PAŃSTWOWY INSTYTUT HYDROLOGICZNO-METEOROLOGICZNY

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ANNUAIRES

ROCZNIK METEOROLOGICZNY

1961

ANNUAIRE MÉTÉOROLOGIQUE

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PRZEDMOWA

W stosunku do *Roczników meteorologicznych* za lata ubiegłe niniejszy rocznik 1961 został uzupełniony danymi o prężności pary wodnej. Wykaz symboli meteorologicznych uaktualniono według *Międzynarodowego atlasu chmur* z r. 1956. Materiał obserwacyjny zestawiono w czterech tablicach.

Tablica pierwsza zawiera codzienne spostrzeżenia meteorologiczne, w tablicy drugiej podano wyniki miesięczne i roczne spostrzeżeń meteorologicznych, w tablicy trzeciej zestawiono daty ostatnich przymrozków wiosennych i pierwszych przymrozków jesiennych (według spostrzeżeń dokonywanych w klatce meteorologicznej — 2 m nad powierzchnią gruntu), zaś w tablicy czwartej — dzienne i miesięczne sumy godzin usłonecznienia.

Uzupełnienie stanowią objaśnienia, wykaz symboli meteorologicznych, skorowidz i mapa rozmieszczenia stacji.

Rocznik został opracowany w Zakładzie Roczników i Monografii Meteorologicznych Państwowego Instytutu Hydrologiczno-Meteorologicznego pod kierownictwem i redakcją mgr Feliksa Janiszewskiego.

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PRÉFACE

L'*Annuaire Météorologique 1961* diffère des annuaires précédants par le fait de l'introduction des données sur la tension de vapeur. L'index des symboles météorologiques a été rendu actuel en se basant sur *l'Atlas International des Nuages*, ed. 1956. Le matériel d'observations y est recueilli sous forme de quatre tableaux.

La première table englobe des observations journalières des stations météorologiques, la seconde cite des résultats mensuels et annuels des observations météorologiques, la troisième table présente les dates des dernières gelées printanières ainsi que les premières gelées d'automne d'après les observations executées dans l'abri météorologique (2 mètres au dessus de la surface du sol), la quatrième table — valeurs diurnes et mensuels d'insolation en heures.

Les explications, le relevé des symboles météorologiques, répertoire et la carte de la dislocation des stations constituent le complément à ces tables.

L'Annuaire a été élaboré dans la Section des Annuaires et des Monographies Météorologiques de l'Institut Hydrologique et Météorologique d'État sous la direction et redaction de M. Feliks Janiszewski.

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OBJAŚNIENIA

Użyte w niniejszym roczniku symbole mają następujące znaczenie:

φ — szerokość geograficzna.

λ — długość geograficzna.

H_s — wysokość terenu ogródka meteorologicznego nad średnim poziomem morza.

H_b — wysokość barometru nad średnim poziomem morza.

Dla stacji posiadających barometry H_s i H_b zostały wyznaczne za pomocą niwelacji, dla pozostałych stacji H_s wyznaczono z mapy topograficznej.

h_w — wysokość wiatromierza nad powierzchnią gruntu.

m — w połączeniu z literowym symbolem elementu oznacza wartość średnią miesięczną (np. U_m oznacza średnią miesięczną wilgotność względną).

P — ciśnienie atmosferyczne w milibarach, zredukowane do 0° i do ciężkości normalnej.

$P_{o,m}$ — wartość średnia miesięczna ciśnienia atmosferycznego, sprowadzona do średniego poziomu morza.

T — temperatura w °C.

Temperaturę wyznaczano za pomocą termometrów umieszczonych w klatce meteorologicznej typu angielskiego na wysokości 2 m nad powierzchnią gruntu. Skrajne dobowe wartości temperatur odnoszą się do okresu od III obserwacji dnia poprzedniego do III obserwacji danego dnia.

$\overline{Max}$ — średnia miesięczna z wartości temperatur maksymalnych dobowych.

$\overline{Min}$ — średnia miesięczna z wartości temperatur minimalnych dobowych.

e — prężność pary wodnej w milibarach

U — wilgotność względna w procentach.

Δ — niedosyt wilgotności w milibarach.

N — zachmurzenie w skali 11-stopniowej (przy tym 0 oznacza niebo bezchmurne, zaś 10 — niebo całkowicie pokryte chmurami).

W tablicy I rocznika obok wartości zachmurzenia podane są za pomocą symboli również dane o zjawiskach zaobserwowanych podczas obserwacji terminowych.

D — kierunek wiatru.

v — prędkość wiatru w m/sek.

n_D — częstotliwość występowania poszczególnych kierunków wiatru.

v_{mD} — średnia prędkość wiatru wg kierunków.

Obserwacje nad wiatrem były dokonywane (z nielicznymi wyjątkami) przy użyciu wiatromierzy Wilda.

R — wysokość opadu w milimetrach.

Wysokość opadu odnosi się do okresu od I (porannej) obserwacji jednego dnia do I obserwacji dnia następnego i jest podawana pod datą dnia poprzedniego. Obserwacje te były dokonywane za pomocą deszczomierzy Hellmanna o powierzchni otworu 200 cm², umieszczonych na wysokości 1 m nad powierzchnią gruntu, z wyjątkiem części stacji górskich, położonych powyżej 500 m nad poziomem morza, gdzie używa się deszczomierzy typu górskiego, mających powierzchnię otworu 500 cm² i umieszczonych na wysokości 1,5 m nad powierzchnią gruntu.

V — widzialność z II terminu obserwacji, wyrażona w następującej skali międzynarodowej:

0 — przedmioty są niewidoczne już z odległości mniejszej od 50 m;

1 — przedmioty są widoczne z odległości 50 m, lecz niewidoczne z odległości 200 m;

2 — przedmioty są widoczne z odległości 200 m, lecz niewidoczne z odległości 500 m;

3 — przedmioty są widoczne z odległości 500 m, lecz niewidoczne z odległości 1 km;

4 — przedmioty są widoczne z odległości 1 km, lecz niewidoczne z odległości 2 km;

5 — przedmioty są widoczne z odległości 2 km, lecz niewidoczne z odległości 4 km;

6 — przedmioty są widoczne z odległości 4 km, lecz niewidoczne z odległości 10 km;

7 — przedmioty są widoczne z odległości 10 km, lecz niewidoczne z odległości 20 km;

8 — przedmioty są widoczne z odległości 20 km, lecz niewidoczne z odległości 50 km;

9 — przedmioty są widoczne z odległości 50 km i więcej.

h — grubość pokrywy śnieżnej w centymetrach wg obserwacji dokonywanych w I terminie.

pł. — śnieg w płatach.

Usłonecznienie — w godzinach. Obserwacji dokonywano za pomocą heliografów Campbell—Stokes'a.

n — liczba dni z poszczególnymi zjawiskami.

Za dzień z mgłą przyjęto w niniejszym roczniku dzień, w którym to zjawisko powodowało zmniejszenie się widzialności poniżej 1 km.

Za dni pogodne uważa się takie, w których średnia wartość zachmurzenia wyznaczona z trzech terminów jest mniejsza od 2.0, zaś za dni pochmurne — w których wartość ta jest większa od 8.0.

I, II, III — terminy obserwacji (7^h, 13^h i 21^h średniego miejscowego czasu słonecznego).

Dies — średnia dobowa, obliczona dla temperatury według wzoru:

śr. = 1/4 (I + II + 2 × III), a dla pozostałych elementów

śr. = 1/3 (I + II + III).

Natężenie zjawisk oznaczono za pomocą małych cyferek: ^{0}, ^{1} albo ^{2} umieszczonych z prawej strony u góry odpowiedniego symbolu („^{0}" oznacza zjawisko o natężeniu słabym, „^{1}" o natężeniu umiarkowanym, a „^{2}" o natężeniu silnym; w przypadku mgły cyferki te oznaczają odpowiednio: mgłę umiarkowaną, mgłę gęstą i mgłę bardzo gęstą).

Do oznaczania czasu obok godzin i minut użyto następujących symboli:

n — czas od III obserwacji dnia poprzedniego do I obserwacji dnia danego,

na — czas od północy do I obserwacji dnia danego,

a — czas między I a II terminem obserwacji,

p — czas między II a III terminem obserwacji,

np — czas od III obserwacji do północy.

Przerwy w czasie trwania zjawiska oznaczono wielokropkiem (...) lub skrótem „z prz.".

Kropka (.) postawiona na miejscu wartości liczbowej oznacza brak zjawiska, kreska (—) zaś brak danych, wartości wątpliwe podano ze znakiem zapytania (?), wartości oszacowane podano w nawiasach.

NOTE EXPLICATIVE

Les symboles employés dans le présent annuaire signifient ce qui suit:

φ — latitude géographique.

λ — longitude géographique.

H_s — hauteur du terrain du jardin météorologique, au-dessus du niveau moyen de la mer.

H_b — hauteur du baromètre au-dessus du niveau de la mer.

Pour les stations disposant d'un baromètre H_s et H_b, ces données ont été déterminées à l'aide de nivellement, pour les autres stations H_s elles l'ont été d'après la carte topograhique.

h_w — hauteur d'une girouette au-dessus du sol.

m — joint à une lettre-symbole de l'élément, indique la valeur mensuelle moyenne (p.e. U_m — indique la valeur mensuelle moyenne de l'humidité relative).

P — pression atmosphérique en millibars, réduite à 0° et à la gravité normale.

$P_{o,m}$ — moyenne d'une valeur mensuelle de la pression atmosphérique réduite au niveau moyen de la mer.

T — température en C°.

La température a été mesurée à l'aide de thermomètres installés dans un abri météorologique du type anglais à une hauteur de 2 mètres au-dessus du sol. Les températures diurnes extrêmes se rapportent à une période partant de la III-ème observation du jour précédent à la III-ème observation du jour donné.

$\overline{\text{Max}}$ — valeur mensuelle moyenne des maxima des températures diurnes.

$\overline{\text{Min}}$ — valeur mensuelle moyenne des valeurs minima des températures diurnes.

e — tension de vapeur en millibars.

U — humidité relative en %.

Δ — déficit de l'humidité en millibars.

N — nébulosité en échelle 11° (0 signifie ciel serein, 10 — ciel entièrement couvert par les nuages). Dans la table I de l'annuaire, à côté des valeurs de la nébulosité, figurent aussi les données se rapportant aux phénomènes remarqués au cours des observations normales, et consignées à l'aide de symboles.

D — direction du vent.

v — vitesse du vent en m/sec.

n_D — fréquence de l'apparition des directions du vent.

v_{mD} — vitesse moyenne du vent selon la direction. Les observations sur le vent ont été faites (avec quelques exceptions) à l'aide d'une girouette, modèle Wild.

R — hauteur de la précipitation en mm. L'hauteur de la précipitation se rapporte à la période comprise entre la première observation (matinale) d'un jour et l'observation du jour suivant. Elle se trouve inscrite à la date du jour précédent. Ces observations ont été faites à l'aide de pluviomètres, modèle Hellmann, dont la superficie de l'ouverture mesure 200 cm², placés à 1 m au-dessus du sol, à l'exception, toutefois, de certaines stations de montagne, situées à une hauteur qui dépasse 500 m au-dessus du niveau de la mer, où l'on emploie des pluviomètres, de type montagnard, à orifice mesurant 500 cm² et placés à une hauter de 1,5 m au-dessus du sol.

V — visibilité à l'heure de la II-ème observation, exprimée d'après l'échelle internationale:

0 — les objets sont invisibles déjà à une distance inférieure à 50 m;

1 — les objets sont visibles à 50 m, mais invisibles à 200 m de distance;

2 — les objets sont visibles à 200 m, mais invisibles à 500 m de distance;

3 — les objets sont visibles à 500 m, mais invisibles à 1000 m de distance;

4 — les objets sont visibles à 1 km, mais invisibles à 2 km;

5 — les objets sont visibles à 2 km, mais invisibles à 4 km;

6 — les objets sont visibles à 4 km, mais invisibles à 10 km;

7 — les objets sont visibles à 10 km, mais invisibles à 20 km;

8 — les objets sont visibles à 20 km, mais invisibles à 50 km;

9 — les objets sont visibles à partir de 50 km de distance.

h — épaisseur de la couche de neige en centimètres selon l'observation enregistrée dans le premier délai.

pł. — neige éparse.

Insolation — en heures. Les observations effectuées à l'aide d'héliographes Campbell — Stokes.

n — nombre des jours avec phénomènes particuliers.

Dans le présent annuaire, on entend par jour avec brouillard le jour où ce phénomène entraine une diminution de visibilité au-dessous de 1 km.

Dans le présent annuaire, on entend par jours sereins les jours dont la valeur moyenne de nébulosité, résultant de trois delais, est inférieure à 2.0 et par jours couverts les jours où cette valeur est supérieure à 8.0.

I, II, III — les délais d'observations (7^h, 13^h et 21^h du temps moyen solaire local).

Dies — moyenne diurne, calculée pour la température d'après la formule:

$m = 1/4\ (I + II + 2 \times III)$, et pour les autres éléments $m = 1/3\ (I + II + III)$.

L'intensité du phénomène est marquée en petits chiffres: ^{0}, ^{1} ou ^{2} placés du coté droit en haut du symbole respectif: („^{0}" indique le phénomène dont l'intensité est faible, „^{1}" modérée et „^{2}" forte; en cas de brouillard modéré, brouillard épais et brouillard très épais).

Pour indiquer le temps (à part les heures et les minutes), on a utilisé les symboles suivants:

n — le temps écoulé depuis la III-ème observation du jour précédent jusqu'à la I-ère observation du jour donné.

na — le temps écoulé depuis minuit jusqu'à l'observation du jour donné,

a — intervalle de temps entre la I-ère et la II-ème observation,

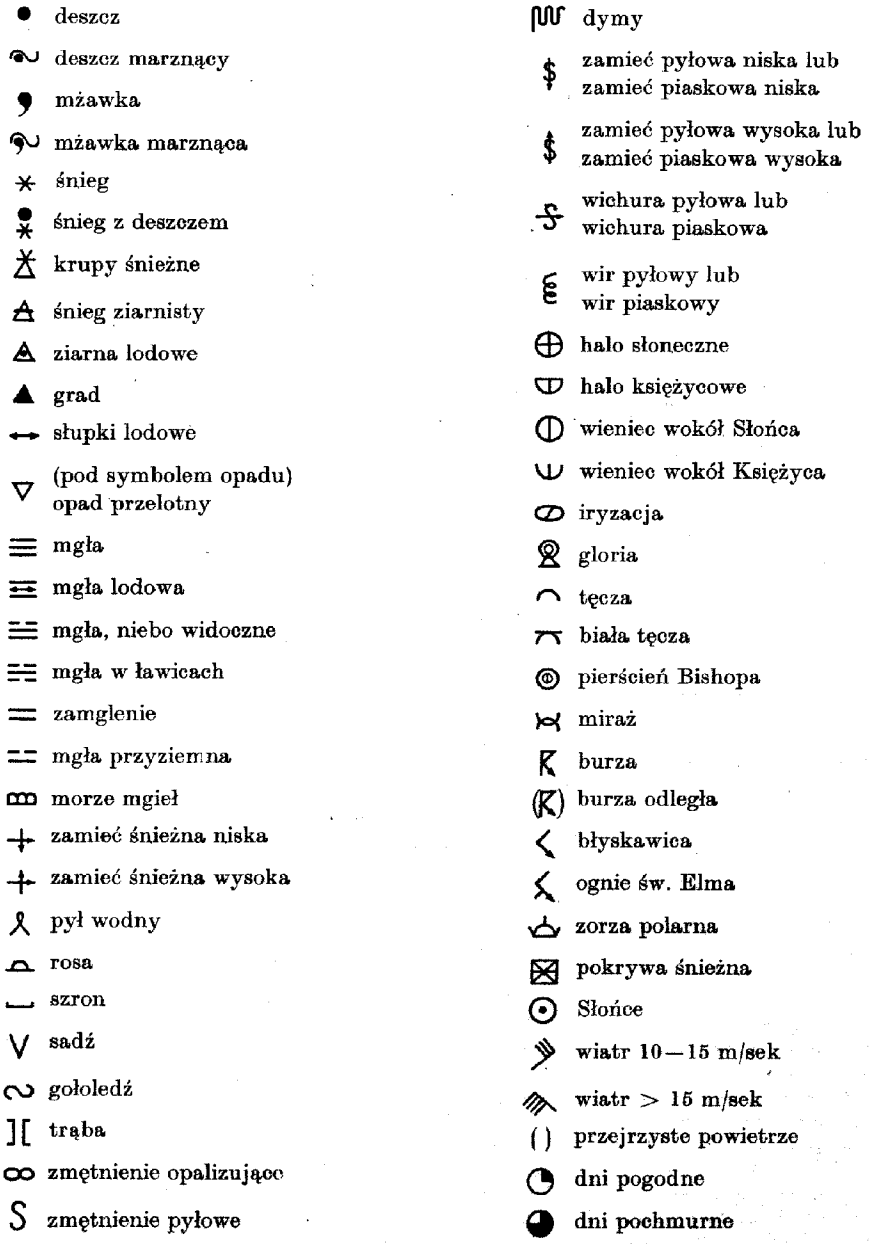
p — intervalle de temps entre la II-ème et la III-ème observation,

np — intervalle de temps entre la III-ème observation et minuit.

Les intervalles de temps, dans la durée d'un phénomène sont indiqués par des points de suspension (...) ou par une abréviation „z prz.".

Un point (.) mis à la place d'une valeur numérique marque l'absence d'un phénomène; un trait d'union (—) indique le défaut de données; un point d'interrogation (?) signale les valeurs douteuses; les parenthèses enferment les valeurs éstimées.

WYKAZ SYMBOLI METEOROLOGICZNYCH



1961

ALFABETYCZNY SPIS STACJI METEOROLOGICZNYCH
LISTE ALPHABÉTIQUE DES STATIONS MÉTÉOROLOGIQUES

Nr	Stacja — Station	Miesiące Mois	Strona — Page				φ N	λ E Gr.	H_s	H_b	Dorzecze Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV [2]					
1	Aleksandrowice	I—XII	—	368	412	—	49°48′	19°00′	398	403.4	Wisła
2	Antołówka [1]	I—XII	—	404	412	—	49 18	19 59	918	—	Dunajec
3	Augustów	I—XII	—	234	412	—	53 51	23 00	130	—	Biebrza
4	Babia Góra [1]	I—XII	—	382	412	—	49 35	19 31	1180	—	Skawa
5	Baligród	I—XII	—	402	412	—	49 20	22 17	450	—	San
6	Bartoszyce	I—XII	—	218	412	—	54 15	20 48	60	—	Łyna
7	Barwinek	I—XII	—	398	412	—	49 26	21 41	420	—	Wisłoka
8	Bełsk	I—XII	—	292	412	418(37)	51 50	20 48	180	—	Wisła
9	Biała Podlaska	I—XII	—	288	412	—	52 01	23 08	145	—	Bug
10	Białowieża	I—XII	—	264	412	418(42)	52 42	23 51	163	163.7	Narew
11	Biały Kościół	I—XII	—	354	412	—	50 10	19 50	400	—	Wisła
12	Białystok	I—XII	—	254	412	418(17)	53 07	23 11	139	140.8	Narew
13	Biebrza	I—XII	—	240	412	418(16)	53 39	22 36	117	—	Biebrza
14	Biecz	I—XII	—	374	412	—	49 44	21 15	260	—	Wisłoka
15	Bielsk Podlaski	I—XII	—	262	412	—	52 47	23 11	145	—	Narew
16	Bieruń Stary	I—XII	—	358	412	—	50 05	19 05	236	239.0	Wisła
17	Bieruto wice	I—XII	—	326	412	—	50 47	15 44	860	—	Bóbr
18	Biłgoraj	I—XII	—	336	412	—	50 33	22 43	190	—	San
19	Biroza	I—XII	—	376	412	—	49 41	22 29	300	—	San
20	Biskupiec	I—XII	—	234	412	—	53 52	20 57	160	—	Łyna
21	Bochnia-Chodenice	I—XII	—	364	412	—	49 59	20 24	200	—	Raba
22	Bodzentyn	I—XII	—	318	412	—	50 57	20 57	270	—	Kamienna
23	Borusowa	I—XII	—	350	412	—	50 17	20 47	170	—	Wisła
24	Brwinów	I—XII	—	284	412	418(32)	52 08	20 43	96	98.0	Bzura
25	Brzegi Dolne	I—XII	—	394	412	—	49 27	22 38	420	—	Strwiąż
26	Brzezna	I—XII	—	382	412	—	49 36	20 37	320	—	Dunajec
27	Bukowina Tatrzańska [1]	I—XII	—	400	412	—	49 21	20 07	880	—	Dunajec
28	Busko — Zdrój	I—XII	—	340	412	—	50 27	20 43	225	—	Nida
29	Bydgoszcz	I—XII	—	254	412	—	53 07	17 58	70	70.5	Brda
30	Bydgoszcz, IMiUZ	I—XII	—	254	412	418(13)	53 08	18 01	47	—	Brda
31	Bystrzyca Kłodzka	I—XII	—	346	412	—	50 18	16 39	370	—	Nysa Kłodzka
32	Bytom	I—XII	—	344	412	—	50 21	18 55	300	—	Przemsza
33	Chełm Lubelski	I—XII	—	314	412	418(46)	51 07	23 30	208	209.6	Bug
34	Chodzież	I—XII	—	258	412	—	52 59	16 54	100	—	Noteć
35	Chojnice	I—XII	50	238	412	418(6)	53 42	17 33	172	177.2	Brda
36	Chorzelów	I—XII	—	346	412	—	50 21	21 27	170	—	Wisła
37	Ciechocinek	I—XII	—	260	412	418(26)	52 53	18 48	44	—	Wisła
38	Cieplice Śl. — Zdrój	I—XII	—	322	412	—	50 52	15 41	345	—	Bóbr
39	Cieszyn	I—XII	—	372	412	418(55)	49 45	18 38	300	—	Olza
40	Cieszyn — Bobrek	I—XII	—	372	412	—	49 45	18 39	300	—	Olza
41	Ciężkowice	I—XII	—	370	412	—	49 47	20 58	280	—	Dunajec
42	Czarna Dąbrówka	I—XII	—	216	412	—	54 21	17 34	120	—	Łupawa
43	Czarniecka Góra	I—XII	—	312	412	—	51 08	20 31	256	—	Pilica
44	Czarny Dunajec	I—XII	—	392	412	—	49 27	19 51	676	—	Dunajec
45	Czernichów	I—XII	—	362	412	—	50 00	19 41	218	—	Wisła
46	Częstochowa	I—XII	—	326	412	—	50 49	19 06	261	262.7	Warta
47	Czorsztyn	I—XII	—	394	412	—	49 26	20 19	496	—	Dunajec
48	Czorsztyn — Nadzamcze [1]	I—XII	—	394	412	—	49 26	20 20	650	—	Dunajec
49	Darłowo	I—XII	—	212	412	—	54 27	16 23	3	—	Wieprza
50	Dębica	I—XII	—	360	412	—	50 03	21 24	205	—	Wisłoka
51	Dobrogoszcz	I—XII	—	328	412	—	50 46	17 01	175	—	Oława
52	Dolina Chochołowska [1]	I—XII	—	404	412	—	49 15	19 49	1028	—	Dunajec
53	Dolina Pięciu Stawów	I—XII	—	408	412	—	49 13	20 03	1668	—	Dunajec
54	Drawno	I—XII	—	252	412	—	53 13	15 46	82	—	Drawa
55	Duszniki — Zdrój [1]	I—XII	—	342	412	—	50 24	16 24	540	—	Nysa Kłodzka
56	Dynów	I—XII	—	370	412	—	49 48	22 14	276	—	San
57	Dziwnów	I—XII	—	228	412	—	54 01	14 44	7	7.1	Przymorze
58	Elbląg	I—XII	—	222	412	—	54 10	19 26	38	42.8	Elbląska
59	Felin	I—XII	—	310	412	—	51 14	22 38	215	—	Wieprz
60	Garlica Murowana	I—XII	—	354	412	—	50 09	19 56	270	—	Prądnik
61	Gdańsk — Nowy Port	I—XII	—	212	412	—	54 24	18 40	7	—	Wisła

[1] Podane w roczniku wysokości opadów otrzymano za pomocą deszczomierza o powierzchni otworu 500 cm².
[2] W nawiasach podane są numery, pod którymi figurują stacje w tabl. IV.

Nr	Stacja – Station	Miesiące Mois	Strona – Page				φ N	λ E Gr.	H_s	H_b	Dorzecze Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV [2]					
62	Gdańsk – Siedlce	I–XII	–	214	412	–	54°21′	18°36′	72	–	Wisła
63	Gdańsk – Wrzeszcz	I–XII	14	214	412	–	54 23	18 36	13	12.4	Wisła
64	Gdynia	I–XII	–	212	412	418(8)	54 31	18 34	2	14.5	Przymorze
65	Giżycko	I–XII	–	228	412	–	54 03	21 46	132	–	Węgorapa
66	Gliwice	I–XII	–	348	412	–	50 18	18 40	220	–	Kłodnica
67	Głodowo	I–XII	–	262	412	–	52 50	19 15	129	–	Wisła
68	Głogów	I–XII	–	296	412	–	51 39	16 06	112	–	Odra
69	Głubczyce	I–XII	–	352	412	–	50 12	17 49	290	–	Odra
70	Głuchołazy	I–XII	–	348	412	–	50 18	17 23	344	–	Nysa Kłodzka
71	Gniezno	I–XII	–	270	412	–	52 33	17 36	110	–	Wełna
72	Goczałkowice	I–XII	–	366	412	–	49 57	18 55	260	–	Wisła
73	Gołdap	I–XII	–	218	412	–	54 19	22 19	150	–	Węgorapa
74	Gorzów Wlkp.	I–XII	–	262	412	418(18)	52 44	15 15	65	59.7	Warta
75	Gorzyń	I–XII	–	268	412	–	52 34	15 54	60	–	Warta
76	Goszyce	I–XII	–	352	412	–	50 11	20 08	260	–	Wisła
77	Góra Św. Anny	I–XII	–	338	412	–	50 27	18 10	370	–	Odra
78	Grabowiec	VII–XII	–	314	412	–	51 06	21 23	210	–	Wisła
79	Grabownica	IV–XII	–	302	412	–	51 28	17 27	119	–	Barycz
80	Grodków	I–XII	–	332	412	–	50 41	17 23	176	–	Nysa Kłodzka
81	Grudziądz	I–XII	–	244	412	–	53 30	18 46	40	–	Wisła
82	Gryfice	I–XII	–	232	412	–	53 55	15 13	40	–	Rega
83	Gubałówka [1]	I–XII	–	402	412	418(63)	49 18	19 56	1000	–	Dunajec
84	Hala Gąsienicowa [1]	I–XII	–	406	412	418(64)	49 15	20 00	1520	1520.8	Dunajec
85	Hala Ornak [1]	I–XII	–	406	412	–	49 14	19 51	1110	–	Dunajec
86	Hel	I–XII	–	210	412	418(7)	54 36	18 49	1	2.6	Przymorze
87	Hopowo	I–XII	–	218	412	–	54 16	18 14	220	–	Radunia
88	Horyniec	I–XII	–	352	412	–	50 11	23 21	240	–	San
89	Inowrocław	I–XII	–	262	412	–	52 48	18 14	90	–	Noteć
90	Istebna – Kubalonka [1]	I–XII	–	380	412	418(56)	49 36	18 54	800	–	Olza
91	Istebna – Stecówka [1]	I–XII	–	380	412	–	49 35	18 57	750	–	Wisła
92	Istebna-Zaolzie [1]	I–XII	–	380	412	–	49 34	18 56	580	–	Olza
93	Iwonicz – Zdrój	I–XII	–	384	412	418(68)	49 34	21 48	410	403.3	Wisłok
94	Jabłonka [1]	I–XII	–	390	412	418(58)	49 28	19 43	620	–	Czarna Orawa
95	Jakubowice	I–XII	–	360	412	–	50 01	17 51	319	–	Odra
96	Janów Lubelski	I–XII	–	330	412	–	50 43	22 25	230	–	San
97	Jarosław	I–XII	–	362	412	–	50 01	22 42	204	–	San
98	Jasło	I–XII	–	374	412	–	49 44	21 28	240	–	Wisłoka
99	Jastrowie	VIII–XII	–	246	412	–	53 25	16 48	120	–	Gwda
100	Jastrzębie-Zdrój	I–XII	–	364	412	–	49 57	18 34	227	–	Olza
101	Jaworzyna Krynicka [1]	I–XII	–	398	413	–	49 25	20 54	995	–	Poprad
102	Jazy	I–XII	–	232	413	–	53 53	23 22	120	–	Niemen
103	Jelenia Góra	I–XII	122	320	413	–	50 54	15 48	342	343.9	Bóbr
104	Jeziory	I–XII	–	278	413	–	52 16	16 48	84	–	Warta
105	Kalisz	I–XII	–	294	413	418(39)	51 44	18 05	140	143.1	Prosna
106	Kamienica	I–XII	–	384	413	–	49 35	20 21	460	–	Dunajec
107	Kamienica Królewska	I–XII	–	214	413	–	54 23	17 54	160	–	Łupawa
108	Kamień Krajeński	I–XII	–	244	413	–	53 32	17 31	124	–	Brda
109	Karpacz [1]	I–XII	–	328	413	–	50 46	15 45	700	708.0	Bóbr
110	Kartuzy	I–XII	–	216	413	–	54 20	18 12	220	–	Radunia
111	Kasprowy Wierch [1]	I–XII	194	406	413	418(65)	49 14	19 59	1991	1988.8	Dunajec
112	Katowice	I–XII	–	350	413	–	50 14	19 02	284	284.1	Przemsza
113	Kętrzyn	I–XII	–	224	413	–	54 06	21 21	110	107.4	Łyna
114	Kielce	I–XII	–	322	413	–	50 51	20 37	268	270.1	Nida
115	Kisielnica	I–XII	–	250	413	–	53 15	22 07	140	–	Narew
116	Kliczmok [1]	I–XII	–	372	413	–	49 44	19 00	1010	–	Wisła
117	Kłodzko	I–XII	–	340	413	–	50 26	16 39	316	320.1	Nysa Kłodzka
118	Kobylec	I–XII	–	260	413	–	52 51	17 12	90	–	Wełna
119	Kolbuszowa	I–XII	–	352	413	–	50 14	21 47	208	–	Wisła
120	Kolno	I–XII	–	246	413	–	53 25	21 56	128	–	Pisa
121	Koło	I–XII	–	282	413	–	52 12	18 38	95	–	Warta
122	Kołobrzeg	I–XII	–	220	413	418(2)	54 11	15 35	3	5.4	Parsęta
123	Kołobrzeg-Wydma	I–XII	–	220	413	–	54 11	15 33	5	–	Parsęta
124	Kołuda Wielka	I–XII	–	264	413	–	52 44	18 09	85	–	Noteć
125	Komańcza	I–XII	–	402	413	–	49 20	22 04	470	–	San
126	Kończewice	I–XII	–	252	413	–	53 11	18 33	94	–	Wisła
127	Kopna Góra	I–XII	–	252	413	–	53 15	23 29	160	–	Narew
128	Korfantów	VII–XII	–	336	413	–	50 29	17 36	200	–	Nysa Kłodzka
129	Koszalin	I–XII	–	220	413	–	54 12	16 10	33	33.9	Przymorze
130	Kościerzyna	I–XII	–	222	413	–	54 08	17 58	180	–	Wierzyca
131	Kórnik	I–XII	–	280	413	418(23)	52 15	17 06	77	–	Warta

Nr	Stacja — Station	Miesiące Mois	Strona — Page				φ N	λ E Gr.	H_s	H_b	Dorzecze Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV [2]					
132	Kraków-Chełm	I—XII	—	358	413	—	50°04′	19°51′	225	—	Rudawa
133	Kraków-Czyżyny	I—XII	—	358	413	—	50 05	20 01	213	213.4	Prądnik
134	Kraków — Nowa Huta	I—XII	—	360	413	—	50 04	20 05	195	—	Wisła
135	Kraków, Obserw. Astr. UJ	I—XII	158	358	413	418(54)	50 04	19 58	206	219.8	Wisła
136	Krasnystaw	I—XII	—	316	413	—	50 59	23 10	190	—	Wieprz
137	Kraśnik Dolny	I—XII	—	308	413	—	51 17	15 36	180	—	Bóbr
138	Krosno	I—XII	—	376	413	—	49 41	21 45	282	—	Wisłok
139	Krościenko	I—XII	—	392	413	—	49 27	20 25	440	—	Dunajec
140	Krynica [1]	I—XII	—	396	413	418(59)	49 26	20 58	613	609.6	Poprad
141	Krynica Góra Parkowa [1]	I—XII	—	396	413	418(60)	49 25	20 58	740	—	Poprad
142	Krynica Morska	I—XII	—	214	413	—	54 23	19 27	4	—	Zalew Wiślany
143	Krzemień	I—XII	—	270	413	—	52 33	22 30	111	—	Bug
144	Krzyż	I—XII	—	258	413	—	52 53	16 01	31	—	Noteć
145	Kudowa-Zdrój	I—XII	—	338	413	418(50)	50 27	16 16	385	—	Łaba
146	Kuźnice [1]	I—XII	—	404	413	—	49 16	19 59	1023	—	Dunajec
147	Kwidzyń	I—XII	—	236	413	—	53 44	18 55	15	—	Wisła
148	Laskowice Oławskie	I—XII	—	316	413	418(25)	51 03	17 21	135	—	Widawa
149	Lądek-Zdrój [1]	I—XII	—	344	413	—	50 21	16 53	460	—	Nysa Kłodzka
150	Legionowo	I—XII	—	274	413	418(28)	52 24	20 58	93	103.7	Wisła
151	Legnica	I—XII	—	310	413	—	51 13	16 10	121	126.3	Kaczawa
152	Lesko	I—XII	—	392	413	418(69)	49 28	22 20	386	—	San
153	Leskowiec [1]	I—XII	—	368	413	—	49 48	19 27	870	—	Skawa
154	Leszno-Strzyżewice	I—XII	—	290	413	—	51 50	16 32	91	—	Barycz
155	Leżajsk	I—XII	—	350	413	—	50 15	22 26	190	—	San
156	Lębork	I—XII	—	210	413	—	54 33	17 45	18	21.8	Łeba
157	Libertów	I—XII	—	364	413	—	49 58	19 53	320	—	Wisła
158	Lidzbark	I—XII	—	250	413	—	53 16	19 50	150	—	Drwęca
159	Lidzbark Warmiński	I—XII	—	224	413	—	54 08	20 36	90	—	Łyna
160	Limanowa	I—XII	—	376	413	—	49 42	20 25	440	—	Dunajec
161	Lipki	I—XII	—	250	413	—	53 21	14 58	30	—	Odra
162	Lipowa	I—XII	—	324	413	—	50 50	21 27	245	—	Wisła
163	Lubaczów	I—XII	—	354	413	—	50 09	23 08	214	—	San
164	Lublin	I—XII	—	308	413	—	51 14	22 34	171	176.7	Wieprz
165	Lubliniec	I—XII	—	332	413	—	50 40	18 41	256	—	Mała Panew
166	Luboń Wielki [1]	I—XII	—	378	413	—	49 39	19 59	1023	—	Raba
167	Łagiewniki	I—XII	—	264	413	—	52 40	18 19	80	—	Noteć
168	Łącko	I—XII	—	386	413	—	49 33	20 26	360	—	Dunajec
169	Łeba	I—XII	—	208	413	—	54 46	17 34	2	—	Łeba
170	Łosice	I—XII	—	282	413	—	52 12	22 43	153	—	Bug
171	Łowicz	I—XII	—	286	413	—	52 07	19 56	95	—	Bzura
172	Łódź-Lublinek	I—XII	98	296	413	418(38)	51 44	19 24	187	187.7	Ner
173	Łódź-Ruda Pabianicka	I—XII	—	296	413	—	51 42	19 27	181	—	Ner
174	Łysa Polana [1]	I—XII	—	404	413	—	49 16	20 07	988	—	Dunajec
175	Maków Podhalański	I—XII	—	374	413	—	49 44	19 40	350	—	Skawa
176	Malbork	I—XII	—	228	413	—	54 02	19 02	20	—	Wisła
177	Maniowy [1]	I—XII	—	390	413	—	49 28	20 15	520	—	Dunajec
178	Miastko	I—XII	—	230	413	—	54 00	16 58	145	—	Wieprza
179	Miechów	I—XII	—	344	413	—	50 22	20 02	292	—	Wisła
180	Mielec	I—XII	—	348	413	—	50 18	21 27	168	170.2	Wisłoka
181	Międzybrodzie Bialskie	I—XII	—	370	413	—	49 47	19 12	320	—	Soła
182	Międzylesie	I—XII	—	—	—	418(31)	52 12	21 11	90	—	Wisła
183	Międzyzdroje	I—XII	—	230	413	418(3)	53 56	14 27	10	—	Przymorze
184	Mikołajki	I—XII	—	234	413	418(15)	53 47	21 35	127	131.1	Pisa
185	Mława	I—XII	—	254	413	—	53 07	20 22	141	145.8	Wkra
186	Młochów	I—XII	—	288	413	418(35)	52 03	20 47	141	—	Bzura
187	Morskie Oko [1]	I—XII	—	408	413	—	49 12	20 04	1400	—	Dunajec
188	Motycz	I—XII	—	308	413	—	51 15	22 25	213	—	Wieprz
189	Mszana Dolna	I—XII	—	378	413	—	49 40	20 05	410	—	Raba
190	Muszyna	I—XII	—	400	413	418(61)	49 21	20 53	445	447.1	Poprad
191	Myczkowce	I—XII	—	398	413	—	49 26	22 25	410	—	San
192	Myślenice	I—XII	—	368	413	—	49 49	19 56	295	—	Raba
193	Myślenickie Turnie [1]	I—XII	—	406	413	—	49 15	19 59	1360	—	Dunajec
194	Nałęczów	I—XII	—	308	413	—	51 17	22 13	166	—	Wisła
195	Namysłów	I—XII	—	314	413	—	51 05	17 43	151	—	Widawa
196	Nidzica	I—XII	—	248	413	—	53 22	20 25	170	—	Wkra
197	Niepokalanów	I—XII	—	282	413	—	52 12	20 25	92	—	Bzura
198	Nisko	I—XII	—	336	413	—	50 31	22 09	164	—	San
199	Nowa Wieś	I—XII	—	302	413	—	51 27	22 45	179	—	Wieprz
200	Nowe Miasto n. P.	I—XII	—	298	413	—	51 37	20 35	155	—	Pilica

Nr	Stacja—Station	Miesiące Mois	Strona—Page				φ N	λ E Gr.	H_s	H_b	Dorzecze Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV [2]					
201	Nowogard	I—XII	—	240	413	—	53°40′	15°07′	60	—	Przymorze
202	Nowy Dwór Gdański	I—XII	—	220	413	—	54 13	19 08	0	—	Wisła
203	Nowy Dwór Mazowiecki	I—XII	—	272	413	—	52 26	20 43	70	—	Wisła
204	Nowy Sącz	I—XII	—	380	413	—	49 37	20 42	292	295.4	Dunajec
205	Nowy Targ [1]	I—XII	—	390	414	—	49 29	20 02	600	—	Dunajec
206	Nur	I—XII	—	266	414	—	52 40	22 19	110	—	Bug
207	Obidowa [1]	I—XII	—	386	414	—	49 33	19 58	800	—	Raba
208	Oborniki Śląskie	I—XII	—	306	414	418(24)	51 18	16 55	180	—	Odra
209	Ochaby	I—XII	—	366	414	—	49 51	18 46	270	—	Wisła
210	Olecko	I—XII	—	228	414	—	54 03	22 30	181	177.7	Biebrza
211	Olesno	I—XII	—	320	414	—	50 53	18 25	238	—	Stobrawa
212	Olkusz	I—XII	—	348	414	—	50 17	19 34	360	—	Przemsza
213	Olsztyn-Dajtki	I—XII	38	236	414	—	53 46	20 25	133	135.4	Łyna
214	Oława-Zwierzyniec	I—XII	—	318	414	—	50 57	17 18	137	—	Odra
215	Opole	I—XII	—	332	414	418(49)	50 40	17 58	176	177.9	Odra
216	Opole Lubelskie	I—XII	—	312	414	—	51 09	21 59	149	—	Wisła
217	Orneta	IX—XII	—	224	414	—	54 07	20 07	70	—	Pasłęka
218	Osiny	I—XII	—	302	414	—	51 28	22 04	153	—	Wisła
219	Osowiec	I—XII	—	244	414	—	53 29	22 39	110	—	Biebrza
220	Ostrołęka	I—XII	—	256	414	—	53 05	21 34	95	96.3	Narew
221	Ostroszowice	I—XII	—	334	414	—	50 39	16 38	375	—	Nysa Kłodzka
222	Ostrowy	I—XII	—	276	414	—	52 18	19 10	120	—	Bzura
223	Ostróda	I—XII	—	240	414	—	53 42	19 58	106	—	Drwęca
224	Ostrów Wlkp.	I—XII	—	298	414	—	51 39	17 49	126	—	Prosna
225	Ostrzeszów	I—XII	—	304	414	—	51 26	17 56	198	—	Prosna
226	Otmuchów	I—XII	—	338	414	—	50 28	17 10	211	—	Nysa Kłodzka
227	Ożańsk	I—XII	—	362	414	—	50 01	22 35	250	—	San
228	Paproć	I—XII	—	274	414	—	52 19	16 08	75	—	Obra
229	Pętkowo	I—XII	—	282	414	—	52 12	17 15	86	—	Warta
230	Pilsko [1]	I—XII	—	388	414	—	49 32	19 19	1270	—	Soła
231	Piotrków Trybunalski	I—XII	—	304	414	—	51 25	19 42	200	—	Pilica
232	Pisz	I—XII	—	242	414	—	53 38	21 48	118	—	Pisa
233	Piwniczna	I—XII	—	396	414	—	49 26	20 42	380	—	Poprad
234	Pleszew	VI—XII	—	290	414	—	51 54	17 47	120	—	Prosna
235	Plewiska	I—XII	—	—	—	418(22)	52 22	16 48	80	—	Warta
236	Płock-Radziwie	I—XII	—	270	414	—	52 32	19 40	63	63.8	Wisła
237	Płocko	I—XII	—	222	414	—	54 09	16 50	125	—	Wieprza
238	Polanica-Zdrój	I—XII	—	342	414	418(51)	50 24	16 30	400	—	Nysa Kłodzka
239	Połczyn-Zdrój	I—XII	—	236	414	—	53 46	16 06	50	—	Parsęta
240	Poraj	III—XII	—	208	414	—	54 40	17 36	5	—	Łeba
241	Porąbka	I—XII	—	368	414	—	49 49	19 13	315	—	Soła
242	Poronin [1]	I—XII	—	400	414	—	49 20	20 02	800	—	Dunajec
243	Poświętne	I—XII	—	266	414	—	52 38	20 23	101	—	Wkra
244	Poznań-Ławica	I—XII	74	272	414	418(21)	52 25	16 50	86	92.1	Warta
245	Poznań-Sołacz	I—XI	—	272	414	—	52 26	16 54	71	—	Warta
246	Prabuty	I—XII	—	238	414	418(12)	53 44	19 13	98	—	Wisła
247	Prudnik	I—XII	—	346	414	—	50 19	17 34	265	—	Odra
248	Przasnysz	I—XII	—	256	414	—	53 01	20 53	120	—	Narew
249	Przebędowo	I—XII	—	268	414	418(19)	52 35	17 01	82	—	Warta
250	Przedbórz	I—XII	—	316	414	—	51 05	19 53	235	—	Pilica
251	Przehyba	I—XII	—	392	414	—	49 28	20 34	1175	—	Poprad
252	Przelewice	I—XII	—	256	414	—	53 06	15 05	60	—	Odra
253	Przemyśl	I—XII	170	370	414	—	49 48	22 46	237	238.9	San
254	Przybroda	I—XII	—	270	414	418(20)	52 31	16 40	88	—	Warta
255	Pszczela Wola	I—XII	—	314	414	—	51 07	22 31	195	—	Wieprz
256	Pszczyna	I—XII	—	362	414	—	50 00	18 55	270	—	Wisła
257	Ptaszkowa [1]	I—XII	—	382	414	—	49 36	20 53	522	—	Dunajec
258	Ptusza	I—VIII	—	248	414	—	53 22	16 48	95	—	Brda
259	Puck	I—XII	—	208	414	—	54 43	18 25	1	—	Przymorze
260	Puczniew	I—XII	—	294	414	—	51 47	19 05	142	—	Ner
261	Puławy	I—XII	—	306	414	418(45)	51 25	21 58	142	155.2	Wisła
262	Pułtusk	I—XII	—	264	414	—	52 42	21 06	80	—	Narew
263	Raba Wyżna [1]	I—XII	—	384	414	—	49 34	19 53	600	—	Raba
264	Rabka	I—XII	—	382	414	418(57)	49 36	19 58	512	552.5	Raba
265	Racibórz	I—XII	—	356	414	—	50 05	18 13	189	192.6	Odra
266	Radom	I—XII	—	304	414	—	51 25	21 07	178	—	Wisła
267	Radostowo	I—XII	—	230	414	418(11)	53 59	18 45	40	—	Wisła
268	Radzyń Podlaski	I—XII	—	292	414	—	51 48	22 38	151	—	Wieprz
269	Reguły	I—XII	—	284	414	—	52 10	20 51	98	—	Bzura

Nr	Stacja — Station	Miesiące Mois	Strona — Page				φ N	λ E Gr.	H_s	H_b	Dorzecze Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV [2]					
270	Resko	I—XII	—	234	414	418(4)	53°46′	15°25′	55	56.2	Rega
271	Rosnowo	I—XII	—	226	414	—	54 04	16 18	62	—	Parsęta
272	Rozewie	I—XII	—	208	414	—	54 50	18 20	54	—	Przymorze
273	Rożnów	I—XII	—	372	414	—	49 46	20 41	300	—	Dunajec
274	Różanystok	I—XII	—	242	414	—	53 38	23 24	160	—	Biebrza
275	Rybnik	I—XII	—	356	414	—	50 06	18 33	243	—	Odra
276	Rymanów-Zdrój	I—XII	—	388	414	—	49 33	21 51	360	—	Wisłok
277	Rzeszów-Jasionka	I—XII	—	356	414	—	50 06	22 03	200	201.7	Wisłok
278	Sandomierz	I—XII	146	332	414	—	50 41	21 45	202	200.3	Wisła
279	Sanok	I—XII	—	384	414	—	49 34	22 12	314	—	San
280	Sejny	I—XII	—	226	414	—	54 06	23 21	130	—	Niemen
281	Siedlce	I—XII	—	284	414	—	52 11	22 16	146	149.1	Liwiec
282	Siejnik	I—XII	—	230	414	—	54 01	22 29	170	—	Biebrza
283	Sielec	I—XII	—	346	414	—	50 19	20 25	202	—	Wisła
284	Siemianice	I—XII	—	310	414	—	51 11	18 09	182	—	Prosna
285	Siemiatycze	I—XII	—	274	414	—	52 26	22 52	145	—	Bug
286	Sieniawa [1]	I—XII	—	388	414	—	49 32	19 55	578	—	Raba
287	Sieradz	I—XII	—	298	414	—	51 36	18 44	137	—	Warta
288	Silniczka	VII—XII	—	318	414	—	50 55	19 46	215	—	Pilica
289	Sinołęka	I—XII	—	280	414	—	52 13	21 55	160	—	Liwiec
290	Skierniewice	I—XII	—	290	414	418(36)	51 58	20 10	128	129.5	Bzura
291	Skroniów	I—XII	—	334	414	418(52)	50 38	20 16	256	—	Nida
292	Słubice	I—XII	—	274	414	—	52 21	14 36	20	22.2	Odra
293	Słupca	I—XII	—	276	414	—	52 17	17 52	90	—	Warta
294	Słupia Nowa	I—XII	—	322	414	—	50 52	21 05	307	—	Kamienna
295	Słupsk	I—XII	—	212	414	—	54 28	17 01	16	—	Słupia
296	Smolice	I—XII	—	296	414	—	51 42	17 11	107	—	Barycz
297	Sobieszyn	I—XII	—	300	414	418(44)	51 36	22 10	159	—	Wieprz
298	Sobótka	I—XII	—	320	414	—	50 54	16 45	204	—	Bystrzyca
299	Sokołowsko [1]	I—XII	—	330	414	—	50 41	16 14	570	—	Nysa Kłodzka
300	Sokółka	I—XII	—	248	414	—	53 24	23 30	180	—	Narew
301	Stańcowa [1]	I—XII	—	386	414	—	49 33	19 32	850	—	Czarna Orawa
302	Stare Pole	I—XII	—	226	414	418(10)	54 04	19 13	3	—	Wisła
303	Stary Sącz	I—XII	—	388	414	—	49 33	20 39	320	—	Poprad
304	Staszów	I—XII	—	334	414	—	50 34	21 10	193	—	Wisła
305	Strzelna	I—XII	—	292	414	—	51 49	19 54	194	—	Bzura
306	Strzyżów	I—XII	—	324	414	—	50 51	24 02	185	—	Bug
307	Suchedniów	I—XII	—	316	414	—	51 03	20 50	272	—	Kamienna
308	Sulejów	V—XII	—	306	414	—	51 22	19 53	186	—	Pilica
309	Suwałki	I—XII	26	224	414	418(14)	54 06	22 57	165	169.6	Niemen
310	Szamotuły	I—XII	—	266	415	—	52 37	16 34	70	—	Warta
311	Szczawnica	I—XII	—	394	415	—	49 26	20 29	500	—	Dunajec
312	Szczawno-Zdrój	I—XII	—	326	415	418(47)	50 48	16 16	415	—	Bystrzyca
313	Szczecin-Dąbie	I—XII	62	246	415	—	53 24	14 37	1	6.9	Odra
314	Szczecin-Niebuszewo	I—XII	—	244	415	—	53 28	14 33	69	—	Odra
315	Szczecinek	I—XII	—	238	415	418(5)	53 43	16 41	137	142.6	Gwda
316	Szczekociny	VII—XII	—	334	415	—	50 38	19 49	262	—	Pilica
317	Szczerców	I—XII	—	306	415	—	51 20	19 07	160	—	Warta
318	Szczuczyn	I—XII	—	242	415	—	53 34	22 17	130	—	Biebrza
319	Szczytno	I—XII	—	242	415	—	53 34	21 02	144	—	Narew
320	Szepietowo	I—XII	—	260	415	418(41)	52 51	22 33	150	—	Bug
321	Szklarska Poręba [1]	I—XII	—	324	415	—	50 50	15 32	640	—	Bóbr
322	Szprotawa	I—XII	—	300	415	—	51 34	15 32	122	—	Bóbr
323	Szrenica [1]	I—XII	—	326	415	—	50 48	15 31	1323	1363.6	Bóbr
324	Śliwice	I—XII	—	238	415	—	53 43	18 11	115	—	Czarna Woda
325	Śnieżka [1]	I—XII	134	328	415	418(48)	50 44	15 44	1603	1610.6	Bóbr
326	Śrem	I—XII	—	286	415	—	52 05	17 01	85	—	Warta
327	Świbno	I—XII	—	216	415	—	54 20	18 56	3	—	Wisła
328	Świbno-Ujście Wisły	I—III	—	216	415	418(9)	54 21	18 56	5	—	Wisła
329	Świder	I—XII	—	286	415	418(33)	52 07	21 15	94	—	Świder
330	Świdnica	I—XII	—	322	415	—	50 51	16 29	230	—	Bystrzyca
331	Świdwin	I—XII	—	236	415	—	53 46	15 46	94	—	Rega
332	Świebodzin	I—XII	—	280	415	—	52 15	15 32	78	—	Odra
333	Świeradów — Zdrój	I—XII	—	320	415	—	50 54	15 20	549	—	Bóbr
334	Świerklaniec	I—XII	—	340	415	418(53)	50 26	18 57	284	—	Przemsza
335	Święty Krzyż	I—XII	—	324	415	—	50 51	21 03	575	—	Kamienna
336	Świnoujście	I—XII	—	232	415	—	53 55	14 14	6	—	Przymorze
337	Tarnobrzeg	I—XII	—	336	415	—	50 34	21 40	175	—	Wisła
338	Tarnogród	I—XII	—	344	415	—	50 22	22 45	217	—	San

Nr	Stacja — Station	Miesiące Mois	Strona — Page				φ N	λ E Gr.	H_s	H_b	Dorzecze Bassin
			Tabl. I	Tabl. II	Tabl. III	Tabl. IV [2])					
339	Tarnów	I—XII	—	360	415	—	50°02′	20°59′	209	209.1	Dunajec
340	Tczew	I—XII	—	226	415	—	54 05	18 48	10	—	Wisła
341	Terespol	I—XII	—	288	415	418(43)	52 05	23 37	133	135.0	Bug
342	Tęgoborze	I—XII	—	374	415	—	49 43	20 39	272	—	Dunajec
343	Tolkmicko	I—XII	—	218	415	—	54 19	19 32	1	—	Zalew Wiślany
344	Tomaszów Lubelski	I—XII	—	340	415	—	50 27	23 25	273	—	Bug
345	Topola-Błonie	I—XII	—	286	415	418(34)	52 05	19 11	109	—	Ner
346	Toruń-Wrzosy	I—XII	—	256	415	—	53 03	18 35	69	70.2	Wisła
347	Trzcińsko-Zdrój	I—XII	—	258	415	—	52 58	14 36	60	—	Odra
348	Trzebiechów	I—XII	—	288	415	—	52 01	15 44	55	—	Obrzyca
349	Trzebież	I—XII	—	240	415	—	53 40	14 31	1	—	Zalew Szczeciński
350	Trzebinia	I—XII	—	354	415	—	50 10	19 28	320	—	Wisła
351	Trzemeszno	I—XII	—	268	415	—	52 34	17 49	105	—	Noteć
352	Turbacz [1])	I—III, V—XII	—	386	415	—	49 33	20 07	1308	—	Raba
353	Tychy	I—XII	—	356	415	—	50 08	18 59	280	—	Wisła
354	Ustka	I—XII	—	210	415	418(1)	54 35	16 52	6	8.1	Słupia
355	Ustka-Wydma	I—XII	—	210	415	—	54 35	16 52	7	—	Słupia
356	Ustrzyki Górne	I—XII	—	408	415	—	49 07	22 40	650	—	San
357	Wadowice	I—XII	—	366	415	—	49 53	19 31	260	—	Skawa
358	Wałcz	I—XII	—	250	415	—	53 17	16 28	111	113.8	Gwda
359	Warka	I—XII	—	294	415	—	51 47	21 12	120	—	Pilica
360	Warszawa-Bielany	I—XII	86	276	415	418(29)	52 17	20 58	101	104.7	Wisła
361	Warszawa, Inst. Geogr. UW	I—XII	—	276	415	—	52 14	21 01	108	—	Wisła
362	Warszawa, Min. Kom.	I—XII	—	—	—	418(30)	52 13	21 01	—	—	Wisła
363	Warszawa, Obserw. Astr.	I—XII	—	278	415	—	52 13	21 02	110	114.8	Wisła
364	Warszawa-Okęcie	I—XII	—	278	415	—	52 09	20 59	106	106.9	Wisła
365	Warszawa, St. Pomp Rz.	I—XII	—	278	415	—	52 13	21 03	85	—	Wisła
366	Wądolki Borowe	I—XII	—	258	415	—	52 57	22 13	130	—	Narew
367	Werbkowice	I—XII	—	328	415	418(66)	50 45	23 46	204	—	Bug
368	Wielichowo	I—XII	—	284	415	—	52 07	16 21	65	—	Obra
369	Wieliczka	I—XII	—	364	415	—	50 00	20 03	225	—	Wisła
370	Wieliszew	I—XII	—	272	415	—	52 27	20 58	78	—	Bug
371	Wieluń	I—XII	—	310	415	418(40)	51 13	18 35	195	198.4	Warta
372	Wieniec-Zdrój	I—XII	—	266	415	—	52 40	19 00	82	—	Wisła
373	Wierzchowo	I—XII	—	246	415	—	53 27	16 06	140	—	Drawa
374	Więcławice	I—XII	—	260	415	418(27)	52 51	18 19	90	—	Noteć
375	Wińsko	I—XII	—	302	415	—	51 28	16 37	180	—	Barycz
376	Wirty	I—XII	—	232	415	—	53 54	18 23	121	—	Wierzyca
377	Wisła	I—XII	—	378	415	—	49 39	18 52	430	—	Wisła
378	Wisznice	I—XII	—	294	415	—	51 47	23 13	152	—	Bug
379	Witów [1])	I—XII	—	400	415	—	49 20	19 50	835	—	Dunajec
380	Włodawa I	I—V	—	300	415	—	51 33	23 33	174	—	Bug
381	Włodawa II	I—XII	—	300	415	—	51 33	23 33	175	175.9	Bug
382	Wojcieszów Górny	I—XII	—	318	415	—	50 57	15 55	358	—	Kaczawa
383	Wolbrom	I—XII	—	342	415	—	50 23	19 45	373	—	Przemsza
384	Wrocław-Gądów Mały	I—XII	110	312	415	—	51 08	16 59	116	118.6	Odra
385	Wyrzysk	I—XII	—	252	415	—	53 09	17 16	90	—	Noteć
386	Wysowa [1])	I—XII	—	396	415	—	49 26	21 11	525	—	Wisłoka
387	Wyszków	I—XII	—	268	415	—	52 35	21 27	96	—	Bug
388	Zakopane [1])	I—XII	182	402	415	418(62)	49 18	19 57	844	838.2	Dunajec
389	Zakrzów	I—XII	—	350	415	—	50 16	18 09	217	—	Odra
390	Zamość	I—XII	—	330	415	—	50 44	23 15	219	218.8	Wieprz
391	Zawiercie	I—VIII	—	338	415	—	50 29	19 26	335	—	Warta
392	Zawodzie	I—XII	—	248	415	—	53 23	21 24	122	—	Narew
393	Zawoja [1])	I—XII	—	378	415	—	49 37	19 31	670	—	Skawa
394	Zawołocze	I—XII	—	304	415	—	51 26	23 34	165	—	Bug
395	Ząbkowice	I—XII	—	342	415	—	50 22	19 17	314	—	Przemsza
396	Zbąszyń	I—XII	—	280	415	—	52 15	15 56	57	—	Odra
397	Zdanów	I—XII	—	330	415	418(67)	50 43	21 33	236	—	Wisła
398	Zgorzelec	I—XII	—	312	415	—	51 08	15 02	219	217.9	Nysa Łużycka
399	Zielona Góra	I—XII	—	290	415	—	51 56	15 30	180	173.8	Odra
400	Zwardoń [1])	I—XII	—	390	415	—	49 30	18 59	690	—	Soła
401	Żarnowa	I—XII	—	366	415	—	49 52	21 50	256	—	Wisłok
402	Żary	I—XII	—	298	415	—	51 38	15 08	162	—	Bóbr
403	Żegiestów-Zdrój	I—XII	—	398	415	—	49 22	20 49	440	—	Poprad
404	Żelechów	I—XII	—	292	415	—	51 49	21 54	175	—	Wisła
405	Żelisławki	I—XII	—	222	415	—	54 10	18 39	68	—	Wisła
406	Żywiec-Sporysz	I—XII	—	376	415	—	49 41	19 13	360	—	Soła

1961

TABLICA I

SPOSTRZEŻENIA CODZIENNE STACJI METEOROLOGICZNYCH

OBSERVATIONS DIURNES DE STATIONS MÉTÉOROLOGIQUES

1. Gdańsk-Wrzeszcz
2. Suwałki
3. Olsztyn-Dajtki
4. Chojnice
5. Szczecin-Dąbie
6. Poznań-Ławica
7. Warszawa-Bielany
8. Łódź-Lublinek
9. Wrocław-Gądów Mały
10. Jelenia Góra
11. Śnieżka, Obserwatorium Wysokogórskie
12. Sandomierz
13. Kraków, Obserwatorium Astronomiczne UJ
14. Przemyśl
15. Zakopane
16. Kasprowy Wierch, Obserwatorium Wysokogórskie

Gdańsk - Wrzeszcz — φ = 54°23' — λ = 18°36' — Styczeń - Janvier 1961

Dni	Ciśnienie P = 900 + I	II	III	Dies	Temperatura T I	II	III	Dies	Max	Min	Wilgotność względna U I	II	III	Dies	Niedosyt wilgotności Δ I	II	III	Dies	Zachmurzenie i pogoda N,w I	II	III	Kierunek i prędkość wiatru D,v I	II	III
1	111.5	112.5	113.7	112.6	-1.0	0.2	1.4	0.5	1.4	-2.8	93	92	96	94	0.4	0.5	0.3	0.4	10 *	10 *	10	SSE 1	C 0	C 0
2	113.3	111.7	109.4	111.5	-0.8	0.8	0.5	0.2	1.8	-1.0	91	90	92	91	0.5	0.7	0.5	0.6	1	9	10	C 0	SSE 3	SSE 2
3	101.7	98.1	96.6	98.8	0.1	0.8	2.0	1.2	2.1	-0.6	90	86	87	88	0.7	0.9	0.9	0.8	10	10 *	10	SE 6	SSE 7	SSE 5
4	98.6	95.5	96.6	96.9	1.5	2.6	4.0	3.0	4.1	1.2	94	93	93	93	0.4	0.6	0.5	0.5	10	9	4	SSE 3	S 2	S 4
5	102.1	102.8	103.7	102.9	2.0	3.1	2.6	2.6	4.6	1.1	93	86	84	88	0.6	1.0	1.2	0.9	10	9	10	C 0	C 0	SSW 6
6	108.3	110.3	108.6	109.1	2.6	2.8	0.6	1.6	3.3	0.2	86	76	90	84	1.1	1.9	0.6	1.2	9	5	0	SSW 6	S 3	SSE 5
7	107.8	108.3	108.6	108.2	0.0	1.2	0.9	0.8	1.4	-0.1	90	87	90	89	0.6	0.9	0.6	0.7	10	9	10	C 0	SSE 1	C 0
8	107.6	107.9	106.4	107.3	1.2	2.2	1.0	1.4	2.4	0.4	92	82	92	89	0.5	1.3	0.5	0.8	10	8	10 *	C 0	SW 3	SSW 3
9	103.8	105.9	107.7	105.8	1.7	3.1	1.9	2.2	3.8	0.6	94	90	89	91	0.4	0.8	0.8	0.7	10	10	9	SSW 3	SW 2	S 2
10	108.3	109.9	109.9	109.4	1.9	2.8	0.7	1.5	2.9	0.5	93	84	96	91	0.5	1.2	0.2	0.6	9	9	10	WSW 6	S 4	SSE 3
11	110.0	111.7	114.8	112.2	1.0	1.3	1.4	1.3	2.1	0.4	90	91	85	89	0.7	0.6	1.0	0.8	10	10	10	S 3	SSE 3	W 7
12	119.1	123.6	128.5	123.7	-0.6	-0.7	-0.8	-0.7	1.4	-2.1	95	95	83	91	0.3	0.3	1.0	0.5	9 *	7	9	NW 6	NW 7	W 5
13	127.5	123.7	121.1	124.1	-1.7	0.1	1.8	0.5	1.9	-3.6	67	68	93	76	1.8	2.0	0.6	1.5	9	10 •	10	SW 3	S 5	S 3
14	122.3	125.9	129.9	126.0	2.6	3.9	1.0	2.1	4.1	0.4	95	85	92	91	0.4	1.2	0.5	0.7	10	10	0	NW 4	NW 4	W 5
15	129.9	128.2	126.9	128.3	-0.2	2.4	3.4	2.2	3.4	-0.4	88	93	86	89	0.7	0.6	1.1	0.8	0	9	9	W 8	W 9	WNW 3
16	124.8	126.5	129.7	127.0	1.4	4.0	1.1	1.9	4.4	0.7	92	80	66	79	0.6	1.6	2.2	1.5	0	9	9	NW 5	N 6	NNE 8
17	134.3	136.2	139.7	136.7	-3.4	-1.1	-3.8	-3.0	1.1	-4.3	56	63	60	60	2.1	2.1	1.9	2.0	0	7	1	ENE 5	NE 4	SE 3
18	142.5	142.8	141.4	142.2	-8.8	-3.5	-5.5	-5.8	-2.0	-9.5	68	36	57	54	1.0	3.0	1.7	1.9	0	3	2	C 0	SSW 1	C 0
19	137.3	135.6	133.5	135.5	-4.8	-2.0	-6.0	-4.7	-0.6	-6.3	43	26	58	42	2.4	3.9	1.6	2.6	10	4	0	C 0	S 2	SSE 1
20	130.7	128.7	126.6	128.7	-7.4	0.4	-4.2	-3.8	1.4	-8.6	60	59	82	67	1.4	2.6	0.8	1.6	0	0	0	C 0	C 0	C 0
21	124.2	123.3	121.0	122.8	-7.5	-2.8	-5.9	-5.5	-2.2	-10.5	93	71	79	81	0.2	1.4	0.8	0.8	1	7	3	C 0	S 3	C 0
22	117.4	115.5	115.4	116.1	-7.0	-1.8	-5.2	-4.8	-0.7	-7.3	85	63	85	78	0.5	2.0	0.6	1.0	9	4	9	C 0	C 0	C 0
23	116.7	118.0	116.0	116.9	-5.0	-4.5	-3.1	-3.9	-3.0	-7.7	90	74	88	84	0.4	1.1	0.6	0.7	9	5	10 *	ENE 3	NE 4	NW 3
24	114.6	115.0	115.9	115.2	-2.4	-2.1	-8.1	-5.2	-0.6	-8.4	78	77	78	78	1.1	1.2	0.7	1.0	9	9 *	9	NNW 4	NE 6	C 0
25	115.7	117.6	119.8	117.7	-7.1	-6.8	-10.0	-8.0	-5.7	-11.8	88	56	71	72	0.4	1.6	0.8	0.9	10 *	3	9	C 0	SE 3	SSW 2
26	122.5	124.9	127.8	125.1	-8.9	-5.4	-7.3	-7.2	-4.5	-10.8	61	62	79	67	1.2	1.5	0.7	1.1	10	1	0	WSW 6	SW 6	NNE 2
27	130.8	131.6	127.0	129.8	-7.8	-2.9	-7.6	-6.5	-2.3	-8.9	87	53	48	63	0.4	2.3	1.8	1.5	0	6	0	SW 4	SW 5	S 2
28	120.7	118.8	115.4	118.3	-5.6	-1.6	-4.7	-4.2	0.0	-10.4	49	65	64	59	2.0	1.9	1.5	1.8	4	9	2	S 5	SW 4	S 3
29	108.4	109.7	108.0	108.7	-3.7	3.4	5.0	2.4	5.2	-6.6	71	78	76	75	1.3	1.7	2.0	1.7	9	9	9	S 6	SW 8	SSW 7
30	98.2	94.2	94.4	95.6	4.4	3.9	4.6	4.4	5.6	2.7	87	87	87	87	1.1	1.1	1.1	1.1	10 •	10 •	10 •	SSW 10	SSW 9	WSW 8
31	97.1	96.5	96.9	96.5	4.0	5.6	4.0	4.4	5.9	3.4	87	77	87	84	1.1	2.1	1.1	1.4	9	9	10 •	SW 5	SW 5	WSW 4
M	116.4	116.4	116.5	116.4	-1.9	0.3	-1.1	-1.0	1.4	-3.6	82	75	81	79	0.9	1.5	1.0	1.1	7.0	7.4	6.6	3.3	3.8	3.1

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1	98.0	97.2	94.3	96.5	2.6	3.6	1.7	2.4	4.7	1.5	86	81	92	86	1.1	1.5	0.5	1.0	9	9	10 •	SW 2	S 3	SSE 3
2	89.7	89.0	89.9	89.5	1.9	3.9	1.6	2.2	4.6	0.7	93	78	89	87	0.5	1.8	0.8	1.0	10	9	9	SSE 4	SSW 4	SSE 3
3	91.5	93.1	96.0	93.5	-0.4	1.6	1.4	1.0	1.8	-0.7	96	85	89	90	0.2	1.1	0.8	0.7	9	10	10	C 0	W 2	W 3
4	99.7	100.9	101.2	100.6	-0.5	0.8	-2.7	-1.5	1.5	-3.5	90	71	84	82	0.6	1.9	0.8	1.1	6	7 *	2	SW 4	W 7	SSW 1
5	107.2	111.4	115.0	111.2	-3.0	1.2	-0.3	-0.6	1.6	-5.2	79	66	92	79	1.0	2.3	0.5	1.3	2	9	7 *	W 3	WNW 4	WSW 2
6	116.4	113.3	105.6	111.8	-3.1	0.6	1.4	0.1	1.6	-4.3	93	74	74	80	0.4	1.7	1.8	1.3	0	9	10	C 0	S 8	SSE 7
7	102.2	101.7	102.3	102.1	2.4	5.1	2.6	3.2	5.1	0.9	93	80	89	87	0.6	1.8	0.8	1.1	10	6	9	SSE 3	SSE 4	S 4
8	104.6	109.1	113.9	109.2	2.8	4.9	3.1	3.5	5.4	1.7	96	72	78	82	0.3	2.5	1.7	1.5	10	5	9	WSW 2	NW 7	WNW 3
9	113.1	107.7	105.6	108.8	0.8	1.4	0.7	0.9	3.2	0.4	88	94	98	93	0.8	0.4	0.1	0.4	9	10 *	10 *	SSE 2	SSE 5	SE 3
10	115.4	121.9	122.1	119.8	1.1	1.6	1.9	1.6	2.1	0.2	96	89	87	91	0.2	0.8	0.9	0.6	10 *	10	10	NE 4	N 6	S 1
11	112.9	107.5	103.3	107.9	2.0	4.3	4.5	3.8	4.5	1.8	93	88	87	89	0.6	1.0	1.1	0.9	10 •	10	10	S 5	S 4	SSW 4
12	103.8	108.9	115.4	109.4	3.6	5.0	3.5	3.9	5.3	2.1	90	76	85	84	0.8	2.0	1.2	1.3	7	9	10	SW 4	W 3	W 3
13	118.8	121.4	124.8	121.7	2.4	4.2	1.4	2.4	4.3	0.9	95	85	96	92	0.4	1.2	0.3	0.6	10 •	10	3	W 4	NW 2	WSW 1
14	125.1	124.9	124.2	124.7	1.3	3.1	2.9	2.6	3.5	-1.4	92	90	93	92	0.5	0.8	0.5	0.6	10	10 •	10	C 0	E 4	S 2
15	122.9	124.1	124.7	123.9	4.6	8.3	3.6	5.0	11.5	2.7	84	79	97	87	1.4	2.3	0.3	1.3	0	5	9	SW 1	S 1	C 0
16	127.3	130.7	132.0	130.0	4.5	4.6	4.0	4.3	5.2	3.0	97	90	93	93	0.3	0.8	0.5	0.5	10	10	10	WNW 2	NW 6	W 7
17	131.3	132.6	130.4	131.4	4.4	7.4	5.0	5.4	9.2	3.9	84	72	84	80	1.4	2.9	1.4	1.9	9	6	0	W 7	W 6	SW 6
18	128.1	128.2	125.1	127.1	6.5	14.2	8.4	9.4	16.1	4.9	82	48	64	65	1.7	8.4	4.0	4.7	0	0	0	W 8	WNW 7	SSW 3
19	124.6	125.5	127.3	125.8	3.5	6.0	4.9	4.8	8.5	3.2	91	86	94	90	0.6	1.3	0.6	0.8	10	10	10 •	W 5	WNW 6	WNW 3
20	131.4	133.4	133.4	132.7	2.1	3.9	3.5	3.2	5.1	1.9	95	88	91	91	0.4	1.0	0.6	0.7	10	10	9	NNE 3	SSW 1	SW 5
21	132.6	132.9	132.2	132.9	2.3	3.7	2.1	2.6	4.0	1.9	95	87	93	92	0.4	1.1	0.5	0.7	10	10	10	W 1	SW 3	WNW 2
22	134.7	136.2	136.0	135.6	2.3	3.0	2.3	2.5	3.4	1.6	98	90	93	94	0.1	0.8	0.5	0.5	10	10	10	C 0	SSE 1	SE 1
23	134.5	133.5	131.8	133.3	1.6	0.9	0.3	0.8	2.4	0.1	96	94	96	95	0.3	0.4	0.2	0.3	10	10	10	C 0	C 0	SSE 2
24	130.9	130.6	130.2	130.6	-0.9	-0.4	0.5	-0.1	0.5	-1.4	96	94	88	93	0.2	0.3	0.7	0.4	10 •	10	10	SSE 2	SE 3	S 3
25	131.0	132.8	133.4	132.4	0.7	1.7	-0.5	0.4	2.4	-0.6	96	90	84	90	0.2	0.6	1.0	0.6	10	10	10	SSE 4	S 6	SSE 6
26	131.8	131.4	130.4	131.2	-0.4	1.9	0.5	0.6	3.4	-0.7	84	73	90	82	0.9	1.9	0.6	1.1	10	2	0	SSE 9	S 8	SSE 5
27	124.9	121.2	119.3	121.8	0.6	6.5	8.1	5.8	8.2	0.3	92	81	85	86	0.5	1.9	1.6	1.3	3	10	10	SSE 4	S 5	WSW 4
28	110.2	103.8	100.0	104.7	3.4	2.9	2.0	2.6	9.5	1.8	98	98	93	96	0.1	0.1	0.6	0.3	10 •	10 •	10 •	C 0	NNE 2	NW 12
29																								
30																								
31																								
M	117.7	118.0	117.9	117.8	1.8	3.8	2.4	2.8	5.0	0.6	92	82	88	87	0.6	1.6	0.9	1.0	8.0	8.4	8.1	3.0	4.2	3.5

Gdańsk – Wrzeszcz $H_s = 13\,m$ $H_{\frac{1}{3}} = 12{,}4\,m$ $h_w = 15{,}5\,m$ **Styczeń – Janvier 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	0.2	1	–	$*^{o}0^{35}-14^{38}$, $=0^{00}-24$; $\sqcup^{o}0^{00}-2^{00}$
2	5	.	2	–	$=0^{00}-24$
3	5	3.0	1	–	$*^{o-1}12^{15}-14^{20}$ $\bullet^{o}*-16^{30}$; $=0^{00}-24$
4	4	0.8	.	–	$\bullet^{o}4^{40}-9^{45}$
5	6	.	.	–	$=6^{15}-24$
6	7	.	.	–	$=0^{00}-7^{30}$, $14^{35}-24$
7	5	0.4	.	–	$=0^{00}-24$; $\triangledown 3^{30}-5^{40}$
8	7	1.0	1	–	$\triangle^{o}0^{40}-1^{45}$ $\bullet^{o}10^{35}$ 11^{10} $19^{40}-24$; $=$ nad – a, p -24
9	6	1.8	.	–	$\bullet^{o}0^{00}-1^{45}$ $*^{o}-3^{35}$ $\bullet^{o}22^{45}-24$; $=0^{00}-22^{45}$
10	7	.	.	–	$\bullet^{o}0^{00}-2^{50}$; $=2^{50}-9^{15}$, $14^{50}-24$
11	5	3.6	.	–	$\bullet^{o}8^{50}-9^{45}$ $\bullet^{o}*-11^{35}$ $\bullet^{o}14^{50}$ 20^{25}; $=0^{00}-22^{30}$
12	7	1.7	3	–	$*^{o}0^{45}-2^{30}$ $*^{o}-5^{35}$ $*^{o}\triangledown 6^{35}-7^{40}$ $*^{o-1}\triangledown 8^{15}-11^{15}$ $*^{o}14^{50}-15^{05}$
13	7	0.1	10	–	$\bullet^{o}12^{25}$ 14^{52}; $=14^{52}-24$
14	7	.	3	–	$=0^{00}-9^{20}$; $\sqcup^{o}23^{00}-24$
15	7	.	pł.	–	$\sqcup^{1}0^{00}-10^{00}$
16	7	0.0	.	–	$\bullet^{o}\triangledown 16^{10}-25$
17	8	.	.	–	
18	7	.	.	–	∞ $16^{40}-19^{15}$
19	7	.	.	–	∞ $16^{30}-20^{20}$
20	7	.	.	–	∞ $6^{10}-11^{15}$, $15^{30}-16^{45}=-24$; $\sqcup^{o}1^{00}-11^{00}$ $\sqcup^{1}20^{00}-24$
21	6	.	.	–	$=0^{00}-24$; $\sqcup^{1}0^{00}-12^{00}$
22	7	.	.	–	$=0^{00}-11^{30}$ ∞ $15^{15}-16^{10}$
23	8	0.4	.	–	$*^{o}20^{20}-24$; $=8^{20}-11^{10}$, $16^{30}-20^{20}$
24	7	0.5	1	–	$*^{o}0^{00}-6^{43}$ $\triangledown^{1}9^{10}-10^{35}$ $\triangledown^{o}11^{40}-13^{15}$ $\triangledown^{o}22^{05}-23^{20}$, $23^{40}-24$
25	7	1.2	3	–	$\triangledown^{o}0^{00}-15$ $*^{o-1}4^{35}-8^{10}$ $\triangledown^{o}-9^{35}$; $=16^{40}-24$
26	7	.	5	–	$=0^{00}-12^{0}$
27	7	.	4	–	
28	7	.	3	–	∞; $=13^{15}-24$
29	6	1.6	3	–	$=0^{00}-24$
30	7	4.4	.	–	$\bullet^{o}2^{45}-3^{15}$ $\bullet^{1}-4^{20}$ $\bullet^{o}-24$; $=0^{00}-2^{45}$; $\gg 0^{30}-7^{30}$
31	7	0.4	.	–	$\bullet^{o}0^{00}-2^{20}$, $19^{25}-21^{20}$; $=7^{15}-10^{35}$, $17^{10}-22^{40}$
Σ	–	21.1	–	–	UWAGI. *Kierunki i prędkości wiatru w ciągu całego roku – wg anemometru.*

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1	7	1.9	.	–	$\bullet^{o}20^{35}-24$; $=6^{20}-10^{30}$ $14^{20}-20^{35}$
2	7	.	.	–	$\bullet^{o}0^{00}-2^{25}$; $=2^{25}-9^{30}$, $17^{20}-24$
3	4	0.9	.	–	$*^{o}7^{50}-10^{30}$ $*^{1}-11^{40}$; $=0^{00}-24$
4	7	0.2	.	–	$*^{o}\triangledown 6^{05}$ 16^{40}
5	7	0.5	.	–	$*^{o}\triangledown 19^{35}-21^{10}$, $21^{28}-22^{15}$
6	6	0.4	2	–	$\bullet^{o}22^{45}-24$; $=7^{10}-13^{20}$
7	6	.	.	–	$\bullet^{o}0^{00}-1^{45}$ $\bullet^{o}*-4^{20}$; $=4^{20}-19^{40}$
8	8	0.0	.	–	$\bullet^{o}7^{50}-9^{20}$; $=6^{30}-9^{40}$
9	5	6.2	.	–	$*^{o-1}12^{32}-24$; $=6^{20}-12^{32}$
10	7	2.6	2	–	$*^{o}0^{00}-7^{30}$ $\bullet^{o}-8^{20}$; $=8^{00}-9^{20}$
11	6	2.9	.	–	$\bullet^{o-1}1^{45}-10^{30}$ $\bullet^{o}14^{40}-17^{35}$ $\bullet^{o}18^{45}-20^{10}$, np; $=a-24$
12	7	0.2	.	–	$\bullet^{o}23^{40}-24$; $=0^{00}-10^{25}$
13	7	0.0	.	–	$\bullet^{o}0^{00}-1^{45}$ $6^{40}-7^{40}$; $=14^{15}-24$; $\sqcup^{o}23^{00}-24$
14	5	0.1	.	–	$\bullet^{o}12^{33}$ 16^{20}; $=0^{00}-24$; $\sqcup^{o-1}0^{00}-10^{00}$
15	6	.	.	–	$=0^{00}-24$
16	6	.	.	–	$=0^{00}-3^{45}$ $\equiv^{1-0}5^{40}=-24$
17	7	.	.	–	$=0^{00}-3^{40}$; $\gg 4^{15}-5^{30}$
18	6	.	.	–	$=4^{30}-10^{20}$ ∞ -14^{40} $16^{35}-21^{30}=-24$
19	7	0.0	.	–	$\bullet^{o}9^{35}$ 12^{20}, $17^{45}-22^{35}$; $=0^{00}-9^{35}$, $15^{10}-24$
20	7	.	.	–	$=0^{00}$ 11^{30}, $17^{30}-24$
21	7	.	.	–	$=0^{00}-11^{40}$ $16^{30}-24$
22	6	.	.	–	$=0^{00}-5^{40}\equiv^{o}6^{45}=-24$
23	5	0.0	.	–	$\bullet^{o}21^{35}-24$; $=0^{00}-24$
24	6	0.0	.	–	$\bullet^{o}0^{00}$ 11^{20}; $=0^{00}-24$
25	4	.	.	–	$=0^{00}-24$
26	6	.	.	–	$=0^{00}-24$
27	6	4.3	.	–	$\bullet^{o}10^{50}-11^{03}$ 14^{52} 16^{45}; $=0^{00}-24$; $\sqcup^{o}3^{00}-8^{00}$
28	5	14.7	.	–	$\bullet^{o-1}2^{40}-24$; $=0^{00}-1^{30}$, $9^{50}-24$; $\gg 20^{25}-23^{30}$
29					
30					
31					
Σ	–	54.9	–	–	UWAGI.

Gdańsk - Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ Marzec - Mars 1961

Dzień	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			WIATR D,v		
	I	II	III	Dias	I	II	III	Dias	Max	Min	I	II	III	Dias	I	II	III	Dias	I	II	III	I	II	III
1	110.8	114.6	119.1	114.8	1.9	5.5	5.7	5.7	6.0	1.5	91	78	87	85	0.6	1.9	1.1	1.2	10 •	9	4	W 5	WNW 9	W 9
2	120.6	121.6	122.6	121.6	2.8	6.3	2.6	3.6	7.5	1.7	86	65	79	77	1.1	3.3	1.6	2.0	4	0	0	W 7	W 8	C 0
3	125.9	126.5	129.1	126.5	3.2	5.4	6.0	5.2	6.8	1.4	90	95	92	92	0.8	0.5	0.8	0.7	10 •	10	10	C 0	C 0	WNW 5
4	131.4	131.5	127.9	130.2	4.4	9.3	7.7	7.3	11.2	3.8	89	66	64	73	1.0	4.0	3.8	2.9	10	8	4	W 4	SW 5	WSW 7
5	128.5	130.7	131.2	130.1	5.9	7.9	4.1	5.5	8.7	3.9	83	64	83	77	1.6	3.8	1.4	2.3	9	9	10	WNW 6	NW 7	W 6
6	129.2	130.1	126.7	128.7	4.8	6.3	5.3	5.4	8.4	3.7	87	84	87	86	1.1	1.5	1.1	1.2	7	9	1	W 6	WNW 7	W 10
7	121.6	123.4	127.5	124.2	7.0	10.0	5.4	7.0	11.2	5.1	71	65	84	73	2.9	4.4	1.4	2.9	7	1	0	W 8	NW 7	W 6
8	128.8	128.3	127.6	128.2	2.4	11.4	7.0	7.0	12.4	2.2	93	49	82	75	0.6	6.8	1.7	3.0	6	1	0	WSW 7	WNW 7	W 8
9	126.0	125.3	123.8	125.0	7.0	11.3	9.1	9.1	12.7	6.7	84	66	77	76	1.6	4.5	2.7	2.9	6	1	3	W 9	NW 8	W 10
10	122.5	121.1	117.4	120.3	8.9	16.0	11.5	12.0	18.6	8.4	72	35	52	53	3.2	11.8	6.6	7.2	1	0	0	WNW 5	WSW 3	WSW 4
11	115.9	116.3	117.1	115.8	8.7	8.1	5.4	6.9	11.8	5.2	80	79	78	79	2.2	2.3	2.0	2.2	4	10	0	WSW 7	W 8	W 9
12	112.5	105.4	95.8	104.6	5.9	8.8	9.4	8.4	11.4	4.6	80	82	85	82	1.9	2.0	2.0	2.0	9	10 •	9 •	WSW 8	WSW10	WSW12
13	99.6	105.2	110.7	105.2	4.8	6.8	3.1	4.4	9.5	2.0	61	38	65	54	3.4	6.1	2.8	4.1	1	1	0	WNW12	NW 12	WNW 7
14	111.2	110.5	108.3	110.0	2.0	6.7	8.1	6.2	8.2	1.5	85	72	90	82	1.1	2.7	1.1	1.6	9	10	10 •	C 0	WSW 3	NW 7
15	108.3	112.8	116.0	112.4	7.2	10.6	6.5	7.7	11.4	6.3	77	54	79	70	2.4	5.9	2.0	3.4	1	2	0	W 12	NW 12	W 6
16	109.4	110.6	116.7	112.2	7.9	9.5	6.7	7.7	10.9	5.2	79	60	78	72	2.2	4.8	2.2	3.1	10	9	0	W 16	WNW16	W 8
17	117.5	114.5	109.2	113.7	5.1	14.0	11.2	10.4	15.2	4.4	87	54	71	71	1.1	7.4	3.9	4.1	10	10	0	WSW 9	W 12	SW 5
18	96.2	98.7	95.5	96.8	10.3	9.4	6.4	8.1	12.3	6.2	66	45	55	55	4.2	6.4	4.3	5.0	8	4	0	SW 6	W 12	SW 7
19	94.3	101.3	107.4	101.1	2.8	1.4	-1.8	0.2	6.5	-2.0	86	85	83	85	1.1	1.0	0.9	1.0	10	9 ⚹	1	WSW 8	N 8	NW 5
20	107.9	103.1	94.2	101.7	-2.4	4.3	2.3	1.6	5.0	-5.4	76	38	65	60	1.2	5.1	2.5	2.9	0	9	10	SSW 4	SSW 8	S 4
21	85.3	88.4	97.5	90.4	0.7	2.6	2.0	1.8	3.1	0.2	96	91	89	92	0.2	0.7	0.8	0.6	10	10 •	10 •	C 0	NNW 3	N 9
22	107.4	109.7	108.0	108.4	-1.0	3.5	1.0	1.1	4.0	-2.0	71	55	85	70	1.7	3.5	1.0	2.1	4	4	10	WNW 4	WNW 7	S 5
23	105.3	105.3	106.1	105.6	3.3	7.3	7.2	6.3	8.3	0.5	95	74	70	80	0.4	2.6	3.1	2.0	10	10	9	C 0	W 7	W 12
24	105.6	107.8	109.8	107.7	7.2	9.9	7.1	7.8	10.4	5.3	76	56	76	69	2.5	5.4	2.5	3.5	9	8	4	W 12	WNW14	WNW10
25	111.6	114.5	115.3	113.8	6.3	8.6	6.8	7.1	9.8	5.2	78	60	86	75	2.1	4.5	1.5	2.7	9	7	9	WNW 8	WNW 8	W 5
26	111.6	105.3	96.6	104.5	7.4	11.5	7.5	8.5	11.6	6.3	80	50	82	71	2.1	6.9	2.0	3.7	9	10	9	SW 5	SW 10	WSW10
27	94.6	96.2	97.0	95.9	4.7	5.8	1.6	3.4	7.6	0.7	64	67	67	66	3.1	3.0	2.3	2.8	9 ⚹	9 •	2	W 14	WNW12	W 10
28	98.0	100.6	105.1	101.2	1.2	6.5	2.5	3.2	7.0	-1.3	81	48	73	67	1.3	5.0	1.9	2.7	8	9	1	W 7	WNW12	W 6
29	103.7	102.3	98.2	101.4	1.3	4.8	6.3	4.8	6.6	0.7	79	87	90	85	1.4	1.1	1.0	1.2	10 ⚹	9	10 •	SSW 3	SW 6	SSW 5
30	91.2	97.7	98.3	95.7	8.0	6.8	3.9	5.6	8.2	3.7	79	43	65	62	2.2	5.6	2.8	3.5	7	7	10	WSW 8	W 15	C 0
31	101.6	103.4	100.1	101.7	1.2	6.0	4.3	4.0	7.1	0.6	77	47	62	62	1.3	5.0	3.2	3.2	4	6	9	NW 5	W 7	SSE 3
M	110.6	111.7	111.5	111.3	4.6	7.8	5.5	5.8	9.3	2.8	81	63	77	74	1.7	4.2	2.2	2.7	7.1	6.8	4.7	6.6	8.5	6.7

Kwiecień - Avril

Dzień																								
1	104.1	102.8	101.8	102.9	1.0	4.2	0.0	1.3	4.5	-0.3	81	46	92	73	1.3	4.4	0.5	2.1	3	10	10 *	W 6	SSE 2	C 0
2	107.7	109.5	108.9	108.7	-1.0	4.9	0.6	1.3	6.1	-3.0	87	46	82	72	0.8	4.7	1.1	2.2	3	9	6	C 0	NE 5	C 0
3	103.8	102.8	105.0	103.9	0.9	2.7	2.4	2.1	3.7	-0.9	85	84	86	85	1.0	1.2	1.1	1.1	10 *	10	5	SE 1	ENE 3	WSW 3
4	105.0	104.7	111.5	106.4	1.0	6.0	2.8	3.2	6.7	0.4	96	53	74	74	0.3	4.5	2.0	2.3	10 ⚹	7	5	SSE 3	W 10	WSW 5
5	113.5	110.1	104.2	109.3	1.8	4.6	9.3	6.2	9.7	0.9	87	81	93	87	0.9	1.7	0.8	1.1	10	10	10	C 0	SE 5	S 2
6	105.5	109.3	110.1	108.3	11.7	18.2	11.0	13.0	20.2	8.8	84	46	72	67	2.1	11.3	3.7	5.7	9	3	6	SSW 4	W 7	C 0
7	105.3	106.0	108.4	106.6	15.4	23.6	12.1	15.8	24.3	9.8	60	37	85	60	7.0	18.3	2.3	9.2	4	6	9	SW 8	WSW 7	NW 5
8	110.5	111.0	112.3	111.3	7.6	4.7	3.5	4.8	12.4	3.3	77	95	85	86	2.3	0.4	1.2	1.3	10	10 •	1	WNW 3	N 7	WSW 4
9	113.6	118.4	120.5	117.5	3.5	6.5	2.9	4.0	7.4	2.7	65	37	51	51	2.7	6.1	3.7	4.2	4	2	0	NW 9	N 9	WNW 4
10	119.7	118.6	115.5	117.9	1.6	7.1	2.5	3.4	7.9	0.2	78	38	63	60	1.6	6.3	2.7	3.5	10	9	0	C 0	ENE 3	C 0
11	112.5	112.0	115.6	113.4	0.8	9.5	1.8	3.5	11.0	-2.7	79	36	82	66	1.4	7.6	1.3	3.4	7	2	0	C 0	NE 2	NNW 2
12	117.9	117.6	115.8	116.4	2.3	10.3	9.5	7.9	13.6	-0.4	86	34	43	54	1.0	8.3	6.8	5.4	4	6	6	C 0	C 0	S 1
13	109.6	110.3	111.1	110.3	9.9	16.5	10.6	11.9	17.3	8.8	71	37	86	71	3.6	8.2	1.8	4.5	10	9	3	C 0	NW 8	C 0
14	110.8	109.2	107.2	109.1	12.1	22.5	17.5	17.4	25.4	9.8	75	39	56	57	3.5	16.7	8.8	9.7	3	3	0	SSW 1	SE 3	C 0
15	108.4	111.2	113.4	111.0	11.8	14.7	7.0	10.1	17.8	6.7	87	72	93	84	1.8	4.7	0.7	2.4	7	1	4	NW 3	NNE 6	NNE 2
16	113.4	112.9	112.4	112.9	6.1	7.4	5.4	6.1	9.5	5.1	97	94	97	96	0.3	0.6	0.3	0.4	10	10	7	NNE 2	NE 3	N 2
17	112.2	112.5	112.2	112.3	5.3	10.5	9.3	8.6	11.8	3.0	100	77	79	85	0.0	2.9	2.5	1.8	10 ≡	1	9	N 2	NE 2	C 0
18	110.4	111.2	112.3	111.3	9.3	12.4	8.2	9.3	13.6	8.0	96	79	86	87	0.5	3.0	1.5	1.7	10	9	2	C 0	W 5	WNW 2
19	113.8	116.7	120.6	117.0	7.3	9.8	4.8	6.7	12.5	4.0	70	61	81	71	3.0	4.8	1.7	3.2	2	1	0	W 5	ENE 8	NE 2
20	124.5	126.0	125.5	125.3	6.4	6.7	4.5	5.5	8.0	3.5	51	49	63	54	4.7	5.0	3.1	4.3	0	1	0	ENE 5	NE 6	NE 3
21	124.9	122.1	118.1	121.7	4.1	13.2	9.9	9.3	14.6	0.3	61	30	41	44	3.2	10.7	7.2	7.0	0	0	0	SE 1	ESE 3	SE 2
22	114.1	110.3	108.2	110.9	5.6	17.6	12.8	12.2	20.2	2.7	56	38	55	50	4.0	12.4	6.7	7.7	1	1	0	S 2	SSE 5	SE 1
23	107.6	107.4	108.8	107.9	8.1	19.6	14.6	14.2	20.4	5.6	66	38	39	48	3.7	14.1	10.0	9.3	0	2	0	S 5	SE 7	SE 3
24	112.6	112.5	114.3	113.1	9.3	18.2	13.1	13.4	19.0	6.8	56	35	55	49	3.1	13.5	6.9	8.5	0	1	0	SE 2	SE 6	SE 2
25	117.4	116.3	116.3	116.7	9.7	14.3	11.2	11.6	15.6	4.3	60	47	63	57	4.7	8.8	4.7	6.1	0	9	0	SE 4	ESE 6	C 0
26	115.0	112.2	110.3	112.5	9.0	15.7	11.6	12.0	17.0	3.6	61	43	64	56	4.5	10.0	4.8	6.4	0	1	3	SE 1	ENE 7	C 0
27	110.2	110.1	110.9	110.4	10.7	14.9	10.2	11.3	15.8	6.3	74	54	70	66	3.4	7.7	3.7	4.9	4	3	0	C 0	NE 3	C 0
28	110.2	111.1	112.0	111.1	9.4	10.9	7.3	8.8	11.8	5.0	79	77	84	80	2.3	3.0	1.7	2.4	0	1	4	C 0	NNE 7	N 3
29	115.8	116.3	115.3	115.9	6.2	9.9	6.6	7.3	10.8	5.1	64	50	74	63	3.4	6.1	2.3	4.0	1	1	0	ENE 8	NE 6	C 0
30	113.6	112.1	111.4	112.4	7.7	9.8	7.8	8.3	11.2	0.7	49	52	71	57	5.3	5.8	3.1	4.7	1	9	8	C 0	ENE 4	ENE 2
31																								
M	112.0	112.1	112.3	112.1	6.3	11.6	7.7	8.4	13.3	3.6	73	54	72	67	2.7	7.1	3.3	4.4	4.8	4.9	3.3	2.3	3.2	1.7

Gdańsk - Wrzeszcz $H_s = 13\,m$ $H_b = 12{,}4\,m$ $h_w = 15{,}5\,m$ Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	–	• 0⁰⁰–2⁴⁰ ▽• 3⁴⁵–4³⁵ • 4⁵⁰–8⁰⁵, = 0⁰⁰–1⁴⁰
2	7	.0.0	.	–	
3	5	1.0	.	–	• 5⁴⁵–12³⁰, = 12³⁰–24
4	7	.	.	–	= 0⁰⁰–8⁴⁰
5	7	.	.	–	= 6³⁵–9¹⁵
6	7	.	.	–	» 17¹⁰–21⁴⁰
7	7	.	.	–	= 8²⁰–12²⁵
8	7	.	.	–	
9	7	.	.	–	= 6¹⁰–12²⁰, » 20¹⁵–21³⁵
10	7	.	.	–	= 3¹⁵–8³⁵
11	6	0.0	.	–	• 14⁴⁰–15²⁰, » 9⁴⁰–11⁴⁰, = 5¹⁵–21⁴⁰
12	6	4.0	.	–	• 9⁴⁸–13³⁵ 18⁴⁰ 19²⁰ •1–20³⁰ ▽1-0 24, » 12³⁰–23¹⁰ ≈ –24 = p
13	8	.	.	–	•▽ 0⁰⁰–05 ≈ 0⁰⁰–4⁴⁰ » –17²⁵
14	7	0.0	.	–	• 15²⁰–45, 20⁴⁰–22³⁵
15	8	0.0	.	–	» 0²⁰–16⁴⁰
16	7	.	.	–	•1-0 2⁴⁵–4³⁵, » – ≈ 4³⁵–17²⁰
17	8	.	.	–	» 11²⁵–14⁴⁵
18	8	0.2	.	–	= 7²⁵–8¹⁵, a, » 8¹⁵–19²⁰
19	6	0.6	.	–	▽• 4³⁵–6¹⁰ 7¹²-³⁰ ▽•– 9²⁵ ▽a-1 14²⁰ ▽a 15⁰⁷–¹⁵
20	8	1.8	1	–	* 22²⁰–24
21	6	1.6	1	–	* 0⁰⁰–5⁴⁰ *– 6³⁵ • 9⁴⁵–13¹⁰ ✕– 13²⁰ 16²⁰-³⁵ ▽•, ▽* 17⁴⁵ 20¹⁰ • * 20⁴⁰–23⁴⁰, = 6³⁵–13¹⁰, » 21⁴⁰–24
22	8	0.0	.	–	△ 2⁴⁵–3¹⁰ ▽* 7³¹–⁴⁰ ▽a-1 17⁵⁰ 9¹⁵ * 19³⁰ 24, » 0⁰⁰–3⁴⁰
23	7	.	.	–	* 0⁰⁰–³⁰ • 1⁰⁰–⁴⁰ = 5³⁰–8¹⁰, » 19¹⁰–24
24	7	.	.	–	» 0⁰⁰–15³⁵, 17¹⁵–21³⁵
25	8	.	.	–	
26	7	2.3	.	–	• 16¹⁵–19⁴⁰ ▽• 22¹⁵ 23⁴⁰, = 19²⁰–21³⁰, » 12⁴⁰–24, ⊕1 11¹⁵–12¹⁵
27	8	2.1	.	–	▽• 2⁴⁰–3⁰⁵ ✕1 5⁰⁵-¹⁵ △• 6⁴⁰–7⁰⁵ ▽a-1 9²⁰ 17²⁰ ▽a1 17²⁰-³³, 19⁰⁵-¹², 23²⁷–³⁵, » 0⁰⁰–22²⁵
28	8	0.0	.	–	▽* 0¹⁵–1²⁰, » 8³⁵–16²⁰
29	7	4.0	.	–	* 6⁴⁰–9³⁵ • 12³⁵ 17¹⁵–24
30	8	.	.	–	• 0⁰⁰–6³⁵, ≈ 7⁰⁵–14²⁰ » 16³⁰, ⊕1 15¹⁵–16⁴⁰
31	8	1.8	.	–	▽* 7⁴⁵–8³⁵ • 22²⁰–⁴⁵ *–23³⁰
Σ	–	19.4	–	–	UWAGI:

Kwiecień – Avril

1	8	2.1	.	–	*▽ 0¹⁵–2¹⁵ •▽ 3¹⁵–⁴⁰ *▽a-1 6⁰⁵ *a-1 14³⁵–15¹⁰, 16¹⁰–22³⁰, » 3¹⁰–5⁴⁰
2	8	0.1	2	–	*▽ 13⁰⁹–³⁵, 15¹⁵–³⁰
3	7	0.4	.	–	* 6³⁵–10⁴⁵ •– 12⁴⁵ 16¹⁵–18⁵⁰
4	8	2.0	.	–	• 5⁴⁵–6¹⁵ *1-a 9⁴⁰ ✕1 13¹⁵-²⁰ △• 14¹⁵-²⁰, » 10⁴⁰–16²⁰
5	7	2.0	.	–	• 15³⁰–18¹⁵, = 6⁴⁰–11³⁰ 18¹⁵–24
6	7	0.8	.	–	• 1⁰⁷–2²⁵ (K) 21⁴⁸–22⁰⁷ SSE K•– 23⁰³ (K) –23³⁰ NE, = 0⁰⁰–2²⁵, 19¹⁰–20¹⁵
7	7	0.0	.	–	▽• 1⁰⁴-²⁰, K• 1²⁰–2⁰⁵ (K) –2²⁵ S-NW, 14⁴⁵–15⁴⁵ SW–NW
8	6	1.1	.	–	▽• 0¹⁰–1¹⁵ • 12²⁰–16⁴⁵, = 11¹⁵–14⁴⁵
9	8	.	.	–	
10	7	.	.	–	= 7¹⁰–10³⁰, ⌣• 2⁰⁰–8⁰⁰
11	8	.	.	–	= 6³⁰–8⁴⁰, 19⁴⁰–24, ⌣• 1⁰⁰–8⁰⁰
12	7	.	.	–	= 0⁰⁰–8⁴⁵, ⌣• 1⁰⁰–7⁰⁰
13	7	.	.	–	=, ∞ 15¹⁰–24, ⌒• 23⁰⁰–24
14	6	0.0	.	–	= 0⁰⁰–7⁴⁰ ∞ –20¹⁵, ⌒• 0⁰⁰–7⁰⁰
15	6	.	.	–	▽• 6¹⁵–³⁰, = 4⁴⁰–24
16	5	.	.	–	=, ≡• 0⁰⁰–24
17	7	0.4	.	–	= 0⁰⁰–6¹⁰ ≡• –8⁵⁰ = –12²⁰
18	7	.	.	–	• 1¹⁰–4³⁵, = 4³⁵–10⁴⁰
19	8	.	.	–	
20	8	.	.	–	
21	8	.	.	–	⌣• 2⁰⁰–8⁰⁰
22	7	.	.	–	⌣• 3⁰⁰–6⁰⁰
23	8	.	.	–	
24	8	.	.	–	
25	8	.	.	–	
26	8	.	.	–	
27	7	.	.	–	= 4²⁵–8¹⁵ ∞ –8⁴⁵
28	8	.	.	–	
29	8	.	.	–	
30	8	.	.	–	
31					
Σ	–	8.9	–	–	UWAGI:

Gdańsk - Wrzeszcz — φ = 54°23' — λ = 18°36' — Maj – Mai 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	111.9	113.8	115.0	113.6	7.9	8.1	5.5	6.8	9.7	5.6	85	74	81	80	1.6	2.8	1.7	2.0	10	8	4	NNE 5	NNE 8	N 3
2	113.1	112.6	110.7	112.1	7.7	11.9	9.5	9.6	13.6	1.3	79	68	83	77	2.2	4.4	2.1	2.9	0	1	0	C 0	NE 4	C 0
3	109.1	107.1	109.9	108.7	9.3	19.5	11.6	13.0	19.5	7.7	95	45	95	77	0.8	12.5	1.0	4.8	10	10	2	SSE 2	S 3	C 0
4	113.7	115.3	116.4	115.1	11.1	15.4	8.9	11.1	16.0	7.2	83	63	93	80	2.3	6.5	0.8	3.2	2	6	0	WNW 2	NE 6	C 0
5	116.1	113.5	110.4	113.3	11.0	20.7	17.8	16.8	22.0	6.5	80	36	62	59	2.6	15.7	7.8	8.7	1	9	10	SSE 3	SSE 6	S 4
6	110.0	110.5	112.8	111.1	13.7	15.4	11.7	13.1	18.0	11.6	98	78	89	88	0.4	3.9	1.5	1.9	10 •	10	0	C 0	WSW 3	C 0
7	111.7	108.1	104.8	108.2	11.9	16.5	10.6	12.4	18.0	9.6	94	75	86	84	0.8	5.2	1.8	2.6	9	10 •	10	S 3	SW 8	W 2
8	107.5	106.7	104.9	106.4	9.7	10.3	9.2	9.6	12.5	7.0	75	77	76	76	2.9	2.8	2.7	2.8	8	9	9	WSW 5	SW 5	SW 3
9	101.4	99.9	101.2	100.8	8.6	11.9	8.3	9.3	13.0	7.8	88	66	86	80	1.4	4.7	1.6	2.6	10	9 •	4	SW 5	SW 6	C 0
10	103.5	106.2	110.6	106.8	6.7	7.9	7.0	7.2	8.7	5.4	90	80	93	88	1.0	2.0	0.7	1.2	10 •	10 •	10	WNW 7	NNW 9	NNW 9
11	112.8	116.5	119.0	116.1	6.7	7.4	4.9	6.0	8.5	4.7	85	85	86	85	1.4	1.8	1.3	1.5	10	10	2	NNW 8	N 9	NW 4
12	117.4	116.0	114.7	116.0	6.8	8.0	6.3	6.8	9.0	5.6	82	72	78	77	1.8	2.9	2.1	2.3	10	6	9	NW 1	NNE 8	N 4
13	110.7	107.7	107.0	108.5	8.1	11.6	7.8	8.8	14.4	2.5	63	67	78	69	4.0	4.5	2.4	3.6	9	10 •	1	SW 6	SW 5	C 0
14	105.0	105.8	106.7	105.8	8.7	8.7	7.3	8.0	10.4	5.5	78	84	93	85	2.4	1.8	0.7	1.6	4	10 •	10 •	SW 5	SSW 4	C 0
15	109.1	111.6	112.5	111.1	6.9	7.8	7.2	7.3	8.4	6.7	88	90	91	90	1.1	1.1	0.9	1.0	10 •	10	10	NNE 5	N 8	NW 5
16	108.7	109.9	113.3	110.6	7.1	9.0	7.0	7.5	9.8	6.5	93	84	90	89	0.8	1.9	1.0	1.2	10 •	7	7	W 2	NE 5	NNW 4
17	113.6	115.2	116.8	115.2	8.0	11.3	6.5	8.1	11.8	6.0	94	78	90	87	0.6	3.0	1.0	1.5	10 •	9	2	NNW 8	N 9	NW 1
18	116.7	116.6	115.3	116.2	8.5	11.3	7.2	8.6	12.2	4.1	66	50	86	67	3.7	6.7	1.5	4.0	5	2	2	N 5	W 3	C 0
19	111.8	111.2	109.8	110.9	9.9	13.5	9.5	10.6	15.4	6.2	95	75	84	84	0.8	3.9	1.9	2.2	10	9	9	C 0	NE 6	C 0
20	107.2	107.2	109.1	107.8	10.9	14.5	9.1	10.9	15.5	8.8	79	59	95	78	2.7	6.8	0.7	3.4	10	9	8	SSW 3	S 5	C 0
21	111.2	112.7	114.3	112.7	9.4	8.0	6.5	7.6	10.7	6.3	95	96	93	95	0.6	0.4	0.7	0.6	1	10	10	C 0	N 7	N 6
22	114.2	113.7	112.4	113.4	9.6	12.1	8.4	9.6	13.1	4.1	69	66	74	70	3.8	4.8	2.8	3.8	3	3	5	N 4	NE 7	W 1
23	111.6	110.1	111.1	110.9	11.7	17.5	10.3	12.4	18.0	5.3	59	40	75	58	5.6	12.0	3.1	6.9	4	8	9	SW 5	SW 4	W 3
24	111.1	112.4	112.8	112.1	11.3	12.7	10.8	11.4	15.4	9.1	79	66	74	73	2.8	5.1	3.4	3.8	10	10	0	SW 3	W 7	W 2
25	112.3	112.8	112.7	112.6	11.6	15.2	10.8	12.1	16.8	8.5	69	58	80	69	4.2	7.3	2.6	4.7	0	9	4	SW 7	W 6	C 0
26	113.2	112.2	110.2	111.9	12.5	18.3	11.9	13.6	19.9	4.4	67	40	70	59	4.9	12.7	4.1	7.2	2	2	2	C 0	E 3	E 2
27	106.0	107.1	110.9	108.0	12.9	15.7	10.0	12.2	17.9	7.4	74	68	82	75	3.9	5.7	2.2	3.9	7	9	10	C 0	NNE 5	N 2
28	111.1	109.9	108.7	109.9	9.8	9.5	9.2	9.4	11.5	7.8	87	96	89	91	1.6	0.5	1.2	1.1	9	10 •	10	NE 3	N 8	NW 7
29	107.2	106.3	105.7	105.7	9.8	10.7	8.7	9.5	11.8	8.6	92	90	99	94	0.9	1.3	0.1	0.8	10	10	10 =	C 0	NNE 6	N 5
30	99.8	98.4	101.0	99.7	14.8	19.1	14.8	15.9	19.5	8.3	84	72	83	80	2.7	6.2	2.9	3.9	0	3	9	NNE 3	NE 3	C 0
31	104.4	104.7	105.4	104.8	11.2	16.9	11.3	12.7	17.6	11.0	84	63	93	80	2.1	7.2	1.0	3.4	10 •	9	7	C 0	S 1	NE 1
M	110.1	110.1	110.5	110.2	9.8	12.8	9.2	10.2	14.1	6.6	82	70	85	79	2.2	5.1	1.9	3.1	6.9	8.0	6.0	3.2	5.7	2.2

Czerwiec – Juin

1	104.7	104.7	104.0	104.5	13.3	20.0	16.1	16.4	20.2	7.8	84	48	79	70	2.5	12.2	3.8	6.2	0	2	0	C 0	ENE 3	E 1
2	104.3	105.2	106.1	105.2	17.8	21.0	17.5	18.4	24.3	11.7	74	65	80	73	5.4	8.7	4.0	6.0	1	1	2	C 0	C 0	C 0
3	108.0	109.3	110.7	109.3	18.5	20.5	16.5	18.0	22.3	13.9	74	74	79	76	5.5	6.3	4.1	5.3	3	1	1	C 0	NNE 6	N 3
4	112.0	112.7	113.3	112.7	17.4	21.2	18.0	18.6	21.9	14.4	82	69	75	75	3.6	8.0	5.2	5.6	4	2	1	NNE 4	NE 6	NNE 1
5	115.3	115.9	116.1	115.8	18.9	24.3	18.5	20.0	26.0	15.2	74	57	79	70	5.5	13.1	4.5	7.7	5	4	2	N 1	NE 5	C 0
6	116.3	115.6	115.4	115.1	19.9	25.3	18.9	20.8	25.9	14.2	73	39	74	62	6.1	19.6	5.7	10.5	0	1	0	C 0	ENE 5	C 0
7	112.5	110.0	107.1	109.9	18.7	25.7	17.8	20.0	26.3	14.5	65	40	95	67	7.5	19.9	1.0	9.5	6	8	10 •	ENE 1	SE 5	C 0
8	106.5	106.5	109.6	107.5	17.7	24.7	17.1	19.2	25.9	16.3	90	49	84	74	2.0	16.0	3.2	7.1	8	4	5	C 0	WSW 5	W 3
9	111.2	112.5	112.8	112.2	16.4	21.1	16.8	17.8	21.5	13.1	76	56	84	72	4.4	10.9	3.1	6.1	0	1	4	W 2	NE 4	C 0
10	112.2	111.5	111.5	111.7	18.5	24.2	19.5	20.4	27.6	13.6	80	66	65	70	4.3	10.4	7.9	7.5	1	4	9	NNE 1	NE 3	WSW 6
11	111.5	112.8	111.6	112.0	19.2	17.7	16.9	17.7	20.9	14.6	76	85	81	81	5.2	3.0	3.7	4.0	2	9 •	9	W 2	NNE 1	NW 3
12	109.7	108.9	108.0	108.9	15.7	16.4	14.1	15.1	17.1	13.9	86	84	93	88	2.4	2.8	1.1	2.1	10	10	0	N 2	N 2	C 0
13	106.8	104.8	102.8	104.8	15.4	21.8	17.7	18.2	22.0	11.3	77	46	74	66	4.1	14.1	5.3	7.8	0	4	9	SSW 1	SSE 5	ESE 2
14	101.2	101.3	104.2	102.2	15.5	19.6	15.0	16.3	20.0	12.6	90	72	89	84	1.7	6.3	1.8	3.3	10 •	9	10 •	C 0	NE 4	NW 5
15	106.2	107.6	110.5	108.1	14.0	14.5	12.9	13.6	17.0	12.7	88	79	92	86	2.0	3.4	1.3	2.2	10	10	10	WNW 4	W 5	WNW 3
16	110.6	112.5	114.0	112.4	14.6	15.4	14.3	14.6	16.2	12.4	87	76	73	79	2.2	4.3	4.5	3.7	9	9	9	W 7	W 9	SW 5
17	114.1	114.6	114.4	114.4	16.3	21.5	18.5	18.7	22.6	13.5	78	49	70	66	4.0	13.2	6.5	7.9	2	4	10	W 8	WNW 8	WSW 2
18	111.7	109.5	110.1	110.4	18.8	26.2	18.0	20.2	26.9	17.1	65	42	86	64	8.1	19.9	2.8	10.3	9	1	10 •	S 3	SW 12	WSW 5
19	113.5	115.6	117.7	115.6	14.6	18.9	14.5	15.6	19.6	12.8	67	43	59	56	5.5	12.4	6.8	8.2	3	4	2	W 9	W 9	WSW 5
20	121.1	123.5	123.1	122.6	13.1	17.4	13.6	14.4	18.6	10.8	66	46	57	56	5.1	10.9	6.7	7.6	5	5	5	W 8	WNW 10	SW 1
21	120.3	119.1	120.8	120.1	15.1	14.3	12.3	13.5	20.0	11.8	56	78	76	70	7.7	3.6	3.4	4.9	7	9	0	SW 3	N 7	W 2
22	122.1	120.0	115.3	119.1	14.1	19.9	15.5	16.2	21.3	8.8	74	36	69	60	4.3	14.9	5.5	8.2	0	7	3	SW 4	SSW 4	C 0
23	112.1	113.5	112.9	112.8	18.4	19.8	16.9	18.0	21.5	11.9	59	52	65	59	8.7	11.0	6.8	8.8	1	5	10	WSW 5	WNW 8	WSW 2
24	113.3	114.6	113.4	113.8	14.5	19.3	18.6	17.8	21.7	13.9	71	38	53	54	4.8	13.8	10.0	9.5	9	6	6	W 5	W 9	SW 1
25	111.5	110.0	108.3	109.9	17.2	25.8	22.3	21.9	27.5	15.4	60	31	53	48	7.8	22.8	12.7	14.4	9	2	9	WSW 9	SW 7	WNW 5
26	109.8	110.8	110.3	110.3	17.8	24.7	17.4	19.3	25.5	15.2	68	39	78	62	6.5	18.9	4.4	9.9	2	2	0	W 5	WSW 6	C 0
27	106.1	102.6	104.2	104.3	19.6	28.8	19.1	21.6	29.6	15.1	67	51	85	68	7.5	19.3	3.4	10.1	1	8	9	SE 3	SSE 6	C 0
28	111.6	116.9	120.9	116.5	14.6	17.5	14.4	15.2	19.8	13.8	62	37	59	53	6.3	12.5	6.6	8.5	7	4	1	W 9	W 14	WSW 5
29	123.7	124.3	123.7	123.9	14.1	18.9	16.0	16.2	20.3	13.1	80	55	69	67	3.2	10.3	5.6	6.4	10	6	1	WSW 7	WSW 8	C 0
30	124.3	124.3	124.7	124.4	17.2	23.4	16.9	18.6	23.8	13.2	65	38	61	55	6.9	17.9	7.5	10.8	0	0	0	W 7	NE 5	C 0
31																								
M	112.1	112.4	112.5	112.3	16.6	21.0	16.7	17.8	22.5	13.3	74	55	75	68	5.0	12.0	5.0	7.3	4.5	4.7	4.9	3.7	6.0	2.0

Gdańsk - Wrzeszcz $H_s = 13\,m$ $H_b = 12{,}4\,m$ $h_w = 15{,}5\,m$ Maj - Mai 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ LODU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	.	.	–	$= 20^{15}-24$, $\sqcup^{0}\,1^{00}-7^{00}$
3	7	4.2	.	–	$\bullet^{0}\,16^{30}-17^{15}$, $18^{45}-19^{10}$, (K) 13^{05} SW – K^{1} $13^{15}-14^{35}$ NE K^{0} $16^{40}-17^{15}$ S–E, $= \infty\,0^{00}-11^{45} = 19^{35}-22^{10}$, $\frown^{0}\,0^{00}-6^{00}$
4	8	0.7	.	–	$\bullet^{1}\,15^{15-40}$, $= 3^{40}-4^{45}$, $20^{15}-24$
5	7	2.8	.	–	$= 0^{00}-4^{15}$, $\frown^{2}\,2^{00}-9^{00}$
6	7	10.4	.	–	$\bullet^{0}\,0^{35}\,2^{40}$ $\bullet^{0-1}\,14^{40}\,11^{40}$ $\bullet^{0}\,13^{40}-14^{45}$ 17^{15-30}, $= 3^{40}-4^{40}$, $19^{35}-24$
7	7	4.1	.	–	$\bullet^{0}\,12^{34}-13^{45}$, $15^{32}-17^{20}$ $\bullet^{0-1}\,20^{10}$ $\bullet^{0}\,22^{02-10}$, $= 0^{00}-9^{15}$, $\frown^{0}\,1^{00}-8^{00}$
8	7	1.9	.	–	$\bullet^{0-1}\,10^{45}-16^{15}$
9	7	1.2	.	–	$\bullet^{0}\,6^{10}\,24$
10	7	0.7	.	–	$\bullet^{0}\,0^{00}\,14^{40}$ $\bullet^{0}\,20^{10}$, $\gg 15^{40}-20^{30}$
11	7	0.0	.	–	$\bullet^{0}\,7^{10}-8^{25}$
12	8	.	.	–	
13	7	0.3	.	–	$\bullet^{0}\,11^{35}\,17^{35}$, $\frown^{0}\,2^{00}-6^{00}$
14	7	10.2	.	–	$\bullet^{0}\,9^{15}-11^{30}$ $\bullet^{0-1}\,11^{45}\,18^{15}$ $\bullet^{0}\,19^{30}-24$
15	7	2.0	.	–	$\bullet^{0}\,0^{00}\,1^{10}\,3^{10}-4^{35}\,6^{40}-9^{45}\,10^{45}\,11^{45}$, $= 2^{15}-4^{35}$
16	8	2.1	.	–	$\bullet^{2}\,2^{55}-4^{15}$, $5^{40}-10^{45}$, $= 22^{35}-24$
17	7	0.0	.	–	$\bullet^{0}\,0^{20}\,7^{50}$, $= 0^{00}-9^{40}$, $\frown^{0}$ np
18	8	3.6	.	–	$\frown^{0}\,0^{00}-7^{00}$
19	7	0.0	.	–	$\bullet^{0}\,1^{35}-2^{45}$ $\bullet^{0}\,3^{45}\,9^{05}$, $= 6^{40}-7^{20}$
20	7	.	.	–	$=$ np
21	5	.	.	–	$=$ na, a–p, np
22	8	.	.	–	$=$ na, $\frown^{0}$ na – a
23	8	.	.	–	$\frown^{0}$ na
24	7	.	.	–	
25	7	.	.	–	
26	8	.	.	–	
27	7	.	.	–	$= 1^{30}-9^{15}$ $\infty-10^{15}$
28	7	1.2	.	–	$\bullet^{0}\,12^{30}\,14^{05}$ $\bullet^{0}\,17^{37}-18^{40}$ $\bullet^{0}\,20^{45}-21^{35}$, $=$ na
29	6	.	.	–	$= 6^{10}\,20^{10}$ $\equiv^{0}-22^{15}$ $=-24$
30	7	1.2	.	–	(K) 14^{30-41} K$^{0}-15^{02}$ (K) -15^{16} E-W, $=$ na, p–np
31	7	0.1	.	–	$\bullet^{0}\,7^{21}\,8^{10}\,11^{15}\,12^{50}$, $= 5^{30}-9^{40}$, $17^{20}-24$
Σ	–	46.7	–	–	UWAGI:

Czerwiec - Juin

1	7	.	.	–	$= 0^{00}-8^{40}$ $\infty-10^{40} = 22^{00}-24$, $\frown^{0}\,2^{00}-7^{00}$
2	7	.	.	–	$= 0^{00}-7^{45}$, $\frown^{0}\,3^{00}-7^{00}$
3	7	.	.	–	$= 3^{35}-6^{30}$
4	7	.	.	–	
5	8	.	.	–	
6	8	.	.	–	$= 3^{30}-8^{20}$ $\infty-9^{40}$ $\frown^{0}\,2^{00}-8^{00}$
7	6	4.8	.	–	$\bullet$ K$^{0}\,16^{03-35}$ SE-NW $\bullet^{0}\,19^{10}-24$ $\bullet$ K$^{0}\,22^{35}-24$ SW–W
8	7	8.0	.	–	$\bullet$ K$^{0}\,0^{00-15}$ W $\bullet^{0}-0^{50}$ (K) $14^{40}\,16^{35}$ $\bullet$ K$^{1}-18^{10}$ W HSW $\bullet^{0}-18^{20}$, $= p-24$
9	8	.	.	–	$=$ na
10	7	.	.	–	(K)$^{0}\,21^{55}-22^{40}$ N–NE, $=$ na, $\frown^{0}\,3^{00}-9^{00}$
11	7	0.2	.	–	$\bullet^{0}\,13^{45-55}$, (K) $12^{10}-13^{40}$ SW–SE, $= p$
12	6	13.4	.	–	$\bullet^{0}\,14^{20}-15^{35}$ $\bullet^{0-1}\,15^{35}-19^{40}$, $= 10^{05}-24$
13	8	0.9	.	–	$= 0^{00}-7^{15}$
14	7	14.6	.	–	$\bullet^{0}\,5^{10}-6^{15}$, $7^{15}-8^{20}$ $\bullet^{0}\,11^{18-32}$ $21^{43}-22^{35}$, (K) 14^{45-55} SW K$^{2}-16^{20}$ N, $=$ a
15	7	5.8	.	–	$\bullet^{0}\,0^{40}\,3^{10}$ $\bullet^{0-1}\,3^{10}\,10^{50}$ $\bullet^{0}\,12^{15}-13^{40}$ $19^{35}-20^{30}$ $\bullet^{0}-21^{40}$
16	7	0.9	.	–	$\bullet^{0}\,2^{20}-3^{15}$, $9^{50}\,13^{05}$
17	7	0.0	.	–	
18	7	0.0	.	–	$\bullet^{0}\,2^{35}-3^{15}$, $21^{15}\,23^{35}$, $\gg 11^{40}-17^{15}$
19	8	.	.	–	
20	8	.	.	–	$\gg 12^{40}-15^{15}$
21	8	1.6	.	–	$\bullet^{0}\,14^{40}-15^{37}$
22	8	.	.	–	
23	8	.	.	–	
24	8	.	.	–	$\gg 16^{40}-17^{20}$
25	8	.	.	–	
26	8	.	.	–	
27	7	6.2	.	–	$\bullet^{0-2}\,14^{40}-15^{20}$ (K) 14^{20-40} SSE K$^{2}-15^{20}$ (K) -15^{30} WNW, $= 19^{40}-24$
28	8	.	.	–	$= 0^{00-35}$, $\gg 9^{40}-16^{20}$
29	8	.	.	–	
30	8	.	.	–	
31					
Σ	–	56.4	–	–	UWAGI:

2*

Gdańsk - Wrzeszcz — $\varphi = 54°23'$ — $\lambda = 18°36'$ — Lipiec - Juillet 1961

DNI	CIŚNIENIE Pśr 900 +				TEMPERATURA t						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			POGODA			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	125.1	124.5	122.3	124.0	16.5	20.0	16.5	17.3	21.7	10.1	69	64	80	71	5.8	8.4	5.9	6.0	1	5	2	C 0	NE 2	C 0
2	121.0	120.8	118.7	120.2	20.1	24.0	21.2	21.6	25.4	11.7	58	45	64	56	9.9	16.4	9.2	11.8	0	0	0	WNW 4	NE 5	C 0
3	116.7	112.3	110.7	113.2	22.9	32.3	20.0	25.8	33.1	18.8	60	26	68	51	11.2	35.8	7.4	18.1	0	5	10	C 0	SSW 7	NW 7
4	109.8	107.2	102.8	106.6	16.7	19.2	16.2	17.1	20.6	13.5	75	68	73	71	5.2	7.2	4.9	5.8	6	9	10•	SSW 3	SSW 5	S 5
5	104.9	107.4	108.9	107.1	13.3	15.1	12.3	13.2	18.1	12.0	71	70	71	71	4.5	5.1	4.2	4.6	9 •	7	2	SW 9	SW 8	SSW 5
6	110.4	112.0	114.1	112.2	11.0	14.0	12.6	12.6	15.3	8.9	74	61	87	74	3.4	6.2	1.9	3.8	7	9	4	SW 7	SSW 6	WSW 5
7	114.9	116.4	117.5	116.3	12.1	14.3	12.8	13.0	17.0	10.4	82	84	76	81	2.5	2.5	3.6	2.9	7	9 •	1	SW 8	WSW 8	C 0
8	116.6	115.7	112.8	115.0	13.7	18.2	14.3	15.1	20.3	10.3	75	58	93	75	3.9	8.8	1.1	4.6	9	9	10 •	SW 4	S 4	SSE 2
9	106.6	105.1	106.3	106.0	15.3	18.9	13.8	15.4	19.7	12.5	79	66	91	79	3.7	7.5	1.5	4.2	7	10	10	SSE 2	S 3	W 1
10	106.5	107.1	108.2	107.3	13.3	17.2	14.5	14.9	18.2	11.7	86	56	75	72	2.1	8.7	4.1	5.0	9	9	9	WSW 3	WSW 7	SW 3
11	108.9	109.9	110.2	109.7	14.1	17.9	15.6	15.8	20.1	11.1	77	51	75	68	3.7	10.1	4.4	6.1	5	8	10	SW 4	WSW 7	C 0
12	107.9	107.3	107.1	107.4	16.5	22.7	15.5	17.6	23.0	13.3	89	58	87	78	2.2	11.7	2.3	5.4	9	4	3	SSW 1	WSW 6	C 0
13	102.9	98.5	99.2	98.2	16.3	25.8	18.8	19.9	25.8	13.6	91	61	94	82	1.7	13.1	1.3	5.4	9	4	10 • K	C 0	ENE 5	SW 2
14	95.6	100.4	104.8	100.3	16.5	15.4	14.7	15.5	18.9	14.1	89	75	77	80	2.2	4.4	3.8	3.5	9	10	10	S 2	SSW 8	SSW 2
15	106.6	107.2	110.5	108.1	14.2	20.3	15.1	16.2	20.6	12.8	82	66	87	78	2.9	8.0	2.3	4.4	7	9	1	SSE 2	S 3	C 0
16	109.2	109.1	108.3	108.9	14.7	15.6	15.2	15.2	17.4	10.5	85	89	87	87	2.5	1.9	2.3	2.2	10	10 •	10	C 0	WSW 1	C 0
17	106.2	105.3	104.2	105.2	15.3	20.4	16.5	17.2	22.7	11.9	82	56	84	74	3.2	10.7	3.1	5.7	5	6	9	C 0	S 2	C 0
18	103.5	103.8	103.6	103.6	13.9	16.1	15.5	15.2	18.6	12.8	89	79	85	84	1.8	3.8	2.6	2.7	9	10	10	C 0	NW 2	SSW 1
19	104.4	105.4	106.2	105.3	14.7	17.7	15.5	15.8	20.2	13.0	86	73	87	82	2.4	5.5	2.3	3.4	9	7	6	SW 5	SSW 4	C 0
20	107.4	107.5	108.6	107.8	15.2	20.8	15.1	16.6	21.4	11.8	85	58	86	76	2.6	10.2	2.5	5.1	5	9	9	S 1	SW 2	C 0
21	106.9	106.5	106.3	106.6	14.5	16.6	15.3	15.4	19.7	12.2	93	79	89	87	1.1	4.1	1.9	2.4	10 •	9	9	C 0	NW 3	C 0
22	106.2	107.4	108.4	107.3	16.5	15.4	15.2	15.6	19.7	13.4	82	88	79	83	3.5	2.1	3.7	3.1	3	9 • K	9	WSW 9	W 7	SW 2
23	109.0	111.0	113.1	111.0	14.7	17.0	14.6	15.2	19.1	13.7	85	74	78	79	2.5	5.1	3.6	3.7	9	9	6	SW 6	WSW 6	SW 2
24	113.9	116.5	118.9	116.4	14.6	18.0	13.5	14.9	19.3	12.5	85	65	74	75	2.5	7.2	4.0	4.6	8	8	2	WSW 7	W 9	SW 2
25	119.8	121.0	119.4	120.1	14.9	16.8	14.3	15.1	17.6	12.0	81	59	71	70	3.3	7.9	4.8	5.3	9	9	10	WSW 5	WNW 9	SSW 5
26	115.0	111.8	106.5	111.1	14.8	18.0	19.7	18.0	21.0	13.7	84	74	61	73	2.7	5.4	9.0	5.7	10	10 •	10	SW 3	SW 8	SSW 5
27	105.4	102.0	103.2	102.9	17.4	19.5	14.9	16.7	20.3	14.8	78	68	76	74	4.4	7.3	4.0	5.2	8	10	9	SW 8	SW 6	SW 5
28	101.4	100.6	102.2	101.4	14.5	14.6	14.0	14.3	16.2	13.0	80	88	89	86	3.2	2.0	1.8	2.3	10	10 •	9	S 3	S 2	C 0
29	105.3	108.8	112.2	108.8	14.1	16.9	14.5	15.0	18.9	11.7	83	61	76	73	2.7	7.5	3.9	4.7	9	9	8	WSW 4	SW 7	SW 4
30	114.4	115.1	116.0	115.2	14.3	18.3	15.6	16.0	18.5	11.6	83	75	90	83	2.7	5.2	1.7	3.2	9	9	9	WSW 2	NE 3	NNE 1
31	112.1	108.3	106.4	108.9	14.9	15.2	15.7	15.4	18.1	13.8	94	97	83	91	0.9	0.6	3.0	1.5	10 •	10 •	9	NNW 8	N 8	ESE 4
M	109.4	109.4	109.4	109.4	15.2	18.5	15.5	16.2	20.2	12.5	81	67	80	76	3.4	7.8	3.6	4.9	7.3	8.0	7.3	3.5	5.3	1.9

Sierpień - Août

1	105.2	107.1	110.3	107.5	14.8	15.6	14.1	14.6	17.2	13.8	94	87	91	91	0.9	2.3	1.5	1.6	9	10 •	10 •	W 2	WSW 6	SW 7
2	111.7	111.9	112.2	111.9	15.7	21.1	16.0	17.2	21.4	13.4	78	53	85	72	3.9	11.8	2.7	6.1	6	9	10	S 3	SSW 7	C 0
3	112.7	113.1	116.7	114.2	15.6	19.0	12.6	15.0	19.9	12.5	88	73	89	83	2.1	6.0	1.6	3.2	10	8	0	C 0	SSW 5	SW 2
4	116.8	114.3	110.0	113.7	12.6	16.4	13.5	14.0	17.6	10.5	86	66	93	82	2.1	6.3	1.1	3.2	7	10 •	10 •	SSW 2	S 3	S 4
5	111.0	112.8	111.5	111.8	15.6	20.2	16.5	17.2	20.8	13.0	82	48	88	73	3.2	12.3	2.4	6.0	9	6	10	WSW 5	WSW 8	W 3
6	107.2	107.6	109.8	108.2	18.7	26.7	17.2	20.0	27.3	15.3	87	50	74	70	2.8	17.4	5.1	8.4	4	6	9	C 0	SW 8	NW 1
7	110.7	110.9	111.2	110.9	13.9	15.8	15.1	15.0	18.0	12.8	95	82	91	89	0.7	3.2	1.5	1.8	10 •	10 •	6	C 0	C 0	WNW 2
8	116.4	116.6	115.2	116.1	14.5	19.3	15.9	16.4	19.6	12.0	82	63	86	77	2.9	8.2	2.5	4.5	4	7	10	W 5	NE 3	SE 2
9	114.8	117.5	119.8	117.4	17.5	22.5	16.4	18.2	23.3	14.2	83	52	81	72	3.4	13.0	3.4	6.6	7	6	7	NW 2	SW 4	C 0
10	120.2	119.0	116.5	118.6	17.4	22.3	15.5	17.7	24.3	13.1	71	56	95	74	5.9	11.7	0.9	6.2	2	9	10 •	C 0	S 3	NNW 2
11	112.9	113.5	114.1	113.5	16.5	16.8	15.5	16.1	17.5	14.7	89	87	94	90	2.2	2.5	1.1	1.9	10	10 •	5	NNE 5	NNE 5	C 0
12	113.1	112.3	114.1	113.2	16.2	19.5	14.7	16.3	23.0	13.6	93	71	83	82	1.4	6.5	2.9	3.6	9	8	6	C 0	NNW 6	NW 2
13	114.6	116.0	117.6	116.1	13.8	17.7	13.6	14.7	18.7	11.1	77	56	80	71	3.7	8.8	3.2	5.2	4	6	2	SW 3	W 8	W 2
14	117.6	116.7	115.4	115.9	13.0	19.9	13.4	14.9	20.1	10.7	88	45	91	74	1.8	13.2	1.4	5.5	10	7	9	SW 2	SW 6	C 0
15	108.2	107.5	105.2	107.0	13.8	17.1	13.5	14.5	17.4	11.4	86	65	87	79	2.2	6.9	2.0	3.7	9	9	9	S 1	SSW 6	S 2
16	104.1	103.4	102.3	103.3	15.1	12.2	12.2	12.4	16.9	11.7	80	87	86	84	3.0	1.9	2.0	2.3	9	9 •	6	S 5	SW 7	S 1
17	102.0	103.2	105.3	103.5	13.6	16.4	12.3	15.6	17.8	10.9	83	64	89	79	2.7	6.7	1.5	3.6	7	9	2	SW 3	S 4	C 0
18	104.3	104.6	103.7	104.2	13.9	18.3	14.0	15.0	19.1	10.6	89	60	84	78	1.8	8.4	2.5	4.2	9	8	1	W 6	NW 5	W 6
19	99.8	98.5	99.7	99.3	13.6	14.0	13.2	13.5	15.3	11.9	85	92	90	89	2.3	1.3	1.6	1.7	6	10 •	9	SW 4	S 2	SW 1
20	99.4	101.8	103.9	101.7	13.7	18.1	15.6	15.8	19.4	12.7	86	53	73	71	2.2	9.7	4.8	5.6	7	6	7	WSW 4	W 8	W 8
21	104.1	105.7	104.8	104.9	13.8	16.1	15.7	15.3	16.7	12.7	79	81	85	82	3.4	3.4	2.6	3.1	9	10	9	WSW 7	SW 7	SW 6
22	101.5	100.4	100.4	100.8	16.4	18.6	13.5	15.5	20.0	13.3	81	71	84	79	3.4	6.3	2.1	3.9	8	9	7 •	SSW 6	SW 6	SW 7
23	101.5	103.7	107.3	104.2	13.8	14.3	13.9	14.0	17.2	11.9	86	88	79	84	2.2	2.0	3.4	2.5	7	9 •	6	SW 5	WNW 7	WSW 8
24	110.1	112.0	112.4	111.5	13.1	16.7	13.5	14.1	17.3	12.5	93	58	90	80	1.1	8.0	1.6	3.6	9	5	9	WNW 3	WNW 8	SW 2
25	110.4	112.6	114.1	112.4	14.2	16.9	12.6	14.1	17.4	12.1	83	46	72	67	2.7	10.4	4.1	5.7	7	6	1	NW 5	W 9	WSW 6
26	116.3	118.0	118.1	117.5	12.6	14.2	15.8	14.6	16.0	11.2	85	78	91	85	2.2	3.6	1.5	2.4	10	10 •	10	WSW 5	SW 3	C 0
27	117.5	117.6	119.7	118.3	17.0	25.0	16.3	18.6	25.7	15.3	88	52	80	73	2.4	15.4	3.6	7.1	7	5	7	SW 2	WSW 8	W 4
28	121.1	122.1	122.0	121.7	14.1	18.9	16.5	16.5	19.8	13.5	83	65	81	76	2.7	7.7	3.7	4.7	10	8	4	W 7	W 8	W 8
29	121.5	123.1	123.1	122.6	15.6	19.1	13.8	15.6	20.1	13.7	85	63	89	79	2.6	8.1	1.8	4.2	4	7	0	NW 8	NW 6	NW 1
30	124.2	124.4	124.8	124.5	12.2	21.1	15.5	16.1	22.6	10.7	93	56	92	80	1.0	11.1	1.3	4.5	7	4	0	SSW 2	C 0	C 0
31	126.8	127.5	127.9	127.4	14.1	22.4	15.8	17.0	23.3	11.6	95	59	90	81	0.7	11.2	1.7	4.5	0	7	0	C 0	NE 2	C 0
M	111.5	112.1	112.5	112.0	14.7	18.5	14.6	15.6	19.7	12.5	86	65	86	79	2.4	7.9	2.4	4.2	7.3	7.8	6.2	3.2	5.4	2.8

Gdańsk - Wrzeszcz $H_s = 13\ m$ $H_b = 12{,}4\ m$ $h_w = 15{,}5\ m$ Lipiec - Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	.	.	–	⌓ 2⁰⁰–8⁰⁰
3	7	.	.	–	∞ 9³⁵–10³⁰
4	8	0.0	.	–	● 11⁴⁰–13³⁵
5	8	0.6	.	–	▽● 7³⁵–18⁵⁰
6	8	2.6	.	–	▽ 0-1 17¹⁰–18³⁵
7	8	0.0	.	–	▽● 11⁰³–18 12⁴⁷–14³⁵
8	7	3.8	.	–	● 12⁴⁰–13³⁰ 14³⁵–15¹⁵ (R) 17²⁸⁻³³ SW ● R 18³⁰ (R)–18⁴⁰ E. = np
9	7	7.1	.	–	● 0⁰⁰–3¹⁵ ● 0-1 15¹⁶–16³⁰ ● 1 –17²⁰ : = 0⁰⁰–8⁴⁵
10	8	0.0	.	–	▽● 11⁰⁵ 15⁰⁵
11	8	2.3	.	–	
12	7	.	.	–	● 1³⁵–2²⁸ ▽● 4³⁵–5⁴⁵ : = 5⁴⁵–8⁴⁵
13	7	14.9	.	–	(R) 19⁵⁰–20⁰⁵ SW ● R 20¹⁵ (R)–21⁰⁰ NE, 21⁰⁰⁻¹⁰ SW ● R 1–22³⁵ (R)–23¹⁰ NE. = 3³⁰–10²⁰ ∞–11⁴⁰
14	7	0.0	.	–	● 0⁴⁹–5⁴⁰ ▽● 8⁵⁰–9⁰⁵ » 2⁴⁰–5³⁰
15	7	0.0	.	–	▽● 10³⁵–11¹⁰ 11⁴⁰–12¹⁵
16	6	0.9	.	–	● 12¹⁵–14⁴⁰ 16⁴⁰ 17¹⁰ , = 3⁴⁰–11⁴⁰
17	7	9.4	.	–	= 3⁴⁰–10⁴⁵
18	7	0.8	.	–	● 1¹⁵–2²⁰ (R) 2³⁵⁻³⁷ ● R 4³⁵ (R)–6¹⁵ NE ● 6⁴⁵–7¹⁵ 10¹⁰ 11²⁰, 22⁴⁵ 24
19	8	2.9	.	–	● 0⁰⁰ 3¹⁰ ▽ 1-0 13⁰⁵⁻³⁰
20	7	0.8	.	–	▽● 12⁴⁵–13⁰² ▽ 1 14¹⁰–15⁴⁰ ▽● 16⁴⁵–17⁰⁵ R 1 14¹⁸–15¹⁵ W-N, = np; ⌓ 1 na
21	7	6.2	.	–	● 2⁵⁰–3³⁵ 6⁴⁰–10¹⁰ ▽● 10²³–16¹⁰ ▽ 1 19⁰⁷⁻⁴⁵ : = 0⁰⁰–9⁴⁵
22	7	4.3	.	–	● R 1 11⁵⁰–14⁴⁵ NW-E
23	8	0.0	.	–	▽● 18²⁸–40
24	7	0.2	.	–	▽● 8¹⁸–10²⁰ 12²⁰–13¹⁵
25	8	0.0	.	–	▽● 9²⁰–30
26	6	0.9	.	–	● 5⁴⁰–6¹⁰ 9³⁵ 14¹⁰ 22⁴⁰–24 : = 8⁴⁰–14⁴⁰ ∞–23¹⁵ =–24
27	7	1.6	.	–	● 0⁰⁰–40 ▽● 12⁵⁰ 17¹⁵ , = 0⁰⁰–5⁴⁰
28	6	0.9	.	–	● 10²⁰ 16⁴⁰
29	8	.	.	–	
30	8	1.4	.	–	
31	5	24.4	.	–	● 2⁴⁵–4²⁵ 6⁴⁵–13⁴⁵ ● 1–15²⁰ ● 0–16³⁵
Σ	–	86.0	–	–	UWAGI.

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1	6	6.0	.	–	● 0-1 1⁰⁵–2⁴⁰ 4³⁵ ▽● 6³⁵–7¹⁵ ▽ 0-1 9²⁰ 22⁴⁰
2	7	0.5	.	–	● 17¹⁵ 23⁴⁰ , = 23⁴⁰–24
3	6	5.3	.	–	▽● 14²⁰ 17³⁵ , R 1 14³⁰–15¹⁰ W-E : = 0⁰⁰–15³⁵
4	7	1.9	.	–	● 13³⁵ 18⁴⁰ ● 1–19¹⁵ ● 0 23⁴⁰ ● 1–24
5	7	0.4	.	–	● 1 0⁰⁰–30
6	7	9.2	.	–	● 0 4⁴⁰–7¹⁵ ▽ 1 23¹⁵–24 : (R) 23¹⁰–20 R 1–24
7	7	1.8	.	–	▽ 0-1 0⁰⁰–2³⁵ ● 0 5⁴⁵ 10⁴⁰ 13⁴⁵–14⁴⁰ ▽ 0-1 19⁴⁰–20⁴⁰, R 1 0⁰⁰⁻⁵⁰ NE : = 10⁴⁰–12⁴⁰
8	8	0.3	.	–	● 20¹⁵ 21⁴⁰
9	8	.	.	–	
10	7	12.0	.	–	● 0 19²⁰ 21⁰⁵ ● 1–24
11	7	0.0	.	–	● 1-0 0⁰⁰–35 ● 0 11³⁵ 16⁴⁰ , = 21¹⁵–24, ⌓ 1 23⁰⁰–24
12	7	.	.	–	= 0⁰⁰–11¹⁵, ⌓ 1 0⁰⁰–8⁰⁰
13	8	.	.	–	
14	8	1.2	.	–	▽● 0 17⁴⁵–18¹⁵
15	7	2.4	.	–	● 4³⁵–5⁴⁰ 12²⁰ 13⁴⁰ ▽● 1-0 14²⁰–15⁰⁵ ▽● 0 15²⁰–16¹⁵
16	7	0.8	.	–	▽● 0 12²⁰–3⁵ 13²⁵ 14⁰⁵ 16⁵⁰–17¹⁰
17	7	0.6	.	–	▽● 0 12⁴⁵–13¹⁵ 17⁰²–18¹⁰
18	7	0.0	.	–	▽● 0 14⁰⁶–20 » 15¹⁵–17⁴⁰
19	6	10.8	.	–	● 0 11¹⁰–14¹⁰ ▽● 0-1 15¹⁰–16²⁰ ● 0–18¹⁵
20	8	0.8	.	–	▽● 0 10⁴³–11³⁵ » 17¹⁵–20¹⁰
21	7	0.2	.	–	▽● 0 3⁰³–20 ● 0 9³⁵–19⁴⁰
22	7	2.1	.	–	▽● 1 18⁰⁵–50 ▽● 0 21²⁰–50
23	8	12.0	.	–	▽● 0 3³⁰–50 ▽● 0-1 10¹⁵ 14³⁰ ▽● 0 22⁴⁰–23⁰⁵
24	8	1.1	.	–	▽● 0-1 5¹⁵–7⁴⁵ ▽● 0 8⁴⁰–10¹⁰
25	8	.	.	–	● 6¹⁵ 7²⁰
26	7	0.2	.	–	● 0 8³² 9¹⁰ 12¹⁵ 14³⁵ , = 21³⁵–24
27	8	3.4	.	–	● 0 1⁴⁰ 2³⁵ ▽● 1 15⁴⁰–16⁰⁵ , = 0⁰⁰–8⁴⁰
28	7	.	.	–	
29	8	.	.	–	
30	7	.	.	–	= 3³⁰–5³⁰ ≡ 0–5⁵⁵ =– 10⁴⁰
31	7	.	.	–	= 4³⁰–10²⁰ , 20⁴⁰–24, ⌓ 2 3⁰⁰–8⁰⁰, np
Σ	–	73.0	–	–	UWAGI.

Gdańsk - Wrzeszcz — φ = 54°23' — λ = 18°36' — Wrzesień - Septembre 1961

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	126.9	125.1	121.6	124.5	19.1	26.5	20.7	21.8	27.2	13.8	71	45	65	60	6.4	19.0	8.6	11.3	1	1	0	SW 2	SW 4	SSW 2
2	119.0	117.4	115.2	117.2	19.0	27.5	15.5	19.4	28.0	15.3	70	43	85	66	6.6	21.1	2.6	10.1	0	0	0	SW 2	W 5	C 0
3	111.0	110.1	109.0	110.0	15.8	21.5	14.9	16.8	23.4	13.4	84	61	86	77	2.8	10.0	2.4	5.1	1	1	0	C 0	NE 3	C 0
4	111.2	114.4	114.7	113.4	16.2	16.5	14.1	15.2	17.5	11.6	84	69	78	77	2.9	5.9	3.6	4.1	9	9	9	ENE 3	NE 5	NE 1
5	114.5	113.9	109.8	112.7	14.1	17.7	15.6	15.8	18.5	13.6	70	55	63	63	4.8	9.0	6.5	6.8	9	4	10	SE 1	NE 5	C 0
6	104.1	104.6	104.2	104.3	15.6	21.5	17.1	17.8	21.9	13.4	95	68	93	85	0.9	8.2	1.4	3.5	9	7	10	C 0	SW 2	C 0
7	101.3	101.6	98.8	100.6	14.0	16.0	13.2	14.1	18.2	13.2	94	68	80	81	0.9	5.8	3.0	3.2	10	10	4	C 0	SW 5	S 6
8	99.3	101.2	106.0	102.2	12.2	13.3	12.7	12.7	14.0	11.0	86	84	87	86	2.0	2.5	1.9	2.1	9	9	10	SW 8	SW 10	W 6
9	109.4	110.5	112.0	110.6	13.5	17.7	11.7	13.6	18.2	11.6	87	65	89	80	2.0	7.0	1.5	3.5	5	9	9	W 6	NW 8	WNW 3
10	113.2	113.9	114.8	114.0	12.8	14.8	12.3	13.0	16.0	11.5	86	85	92	88	2.1	2.5	1.2	1.9	8	9	3	NW 2	NW 2	W 4
11	113.3	112.6	110.8	112.2	12.6	16.7	14.1	14.4	18.1	11.2	88	72	81	80	1.7	5.4	3.1	3.4	10	9	0	SW 3	SW 3	C 0
12	107.3	107.6	108.5	107.8	13.3	17.7	12.8	14.2	18.3	11.9	82	66	81	76	2.8	6.8	2.8	4.1	10 •	9	9	SW 7	SW 9	SW 2
13	108.9	111.7	112.5	111.0	11.9	17.4	14.5	14.6	17.9	10.7	84	51	73	69	2.1	9.8	4.5	5.5	4	8	10	SW 5	WNW 8	C 0
14	108.2	106.1	105.5	106.6	13.5	15.6	16.1	15.3	17.6	12.7	84	90	83	86	2.5	1.7	3.1	2.4	10 •	10	10 •	SSE 3	S 3	WSW 4
15	109.1	114.1	116.9	113.4	14.3	17.1	13.9	14.8	17.7	13.7	84	61	79	75	2.5	7.6	3.4	4.5	5	6	9	WNW 8	W 8	SW 3
16	116.9	117.8	117.9	117.5	17.7	23.0	18.5	19.4	23.4	13.1	85	65	85	78	3.0	9.7	3.1	5.3	9	7	0	WSW 4	WSW 8	C 0
17	117.2	116.4	116.6	116.7	15.1	28.3	18.1	19.9	28.8	14.4	91	48	90	76	1.5	19.8	2.1	7.8	0	0	0	SE 1	S 5	C 0
18	114.6	117.8	119.4	117.3	17.8	21.1	13.3	16.4	21.7	13.1	91	49	84	75	1.8	12.8	2.5	5.7	1	0	0	C 0	NW 8	W 5
19	120.8	122.0	123.7	122.2	12.5	19.7	13.5	14.8	19.8	10.4	88	51	76	72	1.7	11.3	3.7	5.6	0	1	6	NW 3	NW 6	N 5
20	125.5	126.1	125.5	125.7	11.5	14.9	12.9	13.0	16.3	10.6	87	70	84	80	1.9	5.0	2.4	3.1	8	4	5	C 0	NE 4	E 1
21	126.8	127.1	127.5	127.1	10.5	16.0	12.0	12.6	17.0	8.7	94	60	69	74	0.8	7.4	4.3	4.2	7	1	0	C 0	E 5	C 0
22	129.6	129.6	129.1	129.4	5.4	16.4	9.3	10.1	17.6	3.9	94	47	89	77	0.6	9.8	1.3	3.9	0	0	4	C 0	SE 3	C 0
23	129.2	127.9	126.9	128.0	5.4	17.8	8.7	10.2	17.8	4.7	94	41	90	75	0.6	12.0	1.0	4.5	0	0	0	C 0	C 0	C 0
24	125.4	124.1	122.3	123.9	4.8	17.9	9.3	10.3	18.1	3.1	90	37	88	72	0.8	12.9	1.4	5.0	0	0	0	C 0	SE 1	C 0
25	118.9	116.9	118.4	118.1	5.2	19.8	12.2	12.4	20.1	4.6	89	44	83	72	0.9	13.0	2.4	5.4	4	7	0	C 0	S 3	W 7
26	119.8	120.1	119.9	119.9	8.7	15.6	11.2	11.7	16.5	7.7	88	55	78	74	1.3	7.9	2.9	4.0	4	9	7	SW 6	WNW 7	C 0
27	118.7	118.1	118.6	118.5	8.2	15.7	9.4	10.7	16.6	7.4	94	62	92	83	0.6	6.7	1.0	2.8	1	4	2	C 0	N 1	C 0
28	119.9	120.1	121.3	120.4	5.1	17.7	9.6	10.5	18.4	4.7	95	51	89	78	0.4	9.8	1.3	3.8	0	1	0	C 0	ESE 4	C 0
29	121.6	120.4	120.0	120.7	6.5	19.2	12.6	12.7	19.7	5.1	94	44	77	72	0.6	12.3	3.4	5.4	1	2	7	SE 1	S 7	SSE 2
30	120.4	120.1	121.4	120.6	10.6	15.9	11.9	12.6	18.1	10.5	92	66	76	78	1.0	6.1	3.3	3.5	10	5	0	SE 2	SE 3	C 0
31																								
M	116.1	116.3	116.3	116.2	12.1	18.6	13.4	14.4	19.4	10.4	87	59	82	76	2.0	9.3	2.9	4.7	4.8	4.7	4.1	2.2	4.8	1.7

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1	124.1	124.9	127.0	125.3	6.9	13.9	12.3	11.4	15.2	6.1	97	72	82	84	0.3	4.4	2.5	2.4	0	4	9	C 0	SE 1	C 0
2	129.2	130.3	130.2	129.9	7.0	10.8	10.2	9.6	12.7	5.2	96	92	97	95	0.4	1.0	0.3	0.6	4	10	0	C 0	E 2	C 0
3	131.2	131.0	130.0	130.7	6.8	15.2	12.1	11.6	15.4	5.4	99	78	93	90	0.2	3.9	1.0	1.7	0	1	0	C 0	NE 4	E 2
4	129.0	127.9	127.3	128.1	6.9	19.0	13.1	13.0	19.6	5.5	96	52	72	73	0.4	10.5	4.3	5.1	0	1	0	C 0	SE 6	SE 1
5	126.3	124.8	125.2	125.4	8.9	19.3	11.7	12.9	19.6	8.6	85	41	77	68	1.7	13.3	3.1	6.0	0	0	0	C 0	SE 7	C 0
6	124.0	122.2	120.3	122.2	7.3	18.4	11.7	12.3	19.5	6.9	90	48	78	72	1.0	11.0	2.9	5.0	0	0	0	SSE 2	SSE 4	SE 1
7	117.9	114.7	113.2	115.3	7.5	16.8	11.7	11.9	17.2	6.8	93	52	61	69	0.8	9.2	5.3	5.1	0	0	0	SE 2	SE 7	SE 3
8	112.0	111.1	112.3	111.8	8.9	13.2	11.8	11.4	15.5	8.8	82	63	74	73	2.0	5.6	3.6	3.7	10	9	9	SE 2	SE 4	C 0
9	117.8	122.0	125.8	121.9	9.9	14.8	12.5	12.4	17.3	9.7	93	77	83	84	0.8	3.8	2.4	2.3	10 •	9	1	C 0	SW 5	SSW 2
10	128.0	126.1	127.2	127.8	8.8	18.4	12.7	13.2	19.6	8.3	97	60	86	81	0.3	8.5	2.1	3.6	10	7	0	C 0	SW 4	SSE 1
11	126.3	124.2	121.9	124.1	7.9	17.7	11.5	12.2	17.8	7.8	94	58	79	77	0.6	8.4	2.8	3.9	2	2	6	SSE 1	S 7	SSE 3
12	121.8	124.9	125.3	124.0	12.9	16.1	10.5	12.5	16.7	10.0	89	58	82	76	1.6	7.7	2.3	3.9	9	3	0	W 4	NW 8	W 7
13	124.5	125.9	126.5	125.6	8.5	14.8	8.6	10.1	15.6	8.2	90	54	92	79	1.1	7.7	1.0	3.3	6	4	0	WSW 3	WNW 7	NW 2
14	122.8	122.1	122.9	122.6	10.7	14.8	10.4	11.6	16.0	7.3	89	68	91	83	1.5	5.3	1.1	2.6	9	9	1	W 7	NW 8	WNW 5
15	119.9	118.1	117.1	118.4	11.4	13.8	12.3	12.4	14.6	9.5	85	69	78	77	2.0	4.9	3.2	3.4	6	8	10	WSW 6	W 9	W 6
16	116.0	115.1	110.9	114.0	11.9	12.5	8.7	10.4	12.8	8.5	72	69	88	76	3.9	4.5	1.3	3.2	9	10	0	SW 3	SW 4	S 2
17	106.1	102.7	96.0	101.6	10.6	11.3	10.7	10.8	13.0	8.3	82	78	87	82	2.3	3.0	1.7	2.3	9	10	10 •	SSW 4	SSW 8	S 6
18	89.8	90.1	92.6	90.8	10.6	12.7	11.9	11.8	13.0	8.6	87	87	94	89	1.6	1.9	0.8	1.4	9	10 •	10	SSE 5	SSE 3	S 2
19	94.8	98.3	101.3	98.1	11.5	13.1	12.3	12.3	13.9	10.9	89	88	96	91	1.5	1.8	0.5	1.3	10	10 •	10 •	SSE 2	SE 3	C 0
20	106.9	110.1	112.4	109.8	11.8	15.1	11.8	12.6	15.7	11.4	93	76	96	88	1.0	4.1	0.5	1.9	4	3	0	C 0	E 2	C 0
21	112.5	113.5	117.3	114.4	10.7	12.2	9.8	10.6	12.6	8.7	87	76	87	83	1.7	3.4	1.6	2.2	2	10	0	ESE 2	ESE 7	SE 3
22	120.9	123.3	125.2	123.1	6.6	11.9	7.8	8.5	12.9	5.8	97	74	90	87	0.3	3.6	1.1	1.7	10	6	1	SSE 5	S 4	C 0
23	124.5	122.9	121.1	122.8	4.3	8.9	7.3	7.0	10.2	3.3	76	66	77	73	2.0	5.9	2.3	2.7	2	4	0	SE 4	SSE 7	SSE 5
24	117.8	119.7	117.2	118.2	9.0	13.0	9.2	10.1	14.1	6.4	70	68	96	78	3.5	4.8	0.4	2.9	10 •	7	9	S 2	SW 4	SSE 2
25	111.4	110.6	111.0	111.0	7.4	11.2	12.0	10.6	12.3	7.2	88	78	86	84	1.2	2.9	2.0	2.0	9	10 •	10	S 7	S 6	SSE 2
26	111.8	110.1	110.9	110.9	11.4	12.9	12.0	12.1	14.4	10.6	93	92	91	92	1.0	1.3	1.2	1.2	10 •	10	9	S 2	SE 5	S 1
27	109.1	107.9	107.8	108.3	10.1	15.2	12.8	12.7	16.4	9.6	91	71	80	81	1.2	5.0	2.9	3.0	10	9	9	S 3	SSE 5	S 1
28	110.2	110.3	109.8	110.1	10.6	14.5	11.7	12.1	14.8	10.3	94	76	94	88	0.8	3.9	0.8	1.8	9	10	9	C 0	C 0	C 0
29	109.8	110.4	111.2	110.5	10.5	10.7	9.6	10.1	12.7	9.4	86	92	93	90	1.8	1.0	0.8	1.2	9	10 •	5	C 0	C 0	C 0
30	112.5	112.2	114.7	113.1	6.5	11.2	7.9	8.4	11.5	5.5	96	83	90	90	0.5	2.3	1.0	1.3	9	9	0	SW 2	SSW 5	SW 1
31	113.2	109.7	108.6	110.5	5.2	10.6	8.4	8.2	10.8	4.5	90	74	85	83	0.8	3.4	1.6	1.9	4	9	7	S 2	SSW 8	SW 6
M	116.8	116.7	116.8	116.8	9.0	14.0	10.9	11.2	14.9	7.8	89	71	86	82	1.3	5.0	1.9	2.7	6.2	6.6	4.0	2.3	5.0	2.1

Gdańsk - Wrzeszcz $H_s = 13\,m.$ $H_6 = 12{,}4\,m$ $h_w = 15{,}5\,m$ Wrzesień - Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–4²⁰, ⌓ ᵍ 0⁰⁰–5⁰⁰
2	7	.	.	–	
3	6	.	.	–	= 1³⁰–10³⁵ ∞–14²⁰ = 21⁴⁰–24
4	8	.	.	–	= 0⁰⁰–5⁴⁰
5	8	1.4	.	–	• ° 23³⁵ 24
6	6	5.2	.	–	• ° 0⁰⁰ 1⁴⁰, 3⁴⁰–4³⁰ • ¹⁻⁰ 22³⁰–23¹⁰ 24, = 6²⁰–24
7	7	10.7	.	–	• ° 0⁰⁰ ²⁰ 9²⁰⁻³⁵, ▽ ¹⁻⁰ –10¹⁵ ▽ ° 12⁰⁵–⁴⁰, = 0⁰⁰–11¹⁵
8	8	0.7	.	–	▽ ° 0²⁰–5³⁵, 8⁴⁰–9¹⁵ ▽ ° 14¹⁰ 18⁰⁵, ≫ 11⁴⁰–15¹⁵
9	8	0.0	.	–	• ▽ ° 15⁰⁵–¹²
10	7	0.2	.	–	• ▽ ° 13³⁵–14⁰³, 16⁰⁵⁻²⁰, 19²⁰⁻⁴⁰, 22⁴⁰–23²⁰
11	7	0.0	.	–	= 19¹⁵–21¹⁰
12	6	2.9	.	–	• ° 7¹⁵ 9⁴⁵ ▽ ¹⁻⁰ 14⁰⁵⁻³⁰, = 5⁴⁰–13⁴⁰ ∞–14⁰⁵
13	8	0.0	.	–	▽ ° 3⁵⁰–4²⁰
14	6	11.7	.	–	• ° 0⁴⁰–3³⁵ 7⁴⁵–13²⁰ 21⁴⁰–24 = 6³⁰–24
15	8	0.0	.	–	• ⁰⁻¹ 0⁰⁰–4³⁰ ▽ ° 10⁵⁰–11¹⁰; = 0⁰⁰–5⁴⁵
16	7	.	.	–	= 19⁴⁰–24, ⌓ ¹ 21⁰⁰–24
17	8	.	.	–	= 0⁰⁰–8⁴⁰, ⌓ ¹ 0⁰⁰–8⁰⁰
18	8	.	.	–	= 5³⁰–11⁴⁰, ⌓ ¹ 2⁰⁰–9⁰⁰
19	8	.	.	–	⌓ ¹ 2⁰⁰–8⁰⁰
20	8	.	.	–	
21	8	.	.	–	= 8¹⁵–9²⁰, ⌓ ¹ 0⁰⁰–8⁰⁰
22	8	.	.	–	= 8³⁰–10²⁰, 20⁴⁰–24, ⌓ ¹ 0⁰⁰–6⁰⁰, np, ⌴ ° 6⁰⁰–8⁰⁰
23	7	.	.	–	= 0⁰⁰–10¹⁵, ∞–11⁴⁰, ⌓ ¹ 0⁰⁰–4⁰⁰ ⌴ ¹–8⁰⁰ ⌓ ° np
24	7	.	.	–	= np, ⌓ ° 0⁰⁰–3⁰⁰ ⌴ ¹– 10⁰⁰
25	7	0.1	.	–	• ° 15²⁰⁻⁴⁵, = 0⁰⁰–9¹⁰ ∞–11⁴⁰ = 18⁴⁰–21²⁰, ⌴ ° 3⁰⁰–8⁰⁰
26	8	.	.	–	⌓ ° 0⁰⁰–9⁰⁰
27	8	.	.	–	= 18⁴⁰–24 ⌓ ° 3⁰⁰–9⁰⁰, np
28	7	.	.	–	= ∞ 0⁰⁰–11²⁰ = 19¹⁵–24, ⌓ ⁰⁻¹ a, np ⌴ ° 5⁰⁰–9⁰⁰
29	7	0.6	.	–	= 0⁰⁰–11¹⁵, 21³⁰–24, ⌓ ¹ 0⁰⁰–2⁰⁰ ⌴ °–10⁰⁰
30	7	.	.	–	• ° 0¹⁶–3³⁵, = na, p, np
31					
Σ	—	33.5	—	–	UWAGI:

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1	7	.	.	–	= 0⁰⁰–10⁴⁰ ⌓ ° 1⁰⁰–9⁰⁰
2	5	.	.	–	= 1³⁰–15³⁰, 17⁴⁰–24, ⌴ ¹ 2⁰⁰– a ⌓ ¹ p – np
3	7	.	.	–	= 0⁰⁰–10⁵⁰, 14³⁵–24, ⌓ ¹ 0⁰⁰–9⁰⁰
4	7	.	.	–	= 0⁰⁰–9⁴⁰, ⌴ ° 2⁰⁰– a
5	7	.	.	–	= 5²⁰–9³⁰ ⌓ ° 5⁰⁰– a
6	7	.	.	–	= 5³⁰–11³⁰, 17¹⁰–24
7	7	0.1	.	–	= 0⁰⁰–9⁴⁰, ⌓ ¹ 3⁰⁰–9⁰⁰
8	7	0.9	.	–	• ° 0³⁵–5⁴⁵, 18⁰⁵–19³⁵
9	7	2.6	.	–	• ° 4⁴⁰–5⁴⁰ 6¹⁸–9⁴⁰, = 5⁴⁰–7³⁰ ≡ °–8³⁷ = –10⁻⁰, 18⁴⁰–21³⁰
10	7	.	.	–	= 5¹⁵–10³⁰ 17⁴⁰–24, ⌴ ¹ 2⁰⁰–10⁰⁰, ⊕ 7⁴⁵–8³⁰
11	7	.	.	–	= 0⁰⁰–11³⁵, ⌓ ° 3⁰⁰–10⁰⁰
12	8	.	.	–	= 4⁴⁰–8⁴⁰
13	8	.	.	–	⌓ ° 4⁰⁰–9⁰⁰
14	8	.	.	–	
15	7	.	.	–	
16	7	.	.	–	= 17¹⁵–24
17	6	0.6	.	–	• ° 16⁴⁰–18³⁰, 19¹⁰–22³⁵, = 0⁰⁰–24
18	6	25.0	.	–	• ° 2³⁰ 5³⁰ • ⁰⁻¹ 12⁴⁰–18³⁵ 19⁴⁵ • ° 23³⁵ 24, = 0⁰⁰–12⁴⁰, 19⁴⁵–24
19	6	1.3	.	±	• ⁰⁻¹ 0⁰⁰–5³⁵ • ° 8²⁰ 21³⁵, = 0⁰⁰–24
20	6	.	.	–	= 0⁰⁰–24, ⌓ ⁰⁻¹ 19⁰⁰–24
21	7	.	.	–	= 0⁰⁰–1¹⁵, 14²⁵–24, ⌓ ¹ 0⁰⁰–8⁰⁰ ⌓ ° 21⁰⁰–24
22	6	.	.	–	= 0⁰⁰–24, ⌓ ¹ 1⁰⁰–10⁰⁰
23	7	3.5	.	–	= 0⁰⁰–11¹⁸, 15³⁶–20²⁸
24	7	0.3	.	–	• ° 4⁴⁰–8¹⁰ = a, p – 24 ⌓ ⁰⁻¹ 20⁰⁰–24
25	6	1.4	.	–	• ° 11⁴⁰–14³⁰ = 0⁰⁰–15²⁵, ⌓ ¹ 0⁰⁰–9⁰⁰
26	6	1.8	.	–	• ° 1³⁰–4⁴⁰, 6³⁰ 10³⁵–11⁵⁰ 12²⁰, = 4⁴⁰–14⁴⁵, 17¹⁵–24
27	7	.	.	–	• ° 2³⁵–3⁵⁰, = 0⁰⁰–12⁴⁰, 15³⁰–24
28	6	.	.	–	= 0⁰⁰–24, ⌓ ° 2⁰⁰–9⁰⁰
29	5	4.1	.	–	• ° 10²⁰ 11¹⁰–19⁴⁰, = 0⁰⁰–24, ⌓ ° 2⁰⁰–9⁰⁰
30	6	.	.	–	= 0⁰⁰–24
31	6	2.0	.	–	• ° 8⁴⁰–9¹⁰ 14³⁵–15³² ▽ ⁰⁻¹ 19²⁰ 22¹⁵, = 0⁰⁰–19²⁰, ≫ 18²⁰–20⁴⁰, ⌓ ° na – a
Σ	—	41.6	—	–	UWAGI:

Gdańsk – Wrzeszcz $\varphi = 54°23'$ $\lambda = 18°36'$ Listopad – Novembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	111.8	111.4	114.3	112.5	8.4	10.8	10.5	10.0	11.7	7.7	90	90	82	87	1.0	1.4	2.3	1.6	10 •	10 •	4	WSW 8	SW 8	W 6
2	117.9	116.1	109.4	114.5	8.7	10.9	9.3	9.6	11.0	8.3	86	75	85	81	1.5	3.5	2.0	2.3	8	9	5	SW 5	S 8	S 4
3	101.0	99.3	99.9	100.1	9.9	10.7	8.0	9.2	11.1	7.8	86	74	75	78	1.8	3.4	2.7	2.6	10	10	0	SSW 7	S 8	SW 8
4	102.8	105.7	110.7	106.4	4.1	7.7	5.8	4.8	8.1	3.3	82	56	82	75	1.5	4.6	1.5	2.5	3	2	6	SW 8	SW 8	SW 4
5	115.6	114.5	117.5	115.2	3.2	8.0	7.9	6.8	8.3	2.2	90	79	78	82	0.8	2.2	2.3	1.8	10	10	9	C 0	N 8	NE 6
6	119.1	118.7	116.8	118.2	8.5	9.1	8.9	8.8	9.2	7.7	70	83	95	82	3.3	2.0	0.8	2.0	9	10	10	NNE 8	NE 7	ENE 6
7	112.2	110.4	108.1	110.2	9.2	8.7	9.1	9.0	9.6	8.1	95	89	91	92	0.6	1.2	1.1	1.0	10 •	10	10	ESE 3	E 6	ESE 3
8	107.5	107.4	106.6	107.2	9.1	8.2	7.9	8.3	10.1	7.5	95	92	94	94	0.7	0.9	0.6	0.7	10 •	10	10 •	SE 4	SE 5	SE 5
9	105.2	104.4	104.6	104.7	5.3	7.3	6.2	6.2	8.0	5.0	84	79	86	83	1.4	2.2	1.3	1.6	10	10	2	S 2	SSE 6	SSE 3
10	104.3	103.7	103.4	103.8	4.9	7.7	7.7	7.0	8.2	4.0	92	84	97	91	0.7	1.6	0.3	0.9	10	10	10	SSE 4	SE 3	SSE 2
11	105.3	106.2	110.3	107.3	6.8	8.1	8.8	8.1	9.1	6.4	99	99	95	98	0.2	0.2	0.6	0.3	10	10 •	10	C 0	C 0	ESE 3
12	115.6	115.9	118.5	116.0	7.4	5.6	3.9	5.2	9.1	3.7	93	88	83	88	0.8	1.1	1.4	1.1	10	10	10 •	E 5	E 8	E 6
13	119.1	117.9	116.5	117.8	2.8	2.6	2.0	2.4	4.0	1.8	84	82	82	83	1.2	1.3	1.3	1.3	10	10	10	E 6	E 6	NE 7
14	114.2	115.9	118.4	116.2	2.0	3.0	4.4	3.4	4.4	1.5	85	83	74	81	1.1	1.3	2.2	1.5	10	10	10	NE 8	NNE 9	NE 5
15	118.0	116.9	114.9	116.6	3.9	5.8	4.9	4.9	6.0	3.2	74	62	78	71	2.2	3.4	2.0	2.5	10	10	10	C 0	WNW 4	SW 3
16	113.4	111.4	107.7	110.8	4.8	5.5	5.5	5.3	6.1	3.7	89	92	86	89	1.0	0.7	1.2	1.0	10	10 •	10	SW 4	SW 5	SSW 6
17	103.9	106.1	107.0	105.7	7.9	7.9	5.0	5.4	8.4	2.3	86	70	64	73	1.4	3.2	2.8	2.5	10	6 ⌒	2	WSW 7	NW 8	W 6
18	102.9	104.8	108.8	105.5	2.9	6.1	4.5	4.5	6.6	1.7	81	51	68	67	1.4	4.6	2.7	2.9	7	3	9	W 8	NNW 10	NW 8
19	112.9	119.2	124.6	118.9	2.8	1.8	4.4	3.4	5.1	-2.0	84	89	62	78	1.2	0.8	3.3	1.8	5	9 ⁂	9	NW 8	NNE 9	N 10
20	130.7	133.5	135.7	132.6	2.6	4.5	3.4	3.5	5.2	0.5	82	73	86	80	1.3	2.3	1.1	1.6	3	9	10	NE 8	NNW 1	W 2
21	129.1	127.4	125.1	127.2	2.8	5.0	2.3	3.1	5.3	1.5	77	73	77	76	1.7	2.3	1.7	1.9	10	7	8	W 3	W 7	WSW 5
22	122.1	120.8	118.9	120.6	2.8	4.9	0.6	2.2	5.8	0.0	86	73	60	73	1.1	2.4	2.6	2.0	10	4	0	SW 3	WSW 5	SW 3
23	115.6	113.3	111.8	113.6	-4.0	3.1	-0.7	-0.6	4.6	-4.6	94	71	81	82	0.3	2.2	1.1	1.2	0	0	0	C 0	SSE 3	S 1
24	112.3	114.5	116.6	114.5	0.2	4.9	3.0	2.8	5.6	-3.0	94	94	93	94	0.4	0.6	0.6	0.5	7	10	7	C 0	NW 4	SW 2
25	115.2	112.5	111.3	113.0	0.0	2.0	2.1	1.6	3.3	-1.1	96	100	89	95	0.2	0.0	0.8	0.3	9	10 =	6	C 0	C 0	SW 4
26	109.4	109.2	107.5	108.7	1.0	2.2	1.4	1.5	2.6	0.4	94	89	98	94	0.4	0.8	0.2	0.5	9	9	10	S 1	C 0	C 0
27	104.5	103.6	103.5	103.9	0.6	3.1	3.8	2.8	3.9	0.4	98	97	95	97	0.1	0.2	0.4	0.2	10	10 •	10	C 0	C 0	C 0
28	107.5	110.5	113.7	110.6	1.1	5.0	-1.3	0.9	6.0	-1.8	85	72	94	84	1.0	2.4	0.4	1.3	2	6	0	W 1	NW 2	C 0
29	113.0	111.5	109.4	111.3	0.4	2.2	4.9	3.1	5.1	-2.7	96	100	90	95	0.3	0.0	0.9	0.4	10	10 =	10	SSE 2	C 0	SSW 6
30	100.6	100.3	91.9	97.6	2.7	6.1	6.2	5.3	6.3	2.2	91	76	89	85	0.6	2.2	1.0	1.3	10 •	9	10 •	SW 9	WSW 10	SSW 10
31																								
M	112.0	112.1	112.0	112.0	4.1	6.0	4.9	5.0	6.9	2.5	88	81	84	84	1.0	1.8	1.4	1.4	8.4	8.4	7.2	4.1	5.3	4.5

Grudzień – Décembre

1	83.8	90.1	92.6	88.8	8.9	6.4	5.0	6.8	9.5	3.9	81	72	79	77	2.2	2.7	1.8	2.2	10 •	9	0	SW 12	WSW 8	SW 7
2	89.6	83.1	88.4	87.0	3.7	4.6	4.5	4.3	10.7	2.5	95	95	82	91	0.4	0.4	1.5	0.8	10 •	10	6	SSE 2	S 2	WSW 16
3	99.5	101.7	102.3	101.2	3.6	4.2	2.8	3.4	4.5	2.0	76	64	77	72	1.9	2.9	1.7	2.2	3	5	6	WSW 10	SW 10	SSW 7
4	100.2	104.1	108.5	104.3	1.0	4.1	2.2	2.4	4.6	0.8	87	77	89	84	0.9	1.9	0.8	1.2	0	9	10	S 2	SW 5	SW 3
5	97.3	98.8	97.0	97.7	7.4	12.8	10.4	10.2	13.7	0.1	91	78	81	83	0.9	3.3	2.4	2.2	10 •	8	10 •	SSW 7	SW 6	WSW 12
6	102.8	104.2	107.9	105.0	4.6	3.8	2.7	3.4	11.4	1.9	57	58	74	63	3.6	3.3	1.9	2.9	5	6	0	SW 9	SW 9	SW 10
7	110.1	112.3	113.2	111.9	1.0	1.7	0.5	0.9	2.8	-0.1	88	76	77	80	0.8	1.6	1.5	1.3	2	9	2	SW 4	SW 6	SW 6
8	112.9	112.7	113.5	113.0	0.6	2.1	1.0	1.2	2.4	-1.0	81	71	77	76	1.3	2.0	1.5	1.6	2	7	6	SSW 5	SW 8	SW 7
9	116.0	117.3	116.4	116.6	-0.2	1.6	-1.6	-0.4	1.9	-1.8	90	74	96	87	0.6	1.8	0.2	0.9	2	1	10	W 6	SW 4	C 0
10	111.0	109.6	107.4	109.3	-1.0	0.1	1.4	0.5	1.5	-2.4	87	90	94	90	0.8	0.7	0.4	0.6	9	10 ⁂	10 •	SSE 4	SSE 3	S 2
11	102.5	96.3	96.1	98.3	1.7	1.6	1.5	1.6	2.1	0.4	96	94	96	95	0.3	0.4	0.3	0.3	10	10 •	10	SSE 1	SE 2	C 0
12	105.5	109.6	116.0	110.4	2.5	0.7	-0.3	0.6	3.1	-1.1	88	83	66	79	0.9	1.1	2.0	1.3	10	10	10	NE 5	NE 6	NE 6
13	122.7	127.8	131.0	127.2	1.0	-0.6	-3.5	-1.6	1.0	-3.7	55	81	78	71	3.0	1.1	1.0	1.7	9	6	9	NNE 5	NE 5	S 1
14	131.5	131.7	129.6	130.9	-4.8	-3.1	-1.2	-2.6	0.0	-6.0	88	77	60	75	0.5	1.1	2.2	1.3	10 ⁂	10 ⁂	7	S 2	NE 6	NNE 13
15	125.9	125.9	132.0	127.3	-0.2	0.0	-8.0	-4.0	1.3	-8.2	61	98	78	79	2.3	0.1	0.7	1.0	9	10 ⁂	10 ⁂	NNE 15	NNE 17	SE 2
16	137.8	141.8	145.7	141.8	-10.9	-10.7	-13.7	-12.2	-7.6	-15.8	80	73	83	79	0.5	0.7	0.4	0.5	3	1	0	SE 1	C 0	C 0
17	145.2	144.0	142.0	143.7	-9.3	-5.0	-6.9	-7.0	-4.9	-14.8	60	73	83	72	1.2	1.1	0.6	1.0	10	9	0	WSW 2	W 4	C 0
18	138.0	135.6	131.9	135.2	-5.0	0.6	2.1	0.4	2.3	-7.9	84	80	93	86	0.8	1.3	0.5	0.9	9	10	10	WNW 2	W 8	NW 5
19	128.6	128.6	128.2	128.5	3.5	4.2	1.4	2.6	4.5	0.8	88	79	92	86	0.9	1.7	0.6	1.1	10	3	2	NW 7	NW 7	WNW 5
20	117.4	111.9	112.2	113.8	3.2	3.5	2.1	2.7	4.7	0.8	88	90	85	88	0.9	0.8	1.0	0.9	7	9	9	WSW 9	WNW 9	WNW 10
21	109.8	113.2	113.7	112.2	-0.6	-0.6	-2.4	-1.5	2.4	-3.0	88	89	74	84	0.7	0.6	1.3	0.9	10 ⁂	8	8	NNW 14	N 15	WNW 6
22	106.8	105.1	109.1	107.0	-4.0	-2.1	-5.1	-4.1	-1.4	-5.5	77	52	88	72	1.0	2.5	0.5	1.3	3	5	9 ⁂	W 7	N 9	NW 1
23	111.9	113.0	114.6	113.2	-5.5	-2.8	-4.8	-4.5	-0.6	-7.5	82	88	91	87	0.7	0.6	0.4	0.6	4	6	3	W 5	N 7	WNW 5
24	114.5	113.2	111.5	113.1	-7.5	-5.3	-7.1	-6.8	-4.4	-9.5	79	68	74	74	0.7	1.3	0.9	1.0	5	1	9	SW 3	SSW 7	SW 7
25	109.3	109.3	108.1	108.9	-7.3	-4.7	-8.6	-7.3	-5.5	-8.6	74	55	56	62	0.9	1.9	1.4	1.4	9	8	2	SW 3	S 1	SW 6
26	105.5	105.6	105.9	106.0	-12.0	-10.8	-10.3	-10.8	-8.3	-14.6	74	73	84	77	0.6	0.7	0.4	0.6	0	2	7	SSE 1	SE 1	C 0
27	111.7	114.8	117.1	114.5	-7.7	-6.5	-13.5	-10.3	-4.9	-14.9	96	91	84	90	0.1	0.3	0.4	0.3	10 =	10	0	C 0	C 0	C 0
28	113.0	112.5	109.4	112.3	-17.5	-15.0	-10.9	-13.5	-10.8	-17.5	85	82	85	85	0.2	0.3	0.4	0.3	0	9	10	C 0	SSE 1	SSE 2
29	107.6	107.8	108.4	107.9	-6.4	-4.1	-2.7	-4.0	-2.5	-11.0	86	87	95	89	0.5	0.6	0.3	0.5	10	10	10	S 2	SSE 3	SSE 2
30	105.9	104.4	104.4	104.9	-2.7	0.4	-0.3	-0.7	1.0	-4.2	95	92	94	94	0.2	0.5	0.4	0.4	10	10	10	SSE 4	S 4	SSE 3
31	102.8	103.6	100.3	102.3	1.1	3.2	-0.4	0.9	3.9	-0.9	90	81	88	86	0.6	1.3	0.7	0.9	10	3	0	SSE 4	S 1	SSE 3
M	112.3	112.3	113.4	112.7	-1.8	-0.3	-2.1	-1.6	1.3	-4.7	82	79	82	81	1.0	1.3	1.0	1.1	6.8	7.2	6.3	4.9	5.6	4.7

Gdańsk - Wrzeszcz $H_s = 13\,m$ $H_b = 12.4\,m$ $h_w = 15.5\,m$ Listopad - Novembre 1961

DNI	WIATR KIERUNEK	WIATR SIŁA V	OPAD R	GRUBOŚĆ POKRYWY SNIEŻNEJ h	USŁONECZNIENIE	POGODA
1	6	0.4	.	.	-	• 5³⁵ 9³⁵ 10¹⁵–17³⁵ 22⁰⁵–³⁵ = 8¹⁰–9³⁵
2	7	0.6	.	.	-	= 16⁴⁰–24
3	7	.	.	.	-	• 0⁴⁵–3⁴⁰ 4⁴⁰–5⁴⁰ = 0⁰⁰–11¹⁵
4	8	.	.	.	-	≫ 9¹⁵–11⁴⁵
5	7	0.9	.	.	-	•⁺⁰ 12⁰¹–19¹⁰
6	8	0.1	.	.	-	= 16¹⁰–⁵⁰
7	6	0.3	.	.	-	• 0³⁵–3⁴⁰ 6³⁵–8⁴⁰ 15²⁰–18³⁵ = 5⁴⁰–24
8	5	0.1	.	.	-	•¹⁻⁰ 4⁴⁰–6⁴⁰ •⁰–7¹⁵ • 9²⁰–12⁴⁰ 19⁴⁰–21¹⁵ •¹–22⁴⁰ = 0⁰⁰–24
9	6	0.0	.	.	-	• 15³⁵–16⁴⁰ = 0⁰⁰–24
10	6	1.8	.	.	-	• 14²⁰–24 = 0⁰⁰–21¹⁵
11	3	18.0	.	.	-	• 0⁰⁰–2³² 9³⁵–16⁴⁰ = ≡⁰ 23²–24
12	6	1.6	.	.	-	• 1⁰⁵–21¹⁰ = 0⁰⁰–17⁴⁵
13	7	.	.	.	-	
14	7	.	.	.	-	
15	7	0.0	.	.	-	• 23³⁵–24
16	6	0.0	.	.	-	• 0⁰⁰–2³⁵ •⁰ 17³⁵–17¹⁵ 17⁴⁵–20⁴⁵ 21³⁵–23⁴⁰ = 6¹⁰–10⁴⁰
17	8	0.4	.	.	-	• 2⁴⁰–4⁴⁵ ▽⁰ 7⁰⁵–⁴⁰ 8¹⁰–9⁰⁵
18	8	2.3	.	.	-	•▽⁰ 21⁴⁵–22¹⁰ 23⁴⁵–24 ≫ 11¹⁵–15⁴⁰
19	8	2.7	.	.	-	•▽⁰ 0⁰⁰⁻¹⁵ 4⁴⁰–8¹⁵ ▽⁰ 10⁴⁵–11¹⁵ •▽⁰ 11⁵⁰–12³⁰ ▽¹ 13¹⁵ 14²⁰⁻³⁵ ≫ 13⁴⁰–24
20	8	.	.	.	-	•▽⁰ 0³⁰–1³⁰ ≫ 0⁰⁰–3⁴⁵
21	8	.	.	.	-	
22	6	.	.	.	-	= ∞ 7¹⁵–24
23	5	.	.	.	-	∞ = 0⁰⁰–9¹⁵ ≡⁰–9⁵⁰ = –24 ⌴² 2⁰⁰–11⁰⁰
24	6	.	.	.	-	= 0⁰⁰–7⁵⁰ ≡⁰–8⁴⁵ = –24 ⌴² 0⁰⁰–10⁰⁰ ⌴D
25	3	0.9	.	.	-	•⁰ 9¹⁰–10¹⁰ = 0⁰⁰–9⁰³ ≡⁰–13⁵⁵ = –24 ⌴⁰⁻⁷ 0⁰⁰–9⁰⁰
26	6	.	.	.	-	= 0⁰⁰–24 ⊕ 11²⁰–12³⁰
27	4	1.9	.	.	-	• 11⁴⁵–13¹⁰ •⁰–17¹⁰ = ≡⁰ 0⁰⁰–24
28	6	.	.	.	-	= 0⁰⁰–13³⁰ 15¹⁰–24 ⌴⁰ 20⁰⁰–24
29	3	2.1	.	.	-	= 0⁰⁰–7⁵⁰ ≡⁰⁻¹ 16⁴⁵ = –24 ⌴¹ 0⁰⁰–10⁰⁰
30	7	2.2	.	.	-	•⁰⁻¹ 3³⁵–7¹⁵ •⁰ 16⁴⁵–24 ≫ 10²⁰–13³⁰ 20¹⁰–24 = 0⁰⁰–7¹⁵
31						
Σ	—	36.3	—		-	UWAGI.

Grudzień - Décembre

1	7	2.3	.	.	-	• 0⁰⁰–7¹⁵ •▽ 13¹⁰–15 ≫ 0⁰⁰–8³⁰ 11¹⁵–35
2	5	11.7	.	.	-	•⁰⁻¹ 4⁴⁰–11⁴⁵ 14⁰⁵–⁴⁰ •⁰⁻¹ 20¹⁵ 23⁴⁰ ≫ – ≫ 16¹⁵–24 = a
3	8	.	.	.	-	•▽⁰ 2⁴⁵–3¹⁰ ≫ 0⁰⁰–14⁴⁰
4	6	3.8	.	.	-	= 6⁴⁰–24 ⌴⁰ 2⁰⁰–9⁰⁰
5	7	2.8	.	.	-	• 0³⁰–3⁴⁰ •⁰–5⁴⁵ •⁰–7²⁰ •▽⁰ 8²⁵–³⁵ 13⁴⁰–14⁰⁵ •▽¹ 20⁰³–²⁵ •▽⁰ 20³²–21³⁵ ≫ 17²⁰–24 = 0⁰⁰–7²⁰
6	7	.	.	.	-	≫ – ≫ 0⁰⁰–4³⁰ ≫ 15⁴⁰ 17³⁵–20¹⁵–24
7	8	.	.	.	-	= 8¹⁰–9⁴⁰ ≫ 0⁰⁰–2³⁵
8	7	0.3	.	.	-	*▽⁰ 13³⁵–14¹⁰ 14¹⁵–²⁵ ⌴⁰⁻¹ 2⁰⁰–11⁰⁰
9	7	.	1	.	-	*▽⁰ 1⁴⁵–2¹⁵ = 14⁴⁰–24
10	5	0.1	1	.	-	*⁰⁻¹ 10³⁵–12⁰⁵ 13⁴⁰ •⁰ 19³¹ 21⁴⁵ = 0⁰⁰–24
11	5	4.4	.	.	-	•⁰ 10³⁵–11¹⁵ 11⁴⁵–24 = 0⁰⁰–8¹⁵ ≡⁰–8⁵⁰ = –24
12	7	.	.	.	-	•⁰ 0⁰⁰–2³⁵ = 0⁰⁰–2³⁵
13	8	2.8	.	.	-	*▽¹ 11¹⁵–8²⁰ *▽⁰⁻¹ 12³⁵ 16³⁵–21³⁵ 23⁵⁰
14	7	3.0	7	.	-	*▽⁰ 0⁴⁵–1¹⁰ *⁰–5²⁰ *▽¹⁻⁰ 6²⁰–7³⁰ 7⁴⁵–12³⁵ 18¹⁰ ⫫ ¹ 17¹⁰–²⁰ ≫ 16²⁰–23⁴⁰ ≡ –24
15	5	1.3	13	.	-	*▽⁰⁻² 0³⁰–5⁴⁰ *▽¹⁻⁰ 11³⁵–15³⁰ 20³⁵–24 ⫫ ¹ 0⁰⁰–13¹⁵ ≡ 0⁰⁰–13¹⁵ ≫ –14³⁰
16	6	.	13	.	-	* ⁰ 0⁰⁰–3⁴⁰ = 7³⁰–24
17	7	.	12	.	-	= 0⁰⁰–5⁴⁰ 17⁴⁰–24
18	6	.	11	.	-	= 0⁰⁰–24
19	7	.	pz.	.	-	= 0⁰⁰–10⁴⁰
20	7	1.8	pł.	.	-	•⁰ 11³³–12³⁰ ≫ 16¹⁵–12²⁰ 20¹⁰–21³⁰ = 10¹⁵–11³³
21	7	0.1	2	.	-	*▽¹ 0⁴⁰–1⁴⁵ 3³⁷–7⁰⁸ *▽⁰⁻¹ 9⁴⁵–12⁴⁰ *▽⁰ 14⁰⁵–⁴⁰ 17⁰⁵–⁴⁵ 18¹⁰–⁴⁵ ≫ – ≫ 5¹⁰–13⁵⁰
22	8	3.8	3	.	-	*▽⁰⁻² 10⁰⁵–24
23	7	6.6	15	.	-	*▽⁰⁻² 0⁰⁰–20¹⁰
24	8	.	24	.	-	
25	7	. .	21	.	-	
26	4	.	16	.	-	= 7³⁰–24
27	4	.	15	.	-	= ≡⁰ 0⁰⁰–24 V⁰ 8⁵⁰–9⁴⁰
28	5	.	15	.	-	= 0⁰⁰–8¹⁵ ≡⁰–8⁵⁰ = –24
29	5	.	15	.	-	= 0⁰⁰–24
30	5	.	12	.	-	= 0⁰⁰–24
31	6	0.0	12	.	-	= 0⁰⁰–24
Σ	—	44.8	—		-	UWAGI.

Sumatki — φ = 54°06' — λ = 22°57' — Styczeń – Janvier 1961

Dnia	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dnia	I	II	III	Dnia	Max	Min	I	II	III	Dnia	I	II	III	Dnia	I	II	III	I	II	III
1	95.7	94.0	95.5	94.5	-1.9	-1.0	-0.5	-1.0	-0.3	-2.2	96	97	96	96	0.2	0.2	0.3	0.2	10	10	10	C 0	S 3	SW 2
2	96.5	95.5	92.4	94.8	-1.7	-0.3	-0.9	-1.0	0.0	-1.9	98	96	99	98	0.1	0.3	0.0	0.1	10	10 *	10 *	SW 2	SW 2	SE 5
3	87.9	85.3	82.7	85.3	-0.9	-1.1	-0.1	-0.6	0.1	-1.4	99	97	98	98	0.0	0.2	0.2	0.1	10 =	10	10	SE 3	SE 5	SSE 5
4	82.5	83.4	85.3	83.1	-0.1	2.9	2.1	1.8	4.0	-0.5	98	95	89	94	0.2	0.4	0.8	0.5	10	8 ⊙	10	SE 2	SE 2	SE 4
5	85.0	84.9	86.4	85.4	0.5	0.1	0.3	0.3	2.1	-0.3	94	98	98	97	0.3	0.2	0.1	0.2	10 •	10 *	10 *	ESE 4	ESE 3	W 5
6	90.4	92.8	94.5	92.6	0.8	0.9	-3.1	-1.1	1.3	-3.2	96	92	90	93	0.3	0.5	0.5	0.4	10	10	7	S 7	SSW 6	SSW 1
7	93.0	92.7	91.3	92.3	-4.9	-0.6	0.3	-1.2	0.5	-5.0	93	93	94	93	0.3	0.4	0.3	0.3	8	10	10	S 4	SE 6	SSE 4
8	89.9	89.8	90.1	89.9	-0.5	-0.2	0.1	-0.1	0.4	-0.7	98	100	100	99	0.1	0.0	0.0	0.0	10 *	10	10	S 3	SW 3	SSW 6
9	86.7	86.8	90.4	88.0	-0.1	0.9	0.9	0.6	1.1	-1.0	98	100	98	99	0.2	0.0	0.1	0.1	10 *	10 =	10	S 5	S 6	S 5
10	91.3	92.6	94.0	92.6	-0.3	-0.3	0.1	-0.1	1.1	-0.7	98	92	98	96	0.2	0.5	0.2	0.3	8	10	10	S 5	SSW 3	SSW 3
11	95.0	95.6	96.1	95.6	-1.1	-1.0	-1.7	-1.4	0.2	-2.2	93	95	96	95	0.4	0.3	0.2	0.3	10	10	10	SSE 6	S 5	S 6
12	94.6	95.8	102.0	97.5	-0.7	0.2	-0.1	-0.2	1.0	-1.8	93	96	92	94	0.4	0.3	0.5	0.4	10 *	10 *	10 *	S 3	NW 7	NNW 7
13	107.3	106.2	102.7	105.4	-3.1	-2.1	-2.7	-2.6	0.1	-4.7	93	92	91	92	0.4	0.4	0.5	0.4	10	9	10 *	NW 3	SW 4	SW 7
14	101.6	103.4	106.6	103.9	-0.4	0.7	1.1	0.6	1.4	-2.7	100	100	90	97	0.0	0.0	0.6	0.2	10 •, =	10 •, =	10	SW 5	WSW 2	WSW 5
15	107.7	106.6	102.8	105.7	0.5	-1.0	0.9	0.3	1.3	-1.1	90	92	94	92	0.6	0.5	0.4	0.5	9	10	10	W 6	WSW 6	W 6
16	99.9	101.2	105.5	102.2	1.6	0.2	-4.3	-1.7	1.7	-4.4	89	84	79	84	0.8	1.0	0.9	0.9	10	9	10	NW 8	N 9	NE 9
17	109.4	111.3	116.2	112.3	-9.7	-8.1	-10.3	-9.6	-4.3	-10.3	88	66	81	78	0.4	1.1	0.5	0.7	0	6	0	NNW 6	NNE 10	N 6
18	119.9	120.7	118.9	119.8	-13.1	-8.1	-6.7	-8.6	-6.6	-13.7	84	66	75	75	0.4	1.1	0.9	0.8	0	7 ⊙	10	N 5	N 3	WNW 3
19	115.4	113.2	112.1	113.6	-4.3	-2.7	-3.9	-3.7	-2.3	-6.7	86	73	80	80	0.6	1.3	0.9	0.9	10 *	10	9	NW 5	WNW 3	NW 2
20	110.0	109.1	107.0	108.7	-6.7	-4.9	-5.9	-5.8	-3.8	-8.7	86	88	81	85	0.5	0.5	0.7	0.6	9	10	10	C 0	C 0	C 0
21	104.7	103.3	100.8	102.9	-8.7	-6.9	-8.9	-8.4	-5.9	-10.5	92	91	89	91	0.3	0.3	0.4	0.3	10	6 ⊙	10	C 0	SSW 1	SSW 3
22	96.2	95.2	95.8	95.7	-5.9	-5.1	-13.5	-9.5	-4.8	-13.5	84	88	92	88	0.6	0.5	0.2	0.4	10	10 *	0	WSW 4	WSW 2	ENE 2
23	94.6	94.4	92.4	93.8	-12.2	-10.7	-7.5	-9.5	-7.4	-17.2	89	80	87	85	0.3	0.5	0.4	0.4	10 *	9	10 *	NNE 2	N 2	WNW 4
24	91.7	93.0	94.3	93.0	-5.1	-8.3	-12.1	-9.4	-4.8	-13.4	93	78	85	85	0.3	0.7	0.4	0.5	10 *	2 ⊙	0	WNW 2	NNE 4	C 0
25	94.3	95.4	97.2	95.6	-14.7	-11.7	-19.4	-16.3	-11.3	-19.4	87	93	95	92	0.3	0.2	0.1	0.2	8	1 ⊙	0	N 2	NNE 2	C 0
26	100.3	102.0	104.7	102.3	-15.9	-8.2	-6.2	-8.6	-6.1	-20.4	87	69	81	79	0.3	1.0	0.7	0.7	9	8 *	9	W 3	SW 6	WSW 5
27	108.5	109.9	109.1	109.2	-4.9	-3.1	-9.3	-6.6	-2.8	-9.4	88	81	85	85	0.5	0.9	0.4	0.6	10	10	0	WSW 5	WSW 6	SW 2
28	104.5	100.5	98.5	101.2	-13.3	-7.3	-7.7	-9.0	-5.3	-14.4	72	63	84	73	0.6	1.3	0.5	0.8	1	9 ⊙	7	C 0	SW 7	SW 5
29	94.5	93.0	93.4	93.6	-10.7	-5.7	0.9	-5.2	0.9	-11.4	80	85	88	84	0.5	0.8	0.7	0.7	6	10	10	SSW 4	SW 6	SW 6
30	85.0	80.3	76.3	80.5	-0.4	0.2	1.0	0.4	1.2	-1.6	82	92	96	90	1.1	0.5	0.3	0.6	10	10 *	10 ‡	SSW 13	SSW 10	SW 9
31	79.6	78.4	77.0	78.3	1.9	1.5	0.9	1.3	2.6	0.4	91	98	100	96	0.6	0.1	0.0	0.2	10	10	10 =	SW 6	SW 6	C 0
M	97.1	97.0	97.1	97.1	-4.3	-2.9	-5.7	-5.6	-1.4	-6.6	91	88	90	90	0.4	0.5	0.4	0.4	8.6	8.8	8.1	3.9	4.5	4.0

Luty – Février

1	78.8	80.1	79.4	79.4	1.1	1.4	0.5	0.9	2.0	0.0	94	89	98	94	0.4	0.8	0.1	0.4	10	10	10	WSW 5	WSW 4	SW 5
2	73.6	73.9	74.1	73.9	0.3	1.0	0.7	0.7	1.4	0.1	98	94	96	96	0.1	0.4	0.2	0.2	10	10	10	S 6	SSW 5	SSW 2
3	74.8	75.0	75.3	75.0	-2.2	-1.6	-3.5	-2.7	0.7	-3.6	100	98	99	99	0.0	0.1	0.0	0.0	10 =	10 =	10 =	C 0	C 0	C 0
4	78.9	80.8	81.4	80.5	-0.4	-1.1	-2.7	-1.7	-0.2	-3.5	98	89	91	93	0.1	0.6	0.5	0.4	10	8	9	SSW 4	WSW 5	SW 2
5	85.9	89.4	95.8	89.7	-8.5	-4.1	-2.5	-4.4	-1.3	-11.7	98	89	91	93	0.1	0.5	0.5	0.4	10 =	4 ⊙	8	C 0	SW 2	SW 4
6	98.2	98.6	95.0	97.3	-2.5	-0.1	-4.4	-2.8	0.3	-5.5	87	78	79	81	0.7	1.3	0.9	1.0	9	6	0	WSW 2	SSW 4	SSW 8
7	87.7	86.8	87.2	87.2	-2.9	-2.7	-1.1	-2.0	-0.9	-5.5	77	91	99	89	1.1	0.5	0.1	0.6	10	10 *	10 •, =	SSE 8	S 6	SSE 4
8	87.3	89.0	93.1	89.8	-0.9	-0.1	0.3	-0.1	1.0	-1.4	95	96	94	95	0.3	0.3	0.3	0.3	10	10 *	10	SSE 3	SSE 2	SSE 1
9	95.2	93.8	91.7	93.6	-0.1	0.1	-1.1	-0.6	2.3	-1.7	90	94	93	92	0.7	0.4	0.4	0.5	10	10	10	SW 3	SW 8	SW 7
10	94.9	99.3	102.6	98.9	-1.3	-1.3	-2.2	-1.8	-0.9	-2.2	93	90	96	93	0.4	0.5	0.2	0.4	10	10	10	E 5	NE 3	NW 2
11	97.8	92.3	86.5	92.3	-1.3	0.1	0.1	-0.2	0.7	-3.1	90	90	94	91	0.5	0.7	0.4	0.5	10	10 *	10 *	SSW 7	SSW 8	SSW 7
12	84.9	87.9	95.2	88.7	1.3	1.7	1.2	1.4	2.3	0.1	100	100	98	99	0.0	0.0	0.2	0.1	10 =	10 =	10	SSW 5	WSW 3	W 3
13	97.0	99.6	103.2	99.9	0.5	1.3	-1.9	-0.5	1.9	-2.2	96	91	92	93	0.2	0.6	0.4	0.4	10	10	0	WNW 3	NW 2	NW 2
14	106.2	106.8	104.8	105.9	-3.7	1.0	-0.1	-0.7	1.4	-4.9	94	81	94	90	0.3	1.3	0.4	0.7	8	9	10	NW 1	SW 5	SW 7
15	101.8	102.8	104.8	103.1	1.7	4.3	2.2	2.8	5.4	-0.2	94	84	100	93	0.4	1.3	0.0	0.6	10	7	10 =	WSW 10	WSW 5	C 0
16	106.9	108.0	109.1	108.0	1.0	1.8	1.7	1.6	2.2	0.8	100	100	98	99	0.0	0.0	0.1	0.0	10 =	10 =	10 •	C 0	SSE 2	WNW 4
17	109.5	109.5	109.2	109.4	2.1	2.9	2.5	2.5	3.2	1.1	96	100	98	98	0.3	0.0	0.1	0.1	10	10 =	10	WNW 2	W 5	W 5
18	106.6	106.6	105.5	106.2	2.1	4.4	4.2	3.7	7.2	1.8	95	85	84	88	0.4	1.3	1.3	1.0	10	5	0	W 6	WSW 5	WSW 4
19	102.0	102.6	104.5	103.0	0.9	1.9	2.3	1.8	4.2	0.7	98	100	96	98	0.1	0.0	0.3	0.1	10	10 •, =	10 •	WSW 4	WSW 7	W 3
20	108.5	111.6	113.0	111.0	0.9	1.0	0.4	0.7	2.5	0.3	94	96	100	97	0.4	0.3	0.0	0.2	10	10	10 =	WSW 3	NW 2	W 4
21	112.0	111.3	111.8	111.7	-1.0	0.5	0.7	0.2	1.2	-1.2	99	100	100	100	0.1	0.0	0.0	0.0	10 =	10 •, =	10 •, =	WSW 4	WSW 7	WSW 5
22	113.7	116.2	116.0	115.3	0.5	3.3	-0.7	0.6	4.4	-0.8	98	81	98	92	0.1	1.4	0.1	0.5	10 •	5 ⊙	0	NNW 4	E 3	C 0
23	114.9	113.6	111.7	113.4	-2.3	-1.0	-1.9	-1.8	-0.5	-3.3	100	91	92	94	0.0	0.5	0.4	0.3	10 =	10	10	C 0	NE 2	C 0
24	111.3	111.6	112.7	111.9	-3.1	-2.5	-2.6	-2.7	-1.8	-3.1	93	95	89	92	0.4	0.3	0.6	0.4	10	10	10	C 0	C 0	ESE 4
25	114.6	115.9	116.7	115.7	-2.7	-0.9	-0.3	-1.0	-0.1	-3.1	91	89	82	87	0.5	0.6	1.1	0.7	10	10	10	ESE 5	SE 7	SE 7
26	116.3	115.3	114.1	115.2	-5.7	2.3	-1.1	-0.9	3.4	-5.9	85	59	87	77	0.7	2.9	0.7	1.4	0 ⊙	1 ⊙	0	SE 6	S 8	S 2
27	110.5	107.1	101.5	106.4	-2.1	3.5	2.5	1.6	4.4	-2.3	91	71	95	86	0.4	2.2	0.4	1.0	8	8	10 •	SSW 6	SSW 8	SW 6
28	92.7	88.1	82.5	87.8	3.1	3.9	5.1	4.3	5.9	2.4	97	98	97	97	0.2	0.2	0.3	0.2	10 •	10 •	10 •	SSW 6	SSW 5	S 8
29																								
30																								
31																								
M	98.7	99.0	99.1	98.9	-0.8	0.8	-0.1	0.0	1.9	-2.0	94	90	94	93	0.3	0.7	0.3	0.4	9.3	8.7	8.1	3.9	4.4	3.8

Suwałki — $H_s = 165\,m$ — $H_b = 169{,}6\,m$ — $h_w = 13\,m$ — Styczeń – Janvier 1961

DNI	WILGOTNOŚĆ v	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	UTRUDNIENIE	POGODA
1	5	2.1	.	–	◉° 7³⁰–10¹⁵ *° 12⁴⁵–16³⁰; V° 0⁰⁰–24; ∼° 0⁰⁰–24; = 0⁰⁰–24
2	5	1.2	1	–	*° 12¹⁵–24; = 0⁰⁰–6⁴⁵ ≡° –8⁴⁰ = –24; V° ∼ 0⁰⁰–16⁰⁰
3	5	.	2	–	*° 0⁰⁰–1⁵⁰; = 0⁰⁰–4⁵⁰ ≡° –9⁴⁰ = –24
4	6	0.7	2	–	•° 21⁴⁰–22¹⁵; = 0⁰⁰–13³⁰
5	5	11.8	pż.	–	•° 5⁰⁵–9²⁰ *⁰·¹ 9⁴⁰–21¹⁰; = 2³⁰–24
6	4	.	7	–	= 0⁰⁰–24
7	6	0.0	6	–	*° 11⁴⁰–12¹⁵; = 0⁰⁰–24
8	5	0.4	6	–	*° 6¹⁰–7¹⁵ 8⁰⁵–³⁵; = 0⁰⁰–12⁴⁰ ≡° –19³⁰ = –24
9	3	0.4	7	–	*° 2³⁰–10¹⁵ 13²⁵–15⁴⁰; = ≡⁰·¹ 0⁰⁰–24
10	6	0.0	6	–	*° 13⁴⁰ 14¹⁰–15³⁵; = 0⁰⁰–24
11	6	3.4	4	–	*° 22⁴⁰–24; = 0⁰⁰–24
12	8	0.8	8	–	*° 0⁰⁰–8⁴⁵; 12²⁰ 13¹⁰–16³⁰ 20¹⁵–24; = 0⁰⁰–24
13	7	1.0	9	–	*° 0⁰⁰–1³⁵ 18⁴⁰–21³⁰; = 0⁰⁰–8⁴⁵ ≡° –10³⁰ = –11³⁰
14	3	0.0	10	–	◉° 1⁴⁰–13¹⁰ •¹ –14⁴⁰ = 1⁰⁰–6²⁵ ≡° –15⁴⁵ = –24
15	7	0.1	7	–	*° 10⁴⁵–55 •° 13¹⁵; 14²⁰–20¹⁰; = 0⁰⁰–7¹⁰; 13¹⁵–24
16	7	.	6	–	= 0⁰⁰–7³⁰
17	7	0.0	6	–	▽° 12⁵⁵–13⁰⁵; = 11¹⁰–⁵⁰; ≫ 10²⁰–15⁰⁵
18	8	0.5	6	–	*° 23³⁰–24
19	6	0.0	8	–	*° 0⁰⁰–10⁵⁰; = 10⁵⁰–18²⁰
20	6	.	8	–	= 7¹⁰–24
21	5	0.0	8	–	*° 21⁴⁵–23²⁰; = ≡⁰·¹ 1⁰⁰–24
22	6	1.1	8	–	*° 0⁴⁵–2²⁰; 10²⁰–³⁰ 11³⁰–17³⁰ ↔° 18³⁵–20¹⁵; = 0⁰⁰–24
23	6	0.3	10	–	*° 5¹⁵–8³⁵ ↔° –10⁵⁰ *° 15²⁰–17³⁵ 18²⁵–24; = 0⁰⁰–24
24	8	0.1	12	–	*° 0⁰⁰–2⁴⁰ 4¹⁵–10³⁰; = 0⁰⁰–10³⁰
25	7	.	13	–	= 2⁴⁵–7⁴⁰; 18³⁰–24; V 2⁰⁰–12³⁰
26	7	0.1	13	–	*° 10¹⁵..45; 11¹⁰ 13¹⁰–16²⁰; 17²⁵ 20³⁰; 22¹⁵ 24; = 0⁰⁰–8³⁰
27	6	.	13	–	*° 0⁰⁰ 1⁴⁵; = 10⁵⁰–17³⁰
28	7	.	13	–	= 0⁰⁰–8²⁰; 13³⁰–24
29	6	.	13	–	= 0⁰⁰–24
30	6	13.1	13	–	•° 7²⁵–8⁴⁵ ◉° –10³⁰ •° –11⁴⁰ *° –16³⁰ •° –20¹⁵ *° –21²⁰ *¹ –23¹⁵; = 0⁰⁰–24; ≫ 0⁰⁰–17¹⁵
31	5	0.3	7	–	•° 3³⁵–4³⁰; = 0⁰⁰–2³⁰; 11¹⁰–13²⁷ ≡¹ –24
Σ	–	37.4	–	–	UWAGI. Kierunki i prędkości wiatru w ciągu całego roku — wg anemometru.

