	10	2	7	5	2	—	·	1
X	14	1.8	10	2.1	·	·	2	1.0	18.5	2.4	14.5	2.5	·	·	·	·	34	1.4	22	7.6	4	·	·	11	·	·	·	9	9	8	6	·	—	·	·
XI	13.5	2.1	7.5	1.3	·	·	1	1.0	17.5	5.8	20.5	5.4	1	1.0	2	1.0	27	2.8	91	34.7	11	3	10	22	·	4	3	3	16	16	12	1	—	12	·
XII	5	1.6	2	1.0	·	·	1	1.0	32	4.5	32	4.6	1	1.0	·	·	20	3.3	30	7.0	18	2	7	27	·	1	1	2	18	14	11	·	—	12	·
Rok	152.5	1.7	90	1.7	13	0.6	21.5	1.1	243.5	3.5	213.5	3.5	3.5	0.3	9.5	0.6	348	2.0	1025	46.7	26. VIII	30	64	155	14	12	8	53	135	181	141	29	—	102	25

Sieniawa — φ = 49°32' — λ = 19°55' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.8	-7.0	7.5	30	-17.2	8	-4.0	-0.3	-3.1	-2.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.4	7.1	7.3
II	—	—	—	—	-4.1	-12.9	0.4	14	-25.6	7	-9.7	-5.2	-9.0	-8.2	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.4	8.0	7.9
III	—	—	—	—	4.8	-5.5	13.5	30	-18.8	11	-3.0	3.4	-1.4	-0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.3	6.5	6.7
IV	—	—	—	—	9.7	0.5	16.5	7	-4.8	2	3.1	8.3	3.5	4.6	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.3	6.4	7.3
V	—	—	—	—	13.6	3.8	24.1	19	-5.2	3, 4	7.3	12.2	7.5	8.6	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.2	6.9	7.0
VI	—	—	—	—	19.4	7.9	29.1	26	0.8	3	13.0	18.3	12.0	13.8	—	—	—	—	—	—	—	—	—	—	—	—	4.8	5.6	6.6	5.7
VII	—	—	—	—	19.4	9.0	27.2	15	2.6	6	13.6	18.0	12.5	14.2	—	—	—	—	—	—	—	—	—	—	—	—	6.4	6.8	6.2	6.5
VIII	—	—	—	—	18.2	7.8	28.4	8	2.1	31	11.0	16.9	11.0	12.5	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.1	5.3	5.7
IX	—	—	—	—	18.9	6.5	26.4	3	1.2	22	9.9	17.5	10.3	12.0	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.3	4.0	5.0
X	—	—	—	—	12.9	-0.1	22.9	2	-6.4	21	2.8	11.7	3.8	5.3	—	—	—	—	—	—	—	—	—	—	—	—	4.8	3.6	3.5	4.0
XI	—	—	—	—	2.9	-4.9	11.7	9	-15.4	24	-2.5	1.4	-2.0	-1.3	—	—	—	—	—	—	—	—	—	—	—	—	7.6	6.8	7.0	7.1
XII	—	—	—	—	1.6	-5.1	8.3	20	-17.3	15	-1.9	0.2	-1.4	-1.1	—	—	—	—	—	—	—	—	—	—	—	—	7.5	8.1	7.4	7.7
Rok	—	—	—	—	9.8	0.0	29.1	26.VI	-25.6	7. II	3.3	8.5	3.6	4.8	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.5	6.2	6.5

Zwardoń — φ = 49°30' — λ = 18°59'

I	—	—	—	—	0.0	-6.3	6.4	29	-17.2	8	-3.7	-1.3	-3.3	-2.9	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.5	8.0	8.3
II	—	—	—	—	-4.4	-12.4	0.4	1	-24.8	6	-9.6	-6.0	-8.8	-8.3	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.1	6.7	7.3
III	—	—	—	—	4.4	-4.9	13.4	30	-17.2	11	-2.6	2.7	-0.9	-0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.3	6.1	6.6
IV	—	—	—	—	9.0	0.5	17.1	7	-4.7	2	2.0	7.2	3.5	4.0	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.7	6.0	6.9
V	—	—	—	—	12.8	4.2	23.3	19	-4.1	3, 4	6.6	11.0	7.8	8.3	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.1	7.4	7.2
VI	—	—	—	—	19.2	8.2	29.8	26	0.4	3	12.0	16.8	12.5	13.4	—	—	—	—	—	—	—	—	—	—	—	—	4.9	6.4	6.9	6.1
VII	—	—	—	—	19.1	9.9	27.8	14	4.6	6, 10	13.0	16.5	13.1	13.9	—	—	—	—	—	—	—	—	—	—	—	—	6.4	7.7	6.6	6.9
VIII	—	—	—	—	18.3	8.1	27.3	8	3.0	31	10.4	16.6	11.5	12.5	—	—	—	—	—	—	—	—	—	—	—	—	4.6	6.6	4.5	5.2
IX	—	—	—	—	18.9	7.4	25.3	2, 10	1.7	22	9.8	16.1	11.2	12.1	—	—	—	—	—	—	—	—	—	—	—	—	4.3	5.0	3.8	4.4
X	—	—	—	—	12.1	0.5	23.1	2	-7.0	22	2.2	10.7	4.1	5.3	—	—	—	—	—	—	—	—	—	—	—	—	4.0	3.3	2.8	3.4
XI	—	—	—	—	2.8	-4.6	10.7	2	-16.8	17	-2.5	0.4	-2.0	-1.5	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.0	7.5	7.5
XII	—	—	—	—	0.8	-4.4	6.9	20	-14.1	15	-2.2	-0.7	-2.0	-1.7	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.3	7.3	8.0
Rok	—	—	—	—	9.4	0.5	29.8	26.VI	-24.8	6. II	3.0	7.8	3.9	4.6	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.7	6.1	6.5

Nowy Targ — φ = 49°29' — λ = 20°02'

I	—	—	—	—	-0.6	-9.6	4.9	29, 30	-24.2	8	-6.6	-2.1	-4.8	-4.6	3.7	4.5	4.2	4.1	92	85	92	90	0.3	0.8	0.3	0.5	7.7	7.1	6.6	7.1
II	—	—	—	—	-4.0	-14.0	2.0	14	-32.1	7	-10.8	-5.5	-9.1	-8.6	2.8	3.2	3.0	3.0	91	76	88	85	0.3	1.0	0.4	0.6	7.8	6.5	6.8	7.0
III	—	—	—	—	4.6	-6.5	13.9	30	-23.5	1	-4.6	2.9	-1.2	-1.0	4.4	5.6	5.2	5.1	91	74	89	85	0.4	2.2	0.7	1.1	7.1	5.9	6.0	6.3
IV	—	—	—	—	10.3	1.3	16.9	7	-3.4	2	2.7	8.9	4.6	5.2	6.8	7.9	7.3	7.3	90	71	86	82	0.7	3.2	1.2	1.9	7.8	7.7	7.0	7.5
V	—	—	—	—	14.2	4.9	25.4	19	-4.5	3	7.1	12.8	8.7	9.3	9.5	9.6	10.2	9.8	91	66	88	82	1.0	5.9	1.3	2.7	6.8	7.3	6.9	7.0
VI	—	—	—	—	20.7	8.8	30.8	26	4.2	16	12.3	18.7	13.5	14.5	12.5	12.7	13.7	13.0	86	60	88	78	2.0	9.5	2.0	4.5	5.0	6.2	6.5	5.9
VII	—	—	—	—	20.1	9.5	28.3	15	3.1	10	12.6	18.1	13.7	14.5	13.5	14.5	14.1	14.0	92	70	89	84	1.3	7.0	2.0	3.4	6.4	7.6	5.7	6.6
VIII	—	—	—	—	19.1	7.7	28.8	7	1.9	31	9.7	17.9	12.0	12.9	11.6	13.0	12.2	12.3	95	65	87	82	0.7	8.5	2.0	3.7	7.2	6.4	5.5	6.3
IX	—	—	—	—	19.6	6.4	26.8	3	0.6	22	9.0	17.9	10.9	12.2	10.8	12.7	11.5	11.7	93	63	88	81	1.1	8.2	1.7	3.7	7.7	4.7	4.3	5.6
X	—	—	—	—	12.7	-0.6	22.9	2	-6.2	22	0.6	11.2	4.0	5.0	6.6	8.7	7.9	7.7	97	63	92	84	0.2	5.1	0.7	2.0	5.3	3.1	2.9	3.8
XI	—	—	—	—	2.4	-5.1	11.9	2	-17.7	18	-3.2	1.0	-2.2	-1.6	4.7	5.2	5.0	5.0	92	77	90	86	0.5	1.8	0.6	1.0	6.9	7.0	7.2	7.0
XII	—	—	—	—	1.2	-6.4	6.9	10	-18.2	15	-3.8	-0.6	-2.3	-2.2	4.5	5.1	4.9	4.8	94	86	92	91	0.3	0.9	0.4	0.5	7.5	7.9	7.4	7.6
Rok	—	—	—	—	10.0	-0.3	30.8	26.VI	-32.1	7. II	2.1	8.4	4.0	4.6	7.6	8.6	8.3	8.2	92	71	89	84	0.7	4.6	1.1	2.1	6.9	6.4	6.1	6.5

Jabłonka — φ = 49°28' — λ = 19°43'

I	—	—	—	—	-0.3	-9.7	4.7	29	-27.0	8	-5.4	-1.8	-5.3	-4.4	3.9	4.7	4.2	4.3	91	86	92	90	0.4	0.8	0.3	0.5	8.0	8.4	7.6	8.0
II	—	—	—	—	-4.9	-16.4	0.3	1, 14	-32.7	7	-12.0	-6.7	-10.7	-10.0	2.6	3.0	2.6	2.7	88	78	87	84	0.3	0.9	0.4	0.5	7.9	6.5	7.1	7.2
III	—	—	—	—	3.6	-6.7	13.4	30	-23.9	1	-4.7	1.8	-1.9	-1.7	4.4	5.4	4.9	4.9	91	76	87	85	0.4	1.9	0.7	1.0	8.1	6.3	6.2	6.9
IV	—	—	—	—	9.4	0.4	15.9	7	-3.9	1	2.1	7.8	3.9	4.4	6.6	6.9	7.1	6.9	92	67	88	82	0.6	3.9	1.0	1.8	8.1	7.8	5.6	7.2
V	—	—	—	—	13.6	4.1	23.2	19	-5.0	4	6.9	11.8	8.1	8.7	8.8	8.9	9.4	9.0	86	64	84	78	1.6	5.5	1.7	2.9	7.6	7.5	6.8	7.3
VI	—	—	—	—	19.8	8.0	29.7	26	-1.1	3	11.8	18.0	12.9	13.9	12.1	12.0	13.1	12.4	86	59	87	77	1.9	9.3	2.0	4.4	6.0	6.4	6.4	6.3
VII	—	—	—	—	19.4	9.5	27.3	14	2.5	10	12.8	17.7	13.4	14.3	13.3	13.8	13.5	13.5	89	69	87	82	1.7	7.2	2.0	3.6	7.0	7.3	6.0	7.0
VIII	—	—	—	—	18.5	7.4	27.4	8	1.9	31	9.7	17.3	11.3	12.4	11.4	12.6	12.2	12.1	93	64	91	83	1.0	8.0	1.4	3.5	7.8	6.7	4.9	6.5
IX	—	—	—	—	18.6	6.0	25.7	2	1.2	22	8.5	16.9	10.5	11.6	10.4	12.1	11.3	11.3	92	64	89	82	1.1	7.8	1.7	3.5	7.8	5.9	3.9	5.9
X	—	—	—	—	12.6	-1.3	22.9	2	-7.6	21	1.0	11.2	3.1	4.6	6.6	8.5	7.4	7.5	95	62	92	83	0.4	5.3	0.7	2.1	7.8	3.6	3.2	4.9
XI	—	—	—	—	2.2	-5.9	11.3	7	-17.9	18	-3.8	0.5	-2.5	-2.1	4.6	5.2	4.9	4.9	93	80	91	88	0.4	2.9	0.6	1.3	8.0	7.5	7.9	7.8
XII	—	—	—	—	0.8	-5.6	5.6	20	-23.2	15	-3.1	-0.5	-2.0	-1.9	4.6	5.2	4.8	4.9	91	86	89	89	0.5	0.8	0.6	0.6	8.2	8.5	7.1	7.9
Rok	—	—	—	—	9.4	-0.8	29.7	26.VI	-32.7	7. II	2.0	7.8	3.4	4.2	7.4	8.2	8.0	7.9	91	71	89	84	0.9	4.5	1.1	2.2	7.7	6.9	6.1	6.9

Sieniawa

$H_s = 578\ m$ $h_w = 16\ m$ **1965**

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	1	1.0	7	1.3	11	1.5	19	1.3	4	2.8	10	2.1	9	1.7	4	1.2	28	1.1	59	13.3	31	9	15	29	·	·	·	2	16	15	11	1	3	31	—
II	12	1.0	9	1.1	3	1.0	2	1.0	2	1.5	9	3.1	18	1.9	16	1.9	13	1.5	58	6.2	18	18	26	28	·	·	·	1	18	19	17	·	1	28	—
III	6	1.0	12	1.0	7	1.0	17	1.5	7	1.3	11	2.3	5	1.6	9	1.3	21	1.1	39	6.2	27	7	7	24	·	·	·	5	13	16	10	·	10	27	—
IV	7	1.4	20	1.2	9	1.2	12	1.2	1	1.0	11	1.2	16	2.2	3	1.0	11	1.3	42	15.5	22	·	·	11	·	·	·	2	15	16	7	1	9	·	—
V	8	1.2	11	1.1	5	1.0	6	1.7	9	2.0	5	1.4	14	1.6	13	1.7	22	1.1	111	21.8	19	·	·	8	·	·	·	3	13	23	17	3	4	·	—
VI	7	1.3	12	1.1	2	1.0	2	1.0	2	1.0	11	1.3	26	1.9	8	1.0	29	1.1	258	82.4	10	·	·	·	4	·	·	4	8	16	15	8	2	·	—
VII	4	1.0	4	1.0	2	1.0	5	1.2	3	2.3	17	1.4	20	1.9	9	1.1	29	1.0	86	16.0	8	·	·	·	3	·	·	2	10	19	16	2	6	·	—
VIII	9	1.2	5	1.2	4	1.5	9	1.4	3	1.7	9	1.8	14	1.5	9	1.0	31	0.9	155	60.2	1	·	·	·	3	·	·	7	11	14	9	5	15	·	—
IX	3	1.0	3	1.0	2	1.0	12	1.8	3	1.7	21	1.7	13	1.3	2	2.0	31	1.0	58	21.2	11	·	·	·	2	·	·	6	5	8	6	1	9	·	—
X	8	1.1	9	1.0	23	1.2	·	·	4	1.0	11	1.5	4	1.2	2	2.0	33	0.8	18	9.4	4	·	·	16	·	·	·	12	5	8	5	·	14	·	—
XI	6	1.0	8	1.0	2	1.0	10	1.1	5	1.8	14	3.0	7	1.7	3	1.3	35	1.0	38	13.3	11	5	10	27	·	·	·	5	16	17	8	1	10	14	—
XII	1	1.0	6	1.7	5	1.0	14	1.9	10	3.2	20	2.2	10	1.1	6	1.2	21	1.5	46	10.4	3	3	10	26	·	·	·	1	18	18	11	1	3	28	—
Rok	70	1.1	105	1.1	75	1.1	108	1.3	53	1.8	149	1.9	156	1.6	84	1.4	295	1.1	968	82.4	10.VI	42	68	169	12	·	·	50	148	189	132	23	86	128	—

Zwardoń

$H_s = 690\ m$ $h_w =$ 16 m I–VI, 19 m VII–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	5	2.8	17.5	2.6	5	2.0	4.5	2.0	23	3.2	24.5	3.2	9	2.7	2.5	2.8	2	2.8	74	13.9	10	7	17	28	·	·	·	2	21	16	12	2	3	31	·
II	9.5	2.9	14	3.1	3	2.8	·	·	11	3.7	12.5	3.6	14.5	2.7	18.5	3.3	1	3.2	95	11.4	4	19	27	28	·	·	·	2	14	18	16	3	1	28	·
III	9.5	2.6	20.5	3.0	1.5	3.7	1.5	3.0	20	2.9	24	3.3	6.5	2.6	8.5	2.9	1	2.9	31	8.3	21	6	6	22	·	·	·	6	16	15	7	·	8	25	·
IV	4.5	3.9	28	2.7	5	2.6	2	2.8	10	2.8	19.5	3.0	17	2.9	4	2.8	·	2.9	77	13.7	22	·	·	11	·	·	·	5	16	19	14	1	10	·	1
V	6.5	2.8	26	2.6	4.5	2.9	3.5	2.3	10.5	2.7	21	3.2	10	2.3	11	2.4	·	2.7	160	32.2	19	·	·	4	·	·	·	4	18	20	17	6	6	1	3
VI	10	2.6	10.5	2.4	4	2.5	1	4.0	11	3.1	21.5	2.7	16	2.6	15	2.4	1	2.6	215	53.6	11	·	·	·	4	·	·	4	11	15	13	9	3	·	6
VII	4.5	2.2	11	2.5	6	2.3	3.5	2.0	16.5	2.9	34	2.8	10.5	2.5	6	2.5	1	2.6	181	30.5	18	·	·	·	3	·	·	2	12	21	17	6	6	·	6
VIII	17.5	2.4	13	2.7	3.5	2.0	3.5	2.6	8.5	2.9	21	2.9	8.5	2.5	7.5	2.5	10	2.4	116	30.7	24	·	·	·	3	·	·	11	10	14	11	4	6	·	1
IX	3	2.7	4	2.4	3.5	2.9	6.5	2.4	29	3.2	29	2.6	6	2.2	·	·	9	2.5	133	38.4	19	·	·	·	2	·	·	12	7	12	9	5	6	·	1
X	9	2.6	27	2.4	1.5	2.3	2.5	2.6	9	2.7	27	2.6	4	2.1	3	2.2	10	2.2	17	9.4	31	·	·	15	·	·	·	16	5	7	4	·	12	·	·
XI	7.5	2.3	20.5	2.4	5.5	2.3	·	·	9	2.9	39	2.8	2	3.0	3.5	2.0	3	2.5	61	13.4	11	5	10	26	·	·	·	5	19	16	11	1	7	11	·
XII	6	2.8	5	2.0	·	·	·	·	28.5	3.3	42.5	3.1	7	2.4	3	2.0	1	3.0	82	16.2	18	2	14	28	·	·	·	1	20	22	14	2	3	31	·
Rok	92.5	2.7	197	2.6	43	2.4	28.5	2.0	186	3.0	315.5	3.0	111	2.5	82.5	2.3	39	2.7	1242	53.6	11.VI	39	74	162	12	·	·	70	169	195	145	39	71	127	18

Nowy Targ

$H_s = 600\ m$ $h_w = 21{,}5\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	3.5	1.4	3	1.0	22	1.3	2	1.0	·	·	3	1.3	17.5	2.0	13	1.8	29	1.1	52	10.8	31	15	19	29	·	·	·	3	15	16	11	1	—	31	—
II	1.5	1.0	1.5	1.0	5.5	1.4	1	1.0	·	·	15	2.4	35.5	2.0	16	2.2	8	1.8	52	6.8	8	18	24	28	·	·	·	3	15	18	15	·	—	28	—
III	4	1.0	3	1.0	20	2.0	12	1.2	3	1.3	9	1.2	14	2.1	7	1.9	21	1.3	32	7.0	26	8	5	26	·	·	·	5	11	15	9	·	—	25	—
IV	1.5	2.3	5.5	2.2	26	1.8	11	1.0	3	2.3	10.5	1.5	19.5	1.6	4	2.2	9	1.5	31	10.0	22	·	·	8	·	·	·	2	16	13	7	·	—	·	—
V	6.5	1.8	5	1.0	28.5	1.4	5.5	1.4	5	1.2	11	1.3	13	2.4	10.5	2.0	8	1.5	109	19.7	6	·	·	4	1	·	·	5	16	21	16	4	—	·	—
VI	2	1.2	4	1.5	22	1.6	3	1.7	3.5	1.6	9.5	2.8	11	2.7	17	2.1	18	1.6	201	52.0	10	·	·	·	5	·	·	2	10	16	15	8	—	·	—
VII	10	1.2	5	1.2	22	1.2	9	1.1	·	·	12	2.5	15.5	1.8	9.5	1.7	10	1.4	97	22.0	8	·	·	·	3	·	·	·	9	21	16	2	—	·	—
VIII	4	2.0	2	1.0	19	1.1	6	1.0	3	1.0	13.5	1.8	18	1.7	13.5	2.2	14	1.3	147	55.2	1	·	·	·	4	·	·	4	14	11	9	4	—	·	—
IX	1	2.0	3	1.0	16.5	1.2	14	1.2	10.5	1.7	9.5	1.1	10.5	1.7	4	1.5	21	1.0	69	24.5	11	·	·	·	1	·	·	1	6	9	6	2	—	·	—
X	0.5	2.0	2	1.0	13	1.3	16.5	1.1	7	1.1	11.5	2.4	11	1.8	8.5	2.6	23	1.2	9	3.3	31	·	·	19	·	·	·	10	3	6	3	·	—	·	—
XI	3	1.3	1	1.0	15	1.6	14	1.1	3	1.0	8.5	1.8	27	2.4	4.5	1.6	14	1.5	32	11.3	11	6	10	24	·	·	·	3	16	12	6	1	—	10	—
XII	1	2.0	3	1.0	23	1.2	7	1.4	3.5	1.3	14	2.4	18.5	2.3	7	2.1	16	1.5	39	8.2	3	6	12	28	·	·	·	2	19	15	10	·	—	31	—
Rok	38.5	1.6	38	1.2	232.5	1.4	101	1.2	41.5	1.0	127	1.9	211	2.0	114.5	2.0	191	1.4	870	55.2	1.VIII	55	70	166	14	·	·	40	150	173	123	22	—	125	—

Jabłonka

$H_s = 620\ m$ $h_w = 19{,}2\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V>15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K
I	2	3.5	13.5	2.7	6	1.6	1	1.0	·	·	22	4.9	6.5	2.9	3	4.2	39	2.1	51	10.5	31	17	19	29	·	4	·	·	20	16	12	1	3	31	·
II	6.5	3.3	12	2.6	2	2.0	·	·	·	·	20.5	7.2	1.5	2.7	6.5	3.4	35	2.8	47	7.8	8	20	26	28	·	6	3	3	14	18	15	·	·	28	·
III	7	2.9	16	2.7	10.5	1.7	1.5	1.7	·	·	18	4.7	3.5	6.1	0.5	1.0	36	2.1	29	6.6	24	8	8	24	·	2	·	4	16	16	9	·	5	22	·
IV	4	3.8	14.5	3.1	9	2.4	1	1.0	1	5.0	15.5	2.9	7	3.1	3	3.5	35	1.8	50	10.3	22	·	·	13	·	1	·	3	14	22	12	1	2	1	2
V	11.5	3.1	16.5	2.2	5	3.2	·	·	1	9.0	24	3.5	7	3.2	2	3.0	26	2.3	106	17.7	19	·	·	6	·	1	1	2	14	23	16	3	4	·	3
VI	6.5	3.1	4	2.0	6.5	1.3	1	3.0	·	·	14.5	3.8	9.5	3.4	5	2.7	43	1.6	190	56.1	10	·	·	1	5	1	1	·	9	17	15	6	4	·	6
VII	3	2.0	4.5	2.2	0.5	2.0	1	2.0	2.5	2.2	31.5	3.6	5.5	2.9	0.5	1.0	44	1.7	103	24.1	8	·	·	·	3	2	·	1	11	21	15	2	3	·	5
VIII	10	4.5	9.5	2.9	2.5	2.0	0.5	2.0	1.5	3.7	14	3.5	3	3.5	4	2.2	48	1.6	149	59.2	1	·	·	·	2	2	1	2	10	15	12	4	9	·	3
IX	2.5	2.6	7	2.2	3	1.3	2.5	1.6	2.5	3.6	26.5	4.3	5.5	4.6	0.5	5.0	40	2.0	85	26.1	11	·	·	·	2	3	1	1	5	16	7	4	12	·	·
X	5.5	2.3	7.5	1.8	6	1.7	·	·	2	1.5	12	3.3	3.5	2.9	1.5	3.0	55	1.0	8	4.0	31	·	·	20	·	·	·	5	5	12	2	·	15	·	·
XI	3.5	2.7	13.5	2.8	10.5	1.6	0.5	1.0	1.5	1.3	23	6.3	5	5.4	0.5	5.0	32	2.7	39	9.2	11	7	10	24	·	8	4	3	20	17	9	·	2	16	·
XII	1.5	4.0	6	2.6	7	1.6	1	1.0	0.5	5.0	48	5.2	5.5	2.7	2.5	3.0	21	3.3	46	12.8	3	6	11	29	·	7	4	1	18	19	8	2	1	23	·
Rok	63.5	3.2	124.5	2.5	68.5	1.9	10	1.2	12.5	2.6	269.5	4.4	63	3.6	29.5	3.1	454	2.1	903	59.2	1.VIII	58	74	174	12	37	15	25	156	212	132	23	60	121	19

Maniowy — φ = 49°28' — λ = 20°15' — 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PREŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−1.1	−10.3	3.9	29	−25.5	8	−6.7	−3.3	−5.3	−5.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	−3.9	−15.3	2.7	14	−34.0	7	−11.0	−5.8	−9.9	−9.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	4.1	−7.2	14.4	30	−26.9	1	−4.8	1.9	−2.1	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	10.5	1.2	17.4	7	−3.1	1	2.9	9.3	4.7	5.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	14.7	4.5	25.5	19	−5.0	3	6.8	12.8	8.8	9.3	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	20.7	8.2	29.5	26, 27	0.1	3	12.3	18.8	13.2	14.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	20.6	8.9	27.4	14	2.7	10	12.4	18.6	13.4	14.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	19.7	7.3	30.0	7, 8	1.8	3	10.0	17.9	11.8	12.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.6	6.6	25.5	3	1.8	22	9.6	17.9	11.1	12.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	13.1	−0.6	24.5	2	−7.5	22	1.1	10.7	3.2	4.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	3.2	−5.1	13.1	2	−15.2	18	−3.0	1.6	−2.0	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	1.0	−8.1	5.9	19	−16.3	15	−5.0	−0.9	−2.9	−2.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	10.2	−0.8	30.0	7, 8, VIII	−34.0	7, 11	2.0	8.3	3.7	4.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Przehyba — φ = 49°28' — λ = 20°34'

I	—	—	—	—	−2.4	−7.1	2.8	31	−13.5	8	−5.3	−3.9	−4.9	−4.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.8	7.5	7.4
II	—	—	—	—	−7.8	−13.3	0.0	1	−20.3	6	−11.8	−9.3	−11.4	−11.0	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.7	7.4	7.8
III	—	—	—	—	0.9	−5.6	9.2	19	−13.2	1	−3.8	−0.7	−3.0	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.5	6.0	6.3
IV	—	—	—	—	4.5	−1.2	12.2	7	−9.0	1	0.3	2.7	1.0	1.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.7	6.5	7.1
V	—	—	—	—	9.2	2.4	19.9	18	−5.4	3	3.8	7.2	5.1	5.3	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.8	6.6	7.2
VI	—	—	—	—	15.3	7.4	24.7	26	2.6	3	9.6	13.5	10.0	10.8	—	—	—	—	—	—	—	—	—	—	—	—	4.3	5.9	6.2	5.5
VII	—	—	—	—	15.3	8.8	21.4	15	3.1	6	10.5	13.5	11.3	11.6	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.3	5.9	5.9
VIII	—	—	—	—	14.3	7.3	23.1	8	2.7	26, 27	8.8	11.7	9.7	10.0	—	—	—	—	—	—	—	—	—	—	—	—	5.4	6.7	6.3	6.1
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.6	4.7	5.2
X	—	—	—	—	9.1	1.4	18.9	1, 2	−5.0	21	3.4	6.7	3.9	4.5	—	—	—	—	—	—	—	—	—	—	—	—	5.1	5.3	4.3	4.9
XI	—	—	—	—	−0.2	−6.5	8.5	9	−16.0	25	−4.7	−2.4	−4.2	−3.9	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.1	7.1	7.2
XII	—	—	—	—	−1.2	−7.7	4.4	20	−15.0	29, 30	−4.5	−3.1	−4.8	−4.3	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.9	7.1	7.5
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.8	6.3	6.5

Lesko — φ = 49°28' — λ = 22°20'

I	967.8	981.3	942.6	1014.4	1.1	−4.4	6.5	31	−15.3	12	−2.4	0.1	−1.4	−1.3	4.4	4.5	4.6	4.5	83	74	83	80	0.9	1.7	1.0	1.2	7.8	8.3	7.2	7.8
II	969.4	981.7	949.2	1017.4	−4.0	−10.3	1.1	12	−21.9	7	−8.2	−5.3	−7.2	−7.0	2.9	3.1	3.1	3.0	84	74	82	80	0.6	1.1	0.6	0.8	9.0	7.8	7.4	8.1
III	972.1	986.9	947.0	1018.4	6.2	−2.8	15.1	30	−17.5	1	−1.0	4.5	1.6	1.7	5.2	5.6	5.6	5.5	87	67	80	78	0.8	3.3	1.5	1.9	7.5	6.9	5.9	6.8
IV	965.6	981.7	949.3	1010.8	11.0	1.5	15.5	27	−4.0	6	3.4	9.0	5.7	6.0	6.8	7.0	7.1	7.0	86	61	77	75	1.1	4.8	2.1	2.7	8.1	8.0	6.0	7.4
V	969.1	983.0	959.4	1013.9	14.9	5.7	26.4	19	−3.8	3	7.8	12.9	10.1	10.2	9.2	9.2	9.9	9.4	85	61	78	75	2.0	6.4	3.0	3.8	8.2	7.8	6.6	7.5
VI	970.4	977.7	957.3	1014.4	20.7	10.3	30.1	26	4.4	8	13.2	18.7	14.9	15.4	13.4	13.5	14.1	13.7	87	64	83	78	2.1	8.7	3.1	4.6	6.2	6.9	6.4	6.5
VII	969.9	976.8	960.8	1013.7	21.2	11.5	28.0	17	6.1	12	13.9	19.4	15.4	16.0	14.1	14.9	14.6	14.5	88	67	83	79	2.0	8.3	3.2	4.5	6.0	6.6	6.4	6.3
VIII	972.3	979.8	953.5	1016.6	19.5	9.6	29.2	8	4.1	31	11.6	17.7	13.5	14.1	12.3	12.7	13.1	12.7	90	64	84	79	1.7	8.5	2.8	4.3	6.0	6.3	4.6	5.6
IX	973.4	988.6	963.3	1017.7	20.5	8.3	26.7	2	2.8	17	10.8	19.0	12.7	13.8	11.1	12.6	12.5	12.1	86	58	85	76	2.2	10.0	7.4	6.5	5.8	5.6	3.0	4.8
X	978.5	990.1	969.1	1024.2	12.2	1.8	24.5	2	−6.0	22	3.6	11.0	6.1	6.7	7.4	8.0	8.0	7.8	90	61	83	78	0.8	5.8	1.8	2.8	6.4	5.8	4.2	5.5
XI	967.4	985.0	945.2	1013.7	3.7	−2.9	14.6	2	−17.4	18	−0.9	1.9	0.0	0.2	5.0	5.1	5.2	5.1	84	72	81	79	1.1	2.4	1.4	1.6	8.4	7.7	7.5	7.9
XII	964.2	978.3	945.8	1010.4	2.8	−2.2	7.9	10, 11	−10.8	17	−0.1	1.5	0.3	0.5	5.2	5.2	5.1	5.2	84	75	81	80	1.0	1.8	1.3	1.4	7.9	8.0	7.5	7.8
Rok	970.0	990.1	942.6	1015.4	10.8	2.2	30.1	26.VI	−21.9	7, 11	4.3	9.2	6.0	6.4	8.1	8.4	8.6	8.4	86	66	82	78	1.4	5.2	2.4	3.0	7.3	7.1	6.1	6.8

Czarny Dunajec — φ = 49°27' — λ = 19°51'

I	—	—	—	—	−0.6	−8.4	5.1	30	−16.9	12	−5.5	−2.2	−4.3	−4.1	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.6	6.8	7.9
II	—	—	—	—	−4.8	−13.3	1.0	14	−27.1	7	−10.6	−6.7	−9.5	−9.1	—	—	—	—	—	—	—	—	—	—	—	—	8.4	6.7	7.4	7.5
III	—	—	—	—	3.7	−6.7	12.7	30	−21.1	1	−4.8	1.5	−1.6	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.3	6.1	6.8
IV	—	—	—	—	9.1	0.0	16.0	7	−4.7	1	1.5	8.0	3.9	4.3	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.8	7.6	8.3
V	—	—	—	—	13.4	4.1	24.4	19	−4.5	3, 4	6.3	11.6	8.4	8.7	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.6	8.1	8.2
VI	—	—	—	—	19.6	7.9	29.7	26	0.5	3	11.8	17.8	13.3	14.0	—	—	—	—	—	—	—	—	—	—	—	—	5.4	7.1	7.2	6.6
VII	—	—	—	—	19.3	8.8	27.6	15	3.9	10, 11	12.5	17.4	13.6	14.3	—	—	—	—	—	—	—	—	—	—	—	—	7.1	8.4	7.6	7.7
VIII	—	—	—	—	18.0	7.4	27.6	7	2.4	31	9.8	16.5	12.2	12.7	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.0	6.1	6.3
IX	—	—	—	—	18.2	5.8	26.4	3	−0.6	22	8.1	16.6	11.4	11.9	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.2	3.8	5.6
X	—	—	—	—	11.8	−0.9	22.3	2	−6.6	21	1.1	10.8	4.6	5.3	—	—	—	—	—	—	—	—	—	—	—	—	6.9	4.8	2.9	4.9
XI	—	—	—	—	1.9	−5.6	11.0	2	−15.9	24	−3.7	0.1	−2.2	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.6	6.8	7.6
XII	—	—	—	—	0.6	−6.2	7.7	20	−16.8	15	−2.9	−0.9	−2.6	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.6	8.1	8.2
Rok	—	—	—	—	9.2	−0.6	29.7	26.VI	−27.1	7, 11	2.0	7.5	3.9	4.3	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.4	6.5	7.1

Maniowy $H_s = 520$ m $h_w = 16{,}7$ m 1965

MIESIĄC	ROZKŁAD WIATRU																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	●	Opad R			≡	⊠	K (K)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15			R≥0.1	R≥1.0	R≥10.0			
I	1.5	1.7	2.5	2.0	21	3.7	1.5	2.0	·	·	4	4.6	18	3.3	6.5	4.0	38	2.1	46	9.5	31	16	20	30	·	1	·	—	—	15	11	·	8	31	—
II	2.5	2.4	2	2.5	2	1.5	2	2.0	0.5	1.0	5	5.6	32	4.6	16	4.1	22	3.1	30	6.7	7	17	24	28	·	2	1	—	—	17	12	·	6	28	—
III	5	4.2	2	2.8	15	4.3	2	1.5	0.5	8.0	2.5	4.8	16	2.8	4	4.8	46	1.9	38	8.4	31	10	8	26	·	2	1	—	—	17	12	·	11	26	—
IV	6.5	3.5	12	4.2	16	4.4	4	5.2	·	·	1	2.0	24	3.8	8.5	3.8	18	3.2	31	9.2	22	·	·	10	·	2	·	—	—	20	7	·	3	–	—
V	7	3.7	4.5	3.8	19.5	2.2	0.5	6.0	·	·	1.5	6.0	31.5	2.8	11.5	3.5	17	2.5	103	14.1	6	·	·	6	1	4	·	—	—	25	17	2	4	·	—
VI	0.5	4.0	7.5	3.4	14	3.1	0.5	6.0	1.5	7.3	1.5	5.3	32.5	3.3	11	2.8	21	2.6	174	52.3	10	·	·	·	6	1	1	—	—	20	14	7	2	–	—
VII	1.5	2.7	2.5	4.4	16.5	1.8	1	8.0	0.5	2.0	2	4.0	26.5	2.7	7.5	3.4	35	1.7	87	20.5	8	·	·	·	5	1	·	—	—	27	15	2	7	·	—
VIII	7	2.3	3.5	2.3	14	3.1	2	3.5	·	·	·	·	25.5	2.0	8	3.6	33	1.6	134	44.7	1	·	·	·	4	1	1	—	—	19	12	4	8	·	—
IX	0.5	2.0	3.5	6.7	21.5	4.3	6.5	6.7	·	·	1	4.5	9	2.3	7	3.2	41	2.3	79	25.8	11	·	·	·	1	3	1	—	—	17	7	3	10	·	—
X	2.5	2.4	8	1.9	10.5	1.6	1.5	2.0	·	·	1.5	2.7	26.5	2.0	4.5	3.1	38	1.2	11	4.1	31	·	·	20	·	·	·	—	—	12	4	·	19	·	—
XI	3.5	3.0	4	4.1	18.5	4.3	3	2.3	0.5	4.0	5.5	3.6	31	4.2	5	4.9	19	3.2	27	7.9	11	7	10	23	·	6	1	—	—	14	6	·	2	10	—
XII	1.5	2.3	1.5	3.7	18	2.0	3	1.3	·	·	2.5	2.2	29.5	3.0	5	3.4	32	1.7	33	8.4	18	14	11	31	·	·	·	—	—	18	8	·	7	31	—
Rok	39.5	2.8	53.5	3.5	186.5	3.0	27.5	3.9	3.5	1.9	28	3.8	302	3.1	94.5	3.7	360	2.3	793	52.3	10.VI	64	73	174	17	23	6	—	—	221	125	18	87	126	—

Przehyba $H_s = 1175$ m $h_w = 13{,}5$ m

I	15.5	3.7	·	·	1	4.0	3	6.0	44	7.4	7	3.6	3.5	3.0	8	4.1	11	5.1	77	21.8	4	3	26	31	·	7	4	2	16	16	11	2	19	31	·
II	3.5	2.9	·	·	·	·	2	6.5	14	6.0	6.5	3.2	5.5	4.4	39.5	4.5	13	3.9	88	12.3	16	24	27	28	·	4	·	1	15	23	18	3	15	28	·
III	14	4.4	1	2.5	2	3.5	10	3.4	37	7.0	3	5.5	5.5	3.5	11.5	3.9	9	4.8	60	10.8	27	8	11	29	·	3	3	6	10	16	13	1	18	31	·
IV	15.5	4.1	·	·	2	2.5	2	2.2	27.5	5.0	11	3.1	6	2.8	20	4.1	6	3.8	48	14.0	22	·	3	19	·	4	1	2	16	16	12	2	20	15	3
V	19.5	5.0	2	5.5	2	3.0	2	4.8	26	6.2	12.5	4.3	5	2.5	18	4.4	6	4.6	127	16.8	11	·	·	7	·	5	1	1	12	23	20	4	15	4	4
VI	4.5	5.1	1	4.0	1.5	5.0	3.5	5.9	39	6.3	15	4.7	8.5	2.7	13	4.4	4	5.0	277	48.5	10	·	·	·	·	4	2	4	8	18	15	11	10	·	8
VII	7.5	3.1	1.5	5.3	1	4.0	1	4.0	32.5	4.5	28.5	2.7	7	1.6	7	2.6	7	3.2	172	33.7	17	·	·	·	·	1	1	2	5	22	17	7	12	·	8
VIII	24	4.8	6	1.7	2	2.0	·	·	27	6.0	7	2.6	7	2.0	20	4.6	·	4.5	199	43.2	1	·	·	·	·	5	1	6	13	16	15	6	11	·	1
IX	11	3.3	·	·	·	·	2	3.0	58.5	8.1	14.5	3.6	·	·	4	2.2	·	6.4	65	20.2	7	—	—	—	—	11	2	6	8	9	7	3	10	·	·
X	29	4.1	2	2.0	3	3.7	1	2.0	25	3.7	9	3.8	11	2.9	13	3.3	·	3.6	16	7.8	9	·	·	14	·	·	·	8	8	7	6	·	11	·	·
XI	29	4.7	1	2.0	1	3.0	1	6.0	29	10.0	7	5.3	14	3.2	8	3.4	·	6.0	41	19.1	11	10	13	25	·	7	4	1	16	15	10	1	19	20	·
XII	·	·	·	·	·	·	·	·	50	8.0	32	5.6	6	9.0	5	5.0	·	7.1	58?	14.3	12	7	25	31	·	13	7	1	16	12	10	1	15	31	·
Rok	173	3.8	14.5	1.9	15.5	2.6	27.5	3.6	409.5	6.5	153	4.0	79	3.1	167	3.9	56	4.8	1228?	48.5	10.VI	—	—	—	—	64	26	40	143	193	154	41	175	160	24

Lesko $H_s = 386$ m $H_b = 375{,}2$ m $h_w =$ 17,6 m wiatromierz Wilda, 17,6 m anemometr M-47

I	3.5	3.0	1	3.0	3	1.5	4.5	4.8	27.5	6.2	3	9.7	10.5	5.0	2	5.5	38	3.3	66	18.9	31	5	10	28	·	9	2	1	20	20	13	1	7	31	·
II	6.5	3.0	8.5	3.9	3.5	4.7	3.5	3.0	16	8.3	7	5.2	5.5	5.5	19.5	3.0	1.4	4.0	39	6.9	16	11	24	28	·	6	2	1	19	23	12	·	1	28	·
III	4.5	2.6	4.5	2.4	10	2.3	5	2.8	29	5.6	8	4.1	1	8.0	5	5.1	26	3.1	41	9.1	3	4	5	19	·	8	·	4	15	14	9	·	1	16	·
IV	8.5	3.9	6	4.3	19	4.4	6.5	2.5	12.5	3.5	4.5	6.1	6	3.6	8	3.6	19	3.1	35	7.3	30	·	·	8	·	2	·	1	13	14	8	·	3	1	3
V	12	3.4	5	4.0	5	3.4	4	2.0	23.5	4.0	5.5	6.6	6.5	3.5	14.5	3.9	17	3.2	68	11.4	10	·	·	2	1	3	1	1	11	18	12	1	5	·	4
VI	6	3.4	3	3.5	3	3.2	6.5	2.5	24	3.1	5	6.6	7.5	2.3	16	3.5	19	2.6	165	29.0	10	·	·	·	4	2	·	1	9	16	13	7	7	·	9
VII	4	2.1	4	1.6	6	2.6	7	1.8	22.5	3.9	11.5	3.1	3	3.8	9	2.8	26	2.2	209	54.9	25	·	·	·	6	1	·	3	6	21	18	8	8	·	10
VIII	6	2.0	3	1.8	3.5	2.3	12.5	2.4	15	4.1	6	4.2	8	4.6	16	2.8	23	2.4	206	53.7	26	·	·	·	5	·	·	8	10	14	11	6	6	·	4
IX	3	4.8	2	1.0	4.5	1.4	28	2.7	29	4.8	2	4.5	5.5	3.4	5	3.8	11	3.2	73	35.8	11	·	·	·	2	5	·	6	2	9	4	2	6	·	1
X	5.5	2.3	3	1.5	5	2.3	16.5	2.7	12	6.4	5	5.6	13.5	2.7	10.5	3.4	22	2.7	18	5.2	4	·	·	13	·	4	·	7	11	15	6	·	9	·	·
XI	4.5	3.0	5	2.9	7	3.4	5	4.0	27.5	7.9	3.5	4.3	14	4.1	5.5	2.6	18	4.2	63	20.7	11	2	8	21	·	7	3	1	17	16	11	2	4	15	·
XII	5	1.9	3	2.3	3	2.5	17.5	3.5	41	7.4	5	8.6	4.5	4.7	7	3.7	7	5.2	45	8.2	8	1	7	26	·	15	3	1	18	18	9	·	1	15	·
Rok	69	3.0	48	2.7	72.5	2.8	116.5	2.9	279.5	5.4	66	5.7	85.5	4.3	118	3.6	240	3.3	1028	54.9	25.VII	23	54	145	18	62	11	35	151	198	126	27	58	106	31

Uwaga. Kierunki i prędkości wiatru w ciągu roku – częściowo wg wiatromierza Wilda, częściowo wg anemometru M-47.

Czarny Dunajec $H_s = 676$ m $h_w = 18$ m

I	7.5	2.5	5.5	2.4	2.5	2.2	2	1.0	2.5	2.0	13	3.5	16.5	4.6	2.5	2.2	41	1.8	55	14.1	31	11	19	31	·	2	1	1	18	14	12	1	·	31	·
II	5.5	3.5	8.5	3.1	1	1.0	·	·	·	·	11	4.5	11.5	4.9	6.5	4.7	40	2.2	50	7.0	8	19	25	28	·	4	·	3	15	18	15	·	·	28	·
III	8.5	4.9	9	3.2	2.5	3.0	1	2.0	·	·	6.5	5.4	7.5	4.5	3	4.8	55	1.8	31	7.5	24	10	6	26	·	1	1	4	15	15	10	·	8	30	·
IV	6	3.2	12.5	3.0	11.5	2.9	1	3.5	1	3.0	12	3.3	12.5	3.7	4.5	3.4	29	2.2	37	10.1	22	·	·	14	·	2	1	5	21	13	8	1	3	1	1
V	11	4.8	13	3.5	6	2.2	1	2.5	1	2.0	14.5	3.6	15	3.0	2.5	2.8	29	2.4	98	14.9	19	·	·	6	·	3	1	2	22	19	19	1	1	·	4
VI	7.5	3.2	6.5	2.3	5.5	2.0	2	2.5	1	5.0	13.5	3.8	14.5	3.3	12.5	3.4	27	2.2	226	67.9	10	·	·	·	4	2	1	3	10	16	14	6	2	·	6
VII	5.5	2.4	5	2.5	4	2.1	·	·	4	4.4	18	3.2	12	3.8	3.5	2.6	41	1.8	121	40.0	8	·	·	·	3	1	1	1	17	20	14	4	4	·	9
VIII	9.5	4.6	10.5	2.9	2.5	1.4	2	2.5	1	4.0	6	3.0	9.5	2.5	10	3.4	42	1.7	159	70.0	1	·	·	·	3	1	1	4	12	13	9	4	6	·	2
IX	3.5	3.0	5	2.1	6.5	2.1	6	3.3	6	3.9	5.5	2.6	9	3.1	1.5	3.0	47	1.4	77	28.3	11	·	·	1	2	1	·	5	5	8	7	3	6	·	·
X	8	3.6	8.5	2.6	5.5	2.0	0.5	1.0	·	·	7.5	3.5	10	4.4	3	3.3	50	1.5	12	7.7	31	·	·	20	·	·	·	7	7	3	3	·	10	·	1
XI	8	3.4	9.5	2.9	4.5	1.6	0.5	1.0	1.5	4.7	11.5	6.7	10.5	6.3	2	2.8	42	2.4	43	17.1	11	7	10	26	·	6	6?	3	19	16	7	1	3	17	·
XII	4.5	4.0	1	3.0	1	3.0	2	1.5	·	·	24	4.7	23	3.7	1.5	5.3	36	2.5	41	10.4	3	6	15	28	·	4	1	1	19	16	10	1	4	30	·
Rok	85	3.6	94.5	2.8	53	2.1	18	1.7	18	2.4	143	4.0	151.5	4.0	63	3.5	479	2.0	950	70.0	1.VIII	53	75	180	12	27	14?	39	180	171	28	22	47	137	23

Krościenko — φ = 49°27′ — λ = 20°25′ — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m.}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	1.0	−7.3	7.6	30	−21.0	8	−4.0	−0.1	−3.5	−2.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.0	7.0	7.3
II	—	—	—	—	−3.0	−13.0	3.4	14	−27.7	7	−9.6	−4.3	−8.8	−7.9	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.1	6.8	7.4
III	—	—	—	—	5.8	−5.4	15.2	30	−20.0	1	−2.2	4.1	−0.8	0.1	—	—	—	—	—	—	—	—	—	—	—	—	7.9	6.5	6.1	6.8
IV	—	—	—	—	10.8	1.2	17.5	7	−3.3	6	3.7	9.7	4.7	5.7	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.6	7.3	7.7
V	—	—	—	—	15.1	4.7	26.6	19	−4.5	3, 4	8.4	13.4	8.8	9.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.8	7.1	7.6
VI	—	—	—	—	21.3	8.9	31.1	26	1.1	3	13.8	19.6	13.0	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.3	5.9	6.0
VII	—	—	—	—	21.3	9.0	28.6	14	3.0	10	13.9	19.4	12.9	14.8	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.4	6.3	6.9
VIII	—	—	—	—	20.0	8.4	29.8	7	2.5	31	12.1	18.6	11.9	13.6	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.9	5.9	6.4
IX	—	—	—	—	20.0	7.3	25.9	3	1.5	22	11.1	18.5	11.0	12.9	—	—	—	—	—	—	—	—	—	—	—	—	7.5	5.6	4.3	5.8
X	—	—	—	—	13.3	−0.3	25.1	2	−7.4	22	1.9	11.8	3.3	5.1	—	—	—	—	—	—	—	—	—	—	—	—	7.2	4.4	4.2	5.3
XI	—	—	—	—	3.3	−4.6	13.4	2	−15.0	25	−2.2	2.1	−2.0	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.6	6.8	7.1
XII	—	—	—	—	1.9	−5.7	7.6	10	−12.6	15	−3.0	0.4	−2.1	−1.7	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.4	6.5	7.2
Rok	—	—	—	—	10.9	0.3	31.1	26.VI	−27.7	7. II	3.7	9.4	4.0	5.3	—	—	—	—	—	—	—	—	—	—	—	—	7.4	6.7	6.2	6.8

Brzegi Dolne — φ = 49°27′ — λ = 22°38′

I	—	—	—	—	1.4	−6.5	6.5	30	−24.9	12	−3.4	0.3	−2.4	−2.0	—	—	—	—	—	—	—	—	—	—	—	—	7.9	8.4	7.5	7.9
II	—	—	—	—	−4.2	−12.3	0.6	12	−27.5	7	−8.2	−5.3	−8.3	−7.5	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.3	6.7	8.0
III	—	—	—	—	5.9	−5.0	15.1	30	−25.3	1	−2.2	4.6	−0.1	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.8	5.3	6.7
IV	—	—	—	—	10.4	−0.3	15.6	26	−4.4	2	2.4	9.0	4.1	4.9	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.5	6.2	7.9
V	—	—	—	—	14.7	3.8	25.6	19	−7.0	3	7.5	13.1	8.6	9.4	—	—	—	—	—	—	—	—	—	—	—	—	7.8	8.7	5.9	7.5
VI	—	—	—	—	20.4	8.2	29.2	26	1.2	8	13.4	19.0	13.1	14.6	—	—	—	—	—	—	—	—	—	—	—	—	5.3	7.1	6.2	6.2
VII	—	—	—	—	21.1	9.5	27.9	16	3.7	12	13.9	19.8	13.8	15.3	—	—	—	—	—	—	—	—	—	—	—	—	5.5	7.4	6.2	6.4
VIII	—	—	—	—	19.0	7.4	28.1	8	2.4	31	11.3	17.6	10.9	12.7	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.2	4.6	5.9
IX	—	—	—	—	19.9	5.2	25.7	2	−0.6	17	9.4	19.2	10.0	12.2	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.4	3.9	5.1
X	—	—	—	—	12.0	−0.7	22.9	1	−8.9	22	2.3	11.0	3.4	5.0	—	—	—	—	—	—	—	—	—	—	—	—	6.9	5.8	4.7	5.8
XI	—	—	—	—	3.3	−4.5	13.6	2	−25.5	18	−1.5	1.2	−1.1	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.1	8.1	8.3
XII	—	—	—	—	2.9	−3.7	8.8	10	−17.6	17	−0.6	1.4	−0.4	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.8	8.2	7.9
Rok	—	—	—	—	10.6	0.1	29.2	26.VI	−27.5	7. II	3.7	9.2	4.3	5.4	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.5	6.1	7.0

Czorsztyn — φ = 49°26′ — λ = 20°19′

I	—	—	—	—	0.4	−9.9	6.6	29	−23.8	8	−6.6	−2.6	−5.1	−4.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	6.9	7.1	7.4
II	—	—	—	—	−2.6	−13.9	4.4	14	−31.5	7	−11.0	−5.0	−8.8	−8.4	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.5	6.6	6.9
III	—	—	—	—	5.0	−6.5	14.6	30	−21.5	1	−4.1	2.5	−1.7	−1.2	—	—	—	—	—	—	—	—	—	—	—	—	8.9	5.8	6.5	7.1
IV	—	—	—	—	10.2	0.9	17.2	7	−4.3	2	2.9	9.1	4.6	5.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.3	6.3	7.1
V	—	—	—	—	14.4	4.6	26.6	19	−5.3	3	7.0	13.0	8.6	9.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.5	7.3	7.5
VI	—	—	—	—	20.6	8.8	30.7	26	0.8	3	12.5	19.2	13.2	14.5	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.7	6.5	5.9
VII	—	—	—	—	20.5	9.7	27.1	15	3.0	10	12.7	18.8	13.2	14.5	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.3	5.2	6.5
VIII	—	—	—	—	19.6	7.9	30.1	8	3.1	31	10.3	18.1	12.1	13.2	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.1	6.0	6.7
IX	—	—	—	—	19.5	6.8	25.0	3	2.3	22	9.8	18.0	11.4	12.6	—	—	—	—	—	—	—	—	—	—	—	—	8.4	4.7	4.8	6.0
X	—	—	—	—	—	−0.3	24.6	2	−7.3	22, 23	1.3	11.2	3.2	4.7	—	—	—	—	—	—	—	—	—	—	—	—	9.3	3.8	3.4	5.5
XI	—	—	—	—	2.9	−4.9	13.2	2	−15.9	25	−3.1	1.8	−2.2	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.4	5.6	6.4
XII	—	—	—	—	1.2	−7.2	6.4	6	−16.1	30	−4.7	−0.5	−3.0	−2.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.9	6.8	7.1
Rok	—	—	—	—	—	−0.3	30.7	26.VI	−31.5	7. II	2.2	8.6	3.8	4.6	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.2	6.0	6.7

Czorsztyn-Nadzamcze — φ = 49°26′ — λ = 20°20′

I	—	—	—	—	−0.6	−7.2	6.1	30	−19.4	8	−5.5	−1.9	−4.1	−3.9	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.6	6.4	6.7
II	—	—	—	—	−5.2	−12.3	1.8	14	−24.9	7	−10.5	−6.6	−9.2	−8.9	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.9	6.2	7.0
III	—	—	—	—	4.1	−5.4	12.9	30	−18.4	1	−3.8	2.2	−1.0	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	7.5	5.9	6.3	6.6
IV	—	—	—	—	8.9	0.8	15.9	7	−5.3	2	2.4	7.8	3.6	4.4	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.8	5.8	6.5
V	—	—	—	—	13.4	4.5	24.5	19	−3.7	4	6.2	11.7	7.9	8.4	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.4	6.0	6.7
VI	—	—	—	—	19.5	8.8	28.8	26	1.1	3	11.7	17.7	12.8	13.8	—	—	—	—	—	—	—	—	—	—	—	—	5.0	6.0	5.8	5.6
VII	—	—	—	—	19.5	9.6	26.4	15	3.4	10	12.1	17.7	13.1	14.0	—	—	—	—	—	—	—	—	—	—	—	—	5.4	7.0	4.8	5.7
VIII	—	—	—	—	18.2	8.1	28.3	7	2.5	31	10.2	16.7	12.1	12.8	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.2	5.4	6.2
IX	—	—	—	—	18.3	7.7	23.5	3	3.2	23	9.9	16.5	11.6	12.4	—	—	—	—	—	—	—	—	—	—	—	—	6.8	5.6	3.9	5.4
X	—	—	—	—	12.1	−0.2	23.4	2	−6.5	22	0.9	10.4	4.4	5.0	—	—	—	—	—	—	—	—	—	—	—	—	6.7	4.1	3.5	4.8
XI	—	—	—	—	2.1	−4.9	11.5	2	−15.7	26	−3.4	0.5	−2.4	−1.9	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.0	6.1	6.2
XII	—	—	—	—	0.7	−5.8	7.3	10	−13.6	15	−4.2	−0.6	−2.7	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	6.2	6.8	5.4	6.1
Rok	—	—	—	—	9.2	0.3	28.8	26.VI	−24.9	7. II	2.2	7.7	3.8	4.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.3	5.5	6.1

Krościenko $H_s = 440$ m $h_w = 24,2$ m 1965

MIESIĄC	ROZKŁAD WIATRU (n, V_{mD}) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V V≥10	V>15	◔	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	·	·	1.5	1.7	10	1.4	3	2.2	2.5	2.2	20	1.2	15	1.6	2	1.0	39	0.8	53	10.5	31	12	14	29	·	1	·	1	15	16	12	1	5	31	—
II	1	1.0	·	·	·	·	2	1.2	1	1.5	8.5	2.2	45.5	2.1	3	1.0	23	1.5	50	7.5	7	17	25	28	·	1	·	2	14	21	15	·	3	28	—
III	5.5	1.5	8	1.5	2.5	1.2	6	2.4	4.5	3.6	14	1.4	24	1.9	0.5	1.0	28	1.3	47	10.1	24	8	4	23	·	1	·	4	12	18	13	1	4	27	—
IV	6.5	1.3	20	1.1	11.5	1.0	4	1.1	1.5	1.3	10	1.8	21	2.0	0.5	1.0	15	1.2	38	8.3	22	·	·	10	·	·	·	1	15	17	8	·	1	1	—
V	10	1.3	16.5	1.4	8	1.0	·	·	2	1.0	10.5	1.2	23.5	1.7	3.5	1.0	19	1.1	119	32.0	29	·	·	6	2	2	·	1	17	22	15	3	1	·	—
VI	2.5	1.0	9.5	1.1	6.5	1.3	3.5	1.3	3	1.2	4.5	1.4	23.5	1.7	6	1.0	31	0.9	170	41.3	10	·	·	·	7	2	·	2	10	17	15	5	·	·	—
VII	2.5	1.2	5.5	1.0	7	2.1	2.5	1.0	·	·	10.5	1.2	24.5	1.2	3.5	1.1	37	0.8	119	29.0	8	·	·	·	6	2	·	1	10	19	16	4	2	·	—
VIII	6	1.0	10.5	1.1	11.5	1.3	2.5	1.4	1.5	1.7	8	1.1	15.5	1.1	3.5	1.0	34	0.7	135	46.1	1	·	·	·	4	·	·	2	13	14	11	4	2	·	—
IX	0.5	1.0	3	1.3	10.5	1.5	10.5	1.7	6.5	1.6	13.5	1.7	14.5	1.4	4	1.0	27	1.1	50	25.5	29	·	·	·	1	2	·	1	5	9	7	2	8	·	—
X	·	·	6	1.0	1.5	1.0	5	1.0	1.5	1.7	6.5	1.0	17	1.5	1.5	2.3	54	0.5	11	4.4	9	·	·	21	1	·	·	5	8	5	4	·	10	·	—
XI	1.5	1.0	3.5	1.3	6.5	1.3	6	2.7	2.5	3.0	6	1.9	17	2.0	1	5.0	46	1.0	53	12.2	11	5	10	23	·	5	·	3	15	13	10	1	5	11	—
XII	·	·	2.5	1.0	4	1.0	2.5	2.2	5	3.0	13	1.4	12	1.3	2	1.0	52	0.7	32	5.8	13	3	5	31	·	2	1	1	13	14	9	·	2	25	—
Rok	36	0.9	86.5	1.1	79.5	1.2	47.5	1.5	31.5	1.8	125	1.5	253	1.6	31	1.4	405	1.0	867	46.1	1.VIII	45	58	171	21	18	1	24	147	185	135	21	43	123	—