Luty – Février

1	6	3.3	4	–	•° 1²⁵–3³⁰; ≡⁰·¹ = 0⁰⁰–24
2	6	.	5	–	*° 0⁰⁰–2³⁰ *° –3¹⁵ •° –5¹⁰ •° –6²⁸; = 0⁰⁰–24
3	2	0.4	3	–	= 0⁰⁰–2⁴⁰ ≡¹·² 24
4	7	0.6	3	–	*⁰·¹ 4¹⁰ 10⁴⁵ ▽° 11⁵⁰–12⁰⁵ △° 13³⁵–⁴² *° 14²⁰–⁴⁵; ≡² 0⁰⁰–1⁴⁵ = 11¹⁰
5	7	.	2	–	= 2²⁰–6³⁰ ≡² –9⁴⁷ = –12²⁰
6	7	0.0	2	–	*° 10²⁰..⁵⁰
7	5	1.3	2	–	*° 7³⁰–9²⁰ △° 11⁴⁰ *⁰·¹ 15³⁵ •° 18¹⁵–22¹⁰; = 12⁰⁰–20¹⁰ ≡° –23⁴⁵ = –24
8	5	0.0	4	–	*° 8⁴⁰–10³⁰ △° –11¹⁰ ▽ 12¹⁰–²⁵; 12³⁵–13⁴⁰ •° 16⁵⁰–17³⁵; = 0⁰⁰–15⁴⁰ ≡ –18³⁵
9	7	.	3	–	= 13¹⁰–24
10	6	.	2	–	= 0⁰⁰–24
11	6	1.1	2	–	*° 8²⁰ 10¹⁵; 11¹⁰–13¹⁵ 17³⁰–20³⁵ *° –24; = 0⁰⁰–24
12	3	0.9	3	–	•° 0⁰⁰–2³⁰ •° –6²⁰ 19⁵⁰–20³⁰ 21³⁰–23⁴⁰; = ≡⁰·¹ 0⁰⁰–24
13	7	.	2	–	•° 2¹⁵ 3³⁰ *° –4³⁵; = 0⁰⁰–9¹⁰; 16⁴⁵–23³² ≡° –24
14	7	.	pż.	–	= 9¹⁰–12¹⁵
15	6	0.7	pż.	–	•° 23³⁰–24; = 1⁰⁰–20⁴⁰ ≡¹·² 24
16	2	0.9	pż.	–	•° 0⁰⁰–45 •° 11¹²–16⁴⁵ 19⁴⁵–24; ≡²·¹ 0⁰⁰–4³⁵ = –6²⁰ ≡¹·² 19⁴⁰ = –24
17	3	0.0	pż.	–	•° 0⁰⁰–6³⁰ 8¹⁰–11²⁰ 13²⁸–15³⁵; = 0⁰⁰–12²⁵ ≡° –17⁴³ = –24
18	6	.	.	–	•° 0⁴⁰–2¹⁵; = 0⁰⁰–24
19	3	0.6	.	–	•° 0²⁰–24; = 0⁰⁰–7⁴⁰ ≡¹ –14⁴⁵ = –24
20	6	0.0	.	–	•° 0⁰⁰–5³⁰ 17²⁵–18³⁵; = 0⁰⁰–6¹⁰ 9⁰⁰–15⁴⁰ ≡° –24
21	3	0.1	.	–	◉° 8⁴⁵–10⁴⁵ •° –15⁴⁰ 17⁵⁰–24; ≡° 0⁰⁰–15⁴⁵ = –16⁴⁰ ≡° –24
22	7	(0.0)	.	–	•° 0⁰⁰–2³⁰ •¹ –3⁴⁵ •° –7³²; ≡° 0⁰⁰–6¹⁰ = –22⁴⁰ ≡¹ –24; ⌴° 19⁰⁰–24
23	6	.	.	–	≡¹ 0⁰⁰–6⁵⁰ = –14²⁰; ⌴° 0⁰⁰–13⁰⁰
24	6	.	.	–	= 8²⁰–18²⁵
25	8	.	.	–	= 7⁴⁰–9¹⁰
26	8	.	.	–	= 7⁴⁰–50
27	5	5.1	.	–	•° 17⁴⁰–23³⁰; = 6¹⁰–24; ≫ 15³⁰–16³⁰; ⌴° 1⁰⁰–11⁰⁰
28	5	11.1	.	–	•⁰·¹ 2¹⁵–8³⁵ •° –10⁴⁰ •° –18³⁵; 20³⁵–21²⁰; = 0⁰⁰–19²⁵; 20¹⁰–21³⁰
29					
30					
31					
Σ	–	26.1	–	–	UWAGI.

Suwałki φ=54°06' λ=22°57' Marzec – Mars 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	84.9	90.3	96.1	90.4	1.9	2.5	1.9	2.0	6.0	1.2	91	93	91	92	0.6	0.4	0.6	0.5	10	10 •	7	W 10	WSW 6	W 6
2	99.8	100.9	101.3	100.7	0.7	2.6	1.7	1.7	3.3	0.4	94	77	90	87	0.4	1.7	0.6	0.9	10	10	10	WSW 4	W 5	W 2
3	104.4	107.1	109.3	106.9	0.3	3.8	2.3	2.2	5.2	0.2	90	77	77	81	0.6	1.9	1.7	1.4	10	9	7	NW 3	W 2	C 0
4	109.9	110.5	108.4	109.6	1.9	5.3	2.1	2.8	6.2	0.4	100	89	95	95	0.0	1.0	0.4	0.5	10 , ≡	9	3	W 1	W 6	SW 5
5	103.3	105.0	108.6	105.6	4.3	7.1	2.1	3.9	7.8	1.7	95	62	77	78	0.4	3.9	1.7	2.0	10	8 ⊙	6	WNW 6	WNW 9	NW 7
6	107.3	107.2	104.7	106.4	1.2	5.0	4.1	3.6	5.0	0.2	94	86	90	90	0.4	1.2	0.8	0.8	10	10	10	W 5	WSW 7	W 9
7	99.8	98.0	103.3	100.4	3.7	9.1	3.3	4.8	9.8	3.2	88	72	78	79	1.0	3.2	1.7	2.0	10	7	0	WSW 9	WNW12	WNW 4
8	107.7	106.7	104.8	106.4	0.9	6.9	1.8	2.8	9.3	-0.2	79	75	96	83	1.4	2.4	0.3	1.4	9	3 ⊙	0	WNW 2	WSW 3	WNW 3
9	101.7	102.6	100.9	101.7	4.3	6.0	5.1	5.1	6.6	1.4	95	91	94	93	0.4	0.9	0.6	0.6	10	10	10	WNW 5	WSW 7	W 5
10	100.4	99.6	97.9	99.3	5.5	13.5	4.7	7.1	14.1	4.2	92	63	85	80	0.7	5.7	1.2	2.5	8	8	0	W 5	W 7	W 3
11	94.1	92.0	95.8	94.0	3.3	11.8	5.0	6.3	12.2	3.0	88	59	94	80	0.9	5.6	0.5	2.3	8	9	10	W 2	W 6	W 5
12	93.0	86.4	76.7	85.4	2.5	5.1	8.3	6.0	8.6	2.1	93	95	84	91	0.5	0.4	1.7	0.9	9	10 •	10 •	W 4	SW 9	WSW 8
13	68.6	76.7	82.4	75.9	3.1	2.8	1.9	2.4	8.5	1.0	91	74	69	78	0.6	2.0	2.2	1.6	10 •	9 *	8	NW 14	NW 12	NW 13
14	87.9	88.7	86.7	87.8	-0.5	5.1	2.7	2.5	6.5	-0.6	65	38	84	62	2.1	5.5	1.2	2.9	3 ⊙	2 ⊙	10 •	WNW 7	WNW 9	SW 2
15	81.7	85.6	94.4	87.2	5.7	7.8	1.5	4.1	8.6	0.3	92	75	60	76	0.8	2.7	2.7	2.1	10	6	0	WNW10	WNW11	NW 8
16	89.6	85.3	92.7	89.2	0.9	5.3	3.5	3.3	5.8	-1.1	81	94	95	90	1.2	0.6	0.4	0.7	10 ⁎̣	10 •	4	SW 3	SW 9	WNW 6
17	96.9	94.0	90.0	93.6	0.1	7.5	7.3	5.6	10.4	-0.2	100	76	76	84	0.0	2.5	2.5	1.7	10 ≡ ,	9	0	WSW 4	W 7	WSW 3
18	79.7	77.1	77.3	78.0	5.1	9.7	3.1	5.2	11.6	3.0	89	72	76	79	1.0	3.4	1.8	2.1	9 ⊙	10 •	1	SSW 7	WSW 8	W 2
19	74.3	76.6	82.9	77.9	2.1	1.9	-1.5	0.2	4.3	-1.7	80	80	76	79	1.4	1.4	1.4	1.4	9	6 * ⊙	0	SW 9	W 10	WNW 3
20	87.1	85.6	81.6	84.8	-3.9	1.0	-0.9	-1.2	2.8	-4.7	89	62	65	72	0.5	2.5	2.0	1.7	8 *	6 ⊙	0	WSW 4	SW 5	SSW 6
21	73.1	70.4	73.0	72.2	-0.7	1.1	0.6	0.4	1.9	-2.0	69	89	92	83	1.8	0.7	0.5	1.0	10 *	10	10 *	SSE10	SSW 9	SSW 2
22	80.0	85.9	89.5	85.1	-1.0	-0.5	-2.9	-1.8	1.3	-3.0	85	70	77	77	0.9	1.8	1.1	1.3	10 *	10 *	0	NW 7	NW 8	WSW 2
23	86.5	85.7	85.0	85.7	-1.7	1.9	3.9	2.0	4.1	-4.7	79	91	88	86	1.1	0.6	1.0	0.9	10	10	10	SW 6	SW 4	SW 6
24	83.4	83.1	84.8	83.8	4.3	5.5	4.7	4.8	7.7	3.6	88	86	73	82	1.0	1.2	2.3	1.5	10 •	10 •	10 •	WSW 5	W 9	WNW 7
25	87.9	89.8	94.7	90.8	3.7	7.9	1.5	3.6	8.2	1.1	82	60	76	73	1.5	4.2	1.6	2.4	10	6 ⊙	10	W 6	W 13	W 1
26	91.5	87.6	79.2	86.1	3.7	8.3	7.3	6.6	8.6	0.4	92	66	79	79	0.7	3.8	2.2	2.2	8 ⊙	10	10 •	SW 7	SW 10	SW 10
27	72.6	74.8	75.5	74.3	3.4	3.5	0.1	1.8	7.4	-0.1	66	86	84	79	2.6	1.0	1.0	1.5	9	10 ▪	10 *	SW 12	W 15	SW 2
28	77.3	78.2	83.2	79.6	-1.9	1.7	0.5	0.2	4.2	-2.2	87	83	77	82	0.7	1.1	1.5	1.1	10 *	10 *	4	SW 4	WSW10	W 4
29	84.4	84.7	81.6	83.6	-0.1	3.9	2.1	2.0	4.4	-1.4	82	53	96	77	1.1	3.8	0.3	1.7	9	9	10	WSW 8	SW 7	SW 5
30	74.2	74.5	79.4	76.0	5.2	8.1	1.3	4.0	8.5	1.2	92	55	76	74	0.7	4.8	1.6	2.4	10 •	8 ⊙	9	SW 9	W 14	WSW 4
31	79.6	83.1	84.4	82.4	-1.1	3.3	-0.8	0.2	4.4	-1.5	89	60	91	80	0.6	3.1	0.5	1.4	10	9	10	NW 2	N 4	W 2
M	89.1	89.5	90.5	89.7	1.8	5.3	2.5	3.0	6.9	0.7	87	74	83	81	0.9	2.4	1.3	1.5	9.3	8.5	6.1	6.1	8.2	4.7

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DNI	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	77.2	82.2	80.9	80.1	0.0	0.7	-0.5	-0.1	2.2	-1.1	86	85	92	88	0.9	1.0	0.5	0.8	10 *	9	10 *	S 3	WNW10	C 0
2	85.7	88.9	89.5	88.0	-2.1	3.5	-0.5	0.1	5.6	-3.5	87	52	86	75	0.6	3.7	0.9	1.7	0 ⊙	6 ⊙	4	WNW 3	WNW 5	WNW 1
3	85.5	82.7	84.0	84.1	-0.5	1.9	1.9	1.3	2.1	-1.6	80	94	98	91	1.2	0.4	0.1	0.6	10 △	10 ⁎̣	10	SW 3	E 5	SE 2
4	85.6	84.0	90.5	86.7	1.0	1.0	1.6	1.3	3.4	0.6	92	94	74	87	0.5	0.4	1.8	0.9	10	10 *	0	W 3	S 3	W 8
5	95.4	94.7	89.4	93.2	-0.3	6.1	5.3	4.1	6.7	-1.1	88	60	95	81	0.8	3.8	0.4	1.7	9	10	10 •	WSW 2	SSW 5	S 5
6	87.5	89.4	92.5	89.8	8.9	16.9	8.7	10.8	18.9	5.3	93	65	80	79	0.8	6.6	2.2	3.2	9 ⊙	7	0	SE 6	WSW 9	C 0
7	90.3	87.9	87.9	88.7	10.7	22.0	15.1	15.7	23.0	6.0	91	49	72	71	1.2	13.4	4.8	6.5	7 ⊙	6 ⊙	10	WNW 2	SSW10	SSW 4
8	88.7	88.5	88.5	88.6	8.1	10.7	3.9	6.6	15.1	3.9	93	74	92	86	0.8	3.4	0.7	1.6	5 ⊙	10	10	NW 5	W 3	W 8
9	86.5	90.5	97.3	91.4	2.7	4.9	0.5	2.2	5.3	0.0	77	56	75	69	1.7	3.8	1.6	2.4	10 *	8	0	NW 14	WNW15	WNW 7
10	98.8	97.8	95.5	97.4	-0.2	5.9	0.3	1.6	7.0	-2.5	82	38	78	66	1.1	5.7	1.3	2.7	5 ⊙	9 ⊙	4	W 3	WSW 6	NW 3
11	93.7	91.8	92.9	92.8	0.1	7.1	2.1	2.8	8.3	-3.2	80	43	69	64	1.3	5.8	2.2	3.1	7 ⊙	9	0	C 0	W 2	NW 3
12	96.5	98.3	97.2	97.3	-1.5	6.9	2.3	2.5	8.3	-2.4	96	40	86	74	0.2	6.0	1.0	2.4	8	4 ⊙	0	NW 2	WNW 6	C 0
13	91.7	91.0	92.0	91.6	4.1	8.1	8.2	7.2	10.5	1.3	71	78	97	82	2.4	2.4	0.3	1.7	10 •	10 •	10 •	SSW 4	SSW 3	C 0
14	93.0	92.8	91.8	92.5	6.5	18.5	11.7	12.1	20.6	3.6	100	50	82	77	0.0	10.7	2.5	4.4	5 ≡	8 ⊙	6	C 0	WSW 2	C 0
15	90.2	89.7	92.0	90.6	8.5	22.1	11.1	13.2	22.9	6.2	94	36	84	71	0.6	17.1	2.1	6.6	0 ⊙	1 ⊙	0	S 2	SSW 7	NW 3
16	92.6	92.6	91.6	92.3	7.2	13.5	9.4	9.9	15.0	6.2	96	68	83	82	0.5	5.0	2.0	2.5	10	6 ⊙	0	NNE 4	NNE 4	ENE 5
17	92.0	92.3	93.2	92.5	7.5	15.5	8.9	10.2	16.7	4.1	84	45	75	68	1.7	9.7	2.9	4.8	3 ⊙	3 ⊙	0	ENE 5	ESE 6	E 1
18	92.8	92.3	90.8	92.0	5.3	10.7	10.4	9.2	13.1	2.5	100	94	90	95	0.0	0.9	1.3	0.7	10 ≡	10 •	8	E 2	SSE 4	SE 3
19	91.4	93.3	96.9	93.9	7.7	13.7	6.1	8.4	15.1	5.7	90	36	54	60	1.0	10.1	4.3	5.1	4 ⊙	4 ⊙	0	W 4	WNW 7	WNW 7
20	101.7	102.6	104.1	102.8	1.6	7.9	1.9	3.3	8.6	-0.7	60	50	73	61	2.8	5.3	1.9	3.3	0 ⊙	0 ⊙	8	N 8	NNE 9	N 2
21	105.9	104.6	102.1	104.2	1.5	10.9	4.7	5.4	12.4	-2.4	72	30	51	51	1.9	9.1	4.1	5.0	0 ⊙	0 ⊙	1	E 3	E 4	SSE 3
22	99.9	95.9	94.0	96.6	4.9	14.9	6.7	8.3	16.3	-1.3	67	30	65	54	2.9	11.8	3.4	6.0	1 ⊙	4 ⊙	1	SSE 4	S 10	S 4
23	93.5	93.3	93.8	93.5	6.1	16.7	8.5	10.0	17.3	0.1	66	30	56	51	3.2	13.3	4.9	7.1	3 ⊙	1 ⊙	0	S 7	SE 10	SE 5
24	96.7	96.6	97.2	96.8	7.7	15.9	10.1	11.0	17.2	2.1	60	38	52	50	4.2	11.2	6.0	7.1	1 ⊙	1 ⊙	0	SE 4	SE 10	E 5
25	100.0	99.2	98.4	99.2	7.3	16.7	9.1	10.6	16.9	2.8	73	52	52	52	2.7	13.0	5.6	7.1	0 ⊙	0 ⊙	0	E 5	ESE10	ESE 4
26	97.7	95.3	93.2	95.4	7.7	17.2	11.1	11.8	18.1	3.6	57	28	47	44	4.5	14.2	7.0	8.6	0 ⊙	1 ⊙	6	E 6	ESE10	ESE 3
27	92.3	90.5	90.1	91.0	11.4	17.9	9.1	11.9	18.9	7.4	55	28	67	50	6.1	14.8	3.8	8.2	8 ⊙	8 ⊙	6	ENE 2	E 4	E 1
28	89.2	89.1	91.1	89.8	11.9	17.1	8.3	11.4	18.1	5.4	53	33	63	50	6.6	13.0	4.0	7.9	2 ⊙	7 ⊙	1	N 2	NNE 5	NE 8
29	97.1	98.0	97.9	97.7	2.7	8.8	2.4	4.1	10.5	0.1	70	27	54	50	2.2	8.2	3.3	4.6	3 ⊙	0 ⊙	0	SE 8	E 9	E 4
30	96.3	93.2	91.4	93.6	4.2	14.9	11.9	10.7	17.5	-1.7	55	40	64	53	3.7	10.1	5.0	6.3	0 ⊙	7 ⊙	9	E 5	SE 6	NE 4
31																								
M	92.8	92.6	92.9	92.8	4.7	11.6	6.3	7.2	13.1	1.5	79	51	73	68	1.9	7.8	2.7	4.1	5.0	5.6	3.8	4.0	6.6	3.4

Suwałki $H_s = 165\ m$ $H_b = 169.6\ m$ $h_w = 13\ m$ **Marzec - Mars 1961**

DNI	WIATR KIERUNEK	WIATR SIŁA V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	1.9	.	–	• 3¹⁵–6²⁰ 7³⁰ 8¹⁰ ✶ 11³² • 14³⁰ 14⁵⁵, ≫ 0⁵⁰–7³⁰
2	7	0.0	.	–	✶ 8⁰⁵ ¹⁵ 23⁴⁵ 24, = 1⁴⁵–8¹⁵
3	7	0.4	.	–	✶ 0⁰⁰ ²⁰
4	6	0.0	.	–	• 0⁴⁰–6²⁰ • 9⁴⁰ 10³⁵, = 3³⁰–4⁴⁵ ≡ 11¹³ – 14³⁰, np
5	7	.	.	–	• 4⁴⁰–6²⁵ = 0⁰⁰–3¹⁵ 4³⁰–11⁴⁵
6	6	0.0	.	–	• 6⁴⁰ 8⁴⁰ = 5¹⁰–13³⁰
7	6	.	.	–	= 5¹⁵–18³⁰, ≫ 8¹⁵–15³⁰ 17²⁰–18⁴⁰
8	7	.	.	–	= 7¹⁰–40 9¹⁰–10³⁰, 15⁴⁵–24
9	6	.	.	–	= 0⁰⁰–24
10	6	.	.	–	= 0⁰⁰–24
11	6	0.0	.	–	• 15³⁰–16¹⁵ • 18³⁵–20²⁰ = 0⁰⁰–12¹⁵ ∞ – 15³⁰ = –24; ≫ 12³⁵–16³⁰
12	6	14.6	.	–	▽ 9³⁵ 10¹⁰ • –24, ≫ 23³⁰–24 = 0⁰⁰–6¹⁵ 15³⁰–24
13	7	0.3	.	–	• 0⁰⁰ 7³⁰ ▽ 7⁴⁵–8²⁸ 9¹⁰–25 ✶ 10⁰⁰–14⁴⁸ ✶ 20⁴⁵–21⁰⁵, = 0⁰⁰–7⁴⁵, ≫ 0⁰⁰–24
14	8	1.3	.	–	• 20²⁸–22³⁵ • –24, = np, ≫ 0⁰⁰–50 10¹⁵–13⁵⁰
15	7	0.0	.	–	• 0⁰⁰–3²⁰ • 4⁴⁵–5⁴⁰ = 0⁰⁰–8⁴⁰, ≫ – 5⁴⁵–20²⁵
16	6	3.2	.	–	✶ 6²⁵–7¹⁰ • 8¹⁵ • 9¹⁰ • 17²⁵ = 7¹⁰–19⁴⁵
17	7	0.0	.	–	• 6⁴⁵–8⁰⁰ = 0⁰⁰–4⁴⁵ ≡ 9³⁵ = –11³⁰ ≫ 14⁴⁰–16³⁵
18	6	0.0	.	–	▽ 12²⁰–13²⁵ = 5²⁰–15¹⁵ ≫ 11⁴⁰–12²⁵ 15⁰⁵–30
19	8	0.2	.	–	▽ 9³⁵ 11¹⁰ ✶ 12²⁸–17³⁰ ≫ 3¹⁰–4⁴⁰ 7²⁰–17⁰⁰
20	7	0.0	.	–	✶ 6¹⁵–30 7⁰⁰–03 7¹⁸–40, = 6¹⁰–8³⁵, ≫ 16¹⁰–17⁴⁰, ⌴ 0⁰⁰–7⁰⁰
21	7	2.3	.	–	✶ 6⁵⁵–12²⁰, 13⁰⁴ 14¹⁵ 20²⁰–21⁴⁵, ≫ 3³⁵–11⁴⁰
22	7	0.1	2	–	✶ 0³⁵–3³⁵ ✶ 5¹⁰–10⁵⁰ ▽ 11⁰⁵ 17¹⁰, = 0⁰⁰–10¹⁰, ≫ 11⁴⁰–13¹⁵
23	6	1.6	pł.	–	• 15³⁵–16²⁵ • 16³⁰–17³⁸ 22¹⁰–24, = 7²³–14³⁰
24	6	5.2	.	–	• 0⁰⁰–1⁴⁵ • 5⁰³–12⁴⁵ • 19³⁵–21²⁰ = 5³⁰–15¹⁵, ≫ 5⁰⁷–40, p
25	7	0.2	.	–	• 7⁰⁵ 10¹⁰, = 7²⁰–12⁰⁵, ≫ 9⁰⁵–17⁵⁰, ◡ 19³⁰–21¹⁰
26	7	3.0	.	–	• 19⁴⁵–24, = 2³⁰–8¹⁵ 12³⁵–24 ≫ 9⁰⁵–24
27	6	8.8	.	–	• 0⁰⁰ 2¹⁵–3³⁰ ✶ 7²⁸–33 ✶ –7⁵⁰ ✶ ✶ ✶ 11⁴⁵ 20¹⁰ ▲ 14³⁰–35 ✶ 20¹⁰–22⁴⁰, = na, a, ≫ ≈ 0¹⁰–14¹⁵
28	6	0.3	5	–	▽ 0³⁵–1¹⁰ ✶ 7²⁰, 9⁴⁰–13²⁰, = 0⁰⁰–6²³ ≫ 10¹⁵–20, ◡ 23⁰⁵–24
29	7	3.4	.	–	✶ 12³⁰–14³⁰ ✶ 15²⁵–17⁴⁵ • 21¹⁰–24, ≫ 14⁰²–25, ⌴ 0⁰⁰–8⁰⁰
30	7	5.0	.	–	• 0⁰⁰, 11⁰⁵ ✶ 11³⁰–55 ✶ 23⁴⁵–24, ≫ 7¹⁰–17³⁵
31	8	4.1	3	–	✶ 0⁰⁰–3⁴⁵ ✶ 11¹³–38, 13⁰⁵–35, = 3³⁰–8⁰⁰, ◡ 19⁵⁰–24
Σ	–	55.9	–	. .	UWAGI:

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1	8	0.3	5	–	✶ 3²⁰–6⁴⁵ ✶ 8³⁰ 12¹⁰ ✶ 19¹⁰–20¹⁵ ✶ 21²⁰ 22¹⁰, ≫ 12¹⁰–13³⁰
2	8	0.0	1	–	◡ 21³⁰–24
3	7	2.6	.	–	△ 6²⁰–7⁴⁵ ✶ 11³⁰ • 12¹⁵ ✶ 13²⁰ • 17²⁵, 21¹⁰–30, ⌴ 2⁰⁰–7⁰⁰, ◡ 0⁰⁰–4⁰⁰
4	6	3.6	.	–	✶ 7¹⁰–15⁴⁰ ▽ 15⁵² 17¹⁰ ▽ 17⁴⁵–18⁰⁵
5	7	4.6	.	–	▽ 13⁰²–06 • 13³⁰–15²⁰ • –22⁴⁵
6	7	.	.	–	• 0⁴⁵ 2⁴⁶, = 0⁰⁰–11⁴⁰ ⌒ 21⁰⁰–24
7	6	6.4	.	–	▽ 20⁴⁵–22¹⁰ 23¹⁵–24, R¹ 20³⁰–22³⁰ W-E, = 3¹⁰–14¹⁰, ⌒ 1⁰⁰–8⁰⁰
8	7	0.1	.	–	• 0⁰⁰–25 • 3¹⁰–6⁰⁵ • 16⁴⁵–17⁰⁵ • – 18⁴⁵ ▽ – 19¹⁰, = 6⁰⁵–9⁴⁵ 15⁵⁰–24
9	7	0.3	.	–	▽ 4⁴⁰ 5¹⁰ ✶ 6³⁸ 13⁰⁵, ≫ ≈ 6⁰⁵–16⁴⁰, = 0⁰⁰–6¹⁵
10	8	.	.	–	⌴ 1⁰⁰–6⁰⁰
11	8	.	.	–	⌴ 1⁰⁰–6⁰⁰
12	8	0.0	.	–	= 3⁴⁵ 4⁴⁰ ≡ – 5⁴⁵ – –8⁰⁰, ⌴ 2⁰⁰–7⁰⁰
13	7	0.2	.	–	• 5¹⁰ 7²⁰–10²⁰ 12³⁵–14⁴⁵ 15¹⁵ 20⁵⁰ 21²⁰–24, = 14⁵⁰–24
14	7	.	.	–	• 0⁰⁰–30 = 0⁰⁰–3⁴⁵ ≡ – 7⁴⁰ = – 12⁴⁵, 18³⁰–24, ⌒ 1⁰⁰–8⁰⁰, 21⁰⁰–24
15	7	.	.	–	= 0⁰⁰–8⁰⁰, ⌒ 1⁰⁰–8⁰⁰
16	7	.	.	–	= 2⁴⁵–11³⁰
17	8	.	.	–	= 3⁴⁰–6⁰⁰, ⌒ 1⁰⁰–7⁰⁰ ⌒ 23⁰⁰–24
18	6	0.5	.	–	• 11⁴⁵ 12³⁵ ▽ 22³⁵–24, = 2³⁰–3⁴⁵ ≡ 2-0 6⁵⁰ = –8⁰⁰, 10³⁰–24, ⌒ 1⁰⁰–8⁰⁰
19	8	.	.	–	▽ 0⁰⁰–15 = 0⁰⁰–9³⁰, ⌒ 0⁰⁰–7⁰⁰
20	8	.	.	–	⌴ 2⁰⁰–7⁰⁰
21	8	.	.	–	⌴ 0⁰⁰–7⁰⁰
22	8	.	.	–	≫ 7¹⁵–14⁴⁵, ⌴ 2⁰⁰–5⁰⁰
23	8	.	.	–	≫ 9²⁵–16¹⁰, ⌴ 3⁰⁰–5⁰⁰
24	8	.	.	–	≫ 9⁵⁰–13⁵⁵ ⌴ 4⁰⁰–6⁰⁰
25	8	.	.	–	≫ 9¹⁵–16⁴⁵
26	8	.	.	–	≫ 8²⁰–13⁴⁰
27	7	.	.	–	
28	8	.	.	–	
29	8	.	.	–	≫ 8⁴⁵–11¹⁵ 11⁴⁵–12¹⁵
30	8	2.1	.	–	< 20³⁵–21¹⁵ E, ⌴ 1⁰⁰–5⁰⁰
31					
Σ	–	20.7	–	–	UWAGI:

Suwałki — φ = 54°06' — λ = 22°57' — Maj – Mai 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.7	95.1	95.4	92.7	8.5	8.9	7.7	8.2	10.6	7.5	96	96	96	96	0.5	0.5	0.5	0.5	10 •	10 •	6	NE 4	ENE 4	E 2
2	94.5	94.3	94.1	94.3	5.9	13.1	7.7	8.6	14.5	5.2	100	63	87	85	0.0	5.6	1.3	2.3	10 =	8 ⊙	4	E 4	E 4	SE 2
3	93.6	95.0	91.8	92.8	8.5	16.3	10.7	11.6	17.3	6.7	96	59	84	80	0.5	7.6	2.1	3.4	10	8 ⊙	6	SE 5	SSE 7	SE 3
4	92.8	94.2	96.1	94.4	11.3	12.7	9.5	10.8	14.7	9.3	89	93	86	89	1.5	1.1	1.7	1.4	9	10 •	4	C 0	NW 3	WNW 2
5	98.8	98.3	97.0	98.0	9.4	17.3	11.1	12.2	18.5	2.3	95	57	86	79	0.6	8.5	1.8	3.6	3 ⊙	6 ⊙	2	C 0	WSW 2	SSW 2
6	95.4	90.8	95.4	92.5	14.0	17.9	11.5	13.7	18.1	9.4	65	65	96	75	5.6	7.3	0.5	4.5	8	10	6	S 6	S 8	W 2
7	95.1	95.0	86.4	91.5	10.3	16.7	11.3	12.4	17.6	8.5	96	63	99	86	0.5	7.0	0.2	2.6	9 ⊙	7 ⊙	10 • R	SW 3	SSW 6	SSW 6
8	86.3	87.0	86.4	86.6	8.8	11.5	7.0	8.6	13.1	6.9	86	65	90	80	1.5	4.7	1.0	2.4	9	8	6	W 8	W 8	WSW 3
9	84.1	82.3	81.9	82.8	6.5	10.1	7.5	7.9	12.4	4.6	96	73	93	87	0.5	3.4	0.8	1.6	10	9	10 •	SW 5	SW 4	SW 2
10	81.6	82.7	84.8	83.0	7.7	9.1	7.1	7.8	10.4	6.3	91	75	90	85	0.9	3.0	1.0	1.6	10	9 ⊙	9	SW 3	WSW 3	SW 2
11	87.4	89.9	92.9	90.1	6.3	10.3	7.5	7.9	11.5	5.9	95	80	94	90	0.4	2.5	0.6	1.2	10 •	9	8	WSW 3	NW 4	NW 5
12	93.9	93.4	92.2	93.2	5.5	6.3	4.9	5.4	7.6	4.9	98	92	86	92	0.1	0.7	1.3	0.7	10 •	10	10	N 6	NNW 6	NW 4
13	89.6	90.0	89.8	89.8	5.1	10.5	7.9	7.8	11.9	4.0	92	62	74	76	0.7	4.9	2.8	2.8	10	9	9	W 3	WSW 7	S 4
14	88.4	88.4	88.8	88.5	7.7	11.7	7.9	8.8	12.2	6.8	90	59	89	79	1.0	5.6	1.2	2.6	10 •	6 ⊙	8	SSW 2	SSW 5	S 2
15	88.8	89.3	89.7	89.3	4.9	10.8	8.7	8.3	13.1	2.3	100	64	84	85	0.0	4.6	1.8	2.1	10 =	9	9 •	S 1	N 3	NNE 2
16	90.5	90.8	90.4	90.6	6.9	10.8	9.7	9.3	12.8	5.9	82	66	75	74	1.7	4.5	2.9	3.0	9	10	10	C 0	C 0	WNW 5
17	89.5	89.9	92.0	90.5	9.7	13.9	8.4	10.1	14.9	8.4	91	62	83	79	1.1	6.1	1.8	3.0	10	9 ⊙	6	NW 5	NW 8	N 2
18	93.6	93.8	93.8	93.7	6.7	11.1	9.5	9.2	13.3	3.2	75	53	80	69	2.4	6.2	2.4	3.7	3 ⊙	8 ⊙	7	NW 5	NNW 3	WNW 2
19	92.7	92.3	91.4	92.1	8.3	14.8	11.5	11.5	15.8	4.6	78	47	82	69	2.5	8.8	2.5	4.6	7 ⊙	7	8	WNW 2	WSW 3	WSW 1
20	90.0	89.3	90.2	89.8	11.7	16.9	11.4	12.8	18.3	6.9	81	49	90	73	2.6	9.8	1.4	4.6	9	9	10	SW 4	SSW 6	SSW 1
21	90.2	90.5	90.1	90.3	12.5	16.3	12.5	13.4	18.8	6.9	79	59	82	73	3.1	7.6	2.6	4.4	6 ⊙	9	9	C 0	SSE 4	NNW 2
22	90.8	90.7	90.0	90.5	8.5	10.5	9.1	9.3	13.5	6.9	61	55	70	62	4.3	5.8	3.6	4.6	1 ⊙	7 ⊙	4	N 10	N 8	N 4
23	91.4	91.6	91.4	91.5	8.9	14.7	11.1	11.4	16.9	1.7	59	42	74	58	4.6	9.7	3.4	5.9	2 ⊙	5 ⊙	7	C 0	NW 2	C 0
24	91.6	92.5	93.4	92.5	10.3	12.3	10.3	10.8	13.2	6.9	71	60	83	71	3.6	5.8	2.1	3.8	8	10	9	W 4	W 4	WSW 2
25	94.0	93.3	93.1	93.5	11.7	16.5	10.8	12.4	18.4	6.9	75	48	86	70	3.4	9.7	1.8	5.0	6 ⊙	6 ⊙	2	WSW 3	SW 5	NNW 2
26	93.7	93.5	92.3	93.2	10.5	15.3	11.5	12.2	18.1	9.4	74	64	79	72	3.3	6.3	2.8	4.1	10	10	0	NE 2	ENE 2	NNE 2
27	90.7	89.5	90.0	90.1	15.7	23.5	17.3	18.0	24.1	7.8	76	35	64	58	3.7	19.4	7.1	10.1	5 ⊙	8 ⊙	10	NE 2	SSE 7	NW 3
28	90.7	90.2	88.6	89.8	15.5	25.0	19.1	19.7	25.6	10.4	76	34	55	55	4.3	21.1	10.0	11.8	4 ⊙	6 ⊙	7	NE 1	SSE 7	SSE 5
29	88.0	86.4	84.3	86.2	17.2	24.2	17.9	19.3	25.9	11.6	70	41	77	63	5.8	17.8	4.6	9.4	8 ⊙	8 ⊙	5	SSE 2	SE 5	ESE 4
30	82.2	81.6	82.7	82.2	16.1	25.0	15.7	18.1	26.0	14.3	90	44	97	77	1.7	17.9	0.6	6.7	8 ⊙	8 ⊙	10 R	E 6	SE 6	NE 3
31	83.7	84.9	85.7	84.8	14.7	17.0	14.7	15.3	17.2	13.8	97	89	90	92	0.5	2.2	1.6	1.4	9	9 ⊙	9	NW 3	NW 4	WNW 2
M	90.4	90.3	90.3	90.3	9.8	14.5	10.6	11.4	16.0	7.0	85	62	84	77	2.0	7.3	2.3	3.9	7.8	8.3	7.1	3.2	4.8	2.7

Czerwiec – Juin

1	86.8	86.8	87.4	87.0	14.9	21.0	15.9	16.9	22.4	11.0	82	49	76	69	3.1	12.6	4.4	6.7	0 ⊙	5 ⊙	0	W 2	S 3	NE 3
2	87.8	87.6	87.6	87.7	17.3	23.6	18.3	19.4	24.4	11.0	73	47	81	67	5.2	15.4	3.8	8.1	3 ⊙	4 ⊙	5	NE 2	N 3	NNE 2
3	88.3	89.3	90.7	89.4	19.1	22.5	18.7	19.8	24.8	13.6	84	61	74	73	3.6	10.6	5.6	6.6	5 ⊙	8 ⊙	4	NE 1	E 3	NE 4
4	93.0	93.1	94.3	93.5	19.7	26.1	19.0	21.0	27.1	14.8	73	38	65	58	6.1	20.8	8.1	11.7	0 ⊙	6 ⊙	2	NE 3	E 8	NE 3
5	97.6	98.1	98.0	97.9	18.6	24.7	17.9	19.8	25.7	13.6	75	39	66	60	5.3	19.1	7.1	10.5	6 ⊙	6 ⊙	0	E 2	E 7	C 0
6	99.5	98.2	96.0	97.9	18.1	24.6	17.1	19.2	25.9	11.0	61	34	71	55	8.1	20.3	5.6	11.3	0 ⊙	1 ⊙	1	E 2	SE 3	C 0
7	95.8	94.4	92.0	94.1	19.1	23.1	18.1	19.6	25.1	11.3	67	45	76	63	7.4	15.5	5.1	9.3	1 ⊙	8	10	SE 1	SE 9	E 3
8	90.3	90.2	90.1	90.2	18.7	23.4	16.9	19.0	25.1	15.4	74	61	97	77	5.6	11.2	0.6	5.8	9	9	10 • R	SE 7	S 8	SW 3
9	91.7	93.1	93.9	92.9	17.5	19.9	16.9	17.8	21.2	15.2	91	80	95	89	1.8	4.5	1.0	2.4	9	10	6	C 0	SW 4	C 0
10	94.5	95.0	94.0	94.5	19.3	25.8	20.2	21.4	27.5	15.5	77	38	68	61	5.2	20.6	7.7	11.2	3 ⊙	7 ⊙	8	NE 1	SE 5	C 0
11	94.2	93.2	91.2	92.9	18.1	25.8	18.2	20.1	26.9	14.6	79	46	77	67	4.3	17.9	4.9	9.0	3 ⊙	7 ⊙	6	S 5	S 4	C 0
12	89.8	89.0	88.2	89.0	17.1	24.6	15.9	18.4	25.9	15.6	92	47	93	77	1.6	16.3	1.4	6.4	8	6 ⊙	10	E 2	SSW 2	C 0
13	87.3	86.7	86.2	86.7	15.5	19.2	17.9	17.6	22.0	14.7	92	63	81	79	1.3	8.1	3.8	4.4	10	7	10	WNW 4	SW 3	NE 2
14	84.9	85.6	85.6	85.4	14.7	15.9	14.7	15.0	17.9	12.8	92	97	90	93	1.3	0.6	1.6	1.2	10 •	10 •	10	C 0	SSE 6	SSE 2
15	84.8	86.6	88.9	86.8	13.7	15.5	13.3	14.0	16.8	11.8	94	80	93	89	0.9	3.5	1.1	1.8	10 •	10 •	10	S 2	W 7	SW 7
16	91.1	92.2	93.6	92.3	11.7	15.5	12.1	12.8	15.7	10.9	89	76	87	84	1.5	4.3	1.8	2.5	10 •	10	10 •	W 3	SW 8	WSW 7
17	93.8	95.2	95.5	94.8	12.7	14.3	14.2	13.8	18.1	11.6	92	94	80	89	1.2	0.9	3.2	1.8	10	10 •	2	WSW 3	SW 6	WSW 3
18	95.2	95.6	90.8	93.2	14.5	19.1	19.6	18.2	22.9	10.1	94	76	69	80	0.9	5.2	7.1	4.4	10	10	9	SW 2	S 9	S 4
19	92.7	95.3	96.8	94.9	15.5	18.6	12.9	15.0	20.6	12.8	90	38	76	68	1.7	13.3	3.6	6.2	7	7 ⊙	5	W 8	W 7	W 3
20	100.0	101.7	103.4	101.7	12.5	16.2	11.3	12.8	18.1	9.4	76	56	77	70	3.6	8.1	3.1	4.9	8 ⊙	7 ⊙	2	W 6	WSW 7	W 2
21	103.5	101.5	98.3	101.1	12.9	18.3	13.1	14.4	19.3	6.8	67	43	76	62	4.9	12.0	5.6	6.8	8 ⊙	9	10	S 5	SW 5	NNW 3
22	102.7	102.6	99.2	101.5	11.9	17.3	13.1	13.8	19.0	9.9	84	50	83	72	2.1	9.9	2.6	4.9	4 ⊙	7 ⊙	2	W 4	W 6	C 0
23	92.8	92.7	94.8	93.4	12.1	21.1	13.9	15.2	22.4	9.9	94	47	91	77	0.8	13.2	1.5	5.2	10 •	6 ⊙	5	SE 6	NW 8	W 5
24	93.0	94.3	94.5	93.9	14.9	18.7	14.3	15.6	19.2	11.6	77	60	77	71	3.8	8.6	3.8	5.4	10	7 ⊙	4	SW 6	W 7	SW 4
25	92.0	91.5	89.7	91.1	17.3	22.8	18.7	19.4	24.1	11.9	64	46	67	59	7.1	14.9	7.1	9.7	8 ⊙	8 ⊙	3	SW 8	W 9	NW 3
26	89.7	91.6	92.3	91.2	17.9	23.0	17.1	18.8	24.2	12.9	72	49	76	66	5.7	13.3	4.7	7.9	1 ⊙	4 ⊙	1	W 4	W 7	N 2
27	92.6	89.5	86.4	89.5	19.3	27.8	21.8	22.7	29.9	10.5	68	48	74	63	7.2	19.5	6.8	11.2	5 ⊙	3 ⊙	10	E 5	SE 10	W 5
28	88.0	94.3	100.1	94.1	18.1	13.5	11.7	13.8	22.0	11.7	93	78	75	82	1.5	3.4	3.4	2.8	10 •	10	4	NW 7	W 6	W 3
29	102.5	104.0	103.9	103.5	13.5	15.1	12.8	13.6	16.4	8.5	82	78	84	81	2.8	3.9	2.4	3.0	7 ⊙	10	8	W 5	W 4	W 2
30	103.8	103.7	103.9	103.8	14.9	20.3	15.1	16.4	22.0	9.4	86	60	80	75	2.4	9.4	3.5	5.1	4 ⊙	6 ⊙	1	W 5	W 8	NW 2
31																								
M	93.3	93.7	93.6	93.5	16.0	20.6	16.0	17.2	22.4	11.9	81	58	79	73	3.6	11.2	4.0	6.3	6.4	7.3	5.5	3.7	6.1	2.5

Suwałki $H_s = 165\ m$ $H_b = 169{,}6\ m$ $h_w = 13\ m$ **Maj – Mai 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	12.2	•	–	▽° 2⁰⁵–⁴⁵ 4⁵⁰–5³⁵ ●⁰⁻¹ –15⁰⁵, = 3²⁰–15¹⁵, 22³⁰–24
2	7	•	•	–	= 0⁰⁰–3³⁰ ≡¹⁻⁰–7⁴⁰ ≡– 11²⁰
3	8	0.1	•	–	▽° 18⁴⁵–19⁰⁵, 23¹⁵–⁴⁰, = 2⁰⁰–8⁰⁰, ⌒° 2⁰⁰–8⁰⁰
4	6	9.5	•	–	▽° 2⁴⁵–3¹⁵ 9⁵⁰–10¹⁰ ▽¹ 10⁴⁵–13²⁰ ▽° 17³⁵–18⁴⁰ ↖° 10³⁰–11⁴⁰ SW–NE
5	7	•	•	–	≡¹⁻⁰ 1¹⁰–4⁴⁰ ≡–8³⁵ 22²⁰–24, ⌒² 1⁰⁰–8⁰⁰
6	7	15.3	•	–	●⁰⁻¹ 13¹⁰–19⁵⁰ ●° 19⁵⁵–20¹⁵, = na ≡² np
7	8	12.4	•	–	▽¹ 13²⁵–⁵⁰ ▽⁰⁻¹ 17⁴⁵–21¹⁰ ●° –24, ↖° 19²⁰–20⁴⁰ SW–SE, ≡² 0⁰⁰–1⁴⁵ ≡–8⁰⁰
8	7	0.5	•	–	●° 0⁰⁰–4⁵⁵ ▽° 11⁰⁵–³⁵ 13²⁵–14⁰⁵, ≫ 9¹⁵–11⁴⁵
9	7	5.3	•	–	●° 7³⁵–8²⁵ ▽ 11⁴⁰ 18³⁰ ▲¹ 11⁵⁵–⁵⁶ ▽° 20⁰⁷–21³⁵, = na a, p–24, ⌒¹ p
10	7	8.0	•	–	●° 5⁴⁰–6²⁰, 8¹⁰–11⁰⁵ ▽° 13⁴⁰–14⁰², 20³⁶–⁴⁵ = 0⁰⁰–11¹⁰
11	7	5.2	•	–	●° 0⁰²–2³⁵, ●⁰⁻¹ 4⁰⁰–7²⁰ ●° –8¹⁰ ●⁰⁻¹ –10²⁵ 11¹⁰–12⁵⁵ ▽° 16⁴⁰–17⁵⁰
12	7	0.5	•	–	●° 0⁴⁵–1⁴⁵ 2³⁰ ●° 4¹⁰ 7²⁵ ●° –8¹⁵ ●° 11²⁵, = 1⁰⁰–12¹⁰
13	8	3.8	•	–	●° 0³⁵ 2¹⁰ 4¹⁵–5²⁰ 6²⁰ ●° 22³⁰–24
14	8	2.0	•	–	●° 0⁰⁰–5²⁰ ●⁰⁻¹ 5⁴⁰–7⁰⁵ ▽° 10²⁵ 15²⁵ 21⁴⁵–⁵⁰ 22³⁰–³³, = 1⁰⁰–7¹⁵
15	7	0.6	•	–	▽° 10³⁰–11⁵⁵, 15²⁵–³⁰, 20³⁰–22¹⁰, = 0⁰⁰–2⁴⁵ ≡° –6⁴⁸ ≡–8⁰⁰
16	7	3.4	•	–	●° 23¹⁰–24
17	7	•	•	–	●° 0⁰⁰–5⁵⁵
18	7	•	•	–	⌒¹ 1⁰⁰–8⁰⁰
19	8	0.0	•	–	▽° 14⁴⁰–16⁵⁰, ⌒° 2⁰⁰–8⁰⁰
20	8	2.6	•	–	●² 14⁴⁵–15⁴⁵ ▽° 17⁴⁰–18¹⁰, ⌒° 1⁰⁰–7⁰⁰
21	7	0.0	•	–	▽ 11⁴²–12¹⁹, = 4³⁰–8¹⁰
22	8	•	•	–	≫ 6³⁰–7⁴⁰, ⌒¹ 2⁰⁰–9⁰⁰
23	8	•	•	–	= 1¹⁰–4¹⁵ ⌒¹ 1⁰⁰–9⁰⁰
24	8	•	•	–	⌒° 1⁰⁰–5⁰⁰
25	7	•	•	–	= 19³⁰–24, ⌒° 2⁰⁰–6⁰⁰
26	7	•	•	–	= 0⁰⁰–8¹⁰ 16³⁰–24, ⌒° 2⁰⁰–8⁰⁰
27	7	•	•	–	= 0⁰⁰–8⁰⁰, ⌒¹ 2⁰⁰–6⁰⁰
28	7	0.0	•	–	▽° 15¹⁵–25, 16²⁵–³⁵, ⌒° 2⁰⁰–7⁰⁰
29	7	0.0	•	–	▽° 20³⁵–⁴³, ⌒° 2⁰⁰–7⁰⁰
30	7	7.8	•	–	●⁰⁻¹ 14³⁰ 23⁰⁵ ↖° 14¹⁰–22³⁵ SW–NE, = 23³⁰–24
31	6	0.0	•	–	▽° 9⁰¹–¹², 10¹⁶–²⁴, 11¹⁵–²⁰, = 0⁰⁰–1⁴⁵ ≡–3⁴⁵ ≡–24
Σ	–	89.2	–	–	UWAGI.

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1	7	•	•	–	= 0⁰⁰–6³⁰, ⌒° 2⁰⁰–8⁰⁰
2	7	•	•	–	⌒° 2⁰⁰–7⁰⁰ 23⁰⁰–24
3	7	•	•	–	(↖) 12³⁰–14²⁵ SE–NW, ⌒° 0⁰⁰–8⁰⁰
4	8	•	•	–	⌒° 2⁰⁰–8⁰⁰
5	8	•	•	–	⌒° 2⁰⁰–7⁰⁰
6	8	•	•	–	⌒° 3⁰⁰–7⁰⁰
7	8	0.0	•	–	●° 17⁰⁵ 19⁴⁵, ≫ 13³⁰ 16³⁰, ⌒° 2⁰⁰–8⁰⁰
8	8	6.2	•	–	▽° 18¹⁰–¹⁵ 19¹⁵–23¹⁵, ↙² 10–50 W, ↖° 18⁵⁰–22³⁵ S–N
9	6	0.0	•	–	▽° 16¹⁵ 17⁰⁵, ↙° 12³⁵ 16²⁰ SE, E, = 3¹⁵–24, ⌒° 23⁰⁰–24
10	8	1.6	•	–	▽² 15¹⁰–16²⁰ ▲° 16⁰⁵–⁰⁸, ↖¹ 14⁵⁰–16⁴⁰ SW–NE, = 0⁰⁰–8⁰⁰, ⌒° 0⁰⁰–8⁰⁰
11	8	0.0	•	–	▽° 15¹⁰–16⁰⁵, ↖° 14⁵⁰–16⁴⁵ NW–SE
12	7	20.5	•	–	●²⁻⁰ 17³⁰–18²⁵ ▽° 19³⁰ 21⁴⁵, ↖² 16⁵⁰–19²⁵ E–W, = 19²³–24, ≫ 17⁰⁵–⁵⁰
13	8	0.1	•	–	●° 22⁴⁰–24, = 0⁰⁰–8⁴⁰
14	6	7.0	•	–	●° 0⁰⁰ 2²⁰ ●⁰⁻¹ 6³⁵–10²⁵ ●⁰⁻² 11⁰⁵–14⁴⁰ ▽ 21¹⁵–²⁵, = 10²⁵–15⁰⁶, 21¹⁰–24
15	6	12.7	•	–	●° 6³⁵–7²⁰ 7²⁸–⁴⁰ ●° –9⁴⁵ ●⁰⁻¹ 10¹⁵, 22⁰⁵, = 0⁰⁰–9⁰⁰
16	8	13.1	•	–	▽⁰⁻¹ 1⁴⁵ 17³⁰ ●¹⁻⁰ 17³⁰–21²⁵ 22¹⁵
17	6	2.4	•	–	●° 0⁴⁰ 2⁵⁰ 9³⁰–14¹⁰ ▽° 17²⁴–³⁰, = a–p, np
18	6	0.1	•	–	●° 8¹⁰ 12⁴⁰, = 0⁰⁰–18⁰⁰
19	8	•	•	–	●° 2¹⁵ 3³⁰–4⁴⁵
20	8	0.0	•	–	▽° 10⁰¹–⁰⁵ 12²⁵–³⁴, ⌒° 2⁰⁰–7⁰⁰
21	8	3.4	•	–	▽¹ 22¹⁰–23¹⁵, = 23²⁰–24, ⌒¹ 0⁰⁰–9⁰⁰
22	8	2.7	•	–	▽° 0⁵⁰ 1²⁰, = 0⁰⁰–6⁴⁰
23	7	0.0	•	–	●° 3⁰³–9⁴⁰ = 9⁴⁰–13²⁰, ⌒¹ 2⁰⁰–3⁰⁰
24	7	•	•	–	= 8²⁰–11¹⁰
25	7	•	•	–	
26	8	•	•	–	
27	8	3.0	•	–	▽° 22⁴⁵–24, ↖¹ 21⁴⁰–24 SW–NE, = 4⁴⁰–7¹⁰, ≫ 13²⁰–14⁵⁰, 21¹⁵–⁴⁵, ⌒² 2⁰⁰–8⁰⁰
28	7	11.9	•	–	▽° 0⁰⁰–3²⁰ ▽⁰⁻¹ 5⁰⁵–13²⁶, ↖¹ 0⁰⁰–⁴⁵ ↖° 8⁴⁵–9⁴⁰ NW–SE, ≫ 14⁵⁵–20⁴⁵
29	7	0.0	•	–	▽° 11²³–⁴⁰ 14³⁰–15⁰³, ⌒¹ 23⁰⁰–24
30	8	0.0	•	–	= 2²⁰–8³⁰, ⌒° 0⁰⁰–8⁰⁰
31					
Σ	–	84.7	–	–	UWAGI.

Suwałki — φ = 54°06' — λ = 22°57' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	104.8	104.7	103.3	104.3	12.9	20.8	17.0	16.9	22.5	10.9	96	56	70	74	0.6	10.8	5.8	5.7	10	6 ⊙	1	NNW 2	C 0	C 0
2	101.9	100.2	99.5	100.5	18.6	25.4	19.3	20.6	26.4	10.0	75	43	68	62	5.3	18.5	7.2	10.3	1	2 ⊙	0	WSW 3	W 7	WNW 2
3	98.4	96.9	91.7	95.7	18.7	27.2	23.0	23.0	28.5	12.2	75	39	61	58	6.0	21.9	11.0	13.0	0 ⊙	6 ⊙	0	SW 3	SW 7	SSW 3
4	90.4	89.3	86.3	88.7	16.1	22.0	18.1	18.6	23.6	15.2	82	51	73	69	3.1	13.0	5.6	7.2	4 ⊙	5 ⊙	6	W 7	WSW 7	WNW 3
5	86.6	89.6	91.6	89.3	14.9	16.9	12.7	14.3	18.3	14.1	87	60	76	74	2.2	7.7	3.6	4.5	9	8 ⊙	8	SW 5	SW 9	SSW 2
6	93.1	93.8	95.3	94.1	12.5	16.9	12.1	13.4	17.6	6.8	76	46	73	65	3.6	10.4	5.8	5.9	4 ⊙	9	8	SW 3	SW 9	S 4
7	96.5	97.1	97.7	97.1	12.5	16.6	11.7	13.1	18.5	8.2	81	51	89	74	2.7	9.2	1.5	4.5	9	8	8	SW 3	SW 8	WSW 3
8	98.5	97.7	95.9	97.4	13.1	17.5	15.3	15.3	18.7	10.5	82	48	72	67	2.8	10.4	5.0	6.1	7 ⊙	7 ⊙	10	SW 3	WSW 6	SSW 2
9	92.1	89.3	86.7	89.4	14.2	20.8	14.3	15.9	22.5	11.5	65	42	88	65	5.6	14.4	2.0	7.3	8 ⊙	7 ⊙	10	S 4	S 6	SSE 2
10	86.6	88.1	89.0	87.9	13.1	13.9	12.2	12.8	18.5	12.0	87	85	88	87	1.9	2.3	1.7	2.0	10	9	9	W 6	WNW 6	SW 3
11	90.4	91.2	92.5	91.4	15.0	16.5	12.7	13.7	18.3	9.6	84	57	71	71	2.5	8.0	4.3	4.9	8	10 •	3	WSW 6	WSW 4	C 0
12	91.5	91.4	89.7	90.9	13.5	16.1	13.7	14.2	18.7	7.5	85	88	94	89	2.3	2.1	0.9	1.8	9	10	2	SSW 2	SSE 3	C 0
13	87.3	84.5	78.9	83.6	13.7	23.8	22.4	20.6	26.9	9.9	99	53	68	73	0.2	13.9	8.7	7.6	8	9	10	SE 1	E 5	E 5
14	78.8	83.1	87.3	83.1	16.1	17.7	13.9	15.4	22.4	13.5	88	77	74	80	2.1	4.5	4.1	3.6	10	10	10	WSW 8	SW 7	WSW 5
15	90.0	89.9	91.4	90.4	14.1	22.8	15.2	16.8	23.8	9.6	68	38	91	66	5.1	17.2	1.5	7.9	0 ⊙	5 ⊙	3	SW 2	S 5	NW 1
16	90.8	88.4	85.9	88.4	15.9	22.4	15.8	17.5	23.1	8.0	84	47	93	75	2.9	14.4	1.3	6.2	5 ⊙	9	10	E 3	E 4	NNW 5
17	85.5	86.5	86.7	86.2	14.1	19.5	14.9	15.8	21.9	12.6	88	48	79	72	2.0	11.8	3.4	5.7	10	9 ⊙	4	WSW 5	W 4	W 2
18	84.7	85.0	85.0	84.9	14.3	16.7	13.1	14.3	18.1	11.2	89	65	89	81	1.8	6.6	1.6	3.3	8	9	9	SW 3	SW 7	W 1
19	87.1	87.9	88.7	87.9	11.9	20.0	14.7	15.3	21.9	8.6	99	56	90	82	0.1	10.3	1.6	4.0	10	8 ⊙	10	S 4	SW 3	C 0
20	89.6	89.7	89.1	89.5	15.0	21.6	15.7	17.0	22.4	10.8	87	46	82	72	2.2	14.0	3.2	6.5	0 ⊙	7 ⊙	4	C 0	SW 1	NW 2
21	89.1	88.0	87.7	88.3	15.5	20.8	13.0	15.6	22.1	9.4	88	50	95	78	2.1	12.4	0.7	5.1	0	8 ⊙	7	NW 2	W 5	SW 3
22	86.5	87.0	88.2	87.2	14.5	16.5	13.9	14.7	19.5	12.9	88	85	91	88	2.0	2.9	1.5	2.1	9	9 •	10	SW 3	W 4	WSW 3
23	91.0	92.1	93.6	92.2	14.5	15.1	14.5	14.6	17.8	12.5	91	82	84	86	1.5	3.2	2.7	2.5	10	10 •	8	WSW 2	W 4	SW 2
24	95.5	96.3	98.0	96.6	13.7	18.0	14.7	15.3	19.4	12.7	92	59	84	78	1.3	8.4	2.7	4.1	9 ⊙	9 ⊙	9	SSW 3	WSW 6	WNW 6
25	99.3	100.0	99.9	99.7	12.1	16.5	13.3	13.8	17.9	9.6	88	69	78	78	1.7	5.9	3.3	3.6	10	10	9	SW 4	WSW 7	W 4
26	97.3	95.3	91.7	94.8	13.6	13.7	14.5	14.1	15.8	11.7	86	92	94	91	2.2	1.3	0.9	1.5	10	10	10	SSW 3	SW 4	S 7
27	86.2	85.4	84.9	85.5	14.7	21.8	15.7	17.0	23.0	13.8	92	53	80	75	1.3	12.1	3.5	5.6	10 •	9 ⊙	10	S 6	SW 7	WNW 4
28	84.9	84.3	83.0	84.1	15.3	18.1	15.2	16.0	18.3	12.6	88	71	97	85	2.1	6.0	0.6	2.9	9	10 •	10 •	SSW 4	SSW 3	SW 5
29	85.9	89.0	93.1	89.3	13.5	14.9	13.9	14.0	18.8	13.2	99	88	83	90	0.2	2.0	2.7	1.6	10 •	10 •	9	C 0	NW 2	WNW 1
30	95.5	96.2	95.2	95.6	13.9	14.3	12.7	13.4	14.8	10.9	90	94	94	93	1.6	0.9	0.9	1.1	10	10 •	10 •	NW 1	NW 4	NNE 7
31	90.4	93.2	92.8	92.1	15.5	19.2	15.8	16.6	20.6	12.5	100	69	71	80	0.0	7.0	5.1	4.0	10 ≡	9	8	NNE 3	SSE 10	SSE 8
M	91.2	91.5	91.0	91.2	14.4	18.8	15.0	15.8	20.7	11.1	86	62	82	77	2.3	9.1	3.3	4.9	7.3	8.3	7.3	3.4	5.3	3.1

Sierpień – Août

1	91.9	91.9	93.3	92.4	13.1	12.5	13.9	13.4	16.5	12.0	86	94	90	90	2.1	0.9	1.6	1.5	10	10 •	10 •	SE 7	S 8	SSW 6
2	95.2	95.3	94.0	94.8	14.3	21.0	16.3	17.0	22.4	11.8	81	49	84	71	3.1	12.6	2.9	6.2	2 ⊙	8	0	SSW 5	SW 7	C 0
3	93.7	94.7	96.0	94.8	16.1	20.2	16.3	17.2	22.2	12.0	86	82	79	82	2.5	4.2	3.8	3.5	6	9	10	SSW 1	W 5	WSW 3
4	97.9	97.2	95.3	96.8	13.3	18.7	14.7	15.4	19.3	10.9	87	48	76	70	2.0	11.2	4.0	5.7	9	9	9	W 2	WSW 5	SSW 3
5	91.9	92.9	94.0	92.9	15.0	18.7	14.3	15.6	20.7	12.5	91	58	83	77	1.5	9.0	2.7	4.4	10	8 ⊙	5	WSW 6	SW 8	WSW 2
6	92.3	90.4	91.0	91.2	15.7	26.8	20.2	20.7	27.9	10.6	88	52	83	74	2.1	16.8	4.0	7.6	10	8	3	WSW 3	SSW 7	NNW 2
7	90.8	91.3	91.4	91.2	15.7	19.1	16.5	17.0	20.6	13.5	90	86	93	90	1.7	3.2	1.4	2.1	8	10	10	E 3	NE 2	WSW 3
8	96.6	97.3	97.4	97.1	13.9	17.7	14.9	15.4	19.9	12.8	85	65	88	79	2.3	7.0	2.0	3.8	7 ⊙	9	6	W 4	W 3	C 0
9	97.3	97.4	99.6	98.1	15.5	24.4	16.3	18.1	25.6	13.0	90	61	76	76	1.7	12.0	4.3	6.0	9	7 ⊙	10	SSW 2	SSW 5	NW 3
10	101.7	101.8	98.3	100.6	15.7	22.1	17.9	18.4	23.2	11.2	77	46	68	64	4.1	14.4	6.5	8.3	4 ⊙	5 ⊙	8	NE 1	E 7	ENE 3
11	92.7	92.4	92.6	92.6	15.6	20.4	15.5	16.8	21.0	14.7	90	80	98	89	1.7	4.9	0.4	2.3	6 ⊙	10	10	NE 3	ESE 4	WNW 2
12	95.1	94.6	93.1	94.3	15.9	19.1	15.6	16.6	21.0	13.3	90	73	94	86	1.8	6.0	1.1	3.0	8	9 ⊙	10 •	W 5	WSW 3	NW 3
13	93.4	94.2	97.0	94.9	13.7	17.9	12.4	14.1	18.5	12.3	94	60	86	80	0.9	8.2	2.0	3.7	10	9	0	WNW 2	W 7	WNW 3
14	98.0	98.1	96.0	97.4	11.1	17.7	12.5	13.4	19.9	8.8	99	55	87	80	0.2	9.0	1.9	3.7	10	8	8	WSW 3	SW 4	C 0
15	93.2	90.7	88.3	90.7	12.9	19.8	13.1	14.7	19.9	8.2	87	57	96	80	1.9	9.9	0.6	4.1	7 ⊙	9 ⊙	10	S 3	SSW 8	SSW 2
16	87.4	87.1	86.2	86.9	12.8	14.6	12.1	12.9	17.1	11.7	95	87	88	90	0.7	2.2	1.7	1.5	9	10 •	9	SSW 5	S 7	SSW 3
17	84.3	85.2	86.4	85.3	11.5	15.5	12.3	12.9	18.6	10.3	90	70	89	83	1.4	5.3	1.5	2.7	10	8 ⊙	4	SSW 5	NW 3	WNW 1
18	84.9	82.3	81.1	82.8	10.7	16.9	11.9	12.8	18.5	5.8	99	64	88	84	0.2	7.0	1.7	3.0	6 ⊙	9	2	W 1	W 5	WNW 5
19	78.9	78.6	79.5	79.0	12.9	17.2	12.5	13.8	18.1	10.3	87	59	92	79	1.9	8.0	1.2	3.7	10	6	8	W 8	WSW 11	WSW 5
20	80.4	81.1	83.4	81.6	12.7	15.6	11.5	12.8	16.4	10.0	92	71	96	86	1.2	5.1	0.5	2.3	10 •	9	0	SW 8	W 10	SW 4
21	83.6	85.6	87.5	85.6	12.1	17.7	13.8	14.4	17.8	10.3	89	52	94	78	1.5	9.7	0.9	4.0	9	8 ⊙	10	WSW 8	SW 10	SW 7
22	85.6	85.0	82.2	84.3	15.9	19.7	14.3	16.0	20.4	13.7	84	68	95	82	2.9	7.3	0.7	3.6	7 ⊙	9	8	SSW 6	SSW 9	WSW 3
23	83.8	84.4	86.4	84.9	12.5	16.3	11.7	13.0	16.7	11.7	94	76	95	88	0.9	4.3	0.6	1.9	10	8	4	WSW 7	WSW 7	W 5
24	87.5	90.4	92.6	90.2	12.3	14.7	11.7	12.6	18.2	10.4	89	73	95	86	1.5	4.5	0.6	2.2	10	8	9	W 6	WNW 4	W 5
25	91.2	91.9	92.8	92.0	12.0	13.1	11.3	11.9	16.9	10.3	98	93	82	91	0.3	1.1	2.5	1.3	10 •	10 •	9	SSW 4	WSW 6	SSW 3
26	94.1	96.2	98.8	96.4	11.1	16.9	11.2	12.6	17.8	8.7	89	53	85	76	1.5	9.1	2.0	4.2	7 ⊙	8 ⊙	9	WSW 5	W 9	W 2
27	99.0	99.0	98.0	98.7	13.2	21.2	17.3	17.2	22.5	11.0	100	65	91	85	0.0	8.8	1.8	3.5	10 ≡	8	10 • R	WSW 2	W 4	W 4
28	99.5	100.9	99.7	100.0	13.1	17.2	15.3	15.2	17.8	11.8	92	67	84	81	1.3	6.5	2.8	3.5	9	9	10	W 4	W 11	W 6
29	99.5	100.0	100.9	100.1	14.1	19.1	12.5	14.6	19.3	11.7	90	48	92	77	1.6	11.4	1.2	4.7	9	8	2	WNW 5	WNW 8	NW 4
30	103.6	104.3	104.6	104.2	11.3	18.3	11.7	13.2	18.8	8.0	94	48	84	75	0.8	11.0	2.1	4.6	6 ⊙	3 ⊙	0	NNW 2	N 3	NW 1
31	106.2	107.2	107.8	107.1	13.9	21.5	15.9	16.8	22.9	10.7	76	54	86	72	3.9	11.8	2.5	6.1	1 ⊙	2 ⊙	0	NW 4	NNW 2	WNW 2
M	92.6	92.9	93.1	92.9	13.5	18.4	14.1	15.0	19.9	11.1	90	65	88	81	1.7	7.8	2.0	3.8	8.0	8.1	6.5	4.1	6.2	3.1

Suwałki

$H_s = 165\ m$ $H_b = 169{,}6\ m$ $h_w = 13\ m$

Lipiec – Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	●° 5³⁵ 6⁴⁵, = 0¹⁰ 8⁰⁰
2	7	.	.	–	⌓° 2⁰⁰ 8⁰⁰, 23⁰⁰ 24
3	6	0.3	.	–	= 0⁰⁰ 13³⁰, ⌓¹ 0⁰⁰ 7⁰⁰
4	8	0.8	.	–	▽° 3⁰⁵ 14⁰⁵, ☇° 3⁰⁰ 4¹⁰ NW-E
5	7	.	.	–	●¹ 2⁰⁰ 3⁰⁰, ●° 3⁴⁵ = 4⁰⁰ 7⁰⁰ 8⁴⁰ 10¹⁰
6	8	0.2	.	–	▽° 17²⁰ 18²⁵, 18⁴⁰ 19⁴⁵, ⌓° 2⁰⁰ 8⁰⁰
7	8	0.0	.	–	●° 18²⁰ 19²⁵
8	8	0.2	.	–	●° 12⁰¹⁻⁰⁷ = 21²⁵ 24
9	7	0.0	.	–	●° 2³⁰ 3⁰⁵, ●° 5¹⁰, = 0⁰⁰ 5⁴⁵ 20¹⁰ 24
10	8	2.8	.	–	●° 6²⁰⁻³⁵ 6⁴⁵ 7⁰⁵, ●°² 12²⁵ 18²⁵, = 0⁰⁰⁻²⁰
11	8	0.0	.	–	●° 13³⁰⁻³⁸
12	6	1.9	.	–	●°¹ 0³⁵ 12⁴⁰ = 2⁰⁰⁻²⁰ ≡° 2³⁵ = 17³⁰, 21³⁰ 24
13	7	0.0	.	–	●° 21⁴⁰ 22⁰⁵, = 0⁰⁰ 1⁴⁰ ≡¹ 7³⁵ = 12²⁰
14	7	0.0	.	–	●° 6⁵³ 7¹⁰, 13³⁰⁻³³
15	7	.	.	–	(☇)° 19³⁵, 20¹² W-E, = 2³⁰ 7³⁰, np, ⌓¹ np
16	8	3.4	.	–	●° 14³⁵ 15¹⁰, ●° 20²⁰, ▽¹ 20⁴⁰, = 0⁰⁰ 1⁵⁰ ≡° 5³⁵ = 7³⁰, ⌓° 0⁰⁰ 8⁰⁰
17	8	3.6	.	–	= 2⁰⁰ 7¹⁵, ⌓¹ 22⁰⁰ 24
18	7	0.3	.	–	●¹ 2⁰³⁻⁰⁵, ●° 3¹⁵, ▽° 18⁴⁰ 19²⁵, (☇)° 18²⁵ 19¹⁰ SW-NW, = 5³⁰ 7⁴⁵, ⌓¹ 0⁰⁰ 2⁰³
19	8	0.5	.	–	●° 19⁰⁶⁻¹⁰, 20⁰² 21¹⁰, ☇ 21¹⁰ 22⁰⁰ E, = 1⁴⁰ 3²⁰ ≡¹ 7⁴⁰ = 11¹⁰
20	7	.	.	–	= 4¹⁵ 10³⁰, 23³⁰ 24
21	7	0.5	.	–	●° 17³⁵ 18³⁵, (☇)° 17¹⁰⁻⁵⁰ S-E, = 0⁰⁰ 9³⁰, ⌓¹ 2⁰⁰ 9⁰⁰
22	7	3.9	.	–	●° 9¹⁰⁻³⁰ 10⁵⁰ 14⁴⁰, = 23³⁰ 8⁰⁰
23	8	1.6	.	–	●° 0⁴⁵ 2²⁵, ●° 3⁴⁰ 4¹⁵, ●° 5¹⁵, ▽° 13³⁰⁻³⁷
24	7	0.0	.	–	●°¹ 0¹⁰ 3¹⁵, 17⁰¹⁻²⁶, = 3¹⁰ 7⁴⁵
25	8	0.0	.	–	●° 14¹⁵⁻³⁰, 15²⁰⁻³⁵
26	6	2.9	.	–	●° 12³² 13²⁵, ●°¹ 15⁴⁰ 18⁴⁵ 19⁴⁰, ●° 20²⁰, = 13²⁵ 24
27	7	0.0	.	–	●° 4⁴⁰ 8⁰⁵, 22⁴⁰ 23³⁵, = 0⁰⁰ 13⁴⁰
28	6	15.5	.	–	●° 11³⁰ 23⁴⁰, = 0²⁰ 8⁰⁵
29	6	4.0	.	–	●°³ 0³⁵ 11⁶³, ▽° 12⁰³⁻²⁵, 13⁰¹ 14²⁰
30	6	21.3	.	–	●°¹ 9¹⁰ 23¹²
31	8	0.1	.	–	●° 0¹⁰ 2⁰⁵, ●²⁻⁰ 4²⁰, ▽° 6¹⁵⁻³⁰, ●° 10⁴⁵ 11²⁵, (☇) 2²⁰ 4²⁵ E-NW, = 6⁰⁰ 7⁴⁰ ≡° 10⁴⁵, ≫ 13⁴⁰ 19³⁰
Σ	–	63.8	–	–	UWAGI.

Sierpień – Août

1	6	1.6	.	–	▽° 2²⁰⁰ 5¹⁰, 8¹⁵ 10³⁶, ●° 14⁵⁰ 16²⁵ 17⁴⁰, 20⁴⁵ 21⁰⁵ 22⁴⁰, 23⁴⁸ 24
2	7	.	.	–	●° 0⁰⁰⁻¹⁰, = 20²⁵ 24, ⌓° 22⁰⁰ 24
3	6	.	.	–	= 0⁰⁰ 24, ⌓¹ 0⁰⁰ 8⁰⁰
4	8	0.7	.	–	= 0⁰⁰ 8⁰⁰
5	7	0.0	.	–	▽° 1⁴⁵ 3³⁰, ●° 5⁵⁰ 6⁴⁰, ●° 7²⁰, ≫ 12⁵⁵ 14⁵⁰
6	7	8.4	.	–	▽° 20²⁻²⁰, = 22²⁰ 24, ⌓¹ 23⁰⁰ 24
7	6	1.4	.	–	●°² 2⁵⁰ 4⁰⁵, ▽° 9⁴⁵ 13²⁰, 15¹⁰ 16²⁵, ●° 17⁰⁵ 20⁴⁰, ☇¹ 2⁴⁰ 4¹⁵ SW-NE, = 0⁰⁰ 14¹⁰
8	7	0.0	.	–	●° 23⁴⁵ 24
9	7	.	.	–	
10	8	0.7	.	–	⌓¹ 3⁰⁰ 8⁰⁰
11	7	3.9	.	–	●° 1⁴⁵ 2³⁰, ▽° 2³⁰ 4⁴⁵, ●° 14²⁸ 15⁵⁰, 16⁰⁰ 17¹⁵ 17²⁵ 21²⁰, ☇° 3¹⁰ 4⁴⁰ S-W
12	7	19.3	.	–	▽¹⁻⁰ 21⁰⁷ 23²⁵, ☇° 21⁰⁵ 23⁴⁰ N-S, = 4¹⁰ 9²⁰, 20³⁰ 24
13	8	.	.	–	●° 2⁰⁶ 6²⁵, = 0⁰⁰ 11²⁰
14	7	.	.	–	= 4³⁰ 8³⁰, ⌓¹ 2⁰⁰ 5⁰⁰
15	7	10.7	.	–	▽¹⁻⁰ 15⁰³⁻⁴⁰, ▽¹ 18⁴⁰ 19⁰⁵ ▲° 18⁴⁶⁻⁴⁸, 18⁵⁰⁻⁵¹ ▽° 19³⁵ 20⁰³, ☇° 15¹⁰⁻⁴⁵ S-N, 19⁵⁶ 20⁴² SW-NE, = 5¹⁵ 7³⁰ 21²⁰ 24
16	6	0.5	.	–	●° 0⁴⁵ 1³⁰ 12⁰², 14³⁵, = 0⁰⁰ 16³⁰ **[15.VIII: ⌓° 2⁰⁰ 8⁰⁰]**
17	7	0.0	.	–	●° 2⁰³ 3⁴⁵, ▽° 20⁴⁰ 21⁰³, = 3⁴⁵ 7¹⁵
18	7	0.4	.	–	▽⁰⁻¹ 16⁰²⁻²⁹, ▽° 17²⁶⁻³⁸, = 2³⁰ 3⁴⁰ ≡° 6⁴⁵ = 8³⁰, ≫ 18⁰⁵ 19⁰⁵
19	7	1.7	.	–	▽° 15⁴⁰ 22⁴⁵, ≫ 11³⁰ 15⁴⁵
20	7	3.8	.	–	●° 7²⁵ 12⁴⁰, ▽¹ 14¹⁰ 15⁵⁰, ≫ 13¹⁰⁻⁴⁰, = 3³⁰ 12³⁰
21	8	1.2	.	–	▽¹ 3³⁵ 4⁰⁵, ▽° 7⁰⁵⁻¹⁰, ●° 14⁴⁵ 16³⁰, ●° 19³⁵ 21⁰², ●° 21³⁰, ●° 24, ≫ 8²⁰ 14⁵⁰
22	6	6.7	.	–	●° 0⁰⁰⁻¹⁰, ▽° 16⁴⁰⁻⁵⁰, ▽¹ 17¹⁵ 18¹⁰, 18²⁰ 19²⁵, ☇° 17¹⁰⁻⁴⁵ W-E, = 3⁴⁰ 18²⁰
23	7	3.0	.	–	▽⁰⁻² 11⁵⁵ 17²⁵, ●° 17⁵⁰ 20⁴⁰, = 4¹⁰ 13¹⁵
24	8	3.1	.	–	▽° 12⁰⁻⁴⁵ 13⁵², 14¹⁰, ▽¹ 14²⁷⁻⁵⁰, ▽° 16²⁵⁻⁴⁰, = 2⁰⁰ 5⁰⁰
25	6	1.2	.	–	●° 6⁰⁰ 8³⁵, ▽¹ 9⁴⁰ 11¹⁰, ●° 14⁴⁰, ⌓¹ 23⁰⁰ 24
26	8	0.0	.	–	⌓¹ 0⁰⁰ 8⁰⁰
27	6	1.1	.	–	●¹⁻⁰ 5⁴⁵ 8²⁰, ▽° 20⁴⁰ 21⁰⁵, ☇° 20⁴⁷ 21¹⁰ W-E, = 4³⁰ 6⁵⁰ ≡¹ 9⁴⁰ = 14²⁵, np
28	7	0.1	.	–	▽° 19⁴⁰⁻⁵⁰ 22¹⁵ 23¹⁵, ●° 24, = 0⁰⁰ 7³⁰, ≫ 10¹⁰ 15⁵⁰
29	8	.	.	–	●° 0⁰⁰ 1¹⁰
30	8	.	.	–	⌓¹ 0⁰⁰ 10⁰⁰, 22⁰⁰ 24, ▽ 3³⁰ 4¹⁰
31	8	.	.	–	⌓¹ 0⁰⁰ 8⁰⁰
Σ	–	69.5	–	–	UWAGI.

Suwałki $\varphi = 54°06'$ $\lambda = 22°57'$ Wrzesień - Septembre 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			POGODA			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	107.9	106.8	104.1	106.3	13.5	23.6	16.3	17.4	25.1	10.5	97	56	93	82	0.6	12.9	1.3	4.9	4 ○	7 ⊙	0	W 3	NW 2	C 0
2	101.1	98.4	96.0	98.5	14.5	26.0	17.1	18.7	27.0	11.8	94	45	87	75	0.9	18.5	2.6	7.5	6 ○	5 ⊙	0	W 1	S 6	W 1
3	92.8	90.9	89.3	91.0	14.9	26.6	17.7	19.2	27.8	11.0	90	47	79	72	1.6	18.4	4.2	8.1	2 ○	0 ⊙	0	W 1	SW 2	C 0
4	90.2	95.0	94.8	92.7	12.3	16.8	9.1	11.8	17.8	9.0	94	60	83	79	0.9	7.7	2.0	3.5	10	5 ⊙	0	N 5	N 5	C 0
5	95.1	95.7	94.6	95.1	11.1	16.5	12.5	13.2	17.3	7.7	83	47	64	65	2.3	10.0	5.2	5.8	7 ○	7 ⊙	10	NW 3	E 3	E 3
6	88.6	87.3	85.3	87.1	13.7	14.7	15.7	15.0	17.0	10.3	76	98	98	91	3.7	0.4	0.4	1.5	9	10 •	10 •	SE 6	E 4	ESE 1
7	84.3	84.6	82.7	83.9	16.3	19.9	15.9	17.0	20.0	15.1	99	67	88	85	0.2	7.7	2.1	3.3	10	10	10	SW 4	SW 6	SW 8
8	79.7	81.3	81.8	80.9	9.7	12.7	11.9	11.6	16.1	9.1	93	81	93	89	0.8	2.8	1.0	1.5	10 •	10	10 •	SW 10	SW 9	SW 6
9	87.0	88.8	90.0	88.6	12.4	15.5	12.5	13.2	16.9	11.3	90	73	83	82	1.4	4.8	2.4	2.9	10	9 ⊙	0	W 3	W 6	W 5
10	92.7	93.4	93.8	93.3	8.8	14.7	9.5	10.6	15.5	6.8	90	67	86	81	1.1	5.5	1.7	2.8	2 ○	7 ⊙	0	W 3	WNW 6	W 2
11	93.6	93.4	92.8	93.3	7.9	13.3	12.5	11.6	14.4	6.3	100	78	92	90	0.0	3.3	1.2	1.5	10 ≡	10	10	SW 4	SW 5	SW 4
12	91.1	90.6	89.2	90.3	11.9	16.6	13.2	13.7	17.9	11.3	91	54	86	77	1.2	8.7	2.1	4.0	9	10	10 •	SW 3	SW 10	W 4
13	89.0	90.8	94.2	91.3	11.4	14.5	9.1	11.0	15.6	9.0	90	63	91	81	1.4	6.2	1.1	2.9	9	9	0	SW 6	W 9	W 1
14	93.3	92.1	88.2	91.2	9.6	14.6	12.9	12.5	15.0	7.9	97	92	100	96	0.4	1.3	0.0	0.6	9	10 •	10	SW 1	S 3	SE 2
15	85.3	90.0	95.7	90.3	13.3	14.9	11.3	12.7	16.9	11.3	96	79	89	88	0.6	3.4	1.5	1.8	10 •	10	0	SW 4	WNW 7	W 3
16	97.3	98.4	100.2	98.6	12.1	16.9	14.7	14.6	18.0	10.3	94	89	87	90	0.8	2.1	2.2	1.7	10	10 ●	0	SW 2	SW 4	WSW 2
17	101.4	100.4	99.6	100.5	12.5	24.6	18.1	18.3	25.7	11.8	100	64	87	84	0.0	11.2	2.7	4.6	10 ≡	0 ⊙	0	C 0	SW 7	SW 3
18	96.4	94.6	97.7	96.2	14.6	24.9	12.5	16.1	25.4	12.5	94	65	83	81	0.9	11.1	2.4	4.8	8 ⊙	3 ⊙	0	SW 3	W 4	W 5
19	98.5	99.4	101.3	99.7	11.1	17.1	9.9	12.0	17.5	9.8	96	58	91	82	0.5	8.1	1.1	3.2	3 ⊙	7	2	NW 5	NW 6	NW 3
20	104.6	105.4	105.7	105.2	8.7	15.2	9.1	10.5	15.6	6.1	96	54	85	78	0.4	8.0	1.8	3.4	6 ⊙	9	9	N 3	NE 5	N 2
21	107.6	108.3	108.6	108.2	6.5	12.9	6.3	8.0	13.3	3.3	88	54	84	75	1.2	6.8	1.5	3.2	0 ⊙	0 ⊙	0	E 3	NE 5	NE 2
22	110.8	111.2	110.8	110.9	4.1	13.7	6.3	7.6	14.8	1.7	92	55	92	80	0.7	7.0	0.7	2.8	0	1 ⊙	1	C 0	E 2	C 0
23	111.1	109.8	107.9	109.6	4.3	16.5	5.7	8.0	17.5	1.4	93	40	89	74	0.5	11.4	1.0	4.3	4 ⊙	2 ⊙	2	C 0	ESE 1	C 0
24	106.8	105.8	104.1	105.6	4.7	16.8	6.9	8.8	17.6	0.4	85	36	81	67	1.2	12.2	1.8	5.1	0 ⊙	0 ⊙	0	C 0	SE 3	C 0
25	101.3	99.4	97.7	99.5	5.2	18.0	10.1	10.8	19.1	3.4	87	48	91	75	1.1	10.7	1.2	4.3	1 ⊙	1 ⊙	10	SE 1	S 5	C 0
26	98.3	99.4	99.1	98.9	9.9	15.5	10.7	11.7	15.6	9.3	95	62	84	80	0.6	6.7	2.1	3.1	10 •	8 ⊙	9	W 3	W 5	WSW 2
27	98.2	98.2	98.7	98.4	10.4	15.5	7.5	10.2	16.3	7.4	95	56	90	80	0.6	7.7	1.1	3.1	10	7 ⊙	3	WNW 2	N 5	C 0
28	100.7	102.1	103.6	102.1	4.3	16.2	9.0	9.6	16.6	2.4	98	54	88	80	0.1	8.4	1.4	3.3	0 ⊙	5 ⊙	0	C 0	C 0	C 0
29	104.6	105.0	104.9	104.8	6.7	10.1	4.9	6.6	11.2	4.9	100	96	98	98	0.0	0.5	0.2	0.2	10 ≡	10	0	C 0	E 5	C 0
30	104.7	104.2	104.9	104.6	4.1	13.9	7.9	8.4	14.3	2.5	100	65	93	86	0.0	5.6	0.7	2.1	10 ≡	4 ⊙	0	C 0	E 6	E 3
31																								
M	97.1	97.3	97.2	97.2	10.0	17.0	11.2	12.4	18.0	7.9	93	63	88	81	0.9	7.6	1.7	3.4	6.6	6.2	3.5	2.6	4.8	2.1

Październik - Octobre

1	105.1	106.5	108.5	106.7	6.1	10.5	8.9	8.6	13.3	5.1	100	96	93	96	0.0	0.5	0.8	0.4	10 ≡	10	0	NE 4	E 4	NE 3
2	110.0	111.4	111.8	111.1	7.7	13.9	9.9	10.4	14.8	6.3	100	80	96	92	0.0	3.2	0.5	1.2	10 ≡	3 ⊙	0	ENE 2	ENE 5	ENE 3
3	112.5	113.1	112.3	112.6	6.9	14.5	9.9	10.3	16.6	6.2	100	77	82	86	0.0	3.8	2.2	2.0	10 ≡	1 ⊙	0	ENE 3	E 4	ENE 3
4	112.6	112.3	111.5	112.1	6.6	17.7	9.0	10.6	17.9	5.7	98	54	92	81	0.1	9.3	1.0	3.5	0 ⊙	1 ⊙	0	ENE 2	ESE 6	ESE 2
5	110.9	110.3	109.9	110.4	4.7	16.1	7.3	8.8	16.3	4.0	95	53	90	79	0.4	8.6	1.0	3.3	0	2 ⊙	0	E 1	SE 5	ESE 3
6	109.2	108.2	106.0	107.8	4.7	14.8	8.7	9.2	15.3	3.3	98	63	85	82	0.1	6.2	1.6	2.6	5 ⊙	0 ⊙	0	SE 5	SE 7	ESE 4
7	104.6	102.1	100.6	102.4	5.7	14.7	8.3	9.2	14.9	5.1	89	44	65	66	1.0	9.3	3.9	4.7	1 ⊙	5 ⊙	0	ESE 7	SE 10	SE 6
8	99.2	97.5	98.9	98.5	5.1	14.0	8.0	8.8	14.2	5.0	80	43	70	64	1.8	9.1	3.2	4.7	5	6 ⊙	0	ESE 7	SE 12	SE 5
9	101.0	103.5	106.7	103.7	6.5	13.2	10.1	10.0	13.6	5.4	87	64	93	81	1.3	5.5	0.8	2.5	9	7	10	SE 6	SE 4	SE 1
10	109.2	110.8	110.7	110.2	6.8	14.1	8.9	9.7	15.3	6.6	100	78	100	93	0.0	3.6	0.0	1.2	10 ≡	9 ⊙	10 ≡	C 0	WSW 2	WSW 2
11	110.3	109.5	106.8	108.9	8.1	13.9	8.1	9.6	15.6	6.8	100	74	85	86	0.0	4.1	1.6	1.9	10 ≡	5 ⊙	0	SSW 2	SSW 4	S 3
12	105.6	105.8	104.5	104.0	5.0	11.9	7.1	7.8	13.8	4.4	69	65	96	77	2.7	4.9	0.5	2.7	8 ⊙	5 ⊙	0	S 3	SW 4	W 1
13	102.5	103.0	103.6	103.0	7.9	12.9	7.5	9.0	13.7	4.2	99	62	93	85	0.1	5.7	0.8	2.2	10	6	0	W 4	W 5	WSW 2
14	100.8	99.8	100.2	100.3	6.1	9.8	8.8	8.4	11.2	5.1	100	91	93	95	0.0	1.1	0.8	0.6	10 ≡	10	6	SW 3	WNW 2	WNW 3
15	99.3	96.4	93.8	96.5	7.9	11.5	11.1	10.4	11.8	4.9	100	91	86	92	0.0	1.2	1.8	1.0	10 •	10	10 •	WSW 2	WSW 7	WSW 7
16	94.9	95.4	94.0	94.8	7.9	13.3	9.9	10.2	13.9	7.9	99	68	89	85	0.1	5.0	1.3	2.1	6	9	10	W 1	WSW 5	SW 4
17	90.1	87.6	83.2	87.0	7.1	10.1	7.5	8.0	10.3	6.9	93	85	99	92	0.8	2.1	0.2	1.0	10	10	10	S 3	S 5	S 2
18	78.3	78.5	81.3	79.4	10.1	14.4	11.8	12.0	14.8	7.4	78	66	77	74	2.7	5.6	3.1	3.8	8	10	10	SE 8	SE 10	SE 10
19	85.5	85.2	88.7	85.8	10.1	15.9	13.3	13.2	16.6	10.1	93	64	79	79	0.8	6.5	3.2	3.5	9	8 ⊙	4	SE 13	SE 10	SE 9
20	92.3	94.9	96.8	94.7	9.9	12.9	11.3	11.4	13.5	9.7	96	87	89	91	0.5	1.9	1.5	1.3	9	10	10	ESE 6	SE 8	ESE 5
21	98.9	99.8	102.6	100.4	6.9	10.1	8.3	8.4	11.8	6.8	90	73	79	81	1.0	3.4	2.3	2.2	4	6	9	ESE 10	ESE 10	ESE 8
22	105.2	107.4	110.1	107.6	6.9	11.9	5.9	7.6	12.3	5.7	78	59	80	72	2.2	5.7	1.9	3.3	10	6 ⊙	0	SE 6	SE 10	SE 5
23	110.4	108.8	107.8	109.0	0.0	9.4	3.7	4.2	9.8	−0.8	84	42	62	63	1.0	6.9	3.1	3.7	2 ○	4 ⊙	0	SE 6	SE 11	SE 7
24	104.6	103.3	102.0	103.3	3.3	6.6	9.3	7.1	9.8	1.6	71	85	83	80	2.2	1.4	2.0	1.9	10	10	10	SSE 6	SSE 3	S 4
25	99.3	96.8	95.4	97.2	4.9	12.3	11.3	10.0	13.8	4.8	94	62	67	74	0.6	5.4	4.4	3.5	3 ⊙	8	10 •	S 3	S 6	SSW 7
26	95.3	95.3	95.3	95.4	9.5	9.7	9.1	9.4	11.5	8.8	88	92	85	88	1.4	0.9	1.8	1.4	10 •	10 •	9	SSW 3	S 5	S 4
27	94.3	93.8	92.5	93.5	6.7	15.5	6.0	8.6	15.9	5.1	90	62	85	79	1.0	6.7	1.5	3.1	9	9	4	S 2	S 6	S 2
28	92.2	92.6	92.0	92.3	4.2	10.5	4.7	6.0	12.7	3.5	90	71	93	85	0.8	3.7	0.4	1.6	9	8 ⊙	0	C 0	S 2	C 0
29	91.9	91.2	91.1	91.4	3.7	4.8	5.5	4.9	5.7	1.8	100	100	98	99	0.0	0.0	0.1	0.0	10 ≡	10 ≡	10 •	S 3	S 6	S 2
30	93.3	93.0	96.0	94.8	7.1	7.9	7.4	7.4	8.8	5.5	99	96	96	97	0.2	0.4	0.5	0.4	10	10	10	WSW 3	WSW 3	WSW 3
31	96.6	94.9	90.2	93.9	6.3	8.2	8.6	7.9	8.7	6.2	97	87	85	90	0.2	1.4	1.7	1.1	10	9	10	SSW 3	SSW 3	SW 10
M	100.4	100.3	100.2	100.3	6.5	12.2	8.6	9.0	13.2	5.5	92	72	86	85	0.7	4.3	1.6	2.2	7.6	7.0	4.9	4.1	6.0	4.3

Suwałki $H_s = 165\ m$ $H_b = 169{,}6\ m$ $h_w = 13\ m$ **Wrzesień – Septembre 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌒ 0⁰⁰–9⁰⁰ ⌒ 1 21⁰⁰–24
2	7	.	.	–	= 20³⁰–24; ⌒ 0⁰⁰–10⁰⁰ ⌒ 1 21⁰⁰–24
3	7	.	.	–	= 0⁰⁰–9³⁰; ⌒ 1 0⁰⁰–8⁰⁰
4	8	.	.	–	= 6¹⁰–7⁵⁰ ⌒ 1 21⁰⁰–24
5	8	.	.	–	⌒ 0 0⁰⁰–9⁰⁰
6	5	20.7	.	–	▽ 0-2 7⁵⁶ 15⁴⁰ • 16⁴⁰ 22¹⁰; ↙ 0 10¹⁰–12⁴⁰ S–N 13²² 14¹⁰ W-E; = 14⁰⁶–24
7	7	3.0	.	–	• 1²⁰–5²⁵ 15¹⁰ 16⁰² • ▽ 17²⁰–27 • 0-1 18³⁵ 20⁴⁵; (↙) 0 16⁰⁴–⁴⁵; =, ≡ 1 0⁰⁰–13²⁰ = p–np
8	7	4.5	.	–	• 0 7⁰³–9³⁸; 15⁴⁵ 20¹⁰ 21¹⁵ 24; » 4¹⁰–13⁵⁰
9	8	0.0	.	–	• 0 0⁰⁰–¹⁰; 4⁴⁰–5⁴⁵ ▽ 0 17⁴⁰–⁵²
10	8	.	.	–	⌒ 0 3⁰⁰–10⁰⁰ 22⁰⁰–24
11	7	0.2	.	–	• ▽ 0 12¹⁰–¹³; 12²³–²⁸; ≡ 0 6³⁵–8⁴⁸ = –9⁴⁵ ⌒ 1 0⁰⁰–6⁰⁰
12	7	0.2	.	–	• 0 20⁴⁰–22⁴⁵; = 2⁰⁰–13²⁰; » 12¹⁰–13⁵⁶
13	8	2.6	.	–	• 0 3²⁵–⁴⁰ ▽ 1 10²⁰–⁵⁰ 13⁴³–⁵⁰
14	6	14.2	.	–	• 0 5²⁵–6⁵⁰ • 0-1 11⁴⁰–18³⁰ • 0 21²⁰–; = 3³⁰–8³⁰, 11³⁵–23³⁵ ≡ 0 –24; ⌒ 0 rsa
15	7	2.6	.	–	• 0-1 0²⁰ 13²⁸; ≡ 0 0⁰⁰–2³⁰ = –6⁰⁰ » 10²⁰–11³⁵ 12¹⁵–16⁵⁰
16	6	0.0	.	–	• 0 6¹⁵ 7²³ 9⁴⁵–10¹⁵ • 0 11⁵⁷ 13¹⁵–14⁵⁵, 16⁰⁵–18¹⁰; = 18¹⁰–24
17	7	.	.	–	= 0⁰⁰–1⁴⁵ ≡ 1-2 8⁴⁰ = –10³⁵ 19³⁰–24; ⌒ 0 21⁰⁰–24
18	6	.	.	–	= 0⁰⁰–16³⁰; ⌒ 0 0⁰⁰–10⁰⁰; 22⁰⁰–24
19	7	.	.	–	» 15⁴⁵–17²⁰; ⌒ 0 0⁰⁰–9⁰⁰ ⌒ 1 np
20	8	.	.	–	⌒ 1 0⁰⁰–9⁰⁰
21	8	.	.	–	⌒ 0 2⁰⁰–9⁰⁰
22	8	.	.	–	⌒ 1 20⁰⁰–24; ⌴ 0 0⁰⁰–9⁰⁰
23	7	.	.	–	= 3²⁰–8³⁰; ⌒ 1 0⁰⁰–3⁰⁰ ⌴ 0 8⁰⁰–⌒ 0 np
24	8	.	.	–	= 0³⁰–8¹⁰; ⌒ 0 0⁰⁰–3⁰⁰ ⌴ 0 7⁰⁰–⌒ 0 20⁰⁰–24
25	7	0.1	.	–	• 0 22²⁵–23¹⁰ 24; = 19⁴⁰–24, ⌒ 0 0⁰⁰–3⁰⁰ ⌴ 0 –8⁰⁰
26	7	0.0	.	–	• 0 0⁰⁰–²⁵ 7⁰¹ 9³⁵ = 0⁰⁰–6³⁰
27	7	.	.	–	= 4²⁰–8³⁰; 22⁴⁵–24; ⌒ 17¹⁵–⁵⁸
28	8	.	.	–	= 0⁰⁰–⁴⁵ ≡ 0 2⁴⁰ = –11²⁰; ⌒ 1 0⁰⁰–5⁰⁰ ⌴ 1 5⁰⁰–7⁰⁰
29	5	.	.	–	= 2⁰⁰–3⁴⁵ ≡ 1 12⁴⁵ = –22⁴⁰ ≡ 1 –24; ⌴ 0 2⁰⁰–5⁰⁰
30	6	.	.	–	≡ 1-0 0⁰⁰–4⁴⁵ = –7⁰⁵ ≡ 2 11²⁰ = –14³⁵; 18³⁰–24; ⌴ 0 3⁰⁰–8⁰⁰
31					
Σ	–	48.1	–	–	UWAGI.

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1	6	.	.	–	= 1⁰⁰–3⁴⁰ ≡ 1 8⁴⁵ = –19³⁰; ⌒ 1 1⁰⁰–3⁰⁰
2	7	.	.	–	= 0³⁰–5¹⁵ ≡ 0-1 10⁴⁵ = –12²⁰ 21¹⁵–⁵⁰ ≡ 1 –24; ⌒ 1 1⁰⁰–10⁰⁰
3	7	.	.	–	≡ 1 0⁰⁰–10⁴⁵ = –11³⁰; ⌒ 1 0⁰⁰–9⁰⁰
4	7	.	.	–	= 1⁰⁰–10³⁰; 21²⁰–23³⁰; ⌒ 0 1⁰⁰–10⁰⁰; np
5	7	.	.	–	= 5²⁵–9⁰⁰; ⌒ 1 0⁰⁰–9³⁰
6	7	.	.	–	= 4¹⁵–9³⁰ ⌒ 1 10⁰⁰–9⁰⁰
7	8	.	.	–	= 6³⁰–8³⁰; » 7⁴⁵–15⁴⁵; ⌒ 0 10⁰⁰–7⁰⁰
8	7	.	.	–	» 9³⁰–16⁴⁰
9	7	0.0	.	–	• 0 18³⁵ 19³² = 5³⁰–12³⁰
10	7	.	.	–	• 0 1⁰²–⁰⁷; = 3²⁵–4⁴⁰ ≡ 1-0 9⁵⁰ = –10³⁰; 16²⁰–17⁴⁵ ≡ 2 –24
11	6	.	.	–	≡ 2-1 0⁰⁰–8⁴⁵ = –13³⁰; 14³⁰–24
12	7	.	.	–	= 0⁰⁰–3¹⁰ 14³⁵–18³⁰; 20²⁰–24; ⌒ 1 20⁰⁰–24
13	8	.	.	–	= 0⁰⁰–9³⁰; ⌒ 1 0⁰⁰–8⁰⁰ ⌒ 0 np
14	7	0.2	.	–	• ▽ 0 8³⁰–⁵⁰ • 0 9²⁵ 11⁵⁰ • ▽ 0 12⁴⁰–13⁵⁵ ≡ 0-1 0⁴⁵–8²⁵; ⌒ 1 0⁰⁰–3⁰⁰
15	7	0.2	.	–	• ▽ 0 4⁴⁰–5²⁵ • 0 7¹⁵ • 1–8⁴⁰ • 0 9⁴⁵ 11⁴⁰–17²⁰–18³⁰–20³⁰–21⁴⁵; = 2³⁰–12¹⁵
16	6	.	.	–	= 5⁴⁵–13⁴⁰
17	5	.	.	–	= 5³⁰–24
18	7	0.0	.	–	• 0 10³⁵–12¹⁵ 13⁴⁵–14¹⁵; = 0⁰⁰–5³⁰, » 7⁰⁵–8⁴⁵, 11²⁰–13⁵⁰, 17¹⁵–20⁴⁵
19	7	.	.	–	» 1²⁰–17³⁰, 20¹⁰–22⁴⁰
20	6	.	.	–	= 5³⁰–22³⁰; » 9⁰⁵–10³⁵, 13¹⁵–⁵⁰ 16²⁰–17⁴⁰
21	6	.	.	–	= 6²⁰–22¹⁰; » 6¹⁰–11³⁵, 11⁵⁸–13⁵⁵, 14²⁵–15⁵⁰
22	7	.	.	–	» 10²⁰–13⁵⁰
23	7	.	.	–	= 5¹⁰–9²⁰; » 10¹⁰–16⁴⁵; ⌴ 0 4⁰⁰–9⁰⁰
24	7	0.0	.	–	• ▽ 0 11²⁵–12³⁰; = 12⁴⁰–24
25	7	0.4	.	–	• 0 20²⁵–³⁵ = 0⁰⁰–8³⁵ ⌒ 0 5⁰⁰–8⁰⁰
26	6	3.1	.	–	• 0 6⁰⁵–17²⁰ 18¹⁵ 23⁵⁰ 24; = 5³⁰–24
27	7	.	.	–	• 0 0⁰⁰–¹⁴⁵; = 0⁰⁰–8³⁰
28	7	.	.	–	= 18³⁰–24; ⌒ 1 19⁰⁰–24
29	3	2.0	.	–	• 0 14²⁵–19³⁵ • 0 19⁵⁵–24; = 0⁰⁰–5³⁵ ≡ 0-1 19⁴⁵ = –24; ⌒ 0 0⁰⁰–14³⁵
30	6	.	.	–	• 0 0⁰⁰–12⁵; = 0⁰⁰–24
31	6	0.6	.	–	▽ • 0 17⁰⁵–¹⁵; 23¹⁵–24; = 0⁰⁰–22⁰⁰; » 17²⁰–22³⁰
Σ	–	6.5	–	–	UWAGI.

Suwałki — φ = 54°06' — λ = 22°57' — Listopad - Novembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N.w			OPADY D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.4	92.8	92.3	92.2	6.7	7.9	8.7	8.0	9.7	6.5	81	96	96	91	1.9	0.4	0.4	0.9	7	10 ●	10	SSW 6	SW 5	WSW 8
2	97.4	98.6	95.5	97.2	6.5	9.9	6.9	7.6	10.6	6.4	93	76	90	86	0.7	3.0	1.0	1.6	5 ⊙	8 ⊙	0	WSW 4	WSW 5	S 6
3	87.9	85.0	85.1	86.0	5.3	9.9	8.1	7.8	10.1	4.8	95	76	82	84	0.4	3.0	2.0	1.8	9	10	0	SSW 6	SSW 8	SSW 7
4	86.5	88.6	92.0	89.0	6.4	8.6	4.9	6.2	8.8	4.8	91	72	81	81	0.9	3.2	1.7	1.9	10	9 ⊙	10 ●	SSW 6	SSW 5	C 0
5	92.9	93.0	94.9	93.6	2.7	4.3	7.9	5.7	8.2	1.9	98	98	99	98	0.1	0.1	0.1	0.1	10	10 ●	10 ●	NE 4	NE 5	E 4
6	97.8	98.5	98.9	98.4	7.3	8.5	8.5	8.2	8.8	7.0	99	99	95	97	0.1	0.2	0.8	0.4	10	10	10	E 2	E 4	E 5
7	96.4	95.1	93.9	95.1	6.1	4.9	7.1	6.3	8.7	4.7	95	98	90	94	0.4	0.2	1.0	0.5	10	10 ●	10	E 7	E 6	SE 7
8	95.1	91.9	90.2	91.7	4.7	5.7	4.1	4.6	7.2	4.1	95	98	98	97	0.4	0.2	0.2	0.3	10	10	10 ●	SE 7	SE 6	SE 5
9	88.6	90.1	89.8	89.5	5.5	6.3	6.3	6.2	6.6	4.1	97	84	93	91	0.3	1.5	0.7	0.8	10 ●	10	10	SSE 5	SSE 3	SSE 5
10	90.1	89.1	89.0	89.4	5.9	8.1	7.9	7.4	8.4	5.8	95	87	99	94	0.5	1.4	0.1	0.7	10	10	10 ●	SE 5	SE 8	SE 7
11	89.7	92.0	95.7	92.5	7.7	7.1	5.7	6.6	8.2	5.7	96	96	92	95	0.5	0.5	0.8	0.6	10 ●	10 ●	10 ●	SE 8	SE 10	ESE 11
12	98.0	99.3	101.4	99.6	2.3	1.6	0.3	1.1	5.8	0.2	89	85	90	88	0.8	1.1	0.6	0.8	10	10	10	E 8	E 12	E 8
13	101.7	100.0	98.0	99.9	-1.5	-2.1	-3.1	-2.4	0.3	-3.2	86	87	90	88	0.8	0.6	0.5	0.6	10	10	10	ESE 9	E 9	ENE 8
14	92.7	92.4	96.1	93.7	-2.6	-2.1	-2.7	-2.5	-1.9	-3.4	93	87	91	90	0.3	0.6	0.5	0.5	10 ●	10	10	ENE 5	NNE 9	N 7
15	97.4	96.4	94.5	96.1	-3.9	-2.6	-0.1	-1.7	0.1	-4.1	94	98	92	95	0.3	0.1	0.5	0.3	10	10	10	NNW 3	WSW 2	WSW 5
16	95.6	92.3	88.9	91.6	1.4	2.1	1.5	1.6	2.2	-0.2	98	98	98	98	0.2	0.1	0.1	0.1	10 ●	10	10 ●	SW 4	SW 5	SW 6
17	85.4	81.9	85.0	85.4	2.2	5.5	-0.3	1.8	6.6	-0.5	95	94	90	92	0.6	0.5	0.6	0.6	10 ●	10 ●	0	SW 8	WNW 7	SW 5
18	81.7	79.1	83.8	81.5	-0.9	1.5	0.7	0.5	1.9	-1.4	93	91	94	93	0.4	0.6	0.4	0.5	5	10 ✱	9	SW 5	WSW 8	WNW 4
19	87.5	92.8	100.6	93.6	0.4	-1.3	-1.4	-0.9	0.8	-2.4	98	74	86	86	0.1	1.4	0.8	0.8	10 ✱	10 ✱	10	NW 5	NNW 7	NNW 4
20	107.0	110.7	111.6	109.8	-1.7	-1.6	-3.3	-2.5	-0.9	-5.1	92	82	88	87	0.4	1.0	0.6	0.7	10	3 ⊙	9	N 3	NNW 4	SW 3
21	106.3	103.8	101.4	103.8	-0.3	2.1	2.3	1.6	2.6	-3.5	90	87	91	89	0.6	0.9	0.6	0.7	9	10	10	WSW 4	W 8	W 5
22	99.6	99.1	98.1	98.9	2.2	3.9	3.1	3.1	4.3	1.7	93	92	88	91	0.6	0.7	0.9	0.7	10	10	10	W 4	WSW 5	WSW 2
23	97.0	96.2	95.2	96.1	1.9	1.3	-3.6	-1.0	3.2	-3.6	87	77	94	86	0.9	1.5	0.3	0.9	10	9	0	WSW 3	SW 3	C 0
24	94.3	94.7	93.9	93.0	-3.3	-0.6	-0.6	-1.8	0.0	-6.6	97	87	93	93	0.1	0.7	0.3	0.4	7	4 ⊙	10	C 0	S 2	SW 3
25	96.3	93.7	92.4	94.3	-2.4	0.3	1.3	0.2	1.3	-2.8	100	100	98	99	0.0	0.0	0.1	0.0	10 ≡	10 ≡	10 ●	C 0	C 0	SW 3
26	91.6	91.2	89.9	90.9	-0.3	0.9	1.1	0.6	1.3	-0.6	100	98	100	99	0.0	0.1	0.0	0.0	10 ≡	10	10 ≡	C 0	SW 2	C 0
27	85.8	84.1	82.6	84.2	1.9	2.3	1.9	2.0	2.4	0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ●≡	SW 2	C 0	C 0
28	85.2	88.8	94.6	89.5	1.1	3.9	-1.1	0.7	3.1	-1.4	100	78	94	91	0.0	1.8	0.3	0.7	10 ≡	5 ⊙	0	WNW 2	WNW 3	SW 1
29	97.0	96.5	93.9	95.8	-3.0	-1.1	-1.1	-2.1	-0.6	-3.9	95	95	95	94	0.2	0.4	0.3	0.3	0	5 ⊙	10	C 0	S 6	S 6
30	85.1	82.1	78.1	81.8	1.9	2.3	2.7	2.4	3.1	-1.2	98	91	98	96	0.1	0.6	0.1	0.3	10	10	10 ●	S 7	SW 7	SW 9
31																								
M	95.1	95.1	95.3	95.2	1.9	3.3	2.5	2.6	4.4	0.4	94	89	93	92	0.4	0.9	0.5	0.6	9.1	9.1	8.3	4.4	5.5	4.7

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1	65.8	68.5	73.8	69.4	5.3	5.4	2.4	3.9	7.5	2.3	95	80	91	89	0.4	1.8	0.7	1.0	10 ●	9	0	SW 12	SW 10	SW 6
2	74.5	68.1	67.6	70.1	2.8	6.5	7.9	6.3	10.0	1.9	93	97	64	85	0.6	0.3	3.8	1.6	10	10 ●	4	SW 4	SW 8	SW 12
3	81.0	84.1	86.5	83.9	2.8	4.3	0.6	2.1	7.9	0.5	81	63	88	77	1.5	3.1	0.8	1.8	7	7 ⊙	0	W 10	SW 10	S 5
4	83.0	83.9	90.3	85.7	-0.5	1.5	-0.2	0.2	2.1	-0.8	94	91	94	93	0.4	0.6	0.4	0.5	7	10	0	S 4	S 5	SW 4
5	84.0	81.7	81.8	82.5	1.1	10.9	9.9	8.0	11.4	-1.3	98	94	89	94	0.1	0.8	1.3	0.7	10 ●	10 ●	4	SE 7	SW 10	SW 8
6	84.4	86.7	89.4	86.8	6.1	3.9	1.5	3.2	10.0	1.4	53	59	72	61	4.4	3.3	1.9	3.2	10	9	6	W 10	SW 8	SW 6
7	90.9	91.7	93.2	91.9	-1.5	0.1	-0.5	-0.6	1.6	-2.0	92	94	96	94	0.4	0.4	0.3	0.4	7	10	10	SW 2	WSW 1	SW 2
8	94.7	94.3	93.9	94.3	-2.0	-0.5	-0.7	-1.0	0.1	-2.6	89	78	85	84	0.6	1.3	0.9	0.9	10	9	9	WSW 3	SW 4	SW 5
9	93.3	96.3	98.3	96.0	-0.5	0.7	-3.1	-1.3	1.4	-3.4	86	83	93	88	0.9	1.1	0.3	0.8	10	4 ⊙	0	WSW 6	SW 3	C 0
10	96.9	93.7	90.8	93.8	-3.1	-2.1	-1.9	-2.2	-1.3	-4.6	93	87	90	91	0.3	0.6	0.5	0.5	10	10	10	S 4	SE 8	S 5
11	86.1	81.9	77.2	81.7	-0.7	-0.1	0.2	-0.1	0.4	-1.9	97	98	94	96	0.2	0.2	0.4	0.3	10	10 9	10 ✱	S 5	S 3	SE 3
12	82.0	86.8	93.1	87.3	-0.3	-3.7	-3.1	-3.6	0.4	-3.1	96	94	83	91	0.3	0.3	0.7	0.4	10	10 ✱	10	NE 5	NE 8	NE 8
13	98.8	103.2	107.3	103.1	-7.7	-6.1	-8.3	-7.6	-5.0	-8.8	84	81	83	83	0.5	0.7	0.5	0.6	6	6 ⊙	0	NW 4	N 9	N 6
14	106.1	104.3	102.4	104.3	-11.0	-9.8	-11.1	-10.8	-8.3	-11.5	83	72	69	75	0.4	0.8	0.8	0.7	1	3 ⊙	1	N 8	N 10	N 10
15	99.3	102.1	103.3	103.6	-12.0	-12.5	-12.7	-12.5	-11.1	-13.1	85	81	77	81	0.4	0.4	0.3	0.4	10 ✱	10 ↔	0	N 7	NE 7	ENE 6
16	116.5	120.3	123.3	120.1	-16.3	-13.3	-11.7	-13.2	-11.5	-17.6	90	84	93	89	0.2	0.4	0.2	0.3	0	0 ⊙	10	NE 1	ENE 1	C 0
17	121.8	120.0	118.2	120.0	-9.1	-4.8	-3.9	-5.4	-3.7	-11.9	70	86	89	82	0.9	0.6	0.5	0.7	10	10 ✱	10	WSW 3	NW 4	NW 2
18	114.6	112.1	109.0	111.9	-2.6	-1.4	-0.6	-1.3	-0.2	-4.1	93	94	97	95	0.3	0.3	0.2	0.3	10	10 ✱	10 9	W 4	SW 2	W 3
19	104.2	103.1	102.9	103.4	1.1	1.9	-0.1	0.7	2.3	-0.6	98	91	90	93	0.1	0.6	0.7	0.5	10 9	10	4	W 5	NW 6	NW 4
20	95.1	86.3	86.9	89.5	0.3	0.7	-1.1	-0.3	2.0	-1.3	90	98	85	91	0.6	0.1	0.9	0.5	10	10 ✱	8	SW 4	W 7	N 7
21	81.5	85.9	88.5	85.3	-4.1	-4.9	-7.3	-6.0	-0.9	-7.3	98	69	84	84	0.1	1.3	0.3	0.6	10 ✱	1 ⊙	0	NW 9	NW 8	NW 5
22	83.2	82.9	86.3	84.1	-5.4	-8.3	-12.3	-9.6	-5.1	-15.2	90	77	93	87	0.4	0.7	0.2	0.4	10 ✱	2 ⊙	9	W 4	NW 1	NW 2
23	89.0	90.0	92.3	90.4	-10.8	-8.7	-13.7	-11.7	-8.4	-14.1	94	83	92	90	0.2	0.5	0.2	0.3	10	9 ↔	0	W 1	W 3	WNW 2
24	93.5	93.8	92.9	93.4	-11.9	-8.7	-8.7	-9.5	-7.7	-17.0	93	77	89	86	0.2	0.7	0.4	0.4	10	3 ⊙	10	SW 4	SW 4	SW 7
25	91.0	90.4	91.0	90.8	-10.5	-10.5	-14.1	-12.3	-7.9	-14.2	87	87	92	89	0.4	0.4	0.2	0.3	10	10	1	SW 9	SSW 10	SSW 2
26	89.3	88.5	87.4	88.4	-18.9	-14.3	-19.9	-18.2	-13.9	-19.9	89	85	89	87	0.1	0.3	0.1	0.2	0	3 ⊙	0	SSW 2	SSW 2	C 0
27	90.2	93.9	97.6	93.9	-21.3	-12.7	-12.7	-14.8	-12.5	-23.5	89	92	96	92	0.1	0.2	0.1	0.1	0	0 ⊙	10	C 0	C 0	C 0
28	98.1	96.3	93.4	95.9	-18.3	-14.5	-11.9	-14.2	-11.8	-19.5	93	91	93	93	0.1	0.2	0.2	0.2	3	10 ✱	10 ✱	SE 2	E 3	SE 6
29	91.1	90.7	92.4	91.4	-8.3	-5.6	-5.3	-6.1	-5.1	-11.9	89	90	98	92	0.3	0.4	0.1	0.3	10 ✱	10	10	SE 6	SE 4	S 6
30	91.8	89.7	88.9	90.1	-5.3	-2.7	-0.5	-2.2	-0.3	-5.4	100	95	100	98	0.0	0.2	0.0	0.1	10 ≡	10	10 9≡	S 4	S 2	S 2
31	87.8	87.6	86.5	87.3	-1.5	-0.2	-0.1	-0.5	0.4	-2.2	99	100	100	100	0.1	0.0	0.0	0.0	10	10	10 ≡	SE 2	S 1	S 3
M	92.2	92.2	93.3	92.6	-5.3	-3.5	-4.7	-4.6	-1.8	-7.6	90	85	89	88	0.5	0.7	0.6	0.6	8.1	7.6	5.7	4.9	5.3	4.4

Suwałki $H_s = 165\,m$ $H_b = 169{,}6\,m$ $h_w = 13\,m$ **Listopad – Novembre 1967**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU L	USŁONECZNIENIE	POGODA
1	6	3.4	.	-	•° 0⁰⁰–1³⁵, 3¹⁵–⁴⁰, 11¹⁰–12¹⁵ •, •°–20³⁰, =, 12²⁰–24, ≫ 17²⁰–19³⁰
2	7	.	.	-	•¹⁻⁰ 2²⁰–3³⁰, =, 0⁰⁰–6²⁰
3	6	.	.	-	=, 6³⁰–13³⁰, ⌒° 1⁰⁰–8⁰⁰
4	7	4.3	.	-	•° 20²⁵–24
5	5	3.7	.	-	•° 0⁰⁰–5¹⁰ •⁰⁻¹ 8³⁰–10⁴⁰, 12¹⁵–23¹⁵, =, ≡° 8¹⁰–24
6	4	0.0	.	-	=, 0⁰⁰–14⁴⁵, ≡°–16⁵⁰, =–24
7	5	0.0	.	-	•° 1⁴⁰–2¹⁵, • 8¹⁵–13⁴⁵, =, 0⁰⁰–24
8	5	4.0	.	-	•° 10⁴⁵–11¹⁰, 12²⁵–20²⁰–21³⁵ •°–24, =, 0⁰⁰–24
9	6	0.0	.	-	•° 0⁰⁰–2³⁰, •°–3²⁰ •° 5¹⁵ •°–7³⁵, =, 0⁰⁰–24
10	6	4.6	.	-	•⁰⁻¹ 13⁴⁵–14⁴⁵ •⁰⁻¹ 17⁵⁰–24, =, 0⁰⁰–24
11	6	1.5	.	-	•° 0⁰⁰–2⁵⁰, 3¹⁰–15⁴⁰, 18¹⁰–20²⁰–24, =, 0⁰⁰–24, ≫ 8²⁰–23¹⁵
12	7	0.0	.	-	•° 0⁰⁰–2⁰⁵, 15⁵⁰–16²⁰ *° 18¹⁰, =, 0⁰⁰–3²⁵, ≫ 7⁴⁰–18³⁰
13	7	0.0	.	-	*° 3⁰⁵–4⁴⁵, ≫ 8²⁰–16⁴⁵
14	7	0.0	.	-	•° 4¹⁰⁻²⁰ ◉⌒° 5³⁵–7⁴⁰, ∼ 6¹⁰–9⁰⁰, =, 6³⁰–8³⁰, ≫ 13⁰⁵⁻⁵⁵, 14³⁰⁻⁵⁰
15	5	0.3	.	-	◉⌒° 12⁴⁵–14⁴⁰, =, 0⁰⁰–24
16	5	1.6	.	-	•° 3³⁰–4¹⁰ •°–7⁴⁰ •° 18³⁰–19⁴⁰ •° 20²⁵–22⁰⁵, =, ≡⁰⁻¹ 0⁰⁰–24
17	6	1.5	.	-	•° 0¹⁵–3⁴⁰ 4⁴⁰–6¹⁰–9³⁰ •°–10⁴⁵ •° 11⁴⁰–12³⁰ •°–13⁰⁵, =, 0⁰⁰–13¹⁵
18	5	3.0	1	-	*⁰⁻¹ 3²⁵–12¹⁵ •⁰⁻¹–13²⁰ *⁰⁻¹ 13³⁸–14⁴⁵
19	7	0.0	1	-	*¹ 5¹⁰⁻⁵⁵ *° 6¹³–7²⁵ *° 11⁴⁵–12¹⁷, 12⁵⁰–13⁴⁵
20	8	.	1	-	*° 0⁴⁵–2¹⁵
21	7	.	1	-	=, 20²⁰–24
22	7	.	.	-	=, 0⁰⁰–8³⁰
23	7	.	.	-	=, 19⁰⁰–24, ⌴¹ 17²⁰–24
24	6	.	.	-	=, 0⁰⁰–23⁵⁰ ≡¹–24, ⌴¹ 0⁰⁰–24
25	3	0.9	.	-	•° 15⁴⁰–17²⁰ •°–18¹⁰ •⁰⁻¹–22²⁰, ≡⁰⁻¹, =, 0⁰⁰–24, ⌴° 0⁰⁰–11⁰⁰
26	5	.	.	-	≡¹⁻⁰, =, 0⁰⁰–24
27	2	3.6	.	-	•° 9³⁰–12²⁵ •° 15⁰⁵–24, =, ≡⁰⁻² 0⁰⁰–24
28	7	.	.	-	•° 0⁰⁰–3¹⁵, =, 0⁰⁰–6²⁰ ≡°–8⁴⁰, =–11¹⁰, ⌴° 19⁰⁰–24
29	6	.	.	-	=, 0³⁰–24, ⌴¹ 1⁰⁰–24
30	6	10.3	.	-	•° 9¹²–⁴⁰ *°–11¹⁵ •° 11⁴⁰–18²⁰–24, =, ≡° 0⁰⁰–24, ≫ a. p.–24, ⌴° ra
31					
Σ	–	42.7	–	-	UWAGI.

Grudzień – Décembre

1	8	3.1	.	-	•° 0⁰⁰–11⁴⁵ •° 14⁰⁸–³⁵ •° 15⁵⁵–16¹⁵, ≫ 0⁰⁰–12³⁰, 15⁴⁵–16²⁰
2	6	11.4	.	-	•⁰⁻¹ 7⁰⁵–13⁴⁰, ≫ 17²⁰–24
3	8	.	.	-	≫ 0⁰⁰–17²⁰
4	6	3.9	.	-	=, 6²⁵–24, ⌴° 19⁰⁰–24
5	6	10.3	.	-	◉⌒ ∼ 4¹⁰ 5³⁰ •¹⁻⁰–9³⁰ 13³⁵, =, ≡° 0⁰⁰–14³⁰, ≫ 12¹⁰–13⁴⁵, ⌴° ra
6	8	.	.	-	≫ 4¹⁵–7⁵⁰
7	6	.	.	-	=, 3⁴⁵–24, ⌴° 4⁰⁰–10⁰⁰
8	8	0.0	.	-	=, 0⁰⁰–8³⁰, ⌴° 5⁰⁰–10⁰⁰
9	8	0.0	1	-	*° 2⁴⁵–3⁰⁵, 7²⁵–8¹⁰ *°–10⁵⁵, ⌴¹ 19⁰⁰–24
10	7	0.0	.	-	*° 21³⁵–22⁴⁰, ⌴¹ 0⁰⁰–24
11	5	1.5	.	-	*° 1¹⁰–2⁴⁰ ◉⌒ ∼ 2⁴⁰–6²⁰ 8²⁰–13⁵⁰ △° 15²⁵–16⁴⁰, =, ≡° 1⁰⁰–24
12	6	0.3	2	-	*° 0⁰⁰–5³⁵, 7¹⁵–12¹⁵ 13⁴⁶, 22⁴⁰–23⁴⁰–24, =, 0⁰⁰–17³⁰
13	7	0.0	3	-	*° 0⁰⁰–2⁴⁰ *° 8³⁵–10⁵⁵
14	8	0.3	3	-	*° 10⁴⁵–11¹⁰, 23⁴⁵–24, ≫ 7¹⁵–24, ⊹¹ 23⁴⁵–24
15	6	0.3	5	-	*° 0⁰⁰–1³⁰ *¹⁻⁰–10¹⁵ ↔° 12²⁰–13²⁰, 17³⁵–19⁴⁰, ≫ 0⁰⁰–6³⁰, ⊹¹ 0⁰⁰–11¹⁰
16	7	0.0	6	-	*° 23⁴⁵–24
17	7	0.0	6	-	*° 0⁰⁰–2⁴⁰, 10¹⁵ 13⁴⁸
18	6	0.6	5	-	*° 8³⁵ 9⁰⁵ ◉⌒° 9²⁵ △° 11¹⁵ *¹⁻⁰ 12¹⁰ 14¹⁵ ◉⌒° 15²⁵–22⁴⁵ •°–24, =, 8¹⁰–24
19	7	0.0	4	-	•° 0⁰⁰–7¹⁵, =, 0⁰⁰–12²⁰
20	6	5.6	2	-	⁵°3¹⁵–²⁰ * *⁰⁻¹ •° 7³⁵–13¹⁵ •°, *° 13³²–16²⁵
21	8	0.8	7	-	*⁰⁻¹ 2³⁸–6³⁰, ⊹⁰⁻¹ 6³²–7⁵⁰ ≫ 9²⁰–10⁴⁰
22	8	0.6	8	-	*° 2¹⁵–3¹⁵ 6¹⁰–7²⁰ *¹–8²⁵, =, 16¹⁵–20⁰⁰, ☿° 23³⁰–24
23	6	0.0	8	-	↔° 12¹⁰–³² *°–13⁴⁵, =, 9²⁰–24
24	7	0.0	8	-	*° 7²⁵–10²⁰, =, 0⁰⁰–6²⁰
25	7	0.0	8	-	*° 0³⁵–8¹⁰, =, 7¹⁰–9¹⁵, 23³⁰–24, ≫ 4¹⁰–6²⁵, 7²⁰–16³⁰
26	6	0.0	8	-	↔¹ 11⁰²–12⁴⁰, =, 0⁰⁰–24
27	5	0.0	8	-	*° 9³⁵–12²⁴ ↔° 12⁴⁰–14²⁵ *° 16⁴⁰–18¹⁰, =, ≡° 0⁰⁰–24, V¹ 21⁰⁰–24
28	6	0.8	9	-	*° 9⁴⁰–15³⁰, 16¹⁵–18¹⁰, 20¹⁰–24, =, 0⁰⁰–15³⁰, V¹ 0⁰⁰–9⁴⁰
29	6	0.0	10	-	*° 0⁰⁰–7¹⁰, =, 8²⁰–24 V¹ 22⁴⁵–24
30	5	0.0	10	-	◉⌒° 10⁴⁵–11³⁸, 16⁴⁸–23⁰⁰, =, ≡° 0⁰⁰–24, V¹ 0⁰⁰–24
31	5	.	10	-	≡° 0⁰⁰–3⁴⁶, =–15¹⁵ ≡²–24, ∩° 0⁰⁰–14⁰⁰, V¹ 0⁰⁰–14⁰⁰
Σ	–	39.9	–	-	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Styczeń – Janvier 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dias	I	II	III	Dias	Max	Min	I	II	III	Dias	I	II	III	Dias	I	II	III	I	II	III
1	96.1	97.7	98.9	97.6	-0.6	-0.3	0.8	0.2	0.8	-4.1	97	94	96	96	0.2	0.4	0.3	0.3	10 △	10	10	SE 1	SW 1	SW 2
2	99.0	97.8	95.1	97.3	0.0	0.4	-0.2	0.0	0.9	-0.6	96	94	98	96	0.2	0.4	0.1	0.2	10	10	10	S 1	SSE 1	SE 1
3	88.5	85.5	84.2	86.1	-0.4	0.7	1.5	0.8	1.6	-0.7	92	92	94	93	0.5	0.5	0.4	0.5	10	10	10	SE 3	SE 2	SE 2
4	84.7	85.6	84.1	84.1	0.7	3.6	5.8	4.0	6.1	0.4	96	97	85	92	0.2	0.3	1.5	0.7	10	10 •	10	SE 1	SE 1	S 3
5	87.5	88.1	90.1	88.6	1.9	3.1	1.9	2.2	5.8	0.3	96	97	93	95	0.3	0.2	0.5	0.3	10	10	10	SE 1	S 1	SSW 2
6	94.5	96.7	95.8	95.7	1.2	2.5	-0.2	0.8	2.6	-0.4	89	77	92	86	0.8	1.7	0.5	1.0	9	4	0	SW 3	SW 4	S 1
7	94.1	94.1	94.1	94.1	-0.8	1.0	-0.1	0.0	1.3	-1.4	91	87	94	91	0.5	0.9	0.4	0.6	10	10	10	SE 2	SSE 2	SE 1
8	95.2	95.3	92.9	95.1	-0.6	0.8	0.8	0.4	0.9	-1.3	95	100	96	97	0.3	0.0	0.3	0.2	9	10 ≡	10	SSW 1	SW 2	S 3
9	89.1	91.2	94.1	91.5	1.2	1.6	1.5	1.4	2.5	0.5	100	100	98	99	0.0	0.0	0.1	0.0	10 *	10 ,	9	SSW 3	SW 2	S 1
10	94.1	95.8	96.9	95.6	1.1	1.8	-0.3	0.6	2.1	-1.2	96	93	94	94	0.2	0.6	0.4	0.4	10	9	10	SW 3	SW 2	S 3
11	96.4	98.1	99.2	97.9	0.0	0.3	0.4	0.3	0.5	-0.6	96	88	98	94	0.2	0.7	0.1	0.3	10	10	10 *	S 4	S 3	S 1
12	101.2	104.8	110.1	105.4	-1.2	-0.3	-0.7	-0.8	0.3	-1.2	99	98	97	98	0.1	0.2	0.2	0.2	10 *	4 ⊙	10	SW 3	NW 4	WNW 3
13	112.9	110.7	107.3	110.4	-4.3	-1.8	-1.3	-2.2	-0.6	-3.6	91	81	93	89	0.4	1.0	0.3	0.6	2	9	10 •	W 2	SW 4	SW 3
14	107.0	109.6	113.2	109.9	0.3	1.1	1.3	1.0	1.4	-1.4	100	100	98	99	0.0	0.0	0.1	0.0	10	10 , ≡	10	SW 2	SW 2	NW 3
15	114.4	113.7	110.8	113.0	-1.4	-1.3	0.3	-0.4	1.4	-2.7	98	93	98	96	0.1	0.4	0.1	0.2	10	10	10 ,	WSW 2	W 4	W 3
16	107.6	107.9	111.1	108.9	1.7	3.0	-1.2	0.6	3.3	-2.3	96	84	70	83	0.3	1.2	1.7	1.1	10	6	3	NW 4	N 3	W 6
17	116.4	117.3	122.3	118.7	-8.4	-3.7	-8.8	-7.4	-1.2	-10.2	86	67	71	75	0.4	1.6	0.9	1.0	0	4	0	NE 6	NNE 8	NE 4
18	125.3	126.0	124.6	125.3	-14.2	-6.8	-8.0	-9.2	-3.7	-14.6	92	64	78	78	0.2	1.3	0.7	0.7	0	1	2	NE 1	N 1	WNW 1
19	121.4	119.4	117.7	119.5	-6.8	-3.6	-4.6	-4.9	-3.2	-8.1	75	47	67	63	0.9	2.3	1.4	1.6	9	8	10	C 0	W 1	WNW 1
20	114.9	113.7	111.2	113.3	-7.3	-0.6	-8.2	-6.1	-0.4	-10.2	85	56	92	78	0.5	2.6	0.2	1.1	3	3	0	C 0	W 1	C 0
21	108.3	107.6	105.4	107.2	-11.2	-4.6	-6.3	-7.1	-3.3	-11.8	93	81	86	87	0.2	0.8	0.3	0.5	4	9	9	C 0	SE 1	C 0
22	101.7	100.2	99.2	100.4	-8.7	-4.6	-5.4	-6.0	-3.9	-8.9	92	64	85	80	0.3	1.3	0.6	0.8	8	9	10	C 0	SW 1	C 0
23	99.3	100.1	99.4	99.7	-12.6	-8.8	-7.6	-9.2	-3.0	-13.1	92	80	87	86	0.2	0.6	0.4	0.4	0	8	10 *	NE 1	NNE 4	WNW 1
24	97.4	97.7	99.6	98.2	-4.3	-3.2	-13.8	-9.3	-3.0	-15.3	96	88	92	92	0.2	0.3	0.2	0.3	10	6	0	WNW 2	NE 3	C 0
25	98.9	100.6	103.1	100.9	-17.6	-10.9	-18.7	-16.3	-9.9	-20.3	90	83	89	87	0.2	0.4	0.1	0.2	2	0	0	C 0	NE 1	C 0
26	107.0	108.8	112.0	109.3	-19.3	-7.3	-9.0	-11.2	-7.4	-21.9	89	62	79	77	0.1	1.3	0.6	0.7	3	9	9	SW 1	SW 6	SW 2
27	114.9	115.9	115.3	114.7	-7.7	-4.7	-8.9	-7.6	-3.3	-9.3	79	71	70	73	0.7	1.2	0.9	0.9	3	8	2	WSW 3	WSW 3	SSW 3
28	108.1	105.2	102.0	105.1	-11.6	-3.6	-7.0	-7.3	-2.3	-12.2	68	51	77	65	0.8	2.3	0.8	1.3	2	8	2	S 3	SSW 4	S 3
29	96.8	96.8	97.2	96.9	-7.7	0.3	2.1	-0.8	2.9	-8.3	76	84	84	81	0.8	0.9	1.2	1.0	1	10	10	S 3	SW 3	S 3
30	87.8	83.3	80.7	84.0	2.1	1.1	3.4	2.3	3.3	0.9	84	98	93	92	1.2	0.1	0.4	0.6	10 •	10 *	10 •	SW 6	SW 6	SW 6
31	84.3	82.0	81.8	82.7	2.3	3.3	1.9	2.4	3.8	1.7	93	98	100	97	0.3	0.1	0.0	0.2	9	10	10	SW 2	SW 3	SW 2
M	101.4	101.4	101.3	101.4	-4.3	-1.4	-2.9	-2.9	-0.3	-6.0	91	83	89	88	0.4	0.8	0.3	0.6	7.0	7.9	7.3	2.3	2.8	2.4

Luty – Février

1	84.2	82.9	80.7	82.6	1.3	2.3	1.6	1.7	3.0	0.6	94	87	96	92	0.4	0.9	0.3	0.5	10	10	10	SW 2	SSW 2	SE 2
2	76.7	76.4	76.9	76.7	1.1	2.0	1.2	1.4	2.5	0.2	96	89	92	92	0.2	0.8	0.5	0.5	10	10 •	9	SW 2	SW 3	S 2
3	77.0	78.1	80.1	78.4	-1.8	1.4	0.2	0.0	3.0	-2.0	100	89	96	95	0.0	0.8	0.3	0.4	10 =	9	10 *	SE 1	SE 1	W 2
4	84.7	86.0	86.2	85.6	-0.4	-0.4	-5.8	-2.1	0.4	-4.0	84	88	94	89	0.9	0.7	0.3	0.6	10	8	3	W 4	WSW 4	SW 2
5	90.9	94.9	99.3	95.1	-3.4	-0.1	-0.9	-1.3	0.3	-6.8	94	73	73	81	0.3	1.7	1.4	1.1	9	4	7	SW 1	WNW 6	SW 2
6	102.2	101.9	99.2	99.8	-1.9	-1.3	-0.6	-1.2	-0.3	-3.4	87	90	70	82	0.7	0.3	1.8	1.0	9	9	3	SW 1	S 3	S 9
7	89.3	88.9	89.6	89.3	-0.6	1.2	0.9	0.6	1.9	-1.2	93	98	96	96	0.4	0.2	0.2	0.3	10 *	10	0	S 4	SSW 4	SSW 2
8	90.1	93.4	98.7	94.1	0.8	1.8	0.7	1.0	2.7	-0.2	98	96	92	95	0.2	0.3	0.3	0.3	10 △	10 ,	10	SSW 3	W 3	W 3
9	99.4	95.9	91.6	95.6	-0.6	0.7	0.3	0.3	1.4	-0.9	94	94	100	96	0.3	0.4	0.0	0.2	9	10	10 *	S 2	SSE 4	SE 2
10	97.6	104.1	107.4	103.0	0.1	0.6	-0.3	0.0	0.8	-0.7	94	92	90	92	0.4	0.3	0.6	0.3	10 *	10	10	ENE 3	N 3	W 1
11	100.7	94.9	89.3	95.0	0.9	1.1	2.3	1.6	2.3	-0.6	92	98	98	96	0.3	0.1	0.1	0.2	10	10 *	10 ≡	S 4	SSW 3	SW 3
12	88.8	93.0	99.0	93.6	2.6	3.2	2.2	2.6	4.4	1.6	100	100	96	99	0.0	0.0	0.3	0.1	10 =	10 =	10 •	SW 3	NW 2	NW 2
13	102.7	105.1	108.3	105.4	0.8	2.4	-0.9	0.4	3.4	-1.3	96	91	100	96	0.3	0.7	0.0	0.3	10	9	0	WNW 2	NW 2	WNW 1
14	110.3	111.4	110.1	110.7	-2.3	1.1	0.4	-0.1	1.4	-3.6	98	92	98	96	0.1	0.3	0.1	0.2	9	9	10 ,	C 0	S 3	SSW 3
15	108.6	109.4	109.3	109.2	2.0	3.9	3.2	3.0	6.3	0.2	100	83	100	94	0.0	1.6	0.0	0.5	10 =	3	10 =	WSW 4	WSW 3	SW 1
16	111.2	113.7	113.7	113.3	2.3	3.3	3.2	3.0	3.7	1.6	100	100	98	99	0.0	0.0	0.2	0.1	10 =	10 , ≡	10 ,	C 0	NW 3	WNW 4
17	113.6	116.7	113.3	113.9	3.4	5.0	3.3	3.8	3.7	1.7	98	94	97	96	0.1	0.3	0.2	0.3	10	10	10	WNW 3	W 4	SW 4
18	112.8	113.2	111.0	112.3	1.3	10.7	6.0	6.0	13.0	1.1	96	63	80	80	0.2	4.8	1.9	2.3	0	0	0	W 2	W 2	SW 2
19	108.0	109.3	111.1	109.3	1.4	3.1	3.4	2.3	6.7	1.2	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 ,	10 ,	W 4	WNW 4	NW 3
20	114.2	117.6	118.4	116.7	1.4	1.8	0.2	0.9	3.6	0.0	98	98	100	99	0.2	0.2	0.0	0.1	10	10	10 , =	NW 3	NW 2	WSW 2
21	117.3	117.4	117.2	117.3	1.2	1.9	1.9	1.7	2.2	-0.1	100	100	96	99	0.0	0.0	0.3	0.1	10 =	10 =	10	SW 3	SW 4	WSW 3
22	118.4	118.2	119.9	119.3	0.9	2.4	1.0	1.3	2.8	0.7	100	93	98	97	0.0	0.6	0.2	0.3	10 =	10	10	C 0	E 1	E 1
23	118.6	118.0	115.8	117.5	-0.4	-0.2	-1.0	-0.6	1.2	-1.2	100	100	96	99	0.0	0.0	0.3	0.1	10 =	10 , =	10	C 0	S 1	SE 1
24	115.3	115.4	115.6	115.4	-2.0	-1.1	-1.6	-1.6	-0.1	-2.3	98	89	94	94	0.1	0.6	0.3	0.3	10 =	10	10	SE 1	C 0	S 1
25	117.1	118.8	119.2	118.4	-1.9	-0.9	-2.0	-1.7	0.0	-2.3	96	85	81	87	0.2	0.8	1.0	0.7	10	10	10	SE 1	SE 3	SE 2
26	118.2	117.3	116.9	117.5	-1.9	4.6	-0.6	0.4	5.1	-2.3	94	62	92	83	0.3	3.3	0.4	1.3	2	0	9	SE 2	SSW 4	SSW 4
27	112.9	109.3	105.2	109.1	-1.3	5.6	5.2	3.7	5.8	-2.3	93	74	93	87	0.4	2.4	0.4	1.1	10	10	10	S 4	S 4	SW 3
28	93.3	90.3	85.2	90.4	4.6	7.6	7.7	6.9	8.3	3.9	98	99	84	94	0.2	0.1	1.6	0.6	10 •	10 •	10	SW 3	SSW 2	SW 3
29																								
30																								
31																								
M	102.8	103.3	103.2	103.2	0.3	2.3	1.2	1.2	3.3	-0.8	96	90	93	93	0.2	0.8	0.3	0.3	9.2	8.6	8.2	2.2	3.0	2.6

Olsztyn - Dajtki — $H_s = 133\ m$ — $H_b = 135{,}4\ m$ — $h_a = 12\ m$ — Styczeń – Janvier 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	0.0	1	-	△ 1⁰⁰–10⁵², = 0⁰⁰–24
2	5	1.0	1	-	✳° 11⁵⁰–12³⁰, 13⁴⁸–18⁴⁰, = 0⁰⁰–24
3	6	.	1	-	= 0⁰⁰–24
4	6	0.4	1	-	●° 10⁴⁰–12²⁰, 16³⁵–18³⁵, = 0⁰⁰–24, ⊽ 3⁴⁰–4²⁰
5	6	0.0	.	-	●° 10⁵²–11⁵⁰, 12³⁰, = 0⁰⁰–24
6	7	.	.	-	= 0⁰⁰–7¹⁵, 15³⁰–24, ⌴° 20⁰⁰–24
7	6	.	.	-	= 0⁰⁰–24, ⌴° 0⁰⁰–24
8	3	1.0	.	-	△ 9¹⁵⁻²⁸, 11²⁵⁻²⁸, 13³⁵–14³⁵, ✳° 22¹⁰–24, = 0⁰⁰–11⁴⁰ ≡⁰⁻¹ 13³⁶ = –24, ⌴ 0⁰⁰–12⁰⁰
9	4	1.6	1	-	✳° 0⁰⁰–7⁴⁰, ●° –9⁵⁰, ●° –10³³, ✳° –11⁵, ●° 12³⁵, ●° –14⁰², = 0⁰⁰–7⁵⁰ ≡° –11³⁵ = –24
10	6	0.0	.	-	●° 7¹⁵–40, ●° –8⁴⁸, = 0⁰⁰–7⁴⁰ ≡° –10⁴⁵ = –24
11	6	2.0	.	-	✳° 18⁴⁰–23³⁰, ✳¹–24, = 0⁰⁰–24
12	8	2.1	3	-	✳⁰⁻¹ 0⁰⁰–8²⁰, ✳⁰⁻² 9⁵⁰–20²⁰, = 0⁰⁰–8⁰⁰
13	9	1.0	8	-	✳° 17⁵⁰–18³⁵, ☁ –23⁴⁰, = 18³⁵–24, ∞ –24
14	3	0.0	7	-	●° 10⁵⁰–13⁴⁰, = 0⁰⁰–8²⁵ ≡° –16⁵⁰ = –24, ∞° 0⁰⁰–8⁰⁰
15	6	0.0	7	-	●° 15⁴⁰–17¹⁰, ☁ ∞ –20³⁰, ●° –24, = 0⁰⁰–7⁴⁵ ≡° –9¹⁰ = –24
16	8	0.0	3	-	●° 0⁰⁰–3⁴⁰, ●° ▽ 13⁰⁵–10, = 0⁰⁰–9²⁰
17	8	.	pł.	-	
18	8	.	pł.	-	
19	8	.	pł.	-	
20	6	.	pł.	-	= 9⁴⁰–13¹⁰, ⌴° 19⁰⁰–24
21	7	.	pł.	-	⌴° 0⁰⁰–13⁰⁰
22	7	0.0	pł.	-	✳° 22⁵⁰–24, = 1³⁰–12²⁰
23	7	0.5	1	-	✳° 0⁰⁰–1¹⁰, 17⁴⁰–24
24	8	0.3	3	-	✳⁰⁻¹ 0⁰⁰–5¹⁰, ✳° 6¹⁰–11²⁵
25	7	0.0	4	-	✳° ▽ 7⁵⁰–8¹⁵, = 7²⁰–8¹⁵
26	8	.	4	-	= 7³⁰–8²⁰
27	7	.	4	-	
28	7	.	4	-	
29	7	0.1	3	-	= 16³⁰–24
30	5	1.9	pł.	-	●° 4⁵⁵–9⁴⁵, ●° –10⁴⁰, ●¹ –13³⁵, ●° –15²⁰, ●° –21³⁵, = 0⁰⁰–24
31	5	2.2	.	-	●° 22²⁰–24, = 0⁰⁰–6¹⁰, 8²⁰–17⁴⁰ ≡° –20³⁵ = –24
Σ	–	20.1	–	–	UWAGI: Kierunki i prędkości wiatru w ciągu całego roku – wg anemometru.

Luty – Février

1	7	1.2	.	-	●° 0⁰⁰–30, ●° 22⁵⁵–23⁴⁰, ✳° –24, = 0⁰⁰–12¹⁰, 19²⁰–24
2	6	0.1	1	-	✳° 0⁰⁰–3²⁰, ✳° ▽ 9⁵⁸–10³⁵, ●° ▽ 12³⁵–13⁰⁵, = 0⁰⁰–24
3	6	0.0	.	-	✳° ▽ 15⁵²–16⁰⁶, 17³³–18⁴⁰, 20³⁶–22²¹, = 0⁰⁰–6³⁵ ≡° –8³⁵ = –24, ⊽ 2⁴⁰–6⁰⁰
4	7	0.1	1	-	✳⁰⁻¹ 10⁴ 17³⁵, = 0⁰⁰–5⁵⁰
5	7	0.1	2	-	✳° ▽ 7⁰⁵–40, 21⁵⁰–22²⁰, ≡ 3⁴⁵–5⁴⁰ = –11⁷⁰, ∨ 3⁴⁵–5⁴⁰
6	7	0.2	1	-	✳° ▽ 1⁰⁰–4²⁰
7	5	1.9	1	-	✳° 2⁵⁵–5⁴⁶, ☁ –6³⁰, ✳° –7⁴⁰, ✳¹ –10⁵⁵, = 6⁰⁰–24
8	6	1.6	pł.	-	△ 6³⁰–45, ●° 7³⁰, ✳° –7⁴⁵, ●° –8²⁵, ✳⁰⁻¹ –11²⁰, ● 12¹⁰–13⁰⁵, = 0⁰⁰–14²⁰
9	6	2.1	pł.	-	✳⁰⁻¹ 16²⁵–23²⁰, ●° –24, = 8²⁰–24
10	6	0.1	5	-	✳° 0⁰⁰–2³⁰, ✳° –4⁵⁰, 5⁵⁵–9³⁵, = 0⁰⁰–24
11	5	6.0	3	-	△ 6⁵⁵–7²⁰, ✳° –8⁵², ●° 9⁵⁶–12³⁰, ✳° –13⁴⁰, ●° –21⁴⁰, ●° –24, = 0⁰⁰–24
12	3	0.0	.	-	●° 0⁰⁰⁻⁴⁵, 20⁴⁰–21³⁵, = 0⁰⁰⁻⁴⁵ ≡° –13³⁵ = –24
13	7	0.0	.	-	●° 10⁵–5²⁰, ●° 9⁵²–10⁰⁵, ✳° –11¹⁵, = 0⁰⁰–12¹⁰, 17³⁰–21⁴⁵ ≡° –24, ⌴° 19⁰⁰–24
14	6	0.6	.	-	●⁰⁻¹ 18⁵⁵–24, ≡° 0⁰⁰–5⁵⁰ = –24, ⌴° 0⁰⁰–10⁰⁰
15	5	.	.	-	●° 0⁰⁰–3⁴⁰, = 0⁰⁰–5⁵⁰ ≡° –10¹⁵ = –18⁴⁰ ≡⁰⁻¹ –24
16	3	0.7	.	-	●⁰⁻¹ 9⁴⁰–24, ≡⁰⁻² 0⁰⁰–14²⁰ = –16¹⁰ ≡° –17⁴⁰ = –24
17	6	.	.	-	●⁰⁻¹ 0⁰⁰–6³⁰, = 6³⁰–24
18	6	.	.	-	= 0⁰⁰–24, ⌴° 5⁰⁰–9⁰⁰
19	4	0.7	.	-	●⁰⁻¹ 8⁴⁰–24, = 0⁰⁰–6²⁰ ≡⁰⁻² 11³⁰ = –16⁴⁰ ≡° –19⁴⁰ = –24
20	4	0.1	.	-	●° 0⁰⁰–4⁴⁰, 18⁴⁰–24, = 0⁰⁰–15⁴⁰ ≡⁰⁻² 16⁴⁰–24
21	2	.	.	-	●° 10⁰–40, ≡⁰⁻¹ 10⁰–4⁴⁵ = –6⁴⁰ ≡⁰⁻¹ 18⁴⁵ = –24
22	6	0.1	.	-	●° 7⁵⁰–8²⁰, = 0⁰⁰–4⁵⁰ ≡⁰⁻¹ 9⁵⁰ = –20⁴⁵ ≡⁰⁻¹ 24
23	3	0.0	.	-	●° 0⁵⁴–6²⁰, 10⁵⁵–15⁴⁰, ≡⁰⁺¹ 0⁰⁰–13³⁰ = –15²⁰ ≡° –18⁴⁰ = –24
24	6	.	.	-	= 0⁰⁰–6⁴⁵ ≡° –8⁴⁰ = –24
25	6	.	.	-	= 0⁰⁰–14³⁰
26	7	.	.	-	
27	6	5.4	.	-	●° 17⁰⁵–19²⁰, 22⁵⁰–24, = 1¹⁵–24, ⌴° 1³⁰–9⁰⁰
28	5	7.3	.	-	●⁰⁻¹ 0⁰⁰–14²⁰, ●° 15⁴⁰–17¹⁰, = 0⁰⁰–8³⁰ ≡° –9⁴⁰ = –24
29					
30					
31					
Σ	–	28.1	–	–	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Marzec – Mars 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.5	98.2	102.8	98.2	1.6	5.6	1.3	2.0	7.6	1.1	100	95	92	96	0.0	0.4	0.5	0.3	10 •	10 •	4	W 7	W 6	W 4
2	105.1	106.5	107.1	106.2	1.2	5.5	2.6	2.5	5.0	0.4	87	76	89	84	0.9	1.8	0.8	1.2	10	10	3	W 2	W 2	W 2
3	109.0	111.6	113.5	111.4	0.0	3.4	3.7	2.7	4.0	−1.6	92	91	100	94	0.5	0.7	0.0	0.4	9	10 •	10 ⚊	C 0	SW 1	SW 1
4	115.2	116.8	114.1	115.4	4.2	4.1	4.2	4.2	5.6	3.4	100	95	92	95	0.0	0.6	0.6	0.4	10 ≡	10	7	W 2	W 2	SW 3
5	110.9	113.2	115.4	113.2	5.1	7.7	2.4	4.4	8.4	1.6	90	68	93	84	0.9	3.4	0.6	1.6	10	4	3	WNW 5	NW 5	WNW 2
6	114.0	113.9	111.5	113.1	2.0	8.8	4.7	5.0	10.1	1.1	98	76	92	89	0.2	2.7	0.7	1.2	10	8	0	SW 2	WSW 4	W 4
7	106.8	106.2	110.5	107.8	4.5	10.0	2.4	4.8	10.4	2.1	95	65	91	84	0.4	4.4	0.7	1.8	9	8	0	WSW 4	NW 5	NW 2
8	113.2	112.9	111.5	112.5	−0.4	5.8	3.3	3.0	10.2	−0.9	98	76	90	88	0.1	2.2	0.7	1.0	0 ≡	4 ⊙	0	WSW 1	WSW 3	NW 2
9	109.4	109.7	107.8	109.0	6.2	7.6	8.1	7.5	9.5	3.1	91	85	82	85	0.9	1.7	2.0	1.5	10	10	0	WNW 5	W 5	W 4
10	107.6	106.5	103.1	105.7	5.1	14.9	9.0	9.5	16.1	4.3	97	37	64	66	0.3	10.6	4.1	5.0	10	3	0	W 2	WSW 3	SW 2
11	99.5	100.3	102.2	100.7	6.7	9.8	6.1	7.2	11.1	5.5	77	70	76	74	2.3	3.6	2.2	2.7	2	9	10	SW 4	WNW 6	W 6
12	98.8	91.7	82.3	90.9	4.1	7.2	11.1	8.4	11.4	3.2	90	93	63	82	0.8	0.8	4.9	2.2	10	10 •	10 •	WSW 5	SW 6	WSW 6
13	81.2	87.2	93.1	87.2	3.8	5.6	1.3	3.0	11.4	1.1	77	46	61	61	1.9	4.9	2.6	3.1	9	3	0	WNW 8	WNW 8	WNW 4
14	95.4	95.2	92.8	94.5	0.1	6.9	6.4	5.0	7.8	−0.4	82	41	94	72	1.2	5.8	0.6	2.5	5	9	10 •	W 1	WNW 4	WSW 5
15	90.8	94.8	100.4	95.3	6.8	8.9	2.0	4.9	10.6	0.5	87	63	98	83	1.3	4.2	0.2	1.9	10	6	0	WNW 6	NW 7	NW 2
16	93.8	93.5	99.9	95.7	6.8	8.5	5.2	6.4	10.5	0.3	87	69	84	80	1.3	3.5	1.4	2.1	10 •	9 •	0	WNW 10	WNW 8	WNW 3
17	102.5	100.3	95.9	99.6	2.5	11.7	9.4	8.2	13.8	1.6	96	57	78	77	0.3	5.9	2.6	2.9	10	6	0	SSW 4	W 5	WSW 3
18	83.4	83.0	82.2	82.9	7.9	11.5	5.1	7.4	12.8	4.4	74	44	63	60	2.8	7.6	3.3	4.6	0	8	1	SW 4	WSW 8	W 2
19	79.2	83.8	89.9	84.3	3.6	1.0	−1.4	0.4	5.5	−2.9	75	79	98	84	2.0	1.4	0.1	1.2	10	6 *	3 *	SW 7	NW 7	NW 3
20	92.9	90.5	83.0	88.8	−4.5	2.6	1.0	0.0	3.4	−5.5	93	50	53	65	0.3	3.7	3.1	2.4	2	7 ⊙	6	WSW 3	WSW 5	SW 5
21	71.9	73.2	78.6	74.6	0.0	1.8	0.5	0.7	2.9	−0.8	98	94	96	96	0.1	0.4	0.2	0.2	10 *	10 *	10	S 5	SSW 3	NW 4
22	88.8	93.0	93.9	91.9	−1.3	1.4	−1.8	−0.9	2.8	−2.1	86	47	77	70	0.8	3.6	1.2	1.9	9 *	8 *	5	NW 6	NW 6	NE 2
23	90.5	90.4	91.6	90.8	1.0	6.6	6.5	5.2	7.5	−1.4	98	78	76	84	0.2	2.1	2.3	1.5	10	10 •	10	WSW 3	WSW 4	W 6
24	90.9	91.8	93.1	91.9	6.0	6.9	6.9	6.7	9.3	5.6	77	72	80	76	2.2	2.7	2.0	2.3	10	10	8	WSW 7	W 8	W 8
25	95.2	97.6	100.6	97.8	4.8	8.2	2.2	4.4	9.6	1.6	89	67	95	84	1.0	3.6	0.4	1.7	8	8	6	W 6	NW 7	NW 2
26	97.6	95.5	84.7	91.9	5.2	10.1	6.9	7.3	10.8	1.7	94	61	88	81	0.5	4.8	1.1	2.1	10	9	10 •	WSW 4	WSW 5	WSW 6
27	80.0	81.9	82.2	81.4	3.6	5.2	0.6	2.5	7.1	0.3	70	70	81	74	2.4	2.6	1.3	2.1	8	10	3	W 9	W 10	W 7
28	83.7	85.2	89.3	86.1	−1.0	3.3	−0.1	0.5	4.9	−1.9	85	78	94	86	0.9	1.7	0.4	1.0	7	8 *	6	WSW 7	WSW 5	W 5
29	90.1	88.3	85.4	87.9	−0.9	0.9	4.0	2.0	4.0	−1.8	89	92	100	94	0.6	0.5	0.0	0.4	9	10 *	10 •	WSW 4	SSW 3	SSW 2
30	78.9	81.8	83.5	81.4	5.8	8.0	3.6	5.2	8.5	3.1	94	37	65	65	0.6	6.7	2.8	3.4	10 •	7	10 •	SW 7	W 8	W 3
31	85.1	88.5	87.2	86.9	0.3	4.9	2.8	2.7	6.8	−0.4	96	52	69	72	0.2	4.2	2.4	2.3	4	8	10	W 2	WNW 5	S 3
M	95.3	96.2	96.4	96.0	2.9	6.5	3.9	4.3	8.4	0.8	89	68	83	80	0.9	3.3	1.5	1.9	8.1	8.0	4.9	4.6	5.3	3.6

Kwiecień – Avril

1	85.9	88.5	85.7	86.7	0.4	3.0	−1.0	0.4	3.5	−1.3	100	58	95	84	0.0	3.2	0.3	1.2	10 *	9	10 *	WNW 9	WSW 4	E 1
2	91.1	93.8	93.5	92.8	−4.4	3.7	−0.3	−0.3	4.6	−4.7	96	54	90	80	0.2	3.7	0.6	1.5	5	8	9	ENE 1	E 1	NW 1
3	88.2	86.3	89.8	88.1	−0.1	2.6	2.2	1.7	2.9	−1.4	96	95	91	94	0.5	0.4	0.7	0.5	10 *	10 *	10	E 3	E 2	W 3
4	88.3	89.4	96.2	91.3	1.1	2.7	2.0	2.0	6.3	0.5	98	93	68	86	0.1	0.5	2.3	1.0	10 *	10 •	3	S 1	SW 3	W 3
5	98.8	96.1	91.6	95.5	0.0	2.5	8.8	5.0	8.9	−1.8	90	95	97	94	0.6	0.4	0.3	0.4	10	10 •	10	SW 1	E 5	S 2
6	91.7	94.4	95.7	93.9	10.6	18.8	12.7	13.7	19.7	8.4	86	44	85	72	1.8	12.1	2.3	5.4	10	3 ⊙	6	SW 3	WSW 7	SW 1
7	93.1	91.9	94.2	93.1	14.1	23.1	12.9	15.8	23.4	11.2	67	36	89	64	5.3	18.2	1.6	8.4	10	6	10 ☇	SW 3	SW 6	NW 3
8	94.4	94.2	96.0	94.9	7.4	8.5	2.6	5.5	13.0	2.4	99	74	93	89	0.2	2.9	0.6	1.2	10	10	10	WNW 3	NW 2	NW 3
9	95.2	100.4	104.2	99.9	2.5	5.7	−0.8	1.6	6.6	−1.8	82	46	83	70	1.3	5.0	1.0	2.4	9 *	7	0	W 8	NW 10	NW 2
10	104.2	103.1	100.0	102.4	−1.6	6.0	1.6	1.9	6.9	−3.7	82	36	72	63	1.0	6.0	1.9	3.0	7	10	6	WSW 1	WNW 3	N 1
11	97.2	95.9	98.6	97.2	0.7	9.4	0.0	2.5	10.2	−4.6	73	29	72	58	1.7	8.4	1.7	3.9	2	6 ⊙	0	NNE 1	N 2	NW 2
12	101.9	103.0	100.6	101.8	−1.0	8.7	5.2	4.5	11.2	−4.3	100	24	54	59	0.0	8.6	4.0	4.2	10 ≡	3	2	N 2	NE 1	S 3
13	95.3	95.8	96.7	95.9	7.2	15.5	10.2	10.3	15.8	4.5	63	71	90	75	3.8	4.5	1.2	3.2	10	10	6	SW 3	W 4	SW 1
14	96.6	96.0	94.0	95.5	7.9	20.7	15.7	15.0	21.9	3.7	94	36	63	64	0.6	15.6	6.6	7.6	0	8	4	SW 1	SW 2	S 1
15	92.7	94.7	96.8	94.7	11.5	18.1	10.4	12.6	19.0	8.6	73	58	92	74	3.6	8.8	1.0	4.5	3	0	0	S 2	N 3	NW 4
16	96.7	95.9	95.0	95.9	6.9	16.5	11.9	11.8	16.9	5.2	99	65	69	78	0.1	6.6	4.3	3.7	10	6	6	NE 2	NE 3	NE 3
17	95.4	96.3	96.5	96.1	8.4	17.0	11.8	12.2	18.0	6.2	90	42	87	73	1.0	11.2	1.8	4.7	0	3	9	NE 2	E 3	SW 1
18	95.7	95.3	96.4	95.9	11.3	14.0	9.9	11.3	15.6	7.4	95	71	92	86	0.7	4.6	1.0	2.1	10	9	10	SSW 2	SW 2	WNW 2
19	97.3	99.6	102.8	99.9	6.3	13.3	4.6	7.2	14.2	2.7	89	37	65	64	1.0	9.8	3.0	4.6	0	2 ⊙	0	WNW 3	N 6	N 3
20	107.2	107.6	108.6	107.8	2.9	8.8	3.1	4.3	9.8	−0.9	57	34	68	53	3.2	7.4	2.3	4.4	0	0	2	NE 5	NE 6	NE 3
21	109.6	107.3	104.2	107.1	2.9	12.3	8.3	8.0	14.2	−3.3	59	25	44	43	3.1	10.7	6.2	6.7	0	0	0	E 3	E 4	SE 3
22	99.9	97.0	94.9	97.3	6.7	18.0	11.8	12.1	18.8	−3.3	57	36	49	47	4.2	13.2	7.0	8.1	0	3	1	ESE 3	SE 5	SSE 3
23	94.1	93.9	94.8	94.3	7.4	18.7	11.8	12.4	19.4	5.2	63	34	48	48	3.8	14.3	7.2	8.4	1	0	0	SE 4	SE 6	SE 3
24	97.3	98.1	99.2	98.3	9.3	15.3	10.8	11.6	17.2	5.2	59	42	59	53	4.9	10.2	5.4	6.8	0	3	0	E 4	E 6	SE 2
25	102.0	101.3	101.1	101.5	8.1	13.1	7.1	8.8	15.0	3.1	72	49	76	66	3.0	7.7	2.3	4.4	0	8	0	E 6	ESE 3	SE 1
26	99.3	96.8	95.3	97.3	8.6	17.3	12.6	12.8	18.2	5.1	59	32	48	46	4.6	13.4	7.3	8.5	0	2 ⊙	3	E 3	ESE 8	E 3
27	94.9	94.9	94.7	94.8	9.3	16.9	9.7	11.4	18.1	5.6	70	42	79	64	3.3	11.1	2.3	5.7	9	7	0	E 1	S 2	NW 1
28	94.1	93.3	94.2	93.9	6.6	18.6	12.2	12.4	19.2	2.6	94	27	57	59	0.3	15.6	6.0	7.4	2 ⊙	3	8	C 0	N 4	NE 3
29	99.0	100.1	100.2	99.8	3.3	12.6	6.6	7.8	13.7	3.7	59	30	44	44	3.7	10.2	3.4	6.4	6	4	3	E 6	E 6	E 3
30	97.9	93.3	93.8	93.7	6.2	17.3	13.4	12.6	19.2	2.6	34	41	60	52	4.3	11.9	6.2	7.3	9	7	10	E 3	E 4	E 2
31																								
M	96.3	96.6	96.8	96.6	5.4	12.6	7.6	8.3	14.0	2.1	79	49	73	67	2.1	8.3	3.2	4.8	5.4	5.6	4.6	3.0	4.2	2.2

Olsztyn – Dajtki $H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$ Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	6	0.6	.	–	●° 0⁵⁰–7¹⁵ 9³⁵ ✱°–12²⁰ ●° 13³⁵, = na..., a–24; ⌴° np
2	7	0.0	.	–	●° 18⁵²–19⁰⁵, = 0⁰⁰–6²⁰
3	6	0.3	.	–	●° 9⁴⁰–16⁴⁰ ●² 0³⁵–24; = 10²⁰–17⁴⁵ ≡⁰⁻¹–24; ⌴° 10⁰⁰–8⁰⁰
4	6	,	.	–	≡° 0⁰⁰–1³⁰ ≡¹–8³⁰ =–24
5	7	.	.	–	= 0⁰⁰–11²⁰
6	7	.	.	–	= 3²⁰–12³⁰
7	6	.	.	–	= 5⁴⁰–24
8	6	.	.	–	= 0⁰⁰–6³⁰ ≡¹–9⁴⁰ =–13¹⁰; ⌴° 0⁰⁰–8⁰⁰
9	6	.	.	–	= 6¹⁵–24
10	7	.	.	–	= 0⁰⁰–12³⁰, ⌓° 2⁰⁰–9⁰⁰
11	6	0.0	.	–	●° 16¹⁵–17²⁵, = 5³⁰–24
12	6	7.1	.	–	●° 7¹⁵–24; = 0⁰⁰–24
13	8	.	.	–	●° 0⁰⁰–2⁵⁰ 5⁵⁰, = 0⁰⁰–2³⁰, 4³⁰–5⁴⁰
14	8	0.5	.	–	●° 16⁵²–24
15	7	0.1	.	–	●° 0⁰⁰–2²⁵ 3⁴⁰
16	7	0.2	.	–	●° 4⁵⁰–9⁴⁰ ▽° 12¹⁸ 14³⁹, = 4⁵⁰–10³⁰
17	7	.	.	–	= 5³⁰–10³⁰
18	6	.	.	–	= 5³⁰–12¹⁰
19	7	0.1	.	–	●° 7⁴⁵–8³⁵, 9⁰⁹–20 ▽°10⁰⁸ 20⁴⁰
20	8	2.5	.	–	▽° 1⁰¹–2¹⁵
21	6	2.6	4	–	●° 0⁴⁰–1³⁰ ✱⁰⁻¹10⁴⁰ ▽° 12¹⁰ 13¹⁰ ✱° 16⁰³⁻¹⁰ ▽°⁻¹ 17²⁰ ▽° 19⁴⁵–20²⁰, = 1³⁰–10⁰⁰
22	6	0.3	1	–	▽⁰⁻² 1¹⁰ 15²⁰ ▽° 23⁰⁵⁻³⁰
23	6	0.0	1	–	✱° 1⁰⁵–2²⁵ 3⁴⁵–5⁴⁰ ●° 12³⁰–13¹⁶, = 1⁰⁰–8⁴⁰ ≡°–9³⁰ =–13¹⁰
24	8	0.7	.	–	▽° 9⁴⁵–10²⁰, 12⁰⁴⁻²⁰, 19⁴⁶–20²⁰
25	7	.	.	–	
26	6	1.5	.	–	●° 18³⁵–24; = 6⁰²–13³⁰ 18³⁵–24
27	7	4.6	.	–	●° 0⁰⁰–3³⁰ ⛌ 7²⁸⁻³⁸ ✱ 7⁴³⁻⁵⁵ ▽–8⁰² ✱ 12¹⁰ ● 12⁴⁸⁻⁵⁰ ✱° 13⁰⁵⁻²⁵ ✱⁰⁻² ⛌⁰⁻¹ 14²⁵–16¹⁰ ✱ 16⁵⁰–18⁴⁰, = na
28	7	0.3	.	–	✱° 7³⁵–16⁰⁵
29	6	4.3	.	–	✱⁰⁻¹ 8²⁵–13³⁰ ●° 13³⁶–14²⁰ 14³⁰ 16¹⁰ 18⁰⁵–24, = 8²⁵–24, ⌴ 2⁰⁰–7⁰⁰
30	8	3.4	.	–	●° 0⁰⁰–3⁵⁰, 5⁵⁰–8¹⁰ ●⁰⁻¹ 9⁰⁵–10⁰⁵ ●° 20²⁵–23³⁵ ✱°–24, = 0⁰⁰–10⁰⁰
31	8	3.0	3	–	✱ 0⁰⁰⁻⁵⁰ ✱°–3⁵⁰ ▽° 7⁰⁷⁻²⁷, 10⁰⁴⁻⁰⁶, 10⁴⁵⁻⁴⁹, 11³⁰–46
Σ	–	32.1	–	–	UWAGI:

Kwiecień – Avril

1	7	2.1	4	–	✱° 0⁰⁵–10 ✱⁰⁻¹ 8⁰⁷ ▽° 9³⁶–10¹², 14⁰⁶⁻²⁰ ✱¹ 16⁰⁵–22²⁵
2	8	0.3	3	–	▽° 13¹⁰⁻¹⁷ 14⁴³–15³⁵, = 2⁰⁵–3⁴⁰ ≡⁰⁻¹ 8⁴⁰ =–9³⁰
3	6	1.9	1	–	●° 3⁵⁰–5¹⁰ ✱⁰⁻¹ 12⁴⁰ ●°–14⁴⁰, = 5¹⁰–14³⁰
4	6	1.7	.	–	✱⁰⁻¹ 4⁵⁵–11⁴⁰ ✱¹–12²⁰ ●°–13⁰⁵, = 6²⁰–13⁰⁵
5	6	6.8	.	–	●° 9¹⁰–10¹⁵ ✱–11³⁵ ●° 11³⁵–13¹⁰ 14²⁵, 15⁵⁰–19³⁵ ●² 22¹⁵⁻⁴⁰ ▽°–23²⁰, = 20⁰⁰–21⁰⁰; ↖ 22⁴⁰–23²⁰; ⌴° 1⁰⁰–7⁰⁰; ⌀ 10⁰⁰–4⁰⁰
6	7	.	.	–	
7	7	3.0	.	–	▽° 18²⁸⁻⁴⁰, 20⁰¹–21¹⁰; ↙ 10³–3³⁰ ◹° 18⁰²–21⁴⁰ SW-NE, = 22³⁰–24
8	7	0.5	.	–	●° 10³–3⁵⁴ 14⁵⁴–18⁰⁸, = 0⁰⁰–8⁴⁰
9	8	0.0	.	–	✱¹⁻⁰ 6³⁵ 11³⁵
10	8	.	.	–	⌴ 0⁰⁰–9⁰⁰
11	8	.	.	–	⌴° 1⁰⁰–8⁰⁰ 23⁰⁰–24
12	8	.	.	–	≡⁰⁻² 5⁵⁵–7⁵⁰ =–9³⁰ ⌴° 0⁰⁰–9⁰⁰
13	7	0.0	.	–	●° 9⁵⁰–10²⁰, = 18³⁰–24
14	6	.	.	–	(K) 19⁴⁵–20¹⁵ SE-NE, = 0⁰⁰–3⁴⁰ ≡°–5³⁵ =–9³⁰ ∞–24
15	6	.	.	–	∞ 0⁰⁰–20⁰⁰ =–24
16	6	.	.	–	= 0⁰⁰–1⁰⁰ ≡°–4⁴⁵ =–10³⁰ ∞–18³⁰
17	8	.	.	–	= 3³⁰–9³⁰, ⌓° 4⁰⁰–10⁰⁰
18	6	.	.	–	= 2²⁰–24
19	8	.	.	–	= 0⁰⁰–1³⁰, 4³⁰–7³⁰, ⌓¹ 2⁰⁰–8⁰⁰
20	8	.	.	–	⌴° 4⁰⁰–7⁰⁰
21	8	.	.	–	⌴¹ 1⁰⁰–8⁰⁰
22	8	.	.	–	
23	8	.	.	–	
24	8	.	.	–	
25	8	.	.	–	⌓° 4⁰⁰–7⁰⁰
26	8	.	.	–	
27	7	.	.	–	
28	7	.	.	–	≡° 1¹⁵–5⁴⁰ =–6²⁰, ⌓¹ 1⁰⁰–8⁰⁰
29	7	.	.	–	
30	8	.	.	–	
31					
Σ	–	16.3	–	–	UWAGI:

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Maj – Mai 1961

DNI	CIŚNIENIE P – 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.3	96.5	97.4	96.4	10.2	12.5	9.0	10.2	13.7	7.2	81	85	97	88	2.4	2.2	0.3	1.6	8	10	10	E 3	E 2	NE 1
2	97.4	97.1	96.7	97.1	6.9	14.9	10.3	10.6	17.2	3.6	100	62	87	83	0.0	6.4	1.6	2.7	9 =	7	3	E 1	SE 2	SE 2
3	95.3	94.3	94.8	94.8	9.6	19.5	11.5	13.0	19.7	6.5	95	50	95	80	0.7	11.3	0.7	4.2	10	8	10 •	SE 2	SE 3	SW 1
4	97.9	99.5	100.6	99.3	10.0	16.2	11.9	12.5	17.0	9.1	93	53	75	73	0.8	8.6	3.8	4.4	10	4	7	WNW 3	WNW 3	C 0
5	102.1	100.9	98.5	100.5	10.3	20.0	16.2	15.7	20.6	3.2	87	42	57	62	1.6	13.6	7.9	7.7	0	10	9	N 1	SSE 3	ESE 2
6	95.1	95.3	97.9	96.1	13.6	13.2	12.0	12.7	16.2	11.3	79	99	99	92	3.4	0.2	0.2	1.3	10	10	7	S 3	SW 2	SSW 2
7	98.5	95.1	89.3	94.3	10.6	16.9	11.0	12.4	18.7	5.7	97	73	95	88	0.4	5.2	0.6	2.1	6	8 •	10 •	S 2	SSW 2	S 2
8	92.7	91.8	90.5	91.7	8.7	13.2	7.3	9.1	13.6	7.1	89	61	95	81	1.2	6.0	0.7	2.6	7	5	3	W 4	WSW 4	SW 3
9	88.2	86.0	85.9	86.7	7.9	9.8	7.2	8.0	12.1	6.3	90	79	97	89	1.0	2.5	0.3	1.3	9	9	6	SW 3	WSW 3	SW 2
10	86.9	88.3	91.8	89.1	6.1	8.4	6.8	7.0	9.0	5.6	98	87	99	95	0.1	1.4	0.2	0.6	9 •	9	10 •	W 4	WNW 5	NW 5
11	94.7	97.3	100.8	97.6	5.5	8.4	4.5	5.7	9.4	4.3	100	93	90	94	0.0	0.7	0.8	0.5	10 =	9	10	NW 6	WNW 5	NNW 7
12	101.0	99.5	98.2	99.5	5.1	7.9	4.6	5.6	8.8	3.8	84	70	92	82	1.4	3.2	0.7	1.8	10	9	10 •	N 3	NW 5	NW 3
13	96.4	94.4	92.6	94.5	4.9	12.3	8.3	8.4	13.0	3.7	87	54	97	79	1.1	6.5	0.4	2.7	10	9	9	SW 3	SW 5	SW 3
14	91.8	91.7	92.7	92.1	7.7	10.9	6.8	8.0	12.6	5.4	93	59	93	82	0.7	5.3	0.8	2.3	9	9	9 •	SW 2	W 4	WSW 2
15	95.3	93.6	95.8	94.2	7.1	12.1	6.5	8.0	15.0	3.0	94	58	97	83	0.6	5.9	0.3	2.3	9	9	10	SW 1	ESE 2	NW 5
16	94.1	94.9	96.0	95.0	7.1	11.0	6.8	7.9	13.7	5.7	96	73	97	89	0.5	3.2	0.3	1.3	10	8	4	SW 2	S 3	C 0
17	95.9	96.8	99.1	97.3	8.6	11.0	7.0	8.4	13.5	4.7	99	86	93	93	0.2	1.8	0.7	0.9	10 •	9	6	WNW 3	NW 5	NW 5
18	99.8	99.9	99.3	99.7	6.3	10.9	5.4	7.0	13.4	4.7	89	59	89	79	1.0	5.3	1.0	2.4	9	8	3	NNW 4	NNW 2	NW 2
19	97.9	96.7	94.5	96.4	6.1	13.1	11.0	10.5	16.5	-0.4	94	76	80	83	0.6	3.6	2.6	2.3	9	10	8	WSW 1	WSW 3	S 2
20	95.5	92.7	93.7	93.3	10.7	13.9	10.2	11.8	16.6	6.9	78	57	87	74	2.9	7.9	1.6	4.1	10	8	6	SSW 2	SW 5	E 1
21	94.0	94.8	96.2	95.0	12.2	13.5	10.1	11.5	18.5	6.9	85	78	79	80	2.4	5.4	2.6	2.8	7	10 • ☾	4	NNE 2	E 3	N 5
22	96.8	96.3	96.1	96.4	9.6	12.6	6.4	8.8	14.1	5.4	70	53	78	67	3.6	6.9	2.1	4.2	0	8	4	N 5	NW 6	NW 5
23	96.6	96.1	95.1	95.9	9.2	14.6	15.3	12.6	17.3	1.1	76	45	60	60	2.7	9.1	6.1	6.0	2	7	10	NW 2	NW 2	SW 2
24	96.3	97.4	97.7	97.1	10.0	12.0	9.4	10.2	13.4	5.7	77	67	84	76	2.9	4.6	1.9	3.1	10	10	0	SW 1	SW 4	SW 1
25	98.2	97.5	97.2	97.6	11.1	16.0	13.1	13.5	16.7	4.5	81	54	77	71	2.4	8.4	3.5	4.8	0	8	10	SSW 3	SSW 4	N 2
26	97.8	97.3	95.5	96.9	10.0	16.1	13.1	13.1	17.8	9.3	74	54	70	66	3.2	8.4	4.5	5.4	9	9	0	NNE 2	WNW 1	E 1
27	92.6	91.4	93.8	92.6	14.7	23.2	10.8	14.9	23.6	8.1	69	48	96	71	5.2	14.8	0.5	6.8	0	6	9	ESE 3	SSW 5	N 4
28	94.5	92.7	92.1	93.1	10.4	20.3	14.5	14.9	22.6	9.4	100	77	98	92	0.0	5.4	0.4	1.9	0 =	1	10 •	N 3	ENE 3	C 0
29	91.5	89.8	86.6	89.3	10.0	17.6	16.7	15.2	21.1	9.0	96	83	85	88	0.5	3.4	2.9	2.3	10	6	3	NNW 1	NNE 2	NE 3
30	84.2	85.2	87.1	84.8	17.6	21.2	13.9	16.6	25.4	13.9	81	82	85	83	3.8	4.6	2.3	3.6	2	9	10	ENE 4	ESE 1	SW 1
31	89.4	89.9	90.0	89.8	10.9	15.6	14.1	13.7	18.2	10.4	92	68	84	81	1.0	5.7	2.5	3.1	10 •	7	8	SW 1	WSW 3	C 0
M	94.8	94.5	94.6	94.6	9.3	14.2	10.0	10.9	16.0	6.2	88	67	87	81	1.6	5.7	1.8	3.0	7.2	8.0	7.0	2.6	3.3	2.3

Czerwiec – Juin

1	90.4	90.1	89.6	90.0	14.0	25.3	18.3	18.5	24.4	6.1	84	50	69	68	2.5	14.2	6.6	7.8	0	4	1	NNE 1	SSW 2	E 2
2	89.9	90.0	90.7	90.2	17.6	25.4	20.7	21.1	26.2	12.9	74	45	64	61	5.3	17.0	8.8	10.4	6	6	8	E 2	ENE 3	ENE 3
3	92.1	92.3	93.9	92.8	19.3	24.9	19.0	20.6	25.6	12.6	80	58	79	72	4.4	13.3	4.6	7.4	0	3 ⊙	3	ENE 2	NE 2	NE 1
4	96.0	96.5	97.4	96.6	20.0	25.7	19.4	21.1	26.1	12.8	77	45	69	64	5.4	18.1	7.0	10.2	2	4 ⊙	3	E 3	NE 5	NE 2
5	100.5	100.9	100.9	100.8	19.0	25.5	16.8	19.3	25.8	13.9	75	42	82	66	5.4	18.8	5.5	9.2	3	6	2	NE 2	E 3	E 1
6	102.2	100.8	98.8	100.6	18.3	24.8	19.5	20.5	25.7	10.3	68	28	59	52	6.8	22.6	9.2	12.9	0	1	0	E 2	E 4	E 1
7	97.7	95.9	94.2	95.9	19.3	24.0	15.9	18.8	24.5	10.3	65	47	96	69	7.8	15.8	0.8	8.1	3 ⊙	9	10 ☾	SE 2	E 5	SE 4
8	92.3	92.4	93.8	92.8	17.1	24.0	16.4	18.5	25.2	15.5	96	58	97	84	0.8	12.5	0.6	4.6	9	8	9	SE 2	S 2	SW 1
9	96.1	97.3	97.3	96.9	16.8	21.7	19.1	19.2	22.9	14.1	95	64	79	79	1.4	9.4	4.6	5.1	9	3	6	N 1	NE 1	NE 2
10	96.9	97.2	96.5	96.9	19.6	26.7	17.0	20.1	27.6	14.4	83	40	91	71	3.9	20.9	1.8	8.9	4	8	4	E 2	S 4	E 1
11	96.5	95.7	95.0	95.7	19.8	27.0	16.3	19.8	27.0	13.4	69	43	93	68	7.1	20.2	1.3	9.5	6	9	7	E 1	SSW 2	NW 1
12	94.2	93.9	92.7	93.6	15.1	18.1	15.4	16.0	19.9	13.5	98	86	95	93	0.4	2.9	1.0	1.4	10 •	10	4	N 1	WSW 1	W 1
13	92.4	91.0	88.8	90.7	13.1	21.2	16.8	17.0	22.2	11.6	100	48	72	73	0.0	13.1	5.3	6.1	10	7	7	W 1	S 2	S 1
14	87.2	86.9	88.5	87.5	14.9	20.5	14.3	16.0	20.8	11.6	94	63	98	85	0.9	8.9	0.4	3.4	10	9	9	SE 3	SE 3	S 2
15	90.0	93.0	94.6	92.5	13.0	14.1	12.5	13.0	15.6	12.5	96	95	94	95	0.6	0.7	0.9	0.7	10 •	10 •	10	W 5	W 5	W 5
16	96.2	97.1	99.4	97.6	12.6	14.4	12.6	13.0	16.1	11.5	94	92	95	94	0.9	1.3	0.7	1.0	10 •	10 •	10 •	WSW 5	WSW 5	WSW 3
17	99.0	99.8	99.7	99.5	12.8	19.4	16.7	16.4	21.1	11.0	92	68	83	81	1.2	7.2	3.3	3.9	9	10	10	WSW 4	W 5	W 2
18	98.9	96.7	94.7	96.8	17.6	24.1	21.7	21.3	25.7	11.1	77	47	64	63	4.5	15.9	9.4	9.9	10	8	10	SW 3	SW 5	NNW 4
19	98.3	100.3	102.1	100.2	14.9	18.3	14.7	15.6	21.7	13.9	78	55	58	64	3.6	9.5	7.0	6.7	3	4	3	W 5	W 4	W 4
20	105.9	108.0	108.6	107.5	12.6	15.9	12.1	13.2	17.1	9.7	72	54	76	67	4.1	8.4	3.3	5.3	7	7	1	WSW 5	WNW 6	C 0
21	107.1	104.7	105.1	105.6	13.8	18.6	10.4	13.3	20.4	8.5	68	46	97	70	5.1	11.6	0.3	5.7	9	9	7	S 2	SW 4	N 1
22	107.8	106.3	101.3	105.1	12.1	19.0	15.4	15.5	20.2	8.4	84	52	68	68	2.2	10.5	5.7	6.1	1	4	6	W 3	SW 3	SSE 1
23	97.0	97.6	99.1	97.9	15.6	21.6	14.2	16.4	22.6	12.0	78	50	89	72	3.9	12.9	1.8	6.2	8	8	4	SSW 1	NW 5	NNW 2
24	98.6	99.5	99.5	99.2	15.0	17.7	16.8	16.6	20.0	12.6	81	52	66	66	3.3	9.7	6.4	6.5	10	8	10	WSW 3	W 5	SW 1
25	97.6	96.7	94.3	96.2	18.0	24.7	21.0	21.2	26.4	14.9	71	42	52	55	5.9	18.1	11.9	12.0	6	6 ⊙	9	W 5	WSW 4	SW 2
26	95.2	96.0	95.9	95.7	17.9	25.2	18.5	20.0	25.9	15.2	72	38	80	63	5.7	20.0	4.5	10.0	2 ⊙	5	0	WSW 2	WNW 3	NE 2
27	93.8	90.4	90.3	91.5	19.1	30.0	21.2	22.9	31.0	15.2	82	48	93	74	4.0	21.8	1.9	9.2	6	5	9	E 1	S 4	E 1
28	95.1	101.0	105.8	100.6	15.4	16.6	12.5	14.2	21.3	12.5	91	52	65	69	1.5	9.1	5.0	5.2	10 •	7	2	W 4	WNW 7	W 5
29	108.1	109.6	109.1	108.9	14.6	15.9	13.4	14.3	17.1	9.9	82	70	87	80	2.9	5.4	2.0	3.4	9	9	3	W 4	W 4	WNW 1
30	109.2	109.1	108.9	109.1	15.6	21.6	12.8	15.7	22.9	10.5	78	58	88	75	3.7	10.9	1.8	5.5	0	2	0	W 3	W 4	NNW 2
31																								
M	97.4	97.6	97.6	97.5	16.2	21.7	16.4	17.6	23.0	12.1	82	55	80	72	3.5	12.7	4.0	6.7	6.1	6.6	5.6	2.7	3.7	1.9

Olsztyn - Dajtki $H_s = 133\ m$ $H_b = 135{,}4\ m$ $h_w = 12\ m$ **Maj - Mai 1961**

DNI	WIELKOŚĆ ZACHMURZENIA v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	1.3	.	-	•° 8¹⁵–12³⁰ 15⁴⁰–16⁰³ ▽° 16²⁴ = 8¹⁵–12³⁰, 19³⁰–24
2	7	.	.	-	= 0⁰⁰–5³⁰ ≡° –7³⁵ = –9²⁵, 23³⁰–24
3	7	4.4	.	-	•¹ ▽ 6²⁰–18¹⁰ •° ▽ 19²⁰–21⁴⁰, = 0⁰⁰–10³⁰, 22³⁰–24
4	7	.	.	-	= 0⁰⁰–9⁴⁰
5	8	0.0	.	-	= 2⁴⁰–3⁴⁶ ≡° –5³² = –7³⁰, ⌒¹ 10⁰⁰–7⁰⁰
6	6	7.7	.	-	•° ▽ 6³⁷-³² •⁰⁻¹ ▽ 8⁰² 12¹⁰ •¹⁻⁰ –17³⁵ = 9⁴⁰–24
7	7	10.1	.	-	•° ▽ 12³³-⁴⁰ •⁰⁻¹ ▽ 15³⁵ 19³⁰ •° –21⁵⁰ •° ▽ 23²⁵–24, ↖° 14⁴⁰–15⁵⁰ S-N, 17¹¹-⁵⁰ SW-NE, = ≡° 0⁰⁰–10³⁰
8	7	2.4	.	-	•¹ ▽ 0⁰⁰-²⁵ •¹⁻⁰ ▽ 9⁴⁶–16¹⁰
9	7	6.4	.	-	•⁰⁻¹ ▽ 8⁴⁰ 17¹⁵ •° ▽ 21²²-⁴⁷
10	7	10.3	.	-	•⁰⁻¹ ▽ 2¹⁰ 23⁵⁰, = 4¹⁵–11⁴⁰
11	6	0.3	.	-	•° ▽ 1¹³–2⁵⁰ •° 4⁰⁵–6²⁰ •° ▽ 10¹⁵ 13⁰⁵, = 3³⁰–6³⁰ ≡° –8⁴⁵ = –24
12	8	0.0	.	-	•° 10⁵² 21⁵⁶, = 0⁰⁰ 3³⁰
13	7	2.2	.	-	•° ▽ 16⁴⁵ 19¹⁰ •⁰⁻¹ 23⁴⁰, = 18³⁰–24
14	7	0.6	.	-	•¹ 3⁰²-¹⁵ ▽ •⁰⁻¹ 9⁰¹ 10¹⁷ ▽ •° 20⁴⁰-⁵⁰, = 0⁰⁰–7³⁰
15	7	2.1	.	-	•° ▽ 9⁴²–10⁰⁶ ▽ •⁰⁻¹ 13⁵⁰ 15⁰⁴ ▽ ° 17⁴⁸–19¹⁰, ⌒° 0⁰⁰–6⁰⁰
16	7	1.7	.	-	•° 6⁵¹–8⁵⁶ ▽ •¹⁻⁰ 9¹⁵ 10⁴⁵ ▽ •° 16⁰³-⁴⁵, = 3⁴⁰–8⁵⁰, 20³⁰–24
17	6	0.0	.	-	•° 3⁵⁰–9⁴⁰, = 0⁰⁰–14¹⁵
18	8	.	.	-	
19	7	0.0	.	-	•° 8⁵²–10⁰⁵ ▽ •° 10⁵⁰–11¹⁵, 12⁵²–13⁴⁰, ⌒° 2⁰⁰–8⁰⁰
20	7	.	.	-	= 3³⁰–7³⁰, 19³⁰–24, ⌒° 2⁰⁰–8⁰⁰ 19⁰⁰–24
21	6	5.1	.	-	▽ •¹ 12¹⁵-¹⁶ ▽ •⁰⁻¹ 12²⁶–14³⁶, ↖° 12⁰⁶–14¹⁰ SE-NW, = 0⁰⁰ 7³⁰, ⌒⁰⁻¹ 0⁰⁰–9⁰⁰
22	8	.	.	-	
23	8	.	.	-	⌒° 1⁰⁰–8⁰⁰
24	7	.	.	-	⌒° 0⁰⁰–7⁰⁰, 23⁰⁰–24
25	8	.	.	-	= 2³⁰–7³⁰, 18³⁰–24, ⌒° 0⁰⁰–9⁰⁰
26	7	.	.	-	= 0⁰⁰–9³⁰ ∞ 18³⁰–22³⁰ = –24
27	6	2.3	.	-	▽ •° 17⁵⁰–18¹⁵ 19⁴⁰–20⁰⁵ 21³⁵–22¹⁰, = 0⁰⁰–7³⁰ ∞ –17³⁰, ⌒° 1⁰⁰–8⁰⁰
28	7	18.2	.	-	▽ •⁰⁻² 16⁴³–19¹⁰ ▽ •⁰⁻¹ 20⁰¹–22²⁵, ↖ 15⁰³–21²⁵ SE-NW, = 0⁰⁰–2¹⁰ ≡° –8⁴⁰ = –13²⁰ ∞ 14⁴⁰–16⁴³ = 22²⁵–24
29	6	.	.	-	▽ •° 1⁵⁰–4⁴² = 0⁰⁰–17⁴⁰
30	7	1.8	.	-	▽ •¹ 12³⁹-⁵⁹ ▽ •° 14⁵⁰-⁵⁵ 15⁰³-⁰⁵, ↖° 12³⁴ 13⁰⁵ SE-SW, 15⁰³-¹⁰ SE-NW, ⌒° 3⁰⁰–8⁰⁰
31	7	0.7	.	-	•° 5⁵² 8⁴⁰ 9⁰⁷ ▽ •° 11³⁰-³⁶, = 9⁰⁷ 12³⁰, 22³⁵–24, ⌒° 3⁰⁰–6⁰⁰, 21⁰⁰–24
Σ	—	77.6	—	-	UWAGI.