Brzegi Dolne $H_s = 420$ m $h_w = 17$ m

I	3.5	2.4	1	2.0	6	1.5	8	2.6	21	3.8	8	3.4	7.5	5.3	6	1.5	32	2.1	59	14.0	31	7	10	28	·	1	·	4	23	17	12	1	—	30	—
II	8	2.0	9	2.2	1	1.0	·	·	8.5	4.6	20.5	3.5	13	4.5	12	1.9	12	2.8	61	11.2	18	13	24	28	·	2	·	1	18	22	15	2	—	28	—
III	2	2.0	8	2.1	1	2.0	11	2.9	16	4.6	1	2.0	3	2.7	5	1.8	46	1.6	37	9.0	3	5	5	24	·	1	·	4	13	12	8	·	—	17	—
IV	2	2.0	12.5	2.3	15.5	3.5	4	2.0	4	2.5	7	4.6	3	2.7	5	1.6	37	1.7	41	9.8	30	·	·	19	·	·	·	·	15	12	7	·	1	1	—
V	7.5	1.9	2.5	2.6	3.5	3.0	3.5	1.9	10.5	2.7	8.5	6.4	8	3.5	8	2.1	41	1.8	81	14.6	10	·	·	8	1	1	1	1	14	18	14	3	—	·	—
VI	3	1.3	4.5	1.8	2.5	2.8	5	2.8	3.5	2.6	6.5	3.1	10	3.0	12	2.8	43	1.4	228	59.4	9	·	·	·	5	·	·	4	9	15	14	7	—	·	—
VII	2.5	2.2	2	2.0	3	1.3	1.5	4.0	8.5	2.8	15	2.1	13	2.0	5.5	2.0	42	1.2	182	20.5	2	·	·	·	6	·	·	4	10	21	19	9	—	·	—
VIII	6	2.0	4	2.0	1	1.0	1	4.0	9	2.7	10.5	2.3	9.5	3.2	5	1.9	47	1.2	200	48.7	26	·	·	·	4	·	·	6	12	13	13	7	—	·	—
IX	2	2.0	3	1.3	·	·	13	2.4	13	2.4	3.5	2.3	3.5	2.3	3	2.3	49	1.0	50	19.2	11	·	·	2	3	·	·	8	8	7	5	2	3	·	—
X	6	2.2	3.5	2.0	2.5	2.2	·	·	5	2.6	7.5	3.3	10.5	2.7	7	2.3	51	1.2	12	4.5	10	·	·	19	·	·	·	6	12	8	4	·	8	·	—
XI	1	2.0	10.5	2.1	4	5.0	4	1.8	11	5.7	18.5	3.5	12	2.5	3	2.7	26	2.4	60	22.0	11	3	8	24	·	3	·	1	21	14	12	1	—	13	—
XII	1	2.0	1.5	1.3	3.5	1.7	9.5	4.1	26.5	3.8	21	4.3	5	2.1	4	2.0	21	2.8	57	11.5	11	3	7	24	·	3	·	1	19	17	12	1	—	15	—
Rok	44.5	2.0	62	2.0	43.5	2.1	60.5	2.4	136.5	3.4	127.5	3.4	98	3.0	75.5	2.1	447	1.8	1068	59.4	9.VI	31	54	176	19	11	1	40	174	176	135	33	—	104	—

Czorsztyn $H_s = 496$ m $h_w = 18,4$ m

I	·	·	0.5	2.0	5	3.7	1.5	5.7	2	4.0	·	·	2	3.5	12	6.0	70	1.2	51	10.7	31	16	12	30	·	2	·	2	17	14	13	1	1	31	—
II	1	4.0	2	2.5	1	3.0	·	·	·	·	·	·	11.5	3.9	23.5	4.4	45	1.9	46	6.5	7	17	23	28	·	·	·	2	10	21	13	·	·	28	—
III	1	2.0	0.5	5.0	3.5	3.3	7.5	8.0	0.5	10.0	·	·	2.5	2.6	14.5	4.7	63	1.7	41	8.6	31	9	2	27	·	3	·	·	10	20	11	·	8	27	—
IV	·	·	8	3.9	12	3.3	6.5	5.0	2.5	6.6	·	·	1.5	8.3	17.5	4.8	42	2.4	32	9.3	22	·	·	12	·	1	·	3	16	16	8	·	·	1	—
V	1	3.0	3	3.3	5.5	2.8	6	3.4	0.5	2.0	0.5	3.0	7	4.6	17.5	4.5	52	1.7	120	24.7	16	·	·	6	1	1	1	2	18	22	15	2	2	·	—
VI	1	2.0	·	·	9.5	3.4	7.5	4.1	3	3.3	1	2.0	11	3.6	16	3.9	41	2.0	194	49.9	10	·	·	·	5	·	·	1	10	16	15	6	2	·	—
VII	·	·	0.5	4.0	3	3.2	4.5	4.6	·	·	·	·	4	3.8	17	3.4	64	1.1	113	21.4	2	·	·	·	5	1	·	1	8	21	16	3	1	·	—
VIII	0.5	2.0	2	1.5	10	3.3	4	3.2	5	4.6	1	3.0	5.5	3.5	10	2.9	55	1.3	155	42.8	1	·	·	·	3	1	·	3	13	15	13	4	8[2]	·	—
IX	·	·	1.5	2.7	5	5.9	15	5.4	4.5	6.4	1	4.0	3	3.0	7	4.1	53	2.1	66	25.6	11	·	·	·	·	3	·	·	6	13	8	2	11	·	—
X	0.5	3.0	1.5	2.3	9	2.3	·	·	·	·	·	·	3.5	3.4	7.5	2.4	71	0.6	16	4.3	31	·	·	21	·	·	·	·	8	10	5	·	20	·	—
XI	2	2.5	4	2.8	8	4.0	8.5	4.7	0.5	10.0	·	·	6.5	5.5	8.5	4.2	52	1.8	34	16.5	11	5	10	23	·	2	·	3	13	15	8	1	·	9	—
XII	·	·	1	3.0	2.5	3.2	6	4.0	0.5	4.0	·	·	3	6.3	7	3.4	73	0.8	36	6.5	15	12	8	30	·	1	·	1	13	18	9	·	·	29	—
Rok	7	1.5	24.5	2.8	74	3.4	67	4.0	19	4.2	3.5	1.0	61	4.2	158	4.1	681	1.6	904	49.9	10.VI	59	55	177	14	15	1	18	142	201	134	19	53[2]	125	—

Czorsztyn-Nadzamcze $H_s = 650$ m $h_w =$ 16,6 m I–VII; 19,2 m VIII–XII

I	3	1.0	17	1.4	15	3.6	5	4.6	·	·	·	·	21	6.8	9	2.3	23	2.9	20[2]	3.2	3	9	16	30	·	7	1	2	12	13	8	·	2	31	·
II	4	1.0	2	1.5	3	2.7	1	2.0	·	·	6	15.2	52	5.9	5	6.2	11	5.3	44	6.2	16	18	25	28	·	13	4	2	13	17	14	·	·	28	·
III	4	1.2	15	1.6	17	2.4	7	11.1	·	·	2	1.5	12	6.5	19	2.8	17	3.0	39	10.8	31	6	7	26	·	7	4	3	11	16	12	1	12	30	·
IV	5	2.0	21	3.2	16	2.8	7	11.0	·	·	1	14.0	13	8.1	12	3.8	15	4.0	32	9.8	22	·	1	8	·	13	4	1	11	14	7	·	5	2	2
V	5	3.4	7	1.4	12	3.7	4	3.5	·	·	4	10.0	17	4.0	29	2.7	15	2.9	109	15.7	16	·	·	6	·	12	1	1	11	21	15	3	5	·	5
VI	1	2.0	18	1.9	9	1.4	6	13.3	1	1.0	5	9.6	18	5.8	17	3.2	15	3.7	188	46.7	10	·	·	·	4	12	3	4	8	16	15	7	6	·	5
VII	2	1.0	15	1.7	7	1.7	5	5.0	1	1.0	5	6.8	21	6.0	13	2.4	24	2.5	103	22.6	1	·	·	·	3	8	1	2	6	19	16	2	4	·	6
VIII	2	2.5	·	·	17	1.6	13	7.7	8	1.4	11	2.7	13	5.3	5	3.2	24	2.8	140	32.0	1	·	·	·	3	11	1	5	7	14	13	4	5	·	2
IX	1	1.0	2	2.0	19	4.1	21	13.3	8	1.0	2	1.0	12	3.9	2	2.0	23	4.7	61	25.2	11	·	·	·	·	14	5	3	2	7	7	2	13	·	·
X	4	1.0	4	2.8	11	1.5	4	1.0	12	1.0	5	3.0	15	5.1	2	1.5	36	1.5	11	3.6	31	·	·	18	·	4	·	5	4	5	5	·	13	·	·
XI	1	2.0	1	2.0	15	1.9	10	6.1	7	1.0	12	14.4	16	5.1	·	·	28	3.6	38	9.7	11	6	10	25	·	10	4	5	11	9	8	·	2	10	·
XII	1	1.0	·	·	19	1.9	8	8.5	13	2.0	15	5.3	13	4.3	1	4.0	23	2.9	32	7.8	18	2	15	31	·	9	3	2	5	10	8	·	3	31	·
Rok	33	1.6	102	1.6	160	2.4	91	7.3	50	0.7	68	6.9	223	5.5	114	2.8	254	3.3	817	46.7	10.VI	41	74	172	10	120	31	35	101	161	128	19	70	132	20

Szczawnica

$\varphi = 49°26'$ $\lambda = 20°29'$ **1965**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o,m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	1.8	−6.0	7.6	30	−12.0	8	−3.9	−0.2	−2.8	−2.4	4.3	5.3	4.7	4.8	90	86	90	89	0.4	0.9	0.5	0.6	8.1	7.4	7.3	7.6
II	—	—	—	—	−2.5	−11.8	4.0	14	−25.0	7	−9.3	−4.2	−8.1	−7.4	2.8	3.6	3.1	3.2	86	79	86	84	0.4	1.0	0.4	0.6	8.5	7.1	7.6	7.7
III	—	—	—	—	6.0	−4.2	15.5	30	−15.4	11	−2.6	4.4	0.1	0.5	5.1	6.4	5.9	5.8	90	75	92	86	0.5	2.4	0.6	1.2	7.5	6.1	6.7	6.8
IV	—	—	—	—	11.2	1.3	17.6	7	−3.3	2	3.1	9.3	5.2	5.7	6.9	7.8	7.4	7.4	90	67	83	80	0.9	4.2	1.5	2.2	7.7	7.8	6.6	7.4
V	—	—	—	—	15.3	5.1	25.8	19	−4.6	3	7.4	13.5	9.1	9.8	9.1	9.4	9.9	9.5	88	61	83	77	1.4	6.6	1.9	3.3	7.5	8.0	7.4	7.6
VI	—	—	—	—	21.2	9.5	30.5	26	1.5	3	12.8	19.5	14.1	15.1	13.0	13.1	13.5	13.2	87	59	83	76	2.0	10.4	2.9	5.1	5.3	6.0	5.8	5.7
VII	—	—	—	—	21.0	10.3	29.0	15	4.1	10	13.0	19.1	14.4	15.2	13.9	14.4	14.6	14.3	92	67	88	82	1.2	8.5	2.0	3.9	6.1	7.5	4.9	6.2
VIII	—	—	—	—	19.7	9.1	28.7	7	3.2	31	11.0	17.9	12.9	13.7	12.1	12.5	12.9	12.5	92	63	86	80	1.3	9.0	2.3	4.2	6.5	7.1	4.6	6.1
IX	—	—	—	—	19.4	8.2	24.8	3	1.5	22	10.7	18.0	12.3	13.3	11.5	12.6	12.2	12.1	89	62	86	79	2.0	8.4	2.4	4.3	6.5	4.7	3.3	4.8
X	—	—	—	—	12.6	0.5	23.1	2	−7.8	22	1.7	11.0	4.4	5.4	7.0	8.9	8.1	8.0	96	66	92	85	0.3	4.7	0.6	1.9	7.2	3.8	4.2	5.1
XI	—	—	—	—	3.2	−3.9	13.3	2	−15.2	25	−2.3	1.6	−1.5	−0.9	4.9	5.4	5.2	5.2	89	77	91	86	0.6	1.9	0.5	1.0	7.7	6.5	5.9	6.7
XII	—	—	—	—	2.3	−4.3	6.6	10	−13.4	15	−2.4	0.7	−1.4	−1.1	4.8	5.4	5.1	5.1	91	84	91	89	0.4	1.1	0.5	0.7	7.5	7.1	6.1	6.9
Rok	—	—	—	—	10.9	1.2	30.5	26.VI	−25.0	7. II	3.3	9.2	4.9	5.6	8.0	8.7	8.6	8.4	90	70	88	83	1.0	4.9	1.3	2.4	7.2	6.6	5.9	6.6

Piwniczna

$\varphi = 49°26'$ $\lambda = 20°42'$

I	—	—	—	—	0.7	−6.1	5.5	30	−15.5	8	−3.6	−0.2	−2.6	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	9.0	7.9	8.0	8.3
II	—	—	—	—	−2.4	−11.0	4.0	14	−24.7	7, 10	−8.8	−3.7	−7.1	−6.7	—	—	—	—	—	—	—	—	—	—	—	—	8.5	6.9	7.1	7.5
III	—	—	—	—	6.0	−4.0	15.9	30	−18.7	1	−2.1	4.5	0.0	0.6	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.9	7.0	7.3
IV	—	—	—	—	11.4	1.8	15.7	7	−2.3	6	3.8	9.8	5.4	6.1	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.1	6.7	7.7
V	—	—	—	—	15.4	5.6	26.3	18	−3.3	3	8.3	13.7	9.5	10.2	—	—	—	—	—	—	—	—	—	—	—	—	7.5	8.3	7.0	7.6
VI	—	—	—	—	21.5	9.8	31.1	26	2.8	3	14.0	19.8	14.1	15.5	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.4	5.5	5.9
VII	—	—	—	—	21.7	10.6	29.3	15	4.7	10	14.3	19.7	14.3	15.6	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.6	4.7	6.3
VIII	—	—	—	—	20.0	9.5	29.6	8	4.5	3	11.7	18.2	12.5	13.7	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.4	5.5	6.6
IX	—	—	—	—	20.2	8.2	25.3	11	3.1	22	11.0	18.8	11.6	13.2	—	—	—	—	—	—	—	—	—	—	—	—	8.0	5.1	3.6	5.6
X	—	—	—	—	12.8	1.1	23.1	2	−6.4	22	2.8	11.8	4.5	5.9	—	—	—	—	—	—	—	—	—	—	—	—	7.7	4.5	4.6	5.6
XI	—	—	—	—	3.5	−3.2	14.3	2	−14.3	25	−1.7	2.0	−0.6	−0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.2	7.4	7.5
XII	—	—	—	—	1.9	−3.9	7.3	6	−14.3	15	−2.0	0.9	−1.1	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.4	7.6	7.5
Rok	—	—	—	—	11.1	1.5	31.1	26.VI	−24.7	7.10. II	4.0	9.6	5.0	5.9	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.9	6.2	6.9

Krynica

$\varphi = 49°26'$ $\lambda = 20°58'$

I	—	—	—	—	−0.4	−6.3	4.8	30	−16.7	8	−4.3	−1.6	−3.7	−3.3	4.1	4.5	4.3	4.3	89	82	89	87	0.5	1.0	0.5	0.7	8.9	8.1	8.0	8.3
II	—	—	—	—	−3.7	−11.5	2.0	12	−22.8	7	−10.0	−5.8	−8.6	−8.2	2.7	3.0	2.6	2.8	88	74	83	82	0.3	1.1	0.5	0.6	8.5	7.1	7.7	7.8
III	—	—	—	—	4.7	−4.1	13.3	30	−16.8	1	−2.5	2.8	−0.7	−0.3	4.9	5.3	5.1	5.1	91	79	84	82	0.5	2.5	1.0	1.3	7.9	7.0	6.8	7.2
IV	—	—	—	—	9.4	0.4	13.2	7	−5.0	2	2.2	7.7	3.8	4.4	6.6	6.8	6.8	6.7	90	66	84	80	0.7	4.0	1.3	2.0	7.9	8.2	5.6	7.2
V	—	—	—	—	13.4	4.7	23.5	19	−4.3	4	6.6	11.6	8.2	8.6	8.6	8.6	9.3	8.8	86	62	82	77	1.6	5.6	1.9	3.0	7.5	8.7	6.6	7.6
VI	—	—	—	—	19.7	9.0	28.6	26	2.0	3	12.2	18.0	13.4	14.2	12.4	11.7	12.9	12.3	86	58	83	76	2.0	9.7	2.8	4.8	4.9	6.5	6.9	6.1
VII	—	—	—	—	19.9	9.8	26.8	15	3.9	10	12.6	18.1	13.7	14.5	13.3	13.5	13.8	13.5	90	66	87	81	1.5	8.0	2.1	3.9	5.8	8.0	5.5	6.4
VIII	—	—	—	—	18.0	8.5	27.3	8	2.8	3	10.3	16.5	11.8	12.6	11.8	11.7	12.1	11.9	93	64	87	81	1.0	7.9	2.1	3.7	5.9	6.9	5.2	6.0
IX	—	—	—	—	18.5	7.3	23.0	3	0.0	22	9.5	17.1	11.1	12.2	11.0	11.6	11.6	11.4	91	60	87	79	1.2	8.3	1.9	3.8	6.4	5.4	3.1	5.0
X	—	—	—	—	11.8	0.4	23.0	2	−7.5	22	1.6	10.3	4.1	5.0	6.8	7.9	7.6	7.4	94	62	89	82	0.4	5.3	1.0	2.2	6.9	4.3	4.4	5.2
XI	—	—	—	—	1.9	−4.3	12.7	2	−15.4	25	−3.1	0.4	−1.9	−1.6	4.6	4.9	4.7	4.7	90	75	85	84	0.5	1.8	0.9	1.1	7.8	7.2	7.7	7.6
XII	—	—	—	—	0.3	−4.8	4.5	10	−14.0	13	−3.4	−0.8	−2.5	−2.3	4.4	4.7	4.5	4.5	91	81	87	85	0.5	1.2	0.7	0.8	8.1	7.5	8.1	7.9
Rok	—	—	—	—	9.5	0.8	28.6	26.VI	−22.8	7. II	2.6	7.9	4.1	4.7	7.6	7.8	8.0	7.8	90	68	86	81	0.9	4.7	1.4	2.3	7.2	7.1	6.3	6.9

Krynica - Góra Parkowa

$\varphi = 49°25'$ $\lambda = 20°58'$

I	—	—	—	—	−1.7	−6.4	3.0	30	−14.1	8	−4.5	−2.6	−4.2	−3.9	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.9	8.0	8.3
II	—	—	—	—	−5.0	−11.4	−0.2	1	−19.0	7	−10.1	−6.2	−8.9	−8.5	—	—	—	—	—	—	—	—	—	—	—	—	8.8	7.2	7.4	7.8
III	—	—	—	—	3.3	−3.9	11.6	30	−12.7	1	−2.6	1.7	−0.9	−0.7	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.0	6.6	7.3
IV	—	—	—	—	8.5	0.5	12.4	4, 19	−5.3	1	2.3	6.5	3.5	4.0	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.3	6.3	7.6
V	—	—	—	—	12.9	4.4	22.5	19	−3.3	3	6.5	10.9	7.2	8.0	—	—	—	—	—	—	—	—	—	—	—	—	7.7	8.4	7.3	7.8
VI	—	—	—	—	19.1	9.3	27.8	26	3.4	3	12.2	17.1	12.9	13.8	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.9	7.3	6.6
VII	—	—	—	—	19.1	10.2	26.1	15	5.0	10	12.9	17.2	13.4	14.2	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.8	5.5	6.4
VIII	—	—	—	—	17.3	9.0	25.7	8	4.7	3, 14	11.1	15.7	12.1	12.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.4	5.1	6.3
IX	—	—	—	—	17.7	8.1	21.7	2	3.3	22	10.2	16.3	11.6	12.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	5.7	3.2	5.2
X	—	—	—	—	10.9	1.8	21.6	2	−5.3	22	2.7	9.8	4.7	5.5	—	—	—	—	—	—	—	—	—	—	—	—	6.6	4.5	4.6	5.2
XI	—	—	—	—	1.0	−4.6	12.2	2	−12.9	25	−3.4	−0.5	−2.4	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.5	7.8	7.7
XII	—	—	—	—	−0.9	−4.9	2.9	10	−11.9	15	−3.6	−1.8	−3.2	−3.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.9	7.7	8.0
Rok	—	—	—	—	8.5	1.0	27.8	26.VI	−19.0	7. II	2.8	7.0	3.8	4.4	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.2	6.4	7.0

Szczawnica

$H_s = 500$ m $h_w = 22{,}3$ m **1965**

MIESIĄC	ROZKŁAD WIATRU *D V=D N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max≥25°	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥5.0	≥10.0	≡	⊠	K ⊗
I	6	1.8	1	2.0	31	2.4	8	3.1	1	2.0	3	2.3	7	2.9	22	2.0	14	2.0	55	12.7	31	6	10	29	·	1	·	·	18	16	11	2	·	31	·
II	6	1.8	1	1.0	2	1.5	2	2.0	·	·	2	1.5	8	2.5	56	2.4	7	2.1	87	11.5	16	16	21	28	·	·	·	1	15	22	15	2	·	28	·
III	19	2.0	1	2.0	16.5	2.1	17.5	3.5	4	1.8	·	·	2	4.0	22	2.5	11	2.2	38	6.6	17	5	3	21	·	1	·	2	11	15	11	·	6	18	·
IV	8.5	3.2	6.5	1.8	14	2.2	13	2.2	4	2.0	·	·	6	2.8	27	2.6	11	2.1	36	10.8	22	·	·	9	·	·	·	1	15	18	9	1	1	1	2
V	7	2.0	5	1.8	13	1.6	8	4.8	4	2.5	2	2.5	9	1.6	33	2.0	12	1.9	87	9.4	6	·	·	6	2	1	1	·	16	23	17	·	2	·	4
VI	17	1.9	7	1.4	9	2.6	8	4.2	4	5.0	1	1.0	8	2.0	31	2.6	5	2.4	209	50.5	10	·	·	·	5	1	·	2	10	15	15	8	2	·	3
VII	8	2.0	1.5	2.0	10	2.3	6.5	1.8	9	2.1	6	1.8	8.5	2.9	31.5	2.0	12	1.8	104	16.1	8	·	·	·	7	1	·	1	9	20	15	3	1	·	6
VIII	17	2.2	2	1.0	12.5	2.2	13.5	3.0	2	1.0	2	1.0	13	1.9	23	2.1	8	2.0	134	35.1	1	·	·	·	3	·	·	3	12	14	11	5	2	·	2
IX	2.5	1.0	2	1.5	23	2.6	30	2.9	6	4.5	·	·	2	1.0	19.5	1.8	5	2.4	59	22.3	29	·	·	·	·	·	·	5	5	9	6	2	8	·	1
X	20.5	1.6	4.5	1.8	25	1.5	8	1.6	1	3.0	2	2.0	6	2.3	14	2.5	12	1.6	70	3.0	31	·	·	17	·	·	·	4	6	7	4	·	14	·	·
XI	26	1.9	5	1.0	20	1.8	6	6.3	1	12.0	·	·	10	4.0	8	2.2	14	2.2	30	12.9	11	2	10	23	·	4	·	3	14	14	7	1	2	12	·
XII	8	1.8	·	·	28.5	2.3	11.5	3.8	5	1.4	3	2.0	5.5	2.2	21.5	2.0	10	2.1	39	7.1	15	2	5	26	·	2	1	3	12	17	10	·	1	21	·
Rok	145.5	1.9	36.5	1.4	204.5	2.1	132	3.3	41	3.1	21	1.2	85	2.5	308.5	2.2	121	2.1	888	50.5	10.VI	31	49	159	17	11	2	25	143	190	131	24	39	111	18

Piwniczna

$H_s = 380$ m $h_w = 17{,}4$ m

I	·	·	·	·	9	2.9	24	2.9	3	1.3	1	1.0	27	2.4	·	·	29	1.8	44	10.2	31	7	9	29	·	·	·	1	20	15	7	1	1	31	·
II	·	·	·	·	5	3.0	3	3.7	·	·	4	2.8	45	2.8	3	5.3	24	2.1	62	8.4	8	14	22	28	·	·	·	1	13	18	16	·	4	28	·
III	·	·	·	·	6	4.0	13	2.8	3	1.7	2	2.5	37	2.2	1	2.0	31	1.7	51	7.8	17	5	5	22	·	·	·	2	13	17	13	·	5	17	·
IV	·	·	1	1.0	2	2.0	17	2.2	7	1.9	8	1.9	25	2.3	2	3.5	28	1.5	46	9.5	26	·	·	8	·	·	·	1	16	15	11	·	3	1	1
V	·	·	2	2.0	3	2.0	6	3.0	4	2.8	9	2.0	39	2.2	·	·	30	1.5	76	9.2	6	·	·	2	2	·	·	1	15	22	17	·	5	·	4
VI	·	·	·	·	11	2.7	5	1.8	5	2.2	15	2.5	21	2.3	1	3.0	32	1.5	201	43.1	10	·	·	·	7	·	·	3	9	16	14	8	2	·	5
VII	·	·	1	2.0	4	2.2	12	1.9	4	1.8	5	2.0	23	1.8	1	4.0	43	1.0	122	16.4	8	·	·	·	7	·	·	3	6	21	16	6	5	·	8
VIII	·	·	1	1.0	1	3.0	8	2.2	5	1.4	5	1.2	31	1.9	2	1.5	40	1.0	180	43.0	26	·	·	·	5	·	·	2	12	17	12	5	8	·	2
IX	·	·	·	·	1	3.0	26	2.6	3	1.7	8	2.0	8	1.5	1	3.0	43	1.2	51	15.0	11	·	·	·	1	·	·	2	6	10	6	3	11	·	·
X	·	·	1	2.0	3	1.3	6	2.0	1	1.0	5	2.2	34	1.5	1	1.0	42	0.9	11	2.4	9, 31	·	·	16	·	·	·	5	8	7	5	·	11	·	·
XI	·	·	·	·	5	3.0	20	3.6	1	2.0	1	2.0	28	1.7	3	2.3	32	1.6	50	16.5	11	3	10	21	·	1	·	2	17	16	10	1	2	11	·
XII	·	·	·	·	13	2.7	25	2.6	1	3.0	6	1.8	21	1.7	1	2.0	26	1.6	44	8.2	18	2	7	26	·	·	·	2	17	15	11	·	1	22	·
Rok	·	·	6	0.7	63	2.6	165	2.6	37	1.7	69	2.0	339	2.0	16	2.3	400	1.4	938	43.1	10.VI	31	53	152	22	1	·	25	152	189	138	24	58	110	20

Krynica

$H_s = 613$ m $h_w = 18$ m

I	2.5	1.8	1.5	1.0	0.5	3.0	14.5	3.2	27.5	3.1	8.5	3.2	6	5.2	15	3.8	17	2.7	56	7.3	31	6	19	29	·	·	·	1	23	17	13	·	3	31	·
II	14.5	4.1	·	·	·	·	7.5	2.7	3.5	3.6	3	2.3	12	5.3	25.5	3.7	18	3.1	82	11.5	8	16	24	28	·	·	·	1	17	20	16	1	1	28	·
III	6.5	1.8	1.5	1.7	2	3.2	12.5	2.4	17.5	3.1	9	3.8	5	3.4	20	2.5	19	2.2	60	10.2	31	4	6	20	·	·	·	2	15	17	15	1	7	23	·
IV	8.5	2.8	2	2.0	1	3.0	13.5	3.0	10.5	2.2	10.5	2.4	5	4.4	13	3.5	26	2.1	60	14.1	26	·	·	12	·	·	·	2	14	14	10	2	3	3	2
V	12.5	2.3	1	2.0	·	·	8	2.2	10.5	3.0	14.5	2.5	6	3.7	24.5	3.1	16	2.3	86	12.2	15	·	·	4	·	·	·	·	17	23	17	2	7	·	5
VI	11	2.2	3	1.0	2.5	2.6	15.5	2.9	20	3.2	4	2.2	6	3.0	16	3.6	12	2.5	190	56.0	10	·	·	·	3	·	·	3	11	16	13	7	·	·	4
VII	14	1.9	0.5	3.0	0.5	3.0	10	3.1	15	3.4	9.5	2.7	4.5	5.0	6	2.7	33	1.9	174	34.9	25	·	·	·	6	·	·	1	6	20	16	7	2	·	8
VIII	8.5	3.8	2	2.0	·	·	6.5	2.4	12.5	3.3	5	3.0	10.5	4.3	15	3.7	33	2.3	160	42.5	1	·	·	·	3	·	·	5	12	15	11	4	3	·	3
IX	5.5	2.5	2	3.0	2	2.0	9.5	3.5	24	3.4	8.5	4.4	1.5	3.0	8	2.6	29	2.3	43	19.4	11	·	·	·	·	·	·	5	5	9	5	2	5	·	·
X	16	2.3	3.5	2.4	0.5	3.0	4.5	1.7	12	2.2	4.5	2.8	3	3.3	18	2.6	31	1.6	14	4.2	11	·	·	17	·	·	·	6	8	8	5	·	10	·	·
XI	7	2.1	1	1.0	1	3.0	18.5	2.5	19.5	3.6	5.5	4.5	6.5	4.2	20	2.6	11	2.7	54	18.8	11	5	12	23	·	3	·	2	18	18	11	1	7	19	·
XII	5	1.8	3	1.0	0.5	3.0	28.5	2.5	25	3.1	7	5.0	2	4.5	8	4.2	14	2.6	46	8.6	18	2	12	29	·	3	·	2	20	17	11	·	4	31	·
Rok	111.5	2.4	21	1.7	10.5	2.2	148	2.7	197.5	3.1	89.5	3.2	68	4.1	189	3.2	253	2.4	1025	56.0	10.VI	33	73	162	12	6	·	30	166	194	143	27	52	135	22

Krynica - Góra Parkowa

$H_s = 740$ m $h_w =$ 18,9 m I–VI; 19.2 m VII–XII

I	5.5	2.9	1	5.0	1	1.0	4	1.0	31	3.0	19.5	3.0	2	2.7	15	3.3	14	2.5	48	6.7	31	5	25	30	·	1	·	1	21	16	12	·	7	31	—
II	14.5	3.1	1.5	1.0	·	·	0.5	2.0	16	2.4	6.5	2.2	7.5	3.2	28.5	3.0	9	2.5	79	11.1	8	18	28	28	·	1	·	1	16	21	16	1	4	28	—
III	17.5	1.6	1	1.0	·	·	0.5	3.0	28	2.7	19.5	2.4	2.5	1.2	18	2.8	6	2.2	43	9.7	31	4	7	26	·	·	·	2	12	17	11	·	13	26	—
IV	13.5	2.0	4.5	1.9	2	1.0	10	1.6	19.5	2.4	12.5	2.4	4	1.5	13	2.7	11	1.9	49	13.3	26	·	1	10	·	·	·	·	13	15	8	1	5	2	—
V	21.5	2.4	5.5	2.5	1	1.0	1.5	1.3	33	1.8	2.5	1.2	4	1.5	23.5	1.9	10	1.6	71	13.3	27	·	·	4	·	1	·	1	15	23	14	1	5	·	—
VI	12	2.0	2	1.0	3	1.7	6.5	1.5	26	2.8	4.5	2.6	6	1.3	20	3.2	11	2.2	184	54.5	10	·	·	·	3	·	·	1	10	18	13	6	·	·	—
VII	8.5	1.8	4	2.1	·	·	1	2.0	37	2.2	14	2.0	3.5	2.7	13	2.0	12	1.8	172	37.7	25	·	·	·	3	·	·	2	6	20	16	6	3	·	—
VIII	13	2.1	2.5	1.4	2	1.2	4	2.9	26	2.3	2	2.8	6	1.8	22.5	2.9	15	2.0	165	44.2	1	·	·	·	1	·	·	4	10	17	12	4	4	·	—
IX	2	1.8	1.5	1.3	0.5	1.0	12	3.4	52	3.2	6	1.8	1	1.0	8	1.9	7	2.7	45	18.8	11	·	·	·	·	1	1	5	4	12	5	2	5	·	—
X	16.5	1.5	1	2.5	1	2.0	1.5	1.7	33	1.8	2.5	1.2	4	1.5	23.5	1.9	10	1.6	15	13.7	11	·	·	9	·	·	·	7	7	10	6	·	8	·	—
XI	4	2.5	·	·	·	·	7.5	5.2	32	3.8	6	3.8	3.5	3.6	28	2.0	9	2.9	58	27.0	11	6	12	25	·	3	1	3	21	18	12	1	8	19	—
XII	1.5	4.0	0.5	2.0	1	3.0	8	2.1	50	3.8	7.5	1.9	2	2.2	15.5	3.5	6	3.1	32	6.0	18	2	18	31	·	3	1	·	19	18	9	·	3	31	—
Rok	130	2.3	25	1.8	11.5	1.0	58	2.3	365.5	2.7	114	2.5	48	2.0	224	2.6	119	2.3	961	54.5	10.VI	35	91	163	7	10	3	27	154	205	134	22	65	127	—

Wysowa — φ = 49°26' — λ = 21°11' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−1.7	−6.7	2.4	29	−17.2	8	−4.1	−2.7	−3.7	−3.6	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.4	8.1	8.5
II	—	—	—	—	−5.2	−13.7	0.2	1	−27.4	7	−10.6	−6.2	−9.3	−8.8	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.6	7.2	7.6
III	—	—	—	—	3.5	−5.0	13.7	30	−20.0	11	−1.9	2.1	−0.8	−0.4	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.2	6.5	7.1
IV	—	—	—	—	9.8	0.3	13.8	19	−4.8	6	3.4	8.3	3.7	4.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.8	5.4	7.1
V	—	—	—	—	13.8	4.1	24.3	19	−6.6	4	7.6	12.1	7.9	8.9	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.9	7.0	7.4
VI	—	—	—	—	19.7	8.5	26.9	26	0.5	3	13.6	18.1	12.8	14.3	—	—	—	—	—	—	—	—	—	—	—	—	4.9	6.1	6.3	5.8
VII	—	—	—	—	20.1	8.8	27.1	15	2.5	10	14.0	18.1	12.9	14.5	—	—	—	—	—	—	—	—	—	—	—	—	5.7	8.3	5.5	6.5
VIII	—	—	—	—	17.9	7.8	26.8	8	1.5	31	11.3	16.5	11.2	12.6	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.6	5.4	6.1
IX	—	—	—	—	17.7	7.2	22.2	11	−0.5	22	10.6	15.6	10.6	12.1	—	—	—	—	—	—	—	—	—	—	—	—	6.2	5.3	4.4	5.3
X	—	—	—	—	10.4	0.1	20.5	2	−9.0	22	2.7	9.5	3.8	4.9	—	—	—	—	—	—	—	—	—	—	—	—	6.7	4.7	4.3	5.2
XI	—	—	—	—	1.1	−4.5	12.6	2	−15.2	25	−2.8	0.0	−1.9	−1.6	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.5	7.8	7.9
XII	—	—	—	—	−0.4	−5.0	4.8	10	−16.1	16	−3.5	−1.5	−2.3	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	8.6	8.7	8.5
Rok	—	—	—	—	8.9	0.2	27.1	15. VII	−27.4	7. II	3.4	7.6	3.7	4.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.2	6.4	6.9

Barwinek — φ = 49°26' — λ = 21°41'

I	—	—	—	—	−0.9	−6.6	3.0	31	−18.3	11	−3.7	−2.0	−3.5	−3.2	—	—	—	—	—	—	—	—	—	—	—	—	9.4	8.8	8.8	9.0
II	—	—	—	—	−5.1	−14.0	0.4	1	−28.6	7, 8	−10.2	−6.2	−9.5	−8.8	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.4	7.3	8.2
III	—	—	—	—	4.2	−5.5	15.1	30	−21.1	11	−1.9	2.8	−1.0	−0.3	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.5	6.9	7.3
IV	—	—	—	—	10.3	−0.4	13.3	20	−5.4	6	3.3	8.8	2.7	4.4	—	—	—	—	—	—	—	—	—	—	—	—	9.2	7.6	5.9	7.6
V	—	—	—	—	14.0	3.9	24.1	19	−7.2	4	7.6	12.4	8.4	9.2	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.4	7.6	7.5
VI	—	—	—	—	19.5	7.9	27.7	26	0.7	3	13.3	18.0	12.1	13.9	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.8	6.4	6.2
VII	—	—	—	—	20.0	9.1	26.9	15	2.4	12	14.2	18.3	12.9	14.6	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.1	6.3	6.4
VIII	—	—	—	—	—	8.3	25.7	8	4.2	29	12.4	17.2	11.3	13.0	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.1	5.8	6.3
IX	—	—	—	—	18.3	7.2	23.1	2	−0.2	22	11.3	17.3	11.3	12.8	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.4	3.5	5.0
X	—	—	—	—	10.8	−0.1	21.9	2	−9.0	22	3.2	10.0	4.5	5.6	—	—	—	—	—	—	—	—	—	—	—	—	6.8	5.3	5.0	5.7
XI	—	—	—	—	1.7	−4.4	11.9	2	−16.8	17	−2.1	0.0	−1.5	−1.3	—	—	—	—	—	—	—	—	—	—	—	—	9.1	8.5	8.9	8.8
XII	—	—	—	—	0.4	−4.3	5.5	11	−17.3	15	−2.6	−1.0	−1.8	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	8.8	9.5	9.1	9.1
Rok	—	—	—	—	—	0.1	27.7	26. VI	−28.6	7, 8. II	3.7	8.0	3.8	4.8	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.4	6.8	7.3

Myczkowce — φ = 49°26' — λ = 22°25'

I	—	—	—	—	1.6	−5.8	6.7	31	−20.2	12	−2.8	0.4	−1.8	−1.5	—	—	—	—	—	—	—	—	—	—	—	—	8.0	8.0	7.1	7.7
II	—	—	—	—	−3.7	−11.1	1.3	12	−25.0	7	−8.3	−4.8	−7.4	−7.0	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.6	8.1	7.9
III	—	—	—	—	6.1	−3.4	14.8	30	−21.9	1	0.8[2]	5.0	1.1	2.0[2]	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.4	5.5	6.3
IV	—	—	—	—	11.2	1.8	16.4	26	−3.8	6	5.6[2]	9.7	5.3	6.5[2]	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.6	8.3	7.8
V	—	—	—	—	15.1	5.5	25.7	19	−3.9	4	9.7[2]	13.2	9.2	10.3[2]	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.5	7.2	7.2
VI	—	—	—	—	20.9	10.0	30.4	26	4.6	3, 8	15.5[2]	19.2	14.0	15.7[2]	—	—	—	—	—	—	—	—	—	—	—	—	5.7	7.5	6.6	6.6
VII	—	—	—	—	21.4	11.4	28.1	16	6.2	7	16.4[2]	19.8	15.0	16.6[2]	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.7	6.9	6.5
VIII	—	—	—	—	19.6	9.1	28.9	8	4.1	31	14.0[2]	17.7	12.6	14.2[2]	—	—	—	—	—	—	—	—	—	—	—	—	5.6	6.8	5.0	5.8
IX	—	—	—	—	20.5	8.1	27.1	2	3.1	17	12.9[2]	19.0	12.0	14.0[2]	—	—	—	—	—	—	—	—	—	—	—	—	5.0	5.3	3.1	4.5
X	—	—	—	—	12.4	1.3	25.2	2	−5.3	23	5.2[2]	11.1	5.1	6.6[2]	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.8	4.3	5.3
XI	—	—	—	—	4.1	−3.6	14.5	2	−18.5	18	−1.2	2.4	−0.5	0.0	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.7	8.2	7.8
XII	—	—	—	—	3.3	−2.4	8.6	10	−12.9	17	−0.6	2.0	0.3	0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.5	8.5	8.5
Rok	—	—	—	—	11.0	1.7	30.4	26. VI	−25.0	7. II	5.6[2]	9.6	5.4	6.5[2]	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.1	6.6	6.8

Jaworzyna Krynicka — φ = 49°25' — λ = 20°54'

I	—	—	—	—	−3.1	−6.6	2.9	31	−12.7	8	−5.3	−4.3	−4.7	−4.8	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.2	8.3	8.5
II	—	—	—	—	−7.5	−12.8	−2.2	1	−21.2	6	−11.1	−8.8	−10.3	−10.1	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.9	8.9	8.6
III	—	—	—	—	1.3	−4.9	9.0	30	−13.1	1	−3.3	0.0	−2.2	−1.9	—	—	—	—	—	—	—	—	—	—	—	—	7.6	6.7	6.4	6.9
IV	—	—	—	—	5.6	0.4	10.1	7	−7.2	1	1.7	4.4	2.1	2.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	8.1	6.6	7.7
V	—	—	—	—	10.1	3.1	21.2	18, 19	−4.3	3	5.5	8.9	5.5	6.4	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.2	7.6	8.0
VI	—	—	—	—	16.4	8.6	26.7	26	5.3	18, 29	11.4	15.3	11.2	12.3	—	—	—	—	—	—	—	—	—	—	—	—	6.1	6.7	7.2	6.7
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	15.9	8.9	21.7	19	4.7	27	10.8	14.4	11.0	11.8	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.8	6.5	6.4
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Wysowa $H_s = 525$ m $h_w = 25.5$ m 1965

MIESIAC	ROZKŁAD WIATRU $n_D V_{mD}$ N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V V ≥ 10	V ≥ 15	◔	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	9	5.1	·	·	·	·	45.5	6.9	10	4.7	0.5	2.0	·	·	20	5.5	8	5.5	49	7.4	31	6	24	31	·	5	1	1	21	18	12	·	4	31	·
II	10.5	5.9	·	·	·	·	13.5	5.7	9.5	4.0	·	·	0.5	2.0	42	6.4	8	5.3	51	5.8	8	16	27	28	·	5	·	1	16	19	15	·	3	28	·
III	14	3.9	·	·	·	·	22.5	4.4	24.5	5.0	2	3.5	0.5	14.0	15.5	5.1	14	4.0	41	5.5	24	7	7	24	·	3	·	4	13	18	12	·	7	24	·
IV	4.5	3.6	5.5	3.3	3.5	3.3	17.5	3.9	12.5	3.1	4	2.5	4.5	4.1	20	4.8	18	3.1	56	16.7	26	·	·	12	·	1	·	1	11	16	10	2	2	1	1
V	12.5	4.6	·	·	1	3.0	15	3.7	9.5	4.3	5.5	4.4	2.5	3.4	28	4.2	19	3.3	84	10.8	18	·	·	8	·	1	·	1	15	24	17	2	1	·	3
VI	14	4.1	1	3.0	·	·	18.5	4.4	11.5	4.0	1	2.0	1	4.0	24	3.6	19	3.1	174	46.4	10	·	·	·	4	1	·	3	6	15	13	7	2	·	3
VII	6	3.1	0.5	3.0	0.5	3.0	10	4.6	9.5	3.9	2.5	4.0	0.5	4.0	11.5	3.3	52	1.7	143	31.0	21	·	·	·	3	1	·	3	6	19	18	6	·	·	4
VIII	11.5	3.1	·	·	1	2.0	16	4.3	15	2.6	2	2.5	1	3.0	23.5	3.5	23	2.5	142	35.1	1	·	·	·	2	2	·	6	11	18	15	5	·	·	2
IX	6	3.0	·	·	·	·	34.5	4.8	21.5	4.3	·	·	0.5	2.0	10.5	3.0	17	3.4	39	18.9	11	·	·	1	·	·	·	5	7	11	5	1	2	·	·
X	13	3.5	2.5	2.4	1	1.5	18.5	3.9	12	2.2	0.5	3.0	2	2.8	23.5	3.4	20	2.6	11	2.9	31	·	·	13	·	·	·	8	9	8	4	·	8	·	·
XI	15.5	3.9	0.5	2.0	0.5	2.0	24	5.5	21	4.8	·	·	2.5	3.6	20	3.7	6	4.2	56	22.1	11	5	12	27	·	3	·	3	18	19	10	1	7	12	·
XII	8	4.3	·	·	·	·	34	4.7	32	4.5	·	·	0.5	3.0	10.5	4.0	6	4.1	40	9.3	18	4	18	30	·	4	·	2	21	19	10	·	6	31	·
Rok	124.5	4.0	10	1.1	7.5	1.2	269.5	4.7	188.5	4.0	18	2.0	16	3.8	249	4.2	212	3.6	886	46.4	10.VI	38	88	174	9	26	1	38	154	204	141	24	42	127	13

Barwinek $H_s = 420$ m $h_w = 16$ m

I	10.5	3.8	0.5	1.0	0.5	1.0	8.5	8.4	40.5	5.8	14	5.6	·	·	18.5	4.7	·	5.5	51	9.9	31	7	21	29	·	10	2	·	25	21	14	·	—	31	—
II	4.5	3.0	·	·	·	·	3.5	5.6	16.5	6.1	9	2.9	4	6.2	46.5	5.4	·	5.2	62	9.7	8	15	27	28	·	6	·	1	18	24	16	·	—	28	—
III	8.5	3.6	4	1.2	·	·	7.5	4.9	36	4.8	7.5	3.4	1	1.0	28.5	3.1	·	3.9	53	10.3	17	8	5	23	·	3	1	3	15	18	12	1	—	29	—
IV	16.5	2.6	6	2.7	1	1.0	8.5	2.6	26	2.0	12.5	2.0	3	1.0	16.5	3.4	·	2.4	83	25.2	22	·	·	17	·	1	·	·	13	19	14	2	—	3	—
V	15	2.1	2	2.0	·	·	1.5	4.3	25.5	3.0	11	2.1	2	1.8	36	2.7	·	2.6	85	14.1	16	·	·	9	·	·	·	1	16	21	16	2	—	·	—
VI	15.5	2.0	2	2.5	·	·	7.5	5.9	24	2.5	5	1.6	2.5	3.6	32.5	2.2	1	2.5	146	34.4	10	·	·	·	3	·	·	1	8	19	15	5	—	·	—
VII	8.5	2.3	2	1.0	1	1.0	10.5	2.6	30	2.3	14.5	1.9	2	1.5	24.5	1.4	·	2.0	217	48.8	17	·	·	·	4	1	·	4	8	20	17	7	—	·	—
VIII	7	1.1	·	·	·	·	3.5	6.0	20	4.3	10.5	1.6	3.5	2.1	46.5	2.0	2	2.5	145	34.9	26	·	·	·	—	·	·	5	14	16	13	6	—	·	—
IX	9	1.7	·	·	·	·	6	5.0	40	3.4	17	3.2	2.5	1.2	15.5	1.4	·	2.9	60	27.0	11	·	·	1	·	·	·	5	4	10	7	3	—	·	—
X	25	2.1	2.5	1.4	·	·	1.5	1.0	25.5	2.5	16	2.1	2	2.5	19.5	2.3	1	2.2	22	6.3	9	·	·	14	·	·	·	5	9	8	6	·	—	·	—
XI	15	2.6	1	3.0	·	·	1.5	1.3	36	4.9	12	2.6	3	1.3	21.5	2.9	·	3.5	95	20.8	30	5	11	26	·	4	1	·	23	18	13	4	—	19	—
XII	3	1.7	·	·	·	·	0.5	9.0	57	4.6	10.5	4.1	2.5	1.0	18.5	2.7	1	3.9	59	12.3	17	2	11	27	·	4	·	·	24	23	14	1	—	28	—
Rok	138	2.4	20	1.2	2.5	0.2	60.5	4.7	377	3.8	139.5	2.8	28	1.9	324.5	2.8	5	3.3	1078	48.8	17.VII	37	75	174	—	29	4	25	177	217	157	31	—	138	—

Myczkowce $H_s = 410$ m $h_w = 20.5$ m

I	3	5.3	·	·	3	4.0	4.5	3.8	12.5	5.5	3	3.8	4	7.6	3	11.5	60	2.0	63	15.8	31	9	14	28	·	4	·	2	19	13	13	2	—	30	—
II	8.5	5.1	7.5	4.3	4.5	3.4	5	6.2	6	11.8	2	8.2	10	7.6	12.5	7.4	28	4.5	44	6.5	18	11	24	28	·	7	·	1	15	17	14	·	—	28	—
III	2	4.0	1	3.0	1	2.5	12.5	5.5	8.5	5.9	5.5	5.3	3	4.2	7.5	2.6	52	2.1	33	7.8	27	5	6	20	·	4	·	7	16	15	9	·	—	13	—
IV	6	6.3	4	4.5	5.5	4.4	3	4.8	9	7.2	5.5	7.8	7.5	5.0	5.5	5.9	44	3.0	43	10.2	30	·	·	8	·	3	·	1	18	15	12	1	—	1	—
V	7.5	4.8	5	5.5	3	4.7	2.5	4.0	7	8.3	1.5	5.0	8.5	4.9	14	6.4	44	3.1	72	13.8	10	·	·	3	1	4	·	2	13	17	14	1	—	·	—
VI	6.5	5.9	1.5	4.3	3.5	4.7	2	4.0	5.5	7.2	3	7.7	6	6.8	15	5.8	47	2.9	165	25.0	5	·	·	·	5	1	·	1	11	16	15	7	—	·	—
VII	1	2.0	2	4.0	3	5.3	5	4.8	16.5	5.8	9.5	5.0	6.5	6.2	3.5	4.1	47	2.6	224	24.4	25	·	·	·	6	3	·	4	11	20	20	10	—	·	—
VIII	6	3.9	2.5	3.2	4.5	3.8	1.5	3.3	6	4.8	7.5	5.7	2.5	6.8	11.5	5.3	51	2.2	220	70.9	26	·	·	·	5	1	·	5	12	16	12	6	—	·	—
IX	2.5	3.2	3	4.3	2.5	6.8	12	4.5	10	5.4	4.5	4.8	2	3.8	5.5	4.5	48	2.2	75	38.8	11	·	·	·	1	·	·	6	6	6	5	2	—	·	—
X	8.5	4.8	5	4.3	1	4.0	2	5.5	·	·	2.6	7.0	6.5	7.0	7.5	5.3	60	1.9	19	5.1	16	·	·	14	1	·	·	6	11	9	5	·	—	·	—
XI	5	7.6	·	·	·	·	1.5	8.0	3.5	6.4	8	6.7	11	4.0	9	5.7	52	2.5	61	14.5	27	4	5	26	·	2	1	1	18	20	15	1	—	10	—
XII	4	4.6	6.5	4.8	1	4.0	2	5.8	9	5.9	13	6.4	1	2.0	25	4.4	54	2.3	53	10.2	18	1	5	26	·	1	·	·	24	18	12	2	—	11	—
Rok	60.5	4.8	38	3.5	32.5	4.0	53.5	5.0	92.5	6.2	65.5	6.1	68.5	5.5	97	5.7	587	2.6	1071	70.9	26.VIII	30	54	153	19	30	1	36	174	182	146	32	—	93	—

Jaworzyna Krynicka $H_s = 995$ m $h_w = 15.7$ m

I	4	6.0	4	4.0	1	7.0	7	4.3	22.5	4.6	27.5	5.1	9	5.8	15	5.8	3	4.9	66	8.0	10	3	29	31	·	2	·	·	22	17	15	·	8	31	·
II	15.5	6.7	6.5	4.4	·	·	·	·	4	4.0	8.5	5.0	27.5	4.1	19	7.1	3	5.2	73	6.7	16	21	28	29	·	4	·	1	22	24	16	·	4	28	·
III	8	6.2	2	2.5	·	·	5	4.6	24	3.6	21	4.8	11	4.1	14	4.8	8	4.1	57	9.0	31	5	10	28	·	2	1	3	12	17	14	·	11	31	·
IV	8.5	5.5	9.5	3.1	4	3.5	16	2.8	3.5	2.4	20	3.3	15.5	3.9	9	4.6	4	3.5	56	12.4	22	·	1	11	·	1	·	1	14	17	10	2	11	25	·
V	9.5	5.2	15.5	3.2	2	1.0	3	3.0	10.5	3.2	16	2.6	20.5	4.1	11	5.2	5	3.5	92	18.0	29	·	·	4	·	·	·	1	18	21	15	2	14	·	4
VI	2	3.0	8	2.8	4	1.5	10	2.6	19.5	2.8	16.5	3.0	12.5	4.7	14.5	6.1	3	3.5	194	35.8	10	·	·	·	1	·	·	·	11	17	14	8	7	·	2
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	1.5	12.3	·	·	1	1.0	15	2.7	11	2.8	26	3.0	23	4.7	14.5	5.1	1	3.8	171	43.5	1	·	·	·	·	2	1	1	13	16	13	6	5	·	1
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Żegiestów-Zdrój

φ = 49°22' λ = 20°49' 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.3	−6.2	4.9	30, 31	−18.4	8	−3.5	−1.0	−3.0	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	8.2	8.1	7.7	8.0
II	—	—	—	—	−3.1	−11.9	0.4	1, 14, 15	−27.5	7	−9.1	−5.2	−7.7	−7.4	—	—	—	—	—	—	—	—	—	—	—	—	8.2	6.2	6.8	7.1
III	—	—	—	—	4.9	−4.0	12.5	19	−20.3	1	−2.3	3.8	0.2	0.5	—	—	—	—	—	—	—	—	—	—	—	—	8.5	5.2	5.7	6.5
IV	—	—	—	—	10.8	1.3	16.6	25	−2.7	6	3.2	10.1	5.2	5.9	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.2	5.1	6.5
V	—	—	—	—	15.0	5.5	25.2	19	−3.6	3	7.8	13.9	9.3	10.1	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.8	6.9	7.4
VI	—	—	—	—	20.9	9.5	29.7	26	(2.4)	3	12.0	19.0	14.5	15.0	—	—	—	—	—	—	—	—	—	—	—	—	6.3	4.2	6.9	5.8
VII	—	—	—	—	21.3	10.2	28.4	15	4.3	10	12.1	19.0	14.5	15.0	—	—	—	—	—	—	—	—	—	—	—	—	6.3	5.1	6.6	6.0
VIII	—	—	—	—	19.3	8.4	28.1	8	3.2	3	10.1	17.2	12.6	13.1	—	—	—	—	—	—	—	—	—	—	—	—	8.9	5.6	7.8	7.4
IX	—	—	—	—	19.4	7.3	24.1	28	1.9	22	9.4	17.7	11.6	12.6	—	—	—	—	—	—	—	—	—	—	—	—	8.3	5.2	5.8	6.4
X	—	—	—	—	12.6	0.3	23.0	2	−7.4	22	2.3	11.5	4.3	5.6	—	—	—	—	—	—	—	—	—	—	—	—	9.3	3.2	5.4	6.0
XI	—	—	—	—	2.5	−4.2	13.7	2	−15.3	25	−2.1	1.3	−1.4	−0.9	—	—	—	—	—	—	—	—	—	—	—	—	9.3	7.1	8.2	8.2
XII	—	—	—	—	0.9	−4.3	6.5	10	−13.5	15	−2.5	−0.2	−1.5	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	9.5	7.3	8.0	8.3
Rok	—	—	—	—	10.4	1.0	29.7	26. VI	−27.5	7. II	3.1	8.9	4.9	5.4	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.0	6.7	6.9

Bukowina Tatrzańska

φ = 49°21' λ = 20°07'

I	—	—	—	—	−0.5	−5.9	6.6	31	−13.5	8	−4.4	−2.2	−3.5	−3.4	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.5	6.8	7.4
II	—	—	—	—	−5.5	−11.5	1.4	13	−21.0	6	−9.8	−7.6	−9.1	−8.9	—	—	—	—	—	—	—	—	—	—	—	—	8.1	6.5	7.2	7.3
III	—	—	—	—	3.4	−4.1	10.9	16	−12.8	1	−2.4	1.4	−1.2	−0.8	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.2	6.0	6.2
IV	—	—	—	—	7.5	0.6	13.3	7	−5.8	1	2.1	5.9	2.9	3.4	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.5	6.8	7.3
V	—	—	—	—	11.6	4.3	22.3	19	−3.3	4	6.5	9.8	7.3	7.7	—	—	—	—	—	—	—	—	—	—	—	—	7.3	8.0	7.5	7.6
VI	—	—	—	—	17.6	8.9	27.3	26	4.6	3	12.3	15.9	12.3	13.2	—	—	—	—	—	—	—	—	—	—	—	—	5.5	6.4	6.8	6.2
VII	—	—	—	—	17.9	10.2	24.6	16	5.8	4	13.4	15.8	13.0	13.8	—	—	—	—	—	—	—	—	—	—	—	—	6.1	7.8	6.1	6.7
VIII	—	—	—	—	16.7	9.2	27.3	7	4.8	2	11.5	14.9	11.8	12.5	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.5	5.8	6.2
IX	—	—	—	—	16.9	7.9	24.5	3	4.1	22, 30	10.6	15.0	11.3	12.0	—	—	—	—	—	—	—	—	—	—	—	—	5.2	5.6	4.6	5.1
X	—	—	—	—	10.6	2.0	20.8	2	−4.4	22	3.6	9.2	5.0	5.7	—	—	—	—	—	—	—	—	—	—	—	—	4.6	3.8	2.8	3.7
XI	—	—	—	—	1.9	−4.8	12.9	2	−13.7	18, 24	−3.0	−0.4	−2.0	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.6	5.7	6.5
XII	—	—	—	—	0.6	−5.3	8.3	19	−13.5	15	−2.9	−1.3	−2.7	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.1	6.6	7.0
Rok	—	—	—	—	8.2	1.0	27.3	26.VI, 27.VIII	−21.0	6. II	3.1	6.4	3.8	4.3	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.6	6.1	6.5

Muszyna

φ = 49°21' λ = 20°53'

I	958.6	971.5	934.8	1014.4	0.4	−7.0	5.2	30	−19.7	8	−3.9	−0.4	−3.1	−2.6	4.1	4.4	4.3	4.3	86	74	86	85	0.7	1.6	0.8	1.0	8.2	8.2	8.3	8.2
II	960.5	972.1	941.5	1017.4	−3.3	−12.8	0.9	14	−27.4	7	−10.0	−4.4	−8.1	−7.6	2.7	3.1	3.0	2.9	86	67	85	79	0.4	1.4	0.5	0.8	8.6	7.2	7.2	7.7
III	963.0	978.7	936.9	1018.4	5.7	−4.5	15.2	30	−21.3	1	−2.2	4.0	0.0	0.4	4.9	5.5	5.3	5.2	90	66	84	80	0.6	3.0	1.1	1.6	8.5	6.5	6.5	7.2
IV	956.6	972.8	941.1	1010.5	10.8	0.7	15.8	7	−3.2	6	2.5	9.3	4.7	5.3	6.7	6.8	7.2	6.9	90	59	84	78	0.8	5.2	1.4	2.5	7.7	8.1	4.2	6.7
V	960.5	974.1	950.7	1013.8	14.7	5.0	24.4	19	−4.2	3, 4	7.6	13.0	9.1	9.7	8.9	9.1	10.0	9.3	84	60	84	76	1.9	6.4	1.9	3.4	8.3	8.5	6.5	7.8
VI	961.8	969.4	948.9	1014.2	20.8	9.6	29.8	26	2.2	3	12.9	19.3	14.3	15.2	12.8	12.1	13.7	12.9	85	55	83	74	2.3	11.1	2.8	5.4	5.3	6.2	6.6	6.0
VII	961.3	968.1	953.0	1013.7	20.9	10.3	27.8	15	4.5	10	12.9	19.1	14.4	15.2	13.6	14.6	14.5	14.2	91	67	88	82	1.5	8.2	2.1	3.9	8.0	6.9	5.1	6.7
VIII	963.9	971.6	948.4	1016.9	19.3	8.8	28.3	8	4.1	3, 31	10.5	18.0	12.3	13.3	12.1	12.1	13.0	12.4	94	60	90	81	0.9	9.4	1.7	4.0	8.4	6.8	4.8	6.7
IX	964.3	979.7	953.4	1017.3	19.7	7.6	24.2	11	2.2	22	10.1	18.4	11.4	12.8	11.2	12.0	12.1	11.8	90	58	90	79	1.6	9.5	1.7	4.3	7.9	5.9	3.7	5.8
X	970.0	981.5	961.0	1024.8	13.1	0.0	23.7	2	−7.7	22	1.7	11.7	3.7	5.2	6.9	8.0	7.7	7.5	94	57	92	81	0.5	6.4	0.7	2.5	8.5	4.2	3.2	5.3
XI	958.5	976.4	936.8	1013.8	3.1	−3.9	14.5	2	−15.0	25	−2.1	1.8	−1.2	−0.7	4.8	5.0	5.0	4.9	87	70	86	81	0.6	2.4	0.9	1.3	7.3	7.5	7.3	7.4
XII	955.3	969.6	937.4	1010.4	1.1	−4.3	5.6	10	−14.7	15	−2.7	0.2	−1.6	−1.4	4.6	4.9	4.8	4.8	90	77	87	85	0.5	1.4	0.7	0.9	8.1	7.5	7.6	7.7
Rok	961.2	981.5	934.8	1015.5	10.5	0.8	29.8	26.VI	−27.4	7. II	3.1	9.2	4.7	5.4	7.8	8.1	8.4	8.1	89	64	87	80	1.0	5.5	1.4	2.6	7.9	7.0	5.9	6.9

Witów

φ = 49°20' λ = 19°50'