Czerwiec - Juin

1	7	.	.	-	= 0⁰⁰ 5²⁰ ≡° –6⁵⁰ = –10³⁰, ⌒¹ 0⁰⁰–11⁰⁰ ⌒° 22⁰⁰–24
2	7	.	.	-	⌒° 0⁰⁰–10⁰⁰
3	8	0.5	.	-	▽ •° 15²⁰–16⁰⁵, ↖° 15³⁵-⁵⁰ NE-SW, = 2³⁰–7³⁰, ⌒° 0⁰⁰–9⁰⁰, 22⁰⁰–24
4	7	.	.	-	⌒° 0⁰⁰–3⁰⁰ ⌒¹ –10⁰⁰
5	8	.	.	-	⌒° 3⁰⁰–11⁰⁰
6	8	.	.	-	⌒° 2⁰⁰–8⁰⁰
7	7	24.7	.	-	▽ •⁰⁻² 20³⁰–24, ↖ 20²⁵–24 SE-N, ⌒° 2⁰⁰–9⁰⁰
8	7	5.9	.	-	▽ •° 0⁰⁰–2¹⁰ 15²⁵-⁴⁰ ▽ •¹⁻⁰ 16⁰⁷–19³⁵, ↖° 0⁰⁰–2¹⁵, 15²⁰–19³⁵ SE-NE, = 20³⁰–24
9	7	.	.	-	= 0⁰⁰–12³⁰
10	7	1.6	.	-	↖ 22⁰⁶–24 NE, = 3³⁰–7²⁰ 21³⁰–24, ⌒° 2⁰⁰–11⁰⁰ ⌒¹ 21⁰⁰–24
11	7	1.3	.	-	▽ •° 0⁰⁴ 3²⁷ 12⁵⁴–13²⁰ 15¹¹–16⁴⁵ ↖° 0¹¹ 2³³ 12⁵⁴–17²⁰ SW-NE, = 0⁰⁰–5³⁰, 20²⁰–24, ⌒° 20⁰⁰–24
12	6	0.6	.	-	•° 7²⁵ 9⁵⁰ 14³⁵ ▽ •° 19⁵⁰–20²⁰, = 0⁰⁰–15³⁰, 22¹⁵–24
13	7	0.6	.	-	= 0⁰⁰ 2³⁶ ≡° –3³⁰ ≡¹ –6¹⁵ ≡° –6⁴⁰ = –10³⁰
14	7	15.3	.	-	•° 2²⁰⁰–4⁰⁰ ▽ •° 6⁴⁵ 7²⁵ 12⁴⁰–⁴⁸ 15²⁵–³⁴ 18¹⁰-⁵⁰ ▽ •° 20²⁰ 21⁰⁵ = na – a
15	6	13.1	.	-	▽ •⁰⁻¹ 4³⁷ 8³⁸ 11²⁵–12³⁰ 12⁴⁵–15¹⁰ 16⁰⁴–19³⁵ 21⁵⁵–24, = 5⁰⁰–11²⁰
16	7	15.3	.	-	▽ •° 0⁰⁰ 3²⁰ 6⁴⁵ 24
17	7	0.0	.	-	▽ •° 0⁰⁰ 3³⁸ 14⁰²-¹⁵ 22¹⁰-²⁵, = 21³⁰–24
18	7	2.0	.	-	•° 23⁵³–24, = 0⁰⁰–12³⁰ ∞ 14¹⁰–21²⁰ = –24
19	8	.	.	-	•° 0⁰⁰-³⁵ 1¹⁰–3⁵⁵ = 0⁰⁰–3⁰⁰
20	8	.	.	-	⌒° 2⁰⁰–8⁰⁰ ⌒¹ 21⁰⁰–24
21	8	2.8	.	-	▽ •° 18³⁵–20²⁵, (↖)° 18⁴⁰ N-E, = 21³⁰–24, ⌒° 0⁰⁰–9⁰⁰
22	8	0.0	.	-	= 0⁰⁰–5³⁰
23	7	.	.	-	▽ •° 0⁰⁰⁶-¹⁰ = 22³⁰–24, ⌒° 21⁰⁰–24
24	7	.	.	-	= 0⁰⁰–8³⁰
25	7	.	.	-	
26	8	.	.	-	
27	7	15.0	.	-	▽ •⁰⁻² 17⁴⁰–18²⁵ ▽ •° 22⁴⁰–24, ↖° 17⁴²–18⁴⁸ SW-NE, 21⁴⁵–24 E-W
28	8	0.5	.	-	▽ •° 0⁰⁰-⁰³, 7⁰⁸–8²⁶, ↖° 0⁰⁰-⁴⁰
29	8	0.0	.	-	▽ •° 9⁵⁰–10⁰³, ⌒° 3⁰⁰ 9⁰⁰, 19⁰⁰–24
30	8	.	.	-	= 0⁰⁰–7³⁰, ⌒° 0⁰⁰ 9⁰⁰, 21³⁰–24
31					
Σ	—	99.2	—	-	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Lipiec – Juillet 1961

DNI	CIŚNIENIE P−900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	109.8	109.3	106.9	108.7	11.8	20.6	17.4	16.8	24.6	7.4	100	59	81	80	0.0	9.9	3.8	4.6	10 =	4	1	N 1	N 2	C 0
2	105.8	105.1	104.1	105.0	19.4	26.5	18.4	20.7	26.8	12.3	69	32	72	58	7.0	23.6	5.9	12.2	0	0	0	SW 2	NW 2	C 0
3	102.6	100.0	94.5	99.0	20.2	30.2	24.0	24.6	30.8	12.3	62	34	50	49	9.1	28.5	14.8	17.5	0	2	4	SW 1	SW 2	NW 3
4	95.6	95.4	90.1	93.0	15.5	21.6	15.1	16.8	24.4	14.0	84	55	89	75	2.8	12.1	1.9	5.6	2	8	10 •	W 3	SW 3	SW 3
5	90.6	94.3	95.5	93.5	13.6	16.2	13.4	14.2	17.0	12.4	89	49	65	68	1.8	9.4	5.3	5.5	10 •	7 ⊙	8	SW 4	SW 7	SW 2
6	97.0	98.0	99.3	98.1	10.1	15.5	11.7	12.2	16.8	8.0	88	54	85	76	1.5	8.1	2.0	3.9	9	7	9	SW 3	SW 3	SW 3
7	101.3	102.1	102.8	102.1	11.8	13.4	11.5	12.0	16.0	9.1	87	76	81	81	1.8	3.7	2.7	2.7	6	9	9	SW 3	WSW 4	C 0
8	102.9	102.2	99.7	101.6	12.9	16.2	13.4	14.0	18.8	9.1	84	68	92	81	2.4	6.0	1.3	3.2	2	10	10	SW 2	SW 2	C 0
9	94.0	90.9	90.5	91.8	14.9	22.5	15.0	15.8	23.5	9.5	69	40	98	69	5.2	16.3	0.4	7.3	0	6	10 •	S 1	S 5	W 6
10	91.8	92.5	93.7	92.7	12.5	15.9	13.1	13.6	17.1	11.0	92	61	77	77	1.2	7.0	3.5	3.9	10	9	8	SW 3	W 3	SW 3
11	95.1	95.3	95.7	95.4	13.0	18.1	15.7	14.6	19.2	10.1	78	55	78	70	3.3	9.4	3.5	5.4	7	7	3	SW 3	SW 4	SW 1
12	94.1	93.3	92.2	93.3	14.2	20.6	17.8	17.6	23.4	13.0	98	67	84	83	0.4	7.9	3.2	3.8	10	7	1	S 1	SE 1	E 1
13	89.1	85.2	78.9	84.4	16.5	26.5	22.8	22.2	27.2	13.2	90	57	68	72	2.0	15.0	8.8	8.6	10	4	9	E 3	E 4	E 3
14	82.9	87.6	91.6	87.4	15.3	15.4	12.8	14.1	22.8	12.7	95	82	84	87	0.9	3.2	2.4	2.2	10	10	10	SW 4	SW 4	SW 1
15	92.6	93.2	93.2	93.7	14.3	18.6	15.2	15.9	21.6	9.9	76	73	91	80	3.9	5.7	1.3	3.7	3	10	2	S 2	SSW 3	C 0
16	94.0	92.3	92.8	93.1	13.2	15.4	13.1	13.7	18.4	8.3	100	87	92	93	0.0	2.3	1.3	1.2	10	10 •	4	NW 1	E 1	NW 1
17	91.4	90.6	89.4	90.5	11.4	21.1	15.3	15.9	22.2	8.1	100	59	82	80	0.0	10.3	3.2	4.3	10 =	8	9	C 0	S 1	W 1
18	88.6	88.3	89.3	88.9	12.0	16.4	13.0	13.8	17.3	8.0	91	76	94	87	1.2	4.4	0.9	2.2	10	9	10	SSW 1	NW 2	SW 1
19	90.3	91.0	92.2	91.2	14.6	20.8	14.2	16.0	21.1	8.0	90	56	97	81	1.6	10.8	0.6	4.3	8	6	5	SW 2	S 3	SW 1
20	93.1	93.3	93.8	93.4	13.4	21.0	13.6	15.9	22.0	12.0	90	52	86	76	1.7	11.9	2.2	5.3	2	8	2	SSW 1	WSW 3	NW 1
21	93.0	92.6	92.0	92.5	13.7	17.1	13.0	14.2	17.3	10.3	92	84	99	92	1.3	3.2	0.2	1.6	9	9	8	SW 1	SW 2	SW 3
22	91.3	92.2	93.6	92.4	13.3	15.3	14.4	14.4	16.6	12.6	96	94	94	95	0.6	1.0	0.9	0.8	10 •	10 ⊼	9	W 5	SW 2	W 1
23	95.3	96.3	98.4	96.7	13.1	16.3	14.0	14.4	18.4	12.3	93	74	94	88	0.7	5.0	0.9	2.2	10	9	8	SW 1	SW 3	SW 2
24	100.2	101.9	104.2	102.1	13.0	14.9	13.7	13.8	16.7	11.1	94	87	90	90	0.9	2.2	1.6	1.6	10	9 •	8	SW 4	W 4	W 2
25	104.3	105.7	105.0	105.1	13.3	15.3	14.0	14.2	17.1	10.4	92	76	76	81	1.3	4.3	3.9	3.2	9	9	10	WSW 4	WSW 3	W 2
26	100.9	99.3	94.3	98.2	12.4	15.7	16.3	15.3	17.1	10.4	96	84	83	88	0.3	2.8	3.3	2.2	10	10	10	SW 2	SW 3	SW 4
27	90.3	88.9	89.3	89.3	16.2	21.0	15.2	16.9	22.2	14.6	92	61	92	82	1.6	9.7	1.3	4.2	9	9	10	WSW 2	WSW 3	NW 1
28	88.3	86.4	87.8	87.5	14.1	15.0	14.1	14.3	16.7	12.4	90	99	94	94	1.6	0.1	0.9	0.9	10	10 •	10 •	SW 2	E 1	W 1
29	90.0	93.7	97.3	93.7	12.7	18.3	12.6	14.0	18.6	12.4	99	62	87	83	0.2	7.9	1.9	3.3	10	7	4	W 2	SW 3	SW 2
30	100.0	100.3	100.0	100.1	12.3	17.4	14.1	14.3	17.6	9.0	96	68	93	86	0.3	6.4	0.7	2.3	9	9	10 •	C 0	NE 1	N 2
31	94.9	93.4	91.7	93.3	12.9	15.6	14.0	14.1	16.3	12.4	100	94	93	96	0.0	1.1	0.7	0.6	10 •	10	9	N 3	SE 3	SE 3
M	95.2	95.1	94.9	95.1	13.9	18.3	14.8	15.3	20.2	11.2	89	67	85	80	1.8	8.0	2.8	4.2	7.6	7.8	7.1	2.2	3.0	1.7

Sierpień – Août

1	91.5	93.2	97.3	94.0	12.1	15.1	13.4	13.5	16.1	11.5	98	94	94	95	0.3	1.0	0.9	0.7	10 •	10 •	10 •	S 4	SW 3	SW 4
2	98.7	97.9	97.1	97.9	14.0	22.2	16.7	17.4	22.5	10.8	84	54	93	77	2.5	12.4	1.4	5.4	2	6	10 •	S 3	SSW 4	NW 5
3	98.0	99.0	101.2	99.4	15.2	17.5	13.8	15.1	19.0	10.8	98	81	94	91	0.4	3.8	0.9	1.7	10	9	9	WNW 2	SW 3	WSW 3
4	102.6	101.3	98.2	100.7	11.7	17.3	12.8	13.6	17.6	8.7	94	61	92	82	0.8	7.6	1.2	3.2	3 ⊙	10 •	10 •	SW 2	S 2	SSW 2
5	96.8	97.8	97.6	97.4	15.0	19.8	15.2	16.3	20.7	12.6	90	60	92	81	1.6	9.3	1.3	4.1	9	8	4	SW 4	WSW 5	WSW 1
6	95.0	95.9	95.3	94.7	16.4	27.5	17.2	19.6	27.7	14.1	97	56	86	80	0.6	16.3	2.8	6.6	9	4	9	NW 2	SW 4	N 3
7	95.0	95.4	96.2	95.5	15.2	14.5	14.2	14.5	17.2	13.4	79	98	99	92	3.7	0.4	0.2	1.4	10	10 •	8	SE 1	N 1	SW 1
8	101.1	102.2	101.3	101.5	12.8	18.4	16.6	16.1	19.8	10.8	92	65	81	79	1.2	7.4	3.7	4.1	2	7	9	W 4	NNW 2	E 1
9	100.4	101.6	104.6	102.2	17.3	25.6	15.8	18.6	25.7	11.1	87	54	75	72	2.6	15.2	4.4	7.4	6	4	7	S 2	SW 5	N 2
10	105.4	104.8	100.4	103.5	14.9	19.7	18.0	17.6	20.8	10.5	92	71	81	81	1.3	6.7	3.8	3.9	4	9	10	C 0	E 1	E 1
11	97.3	98.0	98.7	98.0	15.6	16.7	15.7	15.9	19.2	14.7	94	89	99	94	1.1	2.2	0.2	1.2	10	10 •	10	W 1	NNE 4	NW 2
12	99.4	98.2	98.0	98.5	15.0	20.4	16.1	16.9	21.5	13.2	100	77	93	90	0.0	5.5	1.3	2.3	9	6	10	W 1	SW 3	NW 3
13	99.1	100.4	102.4	100.6	12.8	15.3	12.0	13.0	17.6	11.2	92	68	79	80	1.2	5.7	3.0	3.3	6	9	1	WNW 3	WNW 5	W 2
14	102.9	102.4	99.7	101.7	11.5	16.4	13.6	13.8	18.8	8.3	90	67	84	80	1.4	6.2	2.5	3.4	3	8	4	SW 4	W 3	WSW 1
15	95.2	94.1	91.8	93.7	13.1	15.0	13.5	13.8	17.2	8.3	86	91	93	90	2.1	1.5	1.1	1.6	10	9 •	10 •	S 2	S 3	SW 2
16	90.4	90.1	89.1	89.9	12.4	17.1	11.6	13.2	17.4	11.1	92	51	96	80	1.2	9.5	0.5	3.7	9	6	9	SW 2	SSW 3	SW 3
17	88.1	89.0	90.3	89.2	11.8	15.2	11.2	12.4	18.1	10.8	87	67	89	81	1.8	5.6	1.3	3.0	10	8	4	SW 2	WSW 3	SW 1
18	89.6	88.6	88.2	88.8	10.9	15.4	12.9	13.0	17.6	8.3	97	82	96	92	0.3	3.2	0.6	1.4	9	8	8	W 1	NW 7	W 2
19	85.7	84.3	85.3	85.2	11.7	13.0	12.4	12.4	17.0	10.3	94	94	89	92	0.8	0.9	1.6	1.1	9	10 •	7	W 4	SW 2	SW 1
20	85.2	86.4	89.6	87.1	12.4	16.1	13.0	13.6	16.3	11.3	96	73	80	84	0.3	4.3	3.0	2.7	10	9	4	SW 4	WSW 6	W 5
21	89.7	91.6	91.9	91.1	12.3	13.9	14.8	14.0	15.4	11.2	89	90	94	91	1.3	1.6	0.9	1.3	9 •	10 •	10	W 6	SW 4	SW 4
22	89.1	87.8	86.4	87.8	13.7	17.2	12.9	14.7	18.3	12.3	82	84	94	87	3.2	3.2	0.9	2.4	9	9 •	3	SW 4	SW 3	SW 3
23	87.8	88.2	92.3	89.3	13.3	16.2	12.3	13.6	16.6	11.7	90	83	82	85	1.6	3.1	2.6	2.4	10	9	7	SW 3	WSW 3	W 3
24	94.3	96.3	98.2	96.3	12.0	15.2	12.0	12.8	16.0	10.3	96	80	94	90	0.3	3.3	0.8	1.6	9 •	10	10 •	W 4	WNW 6	WSW 2
25	95.9	97.1	98.9	97.3	12.8	17.7	11.6	13.4	18.0	11.3	92	59	69	73	1.2	8.2	4.2	4.5	10 •	7	2	WSW 3	W 7	W 4
26	100.3	102.8	103.3	102.3	11.3	15.2	12.6	12.9	15.6	8.7	89	67	94	83	1.3	5.6	0.9	2.7	10	9	9	W 3	WNW 4	SW 1
27	103.6	103.3	104.3	103.8	14.8	22.8	15.9	17.4	24.2	12.4	99	64	97	87	0.2	10.1	0.6	3.6	9	4	3	SW 1	SW 3	NNW 2
28	105.4	107.3	106.2	106.3	13.2	18.0	15.9	15.8	18.6	11.8	94	69	81	81	0.9	6.3	3.3	3.6	9	9	3	W 4	W 6	W 5
29	105.7	106.7	107.3	106.6	13.8	17.6	11.3	13.6	18.1	11.3	94	72	96	87	0.9	5.7	0.3	2.4	9	10	0	W 4	NW 5	NW 1
30	108.7	109.3	109.4	109.1	11.4	18.7	12.3	13.7	19.6	8.3	100	51	92	81	0.0	10.6	1.2	3.9	9 =	1	0	NW 1	N 2	NW 1
31	111.2	112.2	112.7	112.0	11.0	22.3	15.4	16.0	23.4	7.2	97	59	90	82	0.3	10.9	1.7	4.3	0	2 ⊙	0	C 0	NNW 1	C 0
M	97.1	97.5	97.9	97.5	13.3	17.8	14.0	14.8	19.1	10.9	92	72	89	84	1.2	6.3	1.7	3.1	7.8	7.7	6.3	2.6	3.9	2.3

Olsztyn - Dajtki $H_s = 133\ m$ $H_b = 135{,}4\ m$ $h_w = 12\ m$ Lipiec - Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	-	≡° 5⁴⁵ 7⁵⁰ = – 11³⁰ ⌒ 0-1 0⁰⁰ – 6⁰⁰
2	8	.	.	-	= 22³⁰ 24 . ⌒ 0-1 1⁰⁰ – 9⁰⁰ 19³⁰ – 24
3	8	3.0	.	-	▽° 22¹⁰ – 23¹⁰ . ↖° 22¹⁵ – 24 SW-NW . = 0⁰⁰ – 3³⁰ . ⌒° 0⁰⁰ – 9⁰⁰
4	8	1.3	.	-	▽¹ 0¹⁵⁻⁵⁰ ▽° 1¹⁰ 16²⁵ 18⁴⁰ •° 24 . ↖° 0⁰⁰⁻⁴⁵ SW . = 2³⁰ – 6³⁰
5	8	0.1	.	-	•° 0⁰⁰⁻⁵⁰ ▽° 7³⁰ – 8⁵⁰ . = 2³⁰ – 8⁵⁰
6	8	1.6	.	-	▽° 21⁵² – 22¹⁰ 23⁴⁵⁻⁵⁵
7	7	2.3	.	-	▽° 11⁴⁵ – 12³⁵ ▽²⁻⁰ 16³⁵ – 17⁰⁷ 19³⁷ – 20¹⁰
8	7	0.4	.	-	▽° 0⁵⁰ – 1⁰⁵ 21⁰⁵⁻³⁰ 22⁰⁴⁻²⁰ . = 21³⁰ – 24
9	7	9.4	.	-	▽¹ 14⁴⁷ – 15¹⁵ . 16⁵⁰ 17¹⁰ ▽¹⁻⁰ 20⁵⁰ – 23⁰⁵ . = 0⁰⁰ – 5³⁰
10	7	0.0	.	-	▽° 9³⁸⁻⁴⁵ 15²⁰⁻³⁰
11	8	0.7	.	-	⌒° 3⁰⁰ – 9⁰⁰
12	7	0.0	.	-	•° 5⁵⁰ – 8¹⁰ . = 6³⁰ – 11²⁰ 19³⁰ – 24 . ⌒° 2⁰⁰ – 6⁰⁰
13	7	23.0	.	-	▽⁰⁻² 21⁴⁰ – 24 . ↖ 21⁴⁰ – 24 SE – NW . = 0⁰⁰ – 11³⁰ . ⌒¹ 2⁰⁰ – 11⁰⁰
14	7	0.0	.	-	▽¹ 0⁰⁰⁻⁴⁵ ▽° 2¹⁵ – 8⁴⁵ – 10⁰⁵
15	8	0.5	.	-	▽¹⁻⁰ 13¹⁰ – 14³⁵ ▽° 18³⁵⁻⁴⁵ . ⌒° 21⁰⁰ – 24
16	6	9.8	.	-	▽⁰⁻¹ 12³⁰ – 17¹⁰ •° – 18²⁰ . = 0⁰² – 1⁴⁰ ≡°⁻¹ 7⁴⁰ = – 13⁰⁰ ≡° 23⁵⁰ – 24 . ⌒° 0⁰⁰ – 1⁴⁰
17	8	.	.	-	≡⁰⁻¹ 0⁰⁰ – 8³⁵ = – 9⁴⁰
18	7	1.4	.	-	▽° 14²⁰⁻³⁵ ▽¹⁻⁰ 15¹⁰ – 17⁰⁶ . ↖ 14¹⁵ – 15³⁵ SE-NW
19	7	2.5	.	-	▽° 14²⁰ 16³⁵ . ↖° 15¹⁵ – 16⁴⁴ S-N . = 3³⁰ – 9⁴⁰ 21³⁰ – 24 . ⌒¹ 2⁰⁰ – 9⁰⁰ ⌒° 22⁰⁰ – 24
20	7	0.0	.	-	▽° 13⁵⁵ – 14⁰⁸ 16²⁰⁻³⁰ ↖° 15⁴⁰ – 17³² NW-SE . = 0⁰⁰ – 8³⁰ 22³⁰ – 24 ⌒¹ 0⁰⁰ – 8⁰⁰ ⌒° np
21	7	17.3	.	-	▽⁰⁻¹ 10⁵⁷ – 13⁰⁵ ▽¹ 16³⁰ – 18¹⁰ 18⁵² – 19⁵⁰ . ↖ 16²⁷⁻⁴⁰ SW-NW . = 0⁰⁰ – 11³⁰ . ⌒° na – a
22	6	10.6	.	-	•° 3⁵⁰ – 4⁵⁶ ▽⁰⁻² 6⁴⁸ – 13³⁰ ▽° 14⁰⁴⁻⁵⁰ 15¹⁰ – 16¹³ 19⁵⁰ – 20⁰³ . ↖ 11⁴⁵ – 15⁴⁰ SW – NE . = 2⁴⁰ – 14³⁰ . p – 24
23	7	3.3	.	-	▽° 15⁴⁰ – 16²⁰ ▽¹ 17²⁸ – 19⁰⁴ ▽° 19²⁸⁻⁴⁰ . = 0⁰⁰ – 4³⁰
24	7	4.3	.	-	▽° 8⁵⁰ – 9⁴⁵ . 11²⁸⁻⁴⁰ 12³⁵⁻⁵⁰ ▽¹ 16²⁵ – 17⁰⁵ ▽° – 17⁵⁰
25	8	0.0	.	-	
26	6	2.4	.	-	•° 5⁵⁰ – 6⁴⁰ 7¹⁰ – 10⁰⁵ 15⁰² – 18¹⁰ . = 7³⁰ – 24
27	7	0.0	.	-	•° 1⁵² – 3⁴⁵ . = 0⁰⁰ – 12³⁰
28	5	11.7	.	-	•⁰⁻¹ 7⁵⁰ – 14⁴⁰ ▽° 18¹⁵⁻⁴⁰ . 20⁴⁵ – 24 . = 14⁴⁰ – 24 . ⌒¹ 2⁰⁰ – 8⁰⁰
29	7	.	.	-	•° 2⁵⁰ – 5³⁵ . = 0⁰⁰ – 10⁴⁰
30	8	12.1	.	-	•° 15²⁸ – 20⁰⁴ . 21¹² – 24 . ⌒¹ 2⁰⁰ – 11⁰⁰
31	7	7.5	.	-	•⁰⁻¹ 0⁰⁰ – 12²⁰ . ▽° 16⁵⁰⁻⁵⁴ . 18²⁰⁻³⁰ . 20⁰¹ – 21⁰⁴
Σ	–	125.2	–	-	UWAGI.

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1	6	16.1	.	-	▽° 1⁴³ – 4²⁰ •° – 5⁴⁰ •° – 6²⁰ •⁰⁻² 14⁰⁷ ▽⁰⁻² 14⁴⁰ – 15⁵⁰ ▽° 17⁵⁰ – 18⁴⁵ 21⁰² – 23⁰⁵
2	7	15.2	.	-	•⁰⁻¹ 20²⁵ – 24 . = 6³⁰ – 9³⁰
3	6	1.0	.	-	•° 0⁰⁰⁻³⁵ ▽¹⁵⁰ 3⁴⁵ ▽¹ 9⁴⁸ 10²⁰ 10²⁸ 13⁰⁵ 15⁴² 16⁴⁰ . ↖° 15⁴⁰ 16²⁵ . = 0⁴⁵ 1⁵⁰ 3⁴⁵ – 24
4	7	3.1	.	-	•⁰⁻¹ 17¹⁰ 18⁴⁵ •° 20⁰² – 24 . = 0⁰⁰ – 8³⁰
5	7	0.6	.	-	•° 0⁰⁰ – 3⁰⁵ . = 2⁰⁰ – 9³⁰ 20³⁰ – 24 . ⌒° 20⁰⁰ – 24
6	7	0.0	.	-	•° 6⁵⁰ 7⁴⁵ . = 7⁴⁵ – 9²⁰ . ⌒° 0⁰⁰ – 6⁵⁰
7	6	13.6	.	-	▽⁰⁻¹ 7⁴⁰ – 9⁵⁹ •⁰⁻¹ 14⁰⁶ 15²⁴ – 16³² •° – 17³⁵ . ↖ 0²⁵ – 4⁰⁷ . = 17³⁵ – 24
8	8	0.0	.	-	•° 22⁰⁵⁻³⁵ . = 0⁰⁰ – 7²⁰
9	7	0.3	.	-	▽¹ 14²⁸⁻⁴⁰ . ⌒¹ 18⁰² – 24
10	8	0.3	.	-	▽¹ 13³⁵⁻⁵⁰ •¹ 21⁵¹ – 23⁴⁸ . ↖ 23⁵⁵ – 24 . ⌒¹ 0⁰⁰ – 1²⁰⁰
11	6	9.2	.	-	•⁰⁻¹ 13²⁵ – 20²⁵ . (↖)° 1¹⁰ – 2⁴⁰ S-N . = 20²⁵ – 24
12	7	0.0	.	-	▽° 20⁰²⁻⁰⁴ . = 0⁰⁰ – 2¹⁵ ≡¹ – 5³⁰ ≡° – 7³⁵ = 20³⁰ – 24
13	8	0.0	.	-	▽° 17⁵³ – 18⁰² . = 0⁰⁰ – 7¹⁵ . ⌒¹ 23⁰⁰ – 24
14	8	.	.	-	⌒° 0⁰⁰ – 11⁰⁰ 21⁰⁰ – 24
15	7	3.3	.	-	•° 9²⁰ – 11³⁵ . 11³²⁻⁵⁰ 20⁴⁰ – 22²² . = 17³⁰ – 24 . ⌒° 0⁰⁰ – 9⁰⁰
16	7	0.3	.	-	▽° 15⁰⁵⁻⁵⁰ 16⁴⁵ – 17²⁰ . 18⁴³ – 19⁰³ . = 0⁰⁰ – 10³⁰
17	8	0.1	.	-	▽° 14¹⁷ 14⁵¹ 18⁴⁶⁻⁴⁸ . ⌒ 22⁰⁰ – 24
18	7	2.4	.	-	▽° 11⁵⁴⁻⁵⁸ ▽¹ 12⁴⁰⁻⁵² . 20⁴³ – 21⁰⁹ . = 4³⁰ 10⁴⁰ . 22³⁰ – 24 . ⌒° 0⁰⁰ – 9⁰⁰
19	6	2.2	.	-	• 13²⁸ – 14²⁵ ▽° 16⁵⁰ – 17⁰⁵ . = 0⁰⁰ – 17³⁰
20	7	9.0	.	-	▽° 2⁵⁰ 16⁴⁶ ▽¹ 17⁴⁷⁻⁵² ▽° – 17⁵⁵ 18⁰²⁻¹⁶ ▲ 17⁴⁹⁻⁵⁰ . = 7¹⁰ – 11³⁰
21	6	2.3	.	-	▽° 2⁰⁷ – 5⁴⁰ 7⁰⁵ 14⁴⁰ . 17²⁰ – 21⁰⁹ . = 18³⁰ – 24
22	7	7.7	.	-	▽⁰⁻¹ 10⁵⁰ 17¹⁷ . = 0⁰⁰ – 11³⁰
23	7	2.6	.	-	▽⁰⁻¹ 10²² 19⁵³
24	8	0.2	.	-	▽° 4⁵⁰ 15¹⁵ . 21⁰⁶ – 22⁰⁰ . = 21⁰⁴ – 23⁰⁰
25	7	0.0	.	-	▽⁰⁻¹ 7¹⁸ 11⁰⁵ . = 2³⁰ – 12³⁰
26	8	0.0	.	-	•° 17²⁰ – 18⁰⁶ . ⊕ 7³⁰ – 8³⁰ . ⌒ 23⁰⁰ – 24
27	7	2.2	.	-	•° 4⁵⁰ – 5⁰⁹ ▽¹ 18⁵² – 19¹² . ↖° 18⁵⁵ – 19¹⁰ W-SE . = 1³⁰ – 10³⁰ . ⌒° 0⁰⁰ – 4⁵⁰
28	7	.	.	-	
29	7	.	.	-	⌒¹ 2⁰⁰ – 10¹⁰ 21⁰⁰ – 24 . ⌓ 2⁰⁰ – 3⁴⁰
30	8	.	.	-	= 0⁰⁰ – 4⁵⁰ ≡° – 8⁵⁰ = – 10³⁰ 22³⁰ – 24 . ⌒° 0⁰⁰ – 10⁰⁰ 21⁰⁰ – 24
31	8	.	.	-	= 0⁰⁰ – 5³⁵ ≡° – 6⁴⁰ = – 8¹⁰ . ⌒° 0⁰⁰ – 9⁰⁰ . 21⁰⁰ – 24
Σ	–	91.7	–	-	UWAGI.

Olsztyn – Dajtki φ = 53°46' λ = 20°25' Wrzesień – Septembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dias	I	II	III	Dias	Max	Min	I	II	III	Dias	I	II	III	Dias	I	II	III	I	II	III
1	112.5	110.9	108.1	110.5	13.4	24.6	17.4	18.2	25.7	10.6	99	57	86	81	0.2	13.2	2.8	5.4	3	1 ⊙	0	C 0	WSW 3	SW 1
2	104.9	105.4	100.4	102.9	15.8	26.5	18.7	19.9	27.6	13.7	89	48	77	71	1.9	18.2	5.0	8.4	0	0 ⊙	0	SW 1	W 3	SW 1
3	96.8	95.1	93.5	95.1	15.1	26.9	16.3	18.6	27.1	10.7	90	42	90	74	1.7	20.6	1.9	8.1	0 ⊙	1	0	SW 1	W 4	NW 1
4	95.1	98.0	99.3	97.5	12.7	16.1	12.2	13.3	18.2	11.8	99	78	82	86	0.2	4.0	2.5	2.2	10	3	3	NE 4	N 3	N 1
5	99.3	99.3	95.8	98.1	12.0	17.0	13.9	14.2	18.0	8.9	82	63	67	71	2.5	7.2	5.2	5.0	9	9	3	E 1	E 3	E 3
6	90.3	89.9	89.2	89.8	13.7	21.7	16.4	17.0	22.7	12.5	94	75	99	89	0.9	6.6	0.2	2.6	9	8 ⊙	10	S 1	NW 1	SSW 1
7	88.2	88.0	85.7	87.3	14.0	16.7	14.4	14.9	17.9	12.7	97	89	90	92	0.6	2.2	1.6	1.5	6	10 •	0	SW 1	SSW 3	SW 4
8	85.1	87.0	89.7	87.3	11.0	13.6	12.1	12.2	14.4	9.8	92	74	98	88	1.0	4.0	0.3	1.8	10	10 •	10 •	SW 7	SW 8	W 5
9	93.8	94.8	96.1	94.9	11.7	16.8	12.0	13.1	17.3	9.9	94	67	84	82	0.8	6.3	2.2	3.1	9	8	4	W 3	WNW 6	WNW 2
10	97.5	98.4	99.1	98.3	11.3	15.4	12.2	12.8	16.2	9.9	97	63	94	85	0.4	6.3	0.9	2.6	9	8	10	W 2	WNW 2	W 2
11	98.7	98.3	97.0	98.1	11.4	15.0	14.1	13.6	15.8	10.2	91	78	85	85	1.2	3.6	2.4	2.4	9	10	10	W 3	W 2	SW 1
12	94.7	95.7	94.0	94.1	13.3	18.4	11.7	13.8	18.7	9.8	75	61	93	76	3.8	8.4	1.0	4.4	10	4	4	SSW 4	SSW 4	SW 2
13	94.3	96.8	98.3	96.5	11.0	15.2	12.4	12.8	17.0	10.6	92	60	81	78	1.0	7.0	2.7	3.6	9 •	5 ⊙	4	WSW 5	W 3	SW 2
14	95.7	93.1	92.0	93.6	12.8	14.1	13.7	14.6	15.7	11.4	85	98	97	93	2.3	0.4	0.6	1.1	10	10 •	10	S 2	SSE 2	SSW 2
15	92.4	98.4	102.2	97.7	13.4	14.0	12.5	13.1	16.9	12.2	96	83	83	87	0.6	2.7	2.4	1.9	10 •	9	4	NW 6	NW 6	WSW 3
16	102.2	103.3	104.2	103.2	14.3	21.7	15.3	16.6	22.0	11.9	90	77	97	88	1.6	6.0	0.6	2.7	10	6	0	SW 2	SW 2	C 0
17	104.2	103.7	103.1	103.7	15.3	27.2	18.7	20.0	27.8	13.1	94	51	86	77	1.0	17.8	3.2	7.3	0 ⊙	0 ⊙	0	SSW 2	S 3	SSW 1
18	100.5	101.4	103.9	101.9	15.8	20.6	12.2	15.2	23.9	11.7	91	86	88	88	1.3	3.3	1.7	2.2	2 ⊙	10	0	SSW 1	W 5	NW 2
19	104.9	106.1	107.0	106.0	10.4	17.2	9.7	11.8	18.3	8.9	96	65	97	86	0.5	6.9	0.3	2.6	2	4	0	W 3	NNW 4	NNW 2
20	109.3	109.7	109.8	109.6	6.8	15.2	8.6	9.8	16.5	4.3	100	61	93	85	0.0	6.8	0.8	2.5	0 ⊙	3	2	N 1	E 3	NE 1
21	111.1	111.5	112.4	111.7	10.0	15.6	6.4	9.6	15.9	6.2	89	51	88	76	1.3	8.7	1.1	3.7	9	0 ⊙	0	ENE 1	E 3	E 1
22	114.0	114.3	114.3	114.2	3.4	15.5	5.8	7.6	15.9	0.2	98	52	97	82	0.1	8.4	0.3	2.9	0	1 ⊙	0	C 0	E 2	C 0
23	114.0	113.1	111.1	112.7	3.7	17.3	5.2	7.8	18.2	0.8	100	39	92	77	0.0	12.1	0.7	4.3	3	0	0	C 0	SE 2	C 0
24	109.9	108.8	107.1	108.6	2.6	17.2	6.3	8.1	17.6	0.0	100	39	85	75	0.0	11.9	1.4	4.4	0	0	0	C 0	ESE 4	C 0
25	109.8	102.7	103.0	105.2	2.5	13.3	13.8	12.4	20.3	1.4	98	41	85	75	0.1	13.1	2.3	5.2	0	3	10	C 0	SSW 3	W 3
26	104.5	104.9	104.3	104.6	8.7	13.8	7.7	9.5	15.5	7.5	95	56	91	80	0.7	7.0	0.9	2.9	0	6	8	WSW 3	W 4	W 1
27	103.4	102.9	102.8	103.0	5.2	14.0	5.7	7.6	16.1	3.5	100	58	97	85	0.0	6.7	0.3	2.3	4	5	0	C 0	NW 3	C 0
28	104.6	105.3	106.6	105.5	1.0	17.2	8.2	8.6	18.2	0.5	100	55	90	82	0.0	8.8	1.1	3.3	0 =	3 ⊙	0	C 0	SSE 3	C 0
29	107.6	106.9	106.3	106.9	7.2	16.3	10.4	11.1	17.4	4.2	99	61	92	84	0.2	7.2	1.0	2.8	5	6 ⊙	3	C 0	SE 3	SE 1
30	106.2	106.0	106.8	106.3	8.0	16.2	9.9	11.0	17.5	7.2	96	60	84	80	0.4	7.4	1.9	3.2	8	6	0	ESE 3	SE 4	E 2
31																								
M	101.3	101.5	101.4	101.4	10.3	17.9	11.9	13.0	19.0	8.2	94	63	89	82	0.9	8.1	1.6	3.5	5.2	5.0	5.2	1.9	3.4	1.5

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1	108.5	109.4	111.3	109.7	7.2	10.8	9.5	9.2	12.0	4.8	100	85	97	94	0.0	2.0	0.3	0.8	10 =	10	4	E 4	E 3	NE 2
2	113.2	114.3	114.6	114.0	9.2	14.4	10.2	11.0	16.5	6.3	100	81	93	91	0.0	3.1	0.8	1.3	10	1	0	E 4	E 4	E 1
3	115.5	115.2	114.8	115.2	6.9	16.6	9.9	10.8	17.6	6.4	100	65	87	84	0.0	6.6	1.6	2.7	2 =	1	0	E 1	E 4	E 2
4	114.4	113.8	113.1	113.8	8.0	18.9	10.6	12.0	19.2	6.6	97	48	85	77	0.3	11.3	2.0	4.5	0	0	0	E 3	E 6	E 1
5	112.2	111.5	111.4	111.7	7.3	18.2	13.1	11.9	18.7	7.0	91	51	75	72	0.9	10.2	3.2	4.8	0	0 ⊙	0	E 4	E 5	ESE 3
6	110.5	108.7	106.7	108.6	5.7	17.4	10.9	11.2	18.2	5.3	97	52	83	77	0.3	9.7	2.2	4.1	0	0	0	E 3	ESE 5	E 4
7	104.0	101.5	99.7	101.7	6.9	15.8	11.4	11.4	15.9	6.6	88	49	57	65	1.1	9.1	5.8	5.3	0	0	0	E 3	E 6	ESE 4
8	98.5	98.0	98.7	98.4	7.9	14.5	13.5	11.4	15.4	7.7	70	50	59	60	3.2	8.3	5.7	5.7	9	4	0	ESE 6	SE 6	E 3
9	103.4	107.1	111.1	107.2	6.6	10.0	7.4	7.8	12.6	6.3	85	96	100	94	1.4	0.3	0.0	0.6	4	10 •	0 =	S 1	SSW 1	WSW 1
10	113.5	113.9	113.7	113.7	2.7	16.6	10.3	10.1	17.8	2.0	100	67	100	89	0.0	6.3	0.0	2.1	8	8	10	C 0	SW 2	S 1
11	112.7	111.6	108.8	111.0	9.1	16.2	10.9	11.8	16.8	8.8	100	58	78	79	0.0	7.7	2.9	3.5	10 =	0	0	S 2	S 4	S 1
12	106.7	108.6	109.9	108.4	7.2	13.1	5.4	7.6	14.6	5.4	93	88	97	93	0.8	1.8	0.3	1.0	8	10	0	C 0	NW 3	W 1
13	108.4	109.5	110.0	109.3	7.0	13.6	7.8	9.0	14.0	5.0	100	62	96	86	0.0	6.0	0.5	2.2	10 =	6 ⊙	0	W 4	NW 6	WNW 2
14	106.7	105.6	106.0	106.1	7.6	11.8	10.4	10.0	12.7	6.1	99	87	97	94	0.1	1.8	0.3	0.7	9	10 •	10	W 4	WNW 6	NW 3
15	105.1	102.6	101.5	103.1	10.4	12.5	10.0	10.7	13.3	9.6	96	83	93	91	0.5	2.4	0.8	1.2	10	10	10 •	W 3	W 5	W 4
16	101.0	100.4	97.6	99.7	9.0	12.7	8.2	9.5	13.1	8.0	95	77	90	87	0.7	3.4	1.1	1.7	4	10	0	W 3	WSW 4	SW 2
17	93.2	90.1	84.2	89.2	8.2	12.3	10.1	10.2	12.8	6.7	93	74	86	84	0.8	3.7	1.8	2.1	9	10	9	SW 3	WSW 4	SE 3
18	77.9	77.9	79.5	78.4	9.9	12.2	12.6	11.8	12.8	9.0	86	93	73	85	1.8	0.7	3.9	2.1	10	10 •	9	SE 4	SSE 4	SE 4
19	81.9	84.6	87.9	84.8	12.4	16.9	15.3	15.0	17.8	12.2	68	59	68	65	4.7	7.9	5.7	6.1	9	8	3	SE 4	SE 4	SE 5
20	92.4	95.1	97.3	94.9	10.7	17.8	13.2	13.7	17.9	10.3	91	68	84	81	1.2	6.5	2.5	3.4	3	1 ⊙	8	SE 3	E 4	SE 5
21	97.8	99.8	103.1	100.2	9.6	10.8	10.4	10.3	13.4	9.4	86	80	81	82	1.8	2.6	2.4	2.3	0	10	10	E 6	ESE 6	SE 3
22	106.6	109.2	110.3	108.8	9.6	10.3	7.4	8.7	10.6	5.9	87	82	83	84	1.6	2.3	1.8	1.9	10	10	5	SSE 3	SSE 3	E 2
23	110.2	109.3	108.6	109.4	2.3	9.4	6.1	6.0	10.3	2.3	77	61	72	70	1.7	4.6	2.7	3.0	1	2	3	SE 4	SE 3	SE 2
24	105.3	106.2	104.6	105.4	6.0	9.2	10.0	8.8	10.3	4.3	89	96	91	92	1.1	0.4	1.1	0.9	9	10	8	SSE 3	S 3	S 3
25	100.6	98.3	98.6	99.2	6.6	12.2	11.4	10.4	12.6	6.4	90	68	82	80	1.0	4.3	2.3	2.7	4	10	10	S 4	SSW 6	S 6
26	98.2	98.3	97.7	98.1	10.4	11.3	10.6	10.7	11.7	10.0	97	93	98	93	0.3	1.0	1.3	0.9	10 •	10	10	SSW 2	S 3	S 1
27	96.1	95.4	94.3	95.3	8.1	13.8	9.8	10.9	16.9	7.8	94	63	73	77	0.6	6.6	3.0	3.4	7	9	2	S 1	S 4	S 2
28	95.3	95.3	95.3	95.4	5.9	14.6	10.9	10.6	16.1	4.2	100	78	92	90	0.0	3.6	1.0	1.5	5	7	10	WSW 1	E 2	S 1
29	94.6	94.1	95.7	94.8	10.3	10.3	8.7	9.6	11.4	8.3	97	100	100	99	0.3	0.0	0.0	0.1	10	10 9	10 •	SW 1	C 0	NW 2
30	97.9	98.3	100.2	98.9	8.4	10.4	8.4	8.9	10.9	7.4	100	88	96	95	0.0	1.4	0.4	0.6	10	10	10	SW 1	SW 3	SW 1
31	100.3	97.9	95.3	97.8	6.6	8.9	8.6	8.2	9.8	6.1	100	89	82	90	0.0	1.2	2.0	1.1	10 =	10	0	SW 3	SW 3	SW 6
M	102.6	102.6	102.6	102.6	7.9	13.4	10.0	10.3	14.3	6.9	92	74	85	84	0.8	4.4	1.9	2.4	6.5	6.7	4.5	2.9	4.0	2.6

Olsztyn – Dajtki

$H_s = 133$ m $H_b = 135{,}4$ m $h_w = 12$ m

Wrzesień – Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–8²⁰, ⌒ 1 0⁰⁰–10⁰⁰, 22⁰⁰–24
2	8	.	.	–	⌒ 1 0⁰⁰–11⁰⁰
3	7	.	.	–	= 2¹⁵–10³⁰, ⌒ 0 3⁰⁰–10⁰⁰ ⌒ 1 22⁰⁰–24
4	7	0.0	.	–	= 3³⁰–11⁴⁰, ⌒ 1 0⁰⁰–11⁰⁰
5	8	0.0	.	–	• 0 4⁵⁰–5³², ⌒ 0 0⁰⁰–5⁰⁰
6	7	15.8	.	–	• 0 5⁵²⁻⁵⁸ ▽ 0 16⁴⁰–17²⁰ • 0-1 17⁴⁵–19⁴⁰ ▽ 0 22¹²⁻¹⁴, (K) 16¹⁷–19⁴⁰ SW-NE, = 19⁴⁰–24
7	6	5.1	.	–	▽ 0 10³² 18⁴⁰ • 1-0 19²⁰, = 0⁰⁰–15³⁰, 19²⁰–21⁰⁰
8	7	2.4	.	–	• 0 4¹⁰–6²⁵ ▽ 0-1 10⁵⁴ 24
9	8	1.7	.	–	▽ 0 0⁰⁰ 5¹⁴, 15²⁰⁻²⁵ 17¹⁵–18¹⁰, 23⁵⁰–24, = 18⁴⁰–21³⁰
10	8	.	.	–	▽ 0 0⁰⁰⁻²⁰, 2⁵² 3¹⁰, 4⁴⁵–5¹⁵
11	7	.	.	–	⌒ 0 3⁰⁰–12⁰⁰
12	7	2.6	.	–	▽ 0 18⁵⁶–20³³, = 6²⁰–12⁴⁰ ∞ 15²⁰–18⁴⁰ =–24
13	8	0.4	.	–	▽ 0 0⁵⁰ 1⁴⁰, 6¹⁰–7⁵⁰, = 0⁰⁰–8¹⁰
14	5	15.9	.	–	▽ 0 1³⁰ 3⁴⁵ • 0 8⁴⁰–14⁴⁰ • 0 15³⁵ • 0 23³⁰–24, = 8³⁰–24
15	7	0.0	.	–	• 0-1 0⁰⁰ 7⁵⁰ ▽ 0 8⁵⁰⁻⁵⁵, 10⁴⁰–45, 13²⁷–38, = 0⁰⁰–10⁰⁰
16	7	.	.	–	• 0 4⁵⁵ 5⁴⁵, = 19³⁰–24, ⌒ 0 21⁰⁰–24
17	7	.	.	–	= 0⁰⁰–10³⁰, ⌒ 0-1 0⁰⁰–9⁰⁰ ⌒ 1 21⁰⁰–24
18	6	.	.	–	= 13¹⁵–14³⁰, ⌒ 1 0⁰⁰–11⁰⁰ ⌒ 0 20⁰⁰–24
19	7	.	.	–	= 6³⁰–8¹⁰, ⌒ 1 0⁰⁰–12⁰⁰ 21⁰⁰–24
20	8	.	.	–	= 6³⁰–7¹⁰ ≡ 0–7⁵⁰ =–8⁰⁵, ⌒ 0 21⁰⁰–24
21	8	.	.	–	⌒ 0 0⁰⁰–9⁰⁰, 21⁰⁰–24
22	8	.	.	–	= 5¹⁰–6²⁰ ≡ 0–6⁵⁴ =–8³⁰ ⌒ 1 0⁰⁰–4⁰⁰ ⌴ 1–7⁰⁰ ⌒ 1 21⁰⁰–24
23	8	.	.	–	⌒ 1 0⁰⁰ 4⁰⁰ ⌴ 0–10⁰⁰ ⌒ 0 21⁰⁰–24
24	8	.	.	–	⌒ 0 0⁰⁰ 3⁰⁰ ⌴ 0 3⁰⁰–8⁰⁰ ⌒ 1 23⁰⁰–24
25	8	0.0	.	–	• 0 18⁴⁰–19³⁷, = 7³⁰–8²⁰, ⌒ 0 0⁰⁰–3⁰⁰ ⌴ 0–9⁰⁰
26	8	.	.	–	⌒ 0 3⁰⁰–10⁰⁰ ⌒ 1 21⁰⁰–24
27	8	.	.	–	= 22⁵⁰–24, ⌒ 1 0⁰⁰–11⁰⁰, 20⁰⁰–24
28	8	.	.	–	= 0⁰⁰⁻⁴⁵ ≡ 0–8⁴⁰ =–10³⁰, ⌒ 1 0⁰⁰–6⁰⁰ ⌴ 0–9⁰⁰ ⌒ 1 22⁰⁰–24
29	7	.	.	–	= 21³⁰–24, ⌒ 1 0⁰⁰–10⁰⁰ ⌒ 0 21³⁰–24
30	7	.	.	–	= 0⁰⁰–13²⁰, ⌒ 0 0⁰⁰–11⁰⁰
31					
Σ	–	43.9	–	–	UWAGI.

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1	6	.	.	–	= 2³⁰–4⁴⁵ ≡ 0–10¹⁵ =–24, ⌒ 0 1⁰⁰–10⁰⁰ ⌒ 1 20⁰⁰–24
2	7	.	.	–	= 0⁰⁰–6²⁰ ≡ 0-1–9⁴⁵ =–12³⁰, ⌒ 1 0⁰⁰–9⁰⁰ ⌒ 0 20⁰⁰–24
3	7	.	.	–	= 1³⁰–6²⁰ ≡ 0–10⁴⁰ ⌒ 0 0⁰⁰–10⁰⁰, 22⁰⁰–24
4	7	.	.	–	= 6³⁰–8³⁰, ⌒ 0 0⁰⁰–10⁰⁰
5	7	.	.	–	⌒ 0 2⁰⁰–9⁰⁰
6	7	.	.	–	= 1³⁰–11³⁰, ⌒ 0 2⁰⁰–11⁰⁰
7	7	0.0	.	–	• 0 23³⁰–24, ⌒ 0 1⁰⁰–8⁰⁰
8	7	.	.	–	• 0 0⁰⁰⁻¹⁰, 3⁵⁶–4¹⁰
9	6	2.1	.	–	• 0 9⁴³–13²⁰, = 10³⁰–17³⁵ ≡ 0-1 24
10	7	.	.	–	≡ 1-0 0⁰⁰–6³⁵ =–11³⁰, 18⁵⁰–20⁵⁰ ≡ 0–24
11	7	.	.	–	≡ 0 0⁰⁰–7⁴⁰ =–11⁴⁰
12	6	.	.	–	= 5³⁰–13³⁰, ⌒ 0 2⁰⁰–10⁰⁰
13	8	.	.	–	≡ 0 5⁴⁰–8³⁸ =–10²⁰, ⌒ 1 1⁰⁰–10⁰⁰, 19⁰⁰–24
14	7	2.1	.	–	• 0 12⁰⁴⁻⁴⁵, 15⁵⁰–18¹⁰, = 0¹⁰–12⁵ ≡ 0–3⁴⁰ =–7³⁰, 15³⁰–21³⁰, ⌒ 1 0⁰⁰–11⁰⁰
15	7	0.0	.	–	• 0 7⁰⁵–25, 19⁵²–23³³, = 6¹⁰–10³⁰
16	7	.	.	–	= 5³⁰–7³⁰
17	5	0.0	.	–	= 2³⁰–24, ⌒ 0 1⁰⁰–9⁰⁰
18	6	2.6	.	–	• 0 0⁴⁰–1³⁰ 5²², 8¹²–18⁰², = 0⁰⁰–18³⁰
19	7	.	.	–	
20	7	.	.	–	= 6³⁰–8³⁰
21	6	.	.	–	= 12¹⁵–17³⁰
22	7	.	.	–	
23	7	.	.	–	
24	6	3.5	.	–	• 0-1 7⁴³–9⁵⁵, = 8³⁰–24
25	7	5.5	.	–	• 0 15³¹–17³⁵, = 0⁰⁰–10²⁰, ⌒ 0 1⁰⁰–9⁰⁰
26	6	1.9	.	–	• 0-1 9³⁸–11³⁵ 13⁵⁵–17²³, = 1³⁰–24, ▽ 0 23⁰⁰–24
27	7	.	.	–	= 0⁰⁰–12²⁰
28	6	.	.	–	= 6³⁰–24, ⌒ 0 1⁰⁰–10⁰⁰, 21⁰⁰–24
29	3	9.4	.	–	• 0-1 9¹⁸–13⁴⁰ • 0–22⁴⁸, = 0⁰⁰–10⁴⁰ ≡ 0-1–16³⁰ =–22⁰⁰, ⌒ 0 0⁰⁰–9⁰⁰
30	6	.	.	–	• 1 4⁵⁰–5⁵⁶, ≡ 0 1⁴⁵–6²⁰ =–24
31	6	0.5	.	–	• 0 14²⁵–15⁰, 18⁵⁵ 19⁴⁰, = 0⁰⁰–6³⁵ ≡ 0–7⁴¹ =–24, ⌒ 0 0⁰⁰–10⁰⁰
Σ	–	27.6	–	–	UWAGI.

Olsztyn – Dajtki $\varphi = 53°46'$ $\lambda = 20°25'$ Listopad – Novembre 1961

DNI	CIŚNIENIE P-m 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	97.3	98.0	98.6	98.0	8.0	8.8	9.7	9.0	9.7	7.0	97	96	92	95	0.3	0.4	0.9	0.5	10 •	10	10	SSW 5	WSW 6	WSW 5
2	103.6	103.4	97.7	101.6	7.6	9.1	7.6	8.0	9.8	7.1	91	84	84	86	0.9	1.9	1.6	1.5	4	9	0	SW 3	SW 3	S 3
3	89.5	87.3	87.5	88.2	7.4	9.9	8.8	8.7	10.3	5.5	96	77	77	83	0.5	2.8	2.6	2.0	9	9	6	S 3	SSW 6	SSW 6
4	89.7	92.7	96.2	92.9	5.5	5.5	3.2	4.4	8.8	3.1	91	74	90	85	0.8	2.3	0.8	1.3	9	9	10	SW 3	WSW 3	SW 1
5	97.3	97.4	99.9	98.3	1.9	3.2	4.2	3.4	4.3	1.7	100	98	100	99	0.0	0.2	0.0	0.1	10 •	10 •	10 •	N 1	N 6	N 4
6	101.9	102.1	100.7	101.6	4.5	6.4	8.8	7.1	8.8	4.1	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 ≡	0	NNE 3	NNE 2	E 5
7	97.0	95.5	94.2	95.6	7.8	7.7	9.2	8.5	8.8	6.5	95	96	93	94	0.8	0.5	0.8	0.7	10	10 ●	10	ESE 6	E 6	SE 3
8	93.6	95.3	92.1	93.0	6.4	7.1	6.5	6.6	9.4	6.2	98	97	100	98	0.1	0.3	0.0	0.1	10 ●	10 ●	10 ●	ESE 4	E 4	SE 2
9	90.9	91.6	91.4	91.3	5.2	5.8	5.6	5.6	6.6	4.8	95	85	94	91	0.4	1.4	0.6	0.8	10	10	0	S 2	S 4	SE 3
10	90.3	89.3	89.5	89.7	4.1	8.0	8.5	7.3	8.5	3.6	100	90	97	96	0.0	1.0	0.3	0.4	10	10	10	E 4	E 3	SE 2
11	90.6	91.9	95.3	92.6	8.8	9.1	8.2	8.6	9.4	8.1	100	92	97	96	0.0	1.0	0.3	0.4	10 =	10	10 •	SE 2	SE 5	ESE 4
12	98.1	100.1	102.3	100.2	5.5	3.5	2.0	3.2	8.3	1.7	92	93	89	91	0.7	0.5	0.8	0.7	10	10 •	10	ESE 7	E 6	E 8
13	102.6	101.8	99.8	101.4	0.4	0.1	-1.2	-0.5	2.0	-1.6	88	86	96	90	0.8	0.9	0.2	0.6	10	10	10	E 8	E 7	E 7
14	96.1	97.7	101.7	98.5	-1.8	-1.4	-1.2	-1.4	-1.0	-2.6	96	90	86	91	0.2	0.5	0.8	0.5	10	10	10	NE 5	NNE 6	N 3
15	102.3	101.5	100.1	101.3	-2.0	1.0	2.0	0.8	2.2	-2.8	96	87	87	90	0.2	0.9	0.9	0.7	10	9	9	NNE 1	SW 1	WSW 3
16	98.3	97.2	95.9	96.5	1.8	1.9	2.3	2.1	2.4	1.3	98	98	100	99	0.2	0.1	0.0	0.1	10 ●	10 ●	10	WSW 4	SW 5	SW 5
17	88.9	89.0	91.3	89.7	3.3	6.6	0.9	2.9	6.9	0.6	98	94	85	92	0.1	0.5	1.0	0.5	10 •	8	2	SW 6	W 5	W 3
18	87.6	86.9	91.4	88.6	0.6	4.2	1.4	1.9	4.8	-0.6	92	79	98	90	0.5	1.7	0.2	0.8	8	3	9	WSW 6	WSW 7	WNW 5
19	94.9	100.3	107.0	100.7	0.8	0.0	-2.4	-1.0	1.8	-4.5	100	92	93	95	0.0	0.5	0.3	0.3	10 ✳	8 ✳	9	WNW 4	N 7	NW 2
20	113.4	116.9	117.7	116.0	-4.6	0.3	[illegible]	-1.7	0.8	-5.4	93	79	84	85	0.3	1.3	0.9	0.8	3	2 ⊙	10	NW 3	N 2	SW 3
21	115.6	112.2	109.4	111.7	0.1	2.[illegible]	[illegible]	1.2	2.9	-1.4	83	79	77	80	1.1	1.5	1.5	1.4	10	9	9	SW 6	W 5	SW 5
22	106.2	105.2	103.6	105.0	1.0	[illegible]	[illegible]	-0.2	3.0	-2.8	90	81	95	89	0.7	1.5	0.2	0.8	10	3	8	W 3	W 3	C 0
23	100.9	99.1	97.4	99.1	-6.5	[illegible]	-3.0	-2.3	4.0	-7.4	97	65	88	83	0.1	2.8	0.6	1.2	0	2 ⊙	0	SW 1	S 2	SE 1
24	97.7	98.7	100.9	99.1	-4.4	1.1	1.0	-0.3	1.5	-6.4	93	85	100	92	0.3	1.1	0.0	0.5	4	7	10 =	SSW 1	SW 1	SW 1
25	100.2	98.2	96.9	98.4	1.9	2.3	1.5	1.8	2.5	0.5	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 • ≡	10 ≡	C 0	S 1	SW 1
26	95.0	95.0	92.4	94.1	0.4	0.2	0.6	0.4	1.5	-0.7	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 =	SSW 1	S 1	C 0
27	88.6	87.3	87.3	87.7	1.8	3.1	2.4	2.4	3.3	0.5	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 • =	C 0	S 1	W 1
28	90.8	94.4	98.4	94.5	1.9	4.6	-5.4	-0.1	4.9	-3.7	100	76	92	89	0.0	2.1	0.4	0.8	9 =	1	0	W 1	W 1	C 0
29	99.1	98.4	96.0	97.8	-0.8	1.6	2.4	1.4	2.4	-3.3	97	98	100	98	0.2	0.2	0.0	0.1	10	10	10 =	C 0	SE 1	S 1
30	87.1	87.5	80.7	85.1	3.2	4.1	4.7	4.2	4.6	1.0	90	90	94	91	0.8	0.8	0.5	0.7	10 •	9	10 •	S 6	WSW 5	SW 5
31																								
M	96.8	97.0	97.0	96.9	2.3	4.1	2.9	3.1	5.1	0.6	95	89	93	92	0.3	1.0	0.5	0.6	8.9	8.3	7.7	3.3	3.8	3.1

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1	71.0	75.4	79.1	75.2	7.5	6.0	3.8	5.3	8.0	3.7	93	80	90	88	0.8	1.9	0.8	1.2	10 •	8	8	SW 8	W 6	SW 6
2	76.8	72.2	73.8	73.9	3.4	10.1	6.0	6.4	11.6	3.3	98	90	71	86	0.1	1.3	2.7	1.4	10 •	10	7	SSW 2	SSW 7	WSW 9
3	87.1	88.6	89.8	88.5	3.1	4.8	1.8	2.9	6.1	1.3	81	53	80	71	1.4	4.0	1.5	2.3	9	2	3	WSW 6	SW 8	S 3
4	86.3	89.0	94.5	89.9	0.4	3.8	0.3	1.2	4.1	0.2	88	80	98	89	0.8	1.6	0.1	0.8	9	6 ⊙	0	SSW 3	W 3	SW 1
5	85.1	86.9	84.5	85.5	6.9	12.9	12.7	11.3	13.1	0.1	100	84	70	85	0.0	2.4	4.4	2.3	10 •	8	0	SSW 4	WSW 6	WSW 5
6	89.6	91.2	93.7	91.5	4.5	2.9	1.4	2.6	13.2	1.2	49	64	76	63	4.2	2.7	1.7	2.9	6	10	2	SW 5	SW 6	SW 6
7	95.7	96.5	98.6	96.9	-0.7	0.1	-0.6	-0.4	1.4	-1.0	94	92	88	91	0.4	0.5	0.7	0.5	10	10	10	SW 4	W 2	SW 2
8	98.9	98.6	99.3	98.9	-0.4	0.5	-1.4	-0.7	0.6	-2.5	80	81	90	84	1.2	1.1	0.5	0.9	10	9	0	SW 1	SW 4	SW 4
9	100.2	102.1	102.2	101.5	-0.4	1.2	-2.0	-0.8	1.4	-2.6	92	79	94	88	0.5	1.4	0.4	0.8	9	2	0	SW 6	SW 4	S 1
10	97.4	95.6	95.7	95.6	-2.5	-1.7	-0.1	-1.1	0.0	-2.6	82	94	92	89	0.9	0.3	0.5	0.6	9	10 ✳	10 •	SE 3	S 3	SSW 3
11	89.2	85.6	79.6	84.1	0.7	1.0	0.4	0.6	1.4	-0.1	100	98	100	99	0.0	0.2	0.0	0.1	10 =	10	10	SSW 2	SE 2	E 1
12	87.4	92.4	98.4	92.7	0.1	-2.1	-4.0	-2.5	0.6	-4.1	96	92	84	91	0.3	0.4	0.7	0.5	10	10	10	NNE 5	NE 4	NE 4
13	105.7	109.8	113.8	109.8	-9.8	-4.8	-7.4	-7.4	-4.0	-10.1	88	71	87	82	0.4	1.2	0.4	0.7	2	4 ⊙	0	NW 1	NNE 5	N 1
14	113.8	113.3	111.0	112.7	-9.2	-6.9	-6,7	-7.4	-6.2	-12.7	82	64	80	75	0.5	1.3	0.7	0.8	0	1	0	N 3	N 7	NE 6
15	105.9	107.1	113.7	108.9	-6.2	-10.7	-13.2	-10.0	-5.4	-15.4	84	87	84	85	0.6	0.4	0.4	0.5	10 ✳	10 ✳	0	N 7	NE 6	NE 5
16	120.4	124.4	128.1	124.3	-14.9	-13.0	-18.6	-16.3	-13.0	-20.1	82	80	84	82	0.3	0.5	0.2	0.3	0	2 ⊙	0	NNE 5	E 3	C 0
17	128.1	126.5	124.4	126.3	-12.9	-7.7	-5.4	-7.8	-5.2	-20.7	84	81	90	85	0.4	0.6	0.4	0.5	10	10	10	C 0	WNW 2	WNW 3
18	121.2	119.2	115.3	118.6	-4.2	-3.5	-0.8	-2.3	-0.6	-5.4	87	88	99	91	0.6	0.6	0.0	0.4	10	10	10	W 5	W 4	W 5
19	111.5	110.9	110.6	111.0	0.8	2.0	-0.1	0.6	2.5	-1.0	98	98	94	97	0.2	0.2	0.4	0.3	10	9	4	W 6	W 4	WNW 3
20	102.4	94.8	94.3	97.2	0.4	0.5	0.6	0.5	2.4	-0.8	90	98	82	90	0.6	0.1	1.1	0.6	10	10 ✳	9	WSW 4	W 7	N 3
21	90.1	94.9	95.9	95.6	-1.9	-5.6	-5.8	-5.3	0.8	-4.6	92	85	94	90	0.4	0.8	0.3	0.5	10 ✳	2	5	NW 7	W 5	WNW 3
22	90.1	88.0	92.2	90.1	-7.8	-5.3	-13.3	-9.9	-5.5	-13.8	87	87	84	86	0.4	0.5	0.4	0.4	2	9	0	W 5	W 2	C 0
23	95.4	95.8	98.3	96.5	-16.5	-7.5	-10.2	-11.1	-6.9	-20.0	80	95	91	88	0.3	0.2	0.3	0.3	4	9	10	C 0	C 0	C 0
24	98.9	98.9	97.7	98.5	-11.4	-9.7	-8.2	-9.4	-7.8	-12.0	90	85	92	89	0.3	0.4	0.2	0.3	0	2	10	SW 1	S 4	SW 6
25	95.7	95.4	94.3	95.1	-11.8	-10.3	-14.5	-12.8	-7.9	-14.8	86	77	83	82	0.4	0.6	0.3	0.4	2	7	0	SW 5	SW 6	SW 5
26	92.6	91.4	90.5	91.5	-19.1	-13.6	-20.4	-18.4	-12.8	-21.1	85	75	82	80	0.2	0.5	0.2	0.3	0	0	0	S 1	S 3	C 0
27	94.6	98.4	101.1	98.0	-24.0	-15.2	-17.8	-18.7	-13.3	-26.0	79	77	79	78	0.2	0.4	0.5	0.3	0	0	0	C 0	E 1	C 0
28	99.3	97.4	94.4	97.0	-16.7	-15.2	-9.6	-12.8	-9.6	-20.6	80	86	88	85	0.3	0.3	0.4	0.3	10	9	10 ✳	ESE 5	ESE 3	SE 4
29	95.0	95.4	94.3	95.6	-5.9	-3.5	-2.6	-5.6	-2.3	-9.8	89	92	95	91	0.4	0.4	0.3	0.4	10	10	10	S 3	S 3	SSE 2
30	92.6	90.8	91.8	91.7	-1.4	-0.8	0.3	-0.3	0.6	-3.2	99	99	100	99	0.1	0.0	0.0	0.0	10	10 =	10	SE 4	S 4	S 5
31	89.9	90.0	88.3	89.3	1.2	2.2	-1.4	0.2	2.7	-1.4	98	89	100	96	0.2	0.8	0.0	0.3	10	8	10 =	S 1	S 3	SE 2
M	97.0	97.1	98.0	97.4	-4.8	-2.8	-4.3	-4.0	-0.9	-7.6	87	84	88	86	0.6	0.9	0.7	0.7	7.2	7.0	5.1	3.3	4.1	3.2

Olsztyn – Dajtki

$H_s = 133$ m $H_b = 1354$ m $h_w = 12$ m

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	1.8	.	–	▽° 5⁵⁴ 9³¹ ●° 11⁶⁰ 13²⁵ ● 16⁰⁵– 17⁴², = 7³⁰– 24
2	7	1.0	.	–	●° 0⁵⁰– 1²⁰, = 0⁰⁰– 1³⁰
3	6	.	.	–	●▽° 4⁵⁰– 5⁴⁴, = 2³⁰– 4⁵⁰, 5⁴⁴– 16⁴⁰, ⌒° 0⁰⁰– 4⁵⁰
4	8	1.3	.	–	
5	6	6.5	.	–	●° 3⁵⁵ 5¹⁰– 23¹⁰, = 8³⁰– 24
6	3	0.0	.	–	●° 22⁰⁸– 23³², = 0⁰⁰– 5⁴⁵ ≡0-2 21⁴⁵
7	5	0.0	.	–	●° 9⁵²– 17³⁷, = 0⁰⁰– 24
8	5	0.4	.	–	●° 4¹⁵– 7¹², 8⁵⁰ 10¹⁰, 11⁵⁵ 13¹⁰– 24, = 0⁰⁰– 24
9	6	.	.	–	●° 0⁰⁰ 3⁰⁵, = 0⁰⁰– 24
10	6	5.5	.	–	●° 13³⁶– 17⁴⁰ 20⁵⁰– 24, = 0⁰⁰– 24, ⌒° 1⁰⁰– 10⁰⁰
11	5	4.8	.	–	●° 0⁰⁰– 3⁴⁵, 8⁰⁷ 10¹⁴ 13⁴⁹– 24, = 0⁰⁰– 6³⁵ ≡°– 7⁴⁰ =– 24
12	6	0.3	.	–	●° 0⁰⁰– 3⁴⁰ ●°– 5¹⁰, 8⁵² 9²⁰ ●° 11⁵⁰ 17²⁰ ●° 18²⁰, = 0⁰⁰– 24
13	7	.	.	–	= 0⁰⁰– 1³⁰
14	6	0.0	.	–	✱° 23⁵⁰– 24, = 6³⁰– 24
15	6	0.3	.	–	✱° 0⁰⁰– 25, = 0⁰⁰– 24
16	5	2.1	.	–	●° 1⁰⁶– 6⁴⁰ 11¹⁰– 13⁴⁰ ●°– 17²⁵ 21⁵² 24, = 0⁰⁰– 24
17	6	0.7	.	–	●° 0⁰⁰– 2⁴⁰ ●°– 6¹⁰ ●°– 8³³, 9⁵⁰ 10¹⁰ 11²⁰ ▽° 13⁰⁵. ³⁰, = 0⁰⁰– 14³⁰, ⌴ 21⁰⁰– 24
18	8	4.7	.	–	✱° 2⁵⁶– 3⁰⁵ ✱¹ 7³⁵ 8⁵⁹ ▽ 13⁵⁵– 14¹⁵, 14²⁵– 17⁴⁰, 19⁵⁰ 21¹⁰ ⌴° 0⁰⁰– 3⁰⁰
19	7	0.2	.	–	▽° 3⁵⁰– 5⁴⁵ ✱° 6⁵⁰– 7⁴⁵, 8²³– 10³⁴, 11²⁵– 12⁵⁰
20	8	.	.	–	◡ 20²⁰– 24
21	8	.	.	–	
22	7	.	.	–	= 2³⁰– 24
23	6	.	.	–	= 0⁰⁰– 3⁵⁰ 15³⁰– 24, ⌴° 0⁰⁰– 1¹⁰⁰ 19⁰⁰– 24
24	5	0.5	.	–	= 0⁰⁰– 14⁴⁵ ≡0-1 24, ⌴ 0⁰⁰– 11⁰⁰
25	3	0.7	.	–	●° 5⁵⁵ 7²⁰, 8⁵³– 9³⁵, 11⁵⁰– 18²⁰, ≡0-2 0⁰⁰– 21⁴⁰ =– 22²⁰ ≡0-2 24
26	2	.	.	–	≡2-0 0⁰⁰– 24
27	0	3.9	.	–	●° 13²⁵– 21²⁰ ●°– 24, ≡1-2 0⁰⁰– 24
28	7	.	.	–	●° 0⁰⁰– 1⁰⁶, ≡0-1 0⁰⁰– 10²⁵ =– 10³⁵, 21³⁰– 22³⁰ =– 24
29	5	1.4	.	–	●° 13⁵⁰– 17²⁰ ●° 21⁵⁴– 22²⁵, = 0⁰⁰–²⁰ =, ≡0-2 3⁵⁰– 24, ⌴1-2 0⁰⁰– 10⁰⁰
30	6	6.3	.	–	●° 6³⁵– 7⁴⁰ ✱°– 8⁵² ●° 16⁵²– 24, = 0⁰⁰– 24
31					
Σ	–	42.4	–	–	UWAGI.

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1	8	1.6	.	–	●° 0⁰⁰– 7³⁵ 8⁰³ 9⁴⁰ ▽°– 10⁰⁰, = 0⁰⁰– 9³⁰
2	6	6.0	.	–	●° 4⁴⁰– 12⁴⁰ ▽° 17⁵⁴– 18¹⁰⁵, 21⁴⁵– 22⁰⁵, = 6¹⁵– 15³⁰
3	8	.	.	–	
4	7	7.0	.	–	= 20²⁰– 24
5	8	5.0	.	–	●0-1 10⁴ 9¹⁰ ▽° 10⁵⁵– 11¹⁰, = 0⁰⁰– 9⁰⁰
6	7	.	.	–	
7	6	.	.	–	= 7³⁰– 24, ⌴° 3⁰⁰– 11⁰⁰
8	7	.	.	–	= 0⁰⁰– 1⁴⁰, ⌴° 2⁰⁰– 8⁰⁰
9	7	.	.	–	⌴° 19⁰⁰– 24
10	6	0.9	.	–	✱° 10¹⁴– 16⁵⁰ ●° 20²² 21⁰⁸, 22⁴⁰– 23⁰⁶, ⌴° 0⁰⁰– 10⁰⁰, = 10³⁰– 24
11	6	2.8	1	–	●° 7⁵³– 8²⁰ ●° 13⁰³– 15¹⁰ ✱° 19¹⁰, = 0⁰⁰– 10⁵ ≡0-1 9⁴⁰ =– 24
12	6	.	2	–	●° 1⁰⁵– 5⁵⁰, = 0⁰⁰– 7⁵⁵ ≡°– 9¹⁰ =– 20²⁰
13	8	.	2	–	
14	8	0.0	2	–	
15	4	0.5	2	–	▽✱° 5⁵⁰ 8²⁰ ✱0-2 13¹⁰, ⊹° 7⁴⁰– 13³⁰
16	7	.	5	–	= 19³⁰– 24
17	6	0.0	5	–	✱° 12⁵²– 15⁴⁰, = 0⁰⁰– 24
18	6	0.4	5	–	◡ ≈ 18⁴⁰– 24, = 0⁰⁰– 24
19	5	0.0	5	–	◉ 0⁰⁰– 3²⁰ ●° 4⁴² 10⁵¹, = 0⁰⁰ 7⁴⁰ ≡°– 11⁴⁵ =– 14³⁰, 22³⁰– 24, ≈ 0²⁰ 9²⁰
20	5	4.3	2	–	✱° 7⁴⁰– 8¹⁵ ✱° 8¹⁵– ⁴⁵ ✱0-1 9²⁵– 14⁴⁰ ●° 15⁵⁰ 17⁴⁸, = 0⁰⁰ 6¹⁵, 9²⁰– 14⁴⁵ ≡°– 15²⁵ =– 17²⁰
21	8	2.8	6	–	▽✱° 0⁵⁰– 2²⁵ 5⁵⁵ 8⁰³ ▽✱ 15⁸⁰ 19²⁰, ⩥ 7⁴⁵– 8⁰³
22	7	0.2	12	–	▽✱¹ 0⁵⁰– 1⁴⁵, ✱° 8⁰⁷–¹⁷ 9¹⁵– 12²⁰, = 17³⁰– 18⁴⁵ ≡°– 20¹⁷ =– 24, ▽° 17⁴⁰– 24
23	7	0.5	12	–	✱1-0 10³⁸– 12²⁰ ✱° 23⁵⁰– 24, = 0⁰⁰– 1³⁰, ▽° 0⁰⁰– 24
24	8	.	13	–	▽✱° 0⁰⁰– 2²⁵, = 0⁰⁰– 2²⁰, ▽° 0⁰⁰– 13⁰⁰
25	7	.	13	–	
26	6	.	13	–	= 7²⁰– 24
27	5	.	13	–	= 0⁰⁰– 24
28	5	0.0	13	–	✱° 13⁵² 17⁵⁰, 18⁴⁸– 22⁰⁶, = 0⁰⁰– 24
29	5	.	12	–	= 0⁰⁰– 24
30	3	.	12	–	= 0⁰⁰– 12⁴⁰ ≡°– 20³⁵ =– 24
31	5	.	10	–	= 0⁰⁰– 7⁵⁰ ≡°– 10⁴⁵ =– 15⁴⁰ ≡0-1 24
Σ	–	32.0	–	–	UWAGI.

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$ **Styczeń – Janvier 1961**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.0	92.7	94.0	92.6	-1.7	0.2	0.3	-0.2	0.6	-2.8	94	98	98	97	0.3	0.1	0.1	0.2	10		10 ≡	10 ≡		SSE 2	SW 4	SW 2
2	92.8	90.7	87.3	90.3	-0.2	-0.6	0.0	-0.2	0.6	-1.0	94	95	92	94	0.4	0.3	0.5	0.4	10		10	10		SSW 3	SSE 3	SSE 5
3	78.6	74.6	76.3	76.5	-0.3	0.0	1.7	0.8	1.9	-0.3	92	92	85	90	0.5	0.5	1.0	0.7	10		10	10		SE 5	SE 5	SSE 3
4	77.2	74.9	78.2	76.8	1.0	2.3	1.8	1.7	2.9	1.0	98	93	94	95	0.2	0.5	0.4	0.4	10 ≡		10	10		ESE 2	ESE 3	SW 4
5	81.5	82.4	84.7	82.9	0.0	0.8	1.1	0.8	2.0	-0.1	98	92	92	94	0.1	0.5	0.5	0.4	8		10	10 *		SSW 2	S 2	SW 5
6	89.2	89.8	87.7	88.9	1.1	2.0	0.2	0.9	2.1	0.1	94	78	86	86	0.4	1.6	0.9	1.0	10		3	8		SW 7	S 4	SSE 3
7	87.1	87.4	88.0	87.5	-0.7	0.7	0.0	0.0	1.4	-1.0	91	88	92	90	0.5	0.7	0.5	0.6	8		10	10 *		SSE 2	SSE 1	SE 1
8	88.3	87.9	85.0	87.1	0.3	0.4	0.6	0.5	0.8	0.0	96	94	98	96	0.2	0.4	0.1	0.2	10 ≡		10	10 *		SW 1	SW 3	S 4
9	84.2	86.0	87.0	85.7	1.3	1.9	1.4	1.5	2.3	0.6	98	94	92	95	0.1	0.4	0.6	0.4	10 •		10	10 •		SW 3	SW 4	S 2
10	89.1	89.8	88.5	89.1	0.5	1.1	1.0	0.9	1.7	0.5	96	90	90	92	0.2	0.6	0.7	0.5	10		10	8		WSW 3	SSW 4	SE 2
11	89.3	91.8	96.2	92.4	0.0	0.3	-1.0	-0.4	1.3	-1.1	98	94	87	93	0.1	0.3	0.8	0.4	10 △		10 *	2		SSE 3	S 1	WNW 4
12	100.8	104.7	109.1	104.9	-2.7	-1.4	-2.1	-2.1	-0.7	-4.4	84	90	83	86	0.8	0.5	0.9	0.7	2		9	10		WNW 4	NW 5	NW 3
13	108.2	104.7	103.1	105.3	-5.9	-1.6	-0.2	-1.5	0.0	-8.1	89	84	96	90	0.5	0.9	0.2	0.5	10		10	10		WSW 2	SW 5	W 5
14	103.8	106.3	110.9	107.0	0.8	1.2	0.6	0.8	1.9	-0.2	98	96	90	95	0.2	0.3	0.6	0.4	10		10 ≡	10		W 1	W 1	NNW 3
15	111.9	110.6	108.4	110.3	-1.6	-1.1	0.3	-0.5	0.8	-2.3	96	97	94	96	0.2	0.2	0.3	0.2	10		10	10 ,		W 3	WNW 6	WNW 5
16	104.8	106.0	108.3	106.4	0.7	2.1	0.4	0.9	2.9	0.3	94	91	75	87	0.4	0.6	1.6	0.9	10		8	0		NW 5	NNW 3	NE 5
17	112.1	115.1	118.4	115.2	-5.4	-5.8	-5.8	-5.2	0.8	-6.3	85	53	74	71	0.6	2.2	1.0	1.3	0		1 ⊙	0		NE 3	E 4	ENE 2
18	121.3	121.6	120.4	121.1	-10.7	-5.4	-8.0	-8.0	-4.5	-11.2	80	57	69	69	0.5	1.7	1.0	1.1	2		2	0		E 1	SE 1	SSE 1
19	116.2	114.2	112.4	114.3	-9.5	-4.7	-7.2	-7.2	-4.1	-10.0	79	52	71	67	0.6	2.0	1.0	1.2	2		7	0		SSE 1	SE 2	SE 2
20	109.2	107.7	105.3	107.4	-8.2	-0.6	-5.2	-4.8	0.3	-8.4	75	79	85	80	0.8	1.2	0.6	0.9	0		0	0		SE 3	S 2	SSE 2
21	102.6	101.8	99.8	101.4	-8.3	-4.1	-6.4	-6.3	-3.2	-8.8	89	70	89	83	0.3	1.3	0.4	0.7	0		1	8		SE 2	SE 3	SE 2
22	95.8	94.4	93.9	94.7	-7.8	-2.8	-8.0	-6.6	-1.6	-8.4	90	71	81	81	0.3	1.4	0.6	0.8	10		0	0		SSE 1	S 1	S 1
23	93.9	95.5	96.8	95.4	-8.1	-5.0	-7.8	-7.2	-4.4	-10.2	84	68	84	69	0.5	1.3	0.5	0.8	0		2	7		ENE 3	ENE 4	ENE 2
24	94.9	95.2	94.5	94.2	-6.4	-2.5	-9.4	-6.9	-2.2	-9.7	91	84	85	87	0.3	0.8	0.4	0.5	2		9 *	0		NNW 1	NW 1	NE 1
25	94.0	95.7	98.6	96.1	-10.6	-7.0	-12.4	-10.6	-6.8	-13.9	84	61	74	73	0.4	1.4	0.6	0.8	9		2	0		NE 1	ENE 3	E 1
26	102.9	105.6	108.6	105.7	-15.0	-8.0	-9.7	-10.6	-7.0	-17.6	82	75	75	77	0.3	0.8	0.7	0.6	2		1	9		S 1	SW 2	W 1
27	110.8	110.5	107.0	109.4	-12.6	-5.8	-10.1	-9.6	-5.3	-13.8	69	56	68	64	0.7	1.7	0.9	1.1	0		8	0		W 2	S 4	SSE 3
28	101.2	99.1	94.6	98.3	-10.8	-4.0	-6.7	-7.0	-5.1	-12.6	70	68	75	71	0.8	1.4	0.9	1.0	4		10	6		SSW 5	SW 5	SE 2
29	89.2	91.1	89.4	89.9	-5.4	2.5	3.4	1.0	3.9	-8.4	75	80	81	79	1.0	1.4	1.5	1.3	9		8	9		SSW 7	SW 9	SW 10
30	80.6	75.9	76.9	77.8	2.7	2.8	3.8	3.3	5.5	1.8	93	93	90	92	0.5	0.6	0.8	0.6	10 •		10 •	9		SW 14	SW 10	WSW 10
31	78.3	76.4	78.5	77.7	2.2	3.5	2.6	2.7	4.1	1.5	95	100	96	97	0.4	0.0	0.3	0.2	10		10 ≡	8		SW 5	SW 5	W 3
M	96.2	96.1	96.4	96.2	-5.8	-1.2	-2.6	-2.6	-0.2	-5.0	89	82	85	85	0.4	0.9	0.7	0.7	6.7		7.1	6.3		3.2	3.5	3.2

Luty – Février

1	78.9	75.5	73.6	76.0	0.6	2.4	0.5	1.0	4.1	0.5	98	95	98	97	0.1	0.4	0.1	0.2	10		10	10 *		SW 3	SE 3	S 2
2	70.1	69.4	69.3	69.6	1.7	2.1	0.7	1.3	2.4	0.4	85	91	88	88	1.0	0.6	0.7	0.8	10		10	8		SW 9	SW 7	SSW 2
3	71.0	73.2	77.6	73.9	-0.4	0.4	-0.2	-0.1	1.0	-1.2	96	90	92	93	0.2	0.6	0.5	0.4	10 *		10	10		S 1	W 2	WNW 6
4	81.4	81.3	80.6	81.1	-1.2	0.1	-2.8	-1.7	0.3	-3.1	91	70	91	84	0.5	1.9	0.5	1.0	10 *		5	6		W 5	W 7	C 0
5	87.9	92.6	96.2	92.2	-4.1	-0.2	-1.5	-1.8	0.5	-6.7	89	80	90	86	0.5	1.2	0.5	0.7	4		7	0		C 0	NW 3	WSW 3
6	96.3	92.8	84.9	91.3	-3.6	0.4	0.9	-0.4	1.1	-4.0	94	71	75	80	0.3	1.9	1.6	1.3	10		10	10		SSE 3	SSE 8	SSE 10
7	82.3	82.2	82.4	82.3	1.4	4.6	2.5	2.8	4.9	0.8	96	82	82	87	0.3	1.5	1.3	1.0	10		2	5		SW 4	SW 4	SSW 4
8	86.6	90.3	94.9	90.6	2.0	3.4	1.7	2.2	3.8	1.5	91	76	87	85	0.7	1.9	0.9	1.2	10		9	10		WNW 6	W 6	W 3
9	92.9	85.8	84.4	87.7	-0.7	0.4	0.9	0.4	2.0	-1.0	96	98	98	97	0.2	0.1	0.1	0.1	10 ≡		10 * ≡	10 ,		SW 4	SSE 3	SE 2
10	94.5	102.2	102.8	99.8	0.8	2.1	0.8	1.1	2.3	0.8	96	87	96	93	0.3	0.9	0.3	0.5	10 ,		10	10		NNW 5	NNW 5	SW 3
11	95.2	88.3	84.6	88.7	1.8	3.1	3.9	3.2	4.1	0.8	96	97	97	97	0.3	0.2	0.3	0.3	10 •		10 •	10		SW 6	SW 6	W 7
12	84.0	88.9	96.0	89.6	2.6	4.2	1.9	2.6	4.7	1.8	100	97	94	97	0.0	0.2	0.4	0.2	10 ≡		10	10		C 0	NW 3	NW 2
13	98.8	101.3	104.5	101.6	1.0	2.9	1.7	1.8	3.6	0.9	96	98	94	96	0.3	0.1	0.4	0.3	10		10	0		SW 2	C 0	C 0
14	105.4	105.9	104.8	105.4	0.2	0.6	1.6	1.0	2.0	0.0	94	98	98	97	0.4	0.1	0.2	0.2	10		10 • ≡	10 ≡		SSE 3	SSW 3	SSW 2
15	104.9	104.8	105.5	105.1	0.0	3.8	2.0	2.0	5.4	-0.6	100	100	96	99	0.0	0.0	0.3	0.1	10 ≡		10 ≡	10 ≡		WSW 3	SW 5	SW 3
16	108.3	111.6	113.6	111.2	3.5	3.2	3.3	3.3	5.8	1.8	100	98	100	99	0.0	0.2	0.0	0.1	10 , ≡		10	10 ,		NW 2	NNW 3	NW 3
17	113.4	114.3	112.4	113.4	3.2	4.5	1.7	2.8	6.0	1.6	93	87	94	91	0.5	1.1	0.4	0.7	10		9	0		WNW 5	WNW 6	NW 2
18	110.5	109.6	106.9	109.0	2.7	10.5	2.7	4.6	11.8	1.3	89	76	95	86	0.8	3.0	0.5	1.4	0		0	0		WNW 1	WSW 2	SW 3
19	105.7	106.9	108.3	107.0	1.5	3.8	3.4	3.0	4.5	1.4	96	98	98	97	0.3	0.1	0.1	0.2	10 ≡		10	10 ,		WNW 6	WNW 5	WNW 4
20	111.1	113.4	114.0	112.8	2.9	3.7	2.0	2.6	4.2	2.0	96	90	94	93	0.2	0.8	0.4	0.5	10		10	10		NNW 1	NW 1	W 2
21	113.4	113.4	113.3	113.4	0.7	2.0	1.6	1.5	2.3	0.7	98	98	94	97	0.1	0.2	0.4	0.2	10 , ≡		10 ≡	10		WSW 3	WSW 4	W 1
22	114.0	115.0	114.8	114.6	0.6	1.4	1.2	1.1	2.6	0.5	98	98	98	98	0.1	0.2	0.2	0.2	10 ≡		10 ≡	10 ≡		C 0	C 0	SE 2
23	113.5	112.7	110.8	112.3	0.7	0.0	-0.6	-0.1	1.8	-0.7	98	98	97	98	0.1	0.1	0.2	0.1	10 ≡		10 ≡	10 ≡		SE 1	ESE 2	SE 2
24	109.3	109.0	109.0	109.1	-1.7	-0.5	0.5	-0.3	0.7	-1.9	96	98	94	96	0.2	0.1	0.3	0.2	10 ≡		10 ≡	10		SE 2	SE 3	SE 3
25	110.2	111.9	112.3	111.5	-0.7	0.0	-1.2	-0.8	1.3	-1.2	99	98	95	97	0.0	0.1	0.4	0.2	10 ≡		10 ≡	10		SE 3	SSE 3	SE 3
26	110.9	111.3	110.0	110.7	-1.7	0.0	0.6	-0.1	3.3	-2.0	92	86	90	89	0.4	0.9	0.6	0.6	10		9	0		SE 3	S 3	SE 3
27	105.6	102.6	99.7	102.6	0.3	5.2	6.2	4.5	6.5	0.0	94	84	97	92	0.3	1.4	0.3	0.7	6		10	10 •		S 3	SW 5	W 1
28	88.4	82.3	85.9	85.5	3.4	10.2	1.3	4.2	10.5	1.4	97	88	91	92	0.3	1.4	0.6	0.8	10 •		10	10 •		NE 3	SSW 6	WNW 8
29																										
30																										
31																										
M	97.9	98.2	98.3	98.1	0.6	2.7	1.3	1.5	3.7	-0.1	95	90	95	95	0.3	0.8	0.4	0.5	9.3		9.0	7.8		3.2	3.9	3.2

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 12{,}5\,m$ **Styczeń – Janvier 1961**

DNI	WIELKOŚĆ WIATRU v	OPAD R	GRUBOŚĆ GRUBOŚCI h	USŁONECZNIENIE	POGODA
1	2	0.0	1	-	✳°0⁰⁰–1⁴⁰ 9⁵⁰–10⁴⁵, = 7³⁰–8⁴⁰ ≡⁰⁻¹–24
2	5	.	1	-	≡°0⁰⁰–2⁴⁰ ≡–8⁴⁰ ≡'–10³⁰ ≡°–10⁵⁰ =–21⁴⁵
3	6	1.9	pż.	-	✳°10³⁵–11⁵⁰ ●°–12²⁰ ✳°14⁰¹–⁰⁷ ▽°15⁵⁵–16¹⁵ ●°18⁵⁰–19⁰⁷, = 7¹⁵ 18³⁰
4	5	0.4	pż.	-	●°1⁵⁵–2¹⁵ 4⁵⁰–6⁴⁰ 14³⁰⁻⁴⁵ 16⁵⁰–18⁴⁰, = 1³⁰–6²⁵ ≡⁰⁻¹ 11⁴⁵ =–24
5	6	0.5	.	-	✳°20⁴⁰–21²⁰, = 1⁰⁰–19²⁰, 20³⁰–21²⁵, ⌴°8⁰⁰–13⁰⁰
6	7	.	pż.	-	✳°0³⁰–2⁴⁰
7	6	0.3	pż.	-	✳°20⁵⁰–21²⁰, 23⁵⁵–24, = 7³⁰–18¹⁵, ▽ 21⁵⁵–6³⁰
8	6	2.7	1	-	✳°0⁰⁰⁻⁰⁵ 3⁵⁰–4¹⁵ 7¹⁰–8²⁰ 17³⁵–23⁴⁰ ≡⁰⁻¹ 0⁵⁰–9⁴⁵ =–17⁵⁵
9	6	2.7	1	-	●°3³⁰–5²⁰ ●°–8⁴⁵ ●°11⁴⁵–12⁴⁰ ▽°20⁴⁵–21³⁰ ✳°–22⁴⁰ ✳°–23²⁰, = 1¹⁰–3³⁰ ≡°7³⁰–9¹⁵ =–14¹⁵
10	6	0.0	pż.	-	●°0⁴⁰–2¹⁵, = 0³⁰–2³⁰, 7¹⁰–19²⁰
11	6	2.5	pż.	-	△°6⁵⁰–7¹⁰ ✳⁰⁻¹ 7¹⁰ 19⁴⁵ ●°17¹⁰–18⁰⁰
12	7	0.8	2	-	✳⁰⁻¹ 0⁵⁰–1⁴⁰ ✳°7⁵⁰–8⁴⁰ 9⁰⁵–12²⁵
13	7	0.4	4	-	= 15³⁰–22⁵⁰ ≡°–24, V° 0⁵⁰–6⁵⁰
14	2	.	2	-	●°1⁰⁰–3⁴⁰, =, ≡⁰⁻¹ 0⁰⁰–22²⁰
15	5	0.1	1	-	☺°17⁵⁰–23⁴⁰ ☺°17⁴⁰–24, = 2³⁰–8¹⁵ =,≡°11²⁰–20¹⁵
16	7	.	1	-	☺°0⁰⁰–5⁰⁹, = 7⁴⁰–12¹⁵
17	7	.	pż.	-	
18	7	.	pż.	-	= 7²⁰–10³⁰
19	7	.	pż.	-	
20	7	.	.	-	= 7³⁰–9³⁰, 16³⁰–19¹⁵
21	7	.	.	-	= 8¹⁵–11⁴⁰
22	7	.	.	-	= 7¹⁵–10⁴⁰, 15³⁰–21¹⁰
23	7	0.0	.	-	
24	6	0.3	1	-	✳°2⁵⁰–3³⁵, 7⁴⁵–8⁰⁵ ✳°8²⁰–10¹⁵, 12³⁵–16⁴⁰
25	7	0.0	2	-	✳°9⁵⁰⁻⁵⁵
26	7	.	2	-	
27	7	.	2	-	
28	7	.	2	-	= 7¹⁵–10⁴⁰
29	7	2.3	1	-	≫ 20³⁰–24
30	7	9.3	.	-	●⁰⁻¹ 3⁵⁰–19⁴⁰, = 19⁴⁰–20²⁰, ≫ 0⁰⁰–15³⁰, 20²⁰–24
31	2	0.3	.	-	●°18⁵⁰–20¹⁹, = 6³⁰–8⁵⁰ ≡⁰⁻¹–19⁵⁰, ≫ 0⁰⁰–1³⁰
Σ	–	24.5	–	-	UWAGI: Stacja notowała burze w sposób niejasny, używając tylko znaku T. Uwaga niniejsza odnosi się do całego roku.

Luty – Février

1	6	2.8	.	-	●°19⁵⁰–20⁰⁵ ✳°–20¹⁵ ✳¹–22⁴⁰ = 1⁰⁰–19⁵⁰, 22⁴⁰–24
2	6	2.1	.	-	●°5⁵⁰–6³⁵ ●¹0⁴⁸–10¹⁵ ✳°10²⁸–12²⁰, = 0⁰⁰–3³⁰ P
3	6	0.4	1	-	✳°4⁴⁰–9⁴⁵ ✳°16⁴⁵ 20⁰⁵ ✳°22⁵⁰ 24, = 2³⁰–24
4	7	0.0	2	-	✳✳°0⁰⁰⁻⁵⁰ ✳°2⁴⁵ 7¹⁵, = 0⁰⁰–7³⁰, V°23⁴⁵–24
5	7	0.0	1	-	▽°14⁵⁷–15²⁰, V°0⁰⁰–9⁵⁰
6	7	.	1	-	= 6³⁰–10³⁰
7	6	1.5	pż.	-	✳✳°22⁵⁵–23⁰³, = 5³⁰–7²⁰ ≡⁰⁻¹–10⁵⁰ =–13³⁰
8	7	.	.	-	●°2⁰⁵–6¹⁰ ≫ 7²⁰–9³⁰
9	3	7.1	.	-	✳¹8⁵⁵–12⁴⁰ ✳¹–13⁵⁰ ●°*⁰⁻²15²⁰ ●⁰⁻¹–24, = 3¹⁰–6⁴⁵ ≡⁰⁻¹–12⁵⁵
10	7	0.4	2	-	●°0⁰⁰–8¹⁰ ✳°23⁵⁵–24, ≡°3⁵⁰–5⁴⁰ = 8¹⁰–12³⁰ 22²⁰–23⁵⁵
11	5	3.6	.	-	✳°0⁰⁰⁻⁴⁰ ●°5⁵⁰–11²⁰, 12¹⁵–20⁴⁵ ●¹22⁵⁰–23⁴⁰ = 0⁴⁰–3¹⁵ 20⁴⁵–24
12	6	0.5	.	-	●°8⁴⁸–9⁴⁰ 21⁴⁵–24, = 0⁰⁰–1¹⁵ 2⁴⁰–5³⁰ ≡⁰⁻²–11⁴⁰ =–15¹⁵, 21³⁰–24
13	5	0.0	.	-	●°0⁰⁰ 1⁴⁵ ●°11⁵⁰–12⁴⁰, = 0⁰⁰–8³⁵ ≡⁰⁻²–10³⁰ =–20¹⁰ =,≡¹ np
14	3	0.3	.	-	●°11⁴⁸–15⁴⁵ ≡⁰⁻¹ 0⁰⁰–3⁵⁰ =–10⁵⁰ ≡²–24
15	2	0.2	.	-	≡⁰⁻² 0⁰⁰–11⁴⁵ =–12³⁵ ≡⁰⁻²–21⁴⁰ =–24
16	5	0.0	.	-	●⁰⁻² 2²⁸–4⁴⁵ ●¹6³⁰–7⁴⁰ ●°19⁴⁰–24, = 0⁰⁰–5⁵⁰ ≡⁰⁻¹ 11⁵⁰ =°–19⁴⁰
17	6	.	.	-	●°0⁰⁰⁻¹⁰ ●°2⁵⁰–3³⁵ ●°–5³⁵, = 8³⁰–13³⁰ 21³⁰–24
18	6	.	.	-	= 0⁰⁰–24
19	6	0.3	.	-	●°8¹⁰–12²⁰, 15⁵⁰–24, = 0⁰⁰–2⁵⁰ ≡°–9⁵⁰ =–24
20	7	0.0	.	-	●°0⁰⁰–2²⁰, = 0⁰⁰–10¹⁵, 20¹⁰–24
21	3	0.1	.	-	●°6⁴⁸–10⁵⁰ = 0⁰⁰⁻⁵⁰ ≡⁰⁻¹–13⁴⁰ =–22⁴⁵ ≡°–24
22	3	0.0	.	-	≡⁰⁻¹ 1⁰⁰–14²⁰ =–19⁵⁰ ≡°–20¹⁵ ≡¹–24
23	1	0.0	.	-	●°3⁵⁵–6¹⁰ 17³⁰–19³⁰ 22²⁰–23²⁰, ≡²0⁰⁰–24
24	3	.	.	-	≡⁰⁻² 0⁰⁰–13¹⁵ =–24
25	1	.	.	-	= 0⁰⁰–1⁴⁰ ≡⁰⁻²–15⁴⁵ =–21¹⁵
26	6	.	.	-	= 6³⁰–24
27	6	7.6	.	-	●°9⁵⁰ 10¹⁵ 14³⁵–15⁴⁵ 19⁵⁰–21³⁰, = 0⁰⁰–24
28	7	8.7	.	-	●⁰⁻¹ 0⁴⁰–11³⁵, 13⁴⁵–15⁵⁰, 16³⁰–17⁵⁵, 20⁴⁰–24
29					
30					
31					
Σ	–	55.8	–	-	UWAGI:

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$ **Marzec – Mars 1961**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	-	-	-	-	2.0	4.0	1.9	2.4	4.2	1.5	94	85	82	86	0.4	1.5	1.3	1.0	10 •	10	9	WNW 6	NW 5	WNW 7
2	-	-	-	-	2.2	4.3	2.7	3.0	4.7	1.3	93	74	89	85	0.6	2.2	0.8	1.2	10	8 ⊙	10	W 4	NW 6	W 1
3	-	-	-	-	2.5	5.9	4.9	4.6	6.4	2.1	100	94	97	97	0.0	0.6	0.3	0.3	10 ≡	10	10 ≡	SW 1	W 3	W 2
4	-	-	-	-	3.1	7.4	4.5	4.9	9.1	3.0	97	75	81	84	0.2	2.6	1.6	1.5	10	6	10	W 2	WSW 3	WSW 5
5	-	-	-	-	4.4	5.9	2.5	3.8	6.1	2.3	93	79	89	87	0.6	2.0	0.8	1.1	10	10	10	NW 7	NW 6	NW 4
6	-	-	-	-	2.6	6.4	5.1	4.8	7.0	1.9	100	91	89	93	0.0	0.9	1.0	0.6	10 ≡	10	9	WNW 4	NW 5	WNW 8
7	-	-	-	-	3.0	11.5	3.5	5.4	11.5	3.0	93	59	97	83	0.6	5.7	0.2	2.2	9	5 ⊙	10	W 1	NW 9	NW 4
8	-	-	-	-	2.5	9.5	6.1	6.0	11.4	2.2	98	65	89	84	0.1	4.2	1.0	1.8	10 ≡	6	6	NW 4	WNW 6	NW 5
9	-	-	-	-	4.3	12.2	8.2	8.2	13.3	4.2	92	68	77	79	0.7	4.5	2.6	2.6	10	10	0	NW 5	NW 8	NW 7
10	-	-	-	-	4.9	15.8	8.4	9.4	16.5	3.6	94	36	69	66	0.6	11.4	3.4	5.1	3	1	0	WNW 1	WSW 4	C 0
11	-	-	-	-	3.6	8.1	5.0	5.4	8.6	3.5	91	85	90	89	0.7	1.6	0.8	1.0	4 ⊙	10	7	WSW 4	WNW 7	W 5
12	-	-	-	-	5.0	9.4	8.8	8.0	11.8	3.1	89	76	90	85	1.0	2.8	1.1	1.6	10	10	10 •	W 7	WSW 12	W 10
13	-	-	-	-	3.5	6.6	2.2	3.6	8.8	2.0	80	54	75	70	1.5	4.5	1.8	2.6	6 ⊙	7 ⊙	0	NW 10	NW 9	NW 4
14	-	-	-	-	2.0	6.2	7.4	5.8	7.5	0.8	84	94	97	92	1.2	0.6	0.3	0.7	10	10 •	10 •	C 0	WSW 3	NW 5
15	-	-	-	-	6.7	9.4	6.0	7.0	10.4	5.7	81	66	83	77	1.9	4.0	1.6	2.5	9	5	0	NW 12	NW 12	NW 5
16	-	-	-	-	6.5	9.9	5.6	6.9	10.9	5.3	85	56	81	74	1.5	5.4	1.7	2.9	10	8	0	WNW 12	WNW 16	NW 7
17	-	-	-	-	4.4	12.8	7.4	8.0	14.1	2.9	92	63	90	82	0.7	5.6	1.0	2.4	10	7	2	NW 5	WNW 9	SW 3
18	-	-	-	-	7.6	10.2	4.6	6.8	10.8	4.6	82	46	60	63	1.9	6.7	3.4	4.0	8	1	0	WSW 8	WNW 10	W 9
19	-	-	-	-	1.8	1.1	-2.3	-0.4	4.8	-2.3	91	81	96	89	0.7	1.2	0.3	0.7	10	9 *	0	WNW 8	NW 10	NW 3
20	-	-	-	-	-4.4	3.3	-0.3	-0.4	4.2	-5.2	86	63	96	82	0.6	2.8	0.3	1.2	0	7 ⊙	10 *	WSW 1	WSW 8	SW 9
21	-	-	-	-	0.2	1.3	0.4	0.6	2.9	-0.3	96	92	92	93	0.3	0.5	0.5	0.4	10	10	10	SW 4	W 2	N 6
22	-	-	-	-	-2.6	0.9	-0.2	-0.5	2.9	-3.4	91	64	96	84	0.5	2.3	0.2	1.0	9 *	8	10 *	NW 5	NW 6	SW 4
23	-	-	-	-	4.1	6.1	6.1	5.6	6.8	-0.3	95	91	77	88	0.4	0.8	2.1	1.1	9 •	10	10	W 5	WNW 7	WNW 9
24	-	-	-	-	5.6	8.4	7.2	7.1	9.5	5.0	85	65	81	77	1.4	3.8	2.0	2.4	10	9	9	W 9	WNW 14	NW 10
25	-	-	-	-	5.5	6.7	4.7	5.4	8.7	4.3	92	75	92	86	0.7	2.4	0.7	1.3	10 •	10	10	WNW 6	NW 5	W 3
26	-	-	-	-	6.0	10.0	6.0	7.0	10.7	3.6	91	60	89	80	0.9	5.0	1.1	2.3	10	10	10 •	WSW 5	WSW 12	W 12
27	-	-	-	-	1.5	4.1	-0.8	1.0	6.1	-0.9	87	74	93	85	0.9	2.2	0.4	1.2	10 *	9 *	8 *	W 16	W 16	NW 5
28	-	-	-	-	-0.6	2.6	1.0	1.0	4.0	-2.2	93	81	81	85	0.4	1.5	1.3	1.1	8 *	9	1	W 8	WNW 8	W 5
29	-	-	-	-	0.3	3.7	5.5	3.8	6.1	-0.7	94	98	94	95	0.3	0.2	0.5	0.3	10 *	10 ,	10 •	SW 2	W 3	W 7
30	-	-	-	-	6.6	7.2	1.2	4.0	7.6	1.2	96	44	92	77	0.4	5.7	0.5	2.2	10 •	10	10 *	SW 10	WNW 12	NW 2
31	-	-	-	-	0.0	5.3	0.0	1.3	5.9	-0.1	88	51	98	79	0.7	4.3	0.1	1.7	10	8	10 *	NW 4	W 5	W 8
M	-	-	-	-	3.1	7.0	4.0	4.5	8.2	1.7	91	71	87	83	0.7	3.2	1.1	1.7	8.9	8.2	6.8	5.7	7.8	5.6

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1	-	-	-	-	-1.6	-1.5	-0.6	-1.1	1.0	-1.9	88	96	91	92	0.6	0.2	0.5	0.4	8	10 *	10	W 5	SW 5	SE 1
2	-	-	-	-	-1.2	3.3	2.4	1.7	4.5	-2.0	89	55	72	72	0.6	3.5	2.1	2.1	8	9	10	NNW 2	C 0	NW 1
3	-	-	-	-	-0.1	1.7	0.6	0.7	2.5	-0.1	96	90	96	94	0.3	0.6	0.3	0.4	10 *	10	8	E 3	SE 2	SW 3
4	-	-	-	-	0.6	6.2	0.6	2.0	7.3	0.4	98	59	88	82	0.1	3.9	0.8	1.6	10 *	6	5	SW 2	W 10	WNW 1
5	-	-	-	-	1.2	5.2	9.9	6.6	10.4	0.1	92	92	96	93	0.5	0.7	0.5	0.6	10 *	10	10	SE 2	ESE 4	S 2
6	-	-	-	-	9.0	18.3	15.1	14.4	19.8	8.0	95	47	73	72	0.7	11.1	4.6	5.5	10	1	0	SW 1	WSW 6	S 1
7	-	-	-	-	12.6	19.0	11.0	13.4	22.0	10.6	74	61	92	76	3.7	8.7	1.0	4.5	7	8	10	SW 4	SW 5	NW 4
8	-	-	-	-	6.7	5.6	2.1	4.1	11.2	2.1	97	85	91	91	0.3	1.4	0.6	0.8	10	10 •	0	NW 3	NW 2	WNW 3
9	-	-	-	-	2.4	6.4	0.9	2.6	7.0	0.8	68	41	58	56	2.4	5.6	2.7	3.6	8	5	0	NW 10	NW 9	NW 1
10	-	-	-	-	-0.6	8.1	3.6	3.7	9.0	-2.0	85	56	55	59	0.9	6.9	3.5	3.8	9	4 ⊙	0	NW 1	E 2	SE 1
11	-	-	-	-	1.0	10.7	3.7	4.8	12.0	-1.0	64	38	59	54	2.4	8.0	3.3	4.6	0 ⊙	3 ⊙	2	E 2	SE 1	NE 2
12	-	-	-	-	2.7	10.6	7.0	6.8	12.4	-1.3	72	33	59	55	2.1	8.5	4.1	4.9	3 ⊙	2 ⊙	3	E 1	SE 2	S 2
13	-	-	-	-	7.5	18.8	12.5	12.8	19.6	5.9	79	49	71	66	2.2	11.2	4.2	5.9	9	6 ⊙	0	SW 3	W 6	C 0
14	-	-	-	-	10.1	22.2	15.8	16.0	23.2	8.9	79	47	49	58	2.6	14.3	9.1	8.7	0 ⊙	1 ⊙	0	E 1	SSE 3	SE 2
15	-	-	-	-	10.5	18.8	10.6	12.6	20.0	8.3	91	48	84	74	1.1	11.3	2.1	4.8	0 ⊙	4 ⊙	9	NW 3	NW 3	NE 1
16	-	-	-	-	6.3	11.6	8.6	8.8	14.7	6.0	97	79	82	86	0.2	2.8	2.0	1.7	10 ≡	9	10	NE 3	NE 4	NE 4
17	-	-	-	-	7.3	15.4	11.9	11.6	16.2	5.6	88	64	90	81	1.2	6.4	1.3	3.0	8	10	10 •	NE 2	SSE 4	C 0
18	-	-	-	-	10.5	11.0	8.2	9.5	12.8	8.1	97	89	94	93	0.3	1.5	0.6	0.8	10	10	0	NW 1	WNW 3	C 0
19	-	-	-	-	4.5	13.9	5.1	7.2	15.9	2.4	84	42	60	62	1.3	9.3	3.6	4.7	0 ⊙	2 ⊙	0	NW 3	NNW 3	NE 4
20	-	-	-	-	4.6	10.6	2.3	5.0	10.8	0.8	47	34	59	47	4.5	8.4	2.9	5.3	0 ⊙	1 ⊙	0	NE 5	NE 3	ENE 2
21	-	-	-	-	3.4	12.7	8.6	8.3	13.7	-0.6	57	28	47	44	3.4	10.5	5.9	6.6	0 ⊙	0 ⊙	0	E 4	SE 6	ESE 4
22	-	-	-	-	5.2	17.9	12.6	12.1	19.8	3.3	63	40	56	53	3.2	12.2	6.5	7.3	0 ⊙	1 ⊙	0	ESE 3	SE 5	E 2
23	-	-	-	-	8.6	18.4	13.0	13.2	19.2	7.0	74	37	52	54	2.9	13.3	7.2	7.8	0 ⊙	7 ⊙	0	ESE 3	SE 6	E 3
24	-	-	-	-	8.4	17.3	12.3	12.6	17.6	5.1	58	39	60	52	4.6	11.9	5.8	7.4	0 ⊙	0 ⊙	3	E 5	SE 7	ESE 3
25	-	-	-	-	8.3	11.5	11.0	10.4	12.2	6.3	69	56	67	64	3.5	6.0	4.3	4.6	0 ⊙	10	10	E 5	E 8	ESE 3
26	-	-	-	-	8.6	15.6	11.2	11.6	16.7	5.6	64	40	77	60	4.1	10.7	3.1	6.0	0 ⊙	10	10	ESE 3	ESE 6	E 3
27	-	-	-	-	10.1	18.2	11.5	12.8	18.9	8.1	92	51	82	75	1.0	10.2	2.5	4.6	4	9	6	E 2	E 5	E 2
28	-	-	-	-	10.9	18.8	9.4	12.1	20.0	5.3	70	39	79	63	3.8	13.3	2.5	6.5	2	4 ⊙	10	E 1	SE 3	NE 2
29	-	-	-	-	5.6	13.2	7.4	8.4	13.9	5.1	67	51	61	60	2.9	7.5	4.0	4.8	8 ⊙	8 ⊙	0	ENE 5	ESE 5	E 1
30	-	-	-	-	6.7	17.1	9.7	10.8	18.3	3.4	67	43	58	56	3.3	11.1	5.0	6.5	3	0	8	NE 1	E 3	NE 2
31																								
M	-	-	-	-	5.7	12.6	7.9	8.5	14.1	3.6	79	54	72	68	2.0	7.7	3.2	4.3	4.9	5.7	4.5	3.0	4.4	2.0

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 12{,}5\,m$ **Marzec – Mars 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBIENIE GU h	USŁONECZNIENIE	POGODA
1	7	0.1	.	–	●° 0⁰⁰–2⁵⁵, 4⁰⁰–8⁴⁰
2	7	0.3	.	–	= 5³⁰–7³⁰
3	6	0.2	.	–	●° 0⁵⁵–2⁴⁵ ●16⁵⁰–8⁴⁰ ●° 16⁴⁵–18⁴⁰, =, ≡0-2 2⁴⁵–24
4	7	0.0	.	–	≡1-0 10⁰–6⁴⁰ =–10³⁰
5	7	.	.	–	●° 5⁵⁰–6⁴⁰, = 5¹⁵–8¹⁰
6	6	.	.	–	= 4²⁰–5⁵⁰ ≡°–7⁴⁰ =–15³⁰
7	7	.	.	–	= 3¹⁵–12²⁰, 20²⁰–22⁴⁵ ≡°–24
8	7	.	.	–	≡° 10⁰–7⁴⁰ =–10³⁰
9	7	.	.	–	= 16¹⁵–19³⁰
10	7	.	.	–	= 5¹⁵–12²⁰
11	6	0.2	.	–	▽° 14²⁰–35 ●° 15¹⁵–17²⁰, = 6¹⁰–22³⁰
12	7	3.0	.	–	●° 7⁰⁵–9⁴⁰ ▽° 19⁵⁰–21⁴⁰ ●°–23³⁵, = 8¹⁰–12²⁰, ≫ 8³⁰–16¹⁵, 19²⁰–24
13	7	.	.	–	≫ 0⁰⁰–7⁴⁵
14	6	1.1	.	–	●° 7²⁵–19¹⁰..24, ≫ 23²⁰–24
15	7	.	.	–	●° 0⁰⁰..50, ≫ 0⁰⁰–1³⁰, 2⁴⁰–17³⁰
16	7	.	.	–	≫–≋ 2³⁰–19²⁰
17	7	.	.	–	
18	8	0.0	.	–	= 5³⁰–9³⁰, ≫ 9²⁰–18⁴⁰
19	6	0.0	.	–	●°5⁵⁰–6⁴⁵ ✳° 8¹⁰–13⁰³ ⛬° 13¹⁰..15⁰² ✳0-1 17⁵⁰–18⁰⁵, ⌴° 21⁰⁰–24
20	7	2.2	.	–	✳1 20⁰⁸–22¹⁰ ✳°–24, ≫ 22⁰⁰–24, ⌴1 0⁰⁰–9¹⁰
21	7	1.0	3	–	✳° 0⁰⁰–6⁴⁰, 7⁵⁵–8⁴⁰, 14⁵⁰–15¹², 17⁵²–18⁰⁰ ✳1 22⁴³–24, = 6⁰⁰–7⁵⁵, ≫ 0⁰⁰–2³⁰
22	7	0.7	1	–	✳1 0⁰⁰–15, 6⁴⁸–7⁰⁰, 12²⁰–25 ✳° 17⁴⁰–21²⁰ ●°–22⁰⁵ ●° 23⁰⁵–24
23	7	0.2	pł.	–	●° 0⁰⁰–50, 1³⁰–3⁴⁰ ▽° 6⁴⁵–55 7¹⁰–45, ≡° 0⁵⁰–5⁴⁵ =–6⁴⁰, ≫ p, np
24	7	1.0	,	–	▽° 9¹⁰–35 17⁵⁰–19³⁰, ≫ 0⁰⁰–4⁵⁰, 7³⁰–21⁰⁰
25	7	0.0	.	–	●° 5⁵⁰–8³⁵
26	7	2.1	.	–	▽° 16⁵⁰–17³⁰ ●°..18²⁰–23⁴⁰, = 5²⁰–8¹⁰, ≫ 10¹⁰–24
27	6	3.4	.	–	▽° 5⁵⁰–6¹⁰ ▽° ●, ✳°..9²⁵ ✳0-1 10⁰⁴ 23²⁰, ≫–≋ 0⁰⁰–20⁰⁰ ≫ 22⁰⁰–24
28	7	2.1	1	–	✳0-1 0⁴⁰–2¹⁵, 6⁴⁵–8⁵⁰ ●° 9⁴⁰–10²⁵ 10⁵⁰–12¹⁰ ●1 ✳ 14²⁵–15⁴⁰, ≫ 0⁰⁰–3³⁰, a
29	6	4.7	2	–	✳° 4⁴⁸ 7⁴⁰, 7⁴⁵–8³⁵ ●°–9³⁰ ●° 13⁴⁵–18⁵⁰, 19⁰⁰–24, = 10²⁰–13⁴⁵, p, ≫ 23⁴⁵–24
30	7	2.6	.	–	●° 1⁵⁰–2¹², 4⁵³–7⁴⁰ 17⁴⁵–20³⁰ ●°–21⁴⁰ ✳°–23⁴⁰, ≫ 0⁰⁰–15³⁰
31	7	0.7	.	–	⛬° 10⁵³–11⁰⁰ ✳2 ▽ 20⁴⁵–21⁰⁵ ✳° 21⁵⁰–24, ≫ 22⁴⁰–24, ⌴° 4⁰⁰–9⁰⁰
Σ	–	25.6	–	–	UWAGI.

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1	4	3.2	1	–	⛬° 0⁰⁰–1²⁰ ●°–3⁴⁰ ✳1 11⁴⁷–12¹⁵ ✳2-0 17⁵⁰, ≫–≋ 0⁰⁰–5³⁰
2	7	1.6	1	–	
3	7	2.7	2	–	✳0-1 14⁸–10⁵⁰
4	7	0.4	1	–	●° 1⁵⁰–3³⁵ ✳°–4¹⁵ ✳0-1 8⁴⁰ ●°–9⁵⁵ ✳°–10⁰³ ●°–10¹⁰, ≫ 12³⁰–15⁴⁰
5	6	2.1	1	–	✳° 6²⁰–8³⁵ ●°–10⁵⁰
6	7	.	.	–	●° 0⁰⁰–1⁴⁵, = 0⁰⁰–2⁴⁵
7	7	1.5	.	–	▽° 17⁴⁵–18¹⁰ 21⁵⁵–22⁰⁵ 23⁴⁵–24, (↖) 17⁴⁵–18³⁰ W-E
8	6	2.6	.	–	▽° 0⁰⁰–10 ●° 7¹⁰–25 ▽° 11⁴⁵–56, = 5²⁰–14⁵⁰
9	7	.	.	–	≫ 6⁰⁰–11³⁰
10	7	.	.	–	⌴° 0⁰⁰–8⁰⁰
11	7	.	.	–	⌴° 2⁰⁰–7⁰⁰,
12	7	.	.	–	⌴1 3⁰⁰–7⁰⁰
13	7	.	.	–	= 7²⁰–9³⁰
14	6	.	.	–	= 7¹⁵–14³⁰
15	7	.	.	–	= 6¹⁰–8⁵⁰
16	7	0.4	.	–	▽° 8²⁰ 9¹⁰ 10⁴⁵–55 11⁰⁵–10, 11⁵⁵–12⁰⁵, = 1⁰⁰–2³⁰ ≡°–7⁴⁵ =–9³⁰
17	7	5.0	.	–	▽° 14⁴⁵–15⁰⁵ ▽1 20³⁰–21⁴⁰
18	7	.	.	–	▽1 1⁴⁰–2²⁰ ▽° –3¹⁰, = 3¹⁰–12²⁰, ⌓1-2 19⁰⁰–24
19	8	.	.	–	⌓2 0⁰⁰–8⁰⁰
20	8	.	.	–	
21	8	.	.	–	
22	7	.	.	–	
23	7	.	.	–	
24	7	.	.	–	
25	7	.	.	–	
26	7	0.0	.	–	●° 14⁵²–55 14⁵⁸–15⁰⁷, 18⁴⁸–55, 18⁵⁸–19⁰³
27	7	0.8	.	–	▽ 15²⁵–50
28	8	5.6	.	–	▽0-2 14³⁷–17²⁰ ▽° 18⁵⁰–19¹⁵, 22⁵⁰–24, = 1³⁰–7³⁰, ⌓1 0⁰⁰–7⁰⁰
29	7	.	.	–	▽° 0⁰⁰–35
30	8	.	.	–	
31					
Σ	–	25.9	–	–	UWAGI.

Chojnice $\varphi = 53°42'$ $\lambda = 17°33'$ Maj - Mai 1961

DNI	CIŚNIENIE P= 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	-	-	-	-	8.1	14.8	7.6	9.5	15.9	6.4	82	61	66	70	2.0	6.5	3.5	4.0	5	10	8	NE 1	NE 3	NE 2
2	-	-	-	-	6.3	16.6	12.0	11.7	18.1	0.6	78	36	77	64	2.1	12.2	3.2	5.8	2 ⊙	5 ⊙	6	NE 1	SSE 3	SSW 1
3	-	-	-	-	9.8	16.9	9.3	11.3	18.2	8.6	96	56	96	83	0.5	8.4	0.5	3.1	9 ▬	9	0	SE 3	S 5	C 0
4	-	-	-	-	9.7	15.5	11.6	12.1	17.4	5.1	91	49	78	73	1.1	9.0	2.9	4.3	4	8	2	C 0	W 2	E 1
5	-	-	-	-	12.0	19.2	15.2	15.4	20.7	8.1	73	50	89	71	3.8	11.1	1.9	5.6	8	9	10	SE 3	SSE 6	SSE 3
6	-	-	-	-	13.4	13.5	10.4	11.9	16.1	10.4	95	88	86	90	0.7	1.8	1.8	1.4	10 ●	10 ●	1	NW 1	W 3	W 1
7	-	-	-	-	10.3	15.0	8.9	10.8	15.5	8.3	100	80	93	91	0.0	3.4	0.8	1.4	10 ▬	10	10 ●	SW 3	SW 7	W 5
8	-	-	-	-	7.9	10.5	7.1	8.2	11.3	6.4	87	74	84	82	1.3	3.3	1.6	2.1	8	7 ⊙	3	W 5	W 7	WSW 3
9	-	-	-	-	7.4	10.0	7.3	8.0	11.3	6.4	93	82	91	89	0.8	2.2	0.9	1.3	10	9	8	SW 3	WSW 3	WNW 4
10	-	-	-	-	6.4	7.2	6.1	6.4	8.4	5.4	89	88	94	90	1.0	1.2	0.6	0.9	10	10	10	NW 5	NW 8	NW 7
11	-	-	-	-	6.3	8.3	5.3	6.3	10.3	5.0	82	89	78	83	1.7	1.3	1.9	1.6	10	10	1	N 6	N 6	N 2
12	-	-	-	-	6.6	10.4	5.5	7.0	12.2	3.1	84	59	84	76	1.5	5.1	1.4	2.7	10	8	5	C 0	NNW 3	N 2
13	-	-	-	-	5.3	9.6	7.4	7.4	12.4	0.9	84	84	84	84	1.4	1.9	1.6	1.6	6	10 ●	9 ●	SW 4	SW 7	W 5
14	-	-	-	-	7.5	9.8	7.4	8.0	12.4	5.8	82	69	91	81	2.0	3.7	0.9	2.2	6 ⊙	9	10	WSW 6	SW 8	SW 4
15	-	-	-	-	6.3	7.6	6.2	6.6	9.1	6.0	91	89	89	90	0.8	1.2	1.0	1.0	10	10	10	N 4	N 7	N 4
16	-	-	-	-	7.3	8.4	8.0	7.9	9.8	5.9	88	96	87	90	1.2	0.4	1.3	1.0	10	10 ●	3	NW 4	N 4	NE 2
17	-	-	-	-	7.1	13.2	7.8	9.0	13.3	5.5	96	66	87	83	0.5	5.1	1.4	2.3	10 ●	8	9	N 3	N 6	N 3
18	-	-	-	-	8.0	16.2	10.2	11.2	17.4	3.2	83	51	76	70	1.8	9.1	3.0	4.6	4 ⊙	6 ⊙	2	NW 5	NW 4	N 1
19	-	-	-	-	9.6	17.1	10.5	11.9	18.2	6.3	89	40	75	68	1.3	11.7	3.2	5.4	8 ⊙	5 ⊙	9	SW 2	WSW 6	W 2
20	-	-	-	-	9.8	12.0	9.8	10.4	12.7	6.9	83	68	87	79	2.0	4.4	1.6	2.7	9	10	10	WSW 4	WSW 4	C 0
21	-	-	-	-	9.8	18.0	9.6	11.8	18.5	5.6	90	55	80	75	1.3	9.2	2.4	4.3	10	6 ⊙	3	NE 1	NE 4	NE 2
22	-	-	-	-	7.8	14.8	11.0	11.2	16.2	3.6	79	47	73	66	2.2	8.8	3.5	4.8	2 ⊙	9	1	NE 4	NNW 3	C 0
23	-	-	-	-	8.6	16.2	9.0	10.7	16.9	3.8	74	43	86	68	2.9	10.4	1.6	5.0	2 ⊙	8	6	S 1	SW 5	NW 2
24	-	-	-	-	9.5	11.8	8.6	9.6	15.9	8.6	84	65	88	79	1.9	4.9	1.4	2.7	10	10	1	W 4	W 6	WNW 1
25	-	-	-	-	10.0	15.8	11.9	12.4	17.3	4.8	81	52	69	67	2.4	8.6	4.3	5.1	7 ⊙	9	9	WSW 2	WNW 5	N 1
26	-	-	-	-	9.4	18.5	14.2	14.1	20.2	6.4	71	40	55	55	3.4	12.8	7.3	7.8	8	2 ⊙	3	NNW 1	S 1	E 1
27	-	-	-	-	13.6	14.2	8.9	11.4	18.1	8.8	71	74	85	77	4.5	4.3	1.7	3.5	9	10	6	S 3	NW 8	NE 3
28	-	-	-	-	9.1	13.3	7.6	9.4	14.6	7.6	83	64	93	80	2.0	5.5	0.7	2.7	10	10	10	N 2	N 5	NNW 3
29	-	-	-	-	8.3	13.2	12.4	11.6	16.3	7.3	93	78	88	86	0.8	3.3	1.7	1.9	10	10	10	NNE 1	NE 3	NE 5
30	-	-	-	-	17.2	22.1	10.9	15.3	24.9	10.9	76	68	83	76	4.7	8.6	2.2	5.2	0 ⊙	9	10	ENE 4	S 5	SSW 5
31	-	-	-	-	10.7	15.2	11.9	12.4	16.6	8.4	76	61	80	72	3.1	6.7	2.8	4.2	6 ⊙	9	2	S 3	SSW 5	SE 1
M	-	-	-	-	9.0	13.7	9.3	10.4	15.4	6.1	85	65	83	78	1.8	6.0	2.1	3.3	7.5	8.5	6.0	2.9	4.9	3.4

Czerwiec - Juin

1	84.5	84.1	83.9	84.2	14.7	22.8	17.9	18.3	24.4	8.7	69	43	57	56	5.2	15.7	8.9	9.9	6 ⊙	6 ⊙	0	ESE 2	SE 5	C 0
2	84.2	84.6	85.8	84.9	19.4	27.3	20.4	21.9	27.9	12.8	65	35	65	55	7.8	23.6	8.5	13.3	0 ⊙	5 ⊙	4	E 2	SE 6	NE 1
3	87.8	88.4	90.9	89.0	18.5	25.9	19.8	21.0	27.2	14.0	78	45	69	64	4.7	18.4	7.1	10.1	1 ⊙	9	1	NE 1	NE 2	NE 1
4	91.6	91.6	93.1	92.1	19.3	23.6	19.6	20.5	27.0	12.7	79	56	71	69	4.6	12.7	6.5	7.9	0	9 ☈	10	NE 2	E 6	NE 3
5	95.8	95.7	96.5	96.0	20.1	26.5	17.0	20.2	26.8	14.1	67	42	86	65	7.8	20.1	2.8	10.2	8 ⊙	8 ⊙	8	NE 3	SE 6	N 3
6	96.4	95.0	95.5	95.0	19.2	25.7	19.8	21.1	26.1	14.6	66	33	62	54	7.5	22.1	8.7	12.8	0 ⊙	1 ⊙	1	E 2	ESE 5	E 2
7	91.7	89.9	87.2	89.6	15.8	21.5	14.5	16.6	22.3	14.3	91	72	97	87	1.5	7.1	0.6	3.1	10	9	10 ● ☈	E 5	E 5	NE 5
8	87.4	88.0	91.0	88.8	16.1	22.7	15.1	17.2	23.6	14.2	96	67	92	85	0.8	9.2	1.4	3.8	10	6	10	S 2	WSW 4	NW 1
9	92.2	93.0	92.1	92.4	15.3	22.2	18.4	18.6	23.3	11.1	89	57	72	73	1.9	11.6	5.9	6.5	2 ⊙	5 ⊙	0	NW 1	E 2	ENE 3
10	91.8	91.2	92.0	91.7	18.5	26.0	16.4	19.3	27.1	14.5	84	58	94	79	3.3	14.1	1.1	6.2	0 ⊙	9 ☈	10 ● ☈	E 2	SSE 5	NE 3
11	93.0	93.4	92.7	93.0	16.6	17.6	14.4	15.8	18.6	14.3	92	86	89	89	1.6	2.8	1.8	2.1	10	10	9	NW 1	NW 3	NW 4
12	90.2	89.6	88.6	89.5	13.9	15.1	13.9	14.2	18.3	13.3	95	89	93	92	0.7	1.9	1.1	1.2	10 ●	10	6	NW 1	W 5	NW 1
13	87.5	85.3	82.3	85.0	13.6	19.2	16.9	16.6	20.0	9.1	86	55	69	70	2.2	10.0	5.9	6.0	1 ⊙	6 ⊙	10	WSW 1	S 5	E 1
14	81.4	82.5	87.4	83.8	14.2	16.6	13.0	14.2	18.2	12.7	94	81	93	89	0.9	3.7	1.1	1.9	10	10	10	SE 2	SW 3	NW 5
15	89.2	90.2	92.7	90.7	12.7	14.7	12.2	13.0	16.7	12.0	94	86	96	92	0.9	2.4	0.5	1.3	10	9 ●	10 ●	W 8	W 10	WNW 5
16	93.4	95.1	96.3	94.9	11.9	13.1	10.5	11.5	16.2	10.3	95	86	87	89	0.7	2.1	1.6	1.5	10 ●	10	2	W 7	WSW 9	W 1
17	96.3	96.5	96.2	96.3	14.8	20.4	17.0	17.3	21.8	9.1	85	58	80	74	2.5	10.1	3.9	5.5	2	6 ⊙	10	W 5	W 6	W 2
18	93.6	91.4	91.9	92.3	17.4	25.5	18.5	20.0	26.1	15.0	72	48	87	69	5.5	17.1	2.7	8.4	9 ⊙	5 ⊙	10	SW 4	SW 8	WNW 4
19	95.9	97.4	99.5	97.6	13.6	18.0	11.4	13.6	18.7	11.4	73	46	85	68	4.2	11.2	2.0	5.8	3 ⊙	6 ⊙	2	WNW 7	W 7	W 4
20	102.8	104.5	103.7	103.7	12.1	16.9	13.2	13.8	18.7	7.7	77	46	64	62	3.2	10.4	5.5	6.4	6	5	3	WNW 7	NW 8	C 0
21	101.2	99.4	102.4	101.0	12.3	19.0	10.4	13.0	19.9	7.7	78	44	82	68	3.2	12.3	2.2	5.9	8 ⊙	8 ⊙	0	S 2	W 5	NW 2
22	103.1	100.4	95.1	99.5	12.5	18.0	16.6	15.9	20.7	6.2	81	51	67	66	2.7	10.1	6.3	6.4	0 ⊙	6 ⊙	1	SW 2	SSE 5	SE 1
23	93.6	95.2	94.3	94.4	16.2	19.7	16.1	17.0	20.4	12.1	70	45	74	63	5.4	12.5	4.7	7.5	9	6 ⊙	10	W 4	W 10	SW 5
24	95.0	96.2	95.3	95.5	14.0	18.6	16.6	16.4	22.1	12.0	82	50	70	67	2.9	10.7	5.7	6.4	9	6	7	WSW 5	WSW 10	SW 5
25	94.1	92.6	90.2	92.3	17.6	25.4	19.0	20.2	26.5	12.5	65	38	75	59	7.0	19.9	5.4	10.8	4 ⊙	5 ⊙	5	W 8	WSW 9	W 1
26	91.8	91.7	89.7	91.1	17.8	25.3	21.9	21.7	27.1	12.5	73	38	55	55	5.6	19.8	11.8	12.4	0 ⊙	4 ⊙	0	W 3	W 5	E 2
27	86.2	85.4	85.8	85.8	20.3	26.0	20.3	21.9	26.8	16.6	77	63	79	73	5.5	12.5	5.0	7.7	6 ⊙	10	10	SE 2	SW 7	WSW 5
28	95.6	98.4	102.9	98.3	13.5	16.9	12.9	14.0	20.7	12.1	67	46	88	67	5.2	10.4	1.8	5.8	6	5	8	NW 10	WNW 10	NW 5
29	105.4	106.1	105.6	105.7	13.4	17.6	13.8	14.6	20.0	11.7	82	63	82	76	2.8	7.3	2.9	4.3	9	8 ⊙	3	W 6	W 6	WNW 2
30	105.8	105.1	105.0	105.3	16.7	23.3	15.8	17.9	24.4	10.0	74	41	54	56	5.0	16.8	8.3	10.0	0 ⊙	0 ⊙	0	W 3	WNW 5	NW 2
31																								
M	93.2	93.3	93.5	93.3	15.7	21.0	16.1	17.2	22.6	12.0	80	56	78	71	3.8	12.0	4.4	6.7	5.3	6.7	5.7	3.7	5.9	2.4

Chojnice — $H_s = 172\,m$ — $H_b = 177{,}2\,m$ — $h_w = 12{,}5\,m$ — Maj - Mai 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	-	
2	7	.	.	-	
3	7	2.8	.	-	▽0-1 9⁵⁰ 16⁰⁵, = 3³⁰–6³⁰ ≡⁰–7⁴⁰ =–12³⁰, 21¹⁵–24, ⌒¹ 21⁰⁰–24
4	7	0.0	.	-	▽⁰ 13⁵⁵–14¹⁰, = 0⁰⁰–1⁴⁰ ≡¹⁻⁰–2⁵⁰ =–3³⁰, ⌒² 1⁰⁰–8⁰⁰
5	7	13.6	.	-	▽⁰ 22¹²⁻⁴⁰, ↖⁰ 20⁴⁵–21³⁵ NW–NE, 22⁴⁰–24 N–E, = 3³⁰–6³⁰, ⌒¹ 0⁰⁰–8⁰⁰
6	7	13.3	.	-	▽0-1 6²⁰–11³⁰ ●⁰–13⁴⁵ ▽0-1 16²⁵–17²⁰, ↖⁰ 0⁰⁰–35 N–NE, 16¹⁵–17¹⁰ W–E, = na
7	7	10.5	.	-	▽0-2 13⁵⁰–21³⁰, ↖ 13⁴⁵–14³⁰ W–NE, = 3¹⁰–5³⁰ ≡⁰-¹ 7⁵⁰–12³⁰
8	7	1.6	.	-	▽⁰ 9⁴⁸ 15¹⁷ 21⁵⁰–58 22²⁰–30
9	7	5.1	.	-	▽⁰ 4⁵⁵–5⁰⁸ ●⁰ 7¹⁵–8¹⁰ ▽⁰ 9⁴⁶–24
10	7	0.8	.	-	▽⁰ 0⁰⁰–2²⁰, 10³⁰–40, 11⁴⁵–55, 13⁴⁵, 17⁴⁰, 21⁴⁰–50
11	7	.	.	-	
12	7	0.2	.	-	▽⁰ 9⁴⁰ 12⁴²
13	7	1.3	.	-	▽0-1 11³⁵–14⁴⁰ ▽⁰ 15⁵⁰–16³⁵ ▽¹ 20⁴⁵–21³⁵, ⌒² 0⁰⁰–8⁰⁰
14	7	2.8	.	-	▽⁰ 8²⁵–9³⁵, 17⁵⁰–18¹⁵, ⌒¹ 0⁰⁰–8⁰⁰
15	7	0.2	.	-	●⁰ 3⁵⁰–5⁵⁵ ▽⁰ 9⁵³–10⁰⁵, 11⁴⁵–58 22⁵⁵–23⁰⁵
16	6	5.0	.	-	▽⁰ 1⁰⁰–15, 3⁵⁵–4⁰⁴, 6⁴⁵–50, 7²⁵–10¹⁵ ●⁰–13³⁰
17	7	0.3	.	-	●⁰ 2⁴⁵–6⁵², 7⁰⁵ 9³⁵
18	7	.	.	-	= 2³⁰–4⁴⁰, ⌒⁰-² 19⁰⁰–24
19	7	.	.	-	⌒² 1⁰⁰–8⁰⁰
20	7	.	.	-	= 20³⁰–24, ⌒¹ 0⁰⁰–8⁰⁰, 19⁰⁰–24
21	7	0.0	.	-	▽⁰ 15⁵⁰–16⁰¹, = 0⁰⁰–7³⁰, ⌒¹ 1⁰⁰–8⁰⁰
22	7	.	.	-	⌒¹ 1⁰⁰–8⁰⁰ ⌒¹⁻² 20⁰⁰–24
23	7	0.0	.	-	▽⁰ 14⁵⁰–53, ⌒² 1⁰⁰–9⁰⁰
24	7	.	.	-	⌒⁰ 0⁰⁰–8⁰⁰ ⌒⁰-¹ 20⁰⁰–24
25	7	.	.	-	⌒¹ 1⁰⁰–8⁰⁰
26	7	.	.	-	⌒⁰ 0⁰⁰–8⁰⁰
27	7	.	.	-	
28	7	.	.	-	
29	7	.	.	-	= 7³⁰–8⁴⁰
30	7	0.7	.	-	▽ 12⁵²–13³⁰, ↖ 13⁰⁵–45 SW–SE, = 3³⁰–7³⁰, ⌒¹ 0⁰⁰–8⁰⁰
31	7	.	.	-	
Σ	–	58.2	–	-	UWAGI.

Czerwiec – Juin

1	7	.	.	-	⌒¹ 21⁰⁰–24
2	7	.	.	-	⌒² 1⁰⁰–9⁰⁰
3	7	0.0	.	-	▽⁰ 12⁴⁰–42, (↖)⁰ 0⁰⁶–55 NE–SE = 4⁴⁰ 7²⁰, ⌒⁰ 21⁰⁰–24
4	7	0.0	.	-	▽⁰ 16³²–37, ↖⁰ 13¹⁵–14²⁰ E–SW (↖)⁰ 15⁴⁰–16³⁰; ⌒⁰ 1⁰⁰–8⁰⁰
5	7	0.0	.	-	▽⁰ 18⁴⁸–19⁰⁰ 19⁰⁵–10, (↖)⁰ ↖⁰ 12³⁰–13⁴⁰ NW–NE, 17⁵⁰, 18⁵⁸–20³⁰ N–W
6	7	3.4	.	-	⌒⁰ 1⁰⁰–8⁰⁰
7	7	47.1	.	-	▽⁰ 4⁴⁵–5⁰⁰ ●⁰-² 6⁴⁰–7⁰³ ▽⁰ 12⁵²–13⁰⁵ ▽¹-² 21¹⁰–24, (↖)⁰ 5⁵⁵–6⁴⁵ E–W ↖² 20³⁵–24; = a
8	8	0.3	.	-	●¹ 0⁰⁰–0⁵ ▽⁰ 15⁵²–16⁰⁷ 17⁰³–42, ↖² 0⁰⁰–5⁰ W–E ↖⁰ 14¹⁵–16³⁰ SW–E, 16⁵⁰–17⁴⁰ NW–E, = 4¹⁰–11¹⁵
9	7	.	.	-	= 0²⁰ 9³⁰, ⌒² 0⁰⁰ 10⁰⁰ ⌒⁰ 21⁰⁰–24
10	7	5.2	.	-	▽⁰ 18²⁰–30 ▽¹⁻⁰ 20¹⁰–40 ▽⁰-² 20⁴⁵–23⁵⁰, (↖), ↖⁰ 13⁴⁰–14⁵⁰ NE–E 18⁵⁰–22⁴⁵ W–E, ⌒¹-² n–a
11	7	3.3	.	-	▽¹ 4⁵⁵–5¹⁵ ▽⁰ 8³⁸–45 9²⁵–13¹⁰ 22⁵²–23¹⁰; ↖⁰ 9²⁵–11⁴⁵ S–N, = na, a
12	7	2.3	.	-	●⁰ 7³⁰ 10⁴⁰ ▽⁰ 12²⁰–13¹⁵, = 4²⁰–11³⁰, ⌒¹ 21⁰⁰–24
13	7	3.1	.	-	▽⁰ 22²⁵–23²⁰ 23⁴⁰–24, = 5³⁰–8³⁰, ⌒² 1⁰⁰–10⁰⁰
14	7	11.9	.	-	●⁰ 0⁰⁰-³⁵ ▽⁰-¹ 3³⁵–5¹⁵ ▽⁰ 14²² 20³⁵ ●⁰ 20⁴⁵–21⁴⁰, ↖⁰ 13⁵⁵–15⁴⁰ NW–SE; = n–a
15	7	8.3	.	-	●⁰ 0⁵⁰ 12³⁵ ▽⁰-¹ 13⁴⁰ 19¹⁵ ●⁰ 19²⁵–24
16	7	1.6	.	-	●⁰ 0⁰⁰–1⁵⁰ ▽⁰-¹ 7³⁵–9¹⁵ ▽⁰ 13⁴⁰–45, = n–a
17	7	.	.	-	= 4²⁰–9³⁰, ⌒¹ 0⁰⁰–8⁰⁰
18	7	0.7	.	-	▽⁰ 20⁵²–21⁰⁷ ●² 22¹⁵–24, = 4²⁰–7¹⁵
19	7	0.5	.	-	●⁰ 0⁰⁰–1¹⁰ ▽⁰ 18⁴⁵–50, 19⁴⁰–20⁰⁵
20	7	.	.	-	⌒¹ 21⁰⁰–24
21	7	3.0	.	-	▽⁰ 15⁰⁵–17¹⁵, ⌒² na–a
22	7	.	.	-	⌒¹⁻² np
23	7	.	.	-	≫ 13²⁰–17⁴⁰, ⌒²⁻⁰ na–10⁰⁰ ⌒⁰ np
24	7	.	.	-	≫ 13³⁰–16²⁰, ⌒¹ 1⁰⁰–9⁰⁰
25	7	.	.	-	⌒⁰ 0⁰⁰–8⁰⁰
26	8	.	.	-	⌒¹ 0⁰⁰–9⁰⁰
27	7	0.0	.	-	▽⁰ 22⁴⁵–48
28	7	0.0	.	-	▽⁰ 4⁵⁵–5⁰³, 16²⁵⁻³³, 21³⁰–35, ≫ 7³⁰–17¹⁵
29	7	0.0	.	-	▽⁰ 9³⁰–33, 11⁵⁸–63
30	8	.	.	-	⌒²⁻⁰ na ⌒⁰ np
31					
Σ	–	90.7	–	-	UWAGI.

Chojnice — $\varphi = 53°42'$ — $\lambda = 17°33'$ — Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	105.3	104.5	103.0	104.3	15.2	24.3	20.2	20.0	26.7	6.3	81	36	71	63	3.4	19.6	6.9	10.0	0 ⊙	4 ⊙	0	SE 2	SW 1	SW 3
2	102.0	101.1	99.3	100.8	17.4	28.0	22.5	22.6	28.9	6.4	81	29	53	54	3.8	27.0	12.8	14.5	0 ⊙	0 ⊙	0	NW 2	NW 2	NW 1
3	97.5	94.2	92.9	94.9	20.8	30.8	18.2	22.0	31.6	13.9	72	32	81	62	6.8	30.1	3.9	13.6	6 ⊙	2 ⊙	10 (⊼)	S 1	SW 5	NW 5
4	91.0	88.5	84.2	87.9	14.9	17.0	13.6	14.8	18.2	8.8	83	80	94	86	2.9	3.9	0.9	2.6	2 ⊙	10	10	SW 3	SW 5	SW 5
5	87.4	89.2	90.2	88.9	11.4	15.0	9.2	11.2	15.5	7.7	72	56	91	73	3.8	7.4	1.1	4.1	9	7 ⊙	6	W 14	SW 12	SW 5
6	91.2	92.8	96.0	93.3	8.8	12.0	10.3	10.4	13.9	5.3	86	80	91	86	1.5	2.8	1.1	1.8	10	10	1	SW 5	SW 4	W 1
7	96.8	97.9	98.8	97.8	10.3	12.9	11.5	11.6	16.5	6.5	90	75	95	86	1.3	3.8	1.0	2.0	10	9	7	WSW 5	W 5	C 0
8	97.7	96.3	92.9	95.6	11.8	18.1	13.8	14.4	19.5	7.6	84	70	91	82	2.1	6.2	1.5	3.3	10	8 ⊙	10	SW 4	SW 4	SE 3
9	87.4	85.9	88.7	87.3	13.3	14.5	12.0	13.0	15.4	10.7	90	97	95	94	1.6	0.6	0.7	1.0	10	10 •	9	SSW 4	SE 2	W 2
10	87.9	88.5	90.2	88.9	11.7	15.5	11.7	12.6	16.5	9.6	89	67	88	81	1.5	5.8	1.6	3.0	9	8	8 •	W 3	W 5	WSW 5
11	90.7	91.6	91.0	91.1	12.3	17.1	15.0	14.8	19.5	8.8	89	60	87	79	1.5	7.8	2.2	3.8	8	9	8	SW 4	W 7	WSW 1
12	88.9	88.6	86.7	88.1	15.4	20.6	18.4	18.2	23.5	14.0	97	72	82	84	0.6	6.7	3.9	3.7	10	7 ⊙	4	S 2	SW 2	C 0
13	81.5	77.9	74.6	78.0	17.5	26.6	18.0	20.0	27.5	13.3	93	63	99	85	1.4	13.0	0.2	4.9	8	5	10	E 3	ESE 6	WSW 3
14	78.0	82.4	85.7	82.0	12.9	12.1	11.5	12.0	16.1	11.4	95	95	90	93	0.7	0.7	1.4	0.9	10	10	3	SW 9	SW 7	SSW 3
15	87.1	88.7	91.0	88.9	15.3	19.8	15.4	16.5	21.4	10.9	89	69	82	80	1.9	7.1	3.2	4.1	9	7 ⊙	4	S 1	W 5	C 0
16	89.6	89.7	88.4	89.2	13.3	14.8	13.2	13.6	16.9	12.9	98	91	93	94	0.4	1.5	1.1	1.0	10 •	10 •	8	SE 1	E 2	SE 2
17	86.4	85.7	85.5	85.9	12.3	18.3	13.3	14.3	19.1	10.9	98	68	98	88	0.3	6.8	0.4	2.5	9	8	10 •	WSW 3	SW 1	W 1
18	84.8	84.7	85.1	84.9	12.8	16.5	13.6	14.1	17.3	11.7	100	79	98	92	0.0	4.1	0.4	1.5	10 •	9	8	WNW 3	W 3	C 0
19	85.6	86.0	86.7	86.1	13.3	18.9	13.7	14.9	20.1	10.9	96	70	95	87	0.6	6.5	0.7	2.6	10	6	6	WSW 3	SW 3	SSW 2
20	88.3	89.3	89.2	88.9	13.6	15.0	13.3	13.8	19.6	11.3	97	78	96	90	0.6	3.6	0.6	1.6	9	10 • ⊼	8	S 2	SW 4	SW 2
21	88.0	87.7	87.6	87.8	14.1	16.7	13.7	14.6	18.3	12.8	97	86	100	94	0.6	2.7	0.0	1.1	10	10 ⊼	10 •	SW 5	WSW 7	W 5
22	88.9	89.3	89.9	89.4	14.6	17.2	13.8	14.8	18.1	11.8	95	88	93	92	0.7	2.4	1.1	1.4	9	8 ⊙	10	W 5	W 7	W 3
23	91.1	92.6	94.8	92.8	13.9	15.9	12.6	13.8	16.4	12.3	90	84	92	89	1.6	2.9	1.2	1.9	9	10	8	WSW 4	WSW 5	WSW 2
24	96.1	98.8	100.3	98.4	12.5	15.0	12.9	13.5	16.4	11.7	94	71	85	83	0.9	4.8	2.3	2.7	9 •	10	9	SW 5	WNW 6	W 2
25	101.7	102.4	100.4	101.5	13.8	15.9	13.1	14.0	16.2	9.9	90	65	89	81	1.6	6.3	1.6	3.2	9	10	10	W 5	W 7	SW 4
26	96.1	93.1	88.4	92.5	13.3	17.5	18.1	16.8	21.0	12.1	98	84	68	83	0.4	3.2	6.6	3.4	10	10	10 •	SW 3	SW 5	SW 4
27	85.7	83.8	84.8	84.8	15.8	18.7	12.9	15.1	20.1	12.8	93	70	96	86	1.3	6.5	0.6	2.8	10	10	4	SW 5	SW 8	SW 3
28	82.8	81.2	83.5	82.5	12.8	13.3	11.5	12.3	15.1	11.5	91	96	99	95	1.4	0.6	0.2	0.7	10 •	10 •	9	SW 2	SW 1	C 0
29	86.7	90.2	93.6	90.2	11.7	14.9	12.5	12.9	17.1	10.1	96	70	88	85	0.5	5.0	1.7	2.4	8	10	10	W 3	W 5	W 1
30	95.6	95.7	96.4	95.9	14.0	17.7	14.0	14.9	17.9	10.9	85	75	97	86	2.3	5.1	0.6	2.7	7 ⊙	10 •	10	W 2	NW 2	NW 2
31	93.1	90.0	86.1	89.7	13.7	13.7	12.9	13.3	14.6	12.6	95	98	99	97	0.7	0.4	0.2	0.4	10	10 •	10 •	NW 5	NW 7	WNW 3
M	90.7	90.6	90.5	90.6	13.7	17.6	14.1	14.9	19.3	10.6	90	73	88	84	1.6	6.6	2.0	3.4	8.4	8.3	7.4	3.8	4.7	2.4

Sierpień – Août

1	87.8	90.0	92.8	90.2	14.4	16.2	12.6	14.0	17.4	12.4	94	83	96	91	0.9	3.1	0.5	1.5	10	9	5	WNW 6	W 10	SW 3
2	92.9	93.0	93.1	93.0	12.8	20.2	14.7	15.6	20.6	9.2	95	64	97	85	0.7	8.5	0.5	3.2	9 ⊙	10	10	SW 2	SW 1	S 1
3	93.6	94.1	98.1	95.3	13.5	16.9	10.6	12.9	17.9	10.6	98	87	96	94	0.4	2.5	0.5	1.1	10 ≡	10 • ⊼	0	SSW 2	SW 5	WSW 2
4	96.9	95.0	91.7	94.5	11.1	13.8	13.4	12.9	15.3	7.3	95	88	99	94	0.7	2.0	0.2	1.0	10	10 •	10 •	SW 2	SSW 5	SW 7
5	93.0	93.7	91.9	92.9	14.4	20.1	18.0	17.6	21.6	13.0	93	61	87	80	1.1	9.2	2.6	4.3	10 ●	9 ⊙	9	W 5	W 7	C 0
6	88.3	89.2	89.0	88.8	17.7	25.9	17.9	19.8	26.4	15.9	92	61	80	78	1.6	13.1	4.0	6.2	0 ⊙	5 ⊙	10 ⊼	SW 3	WSW 5	NE 3
7	91.3	91.3	93.0	91.9	13.5	17.5	12.6	14.0	18.5	11.9	99	87	93	93	0.2	2.6	1.1	1.3	10 •	10	1	C 0	NW 2	W 2
8	97.3	96.8	94.4	96.2	11.3	20.1	16.1	15.9	21.1	10.1	99	51	78	76	0.2	11.5	4.0	5.2	8	6 ⊙	10	W 2	SE 2	E 3
9	96.5	98.5	100.0	98.3	16.0	22.2	16.9	18.0	22.6	12.6	85	54	81	73	2.7	12.4	3.7	6.3	7 ⊙	9 ⊙	8	NW 2	W 6	NW 1
10	100.1	98.9	95.5	98.2	16.2	18.2	15.1	16.2	19.8	13.4	85	82	96	88	2.7	3.7	0.8	2.4	7 ⊙	10	10	SE 3	SE 1	NE 1
11	93.9	93.8	94.8	94.2	15.3	16.6	15.5	15.7	17.4	14.4	96	94	98	96	0.8	1.2	0.4	0.8	10	10 •	9	NNE 2	NE 1	C 0
12	93.5	93.5	95.2	94.1	15.4	20.3	13.8	15.8	21.3	13.5	100	69	89	86	0.0	7.2	1.8	3.0	10	8	10	SW 2	W 3	NW 3
13	96.3	97.4	99.2	97.6	12.6	16.3	9.4	11.9	17.8	9.0	87	66	92	82	1.9	6.3	1.0	3.1	6 ⊙	8 ⊙	0	W 3	WNW 8	WNW 1
14	98.9	97.5	95.7	96.7	11.0	17.8	14.1	14.2	18.4	7.0	94	59	76	76	0.8	8.4	3.9	4.4	10	9	9	SW 2	SW 5	SSW 3
15	89.5	86.4	86.4	88.1	13.1	14.4	12.0	12.9	15.1	10.9	95	81	95	90	0.7	3.1	0.7	1.5	9	10 •	10	SW 3	SW 5	SSW 2
16	85.4	84.5	84.1	84.7	11.3	11.0	9.5	10.3	14.4	9.3	88	96	97	94	1.7	0.5	0.3	0.8	6	10	10	SW 5	SW 5	SW 2
17	83.8	84.9	86.8	85.2	11.5	14.2	10.9	11.9	15.7	9.5	93	75	97	88	1.0	4.1	0.3	1.8	10	9	8	SW 3	WSW 5	C 0
18	86.6	86.7	86.4	86.6	12.0	15.5	10.4	12.1	18.6	8.0	98	84	95	92	0.3	2.8	0.6	1.2	10	9	1	NW 3	NW 3	W 1
19	81.3	79.9	81.6	80.9	11.1	13.5	11.8	12.0	16.6	8.3	99	91	97	96	0.2	1.5	0.3	0.7	10 •	9	10 •	SW 2	W 5	W 2
20	81.8	84.2	87.4	84.5	12.8	14.8	13.0	13.4	17.4	11.6	95	91	88	91	0.7	1.5	1.8	1.3	10	4	3	SW 4	W 3	W 4
21	86.7	88.0	87.1	87.3	13.0	14.7	14.7	14.3	15.6	12.1	95	90	87	91	0.7	1.6	2.2	1.5	10 •	10	10	W 7	W 8	SW 6
22	85.1	81.7	82.6	82.5	14.7	15.4	12.5	13.8	17.5	12.4	89	95	89	91	1.8	1.0	1.5	1.4	10 •	10 •	8	SW 7	SW 6	SW 5
23	83.3	86.4	90.0	86.6	12.4	16.2	12.2	13.2	17.6	11.3	96	67	87	83	0.5	6.2	1.9	2.9	10 •	9	10	WSW 4	NW 10	WSW 5
24	92.5	94.2	95.8	95.5	11.6	13.5	12.2	12.4	15.3	10.8	90	74	95	86	1.3	4.0	0.7	2.0	7 ⊙	10	4	W 4	W 5	SW 2
25	92.6	94.5	96.0	94.4	12.8	16.4	9.4	12.0	17.0	8.9	98	56	89	81	0.4	8.1	1.3	3.3	10	8	5	W 3	W 8	W 3
26	97.7	98.5	99.2	98.5	10.5	15.0	15.1	13.9	17.2	7.8	94	96	97	96	0.8	0.7	0.6	0.7	10	10 •	10	W 1	SW 2	C 0
27	99.0	99.5	101.4	100.0	15.1	23.4	13.7	16.5	24.0	12.4	99	64	93	85	0.2	10.3	1.1	3.9	7	8	2	SW 2	SW 6	C 0
28	103.2	104.4	104.3	104.0	15.1	17.6	14.3	14.8	19.6	10.6	94	74	87	85	0.9	5.3	2.2	2.8	9 ⊙	10	2	W 5	WNW 8	WNW 3
29	103.1	103.6	103.7	103.5	12.9	19.3	12.4	14.2	20.0	11.9	98	70	96	88	0.4	6.6	0.5	2.5	10	6	3	NW 5	NW 5	NNW 1
30	104.3	105.2	105.0	104.8	13.3	20.4	16.7	16.8	23.1	9.5	98	66	89	84	0.4	8.1	2.2	3.6	9	6 ⊙	0	SE 1	SW 1	C 0
31	106.7	107.7	108.1	107.5	14.0	24.2	17.5	18.3	25.1	11.4	94	55	83	77	0.9	13.7	3.4	6.0	0 ⊙	1 ⊙	0	C 0	SW 1	C 0
M	92.9	93.4	93.8	93.4	13.2	17.5	13.5	14.4	18.9	10.9	94	75	91	87	0.9	5.5	1.5	2.6	8.5	8.5	6.4	3.0	4.7	2.1

Chojnice — $H_s = 172\,m$ — $H_b = 177{,}2\,m$ — $h_w = 12{,}5\,m$ — Lipiec – Juillet 1961

DNI	WYDZIAŁ NOŚC V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	$\overset{2}{\frown}\ 0^{00}-9^{00}$
2	8	.	.	–	$=4^{20}-7^{30}$, $\overset{2-1}{\frown}$ na – a $\overset{0}{\frown}$ np
3	7	.	.	–	$(K)^{0}\ 21^{10}-50$ SE-NE, $\overset{1}{\frown}$ na – a, np
4	7	0.5	.	–	$\bullet^{0}\ 11^{48}\ 16^{35}$, $\overset{1}{\frown}\ 10^{00}-9^{00}$
5	7	0.3	.	–	$\bullet^{0}\ 16^{45}\ 20^{02}$
6	7	1.8	.	–	$\bullet^{0-1}\ 15^{56}\ 18^{33}$
7	7	0.2	.	–	$\bullet^{0}\ 12^{20}-35$
8	7	7.0	.	–	$\bullet^{0}\ 8^{05}-10^{40}$ $\bullet^{0}-11^{40}$ $\bullet^{0-1}\ 12^{05}\ 23^{05}$, $=19^{30}-24$, $K^{0}\ 15^{40}\ 17^{40}$ W-E
9	6	10.7	.	–	$\bullet^{0}\ 7^{10}-9^{40}$ $\bullet^{0}-10^{51}$ $\bullet^{0}\ 12^{55}-13^{20}$ $\bullet^{1-2}\ 13^{30}-15^{15}$ $\bullet^{0}-19^{25}$, $=0^{00}-11^{30}$
10	7	0.1	.	–	$\bullet^{0}\ 12^{50}-13^{00}$, $14^{20}-28$, $21^{40}-22^{05}$
11	7	6.3	.	–	
12	7	.	.	–	$\bullet^{0}\ 0^{55}\ 1^{30}$ $\bullet^{0-1}\ 2^{40}-5^{00}$ $K^{0}\ 3^{30}-5^{30}$ N, $=2^{20}-8^{40}$, $\overset{1-2}{\frown}\ 20^{00}-24$
13	7	27.1	.	–	$\bullet^{2-0}\ 15^{25}-16^{10}$ $\bullet^{0}\ 17^{45}-18^{10}$, $18^{53}-19^{55}$, $23^{40}-24$, $K^{0}\ 15^{30}-16^{25}$, $17^{45}-20^{30}$ SE-W, $=1^{30}-12^{10}$, p – 24, $\overset{2}{\frown}\ 0^{00}-9^{00}$
14	6	0.4	.	–	$\bullet^{0}\ 0^{00}-4^{20}$, $13^{45}-15^{10}$, $=0^{00}-9^{30}$
15	7	1.4	.	–	$\bullet^{0}\ 1^{45}-2^{20}$, $\overset{1}{\frown}\ 21^{00}-24$
16	6	6.4	.	–	$\bullet^{0-1}\ 4^{55}\ 8^{15}$ $\bullet^{0}-14^{10}$ $\bullet^{0}\ 23^{45}-24$, $K^{0}\ 23^{30}-24$ SE-W, $\overset{1}{\frown}\ 0^{00}-4^{00}$
17	7	12.3	.	–	$\bullet^{0}\ 0^{00}-45$, $17^{45}-19^{20}$, $20^{15}-22^{30}$ $\bullet^{1}-24$, $K^{0}\ 0^{00}-30$ SE-W, $=3^{30}-6^{30}$ $\equiv^{0}-7^{30}$
18	7	1.6	.	–	$\bullet^{1-0}\ 0^{00}\ 3^{40}$ $\bullet^{0}\ 5^{20}-7^{10}$ $\bullet^{0}-8^{30}$ $\bullet^{0}\ 18^{02-05}$, $22^{10}-23^{15}$, $=3^{40}-12^{30}$, $21^{30}-24$
19	7	4.1	.	–	$\bullet^{0-2}\ 16^{25}\ 16^{37}\ 17^{15}$ $\bullet^{0}\ 18^{08}-19^{05}$, $K^{0}\ 15^{45}-16^{20}$ SE-E, $18^{05}-19^{15}$ SW-E, $=0^{00}-9^{30}$
20	6	4.8	.	–	$\bullet^{0}\ 13^{30}\ 21^{25}$ $K^{0}\ 11^{30}-12^{30}$ SE-SW, $13^{30}-16^{30}$ E, $16^{15}-21^{30}$ SE-SW, $=2^{30}-10^{10}$
21	7	20.2	.	–	$\bullet^{0}\ 2^{00-40}\ 6^{05}-7^{10}\ 9^{42}-10^{03}$ $\bullet^{0-2}\ 19^{40}-21^{16}$ $\bullet^{0-1}\ 21^{43}-22^{40}$, $K^{0}\ 12^{45}-15^{10}$ NW-E, $=$ na, a, p
22	7	1.4	.	–	$\bullet^{0-1}\ 9^{48}\ 13^{25}$, 17^{03-12}, $=0^{00}-8^{30}$
23	7	0.3	.	–	$\bullet^{0}\ 3^{56}-4^{02}$, $10^{35}-11^{04}$, $11^{28}-12^{16}$, 22^{47-58}, $\overset{1}{\frown}\ 5^{00}-7^{00}$
24	7	0.0	.	–	$\bullet^{0}\ 7^{45-52}$, $11^{50}-12^{20}$, $\overset{0}{\frown}\ 0^{00}-7^{00}$
25	8	1.0	.	–	$\bullet^{0}\ 6^{40-50}$
26	6	1.3	.	–	$\bullet^{0}\ 1^{14}-6^{10}$, $8^{48}-10^{05}$, $12^{52}-14^{20}$ $\bullet^{0}\ 22^{35}\ 23^{50}$, $=5^{00}-16^{30}$
27	7	0.9	.	–	$\bullet^{0}\ 0^{15}-3^{05}$, 3^{25} $\bullet^{0}\ 17^{52}-18^{06}$, $=4^{30}-9^{30}$
28	6	6.3	.	–	$\bullet^{0}\ 6^{35}-15^{40}$ $\bullet^{0}\ 17^{20-36}$, $=4^{15}-15^{45}$, $21^{15}-24$
29	7	0.0	.	–	$\bullet^{0}\ 16^{50}-17^{05}$, $=0^{00}-6^{30}$, $\overset{1}{\frown}\ 21^{00}-24$
30	7	4.7	.	–	$\bullet^{0}\ 13^{57}-14^{25}$, 15^{45-52} $\bullet^{0-1}\ 16^{40}-19^{10}$, $\overset{1}{\frown}\ 0^{00}-8^{00}$
31	5	24.8	.	–	$\bullet^{0-1}\ 8^{35}-18^{40}$ $\bullet^{0}\ 19^{45}-21^{15}$ $\bullet^{1}-22^{30}$
Σ	–	145.9	–	–	UWAGI.

Sierpień – Août

DNI	WYDZIAŁ NOŚC V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	7	2.7	.	–	$\bullet^{0}\ 3^{30}-4^{40}$ $\bullet^{0-1}\ 8^{38}-9^{20}$ $\bullet^{0}\ 14^{25}\ 16^{35}$ $\bullet^{0-1}\ 17^{08}\ 18^{45}$, $=0^{00}-4^{50}$, $19^{10}-24$; $\gg$ p, $\overset{1}{\frown}$ np
2	7	0.2	.	–	$\bullet^{0}\ 16^{50}\ 19^{55}$, $=0^{00}-9^{40}$, p – np, $\overset{2}{\frown}\ 0^{00}$ a $\overset{}{\frown}$ np
3	6	0.6	.	–	$\bullet^{0}\ 12^{10-18}\ 13^{50}-14^{20}$ $K^{1}\ 12^{25}\ 13^{50}$ NW-NE, $=0^{00}-5^{50}$ $\equiv^{0-1}\ 9^{45}=-14^{30}$, $\overset{2}{\frown}$ na, a $\overset{1-2}{\frown}$ p, np
4	6	3.5	.	–	$\bullet^{0}\ 12^{45}-22^{40}$, $=3^{30}-6^{10}$, $16^{30}-24$, $\overset{2}{\frown}\ 0^{00}-11^{00}$
5	7	3.2	.	–	$=0^{00}-8^{15}$, $21^{10}-23^{30}$, $\overset{1}{\frown}\ 20^{00}-24$
6	8	19.7	.	–	$\bullet^{0-1}\ 3^{52}-4^{20}$ $\bullet^{0-2}\ 22^{10}-24$, K^{0} SW-N $21^{40}-24$, $=$ na – a, $\overset{1}{\frown}$ na
7	7	1.9	.	–	$\bullet^{0}\ 0^{00-40}\ 2^{00}-3^{10}$ $\bullet^{0}\ 6^{20}-11^{10}$ $11^{25}-12^{03}$ $\bullet^{0}\ 14^{40}-15^{25}$, $K^{0}\ 0^{00-35}$ SW, $=4^{30}-12^{15}$, p, $\overset{1}{\frown}$ np
8	8	0.1	.	–	$\bullet^{0}\ 17^{50}-19^{15}$, $=4^{30}-8^{15}$, $\overset{1-2}{\frown}\ 0^{00}-11^{00}$
9	7	.	.	–	$=4^{15}-7^{30}$, $\overset{1}{\frown}\ 0^{00}-8^{00}$, $20^{00}-24$
10	7	11.9	.	–	$\bullet^{0-1}\ 18^{58}-20^{40}$ $\bullet^{0}\ 21^{28}-22^{15}$, $=20^{40}-21^{58}$
11	6	1.3	.	–	$\bullet^{0-1}\ 0^{50}-2^{15}$ $\bullet^{1-0}\ 2^{40}-3^{20}$ $\bullet^{0}\ 10^{46}-15^{20}$, $=$ na, a, np
12	7	.	.	–	$=0^{00}-2^{50}$ $\equiv^{0-1}-7^{45}=-11^{20}$
13	8	.	.	–	$\overset{1}{\frown}\ 0^{00}-8^{00}$ $20^{00}-24$
14	8	0.1	.	–	$\overset{1-0}{\frown}\ 0^{00}-11^{00}$
15	7	0.4	.	–	$\bullet^{0}\ 6^{50}-7^{15}$ $\bullet^{0}\ 9^{55}-10^{40}$ $\bullet^{0-1}\ 13^{45}-14^{57}$ $\bullet^{0}\ 15^{06-25}$ 20^{40-46}, $=5^{10}-11^{30}$
16	7	1.8	.	–	$\bullet^{0}\ 10^{50}\ 14^{15}$, $=22^{30}-24$, $\overset{2-1}{\frown}\ 2^{00}-10^{00}$ $\overset{1}{\frown}\ 20^{00}-24$
17	7	3.6	.	–	$\bullet^{0}\ 8^{05}\ 9^{35}$ $\bullet^{0-1}\ 14^{20-52}$, $=0^{00}-5^{30}$, $\overset{1}{\frown}\ 0^{00}-8^{00}$ $\overset{1-2}{\frown}\ 20-24$
18	7	2.3	.	–	$\bullet^{0}\ 12^{52-56}$, 13^{20-30}, $=2^{30}-4^{40}$ $\equiv^{1-0}\ 6^{45}=-9^{15}$, $\overset{2}{\frown}\ 0^{00}-9^{00}$
19	7	12.4	.	–	$\bullet^{2-0}\ 7^{25}-11^{25}$ $\bullet^{1}\ 13^{30-45}$ $\bullet^{2-0}\ 16^{30}\ 22^{30}$, $=$ na – p, np
20	7	4.3	.	–	$\bullet^{0}\ 4^{55}\ 13^{43}$, $=0^{00}-2^{00}$, $4^{30}-7^{20}$
21	7	0.8	.	–	$\bullet^{0}\ 2^{52}-3^{07}$, $5^{45}-11^{35}$, $15^{50}-18^{20}$, $\gg 9^{15}-10^{30}$, $11^{20}-12^{40}$
22	6	0.8	.	–	$\bullet^{0}\ 7^{40}\ 9^{15}$, $13^{30}-14^{10}$
23	8	2.0	.	–	$\bullet^{0}\ 6^{50}\ 9^{50}$, $\gg 9^{20}-16^{15}$
24	7	3.6	.	–	$\bullet^{0}\ 3^{20-40}$ $\bullet^{0}\ 15^{40}-16^{30}$, $=22^{15}-24$
25	7	0.0	.	–	$\bullet^{0-1}\ 5^{40}-6^{50}$, $=0^{00-30}$, $5^{10}-7^{40}$, $\triangledown\ 22^{30}-21^{15}$
26	6	0.7	.	–	$\bullet^{0}\ 6^{25}\ 14^{35}$, $21^{55}-22^{40}$, $=10^{15}-24$
27	7	.	.	–	$=1^{00}-11^{30}$, $\overset{0}{\frown}\ 21^{00}-24$
28	8	.	.	–	$=2^{00}-4^{30}$, $\overset{1}{\frown}\ 1^{00}-10^{00}$
29	7	.	.	–	$=4^{30}-9^{40}$, $\overset{1-2}{\frown}\ 0^{00}-11^{00}$
30	7	.	.	–	$=4^{20}-9^{30}$, $\overset{1}{\frown}\ 0^{00}-10^{00}$, $20^{00}-24$
31	8	.	.	–	$=4^{30}-7^{20}$, $\overset{2-0}{\frown}$ na – a $\overset{1}{\frown}$ p – np
Σ	–	77.9	–	–	UWAGI.

Chojnice — φ = 53°42' — λ = 17°33' — Wrzesień – Septembre 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	108.1	106.0	103.0	105.7	15.4	24.8	17.8	19.0	25.6	12.9	95	51	82	76	1.0	15.2	3.6	6.6	0 ⊙	0 ⊙	0	SW 1	S 5	S 1
2	100.3	98.7	95.9	98.3	14.7	26.7	17.9	19.3	27.2	12.7	95	48	81	74	1.1	18.1	3.8	7.7	0 ⊙	0 ⊙	0	C 0	SW 3	C 0
3	91.8	90.8	89.9	90.8	14.6	26.2	17.5	19.0	26.9	12.6	98	50	84	77	0.4	16.9	3.2	6.8	0 ⊙	0 ⊙	1	C 0	W 1	C 0
4	91.7	93.8	94.2	93.2	12.2	20.8	13.3	14.9	21.1	10.8	98	67	91	85	0.3	8.2	1.4	3.3	7 ⊙	8 ⊙	0	NE 1	E 3	ENE 2
5	93.3	92.2	88.2	91.2	12.0	20.1	16.6	16.3	20.9	10.4	94	68	86	83	0.8	7.4	2.7	3.6	0 ⊙	4 ⊙	10 •	E 3	E 5	E 5
6	85.4	85.6	85.2	85.4	15.9	20.9	15.7	17.0	21.2	14.4	100	68	95	88	0.0	7.8	0.9	2.9	10 ≡	5 ⊙	10	SW 2	WSW 3	W 1
7	82.3	82.8	81.1	82.1	14.2	15.4	10.3	12.6	16.5	10.3	98	79	94	90	0.4	3.7	0.8	1.6	10 •	8 ⊙	10	SW 4	SW 4	WSW 8
8	82.2	84.1	88.7	85.0	10.9	12.5	11.4	11.6	14.1	10.1	95	85	98	92	0.6	2.4	0.4	1.1	10	10 •	10	WSW 7	SW 9	W 5
9	91.6	92.4	93.4	92.5	12.4	16.2	11.5	12.9	16.3	10.1	98	75	95	89	0.4	4.5	1.0	2.0	9	7	9	W 3	W 7	W 5
10	94.7	95.8	96.4	95.6	12.8	14.0	11.2	12.3	14.4	10.8	91	82	97	90	1.4	2.9	0.3	1.5	10	10	10	WNW 4	W 4	WNW 1
11	94.8	93.9	92.6	93.8	11.7	16.7	12.0	13.1	17.5	10.6	99	72	95	89	0.1	5.4	0.7	2.1	10	9	8	WSW 3	WSW 5	SW 1
12	89.6	89.2	90.2	89.7	11.4	17.5	11.5	13.0	17.5	10.8	91	77	94	87	1.2	4.6	0.9	2.2	10	9	8	SW 3	WSW 5	W 3
13	91.4	93.5	93.0	92.6	11.1	16.4	12.8	13.3	16.7	10.4	94	62	91	82	0.8	7.0	1.4	3.1	5 ⊙	8 ⊙	10	WSW 3	NW 6	SSE 1
14	88.4	87.3	87.5	87.7	12.8	15.9	14.6	14.5	17.8	12.2	96	96	93	95	0.5	0.8	1.1	0.8	10 •	9	10 •	SSE 2	SW 5	W 3
15	92.1	96.7	98.1	95.6	13.0	14.6	12.1	13.0	16.8	11.7	91	79	95	88	1.4	3.4	0.7	1.8	9	8	8	WNW 7	W 7	WSW 1
16	98.7	99.5	98.8	99.0	15.0	21.8	17.2	17.8	23.2	12.0	91	72	92	85	1.5	7.4	1.6	3.5	8 ⊙	7 ⊙	0	SW 5	SW 6	SSE 1
17	98.5	98.1	98.1	98.2	14.7	25.7	18.8	19.5	26.5	13.5	93	58	88	80	1.1	13.7	2.5	5.8	0 ⊙	0 ⊙	2	SE 3	SSW 5	SW 1
18	97.0	99.5	100.8	99.1	15.8	21.6	11.1	14.9	22.0	11.1	96	63	88	82	0.7	9.5	1.6	3.9	0 ⊙	0 ⊙	0	SW 1	NW 4	NW 2
19	102.2	102.9	103.6	102.9	10.8	18.0	10.8	12.6	18.9	9.1	97	64	95	85	0.4	7.4	0.7	2.8	0 ⊙	2 ⊙	0	NW 2	NW 3	NE 1
20	105.0	104.9	104.8	104.9	8.0	16.9	10.6	11.5	17.6	6.3	96	66	92	85	0.4	6.4	1.0	2.6	0 ⊙	3 ⊙	0	NE 1	E 4	NE 1
21	105.7	105.9	106.9	106.2	10.0	17.2	9.3	11.4	18.2	7.6	84	62	89	78	1.9	7.4	1.3	3.5	2 ⊙	1 ⊙	0	E 2	ESE 3	C 0
22	108.4	108.9	108.5	108.6	5.4	16.8	9.0	10.0	17.4	4.0	95	55	85	77	0.5	8.9	2.0	3.8	0 ⊙	1 ⊙	7	E 3	SE 3	E 1
23	108.2	107.3	105.8	107.1	6.0	17.2	7.4	9.5	17.9	4.8	91	50	86	76	0.9	9.9	1.5	4.1	0 ⊙	0 ⊙	0	E 1	E 2	C 0
24	104.1	103.2	101.8	103.0	5.0	18.0	9.4	10.4	18.2	3.9	86	44	78	69	1.2	11.5	2.6	5.1	0 ⊙	0 ⊙	0	ENE 2	ESE 1	E 1
25	98.6	97.6	100.6	98.9	6.6	18.3	9.9	11.2	18.9	4.9	90	57	97	81	1.0	9.0	0.3	3.4	4 ⊙	10	2	SE 1	SSW 1	W 2
26	101.1	101.4	100.7	101.1	7.2	14.6	9.0	10.0	15.7	5.6	97	61	92	83	0.3	6.5	1.0	2.6	5 ⊙	7 ⊙	8	W 3	WNW 5	NW 1
27	99.3	98.6	98.2	98.7	5.1	15.4	9.0	9.1	16.9	2.4	98	68	86	84	0.1	5.7	1.6	2.5	2 ⊙	5 ⊙	0	NW 1	NW 1	C 0
28	99.2	99.4	100.4	99.7	6.6	16.8	11.4	11.6	18.3	5.6	90	58	76	74	1.0	8.0	3.3	4.1	0 ⊙	4 ⊙	0	ESE 2	SE 3	E 3
29	100.3	99.0	98.8	99.4	7.5	17.9	13.2	13.0	18.6	7.5	89	58	80	76	1.2	8.5	3.0	4.2	2 ⊙	4 ⊙	10	SE 4	SE 6	E 5
30	98.6	98.5	99.6	98.9	10.8	12.5	10.8	11.2	13.6	10.8	96	89	90	92	0.5	1.5	1.4	1.1	10	10	0	E 2	E 4	E 4
31																								
M	96.8	96.9	96.8	96.8	10.9	18.2	12.4	13.5	19.1	9.3	94	66	89	83	0.8	7.6	1.6	3.3	4.4	5.0	4.4	2.5	4.0	2.0

Październik – Octobre

1	102.2	103.2	103.7	103.7	6.4	12.8	9.4	9.5	13.9	6.0	100	75	89	88	0.0	3.8	1.3	1.7	9	7 ⊙	5	E 4	SE 6	E 3
2	107.8	108.6	108.9	108.4	9.0	10.9	10.3	10.1	11.7	7.7	100	95	99	98	0.0	0.6	0.1	0.2	10 ≡	10	0	E 4	E 5	ENE 1
3	108.8	108.9	108.0	108.6	7.9	16.8	10.4	11.4	17.2	7.5	97	65	85	82	0.2	6.6	1.9	2.9	0 ⊙	3 ⊙	0	E 3	E 6	E 2
4	106.6	105.5	105.1	105.7	7.8	17.3	11.5	12.0	17.8	6.4	97	63	72	77	0.3	7.3	3.8	3.8	0 ⊙	0 ⊙	0	E 5	ESE 5	E 5
5	103.7	103.2	103.3	103.4	8.1	17.2	12.4	12.5	18.4	8.1	89	59	72	73	1.2	8.0	4.0	4.4	0 ⊙	5 ⊙	0	ESE 5	ESE 4	ESE 6
6	102.2	100.5	98.2	100.3	8.0	17.4	11.6	12.2	18.3	7.9	90	64	77	77	1.0	7.2	3.1	3.8	0 ⊙	0 ⊙	0	ESE 5	ESE 5	ESE 3
7	94.9	92.4	91.1	92.8	7.5	15.1	11.4	11.4	16.1	7.3	91	59	66	72	0.9	7.0	4.6	4.2	0 ⊙	0 ⊙	0	ESE 6	E 7	ESE 5
8	89.8	89.7	92.0	90.5	9.2	12.1	12.2	11.4	13.3	9.1	79	72	73	75	2.4	4.0	3.8	3.4	10	10	10	ESE 5	SE 3	SE 3
9	98.7	102.7	106.5	102.6	10.3	14.8	9.8	11.2	16.1	9.5	99	76	95	90	0.1	4.0	0.6	1.6	10	4 ⊙	0	SW 1	SW 3	SW 1
10	108.6	108.5	107.5	108.2	6.4	17.9	11.3	11.7	18.0	5.8	100	66	89	85	0.0	6.9	1.5	2.8	7 ≡	5	0	C 0	S 4	SSE 2
11	106.1	104.2	102.3	104.2	7.3	17.0	10.2	11.2	17.5	7.2	96	57	88	80	0.4	8.3	1.4	3.4	2 ⊙	4 ⊙	2	SE 2	SSE 5	S 1
12	103.3	105.3	106.5	105.0	10.2	14.6	7.7	10.0	16.1	5.9	97	65	91	84	0.3	5.8	0.9	2.3	10	5 ⊙	0	NW 2	NW 7	WNW 2
13	105.8	106.9	107.3	106.7	7.6	15.3	6.7	8.6	14.3	6.3	100	59	94	84	0.0	6.3	0.6	2.3	10 ≡	9	0	NW 1	NNW 6	NW 1
14	104.3	103.6	104.3	104.1	8.6	13.1	10.8	10.8	14.2	5.8	97	79	92	89	0.3	3.1	1.0	1.5	10	9	10	WNW 4	NW 7	NW 5
15	102.3	100.5	98.9	100.6	10.2	11.4	10.9	10.8	11.9	10.0	92	79	78	83	0.9	2.8	2.9	2.2	10	10	10	W 2	WNW 9	NW 7
16	97.3	95.5	92.2	95.0	9.8	12.0	9.4	10.2	12.6	8.7	88	72	92	84	1.4	4.0	1.0	2.1	10	6 ⊙	10	WSW 2	SW 4	W 3
17	87.5	83.4	76.2	82.4	8.8	8.8	7.6	8.2	10.0	7.6	93	96	93	94	0.8	0.4	0.7	0.6	10	10	10	SW 4	SSW 3	S 3
18	69.1	70.1	72.6	70.6	9.8	12.0	9.8	10.4	12.4	7.4	92	81	100	91	0.9	2.7	0.0	1.2	10	10	10	SE 3	SSE 3	E 1
19	75.2	78.0	80.7	78.0	8.9	10.1	12.2	10.8	12.2	8.7	97	97	98	97	0.3	0.4	0.3	0.3	10	10 •	10 •	S 3	SE 1	SE 3
20	86.3	89.8	91.3	89.1	11.2	11.8	11.4	11.4	12.4	11.1	99	87	99	95	0.2	1.8	0.2	0.7	10 ≡	10	8	SSE 1	C 0	NE 1
21	90.8	91.4	95.8	92.7	10.0	13.1	9.4	10.5	13.6	9.3	95	84	83	87	0.7	2.5	2.0	1.7	9	9	6	E 4	E 6	SE 3
22	99.6	102.7	103.8	102.0	5.8	11.0	7.6	8.0	12.1	5.7	91	73	94	86	0.8	3.5	0.6	1.6	2 ⊙	9	0	SE 5	SSE 2	ESE 2
23	102.4	101.7	100.3	101.5	6.0	10.4	7.6	7.9	10.9	5.8	95	72	94	87	0.5	3.5	0.6	1.5	10	3 ⊙	9	E 3	SE 4	SE 4
24	98.9	100.1	97.1	98.7	8.6	11.2	9.5	9.7	11.6	7.5	100	80	96	92	0.0	2.6	0.5	1.0	10	9	8	SW 4	SW 3	SSE 3
25	91.8	91.5	92.1	91.8	6.7	10.4	10.6	9.6	11.1	6.6	93	90	92	92	0.7	1.3	1.0	1.0	10	10 •	9	SSE 5	SW 7	SSW 4
26	92.1	91.0	91.4	91.5	10.3	12.4	10.0	10.7	12.9	9.8	99	90	93	94	0.2	1.4	0.8	0.8	10 •	10	10	S 2	S 4	SSE 1
27	89.3	88.1	88.8	88.7	9.0	15.1	10.9	11.5	15.4	8.8	92	69	92	84	1.0	5.3	1.0	2.4	7	9	9	SSE 1	SSE 4	S 1
28	90.5	90.4	90.4	90.4	10.3	13.2	8.6	10.2	13.2	7.9	93	86	97	93	0.6	2.1	0.3	1.0	10	10	10 ≡	ESE 1	SE 1	S 1
29	90.6	90.9	91.9	91.1	8.6	9.6	9.2	9.2	10.1	7.3	94	92	96	94	0.6	1.0	0.4	0.7	10	10 •	10	C 0	NW 1	WSW 1
30	92.8	93.4	95.4	93.9	7.7	8.6	6.0	7.1	9.8	6.0	97	94	97	96	0.3	0.6	0.3	0.4	10 ≡	10	0	S 2	SW 4	SW 1
31	94.4	91.5	91.5	92.5	5.0	8.3	7.8	7.3	9.2	2.3	97	93	91	94	0.3	0.8	0.9	0.7	10 ≡	10	1	SW 3	SW 6	SW 6
M	96.6	96.6	96.7	96.6	8.4	12.9	9.8	10.2	13.7	7.4	95	77	89	87	0.6	3.7	1.4	1.9	7.6	7.3	5.1	2.9	4.4	2.7

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 125\,m$ **Wrzesień – Septembre 1961**

DNI	WIDZIALNOŚĆ v	OPAD r	GRUBOŚĆ ŚNIEGU h	USŁONIECZNIENIE	POGODA
1	7	.	.	–	= 5²⁰–9³⁰, ⌒ 1-0 0⁰⁰–10⁰⁰ ⌒ ° 22⁰⁰–24
2	8	.	.	–	= 5³⁰–7¹⁵, ⌒ 1-2 0⁰⁰–10⁰⁰ ⌒ ¹ 20⁰⁰–24
3	7	.	.	–	= 4¹⁵–9³⁰, 16¹⁰–21⁴⁰ ≺ 21¹⁰–23⁴⁰, ⌒ 2-1 na – a ⌒ 1-2 p – np
4	7	.	.	–	= 3¹⁰–11³⁰, ⌒ 2-1 1⁰⁰–10⁰⁰, ⌒ ¹ 20⁰⁰–24
5	7	5.3	.	–	• ° 21⁵⁰–22¹⁰, ⌒ 2-0 na – a
6	7	0.3	.	–	• ° 2⁰⁰–3³⁵ 18²⁰–19¹⁰, ▽ ° 2⁰⁰–3³⁰ E-W, ≡ 0-1 4³⁵–9¹⁵ = –13³⁰
7	7	7.6	.	–	• ° 7³⁰–12¹⁰, 16⁴⁶–19⁰⁰, = 4³⁰–11³⁰, ⌒ 18²⁰–35
8	6	0.6	.	–	• ° 0⁵⁰–7⁰⁵, 13²⁵–16¹⁰, 17²⁰–18¹⁵, 23⁴⁵–24, » 9³⁰–13²⁰, = p
9	7	0.3	.	–	• ° 0⁰⁰–10 10⁴⁸–12¹⁵, = 0⁰⁰–8³⁰
10	7	1.2	.	–	• ° 3⁴⁵–4¹⁰, 14¹⁸–19¹⁰, = na – a
11	7	0.0	.	–	= na, a p, np, ⌒ ¹ 20⁰⁰–24
12	7	0.6	.	–	• ° 6⁴⁵–48 • ¹ 15¹⁰–25 ▽ ° 20³⁵–21¹⁵, = 0⁰⁰–13³⁰ 21⁵–24, ⌒ 1-0 0⁰⁰–8⁰⁰
13	7	1.0	.	–	• ° 3⁴⁰–4³⁰ 18⁵⁴–19⁰² 22⁴³–23⁰⁷, = 0⁰⁰–1⁰⁰, 4³⁰–6¹⁵
14	6	10.9	.	–	• ° 5⁴⁰–11⁴⁰ • ° 15²⁰–40 19⁴⁵–20⁰⁵ • °–23³⁵, = 5⁴⁰–24
15	7	0.0	.	–	• 0-1 0⁰⁵–3¹⁵ • ° 10¹⁰–20, = 0⁰⁰–6³⁰
16	7	.	.	–	= 19¹⁵–21⁴⁰, ⌒ 1-2 20⁰⁰–24
17	8	.	.	–	= 5¹⁰–7³⁰, ⌒ 2-1 0⁰⁰–11⁰⁰ ⌒ 1-2 20⁰⁰–24
18	7	.	.	–	= 4³⁰–8⁵⁰ ≡ 0-1 10⁴⁵ = –12¹⁵, ⌒ 2-1 0⁰⁰–11⁰⁰ ⌒ ¹ p – np
19	7	.	.	–	⌒ 2-1 na – a, p – np
20	7	.	.	–	= 5¹⁵–8³⁰, ⌒ 2-1 1⁰⁰–11⁰⁰ ⌒ ¹ 20⁰⁰–24
21	7	.	.	–	⌒ 2-1 0⁰⁰–11⁰⁰ ⌒ ¹ p – np
22	8	.	.	–	⌒ ² na – a ⌒ ¹ p – np
23	7	.	.	–	⌒ 2-1 0⁰⁰–10⁰⁰ ⌒ 0-2 19⁰⁰–24
24	7	.	.	–	⌒ 2-1 na – p ⌒ ¹ 20⁰⁰–24
25	7	0.2	.	–	• ° 13¹⁵–35 14⁰²–15, = 15⁰⁵–24, ⌒ 2-1 0⁰⁰–11⁰⁰ ⌒ 0-1 20⁰⁰–24
26	8	.	.	–	= 0⁰⁰–7³⁰, ⌒ ² 0⁰⁰–8⁰⁰ ⌒ ¹ 20⁰⁰–24
27	8	.	.	–	= 6¹⁰–9³⁰, ⌒ ² 0⁰⁰–10⁰⁰, 20⁰⁰–24
28	7	.	.	–	= 5³⁰–7⁴⁵ 18¹⁰–24, ⌒ ² 0⁰⁰–4⁰⁰ ⌴ ¹–8⁰⁰ ⌒ ¹ 20⁰⁰–24
29	7	2.2	.	–	= 0⁰⁰–7⁴⁰, ⌒ 1-0 0⁰⁰–11⁰⁰
30	6	.	.	–	• ° 3²⁰–4⁰⁵, = 2³⁰–11⁴⁰, 12¹⁵–21³⁰, ⌒ 0-1 21⁰⁰–24
31					
Σ	–	30.2	–	–	UWAGI

Październik – Octobre

1	7	.	.	–	= 5¹²–12³⁰, np, ⌒ 2-0 0⁰⁰–10⁰⁰
2	5	.	.	–	= 0⁰⁰–6⁴⁵ ≡ ° 8³⁰ = –24, ⌒ 2-1 0⁰⁰–11⁰⁰ ⌒ ¹ 20⁰⁰–24
3	7	.	.	–	= 0⁰⁰–9³⁰, ⌒ 2-1 na – a
4	7	.	.	–	= 5¹⁰–10³⁰, ⌒ ¹ 0⁰⁰–11⁰⁰, 21⁰⁰–24
5	7	.	.	–	⌒ ¹ 1⁰⁰–8⁰⁰
6	7	.	.	–	⌒ ¹ 20⁰⁰–24
7	7	0.0	.	–	⌒ 1-0 0⁰⁰–10⁰⁰
8	7	1.3	.	–	• ° 0⁴⁵–1³⁵ 14⁴⁵–16²⁰
9	7	.	.	–	• ° 4²⁰–6⁴⁵, = 6³⁰–12³⁰, 21³⁰–23⁴⁰ ≡ ¹–24, ⌒ ° np
10	7	.	.	–	≡ 0-1 0⁰⁰–7⁵⁰ = –9³⁰, ⌒ ² 0⁰⁰–10⁰⁰
11	7	.	.	–	= 4²⁰–10³⁰, ⌒ ¹ 0⁰⁰–11⁰⁰
12	7	.	.	–	= 1⁰⁰–9³⁰, ⌒ ¹ 0⁰⁰–10⁰⁰, 20⁰⁰–24
13	7	0.2	.	–	= 3¹⁵–5³⁵ ≡ ° 7²⁰ = –9³⁰, ⌒ ¹ 1⁰⁰–10⁰⁰
14	7	.	.	–	• ° 5⁶⁰–6⁴⁵, = 12⁰–8³⁰
15	7	.	.	–	
16	7	.	.	–	= 18³⁰–24
17	6	3.5	.	–	• ° 10⁴⁵–11³⁵ • ° 13⁴⁰–16²⁰ • °–17¹⁵ 18⁵⁰–19¹⁰, = na – p, ⌒ ° na – a
18	7	7.4	.	–	▽ ° 11¹⁵–23 14⁵⁵–15²⁰ • °–17⁴⁰ 23¹⁰–24, = 8³⁰–12³⁰ ¹ 15³⁰–24
19	5	11.6	.	–	• 0-1 0⁰⁰–6²⁰, 10⁴⁸–16⁵⁴, 20³⁵–24, = 0⁰⁰–24
20	6	0.6	.	–	• ° 0⁰⁰–1⁵² • ° 7³⁵–8¹⁵ • ° 9⁴⁵–10⁴⁰, = 0⁰⁰–6⁴⁰ ≡ °–7⁵⁰ = –24, ⌒ ° p – np
21	6	.	.	–	= 0⁰⁰–20³⁰, ⌒ ¹ 0⁰⁰–10⁰⁰
22	7	.	.	–	= a, p – 24
23	7	5.6	.	–	= na, a
24	7	.	.	–	• ° 3⁰⁵–5²⁰, = 3³⁰–9¹⁰, 15¹⁵–24
25	6	2.2	.	–	• ° 10⁵⁰–11⁰⁵, 11⁴⁵–13²⁵, 23⁴⁰–50, = 0⁰⁰–2⁵⁰
26	6	1.1	.	–	• ° 1⁰⁰–2³⁰ 6⁵⁰–8⁴⁰ • ° 9⁵⁰–11³⁵, = 1⁰⁰–18¹⁵, 20⁰⁵–24
27	7	.	.	–	= 0⁰⁰–11²⁰ 16⁰⁵–17³⁰
28	6	0.0	.	–	= 5¹⁰–18⁵⁰ ≡ 0-1 24, ⌒ ¹ 0⁰⁰–10⁰⁰, 19⁰⁰–24
29	6	5.8	.	–	• ° 6³⁵–38 • ° 8¹⁵–13¹⁰ 16⁵⁰–17⁴⁵ 19³⁰, = ¹ 0⁰–3⁴⁵ = –16³⁰, p – 24, ⌒ ¹ na
30	5	.	.	–	= 0⁰⁰–5⁴⁵ ≡ 0-1 9⁵⁰ = –21⁴⁰ ≡ 0-2 24, ⌒ ¹ np
31	6	1.1	.	–	• ° 16⁴⁵–50 • ¹ 17²⁵–40, ≡ 2-0 0⁰⁰–8⁴⁰ = –17¹⁵, ⌒ ² na – a
Σ	–	40.4	–	–	UWAGI

Chojnice — φ = 53°42' — λ = 17°33' — Listopad – Novembre 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.6	95.6	96.7	94.6	9.0	8.7	9.1	9.0	9.8	6.6	93	93	89	92	0.8	0.7	1.3	0.9	10 •	10	10	W 5	SW 9	W 7
2	99.2	96.8	89.8	95.3	7.5	8.9	8.8	8.5	9.7	6.6	91	86	86	88	0.9	1.5	1.5	1.3	10	10	10	SW 5	SW 7	S 6
3	82.5	80.7	82.3	81.8	8.6	9.2	5.4	7.2	9.4	5.1	85	79	87	84	1.7	2.4	1.2	1.8	10	10	0	S 6	SW 12	SW 6
4	84.5	86.9	91.3	87.6	3.0	4.3	1.9	2.8	5.4	1.9	88	77	93	86	0.9	1.9	0.5	1.1	5	10	0	SW 8	SW 5	SW 3
5	93.3	94.8	97.8	95.3	0.9	5.6	5.0	4.1	6.3	−0.5	94	85	87	89	0.4	1.4	1.1	1.0	10	10	10	NW 2	NNW 1	N 2
6	98.5	97.5	94.8	96.9	6.0	8.0	7.0	7.0	8.2	4.2	88	80	97	88	1.2	2.1	0.3	1.2	9	10	10	NNE 2	NE 6	NE 4
7	90.4	88.0	86.5	88.3	8.0	8.4	9.4	8.8	9.5	6.8	94	93	93	93	0.6	0.7	0.8	0.7	10	10 ◕	10	ENE 4	E 6	ESE 4
8	86.4	86.5	86.8	86.6	8.8	8.0	4.5	6.4	9.5	4.3	97	94	87	93	0.3	0.6	1.1	0.7	10 •	10 •	10	SE 2	SSW 2	SW 2
9	84.4	83.9	83.5	83.9	4.0	5.5	5.5	5.1	6.3	2.4	92	88	94	91	0.6	1.1	0.5	0.7	10	10	10	SSE 1	SSE 4	SE 4
10	83.0	82.6	84.1	83.2	4.7	6.2	5.6	5.5	6.4	4.2	94	88	97	93	0.5	1.2	0.3	0.7	10	10 •	10 ◕ ▬	ESE 4	E 3	SW 2
11	85.1	85.9	89.0	86.7	6.0	7.0	8.1	7.3	8.3	5.4	100	96	96	97	0.0	0.4	0.5	0.3	10 ▬	10 •	10	SW 1	C 0	E 2
12	91.1	92.9	95.1	93.0	7.2	5.6	2.9	4.6	8.3	2.8	94	91	88	91	0.6	0.9	0.9	0.8	10 ◕	10	10	E 5	E 5	E 6
13	95.3	94.6	92.8	94.2	1.3	1.2	−0.1	0.6	3.0	−0.2	92	89	90	90	0.5	0.8	0.7	0.7	10	10	10	NE 8	NE 6	NE 6
14	92.4	94.7	98.2	95.1	0.2	2.0	2.6	1.8	2.6	−1.0	96	89	88	91	0.3	0.8	1.0	0.7	10 ◕	10	10	NE 5	NE 5	NE 3
15	98.1	97.6	96.3	97.3	2.1	4.4	2.4	2.8	4.8	1.7	78	69	89	79	1.5	2.6	0.8	1.6	10	10	10	N 1	W 1	WSW 5
16	94.7	92.8	89.9	92.5	1.2	2.5	2.3	2.1	2.9	1.2	96	95	95	95	0.3	0.4	0.4	0.4	10	10	10	WSW 5	WSW 8	WSW 6
17	86.0	87.4	88.7	87.4	5.2	6.6	1.1	3.5	7.8	0.7	97	91	94	94	0.2	0.8	0.4	0.5	10 ◕	10 •	3	W 4	W 4	W 1
18	85.0	85.9	90.3	87.1	1.5	5.2	1.2	2.3	5.4	0.0	94	63	83	80	0.4	3.2	1.2	1.6	10	2	9	W 2	NW 9	NW 1
19	94.1	99.3	105.8	99.7	0.7	1.8	1.0	1.1	3.5	0.0	86	89	77	84	0.9	0.8	1.5	1.1	9	4 ⊙	8 ⚹	NW 2	NW 3	NW 2
20	111.1	113.2	114.1	112.8	1.0	4.5	0.0	1.4	4.8	−0.2	88	60	86	78	0.8	3.3	0.9	1.7	8	6	10	N 2	NW 2	C 0
21	110.8	109.0	106.5	108.8	−0.6	2.4	−1.9	−0.5	2.5	−1.9	87	66	87	80	0.7	2.5	0.7	1.3	10	10	8	W 4	W 6	W 1
22	102.9	101.2	98.7	100.9	−4.3	3.0	−2.7	−1.7	4.0	−4.9	86	66	89	80	0.6	2.6	0.6	1.3	6	2 ⊙	0	C 0	SW 1	WSW 1
23	94.9	93.0	91.7	93.2	−4.6	4.7	−2.2	−1.1	5.8	−5.4	88	62	89	80	0.5	3.2	0.6	1.4	0	2 ⊙	0	C 0	SSE 1	SW 1
24	92.8	95.0	96.6	94.8	−1.6	2.9	0.4	0.5	3.1	−3.5	90	96	98	95	0.5	0.2	0.1	0.3	10	10 ▬	10 ▬	C 0	C 0	C 0
25	94.3	92.4	91.2	92.6	1.2	1.5	0.5	0.9	1.8	0.3	96	100	100	99	0.3	0.0	0.0	0.1	10 ▬	10 ▬	10 ▬	SE 2	SW 2	SSW 1
26	89.4	89.1	86.6	88.4	0.1	0.1	0.6	0.4	0.8	−0.4	100	98	98	99	0.0	0.2	0.1	0.1	10 ▬	10 ▬	10 ▬	SW 2	S 1	E 1
27	83.6	82.9	83.7	83.4	0.1	1.6	2.1	1.5	2.2	−0.2	98	98	98	98	0.2	0.2	0.1	0.2	10 ▬	10 ◕ ▬	10 ◕ ▬	E 1	NE 1	N 1
28	87.7	90.3	92.5	90.2	0.3	2.6	1.0	1.2	3.4	−1.7	98	89	94	94	0.1	0.8	0.4	0.4	10 ▬	3	10	C 0	NE 1	ESE 2
29	91.9	91.0	90.4	91.1	1.4	3.9	3.2	2.9	3.9	0.5	98	98	86	94	0.2	0.2	1.1	0.5	10 ▬	10 ▬	4	SE 3	SW 3	SW 4
30	82.8	82.5	74.1	79.8	2.2	4.6	5.1	4.2	5.2	1.5	93	87	90	90	0.6	1.1	0.9	0.9	10	10	10 •	SW 7	SW 5	SW 10
31																								
M	92.0	92.1	92.2	92.1	2.7	4.7	3.0	3.4	5.5	1.2	92	85	91	89	0.6	1.3	0.7	0.9	9.2	8.6	8.1	3.1	4.0	3.1

Grudzień-Décembre

1	67.8	72.9	75.1	71.9	7.8	5.2	4.2	5.4	8.2	2.0	87	78	90	85	1.4	1.9	0.8	1.4	10 •	9	10	W 12	W 8	WSW 8
2	68.1	64.8	72.4	68.4	3.2	10.3	3.6	5.2	10.9	2.5	97	87	86	90	0.3	1.6	1.1	1.0	10 •	10 •	10	SE 5	SW 8	W 12
3	82.5	83.6	83.4	83.2	1.5	3.0	1.2	1.7	3.7	0.4	85	72	85	81	1.0	2.1	1.1	1.4	10	4	10	WSW 7	SW 9	SW 5
4	81.3	86.2	88.7	85.4	0.3	3.8	0.5	1.3	4.0	−0.4	94	83	96	91	0.3	1.3	0.2	0.6	7	7 ⊙	10	SW 2	W 3	SE 3
5	79.7	80.9	78.3	79.6	10.2	12.0	11.2	11.2	12.4	0.4	97	87	73	86	0.3	1.8	3.6	1.9	10 •	9	9	SW 7	SW 7	SW 12
6	85.2	86.2	89.9	87.1	1.6	2.1	0.6	1.2	11.3	0.4	71	69	82	74	2.1	2.2	1.1	1.8	2	9	2	WSW 8	WSW 10	WSW 8
7	90.8	92.1	94.4	92.4	−0.9	−0.2	−0.4	−0.5	0.7	−1.5	92	94	92	93	0.5	0.4	0.5	0.5	9	10	10	W 3	WSW 4	W 3
8	93.7	94.0	95.5	94.4	−0.3	0.4	−0.5	−0.2	0.6	−1.0	92	82	84	86	0.5	1.1	1.0	0.9	10	6 ⊙	10	SW 5	SW 6	WSW 6
9	96.7	96.9	94.0	95.9	−1.3	−1.5	−1.2	−1.3	−0.4	−3.4	86	92	80	86	0.8	0.4	1.1	0.8	3	10	0	W 3	S 1	SE 2
10	90.0	89.0	87.5	88.8	−1.5	−0.6	0.5	−0.3	0.6	−1.7	82	95	98	92	1.0	0.3	0.1	0.5	10	10	10 ▬	SE 2	SSW 4	SSW 2
11	81.8	74.7	74.6	77.0	0.6	0.7	0.6	0.6	1.5	0.5	98	98	98	98	0.1	0.1	0.1	0.1	10 ▬	10 • ▬	10 ▬	SE 2	SE 2	ENE 1
12	84.4	88.0	94.5	89.0	1.2	0.3	−2.2	−0.7	1.3	−2.2	96	92	79	89	0.3	0.5	1.1	0.6	10	10	10	NE 4	NE 4	NE 3
13	103.1	106.7	109.8	106.5	−4.4	−0.9	−5.3	−4.0	−0.7	−5.3	81	69	85	78	0.8	1.8	0.6	1.1	0	4	0	C 0	NE 3	NE 2
14	110.2	111.0	110.0	110.4	−5.7	−5.4	−4.9	−5.2	−4.4	−6.4	84	72	86	81	0.6	1.1	0.6	0.8	9	8	2	ENE 1	NNE 1	NW 3
15	105.9	103.0	110.0	106.3	−2.3	−0.9	−11.2	−6.4	−0.5	−11.4	83	83	72	79	0.9	1.0	0.7	0.9	10	10 ⚹	2	NW 4	NW 8	NE 4
16	115.8	118.9	123.4	119.4	−14.3	−10.9	−13.9	−13.2	−10.9	−15.1	79	73	79	77	0.4	0.7	0.4	0.5	0	0	0	NE 3	E 2	E 1
17	123.8	123.1	121.6	122.8	−15.3	−9.5	−10.7	−11.6	−9.5	−16.6	82	66	80	76	0.3	1.0	0.5	0.6	0	6	3	C 0	NW 3	NW 2
18	118.3	116.1	113.5	116.0	−7.1	−5.3	−3.6	−4.4	−2.6	−11.2	74	83	87	81	0.9	0.8	0.6	0.8	10	9	10	NW 6	WNW 4	W 7
19	109.8	109.3	108.8	109.3	−0.7	1.1	0.2	0.2	1.7	−3.7	93	98	92	94	0.4	0.1	0.5	0.3	10	10	9	WNW 8	NW 5	NW 1
20	100.7	99.3	99.0	99.7	0.0	0.3	1.1	0.6	2.1	−0.6	94	92	89	92	0.4	0.5	0.7	0.5	10	10 ◕ ▬	10	W 8	WNW 10	NW 5
21	91.0	94.5	94.9	93.5	−0.8	−1.7	−5.4	−3.3	1.2	−5.4	65	84	80	76	2.0	0.9	0.8	1.2	2	2	0	NW 9	NW 7	NW 3
22	87.8	86.0	89.2	87.7	−6.9	−3.6	−7.5	−6.4	−3.5	−8.8	80	87	84	84	0.7	0.6	0.5	0.6	1	9 ⚹	5	C 0	NW 4	NW 3
23	92.5	93.3	95.1	93.6	−10.9	−4.4	−8.5	−8.1	−4.3	−11.7	87	84	86	86	0.4	0.7	0.4	0.5	6	1	0	C 0	NW 3	NW 1
24	94.8	94.1	92.6	93.8	−12.3	−10.4	−9.3	−10.3	−8.4	−14.4	85	80	85	83	0.4	0.5	0.4	0.4	0	0 ○	10	SW 1	SW 4	SW 8
25	91.1	90.4	88.6	90.0	−11.5	−10.3	−15.1	−13.0	−8.9	−15.3	86	81	86	84	0.4	0.5	0.3	0.4	10	0	0	SW 6	SW 3	S 2
26	86.5	85.2	85.8	85.8	−17.7	−12.8	−16.4	−15.8	−12.2	−19.0	84	85	80	83	0.2	0.4	0.3	0.3	0	2	0	C 0	SSW 2	SW 1
27	90.2	92.9	94.7	92.6	−6.8	−5.8	−13.7	−10.0	−5.4	−16.7	88	89	75	84	0.4	0.4	0.5	0.4	10	8	0	N 2	E 2	E 1
28	91.8	89.4	87.8	89.7	−16.8	−13.4	−11.6	−13.4	−11.6	−18.3	80	84	86	83	0.3	0.4	0.4	0.4	10	10	10	ESE 3	ESE 3	SE 2
29	86.9	87.3	87.4	87.2	−7.4	−4.6	−4.3	−5.2	−2.8	−11.7	87	91	89	89	0.4	0.4	0.5	0.4	10	10	5	SSE 1	SSE 1	SE 2
30	84.9	83.9	84.1	84.3	−2.5	−1.8	−1.7	−1.9	−1.6	−4.5	91	96	92	93	0.5	0.2	0.4	0.4	10 ▬	10 ▬	10	SE 3	SE 3	SE 2
31	83.3	84.0	79.7	82.3	−1.7	0.6	−0.8	−0.7	0.7	−2.5	92	94	93	93	0.4	0.4	0.4	0.4	0	4	0	S 1	S 2	SE 3
M	92.6	92.6	93.5	92.9	−4.0	−2.0	−4.0	−3.5	−0.9	−6.5	86	85	85	85	0.6	0.8	0.7	0.7	6.7	7.0	5.7	3.7	4.4	3.8

Chojnice — $H_s = 172\,m$ — $H_b = 177{,}2\,m$ — $h_w = 12{,}5\,m$ — Listopad - Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	0.9	.	–	▽° 1⁰⁰–2⁰ ●° 3⁴⁵–5³⁵ ●° 6⁵⁰ 13⁴⁵ ▽° 15⁴⁰–19¹⁵, = 7³⁰–24
2	6	0.5	.	–	= 0⁰⁰–2³⁰, 7¹⁵–17³⁰
3	7	1.9	.	–	●° 0¹⁵–⁴⁵, 1⁰⁵–2⁵² ▽° 14⁰³–15¹⁵, = 5¹⁰–10³⁰
4	7	.	.	–	
5	7	.	.	–	⌴¹ 3⁰⁰–7⁰⁰
6	7	0.1	.	–	= 22¹⁵–23⁵⁰ ≡° –24
7	6	1.1	.	–	●° 1⁴⁵–3¹⁰ ●°–5¹⁵ ●° 9⁴⁷ 10³⁰ 13¹⁰–15⁵⁰ ●° 17⁵⁷ 18⁴⁰, ≡° na = a–p
8	5	2.7	.	–	●⁰⁻¹ 5⁵⁰–7¹⁵ ●°–13¹⁰ 14⁵⁰, = 4³⁰–17³⁰
9	6	0.0	.	–	▽° 13⁵⁰–14¹⁵, = 5³⁰–17²⁰
10	6	2.7	.	–	▽° 8⁵⁵–9⁰⁴ 12⁵⁰–14¹⁰ ●° 14³⁰–15²⁰ ●² 21⁴⁰ ●° 23¹⁰, = 3³⁰–20⁴⁵ ≡°–24, ⌓° na–a
11	5	1.3	.	–	●° 3⁰⁵–5³⁰ 12¹⁰–13⁴⁰ ●° 16⁰⁵–17³⁵ 21⁴⁵–23³⁵, ≡⁰⁻¹ 0⁰⁰–11⁴⁵ =–24
12	7	0.4	.	–	●⁰⁻² 1⁰⁰–9³⁰ ●°–11²⁰ ▽° 13⁵⁰–14³⁵, = 0⁰⁰–11⁴⁰
13	7	0.0	.	–	
14	6	0.3	.	–	●° 5³⁵–7³⁰ 9¹⁰–11⁵², = 11³⁰–13²⁰
15	7	.	.	–	
16	6	0.3	.	–	●° 9⁵⁰–11⁵⁵ ●¹⁻⁰ 13²⁸–17⁵⁰ ●° 18⁵⁵–19³⁵ 21⁴⁵–23⁵², = 6¹⁰–24
17	5	4.9	.	–	●° 4⁵⁵–8¹⁰ ●°–9⁴⁵ ▽° 10⁰⁵–25 12⁴⁰–13³⁰, = 0⁰⁰–9⁵⁰
18	7	0.4	.	–	⛬° 0⁵⁵–1⁰³ ▽°–1¹⁰ ▽° 5³⁰–45, 6¹⁵–35 ▽° 7⁴⁵–8¹⁰
19	7	0.5	.	–	▽° 9⁵²–⁵⁵ 12¹⁰–²⁰ ⛬° 13⁵⁵ 20⁵⁵, ⌴¹ 5⁰⁰–8⁰⁰
20	7	.	.	–	⌴¹ 3⁰⁰–9⁰⁰
21	7	.	.	–	⌴¹ 0⁰⁰–9⁰⁰ ⌴° 22⁰⁰–24
22	6	.	.	–	= 6¹⁰–13³⁰, 15⁴⁰–24, ⌴¹⁻⁰ 0⁰⁰–11⁰⁰, np
23	6	.	.	–	= 0⁰⁰–24, ⌴²⁻¹ 0⁰⁰–11⁰⁰ ⌴¹ 19⁰⁰–24
24	1	0.5	.	–	= 0⁰⁰–9³⁵ ≡⁰⁻² 24, ⌴²⁻¹ 1⁰⁰–12⁰⁰
25	1	0.1	.	–	●° 3⁰⁵–5¹⁰ 7⁰⁵–²⁰, ≡⁰⁻² 0⁰⁰–16⁴⁰ =–18⁴⁰ ≡⁰⁻²–24
26	2	0.0	.	–	≡²⁻¹ 0⁰⁰–24
27	2	1.2	.	–	●° 12⁴⁰–15⁵⁰ ●° 19³⁰–20²⁰ ●²–22¹⁵, ≡¹⁻² 0⁰⁰–24
28	6	0.0	.	–	≡⁰⁻¹, = 0⁰⁰–18¹⁰
29	2	1.4	.	–	●¹ 16⁴⁰–18³⁵, = 2²⁰–3⁵⁰ ≡⁰⁻² 17⁴⁵ =–20²⁰
30	6	4.8	.	–	▽° 2⁵⁰ 6⁰⁵, 14⁴⁰–16³⁰ ●°–24, = 6⁰⁰–24, ≫ 19³⁰–24
31					
Σ	–	26.0	–	–	UWAGI

Grudzień – Décembre

1	7	5.0	.	–	●° 0⁰⁰–8¹⁵ ▽° 14⁵⁰ 15⁰³ ▲° 14⁵³⁻⁵⁶ ▽° 23⁵³–24, = 0⁰⁰–8³⁰, ≫ 0⁰⁰–8³⁰
2	6	2.8	.	–	▽° 0⁰⁰ 3¹⁰ ●°–8⁴⁰, 9⁵⁵ 10¹⁰ ▽⁰⁻² 12⁴⁰–20⁰⁵, ≫ 8³⁰–11¹⁵ ≫–≫ 15¹⁵–24
3	7	.	.	–	≫ 0⁰⁰–3³⁰
4	7	7.4	.	–	▽° 23³⁰–24, = 16³⁰–24, ⌴° 5⁰⁰–9⁰⁰
5	7	3.2	.	–	▽° 1⁰⁰–⁰⁵ ●°–3³⁵ 4⁴⁰–5³⁵ ▽⁰⁻¹ 6⁵⁰–9⁰⁵, =, ≡° 0⁰⁰–8²⁰, ≫ 18²⁰–22⁴⁰, 23¹⁰–24
6	7	.	.	–	≫ 0⁰⁰–6²⁰, 8³⁰–15⁴⁰
7	7	.	.	–	⌴¹ 0⁰⁰–10⁰⁰
8	7	0.0	.	–	⛬° 7⁴⁵–⁵⁰ 8⁴⁰–9⁰⁵ ✳° 10²⁰–³⁰, 10⁴⁰–11¹⁵
9	6	.	.	–	= 10¹⁵–18¹⁰, ⌴° 5⁰⁰–9⁰⁰
10	5	0.1	.	–	✳° 8⁵²–10⁴⁷, = 7¹⁰–14⁵⁰ ≡⁰⁻¹–24
11	2	6.6	.	–	●° 9¹⁵–17⁴⁵, ≡¹⁻⁰ 0⁰⁰–8⁴⁵ =–11¹⁰ ≡⁰⁻¹–23⁵⁰ =–24
12	6	.	.	–	= 0⁰⁰–21³⁰
13	7	0.0	.	–	✳⁰⁻¹ 9¹⁵–11⁰⁸ ✳° 13⁴⁸–14⁰⁷, ⌴° 2⁰⁰–8⁰⁰
14	7	0.0	.	–	✳° 10⁵⁰–11²⁰ 11⁵⁵–12⁰⁵
15	6	0.6	.	–	✳° 9⁴⁵–12³⁰ ✳°–17⁴⁰, ≫ 14³⁰–15²⁰
16	7	.	1	–	
17	7	.	1	–	V° 2⁰⁰–12⁰⁰
18	7	.	1	–	
19	5	0.0	1	–	●° 9³⁰–12¹⁵ = 4³⁰–7³⁰ ≡°–12³⁰ =–19²⁰
20	5	0.1	p2.	–	◎° 11⁵⁵–14³⁰ ∞° 12⁰⁵–16⁰⁰, =, ≡° 7⁴⁰–19⁵⁵
21	7	0.2	.	–	✳° 8¹⁰–9³⁰ 14⁴⁰–15¹², 12⁵²–16⁰⁵
22	6	0.2	1	–	✳° 2⁵⁵–3¹⁸ ✳° 10⁴⁶–11²⁰, 11⁴⁵–14²⁰
23	8	0.0	2	–	✳° 8⁰⁵–⁵⁰, V° 1⁰⁰–10⁰⁰
24	8	.	2	–	= 16³⁰–24, V° 4⁰⁰–11⁰⁰ 19⁰⁰–24
25	6	.	2	–	= 1⁰⁰–18³⁰, V° 0⁰⁰–24
26	6	.	2	–	= 7¹⁰–24, V¹ 1⁰⁰–24
27	6	.	2	–	= 0⁰⁰–24, V° 1⁰⁰–24
28	6	0.5	2	–	✳° 9⁵⁰–11¹⁵, 12⁵⁵–16¹⁵, = 0⁰⁰–20³⁰, V² 1⁰⁰–24
29	5	.	2	–	= 7¹⁰–22⁴⁰ ≡°–24, V² 0⁰⁰–24
30	2	.	3	–	≡⁰⁻² 0⁰⁰–18⁴⁰ =–24, V² 0⁰⁰–24
31	6	0.1	3	–	●° 23⁵⁰–24, = 9³⁰–22³⁰, V° 0⁰⁰–13⁰⁰
Σ	–	26.8	–	–	UWAGI

Szczecin - Dąbie — φ = 53°24' — λ = 14°37' — Styczeń - Janvier 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dias	I	II	III	Dias	Max	Min	I	II	III	Dias	I	II	III	Dias	I	II	III	I	II	III
1	110.9	112.3	112.6	111.9	1.4	2.3	2.1	2.0	2.8	-0.6	96	93	89	93	0.3	0.5	0.8	0.5	10	10	7	SW 2	SW 2	SW 2
2	111.0	108.6	105.4	107.7	0.8	1.3	0.8	0.9	2.3	-1.4	88	87	86	87	0.8	0.9	0.9	0.9	8	9	8	S 3	SE 5	SSE 8
3	95.1	89.9	94.8	92.6	0.1	2.3	3.7	2.4	4.7	-0.4	88	89	85	87	0.8	0.8	1.2	0.9	10	10 •	10	SSE 8	SSE 8	SW 5
4	95.3	94.0	97.0	95.4	1.1	2.0	1.8	1.7	3.7	0.5	94	100	96	97	0.4	0.0	0.3	0.2	9	10 •	9	SSW 4	C 0	SW 5
5	99.7	101.3	107.0	102.7	2.2	2.8	1.8	2.2	3.2	0.4	84	82	93	86	1.2	1.3	0.6	1.0	9	10	10	SW 4	SW 4	SW 4
6	109.2	106.5	104.8	106.8	1.3	2.1	2.3	2.0	2.3	0.4	87	75	80	81	0.9	1.8	1.4	1.4	6	8	10 •	SW 4	S 7	S 7
7	105.1	105.8	108.5	106.5	2.2	3.0	1.7	2.2	3.3	1.1	78	85	94	85	1.6	1.3	0.4	1.1	9	9	10	S 5	SSE 2	C 0
8	109.3	106.4	102.9	106.2	1.1	2.2	2.1	1.9	2.7	0.4	96	89	95	93	0.2	0.8	0.4	0.5	10	10 *	10 •	W 2	S 2	SW 3
9	105.4	106.0	106.3	105.9	3.2	4.9	2.2	3.1	5.0	1.0	95	82	100	92	0.4	1.6	0.0	0.7	10	7	10	SW 3	SW 4	SW 1
10	108.4	107.2	105.8	107.1	1.4	3.1	2.8	2.5	4.1	0.9	96	84	89	90	0.3	1.2	0.8	0.8	4	9	10 •	SW 4	S 5	SW 6
11	108.8	114.1	120.5	114.5	2.2	2.1	0.8	1.5	3.2	0.7	96	91	77	88	0.3	0.6	1.5	0.8	10 •	10	9	SW 3	N 4	NW 5
12	125.9	128.9	131.3	128.7	-0.1	1.1	-2.6	-1.0	1.2	-2.7	76	72	93	80	1.5	1.9	0.3	1.2	10	2	0	NW 4	NW 5	W 2
13	128.3	125.9	125.0	126.4	-0.8	0.1	1.2	0.4	1.2	-3.1	75	86	98	86	1.4	0.9	0.2	0.8	10	10	10	SW 7	SW 6	SW 3
14	126.1	128.7	133.3	129.4	1.6	2.8	1.4	1.8	3.0	1.2	100	100	96	99	0.0	0.0	0.3	0.1	10 •	10 =	10	SW 2	C 0	C 0
15	135.0	133.8	130.8	133.2	-1.9	0.0	0.2	-0.4	1.5	-2.1	98	98	98	98	0.1	0.1	0.1	0.1	10 =	10 ⊖	10 ⊖	C 0	C 0	W 1
16	127.4	128.4	129.9	128.6	0.1	1.5	0.7	0.8	2.3	-0.2	100	98	98	99	0.0	0.1	0.1	0.1	10 =	10	0	WSW 1	C 0	C 0
17	132.8	135.3	138.5	135.5	-4.5	-1.2	-4.8	-3.8	0.8	-5.6	87	62	64	71	0.6	2.1	1.5	1.4	1	0	0	E 1	SE 4	C 0
18	141.3	142.0	139.9	141.1	-8.9	-4.9	-8.6	-7.8	-4.4	-10.0	76	56	62	65	0.7	1.8	1.2	1.2	0	1	0	C 0	SE 2	SE 1
19	135.1	132.8	131.0	133.0	-9.6	-1.8	-5.6	-5.6	-1.4	-10.4	63	55	49	55	1.1	2.5	2.0	1.9	0	0	0	SSE 1	S 4	SE 3
20	127.1	125.4	125.3	125.3	-6.9	1.2	-3.6	-3.2	1.9	-7.9	66	54	85	68	1.2	3.1	0.7	1.7	0	0	0	SE 3	SE 4	SE 3
21	121.3	120.4	119.1	120.3	-7.0	-2.4	-6.3	-5.5	-0.8	-7.8	88	78	81	82	0.4	1.1	0.7	0.7	0	1	0	SE 3	SE 3	SE 4
22	115.7	113.4	112.6	113.9	-8.5	-3.4	-2.9	-4.3	-1.8	-8.8	86	85	93	87	0.4	0.8	0.3	0.5	6	9	10 *	SE 4	SE 4	SE 3
23	112.7	114.4	117.4	114.8	-7.3	-2.0	-6.9	-5.8	-1.5	-8.1	82	54	74	70	0.6	2.5	0.9	1.3	2	1	0	E 5	E 5	E 3
24	117.2	115.8	113.9	115.6	-7.4	-2.3	-5.0	-4.9	-1.2	-11.5	90	85	95	90	0.3	0.8	0.2	0.4	10 *	9 *	9	C 0	E 2	E 1
25	114.2	115.6	119.2	116.3	-12.2	-5.0	-13.6	-11.1	-4.0	-14.7	85	56	84	75	0.4	1.8	0.4	0.9	2	1	0	C 0	SE 6	C 0
26	124.3	127.4	130.0	127.2	-16.8	-6.9	-15.8	-13.8	-6.6	-17.8	90	50	81	74	0.2	1.8	0.3	0.8	0	0	0	C 0	SE 4	C 0
27	130.9	129.7	125.4	128.7	-14.4	-6.0	-8.2	-9.2	-4.8	-17.3	74	58	57	63	0.5	1.6	1.4	1.2	0	3	0	SE 3	S 1	E 4
28	121.1	118.9	111.7	117.2	-6.1	-2.8	-5.6	-4.0	-1.8	-9.4	71	64	65	67	1.1	1.8	1.7	1.5	8	8	6	SW 7	SW 2	SW 3
29	108.2	111.2	107.4	108.9	2.1	5.3	5.5	4.6	6.2	-4.2	77	75	78	77	1.7	2.2	1.9	1.9	10	9	3	SW 8	SW 8	SW 9
30	99.0	95.6	99.9	98.2	5.2	5.3	3.6	4.5	6.9	3.1	89	91	93	91	0.9	0.8	0.5	0.7	10 •	10	4	SW 9	SW 8	SW 4
31	97.9	96.7	100.2	98.3	4.2	5.9	3.3	4.2	6.5	3.0	92	91	95	93	0.6	0.9	0.4	0.6	10	9	10	SW 5	SW 4	W 4
M	116.1	115.9	116.2	116.1	-2.7	0.4	-1.6	-1.4	1.3	-4.2	86	78	85	83	0.7	1.3	0.8	0.9	6.6	6.6	5.6	3.5	3.8	3.1

Luty - Février

1	96.6	92.3	92.0	93.6	2.1	4.3	3.7	3.3	5.0	1.3	89	82	85	85	0.8	1.5	1.2	1.2	10	10	9	S 4	S 7	SW 7
2	90.6	89.1	89.0	89.6	1.8	4.4	1.2	2.2	3.1	0.8	93	77	85	85	0.6	1.9	1.1	1.2	10 •	6	4	SW 3	SW 7	SW 3
3	91.9	93.3	101.4	96.2	0.8	1.6	1.1	1.2	1.7	-0.3	98	93	81	91	0.2	0.6	1.2	0.7	10 *	10	10	NW 4	W 2	NW 4
4	104.2	102.9	100.0	102.4	0.4	1.2	0.4	0.6	2.3	-1.1	94	77	90	87	0.4	1.3	0.6	0.8	9	9	10	WSW 4	WSW 4	SE 1
5	110.7	115.2	117.7	114.5	-3.6	0.6	-2.9	-2.2	1.0	-3.3	92	82	93	89	0.4	1.1	0.3	0.6	2	6	0	NW 2	NW 3	SW 4
6	112.8	109.0	101.9	107.9	-0.4	1.7	4.2	2.4	4.2	-4.0	80	89	82	84	1.2	0.8	1.4	1.1	10	10	10	S 7	SSW 7	SSW 8
7	101.3	101.3	100.9	101.2	3.6	6.3	4.4	4.7	6.6	3.0	88	71	87	82	0.9	2.9	1.1	1.6	8	8	10	SW 5	SW 7	SW 7
8	110.0	113.4	116.2	113.2	3.2	3.4	1.3	2.3	5.2	0.8	91	93	91	92	0.7	0.3	0.6	0.6	9	10 •	0	W 3	NW 3	C 0
9	108.7	103.6	106.9	106.4	3.0	6.3	6.1	5.4	7.8	0.4	96	100	97	98	0.3	0.0	0.3	0.2	10 •	10 •	10 ⊖	S 3	SW 6	W 3
10	120.2	125.7	122.6	122.8	2.3	3.0	3.4	3.1	6.3	2.2	98	91	91	93	0.1	0.7	0.7	0.5	10 ⊖	10	10	N 6	NW 2	SW 3
11	113.2	108.3	107.4	109.7	4.2	4.7	5.0	4.7	6.3	3.2	95	97	92	95	0.4	0.2	0.7	0.4	10 •	10 •	9	SW 3	SW 3	SW 4
12	103.7	110.9	118.3	111.0	3.4	3.3	2.2	3.3	6.4	1.9	98	94	96	96	0.1	0.6	0.3	0.3	10 ≡ ≈	10	10	C 0	NE 3	NNW 1
13	120.1	122.3	124.7	122.4	1.4	3.0	2.4	2.3	4.3	1.2	100	98	100	99	0.0	0.2	0.0	0.1	10 =	10	10 =	SW 3	C 0	SE 4
14	124.9	125.3	124.8	125.0	4.9	6.3	5.6	5.6	6.8	2.2	97	92	88	92	0.3	0.7	1.1	0.7	10 ⊖	10	9	SW 1	SW 2	C 0
15	125.0	125.6	127.2	125.9	-1.4	8.7	7.6	5.6	11.6	-1.7	100	71	90	87	0.0	3.3	1.0	1.4	0 ≈	4	2	SW 1	W 4	SW 4
16	131.7	134.5	135.9	134.0	6.1	5.8	5.8	5.9	7.8	4.3	97	95	94	95	0.3	0.4	0.6	0.4	10 ⊖	10 ⊖	10	NW 3	NNW 1	NW 1
17	135.3	135.0	133.3	134.5	5.6	8.1	5.7	6.3	9.8	5.1	85	75	88	83	1.4	2.7	1.2	1.8	10	2	0	W 3	SW 3	SW 4
18	131.1	129.6	128.2	129.6	-2.4	11.1	5.0	4.7	12.8	-2.7	100	64	79	81	0.0	4.8	1.8	2.2	10 =	0	0	C 0	SW 3	SW 3
19	128.6	130.1	131.7	130.1	4.0	5.3	5.1	4.9	6.5	3.2	93	94	92	93	0.3	0.3	0.7	0.6	10 ⊖	10	10	NW 1	NW 4	W 3
20	133.2	134.7	134.7	134.2	5.0	4.9	4.8	4.9	6.1	4.3	92	87	89	89	0.7	1.1	1.0	0.9	10	10	10	C 0	WSW 2	WSW 1
21	133.7	133.6	133.0	133.4	3.4	5.6	1.2	2.8	7.1	1.1	93	78	94	88	0.5	2.0	0.4	1.0	10	10	0	S 3	SW 2	S 2
22	133.6	134.3	134.0	134.0	-2.4	7.8	0.4	1.6	8.3	-3.7	98	71	100	90	0.1	3.1	0.0	1.1	1	1	10 ≈	C 0	SE 3	E 2
23	132.8	132.0	130.0	131.6	-0.6	1.4	1.4	0.9	2.1	-0.7	100	96	96	97	0.0	0.3	0.3	0.2	10 ≈	10	10	C 0	SE 5	SE 5
24	127.3	125.7	126.0	126.3	2.0	7.1	2.9	3.7	8.0	1.3	91	70	89	83	0.7	3.1	0.8	1.5	10	1	2	SE 7	S 7	SE 5
25	127.4	128.5	128.4	128.1	1.8	9.1	2.1	3.8	9.1	1.1	89	66	93	83	0.8	4.0	0.5	1.8	5	6	9	SE 3	SE 7	SE 7
26	128.4	129.0	128.0	128.5	0.1	7.6	4.7	4.3	9.6	-0.4	90	64	85	80	0.7	3.7	1.2	1.9	4	9	0	SE 3	S 4	C 0
27	129.2	122.2	120.0	121.8	6.1	10.3	7.7	8.0	12.7	3.0	86	83	90	87	1.3	1.9	1.0	1.4	10 •	10	10	SW 7	SW 6	C 0
28	107.6	99.4	112.3	106.4	4.7	13.1	3.2	6.0	13.1	2.3	98	78	93	90	0.1	3.3	0.3	1.3	10 •	10 •	10 •	E 3	SW 9	W 7
29																								
30																								
31																								
M	118.1	118.2	118.8	118.3	2.1	5.7	3.4	3.6	6.9	0.8	94	83	90	89	0.5	1.7	0.8	1.0	8.3	7.9	6.9	3.1	4.3	3.4

Szczecin-Dąbie $H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 20\,m$ **Styczeń - Janvier 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	p2.	-	= 0⁰⁰–24
2	6	.	.	-	= 0⁰⁰–24
3	6	1.8	.	-	●° 12⁴⁰ 14²⁰ ✱° 7⁴⁵–8⁴⁰ ●° 10³⁰ 11³⁰–12⁴⁰, = 0⁰⁰–6³⁰
4	4	5.3	.	-	●0-1 9³⁷–16³⁵, = 2³⁰–24
5	7	1.0	.	-	●●° 13⁰⁵–14¹⁵, ●° 15³⁵–16²⁰ ✱°–17²⁵ ●°–18³⁵, = 0⁰⁰–7¹⁵, 14³⁰–24
6	7	0.0	.	-	●° 19⁵⁰–21⁴⁵, = 0⁰⁰–8¹⁵
7	7	0.0	.	-	●° 14⁴⁵ 15²⁵, 16²⁰ 18²⁰ = 14³⁰–24, ▽ 1⁵⁰–3⁵⁸
8	6	1.9	.	-	●° 7¹⁵–8⁴⁵, ✱° 12⁴² 14³⁵ = ●° 16⁰⁸–22²⁰, 23³⁵–24, = 0⁰⁰–24, ⊕ 10³⁰–11⁵⁰
9	7	4.0	.	-	●° 0⁰⁰–1²⁵ 16¹⁵–19⁵⁰, = 0⁰⁰–7³⁰, 19⁵⁰–24
10	6	4.1	.	-	●° 16⁴⁵–23³⁰ °–24, = 0⁰⁰–15³⁰, ⌴ 3⁰⁰–11⁰⁰
11	7	0.9	.	-	●° 0⁰⁰–40 ●° 3⁵⁵ 6¹⁵–10³⁰ ●°–12⁴⁰, = 0⁴⁰–12⁴⁰
12	8	.	.	-	✱° 0⁴⁰–3²⁰, ⌴° 20⁰⁰–24
13	5	5.9	.	-	✱° 8⁰⁴ 9⁴⁰ ●°–10⁴⁵ 11⁴⁵–12⁴⁵ 13¹⁵–20⁴⁵, 21⁴⁵–24, = a–24, ⌴° na
14	3	1.0	.	-	●° 0⁰⁰ 8⁴⁵ = 0⁰⁰–10²⁵ ≡0-1 13³⁵ ≡–24
15	4	0.0	.	-	◑° 11³⁵–13³⁰ ●°–16⁵⁰ 17⁵⁰–23⁵⁰ = 0⁰⁰–3¹⁵ ≡°–9¹⁰ ≡–24
16	4	.	.	-	= 0⁰⁰–5⁴⁵ ≡°–9³⁵ ≡–14³⁰, 18³⁰–19³⁰, ⌴° np
17	8	.	.	-	⌴° 0⁰⁰–14⁰⁰, 16⁰⁰–24
18	8	.	.	-	⌴° 0⁰⁰–24
19	8	.	.	-	⌴° 0⁰⁰–24
20	7	.	.	-	= 7⁰⁵–9²⁰ ∞–15³⁰, ⌴° 0⁰⁰–14⁰⁰
21	6	.	.	-	∞ 10³⁰–18³⁰, ⌴° 2⁰⁰–12⁰⁰
22	6	1.6	.	-	✱° 15⁴⁵–16⁴⁵, 18⁴⁵–24, = 7³⁰–24, ⌴° 1⁰⁰–15⁰⁰
23	8	0.0	2	-	✱° 0⁰⁰–4⁴⁵, = 0⁰⁰–7³⁰
24	6	0.1	2	-	✱° 6¹⁰–9⁴⁰ ▽° 11¹⁰⁻³⁰, 11⁴⁰–13⁴⁰, = 4⁴⁰–13⁴⁰, np
25	8	.	2	-	
26	8	.	2	-	
27	6	.	2	-	∞ 11³⁰–24
28	6	.	2	-	= 5³⁰–24
29	7	2.4	2	-	●° 13¹⁰ 14⁵⁰, 23⁵⁰–24, = 0⁰⁰–8¹⁵
30	7	4.1	.	-	●° 0⁰⁰ 7³⁰–3⁵⁰, 4¹⁵–5³⁰ 9⁰⁰–12³⁵, 15⁰⁵–17²⁰
31	6	1.8	.	-	●° 17⁴⁰ 21²⁰, = 7³⁰–21²⁰
Σ	–	35.9	–	-	UWAGI: Kierunki i prędkości wiatru w ciągu całego roku — wg anemometru

Luty - Février

1	8	1.9	.	-	●° 13²⁵–15⁰⁰, 21⁴⁰ 23¹⁵, = 16¹⁰–24
2	7	1.9	.	-	●° 0²⁵–3²⁵ ▽° 4³⁵ 9⁴⁰, = 0⁰⁰–3⁴⁰
3	6	0.1	1	-	✱° 2⁴⁵ 14⁵⁰ ✱° 13³⁵–14²⁰, = 0⁰⁰–15³⁰, 17³⁰–24
4	7	0.1	.	-	✱▽° 17⁰³⁻⁰⁸ ✱° 21¹⁰–24, = 0⁰⁰–3⁰
5	7	.	1	-	✱° 0⁰⁰–15, = 9¹⁰–10⁴⁰
6	6	0.5	.	-	✱° 9⁰³–10³⁰ 11⁵⁰ ●° 21³⁰–22³⁰ 23³⁰, = 11⁵⁰–24
7	7	2.9	.	-	▽° 16⁴⁰–22¹⁵ ●° 23³⁰–24, = 0⁰⁰–7³⁰
8	7	5.9	.	-	●° 0⁰⁰ 2⁴⁵ ▽° 9⁵³–10⁰⁶ 12³²–13¹⁵
9	5	6.0	.	-	●° 3⁴⁰–10⁴⁰ ●°–12⁴⁵ ●°–16¹⁰ 18⁵⁰ 20³⁰ ●°–21⁴⁰ 22²⁵–24
10	6	2.3	.	-	●° 0⁰⁰–9⁴⁸ ●° 18⁵⁰ 19⁵⁵, 22⁵¹ 23¹⁰, = 9⁵⁰–14²⁰ 17²⁰–24
11	6	13.8	.	-	●° 3⁰⁵–15⁴⁵, = 0⁰⁰–24
12	6	0.3	.	-	●° 3⁴⁵–7⁴⁵, = 0⁰⁰–6⁰⁰ ≡°–10³⁵ ≡–24
13	5	0.0	.	-	●° 0⁰⁰ 2⁵⁰ = ≡° 0⁰⁰–24
14	5	0.0	.	-	●° 4⁴⁰–8⁴⁰, 9⁰⁵–10⁴⁸, = 0⁰⁰–24
15	7	0.0	.	-	= ≡ 0-1 0⁰⁰–12⁴⁰ = 14⁴⁵–24, ⌴° 3⁴⁰–8⁰⁰
16	5	0.1	.	-	●° 3⁴⁵–15⁴⁰, = 0⁰⁰–24
17	7	.	.	-	= 0⁰⁰–6³⁰ 16⁴⁵–24
18	6	0.0	.	-	= 0⁰⁰–4⁴⁰ ≡0-2 11¹⁵ = –14¹⁰, 15²⁰–24
19	6	0.0	.	-	●° 3¹⁵–10⁴⁵ 16⁴⁵–19⁵⁸ = 0¹⁰–24
20	6	0.0	.	-	●° 7⁴⁵–8⁴⁵, = 0⁰⁰–14³⁰, 18³⁰–24
21	7	.	.	-	= 0⁰⁰–12³⁰ 16⁴⁰–24
22	7	.	.	-	= ≡° 0⁰⁰–11²⁰ = 17¹⁵–19²⁷ ≡0-2 24, ⌴° 4⁰⁰–9⁰⁰
23	5	0.0	.	-	●° 21⁵⁰–24 ≡1-0 0⁰⁰–10³⁰ = –24
24	6	.	.	-	●° 0⁰⁰–2⁵⁰ = ∞ 0⁰⁰–24
25	6	.	.	-	= ∞ 0⁰⁰–24
26	6	0.1	.	-	= ∞ 0⁰⁰–24
27	6	12.4	.	-	●° 5⁴⁰ 12⁴⁵ ●0-1 16¹⁰–17⁴⁵ ●° 20¹⁰ 21⁰⁰–24, = 0⁰⁰–17⁴⁵
28	7	7.7	.	-	●° 0⁰⁰–10⁴⁰ ▽° 11⁰⁷ 15¹⁸ ●° 15⁴⁵ 23⁰⁰–24, = 9¹⁵–10⁴⁰
29					
30					
31					
Σ	–	56.0	–	-	UWAGI:

Szczecin – Dąbie φ = 53°24' λ = 14°37' Marzec – Mars 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	114.3	119.6	124.0	119.3	4.3	5.6	3.0	4.0	6.0	2.6	93	88	88	90	0.5	1.1	0.9	0.8	10 •	9	6	C 0	NNW 1	W 4
2	125.3	125.9	122.3	124.5	3.6	5.1	5.3	4.8	6.5	1.1	85	75	91	84	1.2	2.2	0.8	1.4	10	10	10 •	W 4	W 5	SW 3
3	125.1	128.4	132.0	128.5	5.3	7.9	5.7	6.2	8.2	4.8	98	90	88	92	0.1	1.0	1.2	0.8	10	10	9	C 0	C 0	C 0
4	134.6	134.4	132.7	133.9	2.4	9.9	6.6	6.4	11.6	2.1	100	54	78	77	0.0	5.7	2.1	2.6	10 ≡	5	5	C 0	W 4	SW 6
5	133.3	134.3	135.0	134.2	5.4	9.3	5.0	6.2	10.6	4.7	92	66	92	83	0.7	4.0	0.7	1.8	10	8	7	NW 3	W 3	W 3
6	134.5	134.3	131.2	133.3	4.5	5.7	1.3	3.2	7.2	0.5	97	89	98	95	0.3	1.0	0.1	0.5	10	10	0	W 2	SW 2	C 0
7	127.5	128.1	130.6	128.7	2.6	12.2	4.9	6.2	13.3	1.3	96	53	94	81	0.3	6.7	0.6	2.5	8	6	0	SW 4	W 4	N 3
8	133.1	134.0	133.6	133.6	1.7	8.9	6.4	5.8	12.9	0.4	98	75	89	87	0.1	2.9	1.0	1.3	0 ≡	1	0	WSW 1	W 4	W 3
9	132.1	131.5	129.2	130.9	2.9	13.3	8.3	8.2	15.3	2.6	96	46	77	73	0.2	8.3	2.6	3.7	4	2	0	WSW 3	W 4	W 2
10	125.2	122.2	119.3	122.2	-1.6	14.9	11.2	8.9	17.4	-1.9	98	46	63	69	0.1	9.2	5.0	4.8	10 ≡	1	0	C 0	SW 4	SW 4
11	119.1	120.8	122.2	120.7	7.5	9.9	7.9	8.3	11.2	6.0	86	74	86	82	1.5	3.1	1.4	2.0	10	10	9	W 6	W 7	W 5
12	117.1	111.1	103.1	110.4	7.3	12.8	11.3	10.7	14.6	6.0	88	58	77	74	1.2	6.2	3.1	3.5	10 •	6	10 •	SW 6	WSW 8	W 10
13	108.9	111.9	115.2	112.0	5.9	8.3	4.8	6.0	11.3	4.3	77	54	75	69	2.1	5.0	2.2	3.1	9	7	9	NW 8	N 8	NNW 2
14	112.3	114.3	114.8	113.8	6.5	9.6	9.9	9.0	10.1	4.3	97	91	84	91	0.3	1.2	1.9	1.1	10 •	10	10	SW 1	W 7	W 5
15	116.0	120.2	121.5	119.2	9.3	13.1	10.7	11.0	13.7	8.9	85	51	80	72	1.7	7.4	2.6	3.9	10	4	9	W 6	NW 7	NW 5
16	118.6	118.3	122.1	119.7	8.7	11.7	9.2	9.7	13.6	8.5	78	64	75	72	2.4	4.8	2.9	3.4	10	6	0	W 8	WNW 8	NW 4
17	122.2	119.1	109.3	116.9	3.4	14.5	12.8	10.9	16.9	3.0	97	55	50	67	0.3	7.5	7.4	5.1	9	10	0	SW 2	SW 5	SW 6
18	101.7	101.6	100.2	101.2	10.8	10.7	6.5	8.6	12.8	6.4	66	43	65	58	4.5	7.4	3.4	5.1	9	1	0	W 7	WSW 8	W 8
19	100.7	106.0	110.5	105.7	3.4	4.4	0.2	2.0	6.5	0.0	86	40	72	66	1.1	5.0	1.7	2.6	9	4	1	W 6	NW 8	N 3
20	110.2	104.1	89.4	101.2	-2.4	4.9	1.0	1.1	5.6	-3.2	91	46	96	78	0.4	4.7	0.3	1.8	4	10	10 *	NW 5	WSW 8	SW 9
21	86.3	91.3	105.2	94.3	1.0	5.7	1.4	2.4	6.1	0.6	96	77	89	87	0.3	2.1	0.8	1.1	10 *	8	8 *	WSW 7	NNW 8	N 8
22	112.6	112.7	109.6	111.6	-2.0	4.5	4.8	3.0	4.8	-2.1	85	51	90	75	0.8	4.1	0.8	1.9	1	10	10	NW 4	W 5	W 5
23	110.1	112.0	114.2	112.1	5.3	7.9	7.7	7.2	8.6	4.5	94	80	79	84	0.6	2.0	2.2	1.6	10	10 •	10	W 4	WNW 7	WNW 6
24	115.7	114.7	116.4	114.9	6.7	10.8	8.7	8.7	10.8	6.1	79	67	78	75	2.0	4.3	2.4	2.9	10	9	5	W 8	W 8	W 7
25	117.8	119.4	119.0	118.7	7.1	9.7	9.0	8.7	13.1	6.1	85	77	77	80	1.5	2.8	2.6	2.3	9	10	8	W 7	WNW 3	WSW 4
26	114.9	108.8	102.3	108.7	7.1	11.7	8.1	8.8	11.9	6.5	85	56	83	75	1.5	6.1	1.8	3.1	9	10	10	WSW 5	WSW 8	W 8
27	103.4	104.1	105.3	104.3	4.0	3.4	1.2	2.4	8.1	1.0	67	90	74	77	2.6	0.8	1.8	1.7	6	6	2	WNW 8	WNW 8	NW 9
28	106.1	106.8	111.1	108.0	1.4	2.5	3.8	2.9	6.6	0.2	92	91	73	85	0.6	0.6	2.1	1.1	7	9 *	10	NW 8	NW 8	NW 5
29	104.3	105.5	102.3	104.0	3.6	7.9	7.5	6.6	8.0	1.8	93	89	89	90	0.5	1.2	1.2	1.0	10 •	10 •	10	WSW 6	W 7	SW 8
30	98.2	101.5	100.0	99.9	8.8	8.9	3.6	6.2	9.0	3.2	88	51	91	77	1.4	5.6	0.7	2.6	9	10	10 •	W 7	WNW 5	NNE 2
31	105.8	106.1	105.1	105.7	0.8	5.9	3.0	3.2	6.4	0.2	88	57	66	70	0.8	4.0	2.6	2.5	4	10	6	WNW 3	W 5	WNW 9
M	115.6	116.2	115.8	115.9	4.4	8.8	6.2	6.4	10.3	2.9	89	66	81	79	1.0	4.1	2.0	2.4	8.3	7.5	5.9	4.5	5.7	5.0

Kwiecień – Avril

1	106.9	99.2	102.6	102.9	0.1	2.0	5.1	3.1	7.5	-0.6	88	96	69	84	0.8	0.3	2.8	1.3	10	10	2	W 4	SSW 7	W 8
2	109.5	109.6	106.1	108.4	1.7	5.3	3.4	3.4	6.0	1.2	90	62	76	76	0.6	3.4	1.9	2.0	9	9	10	NW 1	C 0	SSW 3
3	100.9	104.9	106.6	104.1	0.9	3.6	3.2	2.7	5.8	0.4	98	85	83	89	0.1	1.2	1.3	0.9	10 •	10	10	E 2	W 4	W 3
4	105.9	108.7	112.1	108.2	3.2	8.3	3.8	4.8	9.8	2.1	93	44	77	71	0.5	6.2	1.9	2.9	10	5	8	SW 5	WNW 7	SE 3
5	107.8	104.8	102.5	105.0	4.0	11.5	15.6	11.7	15.6	1.1	92	91	69	84	0.6	1.2	5.5	2.4	10 •	10 •	10	ESE 6	S 4	SW 6
6	107.3	109.4	106.8	107.8	11.5	19.9	17.9	16.8	21.4	11.0	81	53	61	65	2.7	10.8	8.0	7.2	8	4	7	WSW 2	SW 5	S 5
7	106.3	107.0	112.4	108.6	14.7	22.7	10.1	14.4	23.0	10.1	61	47	92	67	6.5	14.7	1.0	7.4	2	6	10 •	SW 6	WSW 4	NNW 1
8	112.0	114.1	116.7	114.3	7.9	6.7	5.3	6.3	10.2	5.1	94	88	78	87	0.6	1.2	1.9	1.2	9	10 •	0	NW 1	NNW 4	WNW 2
9	120.0	122.3	121.2	121.2	2.8	7.9	2.4	3.9	8.6	2.0	76	43	65	61	1.9	6.0	2.6	3.5	5	6	0	NW 4	N 5	E 3
10	118.3	115.5	112.5	115.4	1.2	7.8	2.3	3.4	10.1	0.2	77	42	77	65	1.5	6.2	1.7	3.1	10	7	0	SE 6	SE 6	SSE 2
11	111.2	112.1	115.3	112.9	1.9	12.5	6.9	7.0	12.9	-0.1	73	36	57	55	1.9	9.3	4.2	5.1	0	0	4	E 1	N 2	NNE 5
12	117.2	116.1	113.1	115.5	3.6	15.1	13.7	11.5	17.1	-0.2	63	29	49	47	2.9	12.3	8.0	7.7	1	3	8	ESE 5	SW 3	SW 3
13	111.7	111.3	110.6	111.2	9.7	19.3	11.2	12.8	21.1	7.6	82	45	82	70	2.2	12.4	2.5	5.7	0	4	4	SW 2	WSW 4	C 0
14	108.8	106.2	107.2	107.4	9.5	23.5	14.0	15.2	25.0	5.2	95	40	78	71	0.7	17.3	3.6	7.2	6	6	10 ⊼	C 0	S 6	N 1
15	111.1	112.5	112.9	112.2	12.2	13.2	7.5	10.1	16.2	7.2	88	77	91	85	1.7	3.5	0.9	2.0	6	10	9	NNW 1	NNE 4	NNE 3
16	111.9	110.5	109.9	110.8	7.5	15.3	9.9	10.6	15.4	6.7	94	64	87	82	0.6	6.3	1.6	2.8	8	9	9	NE 3	NE 4	NE 3
17	110.1	111.4	111.6	111.0	9.4	11.4	10.1	10.2	11.8	8.4	87	84	96	89	1.6	2.2	0.5	1.4	8	10 •	8	NE 2	N 1	NNE 1
18	112.2	113.0	115.0	113.4	9.5	11.4	8.1	9.3	12.9	7.9	96	84	93	91	0.5	2.2	0.8	1.2	10	10	3	SW 1	NW 1	NW 2
19	117.3	118.1	118.5	118.0	5.7	11.9	7.3	8.0	13.3	2.4	85	54	79	73	1.5	6.4	2.2	3.4	2	3	0	W 1	NE 4	NE 3
20	121.5	121.6	121.3	121.5	5.0	13.9	7.5	8.5	14.4	1.3	60	33	48	47	3.5	10.6	5.5	6.5	6	1	0	SE 6	SE 6	ESE 3
21	120.0	117.5	113.9	117.1	5.0	14.8	10.6	10.2	15.8	0.9	63	36	50	50	3.3	10.7	6.4	6.8	0	0	0	ESE 6	ESE 10	ESE 3
22	109.3	105.6	102.6	105.8	7.6	19.8	15.9	13.8	21.1	5.1	69	41	62	57	3.2	13.5	6.1	7.6	3	1	0	ESE 5	SSE 7	SE 4
23	102.3	101.6	103.1	102.3	10.2	19.7	13.3	14.1	20.7	7.4	78	40	59	59	2.7	13.6	6.3	7.5	0	4	0	SE 7	S 8	SE 2
24	107.0	107.6	110.3	108.3	10.0	19.1	13.5	14.0	20.0	6.4	69	37	60	55	3.8	13.9	6.2	8.0	1	1	0	SE 4	SE 6	ESE 6
25	113.2	113.2	112.4	112.9	8.5	13.0	11.5	11.1	13.5	5.0	77	54	68	66	2.6	6.9	4.4	4.6	9	9	10	SE 2	SE 8	ESE 2
26	110.0	107.7	107.6	108.4	11.2	18.3	13.6	14.2	18.9	8.7	65	58	61	55	4.7	13.0	6.2	8.0	0	6	9	ESE 5	SE 12	ESE 3
27	108.0	108.1	108.8	108.3	8.4	19.0	13.5	13.6	20.0	5.8	93	50	81	75	0.7	11.1	3.0	4.9	1	6	9	ENE 2	SW 4	SW 4
28	109.4	109.5	109.8	109.6	10.5	13.3	9.3	10.6	13.6	8.4	96	87	96	93	0.5	2.0	0.5	1.0	9	10	9	C 0	WNW 1	NE 4
29	111.3	111.7	112.1	111.7	7.7	14.8	9.3	10.3	15.7	7.2	91	57	79	76	0.9	7.2	2.5	3.5	9	4	5	NE 5	ESE 8	E 4
30	110.6	109.4	109.4	109.8	7.4	16.6	10.9	11.4	18.9	6.0	77	56	70	68	2.3	8.4	3.8	4.8	9	4	9	E 4	NE 4	NNE 3
31																								
M	110.9	110.7	110.8	110.8	7.0	13.7	9.5	9.9	15.2	4.6	82	56	73	70	1.9	7.8	3.5	4.4	5.7	5.9	5.4	3.3	5.0	3.2

Szczecin – Dąbie $H_s = 1\,m$ $H_p = 6{,}9\,m$ $h_w = 20\,m$ Marzec – Mars 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	1.1	.	–	• 0⁰⁰–9⁰⁰ 10⁵⁰ 11²⁵ = 4³⁰–11³⁰, np
2	8	2.9	.	–	• 18³⁰–24 = 0⁰⁰–6¹⁰
3	6	0.0	.	–	• 0⁰⁰–2⁰⁰, 3³⁰ •–6⁴⁰ 16⁴⁵–17⁴⁰, = 20⁰⁰–24
4	8	.	.	–	= 0⁰⁰–6¹⁵ =⁰–9¹⁵ = –10³⁰
5	7	.	.	–	= 2³⁰–10¹⁵, 22³⁰–24
6	6	.	.	–	= 0⁰⁰–15³⁰, 18³⁰–24
7	7	.	.	–	= 0⁰⁰–10⁴⁰, 18⁴⁰–24
8	7	.	.	–	= 0⁰⁰–1⁰⁰ ≡⁰⁻¹–8²⁰ ≡¹⁻⁰–9²⁵ = –12³⁰
9	7	.	.	–	= 2³⁰–9³⁰
10	6	.	.	–	= 1¹⁵–5³⁰ ≡⁰⁻¹–6⁴⁰ ≡²⁻¹–8⁴⁰ =⁰–9³⁵ = –13³⁰ ∞ –23³⁰ = –24
11	6	0.1	.	–	= ∞ 0⁰⁰–24
12	7	0.1	.	–	• 5⁴⁰–7²⁰, 20⁰⁵ 21³⁰–22⁴⁰, = 0⁰⁰–8³⁰, ≫ 20²⁵–24
13	8	1.8	.	–	≫ 0⁰⁰–4³⁰
14	6	0.5	.	–	▽• 2⁴⁸ 3¹⁰ •⁰ 3²⁰ 4⁰⁰–9³⁰ 12¹⁰ •⁰ 15⁴⁰ 16²⁰, = 6³⁰–24
15	8	.	.	–	= 0⁰⁰–6³⁰
16	8	.	.	–	
17	7	.	.	–	= 0³⁰–10³⁰ ∞–15³⁰, ⌓⁰ 1⁰⁰–9⁰⁰, ⊕ 12¹⁵–16³⁰
18	8	1.1	.	–	
19	8	.	.	–	▽• 3⁵⁶–4⁰⁵, 4³⁵–5¹², • 5²⁵–6⁴⁰
20	8	4.2	.	–	▽• 15⁴⁸–56 ✳⁰ 16⁰⁵–10 ✳¹⁻⁰ 16³⁰–22³⁰ •⁰–23³⁰ 24, ⌴⁰ 1⁰⁰–8⁰⁰
21	8	3.3	.	–	• 0⁰⁰. 50 ✳⁰ 6³⁵–7³⁰ ▽⁰ 10⁴⁹ ✳⁰ 15²⁸ ▽•⁰ 21¹² ≫ 16¹⁵–19⁰⁵
22	8	4.1	.	–	✳⁰ 4¹⁰–20 ✳⁰ 13¹⁷. 33 ✳⁰ •⁰–19¹⁰, = 20¹⁵–24, ⊕ 10³⁰–12¹⁵
23	7	0.6	.	–	• ⁰ 2²⁰ 14³⁵ = 0⁰⁰–6⁴⁰
24	7	0.0	.	–	▽• ⁰ 17¹⁰. 24
25	7	0.2	.	–	• ⁰ 10⁴⁰ 12⁰⁰
26	7	1.8	.	–	• ⁰ 16¹⁰–19⁴⁵ ▽•⁰ 21⁴⁰–22⁰⁵, = 3³⁰–8¹⁵ ∞ a, ⊕ 8³⁰–13³⁰
27	8	0.3	.	–	✳⁰⁻² 12⁰⁵ 15³², ≫ 9¹⁰–12⁴⁰
28	8	6.8	.	–	✳⁰ 2⁵⁵–3⁰⁵ ✳⁰ 5⁴⁵–6³⁵ •⁰ ✳ 9³⁵–11⁰⁰ ▽⁰⁻¹ 12²⁵–40 ✳⁰ ▽⁰ ✳⁰ ✳⁰ 12⁵⁰ 14²¹ •⁰ 21⁴⁰–24
29	7	7.3	.	–	• 0⁰⁰–1⁴⁰, 4³⁰–10³⁰, 13⁰⁰–19³⁵
30	7	6.8	.	–	• 4¹⁵–5⁴⁰, 13⁵⁰ 14³⁰–22⁴⁰
31	8	1.6	.	–	▽✳¹ 17³⁵–18⁰⁵ ▽•⁰ 18³⁵–40
Σ	–	44.6	–	–	UWAGI

Kwiecień – Avril

1	7	1.3	.	–	✳¹⁻⁰ 8¹⁰–11⁴⁰ ✳⁰ 12⁰⁶–28 ▽⁰ 17¹⁹–22
2	8	4.0	.	–	▽• ⁰ 0¹⁹–32 ✳⁰ 23⁴⁵–24
3	7	0.2	1	–	▽•⁰⁻¹ 0⁰⁰ 6⁵⁰ •⁰–7¹⁰ 8¹⁰, ⁰8⁵⁰–9³⁰ ▽⁰ 18⁰⁵–10, = a
4	8	0.6	.	–	▽• ⁰ 4⁰⁵–08
5	6	0.0	.	–	• ⁰ 3⁰⁵–5³⁰ 13⁴⁰, = a–p
6	8	.	.	–	
7	7	5.8	.	–	▽•⁰⁻¹ 14⁴⁰–15¹² •⁰ 20¹⁵–21³⁵, ↘⁰ 14⁵⁰–15²⁵ SW–NE, ∞ a–p = p–24
8	7	3.4	.	–	▽• ⁰ 8⁵⁷–9¹⁵, 9⁴⁰–10⁰⁵ •⁰–13⁰³, = 0⁰⁰–12⁴⁵
9	8	.	.	–	
10	8	.	.	–	
11	8	.	.	–	⌴⁰ 3⁰⁰–6⁰⁰
12	8	.	.	–	⌓⁰ 1⁰⁰–8⁰⁰
13	7	.	.	–	= 4³⁰–9³⁰ ∞–11³⁰
14	7	7.7	.	–	▽• ⁰ 21²¹–23¹⁷, ↘⁰ 20⁴⁵–22³⁰ SW–NW, = na ≡⁰ 4⁴⁵–6⁴⁰ = ∞ –p, ⌓⁰ na–a
15	7	.	.	–	= 0⁴⁰–1¹² ≡⁰⁻¹ 3³⁵ = –6²⁰, np; ⊕ a–p
16	8	.	.	–	= 0⁰⁰–8⁴⁰
17	7	0.4	.	–	• ⁰ 9⁴⁵ 11³⁰–12³⁰ 14⁴⁰, = 15³⁰–24, ⌓⁰ 1⁰⁰–8⁰⁰
18	7	.	.	–	=, ≡⁰⁻¹ 0⁰⁰–12³⁰ ⌓⁰ 21⁰⁰–24
19	8	.	.	–	⌓⁰ 0⁰⁰–9⁰⁰, 21⁰⁰–24
20	8	.	.	–	= 1¹⁰–3²⁰, ⌓⁰ 0⁰⁰–9⁰⁰
21	8	.	.	–	≫ 11³⁰–14³⁰ ⌓⁰ 2⁰⁰–8⁰⁰
22	8	.	.	–	⌓⁰ 2⁰⁰–7⁰⁰
23	8	.	.	–	⌓⁰ 0⁰⁰–7⁰⁰
24	8	.	.	–	⌓⁰ 1⁰⁰–8⁰⁰
25	8	.	.	–	⌓⁰ 3⁰⁰–9⁰⁰
26	8	.	.	–	≫ 12⁴⁵–13³⁰
27	8	.	.	–	= 4¹⁵–5³⁰, ⌓⁰ 1⁰⁰–9⁰⁰ 22⁰⁰–24
28	7	3.3	.	–	• ⁰ 8³⁵ 9¹⁰–12²⁵ 13⁰⁵–15¹² 16⁰⁰, = 3⁵⁰–5³⁰ = –11¹⁰, p–24; ⌓⁰ na–a
29	8	0.0	.	–	= 0⁰⁰–4¹⁵, ⌓⁰ 23⁰⁰–24
30	8	.	.	–	▽• ⁰ 5¹⁵–6⁴⁰, ⌓⁰ 0⁰⁰–5⁰⁰
31					
Σ	–	26.7	–	–	UWAGI

Szczecin - Dąbie φ = 53°24' λ = 14°37' Maj - Mai 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N.w			KIERUNEK I PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	111.2	111.8	113.2	112.1	7.5	16.4	10.3	11.1	17.4	6.9	70	58	70	66	3.1	7.7	3.8	4.9	9	7	10	NE 5	NE 3	NNE 3
2	112.0	110.8	108.6	110.5	6.7	12.9	11.4	10.6	16.4	6.5	94	83	93	90	0.6	2.7	1.0	1.4	10	9	10	NE 1	ESE 3	C 0
3	106.0	107.0	111.0	108.0	12.5	13.9	11.6	12.4	16.3	10.7	88	79	90	86	1.7	3.4	1.3	2.1	8	9	3	SW 1	SW 5	SW 1
4	114.1	114.7	113.8	114.2	9.3	17.9	13.1	13.4	19.4	3.8	97	51	76	75	0.3	10.1	3.6	4.7	1	7	9	WNW 2	C 0	SE 4
5	112.0	109.7	109.2	110.3	12.2	20.3	15.5	15.9	21.5	10.0	86	67	96	83	2.0	7.8	0.8	3.5	10	7	7	E 1	S 7	SW 2
6	110.8	111.7	113.2	111.9	12.8	17.7	13.6	14.4	18.2	12.2	94	64	84	81	0.9	7.2	2.5	3.5	10 •	8	3	SW 2	WSW 6	SW 6
7	111.4	107.9	109.4	109.6	12.7	12.9	9.7	11.2	14.4	9.0	95	95	89	92	1.1	0.7	1.2	1.0	9	10 •	6	WSW 2	SW 5	W 1
8	109.5	108.6	108.0	108.7	7.7	13.3	7.3	8.9	15.1	6.6	97	58	94	83	0.3	6.4	0.6	2.4	10 •	8	8	WSW 4	W 7	SW 5
9	102.3	101.8	105.9	103.3	8.4	10.4	9.3	9.4	12.9	7.2	90	86	89	88	1.0	1.8	1.3	1.4	9	9	9	WSW 6	W 5	NW 3
10	108.7	112.3	115.3	112.1	9.9	10.9	8.3	9.4	11.6	8.1	84	71	86	80	1.9	3.7	1.6	2.4	9	10	9 •	NNW 7	NNW 7	N 3
11	116.3	119.2	122.1	119.2	8.0	9.4	6.5	7.6	10.9	6.4	89	85	91	88	1.2	1.7	0.9	1.3	8 •	9	4	NW 2	N 7	N 1
12	119.1	116.8	116.1	117.3	8.5	12.0	7.5	8.9	13.7	5.3	81	65	79	75	2.1	4.9	2.2	3.1	8	9	1	WNW 1	W 4	C 0
13	111.7	109.8	109.4	110.3	8.1	10.5	10.0	9.6	13.6	4.6	97	87	66	83	0.3	1.6	4.2	2.0	10 •	10	9	SW 4	WNW 4	WNW 5
14	107.5	106.6	109.1	107.7	7.8	12.7	9.1	9.7	13.4	6.4	78	54	84	72	2.4	6.8	1.9	3.7	9	9	6	W 4	W 6	NW 2
15	112.6	114.1	115.8	114.2	8.7	12.9	8.8	9.8	13.3	5.9	89	63	75	76	1.2	5.6	2.9	3.2	9	9	9	N 4	N 6	N 4
16	114.0	113.2	115.4	114.2	8.0	8.9	8.3	8.4	9.6	5.3	96	94	94	95	0.4	0.6	0.7	0.6	10 •	10 •	10	NW 3	NNW 5	NNE 7
17	117.6	118.3	119.9	118.6	8.9	14.5	8.5	10.1	15.0	7.9	85	58	86	76	1.7	7.0	1.5	3.4	9	6	0	NNE 5	N 6	C 0
18	119.0	118.1	116.5	117.8	10.0	17.8	9.8	11.8	19.4	5.2	71	46	81	66	3.6	11.0	2.3	5.6	7	6	2	C 0	NNE 4	C 0
19	114.5	112.5	110.4	112.5	9.2	14.6	11.1	11.5	15.7	7.3	89	53	77	73	1.2	7.8	3.1	4.0	7	9	10	W 2	W 6	WSW 5
20	107.7	107.1	107.4	107.4	9.5	12.8	10.7	10.9	13.5	9.1	92	68	87	82	1.0	4.7	1.7	2.5	10 •	10	8	W 3	WSW 5	C 0
21	109.7	111.0	114.1	111.6	10.5	16.9	10.1	11.9	18.0	9.1	92	65	82	80	1.0	6.6	2.3	3.3	9	4	1	C 0	NE 3	NNE 3
22	115.4	114.4	113.1	114.3	8.7	16.7	11.3	12.0	17.7	6.4	86	45	74	68	1.5	10.4	3.4	5.1	2	7	9	NE 4	NE 2	C 0
23	111.4	112.1	112.7	112.1	11.9	15.7	10.8	12.3	16.2	9.4	77	51	85	71	3.1	8.7	2.0	4.6	3	6	9	SW 3	W 4	W 2
24	113.7	115.1	114.3	114.4	10.7	13.5	10.3	11.2	15.3	10.3	71	59	85	71	3.7	6.3	2.1	4.0	10	9	2	W 4	W 4	C 0
25	114.4	113.6	112.8	113.6	10.1	16.3	11.5	12.4	18.1	6.3	85	56	78	73	2.0	8.1	3.0	4.4	3	9	3	W 3	W 3	C 0
26	111.8	109.3	107.4	109.5	10.9	21.2	14.3	15.2	22.6	9.1	78	42	88	69	2.9	14.6	2.0	6.5	3	0	10	E 4	SE 8	NE 3
27	108.6	111.3	111.7	110.5	9.5	11.7	9.7	10.2	14.4	9.3	92	72	82	82	1.0	3.7	2.2	2.3	10	10	10 •	NW 8	N 7	C 0
28	112.8	113.0	111.5	112.4	7.1	8.1	7.4	7.5	10.0	6.9	94	91	93	93	0.6	0.9	0.8	0.8	10 •	10 •	2	WNW 3	NW 3	C 0
29	108.4	105.1	102.2	105.2	7.7	11.7	10.0	9.8	12.2	1.6	93	78	93	88	0.7	2.9	0.8	1.5	7	10	10	E 1	NE 4	NNE 6
30	98.1	96.4	100.1	98.2	10.8	17.5	10.9	12.5	18.9	9.2	97	85	89	90	0.4	3.4	1.4	1.7	10	9 (K)	10	N 4	WNW 2	S 4
31	102.0	103.1	103.5	102.9	9.9	13.3	10.8	11.2	15.4	8.9	87	68	94	83	1.6	5.0	0.9	2.5	10	9	10	SE 6	S 7	C 0
M	111.1	110.9	111.4	111.1	9.5	14.0	10.2	11.0	15.5	7.3	87	68	85	80	1.5	5.6	1.9	3.0	8.0	8.2	6.7	3.2	4.8	2.3

Czerwiec - Juin

1	102.7	102.7	102.0	102.5	12.1	19.9	17.3	16.6	22.3	10.2	94	57	78	76	0.8	10.0	4.3	5.0	9	1	9	C 0	SSW 1	E 1
2	101.3	102.4	105.4	103.0	16.1	25.5	17.9	19.4	26.1	12.5	80	53	73	69	3.6	15.4	5.6	8.2	6	4	4	C 0	SSE 7	SW 3
3	108.2	108.9	111.0	109.4	16.9	22.5	15.3	17.5	24.7	11.9	69	66	90	75	5.9	9.3	1.7	5.6	2	6	5	W 3	NW 2	NW 2
4	112.2	111.5	113.5	112.4	14.5	24.6	18.3	18.9	25.5	13.4	92	70	91	84	1.3	9.1	1.8	4.1	9	2	9	N 3	N 4	E 4
5	114.3	113.7	114.5	114.2	18.4	26.4	17.9	20.2	27.3	14.5	82	53	87	74	3.9	16.3	2.6	7.6	6	4	3	N 1	C 0	NNE 1
6	114.1	113.2	110.7	112.7	18.4	25.0	18.7	20.2	25.5	14.6	79	42	65	62	4.5	18.3	7.5	10.1	1	2	1	E 2	SE 7	SE 3
7	109.6	107.3	105.7	107.5	17.1	23.6	17.7	19.0	24.8	13.1	82	67	87	79	3.5	9.7	2.6	5.3	2	4	8	E 5	E 4	E 3
8	107.0	109.5	111.1	109.2	17.3	18.9	16.7	17.4	22.0	11.9	86	76	87	83	2.7	5.1	2.5	3.4	9	10	0	SW 3	W 5	C 0
9	110.9	110.9	110.0	110.6	17.1	23.5	16.6	18.4	24.5	11.0	87	55	84	75	2.6	12.9	3.1	6.2	9	4	3	E 1	S 7	ESE 2
10	109.5	109.3	113.5	110.8	17.4	21.9	15.4	17.5	25.3	13.9	87	75	95	85	2.6	6.6	1.1	3.4	7	9 (K)	10	E 1	NW 5	NW 4
11	114.3	113.8	112.7	113.6	15.3	20.1	16.1	16.9	20.5	14.4	88	62	73	74	2.1	9.0	4.9	5.3	9	3	3	NW 4	NNW 5	NNE 2
12	110.2	110.0	108.5	109.6	14.7	14.5	13.9	14.2	18.0	11.0	92	87	85	88	1.3	2.2	2.3	1.9	9	10	0	SSW 4	SW 1	S 2
13	105.9	103.2	100.7	103.3	13.7	18.3	14.7	15.4	19.2	11.4	79	57	94	77	3.4	9.0	0.9	4.4	0	10 •	10 •	SSW 1	S 7	C 0
14	102.3	106.7	111.1	106.7	13.7	15.0	13.9	14.1	17.6	13.5	97	93	79	90	0.6	1.1	3.4	1.7	10 •	9	10	WNW 2	NW 5	W 6
15	112.1	113.7	115.5	113.8	12.3	13.7	13.0	13.0	14.9	11.5	88	80	79	82	1.7	3.2	3.1	2.7	10 •	10	10	WSW 7	W 6	W 5
16	116.1	117.0	117.2	116.8	12.3	15.3	14.7	14.2	20.4	11.3	78	68	76	74	3.2	5.7	4.0	4.3	9	8	2	WSW 4	W 6	SW 2
17	117.7	116.5	115.2	116.5	14.8	21.9	19.1	18.7	22.7	11.7	84	55	69	69	2.7	11.8	6.8	7.1	0	9	10	SW 4	W 5	SW 3
18	112.7	111.8	113.1	112.5	18.6	24.5	16.3	18.9	25.1	16.3	73	53	91	72	5.7	14.4	3.7	7.3	3	4	10 •	SW 7	SW 9	WNW 5
19	117.7	118.8	121.4	119.3	13.7	18.5	14.9	15.5	19.7	11.5	74	48	59	60	4.1	11.1	6.9	7.4	3	8	1	W 4	WNW 6	WNW 4
20	125.8	125.8	123.2	124.9	13.3	18.2	13.1	14.4	20.4	8.6	75	39	74	63	3.8	12.8	4.0	6.9	1	4	3	WNW 6	W 4	WSW 1
21	120.5	121.3	122.8	121.5	15.0	16.2	13.1	14.4	19.1	9.4	61	67	75	68	6.6	6.2	3.8	5.5	9	9	0	SW 4	NNW 4	C 0
22	121.9	118.2	113.6	117.9	15.4	20.9	16.5	17.3	23.4	6.5	64	42	79	62	6.4	14.2	4.1	8.2	1	4	6	SW 6	S 9	C 0
23	115.8	115.7	114.8	115.4	15.3	20.3	18.0	17.9	22.8	12.7	78	51	63	64	3.9	11.7	7.6	7.7	7	9	9	NW 5	W 6	W 4
24	116.7	117.1	115.0	116.3	15.0	21.9	19.3	18.9	24.3	15.3	78	41	70	63	3.6	15.5	6.6	8.6	6	9	4	W 5	W 6	SW 3
25	114.2	112.0	110.0	112.1	18.1	25.3	21.3	21.5	28.1	14.7	76	46	61	61	5.1	17.4	9.7	10.7	0	7	1	SW 4	WNW 7	W 1
26	111.8	110.3	106.1	109.4	17.3	25.7	21.9	21.7	27.7	14.3	77	44	68	63	4.5	18.5	8.3	10.4	1	2	4	WSW 2	WSW 4	SE 5
27	102.7	103.8	107.3	104.6	20.4	22.8	16.9	19.2	24.5	16.9	87	76	85	83	3.2	6.5	2.9	4.2	4	9	9	SW 6	SW 7	WNW 6
28	117.6	121.5	124.5	121.2	13.7	17.6	15.4	15.5	19.1	11.3	72	55	82	69	4.4	9.5	5.2	5.7	4	6	9	W 6	WNW 7	W 5
29	127.7	127.4	125.7	126.9	14.2	20.9	17.7	17.6	23.5	11.6	80	56	75	70	3.2	10.8	4.9	6.3	9	6	0	W 3	NW 5	W 2
30	126.9	126.1	125.0	126.0	17.0	24.5	18.3	19.5	24.8	11.2	82	50	70	67	3.6	15.4	6.4	8.5	0	6	0	WNW 1	W 2	NE 2
31																								
M	113.3	113.3	113.4	113.3	15.6	20.9	16.7	17.5	22.8	12.3	81	59	78	73	3.5	10.6	4.3	6.1	5.2	6.3	5.1	3.5	5.1	2.6

Szczecin – Dąbie $H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 20\,m$ Maj – Mai 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ LODU i	USŁONECZNIENIE	POGODA
1	8	2.1	.	–	⌒ ° 1^{00} – 6^{00}
2	7	3.4	.	–	● $^{0\text{-}1}$ 5^{35} – 8^{20} ▽ $^{0\text{-}1}$ 17^{58} – 18^{55} ● ° 19^{15} – 21^{45} 23^{25}, ↘ ° 17^{50} – 18^{45} SW–NE, = np – np
3	7	8.8	.	–	● ° 0^{10} – 1^{45} ▽ $^{0\text{-}1}$ 11^{48} – 12^{35} ▽ $^{0\text{-}2}$ 13^{55} – 15^{05}, ↘ ° $12^{10\text{-}40}$ SW–NE ↘ ^{1} 13^{45} – 14^{40} W–E, = 0^{00} – 7^{20} = ° np
4	7	.	.	–	= ° 0^{00} – 6^{40} = – 7^{30} ⌒ ° 22^{00} – 24
5	7	18.8	.	–	▽ ^{2} 16^{15-30} ▽ ° 20^{24-30}, ↘ ^{2} 16^{20-30} SW–NE (↘) – 16^{40} 19^{40} 20^{14} ↘ ° 20^{35-50} W–NE, ⌒ ° 0^{00} – 9^{00}
6	8	7.8	.	–	● ° 1^{40} 2^{50} – 8^{20} 9^{40} ▽ $^{0\text{-}1}$ 13^{38} 14^{07} ▽ ° 15^{14-17}, ↘ ° 13^{50} 14^{12} W–SE, 15^{14-20} NW–NE, = np
7	6	12.7	.	–	● ° 3^{20} 10^{00} ● $^{0\text{-}1}$ – 14^{40} 15^{30} ▽ 16^{48} – 17^{43}, 20^{05-10}, ↘ ° 17^{05-35} W–S, = na
8	8	10.1	.	–	● ° 6^{21} – 7^{30} 8^{10} ▽ ^{1} 11^{01-14} ▽ $^{0\text{-}1}$ 16^{45} 18^{45} ▲ ° 17^{33-37}, 18^{20-22}, ⌒ 17^{08-15}
9	7	8.8	.	–	▽ ° 0^{50} – 1^{10} ▽ $^{0\text{-}2}$ 6^{20} 23^{50}
10	8	3.0	.	–	● ° 0^{01} – 2^{20} ▽ ° 9^{03-12} ● ° ▽ ° 11^{10} 23^{20}
11	8	1.2	.	–	● ° 2^{45} – 8^{00} ▽ $^{0\text{-}1}$ 8^{12} – 13^{07}
12	8	0.1	.	–	▽ ° 10^{55} – 11^{10}, ⌒ ° 0^{00} – 7^{00} ⌒ ^{1} 21^{00} – 24
13	7	2.1	.	–	● ° 5^{45} 6^{30} – 9^{20} ▽ ° 12^{07-28} – 13^{02-07}, = ° na = – 9^{15} np, ⌒ ^{1} na
14	8	2.7	.	–	▽ ° 4^{35} – 5^{00} ▽ $^{1\text{-}0}$ 13^{10} 16^{07}, ↘ ° 15^{52} – 16^{20} N–E, = na
15	8	0.5	.	–	⌒ ° np
16	7	4.4	.	–	▽ $^{1\text{-}0}$ 4^{12} 5^{57} ● $^{0\text{-}1}$ 6^{30} 7^{05} 12^{30} 14^{15}, ⌒ ° 0^{00} – 4^{00}
17	8	.	.	–	⌒ ° 21^{00} – 24
18	8	.	.	–	⌒ ° 0^{00} – 9^{00}, 21^{00} – 24
19	8	0.0	.	–	⌒ ° 0^{00} – 8^{00}
20	8	0.2	.	–	● ● ° 4^{05} 5^{10} ● ° 7^{20} ● ° 12^{05} 16^{40}, 22^{10} 23^{45}, = 1^{20} – 3^{10}
21	7	.	.	–	● ° 6^{20} 50, ⌒ ° 20^{00} – 24
22	8	.	.	–	= 3^{35} – 4^{20}, ⌒ ° 0^{00} – 9^{00}, np
23	8	.	.	–	⌒ ° 0^{00} – 9^{00}
24	8	.	.	–	= 20^{30} – 24, ⌒ ° 20^{00} – 24
25	7	.	.	–	= 0^{00} – 3^{20} ∞ 8^{10} – 11^{30}, ⌒ ° 0^{00} – 8^{00}, 21^{00} – 24
26	7	5.3	.	–	● ° 19^{10} – 20^{15}, 21^{20} – 24, = 1^{30} – 3^{30} ∞ 9^{30} – 10^{30}, ⌒ ° 0^{00} – 8^{00}
27	8	2.8	.	–	● ° 0^{00} – 3^{40}, 20^{35} – 22^{20} 23^{20} 24
28	7	11.7	.	–	● ° 0^{00-15}, 5^{15} – 7^{00} – 13^{10}, 14^{15}, = 22^{30} – 24
29	7	20.8	.	–	● $^{0\text{-}1}$ 18^{15} – 21^{25} ▽ $^{0\text{-}2}$ 23^{17} – 24; ↘ ° 23^{17} – 24, = 0^{00} – 3^{50} = ° – 7^{25} = np
30	6	0.0	.	–	▽ ^{1} 0^{00-12} ● ° 22^{45} – 23^{40}, ↘ ° 0^{00-15} SE–SSW (↘) 13^{17} – 14^{20} NE–NW; = 0^{00} – 14^{15}
31	7	2.2	.	–	▽ ° 18^{50} – 20^{40}, = 20^{40} – 24
Σ	–	127.5	–	–	UWAGI.

Czerwiec – Juin

1	8	.	.	–	= 0^{00} – 9^{15}, ⌒ ° 21^{00} – 24
2	8	.	.	–	= 1^{20} – 5^{40} ⌒ ° 0^{00} – 10^{00}, 22^{00} – 24
3	7	0.0	.	–	▽ ° 18^{42-46}, (↘) 16^{28} – 17^{45} E–SE, = 2^{00} – 5^{20}, ⌒ ° 0^{00} – 9^{00}, np
4	7	4.4	.	–	▽ ^{1} 17^{12-35} ▽ ° 19^{05-20} ↘ ° 17^{05-45} NE–SW, 18^{40} – 19^{40} NE–SSW, = 2^{00} – 7^{45}, ⌒ ° 0^{00} – 8^{00}
5	8	0.0	.	–	▽ ° 14^{50} 16^{01}, ↘ ° 14^{17} – 17^{10} E–SSW–NE; = na, np, ⌒ ° np
6	8	.	.	–	= 0^{00} – 6^{20}, ⌒ ° 0^{00} – 10^{00}, 22^{00} – 24
7	8	.	.	–	⌒ ° 0^{00} – 9^{00}, 21^{00} – 24
8	7	.	.	–	= 0^{20} – 1^{30} = 3^{35} – 5^{15}, ⌒ $^{0\text{-}1}$ na – a ⌒ ° np
9	7	.	.	–	∞ 10^{15} – 15^{20} = 23^{15} – 24, ⌒ ° 0^{00} – 9^{00}, np
10	7	9.4	.	–	▽ ^{2} 14^{17} – 16^{40} ▽ ° 17^{14} – 18^{33}, (↘) 13^{25-45} ↘ ^{2} 16^{40} (↘) 16^{50} NW–SE; = 0^{00} – 7^{30}, ∞ 10^{00} – 13^{45} = np; ⌒ na, a
11	8	.	.	–	= 0^{00} – 8^{20} ⌒ ° np
12	7	0.7	.	–	● ° 9^{40} ▽ ° 16^{10-25}, ⌒ $^{0\text{-}1}$ 0^{00} – 9^{00}, ⌒ ° np
13	8	26.3	.	–	● ° 13^{49} 19^{07} 21^{47} – 24; = 20^{15} – 22^{10}, ⌒ ° 0^{00} – 10^{00}
14	7	15.6	.	–	● $^{0\text{-}1}$ 0^{00} – 12^{15} ▽ ° 13^{10-30} ▽ $^{0\text{-}1}$ 17^{01} – 18^{45}, = 4^{10} – 12^{15}
15	8	0.8	.	–	● ° 7^{50} 10^{15}, ▽ ° 15^{17-36}
16	8	.	.	–	⌒ ° 22^{00} – 24
17	7	.	.	–	= 5^{30} – 10^{15} ∞ – 13^{30} = 22^{40} – 24, ⌒ ° 0^{00} – 10^{00}
18	8	1.2	.	–	● ° 19^{05} – 20^{15}, 21^{20} 22^{10}, = 0^{00} – 8^{10} ∞ – 10^{30}
19	8	0.0	.	–	▽ ° 18^{09-12}
20	8	.	.	–	⌒ ° 2^{00} – 10^{00} 21^{00} – 24
21	8	.	.	–	= 22^{20} – 24, ⌒ ° 0^{00} – 10^{00}, 22^{00} – 24
22	8	.	.	–	= 0^{00} – 4^{40} ⌒ ° 0^{00} – 10^{00}, 22^{00} – 24
23	8	.	.	–	⌒ ° 0^{00} – 9^{00}
24	8	.	.	–	
25	8	.	.	–	= np, ⌒ ° 4^{00} – 9^{00}, np
26	8	1.9	.	–	= 0^{00} – 3^{35} ⌒ ° 0^{00} – 8^{00}
27	7	1.8	.	–	▽ ^{1} 4^{43} – 5^{05} ● ° 11^{46} – 13^{08} ▽ ° 14^{53-56}, 16^{40-42}, (↘) 4^{35} ↘ – 4^{40} – (↘) 5^{15} SW–NE
28	8	0.1	.	–	▽ ° 21^{12-23}, 21^{30-37}, ⌒ 21^{25-28}
29	8	.	.	–	⌒ ° 22^{00} – 24
30	7	.	.	–	= 0^{10} – 2^{00} = ° – 5^{40}, ⌒ ° 0^{00} – 9^{00}, 23^{00} – 24
31					
Σ	–	62.2	–	–	UWAGI.

Szczecin – Dąbie — φ = 53°24' — λ = 14°37' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	125.1	124.1	122.4	123.9	17.0	25.7	21.0	21.2	27.5	8.5	79	48	62	63	4.1	17.2	9.5	10.3	0	1	0	C 0	E 1	C 0
2	121.5	120.5	117.8	119.9	19.5	29.6	25.5	24.0	30.8	11.8	82	33	65	60	4.0	27.9	10.1	14.0	0	1	0	C 0	W 1	E 2
3	115.2	112.8	115.0	114.3	21.1	31.4	17.7	22.0	32.0	16.5	75	38	74	62	6.2	28.4	5.5	13.3	0	5	3	C 0	WSW 6	WNW 4
4	110.5	106.7	103.4	106.9	14.7	17.2	15.2	15.6	19.0	13.9	77	72	72	74	3.8	5.4	4.8	4.7	8	10	6	SW 4	SW 7	WSW 6
5	108.0	108.7	109.4	108.7	12.3	16.4	11.6	13.0	17.1	11.3	72	59	79	70	4.0	7.6	2.8	4.8	9	9	5	W 7	WSW 8	WSW 7
6	108.5	114.5	117.7	113.5	10.9	16.3	12.4	13.0	17.9	9.6	96	69	81	82	0.5	5.8	2.7	3.0	10	7	9	WSW 5	WNW 8	WNW 3
7	118.8	119.1	118.3	118.7	12.1	17.1	14.7	14.6	18.1	10.0	80	50	73	68	2.8	9.7	4.5	5.7	10	6	6	WSW 5	W 4	WSW 1
8	116.1	114.9	110.6	113.9	14.3	20.3	16.9	17.1	21.2	14.2	79	57	77	71	3.4	10.2	4.4	6.0	10 •	9	9	SW 6	SW 5	SW 4
9	105.9	107.5	109.5	107.6	14.4	16.7	13.5	14.5	18.6	13.5	95	82	92	90	0.7	3.5	1.3	1.8	10 •	10	9	WNW 2	WNW 6	WSW 4
10	109.1	109.9	111.2	110.1	12.5	16.3	12.7	13.6	17.1	10.9	88	65	89	81	1.7	6.5	1.6	3.3	9	8	9	WSW 4	W 7	W 1
11	111.5	111.3	108.9	110.6	13.3	18.5	16.5	16.2	19.4	10.7	84	62	94	80	2.5	8.2	1.2	4.0	8	7	10	W 4	WSW 6	SE 2
12	108.4	107.7	103.4	106.5	16.1	22.7	19.7	19.6	24.7	13.5	96	59	76	77	0.8	11.3	5.5	5.9	7	5	6	WSW 1	C 0	E 3
13	96.9	95.0	95.2	95.7	19.2	25.9	16.9	19.2	24.7	16.3	81	69	93	81	4.2	9.1	1.4	4.9	8	9	10	SE 7	S 7	SW 4
14	97.1	101.3	103.2	100.5	12.4	13.5	16.3	14.6	20.0	12.3	96	90	71	86	0.5	1.6	6.4	2.8	10 ••	10 •	9 •	SW 8	SW 7	SSW 5
15	106.1	108.2	108.2	107.5	15.0	21.5	18.2	18.2	22.8	13.9	89	45	62	65	1.8	14.1	7.9	7.9	3	6	7	WSW 4	WSW 2	ESE 8
16	107.6	106.8	106.9	107.1	14.5	22.0	13.4	15.8	22.5	12.9	94	42	92	76	0.9	15.3	1.3	5.8	6	5	10	W 1	WSW 2	WSW 1
17	105.5	106.2	105.9	105.9	13.8	15.7	15.1	14.9	18.0	11.3	91	80	81	84	1.5	3.5	3.4	2.8	6	9	6	SW 1	SW 5	W 4
18	105.3	105.3	105.3	105.3	14.5	17.2	14.7	15.3	19.0	11.8	89	76	85	85	1.8	4.7	2.9	3.1	9	9	6	WSW 4	WNW 6	W 3
19	105.7	105.4	105.5	105.5	13.3	19.5	15.3	15.8	20.8	11.9	94	54	78	75	0.9	10.5	3.9	5.1	6	4	4	SW 5	WSW 7	SW 2
20	107.2	107.6	107.3	107.4	14.7	17.1	14.7	15.3	18.4	13.7	89	64	94	82	1.8	7.1	0.9	3.3	9	9	10	WSW 5	SW 5	SSW 5
21	108.2	108.8	110.1	109.0	14.3	15.9	14.5	14.8	18.1	14.0	94	88	94	92	0.9	2.1	0.9	1.3	10 •	9	6	WSW 3	WSW 4	WNW 2
22	110.2	110.6	110.8	110.5	14.3	16.7	14.1	14.8	17.5	13.6	92	66	84	81	1.3	6.4	2.5	3.4	10	9	10	W 4	W 6	W 5
23	111.5	113.5	115.4	113.5	13.9	16.3	14.1	14.6	17.6	13.3	92	71	80	81	1.3	6.4	3.2	3.6	10	9	8	WSW 5	WSW 5	WSW 3
24	118.2	120.4	122.2	120.3	13.3	16.3	13.3	14.0	16.7	12.7	82	64	83	76	2.8	6.7	2.7	4.1	10	10	7	W 4	W 6	W 3
25	123.5	123.2	119.7	122.1	13.9	17.2	15.0	15.3	19.3	13.0	88	66	89	81	2.0	6.7	1.8	3.5	10	9	10	W 2	WSW 4	SW 3
26	115.4	111.2	108.5	111.7	15.5	21.1	17.0	17.6	23.5	14.8	86	60	92	79	2.4	10.1	1.6	4.7	9	10	10	SW 7	SW 8	W 2
27	104.9	103.7	104.6	104.4	16.7	18.7	16.1	16.9	19.8	15.4	93	73	77	81	1.4	6.0	4.2	3.9	9	10	10	SW 4	WSW 8	WSW 5
28	101.6	101.2	103.1	102.0	12.4	12.9	13.7	13.2	16.3	12.4	93	94	85	91	1.0	0.9	2.3	1.4	10 •	10 •	9	C 0	W 2	SW 4
29	107.9	111.3	113.9	111.0	13.1	16.1	12.9	13.8	18.2	11.4	85	65	87	79	2.3	6.5	1.9	3.6	7	9	2	WSW 5	WSW 4	W 2
30	116.9	117.7	118.2	117.6	12.2	16.5	16.1	15.2	18.0	10.0	93	74	74	80	1.0	5.0	4.7	3.6	9	9	6	SW 2	NW 6	NNW 4
31	116.9	116.0	113.1	115.3	14.0	16.1	13.8	14.4	17.0	13.2	90	84	80	85	1.6	2.9	3.2	2.6	9 •	10	10 •	NNW 4	N 6	WNW 8
M	110.5	110.7	110.5	110.6	14.5	18.8	15.5	16.1	20.4	12.7	88	65	81	78	2.1	8.6	3.6	4.8	7.8	7.8	7.2	3.5	5.1	3.5

Sierpień – Août

1	112.4	113.6	113.2	113.1	15.7	17.4	15.2	15.4	19.8	12.6	94	65	82	80	0.9	7.0	3.2	3.7	10 •	9	1	WNW 6	NW 6	W 1
2	112.3	112.0	111.9	112.1	15.9	18.9	14.2	15.3	19.5	12.4	87	74	97	86	2.2	5.7	0.6	2.8	9	10	10	SW 5	SW 1	C 0
3	113.3	116.4	118.4	116.0	15.6	16.5	12.4	13.7	18.9	11.9	98	77	90	88	0.4	4.4	1.4	2.1	10 •	7	2	WSW 2	WNW 2	SW 2
4	115.1	112.0	112.0	113.0	13.1	14.2	15.8	14.7	16.0	10.7	78	86	91	85	3.3	2.4	1.5	2.4	10	10	9	SW 5	SW 8	SW 5
5	113.0	112.8	109.5	111.8	15.7	21.2	20.1	19.3	22.8	14.0	94	72	78	81	1.1	7.1	5.2	4.5	8	9	9	WSW 3	W 5	SW 2
6	107.6	109.0	110.5	109.0	19.3	24.2	17.1	19.4	24.9	16.7	82	61	77	73	4.0	11.7	4.5	6.7	4	5	10	SW 4	W 4	NNE 2
7	110.1	110.8	114.8	111.9	15.6	15.7	13.2	14.4	20.8	13.1	94	97	91	94	1.1	0.6	1.4	1.0	10	10 •	0	WSW 1	W 5	W 3
8	117.1	114.3	111.4	114.3	13.0	18.5	18.8	17.3	19.6	8.5	94	62	74	77	0.9	8.2	5.7	4.9	2	10	4	C 0	SE 6	S 1
9	117.1	118.1	118.7	118.0	16.2	22.6	16.9	18.2	23.9	14.1	85	46	84	72	2.7	14.7	3.1	6.8	2	9	9	W 1	W 6	C 0
10	118.0	116.4	115.0	116.5	15.7	22.0	16.7	17.8	22.8	12.6	87	72	95	85	2.2	7.5	1.0	3.6	6	10	10 •	C 0	SE 3	NNE 2
11	113.7	114.7	114.4	114.3	16.1	18.7	16.3	16.8	19.0	15.2	96	84	95	92	0.8	3.6	1.0	1.8	10 •	10	10	C 0	C 0	N 1
12	113.6	114.9	116.7	115.1	14.5	19.0	14.9	15.8	20.2	14.3	96	67	86	83	0.7	7.4	2.4	3.5	9	8	6	SW 4	WSW 5	C 0
13	118.8	119.6	119.8	119.4	12.2	17.1	14.1	14.4	19.4	9.5	87	60	81	76	1.9	7.8	3.1	4.3	3	9	7	W 6	NW 6	C 0
14	118.1	116.1	111.8	115.3	13.4	16.3	15.3	15.1	18.9	12.2	82	69	77	76	2.8	9.8	4.1	4.2	10	10	6	SW 4	SSE 3	SSW 3
15	108.7	107.1	105.4	107.1	13.2	14.4	12.1	13.0	16.1	11.6	95	87	89	90	0.7	2.2	1.5	1.5	10 •	10	6	SW 5	SW 7	SSW 4
16	103.8	103.2	104.5	103.8	10.9	15.8	12.7	13.0	16.7	10.6	95	78	92	88	0.6	5.9	1.2	1.9	10 •	7	8	SW 7	SW 6	SW 4
17	104.3	104.8	107.4	105.5	11.0	17.0	12.5	13.2	17.7	10.3	89	55	94	79	1.5	8.7	0.9	3.7	8	8	0	SW 4	W 5	SW 2
18	109.1	109.1	107.5	108.6	13.3	18.5	13.5	14.7	19.7	10.9	94	60	88	81	0.9	8.5	1.8	3.7	9	9	9	WNW 5	NW 6	SW 2
19	101.1	100.9	101.4	101.1	14.3	16.7	14.1	14.8	17.4	13.0	94	72	90	85	0.9	5.4	1.6	2.6	10	9	10	SW 6	W 7	SW 5
20	104.1	106.4	108.7	106.4	13.9	18.5	15.8	16.0	20.0	13.0	92	60	73	75	1.3	8.5	4.8	4.9	9	6	10 •	W 5	WNW 7	SW 5
21	108.4	108.2	106.3	107.6	13.8	17.1	16.9	16.2	18.4	13.8	89	78	78	82	1.8	4.3	4.2	3.4	10	10 •	10	WSW 5	SW 7	SSW 5
22	102.1	100.9	102.7	101.9	15.1	15.2	13.9	14.5	18.2	13.2	89	90	90	90	1.9	1.7	1.6	1.7	10	10	7	SSW 6	SW 6	SW 6
23	105.8	109.7	112.7	109.4	15.7	15.3	12.3	13.4	17.4	12.3	90	72	73	78	1.6	5.0	3.9	3.5	9	9	2	W 5	WNW 6	W 2
24	114.7	114.9	113.6	114.4	10.9	15.9	14.5	14.0	18.9	9.3	96	81	86	88	0.5	3.5	2.4	2.1	9	9	4	SW 4	W 5	SW 2
25	114.2	115.8	116.4	115.5	13.6	17.1	10.9	13.1	18.7	10.7	89	55	89	78	1.8	9.9	1.4	4.4	8	5	6	NW 2	WNW 5	C 0
26	116.7	117.9	118.3	117.6	14.5	20.5	17.1	17.3	21.5	9.3	94	76	93	88	0.9	5.7	1.4	2.7	10	10	9	SSW 5	SW 2	SW 1
27	118.3	119.7	121.9	120.0	17.1	23.9	16.7	18.6	24.9	16.0	85	61	91	79	3.0	11.5	1.8	5.4	9	6	4	SW 4	W 5	C 0
28	124.7	125.8	125.3	125.3	12.7	21.5	16.7	16.9	22.6	11.4	89	60	86	78	1.6	10.2	2.7	4.8	6	1	1	SW 3	W 6	SW 2
29	125.2	124.6	125.7	124.5	13.3	21.1	14.6	15.9	21.7	12.7	95	69	93	86	0.7	7.7	1.1	3.2	3	1	0	WSW 1	NE 4	N 1
30	124.0	124.1	124.5	124.2	11.5	22.9	13.5	16.3	24.4	8.9	99	69	90	86	0.2	8.6	1.7	3.5	10 =	1	0	C 0	E 1	C 0
31	126.2	126.7	126.7	126.5	12.7	25.7	17.6	18.4	26.4	8.9	96	52	81	76	0.5	15.9	3.8	6.7	0	2	0	C 0	NE 4	SE 1
M	113.5	113.6	113.7	113.5	13.9	18.7	15.1	15.7	20.2	12.1	91	70	86	82	1.5	6.9	2.5	3.6	7.8	7.7	5.8	3.5	4.7	2.1

Szczecin - Dąbie — $H_s = 1\,m$ — $H_k = 6{,}9\,m$ — $h_w = 20\,m$ — Lipiec - Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚCIENIE GU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌓ ° 0⁰⁰ – 9⁰⁰ ⌓ ° np
2	8	.	.	–	= 1²⁰ – 8⁴⁰ ⌓ ° 0⁰⁰ – 9⁰⁰
3	7	.	.	–	= 7¹⁵ – 8³⁵ ∞ 10¹⁰ – 17⁰⁵ ⌓ ° na – a
4	6	0.0	.	–	• ° 9⁰⁵ 12¹⁵ ▽ ° 13⁰²⁻⁰⁵ • ° 14¹⁰ 15¹⁵ ▽ ° 17¹⁶·⁴² ; ∞ 13⁰⁵ – 15¹⁵ ; ⌓ ° na – a
5	8	3.1	.	–	▽ ⁰⁻¹ 12¹⁸ 16³⁵
6	8	8.7	.	–	• ° 5⁰⁵ – 6³⁰ ; 7¹⁰ ▽ ⁰⁻¹ 7¹⁵ 12⁵³ ▽ ° 21⁴⁶⁻⁵⁷
7	8	0.0	.	–	
8	8	9.3	.	–	• ° 7⁴⁵ 8¹² ▽ ⁰⁻¹ 14²⁰ 18¹⁷ • ° 23⁴⁰ 24 ; ☇ 16⁴⁵ ; ∞ 9³⁰ – 11³⁰
9	7	6.4	.	–	• ° 0⁰⁰ ³⁰ • ⁰⁻¹ – 11³⁰ 12³⁵ ▽ ° 14³⁸⁻⁴⁰ 16⁰¹⁻⁰⁹ 18⁵⁰⁻⁵²
10	8	1.7	.	–	▽ ¹⁻⁰ 1⁰⁵ – 1⁵⁰ ; 2⁰²⁻¹⁵ ▽ ° 12¹⁰ 20⁰⁶
11	8	6.8	.	–	• ° 15⁴⁷·⁵⁶ 19⁴⁹ 20⁰³ – 20⁵⁰ ; ☇ 23⁰⁵⁻⁵⁰ S ; = 20⁴⁵ 24
12	7	.	.	–	▽ ⁰⁻² 0¹⁵ 1⁰⁴ ; (☇) 0²⁰⁻⁴² NW ☇ ¹⁻ 0⁴⁸ (☇) – 1¹² NE ; = 0⁰⁰ – 4⁴⁰ = ⁺⁰ 5²⁰ = – 11³⁰
13	7	3.0	.	–	▽ ° 15²⁰ – 16⁰⁵ • ° 16¹² – 17³⁰ 18²⁰ 23²⁰ 24
14	7	0.2	.	–	• ° 0⁰⁰ ¹³⁰ • • ° 7³⁰ – 8³⁰ • ° 14³⁵ ▽ ° 21⁵² – 22⁰⁷
15	8	.	.	–	▽ ° 0⁰⁷⁻¹⁰
16	8	4.3	.	–	▽ ⁰⁻¹ 17⁵⁰ – 18³⁵ 19⁴³ 20¹⁷ ; ☇ ° 18¹⁰⁻³⁵ E ; = 2¹⁰ – 6³⁰ ; ⌓ ° 0⁰⁰ – 9⁰⁰
17	8	0.1	.	–	▽ ° 12³⁶ – ⁴¹ 13⁰⁴⁻²⁸ ; ⌓ ° 2⁰⁰ – 11⁰⁰
18	7	6.4	.	–	• ° 9³⁵⁻³⁸ ▽ ¹⁰¹⁷⁻³⁰ ▽ 22⁵⁴ (☇) 18³⁵⁻²⁵ ☇ – 18³⁵ (☇) – 18⁴⁵ W-E ; = na ; ⌓ ° na – a
19	8	.	.	–	
20	8	4.9	.	–	• ° 15²⁰ – 16¹⁵ ▽ ° 17²⁵⁻³⁰ • ⁰⁻¹ 18⁴⁵ – 20³⁰ 21²⁰ ; = 21²⁰ 24
21	8	14.3	.	–	• ° 0⁰⁵ 3³⁰ 4⁴⁰ 7¹⁰ 9¹⁰ – 10⁰⁵ ▽ ⁰⁻¹ 10³³ 20²² ; ☇ ° 13³²⁻⁴³ NW–SE ; 14¹⁵⁻³⁰ NW–SE ; = na
22	8	0.0	.	–	• ° 9⁴⁵ 10¹⁰ ▽ ° 10⁴⁰⁻⁴³ 17³⁰⁻³⁵
23	8	0.0	.	–	• ° 5¹⁰ 6⁴⁰ • ° 9³⁵ 10¹⁰
24	8	.	.	–	
25	8	0.1	.	–	▽ ° 20²³⁻⁴⁰ • ° 22⁴⁰ – 21²⁰ ; = 20⁴⁵ – 22³⁰
26	6	1.4	.	–	• ° 7⁰²⁻⁴⁰ 9⁴⁵ – 12¹⁰ ; 20⁵⁰ – 21¹⁰ ; 22³⁰ – 24 ; = 1¹⁵ – 12¹⁰ ∞ – 16³⁰ = np
27	7	3.4	.	–	• ° 0⁰⁰ 2⁴⁰ ; = 0⁰⁰ – 9²⁰
28	6	2.4	.	–	• ° 2³⁵ – 14³⁰ 15²⁰
29	8	.	.	–	⌓ ° 21⁰⁰ – 24
30	8	0.0	.	–	⌓ ⁰⁻¹ 0⁰⁰ – 10⁰⁰
31	7	12.3	.	–	• ° 6⁴⁵ 8¹⁰ ▽ ° 10¹⁷ ; 16¹⁵ • ° 20¹² 21³⁵ • ⁰⁻¹ 24 ; ⌒ 20⁴⁰ – 21⁰³
Σ	–	88.8	–	–	UWAGI

Sierpień - Août

1	7	0.0	.	–	• ° 0⁰⁰ 4⁴⁰ 7²⁵ – 8¹⁰ 9¹⁵ ⌓ ° 22⁰⁰ – 24
2	7	7.2	.	–	• ⁰⁻¹ 14¹⁵ – 15¹⁵ 15⁴⁵ • ° 18¹⁰ 19⁰⁰ = 5³⁰ – 8³⁰ ; 14¹⁰ – 22³⁰ ≡ ⁰⁻¹ 24 ; ⌓ ° 0⁰⁰ – 9⁰⁰
3	8	17.6	.	–	• ° 7⁴⁰ 8¹⁰ • ⁰⁻¹ – 11⁰⁵ ▽ ° 15²⁷⁻³⁰ 18¹⁵⁻²⁰ 19¹⁵⁻²⁷ ; ≡ ⁰⁻¹ 0⁰⁰ – 4⁴⁰ = – 11⁰⁵ ⌒ 18²⁵⁻³⁰
4	7	1.4	.	–	• ⁰⁻¹ 9²³ – 13²⁵ • ° 15⁰¹ 18²⁵ •• ° – 19⁰⁰ • ° 19²⁰ ; = 11¹⁵ – 13⁴⁰ ; 15²⁰ 24
5	7	5.4	.	–	= 0⁰⁰ – 9³⁰ ; ⌓ ° 21⁰⁰ – 24
6	8	1.4	.	–	▽ ° 0⁰⁵⁻¹⁰ ▽ ⁻² – 0⁴⁰ • ° 22⁴⁰ 24
7	7	8.7	.	–	• ° 0⁰⁰ 7¹⁵ • ⁰⁻¹ 9⁰⁵ 13³⁵ 14⁴⁰ ▽ ⁻¹ 18¹⁵⁻²⁵
8	8	0.7	.	–	• ° 14⁰³ – 16²⁰ ; 18⁰⁴ 19 ; = 4³⁰ – 7⁴⁰
9	8	.	.	–	▽ ° 13³³ – ⁴² ⌓ ° 21⁰⁰ – 24
10	8	6.9	.	–	• ° 14¹⁰ 16⁰⁰ – 22³⁰ ; ⌓ ° 0⁰⁰ – 9⁰⁰
11	7	0.6	.	–	• ° 7¹⁵ 10⁴⁰ ; = 0³⁰ – 8³⁰ ; 20³⁰ 24
12	8	.	.	–	▽ ° 1⁴⁰ – 2³⁵ (☇) ° 1⁴⁰ ☇ ° 2³⁵ (☇) ° 2⁴⁵ SW-NE ; = 0⁰⁰ – 8³⁰ ⌓ ° np
13	8	.	.	–	⌓ ° 0⁰⁰ – 9⁰⁰ ; 22⁰⁰ – 24
14	7	1.2	.	–	• ° 9¹⁰ 12²⁰ ▽ ° 22⁵⁵ – 23⁰⁰ 23⁴⁰⁻⁵⁰ ⌓ ° 0⁰⁰ – 9⁰⁰
15	7	5.4	.	–	• ° 0⁴⁰ 3⁴⁰ ; 6¹⁵ 9¹⁰ ▽ ° 13⁴⁰⁻⁴² 16²⁰⁻⁴⁵ ; (☇) ° 16³⁰ ☇ 16³⁵ (☇) 16⁵⁰ SW-NE
16	8	5.7	.	–	• ° 5³⁵ 6³⁰ – 8¹⁵ ▽ ° 12⁴³ – 13⁰³ ▽ ⁻² – 13⁰⁶ ▽ ° 17³⁸
17	8	6.0	.	–	▽ ⁰⁻¹ 16⁰²·⁴⁰ ▽ ° 19⁰³⁻¹² ⌒ 19³⁶⁻⁴⁵
18	8	4.7	.	–	= 4¹⁵ – 6³⁰ ; ⌓ ° 22⁰⁰ – 24
19	8	3.7	.	–	• ° 0¹⁰ – 3²⁰ ▽ ° 17⁰¹ – 18⁰⁵ • ° 22⁰⁵ – 24 = 4¹⁵ – 9³⁰
20	8	0.1	.	–	• ° 0⁰⁰ – 2⁴⁰ ▽ ° 11¹¹⁻¹⁸ • ° 21⁴⁰ 22⁰⁵ – 23³⁵ 24 ; = 2⁴⁰ 8²⁰
21	7	0.4	.	–	• ° 0⁰⁰ 2⁴⁵ 7⁰³ ³⁷ 13⁰⁴ 15²⁰ 16⁴⁵ 17²⁵ ; = 3³⁰ – 6²⁰
22	7	6.8	.	–	• ° 1³⁵ 2⁴⁵ 4²⁵ 5⁰⁰ – 6²⁵ 9³⁵ – 10¹⁵ ▽ ⁰⁻¹ 13³¹·⁵³ ; 18⁰⁵ 19²⁰
23	8	1.6	.	–	▽ ° 3⁵⁰ – 5⁰⁰ • ° – 6¹⁵ ▽ ° 10⁴² 12⁴⁰
24	7	1.3	.	–	• ° 8⁴⁵ 10¹⁰ ; 12³⁵ – 13¹⁵ ⌓ ° 3⁰⁰ – 8⁰⁰
25	8	0.2	.	–	▽ ° 1³³ – ⁴⁸ • ° 3¹⁰ – 4²⁵ = 2¹⁵ – 6²³ ; ⌓ ° 22⁰⁰ – 24
26	7	.	.	–	• ° 5⁴⁰ 7¹⁰ = 6¹⁵ – 13³⁰ 20³⁰ 24 ⌓ ° na np
27	6	.	.	–	= 0⁰⁰ – ³⁰ = 21³⁰ – 24 ; ⌓ ° 0⁰⁰ – 9⁰⁰ ; 20⁰⁰ – 24
28	8	.	.	–	= na np ; ⌓ ° 0⁰⁰ – 10⁰⁰ 21⁰⁰ – 24
29	8	.	.	–	= 0⁰⁰ – 10²⁰ = np ; ⌓ ° 0⁰⁰ – 12⁰⁰ ; 21⁰⁰ – 24
30	8	.	.	–	= 0⁰⁰ – 3¹⁵ = ≡ ⁰⁻¹ 3¹⁵ – 10³⁰ = np ; ⌓ ⁰⁻¹ 0⁰⁰ – 10⁰⁰ ⌓ ¹ 20⁰⁰ – 24
31	8	.	.	–	= 0⁰⁰ – 1⁴⁵ ≡ ° – 3⁵⁰ = – 4⁵⁰ ≡ ° – 7⁴⁵ = – 8³⁰ ; ⌓ ¹ 0⁰⁰ – 10⁰⁰ ; 21⁰⁰ – 24
Σ	–	87.0	–	–	UWAGI

Szczecin – Dąbie φ = 53°24' λ = 14°37' Wrzesień – Septembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	125.9	124.5	121.2	123.8	15.4	26.8	17.5	19.2	28.1	12.2	93	49	94	79	1.1	17.7	1.2	6.7	0	0	0	C 0	S 4	C 0
2	119.4	117.7	114.4	117.2	12.9	27.0	18.5	19.1	28.5	11.7	96	56	97	83	0.6	15.5	0.6	5.6	0	0	0 =	C 0	C 0	C 0
3	111.0	109.9	109.4	110.1	14.9	25.6	17.3	18.8	27.6	14.6	100	66	79	82	0.0	11.1	4.1	5.1	0 =	0	0	C 0	C 0	C 0
4	111.6	112.7	112.9	112.4	13.5	22.5	16.1	17.0	23.0	12.0	94	68	90	84	0.9	8.7	1.7	3.8	2	4	0	SW 1	NNE 1	C 0
5	110.7	107.9	105.1	107.9	14.2	24.1	17.9	18.5	25.1	11.9	98	72	93	88	0.4	8.3	1.4	3.4	1	8	2	W 1	SE 5	S 5
6	105.0	104.9	102.6	104.2	16.3	19.9	16.9	17.5	20.7	15.4	93	71	77	80	1.3	6.7	4.4	4.1	4	7	0	SW 2	SW 5	S 5
7	101.9	100.4	101.3	101.2	12.3	15.5	11.5	12.7	17.9	11.2	92	71	90	84	1.2	5.1	1.4	2.6	9	9	10 •	SW 6	S 4	SW 8
8	104.5	106.6	110.6	107.2	11.5	13.6	11.7	12.1	16.0	11.2	85	89	90	88	2.0	1.8	1.3	1.7	9	10	3	WSW 7	W 5	W 2
9	113.6	114.5	115.6	114.6	12.7	13.7	13.1	13.2	15.2	11.7	94	83	88	88	0.9	2.7	1.8	1.8	10	9	9	SW 2	WNW 6	WNW 5
10	116.9	117.4	117.5	117.3	12.3	15.7	13.3	13.6	16.4	12.1	88	65	90	81	1.7	6.2	1.6	3.2	10	9	10	W 4	NW 5	SW 3
11	115.4	113.8	111.2	113.5	13.3	18.9	14.9	15.5	20.5	12.7	90	57	76	74	1.6	9.4	4.0	5.0	9	8	10	SW 3	W 4	SW 3
12	109.3	110.2	111.4	110.3	13.6	18.7	13.4	14.8	19.4	13.0	92	55	85	77	1.3	9.7	2.3	4.4	10	6	10	SW 4	W 7	SW 3
13	112.3	113.1	110.6	112.0	12.3	17.3	16.2	15.5	17.5	12.0	95	63	79	79	0.7	7.3	3.8	3.9	9	9	10	WSW 2	WSW 2	S 4
14	105.8	106.7	105.6	106.0	14.9	19.9	14.5	16.0	20.5	14.4	94	73	96	88	0.9	6.3	0.7	2.6	10 •	9	10 •	SSW 3	SW 6	SSW 6
15	115.1	118.1	117.5	116.9	12.5	18.1	17.2	16.2	19.2	12.0	87	61	69	72	1.9	8.1	6.0	5.3	1	8	10	WSW 6	W 7	SW 6
16	118.5	117.9	115.5	117.3	17.3	24.4	22.6	21.7	25.4	16.2	87	61	65	71	2.6	11.8	9.6	8.0	5	2	0	SW 5	SSW 8	S 8
17	116.2	116.7	115.9	116.3	17.9	27.2	19.4	21.0	28.1	17.2	84	57	91	77	3.2	15.5	1.9	6.9	0	0	1	C 0	SSW 1	S 1
18	118.2	120.8	122.0	120.3	17.9	21.9	13.7	16.8	22.3	13.6	98	67	85	83	0.4	8.8	2.3	3.8	10	0	0	NNW 2	NNE 4	C 0
19	123.2	123.4	122.9	123.2	9.4	18.2	11.5	12.6	19.9	7.0	100	66	91	86	0.0	7.1	1.2	2.8	0 =	1	0	SW 1	N 1	C 0
20	123.8	123.6	122.9	123.4	9.9	18.3	10.2	12.2	19.2	8.8	92	51	87	77	1.0	10.2	1.6	4.3	0	0	0	SE 3	E 4	SE 2
21	123.2	123.6	124.9	123.9	9.3	18.9	11.8	13.0	19.5	7.9	88	50	82	73	1.4	10.8	2.5	4.9	0	0	0	E 1	SE 8	SE 3
22	126.6	127.3	127.2	127.0	8.0	18.6	9.1	11.2	19.4	7.0	90	47	92	76	1.0	11.2	1.0	4.4	0	1	4	ESE 2	SE 5	ESE 1
23	127.3	125.9	124.5	125.9	7.0	18.5	7.9	10.3	19.4	5.1	96	45	86	76	0.4	11.8	1.4	4.5	0	0	0	E 2	S 2	SE 3
24	122.9	121.6	120.4	121.6	6.0	18.7	8.1	10.2	19.7	2.0	86	42	89	72	1.3	12.6	1.2	5.0	0	0	0	E 4	ESE 6	SE 1
25	117.5	119.3	122.2	119.7	6.3	18.3	11.3	11.8	18.9	3.4	97	72	80	83	0.2	5.8	2.6	2.9	6	9	8	ESE 1	W 5	NW 2
26	122.5	122.3	121.3	122.0	7.5	15.8	5.3	8.5	16.2	5.3	97	53	91	80	0.3	8.4	0.8	3.2	6	6	0	WSW 2	NE 1	C 0
27	119.7	117.7	116.4	117.9	1.0	16.7	9.8	9.3	17.4	0.5	100	47	77	75	0.0	10.1	2.8	4.3	6 =	1	0	C 0	SSE 5	SSE 4
28	115.5	116.2	117.2	116.3	8.1	19.8	14.7	14.3	21.6	7.1	91	62	86	80	0.9	8.7	2.4	4.0	0	4	0	ESE 4	S 6	SE 7
29	116.2	115.1	115.8	115.7	11.4	20.5	16.8	16.4	21.5	11.2	93	69	87	83	1.0	7.5	2.5	3.7	6	9	10	SE 7	ESE 7	C 0
30	116.3	115.1	115.3	115.6	13.4	19.7	14.5	15.5	20.8	13.1	91	68	81	80	1.4	7.3	3.1	3.9	8	5	1	E 2	SE 4	ESE 9
31																								
M	116.2	116.2	115.7	116.0	11.8	19.8	13.9	14.8	20.8	10.4	93	62	85	80	1.1	9.1	2.4	4.2	4.4	4.5	3.6	2.6	4.3	3.0

Październik – Octobre

1	117.9	119.4	123.3	120.2	11.5	17.4	9.4	11.9	18.0	9.1	75	40	84	66	3.5	11.9	1.9	5.8	3	2	0	ESE 7	SE 12	E 4
2	125.1	126.1	126.1	125.8	9.2	14.1	12.4	12.0	14.8	7.4	96	68	80	81	0.4	5.1	2.9	2.8	9	8	0	E 6	E 7	E 5
3	125.5	125.6	124.9	125.3	10.2	18.7	12.9	13.7	19.4	9.4	88	48	71	69	1.4	11.2	4.3	5.6	0	1	0	E 4	SE 9	ESE 4
4	123.0	121.7	121.3	122.0	9.5	18.6	12.5	13.3	19.3	8.9	87	51	76	71	1.6	10.5	3.6	5.2	0	3	0	E 8	ESE 9	E 4
5	120.2	119.0	119.5	119.6	8.3	18.5	12.9	13.2	20.0	7.5	89	57	83	76	1.3	9.3	2.7	4.4	1	1	0	ESE 6	SE 8	SE 6
6	118.9	116.3	113.3	116.2	9.2	20.2	15.0	14.8	21.7	9.0	95	56	68	73	0.6	10.4	5.4	5.5	1	0	0	SE 5	SE 8	SE 8
7	109.4	106.3	105.6	107.1	10.0	18.5	15.8	15.0	19.6	9.4	81	46	58	62	2.4	11.4	7.4	7.1	0	0	10	SE 7	SE 10	ESE 9
8	104.9	104.9	110.8	106.9	11.8	14.5	12.1	12.6	16.0	11.2	81	76	98	85	2.6	3.9	0.3	2.3	8	10	10 •	SE 7	SE 8	WSW 5
9	118.3	122.1	125.6	122.0	9.3	16.5	8.1	10.5	17.6	7.4	95	73	97	88	0.6	5.2	0.3	2.0	4	8	0	SW 4	SW 5	SW 2
10	127.0	126.6	125.4	126.3	5.0	19.2	11.5	11.8	19.9	4.3	98	62	94	85	0.1	8.5	0.9	3.2	4 =	1	0	C 0	SW 5	C 0
11	123.5	121.6	120.8	122.0	9.2	19.7	15.1	14.8	20.0	7.4	93	54	71	73	0.8	10.5	5.0	5.4	3	8	3	SSE 1	S 5	SW 3
12	125.2	127.5	128.2	127.0	9.4	16.7	9.1	11.1	16.8	8.9	100	52	88	80	0.0	9.0	1.4	3.5	1	4	0	C 0	NW 5	NW 2
13	128.3	129.1	129.3	128.9	6.4	13.9	6.9	8.5	14.5	6.1	98	71	96	88	0.1	4.6	0.4	1.7	1	5	0	W 2	NNW 1	WNW 3
14	128.0	127.6	126.1	127.2	4.8	12.1	12.0	10.2	16.0	4.4	100	87	88	92	0.0	1.8	1.7	1.2	10 =	9	9	SW 2	NW 5	W 3
15	124.4	123.2	121.0	122.9	11.0	12.3	11.3	11.5	12.7	10.8	92	75	85	84	1.0	3.5	2.0	2.2	9	10	10	W 3	WNW 4	WSW 1
16	117.2	115.1	112.1	114.8	8.7	9.5	10.7	9.9	12.6	8.4	89	87	87	88	1.2	1.6	1.7	1.5	2	4	10	SSW 2	SW 5	SW 4
17	106.6	101.1	91.1	99.6	9.9	11.3	8.6	9.6	11.5	8.3	92	80	94	89	1.0	2.6	0.6	1.4	10	10	10	SW 5	SW 7	S 9
18	84.0	86.8	90.8	87.2	9.9	12.7	9.1	10.2	13.4	8.5	84	71	79	78	1.9	4.3	2.5	2.9	7	9	10	S 8	S 6	SSW 2
19	93.4	95.5	98.8	95.9	6.7	11.2	8.3	8.6	11.5	6.3	88	70	93	84	1.2	4.0	0.8	2.0	9	6	10	SSE 4	SSE 5	SSE 6
20	104.8	108.7	111.9	108.5	6.8	12.0	9.1	9.2	12.8	6.3	87	67	96	83	1.3	4.6	0.5	2.1	7	8	10 •	E 1	SE 4	C 0
21	110.5	109.1	111.6	110.4	10.2	11.5	10.9	10.9	12.1	8.6	97	99	90	95	0.3	0.2	1.3	0.6	10	10 •	10	C 0	C 0	SE 6
22	115.5	120.4	121.1	119.0	8.5	11.3	6.9	8.4	12.4	6.5	94	72	94	87	0.6	3.8	0.5	1.6	10	6	2	S 7	SSW 7	SE 7
23	119.8	118.4	115.7	118.0	7.7	11.0	11.7	10.5	11.9	6.5	97	83	80	87	0.3	2.3	2.8	1.8	9	1	9	SE 8	SE 9	S 10
24	119.0	118.4	112.8	116.7	8.1	11.7	13.1	11.5	13.1	7.4	99	82	82	88	0.2	2.5	2.8	1.8	9	6	4	WSW 5	S 5	S 10
25	107.2	108.4	111.3	109.0	12.0	13.9	12.8	12.9	15.6	11.2	70	79	95	81	4.1	3.4	0.7	2.7	9	10	10	SSW 9	SSW 8	SW 1
26	109.5	109.0	109.0	109.2	11.8	14.6	14.5	13.8	15.0	11.0	93	87	87	89	1.0	2.2	2.2	1.8	10 •	9	10	SSW 4	SW 5	S 5
27	105.2	105.3	108.2	106.2	12.5	17.1	13.7	14.2	17.6	12.0	79	62	90	77	3.1	7.4	1.6	4.0	9	6	10 •	SW 5	SW 6	SW 5
28	109.6	109.5	109.5	109.5	9.3	14.3	11.1	11.4	14.9	9.1	95	64	80	80	0.6	5.8	2.6	3.0	4	9	5	SW 1	SSW 5	SSW 6
29	110.1	110.8	111.7	110.9	8.9	11.0	9.3	9.6	12.4	5.5	89	85	95	90	1.2	1.9	0.6	1.2	4	10	9	SW 2	SW 2	SW 2
30	111.9	113.3	115.7	113.6	8.0	11.4	8.0	8.8	11.8	6.6	93	79	96	89	0.7	2.8	0.4	1.3	10	9	0	WSW 4	W 4	SW 2
31	113.2	111.6	112.9	112.6	7.7	11.3	10.5	10.0	11.4	5.9	91	69	90	83	0.9	4.2	1.3	2.1	9	10	10 •	SW 6	SW 8	SW 8
M	114.7	114.8	115.0	114.8	9.1	14.4	11.1	11.4	15.4	8.0	90	69	86	82	1.2	5.5	2.0	2.9	5.9	6.2	5.5	4.3	6.0	4.5

Szczecin – Dąbie H_s = 1 m H_b = 6,9 m h_w = 20 m Wrzesień – Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD p	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 1^{40}–7^{20}, ⌒ °0^{00}–10^{00}, 23^{00}–24
2	7	.	.	–	= 6^{30}–7^{30}, = –10^{15}, =, =, = °18^{35}–24, ⌒ °0^{00}–10^{00}
3	7	.	.	–	= $^{0-1}$, = $^{0-2}$ 0^{00}–10^{35}, = –12^{30}, ⌒ °21^{00}–24
4	8	.	.	–	=, = 2^{30}–12^{10}, = 20^{25}–24, ⌒ $^{0-1}$ 0^{00}–10^{00}, ⌒ °21^{00}–24
5	7	1.9	.	–	• °16^{30}–18^{05}, ↘ °17^{15}–18^{20} E; ↘ np, = 0^{00}–5^{35}, = $^{0-1}$–7^{12}, = –11^{30}, ⌒ °na–a
6	7	0.2	.	–	• °1^{15}–2^{20}, ↘ na, = 0^{30}–12^{30}, ⌒ °np, ⊕ p
7	7	5.6	.	–	• °4^{01}–5^{10} 6^{10} ▽ 15^{20} 22^{10} • °22^{15}–24, ⌒ °0^{00}–4^{00}
8	8	0.0	.	–	▽ °2^{07}–18, 2^{30}–45 • °12^{35}–13^{20}
9	8	0.0	.	–	• °8^{24}–33 9^{10}–10^{45} 14^{13}–21^{30}–40
10	8	0.0	.	–	▽ °9^{09}–15, 16^{32}–36
11	7	0.0	.	–	= 5^{30}–11^{30}, ⌒ °22^{00}–24
12	8	1.4	.	–	• °1^{50}–2^{30} 3^{20} ▽ °17^{45}–18^{00}, = 5^{15}–9^{40}
13	8	4.0	.	–	• $^{1-0}$ 1^{45}–2^{00} • °–5^{37}
14	7	8.6	.	–	• $^{0-1}$ 3^{40}–4^{20}–9^{05} • °17^{42}–18^{20}–20^{20}, 21^{15}–22^{10}, = a, ⊕ p
15	8	.	.	–	▽ °10^{8}–15
16	8	.	.	–	⌒ °6^{00}–9^{00}
17	7	.	.	–	= 4^{20}–6^{15}, 22^{30}–24, ⌒ °22^{00}–24
18	8	.	.	–	= 0^{00}–9^{40} = 23^{50}–24, ⌒ °0^{00}–11^{00}, 21^{00}–24
19	8	.	.	–	= 0^{00}–1^{50} ≡ $^{0-1}$ = °–11^{40} = –11^{50}, ⌒ °0^{00}–12^{00}, 19^{00}–24
20	8	.	.	–	⌒ $^{0-1}$ 0^{00}–10^{00} ⌒ °22^{00}–24
21	8	.	.	–	= 5^{30}–7^{15}, ⌒ °0^{00}–11^{00}, 21^{00}–24
22	8	.	.	–	= 4^{20}–7^{20}, ⌒ °0^{00}–10^{00}, 21^{00}–24
23	8	.	.	–	= 21^{00}–24, ⌒ °0^{00}–10^{00}, 18^{00}–24
24	8	.	.	–	= 5^{30}–8^{40} ⌒ °0^{00}–11^{00}, 21^{00}–24
25	6	0.0	.	–	• °10^{40}–11^{07} ▽ °–11^{11} = 2^{15}–6^{40} ≡ °–7^{05} = –14^{30}, ⌒ °0^{00}–10^{00}, np
26	8	.	.	–	= 9^{15}–10^{20} = 21^{10}–23^{35} = $^{0-1}$–24, ⌒ °0^{00}–10^{00}, 20^{00}–24
27	8	.	.	–	= $^{1-2}$ 0^{00}–9^{20} = –10^{30} ⌒ $^{1-0}$ 0^{00}–10^{00} ⌒ °np
28	7	.	.	–	= 18^{50}–21^{30}, 23^{50}–24, ⌒ °0^{00}–11^{00}, 18^{00}–24
29	6	0.1	.	–	• °23^{35}–24, = 0^{00}–2^{10} ≡ °–4^{50} = –24, ⌒ °0^{00}–9^{00}
30	7	.	.	–	• °0^{00}–2^{15}, =, ∞ 0^{00}–24, ≫ 23^{10}–24
31					
Σ	–	21.8	–	–	UWAGI

Październik – Octobre

1	8	.	.	–	= na, ≫ 0$^{00-40}$, 8^{15}–15^{30}
2	7	.	.	–	= 5^{30}–9^{40} ⌒ °23^{00}–24
3	8	.	.	–	⌒ °0^{00}–8^{00}
4	7	.	.	–	⌒ °2^{00}–8^{00}
5	7	.	.	–	= 17^{15}–24, ⌒ °4^{00}–9^{00}
6	7	.	.	–	= 0^{00}–10^{30}, ⌒ °10^{0}–9^{00}
7	7	.	.	–	≫ 9^{30}–10^{30}, 12^{35}–17^{20}
8	7	1.9	.	–	• °11^{40}–15^{35}, 17^{40}–19^{20}–21^{30}–23^{10}, = 17^{15}–24
9	7	.	.	–	= 0$^{00-30}$–5^{30}–8^{15}–10^{30}–24 = 21^{15}–24, ⊕ 13^{30}–14^{15}
10	7	.	.	–	=, = 0$^{00-10}$ = $^{0-1}$–8^{40} = –11^{15}, 17^{15}–23^{40} = °–24, ⌒ °20^{00}–24
11	7	.	.	–	= $^{0-1}$ 0^{00}–1^{45} = –6^{15}–18^{30}–19^{30}, ⌒ $^{1-0}$ 0^{00}–9^{00}, ⊕ 14^{30}–16^{30}
12	8	.	.	–	=, = 2^{30}–7^{30} = 18^{30}–24, ⌒ °20^{0}–10^{00}–18^{00}–24
13	8	.	.	–	= 0^{00}–11^{15}, 22^{30}–24, ⌒ °0^{00}–12^{00}, 19^{00}–24
14	6	.	.	–	= 0^{00}–2^{50} = $^{0-1}$–8^{05} = –8^{15} = °–10^{15} = –19^{30} ⌒ $^{0-1}$ 0^{00}–11^{00}
15	8	.	.	–	= 0^{30}–6^{30}, 21^{35}–24
16	6	.	.	–	= 0^{00}–24
17	6	4.5	.	–	• °13^{10}–24, = 0^{00}–24
18	8	0.3	.	–	• °0^{00}–2^{20}, 23^{45}–24, = 0^{00}–2^{20}
19	7	.	.	–	• °0^{00}–2^{00}, 3^{10}, ⌒ °np
20	8	13.5	.	–	• °17^{40}–18^{10}–21^{35}–22^{15}–23^{05}–24, = 17^{10}–18^{25}, ⌒ °0^{00}–8^{00}
21	4	1.0	.	–	• $^{0-1}$ 0^{00}–0^{10}–3^{25} • °4^{20}–5^{20} • °7^{40}–9^{15}, 11^{45}–14^{15} • °14^{45}–16^{35}, =, = °6^{10}–20^{30}
22	7	.	.	–	= 5^{30}–9^{30}, 18^{50}–20^{30}, ⌒ °18^{00}–24
23	6	2.8	.	–	• °22^{40}–24, = 5^{45}–21^{30}, ≫ 19^{35}–21^{30} ⌒ °0^{00}–11^{00}
24	7	.	.	–	• °0^{00}–1^{45}, =, = 1^{45}–10^{30}, ≫ 10^{30}–22^{30}
25	8	5.9	.	–	• °7^{05}–7^{35}–10^{25} ▽ $^{0-1}$ 16^{11}–17^{35}, = 17^{45}–24
26	6	7.6	.	–	• $^{0-1}$ 5^{05}–9^{20}, = 0^{00}–10^{10}, 11^{30}–24
27	7	0.1	.	–	• °19^{45}–24, = 0^{00}–5^{30}, 17^{15}–24
28	7	0.0	.	–	• °0^{00}–2^{30} 16^{35} 17^{20}, = 0^{00}–3^{50}
29	7	.	.	–	= 5^{30}–10^{30} 17^{30}–24, ⌒ °1^{00}–10^{00}, 18^{00}–24
30	7	.	.	–	= 0^{00}–12^{20}, 16^{20}–21^{40} = $^{2-1}$–22^{05} = –24, ⌒ °0^{00}–11^{00}, 16^{00}–24
31	7	1.3	.	–	• °17^{10}–22^{10}, = 0$^{00-20}$ = –10^{30}, ⌒ °0^{00}–9^{00}
Σ	–	58.7	–	–	UWAGI

Szczecin – Dąbie φ = 53°24' λ = 14°37' Listopad – Novembre 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE : POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	114.6	115.1	120.0	116.6	9.2	11.9	10.5	10.5	11.9	9.0	96	84	82	87	0.4	2.1	2.5	1.6	10 •	10	9	WSW 7	WSW 7	W 4
2	119.4	115.1	108.2	114.2	8.6	11.6	11.2	10.6	12.0	6.9	94	79	92	88	0.6	2.8	1.0	1.5	10	10	10 •	WSW 5	SSW 7	SSW 6
3	100.9	98.9	101.8	100.5	9.7	10.2	5.6	7.8	11.4	5.6	79	77	92	85	2.5	2.8	0.7	2.0	9	9	0	SW 7	SW 9	SW 6
4	103.8	106.9	111.8	107.5	3.8	6.1	3.0	4.0	6.2	2.8	85	75	86	81	1.3	2.5	1.1	1.6	10	9	0	WSW 7	SW 7	SW 2
5	113.3	117.6	120.3	117.7	-0.1	7.0	2.7	3.1	7.6	-1.1	98	81	88	89	0.2	1.9	0.9	1.0	10 =	7	2	WSW 2	NE 3	N 3
6	120.0	118.1	114.1	117.4	0.0	8.9	7.2	5.8	9.3	-0.6	98	80	90	89	0.1	2.3	1.1	1.2	9	9	10	C 0	NNE 5	NE 2
7	108.1	105.6	105.6	105.8	8.8	9.7	10.1	9.7	10.2	7.2	99	95	99	98	0.1	0.6	0.2	0.3	10	10 ,	10 ,	NE 3	E 3	ESE 4
8	105.3	105.9	104.8	105.3	7.1	7.3	5.6	6.4	10.7	5.1	91	74	85	85	0.9	2.6	1.4	1.6	10	5	10	SSW 5	SW 4	SSE 3
9	101.3	100.5	100.6	100.8	4.4	7.7	8.4	7.2	8.5	4.0	87	84	82	84	1.1	1.6	2.0	1.6	8	9	9	S 7	S 3	S 4
10	99.9	101.5	104.3	101.9	6.7	7.6	5.5	6.3	8.7	5.4	94	99	94	96	0.6	0.1	0.5	0.4	10 •	10 •	2	SSE 4	SW 3	WSW 2
11	105.1	105.5	107.2	105.9	2.8	8.3	6.7	6.1	8.6	2.3	98	86	97	93	0.2	1.6	0.3	0.7	10	4	9	SW 1	NE 1	NE 1
12	108.2	110.0	112.7	110.3	8.6	9.5	6.3	7.7	10.1	6.3	94	84	84	87	0.6	1.9	1.5	1.3	10	10	10	E 2	E 5	E 5
13	112.6	111.7	111.8	112.0	4.1	4.7	3.4	3.9	6.3	3.1	85	85	86	85	1.2	1.2	1.1	1.2	10	10	10	E 8	E 7	E 6
14	112.7	116.8	119.6	116.4	3.3	4.6	4.0	4.0	4.8	2.6	90	79	77	82	0.7	1.8	1.9	1.5	10	10	10	NE 6	NE 6	NE 4
15	119.8	119.6	118.6	119.3	2.8	5.0	2.8	3.4	5.0	2.0	93	75	82	83	0.6	2.2	1.3	1.4	10	10	9	C 0	WSW 2	W 4
16	116.3	114.8	112.3	114.5	2.7	4.0	3.9	3.6	4.4	1.9	86	88	95	89	1.0	0.9	0.6	0.8	10	10 •	10 ,	WSW 5	WSW 3	WSW 3
17	109.7	110.5	112.5	110.9	6.3	8.9	3.0	5.3	9.2	2.8	95	67	93	85	0.4	3.8	0.6	1.6	10 ,	4	4	W 4	WNW 4	W 2
18	108.8	110.8	114.1	111.2	5.3	7.3	2.2	4.3	8.0	2.1	84	58	82	75	1.4	4.3	1.3	2.3	9	6	2	WSW 4	N 2	NE 1
19	117.7	122.5	129.4	123.2	0.2	5.9	0.4	1.7	6.9	-0.9	88	67	92	82	0.7	3.1	0.5	1.4	1	6	0	NW 1	N 4	C 0
20	133.8	135.8	135.8	135.1	-1.8	3.3	-0.6	0.6	3.8	-4.1	96	77	93	89	0.2	2.1	0.4	0.9	4	4	8	C 0	C 0	C 0
21	133.2	130.8	127.8	130.6	-3.9	2.2	-3.3	-2.6	2.4	-7.4	89	63	93	82	0.4	2.7	0.3	1.1	4	7	1	C 0	C 0	C 0
22	123.8	121.9	118.6	121.4	-3.0	2.2	-3.6	-4.2	3.3	-8.4	87	66	93	83	0.4	2.3	0.2	1.0	1	0	0	C 0	W 3	C 0
23	113.7	111.7	111.4	112.3	-3.8	4.0	0.7	-0.1	4.4	-8.0	93	62	79	79	0.2	3.0	1.3	1.3	0	1	2	C 0	C 0	SW 2
24	114.4	116.7	116.6	115.9	2.9	3.9	2.6	3.0	4.2	0.3	93	98	100	98	0.4	0.2	0.0	0.2	10	10 , =	10 =	C 0	C 0	C 0
25	114.9	113.2	111.6	113.2	2.3	2.8	3.4	3.0	3.4	2.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10 =	10 =	C 0	SW 2	C 0
26	109.4	108.0	105.1	107.5	1.6	2.6	2.2	2.2	3.3	0.9	98	96	100	98	0.2	0.3	0.0	0.2	10	10	10 =	SW 2	SE 2	ESE 2
27	102.9	103.3	104.4	103.3	2.0	3.3	3.1	2.9	3.6	1.3	96	98	98	97	0.3	0.1	0.1	0.2	10	10 ,	10 • ,	NE 2	NE 1	NE 1
28	107.7	109.8	111.0	109.3	2.0	4.2	4.1	3.4	4.3	1.3	98	93	93	93	0.2	0.4	0.6	0.4	10	10 •	10	C 0	E 1	SSW 2
29	110.6	111.6	108.8	110.3	4.6	5.0	4.2	4.3	5.1	2.9	97	97	85	93	0.3	0.3	1.2	0.6	10	10 •	6	SW 2	SW 3	SW 5
30	103.9	102.3	99.2	99.8	4.9	5.9	7.2	6.3	7.3	3.6	87	94	86	89	1.1	0.6	1.3	1.1	9	10 •	10	SW 5	SW 6	SW 9
31																								
M	112.3	112.4	112.4	112.4	3.1	6.3	4.0	4.4	6.9	1.7	92	82	90	88	0.6	1.7	0.9	1.1	8.5	8.0	6.8	3.0	3.4	2.8

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1	90.5	94.3	95.6	93.5	7.3	7.1	5.7	6.4	9.3	5.5	86	80	88	85	1.5	2.1	1.2	1.6	10 •	9	10 •	W 6	WSW 5	SW 5
2	84.2	82.9	96.4	87.8	10.1	11.9	5.1	8.0	11.9	3.8	90	67	78	78	1.3	4.6	2.0	2.6	10	7	9	SW 8	WSW 7	W 8
3	103.0	103.9	102.4	103.1	1.7	4.9	3.6	3.4	5.4	1.4	81	72	78	77	1.3	2.3	1.7	1.8	2	6	9	W 6	SW 7	SW 6
4	102.0	107.1	105.0	104.7	1.6	3.8	4.4	3.6	4.5	0.8	93	87	89	90	0.6	1.1	1.0	0.9	2	9	10 •	SW 3	WSW 2	SE 3
5	99.2	97.9	97.8	98.3	10.9	14.3	10.7	11.7	14.9	4.1	89	72	70	77	1.4	4.6	3.9	3.3	9	9	9	SW 5	WSW 8	WSW 7
6	106.2	107.7	111.1	108.3	3.0	4.0	0.8	2.2	11.1	0.7	66	64	90	73	2.6	2.9	0.7	2.1	8	9	0	WSW 6	WSW 8	WSW 5
7	112.5	114.4	115.3	114.1	0.1	1.0	1.4	1.0	1.4	-1.2	92	85	81	86	0.5	1.0	1.3	0.9	10	10	10	WSW 3	W 4	SW 3
8	114.8	116.3	117.5	116.2	1.0	2.3	2.0	1.8	2.6	0.4	87	80	82	83	0.9	1.4	1.3	1.2	9	8	9	SW 4	W 4	WSW 3
9	116.8	114.3	110.9	114.0	-1.7	1.6	0.4	0.2	2.1	-1.9	96	74	75	82	0.2	1.8	1.6	1.2	9	10	0	SW 1	SSE 4	SE 5
10	108.6	107.9	106.3	107.6	1.8	3.8	3.0	3.9	5.0	0.2	85	87	90	87	1.1	1.1	0.8	1.0	10	9	10	SSW 3	WSW 4	SW 3
11	97.5	91.3	94.8	94.5	4.6	6.6	9.2	7.4	9.7	3.3	95	96	96	96	0.4	0.4	0.4	0.4	10	10 •	10 •	S 2	SSW 3	W 3
12	104.4	107.4	113.3	109.0	4.0	3.4	1.1	2.4	9.4	0.9	98	97	96	97	0.1	0.3	0.2	0.2	10 • ,	10 ,	10 •	ENE 1	E 4	NE 3
13	124.7	128.2	129.7	127.5	-0.4	1.6	-4.4	-1.9	1.6	-5.4	88	59	91	79	0.7	2.9	0.4	1.3	10	1	1	NE 4	S 2	SE 2
14	130.5	132.6	133.0	132.7	-8.2	-5.0	-6.0	-5.8	-2.8	-8.3	87	60	81	76	0.4	2.0	0.7	1.0	0	1	3	ESE 2	E 3	WSW 1
15	131.7	130.3	130.2	130.7	0.6	0.8	0.6	0.6	1.4	-6.2	72	76	96	81	1.8	1.6	0.3	1.2	10	3	10 *	N 4	N 8	NNE 5
16	137.3	140.4	144.7	140.8	-10.6	-9.2	-12.2	-11.0	0.7	-13.6	84	70	81	78	0.4	0.9	0.4	0.6	0	1	0	ESE 1	SE 3	E 2
17	146.3	146.2	145.0	145.9	-16.0	-9.6	-14.0	-13.4	-8.4	-17.2	81	75	83	80	0.3	0.7	0.3	0.4	1	0	0	E 2	C 0	C 0
18	143.0	141.3	138.7	141.0	-10.4	-5.4	-6.9	-7.4	-4.3	-14.6	84	65	72	74	0.4	1.4	1.0	0.9	8	2	0	SW 2	W 3	WSW 2
19	134.3	133.6	132.3	133.3	-2.2	0.7	0.2	-0.3	0.7	-7.7	76	84	100	87	1.2	1.0	0.0	0.7	10	10	10 , =	W 3	WNW 4	W 3
20	125.7	118.3	116.9	120.3	-0.4	2.7	1.9	1.3	4.4	-0.9	100	98	96	98	0.0	0.1	0.3	0.1	10 =	10 ,	9	W 3	W 4	NW 1
21	116.8	119.2	118.4	118.1	0.8	1.0	-3.0	-1.0	2.2	-5.8	83	72	84	79	1.3	1.9	0.8	1.3	1	6	9	NW 2	N 3	SW 3
22	110.0	109.3	113.6	111.0	-2.3	-0.9	-6.1	-3.8	-0.1	-6.7	96	79	92	89	0.3	1.2	0.3	0.6	10 *	2	10 *	C 0	W 2	N 1
23	116.1	117.3	118.0	117.1	-9.8	-2.2	-9.3	-7.8	-1.9	-11.3	88	94	91	91	0.4	0.3	0.3	0.3	1	8	4	W 1	NNW 2	W 2
24	117.4	116.3	114.4	116.0	-11.7	-11.0	-8.4	-9.9	-8.3	-12.7	89	86	92	89	0.3	0.4	0.3	0.3	0	4	10	W 3	SW 4	SW 3
25	112.2	111.4	109.3	111.0	-10.8	-10.8	-18.3	-14.6	-8.2	-19.1	83	83	78	81	0.4	0.4	0.3	0.4	10	0	0	SW 3	WSW 1	C 0
26	106.6	103.9	103.2	106.9	-21.6	-14.8	-18.0	-18.1	-12.9	-22.3	89	91	84	88	0.1	0.2	0.2	0.2	0	1	3	C 0	C 0	C 0
27	112.2	113.9	113.7	113.3	-9.2	-8.7	-9.9	-9.4	-8.3	-19.3	92	93	91	93	0.3	0.2	0.3	0.3	10 =	10	8	C 0	SE 2	E 2
28	110.7	108.2	107.1	108.7	-13.9	-8.7	-7.2	-9.2	-7.2	-16.6	87	89	88	88	0.3	0.4	0.4	0.4	10 ≙	10 *	10	SSE 3	SSE 2	C 0
29	106.2	103.4	103.8	103.1	-3.0	-1.0	-1.8	-2.4	-0.6	-7.6	90	91	90	90	0.4	0.3	0.3	0.3	10	10	4	C 0	S 1	SE 2
30	102.6	101.6	101.1	101.8	-0.6	1.3	3.7	2.0	3.8	-3.3	87	76	72	78	0.7	1.6	2.3	1.5	10	9	10 •	SSE 4	SE 2	SSW 3
31	101.3	101.9	99.9	99.7	3.1	3.7	3.6	4.0	5.9	1.3	84	76	76	79	1.2	2.3	1.9	1.8	0	9	10	SW 6	SW 4	SW 4
M	113.7	113.8	114.3	113.9	-2.7	-0.2	-2.1	-1.8	1.3	-5.7	87	80	86	84	0.7	1.4	0.9	1.0	6.8	6.6	6.7	3.0	3.3	3.0

Szczecin – Dąbie $H_s = 1\,m$ $H_b = 6{,}9\,m$ $h_w = 20\,m$ Listopad – Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.3	.	–	●° 4^15 5^10 – 8^20 11^15 . = 5^30 – 12^30
2	6	1.3	.	–	●° 14^09 – 15^05 10^42 – 21^25 . 22^45 – 24 . = 5^30 – 24
3	7	1.9	.	–	●° 0^00–20 ▽¹ 15^45 – 16^05 . = 0^00 – 4^30
4	8	.	.	–	
5	8	.	.	–	= 2^10 – 6^40 ≡^0-1 ≡¹ – 9^20 = – 11^40 . ⌴° 1^00 – 8^00 ⌓° np
6	8	0.1	.	–	●° 21^35 – 22^20 ●° 23^45 – 24 . = 4^50 – 9^15 . ⌓° na . ⌴° 8^00
7	6	0.9	.	–	●° 0^00–15 ●° – 2^15 ●° 11^10 – 16^40 . 17^40 – 18^10 ●° – 19^10 . 20^05 ●° – 24 . = 1^30 – 2^20
8	7	0.1	.	–	●° 0^00–10 ●° 13^40 – 24 . = 0^00 – 3^30 . 16^10 – 24
9	7	0.0	.	–	●° 0^00..15 . 12^25–50 . 15^10 16^20 . = 0^00 – 7^20
10	5	2.3	.	–	●° 6^20 – 15^35 . = 9^30 – 24
11	7	.	.	–	= 0^00 – 1^35 ≡° – 6^45 = – 12^10 . 16^30 – 24
12	7	0.0	.	–	●° 13^12..30 . = 0^00 – 10^15
13	8	6.2	.	–	
14	8	.	.	–	●° 0^00 – 4^10
15	7	.	.	–	
16	5	0.7	.	–	●° 12^20 – 15^45 . 16^47 – 17^15 ●●° – 19^25 . ●° 20^20 . 21^15 . = 11^05 – 24
17	8	0.0	.	–	●° 3^35 – 6^12 . 7^17 . = 0^00 – 9^30
18	8	0.0	.	–	▽° 8^44 . 9^51
19	8	.	.	–	= 20^30 – 24 . ⌴° 2^00 – 9^00 . 23^00 – 24
20	6	.	.	–	= 0^00 – 13^15 . 15^20 – 24 . ⌴° 0^00 – 10^00 . 19^00 – 24
21	7	.	.	–	= 0^00 – 11^30 . 20^50 – 24 . = 0^00 – 11^30 ≡ 20^50 – 24
22	6	.	.	–	= 0^00 – 24 . ⌴¹ 1^00 – 12^00 ⌴° 20^00 – 24
23	7	.	.	–	= 0^00–40 ≡ – 2^20 = – 12^30 ∞ p . = p – 24 . ⌴^0-1 0^00 – 11^00
24	2	1.2	.	–	●° 9^25 – 13^15 . 14^10 . = 0^00 – 7^10 ≡^0-1 14^20 ≡° – 18^15 ≡^1-2 24
25	3	.	.	–	●●° 1^20 – 4^10 ●° – 6^20 . ≡² 0^00 – 4^25 = – 7^10 ≡° – 7^40 ≡^1-0 – 24
26	5	.	.	–	≡° . = 0^00 – 24
27	4	3.2	.	–	●° . ●●° 10^10 – 15^40 ●° . ●●° . ●° 16^40 – 24 . ≡° 0^00 – 3^40 = – 24
28	5	0.6	.	–	●● 0^00 – 2^10 ●° 11^05 . 12^20 – 15^10 ●●° 16^12 . = 0^00 – 24
29	4	1.7	.	–	●● ° 0^20 – 2^15 ●° 9^45 – 13^10 . = 0^00 – 7^10 ≡^0-1 9^45 = – p
30	6	5.9	.	–	●° 11^32 – 16^20 . 18^40 . 19^45 . 23^45 . 24 . ≫ 20^30 – 24
31	.				
Σ	–	26.4	–	–	UWAGI.

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1	8	8.9	.	–	●° 0^00 . 1^30 – 8^20 . 19^20 – 20^30 . 24 . ≫ 0^00 – 4^30
2	8	2.9	.	–	●° 0^00 . 0^15 – 4^35 . 5^10 – 6^15 ▽° 8^21-27 . 10^58 – 11^53 . 18^12–48
3	8	.	.	–	
4	7	10.6	.	–	●° 20^40 – 24 . = 8^30 – 10^30 . 16^30 – 24
5	8	2.3	.	–	●° 0^00 – 2^30 . 6^25 ▽° 10^17–19 . 17^25–28 ▽¹ 18^06–28 . = 0^00 – 6^25 . ≫ np
6	8	.	.	–	
7	7	.	.	–	⌴° 1^00 – 11^00
8	7	0.0	.	–	▽° 7^35 – 8^25
9	6	0.0	.	–	●° 23^40 – 24 . = 6^30 – 14^15 . ⊕ 10^15 – 13^30
10	6	1.7	.	–	●° 0^00–30 . 22^55 – 23^20 . = 0^30 – 24
11	6	10.4	.	–	●° 2^10 . 4^00 – 6^10 ●^0-1 7^25 – 14^45 ●° . ●° 15^05 . 19^20 – 24 . = 0^00 – 24
12	5	3.7	.	–	●° . ●° . ●●° 0^00 – 8^20 . 13^20 – 21^30 * ° 24 . = 0^00 – 21^30
13	8	.	.	–	*° 0^00 – 2^20 . ⌴° 19^00 – 24
14	8	0.1	.	–	= 18^15 – 24 . ⌴° 0^00 – 24
15	8	0.8	1	–	△° 0^40 . 6^10 *° 9^35 . 11^20 △° 16^05 – 18^10 *° 20^15 . 21^30 . = na
16	7	.	1	–	
17	6	.	1	–	= 9^30 – 24
18	7	.	1	–	= 0^00 – 8^30
19	6	0.0	1	–	⌓° 18^35 – 24 . = 7^15 – 19^15 ≡° – 22^30 = – 24 . ∽ 18^35 – 24
20	5	0.0	1	–	⌓° 0^00 . 1^40 ●° 11^15 – 13^30 . 15^20 . = ≡° 0^00 – 24 . ∽ 0^00 – 4^00
21	8	3.4	.	–	△° 10^25–30 *° 13^35–37 *° 22^10 . 24 . = 0^00 – 6^30
22	7	1.1	5	–	*° 0^00 . 1^00 – 7^10 *^2-0 14^30 – 15^05 *^0-1 15^30 – 16^10 *° 20^50 – 21^15
23	6	0.4	7	–	*° 10^03 . 12^13 . = 7^30 – 13^10 . 14^40 – 23^30
24	7	0.0	8	–	*° 1^10 – 1^10 ↔ – 18^20
25	6	.	9	–	= 12^30 – 24
26	5	.	7	–	= 0^00 – 24
27	4	0.0	7	–	= 0^00 – 3^00 ≡^0-2 12^10 = – 24
28	6	0.0	7	–	△° 4^25 – 9^30 *° 14^40 . = 0^00 – 24
29	5	.	7	–	= 0^00 – 24
30	6	0.0	7	–	●° 20^45 – 21^20 . = 0^00 – 21^20
31	6	1.4	5	–	●° 21^35 – 23^40 . = 12^15 – 20^30
Σ	–	47.7	–	–	UWAGI.

Poznań – Ławica φ = 52°25' λ = 16°50' Styczeń – Janvier 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	103.0	104.5	105.1	104.2	0.4	1.4	0.3	0.6	1.5	-1.6	96	89	90	92	0.3	0.8	0.6	0.6	10	10	9	SSW 3	SSW 3	SSE 2
2	103.5	101.7	97.1	100.8	-0.9	0.8	-0.3	-0.2	1.1	-1.5	93	92	94	93	0.4	0.5	0.4	0.4	10	9 *	9	C 0	SSE 2	SE 5
3	88.2	85.1	87.7	87.0	-0.8	2.1	3.0	1.8	3.5	-1.4	87	85	83	85	0.7	1.0	1.3	1.0	10	9	10	SE 6	SSW 4	S 4
4	86.2	84.8	90.4	87.1	1.8	4.0	1.4	2.2	4.4	0.9	96	88	92	92	0.3	0.9	0.6	0.6	10	10	6	E 3	ESE 3	S 4
5	92.4	94.0	98.3	94.9	-0.6	1.6	1.6	1.0	2.9	-0.7	94	87	89	90	0.3	0.9	0.8	0.7	8	9	10	SSE 1	S 3	W 6
6	102.7	100.6	98.3	100.5	0.4	3.1	0.8	1.3	3.6	-0.2	92	73	79	81	0.5	2.1	1.4	1.3	4	6	10	SSW 4	SSE 5	SSE 4
7	97.8	98.3	99.0	98.4	-0.2	3.6	1.2	1.4	4.0	-0.4	92	73	92	86	0.5	2.1	0.5	1.0	9	5	10 •	SE 2	S 3	S 1
8	101.0	99.4	96.4	98.9	1.2	2.4	1.4	1.6	2.7	1.0	96	89	92	92	0.3	0.8	0.6	0.6	10	10	10 *	WSW 2	S 4	S 6
9	97.2	98.5	98.1	97.9	2.8	4.4	3.0	3.3	5.4	1.3	93	82	88	88	0.6	1.5	0.9	1.0	10 •	6	10 •	SW 5	SW 3	S 4
10	101.4	100.9	99.3	100.5	0.9	4.7	1.2	2.0	5.2	0.3	94	79	89	87	0.4	1.7	0.8	1.0	9	3 ⊙	9	SSW 2	SSE 3	SSE 3
11	99.9	103.8	109.3	104.3	-1.0	1.1	0.3	0.2	1.3	-1.0	94	92	92	93	0.4	0.5	0.5	0.5	6	10 *	10	SE 2	SSW 3	WNW 5
12	114.3	117.6	121.5	117.8	-1.4	-0.9	-3.1	-2.1	0.3	-3.2	82	81	90	84	1.0	1.1	0.5	0.9	9 *	10 *	4	W 7	WNW 8	WNW 7
13	121.6	118.9	116.8	119.1	-4.4	-1.0	0.0	-1.4	0.3	-6.4	91	77	92	87	0.4	1.3	0.5	0.7	9	10	10 •	SSW 3	SSW 7	SW 4
14	116.0	117.8	121.8	118.5	0.8	0.6	0.7	0.7	0.9	-0.2	96	92	98	95	0.3	0.5	0.1	0.3	10 ⸗	10 •	10 =	SW 1	WNW 2	NW 1
15	124.7	124.0	121.1	123.3	-1.5	-2.2	-3.0	-2.4	0.9	-3.1	96	96	97	96	0.2	0.2	0.1	0.2	10	10 ≡	10	W 3	WSW 4	NW 5
16	117.3	117.3	118.2	117.6	-2.0	-0.2	1.3	0.1	1.3	-3.3	98	96	83	92	0.1	0.2	1.1	0.5	10 ⸗	10	10	SW 3	WNW 3	NNE 3
17	121.3	125.0	127.8	124.7	-4.6	-4.1	-8.8	-6.6	1.4	-11.1	81	66	77	75	0.8	1.5	0.7	1.0	0	1	0	ENE 4	ENE 5	C 0
18	131.9	132.8	131.1	131.9	-12.1	-6.7	-10.5	-10.0	-6.5	-12.9	82	59	70	70	0.4	1.5	0.8	0.9	0	2 ⊙	0	ESE 1	C 0	SE 2
19	126.8	124.7	123.0	124.8	-12.0	-4.9	-7.0	-7.7	-4.6	-12.5	63	54	47	55	0.9	1.9	1.9	1.6	0	0	0	SE 3	SE 2	SE 2
20	119.6	117.8	115.1	117.5	-8.6	-1.2	-5.8	-5.4	-1.0	-9.2	80	74	77	77	0.6	1.4	0.9	1.0	0	0 ⊙	0	SE 5	ESE 2	ESE 5
21	112.5	111.9	110.5	111.6	-9.2	-5.8	-7.0	-6.8	-3.3	-9.9	82	71	74	76	0.5	1.3	0.9	0.9	0	2	2	ESE 3	ESE 3	SE 3
22	107.0	105.0	103.5	105.2	-11.7	-4.1	-4.6	-6.2	-3.8	-12.2	82	70	81	78	0.4	1.3	0.8	0.8	2	2 ⊙	10 *	SE 1	SE 1	C 0
23	102.6	103.9	106.8	104.4	-9.0	-4.6	-9.6	-8.2	-4.4	-11.3	76	72	78	75	0.7	1.2	0.6	0.8	8	0	0	ENE 6	E 7	C 0
24	106.9	105.1	103.6	105.2	-9.8	-6.2	-10.0	-9.0	-5.2	-14.7	81	71	78	77	0.5	1.1	0.6	0.7	9	6 ⊙	7	C 0	C 0	C 0
25	103.4	104.5	108.2	105.4	-11.3	-7.3	-12.5	-10.9	-6.0	-14.0	72	68	73	71	0.7	1.1	0.6	0.8	0	3	0	C 0	E 5	ENE 3
26	113.5	117.1	120.0	116.9	-16.1	-9.1	-13.6	-13.1	-8.4	-16.5	81	64	80	75	0.3	1.1	0.4	0.6	0	0 ⊙	0	E 3	E 4	C 0
27	122.7	121.6	118.6	121.0	-15.4	-6.8	-12.3	-11.7	-5.9	-16.2	82	48	66	65	0.3	1.9	0.8	1.0	0	6 ⊙	0	SE 3	S 1	SE 2
28	114.5	111.9	105.7	110.7	-14.7	-1.6	-6.5	-7.3	-1.1	-16.0	74	67	81	74	0.5	1.8	0.7	1.0	1	9	6	C 0	S 4	SE 4
29	103.3	105.5	104.4	104.4	-3.8	3.6	1.5	0.7	4.4	-8.7	76	70	85	77	1.1	2.4	1.0	1.5	4	1 ⊙	8	SSW 8	SSW 6	SSW 8
30	95.0	91.1	92.6	92.9	3.0	3.0	4.9	4.0	5.4	1.4	81	90	89	87	1.5	0.8	1.0	1.1	10	10 •	9	SSW 8	SSW 9	WSW 10
31	91.0	87.7	91.9	90.2	3.4	3.7	3.6	3.6	5.0	2.1	95	97	95	96	0.4	0.3	0.4	0.4	9	10 ≡	10 •	SSW 4	C 0	WSW 5
M	107.7	107.5	107.8	107.7	-4.4	-0.8	-2.9	-2.8	0.2	-5.8	86	78	84	83	0.5	1.2	0.7	0.8	6.0	6.1	6.4	3.1	3.5	3.5

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1	89.5	85.3	85.8	86.9	1.0	4.7	2.5	2.7	5.7	0.7	94	81	93	89	0.4	1.6	0.5	0.8	6	9	10	SE 3	SE 3	WSW 2
2	84.2	82.7	80.6	82.5	1.8	4.4	-0.1	1.5	5.2	-0.1	85	77	88	83	1.1	1.9	0.8	1.3	9	5	7	SSW 5	SSW 7	SSE 2
3	82.5	85.1	90.7	86.1	0.6	1.1	0.2	0.5	1.4	-1.0	94	90	82	89	0.4	0.6	1.1	0.7	10 *	10 *	8	W 4	W 5	NW 7
4	95.8	94.8	90.4	93.7	-0.3	1.3	0.2	0.4	1.4	-0.5	84	76	92	84	1.0	1.6	0.5	1.0	8	9	10	WSW 7	SW 7	ESE 3
5	98.7	105.0	109.2	104.3	-0.3	0.9	-1.1	-0.4	1.8	-3.0	94	73	85	84	0.4	1.7	0.9	1.0	10 *	3 ⊙	10	NNE 6	NW 7	WSW 2
6	107.5	104.2	97.4	103.0	-2.9	1.0	1.7	0.4	1.8	-4.0	88	77	81	82	0.5	1.5	1.3	1.1	8	10	10	SSE 3	SSE 6	SSE 6
7	95.3	95.6	95.2	95.4	1.9	5.6	3.1	3.4	6.2	1.0	94	80	85	86	0.4	1.8	1.3	1.2	10	2 ⊙	4	SSW 5	S 8	SSW 7
8	100.2	103.4	108.0	103.9	2.8	4.4	0.9	2.2	4.5	0.9	93	85	94	91	0.6	1.3	0.4	0.8	9 •	10	0	W 7	W 8	SW 3
9	104.2	98.3	96.7	99.7	0.6	1.6	5.5	3.3	5.6	-1.3	94	96	95	95	0.4	0.3	0.4	0.4	10 •	10 •	10	SSE 4	SSE 5	W 5
10	106.2	113.7	115.8	111.9	2.8	2.6	1.8	2.2	5.6	1.5	91	86	87	88	0.7	1.1	0.9	0.9	10 •	10	10	NW 9	NW 6	SW 4
11	106.9	101.6	99.1	102.5	2.3	6.0	5.4	4.8	8.1	1.0	93	77	94	88	0.5	2.2	0.6	1.1	10 •	10	10	SSW 5	SSW 7	WSW 5
12	94.8	99.3	108.2	100.8	3.3	4.5	3.2	3.6	5.5	3.0	97	97	93	96	0.2	0.3	0.5	0.3	10	10 •	9	SSE 1	C 0	NW 4
13	111.1	112.5	115.4	113.0	1.6	5.6	1.5	2.6	6.8	1.0	96	86	92	91	0.3	1.3	0.5	0.7	9	6	6	SW 3	WNW 4	E 2
14	117.0	117.2	116.6	116.9	0.2	2.0	4.0	2.6	4.2	-0.8	96	98	97	97	0.3	0.2	0.2	0.2	10 ≡	10 ≡	10	SE 2	SSE 2	SSE 1
15	116.7	117.6	117.5	117.3	0.6	7.5	6.4	5.2	10.3	0.3	98	84	87	90	0.1	1.7	1.3	1.0	10 ≡	0 ⊙	0	SSW 2	SSW 2	SW 3
16	120.3	123.4	125.9	123.2	5.2	5.4	4.0	4.6	6.5	3.1	95	89	95	93	0.4	1.0	0.4	0.6	10 ⸗	10	10 ⸗	W 5	NW 3	NW 4
17	125.8	126.3	124.6	125.6	4.7	5.1	0.8	2.8	6.0	0.8	94	84	94	91	0.5	1.4	0.4	0.8	10	10	0	WSW 3	WNW 2	C 0
18	122.9	121.8	118.9	121.2	-2.6	9.0	3.1	3.2	12.6	-2.6	98	70	91	86	0.1	3.5	0.6	1.4	0 ≡	0 ⊙	0	C 0	SSW 2	C 0
19	118.1	119.7	121.2	119.7	2.3	3.2	4.1	3.4	5.3	0.7	95	90	95	93	0.4	0.8	0.4	0.5	10 ≡	10	10 ⸗	SW 3	WNW 6	W 6
20	122.6	124.7	125.6	124.3	3.8	5.1	4.4	4.4	5.8	3.2	93	87	82	87	0.5	1.1	1.5	1.0	10 ⸗	10	10	NNW 3	NW 3	WSW 1
21	124.5	124.4	123.6	124.2	2.7	6.2	1.7	3.1	7.7	1.7	89	69	90	83	0.8	3.0	0.6	1.5	9	10	0	SW 1	S 3	ENE 1
22	124.2	124.5	124.1	124.3	-1.5	7.5	0.6	1.8	8.2	-1.9	96	56	96	83	0.3	4.6	0.3	1.7	0 ⸗	2 ⊙	10 ≡	E 1	ESE 5	ESE 5
23	123.2	122.5	120.7	122.1	-0.6	1.2	1.4	0.8	2.1	-0.8	100	96	92	96	0.0	0.3	0.6	0.3	10 ≡	10	10	E 3	E 2	ESE 3
24	119.2	119.1	118.9	119.1	1.6	2.5	1.9	2.0	4.0	1.1	89	86	91	89	0.8	1.0	0.6	0.8	10	9	0	ESE 3	SSE 4	ESE 2
25	120.0	121.7	120.8	120.8	-0.8	1.9	0.1	0.3	3.0	-1.0	95	89	88	91	0.3	0.8	0.8	0.6	5	9	9	ESE 3	ESE 6	ESE 6
26	121.7	121.8	120.8	121.4	-1.2	6.3	3.3	2.9	8.5	-1.5	94	65	85	81	0.4	3.3	1.2	1.6	10	0 ⊙	0	S 4	SSE 3	S 2
27	117.9	115.9	112.1	115.3	0.6	8.7	8.0	6.3	10.3	0.0	92	72	80	81	0.5	3.1	2.1	1.9	7	10	10	S 3	S 7	SSW 5
28	100.7	95.8	102.1	99.5	7.8	9.6	3.4	6.0	11.1	3.0	90	88	86	88	1.1	1.5	1.1	1.2	9	10 •	10	S 8	S 7	W 13
29																								
30																								
31																								
M	109.7	109.9	110.2	109.9	1.4	4.5	2.6	2.8	5.8	0.2	93	82	90	88	0.5	1.6	0.8	1.0	8.2	7.6	6.9	3.8	4.6	3.7

Poznań-Ławica

$H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_n = 13\,m$

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	0.4	1	-	✳°00–05 10⁰³ 12⁰⁵ 23¹⁵–24. = 00⁰⁰–24
2	5	0.2	1	-	✳°00⁰⁰ 11⁵ 11¹⁵–13⁴⁰. = 00⁰⁰–24. ψ 19⁴⁰–23⁴⁰
3	6	4.8	pż.	-	●9⁰⁵–10³⁰ 13²⁷–⁴⁰ 14¹⁰–16²⁵ ✳°21⁴⁰–24. = 00⁰⁰–24. ψ 1³⁰–6⁵⁰. ⌒ 8³⁰–³⁵
4	5	0.7	.	-	✳°00⁰⁰–³⁰ ●° 4¹⁰ 8⁵⁰–9²⁵ 11⁰⁵–12¹⁰ 13¹⁵–15⁰⁵. = 00⁰⁰–24. ⌴ °22⁰⁰–24
5	6	0.0	.	-	●°10¹⁵–⁴⁵ ✳°–20²⁰ = 00⁰⁰–24. ⌴ °0-1 00⁰⁰–10⁰⁰ ⊖ 4¹⁰–7³⁰
6	6	.	.	-	= 00⁰⁰–11³⁵ ∞–19⁴⁰ = –24. ⌴ ° na–10⁰⁰ 23⁰⁰–24
7	6	0.6	.	-	●°15³⁵ 21²⁵ °22³⁰–24. = 00⁰⁰–12³⁰ ∞–15³⁰ = –23⁴⁰ ≡0-1 –24. ⌴ °0⁰⁰–11⁰⁰. ⊖ 5⁰⁵–6³⁵
8	5	1.4	.	-	●°00⁰⁰–2⁰⁰ ●°3³⁵ 4¹⁰ ✳°–4³⁰ ✳°5³⁰–⁴⁰ ●°10⁴⁰–11²⁵ ●°✳°17⁴⁵–22³⁰ 23²⁵. ≡¹ 0⁰⁰–1⁴⁰ = –5¹⁵ ≡¹–6¹⁵ = –24
9	6	0.7	.	-	●°6³³–7²⁵. 19⁴⁰–24. = 00⁰⁰–24
10	6	.	.	-	●°00⁰⁰–⁴⁰ ●°–1³⁰. = 00⁰⁰–13⁴⁰ ∞–15³⁰ = –24. ⌴ °18⁰⁰–24
11	5	2.6	.	-	✳°0-1 10⁰⁸–13³⁰ ●°✳°–16²⁵ ✳°–20²⁵. = 00⁰⁰–21³⁰. ⌴ ° 0⁰⁰–10⁰⁰
12	7	0.0	1	-	✳°4²⁵ 7²⁰ 12⁰⁵–13²⁵
13	6	0.9	1	-	●°10³⁰–20²⁵. 20²⁸–21⁵⁰ ◎ –24. = 7²⁵–13⁴⁰ ∞–15³⁰ = –24. ≈ 21⁵⁰–24
14	4	9.8	1	-	◎ 00⁰⁰–1⁴⁵ ●°4³⁵–7³⁵ ●°–8⁴⁰ ●°9³⁵ ✳°–12²⁰ ●°–12⁴⁰ ●°–16²⁵. = 00⁰⁰–15⁴⁰ ≡0-1 –22¹⁵ = –24. ≈ 00⁰⁰–8²⁰
15	3	0.0	2	-	●°22¹⁵–24. = 00⁰⁰–9¹⁵ ≡°–13¹⁰ = –22¹⁰ ≡°–24
16	5	0.0	2	-	●°00⁰⁰–1³⁵ ◎ –3³⁰ ●°–4³⁵. 5⁴⁵–7²⁵. 15⁰⁰–17³⁵. ≡° 0⁰⁰–0⁵ = –23³⁰
17	7	.	1	-	
18	6	.	1	-	= 7²⁵–9⁴⁰ ∞–24
19	6	.	1	-	∞ 00⁰⁰–24
20	6	.	1	-	∞ 00⁰⁰–5⁴⁰ = –10³⁰ ∞–14³⁰ = –24
21	6	.	1	-	= 00⁰⁰–11³⁰ ∞–21²⁵ = –24
22	4	0.3	1	-	✳°20²⁵–24. = 00⁰⁰–10⁴⁰ ∞–16⁴⁵ = –24
23	6	0.0	2	-	✳°00⁰⁰–3⁴⁰ 10¹⁵–11²⁵. = 00⁰⁰–12³⁰ ∞–19⁴⁰ = –24
24	5	0.1	2	-	✳°10¹⁰ 12⁰⁵. 21²⁵ 24. = 00⁰⁰–12⁰⁰ ∞–16³⁰ = –24
25	7	.	3	-	✳°00⁰⁰ 2⁴⁰. = 00⁰⁰–5⁴⁰ ∞–12¹⁵. 16⁴⁵–22³⁰ = –24
26	6	.	3	-	= 4⁴⁵–8⁴⁰ ∞–20⁴⁵ = –21⁴⁰ ∞–23²⁰ = 23⁴⁰–24
27	6	.	2	-	= 00⁰⁰–8²⁵ ∞–21⁴⁰ = –24
28	6	.	2	-	= 00⁰⁰–10¹⁰ ∞–19²⁵ = –23²⁰ ∞–24
29	6	0.2	2	-	∞ 00⁰⁰–4⁴⁰ = –11³⁰ ∞–15³⁰ = –24. ψ 15⁴⁰–18¹⁵. 19⁵⁰–24
30	6	2.8	1	-	●°3¹⁰–²⁵ 4¹⁵–6²⁵ 8¹⁵ 10²⁰–17³⁰. = 00⁰⁰ 24. ⩓ 19³⁰–21¹⁰
31	2	6.5	pż.	-	●°8⁰⁵–17¹⁰. 18⁴⁵–19⁵⁰ 20⁴⁰ 21¹⁰–22⁴⁵. = 00⁰⁰–11¹⁰ ≡0-1 –15³⁵ = –24
Σ	–	51.0	–	-	UWAGI. Kierunki i prędkości wiatru w ciągu całego roku – wg anemometru.

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1	6	2.3	.	-	●°14³⁵–20¹⁰. = 00⁰⁰–24
2	7	0.0	.	-	= 00⁰⁰–9¹⁵. 16³⁰–24. ⌴ °21⁰⁰–24. ⊖ 21³⁰–23¹⁵
3	5	0.3	.	-	✳°6⁴⁰ 24. = 00⁰⁰–20⁴⁰ 21⁴⁰–24. ⌴ °00⁰⁰–6⁴⁰
4	7	0.6	pż.	-	✳°00⁰⁰ 1⁴⁰. 14³⁰ 15³⁰. 15⁵⁵–17³⁵. 18²⁵–20¹⁰. = na a.p
5	7	.	1	-	✳°1¹⁰ 2³⁵. 4⁴⁰–5⁴⁵. 6²⁵–7¹⁰. = 00⁰⁰–10⁴⁰ 20³⁰–24
6	6	3.4	.	-	✳°13⁴⁵ 14²⁵. = 00⁰⁰–9³⁰ 12¹⁰–14³⁰ ∞–15³⁰ = –24. ⌴ 00⁰⁰–9⁰⁰
7	6	1.4	.	-	●°0²⁵–4¹⁰. 4³⁵ 6¹⁵. 16¹⁵–²⁵. = 00⁰⁰–22¹⁰
8	7	1.5	.	-	●°0⁴⁰ 1³⁵ ●●1-0 4²⁵ ●°8¹⁵ ▽°14¹⁵–⁴⁰ △°–15⁰⁵ ●°–15⁴⁵. = 1³⁰–8³⁰ ⩓ 3³⁰–4³⁰
9	5	16.8	.	-	●°6¹⁵. 7³⁵ ✳°–8¹⁵ ●°–20¹⁵ 22⁴⁰ 24. = 5¹⁰–15⁵⁰ = ⁰-1 –18¹⁰ = –24. ⌴ °1⁰⁰–7⁰⁰
10	6	1.3	.	-	●°0⁰⁰–3²². 5¹⁵–8⁴⁰ ●°13²⁵ 14¹⁰ ●°23²⁵ 24. = 00⁰⁰–24
11	6	3.9	.	-	●°0⁰⁰–²² 0²⁵–1⁴⁸ 5³⁰ 10³⁵ 14⁰⁵–15³⁰ ●●°–18⁴⁰ ●°19²⁵ 20²⁰. = 00⁰⁰–24
12	4	3.4	.	-	●°3⁴⁵–4⁴⁰ 8²⁸ 9³⁰ ●°9³⁵ 10⁴⁰ ●°–17³⁵ = 00⁰⁰ 24
13	6	.	.	-	●●°3²²–4¹⁵. = 00⁰⁰–9⁰⁰ ≡0-1 10¹⁴ = –24
14	3	.	.	-	= 00⁰⁰–6⁵⁰ ≡2-0 14⁰⁵ = –24. ⌴ ° 0⁰⁰–10⁰⁰
15	5	0.0	.	-	= 00⁰⁰–3¹⁵ ≡0-2 11¹⁵ = –14³⁰ ∞–15⁴⁰ = –24. ⌴ °4⁰⁰–9⁰⁰
16	6	0.0	.	-	●°6⁴⁵–8²⁰. 17⁴⁰–24. = 00⁰⁰–7²⁵ ≡°–8³⁵ = –24
17	6	.	.	-	●°00⁰⁰–3³⁵ = 00⁰⁰–13³⁵ ∞–14⁴⁰ = –17⁴⁰ = –19⁰⁵ = –19³⁰ = –21³⁰ ≡0-2 –24. ⌴ °21⁰⁰–24
18	5	.	.	-	≡² 0⁰⁰–2²⁵ = –2⁴⁰ ≡2-1 10¹⁵ = –12³⁰ ∞–17⁴⁰ = –24. ⌴ 0-1 0⁰⁰ 9⁰⁰ ⌴ °23⁰⁰–24
19	6	1.0	.	-	●°8⁴⁰–10⁴⁰. 13¹⁵–⁴⁰ 15³⁵ 16³⁵ ●°18¹⁵–⁴⁵ ●°19¹⁰–24. = 00⁰⁰–6³⁵ ≡0-1 –10²⁰ = –24. ⌴ °0⁰⁰–4⁰⁰
20	5	0.0	.	-	●°0⁰⁰–7²⁵. = 00⁰⁰–24
21	8	.	.	-	= 00⁰⁰–9³⁰ ∞–10¹⁵ = 17⁴⁰–24
22	6	.	.	-	= 00⁰⁰–4⁴⁰ ≡°–5²⁵ = –6⁴⁵ ≡°–9²⁵ = –10³⁰ ∞–18²⁵ = –19⁰⁵ ≡0-1 –24. ⌴ ° 1⁰⁰–10⁰⁰ V °4⁰⁰–9⁰⁰
23	4	0.0	.	-	●°22⁴⁰–24. ≡1-0 00⁰⁰–11⁴⁰ = –24
24	5	.	.	-	●°0⁰⁰–4²⁵. = 00⁰⁰–24. ⌴ ¹ 20⁰⁰–24
25	5	.	.	-	= 00⁰⁰–8⁰⁵ ≡0-1 –9²⁰ = –24. ⌴ ¹-² 0⁰⁰–10⁰⁰
26	6	.	.	-	= 00⁰⁰–10¹⁵ ∞–17³⁰ = –24. ⌴ ° 0⁰⁰–9⁰⁰
27	4	0.9	.	-	●°15¹⁰ 17⁴⁰–23⁴⁰–24. = 00⁰⁰–12³⁰ ∞–15³⁰ = –24. ⌴ ° 2[illegible]–8⁰⁰
28	6	4.2	.	-	●°0⁰⁰–³⁰ ●°–10⁵ ●°2³⁵. 10³⁵ 22²⁵. = 00⁰⁰–16³⁰ ∞–17²⁵ = –21[illegible]. ⩓ 16⁴⁰–23³⁰
29					
30					
31					
Σ	–	41.0	–	-	UWAGI.

Poznań – Ławica

$\varphi = 52°25'$ $\lambda = 16°50'$

Marzec – Mars 1961

Dnia	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	104.4	108.4	113.8	108.9	3.4	4.5	4.0	4.0	5.8	3.0	93	84	85	87	0.5	1.3	1.3	1.0	10 •	10 •	10	WSW 6	WNW 7	W 4
2	115.6	116.5	114.7	115.6	2.2	3.7	3.0	3.0	4.5	0.1	91	77	86	85	0.7	1.9	1.1	1.2	10	10	10	W 4	W 6	SSW 2
3	115.9	118.9	121.5	118.8	2.7	6.3	5.8	5.2	6.8	2.6	96	91	97	95	0.2	0.8	0.3	0.4	10	10	10	SSW 2	W 2	WNW 2
4	124.0	125.8	124.0	124.6	4.4	4.6	3.8	4.2	8.8	3.8	90	82	92	88	0.9	1.5	0.7	1.0	10	9 ⊙	1	WNW 3	WNW 4	SSW 5
5	122.3	124.2	124.9	123.8	4.0	6.8	4.5	5.0	8.3	3.5	88	81	90	86	0.9	1.9	0.8	1.2	10	10	8	WSW 5	W 8	WSW 4
6	125.0	124.4	121.9	123.8	2.8	5.7	3.2	3.7	7.2	0.7	96	83	95	91	0.3	1.6	0.5	0.8	10	9	0	W 6	W 6	W 2
7	117.9	117.3	119.8	118.3	2.0	12.1	4.9	6.0	13.2	0.1	96	50	87	78	0.3	7.1	1.1	2.8	3 ≡	4 ⊙	0	WSW 3	W 7	WNW 4
8	122.9	123.2	123.0	123.0	2.2	10.4	5.6	6.0	12.7	1.7	98	64	80	81	0.2	4.5	1.8	2.2	10 =	1	0	WNW 4	WNW 8	W 5
9	121.6	120.6	119.3	120.5	3.6	13.6	7.9	8.2	15.0	2.9	93	47	74	71	0.5	8.2	2.8	3.8	4 ⊙	8	0	WSW 6	WNW11	W 5
10	116.8	114.3	110.6	113.9	0.6	16.3	7.8	8.1	18.6	0.3	94	38	76	69	0.4	11.4	2.5	4.8	1	4	4	SW 1	SW 3	SSW 2
11	110.2	112.0	112.6	111.6	6.6	9.1	8.9	8.4	10.4	4.7	82	74	80	79	1.7	3.1	2.3	2.4	7	10	10	WSW 5	W 9	W 7
12	110.1	104.0	94.4	102.8	7.5	12.5	14.0	12.0	14.5	7.1	79	54	49	61	2.2	6.7	8.2	5.7	10 •	10	10 •	WSW 8	WSW10	WSW 9
13	97.2	100.5	105.4	101.0	6.0	7.9	1.4	4.2	14.2	1.4	69	51	74	65	3.0	5.2	1.8	3.3	8	8	2	WNW12	WNW12	W 4
14	104.1	103.4	104.9	104.1	4.0	8.4	8.9	7.6	9.4	0.9	90	94	90	91	0.8	0.6	1.1	0.8	10 •	10 •	10 9	WSW 2	WNW 6	W 8
15	105.3	108.1	111.6	108.3	9.2	12.2	7.8	9.2	13.8	7.5	84	51	76	70	1.8	7.0	2.5	3.8	9	5 ⊙	2	W 9	WNW12	W 5
16	107.8	107.7	111.7	109.1	8.8	11.5	7.4	8.8	12.9	6.2	78	62	72	71	2.4	5.2	2.9	3.5	10	8	2	W 12	W 14	WNW 6
17	113.4	110.8	105.6	109.3	3.1	14.0	8.1	8.3	16.4	2.9	93	54	82	76	0.5	7.4	2.0	3.3	6	2 ⊙	0	SW 4	W 8	SSW 3
18	95.3	95.1	92.4	92.9	8.3	13.2	5.6	8.2	13.8	5.5	69	36	59	55	3.5	9.7	3.7	5.6	9	4	0	SW 5	WNW12	WSW 5
19	91.2	95.7	99.7	94.9	3.4	4.4	-1.8	1.0	5.6	-1.9	75	65	65	68	2.0	3.0	1.9	2.3	9	9	2	WSW 7	NW 7	N 3
20	101.8	97.5	87.3	95.5	-5.8	4.9	0.8	0.2	6.0	-6.7	84	34	90	69	0.6	5.7	0.7	2.3	0 ⊙	7	10 ✳	SW 1	SW 7	S 10
21	79.0	80.5	90.6	83.4	0.8	3.9	2.1	2.2	5.4	0.3	94	82	75	84	0.4	1.5	1.8	1.2	9	9 ⚹	9	SW 6	W 9	N 7
22	101.4	103.6	101.1	102.0	-1.4	2.2	0.4	0.4	3.9	-1.9	80	57	96	78	1.1	3.1	0.3	1.5	6	8	10 ✳	NW 6	WSW 8	SSW 6
23	100.6	101.8	104.9	102.4	4.6	7.1	6.8	6.3	8.4	0.4	93	85	80	86	0.6	1.5	2.0	1.4	10 •	9 •	10	WSW 7	WSW12	WSW 8
24	105.1	105.6	106.5	105.7	6.3	9.4	7.8	7.8	11.5	6.1	79	65	82	75	2.0	4.1	2.0	2.7	10	9 •	10	WSW 9	WSW12	WSW 8
25	108.0	109.6	110.0	109.2	6.4	8.9	7.0	7.5	9.5	5.6	84	79	88	84	1.6	2.4	1.2	1.7	10	9	9	WSW 8	WSW12	SW 4
26	107.3	102.5	95.9	101.9	5.8	11.8	7.6	8.2	13.5	5.3	91	50	82	74	0.8	6.9	1.9	3.2	10	10	10	SW 5	WSW10	WSW 8
27	95.3	95.7	95.9	95.6	4.1	3.5	-0.4	1.7	7.7	-0.4	66	66	88	73	2.8	2.6	0.7	2.0	5	6 ⊙	0	WSW12	W 15	WSW 8
28	96.7	97.0	101.0	98.2	0.7	1.6	0.7	0.9	5.3	-0.4	85	93	81	86	1.0	0.6	1.2	0.9	10 ✳	10 ✳	5	W 10	W 7	W 5
29	97.9	97.0	95.6	96.8	2.3	6.0	6.7	5.4	7.0	0.5	91	92	87	90	0.6	0.8	1.3	0.9	10 •	10 •9	10 •	SW 7	W 9	WSW10
30	90.8	92.4	87.3	90.2	6.8	9.2	5.9	7.0	10.0	5.6	80	87	94	87	2.0	1.5	0.6	1.4	10 •	10 •	10	SW 10	WNW 6	NE 5
31	95.9	97.2	95.4	96.2	1.9	6.1	0.4	2.2	7.7	0.4	89	54	96	80	0.8	4.3	0.3	1.8	8 ⊙	10	3	W 6	W 5	W 8
M	106.4	106.7	106.5	106.5	3.8	8.1	5.1	5.5	9.9	2.2	86	67	82	78	1.2	4.0	1.7	2.3	8.2	8.0	5.6	6.2	8.5	5.5

Kwiecień – Avril

1	99.4	92.1	94.0	95.2	-0.8	-0.1	4.0	1.8	4.4	-1.0	95	98	87	93	0.3	0.2	1.1	0.5	10	10 ✳	8	SW 4	SSE 5	WSW 6
2	99.6	100.7	97.6	99.3	0.3	4.2	2.0	2.1	5.2	0.2	82	57	89	76	1.1	3.5	0.8	1.8	9	9	10 •	NW 4	NW 2	ESE 2
3	90.7	95.1	98.3	94.7	1.8	5.7	2.2	3.0	6.7	1.0	96	79	89	88	0.3	2.0	0.8	1.0	10 •	10	2	ESE 2	W 12	SW 1
4	95.6	100.1	103.3	99.0	0.8	8.2	4.8	4.6	9.3	0.3	96	52	79	76	0.3	5.3	1.8	2.5	10	7	10	C 0	W 10	SW 1
5	99.8	97.9	96.3	98.1	5.2	15.0	13.3	11.7	15.8	4.4	95	72	76	81	0.4	4.7	3.7	2.9	10 •	10	2	ESE 4	S 5	SSE 5
6	99.5	101.6	99.8	100.3	9.3	21.3	15.2	15.2	22.8	8.3	87	53	77	72	1.6	11.9	4.1	5.9	8	4 ⊙	0	SSW 4	SW 3	SE 2
7	99.4	99.1	100.3	99.7	12.1	23.7	15.4	16.6	25.1	9.0	79	42	79	67	3.0	17.1	3.7	7.9	4	4	9	S 4	SSW 6	E 1
8	101.8	101.2	106.7	103.2	8.3	9.3	4.2	6.5	15.6	4.1	93	93	80	89	0.8	0.8	1.6	1.1	8	10 =	0	N 3	NNW 5	WNW 5
9	109.0	111.0	111.5	110.5	2.9	8.0	3.1	4.3	9.6	1.8	79	37	54	57	1.6	6.7	3.5	3.9	4 ⊙	6 ⊙	0	WNW 8	NW 7	N 3
10	108.9	106.5	103.3	106.2	1.3	8.0	4.1	4.4	9.0	-1.1	83	45	63	64	1.1	5.9	3.1	3.4	10	6 ⊙	0	E 3	SE 5	E 3
11	100.3	101.1	104.2	101.9	3.4	12.6	7.6	7.8	14.3	0.9	66	37	62	55	2.6	9.2	3.9	5.2	2 ⊙	3 ⊙	2	E 3	E 3	NE 1
12	107.7	108.2	105.3	107.1	3.3	13.1	9.8	9.0	16.0	0.9	65	34	58	52	2.7	9.9	5.0	5.9	3	2 ⊙	0	E 4	ESE 3	SE 2
13	103.2	102.9	102.7	102.9	8.4	19.0	13.4	12.6	20.3	4.3	79	31	79	70	2.2	10.9	2.8	5.3	0 ⊙	3	0	WSW 3	SW 3	C 0
14	101.1	99.3	97.4	99.3	11.2	24.1	15.8	16.7	24.3	8.0	84	30	58	57	2.1	20.9	7.4	10.1	3 ⊙	7 ⊙	2	SE 2	SE 6	C 0
15	100.3	100.9	101.0	100.8	10.6	20.2	15.4	15.4	20.9	7.3	86	50	69	68	1.8	11.9	5.3	6.4	1 ⊙	6	9 • ⛆	NW 4	C 0	ENE 3
16	100.2	99.3	98.9	99.3	9.4	16.1	12.1	12.4	17.7	9.1	93	71	94	86	0.8	5.2	0.8	2.3	10	9	10 •	NNE 3	E 4	SW 3
17	100.3	101.7	102.6	101.6	9.6	11.2	10.4	10.4	12.1	9.3	99	86	93	93	0.2	1.8	0.6	0.9	10 • =	10	10	WNW 2	C 0	C 0
18	102.6	102.6	103.6	102.9	7.4	17.8	10.3	11.6	18.7	6.3	99	50	88	79	0.2	10.1	1.3	3.9	10 =	7 ⊙	2	C 0	NW 2	NNW 3
19	106.8	107.2	107.4	107.1	5.9	13.3	9.2	9.4	15.4	4.4	82	39	62	61	1.7	9.4	4.4	5.2	0 ⊙	1 ⊙	0	NW 3	WNW 5	N 4
20	111.6	112.4	112.0	112.0	4.8	10.3	5.8	6.7	12.4	3.4	68	33	58	53	2.7	8.4	3.9	5.0	6 ⊙	4	0	ENE 6	E 8	E 3
21	111.3	109.3	105.4	108.7	5.8	14.1	10.8	10.4	15.4	2.9	59	33	55	49	3.7	10.8	5.9	6.8	0 ⊙	1 ⊙	0	ESE 6	ESE 5	ESE 4
22	101.6	98.3	95.8	98.6	6.6	20.5	14.5	14.0	21.3	5.0	64	31	54	50	3.5	16.5	7.6	9.2	0	1 ⊙	0	SE 1	SSE 8	SE 4
23	95.2	94.5	94.9	94.9	9.9	18.7	15.2	14.8	20.4	7.6	72	36	43	50	3.4	15.9	10.0	9.1	0 ⊙	4	4	SE 6	SSE 8	ESE 5
24	97.9	98.7	101.7	99.4	9.0	17.1	11.3	12.2	18.5	7.5	57	48	57	54	5.0	10.2	5.8	7.0	0 ⊙	0 ⊙	0	ESE 5	ESE 7	ESE 5
25	103.3	103.8	103.2	103.4	8.8	10.8	11.3	10.6	12.3	8.2	69	62	64	65	3.3	5.0	4.9	4.3	9 ⊙	10	10	ENE 6	E 7	E 7
26	100.4	98.3	97.7	98.9	9.8	14.7	12.0	12.1	16.6	6.3	62	51	73	62	4.6	8.2	3.8	5.3	2 ⊙	9	1	E 6	E 8	E 5
27	98.8	98.7	100.7	99.4	9.7	18.7	11.8	13.0	20.2	8.3	83	54	80	72	2.0	9.9	2.8	4.9	10 • ⛆	6	9 •	C 0	SSE 2	SSW 1
28	100.1	100.1	99.3	99.8	10.8	12.2	11.3	11.4	13.1	9.3	93	93	88	92	0.7	1.0	1.7	1.1	9 •	10 •	9	C 0	C 0	ESE 2
29	100.4	101.8	101.9	101.4	10.3	12.1	8.9	10.0	12.6	8.8	78	74	75	76	2.7	3.7	2.9	3.1	8	10	9	ENE 8	E 8	ENE 6
30	100.1	98.8	98.2	99.0	7.9	17.2	13.3	12.9	18.7	5.3	66	49	72	62	3.6	10.0	4.3	6.0	4 ⊙	0 ⊙	0	E 4	NE 6	ENE 4
31																								
M	101.5	101.5	101.5	101.5	6.8	13.9	9.9	10.1	15.3	5.0	80	55	72	69	2.0	8.2	3.7	4.6	5.7	6.0	3.9	3.6	5.1	3.1

Poznań-Ławica

$H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_w = 13\,m$

Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	1.3	.	-	
2	7	0.8	.	-	
3	5	2.2	.	-	
4	6	.	.	-	
5	6	.	.	-	
6	6	.	.	-	
7	6	.	.	-	
8	6	.	.	-	
9	7	.	.	-	
10	6	.	.	-	
11	5	0.0	.	-	
12	6	3.3	.	-	
13	7	0.2	.	-	
14	5	2.8	.	-	
15	8	.	.	-	
16	7	.	.	-	
17	7	.	.	-	
18	7	.	.	-	
19	8	0.1	.	-	
20	8	4.4	.	-	
21	6	2.4	1	-	
22	7	1.2	.	-	
23	7	0.3	.	-	
24	7	0.0	.	-	
25	7	0.0	.	-	
26	7	1.2	.	-	
27	8	0.4	.	-	
28	5	4.2	pł.	-	
29	6	7.6	.	-	
30	6	10.4	.	-	
31	7	0.8	.	-	
Σ	—	45.6	—	-	UWAGI.

Kwiecień – Avril

1	5	7.6	.	-	
2	8	3.6	.	-	
3	6	4.0	.	-	
4	7	1.7	.	-	
5	6	0.3	.	-	
6	7	.	.	-	
7	7	4.9	.	-	
8	6	4.8	.	-	
9	7	.	.	-	
10	7	.	.	-	
11	7	.	.	-	
12	7	.	.	-	
13	6	.	.	-	
14	7	.	.	-	
15	7	30.0	.	-	
16	6	11.1	.	-	
17	6	0.4	.	-	
18	7	.	.	-	
19	7	.	.	-	
20	8	.	.	-	
21	8	.	.	-	
22	7	.	.	-	
23	7	.	.	-	
24	7	.	.	-	
25	7	.	.	-	
26	7	0.0	.	-	
27	7	10.8	.	-	
28	5	5.6	.	-	
29	7	.	.	-	
30	7	.	.	-	
31					
Σ	—	85.0	—	-	UWAGI.