I	—	—	—	—	0.6	−8.2	8.4	1	−18.6	8	−5.3	−1.1	−4.5	−3.8	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.8	7.0	7.6
II	—	—	—	—	−5.1	−13.9	0.8	1	−25.4	6	−10.9	−6.7	−10.0	−9.4	—	—	—	—	—	—	—	—	—	—	—	—	8.3	6.6	7.9	7.6
III	—	—	—	—	3.9	−6.7	11.1	19, 30	−20.2	1	−3.9	2.1	−2.5	−1.7	—	—	—	—	—	—	—	—	—	—	—	—	7.1	6.6	7.3	7.0
IV	—	—	—	—	7.9	−0.3	14.3	7	−5.5	1	1.7	6.6	2.5	3.3	—	—	—	—	—	—	—	—	—	—	—	—	8.1	8.0	6.9	7.7
V	—	—	—	—	12.3	3.2	22.4	19	−5.6	4	6.5	10.5	6.8	7.6	—	—	—	—	—	—	—	—	—	—	—	—	7.6	8.2	7.6	7.8
VI	—	—	—	—	18.4	7.3	28.9	26	1.4	3	12.3	16.7	11.3	12.9	—	—	—	—	—	—	—	—	—	—	—	—	6.3	6.8	6.7	6.6
VII	—	—	—	—	18.5	8.3	25.8	15	2.8	10	13.1	16.5	12.2	13.5	—	—	—	—	—	—	—	—	—	—	—	—	6.5	8.2	6.0	6.9
VIII	—	—	—	—	17.2	7.2	28.4	7	2.4	31	10.7	15.6	10.5	11.8	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.1	6.0	6.4
IX	—	—	—	—	17.4	5.7	24.8	3	0.7	22	9.7	15.8	9.7	11.2	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.1	4.1	5.3
X	—	—	—	—	11.7	−1.3	22.0	2	−7.7	22	1.0	10.5	2.8	4.3	—	—	—	—	—	—	—	—	—	—	—	—	4.9	4.4	3.6	4.3
XI	—	—	—	—	2.8	−6.2	12.1	1, 2	−18.3	24	−4.0	0.4	−2.8	−2.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.2	7.7	7.6
XII	—	—	—	—	1.6	−6.8	8.0	20	−17.5	15	−2.5	−0.4	−2.4	−1.9	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.7	7.7	7.7
Rok	—	—	—	—	8.9	−1.0	28.9	26.VI	−25.4	6. II	2.4	7.2	2.8	3.8	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.1	6.5	6.9

Żegiestów-Zdrój

$H_s = 440\ m$ $h_w = 18.4\ m$ 1965

Miesiąc	Rozkład wiatru (%) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10	Min<0	Max<0	Max≥25	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥5	≥100	≡	⊠	K
I	3.5	2.4	1	3.0	2	1.5	1	3.0	1	1.0	4	2.8	·	·	20.5	3.3	60	1.1	65	9.9	9	6	17	28	·	·	·	·	19	15	12	·	1	31	—
II	4	3.4	·	·	·	·	1	2.0	·	·	·	·	2	3.2	29	3.7	48	1.5	59	8.6	8	15	24	28	·	·	·	2	13	18	16	·	2	28	—
III	·	·	·	·	·	·	·	·	·	·	0.5	3.0	3	2.2	17.5	2.4	72	0.5	43	6.2	24	5	8	21	·	·	·	3	10	19	14	·	5	23	—
IV	3	2.0	1	2.0	1	2.0	·	·	1	3.0	·	·	3	4.0	7	3.1	74	0.5	54	13.1	22	·	·	11	·	·	·	2	11	17	11	1	2	1	—
V	2	3.0	·	·	1	1.0	1	2.0	1	3.0	3	3.7	13	3.5	3	3.0	69	0.8	85	16.7	27	·	·	4	1	·	·	2	16	22	17	1	2	·	—
VI	3	2.0	·	·	·	·	4	1.5	4	1.5	·	·	4	1.5	14	1.5	61	0.5	162	37.8	10	·	·	·	5	·	·	3	11	18	13	7	1	·	—
VII	3.5	1.7	·	·	·	·	·	·	1	1.0	·	·	·	·	24.5	1.5	64	0.5	146	35.5	25	·	·	·	7	·	·	1	7	22	14	7	·	·	—
VIII	4	1.2	1	2.0	·	·	·	·	·	·	·	·	·	·	44	2.2	44	1.1	135	41.1	1	·	·	·	3	·	·	1	14	15	11	4	4	·	—
IX	9	2.1	·	·	·	·	2	3.5	10	2.7	4	2.5	·	·	21	2.4	44	1.3	33	17.3	11	·	·	·	·	·	·	·	7	10	4	1	6	·	—
X	16	2.4	9	1.9	2	2.0	1	1.0	6	2.0	8	1.9	·	·	5	3.2	46	1.1	4	1.3	11, 31	·	·	18	·	·	·	·	6	9	2	·	19	·	—
XI	9.5	2.5	4	2.2	·	·	4	1.2	8	1.8	15	1.6	·	·	25.5	2.5	24	1.5	47	14.3	11	4	11	24	·	·	·	·	17	16	11	2	2	9	—
XII	6	1.7	1.5	2.7	2.5	1.6	6	1.7	4.5	1.0	11	1.8	2.5	1.4	14	2.7	45	1.0	32	9.3	18	2	10	30	·	·	·	·	18	20	9	·	3	16	—
Rok	63.5	2.0	17.5	1.2	8.5	0.7	20	1.3	36.5	1.4	45.5	1.4	27.5	1.3	225	2.6	651	1.0	865	41.1	1.VIII	32	70	164	16	·	·	14	149	201	134	23	47	108	—

Bukowina Tatrzańska

$H_s = 880\ m$ $h_w = 16\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10	Min<0	Max<0	Max≥25	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥5	≥100	≡	⊠	K
I	0.5	1.0	1	2.0	2	2.0	·	·	·	·	10.5	3.8	20.5	5.0	1.5	2.3	57	1.6	39	8.5	31	2	22	31	·	1	·	1	17	16	11	·	2	31	·
II	·	·	1	1.0	1	2.0	·	·	1	3.0	16	5.1	38.5	4.9	6.5	5.6	20	3.7	32	4.6	17, 18	18	25	28	·	2	·	2	15	18	13	·	1	28	·
III	1	5.0	4.5	2.8	1	5.0	1.5	2.7	0.5	2.0	8.5	3.8	23	3.8	12	2.0	41	1.8	30	5.3	24	2	5	24	·	·	·	6	8	14	8	·	4	31	·
IV	6	2.1	10	2.5	7.5	2.7	3.5	4.1	1.5	6.7	12	3.9	16	3.6	6.5	4.8	27	2.4	49	12.0	22	·	1	7	·	·	·	2	15	18	11	2	4	8	·
V	2.5	1.8	0.5	4.0	6	2.8	2	2.0	1	2.5	15.5	4.0	31.5	4.1	7	3.1	27	2.6	133	33.7	6	·	·	5	·	2	·	2	18	24	17	3	·	·	3
VI	2.5	2.4	1	4.0	·	·	2.5	2.5	4	5.1	8.5	3.9	34.5	4.2	13	3.6	24	2.9	243	59.0	10	·	·	·	2	2	·	1	9	17	15	9	·	·	6
VII	2.5	2.4	2.5	3.0	3	2.7	1	2.0	1	3.5	15	3.4	36	3.3	7	3.1	25	2.4	126	25.9	8	·	·	·	·	·	·	2	11	16	11	3	1	·	6
VIII	3.5	2.4	1.5	2.3	2.5	1.8	1	2.0	1	1.0	16	2.9	24.5	3.6	13	3.1	30	2.1	175	56.9	1	·	·	·	2	·	·	5	12	13	9	5	2	·	1
IX	3.5	2.1	0.5	1.0	1	3.0	2.5	2.6	7.5	3.9	11	3.0	17.5	2.7	6.5	2.5	40	1.6	82	24.5	11	·	·	·	·	1	·	7	6	12	9	3	·	·	·
X	12.5	1.8	3	2.0	·	·	·	·	0.5	1.0	8.5	2.8	18.5	3.0	10	2.6	40	1.4	14	5.7	5	·	·	9	·	·	·	11	2	10	4	·	2	·	·
XI	2.5	2.4	·	·	2	2.5	3.6	2.1	0.5	3.0	16	5.3	23.5	4.1	7	3.1	35	2.5	22	9.6	11	7	11	23	·	2	·	4	13	13	4	·	5	16	·
XII	2	2.0	1.5	1.7	4	2.2	1.6	2.3	0.5	3.0	17.5	3.9	22.5	4.7	6.5	3.6	37	2.4	32	7.0	18	3	17	27	·	2	·	2	15	16	9	·	·	29	·
Rok	39	2.1	27	2.2	30	2.2	19	1.9	19	2.9	155	3.8	306.5	3.9	96.5	3.3	403	2.3	977	59.0	10.VI	32	81	154	4	12	·	45	141	187	121	25	21	143	16

Muszyna

$H_s = 445\ m$ $H_b = 447.1\ m$ $h_w = 21.2\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10	Min<0	Max<0	Max≥25	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥5	≥100	≡	⊠	K
I	16.5	2.2	8.5	2.1	2	1.0	1	2.0	10.5	3.2	27	2.9	3.5	2.1	1	2.0	23	1.9	33	6.1	9	11	15	27	·	·	·	1	22	16	9	·	6	31	·
II	10.5	1.8	10	2.2	3.5	1.3	3.5	1.6	3	2.0	34.5	2.5	5	2.7	·	·	14	1.8	45	7.4	8	16	24	28	·	·	·	1	15	21	15	·	2	28	·
III	10.5	1.6	11	1.7	·	·	3	1.5	7.5	2.4	22	3.7	4.5	2.4	2.5	1.8	32	1.7	44	7.3	24	5	5	22	·	·	·	1	13	16	13	·	6	19	·
IV	12	2.5	12	3.0	2	1.0	3.5	1.3	5.5	1.7	13.5	3.2	0.5	3.0	2	3.0	39	1.5	55	19.2	22	·	·	11	·	·	·	1	11	17	8	2	4	1	1
V	11.5	2.1	8	2.8	1	1.0	·	·	4	2.0	13.5	3.8	5.5	2.1	2.5	2.0	47	1.3	72	9.8	29	·	·	4	·	·	·	1	17	22	15	·	4	·	4
VI	8	1.9	7	2.0	1	1.0	3	2.0	4	1.8	19	3.7	7	1.3	·	·	41	1.4	163	48.6	10	·	·	·	6	·	·	3	9	15	13	6	2	·	4
VII	5	1.2	9	1.4	1	2.0	1	1.0	7.5	3.0	13	2.9	4.5	1.4	1	1.0	51	1.0	135	21.2	21	·	·	·	7	·	·	1	7	19	17	6	5	·	8
VIII	8	2.2	7.5	2.5	1	1.0	·	·	7	3.7	16	2.7	5	2.0	4.5	1.0	44	1.3	120	46.5	1	·	·	·	3	·	·	3	10	14	11	3	9	·	·
IX	2.5	1.8	3.5	3.4	1	7.5	·	·	8	3.9	21.5	4.6	2.5	1.8	·	·	51	1.8	38	17.5	11	·	·	·	·	3	·	·	6	8	5	2	11	·	·
X	8	2.3	12.5	2.6	0.5	6.0	1	2.0	2	2.0	7	2.7	2	1.0	2	2.0	58	0.9	4	1.8	31	·	·	20	·	1	·	3	7	5	2	·	19	·	·
XI	6	2.2	14	1.9	·	·	·	·	2	9.0	22.5	4.3	2	3.2	2.5	1.6	41	1.8	44	17.5	11	4	11	25	·	1	1	3	16	16	8	1	6	9	·
XII	8	1.4	9	1.8	·	·	1	1.0	5	4.4	23	4.7	2	2.0	1	3.0	44	1.8	28	9.3	18	2	7	28	·	2	1	2	17	20	6	·	5	25	·
Rok	106.5	1.9	112	2.3	13	1.8	17	1.0	66	3.3	232.5	3.5	44	2.1	19	1.4	485	1.5	781	48.6	10.VI	38	62	165	16	7	2	20	150	189	122	20	79	113	17

Witów

$H_s = 835\ m$ $h_w = 16\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura T Min<-10	Min<0	Max<0	Max≥25	Wiatr V ≥10	≥15	◔	◕	Opad R ≥0.1	≥5	≥100	≡	⊠	K
I	0.5	2.0	1.5	2.0	·	·	3.5	2.4	5	1.1	20.5	2.9	8.5	1.5	6.5	2.0	47	1.1	53	11.7	31	14	17	30	·	·	·	1	16	14	11	1	1	31	—
II	1	2.0	6.5	1.5	·	·	2	1.0	0.5	1.0	28.5	3.1	15.5	1.8	11	1.8	19	1.8	62	8.4	18	20	25	28	·	3	·	2	18	19	16	·	·	28	—
III	1	2.0	0.5	1.0	·	·	3	4.2	2.5	4.0	19.5	2.7	10.5	1.7	10	1.7	46	1.2	48	10.9	27	9	6	26	·	3	·	5	15	17	13	1	4	31	—
IV	2	1.5	9.5	2.5	1	1.5	4.5	1.7	4	1.6	19.5	2.3	15.5	1.5	13	1.2	21	1.4	70	15.2	22	·	1	15	·	·	·	2	16	19	11	3	1	3	—
V	6	1.6	5	1.7	0.5	1.0	5	1.4	3	4.3	24	3.0	10.5	1.6	10	1.5	29	1.5	141	22.4	6	·	·	6	·	2	·	2	18	24	18	5	2	1	—
VI	2	2.2	2	1.5	1	4.0	2	3.8	3.5	3.0	15	2.7	24.5	2.5	17	1.7	23	1.8	236	75.4	10	·	·	·	3	2	·	1	11	19	15	7	·	·	—
VII	1.5	2.7	2.5	2.0	·	·	1	2.0	5	2.2	32	2.5	15	2.2	10	1.6	26	1.6	112	18.7	8	·	·	·	1	1	·	·	9	21	17	3	1	·	—
VIII	5	1.8	8.5	1.4	0.5	1.0	1.5	1.7	7	3.1	22	2.7	9.5	1.9	10	1.5	29	1.5	208	72.6	1	·	·	·	3	1	·	3	10	16	11	6	1	·	—
IX	1	1.0	2.5	2.2	2	3.5	6	5.3	8	2.4	29.5	2.5	8	2.4	4	2.0	29	1.8	88	30.4	11	·	·	·	·	3	·	6	4	10	7	3	1	·	—
X	2.5	2.2	6	2.0	4.5	1.2	4.5	1.1	3	1.3	18.5	1.5	6.5	2.3	13.5	1.4	34	1.0	13	6.6	31	·	·	22	·	·	·	11	6	8	3	·	1	·	—
XI	1	1.0	6.5	1.0	1.5	1.0	2	1.0	5.5	2.7	27.5	3.7	7	3.2	2	2.2	38	1.7	43	12.4	11	8	10	26	·	5	1	2	16	17	7	2	2	17	—
XII	3.5	1.4	0.5	1.0	·	·	·	·	6	2.8	41	3.0	10	1.6	8	1.4	24	1.8	38	8.0	13	10	11	28	·	5	·	·	16	18	10	·	·	25	—
Rok	27	1.8	50.5	1.6	11	1.1	35	2.1	53	2.5	297.5	2.7	141	2.0	115	1.7	365	1.5	1112	75.4	10.VI	61	70	181	7	25	1	35	155	202	139	31	14	136	—

Poronin

φ = 49°20′ λ = 20°02′ 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	−10.9	8.0	31	−24.3	8	−6.2	−1.1	−6.0	−4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	7.2	7.3
II	–	–	–	–	−4.3	−16.3	2.7	13	−30.0	7	−11.9	−6.1	−11.2	−10.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	6.6	6.8	7.3
III	–	–	–	–	4.3	−8.3	12.0	19	−23.2	1	−4.8	2.9	−3.5	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.8	6.6	6.2
IV	–	–	–	–	8.5	−1.0	15.3	7	−6.9	2	1.3	7.2	1.9	3.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.5	7.1	7.5
V	–	–	–	–	12.6	2.6	23.0	18	−6.8	4	6.6	11.0	6.2	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	8.4	7.7
VI	–	–	–	–	18.5	6.0	28.2	26	−2.2	3	12.1	17.0	9.9	12.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.2	5.3	5.3
VII	–	–	–	–	19.0	7.1	26.6	15	0.2	10	13.3	16.9	11.0	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	6.3	6.4
VIII	–	–	–	–	17.5	6.2	28.4	7	0.4	31	10.4	15.9	9.5	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.9	6.6	6.3
IX	–	–	–	–	17.9	4.1	25.0	3	−2.0	22	8.8	16.3	8.7	10.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.7	3.6	4.8
X	–	–	–	–	12.3	−3.1	22.4	2	−9.5	22	−0.2	11.0	1.2	3.3	–	–	–	–	–	–	–	–	–	–	–	–	4.3	3.5	2.4	3.4
XI	–	–	–	–	3.3	−7.2	14.2	1	−20.9	24	−4.6	1.2	−3.4	−2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	7.4	7.2
XII	–	–	–	–	1.9	−8.8	9.7	20	−22.3	15	−4.7	−0.2	−3.7	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.3	6.6	7.0
Rok	–	–	–	–	9.3	−2.5	28.4	7.VIII	−30.0	7. II	1.7	7.7	1.7	3.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.2	6.4

Komarńcza

φ = 49°20′ λ = 22°04′

I	–	–	–	–	0.1	−7.1	4.2	31	−21.6	12	−3.2	−0.8	−3.3	−2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.5	7.2	8.2
II	–	–	–	–	−4.8	−13.8	0.6	1	−27.1	7	−9.9	−5.9	−9.0	−8.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	7.5	8.2
III	–	–	–	–	5.0	−4.4	14.4	30	−23.0	1	−1.1	3.7	0.2	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	5.1	6.7
IV	–	–	–	–	10.4	0.3	14.8	8	−5.1	6	3.5	9.0	4.3	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	4.5	6.9
V	–	–	–	–	14.4	4.5	25.5	19	−6.3	4	8.0	12.8	9.1	9.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.4	7.3	7.8
VI	–	–	–	–	19.9	9.0	28.7	26	1.7	3, 8	13.8	18.7	13.2	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.2	6.0	6.3
VII	–	–	–	–	20.5	9.1	26.7	16	2.3	7	14.1	18.9	14.2	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.5	6.7	6.6
VIII	–	–	–	–	18.6	8.3	27.7	8	2.5	31	12.1	17.2	12.0	13.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.5	4.7	5.7
IX	–	–	–	–	18.9	6.7	25.1	2	−0.1	22	11.1	18.0	11.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.5	2.4	4.7
X	–	–	–	–	11.3	0.5	22.9	2	−9.0	22	3.5	10.8	4.4	5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	4.8	3.7	5.1
XI	–	–	–	–	2.8	–	12.8	2	–	–	−1.5	1.4	−0.8	−0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.3	7.4	7.4	8.0
XII	–	–	–	–	1.1	–	6.6	10	–	–	−1.6	0.0	−1.2	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.5	7.6	8.3
Rok	–	–	–	–	9.8	–	28.7	26.VI	−27.1	7. II	4.1	8.6	4.5	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	5.8	6.9

Baligród

φ = 49°20′ λ = 22°17′

I	–	–	–	–	1.2	−5.1	6.4	31	−18.5	12	−2.3	0.1	−1.8	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.9	7.4	7.8
II	–	–	–	–	−4.0	−10.9	0.7	12	−24.9	7	−8.5	−5.3	−7.5	−7.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.5	7.2	8.2
III	–	–	–	–	5.7	−2.7	14.7	30	−17.8	1	0.0	4.6	1.0	1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.8	5.1	6.5
IV	–	–	–	–	10.8	1.6	15.7	8	−3.6	6	4.6	9.6	5.1	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.1	5.1	6.9
V	–	–	–	–	14.7	5.5	25.3	19	−4.8	3	8.9	13.0	9.3	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.7	7.2	7.3
VI	–	–	–	–	20.4	9.8	29.6	27	4.1	8	14.1	18.9	13.4	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.0	5.5	6.0
VII	–	–	–	–	21.0	10.8	27.9	16	5.0	12	15.0	19.4	14.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.9	5.5	6.1
VIII	–	–	–	–	18.8	9.4	27.6	8	5.5	17	13.0	17.6	12.5	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	5.2	5.7
IX	–	–	–	–	19.8	7.9	26.2	2	1.5	22	12.0	18.9	11.9	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.1	2.6	4.3
X	–	–	–	–	11.9	2.1	23.7	2	−6.9	22	5.2	10.9	5.6	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.6	4.1	5.3
XI	–	–	–	–	3.4	−3.2	13.5	2	−19.6	18	−0.9	2.0	−0.4	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	7.1	7.6
XII	–	–	–	–	2.3	−3.1	7.6	11	−15.6	17	−0.1	1.0	−0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	7.1	7.7
Rok	–	–	–	–	10.5	1.8	29.6	27.VI	−24.9	7. II	5.1	9.2	5.3	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	5.8	6.6

Gubałówka

φ = 49°18′ λ = 19°56′

I	–	–	–	–	0.4	−5.5	7.3	1	−12.0	7	−3.0	−1.2	−2.8	−2.4	4.0	4.3	4.3	4.2	81	77	85	81	1.1	1.4	0.8	1.1	8.3	7.8	7.5	7.9
II	–	–	–	–	−6.7	−12.2	2.6	1	−19.8	6	−10.2	−7.2	−9.7	−9.2	2.5	2.7	2.5	2.6	84	76	83	81	0.5	0.9	0.5	0.6	8.5	6.9	8.0	7.8
III	–	–	–	–	3.2	−3.9	10.2	19	−10.6	1, 11	−1.6	1.9	−1.0	−0.4	4.5	4.6	4.7	4.6	79	67	80	75	1.2	2.7	1.2	1.7	6.7	6.9	6.8	6.8
IV	–	–	–	–	6.5	0.3	13.4	7	−6.7	1	2.0	5.4	2.5	3.1	6.1	6.3	6.2	6.2	86	71	85	81	1.1	2.9	1.2	1.7	8.4	7.8	6.8	7.7
V	–	–	–	–	10.6	3.7	20.7	19	−3.5	3	5.9	9.3	6.6	7.1	7.7	8.1	8.2	8.0	82	70	83	78	2.0	4.1	1.8	2.6	8.1	8.2	7.7	8.0
VI	–	–	–	–	16.5	8.6	27.0	26	4.3	3	11.9	15.1	11.5	12.5	10.9	11.1	11.2	11.1	78	66	83	76	3.4	6.9	2.7	4.3	6.0	7.1	6.8	6.6
VII	–	–	–	–	17.3	10.0	24.6	15	4.2	6	13.2	15.4	12.5	13.4	12.0	12.5	11.7	12.1	79	72	80	77	3.6	5.5	3.2	4.1	6.7	8.3	5.7	6.9
VIII	–	–	–	–	15.9	9.1	26.7	7	3.7	2	11.4	14.2	11.3	12.0	10.6	10.6	10.7	10.6	80	68	80	76	3.3	6.5	3.3	4.4	6.3	7.1	6.0	6.5
IX	–	–	–	–	16.6	8.3	22.9	3	4.8	20, 30	11.4	14.9	11.3	12.2	10.4	11.1	10.4	10.6	78	67	78	74	3.5	6.3	3.4	4.4	6.0	6.3	4.3	5.5
X	–	–	–	–	11.3	2.5	24.9	2	−3.9	21	4.6	9.9	5.4	6.3	6.4	7.5	7.2	7.0	73	60	78	70	2.5	5.3	2.2	3.3	4.7	4.0	3.2	4.0
XI	–	–	–	–	2.2	−4.9	12.3	1	−15.2	17	−2.6	0.3	−2.0	−1.6	4.3	4.7	4.3	4.4	83	74	79	79	1.1	2.1	1.5	1.6	7.5	7.2	6.6	7.1
XII	–	–	–	–	0.9	−5.0	10.2	19	−13.4	15	−2.1	−1.1	−2.3	−2.0	4.4	4.5	4.4	4.4	81	79	83	81	1.1	1.3	1.0	1.1	8.2	7.5	7.2	7.6
Rok	–	–	–	–	8.0	0.9	27.0	26.VI	−19.8	6. II	3.4	6.4	3.6	4.2	7.0	7.3	7.2	7.2	80	71	81	77	2.0	3.8	1.9	2.6	7.1	7.1	6.4	6.9

Poronin

H_s = 800 m h_w = 16 m I–VIII, 17.2 m IX–XII **1965**

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	V≥10	V>15	◔	◕	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	6	1.2	·	·	·	·	·	·	1	4.0	3	1.7	10	2.0	4	2.5	69	0.5	43	8.9	31	17	17	29	·	·	·	4	16	16	12	·	1	31	·
II	0.5	1.0	·	·	·	·	·	·	·	·	·	·	27	1.7	3.5	1.7	53	0.6	52	8.7	17	21	24	28	·	·	·	2	15	17	11	·	·	28	·
III	3	1.5	1.5	1.0	10	1.0	1.5	2.0	2	3.0	6.5	4.6	4	1.8	5.5	1.8	59	0.8	54	9.4	27	11	5	30	·	·	·	6	11	16	13	·	4	30	·
IV	1.5	1.7	·	·	9	1.4	1.5	1.0	3.5	1.9	3.5	2.1	8.5	2.1	1.5	1.7	61	0.6	72	14.4	22	·	·	17	·	·	·	1	16	22	13	3	2	6	·
V	3	1.0	·	·	2	1.5	·	·	2.5	6.0	7.5	4.3	3	2.0	8	2.1	67	0.8	134	39.6	6	·	·	8	·	1	1	2	19	24	18	4	·	·	5
VI	2	1.0	1	1.0	1	1.0	·	·	6	4.1	3	2.2	16	1.8	3	3.7	58	0.8	250	55.0	10	·	·	1	2	1	·	6	9	18	15	9	·	·	6
VII	·	·	·	·	3	1.3	·	·	1	6.0	2.5	1.8	17.5	2.0	2	1.5	67	0.6	104	21.4	8	·	·	·	2	·	·	4	8	21	13	3	·	·	7
VIII	3.5	1.3	2	1.0	1	1.0	·	·	2	1.5	2	3.5	8	1.8	0.5	1.0	74	0.3	204	57.5	1	·	·	·	3	·	·	6	16	15	12	6	2	·	·
IX	·	·	2	1.0	3	1.3	·	·	5	4.2	3	2.7	10	3.0	1	2.0	66	0.7	75	25.2	11	·	·	4	·	·	·	9	7	11	8	2	1	·	·
X	1	1.0	1	2.0	3	1.0	·	·	·	·	1	2.0	8	1.4	2	2.0	77	0.2	11	2.7	31	·	·	25	·	·	·	14	2	10	4	·	2	·	1
XI	·	·	·	·	1	1.0	·	·	·	·	4	9.5	16	3.4	1	3.0	68	1.1	29	9.0	11	9	10	27	·	3	·	5	16	14	6	·	3	15	·
XII	·	·	·	·	·	·	·	·	·	·	1	2.0	24	2.7	3	2.0	65	0.8	41	7.2	13	18	9	29	·	1	·	3	13	16	11	·	·	28	·
Rok	20.5	0.8	7.5	0.5	33	0.9	3	0.2	23	2.6	37	3.0	152	2.1	35	2.1	784	0.6	1069	57.5	1.VIII	76	65	198	7	6	1	62	148	200	136	27	15	138	19

Komańcza

H_s = 470 m h_w = 15 m

I	5	2.6	2	1.5	9	1.4	13	3.6	19	2.2	1	6.0	2	2.5	7	3.1	35	1.6	59	9.8	31	7	15	29	·	·	·	1	20	18	15	·	—	31	—
II	10	2.7	8	1.9	6	2.2	8	4.5	9	1.4	1	1.0	8	3.0	11	3.4	23	2.0	46	7.5	8	16	27	28	·	·	·	2	18	16	15	·	—	28	—
III	8	2.5	3	1.7	10	2.2	4	2.2	26	2.7	·	·	1	3.0	·	·	41	1.4	51	12.5	3	6	4	23	·	·	·	6	13	13	12	1	—	19	—
IV	6	2.0	8	3.6	5	2.2	6	1.5	9	2.0	4	2.2	3	1.0	6	2.2	43	1.2	61	14.2	20	·	·	16	·	·	·	2	12	15	10	2	—	1	—
V	9	2.3	6	2.5	4	1.5	5	2.0	8	3.5	1	3.0	3	2.7	6	1.8	51	1.1	86	19.1	10	·	·	7	1	·	·	1	20	16	13	1	—	·	—
VI	6	1.8	3	2.0	4	2.0	4	2.2	13	2.2	1	3.0	5	2.0	8	1.6	46	1.0	169	30.5	10	·	·	·	3	·	·	3	12	17	16	7	—	·	—
VII	4	1.0	4	1.8	7	1.6	8	2.0	19	2.2	·	·	5	2.2	1	3.0	45	1.0	228	75.7	25	·	·	·	5	·	·	3	11	20	16	6	—	·	—
VIII	8	1.5	7	1.3	1	2.0	10	1.9	15	2.1	·	·	1.5	1.0	12.5	2.8	38	1.2	129	36.6	26	·	·	·	2	1	·	6	9	14	12	5	—	·	—
IX	4	2.0	1	1.0	6	1.3	11	3.1	20	2.2	3	2.3	2	1.0	1	3.0	42	1.2	99	49.0	11	·	·	1	1	·	·	7	4	9	7	3	—	·	—
X	15	1.7	4	1.8	2	1.5	4	1.2	7	1.7	1	2.0	5	1.4	5	2.2	50	0.8	9	2.1	29	·	·	12	·	·	·	8	10	7	5	·	—	·	—
XI	13	2.2	4	2.8	1	1.0	6	4.3	12	4.4	4.5	2.3	5.5	2.1	6	1.8	38	1.7	111	27.1	21	—	10	—	·	1	·	1	18	18	14	4	—	16	—
XII	9	1.9	3	2.7	2	3.0	9	3.8	19	2.2	3	5.0	14	2.9	5	1.8	29	1.8	55	6.4	18	—	10	—	·	1	·	1	21	21	16	·	—	18	—
Rok	97	2.0	53	2.0	57	1.8	88	2.7	176	2.4	19.5	2.2	55	2.1	68.5	2.2	481	1.3	1103	75.7	25.VII	—	66	—	12	3	·	41	168	184	151	29	—	113	—

Baligród

H_s = 450 m h_w = 16,9 m

I	11	2.0	1	1.0	·	·	1	1.0	35	3.5	9	2.3	7	1.0	6	2.8	23	2.0	55	19.0	31	5	10	29	·	1	·	3	21	14	11	1	—	30	—
II	30	2.0	1	1.0	1	1.0	·	·	22	4.1	6	2.7	3	1.0	9	2.6	12	2.3	50	9.0	16	13	25	28	·	2	1	·	19	18	13	·	—	28	—
III	16	1.6	2	1.5	·	·	2	2.0	41	2.2	5	2.2	2	2.5	3	2.3	22	1.6	50	10.3	3	4	4	19	·	·	·	4	11	15	11	1	—	17	—
IV	8	2.1	5	1.4	10	1.7	2	1.5	29	1.7	6	2.0	·	·	3	2.3	27	1.2	43	9.0	20	·	·	6	·	·	·	1	11	14	10	·	—	1	—
V	16	1.8	3	2.7	1	3.0	2	2.0	27	2.1	3	2.0	3	2.0	5	2.4	33	1.4	117	26.0	20	·	·	5	1	·	·	1	14	20	18	2	—	·	—
VI	9	1.8	1	2.0	3	1.3	6	2.2	39	1.7	3	2.3	4	1.2	9	2.3	16	1.5	159	33.3	4	·	·	·	3	·	·	1	8	17	15	5	—	·	—
VII	5	1.8	2	1.5	3	1.7	3	1.7	38	1.7	12	1.8	1	1.0	4	1.8	25	1.2	196	46.5	17	·	·	·	5	·	·	4	4	20	18	7	—	·	—
VIII	18	1.6	·	·	·	·	1	1.0	32	2.1	8	2.5	5	1.8	7	2.3	22	1.5	171	54.0	26	·	·	·	2	·	·	8	10	15	12	6	—	·	—
IX	7	1.9	·	·	·	·	2	2.0	37	1.9	6	1.7	1	1.0	3	2.0	34	1.2	81	30.4	11	·	·	·	1	·	·	8	2	5	5	3	—	·	—
X	16	1.8	1	2.0	1	2.0	1	3.0	26	2.8	4	2.2	2	2.0	5	2.2	37	1.4	10	5.3	4	·	·	9	·	·	·	7	11	7	3	·	—	·	—
XI	7	1.9	1	2.0	14	1.4	·	·	25	3.3	5	3.0	3	1.7	2	2.0	33	1.6	84	18.0	11	3	9	19	·	·	·	1	18	17	12	3	—	14	—
XII	10	2.2	1	2.0	1	1.0	2	1.5	48	3.6	14	3.4	2	5.0	3	1.3	12	2.8	59	11.0	11	2	7	24	·	4	·	2	19	16	12	1	—	13	—
Rok	153	1.9	16	1.4	34	1.1	22	1.5	399	2.6	81	2.3	33	1.7	59	2.2	296	1.6	1075	54.0	26.VIII	27	55	139	12	7	1	40	148	178	140	29	—	103	—

Gubałówka

H_s = 1000 m h_w = 15 m

I	4	1.5	·	·	·	·	·	·	6	2.8	5	4.4	44	2.8	22	1.4	12	2.1	56	10.4	31	3	14	30	·	5	·	1	20	17	13	1	2	31	·
II	3	1.3	·	·	4	1.8	1	2.0	2	2.0	7	3.1	50	2.1	13	1.5	4	2.0	92	11.6	8	21	26	28	·	·	·	1	17	22	16	2	·	28	·
III	8	1.4	1	1.0	2	3.0	·	·	1	4.0	11	4.0	33	1.8	22	1.5	15	1.7	58	13.5	27	3	6	24	·	1	·	6	14	20	14	1	3	31	·
IV	8	2.1	·	·	8	1.9	·	·	1	4.0	10	2.6	38	1.8	19	1.5	6	1.8	65	17.1	21	·	2	10	·	·	·	2	19	22	14	3	5	4	1
V	6	1.5	3	1.7	22	2.2	3	1.7	14	2.7	13	4.4	14	1.8	8	1.9	10	2.2	134	31.8	6	·	·	6	·	2	·	2	19	23	18	5	3	1	6
VI	20	2.0	4	1.5	20	1.6	7	3.7	22	2.5	9	5.1	3	2.7	2	2.0	3	2.4	290	66.7	10	·	·	·	1	3	·	1	11	18	15	9	2	·	6
VII	12	1.8	6	1.5	22	1.7	1	2.0	21	1.9	18	4.6	5	2.2	2	2.5	6	2.2	118	17.8	8	·	·	·	·	1	·	2	10	21	13	5	·	·	6
VIII	17	1.7	6	1.5	25	1.4	7	2.3	14	1.9	4	8.5	5	2.2	·	·	15	1.7	236	73.7	1	·	·	·	2	1	·	7	15	16	12	7	2	·	2
IX	10	1.7	·	·	22	1.5	8	3.6	16.5	3.5	12.5	7.8	8	2.0	3	2.3	10	2.9	102	29.2	11	·	·	·	·	6	·	5	6	11	8	4	1	·	1
X	24	1.5	8	1.5	27	1.4	4	1.8	10	1.9	2	6.0	5	2.0	2	2.0	11	1.5	20	5.5	31	·	·	11	·	1	·	12	4	9	7	·	5	·	1
XI	19	1.7	3	1.7	29	1.5	1	2.0	5	2.4	15	10.1	11	3.3	·	·	7	3.1	41	11.2	21	7	10	24	·	5	2	4	17	18	7	1	1	18	·
XII	4	2.8	1	1.0	8	1.8	5	1.8	27	2.2	12	5.2	25	2.9	2	3.0	9	2.5	47	7.6	13	2	12	26	·	7	·	2	18	21	13	·	·	27	·
Rok	135	1.8	32	1.0	189	1.6	37	1.7	139.5	2.6	118.5	5.5	241	2.3	95	1.6	108	2.2	1259	73.7	1.VIII	36	70	159	3	32	2	45	170	218	150	39	24	140	23

Zakopane φ = 49°18' λ = 19°57' 1965

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	913.7	925.2	891.5	—	1.0	−8.0	9.5	1	−18.4	8	−4.8	−1.1	−4.2	−3.6	3.8	4.4	4.0	4.1	85	76	87	83	0.8	1.4	0.6	0.9	8.2	8.1	6.9	7.7
II	915.6	927.3	896.8	—	−4.7	−13.7	2.2	13	−25.6	6	−10.5	−6.1	−9.7	−9.0	2.4	2.7	2.5	2.5	83	68	82	78	0.5	1.3	0.5	0.8	7.9	6.2	7.5	7.2
III	918.1	932.7	892.4	—	4.2	−6.1	12.5	30	−18.5	1	−3.6	2.7	−1.6	−1.0	4.4	4.8	4.9	4.7	87	65	86	79	0.6	2.9	0.8	1.4	7.1	6.5	7.0	6.9
IV	912.9	929.1	898.0	—	8.2	−0.3	14.9	7	−6.1	2	1.8	6.8	2.7	3.5	6.1	6.2	6.5	6.3	87	64	86	79	0.9	4.0	1.0	2.0	8.0	7.8	7.5	7.8
V	917.2	929.9	907.1	—	12.2	3.6	22.4	18	−5.4	4	6.5	10.7	6.9	7.8	7.9	8.0	8.6	8.2	80	62	84	75	2.3	5.5	1.7	3.2	7.9	8.1	7.7	7.9
VI	919.5	928.2	906.1	—	18.3	7.3	28.8	26	1.3	3	12.2	16.7	11.7	13.1	11.0	11.0	11.8	11.3	77	59	86	74	3.5	8.8	2.2	4.8	5.9	6.5	6.6	6.3
VII	919.0	925.5	910.3	—	18.6	8.3	26.1	15	2.5	10	12.9	16.5	12.3	13.5	12.1	12.5	12.1	12.2	81	67	84	77	3.0	7.0	2.5	4.2	6.5	7.9	6.3	6.9
VIII	921.4	928.8	910.4	—	17.4	8.0	28.4	7	3.3	31	10.7	15.6	11.0	12.1	10.7	10.4	11.0	10.7	84	61	84	76	2.4	8.3	2.5	4.4	6.1	6.6	5.8	6.2
IX	921.2	936.4	910.4	—	17.8	6.2	25.1	3	0.5	22	9.8	16.0	10.4	11.6	9.8	10.5	10.0	10.1	83	59	81	74	2.9	8.2	3.2	4.8	6.2	5.9	4.5	5.5
X	926.1	935.6	917.7	—	12.0	−1.4	21.5	2	−8.2	22	0.5	10.9	2.8	4.2	6.1	7.3	7.0	6.8	91	55	89	78	0.5	6.3	0.9	2.6	5.4	4.3	4.0	4.6
XI	913.4	932.2	892.3	—	3.0	−6.1	14.4	1	−18.3	24	−3.8	1.1	−2.4	−1.9	4.1	4.7	4.3	4.4	84	71	82	79	0.9	2.4	1.3	1.5	7.3	7.0	6.9	7.1
XII	910.3	924.4	893.6	—	1.8	−6.7	10.3	20	−17.4	15	−2.9	−0.5	−2.4	−2.0	4.4	4.6	4.4	4.5	84	77	83	81	0.9	1.3	1.0	1.1	7.7	7.5	7.6	7.6
Rok	917.4	936.4	891.5	—	9.2	−0.7	28.8	26. VI	−25.6	6. II	2.4	7.4	3.1	4.0	6.9	7.3	7.3	7.2	84	65	84	78	1.6	4.8	1.5	2.6	7.0	6.9	6.5	6.8

Antołówka φ = 49°18' λ = 19°59'

I	—	—	—	—	0.5	−6.0	8.4	1	−14.0	7	−4.0	−1.5	−3.6	−3.2	—	—	—	—	—	—	—	—	—	—	—	—	8.3	8.1	7.7	8.0
II	—	—	—	—	−4.9	−12.1	2.7	13	−21.0	6	−10.1	−6.7	−9.5	−9.0	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.4	8.0	7.5
III	—	—	—	—	3.6	−4.5	11.6	30	(−13.5)	1	−2.4	2.0	−1.1	−0.6	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.7	7.7	7.2
IV	—	—	—	—	7.7	−0.2	15.0	7	−6.1	2	1.8	6.2	2.7	3.4	—	—	—	—	—	—	—	—	—	—	—	—	7.9	8.0	7.8	7.9
V	—	—	—	—	11.8	3.6	22.1	18	−5.0	4	6.4	10.3	6.6	7.5	—	—	—	—	—	—	—	—	—	—	—	—	8.1	8.3	8.4	8.3
VI	—	—	—	—	17.8	8.3	28.2	26	3.0	3	12.1	16.2	11.9	13.0	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.5	7.2	7.0
VII	—	—	—	—	18.3	9.4	24.9	14, 15	4.3	4	13.4	16.4	12.5	13.7	—	—	—	—	—	—	—	—	—	—	—	—	6.9	8.4	6.6	7.3
VIII	—	—	—	—	16.6	8.7	27.3	8	4.2	2	11.1	15.1	11.5	12.3	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.0	6.6	6.8
IX	—	—	—	—	17.2	7.5	23.8	3	3.3	22, 30	10.7	15.4	11.1	12.1	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.2	4.5	5.8
X	—	—	—	—	11.3	0.8	19.9	2	−5.0	22	2.8	10.0	4.2	5.3	—	—	—	—	—	—	—	—	—	—	—	—	4.3	3.9	3.4	3.9
XI	—	—	—	—	2.4	−5.5	14.1	2	−14.8	24	−3.1	0.4	−2.2	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	7.5	6.7	7.2	7.1
XII	—	—	—	—	1.5	−6.1	9.8	20	−14.6	15	−2.7	−0.9	−2.5	−2.2	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.8	7.6	7.7
Rok	—	—	—	—	8.6	0.3	28.2	26. VI	−21.0	6. II	3.0	6.9	3.5	4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.1	6.9	7.0

Smolnik φ = 49°17' λ = 22°07'

I	—	—	—	—	0.0	−6.6	4.3	31	−21.5	11	−3.3	−1.3	−3.4	−2.8	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.0	7.3	8.0
II	—	—	—	—	−5.0	−12.8	1.0	1	−26.8	7	−10.4	−6.3	−8.9	−8.6	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.6	8.1	8.1
III	—	—	—	—	4.5	−4.6	14.8	30	−24.0	1	−1.7	2.9	−0.3	0.2	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.4	5.8	6.9
IV	—	—	—	—	10.3	−0.4	15.0	8	−6.6	6	2.9	8.7	3.6	4.7	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.0	5.2	6.6
V	—	—	—	—	14.3	4.3	24.5	19	−6.8	4	7.4	12.2	8.5	9.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.7	7.3	7.4
VI	—	—	—	—	19.6	8.3	27.3	26	1.4	8	12.8	18.0	12.4	13.9	—	—	—	—	—	—	—	—	—	—	—	—	5.3	6.9	5.4	5.9
VII	—	—	—	—	20.1	9.2	26.1	15	2.2	7	13.3	18.4	13.8	14.8	—	—	—	—	—	—	—	—	—	—	—	—	5.8	7.3	6.8	6.6
VIII	—	—	—	—	18.3	7.3	26.5	8	2.0	31	10.7	16.7	11.0	12.4	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.9	5.5	6.3
IX	—	—	—	—	18.8	6.7	24.5	2	−1.2	17	10.1	17.9	10.7	12.4	—	—	—	—	—	—	—	—	—	—	—	—	5.8	5.3	3.5	4.9
X	—	—	—	—	11.3	−0.4	22.6	2	−10.1	22	2.4	10.3	3.4	4.9	—	—	—	—	—	—	—	—	—	—	—	—	5.9	5.2	3.7	4.9
XI	—	—	—	—	2.7	−4.4	13.0	2	−13.7	18	−1.8	1.0	−1.6	−1.0	—	—	—	—	—	—	—	—	—	—	—	—	8.9	8.3	7.3	8.2
XII	—	—	—	—	0.9	−3.9	6.3	10	−14.2	15	−1.8	−0.3	−1.5	−1.3	—	—	—	—	—	—	—	—	—	—	—	—	8.7	9.0	8.8	8.8
Rok	—	—	—	—	9.6	0.2	27.3	26. VI	−26.8	7. II	3.4	8.2	4.0	4.9	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.2	6.2	6.9

Kuźnice φ = 49°16' λ = 19°59'

I	—	—	—	—	0.3	−6.5	8.2	1	−15.6	7, 8	−3.6	−1.5	−3.2	−2.9	—	—	—	—	—	—	—	—	—	—	—	—	7.9	7.8	7.2	7.6
II	—	—	—	—	−5.7	−13.1	2.1	1	−21.1	6	−10.9	−7.2	−10.1	−9.6	—	—	—	—	—	—	—	—	—	—	—	—	7.8	6.6	7.9	7.4
III	—	—	—	—	2.9	−5.3	10.2	19	−14.6	11	−3.0	1.3	−1.9	−1.4	—	—	—	—	—	—	—	—	—	—	—	—	7.4	7.0	7.2	7.2
IV	—	—	—	—	6.2	−1.2	12.1	7	−8.4	2	0.9	4.8	0.7	1.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	7.6	7.6	7.7
V	—	—	—	—	10.3	2.0	20.3	18	−5.3	3	5.1	8.8	4.8	5.9	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.8	8.4	7.9
VI	—	—	—	—	16.1	6.2	26.5	26	1.1	3	10.5	14.5	9.3	10.9	—	—	—	—	—	—	—	—	—	—	—	—	6.0	7.3	6.9	6.7
VII	—	—	—	—	16.5	7.4	23.9	15	2.4	10	11.8	14.9	10.2	11.8	—	—	—	—	—	—	—	—	—	—	—	—	6.1	8.4	6.4	7.0
VIII	—	—	—	—	15.2	6.9	26.1	8	2.3	2	9.7	13.5	9.3	10.4	—	—	—	—	—	—	—	—	—	—	—	—	5.9	7.2	6.7	6.6
IX	—	—	—	—	15.8	5.8	22.2	2, 3	1.7	22	9.5	13.9	9.3	10.5	—	—	—	—	—	—	—	—	—	—	—	—	5.7	6.4	5.1	5.7
X	—	—	—	—	10.4	−0.4	19.9	2	−6.0	21	1.0	9.2	2.4	3.8	—	—	—	—	—	—	—	—	—	—	—	—	4.4	4.0	4.3	4.2
XI	—	—	—	—	1.4	−5.8	13.6	1	−17.3	17	−3.8	−0.4	−3.0	−2.6	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.9	7.4	7.1
XII	—	—	—	—	0.9	−6.4	11.1	20	−15.7	15	−2.9	−1.1	−2.8	−2.4	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.0	7.9	8.1
Rok	—	—	—	—	7.5	−0.9	26.5	26. VI	−21.1	6. II	2.0	5.9	2.1	3.0	—	—	—	—	—	—	—	—	—	—	—	—	6.8	7.1	6.9	6.9

Zakopane $H_s = 844$ m $H_b = 838{,}2$ m $h_w = 17{,}7$ m **1965**

MIESIĄC	ROZKŁAD WIATRU n(D), V(mD): N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	1	1.0	16.5	1.7	6	1.1	0.5	1.0	·	·	15.5	2.6	8	3.3	0.5	3.0	46	1.1	52	9.2	31	13	16	29	·	2	·	1	16	16	14	·	1	31	·
II	·	·	8.5	1.6	9.5	1.5	2	1.5	1	3.5	18.5	2.5	17	3.2	6.5	2.6	21	1.8	74	12.6	18	20	24	28	·	·	·	2	15	20	14	2	·	28	·
III	1	3.0	15.5	1.6	6.5	1.1	7.5	1.3	5.5	3.1	9	3.6	7.5	4.1	1.5	2.3	39	1.4	58	14.1	27	9	5	26	·	1	·	4	13	18	13	1	2	30	·
IV	3	2.3	16	2.0	3.5	1.9	3	3.0	4.5	1.6	16.5	1.7	9.5	2.3	2	3.0	32	1.3	72	17.3	21	·	1	14	·	·	·	2	16	22	13	3	2	5	·
V	4	2.5	18.5	2.0	8	1.6	2	1.0	2.5	6.4	15.5	2.1	13	2.5	7.5	2.7	22	1.7	155	38.7	6	·	·	7	·	1	·	1	16	25	21	6	1	·	4
VI	1	3.0	15	1.5	8	1.9	12.5	1.9	8.5	3.4	7	3.0	4.5	3.1	9.5	2.7	24	1.7	283	59.7	10	·	·	·	2	1	1	1	9	20	14	9	1	·	6
VII	5	2.3	13.5	1.7	4.5	1.1	5.5	1.4	5	2.8	13.5	2.6	13.5	3.4	3.5	3.1	29	1.6	118	19.1	8	·	·	·	2	1	·	·	11	22	12	5	·	·	5
VIII	1.5	2.7	11	2.0	8	1.6	8	1.9	9	4.4	15	2.3	6.5	2.6	4	2.5	30	1.7	234	67.9	1	·	·	·	3	1	·	8	13	16	10	7	·	·	1
IX	1	2.5	10	2.0	10.5	1.6	9	2.4	13.5	5.7	11.5	3.5	6	2.9	1.5	3.3	27	2.2	104	27.9	11	·	·	·	1	2	1	4	6	14	8	4	1	·	·
X	·	·	13.5	1.5	15	1.2	5.5	1.5	1.5	1.7	3	2.0	3.5	4.6	2	2.2	49	0.8	17	3.7	31	·	·	23	·	·	·	8	5	9	6	·	3	·	1
XI	2	2.2	18	1.6	7	1.4	3.5	2.3	3.5	4.6	9	6.3	12.5	4.4	4.5	3.2	30	2.1	40	9.6	30	8	10	27	·	4	2	2	13	16	7	·	6	17	·
XII	3.5	2.1	11.5	1.7	2.5	2.2	1	3.0	8	3.1	15.5	3.3	14	2.8	9	2.9	28	1.9	43	7.8	13	11	12	28	·	1	·	1	17	20	12	·	3	26	·
Rok	23	2.0	167.5	1.7	89	1.5	60	1.8	62.5	3.4	149.5	3.0	115.5	3.3	52	2.8	376	1.6	1250	67.9	1.VIII	61	68	182	8	14	4	34	150	218	144	37	20	137	17

Antołówka $H_s = 918$ m $h_w = 18{,}5$ m

I	12.5	1.4	1.5	1.0	·	·	4	1.5	15	5.0	12	2.9	4	2.6	3	1.8	41	1.6	54	8.0	31	3	17	28	·	7	4	1	19	16	13	·	6	31	·
II	10.5	1.5	0.5	2.0	·	·	·	·	5.5	3.6	24.5	3.1	10.5	2.3	4.5	2.2	28	1.8	80	10.1	18	18	24	28	·	4	2	1	16	18	15	1	2	28	·
III	13	2.1	3.5	2.4	3	1.3	5	4.0	19	5.9	9.5	2.9	2.5	3.8	1.5	2.0	36	2.3	61	13.7	27	4	6	23	·	3	2	4	16	18	14	1	6	30	·
IV	5	2.4	9.5	2.4	2.5	2.8	4.5	3.3	12	2.4	9	2.4	9.5	2.6	5	2.5	33	1.6	71	16.7	21	·	1	11	·	2	·	1	20	21	14	3	8	3	2
V	6	2.2	2	2.0	1	2.0	3	4.5	18.5	2.6	15.5	2.7	10.5	2.6	10.5	2.7	26	1.9	146	32.4	6	·	·	5	·	4	1	1	22	24	20	4	4	·	6
VI	5	1.3	3.5	1.9	·	·	3	5.5	14.5	4.2	10.5	2.8	13	3.2	11.5	2.5	29	2.1	284	60.2	10	·	·	·	1	1	·	1	11	19	14	9	2	·	8
VII	5.5	2.1	5.5	2.3	·	·	1	7.5	18	3.4	24.5	2.3	6	2.8	6.5	2.0	26	1.9	129	30.2	8	·	·	·	·	4	·	·	12	20	14	5	4	·	8
VIII	7	2.1	6	1.8	0.5	1.0	3.5	2.1	27.5	4.4	9	3.2	11	2.3	9.5	2.9	19	2.5	241	67.0	1	·	·	·	2	4	·	4	15	15	11	7	3	·	2
IX	14	2.2	5	2.4	·	·	7	3.5	31	4.4	8.5	2.7	4	2.4	4.5	2.2	16	2.7	120	29.9	11	·	·	·	·	9	1	4	6	12	9	6	3	·	1
X	9.5	1.3	3.5	1.1	7	1.1	5	1.0	11	1.5	5	2.4	4.5	1.2	16.5	1.5	31	0.9	18	3.4	31	·	·	15	·	·	·	12	2	10	7	·	1	·	1
XI	3.5	1.4	3.5	1.3	·	·	·	·	16	9.7	20	3.8	13	2.4	7	1.4	27	3.1	44	11.5	21	9	10	25	·	7	6	2	16	18	9	2	4	16	·
XII	13	1.3	0.5	1.0	·	·	0.5	4.0	15	5.9	16.5	1.9	15	2.4	11.5	1.7	21	2.1	47	7.5	18	5	9	27	·	7	2	1	19	17	12	·	1	26	·
Rok	104.5	1.8	44.5	1.8	14	0.7	36.5	3.1	203	4.4	164.5	2.8	103.5	2.6	91.5	2.1	333	2.0	1295	67.0	1.VIII	39	67	162	3	52	18	32	174	208	152	38	43	134	28

Smolnik $H_s = 510$ m

I	24	4.2	·	·	2	5.0	7	5.3	47	4.5	·	·	1	4.0	6	6.0	6	4.3	52	14.0	31	7	14	28	·	·	·	·	18	19	13	1	2	31	—
II	35	5.9	2	6.5	10	2.8	4	5.8	20	4.8	2	4.0	1	4.0	6	5.3	4	4.9	29	4.5	8	15	27	28	·	·	·	2	18	18	10	·	1	28	—
III	21	3.9	·	·	2	5.5	7	4.1	38	5.2	·	·	1	4.0	12	4.8	12	4.1	53	11.3	2	7	5	21	·	2	·	3	14	15	12	2	4	20	—
IV	18	2.9	4	3.5	12	4.0	3	3.3	32	3.5	·	·	7	3.0	2	2.0	12	2.9	47	8.0	28	·	·	19	·	1	·	2	9	14	10	·	1	2	—
V	31	3.8	·	·	8	1.5	9	3.0	24	2.8	·	·	5	3.0	4	4.5	12	2.8	88	12.8	25	·	·	7	·	1	·	2	18	18	14	3	2	·	—
VI	27	3.1	2	5.0	3	1.3	4	2.0	24	3.1	1	2.0	2	2.5	2	4.0	25	2.2	159	26.2	4	·	·	·	3	·	·	2	8	17	16	7	3	·	—
VII	20.5	1.7	0.5	1.0	9	2.2	1	1.0	32	2.7	·	·	8	3.6	2	4.0	20	1.9	153	25.5	25	·	·	·	4	·	·	4	8	18	16	7	1	·	—
VIII	32	2.7	1	7.0	5	2.4	1	1.0	26	2.7	·	·	1	1.0	1	4.0	26	1.9	147	44.2	26	·	·	·	1	·	·	6	13	13	10	6	9	·	—
IX	8	3.5	·	·	5	2.8	4	3.0	56	3.0	1	2.0	2	1.5	1	4.0	13	2.5	80	42.0	11	·	·	1	·	·	·	5	4	8	5	2	4	·	—
X	30	2.5	·	·	11	2.9	2	4.0	27	2.0	·	·	1	2.0	1	4.0	21	1.9	11	3.6	29	1	·	17	·	·	·	6	8	9	5	·	4	·	—
XI	25	3.6	1	4.0	4	1.8	2	4.0	40	4.3	·	·	2	1.5	5	5.8	11	3.5	114	29.1	21	5	10	24	·	3	·	1	18	15	12	4	·	17	—
XII	17	4.6	·	·	5	2.8	5	3.8	58	4.2	·	·	·	·	·	·	8	3.8	50	8.4	10	3	11	27	·	3	·	·	22	19	13	·	1	22	—
Rok	288.5	3.5	10.5	2.2	76	2.9	49	3.4	424	3.6	4	0.7	31	2.5	42	4.0	170	3.1	983	44.2	26.VIII	38	67	172	8	10	·	33	158	183	136	32	32	120	—

Uwaga. Prędkości wiatru oceniano na podstawie skali Beauforta i notowano w m/s, kierunki wiatru są orientacyjne, oceniane przez obserwatora wg ustawienia klatki meteorologicznej.

Kuźnice $H_s = 1023$ m $h_w = 21{,}5$ m

I	10.5	1.3	10	1.9	2.5	1.0	1.5	3.7	24.5	5.3	13.5	3.8	·	·	2.5	1.0	28	2.4	74	12.9	31	5	14	27	·	2	1	1	16	20	15	1	6	31	·
II	15	1.6	8.5	2.2	0.5	3.0	1	2.5	18	3.5	11	3.0	·	·	2	1.0	28	1.7	116	17.4	18	22	27	28	·	·	·	3	18	20	17	4	2	28	·
III	8.5	1.1	3.5	1.9	2	2.0	2	6.5	29	4.8	17	3.3	·	·	2	1.0	29	2.5	96	18.8	27	6	8	27	·	4	1	5	18	21	15	2	6	31	·
IV	11	1.5	5.5	2.5	0.5	3.0	2	1.0	17.5	2.7	11.5	2.0	1.5	1.0	1.5	1.0	39	1.2	101	25.4	21	·	1	16	·	·	·	2	19	23	17	3	11	14	·
V	12	1.8	7.5	2.5	3	1.3	2	5.8	21.5	3.3	17.5	1.9	1	1.0	0.5	3.0	28	1.7	177	45.7	6	·	·	6	·	1	1	1	17	25	22	7	5	1	3
VI	15.5	2.7	10	3.4	4	3.9	2.5	2.4	19	4.0	12.5	3.4	·	·	1.5	1.0	25	2.4	335	66.9	10	·	·	·	1	2	·	1	12	20	17	9	5	·	5
VII	7	1.6	9.5	1.9	2.5	1.0	4.5	1.2	21.5	3.9	15.5	2.7	·	·	1.5	2.3	31	1.8	167	39.1	8	·	·	·	·	1	1	·	10	21	17	7	3	·	6
VIII	8	1.2	8.5	1.4	2.5	1.8	3	2.0	25.5	3.2	20.5	3.2	·	·	3	1.0	22	2.0	274	67.5	1	·	·	·	2	2	·	4	14	16	12	7	5	·	1
IX	7.5	1.1	5.5	1.9	1.5	3.0	2.5	4.0	36.5	3.5	23.5	2.7	3	1.3	2	1.0	8	2.5	145	34.3	11	·	·	·	·	1	·	5	6	14	12	5	1	·	·
X	15	1.2	2.5	1.8	2.5	1.8	1.5	1.0	25	1.8	23	1.8	0.5	1.0	4	1.1	19	1.3	24	4.5	8	·	·	21	·	·	·	11	4	10	7	·	3	·	1
XI	7	1.7	6	2.0	·	·	0.5	1.0	21	6.2	13.5	4.5	·	·	1	1.0	41	2.4	100	32.3	21	8	11	27	·	4	2	3	16	19	12	3	6	20	·
XII	4.5	1.4	8	1.4	0.5	3.0	1.5	1.7	33	4.9	20	4.2	1	1.0	0.5	3.0	24	2.9	85	10.7	10	5	12	30	·	5	3	·	20	22	16	2	1	31	·
Rok	121.5	1.5	85	2.1	22	2.1	24.5	2.7	292	3.9	199	3.0	7	0.4	22	1.4	322	2.1	1694	67.5	1.VIII	46	73	182	3	22	9	36	170	231	179	50	54	156	16

Łysa Polana — φ = 49°16' — λ = 20°07' — 1965

MIESIĄC	CIŚNIENIE P: P_m	Max	Min	$P_{o,m}$	TEMPERATURA T: $\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	ŚREDNIA PRĘŻNOŚĆ PARY e_m: I	II	III	Dies	ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m: I	II	III	Dies	ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m: I	II	III	Dies	ŚREDNIE ZACHMURZENIE N_m: I	II	III	Dies
I	–	–	–	–	0.3	−7.8	8.5	1	−18.1	8	−5.3	−1.0	−4.5	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.8	7.4	7.2
II	–	–	–	–	−4.9	−14.1	1.4	13	−23.1	7	−11.5	−6.4	−10.4	−9.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.2	7.2	6.8
III	–	–	–	–	3.4	−6.5	9.8	19	−17.2	11	−4.1	1.8	−2.5	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.9	7.3	6.6
IV	–	–	–	–	6.7	−1.7	12.5	7	−10.2	2	0.6	5.3	1.0	2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	7.2	7.4
V	–	–	–	–	11.0	1.9	21.3	19	−6.8	4	5.2	9.4	5.2	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.9	7.7	7.3
VI	–	–	–	–	18.6	6.2	27.1	26	−1.1	3	10.9	15.2	10.2	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.3	6.9	6.4
VII	–	–	–	–	17.5	6.7	24.5	15	0.6	10	11.9	15.3	10.8	12.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	6.0	6.3
VIII	–	–	–	–	16.1	6.5	27.9	7	1.3	3, 31	10.0	14.3	9.8	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.7	6.3	6.4
IX	–	–	–	–	16.4	5.0	23.8	3	−0.9	22	8.3	14.5	8.8	10.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.8	4.7	5.4
X	–	–	–	–	11.4	−1.7	20.5	2	−7.4	22	0.2	10.1	1.8	3.5	–	–	–	–	–	–	–	–	–	–	–	–	4.5	3.6	3.0	3.7
XI	–	–	–	–	2.6	−6.6	12.9	1	−18.0	18	−4.6	0.3	−3.5	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	6.0	6.3
XII	–	–	–	–	1.2	−7.6	8.9	20	−18.7	13	−3.2	−1.1	−3.8	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.6	7.3	7.0
Rok	–	–	–	–	8.4	−1.6	27.9	7. VIII	−23.1	7. II	1.5	6.5	1.9	3.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.4	6.4

Dolina Chochołowska — φ = 49°15' — λ = 19°49'

I	–	–	–	–	0.9	−7.1	8.3	1	−18.7	7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−5.6	−14.7	4.7	1	−24.5	6	−11.8	−7.4	−11.0	−10.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.4	−6.3	10.5	19	−18.5	1	−4.0	1.4	−2.3	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	6.2	−1.4	11.9	7	−9.2	2	0.2	4.7	0.8	1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	10.1	1.3	19.9	18	−6.7	4	3.3	8.4	4.5	5.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16.3	6.2	26.8	26	−0.9	3	8.5	14.7	9.5	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	16.4	7.1	23.9	15	1.0	10	10.3	14.9	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	15.2	6.4	26.3	7	1.4	31	8.3	13.7	9.4	10.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	15.6	5.8	21.9	3	−0.3	22	8.6	14.2	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	10.8	−1.2	21.3	1	−7.5	21	−0.2	10.0	2.3	3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	1.9	−6.1	12.1	2	−18.0	17	−4.0	0.0	−2.9	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1.4	−6.6	9.5	20	−17.6	15	−3.2	−1.1	−2.8	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	7.7	−1.4	26.8	26. VI	−24.5	6. II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Myślenickie Turnie — φ = 49°15' — λ = 19°59'

I	–	–	–	–	−0.5	−6.2	6.1	31	−14.1	7	−4.0	−3.2	−3.1	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.2	7.6	7.8
II	–	–	–	–	−7.4	−13.8	6.7	1	−19.9	6	−11.6	−9.9	−11.3	−11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	7.6	7.4
III	–	–	–	–	0.7	−5.6	7.2	19	−12.8	10	−3.3	−1.5	−3.0	−2.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.3	7.0	7.2
IV	–	–	–	–	3.6	−1.8	9.6	7	−9.9	1	−0.2	1.8	0.3	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	7.1	7.9
V	–	–	–	–	7.5	1.5	17.3	18	−5.9	3	3.2	5.6	4.2	4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.2	7.9	8.0
VI	–	–	–	–	14.1	6.5	24.3	26	1.9	14	9.1	11.7	9.6	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.4	7.3	7.0
VII	–	–	–	–	14.5	8.1	21.2	15	2.3	6	10.6	12.0	10.5	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	6.8	7.5
VIII	–	–	–	–	12.9	7.0	23.4	8	0.0	2	8.6	10.4	9.1	9.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.5	6.3	6.7
IX	–	–	–	–	12.7	6.6	19.0	2, 3	1.7	20	8.9	10.8	9.1	9.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	6.1	6.5
X	–	–	–	–	8.7	2.3	18.2	2	−6.1	21	4.6	6.3	5.0	5.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.8	4.4	4.8
XI	–	–	–	–	0.3	−6.1	11.6	1	−15.7	17	−3.2	−2.3	−3.1	−2.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.3	7.0	7.2
XII	–	–	–	–	−0.6	−6.5	11.4	20	−14.5	15	−3.8	−3.3	−3.9	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.8	8.1
Rok	–	–	–	–	5.5	−0.7	24.3	26. VI	−18.9	6. II	1.6	3.2	2.0	2.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	6.9	7.2

Hala Gąsienicowa — φ = 49°15' — λ = 20°00'

I	837.5	847.6	816.3	–	−1.3	−7.6	4.4	31	−17.5	7	−5.0	−3.5	−4.2	−4.2	3.2	3.7	3.5	3.5	75	78	76	76	1.2	1.2	1.2	1.2	7.4	7.5	7.3	7.4
II	837.0	847.0	820.0	–	−8.6	−15.6	4.0	1	−21.5	7	−13.2	−11.0	−12.4	−12.2	1.9	2.0	1.8	1.9	81	78	76	77	0.4	0.7	0.6	0.6	7.4	6.9	7.1	7.1
III	841.6	854.7	818.8	–	−0.6	−7.3	4.5	30	−15.8	10	−4.2	−2.5	−3.9	−3.6	3.5	4.0	3.6	3.7	75	77	74	75	1.1	1.3	1.2	1.2	6.9	7.0	5.9	6.6
IV	837.9	850.5	823.9	–	2.3	−3.2	6.7	7	−12.1	2	−1.0	0.9	−0.6	−0.3	4.6	4.9	4.8	4.8	81	75	82	79	1.1	1.8	1.2	1.4	7.3	8.0	6.7	7.3
V	842.7	853.0	832.9	–	6.1	0.2	14.5	18	−8.7	3	2.5	4.4	3.0	3.2	5.8	6.2	6.4	6.1	78	74	83	78	1.9	2.5	1.6	2.0	7.8	8.1	7.9	7.9
VI	846.1	853.9	833.1	–	12.2	4.9	22.6	26	−0.8	3	8.6	10.6	8.2	8.9	8.0	8.8	9.0	8.6	72	70	82	75	3.6	4.5	2.2	3.4	6.3	7.2	6.8	6.8
VII	846.1	852.7	838.8	–	12.8	6.5	19.9	15	0.7	5	10.0	11.1	8.9	9.7	8.8	9.7	9.1	9.2	72	73	79	75	3.8	4.0	2.6	3.5	6.6	8.1	6.3	7.0
VIII	847.9	855.0	836.6	–	11.3	5.2	21.7	7	−0.2	2	7.8	9.3	7.6	8.1	7.9	8.2	8.3	8.1	77	73	81	77	3.2	4.2	2.6	3.3	6.4	7.5	6.0	6.6
IX	847.6	860.1	838.4	–	11.7	5.4	17.3	3	0.2	20	8.1	10.3	8.2	8.7	7.5	8.3	7.4	7.7	69	68	69	69	3.6	4.6	3.7	4.0	6.3	6.6	4.7	5.9
X	850.7	858.1	842.5	–	8.4	0.5	17.8	2	−7.8	21	3.0	6.6	3.0	3.9	3.9	5.6	4.6	4.7	52	58	60	57	4.1	4.8	3.3	4.1	6.0	4.7	3.6	4.4
XI	837.3	854.2	818.7	–	0.0	−7.1	9.7	1	−16.3	23, 24	−4.1	−2.3	−3.9	−3.6	3.1	3.7	3.2	3.3	68	72	70	70	1.7	1.9	1.7	1.8	7.1	7.1	5.9	6.7
XII	834.2	846.1	819.0	–	−1.1	−7.7	10.0	20	−16.5	15	−4.6	−3.9	−4.5	−4.4	3.2	3.4	3.3	3.3	70	74	74	73	1.3	1.3	1.3	1.3	7.8	7.6	7.0	7.5
Rok	842.2	850.1	816.3	–	4.4	−2.1	22.6	26. VI	−21.5	7. II	0.7	2.5	0.8	1.2	5.1	5.7	5.4	5.4	72	72	76	73	2.2	2.7	1.9	2.3	6.9	7.2	6.3	6.8

Łysa Polana H_s = 988 m h_w = 16,8 m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_mD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) Temperatura T: Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr V: V≥10	V≥15	◔	●	Opad R: R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	5	1.8	8	2.2	7	2.1	10	2.8	7.5	3.9	17	2.1	5.5	1.9	·	·	33	1.6	56	7.9	31	11	19	30	·	—	—	1	14	18	14	·	3	31	·
II	12	2.3	17.5	1.9	12	2.2	6	2.6	2.5	2.8	8.5	2.9	3.5	3.4	2	2.5	20	1.8	82	11.6	8	22	24	28	·	—	—	4	13	21	15	2	·	28	·
III	5.5	2.4	9.5	2.4	9	2.3	9.5	2.3	4.5	3.9	18.5	3.1	5	2.3	0.5	2.0	31	1.8	66	11.1	27	10	6	30	·	—	—	4	12	20	15	1	3	31	·
IV	10	2.1	14.5	1.9	8	2.0	7.5	2.3	4.5	3.0	15.5	2.5	5	2.9	2	2.0	23	1.7	71	13.4	21	1	2	22	·	—	—	1	16	22	14	3	7	15	1
V	14	2.2	6.5	2.1	5	2.0	10	2.5	11	3.1	24.5	2.4	7	2.1	3	2.3	12	2.1	140	38.6	6	·	·	11	·	—	—	1	14	25	20	3	2	·	5
VI	0.5	3.0	11	2.5	5.5	2.3	12.5	2.6	6	3.2	31	2.6	13.5	2.5	4	2.5	6	2.4	283	58.4	10	·	·	1	1	—	—	1	9	19	15	9	·	·	6
VII	7	2.4	5.5	2.4	4.5	2.6	10	2.0	13	3.1	25.5	2.8	10.5	2.4	1	3.0	16	2.2	116	19.9	8	·	·	·	·	—	—	2	6	21	16	5	1	·	8
VIII	8.5	2.1	13.5	2.1	5	2.5	8	2.2	7.5	3.7	19.5	2.6	6.5	2.2	0.5	2.0	24	1.8	233	61.4	1	·	·	·	2	—	—	2	10	18	10	6	2	·	2
IX	·	·	4.5	2.3	3.5	2.3	18	3.0	15	4.9	16.5	2.8	11.5	2.9	2	2.0	19	2.6	102	22.7	11	·	·	1	·	—	—	6	6	15	12	3	1	·	1
X	10	2.3	11	2.0	11	2.2	11	2.6	5.5	2.5	11	1.9	3.5	2.3	·	·	30	1.5	16	3.2	29	·	·	24	·	—	—	11	2	9	7	·	2	·	1
XI	7.5	2.1	8.5	2.1	6	2.1	18	2.9	4.5	4.9	8	4.8	5	3.8	1.5	2.0	31	2.0	49	17.9	21	8	10	27	·	—	—	1	11	16	8	1	4	17	·
XII	7.5	2.3	12	1.9	4.5	2.2	17.5	2.6	5	3.2	23	3.5	7	2.1	0.5	2.0	16	2.2	65	14.1	18	11	12	28	·	—	—	2	12	23	15	1	·	27	·
Rok	87.5	2.1	122	2.2	81	2.2	138	2.5	86.5	3.5	218.5	2.8	83.5	2.6	17	1.9	261	2.0	1279	61.4	1, VIII	63	73	202	3	—	—	36	125	227	161	34	25	149	24

Dolina Chochołowska H_s = 1028 m h_w = 19 m I–VIII, 18,9 m IX–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	7	3.7	5.5	2.5	7.5	1.4	2.5	1.4	15.5	4.9	9	5.7	·	·	1	1.0	45	2.0	43	8.4	4	13	13	27	·	4	·	—	—	16	10	·	—	31	—
II	17	2.6	13	3.0	5	1.2	1.5	1.3	16.5	2.0	·	·	·	·	·	·	31	1.5	56	12.5	18	22	26	28	·	1	·	—	—	21	16	1	—	28	—
III	3	4.7	12	2.5	6	1.7	1	10.0	25	4.5	9	11.6	·	·	·	·	37	3.0	45	8.6	27	7	6	28	·	6	2	—	—	18	8	·	—	31	—
IV	7.5	1.6	14.5	2.5	5	2.6	·	·	15	2.0	7	2.6	·	·	·	·	41	1.2	95	21.3	21	·	1	18	·	2	·	—	—	19	16	4	—	30[2]	—
V	9.5	2.3	10.5	3.2	·	·	·	·	23.5	4.0	5.5	1.6	·	·	·	·	44	1.7	164	29.5	6	·	·	7	·	2	1	—	—	23	19	6	—	3	—
VI	6.5	2.6	23	2.1	1.5	1.0	4	1.5	20.5	2.2	2.5	16.4	·	·	·	·	32	1.8	313	59.9	10	·	·	1	1	1	1	—	—	20	16	9	—	·	—
VII	4.5	1.9	10.5	2.3	2	1.5	1	2.0	21	3.6	6	2.2	·	·	·	·	48	1.4	193	31.2	16	·	·	·	·	1	1	—	—	21	17	7	—	·	—
VIII	8.5	1.6	27.5	1.9	1	2.0	2	1.5	23.5	3.1	6.5	4.0	·	·	·	·	24	1.8	264	69.6	1	·	·	·	2	1	·	—	—	16	10	8	—	·	—
IX	1	2.0	11	1.3	13.5	1.2	2.5	3.2	23	4.7	22	10.5	·	·	·	·	17	4.2	134	34.5	11	·	·	1	·	8	4	—	—	12	11	5	—	·	—
X	·	·	25	1.5	32	1.2	8	1.8	1	2.0	2	2.0	·	·	·	·	25	1.0	17	7.8	31	·	·	21	·	·	·	—	—	6	5	·	—	·	—
XI	3	1.7	19	2.2	10	1.6	·	·	2	5.0	12	11.3	·	·	·	·	44	2.3	84	34.2	21	8	11	26	·	7	2	—	—	14	8	2	—	20	—
XII	2.5	2.2	9.5	1.8	7	1.6	1.5	3.7	6.5	8.2	10	8.8	2	8.0	·	·	54	2.1	62	9.4	10	10	10	30	·	5	2	—	—	20	15	·	—	30	—
Rok	70	2.2	181	2.2	90.5	1.4	24	2.2	193	3.8	91.5	6.4	2	0.7	1	0.1	442	2.0	1470	69.6	1. VIII	60	67	187	3	38	13	—	—	206	151	42	—	173[2]	—

Myślenickie Turnie H_s = 1360 m h_w = 19,5 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	2.5	4.0	9.5	2.9	7.5	1.4	1	1.0	7	4.2	35.5	8.7	8	5.3	2	6.0	20	4.7	39	6.0	31	6	16	29	·	9	4	2	18	16	12	·	7	31	·
II	9.5	4.6	14	3.0	8.5	2.3	4.5	1.8	1	1.0	19.5	5.0	7.5	3.7	2.5	3.0	17	2.9	54	9.7	18	25	27	28	·	5	·	4	18	20	15	·	1	28	·
III	3	4.0	12.5	2.1	9	1.7	3	1.0	9	8.4	33.5	7.3	5	6.5	·	·	18	4.4	53	13.7	27	8	11	30	·	10	3	3	16	19	10	1	7	31	·
IV	5	3.4	12	2.5	14	2.0	3.5	1.9	9	3.7	25.5	4.9	6	4.4	2	2.0	13	3.0	84	19.7	21	·	3	26	·	2	·	1	19	21	14	3	10	30	1
V	4.5	4.3	18.5	2.6	12.5	1.9	3.5	1.4	12.5	3.2	21	5.1	5.5	6.8	2	5.0	13	3.1	195	48.5	6	·	·	13	·	3	2	1	20	24	21	6	5	23	4
VI	11.5	4.3	17	2.8	13.5	2.0	2	1.0	7	5.4	25.5	5.4	8.5	3.9	·	·	5	3.7	363	55.3	10	·	·	·	·	4	2	1	12	19	17	10	7	·	6
VII	3.5	2.9	17	1.9	10.5	1.6	8	1.1	11	3.1	29.5	5.6	8.5	5.2	1	3.0	4	3.4	186	32.1	8	·	·	·	·	3	1	·	16	21	18	6	3	·	7
VIII	4	3.0	16	2.9	17.5	2.0	4.5	1.7	12	2.9	28	7.2	4	4.1	1	5.0	6	3.9	248	51.3	1, 26	·	·	·	·	6	1	2	13	19	12	7	7	·	2
IX	·	·	6	3.1	12.5	1.6	8.5	1.5	17.5	6.5	37.5	8.7	5.5	6.7	0.5	4.0	2	5.9	179	32.5	19	·	·	·	·	12	5	4	9	13	12	6	3	·	·
X	2.5	4.2	21	1.3	22	1.2	3.5	1.6	11	1.9	20.5	3.0	5.5	2.0	1	4.0	6	1.8	16	4.9	29	·	1	13	·	2	·	9	6	9	5	·	5	·	1
XI	0.5	3.0	13	2.0	8.5	1.5	1	1.0	6.5	3.5	29.5	8.1	10.5	4.6	1.5	5.7	19	4.0	63	15.0	21	8	13	25	·	8	5	2	15	15	12	3	9	21	·
XII	3.5	3.9	3	3.0	7	2.0	2	1.5	11	6.1	52	8.6	3	7.0	2.5	9.0	9	6.4	62	11.2	18	3	19	29	·	12	8	·	17	22	13	1	4	31	·
Rok	50	3.5	159.5	2.5	143	1.8	45	1.4	114.5	4.2	357.5	6.5	77.5	5.0	16	3.9	132	3.9	1542	55.3	10.VI	50	90	193	·	76	31	29	179	218	161	43	68	195	21

Hala Gąsienicowa H_s = 1520 m H_b = 1520,8 m h_w = 16 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	V≥10	V≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	K (K)
I	1	3.0	6	3.0	3.5	4.4	1.5	3.7	10.5	10.1	50.5	5.4	3	2.7	·	·	17	4.6	54	11.6	10	10	17	30	·	8	2	2	15	19	12	1	7	31	·
II	9	4.6	14	2.4	2	1.0	1.5	2.0	4.5	4.3	36	3.4	4.5	3.1	5.5	3.3	7	3.0	81	16.4	18	26	27	28	·	2	·	5	18	20	16	2	5	28	·
III	3	4.0	·	·	·	·	·	·	13.5	9.6	54.5	5.2	8.5	2.4	6.5	2.8	7	5.0	83	15.4	27	10	14	31	·	7	2	4	13	22	13	2	10	31	·
IV	8	3.1	7	2.2	·	·	·	·	9	6.3	42.5	3.9	7.5	2.0	3	4.7	13	3.2	89	18.4	21	2	4	27	·	2	·	1	14	23	16	2	16	30	1
V	6.5	2.7	7	2.6	·	·	1	4.0	5	7.7	44	4.0	13.5	2.3	7	2.7	9	3.3	222	56.5	6	·	·	16	·	5	·	1	16	25	23	6	14	25	5
VI	9.5	2.8	6.5	3.8	1.5	3.3	2	3.5	9.5	7.7	31	3.9	10	2.6	11	3.1	9	3.5	399	75.0	10	·	·	1	·	3	·	1	10	19	17	11	12	·	9
VII	7	2.1	2.5	2.2	·	·	·	·	7.5	6.1	50.5	4.2	12.5	2.9	3	3.0	10	3.5	187	34.7	8	·	·	·	·	2	1	·	8	22	18	6	7	·	8
VIII	6	3.2	5	2.5	1	4.0	·	·	11	6.0	39.5	4.2	14	2.4	11.5	2.2	5	3.5	327	91.6	26	·	·	2	·	3	·	2	13	19	13	8	13	4	2
IX	2.5	2.6	1	2.0	0.5	2.0	3	2.2	20.5	9.5	50.5	6.4	5	2.5	3	2.3	4	6.1	155	32.2	11	·	·	·	·	11	3	5	7	14	13	5	7	1	1
X	3.5	2.4	3	2.7	·	·	2.5	3.2	8	2.8	50.5	3.5	15.5	2.4	5	2.4	5	2.9	18	3.6	29	·	1	17	·	·	·	9	4	9	8	·	7	2	1
XI	2	1.0	3	1.3	1	4.0	1	3.5	13.5	7.3	42	5.2	3.5	3.3	3	2.7	21	3.9	67	23.6	21	9	12	26	·	6	2	3	12	21	10	1	9	21	·
XII	8	3.6	·	·	·	·	·	·	7.5	9.3	60	6.0	7.5	3.9	8	2.6	2	5.5	72	13.2	18	9	22	29	·	9	1	·	13	23	17	1	7	31	·
Rok	66	2.9	55	2.1	9.5	1.6	12.5	1.8	120	7.2	551.5	4.6	105	2.7	66.5	2.6	109	4.0	1754	91.6	26.VIII	66	97	207	·	58	11	33	143	236	176	45	114	204	27

Hala Ornak — φ = 49°14' — λ = 19°51' — 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies		I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.1	−7.5	7.4	1	−19.4	7, 8	−4.6	−1.1	−3.9	−3.4		–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	6.9	7.4
II	–	–	–	–	−5.9	−15.2	3.8	1	−24.9	6	−12.5	−7.0	−11.9	−10.8		–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.9	7.5	7.3
III	–	–	–	–	3.0	−6.8	10.1	19	−19.9	1	−4.3	2.1	−3.0	−2.0		–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	6.2	6.6
IV	–	–	–	–	5.7	−2.3	11.5	7	−10.2	2	0.1	4.2	0.2	1.2		–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	5.7	6.6
V	–	–	–	–	9.8	0.4	19.4	18	−8.1	4	3.9	8.2	3.8	4.9		–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.4	7.0	7.1
VI	–	–	–	–	16.3	5.4	26.4	26	−2.5	3	9.1	14.8	9.5	10.8		–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.7	7.2	6.7
VII	–	–	–	–	16.4	6.3	24.8	15	−0.4	10	10.1	14.7	9.8	11.1		–	–	–	–	–	–	–	–	–	–	–	–	6.6	8.4	7.0	7.3
VIII	–	–	–	–	14.9	5.3	25.4	8	0.0	31	8.1	13.2	8.5	9.6		–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.8	6.3	6.8
IX	–	–	–	–	15.1	4.5	21.2	3	−1.9	22	7.5	13.5	8.4	9.4		–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.1	4.8	5.5
X	–	–	–	–	10.4	−2.9	21.0	1, 2	−9.3	21	−1.2	9.5	0.4	2.3		–	–	–	–	–	–	–	–	–	–	–	–	3.4	3.3	2.2	3.0
XI	–	–	–	–	1.4	−6.8	11.5	1	−18.9	17	−5.0	−0.2	−3.8	−3.2		–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.9	6.4	6.8
XII	–	–	–	–	0.9	−7.3	11.1	20	−19.3	15	−3.7	−1.3	−3.1	−2.8		–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	6.5	7.4
Rok	–	–	–	–	7.3	−2.2	26.4	26.VI	−24.9	6. II	0.6	5.9	1.2	2.2		–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	6.1	6.5

Kasprowy Wierch — φ = 49°14' — λ = 19°59'

I	788.5	798.9	768.7	–	−4.4	−10.0	0.4	12	−18.2	7	−7.7	−6.4	−6.7	−6.9		3.0	3.2	3.2	3.1	86	84	82	84	0.6	0.7	0.7	0.7	7.6	8.4	7.8	7.9
II	786.6	796.6	771.7	–	−12.1	−18.0	−0.8	1	−23.6	6	−15.8	−14.3	−15.3	−15.2		1.6	1.7	1.6	1.6	86	82	81	83	0.3	0.4	0.4	0.4	7.4	6.6	7.6	7.2
III	792.7	805.9	771.2	–	−3.8	−9.6	0.5	19	−17.2	1	−6.9	−5.6	−6.9	−6.6		3.0	3.6	3.0	3.2	79	88	80	82	0.8	0.5	0.8	0.7	7.4	7.5	6.8	7.2
IV	789.7	800.1	776.5	–	−1.6	−5.9	2.2	9	−14.1	1	−4.4	−2.7	−3.6	−3.6		4.3	4.6	4.4	4.4	95	91	93	93	0.2	0.5	0.4	0.4	8.3	8.0	7.7	8.0
V	795.0	804.9	784.3	–	1.9	−2.7	8.9	18	−10.4	2	−1.3	0.1	−0.4	−0.5		5.1	5.7	5.8	5.5	88	91	95	91	0.7	0.6	0.3	0.5	8.5	8.7	8.4	8.5
VI	799.3	808.6	785.8	–	8.9	2.4	19.9	26	−2.5	3	4.3	6.8	4.9	5.2		7.1	8.0	8.2	7.8	85	82	94	87	1.5	2.2	0.7	1.5	6.7	7.8	7.9	7.5
VII	799.5	807.3	791.3	–	9.0	3.7	16.7	15	−2.4	6	5.5	7.1	5.9	6.1		8.0	9.0	8.2	8.4	87	89	87	88	1.3	1.4	1.4	1.4	7.2	9.0	7.3	7.8
VIII	800.8	808.7	787.8	–	7.9	2.8	17.2	8	−2.7	2	4.0	5.7	4.8	4.8		7.0	7.8	7.6	7.5	87	86	89	87	1.4	1.8	1.4	1.5	6.5	8.0	6.5	7.0
IX	800.6	811.9	791.2	–	7.8	2.5	13.7	23	−2.1	20	4.6	6.1	4.8	5.1		6.8	7.5	6.6	7.0	81	82	79	81	1.9	2.1	2.2	2.1	6.8	7.3	6.4	6.8
X	803.0	809.8	793.4	–	5.1	−0.9	13.8	2	−8.2	20, 21	1.4	3.4	1.6	2.0		3.5	4.9	3.9	4.1	52	62	56	57	3.6	3.4	3.3	3.4	4.9	4.9	3.9	4.6
XI	788.7	806.2	770.4	–	−2.7	−8.5	7.5	8	−20.0	16	−6.3	−5.1	−5.7	−5.7		2.9	3.4	2.9	3.1	70	81	74	77	1.3	1.2	1.4	1.3	7.4	7.5	6.5	7.1
XII	785.5	798.9	772.4	–	−5.3	−11.1	6.2	20	−18.6	14, 15	−8.5	−7.8	−8.6	−8.4		3.1	3.3	3.0	3.1	90	94	91	92	0.3	0.2	0.4	0.3	8.4	8.4	8.0	8.3
Rok	794.2	811.9	768.7	–	0.9	−4.6	19.9	26.VI	−23.6	6. II	−2.6	−1.1	−2.1	−2.0		4.6	5.2	4.9	4.9	83	84	83	83	1.2	1.2	1.1	1.2	7.3	7.7	7.1	7.4

Dolina Pięciu Stawów — φ = 49°13' — λ = 20°03'

I	–	–	–	–	−3.1	−8.3	2.8	31	−16.0	7	−5.8	−5.0	−5.4	−5.4		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−9.5	−16.4	−0.6	1	−22.0	6	−14.0	−11.8	−12.9	−12.9		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	−1.4	−9.6	4.5	29, 30	−17.2	1	−5.7	−3.8	−5.8	−5.3		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	0.6	−5.2	4.5	7	−15.1	2	−2.3	−1.1	−2.6	−2.2		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	4.1	−2.4	12.5	18, 19	−11.1	4	−0.1	2.2	0.3	0.7		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	11.5	2.9	25.1	26	−1.5	3	6.4	9.7	6.6	7.3		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	11.4	4.4	21.7	16	−3.0	6	7.1	9.5	7.2	7.8		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	9.9	3.1	21.0	8	−2.3	3	6.0	7.8	6.5	6.7		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	11.0	3.8	16.5	23	−0.9	20	6.6	8.9	7.3	7.5		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	7.8	−0.5	16.4	2	−7.3	21	2.5	5.6	2.3	3.2		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	−2.2	−8.0	9.6	8	−20.9	17	−5.5	−4.1	−5.6	−5.2		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	−3.6	−10.5	5.2	19	−19.1	16	−7.4	−5.9	−7.1	−6.9		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	3.0	−3.9	25.1	26.VI	−22.0	6. II	−1.0	1.0	−0.8	−0.4		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Morskie Oko — φ = 49°12' — λ = 20°04'

I	–	–	–	–	−0.6	−8.6	5.4	1	−21.1	7	−5.0	−3.4	−4.3	−4.2		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	−7.7	−16.6	−1.8	21	−25.6	5	−13.2	−9.6	−12.6	−12.0		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	1.7	−8.0	8.4	30	−20.1	10	−4.6	−0.2	−3.8	−3.1		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	4.1	−3.4	8.6	7	−13.5	2	−0.6	2.4	−0.4	0.2		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	8.2	0.1	15.6	19	−9.9	3	2.3	5.6	3.0	3.5		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	14.1	4.6	23.7	26	−1.1	3	8.2	12.2	8.0	9.1		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	14.4	6.6	22.4	15	0.5	10	9.7	12.2	9.5	10.2		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	13.3	5.3	25.1	8	−0.4	27	7.7	10.8	8.5	8.9		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	13.5	5.4	19.1	3	0.5	22	8.2	11.7	8.2	9.1		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	10.8	0.0	19.2	2	−7.7	21	1.6	7.5	2.3	3.4		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	0.7	−6.8	10.4	8	−16.3	25	−4.6	−2.1	−3.9	−3.6		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	0.0	−8.5	10.8	20	−17.9	15	−4.1	−3.4	−4.1	−3.9		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	6.0	−2.5	25.1	8. VIII	−25.6	5. II	0.5	3.6	0.9	1.5		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Hala Ornak $H_s = 1110$ m $h_w = 17{,}8$ m 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD}																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr V		◔	●	Opad R			≡	⊠	K (K)
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					$Min < -10°$	$Max < 0°$	$Min < 0°$	$Max > 25°$	$V \geq 10$	$V > 15$			$R \geq 0.1$	$R \geq 1.0$	$R \geq 10.0$			
I	10	1.8	1	3.0	2.5	2.4	0.5	2.0	18	5.2	3	1.7	1	1.0	2	1.0	55	1.4	68	13.7	10	11	15	27	·	1	·	2	17	20	13	1	17	31	—
II	24	1.5	·	·	·	·	1	3.0	3	4.3	3.5	1.3	1.5	1.7	·	·	51	0.7	70	10.8	8	23	26	28	·	·	·	4	15	21	14	1	21	28	—
III	13.5	1.1	2	6.0	·	·	2.5	3.0	24	5.9	1	3.0	0.5	3.0	1.5	2.3	48	2.0	31	8.1	29	9	5	29	·	3	·	5	13	19	8	·	18	31	—
IV	12	2.3	·	·	·	·	2	2.0	10	2.4	·	·	·	·	·	·	66	0.6	35	5.7	21	1	1	21	·	·	·	4	11	19	13	·	15	30	—
V	16	1.9	4	2.8	·	·	3	6.7	6	2.0	·	·	1	5.0	1	3.0	62	0.9	48	14.7	31	·	·	9	·	1	·	4	18	22	12	1	20	7	—
VI	20.5	1.9	·	·	1	1.0	2	8.0	10	4.3	2	2.5	1	1.0	3.5	1.3	50	1.2	369	78.5	10	·	·	1	1	1	·	2	12	20	15	9	9	·	—
VII	4	1.0	·	·	·	·	0.5	1.0	14.5	2.5	2.5	1.4	1.5	1.7	1	1.0	69	0.5	202	33.3	8	·	·	1	·	·	·	·	12	22	17	8	9	·	—
VIII	10	1.8	·	·	·	·	·	·	18	4.2	1	3.0	0.5	1.0	1.5	1.0	62	1.1	316	78.1	26	·	·	·	1	1	·	4	16	18	12	8	12	·	—
IX	3	1.0	1	1.0	0.5	1.0	2	1.0	40.5	5.7	·	·	·	·	1	1.0	42	2.7	152	34.2	11	·	·	4	·	4	·	6	8	14	9	5	3	·	—
X	9	1.4	·	·	1	1.0	·	·	1	3.0	·	·	2.5	1.8	1.5	1.0	78	0.2	20	6.4	31	·	·	24	·	·	·	15	2	7	4	·	3	·	—
XI	8	1.2	·	·	·	·	·	·	21	5.1	0.5	1.0	6.5	1.6	1	1.0	53	1.4	78	22.0	21	8	10	27	·	2	·	4	15	18	11	3	11	20	—
XII	11	2.1	·	·	2	5.0	4	5.8	18.5	3.8	6	2.2	2.5	3.0	·	·	49	1.6	82	8.5	5	10	12	30	·	1	·	·	15	22	18	·	11	31	—
Rok	141	1.6	8	1.1	7	0.9	17.5	2.7	184.5	4.0	19.5	1.3	18.5	1.7	14	1.0	685	1.2	1471	78.5	10.VI	62	69	201	2	14	·	50	154	222	146	36	149	178	—

Kasprowy Wierch $H_s = 1991$ m $H_b = 1988{,}8$ m $h_w = 15{,}4$ m

I	10	9.6	6	5.2	3.5	3.1	17	8.2	30	9.5	11	9.1	7.5	8.6	6	9.8	2	8.5	114	19.1	10	16	29	31	·	23	12	·	18	21	18	3	23	31	·
II	29.5	9.9	8.5	7.7	1.5	2.7	2	7.2	5	10.9	9.5	6.9	5	9.1	22	8.4	1	8.7	155	22.7	8	28	28	28	·	23	8	5	16	23	20	5	27	28	·
III	19	6.6	7.5	4.3	1.5	8.7	11	9.6	35.5	10.1	9.5	5.5	4	4.8	3	4.8	2	7.8	161	26.1	2	12	30	31	·	20	7	2	16	25	18	5	24	31	·
IV	22.5	5.3	5	3.9	·	·	12.5	4.5	26.5	6.3	8.5	5.6	5	6.7	6	6.8	4	5.4	144	25.7	22	2	23	30	·	12	1	2	19	26	19	5	27	30	2
V	28	6.3	5	4.3	0.5	1.0	8.5	6.9	20	9.0	10.5	6.2	9.5	7.2	9	6.5	2	6.9	217	55.8	6	1	12	23	·	18	4	1	22	25	24	6	27	31	6
VI	24	7.4	5	5.9	0.5	4.0	9	7.6	16.5	8.2	9	7.8	11.5	5.2	9.5	5.0	5	6.6	374	66.9	10	·	·	9	·	22	7	1	13	19	18	10	24	10	8
VII	12.5	4.6	2	4.2	1	3.0	9.5	9.1	12.5	8.3	17.5	6.7	21	6.2	11	4.8	6	6.0	211	25.8	16	·	·	5	·	16	4	·	16	22	18	9	25	1	7
VIII	30	6.6	3	2.2	·	·	6.5	10.5	21.5	7.8	13	6.0	11	4.5	7	4.6	1	6.5	290	67.6	26	·	·	10	·	15	7	1	13	17	13	7	20	8	2
IX	9	6.5	3	4.2	1.5	4.0	14	11.6	41	11.5	13	8.6	4	5.9	1.5	4.7	3	9.5	149	28.1	4	·	1	6	·	20	12	5	13	15	14	6	22	4	·
X	21.5	5.5	14	4.5	2.5	1.6	2.5	4.2	13.5	7.0	15	5.3	13	5.4	6	5.0	5	5.0	16	3.5	11	·	4	17	·	10	·	9	3	9	8	·	14	4	1
XI	12	5.6	6.5	3.6	0.5	1.0	7	12.6	27.5	8.9	20.5	6.9	11	8.5	4	5.0	1	7.5	108	26.5	21	12	22	27	·	15	8	1	16	21	14	4	20	25	·
XII	13	7.9	2	5.8	·	·	5	12.6	29	12.7	17.5	10.2	18	9.4	7.5	6.3	1	10.1	102	13.9	14	23	27	31	·	26	15	·	18	27	21	2	29	31	·
Rok	231	6.8	67.5	4.6	13	2.4	104.5	8.7	278.5	9.2	154.5	7.1	120.5	6.8	92.5	6.0	33	7.4	2041	67.6	26.VIII	94	176	248	·	220	85	27	183	250	205	62	282	234	26

Uwaga. Kierunki i prędkości wiatru – wg anemografu, w okresach obladzenia tego przyrządu prędkości wiatru mierzono anemotachimetrem.

Dolina Pięciu Stawów $H_s = 1668$ m $h_w = 13{,}6$ m

I	4	4.2	·	·	3	2.3	5	8.0	10	12.4	19	11.1	14	8.4	·	·	38	5.5	45	8.1	17	10	27	31	·	10	7	—	—	20	10	·	15	31	—
II	4	1.5	7	3.1	8	3.4	4	4.0	3	5.7	7	10.7	23	9.7	·	·	28	4.6	118	19.8	27	28	28	28	·	7	3	—	—	21	18	3	6	28	—
III	6	7.8	1	2.0	3	9.0	1	2.0	4	3.2	24	5.7	16	9.9	·	·	38	4.2	72	19.6	31	11	17	31	·	10	1	—	—	17	13	2	17	31	—
IV	15	4.8	4	2.2	1	9.0	4	7.0	1	15.0	11	4.0	16	6.9	1	2.0	37	3.2	74	11.2	1	2	12	28	·	8	·	—	—	19	14	1	10	30	—
V	25	5.0	3	3.0	1	1.0	·	·	1	3.0	2	3.5	17	11.1	·	·	44	3.6	151	34.1	15	3	4	19	·	8	4	—	—	20	17	5	6	31	—
VI	8	4.1	3	4.7	3	4.0	·	·	1	7.0	17	5.6	4	6.2	·	·	54	2.1	328	37.7	3	·	·	3	1	3	1	—	—	19	18	11	6	20	—
VII	33	5.2	3	5.3	·	·	·	·	6	10.7	11	10.5	12	5.5	4	9.2	24	5.0	243	42.6	17	·	·	3	·	10	1	—	—	22	19	10	2	·	—
VIII	43	7.6	·	·	·	·	·	·	7	8.7	8	10.6	7	9.6	·	·	28	5.8	241	61.1	26	·	·	8	·	13	2	—	—	15	12	8	5	8	—
IX	1	3.0	1	5.0	2	5.0	·	·	7	10.9	26	11.0	18	9.3	·	·	35	6.1	119	30.5	4	·	·	2	·	15	8	—	—	13	10	5	4	·	—
X	9	4.3	·	·	·	·	·	·	18	6.2	5	3.0	8	2.6	·	·	53	2.0	12	4.7	29	·	2	17	·	3	1	—	—	4	3	·	5	2	—
XI	13	1.4	·	·	·	·	1	2.0	8	16.2	18	12.1	15	11.4	1	20.0	34	6.2	59	14.0	29	13	17	27	·	12	10	—	—	16	10	3	8	21	—
XII	6	7.5	·	·	·	·	·	·	21	10.7	13	13.2	31	8.1	1	12.0	21	7.6	94	18.1	14	17	27	30	·	19	6	—	—	22	15	2	10	31	—
Rok	167	4.7	22	2.1	21	2.8	15	1.9	87	9.1	161	8.4	181	8.2	7	3.6	434	4.7	1556	61.1	26.VIII	84	134	227	1	118	44	—	—	208	159	50	94	233	—

Morskie Oko $H_s = 1400$ m $h_w = 14$ m

I	13.5	3.5	3.5	7.1	2	11.0	4.5	9.8	7.5	11.7	20	10.4	2	7.0	1	5.0	39	4.9	69	9.2	10	11	15	28	·	13	4	—	—	23	17	·	3	31	—
II	18	3.8	7	7.4	3	3.7	4	10.5	1	8.0	10	8.3	·	·	1	3.0	40	3.2	94	26.4	18	26	28	28	·	6	1	—	—	24	20	2	1	28	—
III	9	3.1	2	7.0	1	20.0	1	20.0	9.5	4.8	14	11.1	9.5	7.4	·	·	47	3.8	81	12.2	1	12	8	30	·	6	2	—	—	21	18	3	4	31	—
IV	10	3.7	8.5	5.1	1.5	5.3	4	3.8	4	6.8	14	4.3	9	3.7	2	3.0	37	2.5	99	18.4	21	2	2	26	·	6	·	—	—	24	18	3	6	30	—
V	26.5	2.8	2.5	3.2	·	·	1	14.0	8	5.3	14	4.8	3	3.0	1	4.0	37	2.4	180	30.1	23	·	·	13	·	3	3	—	—	24	20	6	3	31	—
VI	21.5	2.9	6.5	2.5	1.5	5.0	3.5	3.6	7.5	4.4	14.5	7.2	4	2.8	4	3.8	27	2.9	453	74.1	11	·	·	1	·	6	4	—	—	21	17	10	3	2	—
VII	12	2.1	1	6.0	9	4.6	7.5	7.9	10.5	5.5	11	8.1	1	6.0	2	3.0	39	3.1	227	36.2	4	·	·	·	·	6	3	—	—	24	19	9	2	·	—
VIII	26.5	2.5	6	4.8	4.5	8.0	8	1.3	4	7.9	6	5.1	6	5.0	1	10.0	31	3.6	225	63.9	1	·	·	1	1	7	5	—	—	20	15	7	2	·	—
IX	8	3.0	4	6.8	4.5	12.0	7.5	6.1	9.5	18.3	20.5	11.5	8	2.9	2	5.5	26	6.6	184	37.5	11	·	·	·	·	13	10	—	—	16	14	5	·	·	—
X	27	2.3	·	·	1	5.0	1	8.0	5	4.2	6	4.3	2	1.5	·	·	51	1.3	9	2.9	29	·	1	18	·	·	·	—	—	8	4	·	4	·	—
XI	18	2.4	·	·	2	6.0	·	·	8	5.3	14	12.0	9	6.6	·	·	39	3.6	138	57.8	21	9	10	28	·	8	5	—	—	21	10	4	7	20	—
XII	18.5	4.4	3.5	4.0	2	9.5	4	5.8	7	13.6	25	11.1	7	5.1	2	2.5	24	5.9	125	18.2	10	12	15	30	·	16	11	—	—	26	19	4	3	31	—
Rok	208.5	3.0	44.5	4.5	32	7.5	46	7.6	81.5	8.0	169	8.2	60.5	4.2	16	3.3	437	3.6	1884	74.1	11.VI	72	79	203	1	90	48	—	—	252	191	53	38	204	—

Ustrzyki Górne $\varphi = 49°07'$ $\lambda = 22°40'$ 1965

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.1	−6.5	3.8	31	−20.8	12	−3.7	−1.3	−3.5	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.8	6.9	7.6
II	–	–	–	–	−5.6	−13.5	4.6	1	−27.5	10	−10.5	−6.9	−9.5	−9.1	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.5	7.1	7.8
III	–	–	–	–	4.3	−4.4	11.8	30	−23.1	11	−2.1	2.8	−0.2	0.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.6	7.1	7.6
IV	–	–	–	–	9.3	−0.8	13.8	8	−6.3	6	2.3	8.1	2.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	6.5	7.7
V	–	–	–	–	13.2	3.7	23.9	19	−6.7	4	7.5	11.4	7.8	8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	6.5	7.2
VI	–	–	–	–	19.1	7.2	26.9	26	1.7	8	12.6	17.5	11.8	13.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.3	6.6	6.7
VII	–	–	–	–	19.4	9.1	25.6	16	2.9	12	13.0	18.2	13.2	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	6.3	6.6
VIII	–	–	–	–	17.8	6.9	26.2	8	1.4	31	10.6	16.5	9.9	11.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	5.2	6.1
IX	–	–	–	–	18.1	5.1	24.2	2	−1.2	17	9.1	17.0	9.2	11.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.3	3.9	5.2
X	–	–	–	–	10.8	−0.5	22.4	2	−9.2	22	2.0	10.0	3.0	4.5	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.0	4.3	5.1
XI	–	–	–	–	2.3	−3.8	11.7	8	−17.4	18	−1.9	0.9	−1.4	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.2	8.7	8.8
XII	–	–	–	–	0.5	−3.8	6.7	10	−12.1	9	−1.7	−0.6	−1.4	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	9.4	9.3	9.1	9.3
Rok	–	–	–	–	9.1	−0.1	26.9	26.VI	−27.5	10.II	3.1	7.8	3.4	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	6.5	7.1

Ustrzyki Górne

$H_s = 650\ m$ $h_w = 20\ m$ 1965

MIESIĄC	ROZKŁAD WIATRU n_D, V_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr V V ≥ 10	V > 15	◔	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K (K)
I	11.5	3.1	8.5	3.2	·	·	1	4.0	41.5	5.8	2.5	5.4	·	·	1	5.0	27	3.5	76	19.4	31	5	19	29	·	7	1	1	18	19	16	1	5	31	–
II	40	4.0	·	·	·	·	·	·	21	5.9	·	·	1	2.0	·	·	22	3.4	59	7.3	8	16	27	28	·	5	2	·	15	21	17	·	·	28	–
III	12	4.3	5	5.2	·	·	2	4.5	34	8.2	4	4.2	·	·	·	·	36	4.1	86	23.6	2	4	4	23	·	6	4	3	19	16	12	2	2	21	–
IV	16	4.7	10	3.6	1	2.0	1	8.0	24	5.3	2	2.0	·	·	1	6.0	35	2.9	91	13.0	21	·	1	20	·	2	·	1	16	19	14	5	1	2	–
V	23	4.0	10	3.8	1	2.0	2	2.0	22	7.6	2	2.5	·	·	·	·	33	3.3	158	29.3	24	·	·	6	·	3	1	1	15	21	19	5	·	1	–
VI	12	4.2	6	2.5	·	·	2	4.5	18	3.9	4	3.8	·	·	·	·	48	1.8	166	27.9	4	·	·	·	3	1	·	2	11	15	13	7	2	·	–
VII	8	2.5	11	2.7	·	·	·	·	28	5.4	1	6.0	1	1.0	·	·	44	2.2	217	46.7	25	·	·	·	1	3	·	2	8	19	19	6	3	·	–
VIII	9	3.4	7	3.1	1	3.0	·	·	20	5.6	3	4.0	·	·	3	3.0	50	2.0	171	29.5	26	·	·	·	1	2	·	6	14	16	12	7	8	·	–
IX	4	2.8	7	3.1	·	·	1	2.0	33.5	5.5	4.5	3.2	·	·	·	·	40	2.6	91	39.9	11	·	·	1	·	3	·	7	7	11	6	2	6	·	–
X	16.5	4.1	7.5	6.3	1	6.0	2	8.0	25	6.4	1	8.0	·	·	·	·	40	3.3	21	5.0	4	·	·	18	·	8	·	6	8	10	6	·	5	·	–
XI	17	5.0	8.5	2.8	0.5	4.0	2	4.5	32	8.7	6	4.0	·	·	·	·	24	4.5	173	42.8	30	3	10	22	·	9	2	1	24	20	16	5	1	18	–
XII	13.5	2.5	3.5	4.3	·	·	2	2.5	51	6.7	3	11.3	·	·	·	·	20	4.6	158	35.8	10	4	15	26	·	7	2	·	25	21	18	5	5	26	–
Rok	182.5	3.7	84	3.4	4.5	1.4	15	3.3	350	6.2	33	4.5	2	0.2	5	1.2	419	3.2	1467	46.7	25.VII	32	76	173	5	56	12	30	180	208	168	45	38	126	–

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TABLICA III

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

DATES LIMITES DU GEL

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Aleksandrowice	20.V	12.X	144
Antołówka	22.V	10.X	140
Augustów	22.V	-	-
Babia Góra	31.V	10.X	131
Baligród	22.V	13.X	143
Bartoszyce	7.V	12.X	157
Barwinek	22.V	22.IX	122
Bełsk	31.V	12.X	133
Biała Podlaska	8.V	12.X	156
Białowieża	22.V	11.X	141
Biały Kościół	4.V	21.X	169
Białystok	5.V	12.X	159
Biebrza	8.VI	21.IX	104
Biecz	4.V	13.X	161
Bielsk Podlaski	5.V	12.X	159
Bieruń Stary	4.V	12.X	160
Bierutowice	22.V	11.X	141
Biłgoraj	21.V	7.X	138
Bircza	21.V	13.X	144
Biskupiec	4.V	12.X	160
Bochnia-Chodenice	4.V	12.X	160
Bodzentyn	22.V	12.X	142
Bolesławiec	1.IV	13.X	194
Borusowa	4.V	12.X	160
Brwinów	4.V	12.X	160
Brzegi Dolne	22.V	17.IX	117
Brzezna	4.V	12.X	160
Bukowina Tatrzańska	21.V	12.X	143
Busko-Zdrój	4.V	12.X	160
Bydgoszcz	22.V	12.X	142
Bydgoszcz, IMiUZ	4.V	12.X	160
Bystrzyca Kłodzka	22.V	11.X	141
Bytom	3.V	13.X	162
Chełm Lubelski	5.V	7.X	154
Chodzież	4.V	12.X	160
Chojnice	4.V	12.X	160
Chorzelów	4.V	12.X	160
Ciechocinek	3.V	12.X	161
Cieplice Śl.-Zdrój	22.V	6.X	136
Cieszyn-Bobrek	4.V	12.X	160
Ciężkowice	21.V	12.X	143
Czarna Dąbrówka	31.V	12.X	133
Czarniecka Góra	22.V	12.X	142
Czarny Dunajec	22.V	22.IX	122
Czernichów	4.V	13.X	161
Częstochowa	4.V	12.X	160
Czorsztyn	22.V	11.X	141
Czorsztyn-Nadzamcze	21.V	7.X	138
Darłowo	3.V	20.X	169
Dębica	4.V	13.X	161
Długopole-Zdrój	21.V	11.X	142

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Dobrogoszcz	3.V	13.X	162
Dolina Chochołowska	3.VI	22.IX	110
Dolina Pięciu Stawów	Temperatura spadała poniżej 0° we wszystkich miesiącach roku		
Duszniki Zdrój	21.V	11.X	142
Dynów	4.V	12.X	160
Dziwnów	5.IV	12.XI	220
Elbląg	3.V	21.X	170
Felin	4.V	12.X	160
Garlica Murowana	4.V	12.X	160
Gdańsk-Nowy Port	4.V	9.XI	188
Gdańsk-Wrzeszcz	2.V	9.XI	190
Gdynia	6.IV	13.XI	220
Giżycko	4.V	12.X	160
Gliwice	3.V	13.X	162
Głodowo	22.V	12.X	142
Głogów	23.III	12.X	202
Głubczyce	4.V	13.X	161
Głuchołazy	3.V	13.X	162
Gniezno	4.V	12.X	160
Gołdap	16.V	11.X	147
Gorzów Wlkp.	3.V	12.X	161
Gorzyń	3.V	12.X	161
Goszyce	4.V	13.X	161
Grabowiec	4.V	12.X	160
Grabownica	4.V	12.X	160
Grodków	3.V	13.X	162
Grudziądz	3.V	21.X	170
Gryfice	5.IV	12.X	189
Gubałówka	21.V	10.X	141
Hala Gąsienicowa	Temperatura spadała poniżej 0° również w letnich miesiącach		
Hala Ornak	10.VII	17.IX	68
Hel	31.V	8.XI	160
Hopowo	31.V	26.X	147
Horyniec	21.V	12.X	143
Inowrocław	4.V	12.X	160
Istebna-Kubalonka	20.V	12.X	144
Istebna-Stecówka	21.V	12.X	143
Istebna-Zaolzie	3.VI	22.IX	110
Iwonicz-Zdrój	4.V	13.X	161
Jabłonka	3.VI	12.X	130
Jabłonowo Pomorskie	4.V	21.X	169
Jakubowice	4.V	13.X	161
Janów Lubelski	4.V	12.X	160
Jarosław	4.V	12.X	160
Jasło	4.V	13.X	161
Jastrowie	22.V	12.X	142
Jastrzębie-Zdrój	4.V	13.X	161
Jaworzyna Krynicka	20.V	-	-

STACJA	Temperatura spadła poniżej 0° po raz ostatni	Temperatura spadła poniżej 0° po raz pierwszy	Okres bez przymrozków (dni)
Jazy	21.V	11.X	142
Jelenia Góra	22.V	11.X	141
Jeziory	2.V	12.X	162
Kalisz	4.V	12.X	160
Kamienica	22.V	22.IX	122
Kamienica Królewska	31.V	12.X	133
Kamień Krajeński	22.V	12.X	142
Karpacz	21.V	11.X	142
Kartuzy	4.V	8.XI	187
Kasprowy Wierch	Temperatura spadała poniżej 0° we wszystkich miesiącach roku		
Katowice	4.V	12.X	160
Kętrzyn	4.V	12.X	160
Kielce	22.V	12.X	142
Kisielnica	5.V	12.X	159
Kłodzko	4.V	11.X	159
Kmiecin	31.V	21.X	142
Kolbuszowa	4.V	12.X	160
Kolno	5.V	12.X	159
Koło	4.V	12.X	160
Kołobrzeg	3.V	12.XI	192
Komańcza	22.V	22.IX	122
Kończewice	4.V	21.X	169
Kopna Góra	22.V	11.X	141
Korfantów	4.V	13.X	161
Koszalin	3.V	26.X	175
Kościerzyna	31.V	12.X	133
Kórnik	4.V	12.X	160
Kraków-Balice	4.V	12.X	160
Kraków-Chełm	4.V	12.X	160
Kraków-Nowa Huta	4.V	12.X	160
Kraków, Obserw.Astr.UJ	4.V	13.X	161
Krasnystaw	4.V	7.X	155
Kraśnik Lubelski	4.V	12.X	160
Krosno	21.V	13.X	144
Krościenko	22.V	7.X	137
Krynica	21.V	12.X	143
Krynica-Góra Parkowa	21.V	12.X	143
Krynica Morska	10.IV	12.XI	215
Krzemień	4.V	12.X	160
Krzyż	31.V	12.X	133
Kudowa-Zdrój	21.V	11.X	142
Kuźnica	22.V	10.X	140
Kwidzyń	31.V	22.X	143
Laskowice Oławskie	4.V	12.X	160
Lądek Zdrój	21.V	11.X	142
Legionowo	4.V	12.X	160
Legnica	3.V	12.X	161
Lesko	4.V	12.X	160
Leskowiec	21.V	12.X	143
Leszno-Strzyżewice	2.V	12.X	162
Leżajsk	8.V	12.X	156
Lębork	4.V	12.X	160
Libertów	4.V	13.X	161
Lidzbark	31.V	12.X	133
Lidzbark Warmiński	4.V	12.X	160
Limanowa	22.V	12.X	142
Lipki	5.IV	12.X	189
Lipowa	4.V	13.X	161
Lubaczów	8.V	7.X	151
Lublin	8.V	12.X	156
Lubliniec	4.V	12.X	160
Luboń Wielki	21.V	10.X	141
Łagiewniki	4.V	12.X	160
Łącko	4.V	12.X	160
Łeba	4.V	20.X	168
Łosice	4.V	12.X	160
Łowicz	4.V	12.X	160
Łódź-Lublinek	4.V	12.X	160
Łódź-Ruda Pabian.	22.V	12.X	142
Łysa Polana	3.VI	22.IX	110
Maków Podhalański	4.V	12.X	160
Malbork	4.V	21.X	169
Maniowy	22.V	12.X	142
Miastko	22.V	12.X	142
Miechów	4.V	12.X	160
Mielec	4.V	12.X	160
Międzybrodzie Bialskie	4.V	13.X	161
Międzyzdroje	5.IV	23.X	200
Mikołajki	4.V	21.X	169
Mława	4.V	12.X	160
Młochów	4.V	12.X	160
Morąg	31.V	12.X	133
Morskie Oko	Temperatura spadała poniżej 0° również w letnich miesiącach		
Motycz	4.V	12.X	160
Mszana Dolna	4.V	12.X	160
Muszyna	22.V	12.X	142
Myczkowce	8.V	13.X	157
Myślenice	4.V	12.X	160
Myślenickie Turnie	21.V	9.X	140
Nałęczów	22.V	12.X	142
Namysłów	3.V	12.X	161
Nidzica	31.V	12.X	133
Niepołomianów	4.V	12.X	160
Nisko	8.V	12.X	156
Nowa Wieś	4.V	7.X	155
Nowe Miasto n.Pilicą	4.V	12.X	160
Nowogard	3.V	12.X	161
Nowy Dwór Mazowiecki	4.V	15.X	163
Nowy Sącz	4.V	13.X	161
Nowy Targ	8.V	12.X	156
Nur	4.V	12.X	160
Obidowa	21.V	12.X	143

STACJA	Temperatura spadła poniżej 0° po raz ostatni	Temperatura spadła poniżej 0° po raz pierwszy	Okres bez przymrozków (dni)
Oborniki Śląskie	2.V	13.X	163
Ochaby	4.V	12.X	160
Olecko	4.V	12.X	160
Olesno	4.V	12.X	160
Olkusz	4.V	12.X	160
Olsztyn Dajtki	4.V	12.X	160
Oława-Zwierzyniec	3.V	13.X	162
Opoczno	4.V	12.X	160
Opole	4.V	12.X	160
Opole Lubelskie	4.V	12.X	160
Orneta	4.V	21.X	169
Ostrołęka	4.V	12.X	160
Ostroszowice	4.V	12.X	160
Ostrowy	22.V	12.X	142
Ostróda	4.V	21.X	169
Ostrów Wielkopolski	3.V	12.X	161
Ostrzeszów	4.V	12.X	160
Otmuchów	4.V	12.X	160
Ożańsk	4.V	12.X	160
Paproć	2.V	10.X	160
Pętkowo	4.V	12.X	160
Piaszczyna	4.V	12.X	160
Piotrków Trybunalski	4.V	12.X	160
Pisz	22.V	12.X	142
Piwniczna	4.V	12.X	160
Pleszew	4.V	12.X	160
Płock-Radziwie	4.V	12.X	160
Polanica-Zdrój	21.V	11.X	142
Połczyn-Zdrój	31.V	12.X	133
Porąbka	4.V	12.X	160
Poronin	Temperatura spadała poniżej 0° we wszystkich miesiącach roku		
Poświętne	4.V	12.X	160
Poturzyn	5.V	12.X	159
Poznań-Ławica	4.V	12.X	160
Poznań-Sołacz	5.IV	12.X	189
Prabuty	31.V	21.X	142
Prudnik	3.V	12.X	161
Przasnysz	4.V	12.X	160
Przebędowo	3.V	12.X	161
Przedbórz	4.V	12.X	160
Przehyba	21.V	10.X	14[illegible]
Przelewice	3.V	12.X	161
Przemyśl	5.V	21.X	168
Przybroda	3.V	12.X	161
Pszczela Wola	4.V	7.X	155
Pszczyna	4.V	13.X	161
Ptaszkowa	4.V	12.X	160
Puck	2.V	8.XI	189
Puczniew	4.V	12.X	160
Puławy	4.V	12.X	160
Pułtusk	4.V	12.X	160
Raba Wyżna	21.V	12.X	143