[27.IV.: = na a.p – 24 ∞ a.p]

Poznań – Ławica φ = 52°25' λ = 16°50' Maj – Mai 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.8	100.7	102.6	101.0	8.3	17.6	11.4	12.2	18.6	6.1	81	56	90	76	2.2	8.8	1.4	4.1	6	8	9	N 2	C 0	ESE 1
2	102.8	102.1	100.6	101.8	8.2	14.6	12.7	12.0	15.9	7.6	96	74	86	85	0.5	4.3	2.1	2.3	10 ▬	9	8	NE 2	SE 2	SE 1
3	98.9	98.6	102.1	99.9	11.4	17.1	11.7	13.0	18.6	8.9	88	65	88	80	1.7	6.9	1.6	3.4	9	9	9	S 3	SSW 5	WSW 3
4	105.1	106.0	105.9	105.7	10.1	18.1	13.4	13.8	19.3	6.5	93	36	71	67	0.8	12.8	4.5	6.0	0 ⊙	5 ⊙	4	SW 1	W 3	SE 1
5	105.3	103.1	102.0	103.5	12.8	20.7	17.0	16.9	20.8	9.1	68	57	76	67	4.7	10.5	4.7	6.6	10 ⊙	10	9	SSE 3	SSE 6	S 5
6	100.9	104.1	105.5	103.5	15.6	15.1	12.4	12.9	17.5	12.4	94	91	88	91	0.9	1.4	1.7	1.3	10 ●	10 ●	3	NNE 7	WNW 4	C 0
7	104.2	101.1	101.1	102.1	12.8	17.0	9.8	12.4	18.4	9.1	92	65	88	82	1.2	6.9	1.4	3.2	8 ⊙	9 ●	0	SSW 3	SW 9	WSW 6
8	102.1	100.4	99.9	100.8	9.5	12.5	8.0	9.5	14.3	7.0	87	62	87	79	1.6	5.5	1.3	2.8	6	7	3	W 6	WSW 10	WSW 7
9	95.5	95.8	95.7	95.0	7.4	9.6	8.3	8.4	11.9	6.7	93	84	93	90	0.8	1.9	0.8	1.2	10 ●	10	2	SW 5	SW 6	WSW 6
10	97.8	100.4	103.8	100.7	8.6	9.8	7.9	8.6	10.3	7.0	89	78	79	82	1.3	2.7	2.2	2.1	10 ●	9	7	WNW 10	NW 8	NNW 5
11	104.9	106.6	110.4	107.3	7.8	10.8	6.6	8.0	12.7	6.6	83	69	81	78	1.8	4.0	1.8	2.5	9	8 ⊙	2	NW 6	NNW 8	NNW 4
12	109.8	106.5	105.8	107.4	5.8	12.1	6.7	7.8	13.0	3.1	83	51	90	75	1.5	6.9	1.0	3.1	9	7 ⊙	3	WNW 1	NW 7	NW 4
13	104.4	101.7	100.7	102.3	5.0	9.7	8.0	7.7	11.5	2.2	98	89	93	93	0.1	1.2	0.7	0.7	10 ≡	10 ●	3	SSW 6	SW 7	SW 3
14	99.5	99.4	99.4	99.4	7.9	11.3	8.1	8.8	11.8	5.4	67	62	85	71	3.5	5.1	1.6	3.4	8	8	9	WSW 8	SW 8	WSW 4
15	101.2	102.6	104.6	102.8	7.8	10.3	6.8	7.9	11.9	6.8	82	77	86	82	2.0	2.8	1.5	2.1	9	9 ●	9	W 7	NNW 8	N 4
16	103.7	101.4	101.5	102.2	6.8	8.4	7.9	7.8	9.4	2.7	88	85	91	88	1.2	1.6	0.9	1.2	10 ●	10 ●	10	W 7	WNW 9	N 7
17	105.2	106.7	108.2	106.7	6.8	10.1	8.0	8.2	13.0	5.5	96	88	82	89	0.5	1.5	1.9	1.3	10 ●	10	3	NW 4	NNW 5	NNW 5
18	109.1	107.0	106.1	107.4	6.2	15.1	10.5	10.6	16.8	4.3	95	44	74	71	0.5	9.6	3.3	4.5	8	9	2	C 0	W 8	NNW 6
19	105.0	103.5	102.0	103.5	10.5	17.0	10.1	11.9	17.6	5.1	77	43	86	69	2.9	11.0	1.8	5.2	4 ⊙	9	9	W 1	W 7	SSW 3
20	100.1	98.7	98.5	99.1	9.3	15.3	11.3	11.8	16.3	6.3	85	52	83	73	1.7	8.4	2.3	4.1	9	8 ⊙	4	SW 3	WSW 5	C 0
21	99.5	100.0	102.3	100.6	12.0	14.8	13.0	13.2	18.4	8.0	76	70	79	75	3.3	5.0	3.1	3.8	6	9	10	E 1	NNE 6	NE 5
22	104.1	103.6	103.0	103.6	6.2	15.6	10.8	10.8	16.8	5.5	88	40	75	68	1.2	10.7	3.3	5.1	9	6 ⊙	5	NNE 7	NE 8	NNW 3
23	103.2	102.5	102.5	102.7	11.4	18.6	12.2	13.6	19.0	8.3	66	43	73	61	4.6	12.3	3.8	6.9	9	8	3	C 0	SW 5	NW 4
24	104.8	106.0	105.5	105.4	10.8	13.1	9.7	10.8	16.2	7.9	73	59	82	71	3.6	6.3	2.2	4.0	9	10	0	W 4	W 8	WNW 1
25	105.6	104.4	103.0	104.3	10.7	17.6	14.2	14.2	19.7	4.9	80	49	74	68	2.6	10.2	4.3	5.7	0 ⊙	9	3	W 2	N 3	NNE 1
26	103.0	101.5	98.1	100.9	12.7	21.8	17.2	17.2	22.4	9.6	80	40	53	58	2.9	15.8	9.2	9.3	2	3 ⊙	6	E 3	SE 3	ESE 5
27	97.1	99.2	100.6	99.0	15.6	16.9	12.3	14.3	17.8	11.4	79	63	71	71	3.7	7.2	4.2	5.0	9 ⊙	9	10	WSW 5	NW 5	N 5
28	100.5	100.7	101.3	100.8	8.4	8.4	7.9	8.2	12.4	7.7	92	90	89	90	0.9	1.0	1.2	1.0	10 ●	10 ●	10	N 4	NW 7	NNW 5
29	97.6	95.8	88.2	93.2	8.0	11.5	14.3	12.0	14.8	7.3	93	84	84	87	0.7	2.2	2.5	1.8	10 ●	10	10	NNE 4	NE 8	NNE 8
30	86.7	90.4	93.2	90.1	13.9	12.1	9.8	11.4	15.1	9.6	97	80	84	87	0.6	2.8	1.9	1.8	10 ≡	10	6	S 2	SSW 8	SSW 3
31	94.8	94.9	94.5	94.7	10.1	14.1	13.4	12.8	16.2	6.0	86	66	75	76	1.8	5.4	3.8	3.7	10	9	9	SE 3	SSE 4	ESE 2
M	101.7	101.3	101.6	101.5	9.6	14.0	10.7	11.2	15.8	6.9	85	65	82	77	1.8	6.2	2.5	3.5	8.0	8.6	5.8	3.9	6.1	3.7

Czerwiec – Juin

1	95.4	94.0	95.0	95.5	14.6	23.2	18.8	18.8	25.3	11.0	74	40	72	62	4.3	16.9	6.1	9.1	0	0 ⊙	2	SE 1	SSW 4	E 2
2	92.5	94.2	95.5	94.0	19.0	24.2	19.3	20.4	25.7	14.2	64	53	72	63	7.9	14.3	6.2	9.5	4 ⊙	6 ⊙	2	SE 3	S 3	C 0
3	97.0	97.2	99.4	97.9	19.1	25.6	17.8	20.1	26.0	13.5	66	52	76	65	7.5	15.6	4.8	9.3	5 ⊙	5	4	NNW 7	WNW 4	N 7
4	100.1	99.9	102.1	100.7	17.8	25.2	18.6	20.0	26.1	15.3	80	53	80	71	4.0	15.2	4.3	7.8	3	6 ⊙	10	NE 8	ENE 5	NE 6
5	104.3	104.7	105.0	104.7	19.9	24.3	18.1	20.1	25.4	14.7	75	53	83	70	5.7	14.4	3.5	7.9	4 ⊙	9 ⊙	8	E 2	E 6	E 3
6	105.0	103.6	101.6	103.4	19.2	24.2	19.4	20.6	25.0	13.9	62	35	70	56	8.5	19.5	6.6	11.5	2 ⊙	3 ⊙	3	E 3	E 5	E 7
7	99.8	98.8	97.2	98.6	18.2	22.2	17.2	18.7	24.4	15.7	81	68	92	80	4.1	8.7	1.6	4.8	9	8 ⊙	10 ☈	ESE 5	SSE 4	E 3
8	97.9	99.0	101.7	99.5	16.8	23.7	16.9	18.6	23.7	14.3	95	64	89	83	1.0	10.6	2.1	4.6	9	8 (☈)	5	SSW 2	WNW 8	N 2
9	102.7	102.7	101.3	102.2	15.0	23.0	19.4	19.2	24.0	11.5	98	45	79	74	0.3	15.5	4.6	6.8	4 ≡	3 ⊙	8	C 0	E 3	SE 2
10	100.8	100.5	103.9	101.7	18.4	26.3	13.9	18.1	27.5	13.7	87	47	97	77	2.7	18.0	0.6	7.1	7	5	10 ● ☈	SE 2	SSE 4	SSE 5
11	103.6	104.1	102.9	103.5	15.8	16.9	15.8	16.1	17.5	13.8	89	85	85	86	1.9	2.9	2.6	2.5	9	10	7	WNW 5	WNW 4	N 1
12	101.3	100.9	100.3	100.8	13.6	17.8	14.0	14.8	20.2	10.6	92	65	91	83	1.3	7.1	1.5	3.3	9	9	3	N 1	W 6	SW 3
13	98.3	95.4	92.1	95.3	13.5	20.4	15.2	16.1	21.7	9.7	85	52	89	75	2.3	11.4	1.9	5.2	4	8 ⊙	9	SW 2	SSW 5	SE 3
14	92.4	95.4	100.6	96.1	14.0	14.0	13.6	13.8	15.4	12.9	92	89	91	91	1.3	1.8	1.5	1.5	9 ●	10 ●	10 ●	WSW 7	WSW 9	W 8
15	103.2	104.5	105.9	104.5	12.0	13.9	12.7	12.8	15.0	11.0	80	69	76	75	2.8	4.9	3.6	3.8	9	10	10	WSW 7	W 9	SW 5
16	107.2	107.1	108.2	107.5	10.7	18.2	12.5	13.5	19.9	8.2	85	48	85	73	2.0	10.8	2.2	5.0	10	7	1	WSW 5	W 7	NNW 1
17	109.1	108.3	107.7	108.4	14.7	23.0	17.4	18.1	23.4	7.7	73	44	77	65	4.5	15.9	4.6	8.3	1	4	10	WSW 3	W 6	SW 3
18	106.2	103.9	103.0	104.4	16.8	26.6	21.3	21.5	28.2	12.4	70	40	66	59	5.7	21.0	8.5	11.7	2 ⊙	1	8	SSW 4	SW 8	SW 3
19	107.4	109.0	111.5	109.3	16.0	19.9	15.2	16.6	21.7	15.2	77	41	63	60	4.2	13.7	6.3	8.1	9	3	6	NW 5	WNW 7	WSW 4
20	116.0	116.2	114.7	115.6	12.8	18.2	14.8	15.2	20.4	8.5	68	34	55	52	4.7	13.8	7.5	8.7	1 ⊙	3 ⊙	0	WNW 6	WNW 6	C 0
21	112.2	110.3	113.6	112.0	14.8	21.1	12.8	15.4	22.2	8.7	61	35	75	57	6.5	16.3	3.8	8.9	8 ⊙	9 ⊙	1	SSE 3	WNW 5	NW 4
22	114.6	109.9	104.3	109.6	14.4	21.3	18.4	18.1	23.0	6.8	68	39	71	59	5.3	15.3	6.1	8.9	1 ⊙	3 ⊙	6	SSE 3	SSE 6	E 2
23	105.6	107.7	107.1	106.8	18.1	21.4	15.9	17.8	22.7	15.6	59	44	73	59	8.6	14.3	4.9	9.3	0	7	2	W 5	W 10	SW 3
24	108.1	108.6	107.3	108.0	16.4	22.9	18.2	18.9	25.2	11.5	73	31	76	60	5.1	19.4	5.1	9.9	9	9	7	WSW 5	W 8	SW 5
25	106.6	104.4	101.5	104.2	19.0	27.4	21.8	22.5	29.6	13.2	69	33	64	55	6.8	24.4	9.3	13.5	2 ⊙	3 ⊙	4	WSW 4	WSW 8	W 1
26	102.7	101.9	99.7	101.4	20.9	27.0	22.0	23.0	29.1	14.2	59	40	64	54	10.0	21.3	9.4	13.6	1 ⊙	6	2	NNE 2	WSW 2	SSE 2
27	96.1	96.4	97.5	96.7	21.4	26.0	20.4	22.0	28.1	17.1	75	57	84	72	6.3	14.3	3.8	8.1	6	9	6	SSE 3	WSW 5	SSW 3
28	107.4	112.3	115.5	111.7	14.2	16.8	14.8	15.2	20.4	13.0	63	46	66	58	6.0	10.3	5.7	7.3	8 ⊙	8 ⊙	4	WNW 10	WNW 10	W 3
29	118.2	117.9	116.9	117.7	14.3	20.0	16.6	16.9	22.3	10.8	75	44	72	63	4.5	15.1	5.3	7.6	3 ⊙	6 ⊙	0	WNW 6	NW 8	C 0
30	117.6	116.2	114.8	116.2	17.6	25.3	20.8	21.1	26.9	10.3	64	37	58	53	7.2	20.2	10.2	12.5	0 ⊙	3 ⊙	0	WSW 1	WNW 5	N 4
31																								
M	104.2	104.2	104.2	104.2	16.3	22.0	17.1	18.1	23.5	12.3	75	49	76	67	4.8	14.0	4.8	7.9	4.9	6.0	5.3	3.9	6.0	3.1

Poznań-Ławica

$H_s = 86\,m$ $H_g = 92{,}1\,m$ $h_w = 13\,m$

Maj - Mai 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	5.5	.	-	▽° 10³⁴–11⁰⁵ ●⁰⁻¹ 16⁴⁰–20¹⁰, ☇ 17⁴⁰–19³⁵ N-SE, = 17¹⁵–24, ⌒ 17³⁰–37
2	6	10.0	.	-	●° 7⁴⁰–8²⁰ ▽° 15³⁴–45, = 0⁰⁰–6⁰⁵ ≡° –7⁴⁵ ∞ – 18⁴⁰ = –24, ⌓° 22⁰⁰–23³⁰
3	7	11.5	.	-	●¹⁻⁰ 10⁴⁰ 16⁰³, ☇¹ 13⁰² 14⁰⁵ W-E, = 10⁰⁰–9³⁰ ∞ – 10²⁰ = 20³⁰–24, ⌓¹ 0⁰⁰–7⁰⁰
4	7	.	.	-	= 0⁰⁰–3¹⁰ = –5³⁰ = –8²⁰ ∞ 19³⁰–21²⁰ = –24, ⌓¹ 22⁰⁰–24
5	7	23.4	.	-	●° 14⁴⁰ 15⁰⁵ ▽⁰⁻¹ 22¹⁵–24, ☇⁰⁻¹ 22³⁸–23⁴⁰ W-N, ∞ na, a = na, np, ⌓¹ 0⁰⁰–8⁰⁰, ⊕ 6⁵⁰–11⁴⁰, 12⁴⁰–13¹²
6	6	4.4	.	-	●¹ 0⁰⁰–10 ●° ●⁰⁻¹ 4³² 13⁴⁰ ☇¹ 5⁰⁴–6¹⁵ W-NE, = 0⁰⁰–14¹⁰ 20⁴⁰–24
7	6	6.6	.	-	▽° 12⁵² 13⁰⁵ 15⁰⁵–23 ▽⁰⁻² 16³³–17⁰⁵ 20⁰²–10 ☇ 16³⁸–17¹⁵ W-E, ≫ 16³⁸⁻⁵⁰, = 0³⁰–10⁴⁰ ∞ – 13³⁰
8	7	4.5	.	-	▽⁰⁻¹ 6¹⁵ 16⁵⁰ ▽° 23⁴⁰–24, ☇¹ 16⁰⁸⁻³⁵ W-E, ≫ 9¹⁰–13⁴⁵ ≫ 16¹⁰⁻²⁰ ≫ – 16³⁵
9	6	5.4	.	-	▽° ●° 0⁰⁰ 17³⁰ ▽° 22⁵⁰–23³⁵ = 5³⁰–24
10	7	1.8	.	-	▽⁰⁻¹ 0⁴⁰ 13⁵⁰ ≫ 5²⁰–7³⁰ 15⁰⁵⁻²⁵ = 0⁰⁰–9³⁰
11	7	1.4	.	-	▽¹⁻⁰ 10⁰⁵–11⁰² ▽° 16⁴⁵⁻⁵⁵ ≫ 16³⁵⁻⁵⁰
12	7	0.0	.	-	▽° 5¹⁵⁻⁴⁰ 10⁵⁰ 11¹⁰ ⌓° 3⁰⁰–5¹⁵ 23⁰⁰–24
13	6	4.5	.	-	●° 11²⁰ 14⁴⁰ 15⁴⁵ 16²⁷ ▽⁰⁻¹ 18¹³ 19⁰⁵, = 3³⁵–6⁴⁵ ≡⁰⁻¹ 8¹⁵ = –24, ≫ 18¹⁰⁻²⁰ ⌓° na
14	7	3.4	.	-	▽° 8²⁸ 15⁰⁷ 18³⁰–40 23⁴⁰–50, = 0⁰⁰–5¹⁰
15	7	1.6	.	-	▽° 7²⁰ 16²⁰
16	7	4.5	.	-	▽° 6⁵⁰ 16⁴⁰ ●° 17³⁵ 19⁰⁰, = 17³⁰–19¹⁵, ≫ 11¹⁰⁻¹⁵, ⌓° 2⁰⁰–7⁰⁰
17	8	1.2	.	-	●° 6⁰² 12⁴⁰ 13³⁰–45 ▽° 16³⁰–40, = 5³⁰–15³⁰
18	8	.	.	-	= 3³⁰–7¹⁰, ⌓° 22⁰⁰–24
19	7	0.0	.	-	▽° 13²⁰–25 ⌓° 0⁰⁰–9⁰⁰
20	7	.	.	-	= 1⁰⁰–8³⁰, 20¹⁰–24, ⌓¹ 22⁰⁰–24
21	6	2.8	.	-	▽° 11⁴⁵–12⁵⁰ ▽¹⁻⁰ 16⁰⁷ 18⁰², ☇° 12⁴⁰⁻⁵⁰, = n–a ∞–p = –24
22	8	.	.	-	= 0⁰⁰–8³⁵, ⌓° 22⁰⁰–24
23	7	.	.	-	= 3⁴⁰–6⁵⁰ ∞ – 7³⁰, ⌓° 0⁰⁰–5⁰⁰, 23⁰⁰–24
24	8	.	.	-	= 4³⁰–6³⁰, 20⁴⁰–24, ⌓° 0⁰⁰–7⁰⁰, 22⁰⁰–24
25	7	.	.	-	= = 0⁰⁰–7³⁵ ∞ – 9⁴⁰, 18³⁰–21¹⁵ = –24, ⌓° 0⁰⁰–8⁰⁰
26	7	.	.	-	= 0⁰⁰–7³⁰ ∞ – 11³⁰, 20²⁰–24, ⌓° 2⁰⁰–8⁰⁰
27	7	1.6	.	-	∞ 0⁰⁰–3³⁰ = – 11⁴⁵ ∞ – 21⁴⁰ = –24
28	6	12.0	.	-	●° 5⁰⁸–8¹⁰ ▽¹⁻⁰ 12¹⁰ ●° 13⁴⁰ 14¹⁵ ▽° 14²⁰–15¹⁵, = 0⁰⁰–3⁴⁵ ∞ – 4¹⁵ = a–p
29	6	6.0	.	-	●° 6⁴⁰–8²⁰ ▽⁰⁻¹ 20⁴⁰–24; ☇ 22⁴⁵–23⁰⁰ SW-W, = 5⁵⁰–24
30	8	3.1	.	-	▽° 0⁰⁰–1²⁸ ●° 5¹⁰ 6¹⁰–8²⁰ ●⁰⁻¹ 9⁴⁵–11¹⁵, = 0⁰⁰–7⁴⁵ ≡⁰⁻¹ 8⁴⁰ = – 11²⁰, 18³⁵–24
31	6	.	.	-	= 0⁰⁰–9³⁰ ∞ a, p, p–24
Σ	–	105.0	–	-	UWAGI:

Czerwiec - Juin

1	7	.	.	-	∞ 0⁰⁰–2⁴⁰ = –6³⁰ ∞ – 12³⁰ = 23³⁰–24, ⌓° 3⁰⁰–9⁰⁰
2	7	.	.	-	= ∞ 0⁰⁰–10⁴⁰ = 23⁵⁰–24, ⌓¹ 0⁰⁰–7⁰⁰, 23⁰⁰–24
3	7	15.7	.	-	▽° 11⁰⁶–30 ●¹⁻⁰ 14²⁹–16¹⁰ ▽° 20⁰⁵–15, (☇) 10⁴⁰⁻⁵², ☇° – 12¹⁰ N-SW (☇) 14²⁰⁻³⁰ ☇¹ – 16¹⁰ (☇) – 16⁰⁵ E-W, = na, np;
4	7	.	.	-	☇ 14⁴⁰ 18³⁵ SE-W, = 0⁰⁰–5¹⁰ 22⁵⁰–24, ⌓¹ 23⁰⁰–24 [3.VI: ⌓ 0⁰⁰–8⁰⁰
5	7	2.6	.	-	▽° 16⁵⁵ 18¹⁰, ☇° 16⁵⁸ 17⁰⁵ SW-SE, 17¹⁵⁻⁵⁰ W-E, = 0⁰⁰–8⁵⁰ ∞ – 9¹⁰, p = –24, ⌓¹ 0⁰⁰–7⁰⁰
6	7	.	.	-	= 0⁰⁰–6⁴⁰ ∞ – a, np, ⌒ 20⁰⁵⁻²⁰
7	6	34.3	.	-	▽⁰⁻² 15²⁸–24, ☇ 17²⁰–18⁴⁰ SE-N, 19⁴³–22²⁰ SE-N, 23⁴⁰⁻⁴⁵ SW-S, ∞ na = –11³⁰ ∞ – 18³⁰ = 22³⁰–24
8	6	0.3	.	-	▽⁰⁻¹ 0⁰⁰–35 ▽° 14³⁵ 16⁴⁰, (☇)° 13⁴⁵–14³⁰ W-NE, = 0⁰⁰–3³⁰ = – 5³⁰ = – 12³⁰ ∞ – 19⁴⁰ = np
9	6	.	.	-	= 0⁰⁰–3¹⁵ = ¹⁻⁰ 8⁰⁵ = – 8⁴⁰ ∞ – 21⁴⁰ = – 24, ⌓¹ 0⁰⁰–10⁰⁰
10	7	38.7	.	-	▽° 16⁰¹⁻¹³ 17²⁰–18⁰² ▽¹⁻² 20³³–24, (☇) 17⁰¹⁻³⁵ ☇° – 18¹⁵ E, N-NW (☇) N 20⁷³⁻³⁰ ☇¹⁻² 23⁴⁰ S-NW; = ∞ 0⁰⁰ 10²⁰ 19¹⁰–24,
11	6	.	.	-	▽° 0⁰⁰–45 ●° 3⁰⁵–30 5¹⁰..30 = 0⁰⁰–24 [10.VI: ⌓⁰⁻¹ 0⁰⁰ 9⁰⁰
12	7	0.2	.	-	▽° 11²⁰–45 19⁵⁰–20⁰⁵, = 0⁰⁰–12³⁰, 22¹⁰–24, ⌓¹ 0⁰⁰–7⁰⁰
13	7	2.7	.	-	●° 17⁴⁵–20⁰⁵ ▽° 22⁵⁰–24 = 0⁰⁰–8⁴⁰ ∞ – 18²⁰ = –24, ⌓¹ 0⁰⁰–10⁰⁰
14	6	6.9	.	-	▽° 0⁰⁰–35 ●° 5⁴⁵–6¹⁰ ▽⁰⁻³ 7¹⁵–24, = 0⁰⁰–8⁴⁰, 17³⁰–24
15	7	.	.	-	▽° 0⁰⁰–15 = 0⁰⁰–4³⁰
16	7	.	.	-	= 3³⁰–9³⁰, 22¹⁰–24, ⌓° 1⁰⁰–8⁰⁰, 22⁰⁰–24
17	6	.	.	-	= 0⁰⁰–7⁴⁵ ∞ – 21⁵⁰ = – 24, ⌓⁰⁻¹ 0⁰⁰–9⁰⁰ ⌓° 22⁰⁰–24
18	6	0.1	.	-	= 0⁰⁰–7²⁵ ∞ – 14¹⁵, 18¹⁰–24, ≫ 14¹⁰⁻⁴⁰, ⌓⁰⁻¹ 0⁰⁰–9⁰⁰
19	7	.	.	-	▽° 2⁰⁵–3¹⁰, ∞ 0⁰⁰⁻⁴⁰ = – 3²⁰
20	8	.	.	-	
21	7	.	.	-	= 2³⁰–6³⁰ ∞ – 7⁴⁰, 17²⁰–22³⁰ = – 24, ⌓° 0⁰⁰–7⁰⁰ 23⁰⁰–24
22	8	0.0	.	-	▽° 23¹⁵–20 (☇)° 23²⁰–24 SW-S, = = 0⁰⁰–7⁴⁰ ∞ – 8³⁰, 20⁴⁰–22⁴⁰ = – 24, ⌓⁰⁻¹ 0⁰⁰–10²⁰
23	7	.	.	-	(☇)° 0⁰⁰⁻⁴⁰ = 0⁰⁰–7³⁰ ∞ – 13³⁰, ≫ 11³⁰–15⁴⁵
24	6	.	.	-	= ∞ 4³⁰–11²⁰ 20³⁰–24, ≫ 10³⁰–12⁴⁰, ⌓° 2⁰⁰–7⁰⁰
25	7	.	.	-	= ∞ 0⁰⁰–24, ⌓¹ 0⁰⁰–7⁰⁰ ⌓° 23⁰⁰–24
26	7	.	.	-	= 0⁰⁰–7⁵⁰ ∞ – 8³⁰ 20⁴⁰–24, = 0⁰⁰–7⁵⁰, ⌓° 0⁰⁰–7⁰⁰
27	6	0.0	.	-	▽° 22⁴⁰–23¹⁵ ∞ 0⁰⁰–1⁴⁵ = – 8³⁰ ∞ – 15¹⁵, ≫ 20⁰⁵–22⁴⁰
28	8	0.0	.	-	▽° 13³⁰⁻³⁵, ≫ 0³⁵–17⁰⁵
29	8	.	.	-	∞ 20²⁰–22⁵⁰ = – 24
30	7	.	.	-	= 0⁰⁰–7⁴⁰ ∞ – 8²⁰, 21⁴⁰–24, ⌓⁰⁻¹ 0⁰⁰–10⁰⁰
31					
Σ	–	101.5	–	-	UWAGI:

Poznań – Ławica φ = 52°25' λ = 16°50' Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			POGODA N.w			KIERUNEK I PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	115.3	114.4	115.0	114.2	19.6	26.9	22.4	22.8	28.7	12.3	62	33	60	52	8.6	25.7	10.8	14.4	0 ⊙		2 ⊙	1			C 0	N 3	ENE 1
2	112.6	111.8	109.8	111.4	20.4	29.4	25.9	24.4	31.9	12.7	68	32	63	54	7.7	28.0	11.1	15.6	0 ⊙		0 ⊙	0			C 0	NW 3	C 0
3	108.1	105.3	104.1	105.8	21.6	32.9	22.2	24.7	34.0	16.5	66	26	73	56	8.9	36.0	7.4	17.4	3 ⊙		2 ⊙	9			SSW 2	S 7	NW 7
4	102.7	99.7	97.0	99.8	17.6	18.0	14.6	16.2	24.0	14.6	80	82	92	85	4.0	3.6	1.3	3.0	8		10 •	9			S 2	NW 4	NW 5
5	101.5	102.3	102.9	102.2	12.4	16.3	10.5	12.4	17.7	10.3	72	51	88	70	4.0	9.1	1.5	4.9	8		8	4			W 8	WSW 9	SSW 4
6	103.8	104.5	109.2	105.8	10.7	13.9	12.2	12.2	17.1	6.9	81	87	95	87	2.5	2.2	1.0	1.9	9		9	9 •			SW 8	WSW 9	WSW 5
7	110.1	110.8	110.6	110.5	11.7	14.0	13.9	13.4	17.0	9.6	87	67	74	76	1.8	5.3	4.1	3.7	9		9	8			W 7	SW 5	WSW 2
8	109.4	107.7	105.7	106.9	13.0	20.7	15.8	16.5	22.3	9.3	75	51	76	67	3.8	12.1	4.3	6.7	9		9	4			SSW 3	SW 5	SSE 4
9	98.6	98.3	101.0	99.3	13.0	15.6	13.0	13.6	17.9	11.9	95	89	95	93	0.7	1.9	0.7	1.1	10 •		10 •	4			S 3	W 8	SW 2
10	100.8	101.0	103.3	101.7	12.7	15.6	12.7	13.4	17.3	11.0	87	60	78	75	1.9	7.1	3.3	4.1	4		8	7 •			W 5	W 9	W 4
11	103.0	103.3	101.5	102.6	12.9	19.6	16.8	16.5	21.8	8.9	85	54	86	75	2.3	10.5	2.7	5.2	7		9	9			WSW 4	SW 5	SSE 2
12	99.1	98.4	95.6	97.7	16.7	24.1	21.3	20.8	27.2	14.8	94	56	73	74	1.2	13.2	6.9	7.1	7 ⊙		5	3			S 2	WNW 2	E 4
13	89.8	86.2	87.6	87.9	19.6	27.7	16.2	19.9	28.0	16.2	83	53	96	77	3.9	17.6	0.8	7.4	8		6 •	8 •			SE 3	SSE 6	SW 4
14	92.0	95.4	96.3	94.6	13.6	16.5	16.2	15.6	18.9	13.4	73	57	78	69	4.2	8.0	4.0	5.4	10		10	10			WSW 9	WSW 8	SE 2
15	98.2	99.9	100.3	99.5	13.8	21.2	18.2	17.8	23.4	13.0	98	50	68	72	0.4	12.5	6.8	6.6	9 •		6	5			SSW 3	WSW 5	E 3
16	99.3	98.9	99.0	99.1	14.6	20.0	15.3	16.3	21.7	15.1	97	58	85	80	0.5	9.8	2.6	4.3	10 •		9	5			S 3	WNW 3	SW 1
17	96.9	96.6	96.8	96.8	14.6	16.5	12.7	14.1	18.3	9.4	89	78	98	88	1.8	4.3	0.4	2.2	3 ⊙		9	10 •			S 1	SW 1	SW 2
18	96.9	97.0	97.0	97.0	15.2	16.1	15.2	15.9	19.7	12.5	92	79	95	89	1.3	5.8	0.7	1.9	10		9	8			W 6	WSW 7	C 0
19	97.5	97.7	98.2	97.8	13.7	17.2	14.0	14.7	19.0	11.2	94	75	93	87	0.9	4.9	1.1	2.3	8		8	7			WSW 1	SW 4	SSE 2
20	99.2	99.5	100.7	99.8	15.4	19.3	16.2	16.3	20.2	10.3	94	71	75	80	0.9	6.4	4.5	3.9	9		9	10			SSW 2	NW 5	SW 3
21	100.2	100.7	100.7	100.5	15.1	16.5	14.2	15.0	17.6	14.0	92	84	95	90	1.4	5.1	0.7	1.7	10		9	7			WSW 7	WSW 8	WSW 5
22	101.2	101.5	102.4	101.7	14.9	18.0	14.6	15.5	19.0	13.8	93	71	85	83	1.1	5.9	2.5	3.2	10 •,		10	10			WSW 7	W 9	SW 4
23	103.5	105.1	106.9	105.2	13.7	14.6	13.2	13.7	17.3	12.5	87	86	88	87	2.0	2.4	1.8	2.1	10 •		10 •	6			WSW 5	WNW 5	SW 4
24	109.3	111.4	112.9	111.2	12.6	15.0	13.9	13.8	16.4	11.6	89	69	82	80	1.6	5.2	2.9	3.2	9		10	9			W 5	W 7	WSW 3
25	114.3	114.7	112.7	113.9	12.9	16.4	13.2	13.9	17.6	12.1	89	72	86	82	1.6	5.2	2.1	3.0	9		10	8			WSW 5	WSW 6	SW 4
26	108.9	105.3	100.3	104.9	15.0	22.0	18.4	18.4	23.6	11.7	85	58	72	71	2.9	11.0	5.9	6.6	9		10	9			SW 6	WSW 8	S 4
27	97.8	95.8	96.9	96.8	18.0	23.5	17.6	19.2	24.0	14.5	80	59	82	74	4.0	11.8	3.6	6.5	7		8	9			SW 4	WSW 9	SW 3
28	93.5	92.1	95.1	93.6	14.4	18.3	13.8	15.1	19.3	13.8	98	79	98	92	0.4	4.4	0.4	1.7	10 •		9	10 •			S 4	SW 7	SW 3
29	99.5	102.4	105.1	102.3	12.3	17.9	13.5	14.3	18.0	11.5	92	62	85	80	1.2	7.8	2.3	3.8	9		9	9			W 7	WSW 8	W 3
30	107.0	107.0	106.7	106.9	13.1	16.8	14.6	14.8	17.5	11.4	88	79	97	88	1.8	4.1	0.5	2.1	9		9	9			NW 5	W 4	NW 6
31	104.6	103.5	103.7	103.9	13.3	14.2	12.5	13.1	14.6	12.5	96	95	96	96	0.6	0.7	0.5	0.6	10 •		10 •	10 •			NW 9	WNW 9	W 11
M	102.4	102.2	102.3	102.3	14.6	19.2	15.5	16.2	21.0	12.2	86	65	84	78	2.6	9.1	3.2	5.0	7.8		8.1	7.3			4.4	6.1	3.5

Sierpień – Août

1	102.8	104.6	105.0	104.1	12.2	18.2	15.3	14.2	20.0	11.3	95	79	90	88	0.7	4.5	1.6	2.3	10 •		9	0			WSW 9	WSW 9	SW 3
2	104.6	103.5	103.6	103.9	13.1	20.3	14.3	15.5	22.1	9.3	93	72	95	87	1.1	6.6	0.7	2.8	1 ⊙		10 •	8			C 0	C 0	NW 1
3	104.8	107.0	110.1	107.3	14.0	17.3	11.2	13.4	18.7	11.2	98	64	95	86	0.4	7.1	0.7	2.7	9		8 ⊙	1			SSW 3	W 8	W 1
4	109.4	107.2	105.0	107.2	10.9	16.5	15.8	14.8	17.6	7.6	95	72	85	85	0.6	5.4	3.0	3.0	10		10 •	10			S 4	SW 7	SW 5
5	105.0	104.7	102.6	104.1	15.5	23.6	18.6	19.1	24.7	14.0	95	67	88	83	0.9	9.7	2.5	4.4	9		7	1			SW 5	WSW 6	SSE 3
6	99.9	100.4	99.2	99.8	20.0	28.5	19.5	21.9	30.2	16.2	80	49	95	75	4.8	19.8	1.1	8.6	3 ⊙		4 ⊙	8			SW 5	WSW 4	C 0
7	101.4	101.9	104.9	102.7	15.7	19.5	16.3	17.0	21.2	15.6	98	86	94	93	0.4	3.3	1.1	1.6	10 •		9	9			WNW 3	SW 1	SW 3
8	108.5	106.3	104.1	106.3	12.6	22.0	19.6	18.4	22.4	8.8	93	64	84	80	1.1	9.4	3.6	4.7	2 ⊙		7	9			C 0	SSE 4	SSE 3
9	107.7	109.2	110.0	109.0	17.6	23.7	19.0	19.8	24.1	15.6	86	67	79	77	2.8	9.5	4.6	5.6	8		6	8			N 5	NW 2	NNE 2
10	109.4	107.1	104.0	106.8	17.6	25.0	19.2	20.2	26.4	16.5	86	69	97	84	2.8	9.8	0.6	4.4	10		9 ⊙	8			SE 3	E 5	NNE 3
11	103.2	103.7	105.6	104.2	16.6	17.3	16.1	16.5	19.2	16.1	98	96	97	97	0.4	0.8	0.6	0.6	10		10 •	4			NNW 4	NNW 3	NW 1
12	105.2	104.7	106.4	105.4	15.6	21.5	15.0	16.8	22.4	14.5	100	56	89	82	0.0	11.2	1.8	4.3	9 ≡		9	9			S 2	WNW 6	W 3
13	108.5	109.8	111.0	109.8	12.8	16.8	14.4	14.6	18.3	11.9	83	61	76	73	2.6	7.5	3.9	4.7	8		9	7			NW 6	NW 8	WSW 4
14	110.1	108.4	105.0	107.8	11.2	18.8	13.9	14.4	19.8	8.1	92	49	88	76	1.0	11.0	2.0	4.7	9 ⊙		8	9			SSW 2	S 5	S 3
15	101.6	99.9	98.4	100.0	13.0	15.5	12.5	13.4	17.1	11.9	96	83	90	90	0.6	3.0	1.4	1.7	10		10 •	2			SW 3	SW 4	SSW 5
16	98.3	97.1	97.2	97.5	11.6	11.4	10.0	10.8	14.0	9.9	84	94	95	91	2.1	0.9	0.7	1.2	7 ⊙		10 •	2			SSW 7	SSW 9	SSW 5
17	96.0	96.8	98.3	97.0	11.6	13.6	10.9	11.8	16.7	9.6	85	81	92	86	1.9	3.0	1.0	2.0	3 ⊙		10	3			WSW 5	SSW 6	SW 2
18	98.9	98.7	99.1	98.9	10.4	18.1	14.3	14.3	20.0	7.6	99	59	79	79	0.2	8.4	3.4	4.0	10 ≡		7 ⊙	4			W 5	WNW 9	WSW 4
19	93.6	92.5	94.1	93.4	12.7	19.1	14.1	15.0	19.7	11.7	95	57	77	76	0.7	9.4	3.7	4.6	10		9	10			SSW 5	WSW 9	SW 5
20	95.2	97.3	100.9	97.8	13.4	17.0	13.2	14.2	19.6	12.3	84	70	85	80	2.5	5.8	2.3	3.5	10		8	9 •			WSW 7	W 9	WSW 8
21	101.0	101.7	99.7	100.8	13.8	17.4	16.0	15.8	19.8	12.9	89	73	87	83	1.8	5.3	2.3	3.1	10		10	9			WSW 8	WSW 9	SSW 3
22	96.1	95.4	95.5	95.7	16.2	13.8	13.1	14.0	18.7	13.0	77	95	87	86	4.2	1.1	1.9	2.4	8		10 •	3			SW 7	W 6	SW 5
23	97.5	100.3	103.5	100.4	12.8	13.8	12.2	12.8	17.3	12.2	89	90	83	87	1.6	1.6	2.4	1.9	10 •		9 •	5			SW 7	W 8	SW 4
24	105.9	106.9	106.3	106.4	10.6	14.9	12.1	12.4	15.4	9.1	91	73	94	86	1.2	4.5	0.8	2.2	4 ⊙		10	6			W 7	W 7	SSW 3
25	104.5	106.7	107.3	106.2	11.6	17.6	15.0	14.8	19.2	10.1	93	55	84	77	1.0	9.0	2.7	4.2	10 •		9	9			SSW 5	WNW 8	W 2
26	109.1	109.6	110.2	109.6	15.4	21.8	17.2	17.4	22.2	11.7	94	66	92	84	0.9	8.9	1.6	3.8	9		8	7			WSW 1	W 6	C 0
27	110.6	110.8	112.3	111.2	15.6	26.1	17.9	19.4	26.7	13.0	96	52	91	80	0.7	16.2	1.8	6.2	4 ⊙		4 ⊙	1			SSW 4	WSW 5	WNW 2
28	115.1	116.7	116.1	116.0	15.2	20.4	16.2	17.0	22.1	13.6	89	50	83	74	1.9	12.0	3.1	5.7	3 ⊙		4	4			NW 3	WNW 7	W 4
29	115.6	114.4	113.8	114.6	13.1	22.1	17.2	17.4	25.6	9.7	96	56	77	76	0.6	11.7	4.5	5.6	7		3	0			WSW 1	WNW 6	NNE 4
30	114.5	115.4	115.5	115.1	14.2	22.2	15.8	17.0	25.9	11.9	91	54	86	77	1.5	12.4	2.4	5.4	9		0 ⊙	0			E 2	E 2	SE 1
31	117.7	118.4	118.6	118.2	14.2	25.0	17.2	18.4	25.6	11.2	93	50	86	76	1.1	15.8	2.8	6.6	0		4 ⊙	0			C 0	S 2	SE 1
M	104.9	105.1	105.3	105.1	13.8	19.3	15.2	15.9	20.9	11.9	91	68	88	82	1.4	7.9	2.1	3.8	7.5		7.7	5.3			4.1	5.8	3.0

Poznań-Ławica — $H_s = 86\,m$ — $H_b = 92{,}1\,m$ — $h_w = 13\,m$ — Lipiec – Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	∞ 0^{00}–2^{30} = –6^{15} ∞ –11^{40} 21^{20}–24
2	7	.	.	–	∞ 0^{00}–30 = –7^{45} ∞ –24
3	7	.	.	–	∞ 0^{00}–40 = –6^{45} ∞ –12^{15} 19^{45}–22^{30} = –24
4	6	4.4	.	–	• ^{0} 12^{45}–13^{30}–20^{10}, = 0^{00}–8^{30} ∞ –9^{45} = 13^{30}–24
5	8	0.0	.	–	▽ ^{0} 17^{30}–18^{05}, 19^{30}–40 20^{30}–35, K ^{0} 19^{50}–20^{05} SSW-E, = 0^{00}–3^{30}, ≫ 3^{30}–4^{30}, ⌒ 19^{45}–20^{05}
6	7	6.7	.	–	▽ $^{0-1}$ 8^{45}–16^{15}, 21^{04}–22^{40}, = 22^{30}–24, ⌒ ^{0} 0^{00}–8^{00}, ≫ 17^{15}–19^{20}
7	8	0.0	.	–	▽ ^{0} 0^{40}–1^{30}, 8^{42}–9^{05}, 12^{15}–30, = 0^{00}–5^{15}, ⌒ ^{0} 21^{00}–24
8	6	0.3	.	–	∞ 8^{30}–21^{40} = –24, ⌒ ^{0} 0^{00}–9^{00}
9	7	6.4	.	–	• $^{0-1}$ ▽ $^{0-1}$ 6^{05}–15^{10} ▽ $^{0-2}$ 16^{04}–40 19^{44}–50 • ^{0} 23^{45}–24, = 0^{00}–45 ∞ –2^{40} = –11^{40}, 23^{10}–24
10	7	3.1	.	–	• ^{0} 0^{00}…30 3^{20}–4^{05} ▽ $^{0-1}$ 11^{01}–22^{10}, = 0^{00}–9^{30}
11	7	3.2	.	–	K ^{0} 23^{40}–24, = 0^{00}–1^{30}, 6^{30}–9^{20} ∞ 18^{45}–20^{45} = –24
12	6	.	.	–	▽ ^{0} ^{03}–4^{30} K ^{0} 0^{00}–4^{25} W-NE, = 0^{00}–10^{30} ∞ –17^{30}–20^{10}–24, ≫ 3^{15}–20
13	7	8.7	.	–	▽ ^{1} 13^{25}–15^{10} ▽ ^{0} 16^{45}–17^{20} • ^{0} 21^{10}–24, K ^{0} 15^{10}–16^{06} S-NW, ∞ 0^{00}–2^{30} = –8^{30} ∞ –15^{10} = 21^{10}–24
14	8	3.9	.	–	• ^{0} 0^{00}–2^{20} ▽ ^{0} 23^{15}–25, = 0^{00}–3^{45}, ≫ 8^{20}–13^{30}
15	8	2.3	.	–	▽ $^{0-1}$ 5^{35}–8^{55} ▽ ^{0} 23^{01}–15, = 8^{55}–10^{40} ∞ 20^{40}–24, ⌒ ^{0} 3^{00}–6^{05}
16	7	0.7	.	–	• ^{0} 3^{45}–4^{40}–9^{40}, ∞ 0^{00}–1^{45} = –13^{30}, ⌒ ^{1} 21^{00}–24
17	7	7.9	.	–	• ^{0} 11^{30}–12^{40} ▽ $^{0-1}$ 13^{30}–24, K ^{0} 15^{10}–16^{20} SW-E, 20^{03}–21^{35} W-NE, = 3^{20}–6^{30}, 20^{15}–24, ⌒ ^{1} 0^{00}–10^{00}
18	6	12.3	.	–	▽ ^{0} 0^{00}–10 10^{30}–12^{24} ▽ $^{1-0}$ 20^{38}–21^{50}, (K) W 20^{36}–47 K $^{1-0}$ –21^{30} (K) –21^{40} W
19	7	0.0	.	–	• ^{0} 12^{15}–45 17^{02}–12, K ^{0} 11^{35}–12^{45} N-E, = 0^{00}–11^{30}, 21^{15}–24, ⌒ ^{1} 20^{00}–24
20	7	8.6	.	–	▽ ^{0} 12^{30}–13^{20} ▽ $^{0-2}$ 14^{15}–15^{05} • ^{0} 22^{15}–23^{35}, = 0^{00}–a ∞ p–rp = –24, K ^{0} 14^{15}–15^{20} NW-E, ⌒ ^{1} 0^{00}–11^{00}
21	7	4.9	.	–	• ^{0} 3^{40}–5^{02} ▽ ^{0} 8^{02}–20^{10}, = 0^{00}–10^{30} 22^{30}–24
22	7	1.2	.	–	• • ^{0} 7^{48}–8^{10} • –9^{20} ▽ ^{0} –10^{15} 14^{02}–15^{20}, = 0^{00}–11^{00}
23	7	0.1	.	–	▽ ^{0} 7^{50}–8^{10} • ^{1} 12^{35}–13^{15} • ^{0} 13^{40}–14^{15} ▽ ^{0} 22^{35}–23^{20}
24	7	.	.	–	
25	8	.	.	–	= 3^{45}–7^{10}, ⌒ ^{0} 3^{00}–9^{00}
26	7	0.0	.	–	= 4^{30}–10^{45} ∞ –23^{35} = –24, ⊕ 14^{10}–15^{40}
27	6	3.0	.	–	• ^{0} 1^{45}–2^{35}, = 0^{00}–9^{40} ∞ –19^{30} = –24, ≫ 13^{55}–17^{15}, ⌒ ^{1} 4^{00}–10^{00}
28	6	4.6	.	–	• $^{0-1}$ 4^{45}–11^{35} ▽ ^{0} 14^{15}–20 15^{55}–16^{15} • ^{0} 16^{24} 16^{46}–18^{02}, = 0^{00}–14^{15}, 16^{20}–24, ⌒ ^{0} 3^{00}–5^{00}
29	8	.	.	–	• ^{0} 0^{00}–40, = 0^{00}–9^{30}, ⌒ ^{0} 22^{00}–24
30	8	1.3	.	–	▽ ^{0} 14^{33}–15^{35}, 16^{40}–18^{40}, 20^{45}–21^{10} • ^{0} 23^{10}–24, = 21^{35}–24, ⌒ $^{1-0}$ 1^{00}–9^{00}
31	6	48.9	.	–	• ^{0} 0^{00}…30 • $^{0-1}$ 7^{07}–24, = 0^{00}–5^{45}, ≫ 15^{06}–23^{05}
Σ	–	132.5	–	–	UWAGI.

Sierpień – Août

1	7	0.2	.	–	• ^{0} 0^{00}–6^{05} 6^{45}–11^{20}, = 11^{20}–13^{30} ∞ 15^{40}–17^{50} = 20^{40}–24, ≫ 1^{5}–5^{20} 9^{00}–12^{55}
2	6	3.6	.	–	• ^{0} 13^{30}–16^{25} 19^{40}, = 0^{00}–10^{30} ∞ –14^{30} = –22^{25} = ^{2} –24, ⌒ $^{0-1}$ 3^{00}–11^{00}
3	7	0.6	.	–	• ^{0} 9^{35}–40 10^{27}–11^{02} ▽ ^{0} 18^{37}–45, = $^{2-1}$ 0^{00}–2^{40} = –3^{10} = $^{0-1}$ –5^{45} = –12^{15}, ≫ 18^{35}–45
4	6	0.1	.	–	• ^{0} 12^{10}–14^{40} 17^{05}–18^{20}, = 2^{30}–10^{30} ∞ a, p = –24, ⌒ ^{1} 0^{00}–10^{00}, ⊕ ^{1} 7^{10}–10^{50}
5	7	.	.	–	= 0^{00}–10^{20} ∞ –13^{40} = –20^{30}–24, ⌒ $^{0-1}$ 2^{00}–1^{00} ⌒ ^{1} 23^{00}–24
6	7	5.9	.	–	▽ $^{0-1}$ 19^{35}–21^{40}, K ^{0} 19^{20}–22^{15} SW-E, = 0^{00}–7^{40}, ⌒ $^{1-0}$ 0^{00}–10^{00}, ≫ 19^{15}–25
7	6	2.8	.	–	▽ ^{0} 4^{40}–6^{05} • ^{0} 6^{35}–11^{40} ▽ ^{0} 14^{50}–15^{10} = 3^{15}–17^{40} 18^{50}–24, ⌒ $^{0-1}$ 20^{00}–24
8	8	0.0	.	–	• ^{0} 17^{40}–18^{40}, = 0^{00}–8^{45} ∞ –10^{40} = 19^{45}–24, ⌒ ^{1} 0^{00}–11^{00} ⌒ ^{0} 23^{00}–24
9	7	.	.	–	= 0^{00}–9^{15} ∞ –11^{20} = 21^{20}–24, ⌒ $^{0-1}$ 0^{00}–10^{00}
10	7	2.6	.	–	• ^{0} p… ▽ $^{1-0}$ 19^{03}–50, K ^{0} 18^{30}–19^{30} NW–NE, = 0^{00}–6^{10}, 18^{20}–24, ≫ ≫ 19^{01}–20, ⌒ ^{1} 2^{00}–6^{00}
11	6	7.4	.	–	• ^{0} 9^{25}–14^{55} = 0^{00}–40 = $^{0-1}$ 6^{50} = = –20^{40} = = –21^{20} = –24
12	6	.	.	–	= 0^{00}–10^{5} = $^{0-1}$ –2^{40} = ^{2} 7^{50} = ^{1} –8^{20} = ^{0} –8^{50} = –12^{30} ∞ –14^{30} = 22^{00}–24, ⌒ ^{1} 22^{00}–24, ⊕ 13^{40}–14^{20}
13	8	.	.	–	= 0^{00}–5^{30}, ⌒ ^{1} 0^{00}–10^{00} ⌒ ^{0} 23^{00}–24
14	7	2.6	.	–	= 4^{40}–8^{15} 19^{50}–24, ⌒ ^{1} 1^{00}–10^{00} ⌒ ^{0} 22^{00}–24
15	6	3.8	.	–	• ^{0} 2^{40}–3^{30} • $^{1-0}$ 7^{05} 11^{40} ▽ ^{0} 13^{40}–18^{05}, = 0^{00}–12^{40} ∞ –13^{40} = –24, ⌒ ^{0} 0^{00}–2^{40}
16	6	1.8	.	–	▽ ^{0} 11^{20}–15^{08} 15^{12}–15^{20}, = 0^{00}–7^{15}, 21^{10}–24
17	7	.	.	–	• ^{0} 1^{10}–2^{35}, = 0^{00}–6^{45}, 21^{20}–24, ⌒ ^{1} 21^{00}–24
18	7	1.9	.	–	▽ ^{0} 16^{36}–17^{05} 17^{40}–50, = 0^{00}–5^{40} = ^{0} –8^{30} = –12^{30}, ≫ 14^{10}–15^{35}, ⌒ ^{1} 0^{00}–9^{00}
19	7	0.0	.	–	• ^{0} 3^{27}–5^{35} 7^{04}–35 ▽ ^{0} 17^{50}–18^{05} • ^{0} 23^{35}–24, = 3^{30}–12^{15} 23^{10}–24
20	7	5.0	.	–	• ^{0} 0^{00}–10 ▽ $^{0-1}$ 8^{23} 22^{05}, = 0^{00}–5^{30} 8^{30}–10^{20} 21^{15}–24, ≫ 14^{10}–15^{15}
21	6	0.0	.	–	▽ ^{0} 0^{40}–1^{15} • ^{0} 1^{30} 2^{30}–5^{20} 6^{35} 7^{10}, 23^{45}–24, = 0^{00}–14^{30}, 20^{30}–24, ≫ 11^{05}–12^{20}, 15^{30}–16^{05}
22	7	7.0	.	–	• ^{0} 0^{00}–25 ▽ $^{0-1}$ 10^{20} 18^{40} ▽ ^{0} 23^{47}–24, = 0^{00}–8^{15}, 20^{15}–24
23	7	4.6	.	–	▽ ^{0} 0^{00}–05 ▽ $^{0-1}$ 6^{20} 15^{45}, = 0^{00}–6^{00}
24	7	0.0	.	–	= 10^{25}–24, ⌒ ^{1} 22^{00}–24
25	7	0.0	.	–	• ^{0} 5^{45}–8^{10} • ^{0} 8^{40} 11^{05}, = 0^{00}–12^{10} 20^{35}–24, ⌒ ^{1} 0^{00}–5^{45} ⌒ ^{0} 22^{00}–24
26	6	(0.0)	.	–	• ^{0} 9^{07}…45, = 0^{00}–12^{30}, ∞ –16^{30} = 19^{20}–24, ⌒ $^{0-1}$ 0^{00}–9^{07} ⌒ ^{1} 20^{00}–24
27	7	.	.	–	= 0^{00}–5^{25} = –6^{30} = –9^{30} ∞ –12^{10} = 20^{30}–24, ⌒ ^{1} 0^{00}–10^{00}, 22^{00}–24
28	8	.	.	–	= 0^{00}–9^{05}, 21^{30}–24, ⌒ ^{1} 0^{00}–10^{00} ⌒ ^{0} 22^{00}–24, ⊕ 8^{35}–9^{40}, 11^{40}–12^{20}
29	7	.	.	–	= 0^{00}–5^{40} = –7^{50} = –9^{50} 20^{40}–24, ⌒ $^{0-1}$ 0^{00}–10^{00}
30	7	.	.	–	= 0^{00}–9^{30} ∞ –13^{40} = 22^{30}–24, ⌒ ^{1} 2^{00}–9^{00}, 22^{00}–24
31	8	.	.	–	= 0^{00}–5^{20} = –7^{10} = –8^{35}, 20^{30}–24, ⌒ ^{1} 0^{00}–10^{00} ⌒ ^{0} 22^{00}–24
Σ	–	49.9	–	–	UWAGI.

Poznań – Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ **Wrzesień – Septembre 1961**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	118.2	116.7	115.6	116.2	15.4	27.3	18.4	19.9	28.3	12.0	87	41	80	69	2.3	21.6	4.3	9.4	0 ⊙	1 ⊙	0	SSE 3	S 5	SSE 2
2	111.6	109.7	105.8	109.0	15.0	29.2	18.8	20.4	30.3	12.9	92	33	77	67	1.3	27.1	4.9	11.1	0 ⊙	0 ⊙	0	SSE 2	SSW 7	SSE 3
3	102.9	101.6	100.4	101.6	15.5	27.2	17.8	19.6	28.2	13.0	77	47	86	70	4.1	19.1	2.8	8.7	3 ⊙	1 ⊙	10 • ⚐	S 4	SSW 7	SSE 3
4	101.7	103.5	103.8	103.0	15.4	22.7	16.5	17.8	23.9	14.5	96	91	78	75	0.8	13.6	4.3	6.2	1 ⊙	7 ⊙	2	NNW 3	N 3	ENE 2
5	102.6	100.8	96.9	100.1	13.6	25.8	19.0	19.4	26.4	12.1	91	53	84	76	1.5	15.8	3.6	7.0	0 ⊙	0 ⊙	10 ⚐	SE 1	SE 3	ESE 2
6	96.8	96.9	96.1	96.6	15.7	22.4	15.0	17.0	22.6	15.0	99	62	91	84	0.2	10.4	1.5	4.0	10 ≡	7 ⊙	0	W 4	SW 5	S 3
7	94.2	93.9	95.1	94.4	14.8	17.0	12.2	14.0	18.7	10.9	92	67	73	77	1.3	6.3	3.8	3.8	10	7 ⊙	9	SSW 5	SSW 6	SW 8
8	96.6	98.0	101.2	98.6	12.1	13.5	13.0	12.9	14.2	11.3	79	76	88	81	3.0	3.7	1.8	2.8	9	9	9	WSW 8	WSW 9	WSW 6
9	103.9	105.0	106.2	105.0	13.2	15.6	12.2	13.5	17.1	11.3	91	66	90	82	1.4	6.0	1.4	2.9	9	9	10	W 7	WNW 7	W 6
10	107.5	108.0	108.7	108.1	12.0	13.9	12.5	12.7	14.9	10.7	87	70	89	82	1.8	4.7	1.5	2.7	9	9	10	W 7	WNW 8	WSW 5
11	107.1	106.0	104.1	105.7	12.0	18.6	14.1	14.7	19.6	11.7	91	72	74	79	1.2	6.1	4.3	3.9	10	8 ⊙	8	SSW 3	SW 7	SSW 4
12	101.4	102.1	102.9	102.1	11.8	14.9	13.6	13.5	17.7	10.6	81	92	91	88	2.6	1.3	1.5	1.8	8	10 •	10	S 4	W 7	SW 4
13	103.8	105.0	103.6	104.1	11.7	17.6	14.3	14.5	18.7	11.2	91	57	82	77	1.1	8.6	2.9	4.2	9	9	8	SW 3	W 4	SSE 3
14	99.2	99.8	98.7	99.2	14.4	19.3	15.8	16.3	20.9	13.5	86	79	96	87	2.4	4.6	0.7	2.6	10 •	10	10 •	S 4	SW 7	SW 3
15	105.9	109.7	110.4	108.7	13.0	17.9	12.4	13.9	18.5	12.3	84	58	88	77	2.5	8.7	1.7	4.3	4	6 ⊙	2	W 9	W 10	SW 3
16	110.6	110.5	109.2	110.1	14.3	24.4	18.0	18.7	25.4	11.9	89	59	86	78	1.8	12.5	2.8	5.7	8 ⊙	4 ⊙	0	SSW 3	SSW 4	SE 2
17	109.4	108.9	108.4	108.9	14.6	28.0	18.5	19.9	29.1	13.2	91	46	87	75	1.5	20.3	2.7	8.2	0	1	0	SE 1	S 2	SSE 2
18	108.5	110.2	111.8	110.2	15.7	25.0	15.9	18.1	25.0	14.4	92	68	80	80	1.3	10.0	3.6	5.0	6	3	0	SW 1	NW 5	N 5
19	113.7	113.4	112.7	113.3	10.6	19.2	12.0	13.4	20.5	8.4	95	51	84	77	0.7	10.9	2.2	4.6	0	0 ⊙	0	NNE 1	N 5	NE 2
20	114.5	114.0	113.7	114.1	9.6	18.0	11.4	12.6	18.3	8.4	95	54	85	78	0.7	9.4	2.0	4.0	0 ⊙	0 ⊙	0	E 5	E 5	E 3
21	114.5	114.7	115.8	115.0	9.5	18.4	13.1	13.5	18.6	7.7	85	49	68	67	1.7	10.9	4.8	5.8	0 ⊙	0 ⊙	0	E 3	E 5	E 5
22	118.0	118.0	117.9	118.0	6.8	17.6	10.4	11.3	18.5	5.5	87	45	76	69	1.3	11.1	3.0	5.1	0 ⊙	0 ⊙	2	E 4	SE 5	E 3
23	117.8	116.4	115.0	116.4	6.4	17.7	9.0	10.5	18.7	4.8	84	37	72	64	1.6	12.7	3.2	5.8	1 ⊙	0 ⊙	0	E 3	E 5	E 3
24	113.3	112.2	111.1	112.2	5.1	18.8	10.0	11.0	19.8	3.8	84	41	83	69	1.4	12.7	2.1	5.4	0	0 ⊙	0	E 4	E 5	E 2
25	109.4	109.4	112.4	110.4	6.4	20.3	14.0	13.7	20.5	4.2	95	52	93	80	0.4	11.5	1.1	4.3	1	8	9	E 2	W 6	W 4
26	113.0	112.7	110.9	112.2	7.6	15.8	12.4	12.0	16.8	6.1	99	57	82	79	0.1	7.6	2.6	3.4	8	7 ⊙	9	C 0	C 0	NW 2
27	110.1	108.8	108.3	109.1	5.8	16.1	9.1	10.0	17.4	4.5	95	50	81	75	0.4	9.2	2.2	3.9	2 ⊙	2 ⊙	0	NE 1	NE 2	E 2
28	108.3	108.5	109.5	108.8	7.8	19.8	14.2	14.0	20.5	7.0	90	61	83	78	1.1	9.1	2.7	4.3	0	1	0	SE 3	SE 5	ESE 3
29	109.8	108.0	107.3	108.4	10.0	20.4	15.8	15.5	20.7	9.4	86	50	64	67	1.8	12.0	6.4	6.7	4	6	9	SE 4	SE 5	ESE 4
30	107.4	106.7	107.3	107.1	13.2	18.0	14.0	14.8	19.7	13.0	76	59	65	67	3.7	8.4	5.6	5.9	9	7 ⊙	0	SE 3	E 5	E 5
31																								
M	107.7	107.6	107.3	107.5	11.6	20.0	14.1	15.0	21.0	10.2	89	57	82	76	1.6	10.9	2.9	5.1	4.4	4.4	4.2	3.5	5.3	3.4

Październik – Octobre

1	110.1	111.5	113.8	111.7	9.5	14.0	9.6	10.7	14.6	9.3	76	62	80	73	2.8	6.1	2.4	3.8	2 ⊙	1 ⊙	0	E 7	E 7	E 5
2	115.8	116.8	117.3	116.6	8.5	14.6	11.3	11.4	15.1	7.8	94	64	89	82	0.6	6.0	1.5	2.7	9	9	0	E 4	E 6	E 6
3	117.0	116.4	115.7	116.4	10.1	18.2	13.6	13.9	18.4	10.0	82	48	65	65	2.3	10.8	5.5	6.2	0 ⊙	1 ⊙	0	E 7	E 8	E 5
4	114.4	113.5	112.8	113.5	9.1	19.7	13.4	13.9	20.0	8.8	85	40	61	62	1.8	13.6	6.0	7.1	0 ⊙	2 ⊙	0	E 6	SE 7	ESE 5
5	112.4	111.4	111.8	111.9	9.0	19.8	14.6	14.5	20.2	9.0	77	46	63	62	2.6	12.5	6.2	7.1	3 ⊙	1 ⊙	0	ESE 5	SE 6	E 5
6	111.2	109.1	106.2	108.8	9.6	21.1	14.7	15.0	22.2	9.3	78	45	57	60	2.7	13.7	7.2	7.9	0 ⊙	0 ⊙	0	E 5	SE 5	SE 5
7	102.3	98.8	98.3	99.8	9.1	18.3	14.1	13.9	19.2	9.0	75	42	65	61	3.0	12.2	5.6	6.9	0 ⊙	1 ⊙	10	ESE 8	ESE 9	ESE 7
8	97.5	98.6	102.2	99.4	12.4	14.0	13.2	13.2	14.6	11.9	68	67	82	72	4.7	5.3	2.8	4.3	9	10 •	10	E 3	SE 4	SSW 2
9	110.4	113.9	117.4	113.9	10.4	17.1	9.3	11.5	18.5	9.1	95	58	93	82	0.6	8.1	0.8	3.2	9	3 ⊙	0	SW 2	W 3	C 0
10	119.2	119.1	117.8	118.7	4.8	20.2	11.4	12.0	20.8	4.8	98	54	83	78	0.1	11.0	2.3	4.5	2 ≡	2 ⊙	0	SSE 1	SSW 4	SE 3
11	116.8	114.3	113.1	114.7	6.8	18.3	10.0	11.3	19.0	6.6	94	57	91	81	0.6	9.0	1.1	3.6	0	1 ⊙	2	E 3	SE 2	SE 1
12	114.6	116.4	118.5	116.5	11.0	17.4	6.0	10.1	17.7	6.0	92	56	89	79	1.0	8.8	1.1	3.6	4	2 ⊙	0	NW 3	N 6	C 0
13	117.9	119.5	119.1	118.8	2.5	11.0	6.7	6.7	13.2	1.9	98	75	90	88	0.1	3.2	1.0	1.4	2 ⊙	8 ⊙	4	NW 2	NW 7	NW 4
14	117.6	116.6	116.2	116.8	4.2	12.5	10.5	9.4	13.4	2.0	97	59	88	81	0.2	6.0	1.5	2.6	9	8 ⊙	10	W 2	WNW 9	WNW 5
15	114.8	113.6	111.8	113.4	10.1	12.2	10.2	10.7	12.4	9.6	95	73	80	82	0.8	3.8	2.5	2.4	10	10	10	W 4	W 7	W 3
16	109.3	106.7	104.6	106.9	9.0	14.9	8.7	10.3	15.0	7.1	83	60	86	76	2.0	6.7	1.5	3.4	9	3 ⊙	9	SSW 3	SSW 7	SW 3
17	99.9	95.2	86.4	93.8	8.9	12.5	10.0	10.4	13.3	8.5	86	72	92	83	1.5	4.1	1.0	2.2	8	9	10	SW 5	SSW 7	S 3
18	78.4	79.4	81.7	79.8	10.2	12.8	10.3	10.9	12.9	9.7	87	74	95	85	1.6	3.9	0.6	2.0	9	10 •	10 •	SSE 6	S 6	C 0
19	86.0	87.9	90.1	88.0	7.6	8.4	10.7	9.4	10.8	7.5	96	90	96	94	0.4	1.0	0.5	0.6	10	10 •	10 •	C 0	SW 1	SE 2
20	97.4	99.5	100.5	99.1	8.9	11.5	9.1	9.6	11.7	8.4	96	77	92	88	0.5	3.2	1.0	1.6	8	10	10	SE 2	N 1	N 6
21	99.0	99.8	104.8	101.2	10.9	13.0	7.8	9.9	13.1	7.8	96	86	87	90	0.5	2.1	1.4	1.5	10 ≡	10	0	E 2	E 5	SE 3
22	109.7	112.4	112.8	111.6	5.5	11.2	8.6	8.5	12.4	5.4	92	74	89	85	0.8	3.4	1.3	1.8	2	7	0	S 1	SE 3	E 3
23	112.0	112.0	110.5	111.5	8.1	12.6	10.5	10.4	14.2	7.3	96	81	84	87	0.5	2.7	2.1	1.8	10	2 ⊙	4	SE 4	SE 6	SSE 5
24	111.1	111.3	107.9	110.1	9.5	12.7	10.3	10.7	13.8	9.0	95	85	87	89	0.7	2.3	1.6	1.5	10	10	4	SW 3	S 6	SE 5
25	103.4	104.1	103.9	103.8	8.1	12.2	10.7	10.4	13.5	7.3	81	85	87	84	2.1	2.4	1.7	2.1	7	10 •	4	S 5	S 7	S 6
26	103.3	102.6	102.3	102.7	11.6	12.6	10.0	11.0	13.7	9.9	85	84	93	87	1.9	2.4	0.8	1.7	10	9 •	10	S 5	S 5	S 2
27	99.4	98.5	99.6	99.2	9.8	17.2	11.8	12.6	17.5	9.4	86	62	90	79	1.7	7.4	1.3	3.5	9	4	9	SE 5	S 5	S 3
28	100.9	101.2	101.2	101.1	8.8	15.4	9.1	10.6	15.5	6.9	97	76	99	91	0.3	4.3	0.2	1.6	10	6 ⊙	2 ≡	SW 1	SSW 2	C 0
29	101.3	102.0	103.5	102.3	9.6	10.0	9.1	9.4	10.1	8.9	93	93	97	94	0.8	0.8	0.4	0.7	10 •	10 •	10	NW 4	C 0	SSW 2
30	104.5	104.7	106.7	105.3	4.2	10.4	3.9	5.6	11.7	3.9	98	83	97	93	0.1	2.1	0.3	0.8	8	9	0 ≡	S 1	SW 5	SW 1
31	106.9	105.6	106.2	106.2	3.9	10.7	10.4	8.8	11.1	2.0	100	80	71	84	0.0	2.6	3.6	2.1	10 ≡	10	10	S 3	SW 7	WSW 9
M	106.9	106.8	106.9	106.9	8.4	14.4	10.3	10.8	15.1	7.6	89	68	84	80	1.3	5.9	2.2	3.1	6.4	6.1	4.8	3.5	5.3	3.5

DNI	WIATR	OPAD	OBSERWACJE	USŁONECZNIENIE	POGODA
	v	R	h		
1	7	.	.	–	= 0⁰⁰–6¹⁵ = –6⁴⁰ = –9³⁰ 20¹⁵–24, ⌒ 0-1 0⁰⁰–9³⁰ ⌒ 0 21⁰⁰–24
2	7	.	.	–	= 0⁰⁰–8⁴⁵ ∞ –14¹⁰ 19⁴⁰–21⁴⁰ = –24, ⌒ 0-1 0⁰⁰–10⁰⁰ 21⁰⁰–23⁰⁰
3	7	17.4		–	● 0-1 21⁰⁸–22⁴², (K) 20¹⁷–21⁰⁵ K¹–22³⁵ (K)⁰–22⁴⁵ SW–NE, = na, np ∞ a, p, ⌒ 1-0 0⁰⁰–10⁰⁰
4	7	.	.	–	= 0⁰⁰–10³⁰ ∞ –13¹⁵ 19³⁰–20³⁰ = –24, ⌒ 0 21⁰⁰–24
5	6	11.3	.	–	● 0-2 20⁴⁰–22⁰⁵ ● 0 23¹⁰–24, K 0-1 19⁴⁰–23¹⁰ SW–ENE K⁰ 23¹⁵–24 SSW–E, = na–a, p–np, ≫ 23²⁰⁻³⁰, ⌒ 0-1 na–a
6	6	0.5	.	–	● 0 0⁰⁰–1²⁰, 15⁵⁰–16¹⁰ ● 0 16³⁰–17²⁵ K⁰ 0⁰⁰⁻³⁵, = na = 0-2 na, a = 0 6⁴⁰⁻⁵⁰, = na, a, p ∞ a–p
7	7	0.9	.	–	● 0 5⁴⁰–6³⁵, 7⁴⁰–8⁴⁰–9³⁰ 11¹⁵ ● 0 13¹⁰⁻²⁰ 16²⁰⁻³⁵, 18⁰⁵⁻²⁶, = 0⁰⁰–12³⁰, ≫ 16¹⁵⁻⁴⁰, 17¹²–19¹⁵
8	7	0.1	.	–	● 0 12⁴⁰–13³⁰ 14³⁰–40 17⁰²–18¹⁰ 21²⁰⁻³², = na–a, p, ≫ 2⁴⁰–3¹⁰
9	8	1.1	.	–	● 0 5¹⁵⁻³⁵, 18¹⁷–20³⁵, = 20¹⁵–24
10	8	0.0	.	–	● 0 11⁴⁰–12⁰⁵, 12⁵⁰⁻⁵⁵ = 0⁰⁰–6¹⁰
11	6	.	.	–	= 4³⁰–12³⁰ ∞ –19³⁰ = –24, ⌒ 0 3⁰⁰–9⁰⁰
12	5	0.9	.	–	● 0 13¹²–15¹⁰, 22⁴⁵–23⁴⁰, = 0⁰⁰–10⁴⁰ ∞ –12³⁰ = –17⁴⁵ ∞ –18³⁰ = –24, ⌒ 0 2⁰⁰–10⁰⁰
13	7	0.0	.	–	● 0 17³⁵–18⁴⁰, = 0⁰⁰–10³⁵ ∞ –18¹⁵ = –24, ⌒ 0 23⁰⁰–24
14	6	19.8	.	–	● 0 6¹⁵–8⁴⁰–10⁴⁰ ● 0-1 12⁴⁰–22²⁰ ● 0 23⁴⁰–24, = 0⁰⁰–14³⁰, 18³⁰–24, ⌒ 1 1⁰⁰–7⁰⁰
15	8	.	.	–	● 0 0⁰⁰–1²⁵, = 0⁰⁰–1⁴⁰ ⌒ 1 21⁰⁰–24, ≫ na, a, a, p, ⌒ 1 21⁰⁰–24
16	7	.	.	–	= 0⁴⁵–9⁵⁰ ∞ –18⁴⁰ = –24, ⌒ 1 0⁰⁰–9⁰⁵ ⌒ 0 20⁰⁰–24
17	7	.	.	–	= 0⁰⁰–9³⁰ ∞ –10¹⁵ = 20²⁰–24, ⌒ 0-1 0⁰⁰–11⁰⁰ ⌒ 1 21⁰⁰–24
18	6	.	.	–	= 0⁰⁰–12³⁰ ∞ –18³⁰ = –24, ⌒ 1 0⁰⁰–11⁰⁰ ⌒ 0 22⁰⁰–24
19	7	.	.	–	= 0⁰⁰–5³⁰ = –7⁴⁰ = –9³⁰, ⌒ 0 0⁰⁰–9⁰⁰ ⌒ 1 21⁰⁰–24
20	7	.	.	–	⌒ 1-2 0⁰⁰–10⁰⁰ ⌒ 1 22⁰⁰–24
21	7	.	.	–	= 5³⁰–8⁴⁵, ⌒ 1 0⁰⁰–8⁰⁰
22	8	.	.	–	= 5³⁰–8³⁰ ∞ –10⁴⁰ = 19⁴⁵–23³⁰, ⌒ 0 3⁰⁰–10⁰⁰, 22⁰⁰–24
23	7	.	.	–	= 4⁴⁰–8⁴⁰ ∞ –11¹⁵ 20³⁰–24, ⌒ 0 0⁰⁰–9⁰⁰
24	7	.	.	–	∞ 0⁰⁰⁻³⁰ = –9³⁰, 19²⁰–24, ⌒ 0 3⁰⁰–10⁰⁰, 19⁰⁰–24
25	6	.	.	–	= na, a, p, p–np = na, p ∞ a, ⌒ 0 0⁰⁰–10⁰⁰, 21⁰⁰–24, ≫ 15⁰²–²⁰
26	7	.	.	–	= 0⁰⁰–10 = –0⁴⁰ = 1-2 3⁴⁵ = –6⁴⁰ = –7³⁰ = –10³⁰, ⌒ 0 0⁰⁰–9⁰⁰, ⏚ 0⁴⁰–4⁰⁰
27	7	.	.	–	= 3⁴⁰–6⁴⁰ = –7³⁵ = –9³⁰ ∞ –11⁴⁰ 18³⁰–19³⁰ = –24, ⌒ 1 4⁰⁰–10⁰⁰, 20⁰⁰–24
28	6	.	.	–	= 0⁰⁰–10³⁰ ∞ –20⁴⁵ = –22³⁰ ∞ –23⁴⁰ = –24, ⌒ 1 0⁰⁰–11⁰⁰
29	6	.	.	–	= 0⁰⁰–9³⁰ ∞ –24, ⌒ 0 5⁰⁰–10⁰⁰
30	6	.	.	–	∞ 0⁰⁰–6³⁰ = –10⁴⁰ ∞ –24
31					
Σ	–	52.0	–	–	UWAGI

Październik – Octobre

1	7	.	.	–	∞ 0⁰⁰–10³⁰ = 18³⁰–24, ⌒ 1 23⁰⁰–24
2	7	.	.	–	= 0⁰⁰–10⁴⁰ ∞ 17⁵⁰–18⁴⁰ = –24, ⌒ 1 0⁰⁰–9⁰⁰ ⌒ 0 20⁰⁰–24
3	7	.	.	–	= 0⁰⁰–8⁴⁰ ∞ –9³⁰ ⌒ 0 0⁰⁰–10⁰⁰
4	7	.	.	–	= 5³⁰–8⁴⁰ ∞ –11¹⁰ 18¹⁵–24
5	7	.	.	–	∞ 0⁰⁰–6⁴⁵ = –7³⁰ ∞ –11³⁰ 16³⁰–21³⁰ = –24
6	6	.	.	–	= 0⁰⁰–8⁴⁰ ∞ –24
7	6	0.0	.	–	∞ 0⁰⁰–24, ≫ 13¹⁰–14⁴⁰ 17¹²–²⁰
8	7	1.1	.	–	● 0 4⁴⁰ 5⁰⁵, 8⁰²…⁴⁰ 9⁴¹ 14³⁵, 23¹⁰–24, ∞ 0⁰⁰–8¹⁵, 18³⁰–19³⁰ = –24
9	7	.	.	–	● 0 0⁰⁰ 5⁴⁵, = 0⁰⁰–11³⁰ ∞ –13³⁰ = 17³⁰–24, ⌒ 1 19⁰⁰–24
10	7	.	.	–	= 0⁰⁰–1¹⁵ = 0–2²⁰ = –3²⁰ = 0-1 –8⁰⁵ = 0 –8¹⁵ = –10⁴⁰ ∞ –17³⁵ = –24, ⌒ 2-1 na, p, np
11	6	.	.	–	= 0⁰⁰–9³⁰ ∞ –17¹⁵ = –24, ⌒ 0 0⁰⁰–9⁰⁰ ⌒ 1 20⁰⁰–24
12	7	.	.	–	= 0⁰⁰–10³⁰ ∞ –11³⁰ = 18³⁰–24, ⌒ 1-2 0⁰⁰–10⁰⁰ ⌒ 0 20⁰⁰–24
13	6	.	.	–	= 0⁰⁰–5³⁰ = –7¹⁵ = –13⁴⁰ ∞ –17³⁰ = –24, ⌒ 0 0⁰⁰–2⁰⁰ ⌒ 1 –8⁰⁰
14	7	.	.	–	= 0⁰⁰⁻³⁵ = 0-1 5⁴⁵ = –7³⁰ = 0-1 –8¹⁰ = –10⁴⁵ = 16³⁰–24, ⌒ 0 0⁰⁰–1⁰⁰
15	7	.	.	–	= 0⁰⁰–12³⁰
16	6	.	.	–	= 12⁰–11⁴⁰ ∞ –16⁵⁰ = –24, ⌒ 0 20⁰⁰–24
17	6	1.3	.	–	● 0 10¹²–11¹⁰ 12¹⁵ 15¹⁵ 23⁴⁰, = 0⁰⁰–11³⁰ ∞ –17³⁰ = –24, ⌒ 0 0⁰⁰–8⁰⁰
18	7	4.7	.	–	● 0 0⁵⁵ 4³⁵ 8⁰⁵ 9³⁰ 12⁴⁰–15³⁰ 20⁴⁰ 24 = 0⁰⁰–8³⁰, 13³⁰–15²⁰, 16³⁰–24
19	5	5.5	.	–	● 0 0⁰⁰–1³⁰ ● 2⁴⁵ ● 0 8⁴⁰–14¹⁵ 16⁵⁰–22¹⁰, = 0⁰⁰–24
20	7	2.2	.	–	● 0 13²⁵–⁴⁰ 14¹³–18²⁵, = 0⁰⁰–11¹⁵ 14³⁰–24
21	5	0.2	.	–	● 0 2⁰⁵–⁴⁰ ● 0 8⁰⁵ 9⁴⁰, = 0⁰⁰–6¹⁰ = 0 –6³⁰ = 1 –8⁵⁰ = –24
22	7	.	.	–	= 0⁰⁰–10³⁰ 16³⁰–24 ⊕ 11⁴⁵ 15³⁰
23	6	2.4	.	–	= 0⁰⁰–13⁴⁰ ∞ –15⁵⁰ = –24, ⌒ 1 1⁰⁰–11⁰⁰ ⌒ 0 23⁰⁰–24
24	6	.	.	–	● 1 3⁵⁰–4³⁰ ● 0–6⁴⁰, = 0⁰⁰–24, ⌒ 0 0⁰⁰–4⁰⁰, 20⁰⁰–24 ⏚ 20³⁰–21⁵⁰
25	6	1.3	.	–	● 1 11³⁵–14⁴⁵ = 0⁰⁰–9⁴⁰ ∞ –11³⁰ = –24, ⌒ 0-1 0⁰⁰–12⁰⁰, ⏚ 3³⁰–4³⁰
26	6	1.2	.	–	● 0 1⁴⁰–5²⁵ 9¹⁵ 9⁴⁰–11⁴⁰ 12⁵⁰–13¹⁰ 13¹⁵–³⁵, = 0⁰⁰–24
27	6	.	.	–	= 0⁰⁰–9³⁰ ∞ –16³⁰ = –24, ⌒ 1 20⁰⁰–24
28	6	0.2	.	–	= 0⁰⁰–16⁴⁵ = –18¹⁵ = –20²⁵ = –23¹⁰ = –24, ⌒ 1 0⁰⁰–9⁰⁰ 20⁰⁰–24
29	6	5.4	.	–	● 0 5⁴⁰–11⁴⁰ 12⁴⁵–13³⁵ ● 1–14¹⁰ ● 0–16⁴⁰, = 0⁰⁰–22¹⁰ = 0-2 –24, ⌒ 1 0⁰⁰–5⁴⁰
30	6	.	.	–	= 2-0 0⁰⁰–6²⁰ = –19¹⁵ = 0-2 –24
31	6	0.2	.	–	= 1 0⁰⁰–1⁴⁰ = 2 –8¹⁰ = –15³⁰ ∞ –17⁴⁰ = –20³⁰ ∞ –23³⁰, ≫ 22¹⁵–24
Σ	–	25.4	–	–	UWAGI

Poznań – Ławica $\varphi = 52°25'$ $\lambda = 16°50'$ **Listopad – Novembre 1961**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	108.1	108.5	111.1	109.2	8.7	8.5	9.5	9.0	10.6	7.9	82	94	91	89	1.9	0.6	1.1	1.2	10 ●	10 ●	10	SW 8	WSW 9	WSW 6
2	112.8	108.9	102.6	108.1	7.6	12.2	9.6	9.8	12.6	7.2	96	75	80	85	0.4	3.8	2.4	2.2	10	8	10	SW 5	SW 8	SW 5
3	95.9	95.7	95.5	95.0	8.2	11.6	5.8	7.8	12.0	5.5	82	67	91	80	2.0	4.5	0.8	2.4	6	9	0	SW 8	SW 11	SSW 4
4	97.7	99.4	102.9	100.0	2.4	7.0	1.6	3.2	7.2	1.6	95	64	95	83	0.6	3.6	0.6	1.6	6	8	10	SSW 5	WSW 6	SW 5
5	105.8	105.1	107.9	105.6	1.1	5.1	5.4	4.2	6.4	1.1	94	83	80	86	0.4	1.5	1.8	1.2	10	10	10	NNW 6	NNW 7	N 7
6	107.3	105.0	102.4	104.9	5.9	7.7	8.3	7.6	8.4	4.9	85	86	94	88	1.4	1.5	0.7	1.2	10	10	10 ●	N 6	NE 8	NE 8
7	97.6	95.9	95.8	96.4	9.2	10.2	10.4	10.0	11.6	8.0	95	95	85	90	0.6	0.8	2.1	1.2	10 ●	10 ●	0	E 8	E 5	SE 3
8	97.4	98.0	97.5	97.6	6.2	5.9	3.2	4.6	10.5	2.1	95	82	97	91	0.5	1.7	0.3	0.8	10	9	4	SW 3	SW 3	SE 2
9	95.0	94.2	93.3	94.2	3.0	7.6	7.0	6.2	8.8	2.0	95	75	84	84	0.6	2.6	1.6	1.6	9	9	6	S 2	S 6	SE 3
10	91.6	92.7	95.2	93.2	5.9	8.4	6.6	6.9	8.6	5.4	85	85	97	89	1.4	1.6	0.3	1.1	10	10	10	SE 3	SW 3	W 2
11	95.1	95.7	97.6	96.1	6.2	8.1	7.8	7.5	8.3	5.5	97	91	96	95	0.3	0.9	0.5	0.6	10	9	10	NE 1	E 3	E 3
12	98.7	100.7	102.1	100.5	8.6	8.3	4.8	6.6	9.2	4.8	89	84	87	87	1.3	1.7	1.1	1.4	10	10	10	E 8	E 8	E 8
13	101.5	100.6	99.6	100.6	3.3	3.0	1.2	2.2	4.8	1.1	95	93	92	93	0.4	0.6	0.5	0.5	10	10	10 ●	E 11	E 12	E 10
14	100.9	104.6	108.5	104.7	0.3	1.2	1.7	1.2	1.8	0.1	90	92	90	91	0.6	0.5	0.6	0.6	10 ●	10 ●	10 ●	NE 8	NNE 6	NE 5
15	109.3	109.7	109.6	109.5	2.1	2.5	1.8	2.0	2.7	0.9	82	84	87	84	1.3	1.2	0.9	1.1	10	10	10	NE 3	W 2	W 3
16	108.3	106.4	104.1	106.3	0.2	2.4	1.2	1.2	2.4	0.0	92	84	96	91	0.5	1.2	0.3	0.7	9	10	10 ●	SW 4	SW 5	SW 5
17	100.4	100.7	102.0	101.0	3.6	6.9	3.6	4.4	7.2	1.2	97	90	88	92	0.3	1.0	0.9	0.7	10 ●	10	1	W 7	W 8	W 7
18	99.2	99.6	103.2	100.7	4.1	6.4	0.6	2.9	7.0	−0.3	82	78	81	80	1.5	2.1	1.3	1.6	10	8	3	WSW 7	WNW 10	WNW 3
19	106.5	110.4	117.3	111.4	−0.4	4.2	−0.9	0.5	4.7	−2.7	92	77	92	87	0.5	1.8	0.5	0.9	9	8	0	NW 4	NW 7	NW 5
20	122.0	124.6	126.2	124.3	0.1	4.4	−2.4	−0.1	5.0	−2.4	86	69	95	83	0.9	2.6	0.2	1.2	9	2 ⊙	9	NNW 5	N 5	WNW 1
21	125.8	121.9	118.2	121.3	−5.3	4.0	−3.6	−2.1	4.0	−5.8	90	61	92	81	0.4	3.2	0.4	1.3	8	4 ⊙	6	SW 2	S 1	SW 1
22	114.8	113.1	109.8	112.6	−6.0	3.3	−5.0	−2.2	5.0	−6.4	89	61	91	80	0.4	3.0	0.5	1.3	3	3	0	SW 2	SW 2	S 1
23	105.8	104.0	102.9	104.2	−6.2	3.2	−3.8	−2.6	4.0	−7.0	89	69	92	83	0.4	2.4	0.4	1.1	0	1	0	SE 2	SW 2	S 3
24	105.2	107.0	107.2	106.5	−1.2	1.8	1.6	1.0	2.1	−4.2	91	89	98	93	0.5	0.8	0.2	0.5	9	10	10 =	SW 2	W 3	C 0
25	105.5	104.8	103.0	104.4	1.2	2.7	2.1	2.0	3.1	1.1	98	96	98	97	0.2	0.2	0.1	0.2	10 =	10 =	10 =	C 0	NW 5	S 2
26	100.4	99.2	96.0	98.5	1.5	4.3	1.1	2.0	4.4	0.7	98	90	94	94	0.1	0.8	0.4	0.4	10	9 =	2	C 0	SE 1	SE 2
27	92.5	92.3	93.6	92.8	−0.1	2.8	2.6	2.0	3.0	−0.6	96	95	100	97	0.3	0.4	0.0	0.2	10	10 ● ●	10 ●	E 3	N 4	E 1
28	98.1	100.5	102.8	100.5	2.7	3.7	3.4	3.3	3.8	2.6	98	93	97	96	0.1	0.6	0.3	0.3	10	10	10	ENE 2	E 2	SE 2
29	103.1	103.2	103.0	103.1	3.7	5.4	4.6	4.6	5.7	3.1	98	94	93	95	0.2	0.6	0.6	0.5	9	10 ●	10	S 3	SW 5	SW 5
30	97.2	96.8	89.1	94.4	3.3	6.6	5.2	5.1	6.7	2.9	85	79	92	85	1.2	2.0	0.7	1.3	10	10	10 ●	SW 7	WSW 7	SW 10
31																								
M	103.2	103.2	103.3	103.2	2.7	5.6	3.2	3.7	6.4	1.3	91	82	91	88	0.7	1.7	0.7	1.0	8.9	8.6	7.0	4.4	5.5	4.0

Grudzień – Décembre

1	82.2	86.1	88.3	85.5	9.2	6.6	5.2	6.6	9.8	4.9	84	95	89	89	1.8	0.7	0.9	1.1	10	10 ●	10 ●	WSW 13	NW 7	SW 5
2	80.5	79.0	88.0	82.5	8.9	12.9	6.1	8.5	13.4	3.9	90	74	66	77	1.1	3.9	3.2	2.7	10 ●	7	10	SSW 8	SW 10	W 10
3	97.0	97.2	95.5	96.6	0.4	4.4	1.6	2.0	6.1	−0.1	96	66	85	82	0.3	2.9	1.1	1.4	0	6 ⊙	10	SSW 6	SW 7	SW 5
4	92.0	98.4	99.1	96.5	2.6	4.1	4.3	3.8	4.4	1.3	98	87	92	92	0.2	1.1	0.7	0.7	10 ●	9	10 ●	NNE 3	W 4	SE 3
5	94.1	94.0	92.4	93.5	12.6	14.6	13.2	13.4	15.0	4.2	84	72	64	73	2.4	4.6	5.5	4.2	9	9	9 ●	SW 8	SSW 9	SSW 8
6	99.6	100.7	103.0	101.1	3.9	3.8	0.8	2.3	13.8	0.8	55	58	81	64	3.8	3.3	1.3	2.8	8	9	0	W 9	W 9	SW 3
7	103.3	105.0	107.1	105.2	−1.0	−0.1	0.1	−0.2	0.8	−2.0	92	94	88	91	0.5	0.4	0.8	0.6	10	10	10	W 2	W 5	W 2
8	107.0	107.5	108.8	107.8	0.2	1.4	1.1	1.0	1.5	−0.2	88	78	79	82	0.7	1.6	1.4	1.2	10	9	10	SW 4	W 7	W 3
9	108.8	106.9	103.3	106.3	−3.1	1.2	−0.6	−0.8	2.0	−3.1	90	72	79	80	0.5	1.9	1.2	1.2	0	9	10	SW 3	SE 4	SE 5
10	101.1	100.7	99.2	100.3	−0.4	1.3	2.4	1.4	2.4	−0.7	92	91	91	91	0.5	0.6	0.7	0.6	10 ✱	10 ●	10	S 2	S 5	S 3
11	92.5	84.6	84.4	87.2	2.4	3.4	9.2	6.0	9.7	1.7	91	97	95	94	0.7	0.3	0.8	0.6	10 ●	10 ●	10 ●	S 3	S 5	W 10
12	94.7	97.4	103.2	98.4	2.4	2.0	−0.1	1.0	9.3	0.0	95	91	98	95	0.4	0.7	0.2	0.4	10 ● ●	10	10 ✱	NE 3	E 4	NE 5
13	115.8	117.6	119.8	117.1	−4.3	−5.6	−7.2	−5.6	−0.1	−9.4	75	83	85	81	1.1	0.8	0.5	0.8	9	4 ⊙	0	NE 7	N 4	E 4
14	120.8	121.7	122.2	121.6	−9.8	−5.6	−8.0	−7.8	−5.6	−11.4	85	62	81	76	0.4	1.5	0.6	0.8	0	0	8	E 4	E 7	NW 7
15	118.1	114.6	120.0	117.6	−2.4	−1.1	−11.6	−6.7	−0.5	−11.6	85	83	79	82	0.8	1.0	0.5	0.8	9 ✱	10 ✱	0	NW 8	NNW 13	E 3
16	126.0	129.3	134.0	129.8	−14.7	−12.9	−15.6	−14.7	−11.6	−16.4	78	69	81	76	0.4	0.7	0.3	0.5	0	3	0	NE 5	E 7	NE 3
17	135.6	134.8	133.2	134.5	−18.1	−12.1	−12.6	−13.8	−9.2	−19.2	78	74	81	78	0.3	0.6	0.4	0.4	2	8	9	NE 2	C 0	N 1
18	132.1	130.4	128.4	130.3	−14.2	−7.9	−7.1	−9.1	−7.1	−15.4	75	64	71	70	0.5	1.2	1.0	0.9	0	0	10	NW 4	W 4	NW 5
19	124.0	123.0	121.3	122.8	−5.3	−2.8	−1.6	−2.8	−1.6	−7.8	82	91	94	89	0.7	0.5	0.3	0.5	10	10 ●	10	W 3	W 5	W 5
20	115.6	108.2	105.1	109.6	−1.6	−0.4	1.4	0.2	1.5	−1.7	94	96	96	95	0.3	0.2	0.3	0.3	10 ●	10 ●	10	W 6	W 10	WNW 6
21	103.6	106.8	107.9	106.1	0.4	−0.4	−6.0	−5.0	1.5	−6.1	94	84	84	87	0.4	0.9	0.6	0.6	10	4	0	NW 8	N 8	W 4
22	99.1	97.6	100.5	99.1	−3.2	−6.4	−10.1	−7.4	−5.0	−10.6	92	89	84	88	0.3	0.4	0.4	0.4	10 ✱	4 ⊙	3	NE 2	NW 3	N 4
23	104.6	106.2	107.2	106.0	−13.1	−7.2	−6.9	−9.0	−4.8	−16.2	77	85	83	82	0.4	0.5	0.6	0.5	10	10 ✱	10 =	C 0	W 1	NW 1
24	107.8	107.0	106.0	106.9	−7.8	−6.8	−10.0	−8.6	−6.3	−10.2	84	91	84	86	0.5	0.3	0.4	0.4	10 ✱	10	10 ✱	C 0	SW 2	S 1
25	103.8	102.4	100.7	102.3	−11.2	−9.8	−17.8	−14.2	−9.8	−17.9	86	88	68	81	0.4	0.4	0.5	0.4	10 ✱	0	0	S 2	C 0	C 0
26	97.6	96.5	97.7	97.3	−21.4	−15.9	−20.6	−19.6	−14.1	−25.4	81	76	82	80	0.2	0.4	0.2	0.3	0	0 ⊙	0	C 0	NE 1	NW 2
27	101.3	103.4	104.3	103.0	−16.6	−8.7	−13.5	−13.1	−8.2	−25.0	80	86	76	81	0.3	0.4	0.5	0.4	10	10	10 ✱	NW 1	E 2	E 2
28	101.1	99.3	98.4	99.6	−10.5	−9.9	−8.3	−9.4	−8.5	−15.9	77	78	80	78	0.6	0.6	0.6	0.6	10 ✱	10 ✱	10	SE 3	SE 4	SE 3
29	98.1	98.0	97.1	97.7	−3.3	−1.7	−3.5	−4.5	−1.2	−8.7	87	88	92	89	0.3	0.7	0.3	0.5	10	10	0	S 2	SE 2	SE 3
30	95.3	95.1	95.0	95.1	−4.1	0.0	−1.0	−1.5	0.6	−5.5	94	92	91	92	0.3	0.5	0.5	0.4	0 ≡	4 ⊙	9	SE 3	S 1	SE 2
31	94.9	95.3	89.9	93.4	−1.0	1.6	0.2	0.2	2.5	−2.3	93	85	92	90	0.4	1.1	0.5	0.7	2	8	2	S 2	S 2	SE 3
M	104.7	104.7	105.2	104.9	−4.1	−1.8	−3.8	−3.4	0.1	−7.2	85	82	84	84	0.7	1.1	0.9	0.9	7.1	7.2	6.8	4.1	4.9	3.9

Poznań – Ławica $H_s = 86\,m$ $H_b = 92{,}1\,m$ $h_w = 13\,m$ Listopad – Novembre 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	1.2	.	–	● 1¹⁰ 20²⁰ ● 13¹⁵ 14³⁵ = 4⁴⁰ 24 ≫ 0⁰⁰ 1⁴⁰
2	6	0.0	.	–	= 0⁰⁰ 13³⁰ ● 16⁴⁰ 24
3	7	0.9	.	–	● 0⁴⁵ 10⁵ ▽ 14¹⁰⁻³⁵ = 0⁰⁰ 9⁴⁰ ∞ 11²⁵ ≫ 11⁸⁰ 14³⁰
4	7	.	.	–	= 6²⁰ 10⁴⁰ 18³⁰ 24 ⌴ 4⁰⁰ 8⁰⁰ ⌓ 21⁰⁰ 24
5	6	0.4	.	–	● 15⁴⁰ 16³⁵ 19⁴⁵ = 0⁰⁰ 13¹⁵ 17³⁰ 24 ⌓ 0⁰⁰ 9⁰⁰
6	7	0.3	.	–	● 13⁴⁰ 14³⁵ ● 15³⁰ 24 = 0⁰⁰ 1³⁰ 13³⁰ 24
7	5	0.1	.	–	● 0⁰⁰ 2³⁵ ● 4⁴⁰ 5³⁰ ● 14³⁰ 16⁴⁰ 17⁴⁵ 18⁰⁵ = 0⁰⁰ 24
8	6	.	.	–	= 0⁰⁰⁻⁰⁵ ≡ 5⁴⁵ = 24 ⌓ 18⁰⁰ 24
9	6	0.1	.	–	= 0⁰⁰ 13³⁰ ∞ 15³⁰ = 24 ⌓ 8⁰⁰ 9⁰⁰
10	6	3.8	.	–	● 2³⁵ 4²⁵ 13³⁵ 14³⁰ ● 19²⁵ ● 22³⁵ 24 = 0⁰⁰ 24
11	6	1.3	.	–	● 0⁰⁰ 2⁴⁰ 21⁴⁰ 22⁸⁵ = 0⁰⁰ 24
12	6	.	.	–	= 0⁰⁰ 24
13	6	14.7	.	–	● 8²⁰ 12⁴⁰ ● 16⁴⁵ 24 = 0⁰⁰ 24 ≫ 0¹⁰ 4¹⁵ 5³⁵ 22²⁰
14	6	0.9	.	–	● 0⁰⁰ 8⁴⁰ 9⁰⁰ ◡ 10³⁰ ● 14³⁵ 17³⁵ 24 = 0⁰⁰ 24
15	7	.	.	–	● 0⁰⁰ 2²⁵ = 0⁰⁰ 11³⁰ 14⁴⁰ 24
16	6	0.2	.	–	● 18⁵⁰ 21⁴⁰ 22³⁵ 23⁴⁵ 24 = 0⁰⁰ 24
17	6	0.0	.	–	● 0⁰⁰ 2²⁵ 6⁴⁰ 8³⁵ ● 9⁰⁵ 12³⁵ ● 13³⁰⁻²⁵ = 0⁰⁰ 21⁴⁰
18	8	0.0	.	–	▽ 10⁰⁵⁻⁴⁵ ≫ 9⁴⁵ 13³⁰ ⌴ 19⁰⁰ 23⁰⁰
19	7	.	.	–	= 7⁴⁰ 9³⁰ ⌴ 0⁰⁰ 11⁰⁰ ⌴ 20⁰⁰ 24
20	8	.	.	–	= 17³⁰ 24 ⌴ 0⁰⁰ 10⁰⁰ ⌴ 19⁰⁰ 24 ◡ 17³⁰ 24
21	7	.	.	–	= 0⁰⁰ 11³⁰ ∞ 12²⁵ = 16⁴⁰ 24 ⌴ 0⁰⁰ 11⁰⁰ ⌴ 20⁰⁰ 24
22	6	.	.	–	= 0⁰⁰ 10⁴⁰ ∞ 16²⁰ = 24 ⌴ 0⁰⁰ 11⁰⁰ ⌴ 20⁰⁰ 24 ◡ 0⁰⁰ 1³⁰
23	6	.	.	–	= 0⁰⁰ 7¹⁰ ≡ 8¹⁵ = 11³⁰ ∞ 15⁰⁵ = 24 ⌴ 0⁰⁰ 12⁰⁰ ⌴ 19⁰⁰ 24 ⌓ 21³⁰ 22¹⁵ ◡ 23²⁰⁻⁴⁵
24	4	1.0	.	–	● 13²⁰ 14¹⁷ 22²⁶ 24 = 0⁰⁰ 14³⁰ ≡ 14⁵⁰ ≡ 16⁴⁰ ≡ 24 ⌴ 0⁰⁰ 10⁰⁰
25	2	0.1	.	–	● 0⁰⁰⁻⁴⁰ 9²⁰⁻⁴⁵ ≡ 0⁰⁰ 8⁵⁰ = 10⁰⁰ ≡ 11³⁵ ≡ 11⁴⁰ ≡ 13⁵⁰ ≡ 24
26	3	.	.	–	≡ 0⁰⁰ 4³⁵ = 7⁴⁰ ≡ 17²⁰ = 24 ⌴ 20⁰⁰ 24 ◡ 22⁴⁰ 24
27	4	2.8	.	–	● 12³⁰ 18³⁵ ● 19⁴⁰ ● 21²⁰ ● 22⁰⁵ 22⁴⁵ 23³⁰ = 0⁰⁰ 2⁰⁰ ≡ 11⁵⁰ = 23⁴⁰ ⌴ 0⁰⁰ 9⁰⁰ ◡ 0⁰⁰ 1²⁰
28	5	0.0	.	–	● ● ● 1³⁵ 8³⁰ ● 22⁴⁰ 23³⁰ 24 ≡ 0⁷⁰ 4³⁰ = 24
29	5	0.0	.	–	● 0⁰⁰ 1⁴⁰ ● 12²⁵ 14⁴⁰ 15⁴⁵ 16³⁵ = 0⁰⁰ 24
30	6	8.7	.	–	▽ 7³³ 8³⁰ ● 13⁰⁵ 24 = 0⁰⁰ 7¹⁰ 9²⁰ 24 ≫ 18²⁰ 24
31					
Σ	–	56.5	–	–	UWAGI.

Grudzień – Décembre

1	6	9.0	.	–	● 0⁰⁰ 5²⁰ ● 8⁰⁵⁻³⁰ ● ▽ ● 15²⁰ ● 20⁰⁵ 24 = noc. a–p, ap. ≫ 0⁰⁰ 10³⁰
2	7	3.0	.	–	● 0⁰⁰ 3⁴⁵ 6³⁵ 9⁴⁰ ▽ 14²⁰ 15³⁵ 16¹⁰⁻²⁵ = 0⁰⁰ 7¹⁵ ≫ 8⁴⁰ 24
3	7	1.6	.	–	= 17⁵⁰ 24 ≫ 0⁰⁰ 7⁴⁵ ⌴ 20⁰⁰ 22⁰⁰
4	6	4.9	.	–	● 2¹⁰ 5³⁵ ● 7⁴⁵ ● 19⁴⁰ 20³⁵ ● 24 = 0⁰⁰ 24 ⌓ 0⁰⁰ 2¹⁰
5	7	0.0	.	–	● 0⁰⁰⁻⁴⁰ 4⁴⁰ 6²⁰ ▽ 20⁴⁵ 21⁰⁵ = 0⁰⁰ 6³⁰
6	8	.	.	–	≫ 0⁰⁵ 1³⁵ ⊕ 10³⁰ 14²⁵
7	5	.	.	–	= 2³⁰ 24 ⌴ 0⁰ 1⁰⁰ 11⁰⁰
8	6	0.0	.	–	* 8¹⁵ 9¹⁵ 10⁰⁵ 11¹⁰ * ▽ 11³⁵ 12⁰⁵ = 0⁰⁰ 20¹⁰
9	6	0.2	.	–	= 3⁴⁰ 11³⁰ ∞ 15³⁰ = 24 ⌴ 5⁰⁰ 10⁰⁰ ⊕ 12²⁰ 15¹⁵
10	5	1.0	1	–	* 3⁴⁰ 4³⁰ * 5³⁵ * 7⁰⁵ * 8²⁰ ● 9²⁵ 11⁴⁵ 13³⁵ 16¹⁵ 17⁴⁰ = 0⁰⁰ 24
11	5	17.1	.	–	● 6³⁵ 8³⁵ ● ● 8⁴⁰ 16⁰⁵ ● 18⁴⁰ 24 = 0⁰⁰ 14¹⁵ ≡ 16²⁰ 18¹⁰ = 24 ≫ 20⁴⁰ 22¹⁵
12	5	4.7	.	–	● 0⁰⁰ 3⁴⁰ 6¹⁵ ● ● 7⁴⁰ ● 13⁰⁴ 17⁰³ * 17¹⁰ * 24 = 0⁰⁰ 24
13	6	.	2	–	* 0⁰⁰ 2¹⁰ = 0⁵⁰ 7¹⁵ 8³⁵ 24
14	7	0.0	1	–	= 0⁰⁰ 9⁴⁰ ∞ 12¹⁰ = 15⁵⁰ 19¹⁰
15	6	0.7	1	–	* 5⁴⁵ 9⁴⁰ 16³⁵ * 18⁴⁰ = 10³⁰ 13¹⁰ 15⁴⁵ 19¹⁵ ≫ 12²⁰ 17¹⁰
16	6	.	2	–	= 8⁴⁰ 12⁵⁰ ∞ 14³⁰ = 24
17	6	.	1	–	= 0⁰⁰ 10³⁰ ∞ 13⁴⁰ = 24
18	6	.	1	–	= 0⁰⁰ 5¹⁵ 7⁴⁰ 10³⁰ ∞ 22³⁰ = 24
19	5	0.1	1	–	● 11²⁰ 17⁴⁰ = 0⁰⁰ 1³⁰ ∞ 3⁴⁰ = 24
20	4	0.1	1	–	● 2⁴⁰ 8⁰⁵ 12⁴⁰ 19³⁵ = 0⁰⁰ 8²⁰ ≡ 12¹⁵ = 24 ≫ 12⁴⁵ 17³⁵
21	8	4.4	pk.	–	* 6³⁰⁻⁴⁰ * ▽ 12²⁰⁻³⁰ = 0⁰⁰ 9¹⁰ ≫ 7⁴⁵ 8³⁵
22	7	1.3	8	–	* 1⁴⁰ 3¹⁰ * 9¹⁰ 17⁴⁰ 18⁴⁵ = 2⁴⁵ 12¹⁵ 16⁴⁵ 21³⁰
23	4	0.0	10	–	* 12⁴⁰ 13²⁰ = 3³⁰ 13⁰⁵ ≡ 19⁵⁰ = 20²⁰ = 24 V² 1⁰⁰ 24
24	6	0.2	10	–	* 3²⁰ 24 ≡ 0⁰⁰ 3¹⁵ = 24 V² 0⁰⁰ 24
25	5	0.0	8	–	* 0⁰⁰ 9⁴⁵ = 0⁰⁰ 15³⁰ ∞ 17⁴⁵ = 20¹⁰ ∞ 23⁴⁵ = 24 V² 0⁰⁰ 24
26	4	.	8	–	= 0⁰⁰ 7³⁰ ∞ 14³⁰ = 24 V² 0⁰⁰ 24
27	5	0.2	8	–	* 10¹⁵ 11¹⁵ 17⁴⁰ 19⁴⁵ ↔ 20²⁰ * 20⁴⁰ 24 = 0⁰⁰ 7²⁰ ≡ 7³⁵ ≡ 10⁴⁰ V² 0⁰² 24
28	6	0.0	9	–	* 0⁰⁰ 3⁴⁵ 4³⁰ 8²⁵ ↔ 9⁴⁰ * 11³⁵ 12⁴⁰ 15²⁵ = 0⁰⁰ 24 V² 0⁰⁰ 24
29	5	.	7	–	= 0⁰⁰ 15⁴⁰ ≡ 16²⁰ = 21⁴⁰ ≡ 23²⁰ ≡ 24 V² 0⁰⁰ 24
30	5	.	6	–	≡ 0⁰⁰ 1⁴⁰ ≡ 7⁴⁰ ≡ 10⁴⁵ ≡ 11⁰⁵ = 24 V² 0⁰⁰ 11⁰⁰
31	6	0.6	5	–	● 22³⁵ 23³⁰ 24 = 0⁰⁰ 24
Σ	–	49.1	–	–	UWAGI.

Warszawa - Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ Styczeń - Janvier 1961

DNI	CIŚNIENIE P − 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	102.4	104.2	106.1	104.2	-0.1	0.9	1.3	0.8	1.3	-0.8	90	92	87	90	0.7	0.5	0.9	0.7	10 *	10 *	10	S 1	WSW 2	SSW 5
2	104.4	102.8	99.7	102.3	-0.3	0.5	0.0	0.0	1.4	-0.4	90	96	90	92	0.6	0.2	0.6	0.5	10	10 *	10	S 1	C 0	S 1
3	93.9	90.0	89.2	91.0	-0.5	2.6	2.5	1.8	3.0	-0.4	96	82	82	87	0.3	1.3	1.3	1.0	10	9 ⊙	10	SE 5	ESE 7	SE 2
4	89.9	89.1	90.6	89.9	2.9	6.6	6.5	5.6	6.9	1.5	83	75	75	78	1.3	2.4	2.5	2.1	10	9 •	10	SE 5	SE 6	S 5
5	92.3	93.2	97.2	94.2	4.1	2.9	2.3	2.9	6.5	1.6	92	95	84	90	0.7	0.4	1.2	0.8	10 ● ≡	10 •	10	C 0	SW 1	SW 4
6	102.3	104.2	102.2	102.9	1.5	2.8	0.6	1.4	3.0	0.6	83	81	84	83	1.1	1.5	1.0	1.2	9	2 ⊙	0	SW 5	S 5	SSE 4
7	100.4	99.7	99.5	99.9	-0.7	2.4	1.5	1.2	2.7	-0.8	79	75	85	78	1.2	2.0	1.1	1.4	4	8	9	SE 4	SSE 4	S 2
8	99.6	100.4	99.0	99.7	1.2	1.5	1.4	1.4	1.7	0.6	89	94	85	89	0.8	0.4	1.0	0.7	10	10	9	SSW 2	WSW 3	S 4
9	97.1	99.6	100.4	99.0	2.1	2.9	2.4	2.4	3.4	0.7	87	88	87	87	0.9	0.9	1.0	0.9	9	10	9	SW 4	SW 3	SW 1
10	100.9	102.0	102.7	101.9	-0.1	1.1	0.7	0.6	2.4	-0.1	88	98	96	94	0.8	0.1	0.2	0.4	8	10	5	S 2	C 0	S 2
11	102.8	104.1	105.4	104.1	-1.5	1.1	0.7	0.2	1.9	-1.5	99	79	86	88	0.1	1.4	0.9	0.8	10	8 ⊙	10	S 5	SE 2	S 1
12	108.4	110.4	115.5	111.4	-0.9	-1.2	-1.9	-1.5	1.1	-1.9	93	91	85	90	0.4	0.5	0.8	0.6	10	10	9	WSW 5	NW 5	NW 5
13	118.9	118.7	115.4	117.7	-3.1	-2.3	-0.5	-1.6	-0.4	-5.3	86	76	66	76	0.7	1.3	2.0	1.3	9	7 ⊙	10	W 4	SW 4	SW 5
14	113.8	115.3	118.3	115.8	0.3	0.5	0.8	0.6	1.1	-0.5	96	98	98	97	0.2	0.1	0.2	0.2	10 •	10 *	10	W 2	W 2	WNW 2
15	120.8	120.4	118.1	119.8	-0.9	-1.5	-1.9	-1.6	1.1	-2.2	96	96	96	96	0.2	0.2	0.2	0.2	10	10	10	NW 2	W 5	W 4
16	113.3	112.7	114.1	113.4	-1.0	1.1	-0.7	-0.3	1.4	-1.8	99	92	77	89	0.1	0.5	1.3	0.6	10 9	10 9	0	W 4	W 5	NNW 2
17	118.9	120.7	125.8	121.8	-7.5	-4.9	-9.7	-8.0	-0.7	-10.3	79	64	72	72	0.7	1.5	0.8	1.0	0	2	0	N 2	N 6	N 5
18	128.4	130.4	129.6	129.5	-11.6	-6.8	-8.1	-8.6	-6.2	-11.9	82	59	69	70	0.4	1.5	1.0	1.0	0	1	6	N 4	N 2	NW 3
19	126.2	124.3	122.4	124.3	-6.7	-4.2	-4.3	-4.9	-3.6	-9.7	75	56	68	66	0.9	2.0	1.4	1.4	9	8 *	9	NNW 2	NNW 2	NW 2
20	119.5	118.1	116.2	117.9	-4.5	-2.5	-3.7	-3.6	-2.5	-5.1	72	74	67	71	1.2	1.4	1.6	1.4	7	8	9	C 0	W 2	W 2
21	113.1	112.3	111.0	112.1	-5.7	-5.3	-8.2	-6.8	-3.7	-8.3	74	60	75	70	1.0	1.6	0.8	1.1	9	2	9	C 0	ESE 2	W 2
22	107.1	105.2	103.3	105.2	-10.9	-4.2	-6.9	-7.2	-3.9	-11.0	83	61	72	72	0.4	1.8	1.0	1.1	9	9	9	S 2	SSE 1	C 0
23	101.7	102.9	104.5	103.0	-6.9	-9.4	-11.5	-9.8	-6.3	-11.6	94	72	82	83	0.2	0.8	0.4	0.5	10	7	1	NNE 4	NNE 4	NNE 1
24	103.2	102.1	102.7	102.7	-9.9	-6.3	-5.7	-6.9	-5.3	-11.9	84	89	90	88	0.4	0.4	0.4	0.4	10	9 *	10	WSW 4	W 2	NE 4
25	102.1	102.5	106.9	103.8	-15.8	-10.6	-15.5	-14.4	-5.3	-16.5	91	80	91	87	0.2	0.5	0.2	0.3	2	3 ⊙	0	NE 1	NE 4	NNE 1
26	112.2	115.5	117.8	115.2	-17.6	-10.2	-12.8	-13.4	-8.7	-18.1	95	91	81	89	0.1	0.3	0.4	0.3	0	2 ⊙	0	C 0	C 0	WSW 2
27	121.3	122.1	119.6	121.0	-12.8	-7.1	-9.8	-9.9	-5.4	-14.2	77	52	62	64	0.5	1.7	1.1	1.1	10	4 ⊙	0	WSW 4	WSW 2	S 5
28	115.5	113.1	109.5	112.7	-12.1	-2.2	-4.9	-6.0	-1.4	-12.6	67	49	61	59	0.8	2.6	1.6	1.7	2	2 ⊙	8	S 2	SW 3	S 2
29	105.0	105.8	106.3	105.7	-8.1	0.9	0.2	-1.7	1.9	-9.2	69	79	88	79	1.0	1.4	0.7	1.0	7	10	0	S 5	SW 8	S 5
30	98.1	93.2	90.5	93.9	0.6	4.1	3.0	2.7	4.2	-1.9	70	55	90	72	1.9	3.7	0.8	2.1	4	10	10	SW 7	SW 5	SW 9
31	92.3	89.0	89.2	90.2	2.9	2.8	2.1	2.5	4.2	2.1	88	96	98	94	0.9	0.3	0.1	0.4	7	10	10 •	SW 3	SSW 2	W 3
M	107.3	107.2	107.4	107.3	-4.0	-1.4	-2.6	-2.6	-0.1	-5.2	85	79	82	82	0.7	1.1	0.9	0.9	7.6	7.4	6.8	2.7	3.1	3.0

Luty - Février

1	90.5	88.5	85.0	88.0	2.3	2.9	1.3	2.0	3.6	1.3	96	91	94	94	0.3	0.6	0.4	0.4	10	10	10	SW 4	S 5	SE 5
2	84.7	84.3	82.7	83.9	1.6	3.3	0.7	1.6	4.0	0.7	87	78	90	85	0.9	1.7	0.6	1.1	9	9	1	SW 3	SW 4	SW 2
3	81.8	82.3	85.9	83.3	0.3	0.6	0.4	0.4	0.9	0.2	88	88	92	89	0.7	0.8	0.5	0.7	7	10	10	SE 2	SW 1	W 5
4	92.1	93.3	92.2	92.5	-0.1	0.8	0.0	0.2	1.6	-0.1	86	77	86	83	0.9	1.5	0.9	1.1	10	9	9	W 5	W 6	C 0
5	95.3	100.0	106.2	100.5	-1.1	-0.2	-2.1	-1.4	0.0	-3.1	83	94	85	87	1.0	0.4	0.9	0.8	8	9	10	C 0	NW 3	W 3
6	109.4	108.7	105.1	107.1	-2.6	-1.2	-0.8	-1.4	0.4	-4.2	100	82	67	83	0.0	1.0	1.9	1.0	9	2	0	NE 5	SSW 2	S 7
7	96.5	96.4	96.8	96.6	-0.1	1.0	2.2	1.3	2.3	-0.8	71	90	82	81	1.8	0.7	1.3	1.3	10	10 △	6	SSE 6	S 2	SSE 4
8	97.0	100.1	104.8	100.6	1.5	2.5	1.4	1.7	3.7	1.2	83	86	91	87	1.1	1.0	0.7	0.9	10 *	10	8	SSW 2	WNW 5	W 2
9	106.3	102.5	97.5	102.1	-0.1	1.7	0.3	0.6	2.7	-0.2	98	81	96	92	0.2	1.3	0.2	0.6	10	10	10 *	S 3	S 4	SE 7
10	100.5	106.5	113.4	106.8	0.3	0.3	0.5	0.4	0.6	0.3	98	98	82	93	0.1	0.1	1.1	0.4	10 •	10 *	10	C 0	NNE 3	NW 2
11	109.1	105.9	97.6	105.5	0.2	2.6	3.6	2.5	3.6	0.1	88	82	85	85	0.7	1.3	1.2	1.1	10	10	10 •	SSE 2	S 3	SSW 3
12	95.6	97.7	104.1	99.1	3.1	3.6	2.3	2.8	4.2	2.0	95	93	98	95	0.4	0.5	0.1	0.3	10	10	10	SSW 2	SE 1	C 0
13	108.5	110.1	113.1	110.6	1.0	3.1	0.6	1.3	3.4	0.6	94	88	98	93	0.4	0.9	0.1	0.5	10	10	0	W 3	WNW 3	NW 2
14	116.6	117.7	116.4	116.9	-1.5	1.6	1.1	0.6	3.3	-2.2	96	87	85	89	0.2	0.9	1.0	0.7	10 ≡	9	0	NW 1	SW 2	SSW 2
15	115.0	116.1	115.8	115.6	2.7	6.5	4.3	4.4	8.3	0.4	84	76	87	82	1.2	2.3	1.1	1.5	10	0 ⊙	9	SSW 3	WSW 4	SW 3
16	116.1	118.9	121.9	119.0	3.1	4.8	2.8	3.4	5.2	2.8	93	97	93	94	0.5	0.3	0.6	0.5	10	10 9 ≡	10 9	W 2	W 2	WNW 3
17	121.8	122.6	122.0	122.1	3.1	4.8	2.9	3.4	4.8	2.8	95	81	96	91	0.4	1.7	0.2	0.8	10 9	10	10 ≡	W 4	NW 5	W 6
18	119.7	118.9	117.3	118.6	0.9	7.5	5.9	5.0	10.1	0.8	96	76	85	86	0.2	2.5	1.4	1.4	10 9 ≡	0	0	W 5	W 5	WSW 4
19	114.8	115.7	117.2	115.9	1.5	2.4	2.2	2.1	5.9	1.5	92	98	93	94	0.5	0.2	0.6	0.4	10 9	10 9	10 9	WSW 5	W 5	W 3
20	118.7	121.9	123.8	121.5	2.8	4.0	1.7	2.6	4.7	1.7	93	87	92	91	0.4	1.1	0.5	0.7	10	10	10	W 2	NW 2	C 0
21	123.8	123.5	122.9	123.4	1.8	4.7	3.0	3.1	5.0	1.5	91	74	85	83	0.7	2.1	1.3	1.4	10	10	0	W 1	W 4	W 1
22	123.3	124.5	124.3	124.0	0.6	2.2	1.1	1.2	3.2	-0.5	96	91	92	93	0.3	0.7	0.5	0.5	8	10	10	C 0	NW 2	E 2
23	123.1	122.7	120.6	122.1	0.5	0.8	0.3	0.5	1.4	0.3	90	86	86	87	0.6	0.9	0.8	0.8	10	10	10	SE 2	SE 1	SE 1
24	119.8	120.3	120.4	120.2	-0.8	0.3	0.2	0.0	0.9	-0.8	83	80	84	82	1.0	1.2	1.0	1.1	10	10	10	SE 2	SE 1	SE 3
25	122.3	124.0	124.4	123.6	-1.4	-0.4	-0.9	-0.9	0.4	-1.3	84	78	81	81	0.9	1.3	1.1	1.1	10	10	10	SE 3	SE 4	ESE 6
26	123.9	123.6	123.2	123.6	-1.4	3.6	-0.1	0.3	4.3	-1.4	84	65	88	79	0.9	2.8	0.8	1.5	0 ⊙	0 ⊙	0	ESE 3	S 3	S 3
27	120.6	118.1	112.8	117.2	-1.0	6.2	6.0	4.3	7.7	-1.0	87	64	82	78	0.7	3.4	1.8	2.0	1	8	10 •	S 3	SSW 5	SSW 5
28	103.7	99.5	94.9	99.4	4.7	7.4	8.0	7.0	8.3	4.3	85	83	66	78	1.2	1.8	3.7	2.2	10 •	10 •	10 •	S 3	SSW 6	SW 6
29																								
30																								
31																								
M	109.0	109.4	109.3	109.2	0.8	2.8	1.7	1.8	3.7	0.2	90	84	87	87	0.6	1.2	0.9	0.9	9.0	8.4	7.2	2.7	3.2	3.2

Warszawa - Bielany $H_s = 101\,m$ $H_b = 104{,}7\,m$ $h_w = 16\,m$ **Styczeń - Janvier 1961**

DNI	WIATR DZIAŁ.	WIATR NOŚĆ v	OPAD R	OBUR. ŚNIEGU h	USŁO. NECZ. NIENIE	POGODA
1		5	0.0	.	-	$*^{o}\ n\ p\ ,= na-np$
2		5	0.1	0	-	$*^{o}\ 10^{50}-19^{00}\ ,= na-p$
3		7	.	.	-	
4		6	2.4	.	-	$\bullet^{o}\ 10^{00}-15^{10}$
5		5	5.7	.	-	$\bullet^{o}\ na-p\ ,= na\ =^{o}a\ =p$
6		5	0.0	.	-	$*^{o}\ 6^{45}-7^{20}\ ,=p$
7		5	0.5	.	-	$=a-p\ ,\sqcup^{o}\ na-a$
8		5	0.9	0	-	$*^{o}\ 4^{00}-5^{10}\ ,=a-p$
9		6	0.2	pż.	-	$\bullet^{o}\ a\ ,=a-p$
10		4	0.8	.	-	$*^{o}\ 7^{40}-a\ .=n-n\ .\sqcup^{1}\ n-a$
11		6	1.7	1	-	$=n-n\ ,\sqcup^{1}\ n-a$
12		7	0.8	1	-	$*^{1}\ na\ .\ a\ .\ \infty\ n-n$
13		7	0.5	3	-	
14		5	2.0	2	-	$\bullet^{o}\ n-a\ .\ a\ .*^{o}\ a-p\quad \bullet^{o}\ p\ ,=n-n\ .\ \infty\ n-a$
15		6	0.0	2	-	$=a-p$
16		6	0.0	2	-	$\bullet^{o}\ na-p\ .=p$
17		8	.	2	-	
18		8	.	2	-	
19		7	0.0	1	-	$*^{o}\ a-p$
20		6	.	1	-	$=n-p$
21		7	.	1	-	
22		6	.	1	-	$=n-a\quad \infty\ a-p\ =p-n$
23		7	0.2	1	-	$*^{o}\ 9^{00}-10^{05}\ .\ 12^{50}-18^{50}\ ,=na-a$
24		5	0.4	2	-	$*^{o}\ na-p\ .=a$
25		7	.	3	-	$\sqcup^{o}\ na-a$
26		5	.	3	-	$=na-a\ =^{o}\ 7^{05-30}\ .\sqcup^{o}\ na-a$
27		6	.	3	-	
28		5	.	2	-	$=na-a$
29		6	.	2	-	
30		6	2.0	1	-	$\bullet\ ,*\ ,\ \overset{\bullet}{*}\ a\ .\ n$
31		6	9.7	.	-	$\bullet\ n\ .\ n$
Σ		—	27.9	—	-	UWAGI:

Luty - Février

1		6	2.0	.	-	$\bullet\ na\quad \bullet^{o}\ a\ .\ p\ .\ ,=n-n$
2		6	.	.	-	$=a-p\ ,\sqcup^{o}\ n-a$
3		6	0.0	.	-	$\overset{*}{\nabla}{}^{o}\ p\quad *^{o}\ 20^{35}-n\ .=n-p\ ,\sqcup^{o}\ n-a$
4		7	0.0	0	-	$*^{o}\ p\quad \overset{*}{\triangle}\ p$
5		6	0.8	.	-	$*^{1}\ a\ ,=n-n$
6		6	.	0	-	$\equiv^{8-2}\ a\ =a-p$
7		6	0.8	1	-	$*^{o}\ a-11^{30}\ \triangle^{o}\ a-13^{10}\ .=n-np$
8		6	0.4	pż.	-	$\overset{\bullet}{*}{}^{o}\ n-a\ .\equiv n-np$
9		6	3.3	pż.	-	$*^{o}\ np\quad \bullet^{o}\ p\ ,=n-a$
10		5	0.5	2	-	$*^{o}\ n\ .\ p\ .\ \equiv n-a=a-p$
11		6	1.8	1	-	$\overset{\bullet}{*}{}^{o}\ p\ zpr\quad \bullet^{o}\ p\ \ np\ ,=n-np$
12		5	0.0	.	-	$\bullet^{o}\ p\ ,=n-p$
13		6	.	.	-	$=na=np\ ,\sqcup^{o}\ np$
14		6	.	.	-	$\equiv^{o}\ na-8^{20}=np\ ,\sqcup^{o}\ na-8^{20}\ .np$
15		5	.	.	-	$=na-n$
16		3	0.5	.	-	$\bullet^{o}\ 8^{10}-n\ .=na-a\ \equiv^{1-0}\ 9^{00}\ 13^{20}$
17		5	0.0	.	-	$\bullet^{o}\ na-a\ .=a\ .\equiv^{o}\ 10^{10}-np$
18		5	0.0	.	-	$\bullet^{o}\ na-10^{10}\ .\equiv^{o}\ na-10^{15}=p-np$
19		4	0.0	.	-	$\bullet^{o}\ na-np\ .=na-np$
20		6	.	.	-	$=n-p$
21		7	.	.	-	$\frown^{o}\ p-n$
22		6	.	.	-	$=n-p\ ,\sqcup^{1}\ n-a$
23		6	.	.	-	$=n-p$
24		6	.	.	-	$=n-p$
25		6	.	.	-	$=n-p$
26		6	.	.	-	$=a-p\ ,\sqcup^{o}\ n-a\ .\ p-n$
27		6	1.3	.	-	$\bullet^{o}\ p\ .\ n\ .=n-a\ \infty\ a-p\ =p-n\ ,\sqcup^{o}\ n-a$
28		6	3.8	.	-	$\bullet^{o}\ n-a\ .\ p\ .\ n\ ,=n-np$
29						
30						
31						
Σ		—	15.2	—	-	UWAGI:

Warszawa – Bielany $\varphi = 52°17'$ $\lambda = 20°58'$ **Marzec – Mars 1961**

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D_v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.5	104.5	109.2	105.1	3.1	3.3	3.4	3.8	7.7	2.9	84	71	86	80	1.2	2.6	1.1	1.6	10	9	6	W 5	W 4	W 4
2	112.8	113.2	113.3	113.1	1.8	3.4	2.6	2.6	4.1	0.1	82	85	91	86	1.3	1.2	0.7	1.1	10	10 ●	9	W 4	W 6	WSW 4
3	113.1	117.3	119.1	117.2	0.7	6.8	4.7	4.2	7.1	0.4	92	58	87	79	0.3	4.1	1.1	1.9	9	6	10	W 2	WSW 1	WSW 1
4	121.1	122.6	122.3	122.0	4.1	5.4	5.8	4.3	6.2	3.5	100	97	87	95	0.0	0.3	1.1	0.3	10 ≡	10 9	8	W 2	W 2	WSW 3
5	117.3	118.8	120.9	119.0	3.7	6.9	3.1	4.2	6.9	2.4	88	75	86	83	1.0	2.4	1.0	1.3	10	10	2	W 5	NW 5	W 3
6	120.9	120.2	118.7	119.9	0.6	3.3	3.6	3.8	5.7	0.3	98	90	85	91	0.1	0.8	1.4	0.8	10	10	9	WNW 3	W 5	W 4
7	114.4	112.8	114.6	113.9	3.6	9.8	6.6	6.6	13.3	3.2	98	83	81	87	0.1	2.0	1.8	1.3	10 ≡	2 ⊙	0	WSW 4	W 3	NW 3
8	119.1	119.0	116.0	118.0	0.4	4.4	3.8	4.1	8.3	0.0	98	85	85	89	0.1	1.3	1.4	0.9	8 ⊙ ≡	7	8	W 3	WSW 6	W 5
9	115.9	115.1	113.1	114.7	6.6	10.6	10.1	9.4	13.1	3.5	87	69	71	76	1.3	4.0	3.6	3.0	10	3 ⊙	5	W 6	W 9	W 4
10	113.8	112.2	109.2	111.7	4.8	13.5	10.4	10.3	16.3	4.8	89	45	62	65	1.0	9.7	4.8	5.2	9	2 ⊙	0	W 5	W 5	WSW 2
11	106.4	106.8	108.3	107.2	5.3	13.6	8.3	8.9	13.9	4.0	83	61	87	77	1.3	6.2	1.4	3.0	7 ⊙	8	10	WSW 5	WSW 8	W 5
12	106.9	101.3	98.2	100.2	5.9	8.6	12.3	9.9	12.6	5.4	88	81	58	76	1.2	2.2	6.1	3.2	10	10	9	WSW 4	WSW 8	WSW 9
13	88.3	92.7	98.8	93.3	6.1	7.2	2.6	4.6	12.3	2.6	64	46	46	52	3.3	5.6	4.0	4.3	9	9	0	W 10	NW 11	W 6
14	101.0	100.8	99.7	100.5	0.3	7.4	6.2	5.0	8.1	0.3	86	46	97	76	0.8	3.6	0.3	2.2	8 ⊙	7 ⊙	10 ●	W 4	W 5	W 3
15	97.4	101.0	106.2	101.5	8.3	10.0	7.3	8.3	11.6	6.2	80	56	72	69	2.3	5.4	2.9	3.5	9	8 ⊙	1	WNW 8	NW 10	W 4
16	101.2	100.3	103.4	102.4	7.8	11.3	7.3	8.6	11.9	4.4	87	56	72	72	1.4	6.0	3.0	3.5	10	8 ⊙	0	SW 7	WNW 10	WNW 5
17	109.7	107.8	103.7	107.1	2.8	10.6	8.9	7.8	13.1	2.7	96	59	76	77	0.3	5.2	2.8	2.8	8 ⊙	4 ⊙	0	WSW 5	W 6	SW 3
18	92.7	90.6	89.0	90.8	9.1	14.6	10.0	10.9	15.6	8.2	61	51	61	58	4.6	8.1	4.8	5.8	9 ⊙	9	8	SW 3	W 9	W 3
19	88.7	89.4	94.9	91.0	3.7	4.7	−0.2	2.0	10.1	−0.2	75	81	74	77	2.0	1.6	1.6	1.7	9 ⊙	10 ⁂	0	SW 8	W 8	NW 2
20	98.0	97.7	89.4	95.0	−1.8	2.9	1.6	1.1	3.7	−1.8	92	47	53	64	0.4	3.9	3.3	2.5	8 ✳	8	6	WNW 3	SW 6	S 6
21	79.9	79.7	85.6	81.1	0.4	2.1	0.9	1.1	4.7	0.1	98	91	96	95	0.1	0.6	0.2	0.3	10 ✳ ≡	10 ⁂ △	5	SW 5	SW 6	SW 2
22	93.9	96.6	101.2	97.2	0.1	2.4	−0.6	0.3	2.7	−0.6	90	53	72	72	0.7	3.5	1.7	2.0	10 ✳	8	6	W 5	WNW 7	WSW 2
23	97.3	98.1	99.7	98.4	0.7	6.0	6.2	4.8	7.2	−0.6	96	88	86	90	0.2	1.2	1.3	0.9	10 ✳	10 ●	10 ●	SW 3	SW 5	WSW 6
24	99.7	100.0	100.9	100.2	6.3	8.3	7.1	7.2	9.6	5.8	73	73	77	74	2.6	3.0	2.3	2.6	10	8	8 ⁂	WNW 8	W 9	WSW 6
25	102.4	104.3	106.0	104.2	5.2	8.3	4.3	5.7	9.0	4.3	89	70	81	80	0.9	3.3	1.6	1.9	10	9 ⊙	0	W 5	WNW 8	W 3
26	103.9	102.6	99.4	100.6	4.9	10.0	9.7	8.6	11.6	3.9	94	72	62	76	0.6	3.3	4.6	2.9	1 ⊙	9	10	WSW 4	WSW 9	WSW 7
27	90.3	91.3	91.7	91.2	3.1	6.7	1.3	3.6	9.7	1.3	64	61	83	70	3.2	3.8	1.0	2.7	8 ⊙	6 ⁂ ⊙	8	W 10	W 10	SW 6
28	91.8	93.4	94.8	93.3	−0.4	2.9	1.6	1.4	3.0	−0.8	90	93	81	89	0.6	0.4	1.3	0.8	10 ✳	9	10 ✳	WSW 6	WSW 3	WNW 3
29	97.4	93.9	93.7	93.7	−0.2	2.3	3.3	3.3	3.6	−0.8	90	93	94	92	0.6	0.3	0.3	0.3	9 ⊙	10 ●	10 ●	WSW 3	WSW 3	SW 6
30	89.9	89.4	89.0	89.4	3.7	7.4	7.4	7.0	8.6	3.3	82	86	93	87	1.7	1.3	0.8	1.3	10 ●	10	10 ●	SW 7	WSW 6	SW 4
31	90.8	93.0	94.0	93.3	1.7	3.8	3.8	3.8	7.8	1.3	92	48	63	68	0.3	4.8	2.8	2.7	10	6 ⊙	4	WNW 2	W 3	C 0
M	102.6	102.9	103.0	102.8	3.4	7.3	5.4	5.4	9.2	2.4	87	70	78	78	1.2	3.4	2.1	2.2	9.1	7.9	5.9	5.0	6.3	4.1

Kwiecień – April

1	94.8	96.3	91.0	94.1	1.1	3.4	2.4	2.3	4.3	−0.6	74	57	82	71	1.7	3.4	1.3	2.1	9	10	3	W 12	WSW 6	WSW 6
2	93.2	93.7	93.3	93.4	2.3	4.4	3.3	3.4	6.3	1.3	84	60	73	73	1.2	3.4	1.9	2.2	10	9	10	WSW 2	W 3	C 0
3	91.3	90.9	96.9	93.0	0.6	8.6	4.0	4.3	9.1	0.0	100	89	77	89	0.0	1.3	1.9	1.1	10	9 ⊙	9	C 0	W 3	W 3
4	94.0	96.3	101.9	97.3	1.7	6.3	4.1	4.0	7.6	1.4	96	73	74	82	0.3	2.4	2.2	1.6	10 ●	9 ⊙	0	S 3	WNW 8	WSW 2
5	104.0	101.4	98.9	101.4	5.4	12.7	16.0	12.3	17.4	3.3	78	70	68	72	2.0	4.4	5.8	4.1	9	8 ⊙	10	SE 3	SE 6	C 0
6	99.0	101.3	101.6	100.6	12.3	20.6	16.3	16.4	22.1	11.3	72	53	73	66	4.0	11.4	4.9	6.8	8 ⊙	9 ⊙	0	SW 4	W 6	C 0
7	100.6	99.4	98.2	99.4	12.6	22.6	18.7	18.2	23.9	11.0	73	59	55	56	3.9	16.8	9.7	10.1	0 ⊙	0 ⊙	0	C 0	SW 6	SW 2
8	99.1	98.7	100.8	99.5	11.7	11.0	6.3	8.9	18.8	6.3	96	90	90	92	0.3	1.3	1.0	0.9	10	10	10	C 0	NW 1	W 3
9	102.7	106.3	109.3	106.2	3.7	4.4	3.1	3.6	7.6	2.3	83	54	53	63	1.4	3.9	3.6	3.0	8 ⊙	9 ⊙	0	W 6	NW 9	NW 1
10	110.0	108.3	104.8	107.7	1.0	6.6	2.9	3.4	7.2	−1.3	83	33	67	62	1.0	6.3	2.4	3.2	9	8	0	C 0	SE 1	E 2
11	101.2	99.3	102.1	100.9	2.3	11.7	6.4	6.7	12.9	−0.3	68	42	59	56	2.3	7.9	3.9	4.7	3	0	0	E 1	ESE 1	NNW 2
12	106.4	107.9	107.1	107.1	1.8	9.7	6.3	6.1	11.0	−0.2	74	44	51	56	1.8	6.7	4.8	4.4	9	2	0	E 3	WNW 3	C 0
13	102.2	101.3	101.9	101.8	6.7	17.2	13.4	12.7	19.4	4.8	69	34	80	68	3.0	9.0	3.2	5.1	9	9	3	S 3	WNW 6	C 0
14	102.1	101.0	99.7	100.9	9.1	22.7	18.3	17.1	23.5	7.2	92	43	59	65	1.0	15.7	8.6	8.4	0	3	0	C 0	C 0	SSE 3
15	99.0	99.2	99.8	99.3	13.6	22.6	16.8	17.4	24.1	11.7	63	48	73	62	3.9	14.3	4.8	8.3	0	0	8	S 4	WSW 6	C 0
16	100.3	98.3	98.7	99.2	11.1	22.2	14.3	15.3	23.3	10.0	89	47	82	73	1.3	14.1	2.9	6.2	4	3	9	ENE 1	SSW 1	C 0
17	99.2	100.3	101.4	100.4	10.8	14.2	12.2	12.4	16.6	10.1	100	82	96	93	0.0	2.9	0.3	1.1	10 ≡	9	3	W 2	E 2	C 0
18	101.7	101.1	100.8	101.2	11.3	16.9	13.3	13.8	18.9	9.4	89	33	73	73	1.3	8.6	3.9	4.7	8	8	0	SW 2	WSW 2	C 0
19	103.3	103.1	103.4	104.6	8.3	13.2	10.3	11.1	16.4	7.2	94	30	37	67	0.7	8.7	3.3	3.0	3	2	0	C 0	NNW 6	ENE 7
20	109.9	110.6	111.7	110.7	4.0	9.9	6.4	6.7	11.3	2.2	67	33	38	33	2.6	8.2	4.1	3.0	1	1	0	NE 6	ENE 6	NE 3
21	113.1	111.4	108.7	111.1	3.0	12.3	9.3	8.3	13.9	0.0	74	31	43	49	2.0	10.0	6.7	6.2	0	0	0	ENE 3	ESE 7	ESE 6
22	104.7	102.3	99.9	102.4	7.0	16.9	12.3	12.1	17.6	3.8	39	37	43	47	4.1	12.1	7.9	8.0	0	0	0	SE 8	SSE 4	SE 3
23	99.0	98.6	99.0	98.9	8.1	17.8	12.6	12.8	18.2	3.7	62	34	37	44	4.1	13.3	9.2	8.9	0	2	0	ESE 4	ESE 9	SE 6
24	100.7	101.8	102.8	101.8	8.2	14.9	10.1	10.8	16.3	7.0	63	39	60	33	3.9	10.3	3.0	6.4	0 ⊙	6 ⊙	0	E 9	E 9	E 4
25	104.6	104.4	104.2	104.4	7.3	12.2	9.1	9.4	13.0	4.9	73	33	71	66	2.7	6.7	3.4	4.3	9	10	0	E 9	ESE 6	C 0
26	101.9	100.4	98.3	100.3	8.1	16.4	12.0	12.1	16.9	4.0	62	39	72	58	4.1	11.2	4.0	6.4	3 ⊙	9 ⊙	10	E 3	SE 7	C 0
27	98.9	99.4	98.9	99.1	10.0	13.8	12.4	12.6	16.2	9.4	79	33	72	68	2.3	8.4	4.0	5.0	9 ⊙	9 ⊙	9	C 0	C 0	C 0
28	98.8	98.3	97.7	98.3	10.6	18.1	13.8	14.1	19.8	8.6	73	34	33	33	3.2	13.8	7.2	8.1	0 ⊙	8 ⊙	8	0 0	C 0	C 0
29	101.6	103.2	103.4	102.7	8.3	12.2	7.8	9.0	14.8	7.6	63	43	46	51	4.0	7.9	5.8	5.9	9 ⊙	8 ⊙	8	E 7	E 9	E 3
30	101.0	99.8	97.7	99.2	7.2	18.7	14.6	13.8	19.9	4.3	59	36	33	30	4.2	13.8	7.3	8.3	4 ⊙	0 ⊙	0	E 4	E 3	SE 4
31																								
M	101.3	101.4	101.4	101.4	7.0	13.9	10.3	10.4	15.6	3.1	77	31	63	64	2.4	8.6	4.6	5.2	3.3	3.7	3.4	3.4	4.7	2.1

Warszawa – Bielany $H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 16\ m$ **Marzec – Mars 1961**

DNI	WIDZIALNOŚĆ v	OPAD	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	–	▽ a – p
2	6	0.2	.	–	▽° a – p, = n – np, ⌣° n – a
3	7	0.2	.	–	•° p, = n – a, p – n, ⌣° n – a
4	4	(0.0)	.	–	•° na, p, ≡² n – a = a – p
5	6	0.0	.	–	•° a, = n – a
6	5	0.0	.	–	= na – a
7	5	0.0	.	–	•° na – 8^{20}, ≡° na – 10^{30} = a – p
8	5	.	.	–	≡¹ na – 10^{00} = a; ⌣° na – a
9	7	.	.	–	
10	6	.	.	–	= na
11	5	0.0	.	–	•° 17^{50} 19^{40} = na – np, ⫻ a
12	7	1.1	.	–	•° 9^{30} – 12^{15}, np, = na, ⫻ np
13	9	0.2	.	–	• ✳, △ p
14	9	0.2	.	–	•° p
15	9	(0.0)	.	–	⫻ a – p
16	7	.	.	–	•° n, ∞ a – p, ⫻ a – p
17	7	.	.	–	= n – a ∞ a – p, ⌒¹ n – a
18	6	.	.	–	= n – a ∞ a – p
19	6	0.0	.	–	•° a ✳° p •° p
20	7	1.4	0	–	✳ n – a
21	6	5.1	0	–	• n ✳ a – p ⛌ p • np, ≡ np
22	8	0.7	.	–	✳° a, p
23	7	0.6	pł.	–	✳° n – a, •° a, n ▽° a – 15^{20}, = n – a
24	7	0.0	.	–	•° a, p ✳ 20^{36-42}
25	8	1.2	.	–	▽° 6^{45} – 9^{35}, 10^{15} a
26	8	0.6	.	–	= na – a, ⌒° a
27	8	0.2	.	–	▽ na ▽° 10^{45} – 11^{20} ⛌° 11^{50} – 12^{40} ▽° 13^{25} – 14^{05} ✳° 17^{35} – 18^{20}, ⫻ na – p
28	7	0.8	1	–	△° na ✳° 6^{05} – 8^{30}, 10^{00} – 12^{25} △ 13^{40} – 14^{05} ✳° 18^{10} n, = na – a
29	6	3.9	.	–	✳° 8^{25} – 11^{10} •° – n
30	6	16.1	.	–	•° na – n, = na
31	8	0.9	.	–	
Σ	–	33.4	–	–	UWAGI:

Kwiecień – Avril

1	8	2.6	.	–	•° R na ✳° 13^{10} – 18^{55}, ⫻ na
2	9	4.1	.	–	•° p ✳° np
3	7	2.6	2	–	✳ n, = n – a
4	7	0.6	.	–	• a, ∞ a – p, ⫻ a – p
5	7	.	.	–	= n – a ∞ a – p
6	6	.	.	–	= n – a ∞ a – p = p – n, ⌒° p – n
7	7	0.4	.	–	= ⌒¹ n – a
8	6	3.6	.	–	•° n, a, p,
9	9	0.0	.	–	✳ a
10	7	.	.	–	= n – a, ⌣° n – a ⌒° p – n
11	7	.	.	–	⌒° n – a ⌣° a ⌒° p – n
12	8	.	.	–	⊕ na – a, ⌒° n – a
13	6	.	.	–	∞ n – p = p – n, ⌒° p – n, ⊕ a – p
14	7	.	.	–	= n – a, ⌒² n – a
15	7	5.6	.	–	(R) 20^{40} – 21^{10} •° R n, ⌒° n – a, p – n
16	7	1.2	.	–	▽° 16^{30} – 17^{20}, n
17	7	4.1	.	–	▽ 18^{58} – 19^{50}, ≡° n – 6^{50} = – a
18	7	.	.	–	= n, ⌒ n, p, np
19	7	.	.	–	= n – a, ⌒² n – a ⌒° p – n
20	8	.	.	–	
21	8	.	.	–	⌒° n – a
22	7	.	.	–	
23	8	.	.	–	
24	7	.	.	–	= n – a ∞ a – p, ⫻ a
25	7	.	.	–	∞ a, ⌒° p – n
26	8	3.6	.	–	•° 13^{30} 18^{30}
27	6	.	.	–	= n – p
28	8	.	.	–	⌒° n – a, p – n
29	7	0.0	.	–	▽° 7^{00}, 7^{25}
30	8	.	.	–	
31					
Σ	–	28.4	–	–	UWAGI:

Warszawa - Bielany — φ = 52°17' — λ = 20°58' — Maj - Mai 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.5	99.5	101.2	100.1	11.1	17.8	12.8	13.6	19.4	5.8	68	39	78	62	4.2	12.5	3.3	6.7	0	6	10	C 0	E 7	E 5
2	101.9	101.6	101.2	101.6	10.3	15.4	12.2	12.5	17.1	9.5	87	61	86	78	1.6	6.9	2.0	3.5	10	9	8	E 4	ESE 1	E 4
3	100.5	98.7	99.9	99.7	11.2	20.1	15.0	15.3	21.0	8.9	85	45	68	66	2.0	12.9	5.4	6.8	8	8	10 •	SE 2	SSE 3	S 1
4	103.0	104.7	106.2	104.6	12.3	16.5	12.8	13.6	17.3	11.3	88	54	76	73	1.7	8.7	3.6	4.7	9	5	2	NW 2	NW 2	C 0
5	107.4	106.6	104.8	106.3	12.3	20.0	17.1	16.6	21.2	7.1	75	37	50	54	3.5	14.7	9.7	9.3	0	9	6	C 0	SSE 3	SE 5
6	102.0	100.0	104.6	102.2	13.6	21.5	13.7	15.6	21.6	12.8	67	50	92	70	5.2	12.8	1.3	6.4	10	9	9	S 4	SW 7	W 2
7	104.9	102.7	96.8	101.5	12.7	17.2	12.6	13.8	20.0	10.7	88	62	93	81	1.8	7.4	1.1	3.4	9	10 •	9	WSW 3	SW 2	C 0
8	99.9	98.4	97.9	98.7	9.0	13.4	8.5	9.8	14.3	7.7	90	51	86	76	1.1	7.6	1.5	3.4	9	9	6	WSW 4	WSW 3	SW 3
9	95.6	93.7	92.2	93.8	8.2	9.5	9.0	8.9	11.9	7.3	82	88	89	86	2.0	1.4	1.3	1.6	10	9	9	SW 7	WSW 4	SW 3
10	93.0	94.9	96.9	94.9	7.1	11.2	7.6	8.4	11.8	6.6	93	60	84	79	0.8	5.3	1.6	2.6	10 •	6 ⊙	9	WNW 1	WNW 4	W 4
11	99.2	102.0	104.8	102.0	6.7	8.3	7.1	7.3	9.5	6.4	91	79	78	83	0.9	2.3	2.2	1.8	10	10	10	NNW 6	NW 5	WNW 3
12	104.9	103.6	102.5	103.7	4.6	8.6	7.3	7.0	10.2	4.2	82	65	74	74	1.5	3.9	2.6	2.7	10 •	10	6	NNW 5	NNW 5	NW 1
13	102.6	102.1	100.0	101.6	5.2	11.5	9.5	8.9	13.2	4.1	81	54	84	73	1.6	6.3	1.9	3.3	10	8	10 •	W 3	WSW 6	WSW 3
14	98.5	97.8	98.1	98.1	9.1	11.5	8.0	9.2	12.2	7.3	87	59	76	74	1.6	5.7	2.5	3.3	10	10 •	1	WSW 4	SW 4	WSW 2
15	98.9	99.1	99.8	99.3	6.8	10.2	8.3	8.4	12.9	4.9	86	64	87	79	1.5	4.5	1.4	2.5	9	9	9	C 0	W 3	C 0
16	100.8	100.3	101.1	100.7	6.7	10.7	7.4	8.0	12.4	6.5	94	68	93	85	0.6	4.2	0.8	1.9	10	9	4	C 0	C 0,	C 0
17	100.7	101.9	102.8	101.8	8.5	10.5	9.9	9.7	12.9	4.2	88	85	87	87	1.4	1.9	1.6	1.6	4 ⊙	10	6	C 0	NW 3	W 1
18	104.6	104.7	103.7	104.3	6.4	10.5	8.3	8.4	11.4	4.5	78	63	69	70	2.1	4.7	3.5	3.4	9	9	2	NNW 2	C 0	C 0
19	103.2	102.2	100.9	102.1	9.7	15.0	13.9	13.1	16.1	4.8	70	48	63	60	3.5	8.9	5.9	6.1	2 ⊙	9	9	C 0	WNW 4	C 0
20	99.8	97.9	97.7	98.5	12.5	16.9	12.1	13.4	18.4	10.7	71	46	77	65	4.2	10.3	3.2	5.9	10 ⊙	9	6	C 0	SW 2	C 0
21	97.5	97.3	98.2	97.7	10.2	18.7	14.5	14.5	19.6	8.5	93	44	66	68	0.8	12.2	5.7	6.2	10 •	9 ⊙	4	C 0	NNE 4	N 4
22	99.8	99.7	99.7	99.7	8.2	15.3	10.8	11.5	16.3	6.9	92	35	60	62	0.9	11.4	5.3	5.9	10	4	4	N 4	NNE 6	NNW 2
23	101.4	101.4	101.2	101.3	9.2	16.5	15.6	13.2	17.4	5.7	69	40	61	57	3.6	11.4	6.2	7.1	4	5	9	NW 1	NNW 2	C 0
24	102.4	103.4	103.7	103.2	13.5	15.8	12.5	13.6	16.9	11.7	71	54	65	63	4.5	8.3	5.0	5.9	6	10	8	C 0	W 5	C 0
25	104.2	103.0	101.8	103.0	11.8	17.5	14.2	14.4	19.6	7.6	69	47	69	62	4.2	10.7	5.0	6.6	3	6	1	W 2	SE 3	C 0
26	102.2	101.2	99.4	100.9	13.1	20.9	16.2	16.6	22.6	8.7	76	37	60	58	3.6	15.5	7.4	8.8	6	7	0	C 0	NE 2	C 0
27	97.7	96.8	97.8	97.4	16.7	25.2	17.5	19.2	26.1	11.7	59	35	73	56	7.8	20.9	5.5	11.4	0	4	10 •	SE 2	S 4	C 0
28	97.5	96.0	96.9	96.8	16.4	24.6	16.3	18.4	25.1	11.6	72	42	88	67	5.2	17.8	2.3	8.4	0	5	5	SE 2	SSE 5	C 0
29	95.6	93.0	88.2	92.3	11.2	18.7	19.9	17.4	24.7	10.2	94	77	61	77	0.8	5.0	9.1	5.0	9	8 ⊙	4	C 0	ENE 2	E 4
30	86.2	89.3	92.1	89.2	17.0	14.7	13.2	14.5	19.9	13.0	76	85	79	80	4.7	2.5	3.2	3.5	7 ⊙	10	9	ESE 4	SW 5	WSW 1
31	94.3	94.3	94.9	94.5	11.8	18.3	13.6	14.3	19.4	10.3	87	58	72	72	1.8	8.8	4.4	5.0	8	8 ⊙	1	C 0	S 2	C 0
M	100.0	99.6	99.6	99.7	10.4	15.6	12.1	12.5	17.2	8.1	81	56	76	71	2.6	8.6	3.7	5.0	7.2	8.0	6.3	2.0	3.5	1.5

Czerwiec - Juin

1	94.8	94.4	93.5	94.2	14.0	24.8	20.1	19.8	25.6	11.0	79	36	58	58	3.4	20.1	9.7	11.1	7 ⊙	4 ⊙	2	C 0	SW 3	C 0
2	94.0	93.7	94.0	93.9	18.7	26.5	19.2	20.9	26.7	13.6	68	42	65	58	6.9	20.1	7.7	11.6	1 ⊙	6 ⊙	3	ESE 3	E 5	C 0
3	95.0	95.8	96.4	95.7	19.8	26.5	21.3	22.2	27.2	13.9	64	39	67	57	8.3	21.1	8.3	12.6	0 ⊙	3 ⊙	5	ENE 2	NE 4	NE 1
4	98.5	98.5	100.2	99.1	19.0	21.8	17.9	19.2	26.0	16.0	80	65	87	77	4.4	9.5	2.6	5.5	3 ⊙	9 • ☈	4	NE 2	NE 9	NNE 2
5	103.1	104.5	104.8	104.1	18.3	24.8	18.9	20.2	25.2	13.7	73	34	55	55	5.2	20.7	9.9	11.9	2 ⊙	2 ⊙	0	E 6	E 7	C 0
6	105.7	104.4	103.2	104.4	18.5	23.5	18.1	19.6	23.9	11.4	58	43	71	57	8.9	16.5	6.0	10.5	1 ⊙	9 ⊙	10	C 0	E 8	E 5
7	101.3	100.2	98.0	99.8	17.6	21.3	18.2	18.8	23.6	14.6	74	69	86	76	5.1	7.9	2.9	5.3	9 ⊙	9 ⊙	10	ESE 4	SE 5	C 0
8	97.5	97.6	99.1	98.1	17.5	25.1	17.9	19.6	25.7	14.8	88	57	87	77	2.4	13.6	2.6	6.2	2 ⊙	7 ⊙	9	SSE 2	C 0	C 0
9	100.1	101.5	101.1	100.9	16.8	21.1	18.9	18.9	22.6	16.6	97	80	88	88	0.6	4.9	2.5	2.7	10	9 ⊙	2	C 0	C 0	C 0
10	101.3	102.1	101.0	101.5	19.7	27.3	21.1	22.5	27.7	15.0	72	31	61	55	6.3	24.9	9.7	13.6	2 ⊙	9 ⊙	4	C 0	SE 7	C 0
11	101.1	100.8	99.5	100.5	19.0	25.4	16.7	19.4	26.4	14.5	68	42	84	65	7.0	18.9	3.1	9.7	1 ⊙	8 ⊙	9	C 0	SSE 5	C 0
12	99.1	99.0	98.1	98.7	15.8	18.4	17.5	17.3	20.3	15.3	97	78	71	82	0.5	4.7	5.9	3.7	10	9	8	W 5	SW 3	C 0
13	97.8	96.0	93.8	95.9	15.3	21.0	19.5	18.8	22.7	14.0	79	49	65	64	3.7	12.6	7.9	8.1	7	7	10	C 0	SSW 3	E 3
14	92.5	93.8	96.3	94.2	15.7	19.5	13.8	15.7	19.8	13.0	85	56	91	77	2.6	10.0	1.5	4.7	10	9	10 •	SW 3	WSW 8	WSW 6
15	98.7	101.3	102.9	101.0	12.5	15.3	13.1	13.5	16.6	12.2	93	69	79	80	1.0	5.5	3.1	3.2	10 •	9	6	W 7	W 6	WSW 6
16	103.9	105.5	106.2	105.2	11.7	14.4	12.8	12.9	17.2	11.2	95	78	83	85	0.6	3.6	2.6	2.3	10 •	10	2	C 0	WSW 3	C 0
17	106.5	106.7	106.3	106.5	13.1	21.2	18.7	17.9	22.6	10.0	80	47	70	66	3.0	13.5	6.5	7.7	5	7	9	W 5	WNW 6	W 2
18	106.4	104.9	102.2	104.5	16.9	23.9	22.3	21.4	26.6	15.7	65	43	59	56	6.8	16.7	11.1	11.5	9	9	2	W 3	W 5	SW 1
19	103.6	106.1	107.7	105.8	17.3	18.9	16.6	17.4	22.3	16.6	95	73	53	74	1.0	5.9	8.9	5.3	10 •	10	1	W 1	W 2	NW 3
20	112.8	113.0	113.0	112.9	13.7	18.1	14.5	15.2	19.5	10.9	71	39	56	55	4.6	12.6	7.3	8.2	0 ⊙	4 ⊙	0	W 2	NW 4	C 0
21	112.8	110.2	110.4	111.1	15.4	20.7	13.4	15.7	23.2	9.0	60	33	93	62	7.0	16.3	1.1	8.1	1 ⊙	6 ⊙	8 •	SE 2	WSW 1	NW 1
22	113.7	112.0	105.6	110.4	12.3	19.1	19.6	17.6	21.9	10.0	86	51	41	59	2.0	10.7	13.4	8.7	6 ⊙	2 ⊙	2	C 0	SE 1	SE 5
23	102.1	103.9	104.8	103.6	15.4	21.2	17.3	17.9	23.7	15.0	96	66	71	78	0.8	8.6	5.9	5.1	10 •	9	2	C 0	W 4	WSW 2
24	105.3	105.5	107.1	106.0	16.3	22.3	18.0	18.5	23.0	14.0	72	49	59	60	5.3	13.7	8.4	9.1	6 ⊙	6 ⊙	9	WSW 3	WSW 6	W 2
25	104.9	103.6	100.8	103.1	19.0	25.8	23.0	22.7	27.7	16.5	67	39	56	54	7.2	20.2	12.3	13.2	2 ⊙	4 ⊙	3	WSW 5	WSW 5	WSW 2
26	101.1	100.9	100.5	100.8	19.7	27.8	23.5	23.6	28.7	17.5	75	40	67	61	5.7	22.5	9.6	12.6	0 ⊙	7 ⊙	8	C 0	WSW 3	C 0
27	99.5	96.3	96.8	97.5	21.5	32.4	20.7	23.8	33.4	17.5	72	29	81	61	7.1	34.6	4.6	15.4	1 ⊙	5 ⊙	10	SE 3	SW 5	S 2
28	99.8	107.1	112.2	106.4	15.8	15.9	13.9	14.9	22.1	13.9	95	65	64	75	0.9	6.3	5.7	4.3	10	9	1	NW 6	C 0	W 1
29	114.9	115.2	115.1	115.1	13.5	17.5	15.8	15.6	18.5	11.4	82	61	76	73	2.8	7.9	4.3	5.0	9 ⊙	9	2	W 3	W 6	C 0
30	114.6	114.3	112.9	113.9	16.5	23.0	20.0	19.9	25.2	11.7	76	49	59	61	4.6	13.3	9.6	9.2	2 ⊙	8 ⊙	0	C 0	WNW 5	C 0
31																								
M	102.7	103.0	102.8	102.8	16.5	22.2	18.1	18.7	23.9	13.7	79	52	70	67	4.2	13.9	6.5	8.2	5.2	7.1	5.0	2.2	4.3	1.5

Warszawa - Bielany $H_s = 101\,m$ $H_b = 104.7\,m$ $h_w = 16\,m$ **Maj - Mai 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.9	.	-	
2	7	1.3	.	-	▽ r ●° 10⁴⁵–11¹² ▽° p, = n – a
3	7	1.1	.	-	▽° 20³⁰– r, = na
4	8	.	.	-	∞ na
5	7	.	.	-	
6	6	1.6	.	-	▽ a, p, ∞ r – p
7	7	16.9	.	-	▽° 12¹⁵–³⁸ ▽² 16²⁷–⁴⁵ ▽¹ 20⁴⁰– r, (K) 16²⁰–²⁷ K° – 16³⁶
8	8	1.8	.	-	▽° 12⁴⁰–13¹⁵ 13²⁰–⁴⁰
9	7	4.5	.	-	▽° 11²⁵–12³⁵, 17⁴⁵ np
10	8	4.2	.	-	● na 9²⁰, ▽° 13³⁰–⁵⁰ 14²⁵ np
11	7	0.3	.	-	●° na
12	8	0.1	.	-	●° 5⁵⁵–7⁴⁵
13	8	2.0	.	-	●° 19¹⁰– np
14	7	0.1	.	-	●° na ▽° 17²⁰–13⁰⁵
15	9	0.4	.	-	▽° 6³⁰, ⌓° r – a
16	8	1.8	.	-	●¹ na ●° a ●¹ 12⁰⁶ ●⁰⁻¹ 14⁰⁰– p, = r – a
17	7	.	.	-	⌓² r – a, ∞ a – p
18	8	.	.	-	⌓° p – r
19	9	.	.	-	= r – a, ⌓° r – a
20	8	0.1	.	-	= r – a, ⌓° p – r
21	7	0.0	.	-	●° r – 7¹⁰ ▽° 15¹⁰–¹⁵, (K) 11¹⁵– p SSW
22	8	.	.	-	
23	8	.	.	-	
24	7	.	.	-	
25	8	.	.	-	⌓° p – r
26	7	.	.	-	∞ r – a, ⌓° r – a, p – r
27	7	0.3	.	-	▽° 16³⁰–⁵⁰ ●° 20¹⁰– r, ⌓° r – a
28	7	6.7	.	-	●² 17⁰²– 18⁰⁰, K 16⁴⁷–17⁴⁰, ∞ na
29	6	.	.	-	= na – p
30	7	4.2	.	-	●° 9⁰⁰– 11¹⁰
31	6	.	.	-	= na – p, ⌓° np
Σ	–	48.3	–	-	UWAGI

Czerwiec - Juin

1	7	.	.	-	= na – a, ⌓° na, np
2	8	.	.	-	(K) 15¹⁵–²⁵, = na – a, ⌓° na
3	8	.	.	-	= na, ⌓° na
4	9	10.0	.	-	▽° 12²⁵–³⁵ ●⁰⁻¹ 13³⁵–⁵⁵ ▲° 13⁴⁰–⁴⁵ ●¹ 15¹⁵–⁴⁰ ●° – 17⁰⁵, (K) 12⁰⁵–²⁵ K 13²⁰–⁵⁵, 15¹⁰–16⁰⁰ (K) – 19⁵⁰, =, ⌓° na
5	8	.	.	-	=, ⌓° p – r
6	7	4.1	.	-	●² (K) 14²⁸–15⁰⁴ ▽° 20²⁴, ∞ a – p, ⌓¹ r – a
7	7	11.1	.	-	●²·⁰ 16¹⁵–⁴⁸ ●° 17³⁰–19³² ▲¹ 16¹⁸–²¹, (K) 16¹⁰– p, = r – a
8	7	0.3	.	-	▽° 16¹⁵–16⁴⁴, (K) p S-ENE, =, ⌓² r – a ∞ a – p
9	6	.	.	-	= r – r, ⌓° p – r
10	8	0.2	.	-	▽° 13⁴⁶–15⁴² (K) 13¹⁵ SE-NW, =, ⌓² r – a
11	8	0.0	.	-	(K) 16²⁰ SE-NW, 19¹⁰ NW-E, =, ⌓¹ r – a, ⌒ 17³⁰
12	7	0.8	.	-	●° p, = r – a
13	7	.	.	-	● r
14	7	3.6	.	-	●° p – r ●° 19³⁰–20¹⁰, = r – a, p – r
15	7	1.5	.	-	●° r a, = r – a
16	7	0.6	.	-	●, ● a, = na
17	8	.	.	-	∞ p – r
18	7	0.3	.	-	
19	8	0.0	.	-	●° 6³⁰–8³⁵, 14¹⁵–15¹⁰, = na
20	8	.	.	-	
21	8	5.8	.	-	●¹ 20²⁵–21⁵⁰, K 20³⁵–⁴⁵, ≫ 20²⁰–³⁰
22	8	6.5	.	-	= na, ⌓° na
23	8	0.1	.	-	●° na – 8²⁵ ▽° 13²⁰–³⁰, 13⁴⁰–⁵⁵, = na
24	7	.	.	-	= na
25	6	.	.	-	= na – a
26	7	.	.	-	= r – r
27	7	15.5	.	-	●° 18⁰⁶ ●¹ 18¹⁴–¹⁹ ●° – 18²⁵ ●¹ 19⁰⁷, (K) 17³⁴ W-E, =, ⌓° r – a
28	9	4.2	.	-	●¹ r – a
29	8	.	.	-	=, ⌓° p – r
30	7	.	.	-	
31					
Σ	–	64.6	–	-	UWAGI

Warszawa - Bielany — φ = 52°17' — λ = 20°58' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			POGODA w			KIERUNEK I PRĘDKOŚĆ WIATRU D, v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	115.8	113.2	111.7	112.9	16.9	23.5	19.1	19.6	25.6	13.2	79	39	68	62	4.0	17.7	7.2	9.6	0 ⊙	6 ⊙	0	C	O	C	O	C	O
2	111.5	110.2	108.4	110.0	20.3	28.0	23.3	23.7	28.9	16.3	60	37	57	51	9.6	25.6	12.2	15.1	0 ⊙	0 ⊙	0	C	O	SSW	3	C	O
3	108.3	107.3	101.4	105.7	22.3	29.9	25.7	25.9	31.5	16.3	61	34	38	44	10.5	28.0	20.3	19.6	0 ⊙	3 ⊙	3	C	O	WSW	1	S	2
4	101.1	98.9	95.4	98.5	18.5	25.7	17.6	19.4	25.7	17.6	82	62	90	78	3.9	11.1	2.0	5.7	8 ⊙	9 ⊙	10 • R	NW	2	WSW	4	NW	6
5	98.7	101.2	101.9	100.6	14.5	16.9	14.3	15.0	18.4	14.2	76	47	58	61	3.6	10.1	6.8	6.8	10	8	3	WSW	5	WSW	5	C	0
6	103.7	104.7	105.6	103.7	11.6	14.8	12.6	12.9	17.1	8.8	72	58	91	74	3.7	7.0	1.4	4.0	1 ⊙	9	5	W	3	SSW	3	WSW	5
7	108.1	108.9	108.8	108.6	11.6	15.4	13.5	13.5	17.6	9.8	95	68	66	76	1.0	5.7	5.3	4.0	10	8	8	WSW	3	WSW	6	WSW	3
8	109.0	108.3	105.3	107.5	12.5	18.8	16.8	16.2	21.5	10.2	71	46	56	58	4.2	11.7	8.4	8.1	9	9	1	WSW	2	WSW	4	SW	2
9	100.2	96.7	97.6	98.2	15.4	22.8	14.4	16.8	23.9	12.2	61	58	86	62	6.9	17.2	2.4	8.8	0 ⊙	9	5	SSE	5	S	5	W	3
10	98.3	98.7	100.0	99.0	12.6	16.3	13.5	14.0	18.3	10.5	91	64	73	76	1.4	6.7	4.2	4.1	10	9 •	5	WSW	5	W	3	W	5
11	102.2	101.6	101.6	101.8	13.8	19.8	16.8	16.8	20.8	10.9	72	52	68	64	4.4	11.2	6.1	7.2	2 ⊙	9	1	WSW	5	SSW	6	C	0
12	99.5	97.4	96.9	97.9	13.7	25.9	19.6	19.2	25.7	10.9	99	59	83	80	0.2	12.2	3.9	5.4	10 •	6 ⊙	0	C	0	SW	2	NE	1
13	92.8	89.7	84.9	89.1	19.1	28.4	19.9	21.8	29.0	15.0	83	47	84	71	3.8	20.4	3.7	9.3	8 ⊙	2 ⊙	10 • R	E	3	ESE	8	SSE	9
14	90.4	95.2	98.2	94.6	16.3	16.8	14.6	15.6	19.9	14.5	79	57	73	70	3.8	8.2	4.5	5.5	5 ⊙	9	4	WSW	5	WSW	8	C	0
15	98.3	98.9	100.2	99.1	15.1	19.5	16.1	16.7	21.9	13.0	70	70	82	74	5.1	6.9	3.1	5.0	9 ⊙	9 •	1	SE	2	SW	1	C	0
16	98.9	95.1	98.0	97.3	15.2	16.6	14.1	15.0	17.6	13.2	85	93	87	88	2.6	1.4	2.2	2.1	10 •	10 •	1	S	2	ENE	1	WNW	2
17	96.6	96.2	95.6	96.1	15.1	21.4	14.5	16.4	22.5	11.2	87	47	79	71	2.3	13.5	3.4	6.4	8 ⊙	8 ⊙	8	C	0	SW	5	W	3
18	94.6	95.2	95.2	95.0	13.3	15.1	14.5	14.4	17.5	10.9	87	82	89	86	2.0	3.2	1.8	2.3	9	10	9 •	SW	3	SW	6	WSW	1
19	96.8	96.9	97.5	97.1	14.1	20.1	14.8	16.0	20.5	11.5	87	58	83	76	2.2	9.9	2.9	5.0	1 ⊙	9 ⊙	3	SW	2	C	0	C	0
20	98.7	99.1	99.2	99.0	13.7	20.7	16.1	16.6	22.4	11.2	89	51	72	71	1.8	11.9	5.1	6.3	2 ⊙	9 ⊙	9	C	0	C	0	W	3
21	99.5	99.4	99.1	99.3	13.9	18.2	15.1	15.6	19.2	11.9	90	70	84	81	1.6	6.2	2.8	3.5	9 ⊙	9 ⊙	9	W	2	SW	6	SW	5
22	98.1	98.7	100.1	99.0	14.1	19.5	15.8	15.3	20.1	13.9	93	64	89	82	1.1	8.3	1.8	3.7	10	9 ⊙	9	W	4	W	5	SW	2
23	102.1	103.3	105.0	103.5	13.6	16.4	14.7	14.8	17.6	12.5	89	73	86	83	1.8	5.1	2.4	3.1	10	10	9	SW	4	SW	6	WSW	2
24	106.9	108.5	109.8	108.4	13.3	16.2	14.6	14.7	18.9	12.6	88	65	75	76	1.8	6.5	4.1	4.1	9	10	9	W	1	W	5	WSW	3
25	111.9	112.0	111.5	111.8	12.2	16.5	14.3	14.3	17.2	9.5	89	69	77	78	1.5	5.9	3.8	3.7	9	10	9	SW	2	W	3	W	2
26	108.7	106.8	101.8	105.8	15.1	18.6	18.7	17.5	21.3	9.7	82	65	67	71	2.8	7.4	7.1	5.8	9	9	10	SW	2	SW	3	S	1
27	98.2	96.1	95.1	96.5	16.6	24.5	20.5	20.5	25.4	15.0	76	52	66	65	4.6	14.8	8.1	9.2	9 ⊙	8 ⊙	9	SW	1	SW	2	SW	5
28	95.1	92.9	94.2	94.1	16.8	19.5	16.6	17.4	21.6	16.2	87	83	87	86	2.5	3.9	2.5	3.0	9 ⊙	10	9	SW	2	S	2	C	0
29	95.5	100.0	102.7	99.4	15.1	16.1	15.3	15.0	18.7	12.9	98	77	82	86	0.4	4.2	3.2	2.6	10 •	9 ⊙	9	NW	2	W	3	C	0
30	104.2	104.0	103.1	103.8	12.6	13.5	12.7	12.9	15.5	12.6	91	95	99	95	1.4	0.7	0.2	0.8	10 •	10 •	10 •	NW	1	WNW	3	NNW	2
31	98.0	97.3	99.9	98.4	13.7	16.4	13.4	14.2	16.7	12.6	99	72	93	88	0.2	5.2	1.1	2.2	10 •	9	10 •	E	2	SE	8	SSW	3
M	101.3	101.0	100.8	101.0	14.8	19.6	16.2	16.7	21.2	12.6	85	61	77	74	3.1	9.9	4.6	5.9	7.0	8.2	6.1	2.2		3.8		2.3	

Sierpień – Août

1	101.2	103.5	104.8	103.2	12.5	13.7	14.7	13.9	16.9	12.3	88	89	84	87	1.7	1.8	2.7	2.1	10 •	10 •	1	SW	7	WSW	8	SW	1
2	104.6	103.2	101.4	103.1	15.3	24.1	21.5	20.6	25.6	12.3	73	48	54	58	4.8	15.5	11.8	10.7	1 ⊙	2 ⊙	7	C	0	SSE	3	SSE	3
3	103.7	104.3	107.2	105.1	16.2	19.8	14.8	16.4	21.6	14.8	90	66	75	77	1.7	7.9	4.1	4.6	10	9 ⊙	2	W	2	W	3	W	3
4	109.0	107.4	104.8	107.1	11.8	19.0	16.8	16.1	20.2	10.0	88	50	64	67	1.6	11.1	6.8	6.5	1 ⊙	7 ⊙	9	W	1	WSW	4	SW	1
5	103.7	104.6	103.9	104.1	16.7	21.2	18.0	18.5	22.7	15.0	85	63	83	76	2.9	9.8	3.4	5.4	5 ⊙	9 ⊙	0	WSW	5	WSW	3	C	0
6	101.6	100.0	98.2	99.9	18.9	29.5	22.6	23.4	30.7	15.5	78	41	76	65	4.7	24.2	6.5	11.8	1 ⊙	2 ⊙	2	SSW	1	SW	3	C	0
7	98.8	100.1	102.4	100.4	22.4	25.5	19.0	21.5	26.5	19.0	66	57	87	70	9.3	14.0	3.0	8.8	4 ⊙	8 ⊙	9	SW	2	N	3	W	3
8	107.0	106.9	105.3	106.5	15.4	21.9	20.5	19.6	25.9	14.5	80	58	59	59	3.5	16.4	9.9	9.9	2 ⊙	3 ⊙	10	C	0	N	2	SE	2
9	105.8	106.8	108.3	107.0	18.6	27.6	22.3	22.7	28.7	14.7	82	45	74	67	3.9	20.5	6.9	10.4	3 ⊙	2 ⊙	10	SE	1	W	3	NW	2
10	109.5	108.0	104.0	107.2	17.4	25.7	22.2	21.9	26.8	17.0	75	56	83	71	4.9	14.4	4.7	8.0	9	9 ⊙	2	NNE	3	SE	3	E	2
11	102.2	101.1	103.3	102.2	19.5	22.3	18.3	19.6	25.6	17.8	92	80	95	89	1.8	5.4	1.0	2.7	9	10	10	C	0	N	1	W	5
12	104.5	104.0	103.3	103.9	16.7	21.1	15.5	17.2	22.3	15.5	92	67	95	85	1.6	8.3	0.9	3.6	9	9 ⊙	10 •	NW	1	C	0	C	0
13	103.9	105.9	108.1	106.0	14.2	16.6	14.2	14.8	16.9	14.2	93	65	81	80	1.1	6.6	3.1	3.6	10	9	8	NW	1	NW	2	W	3
14	109.4	108.4	105.9	107.9	12.6	18.1	15.0	15.2	18.9	10.1	86	53	80	73	2.1	9.9	3.4	5.1	3	9	2	WSW	1	SW	2	C	0
15	102.1	100.5	99.0	100.5	13.4	16.9	15.1	15.1	20.0	10.4	81	81	86	83	3.0	3.7	2.5	3.1	6	9	8	SSW	1	SSW	4	SW	4
16	97.3	98.2	96.2	97.2	14.0	16.3	14.2	14.7	17.4	13.8	86	60	75	73	2.2	7.4	4.4	4.7	10	9	10	SW	4	WSW	5	C	0
17	95.2	95.9	96.4	95.8	12.5	15.1	12.6	13.2	16.6	11.0	88	70	82	80	1.7	5.1	2.6	3.1	10	9	3	SW	3	WSW	4	C	0
18	95.5	94.4	94.3	94.7	10.4	17.5	13.0	13.5	17.8	9.2	97	61	89	82	0.3	7.9	1.6	3.3	8	9	8 •	W	2	WNW	6	W	5
19	93.6	92.0	92.6	92.7	12.6	16.1	14.3	14.3	18.6	11.0	88	79	87	85	0.7	5.8	2.2	2.2	8	10	4	WSW	4	WSW	7	SW	5
20	93.1	94.5	97.4	95.0	13.7	16.8	13.3	14.3	17.7	12.1	83	69	88	80	2.7	5.9	1.8	3.5	9	8	0	SW	6	WSW	4	W	4
21	98.7	99.9	100.1	99.6	13.5	15.3	16.7	15.6	17.7	12.3	87	81	79	82	2.0	3.4	4.1	3.2	10	10	8	W	7	W	6	W	2
22	97.8	95.8	94.9	96.2	13.7	21.7	14.1	16.4	22.7	14.1	79	58	91	76	3.7	11.0	1.5	5.4	2	9 •	2	SSW	2	SW	5	SSW	3
23	96.2	96.3	99.6	97.4	13.4	17.0	13.1	14.2	17.8	12.4	86	76	88	83	2.1	4.7	1.8	2.9	10	9	9	WSW	5	WSW	7	WSW	5
24	101.2	103.2	104.8	103.1	10.9	15.1	13.0	13.0	16.9	10.7	90	74	81	82	1.3	4.4	2.8	2.8	10	7	10	W	3	W	5	W	3
25	103.9	104.2	103.1	104.4	13.8	16.7	14.1	14.7	18.3	12.5	83	74	91	83	2.7	5.0	1.3	3.1	8	10 •	5	SW	4	WSW	6	WSW	3
26	107.4	109.1	109.4	108.6	12.1	15.7	14.9	14.4	16.5	11.0	83	64	84	77	2.3	6.4	2.7	3.8	9	10 •	10	W	1	W	3	C	0
27	109.4	110.1	109.3	109.7	16.2	25.3	19.9	19.8	24.9	14.3	94	60	76	77	1.2	11.6	5.5	6.1	3	6	9	C	0	WNW	4	WSW	3
28	112.1	112.4	113.3	112.6	16.1	21.2	15.1	16.9	21.7	15.0	92	58	82	77	1.6	10.6	3.2	5.1	9	5	5	W	2	W	4	C	0
29	112.1	111.3	111.3	111.7	14.3	19.3	14.8	15.8	20.1	12.9	91	68	78	79	1.5	7.2	3.6	4.1	6	8	2	W	4	WNW	6	NW	1
30	113.3	114.0	114.0	113.8	10.2	18.3	13.8	14.1	21.0	8.9	99	56	83	79	0.1	9.5	2.7	4.1	10 =	3	0	NNE	1	NNE	3	C	0
31	116.3	117.1	117.5	117.0	12.4	22.3	18.1	17.7	23.8	9.3	89	48	80	72	1.6	13.9	4.1	6.5	0	0	0	C	0	C	0	C	0
M	105.6	105.7	105.8	105.7	14.6	19.7	16.3	16.7	21.1	13.0	86	63	81	77	2.3	9.3	3.8	5.2	6.6	7.4	5.6	2.4		3.8		2.0	

Warszawa - Bielany — $H_s = 101\,m$ — $H_b = 104{,}7\,m$ — $h_w = 16\,m$ — Lipiec - Juillet 1961

DNI	WIATR DZIAŁALNOŚĆ v	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	= n – a ; ⌒² n – a ⌒° p – n
2	8	.	.	-	= p – n ; ⌒° n – a , p – n
3	7	.	.	-	= na
4	6	2.9	.	-	▽•° 15^{20-30} •° 20^{05} np , ↘ 19^{55} 20^{40} , = na – a
5	9	.	.	-	
6	9	1.0	.	-	▽•° 10^{40-45} 11^{20-35} 17^{20} 19^{40} , 23^{10-25}
7	9	0.2	.	-	▽•° 7^{40} 8^{05} , 12^{20} 13^{20} , = na – a , ⌒⁸ na
8	9	.	.	-	
9	8	0.1	.	-	•° 14^{00} 15^{20} , 18^{10} 20^{20} , = na – a
10	9	3.5	.	-	•° 7^{50} 8^{35} , 11^{25} 12^{15} , 13^{35} 14^{10}
11	7	6.1	.	-	= np
12	6	0.1	.	-	•° 5^{30} 7^{45} , = na – np
13	8	1.8	.	-	•° 21^{20-45} , ↘ 21^{30-40} , = na – a , ⌒° na
14	8	.	.	-	
15	7	1.8	.	-	•° 9^{35} 10^{45} , 13^{30-50} , 14^{25-30} , = na ; ⌒° np
16	6	8.4	.	-	•⁰⁻¹ 7^{10} 10^{40} , 13^{20} 14^{45} , = na
17	9	0.3	.	-	▽•° 19^{05}
18	7	2.8	.	-	▽•° 9^{53} ▽•¹ 13^{43} 14^{33} 15^{00} 18^{06} •⁰⁻² 21^{30} 22^{30} , = p – n
19	7	9.8	.	-	•² 14^{02-40} •° 15^{30} p , (↘) 14^{03} ↘ 14^{21-30} (↘) – p , = n – np , ⌒² n – a
20	7	.	.	-	= , ⌒² n – a
21	7	2.4	.	-	▽•° p , = n – p , ⌒° n – a
22	8	1.3	.	-	•² na ▽•¹ p • 15^{25} , (↘) p W-E
23	7	.	.	-	= a – p
24	7	.	.	-	
25	8	0.0	.	-	
26	6	.	.	-	•° n , = n – p
27	7	0.4	.	-	▽•° 18^{05} ▽•¹ 18^{45} , = n – p
28	7	19.9	.	-	•° 9^{50} ▽•¹ 11^{05} 12^{10} •° – p •² 16^{03-10} •¹⁻⁰ 16^{16} ⌒¹ np , = n – p
29	7	0.7	.	-	•¹ np – a •° a
30	6	12.1	.	-	•° n – n
31	9	4.3	.	-	•° na – 9^{50} 18^{10} np , ≡° 5^{10} – 6^{25} = a
Σ	–	79.9	–	-	UWAGI.

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1	5	0.6	.	-	•° na – 15^{10} , = na – a
2	6	.	.	-	= na – a , ⌒² na – a
3	6	.	.	-	= na – a ⌒² na – a
4	7	0.0	.	-	•° 17^{40} 19^{20} , = na , np , ⌒² na ⌒° np
5	6	.	.	-	= na – np , ⌒° na , np
6	8	.	.	-	= na , ⌒° na , np
7	7	0.2	.	-	▽•° 15^{02} p , = na – a , ⌒° p – n
8	7	.	.	-	= ⌒² n – a
9	7	0.0	.	-	•¹ np , = n – a ∞ a – p , ⌒° n – a
10	7	16.7	.	-	•¹ np ; ∞ a – p , ⌒° p – n
11	6	13.0	.	-	•² na ↘ na •²(↘) 16^{00} 17^{02} ▽•² p ; = n – p
12	7	7.0	.	-	• na •° p •¹ 20^{10} – n ; = n – a
13	8	0.0	.	-	• n – a ; = n – a
14	8	.	.	-	⌒² n – a ⌒° p – n
15	8	0.5	.	-	•° 10^{36} 13^{10} ▽•° 15^{45-54} 20^{25} 21^{15} , ⌒² n – a
16	7	0.5	.	-	•¹ 7^{50} p
17	8	0.0	.	-	▽•° a , ⌒² p – n
18	8	1.5	.	-	▽•° 13^{47-52} ▽•¹ 16^{19-34} ▽•° 17^{01-14} ▽•² 21^{34-40} , = n – a , ⌒° n – a
19	7	2.0	.	-	▽•° a – p
20	7	1.6	.	-	▽•° 14^{20-35} , 15^{54} 16^{05} , (↘) 16^{45}
21	7	0.4	.	-	•° a , p
22	7	4.4	.	-	•° a , p ▽•² 18^{43-58} , ↘° 18^{43-51} , ⌒² n – a
23	7	5.6	.	-	▽•¹ a – p
24	7	0.0	.	-	▽• 7^{43-48} 21^{05-30}
25	6	0.1	.	-	•° 13^{15-40} ▽•° 15^{06-20} , = n – a ∞ a – p , ⌒° p – n
26	8	4.0	.	-	•° a p ⌒² np , n – a
27	7	.	.	-	= n – a , ⌒° n – np
28	7	.	.	-	⌒° n – a
29	7	.	.	-	= n – a ; ⌒² n – a ⌒¹ p – n
30	8	.	.	-	≡¹ n – a , ⌒² n – a
31	8	.	.	-	= n – a ; ⌒¹ n – a
Σ	–	58.1	–	-	UWAGI.