STACJA	Temperatura spadła poniżej 0° po raz ostatni	Temperatura spadła poniżej 0° po raz pierwszy	Okres bez przymrozków (dni)
Rabka	21.V	12.X	143
Racibórz	4.V	12.X	160
Radom	4.V	12.X	160
Radostowo	31.V	21.X	142
Radzyń Podlaski	4.V	12.X	160
Reguły	4.V	12.X	160
Reszko	22.V	10.X	140
Rosnowo	22.V	12.X	142
Rozewie	11.IV	12.XI	214
Rożnów	4.V	13.X	161
Różanystok	5.V	11.X	158
Rybnik	4.V	13.X	161
Rymanów-Zdrój	22.V	7.X	137
Rypin	31.V	12.X	133
Rzeszów-Jasionka	8.V	12.X	156
Sandomierz	4.V	12.X	160
Sanok	4.V	13.X	161
Sejny	16.V	11.X	147
Siedlce	4.V	12.X	160
Sielec	8.V	12.X	156
Siemianice	4.V	12.X	160
Siemiatycze	5.V	12.X	159
Sieniawa	22.V	12.X	142
Sieradz	4.V	12.X	160
Silniczka	31.V	12.X	133
Sinołęka	4.V	12.X	160
Skierniewice	4.V	12.X	160
Skroniów	4.V	12.X	160
Słubice	3.V	11.X	160
Słupca	4.V	12.X	160
Słupia Nowa	4.V	12.X	160
Słupsk	3.V	12.X	161
Smolice	4.V	12.X	160
Smolnik	22.V	17.IX	117
Sobieszyn	4.V	12.X	160
Sokołowsko	22.V	11.X	141
Sokółka	5.V	11.X	158
Spalona	21.V	13.X	144
Stańcowa	21.V	10.X	141
Stare Pole	31.V	21.X	142
Stary Sącz	22.V	12.X	142
Staszów	21.V	12.X	143
Strzelna	31.V	12.X	133
Strzyżów	5.V	7.X	154
Suchedniów	31.V	7.X	128
Sulejów	4.V	12.X	160
Sulęcin	22.V	10.X	140
Suwałki	5.V	12.X	159
Szczawnica	22.V	12.X	142
Szczawno-Zdrój	3.V	21.X	170
Szczecin-Dąbie	22.V	12.X	142
Szczecin-Niebuszewo	5.IV	22.X	199
Szczecinek	3.V	12.X	161

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Szczekociny	22.V	12.X	142
Szczerców	4.V	12.X	160
Szczuczyn	22.V	12.X	142
Szczytno	22.V	12.X	142
Szepietowo	5.V	12.X	159
Szklarska Poręba	22.V	10.X	140
Szprotawa	15.IV	12.X	179
Szymanów	3.V	12.X	161
Ślęża	4.V	12.X	160
Śliwice	31.V	12.X	133
Śnieżka	9.VII	20.IX	72
Śrem	3.V	12.X	161
Świbno	4.V	21.X	169
Świder	31.V	12.X	133
Świdnica	3.V	12.X	161
Świdwin	3.V	12.X	161
Świebodzin	5.IV	12.X	189
Świeradów-Zdrój	3.V	20.X	169
Świerklaniec	4.V	12.X	160
Świnoujście	3.V	12.XI	192
Tarnobrzeg	4.V	13.X	161
Tarnogród	4.V	7.X	155
Tarnów	4.V	12.X	160
Tczew	4.V	21.X	169
Terespol	5.V	12.X	159
Tęgoborze	3.V	13.X	162
Tolkmicko	10.IV	8.XI	211
Tomaszów Lubelski II	5.V	7.X	154
Topola-Błonie	4.V	12.X	160
Toruń-Wrzosy	22.V	12.X	142
Trzcińsko-Zdrój	15.IV	10.X	177
Trzebiechów	5.IV	11.X	188
Trzebież	5.IV	12.X	189
Trzebinia	4.V	13.X	161
Trzemeszno	4.V	-	-
Tumbacz	21.V	10.X	141
Tychy	4.V	12.X	160
Tykocin	4.V	12.X	160
Ustka	4.V	8.XI	187
Ustrzyki Górne	21.V	17.IX	118
Wadowice	4.V	12.X	160
Wałcz	4.V	12.X	160
Warka	4.V	12.X	160
Warszawa-Bielany	4.V	21.X	169
Warszawa, Inst.Geogr.UW	11.IV	21.X	192
Warszawa, Obserw.Astr.UW	4.V	21.X	169
Warszawa-Okęcie	4.V	12.X	160
Warszawa, St.Pomp Rz.	4.V	21.X	169
Wądołki Borowe	4.V	12.X	160
Werbkowice	5.V	7.X	154
Wielichowo	3.V	12.X	161
Wieliczka	4.V	13.X	161
Wieliszew	4.V	12.X	160
Wieluń	4.V	12.X	160
Wieniec-Zdrój	22.V	12.X	142
Wierzchowo	22.V	12.X	142
Więcławice	3.V	12.X	161
Wińsko	3.V	21.X	170
Wirty	31.V	12.X	133
Wisła	4.V	12.X	160
Wisznice	4.V	12.X	160
Witów	22.V	11.X	141
Włodawa	5.V	7.X	154
Wojcieszów Górny	3.V	11.X	160
Wolbrom	4.V	12.X	160
Wrocław-Strachowice	4.V	12.X	160
Wschowa	12.IV	10.X	180
Wyrzysk	4.V	12.X	160
Wysowa	22.V	7.X	137
Wyszków	4.V	12.X	160
Zakopane	22.V	7.X	137
Zakrzów	4.V	12.X	160
Zamość-Zamczysko	5.V	7.X	154
Zawiercie	4.V	12.X	160
Zawodzie	22.V	12.X	142
Zawoja	22.V	12.X	142
Zawołocze	5.V	12.X	159
Ząbkowice	4.V	12.X	160
Zbąszyń	2.V	12.X	162
Zdanów	4.V	12.X	160
Zgorzelec	3.V	11.X	160
Zielona Góra	23.III	22.X	212
Zwardoń	21.V	13.X	144
Żarnowa	21.V	13.X	144
Żary	15.IV	12.X	179
Żegiestów-Zdrój	22.V	12.X	142
Żelechów	4.V	12.X	160
Żelistawki	4.V	21.X	169
Żywiec-Sporysz	4.V	12.X	160

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TABLICA IV

USŁONECZNIENIE (w godzinach)

INSOLATION (en heures)

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	0,3	.	0,1	5,9	6,1	0,6	3,4	.	.	.	.	1,3	.	3,2	5,8	.	.	2,7	1,8	1,5	.	.	.	.	.	1,6	.	.	.	.	.	36,3
2	Kołobrzeg	0,7	.	.	5,0	4,8	2,2	2,3	.	.	.	.	1,3	1,2	3,7	4,8	0,9	0,1	0,5	0,1	2,1	.	1,9	1,7	.	.	.	.	.	.	.	0,8	34,1
3	Świnoujście	0,1	0,8	.	4,5	3,9	0,1	.	.	.	0,4	.	0,3	1,7	0,7	2,8	1,0	.	0,1	.	.	.	0,9	3,6	0,2	.	0,1	.	.	.	.	.	21,2
4	Resko	.	.	.	4,3	5,1	0,8	.	.	.	1,7	0,0	0,3	1,6	3,4	5,0	.	0,2	0,9	.	1,5	.	1,0	2,5	0,5	.	.	.	.	.	.	.	28,8
5	Szczecinek	.	2,1	0,1	2,9	4,5	2,1	4,0	.	.	.	.	0,7	.	4,6	5,2	.	.	1,2	0,1	2,0	.	1,5	.	.	.	.	.	.	.	.	.	31,0
6	Chojnice	0,0	2,9	1,7	3,7	5,0	5,4	4,5	.	.	.	0,1	1,7	0,0	4,2	5,7	.	.	1,8	1,3	0,2	.	.	.	.	.	.	.	.	.	.	.	38,2
7	Hel	3,6	.	0,4	5,6	4,4	.	1,8	.	.	.	0,3	.	0,6	3,8	5,2	.	.	3,6	.	0,1	.	.	.	.	.	.	.	.	.	.	4,9	34,3
8	Gdynia	4,8	.	1,0	4,0	.	4,4	.	.	.	.	0,2	.	0,3	5,0	5,2	.	.	3,6	1,5	.	.	0,3	.	.	.	.	.	.	.	.	6,2	36,5
9	Świbno	2,8	0,4	1,5	3,5	4,9	0,1	1,6	.	.	.	0,5	.	0,9	4,1	5,1	.	.	2,9	1,4	.	.	.	.	0,1	.	.	.	.	.	.	3,9	33,7
10	Stare Pole	1,2	0,9	3,4	2,3	4,5	1,0	0,9	.	.	0,5	0,7	.	1,6	4,7	5,5	0,1	.	3,4	2,9	.	.	.	.	0,8	.	.	.	.	.	.	2,2	36,6
11	Radostowo	1,9	0,6	3,4	5,3	5,6	3,8	4,2	.	.	1,1	1,3	0,3	1,1	4,0	5,9	.	.	4,5	.	3,4	.	0,1	0,4	.	.	.	.	.	.	.	1,4	48,3
12	Prabuty	0,7	.	0,8	2,6	4,2	.	4,5	.	0,5	.	2,1	.	.	.	6,2	.	.	4,9	3,1	.	.	.	.	0,2	.	.	.	.	.	.	.	29,8
13	Bydgoszcz, IMiUZ	0,6	.	1,9	4,3	3,8	5,7	4,2	.	0,1	.	1,6	0,6	0,1	5,3	5,9	.	1,2	5,5	3,0	0,3	0,8	.	.	.	.	.	.	.	.	.	.	44,9
14	Suwałki	.	.	.	3,2	1,8	3,0	0,5	.	.	3,1	5,5	0,2	5,0	3,3	1,6	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0,4	29,6
15	Mikołajki	.	0,1	0,0	3,4	-	5,4	-	.	.	1,3	4,9	.	4,4	-	4,5	.	.	0,6	1,5	.	.	.	.	.	.	.	.	.	.	.	3,8	-
16	Biebrza	.	.	.	2,2	2,3	5,2	3,4	.	.	1,3	1,6	.	5,1	3,5	1,7	.	.	1,1	.	.	.	.	.	.	.	.	.	.	.	.	1,0	28,4
17	Białystok	.	.	.	0,4	1,9	2,7	2,5	.	0,1	1,1	2,6	0,0	5,8	2,0	1,2	1,2	.	1,3	.	.	.	.	.	.	1,2	.	.	0,7	.	.	.	24,7
18	Gorzów Wlkp.	.	3,6	.	1,3	0,3	.	1,0	.	.	.	.	3,2	.	3,0	5,8	0,1	0,4	1,6	.	2,2	.	0,3	1,7	.	0,1	.	.	0,7	.	.	.	25,3
19	Przebędowo	0,3	0,9	.	5,5	2,5	.	2,8	.	.	.	3,2	3,5	0,0	5,6	5,7	0,2	0,5	3,4	2,2	2,5	.	0,5	0,5	.	.	.	.	.	.	.	.	39,5
20	Przybroda	.	1,5	.	5,8	2,0	.	2,9	.	.	.	3,5	3,3	0,2	4,1	6,4	0,3	0,6	2,5	2,0	1,8	.	.	1,3	.	.	.	.	.	.	.	.	38,2
21	Poznań-Ławica	0,2	1,1	.	5,1	1,7	.	3,7	.	.	.	2,6	3,5	0,1	4,6	5,6	.	0,3	1,6	1,9	1,7	.	.	0,5	.	.	.	.	.	.	.	.	34,2
22	Plewiska	0,1	1,0	.	5,4	0,8	.	2,6	.	.	.	3,8	3,5	0,2	4,1	6,0	.	0,2	1,5	1,9	1,6	.	0,3	1,0	.	.	.	.	.	.	.	.	34,0
23	Kórnik	0,4	0,6	.	3,1	0,1	.	3,0	.	.	.	3,6	3,8	0,2	5,6	6,4	.	0,3	1,7	2,0	1,6	.	0,1	4,2	.	.	.	.	.	.	.	.	36,7
24	Oborniki Śl.	.	.	.	0,7	.	0,4	4,4	.	.	.	1,7	4,1	2,2	3,9	2,9	.	0,1	4,1	2,0	0,1	.	.	1,5	0,9	.	1,0	.	.	.	.	.	30,0
25	Laskowice Oławskie	.	.	.	.	.	0,7	3,9	0,4	.	.	5,2	3,0	1,2	6,0	6,4	1,5	.	0,4	1,8	.	.	0,8	0,6	.	.	2,1	.	.	1,4	.	.	36,0
26	Ciechocinek	0,3	0,3	.	1,9	4,0	5,1	2,3	.	0,1	3,4	.	0,4	2,0	4,7	5,9	0,2	1,3	5,1	3,1	.	.	.	.	.	.	.	.	.	.	.	.	40,1
27	Więcławice	0,4	1,2	1,3	4,3	3,5	6,4	.	.	0,7	.	3,1	2,4	1,7	5,0	6,1	0,2	.	5,6	3,1	.	.	0,4	.	.	.	.	.	.	.	.	.	45,4
28	Legionowo	.	.	.	2,6	2,9	5,9	0,7	.	.	.	4,5	.	4,9	1,7	4,8	.	.	0,0	3,0	.	.	.	.	.	.	.	.	0,8	.	.	1,7	33,5
29	Warszawa-Bielany	.	.	.	0,8	2,1	2,8	.	.	0,1	.	4,5	0,3	5,4	3,0	4,7	0,0	.	0,2	2,3	.	.	.	.	.	.	.	.	0,7	.	.	0,4	27,0
30	Warszawa, Min.Kom.	0,1	.	.	.	1,3	3,7	0,4	.	.	.	4,2	.	3,7	1,2	.	.	3,2	0,2	3,2	.	.	1,3	.	.	.	.	.	0,4	.	.	.	22,9
31	Międzylesie	.	.	.	0,7	2,3	5,3	2,1	.	.	.	5,2	.	5,8	2,4	4,3	.	.	0,3	2,4	.	.	.	.	.	.	.	.	2,0	.	.	0,2	33,0
32	Brwinów	.	.	.	.	2,9	6,1	.	.	0,0	.	5,1	.	5,1	3,6	3,6	.	.	0,1	2,9	.	.	.	.	.	.	.	.	1,1	.	.	.	30,5
33	Świder	.	.	.	0,6	1,7	5,6	2,3	.	.	.	5,4	.	5,6	2,2	3,5	.	.	0,4	2,0	.	.	.	.	.	.	.	.	1,8	.	.	.	31,1
34	Tępola-Błonie	.	.	.	0,7	2,0	3,8	0,8	.	.	.	4,0	0,1	3,3	4,7	6,0	0,5	.	1,9	4,4	.	.	.	.	.	.	.	.	.	.	.	.	32,2
35	Młochów	.	.	.	0,3	2,3	5,5	.	.	.	.	5,2	.	5,6	4,0	3,9	.	.	0,2	3,5	.	.	.	.	.	.	0,0	.	1,5	.	.	.	32,0
36	Skierniewice	.	.	.	0,5	2,2	5,1	0,3	.	0,2	.	6,3	.	5,8	4,9	5,8	.	0,0	0,5	4,7	.	.	2,1	.	.	.	.	.	0,5	.	.	.	38,9
37	Bełek	.	.	.	0,5	1,8	5,9	0,8	4,4	.	.	.	.	5,5	2,3	3,2	0,0	0,0	0,2	4,1	.	.	.	.	.	.	.	1,3	.	.	.	.	30,0
38	Łódź-Lublinek	.	.	.	0,6	.	1,4	1,5	.	.	.	5,7	.	4,5	3,4	6,0	0,1	.	.	5,8	.	.	2,0	.	.	.	.	.	.	.	.	.	31,0
39	Kalisz	.	0,0	.	1,2	.	0,2	3,1	.	.	.	4,1	0,7	3,0	6,0	6,2	1,8	.	0,5	5,1	.	.	.	0,6	.	.	.	.	.	0,1	.	.	34,6
40	Wieluń	.	.	.	.	.	0,1	4,2	.	.	.	2,9	0,6	3,9	5,5	6,0	0,4	0,3	0,6	5,5	.	.	2,7	0,0	.	.	0,3	.	.	1,4	0,2	.	34,6
41	Szepietowo	.	.	.	2,2	2,5	.	4,0	0,1	.	.	4,7	.	5,1	0,7	2,8	0,8	.	1,1	1,6	.	.	.	.	.	.	.	.	0,7	.	.	.	27,3
42	Białowieża	.	.	.	.	1,5	0,8	1,4	.	0,1	.	5,5	1,6	6,3	2,2	3,3	2,5	0,2	.	0,1	.	.	0,1	.	.	.	.	.	0,2	.	.	2,4	28,2
43	Terespol	.	.	.	.	1,5	1,8	0,6	.	.	.	6,5	4,2	6,4	2,3	2,5	3,5	0,2	1,5	3,5	.	.	0,1	.	.	.	.	.	0,0	.	.	1,3	35,9
44	Sobieszyn	.	.	.	.	1,3	4,0	4,8	.	0,1	.	4,8	1,6	6,6	1,3	2,4	4,4	.	2,4	4,5	.	.	.	.	.	.	.	.	1,9	.	.	0,5	40,6
45	Puławy	.	.	.	.	0,6	3,8	4,5	.	.	.	5,5	1,3	6,1	2,2	1,9	3,9	.	1,8	6,3	.	.	1,7	.	.	.	.	.	1,9	.	.	0,2	41,7
46	Gmina Lubelski	.	.	.	.	0,0	0,2	0,8	.	.	0,0	5,1	4,5	5,7	6,8	2,9	4,5	0,2	.	5,2	.	.	1,4	.	.	.	.	.	0,3	.	.	.	37,6
47	Szczawno-Zdrój	.	.	.	.	.	.	3,0	0,3	0,3	.	4,7	3,6	.	.	6,1	.	.	3,7	.	1,6	.	1,2	1,9	2,1	0,1	0,4	0,2	.	.	.	.	29,2
48	Świeradów	.	.	.	.	.	.	4,8	.	.	.	0,7	3,2	0,2	5,1	6,6	.	.	.	.	0,6	.	.	4,1	1,3	.	.	1,5	0,0	2,4	0,3	.	30,8
49	Opole	.	.	.	.	.	.	3,4	0,1	.	.	4,7	2,8	3,3	5,0	5,3	1,4	0,1	0,3	3,7	.	.	0,4	.	.	.	3,5	.	.	2,5	0,6	.	37,3
50	Kudowa-Zdrój	.	.	.	.	.	.	2,5	.	.	.	0,1	4,8	.	.	3,7	.	.	1,1	0,1	2,6	.	1,0	.	0,3	.	3,4	0,2	.	0,9	.	.	20,7
51	Polanica-Zdrój	.	.	.	.	.	.	4,2	.	.	.	4,1	.	.	5,4	4,5	.	.	2,4	0,8	1,0	.	1,7	3,1	1,2	0,8	1,8	0,1	.	2,6	0,1	.	33,8
52	Skrzeniów	.	.	.	.	.	3,7	3,6	.	.	.	2,5	.	5,3	2,4	4,0	0,0	.	0,1	6,7	.	.	.	.	.	.	0,4	.	0,7	.	2,1	.	31,5
53	Świerklaniec	.	.	.	.	.	1,4	1,5	.	.	.	2,7	0,4	3,7	0,8	2,3	0,1	.	0,1	3,1	.	.	0,5	.	.	.	.	.	.	1,5	.	.	17,9
54	Kraków, Obs.Astr.UJ	.	.	.	.	0,6	3,6	0,2	0,2	.	.	2,6	0,1	3,5	3,7	1,1	.	0,2	0,5	2,6	.	.	.	.	.	.	2,7	.	.	.	2,3	.	23,8
55	Cieszyn	.	.	.	.	.	.	.	.	.	.	5,2	4,9	4,5	3,8	.	.	.	.	3,5	.	.	1,0	.	.	.	0,2	.	.	.	0,5	.	23,6
56	Istebna-Kubalonka	0,1	.	.	.	1,1	0,9	0,6	.	.	.	5,9	5,5	1,3	0,4	1,9	0,2	.	.	4,8	.	.	0,4	0,6	.	.	.	0,1	0,2	.	.	.	24,0
57	Rabka	0,1	.	.	.	1,2	2,7	1,8	.	.	.	6,2	3,3	5,8	4,2	1,3	2,4	0,1	.	5,1	.	.	2,4	.	.	.	5,6	.	0,1	1,5	1,9	.	48,7
58	Jabłonka	.	.	.	.	1,4	2,6	2,3	.	.	.	4,5	2,8	2,9	1,3	2,3	1,5	0,3	.	4,4	1,8	.	3,9	.	.	.	2,6	1,0	.	0,9	2,3	.	38,8
59	Krynica	0,1	.	.	.	2,0	5,5	0,2	.	.	.	4,9	0,8	6,9	2,6	0,5	6,2	.	.	.	.	.	3,0	.	.	.	3,0	.	.	0,2	.	.	35,9
60	Krynica-Góra Park	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
61	Muszyna	.	.	.	0,1	0,8	5,1	0,7	.	.	.	5,5	0,9	6,9	3,7	0,5	5,5	.	.	.	.	.	3,0	.	.	.	1,7	.	.	0,1	.	.	33,9
62	Zakopane	0,9	.	.	.	0,4	2,6	1,3	0,1	.	.	5,3	3,9	6,6	4,6	0,7	5,0	.	.	5,4	0,1	.	3,9	.	.	.	5,8	0,4	0,1	3,8	1,4	.	54,1
63	Gubałówka	0,9	.	.	.	0,9	1,3	1,1	0,3	.	.	5,2	4,3	6,4	3,9	0,9	4,9	0,1	.	4,8	0,2	.	3,7	.	.	.	6,0	0,8	.	4,4	2,5	.	56,2
64	Hala Gąsienicowa	0,9	.	.	.	.	1,1	0,1	.	.	.	4,7	3,1	4,8	.	0,0	4,0	.	.	4,3	0,4	2,0	1,4	.	.	.	3,0	.	.	.	0,1	.	34,9
65	Kasprowy Wierch	1,4	.	.	.	1,1	2,9	2,2	0,0	.	.	7,7	5,0	7,2	6,1	1,3	6,2	.	.	5,1	1,0	3,1	7,4	.	0,4	.	3,8	.	.	.	.	.	57,3
66	Werhowice	.	.	.	.	1,7	0,9	0,4	0,6	.	.	3,2	3,3	7,1	6,9	0,2	5,6	0,4	.	3,4	.	0,2	1,0	.	.	.	.	.	0,1	.	0,4	.	39,4
67	Zdanów	.	.	.	.	.	6,1	1,4	.	.	4,2	.	0,1	5,7	4,8	1,8	4,0	.	1,0	4,4	.	.	2,8	0,2	.	.	.	.	0,3	.	1,8	.	38,0
68	Iwonicz-Zdrój	1,0	.	.	.	1,6	.	.	0,5	.	.	2,1	2,8	4,7	4,3	.	4,9	.	0,2	1,9	.	.	1,0	.	.	.	.	1,0	.	0,2	.	.	28,0
69	Lesko	0,2	.	.	.	1,9	0,3	.	1,7	.	.	4,9	3,5	6,3	6,4	.	5,8	.	.	4,0	0,1	.	1,7	.	.	.	2,0	0,5	1,4	0,1	.	.	40,8

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	Suma
1	Ustka	1,7	6,3	.	.	0,7	.	.	0,0	4,2	3,3	4,6	.	1,1	0,0	1,4	4,6	3,1	.	0,2	.	.	3,3	2,3	0,9	5,4	1,6	.	3,0	49,7
2	Kołobrzeg	2,4	5,3	0,3	0,3	.	.	.	0,2	2,9	3,3	4,0	.	1,4	0,6	1,4	2,7	4,7	2,6	.	.	.	5,7	0,8	2,3	7,9	0,9	0,5	4,4	54,6
3	Świnoujście	1,6	5,2	.	5,2	.	0,1	.	0,3	3,0	0,6	3,8	.	2,1	0,8	0,3	2,1	3,6	3,3	0,1	.	.	5,9	0,3	5,1	7,7	.	3,7	2,1	56,9
4	Resko	1,9	3,9	0,0	.	.	.	.	1,6	2,9	0,3	4,2	.	0,4	.	2,1	4,0	4,4	0,5	.	.	.	4,5	2,5	6,1	7,2	1,6	.	4,4	52,5
5	Szczecinek	2,5	5,6	0,2	.	3,8	.	.	0,7	6,5	0,9	6,5	.	0,0	0,1	1,7	0,4	2,2	.	.	0,6	.	5,6	2,0	7,7	5,7	0,8	2,4	6,7	62,6
6	Chojnice	0,5	3,2	0,2	.	5,5	.	.	1,0	6,8	1,8	6,8	.	.	1,5	4,2	4,6	.	0,3	0,0	1,7	.	6,5	0,2	6,4	4,9	3,5	3,3	7,5	70,4
7	Hel	2,5	3,6	.	0,5	5,2	.	.	2,4	3,9	2,7	7,4	.	0,4	.	2,4	6,2	0,2	.	0,4	2,5	.	4,2	1,0	1,6	3,3	2,5	.	3,0	55,9
8	Gdynia	3,4	.	.	.	5,9	.	1,8	4,1	.	6,8	5,7	.	0,5	1,1	4,2	.	0,4	0,5	.	.	6,4	.	.	4,4	.	4,8	.	.	50,0
9	Świbno	1,6	3,0	0,0	.	6,5	.	.	2,4	4,0	2,0	7,2	.	0,3	0,8	5,0	5,2	0,2	.	0,5	2,7	.	4,2	0,0	2,3	4,3	3,4	.	4,9	60,5
10	Stare Pole	1,1	0,4	.	2,4	7,6	.	.	3,7	6,6	1,9	7,7	.	.	.	6,4	6,8	.	.	.	4,1	.	3,4	0,9	2,8	4,5	5,0	.	5,3	70,6
11	Radostowo	2,6	3,3	.	6,9	.	.	.	2,2	6,4	2,3	8,1	.	.	0,8	6,9	6,1	.	.	.	2,2	.	4,2	1,5	4,1	4,7	4,5	0,3	6,1	73,2
12	Prabuty	1,8	.	2,0	.	6,2	.	.	4,5	6,8	1,2	8,2	.	.	.	4,6	4,3	.	.	.	.	.	6,7	0,9	7,8	.	7,0	.	.	62,0
13	Bydgoszcz,IMiUZ	1,1	5,7	.	.	4,5	.	.	1,6	5,0	.	5,8	.	.	0,6	1,7	.	.	.	.	.	.	4,9	0,8	5,6	3,5	0,8	2,5	8,4	52,5
14	Suwałki	1,9	0,3	1,7	2,9	5,8	0,3	4,6	.	5,4	0,2	3,7	.	.	.	5,5	.	0,9	1,3	0,1	.	.	6,3	6,9	2,0	2,6	5,7	.	0,9	59,0
15	Mikołajki	1,4	2,9	0,2	1,4	3,3	.	1,5	0,0	7,1	.	5,0	.	.	.	5,3	.	0,0	0,3	.	.	4,0	8,2	5,0	0,3	4,5	2,5	.	7,3	60,2
16	Biebrza	1,1	2,3	.	2,9	3,1	2,0	4,0	.	5,6	.	2,0	.	.	.	6,3	.	.	2,5	0,3	4,8	.	8,6	6,0	0,7	5,9	4,0	.	3,5	65,6
17	Białystok	.	0,6	.	0,9	3,9	3,0	3,7	.	3,4	.	2,3	.	.	1,0	4,4	.	0,4	4,1	.	2,2	.	8,1	2,9	3,2	4,7	5,2	.	3,0	57,0
18	Gorzów Wlkp.	2,2	1,9	.	.	1,6	.	.	3,4	7,5	.	.	.	.	0,9	1,0	1,5	3,2	.	.	.	.	2,0	.	8,2	6,9	.	1,6	4,8	46,7
19	Przebędowo	0,5	5,7	1,0	5,6	.	.	.	2,4	6,0	.	7,0	.	1,9	.	3,0	0,5	.	.	.	.	.	1,2	2,1	9,0	6,6	.	3,9	8,2	64,6
20	Przybroda	0,7	7,1	0,4	.	4,6	0,0	.	3,4	6,4	0,0	5,2	.	.	2,5	3,2	.	.	.	0,2	0,3	.	3,3	1,3	7,2	4,8	.	5,1	7,7	63,4
21	Poznań-Ławica	1,2	6,7	0,8	0,1	4,0	.	.	2,6	5,3	.	5,8	.	.	3,0	4,1	1,0	.	.	.	0,1	2,3	1,7	0,9	7,1	4,0	.	4,3	7,9	62,9
22	Plewiska	2,3	6,5	1,0	0,5	4,2	.	.	1,2	5,5	.	7,7	.	.	2,3	4,0	0,7	.	.	.	.	1,0	2,2	0,9	7,0	4,0	0,0	4,5	7,7	63,2
23	Kórnik	1,3	6,2	1,7	0,5	5,4	.	.	1,7	4,6	.	7,7	.	.	2,2	3,4	2,3	.	.	.	0,2	2,0	2,3	1,3	7,9	2,8	0,6	3,3	8,5	65,9
24	Oborniki Śl.	.	.	.	1,0	5,6	1,0	.	.	.	.	5,9	.	.	.	1,6	2,0	.	.	.	.	3,6	2,5	.	:	6,8	.	.	4,1	34,1
25	Łaskowice Oławskie	1,0	0,8	.	0,2	5,7	.	4,9	.	0,8	.	7,0	.	0,5	0,3	2,8	1,4	.	.	.	1,2	.	0,6	0,6	2,9	2,7	2,7	1,3	8,8	46,2
26	Ciechocinek	0,4	3,6	.	6,8	.	.	.	2,6	6,5	.	6,0	.	.	0,1	4,6	2,3	.	.	.	0,4	.	4,1	0,4	3,7	0,7	1,1	0,5	9,1	52,9
27	Więcławice	1,3	5,9	.	.	6,8	.	.	3,8	5,2	.	4,5	.	.	1,5	3,4	4,3	.	.	.	.	.	3,9	3,4	6,5	2,1	.	2,3	8,0	63,9
28	Legionowo	.	0,9	.	0,7	6,1	3,0	6,2	0,1	3,7	.	6,7	.	.	1,4	4,8	1,8	.	.	2,2	2,9	.	6,4	1,0	3,8	1,6	5,1	0,1	7,8	66,3
29	Warszawa-Bielany	0,0	0,7	.	.	5,7	4,6	7,3	0,0	3,0	.	6,6	.	.	0,6	5,2	.	.	.	2,5	1,8	.	5,6	1,3	4,6	1,9	5,7	0,6	7,2	64,9
30	Warszawa,Min.Kom.	0,1	0,3	.	.	4,7	0,8	4,6	.	.	.	5,4	.	.	0,4	4,0	.	.	.	2,1	2,3	.	5,2	2,4	5,2	0,6	4,9	0,1	6,4	49,5
31	Międzylesie	0,1	0,6	.	.	5,6	.	5,4	.	2,3	0,1	5,2	.	.	0,9	4,3	1,0	.	.	2,9	1,4	2,9	5,5	1,9	6,0	2,8	4,7	0,5	6,8	60,9
32	Brwinów	.	0,5	.	0,5	6,3	3,1	7,6	1,7	2,7	.	5,7	.	.	0,4	4,1	0,1	.	.	2,3	1,7	0,3	5,2	2,0	5,9	0,7	5,1	0,4	6,3	62,4
33	Świder	0,2	0,1	.	.	3,9	6,2	6,5	.	2,5	.	6,1	.	.	0,8	6,0	0,1	.	.	0,9	3,7	0,4	5,1	2,1	6,9	3,9	6,5	0,6	6,7	69,2
34	Topola-Błonie	.	2,2	.	.	6,7	.	4,7	4,8	2,5	.	5,3	.	.	0,4	4,4	0,2	.	0,0	.	0,6	.	3,6	0,7	2,3	0,4	0,1	.	7,7	46,6
35	Mlechów	.	0,3	.	.	4,9	5,3	7,1	0,4	2,7	.	7,8	.	.	0,7	5,6	0,1	.	.	1,2	2,5	1,1	5,3	0,8	7,3	0,2	5,8	0,5	6,8	66,4
36	Skierniewice	.	.	.	.	4,6	0,4	7,5	4,2	3,1	.	7,3	.	.	1,2	6,9	.	.	.	2,6	0,1	.	4,4	1,3	5,0	.	4,1	0,2	7,0	59.9
37	Belsk	0,1	0,8	0,0	.	4,8	5,6	7,1	0,1	3,1	.	7,5	.	.	1,1	6,4	0,4	.	.	.	0,6	.	4,9	1,9	7,4	0,4	5,4	0,2	6,7	64,5
38	Łódź-Lublinek	0,1	1,3	.	.	5,7	0,6	6,5	5,5	1,7	.	6,3	.	.	1,0	3,8	0,3	.	.	0,7	0,5	.	3,9	0,7	6,0	0,5	1,8	0,8	7,8	55,5
39	Kalisz	0,8	3,8	.	.	6,9	.	5,0	0,7	2,7	.	6,6	.	.	2,8	6,1	.	.	.	.	.	.	2,4	1,4	4,5	2,4	1,2	3,1	8,9	59,3
40	Wieluń	1,1	0,2	.	.	6,8	.	7,4	0,1	.	.	4,3	.	.	1,6	3,3	1,4	.	.	.	1,2	.	1,6	0,8	6,6	1,6	1,1	1,5	9,1	49,7
41	Szepietowo	1,2	.	0,1	.	4,0	4,9	3,3	.	3,4	.	6,0	.	.	.	5,1	.	0,2	0,3	3,2	2,7	.	7,8	4,4	6,1	4,9	4,4	0,2	5,6	67,8
42	Białowieża	0,6	0,3	0,1	.	5,4	6,2	6,9	.	0,9	.	0,4	.	.	0,4	0,6	.	0,8	.	.	1,1	.	5,5	0,7	5,8	4,6	4,8	.	1,2	46,3
43	Terespol	.	1,2	1,1	.	3,7	6,3	7,2	.	3,5	.	3,9	.	2,3	1,7	1,6	.	.	.	.	0,1	0,3	4,7	3,2	4,3	4,4	6,9	.	3,8	60,2
44	Sobieszyn	0,3	1,2	0,5	.	0,1	5,1	4,9	.	3,1	.	6,4	.	0,5	0,2	3,2	.	.	.	.	5,2	.	4,5	3,2	6,5	1,0	8,3	0,8	6,7	61,7
45	Puławy	0,8	0,3	1,0	.	0,5	6,3	6,8	.	1,7	.	4,0	.	0,5	0,3	1,9	0,1	.	.	.	4,2	.	4,0	1,2	6,3	0,4	6,9	.	5,5	52,7
46	Chełm Lubelski	0,1	3,4	3,4	.	0,6	5,3	6,8	.	1,0	.	6,5	4,9	3,5	4,1	1,6	.	.	.	.	5,3	0,1	2,6	4,4	6,8	2,4	7,0	.	2,1	71,9
47	Szczawno-Zdrój	1,5	0,7	.	0,4	2,7	.	.	.	0,4	0,1	7,8	0,0	1,5	0,8	4,4	3,0	.	.	.	.	2,4	.	.	2,1	0,6	2,7	1,0	7,8	39,9
48	Śnieżka	.	.	0,2	4,2	0,9	.	0,2	.	.	.	8,0	.	.	.	3,4	.	.	.	1,0	3,1	9,2	0,1	.	5,1	.	5,0	1,8	3,5	45,7
49	Opole	1,3	0,6	.	.	6,0	.	5,7	.	0,3	.	5,1	.	0,0	0,2	1,7	4,0	.	.	.	0,3	.	1,1	0,3	2,2	1,1	3,5	.	7,2	40,6
50	Kudowa-Zdrój	0,0	0,6	.	0,9	4,2	.	2,4	1,3	1,7	.	5,2	.	.	1,2	3,1	3,3	0,2	0,0	1,8	1,5	5,9	.	.	4,5	.	4,4	3,0	5,0	50,2
51	Polanica-Zdrój	2,0	1,9	1,0	0,7	1,0	.	3,2	0,1	.	.	7,5	.	.	2,6	3,7	4,4	.	.	.	.	4,2	.	3,7	0,3	.	5,3	2,6	6,5	50,7
52	Skroniów	1,9	1,3	0,0	.	4,5	6,8	5,8	.	1,6	0,6	8,3	5,7	0,1	0,3	5,6	0,2	.	.	.	3,1	.	3,1	.	8,5	0,4	5,8	1,8	8,8	74,4
53	Świerklaniec	0,0	1,9	.	.	5,8	1,3	3,6	0,3	2,6	.	7,3	0,3	.	0,6	3,9	.	.	.	.	4,2	3,9	1,3	.	4,3	.	5,6	1,7	7,2	55,4
54	Kraków,Obs.Astr.UJ	1,0	2,3	.	.	3,8	2,2	3,1	2,3	0,8	0,4	5,7	6,8	0,7	3,2	2,7	.	.	.	.	0,6	.	.	.	3,0	.	8,1	1,2	6,8	54,9
55	Cieszyn	.	0,0	.	.	1,8	0,0	6,3	0,1	0,4	1,6	2,1	4,7	.	1,7	3,2	0,1	.	.	.	5,8	0,1	.	.	5,8	.	5,5	0,4	9,0	48,8
56	Istebna-Kubalonka	1,3	.	0,4	.	7,5	4,0	8,3	.	.	1,7	2,4	7,1	.	.	2,4	1,5	.	.	0,1	5,7	3,3	.	.	8,0	.	2,2	0,2	7,1	61,4
57	Rabka	2,3	0,1	.	.	6,4	5,6	8,0	0,9	.	4,8	3,3	7,2	0,2	3,1	0,7	.	.	.	.	5,0	.	.	.	8,3	.	4,6	0,9	6,9	67,3
58	Jabłonka	2,3	0,9	0,8	0,7	4,3	9,1	6,3	0,1	.	2,9	3,9	6,5	.	0,2	0,7	2,9	.	.	1,5	4,1	4,4	.	.	7,8	.	5,0	1,4	8,3	69,7
59	Krynica	1,9	0,6	0,9	0,2	4,9	6,0	7,1	0,1	.	3,7	2,9	7,3	2,6	2,7	0,1	.	.	.	.	3,0	.	.	.	6,1	0,1	5,9	2,9	6,9	66,8
60	Krynica-Góra Park	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
61	Muszyna	1,0	0,4	0,3	0,3	7,2	9,3	5,0	0,1	0,2	4,3	2,9	7,1	2,6	1,9	.	.	.	.	.	3,9	.	.	.	7,2	0,1	6,8	8,2	9,4	65,0
62	Zakopane	0,1	.	0,3	.	8,1	5,1	8,4	0,0	0,1	7,0	0,9	7,5	1,9	2,8	.	2,8	.	.	1,0	7,3	7,3	.	.	8,5	1,5	7,2	4,4	8,4	90,5
63	Gubałówka	.	.	0,3	.	7,3	4,6	7,7	.	0,3	8,9	1,1	7,8	2,2	2,7	0,1	2,3	.	.	1,3	6,1	6,0	.	.	8,9	1,4	6,3	4,4	9,3	85,8
64	Hala Gąsienicowa	0,3	.	0,1	.	6,2	4,7	8,3	.	.	3,4	0,3	8,9	2,3	0,0	0,6	1,4	.	.	0,0	6,6	7,1	.	.	7,2	0,3	9,0	2,7	9,2	71,1
65	Kasprowy Wierch	2,1	.	.	.	8,6	4,1	8,7	.	.	9,1	0,4	8,9	.	0,1	0,1	1,3	.	.	0,2	9,2	9,3	.	.	9,8	1,1	6,7	1,8	8,8	88,1
66	[illegible]	.	3,8	3,8	0,2	2,0	4,4	9,0	.	2,1	6,5	8,1	4,1	1,6	3,7	0,4	.	.	.	.	6,9	.	1,0	2,7	8,9	2,2	7,0	.	6,5	75,1
67	[illegible]	2,0	1,3	1,7	.	2,4	5,4	4,3	.	.	.	7,4	[illegible]	.	.	2,7	.	.	.	.	9,2	.	2,9	0,7	7,9	.	5,1	0,2	9,2	63,1
68	Iwonicz-Zdrój	.	.	.	.	3,1	.	4,0	.	.	4,6	1,3	7,2	0,6	3,8	.	.	.	.	.	0,1	.	.	.	4,2	.	6,6	0,8	4,8	40,9
69	Lesko	.	0,2	1,6	.	2,9	0,1	7,2	.	1,4	5,6	0,7	6,8	2,1	4,8	.	.	.	.	.	3,2	.	.	.	6,8	.	4,7	.	4,1	52,0

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	.	.	.	0,1	.	3,7	9,3	9,7	0,3	1,0	1,6	6,9	9,1	8,3	2,9	2,1	5,1	5,5	0,2	9,3	0,4	10,5	9,3	0,8	..	1,6	5,3		3,1	5,1	8,9	120,1
2	Kołobrzeg	.	.	.	.	2,0	6,2	7,4	8,6	0,7	1,7	4,4	8,9	9,0	8,3	1,1	0,6	3,1	5,7	.	9,2	.	10,0	8,7	0,6	3,1	1,3	6,1		4,1	4,9	11,3	127,0
3	Świnoujście	.	.	.	.	0,7	1,2	5,9	3,6	4,9	6,1	8,7	8,4	8,3	7,2	0,9	.	2,7	5,8	1,9	7,8	0,6	9,9	8,9	1,6	1,8	6,2	0,7		3,5	3,8	10,7	121,8
4	Resko	.	.	.	.	2,2	3,6	6,9	9,0	.	2,5	7,0	7,7	8,1	8,2	0,1	.	3,2	6,4	.	5,3	.	9,3	10,5	5,4	1,6	3,0	7,1	.	7,0	5,2	10,9	130,2
5	Szczecinek	.	.	.	.	1,4	4,8	7,7	7,7	.	5,6	3,5	8,3	8,2	7,8	3,1	1,6	3,3	5,5	.	6,6	.	10,4	10,0	3,2	1,3	0,3	7,2		5,2	2,5	10,7	125,9
6	Chojnice	.	.	.	.	0,4	4,8	9,1	8,2	0,1	5,5	1,6	6,8	8,8	9,1	4,3	2,0	3,6	2,6	0,2	6,3	.	10,0	9,9	1,4	1,5		7,8		2,4	2,1	11,6	120,1
7	Hel	.	.	.	.	0,1	5,6	7,6	6,5	0,2	7,0	1,9	5,2	7,6	7,8	4,1	4,1	.	.	0,7	7,6	2,2	9,1	8,7	0,0	.	7,5	9,4	.	2,2	4,9	8,8	118,8
8	Gdynia	.	.	.	.	.	2,5	6,3	9,4	0,9	8,1	7,8	4,7	9,2	8,9	3,8	4,8	8,0	4,7	0,3	8,3	2,1	9,4	9,2	0,4	.	3,8	8,4		5,4	4,0	8,5	138,9
9	Świbno	.	0,0	.	.	.	6,8	5,6	7,2	2,8	6,6	5,2	5,5	7,8	5,8	3,5	4,4	0,4	.	0,5	6,4	.	8,4	8,1	0,2	.	4,5	8,9	.	2,4	5,1	7,3	113,4
10	Stare Pole	.	.	.	.	0,4	6,9	5,3	6,1	2,6	7,7	5,5	8,2	9,3	8,7	4,7	4,2	2,9	0,7	1,9	7,2	1,2	9,6	10,8	0,2	4,1		10,0	.	1,7	4,5	9,3	135,7
11	Kadostomo	.	.	.	.	.	6,9	4,4	7,1	0,6	8,9	7,3	7,2	8,8	4,7	5,1	4,3	2,3	.	0,7	7,5	.	10,7	10,4	0,8	2,8	.	9,2		2,7	4,4	9,7	126,5
12	Prabuty	.	.	.	.	5,1	1,0	6,4	5,8	.	7,1	4,4	8,8	7,8	9,3	6,5	4,7	.	.	3,4	8,4	.	8,4	9,1	.	.	2,7	8,9	.	2,6	.	11,2	121,6
13	Bydgoszcz, IMiUZ	.	.	.	.	1,3	.	7,7	5,2	.	5,2	1,3	7,2	4,7	5,7	2,0	1,9	3,6	2,7	0,7	7,3	.	9,6	9,2	0,7	1,5	0,1	5,3	.	2,4	3,7	10,3	99,3
14	Suwałki	0,7	.	.	0,3	0,8	6,0	8,3	8,7	8,1	3,9	.	8,0	8,5	9,5	9,5	0,4	.	0,2	0,7	8,3	2,2	7,4	10,3	.		8,4	11,4	5,6	.	4,0	8,0	139,2
15	Mikołajki	0,8	.	.	0,2	0,0	6,1	6,9	6,4	6,9	8,1	0,2	9,3	8,6	6,6	6,9	1,5	6,0	.	0,8	9,3	4,4	8,6	10,9		0,1	8,3	10,8	2,4	.	4,6	10,8	145,5
16	Biebrza	1,7	.	.	1,8	1,1	6,4	7,3	7,9	7,5	7,0	.	7,4	9,0	7,9	7,6	0,3	.	.	0,1	8,2	4,4	7,6	9,5	.	0,3	9,1	10,8	3,9		3,3	8,2	135,8
17	Białystok	3,3	.	.	1,0	1,6	5,1	6,5	7,3	7,0	6,1	0,2	7,3	6,7	7,8	8,8	2,3	.	.	.	5,2	2,0	6,3	9,0		0,1	7,3	10,1	2,5	.	4,7	6,5	124,7
18	Gorzów Wlkp.	.	.	.	.	0,8	.	6,9	6,1	5,9	5,1	7,5	8,1	7,3	7,4	0,8	.	3,6	4,1	0,1	3,2	.	9,6	9,0	0,3	2,5	0,1	7,3	.	5,6	5,1	10,1	116,5
19	Przebędowo	1,7	.	.	.	2,2	.	7,5	6,2	1,1	5,2	7,9	7,6	8,6	7,8	2,4	0,6	6,6	5,8	2,4	6,6	.	9,5	10,4	1,9	1,5	0,3	6,5	.	8,5	6,6	10,3	135,5
20	Przybroda	2,7	.	.	.	0,5	.	8,8	5,5	2,1	4,5	6,8	7,2	7,3	6,7	1,4	0,1	6,6	4,7	2,0	6,1	.	8,8	9,9	2,2	1,8	0,6	7,5	.	9,5	6,0	10,8	130,1
21	Poznań-Ławica	1,6	.	.	.	0,6	.	8,2	5,9	1,9	4,4	6,8	7,7	7,5	7,2	..	0,5	5,8	4,6	1,8	4,7	.	9,1	8,3	2,0	1,2	0,8	6,2	.	7,6	5,5	10,0	119,9
22	Plewiska	2,0	.	.	.	1,1	0,2	8,7	6,3	.	3,1	10,1	6,6	8,2	8,5	2,1	0,1	7,3	4,9	2,4	6,0		9,9	9,7	1,0	1,1	0,4	6,2		8,2	5,4	10,7	130,2
23	Kornik	1,2	.	.	.	0,1	0,8	7,0	7,2	1,7	6,8	9,2	8,2	8,2	8,3	2,2	0,4	6,7	6,4	3,7	7,6		10,4	9,5	0,7	1,8	0,1	6,9		8,0	5,8	10,0	138,9
24	Oborniki Śl.	2,9	.	.	.	3,0	.	3,8	4,7	1,8	7,5	9,3	8,1	7,5	8,5	1,7	.	6,9	6,1	7,0	8,3		8,5	9,1	3,8		.	3,0		0,6	10,5	9,9	132,5
25	Leśkowice Dąbrowskie	2,5	.	.	.	3,9	.	0,8	3,4	0,5	8,0	7,5	7,8	8,9	9,3	1,1	0,6	6,0	6,3	6,9	7,9	0,1	8,7	6,4	5,4	1,0	1,2	0,9	0,3	2,1	7,1	8,3	122,9
26	Ciechocinek	0,0	.	.	.	.	.	7,2	6,0	0,0	6,4	1,6	4,0	5,9	8,4	2,8	2,0	.	4,5	2,4	7,6		9,7	8,8	1,2	0,2	0,0	5,7	.	1,2	5,3	8,8	99,7
27	Więcławice	.	.	.	.	0,1	.	8,2	3,7	.	4,9	2,8	5,1	5,1	6,6	2,8	2,3	0,5	3,7	2,1	7,0	.	9,2	8,1	0,9	1,4	0,2	5,0		2,2	5,0	.	86,9
28	Legionowo	3,6	.	.	.	0,1	.	7,6	8,8	6,6	7,5	.	5,8	7,3	5,8	5,8	2,0	.	3,8	3,1	8,4	.	8,6	9,7	0,1	0,1		4,7	1,5		5,3	7,6	113,8
29	Warszawa-Bielany	4,3	.	.	.	.	.	6,0	9,6	8,1	7,5	.	9,2	8,7	8,7	6,9	3,2	.	4,5	5,1	9,3	.	9,1	10,5	0,7	0,2	.	5,0	1,6	.	6,6	7,0	131,8
30	Warszawa, Min.Kom.	3,7	.	.	.	.	.	5,2	8,5	7,5	7,3	.	8,5	8,2	7,6	6,2	2,5	.	2,9	3,0	8,9	.	8,7	9,9	0,3	0,5	.	4,2	1,4	.	6,1	6,9	118,0
31	Międzylesie	3,4	.	.	.	.	0,2	7,3	8,9	8,0	7,4	.	8,5	6,6	8,2	5,6	1,4	.	3,1	4,0	6,8	1,1	8,5	8,6	.	0,3	0,1	3,2	5,8	0,5	6,1	7,1	120,7
32	Irwinów	4,0	.	.	.	.	.	5,0	9,6	7,8	8,8	.	8,3	9,1	8,8	5,8	2,3		5,2	4,4	9,3	0,5	7,7	10,5	0,6	.	0,2	3,9	0,9		6,2	7,4	126,3
33	Świder	4,7	.	.	.	.	.	7,3	8,6	8,5	6,9	.	8,6	8,8	8,5	5,8	2,0	.	2,6	4,9	8,7	.	8,2	9,7	0,2	0,1	0,3	2,6	1,6	.	6,2	5,7	120,5
34	Tepole-Błonie	2,4	.	.	.	.	0,5	6,4	6,3	3,5	6,7	5,6	7,7	8,5	8,5	2,4	0,3	.	8,4	5,1	6,9	.	8,4	8,6	1,4		0,5	5,6	2,2	1,7	7,8	5,1	120,5
35	Młochow	3,2	.	.	.	.	.	5,7	10,1	8,1	7,2	.	8,1	9,0	9,5	5,8	1,6	.	4,4	5,9	8,2	.	9,1	10,3	0,0	0,0	0,2	2,8	1,0	0,0	6,7	10,0	126,9
36	Skierniewice	4,1	.	.	.	.	5,3	0,6	9,0	6,5	8,7	2,5	6,0	9,1	8,5	4,8	1,5	1,5	7,0	8,0	6,3	.	7,9	9,4	2,0	0,1	1,1	4,6	3,8	.	6,4	8,5	133,2
37	Bełsk	1,7	.	0,5	.	.	1,2	4,7	8,6	7,0	6,3	0,4	8,3	8,8	8,8	4,8	2,1	.	4,7	6,8	6,6	.	8,2	8,8	0,0	0,0	0,8	2,4	2,7	.	6,6	7,5	118,3
38	Łódź-Lublinek	1,6	.	.	.	.	1,6	2,9	6,7	3,9	5,7	7,9	8,4	8,3	8,5	3,9	1,0	.	8,8	5,8	5,1	.	8,4	8,8	4,1	0,3	0,6	5,1	2,9	0,6	6,6	5,7	123,2
39	Kalisz	0,9	.	.	.	0,5	0,0	3,1	5,5	2,4	5,7	8,3	8,9	8,7	8,2	2,1	0,7	5,0	8,1	6,0	8,4	0,1	9,2	8,1	4,7	1,8	0,7	5,0	0,6	2,9	7,1	9,2	131,9
40	Wieluń	1,7	.	0,0	.	2,6	.	.	7,1	5,8	4,2	9,1	9,7	9,0	9,9	4,4	0,4	4,1	7,5	8,2	6,3	.	9,0	8,7	4,7	1,3	0,3	4,9	5,0	1,5	7,6	6,9	139,9
41	Szepietowo	3,4	.	.	2,5	.	1,4	3,8	6,5	7,9	7,8	3,9	8,3	9,2	7,1	7,1	3,0	.	.	.	6,7	1,1	7,7	9,0	.	0,1	5,6	8,1	1,9	.	5,1	7,9	125,1
42	Białowieża	3,2	.	.	1,1	2,9	.	7,2	6,4	7,0	6,4	2,7	7,6	8,5	9,5	9,1	0,3	.	.	.	1,3	0,1	4,3	8,9	.	.	2,6	5,6	2,7	.	4,4	4,0	105,8
43	Terespol	1,2	.	0,4	3,3	4,8	0,4	6,7	9,2	7,4	6,0	5,6	8,4	9,1	9,2	9,0	2,2	0,4	0,0	1,6	3,1	.	5,5	10,7	.	.	2,5	4,7	4,6	.	5,8	7,4	129,2
44	Sobieszyn	1,9	.	0,1	1,6	3,2	0,6	3,2	9,0	8,3	6,7	.	6,5	8,2	7,4	7,2	3,5	0,8	4,3	7,7	4,7	.	5,4	9,5	.	.	1,3	.	3,9	.	7,4	5,7	118,1
45	Puławy	0,1	.	.	1,1	3,2	2,4	.	8,5	7,7	5,8	.	7,2	8,9	8,9	6,7	4,8	0,2	3,0	7,4	3,0	.	5,0	9,7	0,1	0,2	0,9	.	1,6	.	7,2	3,7	109,3
46	Chełm	1,1	.	0,0	6,7	2,1	.	.	9,2	5,4	3,5	2,6	6,4	9,0	9,4	9,3	5,9	.	.	5,2	.	0,6	3,3	9,6	.	0,1	2,1	.	3,8	.	8,6	4,0	107,9
47	Szczawno-Zdrój	1,8	.	.	.	3,6	.	.	6,0	3,0	7,9	8,2	8,7	8,3	8,4	2,1	.	7,2	5,1	5,0	6,4	.	5,6	5,4	5,2	2,3	.	.	.	1,3	6,8	9,6	117,9
48	Śnieżka	2,5	0,4	.	0,0	4,5	.	1,8	9,6	0,9	8,8	10,0	10,1	10,2	10,2	2,8	.	1,1	5,0	2,6	5,9	.	6,8	6,1	0,1	0,8	0,0	1,4	.	0,2	5,7	9,1	116,6
49	Opole	.	.	0,5	.	5,2	.	0,1	.	2,7	2,1	6,2	8,2	8,2	8,3	5,5	0,7	6,0	7,8	8,1	6,2	0,3	3,0	7,7	7,1	3,9	1,4	0,9	5,9	1,1	7,1	7,4	121,6
50	Kudowa-Zdrój	.	.	0,2	0,7	5,4	.	.	4,7	1,9	8,5	6,3	6,3	6,3	3,6	3,7	0,2	3,4	6,5	5,0	6,0	0,1	7,6	4,6	0,2	0,4	0,1	0,6	.	1,4	1,7	10,3	95,9
51	Polanica-Zdrój	0,2	.	.	.	5,8	.	.	5,4	1,3	6,6	6,6	6,8	7,2	7,2	4,7	0,2	6,9	6,0	5,3	4,9	.	7,2	5,2	0,5	6,1	0,4	..	0,8	1,0	7,4	9,6	113,2
52	Skroniów	0,5	.	2,3	0,1	3,0	.	.	3,9	6,0	6,4	9,4	6,9	6,2	8,6	2,0	0,5	.	6,6	8,3	1,4	1,3	5,7	9,2	0,4	2,6	1,4	.	6,2	.	8,3	3,1	110,3
53	Świerklaniec	2,0	.	1,0	.	6,2	.	0,1	0,7	5,7	2,6	3,4	5,6	6,0	7,3	2,6	.	1,3	7,0	7,1	0,8	0,1	5,9	8,5	0,6	1,9	1,0	.	5,3	0,3	7,6	6,4	97,0
54	Kraków, Obs.Astr.UJ	.	.	4,9	0,9	2,0	.	.	.	3,5	5,0	7,9	7,1	6,2	8,3	0,7	2,7	.	6,6	9,3	0,3	1,8	4,6	8,9	.	1,2	4,3	.	5,2	.	6,0	3,2	103,3
55	Cieszyn	1,6	.	1,7	0,1	1,9	.	.	.	6,7	0,4	8,5	8,9	9,4	8,9	4,3	0,1	3,4	9,9	9,1	.	.	2,6	7,9	.	3,2	2,9	.	5,7	.	2,8	7,0	107,3
56	Istebna-Kubalonka	.	.	.	0,4	2,6	.	.	.	6,7	2,1	9,7	9,8	9,8	9,3	5,0	4,4	0,4	.	6,6	.	.	2,9	9,7	.	4,0	2,5	.	5,8	.	2,3	3,8	97,8
57	Hanka	0,5	1,5	6,7	4,2	5,0	.	.	.	4,9	1,9	7,1	9,5	8,8	9,3	3,6	4,0	.	9,6	7,1	.	2,6	0,8	7,6	.	0,9	4,6	.	6,3	.	5,4	4,4	115,5
58	Jabłonka	1,4	0,9	5,1	2,2	5,4	.	.	.	6,9	5,2	6,0	8,4	7,2	8,3	4,7	4,2	.	5,5	7,3	.	1,8	.	9,2	..	4,0	3,9	.	7,4	.	5,7	7,4	118,0
59	Krynica	.	0,2	5,4	5,8	5,3	.	.	.	1,6	1,5	9,2	5,4	6,4	3,8	4,7	6,4	.	6,1	7,9	.	2,0	0,3	8,1	0,5	4,7	2,1	.	5,3	.	6,1	4,6	103,4
60	Krynica-Góra Park.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
61	Muszyna	1,4	.	6,1	5,1	4,6	.	.	0,5	.	0,7	7,8	4,2	5,9	7,3	6,0	5,9	.	5,3	6,3	.	3,0	0,1	9,5	0,2	5,9	3,3	.	4,3	.	0,4	4,8	105,8
62	Zakopane	0,9	2,8	5,1	4,6	7,0	.	.	.	3,2	2,3	9,6	10,2	10,3	10,1	4,1	(5,4)	.	10,5	7,3	.	3,3	.	10,4	.	2,9	5,4	.	5,0	.	6,3	4,9	(131,8)
63	Gubałówka	0,8	3,1	5,7	4,8	6,9	.	.	.	2,2	1,8	9,2	9,3	9,2	8,8	3,0	3,9	.	9,2	7,4	.	3,2	.	10,0	.	3,8	5,0	.	4,5	.	7,1	4,9	127,0
64	Hala Gąsienicowa	.	.	.	3,6	6,0	.	.	.	1,3	4,0	8,6	8,6	8,9	8,3	4,0	3,9	.	9,8	7,0	.	2,0	.	9,0	.	2,7	3,7	.	5,1	.	3,1	3,7	104,5
65	Kasprowy Wierch	.	.	.	2,7	3,3	.	0,2	0,3	7,3	7,9	11,1	11,5	11,4	1,4	4,3	0,4	.	9,8	7,3	.	1,2	0,4	10,0	.	3,1	2,7	.	10,6	.	2,1	4,2	116,8
66	Warkowicze	2,3	0,1	5,9	7,2	.	.	.	7,4	1,6	3,5	3,3	4,5	7,6	8,3	8,5	7,1	.	1,6	7,0	0,5	2,1	2,6	9,5	3,2	3,1	.	.	9,2	.	7,0	4,4	118,8
67	Zdanów	.	.	3,8	5,3	2,9	.	.	1,2	6,6	8,6	7,1	7,6	7,1	8,1	6,6	1,4	.	4,8	7,7	0,2	1,3	5,8	9,1	.	3,9	1,7	.	4,7	.	(7,7)	5,8	(118,2)
68	Tuchola-Zdrój	0,4	0,2	6,6	4,6	3,7	.	.	.	0,2	1,3	5,3	8,0	9,1	8,8	3,0	7,1	.	8,3	9,3	.	4,2	0,2	9,6	0,2	1,9	2,0	.	4,3	0,1	6,7	4,2	109,3
69	Leszno	0,1	.	5,2	1,2	1,7	.	.	.	.	9,5	6,8	8,6	8,2	6,8	3,1	6,3	.	7,8	9,0	.	4,7	.	9,6	.	0,7	8,1	.	4,6	1,2	5,1	4,7	97,6

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	11,3	10,6	.	2,0	6,8	8,0	.	.	.	5,7	7,3	1,4	3,0	2,0	7,5	7,8	3,6	0,4	0,6	2,4	6,5	8,9	1,9	.	1,3	2,5	5,1	5,0	3,5	10,1	125,2
2	Kołobrzeg	10,9	5,6	1,9	.	9,2	8,9	.	0,2	.	3,5	5,5	1,9	5,4	3,4	7,3	4,0	2,2	0,4	3,7	0,6	7,3	5,5	5,0	.	.	3,2	3,7	7,3	0,0	11,4	118,0
3	Świnoujście	10,5	4,4	4,7	5,3	8,2	6,6	.	.	.	3,0	1,5	2,4	2,5	5,2	5,8	.	1,6	0,4	8,5	.	6,9	0,5	3,2	.	0,3	1,4	0,1	3,7	0,0	9,0	95,7
4	Resko	10,4	4,7	3,1	7,8	9,9	8,5	.	4,1	.	1,9	4,5	0,6	4,6	2,6	7,6	2,1	2,5	0,5	5,1	0,5	4,2	0,6	3,0	.	0,4	2,6	4,9	5,6	0,7	10,7	113,7
5	Szczecinek	11,2	7,3	0,8	3,6	10,7	8,9	.	1,0	2,8	3,0	3,9	-	1,8	2,3	7,5	7,0	2,2	0,4	2,9	0,5	4,5	2,8	.	.	2,7	4,0	5,6	2,6	0,3	9,9	110,2
6	Chojnice	5,3	6,0	.	2,6	7,1	9,8	0,1	.	4,7	2,9	5,5	.	.	0,4	7,8	8,3	0,3	1,2	.	1,2	4,8	2,8	.	.	2,1	5,5	4,1	2,6	1,9	6,9	93,7
7	Hel	8,8	10,3	.	2,4	0,2	5,9	1,1	.	6,4	1,5	9,5	.	.	.	2,1	8,9	0,6	0,4	0,5	2,1	4,6	5,6	0,2	.	0,1	2,9	5,2	5,0	1,4	9,6	94,5
8	Gdynia	8,9	10,4	.	3,2	5,1	5,8	0,3	.	2,3	2,8	10,7	0,3	.	.	4,1	10,0	0,6	0,1	0,6	0,9	1,0	.	.	2,5	0,2	1,9	.	7,0	.	12,3	91,0
9	Świbno	9,3	10,2	0,2	2,6	4,2	6,3	1,3	.	6,7	0,7	9,3	.	.	.	0,2	9,2	0,8	0,4	.	0,5	5,8	3,9	.	.	.	3,1	4,8	3,6	2,4	8,7	94,2
10	Stare Pole	11,0	11,1	0,4	2,2	6,3	8,3	0,1	0,4	8,0	1,0	9,6	.	.	0,1	.	9,3	.	0,6	.	3,0	3,2	3,9	.	.	1,5	2,6	4,0	1,9	1,7	9,0	99,2
11	Radostowo	8,4	11,1	.	4,0	6,4	7,8	1,3	.	4,0	1,5	8,4	.	.	.	1,8	10,2	0,2	0,2	.	1,3	2,2	2,7	.	.	2,1	2,4	4,8	1,3	2,5	8,6	93,2
12	Prabuty	10,2	10,7	0,4	5,0	6,9	10,3	0,5	.	6,9	.	8,8	.	.	.	.	10,3	-	1,3	.	1,8	3,0	4,0	.	.	1,0	2,8	3,9	0,5	2,5	10,7	101,5
13	Bydgoszcz, IMiUZ	10,3	7,9	.	4,3	6,1	9,3	0,2	3,1	1,7	0,9	1,6	.	.	0,5	5,3	7,3	0,1	1,9	.	0,7	1,0	1,0	.	.	0,5	4,3	2,5	1,3	2,7	6,1	80,6
14	Suwałki	11,0	11,4	8,0	0,8	.	4,7	3,8	.	10,3	5,9	10,7	11,0	12,1	2,2	0,1	0,3	3,5	1,2	3,2	1,5	0,9	2,7	.	0,2	2,0	4,5	3,4	10,8	2,9	9,7	138,8
15	Mikołajki	10,6	11,0	2,1	.	3,7	8,3	2,4	.	3,8	1,9	10,7	9,2	6,2	2,4	.	1,4	.	0,3	1,6	2,7	0,1	3,7	.	0,2	1,2	0,2	0,9	4,5	2,0	7,8	98,1
16	Biebrza	10,0	11,1	7,1	1,5	.	5,3	3,5	.	3,8	3,3	10,2	10,6	11,8	0,3	.	2,2	.	2,5	3,4	0,6	0,1	2,3	.	.	4,5	1,7	2,0	6,9	3,4	8,6	116,7
17	Białystok	10,7	11,4	8,1	0,1	3,5	4,7	5,6	0,0	3,7	2,1	10,6	10,3	11,7	0,4	.	0,9	4,8	2,8	5,2	.	0,4	.	.	0,1	3,1	5,5	2,2	7,2	0,3	10,0	125,4
18	Gorzów Wlkp.	10,6	6,6	5,9	7,9	10,0	8,9	1,3	7,1	.	1,5	3,7	0,2	2,2	7,7	3,3	.	3,4	1,4	4,2	.	0,1	0,3	0,2	.	0,2	4,6	0,6	2,5	0,1	5,9	100,4
19	Przebędowo	11,7	10,7	2,5	8,4	11,0	10,1	0,3	4,7	1,7	1,5	.	.	2,4	1,7	4,1	6,1	2,2	1,7	0,5	0,3	1,1	0,9	.	.	0,3	6,2	7,8	.	5,2	5,8	108,9
20	Przybroda	11,4	11,0	4,2	8,2	10,7	9,5	1,0	8,1	1,1	1,9	.	.	5,4	4,7	3,1	5,0	3,8	3,0	1,2	.	1,4	1,8	.	.	1,8	6,7	7,8	0,9	3,2	6,5	123,4
21	Poznań-Ławica	10,4	9,7	5,0	7,9	9,9	8,9	1,5	7,1	.	0,4	.	.	2,0	5,4	5,2	3,9	3,5	3,2	1,9	.	1,1	1,1	.	.	1,2	7,6	7,7	0,2	5,0	4,5	114,3
22	Plewiska	11,4	10,7	6,4	8,2	10,7	10,1	0,5	7,1	0,6	0,1	.	.	1,4	5,4	4,1	3,8	2,6	1,9	1,3	.	0,5	0,5	.	.	1,3	6,4	5,2	0,7	2,1	4,4	107,4
23	Kórnik	11,9	10,6	6,8	8,6	11,8	10,4	0,0	7,7	0,2	0,5	.	0,7	0,7	2,1	6,5	3,0	1,9	3,5	0,8	.	0,8	0,1	.	.	1,4	6,0	8,5	0,5	3,0	6,4	114,4
24	Oborniki Śl.	10,2	10,8	9,3	8,2	7,5	11,0	-	10,3	.	.	.	.	.	1,3	.	.	0,2	0,3	.	.	.	.	.	.	.	5,8	7,7	.	13,6	1,2	97,4
25	Laskowice Oławskie	11,1	10,4	10,4	7,6	10,9	10,1	.	9,8	.	.	2,2	.	0,2	1,0	6,3	2,8	3,1	3,8	.	.	.	.	0,0	0,1	1,7	6,1	4,8	0,2	8,2	6,5	117,3
26	Ciechocinek	9,6	10,2	3,9	6,7	6,1	10,5	4,0	3,6	1,5	.	2,8	2,3	.	.	.	8,7	0,2	2,8	.	3,2	.	1,6	.	0,2	0,6	3,6	2,4	1,1	7,9	6,9	108,4
27	Więcławice	9,1	9,3	3,0	6,5	6,7	3,2	3,3	6,4	2,4	.	1,2	.	.	0,3	4,9	7,3	0,8	.	.	1,0	.	1,4	.	.	0,7	6,1	2,3	3,0	7,0	7,0	92,9
28	Legionowo	9,8	10,3	6,1	5,8	3,6	7,0	4,6	4,2	.	1,6	3,7	1,3	0,7	7,7	.	8,0	.	0,0	.	3,5	.	0,2	.	0,1	2,9	0,4	0,1	0,5	9,0	6,6	103,7
29	Warszawa-Bielany	9,6	10,3	7,7	5,6	3,7	8,5	5,1	5,6	0,2	2,1	10,0	0,5	2,3	7,5	0,2	8,4	.	.	.	3,5	.	0,1	.	0,0	2,1	1,8	.	0,6	8,8	7,8	112,0
30	Warszawa, Min. Kom.	9,2	9,7	6,6	4,2	3,4	6,6	4,0	3,7	0,2	1,5	8,3	0,3	1,4	7,0	.	7,1	.	.	.	3,4	.	0,1	.	.	2,8	2,2	0,0	1,0	7,8	6,9	97,4
31	Międzylesie	9,6	9,0	6,6	6,0	7,1	5,4	3,9	4,6	1,5	3,3	8,7	0,9	1,5	7,3	1,3	7,4	.	0,6	0,7	2,6	.	.	.	0,0	2,5	1,7	0,7	1,0	11,0	5,7	118,6
32	Brwinów	10,4	10,4	7,4	3,9	4,3	10,2	2,8	7,1	1,9	0,8	6,8	0,3	1,7	7,1	.	9,8	.	.	.	0,6	0,1	.	.	.	1,9	.	.	1,6	11,5	7,0	107,6
33	Świder	8,5	9,4	8,2	4,7	9,6	4,6	6,4	5,8	3,1	2,1	9,5	0,2	2,1	5,3	0,6	8,2	2,0	.	.	4,4	.	0,5	.	.	3,8	2,9	0,1	2,2	8,8	5,8	118,8
34	Topola-Błonie	10,4	9,5	7,7	6,1	6,8	10,8	0,4	7,0	3,0	0,1	.	.	.	0,5	3,6	7,6	0,2	1,5	.	1,0	.	0,1	.	.	0,8	2,5	1,3	1,2	10,5	5,2	97,8
35	Łochów	7,2	10,3	6,9	5,0	4,3	10,2	3,7	7,0	2,3	0,7	4,2	.	1,9	5,9	.	9,6	0,0	.	.	1,0	.	0,1	.	.	2,4	2,2	0,2	1,2	10,6	3,9	100,8
36	Skierniewice	10,0	10,1	7,9	7,8	5,3	11,2	4,4	8,3	3,7	0,9	.	.	.	8,2	.	9,5	.	.	.	1,8	.	.	.	.	3,2	4,1	0,5	1,7	11,1	7,3	117,8
37	Belsk	8,5	9,0	7,9	7,1	5,2	9,8	5,8	3,9	4,3	0,8	1,7	.	1,7	5,7	0,3	8,6	.	.	0,0	1,3	.	.	.	.	2,5	2,4	0,4	6,0	11,1	6,1	104,1
38	Łódź-Lublinek	10,8	9,5	9,6	6,9	9,7	10,5	1,6	6,0	3,1	0,0	.	.	.	1,0	4,7	7,5	1,2	1,2	.	4,6	0,0	0,1	0,1	0,1	0,3	4,9	3,3	0,2	11,4	5,0	113,3
39	Kalisz	10,7	9,4	9,8	8,6	10,7	10,8	.	9,9	0,6	0,2	1,3	.	.	4,8	8,8	1,5	2,5	3,7	.	1,1	.	.	.	0,0	2,5	4,9	8,4	.	11,3	6,6	128,1
40	Wieluń	11,3	10,3	10,7	7,9	11,1	11,2	1,6	10,7	0,1	.	4,0	.	.	.	7,3	4,7	1,4	1,7	.	0,3	.	.	.	.	2,5	5,0	8,2	0,2	10,1	6,4	126,7
41	Szepietowo	10,1	11,1	9,2	0,3	4,7	6,9	5,5	1,9	1,1	3,3	10,9	10,7	11,4	.	0,1	3,8	2,0	2,4	8,3	3,8	.	.	.	0,2	2,9	4,3	0,9	4,7	..	8,3	128,8
42	Białowieża	9,6	10,5	8,5	.	8,8	9,6	7,5	0,3	1,7	5,0	3,2	11,7	12,0	.	-	0,5	1,5	2,0	5,2	1,1	0,2	.	0,6	.	2,5	7,8	2,6	9,6	.	8,6	130,6
43	Terespol	8,8	9,1	9,8	.	8,7	8,2	7,8	2,7	0,5	8,0	7,9	11,3	11,8	.	0,3	2,7	2,2	1,5	7,4	1,2	.	.	.	3,2	7,5	7,8	1,3	4,2	.	8,6	142,5
44	Sobieszyn	8,7	9,0	7,8	3,9	5,3	7,5	7,8	2,7	2,3	0,9	5,6	1,8	5,8	.	1,6	5,3	2,6	2,7	0,5	1,4	.	.	.	0,5	5,6	2,8	2,0	0,5	11,3	7,4	113,3
45	Puławy	9,0	6,8	7,9	3,5	5,7	7,5	7,1	2,2	0,4	0,1	4,6	0,2	5,3	.	0,4	6,4	1,6	1,7	0,4	0,5	.	.	0,6	0,1	2,2	1,0	1,5	.	10,5	4,5	89,7
46	Chełm	4,3	8,7	8,9	0,6	4,7	5,8	6,7	0,4	.	.	0,2	8,9	9,4	.	.	6,6	5,1	1,3	6,0	0,7	.	.	0,7	1,7	5,5	5,8	3,0	1,4	8,8	4,9	110,1
47	Szczawno-Zdrój	9,0	9,9	9,4	7,2	9,1	9,4	-	5,5	.	.	3,8	.	4,3	2,7	3,4	0,1	4,8	4,4	.	.	.	.	0,3	0,6	0,4	6,5	1,1	0,1	4,5	3,3	99,8
48	Śnieżka	4,9	10,1	8,8	8,3	8,5	9,7	0,8	3,3	.	7,1	7,0	.	1,8	0,5	4,4	.	3,4	0,9	0,7	.	.	.	.	0,1	0,2	2,4	.	.	.	0,4	83,3
49	Opole	8,2	8,0	9,7	7,7	10,8	9,4	0,2	4,1	.	.	3,3	.	.	0,1	3,7	4,3	1,5	2,7	.	.	.	.	.	0,9	1,8	8,2	6,7	0,9	8,4	5,7	106,3
50	Kudowa-Zdrój	10,7	9,2	9,7	8,2	8,6	9,0	0,7	7,3	.	0,1	4,1	.	4,5	3,2	6,0	0,1	2,7	3,1	0,1	.	.	.	.	1,6	0,2	2,5	1,3	0,3	2,9	6,3	102,4
51	Polanica-Zdrój	9,1	9,6	10,8	8,8	9,7	9,9	0,1	4,7	.	.	2,7	.	1,6	.	5,2	.	5,5	2,1	.	.	.	.	.	1,6	2,2	7,1	2,4	0,1	5,6	5,5	104,3
52	Skroniów	7,5	7,9	10,5	7,8	9,9	9,1	4,2	1,8	.	.	.	.	.	0,7	.	4,6	0,5	.	0,6	4,7	.	.	0,2	0,4	2,5	3,7	4,5	0,8	12,0	3,0	96,9
53	Świerklaniec	10,9	9,8	9,8	8,6	11,1	10,7	2,4	5,2	.	.	0,2	.	.	.	6,7	3,8	0,3	0,7	.	0,8	.	.	0,0	2,0	2,1	5,6	5,2	0,8	4,6	4,6	105,9
54	Kraków, Obs. Astr. UJ	7,9	7,8	9,5	7,9	9,6	10,0	3,8	-	.	.	.	.	0,7	0,5	.	4,5	0,4	0,6	0,6	2,7	0,3	.	0,2	1,9	2,7	.	6,7	2,9	9,7	3,8	94,7
55	Cieszyn	9,1	9,2	10,1	10,1	8,3	10,6	1,7	0,0	.	.	.	.	.	.	8,6	4,7	.	0,6	.	.	4,2	.	.	3,9	0,0	1,9	3,6	3,9	4,0	4,2	98,7
56	Istebna-Kubalonka	9,5	9,0	10,1	9,1	10,5	11,2	5,3	3,1	.	.	.	.	0,1	.	8,9	7,0	.	.	.	1,1	3,6	.	.	2,8	0,2	2,3	8,2	1,2	4,0	5,5	112,7
57	Rabka	5,6	7,5	9,6	9,1	10,4	11,1	5,6	1,9	.	.	.	.	.	0,5	9,4	6,7	3,4	.	0,3	2,2	5,8	.	0,1	1,7	3,9	.	5,9	4,9	5,2	2,8	113,6
58	Jabłonka	8,3	8,6	9,6	8,7	10,1	9,4	6,6	1,2	.	.	.	.	.	.	9,0	4,8	2,5	.	0,2	0,3	4,1	.	1,1	1,1	2,3	.	5,7	4,6	3,9	3,8	105,9
59	Krynica	3,4	8,4	8,2	8,8	8,0	9,7	4,6	1,0	.	.	.	.	0,0	0,2	0,5	7,0	5,1	0,4	1,8	2,1	1,0	.	3,1	1,4	6,3	0,6	6,2	1,9	4,3	2,1	96,1
60	Krynica-Góra Park.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
61	Muszyna	2,8	7,2	8,5	9,7	8,4	9,0	4,3	1,5	.	.	.	.	.	0,6	1,2	7,3	5,0	0,4	1,8	3,2	1,1	.	2,7	1,9	4,8	0,1	4,3	1,6	3,4	2,9	93,7
62	Zakopane	3,9	6,3	10,8	9,0	10,0	11,6	6,3	1,5	.	.	0,4	.	.	.	3,9	5,2	2,4	0,2	0,3	0,5	3,1	.	0,1	2,7	6,8	0,1	7,6	4,1	2,2	1,7	100,7
63	Gubałówka	4,0	6,7	10,2	8,7	8,9	10,8	6,7	1,2	.	.	0,1	.	.	.	3,0	6,4	2,5	0,1	0,7	0,6	4,3	.	0,5	3,5	6,4	.	7,3	3,5	2,7	2,8	101,6
64	Hala Gąsienicowa	0,7	3,0	9,8	7,3	8,1	10,2	5,5	3,1	.	.	0,8	.	.	.	2,4	6,6	2,2	0,2	0,2	0,3	1,2	.	0,3	2,7	6,5	.	9,4	0,4	3,1	2,4	86,4
65	Kasprowy Wierch	0,1	4,4	11,9	8,5	9,5	12,0	6,1	0,6	.	0,1	1,3	.	.	.	7,8	2,2	3,2	.	0,7	.	1,2	.	0,5	3,0	3,9	.	9,3	1,4	4,2	1,5	93,4
66	Werbkowice	3,1	6,9	9,0	1,1	.	4,6	5,8	0,3	.	.	1,0	10,4	10,1	.	.	6,5	2,3	4,1	6,5	1,2	.	.	.	3,0	6,9	6,9	1,5	0,9	10,7	5,4	108,2
67	Zdanów	5,5	6,6	6,7	4,7	11,4	5,8	5,3	0,7	.	.	1,4	.	0,8	.	0,3	5,7	4,0	1,1	0,2	1,3	.	0,6	.	1,2	5,6	2,1	3,8	0,3	10,8	5,3	91,2
68	Iwonicz-Zdrój	1,8	3,9	5,0	5,5	8,3	9,7	5,2	1,2	.	0,2	0,3	.	0,1	1,8	0,1	8,8	7,4	3,4	3,3	1,4	2,4	.	1,6	1,2	9,6	4,0	6,9	1,4	8,6	1,8	104,9
69	Lesko	1,8	1,2	4,2	5,0	8,8	9,7	4,8	0,5	.	.	.	0,5	0,3	1,6	1,0	3,8	5,9	6,1	3,3	2,2	3,1	.	1,5	1,6	7,1	4,6	6,0	0,3	6,0	0,6	91,3

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	13,0	12,4	12,5	9,1	.	2,9	3,1	1,2	2,6	.	5,6	11,2	7,8	0,1	2,1	0,3	1,9	2,0	1,8	13,8	14,6	14,5	14,4	2,6	0,7	14,2	13,6	9,7	14,5	12,9	12,5	227,6
2	Kołobrzeg	12,4	11,1	13,2	7,1	3,6	.	2,5	11,2	1,5	.	1,7	9,9	8,7	.	4,4	-	1,7	2,7	2,7	12,8	9,2	13,9	14,0	0,1	.	9,4	11,5	9,5	13,9	14,0	12,9	215,6
3	Świnoujście	11,3	11,0	12,4	(7,6)	1,5	.	0,9	8,0	.	0,0	0,2	9,2	5,8	0,1	0,5	0,1	1,2	2,0	4,5	7,8	6,6	12,3	12,9	.	.	.	10,7	7,7	12,2	9,3	10,2	(165,8)
4	Resko	12,2	10,3	13,0	9,6	2,8	.	2,1	7,8	0,4	.	3,1	9,8	7,6	.	6,0	3,2	3,4	4,0	1,8	10,3	10,2	12,7	13,8	.	.	0,3	9,6	5,8	12,9	12,4	11,2	196,3
5	Szczecinek	13,1	11,9	12,3	11,5	.	.	1,9	3,2	1,0	.	2,5	6,4	6,1	.	8,4	1,4	3,9	4,8	0,2	9,2	8,1	12,0	12,9	.	.	0,3	4,6	3,0	13,8	13,9	10,3	176,7
6	Chojnice	13,4	13,4	12,4	12,1	.	2,8	1,1	2,2	0,3	.	2,0	7,4	8,5	3,5	7,4	1,1	2,3	6,0	.	10,3	8,1	11,2	13,5	.	.	0,1	2,1	5,0	14,4	13,8	12,9	187,3
7	Hel	12,9	12,0	12,4	11,9	.	9,4	1,0	1,2	4,4	.	12,2	9,5	11,4	9,8	9,9	.	1,0	2,9	.	11,9	11,4	13,4	13,3	2,6	.	12,1	4,2	6,9	12,6	13,1	11,4	234,8
8	Gdynia	11,9	13,1	13,4	3,5	.	8,9	0,7	6,1	1,9	.	12,1	11,1	11,3	8,7	7,3	.	2,6	.	5,4	13,4	12,4	14,1	7,3	2,2	0,6	11,4	5,3	9,3	13,4	11,0	15,6	234,0
9	Świbno	12,9	10,9	12,6	11,9	.	8,0	1,4	2,2	3,2	.	11,5	9,0	11,0	0,3	8,9	.	1,2	4,8	.	11,5	5,8	13,5	13,9	1,4	.	10,6	4,7	5,8	12,6	12,0	12,7	214,3
10	Stare Pole	13,0	11,7	11,6	12,4	0,0	7,2	1,2	.	0,1	.	10,2	7,9	11,7	7,8	11,3	0,2	1,9	5,0	.	10,7	10,4	13,2	15,1	0,5	.	1,1	5,5	3,3	5,8	12,8	11,3	202,9
11	Radostowo	13,6	12,4	11,1	13,0	0,1	5,6	0,3	.	.	.	10,2	9,0	10,1	7,2	7,0	0,1	3,0	.	.	12,5	5,7	11,9	14,4	0,1	.	4,6	8,6	3,8	11,8	14,3	12,5	202,9
12	Prabuty	13,7	12,0	11,5	13,6	.	4,3	1,4	.	.	.	5,2	7,0	9,4	8,3	8,9	.	3,4	5,4	0,0	11,9	3,4	8,1	14,6	.	.	.	2,2	3,9	8,3	11,5	12,0	180,0
13	Bydgoszcz, IMiGW	12,9	9,9	12,3	12,1	.	.	1,8	1,8	.	1,3	1,7	5,5	8,4	1,4	8,6	0,7	2,7	3,8	.	8,8	7,2	13,3	11,8	.	.	.	0,1	5,9	4,1	9,4	9,2	154,7
14	Suwałki	8,9	6,9	3,6	12,4	9,3	9,3	1,7	4,4	0,9	3,2	8,7	1,6	12,3	10,5	10,2	5,1	0,4	3,4	.	4,4	11,4	10,9	15,7	6,5	.	.	0,4	7,1	.	.	15,4	184,6
15	Mikołajki	11,3	9,1	10,5	13,5	5,6	10,0	7,9	2,0	.	1,8	7,4	6,4	10,1	12,4	10,2	.	2,5	3,1	0,4	4,5	9,6	12,4	14,8	1,9	.	.	1,5	3,3	0,0	4,2	14,4	190,8
16	Biebrza	10,4	5,6	6,4	11,1	10,0	8,1	2,6	3,1	0,9	4,5	6,5	0,9	11,3	7,3	7,8	2,1	0,4	3,9	.	3,0	11,5	13,0	14,6	2,7	.	.	0,5	1,9	.	0,1	12,6	162,8
17	Białystok	8,3	2,8	4,0	11,5	6,8	2,1	.	5,0	1,6	2,6	4,7	7,5	10,7	6,9	5,9	1,1	1,4	3,1	0,1	1,7	10,4	13,5	14,8	0,8	.	.	3,4	3,1	.	0,2	15,2	149,2
18	Gorzów Wlkp.	12,3	11,9	13,3	6,8	3,0	.	4,2	4,4	0,1	1,9	1,5	11,2	8,7	0,4	2,7	3,8	4,9	5,2	0,4	10,8	11,7	13,7	5,9	.	.	.	4,2	9,3	12,6	14,2	12,8	191,9
19	Przebędowo	12,8	12,5	13,8	11,4	.	.	3,3	2,0	.	.	4,5	5,8	8,3	0,0	5,7	1,7	4,6	4,6	.	11,4	9,6	13,9	9,2	.	.	.	1,3	9,3	0,5	14,8	10,3	171,3
20	Przybroda	12,4	12,9	13,3	11,0	.	.	3,9	3,3	0,1	2,4	1,7	7,9	1,0	.	3,8	1,6	3,8	3,9	0,1	11,3	11,4	14,1	7,9	.	.	.	1,1	10,2	1,2	14,2	9,9	170,4
21	Poznań-Ławica	11,5	10,1	11,8	9,7	.	.	3,5	1,8	.	2,8	1,0	5,4	8,0	.	3,8	1,7	4,1	5,4	.	10,3	9,9	12,2	6,7	.	.	.	1,6	7,1	0,3	11,9	9,0	149,6
22	Plewiska	13,2	12,0	13,3	11,0	.	.	3,4	3,2	.	1,5	1,3	6,2	7,6	.	3,8	2,1	3,9	4,1	.	11,0	8,2	13,8	8,1	.	.	.	0,4	7,4	.	14,1	8,5	158,1
23	Kórnik	12,9	13,3	13,8	11,0	.	.	4,2	1,7	.	3,4	1,6	5,5	8,8	0,3	4,5	2,7	2,8	3,8	.	9,7	8,8	13,9	6,8	.	.	.	0,3	9,2	.	13,9	10,0	162,9
24	Oborniki Śl.	11,0	11,9	11,8	8,9	.	0,2	0,6	.	.	0,8	.	6,9	9,1	2,1	1,5	7,4	10,2	.	.	1,0	8,8	12,2	.	.	.	.	(5,6)	.	.	8,8	.	118,8
25	Laskowice Oławskie	6,7	12,5	10,9	9,7	.	0,5	2,9	0,8	.	1,3	0,2	1,5	9,6	0,2	3,5	2,8	7,0	1,4	0,1	4,8	8,7	13,0	.	0,2	.	1,6	1,1	.	.	4,3	4,2	109,5
26	Ciechocinek	13,7	13,3	9,4	12,9	.	.	1,7	0,7	.	1,9	1,3	4,3	10,6	1,2	6,7	0,4	3,9	5,8	.	10,1	10,5	13,0	11,3	.	.	.	.	8,6	1,1	9,4	13,5	165,3
27	Więcławice	13,2	12,8	11,7	11,1	.	.	2,2	1,8	.	2,0	2,1	5,7	8,4	1,5	8,7	1,5	3,8	5,2	.	10,5	10,6	13,4	10,4	.	.	.	0,8	9,2	1,5	10,8	13,7	172,4
28	Legionowo	11,8	8,0	6,0	12,8	0,5	.	3,6	0,0	0,0	4,8	4,3	2,2	10,6	3,6	7,3	1,4	7,2	3,2	-	3,1	10,6	13,4	9,4	.	0,0	0,0	0,5	0,3	.	8,9	12,9	146,4
29	Warszawa-Bielany	14,0	9,7	6,9	14,1	0,4	.	3,3	1,9	.	5,3	4,9	3,8	12,7	3,0	8,2	2,8	9,1	3,9	0,3	2,4	10,4	14,5	8,4	.	.	.	0,7	0,3	.	8,8	13,0	162,8
30	Warszawa, Min. Kom.	12,3	8,9	8,0	12,9	0,4	.	3,7	1,5	0,1	5,3	4,3	5,3	11,1	3,9	8,8	1,9	6,4	3,9	0,2	1,5	11,1	12,4	6,5	.	.	.	0,8	0,3	.	7,6	12,4	153,5
31	Międzylesie	12,5	-	3,8	12,2	0,7	0,1	2,3	1,5	.	5,2	3,6	6,3	12,6	4,2	3,3	8,0	9,3	3,5	0,6	2,7	11,3	9,7	6,9	2,9	0,1	0,1	1,3	0,2	.	5,8	9,8	-
32	Brwinów	13,4	8,0	8,6	13,9	.	.	4,9	0,6	.	1,1	3,9	2,8	12,1	5,9	6,7	2,6	7,1	2,6	0,1	3,7	10,6	13,6	4,5	.	0,0	0,1	0,6	0,3	.	7,4	11,4	146,5
33	Świder	12,5	6,7	3,2	12,9	0,9	.	1,7	2,6	0,3	3,1	3,1	8,0	11,6	6,1	7,4	4,1	8,6	5,2	0,6	2,5	9,3	12,4	5,9	.	.	0,2	0,7	.	.	7,9	12,6	150,1
34	Topola-Błonie	12,8	10,5	10,8	12,3	.	.	3,1	1,0	.	5,7	0,7	3,3	11,4	0,6	5,8	1,0	5,7	3,1	0,1	6,6	10,3	13,1	5,5	.	0,3	0,2	0,7	3,2	.	10,3	12,5	150,6
35	Młochów	13,5	5,6	6,0	13,5	.	.	4,0	0,9	.	3,5	4,8	4,3	11,9	5,2	5,2	1,7	8,3	3,0	0,1	1,7	6,4	5,1	13,7	.	.	.	1,3	0,0	.	10,1	13,7	143,5
36	Skierniewice	13,8	6,2	7,7	12,3	.	.	5,2	0,2	.	4,3	2,1	2,1	11,1	2,0	5,9	2,1	7,9	2,0	0,0	4,7	11,2	13,1	4,0	.	0,3	0,2	2,3	0,1	.	10,0	13,7	144,5
37	Balek	12,7	7,6	9,3	12,4	.	.	3,2	0,3	.	4,2	2,7	8,5	10,6	3,7	6,0	0,8	6,9	4,0	0,7	.	11,4	13,0	4,4	0,6	.	0,5	6,5	.	.	10,4	12,4	152,8
38	Łódź-Lublinek	13,1	10,6	11,1	12,5	.	.	3,6	.	.	2,4	0,5	3,5	11,4	0,1	4,1	0,6	3,4	1,5	0,2	3,2	9,1	12,8	3,5	.	0,1	.	2,8	0,5	.	8,5	10,9	130,0
39	Kalisz	12,7	13,2	11,9	10,7	.	.	2,1	0,5	.	2,9	0,7	3,4	11,8	0,1	5,1	3,0	5,4	1,8	0,7	7,3	10,5	13,7	4,0	.	.	1,1	1,5	5,6	.	11,0	8,7	149,4
40	Wieluń	11,7	10,7	12,3	12,0	0,0	.	3,0	1,4	.	2,3	0,1	4,5	12,6	0,3	4,0	3,7	6,8	2,0	3,2	0,0	11,4	12,7	.	0,1	.	0,5	5,6	0,1	.	4,6	8,3	133,9
41	Szepietowo	9,9	4,9	7,4	13,1	6,0	.	1,4	4,7	0,3	5,1	8,4	10,4	12,9	7,3	6,5	3,1	4,8	4,2	0,7	2,6	11,4	12,7	14,5	.	.	.	2,4	.	0,4	.	14,7	169,8
42	Białowieża	7,9	2,9	3,9	9,6	6,7	0,4	.	5,3	2,1	3,2	8,9	6,9	13,3	7,4	8,5	3,7	1,5	5,2	6,7	1,4	14,1	11,7	14,4	0,1	0,5	.	4,6	1,9	.	0,5	14,2	167,5
43	Terespol	9,3	3,4	5,6	9,6	5,2	.	0,1	8,3	2,2	2,9	5,5	11,8	11,3	8,1	10,7	7,0	4,5	5,9	8,2	0,4	14,1	13,8	11,7	.	1,9	.	6,4	0,2	.	2,5	12,8	183,4
44	Sobieszyn	10,4	5,9	5,3	13,5	0,8	.	0,5	7,6	0,7	5,2	2,2	12,8	10,9	6,2	9,3	4,2	8,0	5,2	8,1	.	10,1	12,8	2,0	.	0,4	0,2	9,5	0,2	.	5,6	12,2	169,8
45	Puławy	9,9	4,1	4,7	12,7	8,3	.	0,2	7,4	0,4	1,9	1,0	12,0	10,3	4,2	6,4	2,4	5,1	3,8	7,6	0,2	9,5	11,4	.	.	0,6	0,2	7,0	0,0	0,1	8,7	9,0	145,1
46	Chełm	9,8	3,0	4,8	12,4	1,1	.	.	9,5	3,8	2,7	0,2	6,5	6,7	9,1	6,0	5,9	6,6	5,0	9,4	0,1	10,2	11,9	.	0,5	4,0	1,0	8,8	0,3	0,3	5,4	8,8	153,8
47	Szczawno-Zdrój	9,3	12,1	12,4	5,5	1,6	2,0	5,0	0,3	0,3	2,2	.	4,7	6,0	0,3	2,1	4,6	10,1	2,4	0,4	4,5	5,5	12,2	.	1,4	.	2,8	0,4	.	.	12,1	1,4	121,6
48	Śnieżka	7,9	12,9	13,1	6,0	0,9	0,3	4,9	-	.	0,4	.	0,9	5,2	1,1	2,4	4,2	6,0	0,3	0,8	2,0	5,2	13,5	.	.	.	2,5	0,7	.	.	9,8	3,3	104,3
49	Opole	7,1	12,3	12,7	10,4	1,3	0,4	1,0	0,2	0,1	3,2	0,0	3,7	10,7	0,7	3,9	3,7	8,2	.	1,7	3,4	11,7	11,3	.	0,4	.	3,9	7,6	0,1	.	5,3	3,3	128,3
50	Kudowa-Zdrój	8,6	12,9	13,1	7,9	1,2	2,0	7,1	.	0,8	.	0,1	7,3	9,7	1,9	4,2	1,9	8,8	4,1	1,4	3,1	9,6	12,6	2,8	.	3,5	.	5,9	.	.	13,4	1,8	145,7
51	Polanica-Zdrój	10,0	13,1	12,7	7,1	1,2	2,7	7,1	.	0,3	3,1	.	4,7	5,1	0,2	2,4	3,3	8,5	5,5	0,4	2,4	6,7	11,9	.	1,0	.	4,0	6,0	.	.	10,3	.	127,7
52	Skroniów	11,3	11,6	9,4	12,7	.	.	1,7	2,2	0,9	3,9	1,9	12,4	11,6	3,4	4,8	1,2	5,5	6,3	6,7	0,5	12,3	10,2	.	0,4	1,3	3,6	3,3	1,0	1,4	6,1	4,6	152,2
53	Świerklaniec	9,2	9,5	11,8	11,2	0,5	.	4,1	0,5	0,3	3,6	1,9	7,7	11,3	0,4	4,5	4,0	7,4	4,6	5,8	2,3	12,2	9,9	.	.	.	2,1	4,0	0,6	0,2	4,6	3,5	137,7
54	Kraków, Obs. Astr. UJ	9,5	8,9	10,7	12,1	.	.	0,6	0,7	2,7	4,5	0,6	9,8	10,8	3,8	4,2	0,9	8,9	8,5	7,0	0,3	6,0	8,5	.	0,4	0,1	1,5	3,2	0,2	1,2	6,0	1,1	132,7
55	Cieszyn	4,9	12,8	10,9	10,9	0,3	0,2	3,2	.	0,7	2,0	.	0,8	6,5	0,1	2,6	1,6	6,5	7,8	2,7	0,0	9,2	5,7	.	1,3	.	1,8	3,0	0,2	0,6	2,7	0,8	99,8
56	Istebna-Kubalonka	5,4	12,6	12,3	11,4	.	.	4,1	0,0	0,1	2,5	.	.	9,7	0,9	3,8	1,4	5,9	9,9	7,3	1,3	7,7	7,9	0,5	1,5	0,1	2,8	3,7	0,3	3,8	1,8	1,0	119,7
57	Rabka	6,0	11,4	11,0	11,8	.	.	0,8	1,0	3,0	3,7	0,5	1,9	10,7	2,1	3,9	2,6	9,9	7,4	11,0	1,4	7,4	7,1	0,1	1,8	0,3	4,2	7,6	1,7	5,0	6,1	2,2	143,6
58	Jabłonka	6,3	9,8	11,9	9,6	.	.	1,9	0,9	2,6	3,8	0,4	4,2	11,2	1,8	4,2	1,5	9,7	10,0	6,8	1,5	7,5	6,3	.	2,0	0,5	4,5	4,4	0,5	5,7	3,6	0,3	133,4
59	Krynica	9,3	7,8	7,3	11,0	.	.	1,0	3,5	1,4	3,7	0,4	1,0	7,2	3,6	3,9	.	5,1	4,8	9,5	1,3	8,0	5,3	.	1,9	1,3	4,4	5,3	1,2	6,9	2,7	1,8	120,6
60	Krynica-Góra Park	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	3,8	1,0	1,1	-
61	Muszyna	8,8	7,2	8,5	12,0	.	.	1,2	2,3	1,5	3,9	0,3	0,1	4,3	2,4	4,6	0,9	9,0	6,7	9,0	1,1	3,9	2,7	0,1	1,6	1,8	5,0	4,6	0,8	8,0	1,3	3,6	117,2
62	Zakopane	2,8	9,6	13,3	12,3	.	.	0,1	0,4	2,1	2,1	0,1	.	11,2	2,0	2,9	1,9	9,8	10,7	9,8	2,3	6,2	3,3	0,4	1,2	0,3	5,6	5,0	0,1	5,2	0,2	0,1	121,0
63	Gubałówka	3,2	9,7	12,0	11,6	.	.	.	0,5	2,5	3,9	0,4	0,0	10,9	2,5	3,9	2,2	10,3	10,0	9,0	1,5	6,7	4,6	0,1	0,9	0,4	4,9	6,8	0,6	4,6	0,1	0,2	124,0
64	Hala Gąsienicowa	0,2	10,0	10,3	11,7	.	.	.	0,4	1,9	0,9	.	.	9,9	1,4	1,1	2,1	8,9	9,1	6,1	0,7	5,2	4,7	0,4	1,2	0,0	4,0	6,2	0,4	4,3	0,3	0,6	102,0
65	Kasprowy Wierch	0,3	11,0	11,6	12,8	.	.	.	0,6	1,0	1,2	.	.	9,7	0,9	1,2	2,1	10,4	9,3	6,3	1,2	6,4	5,0	0,6	0,2	0,1	7,9	6,3	0,2	1,1	0,7	0,2	108,3
66	Werbkowice	11,6	3,6	7,2	9,8	3,6	.	1,0	11,1	6,2	3,5	0,5	4,6	3,7	12,0	3,1	5,1	5,9	8,2	5,0	0,1	10,4	11,5	.	0,6	2,2	2,6	10,2	5,3	2,6	4,4	9,8	165,4
67	Zdanów	11,8	9,6	7,6	13,3	.	.	1,2	6,7	2,2	4,2	1,5	12,1	11,0	5,7	3,2	.	6,9	6,0	5,8	0,2	8,3	10,1	0,2	.	1,6	0,5	6,2	0,7	0,4	10,1	6,4	153,5
68	Iwonicz-Zdrój	10,4	5,7	7,1	11,4	.	.	0,9	6,8	1,0	4,6	3,8	.	2,2	6,0	3,6	1,6	8,8	6,9	9,0	.	9,6	1,7	.	2,9	1,1	2,6	8,3	0,4	6,6	2,6	5,0	130,6
69	Lesko	8,3	3,4	5,3	12,5	.	.	2,1	7,8	2,6	5,2	4,1	.	.	7,7	4,6	0,3	5,8	7,7	4,5	.	6,0	0,7	.	3,0	1,9	1,8	6,7	0,9	5,6	2,3	4,0	114,9

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	.	5,6	12,9	14,3	14,3	15,1	14,3	13,4	9,9	8,4	2,8	2,5	.	13,9	13,2	6,2	8,0	3,4	7,6	11,0	12,6	4,9	5,6	8,4	8,9	8,3	10,3	8,2	10,9	11,9	266,8
2	Kołobrzeg	.	8,5	0,2	14,0	15,1	15,1	13,4	14,7	14,6	7,6	6,9	5,8	6,6	14,1	13,9	4,8	2,8	4,0	4,2	12,1	5,7	3,1	1,4	6,4	10,2	7,0	10,1	5,5	7,6	11,5	246,9
3	Świnoujście	.	12,3	.	8,9	11,7	12,7	10,4	7,5	8,7	7,4	10,8	0,8	2,4	9,4	10,0	3,1	1,9	4,1	3,0	8,7	1,4	3,6	0,6	5,4	7,7	6,7	6,9	4,2	6,5	12,2	189,0
4	Resko	.	5,7	0,6	12,9	11,3	13,6	9,8	11,8	13,5	6,2	4,3	4,3	0,3	12,8	12,1	7,7	1,8	4,3	5,7	9,3	7,0	6,4	1,1	7,9	12,0	6,4	8,9	5,9	8,7	11,9	226,2
5	Szczecinek	.	1,1	4,1	12,3	12,3	14,4	13,0	13,9	13,1	6,1	3,0	2,3	4,1	13,3	11,7	9,2	6,8	2,7	4,9	8,4	9,1	5,3	2,3	10,7	13,0	7,8	7,1	7,1	5,1	13,2	237,4
6	Chojnice	.	.	9,9	11,2	12,1	14,8	7,4	14,8	9,8	6,5	2,7	2,8	2,0	14,3	11,7	11,6	7,7	3,2	4,8	10,7	9,1	7,3	4,1	11,6	12,6	8,9	6,3	7,7	4,6	13,5	243,7
7	Hel	.	.	9,4	9,1	13,9	13,7	12,0	13,9	1,5	10,4	5,1	.	.	13,5	13,6	9,8	11,3	2,6	7,4	8,3	12,3	5,3	4,6	7,8	9,0	9,1	10,0	7,7	10,1	13,1	244,5
8	Gdynia	.	.	8,3	10,0	14,6	15,1	14,1	15,1	0,7	11,5	5,1	0,1	0,7	13,9	15,0	11,1	11,6	6,7	1,6	10,7	11,8	6,1	6,0	6,1	9,3	10,5	9,7	8,7	9,1	15,4	258,6
9	Świbno	.	.	9,9	9,0	14,1	14,5	14,1	12,9	2,1	12,3	3,0	.	.	13,4	14,7	11,8	11,6	2,7	3,6	9,2	11,0	7,4	3,3	6,1	10,0	8,9	7,4	8,8	7,6	13,7	243,1
10	Stare Pole	.	.	13,6	12,0	13,8	13,0	14,5	13,5	4,0	8,6	0,3	.	.	12,7	14,3	12,3	11,3	1,3	3,5	9,7	9,7	7,5	4,3	6,8	11,3	9,8	7,1	10,4	6,2	13,7	245,2
11	Radostowo	.	.	9,5	10,3	13,9	14,1	13,8	11,6	7,0	9,8	0,8	1,0	1,6	14,4	14,4	12,2	10,5	3,0	3,9	10,4	10,0	7,6	5,1	7,3	11,4	9,0	6,6	9,9	9,3	13,6	252,0
12	Przebuty	0,6	.	8,1	12,7	13,6	14,1	14,4	13,7	8,0	11,6	.	1,7	0,7	12,6	15,2	13,6	11,1	1,2	3,1	8,9	10,2	9,3	5,2	7,6	11,9	9,9	7,7	10,5	5,6	14,9	257,7
13	Bydgoszcz,IMiUZ	0,1	.	6,8	10,4	5,6	14,5	11,2	13,7	9,0	0,6	.	1,4	0,6	11,5	12,8	11,1	6,2	2,3	4,8	10,3	7,1	7,9	4,0	10,4	10,0	8,2	3,3	8,8	8,9	14,5	216,0
14	Suwałki	0,6	1,1	7,9	13,9	13,8	8,3	0,2	10,5	2,0	8,8	1,0	1,8	2,1	11,7	15,8	13,3	15,4	6,3	2,8	4,4	12,4	12,5	3,1	11,0	7,3	13,7	9,9	9,5	3,9	15,2	240,2
15	Mikołajki	0,5	0,1	10,1	12,7	11,8	9,6	5,1	14,5	1,4	9,2	.	1,5	0,3	11,5	15,2	14,0	14,1	2,6	3,7	5,9	9,3	.	.	11,8	9,9	12,9	8,9	9,1	7,4	14,9	228,0
16	Ełcbrza	1,1	1,4	11,0	11,4	10,4	4,6	2,8	12,2	1,1	8,1	.	4,6	3,0	7,0	14,1	12,2	13,5	4,2	4,0	4,3	11,1	11,0	3,9	10,0	7,8	12,2	8,0	10,0	5,1	14,5	224,6
17	Białystok	2,1	2,2	7,5	12,4	2,3	.	2,5	11,2	3,4	6,7	.	4,0	0,2	1,3	14,9	11,0	15,2	4,9	0,9	3,6	9,9	13,3	5,6	12,8	10,7	14,3	9,5	2,7	4,2	15,4	204,7
18	Gorzów Wlkp.	.	2,3	13,9	12,3	1,4	11,6	10,4	13,6	7,7	1,8	6,2	1,2	4,6	13,4	13,4	7,0	1,7	5,5	7,5	5,8	5,2	7,4	5,5	9,6	12,2	7,6	2,3	10,9	10,0	13,7	225,7
19	Przesędowo	0,5	0,2	12,6	10,5	.	12,6	10,5	13,2	8,0	2,3	2,2	.	4,8	7,1	12,9	11,7	2,7	5,3	5,8	5,7	10,0	8,2	5,1	9,7	11,5	7,9	.	8,3	9,7	13,8	212,8
20	Przybroda	1,1	0,3	13,0	12,3	.	11,6	10,7	12,5	9,3	2,1	3,1	.	7,8	11,6	13,7	11,4	4,3	5,8	6,5	7,3	11,1	10,4	7,5	9,9	11,4	8,5	.	9,1	9,5	13,7	235,5
21	Poznań-Ławica	0,5	0,4	10,2	9,4	.	10,5	10,3	11,3	7,7	2,4	4,2	0,4	6,0	7,7	10,8	10,2	2,1	4,6	6,4	5,1	10,5	8,7	6,0	8,7	10,5	6,1	.	9,9	8,1	11,7	200,4
22	Plewiska	0,2	0,0	9,8	10,8	.	11,8	11,7	12,5	7,5	2,3	.	0,1	4,7	6,7	14,7	11,6	3,0	5,1	5,6	5,7	11,2	9,0	4,0	6,5	12,7	7,3	.	9,5	8,6	14,5	207,1
23	Kórnik	0,8	.	8,8	10,7	.	9,7	12,3	11,8	7,1	0,7	2,0	.	5,1	7,6	14,6	11,8	3,5	5,7	5,9	6,7	11,5	8,4	5,6	10,2	12,9	8,5	.	10,4	8,9	14,7	215,9
24	Oborniki Śl.	.	.	6,1	.	.	.	13,0	10,1	4,2	4,8	.	.	4,4	9,1	13,7	13,0	0,5	8,1	1,3	9,6	12,8	9,7	12,0	11,0	12,7	5,8	9,5	11,7	7,9	10,1	201,1
25	Laskowice Oławskie	4,1	0,2	13,5	.	.	.	13,6	8,9	3,2	3,9	.	0,0	1,5	4,8	13,1	12,3	2,5	8,0	6,6	9,7	11,1	9,2	6,7	11,5	12,3	8,9	1,4	5,8	8,3	13,1	194,2
26	Ciechocinek	1,4	.	8,6	10,1	1,7	11,9	11,3	14,4	8,6	1,4	.	.	0,9	10,1	14,6	11,5	9,3	2,8	3,0	10,2	8,8	8,7	4,5	10,7	11,6	10,1	3,3	6,9	8,9	14,1	219,4
27	Włocławek	1,0	.	10,4	9,8	0,6	13,3	12,4	13,8	8,5	2,5	.	1,8	3,3	10,3	14,0	12,9	4,5	3,7	4,9	8,6	8,5	10,5	3,1	10,4	11,9	9,3	8,5	1,3	9,5	13,1	222,4
28	Legionowo	5,9	0,9	6,8	9,6	.	.	12,1	13,4	6,9	0,8	.	5,8	.	2,1	12,5	12,9	12,6	1,6	3,3	12,6	9,9	11,0	4,9	10,1	12,0	10,6	(5,1)	6,9	5,8	13,7	(209,8)
29	Warszawa-Bielany	7,8	1,5	7,3	10,0	.	0,1	12,7	15,4	6,9	0,9	.	6,8	0,7	3,0	13,2	14,4	13,5	2,1	3,8	12,0	11,1	14,0	8,1	11,7	13,0	11,8	7,3	7,2	7,5	15,4	239,2
30	Warszawa,Mis.Kom.	7,2	1,5	6,3	7,4	.	0,0	13,4	11,9	4,7	0,3	.	4,6	0,2	1,6	10,6	12,8	12,0	1,7	3,4	12,0	10,5	11,5	6,4	9,5	12,0	10,6	6,3	4,7	6,7	13,7	203,5
31	Międzylesie	8,6	1,4	6,8	7,6	.	0,6	12,0	14,5	7,1	1,0	0,1	6,0	0,8	2,0	12,8	13,7	10,5	3,6	1,2	9,3	9,5	12,4	7,9	10,4	12,8	11,1	4,2	7,9	6,8	14,5	217,1
32	Rzeniów	7,6	1,1	9,7	10,0	.	.	7,4	14,8	7,2	0,8	3,6	1,7	.	2,4	13,6	13,5	12,9	2,6	.	11,1	11,2	12,0	7,2	9,4	13,3	11,5	5,6	4,5	8,1	14,5	217,3
33	Świder	7,8	1,2	8,0	7,5	.	.	10,2	13,1	7,7	1,3	.	5,4	.	0,4	9,9	12,6	12,9	2,0	2,7	11,0	11,0	13,3	7,6	9,0	11,9	11,6	7,0	3,3	6,6	13,5	208,5
34	Tępela-Błonie	3,4	.	6,1	10,6	.	.	12,0	13,2	6,8	0,4	.	1,2	4,5	8,4	14,5	11,7	6,5	4,8	4,8	8,1	8,6	9,5	5,8	9,1	12,6	10,2	0,4	5,6	7,4	13,9	200,1
35	Młochów	7,6	1,4	8,9	10,2	.	.	9,5	14,9	6,0	1,2	.	5,3	1,9	1,0	13,9	13,3	13,3	1,8	4,3	12,0	8,6	12,1	6,9	9,8	12,0	11,7	5,1	3,9	6,7	15,1	218,4
36	Skierniewice	3,1	.	11,9	10,6	.	0,5	11,0	14,7	11,5	0,7	.	2,7	7,2	5,5	14,3	13,8	11,4	3,0	4,3	11,9	10,9	12,4	7,9	12,1	14,2	11,3	5,1	6,7	9,5	15,1	243,3
37	Bełsk	9,8	1,1	9,1	9,0	.	.	10,8	14,1	8,4	1,2	.	3,8	4,3	0,6	12,3	13,2	12,1	2,1	3,7	11,3	10,4	11,4	8,2	11,0	11,9	10,8	5,6	4,0	8,1	15,9	222,2
38	Łódź-Lublinek	5,3	.	7,3	9,6	.	0,1	12,3	13,5	9,3	0,6	.	0,3	3,8	4,9	14,0	11,8	6,7	4,7	4,0	8,8	11,5	10,1	6,3	11,9	13,4	10,1	1,9	3,6	7,2	14,0	209,2
39	Kalisz	4,0	0,4	12,1	9,4	.	0,2	13,2	12,3	7,9	1,9	.	0,6	.	4,8	13,2	12,6	6,3	7,4	6,5	7,3	11,9	10,3	7,8	12,0	13,1	9,7	0,5	7,3	8,5	13,4	214,5
40	Wieluń	6,4	.	15,2	5,5	.	.	14,7	12,6	5,2	6,4	.	.	2,4	3,6	15,0	14,3	5,1	11,5	4,5	9,4	13,8	12,5	8,5	13,4	14,5	11,2	1,1	5,3	8,5	15,4	236,0
41	Szepietowo	2,0	1,7	8,1	9,8	0,4	.	6,5	14,2	.	4,9	.	3,7	.	.	8,8	14,9	14,6	2,1	1,0	5,3	11,0	12,3	6,1	12,9	9,6	12,9	8,4	3,9	4,5	14,9	195,4
42	Białowieża	3,4	.	8,7	4,8	1,2	.	0,5	7,2	2,5	5,7	0,1	4,3	.	0,1	11,5	10,6	12,5	4,9	0,8	3,8	11,6	11,6	7,9	12,1	9,5	11,2	8,5	0,4	5,0	14,6	175,0
43	Terespol	4,6	4,8	11,2	9,0	.	.	1,7	10,9	0,2	2,7	0,8	3,4	.	0,0	9,2	12,8	14,1	6,3	1,8	10,1	10,7	12,9	6,1	12,3	8,9	12,5	9,2	0,1	7,4	13,6	197,3
44	Sobieszyn	7,4	3,2	10,0	9,2	.	.	7,3	14,1	3,6	.	1,0	4,7	0,5	.	8,7	12,4	14,4	4,5	3,4	13,5	9,8	14,1	7,8	11,2	10,2	12,5	8,2	0,2	6,6	14,8	213,3
45	Paławy	6,8	3,0	10,5	6,6	.	.	4,8	13,7	3,6	0,1	.	3,2	.	.	7,5	12,9	13,0	2,6	2,0	11,6	7,7	11,3	5,5	10,3	8,6	11,4	6,8	0,1	6,6	12,8	183,0
46	Chełm	4,7	11,6	11,0	7,7	.	.	2,3	14,1	5,5	0,3	2,0	4,2	.	.	1,9	12,9	15,1	3,3	1,6	14,6	9,9	12,7	8,4	12,8	10,2	13,2	12,8	.	8,7	14,7	216,2
47	Szczawno-Zdrój	3,1	1,8	12,4	.	.	.	6,3	7,7	1,2	6,2	0,7	0,9	0,9	3,2	9,2	12,5	1,3	9,1	7,4	6,3	7,1	9,8	8,5	7,2	10,2	9,0	1,6	8,5	8,3	13,8	174,2
48	Śnieżka	.	1,6	9,7	.	.	.	2,8	3,5	0,3	2,7	.	2,7	0,2	0,1	3,1	12,7	.	5,3	7,1	7,8	10,9	6,5	3,0	9,5	14,3	10,0	2,1	7,4	9,4	14,5	147,2
49	Opole	6,0	2,9	10,5	.	.	.	12,4	7,9	4,2	3,5	.	.	3,2	4,9	10,0	12,4	4,1	10,1	8,6	8,7	10,4	11,1	12,4	11,3	12,7	9,7	3,9	9,6	5,5	11,0	207,0
50	Kudowa-Zdrój	0,7	4,3	10,9	0,1	.	5,3	.	7,4	1,9	5,7	0,5	.	0,1	2,6	8,4	13,1	0,5	8,7	7,2	9,4	10,8	12,4	9,7	11,4	13,8	10,0	6,4	8,2	9,8	13,0	192,3
51	Polanica-Zdrój	5,5	1,2	9,4	.	.	.	8,1	10,2	1,2	2,4	0,1	0,2	2,3	2,6	6,6	12,3	1,9	9,3	7,0	10,8	8,1	10,1	12,3	11,8	12,5	8,8	3,5	6,8	9,6	12,3	186,9
52	Skroniów	11,1	1,1	10,1	4,0	.	.	8,8	13,2	5,8	10,8	1,6	3,7	2,9	1,0	14,2	13,3	8,6	4,1	5,8	10,7	12,5	12,1	9,0	12,9	13,6	11,2	8,4	.	10,3	13,6	234,4
53	Świeradzkiniec	7,7	0,1	8,0	.	.	.	11,2	7,2	3,0	3,3	.	.	1,0	1,3	13,3	11,5	4,7	8,8	5,4	9,4	7,8	10,8	8,0	10,8	12,8	9,6	6,5	0,8	7,7	12,7	183,4
54	Kraków,Obs.Astr.U.	10,2	5,7	8,2	0,8	.	.	6,7	10,1	4,7	6,1	2,3	1,5	1,3	1,5	12,7	13,0	7,1	5,6	7,5	8,9	8,5	11,6	9,3	10,6	10,8	11,1	10,6	.	9,0	12,6	206,0
55	Cieszyn	10,4	3,9	6,7	.	.	.	8,1	6,9	1,8	1,3	0,1	.	3,5	0,3	7,3	14,0	4,2	11,7	10,9	.	9,6	14,0	11,6	12,6	13,3	10,7	9,4	0,2	8,5	14,6	195,6
56	Istebna-Kubalonka	8,0	3,0	8,2	.	.	.	6,7	10,1	2,9	1,9	.	.	5,1	0,3	10,2	14,0	6,0	10,1	8,7	10,5	8,7	13,7	6,5	11,6	13,3	11,3	7,2	0,0	10,0	14,0	203,0
57	Rabka	10,0	9,8	9,3	0,7	0,2	0,3	4,2	9,7	4,7	3,0	2,1	.	8,4	1,4	11,9	14,1	3,7	7,8	6,4	8,0	9,7	13,4	8,5	10,3	12,7	10,7	8,6	.	9,1	13,3	212,0
58	Jabłonka	10,4	6,2	7,4	0,1	.	2,0	8,0	8,3	5,8	4,1	4,6	0,8	9,9	1,9	12,9	11,6	6,2	4,8	4,9	10,3	9,3	13,5	10,3	11,8	10,8	9,5	5,9	.	8,6	10,0	209,9
59	Krynica	10,6	10,7	7,6	1,8	0,2	0,1	4,4	7,3	6,9	3,1	.	2,1	10,4	3,3	4,8	11,4	10,3	3,7	5,7	8,7	7,5	12,2	5,5	10,1	11,8	8,9	9,1	.	10,1	12,3	200,6
60	Krynica-Góry Park.	9,4	8,7	6,8	1,2	0,2	.	4,9	6,0	5,1	3,1	.	1,8	9,1	3,3	4,3	11,3	10,8	3,2	5,8	10,4	7,2	12,2	6,4	10,0	12,1	9,4	9,5	.	8,8	13,3	194,3
61	Muszyna	10,5	11,4	9,1	1,6	0,1	.	4,0	8,1	5,4	3,7	.	1,1	8,9	4,7	5,0	12,8	11,0	3,2	4,8	10,0	7,6	12,1	7,9	12,3	9,6	11,0	8,6	.	9,5	11,6	205,6
62	Zakopane	10,6	12,2	8,6	.	.	0,1	1,1	8,3	4,1	1,5	0,1	.	8,3	0,4	11,1	12,9	7,9	2,4	4,5	8,6	9,0	9,7	9,5	10,6	11,6	10,5	5,6	.	9,8	13,3	192,3
63	Gubałówka	10,0	11,2	8,9	.	.	0,5	1,7	8,4	4,9	1,7	0,3	.	7,6	1,0	11,5	11,5	7,5	1,7	4,5	9,0	9,1	9,8	7,7	10,6	9,3	10,3	5,5	.	8,9	11,4	184,5
64	Hala Gąsienicowa	9,6	9,4	7,0	.	0,1	.	0,6	7,7	3,9	1,9	.	.	6,2	.	9,4	9,7	8,5	0,5	4,0	7,7	5,8	11,9	7,1	7,0	8,8	8,3	3,1	.	9,2	12,3	159,7
65	Kasprowy Wierch	9,1	8,8	7,8	0,0	0,1	0,1	0,9	3,8	2,9	0,5	.	.	6,2	.	10,5	10,3	7,6	0,6	3,1	6,9	6,9	12,4	7,1	8,5	11,6	7,5	3,2	.	9,2	15,2	160,6
66	Borkowice	1,5	12,0	8,7	9,6	.	.	1,8	14,2	5,5	1,4	1,7	4,4	0,2	1,3	2,3	12,4	14,5	3,5	0,6	12,8	12,6	12,5	9,6	13,3	12,6	13,4	13,0	.	9,3	14,0	218,7
67	Zdanów	8,0	7,2	10,0	6,6	.	.	6,3	13,8	2,8	0,4	(1,6)	5,7	6,3	3,0	4,8	14,0	2,4	1,8	5,0	12,4	11,9	11,6	7,4	12,7	13,6	(11,2)	8,8	.	11,6	13,3	(214,2)
68	Inowłódz-Zdrój	7,3	6,6	8,6	3,6	.	.	2,5	3,8	1,5	4,2	0,2	0,2	5,0	0,8	1,8	12,6	13,4	2,3	3,6	9,8	8,3	12,2	7,1	7,8	13,1	12,9	12,4	0,1	7,1	13,4	182,2
69	Łeba	5,9	7,7	11,4	4,8	0,4	0,1	2,9	8,8	2,2	5,5	0,1	0,6	4,3	1,5	4,1	9,3	13,8	1,7	3,4	8,2	8,2	13,2	6,5	5,5	13,7	13,4	10,8	.	7,8	13,5	189,3