Warszawa - Bielany φ = 52°17' λ = 20°58' Wrzesień – Septembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE e			POGODA N.w			KIERUNEK I PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	117.8	117.0	115.0	115.9	15.8	25.9	17.7	19.3	26.4	13.0	91	55	81	75	1.5	15.8	3.8	7.0	0	2	0	C 0	SW 2	C 0
2	111.4	109.8	106.2	109.1	17.5	27.0	21.6	21.9	28.7	13.5	74	43	63	60	5.1	20.4	9.5	11.7	2	1	0	SW 2	SW 2	C 0
3	103.1	101.4	99.1	101.2	18.5	27.9	21.7	22.4	29.0	16.8	64	32	57	51	7.6	25.7	11.2	14.8	0 ⊙	0 ⊙	10 •	SW 3	WSW 5	C 0
4	98.4	101.0	103.2	100.9	17.5	22.0	16.4	18.1	22.7	15.3	80	57	77	71	4.0	11.2	4.2	6.5	6	1	0	W 4	NNE 3	NNE 2
5	102.8	102.4	99.4	101.5	14.7	22.3	17.4	18.0	24.0	12.3	81	52	75	69	3.1	12.9	4.9	7.0	8	1 ⊙	0	ESE 2	E 4	E 4
6	95.3	94.9	95.0	95.1	17.3	22.8	17.5	18.8	23.4	16.2	81	65	95	80	3.7	9.6	1.0	4.8	9 ⊙	9	10 •	SE 3	C 0	WSW 2
7	94.5	94.4	95.5	94.1	15.3	19.4	16.2	16.8	20.4	14.5	92	73	80	82	1.3	6.0	3.6	3.6	5 ⊙	9	1	WSW 1	SW 4	SW 6
8	94.6	96.3	97.1	96.0	12.3	14.4	12.2	12.8	16.2	11.6	72	64	89	75	4.0	6.0	1.5	3.8	10	10	10 •	WSW 7	W 7	WSW 6
9	99.4	101.3	102.1	100.9	12.3	16.7	13.4	14.0	17.7	12.1	85	60	77	74	2.2	7.7	3.5	4.5	9	8	1	W 3	W 5	W 3
10	102.9	104.3	105.0	104.1	11.7	15.6	12.4	12.5	14.0	11.4	88	98	80	89	1.6	0.4	2.9	1.6	10	10 •	10	W 3	W 5	WSW 4
11	105.0	104.9	103.6	104.5	11.6	13.7	14.3	13.5	15.4	11.4	95	81	75	84	0.6	3.0	4.1	2.6	10	10	9	W 2	WSW 4	SW 2
12	102.0	100.8	100.6	101.1	11.5	18.6	13.5	14.3	20.6	10.8	76	52	95	74	3.3	10.3	0.7	4.8	4 ⊙	7 ⊙	9	SW 3	SW 5	WSW 2
13	101.4	103.5	103.6	102.8	12.4	15.6	14.4	14.2	18.3	12.2	92	58	78	76	1.2	7.4	3.6	4.1	9	7	9	W 3	NW 5	C 0
14	101.4	99.8	98.6	99.9	13.8	17.3	16.5	16.0	19.0	12.5	84	82	89	85	2.5	3.5	2.2	2.7	10	10	6	S 2	SW 3	SSW 2
15	98.3	104.8	108.6	103.9	15.3	15.9	12.4	14.0	17.3	12.4	80	70	87	79	3.5	5.4	1.9	3.6	10 •	9 •	4	W 9	WNW 6	WSW 3
16	109.0	109.4	109.8	109.4	13.0	20.8	17.9	17.4	22.9	11.5	89	75	89	84	1.6	6.2	2.2	3.3	10 •	9 ⊙	0	W 3	NW 3	C 0
17	110.1	109.7	108.8	109.5	15.7	27.2	21.8	21.6	28.2	14.5	85	46	63	65	2.6	19.6	9.7	10.6	0 ⊙	0 ⊙	0	SW 1	SSW 3	S 3
18	107.8	106.7	108.4	107.6	17.3	26.2	18.1	19.9	26.4	16.7	72	54	78	68	5.4	15.6	4.7	8.6	6 ⊙	5 ⊙	0	SW 3	SW 3	N 1
19	110.6	110.6	111.0	110.7	10.7	18.1	13.5	14.0	18.4	10.3	87	53	74	71	1.7	9.7	4.0	5.1	0 ⊙	1 ⊙	0	W 2	NW 4	NW 2
20	113.1	113.5	113.7	113.4	7.7	16.6	11.2	11.7	17.3	7.0	97	51	80	76	0.3	9.2	2.6	4.0	3 ⊙	2 ⊙	0	NW 2	E 3	ENE 1
21	114.8	115.3	116.5	115.5	6.9	15.8	9.0	10.2	16.5	5.9	96	45	76	72	0.4	9.7	2.8	4.3	2 ⊙	3 ⊙	0	C 0	NE 3	NE 2
22	118.1	118.7	118.6	118.5	4.4	15.0	8.9	9.3	16.1	2.7	90	47	72	70	0.9	9.0	3.2	4.4	0 ⊙	0 ⊙	0	ENE 2	E 4	E 2
23	118.6	117.5	115.2	117.1	4.7	16.7	8.3	9.5	17.0	3.0	84	23	67	58	1.3	14.6	3.6	6.5	2 ⊙	0 ⊙	0	E 1	ESE 4	E 2
24	113.3	111.9	110.6	111.9	4.1	19.1	11.1	11.4	20.1	2.2	80	32	72	61	1.6	14.9	3.7	6.7	1 ⊙	5 ⊙	0	E 1	SE 3	SE 1
25	109.4	108.7	108.3	108.8	6.6	22.3	16.4	15.4	23.2	5.5	96	33	69	66	0.4	17.9	5.8	8.0	0 =	4	10	C 0	WSW 4	WNW 5
26	111.2	111.2	109.8	110.7	9.7	15.4	9.0	10.8	16.8	9.0	95	48	83	75	0.6	9.2	2.0	3.9	5	6	4	W 4	NW 5	NW 2
27	108.4	107.8	107.7	108.0	8.9	16.0	9.7	11.1	17.0	8.3	85	48	79	71	1.7	9.6	2.5	4.6	4	5	5	C 0	NW 2	C 0
28	109.2	110.1	111.1	110.1	5.9	17.7	10.3	11.0	18.3	5.1	94	43	80	72	0.6	11.6	2.5	4.9	2	2	4	C 0	ESE 1	SE 1
29	112.2	111.4	111.2	111.6	7.8	17.4	11.5	12.0	18.3	6.2	93	47	85	75	0.8	10.5	2.0	4.4	8	6	0	C 0	ESE 5	ESE 4
30	110.8	110.3	110.6	110.6	8.9	16.3	9.8	11.2	17.1	8.3	90	54	81	75	1.1	8.4	2.3	3.9	9	9	0	ESE 5	ESE 6	E 4
31																								
M	106.8	107.0	106.7	106.8	11.7	19.1	14.1	14.8	20.2	10.4	86	55	78	73	2.2	10.7	3.7	5.5	5.1	5.0	3.4	2.4	3.8	2.2

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1	112.0	112.6	114.5	113.0	6.1	11.5	11.5	10.2	12.9	4.4	100	77	88	88	0.0	3.2	1.7	1.6	10 =	10	5	E 6	E 3	NNE 4
2	116.0	117.1	117.8	117.0	8.4	15.5	11.1	11.5	16.9	7.1	100	68	90	86	0.0	5.7	1.3	2.3	10 =	5 ⊙	0	NE 2	E 6	E 2
3	118.4	118.3	117.8	118.2	6.1	17.0	10.3	10.9	17.9	5.1	98	50	82	77	0.1	9.7	2.2	4.0	0 ⊙	3 ⊙	0	E 2	E 7	E 2
4	117.2	117.0	116.3	116.8	8.3	19.6	11.7	12.8	19.9	7.6	93	37	66	65	0.8	14.3	4.7	6.6	0 ⊙	1 ⊙	0	E 3	ESE 7	E 3
5	115.6	115.2	115.4	115.4	9.2	19.3	12.4	13.3	19.6	8.9	79	39	58	59	2.4	13.7	6.1	7.4	0 ⊙	0 ⊙	0	ESE 5	ESE 8	SE 4
6	114.3	112.9	111.0	112.7	7.2	18.4	11.5	12.2	19.3	6.6	86	45	76	69	1.5	11.8	3.3	5.5	0 ⊙	0 ⊙	0	ESE 5	SE 7	ESE 6
7	107.5	105.6	103.3	105.5	7.4	15.7	12.7	12.1	16.9	7.2	73	38	49	53	2.8	11.0	7.6	7.1	0 ⊙	0 ⊙	6	E 8	ESE 9	ESE 6
8	102.1	102.4	103.3	102.6	7.1	15.1	11.9	11.5	16.5	7.1	66	45	51	54	3.5	9.5	6.7	6.6	2 ⊙	4 ⊙	0	ESE 9	SE 7	ESE 5
9	107.9	112.9	116.4	112.4	7.3	12.4	9.7	9.8	12.6	7.2	80	87	97	88	2.0	1.9	0.3	1.4	8 ⊙	10	0	SE 1	W 2	W 2
10	119.1	120.1	119.1	119.4	5.5	12.5	8.7	8.8	14.3	4.5	100	86	97	94	0.0	2.1	0.3	0.8	10 =	10	0	C 0	C 0	C 0
11	118.4	116.2	114.6	116.4	6.5	16.9	12.5	12.1	17.4	5.8	100	47	58	68	0.0	10.1	6.1	5.4	10 =	0 ⊙	0	SE 5	SE 7	SE 3
12	113.0	112.9	114.3	113.4	6.5	15.7	13.2	12.2	17.4	6.1	76	69	83	76	2.3	5.5	2.6	3.5	8 ⊙	7 ⊙	9	S 2	C 0	N 2
13	114.3	115.1	115.0	114.8	6.2	13.2	7.5	8.6	14.1	6.2	97	65	89	84	0.3	5.3	1.2	2.3	7 ⊙	7 ⊙	1	NW 2	NW 5	W 3
14	113.2	111.8	110.6	111.9	5.2	9.4	10.5	8.9	10.6	4.0	100	87	97	95	0.0	1.6	0.3	0.6	10 =	10	10	W 5	W 3	NW 2
15	111.1	110.2	108.2	109.8	9.7	11.3	10.6	10.6	11.7	9.6	97	83	77	86	0.3	2.3	2.9	1.8	9	10	10	W 2	W 3	W 5
16	107.2	106.8	103.8	105.9	9.5	12.3	8.0	9.4	12.9	7.8	87	70	84	80	1.6	4.3	1.6	2.5	10	9	0	W 2	W 3	C 0
17	100.5	97.6	91.1	96.4	8.2	11.9	12.0	11.0	12.9	6.9	87	78	74	80	1.4	3.0	3.6	2.7	10 =	10 •	5	C 0	S 2	SSE 5
18	83.1	83.2	84.3	83.5	12.6	15.1	16.6	15.2	16.9	9.8	73	56	41	57	5.9	7.5	11.2	7.5	10 •	10 •	8	SSE 7	SE 9	SE 8
19	86.4	88.8	92.3	89.2	15.9	20.5	16.8	17.5	22.3	14.7	46	37	55	46	9.9	15.3	8.6	11.3	9	8	3	SE 8	SE 6	SSE 6
20	96.5	98.7	101.0	98.7	10.1	20.3	12.8	14.0	20.7	9.6	90	51	85	75	1.3	11.7	2.3	5.1	2	0	0	E 2	E 4	E 3
21	101.5	103.5	108.0	104.3	10.6	15.7	11.0	12.1	15.9	10.5	79	61	83	74	2.8	6.9	2.3	4.0	0	3	1	ESE 6	SE 8	SE 4
22	111.3	113.8	114.6	113.2	9.3	10.9	9.3	9.7	11.3	8.5	88	71	43	67	1.4	3.7	6.7	3.9	10	10	8	ESE 2	ESE 6	ESE 5
23	114.3	114.5	113.4	114.1	3.5	10.5	9.6	8.3	11.1	3.5	63	51	58	57	2.8	6.2	5.1	4.7	3 ⊙	6 ⊙	9	ESE 5	E 6	SE 2
24	112.4	112.7	111.0	112.0	6.2	12.5	10.8	10.1	13.6	5.8	80	70	75	75	1.9	4.4	3.3	3.2	8 ⊙	10 •	8	SE 3	SSW 1	SSW 2
25	107.8	106.1	105.5	106.5	6.0	15.2	12.6	11.6	16.3	6.0	89	47	67	68	1.1	9.1	4.9	5.0	2 ⊙	8 ⊙	10	SE 3	S 4	SSW 4
26	105.1	104.7	103.5	104.4	10.7	13.5	10.7	11.4	14.5	10.6	73	59	64	65	3.6	6.3	4.6	4.8	10	10	0	S 3	S 3	S 3
27	102.4	101.3	99.8	101.2	8.3	13.7	11.4	11.2	15.2	8.0	71	54	52	59	3.2	7.2	6.5	5.6	9	8 ⊙	2	SE 4	ESE 5	SSE 3
28	100.5	100.8	100.6	100.6	8.8	17.5	10.7	11.9	18.0	8.5	71	54	85	70	3.3	9.1	2.0	4.8	7	4 ⊙	0	S 2	SSW 1	C 0
29	99.2	99.1	99.8	99.4	5.3	9.9	8.3	8.0	10.9	3.4	94	74	97	88	0.6	3.1	0.4	1.4	9 ⊙	10	10 •	S 1	ESE 2	WNW 2
30	104.7	105.6	105.7	105.3	7.4	8.4	6.5	7.2	8.9	5.5	100	89	99	96	0.0	1.2	0.2	0.5	10 =	10	0	W 2	SW 2	SW 2
31	106.4	105.9	104.5	105.6	4.7	11.9	10.1	9.2	12.6	4.4	97	72	76	82	0.2	3.9	3.0	2.4	3 =	8	3	SW 1	SW 3	WSW 4
M	107.7	107.9	107.6	107.7	7.9	14.3	11.1	11.1	15.2	7.1	85	62	74	74	1.8	6.8	3.7	4.1	6.3	6.5	3.5	3.5	4.5	3.2

Warszawa - Bielany $H_s = 101\,m$ $H_b = 104{,}7\,m$ $h_w = 16\,m$ Wrzesień - Septembre 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	
2	7	.	.	-	$\frown^0 n-a \quad \frown p-n$
3	7	0.6	.	-	$\bullet^0 20^{00}$ np. $= n-a$, $\frown^0 n-a$
4	7	.	.	-	$\frown^0 p-n$
5	8	.	.	-	$= na$, np. $\frown^1 na$
6	6	4.1	.	-	$\bullet^0 15^{00}-19^{25} \quad 19^{40}$ np. $= na-np$. $\frown^0 na$
7	6	0.2	.	-	$\bullet^0 15^{00}$ p. $= na-p$, $\frown^2 na$
8	7	0.0	.	-	$\bullet^0 19^{40}$ np. $= na$
9	8	.	.	-	
10	7	0.4	.	-	$\bullet^0 a$, $= na$
11	6	.	.	-	$\bullet^0 6^{30}-7^{20} = a$
12	6	6.0	.	-	$\bullet^0 18^{50}-20^{05}$, $= na-a$
13	8	0.0	.	-	$\bullet^0 8^{30-45}$, $= na-a$
14	5	11.1	.	-	$\bullet^0 11^{50}-13^{15}$ $\bullet^{0-1}$ np. $= na-a$, $\frown^2 na$, $\frown^0 np$
15	9	0.4	.	-	$\bullet^0 7^{30}-8^{50} \quad 13^{35-45} \quad 15^{00-35}$
16	6	.	.	-	$\bullet^0 6^{20}-7^{35}$, $= na-np$, $\frown^2 np$
17	7	.	.	-	$= na$, $\frown^2 na$ $\frown^0 np$
18	6	.	.	-	$= n-a \quad \infty a-p$, $\frown^0 n-a$, $p-n$
19	8	.	.	-	$\frown^1 n-p$
20	9	.	.	-	$= n-a$, $\frown^2 n-a$ $\frown^1 p-n$
21	8	.	.	-	$= n-a$, $\frown^2 n-a$ $\frown^1 p-n$
22	8	.	.	-	$= n-a$, $\frown^2 n-a$ $\frown^1 p-n$
23	8	.	.	-	$= n-a$, $\sqcup^0 n-a$ $\frown^1 p-n$
24	8	.	.	-	$= n-a$, $\sqcup^0 n$ $\frown^1 p-n$
25	7	.	.	-	$\equiv^0 n-a = p-n$, $\frown^2 n-a$
26	7	.	.	-	$\frown^2 n-a$ $\frown^1 p-n$
27	7	.	.	-	$\frown^0 n-a$, p
28	7	.	.	-	$\frown^0 n-a$ $\frown^1 p-n$
29	8	.	.	-	$= n-a$, $\frown^2 n-a$
30	7	.	.	-	$\frown^0 n-a$
31					
Σ	—	22.8	—	-	UWAGI

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1	6	.	.	-	$\equiv^2 na$, $\frown^0 na$
2	6	.	.	-	$\equiv^{0-1} na-7^{10} = a-n$, $\frown^1 na-a$ $\frown^0 np$
3	7	.	.	-	$= na-a$; $\frown^2 na-a$ $\frown^0 np$
4	6	.	.	-	$= na$, np; $\frown^1 na$
5	7	.	.	-	$= na$
6	7	.	.	-	$= na$, $\frown^1 na$
7	6	.	.	-	$= na-a$; $\frown^0 na$
8	7	.	.	-	$= na \quad \infty a$
9	6	2.0	.	-	$\bullet^0 a$, $= n-np$
10	4	0.2	.	-	$\bullet^0 na$, $\equiv n-p = p-n$
11	7	0.0	.	-	$\bullet^0 na$, $\equiv n-a$
12	6	.	.	-	$= a-p$
13	7	.	.	-	$= n-a$, $\frown^1 n-a$, $p-n$
14	6	2.2	.	-	$\bullet^1 p$
15	6	.	.	-	$= a-p$
16	6	.	.	-	
17	6	0.2	.	-	$\bullet^0 12^{34-50}$, $\equiv n-a = a-p \quad \infty p-n$, $\frown^2 n-a$
18	6	0.4	.	-	$\bullet^0 n-p$, $= np$
19	7	.	.	-	
20	7	.	.	-	$= n-a$
21	7	.	.	-	$\infty n-a$
22	7	.	.	-	
23	8	.	.	-	$= na$
24	6	0.0	.	-	$\bullet^0 12^{20-45}$, $= na-np$
25	6	.	.	-	$= na-a$, $= a$
26	6	0.0	.	-	$\bullet^0 7^{25-40}$, $= na-a$
27	7	.	.	-	$= na \quad \infty a$
28	7	.	.	-	$= na$, $p-n$, $\frown^1 np$
29	5	2.0	.	-	$\bullet^0 p$ n, $= na \quad \infty a-p = p-n$, $\frown^1 na$
30	6	0.1	.	-	$\bullet^0 7^{45-50}$, $\equiv^0 n-a = a-n$, $\frown^2 p-n$
31	6	.	.	-	$\equiv n-a \quad = a-p$
Σ	—	7.1	—	-	UWAGI

Warszawa - Bielany φ = 52°17' λ = 20°58' Listopad - Novembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	105.8	106.5	107.3	106.5	8.6	9.9	9.3	9.3	10.4	8.0	84	72	91	82	1.9	3.4	1.1	2.1	9	•	10		10		W 4	SW 4	W 5
2	110.9	110.5	105.3	108.9	7.5	11.1	8.1	8.7	11.8	7.4	93	67	75	78	0.8	4.3	2.7	2.6	6	⊙	5	⊙	0		W 5	WSW 4	S 3
3	98.1	96.5	96.1	96.9	5.6	11.9	10.3	9.5	12.9	5.3	85	60	67	71	1.4	5.5	4.1	3.7	7		6	⊙	4		S 3	SW 7	SW 3
4	96.6	98.4	101.2	98.7	7.0	7.4	4.4	5.8	10.3	4.4	82	65	85	77	1.7	3.6	1.3	2.2	10		10		10	•	SW 1	W 2	NW 2
5	99.1	98.8	102.6	100.2	0.8	4.7	5.5	4.1	5.6	0.3	100	98	100	99	0.0	0.1	0.0	0.0	10	•	10	•	10	≡	N 3	NE 1	NE 2
6	104.1	103.7	102.7	103.5	6.9	10.5	9.9	9.3	11.0	5.4	100	91	89	93	0.0	1.1	1.3	0.8	10	≡	10		10		NE 2	NE 4	ENE 6
7	99.2	98.2	98.1	98.5	8.6	11.3	10.0	10.0	11.8	8.5	97	80	83	87	0.3	2.6	2.1	1.7	10	••	10		8		E 8	ESE 7	ESE 8
8	97.1	97.1	98.1	97.4	8.0	8.3	6.9	7.5	10.4	6.9	92	97	91	93	0.9	0.4	0.8	0.7	10	•	10	• ≡	10		ESE 6	E 2	E 2
9	97.3	97.3	96.7	97.1	4.9	7.7	6.3	6.3	8.8	4.6	81	75	91	82	1.7	2.6	0.8	1.7	10		9		0		S 3	SE 4	SE 3
10	94.5	93.6	94.6	94.2	3.7	9.5	9.9	8.2	10.6	2.9	97	84	92	91	0.3	1.9	1.0	1.1	9		10	•	10	•	SE 4	SE 5	SE 2
11	95.1	96.7	98.9	96.9	8.7	8.5	8.6	8.6	9.9	8.5	94	94	92	93	0.6	0.6	1.0	0.7	9		10	•	10		SE 4	SE 4	ESE 6
12	100.7	101.8	104.1	102.2	6.1	5.1	2.4	4.0	8.7	2.4	95	90	91	92	0.4	0.9	0.7	0.7	10	•	10	•	10	•	ESE 8	ESE 9	E 9
13	104.1	103.6	100.5	102.7	1.6	0.9	0.5	0.9	2.4	0.5	94	94	98	95	0.4	0.4	0.1	0.3	10	●	10	●	10	●	ENE 8	NE 9	E 7
14	95.8	99.5	104.8	100.0	0.5	-0.6	-0.5	-0.3	0.9	-0.7	98	97	92	96	0.1	0.2	0.5	0.3	10	•	10	△	10		NE 6	NNE 5	N 5
15	106.7	107.1	107.2	107.0	-1.5	-1.5	-0.1	-0.8	0.0	-2.0	94	94	94	94	0.3	0.3	0.4	0.3	10		10		10		N 3	W 2	W 2
16	105.9	105.1	102.0	104.3	1.1	2.2	1.1	1.4	2.5	-0.1	94	84	92	90	0.4	1.2	0.5	0.7	10		10		10	*	WSW 4	WSW 6	SW 5
17	97.7	97.0	97.4	97.4	1.7	4.3	5.0	4.0	5.6	1.0	94	97	95	95	0.4	0.3	0.4	0.4	10		10		10		SW 5	W 4	W 5
18	95.6	95.5	97.7	96.3	1.8	3.9	3.1	3.0	5.2	1.6	96	90	73	86	0.3	0.8	2.1	1.1	10		10		10		W 3	W 4	WNW 3
19	100.1	104.3	111.7	105.4	1.7	2.8	-1.5	0.4	3.5	-1.5	92	59	76	76	0.5	3.1	1.4	1.7	8		3	⊙	2		NW 4	NW 4	NW 2
20	117.7	121.4	124.0	121.0	-2.3	-0.8	-2.6	-2.1	-0.4	-2.8	85	75	83	81	0.8	1.4	0.9	1.0	2		9	⊙	0		NW 2	NW 3	W 3
21	121.5	119.6	116.6	119.2	-1.9	1.6	-0.9	-0.5	2.8	-3.5	85	83	85	84	0.8	1.2	0.8	0.9	6		8	⊙	8		W 3	W 4	W 4
22	113.1	111.3	109.2	111.2	-3.2	1.8	-0.9	-0.8	2.4	-3.5	86	74	81	80	0.7	1.8	1.1	1.2	3		4	⊙	0		WSW 2	W 3	WSW 3
23	106.6	104.9	103.6	105.0	-3.7	3.3	0.1	0.0	5.4	-6.2	95	48	76	73	0.2	4.6	1.5	2.1	2	≡	0		1		C 0	N 1	S 2
24	104.0	104.6	106.1	104.9	-3.4	1.9	2.3	0.8	2.6	-3.5	88	76	86	83	0.6	1.7	1.0	1.1	2		8	⊙	10		SW 2	WSW 5	WSW 2
25	105.7	103.9	102.7	104.1	1.5	3.0	2.4	2.3	3.1	1.2	96	96	93	95	0.3	0.3	0.6	0.4	10	•	10	• ≡	10		SSW 2	SSW 2	SW 3
26	101.2	100.2	97.2	99.5	0.8	3.6	3.9	3.0	5.0	0.8	96	90	90	92	0.3	0.8	0.8	0.6	10	≡	10	≡	10		SSE 2	S 2	SSE 2
27	93.5	91.2	90.4	91.7	2.4	5.3	3.9	3.9	5.4	1.5	100	91	100	97	0.0	0.8	0.0	0.3	10	≡	10		10	•	C 0	ESE 1	ESE 1
28	96.1	99.3	103.4	99.6	2.9	3.5	1.4	2.3	4.1	1.0	96	95	98	96	0.2	0.4	0.2	0.3	10	●	10		0		WNW 1	WNW 1	C 0
29	104.8	103.7	103.1	103.9	2.5	4.5	4.9	4.2	5.2	-0.7	93	93	94	93	0.5	0.5	0.6	0.5	10		10	•	10		SW 3	SE 3	SSE 2
30	97.7	96.1	91.3	95.0	2.6	5.3	4.9	4.4	5.7	2.3	89	78	84	84	0.8	1.9	1.4	1.4	10		9		10	•	S 4	WSW 8	SW 8
31																											
M	102.2	102.2	102.5	102.3	2.6	5.1	4.0	3.9	6.1	1.7	92	83	88	88	0.6	1.6	1.0	1.1	8.4		8.7		7.4		3.4	4.0	3.5

Grudzień - Décembre

1	82.4	82.9	88.0	84.4	6.6	9.4	6.2	7.1	9.5	4.8	90	83	88	87	1.0	2.0	1.2	1.4	10	•	10	•	9		WSW 9	WSW 9	WSW 5
2	83.6	81.1	84.7	83.1	9.7	11.6	8.8	9.7	12.7	4.2	79	78	71	76	2.5	2.9	3.3	2.9	10		9	•	10		SW 6	WSW 7	WSW10
3	96.0	98.2	97.4	97.2	3.3	5.7	1.4	3.0	8.8	1.4	79	62	83	75	1.5	3.5	1.1	2.0	3		4		0		S 4	SW 4	S 2
4	92.7	94.7	100.8	96.1	2.8	5.8	3.5	3.9	6.0	1.1	93	92	97	94	0.6	0.7	0.2	0.5	10	•	10		9		SSE 4	WNW 5	WSW 2
5	94.1	95.3	94.1	94.5	12.2	14.8	13.1	13.3	15.4	3.5	81	72	65	73	2.6	4.7	5.3	4.2	10		8	⊙	2		WSW 5	WSW 6	SW 6
6	97.0	98.8	101.1	99.0	8.4	5.0	2.2	4.4	15.1	2.2	51	61	73	62	5.4	3.4	2.0	3.6	10		10		2		W 4	SW 6	WSW 3
7	101.4	101.5	103.8	102.2	0.4	1.5	0.4	0.7	2.2	0.2	88	85	90	88	0.8	1.0	0.6	0.8	10		10		10		WSW 2	WSW 3	W 2
8	105.4	105.1	106.2	105.6	-0.3	0.8	-0.1	0.1	1.5	-0.5	80	83	90	84	1.2	1.2	0.7	1.0	10		6	⊙	6		W 4	WSW 2	W 4
9	107.2	108.3	107.4	107.6	-0.1	0.8	-1.3	-0.5	1.0	-1.3	88	73	93	85	0.8	1.8	0.4	1.0	10		9		0		WSW 3	W 3	SE 2
10	103.4	101.9	100.6	102.0	-3.3	0.9	0.5	-0.4	1.3	-3.6	85	68	82	78	0.7	2.1	1.1	1.3	10		9		10	△	SE 5	SSE 3	S 2
11	95.7	89.8	85.2	89.6	0.7	1.9	0.8	1.0	2.1	0.4	81	78	98	86	1.2	1.5	0.2	1.0	8		10		10		SSW 2	S 2	C 0
12	90.3	94.8	100.7	95.3	0.6	1.3	-1.9	-0.5	1.4	-2.0	98	92	85	92	0.1	0.5	0.8	0.5	10		10		10		NW 2	NNE 3	NE 3
13	109.6	112.8	117.0	113.1	-5.0	-4.5	-7.4	-6.1	-1.6	-8.0	66	77	82	75	1.4	1.0	0.6	1.0	10		9	*	0		NE 4	NE 5	NE 2
14	116.7	115.0	113.8	115.2	-9.5	-8.2	-8.2	-8.5	-7.1	-9.8	75	57	72	68	0.7	1.4	0.9	1.0	0		1	⊙	4		NW 2	N 6	NW 4
15	108.6	108.9	115.2	110.9	-8.2	-11.3	-13.9	-11.8	-7.6	-14.4	84	79	85	82	0.5	0.5	0.3	0.4	10	*	3	⊙	0		NW 6	NNE 6	NE 3
16	123.1	127.0	133.0	127.7	-16.6	-13.8	-17.4	-16.3	-15.7	-17.5	80	75	85	80	0.3	0.5	0.2	0.3	2		0	⊙	0		NE 2	NE 5	NE 1
17	131.8	129.1	128.2	129.7	-16.3	-9.5	-5.7	-9.3	-5.7	-19.8	85	75	90	83	0.2	0.7	0.4	0.4	9		10		10	*	N 1	NNW 4	N 1
18	127.2	125.3	122.1	124.9	-5.8	-5.4	-4.3	-4.0	-5.3	-5.7	80	81	84	82	0.9	0.9	0.7	0.8	10		10		10		WNW 6	W 5	W 6
19	119.2	116.5	115.4	117.0	-5.1	-2.1	1.0	-0.8	1.0	-4.4	95	96	92	94	0.3	0.2	0.5	0.3	10	•	10		9		WNW 6	W 4	W 5
20	110.8	102.1	98.3	103.7	-0.7	-1.7	1.2	0.0	1.5	-1.8	91	92	89	91	0.5	0.4	0.8	0.6	10		10	*	10		W 6	W 7	NW 5
21	95.8	99.7	101.5	99.0	-0.9	-2.1	-4.1	-2.8	1.6	-5.1	85	52	82	73	0.8	2.5	0.8	1.4	9	*	1		6		W 6	NNW 5	NW 5
22	97.5	93.3	96.3	95.7	-7.1	-5.3	-5.9	-5.6	-5.3	-8.6	82	72	87	80	0.6	1.4	0.5	0.8	1		4		9	*	WSW 4	W 3	NNE 2
23	101.1	102.7	103.7	102.5	-12.6	-10.2	-7.4	-9.4	-5.5	-14.4	89	87	90	89	0.3	0.4	0.3	0.3	1		9		10		WNW 1	WSW 3	WSW 3
24	105.6	106.2	105.2	105.7	-6.6	-6.6	-7.9	-7.2	-6.1	-7.9	91	86	78	85	0.3	0.5	0.7	0.5	10	*	10		10		WSW 3	W 2	C 0
25	103.5	102.3	100.5	102.1	-12.8	-11.7	-15.2	-13.7	-7.9	-15.8	85	86	93	87	0.4	0.5	0.2	0.3	10	*	0	⊙	0		S 4	S 1	S 1
26	98.7	97.4	95.8	97.3	-19.4	-13.7	-13.5	-15.0	-11.5	-20.1	83	71	76	77	0.2	0.6	0.5	0.4	0		8	⊙	4		C 0	S 2	C 0
27	98.9	102.2	104.9	102.0	-15.1	-14.6	-13.7	-13.8	-12.9	-16.1	88	87	88	88	0.3	0.3	0.3	0.3	10		10	*	10		S 2	WNW 2	E 4
28	103.6	101.3	98.8	101.2	-14.4	-11.3	-6.4	-9.6	-6.4	-16.2	87	90	86	88	0.3	0.3	0.5	0.4	10		10	*	10	*	E 5	ENE 5	ESE 3
29	98.2	99.1	99.9	99.1	-3.1	-1.2	-3.4	-2.8	-1.1	-6.5	86	91	92	90	0.7	0.5	0.4	0.5	9		3	⊙	10	≡	SSE 2	SSE 3	SSE 3
30	97.7	96.6	97.3	97.2	-1.2	0.6	0.4	0.0	0.9	-3.0	96	98	94	96	0.2	0.1	0.4	0.2	10	•	10	≡	0		ESE 4	SSE 3	S 2
31	96.5	96.6	94.5	95.9	0.2	1.7	-2.2	-0.6	1.9	-2.2	92	92	93	92	0.5	0.5	0.4	0.5	9		9		10	≡	S 2	S 3	C 0
M	103.0	102.8	103.5	103.1	-5.7	-2.2	-5.2	-5.1	-0.4	-6.0	84	80	85	83	0.9	1.2	0.8	1.0	8.1		7.5		6.5		3.7	4.2	2.9

Warszawa - Bielany $H_s = 101\ m$ $H_b = 104{,}7\ m$ $h_w = 16\ m$ Listopad - Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	UTRUDNIENIE	POGODA
1	6	0.1	.	-	• ° n − a; = n − p
2	7	.	.	-	= n − a
3	6	.	.	-	= n − p
4	7	11.1	.	-	• ° p − n, = n − a
5	6	1.9	1	-	* n • ° n − p, = n − a ≡ ° n
6	5	0.0	.	-	• ° p, ≡ ° n − 7^{00} = − n
7	6	0.0	.	-	•• ° n − a, = n − p
8	3	0.0	.	-	• ° n − p; ≡ n − a, p − n ≡ a − p
9	6	.	.	-	= n − p, ⌓ ¹ p − n
10	6	2.1	.	-	• ° a … n; = n − n; ⌓ ⁻¹ a
11	6	6.8	.	-	• ° n … p, = n − a
12	7	11.5	.	-	• ° n … p, = n − a
13	5	9.3	.	-	• ° na − p • ° np, = na − p
14	5	7.2	.	-	• ° na − a △ ° a − 14^{10} * ° − 15^{10}, = a; ∞ na − np
15	6	.	.	-	= a, ∞ na
16	6	0.0	.	-	•• ° 17^{10} n, = na
17	6	2.2	.	-	• ° a − p, = na − p
18	6	0.2	.	-	• ° na, a * 12^{46} • ° p, = na − p
19	8	0.1	.	-	▽ ° 6^{58}, ⌴ ° n − a
20	7	.	.	-	= n − a, ⌴ ° n − a
21	6	.	.	-	= n − p, ⌴ ° n − a, p − n
22	6	.	.	-	= n − n, ⌴ ° n − n
23	4	.	.	-	≡ ¹ n − a ∞ a − p = p − n, ⌴ ¹ n − a ⌴ ° a − p ⌴ ³ p − n
24	5	0.6	.	-	= na − n, ⌴ ° na
25	3	2.6	.	-	• ° na − p, = na − 11^{30} ≡ ° − np
26	3	0.0	.	-	≡ ° na − a, // = p − n
27	5	1.0	.	-	• ° na, p … n, ≡ ° n − a = a − n; ⌓ ² n − a
28	5	0.8	.	-	• ° na − a; = n − np, ⌴ ° p − n
29	5	0.8	.	-	• ° 12^{15-42}, p, = n − np
30	7	5.0	.	-	• ° p − n, = n − a
31					
Σ	—	65.3	—	-	UWAGI:

Grudzień - Décembre

1	6	5.6	.	-	• ° n … p, = n − a
2	7	0.0	.	-	• n • ° a … p
3	5	0.6	.	-	= n − a ∞ − a, = p − n
4	5	1.6	.	-	• ° na − 7^{50} = na − n; ⌓ ² np
5	8	.	.	-	• ° na − 6^{30}
6	8	.	.	-	
7	5	.	.	-	= a − p
8	6	.	.	-	= p
9	6	.	.	-	= p, ⌴ ° np
10	7	1.9	.	-	△ ° 19^{15} − np, ⌴ ° na
11	6	5.7	.	-	• ° a * * • a n, = a − p
12	6	.	pł.	-	= a − p ≡ ¹ p
13	6	0.1	.	-	* ° 11^{17} − p
14	8	0.2	pł.	-	⌴ ¹⁻⁰ na − p
15	7	0.8	2	-	* ° n − a
16	7	.	4	-	
17	7	0.0	5	-	* ° p − n; = n − a, ⌴ ° p
18	6	0.0	5	-	
19	4	0.1	5	-	⌒ ⁰·² n − a * ° p … , = n − p
20	5	1.8	2	-	•• 12^{10-43} * ⁰·⁷ − p, = n − np; ∞ a − p
21	7	0.0	5	-	* ° n − a * ⁰·⁹ ▽ a
22	8	0.1	5	-	* ° p … n
23	7	1.0	6	-	* ° p, V ° n − a
24	6	0.0	7	-	* ° n
25	5	0.0	7	-	* ° na − 10^{00}, = a − p, V ° na − n
26	6	.	6	-	= na − np, V ° na − np
27	5	0.1	6	-	* ° 7^{30} n, = na − np, V ° na − np
28	5	0.1	7	-	* ° na np; = a − p, V ¹ na − p V ° np
29	5	0.2	7	-	= na − p ≡ ° np, V ° np
30	3	0.1	6	-	• ° na − 7^{50}, = na − 11^{10} ≡ ° − p = np, V ° na, np
31	5	0.0	4	-	= n − p ≡ ² p − n; V ¹ na, p − n
Σ	—	20.0	—	-	UWAGI:

Łódź - Lublinek — φ = 51°44' — λ = 19°24' — Styczeń - Janvier 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.3	93.2	94.2	92.9	-0.3	0.9	0.5	0.4	1.5	-2.0	100	87	92	93	0.0	0.9	0.5	0.5	10	10	9	SW 3	SW 2	C 0
2	93.0	91.0	87.7	90.6	-1.5	0.2	0.0	-0.3	1.4	-2.3	92	94	98	95	0.4	0.4	0.1	0.3	10	10 *	10	SSE 2	NE 1	ESE 2
3	80.9	77.5	77.7	78.7	-1.7	0.9	1.9	0.8	2.8	-2.0	94	83	84	87	0.3	1.1	1.2	0.9	10	9	9	SE 5	SE 5	SE 2
4	77.2	76.5	79.8	77.8	2.7	5.3	4.4	4.2	7.7	0.7	84	80	93	86	1.2	1.8	0.6	1.2	10	9	10 •	SE 5	SE 7	SW 5
5	81.5	82.5	87.3	83.8	1.3	2.5	1.6	1.8	5.1	0.8	96	93	83	91	0.2	0.5	1.2	0.6	10	10	0	C 0	S 1	SW 6
6	92.1	92.2	89.6	91.3	0.8	3.4	0.4	1.2	4.5	0.5	94	75	82	84	0.4	2.0	1.1	1.2	10	0	0	SW 7	S 6	SE 6
7	87.2	88.2	88.5	88.0	-0.1	2.5	1.0	1.1	4.1	-1.1	80	77	92	83	1.2	1.7	0.5	1.1	9	9	6	S 4	S 4	S 2
8	88.9	89.2	87.7	88.6	0.4	1.4	0.4	0.6	2.8	-1.0	98	94	98	97	0.1	0.4	0.1	0.2	10 *	9	10 *	SW 2	SSW 3	S 2
9	87.0	88.0	88.6	87.9	2.0	2.9	0.6	1.5	4.3	0.5	85	88	90	88	1.1	0.9	0.6	0.9	9	9	0	SW 7	SW 6	S 2
10	89.6	90.7	90.3	90.2	0.7	2.5	-0.4	0.6	4.0	-0.5	98	86	94	93	0.1	1.0	0.3	0.5	10	7	0	WSW 3	SSW 4	SE 1
11	90.3	91.6	94.8	92.2	-1.1	1.9	0.8	0.6	3.6	-2.2	83	80	90	84	0.9	1.4	0.7	1.0	10	9	10	SSE 2	S 3	SW 3
12	99.3	102.7	106.5	102.8	-2.2	-1.7	-1.9	-1.9	1.6	-5.1	87	88	90	88	0.7	0.7	0.5	0.6	9	10	10	W 7	WNW 9	W 4
13	109.1	108.4	104.7	107.4	-5.3	-2.0	-0.7	-1.7	-0.7	-5.3	83	79	79	80	0.8	1.1	1.2	1.0	10	8	10	WNW 2	SW 4	SW 6
14	103.7	104.5	108.2	105.5	0.1	0.2	0.0	0.1	1.0	-0.9	96	100	100	99	0.3	0.0	0.0	0.1	10	10 *	10	WSW 2	W 2	C 0
15	111.2	110.5	107.8	109.8	-0.7	-2.3	-5.7	-2.6	1.2	-5.7	96	96	97	96	0.2	0.3	0.2	0.2	10	10	10	NW 3	W 4	W 6
16	103.6	103.2	103.3	103.4	-5.9	-2.4	0.0	-1.6	1.2	-4.5	92	98	98	96	0.4	0.1	0.1	0.2	10 *	10 ☾	9	W 3	W 2	N 3
17	106.9	109.9	114.0	110.3	-8.7	-7.2	-10.4	-9.2	1.0	-12.0	83	79	74	79	0.5	0.7	0.7	0.6	0	0 ○	0	N 4	N 5	NE 3
18	117.9	119.4	118.4	118.6	-18.7	-12.4	-14.6	-15.1	-9.9	-21.3	84	89	87	87	0.2	0.3	0.3	0.3	0	2	9	C 0	C 0	C 0
19	115.1	112.7	111.2	113.0	-14.6	-6.5	-6.3	-9.4	-5.6	-18.0	91	62	75	76	0.2	1.4	0.8	0.8	9	9	6	C 0	E 1	E 2
20	107.9	106.3	105.8	106.0	-12.2	-5.6	-8.7	-8.3	-1.4	-13.3	96	60	92	83	0.1	1.9	0.3	0.8	0	3	0	C 0	E 1	E 1
21	100.9	100.3	98.9	100.0	-10.4	-6.1	-11.1	-9.7	-4.8	-13.0	90	89	86	88	0.3	0.4	0.4	0.4	8	1 ☉	7	C 0	ESE 2	E 2
22	95.2	92.2	91.5	93.0	-12.6	-5.9	-10.4	-9.8	-5.2	-13.6	89	81	90	87	0.3	0.7	0.3	0.4	7	9	0	E 3	SE 1	E 2
23	89.8	91.0	93.2	91.3	-10.9	-7.3	-13.0	-11.0	-6.4	-14.5	94	96	84	91	0.2	0.1	0.4	0.2	10 =	10 ≙	0	E 3	NE 5	E 3
24	93.4	92.3	90.8	92.2	-17.1	-8.5	-10.4	-11.6	-7.8	-19.1	90	89	97	92	0.2	0.3	0.1	0.2	9	6	10 *	NE 1	NW 1	C 0
25	89.7	90.8	94.5	91.7	-10.0	-10.0	-14.9	-12.4	-6.1	-15.2	84	78	87	83	0.4	0.6	0.3	0.4	6	0 ☉	0	NE 5	ENE 5	NE 4
26	100.1	103.6	106.7	103.5	-18.0	-10.2	-16.4	-15.2	-9.4	-19.0	90	71	95	85	0.2	0.8	0.1	0.4	0	0	0	NE 2	SE 2	C 0
27	110.6	110.0	108.0	109.5	-18.5	-8.1	-12.0	-12.6	-6.4	-20.1	95	61	60	72	0.1	1.3	1.0	0.8	0	0	0	C 0	SE 2	SE 2
28	102.9	102.1	97.7	100.9	-8.3	-1.6	-5.5	-5.2	-0.5	-14.7	63	75	67	68	1.2	1.3	1.3	1.3	0	6	6	S 9	S 7	S 4
29	94.0	95.9	96.0	95.3	-4.6	0.4	-1.5	-1.8	1.2	-13.5	86	85	86	86	0.6	1.0	0.8	0.8	8	10	2	S 8	SW 7	SW 6
30	87.2	85.5	81.8	84.2	-0.3	2.8	2.7	2.0	4.1	-4.1	86	67	79	77	0.9	2.5	1.5	1.6	9	10 •	10	SSW 10	SW 10	SSW 10
31	81.9	76.6	80.3	79.6	2.3	2.4	1.9	2.1	3.6	1.7	93	98	96	96	0.5	0.2	0.3	0.3	10	10 •	10 •	S 7	S 5	W 7
M	96.1	96.0	96.2	96.1	-5.5	-2.1	-4.1	-3.9	-0.2	-7.6	89	83	88	87	0.5	0.9	0.6	0.7	7.5	6.9	5.6	3.5	3.8	3.1

Luty - Février

1	80.0	76.2	74.0	76.7	0.9	3.5	0.2	1.2	5.2	0.0	96	85	100	95	0.2	1.3	0.0	0.5	10	10	10 ≋	SW 2	SE 3	C 0
2	75.0	73.4	71.0	73.1	0.7	2.6	-0.1	0.8	4.2	-0.6	90	79	88	86	0.6	1.6	0.8	1.0	10	7	0	SW 7	SW 5	SSE 1
3	70.1	72.2	77.1	73.1	-0.3	0.3	-0.1	0.0	1.0	-1.2	90	96	92	93	0.6	0.2	0.5	0.4	10	10	10 *	SE 1	NW 2	WNW 2
4	83.6	85.7	80.2	82.5	-1.5	0.3	-0.7	-0.6	2.0	-2.3	86	79	85	83	0.8	1.3	0.9	1.0	3	9	9	W 7	WSW 7	SE 1
5	83.8	90.6	96.7	90.4	-1.6	-0.6	-2.9	-2.0	0.5	-4.5	90	81	93	88	0.5	1.1	0.3	0.6	10	9	9	C 0	N 5	W 2
6	96.5	96.1	90.1	94.8	-4.3	0.0	-0.9	-1.5	1.0	-6.1	98	71	79	83	0.1	1.8	1.2	1.0	10	7	9	S 4	S 6	SSE 6
7	85.1	85.7	85.7	85.5	0.2	3.0	1.0	1.3	4.8	-1.2	80	81	90	84	1.2	1.5	0.7	1.1	10	8	4	SSW 6	SW 5	S 5
8	86.2	90.5	95.1	90.6	1.2	3.0	0.4	1.2	4.7	-0.2	98	84	98	93	0.2	1.2	0.1	0.5	10 •	9	9	WSW 6	WNW 5	W 2
9	95.0	89.7	85.0	89.9	-0.8	1.8	1.9	1.2	2.7	-1.4	99	91	98	96	0.0	0.7	0.1	0.3	10 =	10	10 •	S 3	S 5	SSW 1
10	90.3	96.4	103.1	96.6	3.2	0.8	-0.1	1.0	5.0	-0.4	98	98	94	97	0.2	0.2	0.4	0.3	10 •	10 ☽	10	NW 7	NW 7	NW 5
11	97.6	92.2	87.6	92.5	0.6	3.0	3.0	2.4	5.1	-0.4	90	86	96	91	0.6	1.1	0.3	0.7	10	10	10 ≋	SW 4	SSW 6	SSW 4
12	85.1	86.3	93.2	88.2	2.4	7.4	3.2	4.0	8.0	2.2	98	75	100	91	0.2	2.6	0.0	0.9	10	8	10 ☽	C 0	SE 1	NW 2
13	98.3	99.9	102.7	100.3	1.2	3.1	1.5	1.8	5.1	1.0	98	97	96	97	0.2	0.2	0.3	0.2	10 •	10	10	W 1	W 4	NNE 1
14	105.5	106.4	105.1	105.7	-0.2	1.2	-0.3	0.1	2.5	-0.8	96	87	94	92	0.2	0.9	0.4	0.5	10	9	0	SE 1	S 4	SSE 2
15	104.7	105.9	105.6	105.4	1.2	7.2	4.2	4.2	9.4	-0.5	94	77	95	88	0.4	2.4	0.5	1.1	10	0	0	S 2	SW 4	SW 4
16	106.6	109.4	112.2	109.4	4.2	4.6	2.4	3.4	5.2	1.7	97	100	96	98	0.2	0.0	0.3	0.2	10	10 ☽ ≈	10 ☽	W 4	WNW 7	NW 4
17	112.7	113.5	112.8	113.0	2.9	4.7	3.0	3.4	4.9	1.9	96	92	98	95	0.2	0.7	0.2	0.4	10 ☽	10	10	W 7	WNW 6	WSW 4
18	110.7	109.8	106.9	109.1	-0.6	8.7	3.8	3.9	11.8	-1.2	100	80	95	92	0.0	2.2	0.4	0.9	10 =	0 ☉	0	C 0	WSW 3	C 0
19	105.5	105.6	107.8	106.3	1.5	4.0	2.0	2.4	4.5	0.0	98	98	98	98	0.1	0.1	0.2	0.1	10	10 ☽	10 ☽	WSW 4	WSW 5	WNW 4
20	108.8	111.0	112.7	110.8	2.7	3.5	3.3	3.2	4.9	1.8	98	100	86	95	0.1	0.0	1.0	0.4	10 ☽	10 ☽	10	NW 1	NW 2	C 0
21	112.5	112.6	111.6	112.2	2.4	4.7	1.0	2.3	6.5	0.8	95	74	96	88	0.4	2.1	0.3	0.9	10	10	0	C 0	SW 2	C 0
22	112.4	112.9	112.2	112.5	-1.7	6.7	1.1	1.8	8.4	-2.1	96	62	98	85	0.2	3.7	0.1	1.3	0	0	0	C 0	S 1	E 2
23	110.8	110.4	108.5	109.9	0.4	0.1	0.6	0.4	1.7	-0.5	98	96	94	96	0.1	0.3	0.4	0.3	10	10	10	E 3	E 3	E 1
24	107.8	107.7	107.9	107.8	0.6	3.0	0.9	1.8	7.7	0.4	92	73	92	86	0.5	2.3	0.3	1.1	10	4	0	E 1	SSE 1	ESE 5
25	109.8	111.1	110.9	110.6	-0.4	-0.1	-0.9	-0.6	2.2	-1.1	96	84	87	89	0.2	1.0	0.7	0.6	10	10	0	SE 2	SE 4	SE 5
26	110.8	111.5	111.1	111.1	-2.5	1.6	-0.3	-0.4	5.5	-3.2	98	80	88	89	0.1	1.4	0.8	0.8	10	9	0	SE 5	S 4	S 5
27	108.8	106.6	102.5	106.0	-1.1	8.2	6.2	4.9	10.6	-2.0	91	67	85	80	0.5	3.6	1.6	1.9	0	10	10	S 3	SSW 7	SW 5
28	95.1	88.7	87.9	89.9	4.2	6.5	4.3	4.8	9.1	4.1	90	84	84	86	0.8	1.6	1.4	1.3	10 •	10 •	10	SSW 7	SSW 8	W 10
29																								
30																								
31																								
M	98.2	98.4	98.5	98.4	0.6	3.4	1.3	1.8	5.2	-0.6	94	84	93	90	0.3	1.3	0.5	0.7	9.0	8.2	6.4	3.1	4.4	3.0

Łódź – Lublinek $H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 11\,m$ **Styczeń – Janvier 1961**

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	1	–	= 0⁰⁰–24
2	5	0.0	.	–	✳°10⁴⁰–14⁰⁰ 15⁴⁰. = 0⁰⁰–24
3	6	.	pł.	–	= 0⁰⁰–24
4	6	0.1	.	–	●°7⁴⁵–9⁴⁰ 16⁵⁰ 19¹⁵–21⁰² . = 0⁰⁰–24
5	5	.	.	–	= 0⁰⁰–24
6	7	.	.	–	= 0⁰⁰–11⁴⁰ 15³⁰–18³⁰
7	6	1.3	.	–	✳°22⁵⁰–24 . = 7³⁰–24
8	5	0.5	1	–	✳°0⁰⁰–3³⁵ ✳°5⁴⁸–6¹⁰ ✳⁰·¹7¹⁰ ●°7³⁰–45 . ✳°20⁴⁰–21²⁰ . = . ≡° 0⁰⁰–24
9	6	.	.	–	✳°1⁵⁰–2³⁰ ●°5²⁰..³⁰ . = 0⁰⁰–24
10	6	.	.	–	= 0⁰⁰–24
11	6	1.2	.	–	✳⁰·⁷20⁴⁵–24 . = 0⁰⁰–24 . ⌴° 1⁰⁰–9⁰⁰
12	7	0.0	3	–	✳¹·⁰0⁰⁰–2⁴⁰ ✳°4⁵⁰–6²⁰ ✳°13³⁰–14⁴⁰ . = 0⁰⁰–6⁰⁰
13	7	0.5	3	–	●°23⁵² 24
14	4	7.0	2	–	●°0⁰⁰ 1²⁰ ⊗ ∞ –3⁵⁰ ●°4⁴⁵ 5¹⁰–6³⁵ ●°8¹⁰ 10⁰⁰–11¹⁰ ●✳°–11²⁰ ✳⁰·¹20²⁰ . = 3³⁰–11⁰⁰ ≡⁰·¹ = 14⁰⁰–24
15	4	0.3	12	–	≡¹·⁰ = 0⁰⁰–24
16	5	0.1	11	–	✳°4⁴⁰–8²⁰ ⊗°–17⁴⁵ ∞ 8⁴⁰–17⁴⁵ . ≡° 0⁰⁰–4⁴⁰ = 17⁴⁵–23³⁵
17	7	.	10	–	= 6³⁰–11³⁰
18	5	.	10	–	= 6³⁰–24
19	6	.	10	–	= 0⁰⁰·¹⁰ ≡°–4⁴⁰ = –24
20	6	.	8	–	= 0⁰⁰–24
21	6	.	8	–	= 0⁰⁰–7⁴⁵ ≡⁰·¹–10³⁵ = –24
22	5	.	7	–	= 0⁰⁰–24
23	5	0.1	7	–	△°12¹⁰–17³⁰ ✳°–19⁵⁰ = 0⁰⁰–7¹⁰ ≡⁰·¹–9¹⁵ = –24
24	6	0.0	7	–	✳°10¹⁰ 11⁴⁵ ✳°20⁴⁰ 21³⁰–23²⁵ 24 . = 0⁰⁰–24
25	7	.	7	–	✳°0⁰⁰ 3⁵–5⁴⁰ . = 0⁰⁰–11³⁰ . 15²⁰–19³⁰
26	5	.	7	–	= 6¹⁰–24
27	7	.	7	–	= 0⁰⁰–7¹⁰ ≡°–8¹⁰ = –11³⁰
28	7	.	7	–	= 8³⁰–10³⁰
29	7	.	6	–	
30	7	0.9	6	–	●°12²⁰–13¹⁰ △–13⁴⁰ ●°14²⁰–15⁵⁰ 16⁵⁰ 17³⁰–19⁴⁰ . = p–24 . ≫ 5¹⁰–23²⁰
31	5	10.4	pł.	–	●°7⁵⁰ 8¹⁰ ●⁰·¹20⁵⁰ ●°21⁵⁵–22¹⁵ 23⁰⁵ . = 0⁰⁰–24
Σ	–	22.4	–	–	UWAGI. Ciśnienie powietrza w ciągu całego roku jest za niskie przeciętnie o ok. 0,6 mb.

Luty – Février

1	6	5.8	.	–	●°13³⁵–14⁴⁵ ✳°–15¹⁰ ✳⁰·¹18⁴⁰ ✳°–21⁰⁰ ✳°–24 . = 0⁰⁰–24
2	7	0.1	2	–	✳°0⁰⁰–45 ▽°11¹⁵–45 . = 0⁰⁰–5⁰⁰ . 16³⁰–24
3	5	0.5	1	–	✳°7²⁰ 24 . = 0⁰⁰–24
4	7	0.2	1	–	✳°0⁰⁰ 1⁴⁵ ✳⁰·¹8⁰⁵..⁴⁸ △°9⁰⁷–¹⁰ ▽°14⁵⁰–⁵⁸ ✳⁰·¹ 17⁴⁵–18⁵⁶ . = na . p–24
5	7	0.3	1	–	△°7¹⁵–8⁰⁰ ✳⁰·¹10⁴⁵ ✳°11¹²–²⁰ . = 0⁰⁰–12⁰⁰
6	6	.	3	–	= 5⁵⁰–14³⁰ . ⌴° 1⁰⁰–14³⁰
7	7	1.7	pł.	–	△°6⁵⁰–8⁵⁰ ●°–9⁵⁰ △°–10⁴⁰ . = 10⁴⁰–11³⁰ . ∞ 6⁵⁰–8⁵⁰
8	7	1.3	.	–	●°4⁵⁰ 5²⁰–7¹⁰ ●°–8¹⁵ ●°8³⁵ 9⁰⁵–10⁴⁰ . = 23³⁰–24
9	5	9.5	.	–	●°12⁵⁰–13⁰⁰ ✳⁰·¹ ●°–14³⁰ ✳⁰·¹–16⁵⁰ ●⁰·¹ 17⁵⁰–24 . = . ≡⁰·¹ 0⁰⁰–24
10	4	0.4	.	–	●°0⁰⁰–a ●°a–13¹⁰ . = 0⁰⁰–15¹⁰ ≡⁰·¹–16³⁰ = –24
11	6	3.3	.	–	●°10²⁰–45 ●⁰·¹18⁴⁸–21¹⁵ 22³⁰ ●°–23⁴⁰ 24 . = 0⁰⁰–24 .
12	5	1.4	.	–	●°0⁰⁰..²⁰ 19⁴⁵–21³⁰ ●°–22⁵⁰ = 0⁰⁰–4⁴⁸ ≡°–6³⁰ = –24
13	6	0.2	.	–	●°5⁵⁰ 6⁴⁵ 16⁴⁵–17⁴⁰ . = 0⁰⁰–24
14	7	.	.	–	= 0⁰⁰–5⁰⁰ 14⁴⁰–24
15	6	0.1	.	–	= 0⁰⁰–24
16	5	0.2	.	–	●¹4⁵⁰ 5³⁵ ●°8⁰²–9²⁰ ●¹·⁰–11¹⁵ ●°12²⁰–13⁰⁰ 18²⁰–24 . = . ≡⁰·¹ 0⁰⁰–24
17	6	0.0	.	–	●⁰·¹ 0⁰⁰–9⁵⁰ . = 0⁰⁰–24
18	5	.	.	–	= 0⁰⁰–10 ≡⁰·¹ 5⁴⁰ ≡²·⁰ 10¹⁰ ≡°–10⁴⁰ = –24 . ⌴° 1⁰⁰–8³⁰
19	4	2.2	.	–	●°12³⁵–15¹⁵ 17⁵⁰–22⁵⁰ ●⁰·¹–23⁴⁵ ●°–24 . = 0⁰⁰–7⁵⁰ ≡°–10⁴⁰ = –24 . ⌴° na
20	5	0.1	.	–	●°0⁰⁰–6²⁰ 7²⁰–13⁴⁵ . = 0⁰⁰–24
21	7	.	.	–	= 0⁰⁰–10⁴⁰ 17²⁰–24 . ⌴° 20⁰⁰–24
22	6	.	.	–	= 0⁰⁰–2¹²⁵ ≡°–24 ⌴⁰·¹ 0⁰⁰–12⁰⁰
23	6	.	.	–	= 0⁰⁰–1³⁰ ≡¹·⁰–3⁵⁰ = –24
24	6	.	.	–	= 0⁰⁰–24
25	6	.	.	–	= 0⁰⁰–24 . ⌴° 5⁰⁰–11³⁰
26	6	.	.	–	= 0⁰⁰–24 . ⌴⁰·¹ 2⁰⁰–10⁰⁰
27	6	1.0	.	–	●°16³⁰–17²⁵ = 0⁰⁰–10³⁰ ∞ –16³⁰ = –24 . ⌴°2⁰⁰–9⁰⁰
28	6	1.8	.	–	●°3⁵⁰ 5³⁰–7³⁰ 8⁴⁵ . 10⁴⁵–13²⁰ 14¹⁰ . = 0⁰⁰–18³⁰ . ≫ 19⁴⁰–22³⁰
29					
30					
31					
Σ	–	30.1	–	–	UWAGI.

Łódź - Lublinek φ = 51°44' λ = 19°24' Marzec - Mars 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			POGODA			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	92.2	94.8	99.9	95.6	2.2	3.8	2.8	2.9	5.2	1.6	93	90	91	91	0.6	0.8	0.7	0.7	10		10 •	9	W 1	W 5	WNW 3
2	102.5	103.2	103.0	102.9	2.0	2.5	1.7	2.0	4.4	1.5	91	86	90	89	0.7	1.0	0.6	0.8	10		10 •	.10	W 4	W 7	W 4
3	103.4	106.5	108.4	106.1	0.4	5.3	4.8	3.8	6.6	0.2	94	77	98	90	0.4	2.1	0.1	0.9	8		10	10 ≈ •	C 0	SW 1	C 0
4	110.7	112.2	112.1	111.7	4.2	4.6	2.0	3.2	6.2	1.8	100	97	93	97	0.0	0.3	0.6	0.3	10 =		10	0	C 0	WNW 6.	W 2
5	108.8	110.4	111.2	110.1	3.2	4.9	3.4	3.7	6.3	1.2	88	90	95	91	0.9	0.9	0.4	0.7	10		10	0	W 7	WNW 7	W 3
6	110.9	110.9	109.2	110.3	1.8	3.3	3.6	3.1	5.6	1.3	98	91	93	94	0.2	0.6	0.5	0.4	10		10	0	WNW 6	W 6	W 3
7	105.1	105.6	105.7	104.8	0.6	10.1	5.3	5.3	13.1	0.1	98	66	87	84	0.1	4.3	1.1	1.8	9		6 ⊙	0	W 2	W 7	NW 4
8	109.7	110.0	108.4	109.4	-0.2	4.4	6.6	4.4	11.5	-1.5	100	98	82	93	0.0	0.2	1.7	0.6	10 =		9	0	C 0	W 6	W 7
9	107.7	107.0	105.2	106.6	3.6	11.2	7.4	7.4	13.4	3.4	95	65	84	81	0.4	4.7	1.6	2.2	6		8 ⊙	0	W 6	WNW 9	W 4
10	104.7	102.9	99.3	102.3	2.0	16.1	7.8	8.4	18.2	1.8	98	46	71	72	0.2	9.9	3.1	4.4	6		0 ⊙	0	W 2	SW 3	C 0
11	97.6	98.4	99.6	98.5	3.9	12.9	8.0	8.2	13.7	2.8	93	66	84	81	0.6	5.1	1.6	2.4	8		8	10	SW 1	W 9	W 8
12	97.9	93.3	84.5	91.9	7.2	10.0	11.0	9.8	13.5	7.0	84	66	65	72	1.7	4.2	4.6	3.5	10		8 ⊙	10	W 9	SW 9	WSW 8
13	82.3	85.2	90.8	86.1	4.8	7.2	2.4	4.2	13.3	2.3	73	58	73	68	2.3	4.3	2.0	2.9	7		6	0	WNW 12	WNW 14	NW 5
14	91.7	91.6	90.8	91.4	1.0	4.4	7.6	5.2	7.9	0.2	90	90	96	92	0.7	0.9	0.4	0.7	9		10 •	10 ,	W 3	W 4	W 6
15	90.3	93.1	97.7	93.7	8.2	10.6	6.0	7.7	12.1	5.8	89	61	79	76	1.2	0.5	2.0	2.7	10		6 ⊙	0	W 9	WNW 12	NW 2
16	93.7	93.1	97.6	94.8	8.6	10.4	6.8	8.2	12.1	5.0	81	65	71	72	2.2	4.4	2.9	3.2	10		8	4	W 9	WNW 12	WNW 5
17	100.5	98.8	93.7	97.7	3.0	11.4	7.5	7.4	14.0	1.9	93	53	84	77	0.6	6.4	1.7	2.9	5		5 ⊙	10	W 3	W 8	SSW 2
18	85.5	81.3	80.0	81.6	7.7	13.0	8.9	9.6	16.2	6.5	67	62	79	69	3.5	5.8	2.4	3.9	10		9	10	SSW 7	WSW 9	WSW 6
19	80.2	80.8	85.5	82.2	3.1	4.3	-0.5	1.6	9.3	-0.8	74	77	75	75	1.9	1.9	1.5	1.8	9		10 •	0	W 7	WNW 10	NW 3
20	86.9	87.2	80.1	85.4	-4.4	2.0	0.0	-0.6	5.1	-4.9	93	62	100	85	0.3	2.7	0.0	1.0	9		5 ⊙	10	W 1	WSW 4	S 8
21	70.4	69.8	74.7	71.6	0.3	1.9	0.8	1.0	5.4	-0.2	98	93	96	96	0.1	0.5	0.3	0.3	10		10 •	8	SW 8	SW 8	WSW 5
22	85.1	89.5	91.0	88.5	-0.4	0.1	-0.5	-0.3	3.2	-1.4	84	69	80	78	0.9	1.9	1.2	1.3	10		8	6	NW 7	NW 8	W 2
23	88.2	88.9	91.6	89.6	1.4	6.1	5.2	4.5	6.9	-1.2	98	80	95	91	0.2	1.8	0.4	0.8	10 =		10 •	10 •	WSW 4	W 6	WNW 8
24	92.3	92.1	93.0	92.5	5.3	7.8	7.0	6.8	9.5	5.0	86	75	80	80	1.3	2.7	2.0	2.0	10 •		9	9	W 9	W 10	W 6
25	94.9	96.0	97.6	96.2	4.8	7.2	5.4	5.7	9.3	4.5	92	80	92	88	0.7	2.1	0.7	1.2	9		10	5	W 6	WNW 8	W 3
26	96.2	92.3	84.1	90.9	4.4	10.6	8.8	8.2	12.1	3.2	97	55	62	71	0.3	5.8	4.3	3.5	9		8	10	W 3	SW 9	SW 7
27	82.6	83.4	83.2	83.1	4.2	6.1	0.4	2.8	9.6	0.0	72	50	82	68	2.2	4.7	1.1	2.7	7		6	8	W 9	W 12	W 8
28	83.9	85.0	86.3	85.1	-3.1	2.8	-0.1	0.4	4.8	-1.5	83	70	98	84	1.0	2.2	0.2	1.1	9 *		9	10 *	WSW 10	W 10	WNW 6
29	87.2	85.9	84.7	85.9	0.0	0.9	5.1	2.8	5.1	-1.6	100	94	95	96	0.0	0.4	0.4	0.3	10 *		10 •	10 ⌐	SW 3	SW 6	WSW 7
30	81.3	81.9	78.5	80.6	4.4	6.9	7.0	6.3	8.8	3.8	87	87	90	88	1.1	1.3	1.0	1.1	10 •		10	10 ⌐	WSW 9	SW 8	SW 7
31	82.0	85.4	85.7	83.7	1.7	5.2	4.2	3.8	8.7	1.2	89	48	74	70	0.8	4.5	2.1	2.5	9		8 ⊙	10	NW 5	W 6	SW 4
M	93.8	94.0	93.9	93.9	2.8	6.7	4.7	4.7	9.4	1.6	90	73	85	83	0.9	3.0	1.4	1.8	9.0		8.3	6.1	5.2	7.7	4.7

Kwiecień - Avril

1	87.9	84.1	82.4	84.8	-0.1	0.6	3.1	1.7	7.0	-0.6	78	94	91	88	1.3	0.4	0.6	0.8	4 ⊙		10 *	10	W 9	S 5	WSW 3
2	86.2	88.4	86.2	86.9	2.2	4.2	2.0	2.6	6.1	1.5	84	64	91	80	1.3	2.9	0.7	1.6	10		8	10 •	W 7	W 6	E 2
3	80.1	81.4	86.4	82.6	3.0	10.0	2.9	4.7	10.3	0.8	98	67	89	85	0.2	4.1	0.8	1.7	10 •		9	4	SE 1	W 8	WNW 3
4	81.2	87.1	92.2	86.8	5.4	7.7	4.2	5.4	9.0	0.3	95	69	85	83	0.5	3.2	1.2	1.6	10 •		9 ⊙	10	SW 4	W 8	C 0
5	90.8	88.4	87.6	88.9	5.8	18.0	15.0	13.4	20.1	3.9	85	57	66	69	1.4	8.7	5.7	5.3	8		10 ⊙	9	SE 6	S 8	S 4
6	88.9	90.7	90.0	89.9	12.4	21.2	15.8	16.5	25.5	11.4	72	46	67	62	4.0	13.6	5.9	7.8	9		9	0	SW 4	W 5	E 2
7	89.5	88.7	88.9	89.0	10.8	22.8	16.2	16.5	25.2	9.5	82	43	66	64	2.5	15.9	6.5	8.2	0 ⊙		0 ⊙	0	E 2	SW 2	SW 4
8	89.1	87.9	92.0	89.7	10.6	11.4	5.2	8.1	16.5	5.0	97	88	86	90	0.4	1.7	1.2	1.1	10 =		10	10	NW 2	W 1	NW 5
9	93.9	97.2	98.5	96.5	2.9	6.2	2.2	3.4	8.0	1.2	91	45	73	70	0.6	5.3	2.0	2.6	9		8	0	W 6	NW 10	NNW 1
10	97.7	95.6	91.9	95.1	0.3	6.5	3.7	3.6	8.1	-1.3	74	37	52	54	1.6	6.1	3.8	3.8	10		10	4	ESE 2	SE 5	E 4
11	88.5	88.1	91.1	89.2	3.0	11.6	6.8	7.0	13.3	2.0	66	47	60	58	2.6	7.2	4.0	4.6	9		1 ⊙	0	E 2	ENE 1	NE 2
12	95.4	96.4	95.5	95.8	5.0	9.9	6.4	6.9	13.1	1.0	66	45	66	59	3.0	6.7	5.2	4.3	7		1 ⊙	0	ENE 2	E 2	E 1
13	91.6	91.5	91.2	91.4	7.4	17.9	13.3	13.0	20.0	4.0	69	51	75	65	3.2	10.1	3.8	5.7	8		4 ⊙	0	SSW 2	WNW 8	S 2
14	91.0	90.0	88.0	89.7	9.7	22.3	14.7	15.4	23.6	6.0	86	29	57	57	1.7	19.1	7.2	9.3	5 ⊙		5 ⊙	0	E 1	S 7	SE 2
15	88.5	88.7	88.5	88.6	11.5	22.2	16.4	16.6	24.9	9.3	69	41	72	61	4.3	15.8	5.2	8.4	0 ⊙		0 ⊙	4	C 0	W 2	SE 3
16	88.0	87.4	87.9	87.8	12.4	21.4	10.8	13.8	22.5	9.5	73	40	94	69	3.9	15.4	0.9	6.7	6		3 ⊙	6	ESE 3	S 8	SSW 4
17	88.8	90.2	90.4	89.8	9.4	11.5	10.0	10.2	14.1	7.4	100	87	92	93	0.0	1.9	1.0	1.0	10 =		10	8	C 0	SW 2	W 2
18	90.8	90.2	90.4	90.5	8.0	17.5	11.9	12.3	19.6	5.3	97	46	75	73	0.3	10.9	3.5	4.9	4 ⊙		4 ⊙	9	C 0	W 3	C 0
19	93.1	93.8	94.2	93.7	7.8	14.6	8.1	9.6	16.5	6.3	100	62	71	78	0.0	6.3	3.1	3.1	10 =		8 ⊙	0	C 0	NW 4	NW 2
20	97.3	98.7	99.8	98.6	4.3	10.3	3.8	6.6	11.1	3.0	72	34	55	54	2.3	8.4	4.1	4.9	1 ⊙		7 ⊙	0	NE 6	N 7	E 1
21	100.1	98.2	95.6	98.0	4.4	12.4	8.3	8.4	14.0	1.6	62	32	54	49	3.3	9.8	5.0	6.0	0 ⊙		0 ⊙	0	E 8	E 9	E 7
22	92.2	89.6	87.0	89.6	6.7	18.0	11.8	12.1	19.3	2.6	65	30	56	50	3.4	14.4	6.1	8.0	0 ⊙		0 ⊙	0	ESE 5	SE 9	SSE 4
23	86.1	85.1	85.3	85.6	8.8	18.6	11.8	12.8	20.3	5.2	69	37	36	47	3.3	13.3	8.8	8.6	1 ⊙		3 ⊙	0	E 5	SE 9	ESE 8
24	86.8	88.1	89.8	88.2	7.0	14.6	10.7	10.8	16.0	3.1	73	44	55	57	2.7	9.3	5.8	5.9	0 ⊙		2 ⊙	10	ESE 10	ESE 9	E 9
25	91.3	91.7	91.8	91.7	7.2	11.2	9.6	9.4	12.6	4.3	77	60	73	70	2.4	5.3	3.3	3.7	10		10	7	E 8	E 7	E 7
26	88.8	87.4	86.4	87.5	8.2	13.3	10.3	10.3	15.6	5.3	62	59	80	67	4.2	6.3	2.3	4.3	9		8	6	E 7	E 7	E 4
27	87.0	87.9	88.2	87.7	11.0	17.2	12.7	13.4	18.4	8.2	73	37	66	59	3.2	12.4	5.1	6.9	7		5 ⊙	9	ESE 4	SE 4	E 1
28	88.3	87.7	87.7	87.9	10.3	15.1	9.6	11.2	18.7	9.3	84	61	88	78	2.1	6.7	1.3	3.4	9 •		9 •	3	C 0	E 4	E 1
29	88.1	89.2	89.8	89.0	9.0	13.6	10.4	10.8	16.1	7.3	93	58	53	69	0.7	6.3	3.9	4.4	10 •		8	6	ENE 7	E 12	E 7
30	88.0	86.3	83.3	86.7	7.1	18.6	12.2	12.3	20.7	4.8	64	44	66	58	3.6	11.9	4.8	6.8	8		1 ⊙	0	E 5	ENE 5	E 3
31																											
M	89.8	89.9	90.0	89.9	7.1	14.0	9.4	10.0	16.2	4.6	79	52	70	67	2.1	8.7	3.8	4.9	6.3		5.7	4.2	3.9	5.9	3.3

Łódź-Lublinek

$H_s = 187\,m$ $H_b = 187.7\,m$ $h_w = 11\,m$

Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.8	.	–	▽ 5³⁰–6⁰⁰ ● ⁰8⁵⁰–11²⁰ ▽ 0-1 15³⁵ △¹ 14⁴¹–⁴² . = 7³⁰–13³⁰ . ▽ 18³⁰–19³⁰
2	6	0.4	.	–	● ⁰9²⁵–10¹⁰ ▽ ⁰12³⁴–³⁸ ✳⁰–12⁴⁰ ▽ ⁰12⁴² 14¹⁵ . = 6³⁰–24
3	6	1.5	.	–	● ⁰13⁵⁰–24 . = 0⁰⁰–20⁴⁰ = 0-1 –24
4	6	.	.	–	● ⁰0⁰⁰–⁵⁰ . = ¹0⁰⁰–²⁵ = 2-0 9²⁰ = –16³⁰ . 21³⁰–24 . ▽ 22³⁰–24
5	5	.	.	–	= 0⁰⁰–24 . ⌐ ⁰2⁰⁰–6³⁰ ▽ 0⁰⁰–³⁰
6	6	.	.	–	= 0⁰⁰–⁵⁰ = 0-1 –6⁰² = ⁰–6¹⁰ = –24
7	5	.	.	–	= 0⁰⁰–⁴⁵ = 0-1 –5⁵⁰ = –12⁰⁰ ∞ –20⁰⁰ . ⌓ ⁰21³⁰–24
8	6	.	.	–	= 0⁰⁰–¹⁴⁰ = ⁰–3⁵⁰ = 0-2 11⁴⁵ = –14³⁰ . ⌓ 0-2 0⁰⁰–7⁰⁰
9	7	.	.	–	= 4⁵⁰–9⁴⁰ ⩥ 13³⁰–15⁴⁰
10	7	.	.	–	= 7²⁰–10²⁰
11	6	.	.	–	= 5³⁰–24 . ⩥ 13¹⁵–15³⁰
12	7	4.3	.	–	● ⁰9⁵⁰ 10⁵⁰–12¹⁵ = 0⁰⁰–12²⁰ . ⩥ 12²⁰–14³⁰ 21⁵⁰–24
13	8	0.0	.	–	▽ ⁰2²⁶–⁴⁷ ▲ ⁰ ● ⁰14⁵⁰–15⁰² ▽ ⁰15⁵²–16⁰⁴ . ⩥ –≫ 0⁰⁰–18⁴⁵
14	7	2.8	.	–	● ⁰8⁵⁰–14⁴⁰ ● ⁰–24 . = 14³⁰–24
15	8	.	.	–	● ⁰0⁰⁰–2³⁰ 3⁵⁰ . = 0⁰⁰–6³⁰ ⩥ 7²⁰–11⁴⁰ ≫ –17³⁵
16	7	.	.	–	= 7³⁰–12²⁰ . ⩥ 6²⁰–18²⁰
17	7	.	.	–	= 5³⁰–8³⁰ . ⌐ ⁰2⁰⁰–7⁰⁰ . ⌓ ⁰19³⁰–24
18	7	0.0	.	–	▽ ⁰8³⁰–⁴⁵ = 5³⁰–8⁰⁰ . ⩥ 14⁴⁰–15³⁰ ⌓ ⁰0⁰⁰–6⁰⁰
19	7	0.8	.	–	▽ ⁰11⁰⁰ 14⁴³ ▽ ⁰–15⁰¹ ✳⁰ ▽ –15⁰⁶ ▽ ⁰–16⁰⁸ . 16⁴²–17⁰⁵ . ⩥ 8³⁰–13²⁰
20	9	0.6	1	–	✳⁰ 1⁵⁰ 5⁰² ✳ 1-0 19⁴⁵–20³⁰
21	7	2.4	2	–	✳ 0-1 ✳⁰ ▽ 1²⁵ 8⁰² ● ⁰10¹⁷ 12⁰⁰ ✳ 0-1 12⁰³–¹⁰ ● ⁰12³⁵ 15³⁰ ✳⁰ 17²⁵–³⁰ . 22⁵⁸ 23²⁰ . ⩥ na . a . p
22	8	2.1	1	–	✳⁰ 12⁴⁰ 7⁰² 12⁴¹ ✳⁰ 13⁰¹–⁰⁵ ✳⁰ ▽ 13⁰⁵–14¹⁰ ✳⁰ 21⁵⁰–24
23	6	1.9	1	–	✳ 0-1 0⁰⁰–5³⁵ ● ⁰6⁵⁰–8³⁵ ● ⁰10⁰⁰–11⁰⁷ ● 0-1 11³⁵ 20¹⁰ ● ⁰–22³⁵ . = ⁰6³⁰–7⁵⁰ = –12¹⁰
24	7	3.0	.	–	● ⁰6³⁵–7²⁰ ● ⁰ ▽ 15¹⁵–³⁰ ● ¹22¹⁵–²⁸ . = 4²⁰–11³⁰ ⩥ 9⁰⁵ 22²⁸
25	7	0.0	.	–	● 2-0 0⁰⁰–⁴⁰ ▽ ⁰23⁵⁵–24 . ⩥ 0⁰⁰–¹⁰
26	7	0.4	.	–	● ⁰ ▽ 0⁰⁰–²⁰ ● ⁰23⁴⁵–24 . = 4³⁵–12¹⁰
27	8	0.4	.	–	● ⁰0⁰⁰–3⁴⁰ △ 0-1 ✳ 0-1 12²⁰ 18²⁵ . ⩥ na ⩥ –≫ 6⁵⁵–18²⁵
28	8	1.6	pż.	–	✳ 0-2 5⁵⁰ 22⁰⁷ . ⩥ 12⁰–13³⁵
29	6	6.9	2	–	✳ 0-1 5⁵⁰–9⁵⁰ ● ⁰–12³⁵ ● ⁰–13⁴⁰ 14⁴⁵ ● ● ⁰–15²⁰ ● ⁰–22²⁰ . 24
30	6	5.9	.	–	● ⁰0⁰⁰–³⁰ 2³⁰ 5⁵⁰–6⁴⁵ 8³⁰–11¹⁰ ⁴⁵ ▽ ⁰14⁵⁰ 15¹⁰ ● ⁰21¹⁰–24 . = 2³⁰–24 . ⩥ 7⁴⁵–10⁴⁰
31	8	0.6	.	–	● ⁰0⁰⁰–3⁴⁰ ● ▽ ⁰23⁰⁸–²⁰ . = 0⁰⁰–3⁵⁰
Σ	–	36.4	–	–	UWAGI.

Kwiecień – Avril

1	4	5.8	.	–	✳ 0-1 12¹⁰–13⁵⁷ ✳¹–14⁰⁰ ● ⁰–14⁴⁰ ● 0-1 15⁰⁵–18⁵⁰ . ⩥ 0²⁰–5²⁰ . = 14⁰⁰–17¹⁰ . ▽ 22³⁰–24
2	8	6.7	.	–	△ ⁰8¹²–¹⁵ ● ⁰17⁵⁰ 19³⁸–24 ▽ 0⁰⁰–¹²⁰
3	7	3.4	.	–	● ⁰0⁰⁰–3⁴⁰ 4⁵⁰–6⁵⁰ ● ⁰–7⁴⁰ ● ⁰–10¹⁰ ⁴⁵ = ⁰6⁵²–7³⁰
4	8	0.3	.	–	● 3¹⁵–5⁵⁰ 6⁰² 8⁴⁰ = 3³⁰–8⁴⁰ . ⌓ ⁰20³⁰–24
5	7	.	.	–	● ⁰0⁵⁰–3⁰⁰ ³⁰ . = 4⁴⁵–9⁴⁰ . ⌓ ⁰0⁰⁰–⁵⁰
6	8	.	.	–	
7	7	0.0	.	–	▽ ⁰23⁵⁰–24 . = 5³⁰–8⁴⁰ ∞ –10³⁰ . ⌓ ⁰5³⁰–9⁰⁰
8	6	5.7	.	–	▽ ⁰0⁰⁰–²⁵ ● 0-1 8⁴⁰–10⁰⁰ 13¹⁰ 14¹⁵–16¹⁰ ▽ ⁰–16³⁵ 17⁰⁵–⁰⁹ . = na = 0-1 –7²⁰ = 2-0 –8³⁰ = –19³⁰
9	8	.	.	–	= 4³⁰–7²⁰ ⩥ 8³⁰–13²⁰
10	8	.	.	–	⌐ ⁰13⁰–6⁰⁰
11	7	.	.	–	
12	7	.	.	–	
13	7	.	.	–	= 4³⁰–9³⁰ 18³⁰–24
14	7	.	.	–	= 0⁰⁰–7³⁰ ∞ –10⁴⁰ ⌓ ⁰2⁰⁰–8³⁰
15	7	3.3	.	–	▽ 1-0 21³⁰–22³⁹ (R) 2¹²³–³⁰ R¹–21³⁷ (R) –22⁵⁵ NW–SE . = 3³⁰–9³⁰
16	8	4.6	.	–	▽ 1-0 15⁰⁰–16⁴⁵ (R) 14⁵⁰–15⁰⁰ R¹–16⁰⁰ (R) –16²⁵ SSW–NNE . = 4²⁰–7³⁰ . p . np
17	6	.	.	–	= 0⁰⁰–6⁰⁰ = 0-1 –8²⁵ = –15³⁰ 20¹⁵–24
18	7	.	.	–	= 0⁰⁰–¹⁰ = –2¹⁵ = –10³⁰ 19²⁰–24 . ⌓ 0-2 1⁰⁰–11⁰⁰ ⌓ ⁰20⁰⁰–24
19	8	.	.	–	= 0⁰⁰–5²⁵ = 0-1 5²⁵–6⁰⁵ = ⁰6⁰⁵–8⁰³ = –9³⁰ . ⌓ 0-2 0⁰⁰–10³⁰
20	9	.	.	–	
21	8	.	.	–	na . a . p
22	8	.	.	–	
23	8	.	.	–	
24	8	.	.	–	⩥ 6³⁰–8⁴⁰ 13²⁰–19³⁰
25	7	.	.	–	⩥ 14¹⁰–18³⁰
26	7	.	.	–	
27	7	1.2	.	–	
28	7	7.0	.	–	▽ ⁰4⁴⁵–⁵² 5¹³–7²⁰ 12⁴⁰ 14⁰² . = 7²⁰–8⁰⁰ . ⌓ ⁰np
29	7	1.0	.	–	● 0-1 0⁴⁰ 8¹⁰ ▽ ⁰ 10⁴⁹ 11⁵⁷ . = 4⁰⁰–9³⁰ . ⩥ 10¹⁵–18²⁰ . ⌓ ⁰na
30	7	.	.	–	
31					
Σ	–	39.0	–	–	UWAGI.

Łódź – Lublinek φ = 51°44' λ = 19°24' Maj – Mai 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	87.5	88.7	90.1	88.8	10.2	16.6	12.4	12.9	18.7	5.6	75	47	70	64	3.1	10.1	4.4	5.9	2	5 ⊙	9	E 4	E 5	SE 2
2	90.3	90.4	89.7	90.1	9.0	15.8	12.1	11.8	18.1	7.3	92	80	89	87	1.0	3.2	1.5	1.9	9	10 •	10	SE 2	WSW 4	E 3
3	88.7	87.9	89.5	88.7	10.8	18.2	12.5	13.5	20.5	7.7	82	47	85	71	2.3	11.1	2.2	5.2	9	7	10	E 1	S 7	NW 2
4	93.3	94.0	94.6	94.0	10.3	17.0	12.1	12.9	18.8	8.4	95	44	71	70	0.6	10.9	4.1	5.2	4	7	0	C 0	NW 4	C 0
5	95.5	94.5	92.8	94.3	12.2	20.2	16.4	16.3	21.7	5.6	72	38	51	54	4.0	14.8	9.1	9.3	0	10	5	E 2	SE 6	SE 4
6	90.3	89.6	94.3	91.5	15.0	20.3	10.9	14.3	21.5	10.9	74	63	95	77	4.3	8.8	0.6	4.6	9	9	4	S 5	SW 7	C 0
7	94.2	90.5	88.3	91.0	11.0	19.1	10.0	12.5	20.7	8.0	97	54	91	81	0.3	10.2	1.1	3.9	9 ⊙	7	9	C 0	S 6	WSW 4
8	90.4	89.1	88.4	89.3	8.8	10.6	7.0	8.4	13.8	6.1	89	77	94	87	1.2	2.9	0.6	1.6	8	6	8	W 6	SW 3	W 3
9	86.0	85.5	82.8	84.1	7.6	10.2	8.0	8.4	11.9	5.5	84	80	96	87	1.6	2.5	0.4	1.5	10	9	10 •	WSW 6	SW 8	SW 5
10	84.6	86.3	88.5	86.5	6.6	9.4	7.2	7.6	12.5	6.0	96	74	84	85	0.4	3.1	1.7	1.7	10 •	9	10	WSW 5	WNW 8	WNW 7
11	90.5	92.5	95.5	92.8	6.4	8.8	6.2	6.9	10.7	6.1	85	72	83	80	1.4	3.2	1.6	2.1	10	9	7	NW 8	NNW 7	N 5
12	95.6	94.3	92.7	94.2	4.6	8.6	7.0	6.8	11.9	2.7	82	65	90	79	1.5	3.9	1.0	2.1	9	10	4	N 4	NW 7	C 0
13	92.8	91.2	89.5	91.2	4.5	11.3	8.4	8.2	14.1	2.5	100	55	94	83	0.0	6.1	0.6	2.2	10 =	8	10 •	W 2	SW 5	SW 4
14	87.9	87.9	88.3	88.0	8.0	10.2	6.4	7.8	12.1	6.6	92	55	82	76	0.9	5.5	1.7	2.7	9	9	3	SW 2	W 9	C 0
15	88.3	88.7	90.3	89.2	6.5	10.8	5.8	7.2	12.6	3.1	96	72	95	88	0.5	3.7	0.4	1.5	10	8 ⊙	6	SW 4	W 6	NW 5
16	91.1	89.9	89.5	90.2	6.6	10.7	6.4	7.5	12.3	5.4	91	64	94	83	0.8	4.6	0.6	2.0	9	9	10 •	W 4	WSW 5	SSE 2
17	90.6	92.0	93.1	91.9	7.6	9.9	8.3	8.6	10.3	6.3	89	86	97	91	1.2	1.8	0.3	1.1	9	10 •	9	NNE 2	NW 4	NW 3
18	95.0	94.3	92.9	94.1	6.2	11.3	8.4	8.6	14.4	5.3	85	63	79	76	1.5	5.0	2.2	2.9	4	9	6	NNW 6	N 3	NE 2
19	92.8	91.9	90.7	91.8	8.9	15.1	10.8	11.4	16.1	2.6	75	46	82	68	2.9	9.3	2.3	4.8	6 ⊙	9	10	C 0	NNW 3	C 0
20	88.9	87.2	86.5	87.5	13.8	16.2	13.0	13.5	18.6	9.1	73	47	73	64	3.8	9.7	4.1	5.9	6	9	9	C 0	SW 4	E 2
21	86.2	86.1	87.9	86.7	11.6	17.8	11.8	13.2	19.3	7.0	81	50	90	74	2.6	10.1	1.3	4.7	10	8 ⊙	10	C 0	N 5	N 3
22	88.9	89.3	89.1	89.1	8.2	13.9	9.6	10.3	16.6	7.7	86	51	74	70	1.5	7.8	3.2	4.2	8	5 ⊙	4	NNE 4	NNE 6	NNE 1
23	90.8	90.9	90.8	90.8	8.6	15.8	12.3	12.2	17.7	2.0	68	37	64	56	3.6	11.2	5.1	6.6	2 ⊙	4 ⊙	8	C 0	NNW 2	C 0
24	92.2	93.0	93.3	92.8	11.6	15.2	10.2	11.8	16.9	9.6	77	56	76	70	3.1	7.7	3.0	4.6	6	10	2	N 3	W 7	C 0
25	93.6	92.4	91.2	92.4	10.5	17.0	13.0	13.4	19.3	5.2	79	47	66	64	2.7	10.4	5.1	6.1	0 ⊙	5 ⊙	0	C 0	SW 1	C 0
26	91.1	90.1	87.6	89.6	13.2	19.6	14.8	15.6	22.0	7.3	77	43	60	60	3.5	12.9	6.7	7.7	8	7	0	C 0	NE 1	E 1
27	85.9	85.9	86.8	86.2	15.2	22.4	13.4	16.1	24.0	10.1	71	54	93	73	5.0	12.4	1.1	6.2	0	8 ⊙ (K)	8	ESE 2	W 5	N 2
28	86.1	86.0	87.6	86.6	13.1	16.2	9.6	12.6	21.8	9.4	86	89	92	89	2.5	1.9	1.0	1.8	4 ⊙	10 • (K)	10	C 0	W 6	W 2
29	85.2	80.8	75.8	80.6	8.8	17.3	19.0	16.0	22.5	7.5	92	77	61	77	0.9	4.5	8.5	4.6	10	9	10	E 2	ENE 7	ENE 5
30	77.0	80.4	81.9	79.8	10.8	12.0	12.1	11.8	19.7	10.8	96	82	93	90	0.5	2.5	1.0	1.3	10	10	9	SW 5	SW 5	W 1
31	83.5	83.9	83.8	83.7	10.8	15.0	14.0	13.4	18.6	8.0	91	62	77	77	1.2	6.4	3.7	3.8	8	10	6	S 2	S 3	E 2
M	89.5	89.1	89.2	89.3	9.6	14.5	10.6	11.3	17.1	6.6	85	61	82	76	1.9	7.0	2.6	3.8	7.0	8.2	7.0	2.6	5.1	2.3

Czerwiec – Juin

1	83.2	83.7	82.7	83.2	16.5	24.3	19.6	20.0	25.7	11.5	67	45	60	57	6.2	16.8	9.0	10.7	0 ⊙	6 ⊙	1	SE 4	S 6	SE 1
2	82.4	82.8	83.2	82.8	18.2	25.8	18.1	20.0	27.0	12.6	72	41	76	63	5.8	19.6	5.1	10.2	3 ⊙	4 ⊙	7 (K)	SE 2	SE 3	C 0
3	84.0	84.4	86.1	84.8	20.8	26.4	19.4	21.5	27.7	15.1	71	38	70	60	7.2	21.5	6.6	11.8	5 ⊙	4 ⊙	8	E 5	E 8	S 1
4	87.1	87.9	89.4	88.1	17.6	19.4	18.2	18.4	25.8	15.2	84	64	77	75	5.2	8.2	4.9	5.4	4	9 (K)	9	C 0	NW 4	NE 1
5	91.9	92.9	93.2	92.7	17.6	22.2	17.6	18.8	24.6	14.7	80	60	76	72	4.0	10.8	4.7	6.5	2 ⊙	7 ⊙	3	E 2	E 6	E 1
6	93.5	91.8	90.7	92.0	18.2	22.6	17.4	18.9	24.3	12.2	59	57	72	63	8.6	11.7	5.5	8.6	1 ⊙	8 ⊙	10	E 3	E 7	E 6
7	88.8	87.3	85.9	87.3	16.6	23.2	17.4	18.6	26.0	15.5	87	61	87	78	2.5	11.1	2.6	5.4	10	6 ⊙	8	SE 4	SE 4	ESE 1
8	86.2	87.1	88.4	87.2	17.0	20.0	15.2	16.8	24.7	13.7	86	81	96	88	2.8	4.4	0.8	2.7	5	10 (K)	10 •	SW 3	S 3	W 1
9	89.8	90.7	89.5	90.0	16.2	20.9	19.6	19.1	23.6	13.3	96	72	81	83	0.8	7.0	4.3	4.0	10	8	9	NE 1	C 0	ENE 3
10	90.0	90.3	90.3	90.2	20.1	23.8	16.5	19.2	26.1	14.5	75	62	86	74	6.4	11.4	2.8	6.9	2	6	9	SE 2	E 1	NW 1
11	90.8	90.7	89.9	90.5	15.0	21.1	16.6	17.5	23.0	11.6	98	68	93	86	0.3	7.9	1.4	3.2	10	6 ⊙	6	NW 3	W 5	W 4
12	89.1	88.8	87.9	88.6	15.4	19.5	14.8	16.1	22.2	14.7	91	61	86	79	1.5	8.9	2.4	4.3	10	9	10	W 2	W 3	W 2
13	87.6	85.2	82.9	85.2	14.4	21.0	16.0	16.8	23.1	11.4	80	43	73	65	3.2	14.1	4.9	7.4	4 ⊙	6 ⊙	10	C 0	SSW 3	SE 2
14	82.5	85.2	87.6	85.1	15.0	13.7	13.0	13.7	17.6	12.9	76	86	91	84	4.0	2.2	1.4	2.5	9	10 •	10 •	SSW 4	WSW 9	W 8
15	90.7	92.3	93.5	92.2	11.4	14.3	12.4	12.6	15.8	11.4	85	61	75	74	2.0	6.3	3.5	3.9	10	10	9	W 8	W 7	W 2
16	94.8	95.5	95.5	95.3	11.4	15.6	11.2	12.4	17.1	8.9	80	61	85	75	2.7	6.9	2.0	3.9	8	9	1	W 5	W 6	SSW 2
17	97.2	96.9	96.3	96.8	13.8	21.0	16.0	16.7	23.5	6.7	75	41	72	63	3.9	14.7	5.1	7.9	2 ⊙	4 ⊙	8	W 3	W 5	C 0
18	96.1	94.1	91.9	94.0	15.4	25.8	19.6	20.1	26.6	10.5	70	37	67	58	5.3	20.8	7.5	11.2	8	4	0	C 0	WSW 5	SW 1
19	94.3	96.8	98.7	96.6	17.6	13.6	13.3	15.0	21.6	13.3	94	90	70	85	1.2	1.7	4.7	2.5	10 •	10 •	1	W 2	WNW 3	NW 1
20	102.9	103.1	102.7	102.9	13.4	19.2	11.8	14.0	21.0	7.1	67	44	74	62	5.2	12.3	3.6	7.0	0 ⊙	4 ⊙	1	WNW 5	W 6	C 0
21	101.5	98.7	100.6	100.3	15.2	22.2	12.8	15.8	24.6	6.1	62	33	88	61	6.5	18.1	1.8	8.8	1 ⊙	3 ⊙	0	S 2	WSW 3	NNW 5
22	103.0	99.7	95.0	98.6	9.4	20.0	19.8	17.2	23.4	5.2	100	36	64	67	0.0	15.0	8.3	7.8	9 ≡	3 ⊙	8	C 0	SW 5	SW 2
23	92.9	94.7	95.9	94.5	15.8	22.7	15.7	17.5	24.2	9.3	98	44	66	69	0.3	15.5	6.0	7.3	10	3 ⊙	4	C 0	W 7	W 2
24	96.1	96.4	96.7	96.4	17.0	22.2	16.4	18.0	23.2	11.7	70	46	76	64	5.8	14.3	4.4	8.2	7 ⊙	9	8	WSW 4	WSW 9	SW 1
25	95.1	93.6	91.1	93.3	19.0	27.3	21.2	22.2	30.0	12.3	67	36	61	55	7.4	25.3	9.8	13.5	3	3 ⊙	1	SW 3	W 6	SW 1
26	90.4	90.0	89.6	90.0	20.4	27.6	22.6	23.5	29.8	14.2	68	39	75	60	7.7	22.6	7.4	12.6	4	8 ⊙	8	C 0	NW 2	C 0
27	86.7	85.1	85.7	85.8	21.3	31.7	19.8	23.2	33.3	16.9	75	38	83	65	6.3	29.2	3.9	13.2	8	3 ⊙	10	SE 1	SW 9	S 2
28	92.3	98.8	103.1	98.1	13.6	16.6	12.0	13.6	20.2	12.0	93	53	81	76	1.1	8.9	2.7	4.2	10 •	8	1	WNW 7	WNW 10	W 2
29	103.1	103.3	104.4	104.9	13.9	18.8	14.8	15.6	19.7	8.3	77	53	78	70	3.7	9.7	3.6	5.7	3 ⊙	8	0	WNW 4	NW 6	NW 1
30	105.0	104.2	102.4	103.9	15.6	24.0	17.8	18.8	25.6	9.6	79	38	73	64	3.7	18.4	5.2	9.1	0 ⊙	2 ⊙	0	NW 1	NW 3	C 0
31																								
M	92.4	92.3	92.3	92.4	16.1	21.6	16.6	17.7	24.0	11.7	79	53	77	70	4.0	13.1	4.3	7.2	5.7	6.3	5.7	2.6	5.1	1.8

Łódź - Lublinek

$H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 11\,m$

Maj - Mai 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	-	
2	7	0.3	.	-	▽° 12³⁵–13¹⁰; = 5³⁰–10⁴⁵ 19¹⁵–24; ⌓ 0-1 3⁰⁰–9²⁰ ⌓° 21³⁰–24
3	7	2.5	.	-	▽° 15¹⁶ 22¹⁰; (R) 13⁵⁰–5.3 R°–14²¹ (R)–14³⁵ SW-NE, 17³⁵–48 R°–18³⁰ (R)–19¹⁵ SW-NE; = 0⁰⁰–12²⁰; ⌓ 0-1 0⁰⁰–8⁰⁰
4	7	.	.	-	= 2³⁰–9²⁰
5	7	0.0	.	-	▽° 18⁵⁰–19⁰⁵; = 3³⁰–7²⁰; ⌓ 1 2⁰⁰–8⁰⁰; ⊕ 9⁴⁵–17¹⁵
6	7	0.4	.	-	▽1-0 13³⁰ 15⁵⁸; = 5³⁰–11³⁰, 20³⁰–24; ⌓° 22³⁰–24 [7.V: (R) 17²⁰–35 R°–17⁴⁰ (R)–18⁵⁰ NW-SE
7	7	4.7	.	-	▽° a ▽0-1 p...; (R) 15⁰⁵–08 R°–15¹⁵ (R)–15⁴⁵ NW-SE; ≫ 18¹⁰–2⁵; = 0⁰⁰–8³⁰; ⌓ 0-x na–a
8	7	8.5	.	-	▽0-1 10²⁵ 13⁴⁵ ▲1 10⁵⁶–11⁰² ▲ 13¹⁰–17, 15⁵⁸–16²⁵ ▽° p...; (R) 11³⁷–5² R¹–11⁰⁷ (R)–11³⁵ W-E R¹ 13¹⁵–⁴⁰ (R)–13⁵⁰ W-E R¹ 15⁵⁸–16²⁵
9	7	7.7	.	-	▽° 9³⁷ 22¹⁸ [8.V: ≫ a, p; = na–a
10	8	2.7	.	-	• 0-1 4⁰⁵–9³⁵ ▽0-1 9⁵⁷ 16³⁰ ▽° 19⁴⁰–20¹⁵
11	8	.	.	-	
12	8	0.1	.	-	▽° 17²³–26 ≫ 0⁰⁰–40; ⌓° 21³⁰–24
13	8	0.4	.	-	• 17⁰⁰–19⁴⁰ ▽°–21¹⁰; = 2³⁰–3⁴⁵ ≡ 0-1 7¹⁰ = –9⁴⁰; ⌓ 0-2 0⁰⁰–9³⁰
14	7	0.2	.	-	▽° 12⁰³–14; = 0³⁰–8³⁰
15	8	5.0	.	-	▽° 1⁵⁰–2¹³ 7⁰³ 13³⁵ ▽0-1 15²² 18¹⁰ ▲° 15³⁰–32; = 2²⁰–7³⁰; ⌓° na
16	8	0.9	.	-	▽° 0¹⁴–20 ▽° 0⁵⁰ 16¹⁷ • 18³⁸ 19¹⁵–22²⁰
17	6	1.7	.	-	• 0²⁰–1³⁹ 2²⁰ ▽° 11⁵⁰–12⁴⁰ •0-1 16⁴⁵; = 17²⁰–24
18	8	.	.	-	= 0⁰⁰–6³⁰
19	8	.	.	-	= 2³⁰–8⁰⁰
20	7	0.0	.	-	▽° 12⁰¹–14; = 6²⁰–9⁴⁰, 19⁴⁰–24
21	7	4.0	.	-	(R) 14¹⁵–16 ENE •R°–14²² (R)–15¹⁰ ▽° 14²² 16⁴⁰, 20⁵⁰–22³⁵; = 0⁰⁰–11⁰⁰; ⌓° na–a
22	8	.	.	-	
23	8	.	.	-	⌓° 2⁰⁰–8⁰⁰, 20³⁰–24
24	7	.	.	-	= 20²⁰–24; ⌓° 0⁰⁰–6³⁰; ⊕ 7³⁰–13³⁰
25	7	.	.	-	= 0⁰⁰–7³⁵ 20²⁰–24; ⌓° 1⁰⁰–8⁰⁰ 23³⁰–24
26	7	.	.	-	= 0⁰⁰–8⁴⁰; ⌓ 1-0 10⁰⁰–9⁰⁰
27	7	7.9	.	-	▽0-2 15⁵⁸–18¹⁵; (R) 11⁴⁵–13²⁰ S-E 15²⁰-58 R¹–16⁵⁰ (R)–17³⁰ S; = na–a ∞ a = p–np
28	5	4.5	.	-	(R) 13²⁷–35 ▽° R–13⁵⁷ (R)–14²⁵ SW-NE •°22⁵⁰–23²⁰; = 0⁰⁰–24
29	6	2.5	.	-	• 10⁵⁰–11⁰³; = 0⁰⁰–24
30	8	.	.	-	▽° 0⁵⁰–1²⁰, 1³⁵–3¹⁷ • 5³⁵–7⁰⁰... ³⁵; = 0⁰⁰–7⁰⁰, 21³⁰–24
31	7	.	.	-	= 0⁰⁰–9³⁰, 19²⁰–24; ⌓° 2³⁰–9⁰⁰
Σ	—	54.0	—	-	UWAGI.

Czerwiec - Juin

1	7	.	.	-	= na; ⌓° 2⁰⁰–7³⁰
2	7	1.0	.	-	(R) 18²⁵–19¹⁰ SW-NE, 21³⁰–22⁴⁰ E-NW; = np
3	8	.	.	-	▽0-1 2⁵⁵ 3²⁸; = 0⁰⁰–7⁰⁰
4	7	16.4	.	-	▽° 12⁵⁰–13⁰⁴ ▽0-2 14¹⁰–16¹⁵; (R) 11⁴⁰–12⁵⁰ R°–16¹⁰ (R)–16³⁵ SE-NW; = na–a; ⌓° na–a
5	7	1.0	.	-	▽0-1 14⁵²–15⁰⁵; = 3²⁰–7¹⁰
6	8	0.0	.	-	▽° 16¹⁰–18; ⌓° 2⁰⁰–9⁰⁰
7	7	.	.	-	(R) 16³²–19²⁵ SW-NE = na–a, np
8	7	2.8	.	-	▽° 12⁴⁰ 16³⁵, 20¹⁰ 23⁴⁰; (R) 11⁵⁰–12⁴⁰ R°–13¹⁵ (R)–13⁴² SW-SE, 13⁴⁵ 14⁰⁵ R°–14⁴⁰ (R)–16³⁸ W-E, 19⁰⁸–20¹⁰ R°–20³⁵ (R)–20⁵⁵
9	6	0.0	.	-	▽° 12²²–30 (R) 18⁵⁰–19³⁵ SW, = 0⁰⁰–2²⁰ ≡ –5⁵⁰ = –17³⁰, p–24 [8.VI: W-E; = na–a, ⌓° na–a
10	7	0.4	.	-	▽° 14¹⁷–45, 19⁴⁰–20²⁵; (R) 17⁴⁰–19²⁵ S-SW-NW, = na–a; ⌓ 0-x na–a; ∞ a
11	7	.	.	-	= 2³⁰–10³⁰, np; ⌓° na ⌓ 1-0 –9³⁰
12	7	.	.	-	= 0⁰⁰–9³⁰; ⌓ 1 2⁵⁰–7⁰⁰
13	8	0.0	.	-	▽° 20¹⁵–35 • 21³⁷
14	6	1.0	.	-	▽1-0 12²⁵–13⁵⁴ ▽° 19³³–44 • °20²⁵–23⁴⁰; = na, np
15	8	0.0	.	-	• 1⁵⁰–2⁵⁰, = 0⁰⁰–5⁸⁰
16	8	.	.	-	• 2⁴⁰–3¹⁵; = np; ⌓° np
17	8		.	-	= 0⁰⁰–7³⁰, np; ⌓° 0⁰⁰–8⁰⁰
18	7	0.0	.	-	= 0⁰⁰–8³⁰; ⌓° 2³⁰–7⁰⁰
19	7	0.0	.	-	• 7⁴⁰–8³⁰, 12³⁰ 14³⁵, = 4³⁰–8³⁰; ⌓° np
20	8	.	.	-	⌓° 0⁰⁰–8⁰⁰
21	8	0.0	.	-	▽° 18⁰⁰–19⁰²
22	8	1.5	.	-	(R) W 22⁴⁵–24, = 0¹⁰–1⁵⁰ ≡ 1-0 –8²⁵ = –9¹⁰
23	7	.	.	-	▽° 2²⁰–4²⁰ • °5¹⁰; (R) 0⁰⁰–2²⁰ R°–3⁰⁵ (R)–3¹⁵ W-N, = 5¹⁰–10⁴⁰
24	7	.	.	-	= 3³⁰–7³⁰; ⌓° 3⁰⁰–7³⁰
25	7	.	.	-	= 2⁴⁰–8⁴⁵ ∞ –9⁴⁰
26	7	.	.	-	= 6³⁰–8³⁰ 22³⁰–24
27	7	3.2	.	-	▽° 16²³–28 18³²–40 ▽0-1 19¹³–25; (R) 16²⁰–23 R°–16⁴⁵ (R)–17⁴⁵ SSW-E, 19⁰⁰–13 R°–19²⁵ (R)–20⁰⁰ SE; = 0⁰⁰–8³⁰
28	8	0.5	.	-	•0-1 3³⁰–9¹², ≫ 9²⁵–10⁰², 11¹⁵–14¹⁰
29	8	.	.	-	
30	7	.	.	-	= 5³⁰–8³⁰; ⌓° 3⁰⁰–8⁰⁰
31					
Σ	—	27.6	—	-	UWAGI.

Łódź - Lublinek φ = 51°44' λ = 19°24' Lipiec - Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	102.7	102.3	101.2	102.1	17.0	25.9	19.5	20.5	27.2	10.0	80	54	55	56	5.9	21.9	10.3	12.0	0 ⊙	3 ⊙	3	C 0	NE 2	E 1
2	101.0	99.8	98.3	99.7	19.7	28.5	21.2	22.6	31.1	10.8	61	30	39	30	8.8	27.2	10.4	15.5	0 ⊙	0 ⊙	0	C 0	NW 2	C 0
3	97.8	95.3	91.3	94.8	19.8	31.3	22.2	25.9	32.8	13.2	67	26	60	51	7.7	33.7	10.8	17.4	0 ⊙	0 ⊙	2	C 0	S 3	S 1
4	91.0	88.3	86.6	88.6	17.0	22.2	14.9	17.2	27.0	14.8	92	66	79	79	1.6	9.1	3.4	4.7	9	9	10	C 0	WNW 4	WNW 3
5	89.8	91.2	91.9	91.0	13.5	15.9	11.6	13.2	18.6	11.5	73	50	62	62	4.2	9.0	5.1	6.1	8	8	4	W 8	WSW 8	W 3
6	93.8	94.5	96.6	95.0	9.6	14.6	11.1	11.6	16.1	6.9	89	48	96	78	1.3	8.6	0.5	3.5	8	9 ⊙	8	SW 4	WSW 12	WSW 4
7	98.0	98.9	99.0	98.6	11.2	15.2	10.6	11.9	16.9	8.3	90	47	82	73	1.3	9.1	2.3	4.2	9	8	7	W 3	W 8	C 0
8	98.9	97.4	94.3	96.9	12.6	20.2	15.1	15.8	22.2	4.7	65	36	59	53	5.2	15.2	7.0	9.1	3 ⊙	7 ⊙	0	W 3	SW 4	SE 1
9	88.6	87.2	88.3	88.0	14.8	18.0	12.1	14.2	21.7	8.2	66	59	96	74	5.7	8.4	0.5	4.9	6 ⊙	10	4	SSE 3	SW 6	W 2
10	89.0	89.3	90.4	89.6	12.0	13.7	11.8	12.3	18.1	9.1	93	73	84	83	1.0	4.2	2.1	2.4	9	10 •	8	W 3	SSW 6	W 3
11	91.9	92.3	91.2	91.8	12.2	18.6	16.0	15.7	21.2	7.7	70	49	76	65	4.3	10.9	4.4	6.5	8	9	9	WSW 3	SW 6	C 0
12	88.4	86.9	85.3	86.9	16.0	25.2	20.3	20.6	27.5	11.6	88	50	73	70	2.1	16.0	6.5	8.2	6	6 ⊙	2	E 2	W 2	E 2
13	81.4	77.1	75.2	77.9	19.3	27.7	16.4	20.0	29.7	15.7	82	47	98	76	4.0	19.6	0.4	8.0	8	8	10 •	E 2	SSE 7	WNW 4
14	82.3	85.6	86.4	84.8	14.5	15.2	12.7	13.8	19.4	12.6	67	59	73	66	5.5	7.2	3.9	5.5	5 ⊙	9	2	WSW 9	WSW 9	E 2
15	86.7	88.3	89.7	88.2	15.0	21.6	18.2	18.2	23.4	10.5	78	56	71	68	3.6	11.3	6.0	7.0	10 •	7 ⊙	2	S 3	W 5	E 1
16	85.2	86.9	87.2	86.4	14.1	15.1	14.8	14.7	19.7	12.9	94	78	86	86	0.9	3.9	2.4	2.4	10 •	9	4	NE 3	NW 5	C 0
17	86.4	85.3	85.5	85.7	14.5	16.0	12.5	13.9	21.0	10.8	79	80	89	83	3.4	3.6	1.5	2.8	4 ⊙	9 • R	6	SW 1	WSW 4	SSW 3
18	84.9	85.3	85.5	85.2	12.0	15.6	13.8	13.8	19.4	10.3	96	78	86	87	0.3	3.9	2.2	2.2	10 •	9	2	W 5	W 7	C 0
19	86.4	86.8	86.8	86.7	13.2	16.4	13.0	13.9	19.4	9.8	94	77	91	87	0.9	4.2	1.4	2.2	9	9	2	C 0	SW 2	C 0
20	88.1	87.9	88.9	88.3	13.0	19.2	12.7	14.4	22.3	8.4	91	60	94	82	1.4	8.9	0.9	3.7	8	9 •	4	SE 1	NW 1	C 0
21	89.4	89.3	89.3	89.3	13.4	16.6	13.8	14.4	18.3	10.5	94	76	89	86	0.9	4.6	1.8	2.4	10	10	10	SW 3	WSW 7	WSW 5
22	89.1	89.5	90.3	89.6	13.8	13.6	13.3	13.5	18.8	13.0	91	87	92	90	1.5	2.0	1.3	1.6	10	10 (R)	9	W 5	W 4	W 4
23	91.7	93.0	95.0	93.2	13.0	15.4	14.0	14.1	17.8	10.7	88	73	89	83	1.8	4.8	1.8	2.8	8	10	10	W 3	WSW 6	W 2
24	97.1	98.7	100.6	98.8	12.8	15.5	11.4	12.8	17.1	11.4	84	60	90	78	2.4	7.0	1.4	3.6	9	9	4	W 3	W 5	C 0
25	102.1	102.1	101.3	101.8	12.2	16.1	14.0	14.1	17.1	10.4	85	60	80	75	9.7	7.4	3.2	6.8	9	10	10	W 1	W 6	WSW 2
26	98.4	96.0	90.7	95.0	11.4	20.6	17.6	16.8	22.4	10.0	90	56	67	71	1.4	10.6	6.6	6.2	10	9	10	SSW 3	WSW 5	S 3
27	87.8	85.6	85.9	86.4	17.2	24.2	17.4	19.0	26.5	14.2	73	51	80	68	5.2	14.9	4.0	8.0	6	9	10	SW 3	SW 8	SW 4
28	84.1	82.0	83.1	83.1	15.2	19.8	15.0	16.2	21.0	14.5	91	81	95	88	1.5	4.3	1.1	2.3	9	10	10 •	S 3	SW 6	W 2
29	86.2	89.9	92.2	89.4	11.8	15.9	13.0	13.4	18.6	11.6	95	68	86	83	0.6	5.8	2.1	2.8	10 •	8	6	NW 4	W 5	C 0
30	93.8	93.7	93.4	93.6	11.6	13.4	12.2	12.4	15.3	10.0	93	94	99	95	1.0	0.9	0.2	0.7	10	10 •	10 •	NNW 2	NNE 3	N 1
31	88.3	86.8	91.3	88.8	11.8	13.2	13.0	12.8	14.4	11.3	99	95	93	96	0.1	0.7	1.1	0.6	10 •	10 •	10 •	NW 5	W 8	W 8
M	91.0	90.8	90.7	90.8	14.0	18.7	14.7	15.5	21.4	10.6	84	61	82	76	3.0	9.6	3.4	5.3	7.5	8.2	6.1	2.8	5.4	2.0

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1	91.8	94.2	94.5	93.5	11.2	15.2	13.7	13.4	20.0	11.3	95	77	83	85	0.7	4.1	2.7	2.5	10 •	10	4	SSW 10	SW 7	C 0
2	93.9	91.8	92.1	92.6	14.0	24.4	16.0	17.6	26.0	9.2	80	46	92	73	3.2	16.5	1.6	7.1	0	4 ⊙	10	S 1	SSE 5	NW 4
3	94.0	94.1	97.2	95.1	14.9	16.4	12.6	14.1	20.6	12.6	97	86	88	90	0.5	2.7	1.7	1.6	10	10	0	SW 2	W 5	WNW 2
4	97.6	96.7	95.0	96.4	12.2	19.0	15.8	15.7	20.5	8.0	89	50	65	68	1.5	11.1	6.2	6.3	6	10	10	W 1	SW 4	SW 5
5	94.2	94.0	92.8	93.7	16.0	22.0	17.6	18.3	24.0	14.3	87	57	86	77	2.3	11.2	2.8	5.4	10	4 ⊙	0	W 4	W 7	C 0
6	90.6	89.5	88.3	89.5	19.5	28.9	22.9	23.6	30.8	14.3	73	44	67	61	6.1	22.4	9.5	12.6	3 ⊙	1 ⊙	4	S 6	SW 6	S 2
7	88.3	90.0	92.3	90.2	21.0	21.0	18.0	19.5	24.2	17.4	69	79	92	80	7.7	5.2	1.6	4.8	9	10	10 •	SW 2	W 1	W 2
8	96.1	95.3	94.3	95.3	14.8	21.2	18.4	18.2	23.7	10.7	79	47	75	67	3.4	13.5	5.3	7.4	3	9	5	C 0	E 2	E 2
9	95.6	96.8	98.2	96.9	19.0	27.1	20.2	21.6	28.4	15.0	80	45	94	73	4.4	19.6	1.4	8.5	4 ⊙	7 ⊙	10 •	C 0	W 5	C 0
10	97.7	95.7	90.3	94.6	18.7	25.5	23.1	22.6	28.2	18.1	95	68	88	84	1.1	10.4	3.4	5.0	10	9 ⊙	10 R	ENE 3	E 5	E 5
11	91.5	90.7	93.6	91.9	18.6	19.6	17.8	18.4	24.7	15.9	98	94	92	95	0.4	1.5	1.6	1.1	9	10 (R)	10	NW 2	NNE 3	W 3
12	94.2	92.7	92.4	93.1	15.6	21.1	14.0	16.2	21.3	13.9	96	69	93	86	0.7	7.7	1.1	3.2	9	9	10 •	C 0	S 2	NW 1
13	93.8	96.8	98.6	96.4	13.5	15.2	13.6	14.0	17.0	13.3	87	65	82	78	2.0	6.0	2.8	3.6	9	10	9	NW 4	NW 7	W 2
14	98.5	97.5	94.6	96.9	11.4	17.8	12.8	13.7	19.4	9.2	88	50	80	73	1.7	10.1	2.9	4.9	2 ⊙	9 ⊙	0	C 0	S 2	SE 1
15	91.0	89.9	88.4	89.8	13.6	15.5	14.4	14.5	19.6	10.3	81	89	87	86	3.0	1.9	2.2	2.4	9	9 • R	10	S 2	SW 3	SW 3
16	87.4	87.6	86.2	87.1	12.2	15.3	12.0	12.9	17.1	12.1	95	56	88	80	0.7	7.7	1.7	3.4	10 •	8 ⊙	10	SW 3	WSW 8	SW 8
17	85.3	85.0	85.7	85.3	11.4	16.8	11.6	12.8	18.3	10.3	83	53	88	75	2.3	8.9	1.6	4.3	3 ⊙	8 ⊙	9	SW 5	W 5	NW 3
18	86.0	86.3	85.9	86.1	9.6	12.9	12.2	11.7	17.5	8.5	97	85	88	90	0.4	2.3	1.7	1.5	10	10	5	W 3	W 5	W 5
19	84.1	82.2	83.1	83.1	11.2	17.6	13.6	14.0	19.2	9.4	95	70	86	84	0.7	6.1	2.2	3.0	10 •	10	7	SW 6	SW 10	SW 3
20	83.9	85.3	88.6	85.9	13.2	14.6	11.8	12.8	18.2	11.5	84	78	89	84	2.5	3.6	1.5	2.5	8	9 • ⊙	4	WSW 7	W 9	WSW 5
21	89.8	90.6	89.4	89.9	13.0	16.6	17.0	15.9	19.1	11.1	91	68	76	78	1.4	6.1	4.7	4.1	10	9	10	WSW 8	W 9	SW 4
22	87.4	85.5	85.1	86.0	15.3	20.2	14.5	16.1	22.5	12.0	77	64	84	75	4.1	8.7	2.7	5.2	6 ⊙	10	9	SE 6	SE 9	SW 5
23	86.5	87.4	90.9	88.3	13.1	14.7	11.2	12.6	16.3	10.9	85	81	90	85	2.3	3.1	1.3	2.2	8	8 •	3	SW 7	WSW 6	WSW 5
24	92.5	95.9	94.9	95.8	10.4	15.0	12.4	12.6	17.4	9.0	87	53	87	76	1.6	7.9	1.9	3.8	3 ⊙	5 ⊙	9	W 6	W 9	W 2
25	93.7	94.2	95.3	94.4	12.3	16.1	13.2	13.7	16.7	11.1	85	73	93	84	2.2	4.9	1.1	2.7	7 ⊙	10	9	SW 5	SW 7	SW 3
26	96.8	98.5	98.7	98.0	13.6	16.9	16.6	15.9	20.8	12.5	93	73	89	85	1.1	5.2	2.2	2.8	10	10	9	SW 1	W 3	SE 1
27	99.2	99.7	99.5	99.5	15.6	24.0	18.0	18.9	26.0	13.6	93	55	80	77	0.9	13.5	4.0	6.1	2 ⊙	2 ⊙	0	S 1	W 3	SW 1
28	101.7	103.3	103.3	102.8	14.7	20.4	15.6	15.6	21.7	13.3	98	59	84	80	0.4	9.9	2.5	4.3	6	10	4	C 0	WNW 8	W 1
29	102.7	101.2	100.5	101.5	13.0	21.4	14.3	15.8	22.4	10.3	94	55	88	79	0.9	11.4	2.0	4.8	5 ⊙	8 ⊙	3	W 3	W 6	C 0
30	102.0	102.7	103.2	102.6	9.8	19.6	14.5	14.6	21.3	7.6	97	49	79	75	0.3	11.6	3.4	5.1	2 ⊙	6 ⊙	0	C 0	E 1	C 0
31	105.2	106.3	106.8	106.1	11.2	21.8	16.4	16.4	23.8	8.3	97	54	88	80	0.3	11.9	2.3	4.8	0 ⊙	1 ⊙	0	C 0	W 3	C 0
M	93.3	93.4	93.3	93.4	14.0	19.2	15.3	16.0	21.3	11.8	89	64	85	79	2.0	8.6	2.7	4.4	6.5	7.9	6.2	3.2	5.3	2.4

Łódź – Lublinek $H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 11\,m$ **Lipiec – Juillet 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 2³⁰–9¹⁵, ⌒° 3⁰⁰–7⁰⁰
2	7	.	.	–	⌒° 2⁰⁰–7³⁰
3	8	.	.	–	= 3³⁰–8³⁰ ∞–9³⁰
4	7	1.8	.	–	▽⁰⁻¹ 18³⁰–19⁰⁴, (↙) 15³⁵–17²⁰ SW–SE, 18²⁰⁻³⁰ ↙°–19⁰⁴ (↙)–19³⁵ W–E; = na–a, p
5	7	0.2	.	–	
6	8	2.5	.	–	▽° 7¹⁵–22, 15⁰⁴ 22²⁴, ≫ 13²⁰–15¹⁵
7	8	.	.	–	
8	8	.	.	–	⌒° 2⁰⁰–8³⁰
9	7	4.2	.	–	•° 14²⁵–16³⁵ ▽⁰⁻¹ 17⁵⁵–18⁵⁷; = 5³⁰–7⁰⁰ ∞–9³⁰
10	7	0.0	.	–	•° 13³⁵ 14⁰³ ▽° 15⁴³–16⁰⁵; = 5¹⁵–8²⁰
11	8	10.6	.	–	= 2¹³⁰–24
12	7	.	.	–	▽⁰⁻¹ 3¹⁵–4³⁵, (↙) 2⁵⁰ 3²⁰ ↙–4⁰⁰ (↙)–4⁴⁰ NW–S; = na–a; ⊕ 9³⁰–11¹⁰
13	7	7.3	.	–	▽⁰⁻¹ 19⁰⁷ 24; (↙) 19⁰⁵⁻⁰⁷ ↙°–21⁰⁵ (↙)–21²⁵ S–N; = 3³⁰–10²⁰ ∞ a, ⌒° 4⁰⁰–7³⁰
14	8	0.0	.	–	▽¹⁻⁰ 0⁰⁰–16 ▽° 17²⁻²⁶; ≫ 8¹⁰–12³⁰; = 0¹⁸–1⁵⁰
15	8	19.5	.	–	•° 6⁵⁰ 9⁰⁸ ▽° 14³⁶–15⁰⁴, (↙) 14³⁰⁻³⁶ ↙°–15¹⁰ (↙)–15²⁰ W–E
16	7	4.6	.	–	▽° 4⁴⁸–5³⁰ •¹–6⁵⁰ •°–11⁴⁰ 12³⁵ ⌒° na
17	8	3.3	.	–	▽° 13³⁵–18⁵², (↙) 13²⁵⁻³⁵ ↙°–13⁴⁵ (↙)–13⁵⁵ SW–W; ⌒° na–a
18	7	8.9	.	–	•° 2¹⁰ 3⁴⁵ •⁰⁻¹ 4³⁰–12⁰⁵ ▽° 12²⁰⁻³⁵ 14²⁵⁻⁴⁵; ⌒° np
19	7	1.7	.	–	•° 9⁵⁰ 11⁴⁰–12⁰⁷ ▽° 14⁵⁵–15²⁵, (↙) 17³⁵ 19⁴⁵ SW–SE; = 3¹⁵–13³⁰ np, ⌒⁰⁻² na–a
20	7	0.3	.	–	▽° 13⁴⁰ 14⁰⁸, 19¹⁵–35, (↙) 17⁰²–⁴⁵ S–E; = na–a, p–np, ⌒⁰⁻¹ na–a
21	7	1.2	.	–	▽⁰⁻¹ 8⁵⁰ 17⁵⁸; = 0⁰⁰–9⁰⁵
22	7	5.4	.	–	•° 0³⁵ 3³⁰ ▽° 13⁰²–⁴⁰, 18¹⁰–19³⁰, (↙) 12³⁵–13⁰² ↙°–13⁴⁰ (↙)–14⁴⁵ W–E, 18⁰⁵⁻¹⁰ ↙–19³⁰ (↙)–19⁵⁰ W–E; = na
23	7	.	.	–	= 4³⁰–8⁴⁰
24	8	.	.	–	⌒° 22³⁰–24
25	8	0.2	.	–	⌒° 0⁰⁰–9⁰⁰
26	7	0.0	.	–	•° 5⁴⁵ 6⁰⁵ 7²⁰…³⁵ 9²⁰…⁵⁰; = na–a; ⌒° na
27	7	0.2	.	–	•° 18⁰³ 20³⁰–21²⁰ 22⁵⁵ 23¹⁵
28	7	27.9	.	–	▽° 7²⁰⁻²⁸ •° 7⁵⁸ 13⁰⁵ ▽° 16³²⁻³⁶ •⁰⁻¹ 20³⁵–24; = na; ≫ 14³⁰–⁴⁵
29	8	0.3	.	–	•⁰⁻¹ 0⁰⁰–8²⁵ •° 9⁵⁵–11⁰⁵, ⌒° 22⁰⁰–24
30	6	20.5	.	–	•° 11²⁰–23³⁰ 24, ⌒° 0⁰⁰–10⁰⁰
31	6	29.8	.	–	•⁰⁻¹ 0⁰⁰ 4¹⁰–24
Σ	–	160.4	–	–	UWAGI.

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1	7	1.8	.	–	•°0⁰⁰–2³⁰ 3⁴⁰–6⁰⁰ 7¹⁰ •¹–7²⁰ •°–12⁴⁵; = 20²⁰–24, ≫ 7⁴⁵–10³⁰, ⌒° np
2	7	1.4	.	–	= 0⁰⁰–11²⁰ ∞–12³⁰, 18⁴⁰–24, ⌒⁰⁻² 0⁰⁰–10⁰⁰
3	7	2.0	.	–	•⁰⁻¹ 5⁵⁰–7²⁵ 9⁴⁵ 10⁵⁰ ▽¹⁻⁰ 13⁴⁵ 14⁰⁸; = 0⁰⁰–13¹⁰
4	7	0.1	.	–	•° 21⁴⁸–55; = 1³⁰ 9³⁰, ⌒⁰⁻² 20⁰⁰–11⁰⁰, ⊕ 10¹⁵–13¹⁵
5	7	.	.	–	•° 4⁴⁵–51, = 2⁰⁶–10⁰⁰, 20⁴⁵–24, ⌒° 21⁰⁰–24
6	7	.	.	–	= 0⁰⁰–11¹⁵, ⌒⁰⁻¹ 0⁰⁰–9⁰⁰
7	7	0.6	.	–	▽° 12¹⁵–25 •° 20⁵⁰ 21⁴⁵–22⁴⁵; = 4³⁰–13²⁰
8	8	.	.	–	= 2³⁰–4⁴⁵, = ¹⁻⁰ 6⁴⁰ = –10³⁰
9	7	3.2	.	–	•° 10¹⁵–23¹⁰; = 5³⁰–8⁰⁰ ∞–11⁰⁰ = 23¹⁰–24, ⌒° 2⁰⁰–8⁰⁰
10	7	31.2	.	–	•° 2¹⁸ 3²⁵ •° 6⁵² 7¹⁵ ▽° 21²⁵–22⁰⁷ ▽⁰⁻² 23¹⁰–24; (↙) SW 21¹⁵–25 ↙–22⁰⁷ (↙)–np ↙⁰⁻² 24; = 0⁰⁰ 10⁴⁰, 20³⁰ 24
11	5	2.4	.	–	▽²⁻⁰ 0⁰⁰–2⁴³ ▽⁰⁻¹ 9²⁰ 21⁰⁵, ↙²⁻⁰ 0⁰⁰–1¹⁰ (↙)–1⁴⁰ NE, 12¹⁰ ↙ 12⁴⁰–13³⁰ (↙)–14²⁵ SW–SE; = na
12	7	18.4	.	–	•⁰⁻² 15⁵⁰ 16¹⁰–24, = 2⁰⁰–5⁵⁰ =⁰⁻¹ 7²⁵ = –11³⁰
13	8	.	.	–	•° 0³⁰ 0¹⁰ 4³⁰, = 5²⁰–7³⁰, ⌒° 22⁴⁵ 24
14	8	.	.	–	⌒⁰⁻² 0⁰⁰–11⁰⁰
15	7	3.3	.	–	•° 8⁴⁵ 11³⁵ ▽⁰⁻¹ 13²⁴–⁴⁵ 14²³ 15⁰⁰ 17⁴⁵ 18¹⁰ 22⁵⁰–23⁰⁰, (↙) 13²⁰⁻²⁴ ↙°–13³⁵ (↙)–13⁴⁵ W–E, = na–a, ⌒° na–a
16	8	0.2	.	–	•° 7⁴⁰ 8⁴⁰ ▽° 21⁴⁸–22⁰⁴; = 8⁴⁰–9³⁰
17	8	.	.	–	▽° 1⁴⁵–2²⁵ 4⁰⁵–⁰⁸
18	7	2.5	.	–	▽° 15²⁵–⁴⁰, = 3³⁰–11³⁰, ⌒⁰⁻¹ 2³⁰–15⁰⁰, ⌒ 18³⁰–⁴⁵
19	7	1.0	.	–	•° 6⁵⁰–8⁴⁵ 10⁴⁰ 11⁰⁰ ▽° 14⁴⁵–⁵⁰ 18²⁷–⁴⁵, = 3³⁰–11³⁰, ≫ 13³⁰–14⁴⁰
20	8	4.4	.	–	▽° 13²⁸–⁴⁵ ▽⁰⁻² 16⁴⁰–17³⁵ ▲° 18⁵²–⁵⁸, (↙) 16⁴⁰–⁵⁰ ↙²–17²⁰ (↙)–17³⁵ NW–SSE, = na, ≫ 16⁵⁰–17¹⁰
21	7	0.2	.	–	•° 2⁵⁰ 4³⁰ 7⁴⁵–8³⁰ 9¹⁵
22	7	0.1	.	–	▽° 13⁵⁰–14⁰⁵ 17⁴⁵–18⁰⁷, ≋ 17⁴⁵–18¹⁰
23	7	5.0	.	–	▽⁰⁻¹ 11¹⁵–18⁵⁸
24	8	.	.	–	⌒° np
25	6	0.0	.	–	•° 15⁴⁵ 16¹⁰, = 2¹⁵–24, ⌒⁰⁻¹ 0⁰⁰–9⁰⁰
26	6	1.8	.	–	= 0⁰⁰–15³⁰, 18³⁰–24, ⌒° 2⁰⁰–14⁰⁰ 22³⁰–24
27	7	.	.	–	▽° 20⁷–³⁰ 2⁴⁵–3¹⁰ •° 4¹⁵, ↙° 20⁷ 3²⁵; = 0⁰⁰–11¹⁵, ⌒° na, np
28	7	.	.	–	= 1³⁰ 9³⁰, ⌒⁰⁻² 0⁰⁰–12⁰⁰ 20⁴⁵–24
29	7	.	.	–	= 4³⁰ 5¹⁵ = –6³⁰ = –11³⁰, ⌒⁰⁻² 0⁰⁰–9⁰⁰
30	8	.	.	–	= 4⁰⁰–6²⁵ = °7⁵⁰ = –9³⁰, 23³⁰–24, ⌒⁰⁻¹ 2⁰⁰–9⁰⁰
31	7	.	.	–	= 0⁰⁰–9³⁰, 19⁴⁰–24, ⌒⁰⁻¹ 3⁰⁰–11⁰⁰ ⌒° 22⁰⁰–24
Σ	–	79.8	–	–	UWAGI.

Łódź - Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$

Wrzesień - Septembre 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	107.2	106.1	102.7	105.3	14.8	25.2	18.4	19.2	27.5	11.5	87	47	75	69	2.2	17.1	5.7	8.3	0 ⊙	0 ⊙	0	E 1	C 0	E 1
2	100.9	99.1	96.0	98.7	15.3	28.3	18.4	20.1	30.2	13.0	84	31	65	59	2.8	26.4	8.0	12.4	0 ⊙	1 ⊙	0	C 0	SW 4	S 2
3	92.8	91.4	88.8	91.0	17.1	27.4	19.5	20.9	29.0	13.3	70	33	59	54	5.8	24.4	9.2	13.1	0 ⊙	3 ⊙	1	S 3	SW 6	S 2
4	88.7	90.3	92.4	90.5	15.4	24.0	15.0	17.4	24.8	13.9	79	55	81	72	3.7	13.5	3.3	6.8	8 ⊙	2 ⊙	0	W 1	NNW 3	C 0
5	91.7	90.3	87.3	89.8	12.8	24.8	19.4	19.1	26.5	11.3	93	50	77	73	1.1	15.7	5.2	7.3	8	0 ⊙	7	E 2	ESE 4	E 5
6	84.5	85.5	85.5	85.2	16.2	17.2	16.3	16.5	21.0	15.9	95	95	97	96	1.0	1.0	0.6	0.9	10 •	10 •	10	C 0	W 3	SW 3
7	84.2	83.8	85.2	84.4	14.8	18.0	14.2	15.3	19.0	13.3	93	81	67	80	1.1	3.8	3.3	3.4	10	10 •	1	SSW 3	SW 3	WSW 7
8	85.6	87.1	88.4	87.0	10.9	12.7	12.2	12.0	15.0	10.2	79	71	88	79	2.7	4.3	1.7	2.9	9	10	10	SW 8	WSW 7	WSW 7
9	90.9	92.3	92.9	92.0	11.8	15.4	12.8	13.2	17.4	11.3	93	74	79	82	1.0	4.6	3.1	2.9	7	9	9	WNW 5	WNW 8	W 7
10	94.2	94.8	95.3	94.8	11.0	14.4	11.3	12.0	15.2	10.2	90	68	93	84	1.3	5.3	1.0	2.5	10	10	10	W 6	W 6	W 3
11	95.1	95.0	94.0	94.7	11.2	15.6	12.0	12.7	17.3	10.8	95	67	79	80	0.7	5.9	3.0	3.2	10	9	9	W 2	W 4	SW 2
12	91.5	90.9	91.5	91.3	9.6	18.4	13.4	13.7	21.1	7.6	79	59	95	78	2.6	8.7	0.7	4.0	8	7 ⊙	10	S 3	SW 5	SW 3
13	92.4	93.3	95.4	93.0	12.0	16.6	14.0	14.2	18.5	11.2	93	68	85	82	1.0	6.1	2.3	3.1	10	7 ⊙	10	SW 4	WSW 6	SW 1
14	90.0	89.5	87.8	89.1	12.6	17.4	16.5	15.8	20.1	11.3	91	82	92	88	1.4	3.6	1.6	2.2	10	9	10 •	SE 2	SW 4	SW 3
15	91.7	97.1	99.4	96.1	13.8	14.3	11.3	12.7	17.6	11.2	80	75	85	80	3.2	4.1	2.0	3.1	9	9	0	W 10	W 9	C 0
16	99.4	99.4	99.3	99.4	13.1	22.6	15.8	16.8	24.6	9.5	84	62	94	80	2.5	10.4	1.1	4.7	9	6 ⊙	0	SW 1	W 6	C 0
17	99.2	98.9	97.9	98.7	14.0	27.7	18.8	19.8	28.6	11.5	91	41	74	69	1.5	22.1	5.7	9.8	0 ⊙	0 ⊙	0	C 0	S 7	S 1
18	97.3	97.2	98.3	97.6	15.4	26.4	18.1	19.5	27.9	13.6	76	56	93	75	4.3	15.2	1.5	7.0	7	4 ⊙	0	S 2	WNW 7	NNW 2
19	100.5	100.4	100.1	100.3	10.4	18.7	11.6	13.1	20.1	9.0	96	46	85	75	0.5	11.7	2.3	4.8	0 ⊙	0 ⊙	0	C 0	NNW 5	C 0
20	101.7	101.8	101.4	101.6	8.6	16.4	11.6	12.0	18.4	7.6	94	60	76	77	0.6	7.4	3.2	3.7	5	4 ⊙	0	ENE 3	ENE 7	ESE 4
21	102.5	103.0	103.8	103.1	8.8	16.4	9.3	11.0	18.1	6.0	84	49	75	69	1.8	9.4	2.9	4.7	0 ⊙	1 ⊙	0	E 3	ENE 6	E 2
22	104.9	106.2	106.3	105.8	6.2	16.1	9.2	10.2	18.1	3.5	85	40	66	64	1.5	11.0	3.9	5.5	0 ⊙	0 ⊙	0	E 3	E 5	E 1
23	106.0	104.6	102.9	104.5	7.1	16.8	9.2	10.6	18.7	4.3	64	33	62	53	3.6	12.7	4.4	6.9	7 ⊙	0 ⊙	0	E 3	ENE 5	E 2
24	101.2	100.4	99.4	100.3	5.6	19.1	10.4	11.4	21.2	3.6	77	37	75	63	2.1	13.9	3.2	6.4	0 ⊙	0 ⊙	0	E 2	E 1	ESE 3
25	98.2	97.9	99.6	98.6	7.0	21.8	14.2	14.3	23.5	5.0	84	40	84	69	1.6	15.8	2.5	6.6	0 ⊙	3 ⊙	4	ESE 1	SW 5	WNW 4
26	101.0	100.7	98.6	100.1	9.8	16.8	12.7	13.0	18.4	9.8	100	59	78	79	0.0	7.9	3.3	3.7	10 ≡	8 ⊙	10	NW 2	W 3	E 1
27	97.3	96.6	96.3	96.7	9.4	15.9	9.4	11.0	17.7	9.4	96	56	78	77	0.5	8.0	2.6	3.7	8	5 ⊙	0	C 0	W 1	C 0
28	97.3	98.0	99.1	98.1	6.2	17.0	10.8	11.2	19.5	4.5	98	45	72	72	0.2	10.7	3.7	4.9	0 ⊙	0 ⊙	0	E 2	E 4	SE 2
29	99.2	98.3	97.6	98.4	7.8	19.2	13.2	13.4	20.3	5.9	80	44	71	65	2.1	12.3	4.5	6.3	0 ⊙	5 ⊙	10 •	SE 3	ESE 5	SE 4
30	97.1	97.1	96.9	97.0	10.2	15.6	15.0	12.4	16.1	10.0	92	76	69	79	0.9	3.7	4.6	3.1	10	9	6	ESE 4	SE 6	E 7
31																								
M	96.1	96.2	95.9	96.1	11.3	19.1	13.7	14.4	21.0	9.6	87	57	79	74	1.8	10.6	3.4	5.3	5.5	4.7	3.9	2.6	4.8	2.7

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1	98.4	99.8	101.5	99.9	6.1	11.1	9.9	9.2	15.9	5.6	95	72	88	85	0.4	3.7	1.4	1.8	10	9	0	E 7	E 9	ESE 5
2	103.2	104.5	104.7	104.1	9.3	13.2	11.2	11.2	15.6	8.7	96	76	85	85	0.5	3.7	2.3	2.2	10	10	0	E 5	E 8	E 5
3	105.7	105.0	104.4	105.0	8.4	16.5	12.6	12.5	17.5	7.6	89	54	68	70	1.2	8.7	4.7	4.9	0 ⊙	4 ⊙	0	E 5	E 10	E 7
4	103.6	103.3	102.6	103.2	7.9	17.8	13.0	12.9	19.6	7.2	91	44	55	63	0.9	11.5	6.7	6.4	0 ⊙	1 ⊙	0	E 6	ESE 9	E 7
5	102.2	102.2	102.6	102.3	7.9	18.8	12.3	12.8	20.5	7.3	78	41	60	60	2.3	12.7	5.8	6.9	8 ⊙	8	0	E 6	SE 5	E 5
6	101.8	100.0	97.2	99.7	7.2	18.4	12.6	12.7	21.1	5.7	83	45	61	63	1.8	11.8	5.7	6.4	0 ⊙	0 ⊙	0	E 5	ESE 5	ESE 6
7	93.4	90.4	90.0	91.3	7.6	18.1	12.6	12.7	19.1	7.2	79	38	72	63	2.2	13.0	4.1	6.4	0 ⊙	0 ⊙	10	ESE 8	SE 12	E 5
8	88.5	88.3	90.4	89.1	8.0	16.6	11.2	11.8	18.3	7.7	75	49	66	63	2.7	9.7	4.5	5.6	8	8	8	ESE 7	SE 8	ESE 4
9	98.0	102.5	105.9	102.1	9.8	12.7	7.6	9.4	15.4	6.5	97	85	100	94	0.3	2.3	0.0	0.9	10	10	0	SW 1	W 2	C 0
10	107.8	107.9	107.2	107.6	3.2	18.3	9.0	9.9	19.7	0.1	100	60	89	83	0.0	8.4	1.3	3.2	5 ≡	8 ⊙	0	C 0	E 1	E 1
11	105.9	104.1	102.8	104.3	6.2	18.2	9.2	10.7	19.6	5.6	100	46	81	76	0.0	11.3	2.1	4.5	9 ≡	0 ⊙	0	ESE 2	SE 6	E 2
12	102.1	102.5	104.0	102.9	6.8	16.6	10.0	10.8	18.0	5.4	96	59	95	85	0.3	7.9	0.7	3.0	9	2 ⊙	6	C 0	WNW 5	C 0
13	104.4	104.7	105.1	104.7	3.2	12.3	5.7	6.7	14.1	2.5	98	66	100	88	0.2	4.8	0.0	1.7	8 ⊙	8	3	NW 1	NW 7	NW 1
14	105.6	102.1	101.2	102.3	5.0	10.3	9.6	8.6	11.8	1.6	100	82	95	92	0.0	2.2	0.7	1.0	10 ≡	10	10 •	W 4	W 9	WNW 5
15	101.7	100.3	98.8	100.3	9.4	11.8	10.0	10.3	12.7	9.3	95	76	79	83	0.6	3.3	2.5	2.1	10	10	10	WNW 5	WSW 7	W 6
16	97.6	96.3	93.1	95.7	8.3	11.7	7.6	8.8	14.6	7.4	84	64	86	78	1.7	4.8	1.4	2.6	10	8	0	W 1	SW 3	SW 1
17	90.1	86.1	78.9	85.0	7.8	12.4	12.0	11.0	15.0	5.2	94	71	75	80	0.6	4.2	3.5	2.8	8	9	8	SW 3	SW 4	S 4
18	70.5	69.9	71.5	70.6	11.4	13.5	14.9	13.7	15.8	9.9	90	77	61	76	1.4	3.5	6.5	5.8	10	10 •	9	SE 5	SE 8	SE 8
19	74.0	76.3	79.8	76.7	14.6	17.2	17.1	16.5	19.3	14.0	58	57	58	58	7.0	8.3	8.1	7.8	10	10	8	SE 4	SE 5	SE 4
20	84.3	86.5	87.1	86.0	11.1	16.0	14.4	14.0	18.9	10.4	88	71	80	80	1.6	5.2	3.2	3.3	8	9	5	C 0	ENE 2	E 7
21	87.2	89.9	95.7	90.9	9.4	16.3	9.8	11.3	17.7	9.3	92	52	82	75	1.0	8.9	2.2	4.0	3	8	4	E 5	SSE 9	E 3
22	99.4	101.1	101.6	100.7	3.5	10.2	9.0	7.9	13.1	3.1	97	82	92	90	0.2	2.2	1.0	1.1	8 ⊙	8	10	E 3	SE 3	SE 2
23	101.2	101.9	101.4	101.5	4.7	10.5	8.0	7.8	12.1	4.5	82	77	92	84	1.5	2.9	0.9	1.8	8	10	6	E 5	ESE 4	ESE 3
24	100.9	101.0	99.0	100.3	7.8	13.0	9.0	9.7	14.9	6.9	87	69	84	80	1.4	4.6	1.9	2.6	9	9	4	SSE 3	SW 4	S 4
25	95.5	94.9	94.2	94.9	6.4	14.2	11.4	10.8	15.5	4.9	84	55	76	72	1.6	7.3	3.3	4.1	6 ⊙	10	10	SE 7	S 8	S 7
26	94.2	93.1	92.4	93.2	10.8	14.2	10.0	11.2	15.6	10.0	70	51	79	67	3.9	7.9	2.5	4.8	10	10	10	SSE 3	S 9	SSE 2
27	90.6	89.1	89.1	89.6	8.0	17.0	10.3	11.4	18.4	7.1	82	44	71	66	1.9	10.9	3.6	5.5	8	9	5	SE 2	SE 7	SE 2
28	89.9	89.9	89.0	89.6	7.6	15.8	8.6	10.2	17.6	6.6	90	63	94	82	1.0	6.6	0.6	2.7	4	5 ⊙	0	C 0	S 1	C 0
29	88.3	88.0	91.2	89.2	9.2	11.5	8.4	9.4	12.7	5.5	97	91	94	94	0.3	1.2	0.6	0.7	9	10 •	10	C 0	WNW 2	WNW 4
30	95.8	95.9	94.6	94.1	6.6	8.2	5.0	6.2	11.6	4.8	94	89	100	94	0.5	1.2	0.0	0.6	10	8	0	S 1	S 1	C 0
31	95.9	95.6	95.5	95.7	3.2	9.2	7.8	7.0	11.6	2.5	100	92	82	91	0.0	0.9	2.0	1.0	10 ≡	9	0	C 0	SW 5	SW 8
M	95.9	95.8	95.9	95.9	7.6	14.2	10.3	10.6	16.2	6.5	89	64	81	78	1.3	6.3	2.7	3.4	7.4	7.4	4.4	3.3	5.7	3.8

Łódź – Lublinek

$H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 11\,m$

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–9¹⁰, ⌒ 0-2 0⁰⁰–10¹⁵ ⌒ ° np
2	7	.	.	–	= 5³⁰–9³⁰, ⌒ ° 0⁰⁰–10⁰⁰
3	7	.	.	–	⌒ ° 1¹⁰–8³⁰
4	7	.	.	–	⌒ 2²⁰–4⁴⁰
5	7	0.1	.	–	= 4³⁰–10⁰⁰ ∞–12³⁰ 14⁰⁰–24, ⌒ ° 0⁰⁰–8⁰⁰
6	6	4.4	.	–	• ° 7²⁵–8¹⁰ ▽ 0-1 12⁵⁰–14⁴⁵ • ° 18¹⁵–50 • ° –19⁴⁰, ∞ na = –24, ⌒ ° np
7	6	0.1	.	–	• ° 10⁵⁰ 11¹⁵ ▽ ° 12⁵⁰–13¹⁰, 13³⁵–14⁴⁵ • ° 15⁴⁶ 16¹⁵, = 0⁰⁰–15¹⁰, ⌒ 0-1 0⁰⁰–10⁰⁰
8	8	1.0	.	–	• ° 2⁰⁵⁰–24
9	7	0.0	.	–	• ° 0⁰⁰–10 • ° 0¹⁰–30, 12⁵⁰–56
10	7	0.1	.	–	▽ ° 23⁴⁵–24, ⌒ ° 5⁴⁵–8⁰⁰
11	7	.	.	–	▽ ° 0⁰⁰–10, = 6³⁰–12³⁰, 19²⁰–24
12	7	3.5	.	–	▽ ° 17⁰²–18¹⁷, = 0⁰⁰–10, 5³⁰–12³⁰, 18¹⁷–24, ⌒ ° na – a
13	7	.	.	–	= 0⁰⁰–12³⁰, 19³⁰–24
14	6	4.6	.	–	• ° 10⁵⁰ 12⁰⁵, • 1-0 21¹⁵–23³⁵, = 0⁰⁰–15³⁰, 19³⁰–23⁰⁰
15	8	.	.	–	⩔ 7⁰⁰–50, ⌒ ° 21⁰⁰–24
16	8	.	.	–	= 20⁴⁰–24, ⌒ 0-1 0⁰⁰–9⁰⁰ ⌒ ° 20⁰⁰–24
17	7	.	.	–	= 0⁰⁰–9⁴⁰, ⌒ 0-1 0⁰⁰–10²⁰
18	7	.	.	–	= 19³⁰–24, ⌒ ° 3⁰⁰–9⁰⁰, 21⁰⁰–24
19	8	.	.	–	= na, ⌒ ° na, 21⁰⁰–24
20	8	.	.	–	= 6¹⁵–12²⁵, ⌒ 0-1 0⁰⁰–7⁰⁰
21	8	.	.	–	⌒ ° 4⁰⁰–9⁰⁰
22	8	.	.	–	= 6²⁰–9³⁰, ⌒ ° 3⁰⁰–9⁰⁰
23	8	.	.	–	⌒ ° 2⁰⁰–9⁰⁰
24	7	.	.	–	≈ 6²⁰–10³⁰, = np, ⌒ ° 5⁰⁰–8³⁰, np
25	6	.	.	–	= 0⁰⁰–9⁴⁰ ∞–20³⁰ = – 24, ⌒ ° 0⁰⁰–8⁰⁰
26	8	2.5	.	–	▽ ° 23³⁶–24, (◹) W 23⁰⁶ ◹–24, = na = 0-1 –6⁴⁰ = 2 –9¹⁰ = 0-1 –9²⁰ = –11³⁰ ⌒ 0-2 na – p
27	7	.	.	–	▽ ° ◹ 0⁰⁰–08 (◹) – 0¹⁴ SE ▽ ° 0⁵⁰–3¹⁵, = 5⁴⁰–11⁰⁰, np; ⌒ ° 20³⁰–24
28	8	.	.	–	= 0⁰⁰–12³⁰, 18³⁰–24, ⌒ 0-2 0⁰⁰–10³⁰
29	7	4.9	.	–	• ° 20⁴⁰ 23²⁹, = 0⁰⁰–10³⁰, ⌒ ° 3³⁰–10⁰⁰
30	6	0.0	.	–	▽ 0-1 2⁰⁰ 5³⁵ • ° 9⁵⁰ 19²⁰, (◹) 1²⁸–2⁰⁰ ◹ ° –2²⁰ (◹) – 2⁴⁰ NW – SE, = 6³⁰–14³⁰
31					
Σ	–	21.2	–	–	UWAGI.

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1	7	.	.	–	= 4³⁰ 12³⁰, ⌒ ° 0³⁰–7⁰⁰
2	7	.	.	–	= 5³⁰–9³⁰ 13³⁰ 19³⁰, ⌒ ° 1⁰⁰–9⁰⁰
3	7	.	.	–	= 5¹⁵–9²⁰, ⩔ 10³⁰–14⁴⁰, ⌒ ° 1⁰⁰–9⁰⁰
4	7	.	.	–	= 5³⁰–9³⁰, ⩔ 13¹⁵–16³⁰, ⌒ ° 2⁰⁰–8⁰⁰
5	7	.	.	–	= 5³⁰–7³⁰
6	7	.	.	–	= 6²⁰–9¹⁵
7	7	0.6	.	–	• ° 15⁰² 20⁴⁰, = 5³⁰–9²⁰ ∞–12⁰⁰, ⩔ 10¹⁰–14⁴⁵
8	7	.	.	–	• ° 0⁵⁰ 1²⁰ 2⁰³
9	7	0.1	.	–	• ° 7⁵⁰ 11⁴⁰, = 5³⁰ 11⁴⁰ 17³⁰ 23⁵⁰ = ° –24, ⌒ 0-2 18³⁰–24
10	6	.	.	–	= 0-1 0⁰⁰–8¹⁵ = –24, ⌒ 2-0 0⁰⁰ 11³⁰ ⌒ ° 23⁰⁰–24
11	7	.	.	–	= 0⁰⁰ 3⁵⁵ = ° –5³⁰ = ° –6³² = 1-0 7³⁵ = –9⁴⁰, p, np, ⌒ ° na
12	6	.	.	–	= 0⁰⁰–24, ⌒ ° 1⁰⁰–12³⁰ ⌒ 0-1 19⁰⁰–24
13	7	.	.	–	= 0⁰⁰–9¹⁵, 21⁴⁵–24, ⌒ ° 0⁰⁰–2⁰⁰ ⌒ 0-2 19⁴⁵–24, = 0⁰⁰–9¹⁵, 21⁴⁵–24
14	7	0.4	.	–	• ° 1¹¹⁵ 12²⁵ 14⁵⁰ 16¹⁰ 19⁵⁰ 23⁰⁵, = 0⁰⁰–45 = 0-1 5³⁰ = 2-0 8²⁰ = –11¹⁵, ⌒ ° na – a
15	7	.	.	–	• ° 0²⁰–2¹⁰, = 2³⁰ 11³⁰
16	7	.	.	–	= 6³⁰–12³⁰, 16⁴⁰–24, ⌒ 0-1 18⁰⁰–24
17	6	1.7	.	–	• ° 10⁰⁵–16 = 0⁰⁰–24, ⌒ 0-2 0⁰⁰–9⁰⁰
18	7	3.4	.	–	• ° 4²⁰ 6²⁵ • 0-1 8³⁵ 17²⁰, = 0⁰⁰–11²⁰, ⩔ 13⁴⁰–15⁰⁵
19	7	0.2	.	–	• ° 9⁰⁵ 11¹⁰
20	6	.	.	–	▽ ° 0¹⁵–25 = 2³⁰–13⁴⁰ 14³⁰–18²⁰
21	8	.	.	–	= 1⁴⁰ 9³⁰ 13⁴⁰–24, ⩔ 9⁴⁵–11³⁰, ⌒ 0-1 2⁰⁰ 9³⁰ ⌒ ° 20⁰⁰–24
22	6	0.0	.	–	• ° 20⁵⁰ 22¹⁵, = 0⁰⁰–8¹⁵ = ° –9¹⁰ = –24, ⌒ ° 0⁰⁰–11⁰⁰
23	6	0.1	.	–	• ° 12⁵⁰–14⁴⁰, = 0⁰⁰–24, ⊕ ° 7³⁰–12²⁰, ⌒ ° 22⁰⁰–24
24	7	0.0	.	–	• ° 9²⁰ 10⁴⁵, = 0⁰⁰–11³⁰ 16³⁰ 23³⁰, ⌒ ° 0⁰⁰–9²⁰
25	7	.	.	–	= 2³⁰–10³⁰ 17⁴⁵–22⁵⁰, ⌒ 0-1 2⁰⁰–10³⁰ ∞–12²⁰
26	7	.	.	–	⩔ 20³⁰–22¹⁵
27	7	.	.	–	= 6¹⁵–10²⁰ 16⁴⁰–24, ⌒ ° 3⁰⁰–8⁰⁰
28	6	.	.	–	= 0⁰⁰–21⁴⁵ = 0-1 –24, ⌒ ° 2⁰⁰–9⁰⁰ 20⁰⁰–24
29	5	3.7	.	–	• 0-1 12²⁰ 13¹⁰–19³⁰ 20²⁰, = 0⁰⁰–1⁵⁰ = ° –15³⁵ = ° –16²⁰ = –24, ⌒ ° 0⁰⁰–11⁰⁰
30	5	.	.	–	= 0⁰⁰–24, ⌒ 0-2 16³⁰–24
31	6	.	.	–	= 0⁰⁰–1⁴⁵ = 0-1 –4⁴⁵ = 2-0 –10²⁵ = –19²⁰, ⌒ 2-0 0⁰⁰–11⁰⁰, ⊕ p
Σ	–	10.2	–	–	UWAGI.

Łódź – Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$

Listopad – Novembre 1961

DNI	CIŚNIENIE P.m 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dśr	I	II	III	Dśr	Max	Min	I	II	III	Dśr	I	II	III	Dśr	I	II	III	I	II	III
1	97.0	97.0	98.6	97.5	7.4	9.6	8.9	8.7	10.8	7.0	85	75	89	82	1.8	3.3	1.2	2.1	9	10 •	10	SW 8	WSW 8	W 8
2	101.5	99.2	95.7	98.1	5.3	10.6	6.5	7.2	13.2	5.2	98	70	90	86	0.1	3.8	1.0	1.6	6	7 ⊙	0	WSW 5	WSW 4	S 4
3	86.9	85.5	85.6	86.0	6.2	11.4	8.2	8.5	12.8	6.0	86	66	75	76	1.3	4.1	2.7	2.9	6	9	4	SSW 7	SW 12	SSW 6
4	86.1	88.2	90.1	88.1	6.0	5.0	3.4	4.4	9.3	3.2	89	79	83	84	1.1	1.8	1.3	1.4	10	10	10	SW 3	W 5	NW 1
5	88.7	88.6	92.1	89.8	0.2	0.3	1.9	1.1	4.6	0.0	98	100	98	99	0.1	0.0	0.1	0.1	10 *	10 *	10 9	N 5	N 7	N 3
6	95.1	90.9	89.3	91.1	3.3	7.3	8.8	7.0	10.0	1.4	100	100	99	100	0.0	0.0	0.1	0.0	10 ≡	10 ≡	10	C 0	NE 7	E 8
7	85.3	84.1	85.7	85.1	9.2	12.2	9.2	10.0	13.7	8.6	97	81	92	90	0.3	2.6	0.9	1.3	10	9	10	E 8	E 9	E 5
8	84.8	86.3	86.7	85.9	8.2	6.1	3.3	6.3	10.1	5.4	100	94	89	94	0.0	0.6	1.0	0.5	10 •	10 •	10	E 1	SW 4	SSW 4
9	85.4	84.7	85.9	84.7	4.2	8.5	6.1	6.2	9.7	3.2	84	72	86	81	1.3	3.2	1.3	1.9	10	9	8	S 4	SSE 6	SE 2
10	81.8	81.3	83.6	82.3	4.3	10.4	7.2	7.3	12.2	3.4	92	82	100	91	0.7	2.2	0.0	1.0	10	9	10 •	ESE 5	SSE 3	C 0
11	82.9	84.3	86.1	84.4	7.4	9.2	8.4	8.4	10.2	7.1	100	92	92	95	0.0	0.9	0.9	0.6	10 •	10	10	C 0	E 2	E 3
12	87.2	87.9	89.6	88.2	6.8	6.4	5.3	6.0	9.3	5.3	94	94	98	95	0.6	0.6	0.1	0.4	10 •	10	10	E 7	E 5	E 5
13	89.4	88.0	86.1	87.8	3.2	2.7	1.9	2.4	6.5	1.6	98	98	94	97	0.2	0.1	0.4	0.2	10	10 9	10 •	E 8	E 9	E 8
14	84.3	89.4	94.6	89.4	0.4	-0.1	-0.6	-0.2	2.6	-1.0	98	96	95	96	0.1	0.3	0.3	0.2	10 •	10 9	10	NE 6	N 7	N 4
15	95.6	96.3	96.6	96.2	-0.6	-0.3	0.3	-0.1	0.6	-1.0	97	88	93	93	0.2	0.8	0.4	0.5	10	10	10	N 3	NW 2	WSW 2
16	96.0	94.7	92.3	94.3	0.4	0.8	0.3	0.4	1.6	0.2	94	88	92	91	0.4	0.8	0.3	0.6	10	10	10	WSW 3	WSW 3	WSW 3
17	88.2	87.3	88.3	88.0	1.2	3.8	5.0	3.8	5.9	0.0	100	98	92	97	0.0	0.1	0.7	0.3	10 •	10 9	9	W 6	W 7	WNW 4
18	86.5	85.3	88.1	86.6	2.7	3.4	1.2	2.1	3.7	1.0	88	93	87	89	0.9	0.3	0.9	0.8	10	10	4	W 7	W 6	W 4
19	90.9	94.3	101.0	95.4	-0.3	2.4	-0.1	0.3	3.7	-1.0	92	87	90	90	0.3	1.0	0.7	0.7	4	10 •	4	W 3	NW 8	NNW 7
20	107.0	110.6	113.2	110.3	-0.8	1.0	-3.1	-1.3	2.7	-3.3	89	73	93	85	0.6	1.8	0.4	0.9	1	9	10	NNE 4	N 3	C 0
21	111.3	109.3	105.8	108.9	-3.9	1.8	-2.2	-1.6	2.8	-4.7	92	73	89	85	0.4	2.0	0.6	1.0	2	6	9	WSW 1	W 2	C 0
22	102.3	100.8	98.3	100.5	-4.9	3.2	-2.6	-1.7	4.7	-6.1	95	63	93	84	0.2	2.9	0.3	1.1	9	6	0	C 0	WSW 1	C 0
23	94.6	92.7	91.9	93.1	-3.9	3.3	-1.3	-0.8	6.8	-6.8	92	49	84	75	0.3	4.6	0.9	1.9	0	0 ⊙	0	ESE 3	S 2	C 0
24	93.1	94.0	95.2	94.1	-3.3	3.2	0.9	0.4	3.2	-4.3	90	76	92	86	0.3	1.9	0.3	1.0	0	7	10 •	SSW 1	SW 1	S 1
25	94.2	92.7	92.6	93.2	1.3	3.8	2.0	2.3	4.4	0.7	96	87	98	94	0.3	1.1	0.2	0.3	10 •	6	10 ≡	C 0	SSW 2	SW 1
26	89.3	87.7	85.3	87.6	1.0	3.6	1.0	2.2	6.8	0.0	98	86	98	94	0.2	1.3	0.2	0.6	9	8	4	SE 2	SE 2	E 2
27	81.0	79.3	80.2	80.2	2.4	5.2	3.7	3.8	6.1	-0.3	98	90	98	95	0.2	0.8	0.2	0.4	10	10	10	E 4	ESE 4	WNW 4
28	85.1	88.0	90.7	87.9	2.6	3.0	3.2	3.0	4.6	2.4	98	98	98	98	0.2	0.2	0.2	0.2	10 ≡	10	10	WNW 3	C 0	E 1
29	92.0	92.2	92.7	92.3	3.8	4.6	4.4	4.3	5.3	3.0	98	97	93	96	0.1	0.3	0.6	0.3	10 •	10 •	10	SE 1	S 2	SW 4
30	86.5	86.4	81.2	84.7	2.2	4.9	4.4	4.0	6.0	1.1	87	81	90	86	1.0	1.7	0.9	1.2	9	9	10 •	SW 7	SW 8	SW 9
31																								
M	91.0	90.9	91.3	91.1	2.3	5.0	3.3	3.5	6.9	1.2	94	84	92	90	0.5	1.5	0.6	0.9	8.2	8.8	8.1	3.8	4.8	3.5

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1	73.7	74.2	77.9	75.3	6.4	9.6	5.6	6.8	10.4	4.0	91	79	95	88	0.9	2.6	0.4	1.3	10 •	10	10 •	SW 14	SW 12	WSW 5
2	73.5	71.3	76.8	73.8	8.8	12.0	6.6	8.5	13.5	4.4	81	75	64	73	2.1	3.5	3.5	3.0	6	7	4	SSW 8	SSW12	WSW12
3	86.8	87.2	86.4	86.8	1.9	3.4	0.2	1.4	7.6	0.0	85	75	90	83	1.0	2.0	0.6	1.2	0	8	0	SW 7	SSW 5	S 2
4	81.0	85.7	89.4	85.4	3.2	6.1	4.1	4.4	6.8	-0.7	97	91	97	95	0.3	0.8	0.3	0.5	10	10	10	S 2	WNW 6	SE 2
5	85.3	85.4	85.6	84.8	12.8	14.6	10.6	12.2	14.9	4.0	79	71	80	77	3.1	4.8	2.6	3.5	10 •	8	0	SW 12	SW 9	SW 7
6	86.8	89.6	91.0	89.1	6.4	3.4	1.2	3.0	12.1	1.2	81	58	79	73	1.9	3.3	1.4	2.2	10	10	10	W 4	W 5	W 2
7	90.9	91.3	94.2	92.1	-0.3	0.2	-1.0	-0.5	2.0	-1.0	94	94	94	94	0.4	0.4	0.4	0.4	10	10	10	W 2	NW 2	NW 6
8	95.1	94.8	96.6	95.5	-1.3	0.6	-0.9	-0.6	1.8	-2.0	89	80	91	87	0.6	1.3	0.5	0.8	10	8	4	W 3	WSW 4	W 2
9	97.0	96.8	94.3	96.0	-2.1	-0.1	-2.9	-2.0	1.3	-2.9	89	75	82	82	0.5	1.6	0.9	1.0	8	9	6	SW 3	S 1	SE 4
10	90.9	90.0	89.2	90.0	-0.5	0.8	0.6	0.4	2.0	-3.3	64	69	80	73	2.1	2.0	1.3	1.8	9	9	10	SSE 6	S 5	S 3
11	84.3	77.2	71.9	77.8	0.0	1.1	4.1	2.3	5.1	-0.3	79	94	98	90	1.3	0.4	0.2	0.6	8	10 9	10 9	S 4	S 7	WNW 2
12	80.4	84.4	88.5	84.4	1.3	1.3	-0.3	0.3	3.0	-0.4	98	94	100	97	0.1	0.4	0.0	0.2	10	10	10 *	N 3	N 2	NE 7
13	98.1	102.2	105.6	102.0	-4.6	-5.9	-5.8	-5.0	0.3	-5.8	86	75	74	78	0.6	1.1	1.0	0.9	10	2 ⊙	4	NE 7	NW 6	NNE 4
14	105.6	105.0	104.9	105.2	-9.3	-7.0	-8.3	-8.2	-4.3	-10.4	88	53	85	75	0.4	1.7	0.3	0.9	0	0 ⊙	2	NE 2	N 9	NW 5
15	100.2	96.3	103.3	100.0	-5.6	-6.3	-14.8	-10.4	-3.3	-15.0	82	89	82	84	0.7	0.4	0.3	0.3	10	10 *	0	NNW 9	NNW10	NE 7
16	110.2	114.1	119.6	114.6	-16.0	-14.1	-15.6	-15.3	-13.3	-16.3	81	79	86	82	0.3	0.4	0.3	0.3	0	0	0	NE 7	NE 5	E 4
17	121.1	120.0	118.1	119.7	-20.4	-13.4	-8.9	-12.9	-8.3	-22.2	89	92	85	88	0.1	0.2	0.3	0.3	0	8	10	C 0	NW 2	N 3
18	116.3	115.3	113.4	115.1	-6.9	-6.3	-7.6	-7.1	-3.3	-9.4	91	86	84	87	0.3	0.3	0.3	0.4	10	10 *	10	N 3	W 6	W 3
19	109.3	107.8	106.4	107.9	-7.0	-4.7	-2.3	-4.1	-1.3	-8.3	96	98	98	97	0.1	0.1	0.1	0.1	10 9	10 9	10 ≡	W 3	W 6	WNW 3
20	102.0	95.3	89.3	95.0	-2.3	-2.7	0.3	-1.0	1.3	-3.3	98	97	98	98	0.1	0.1	0.1	0.1	10	10	10 9	W 6	WSW 8	WNW 7
21	87.9	90.0	92.8	90.2	-0.3	-3.2	-7.9	-4.9	1.3	-8.3	88	90	90	89	0.7	0.3	0.3	0.3	10 •	6	0	WNW 8	N 7	NW 3
22	87.2	85.4	85.3	85.4	-6.3	-4.9	-12.4	-9.0	-4.0	-13.3	94	88	89	90	0.2	0.3	0.3	0.3	10 *	8	2	W 2	NNW 3	NW 2
23	90.4	92.8	93.9	92.4	-11.0	-10.2	-8.7	-9.6	-6.3	-15.7	83	91	92	89	0.4	0.3	0.3	0.3	10	10	10	NNW 2	W 4	W 2
24	95.1	95.0	93.8	94.6	-7.9	-7.7	-10.3	-9.2	-6.1	-11.1	93	96	94	94	0.2	0.1	0.2	0.2	10 *	9 *	10 *	WSW 1	WSW 1	S 1
25	91.7	89.9	88.6	90.1	-15.1	-13.3	-18.7	-16.4	-10.2	-19.0	91	84	89	88	0.2	0.4	0.1	0.2	8 *	0	0	S 1	E 2	C 0
26	86.6	84.8	84.2	85.2	-22.0	-11.0	-13.8	-15.2	-10.1	-25.2	81	85	88	84	0.2	0.4	0.3	0.3	0	3	0	E 1	SE 2	SE 1
27	87.5	90.3	91.4	89.7	-16.6	-15.6	-11.4	-13.8	-10.9	-18.2	95	91	90	92	0.1	0.2	0.3	0.2	10 ≡	0	10 *	C 0	E 2	E 5
28	89.2	87.7	86.4	87.8	-14.2	-11.8	-6.7	-9.8	-6.2	-14.7	87	89	94	90	0.3	0.3	0.2	0.3	10 *	10	10	E 6	E 6	SE 2
29	86.9	87.0	87.1	87.0	-6.1	-1.3	-2.9	-3.3	0.0	-7.0	97	88	93	93	0.1	0.6	0.3	0.3	9	10	10	SE 1	SW 1	SE 2
30	85.1	84.8	85.6	85.2	0.0	1.6	-1.3	-0.4	3.0	-3.1	94	96	99	96	0.4	0.3	0.1	0.3	9	8	10 ≡	ESE 3	S 3	E 3
31	85.3	85.4	82.3	84.4	1.3	1.8	-0.3	0.6	3.7	-1.8	94	85	92	90	0.4	1.1	0.3	0.7	9	8 ⊙	0	SSW 4	S 1	S 4
M	92.3	92.0	92.7	92.3	-4.3	-2.6	-4.2	-3.8	0.1	-7.3	88	84	89	87	0.6	1.0	0.6	0.7	7.9	7.3	6.2	4.4	5.0	3.7

Łódź-Lublinek

$H_s = 187\,m$ $H_b = 187{,}7\,m$ $h_w = 11\,m$

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DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.8	•	–	• 9³⁷ 14¹⁰ – 19⁰⁵ = 6²⁰ 24
2	7	•	•	–	= 0⁰⁰ – 12¹⁵, 19³⁰ 24, ⌒ ° 2⁰⁰ – 9⁰⁰ ⌒ 0-1 19³⁰ – 24
3	7	0.0	•	–	▽ ° 14²¹⁻²⁷, = na a, ≫ a ⌒ 1-0 0⁰⁰ – 8⁰⁰
4	6	9.7	•	–	• ° 7⁴² – 8⁴⁵ 21⁴⁵ – 24, = 8⁴⁵ – 24
5	5	7.4	3	–	• ° 0⁰⁰ – 1⁴⁰ * 0-1 – 13¹⁰ • ° – 19⁰¹ • ° – 21³⁵ = ° 21³⁵ 24
6	1	0.1	•	–	• ° 13³⁰ 17⁴⁵, ≡ 0-1 0⁰⁰ – 8⁰⁰ ≡ 2-0 – 15²⁰ = – 24
7	7	5.2	•	–	= 0⁰⁰ – 12³⁰, 20³⁰ – 24, ≫ 2¹⁰ – 4⁴⁰ ⌒ ° 22⁰⁰ – 24
8	6	2.5	•	–	• ° 0⁵⁰ – 1⁵⁰ • ° – 12⁴⁰ 13⁴³, = 0⁰⁰ – 24, ⌒ ° 0⁰⁰ – 50
9	6	•	•	–	
10	6	3.5	•	–	• ° 7⁵⁰ 8¹⁵ – 9⁴⁵ ; • 0-1 16⁵² 21⁴⁰ = 0⁰⁰ – 24
11	6	14.6	•	–	• ° 0⁴⁰ 1⁰⁰ – 1³⁰ • ° – 4³⁵ • 0-1 5⁵⁰ – 10¹⁵ 11¹⁶ 12¹⁰, = 0⁰⁰ – 24
12	7	0.5	•	–	• 0-1 2⁵⁰ – 10⁴⁵, = 0⁰⁰ – 10³⁰ 20³⁰ – 24
13	5	22.2	•	–	• ° 9⁴⁵ 15⁵⁰ • ° 16²⁵ 17¹⁵ – 19⁵⁰ 24, = 0⁰⁰ – 24, ≫ 13¹⁵ – 14³⁰
14	6	6.1	•	–	• 0-1 0⁰⁰ 1⁴⁰ – 9⁰⁸ △ ° – 9⁵⁰ • ° – 10¹⁷ △ – 12¹⁵ ° – 12²⁵ • ° 13⁴⁵, = 0⁰⁰ – 24
15	6	0.0	•	–	* 8⁵⁰ 9⁴⁵, = 0⁰⁰ – 24, ⌒ ° 0⁰⁰ – 11⁰⁰
16	6	0.0	•	–	= 0⁰⁰ 24
17	4	1.0	•	–	* ° 1⁴⁵ 2⁰⁰ – 3⁵⁰ • • • ° • ° 6³⁰ 15⁴⁵ ▽ ° 23⁵⁰ – 24, = 0⁰⁰ – 22²⁰
18	7	0.5	•	–	▽ ° 0⁰⁰⁻⁰⁷ • ° 0⁵⁰ 2²⁰ ▽ 11⁴⁰ – 12¹⁵
19	7	0.1	•	–	* ▽ ° 10⁵⁰ – 11⁰² 11⁴⁷ – 12²⁰ 12³⁵ – 13²⁵ ⌒ ° 5⁰⁰ – 9³⁰
20	8	•	1	–	* ° 0⁴⁵ – 5⁴⁰, ⌒ ° 18⁰⁰ – 24⁰⁰, ⌓ ° 20³⁰ – 24
21	6	•	•	–	= 6³⁰ – 24, ⌒ ° 0⁰⁰ – 10⁵⁰ ⌒ ° 19⁰¹ – 24, ⌓ 0⁰⁰ – 3³⁰ ⌣ 18³⁰ – 24
22	6	•	•	–	= 0⁰⁰ – 24, ⌒ ° 0⁰⁰ – 11²⁰ 17³⁰ – 24, ⌣ 0⁰⁰ – 6²⁰
23	6	•	•	–	= 0⁰⁰ – 12¹⁵ ∞ – 14³⁰ = – 24 ⌒ 1-2 0⁰⁰ – 12³⁰ ⌒ ° 21⁴⁰ – 24
24	6	1.0	•	–	• 20⁴⁵ – 24, = 0⁰⁰ – 24, ⌒ ° 0⁰⁰ – 12³⁰
25	5	0.0	•	–	• ° 0⁰⁰ – 2⁵⁰ 5⁴⁰ 16³⁵, = 0⁰⁰ 8¹⁵ ≡ ° – 10³⁵ = – 17⁵⁰ ≡ ° – 18³⁰ ≡ 1-2 23⁵⁰ ≡ 1 – 24
26	4	•	•	–	= 1-0 0⁰⁰ – 4³⁵ = – 21⁰⁵ ≡ 0-1 24
27	6	0.2	•	–	• ° 21⁴⁵ – 22⁴⁰, ≡ 0-1 0⁰⁰ – 2²⁰ = – 24
28	4	0.9	•	–	• ° 4³⁵ – 5²⁰ • ° – 6¹⁵ • • • ° 7⁴⁰ – 9⁴⁵ • ° 13³⁵ – 15³⁵, = 0⁰⁰ – 3⁴⁰ ≡ 1-0 – 9⁴⁵ = – 24
29	5	2.4	•	–	• ° 4⁵⁵ – 7⁴⁰ 8⁰² – 9²⁵ 16⁴⁰ = 0⁰⁰ – 24
30	6	5.8	•	–	• ° 18³⁵ – 24, = 0⁰⁰ – 24, ≫ 21²⁰ – 24
31					
Σ	–	84.5	–	–	UWAGI.

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1	8	4.5	•	–	• 0-1 0⁰⁰ – 6⁵⁸ • ° 8⁴⁰ 24, = 0⁰⁰ – 1⁰⁰, ≫ 0⁰⁰ – 15¹⁰
2	7	3.6	•	–	• 0⁰⁰ 1⁵⁰ 11⁴² 12⁴⁰ • 1-0 ▽ 17⁴⁰ – 18²⁵, = 1⁰⁰ – 3²⁰, ≫ 9³⁰ – 23⁴⁰
3	7	4.5	•	–	• ° 1⁵ 56, ⌓ ° 23³⁰ – 24
4	6	0.2	•	–	• 0-1 3⁴⁵ – 6⁴⁰ • ° 17⁵⁰ 18²⁰ 23⁴⁰ – 24, = 7³⁰ – 24, ⌓ ° 0⁰⁰ – 3³⁰
5	7	0.0	•	–	• ° 0⁰⁰ – 1⁴⁶ ▽ ° 6³⁵ – 7⁰⁰, = 0⁰⁰ – 3³⁰, ≫ 6¹⁰ – 12³⁰
6	7	0.0	•	–	• ° 7⁴⁰ 9⁵⁰
7	6	0.0	•	–	* ° 6⁵⁰ – 7⁴⁵ = 2³⁰ – 21⁴⁰
8	6	•	•	–	= 6³⁰ – 24, ⌓ ° 23⁰⁰ – 24
9	6	•	•	–	= 0⁰⁰ – 24, ⌓ ° 0⁰⁰ – 10⁰⁰
10	7	0.0	•	–	△ * ° 14¹⁰⁻²⁵ * ° – 14³⁰, = 0⁰⁰ – 7³⁰, 14³⁰ – 24
11	6	10.4	•	–	• ° 8⁵⁰ 12³⁰ – 17²⁰ • • • ° – 21¹⁰ • ° 22²⁵ – 24, = 0⁰⁰ – 1³⁰, 8³⁰ – 21²⁰ ≡ 1 – 24
12	5	0.8	•	–	• ° 0⁰⁰ – 3⁴⁵ • ° 17⁵⁰ 18⁴⁰ * 0-1 – 24, = 3⁴⁵ – 24
13	7	•	2	–	* ° 0⁰⁰ – 2¹⁰ 4⁴⁰ – 5¹⁵, = 0⁰⁰ – 7⁰⁰
14	7	•	2	–	= 8²⁰ – 10³⁰
15	4	0.3	1	–	* 0-2 7¹⁰ 8³⁰ – 15³⁵ = p, ≫ 4²⁰ – 5³⁰, 9³⁰ – 10¹⁵, ∴ 14¹⁰⁻⁴⁰ ∴ – 17²⁰
16	6	0.0	5	–	= 7³⁰ – 24
17	6	0.0	4	–	↔ 4¹⁵ – 6²⁰ * ° 16⁴⁰ 20³⁵, 23⁵⁰ 24, = 0⁰⁰ – 24
18	6	0.0	4	–	* ° 0⁰⁰ – 2⁴⁵, 12²⁵ 13⁴⁰, = 0⁰⁰ – 24
19	4	0.5	5	–	* ° 2⁴⁰ – 5⁵⁵ ∾ ° – 16⁴⁰, = 0⁰⁰ – 17⁵⁰ ≡ 0-1 – 24, ∾ ° 5⁵⁵ – 16⁴⁰
20	4	0.7	5	–	∾ ° 14²⁰ – 15⁴⁰ △ – 19²⁰ ∾ ° – 21⁴⁰ ≡ ° = 0⁰⁰ – 24, ∾ ° 14²⁰ – 15⁴⁰, 19²⁰ – 21⁴⁰
21	7	0.4	4	–	* ° 6⁴⁰ – 8⁴⁰ ▽ * 0-1 10¹⁵ 13⁴⁵, = 0⁰⁰ – 3³⁰, ≫ 9²⁸ – 12³⁵
22	7	1.8	4	–	* ° 5⁴⁵ 6¹⁰ – 11⁴⁰, = 14¹⁰ – 15¹⁵ ≡ 0-2 – 17⁴⁰ = – 21⁴⁵ ≡ ° – 24, ∨ ° 16⁴⁵ – 17⁴⁰
23	6	0.0	5	–	* ° 18⁴⁸ 19²⁵, ≡ ° 0⁰⁰ – 1⁴⁵ = – 24
24	6	0.1	5	–	* ° 6⁴⁰ 24, = 0⁰⁰ – 24
25	6	0.0	5	–	* ° 0⁰⁰ – 2⁴⁸, 3⁴⁰ – 9¹⁵, = 0⁰⁰ – 24
26	5	•	5	–	= 0⁰⁰ – 24
27	4	0.3	5	–	* ° 14⁵⁰ 16¹⁰⁵ 16⁴⁸ 23³⁵, = 0⁰⁰ – 2⁵⁰ ≡ 0-2 – 10¹⁵ ≡ 2-0 – 11²⁵ = – 24, ∨ ° 3¹⁵ – 11²⁵
28	5	0.0	6	–	* ° 2⁵⁰ – 4²⁵, 5⁵⁸ 6⁴⁵ – 7¹⁵, = 0⁰⁰ – 24
29	4	•	6	–	= 0⁰⁰ – 24
30	5	•	6	–	= 0⁰⁰ – 19⁴⁵ ≡ ° – 21⁴⁰ = – 24
31	5	•	5	–	= 0⁰⁰ – 24
Σ	–	28.1	–	–	UWAGI.

Wrocław - Gądów Mały — φ = 51°08' — λ = 16°59' — Styczeń - Janvier 1961

Dzień	CIŚNIENIE P mm 900 + I	II	III	Dek.	TEMPERATURA T I	II	III	Dek.	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dek.	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dek.	ZACHMURZENIE I POGODA N,w I	II	III	KIERUNEK I PRĘDKOŚĆ WIATRU D,v I	II	III
1	100.9	101.5	101.6	101.3	0.6	2.9	-0.4	0.7	4.3	-0.6	81	74	92	82	1.3	1.9	0.5	1.2	10	9	●9	SW 4	S 3	SE 2
2	100.0	97.7	95.5	97.1	-0.4	2.1	-0.3	0.5	3.1	-1.0	88	87	88	88	0.7	0.9	0.8	0.8	10	7	9	SSE 3	SE 4	SSE 5
3	94.4	82.4	85.0	85.9	0.4	2.4	3.0	2.2	4.5	-2.0	88	80	86	85	0.8	1.5	1.1	1.1	10	10	10 ●	SE 9	SE 4	SSW 5
4	81.7	81.7	87.8	83.7	1.1	8.8	2.0	3.5	9.7	0.7	98	65	84	82	0.1	4.2	1.2	1.8	10	9	9	C 0	S 9	SSW 3
5	89.3	91.6	97.0	92.6	-2.3	4.4	3.2	2.1	5.7	-2.4	95	74	76	82	0.3	2.2	1.9	1.5	10	8	10	SE 3	SW 3	W 6
6	100.8	99.4	95.4	98.5	-0.3	5.0	2.8	2.6	5.4	-2.3	82	57	64	68	1.1	3.8	2.7	2.5	0	8 ⊙	10	S 3	SSE 9	SSW 8
7	94.9	95.5	96.6	95.7	1.2	3.3	2.0	2.1	5.4	-0.1	79	68	89	79	1.4	2.5	0.8	1.6	10	7	8	S 4	SSE 5	SSW 3
8	99.4	97.0	94.5	97.0	1.8	4.0	3.4	3.2	4.5	0.4	87	74	73	78	0.9	2.1	2.1	1.7	10	10	10	WSW 3	S 5	SSW 6
9	96.2	96.4	95.6	96.1	3.6	6.7	3.4	4.3	7.0	0.4	76	64	75	72	1.9	3.5	2.0	2.5	10 ●	9	9	SW 5	SSW 6	SSE 5
10	98.9	97.9	96.2	97.7	0.8	5.3	0.8	1.9	5.7	0.2	94	65	88	82	0.4	3.2	0.8	1.5	10	1 ⊙	0	SSW 2	S 5	SE 4
11	96.7	100.3	105.6	100.9	0.4	3.4	1.4	1.6	4.2	-0.6	84	80	92	85	1.0	1.6	0.6	1.1	3	10	10 ●	S 4	WNW 3	WNW 6
12	111.8	115.0	118.5	115.1	-1.1	-0.9	-1.3	-1.2	1.7	-2.3	81	87	84	84	1.1	0.7	0.9	0.9	8	9 *	9	W 6	NW 7	WNW 5
13	119.2	117.2	114.6	117.0	-5.7	-0.1	1.2	-0.8	2.2	-6.0	92	67	72	77	0.3	2.0	1.9	1.4	0	9	10	SW 3	S 4	SW 3
14	113.4	114.3	118.1	115.3	0.9	0.6	0.2	0.5	2.2	0.2	88	94	98	93	0.7	0.4	0.1	0.4	10 ●	10 *	10 *	SW 2	WNW 4	C 0
15	120.5	120.2	117.6	119.4	0.4	0.2	-2.5	-1.1	1.3	-2.5	96	86	93	92	0.3	0.9	0.4	0.5	10	10	10	C 0	SW 2	WSW 2
16	113.9	113.3	113.8	113.7	-4.5	-5.9	-2.7	-3.4	-1.4	-5.1	96	96	95	96	0.2	0.2	0.2	0.2	10	10	10	N 2	W 3	W 2
17	116.3	119.8	123.3	119.8	-4.5	-4.9	-14.3	-9.5	-0.5	-14.7	93	85	91	89	0.3	0.7	0.2	0.4	8	4 ⊙	0	NE 2	NNE 3	WNW 2
18	127.2	128.0	126.4	127.2	-15.1	-8.5	-11.9	-11.8	-7.7	-15.9	91	65	82	79	0.2	1.1	0.4	0.6	0	1	0	E 3	SSE 4	ESE 4
19	122.6	119.9	118.6	120.4	-12.9	-4.8	-8.0	-8.4	-3.9	-14.0	81	57	75	71	0.4	1.8	0.8	1.0	0 ⊙	0 ⊙	0	E 5	SE 6	SE 4
20	115.4	112.9	110.4	112.9	-8.8	-1.7	-5.5	-5.4	-0.6	-8.9	80	75	90	82	0.6	1.3	0.4	0.8	0	0	0	ESE 5	E 6	E 3
21	108.1	107.0	106.1	107.1	-10.0	-4.5	-8.7	-8.0	-3.5	-10.4	91	74	89	85	0.3	1.1	0.4	0.6	0	3 ⊙	1	E 2	ESE 4	E 2
22	103.0	100.9	99.4	101.1	-13.4	-3.7	-1.9	-5.2	-0.7	-15.1	92	80	92	88	0.2	0.9	0.4	0.5	1	6 =	10 *	ENE 2	ENE 2	ESE 1
23	96.9	97.6	101.1	98.5	-1.9	-2.2	-7.7	-4.9	-1.1	-7.7	96	89	90	92	0.2	0.6	0.3	0.4	10 *	10 *	10	ENE 2	E 5	E 4
24	101.8	100.9	99.0	100.6	-11.3	-9.7	-10.1	-10.3	-6.4	-14.7	90	88	87	88	0.3	0.4	0.4	0.4	10	1 ⊙	9	NE 1	NE 1	ENE 3
25	97.0	97.7	102.3	99.0	-7.7	-6.8	-13.2	-10.2	-5.6	-13.2	90	83	80	84	0.3	0.6	0.4	0.4	10	10	0	NE 2	NE 5	E 3
26	108.3	111.5	114.4	111.4	-17.9	-11.9	-14.3	-14.6	-10.8	-18.2	84	71	85	79	0.2	0.7	0.3	0.4	0	0 ⊙	0	ENE 3	ENE 3	E 2
27	117.9	117.6	115.5	117.0	-18.5	-8.7	-13.0	-13.3	-5.9	-19.7	78	65	84	76	0.3	1.1	0.4	0.6	0	0 ⊙	0	E 2	ESE 3	E 2
28	111.5	108.7	105.4	107.8	-15.1	-0.2	-2.3	-5.0	0.4	-16.7	77	69	74	73	0.4	1.9	1.4	1.2	0	10	8	ESE 3	S 6	S 13
29	103.5	105.5	109.4	104.1	-1.1	3.0	2.9	1.9	4.5	-5.5	85	83	84	84	0.9	1.3	1.2	1.1	7	0 ⊙	10	SSW 8	SW 7	S 6
30	95.2	92.5	92.1	93.3	2.2	3.7	5.2	4.1	5.7	0.7	68	59	78	68	2.3	3.3	1.9	2.5	6	9 ●	10	C 0	SSW 8	SSW 5
31	89.1	83.7	91.0	87.9	4.9	5.8	1.6	3.5	6.6	1.3	89	91	96	92	1.0	0.8	0.3	0.7	10 ●	10 ●	9	S 3	S 4	SW 4
M	104.4	104.1	104.4	104.3	-4.3	-0.4	-2.7	-2.5	1.2	-6.3	87	76	85	83	0.7	1.6	0.9	1.1	6.2	6.5	6.8	3.1	4.6	4.0

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1	86.0	81.7	84.4	84.0	2.0	3.0	2.7	2.6	5.5	0.4	89	93	84	89	0.8	0.6	1.2	0.9	10	10	9	SE 4	SE 3	W 7
2	83.3	81.0	76.9	80.4	0.2	5.2	-0.1	1.3	5.7	-1.0	84	69	86	80	1.0	2.7	0.9	1.5	1	6 ⊙	6	SSW 6	S 6	SE 4
3	79.7	82.5	87.8	83.3	0.1	1.6	0.5	0.7	2.0	-0.9	94	83	90	89	0.4	1.2	0.6	0.7	10 *	7	9 *	WNW 5	W 7	W 7
4	93.7	92.6	86.2	90.8	-0.5	2.8	-0.4	0.4	4.2	-2.3	82	65	78	75	1.1	2.6	1.3	1.7	9	7 ⊙	6	WSW 7	SW 4	SE 5
5	93.8	101.3	106.5	100.5	-0.1	1.0	-1.3	-0.4	2.1	-2.1	94	75	84	84	0.4	1.7	0.9	1.0	10 *	7	4	N 3	NNW 4	WNW 5
6	104.7	101.9	96.2	100.9	-2.8	2.2	1.2	0.4	2.6	-6.9	75	80	77	77	1.2	1.5	1.5	1.4	4	10	9	SSE 3	S 7	SSE 6
7	94.2	94.4	94.3	94.3	1.8	4.8	3.2	3.2	6.0	-0.2	87	78	79	81	0.9	1.9	1.6	1.5	9	9	2	SSW 2	SSW 5	SW 6
8	98.9	101.4	103.6	102.0	3.1	5.4	0.8	2.5	5.9	0.5	88	77	96	87	0.9	2.1	0.3	1.1	10	8	9	W 7	W 8	W 3
9	101.6	96.0	95.2	97.6	1.7	2.8	7.2	4.7	7.9	-1.6	90	93	86	90	0.6	0.6	1.5	0.9	10 ●	10 ●9	10	SSE 6	SSE 5	W 7
10	103.3	108.9	113.2	108.5	3.6	2.8	1.8	2.5	7.8	1.8	91	89	93	91	0.7	0.8	0.6	0.7	10 ●9	10	10	NW 10	NNW 5	W 1
11	105.0	99.8	98.1	101.0	1.5	8.3	4.9	4.9	8.6	0.2	91	67	94	84	0.6	3.6	0.6	1.6	4	9	10	S 3	S 6	W 5
12	91.8	95.3	104.1	97.1	4.0	4.9	4.6	4.5	6.0	1.5	95	92	97	94	0.5	0.7	0.3	0.5	10 ●	10	10 ●	S 3	WNW 2	NNW 3
13	108.6	109.3	111.0	109.6	2.6	6.4	4.4	4.4	7.8	1.9	95	82	93	90	0.4	1.7	0.6	0.9	10	9	10	W 1	W 3	C 0
14	113.4	114.6	113.4	113.8	2.0	4.7	3.6	3.5	7.8	1.8	96	90	97	94	0.3	0.8	0.3	0.5	10 =	10	0 =	SE 2	SE 2	SE 1
15	114.0	115.0	113.3	114.8	-5.9	10.2	4.4	3.8	13.1	-4.1	99	67	84	83	0.1	4.0	1.4	1.8	0 =	0	0	C 0	C 0	SW 2
16	117.7	119.2	122.0	119.6	6.0	7.0	5.6	6.0	7.6	-1.3	89	85	91	88	1.1	1.4	0.9	1.1	10	10	10	W 5	WNW 4	NW 1
17	122.1	122.6	121.6	122.1	5.0	8.6	1.6	4.2	10.4	1.2	97	70	96	88	0.3	3.3	0.3	1.3	10	7 ⊙	0	C 0	S 1	S 1
18	119.6	118.3	116.4	118.1	-1.3	9.0	2.8	3.3	12.5	-3.0	100	66	79	82	0.1	4.0	1.6	1.9	10	0	0	C 0	SE 2	WSW 1
19	116.2	116.2	118.3	116.9	2.2	7.0	4.0	4.3	7.4	-1.9	89	82	97	89	0.8	1.7	0.2	0.9	10 =	10	10 ●	WSW 2	NW 2	W 2
20	118.6	120.8	121.7	120.4	4.4	4.8	3.9	4.2	5.7	3.3	93	92	95	93	0.6	0.7	0.4	0.6	10 ●	10 ●	10	WNW 4	N 1	C 0
21	120.8	120.1	120.1	120.3	3.6	8.4	1.4	3.7	9.9	1.2	88	60	85	78	0.9	4.4	1.0	2.1	10	4	0	ESE 2	S 4	SSE 3
22	120.1	119.9	119.0	119.7	-3.1	6.1	0.4	1.0	7.6	-4.2	97	64	94	85	0.1	3.3	0.4	1.3	0 =	7 ⊙	0	E 1	SE 4	SSE 2
23	117.8	117.1	115.6	116.8	-0.6	5.6	1.3	2.0	6.3	-1.7	92	71	89	84	0.4	2.7	0.8	1.3	0	0	0	E 3	SSE 3	E 3
24	115.1	114.8	114.6	114.8	-1.9	4.1	2.3	1.8	8.3	-2.3	98	74	86	86	0.1	2.2	1.0	1.1	10 =	0	0	ESE 2	ESE 1	SE 2
25	115.3	116.4	116.4	116.1	-1.3	6.8	1.2	1.9	8.8	-1.3	96	60	89	82	0.3	4.0	0.8	1.7	0	0	0	ESE 3	SE 5	ESE 3
26	117.1	118.7	118.3	118.1	-1.3	8.6	0.9	2.3	10.1	-4.3	84	50	90	75	0.9	5.6	0.6	2.4	0	0	0	C 0	S 4	SSE 2
27	116.3	114.4	110.9	113.9	-0.5	11.2	8.3	6.8	12.1	-1.2	96	55	73	75	0.3	6.0	3.0	3.1	0	9	10	SSE 2	SW 8	S 3
28	100.2	95.8	101.2	99.1	7.2	7.7	4.6	6.0	11.3	4.1	80	65	71	72	2.1	3.7	2.5	2.8	10	10	10	S 3	SSE 6	W 9
29																								
30																								
31																								
M	106.8	106.8	107.3	107.0	1.2	5.8	2.7	3.1	7.3	-0.8	91	75	88	85	0.6	2.3	1.0	1.4	7.0	6.8	5.5	3.2	4.0	3.4

Wrocław - Gądów Mały $H_s = 116\ m$ $H_z = 118{,}6\ m$ $h_w = 20\ m$ **Styczeń - Janvier 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	OBLUDZENIE ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	.	.	-	= 0⁰⁰–24
2	6	0.0	.	-	✱°8¹⁰–10²⁵ = 0⁰⁰–24 ⌣ 20⁰⁰–24 ⊽ 2⁴²–5²⁵
3	6	3.6	.	-	●°9⁴⁵ 11³⁰ 17³⁰–21¹⁰ 21²⁰–24 = 0⁰⁰–24 ⌣ °0⁰⁰–9⁰⁰ ⊽ 0⁰⁰–2³⁰
4	8	.	.	-	●°0⁰⁰–1³⁰ = 0⁰⁰–11³⁰ 20³⁰–24
5	6	0.0	.	-	●°22⁴⁰–24 = 0⁰⁰–24 ⌣ °6⁰⁰–10⁰⁰ ⊽ 3⁴⁰–6³⁰
6	6	.	.	-	●°0⁰⁰⁻¹⁵ △ 3¹⁰–4⁴⁰ = 0⁰⁰ p. ⩾ 13³⁵–15³⁰ ⌣ 7³⁰–8⁴⁵
7	7	2.0	.	-	●°18⁴⁰ 19³⁰ 22²⁰–23²⁵ ✱°–24 = a. p–24 ⌣ a. ⊽ 4³⁰–5³⁰
8	6	.	.	-	✱ ●°0⁰⁰–2⁵⁰ = 0⁰⁰–24
9	6	0.9	.	-	●°6¹⁵–7¹⁵ ●°8⁴⁰–9⁰⁵ ●°23⁴⁰ 24 = 0⁰⁰–24
10	6	.	.	-	●°0⁰⁰–2³⁰ = 0⁰⁰–24
11	5	0.0	.	-	●°17¹⁵–21²⁰ ✱°–22¹⁰ ✱°–24 = 0⁰⁰–24
12	6	0.8	.	-	✱°0⁰⁰⁻³⁰ 8⁵³–10¹⁵ 10³⁰–11²⁰ ✱°▽–12¹³ ✱°–13¹³ = na. a. p. ∞ 12⁰–7⁵⁰
13	7	0.7	pż.	-	= 7⁴⁰–12³⁰ 15³⁰–24
14	5	6.5	.	-	●°5¹⁷–9³⁵ ✱⁰⁻¹ ✱–22⁴⁰ = 0⁰⁰–24
15	6	.	6	-	= 0⁰⁰⁻³⁵ =⁰⁻¹–23⁰ =–24
16	5	0.9	5	-	●°8⁴⁰–9²⁵ ✱⁰⁻¹ 17⁴⁵–19³⁵ ✱°22⁴⁰–23³⁰ = ≡°0⁰⁰–24
17	7	.	6	-	= 0⁰⁰–7⁴⁰ =°= 16²⁰–24
18	6	.	6	-	=ᵗ 0⁰⁰⁻²⁵ =–24
19	6	.	6	-	= 0⁰⁰–24
20	5	.	6	-	= 0⁰⁰–24
21	4	.	6	-	= 0⁰⁰–8³⁵ =°–17⁵⁰ =–24
22	5	0.7	6	-	✱°18³⁵ 19¹⁵ 20⁴⁰–21¹² 23³⁰–24 = 0⁰⁰–8³⁰ ≡°–17⁴⁰ =–24
23	5	2.0	7	-	✱⁰⁻¹ 0⁰⁰–14³⁶ = 0⁰⁰–24
24	5	0.0	8	-	✱°8¹⁰–11²⁰ = 0⁰⁰–24 ⌣ 17³⁰–22¹⁵ 23³⁰–24
25	6	0.0	8	-	✱°1¹⁵–2²⁷ 3¹⁶–5⁴⁰ 8⁴⁰–12¹⁰ = 0⁰⁰–15³⁰ 22³⁰–24 ⌣ 0⁰⁰⁻¹⁵
26	5	.	9	-	= 0⁰⁰–24
27	5	.	9	-	= 0⁰⁰–14³⁰ ∞–15³⁰ =–22³⁵ ≡°–24
28	7	.	9	-	≡°0⁰⁰–1⁰⁰ =–8¹⁵ ⩾ 19⁴⁰–20¹⁰ ⩽–20³⁵ ⊽ 17³⁵–19²⁰
29	6	.	9	-	= 11³⁰–24 ⌣ 20³⁰–23³⁰
30	8	0.1	pż.	-	●°11⁵¹ 23³⁰ = 0⁰⁰–3¹⁵ 4⁴⁵–5⁴⁰ ⩽ 8⁵⁹ 9⁴⁵ 11⁴⁰–12¹⁰
31	7	6.6	.	-	●°6¹⁵–14³⁵ 16³⁰–19³⁵ = 9³⁰ 19³⁵
Σ	–	24.8	–	-	UWAGI: Kierunki i prędkości wiatru w ciągu całego roku — wg anemometru

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1	5	5.7	.	-	●⁰⁻¹ 9⁴⁰ 17⁴⁵ = 5²⁰–24 ⊽ 2³⁰–4⁴⁰
2	7	5.2	.	-	= 0⁰⁰–7²⁰ 16²⁰–24
3	6	0.0	8	-	✱⁰⁻¹ 1²⁵ 2¹⁰–7¹⁰ 8¹⁵ ✱°▽ 14³⁰–15¹⁰ 18¹⁵–19⁰⁵ 20⁴⁰–22¹⁵ = na. p
4	6	0.1	3	-	✱°0²⁰ 2⁴⁰ 22¹⁵ 24 = 0⁰⁰–11³⁰ 12³⁰–24
5	6	0.0	1	-	✱°0⁰⁰–0³⁰ 2⁰⁵ 6²⁰ 8³⁰ ✱' 9⁴⁰ 10³⁵ = 0⁰⁰–13³⁰
6	7	0.9	pż.	-	= na.
7	7	0.2	.	-	●°3⁴² 5³⁵
8	6	0.7	.	-	●°2⁵⁰ 4⁵⁰ ●°▽ 8⁴⁰ 15⁰⁷ ●'▽–15²⁰ = 0³⁰ 24
9	5	12.2	.	-	●°6²⁰–8⁴⁰ ✱' 9¹⁰ ●°–12³⁰ ●●°–14³⁰ ●°–16³⁰ 17¹⁵ 9²⁰ 23¹⁰ ●°–24 = 0⁰⁰–20³⁰ 23³⁰–24
10	6	5.0	.	-	●●●●°0⁰⁰ 4¹⁰ ●°15⁰⁵ 17⁰⁵ = 0⁰⁰ 24 ⩾ a
11	5	3.8	.	-	●°1⁸⁰ 2⁰⁴ 16³⁰ 17⁴⁰ ●⁰⁻¹ 19⁴⁰ = 0⁰⁰–24
12	6	2.1	.	-	●°4⁵⁰ 6²⁰–10²⁰ 12¹³ ●°13²⁵ 14¹⁵–17¹⁵ 19⁵–20⁴⁰ ●°–21³² 22¹⁰ = na. 24 ≡°17³⁰–18²⁰
13	6	.	.	-	= 0⁰⁰–24
14	5	.	.	-	= ≡⁰⁻² 0⁰⁰–23³⁰
15	6	.	.	-	≡ᵗ⁻⁰ 0⁰⁰– 10³⁰ =–24 ∨ 2⁴⁵–9⁴⁵
16	6	0.0	.	-	●°10¹⁵ 11¹⁰ 16¹⁵ 22¹⁵ = 0⁰⁰–24
17	6	.	.	-	●°0¹⁵ 1³⁰ = 0⁰⁰–5⁴⁰ ≡°–6³⁰ =–13²⁰ 15¹⁰–18³⁰ =–21³⁰ ≡ᵗ⁻²–24
18	6	.	.	-	≡ᵗ⁻⁰ 0⁰⁰– 10¹⁰ =–14⁰⁰ ∞–17⁴⁰ =–24
19	5	1.2	.	-	●⁰⁻¹ 15¹⁵–22²⁰ ●°–23²⁵ ●–24 = 0⁰⁰–24
20	6	0.2	.	-	●ᵗ 0⁰⁰⁻¹⁵ ●°–10³⁰ 14¹⁵ 16⁴⁵–17³⁰ 18²⁰–19²⁰ = 0⁰⁰–24
21	7	.	.	-	= 0⁰⁰ 10¹⁰ 17¹⁵–24
22	6	.	.	-	= 0⁰⁰–6²² ≡°–8²⁰ =–16²⁰ 17³⁰–24 ∨ °6⁵⁰–8²⁰
23	5	.	.	-	= 0⁰⁰–24 ⌣ °0⁰⁰–10⁰⁰ 23⁰⁰–24
24	5	.	.	-	= 0⁰⁰ 2⁴⁰ =⁰⁻² 11³⁰ =–24 ⌣ 0⁰⁰–11⁰⁰
25	5	.	.	-	= 0⁰⁰–24 ∞ 18¹⁵⁻³⁰ ⌣ °2⁰⁰–9⁰⁰
26	6	.	.	-	= 0⁰⁰–12³⁰ ∞–17³⁰ =–24 ⌣ °0⁰⁰–9⁰⁰
27	7	2.4	.	-	●°15³⁵ 16¹⁰ = 0⁰⁰–11²⁰ 18⁴⁰–24 ⌣ 2⁰⁰–8⁰⁰ ⊕ 8²⁰–10¹⁵
28	6	0.0	.	-	●°12⁵–5³⁰ 10³⁰ ▽°16⁵² 19³⁰ = 0⁰⁰–17⁰⁰ ⩾ 16³⁶–18³⁰
29					
30					
31					
Σ	–	39.7	–	-	UWAGI.

Wrocław - Gądów Mały — φ = 51°08' — λ = 16°59' — Marzec - Mars 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.9	105.3	111.0	106.1	3.4	5.2	3.3	3.8	6.6	3.0	88	81	93	87	0.9	1.6	0.5	1.0	9	10 •	9	W 5	W 4	WNW 2
2	113.0	114.2	111.8	113.0	2.3	4.0	2.6	2.9	5.8	0.1	95	74	86	85	0.4	2.1	1.1	1.2	9	10	9	W 3	WNW 7	S 2
3	112.2	115.6	118.3	115.4	3.0	6.4	5.6	5.2	7.0	0.0	96	85	97	93	0.3	1.4	0.3	0.7	10 •	10	10 •	SW 1	WNW 1	WNW 2
4	120.8	122.5	122.3	121.9	4.8	7.4	1.4	3.8	8.1	1.3	94	77	92	88	0.6	2.3	0.6	1.2	10	8	5	NNW 1	WNW 3	SW 3
5	120.8	121.1	121.7	121.2	2.6	8.8	4.4	5.0	10.2	-0.6	86	71	93	85	1.1	3.3	0.6	1.7	9	10	0	W 5	N 5	NNW 2
6	121.4	121.2	118.5	120.4	4.1	8.4	3.5	4.9	10.8	0.7	92	73	93	86	0.7	3.0	0.5	1.4	8	8	0	WNW 2	WNW 3	WSW 1
7	115.9	114.8	116.5	115.7	1.0	12.1	7.6	7.1	14.7	-2.9	92	63	75	77	0.5	5.2	2.6	2.8	2	9	4	WSW 2	W 6	WNW 4
8	119.9	120.2	119.8	120.0	1.3	11.3	5.4	5.8	14.6	-0.8	89	59	80	76	0.8	5.4	1.8	2.7	6 ≡	1	0	WNW 1	W 6	W 3
9	119.5	118.4	116.8	118.2	2.3	14.2	7.0	7.6	16.7	0.2	89	42	74	68	0.8	9.5	2.6	4.3	2	2	0	W 4	WSW 6	W 2
10	114.2	111.1	108.2	111.2	-0.5	18.3	8.0	8.4	20.1	-1.7	90	29	70	63	0.6	15.0	3.2	6.3	3	2 ⊙	0	SSE 1	SSW 1	SW 2
11	108.5	109.9	110.9	109.8	5.7	12.2	9.8	9.4	13.9	2.8	86	61	75	74	1.3	5.6	3.0	3.3	5	2	10	W 2	W 8	W 5
12	109.1	104.1	94.9	102.7	7.6	14.3	14.1	12.5	17.2	7.5	77	50	48	58	2.3	8.1	8.4	6.3	9	9	9	W 6	W 6	SW 11
13	95.3	97.8	101.6	98.2	8.0	9.6	6.0	7.4	15.9	5.5	67	47	79	64	3.5	6.4	2.0	4.0	9	8	1	NW 7	NW 8	NW 2
14	101.3	100.6	103.3	101.7	4.4	9.6	8.7	7.8	10.5	4.2	97	92	88	92	0.3	1.0	1.3	0.9	10 •	10 •	10	S 2	NW 6	W 5
15	103.6	105.9	109.2	106.2	8.8	13.4	8.6	9.8	14.7	8.3	92	60	86	79	0.9	6.2	1.6	2.9	9	6 ⊙	0	WNW 8	WNW 9	W 5
16	106.3	105.9	108.7	107.0	9.3	13.5	9.8	10.6	14.6	8.2	80	55	67	67	2.3	7.0	4.0	4.4	9	10	0	W 9	NW 8	NW 5
17	110.8	109.0	101.9	107.2	3.4	14.6	9.2	9.1	16.9	1.7	95	60	79	78	0.4	6.7	2.4	3.2	9	4	7	WNW 2	W 6	SSW 3
18	92.5	91.2	90.5	91.4	10.0	15.2	8.0	10.3	17.0	6.6	61	57	74	64	4.8	7.5	2.8	5.0	8	4	10	SW 7	WNW 7	W 7
19	91.0	90.9	96.0	92.6	3.8	6.2	1.0	3.0	8.7	0.4	77	67	70	71	1.9	3.1	2.0	2.3	9	10	0	WSW 5	W 11	NNW 2
20	98.8	95.5	87.4	93.9	-4.8	4.5	3.1	1.5	6.8	-5.9	98	54	54	69	0.1	3.9	3.5	2.5	1	3	10	C 0	WSW 3	SSW 7
21	78.8	78.9	86.8	81.5	2.0	5.2	2.5	3.0	6.7	1.6	76	69	86	77	1.7	2.7	1.0	1.8	7	9	10	SW 6	WSW 9	NW 3
22	97.9	101.0	100.9	99.9	-0.2	2.0	0.4	0.6	3.6	-0.5	78	64	92	78	1.3	2.6	0.5	1.5	7	8 *	10 *	NW 3	WNW 6	SW 5
23	99.5	100.6	103.6	101.2	4.0	7.2	6.4	6.0	8.6	-0.1	92	78	87	86	0.6	2.2	1.3	1.4	10	10 •	10	W 7	W 6	W 6
24	104.2	104.5	105.7	104.8	6.5	9.5	8.3	8.2	11.9	5.3	81	66	75	74	1.9	4.0	2.8	2.9	10	10	10	W 6	W 10	W 6
25	106.8	107.4	108.1	107.4	6.0	11.1	7.5	8.0	12.5	5.0	86	64	86	79	1.3	4.8	1.5	2.5	7	8	10	W 6	W 10	W 3
26	106.0	101.3	94.4	100.6	6.4	13.0	9.7	9.7	14.3	5.5	84	44	63	64	1.6	8.4	4.4	4.8	10	6	10	SW 5	WSW 7	SW 5
27	95.5	95.4	95.7	95.5	5.6	8.1	0.8	3.8	11.7	0.3	62	34	85	60	3.5	7.1	1.0	3.9	9	8	9	W 8	W 14	W 9
28	96.6	97.3	99.2	97.7	-0.2	2.6	0.4	0.8	5.1	-1.0	88	88	90	89	0.7	1.0	0.6	0.8	9 *	10 •	3	W 10	W 10	WNW 4
29	97.9	96.6	95.8	96.8	2.0	5.3	6.8	5.2	7.9	0.2	87	89	75	84	0.9	1.0	2.5	1.5	10 •	10 •	10	W 7	W 9	WSW 9
30	91.6	91.8	87.0	90.1	5.8	8.2	8.9	8.0	11.1	4.0	79	81	79	80	2.0	2.1	2.4	2.2	10	10	10	SSW 7	SW 7	SW 8
31	92.8	94.3	93.8	93.6	3.0	6.6	4.9	4.8	10.6	2.8	91	61	84	79	0.7	3.8	1.4	2.0	10	9	10	NW 2	SW 2	W 7
M	104.7	104.7	104.5	104.6	3.9	9.3	5.9	6.2	11.4	2.0	85	64	80	76	1.3	4.6	2.1	2.7	7.9	7.5	6.3	4.5	6.6	4.5

Kwiecień - Avril

1	97.9	90.3	92.6	93.6	0.4	10.5	7.4	6.4	12.3	-1.5	80	67	87	78	1.3	4.3	1.3	2.3	8	10 •	10	S 2	SW 10	W 5
2	96.5	96.6	92.4	95.2	4.0	6.8	4.5	5.0	7.9	3.2	83	67	93	81	1.3	3.3	0.5	1.7	9	10 •	10 •	W 3	W 3	NE 2
3	88.8	92.8	95.4	92.3	8.6	10.2	3.3	6.4	12.1	3.3	88	59	90	79	1.4	5.1	0.7	2.4	10 •	9	7	SW 6	W 8	C 0
4	90.7	97.4	100.4	96.2	9.5	10.6	7.0	8.5	11.9	3.3	88	62	90	80	1.4	4.9	1.0	2.4	10 •	6	10 •	W 6	W 8	NNE 1
5	96.6	95.4	94.8	95.6	7.0	21.3	14.8	14.5	22.4	5.8	93	45	70	69	0.7	13.8	5.0	6.5	7	8 ⊙	10	SE 7	SSW 7	SSE 4
6	97.7	98.2	97.2	97.7	12.0	23.2	15.9	16.8	25.1	9.4	80	45	75	67	2.8	15.6	4.5	7.6	8	3	0	S 1	SSW 5	S 4
7	96.8	97.2	97.9	97.3	11.6	24.2	17.1	17.5	25.6	7.3	82	39	68	65	2.4	18.6	6.2	9.1	5	1 ⊙	6	ESE 2	WSW 4	SW 6
8	98.1	94.3	104.0	98.8	12.4	16.9	6.8	10.7	18.0	6.8	98	81	81	87	0.4	3.7	1.9	2.0	10 •	10 • R	10	N 1	C 0	WNW 5
9	106.3	107.9	107.2	107.1	3.6	8.0	3.0	4.4	10.0	2.7	86	45	74	68	1.1	5.9	2.0	3.0	5 ⊙	9 ⊙	0	WNW 3	WNW 3	NNE 2
10	104.3	101.2	97.8	101.1	1.3	9.6	7.7	6.6	10.6	-1.5	77	35	53	55	1.5	7.8	4.9	4.7	9	10	7	E 2	E 5	NE 2
11	95.6	96.1	99.8	97.2	5.1	14.4	7.5	8.6	16.1	4.1	69	45	72	62	2.8	9.1	3.0	5.0	9	0 ⊙	0	NE 2	NE 1	NNE 1
12	102.9	103.9	102.6	103.1	6.1	14.7	10.6	10.5	16.7	1.2	69	35	55	53	2.9	10.8	5.8	6.5	4 ⊙	2 ⊙	0	C 0	SE 3	SE 4
13	100.9	100.0	99.0	100.0	7.3	19.8	14.6	14.1	21.7	2.7	91	45	77	71	0.9	12.8	3.8	5.8	0 ⊙	4 ⊙	0	C 0	W 3	S 1
14	98.1	95.8	94.7	96.2	11.6	23.0	16.5	16.9	24.5	5.4	74	31	48	51	3.6	19.5	9.9	11.0	8 ⊙	7 ⊙	2	SE 2	SSE 2	S 5
15	97.6	95.8	96.2	96.5	11.3	21.4	14.1	15.2	23.6	7.9	91	46	85	74	1.2	13.7	2.4	5.8	3 ⊙	8	10	C 0	E 2	N 2
16	96.0	95.7	96.8	96.2	10.5	17.3	11.9	12.9	17.8	5.8	97	72	95	88	0.3	5.4	0.7	2.1	9	7 ⊙	10 •	C 0	N 1	WNW 3
17	98.8	98.6	98.9	98.8	9.5	14.6	11.5	11.8	16.9	7.3	95	65	85	82	0.7	5.8	2.0	2.8	9	7	10	WNW 2	W 2	C 0
18	99.0	97.9	98.6	98.5	8.7	19.7	13.9	14.0	21.2	5.8	100	41	76	72	0.0	13.4	3.9	5.8	0 ⊙	4 ⊙	8	SE 1	NE 2	N 1
19	102.7	103.1	103.4	103.1	9.4	15.3	8.5	10.4	16.5	8.4	93	46	72	70	0.8	9.3	3.2	4.4	10	9 ⊙	0	N 2	N 3	NNE 1
20	105.7	106.5	106.9	106.4	7.6	13.4	6.8	8.6	14.5	2.1	62	46	58	55	3.9	8.4	4.1	5.5	8 ⊙	9 ⊙	0	ENE 4	NE 2	NE 2
21	106.2	105.8	100.9	103.6	5.4	14.8	11.8	11.0	17.4	3.1	66	35	51	51	3.1	10.9	6.7	6.9	0 ⊙	0 ⊙	0	E 5	ESE 5	ESE 5
22	97.9	94.5	92.3	94.9	8.7	19.4	12.5	13.5	20.5	4.1	73	40	63	59	3.0	13.5	5.3	7.3	0 ⊙	1 ⊙	1	E 3	SSE 6	S 5
23	91.1	90.4	90.4	90.6	10.3	18.2	13.0	13.6	19.2	7.6	72	48	63	61	3.5	10.9	5.6	6.7	1	7	3	SE 7	SE 9	SE 5
24	92.9	95.3	96.4	94.2	8.9	18.6	10.4	12.1	19.8	5.5	73	47	66	62	3.0	11.4	4.2	6.2	0	1 ⊙	0	ESE 1	NE 5	ENE 4
25	97.7	98.4	97.8	98.0	9.3	10.5	11.0	10.4	11.7	5.9	75	68	74	72	2.9	4.1	3.4	3.5	10	10	9	NE 4	E 6	E 2
26	94.7	92.8	92.8	93.4	9.2	16.7	14.9	13.9	19.2	6.4	77	58	75	70	2.6	8.0	4.1	4.9	9	4 ⊙	4	E 4	SE 5	ESE 2
27	94.3	94.6	96.9	95.3	9.8	17.6	11.0	12.4	19.0	6.8	96	68	99	88	0.5	6.4	0.1	2.3	9	8	10 •	NNW 1	SW 1	C 0
28	96.9	96.2	94.9	96.0	10.4	13.3	9.8	10.8	15.7	3.7	97	86	99	94	0.3	2.1	0.1	0.8	10	7	4	W 1	WSW 1	C 0
29	94.8	94.7	95.6	95.0	10.9	18.5	11.0	12.8	19.6	8.7	91	63	91	82	1.1	8.0	1.1	3.4	9	8	8	NE 2	ESE 3	NE 1
30	94.8	95.0	92.6	93.5	10.0	20.1	14.1	14.6	21.4	6.8	88	47	68	68	1.5	12.6	5.1	6.4	1 ⊙	5	2	NE 1	NE 4	NE 2
31																								
M	97.7	97.2	97.6	97.5	8.4	16.1	10.8	11.5	17.6	5.1	83	53	75	70	1.8	9.3	3.4	4.8	6.3	6.1	5.0	2.5	4.0	2.5

Wrocław - Gądów Mały $H_s = 116\,m$ $H_b = 118{,}6\,m$ $h_w = 20\,m$ Marzec - Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	1.0	.	–	● 2⁴⁰ 3¹⁰ . 3⁵⁰ – 5⁴⁰ , 8⁰⁵ – ³⁰ ▽ p... , = 6³⁰ – 15³⁰
2	6	1.1	.	–	= 6³⁰ – 24
3	6	1.1	.	–	● 1⁰⁰ – 2³⁸ , ● 4³² – 5¹⁵ , ● 22¹⁰ , = 0⁰⁰ – 22⁴⁵ ≡ – 24
4	6	.	.	–	● 0⁴⁵ 1⁴⁰ , 2¹⁰ – 5³⁰ ≡ 0⁰⁰ – 1⁴⁰ , = – 14³⁰ 18³⁰ – 24
5	6	.	.	–	= 0⁰⁰ – 15²⁰ ∞ – 17³⁰ = – 21¹⁰ ≡ ⁰⁻¹ – 24 , ∪ 22⁵⁰ – 24
6	6	.	.	–	≡ 1⁰⁰ – 4²⁵ , = – 13³⁰ , 17¹⁰ – 24 , ∪ 0⁰⁰ – 1³⁰
7	6	.	.	–	= , ≡ 0⁰⁰ – 11²⁰ ∞ – 18³⁰ = – 24 , ⌣ 4³⁰ – 7⁰⁰
8	6	.	.	–	= 0⁰⁰ – 5⁵⁰ ≡ 7⁴⁰ – 24 , ⌣ 3⁰⁰ – 9⁰⁰
9	6	.	.	–	= 0⁰⁰ – 9⁴⁵ ∞ – 13³⁰ = p – 24 , ⌣ 5⁸⁰ – 9⁰⁰
10	7	.	.	–	= 0⁰⁰ – 5¹⁰ = – 6⁴⁵ = – 9²⁰ ∞ – 11⁴⁰ 17²⁵ – 18¹⁵ , ⌣ 6⁰⁰ – 8⁰⁰
11	6	.	.	–	= 6²⁰ – 13³⁰ ∞ – 15³⁰ = – 24 , ⟫ 10³⁰ – 12³⁰
12	7	1.4	.	–	= 0⁰⁰ – 11³⁰ , 16³⁰ – 20³⁰ , ⟫ 18²⁰ – 19⁵⁰ , 20¹⁰ – 24
13	8	1.2	.	–	● 0⁴⁰ 3⁴⁰ – 4²⁰
14	6	7.4	.	–	● ⁰⁻¹ 5³⁵ – 12²⁰ , ● ⁰ – 15³⁰ , 17¹⁰ – 19⁴⁰ , = 7¹⁰ – 24
15	7	.	.	–	● 4⁴⁰ – 5²² , ● 6³³ – ⁴⁰ , = 0⁰⁰ – 9³⁰ , 20³⁰ – 24
16	7	.	.	–	= 0⁰⁰ – 2³⁰ 5³⁰ – 12²⁰ ⟫ 14⁰⁵ – 15³⁰
17	7	.	.	–	= 0⁴⁰ – 9⁴⁰ 16²⁰ – 24 , ⌣ 2⁵⁰ – 7²⁰ , ⌒ 21⁰⁰ – 24
18	7	.	.	–	= 16¹⁵ – 22³⁵ , ⌒ 0⁰⁰ – 4⁰⁰
19	7	0.0	.	–	● ▽ 12¹⁴ 16³⁰ ⟫ 9³⁰ – 13³⁰
20	8	0.0	.	–	✱ ▽ 15²⁸ – ³⁶ , ● 23⁴⁵ 24 , ⌣ 3³⁰ – 7³⁰
21	8	2.3	.	–	● 0⁰⁰ – ³⁰ ● ✱ 3⁴⁰ , ● 5⁵⁰ ▽ 9¹⁰ 13⁴⁵ ▽ △ ⁰⁻¹ 23³⁵ , = p , ⟫ a, p , ⊕ 12⁴⁰ – 13⁰⁵
22	8	1.0	.	–	✱ ▽ 10⁴⁵ 11²⁵ 12⁴⁵ – 13⁰⁵ ✱ 19³⁵ 20¹⁰ – 22³⁰ ✱ – 24 , = 21¹⁵ – 24
23	6	0.5	.	–	✱ 0⁰⁰ – ¹⁰ ● – 0⁵⁰ ● ▽ ⁰⁻¹ 9¹⁵ 18²⁰ = na a, p
24	7	0.0	.	–	● 10⁴⁵ 11⁰⁵ , = ³⁰ – 11²⁰ , ⟫ 11¹⁵ – 16¹⁰
25	7	0.0	.	–	● ▽ 11¹⁰ – ¹⁵ 14⁴⁵ – 15¹⁰ , 15³⁰ 16¹⁵ , = 6⁰⁵ – 7⁴⁰ , p, np , ⟫ 12³⁰ – 13²⁰
26	7	0.0	.	–	= 0⁰⁰ – 10³⁰ , ⟫ 23³⁰ – 24 , ∪ 19⁴⁰ – 20²⁰
27	8	0.5	.	–	● 0¹⁵ – 2¹⁵ 3⁴² – 4¹⁰ ● ▽ ✱ ⁰⁻¹ 12¹² 19³⁰ = p , ⟫ 7³⁰ – 15³⁰
28	6	3.7	1	–	✱ ▽ ⁰⁻² 3¹² 7⁵⁰ ✱ ⁰⁻¹ – 8⁴⁰ ▽ ● 11⁴⁰ 13²⁰ ● ✱ 13⁴⁰ – 15⁰⁵ ✱ ▽ ²⁻¹ 16⁴³ 17⁴⁵ , ◺ 17¹²⁻⁴⁰ , ⟫ na , 4³⁰ – 16²⁰
29	6	3.9	1	–	✱ ▽ 0⁵⁰ 1³⁵ ✱ ▽ – 2⁰⁵ ✱ – 3³⁰ ✱ – 4²⁰ ● – 5¹⁰ , 6²⁵ – 8³⁵ ✱ – 9¹⁵ ● 17¹⁵ , 21³⁵ – 22²⁰ , = 2⁵⁰ – 24 , ⟫ 10⁴⁰ – 12²⁰
30	7	2.9	.	–	● 5⁴⁵ 19¹⁵ , = 0⁰⁰ a, p – np
31	8	0.2	.	–	● 10⁵ 6¹⁰ 16⁴⁵ 17³⁰ – 19¹⁵ , = 17³⁰ – 21³⁰ , ⊕ 14³⁰ – 15³⁰ ∪ 22¹⁵ – 23³⁰
Σ	–	28.2	–	–	UWAGI.