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	12,7	2,8	2,7	10,5	8,4	3,8	0,5	2,2	.	9,1	5,2	2,0	6,9	2,2	12,6	.	3,5	15,5	15,6	15,0	10,4	6,7	2,6	3,2	12,0	0,3	5,1	5,6	.	2,8	2,5	187,4
2	Kołobrzeg	11,8	2,6	4,7	6,7	7,0	3,9	1,2	1,1	2,0	8,5	5,2	1,4	4,9	7,2	8,5	.	1,1	15,2	14,9	14,0	9,4	7,1	2,9	2,1	10,6	0,1	2,7	1,3	.	1,9	8,2	166,2
3	Świnoujście	9,1	2,2	5,2	2,3	6,7	4,1	.	.	4,8	4,9	1,9	2,2	6,4	4,8	3,5	.	.	14,5	14,3	11,4	5,3	4,4	1,9	3,9	9,2	.	1,9	2,2	.	3,7	9,5	140,3
4	Resko	10,1	5,0	4,3	3,0	7,2	4,0	0,1	0,0	5,4	7,6	3,6	2,0	7,5	7,5	10,1	5,9	.	13,7	13,1	13,5	8,4	8,7	2,7	4,9	10,5	1,7	1,3	4,2	.	3,5	8,2	177,7
5	Szczecinek	9,2	6,2	5,5	4,1	9,0	3,4	1,5	.	7,3	8,7	7,0	1,5	10,0	7,5	9,8	1,6	.	15,0	14,4	14,3	5,6	7,8	2,4	9,2	11,2	4,2	0,2	4,5	.	4,0	5,5	190,6
6	Chojnice	9,1	6,4	7,9	5,8	4,7	4,8	1,9	1,9	7,3	9,1	7,6	0,4	9,1	10,6	8,7	2,5	.	14,6	13,7	14,5	5,4	7,1	3,9	8,2	12,4	3,8	1,1	3,8	.	3,2	7,2	196,0
7	Hel	9,9	3,8	0,9	5,1	9,0	1,6	1,7	4,5	1,4	2,6	7,3	0,0	10,3	7,4	11,1	.	1,6	13,8	13,1	13,3	7,0	4,3	3,0	4,4	9,3	2,8	4,1	6,7	.	1,9	7,4	169,3
8	Gdynia	12,3	4,0	4,0	6,6	6,5	5,1	2,5	5,8	.	7,2	5,0	0,6	11,4	9,3	12,9	.	.	15,5	15,3	15,2	9,0	7,9	1,2	10,1	9,7	3,9	0,7	7,8	10,3	0,9	1,5	208,2
9	Świbno	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
10	Stare Pole	6,8	6,3	1,7	8,1	6,5	4,7	4,0	3,5	6,2	7,6	6,0	0,1	11,6	11,3	10,6	2,6	.	13,8	14,8	14,5	6,8	4,1	4,1	6,1	13,6	5,4	2,6	7,8	.	4,4	7,4	203,0
11	Nadostowo	7,9	6,1	3,4	9,3	5,2	5,7	4,5	3,9	4,9	8,8	4,5	0,5	10,4	10,2	11,1	0,1	.	13,4	14,5	14,4	5,1	5,8	2,4	6,4	13,5	3,4	2,8	6,2	.	3,1	6,8	194,3
12	Prabuty	6,7	8,4	2,5	8,2	2,9	6,3	3,6	.	8,5	8,6	4,0	0,8	11,4	12,2	10,8	5,0	.	12,5	13,9	15,2	6,1	3,4	6,1	6,1	14,8	6,6	1,3	4,9	.	4,0	8,0	202,8
13	Bydgoszcz, IMiUZ	6,6	7,2	3,0	7,7	4,0	6,2	1,4	2,3	6,8	8,7	5,7	0,5	6,7	11,2	7,4	3,7	1,4	5,9	13,8	14,0	1,8	6,9	3,9	8,5	10,2	7,4	1,1	3,7	0,1	2,5	6,2	176,5
14	Suwałki	4,2	12,0	6,1	8,7	6,2	9,7	8,3	5,3	8,6	5,9	5,8	9,1	13,2	12,7	13,7	7,8	0,3	14,9	14,5	10,8	13,1	1,0	9,3	7,2	13,9	11,3	0,7	6,2	1,2	3,6	6,0	251,3
15	Mikołajki	4,3	9,3	3,0	6,9	6,2	8,5	6,3	5,1	9,5	7,7	8,6	7,8	14,2	14,3	8,5	9,9	0,2	10,5	15,5	14,7	12,4	.	6,6	7,1	14,7	11,5	0,8	6,2	0,1	3,2	7,9	241,3
16	Biebrza	3,0	10,8	4,3	8,9	5,6	8,0	6,0	6,5	9,7	9,7	7,6	9,5	13,5	12,7	12,5	9,8	0,8	9,2	12,1	12,6	13,7	0,1	8,4	7,6	13,8	10,6	0,7	5,3	0,2	2,2	9,1	244,5
17	Białystok	4,5	10,4	4,9	7,2	2,4	9,1	3,6	6,3	8,5	10,5	7,0	10,9	11,8	12,5	14,0	13,1	3,6	7,6	13,5	14,2	12,5	0,5	5,3	9,1	9,8	8,5	1,6	5,4	0,4	3,8	6,5	239,0
18	Goraów Wlkp.	8,8	6,1	6,5	6,0	7,1	5,2	2,2	0,4	3,1	4,8	4,4	0,9	5,7	11,5	5,4	4,6	.	6,2	11,4	13,8	5,8	10,5	3,5	11,4	8,4	6,8	0,7	0,8	0,2	2,7	0,9	165,8
19	Przebędowo	7,2	9,1	8,5	11,9	4,6	6,8	2,5	0,0	5,4	4,2	7,6	0,0	7,9	13,4	9,6	7,9	0,1	.	14,4	14,5	4,6	9,5	5,1	10,8	13,4	10,8	0,7	1,3	0,5	4,5	0,8	197,6
20	Przybroda	8,7	10,0	8,5	9,8	5,6	6,5	2,5	.	5,2	5,3	8,0	.	8,6	13,0	6,8	9,0	0,1	.	14,7	14,2	3,3	10,8	4,4	10,9	13,3	10,3	0,7	1,1	0,2	5,6	0,3	197,4
21	Poznań-Zawica	5,7	7,9	6,9	8,9	5,7	4,6	3,6	0,0	4,7	2,9	7,7	0,0	4,6	10,9	7,8	6,9	0,6	0,1	12,0	11,5	4,0	10,3	4,7	9,0	11,3	9,3	1,3	1,5	0,2	5,0	0,0	169,6
22	Flewicka	7,1	8,6	8,4	9,8	6,0	7,2	2,7	0,1	5,4	3,4	8,0	0,5	7,2	12,1	8,6	7,3	0,5	.	14,1	13,9	3,5	12,3	5,2	10,4	12,7	10,5	1,1	1,4	0,6	6,1	0,0	194,7
23	Kórnik	6,3	11,5	7,1	9,0	7,0	7,9	2,0	.	6,2	3,7	7,7	1,0	5,9	11,9	11,1	8,4	0,7	.	13,2	14,6	3,4	11,8	4,1	11,6	11,8	11,8	2,0	0,6	0,5	5,7	0,8	199,3
24	Oborniki Śl.	.	10,4	.	6,9	5,8	3,1	2,2	.	8,5	.	9,1	.	1,3	12,2	7,0	5,5	.	.	8,1	5,9	6,5	7,5	1,3	8,2	11,2	12,1	2,8	.	4,7	3,8	.	144,1
25	Laskowice Oławskie	.	5,4	1,4	3,6	3,9	4,1	3,5	0,4	6,2	4,8	7,1	0,3	6,7	13,3	10,2	6,1	1,4	.	2,2	4,7	2,5	11,5	3,4	8,5	6,4	5,5	2,1	0,1	1,9	6,1	1,6	134,9
26	Ciechocinek	6,2	9,3	5,5	12,0	5,5	6,9	1,4	1,3	7,8	7,3	7,4	0,9	10,6	11,5	.	.	.	3,6	14,5	15,2	5,2	2,0	4,1	9,5	11,7	9,8	0,7	4,6	0,6	2,9	2,7	180,7
27	Więcławice	6,9	10,1	8,9	10,9	6,7	.	1,5	1,1	7,0	8,0	8,2	0,5	10,0	11,7	11,7	7,9	4,5	2,0	14,0	14,0	3,5	9,8	4,1	10,8	12,6	10,1	0,4	6,2	0,8	2,6	2,0	208,5
28	Legionowo	3,8	12,8	6,1	7,9	4,2	9,0	2,2	3,0	9,7	7,6	8,7	5,0	10,4	12,4	9,9	11,3	4,2	1,5	14,2	14,2	11,6	7,2	5,3	11,0	10,7	9,5	0,9	5,7	0,8	5,0	6,0	231,8
29	Warszawa-Bielany	2,6	11,9	6,4	8,6	4,1	10,8	2,2	5,8	8,9	3,1	10,3	6,1	7,8	13,6	10,9	13,4	4,1	0,4	14,5	15,3	11,8	7,7	5,8	12,3	12,4	10,1	1,1	6,2	1,2	4,4	3,5	243,3
30	Warszawa, Min.Kom.	3,3	10,5	5,1	6,1	3,3	8,9	0,8	3,3	6,4	7,7	10,0	4,9	8,5	12,8	10,3	11,9	4,7	0,5	13,5	13,5	10,0	7,4	4,0	11,1	11,0	7,5	0,9	.	7,1	4,0	4,3	213,3
31	Międzylesie	3,8	12,1	4,9	4,1	7,8	9,6	1,3	5,7	7,4	8,5	6,6	8,4	10,0	13,5	12,4	12,7	5,0	0,8	14,2	14,4	11,4	7,7	5,7	12,3	11,6	7,3	2,1	6,6	0,4	3,8	4,5	236,6
32	Brwinów	2,4	12,2	4,3	8,2	2,6	8,5	1,0	1,9	6,2	5,9	10,7	4,9	8,7	14,0	8,7	13,0	3,5	.	15,6	15,1	10,7	8,9	3,2	11,8	9,0	5,7	0,7	3,5	0,4	3,7	2,0	207,0
33	Świder	3,8	11,6	4,7	5,1	5,4	8,2	2,3	5,0	6,7	7,4	8,6	7,6	10,0	12,8	12,1	12,2	3,9	0,2	12,9	13,4	10,0	6,9	6,2	10,4	9,5	7,1	1,3	6,3	0,5	4,3	4,3	220,7
34	Topola-Błonie	2,5	10,7	3,5	8,9	4,3	7,0	0,9	2,3	7,4	6,3	9,5	2,5	8,2	12,9	5,9	12,1	3,1	0,1	14,2	14,6	4,7	10,4	2,0	9,0	9,1	10,9	1,7	3,4	1,0	4,8	2,1	196,0
35	Młochów	2,2	11,1	3,1	5,8	2,4	8,5	0,6	3,0	5,9	7,8	9,0	4,9	8,0	13,4	9,9	13,8	5,4	.	15,0	13,6	11,1	7,0	3,4	11,1	8,9	5,8	1,3	3,9	0,4	3,9	2,6	202,8
36	Skierniewice	5,2	9,8	2,4	7,1	4,3	9,2	1,2	2,3	6,4	7,1	11,2	6,0	8,6	12,9	10,4	13,1	3,2	0,3	14,3	13,4	6,5	9,9	4,7	10,7	10,9	8,1	2,0	5,5	1,3	5,6	3,4	217,0
37	Belsk	2,2	10,5	1,5	5,6	2,8	8,7	2,2	4,2	6,6	8,5	10,6	6,5	10,0	12,1	11,0	13,3	4,8	0,4	13,6	12,8	9,5	8,6	4,2	10,7	9,9	6,1	3,4	6,2	2,3	4,9	1,8	215,5
38	Łódź-Lublinek	1,3	9,0	0,5	5,0	2,8	5,7	0,2	1,0	5,3	5,4	9,5	2,9	6,6	11,3	7,9	11,9	2,2	.	13,4	12,9	5,0	9,3	1,6	10,9	8,1	6,5	1,1	1,6	2,4	5,0	1,7	168,0
39	Kalisz	2,7	10,4	4,3	7,9	8,0	5,2	0,7	0,2	5,5	2,5	9,8	1,1	6,6	13,2	10,4	9,9	0,6	.	11,7	13,8	1,4	11,2	3,6	9,9	9,5	12,4	2,4	1,8	2,3	6,2	2,3	187,3
40	Wieluń	0,2	6,7	0,2	4,5	2,5	6,1	1,8	1,6	6,4	5,6	7,8	1,9	8,5	13,3	13,2	11,3	3,0	.	10,3	14,3	3,2	13,2	4,2	9,6	9,1	6,9	2,3	.	2,8	4,2	1,7	176,4
41	Szepietowo	5,3	12,8	5,4	8,6	6,7	10,1	4,3	5,4	8,8	10,0	2,1	12,2	13,3	13,3	14,0	6,7	14,3	6,3	14,6	14,9	12,4	.	6,5	7,5	11,4	9,4	0,9	11,1	1,4	4,0	7,7	261,4
42	Białowieża	5,3	11,8	3,8	7,1	2,5	9,7	5,4	4,5	11,0	11,9	7,6	12,7	11,5	13,2	13,9	12,9	6,9	6,3	12,2	11,3	14,0	3,2	3,6	11,1	9,3	5,9	4,1	5,8	0,7	2,6	6,1	247,9
43	Terespol	5,0	8,9	4,4	6,7	2,0	9,7	4,4	6,6	8,1	10,9	9,9	11,9	9,5	13,1	12,8	11,9	11,8	0,2	13,0	13,0	12,9	1,6	8,1	9,7	7,8	3,2	3,7	8,3	0,5	4,5	4,4	238,5
44	Sobieszyn	3,7	9,2	3,8	5,8	1,0	9,5	3,7	7,4	6,6	9,0	9,9	10,2	12,1	13,5	14,3	13,7	5,8	0,9	13,6	14,1	10,8	4,4	5,1	9,6	8,1	3,4	2,2	5,3	2,5	4,4	1,0	224,6
45	Puławy	2,8	5,8	0,3	4,5	1,0	8,5	2,3	5,8	5,1	7,6	5,2	7,5	9,8	13,3	13,4	12,4	5,4	1,1	11,4	13,5	6,7	5,1	3,2	7,3	7,4	1,4	2,3	2,6	1,1	3,8	0,7	178,3
46	Chełm	5,9	1,4	2,9	7,3	0,9	11,3	5,6	8,5	6,6	8,0	10,0	12,2	9,5	13,1	13,9	12,5	8,9	0,6	12,5	13,9	11,9	4,0	4,4	11,1	6,4	1,1	2,3	2,3	6,1	3,2	0,5	218,8
47	Szczawno-Zdrój	0,2	6,8	1,6	3,7	1,4	3,6	3,9	.	5,6	3,5	4,0	0,6	7,0	13,1	5,9	3,1	2,0	.	2,3	4,7	3,6	10,4	5,8	13,0	5,3	8,7	2,0	.	1,5	7,6	3,3	136,2
48	Śnieżka	0,8	5,6	1,2	2,1	2,8	0,1	1,8	.	4,8	1,3	2,9	.	10,2	14,3	3,7	3,0	0,5	.	0,5	0,5	0,1	9,8	4,9	8,1	3,3	9,4	1,0	0,1	0,6	1,9	0,6	95,9
49	Opole	0,1	3,8	0,1	2,1	4,8	3,0	3,3	2,6	7,1	5,1	9,3	0,9	8,1	12,5	10,0	5,8	1,0	.	7,2	6,8	5,6	9,9	5,7	8,5	7,2	4,0	.	0,0	4,1	5,4	2,9	146,9
50	Kudowa-Zdrój	1,2	6,1	1,9	0,4	1,8	1,1	6,6	0,8	4,2	3,9	7,3	1,5	9,2	13,2	9,0	3,8	5,4	1,5	.	1,5	1,6	9,9	6,1	8,9	7,2	7,5	2,9	.	3,8	5,2	4,5	138,0
51	Polanica-Zdrój	0,3	5,6	1,5	0,3	1,3	2,3	5,6	2,1	7,9	4,7	7,0	1,9	10,2	12,9	9,2	3,8	3,1	.	2,3	2,1	1,9	11,5	6,6	7,2	4,5	8,7	3,9	.	4,6	7,4	5,6	145,8
52	Skroniów	3,8	2,0	.	4,1	0,7	5,8	1,7	4,7	5,6	5,0	7,8	6,1	8,8	12,0	12,0	12,1	3,5	0,0	8,5	11,0	2,3	10,5	5,3	5,3	6,4	0,4	6,0	1,2	0,8	4,3	1,3	169,0
53	Świerklaniec	1,9	3,0	.	3,3	.	4,6	3,8	4,5	6,8	5,3	6,6	3,4	6,8	10,2	9,5	8,2	0,4	.	3,4	9,2	1,4	9,9	3,4	4,8	6,8	1,7	4,8	.	7,1	5,2	3,0	139,0
54	Kraków, Obs.Astr.UJ	5,7	0,2	1,7	1,7	.	7,3	4,0	6,7	6,2	8,1	4,0	6,1	3,4	12,6	12,8	9,0	2,7	.	4,6	7,9	1,9	11,4	4,8	7,5	5,8	.	3,0	0,4	10,2	4,6	1,9	156,0
55	Cieszyn	4,8	1,7	1,3	1,4	0,4	3,9	9,4	4,9	6,0	7,7	5,7	6,1	6,3	13,5	11,3	4,5	2,4	.	2,8	1,6	1,4	13,3	2,9	6,1	2,3	.	1,5	0,1	6,9	0,7	2,3	133,2
56	Istebna-Kubalonka	4,4	0,1	0,5	0,4	0,8	3,1	11,8	6,2	4,8	5,3	6,1	5,5	7,6	11,4	8,6	6,3	5,4	.	3,3	3,0	2,1	6,5	2,3	7,2	3,5	0,1	2,2	0,7	10,1	0,1	3,2	132,6
57	Rabka	6,0	.	2,5	2,3	0,2	3,6	8,0	6,6	5,9	6,8	4,0	6,5	4,2	13,3	13,2	8,7	4,6	.	0,8	3,9	2,7	9,7	5,6	10,2	2,7	.	1,5	1,1	10,6	2,2	1,0	148,4
58	Jabłonka	6,1	.	3,6	0,1	.	5,4	7,5	8,1	9,5	7,2	4,6	5,7	6,0	10,7	11,2	9,1	4,3	0,2	0,8	2,0	2,4	11,4	4,7	9,7	2,2	.	3,6	1,2	10,2	2,7	1,2	151,4
59	Krynica	6,8	.	4,8	1,8	0,2	6,8	5,7	7,5	5,9	5,7	7,1	7,1	1,1	11,9	12,5	9,3	5,5	2,8	2,3	7,5	2,8	8,1	4,0	10,2	4,8	.	2,5	3,4	9,2	0,6	0,5	158,2
60	Krynica-Góra Park	8,0	.	4,5	3,1	.	6,7	5,4	8,1	6,4	6,5	7,9	7,7	.	12,3	13,3	10,5	6,8	2,8	2,2	8,3	3,4	7,2	2,2	10,4	5,2	0,1	3,0	2,6	9,1	0,6	0,5	164,5
61	Muszyna	7,4	.	4,8	2,5	0,0	6,7	6,0	7,9	4,7	4,5	5,6	6,6	1,4	9,6	8,2	9,1	5,3	4,3	2,1	5,0	3,3	8,9	2,1	9,4	6,5	0,1	0,7	2,7	8,7	0,3	0,1	144,5
62	Zakopane	7,5	.	4,2	1,0	0,6	6,2	11,8	6,5	4,5	4,0	3,1	6,9	3,4	13,1	13,0	5,7	3,6	1,4	0,0	0,4	1,3	7,3	3,6	9,6	2,2	.	2,6	1,5	10,0	2,7	0,9	136,6
63	Gubałówka	7,8	.	5,7	1,7	.	7,0	10,5	7,6	4,5	5,5	3,2	7,2	4,8	11,2	11,0	6,3	4,1	1,2	0,9	0,4	2,4	8,0	4,4	10,2	2,8	.	3,3	2,9	10,8	3,0	0,2	148,6
64	Hala Gąsienicowa	6,8	.	3,7	1,3	.	4,6	11,1	5,5	2,7	4,0	1,3	7,5	1,3	8,9	8,6	4,4	3,8	1,1	.	0,1	1,6	4,4	2,9	9,0	3,3	.	1,1	0,5	7,8	1,6	.	108,9
65	Kasprowy Wierch	7,7	.	4,6	1,8	0,1	3,0	7,2	6,2	4,4	3,7	1,7	7,4	2,9	10,8	10,8	5,9	3,6	1,8	0,1	0,4	0,5	6,0	1,3	10,4	3,5	.	2,5	0,4	9,1	1,3	1,1	120,2
66	Werbkowice	6,8	0,2	6,0	7,2	.	10,0	8,3	10,4	3,6	10,8	8,6	12,5	8,8	13,9	14,2	12,3	7,8	0,2	12,5	14,1	12,0	4,4	6,6	10,6	1,4	1,4	0,8	5,4	8,9	2,9	0,7	223,3
67	Zamość	5,0	0,8	5,9	.	0,2	8,0	2,8	7,5	5,3	7,5	6,2	7,9	9,9	13,5	9,5	13,1	7,2	2,3	11,4	12,5	6,4	6,8	13,7	7,4	8,1	.	2,8	1,6	6,4	3,4	0,6	193,7
68	Tomaszów-Zdrój	9,1	.	0,6	4,3	.	6,9	6,9	11,5	5,4	6,7	9,6	10,5	2,9	13,2	13,5	11,5	8,7	7,2	4,1	11,8	4,5	8,4	5,6	11,0	3,9	0,2	1,9	2,2	11,3	0,5	.	191,3
69	Leśko	8,9	.	5,5	5,0	.	6,2	5,8	11,4	2,1	7,6	4,8	9,6	3,3	13,6	13,9	12,5	6,5	1,4	5,1	12,0	4,2	5,5	6,2	10,6	7,1	0,0	0,6	1,8	9,7	0,9	0,7	182,5

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	8,8	14,0	13,8	7,0	5,3	6,5	0,1	0,0	5,1	11,7	9,1	6,2	10,0	1,5	2,6	11,5	13,7	13,8	12,5	3,7	4,3	9,6	11,6	1,1	.	6,4	2,9	2,1	3,9	7,1	7,1	215,0
2	Kołobrzeg	7,5	12,1	11,4	4,1	11,1	4,9	.	.	6,2	10,6	11,7	10,5	10,9	5,9	12,5	12,4	13,1	12,9	9,0	4,1	3,2	8,0	7,7	3,4	.	9,2	8,1	12,7	1,6	7,0	6,0	237,8
3	Świnoujście	8,2	7,7	7,5	1,9	9,3	4,1	.	.	4,6	9,6	7,1	11,4	10,7	11,5	1,6	6,5	11,6	13,5	10,3	5,1	4,0	6,9	1,2	5,1	0,1	10,1	7,6	11,1	1,7	8,2	6,0	204,2
4	Resko	8,9	7,5	10,5	2,5	12,2	6,7	.	0,0	6,3	11,1	8,5	9,8	8,7	7,9	9,0	12,0	9,6	10,6	7,7	6,5	4,3	9,2	6,4	2,9	.	6,5	8,4	9,9	1,6	8,1	4,4	217,7
5	Szczecinek	11,3	8,8	9,4	3,5	12,9	8,3	.	0,9	3,2	8,8	7,8	4,3	10,2	4,4	2,6	10,1	11,7	11,8	10,2	8,7	6,7	10,6	10,0	0,0	.	4,6	5,0	10,4	4,5	7,8	7,8	216,5
6	Chojnice	12,7	7,3	7,6	2,4	12,5	6,8	0,1	0,5	2,6	6,2	2,6	4,2	8,7	0,2	2,5	9,2	10,8	11,1	10,8	6,4	6,3	11,6	10,4	2,4	.	5,3	1,2	7,6	6,9	8,8	8,3	194,0
7	Hel	9,7	6,1	10,8	8,0	6,7	5,9	0,3	1,4	.	10,5	9,4	7,5	3,7	1,8	6,9	3,5	12,0	8,2	10,6	2,3	3,9	7,4	10,5	1,2	.	.	.	1,0	7,8	9,5	10,2	176,8
8	Gdynia	9,5	7,7	10,0	6,2	6,5	7,2	0,7	1,1	.	11,4	7,6	8,7	1,7	0,6	7,5	1,3	13,1	11,9	11,3	4,7	3,6	9,9	11,6	0,6	.	1,0	.	2,7	6,7	8,8	8,0	181,8
9	Świbno	-	-	-	3,7	2,6	7,1	0,1	1,7	.	7,1	10,9	9,7	3,7	1,9	7,4	3,7	13,1	9,2	10,1	4,2	4,5	10,1	11,8	2,3	.	.	.	.	6,9	9,4	10,4	-
10	Stare Pole	12,5	6,0	8,8	0,7	4,3	8,2	.	0,2	0,1	9,0	7,5	8,2	5,0	2,4	7,3	5,7	12,7	8,8	10,7	4,9	7,3	9,3	12,2	1,6	.	.	.	.	6,4	8,4	10,2	178,4
11	Kadcstowo	11,3	7,0	7,7	1,8	5,1	7,6	0,2	0,3	0,1	6,6	3,1	5,6	4,8	.	4,9	6,2	12,6	7,6	9,6	4,1	7,2	10,0	11,0	3,3	.	.	.	0,2	7,6	9,1	8,7	163,3
12	Frombork	12,8	3,5	7,4	1,1	5,5	7,7	0,2	.	.	7,5	1,3	5,7	3,8	0,1	3,8	7,2	13,0	12,6	11,6	8,6	8,7	11,0	12,9	1,9	.	.	.	0,1	5,9	9,6	8,1	171,6
13	Bydgoszcz, IMiGW	10,4	5,8	8,0	0,4	12,8	7,1	4,9	.	0,6	6,4	3,9	1,2	9,5	0,4	4,7	8,4	10,7	10,7	10,1	5,3	6,4	10,4	9,3	2,5	.	7,0	0,1	4,7	6,9	8,6	11,0	188,2
14	Suwałki	10,2	.	11,1	8,1	4,3	10,2	2,2	3,8	1,7	7,9	3,3	10,1	5,3	1,8	6,4	2,1	7,7	11,9	11,6	12,0	12,3	11,4	12,7	8,9	8,6	1,2	2,1	.	1,6	6,1	9,6	201,5
15	Mikołajki	11,2	.	11,0	2,6	7,0	10,0	2,9	1,9	0,3	8,3	4,4	7,0	5,8	3,6	6,7	5,0	12,2	10,6	12,2	7,8	11,9	11,9	12,8	4,1	4,5	.	.	0,3	3,7	6,6	10,1	196,4
16	Biebrza	7,9	.	10,0	3,9	9,5	9,9	5,8	8,7	0,7	6,9	3,0	9,9	5,8	2,2	5,3	3,5	8,4	10,9	8,4	10,9	11,4	11,3	12,4	7,7	5,3	.	0,1	.	3,2	8,3	7,3	198,6
17	Białystok	6,9	.	7,2	3,5	5,6	9,5	7,8	8,4	4,7	7,1	1,0	9,1	6,2	4,5	3,8	3,0	10,4	8,8	9,8	7,8	10,0	11,1	12,3	9,0	8,6	1,1	0,2	.	6,3	7,1	9,9	196,7
18	Gorzów Wlkp.	12,5	8,5	4,9	5,7	9,8	7,8	1,8	0,2	3,7	9,2	3,7	8,7	9,5	10,3	3,6	10,0	13,0	11,7	9,9	7,3	6,0	10,6	5,1	2,2	.	8,9	7,7	6,2	1,8	7,4	5,1	212,8
19	Przebędowo	10,2	7,4	8,8	2,6	11,9	8,7	6,7	1,5	3,1	8,2	4,8	6,9	7,8	7,2	3,1	6,8	12,8	11,7	11,2	11,5	5,6	7,7	7,2	.	.	3,2	.	1,1	4,2	1,9	3,3	187,1
20	Przybroda	11,1	9,4	8,6	5,2	9,9	8,9	6,6	0,6	5,2	8,5	7,0	9,1	9,2	8,5	4,4	5,5	13,6	12,6	11,4	11,7	7,8	12,4	10,3	0,2	.	5,8	4,2	5,7	4,7	7,6	9,7	233,4
21	Poznań Ławica	9,1	7,0	7,0	4,5	9,0	9,1	6,0	2,0	4,4	7,2	6,1	7,7	7,2	7,5	3,0	3,8	11,4	10,5	10,8	10,4	7,1	11,0	8,6	0,1	.	4,1	3,4	2,4	3,5	6,5	9,2	199,6
22	Kiewisko	10,6	7,6	8,1	5,1	8,5	8,4	5,3	1,1	3,7	7,9	5,6	8,3	8,6	8,8	2,8	3,6	12,0	12,0	11,2	11,0	7,4	11,1	9,6	.	.	4,7	3,4	6,3	3,7	7,2	8,3	211,9
23	Kórnik	11,1	8,1	9,3	5,4	11,6	9,1	7,1	2,3	2,8	5,8	7,1	8,6	6,7	6,6	2,4	3,2	13,7	12,9	12,3	12,7	8,9	12,9	10,6	.	.	3,1	2,6	5,7	4,0	5,7	5,4	217,9
24	Oborniki Śl.	9,3	0,9	9,1	6,6	12,3	7,0	0,6	11,3	1,2	5,8	11,4	1,5	11,0	7,8	3,5	6,1	11,4	9,6	11,6	11,8	9,3	10,2	4,4	.	.	3,5	5,8	2,4	8,5	6,9	6,8	208,0
25	Leszkowice Olszewki	6,8	3,6	6,6	3,9	8,9	8,3	10,6	9,7	0,0	6,0	5,6	10,1	8,1	7,1	1,1	8,0	9,7	9,6	10,8	11,1	8,9	11,7	9,1	.	0,0	3,4	2,7	4,3	3,8	7,3	6,3	205,1
26	Ciechocinek	10,8	3,9	10,4	1,1	12,8	9,6	6,4	1,0	0,1	7,2	2,2	3,5	7,4	0,1	3,0	10,6	8,3	11,9	10,8	10,3	7,7	11,6	11,3	3,2	.	.	.	8,0	8,0	7,2	12,1	200,3
27	Więcławice	10,2	5,6	8,8	1,7	10,7	9,9	6,6	0,5	0,9	9,6	1,7	2,7	9,2	1,4	3,3	9,2	12,2	11,1	11,0	8,8	6,5	11,0	9,1	3,5	.	0,6	.	9,9	8,1	7,9	9,3	201,0
28	Legionowo	7,7	0,0	10,7	4,6	10,1	9,2	8,7	7,5	0,8	7,7	4,0	5,2	5,8	2,1	4,6	3,8	9,5	9,7	10,2	10,4	9,6	9,7	10,1	4,1	3,9	.	.	10,1	8,2	6,4	9,2	205,6
29	Warszawa-Bielany	7,4	0,1	13,2	4,2	11,8	12,1	9,5	7,0	1,8	9,9	3,4	5,4	7,9	1,8	2,7	8,2	6,4	10,9	12,2	12,1	10,7	10,2	11,3	3,7	4,2	.	.	8,9	9,5	4,1	7,8	218,4
30	Warszawa, Min.Kom.	6,3	.	12,0	4,0	11,7	10,9	8,7	6,9	2,6	7,5	2,3	11,0	.	.	8,9	8,6	7,3	11,2	11,6	12,2	10,7	9,8	10,9	3,6	0,9	.	.	6,4	5,4	5,0	4,8	201,2
31	Międzylesie	6,6	0,6	12,4	4,4	10,4	11,1	10,2	(8,0)	1,1	9,1	1,9	3,8	6,7	0,6	2,0	11,3	9,4	9,6	11,6	11,6	10,5	(10,4)	9,5	3,4	4,3	.	0,2	8,9	6,2	6,0	9,7	(211,5)
32	Rzeszów	2,9	.	9,2	2,6	10,2	11,9	9,1	6,2	1,3	7,2	3,2	4,6	6,7	0,8	1,9	12,0	9,5	11,8	11,5	12,3	12,7	10,7	9,7	3,3	3,4	.	.	11,4	7,0	6,4	11,0	210,5
33	Świder	5,1	.	11,2	3,6	10,9	11,4	9,5	7,6	2,8	7,2	1,6	2,9	8,3	1,0	1,3	9,4	8,5	9,7	12,0	11,7	10,5	10,0	11,5	2,9	3,8	.	.	10,1	8,0	5,7	10,0	209,2
34	Topolę-Błonie	6,5	2,3	9,6	1,6	10,7	10,1	9,8	4,8	.	7,5	2,7	4,7	8,8	0,3	3,6	11,2	10,0	12,5	10,6	11,0	9,8	10,4	7,2	2,2	.	.	.	10,2	6,7	5,6	10,9	203,3
35	Młochów	4,8	.	11,7	2,7	9,4	10,6	9,1	7,6	0,0	8,1	2,5	4,6	6,5	0,7	2,0	8,3	9,6	10,5	12,8	12,0	10,3	10,9	11,2	3,3	4,1	.	.	10,2	7,1	4,1	9,1	205,8
36	Skierniewice	6,4	0,2	10,1	3,7	11,1	9,4	10,2	6,2	.	7,4	3,1	3,6	5,4	1,3	4,1	10,7	11,5	11,6	12,8	12,0	8,5	11,6	9,1	1,4	2,0	.	.	9,2	6,7	6,3	10,4	206,0
37	Belsk	6,6	.	11,2	2,5	10,7	9,4	9,4	8,7	3,1	6,5	1,0	4,7	9,6	0,3	3,3	9,5	8,7	9,2	12,5	12,4	10,8	10,4	11,1	3,7	3,4	.	.	10,3	9,1	6,5	11,2	218,0
38	Łódź-Lublinek	5,5	2,2	9,0	2,9	9,9	11,3	9,1	8,0	.	5,7	2,2	6,0	7,3	2,5	1,0	6,1	11,1	12,3	12,1	12,4	9,9	11,3	4,1	1,0	.	.	.	9,9	8,8	2,2	7,2	191,6
39	Kalisz	10,9	4,5	9,2	3,8	11,3	8,9	10,7	7,6	.	5,8	5,5	7,0	9,1	7,6	0,2	5,5	12,5	11,9	11,5	11,9	9,7	12,0	9,9	2,4	.	2,4	0,8	9,8	7,7	6,8	10,7	227,6
40	Wieluń	7,7	3,3	10,1	4,4	8,2	11,6	10,2	9,0	.	6,3	3,6	8,5	7,3	6,6	0,8	3,3	10,4	13,3	12,8	13,0	9,8	12,7	9,0	2,3	.	.	.	6,4	6,8	4,7	11,5	213,6
41	Kozieletowo	.	.	10,8	2,4	9,5	10,8	10,0	7,5	4,3	6,1	.	7,6	5,6	2,2	4,0	6,2	12,3	10,6	11,9	11,6	10,8	10,6	12,6	9,8	4,1	.	.	1,9	9,3	6,1	9,0	207,6
42	Białowieża	7,6	.	8,6	4,3	5,2	11,7	9,3	9,3	6,8	5,9	0,7	6,1	7,0	3,6	1,9	4,7	10,6	12,3	10,6	9,4	11,7	9,4	11,9	11,1	6,6	3,5	2,2	0,3	6,2	2,3	8,3	209,3
43	Terespol	8,4	.	8,5	4,3	7,2	12,4	6,9	12,7	10,5	7,3	0,1	4,2	7,2	4,2	4,1	3,7	10,6	11,6	11,7	11,1	11,4	11,3	11,9	10,1	3,8	3,2	0,3	2,1	7,0	2,8	10,7	221,3
44	Sobieszyn	9,8	0,1	11,6	3,9	8,4	10,8	9,8	12,7	7,4	4,3	0,1	4,3	5,4	1,7	3,1	8,1	9,3	9,8	12,5	12,6	11,8	11,1	12,4	6,3	0,1	.	.	7,3	8,5	6,8	9,5	220,1
45	Puławy	7,0	0,4	9,1	2,4	5,2	9,2	8,6	12,0	3,6	2,8	0,1	2,6	4,4	0,9	1,7	9,5	11,2	8,6	10,8	11,2	9,7	9,8	11,2	4,3	0,2	.	.	8,1	6,9	5,4	10,4	187,3
46	Chełm	7,1	.	12,0	3,2	9,6	9,6	7,6	13,4	8,6	.	.	1,0	4,8	1,8	1,9	8,9	10,1	12,4	9,8	12,6	12,2	11,2	12,6	10,0	5,4	.	.	7,3	8,8	3,9	9,4	215,2
47	Szczawno-Zdrój	3,6	6,0	3,3	5,2	10,0	7,8	11,5	7,2	.	4,4	6,6	7,9	7,3	5,8	7,2	6,0	4,2	8,4	10,9	11,3	8,3	10,7	5,9	.	.	4,8	3,7	.	4,5	5,6	6,0	186,1
48	Śnieżka	3,7	4,8	2,3	4,6	9,0	6,3	7,7	6,4	0,1	4,0	3,8	7,4	8,7	7,3	4,1	3,5	3,8	9,6	9,5	11,9	9,2	10,1	6,1	.	.	5,0	7,7	2,3	2,8	6,8	9,5	177,2
49	Opole	7,0	3,3	5,4	5,0	8,1	9,7	8,2	9,1	0,2	.	3,8	10,9	8,6	9,0	.	8,0	8,7	10,3	9,8	9,8	9,7	11,2	9,7	1,9	.	2,3	2,1	4,9	3,7	6,1	6,9	195,2
50	Kudowa-Zdrój	7,2	5,4	3,9	2,5	10,1	9,1	11,4	11,3	.	4,5	9,1	9,6	11,4	6,7	7,4	7,8	7,7	8,6	9,5	10,8	7,8	7,7	7,5	0,1	.	4,3	3,5	3,4	3,6	4,8	7,2	200,9
51	Polanica-Zdrój	3,5	4,5	3,5	6,0	10,7	8,7	10,6	10,3	.	.	8,4	8,3	8,9	6,7	6,8	6,8	4,3	10,0	9,1	9,8	6,9	11,7	7,9	.	.	3,3	2,6	.	5,2	7,1	5,2	186,8
52	Skroniów	7,5	0,3	9,6	1,9	10,5	10,6	9,1	11,9	2,2	.	.	6,8	4,9	4,5	1,7	6,5	9,8	10,0	11,4	11,9	8,0	10,2	6,6	1,7	0,6	.	.	3,5	6,1	6,0	9,2	183,0
53	Świerklaniec	7,4	1,7	8,0	4,1	9,4	10,1	9,4	9,5	0,2	.	0,9	9,2	7,8	6,6	1,9	2,5	5,8	9,6	9,0	9,2	10,9	11,0	9,5	1,6	0,0	.	0,1	7,2	3,7	5,5	10,1	181,9
54	Kraków, Obs.Astr.UJ	6,0	0,4	6,6	2,7	8,2	11,4	9,0	11,7	1,0	.	.	6,9	5,7	4,6	3,1	7,1	7,4	10,5	8,3	11,0	8,9	11,0	1,3	3,2	0,1	.	.	7,2	7,9	3,8	8,0	173,0
55	Cieszyn	3,6	0,6	3,5	2,3	5,1	11,4	11,1	11,0	.	.	.	8,1	6,2	10,5	3,8	10,7	3,2	11,8	10,2	10,2	10,2	12,9	7,1	0,9	.	.	0,5	6,4	7,1	3,5	8,4	180,3
56	Istebna-Kubalonka	0,0	1,3	6,8	4,2	7,3	11,9	10,6	11,7	.	.	.	5,4	5,5	9,7	5,0	7,8	5,2	10,1	11,3	11,0	11,7	11,8	4,4	0,6	0,1	.	0,2	5,3	5,7	5,6	8,3	178,5
57	Rabka	1,6	0,2	6,7	4,4	6,6	11,7	10,7	12,5	.	.	.	3,2	5,0	4,7	2,0	6,5	8,2	10,8	9,5	11,0	11,5	11,5	1,8	2,8	.	.	.	3,2	4,9	3,8	9,2	164,0
58	Jabłonka	5,0	0,9	8,4	5,9	7,8	9,2	11,1	12,3	0,2	.	.	5,8	4,1	7,5	3,7	6,9	7,4	8,7	8,4	8,5	10,0	11,2	5,1	2,3	0,0	.	.	4,3	5,5	5,1	7,5	172,8
59	Krynica	0,0	0,1	5,6	3,8	9,3	10,7	11,1	11,9	1,0	.	.	2,7	5,0	3,8	3,9	2,7	4,1	9,7	9,7	10,3	7,3	10,8	7,5	3,8	0,2	.	.	1,2	3,9	3,0	5,4	148,7
60	Krynica-Góra Park.	.	0,2	6,3	4,2	9,8	11,8	13,2	12,1	.	.	3,9	4,8	.	5,1	3,8	3,1	4,5	10,3	10,5	11,6	9,3	10,7	7,8	3,6	0,2	.	.	0,3	4,0	2,0	3,5	156,6
61	Muszyna	0,1	.	4,8	4,8	8,0	10,6	11,1	12,3	1,4	.	.	2,1	2,9	4,3	3,4	4,7	5,7	8,5	5,4	8,9	9,8	10,2	7,2	4,4	0,2	.	.	1,5	3,1	3,0	6,5	144,9
62	Zakopane	0,3	0,1	5,4	4,4	4,1	12,8	11,8	13,6	0,2	.	.	1,5	1,0	5,4	3,0	1,7	6,4	12,5	9,8	6,9	12,8	12,3	5,4	1,4	.	.	0,1	2,0	2,6	2,5	8,7	148,7
63	Gubałówka	1,1	0,1	6,0	4,5	4,8	10,3	9,0	11,0	0,6	.	.	1,0	1,8	6,6	2,0	2,7	6,8	9,6	7,5	6,6	10,1	9,9	4,3	1,8	.	.	.	3,4	3,5	3,4	7,9	136,5
64	Hala Gąsienicowa	0,9	.	5,6	2,4	2,6	11,3	9,8	11,5	6,4	.	.	.	0,1	3,0	2,0	1,2	3,6	8,1	7,6	4,4	7,1	9,8	3,4	1,1	0,0	.	.	1,5	1,3	2,0	5,8	112,5
65	Kasprowy Wierch	4,4	.	5,5	2,1	4,1	13,3	11,8	13,8	9,8	6,6	.	.	0,4	4,3	2,5	1,8	5,3	8,5	8,4	7,5	7,4	10,8	4,8	1,6	.	.	.	1,8	2,0	2,8	6,2	147,5
66	Wesołowice	8,4	.	10,7	2,7	9,8	10,7	8,0	13,1	9,2	0,3	.	0,5	6,7	1,0	2,4	4,6	6,2	9,5	8,4	12,4	12,1	11,4	12,4	11,8	6,7	.	.	6,3	5,4	0,6	8,6	199,9
67	Zdanów	6,3	.	8,1	2,9	10,0	11,7	7,9	12,8	7,6	.	.	5,4	8,8	1,1	3,1	6,9	9,3	10,7	10,2	12,6	10,3	11,6	10,5	1,4	0,2	.	.	3,4	8,0	5,4	10,9	196,9
68	Iwonicz-Zdrój	0,6	.	8,7	4,9	11,7	11,6	11,5	12,5	0,2	.	.	1,9	5,3	7,0	3,1	8,2	7,5	9,6	10,4	11,0	11,1	11,4	10,8	0,3	.	.	.	4,9	3,8	2,3	9,8	180,1
69	Lesko	1,0	.	8,5	5,6	11,4	12,5	11,8	13,1	1,0	.	.	0,2	5,2	6,2	4,2	8,2	8,9	9,5	10,0	10,3	10,7	11,1	9,6	1,2	0,4	.	.	2,1	3,9	2,0	7,6	176,2

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	3,8	3,1	6,8	1,6	.	8,0	1,9	3,7	5,5	0,7	.	8,6	2,9	4,1	9,4	5,4	4,8	9,0	1,2	7,8	3,8	9,5	9,0	8,8	8,1	9,5	4,3	6,0	.	6,3	153,6
2	Kołobrzeg	1,0	3,0	5,0	6,3	2,5	6,9	0,4	6,4	4,2	0,1	0,1	6,5	6,2	4,6	10,0	6,7	3,5	7,4	1,6	5,3	4,2	9,0	8,9	8,9	8,7	8,4	5,1	4,2	0,0	4,7	149,8
3	Świnoujście	0,9	3,3	4,6	7,3	6,4	3,3	.	7,9	6,8	0,9	0,5	4,7	7,6	5,3	9,2	9,6	1,6	7,6	4,7	6,4	5,2	9,8	9,7	9,1	9,1	9,5	2,2	4,3	2,8	2,1	162,1
4	Resko	3,4	4,3	4,1	6,7	4,3	4,6	.	7,0	5,6	0,1	0,4	6,2	4,3	3,1	8,0	8,1	4,8	8,0	2,2	6,7	3,9	8,6	8,3	8,3	7,7	7,3	3,0	4,4	.	0,9	144,2
5	Szczecinek	2,0	5,3	5,5	3,4	1,3	5,9	0,9	3,9	6,9	1,0	.	7,4	7,7	3,9	7,8	6,5	6,2	8,5	3,0	9,4	2,6	9,4	9,2	9,1	8,4	8,4	3,3	3,6	.	2,3	152,6
6	Chojnice	3,8	4,8	4,4	0,6	0,2	8,2	0,7	3,2	4,0	1,3	0,1	3,8	5,9	4,6	9,3	9,7	,6	9,3	1,8	8,3	0,9	9,4	9,8	9,3	9,1	9,7	3,3	3,2	.	4,6	150,9
7	Hel	9,6	0,6	5,9	0,2	.	10,3	1,9	3,3	2,0	3,8	.	7,8	1,1	1,9	10,0	9,2	5,0	9,2	4,0	8,5	0,4	8,9	8,9	7,9	7,8	8,5	1,2	3,6	.	7,0	148,5
8	Gdynia	8,7	1,5	6,2	.	11,1	.	4,1	4,9	5,9	.	1,1	6,8	1,8	5,9	9,6	9,3	6,3	9,6	5,5	8,3	2,5	9,1	9,7	9,4	8,4	8,9	1,2	1,6	.	7,5	162,9
9	Świnna	5,1	.	4,5	0,1	.	8,3	2,0	4,3	1,8	3,1	0,1	9,3	2,1	2,7	9,5	9,6	7,3	7,7	3,8	7,3	1,6	9,3	8,8	8,8	7,7	8,7	0,6	5,0	.	6,7	145,8
10	Stare Pole	9,2	1,6	6,9	0,3	.	9,5	2,8	3,6	3,7	2,5	.	6,8	2,7	2,1	9,6	7,7	6,2	8,3	3,9	6,1	0,2	10,5	10,0	9,4	8,4	9,2	0,7	3,3	.	6,6	151,8
11	Radomtowo	7,4	2,1	6,7	.	.	9,8	2,7	3,6	4,7	3,3	0,1	5,9	6,4	3,4	11,2	8,5	7,1	9,3	5,6	7,4	0,7	9,7	9,3	9,3	8,8	9,0	0,8	2,8	.	6,3	161,9
12	Frabuty	8,3	4,0	6,4	.	.	9,6	1,5	2,3	5,2	1,9	0,5	7,0	7,1	2,3	8,5	7,3	8,3	9,2	1,3	4,9	0,3	9,5	9,8	9,8	7,9	9,9	1,0	.	3,2	8,9	155,9
13	Bydgoszcz,IMUZ	4,9	6,5	3,2	.	8,2	6,9	3,1	3,1	4,9	1,0	0,3	5,2	8,2	2,4	8,4	9,0	8,4	9,1	3,1	5,7	1,7	9,1	9,4	8,5	7,9	8,8	2,6	1,4	.	5,8	152,8
14	Suwałki	9,9	4,5	6,9	7,0	0,2	7,1	0,7	3,0	7,5	9,4	1,7	4,8	4,4	4,5	6,3	9,0	9,6	9,1	2,7	1,4	0,2	10,1	10,1	10,2	9,6	7,8	6,2	1,2	2,4	7,3	180,8
15	Mikołajki	10,7	6,2	7,2	2,6	0,2	7,4	2,6	7,0	8,8	7,6	0,2	5,7	5,4	4,5	8,5	8,0	9,3	9,3	3,0	2,1	0,9	9,6	9,7	9,2	(9,2)	9,6	3,0	2,5	.	6,8	(176,8)
16	Siedlce	10,6	5,5	7,4	7,9	3,4	7,8	1,6	7,9	7,0	8,2	1,6	4,8	0,5	2,7	7,7	8,2	9,2	8,6	3,1	1,3	0,1	10,3	10,5	9,7	9,1	8,1	3,5	1,2	1,0	7,1	175,5
17	Białystok	10,9	5,5	6,4	7,7	5,5	9,5	1,2	8,9	7,8	8,3	1,6	5,7	6,5	2,1	7,8	10,5	9,8	9,2	1,9	1,7	2,9	9,2	10,1	9,6	9,1	8,3	3,5	2,8	1,7	8,3	194,0
18	Gorzów Wlkp.	2,2	6,9	2,8	4,8	9,9	3,9	1,3	6,4	6,6	1,0	1,3	2,8	3,9	0,8	6,0	8,9	7,2	7,6	3,6	5,3	3,7	8,6	8,8	8,2	6,3	7,2	0,2	2,4	2,0	4,4	147,0
19	Przebędowo	1,1	7,5	6,4	2,2	6,1	7,9	0,7	4,9	5,1	1,6	0,3	5,8	8,4	3,9	6,6	10,1	9,0	9,3	4,5	5,7	3,6	9,2	9,3	9,2	9,4	7,2	4,6	0,3	0,7	5,5	166,1
20	Przybroda	5,1	7,1	5,7	2,3	7,9	7,6	1,8	5,7	4,4	4,2	.	1,2	6,7	3,6	5,5	9,6	9,7	8,6	5,4	5,6	4,3	9,2	9,3	9,6	9,3	7,0	3,6	.	1,3	6,5	167,8
21	Poznań-Ławica	6,1	6,8	6,2	2,0	7,8	7,4	1,6	6,4	4,9	1,6	.	6,6	7,8	3,1	4,6	8,7	7,9	8,3	3,7	5,2	3,1	7,8	8,3	8,1	7,7	5,8	4,4	.	0,9	6,4	159,2
22	Pławieka	7,0	6,8	5,5	1,8	8,4	7,8	1,6	6,7	4,6	1,7	0,2	7,7	8,9	3,2	4,3	9,5	8,5	9,4	4,0	5,8	3,2	9,3	9,6	9,7	9,6	7,1	5,3	0,1	1,4	6,3	175,0
23	Kórnik	5,0	7,8	7,1	1,1	8,2	6,7	2,2	6,2	4,8	0,6	.	8,7	7,3	6,1	3,5	9,3	9,2	9,8	2,4	4,2	1,7	9,0	9,4	9,6	9,1	7,2	4,4	0,3	1,1	6,7	168,7
24	Oberniki Śl.	2,2	5,5	2,6	1,1	10,4	2,9	3,7	7,5	7,7	0,2	2,9	3,8	1,9	5,0	3,0	10,0	9,2	10,6	4,3	2,4	2,9	10,2	10,3	9,6	8,0	9,3	5,4	8,5	.	6,1	167,2
25	Laskowice Olszańskie	3,3	5,0	4,9	0,0	10,3	4,6	4,9	4,6	5,6	0,4	0,1	8,7	3,8	4,7	3,1	9,4	9,3	9,7	0,4	1,3	3,5	10,1	9,7	9,1	6,1	5,5	3,4	.	1,5	6,9	149,9
26	Ciechocinek	4,0	6,0	6,9	.	2,7	9,3	3,0	6,4	6,1	0,4	.	3,9	7,4	3,4	8,8	7,3	9,0	10,0	2,4	3,0	1,8	9,0	9,6	9,7	7,6	9,4	2,4	1,1	.	7,3	157,9
27	Więcławice	3,7	8,1	5,2	.	5,3	.	9,0	5,8	6,3	.	.	5,3	8,5	3,0	8,4	10,7	9,2	9,6	4,3	3,7	2,4	8,8	8,8	9,4	9,0	8,8	3,2	1,3	.	7,8	165,6
28	Legionowo	10,1	6,2	8,6	2,2	6,3	5,1	4,3	7,8	8,3	6,4	.	6,6	5,9	6,4	8,6	10,0	8,1	8,8	0,7	0,8	3,9	8,0	9,1	8,7	8,7	8,3	1,8	1,6	.	8,2	179,5
29	Warszawa-Bielany	10,1	6,1	9,4	1,6	6,3	5,3	5,3	6,8	7,5	7,0	0,1	7,0	5,4	6,2	6,5	10,1	8,7	9,8	0,4	1,0	5,6	8,0	10,5	10,1	10,0	9,9	3,0	1,9	.	9,6	189,4
30	Warszawa,Min.Kom.	9,5	6,1	8,6	1,8	6,6	4,8	3,6	6,9	7,6	6,1	.	6,1	5,2	4,9	6,6	8,6	8,2	9,3	0,5	1,4	5,2	7,3	9,8	9,6	9,6	9,1	2,1	2,0	.	9,3	176,4
31	Międzylesie	9,7	7,2	9,3	3,3	5,6	5,4	4,4	8,4	9,0	7,3	0,7	8,0	5,7	6,0	6,9	10,3	9,0	9,5	0,5	1,0	5,6	8,3	9,3	9,6	9,6	9,5	0,9	1,6	0,5	8,7	190,2
32	Zwinów	9,9	6,4	8,7	1,8	7,2	3,8	4,3	7,3	5,7	6,5	.	3,6	4,7	6,3	3,6	10,9	10,1	10,2	0,2	1,2	3,7	8,0	10,6	10,9	10,4	9,9	3,3	1,3	.	9,8	182,3
33	Świder	10,4	8,4	9,7	3,6	7,3	4,8	5,5	7,1	9,7	7,4	0,6	6,7	4,8	5,8	6,5	10,8	9,0	10,1	0,8	2,2	5,9	7,1	9,6	9,3	9,5	9,7	1,8	2,5	.	8,2	194,6
34	Popela-Błonie	4,5	6,3	6,8	.	6,8	6,4	3,5	5,7	7,7	5,8	.	8,4	5,3	5,9	5,8	9,5	9,3	9,5	0,8	0,3	4,3	9,0	9,9	9,8	6,4	9,4	2,2	0,1	.	9,1	158,5
35	Mława	3,3	2,0	8,8	2,0	6,6	4,6	4,7	8,0	7,2	6,0	.	6,9	5,4	4,5	3,7	10,8	10,0	10,3	0,1	1,2	5,5	7,4	10,3	10,5	9,1	9,8	3,2	1,5	.	9,5	185,9
36	Skierniewice	8,6	5,7	8,4	0,4	6,2	3,4	5,5	5,3	6,8	3,6	.	2,6	5,4	5,9	4,0	10,5	10,2	9,4	0,1	1,2	5,6	8,7	10,0	9,8	10,4	9,8	3,3	1,0	.	9,5	171,3
37	Bełsk	9,2	7,8	8,9	2,5	7,0	(3,9)	(4,3)	7,8	7,7	6,8	0,5	6,9	5,7	6,0	5,1	10,7	8,9	9,3	0,1	3,7	5,6	8,3	8,5	9,2	7,1	9,0	3,3	1,8	.	7,8	183,4)
38	Łódź-Lublinek	5,2	5,8	5,7	.	8,7	4,9	6,9	4,0	7,2	2,3	0,1	7,4	6,1	5,1	2,7	9,6	9,4	9,2	0,5	0,1	4,6	10,0	9,6	9,5	6,7	9,0	3,5	0,2	.	9,1	163,1
39	Kalisz	2,8	5,7	6,2	0,0	9,4	6,3	5,7	5,4	6,7	1,6	.	8,6	4,5	3,0	7,0	9,3	8,6	10,0	1,6	0,3	4,9	8,5	9,8	9,5	8,8	6,6	6,2	0,1	1,4	8,9	169,4
40	Wieluń	3,8	6,1	7,3	0,3	10,5	6,1	9,2	5,2	6,3	1,7	0,2	8,7	4,8	2,7	4,1	9,4	10,5	10,5	.	1,5	4,3	10,3	10,3	9,6	9,0	7,5	4,1	.	1,3	6,3	171,6
41	Szczytno	11,8	4,9	7,4	6,2	7,8	7,1	3,0	6,9	9,8	7,9	0,3	3,3	4,3	3,1	7,7	9,3	9,1	9,6	1,8	2,3	6,3	8,1	9,1	8,9	8,6	8,8	2,6	2,3	.	8,7	187,0
42	Białowieża	10,6	6,9	6,4	7,9	7,3	9,2	1,0	7,3	9,0	8,8	3,0	3,7	7,7	2,5	5,3	8,3	9,9	9,6	1,7	4,7	3,6	7,9	10,8	10,1	9,3	8,6	5,3	3,5	4,3	8,4	202,8
43	Terespol	10,9	9,4	7,4	7,1	10,1	7,8	3,1	9,5	9,8	9,8	2,7	4,3	6,6	5,0	6,1	9,7	10,7	10,2	1,9	7,2	7,8	7,6	9,8	9,4	9,9	8,7	2,8	5,2	4,0	7,6	224,1
44	Sobieszyn	9,5	9,0	9,8	5,0	10,5	6,6	5,7	8,7	8,8	9,9	2,3	5,6	6,9	2,9	4,4	10,6	8,5	9,8	0,2	6,0	6,9	8,7	9,8	10,3	8,7	9,6	0,4	5,6	0,5	7,8	206,8
45	Puławy	7,9	7,4	9,3	3,3	8,9	6,3	6,2	6,9	9,5	7,5	2,2	4,3	6,6	2,6	3,2	9,4	8,6	9,2	0,1	6,0	6,7	7,7	8,8	9,4	8,1	9,2	1,5	5,9	.	7,2	183,9
46	Chełm	8,4	8,4	8,6	6,6	10,0	5,4	4,1	6,3	11,4	10,2	3,9	5,8	9,2	0,7	3,0	10,8	10,8	9,6	3,0	7,0	7,7	9,3	10,4	10,9	10,6	10,4	0,1	7,7	2,3	8,0	221,5
47	Szczawno-Zdrój	0,4	4,4	1,8	1,5	10,5	0,5	7,8	4,0	3,2	.	0,6	9,5	3,3	2,1	8,1	9,7	9,7	9,1	0,4	2,4	3,4	9,9	9,7	9,1	6,0	3,9	3,6	.	3,8	6,8	145,2
48	Świetlica	0,4	5,5	0,4	2,3	10,3	0,6	0,3	0,3	4,2	.	0,4	5,9	4,1	1,1	5,7	9,9	8,8	7,5	0,2	.	7,1	10,4	10,1	8,4	1,3	.	.	.	0,8	7,7	113,7
49	Opole	5,2	7,1	8,1	0,3	10,3	5,0	7,0	4,5	7,8	0,7	0,1	8,2	6,2	1,2	4,2	8,3	9,1	9,9	1,0	3,6	4,9	8,4	9,2	9,1	8,5	6,6	5,3	0,0	2,3	8,1	170,7
50	Kudowa-Zdrój	1,8	4,1	4,4	0,8	10,8	.	2,7	3,7	7,8	.	1,2	6,0	4,2	2,3	6,1	9,3	9,4	9,4	0,1	3,4	5,5	9,0	9,8	9,2	8,1	6,1	4,1	.	3,9	7,3	152,5
51	Polanica-Zdrój	0,7	5,0	3,7	0,5	10,1	.	6,4	3,6	5,9	0,3	.	9,7	8,5	3,2	4,0	9,4	9,4	9,8	0,3	1,6	4,4	9,5	9,5	9,8	9,1	5,4	5,7	0,1	4,9	9,2	159,7
52	Okroniów	3,4	6,4	8,5	0,2	10,5	3,8	5,6	5,6	9,3	3,8	0,0	7,5	5,4	3,0	2,0	7,0	7,6	9,6	.	6,6	7,1	9,6	10,3	5,9	9,2	9,8	6,6	2,5	0,4	7,7	174,9
53	Świerklaniec	0,8	7,6	7,8	.	7,0	5,5	6,9	4,7	9,5	2,0	.	8,9	9,2	6,1	5,4	5,8	9,1	9,3	.	5,1	6,1	8,4	8,8	9,3	8,9	7,3	4,3	0,4	1,3	6,0	171,5
54	Kraków,Obs.Astr.UJ	3,8	6,7	8,6	.	9,3	3,1	7,0	7,3	10,7	3,2	0,7	7,0	3,5	5,7	2,9	7,0	8,8	9,2	.	3,4	7,2	8,7	9,1	9,3	7,0	1,5	7,7	6,5	1,0	5,7	171,6
55	Cieszyn	0,8	7,6	5,8	.	7,0	.	4,9	4,6	9,5	2,5	.	5,4	8,4	1,8	0,8	9,2	9,8	9,8	.	2,1	4,0	9,1	9,7	9,7	7,6	8,0	4,2	1,4	2,0	6,7	152,4
56	Istebna-Kubalonka	0,9	7,2	7,8	.	8,4	2,5	3,1	4,3	10,4	3,0	.	5,7	7,7	2,2	0,3	10,4	10,3	10,7	.	3,0	2,3	9,7	10,0	10,5	9,9	5,8	4,9	3,0	0,1	6,8	160,9
57	Rabka	3,5	6,8	9,2	0,1	6,5	0,9	4,9	4,7	11,2	4,0	2,2	7,7	6,7	1,4	1,1	9,4	10,4	10,7	.	.	3,7	9,9	10,5	10,4	8,5	8,7	6,4	0,7	1,0	8,0	169,6
58	Jabłonka	4,1	6,5	8,6	.	7,3	0,8	4,1	6,2	10,2	4,0	2,9	7,6	2,9	2,2	0,1	7,5	8,3	8,0	.	0,2	1,7	6,4	8,3	7,6	6,2	6,7	5,5	1,2	1,0	7,6	143,7
59	Krynica	2,3	8,0	8,0	1,0	9,3	0,5	7,1	5,9	10,2	5,1	5,3	3,1	6,7	0,3	2,3	8,5	8,3	9,6	2,3	.	2,0	8,5	7,6	8,6	9,6	9,3	7,5	4,7	1,1	7,1	169,8
60	Krynica-Góra Park.	1,8	8,0	8,2	1,5	8,2	0,5	7,2	6,4	9,8	5,2	5,1	1,9	6,4	0,2	1,3	8,7	8,5	9,9	2,5	.	2,0	9,2	7,2	9,4	9,5	9,1	7,2	5,3	1,1	6,3	167,3
61	Muszyna	2,4	7,8	9,0	0,7	8,9	0,2	7,4	7,4	9,7	2,1	4,1	4,2	3,8	0,1	2,0	6,6	7,3	8,6	2,2	.	1,4	6,5	5,6	6,9	8,3	8,6	7,2	4,4	1,4	7,4	152,2
62	Zakopane	2,5	1,0	9,8	0,3	8,7	1,4	7,6	7,3	10,6	2,7	4,3	3,5	3,3	1,1	1,3	10,3	10,0	9,2	0,8	.	0,3	10,6	10,4	10,6	7,9	9,4	(9,6)	3,7	2,9	6,9	(168,0)
63	Gubałówka	2,5	0,7	8,8	0,5	8,6	0,7	6,9	6,5	8,8	2,1	3,4	2,2	3,8	0,5	2,2	9,1	9,0	8,7	0,6	.	0,0	9,1	9,3	9,2	7,3	8,4	7,6	3,0	1,8	6,7	148,2
64	Hala Gąsienicowa	1,1	4,2	7,7	.	7,1	0,2	6,7	3,1	8,9	0,7	1,0	0,9	1,5	.	0,6	9,3	8,7	9,4	0,3	.	0,3	8,9	9,0	9,0	7,8	7,9	4,2	1,9	0,3	3,8	124,5
65	Kasprowy Wierch	.	5,8	8,7	.	1,7	.	5,4	2,9	5,7	.	1,1	2,8	1,5	0,3	1,3	10,9	11,7	11,6	0,2	.	1,5	11,5	11,7	11,7	9,2	6,2	0,6	0,4	.	5,4	129,8
66	Serbkowice	6,2	7,3	8,4	7,0	9,7	3,8	4,9	5,6	11,0	8,4	4,3	2,9	5,2	2,4	1,0	11,4	10,7	9,6	5,1	2,5	6,8	8,2	10,0	9,8	9,7	9,8	0,8	6,3	2,2	8,6	199,6
67	Zdanów	7,9	7,1	7,8	1,0	10,3	6,5	6,0	5,3	10,3	7,2	3,6	6,6	7,0	2,8	2,4	10,8	5,7	10,3	.	3,3	8,8	4,5	10,8	9,5	8,6	10,0	4,9	5,9	0,9	5,8	191,6
68	Iwonicz-Zdrój	3,9	5,8	8,4	1,3	10,5	2,3	6,2	6,6	10,3	6,4	4,2	2,3	5,2	0,7	3,2	7,3	10,0	9,9	1,1	0,0	4,5	9,5	9,5	9,5	8,5	9,0	3,6	5,9	1,2	7,3	174,1
69	Lesko	2,7	4,4	8,5	4,5	10,1	3,1	6,1	4,6	11,4	7,1	2,7	2,5	4,3	0,3	2,8	8,2	11,0	10,9	4,4	.	3,5	7,7	10,6	10,6	9,9	9,6	2,6	7,9	1,2	5,9	179,1

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	9,4	9,4	.	3,9	6,6	4,8	3,2	5,2	2,3	5,6	0,9	3,2	0,7	.	4,0	0,2	8,0	2,6	6,0	7,4	4,7	3,5	1,2	.	.	.	.	.	.	.	.	.	92,8
2	Kołobrzeg	9,5	9,1	4,1	6,3	1,7	4,0	0,3	5,7	5,8	5,2	3,1	4,9	5,1	3,8	3,5	1,3	6,5	3,6	4,7	5,8	5,5	8,4	4,1	.	1,8	5,1	0,6	0,5	.	3,9	1,4	125,3
3	Świnoujście	9,6	7,9	4,1	6,7	5,4	.	1,5	3,6	4,9	4,6	6,9	6,2	6,4	6,6	3,3	1,3	5,4	3,9	7,4	5,2	5,7	8,8	8,1	.	5,2	5,0	2,0	2,6	0,2	3,3	1,6	144,0
4	Resko	9,1	7,9	4,4	6,1	3,6	3,4	3,7	5,0	6,8	3,3	3,4	4,5	5,8	5,1	3,7	1,1	6,5	2,9	4,7	7,2	5,5	7,3	5,6	.	2,9	6,5	.	0,9	.	5,1	0,1	132,1
5	Szczecinek	9,0	8,1	1,6	3,8	3,8	0,1	5,3	4,4	5,4	4,4	1,2	4,4	6,2	5,7	6,0	.	6,8	0,9	3,4	2,4	6,1	7,4	1,2	4,1	0,1	3,3	.	.	3,2	5,7	1,5	115,5
6	Chojnice	9,5	7,0	1,0	3,5	5,9	.	6,3	4,8	2,8	5,1	1,4	5,3	4,9	1,8	5,5	.	8,4	.	4,4	5,0	6,4	8,6	0,5	7,3	2,3	2,5	.	.	4,6	2,9	1,2	118,9
7	Hel	9,0	1,0	.	2,6	5,1	5,0	3,2	5,4	7,2	3,3	0,5	6,3	1,1	.	5,4	.	8,7	0,8	7,3	5,7	3,0	1,8	1,1	.	3,1	5,0	.	0,1	0,2	4,1	2,4	98,4
8	Gdynia	8,7	0,1	2,5	.	2,9	7,0	4,6	6,1	5,6	2,8	2,2	5,2	1,4	1,4	6,7	0,4	6,9	1,5	6,7	4,1	3,5	6,1	1,4	0,1	1,3	7,5	0,2	.	1,2	4,6	2,8	105,5
9	Świbno	9,1	0,7	.	1,0	6,4	3,0	4,8	4,8	3,6	2,0	0,3	5,3	1,3	.	4,2	.	8,3	1,6	7,3	7,0	4,9	3,5	0,2	1,5	1,6	0,7	.	1,1	1,2	5,6	3,7	94,7
10	Stare Pole	8,9	7,4	.	.	3,6	3,3	5,2	4,9	4,7	2,2	0,6	5,5	1,5	.	5,5	.	9,1	1,3	7,8	7,8	5,3	2,7	0,0	1,1	2,0	.	.	1,4	3,4	6,6	3,6	105,4
11	Kadostowo	8,3	6,6	.	2,6	4,9	4,0	6,3	6,4	4,9	4,0	1,2	5,3	3,2	.	.	5,0	9,4	1,1	7,6	7,5	5,5	7,0	0,3	5,2	0,1	.	.	0,4	2,7	5,3	3,8	118,6
12	Frombork	9,8	8,2	.	2,1	5,4	5,5	5,2	2,7	2,0	2,4	0,5	5,3	2,4	.	6,1	.	9,0	.	7,5	8,5	4,6	2,7	.	4,2	1,4	.	.	.	4,2	4,5	1,6	105,8
13	Bydgoszcz, IMUZ	8,2	8,8	1,7	.	1,2	.	5,8	1,8	3,2	3,3	.	8,6	5,8	5,7	4,9	.	7,8	.	0,2	3,3	3,0	7,0	.	7,9	0,3	.	.	0,2	6,8	3,8	4,7	108,0
14	Suwałki	10,1	4,7	8,5	2,2	2,6	0,1	2,4	5,4	2,4	0,1	0,4	0,3	0,4	.	7,9	0,2	2,2	.	2,6	5,0	7,0	0,8	0,7	3,1	0,1	1,3	.	0,1	5,9	1,1	1,4	79,0
15	Mikołajki	8,7	1,4	4,6	4,1	1,6	1,5	6,6	5,3	2,0	1,0	0,8	1,3	3,0	.	6,9	.	8,9	.	6,0	7,7	6,8	0,5	.	1,2	.	3,1	0,1	0,2	5,8	4,2	2,1	95,4
16	Siedlce	7,6	2,6	6,4	0,4	2,9	.	1,7	3,6	3,2	0,4	0,4	0,1	2,8	.	7,1	0,2	7,2	0,1	4,7	4,4	5,4	.	1,3	0,1	.	0,2	.	0,2	6,4	3,8	2,0	75,2
17	Białystok	7,9	2,3	6,6	0,1	2,8	4,9	1,7	1,8	2,8	0,6	.	0,6	2,4	.	7,6	2,2	5,9	.	5,2	2,8	3,2	1,7	2,8	1,9	.	.	0,2	0,3	6,2	1,2	0,6	78,3
18	Gorzów Wlkp.	9,2	4,7	4,9	7,2	0,1	0,6	6,2	0,2	5,5	0,8	4,5	8,5	8,2	5,8	5,2	.	3,9	0,1	1,8	3,9	7,4	7,8	6,4	.	2,3	4,7	.	1,4	3,8	6,4	2,4	123,9
19	Przebędowo	9,8	8,2	4,4	3,9	.	2,3	8,7	0,8	3,8	1,7	2,9	8,4	5,0	6,8	5,7	.	4,7	0,5	.	2,7	6,8	8,1	2,6	4,1	.	6,7	.	.	5,7	5,9	3,7	123,9
20	Przybroda	9,8	6,7	5,3	5,3	0,4	3,5	8,9	0,8	3,5	2,9	4,9	8,8	7,0	7,5	6,7	.	6,1	0,8	0,1	2,9	7,8	8,3	4,3	0,9	.	7,3	0,4	1,3	6,0	4,5	6,2	138,9
21	Poznań-Zawica	8,3	6,4	4,8	4,3	2,1	3,4	7,8	.	3,7	2,4	4,0	8,0	7,1	6,8	5,6	.	6,0	1,0	0,2	4,4	6,8	6,8	3,8	1,2	3,3	6,9	.	0,8	5,3	5,7	4,6	131,5
22	Plewiska	9,8	7,4	5,1	3,6	0,5	4,1	9,3	.	3,5	1,7	5,4	8,9	7,2	7,8	5,9	.	5,6	0,8	.	4,4	7,9	6,9	3,3	1,0	3,8	7,0	0,6	6,5	6,6	5,8	5,1	145,3
23	Kórnik	9,7	8,0	4,5	6,9	1,7	4,5	9,1	0,4	2,4	2,6	4,7	8,1	5,3	8,0	5,9	.	5,1	0,9	.	3,9	7,8	7,3	2,9	1,9	2,9	6,7	1,9	0,3	6,8	6,0	4,3	140,5
24	Oborniki Śl.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
25	Laskowice Oławskie	9,5	7,0	3,6	0,9	2,7	4,2	4,9	.	1,9	2,6	4,0	9,9	8,6	8,3	6,2	5,3	0,0	5,5	.	2,0	7,5	7,1	1,6	0,6	4,8	1,1	7,6	1,9	5,7	7,0	3,0	135,0
26	Ciechocinek	9,2	9,8	.	4,9	.	0,1	4,7	1,6	4,0	2,9	0,1	6,8	5,1	7,6	6,6	.	9,0	.	2,5	5,0	5,9	7,6	.	7,9	1,1	0,4	.	0,1	7,5	6,0	3,5	119,9
27	Więcławice	8,9	9,1	0,9	3,1	.	.	7,0	2,2	3,2	4,8	.	7,9	6,7	7,0	7,2	.	9,1	.	2,3	5,6	6,9	7,5	.	7,9	1,4	.	.	.	7,4	4,5	5,3	125,9
28	Legionowo	7,2	8,2	2,4	.	3,2	.	6,7	0,8	1,6	1,1	0,3	3,4	5,5	6,3	7,8	4,2	9,0	.	5,5	5,9	6,1	7,4	.	5,1	.	1,9	3,2	.	6,3	3,4	3,7	116,2
29	Warszawa-Bielany	9,4	9,5	3,6	.	2,4	0,6	8,5	0,5	1,3	1,4	0,1	2,5	5,6	6,6	7,8	4,9	7,3	0,1	7,4	7,6	7,5	9,1	.	4,8	.	4,2	4,9	0,2	6,7	3,5	3,3	131,3
30	Warszawa, Min.Kom.	9,6	9,6	3,6	.	1,3	3,4	8,5	0,1	1,5	1,4	0,1	2,0	4,8	4,9	6,9	2,1	7,0	0,1	6,6	0,4	7,1	7,8	.	3,8	.	1,8	.	.	.	0,6	1,6	96,6
31	Międzylesie	9,4	9,7	0,7	.	2,7	.	8,1	.	1,7	3,1	0,1	2,8	3,5	5,9	7,9	7,6	(7,3)	.	7,5	5,6	6,4	7,4	.	4,4	.	2,6	3,7	.	6,3	3,8	0,1	(120,3)
32	Brwinów	10,6	10,2	3,3	.	2,6	1,0	9,4	0,7	2,5	0,1	0,2	1,9	5,3	4,7	8,7	(4,9)	(7,5)	0,1	6,3	6,7	7,2	8,9	.	.	3,3	0,6	4,6	0,4	5,8	3,9	.	(121,4)
33	Świder	8,9	9,1	3,2	.	1,9	7,6	3,4	0,3	1,0	0,3	.	3,0	6,0	7,0	8,6	6,0	7,3	0,1	6,2	5,1	6,9	7,0	.	5,1	0,1	2,1	4,2	0,6	7,2	3,8	2,3	124,3
34	Topola-Błonie	9,8	9,2	.	1,8	0,2	2,8	8,8	0,1	3,4	4,1	0,8	5,7	6,3	7,8	6,9	2,5	8,1	0,1	3,4	5,6	7,0	7,4	.	4,6	.	.	.	0,2	7,0	6,1	3,6	123,3
35	Młochów	9,6	9,3	1,4	.	1,8	2,6	9,2	.	0,9	2,6	0,3	2,6	4,8	6,9	8,8	4,9	8,4	0,4	6,6	6,6	8,1	8,9	.	3,5	.	0,9	5,8	0,1	6,5	7,0	2,2	130,7
36	Skierniewice	10,0	.	0,8	.	1,4	3,2	9,0	0,1	0,2	2,1	1,5	3,1	6,1	8,0	8,6	4,2	9,0	0,6	4,9	7,5	6,8	7,1	.	2,0	.	.	3,9	1,4	6,8	7,5	3,0	118,8
37	Belsk	8,9	9,2	1,6	.	1,5	5,8	8,9	0,1	2,4	1,7	0,8	1,4	4,8	6,7	8,3	7,9	0,8	.	5,3	6,8	5,6	7,3	0,2	2,8	.	0,7	6,4	0,4	6,9	6,8	2,5	122,7
38	Łódź-Lublinek	9,9	9,4	.	0,6	4,9	5,0	9,1	.	1,3	2,3	0,9	6,4	6,5	8,0	8,5	4,9	7,2	.	2,2	6,3	7,2	8,7	.	4,6	.	.	6,0	0,3	5,0	5,9	0,8	132,1
39	Kalisz	8,8	8,6	6,6	4,9	2,5	4,2	8,2	.	1,6	3,2	0,5	8,3	4,4	8,6	7,4	3,7	5,4	0,2	.	3,3	5,8	7,5	0,5	2,5	5,0	4,6	6,7	1,8	7,3	6,4	2,9	141,4
40	Wieluń	10,8	9,6	3,2	3,5	3,7	5,3	7,7	.	1,1	2,0	0,5	8,6	6,4	9,7	8,4	6,1	3,2	2,6	0,1	4,3	9,5	9,3	0,4	4,4	0,4	4,0	6,3	1,5	8,0	6,8	1,5	148,9
41	Szepietowo	8,9	7,8	0,3	4,4	3,3	3,4	5,5	1,1	3,3	2,2	.	.	3,5	0,6	7,5	.	5,9	.	7,0	4,1	6,9	4,4	.	2,6	.	.	2,2	.	4,6	6,9	0,6	97,0
42	Białowieża	9,4	2,9	7,8	0,1	1,3	4,5	0,3	1,7	2,4	0,6	.	0,4	1,4	.	8,0	2,5	6,2	.	3,7	0,1	6,5	3,5	1,4	6,4	.	.	.	1,1	6,0	0,2	0,2	78,6
43	Terespol	9,0	7,4	6,6	3,0	3,4	4,1	2,9	0,7	0,6	2,6	.	.	0,8	2,2	8,4	5,1	6,3	0,3	4,7	1,7	7,4	5,5	0,7	6,2	.	.	.	0,2	7,9	1,7	0,2	99,6
44	Sobieszyn	9,9	10,1	5,8	.	5,4	3,5	9,4	1,6	0,1	0,3	0,0	3,7	3,1	6,1	9,0	4,9	7,0	0,5	6,0	6,6	2,5	7,5	.	6,0	.	4,7	6,3	0,4	6,6	6,6	0,2	133,8
45	Puławy	9,0	9,2	4,5	.	3,6	3,5	8,8	1,7	0,2	.	0,1	3,7	3,6	6,9	7,9	2,5	5,4	0,4	5,7	4,7	0,1	6,6	.	6,6	.	4,2	5,2	0,2	5,3	5,8	0,0	115,4
46	Chełm	10,2	10,0	9,1	7,0	9,0	5,4	3,5	2,6	0,2	0,7	.	1,5	0,8	6,7	8,5	7,5	4,5	1,6	5,0	1,3	0,1	7,6	.	5,9	.	6,0	7,3	2,3	7,8	5,9	.	138,0
47	Szczawno-Zdrój	8,7	2,0	3,1	4,2	.	5,2	8,9	2,5	1,4	7,2	7,9	8,3	8,7	7,7	7,2	4,0	.	7,4	1,8	0,6	7,5	6,3	5,0	3,9	7,1	8,1	7,5	4,3	6,6	6,8	2,9	162,8
48	Śnieżka	9,7	.	1,8	7,4	10,1	10,1	9,9	4,8	.	6,0	9,2	8,7	10,1	9,6	8,5	2,7	9,6	6,6	7,6	8,8	9,6	9,3	6,8	9,5	9,6	9,4	9,3	4,4	1,0	8,0	.	248,1
49	Opole	9,0	7,8	3,9	.	2,7	7,4	4,1	2,0	3,7	1,4	6,6	8,6	6,1	8,1	7,4	6,3	.	6,5	0,7	1,4	7,3	6,9	1,7	1,9	4,6	3,5	6,5	2,5	6,4	5,8	1,2	142,0
50	Kudowa-Zdrój	8,4	1,8	3,2	8,2	8,3	8,6	6,5	.	1,4	6,4	7,8	8,1	7,6	8,3	.	4,2	0,5	6,9	6,3	6,7	8,2	7,4	4,3	8,6	7,3	6,8	5,6	2,6	.	6,6	0,3	166,9
51	Polanica-Zdrój	8,7	4,4	0,1	2,0	.	3,9	8,0	5,7	1,5	4,8	8,1	7,6	7,6	8,2	8,0	4,5	1,3	6,7	4,2	0,3	6,9	6,2	4,8	.	4,1	6,1	6,9	2,9	6,7	2,2	0,2	142,6
52	Śnieżnik	10,1	10,0	.	.	2,9	3,5	6,3	0,3	4,3	1,2	0,2	6,0	7,1	8,6	9,2	5,7	3,3	2,9	0,9	4,7	0,2	8,8	3,2	5,4	.	2,1	6,3	2,4	7,4	7,7	.	150,7
53	Świerkleniec	9,8	8,6	0,1	.	3,5	8,3	7,5	3,2	2,7	1,2	4,1	7,4	5,8	9,0	8,1	5,9	0,7	5,1	1,0	1,7	5,7	7,3	1,0	3,9	6,4	4,5	7,1	3,6	7,0	8,1	0,3	148,6
54	Kraków, Obs.Astr.UJ	9,2	7,3	.	.	0,8	5,7	5,1	1,5	2,9	.	2,2	8,5	6,9	8,2	7,5	6,7	0,6	3,2	0,9	1,1	2,5	6,7	0,6	2,9	5,1	5,2	6,8	3,4	6,3	7,4	0,1	124,5
55	Cieszyn	9,7	8,9	0,0	.	.	8,1	9,1	4,2	0,4	0,3	7,6	7,5	7,2	8,6	7,8	6,7	.	7,2	.	0,6	3,9	4,9	2,4	2,0	6,4	6,0	4,0	0,0	7,1	6,0	0,3	136,9
56	Istebna-Kubalonka	10,3	10,1	2,2	0,1	2,2	8,9	7,9	2,5	0,7	0,3	6,0	7,8	8,6	9,5	8,7	8,0	.	8,6	2,5	3,6	9,2	9,2	7,4	4,7	9,4	8,9	8,3	6,3	7,8	5,5	0,0	185,2
57	Rabka	10,1	9,8	4,2	1,4	.	7,9	9,1	5,3	.	1,2	4,6	7,4	8,0	9,5	9,1	7,8	(0,5)	9,0	2,8	1,0	7,6	6,8	4,9	(4,9)	7,7	7,1	8,8	6,3	8,9	3,0	1,2	(175,9)
58	Jabłonka	9,2	7,3	3,4	3,6	.	7,5	5,1	6,0	1,0	1,6	4,5	8,5	6,4	8,2	7,6	7,5	0,2	5,4	5,2	5,1	6,7	5,0	5,0	4,9	5,1	6,2	6,8	3,6	6,7	6,7	0,3	160,3
59	Krynica	9,5	8,4	3,7	3,6	0,1	1,3	7,8	3,2	0,7	0,3	1,8	7,8	7,9	8,2	8,0	5,8	2,4	7,4	1,4	0,9	4,1	7,3	1,4	4,9	6,3	6,6	4,5	3,2	4,9	7,3	.	140,7
60	Krynica-Góra Park	9,8	9,8	3,9	3,6	.	1,6	9,4	2,6	0,5	0,3	2,5	7,9	3,7	8,0	8,7	7,9	2,5	7,4	1,8	0,8	3,7	6,6	0,9	5,4	6,7	7,5	5,6	3,9	5,0	7,1	0,1	145,2
61	Muszyna	8,1	7,0	5,4	3,3	.	3,7	6,1	3,0	.	1,6	6,3	4,3	6,6	7,0	6,8	5,4	5,4	6,5	2,8	0,5	6,0	6,1	0,7	5,6	5,0	5,9	3,8	2,4	3,2	7,6	.	136,1
62	Zakopane	10,2	10,2	4,2	4,8	.	8,9	10,2	7,2	.	0,4	5,1	6,0	9,6	9,1	9,5	7,0	1,5	9,5	3,0	2,0	8,8	9,5	5,7	5,1	9,3	9,3	8,9	5,4	8,2	7,3	0,4	196,3
63	Gubałówka	9,3	9,3	5,2	5,4	.	7,9	9,4	7,2	.	0,8	4,6	6,8	8,8	9,0	8,7	6,8	1,8	8,3	2,5	2,2	8,2	8,1	4,9	4,2	8,1	8,2	8,0	5,7	7,7	6,4	0,6	184,1
64	Hala Gąsienicowa	8,6	8,7	7,0	2,3	.	8,2	8,3	6,6	.	.	5,1	5,0	7,5	7,7	7,4	5,2	2,1	7,2	2,3	4,0	7,0	7,0	3,7	6,9	6,9	6,8	6,4	3,7	6,6	3,7	0,3	162,2
65	Kasprowy Wierch	11,2	11,1	8,0	3,7	0,2	9,8	10,8	7,7	.	.	6,7	8,1	10,1	10,3	10,1	7,6	4,0	10,0	6,7	3,8	9,8	9,8	6,1	9,7	9,7	9,5	9,3	6,1	8,5	8,5	0,4	227,3
66	Werbkowice	9,7	9,6	8,2	8,4	8,2	7,5	4,3	0,9	1,8	0,4	.	2,7	0,2	7,4	9,2	8,1	4,0	1,5	4,2	0,6	.	4,9	.	8,3	.	4,5	4,5	2,4	8,1	7,1	0,2	136,9
67	Zdanów	10,0	9,5	.	.	4,7	4,2	7,9	0,4	2,2	1,9	0,1	6,3	6,2	9,0	8,7	6,9	5,1	2,5	3,8	2,4	.	8,1	.	6,5	.	.	5,0	1,2	7,2	4,2	.	124,0
68	Iwonicz-Zdrój	8,9	8,8	0,1	0,1	0,5	3,1	5,8	1,7	3,0	0,1	1,0	5,1	7,7	8,1	8,0	6,9	0,8	6,6	.	0,9	2,6	6,1	1,0	2,5	0,1	4,9	7,4	4,7	6,1	6,1	0,7	119,4
69	Lesko	10,2	9,8	.	.	1,2	6,1	7,3	1,1	2,8	0,2	0,1	6,2	7,4	9,7	9,7	7,7	2,6	7,6	.	0,3	1,1	9,1	.	4,0	.	5,4	7,7	4,9	4,8	6,1	0,4	133,5

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	.	.	.	.	.	.	.	(5,0)	.	6,6	1,0	2,8	5,5	3,5	0,4	1,3	2,4	3,6	.	.	.	0,1	2,2	2,4	.	.	0,3	.	0,6	0,1	37,8
2	Kołobrzeg	.	.	2,2	1,3	1,2	.	.	1,3	.	.	5,4	6,6	6,9	2,4	4,0	4,0	4,2	1,5	0,2	.	.	.	3,6	.	.	.	0,6	.	.	0,1	45,5
3	Świnoujście	.	.	6,1	4,3	6,8	.	.	0,6	.	.	4,9	7,4	7,2	2,7	2,9	0,9	1,0	2,2	1,8	1,1	.	2,9	3,6	.	0,2	1,0	1,0	0,1	0,6	0,1	59,7
4	Resko	.	.	4,6	1,2	2,3	.	.	1,1	.	.	4,5	4,4	5,8	2,3	1,9	5,4	5,8	1,3	0,7	.	.	.	3,7	0,3	.	.	0,3	.	0,5	.	46,1
5	Szczecinek	.	.	1,0	0,1	0,4	.	.	3,5	.	.	3,8	5,6	5,0	0,7	2,9	5,1	5,1	1,2	.	.	.	1,8	4,5	3,0	.	.	0,4	0,1	0,5	.	44,6
6	Chojnice	.	0,1	1,1	1,7	0,4	.	0,0	6,2	1,2	0,1	4,3	3,3	2,8	3,4	0,7	4,9	.	1,1	.	.	.	2,1	5,3	3,6	.	.	.	.	2,6	0,5	45,4
7	Hel	.	0,1	1,5	0,1	.	.	2,0	6,3	.	4,5	0,4	1,4	1,0	.	.	0,2	0,0	.	.	.	.	0,1	5,3	.	.	.	.	.	3,1	.	26,0
8	Gdynia	0,2	1,3	.	.	0,2	.	.	5,7	.	2,2	0,6	.	0,2	1,0	.	.	.	2,9	.	.	.	0,4	6,6	2,5	0,3	.	0,1	.	4,5	0,1	28,8
9	Świnoujście	.	3,1	.	5,6	.	.	.	2,2	.	3,9	.	0,6	3,9	3,7	.	0,5	0,9	1,4	.	.	.	.	5,6	0,2	.	.	.	.	4,6	.	36,2
10	Stare Pole	.	0,8	1,1	5,4	.	.	.	2,3	.	3,9	4,9	1,3	3,0	3,8	.	3,7	2,1	(4,0)	.	.	.	1,1	5,3	0,9	.	.	.	.	5,6	0,4	(50,5)
11	Radostowo	.	0,4	0,8	4,2	.	.	.	3,7	0,1	3,3	4,9	1,7	1,3	3,6	.	4,1	1,5	4,9	.	.	.	1,8	6,8	2,4	.	.	.	.	5,0	0,3	50,8
12	Frabuty	.	1,5	0,6	2,4	0,4	.	0,0	.	.	3,5	5,6	3,5	.	.	.	5,0	.	3,6	.	.	.	1,3	3,7	5,0	.	.	.	.	1,4	0,1	37,6
13	Bydgoszcz, IMiUZ	.	3,2	3,1	0,1	.	.	.	2,4	0,4	.	1,0	.	0,4	.	.	2,6	.	1,6	.	.	.	4,2	4,7	1,9	.	.	.	.	1,8	0,7	28,1
14	Suwałki	.	2,1	0,1	0,1	0,1	.	2,4	0,2	.	2,0	5,8	.	1,7	0,4	.	3,7	3,8	2,2	.	.	.	.	.	.	.	0,6	.	.	0,6	.	25,8
15	Mikołajki	.	3,5	1,2	1,2	.	.	.	4,7	.	2,3	4,9	0,2	0,1	0,1	.	6,3	.	3,5	.	.	.	.	5,1	3,6	.	0,1	.	.	3,1	0,8	40,7
16	Elbląg	.	3,9	1,2	0,7	0,3	.	.	1,6	0,1	1,9	1,7	.	0,0	.	.	2,5	.	4,8	.	.	.	.	.	.	.	1,1	.	.	2,3	.	22,1
17	Białystok	.	2,6	0,1	.	.	.	.	1,8	0,4	1,4	.	.	1,3	.	.	3,2	.	4,5	.	.	.	.	.	.	.	1,0	.	.	.	.	16,3
18	Gorzów Wlkp.	.	1,3	4,0	1,4	.	.	3,5	1,9	.	.	.	2,8	.	2,7	1,2	.	4,2	.	.	.	.	1,7	1,7	.	.	.	0,3	.	0,5	.	27,2
19	Przebędowo	.	1,0	4,2	.	.	.	.	4,0	.	.	.	1,2	.	.	.	4,3	.	0,7	0,2	.	.	.	2,7	3,8	.	.	.	.	0,5	0,1	22,7
20	Przybroda	.	2,8	5,3	.	.	0,1	1,3	2,3	.	.	.	2,5	.	.	.	2,3	0,3	0,4	.	.	0,1	.	2,3	1,6	.	.	0,2	.	0,6	1,1	23,2
21	Poznań-Ławica	.	3,8	4,3	1,9	.	.	0,5	2,1	.	.	.	1,1	.	.	.	1,0	.	.	.	.	.	0,1	3,5	1,9	.	.	.	.	0,1	0,3	20,6
22	Flewiska	.	4,7	4,9	2,8	.	.	0,5	2,2	.	.	.	0,3	.	.	.	0,4	.	.	.	.	.	.	1,2	2,1	.	.	.	.	.	0,2	19,3
23	Kórnik	.	5,1	3,1	3,0	.	.	0,4	3,1	.	.	.	2,4	.	.	.	0,7	.	0,2	.	.	.	.	4,5	5,1	.	.	.	.	0,7	.	30,3
24	Oborniki Śl.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
25	Laskowice Oławskie	.	2,5	0,9	5,2	0,3	2,2	6,9	4,9	.	.	.	.	.	.	.	0,6	1,6	.	.	.	.	.	4,8	6,1	0,6	.	.	0,4	2,7	.	39,7
26	Ciechocinek	.	4,3	4,1	0,2	.	.	.	0,5	.	.	4,0	1,8	0,9	.	.	2,5	.	3,1	.	.	.	2,4	4,7	5,4	.	.	.	.	2,4	0,1	36,4
27	Więcławice	.	4,3	5,2	.	.	.	0,2	4,0	.	.	3,5	1,9	1,5	.	.	3,6	.	1,2	.	.	.	2,0	3,7	3,1	.	.	.	.	1,8	0,7	36,7
28	Legionowo	.	3,9	4,7	3,8	.	.	.	.	.	0,5	2,6	.	.	.	.	4,5	.	3,1	.	.	.	.	3,3	.	.	0,1	.	0,2	0,4	.	27,1
29	Warszawa-Bielany	.	4,2	5,7	5,5	.	.	.	.	3,5	.	1,3	.	.	.	.	3,2	.	3,0	.	.	.	.	4,7	1,5	1,2	0,3	.	0,4	.	.	34,5
30	Warszawa, Min.Kom.	.	3,4	4,3	3,5	.	.	.	.	.	.	1,1	.	.	.	.	2,4	.	1,3	.	.	.	.	3,5	.	.	.	.	.	.	.	19,5
31	Międzylesie	.	4,6	5,5	5,0	.	.	.	.	.	.	2,1	.	.	.	.	2,4	.	4,8	.	.	.	.	3,9	.	0,8	0,1	.	0,2	.	0,0	29,4
32	Krwinów	.	4,5	5,7	4,7	.	1,0	.	.	1,1	.	1,8	.	.	.	.	4,2	.	4,3	.	.	.	.	3,5	6,1	.	.	.	.	.	.	36,9
33	Śnider	.	5,1	6,4	5,4	.	.	.	0,2	.	.	2,0	.	.	.	.	3,1	.	3,5	.	.	.	.	(5,6)	.	0,8	0,2	.	0,1	.	.	(32,4)
34	Topola-Błonie	.	5,1	6,1	5,1	.	.	.	5,3	.	.	.	.	.	.	.	3,9	.	.	.	.	.	.	[illegible]	[illegible]	.	.	.	0,6	.	.	[illegible]
35	Włocławek	0,1	4,8	6,0	6,0	.	.	.	1,7	3,7	.	2,3	.	.	.	.	.	.	4,4	.	.	.	.	4,5	3,5	0,6	.	.	0,8	.	.	38,4
36	Skierniewice	.	5,6	8,2	7,1	.	.	.	6,7	0,5	.	1,4	.	.	.	.	0,8	.	0,6	.	.	.	.	4,5	3,2	.	0,2	.	2,1	.	.	40,9
37	Bełsk	.	4,8	6,3	5,4	.	.	.	5,7	0,3	.	0,6	.	.	.	3,0	.	.	0,8	.	.	.	0,4	4,4	1,8	1,1	.	.	.	0,9	.	34,8
38	Łódź-Lublinek	.	4,6	4,9	6,3	.	.	.	4,3	.	.	.	.	.	.	.	3,0	.	0,4	.	.	.	.	4,6	4,8	.	.	.	1,2	1,1	.	35,2
39	Kalisz	.	5,9	6,1	7,4	.	.	1,3	3,9	.	.	.	.	.	.	.	4,4	.	0,3	.	.	.	.	3,7	3,0	.	0,2	.	0,2	0,9	.	37,3
40	Kielnik	.	3,3	2,5	5,1	0,2	.	3,7	5,1	.	.	.	.	.	.	.	0,8	2,8	.	.	.	.	.	3,5	5,2	.	.	.	0,5	0,2	.	38,9
41	Szepietowo	.	3,3	1,4	.	.	.	.	2,6	0,1	.	.	.	0,1	.	.	4,5	.	3,8	.	.	.	.	2,5	.	.	1,4	.	.	2,0	.	21,7
42	Białowieża	.	2,4	.	1,7	.	.	.	2,7	1,0	1,2	3,8	.	.	.	.	1,5	.	4,7	.	.	.	.	0,3	.	0,2	0,6	.	.	0,2	.	20,3
43	Terespol	0,1	2,0	3,5	5,6	.	.	.	3,4	.	1,0	0,1	.	.	.	.	.	2,8	2,8	.	.	.	.	2,1	.	2,1	3,0	.	.	.	0,4	29,4
44	Sobieszyn	0,2	1,1	5,3	5,4	.	.	0,1	0,4	0,2	.	.	.	.	.	.	1,3	.	2,3	.	.	.	.	3,8	.	.	0,7	.	.	.	.	20,8
45	Puławy	.	0,8	5,0	4,9	.	.	.	3,7	.	.	.	.	.	.	.	0,2	.	0,5	.	.	.	.	3,0	.	0,6	0,2	.	.	.	.	18,9
46	Chełm	0,2	2,6	6,9	2,7	0,2	.	.	0,1	.	.	0,4	.	.	.	.	0,0	4,1	0,2	.	.	.	.	3,5	.	0,1	3,6	.	.	0,2	0,7	25,5
47	Szczawno-Zdrój	.	0,9	1,7	3,7	3,6	6,3	7,0	5,3	.	.	.	.	.	.	0,6	.	.	.	.	.	.	.	5,1	4,3	1,8	.	.	0,2	1,5	0,1	42,3
48	Śnieżka	.	0,1	0,3	6,5	1,1	8,7	8,6	7,9	0,3	.	.	.	.	.	5,6	.	6,5	.	.	.	.	.	4,4	5,0	3,5	.	.	.	0,5	.	59,0
49	Opole	.	2,6	2,6	3,5	3,8	1,0	5,1	4,0	.	.	.	.	.	.	.	.	1,4	.	0,0	.	.	0,1	0,7	6,2	.	.	.	2,0	2,6	.	35,6
50	Kudowa-Zdrój	0,1	1,2	2,8	1,7	2,9	.	5,6	.	.	.	.	.	.	0,6	.	.	0,1	.	.	.	3,8	.	.	1,9	.	.	.	.	1,6	0,1	22,4
51	Polanica-Zdrój	2,1	2,1	7,2	2,8	3,7	4,8	5,9	5,6	0,4	.	0,5	.	.	.	.	.	.	0,3	1,3	.	.	0,7	3,1	2,8	1,6	.	0,3	0,2	1,3	0,6	47,3
52	Skroniów	.	.	6,2	4,1	4,0	0,8	.	5,8	2,8	.	.	.	.	.	0,6	.	4,4	1,2	0,1	.	.	.	2,3	5,6	.	0,4	.	0,9	3,4	.	42,6
53	Świerklaniec	.	1,4	5,7	3,2	2,2	2,6	5,5	3,4	.	.	.	.	.	.	.	.	3,5	.	.	.	.	.	2,0	1,4	.	.	.	1,1	2,5	.	34,5
54	Kraków, Obs.Astr. UJ	.	4,3	7,6	1,5	.	0,4	5,1	2,7	3,2	.	.	.	.	.	1,3	0,1	4,2	0,7	1,2	.	.	.	0,9	4,5	.	2,3	0,1	3,2	3,2	.	45,3
55	Cieszyn	.	0,7	5,4	1,5	.	6,1	5,8	3,9	5,2	.	.	.	.	.	.	.	3,9	.	0,6	.	.	.	.	5,5	1,6	0,2	.	0,9	3,3	.	44,6
56	Istebna-Kubalonka	.	1,2	5,6	1,9	3,2	6,5	8,1	7,5	7,9	0,5	.	.	.	.	.	.	6,1	.	.	.	.	0,1	.	7,4	0,3	0,6	.	.	0,4	.	60,9
57	Rabka	0,4	2,3	6,5	.	0,7	7,0	7,3	7,7	8,0	0,5	.	.	.	.	1,3	.	6,2	0,1	3,8	.	.	.	.	5,3	2,1	2,3	1,4	0,4	4,8	0,1	68,2
58	Jabłonka	.	3,2	4,8	.	3,7	5,4	5,9	6,1	7,2	.	.	.	.	.	1,5	.	5,9	.	2,3	.	.	.	.	4,9	0,2	2,5	0,2	0,7	3,4	0,1	58,0
59	Krynica	0,1	2,1	7,0	.	2,7	7,2	0,9	6,7	6,1	.	.	.	.	.	0,8	.	5,2	.	.	.	.	0,5	.	5,7	4,1	2,2	.	0,7	6,7	.	58,7
60	Krynica-Góra Park.	.	3,5	6,0	.	2,2	6,6	0,5	7,2	5,9	.	.	.	.	.	.	.	4,3	.	.	.	.	.	0,5	6,7	3,8	2,8	.	.	5,6	.	55,6
61	Muszyna	.	2,4	6,2	.	4,1	7,2	0,5	5,4	5,1	.	.	.	.	.	1,7	.	4,5	.	.	.	.	1,3	.	5,3	3,1	.	.	2,6	5,7	.	55,3
62	Zakopane	0,1	1,1	6,0	.	3,3	8,2	7,7	7,5	8,0	0,0	.	.	.	.	4,8	.	6,7	0,2	4,9	.	.	0,8	.	6,9	1,7	2,5	0,1	0,8	6,3	0,2	77,8
63	Gubałówka	0,1	2,4	6,1	.	3,9	6,6	7,3	7,1	7,5	.	.	.	.	.	1,8	.	4,9	.	4,5	.	.	1,2	.	5,8	2,4	2,8	0,7	1,1	5,9	1,0	73,1
64	Hala Gąsienicowa	0,1	0,4	3,6	0,2	5,2	6,1	6,1	5,4	5,9	2,9	.	.	.	.	4,3	.	5,4	1,1	4,0	.	.	0,8	.	4,9	0,7	0,6	.	0,3	4,6	.	62,6
65	Kasprowy Wierch	0,2	1,1	5,0	.	6,2	8,4	8,4	7,6	8,1	4,7	.	.	.	2,5	4,8	.	7,5	.	4,8	.	.	2,4	.	7,4	2,1	.	.	0,2	4,6	.	86,0
66	Werbkowice	.	2,1	6,8	5,7	1,0	0,8	.	3,2	.	.	.	.	.	.	.	.	4,1	3,2	.	.	.	0,6	0,9	.	0,6	4,6	.	.	2,2	1,6	37,4
67	Zdanów	.	.	4,0	3,7	5,7	0,1	.	6,7	.	.	.	.	.	.	.	.	4,0	.	.	.	.	.	2,4	.	.	1,5	.	.	0,5	.	28,6
68	Iwonicz-Zdrój	.	1,8	6,8	0,5	0,6	0,3	0,7	4,8	5,7	.	.	.	.	.	.	.	2,2	.	1,6	.	.	0,8	.	.	2,7	3,7	.	.	3,9	0,1	36,2
69	Leśka	.	.	6,9	.	0,4	0,1	2,4	6,5	7,6	.	.	.	.	.	.	0,3	5,3	.	1,0	.	0,1	.	.	.	6,1	1,7	.	.	5,7	0,2	43,3

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	-	-	-	.	0,1	.	.	0,4	.	3,1	0,1	.	.	3,2	0,4	0,1	.	.	.	.	.	2,1	.	.	.	.	.	.	1,1	.	.	10,6
2	Kołobrzeg	.	0,8	.	.	0,1	.	.	.	.	1,2	.	.	.	5,8	.	3,7	.	.	.	0,5	.	.	.	.	.	1,7	0,6	.	.	.	.	14,4
3	Świnoujście	.	-	-	.	.	1,3	0,1	0,5	.	1,0	.	.	3,0	6,3	.	0,4	.	.	.	.	0,8	.	.	0,1	.	1,4	1,2	1,3	.	.	.	17,4
4	Resko	-	.	.	.	.	0,5	.	.	.	1,6	.	.	4,4	5,4	.	3,4	.	.	.	0,1	.	.	.	.	.	.	1,0	.	.	.	-	16,4
5	Szczecinek	.	.	.	.	-	0,2	1,1	.	.	2,2	.	.	2,5	5,2	.	4,1	.	.	.	.	.	.	.	.	.	.	0,7	.	.	.	-	16,0
6	Chojnice	.	.	.	.	-	0,6	0,7	0,6	0,1	1,6	0,3	.	1,7	4,2	.	4,0	.	.	.	.	.	.	.	.	.	.	0,3	0,2	1,9	.	.	16,2
7	Hel	.	0,3	.	0,4	3,0	.	.	2,4	.	0,9	2,8	.	2,2	0,1	.	2,6	1,5	.	0,1	0,7	.	.	.	1,5	.	.	2,8	0,5	3,0	.	0,4	25,2
8	Gdynia	.	2,6	.	4,1	.	1,0	.	2,6	.	0,6	1,8	0,2	0,1	.	.	.	.	.	1,2	.	.	1,4	.	.	.	2,9	.	3,1	.	.	.	21,6
9	Świbno	.	0,1	.	.	1,5	0,1	1,2	2,1	.	0,3	0,7	.	0,6	0,1	.	1,9	.	.	.	0,6	.	.	.	2,7	.	.	2,3	1,8	.	.	0,7	16,7
10	Stare Pole	.	0,3	1,0	.	1,6	0,3	0,3	1,7	0,1	1,6	0,9	.	2,1	0,9	0,5	2,7	.	.	.	.	.	.	.	2,3	.	.	2,2	.	3,3	.	0,6	22,4
11	Radostowo	.	0,5	0,1	.	.	0,2	1,6	1,8	.	0,8	0,5	.	0,2	4,8	.	3,7	0,3	.	.	.	0,1	.	.	1,2	.	.	0,6	0,4	2,5	.	.	19,3
12	Prabuty	.	.	.	.	.	0,9	0,9	0,8	.	.	.	.	0,6	1,8	.	0,4	1,4	.	.	.	.	.	.	1,1	.	.	.	.	1,9	.	3,5	13,2
13	Bydgoszcz, IMiUZ	.	.	1,2	1,9	.	1,1	0,7	0,1	0,8	2,2	0,3	2,8	1,4	3,6	.	.	.	.	.	.	.	.	.	.	.	.	0,5	.	1,0	.	.	17,6
14	Suwałki	.	.	.	.	.	1,0	0,5	.	.	.	0,7	.	0,6	2,1	3,9	1,1	4,4	.	.	0,2	.	.	4,2	.	.	.	1,7	.	0,8	.	.	21,2
15	Mikołajki	2,1	.	0,0	.	1,0	1,3	0,3	.	.	.	.	.	-	4,0	1,7	0,7	5,5	.	.	.	.	.	.	.	0,4	.	0,9	.	2,4	0,2	.	-
16	Biebrza	0,8	.	.	.	.	2,5	2,4	.	0,2	.	.	.		3,1	2,2	.	3,7	.	.	0,4	.	.	0,9	.	.	.	1,0	.	0,1	.	.	17,3
17	Białystok	3,3	.	.	.	.	2,2	0,6	.	0,6	.	.	.	.	4,1	0,1	.	3,1	.	.	1,2	.	0,0	0,0	.	.	.	0,1	.	.	0,2	-	15,5
18	Gorzów Wlkp.	.	.	.	1,4	.	.	.	0,0	.	3,2	.		1,2	5,8		0,6	.	.	.	0,2	.	.	1,9	.	.	.	3,3	.	3,0	.	0,0	20,6
19	Przebędowo	.	.	.	1,9	.	1,1	0,6	0,0	1,4	3,1	0,4	0,5	3,9	5,7	.	4,7	.	.	.	1,4	.	.	4,0	.	.	.	1,8	.	3,1	0,1	-	33,7
20	Przybroda	.	.	.	4,1	.	1,6	0,5	.	2,4	3,2	0,2	0,1	2,8	5,5	.	4,3	.	.	.	2,0	.	.	4,1	.	0,2	.	2,6	.	3,8	-	0,3	37,7
21	Poznań-Ławica	.	0,1	.	2,1	.	2,3	0,6	0,1	2,3	3,3	0,5	.	3,1	4,7		3,5	.	.	.	1,4	.	.	2,5	.	.	.	2,0	.	3,4	0,4	0,1	32,4
22	Plewiska	.	.	2,2	.	0,1	2,7	0,4	.	2,4	3,7	0,6	.	2,2	4,8	.	2,9	.	.	.	1,1	.	0,1	3,4	.	.	.	2,4	.	3,7	0,2	.	32,9
23	Kórnik	.	.	.	1,0	0,2	2,5	.	.	2,1	3,3	.	.	3,2	4,3	.	3,2	.	.	.	.	.	0,4	1,3	.	.	.	3,0	.	3,1	.	.	27,6
24	Oborniki Śl.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
25	Laskowice Oławskie	1,4	.	1,4	3,3	0,7	5,6	.	.	3,1	0,1	2,9	.	.	1,6			.	.		1,6	.	3,3	1,1	.	.	.	3,5	0,4	1,6	0,0	.	31,6
26	Ciechocinek	.	.	2,1	1,3	.	2,1	1,2	.	0,1	1,8	.	1,9	1,6	5,2	.			.	.	0,1	.	.	.	3,3	.	1,7	.	.	1,1	.	.	23,5
27	Więcławice	.	.	2,3	0,8	,	2,0	1,4	0,3	0,4	2,4	0,1	1,5	3,4	5,1		.		.	.	0,6	.	.	.	1,6	.	.	1,1	.	1,2	.	.	24,2
28	Legionowo	0,7	.	.	.	.	3,9	0,7	.	0,5	.	0,1	.	0,4	3,6		0,8	.	.	.	3,6	.	.	.	.	0,2		0,8	.	.	0,5	.	15,8
29	Warszawa-Bielany	0,2	.	.	.	.	2,6	.			.		.	.	.		.	.		.	0,0	.	.	.	.	0,1	.	.	.	.	.	.	2,9
30	Warszawa, Min.Kom.	0,1	.	.	.	.	3,7	.			.			0,4	2,9			.	.	.	1,9	.	.	.	.	0,2	.	0,1	.	.	0,0	.	9,3
31	Międzylesie	1,7	.	.	.	0,2	4,5	0,1	.	2,1	.	0,1		0,3	2,7	.			.	.	3,5	.	.	.	.	0,9	.	1,5	.	.	0,4	.	18,0
32	Brwinów	0,9	.	.	.	0,4	4,9	0,0	.	1,4	.	0,6		0,1	3,1	.		0,1	.		1,8	.		0,5	.	0,2	.	1,3	.	.	0,3	.	15,6
33	Świder	1,1	.	.	.	0,2	4,7	.	.	2,8	.	0,1	.	1,2	2,6		.	.		.	2,8	.	.	.	.	1,7	.	1,2	.	0,3	0,9	.	19,6
34	Topola-Błonie	.	.	0,6	1,7	0,1	4,4	1,9		2,2	.	0,2	2,9	1,9	3,7		1,2	.			1,7	.	.	1,1	.	.	.	3,3	.	0,4	.	.	27,3
35	Młochów	.	.	.	0,4	0,2	4,6	.		2,3		.			0,8	.	.	.	.	.	2,8	.	0,2	.	0,0	0,3	1,7	.	.	.	.	.	13,3
36	Skierniewice	1,4	0,1	.	0,9	1,0	5,4	0,1	.	2,3	.	0,5	2,4	0,1	2,7	.			.		3,8	.		.	5,4	0,1	-	1,8	.	.	0,3	0,2	28,5
37	Belsk	.	0,7	0,5	.	0,3	0,3	4,3			2,6	.	.	1,7	0,1	2,2		1,6	.	.	.	4,1	.	.	.	0,2	0,2	,	1,7	.	0,4	0,2	21,1
38	Łódź-Lublinek	.	0,1	0,2	1,1	0,7	5,2	.	.	3,6	.	0,1	0,2	1,3	0,3	.	3,9	.	.	.	4,7	.	.	.	1,8	.	.	2,5	.	0,5	.	0,2	26,4
39	Kalisz	.	0,1	2,5	2,9	0,7	4,1	0,3	0,0	4,7	0,5	3,4	0,0	5,1	2,7	.	4,3	.	.	0,0	1,7	.	.	1,6	.	0,0	.	4,2	.	1,7	0,0	0,0	40,5
40	Wieluń	.	.	0,2	1,0	0,7	6,3	.		2,5	.	0,7	0,1	4,2	0,1	.				.	0,7	.	.	.	.	.	.	2,8	.	1,0	0,1	0,1	20,5
41	Szepietowo	3,4	.	.	.	.	2,6	1,7		0,5	.				4,0	0,7	0,2	3,1	.		2,6	.	.	4,4	.	0,4	.	.	.	1,5	1,3	.	26,4
42	Białowieża	3,8	.	0,1	.	0,3	3,0	.		0,5	.				1,5		.	4,1			1,8	.	.	1,7	.	.	.	1,1	.	-	0,5	-	18,4
43	Terespol	5,0	0,4	0,8	.	0,9	3,7	.		3,3	.	.	.	0,0	4,9		1,6	2,3	.		3,2	.	.	3,3	.	.	.	2,7	.	0,3	1,0	0,1	33,5
44	Sobieszyn	4,8	.	.	0,1	1,1	3,7	.	.	3,8	.	0,1		.	0,9	.		.	.	.	0,3	.	0,1	.	.	0,9	0,6	3,6	.	0,2	1,8	.	22,0
45	Puławy	4,0	-	.	0,1	1,2	4,3	.	-	3,0	.	.		0,5	0,2			.			.	.	.	.	.	1,3	.	3,4	.	0,2	1,6	-	19,8
46	Chełm	5,7	5,3	0,6	1,1	4,5	0,8	.	.	2,7	.	.	.	0,0	0,9		.	.	.	.	0,2	.	.	3,3	.	.	.	4,8	.	3,4	3,7	0,1	37,3
47	Szczawno-Zdrój	.	2,1	0,5	2,8	1,0	2,2	.	.	3,0	0,5	3,0	0,3	.	3,3	0,3	.	.	.	0,2	.	.	4,9	3,4	0,9	2,0	0,1	2,0	1,9	5,0	0,1	1,8	41,3
48	Śnieżka	.	-	.		.	.	-	.	.	.	.	2,1	0,5	5,5	.	0,2	.			.	.	3,7	5,4	.	.	.	.	3,8	6,3	0,5	.	28,0
49	Opole	.	.	0,1	3,5	1,0	5,7	.		4,2	.	1,5	.	.	.	1,2	.	.		.	.	.	0,9	.	.	.	0,1	2,3	0,1	2,2	0,4	0,1	23,3
50	Kudowa-Zdrój	.	.	0,4	.	2,1	0,3	.	.	6,6		1,8	0,8		3,4	.		.		.	.	1,4	.	3,5	.	0,3	.	4,2	1,2	2,5	3,1	.	31,6
51	Polanica-Zdrój	.	0,2	0,9	1,2		3,2			5,5	.	3,5	2,1	.	2,7	.	.	.	.	.	.	.	3,1	.	.	1,7	0,2	2,5	0,0	5,6	1,5	.	33,9
52	Skroniów	5,5	1,2	.	1,7	1,5	5,0	0,1	0,3	4,5	.	0,9	0,2	4,0	.	0,1	.	.	.	.	.	.	.	.	.	1,0	1,9	3,5	.	2,0	2,6	0,2	36,0
53	Świerklaniec	0,6	.	.	1,8	0,6	3,5		.	3,0	.	2,0	.	0,2	0,1	.		.	.		.	.	.	.	.	1,5	2,2	1,8	.	1,4	2,4	0,1	21,2
54	Kraków, Obs. Astr. UJ	4,3	3,3	.	2,6	2,3	3,3	-	.	3,4	.	0,3	.	.	0,2	.		.	.	.	.	0,9	.	.	0,5	2,9	3,2	1,9	.	2,6	3,0	0,4	35,1
55	Cieszyn	0,6	0,2		1,8	0,3	3,5	0,0	.	4,5	.	0,4			.	.	.	.	.	.	.	.	.	2,6	.	0,4	.	0,1	.	3,9	0,8	0,5	19,4
56	Istebna-Kubalonka	0,2	.	.	.	.	0,3	0,1	.	3,8	.	0,7	.	.		.	.	.	.	.	.	.	.	5,5	.	1,5	.	2,4	0,1	3,9	2,1	.	20,6
57	Babka	4,0	2,1	.	2,0	3,4	2,6			4,2	.	.		1,3		.	0,8	.	0,3	.	.	.	0,2	.	.	5,0	2,7	5,0	0,1	0,7	2,6	0,9	37,9
58	Jabłonka	2,7	1,2	.	0,3	1,1	2,2	.	.	4,2	.	0,3	.	1,8	0,4	.	.	.	.	.	.	.	.	.	0,8	5,6	0,5	4,1	0,1	1,7	2,9	.	29,9
59	Krynica	7,1	4,8	.	.	4,1	1,1	.	.	3,6	.		.	4,7	.	.	.	.		.	.	.	.	.	.	.	2,6	3,2	2,2	.	3,8	1,3	40,5
60	Krynica-Góra Park.	5,8	5,7	.	.	4,8	1,3	.	.	3,5	.	.	.	4,8	.	.	.	.	.	.	.	.	.	.	0,1	.	3,2	4,9	-	5,2	4,6	0,5	44,2
61	Muszyna	6,3	4,0	.	.	2,1	1,9	.	.	2,8	.	.	.	4,5	.	.	.	.	.	.	.	.	.	.	0,2	,	2,7	3,8	.	.	2,2	3,3	33,8
62	Zakopane	0,4	6,0	.	0,6	0,7	0,6	.	.	5,0	.	.		3,8	.	.	3,2	0,0	0,1	.	.	.	.	.	1,1	5,0	2,5	3,0	.	5,0	0,9	1,6	39,7
63	Gubałówka	2,4	5,6	.	1,7	2,7	1,4	.	.	5,4	.	.	.	3,8	.	.	3,5	0,2	0,4	.	0,1	.	.	.	1,4	5,4	3,5	4,5	.	4,3	1,9	1,3	49,3
64	Hala Gąsienicowa	.	5,5	.	.	.	.	.	.	3,3	.	.	.	4,5	.	.	2,7	.	.	.	.	.	.	0,9	2,4	3,9	2,6	1,8	.	3,8	0,7	0,4	35,7
65	Kasprowy Wierch	.	0,6	.	0,0	.	0,9	.	.	6,6	.	.	.	2,4	.	.	4,6	0,1	.	.	.	.	.	4,2	1,3	3,0	2,8	2,4	.	3,8	2,3	0,8	40,8
66	Werbkowice	5,4	6,5	1,9	1,7	5,7	0,8	.	.	3,5	.	.	.	0,5	2,0	.	.	.	.	.	.	.	.	6,7	.	0,4	.	5,6	.	4,3	6,3	.	51,3
67	Zdanów	5,0	.	.	1,8	3,4	3,1	.	2,1	.	.	.	.	0,7	.	.	4,9	.	.	.	.	.	.	.	.	3,2	4,4	,	0,1	1,9	4,3	.	34,9
68	Iwonicz-Zdrój	2,6	3,0	0,1	0,1	3,3	.	.	.	0,2	.	.	.	0,9	.	.	.	.	.	.	.	.	.	.	.	1,8	0,4	4,3	.	2,2	3,8	.	22,7
69	Lesko	6,1	6,4	0,4	3,2	4,8	.	.	.	3,4	.	.	.	0,8	.	0,5	.	.	1,7	.	0,0	.	.	.	.	.	1,0	6,[illegible]	.	2,5	5,7	.	42,[illegible]

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STACJE METEOROLOGICZNE
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1965
Stacje podstawowe – Stations principales
" pomocnicze – " auxiliares
0 20 40 60 80 100 km

WYDAWNICTWA KOMUNIKACJI i ŁĄCZNOŚCI — WARSZAWA 1974

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