Kwiecień - Avril

1	7	3.5	.	–	✱ ⁰⁻¹ 8³⁰ – 9⁴⁰ ✱ ⁰ – 10⁰⁰ ● ▽ ⁰ 11⁴⁵ 23²⁰ , ⟫ ⟫ 11¹⁵ – 13⁴⁵ , = 8²⁰ – 10¹⁵ , 18⁴⁰ – 19³⁵
2	7	4.6	.	–	● ⁰⁻¹ 12³⁰ – 24
3	7	2.3	.	–	● ⁰ 0⁰⁰ – 2³⁰ 3⁴¹ ● ⁰⁻¹ 6³⁰ 7⁴⁵ ● ⁰ 8²⁰ 9³⁰ , = 0⁰⁰ – 5³⁰
4	7	1.5	.	–	● ⁰ 1⁴⁰ 4⁵⁰ 5⁵⁰ 7¹⁵ 19⁴⁰ 24 , = 18²⁰ – 24
5	8	.	.	–	● ⁰ 0⁰⁰ .. 3⁵ 1⁸ – 2³⁰ , 4⁴⁰ 5⁰⁵ , = 0⁰⁰ – 10¹⁰ , ⊕ 13¹⁰ – 15³⁰
6	7	0.0	.	–	● ▽ ⁰ 9¹⁰ – ¹⁵
7	8	2.0	.	–	● ▽ ⁰ 17⁰²⁻¹⁴ 20²⁰⁻³⁵ 21³⁵ – 22⁴⁰ ◺ ⁰ 16⁵⁰ – 17¹⁴ , = a ∞ – 11³⁰ , ⌒ ¹ 17¹⁰⁻²⁰
8	6	22.1	.	–	● ⁰ 5⁴⁰ 9²⁵ ● ▽ ⁰⁻² 12⁵⁰ – 14¹⁰ ● ▽ ⁰ 14²⁵ – 17⁵⁸ , (◺) ⁰ 12⁴⁴⁻⁵⁰ SW-NE , = 4⁴⁰ – 14⁰⁵
9	9	.	.	–	⌒ ⁰⁻¹ 19⁰⁰ – 24
10	7	.	.	–	= 0³⁰ – 9²⁰ ∞ – 11³⁰ ⌒ ⁰⁻¹ 0⁰⁰ – 7⁰⁰
11	6	.	.	–	= 6³⁰ – 9²⁰ ∞ – 13⁴⁰
12	7	.	.	–	= 5²⁵ – 7³⁰ , ⌒ ⁰ 1⁰⁰ – 8³⁰ , 19³⁰ – 24
13	7	.	.	–	= 4¹⁵ – 9⁰⁰ ∞ – 13³⁰ 17⁰⁰ – 22⁰⁰ = – 23⁴⁵ ≡ ⁰ – 24 , ⌒ ⁰ 0⁰⁰ – 8⁰⁰ , 19⁰⁰ – 24
14	7	.	.	–	≡ ⁰ 0⁰⁰ – 1²⁰ = – 4⁴⁰ ≡ ⁰ – 5⁰⁵ , ⌒ ⁰⁻¹ 0⁰⁰ – 10⁰⁰ 20⁰⁰ – 23⁰⁰
15	7	8.0	.	–	▽ ¹ 15⁴⁰ – 17⁴⁰ ▽ ⁰⁻² 18³⁰ – 20²⁰ ◺ 16²⁷ – 17³⁰ SW – NE , 18¹⁵ – 20⁴⁵ SW-NE , = 1³⁰ – 11³⁰ ⌒ ⁰⁻¹ 1⁰⁰ – a
16	7	10.1	.	–	● ⁰ 7³⁰ – 8²⁰ ▽ ⁰⁻¹ ● ⁰⁻¹ 13³⁵ 23¹⁰ , ◺ 13⁰⁵ – 14⁴⁵ SW-NE , 21¹⁵ – ³⁰ SW-NE , = , ≡ 0⁰⁰ – 12³⁰ , p
17	8	.	.	–	= 0⁰⁰ – 12⁰⁰ , 18³⁰ – 24 , ⌒ ⁰⁻¹ 19⁰⁰ – 24
18	7	.	.	–	= 0⁰⁰ – 2⁴⁰ ≡ ⁰⁻² – 6⁴⁰ = – 12³⁰ 19³⁰ – 24 , ⌒ ¹⁻² 0⁰⁰ – 7²⁰ ⌒ ¹ 21⁰⁰ – 24
19	8	.	.	–	= 0⁰⁰ – 8³⁰ , ⌒ ¹ 0⁰⁰ – 9⁰⁰ ⌒ ⁰⁻¹ 20⁰⁰ – 24 , ⊕ 12⁰⁰ – 14⁰⁰
20	8	.	.	–	= 0³⁰ – 4¹⁰ , ⌒ ¹ 0⁰⁰ – 8⁰⁰ ⌒ ⁰ 21⁰⁰ – 24 , ⊕ 9⁴⁵ – 10¹⁵
21	8	.	.	–	⌒ ⁰ 0⁰⁰ – 10⁰⁰ , 22⁴⁰ – 24
22	8	.	.	–	= 2⁴⁰ – 8²⁰ , ⌒ ⁰ 0⁰⁰ – 8⁰⁰
23	8	.	.	–	= 1³⁰ – 7¹⁰ , ⌒ ¹ 1⁰⁰ – 7⁰⁰ ⌒ ⁰ 21⁰⁰ – 24
24	8	.	.	–	= 8³⁰ – 10³⁰ , ⌒ ⁰ 0⁰⁰ – 8⁰⁰
25	7	.	.	–	
26	8	.	.	–	– 4²⁰ – 7³⁰ 18¹⁵ – 24 , ⌒ ⁰ 2⁰⁰ – 7³⁰ , 19³⁰ – 24
27	5	7.5	.	–	▽ ⁰⁻² 16⁴⁵ 21³⁰ , ◺ ¹ 16⁵⁶ – 17⁵³ NW – SE , = 0⁰⁰ – 14³⁰ , p , ⌒ ⁰⁻¹ 0⁰⁰ – 8⁰⁰
28	6	0.6	.	–	● ▽ ⁰ 3⁵³ – 4⁰⁰ ● ⁰ 5²² – 6³⁰ 7¹⁰ – 10¹⁰ , = 0⁰⁰ – p , np , ⌒ ⁰ p – 24
29	7	2.1	.	–	▽ ⁰ 16⁴⁰ – ⁵⁸ ▽ ⁰⁻¹ 18²² 19⁰⁷ , ◺ 14⁴² – 17¹⁵ SW – N , = 0⁰⁰ – a, p, np = np ; ⌒ ⁰ na – a
30	7	.	.	–	= , ≡ 0⁰⁰ – 12³⁰ = 19⁴⁰ – 24 , ⌒ ⁰ 21⁰⁰ – 24
31					
Σ	–	64.3	–	–	UWAGI.

Wrocław - Gądów Mały — φ = 51°08' — λ = 16°59' — Maj - Mai 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	96.2	96.6	98.8	97.2	10.3	17.4	11.4	12.6	19.7	5.3	92	65	94	84	0.9	7.0	0.9	2.9	10	7	10	WNW 2	W 3	N 2
2	99.2	98.4	97.5	98.4	11.4	15.9	12.1	12.9	17.9	8.9	83	68	87	79	2.3	5.8	1.8	3.3	10	8 ⊙	9	W 3	WSW 2	C 0
3	96.1	95.6	99.0	96.9	10.4	16.3	11.5	12.4	19.4	6.4	91	70	88	85	1.1	5.6	1.7	2.8	8	8 •	6	SSE 2	W 5	W 2
4	102.0	102.6	102.5	102.4	10.2	19.0	13.2	13.9	19.4	4.1	88	59	76	68	1.4	13.4	3.7	6.2	2	4	5	W 2	W 1	S 2
5	101.8	100.3	99.8	100.6	12.4	21.1	16.7	16.7	22.6	8.7	75	55	76	68	3.5	11.8	4.6	6.6	9	9	2	SE 2	S 7	SSE 5
6	97.7	101.3	103.0	100.7	14.0	14.2	12.0	13.0	19.7	11.7	97	94	89	93	0.6	0.9	1.5	1.0	10	10 •	8	N 1	NW 3	S 2
7	101.9	99.3	99.2	100.1	14.0	18.8	9.1	12.8	19.4	9.0	89	58	84	77	1.8	9.2	1.9	4.3	2	10	1	SW 2	W 8	W 3
8	100.0	99.0	99.4	99.5	10.8	15.8	8.4	10.4	15.2	6.0	84	57	77	73	2.2	6.9	2.5	3.9	6	7 ⊙	9	SW 5	W 9	WSW 7
9	94.6	92.8	93.8	93.7	9.2	10.2	8.2	9.0	13.6	6.2	77	82	90	83	2.6	2.2	1.1	2.0	10	10	9	SW 6	WSW 7	W 5
10	95.9	97.5	100.4	97.9	8.0	11.6	7.7	8.8	12.1	7.3	94	72	96	87	0.6	3.7	0.5	1.6	10 •	9	10	WNW 6	WNW 8	W 6
11	101.9	102.8	105.7	103.5	7.5	9.0	8.2	8.2	11.9	6.3	93	83	87	88	0.8	2.0	1.4	1.4	10 •	8	9 •	NW 2	C 0	N 2
12	106.8	104.1	102.4	104.4	5.6	10.4	6.5	7.2	12.4	3.3	89	59	78	75	1.0	5.1	2.2	2.8	9	8	4	WNW 1	NW 5	W 2
13	102.5	99.8	98.4	100.2	7.4	11.8	9.6	9.6	13.8	2.3	87	63	87	79	1.3	5.0	1.6	2.6	9	10 •	9	WNW 2	SW 6	W 2
14	97.5	97.1	97.3	97.3	8.3	11.5	5.1	7.5	12.4	5.1	86	51	83	73	1.6	6.7	1.5	3.3	9	6	1	NW 3	W 11	SW 2
15	98.9	99.5	100.8	99.7	7.6	12.6	8.9	9.5	14.5	5.1	91	55	79	75	0.9	6.6	2.4	3.3	9	6	9	W 6	WNW 7	NW 2
16	101.3	99.3	97.5	99.4	6.8	11.4	8.2	8.6	13.6	3.0	81	63	99	81	1.9	5.0	0.2	2.4	3	9 •	10	C 0	WSW 5	W 1
17	100.8	102.7	104.2	102.6	7.3	10.7	9.7	9.4	12.3	5.1	94	78	96	89	0.6	2.9	0.4	1.3	10	9	10	N 4	NW 5	WNW 2
18	104.8	104.4	102.2	103.8	6.9	14.4	10.8	10.7	16.2	4.8	96	51	81	76	0.4	8.1	2.5	3.7	9	8	9	WNW 4	NW 3	WNW 3
19	101.8	100.6	99.5	100.6	10.4	16.6	11.2	12.4	17.8	4.4	83	56	85	75	2.1	8.4	2.0	4.2	6	9	10	NW 1	W 4	SW 2
20	97.4	95.0	94.4	95.6	9.6	14.8	11.1	11.6	16.5	7.0	89	70	97	85	1.3	5.0	0.3	2.2	9	10	10	WSW 1	W 2	S 1
21	94.9	94.5	97.0	95.5	9.6	18.5	11.6	12.8	19.6	5.3	96	64	96	85	0.5	7.6	0.5	2.9	8	10	10 •	C 0	ENE 2	C 0
22	98.5	98.8	98.8	98.7	8.8	15.9	9.4	10.9	16.8	8.6	95	63	83	80	0.6	6.7	2.0	3.1	8	3	3	N 2	NNE 5	NNE 1
23	99.5	99.9	99.3	99.6	10.8	16.4	12.2	12.9	18.4	5.3	87	59	78	75	1.7	7.6	3.2	4.2	4	9	10	C 0	NE 2	SW 1
24	101.7	102.0	101.6	101.8	10.9	16.6	9.9	11.8	19.0	7.5	80	77	96	84	2.6	4.4	0.5	2.5	6	10	7	NW 1	W 2	C 0
25	102.0	100.9	99.2	100.7	10.6	17.9	11.6	12.9	20.7	2.7	88	61	88	79	1.5	8.0	1.6	3.7	0	1 ⊙	0	NW 1	NW 3	NNE 2
26	98.8	97.3	94.2	96.8	13.1	21.4	18.9	18.1	23.3	5.6	70	44	46	53	4.5	14.3	11.7	10.2	0 ⊙	3	4	ENE 1	SSE 3	E 3
27	94.4	94.6	95.4	94.8	16.5	19.7	13.6	15.8	21.2	10.7	77	62	84	74	4.4	8.6	2.5	5.2	5	8	7	WSW 4	NW 4	NW 1
28	95.7	97.5	97.7	97.0	10.5	8.8	7.6	8.6	14.1	7.3	86	93	93	91	1.8	0.8	0.7	1.1	10	10 •	10	NNW 4	W 5	W 2
29	92.3	87.8	84.2	88.1	8.4	12.1	11.0	10.6	15.8	7.3	79	84	96	86	2.2	2.2	0.5	1.6	10	10	10 •	NE 1	NE 3	W 5
30	86.3	88.8	90.0	88.4	9.3	11.6	10.4	10.4	13.3	9.1	95	82	90	89	0.6	2.4	1.3	1.4	10 •	10	10	WSW 4	SW 3	W 2
31	90.8	90.9	90.2	90.6	10.9	15.8	14.4	13.9	17.8	9.0	83	57	73	71	2.2	7.6	4.4	4.7	10	7 ⊙	9	S 3	S 3	C 0
M	98.5	98.1	98.2	98.3	9.9	14.7	10.7	11.5	16.8	6.3	87	66	86	80	1.7	6.2	2.1	3.3	7.5	7.9	7.4	2.5	4.4	2.3

Czerwiec - Juin

1	89.8	89.9	88.4	89.4	15.2	25.6	19.9	19.6	26.2	8.1	78	59	65	67	3.9	11.9	8.1	8.0	0	4 ⊙	7	SE 1	SSE 1	SE 3
2	88.8	91.0	92.3	90.7	17.2	24.2	16.4	18.6	26.0	13.4	77	47	80	68	4.5	15.9	3.6	8.0	4	4 ⊙	4	S 2	WSW 2	C 0
3	93.3	93.1	95.0	93.8	13.4	23.3	15.7	17.0	23.8	11.2	88	61	98	82	1.8	11.1	0.4	4.4	9 • R	3	10 (R)	WNW 6	NNW 2	W 1
4	95.9	96.0	98.1	96.7	15.4	23.1	17.1	18.2	24.4	14.1	97	72	94	88	0.6	8.0	1.2	3.3	10	5 ⊙	9	WNW 3	WSW 2	NNE 1
5	99.6	99.5	100.1	99.7	15.3	24.1	17.1	18.4	25.4	11.5	100	59	92	84	0.0	12.3	1.6	4.6	10 ≡	5 ⊙	8	WNW 1	NE 2	ENE 1
6	99.7	98.3	96.7	98.2	17.0	21.7	17.3	18.3	24.3	12.4	77	68	85	77	4.5	8.3	2.9	5.2	2 ⊙	8 •	8	E 3	SE 2	E 2
7	95.6	94.3	95.3	94.4	16.6	25.6	17.5	18.8	24.9	15.1	94	63	89	82	1.2	10.8	2.2	4.7	9	7 ⊙	7	SE 1	SE 3	C 0
8	95.4	96.6	98.1	96.7	16.3	19.3	18.6	18.2	22.9	12.5	94	84	82	87	1.1	3.6	3.9	2.9	10	9	10	WSW 1	WNW 2	NW 1
9	98.8	98.7	97.0	98.2	16.1	21.8	18.9	18.9	25.6	11.2	97	68	88	84	0.6	8.3	2.5	3.8	10	6	8	NE 1	C 0	C 0
10	97.0	97.2	99.1	97.8	18.1	24.0	15.3	18.2	25.8	12.2	82	63	93	79	3.7	10.9	1.2	5.3	1	7	9 • (R)	SE 1	S 6	W 5
11	100.6	101.2	99.7	100.5	13.5	14.3	15.2	14.6	17.0	12.6	98	96	94	96	0.4	0.7	1.0	0.7	10 •	10	10	W 5	WNW 3	C 0
12	98.4	97.4	97.3	97.7	15.0	18.3	15.2	16.0	20.4	12.3	86	68	80	78	2.4	6.8	3.5	4.2	10	8 ⊙	4	W 5	C 0	WSW 2
13	95.2	92.5	89.5	92.4	13.8	20.7	16.2	16.7	22.5	9.1	80	52	86	73	3.2	11.7	2.5	5.8	5 ⊙	7 ⊙	9	C 0	SSE 5	SSE 4
14	92.3	95.7	99.2	95.7	12.3	15.4	13.6	13.7	16.7	11.9	96	73	87	85	0.5	4.8	2.0	2.4	10 •	10	10	WSW 7	W 9	W 5
15	101.9	102.4	103.7	102.7	12.4	15.3	10.2	12.1	17.6	9.5	72	53	81	69	4.0	8.2	2.4	4.9	3 ⊙	8	0	W 6	W 7	WNW 1
16	104.9	105.1	104.8	104.9	10.2	15.9	14.4	13.7	20.2	4.8	83	60	74	72	2.0	7.2	4.3	4.5	10	3	3	W 3	WSW 3	W 2
17	106.7	105.9	105.2	105.9	12.4	21.3	16.3	16.6	22.9	4.5	77	47	79	68	3.4	13.5	3.8	6.9	0	4 ⊙	10	WSW 1	WNW 1	SW 1
18	104.3	102.6	100.9	102.6	16.6	25.7	19.5	20.3	27.2	8.9	72	47	78	66	5.3	17.6	5.1	9.3	0 ⊙	1 ⊙	1	S 1	WSW 5	SSW 2
19	104.0	106.8	108.4	106.4	18.0	16.1	15.3	16.2	20.9	13.6	92	94	67	84	1.6	1.2	5.8	2.9	10 9	10	1	WNW 2	W 3	NW 3
20	112.8	112.7	111.1	112.2	13.0	18.8	11.6	13.8	20.6	5.9	78	41	79	66	3.3	12.9	2.8	6.3	7 ⊙	5 ⊙	0	WNW 3	NW 1	C 0
21	108.6	106.5	110.3	108.5	14.2	22.1	14.8	16.5	24.3	6.4	64	49	80	64	5.8	13.7	3.3	7.6	1 ⊙	4 ⊙	3	SE 2	W 1	N 1
22	110.6	105.9	98.7	105.1	13.4	21.3	21.0	19.2	25.6	4.4	78	54	78	70	3.3	11.5	5.6	6.8	0 ⊙	0	10 (R)	SE 4	SE 3	C 0
23	103.3	105.1	104.9	104.4	16.9	22.3	16.1	17.8	23.3	15.1	86	50	79	72	2.7	13.5	3.8	6.7	6	5	2	W 5	WNW 8	C 0
24	105.8	106.8	105.4	106.0	17.9	22.7	18.5	19.4	24.9	10.0	77	49	77	68	4.8	14.2	4.9	8.0	4	10 ⊙	10	W 5	W 7	S 1
25	104.3	101.9	98.9	101.7	18.1	27.9	21.4	22.2	29.7	10.2	77	37	70	61	4.9	25.6	7.8	12.1	2 ⊙	0	0	WSW 1	SW 5	SSE 1
26	98.5	98.5	96.1	97.7	18.9	26.8	21.7	22.3	28.1	13.5	83	52	76	70	3.7	17.0	6.4	9.0	5	10	0	WSW 1	S 3	SE 2
27	93.1	94.6	94.7	94.1	21.7	25.6	18.8	21.2	28.3	17.5	77	63	91	77	6.0	12.1	1.9	6.7	7	9	6	SSE 3	SW 5	C 0
28	104.9	109.8	113.2	109.3	14.6	16.7	12.6	14.1	21.0	12.5	67	51	79	66	5.5	9.2	3.1	5.9	8 ⊙	7 ⊙	0	NW 7	NW 5	W 5
29	115.3	115.0	113.6	114.6	14.3	20.7	15.5	16.6	22.9	9.0	77	47	83	69	3.8	13.0	3.0	6.6	7 ⊙	3 ⊙	1	W 3	NW 4	C 0
30	114.5	112.7	111.2	112.8	15.9	24.7	17.2	18.8	26.9	7.8	79	45	78	67	3.8	17.2	4.3	8.4	0 ⊙	2 ⊙	0	C 0	SSW 2	C 0
31																								
M	101.1	101.1	100.8	101.0	15.5	21.4	16.6	17.5	23.7	10.7	83	59	82	75	3.1	11.0	3.3	5.9	5.7	5.8	5.3	2.8	3.4	1.5

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁO. NIECZ. NIENIE	POGODA
1	7	1.8	.	–	▽° 17³² 20⁰⁰ ●° – 23⁰⁰ 24. = 0⁰⁰–2⁴⁰ = – 3²⁰ ≡° – 4⁴³ = – 11³⁰. ⌒° n, a
2	6	.	.	–	●° 0⁰⁰..10. = na, a, p – 24 ≡° 3²⁰–50. ⌒° 19⁰⁰–24
3	8	4.6	.	–	▽⁰⁻¹ 12⁴⁷ 19⁰⁵ ▲¹ 15⁰⁸–11. ☇ 14⁵⁰–15¹². = a – a = 4²⁰–⁴⁵. ⌒¹ 0⁰⁰–10¹⁰
4	8	.	.	–	= 0³⁰–3⁴⁰ = – 5⁵⁰ = – 6⁰⁰ = – 10³⁰. 21⁰⁰–24. ⌒ 0⁰⁰–9⁰⁰
5	8	2.0	.	–	= – 0⁰⁰–5³⁰. ⌒° 0⁰⁰–8⁰⁰
6	6	4.4	.	–	▽° 4⁵⁰–5¹⁰ ●°..7⁴⁰ ▽⁰⁻¹ 11²⁸–13⁰⁸. = na – p, np. ⌒ na
7	8	3.4	.	–	▽° 4³⁶–⁴² ▽¹ 11²⁰–⁴⁰ ●¹⁻⁰ 17³³–18²⁰. = 0⁰⁰–a = 5²⁰–³⁵. ≫ 17³⁵–18¹⁰. ⌒ na
8	8	1.2	.	–	▽⁰⁻¹ 7⁰⁷ 19³² ▽° 23²⁸–24. ☇° 15⁵⁴–16⁰² NW–SE. ≫ 10²⁵ 16⁰¹ ≫ 16³⁰–17¹⁰
9	8	5.3	.	–	▽° 0⁰⁰–10 7¹⁴ 7³⁰–9⁰² ▽⁰⁻¹ 11³⁰–12²². ▽° 17¹⁸ 18¹⁷ ●° 19³⁰ 20³⁹
10	7	11.0	.	–	●° 12⁰ 9³⁰ ▽° 13⁰² 16¹⁰ ●° – 18³⁰ ▽° – 18⁴⁵ ▲ – 18⁵⁰ ▽¹⁻⁰ 20³⁰. ≫ 19⁰⁰–15
11	8	5.6	.	–	●° 0¹⁹–2⁴⁰ 7¹⁰ ▽⁰⁻¹ 7³⁰ 21¹⁵ ▲ 11⁴⁵ 14³¹
12	8	0.0	.	–	▽° 7⁴⁰–9³⁵ 18¹²–¹⁴
13	6	2.0	.	–	●¹ 12⁴⁵–15¹⁵ ▽° 18¹⁵–²⁵ ●° 22⁴⁵–23³⁰ 23⁵⁰–24. = 0⁰⁰–10⁰⁰. 18⁴⁰–24
14	8	.	.	–	●° 0⁰⁰..20 ▽° 6³⁰–6⁴⁰. = 0⁰⁰–8³⁰. ≫ 10³⁰–13⁴⁰
15	8	0.0	.	–	▽° 10²⁵–30. = 6³⁰–7¹⁵. ⌒° 21⁰⁰–24
16	8	5.4	.	–	●° 12⁴⁷ 16²⁵ ▽¹ – 16⁴⁵ ▽° – 17⁰⁰ ●° – 20⁴⁰. 21³⁰–22³⁵. ⌒° 0⁰⁰–8⁰⁰
17	-7	0.3	.	–	●° 0⁴⁰ 2³⁰ ●¹ – 3⁵⁰ ●° 14⁵⁰..⁵⁵ ▽° 16⁰⁰–⁰⁵ ●° 16⁴⁰ 17¹⁰ – 17⁴⁰. = p – np
18	8	.	.	–	= 0⁰⁰–8⁵⁰
19	8	.	.	–	= 2⁴⁵–4²⁰
20	6	2.4	.	–	▽⁰⁻¹ 13⁴⁰–15²⁰ ●° 16¹² 19⁵⁰ 20²⁰. = na – a, p, np ∞ a
21	6	3.2	.	–	▽° 13⁵⁰ 15²⁰ ▽¹ 18⁵⁰ 19²⁰ ●° 21²⁰. = na, a, p ≡ 2⁵⁰–5⁵⁰. ⊕ 11⁵⁰–13¹⁶
22	8	.	.	–	●° 5³⁵ 6²⁵. = 0⁰⁰–5⁴⁵. 23⁵⁰–24
23	8	.	.	–	= 0⁰⁰–5²⁵ = na. ⌒ 2⁰⁰–7⁰⁰
24	7	.	.	–	= 2³⁰–4³⁰. np = np. ⌒¹ 22⁰⁰–24. ⊕ ¹0³⁰–15⁰⁰
25	7	.	.	–	= na, a, p – 24 = na. np ≡ 2⁵⁰–5³⁰. ⌒ 0⁰⁰–a, p–24
26	7	0.1	.	–	= na – a, p – np = 0⁰⁰–5²⁰. ⌒° 0⁰⁰–9⁰⁰
27	7	0.0	.	–	●° 4²⁵..³⁵ ▽⁰¹ 13²⁵–⁵⁰. = 0⁰⁰–6³⁰. 17⁵⁰–24
28	6	3.5	.	–	●° 8¹⁵–11¹⁵ ▽⁰⁻¹ 11⁴⁵–¹²⁰⁰ ●° 14¹⁵–19⁵⁰ 20¹⁰. 23³⁰–24. = 0⁰⁰–24
29	6	11.8	.	–	●° 0⁰⁰–1⁰⁰ 9⁴⁰ 11⁰⁵ ▽⁰⁻¹ 18³⁷ 20⁵⁰ ●°–24. (☇) 18⁰⁵–19⁰⁵ ☇ – 20⁴⁰. = 0⁰⁰–24
30	8	0.6	.	–	●° 0⁰⁰..3¹⁵. 3⁴⁰ 6²⁰–9¹⁰ 10¹⁵. = na, a, np
31	8	.	.	–	= na, a, np. ⌒¹ 22⁰⁰–24
Σ	–	68.6	–	–	UWAGI.

Czerwiec - Juin

1	7	.	.	–	= na – a. ∞ 10³⁰ 11³⁰ = np. ⌒ 0⁰⁰ 8³⁰. 21⁴⁵–24
2	8	0.6	.	–	= na – a. np. ☇ 22³⁵–24. ⌒° 0⁰⁰–9⁰⁰. 21⁰⁰–24
3	7	12.0	.	–	▽° 7¹⁵–8¹³ ▽⁰⁻¹ 15³³ 20⁴⁰. ☇° 7⁰⁰–8⁰⁰ SE-SW (☇) 14⁴⁵ 16³⁵ ☇ – 17³⁰ E-W (☇) 20¹⁵–22²⁵ E. = = 0⁰⁰–5³⁰ = p, np ⌒° 0⁰⁰–7¹⁵,
4	7	0.0	.	–	▽¹ 4²⁶ 5⁰⁰ ▽° 17³⁵–18²⁰. (☇) 15⁵⁰–17³⁵ NW-S ☇° – 18²⁰. = na – p = = np **3.V:** ☇ 0⁰⁰ 15⁰⁰ S
5	7	0.0	.	–	▽° 10⁴⁷–⁵¹ ☇ 16³⁵–17³⁰. = = 0⁰⁰–3¹⁵ ≡ – 8¹⁵ = – 9³⁰. ⌒° na, a, np
6	7	2.5	.	–	▽° 13⁵⁰ 14⁰⁷ ▽¹ 16⁵⁰–17⁰⁵. = na – a. np. ⌒° na – a, np. ⊕ ¹ 17⁴⁰–20⁰⁰
7	7	0.3	.	–	▽° 22³⁵–23¹⁰. (☇) 15⁵⁰–18⁴⁰ NW. = na – a, np. ⌒ ¹ 1⁰⁰–9⁰⁰
8	6	0.0	.	–	▽° 16⁴⁵–⁵⁴ (☇) 13⁰⁰–⁴⁰ S-E. 16⁰⁰–17¹⁵ W-E. = = 0⁰⁰–24. ⌒° 22³⁰–24
9	5	0.0	.	–	(☇) 15⁰⁰–²⁵ W-S. 15⁵⁵–16¹⁰ NE-E. = = 0⁰⁰–2⁴⁵ ≡° – 6⁴⁵ = – 15¹⁰. ⌒° na – a, np
10	7	56.4	.	–	▽⁰⁻¹ 14¹⁰ 22²⁰ ●° 23⁰⁰–24 ▲¹ 16²⁰–⁴⁰ ☇° 14²⁵–⁴⁷ S-N ☇⁰⁻² 16⁰³–17⁰⁰ (☇)¹ – 18²⁰ SE-NE (☇)⁰⁻¹ np SE-W. = na – a,
11	6	0.1	.	–	●° 0⁰⁰ 1⁴⁰ 7⁴⁰ 8¹⁵ ●⁰⁻¹ 11¹⁵–17¹⁰. = 0⁰⁰ 24 **10.VI:** p, np ≡ 16⁴⁰–17²⁰. ⌒ n – a
12	7	1.4	.	–	●° 9²² 10¹⁰ 15⁰³–⁴⁰ ▽° 17⁵⁶–18¹⁰. = = 0⁰⁰ 13³⁰ = np. ⊕ 11⁵⁵–12²⁹
13	8	4.4	.	–	●° 16⁴⁵ 17⁰⁵ 21³⁰ 22²⁵. = = 0⁰⁰–9³⁰
14	6	1.9	.	–	●° 3⁰²..⁰⁸ ●⁰⁻¹ 5²⁰–9⁴⁰. 17³⁰ 18²⁰. 19³⁰–20²⁰. = 6⁴⁵–24
15	8	0.0	.	–	= 0⁰⁰–5²⁰
16	8	.	.	–	= = 1³⁰–5¹⁵ = 22⁴⁰–24. ⌒° 0⁰⁰ 8⁰⁰ 21³⁰–24
17	8	.	.	–	= 0⁰⁰–7¹⁵ ∞ 21³⁰–23⁰⁰ = –24. ⌒¹ 0⁰⁰–9⁰⁰ ⌒° 21⁰⁰–24
18	7	0.0	.	–	= = 0⁰⁰–8³⁰ ∞ = 11¹⁰ = p – np. ⌒¹ 0⁰⁰–9⁰⁰ np
19	6	2.8	.	–	●° 7⁰⁰ 8¹⁰ 9¹⁵ 10⁰⁵ ●° 11¹⁰ 11²⁵–13³⁵. = 0⁰⁰–17¹⁰. ⌒¹ 0⁰⁰–7⁵⁰
20	8	.	.	–	= 3²⁰–40. 4³⁰–5¹⁵. ⌒° 4⁵⁰–9⁰⁰
21	8	.	.	–	= 4¹⁵–⁴⁵ = 22³⁰–24. ⌒° na – a ⌒¹ np
22	7	0.9	.	–	●° 22²⁰–24. (☇) 21⁵⁵–22²⁰. = = 0⁰⁰–2³⁰ ≡ – 5⁵⁰ = – 7³⁰. 20³⁰–21⁵⁵. ⌒¹ na; S 16⁵–20³⁰
23	7	.	.	–	●⁰⁻¹ 0⁰⁰–2³⁵. = na – p. p – 24. ⌒° 22⁰⁰–24
24	7	.	.	–	= = 0⁰⁰–9⁰⁰ S – 10³⁰ 20³⁰–24 = 21³⁰–24. ⌒° 0⁰⁰–9⁰⁰. 21⁰⁰–24
25	7	.	.	–	= = 0⁰⁰–9³⁰. S 0⁰⁰–2⁰⁰. ⌒° 0⁰⁰–9⁰⁰
26	7	.	.	–	= 0⁰⁰–10³⁵. np. ⌒° 0⁰⁰–a, np
27	7	5.9	.	–	●° 11⁰⁸–12¹⁰ ▽⁰⁻¹·² 22⁵⁸–23⁵⁵. = na – a. np; ⌒° na – a, np
28	8	.	.	–	●° 1²⁰ 1⁴⁰–4⁰⁶. = 0⁰⁰–4³⁰
29	8	.	.	–	= 0¹⁵–a. np. ⌒° na – a. np
30	8	.	.	–	= = 0⁰⁰–6³⁰. ⌒° 0⁰⁰–7⁰⁰
31					
Σ	–	89.2	–	–	UWAGI.

Wrocław - Gądów Mały $\varphi = 51°08'$ $\lambda = 16°59'$ **Lipiec - Juillet 1961**

Dni	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE · POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	111.4	110.4	108.9	110.2	17.8	27.3	19.5	21.0	29.1	7.6	73	39	71	61	5.6	22.2	6.5	11.4	0 ⊙	2 ⊙	2	C 0	C 0	NE 1
2	109.0	108.3	106.3	107.9	18.2	29.5	19.7	21.8	31.3	9.7	81	27	66	58	3.9	29.9	7.9	13.9	0 ⊙	0 ⊙	0	C 0	N 2	C 0
3	105.2	103.0	100.2	102.8	21.5	31.5	22.9	24.7	32.9	10.7	62	35	70	56	9.8	30.2	8.4	16.1	0 ⊙	2 ⊙	5	C 0	S 4	WSW 3
4	99.9	95.2	95.6	96.9	18.3	24.8	15.1	18.3	26.6	14.9	88	63	88	80	2.4	11.5	2.1	5.3	10	4 ⊙	9	SSW 1	W 1	W 7
5	100.7	100.9	102.0	101.2	12.3	17.1	11.8	13.2	19.2	11.7	67	42	76	62	4.7	11.4	3.3	6.5	5	4 ⊙	9	W 10	W 8	W 4
6	103.0	105.0	107.0	105.0	11.8	15.4	12.8	12.7	17.5	8.3	71	74	74	73	3.9	4.0	3.9	3.9	6 ⊙	10	8	WSW 8	W 9	W 5
7	108.3	107.8	107.6	107.9	12.8	15.9	10.4	12.4	18.0	10.0	76	52	80	69	3.6	8.7	2.6	5.0	4 ⊙	7	9	W 6	W 5	C 0
8	107.0	105.2	101.6	104.6	12.0	21.7	16.3	16.6	23.2	5.6	74	38	68	60	3.6	16.1	6.0	8.6	6	8	4	C 0	SSW 4	S 2
9	96.8	97.0	98.9	97.6	13.2	17.7	12.0	13.7	19.2	9.1	86	71	94	84	2.1	5.9	0.8	2.9	10 •	8	2	S 3	W 8	SW 3
10	98.6	98.7	100.6	99.3	13.8	17.3	11.2	13.4	19.2	7.6	75	47	78	67	3.9	10.4	2.9	5.7	3	4 ⊙	1	W 4	W 8	SW 1
11	100.6	100.8	98.2	99.9	12.2	19.7	19.7	17.8	23.5	6.5	85	60	67	71	2.2	9.2	7.5	6.3	10	9	9	S 1	W 3	ESE 3
12	95.8	94.7	91.0	93.8	18.3	26.5	23.4	22.9	28.7	12.8	82	46	65	64	3.6	18.8	10.1	10.8	2 ⊙	5 ⊙	3	SW 2	SSW 1	E 3
13	86.0	84.1	86.9	85.7	21.1	24.3	14.9	18.8	26.6	14.8	72	61	92	75	7.0	11.8	1.3	6.7	1 ⊙	9	10 •	SW 5	SSW 6	WSW 4
14	92.0	94.1	94.0	93.4	15.1	16.9	15.2	15.6	21.9	12.2	60	57	69	62	6.8	8.2	5.3	6.8	9	7	9	W 10	SW 6	S 2
15	95.4	96.8	96.4	96.2	15.5	23.1	18.7	19.0	25.5	13.9	94	42	71	69	1.1	16.2	6.4	7.9	9	3 ⊙	9	S 1	WNW 5	C 0
16	95.6	96.1	96.3	96.0	14.5	21.1	14.4	16.1	23.6	13.6	94	44	90	76	0.9	13.9	1.6	5.5	9	7 ⊙	8	W 3	W 4	NW 1
17	95.8	94.3	95.1	94.4	14.6	14.7	13.0	13.8	19.9	9.8	81	84	81	82	3.1	2.7	2.8	2.9	9	10 •	10	C 0	WNW 8	W 5
18	94.7	94.2	94.5	94.5	14.1	19.7	14.6	15.8	21.1	11.5	84	59	89	77	2.5	9.4	1.8	4.6	10	6 •	10 • R	W 6	W 5	W 3
19	94.9	95.0	95.1	95.0	14.2	14.6	12.6	13.5	19.2	11.9	90	78	92	87	1.6	3.6	1.2	2.1	10	9 R	6	SSW 3	W 8	S 2
20	96.4	97.1	98.5	97.3	12.6	14.5	13.8	13.7	20.4	7.3	89	86	95	89	1.6	2.4	1.1	1.7	8	9	9	W 2	S 5	SW 2
21	98.9	99.7	99.6	99.4	14.1	15.9	14.2	14.6	17.7	13.5	97	79	86	87	0.6	3.8	2.4	2.3	10 •	10	10	WSW 4	WSW 8	WSW 5
22	99.4	99.7	100.5	99.9	13.8	16.5	14.8	15.0	18.5	13.5	94	85	80	86	0.9	2.9	3.3	2.4	10	8	10	W 7	W 5	W 5
23	101.6	102.6	104.7	103.0	14.6	15.9	14.3	14.8	17.7	8.3	77	73	81	77	3.8	4.9	3.1	3.9	6	10	10	WSW 5	W 5	W 3
24	107.0	108.9	110.5	108.8	13.8	15.7	13.2	14.0	17.5	9.9	82	57	83	74	2.9	7.6	2.6	4.4	8	10	9	W 4	W 8	W 3
25	111.5	111.9	110.3	111.2	12.4	16.3	12.4	13.4	17.8	11.8	88	60	89	79	1.7	7.4	1.6	3.6	10	10	3	W 2	WNW 4	WSW 1
26	107.0	105.6	98.5	103.0	15.2	23.2	17.5	18.4	24.3	9.6	71	43	73	62	5.0	16.1	5.5	8.9	4 ⊙	6 ⊙	3	SSW 2	SW 6	S 2
27	96.1	94.3	95.2	95.2	18.7	23.7	16.1	18.6	25.4	14.2	70	52	94	72	6.5	14.0	1.2	7.2	8	10	10	SSW 2	SW 7	SW 1
28	90.5	91.2	91.3	91.0	15.3	17.2	14.4	15.3	19.6	13.1	96	83	97	92	0.8	3.4	0.6	1.6	10 •	10	9 •	SSE 1	WSW 4	C 0
29	97.1	99.8	101.6	99.5	13.0	16.7	11.5	13.2	18.7	11.5	92	64	85	80	1.3	6.8	2.0	3.4	10	9 ⊙	7	WNW 4	NW 4	W 2
30	103.4	103.7	104.1	103.7	11.2	15.9	12.8	13.2	16.7	9.6	86	67	92	82	1.8	6.0	1.2	3.0	9	10	10 •	W 1	NW 2	WNW 2
31	101.6	101.8	102.7	102.0	13.2	14.3	13.9	13.8	15.7	12.5	94	91	81	89	0.9	1.5	3.0	1.8	10	10 •	9	WNW 3	WNW 8	W 5
M	100.0	99.9	99.8	99.9	14.8	19.4	15.1	16.1	21.8	10.8	82	60	81	74	3.2	10.4	3.5	5.7	7.0	7.3	7.2	3.2	5.2	2.6

Sierpień - Août

1	103.3	103.6	102.6	103.2	14.2	19.3	14.2	15.9	22.2	11.0	74	53	88	72	4.3	10.6	2.0	5.6	2 ⊙	4	0	WSW 8	WNW 7	S 2
2	100.8	98.6	100.5	100.0	12.9	23.9	14.2	16.3	24.9	7.5	95	54	99	83	0.7	13.4	0.2	4.8	2 ⊙	9	9 •	C 0	ESE 2	S 1
3	102.3	104.4	107.1	104.6	13.8	18.1	11.9	13.9	19.6	10.2	98	68	90	85	0.4	6.8	1.3	2.8	9	9	1	WNW 1	WNW 8	C 0
4	106.7	104.8	103.3	104.9	12.1	18.1	15.9	15.5	20.4	5.1	86	63	75	75	2.0	7.7	4.5	4.7	6 ⊙	10 •	10	S 2	WSW 3	SSW 4
5	103.3	102.1	100.2	101.9	18.2	22.6	18.5	19.4	25.7	15.0	82	63	87	77	3.7	10.2	2.7	5.5	5 ⊙	9	1	WSW 3	W 3	SE 1
6	98.1	97.0	95.3	96.8	20.3	30.3	25.0	25.2	31.5	15.2	75	45	69	63	6.0	23.5	9.8	13.1	2 ⊙	2 ⊙	8	C 0	WSW 5	S 4
7	98.5	99.1	102.4	100.0	18.6	21.3	16.5	18.2	25.4	16.5	94	78	94	89	1.2	5.6	1.2	2.7	10	7 ⊙	8	W 3	W 3	WSW 1
8	104.5	102.2	101.1	102.6	14.0	20.2	21.2	19.2	23.8	8.7	97	71	81	83	0.6	6.9	4.8	4.1	5	10	3	ENE 1	SE 4	SSE 3
9	104.6	105.1	106.0	105.2	20.2	26.2	20.1	21.6	27.2	14.0	79	62	94	78	5.0	15.0	1.3	6.4	8	8	10 •	W 3	WNW 1	SE 1
10	104.6	102.1	100.0	102.2	19.4	27.0	20.4	21.8	29.4	17.6	95	65	99	86	1.1	12.4	0.3	4.6	2 ⊙	2 ⊙	10 • R	C 0	ESE 1	C 0
11	98.2	100.3	102.5	100.3	18.4	19.0	15.7	17.2	20.4	15.0	99	97	98	98	0.3	0.7	0.4	0.5	10	10 •	0	SSE 1	W 2	WNW 1
12	102.0	101.3	103.1	102.1	16.5	20.3	15.7	17.0	21.7	13.9	98	79	94	90	0.4	5.0	1.1	2.2	9	10	10	C 0	NW 1	W 3
13	104.1	107.4	107.9	106.5	13.8	17.1	11.1	13.3	18.7	10.8	88	50	92	77	2.0	9.7	1.		10	9	4	NW 2	NNW 3	C 0
14	106.8	105.2	102.4	104.8	10.5	18.5	13.8	14.2	20.5	5.4	94	56	88	79	0.8	9.5	2.		9	9	7	C 0	SW 3	S 2
15	99.5	98.0	96.7	98.1	14.8	17.1	14.8	15.4	19.5	11.4	85	67	75	76	2.5	6.5	4.1	4.4	9	9	10	SW 4	SW 9	SSW 4
16	97.6	96.7	96.4	96.9	12.0	15.6	12.8	13.5	16.9	11.2	85	61	78	74	2.3	6.9	3.3	4.2	7	9	10	SW 3	WSW 8	W 7
17	93.7	92.9	96.3	94.3	11.0	17.5	12.4	13.5	18.4	6.9	87	59	87	78	1.6	8.2	1.9	3.9	9	7	10	S 1	W 5	W 2
18	96.5	96.8	97.5	96.9	12.3	16.3	12.0	13.2	19.2	8.9	93	77	89	86	1.0	4.2	1.5	2.2	9	7	4	W 5	WNW 5	W 3
19	92.9	91.5	92.2	92.2	13.7	18.6	14.2	15.2	21.1	9.9	82	66	93	80	2.9	7.2	1.1	3.7	10 •	8	9 •	SW 6	SW 9	SW 3
20	94.1	95.9	99.8	96.6	13.6	15.3	12.2	13.3	19.2	11.2	86	85	86	86	2.2	2.6	2.0	2.3	10	9	7	WSW 4	W 6	WSW 2
21	100.2	100.1	98.5	99.6	14.7	19.8	17.9	17.6	22.2	11.9	84	57	71	71	2.7	10.1	5.9	6.2	9	9	10	SW 6	W 7	SSW 5
22	95.4	93.5	94.6	94.5	15.3	21.3	11.5	14.9	22.6	11.5	85	65	95	82	2.6	8.9	0.7	4.1	10 •	8 ⊙	6	S 6	SW 10	W 3
23	97.2	99.2	101.9	99.4	13.5	14.5	12.1	13.0	17.3	10.8	86	88	84	86	2.1	2.0	2.2	2.1	10	8	4	WSW 7	W 7	W 5
24	103.6	105.1	104.2	104.3	11.4	12.6	12.0	12.0	16.5	9.7	94	96	94	95	0.9	0.5	0.8	0.7	4 ⊙	10 •	9	W 5	W 4	SW 2
25	103.2	104.8	105.0	104.3	13.6	15.7	15.2	14.9	18.4	9.4	83	85	91	86	2.7	2.6	1.5	2.3	8 ⊙	10	9	WSW 4	W 7	SSW 2
26	106.8	106.9	106.7	106.8	14.3	21.3	18.3	18.0	24.0	11.8	98	71	86	85	0.4	7.3	2.8	3.5	7	8 ⊙	10	W 2	WSW 6	SSW 1
27	107.8	108.0	109.3	108.4	14.7	26.4	17.5	19.0	27.2	10.4	99	49	90	79	0.2	17.7	2.0	6.6	3	6 ⊙	8	C 0	W 2	W 1
28	112.0	113.3	113.3	112.9	15.7	21.8	13.7	16.2	22.6	12.6	100	61	92	84	0.0	10.1	1.3	3.8	3 ⊙	6 ⊙	0	WSW 1	NW 4	C 0
29	112.2	110.9	109.4	110.8	11.5	25.1	13.2	15.2	24.8	7.2	100	54	94	83	0.0	13.1	0.9	4.7	8 ⊙	3 ⊙	0	C 0	NW 1	C 0
30	110.2	111.0	111.6	110.9	11.9	22.5	14.7	16.0	24.0	6.8	99	60	88	82	0.1	10.8	2.0	4.3	7	9	0	C 0	ENE 1	NE 2
31	113.7	114.4	115.1	114.4	11.1	23.5	15.1	16.2	24.8	7.8	100	50	91	80	0.0	14.5	1.5	5.3	0 ⊙	0	0	ENE 1	ENE 4	E 2
M	102.4	102.3	102.7	102.5	14.5	20.2	15.3	16.3	22.3	10.8	90	66	88	81	1.7	8.7	2.2	4.2	6.8	7.5	6.0	2.5	4.5	2.2

Wrocław - Grądów Mały $H_s = 116\,m$ $H_b = 118.6\,m$ $h_a = 20\,m$ **Lipiec - Juillet 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	7	.	.	-	= ≡ 0^30 10^40 23^30 24 : ⌒ 0^00 8^50 . 21^00 24
2	8	.	.	-	= 0^00 2^30 ≡ 6^30 = 9^15 ∞ 10^30 . ⌒ ° 0^00 a, np
3	7	.	.	-	= 0^20 2^45 = 6^20 na a np : ⌒ ° 0^00 9^00
4	6	0.0	.	-	• ° 19^10-20 20^55 21^20 . = 4^00 5^20 = 8^15 = na-p, np, S' p
5	8	0.0	.	-	• ▽ ° 19^49 20^03 : ≫ 7^30 8^10 : ⌒ 19^45 20^10
6	8	1.4	.	-	• ▽ ° 10^05-30 • ° 10^32 12^30
7	8	.	.	-	⌒ ° 22^00 24
8	8	0.2	.	-	= = 3^30 7^30 = 19^40 24 : ⌒ ° 0^00 9^00 21^00 24
9	7	4.0	.	-	• ° 6^32 7^10 12^02 • ▽ ° 16^01-08 = 0^00 12^05 : ⌒ ° 0^00 6^32
10	7	1.8	.	-	• ° 9^40 10^32 • ▽ ° 11^40-45 : ⌒ ° 0^20 8^00 23^00 24
11	6	2.0	.	-	• ° 8^05-30 9^19 10^30 • ▽ ° 13^45-47 , (⧹) 23^50 24 SW-SE : = na, a-p, np ; ⌒ ° n-a
12	7	.	.	-	• ▽ 8.0 0^30-45 : (⧹) 0^00 1^15 . = 0^00-30 4^30 9^20
13	7	3.6	.	-	• ▽ ° 14^45-50 16^03-15 • 0.1 18^05 19^10 • ° 19^30 23^30
14	8	1.4	.	-	• ▽ ° 12^50-56 , ≫ 7^20 9^10
15	8	24.3	.	-	• 3^43 7^20 • ▽ ° 11^11-16 • ° 23^40 24
16	8	0.0	.	-	• ° 0^00 1^05 2^20 • 1.0 2^22 7^05 • ° 20^35 21^10 : ⌒ 20^43 21^00
17	7	1.9	.	-	• ° 9^25 10^20 11^30 . 45 • ▽ ° 13^45 16^15 . ⧹ 15^50 16^00 (⧹) 1 16^20 S-E : = na : ⌒ ° n-a
18	7	2.0	.	-	• ▽ ° 14^01-04 • ▽ ' 21^15 23^05 . ⧹ ° 21^05 22^15 . = 0^30 11^30 np
19	6	8.0	.	-	• ° 1^30 2^30 8^45 9^10 • ▽ 0.2 ° 13^00 16^15 . ⧹ 1 13^15 14^35 NW-SE = 0^00-30 . na-a, np
20	6	3.6	.	-	• ▽ ° • ° 13^10 16^20 19^13 20^25 . (⧹) 0.1 ° 12^38 13^25 SSW-E . 14^53 15^00 NW-N, 18^45 19^30 W-N : = 0^00-p, np
21	6	0.0	.	-	• ° 5^10 7^20 7^57 • ▽ ° 14^50 15^20 15^46-55 : = 0^00 4^50 8^45 24
22	6	0.0	.	-	• ▽ ° 2^40 3^15 • ° 7^10 13^10 • ▽ ° 15^10-15 : = 0^00 15^30 , 23^30 24 . ⌒ ° np
23	7	.	.	-	= 0^00 8^50 : ⌒ ° 0^00 11^00
24	8	.	.	-	= 4^20 5^40
25	8	.	.	-	= 23^40 24 : ⌒ ° 22^00 24
26	6	.	.	-	= 0^00 8^00 S 8^00 14^00 19^30 24 : ⌒ ° 0^00 9^00
27	7	6.5	.	-	• ° 17^45 22^45 . = 0^00 8^00 S 10^00 = 18^00 24
28	8	21.8	.	-	• ° • ▽ ° 5^30 12^40 . 15^25 24 : = . = 0^00 4^50 = 6^30 10^50
29	8	.	.	-	• ° 0^00 6^05 . = 6^00 10^20
30	7	2.8	.	-	• ▽ ° 14^50 15^20 . 17^25 18^15 • ° 18^40 24 : = na-a, np ; ⌒ ° na-a ; ⊕ 8^45 10^15
31	7	5.2	.	-	• ° 0^00 2^50 . 5^15-7^25 . 10^50 15^40 • ' 16^20 • ° 19^15 20^40 : = na
Σ	—	90.5	—	-	UWAGI:

Sierpień - Août

1	7	.	.	-	= 0^00 4^30 20^30 24 : ≫ 8^40 9^30 10^00 11^30 : ⌒ ° np
2	7	4.1	.	-	• ▽ ° 16^58 18^20 • ° 19^25 22^40 : = 0^00 4^40 ≡ ° 5^10 = - p, np ≡ ° np ; ⌒ ° 0^00 9^00
3	6	0.0	.	-	• ° 5^15-40 ▽ ° 8^05-20 . = 0.1 0^00 7^30 = - 14^20 . ⌒ ° 21^00 24
4	7	0.0	.	-	• ° 13^25 15^10 . = na ≡ ' 3^50 5^00 = - 5^50 : ⌒ ° 0^00 10^00 : ⊕ 8^45 10^35 10^59 12^15
5	8	.	.	-	= 2^40 7^30 . 20^30 22^25 : ⌒ ° na, a, np
6	8	0.0	.	-	• ▽ ° 22^20-30 . = 0^20 5^20 : ⧹ 21^50 23^10 . ⌒ ° 0^00 9^00
7	7	0.4	.	-	• ▽ ° 5^40 6^00 • ° 8^35 9^55 • ▽ ° 12^20-30 • ° 18^01 20^40 : ⧹ ° 5^15 6^20 NW-NE : = 4^40 10^40
8	7	.	.	-	= . = 0^15 5^26 ≡ ° 7^20 = - 12^20 20^20 24 : ⌒ ° 3^00 9^00 23^00 24
9	7	8.6	.	-	• p ▽ 1.0 ° 17^10 18^45 19^20-35 • ° 21^15 23^10 : ⧹ 16^55 18^15 SE-NW : = = . ≡ 0^00 8^50 . p-24 : ⌒ ' 0^00 9^30
10	7	30.2	.	-	• 4^25-40 • ▽ ° 20^00-04 • ▽ 0.2 20^27 22^10 . (⧹) ° 19^15 20^20 ⧹ - 22^20 (⧹) - 24 SE, NW-SW
11	7	21.0	.	-	• ▽ ° 4^00-05 • ° 6^00 10^45 • ▽ ° 13^15 14^00 14^40-50 . (⧹) 0^00-27 SW ⧹ 8^55 12^15 W-SE : = na, a, p, np ≡ 23^45 24
12	6	2.9	.	-	• ° 14^20 15^40 17^30 18^40 . ≡ 0^00 1^40 = - 24
13	8	.	.	-	= 0^00 6^45 23^40 24 : ⊕ 12^35 13^25 . ⌒ ' 21^00 24
14	8	0.0	.	-	• ▽ ° 18^25-30 : = . = 0^00 9^15 = np ; ⌒ ' 0^00 9^00 ⌒ ° np
15	7	2.0	.	-	• ▽ ° 12^40 16^00 : = 0^00 13^30 . ⌒ ° 0^00 9^00
16	8	0.0	.	-	• 0.1 0^00 2^30 • ° 14^26-30 • ▽ ° 16^18 18^10 20^15-18 . = 2^30 4^17
17	7	2.8	.	-	• ▽ ° 10^52 20^25 . (⧹) 21^05-30 . = 10^0 5^30 10^50 24 : ⌒ ° 0^00 10^00 : ⊕ 14^40 15^10
18	7	0.8	.	-	• ▽ ° 10^37-45 • ▽ ' 15^30-35 • ▽ ° 17^25 18^40 . = 0^00 14^00
19	8	1.9	.	-	• ° 2^45 11^05 • ▽ ° 17^10 21^14 . = na, a, np
20	8	0.6	.	-	• ▽ 4.0 12^50 13^25 . = 0^00 5^30 : ⌒ ° 3^20 10^00 , np
21	7	0.0	.	-	• ° 2^00 3^10 10^01-10 . = 0^00 11^40 . np : ⌒ ° na
22	7	2.7	.	-	• ▽ 0.1 7^35 10^02 . 15^25-32 . 18^40 10^05 . = na, a, np ; ≫ 13^45 14^15 . 15^45 16^25
23	7	0.8	.	-	• ° 4^23-46 • ▽ ° 8^55 16^57 • ▽ ° 23^15-20 . = 0^00-25 ; ≫ p ; ⊘ 17^30 18^30
24	6	0.1	.	-	• ° 11^52 13^10 • ° 14^30 . = na-a, p-24 . = 20^30 21^30 : ⌒ 0.1 na, a, np
25	6	0.0	.	-	• ° 10^40 . 45 10^56 11^30 . = 0^00 p, np : ⌒ 1.2 0^00 10^00 ⌒ ° np , ⊐ 1^30 4^30
26	7	.	.	-	= 0^00 13^30 18^30 24 . ⌒ 0.1 0^00 10^00 , np
27	7	.	.	-	= . = 0^00 4^35 ≡ - 6^40 = . = - 10^30 , np ; ⌒ ° na - a , np
28	7	.	.	-	= . = 0^00 12^20 = np ; ⌒ ° 0^00 10^00 , np
29	7	.	.	-	= . = 0^00 11^20 = np ; ⌒ 1.2 0^00 10^00 ⌒ ° np
30	7	.	.	-	= . = 0^00 6^03 ≡ 0.1 ' 7^05 = - p, np ; ⌒ ° 0^00 8^00 . np
31	7	.	.	-	= . = 0^00 11^30 = np ; ⌒ 0.1 0^00 10^00 ⌒ ° np
Σ	—	78.9	—	-	UWAGI:

Wrocław – Gądów Mały φ = 51°08' λ = 16°59' Wrzesień – Septembre 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	115.1	113.5	110.6	113.1	14.9	26.3	18.3	19.4	27.6	10.9	84	44	78	69	2.7	19.1	4.6	8.8	0 ⊙	1 ⊙	0	ESE 1	SE 4	S 1
2	108.0	106.4	105.1	105.8	12.9	29.8	19.3	20.3	30.2	8.0	99	38	60	66	0.2	25.9	9.0	11.7	0 ⊙	0	0	C 0	S 6	S 3
3	100.1	98.8	96.9	98.6	14.3	29.1	18.4	20.0	29.6	12.2	90	35	74	66	1.6	26.4	5.5	11.2	1 ⊙	• 2 ⊙	0	E 1	SSW 2	SSW 2
4	98.4	99.3	101.0	99.6	16.9	26.1	16.3	18.9	27.1	12.6	94	56	94	81	1.2	14.8	1.1	5.7	4	4 ⊙	6 ⊠	W 2	W 3	W 6
5	99.1	97.0	92.7	96.3	16.5	26.7	22.5	22.0	28.4	12.8	100	47	66	71	0.0	18.5	9.1	9.2	0 ⊙	9	10 •	C 0	SSE 3	SSE 3
6	93.7	94.5	93.2	93.8	17.3	20.1	15.5	17.1	22.5	15.1	90	67	96	84	2.0	7.8	0.8	3.5	9	10	2	W 2	W 3	SSE 4
7	92.0	91.9	94.4	92.8	15.7	17.5	10.7	13.6	19.8	10.5	88	70	84	81	2.1	6.1	2.1	3.4	10 •	9	2	SSW 4	SW 7	SSW 4
8	96.0	96.9	99.5	97.5	11.9	13.0	12.7	12.6	15.2	9.5	78	71	96	82	3.0	4.3	0.5	2.6	9	10	10 •	SW 6	SW 6	W 6
9	101.5	103.0	104.0	102.8	13.3	15.3	12.8	13.6	16.3	11.6	95	81	92	89	0.7	3.4	1.2	1.8	9	10	10	W 5	WNW 7	W 3
10	105.0	105.9	106.1	105.7	11.7	13.4	12.5	12.5	13.9	11.6	90	80	87	86	1.3	3.2	1.9	2.1	10	10	10	WNW 5	WNW 3	W 2
11	104.7	103.7	102.1	103.5	11.6	17.5	10.2	12.4	18.2	10.2	93	50	85	76	1.0	10.0	1.9	4.3	9	9	3	SSW 2	SSW 4	SSW 1
12	99.6	99.8	101.0	100.1	11.3	19.4	13.1	14.2	21.5	8.0	86	58	93	79	1.8	9.5	1.1	4.1	7	10 •	8	SSE 1	W 9	SW 4
13	101.7	102.1	100.9	101.6	12.6	19.7	15.0	15.6	20.6	11.5	93	59	82	78	1.1	9.4	3.1	4.5	10	6	2	SW 3	W 5	SE 1
14	97.3	98.1	97.2	97.5	12.8	20.8	16.2	16.5	23.6	12.0	96	72	97	88	0.5	6.8	0.6	2.6	10	9	10	SE 1	SW 4	W 2
15	104.8	107.1	108.3	106.7	13.1	17.4	11.6	13.4	19.5	11.6	84	54	89	76	2.5	9.1	1.5	4.4	8	7	0	W 6	W 5	SSW 1
16	108.4	107.3	106.1	107.3	10.5	25.1	16.7	17.2	26.9	7.9	100	49	91	80	0.0	16.2	1.8	6.0	8 ⊙	3	0	C 0	SSE 4	SE 2
17	106.5	105.7	105.5	105.9	12.5	29.3	18.6	19.8	30.2	10.4	98	35	76	70	0.4	26.3	5.1	10.6	0	1	0	SE 1	S 6	S 2
18	106.4	106.8	107.0	106.7	12.5	28.6	19.7	20.1	29.5	9.0	100	51	92	81	0.0	19.1	1.7	6.9	6	1 ⊙	0	C 0	W 4	NNE 2
19	109.0	108.9	108.2	108.7	15.0	21.6	11.1	14.7	22.8	11.0	80	47	81	69	3.4	13.6	2.4	6.5	9	2 ⊙	0	NNE 1	NE 1	NE 2
20	109.2	108.5	108.3	108.7	9.2	19.5	12.4	13.4	20.4	5.6	97	46	74	72	0.3	12.4	3.7	5.5	0 ⊙	0 ⊙	0	ENE 1	E 4	NE 2
21	109.3	109.5	110.9	109.9	9.4	19.1	13.3	13.8	19.9	7.0	85	47	69	67	1.7	11.8	4.8	6.1	0	0 ⊙	0	NE 2	ESE 4	E 3
22	112.8	113.2	113.2	113.1	5.4	18.1	9.8	10.8	19.7	2.5	97	41	79	72	0.3	12.3	2.5	5.0	0 ⊙	0 ⊙	0	ENE 1	E 2	ENE 1
23	112.5	111.1	109.9	111.2	6.6	19.0	8.8	10.8	20.6	2.9	82	35	76	64	1.7	14.4	2.7	6.3	2 ⊙	0 ⊙	0	ENE 1	NE 3	ENE 2
24	108.8	107.6	106.7	107.7	4.7	21.2	9.4	11.2	22.9	3.0	95	42	92	76	0.4	14.6	1.0	5.3	0	0	0	ENE 2	C 0	C 0
25	106.4	106.6	109.6	107.5	3.4	25.0	14.2	13.7	23.4	2.3	98	48	94	80	0.1	14.5	0.9	5.2	0	4 ⊙	9	C 0	W 4	WSW 1
26	109.5	108.2	106.7	108.1	13.7	19.0	14.3	15.3	20.4	10.6	98	67	99	88	0.4	7.2	0.2	2.6	10	9	10	C 0	C 0	ENE 2
27	105.6	104.8	103.9	104.8	12.3	16.9	10.0	12.3	17.3	9.8	100	72	97	90	0.0	5.3	0.3	1.9	10	7	2	C 0	SSE 1	E 2
28	104.3	104.2	105.3	104.6	9.2	19.7	15.5	15.0	21.3	8.6	100	67	83	83	0.0	7.5	3.0	3.5	10 =	7	0	E 1	E 3	E 2
29	105.5	103.8	103.6	104.3	10.7	22.0	17.7	17.0	23.6	10.3	92	64	77	78	1.0	9.6	4.5	5.0	6 ⊙	3	9	E 1	ESE 3	E 1
30	103.8	101.9	102.4	102.7	13.1	19.7	14.3	15.4	20.3	12.8	84	71	71	75	2.5	6.7	4.8	4.7	10	10	10	E 2	E 2	E 2
31																								
M	104.5	104.2	103.9	104.2	11.8	21.1	14.4	15.4	22.4	9.4	92	55	84	77	1.1	12.2	2.8	5.4	5.6	5.1	3.8	1.7	3.7	2.3

Październik – Octobre

1	104.4	104.9	108.3	105.9	10.7	16.5	10.5	12.0	17.1	10.5	80	51	79	70	2.6	9.2	2.7	4.8	8 ⊙	1 ⊙	0	E 4	E 7	E 6
2	109.9	110.8	111.3	110.7	10.5	15.3	12.4	12.6	15.7	7.2	88	67	85	80	1.5	5.8	2.2	3.2	7	9	2	ESE 2	E 6	ENE 3
3	111.8	110.2	109.9	110.6	8.2	19.3	13.3	13.5	19.6	7.3	97	44	82	74	0.3	12.6	2.8	5.2	0 ⊙	1 ⊙	0	ENE 3	E 6	E 3
4	109.7	108.6	107.8	108.7	7.6	19.7	13.6	13.6	19.8	4.2	96	44	68	69	0.4	12.9	5.0	6.1	6	7	3	E 1	ESE 6	E 4
5	107.8	107.3	108.1	107.7	9.9	22.0	14.1	15.0	22.5	9.4	86	46	76	69	1.8	14.3	3.9	6.7	4	0 ⊙	0	ENE 2	SE 5	SE 3
6	107.3	104.6	102.0	104.6	8.4	22.0	14.6	14.9	23.4	7.4	96	45	68	70	0.4	14.5	5.3	6.7	0 ⊙	0 ⊙	0	E 2	SE 8	ESE 4
7	97.0	93.7	93.5	94.7	10.4	17.7	14.8	14.4	19.4	10.2	77	53	77	69	2.9	9.5	3.8	5.4	2	8	9	E 6	ESE 11	E 3
8	95.2	94.3	99.2	95.6	14.1	16.4	13.5	14.4	20.1	13.1	69	76	86	77	4.9	4.4	2.1	3.8	9	10	10	E 3	C 0	SW 3
9	107.8	111.0	114.4	111.1	11.0	17.1	6.6	10.3	18.8	6.6	99	67	100	89	0.1	6.5	0.0	2.2	10	6 ⊙	0	SSW 2	SW 5	SW 1
10	115.9	115.5	114.4	115.3	3.0	19.9	10.0	10.7	20.5	2.0	98	52	97	82	0.2	11.2	0.3	3.9	8	5	0	C 0	SSE 3	E 1
11	112.3	110.7	110.1	111.0	6.8	18.5	8.2	10.4	20.6	5.7	99	61	100	87	0.2	8.3	0.0	2.8	0 ⊙	0 ⊙	0	E 1	ESE 2	S 2
12	111.5	113.1	114.7	113.1	7.4	15.9	10.0	10.8	17.4	2.5	99	83	88	90	0.2	3.1	1.5	1.6	4	9	0	WSW 2	NNW 6	NNW 1
13	114.7	114.9	115.4	115.0	4.7	13.8	3.8	6.5	14.7	1.5	100	65	98	88	0.0	5.6	0.1	1.9	7	8	0	C 0	N 2	NW 1
14	114.6	115.5	113.0	115.7	7.4	12.1	10.0	9.9	13.6	1.4	97	71	91	86	0.3	4.1	1.1	1.8	9	10	10	WNW 1	WNW 6	NW 2
15	112.0	111.1	108.7	110.6	9.8	12.9	10.1	10.7	13.5	9.6	97	80	90	89	0.3	2.9	1.3	1.5	10	10	4	W 1	W 5	W 1
16	106.3	103.9	102.5	104.2	3.2	16.5	9.4	9.6	17.7	2.6	100	53	87	80	0.0	8.9	1.6	3.5	10 =	6	1	C 0	SW 1	WSW 2
17	98.1	95.5	84.1	91.8	10.3	15.3	13.7	13.2	16.0	6.5	86	52	69	69	1.7	8.4	4.9	5.0	10	9	10 •	S 3	SW 8	SSE 10
18	75.1	75.8	77.9	76.3	11.4	11.0	8.4	9.8	14.9	8.2	78	96	96	90	3.0	0.5	0.4	1.3	10	10 •	10 •	S 5	SE 1	W 3
19	82.0	85.8	87.2	84.3	6.7	9.7	10.3	9.2	10.6	6.5	99	95	100	98	0.1	0.6	0.0	0.2	10	10 •	10 •	C 0	ESE 2	SW 1
20	93.3	94.9	96.1	94.8	8.8	11.5	9.3	9.7	11.8	8.0	100	95	100	98	0.0	0.7	0.0	0.2	10	10 •	10 •	C 0	C 0	WNW 2
21	94.8	97.0	101.1	97.6	8.8	10.0	8.8	9.1	12.3	8.4	100	95	84	93	0.0	0.7	1.8	0.8	10	10	8	WSW 1	SE 4	SE 5
22	106.3	108.1	108.4	107.6	3.3	12.8	8.3	8.2	14.9	1.6	100	68	94	87	0.0	4.7	0.7	1.8	4	10	0	C 0	ESE 1	E 2
23	108.2	107.9	107.7	107.9	7.2	13.9	10.3	10.4	15.8	6.8	100	76	82	86	0.0	3.9	2.2	2.0	10	4	2	ESE 5	SE 5	S 4
24	108.7	108.6	106.0	107.8	10.1	14.9	10.0	11.2	15.2	9.4	91	70	85	81	1.2	5.0	2.1	2.8	10	10	0	S 3	S 6	SSE 6
25	102.0	102.9	102.1	102.3	9.0	14.5	12.4	12.1	16.5	8.1	79	62	82	74	2.5	6.3	2.6	3.8	8	10	10	S 8	S 6	S 6
26	100.5	100.5	99.5	100.2	11.5	14.2	11.5	12.2	14.8	11.3	84	72	81	79	2.2	4.6	2.7	3.2	10	9	2	S 6	SW 5	S 4
27	96.0	95.2	96.2	95.8	8.8	18.6	8.4	11.0	19.4	8.4	90	64	95	82	1.1	7.8	0.7	3.2	8	7 ⊙	3	SE 5	S 2	S 1
28	98.2	97.4	97.2	97.6	9.4	14.7	12.2	12.1	15.1	4.4	97	76	87	87	0.3	4.0	1.9	2.1	10	8	10	C 0	SSE 2	SSE 2
29	96.9	98.4	100.5	98.6	10.0	9.3	5.6	7.6	12.5	5.2	100	99	100	100	0.0	0.1	0.0	0.0	10 •	10 •	0 =	WNW 2	NW 4	SW 1
30	101.5	101.6	103.2	102.1	3.4	13.1	5.2	6.7	13.4	1.5	100	75	100	92	0.0	3.8	0.0	1.3	0 =	7	0 =	E 1	E 1	ESE 2
31	104.8	104.4	106.1	105.1	3.2	12.9	6.7	7.4	14.6	2.8	100	69	91	87	0.0	4.6	0.9	1.8	2 =	8	9	SE 2	SSW 7	SW 3
M	103.3	103.2	103.4	103.3	8.2	15.2	10.2	11.0	16.5	6.4	93	68	88	83	0.9	6.1	1.8	2.9	7.0	7.2	4.0	2.3	4.3	3.0

Wrocław-Gądów Mały $H_s = 116\,m$ $H_b = 118{,}6\,m$ $h_m = 20\,m$ Wrzesień-Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU s	USŁONIECZYNIENIE	POGODA
1	8	.	.	–	= 0⁰⁰–9³⁰ ∞–12³⁰. ⌒ ¹0⁰⁰–10⁰⁰ ⌒ ⁰22⁰⁰–24
2	8	.	.	–	= = 2³⁰–8³⁰. ⌒ ⁰0⁰⁰–10⁰⁰
3	9	1.1	.	–	(K)⁰17³⁰ NW. ⌒ ⁰20⁰⁰–10⁰⁰. 22⁰⁰–24
4	6	0.3	.	–	▽•⁰5³⁵–42 22⁷⁸–57 •⁰24. K⁰4³⁰–5³⁰ K–5⁵⁰ (K)⁰21⁵³–22¹⁰ W. = na–a. p–np ∞–p. ⌒⁰na. np
5	7	2.3	.	–	•⁰0⁰⁰–1³⁰ ▽⁰21⁴⁰–22⁰⁵. = 0⁰⁰–4⁵⁴ =⁰⁻²–7³⁵ =. ∞–13³⁰ = p. n. ↘ np
6	7	0.5	.	–	▽¹·⁰1²⁵–2¹⁰ •⁰5⁴⁵ 6⁴⁵ ▽⁰10⁴⁰–11⁰¹ •⁰15⁰⁵–20. = na–a. p–np. ⌒ np
7	8	1.6	.	–	•⁰⁻¹6⁰⁰ 10³⁷ ▽⁰16⁵⁷ 17¹⁵. = 0⁰⁰–8²⁰. ⌒ ⁰0⁰⁰–6⁰⁰. np
8	8	0.6	.	–	•⁰1²²–35 13⁵² 14⁰⁵ ▽⁰19⁵⁰–20⁰⁵. ⌒ ⁰0⁰⁰–9⁰⁰
9	8	0.2	.	–	▽•⁰·¹1³⁵ 6²⁸ ▽•⁰10⁰⁵ 18⁰⁴. = 6²⁰–8²⁰
10	8	0.1	.	–	▽•⁰11⁵⁰–12⁰⁵ ▽•⁰·¹14⁰⁵–20. = 0³⁰–3⁴⁵. 22⁰⁰–24
11	7	.	.	–	= 0⁰⁰–12³⁰ 18²⁰–24. ⌒ ⁰3⁰⁰–10⁰⁰. 22⁰⁰–24
12	6	2.3	.	–	▽•⁰·¹13⁴⁵–14⁴⁰ •⁰15¹⁵–16³⁰. = 0⁰⁰–p. np. ⌒ ⁰na–a
13	7	0.0	.	–	•⁰4⁴⁰ 5³⁵ 18²⁵..³⁵. = 0⁰⁰–10⁴⁰ 18⁴⁵ ¹24
14	7	0.9	.	–	•⁰8²⁵ 11⁴⁵ ▽•⁰·¹19³⁰–57 •⁰–21²⁷. = 0⁰⁰–12⁰⁰. ⌒ ⁰3⁰⁰–8²⁵
15	8	.	.	–	= 21⁰⁰–24. ⌒ ⁰20⁰⁰–24
16	8	.	.	–	= . = 0⁰⁰–10³⁰. ⌒ ⁰·²0⁰⁰–11⁰⁰ ⌒ ⁰21⁰⁰–24. ψ 20⁰⁰–21⁰⁰
17	8	.	.	–	= . = 2³⁰–9¹⁰. ⌒ ¹0⁰⁰–10²⁰ ⌒ ⁰np
18	8	.	.	–	= . = 0⁰⁰–9³⁰. np. ⌒ ¹·⁰0⁰⁰–10⁰⁰ ⌒ ⁰np
19	8	.	.	–	= ⁰0⁴⁰–1²⁰ = –6¹⁰. ⌒ ⁰0⁰⁰–9⁰⁰ 20⁰⁰ ¹24
20	8	.	.	–	= = 0⁰⁰–9³⁰. ⌒ ⁰0⁰⁰–11⁰⁰ 20⁰⁰–24
21	8	.	.	–	= 0⁰⁰–8³⁰. ⌒ ⁰0⁰⁰–8⁰⁰. 22⁰⁰–24
22	8	.	.	–	= . = 5²⁰–9¹⁵. ⌒ ⁰0⁰⁰–10⁰⁰ 21⁰⁰–24
23	7	.	.	–	= 2⁰⁰–11³⁰ S⁰–20³⁰ = –24. ⌒ ⁰na–a. np
24	6	.	.	–	= 0⁰⁰–10³⁰ ∞–14³⁰ = p–np = np. ⌒ ⁰na–a. np
25	6	.	.	–	= = 2⁰⁰–11⁰⁰ S–18⁰⁰ = 17⁰⁰–24
26	7	4.2	.	–	▽⁰19²⁵–57 •⁰–21²⁰. = 0⁰⁰–40 ≡⁰–3⁵⁰ = –12³⁰. p–np. ⌒ ⁰na–a
27	6	.	.	–	= 0⁰⁰–24 = p. ⌒ ¹np
28	6	.	.	–	= na. = ⁰⁻²4⁹⁹–5⁴⁰ ≡¹²·⁰5⁴⁰–10³⁰ ∞ = 14²⁰–24. ⌒ ¹0⁰⁰–12⁰⁰
29	5	0.0	.	–	= 0⁰⁰–2⁵⁰ = –6⁴⁰ = –24. ⌒ ⁰2⁰⁰–10⁵⁵
30	5	.	.	–	•⁰6⁴⁵..⁵⁰. = 0⁰⁰–14⁰⁰ S–20⁰⁰ = –22⁰⁰ S–24
31					
Σ	–	14.1	–	–	UWAGI

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1	8	.	.	–	= 0⁰⁰–na
2	7	.	.	–	= na. a. ⌒ ⁰na–8⁰⁰
3	7	.	.	–	= 4³⁰–10³⁰. ⌒ ⁰0⁰⁰–11⁰⁰. 23⁰⁰–24
4	7	.	.	–	= 1³⁰–12²⁵. 21³⁰–24. ⌒ ⁰0⁰⁰–10⁰⁰. ⊕ 13⁰⁵–15⁴⁰
5	7	.	.	–	= 0⁴⁰–10²⁰. 17³⁵–24. ⌒ ⁰6⁰⁰–10⁰⁰
6	7	.	.	–	= 0⁰⁰–11³⁰ ∞ 13³⁰–19³⁰ = –24. ⌒ ⁰3⁰⁰–8⁰⁰
7	6	.	.	–	= na. a. ∞–p. = –24
8	6	0.0	.	–	•⁰6²⁰..²⁴ 9⁵⁰ 12¹⁰. 19³⁰..³⁵. 21⁴⁰ 24 = 0⁰⁰–20²⁰
9	8	.	.	–	•⁰0⁰⁰–1⁴⁰. 4²⁵ 6³⁰. = 1³⁰–6³⁰. p–np = np. ⌒ ⁰np
10	7	.	.	–	= . = na. a. = ⁰4⁵⁵ 6⁴⁰ = = 17²⁰–24 ⌒ ⁰0⁰⁰–a. p–24
11	6	.	.	–	= 0⁰⁰–14⁰⁰ ∞–17²⁰ = –24. ⌒ ⁰0⁰⁰–11⁰⁰. 20⁰⁰–24
12	6	.	.	–	= = 0⁰⁰–2⁵⁰ = –6⁰⁵ = = –14³⁰ = np. ⌒ ⁰0⁰⁰–9⁰⁰. np
13	8	.	.	–	= 0⁰⁰–10³⁰. 20⁴⁰–24. ⌒ ⁰0⁰⁰–8⁰⁰
14	8	.	.	–	= 0⁰⁰–1³⁰. 4¹⁰–6⁵⁰
15	6	.	.	–	= 4³⁰–24. ⌒ ⁰np
16	6	.	.	–	= 0⁰⁰–1⁴⁵ ≡⁰⁻²–10⁰⁷ = –12³⁰ S–16²⁰ = –24. ⌒ ⁰0⁰⁰–11⁰⁰. 19⁰⁰–24
17	6	0.0	.	–	•⁰20³² 21⁴⁰ 22³⁶ 23⁰⁵ = 0⁰⁰–20³⁰. ⩽ p–np
18	6	11.1	.	–	•⁰·¹7³⁰ 10²⁰–15³⁰. 18⁴⁰–20³⁰ 21³⁰–24 = 10³⁰–23³⁰
19	5	3.6	.	–	•⁰0⁰⁰–3³⁷ 4¹⁵–5²⁰ ⁰6³⁰ •⁰9⁴⁰ 18¹⁰–21⁴⁰. = 0³⁰–24
20	5	13.6	.	–	•⁰3¹⁰..⁶⁰⁰ 10⁴⁰–20¹⁰. 20⁵⁰–21⁴⁰ •⁰·¹22⁰⁵–24. = 0⁰⁰–24 = n–a
21	6	4.7	.	–	•⁰▽ 0⁰⁰ 11²⁰. = 0⁰⁵–10³⁰
22	7	.	.	–	= a. p–24. ⌒ ⁰np. ▽ ¹21³⁰–24
23	5	0.2	.	–	= = 0⁰⁰–14⁴⁵. ⌒ ⁰·¹0⁰⁰–10⁰⁰. ▽ ¹0⁰⁰–1³⁰
24	7	.	.	–	•⁰4¹⁵–5¹⁵. ▽ 0⁰⁰–3³⁰
25	8	1.7	.	–	•⁰14⁰³–17³⁵. = p. np
26	7	0.1	.	–	•⁰3⁵⁰–11²⁵
27	7	.	.	–	= 4⁰⁰–7³⁰. 19³⁰–24. ⌒ ⁰·¹np
28	5	0.6	.	–	= 0⁰⁰–1¹⁵. ≡⁰·⁰10 = –24
29	5	4.0	.	–	•⁰6¹⁵ 7²⁰–13²⁵. 14⁰²–15. = 0⁰⁰–18²⁹ ≡⁰–19³⁰ ≡²–24. ⌒ ⁰na
30	6	.	.	–	≡²0⁰⁰–8²⁶ = –18⁴⁰ ≡⁰·¹–22²⁰ ≡⁵–24
31	6	.	.	–	≡²0⁰⁰–6³⁰ ≡²·¹–8³⁵ = –13¹⁵. 15⁰²–24
Σ	–	39.6	–	–	UWAGI

Wrocław - Gądów Mały — φ = 51°08' — λ = 16°59' — Listopad - Novembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dias	I	II	III	Dias	Max	Min	I	II	III	Dias	I	II	III	Dias	I	II	III	I	II	III
1	107.8	107.6	109.7	108.4	6.4	10.4	9.4	8.9	10.6	4.4	91	75	88	85	0.9	3.2	1.4	1.8	9	10	5	SSW 4	SW 5	W 5
2	110.5	106.8	101.3	106.2	7.4	12.4	8.7	9.5	13.0	6.1	97	68	86	84	0.3	4.7	1.5	2.2	10	4	0	SW 1	SSW 5	S 4
3	95.2	93.6	93.3	94.0	8.1	11.1	9.7	9.6	11.8	5.3	79	74	75	76	2.3	3.4	2.9	2.9	8	9	8	SSW 7	SSW 9	SW 7
4	95.9	96.8	98.6	97.1	4.8	5.8	3.6	4.4	9.7	3.5	82	64	85	77	1.5	3.3	1.2	2.0	10	10	10	W 4	WNW 5	NW 2
5	99.1	100.0	102.8	100.6	2.5	3.7	4.4	3.8	4.6	2.3	91	95	100	95	0.6	0.4	0.0	0.3	10	10 •	10 •	NW 2	NW 5	NW 2
6	101.9	99.0	95.9	98.9	4.6	5.8	8.7	7.0	8.7	4.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ●	10 ●	10 ●	NNE 2	NE 3	ENE 1
7	91.9	91.2	92.4	91.8	9.6	9.9	7.7	8.7	10.9	6.6	100	97	98	98	0.0	0.3	0.1	0.1	10 ●	10 •	7	ENE 2	SE 4	S 3
8	94.4	94.7	93.8	94.3	5.1	6.6	5.6	4.7	8.2	2.8	92	82	88	87	0.7	1.7	0.9	1.1	10	10	0	SW 2	S 1	SSE 4
9	91.8	91.5	89.8	91.0	2.6	9.4	5.8	5.9	10.9	1.9	96	71	91	86	0.3	3.4	0.8	1.5	5	9	8	ESE 2	SSE 5	SE 3
10	87.5	89.9	92.3	89.9	7.0	9.2	6.6	7.4	9.4	4.5	91	92	100	94	0.9	0.9	0.0	0.6	10	10 •	10 •	E 1	W 5	WSW 1
11	90.8	91.4	92.4	91.5	6.1	8.0	7.6	7.3	8.6	5.6	100	94	100	98	0.0	0.6	0.0	0.2	10 ≡	10	10	C 0	C 0	NE 1
12	94.0	94.7	95.8	94.8	6.8	8.4	7.6	7.6	9.6	6.5	100	93	94	96	0.0	0.7	0.6	0.4	10 ≡	10	10	E 1	E 3	E 5
13	95.9	92.4	92.1	92.8	6.8	6.8	5.8	6.5	9.1	5.8	97	100	97	98	0.3	0.0	0.3	0.2	10	10 •	10	ENE 6	ENE 6	ENE 6
14	95.3	99.8	103.9	99.7	2.1	1.6	0.8	1.3	5.8	0.7	96	96	100	97	0.3	0.3	0.0	0.2	10 •	10 •	10 ●	N 2	N 4	NNE 2
15	104.8	105.7	106.7	105.7	0.8	2.2	1.4	1.4	2.4	0.6	100	84	92	92	0.0	1.2	0.6	0.6	10 ●	10	10	N 1	C 0	N 1
16	105.8	104.1	102.2	104.0	1.1	1.5	1.9	1.6	2.5	0.8	90	91	89	90	0.6	0.6	0.8	0.7	10	10	10	SW 2	WNW 1	W 4
17	99.1	98.8	99.6	99.2	3.6	5.4	6.1	5.3	6.4	0.5	95	95	88	93	0.4	0.5	1.1	0.7	10 •	10	8	WNW 4	W 6	WNW 5
18	97.7	97.7	100.3	98.6	4.2	6.0	3.2	4.2	6.6	2.0	80	85	91	85	1.6	1.5	0.7	1.3	10	9	10	WNW 6	W 9	WNW 2
19	103.2	106.5	112.8	107.5	-0.6	3.8	-0.2	0.7	5.2	-1.6	100	87	94	94	0.0	1.1	0.4	0.5	8	6 ⊙	0	W 4	NW 3	WNW 1
20	117.7	120.6	125.0	120.4	0.4	3.5	-4.0	-1.0	4.2	-4.0	86	71	97	85	0.9	2.2	0.1	1.1	9	2 ⊙	8	NW 2	N 2	C 0
21	120.2	117.8	114.5	117.5	-4.5	3.6	-5.4	-2.9	3.9	-5.5	98	67	92	86	0.1	2.6	0.3	1.0	0	3	7 ≡	C 0	SE 3	C 0
22	111.4	109.2	105.6	108.7	-6.3	4.4	-2.2	-1.6	5.4	-7.7	99	66	98	88	0.0	2.9	0.1	1.0	4	8	3	ESE 1	C 0	E 1
23	102.2	100.5	100.2	101.0	-7.6	5.3	-2.5	-1.8	7.1	-8.6	96	57	91	81	0.1	3.8	0.5	1.5	1	1 ⊙	0	ENE 1	WSW 1	S 2
24	102.6	103.5	103.3	103.1	-4.6	5.5	2.6	1.5	5.6	-5.2	98	71	93	87	0.1	2.6	0.6	1.1	8	8	10	C 0	C 0	ESE 1
25	102.6	101.8	99.5	101.3	1.1	5.0	2.6	2.8	5.6	0.6	100	84	89	91	0.0	1.4	0.8	0.7	10	9	9	C 0	S 2	ESE 1
26	97.2	94.7	91.6	94.5	-5.6	6.6	-1.6	0.0	7.2	-5.6	99	75	100	91	0.1	2.4	0.0	0.8	3 ≡	9	2	C 0	SE 4	C 0
27	87.8	87.5	90.6	88.6	1.0	3.2	1.4	1.8	3.6	-3.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	9 ≡	10 ≡	ESE 1	W 2	W 1
28	94.4	96.2	98.4	96.3	0.7	5.9	0.5	1.9	6.2	-2.0	98	95	100	98	0.1	0.5	0.0	0.2	9	7 ≡	10 ≡	S 1	ENE 1	E 1
29	100.0	101.4	100.3	100.6	3.8	5.0	0.9	2.6	6.4	-0.6	98	97	98	98	0.1	0.3	0.1	0.2	9	10 •	0	SSE 1	W 3	S 2
30	96.2	96.1	90.1	94.1	3.0	6.4	5.5	5.1	6.8	0.1	79	73	86	79	1.6	2.6	1.2	1.8	9	9	10 ●	SSW 5	SSW 8	SW 9
31																								
M	99.8	99.7	99.8	99.8	2.4	6.1	3.3	3.8	7.2	0.8	94	83	93	90	0.5	1.6	0.6	0.9	8.4	8.4	7.2	2.2	3.5	2.6

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1	83.9	84.3	86.4	84.9	8.6	11.7	7.0	8.6	12.1	5.3	77	72	98	82	2.6	3.7	0.1	2.1	10	9	10	SW 7	WSW 11	ESE 1
2	80.8	79.9	87.5	82.7	10.7	13.4	5.9	9.0	14.5	6.6	82	68	67	72	2.3	5.0	3.1	3.5	9 ●	8	6	SSW 8	SW 11	W 10
3	96.4	95.3	93.6	95.1	0.4	6.3	1.8	2.6	7.2	-0.4	86	56	83	75	0.9	4.1	1.2	2.1	2	1 ⊙	9	S 4	S 5	SSE 2
4	88.9	95.2	96.1	93.4	7.4	7.4	6.5	7.0	8.4	1.2	87	97	97	94	1.3	0.3	0.3	0.6	10	10 ●	9	SW 2	NW 1	SSE 3
5	94.3	93.3	92.3	93.3	13.9	15.8	12.7	13.8	16.4	6.5	76	65	69	70	3.9	6.2	4.6	4.9	9	9	3	S 6	SSW 8	S 5
6	97.3	99.3	100.3	99.0	6.8	4.0	1.5	3.4	12.8	1.5	56	59	78	64	4.4	3.3	1.5	3.1	10	10	3	W 7	W 6	W 4
7	100.0	101.3	104.3	101.9	0.2	1.1	-1.4	-0.4	2.0	-1.7	92	90	89	90	0.5	0.6	0.6	0.6	10	9	0	WNW 2	NW 3	WNW 4
8	104.6	104.9	106.3	105.3	-0.5	1.6	0.2	0.4	2.1	-3.2	94	76	86	85	0.4	1.7	0.9	1.0	9	8	9	W 3	W 4	W 2
9	105.6	102.7	99.4	102.6	-3.5	1.6	0.0	-0.5	2.0	-4.4	90	69	75	78	0.5	2.2	1.5	1.4	4	4	10	SE 2	SSE 7	SE 5
10	97.9	97.7	97.0	97.5	1.1	3.2	1.4	1.8	3.2	-0.6	79	83	91	84	1.4	1.3	0.7	1.1	9	10	6	S 4	SE 1	SSE 1
11	90.1	82.3	83.8	85.4	2.4	4.1	9.7	6.5	10.2	0.6	87	93	89	90	1.0	0.6	1.2	0.9	10	10 •	10 •	SSE 5	S 8	W 8
12	90.1	92.6	96.9	93.2	8.6	6.5	2.6	5.1	10.0	2.6	96	99	98	98	0.5	0.2	0.2	0.3	10 ●	10 ●	10 •	WNW 6	NE 1	NE 3
13	107.8	113.0	114.6	111.8	-1.2	-5.0	-5.4	-5.8	3.2	-6.0	91	81	87	86	0.5	0.9	0.5	0.6	10 *	4	0	NE 2	C 0	NE 2
14	115.1	115.9	117.5	116.2	-8.2	-4.2	-8.0	-7.1	-3.8	-10.0	92	54	78	75	0.2	2.1	0.7	1.0	0	1 ⊙	0	ENE 1	NNE 2	NW 3
15	114.1	110.2	113.9	112.7	-5.4	-2.8	-10.8	-7.4	-1.7	-11.2	90	88	94	91	0.4	0.6	0.2	0.4	9 *	10 *	9	WNW 7	NW 6	NE 2
16	120.0	123.5	128.9	124.1	-17.6	-15.8	-20.2	-18.0	-10.2	-18.3	95	79	82	85	0.1	0.4	0.2	0.2	0	4 ⊙	0	N 2	NE 4	N 1
17	130.8	130.3	128.9	130.0	-21.6	-15.0	-16.3	-16.8	-12.2	-22.9	81	92	95	89	0.2	0.2	0.1	0.2	0	1 ⊙	9	W 1	NW 1	W 3
18	127.7	127.1	125.4	126.7	-10.8	-8.6	-10.8	-10.2	-7.7	-16.6	94	77	80	84	0.2	0.7	0.5	0.5	10	10	0	NW 4	WNW 5	WNW 4
19	121.7	120.2	118.5	120.1	-7.0	-4.6	-5.6	-4.7	-5.6	-11.9	85	91	99	92	0.5	0.4	0.1	0.3	10	10 ▲	10 •	W 4	W 7	W 5
20	113.9	106.5	101.9	107.4	-2.6	0.2	1.4	0.1	1.8	-4.1	98	94	96	96	0.1	0.4	0.3	0.3	10	10	10 •	W 7	W 10	WNW 4
21	100.1	102.7	104.8	102.5	0.7	1.2	-4.4	-1.7	1.8	-5.1	98	85	89	90	0.1	1.2	0.5	0.6	10 *	7	2	W 3	NNW 5	WNW 2
22	96.2	92.9	96.5	95.2	-1.7	-2.6	-5.5	-3.8	0.1	-8.1	98	100	95	98	0.1	0.0	0.2	0.1	10 *	10 *	10 *	W 4	NNE 5	W 1
23	101.5	102.6	103.7	102.6	-7.7	-6.8	-7.9	-7.6	-4.6	-12.7	99	91	96	95	0.0	0.3	0.1	0.1	10	9	10	WNW 1	W 2	NNW 1
24	104.3	103.0	102.1	103.1	-9.5	-8.0	-10.0	-9.4	-7.6	-11.4	91	90	87	89	0.3	0.3	0.4	0.3	10 *	10	10	C 0	S 2	SSE 2
25	99.7	98.1	96.5	98.1	-15.8	-15.3	-18.3	-16.9	-9.8	-19.1	95	82	84	87	0.1	0.3	0.2	0.2	0	0 ⊙	0	C 0	SE 1	SE 1
26	93.7	92.0	95.4	93.0	-22.6	-10.0	-20.4	-18.4	-9.0	-24.4	80	74	76	77	0.2	0.7	0.3	0.4	0	2	0	E 1	ESE 2	C 0
27	97.2	98.5	99.4	98.4	-21.1	-12.2	-16.6	-16.6	-11.7	-21.4	82	85	90	86	0.2	0.4	0.2	0.3	8	3	0	NW 1	C 0	ENE 4
28	96.1	94.1	93.5	94.6	-11.4	-8.2	-5.4	-7.6	-5.2	-18.7	93	84	85	87	0.2	0.5	0.6	0.4	10	10	9	E 3	SE 3	E 1
29	95.1	94.3	93.5	94.3	-10.4	-2.7	-5.1	-4.8	-1.0	-12.8	90	95	90	92	0.3	0.2	0.3	0.3	10 ≡	0 ≡ ⊙	0	C 0	NE 1	ESE 2
30	91.7	92.2	92.2	92.0	-4.1	3.6	-0.6	-0.4	4.4	-9.7	96	75	90	87	0.2	2.0	0.6	0.9	8	2	8	C 0	SE 3	SE 2
31	92.9	91.8	88.9	91.2	-3.2	3.9	2.3	1.3	4.2	-8.3	99	77	84	87	0.0	1.9	1.2	1.0	9	3	7	ESE 1	ESE 2	SSE 4
M	101.6	101.2	101.9	101.6	-4.0	-1.0	-3.7	-3.1	0.9	-7.7	89	81	87	86	0.8	1.4	0.8	1.0	7.6	6.5	5.8	3.2	4.0	3.0

Wrocław - Gądów Mały $H_s = 116\,m$ $H_b = 118{,}6\,m$ $h_w = 20\,m$ Listopad - Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	2.1	.	-	• 13²⁰–15²⁰ 17²⁰. = 0⁰⁰–24, ▽ 4⁵⁰–5⁴⁰
2	7	.	.	-	= 0⁰⁰–9¹⁰
3	7	1.0	.	-	⩥ 10⁴⁰–12³⁰
4	7	.	.	-	• 5⁰⁰ 6⁵⁰ = 17³⁰–24
5	6	3.9	.	-	• 8¹⁰–14³⁰ 15¹⁵–24, = 0⁰⁰–8²⁰
6	4	6.3	.	-	• 0⁰⁰–1³² • 2¹⁰–14¹⁵ •• –20¹⁵ • –20⁴⁰ 23³⁰. = 0⁰⁰–24
7	5	1.0	.	-	• 1⁴⁵ 9²⁰, 9⁴⁰–10³⁵ • 12³⁰ 13²⁵, 14¹⁰⁻³⁰. = 0⁰⁰–24
8	6	.	.	-	= 0⁰⁰ a, a–24
9	8	.	.	-	= 0⁰⁰–10¹⁵, p–np, ⌴ 6⁰⁰–9⁰⁰
10	6	3.3	.	-	• 10⁰⁰ 14³⁰–23³⁹. = 0⁰⁰–24
11	6	0.0	.	-	• 11⁰⁷–18. = 0⁰⁰–4³⁰ =⁰⁻¹ 7⁴⁰ = –23⁴⁰
12	5	0.0	.	-	• 4³⁰–6³⁰, 7³⁵–8²⁰, =²⁻⁰ 0⁰⁰–9²⁰ = –24
13	5	8.4	.	-	• 7³⁵ 8¹⁰–10⁴⁰ • –15³⁵ 16²⁰–17³⁵ • 23³⁰–24. = 0⁰⁰–24
14	7	2.0	.	-	• 0⁰⁰. 5³⁵ • 6³² 17³⁵ ⛌ 10⁰⁵⁻⁵⁰ 14²⁰–15⁰⁷ • 17³⁵. 22²⁸. = na, a, p–24
15	6	0.0	.	-	• 0²⁰ 8¹⁰ *' –8²⁰ • 9³⁰. = 0⁰⁰–24
16	6	0.2	.	-	= 0⁰⁰–24
17	6	0.0	.	-	• 1¹⁵ 7³⁵ • ' 10³⁵ 12³⁰ • 14⁰⁵ 15¹⁰ •• 16⁴⁰. = 0⁰⁰–24
18	7	(0.0)	.	-	• 9⁴⁵ 10¹⁰, 11³¹–⁴⁵. = na, p–np, ▽ 19³⁰–22²⁰
19	7	0.0	.	-	▽ 15⁴⁵–⁵⁵ 16⁴⁰–⁵⁰ = 0⁰⁰–11³⁰, ⌴ ' 3³⁰–9³⁰
20	8	.	.	-	= = 20¹⁰–24, ⌴ ' 18⁰⁰–24, ⌣ ' ¹⁰⁰⁻¹⁵ ⊖ 19⁴⁰–24
21	6	.	.	-	= 0⁰⁰ 13²⁰ p = ⁰ p–np, ⌴ ¹⁻⁰ 0⁰⁰–11⁰⁰, ▽ 0⁰⁰–1³⁵ Ψ p ⊖ np
22	4	.	.	-	= ⁰ 0⁰⁰ 24, ⌴ 10⁰⁰–15⁰⁰, 19⁰⁰–24, Ψ ¹⁰⁰–6¹⁰
23	6	.	.	-	= ⁰ 0⁰⁰–1⁴⁵ = = ⁰ 1⁴⁵–24, ⌴ 0⁰⁰–12⁰⁰ ▽ 1³⁰–3⁰⁰
24	5	1.1	.	-	• 23³⁰–24, = 0⁰⁰–24, ⌴ ⁰ 0⁰⁰–10³⁰, Ψ 22¹⁵⁻⁴⁰
25	4	0.0	.	-	• 0⁰⁰. 0¹⁵ 5⁵⁰ 9⁴⁰ 11³⁵. = 0⁰⁰–24
26	6	.	.	-	= 0⁰⁰–5³⁰ ≡ ⁰ 10⁴⁰ = –24, ⌴ 5⁵⁰–11⁰⁰, np; ⊖ np
27	3	3.2	.	-	• 14⁴⁰ 16¹⁰–18³⁰, = = ⁰⁻¹ = ² 0⁰⁰–24, ▽ 0⁰⁰–1³⁰
28	4	3.9	.	-	• 23⁵⁰. 24 =⁰⁻² = 0⁰⁰ p = ² –24
29	6	1.9	.	-	• ⁰⁻¹ 0⁰⁰ 0³⁰–3⁵⁷ • ⁰⁻¹ 10⁰¹–13²⁵, =²⁻⁰ 0⁰⁰–3⁰⁵ = –24, ⌴ np
30	6	1.1	.	-	• 18³⁵–19²⁰. 20¹⁵–21⁴⁰. 23¹⁰–24, = na, a–p, ⌴ na–a
31					
Σ	–	39.4	–	-	UWAGI:

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1	8	5.1	.	-	• 0⁰⁰ 5³⁴ 15²⁰–17⁰⁰ • ¹ 17¹⁵ • ⁰ 20¹⁰. 20³⁵, ⩥ a–p, np, = p–np
2	8	0.9	.	-	• 6²² 7³⁰ • ¹ 16²⁰–17⁷⁰, ⩥ na, a–24
3	7	6.2	.	-	= 9²⁰ 11³⁰, 20³⁰–24 ⌴ 4⁵⁰–10⁰⁰
4	6	3.0	.	-	• 1²⁵ 5⁰⁶ 5³⁵ • ⁰ • 8¹⁵ 15³⁵ • 21³⁵–22⁴⁰. = 0⁰⁰–24
5	8	.	.	-	= 0⁰⁰⁻³⁰
6	8	.	.	-	
7	5	0.0	.	-	* ⁰ 7⁵⁰–8¹⁵, = 7³⁰–24
8	6	0.0	.	-	⛌ ⁰ 11³⁰⁻³⁰, = 0⁰⁰–24, ⌴ 3⁰⁰–9⁰⁰
9	6	0.2	.	-	= 0⁰⁰–24, ⌴ 4⁰⁰–11⁵⁰ ⊕ 8⁵⁰–11²⁰
10	6	0.8	.	-	• ⁰ 12. 36 △ 2¹² 3¹⁵. 7⁴⁰ 10²⁰. = 0⁰⁰⁻²⁰. 7³⁰–24 ∽ 6²⁰–10²⁰
11	6	9.4	.	-	• 5⁵⁰ 6³⁰ • ⁰⁻¹ 9²⁵ 12³⁷ 13¹² • ⁰ 15⁵² 24. = 0⁰⁰–14⁴⁰
12	4	9.7	.	-	• ⁰. • ⁰. • ⁰ 0⁰⁰–22⁴⁰. = 3³⁰–24
13	7	0.1	.	-	• ⁰ 0⁴⁵ 2⁴⁰ * ⁰ 7⁴⁰
14	7	0.0	.	-	= 0⁰⁰–2⁵⁰. 5⁴⁰–11⁴⁵. ⌴ 3⁰⁰–24
15	5	2.6	pż.	-	* ⁰ 3⁵⁰–7²⁵ * ⁰⁻² 8³⁵–11⁴⁰. 12³⁵–19²⁰. = 22³⁰–24, ⌴ 0⁰⁰–3⁵⁰
16	7	.	8	-	= 0⁰⁰–11³⁰, 14³⁰–24
17	6	0.0	8	-	* ⁰ 22¹⁵. 24, = 0⁰⁰–24, ▽ 20²⁰⁻⁵⁰
18	6	.	6	-	* ⁰ 0⁰⁰. 0²⁰–1²⁵. = 0⁰⁰–24
19	5	0.0	6	-	△ 10⁴⁰–13³⁰ ⌾ ⁰–24 = 0⁰⁰–24
20	5	1.6	5	-	⌾ ⁰ 0⁰⁰ 8³⁰. 15⁵²–16³⁰ • ⁰–24, = 0⁰⁰–24
21	8	2.1	pż.	-	• ' 0⁰⁰–1⁴⁰ •• ⁰–2²⁰ △ ⁰ 5²⁰–6¹⁰ * '–7³⁰ • ⁰ 8³⁵. 9¹⁵ △ 9⁴⁰–10²⁰ * ⁰ 12⁰⁰⁻³⁰, 13⁴⁵–14²⁰. = 0⁰⁰–10³⁰, Ψ np
22	5	1.5	5	-	* ⁰ 2³⁵–6¹⁵ * ⁰⁻¹ 9²⁵–14⁴⁰ * ⁰ 20³⁵–22¹⁵. = 20³⁵–24, Ψ 0⁰⁰–1³⁵
23	6	0.0	12	-	* ⁰ 10³²–11⁰⁷. = 0⁰⁰–13³⁰. 15³⁰–21³⁰ ≡ 22³⁰–24
24	6	0.3	12	-	* ⁰ 6⁴⁵–7¹⁷. 7²⁵–12¹⁰. 21³⁵–24. ≡ 0⁰⁰–1⁴⁵ = –4²⁰ = –4⁵⁵ = na–p, p–24
25	5	(0.0)	8	-	* ⁰ 0⁰⁰⁻³⁰ 7¹⁵–a. = 0⁰⁰–24
26	4	.	8	-	= 0⁰⁰–24
27	4	0.0	8	-	△ 21³⁰⁻⁵⁵ * –22¹⁵, = 0⁰⁰–16⁴⁰ = –18²⁰ = –24. ▽ 0⁵⁰–3¹⁰
28	5	.	8	-	= 0⁰⁰–24
29	5	.	8	-	= 0⁰⁰–1⁴⁰ ≡ ¹⁻² 8³⁰ ≡ a–p = –24
30	5	.	7	-	= 0⁰⁰–24
31	6	0.0	6	-	• 23²⁵–⁴⁰. = 0⁰⁰–24
Σ	–	45.5	–	-	UWAGI:

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	73.7	74.3	74.3	74.1	−5.6	3.9	−0.5	−0.7	4.2	−6.6	92	64	86	81	0.3	2.9	0.9	1.4	8	9 ⊙	8	ESE 1	C 0	ENE 1
2	72.1	69.5	65.2	68.9	−1.6	4.2	−2.2	−0.4	4.2	−2.8	90	60	91	80	0.5	3.3	0.5	1.4	10	1	7	SW 1	SSE 2	ESE 3
3	55.3	54.5	58.5	56.1	5.6	3.9	2.4	3.6	6.6	−3.1	50	65	86	67	4.5	2.8	1.1	2.8	8	9	10	ENE 7	S 9	ESE 1
4	54.2	54.0	60.4	56.2	5.9	6.4	1.2	3.7	6.8	1.0	74	60	74	69	2.4	3.8	1.8	2.7	10	9	9	ESE 3	WSW 6	SE 1
5	62.6	65.5	71.9	66.7	−0.9	3.4	1.6	1.4	5.2	−2.6	92	66	85	81	0.5	2.6	1.1	1.4	8	8	10	SE 1	WSW 7	W 5
6	72.9	69.6	68.5	70.3	−2.6	4.1	1.8	1.3	5.1	−4.6	91	58	71	67	0.5	5.1	2.1	2.6	0	8 ⊙	10	W 3	SSE 7	SE 5
7	67.5	68.0	70.3	68.6	1.7	3.7	0.9	1.8	5.1	0.2	70	64	92	75	2.0	2.9	0.5	1.8	9	8 ⊙	9 *	SE 6	WSW 3	NW 4
8	72.4	69.4	68.1	70.0	−1.6	2.4	3.2	1.8	3.4	−2.0	93	75	73	80	0.3	1.8	2.1	1.4	8	10	10	SE 2	SE 3	WSW 6
9	69.5	69.3	68.7	69.2	3.4	4.1	4.1	3.9	6.5	2.0	75	58	71	68	2.0	3.5	2.4	2.6	8	9 ⊙	9	WSW 4	SW 6	SSW 2
10	72.0	69.5	67.5	69.7	−0.5	4.7	2.3	2.2	6.2	−2.5	92	53	68	71	0.5	4.0	2.3	2.3	4	5 ⊙	10	SE 1	SE 2	SE 6
11	69.7	73.3	80.5	74.5	1.6	3.7	−0.4	1.1	3.9	−0.6	71	65	92	76	2.1	2.8	0.5	1.8	9	10	10 *	ESE 5	WSW 2	WNW 5
12	85.9	88.4	91.6	88.6	−2.8	−2.8	−3.4	−3.1	−0.4	−3.8	73	84	70	76	1.3	0.8	1.4	1.2	10	10 *	9	WNW 6	WNW 5	WSW 2
13	91.5	89.3	87.7	89.5	−12.2	0.1	−0.5	−3.3	0.9	−14.1	89	58	70	72	0.3	2.6	1.8	1.6	3	9 ⊙	9	NE 1	SE 1	SE 1
14	86.2	87.1	91.2	88.2	−0.3	0.2	−0.9	−0.5	0.8	−1.5	80	90	95	88	1.2	0.6	0.3	0.7	10 *	10 *	10 *	ESE 2	SE 1	C 0
15	93.1	92.5	90.0	91.9	−0.7	0.0	−6.0	−3.2	0.3	−10.7	96	84	97	92	0.2	1.0	0.1	0.4	10	1	10 ≈	C 0	ENE 3	NE 2
16	86.1	86.4	86.5	86.3	−17.5	−7.3	−5.2	−8.8	−3.4	−19.2	85	90	95	90	0.2	0.3	0.2	0.2	0	9	10 ≙	C 0	C 0	0 0
17	88.0	91.1	94.8	91.3	−5.4	−4.2	−17.5	−11.2	−2.9	−17.8	95	79	90	88	0.2	0.9	0.2	0.4	9	2 ⊙	0	C 0	ESE 4	E 4
18	96.1	97.0	95.1	96.1	−14.3	−7.0	−10.1	−10.4	−5.8	−22.5	83	50	65	66	0.3	1.8	1.0	1.0	0	1	0	ENE 5	E 5	ESE 2
19	91.7	89.5	88.7	90.0	−22.6	−5.0	−13.2	−13.5	−2.8	−23.6	88	61	92	80	0.1	1.6	0.7	0.6	0	0	0	SE 3	C 0	C 0
20	86.1	85.8	82.5	84.1	−17.5	−0.9	−14.0	−11.6	−0.3	−18.2	90	61	92	81	0.2	2.2	0.2	0.9	0	0	0	C 0	C 0	ESE 2
21	80.4	78.7	78.3	79.1	−18.3	−1.4	−14.0	−11.9	−0.8	−19.1	90	60	96	82	0.2	2.2	0.1	0.8	0	4	0	C 0	C 0	SE 3
22	75.0	72.8	71.9	73.2	−17.6	0.4	−1.9	−5.2	1.6	−18.6	90	80	85	85	0.2	1.3	0.8	0.8	2	9	10	SE 2	C 0	C 0
23	68.9	69.0	71.8	69.9	−3.5	−1.4	−6.6	−4.5	−1.4	−7.1	90	80	94	88	0.5	1.1	0.2	0.6	10 *	10 *	10 *	E 2	E 4	E 7
24	72.4	70.5	69.4	70.8	−7.5	−5.8	−9.2	−7.9	−5.3	−9.5	87	74	76	79	0.4	1.0	0.7	0.7	9	9	6	E 4	E 5	E 7
25	67.9	68.8	72.9	69.9	−8.0	−7.8	−11.8	−9.8	−6.9	−11.9	84	87	82	84	0.5	0.4	0.4	0.4	10	10 *	10	ESE 5	ESE 7	ESE 8
26	77.4	80.9	85.4	81.2	−14.2	−7.6	−20.1	−15.5	−7.3	−21.1	79	62	89	77	0.4	1.3	0.1	0.6	0	0	0	E 9	ENE 7	C 0
27	89.2	88.0	86.7	88.0	−25.9	−6.1	−17.5	−16.8	−3.9	−29.1	88	61	85	78	0.1	1.5	0.2	0.6	0	0	0	C 0	C 0	C 0
28	82.6	79.7	74.1	78.8	−7.8	−0.4	−5.7	−5.9	0.4	−18.8	61	49	53	54	1.3	3.0	2.2	2.2	3	7	3	ENE 1	E 5	C 0
29	76.3	78.7	76.6	77.2	3.0	4.6	5.6	4.7	5.6	−6.0	74	70	67	70	2.0	2.6	2.9	2.5	5	2 ⊙	8	SW 2	W 6	WSW 6
30	68.1	65.6	65.6	66.4	5.2	5.8	6.4	6.0	7.1	4.4	60	71	78	70	3.5	2.6	2.1	2.7	8	10	10	SW 8	SSW 9	SSW 5
31	62.4	57.6	66.3	62.1	3.8	5.4	5.3	5.0	7.3	3.5	95	91	72	86	0.4	0.9	2.5	1.3	10	10 ⊙	6	C 0	C 0	WSW 6
M	76.4	75.9	76.8	76.4	−5.8	0.1	−4.0	−3.4	1.3	−9.2	83	68	82	78	0.9	2.1	1.1	1.4	5.8	6.4	6.9	2.7	3.5	3.0

Luty – Février

1	59.3	54.2	58.7	57.4	1.8	4.5	2.9	3.0	5.9	0.0	91	79	67	79	0.7	1.8	2.4	1.6	10	10 •	9	S 3	NW 3	WSW 6
2	57.2	53.4	49.0	53.2	2.1	4.2	1.7	2.4	5.0	0.7	66	52	67	62	2.4	3.9	2.3	2.9	9	7 ⊙	4	SW 3	SE 3	SE 5
3	54.3	56.9	62.6	57.9	−0.3	0.3	−0.4	−0.2	2.2	−0.7	92	86	92	90	0.5	0.8	0.5	0.6	9	9 *	10 *	W 6	W 4	W 5
4	67.6	65.5	57.7	63.6	−0.3	1.7	0.0	0.4	2.5	−2.0	84	62	77	74	1.0	2.6	1.4	1.7	10	6 ⊙	10	W 6	WSW 5	SE 3
5	68.1	75.5	79.6	74.4	−0.8	−0.6	−8.3	−4.5	0.5	−8.9	91	67	89	82	0.5	1.9	0.3	0.9	10 *	6	0	WNW 6	WNW 5	C 0
6	76.5	73.6	67.6	72.6	−6.1	2.5	1.8	0.0	4.1	−14.0	81	72	83	79	0.7	2.1	1.2	1.3	9	9	9	C 0	ENE 2	ESE 3
7	67.8	68.0	68.0	67.9	−0.5	5.3	3.5	3.0	5.9	−1.9	94	60	78	77	0.4	3.6	1.7	1.9	2	7	3	C 0	WSW 4	WSW 5
8	73.5	76.0	79.5	76.3	2.6	2.0	0.6	1.4	3.8	0.5	79	89	90	86	1.6	0.8	0.6	1.0	10	10	8	W 6	W 5	SSW 1
9	74.1	69.7	71.1	71.6	0.8	2.5	5.3	3.5	7.8	−0.7	94	98	91	94	0.4	0.1	0.8	0.4	10	10 •	10 •	C 0	E 1	WNW 9
10	79.2	85.2	86.6	83.7	1.9	1.2	1.8	1.7	5.6	0.9	91	96	91	93	0.6	0.3	0.7	0.5	10 •	10 •	10	W 9	WNW 7	WSW 2
11	78.6	72.9	72.1	74.5	0.2	6.8	5.0	4.2	8.0	−0.7	96	72	89	86	0.3	2.7	1.0	1.3	10	9	10	C 0	C 0	NW 7
12	65.6	69.9	78.6	71.4	3.2	3.4	3.7	3.5	6.0	2.2	95	90	93	93	0.4	0.8	0.6	0.6	10 •	10 •	10 •	S 4	W 6	NW 4
13	81.7	82.5	84.6	82.9	1.9	6.6	3.2	3.7	6.9	1.6	98	72	95	88	0.1	2.7	0.5	1.1	10	9	10 •	SE 2	WSW 2	N 1
14	86.2	87.1	86.3	86.5	2.8	6.1	−0.4	2.0	7.4	−0.9	96	95	96	96	0.3	0.4	0.2	0.3	10 ϟ	10	0 ≈	C 0	N 1	C 0
15	87.1	88.3	90.0	88.5	−2.6	11.4	1.6	3.0	14.8	−3.0	98	62	93	84	0.1	5.2	0.6	2.0	1	2	0	C 0	C 0	C 0
16	92.3	94.1	96.2	94.2	5.7	6.2	5.1	5.5	6.5	−1.5	88	85	95	89	1.2	1.6	0.4	1.1	10	10	10 ϟ	W 4	WNW 5	W 2
17	95.5	94.9	94.7	95.0	3.6	9.4	0.6	3.6	11.3	0.4	95	65	94	85	0.4	4.1	0.4	1.6	10	6	0	C 0	NE 2	C 0
18	92.9	90.8	90.7	91.5	−3.6	13.6	0.5	2.8	15.0	−4.3	94	49	96	80	0.3	7.9	0.2	2.8	0	0	0	C 0	WNW 4	C 0
19	90.1	90.6	92.1	90.9	−0.8	4.2	4.0	2.8	4.7	−3.1	95	92	98	94	0.4	0.6	0.2	0.4	10	10	10 ϟ	C 0	NNW 1	WNW 2
20	93.0	93.9	94.0	93.6	3.9	5.0	3.4	3.9	5.7	3.2	88	86	95	90	1.0	1.2	0.4	0.9	10	10	10	WNW 4	NW 2	C 0
21	92.4	91.9	92.1	92.1	2.7	8.4	2.4	4.0	9.1	2.2	89	60	77	75	0.8	4.4	1.7	2.3	10	2	0	NE 2	ESE 4	SE 4
22	92.1	91.4	90.6	91.4	−3.2	7.6	−1.0	0.6	8.3	−4.1	95	56	94	82	0.2	4.6	0.4	1.7	0	0	0	C 0	C 0	E 2
23	89.1	88.1	87.3	88.2	−4.2	7.2	−1.5	0.0	7.9	−6.0	96	63	96	85	0.2	3.8	0.3	1.4	2	4	2	C 0	E 1	C 0
24	87.0	86.7	87.2	87.0	−4.6	10.2	1.2	2.0	12.6	−5.2	98	45	89	77	0.1	6.8	0.8	2.6	10 ≈	0	0	C 0	C 0	C 0
25	87.5	87.5	87.7	87.6	−5.2	9.3	−1.4	0.8	9.5	−5.9	92	53	83	76	0.3	5.5	0.9	2.2	0 ⊙	1 ⊙	0	SE 1	E 3	C 0
26	89.8	90.9	91.2	90.6	−4.4	9.7	1.6	2.1	11.1	−5.4	91	48	87	75	0.4	6.2	0.9	2.5	0	0	0	C 0	ESE 2	ESE 1
27	89.3	87.4	84.2	87.0	1.4	9.3	8.8	7.1	10.3	−0.7	87	67	78	77	0.9	3.8	2.4	2.4	7	10	10	ESE 2	E 3	SSE 1
28	74.3	68.4	76.1	72.9	10.0	10.6	3.2	6.8	13.1	2.3	73	63	81	72	3.3	4.7	1.5	3.2	10	10	10	SW 6	SW 7	WSW 8
29																								
30																								
31																								
M	80.1	79.8	80.6	80.2	0.4	6.0	1.7	2.4	7.6	−1.9	90	71	88	83	0.7	3.0	0.9	1.5	7.3	6.7	5.5	2.3	2.9	2.5

Jelenia Góra $H_s = 342\,m$ $H_b = 343{,}9\,m$ $h_w = 15\,m$ **Styczeń – Janvier 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	= 0⁰⁰–7³⁰; ▽ 22²⁰–24
2	7	.	.	–	▽ 0⁰⁰–1³⁰
3	8	0.3	.	–	• °17⁵⁰ 18⁵⁰, 19⁴⁵–20⁴⁰, 22³⁰–24, » 10⁴⁰–11³⁰
4	8	0.0	.	–	• °0⁰⁰...⁴⁰, 11⁵⁵–12⁰², ▽ 22⁴⁰–24
5	7	.	.	–	▽ 0⁰⁰–5²⁵, ⌴ °2⁰⁰–7⁰⁰
6	8	.	.	–	
7	8	0.8	.	–	✳°▽ 11⁵⁴–12¹⁰, 19⁴⁰–21⁴⁰, •°▽–22³⁵ ✳•▽ 22⁴⁵–23¹⁰ ✳°▽–24
8	8	0.2	pł.	–	✳°▽ 0⁰⁰–2⁴⁰, 14³⁰–15¹⁰
9	8	0.2	pł.	–	✳°0⁴⁰–1⁴⁰, • °18³⁵...⁴⁰, 21³⁵ 23¹⁰–24
10	8	.	.	–	• 0⁰⁰–2⁵⁰, = 2⁴⁵–4³⁰, 5⁴⁰–10³⁰, 18²⁰–20²⁰
11	7	1.2	.	–	△°16¹⁰–³⁰ •–19⁰⁵ ✳¹–21¹⁰ ✳°–24, = 15³⁰–24
12	6	1.0	2	–	✳°0⁰⁰–1²⁰ ✳°7⁵⁰...10²⁰–14⁴⁰, = 0⁰⁰–7⁵⁰
13	8	0.0	3	–	= 18²⁰–22³⁰
14	5	10.7	2	–	✳°6⁴⁵ 7³⁵ •° 9²⁰ ✳⁰⁻¹ 11⁴⁰–12⁴⁵ 24, = 11⁴⁰–13³⁰
15	6	.	20	–	✳°0⁰⁰–2³⁰, 3³⁰–6¹⁵, = 6¹⁵–14⁴⁰ = 15⁴⁰–16⁴⁵ ≡¹–24
16	5	0.2	13	–	△ 19⁰⁵–24, ≡¹ 0⁰⁰–3⁴⁰ =–24
17	7	.	12	–	△ 0⁰⁰–1⁴⁵, = 0⁰⁰–7⁴⁰, 21²⁰–24
18	8	.	11	–	= 0⁰⁰–5¹⁵
19	5	.	10	–	= 8²⁰–14³⁰, 19⁴⁵–24
20	5	.	10	–	= 0⁰⁰–24
21	5		8	–	= 0⁰⁰–24
22	5	0.2	6	–	✳°18²⁰ 19⁴⁰, = 0⁰⁰ 7²⁰, 8⁴⁰–24
23	6	0.7	7	–	✳°3³⁰ 6²⁰–7⁴⁰ ✳¹–8⁴⁰ ✳°–21⁴⁵ 22²⁵–24, = 0⁰⁰–24
24	6	.	8	–	✳°0⁰⁰–1⁴⁵, = 0⁴⁵–20³⁰
25	5	2.0	8	–	✳°7³⁵ 8²⁰ ✳°▽–9⁰⁵ ✳⁰⁻¹ 9⁵⁰–20¹⁰ ✳°23¹⁰–24, = 9⁰⁵–24
26	8	.	11	–	✳°0⁰⁰–2⁰⁵, = 0⁰⁰–6⁰⁵, 20³⁰–24
27	5	.	10	–	= 0⁰⁰–13¹⁰ ∞–16³⁰
28	8	.	10	–	
29	7	.	10	–	par. wiatru do 11 m/sek 14⁵⁵–15⁰⁵, 15¹⁵⁻³⁰ » 21¹⁵–24
30	7	3.6	pł.	–	• °14²⁵–15¹⁰, 15²⁰–16⁰⁵, 22¹⁰–24, » 0⁰⁰–2¹⁵, 3⁴⁰–6²⁰
31	8	2.4	.	–	• 0⁰⁰–3²⁰, 7⁴⁰–10¹⁰...15²⁰, 16²⁰–18¹⁰ •▽–19²⁰
Σ	–	23.5	–	–	UWAGI.

Luty – Février

1	8	4.8	.	–	• °12³⁰...13³⁰ •⁰⁻¹–15⁴⁵
2	8	8.6	.	–	
3	6	0.7	10	–	✳⁰⁻¹▽ 0⁴⁰–2³⁵ ✳ᶻ▽6¹⁰–³⁵ ✳°9⁰⁵–13¹⁵ ✳⁰⁻¹▽ 15³⁰...21¹⁰ ✳°–24
4	7	0.0	11	–	✳°0⁰⁰–2⁴⁰ ✳°▽9³⁶–10⁰⁴ 16¹⁰⁻³⁰ 18⁴⁰⁻⁵⁰, = ra, a, p – np
5	7	0.2	11	–	✳°6¹⁰–7²⁰ △°–8¹⁵ ✳°–9⁴⁵ 10⁵⁰...11¹⁰, = 22²⁰–24
6	8	0.3	8	–	= 0⁰⁰–6³⁰
7	8	1.7	4	–	• °12⁸ 5¹⁰, 22²⁰–23⁴⁵ 24
8	7	2.1	.	–	• 0⁰⁰...2³⁰–5⁴⁰ •°▽7⁴⁵ 12⁴⁰ ✳ 14⁵⁰ 15¹⁵ △°21⁵⁰–22¹⁰ ✳°23⁴⁰–24, = 15¹⁵–24
9	6	21.5		–	✳°0⁰⁰ 5³⁰ ✳¹ 7²⁰–9³⁰ •⁰⁻¹▽ •¹▽ 9³⁰...22³⁵, = 0⁰⁰–6²⁰
10	6	0.7	.	–	• °0⁰⁰–5¹⁵, 6⁴⁵ 14²⁰
11	8	3.8	.	–	• °0⁰⁰ 2²⁰, 16⁵⁰ 17²⁰–20⁴⁰, = 2²⁰–6⁴⁰
12	6	7.4	.	–	• ⁰⁻¹6¹⁰ 20²⁰
13	7	0.2	.	–	• °0⁰⁰ 3³⁵, • °6³⁰ • °13⁵⁰–14¹⁰, 18⁴⁵ 22³⁰, = 0⁰⁰–10³⁰, np
14	5	0.6	.	–	• °2¹⁵ 4²⁰ •⁰⁻¹ 5¹⁵–8³⁰ 10³⁵, = 0⁰⁰–17²⁰ =–19⁵⁰ ≡²–24
15	7	0.3	.	–	≡⁰⁻¹0⁰⁰–3⁵⁰ =–8²⁰
16	6	0.4	.	–	• °3³⁰ 6⁴⁰ • °19¹⁰ 22³⁰ 24, = 0⁰⁰–24
17	7	.	.	–	• °0⁰⁰ 1³⁵, = 0⁰⁰–9⁴⁰ = 17²⁰–20⁴⁰ =–22¹⁰ ≡⁰⁻¹–24
18	7	.	.	–	≡¹0⁰⁰–3⁵⁰ =–10⁰⁰ 17³⁵ 24, ⌴ 4⁵⁰ 9⁰⁰
19	5	1.9	.	–	• 13³⁰–15⁴⁰, 17⁰⁵–18¹⁵ •¹–21⁴⁵ •°–24, = 0⁰⁰–24, ⌴¹2⁵⁰–9³⁰
20	6	0.0	.	–	• °0⁰⁰ 3¹⁵, • °6³⁰ • °7⁰⁵...25 •°–11²⁰, = 0⁰⁰–24
21	7	.	.	–	= 0⁰⁰–10⁴⁰
22	7	.	.	–	= 6¹⁰–7¹⁵ =–12¹⁰, 16³⁰–24, ⌴ 4⁵⁰ 9⁰⁰ 20⁰⁰–24
23	7	.	.	–	= 0⁰⁰–²⁰ ≡°–6⁵⁰ =–12¹⁰ 17³⁰ 22⁵⁰ ≡⁰⁻²–24, ⌴⁰⁻²0⁰⁰–10⁰⁰, ▽ 18⁵⁰–19⁵⁰
24	6	.	.	–	≡¹⁻²0⁰⁰–7⁵⁰ =–14²⁰ ∞–17³⁰ =–24, ⌴ °4⁰⁰ 9⁰⁰, 21⁰⁰–24
25	7	.	.	–	= 0⁰⁰ 9³⁰ 18³⁰–24, ⌴⁰⁻¹0⁰⁰–9⁰⁰, 22⁰⁰–24
26	7	.	.	–	= 0⁰⁰–6³⁰, ⌴⁰⁻¹0⁰⁰–10⁰⁰
27	7	0.0	.	–	⌴°4⁰⁰–8⁰⁰
28	8	1.7	.	–	• °4⁴⁵ 9²⁰ •▽° 16²⁵–18³⁰
29					
30					
31					
Σ	–	56.7	–	–	UWAGI.

Jelenia Góra — φ = 50°54' — λ = 15°48' — Marzec – Mars 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	75.8	79.6	85.1	80.2	3.4	2.9	2.5	2.8	4.4	1.6	76	84	96	85	1.9	1.2	0.3	1.1	10	10	9	W 3	WNW 6	NW 2
2	86.9	87.6	85.2	86.6	3.3	4.7	−0.3	1.8	5.9	−1.3	83	65	90	79	1.3	2.9	0.6	1.6	10	9	9	WNW 7	W 9	SE 2
3	85.7	89.3	92.0	89.0	1.4	6.3	4.6	4.2	6.7	−1.1	96	81	93	90	0.3	1.8	0.6	0.9	10	10	10 •	C 0	C 0	NW 2
4	94.1	96.1	96.4	95.5	4.0	5.6	−0.7	2.0	6.5	−1.2	93	80	98	90	0.5	1.8	0.1	0.8	10	9	0	WNW 2	WNW 5	C 0
5	95.0	95.2	95.4	95.2	−5.1	9.0	6.0	4.5	9.9	−5.4	95	66	85	82	0.3	4.0	1.5	1.9	8	9	10	C 0	W 6	WNW 2
6	95.1	94.5	92.4	94.0	4.0	9.9	2.0	4.5	11.1	−0.6	87	58	96	80	1.1	5.1	0.3	2.2	9	8	0	WSW 3	W 2	C 0
7	90.4	89.6	91.2	90.4	−1.8	11.6	2.7	3.8	13.0	−2.8	96	49	88	78	0.3	7.0	0.9	2.7	4	9 ⊙	0	C 0	WNW 7	C 0
8	94.0	94.6	95.2	94.6	−2.7	12.1	1.6	3.2	13.6	−3.5	100	46	85	77	0.0	7.5	1.1	2.9	0 =	0	0	C 0	WNW 4	SE 2
9	94.5	93.1	91.4	93.0	−2.6	14.3	1.3	5.6	15.4	−3.8	95	28	91	71	0.2	11.8	0.6	4.2	7 ⊙	2 ⊙	0	C 0	NW 4	C 0
10	88.3	84.6	82.9	85.3	−4.8	18.6	4.0	5.4	19.7	−5.1	93	20	82	65	0.3	17.1	1.5	6.3	0	2 ⊙	0	C 0	NW 2	SE 2
11	83.0	84.4	85.8	84.4	0.1	9.9	8.6	6.8	11.5	−0.6	98	68	72	79	0.2	3.9	3.2	2.4	2	9	10	SE 1	WNW 6	W 6
12	85.1	78.7	71.1	77.6	6.9	16.0	14.9	13.2	16.6	6.0	78	42	41	54	2.2	10.5	10.0	7.6	9	8	10	W 3	W 5	SW 9
13	71.7	72.9	76.4	73.7	7.0	8.8	6.6	7.2	14.9	5.9	80	57	74	70	2.0	4.9	2.5	3.1	10	6	8	W 3	WNW 8	WNW 3
14	74.8	76.3	78.7	76.6	7.4	8.1	8.2	8.0	9.2	5.2	96	94	81	90	0.5	0.6	2.1	1.1	10 •	10 •	10	WNW 4	W 7	W 6
15	79.4	82.9	84.7	82.3	8.0	9.4	9.3	9.0	11.2	7.4	90	83	81	85	1.0	2.0	2.2	1.7	10 •	9	9	W 5	W 7	W 8
16	82.1	81.9	83.7	82.6	9.8	11.2	8.1	9.3	12.6	5.6	58	62	76	65	5.0	5.1	2.5	4.2	6 ⊙	7	0	W 7	WNW 8	NW 3
17	85.6	82.4	75.6	81.2	0.2	15.7	6.7	7.3	17.0	−0.7	96	40	88	75	0.3	10.7	1.2	4.1	3	2 ⊙	0	C 0	NW 6	C 0
18	67.4	65.8	64.9	66.0	7.5	12.7	7.0	8.6	17.3	4.2	70	65	59	65	3.1	5.2	4.1	4.1	7 ⊙	9	10	C 0	NW 3	W 3
19	64.7	65.1	69.7	66.5	3.1	3.9	−0.2	1.6	7.4	−0.9	56	74	92	74	3.3	2.2	0.5	2.0	8	9 •	6	W 5	NW 9	NW 3
20	71.9	68.6	60.2	66.9	−5.0	2.7	1.8	0.3	4.1	−5.2	95	53	64	71	0.2	3.4	2.5	2.0	1	9 *	10	C 0	WNW 5	WSW 8
21	52.8	53.1	62.5	56.1	1.5	1.8	0.8	1.2	3.4	0.5	80	94	88	87	1.4	0.4	0.8	0.9	8 *	10 * •	10 *	SW 6	WNW 4	NW 5
22	72.2	74.7	74.3	73.7	−2.1	0.3	0.6	−0.2	1.3	−2.3	85	79	82	82	0.7	1.3	1.2	1.1	9	7	10 *	SW 3	W 6	W 1
23	73.5	75.7	78.6	75.9	3.2	4.8	6.0	5.0	6.0	0.2	91	86	82	86	0.7	1.2	1.8	1.2	10 •	10 •	10	WNW 8	W 6	W 7
24	79.4	79.3	80.2	79.6	6.2	8.2	7.1	7.2	9.1	5.5	73	65	73	70	2.6	3.9	2.8	3.1	10	9	10	W 5	W 7	W 6
25	81.5	81.9	82.2	81.9	5.8	9.8	6.7	7.2	10.6	5.2	86	65	82	77	1.3	4.5	1.7	2.5	10	9	10	W 3	W 7	W 3
26	79.7	75.1	69.0	74.6	4.9	12.0	10.9	9.7	13.8	4.4	84	37	43	55	1.4	8.8	7.4	5.9	10	6 ⊙	8	W 1	WSW 5	W 7
27	70.2	70.3	70.5	70.3	3.7	4.9	0.8	2.6	11.1	0.4	60	61	85	69	3.2	3.4	1.0	2.5	10	4	9 *	W 9	WNW 9	W 8
28	71.7	72.1	73.8	72.5	−0.9	1.2	1.2	0.7	2.0	−1.8	85	85	85	85	0.8	1.1	1.1	1.0	9 *	9 *	9	WNW 9	WNW 10	WNW 8
29	71.6	71.4	70.6	71.2	1.0	5.2	5.5	4.3	7.9	0.5	92	80	74	82	0.5	1.8	2.3	1.5	10 *	10 •	9	W 3	W 5	WSW 5
30	65.9	65.9	62.1	64.6	4.7	9.4	8.6	7.8	10.4	4.5	84	71	76	77	1.3	3.4	2.8	2.5	10 •	9	10	WSW 6	WSW 7	WSW 8
31	66.5	67.6	68.9	67.7	1.8	5.2	4.8	4.2	9.6	1.4	98	70	65	78	0.2	2.6	3.0	1.9	10 *	9	9	WNW 3	C 0	W 10
M	79.0	79.0	79.1	79.0	2.4	8.3	4.8	5.1	10.1	0.8	85	65	80	77	1.2	4.6	2.1	2.6	7.7	7.7	6.9	3.2	5.6	4.2

Kwiecień – Avril

1	70.1	65.3	67.2	67.5	−0.4	11.0	6.3	5.8	11.7	−2.5	84	59	89	77	0.9	5.4	1.0	2.4	9	9	9 •	C 0	WSW 8	WNW 6
2	70.4	69.5	65.5	68.4	3.3	4.0	5.7	4.7	7.1	3.1	79	87	94	87	1.5	1.1	0.6	1.1	9	10 •	10 •	WNW 3	ENE 1	NW 2
3	65.6	66.9	68.7	66.4	8.9	8.6	4.7	6.7	9.1	4.1	72	56	85	71	3.2	4.9	1.2	3.1	10	9	10	W 5	WNW 8	C 0
4	65.1	70.9	73.3	69.8	9.9	9.1	6.1	7.8	10.2	2.2	77	66	88	77	2.8	4.0	1.1	2.6	10	7 ⊙	10 •	WSW 6	NW 4	E 1
5	69.8	69.2	69.1	69.4	8.8	20.1	15.7	15.1	20.9	4.8	84	40	58	61	1.8	14.2	7.4	7.8	9	9	3	ENE 2	SW 5	SE 6
6	72.5	72.1	71.6	72.0	10.8	23.1	16.9	16.9	23.7	9.5	82	38	54	58	2.3	17.6	8.7	9.5	9 •	3	0	C 0	C 0	C 0
7	71.3	72.3	73.4	72.3	8.8	23.2	13.3	14.6	23.7	6.9	84	37	95	72	1.8	17.9	0.7	6.8	1	5 ⊙	10	C 0	NW 6	C 0
8	72.1	70.5	78.3	73.6	11.4	12.0	5.6	8.6	17.6	4.8	96	88	88	91	0.5	1.7	1.1	1.1	9 •	9 • (K)	10 •	SE 1	WNW 6	W 4
9	80.4	81.3	80.1	80.6	3.4	6.4	2.0	3.4	9.1	1.8	86	58	75	73	1.1	4.1	1.8	2.3	10	7	0	WNW 2	NW 2	C 0
10	75.2	72.8	69.7	72.6	2.8	8.7	7.1	6.4	10.0	−1.3	60	48	66	58	3.0	5.8	3.5	4.1	6	10	9	C 0	ENE 7	E 4
11	68.3	69.9	73.7	70.6	6.3	14.9	5.4	8.0	15.8	5.1	84	50	84	73	1.5	8.5	1.4	3.8	8	4	0	C 0	NW 2	SE 2
12	76.6	76.5	76.1	76.4	1.9	15.8	7.4	8.1	16.2	−0.7	96	39	75	70	0.3	10.9	2.6	4.6	0 ⊙	2	1	C 0	C 0	C 0
13	75.3	74.1	73.6	74.3	4.4	19.5	9.8	10.9	20.7	1.9	95	46	95	79	0.5	12.2	0.6	4.4	2	3 ⊙	0	C 0	SW 5	C 0
14	71.3	69.3	69.4	70.0	7.3	22.5	10.7	12.8	22.6	3.1	99	41	76	72	0.1	15.9	3.1	6.4	2 ⊙	8 ⊙	0	C 0	SE 7	NE 3
15	71.4	69.5	70.0	70.3	7.8	19.5	11.2	12.4	19.8	4.5	94	61	95	83	0.6	8.9	0.7	3.4	6	3	10	C 0	E 5	C 0
16	70.4	69.1	71.4	70.3	10.0	14.2	9.2	10.6	15.2	6.5	97	82	93	91	0.3	2.9	0.8	1.3	9	9 (K)	10	C 0	WNW 6	NW 3
17	72.3	72.0	72.9	72.4	8.5	15.7	8.8	10.4	16.4	5.8	94	62	89	82	0.6	6.7	1.2	2.8	9 ⊙	9	0	C 0	NW 3	C 0
18	73.1	71.6	73.3	72.7	4.7	18.4	13.0	12.3	19.6	1.5	98	50	70	73	0.1	10.7	4.5	5.1	2 ⊙	5	9	C 0	C 0	C 0
19	76.0	77.5	77.1	76.9	9.0	13.0	6.9	9.0	15.0	6.6	96	67	88	84	0.5	4.9	1.1	2.2	10	8 ⊙	0	C 0	WSW 3	C 0
20	78.7	79.2	79.6	79.2	3.1	12.5	7.5	7.6	13.5	−0.5	95	60	61	72	0.4	5.8	4.1	3.4	9 ⊙	7 ⊙	0	SE 1	ENE 6	ESE 5
21	77.4	75.7	73.5	75.5	7.1	14.4	9.8	10.3	16.0	0.6	63	36	52	50	3.7	10.5	5.8	6.7	0 ⊙	0	1	C 0	E 6	E 2
22	69.6	67.7	65.1	67.5	11.9	15.8	12.2	13.0	17.6	8.2	62	47	60	56	5.2	9.4	5.7	6.8	3	8	2	SE 8	SSE 7	SSE 8
23	69.4	69.6	69.6	69.5	10.8	13.7	12.5	12.3	16.2	9.6	60	59	59	59	5.3	6.5	5.9	5.9	8 ⊙	8	4	SE 7	SE 8	SE 4
24	65.9	68.4	69.1	67.1	11.2	17.7	10.3	12.4	18.0	9.2	67	40	66	58	4.4	12.1	4.2	6.9	4	4	0	E 2	E 6	E 4
25	70.6	70.5	70.6	70.6	4.0	11.5	7.3	7.5	12.0	2.1	93	65	81	80	0.5	4.7	1.9	2.4	4	4 ⊙	2	C 0	ESE 7	E 5
26	66.7	65.6	66.5	66.3	8.2	16.6	10.1	11.2	17.4	5.0	79	57	88	75	2.3	8.2	1.5	4.0	6 ⊙	7 ⊙	9	ESE 3	ENE 6	ESE 1
27	68.7	70.5	71.9	70.4	10.3	11.2	11.4	11.1	14.8	5.2	86	96	78	87	1.7	0.5	3.0	1.7	9	10 •	10 •	C 0	C 0	C 0
28	71.3	70.3	69.1	70.2	9.1	12.5	9.6	10.2	14.7	7.9	88	74	91	84	1.4	3.7	1.2	2.1	10 •	10	10	C 0	WSW 2	NW 1
29	68.3	68.6	69.6	68.8	7.0	12.4	10.0	9.8	16.8	4.7	97	82	84	88	0.3	2.6	1.9	1.6	4	9 •	4	C 0	ESE 3	ESE 3
30	68.1	67.5	68.3	68.0	7.2	17.7	12.2	12.3	18.3	4.8	97	50	81	76	0.3	8.0	2.6	3.6	5 ⊙	5 (K)	8	C 0	SE 4	C 0
31																								
M	71.1	70.9	71.4	71.1	7.2	14.5	9.3	10.1	16.0	4.1	85	58	79	74	1.6	7.7	2.7	4.0	6.4	6.7	5.0	1.3	4.4	2.1

Jelenia Góra — $H_s = 342\,m$ — $H_b = 343{,}9\,m$ — $h_w = 15\,m$ — Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	2.1	.	–	● 7⁵⁰ 8²⁵ ✳ – 10³⁵ ● 11¹⁵ ▽ 15⁴⁰ 19¹⁰, = 8²⁰ – 24
2	8	1.4	.	–	= 0⁰⁰ – 6²⁵
3	5	4.9	.	–	● 2³⁵ 3⁰⁵ – 6⁴⁰, 16⁴⁵ 17³⁰ – 24, = 0⁰⁰ – 24
4	7	.	.	–	● 0⁰⁰ – 4³⁰, = 0⁰⁰ – 11²⁰ = 18⁴⁰ – 20³⁰ = – 24, ⌴ 0-1 20⁰⁰ – 24
5	6	.	.	–	= 0⁰⁰ – 24, ⌴ 1-2 0⁰⁰ – 9⁰⁰
6	7	.	.	–	= 0⁰⁰ – 11³⁰, 17⁴⁵ – 24, ⌴ 0 22⁰⁰ – 24
7	6	.	.	–	= 0⁰⁰ – 11²⁰ ∞ – 17³⁵ = – 24, ⌴ 0 0⁰⁰ – 8⁰⁰
8	7	.	.	–	= 0⁰⁰ – 6⁴⁵ ≡ 1 – 9³⁵, ⌴ 1-2 20⁰⁰ – 9⁰⁰
9	8	.	.	–	= 0⁰⁰ – 5⁴⁰, 21³⁰ – 24, ⌴ 1 15⁰ – 9⁰⁰, 21⁰⁰ – 24
10	7	.	.	–	= 0⁰⁰ – 3³⁰, ⌴ 2 0⁰⁰ – 9⁰⁰
11	6	.	.	–	= 4³⁰ – 24, ⌴ 0 3⁰⁰ – 8⁰⁰
12	7	1.6	.	–	por. wiatru do 20 m/sek 23¹⁰ – 24, = 0⁰⁰ – 5⁵⁰
13	8	9.4	.	–	▽ 0 3⁴⁵ – 4²⁰ ● 0 5²⁰ – 6³⁰ 23³⁰ – 24, » 3¹⁰ – 4²⁰
14	5	4.8	.	–	● 0 0⁰⁰ 1³⁰ – 12²⁰ 16¹⁵ – 20⁴⁵ 24
15	6	0.2	.	–	● 0 0⁰⁰ . 35 – 4¹⁰ – 7²⁰, 9⁴⁰ 10³⁵, = 0⁰⁰ – 24
16	7	.	.	–	» 10³⁰ – 12⁴⁵, 13⁴⁵ 15³⁰, = 0⁰⁰ – 2³⁰
17	7	.	.	–	= 3³⁰ – 6³⁰ = 18⁴⁰ – 20²⁰, ⌴ 0 4⁰⁰ – 8⁰⁰
18	7	0.0	.	–	▽ 0 13⁵⁰ – 14¹⁰, = 16³⁰ – 20⁰⁰
19	7	2.5	.	–	▽ 0 9³⁰ – 10²⁰ ▽ 0 11⁵⁰ 14¹⁰ ✕ 15⁰⁵ – 10 ▽ 0-1 16²⁵ ▽ 0 – 19²⁰
20	8	0.8	.	–	▽ 12¹⁰ 15¹⁵ ✳ 0 21²⁰ – 24, = 1⁰⁰ – 6³⁰, ⌴ 0 1⁰⁰ – 8⁰⁰
21	7	5.9	pż.	–	✳ 0 0⁰⁰ – 4²⁰ 5¹⁵ ▽ 0-1 6³⁸ 9⁴⁸ 10³⁵ – 12⁴⁰ ▽ 0 – 13⁰⁵ ▽ 0-2 13¹⁵ – 17⁰² 24
22	8	1.9	5	–	▽ 0-1 0⁰⁰ 11³⁵ ▽ 2 11⁵⁰ – 12¹⁰ ▽ 0 15⁴⁵ ✳ 0 20⁴⁵ 21²⁰ ✳ 1-0 – 23³⁰ ● 0 – 24, ⊕ 16³⁰ – 17⁰⁵
23	6	1.3	.	–	● 0 0⁰⁰ 1³⁰ 2¹⁵ – 3³⁰ 11³⁵ ▽ 0 11⁵⁰ – 12¹⁰ ● 0 20³⁰, = 9⁰⁰ – 21³⁰
24	8	0.1	.	–	● 0 17⁴⁰ 18²⁵, = 6³⁰ – 10¹⁰ 16³⁰ – 24
25	7	0.1	.	–	● 0 5³⁵ – 6⁴⁰ ● 0 17⁵⁵ – 18¹⁰, = 0⁰⁰ – 9²⁰
26	7	0.3	.	–	● 0 0⁰⁰ 6¹⁰, = 4²⁰ – 9³⁰, 23³⁰ – 24
27	8	1.1	.	–	● 0 0¹⁰ – 2²⁵ 3¹⁰ – 5¹⁵ ▽ 0-1 10⁴⁰ 24, » na. p, = 0⁰⁰ – 5²⁰
28	5	2.7	4	–	▽ 0-1 0⁰⁰ – 11²⁵ ▽ 0 23⁴⁵ – 24, ⊣ 1 6¹⁰ – 40, » 10²⁰ – 20³⁰
29	6	2.2	.	–	▽ 0 0⁰⁰ 1¹⁵ ● 0 3²⁰ – 4¹⁵ ▽ 0-1 5⁵⁵ 7²⁰ ✳ 0 7²⁵ – 9¹⁰ ● 0 – 13¹⁵ 14²⁰, 21³⁵ – 24
30	8	2.3	.	–	● 0 0⁰⁰ . 20 – 5¹⁵ 10³⁵ ▽ 12²⁵ ● 0 16²⁰ – 20⁴⁰
31	7	0.2	.	–	● 0 1¹⁰ – 2¹⁵ ● – 3¹⁰, 4¹⁰ – 6²⁰ ✳ – 7¹⁰ ● 0 7²⁰, » 20³⁰ – 24
Σ	–	45.8	–	–	UWAGI.

Kwiecień – Avril

1	8	4.9	.	–	✳ 0 7¹⁵ . 50 ● 0 13⁴⁰ 19¹⁵ ▽ 0-1 19⁴⁰ 22⁴⁵ » 0⁰⁰ – 3³⁰ 10⁴⁰ – 12²⁰
2	8	5.5	.	–	● 0 0³⁰ 5⁴⁰ ▽ 0 8⁴⁰ – 9¹⁵ ● 0 9³⁵ 13¹⁰ – 15³⁵ 16³⁵ – 24
3	7	0.8	.	–	● 0 0⁰⁰ – 2⁴⁰, 5¹⁵ – 6⁰⁵ ▽ 0-1 7³⁰ – 9²⁰, = 20³⁰ – 24
4	7	2.2	.	–	● 0 3¹⁰ 5²⁰ 7²⁵ – 8¹⁰ 20⁴⁰ – 24, = 0⁰⁰ – 3³⁰, 9³⁰ – 12²⁰, 16⁴⁰ – 24
5	8	0.0	.	–	● 0 0⁰⁰ – 3⁴⁰, = 0⁰⁰ – 6³⁰
6	8	0.0	.	–	▽ 6⁴⁵ – 7¹⁰
7	8	5.9	.	–	● 0 16⁰⁴ – ⁴⁵ 17⁵⁰ – 19³⁰, ◹ 15⁴⁸ – 16¹⁰ – 16⁴⁰ NE-SE, ⌓ 0 2⁰⁰ – 8⁰⁰
8	8	4.1	.	–	● 0 1¹⁵ 3⁴⁰ ▽ 1-0 5⁴⁰ – 7¹⁰ ▽ 0 11³⁰ 13¹⁰ – 15¹⁰ – 21⁴⁰, ◹ 0 12⁰⁸ – 12⁴⁵ – 13²⁰ NW-SE
9	8	.	.	–	= 6¹⁰ – 9³⁰
10	8	0.2	.	–	● 0 19⁴⁰ 20¹⁵ – 23¹⁰ – 24, ⌴ 0 1⁰⁰ – 7⁰⁰, ⊕ 7³⁰ – 11¹⁵ 14⁴⁰ 15¹⁵
11	7	.	.	–	● 0 0⁰⁰ 4⁴⁰, = 21³⁰ – 24, ⌓ 0 21⁰⁰ – 24
12	8	.	.	–	= 0⁰⁰ – 8³⁰, ⌓ 1 0⁰⁰ – 9⁰⁰
13	6	.	.	–	= 3¹⁵ – 9³⁰ ∞ – 14²⁰ = 18²⁵ – 24, ⌓ 0 1³⁰ – 9⁰⁰ ⌓ 0-1 20⁰⁰ – 24
14	8	.	.	–	= 0⁰⁰ – 7³⁰, ⌓ 1 0⁰⁰ – 9⁰⁰
15	7	5.3	.	–	▽ 0 18³⁰ – 56 ▽ 2 – 19¹⁰ ▽ 0 – 20⁴⁵ (◹) 0 14⁴⁵ – 18³⁰ ◹ 0 18³⁰ – 19⁰⁰ – 20⁴⁰ WNW, NW-SE, = 5¹⁰ 9³⁰ np, ⌓ 1⁰⁰ – 10⁰⁰
16	6	23.2	.	–	▽ 13²⁵ – 17⁰⁷ ● 0 17⁴⁰ – 18³⁵ (◹) 12⁵³ – 13²⁵ ◹ 13²⁵ – 14²⁰ – 15⁴⁰ W-E, = 0⁰⁰ – 24
17	7	.	.	–	= 0⁰⁰ – 11¹⁰ 23¹⁰ – 24, ⌓ 0 21⁰⁰ – 24
18	8	0.2	.	–	▽ 0 15⁴⁵ – 16¹⁵ 21⁴⁵ – 50, = 0³⁰ – 4⁴⁵ ≡ 1 – 5³⁰ ≡ 1 – 6³⁰ = a, np, ⌓ 0-2 0⁰⁰ – 10⁰⁰
19	7	.	.	–	● 0 0⁵⁷ 1³⁰, = 0⁰⁰ – 11³⁵ = 21⁴⁵ – 24, ⌓ 1 19⁰⁰ – 24
20	8	.	.	–	= 0⁰⁰ – 3³⁰ = – 4³⁰ = – 5²⁰, ⌓ 1 0⁰⁰ – 10⁰⁰
21	8	.	.	–	⌓ 0 3⁰⁰ – 10⁰⁰, 22⁰⁰ – 24
22	8	.	.	–	⌓ 0 0⁰⁰ – 8⁰⁰
23	8	.	.	–	
24	8	.	.	–	
25	7	.	.	–	= 18³⁰ – 24, ⌓ 0 2⁰⁰ – 8⁰⁰
26	7	.	.	–	= 0⁰⁰ – 11³⁰ ⌓ 0 3⁰⁰ – 9⁰⁰
27	5	5.5	.	–	▽ ◹ 0 10⁵⁰ – 11³⁰ – 12⁴⁵ W-E ▽ 0 – 14⁴⁰ ● 0 19⁵⁰ 22¹⁵, = a, p – 24
28	6	0.2	.	–	● 0 5³⁰ 9¹⁰, = 0⁰⁰ – 13²⁰ 23¹⁵ – 24, ⌓ 0 21⁰⁰ – 24
29	7	0.3	.	–	▽ 0 11⁴⁵ 19¹⁰, = 0⁰⁰ – 1⁴⁰ ≡ 0 – 3⁴⁵ = – 8²⁵, ⌓ 1-2 0⁰⁰ – 9⁰⁰
30	7	0.8	.	–	▽ 0-1 22⁵⁰ – 24, (◹) 12¹⁵ – 13⁴⁰ S, ◹ 19⁴⁰ – 22¹⁵, = na = na ≡ 0-1 3⁴⁰ – 6¹⁵ = a, ⌓ 2-0 a
31					
Σ	–	62.1	–	–	UWAGI.

Jelenia Góra — φ = 50°54' — λ = 15°48' — Maj - Mai 1961

DNI	CIŚNIENIE P — 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	71.0	71.7	73.5	72.1	9.9	14.6	10.0	11.1	16.8	9.0	92	73	96	87	1.0	4.5	0.5	2.0	10	9	10	W 2	NW 4	C 0
2	72.9	71.9	71.4	72.1	10.0	15.2	10.1	11.4	15.7	6.1	96	60	90	82	0.5	7.0	1.3	2.9	10	9	9	C 0	W 1	C 0
3	69.7	69.8	73.6	71.0	10.9	16.1	9.7	11.6	17.2	7.1	87	57	97	80	1.6	7.9	0.3	3.3	4	9	8	C 0	W 3	C 0
4	76.1	76.4	76.5	76.3	7.3	16.8	9.5	10.8	17.2	2.5	97	46	95	79	0.3	10.3	0.7	3.8	4	9	8	C 0	NW 1	C 0
5	75.0	73.8	73.5	74.1	11.1	19.3	17.5	16.2	20.9	5.3	97	53	70	73	0.3	10.6	5.8	5.6	9	10	0	C 0	ESE 6	S 3
6	72.1	76.2	77.1	75.1	16.9	12.6	10.2	12.5	18.1	9.8	77	93	96	89	4.4	1.1	0.4	2.0	6	10	9	SW 3	NW 3	C 0
7	76.2	73.5	74.4	74.7	13.1	15.8	7.3	10.9	17.0	6.8	85	56	80	74	2.3	7.9	2.0	4.1	4	9	0	C 0	WSW 6	WSW 4
8	74.3	73.5	73.6	73.8	9.8	12.7	5.6	8.4	14.1	4.0	70	48	86	68	3.6	7.7	1.3	4.2	9	8 ⊙	9	WSW 6	W 8	SW 2
9	68.9	66.9	68.9	68.2	7.7	10.7	7.2	8.2	11.1	4.7	73	70	86	76	2.8	3.9	1.5	2.7	9 •	9 ⊙	10	WSW 5	W 7	WNW 5
10	71.7	73.5	75.5	73.6	6.6	7.5	5.1	6.1	9.2	4.7	95	86	94	91	0.7	1.5	0.6	0.9	10	10	10 •	WNW 7	W 7	W 4
11	76.1	76.9	80.3	77.8	4.9	9.0	6.4	6.7	10.3	3.9	94	76	92	87	0.6	2.8	0.7	1.4	10 •	8 ⊙	10 •	W 3	NW 4	NW 4
12	80.7	77.8	77.5	78.7	6.0	7.5	3.4	5.1	9.2	3.0	85	80	97	87	1.5	2.1	0.3	1.3	10	10 •	8	C 0	WNW 5	C 0
13	75.7	73.8	72.8	74.1	6.4	8.5	5.3	6.4	12.1	1.4	82	85	97	88	1.7	1.7	0.3	1.2	8	10 •	7	C 0	SW 2	C 0
14	71.3	71.5	71.6	71.5	6.3	9.4	4.2	6.0	10.0	3.7	73	51	82	69	2.5	5.7	1.4	3.2	9	9	6	W 5	WNW 6	SE 1
15	73.3	74.1	75.2	74.2	7.0	10.0	7.2	7.8	10.3	2.4	91	63	86	80	0.9	4.5	1.5	2.3	10 •	9	9	WNW 5	WNW 5	WNW 3
16	75.0	73.9	72.6	73.8	6.6	10.6	7.3	8.0	12.0	2.2	88	59	94	80	1.1	5.2	0.6	2.3	9	6	10 •	NW 1	W 6	NW 6
17	75.5	77.3	78.8	77.2	5.7	7.8	8.2	7.5	8.5	5.6	98	86	97	94	0.2	1.5	0.3	0.7	10 ≡	10 •	10	NW 4	NW 3	W 2
18	79.7	79.2	77.5	78.8	6.1	12.1	8.6	8.8	14.2	2.0	95	55	89	80	0.4	6.3	1.3	2.7	9	6	8	NW 3	WNW 4	C 0
19	76.4	75.0	73.7	75.0	8.9	14.2	8.3	9.9	14.7	4.9	88	50	94	77	1.4	8.1	0.7	3.4	8	10	9	C 0	W 3	SE 2
20	71.0	68.9	68.5	69.5	8.9	12.5	7.2	9.0	14.5	5.9	92	69	94	85	0.9	4.5	0.6	2.0	5 ⊙	8 ⊙	4	C 0	NW 3	S 2
21	69.8	69.0	72.1	70.3	8.4	15.2	9.3	10.6	16.0	4.6	92	58	95	82	0.9	7.3	0.6	2.9	9	9	9	C 0	W 3	C 0
22	73.1	73.2	73.3	73.2	9.4	14.7	7.4	9.7	15.5	7.3	95	56	87	79	0.6	7.3	1.3	3.1	10	9	2	WNW 2	NNW 3	C 0
23	73.9	74.1	74.0	74.0	7.1	14.6	8.4	9.6	16.6	2.0	91	44	93	76	0.9	9.3	0.7	3.6	9	9	9	C 0	SE 2	SE 2
24	76.3	76.2	75.9	76.1	8.9	15.4	9.1	10.6	16.6	4.6	89	61	92	81	1.2	6.9	1.0	3.0	7	9	6	C 0	W 4	C 0
25	76.1	74.6	73.2	74.6	7.5	18.3	10.7	11.8	19.6	3.0	100	49	82	77	0.0	10.8	2.3	4.4	4 ⊙	2	0	C 0	NW 3	C 0
26	72.4	70.5	68.1	70.3	10.1	20.2	15.3	15.2	21.5	4.8	92	51	64	69	1.0	11.5	6.3	6.3	8	7 ⊙	9	C 0	E 6	C 0
27	68.8	70.3	70.3	69.8	14.7	11.5	10.4	11.8	17.3	10.4	77	91	97	88	3.8	1.2	0.3	1.8	9	10	10	NW 2	NNW 2	C 0
28	71.4	72.2	71.7	71.8	5.8	6.2	6.0	6.0	10.8	5.4	94	95	94	94	0.6	0.5	0.6	0.6	10 •	10 •	10	W 3	WNW 3	C 0
29	65.2	61.8	59.9	62.3	6.3	8.5	8.9	8.2	9.1	5.7	97	93	96	95	0.2	0.8	0.5	0.5	10 •	10 •	10 •	E 1	E 2	W 3
30	60.8	62.5	63.8	62.4	7.8	11.1	9.1	9.3	12.3	7.6	94	73	89	85	0.6	3.6	1.3	1.8	10 •	10	10	WNW 3	SW 3	C 0
31	64.2	64.4	64.2	64.3	10.4	14.4	10.8	11.6	15.7	7.5	74	49	82	68	3.3	8.4	2.3	4.7	9	8 ⊙	8	ENE 3	WSW 2	SE 2
M	72.8	72.4	72.7	72.6	8.6	12.7	8.5	9.6	14.3	5.0	89	66	90	82	1.3	5.6	1.3	2.7	8.3	8.7	7.6	1.8	3.9	1.5

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1	64.4	63.9	62.8	63.7	11.2	23.7	17.1	17.3	24.7	5.6	84	46	68	66	2.1	15.9	6.2	8.1	0 ⊙	5 ⊙	9	C 0	E 4	E 2
2	63.2	65.6	67.5	65.4	17.9	22.9	13.7	17.0	24.1	11.2	66	34	85	62	7.1	18.4	2.3	9.3	3	2	2	ENE 1	W 6	C 0
3	69.5	69.8	70.8	70.0	13.4	17.0	13.8	14.5	19.2	8.9	74	69	97	80	4.0	6.0	0.6	3.5	7 ⊙	7 ⊙(R)	10	NW 3	W 4	C 0
4	71.2	71.9	73.3	72.1	14.4	17.3	13.6	14.7	21.5	11.9	97	88	94	93	0.6	2.4	0.9	1.3	10 •	10	10	NW 3	WNW 3	C 0
5	74.8	74.0	74.5	74.4	14.9	22.1	15.7	17.1	23.1	12.8	92	56	88	79	1.3	11.7	2.1	5.0	10	7	7	C 0	NNE 4	C 0
6	73.7	72.4	70.4	72.2	15.8	20.8	17.8	18.0	21.6	9.2	87	64	85	78	2.2	8.8	3.4	4.8	7 ⊙	9 ⊙	9	C 0	E 7	E 2
7	69.9	68.8	68.3	69.0	15.0	18.8	16.9	16.9	22.6	10.6	96	75	91	87	0.7	5.3	1.8	2.6	9	9 • (R)	9 • (R)	C 0	W 5	C 0
8	70.3	71.9	73.2	71.8	14.9	17.8	15.7	16.0	20.0	12.8	98	81	89	89	0.3	3.8	1.9	2.0	10	10 (R)	10	C 0	WNW 5	C 0
9	72.6	72.9	71.1	72.2	15.6	18.1	15.9	16.4	19.7	11.6	92	84	93	90	1.3	3.3	1.4	2.0	10	10	6	E 1	ESE 3	SE 2
10	70.3	72.3	75.6	72.9	18.8	20.5	11.9	15.8	21.4	11.8	73	69	96	79	5.9	7.3	0.5	4.6	9 ⊙	9	10 •	SE 3	W 4	WNW 3
11	75.8	75.6	74.3	75.2	11.6	14.1	14.1	13.3	16.7	10.0	99	88	95	94	0.1	2.0	0.7	0.9	10 •	10	10	WSW 2	NW 3	C 0
12	72.9	71.8	72.1	72.3	12.4	18.1	13.4	14.3	18.8	12.0	93	59	87	80	1.0	8.4	2.0	3.8	9	9	7	NW 2	NW 2	C 0
13	69.1	65.3	63.9	66.1	13.7	18.2	12.3	14.1	19.7	5.2	78	51	93	74	3.3	10.2	1.0	4.9	9 ⊙	9	7	C 0	SE 6	SSW 4
14	67.3	70.6	74.7	70.9	11.0	15.4	11.3	12.4	15.9	9.3	92	69	93	85	1.0	3.3	1.0	2.3	10 •	9	10	W 7	W 6	WNW 5
15	76.6	76.6	78.0	77.1	10.1	13.8	9.6	10.8	16.0	9.2	77	58	83	73	2.9	6.7	2.1	3.9	10	7 ⊙	2	W 4	NW 6	NW 2
16	79.1	78.9	79.8	79.3	9.8	16.7	9.6	11.4	18.6	3.8	84	50	87	74	1.9	9.6	1.6	4.4	10	2 ⊙	3	C 0	NW 4	C 0
17	81.1	80.3	79.9	80.4	11.6	19.9	13.7	14.7	21.9	2.5	75	45	89	70	5.4	12.8	1.8	6.0	0 ⊙	7 ⊙	10	C 0	W 1	C 0
18	79.0	77.5	76.3	77.6	14.5	24.5	18.7	19.1	26.0	6.8	82	38	70	63	2.9	19.1	6.5	9.5	0 ⊙	1 ⊙	0	C 0	SW 6	NW 2
19	78.7	81.2	83.4	81.1	17.0	17.6	15.9	15.6	18.7	11.8	95	75	76	81	1.4	4.9	3.9	3.4	10 •	8	4	C 0	NW 4	W 1
20	87.4	87.0	85.0	86.5	10.6	17.0	10.7	12.2	19.1	4.5	88	47	84	73	1.5	10.2	2.1	4.6	4 ⊙	3 ⊙	0	C 0	NW 4	C 0
21	82.4	80.7	84.4	82.5	11.1	22.6	12.8	14.8	22.9	3.0	81	44	87	71	2.4	15.2	1.9	6.5	4	7	3	C 0	WSW 4	C 0
22	82.8	78.3	73.5	78.2	12.5	23.9	19.2	18.7	25.8	3.8	87	53	77	72	1.9	13.9	5.0	6.9	4	3	10 (R)	C 0	S 3	C 0
23	78.9	80.0	80.1	79.7	15.8	20.4	14.3	16.2	22.0	12.2	79	49	89	72	3.7	12.2	1.8	5.9	2 ⊙	2 ⊙	7	W 3	NW 7	SE 2
24	80.7	81.6	80.0	80.8	14.3	21.7	15.6	16.8	24.9	7.0	88	48	87	74	2.0	13.5	2.3	5.9	6	9	0	SE 1	NW 7	SE 2
25	79.3	76.9	74.4	76.9	15.3	27.1	19.5	20.4	28.2	8.6	82	37	73	64	3.2	22.6	6.1	10.6	0	1	2	C 0	NW 1	C 0
26	74.3	73.6	70.8	72.9	17.6	25.5	18.3	19.5	26.7	11.3	83	65	83	77	3.4	10.1	3.3	5.7	8	10	5	SE 2	NW 4	SE 1
27	68.1	69.0	71.7	69.6	19.2	24.2	18.0	19.8	26.1	12.6	89	58	76	74	2.3	12.8	4.8	6.6	9	8	8	SSE 2	SW 2	W 8
28	80.8	85.3	88.0	84.7	11.3	15.9	11.7	12.6	18.1	10.7	84	49	75	69	2.2	9.2	3.4	4.9	9	7	2	WNW 7	WNW 7	WNW 2
29	89.7	89.1	87.7	88.8	13.5	20.3	13.3	15.1	21.9	6.8	77	49	84	70	3.5	12.1	2.5	6.0	2	3	3	C 0	NW 4	NE 1
30	88.4	86.9	86.0	87.1	13.7	24.2	15.8	17.4	24.7	5.8	80	45	80	70	2.3	16.6	3.5	7.5	0 ⊙	1 ⊙	0	C 0	E 3	SE 1
31																								
M	75.8	75.7	75.7	75.7	14.0	19.9	14.6	15.8	21.7	8.7	85	58	85	76	2.4	10.4	2.6	5.1	6.4	6.5	5.8	1.4	4.3	1.3

Jelenia Góra $H_s = 342\ m$ $H_b = 343{,}9\ m$ $h_w = 15\ m$ **Maj – Mai 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	6.4	.	–	▽° 0⁰⁰–2¹⁰ •²⁻¹ 17⁴² 19¹⁵ . = 4³⁰–16²⁰ 20²⁵–24
2	6	0.1	.	–	•° 13²⁵–⁴⁰ 16⁴⁵ 17¹⁰ (K) 16⁵⁰ 18³⁵ E . = 0⁰⁰–P, p–24
3	8	7.9	.	–	▽° 10⁵⁰ 12²⁵ 15³⁵–16³⁵ 19¹⁰–20²⁵ (K) 15³⁰⁻³⁵ K° 15³⁵–15⁴⁵–16⁰⁰ W-E . = na, p–23⁴⁵ =°–24
4	7	1.2	.	–	=° 0⁰⁰–1¹⁵ =°–5⁴⁵ =–6³⁰ 19⁴⁰–24 ; ⌓² 21⁰⁰–24
5	8	0.0	.	–	▽° 1¹³⁰⁻⁴⁰ = 0⁰⁰–5²⁰ ⌓² 0⁰⁰–9⁰⁰
6	6	1.0	.	–	•° 3⁴⁰–4¹⁵ 10²⁰–11⁴⁵ . = a–p, p, np = 19³⁰–20⁴⁵ ⌓° 19⁰⁰–24
7	8	1.3	.	–	▽° 16⁵⁰–18¹⁵ . = na . ⌓ 0⁻¹ 0⁰⁰–9⁰⁰ ⌒ 18³⁵–19¹⁰
8	8	5.7	.	–	•° 2⁵⁰ 4²⁰ •° 5¹⁵⁻⁵⁰ 10¹²⁻³⁵ •⁰⁻¹ 15³⁵ 17¹⁰ ▽° 19⁰⁵ 20¹⁵ . = na
9	8	16.5	.	–	•° 1²⁰ 16¹⁵ •¹ 17²⁵ 18⁴⁰ ▽° –18⁴⁵ 19²⁰ 20¹⁵ . 22²⁰⁻³⁵
10	6	20.6	.	–	•° 1¹⁰⁻³⁰ 3²⁵⁻⁵⁰ •° 7²⁰–12²⁵ ▽⁰⁻¹ 15⁴⁰ 24 . = 4¹⁵–14²⁰ ⌒ 18⁴⁰⁻⁵²
11	8	6.5	.	–	▽° 0⁰⁰ 1²⁰ •° 3²⁵ 4¹⁰–9¹⁵ ▽° 9³⁰ 12⁰⁵ 15³⁵ 24 . = 3¹⁰–9²⁰
12	7	4.3	.	–	•° 0⁰⁰ 1⁰⁵ 12¹⁵ 15³⁰ 17²⁵ 18³⁵ . = 20¹⁵–24
13	6	2.0	.	–	•° 11¹⁰ 12¹⁵ •¹–13¹⁰ ▽° 16⁵²–17¹⁰ 17⁴⁵ 18¹⁵ . = na, p–24
14	7	0.1	.	–	=° 0⁰⁰–5³⁵ ⌓° 21⁰⁰–24
15	7	0.4	.	–	•° 5⁰⁵ 7²⁰ ▽° 11³⁰ 12²⁰ 14⁰⁵⁻³⁰ 18⁵⁵ 19⁰⁵ . = a, np; ⌓° na
16	8	20.4	.	–	▽° 13⁰⁵–¹⁵ 16⁴⁵ 19¹⁰ •¹⁻⁰ 19²⁰–24 . = 0⁰⁰–7³⁰
17	6	4.4	.	–	•° 0⁰⁰–4¹⁵ 6³⁵ •°–7⁴⁰ •° ▽° 12²⁰ 16¹⁰ . = 6⁵⁰–8⁴⁰ =. == a–np ='23⁴⁰–24
18	8	.	.	–	='0⁰⁰–4²⁰ =°–5⁴⁰ =–8³⁰ . ⌓° 20⁰⁰–24
19	8	0.1	.	–	= 20²⁰–24 . ⌓ 0⁻¹ 0⁰⁰–10⁰⁰
20	6	0.3	.	–	•° 3²⁵ 4¹⁵ ▽° 9⁵⁰–10¹⁰ 15⁵⁰–16¹⁵ . = na–p, p–np = 21²⁰–22³⁰ ==–24 . ⌓² 21⁰⁰–24
21	7	3.3	.	–	▽°⁻¹ 12¹⁵ 17¹⁰ = 19⁰⁰ 4⁴⁰ =–12⁴⁰ 18³⁰–24 ⌓²¹ 0⁰⁰–9⁰⁰
22	7	.	.	–	= 0⁰⁰–9³⁰ 22³⁰–24 ; ⌓° 19⁰⁰–24
23	8	.	.	–	= 0⁰⁰–5³⁰ . ⌓ 0⁻¹ 0⁰⁰–9⁰⁰ ⌓° 21⁰⁰–24
24	7	.	.	–	= 3²⁰–11²⁰ 19⁴⁰–21⁴⁰ ==–24 . ⌓¹ 0⁰⁰–10⁰⁰ . 21⁰⁰–24
25	6	.	.	–	== 0⁰⁰–4⁴⁵ =²–6⁴⁰ =–10¹⁵ ∞–13³⁰ = np . ⌓¹⁻² 0⁰⁰–9⁰⁰ ⌓° 20⁰⁰–24
26	7	.	.	–	= 0⁰⁰–8⁵⁰ . ⌓ 0⁻¹ 0⁰⁰–9⁰⁰
27	5	14.0	.	–	•¹²⁰ 15⁴⁰ •° –16³⁰ •°K 16⁵⁰–18²⁰ •°–24 = 9¹⁵–24
28	5	5.8	.	–	•° 0⁰⁰–4⁴⁰ •°–6²⁵ •°–11²⁰ 14⁴⁰ •° 14⁵⁰ 16¹⁵–17⁴⁵ . = 0⁰⁰–24
29	5	27.3	.	–	•° 6¹⁵–8¹⁵ 9³⁵ •°–11²⁰ 12⁴⁰ 14¹⁵ •⁰⁻¹–24 . = 0⁰⁰–24
30	8	1.4	.	–	•° 0⁰⁰–3³⁵ 7²⁰ 10¹⁵ . = 0⁰⁰–10²⁰ 22³⁰–24
31	8	0.0	.	–	•° 10⁴⁵ 11¹⁰ . 18⁴⁰–19²⁰ . = 0⁰⁰–7³⁰ . ⌓² 23⁰⁰–24
Σ	—	151.0	—	–	UWAGI:

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1	8	.	.	–	=²²⁰–3³⁰ =–9³⁰ ⌓² 0⁰⁰–10⁰⁰
2	8	.	.	–	⌓° 3⁰⁰–10⁰⁰ 21⁰⁰–24
3	8	7.8	.	–	▽° 17⁵⁰ 19⁴⁰ •° 22⁴⁵–24 (K) 11⁴⁶–15⁴⁰ K° 18⁴⁸–19⁴⁰ E-W . ⌓° 0⁰⁰–9⁰⁰
4	5	0.2	.	–	•⁰⁻³ 6⁴⁰ 7¹⁰–8⁴⁰ (K) 16⁵⁰–17⁵⁰ •°K°–18⁴⁵ W-E . = 2⁴⁰–16¹⁰
5	7	0.4	.	–	(K) 15³⁰–⁴⁵ •K°–17²⁰ = 0⁰⁰–11³⁰
6	7	0.0	.	–	•° 20¹⁰–²⁰ (K) 17¹⁰–18³⁵ NW < 21⁴¹–24 = 1²⁰–8⁴⁰
7	7	6.9	.	–	(K) 12¹⁵–13⁴⁸ •¹K–17⁴⁰ NW-SE (K) 19⁵⁰–21³⁵ •K°–22³⁵ ▽°23⁰⁸⁻⁵⁰ . = n–a ⌓⁻⁸ 0⁰⁰–10⁰⁰
8	6	6.4	.	–	▽° 0¹⁰–1²⁵ ▽¹⁻⁰ 8⁵⁰–10⁴⁰ K° 8³⁵–10³⁰ W-E (K) 13⁴⁵–15³⁵ . = na, a–24 == na =°–a
9	7	3.0	.	–	▽⁰⁻⁰ 10¹⁵–11⁴⁰ •° 12⁴⁰–13²⁰ 14⁰⁵⁻²⁵ = 0⁰⁰–12²⁰ p–24 . ⌓° 2⁰⁰–10¹⁵
10	7	11.1	.	–	▽⁰⁻¹ •° 13¹⁵–24 K° 19³⁵–20¹⁵–20⁴⁰ W-E . = 0⁰⁰–6²⁰ 11³⁰–13¹⁰ 19¹⁰–24
11	5	2.7	.	–	•° 0⁰⁰–3²⁵ 6¹⁵–8³⁵ •• •°–9⁴⁰ •°–10³⁵ . = 0⁰⁰–24
12	7	0.4	.	–	•° 1¹⁵ 2¹⁵ •⁰⁻¹ 5⁰⁵ 6¹⁰ 7²⁰ •¹²¹⁵⁻²⁸ 15³⁵ 17⁰⁵ = na . ⌓¹ p–24
13	8	3.3	.	–	•³ 15¹⁵⁻³⁰ 19³⁵–20³⁵ . == 0⁴⁵–2³⁰ =–8³⁵ . ⌓¹⁻² 0⁰⁰–10⁰⁰
14	7	3.3	.	–	▽°⁵²⁵ 20²⁰ . = 9²⁰–11⁴⁵ 20²⁰–24
15	7	.	.	–	▽°¹⁵⁵–2³⁰ . = 0⁰⁰–5¹⁵ . 21³⁰–24
16	7	.	.	–	= 0⁰⁰–7³⁰ . ⌓²⁻⁰ na–11⁰⁰–22⁰⁰–24
17	7	.	.	–	= 0³⁰–6³⁰ 20⁴⁰–24 . ⌓⁰⁻¹ 0⁰⁰–8⁰⁰ ⌓² 22⁰⁰–24
18	7	0.0	.	–	= 0⁰⁰–11³⁰ S¹–15³⁰ ∞¹–22³⁰ =–24 . ⌓² 0⁰⁰–8⁰⁰
19	7	3.2	.	–	•° 7⁴⁰ 8¹⁰–12²⁰ . = 0³⁰–13³⁰ = 22¹⁵–24 . ⌓¹ 0⁰⁰–7⁴⁰
20	8	.	.	–	= 0³⁰–7¹⁵ == 0⁰⁰⁻³⁰ . ⌓° 3⁰⁰–4⁰⁰ ⌓¹–10⁰⁰
21	7	.	.	–	= ¹⁵–2²⁰ ==–5³⁰ S 16³⁰–21³⁰ =–24 . ⌓¹⁻² 0⁰⁰–9⁰⁰ 22⁰⁰–24
22	7	2.7	.	–	(K) S 21⁴⁵–22¹⁰ •K°–23⁴⁰ (K)–23⁵⁰ == 0⁰⁰–3⁴⁰ ==–5⁴⁰ =–7³⁰
23	7	.	.	–	▽° 0⁰⁵⁻⁴⁵ = 2⁰⁰–12¹⁵ = 21³⁰–24 ; ⌓° 22⁰⁰–24
24	7	.	.	–	= 0⁰⁰–6²⁰ =–10³⁰ 23³⁰–24 . ⌓¹ 0⁰⁰–9⁰⁰
25	7	.	.	–	= 0⁰⁰–2³⁰ =–6³⁰ =–10¹⁰ . ⌓¹ 0⁰⁰–10⁰⁰ ⌓° 22⁰⁰–24
26	6	.	.	–	= 13³⁰–17³⁰ S¹–20³⁰ . ⌓° 0⁰⁰–6⁰⁰ 22⁰⁰–24
27	8	4.3	.	–	•° 9⁴⁰ 10²⁰ (K) 15⁵⁴–16⁴⁵ •¹K°–17²⁵ W-E ▽°20⁵⁰ 21¹⁵ . 23⁴⁰–24 . = 0⁰⁰–3³⁰ . ⌓¹ 0⁰⁰–8⁰⁰
28	8	.	.	–	▽²⁰⁰⁻⁴⁰ 4¹⁵⁻³⁵ 6⁴⁵–7¹⁵ . = 5³⁰–8²⁰ . ⌓° 22⁰⁰–24
29	8	.	.	–	= 0³⁰–7³⁰ 22³⁰–24 . ⌓⁰⁻¹ 0⁰⁰–9⁰⁰ ⌓² 21⁰⁰–24
30	8	.	.	–	= 0⁰⁰–6³⁰ . ⌓² 0⁰⁰–7⁰⁰ . 23⁰⁰–24
31					
Σ	—	95.9	—	–	UWAGI:

Jelenia Góra — φ = 50°54' — λ = 15°48' — Lipiec – Juillet 1961

Dni	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	85.9	84.8	84.0	84.9	16.5	26.0	18.0	19.6	27.7	7.1	80	37	78	65	3.6	21.2	4.4	9.7	0 ○	1 ⊙	1	C 0	E 1	C 0
2	85.7	82.6	81.2	82.5	17.5	28.0	19.0	20.8	28.9	9.5	79	31	75	62	4.1	26.2	5.6	12.0	0	1 ⊙	0	C 0	C 0	C 0
3	80.1	78.5	77.1	78.5	19.0	30.4	20.9	22.8	30.5	8.7	75	28	71	58	5.4	31.4	7.2	14.7	0 ⊙	4 ⊙	8	C 0	WSW 4	W 2
4	74.5	70.2	70.9	71.9	17.7	25.7	14.8	18.2	26.2	14.6	89	40	65	65	2.2	19.9	5.9	9.3	10	4 ⊙	8	C 0	W 5	WSW 4
5	75.2	75.1	76.1	75.5	11.1	14.5	8.8	10.8	16.8	8.6	69	39	92	67	4.0	10.0	0.9	5.0	10	7	7	W 5	WSW 5	W 1
6	77.3	79.6	81.8	79.6	10.6	12.5	11.9	11.7	14.8	8.4	68	69	84	74	4.1	4.5	2.1	3.6	9	9	9	W 4	WSW 8	WSW 2
7	82.3	82.1	81.8	82.1	11.9	15.3	9.4	11.5	16.9	7.7	69	48	84	67	4.3	9.0	1.9	5.1	5	8	9	WNW 3	WNW 5	C 0
8	81.1	79.5	76.0	78.9	9.7	19.3	11.9	13.2	20.1	2.0	86	42	80	69	1.7	13.0	2.8	5.8	8 ○	8	4	C 0	WNW 2	ESE 2
9	70.5	72.3	74.3	72.4	13.6	13.8	12.1	12.9	17.0	5.7	81	79	96	85	3.0	3.4	0.5	2.3	10 •	9	9	SW 1	W 7	S 2
10	73.0	73.7	75.4	74.0	11.8	15.7	9.6	11.7	17.1	6.7	90	53	82	75	1.3	8.4	2.2	4.0	9	9	1	C 0	W 7	C 0
11	75.0	74.6	72.2	73.9	10.3	20.7	16.2	15.8	22.9	4.4	91	57	84	77	1.1	10.5	2.9	4.8	10	8 ⊙	9	C 0	S 2	NE 2
12	70.6	69.1	65.3	68.3	18.9	25.9	19.6	21.0	28.0	12.3	71	52	73	65	6.3	16.0	6.1	9.5	1	7	7	SE 2	ENE 3	SE 2
13	59.0	59.7	60.9	59.9	20.7	16.7	14.0	16.4	24.3	13.7	70	87	94	84	7.4	2.5	0.9	3.6	3	10	10	ESE 6	WNW 5	NE 1
14	66.8	68.0	68.1	67.6	12.3	17.9	17.4	16.2	20.3	11.6	62	40	55	52	5.4	12.4	9.0	8.9	10	7	9	WSW 7	WSW 5	N 1
15	70.3	71.3	71.9	71.2	16.2	22.4	17.4	18.4	23.5	14.2	76	54	70	60	4.4	17.8	6.1	9.4	6	5	10 •	WSW 3	W 6	C 0
16	70.8	70.6	71.1	70.8	14.8	20.6	11.0	14.4	21.8	10.7	78	59	95	71	3.6	14.7	0.6	6.3	5 ⊙	7 ⊙	7	C 0	W 3	SE 2
17	67.9	68.3	70.3	68.8	11.7	16.1	12.1	13.0	16.6	6.1	89	60	84	78	1.5	7.4	2.2	3.7	9	9	9	S 1	W 3	W 4
18	70.0	69.1	69.2	69.4	13.2	17.5	11.3	13.3	18.2	10.7	80	64	99	81	3.0	7.2	0.2	3.5	10	8	10 •	WNW 5	SSW 6	C 0
19	69.7	69.0	69.7	69.5	11.7	14.4	10.5	11.8	17.2	9.2	98	89	96	94	0.3	1.8	0.5	0.9	10	9	4	C 0	S 2	C 0
20	70.9	71.9	73.3	72.0	10.3	15.5	14.3	13.7	18.9	5.9	96	80	75	84	0.5	3.5	4.1	2.7	8	9	9	SE 1	W 2	W 3
21	73.6	74.6	74.6	74.3	13.5	13.8	13.2	13.4	15.4	12.6	85	77	83	82	2.3	3.7	2.6	2.9	9 •	10	10	W 4	W 6	W 4
22	73.8	74.5	74.8	74.4	13.0	14.8	11.8	12.8	16.2	11.0	89	77	81	82	1.6	3.8	2.6	2.7	10	9	7	W 6	W 5	WSW 2
23	76.2	77.4	79.6	77.7	12.1	13.9	12.9	13.0	15.4	6.0	87	76	78	80	1.8	3.9	3.3	3.0	7	10	9	W 2	WNW 5	W 2
24	81.8	83.4	84.8	83.3	12.5	14.2	12.3	12.8	15.2	10.9	79	65	79	74	3.0	6.0	3.0	4.0	9	10	10	W 6	NW 3	C 0
25	86.3	86.3	84.7	85.8	11.3	14.2	9.8	11.3	17.2	9.6	88	66	92	82	1.7	5.4	0.9	2.7	10	10	1	C 0	WNW 3	C 0
26	82.0	77.9	73.5	77.8	10.2	21.9	14.5	15.5	23.5	5.7	91	57	84	71	1.1	16.6	2.7	6.8	0 ⊙	8	3	C 0	S 5	C 0
27	71.1	69.3	70.4	70.3	18.8	23.1	14.9	17.9	23.7	10.9	66	46	94	69	7.3	15.1	0.9	7.8	8	9	9	WSW 4	WSW 5	S 1
28	64.8	65.8	65.6	65.4	15.7	17.4	13.2	14.9	17.8	11.0	88	70	96	85	2.1	6.1	0.6	2.9	10 •	10	10 •	WSW 2	W 5	C 0
29	72.5	74.7	76.8	74.7	11.2	14.8	8.8	10.9	16.0	8.7	92	64	95	83	1.0	6.0	0.8	2.6	9	7	4	WNW 4	WNW 5	C 0
30	78.3	78.8	79.2	78.8	9.9	13.3	11.5	11.6	15.3	6.3	96	78	91	88	0.5	3.3	1.2	1.7	10	9 •	10	C 0	W 3	NW 2
31	78.0	78.3	78.4	78.2	10.7	13.9	12.4	12.4	16.4	10.4	99	82	75	85	0.2	2.9	3.5	2.2	10 •	9	8	WNW 4	WNW 6	W 3
M	74.6	74.6	74.6	74.6	13.5	18.2	13.4	14.6	20.0	9.1	82	58	85	74	2.9	10.1	2.8	5.3	7.3	7.7	7.1	2.3	4.3	1.4

Sierpień – Août

1	78.3	77.9	77.5	77.9	15.6	19.3	12.0	14.2	20.7	11.5	71	48	95	71	4.5	11.7	0.7	5.6	7	4	0	WSW 6	WNW 4	C 0
2	74.7	74.4	75.0	74.7	10.3	18.4	12.2	13.3	22.6	5.2	97	75	98	90	0.3	5.3	0.3	2.0	2	10	8 ≡	C 0	NW 3	C 0
3	77.1	80.0	82.1	79.7	13.6	14.8	9.9	12.0	17.2	9.8	92	76	92	87	1.3	4.0	1.0	2.1	9	9	2	NW 6	WNW 5	W 1
4	81.0	79.4	77.9	79.4	8.6	16.0	17.1	14.7	18.2	3.5	97	66	64	76	0.3	6.1	7.1	4.5	9	10 •	9	C 0	SW 3	W 4
5	77.8	77.2	74.5	76.5	15.7	21.0	16.7	17.5	24.6	13.5	87	68	92	82	2.2	7.9	1.0	3.9	8	8	1	C 0	SW 4	C 0
6	72.9	72.1	70.8	71.9	18.1	29.2	22.6	23.1	30.1	11.5	84	40	67	64	3.3	24.4	9.0	12.2	0	3 ⊙	4	C 0	W 5	SSE 2
7	73.6	73.9	77.5	75.0	16.6	22.1	14.7	17.0	23.4	14.6	98	65	97	87	0.4	9.2	0.5	3.4	10 •	7	9	SE 1	WSW 4	C 0
8	77.9	75.6	76.0	76.5	13.7	21.0	18.1	17.7	25.6	8.2	91	67	90	83	1.5	8.3	2.1	4.0	4	9	6	C 0	E 5	C 0
9	79.7	79.5	80.7	80.0	16.5	24.6	18.2	19.4	25.1	13.6	97	65	97	86	0.6	10.7	0.6	4.0	9	9	10 •	SE 2	NW 1	C 0
10	79.1	76.5	75.6	77.1	17.5	27.7	20.9	21.8	27.9	15.8	97	63	94	85	0.6	13.7	1.4	5.2	8	5	9	C 0	NNE 2	C 0
11	75.0	76.0	77.3	76.1	18.5	18.1	14.1	16.2	21.0	14.1	95	92	99	95	1.1	1.7	0.2	1.0	10 • R	10	2	W 6	W 2	C 0
12	76.8	76.8	78.3	77.3	14.4	17.3	13.3	14.6	19.1	12.7	98	80	95	91	0.4	3.9	0.7	1.7	9	10 •	10	SSE 2	WNW 4	C 0
13	79.8	81.9	82.6	81.4	12.2	14.7	8.7	11.1	15.5	11.2	94	71	97	87	0.9	4.8	0.3	2.0	10	9	3	NW 3	W 5	ESE 1
14	80.6	79.0	77.2	78.9	7.6	17.1	11.0	11.7	19.0	3.2	96	58	90	81	0.4	8.1	1.3	3.3	6	9	0	C 0	W 3	C 0
15	74.1	72.9	70.9	72.6	14.1	14.3	14.2	14.2	17.2	8.4	79	81	75	78	3.4	3.1	4.4	3.6	9	9	7	WNW 2	WSW 5	WNW 2
16	71.7	71.4	71.3	71.5	11.3	13.1	10.5	11.4	14.3	8.9	71	68	86	75	3.9	4.8	1.8	3.5	3	9	10	WSW 6	WSW 7	WSW 2
17	67.3	67.6	70.4	68.4	8.0	14.2	10.7	10.9	14.9	4.2	92	65	85	81	0.9	5.6	2.0	2.8	8	9	9	C 0	W 2	C 0
18	71.7	73.0	72.2	72.3	11.4	12.7	11.0	11.5	15.1	6.6	90	93	85	89	1.4	1.1	1.9	1.5	9	9	3	WNW 7	NW 3	WSW 3
19	67.4	66.2	67.3	67.0	13.4	17.5	11.4	13.4	19.6	9.1	77	64	99	80	3.5	7.2	0.2	3.6	9	7	3	WSW 7	WSW 7	SSE 2
20	69.0	71.8	74.9	71.9	12.1	12.2	12.4	12.4	17.0	8.4	84	89	86	86	2.2	1.6	2.0	1.9	10	9	9	C 0	W 4	C 0
21	75.6	75.0	73.4	74.7	13.9	18.7	17.6	17.0	20.4	11.0	77	61	61	66	3.7	8.4	7.9	6.7	10	4	6	WSW 9	WSW 8	SW 5
22	70.3	68.2	69.5	69.3	16.2	18.3	13.1	15.2	20.0	12.9	71	64	74	70	5.2	7.5	4.0	5.6	9 •	8	2	WSW 3	SSW 5	WNW 3
23	72.3	74.3	77.0	74.5	12.3	14.6	9.9	11.7	15.6	9.8	83	72	92	82	2.4	4.6	1.0	2.7	10	8	8	W 5	W 4	C 0
24	78.5	79.0	78.7	78.7	12.2	13.9	9.4	11.2	15.4	8.0	76	79	92	82	3.4	3.4	1.0	2.6	10	10	5	W 3	W 5	SSE 2
25	77.6	79.3	79.6	78.9	8.7	15.2	13.0	12.3	18.6	5.8	96	80	93	90	0.4	3.5	1.1	1.7	9	10	8	SE 1	WNW 5	C 0
26	81.2	81.5	81.9	81.5	13.1	21.7	16.4	16.9	22.5	8.9	93	54	91	79	1.1	12.0	1.7	4.9	9	7	8	C 0	W 4	C 0
27	82.7	83.2	84.9	83.6	13.1	24.7	15.3	17.1	25.2	11.6	98	49	92	80	0.4	16.0	1.3	5.9	4	5 ⊙	6	C 0	NW 7	C 0
28	87.5	88.5	88.4	88.1	13.0	20.9	12.5	14.7	21.6	10.5	99	59	94	84	0.2	10.0	0.9	3.7	4	8	3	C 0	NW 4	SE 2
29	87.3	85.4	84.5	85.7	9.1	23.1	13.5	14.8	24.5	5.4	96	49	94	80	0.5	14.5	0.9	5.3	3	1	0	C 0	N 2	C 0
30	84.5	85.0	85.9	85.1	8.6	23.7	13.5	14.8	24.2	6.3	96	45	92	78	0.5	16.1	1.3	6.0	0	3	0	C 0	NE 2	C 0
31	87.6	88.0	88.6	88.1	10.3	23.5	13.9	15.4	23.7	6.4	96	49	85	77	0.5	14.7	2.3	5.8	0	1	0	C 0	ESE 2	C 0
M	77.1	77.1	77.5	77.2	12.8	18.8	13.8	14.8	20.6	9.4	89	66	88	81	1.7	8.2	2.0	4.0	7.0	7.4	5.2	2.2	4.1	0.9

Jelenia Góra — $H_s = 342\,m$ — $H_b = 343{,}9\,m$ — $h_w = 15\,m$ — Lipiec – Juillet 1961

DNI	WIELKOŚĆ DZIAŁALNOŚCI V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	= 0^00 – 5^30 = – 9^40 . ⌒ 1-2 0^00 – 9^00 ⌒ ° 22^00 – 24
2	8	.	.	–	= 0^30 – 5^30 = – 7^20 . ⌒ 0-1 0^00 – 9^00
3	7	0.1	.	–	= 0^00 – 2^35 = – 5^15 . ⌒ 1 3^00 – 9^00
4	7	0.2	.	–	●▽ 7^41 – 43 ● ° 18^40 19^10 , = 4^10 – 12^20
5	8	2.2	.	–	●▽ 4^10 – 30 ●▲ ° 17^58 – 18^16 ●▽ ° 19^35 – 38 , 20^35 – 43 , » 18^00 – 10
6	8	0.0	.	–	●▽ ° 10^40 – 11^45
7	8	.	.	–	= 23^35 – 24 . ⌒ 1 23^00 – 24
8	7	0.0	.	–	= 0^00 – 3^20 = – 5^15 = – 10^10 ⌒ 2 0^00 – 11^00 ⌒ ° 22^00 – 24 ⌒ 0-1 0^00 – 7^00
9	7	3.7	.	–	● 0-1 7^50 – 8^00 – 9^05 10^15 ●▽ ° 13^15 – 50 14^25 15^20 – 20^35 21^20 . = na ⌒ 0-1 0^00 – 7^00
10	7	0.0	.	–	●▽ ° 6^15 – 25 ● ° 8^05 – 9^10 ●▽ 1 11^30 – 40 , = 0^30 – 3^20 – 22^30 – 24 . ⌒ 1 22^00 – 24
11	7	0.1	.	–	● ° 4^45 – 9^05 ●▽ 2^30 – 23^05 . (K) 1 W 22^20 – 30 K 1 – 23^10 (K) 1 – 23^45 . = 0^00 – 3^30 = 8^20 – 13^30 , ⌒ 1 0^00 – 4^45
12	8	.	.	–	
13	7	1.8	.	–	●▽ 1 13^50 – 14^00 ●▽ ° – 15^05 ● ° 18^23 – 45
14	8	0.5	.	–	●▽ ° 0^45 – 3^15 – 8^45 – 48
15	8	7.7	.	–	● ° 3^45 – 4^10 – 21^40 – 23^46 ● 1 – 24
16	8	0.6	.	–	● 1 0^00 – 2^35 ● ° 2^50 – 4^40 ●▽ ° 17^10 – 25 18^05 – 45 . = 21^40 – 23^20 = – 24
17	8	2.2	.	–	● ° 7^50 – 8^15 ●▽ ° 11^45 – 19^10 = 0^00 – 4^15
18	7	7.0	.	–	●▽ ° 14^45 – 15^10 (K) 18^25 – 40 ● ° K ° – 19^30 SW-NE ● ° 21^40 – 22^25 ●▽ 1 – 22^30 . = 4^30 – 13^20
19	6	5.6	.	–	●▽ 1 3^45 – 4^10 ● ° 5^20 – 7^15 ●▽ ° 10^30 – 15^35 . (K) 11^14 – 12^40 SE . = 0^00 – 12^15 = 20^40 – 22^45 = – 24
20	7	0.6	.	–	●▽ ° 11^20 – 13^50 – 17^20 – 40 . = 1 0^00 – 3^40 = – 11^30
21	7	3.0	.	–	● ° 4^15 – 5^50 – 7^30 – 8^10 – 11^05 – 15 – 12^50 – 13^15 – 18^45 – 19^10 . = 5^55 – 8^20 , 19^30 – 24
22	6	0.0	.	–	● 1 12^0 . 50 ● ° 2^35 – 6^40 , 8^35 – 9^20 . = 0^00 – 16^10 , P
23	6	.	.	–	= 2^20 – R
24	8	.	.	–	= 0^00 – 7^30
25	7	.	.	–	= 5^20 – 9^30 , 20^25 – 24
26	7	.	.	–	= 2^00 – 10^20 . ⌒ 1 3^00 – 8^30
27	7	13.5	.	–	●▽ ° 15^05 – 10 ●▽ 0-1 16^20 – 20^40 ●▽ ° 21^20 – 22^40 = 23^30 – 24
28	8	19.8	.	–	●▽ ° 4^50 – 7^10 ● ° 7^20 – 10^35 ●▽ ° – 11^40 . 15^20 – 30 ● 0-1 17^30 – 24 . = 0^00 – 50 = – 2^50 = – 6^30
29	8	.	.	–	● 1 0^00 – 1^20 ● ° 5^10 . = 5^10 – 9^40 ⌒ 1 21^00 – 24
30	7	26.0	.	–	● ° 13^50 – 14^40 – 18^20 – 19^50 – 20^45 – 21^45 ● 1 – 24 . = 0^00 – 8^30 , ⌒ 1 0^00 – 10^00
31	7	9.8	.	–	● 0-2 0^00 – 11^15 ●▽ 1-0 11^45 – 12^15 , 13^30 – 35 , = 21^30 – 24
Σ	–	104.4	–	–	UWAGI.

Sierpień – Août

1	8	.	.	–	= 21^40 – 24 . ⌒ 1 22^00 – 24
2	7	2.6	.	–	● ° 14^50 – 20^15 = 0^00 – 5^40 = – 1 6^40 = – 10^30 , 20^15 – 21^45 = ° – 24 , ⌒ 0-2 0^00 – 12^00
3	7	0.0	.	–	●▽ ° 10^30 – 45 = ° 0^00 – 6^30 = – 13^10 21^30 – 23^45 = – 24 . ⌒ 2 22^00 – 24
4	6	0.5	.	–	● 12^50 – 16^35 17^45 – 18^15 . = 0^00 – 45 = – 5^45 = – 8^30 . ⌒ 2 0^00 – 8^00
5	8	.	.	–	= 22^30 – 24 . ⌒ ° 5^00 – 10^00 21^00 – 24
6	8	6.2	.	–	= 0^00 – 6^30 . ⌒ 0-1 0^00 – 9^00 ↘ 21^40 – 22^20
7	8	1.8	.	–	●▽ 0-1 5^25 – 8^45 ● ° 9^10 – 10^30 ●▽ ° 16^50 – 17^15 ● ° 18^20 – 20^15 . K 5^30 – 6^20 = 22^30 – 24
8	7	0.0	.	–	● ° 10^05 . 25 = 0^00 – 10 = ° – 5^50 = – 7^30 23^30 – 24 . ⌒ ° 22^00 – 24
9	7	2.7	.	–	●▽ 0-1 15^25 – 18^35 ● ° 20^35 – 22^15 = 0^00 – 10^30 16^15 – 23^45 = 1 – 24 . ⌒ 0-1 0^00 – 10^00
10	8	2.3	.	–	(K) 19^15 – 55 ● 1 K 1 – 20^21 (K) 1 – 20^30 W-E . = 1-0 0^00 – 7^25 = – 9^10 19^40 – 24
11	6	24.1	.	–	●▽ 0-1 4^08 – 6^15 7^40 – 11^25 ●▽ 2-0 12^45 (K) 7^35 – 40 K 1 – 12^45 W-E . = 0^00 – 21^30 = ° – 24
12	6	4.9	.	–	● 0-1 13^50 – 15^20 – 19^10 . = ° 0^00 – 2^30 = 1 – 5^45 = – 24
13	8	1.0	.	–	● ° 5^40 – 6^10 8^40 – 9^15 ●▽ 1-0 10^50 – 11^30 . = 0^00 – 45 = ° – 4^30 = – 13^30 = 23^25 – 24
14	7	.	.	–	= 0^00 – 40 = – 2^00 = – 2^45 = – 6^50 = – 9^30 , 21^45 – 24 . ⌒ ° 20^00 – 24
15	7	3.3	.	–	●▽ ° 13^20 – 24 13^37 – 45 15^50 – 16^12 17^48 – 18^10 . = 0^00 – 9^40 . ⌒ 1 0^00 – 9^00
16	8	2.1	.	–	●▽ 1 10^50 – 5^30 – 40 ●▽ ° – 6^10 . 12^25 – 45 15^43 – 51 . 17^40 – 20^50 . = 21^45 – 24
17	7	0.2	.	–	●▽ ° 7^10 – 25 = 0^00 – 5^35 18^30 – 24
18	6	3.3	.	–	●▽ 0-1 2^10 13^50 . = 0^00 – 16^15 22^25 – 24
19	8	3.3	.	–	● ° 6^40 7^10 ●▽ ° 9^47 – 10^15 10^30 – 11^15 ●▽ 0-1 17^15 – 18^05 18^48 – 20^05 . = 0^00 – 2^35 . 20^20 – 21^30 = – 22^20
20	7	3.7	.	–	●▽ 1 5^35 – 7^15 11^12 – 20 . 13^25 – 40 ●▽ 0-1 18^40 – 19^05 ●▽ ° 22^45 – 23^15
21	7	0.8	.	–	●▽ ° 2^10 – 25 = 0^30 – 8^30
22	7	1.9	.	–	● 0-1 5^45 – 7^30 – 9^25 ●▽ 10^50 – 11^25 18^02 – 16
23	7	1.3	.	–	● ° 4^45 – 6^05 ●▽ ° 11^05 – 15^15 . = 20^30 – 24 . ⌒ 0-1 22^00 – 24
24	6	0.1	.	–	● ° 8^40 – 10^10 12^50 – 13^20 . = 0^00 – 6^30 8^30 – 16^20 20^45 – 24 . ⌒ 1 0^00 – 9^30 . 22^00 – 24
25	6	0.0	.	–	● ° 10^40 – 11^15 . = 0^00 – 16^10 ∞ – 19^35 = – 24 . ⌒ 1 0^00 – 10^40 23^00 – 24
26	7	.	.	–	= 0^00 – 9^15 ∞ – 11^20 = 22^30 – 24 . ⌒ 1-2 0^00 – 10^00 ⌒ ° – 11^00 . 20^00 – 24
27	7	.	.	–	= 0^00 – 7^30 21^45 – 24 . ⌒ 0-1 0^00 – 10^00 ⌒ 1 20^00 – 24
28	7	.	.	–	= 0^00 – 4^55 = ° – 5^50 = 1 – 7^30 = – 11^45 19^20 – 24 . ⌒ 1 0^00 – 10^00 . 22^00 – 24
29	8	.	.	–	= 0^00 – 9^30 21^30 – 24 . ⌒ 1-0 0^00 – 10^00 ⌒ ° 21^00 – 24
30	8	.	.	–	= 0^00 – 5^45 = 1 – 8^00 = – 10^50 . 23^50 – 24 . ⌒ 1 0^00 – 10^00 . 22^00 – 24
31	8	.	.	–	= 0^00 – 7^20 . ⌒ 1 0^00 – 10^00
Σ	–	66.1	–	–	UWAGI.

Jelenia Góra — φ = 50°54' — λ = 15°48' — Wrzesień – Septembre 1961

DNI	CIŚNIENIE P – 900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	86.3	87.2	84.8	86.8	12.9	26.9	14.3	17.1	28.7	6.3	91	42	86	73	1.4	20.6	2.4	8.1	0	0	0	NE 1	NW 2	C 0
2	82.3	80.8	77.8	80.3	16.9	28.0	17.8	20.1	28.7	11.4	72	27	59	53	5.3	27.6	8.4	13.8	0	0	0	ESE 1	SSE 4	SE 4
3	75.0	73.5	72.7	73.7	14.3	28.2	15.6	18.4	29.2	10.6	87	40	82	70	2.2	22.9	3.2	9.4	2 ⊙	1 ⊙	0	SE 1	S 4	C 0
4	74.3	74.9	75.6	74.9	13.0	25.3	16.9	18.0	26.1	11.3	93	47	92	77	1.1	17.0	1.6	6.6	4	4	10 • R	ESE 1	NW 5	C 0
5	73.6	71.2	69.2	71.3	11.7	27.6	17.2	18.4	28.4	10.7	98	45	93	79	0.3	20.5	1.4	7.4	0	8	9 • R	C 0	E 2	WNW 3
6	69.3	69.4	67.6	68.8	14.6	18.4	13.6	15.0	19.7	13.6	98	75	91	88	0.4	5.3	1.5	2.4	9	10	0	C 0	WNW 2	C 0
7	66.9	66.7	69.3	67.6	14.5	15.8	12.1	13.6	17.8	10.8	81	66	68	72	3.1	6.0	4.5	4.5	10 •	9	0	W 5	SW 7	WSW 5
8	70.4	71.1	74.4	72.0	10.3	12.4	12.6	12.0	14.2	9.9	75	72	84	77	3.1	4.0	2.4	3.2	9	9	8	WSW 4	WSW 9	W 7
9	76.7	78.1	78.9	77.9	12.3	13.3	12.1	12.4	14.2	11.6	94	81	82	86	0.9	3.0	2.5	2.1	10 •	10	10	NW 5	W 5	W 6
10	80.1	80.6	80.7	80.5	9.5	11.8	10.9	10.8	12.3	9.3	96	80	86	87	0.5	2.8	1.8	1.7	10 •	10	10	W,W 3	W 4	WNW 2
11	79.3	77.7	75.8	77.6	9.9	15.6	7.1	9.9	16.9	6.7	95	52	94	80	0.6	8.6	0.6	3.3	10	9	0	SE 1	W 3	C 0
12	73.7	75.3	75.5	74.8	8.8	13.6	13.9	12.6	19.5	4.4	95	94	74	88	0.6	0.9	4.1	1.9	6	10 •	10	SE 1	NNW 2	W 3
13	76.4	76.3	74.6	75.8	11.2	18.7	11.7	13.3	19.3	9.9	97	55	94	82	0.3	9.7	0.8	3.6	9	9	3	S 2	SW 4	C 0
14	72.5	73.0	72.8	72.8	15.5	20.2	16.3	17.1	22.3	8.9	81	64	91	79	3.4	8.7	1.7	4.6	9 •	8 ⊙	6	SW 2	W 7	W 5
15	79.9	82.0	82.9	81.6	11.6	17.2	10.2	12.3	18.7	9.9	85	49	93	76	1.9	10.0	0.8	4.2	8	3	0	W 5	WNW 7	E 1
16	83.1	81.4	80.3	81.6	9.1	25.7	12.9	15.2	27.3	6.4	96	53	94	81	0.5	15.5	0.9	5.6	4 ⊙	2 ⊙	0	C 0	NE 1	C 0
17	80.6	80.2	81.1	80.6	11.3	29.1	13.9	17.0	29.7	7.7	94	43	94	77	0.8	23.0	0.9	8.2	0	1	0	SE 1	SSE 2	NNE 1
18	82.0	82.2	82.1	82.1	10.7	27.3	16.3	17.6	28.2	8.7	97	57	95	83	0.4	15.7	1.0	5.7	3	1	0	C 0	WNW 1	C 0
19	83.0	83.0	82.2	82.7	15.2	21.0	13.5	15.8	21.0	12.6	85	68	70	74	2.6	8.1	4.7	5.1	10	5	0	E 3	ENE 2	SE 2
20	81.8	81.5	81.5	81.6	5.7	19.2	11.7	12.1	19.5	3.8	95	48	68	70	0.5	11.6	4.4	5.5	0 ⊙	0 ⊙	0	C 0	ESE 7	E 4
21	81.7	82.2	83.9	82.6	4.4	19.1	10.7	11.2	19.9	2.5	97	49	79	75	0.3	11.3	2.8	4.8	0 ⊙	0 ⊙	0	C 0	ENE 6	SSE 1
22	85.7	85.9	86.3	86.0	1.6	18.7	8.3	9.2	18.9	0.6	91	36	79	69	0.7	13.9	2.3	5.6	0 ⊙	0 ⊙	0	C 0	E 5	SSE 2
23	85.7	84.0	83.5	84.4	1.0	21.5	6.4	8.8	22.0	-0.2	96	36	94	75	0.3	16.3	0.6	5.7	0 ⊙	0 ⊙	0	C 0	NW 1	C 0
24	82.7	81.2	81.3	81.7	1.6	22.7	8.7	10.4	23.3	0.4	98	38	94	77	0.2	17.0	0.6	5.9	0	0	0	C 0	NW 1	SE 1
25	81.2	82.1	84.3	82.5	2.5	19.5	14.1	12.6	21.0	0.6	98	66	93	86	0.1	7.7	1.1	3.0	0	7	10	C 0	WNW 5	WSW 1
26	83.5	82.1	81.0	82.2	10.9	20.3	12.4	14.0	20.8	9.6	99	46	99	81	0.1	12.8	0.2	4.4	9	7	8	C 0	NW 2	SE 1
27	79.4	78.2	77.2	78.3	12.1	18.2	8.7	11.9	19.2	8.4	99	62	99	87	0.1	7.9	0.1	2.7	10 ≡	3	10 ≡	C 0	NW 1	C 0
28	77.9	77.5	79.0	78.1	6.4	23.5	12.0	13.5	24.9	3.4	97	37	98	77	0.3	18.2	0.3	6.3	7	6	0	C 0	C 0	C 0
29	78.9	77.6	78.8	78.4	8.2	26.7	13.3	15.4	27.1	6.9	97	39	94	77	0.3	21.3	0.9	7.5	2	6	5	SE 1	SSW 2	W 2
30	77.9	75.4	74.2	75.8	12.7	26.2	17.1	18.3	26.4	10.6	92	50	79	67	1.2	23.7	4.1	9.7	9	7	4	C 0	ESE 5	E 7
31																								
M	78.8	78.4	78.3	78.5	10.0	21.1	12.7	14.1	22.2	7.6	92	53	87	77	1.1	13.1	2.1	5.4	5.0	4.8	3.4	1.2	3.6	1.9

Październik – Octobre

1	75.3	77.1	80.2	77.5	11.7	15.9	9.9	11.8	17.2	9.9	77	57	73	69	5.1	7.9	3.3	4.8	9	8	0	E 9	ESE 6	ESE 4
2	81.9	83.2	83.9	83.0	9.2	14.5	10.7	11.5	14.9	6.9	79	59	82	73	2.4	6.8	2.3	3.8	4	5	0	ESE 5	E 7	E 5
3	84.0	83.0	82.8	83.3	3.6	15.9	8.6	9.2	16.8	3.0	97	59	88	81	0.3	7.5	1.4	3.1	0	1	0	C 0	ESE 5	SSE 1
4	80.8	80.9	80.2	80.6	14.1	17.0	14.7	15.1	18.2	6.3	54	51	58	54	7.4	9.5	7.0	8.0	8	8 ⊙	1	SE 7	SE 8	ESE 6
5	79.8	80.3	80.8	80.3	14.7	21.0	13.6	15.7	21.2	11.1	58	48	74	60	7.0	13.0	4.0	8.0	2 ⊙	1 ⊙	0	SE 5	SE 7	SE 3
6	79.2	77.8	73.5	76.8	14.6	20.1	15.4	16.4	20.6	10.7	59	44	52	52	6.8	13.1	8.4	9.4	1 ⊙	1 ⊙	0	SE 7	SE 7	ESE 6
7	67.4	65.3	65.6	66.1	14.2	18.6	15.6	16.0	19.2	13.6	47	43	56	49	8.5	12.1	7.7	9.4	2	7	2	ESE 8	SE 15	SE 10
8	65.7	67.8	73.8	69.1	14.6	17.7	11.1	13.6	18.3	11.1	60	49	91	67	6.7	8.4	1.1	5.4	9	9	10	SE 8	S 5	NW 1
9	81.9	84.8	88.6	85.1	8.0	17.3	6.0	9.3	18.3	5.6	97	59	97	84	0.3	8.0	0.3	2.9	8	2 ⊙	0	C 0	NW 3	SE 1
10	89.9	89.0	87.5	88.8	1.3	19.5	8.1	9.2	20.6	1.0	96	46	93	78	0.2	12.2	0.8	4.4	0	3 ⊙	0	SE 1	NE 2	C 0
11	85.9	84.2	84.6	84.9	1.1	20.7	6.2	8.6	21.8	0.7	100	44	91	78	0.0	15.7	0.9	4.9	10 ≡	0 ⊙	0	C 0	W 1	C 0
12	86.6	87.4	88.8	87.6	6.5	15.3	7.7	9.3	15.7 •	2.4	96	82	97	92	0.5	3.2	0.3	1.3	10	9	4	C 0	NW 4	C 0
13	88.8	89.1	89.5	89.1	5.7	12.8	5.2	7.2	13.1	4.6	95	62	94	84	0.5	5.7	0.5	2.2	9	8	8	C 0	NW 3	C 0
14	88.8	88.4	88.2	88.5	5.6	11.4	7.2	7.8	12.9	4.9	97	65	91	84	0.3	4.7	0.9	2.0	9	9 ⊙	8	C 0	W 5	WNW 2
15	86.6	85.1	82.7	84.8	9.3	11.9	4.1	7.4	12.2	3.9	92	70	95	86	0.9	4.1	0.4	1.8	10	10	0	W 2	W 3	C 0
16	79.9	77.9	76.5	78.1	-1.2	17.5	5.4	6.8	18.3	-1.2	99	50	97	82	0.1	10.0	0.3	5.5	1 ═	8	0	SE 2	WNW 3	C 0
17	71.7	67.2	57.7	65.5	9.9	12.9	12.4	11.9	14.0	2.4	78	67	67	71	2.7	4.9	4.8	4.1	8	10	10 •	NW 2	SSW 5	S 8
18	48.9	49.7	52.6	50.4	10.0	10.5	6.6	8.4	12.6	6.3	75	84	97	85	3.3	2.1	0.3	1.9	10	10 •	10 •	E 6	C 0	SSE 1
19	55.4	57.1	60.8	57.8	5.2	8.8	5.4	6.2	10.8	4.5	94	81	97	91	0.5	2.1	0.3	1.0	9	9	6	C 0	C 0	C 0
20	66.5	69.2	70.6	68.8	3.9	10.1	6.9	7.0	10.2	2.6	97	77	96	90	0.3	2.9	0.4	1.2	8	10	10 •	C 0	C 0	C 0
21	69.2	70.0	73.0	70.7	7.0	8.3	8.0	7.8	9.1	1.8	97	95	80	90	0.3	0.8	2.1	1.1	10	10	10	C 0	W 2	E 5
22	79.1	80.5	81.0	80.2	2.6	12.1	5.2	6.3	13.3	1.8	93	64	92	83	0.6	5.1	0.7	2.1	4 ⊙	7	0	SE 1	SE 5	SE 1
23	80.6	80.4	80.4	80.5	9.0	12.2	7.9	9.2	13.3	1.7	84	73	82	80	1.9	3.8	1.9	2.5	4	9	9	SE 5	SE 6	SE 5
24	82.6	81.1	78.7	80.8	10.5	15.8	10.0	11.6	17.0	7.0	73	56	68	66	3.2	7.9	3.9	5.0	9	8 ⊙	0	SSW 4	SE 3	SE 7
25	75.5	76.3	75.8	75.9	8.7	12.2	13.3	12.0	14.8	6.2	72	70	72	71	3.1	4.3	4.4	3.9	9 ⊙	10	9	SE 2	SSW 5	SSE 3
26	73.9	74.0	72.8	73.6	10.5	16.2	11.7	12.5	17.1	9.9	77	67	78	74	2.9	6.2	2.9	4.0	10	8	9	ENE 3	ESE 2	ESE 6
27	68.5	69.9	70.6	69.7	8.8	18.7	10.2	12.0	19.0	8.1	84	55	87	75	1.8	10.2	1.6	4.5	8	9 ⊙	4	ESE 2	SE 2	E 2
28	72.1	71.5	71.7	71.8	5.9	15.1	7.6	9.0	15.9	3.6	97	65	97	86	0.3	6.0	0.3	2.2	8	7	0	E 1	N 2	C 0
29	72.3	72.7	74.6	73.2	8.6	9.0	2.4	5.6	10.0	2.0	94	92	96	94	0.6	1.0	0.3	0.6	10 •	10	0 ≡	WNW 1	WNW 2	SE 1
30	75.1	75.2	77.3	75.9	-0.6	13.4	5.8	5.1	14.0	-1.3	100	64	100	88	0.0	5.5	0.0	1.8	0 ≡	4	0 ≡	SE 1	C 0	C 0
31	78.6	79.3	80.8	79.6	0.3	11.5	8.4	7.2	12.9	0.0	100	62	66	76	0.0	5.2	3.7	3.0	10 ═	9	0	C 0	WSW 7	WSW 7
M	76.5	76.6	77.0	76.7	7.5	14.6	8.7	9.9	15.6	4.9	84	65	84	77	2.1	6.7	2.2	3.7	6.7	7.1	5.5	2.6	4.0	2.7

Jelenia Góra $H_s = 342\ m$ $H_b = 343{,}9\ m$ $h_w = 15\ m$ **Wrzesień – Septembre 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌓ 1-0 3⁰⁰–10⁰⁰ ⌓ ° 21⁰⁰–24
2	8	.	.	–	⌓ ° 0⁰⁰–10⁰⁰
3	9	.	.	–	⌓ ° 5⁰⁰–9⁰⁰
4	6	2.1	.	–	(K) 19³⁰–50 •K° 19⁵⁰–20¹⁰ SW–NE (K)–21³⁰ •K° –22²⁵ (K)–23⁴⁵ NW–SE; = 7¹⁰–10¹⁵ ∞–20³⁰ = –24; ⌓ 1-0 2⁰⁰–10⁰⁰
5	8	12.2	.	–	(K) 19⁵⁰–20²⁵ •K° –21³⁵ ▽° –22⁰⁵; 22²⁸–24; = 0⁰⁰–2⁵⁰ ≡ ¹–7⁴⁵ = –11¹⁰
6	7	0.0	.	–	▽° 0⁰⁰–1⁴⁰ 13⁴⁰–45; = 2⁴⁵–4³⁰ ≡ –7³⁵ = –11⁴⁰
7	8	1.4	.	–	• ° 7⁴²–9⁴⁰ ▽° 15⁵⁰–16¹⁰
8	8	0.8	.	–	▽° 17¹⁵–25 18²⁰–30 19¹⁰–15; = 17³⁰–22¹⁵
9	8	0.6	.	–	▽° 7²⁵–8²⁵ 16⁰⁵–15; = 5³⁰–10¹⁰
10	7	0.6	.	–	• ° 0⁰⁰–2²⁰; 5⁴⁰–8³⁵; 9¹⁵–11⁴⁵ 16⁵⁵–17¹⁴
11	7	.	.	–	= 0⁴⁰–10⁴⁰ 19²⁰–24 ⌓ ° 18⁰⁰–20⁰⁰ ⌓ ²–24
12	6	1.3	.	–	• ° 13⁰⁵–14⁴⁰; = 0⁰⁰–10¹⁰ ∞–11³⁰ = 12⁴⁵–15³⁰; ⌓ 2-0 0⁰⁰–12⁰⁰
13	7	0.0	.	–	• ° 4¹⁰–5¹⁵; = 2⁰⁰–9³⁰
14	8	8.5	.	–	• ° 7⁴⁰–9²⁰; 19¹⁰–20²⁰ ▽ 2-0 –21³⁵ ▽° 22¹⁰–30
15	8	.	.	–	⌓ ° 21⁰⁰–24
16	7	.	.	–	= 5³⁰–10²⁰ = 20³⁵–24; ⌓ 0-1 0⁰⁰–na
17	8	.	.	–	= 2⁰⁰–7⁴⁵
18	8	.	.	–	= 22¹⁵–24; ⌓ 1-0 2⁰⁰–12⁰⁰ ⌓ ° 22⁰⁰–24
19	6	.	.	–	= 0⁰⁰–14⁰⁰; ⌓ ° 2⁰⁰–11⁰⁰ 20⁰⁰–24
20	8	.	.	–	= 6²⁰–7¹⁵; ⌓ 0-2 0⁰⁰–7⁰⁰
21	8	.	.	–	= 3⁴⁰–7³⁰; ⌴ ° na–8⁰⁰ ⌓ ° a–11⁰⁰; 21⁰⁰–24
22	7	.	.	–	= 2⁰⁰–10³⁰; ⌴ 0-1 0⁰⁰–5⁰⁰ ⌴ °–7⁰⁰ ⌓ ¹ 22⁰⁰–24
23	7	.	.	–	= 3³⁰–8³⁰ = –10²⁰ = np; ⌓ ¹ 0⁰⁰–9⁰⁰
24	7	.	.	–	= 0⁰⁰–11³⁰ 20⁴⁵–24; ⌴ ° 5⁰⁰–9⁰⁰ ⌓ ¹ a–12⁰⁰; 21⁰⁰–24
25	5	0.0	.	–	• ° 17⁵⁵–18¹⁰–19¹⁰; = 0⁰⁰–24; ⌓ 0-1 0⁰⁰–3⁰⁰ ⌴ °–7⁰⁰ ⌓ ¹–10²⁰
26	7	1.0	.	–	• ° 17²⁵–18³⁵; = 20²⁵–40
27	6	.	.	–	• ° 6⁷⁰–50 = 2⁰⁰–7⁴⁵ ≡ ° –9⁴⁰ = –13¹⁵ ∞–20³⁰ = –20⁵⁰ ≡ ° –21⁰⁰ ≡ ² –24
28	7	0.0	.	–	▽° 15²⁰–25; ≡ 1-0 0⁰⁰–6⁴⁵ = –10³⁵; 18³⁰–24; ⌓ ¹ 0⁰⁰–10⁰⁰; 20⁰⁰–24
29	7	.	.	–	= 0⁰⁰–12³⁰; 22³⁰–24; ⌓ ¹ 0⁰⁰–9³⁰; 23³⁰–24
30	7	0.0	.	–	• ° 8⁰⁸…20; = 0⁰⁰–2⁰⁰ ≡ –3³⁰ = –7¹⁵; 19¹⁵–24; ⌓ 1-0 0⁰⁰–11⁰⁰
31					
Σ	–	28.5	–	–	UWAGI:

Październik – Octobre

1	6	.	.	–	= 0⁰⁰–10²⁰ S–16²⁰
2	7	.	.	–	= 5¹⁰–8³⁰
3	6	.	.	–	= 3³⁰–24; ⌴ ° 4⁰⁰–7⁰⁰
4	8	.	.	–	= 0⁰⁰–5⁰⁰
5	8	.	.	–	= 17³⁰–20²⁰
6	8	.	.	–	
7	8	.	.	–	≫ 9³⁰–10¹⁵ 12⁴⁵–13⁵⁰; 20⁴⁰–22²⁰
8	8	3.5	.	–	• ° 19⁴⁰–20²⁰–24
9	8	.	.	–	• ° 0⁰⁰–10; = 12⁰–5³⁰ ≡ ² 20⁴⁰–24
10	8	.	.	–	≡ ° 0⁰⁰–2⁴⁰ = –6¹⁰ ≡ ° –7²⁰ = –10³⁵ 18⁴⁰–24; ⌴ 5⁰⁰–7⁰⁰; ⌓ ¹ 22⁰⁰–24
11	7	.	.	–	= 0⁰⁰–4²⁰ = ° –5⁴⁰ ≡ ¹ –7⁴⁵ = 17⁵⁰–24; ⌓ 1-2 0⁰⁰–9⁰⁰
12	6	.	.	–	= 0⁰⁰–24; = 17¹⁵–30; ⌓ ¹ 2⁰⁰–9⁰⁰; 22⁰⁰–24
13	8	.	.	–	= 0⁰⁰–11²⁰ 18³⁰–24; ⌓ ¹ 0⁰⁰–9⁰⁰; 19⁰⁰–24
14	8	.	.	–	= 0⁰⁰–8²⁰; 23³⁰–24; ⌓ ° 0⁰⁰–9⁰⁰
15	7	.	.	–	= 0⁰⁰–8⁴⁵; 13³⁰–15⁴⁵ ≡ 20³⁰–23⁴⁵ ≡ ¹ –24; ⌓ ¹ 2⁰⁰–9⁰⁰
16	6	0.0	.	–	≡ 0⁰⁰–7³⁵ = –17²⁰ ∞–18¹⁵ = –24; ⌴ ° 3⁰⁰–8⁰⁰ ⌓ ¹ a ⌓ ° 18⁰⁰–24
17	7	2.9	.	–	• ° 6⁰⁵…15; 19⁴⁰–24; = 0⁰⁰–9⁰⁰; ⌓ ° 0⁰⁰–6⁰⁰
18	7	8.2	.	–	• ° 0⁰⁰…5¹⁵ 12²⁰–15¹⁵ • ° 15³⁰–40 • ° –23³⁰
19	6	0.6	.	–	• ° 1⁰⁰–3³⁰ 7⁵⁵–9⁴⁵ 10¹⁰–11²⁵; = 5³⁰–14¹⁵ 17³⁰–24; ▽ 21³⁰–24
20	8	14.2	.	–	• ° 14⁴⁰–15²⁰ • 0-1 –22⁴⁵; = 0⁰⁰–6¹⁵; ▽ 0⁰⁰–2³⁰
21	5	8.2	.	–	• ° 1⁴⁰–5⁴⁵ 7³⁰–8¹⁰ 9⁰⁵ ▽ ¹ 11³⁵; = 1⁰⁰–24
22	8	.	.	–	= 0⁰⁰–2⁵⁰ ⌓ ° 19⁰⁰–24
23	7	0.0	.	–	⌓ ° 0⁰⁰–10⁰⁰
24	8	.	.	–	• ° 0²⁰…35 3⁴⁰ 4³⁵
25	8	.	.	–	
26	8	.	.	–	≫ 23⁰⁰–24; = 16⁴⁰–22⁵⁰
27	8	.	.	–	≫ 0⁰⁰–1²⁰; = 22⁴⁰–24; ⌓ ° 23⁰⁰–24
28	6	1.6	.	–	= 0⁰⁰–5³⁰ = –6²⁰ = –12¹⁰ ∞–16²⁰ = –24; ⌓ 0-1 0⁰⁰–8⁰⁰
29	5	6.7	.	–	• ° 4¹⁰–12⁰⁵; = 1⁰⁰–15²⁰ ≡ ° 17⁴⁰–24
30	7	0.2	.	–	≡ ° 0⁰⁰–1³⁰ ≡ ¹ 5⁴⁰–8⁴⁵ = –10³⁰ = 16¹⁵–17³⁰ = –19⁴⁵ ≡ ° –21³⁰ ≡ ° –24; ⌓ 0-2 9¹⁰–14⁰⁰; 16⁰⁰–24
31	7	.	.	–	≡ ° 0⁰⁰–7⁴⁵ = –10¹⁵; 15⁴⁰–18³⁰; ⌓ ² 0⁰⁰–11⁰⁰
Σ	–	46.1	–	–	UWAGI:

Jelenia Góra $\varphi = 50°54'$ $\lambda = 15°48'$ **Listopad – Novembre 1961**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	82.0	81.9	84.3	82.7	8.0	10.9	9.0	9.2	11.0	3.0	67	69	84	75	3.5	4.0	1.9	3.1	8	10	10	WSW 4	W 6	WNW 4
2	83.7	79.5	74.8	79.3	2.8	12.4	4.3	6.0	13.7	2.6	95	58	92	82	0.4	6.1	0.7	2.4	2	4	3	ENE 1	SW 2	E 2
3	69.0	67.1	68.0	68.0	7.2	10.0	7.6	8.1	12.0	2.8	80	65	71	72	2.1	4.4	3.0	3.2	7	9	7	W 4	WSW 9	W 5
4	69.6	70.1	71.8	70.5	3.0	4.6	2.6	3.2	7.6	2.3	69	56	86	70	2.4	3.8	1.1	2.4	10	9	10	WNW 3	W 4	NW 2
5	73.6	75.0	77.9	75.5	1.0	2.4	1.8	1.8	3.0	0.7	92	82	95	89	0.5	1.3	0.6	0.8	10	10 •	10 *	WNW 2	WNW 3	WNW 4
6	76.3	73.7	70.4	73.5	2.0	2.8	3.3	2.8	3.4	0.1	98	96	98	97	0.2	0.3	0.1	0.2	10 •	10 •	10 •	WSW 2	WSW 3	C 0
7	64.9	64.1	65.7	64.9	5.0	9.8	7.4	7.4	10.3	3.2	100	92	83	92	0.0	0.9	1.8	0.9	10 ●	9	8	C 0	E 3	E 4
8	68.1	67.9	66.4	67.4	0.6	6.0	0.2	1.8	7.4	-0.7	98	70	94	87	0.1	2.9	0.4	1.1	10	8	0	C 0	SW 5	ENE 2
9	65.1	63.6	62.3	63.7	1.8	9.9	6.0	5.9	10.0	-2.0	96	66	80	81	0.3	4.2	1.9	2.1	9	9	9	ESE 2	C 0	C 0
10	61.4	64.8	65.9	64.0	5.3	7.0	4.8	5.5	8.9	4.4	94	88	97	93	0.6	1.2	0.3	0.7	9	10 •	10	WNW 2	W 3	C 0
11	63.4	64.1	65.5	64.3	3.2	7.4	6.8	6.0	7.5	1.8	100	86	88	91	0.0	1.5	1.2	0.9	10	9	9	C 0	E 3	ESE 3
12	66.4	66.0	67.9	66.8	7.2	9.4	6.8	7.6	10.8	5.0	80	74	91	82	2.1	3.1	0.9	2.0	3	8	10	ESE 3	ENE 6	E 4
13	66.3	65.9	64.1	64.8	7.0	6.9	7.6	7.3	7.9	6.1	94	94	94	94	0.6	0.5	0.6	0.6	10 •	10 •	10	ESE 4	E 2	ENE 4
14	68.6	73.1	76.8	72.8	2.2	1.2	0.4	1.0	8.0	0.1	100	94	96	97	0.0	0.4	0.3	0.2	10	10 ●	10 ●	WNW 2	C 0	C 0
15	77.7	78.4	79.8	78.6	-0.1	0.7	0.3	0.3	0.8	-0.5	94	85	90	89	0.4	1.1	0.6	0.7	10	10	10	C 0	C 0	C 0
16	78.6	77.0	75.7	77.1	0.0	0.8	1.0	0.7	1.4	-0.3	92	88	87	89	0.5	0.8	0.9	0.7	10	10	9	W 1	C 0	W 2
17	73.5	73.6	73.8	73.6	3.0	5.3	4.8	4.5	6.5	0.0	93	87	89	90	0.6	1.1	1.0	0.9	10	10	10 •	W 3	WNW 7	WNW 4
18	73.0	72.5	74.7	73.4	3.1	4.4	3.9	3.8	5.1	2.7	76	77	88	80	1.8	1.9	1.0	1.6	10	10 •	9	W 5	W 6	C 0
19	77.4	81.0	86.4	81.6	-0.8	1.8	1.1	0.8	4.5	-2.9	95	82	89	89	0.3	1.3	0.7	0.8	10	9	9	C 0	WNW 3	WNW 3
20	91.3	94.2	95.4	93.6	-0.5	3.0	-4.3	-1.5	4.4	-5.2	88	61	96	82	0.7	3.0	0.2	1.3	8	4 ⊙	2	WNW 2	NE 3	SE 2
21	92.6	89.7	87.9	90.1	-6.8	4.7	-3.2	-2.1	5.1	-8.2	96	48	90	78	0.1	4.4	0.5	1.7	0	1 ⊙	2	C 0	E 2	SE 1
22	84.1	82.3	78.8	81.7	-6.6	6.6	-4.3	-2.2	6.9	-7.8	94	55	96	82	0.2	4.3	0.2	1.6	2	3	0	SE 2	C 0	C 0
23	74.9	75.6	74.0	74.2	-7.3	5.2	-3.6	-2.3	5.7	-7.9	90	50	94	78	0.3	4.4	0.3	1.7	0	2	0	C 0	ENE 3	C 0
24	76.5	76.4	75.9	76.3	-4.2	4.4	1.8	1.0	5.4	-5.2	94	71	93	86	0.3	2.5	0.6	1.1	8	8	8	C 0	C 0	SE 2
25	75.9	74.6	72.9	74.5	1.7	6.1	2.6	3.2	6.5	1.2	89	73	86	83	0.8	2.5	1.1	1.5	10 •	8 ⊙	9	SE 2	C 0	NE 2
26	69.7	67.5	64.2	67.1	1.8	10.7	3.3	4.8	10.7	0.5	89	50	81	73	0.8	6.4	1.4	2.9	9	4	2	C 0	C 0	C 0
27	61.1	61.6	64.2	62.3	-2.2	3.2	0.1	0.3	3.5	-2.9	98	88	100	95	0.1	0.9	0.0	0.3	8 ≡	8	10 ≡	C 0	SE 1	C 0
28	67.6	69.3	72.0	69.6	0.9	8.8	0.2	2.5	8.8	-0.3	98	71	96	88	0.1	3.3	0.3	1.2	7 ≡	2	6	NE 2	NE 2	C 0
29	73.8	73.2	72.9	74.0	5.0	5.6	0.0	2.6	6.4	-1.1	86	83	92	87	1.2	1.6	0.5	1.1	10	9 •	0	WSW 2	WSW 6	NE 1
30	70.4	70.1	64.0	68.2	4.6	7.4	6.0	6.0	7.8	-2.1	67	58	69	65	2.9	4.3	3.0	3.4	1	10	10	WSW 7	WSW 5	SW 6
31																								
M	73.2	73.1	73.1	73.1	1.6	6.0	2.6	3.2	7.0	-0.3	90	74	89	84	0.8	2.6	0.9	1.4	7.7	7.8	7.1	1.8	2.9	1.9

Grudzień – Décembre

1	59.0	60.0	60.2	59.7	8.6	10.6	10.4	10.0	11.5	5.8	76	70	76	74	2.8	3.8	3.0	3.2	10 •	9	9	SW 8	WSW 9	SW 9
2	55.9	54.6	63.7	58.1	10.8	12.7	4.7	8.2	13.2	4.5	73	69	64	69	3.6	4.6	3.1	3.8	10 •	9	0	SW 8	WSW 6	WSW 9
3	69.3	68.5	65.3	67.7	-1.9	6.0	1.9	2.0	6.5	-3.8	89	47	76	71	0.6	5.0	1.7	2.4	3	3	10	C 0	SW 8	SE 2
4	63.1	69.0	69.1	67.1	8.0	8.4	12.6	10.4	12.6	1.4	79	92	70	80	2.2	0.9	4.4	2.5	9 •	10 •	6	SW 4	W 3	SSW 6
5	69.1	68.0	67.1	68.1	14.9	15.9	14.5	15.0	16.3	11.8	63	58	58	60	6.2	7.7	7.0	7.0	8	9	3	SW 5	SW 5	WSW 5
6	71.5	72.9	74.1	72.8	3.8	2.4	1.2	2.2	14.5	1.0	67	55	70	65	2.6	3.5	2.0	2.7	10	10	10	W 9	W 8	W 5
7	74.1	75.1	77.7	75.6	0.2	0.8	-0.8	-0.2	1.7	-3.0	89	81	81	84	0.7	1.3	1.1	1.0	10 *	10	4	NW 3	WNW 2	WNW 1
8	78.0	78.3	79.4	78.6	-0.6	1.4	-1.8	-0.7	1.6	-3.6	72	67	73	71	1.7	2.3	1.4	1.8	10	3	0	WNW 3	W 6	ESE 2
9	76.6	73.4	71.3	73.8	-7.6	6.0	0.0	-0.4	6.3	-8.0	95	29	56	59	0.2	6.7	2.7	3.2	2	5	8	C 0	SSE 2	C 0
10	70.7	70.7	70.0	70.5	0.5	2.6	0.9	1.2	3.6	-0.7	84	77	90	84	1.0	1.7	0.6	1.1	9	9	6	C 0	E 2	SE 2
11	63.5	57.3	60.1	60.3	3.2	8.2	9.1	7.4	10.2	-0.4	85	83	80	82	1.3	1.8	2.4	1.8	10	10 •	10 •	WNW 1	WSW 9	W 9
12	65.7	66.9	70.5	67.7	7.6	8.0	7.4	7.6	9.8	7.1	93	89	91	91	0.7	1.2	0.9	0.9	10 •	10 ●	10 •	WNW 8	W 3	WNW 4
13	80.1	84.8	86.6	83.8	-0.6	-5.0	-5.5	-3.6	7.5	-7.1	87	86	82	85	0.7	0.7	0.7	0.7	10 *	10 *	9	N 3	ENE 5	E 3
14	85.2	87.7	91.7	88.2	-8.0	-6.1	-12.7	-9.9	-5.0	-13.2	75	55	86	73	0.8	1.7	0.3	0.9	3	2 ⊙	9	E 3	ESE 6	C 0
15	89.0	85.9	84.7	86.5	-7.8	-4.6	-6.3	-6.2	-5.1	-13.3	90	88	91	90	0.3	0.5	0.3	0.4	10 *	10 *	10 *	WNW 3	WNW 4	NNW 6
16	91.2	94.1	99.7	95.0	-14.9	-15.0	-24.3	-19.6	-5.8	-25.9	82	78	79	80	0.3	0.4	0.2	0.3	9 *	9 *	2	NW 1	C 0	C 0
17	101.2	100.6	100.9	100.9	-26.6	-14.6	-23.5	-22.0	-11.6	-27.0	77	87	88	84	0.2	0.3	0.1	0.2	0	0	0	C 0	E 1	C 0
18	100.1	99.4	98.2	99.2	-12.4	-8.2	-18.7	-14.5	-12.4	-25.2	81	81	84	82	0.4	0.6	0.2	0.4	10	9	0	C 0	NW 2	C 0
19	95.7	94.4	92.8	94.3	-16.0	-6.3	-4.2	-7.7	-1.9	-21.3	86	94	96	92	0.2	0.2	0.2	0.2	10	10 *	10 ●●	C 0	SE 1	WNW 2
20	87.6	81.8	77.0	82.1	-2.0	-0.4	0.8	-0.2	1.7	-4.3	100	94	94	96	0.0	0.3	0.4	0.2	10	9	10 ●	WNW 3	WNW 3	WNW 6
21	74.7	77.0	78.6	76.8	0.6	-0.2	-5.6	-1.7	1.2	-5.9	96	78	87	87	0.3	1.3	0.6	0.7	10 ●	6	9	WNW 8	WNW 5	NW 1
22	70.1	65.5	69.8	68.5	-0.9	0.2	-10.4	-5.4	0.6	-10.6	77	96	87	87	1.3	0.3	0.4	0.7	10	10 *	9	WSW 4	WNW 6	C 0
23	73.7	74.9	75.9	74.8	-7.4	-6.7	-18.0	-12.5	-5.5	-18.5	93	80	95	89	0.2	0.7	0.1	0.3	10 *	6	0	W 3	NW 2	C 0
24	73.7	74.3	73.3	74.4	-22.2	-13.8	-24.2	-21.1	-12.3	-25.0	96	88	79	88	0.0	0.3	0.2	0.2	0	0	0	C 0	C 0	C 0
25	70.3	69.3	68.3	69.3	-28.0	-14.4	-25.6	-23.4	-11.4	-28.7	76	87	88	84	0.1	0.3	0.1	0.2	0	0 ⊙	0	C 0	C 0	C 0
26	65.3	63.8	65.5	64.9	-24.0	-9.5	-21.4	-19.1	-8.4	-28.0	88	85	81	85	0.1	0.4	0.2	0.2	0	6	0	C 0	SE 2	C 0
27	69.1	69.6	69.3	69.3	-21.5	-11.8	-10.9	-13.8	-9.9	-21.7	81	82	73	79	0.2	0.4	0.7	0.4	7	2	0	SE 1	C 0	ENE 7
28	66.4	65.6	65.7	65.9	-12.2	-6.4	-7.2	-8.2	-4.9	-19.5	85	81	90	85	0.4	0.7	0.3	0.5	10	9	2	C 0	NW 2	W 2
29	67.1	66.7	66.3	66.7	-13.8	-9.2	-11.2	-9.8	-0.5	-14.7	92	70	93	85	0.2	1.4	0.2	0.6	0	1	0	NE 2	C 0	C 0
30	65.0	65.6	65.7	65.4	-11.2	1.6	-0.4	-2.6	2.5	-14.1	90	87	86	88	0.3	0.9	0.8	0.7	2	3	0	C 0	C 0	SE 2
31	66.8	64.3	61.1	64.1	-3.5	3.3	3.9	1.9	7.7	-4.3	94	78	75	82	0.3	1.7	2.0	1.3	4	5 ⊙	10	C 0	SE 1	E 2
M	74.3	74.2	74.8	74.5	-6.0	-1.2	-5.3	-4.4	1.3	-10.1	84	77	81	81	1.0	1.7	1.2	1.3	7.0	6.6	5.0	2.6	3.3	2.7

Jelenia Góra $H_s = 342\ m$ $H_b = 343{,}9\ m$ $h_w = 15\ m$ Listopad – Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.4	.	–	• 11⁴⁰ 12¹⁰ p 17⁰⁰
2	8	.	.	–	= 22³⁰–24 ⌒ 19⁰⁰–24
3	7	0.0	.	–	• 17⁴⁵ 18¹⁵ 23⁴⁵–24 = 0⁰⁰–1¹⁵ ⌒ 0⁰⁰–8⁰⁰
4	8	.	.	–	• 0⁰⁰ 1¹⁰ = 15²⁰–24
5	6	7.1	.	–	• 12⁴⁷ 13¹⁰ * 13⁴⁰–19²⁰ • –24 = 0⁰⁰–24
6	4	10.6	.	–	• 0⁰⁰ 7¹⁰–23⁴⁵ •• –24 = 0⁰⁰–24
7	6	0.3	.	–	•• 0⁰⁰ 4⁴⁵ • –10¹⁵ • p¹⁰…²⁵ = 0⁰⁰–8⁴⁵ ≡ –10⁴⁰ = –13³⁰
8	6	0.0	.	–	= 6⁵⁰ 17¹⁰
9	8	0.0	.	–	• 6¹⁰…³⁰ 12²⁰–³⁵ 0-1 19⁰⁰–24 ⌴ 1⁰⁰–5⁰⁰
10	6	4.2	.	–	• 7⁴⁰ 10¹⁵–17¹⁰ 21²⁰–22¹⁰ = 18⁵⁰–23⁴⁰ ≡ 1–24 ⌒ 1 0⁰⁰–7⁴⁰
11	6	1.0	.	–	• 8²⁰ 10⁴⁰ ≡ 1-0 0⁰⁰–3⁵⁰ = –24
12	7	0.0	.	–	= 0⁰⁰–6²⁰ 8⁵⁰–10⁴⁰ 15²⁰–24
13	5	16.9	.	–	• 6²⁰ 7⁴⁰ • 0-1 –18²⁵ = 0⁰⁰–24
14	4	1.2	.	–	• 3⁵⁰ 4¹⁰ • 13⁴⁵ ☁ 0⁰–15¹⁰ * 0⁰–17⁴⁵ • 19⁰⁵ 24 = 0⁰⁰–24
15	6	0.0	.	–	• 0⁰⁰ 4³⁵ ** 0⁰–6³⁰ △ 8³⁰–9⁴⁰ = 0⁰⁰–24
16	6	0.3	.	–	= 0⁰⁰–24
17	6	0.2	.	–	* 0³⁰–2⁵⁰ • 9⁰²⁰…³⁰ 14⁴⁰–19²⁰ 20³⁰–22²⁵ = 0⁰⁰–24
18	7	0.0	.	–	• 11¹⁰ 15⁰⁵ = 0⁰⁰–7¹⁵
19	6	0.0	.	–	* 10⁴⁵ 20¹⁵ = 3¹⁵–13¹⁰ 14³⁰–22³⁰ ⌴ 0-1 3⁰⁰–8⁰⁰
20	8	.	.	–	= 18³⁵–21⁴⁰
21	7	.	.	–	= 21⁴⁰–24 V 0⁰–10⁰–11¹⁰
22	8	.	.	–	= 0⁰⁰–4¹⁰ 17³⁰–24 ⌴ 0-1 0⁰⁰–11⁰⁰ 19⁰⁰–24
23	7	.	.	–	= 0⁰⁰–5¹⁵ 17³⁰–24 ⌴ 1-2 0⁰⁰–10⁰⁰ ⌴ 0 21⁰⁰–24
24	6	0.2	.	–	• 20³⁰…45 = 0⁰⁰–24 ⌴ 0-2 0⁰⁰–10⁰⁰
25	6	0.0	.	–	• 1⁴⁰ 8¹⁵ = 0⁰⁰–24
26	7	0.0	.	–	= 0⁰⁰–7¹⁵ 8⁴⁵–12¹⁵ ⌴ 0 22⁰⁰–24
27	5	0.4	.	–	• 13³⁵ 14¹⁰–16³⁰ 17¹⁵ = 1³⁰–5⁴⁵ ≡ 0–9⁴⁰ = –18⁴⁵ ≡ 0-1–20³⁵ ≡ 2–24 ⌴ 0-2 0⁰⁰–10⁰⁰
28	6	0.2	.	–	• 21⁴⁰ 23¹⁵ ≡ 1 0⁰⁰–2²⁰ ≡ 1-0 11²⁵ = 11⁴⁰–24 ⌴ 0 6⁰⁰–10⁰⁰
29	7	0.3	.	–	• 6¹⁰…³⁰ 9⁴⁰–10²⁰ • 0 ▽ –11³⁸ 12²⁰–13³⁸ = 0⁰⁰–8³⁰ 16³⁰–24
30	8	0.5	.	–	• 18⁴⁵ 20³⁵ 22⁴⁵–24
31					
Σ	–	45.8	–	–	UWAGI.

Grudzień – Décembre

1	8	0.6	.	–	• 0⁰⁰ 9²⁰ 15⁴⁰ 20¹⁰
2	8	2.1	.	–	• 0⁰²⁵ 7¹⁰ 9²⁰–³⁵ ▽ 0-1 15⁵⁰ 17¹⁵ 17⁵⁰–18⁰⁵ ⩥ 15⁴⁵–16⁵⁰
3	8	0.5	.	–	⌴ 0 5⁰⁰–10⁰⁰ 20⁰⁰–21⁰⁰
4	6	1.8	.	–	• 0-1 2⁴⁰ 13²⁰ = 12³⁵–17⁴⁰ ≡ 0–18³⁵ = –24
5	8	.	.	–	= 0⁰⁰–6¹⁰
6	8	0.0	.	–	
7	6	0.0	.	–	* 0 6⁴⁵ 7²⁰–10¹⁰ = 8⁵⁰–24
8	7	0.0	.	–	* 0 2⁴⁰ 6¹⁰ * 0 ▽ 10³⁵–⁴⁵ = 0⁰⁰–7³⁰
9	7	0.0	.	–	* 0 23⁴⁰ 24 = 6⁴⁰–10³⁰ ⌴ 0 0⁰⁰–11⁰⁰
10	8	.	.	–	• 0 0⁰⁰ 1²⁵ △ 0 2¹⁵–4¹⁰ * 0 6³⁰ = 17³⁰–24
11	6	20.7	.	–	• 0-1 7⁴⁵ 24 = 0⁰⁰–5²⁰
12	5	9.9	.	–	• 0 0⁰⁰ 5¹⁰ • 1–6⁴⁰ • 0–10⁴⁰ • 0 11⁴⁵–13²⁵ • 14⁴⁰ 24 = 0⁰⁰–24
13	5	0.4	2	–	• 1 0⁰⁰–3¹⁵ * 4¹⁰–7¹⁵ 10¹⁵ 11⁴⁵–13¹⁰ = 0⁰⁰–13³⁰
14	8	0.6	2	–	
15	5	7.4	5	–	* 0-1 3¹⁰–12¹⁵ 12⁵⁰–22¹⁵ = 22¹⁵–24
16	5	1.0	22	–	* 0 6¹⁵ 13³⁵ 14⁴⁵ 16⁴⁰ = 0⁰⁰–15¹⁰ p
17	6	0.0	25	–	= 0⁰⁰–6¹⁰ 9¹⁵–12³⁰ 17³⁰–24 ⩥ 12³⁰–15³⁰
18	6	.	25	–	* 3¹⁵ 4²⁰ = 0⁰⁰–24
19	4	0.8	20	–	* 0 9³⁵–15²⁰ ☁ 16⁴⁰–24 = 0⁰⁰–24
20	5	1.3	15	–	☁ 0 0⁰⁰–5⁰⁵ ☁ 0-1 16¹⁰–24 = 0⁰⁰–24
21	8	1.0	11	–	☁ 0 0⁰⁰–7³⁵ 7⁴⁰–9³⁵ △ –11¹⁵ ▽ 14⁰¹–16²⁰ = 0⁰⁰–11²⁰
22	6	3.1	9	–	* 0 3¹⁰ 5³⁵ 7⁴⁵–8⁰⁵–9⁰⁷ * 1-0 9¹⁰–15⁵⁰
23	6	0.1	16	–	* 1⁰⁰–10²⁰ 10⁴⁰–11¹⁵ = 8²⁰–24
24	5	.	15	–	= 0⁰⁰–24
25	6	.	15	–	= 0⁰⁰–6³⁰ 11⁴⁵–24
26	6	.	15	–	= 0⁰⁰–2⁰⁰ 9³⁰–24
27	5	.	14	–	= 0⁰⁰–24
28	6	.	14	–	= 0⁰⁰–24
29	6	.	14	–	= 0⁰⁰–4¹⁰ 6⁵⁰–14²⁰ 16³⁰–22⁴⁰ ≡ –23⁴⁰ ≡ 2–24
30	6	.	14	–	≡ 2-0 0⁰⁰–6²⁰ = –13³⁰ 18³⁰–24
31	7	.	14	–	= 0⁰⁰–6²⁰
Σ	–	51.3	–	–	UWAGI.

Śnieżka — φ = 50°44' — λ = 15°44' — Styczeń - Janvier 1961

DNI	CIŚNIENIE P − 800				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	29.6	30.8	30.7	30.4	-6.2	-5.8	-7.0	-6.5	-5.4	-7.8	94	95	93	94	0.2	0.2	0.2	0.2	8	6 ⊙	8	W 10	SW 8	SW 15
2	29.2	27.3	25.0	26.5	-6.0	-4.6	-7.4	-6.4	-5.7	-8.6	89	96	93	93	0.4	0.2	0.2	0.3	10	0 ⊙	10 =	NW 1	W 5	SW 17
3	15.6	14.8	18.3	16.2	-5.1	-5.2	-2.8	-4.0	-2.5	-8.5	95	90	95	95	0.2	0.4	0.4	0.3	8	9	10 * =	SSW25	SSW25	SSW15
4	14.0	14.3	18.5	15.6	-5.2	-4.1	-5.8	-4.7	-2.8	-5.9	95	96	95	95	0.2	0.2	0.2	0.2	10 =	10 * =	10△ =	SSW20	SW 17	SW 17
5	21.1	21.7	27.0	23.3	-5.7	-6.8	-6.2	-6.2	-5.5	-7.4	95	94	94	94	0.2	0.2	0.2	0.2	8	10 =	10 =	SW 15	SW 20	W 15
6	27.4	26.3	24.8	26.2	-8.8	-8.4	-7.7	-8.2	-6.2	-8.9	92	92	95	92	0.3	0.3	0.2	0.3	9	10 =	10 =	SW 25	SW 20	SW 20
7	22.3	23.0	26.2	23.8	-7.9	-7.3	-6.5	-7.0	-6.5	-7.9	95	95	91	92	0.2	0.2	0.3	0.2	10 =	10 =	10 * =	SW 25	SW 22	W 11
8	28.1	23.4	24.5	25.3	-7.6	-7.4	-7.1	-7.3	-6.5	-8.2	90	90	93	91	0.3	0.3	0.2	0.3	10 =	10 * =	10 * =	W 10	SW 17	SW 17
9	26.1	26.6	25.9	26.2	-6.0	-6.2	-5.4	-5.8	-5.1	-7.1	94	94	95	94	0.2	0.2	0.2	0.2	10 =	10 =	10 * =	SW 15	SW 15	SW 20
10	27.8	26.1	25.2	26.4	-7.0	-7.2	-7.0	-7.0	-5.2	-7.9	93	93	93	93	0.2	0.2	0.2	0.2	10 =	8	10	W 9	WSW20	WSW20
11	27.0	30.3	33.2	30.2	-6.8	-4.4	-8.2	-6.9	-2.1	-8.8	94	64	92	83	0.2	1.6	0.2	0.7	9	10	10 * =	WSW10	W 2	NW 15
12	36.5	39.0	42.2	39.2	-12.9	-12.0	-12.4	-12.4	-8.2	-14.8	92	89	89	90	0.2	0.3	0.3	0.3	10 =	10 * =	0	NW 15	NNW13	N 8
13	43.6	43.5	43.9	43.7	-11.6	-7.0	-0.8	-5.0	-0.8	-12.8	82	85	99	89	0.4	0.5	0.0	0.3	4	7	10	W 2	NNW 4	NW 1
14	42.1	41.7	43.2	42.3	-0.2	-4.3	-6.7	-4.5	0.3	-7.4	100	96	94	97	0.0	0.2	0.2	0.1	10	10 * =	10 * =	WSW 2	NNW 4	N 9
15	43.7	46.7	45.3	45.9	-4.9	-5.5	-0.8	-2.5	-0.8	-6.7	69	35	16	40	1.3	3.1	4.8	3.1	2	1	0	E 12	SE 7	SE 4
16	40.8	39.6	38.9	39.8	-1.8	-0.8	-4.8	-5.0	1.2	-5.9	16	56	88	53	4.4	2.6	0.5	2.5	6	0	2	N 6	N 8	NNE20
17	39.4	41.8	42.9	41.4	-8.8	-8.4	-12.7	-10.6	-5.8	-12.7	30	26	33	30	2.2	2.4	1.6	2.1	0	1 ⊙	0	NNE20	NE 12	NE 18
18	45.1	45.3	45.6	45.3	-12.4	-12.6	-8.6	-10.6	-8.6	-13.4	18	37	20	25	1.9	1.5	2.6	2.0	0	1 ⊙	0	NE 15	SSE15	SSE14
19	44.2	42.2	42.5	43.0	-5.6	-6.6	-5.2	-5.6	-5.1	-9.4	28	25	56	36	2.9	2.9	1.8	2.5	0	0 ⊙	0	S 6	S 9	S 9
20	40.9	39.4	37.2	39.2	-4.8	-5.8	-7.5	-6.4	-4.1	-7.6	57	67	63	62	1.8	1.3	1.3	1.5	0	0 ⊙	0	C 0	SW 6	S 4
21	34.6	34.0	33.2	33.9	-7.5	-5.0	-6.4	-6.3	-3.9	-9.0	63	73	52	63	1.3	1.1	1.8	1.4	0	5 ⊙	0	C 0	C 0	ENE 2
22	31.1	29.8	28.7	29.9	-6.8	-6.6	-5.8	-6.2	-5.2	-7.2	86	88	92	89	0.5	0.4	0.3	0.4	3	9 *	9 *	WNW 6	W 6	W 4
23	25.9	25.6	25.9	25.8	-6.0	-5.2	-7.8	-6.7	-5.0	-8.6	92	95	90	92	0.3	0.3	0.3	0.3	10 * =	10 *	10 * =	W 3	SW 1	SE 6
24	26.5	25.7	25.7	25.3	-8.2	-7.0	-7.8	-7.7	-6.5	-9.5	87	93	87	89	0.4	0.2	0.4	0.3	9	8	8	SE 4	SE 2	SE 2
25	20.7	21.2	22.7	21.5	-14.8	-16.4	-16.8	-16.2	-7.7	-17.4	87	85	85	86	0.3	0.2	0.2	0.2	4	4	1	E 5	E 10	E 15
26	27.5	32.7	37.1	32.4	-12.4	-8.3	-8.6	-9.5	-7.5	-18.3	22	26	25	24	1.8	2.4	2.5	2.2	0	0 ⊙	0	ESE 20	SSE 7	S 9
27	41.2	41.2	39.2	40.5	-7.3	-7.4	-9.6	-8.5	-7.2	-9.6	20	19	29	23	2.8	2.8	2.1	2.6	0	0 ⊙	0	S 7	S 15	SW 20
28	38.6	33.8	30.4	34.3	-7.6	-8.6	-7.2	-7.6	-1.8	-10.0	24	33	50	36	2.6	2.1	1.8	2.2	5	8	7	SW 17	SW 25	SW 35
29	30.5	34.8	30.7	32.0	-4.8	-4.7	-4.6	-4.7	-2.8	-10.1	95	93	95	94	0.2	0.3	0.3	0.3	10 =	10 =	10 =	SW 20	W 18	W 30
30	25.4	20.7	25.2	23.8	-7.0	-5.2	-2.4	-4.2	-2.4	-7.1	91	93	98	94	0.3	0.3	0.1	0.2	10 =	10 * =	10 =	W 30	SW 35	SW 20
31	21.1	16.9	22.2	20.1	-2.3	-1.3	-4.4	-3.1	-1.0	-4.4	98	97	93	96	0.1	0.2	0.3	0.2	10 * =	10 * =	10 * =	SW 17	SW 16	SW 25
M	31.3	31.0	31.5	31.3	-7.0	-6.6	-6.8	-6.8	-4.3	-9.3	74	74	77	75	0.9	0.9	0.8	0.9	6.1	6.4	6.3	11.9	12.3	14.0

Luty - Février

1	17.4	14.5	17.0	16.3	-5.0	-5.8	-6.4	-5.4	-3.7	-7.0	95	96	94	95	0.2	0.2	0.2	0.2	10 * =	10 =	10 =	SW 20	SW 15	W 10
2	15.8	12.4	8.7	12.3	-7.6	-7.4	-7.8	-7.6	-6.3	-7.8	93	87	90	90	0.2	0.4	0.3	0.3	10 *	5 ⊙	10 =	WSW10	WSW13	WSW15
3	11.3	14.0	18.2	14.5	-7.5	-7.9	-8.6	-8.2	-6.9	-9.1	90	90	89	90	0.3	0.3	0.4	0.3	10 * =	10 * =	10 * =	WNW17	NW 15	NNW17
4	22.7	21.2	15.2	19.7	-9.7	-9.0	-9.6	-9.5	-8.6	-10.5	88	92	91	90	0.4	0.3	0.3	0.3	10 * =	10 =	10 =	N 17	WSW12	WSW25
5	21.8	28.5	33.4	27.9	-8.6	-9.0	-10.8	-9.8	-8.2	-11.3	92	86	90	89	0.3	0.4	0.3	0.3	10 * =	10 =	0	NW 15	N 17	NNW 6
6	32.5	31.6	27.8	30.6	-11.0	-9.6	-4.4	-7.4	-4.3	-11.8	90	91	96	92	0.3	0.3	0.2	0.3	10 =	10 =	10 * =	SW 12	SW 15	SSW20
7	25.0	24.3	25.0	24.8	-4.8	-5.4	-5.6	-5.4	-3.2	-6.0	95	98	97	97	0.2	0.1	0.1	0.1	8	10 =	10 =	WSW15	SW 20	SW 24
8	28.4	30.4	34.4	31.1	-6.0	-6.0	-6.2	-6.1	-5.2	-6.3	97	89	92	93	0.1	0.4	0.3	0.3	10 *	10 * =	10 =	NW 18	NW 16	NW 16
9	31.3	27.8	26.1	28.5	-5.0	-2.8	-1.6	-2.8	-1.4	-6.8	90	97	98	95	0.4	0.1	0.1	0.2	10 * =	10 * =	10 * =	WNW18	W 22	NW 26
10	30.4	36.6	41.2	36.1	-5.4	-6.2	-5.6	-5.7	-1.5	-6.2	95	94	92	94	0.2	0.2	0.3	0.2	10 * =	10 * =	10 =	NNW38	NNW30	NNW12
11	35.4	38.8	29.9	32.0	-4.8	-5.9	-5.2	-5.8	-3.0	-6.3	91	94	92	92	0.4	0.3	0.3	0.3	10	9	10 * =	NNW20	SW 20	WSW20
12	23.5	26.1	34.0	27.9	-5.6	-4.0	-5.8	-5.8	-3.0	-4.0	94	96	96	95	0.3	0.2	0.2	0.2	10 * =	10 * =	10 * =	WSW12	W 12	NW 20
13	37.4	38.9	40.6	39.0	-4.5	-5.9	-5.0	-5.6	-3.0	-5.0	96	94	95	95	0.2	0.3	0.3	0.3	10	8 ⊙	10 =	W 8	WNW 4	NW 4
14	42.4	44.1	44.7	43.7	-1.9	1.2	1.8	0.7	2.7	-3.3	96	96	68	87	0.2	0.3	2.3	0.9	10 9 =	3 ⊙	0	NW 6	NW 4	NNW 8
15	45.7	47.6	48.9	47.4	2.7	5.2	4.2	4.1	5.2	1.5	31	35	54	40	5.1	5.7	3.8	4.9	2	1 ⊙	0	NNW10	NNW 8	WNW12
16	46.7	48.7	51.8	49.1	-1.9	-1.8	-0.3	-1.1	4.3	-4.4	98	98	98	98	0.1	0.1	0.2	0.1	10 =	10 =	0	NW 15	NNW14	N 3
17	52.6	53.3	53.3	53.1	5.7	5.4	5.5	5.5	7.1	-1.3	29	43	34	35	6.5	5.2	5.9	5.9	6 ⊙	6 ⊙	0	C 0	C 0	N 4
18	52.0	50.0	48.6	50.2	6.8	5.9	4.4	5.4	7.2	2.6	24	29	34	29	7.5	6.5	5.6	6.5	0 ⊙	0 ⊙	0	N 6	SW 15	NNW 9
19	46.2	46.2	46.2	46.2	-0.5	-0.5	-2.8	-1.6	4.4	-5.1	100	96	93	96	0.0	0.3	0.4	0.2	2 ⊙	10 =	10 =	WNW12	NW 6	N 16
20	45.7	48.4	48.8	47.6	-4.6	-2.4	-1.6	-2.6	-1.0	-5.5	91	98	86	92	0.4	0.1	0.8	0.4	10 =	10 =	0	N 16	N 7	E 10
21	47.4	46.3	45.2	46.3	-0.8	-4.7	-5.8	-4.3	-0.6	-6.2	63	93	92	83	2.1	0.3	0.3	0.9	0 ⊙	10 =	10 =	SE 6	S 15	S 15
22	47.2	47.7	46.6	47.2	-1.3	0.8	1.0	0.4	2.0	-7.0	72	49	69	63	1.6	3.3	2.1	2.3	0 ⊙	1 ⊙	2	NNE 3	ESE 4	E 8
23	44.7	44.4	43.2	44.1	-1.0	0.6	-0.7	-0.4	1.0	-1.5	63	42	64	56	2.2	3.7	2.1	2.7	2 ⊙	4 ⊙	1	S 14	S 7	S 12
24	45.3	44.9	45.6	44.6	1.0	2.0	1.7	1.6	4.0	-1.5	52	46	68	55	3.2	3.9	2.2	3.1	0 ⊙	0 ⊙	2	W 3	NW 3	N 6
25	45.3	45.9	45.2	45.5	2.5	4.6	0.8	2.2	5.1	0.8	21	12	19	17	5.8	7.4	5.2	6.1	1 ⊙	1 ⊙	1	NNE 2	SW 4	SW 17
26	46.4	48.6	48.9	48.0	3.6	3.4	2.4	3.0	4.6	0.5	6	66	88	53	7.4	2.7	0.9	3.7	0 ⊙	1 ⊙	0	WNW 8	NW 8	W 12
27	47.3	45.7	43.0	45.3	1.5	2.0	2.6	2.2	3.1	0.4	94	98	100	97	0.4	0.2	0.0	0.2	8 ⊙	10	10 =	SW 12	SW 20	WSW25
28	34.6	27.6	30.8	31.0	1.0	-2.2	-6.0	-3.3	3.0	-6.0	100	98	94	97	0.0	0.1	0.2	0.1	10 =	10 =	10 * =	SW 20	SW 20	W 25
29																								
30																								
31																								
M	36.4	36.7	37.2	36.8	-2.3	-2.1	-2.5	-2.4	-0.2	-4.7	77	79	81	79	1.6	1.5	1.3	1.5	6.8	7.1	5.9	12.6	12.2	14.2

Śnieżka — $H_s = 1603\,m$ — $H_k = 1610{,}6\,m$ — Styczeń – Janvier 1961

DNI	WILGOTNOŚĆ WZGLĘDNA %	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	0.0	11	–	
2	8	1.8	10	–	
3	8	1.8	12	–	
4	0	3.5	15	–	
5	0	4.9	18	–	
6	0	3.1	21	–	
7	0	6.6	25	–	
8	0	8.8	30	–	
9	0	4.0	35	–	
10	8	4.0	38	–	
11	8	4.0	40	–	
12	0	2.6	41	–	
13	9	.	44	–	
14	1	10.3	42	–	
15	9	.	46	–	
16	9	.	44	–	
17	9	.	44	–	
18	9	.	40	–	
19	9	.	38	–	
20	9	.	36	–	
21	9	.	35	–	
22	8	0.4	34	–	
23	7	1.1	35	–	
24	9	.	40	–	
25	8	.	38	–	
26	9	.	38	–	
27	9	.	36	–	
28	9	.	34	–	
29	0	3.0	34	–	
30	0	6.0	32	–	
31	0	3.8	37	–	
Σ	—	69.7	—	–	UWAGI

Luty – Février

DNI	WILGOTNOŚĆ WZGLĘDNA %	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	8.2	40	–	
2	7	8.1	46	–	
3	0	11.4	55	–	
4	0	7.8	65	–	
5	0	6.7	72	–	
6	0	2.6	75	–	
7	0	7.4	77	–	
8	0	8.1	70	–	
9	0	27.5	64	–	
10	0	4.1	60	–	
11	8	2.1	63	–	
12	0	18.4	65	–	
13	8	0.2	68	–	
14	8	0.1	68	–	
15	9	.	60	–	
16	0	1.0	55	–	
17	9	.	54	–	
18	9	.	50	–	
19	0	3.8	47	–	
20	0	0.2	48	–	
21	0	.	48	–	
22	9	.	48	–	
23	9	.	45	–	
24	9	.	44	–	
25	9	.	42	–	
26	8	.	40	–	
27	8	3.6	36	–	
28	0	2.6	30	–	
29					
30					
31					
Σ	—	124.2	—	–	UWAGI:

Śnieżka — φ = 50°44' — λ = 15°44' — Marzec – Mars 1961

Dni	CIŚNIENIE P − 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			WIATR D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	31.7	34.9	39.4	35.3	−5.8	−5.6	−5.5	−5.6	−5.2	−6.7	89	95	92	92	0.4	0.2	0.3	0.3	10 ≡	10 * ≡	10 * ≡	W 8	NW 12	NNW 14
2	41.1	42.6	40.9	41.5	−6.0	−5.0	−5.2	−5.4	−4.9	−6.8	94	95	90	93	0.2	0.2	0.4	0.3	4 ⊙	5 ⊙	9	NW 17	W 12	W 12
3	40.9	44.6	46.4	44.0	−5.8	−1.1	−5.2	−2.8	−0.8	−5.8	96	97	97	97	0.2	0.2	0.1	0.2	10 ≡	10 ≡	10 * ≡	W 6	NW 4	NW 9
4	48.4	49.7	51.0	49.7	−4.4	−1.8	−4.8	−4.0	−1.0	−4.9	96	98	95	96	0.2	0.1	0.2	0.2	10 ≡	10 ≡	5	N 3	N 8	NW 8
5	50.3	50.4	49.9	50.2	−2.0	−0.8	−2.4	−1.9	−0.7	−6.5	98	85	98	94	0.1	0.9	0.1	0.4	7	8	9	WNW 12	WNW 16	WNW 17
6	50.1	51.5	50.6	50.7	0.7	5.8	6.1	4.7	7.1	−5.4	51	28	23	27	4.4	6.6	7.3	6.1	6 ⊙	9 ⊙	0	NNW 14	N 1	W 2
7	46.6	47.2	48.1	47.3	1.7	2.5	0.2	1.2	6.7	0.2	72	52	60	61	1.9	3.5	2.5	2.6	4 ⊙	7 ⊙	5	WNW 10	NNW 15	NNW 15
8	49.3	52.5	51.7	51.2	−0.2	4.9	2.5	2.4	6.2	−1.6	28	27	22	26	4.3	6.4	5.7	5.5	1 ⊙	2 ⊙	0	NW 15	N 12	N 20
9	50.5	51.4	50.1	50.7	1.4	5.0	5.6	4.4	6.9	1.2	68	50	11	36	2.2	6.1	8.0	5.4	6 ⊙	2 ⊙	0	NW 16	NNW 8	N 7
10	47.9	46.0	43.7	45.9	6.8	6.8	4.3	5.6	8.5	0.5	15	34	64	38	8.4	6.6	3.0	6.0	0 ⊙	2 ⊙	0	NNW 2	SW 6	SW 12
11	41.0	41.8	42.2	41.7	0.6	−0.3	−1.6	−0.7	4.5	−1.6	98	98	96	97	0.1	0.2	0.2	0.2	6 ⊙	9	9	W 17	W 20	W 20
12	40.3	38.4	33.2	37.3	0.2	3.4	4.0	2.9	4.6	−3.3	94	77	63	78	0.4	1.8	3.0	1.7	7	8 ⊙	7	W 18	W 25	WSW 25
13	27.9	30.0	32.4	30.1	−3.8	−3.8	−2.8	−3.3	4.6	−5.0	96	92	97	95	0.2	0.4	0.1	0.2	10 * ≡	8	10 ≡	W 20	NW 20	NW 28
14	32.4	33.5	35.6	33.8	0.3	1.0	−0.7	0.0	1.1	−3.2	100	100	95	98	0.0	0.0	0.3	0.1	10 • ≡	10 • ≡	10 ≡	NW 16	NW 20	NW 18
15	36.5	38.9	41.6	39.0	−0.2	0.1	0.3	0.1	0.4	−1.1	96	98	98	97	0.2	0.2	0.1	0.2	10 ≡	10 ≡	10 ≡	NW 20	WNW 20	WNW 22
16	38.3	38.7	39.8	38.9	0.6	0.8	0.2	0.4	1.0	−0.8	90	80	96	89	0.7	1.3	0.3	0.8	8 ⊙	6 ⊙	10 ≡	NW 22	NW 22	NW 28
17	45.1	45.1	38.1	41.4	0.8	5.9	4.4	3.9	7.0	−2.3	38	70	57	55	4.0	2.8	3.6	3.5	6 ⊙	2 ⊙	8	NW 16	WNW 10	SW 15
18	28.9	27.5	24.4	26.9	4.0	2.0	−2.4	0.3	5.0	−2.5	68	100	93	87	2.6	0.0	0.3	1.0	6 ⊙	10 ≡	10	SW 25	SW 25	SW 16
19	21.7	22.7	26.0	23.5	−7.2	−5.8	−8.6	−7.6	−2.2	−9.0	90	95	92	92	0.3	0.2	0.3	0.3	10 ≡	8	10 ≡	WNW 16	W 15	WNW 10
20	26.5	25.4	14.7	22.2	−12.2	−9.0	−8.8	−9.7	−7.9	−13.5	81	82	92	85	0.4	0.5	0.3	0.4	5 ⊙	9 *	10 * ≡	NW 5	W 8	SSW 30
21	10.4	11.3	17.4	13.0	−7.8	−6.3	−7.6	−7.3	−6.0	−8.8	93	91	90	91	0.2	0.3	0.3	0.3	10 * ≡	10 * ≡	10 * ≡	SSW 20	SW 20	SW 20
22	25.1	28.1	28.8	27.3	−10.8	−8.7	−8.4	−9.1	−7.4	−12.1	87	86	89	87	0.4	0.4	0.3	0.4	10 * ≡	10 * ≡	10 * ≡	SW 18	NNW 12	W 17
23	29.4	31.2	34.0	31.5	−5.0	−3.3	−5.0	−5.6	−3.0	−8.6	95	99	97	97	0.2	0.0	0.1	0.1	10 ≡	10 * ≡	10 * ≡	NW 16	NW 15	NW 18
24	34.8	35.6	35.9	35.4	−5.6	−2.4	−2.4	−2.7	−2.0	−4.0	97	96	96	96	0.2	0.2	0.2	0.2	10 * ≡	10 ≡	10 ≡	WNW 18	WNW 18	WNW 18
25	36.9	39.0	39.7	38.5	−2.3	−1.4	−2.2	−2.0	−1.1	−3.3	96	97	98	97	0.3	0.2	0.1	0.2	10 ≡	10 ≡	10	WNW 19	WNW 10	NW 9
26	37.4	35.0	27.8	33.4	−5.6	−2.2	−1.0	−2.0	−1.0	−5.9	97	98	95	97	0.2	0.1	0.3	0.2	10 *	10	9	W 10	W 10	WSW 20
27	25.5	25.7	24.9	25.4	−7.2	−6.6	−8.9	−7.9	−1.0	−8.9	95	88	89	90	0.2	0.4	0.4	0.3	8	8 * ⊙	10 * ≡	WSW 15	WNW 17	NW 17
28	25.7	25.2	27.1	25.3	−10.4	−8.0	−8.0	−8.8	−7.7	−10.7	87	95	93	91	0.4	0.2	0.2	0.3	10 * ≡	10 * ≡	10 ≡	NW 20	WSW 20	NW 18
29	27.0	27.9	28.4	27.8	−7.2	−2.7	−5.6	−4.5	−2.6	−8.0	95	97	97	96	0.2	0.1	0.2	0.2	10 * ≡	10 * ≡	10 * ≡	WNW 14	NW 20	W 14
30	24.4	26.1	22.8	24.4	−5.6	−1.6	−0.7	−1.6	−0.6	−5.7	94	96	97	96	0.3	0.2	0.2	0.2	10 * ≡	10 * ≡	10 * ≡	W 17	WSW 17	WSW 25
31	25.4	25.7	25.2	24.8	−1.6	−2.4	−5.4	−5.7	0.6	−5.4	96	98	95	96	0.2	0.1	0.2	0.2	10 * ≡	10 ≡	10 ≡	WNW 17	WSW 4	WNW 17
M	35.2	36.2	35.9	35.8	−5.0	−1.3	−2.2	−2.2	0.3	−4.9	85	85	83	85	1.1	1.3	1.2	1.2	7.9	8.2	7.7	14.9	14.3	16.8

Kwiecień – Avril

1	27.1	24.5	26.2	25.9	−6.8	−0.8	0.0	−1.9	0.0	−9.1	94	99	100	98	0.2	0.0	0.0	0.1	10 * ≡	10 ≡	10 * ≡	W 15	SW 17	W 14
2	26.3	27.3	25.8	26.5	−4.3	−2.4	0.3	−1.5	0.4	−4.3	94	96	100	97	0.3	0.2	0.0	0.2	10	10 * ≡	10 • ≡	W 14	W 18	W 20
3	23.3	24.9	27.0	25.1	−0.2	−1.8	−1.2	−1.1	0.4	−1.8	98	94	99	97	0.1	0.3	0.1	0.2	10 * ≡	8	10 ≡	W 25	W 20	W 15
4	25.9	29.9	32.5	29.4	0.0	−0.2	0.2	0.0	0.2	−1.2	100	100	100	100	0.0	0.0	0.0	0.0	10 • ≡	8 ⊙	10 • ≡	W 17	W 14	W 14
5	31.8	32.5	33.2	32.5	4.1	6.1	5.5	5.3	8.5	0.2	84	86	95	88	1.3	1.3	0.4	1.0	7 ⊙	6 ⊙	8	S 17	SW 18	WSW 20
6	35.3	37.1	35.7	36.0	8.2	9.2	6.8	7.8	10.7	5.3	63	72	89	75	4.0	3.3	1.1	2.8	5 ⊙	4 ⊙	3	SW 18	SW 10	W 15
7	36.3	37.9	36.9	37.0	9.2	11.8	8.6	9.6	11.9	5.8	48	59	71	59	6.0	5.7	3.3	5.0	3	4 ⊙	9 •	SSW 7	WSW 8	WSW 17
8	34.1	31.9	33.9	33.3	4.9	5.4	−3.0	1.1	8.6	−3.0	100	100	95	98	0.0	0.0	0.3	0.1	8	10 • ≡	10 ≡	W 17	W 25	W 18
9	35.1	37.9	36.9	36.6	−5.4	−5.2	−5.4	−5.8	−0.4	−6.2	92	97	97	95	0.3	0.1	0.2	0.2	10 ≡	5	5	W 14	WNW 8	W 5
10	33.7	32.4	30.8	32.3	−0.6	−0.3	0.4	0.0	0.6	−6.0	55	58	95	62	3.8	2.5	0.5	2.3	7	9	9 *	WSW 10	SSW 3	SW 8
11	29.9	31.5	33.2	31.5	2.3	4.9	−0.2	1.7	5.0	−0.2	100	85	96	94	0.0	1.3	0.2	0.5	10 ≡	8 ⊙	0	NW 4	N 4	NNW 6
12	35.4	37.7	37.8	37.0	−0.1	5.0	3.2	2.8	6.7	−0.9	70	64	81	72	1.8	3.1	1.5	2.1	1 ⊙	4 ⊙	3	N 3	W 4	W 8
13	36.7	37.5	37.3	37.2	3.7	6.2	7.2	6.1	9.1	2.8	100	86	77	88	0.0	1.4	2.4	1.3	6 ⊙	6 ⊙	3	SW 10	WSW 10	W 8
14	34.9	34.0	34.2	34.4	6.2	9.7	9.6	8.8	11.1	4.9	54	62	53	56	4.3	4.5	5.6	4.8	2 ⊙	4 ⊙	4	WSW 10	S 9	S 8
15	34.1	34.0	32.9	33.7	6.1	9.6	4.4	6.1	11.2	3.9	70	65	100	78	2.8	4.2	0.0	2.3	1 ⊙	8 ⊙	10 ≡	ESE 4	ESE 3	SW 8
16	32.7	32.0	32.1	32.3	4.4	5.6	2.8	3.9	6.5	1.8	90	94	100	95	0.9	0.6	0.0	0.5	9	10	10 ≡	SW 5	SW 8	SW 8
17	32.6	34.1	35.0	33.9	1.4	4.5	3.8	3.4	5.2	0.8	83	91	79	84	1.2	0.7	1.7	1.2	6	9	1	WSW 8	WNW 1	S 1
18	34.6	34.8	35.5	35.0	5.2	7.0	4.0	5.0	8.1	3.4	59	64	79	67	3.6	3.6	1.7	3.0	3 ⊙	9	5	C 0	NE 5	NNE 7
19	36.2	37.6	37.1	37.0	2.2	3.6	0.8	1.8	5.1	0.5	100	91	90	94	0.0	0.7	0.7	0.5	10 ≡	7	0	N 5	N 3	N 10
20	37.4	38.9	38.6	38.3	1.8	3.0	3.0	2.7	4.1	−1.1	91	85	46	54	4.8	1.1	4.1	3.3	7 ⊙	8 ⊙	0	NE 8	E 5	N 4
21	37.3	36.9	34.8	36.3	3.2	6.3	3.3	4.0	7.3	1.3	73	47	100	73	2.1	5.0	0.0	2.4	0 ⊙	0 ⊙	7	N 2	SE 4	S 17
22	30.4	29.1	26.9	28.8	0.7	3.2	1.8	1.9	3.6	−0.1	100	93	100	98	0.0	0.3	0.0	0.2	10 ≡	9	10 ≡	SSW 20	SSW 25	SSE 20
23	23.4	25.2	25.3	24.6	−0.2	1.8	2.0	1.4	2.5	−0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ≡	10 ≡	10 ≡	S 25	S 24	SSW 25
24	27.4	29.9	30.3	29.2	1.4	6.1	1.7	2.7	7.3	0.9	100	72	92	88	0.0	2.6	0.5	1.0	9	7 ⊙	0	SW 16	SSE 4	NE 8
25	30.2	31.3	30.9	30.8	3.4	6.0	−0.4	2.2	8.2	−0.7	50	81	100	77	3.9	1.8	0.0	1.9	0 ⊙	2 ⊙	10 ≡	N 6	N 2	SE 7
26	28.9	29.2	30.0	29.4	3.0	6.0	4.3	4.5	8.2	−1.3	56	79	97	77	3.4	2.0	0.3	1.9	5 ⊙	6 ⊙	7	SSE 2	SSE 8	SE 7
27	30.6	32.0	32.6	31.7	4.6	3.2	1.4	2.6	5.1	1.4	97	97	100	98	0.3	0.3	0.0	0.2	6	10 ≡	10 ≡	NNE 8	WNW 6	WNW 10
28	31.7	31.7	30.9	31.4	0.6	1.9	2.1	1.7	3.1	0.1	96	100	100	99	0.3	0.0	0.0	0.1	10 ≡	10 ≡	9	NW 6	NW 1	NW 2
29	30.0	30.6	31.3	30.6	2.3	3.3	2.7	2.8	4.4	1.0	95	100	100	98	0.4	0.0	0.0	0.1	9 ⊙	10 ≡	10• ≡	S 6	S 8	S 6
30	30.9	31.0	31.0	31.0	3.9	4.2	4.7	4.4	7.3	2.0	77	77	100	85	1.8	1.8	0.0	1.2	6 ⊙	8	10 ≡	E 2	SE 6	NNE 6
31																								
M	31.8	32.5	32.6	32.3	2.2	4.2	2.6	2.9	5.7	0.0	80	83	91	85	1.6	1.6	0.8	1.3	6.7	7.3	6.8	10.1	9.4	10.7

Śnieżka

$H_s = 1603\ m$ $H_b = 1610{,}6\ m$

Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	5.7	31	–	$*^{0}0^{00}-6^{20}$, 8^{30} $18^{00}-21^{30}$, $V^{1}0^{00}-8^{00}$ $V^{0}-24$, $\equiv^{2}0^{00}-24$, $*\overset{+}{\uparrow}^{2-0}0^{00}-6^{20}$ $*\overset{+}{\uparrow}^{0}12^{00}-21^{30}$ $\overset{+}{\uparrow}^{0}-24$, $\nwarrow 0^{00}-4^{30}$ $\gg -6^{20}$, $12^{00}-24$
2	8	0.8	33	–	$V^{0}0^{00}-6^{30}$, $\equiv^{2}0^{00}-6^{50}$ $\equiv -7^{45}$ $\square\ 6^{50}-7^{45}$ $\equiv^{2}-8^{30}$ $\equiv -24$, $\gg 0^{00}-4^{10}$ $\nwarrow -7^{30}$ $\gg -23^{40}$, $\overset{+}{\uparrow}^{0}0^{00}-4^{10}$ $\overset{+}{\uparrow}^{1}-23^{40}$, ○ na-p; $\square\ 21^{20}-23^{10}$
3	0	9.3	33	–	$\triangle^{0-1}16^{00}-18^{20}$ $*^{0-1}23^{30}$ $\bullet^{0}-24$, $V^{0}4^{10}-10^{00}$ $18^{00}-23^{30}$ $V^{0}-24$, $\equiv 0^{00}-3^{40}$ $\equiv^{2}-24$, $\gg 21^{30}-24$, $*\overset{+}{\uparrow}^{0}21^{00}-23^{30}$
4	0	.	35	–	$\bullet^{0}0^{00-40}$ $\overset{*}{\bullet}^{0}-1^{20}$ $\bullet\bullet^{0}-2^{40}$ $*^{0}-3^{00}$ $\bullet^{0}-4^{10}$, $V^{1}0^{00}-5^{00}$ $V^{0}-9^{20}$ $12^{40}-13^{15}$, $\equiv^{2}0^{00}-9^{20}$ $\equiv -11^{40}$ $\equiv^{2}-13^{15}$ $\equiv -14^{30}$ $\square -24$, $\gg 0^{00}-3^{00}$
5	8	.	33	–	$\square\ 0^{00}-18^{20}$ $\equiv 18^{00-20}$ $\equiv^{2}-19^{30}$ $\equiv -24$, $\gg 5^{15}-10^{30}$ $\nwarrow -13^{10}$ $\gg -19^{40}$ $\nwarrow -24$
6	9	.	30	–	$\equiv 0^{00-40}$ $\square -12^{00}$, $\gg 0^{00-10}$, $3^{10}-8^{00}$, ○ na-p
7	9	.	27	–	$\equiv 23^{30}-24$, $\gg 5^{00}-21^{30}$ $\nwarrow -24$, ○ na
8	9	.	24	–	$\equiv 0^{00}-3^{20}$, $\nwarrow 0^{00}-6^{20}$ $\gg -14^{30}$, $16^{45}-19^{30}$ $\nwarrow -24$, ○ na-p
9	9	.	20	–	$\nwarrow 0^{00}-8^{30}$ $\gg -12^{30}$, ○ na-p
10	8	.	18	–	$\gg 17^{15}-22^{00}$ $\nwarrow -24$, ○ na-p
11	7	.	16	–	$\equiv 5^{30}-16^{05}$, $19^{40}-24$, $\nwarrow 0^{00}-24$, ○ na p
12	7	6.4	15	–	$\equiv 0^{00}-4^{30}$ $\square -7^{30}$ $\equiv 6^{40}-7^{10}$ $21^{30}-22^{20}$ $\equiv^{2}-24$, $\nwarrow 0^{00}-24$
13	8	10.8	17	–	$\bullet\ 1^{57}3^{55}$ $\bullet^{0}-5^{55}$ $*^{0}-7^{10}$ $23^{50}-24$, $V^{0}16^{10}-24$, $*\overset{+}{\uparrow}^{1}5^{55}7^{10}$ $\overset{+}{\uparrow}^{1}-9^{00}$ $\overset{+}{\uparrow}^{2}-23^{50}$ $*\overset{+}{\uparrow}^{2}-24$, $\nwarrow 0^{00}-24$
14	0	10.7	17	–	$*^{0}0^{00}1^{30}$ 1^{45} $*^{1}-5^{10}$ $*^{0}-6^{25}$ $\bullet^{0}-7^{55}$, $10^{10}-16^{45}$, $V^{0}0^{00}-4^{30}$ $\sim 16^{50}-22^{10}$ $V^{0}-24$, $\equiv^{2}0^{00}-24$, $*\overset{+}{\uparrow}^{2}0^{00}-6^{25}$ $\overset{+}{\uparrow}^{2}-24$, $\nwarrow 0^{00}-24$
15	0	0.7	16	–	$\bullet\ 10^{30}-18^{20}$, $21^{10}-24$, $V^{0}0^{00}-10^{30}$, $\equiv^{2}0^{00}-24$, $\nwarrow 0^{00}-24$
16	7	0.1	10	–	$\bullet\ 0^{00}-1^{12}$, $V^{0}22^{30}-24$, $\equiv^{2}0^{00}-1^{12}$ $\equiv -1^{20}$ $\square\ 1^{15}-2^{30}$ $\equiv^{2}19^{35}-24$, $\nwarrow 0^{00}-24$, ○ na-p
17	7	.	7	–	$V^{0}0^{00}-1^{40}$, $\equiv^{2}0^{00}-1^{40}$ $\equiv -2^{10}$ $\square -11^{30}$, $\nwarrow 0^{00}-7^{30}$ $\gg -13^{10}$, $19^{30}-21^{30}$ $\nwarrow -24$, ○ na-p
18	0	0.5	5	–	$\overset{*}{\nabla}13^{57}15^{56}$ $\bullet\ 15^{56}-20^{20}$, $V^{0}22^{30}-23^{15}$, $\equiv 9^{40}-10^{25}$ $\equiv^{2}$ $\equiv 11^{08}-24$, $\nwarrow 0^{00}-24$, ○ na-a
19	7	4.7	pł.	–	$*^{0}8^{10}$ 11^{15}, $13^{30}-21^{30}$, $V^{0}4^{20}-7^{50}$ $8^{10}-10^{30}$, $10^{55}-11^{15}$ $13^{30}-24$, $\equiv 0^{00-35}$ $\equiv^{2}$ $\equiv 3^{20}-24$, $\nwarrow \gg 0^{00}-10^{30}$, $*\overset{+}{\uparrow}$, $\overset{+}{\uparrow}$ $8^{10}-21^{30}$
20	7	7.7	pł.	–	$*^{0-1}12^{05}$ $22^{00}-24$, $V^{0}18^{40}-24$, $\equiv 0^{00}-5^{30}$ $\equiv^{2}13^{40}-15^{10}$ $\equiv -16^{10}$, 18^{10-35} $\equiv^{2}-24$, $\overset{+}{\uparrow}^{0}0^{00}-5^{30}$, $11^{50}-12^{05}$ $*\overset{+}{\uparrow}^{0-2}-24$
21	0	31.9	10	–	$*^{0}0^{00}-24$, $V^{0}0^{00}-24$, $\equiv^{2}0^{00}-24$, $*\overset{+}{\uparrow}^{2}0^{00}-24$, $\nwarrow 0^{00}-24$
22	0	13.0	25	–	$*^{0}0^{00}-8^{30}$ $\overset{*}{\nabla}^{1-2}9^{10}$ 10^{20} $*^{0-1}16^{20}$ $20^{45}-24$, $V^{0}0^{00}-10^{30}$ $11^{15}-15^{20}$ $19^{30}-24$, $\equiv^{2}$ $\equiv 0^{00}-17^{10}$, $18^{40}-24$, $*\overset{+}{\uparrow}^{2-1}$, $\overset{+}{\uparrow}^{2}0^{00}-24$, $\nwarrow \gg 0^{00}-24$, ○ a...p
23	0	8.8	32	–	$*^{0}0^{00}-2^{30}$, 8^{55} $14^{30}-24$, $V^{0}0^{00}-24$, $\equiv^{2}0^{00}-24$, $*\overset{+}{\uparrow}^{2}0^{00}-2^{30}$ $\overset{+}{\uparrow}^{1}-8^{55}$ $*\overset{+}{\uparrow}^{1}-24$, $\nwarrow \gg 0^{00}-24$
24	0	2.0	37		$*^{0}0^{00}3^{35}-7^{20}$ $V^{0}0^{00}-24$, $\equiv^{2}0^{00}-24$, $*\overset{+}{\uparrow}^{1}0^{00}-7^{20}$ $\overset{+}{\uparrow}^{2}-24$, $\gg 0^{00}-4^{20}$ $\nwarrow -24$
25	0	0.1	37	–	$*\ 7^{40}-8^{35}$, $V^{0}0^{00}-9^{30}$ $18^{45}-20^{20}$, $\equiv^{2}$ $\equiv 0^{00}-20^{20}$, $\overset{+}{\uparrow}^{2}0^{00}-7^{40}$ $*\overset{+}{\uparrow}^{2}-8^{35}$ $\overset{+}{\uparrow}^{2}-9^{00}$, $\nwarrow 0^{00}-10^{00}$ $\gg -20^{30}$, ○ a z prz.
26	7	0.3	35	–	$*^{0}6^{20}7^{40}$, $V^{0}3^{30}-6^{00}$ $23^{20}-24$, $\equiv^{2}3^{30}-6^{00}$ $\equiv -14^{20}$ $\equiv^{2}23^{20}-24$, $\overset{+}{\uparrow}^{2}18^{20}-24$, $\gg 1^{00}-15^{30}$ $\nwarrow -24$
27	7	5.7	35	–	$V^{0}0^{00}-5^{20}$ $19^{45}-22^{40}$, $*^{0}4^{35}5^{20}$ $\overset{*}{\nabla}^{0-1}10^{10}$ 13^{15} 14^{03-50} $\overset{*}{\nabla}^{1-2}16^{20}$ 18^{45} $\overset{*}{\nabla}^{1}20^{50}-22^{35}$, $\equiv^{2}0^{00}-5^{20}$ $\equiv 7^{15-35}$ $\equiv^{2}16^{45}-18^{35}$ $19^{45}-22^{40}$ $\equiv -24$, $\overset{+}{\uparrow}^{2}$ $*\overset{+}{\uparrow}^{2-1}0^{00}-6^{20}$ $10^{28}-15^{00}$,
28	0	6.0	40	–	$\overset{*}{\nabla}^{1}0^{45}-1^{15}$ $6^{45}-9^{20}$ $*^{1-0}16^{20}$ 17^{10} 19^{30} $*^{0}21^{30}-23^{15}$ $*^{1}-24$, $V^{0}0^{30}-11^{20}$ $17^{45}-24$, $\equiv$, $\equiv^{2}0^{00}-24$, $\overset{+}{\uparrow}^{2}$ $*\overset{+}{\uparrow}^{1-2}0^{00}-24$, $\nwarrow 0^{00}-21^{30}$ $\gg -24$
29	0	4.3	46	–	$*^{0-1}0^{00}-21^{00}-24$, $\equiv^{2}0^{00}-24$, $*\overset{+}{\uparrow}^{0-2}0^{00}-24$, $\gg 0^{00}-9^{05}$ $\nwarrow -18^{30}$ $\gg -24$ [27.III: $16^{20}-24$, $\nwarrow \gg 0^{00}-24$, ○ a...p
30	0	3.8	50	–	$*^{0}4^{50}-8^{30}$ $18^{40}-24$, $V^{1}0^{00}-16^{00}$ $V^{2}-18^{30}$ $V^{1}-24$, $\equiv^{2}0^{00}-24$, $\overset{+}{\uparrow}^{1}0^{00}-1^{30}$ $\overset{+}{\uparrow}^{2}-4^{50}$ $*\overset{+}{\uparrow}^{2}-24$, $\gg 0^{00}-1^{30}$ $\nwarrow -24$
31	0	1.8	55	–	$*^{0}0^{00}1^{30}$ $\overset{*}{\bullet}^{0}-5^{40}$ $*^{0}-8^{20}$, 17^{30} 19^{10}, $V^{1}0^{00}-1^{20}$ $V^{0}5^{30}-7^{20}$ $11^{20}-12^{15}$, $12^{45}-19^{10}$ $20^{20}-21^{30}$, $\equiv^{2}0^{00}-8^{20}$ $\equiv -10^{30}$ $\square -11^{20}$ $\equiv^{2}$ $\equiv -24$, $*\overset{+}{\uparrow}^{2}0^{00}1^{30}$ $5^{40}-8^{20}$ $17^{30}-19^{10}$ $\overset{+}{\uparrow}^{1}-20^{30}$ $\overset{+}{\uparrow}^{2}-24$,
Σ	–	133.1	–	–	UWAGI. [31.III: $\nwarrow \gg 0^{00}-10^{30}$, $16^{20}-24$

Kwiecień – Avril

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	4.3	55	–	$*^{0}6^{30}11^{30}$ $14^{45}-24$, $V^{0}6^{30}-8^{00}$ $V^{1}-24$, $\equiv 0^{00}-3^{30}$ $5^{20}-6^{30}$ $\equiv^{2}-24$, $\overset{+}{\uparrow}^{1-2}$ $*\overset{+}{\uparrow}^{1-2}0^{00}-24$, $\nwarrow \gg 0^{00}-24$
2	0	3.4	58	–	$*^{0}0^{00}-3^{45}$ $7^{45}-10^{40}$ $12^{50}-18^{10}$ $\bullet^{0}20^{30}-21^{40}$ 24, $V^{1}0^{00}-2^{00}$ $V^{0}-3^{00}$ $5^{30}-6^{40}$ $8^{00}-18^{05}$, $\equiv^{2}$ $\equiv 0^{00}-7^{30}$ $\equiv^{2}-24$, $*\overset{+}{\uparrow}^{1-2}$, $\overset{+}{\uparrow}^{1-2}0^{00}-24$, $\gg \nwarrow 0^{00}-24$
3	7	1.7	50	–	$\bullet^{0}0^{00-50}$ $*^{0}-3^{20}$ $\overset{*}{\bullet}^{0}-5^{30}$ $*^{0}-8^{20}$, $V^{0}8^{20}-9^{30}$ $10^{25}-12^{12}$ $V^{1}14^{20}-16^{30}$ $17^{40}-24$, $\equiv^{2}$ $\equiv 0^{00}-24$, $\nwarrow \gg 0^{00}-24$
4	7	2.2	48	–	$*^{0}0^{55}3^{30}$ $\bullet^{0}-6^{30}$ $6^{50}-8^{20}$ $*^{1}8^{25}-9^{45}$ $\bullet^{0}19^{45}-24$, $\equiv^{2}0^{00}-8^{10}$ $\equiv -13^{20}$ $14^{25}-17^{15}$ $\equiv^{2}-24$, $V^{1}0^{00}-3^{30}$ $V^{0}-8^{10}$, $*\overset{+}{\uparrow}^{1}0^{55}3^{30}$ $8^{25}-9^{45}$, $\gg \nwarrow 0^{00}-24$, ○ na...p
5	8	.	40	–	$\blacktriangle\overset{\bullet}{\nabla}^{1}2^{05-25}$, $\equiv^{2}0^{00}-4^{15}$, $\gg 0^{00}-4^{30}$ $\nwarrow -24$, $\cup 4^{15}-5^{30}$, ○ na...p
6	9	.	25	–	$\nwarrow 0^{00}-8^{20}$ $\gg -23^{15}$ $\nwarrow -24$, ○ na
7	8	2.3	22	–	$\triangle\overset{*}{\nabla}\overset{\bullet}{\nabla}^{1}16^{37-50}$ $\overset{\bullet}{\nabla}^{0-1}18^{00}$ $18^{37}-19^{00}$ $20^{45}-22^{35}$ (K) NW $15^{43}-16^{37}$ K 17^{05} (K) E -17^{15} < E S $19^{25}-21^{30}$ (K)$^{0-1}16^{40}$ 17^{10}, $\nwarrow \gg 0^{00}-5^{15}$ $14^{45}-24$, $\frown 17^{02-15}$, ○ na...p
8	0	5.5	12	–	$\bullet^{0}5^{00}6^{25}$ $\overset{\bullet}{\nabla}^{0}8^{40-44}$ 12^{10-16} $\overset{\bullet}{\nabla}^{1}-12^{30}$ $\overset{\bullet}{\nabla}^{0}-13^{20}$ $\bullet\ 14^{30}16^{40}$ $V\ 17^{10}-24$ $\sim 16^{25}-22^{00}$, $\equiv 5^{30}-10^{35}$ $\equiv^{2}-24$, $\nwarrow 0^{00}-24$
9	8	.	10	–	$V^{0}0^{00}-1^{20}$ $V^{0}3^{00}-9^{15}$ $9^{45}-10^{10}$, $\equiv^{2}$ $\equiv 0^{00}-19^{20}$, $\nwarrow 0^{00}-1^{40}$ $\gg -10^{30}$
10	8	0.0	8	–	$*^{0}20^{45}-21^{05}$, $\gg 7^{00}-10^{15}$, $\oplus 7^{30}-9^{15}$
11	7	.	8	–	$\sqcup^{0}22^{00}-24$, $\equiv 3^{30}-6^{40}$ $\equiv^{1}-8^{25}$ $\equiv 13^{45}-14^{40}$ $\equiv -15^{30}$ $\equiv^{2}-19^{20}$ $\equiv -20^{15}$
12	8	.	7	–	$\sqcup^{0}0^{00}-7^{00}$, $\gg 22^{30}-24$, ○ na-p
13	7	.	pł.	–	$\equiv 4^{25}-6^{20}$ $\equiv -7^{35}$, $\gg 0^{00}-17^{30}$, $23^{30}-24$
14	8	0.0	pł.	–	$\gg 0^{00}-7^{20}$ $13^{00}-17^{00}$, ○ na-p, $\oplus 6^{30}-7^{10}$ 11^{00-40}
15	7	0.7	pł.	–	$\bullet^{0}0^{30}1^{10}$ 17^{57} 18^{00} $\bullet^{1}$ 18^{02} $\overset{\bullet}{\nabla}^{0}18^{55}$ 19^{05} $\bullet^{2}19^{12-35}$ $\bullet^{1}-19^{45}$ $\bullet^{0}-20^{20}$ $\equiv^{2}20^{20}-21^{40}$ $\equiv -24$, (K)^{0}NE 18^{31-38} K 19^{10} (K)^{0}ENE -20^{20} < ENE $19^{10}-20^{20}$, (K)$^{0}18^{40}$ 20^{05}
16	6	11.8	pł.	–	$\bullet^{0}8^{25-45}$ $\blacktriangle 13^{50}-14^{50}$ $\bullet^{0-1}15^{25}$ $\overset{\bullet}{*}^{1}16^{15}$ $\bullet^{0}16^{55}$, $\equiv 0^{00}-3^{20}$ $\square -9^{40}$ $\equiv -14^{20}$ $\equiv^{2}-15^{20}$ $\equiv$ $\equiv^{2}17^{25}-24$, K $11^{45}-12^{40}$ $13^{50}-14^{50}$ (K) 16^{00} p; $\gg 13^{40}-14^{20}$ $22^{30}-24$
17	7	.	pł.	–	$\equiv 10^{15}-11^{20}$ $16^{00}-20^{10}$, $\gg 0^{00}-6^{20}$, ○ na-a [15.IV: ○ na...p
18	8	10.2	pł.	–	$\triangle^{0}11^{50}-12^{01}$ $\overset{\bullet}{\nabla}^{0}-12^{05}$ $\bullet^{0}23^{47-55}$ $\bullet^{1}-24$, $\equiv 22^{20-35}$ $\equiv^{2}-24$, ○ na...p
19	6	.	pł.	–	$\bullet^{1}0^{00-20}$ $\bullet^{0}-6^{07}$, $\equiv^{2}0^{00}-9^{45}$ $\equiv$ $\square -16^{25}$ $\equiv^{2}-17^{20}$ $\equiv -19^{20}$, $\gg 19^{20}-24$, $\oplus 14^{30}-15^{20}$
20	8	.	pł.	–	$\gg 0^{00}-4^{20}$, ○ a-p
21	8	0.0	pł.	–	$\equiv 21^{10}-22^{20}$ $\bullet\equiv^{2}-24$, $\gg 20^{00-40}$ $\nwarrow -24$, ○ na-p
22	7	0.7	pł.	–	$\bullet 0^{00}-3^{20}$ $\bullet^{0}18^{55}$ 19^{50} $\bullet -24$, $\equiv^{2}0^{00}-3^{20}$ $4^{40}-8^{25}$ $\equiv -9^{30}$ $\equiv^{2}-10^{15}$ $\equiv -10^{30}$ $13^{00}-16^{35}$ $\equiv^{2}-24$, $\nwarrow 0^{00}-24$
23	0	0.3	pł.	–	$\bullet 0^{00}-14^{10}$ $20^{30}-24$, $\equiv^{2}0^{00}-15^{35}$ $\equiv -16^{10}$ $17^{40}-18^{25}$ $\equiv^{2}-24$, $\nwarrow 0^{00}-24$
24	8	.	pł.	–	$\bullet\equiv 0^{00}-6^{15}$ $\equiv -8^{05}$ $19^{30}-20^{40}$ $\square -24$, $\nwarrow 0^{00}-8^{10}$ $\gg -9^{40}$, ○ a...p
25	9	0.0	pł.	–	$V^{0}21^{30}-22^{40}$, $\square\ 0^{00}-19^{20}$ $\equiv -20^{35}$ $\equiv^{2}-22^{40}$ $\equiv -24$, ○ na-p
26	8	0.0	pł.	–	$\overset{\bullet}{\nabla}^{0}17^{50}-18^{00}$, $\equiv 0^{00-20}$ $\square\ 0^{15}-9^{45}$ $\equiv 17^{05-15}$ 17^{30-40} $\equiv^{0}-20^{20}$ $\equiv^{2}23^{40}-24$, ○ na-p
27	0	7.6	pł.	–	$\overset{\bullet}{\nabla}^{0}10^{53}-14^{35}$ $\blacktriangle\overset{*}{\nabla}^{1}$ $\overset{\bullet}{\nabla}^{1}-14^{50}$ $\overset{\bullet}{\nabla}^{1}-15^{20}$ $\overset{\bullet}{\nabla}^{0}-15^{50}$ $18^{50}-19^{20}$ $\overset{\bullet}{\nabla}^{1}-20^{55}$ $\overset{\bullet}{\nabla}^{0}21^{55}-24$, $\equiv^{2}0^{00-25}$ $\equiv$, $\equiv^{2}-9^{45}$ $12^{30}-24$, (K)^{0}WSW $9^{10}-13^{45}$, ○ a
28	0	1.1	pł.	–	$\overset{\bullet}{\nabla}^{0}0^{00}1^{55}$ $5^{55}-6^{30}$ $\overset{*}{\nabla}^{1}-7^{20}$ $\overset{\bullet}{\nabla}^{0}-8^{15}$ $\overset{*}{\nabla}^{0}-9^{30}$ $\bullet^{0}-12^{40}$ $\bullet -16^{30}$ $\equiv^{2}0^{00}-1^{55}$ $\equiv -3^{30}$ $\equiv^{2}$ $\equiv 7^{20}-24$, $\cup 18^{05}-21^{38}$
29	0	4.4	pł.	–	$\overset{\bullet}{\nabla}^{1}\blacktriangle 11^{30-43}$ $\overset{\bullet}{\nabla}^{0}12^{00}$ $\overset{*}{\nabla}^{0}-12^{10}$ $\overset{\bullet}{\nabla}^{0}-12^{50}$ 13^{10-20} $\blacktriangle 1^{15}45-58$ $\overset{\bullet}{\nabla}^{0}16^{25-40}$ $\bullet 18^{03}-22^{15}$, $\equiv^{2}0^{00}-2^{10}$ $\equiv -7^{40}$ 8^{20-30} $\equiv^{1}8^{40}-10^{15}$ $\equiv 10^{45}-11^{00}$ $\equiv^{2}-22^{10}$ $\equiv 23^{30}-24$, (K)NE $11^{30}-11^{45}$ 12^{45}
30	8	13.5	pł.	–	$\overset{\bullet}{\nabla}^{0}12^{40}-13^{05}$ $\blacktriangle\overset{\bullet}{\nabla}^{0}14^{20-22}$ $\overset{\bullet}{\nabla}^{0}-14^{42}$ $\blacktriangle\overset{\bullet}{\nabla}^{0}21^{11-25}$ $\blacktriangle\overset{\bullet}{\nabla}^{1-2}22^{15}$ $\overset{\bullet}{\nabla}^{1-0}-23^{30}$ $\bullet^{0}-24$, $\equiv 0^{00}-1^{30}$ $3^{30}-4^{15}$ $\equiv^{2}18^{25}-19^{15}$ $\equiv -20^{05}$ $\equiv^{2}-24$, (K)^{0}NNW 12^{08} – NNE 12^{55}
31					[29.IV: ○ na...a [30.IV: (K)^{0}WNW 20^{18} – SSE 22^{45}
Σ	–	69.7	–	–	UWAGI.

Śnieżka — φ = 50°44' — λ = 15°44' — Maj – Mai 1961

DNB	CIŚNIENIE P = 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	31.8	35.8	34.5	33.4	2.7	4.0	5.0	3.2	5.2	1.9	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	NNE10	NE 4	NE 5
2	33.9	34.0	33.4	33.8	1.8	3.2	2.8	2.6	4.7	1.2	100	93	100	99	0.0	0.2	0.0	0.1	10	10	10	NW 4	W 5	SW 7
3	31.4	32.5	34.6	32.8	2.5	3.4	2.2	2.6	4.6	1.7	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	SW 8	SW 8	NW 6
4	37.1	38.0	38.3	37.8	1.8	3.6	4.3	3.5	5.0	0.7	100	97	100	99	0.0	0.3	0.0	0.1	10	9	10	W 6	WSW 8	S 4
5	37.4	37.7	37.9	37.7	5.1	6.8	8.4	7.2	8.7	5.3	100	99	100	100	0.0	0.2	0.0	0.1	10	9	10	SSW10	SW 14	SW 14
6	34.6	37.7	39.1	37.1	7.5	5.4	5.0	5.7	8.4	3.8	100	100	88	96	0.0	0.0	1.0	0.3	10	10	9	SW 18	W 6	W 10
7	37.6	35.3	33.2	35.4	3.8	3.8	0.0	1.9	5.6	-0.6	100	100	65	89	0.0	0.0	2.0	0.7	10	9	1	WSW15	SW 15	NW 17
8	33.6	33.8	31.7	33.0	-1.1	-0.6	-1.6	-1.2	0.3	-1.8	99	95	98	97	0.1	0.3	0.1	0.2	10	8	10	SW 8	W 18	W 20
9	26.5	26.9	27.2	26.9	-2.0	-1.2	-1.2	-1.4	-1.0	-2.7	98	99	99	99	0.1	0.1	0.1	0.1	10	10	10	W 22	W 20	WNW20
10	29.4	31.1	32.8	31.1	-1.4	-0.8	-1.7	-1.4	-0.8	-2.0	99	97	96	97	0.1	0.2	0.2	0.2	10	10	10	WNW18	NW 18	NW 18
11	33.0	34.4	36.9	34.8	-5.0	-0.5	-1.6	-1.7	-0.2	-5.5	97	100	98	98	0.1	0.0	0.1	0.1	10	10	10	NW 14	NW 10	NW 14
12	37.1	36.1	35.0	36.1	-5.6	-0.4	-2.0	-2.0	-0.4	-4.0	94	96	98	96	0.3	0.2	0.1	0.2	9		10	NW 6	NW 6	NW 4
13	34.2	33.5	32.5	33.4	-1.8	-0.5	-0.2	-0.7	0.5	-5.3	94	100	98	97	0.3	0.0	0.1	0.1	8		10	W 8	W 8	NW 10
14	29.7	29.8	30.2	29.9	-2.3	-1.5	-2.6	-2.2	-0.2	-3.1	98	86	89	91	0.1	0.8	0.6	0.5	6	5	5	W 17	W 14	W 14
15	31.3	32.9	33.3	32.5	-1.0	-0.7	-1.5	-1.2	-0.2	-3.1	97	97	99	98	0.2	0.2	0.1	0.2	10	10	10	NW 10	N 10	NNW 8
16	32.8	33.5	30.6	32.3	-1.7	0.2	-0.6	-0.7	1.0	-2.5	98	91	99	96	0.1	0.6	0.0	0.2	10	8	10	NNW 8	NW 4	NW 20
17	31.6	35.1	37.0	34.6	-1.7	0.0	0.2	-0.5	0.2	-2.3	98	100	100	99	0.1	0.0	0.0	0.0	10	10	10	NW 18	NW 6	NW 18
18	35.8	37.7	37.3	36.9	-2.2	-0.4	0.4	-0.4	0.5	-2.3	98	98	96	97	0.1	0.1	0.3	0.2	10	9	10	NW 15	NW 4	NW 7
19	36.2	36.3	34.8	35.8	0.4	1.1	0.6	0.7	1.7	0.1	96	92	90	93	0.5	0.5	0.6	0.5	9	9	10	NW 5	NW 3	NNW 6
20	31.9	30.8	30.7	31.1	0.8	2.2	1.8	1.6	2.5	0.2	98	87	100	95	0.2	1.0	0.0	0.4	6	9	10	W 12	W 6	W 10
21	30.8	30.9	32.2	31.3	1.4	1.4	2.2	1.8	3.0	0.7	91	100	100	97	0.7	0.0	0.0	0.2	9	10	10	W 4	N 8	NNW10
22	32.4	33.5	33.7	33.2	2.4	2.6	1.0	1.8	3.1	1.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	NNW12	NW 14	NW 8
23	34.4	35.5	35.5	35.1	0.8	2.6	3.0	2.4	4.1	-0.3	90	77	73	80	0.7	1.8	2.1	1.5	9	9	9	NW 4	NW 4	NW 2
24	36.3	37.6	37.5	37.1	3.0	4.7	4.9	4.4	5.8	2.2	75	86	67	76	1.9	1.1	2.9	2.0	3	9	6	WNW 5	W 6	W 8
25	37.0	37.3	36.4	36.9	4.5	6.6	6.6	6.1	8.1	3.9	51	89	74	71	4.1	1.0	2.5	2.5	2	10	3	W 5	NW 1	NW 3
26	35.6	35.5	32.7	34.6	6.8	9.0	7.0	7.4	11.2	6.0	71	66	97	78	2.9	3.8	0.3	2.3	9	8	10	NW 2	WSW10	SW 10
27	31.9	32.6	32.1	32.2	5.2	8.1	6.6	6.6	9.1	4.8	100	92	100	97	0.0	0.8	0.0	0.3	7	9	6	WSW 6	SSW 3	ESE 3
28	31.4	31.8	31.4	31.5	4.8	3.5	1.3	2.7	6.7	1.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	SSE 2	S 1	C 0
29	26.3	24.4	25.3	24.7	2.0	5.0	4.2	3.8	5.3	-0.1	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	S 7	SSE 4	SSE 4
30	25.2	24.1	25.2	24.2	1.0	0.6	0.2	0.3	4.6	-0.4	100	98	100	99	0.0	0.1	0.0	0.0	10	10	10	W 4	SW 8	SW 6
31	25.1	25.7	27.3	26.1	-0.4	1.4	5.5	3.0	5.6	-0.5	100	100	82	94	0.0	0.0	1.6	0.5	10	10	4	WSW10	W 16	W 18
M	32.6	33.2	33.2	33.0	1.2	2.5	1.9	1.8	3.6	0.0	95	95	94	95	0.4	0.4	0.5	0.4	8.9	9.3	8.6	9.5	8.4	9.7

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1	29.1	30.5	28.5	29.4	7.8	11.5	8.5	9.1	14.1	5.9	78	77	100	85	2.3	3.2	0.0	1.8	1	7	9	S 7	S 4	S 12
2	28.2	31.6	32.6	30.8	7.6	10.9	8.6	8.9	13.2	6.4	58	64	89	70	4.3	4.6	1.3	3.4	1	3	2	SW 9	WSW 8	N 8
3	31.8	32.7	33.9	32.8	5.8	7.2	8.6	7.6	9.1	5.0	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	N 10	N 10	N 12
4	34.5	36.2	36.7	35.8	8.6	10.8	8.8	9.2	13.0	7.0	94	87	99	93	0.6	1.7	0.1	0.8	9	7	9	N 12	N 4	ENE10
5	38.0	38.9	38.6	38.5	8.9	10.1	8.6	9.0	11.4	7.1	100	96	100	99	0.0	0.5	0.0	0.2	10	7	10	N 7	NE 6	E 10
6	37.3	37.2	35.7	36.7	7.8	10.3	9.4	9.2	10.4	6.2	92	94	100	95	0.8	0.8	0.0	0.5	8	9	10	ESE 8	NE 4	E 4
7	34.4	34.2	33.9	34.2	8.8	10.6	9.9	9.8	10.9	7.4	97	87	80	88	0.3	1.7	2.5	1.5	10	9	9	SW 2	SSW 8	SW 3
8	34.2	36.3	36.9	35.9	8.6	8.8	8.4	8.6	10.2	7.8	100	93	97	97	0.0	0.8	0.3	0.4	10	9	9	N 8	N 6	W 6
9	36.6	37.0	35.6	36.4	8.0	8.9	9.4	8.9	9.8	6.7	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	S 6	SW 3	SSE 9
10	34.7	36.3	37.3	36.2	9.0	8.8	7.4	8.2	9.8	7.0	100	100	99	100	0.0	0.0	0.2	0.1	10	10	10	S 12	SW 12	NNW 7
11	37.0	37.7	37.1	37.3	5.9	7.8	6.4	6.6	8.5	5.3	100	100	100	100	0.0	0.0	0.0	0.0	10	10	10	NNW10	NW 5	NNW 6
12	35.4	35.2	35.0	35.2	5.0	6.3	4.6	5.1	6.7	4.4	100	86	97	94	0.0	1.3	0.3	0.5	10	9	8	WSW 8	W 6	SW 8
13	31.9	29.4	27.1	29.5	3.8	5.1	5.1	4.8	6.3	3.3	88	98	100	95	1.0	0.2	0.0	0.4	8	10	10	WSW14	SW 20	SW 17
14	28.4	32.3	35.3	32.0	3.1	3.4	3.0	3.1	5.2	2.5	100	100	100	100	0.0	0.0	0.0	0.0	10	9	10	W 17	W 18	W 20
15	35.7	37.3	38.0	37.0	1.0	2.6	1.8	1.8	5.9	0.9	100	95	66	87	0.0	0.4	2.4	0.9	10	9	0	W 22	WSW 8	W 8
16	38.6	40.3	41.0	40.0	4.6	7.8	4.8	5.5	8.6	0.3	65	84	68	72	3.0	1.7	2.7	2.5	0	6	6	WNW 7	C 0	NNW10
17	42.1	43.1	43.5	42.9	4.9	9.0	8.6	7.8	11.2	3.4	73	69	79	74	2.3	3.5	2.5	2.8	1	7	8	N 6	N 5	N 4
18	42.6	42.4	41.9	42.3	8.6	12.9	15.0	11.9	13.9	8.3	100	65	75	80	0.0	5.3	3.8	3.0	2	1	1	W 8	SW 8	WSW12
19	42.2	43.0	43.3	42.8	11.1	9.8	4.0	7.2	13.0	4.0	100	97	97	98	0.0	0.3	0.2	0.2	10	9	2	W 10	W 9	NW 13
20	46.2	47.4	46.2	46.6	2.4	6.2	5.2	4.8	7.7	1.4	95	94	94	94	0.4	0.6	0.5	0.5	4	5	1	NNW 6	NW 8	NW 4
21	44.2	44.3	45.2	44.6	4.8	10.1	4.9	6.2	11.2	4.2	82	75	100	86	1.6	3.1	0.0	1.6	5	7	10	WSW 6	SW 3	NNW13
22	44.2	42.8	39.5	42.2	5.6	10.9	12.3	10.3	14.1	4.3	80	93	99	91	1.8	0.9	0.2	1.0	4	7	10	WNW14	NW 14	SW 8
23	41.2	43.0	43.1	42.4	7.1	8.9	9.7	8.8	12.3	6.1	86	74	82	81	1.4	3.0	2.1	2.2	3	6	2	NW 12	W 7	W 8
24	43.2	43.5	44.6	44.4	8.1	13.4	11.7	11.2	15.6	7.3	81	65	69	72	2.1	5.4	4.3	3.9	8	6	4	WNW 9	WNW 3	WNW12
25	43.8	43.4	41.3	42.9	11.3	16.1	14.7	14.2	17.0	10.3	56	50	71	59	6.1	9.1	4.8	6.7	1	1	3	WNW 7	SSW 4	WSW12
26	40.3	40.1	37.7	39.4	13.8	12.7	12.9	13.1	15.7	12.7	68	94	88	83	5.2	0.9	1.8	2.6	8	10	5	WNW 2	WSW 2	WSW 8
27	35.6	33.4	36.1	35.7	14.7	12.3	11.4	12.4	15.3	10.8	73	100	100	91	4.4	0.0	0.0	1.5	9	10	9	WSW10	SSW12	W 10
28	39.2	44.8	47.4	43.8	1.9	2.8	3.2	2.8	11.5	0.6	100	87	93	93	0.0	1.0	0.5	0.5	10	6	3	NNW12	NNW15	NNW13
29	48.8	50.6	49.9	49.8	3.8	8.7	7.9	7.1	10.4	2.9	100	58	77	78	0.0	4.6	2.4	2.3	10	4	1	NNW12	NNW 6	N 4
30	50.0	50.3	49.6	50.0	10.3	13.9	11.7	11.9	15.1	6.9	70	61	76	69	3.7	6.2	3.2	4.4	0	2	0	SE 1	N 2	W 1
31																								
M	38.3	39.3	39.1	38.9	7.1	9.3	8.2	8.2	11.2	5.3	88	85	90	88	1.4	2.0	1.2	1.5	6.7	7.2	6.4	9.1	7.3	9.1

Śnieżka — $H_s = 1603$ m — $H_t = 1610{,}6$ m — Maj - Mai 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	0	9.3	pż.	-	
2	1	3.7	pż.	-	
3	1	1.2	pż.	-	[1.V:
4	8	0.2	pż.	-	
5	8	2.4	pż.	-	
6	0	1.4	pż.	-	
7	8	2.4	pż.	-	
8	8	2.8	1	-	
9	0	12.6	2	-	[8.V:
10	0	30.7	12	-	
11	0	27.1	25	-	
12	0	4.9	35	-	
13	0	0.5	36	-	
14	7	0.8	37	-	[13.V:
15	0	0.8	35	-	
16	7	30.2	34	-	
17	0	10.2	44	-	
18	8	.	44	-	
19	8	0.2	30	-	
20	8	0.5	22	-	
21	0	31.6	20	-	
22	0	0.1	10	-	[21.V:
23	8	.	8	-	
24	7	.	5	-	
25	0	.	pż.	-	
26	6	0.5	pż.	-	
27	7	18.4	pż.	-	
28	0	4.4	pż.	-	[27.V:
29	0	27.4	pż.	-	
30	0	2.7	pż.	-	
31	0	0.3	pż.	-	
Σ	—	227.3	—	-	UWAGI.

Czerwiec - Juin

1	8	.	pż.	-	
2	9	.	pż.	-	
3	0	10.1	pż.	-	
4	7	2.3	pż.	-	
5	7	0.2	pż.	-	
6	7	0.4	pż.	-	[4.VI:
7	7	7.6	pż.	-	
8	7	15.6	pż.	-	
9	0	4.3	pż.	-	[7.VI:
10	0	7.7	.	-	
11	0	9.8	.	-	
12	7	0.4	.	-	
13	0	11.4	.	-	
14	7	5.7	.	-	
15	7	.	.	-	
16	7	.	.	-	
17	8	.	.	-	
18	7	.	.	-	
19	8	2.6	.	-	
20	8	.	.	-	
21	7	.	.	-	
22	7	4.6	.	-	
23	7	.	.	-	
24	7	.	.	-	
25	8	.	.	-	
26	6	0.7	.	-	
27	0	9.9	.	-	
28	8	.	.	-	[27.VI:
29	8	0.0	.	-	
30	8	.	.	-	
31					
Σ	—	99.3	—	-	UWAGI.

Śniezka — φ = 50°44' — λ = 15°44' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P − 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	49.0	49.6	49.1	49.2	12.9	16.6	15.8	14.3	18.4	10.5	72	58	78	69	4.1	7.9	3.5	5.2	0 ⊙	2 ⊙	5	C 0	NW 1	C 0
2	48.3	48.8	47.7	48.3	14.5	17.3	15.3	15.6	19.4	12.1	64	56	74	65	6.0	8.6	4.7	6.4	0 ⊙	6 ⊙	0 ⊙	W 2	W 2	WSW 8
3	46.4	45.5	45.5	45.1	14.7	17.8	15.2	15.7	19.1	13.8	53	54	65	57	7.9	9.4	6.0	7.8	1 ⊙	4 ⊙	6	SW 6	SW 5	NW 4
4	38.7	36.1	33.1	36.0	11.4	12.2	4.8	8.3	16.2	4.4	100	73	100	91	0.0	3.9	0.0	1.3	10 =	6 ⊙	9	SW 12	SW 16	SW 25
5	34.6	36.1	35.9	35.5	−0.2	1.8	1.2	1.0	4.8	−1.4	100	83	100	94	0.0	1.2	0.0	0.4	9	9	10 =	SW 16	SW 14	SW 18
6	35.5	39.1	41.1	38.6	−0.8	0.6	1.8	0.8	2.4	−1.1	99	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 =	WSW 10	W 6	W 8
7	41.3	42.0	42.2	41.8	0.5	3.2	2.6	2.2	5.1	0.2	98	84	93	92	0.1	1.2	0.6	0.6	9	9	7	W 5	W 8	NW 5
8	42.2	41.8	39.6	41.2	4.2	7.9	7.1	6.6	8.5	1.9	76	68	72	72	1.9	3.4	2.9	2.7	7 ⊙	7 ⊙	1	W 6	SW 5	WSW 5
9	32.4	33.9	35.5	33.9	4.8	4.4	3.6	4.1	7.1	2.3	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 =	9	SW 12	SW 10	NW 10
10	34.5	34.6	36.0	35.0	3.8	3.2	2.8	3.2	4.6	2.5	100	97	87	95	0.0	0.3	1.0	0.4	10 =	9	3	NW 16	W 17	W 12
11	36.7	38.6	37.8	37.7	5.0	7.5	10.5	8.4	11.1	2.8	100	100	91	97	0.0	0.0	1.2	0.4	10 =	9	9	W 14	W 8	W 8
12	36.2	36.4	33.0	35.2	10.8	13.5	12.3	12.2	15.5	7.8	95	73	96	88	0.7	4.3	0.5	1.8	3 ⊙	6 ⊙	8	SW 4	S 8	S 16
13	26.1	25.4	26.0	25.8	10.7	9.2	6.1	8.0	12.3	5.8	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 • =	10 =	SW 22	SW 9	W 14
14	27.2	30.4	31.9	29.8	1.3	5.6	5.9	4.2	6.5	0.7	100	82	92	91	0.0	1.4	0.7	0.7	10 =	9 ⊙	9	W 18	W 18	W 16
15	33.4	35.8	36.0	35.1	6.8	8.7	7.5	7.6	10.5	5.2	100	77	99	92	0.0	2.5	0.2	0.9	10 =	7 ⊙	10 • =	W 16	S 3	SW 5
16	33.8	34.7	33.1	33.9	5.1	7.0	4.9	5.5	7.5	4.1	75	82	98	85	2.2	1.8	0.2	1.4	2 ⊙	9	9	WNW 6	W 4	W 12
17	30.2	30.4	31.2	30.6	4.0	2.2	2.8	3.0	5.3	1.6	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 • =	10 =	W 10	WSW 10	WSW 20
18	31.6	32.1	32.1	31.9	3.6	5.0	4.6	4.4	6.1	3.0	100	100	100	100	0.0	0.0	0.0	0.0	10 =	9	10	W 12	WNW 5	W 7
19	31.8	32.3	32.2	32.1	4.1	5.4	5.8	5.3	7.3	3.2	100	100	78	93	0.0	0.0	2.0	0.7	10 • =	8	SW 5	SW 5	SW 8
20	35.5	34.2	35.5	34.4	5.0	5.0	5.2	5.1	7.9	3.8	88	90	100	93	1.0	0.9	0.0	0.6	9	10 •	10 =	WSW 6	W 8	W 6
21	34.9	35.7	36.1	35.6	4.8	4.8	4.6	4.7	5.7	4.4	100	100	100	100	0.0	0.0	0.0	0.0	10 9 =	10 =	10 =	WSW 7	W 10	W 14
22	35.9	36.7	36.4	36.3	5.1	5.6	5.8	4.6	5.9	3.7	100	97	100	99	0.0	0.3	0.0	0.1	10 =	10 =	6	W 12	WSW 6	WSW 14
23	37.0	38.6	40.0	38.5	2.8	4.6	3.6	3.6	4.8	2.6	96	100	100	99	0.3	0.0	0.0	0.1	6	10 =	9	W 8	W 4	NW 8
24	41.0	43.4	44.2	42.9	2.0	3.0	2.2	2.4	3.8	1.3	100	98	100	99	0.0	0.2	0.0	0.1	10 =	10	10 =	NW 8	NW 6	NW 12
25	45.0	46.1	45.4	45.5	1.6	3.8	4.0	3.4	5.0	0.8	94	100	86	93	0.4	0.0	1.1	0.5	10	10	1	NNW 6	NW 3	NW 4
26	43.7	42.2	38.5	41.5	5.7	7.8	11.5	9.1	11.8	3.9	92	81	68	80	0.8	2.0	4.3	2.4	7 ⊙	7 ⊙	4	W 5	W 14	SW 20
27	34.8	34.6	33.2	34.2	8.9	9.7	8.3	8.8	11.8	7.8	100	100	100	100	0.0	0.0	0.0	0.0	9	10 =	10 •	W 16	SW 14	W 18
28	29.2	28.5	29.6	29.1	8.3	6.6	7.5	7.5	10.3	5.8	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 =	10 =	SW 13	SW 18	W 8
29	32.5	35.8	37.4	35.2	3.0	3.1	2.1	2.6	7.6	1.7	100	97	100	99	0.0	0.2	0.0	0.1	10 =	8	10 =	W 12	NW 4	NNW 4
30	38.4	39.3	39.4	39.0	2.6	2.6	3.6	3.1	3.7	1.6	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 =	NW 6	NW 6	NW 10
31	37.3	38.6	39.0	38.3	3.8	4.2	3.6	3.8	4.7	3.4	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 =	9	WNW 18	W 16	W 16
M	36.6	37.3	37.2	37.0	5.5	6.7	6.1	6.1	8.7	3.9	94	89	93	92	0.8	1.6	0.9	1.1	8.1	8.6	7.7	9.9	8.4	10.8

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1	38.9	40.4	40.5	39.9	2.8	7.0	8.7	6.8	9.2	2.0	100	83	66	83	0.0	1.7	3.7	1.8	9	6 ⊙	1	W 16	WSW 7	SW 5
2	38.4	38.6	38.2	38.4	9.5	9.8	7.3	8.5	10.8	6.3	84	93	99	92	2.0	0.8	0.1	1.0	1 ⊙	9	7	SW 8	S 6	SW 10
3	39.0	41.0	42.7	40.9	6.1	6.0	3.8	4.9	8.4	3.7	98	97	100	98	0.1	0.3	0.0	0.1	9	10 =	3	W 3	W 3	NW 10
4	41.8	39.8	40.0	40.5	3.6	4.6	7.0	5.6	7.1	3.4	93	100	100	98	0.5	0.0	0.0	0.2	8 ⊙	10 •	9	W 7	WSW 11	WSW 20
5	40.9	41.3	40.2	40.8	8.2	10.2	11.5	10.4	12.0	7.0	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 =	4	W 6	W 12	SW 14
6	38.2	39.9	38.7	38.9	14.0	16.4	15.4	15.3	17.9	11.0	71	63	77	70	4.7	6.9	4.1	5.2	1 ⊙	3 ⊙	8	SW 17	SW 12	SW 10
7	37.9	38.7	40.9	39.2	10.1	9.8	7.6	8.8	15.5	7.6	96	100	65	87	0.5	0.0	3.6	1.4	10 •	9	9 •	N 4	WSW 6	W 4
8	40.7	39.9	42.1	40.9	7.0	9.8	15.6	11.0	14.5	6.7	92	100	91	94	0.8	0.0	1.5	0.8	7 ⊙	9	4	WSW 6	SSW 10	SW 17
9	43.8	45.2	44.9	44.6	11.5	15.1	12.9	13.1	15.5	11.0	100	91	80	90	0.0	1.6	3.0	1.5	9	9 ⊙	9	SW 4	SW 1	C 0
10	43.8	43.5	41.9	43.1	12.9	16.7	15.7	15.2	19.6	12.0	85	75	97	86	2.2	4.8	0.6	2.5	4 ⊙	5 ⊙	7	S 1	SW 4	W 6
11	39.6	40.3	41.2	40.4	11.3	12.1	10.3	11.0	15.9	9.9	100	99	100	100	0.0	0.1	0.0	0.0	10 ▲ K	10 =	10	WSW 6	W 8	W 12
12	40.4	40.0	39.5	40.0	8.8	8.2	4.8	6.6	10.4	4.5	83	100	87	90	1.9	0.0	1.1	1.0	9	10 • =	9	NW 4	NW 1	NW 8
13	39.9	42.5	42.8	41.7	4.8	3.2	2.2	3.1	5.5	2.1	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 =	7	NW 10	NW 8	NW 4
14	41.2	41.1	39.6	40.6	2.2	5.0	5.8	4.7	6.9	1.9	93	94	94	94	0.6	0.5	0.6	0.6	9	9 •	3	W 6	SW 8	SW 14
15	35.3	34.5	33.1	34.3	4.9	4.8	5.0	4.9	5.9	3.6	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 • =	10 • =	SW 17	SW 18	SW 16
16	31.2	31.4	32.2	31.6	0.6	1.4	2.0	1.5	5.1	0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 • =	10 =	SW 16	SW 20	WSW 20
17	28.6	29.6	31.3	29.8	1.4	2.4	2.1	2.0	2.9	0.7	100	100	100	100	0.0	0.0	0.0	0.0	10	10 =	10 =	WSW 17	W 6	N 14
18	32.5	34.0	34.0	33.4	2.8	3.3	3.3	3.2	4.2	1.8	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 =	NW 14	NW 17	NW 12
19	30.5	29.2	30.3	30.0	4.4	5.8	3.8	4.4	6.7	3.5	100	100	100	100	0.0	0.0	0.0	0.0	10 9 =	10 =	8	WNW 20	W 24	WSW 20
20	30.4	33.1	36.2	33.2	3.2	4.3	4.3	4.0	4.9	3.0	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 • =	10 =	W 17	W 15	NW 17
21	36.3	37.5	35.5	36.4	4.7	6.4	6.8	6.2	7.7	4.3	100	100	100	100	0.0	0.0	0.0	0.0	10 9 =	10 =	8	W 17	WSW 18	WSW 26
22	34.1	30.2	31.5	31.9	6.6	7.6	4.0	5.6	8.6	4.0	100	100	100	100	0.0	0.0	0.0	0.0	10 9 =	10 =	9	W 16	SW 25	SW 16
23	32.7	35.0	36.5	34.7	3.4	3.4	2.4	2.9	4.1	2.4	100	98	95	98	0.0	0.1	0.4	0.2	10 • =	9	5	SW 18	NW 16	NW 20
24	37.8	39.3	40.0	39.0	3.0	4.4	4.0	3.8	4.8	2.3	100	100	83	94	0.0	0.0	1.4	0.5	10 =	10 =	7	NW 18	NW 12	NW 4
25	38.9	40.9	41.9	40.6	4.8	6.4	7.4	6.5	7.8	3.4	100	100	100	100	0.0	0.0	0.0	0.0	9	10 =	10 =	W 10	N 12	W 14
26	42.9	45.2	45.7	44.6	6.8	9.2	9.4	8.7	11.0	6.0	94	95	97	95	0.6	0.8	0.5	0.6	7	7	10	W 10	WSW 7	WSW 8
27	46.0	47.9	48.6	47.5	10.3	13.8	11.7	11.9	15.1	9.4	87	72	92	84	1.6	4.5	1.0	2.4	2	5	8	W 10	W 6	W 6
28	48.3	50.7	50.3	49.8	7.8	10.1	10.5	9.7	11.7	7.2	99	91	54	81	0.2	1.2	5.8	2.4	8	9	7	WNW 12	NW 3	N 4
29	49.3	49.1	47.5	48.6	10.9	13.5	9.6	10.9	15.7	9.3	54	74	100	76	6.0	4.1	0.0	3.4	6 ⊙	4 ⊙	0	W 3	W 1	WNW 8
30	47.2	48.8	48.9	48.3	11.9	15.0	11.5	12.5	17.0	9.6	44	59	94	66	7.8	6.9	0.9	5.2	5	2 ⊙	0	NW 5	N 2	NW 2
31	51.1	51.4	51.8	51.1	11.3	14.9	12.1	12.8	16.4	10.1	59	68	47	58	5.6	5.3	7.4	6.1	0 ⊙	1 ⊙	0	N 2	W 1	S 8
M	39.2	40.0	40.3	39.8	6.8	8.4	7.6	7.6	10.3	5.5	91	92	91	91	1.1	1.3	1.1	1.2	7.8	8.3	6.8	10.3	9.7	11.3

DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	8	·	·	-	⊙ na–p
2	8	·	·	-	⊙ na–p
3	8	·	·	-	≡ 22^20–24; ⊙ na–p
4	7	0.0	·	-	● 7^00–10^30 ▽●⁰ 19^16–31; ∞ 0^00–4^30 ≡≡–5^20 ≡²–20^40, 22^05–24; ⋙ 4^00–11^30 ⋙–15^10, 18^05–24
5	8	1.4	·	-	▲⁰ 14^30–15^15 ▽●⁰–15^40 ▲⁰ 16^50–18^20 ▽●⁰ 19^45–20^30 ▽●⁰–20^45 ● 23^30–24; ≡² 0^00–6^05 ≡≡ 8^20–9^15, 17^25–18^20 ≡²–24; ⋙ 0^00–9^15 ⋙–19^30 ⋙–24
6	0	0.1	·	-	● 0^00–1^30 ▽* 3^55–5^20 *⁰ 6^50–7^30 △⁰ 10^15–11^10 ▽*⁰ 12^45–13^20 ● 14^00–16^40, V⁰ 1^30–9^30; ≡² 0^00–16^40 ≡≡–21^30 ≡²–22^40 ≡≡–24; ⋙ 0^00–6^20 ⋙–11^00
7	8	·	pł.	-	≡≡ 3^30–7^40, 14^30–15^35; ⊙ na...p
8	8	2.0	·	-	⊙ na...p
9	0	10.6	·	-	●⁰⁻¹ 4^00–7^10 ▽●¹–8^40 ▽●⁰–9^35 ●–16^10 ▽●¹ 20^32–46 ≡² 3^40–16^10 ≡≡ 18^30–19^15 ≡²–21^50 ≡≡ 22^30–23^05 ≡²–24; (ꓘ)⁰ 7^10–8^40 ⋙ 0^40–4^00 ⋙–7^00 ⋙–24
10	7	2.0	·	-	▽●⁰ 7^50–8^45, 11^30–12^25; ≡² 0^00–1^10 ≡≡ 4^30–7^40 ≡²–10^30 ≡≡–11^20 ≡²–12^30 ≡≡–14^20; ⋙ 0^00–24
11	7	12.6	·	-	▲▽●⁰ 23^10–30 ▽●¹–24; ≡² 3^20–12^10 ≡≡–13^40 ≡² 23^15–24; ꓘ⁰S 22^50–24; ⋙ 0^00–2^35 ⋙–13^30
12	7	0.8	·	-	▽●¹ 0^00–05 ▽●⁰–2^20 ● 23^10–24; ≡² 0^00–3^30, 22^30–24; ꓘ⁰S 0^00–1^00–2^10 N; ⋙ 2^40–6^30 ⋙ 21^20–24; ⊙ na–p
13	0	5.2	·	-	● 0^00–7^50 ●⁰ 8^30 ●–10^20 ●⁰ 11^40–14^13 ▽●¹⁻⁰ 15^45 ●⁰ 19^40–20^30 ▽●¹ 22^40–50 ▽●⁰⁻¹ 23^40–24; ≡² 0^00–16^45 ≡≡–19^30 ≡²–24; ⋙ 0^00–11^00 ⋙–11^20, 14^45–15^10, 16^40–19^00, 21^00–23^35 ⋙–24
14	8	3.8	·	-	▽●⁰⁻¹ 0^00–1^00 ●⁰ 3^20 ● 9^30–12^25; ≡² 0^00–24; ⋙ 0^00–24
15	9	18.9	·	-	●⁰ 3^50–6^10, 7^50–8^10 ▽●⁰⁻² 19^00–40 ▽●⁰ 20^50–21^00 ●⁰ 22^10 ●¹–24; ≡² 0^00–8^50 ≡≡–11^10, 18^35–50 ≡²–22^40 ≡≡–24; ⋙ 0^00–8^10 ⋙–11^20; ⊙ a...p
16	8	1.7	·	-	●¹ 0^00–1^20 ●⁰–3^30 ▽●⁰ 16^54–17^00, 17^56–18^01 ▽●¹–18^04; ≡≡ 0^00–40, 1^30–3^30, 20^40–24; ꓘ¹ 0^30–1^20; ⋙ 19^10–24; ⊙ na...p
17	0	9.1	·	-	▽●¹ 7^43–9^00 ●¹–10^40 ▽●⁰ 13^20–15^20 ●⁰ 16^30–19^40; ≡≡ 0^00–10, 4^10–6^50 ≡²–20^20 ≡≡–20^40 ≡²–24; ⋙ 0^00–14^15 ⋙–24
18	0	4.3	·	-	●⁰ 11^50–12^55 ▽●⁰ 15^50–16^10 ▽●⁰⁻¹ 17^45–19^40; ≡² ≡≡ 0^00–14^20 ≡≡ 15^50–22^00 ≡²–24; ꓘ⁰ NNE 18^10–19^30 ESE; ⋙ 0^00–5^20 ⋙–9^00; (ꓘ)¹ 17^45–19^10; ⊙ p...
19	0	1.6	·	-	●¹⁻⁰ 3^25–50 ●⁰ 7^40–9^35 ▽●⁰ 10^55–11^35, 14^35–15^20; ≡² ≡≡ 0^00–16^20 ≡² 18^30–19^20 ≡≡–19^40 ≡²–24; ꓘ⁰ SW 11^10 ESE 11^55 ꓘ SW 15^40–16^15
20	7	6.6	·	-	▽●⁰⁻¹ 11^15–14^05, 17^25–18^10 ●⁰ 21^50–22^15; ≡² 0^00–1^30 ≡≡ 8^40–9^30, 10^35–11^15 ≡²–11^26 ≡≡–12^30, 15^55–16^10 ≡≡ 17^30–18^00, 18^40–19^10 ≡² 21^30–24; ꓘ⁰ WNW 11^20–40 E (ꓘ)¹ 13^30–50, 17^40–18^00. [20.VII: ⋙ 19^30–20^20, 23^30–24; ⊙ a...p
21	0	3.5	·	-	● 0^00–17^47 ●⁰–21^10 ●–24; ≡² 0^00–24; ⋙ 0^00–1^00, 9^10–24
22	0	0.1	·	-	● 0^00–2^45 ●⁰–3^30 ●–16^20; ≡² 0^00–16^20 ≡≡–18^30 ≡²–21^15 ≡≡–23^20; ⋙ 0^00–9^20, 19^15–24
23	0	0.1	·	-	≡² 12^10–20^05; ⋙ 0^00–7^20
24	8	·	·	-	≡≡ 0^30–1^40 ≡²–3^00 ≡≡–3^30 ≡² 4^40–8^00, 10^15–12^25 ≡≡ 13^35–14^04 ≡² 17^45–22^45; ⋙ 8^35–9^40, 21^20–24
25	5	·	·	-	● 11^30–13^25 ≡≡ 0^10–1^30 ≡²–2^45 ≡≡–4^35 ≡²–5^15 ≡≡ 9^45–11^30 ≡²–13^25 ≡≡–14^35, 15^20–16^40, 17^30–20^20 ≡–24; ⋙ 0^00–30
26	6	0.1	·	-	≡ 0^00–14^20; ⋙ 11^40–20^15 ⋙–23^10 ⋙–24; ⊙ na–p; ⊕ 12^20–13^40
27	0	8.5	·	-	●⁰ 6^50–7^40, 14^30...45 ●¹ 15^35 ▽●⁰⁻¹ 16^35–18^25 ●¹–20^00 ●⁰–22^30; ≡≡ 6^20–9^20, 10^50–13^10 ≡²–14^15 ≡≡–14^40 ≡²–21^40 ≡≡–22^30; ⋙ 0^00–18^20, 19^20–24
28	0	30.8	·	-	● 3^20–4^00 ●⁰–8^45 ●¹–11^40 ●–16^43 ●⁰–17^30 ●¹–21^45 ●–22^48 ●¹–24; ∞ 0^00–3^20 ≡≡ 2^10–3^20 ≡²–24; ⋙ 0^00–9^30 ⋙–20^40 ⋙–21^30, 23^10–24
29	8	·	·	-	●¹ 0^00–3^10; ≡² ≡≡ 0^00–13^40 ≡≡ 14^15–15^00, 16^55–18^10, 19^25–21^10 ≡²–23^10 ≡≡–24; ⋙ 0^00–9^00; ⊙ a...p...; ⩊ 23^20...24
30	0	38.2	·	-	▽●▲⁰ 9^55–10^15 ● 11^30–15^25 ▽●¹ 13^12–35 ●▲ 13^12–18 ▽●⁰ 14^35–45 ●⁰ 20^50–22^20 ●¹–24; ≡≡ 0^00–30 ≡²–15^25 ≡≡–15^45 ≡²–24; ⋙ 20^30–24; ⩊ 0^00–30
31	0	9.1	·	-	●¹ 0^00–5^20 ●⁰–10^30 ●–14^05; ≡² 0^00–14^05 ≡≡–24; ⋙ 0^00–1^15 ⋙–24
Σ	—	181.1	—	-	UWAGI.

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DNI	WIDZIALNOŚĆ V	OPAD R	GRUB. ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	8	·	·	-	≡≡ 0^00–11^15 ≡ 19^30–20^30; ⋙ 0^00–8^10 ⋙–11^00; ⊙ a p
2	7	1.8	·	-	▽●⁰⁻¹ 14^52–16^20 ●⁰ 16^40–17^20, 17^30–18^20, 18^50 virga 20^50–21^30; ≡≡ 3^40–4^30, 14^45–15^55 ∞ 16^30–24 ≡≡ 21^40–23^10; ⋙ 3^00–4^30, 9^10–12^30, 16^45–20^30, 21^30–24; ⊙ na..p; ⌒ 17^48–57
3	0	2.4	·	-	▽●¹ 12^25–35; ≡² 0^30–2^40 ∞–3^80 ≡≡–8^15 ≡²–10^30 ≡≡–12^25 ≡²–15^40 ≡≡–16^15, 21^20–22^25; ⋙ 0^00–30, 20^20–23^15; ⊙ na...p
4	7	3.5	·	-	●⁰ 11^30–14^20, 17^40 ●¹–18^41; ≡≡ 12^10–17^05, 18^20–22^30 ≡²–24; ⋙ 3^20–5^30, 13^15–15^05 ⋙–24; ⊕ 6^45–10^10; ⊙ na, p z prz.
5	0	0.3	·	-	● 6^10–7^48 ●⁰ 9^30 ●⁰–11^30; ≡² 0^00–14^20 ≡≡–19^05 ≡²–21^20 ≡≡–23^25; ⋙ 0^00–6^20 ⋙–24; ⊙ na...p
6	8	2.1	·	-	< 21^47–23^30 N NE; ⋙ 0^00–15 ⋙–12^10 ⋙–22^30; ⊙ na–p
7	8	3.0	·	-	●⁰⁻¹ 5^45–10^40 ▽●⁰ 16^35–18^40 ●⁰ 21^30; ≡≡ 1^30–3^10, 4^40–5^20 ≡²–6^15 ≡≡–7^10 ∞–11^15 ≡≡–12^30, 13^35–14^20, 17^30–18^40 ≡²–20^20 ≡≡–21^15
8	8	0.0	·	-	●⁰ 18^28...45 virga 18^50–19^30; ∞ 4^30–45 ≡≡ 8^10–9^15 ≡²–12^10 ≡≡–14^30, 16^00–45 ≡²–17^05 ≡≡–18^30, 23^30–24; ⋙ 13^30–23^15; ⊙ na–p
9	7	0.5	·	-	▽●⁰ 15^55–16^04, 16^58–17^31 ●⁰ 19^48–20^30; ≡≡ 0^00–4^30, 6^30–8^40, 13^10–15^20 ≡²–17^40; < 22^05–50 SE; na...p
10	9	5.5	·	-	▲¹▽●¹ 19^55–20^25; ≡≡ 18^30–19^15, 20^40–22^30 ≡²–24; (ꓘ)⁰S 19^25–55 ꓘ¹–20^25 (ꓘ)⁰SE–20^40; ⊙ na–p
11	0	14.2	·	-	▽●⁰ 3^55–5^20 ▲¹ 7^35–45 ▽●⁰⁻¹ 7^35–12^18, 15^00–13; ≡² 0^00–40 ≡≡–2^30 ≡² 7^35–55 ≡≡ 8^05–45 ≡²–10^00 ≡≡ 10^30–11^25 ≡²–12^10 ∞–13^45 ≡²–16^15 ≡≡–17^05 ∞ 17^30–21^00 ≡ 19^30–21^00 ≡≡ 20^45–21^00 ≡²–24;
12	0	18.2	·	-	▽●¹ 13^43–15^10 ▽●⁰–15^30 ●⁰–19^35; ≡² 0^00–4^30 ≡≡–8^05, 10^40–13^30 ≡²–18^10 ≡≡–19^15, 22^35–23^30 ≡²–24; (ꓘ)⁰ 13^50–15^15; ⋙ 0^00–2^30, 22^40–24 [11.VIII: (ꓘ)¹⁻² 8^30–11^30; ꓘ¹ 7^35–45 (ꓘ)¹SE 7^45–8^45 ꓘ¹–10^10
13	0	3.9	·	-	●⁰ 3^35–4^12, 6^40–9^00 ● 10^30–11^50 ●⁰–12^30 ●⁰–12^40; ≡² 0^00–14^00 ≡≡–17^30; ⋙ 0^00–8^30 ⋙ 10^40–12^30 [11.VIII: (ꓘ)¹E 10^10–45 ꓘ⁰–11^20; ⋙ 16^40–24; ⊙ a..p
14	7	0.5	·	-	▽●⁰ 13^40–14^08, 17^55–18^10; ≡≡ 3^20–4^15 ≡²–5^10 ≡≡–5^25, 11^20–12^05, 14^00–15, 14^30–16^45, 19^00–40 ≡² 22^45–24; ⋙ 15^30–24; ⊙ na...p
15	0	8.4	·	-	● 4^20–5^15 ▽●⁰ 8^20–28 ●⁰ 10^43–11^40 ●¹–12^30 ●⁰ 14^45, 15^34–16^57, 21^10–24; ≡² 0^00–5^15 ≡≡–6^10 ≡²–24; ⋙ 0^00–2^30 ⋙–24
16	0	8.2	·	-	●⁰ 0^00–40 ▽●¹ 11^50–13^30 ●⁰–21^45 ●–23^30; ≡² 0^00–5^50 ≡≡, ≡² 6^30–11^40 ≡²–24; ⋙ 0^00–24
17	0	2.6	·	-	●⁰ 15^45–18^45; ≡² 0^00–5^15 ≡≡–6^10 ≡≡ 7^15–8^00 ≡²–8^40 ≡≡–10^20 ≡²–24; ⋙ ⋙ 0^00–12^30, 21^40–24; ⊙ na... a
18	0	7.7	·	-	●⁰ 4^45–5^30 ●–8^35 ●⁰–9^05 ▽●⁰⁻¹ 9^15–14^15; ≡² 0^00–16^30 ≡≡–17^45 ≡²–18^20 ≡≡–19^20 ≡²–24; ⋙ ⋙ 0^00–24; (ꓘ)¹ 9^30–52, 9^55–10^08; ⊙ p
19	0	5.8	·	-	● 0^00–7^40 ●¹–9^50 ●⁰–11^45, 19^50–20^40; ≡² 0^00–15^15 ≡≡–15^45 ≡²–20^40 ≡≡–24; ⋙ 0^00–30 ⋙–24
20	0	8.2	·	-	● 1^10–5^30 ●⁰ 6^10–10^40 ●⁰–11^30 ●⁰–12^00 14^10 ▽●¹ 16^13–30, 19^13–44 ▽●⁰–20^40 ●⁰ 22^30–23^30–24; ≡≡ 0^00–30 ≡²–14^15 ≡≡–15^40, 16^10–40, 18^15–19^40 ≡²–24; ⋙ 0^00–24; ⊙ a–p
21	0	0.7	·	-	●⁰ 0^00–4^30, 6^20–7^00 ●⁰ 7^30–9^40; ≡² ≡≡ 0^00–24; ⋙ 0^00–24
22	0	8.6	·	-	●⁰ 6^10–8^30 ●⁰ 13^40 ●–14^35 ●¹–14^45 ●–17^05 ▽●¹–17^10; ≡≡ 0^00–1^20 ≡²–4^20 ≡≡ 5^30–6^10 ≡²–17^05 ≡≡–19^10, 21^15–22^30 ≡²–24; ⋙ 0^00–24; (ꓘ)⁰ 16^54–17^05
23	8	1.9	·	-	▽●⁰ 2^55–4^10, 4^40–5^35, 6^40–7^50 ▽●¹–8^10 ▽●⁰–9^05 ●⁰ 9^25–10^25, 16^52–17^20; ≡²⁻¹ 0^00–13^32 ≡≡–16^50 ≡²–17^30 ≡≡–24; ⋙ 0^00–9^20 ⋙–12^10 ⋙–24; ⊙ a...p
24	0	0.6	·	-	● 0^15–15^40; ≡≡ 0^00–15 ≡²–15^40 ≡≡–17^30 ≡²–18^10 ≡≡–18^30, 22^40–23^10; ⋙ 0^00–12^30 ⋙–19^10
25	0	0.0	·	-	● 4^00–5^10 ●⁰ 14^35–15^46 ● 20^10–23^40; ≡² 2^30–5^10 ≡≡ 6^30–10^25 ≡²–15^46 ≡≡–19^40 ≡²–23^40; ⋙ 3^40–21^05 ⋙–24; ⊙ p...
26	7	0.0	·	-	●⁰ 23^30–24; ≡≡ 0^00–8^30 ≡²–9^40 ≡≡–12^00; ⋙ 0^00–9^40, 17^30–20^20, 22^15–24
27	8	·	·	-	●⁰ 0^00...40; ≡≡ 22^25–24; ⋙ 0^00–9^30
28	7	·	·	-	≡≡ 0^00–30 ≡²–1^45 ≡≡–2^35 ≡²–4^25 ≡≡–14^00; ⋙ 6^20–10^40; ⊙ p; ⏂ 21^30–22^40
29	8	·	·	-	≡ 20^30–21^04 ≡≡–21^10; ⊙ na–p
30	8	·	·	-	⊙ na–p
31	9	·	·	-	⊙ na–p
Σ	—	108.4	—	-	UWAGI.

Śnieżka — φ = 50°44' — λ = 15°44' — Wrzesień – Septembre 1961

DNI	CIŚNIENIE P = 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	50.5	51.8	49.4	50.6	9.9	14.5	12.5	12.4	15.8	9.0	73	53	67	64	3.3	7.8	4.8	5.3	0 ⊙	1	0	S 14	SW 14	SW 16
2	46.7	46.0	44.0	45.6	10.9	14.5	12.9	12.8	16.3	10.1	65	55	59	60	4.5	7.5	6.0	6.0	1 ⊙	0 ⊙	0	SSW18	SW 16	SW 16
3	41.1	40.9	39.3	40.4	12.9	16.5	13.6	14.2	16.5	8.7	52	56	58	55	7.2	8.4	6.5	7.4	3 ⊙	2 ⊙	2	SW 10	SW 6	W 6
4	39.3	40.7	40.7	40.2	11.8	13.3	11.7	12.1	15.8	11.2	100	84	81	88	0.0	2.5	2.6	1.7	10 ⚌	8 (☂)	9 (☂)	NNW 6	NW 8	W 6
5	39.0	38.7	38.1	37.6	12.1	14.5	10.4	11.8	15.4	9.6	88	74	97	86	1.7	4.4	0.3	2.1	3 ⊙	4 ⊙	9	W 8	W 7	W 14
6	33.9	33.7	32.2	33.3	9.9	8.5	8.4	8.8	13.0	7.1	89	97	100	96	1.3	0.3	0.0	0.5	9	10	10 ⚌	SW 4	SW 6	SW 10
7	30.0	28.3	30.4	29.6	6.6	5.2	2.6	4.2	8.4	2.5	100	100	100	100	0.0	0.0	0.0	0.0	10 • ⚌	10 • ⚌	10 ⚌	SW 12	SW 18	SW 16
8	30.9	31.2	34.6	32.2	0.6	2.3	3.0	2.2	4.0	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 * ⚌	10 ⚌	10 ⚌	WSW18	WSW18	WSW17
9	36.4	38.7	38.2	37.8	4.0	3.4	2.9	3.3	4.8	2.6	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	10 ⚌	10 ⚌	NW 12	NNW12	NW 16
10	38.4	39.3	39.9	39.2	1.6	2.0	1.8	1.8	3.1	1.3	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	10 ⚌	10 ⚌	NNW16	NNW14	NNW14
11	39.5	39.6	37.9	39.0	1.4	3.4	4.9	3.6	4.9	1.1	100	91	91	94	0.0	0.7	0.8	0.5	9	10	5	WNW 8	WNW 5	WNW 9
12	36.7	36.9	37.5	37.0	5.4	5.4	4.8	5.1	7.1	4.5	84	100	100	95	1.5	0.0	0.0	0.5	8 ⊙	10 • ⚌	8	W 18	W 14	WNW14
13	37.6	39.2	37.6	38.1	3.8	5.8	6.6	5.7	6.7	3.4	100	97	100	99	0.0	0.3	0.0	0.1	9 ⊙	9	4	W 12	W 8	W 14
14	35.9	36.2	35.4	35.8	8.8	8.8	8.4	8.6	10.3	6.6	93	100	100	98	0.8	0.0	0.0	0.3	8	10 ⚌	10 ⚌	WSW16	WSW22	WSW28
15	38.3	43.5	44.9	42.2	2.6	7.4	9.6	7.3	9.7	2.4	83	79	76	79	1.2	2.1	2.9	2.1	4 ⊙	7 ⊙	2	NW 18	NNW 5	WNW15
16	46.0	47.5	45.8	46.4	14.3	16.8	12.8	14.2	17.7	9.3	54	68	92	71	7.5	6.0	1.3	4.9	8 ⊙	3 ⊙	1	WNW 5	WNW 3	WSW10
17	45.7	46.9	46.9	46.5	13.4	17.2	13.7	14.5	17.7	12.8	57	57	77	64	6.6	8.4	3.5	6.2	0 ⊙	1 ⊙	0	WSW14	WSW12	WSW10
18	46.9	48.3	47.8	47.7	15.1	17.7	15.1	15.8	20.4	13.1	61	72	77	70	6.7	5.6	4.0	5.4	7 ⊙	3 ⊙	0	NW 6	NNW 3	W 2
19	46.3	46.2	44.9	45.8	11.5	17.2	12.1	13.2	17.4	11.5	100	69	70	80	0.0	6.1	4.2	3.4	10 ⚌	3 ⊙	0	W 4	W 1	NNW 3
20	43.9	44.1	43.7	43.9	12.0	10.5	13.1	12.2	13.9	9.5	11	47	12	23	12.4	6.8	13.3	10.8	0 ⊙	0 ⊙	0	N 4	W 4	W 3
21	45.3	45.1	46.4	44.9	11.8	12.9	11.9	12.1	14.1	9.5	18	55	20	31	11.4	6.6	11.1	9.7	0 ⊙	0 ⊙	0	NE 4	E 4	ENE 3
22	46.8	48.3	48.1	47.7	12.3	14.3	12.5	12.9	15.7	10.8	6	35	4	15	13.5	10.7	13.9	12.7	0 ⊙	0 ⊙	0	ESE 5	SE 2	SW 2
23	46.9	47.2	45.9	46.7	12.0	13.5	8.9	10.8	14.1	8.9	14	45	66	42	12.0	8.4	3.8	8.1	2 ⊙	1 ⊙	0	ESE 4	SW 3	SW 8
24	44.2	45.0	44.5	44.6	7.4	11.7	9.4	9.5	14.1	6.7	62	63	59	61	3.9	5.1	4.8	4.6	0 ⊙	0 ⊙	0	SW 4	SW 3	W 6
25	43.3	45.3	45.8	44.8	10.4	12.9	8.5	10.1	13.3	8.3	23	61	100	61	9.7	5.7	0.0	5.1	1 ⊙	5 ⊙	10 ⚌	W 8	W 6	NW 3
26	44.8	44.7	42.8	44.1	6.8	9.4	7.4	7.8	9.6	6.5	85	78	69	77	1.7	2.6	3.2	2.5	9	9	4	WNW 3	WNW 3	WSW 7
27	40.6	40.7	41.4	40.9	5.2	7.3	8.0	7.1	8.6	4.5	88	96	59	81	1.0	0.4	4.4	1.9	3 ⊙	9	0	W 5	WSW 6	W 4
28	40.9	42.6	43.6	42.4	9.8	12.7	12.7	12.0	13.8	7.6	84	83	54	74	2.0	2.4	6.8	3.7	6 ⊙	8	1	W 8	W 4	NW 3
29	43.7	43.9	43.9	43.8	12.2	14.1	13.2	13.2	14.8	11.0	81	65	51	66	2.7	6.6	7.2	5.5	2 ⊙	7 ⊙	3	W 2	WSW 8	WNW 6
30	42.6	41.3	40.1	41.3	12.5	15.0	12.5	13.1	15.3	11.9	50	56	67	58	7.2	7.4	4.8	6.5	8	9 ⊙	1	SE 8	SE 7	S 8
31																								
M	41.3	42.1	41.6	41.7	9.0	11.0	9.5	9.8	12.4	7.4	71	75	74	73	4.0	4.1	3.7	3.9	5.3	5.6	3.9	9.1	8.0	9.6

Październik – Octobre

1	39.6	39.8	40.2	39.9	9.9	9.7	6.4	8.1	12.8	1.8	80	30	30	47	2.5	8.4	6.8	5.9	9	6 ⊙	1	S 7	SE 6	ESE14
2	41.4	43.0	43.3	42.6	5.3	4.6	2.6	3.8	7.0	2.4	44	71	100	72	5.0	2.4	0.0	2.5	1 ⊙	4 ⊙	10 ⚌	SE 14	SE 10	SE 18
3	43.3	44.0	42.8	43.4	4.2	7.2	4.2	5.0	8.3	2.4	85	79	95	86	1.2	2.2	0.5	1.3	0 ⊙	3 ⊙	0	SE 16	SE 8	SE 16
4	41.5	41.0	41.3	41.3	3.2	4.8	5.3	4.6	5.4	2.3	95	100	90	94	0.5	0.0	0.9	0.5	10	10 ⚌	8	S 20	SW 22	SW 25
5	39.9	42.9	43.7	42.2	4.2	6.6	6.2	5.8	7.2	4.0	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	8	10 ⚌	SW 25	SW 25	SW 20
6	41.9	39.9	34.2	38.7	6.4	7.4	4.6	5.8	8.3	4.4	76	75	82	78	2.3	2.6	1.6	2.2	1 ⊙	1 ⊙	0	SW 20	SW 26	SW 30
7	28.4	27.1	27.3	27.6	2.8	4.4	4.4	4.0	4.7	2.3	79	95	100	91	1.7	0.5	0.0	0.7	2 ⊙	9	10 ⚌	WSW20	SW 25	SSW25
8	28.6	29.6	34.8	31.0	3.5	3.8	3.4	3.5	4.6	3.2	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	10 ⚌	10 • ⚌	SSW18	SW 20	SW 12
9	41.5	46.0	48.9	45.5	2.6	7.6	5.0	5.0	7.9	1.3	96	78	90	88	0.3	2.3	0.9	1.2	7	4 ⊙	0	WNW 6	W 6	NW 6
10	49.7	50.3	49.0	49.7	5.5	9.6	9.4	8.5	12.0	4.4	79	79	12	57	1.8	2.6	10.4	4.9	2	4 ⊙	0	W 4	W 2	SE 6
11	46.7	46.8	46.9	46.8	9.0	9.6	11.1	10.2	11.8	6.4	18	38	25	27	9.4	7.4	9.9	8.9	0 ⊙	1 ⊙	1	SSE 4	SSE 8	WSW 6
12	46.1	47.9	47.0	47.0	6.8	6.2	2.6	4.6	11.2	2.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	10 ⚌	10 ⚌	NW 10	NNW10	N 12
13	44.7	46.8	45.4	45.6	-0.6	1.2	-0.5	-0.1	2.6	-0.7	99	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	9	10 ⚌	N 10	N 10	W 16
14	44.8	46.2	45.0	45.3	-1.6	1.8	0.6	0.4	5.9	-2.4	98	56	100	85	0.1	3.1	0.0	1.1	10 ⚌	8	9	N 12	N 5	NW 12
15	44.2	45.4	43.2	44.3	1.0	7.2	7.6	5.8	9.1	0.6	100	71	32	68	0.0	3.0	7.1	3.4	10 ⚌	5 ⊙	1	NW 12	NW 5	W 6
16	41.2	40.0	37.4	39.5	7.4	8.0	5.3	6.5	8.9	3.7	47	56	59	54	5.5	4.7	3.7	4.6	1 ⊙	6 ⊙	0	W 6	W 5	W 10
17	32.5	28.7	19.8	27.0	0.7	2.0	2.1	1.7	6.3	0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	10 ⚌	10 • ⚌	SW 10	SW 14	SW 25
18	11.6	13.0	14.7	13.1	0.6	0.8	-0.2	0.2	2.3	-0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 • ⚌	10 • ⚌	10 * ⚌	SW 20	SW 14	ESE 3
19	16.4	18.7	22.1	19.1	-2.0	0.0	0.2	-0.4	1.1	-2.3	98	100	100	99	0.1	0.0	0.0	0.0	10 ⚌	10 ⚌	10 ⚌	SW 8	S 7	SSW10
20	27.6	30.1	30.5	29.4	1.8	2.0	3.0	2.4	3.3	-2.9	50	51	100	67	3.5	3.5	0.0	2.3	9	10	10 • ⚌	SSW 6	E 5	N 8
21	30.1	30.0	31.1	30.4	3.8	0.2	-1.8	0.1	4.3	-1.8	100	100	98	99	0.0	0.0	0.1	0.0	10 ⚌	10 • ⚌	10 • ⚌	NE 6	SW 10	SW 14
22	36.7	39.2	40.2	38.7	-2.0	1.0	1.6	0.6	2.9	-2.9	98	96	86	93	0.1	0.3	1.0	0.5	4 ⊙	9	1	SW 15	SW 14	SW 16
23	39.8	38.5	40.7	39.7	2.0	2.3	0.8	1.5	3.0	0.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ⚌	10 ⚌	10 ⚌	SW 18	SSW20	SW 12
24	40.5	42.2	40.4	41.0	0.7	2.8	3.4	2.6	3.9	0.5	100	100	79	93	0.0	0.0	1.7	0.6	10 • ⚌	10 ⚌	2	SW 14	SW 10	WSW16
25	36.1	35.8	37.4	36.4	0.0	0.8	4.0	2.2	5.8	-0.5	100	100	100	100	0.0	0.0	0.0	0.0	7 ⊙	10 ⚌	10 ⚌	WSW20	SW 25	SW 20
26	35.8	35.2	35.8	35.6	2.7	7.0	5.2	5.0	7.4	2.6	100	98	91	96	0.0	0.1	0.7	0.3	9	9	8	SSW20	SSW20	SSW17
27	33.3	34.9	33.7	34.0	12.7	12.5	4.8	8.7	12.9	3.6	35	70	100	68	9.4	4.5	0.0	4.6	9	5	10 ⚌	SSW 8	W 4	SW 14
28	34.2	33.9	33.4	33.8	5.4	5.8	3.3	4.4	10.9	2.8	92	86	100	93	0.8	1.3	0.0	0.7	5	7 ⊙	10 ⚌	WNW 5	N 2	N 2
29	32.2	32.8	34.3	33.2	1.4	2.0	0.7	1.2	3.6	0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 • ⚌	10 • ⚌	0	N 3	N 4	SSE 4
30	35.3	36.1	37.3	36.2	0.9	2.8	1.0	1.4	4.9	0.1	81	83	87	84	1.3	1.2	0.9	1.1	2 ⊙	7 ⊙	5	NW 3	W 4	W 3
31	37.6	37.2	39.1	38.0	-0.8	0.3	-0.4	-0.3	1.4	-1.2	93	98	96	96	0.4	0.1	0.1	0.2	4	9	2	W 12	SW 18	WNW10
M	36.9	37.5	37.5	37.3	3.1	4.6	3.4	3.6	6.4	1.2	85	84	86	85	1.5	1.6	1.5	1.5	6.8	7.5	6.0	12.0	11.6	15.2

Śnieżka — $H_s = 1603\ m$ — $H_k = 1610{,}6\ m$ — Wrzesień – Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ POKRYWY SNIEŻNEJ h	USŁONECZNIENIE	POGODA
1	8	.	.	–	≫ 23⁰⁰ 17³⁰ ≋ –24. ○ na–p
2	8	.	.	–	≋ 0⁰⁰ 24. ○ na–p
3	8	4.0	.	–	● ▽ 18²⁸–⁴⁰ ▲ ² 18³⁰–⁴⁰ ● ▽ –18⁴⁸ = 19³⁰–⁵⁰ (K) SW 18¹⁸–²⁸ K = 18⁴⁵ (K) SE –19¹⁰. (≲) ¹⁻² 18³⁰–³⁵ ≋ 0⁰⁰ 23⁰ ≫ 9³⁰ 18³⁰–⁴⁵ 22³⁰ 24. ○ na p. ∩ 18³⁰ 19¹⁰
4	6	0.3	.	–	● ² ²⁵–²⁸ 19⁰⁰ 20⁴⁵ = 5³⁰ 6⁴⁵ = ² 8⁴⁰ = –0³⁰ 12²⁰ 13³⁰ ≲ S–N 2²⁰ 4³⁰ (K) SW 12⁵⁷ 19²⁰ K 20³⁰ (K) 23⁵⁰ ENE. ≫ 0⁰⁰ 7¹⁵
5	7	8.6	.	–	▽ ⁰⁻² 19⁵⁰ 20⁴⁶ ● ▽ 22¹⁵ ▲ ² 20⁵³–⁵⁶ = 20³⁰ 21⁴⁵ = –22¹⁰. (K) W 19³⁰ 20³⁰ K 21⁰⁰ (K) 21¹⁵ WW. ≲ 19³⁰ 21¹⁵. ≫ 19⁴⁰ 23¹⁵. ○ na–p
6	7	2.1	.	–	● 19³⁰ 24. ≫ 21³⁰ 23³⁰ ≋ –24. ▥ 5³⁰ 14¹⁰ = 8³⁰ 11⁴⁵. 14⁰⁰–¹⁰ = ² 24
7	0	7.6	.	–	● 0⁰⁰ ²⁴⁵ ● ⁰ –4²⁰ ● –5³⁰ ● –10²⁵ 10⁴⁰ ● –12³⁰ ● ... 14⁴⁰ ● –15⁵⁰ ● ▽ –16²⁰ ● ▽ ⁰ 16³⁰ ● –18³⁰ 21²⁰ 24. = ² 0⁰⁰ 18³⁰ = –21⁰⁰ = ² –24. ≋ ≫ 0⁰⁰ 24
8	0	6.0	.	–	● 0⁰⁰ 6⁵⁰ ● ⁰ 7³⁰ ● ⁰ –9⁴⁰ ● 11³⁰ 21¹⁰. = ² 0⁰⁰ 21⁷⁰ = –21⁴⁵ = ² –24. ≋ 0⁰⁰ 24
9	0	6.8	.	–	● 3³⁰ 4³⁰ ● ▽ – 4⁵⁰ ● –10³⁰ ● ¹ 11²⁰ ● –24. = ² 0⁰⁰ 24. ≋ 0⁰⁰ 4⁴⁰ ≫ –19¹⁰ ≋ –24
10	0	1.6	.	–	● 0⁰⁰⁻⁴⁰ ● ⁰ ⁰ –1³⁰ ● –2⁰⁵ ● ⁰ 3³⁰ ● –5²⁰ ● ⁰ 6³⁰ ● –14²⁰. 20³⁰ 24. = ² 0⁰⁰ 24. ≋ 0⁰⁰ 13³⁰ ≫ –18²⁰ ≋ –21³⁰ ≫ 24
11	7	.	.	–	● 0⁰⁰ 2⁵⁰ = ² 0⁰⁰ 3²⁰ = –9⁴⁰ 16³⁵ 19¹⁰. ≫ 0⁰⁰ 6³⁰
12	0	1.5	.	–	▽ ⁰ 13¹² 14²⁰ ● 20¹⁵ 21¹⁰. = ¹⁻³ 3³⁰ = ² 6¹⁰ = –7⁰⁵ ▥ –9¹⁰ = 10²⁰ 12³⁰ = ² –14⁰⁰ = –14¹⁵ 15⁵⁰ 16²⁵ = ² 17⁴⁰ = 19⁴⁵ 20³⁰ 21³⁰ 23³⁰ ≫ 0¹⁰ 4¹⁰ ≋ –9³⁰ ≫ 24. ○ na p. ⊕ 15³⁰ 16²⁵
13	7	0.1	.	–	● ⁰ 3⁴⁵ 4¹⁵ ● 5³⁰ 7⁰⁰ ▽ ● 18³⁵ 19¹⁵. = ² 23⁵⁰ 7⁰⁰ = –13²⁰ = ² 15²⁰⁻⁴⁰ = –17²⁰ = ² –20³⁰ = –22²⁰ ≫ 0⁰⁰ 8³⁰ 19³⁰ 24. ○ na p
14	0	7.3	.	–	● 9³⁰ 16⁴⁵ ● ▽ 16³⁰ 17¹⁰ 17²¹–³⁴ ● 17⁵⁰ 19⁴⁵ 21³⁰ ● 22¹⁰ 24. = = ² 8¹⁰ 24. ≫ 0⁰⁰ 2⁰⁰ ≋ –24
15	9	.	.	–	● 0⁰⁰⁻⁰⁵ = ² 0⁰⁰⁻⁰⁵ = –3¹⁵ ▥ – 11³⁰; ≋ 0⁰⁰ 10¹⁰ ≫ 11²⁰. 19⁴⁰ 23²⁰. ○ na–p
16	8	.	.	–	≫ 21⁴⁰ 24. ○ na–p
17	9	.	.	–	≫ 0⁰⁰ 22⁰⁵. ○ na–p
18	8	.	.	–	○ na–p
19	7	.	.	–	= 0³⁰ 7³⁰ = –7⁴⁵ = ² 8⁰⁰ ▥ 6⁰⁰ 14⁰⁵ = ² 16⁰⁵ = –16⁴⁰ ▥ –24. ○ a–p
20	8	.	.	–	▥ 0²⁰ 12²⁰. ○ na–p
21	9	.	.	–	▥ 4¹⁰ – 11³⁰. ○ na–p
22	9	.	.	–	○ na–p
23	8	.	.	–	▥ 4⁴⁰ 13³⁰. ○ na–p
24	8	.	.	–	○ na–p
25	6	.	.	–	● 18¹⁰ 19¹⁵. = 12³⁰ 18¹⁰ = 14²⁰ 18¹⁰ = ² –19¹⁵ = –20³⁰ = 19⁴⁵ 21⁴⁰ ▥ 19¹⁵ 21⁴⁰ = ² –23³⁰ ▥ –24. ○ na p
26	7	2.0	.	–	● ⁰⁻¹ 15⁵⁵ 17⁵⁰. ▥ 0⁰⁰ 13⁰⁵ = 6³⁰ 8³⁰ = ² 16³⁰ 18²⁰. ○ a–p
27	6	.	.	–	= 1³⁰ 4³⁰ = ² –5⁴⁰ = = –7³⁰ ▥ –9⁰⁰ = –9³⁰ 11⁵⁰ 13²⁰ = 10²⁰ – 15³⁰ = 14³⁰ 15²⁰. ○ na p
28	8	1.3	.	–	▽ ⁰ 14¹¹. 16⁰¹ ● ▽ ⁰⁻² 16¹⁰ ▲ ⁰ 16⁰¹–⁰² = 5²⁰ 7³⁰. 7⁵⁰ 8²⁰ ▥ 5⁰⁰ 10¹⁵ = 17⁵⁰ 18¹⁵. (K) ⁰ SE 16¹² 17²⁰. ≫ 6³⁰ 7²⁰. ○ na p
29	8	.	.	–	○ na p
30	8	.	.	–	○ p
31					
Σ	–	49.2	–	–	UWAGI.

Październik – Octobre

1	7	.	.	–	= 19⁴⁵ 20²⁰ ▥ 23³⁰ 24. ≫ 17³⁰ 23²⁰ ≋ –24. ○ a–p. ⊕ 14³⁰ 16³⁰
2	8	.	.	–	● 20³⁰ 22⁰⁵ ▥ 0⁰⁰ 12⁴⁰ = – 16¹⁰ = ² –22⁰⁵ = –22²⁵. ≋ 0⁰⁰ 2³⁰ ≫ –4³⁰ 5³⁰ 19⁴⁰ ≋ –24. ○ na–p
3	8	.	.	–	= 16³⁰ 17³⁰ = ² 23⁴⁰ 24. ≋ 0⁰⁰ 11²⁰ ≫ – 12³⁰ 17³⁰ 20³⁰ ≋ –24. ○ na–p
4	0	0.4	.	–	● 0⁰⁰ 9³⁰ ● ⁰ 10³⁰ ● –16²⁰. = ² 0⁰⁰ 0³⁰ = = –1²⁰. 6³⁰ 7⁴⁰ = ² 15²⁰ = = –16¹⁵. 22⁴⁰ 23³⁰. ≋ 0⁰⁰ 24
5	7	0.0	.	–	● 4³⁰ 8⁰⁰ 22³⁰ 24. = ² 0⁰⁰ – 4³⁰ 8⁰⁰⁻¹⁰ = –13⁰⁵ 19³⁰ 20¹⁰ = ² –24. ≋ 0⁰⁰ 24. ○ p
6	8	.	.	–	● 0⁰⁰ 2³⁰. = 2³⁰ 5¹⁵. 7⁴⁰ 8²⁵. ≋ 0⁰⁰ 24. ○ a–p
7	8	0.2	.	–	● 19⁰⁰ 24. = 4¹⁵–⁴² = ² –24. ≋ 0⁰⁰ 24
8	0	2.7	.	–	● 0⁰⁰ 2¹⁵ 4¹² 14⁴⁵ ● ⁰ 16³⁰ 21³⁰ ● ¹ –23³⁰ ● –24. = ² 0⁰⁰ 2¹⁵ = –4¹⁰ = ² 24. ≋ 0⁰⁰ 20³⁰ ≫ –21¹⁵
9	9	.	.	–	● 0⁰⁰ ¹⁰⁵. 1³⁰ 3¹⁰ winga 6⁴⁵ 7³⁰. = ² 0⁰⁰ 10⁵. 1³⁰ 3¹⁰ ▥ – 15⁴⁰ = 7⁰³ 8⁴⁰. ○ a–p
10	9	.	.	–	⌴ ⁰ 2³⁰ 6³⁰. ○ a–p
11	9	0.2	.	–	○ a–p
12	0	0.3	.	–	● 5³⁰ 9³⁰. 9⁴⁰ 12⁰⁰. 18³⁰ 24. = ² 4²⁰ 9²⁵ = –9⁴⁰ = ⁴ 15⁵⁰ = – 18³⁰ = ² –24. ≫ 0⁰⁰ 13¹⁰ 20²⁰ 24. ○ a . p
13	7	0.6	.	–	● 0⁰⁰ 5¹⁰ 9³⁰ 10²⁰ 18³⁰ 20³⁰ ▽ ⁰ 5¹⁰ 9³⁰ 20³⁰ 24. = ¹ 0⁰⁰ 10²⁰ = – 13¹⁵ = ² – 14⁰⁰ = – 15²⁰ = ² –24. ≫ 0⁰⁰ 20³⁰ ≋ –23³⁰ ≫ –24
14	8	0.3	.	–	● 21²⁵ 24 ▽ ● 0⁰⁰ 1³⁰ V ⁰ –9²⁵. = ² 0⁰⁰ 9²⁵ = –9³⁵ ▥ – 14¹⁰ = 10⁴⁵ 11³⁰. 17³⁵ 21²⁵ = ² –24. ≫ 0⁰⁰ 9⁴⁰. 20¹⁵ 24. ○ p z prz
15	8	.	.	–	● 0⁰⁰ 8³⁰. = 0⁰⁰ 8³⁰ = –9²⁰ ▥ 8³⁰ 19²⁰. ≫ 0⁰⁰ 9²⁰. @ 8³⁰ 11²⁰
16	8	0.1	.	–	▥ 11⁴⁰ 15⁰⁰ = 18³⁵ 19¹⁵ ▥ – 23²⁰ = –24. ≫ 20⁰⁰ 24. ○ na–p. ⌴ 17²⁰ – 19²⁰
17	0	8.1	.	–	● 0⁰⁰ 13⁴⁰ ● ⁰ 19⁴⁵ ● –20³⁵ ● ⁰ –24. = = 0⁰⁰–15 = ² –24. ≫ 0⁰⁰ 3⁰⁰ ≋ –4¹⁰ ≫ –13³⁰ ≋ –24
18	0	10.5	.	–	● ⁰ 0⁰⁰ 5¹⁰ 13¹⁵ ● ⁰ – 14²⁰ ● ⁰ 15¹⁵ ● ⁰ –15³⁵ ● ⁰ –16¹⁰ ● ⁰ –17²⁰ ● ⁰ –18¹⁰ 18²⁰ 24. = ² 0⁰⁰ 24. ≋ 0⁰⁰ 10³⁰ ≫ – 15³⁵
19	0	0.0	2	–	● ⁰ 0⁰⁰ 1⁴⁰ ● –2⁵⁰ ● 8⁴⁵ 11²⁰ ● ⁰ –11³⁰ ● 15⁰⁰ 22¹⁰. \ 2⁵⁰ 7³⁰. = ² 0⁰⁰ 7³⁰ = –12⁰⁰ = ² –14⁰⁰ ▥ 9³⁰ 11¹⁰ = ² –24. ≫ 8³⁰ 9⁵. 14³⁰ 21⁰⁰
20	7	23.1	.	–	● ⁰ 13²⁰ 14⁵⁰ ● ⁰ – 15²⁰ ● ⁰ –17³⁰ ● ⁰ –19²⁰ ⁰⁻² 22³⁰. = ² 0⁰⁰⁻¹⁰ = 15⁴⁵ 16¹⁰ = ² –24. ≈ 17³⁰ 19³⁰. ≫ 16³⁵ 19³⁰
21	0	5.6	.	–	● 1¹⁰ 7⁴⁰ 3³⁰–³⁵ 18²⁵–⁴⁵ ● ⁰ 19²⁰ ● ⁰ –11³⁰ ● 14⁴⁰ ● ⁰ 18⁵⁰ 19⁵⁵ 20²⁰ 24. ≈ 14⁴⁰ 24. ≫ 10²⁰ 22³⁰ ≋ –24
22	8	0.5	.	–	● ⁰ 0⁰⁰ 3⁴⁰ ▽ 0⁰⁰ 4²⁰. = ² 0⁰⁰ 4²⁰ = –5²⁰ ▥ – 6³⁰ = ² 9⁴⁰ 10¹⁰ = – 10²⁰. ≋ 0⁰⁰ 1¹⁵ ≫ –20³⁰ ≋ –24. ○ na–p
23	0	4.2	.	–	● 4³⁰ 8³⁵ ● ⁰ 9²⁰ ● ⁰ – 10¹⁰ ● ⁰ –11⁴⁰ ● –24. = ² 0⁰⁰ 24. ≋ ≫ 0⁰⁰ 24
24	0	0.8	.	–	● 0⁰⁰ 2⁰⁰ ● ⁰ 6³⁰ ● ⁰ –7¹⁵ ● –9²⁰. = ² 0⁰⁰ 17³⁰ = –18⁴⁰ = ² 19⁰⁰ = – 19⁴⁰ ▥ –24 = 21³⁰ 24. ≫ 0⁰⁰ 6⁰⁰ ≋ –6³⁰ ≫ 18⁴⁰ 20³⁰ ≋ –24
25	0	2.6	.	–	● 11¹⁵. 22²⁰ ▽ ● 8¹⁵ 11³⁰ ▥ 0⁰⁰ 8¹⁵ = 0⁰⁰ 4⁰⁰ 5³⁰ 8¹⁵ = ² –9⁴⁰ = – 10¹⁵ = ² –22²⁰ = –23¹⁰. ∩ ⁰ 9²⁰ 12¹⁵. ≋ 0⁰⁰ 23²⁰ ≫ –24. ⊖ 0³⁰ 4²⁰
26	8	0.2	.	–	● 12⁰ 5⁴⁰ 7⁴⁰ 8³⁵ 15³⁰ 18³⁰ = ² 20⁵⁰ = 6¹⁰ 7⁴⁰ = ² –8¹⁵ = –8⁴⁵ 10¹⁰⁻⁵⁰ = 11²⁰ 15¹⁰ = ² –18³⁰ = – 19²⁰ = ² 23¹⁵ 24 ▥ 6¹⁰ 16¹⁰. 19²⁰ 23¹⁵. ≫ 0⁰⁰ 2²⁵ ≋ –24
27	8	.	.	–	● 1³⁰ 5²⁰. 19²⁰ 24. = ² 0⁰⁰ 5²⁰ ▥ – 19²⁰ = 18³⁰ 19²⁰ = ² –24. ≋ 0⁰⁰ 5⁴⁰ ≫ –5⁵⁰. 18³⁰ 24
28	8	4.3	.	–	● 0⁰⁰ ¹⁴⁰ 15²⁵ 18⁰⁰ 19¹⁵ 24. ▥ – 13⁴⁰ = 6⁴⁰ 7¹⁵. 13³⁰ 15²⁶ = ² – 18⁰⁰ = –18⁰⁴ = ¹ 19¹⁵ 24. ≫ 0⁰⁰ – 1⁴⁰. ○ a . p . ⊕ 12⁴⁵ 13¹⁵
29	0	5.8	.	–	● 0⁰⁰ 4¹⁰ ● 4¹⁰ 9³⁵ ● ⁰ 11⁰⁵ ● ⁰ 12³⁰ 13¹⁰ ● –14³⁰. = ² 0⁰⁰ 14³⁰ ▥ – 15⁰⁵ = –15⁴⁰ ▥ –24. ⌴ ⁰ 19⁰⁰ 23⁰⁰ ⌴ ¹⁻² 24. ⊖ 23³⁰ 24
30	8	.	.	–	= ² 14²⁰ 15⁴⁰ = = –17²⁰ = ² 18³⁰ 19²⁰ ▥ 0⁰⁰ 14³⁰ 15⁴⁰ 18³⁰. ⌴ ¹⁻² 0⁰⁰ 11⁰⁰. ⊖ 0⁰⁰ 4⁰⁰. ○ na–p
31	8	0.1	.	–	● ² 13²⁰ 14³⁰. = = ² 2⁰⁰ 6¹⁰. 7²⁰ 10¹⁰ 11⁴⁰ 20¹⁵. ⌴ 2²⁰ 9³⁰ ▥ 5¹⁵ 8¹⁰. 10¹⁰ 13²⁰ ∨ 14³⁰ 17¹⁵. ≫ 6²⁰ 12³⁰ ≋ –17²⁰ ≫ 19³⁰. 20¹⁰ 24. ○ a . p
Σ	–	70.6	–	–	UWAGI.

Śnieżka — φ = 50°44' — λ = 15°44' — Listopad – Novembre 1961

dni	CIŚNIENIE P = 800 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	39.5	39.5	40.9	39.9	-0.7	2.6	-0.6	0.2	3.6	-1.5	95	100	97	97	0.3	0.0	0.2	0.2	8 ⊙	10 • =	10	W 16	W 20	WNW18
2	42.1	40.1	34.8	39.0	1.6	2.0	1.4	1.6	4.6	-1.9	72	72	100	81	2.0	2.0	0.0	1.3	3 ⊙	4 ⊙	10 • =	WNW 5	W 6	SW 14
3	28.2	25.6	25.7	26.5	-1.8	-0.6	-2.0	-1.6	1.5	-2.5	98	99	98	98	0.1	0.0	0.1	0.1	10 =	10 =	10 * =	WSW18	SW 22	SW 20
4	26.1	27.2	28.5	27.3	-6.0	-6.4	-6.6	-6.4	-1.9	-6.9	94	94	94	94	0.2	0.2	0.2	0.2	9	10 =	10 =	SW 12	SW 6	WNW 8
5	28.1	28.2	32.3	29.5	-6.8	-7.0	-5.7	-6.3	-5.4	-7.4	94	91	92	92	0.2	0.3	0.3	0.3	10 =	10 * =	10 * =	WNW14	NNW18	N 16
6	31.3	30.8	29.6	30.6	-4.8	-0.8	1.8	-0.5	2.1	-5.9	95	99	100	98	0.2	0.0	0.0	0.1	10 =	10 * =	10 • =	N 11	N 14	NE 18
7	27.0	26.1	24.9	26.0	3.2	2.3	-1.6	0.6	4.3	-1.8	100	100	98	99	0.0	0.0	0.1	0.0	10 • =	10 • =	10 =	E 6	SSW 7	SSW12
8	26.6	26.4	26.1	26.4	-1.9	-4.2	-4.0	-3.5	-0.9	-4.9	94	91	96	94	0.3	0.4	0.2	0.3	9	9	10 =	WNW 6	SSW 9	SSW 8
9	24.0	23.4	23.5	23.6	-1.4	-1.6	-1.0	-1.2	0.4	-4.7	99	98	99	99	0.1	0.1	0.1	0.1	10 =	10 * =	9	SSW12	SW 14	S 15
10	23.1	24.7	25.6	24.5	2.9	-1.4	-2.7	-1.0	3.1	-3.0	95	99	97	97	0.4	0.1	0.1	0.2	10	10 * =	10 *	W 7	NW 4	N 4
11	24.0	23.9	23.3	24.4	-2.3	-1.5	-1.3	-1.6	-1.3	-2.7	98	99	99	99	0.1	0.1	0.1	0.1	10 =	10 =	10 =	E 4	S 5	S 9
12	25.8	27.1	27.6	26.8	-0.6	0.4	0.6	0.2	1.0	-1.3	99	98	100	99	0.0	0.1	0.0	0.0	10 =	9	10 =	S 10	S 13	SSW17
13	26.4	24.9	25.6	25.6	0.6	1.2	1.2	1.0	1.6	0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 • =	10 =	SSE18	SSE12	S 8
14	27.6	30.5	32.1	30.1	1.1	1.1	-2.4	-0.6	2.0	-2.6	100	100	98	99	0.0	0.0	0.1	0.0	10 =	9	10 =	WNW 8	NNW 1	N 8
15	32.9	34.1	35.1	34.0	-4.9	-1.5	-0.6	-1.9	-0.1	-5.2	90	90	39	73	0.4	0.6	3.6	1.5	1	3	3	N 2	ENE 2	NE 8
16	35.2	33.9	32.7	33.9	1.0	2.8	0.2	1.0	3.3	-1.3	23	38	22	28	5.1	4.7	4.8	4.9	8	1 ⊙	3	NNW 6	W 1	NW 3
17	30.3	30.3	30.6	30.4	-3.1	-3.1	-3.6	-3.4	0.3	-4.3	97	97	97	97	0.1	0.1	0.2	0.1	10 =	10 =	10 =	N 10	N 10	NNW12
18	28.6	28.6	30.4	29.2	-6.4	-5.0	-4.6	-5.2	-3.6	-7.2	94	95	96	95	0.2	0.2	0.2	0.2	10 =	10 =	10 =	N 15	NNW13	NNW13
19	32.3	34.4	39.1	35.3	-7.2	-7.1	-7.2	-7.2	-4.4	-7.9	93	91	93	92	0.2	0.3	0.2	0.2	10 =	10 △ =	10 △ =	NNW12	NNW14	NNW12
20	41.6	45.6	47.8	45.0	-9.8	-7.3	-6.6	-7.6	-6.4	-10.1	91	95	39	74	0.3	0.2	2.3	0.9	10	10	1	N 17	N 10	N 6
21	46.8	46.2	45.6	46.2	-0.3	1.4	1.6	1.1	1.6	-6.7	25	29	48	33	4.6	4.9	3.6	4.4	3	1 ⊙	4	SE 6	SSW 3	N 3
22	43.0	41.9	39.4	41.4	4.2	4.6	5.3	4.8	6.1	0.3	34	36	26	32	5.4	5.4	6.6	5.8	7	4 ⊙	1	N 2	S 2	S 3
23	35.3	34.8	34.3	34.9	6.7	7.7	3.8	5.5	8.4	3.2	14	9	75	33	8.3	9.6	1.9	6.7	0	1 ⊙	1	S 3	S 3	NW 10
24	35.9	36.6	36.0	36.2	4.3	3.3	2.0	3.0	5.1	1.3	69	68	86	74	2.6	2.4	1.0	2.0	8	9	10	NW 12	SW 6	SSW14
25	34.7	34.3	33.3	34.1	0.8	0.9	0.1	0.3	2.2	-1.7	92	69	65	75	0.3	2.0	2.2	1.6	9	8	9	WNW 6	W 2	SW 5
26	30.6	28.8	25.3	28.3	0.3	1.2	0.2	0.3	2.0	-0.6	62	63	87	71	2.4	2.6	0.9	2.0	9	6 ⊙	4	WSW 3	SW 4	S 6
27	23.8	23.2	23.4	23.5	3.8	6.2	1.0	3.5	-0.2	0.0	52	49	90	64	4.4	4.8	0.7	3.3	6	9 •	8	C 0	WSW 8	W 20
28	26.7	29.2	30.7	28.9	-2.3	-1.1	-2.0	-1.8	1.0	-2.3	96	89	98	94	0.3	0.7	0.1	0.4	8	4 ⊙	10 * =	W 17	WNW 6	W 10
29	31.3	31.9	31.7	31.7	-3.2	-2.4	-4.4	-3.6	-1.7	-4.4	97	98	96	97	0.1	0.1	0.2	0.1	10 =	10 =	10 =	SW 6	SW 8	SW 8
30	27.3	27.1	21.3	25.3	-4.6	-3.6	-4.4	-4.2	-3.6	-4.7	96	97	96	96	0.2	0.2	0.2	0.2	9	10 =	10 * =	SW 22	SW 25	SW 40
31																								
M	31.2	31.3	31.3	31.3	-1.2	-0.6	-1.4	-1.2	0.6	-3.3	82	82	84	83	1.3	1.4	1.0	1.2	8.2	7.9	8.1	9.3	9.1	11.7

Grudzień – Décembre

1	19.3	19.3	21.6	20.2	-1.0	0.2	1.3	0.4	1.4	-4.3	99	100	100	100	0.1	0.0	0.0	0.0	10 =	10 =	10 • =	SW 30	SW 30	SW 24
2	16.3	17.2	21.0	18.2	1.3	2.0	-3.4	-1.9	2.0	-5.7	100	100	93	98	0.0	0.0	0.2	0.1	10 • =	10 =	8	SW 30	SW 30	WNW25
3	26.8	26.6	23.3	25.6	-7.8	-6.6	-4.7	-6.0	-4.3	-8.3	90	94	96	93	0.3	0.2	0.2	0.2	4	9	10 =	SW 8	SW 14	SW 22
4	24.3	29.1	30.3	27.9	0.4	2.1	3.0	2.1	3.0	-4.7	100	100	100	100	0.0	0.0	0.0	0.0	10 * =	10 • =	10 • =	SW 18	SW 14	SW 17
5	30.4	28.9	26.7	28.7	4.9	4.4	3.0	3.8	5.2	3.0	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	10 =	SW 20	SW 25	SW 30
6	28.3	29.1	29.3	29.0	-6.2	-9.2	-8.6	-8.2	3.0	-9.4	92	92	92	92	0.3	0.3	0.3	0.3	10 =	10	10 =	W 8	WNW 8	NW 12
7	28.8	29.3	31.9	30.0	-8.2	-8.4	-10.3	-9.4	-7.7	-10.3	92	92	84	89	0.2	0.3	0.4	0.3	10 * =	10 * =	4	W 8	W 6	W 3
8	31.7	32.7	33.9	32.8	-10.3	-8.3	-9.9	-9.6	-6.0	-11.6	91	83	88	87	0.3	0.3	0.4	0.4	10 =	10 =	0	NW 6	NW 6	NW 3
9	32.3	31.0	29.3	31.0	-8.2	-6.2	-4.4	-5.8	-3.6	-10.6	60	40	96	65	1.3	2.3	0.2	1.3	6	8 ⊙	10 =	SW 12	SW 12	SW 12
10	29.1	29.7	28.3	29.1	-2.6	-1.4	-2.6	-2.3	-0.9	-3.9	98	99	98	98	0.1	0.1	0.1	0.1	10 =	8	10 =	SW 10	WSW 6	WSW10
11	21.9	17.8	19.3	19.7	-1.6	-0.6	0.0	-0.6	0.3	-2.6	98	99	100	99	0.1	0.0	0.0	0.0	10 =	10 =	10 =	WSW17	W 18	W 18
12	24.0	26.3	28.3	26.3	-0.2	0.0	-0.8	-0.4	0.2	-1.0	100	100	99	100	0.0	0.0	0.0	0.0	10 =	10 =	10 * =	WNW15	NW 10	NW 14
13	34.0	37.3	37.2	36.2	-6.2	-8.1	-9.0	-8.1	-0.8	-11.1	100	69	34	68	0.0	1.0	2.0	1.0	10 * =	1	1	NW 10	NW 3	NW 9
14	36.8	37.2	38.3	37.4	-11.0	-12.0	-17.8	-14.6	-5.9	-18.9	23	21	95	46	2.0	1.9	0.1	1.3	5	2 ⊙	10 =	ESE 8	NE 6	N 14
15	34.9	33.3	33.3	33.8	-15.0	-13.4	-13.0	-13.6	-12.0	-18.1	96	88	88	91	0.1	0.3	0.3	0.2	10 * =	10 * =	10 * =	NW 25	WNW25	NW 25
16	34.0	36.3	43.7	38.1	-23.6	-23.7	-19.4	-21.5	-12.6	-24.9	80	88	89	86	0.2	0.1	0.1	0.1	8	9	8	NW 10	N 10	SE 10
17	45.9	45.9	45.3	45.8	-18.6	-15.7	-14.8	-16.0	-14.4	-19.9	84	68	61	71	0.2	0.6	0.8	0.5	0	0 ⊙	0	SE 10	NNE14	N 17
18	45.7	45.6	45.3	45.5	-13.4	-14.6	-12.7	-13.4	-10.4	-15.4	84	91	92	89	0.4	0.2	0.2	0.3	10 =	9	0	N 13	N 10	N 12
19	44.4	43.9	43.2	43.8	-10.0	-9.6	-8.2	-9.0	-6.7	-12.7	33	91	92	72	1.9	0.3	0.2	0.8	0	10 =	10 =	N 12	NNW10	N 12
20	40.0	33.9	30.4	33.4	-7.2	-3.9	-6.3	-6.0	-2.7	-9.9	93	94	91	93	0.2	0.3	0.3	0.3	7	9	10 =	NW 10	NW 14	NW 18
21	28.3	29.1	29.9	29.1	-7.2	-10.4	-11.6	-10.2	-3.1	-11.7	90	90	89	90	0.3	0.3	0.3	0.3	10 =	10	10 =	NW 17	NNW16	NNW16
22	24.8	21.4	22.0	22.7	-9.8	-7.8	-13.0	-10.9	-6.9	-13.1	91	90	88	90	0.3	0.3	0.3	0.3	10 =	10 * =	10 * =	NW 18	NNW17	N 8
23	24.8	26.0	27.0	25.9	-15.8	-15.2	-14.8	-15.2	-12.3	-16.4	86	86	87	86	0.3	0.3	0.3	0.3	10 * =	10 =	10	NNW 6	N 6	N 12
24	26.8	26.4	25.3	26.2	-15.2	-14.6	-13.4	-14.2	-13.0	-15.7	33	74	29	33	0.8	0.3	1.3	0.9	0	0 ⊙	0	ESE 8	S 4	SE 6
25	25.7	23.3	23.6	23.6	-10.0	-8.8	-7.6	-8.5	-6.9	-14.0	17	30	22	23	2.4	2.2	2.7	2.4	0	0 ⊙	0	SSE 9	SSE 9	S 12
26	21.3	20.8	20.2	20.8	-8.0	-4.4	-8.1	-7.2	-3.0	-9.1	25	24	41	30	2.3	3.4	2.0	2.6	0	6 ⊙	3	S 16	SW 3	N 6
27	21.6	23.8	23.6	23.0	-9.2	-9.4	-9.0	-9.2	-7.4	-10.7	40	33	26	33	1.8	2.0	2.3	2.0	8	3	0	NE 14	NE 10	SE 12
28	22.3	21.8	22.2	22.2	-3.4	-3.7	-4.7	-3.1	-3.4	-9.8	98	93	96	96	0.1	0.2	0.2	0.2	10 =	10 =	10 =	S 2	WSW 8	SW 16
29	23.7	23.1	26.3	23.0	-3.6	-3.6	-2.4	-3.0	-1.3	-3.0	97	97	84	93	0.2	0.2	0.8	0.4	10 =	10 =	2	SW 13	SW 14	SW 8
30	23.1	26.7	27.2	26.3	-1.0	0.4	1.3	0.3	2.6	-2.8	89	67	47	68	0.7	2.1	3.6	2.1	4	6 ⊙	6	SW 16	SSW11	S 12
31	27.4	26.6	23.6	25.9	1.4	1.2	2.2	1.8	3.9	-0.1	89	77	68	78	0.8	1.6	2.3	1.6	8	7	7	WSW11	SW 14	SW 16
M	29.0	29.2	29.4	29.2	-7.4	-6.8	-7.2	-7.2	-4.1	-10.0	80	80	80	80	0.6	0.7	0.7	0.7	7.4	7.7	6.8	13.3	12.4	13.9

Śnieżka — $H_s = 1603$ m — $H_b = 1610{,}6$ m — Listopad – Novembre 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	1.3	.	–	
2	8	2.0	.	–	
3	0	6.0	.	–	
4	0	0.8	2	–	
5	0	16.5	2	–	
6	0	14.9	6	–	
7	0	3.0	pł.	–	
8	8	0.5	pł.	–	
9	0	0.8	pł.	–	
10	0	5.7	pł.	–	9.XI: ≫ 3^{40} 24
11	0	0.4	4	–	
12	7	1.1	4	–	
13	0	25.8	3	–	
14	6	.	2	–	
15	9	.	pł.	–	
16	9	0.2	pł.	–	
17	0	4.0	pł.	–	
18	0	3.3	pł.	–	
19	0	5.2	pł.	–	
20	8	.	pł.	–	
21	8	.	pł.	–	
22	9	.	pł.	–	
23	9	.	pł.	–	
24	8	0.2	pł.	–	
25	9	0.0	pł.	–	
26	9	.	pł.	–	
27	8	0.5	pł.	–	
28	8	3.1	pł.	–	
29	0	1.4	2	–	
30	0	5.2	2	–	
31					
Σ	–	101.9	–	–	UWAGI.

Grudzień – Décembre

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	8.8	4	–	
2	0	3.7	pł.	–	
3	8	3.1	pł.	–	2.XII: ☇ 16^{40} 17^{00}, 17^{30} 15^{45}
4	0	10.0	pł.	–	
5	0	0.8	pł.	–	
6	8	1.6	pł.	–	
7	0	2.9	1	–	
8	0	0.0	3	–	
9	9	0.3	3	–	
10	8	1.5	5	–	
11	0	5.5	4	–	
12	0	17.7	6	–	11.XII: ⁺/₋ 21^{00} 24
13	9	0.0	20	–	
14	9	3.2	10	–	
15	0	10.1	12	–	
16	8	.	25	–	
17	8	0.2	20	–	
18	8	0.6	20	–	
19	0	3.3	20	–	
20	8	2.8	22	–	
21	0	11.8	22	–	
22	0	6.5	28	–	
23	0	1.3	25	–	
24	9	.	30	–	
25	9	.	30	–	
26	9	.	25	–	
27	8	0.2	20	–	
28	0	0.1	18	–	
29	0	0.7	18	–	
30	9	.	17	–	
31	9	.	16	–	
Σ	–	96.7	–	–	UWAGI.

Sandomierz — φ = 50°41' — λ = 21°45' — Styczeń – Janvier 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N, w			KIERUNEK i PRĘDKOŚĆ WIATRU D, v
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I II III
1	92.5	95.9	95.4	95.9	−5.0	−1.6	−1.3	−2.3	−0.6	−5.4	98	98	99	98	0.1	0.1	0.1	0.1	9	10	10	C 0 SSW 1 SW 1
2	95.6	91.2	88.3	91.0	−2.1	−0.2	0.0	−0.6	0.4	−2.2	100	94	98	97	0.0	0.4	0.1	0.2	10	10 *	10	SSW 2 SE 1 SSE 1
3	85.4	79.8	79.4	80.9	−1.4	3.6	4.3	2.7	5.0	−2.3	99	80	79	86	0.1	1.6	1.8	1.2	8	9	3	SE 2 SSW 4 SSW 5
4	80.7	80.1	80.8	80.5	4.5	7.3	2.2	4.0	6.0	2.2	85	70	86	80	1.2	3.0	1.1	1.8	9	9	10	SSE 4 S 8 S 5
5	80.1	82.1	89.1	83.8	1.2	2.1	0.1	0.9	3.1	0.1	94	95	98	96	0.4	0.4	0.2	0.3	10	10 •	8	SE 3 WNW 2 SW 2
6	93.4	94.6	92.8	93.6	0.3	2.0	−0.8	0.2	3.6	−1.1	96	85	92	91	0.2	1.1	0.5	0.6	10	0 ⊙	0	SW 4 WSW 4 SSW 3
7	90.1	89.5	89.8	89.8	−2.2	4.0	0.6	0.8	4.8	−2.6	91	80	92	88	0.5	1.6	0.5	0.9	3	7 ⊙	3	SE 4 S 4 WSW 2
8	90.2	90.6	89.6	90.1	0.4	1.3	−0.2	0.5	2.2	−0.9	92	89	88	90	0.5	0.8	0.7	0.7	10	8	10	SW 5 SW 4 SSW 3
9	88.6	89.4	90.6	89.5	0.8	3.0	−1.3	0.5	3.4	−1.3	86	72	94	84	0.9	2.1	0.4	1.1	8	2 ⊙	0	SW 5 SW 4 SW 2
10	90.8	91.4	92.0	91.4	−2.8	−0.1	−1.6	−1.5	1.4	−3.5	95	90	96	94	0.3	0.7	0.2	0.4	2	10	10 =	SW 1 SSW 2 ESE 4
11	91.8	92.6	95.2	93.2	−3.1	1.4	−1.0	−0.9	3.1	−3.1	95	76	99	90	0.3	1.7	0.1	0.7	0	1 ⊙	9	E 1 S 3 SW 3
12	98.5	100.6	104.2	101.1	−1.2	−1.2	−2.3	−1.8	0.7	−2.6	91	72	83	82	0.5	1.6	0.9	1.0	10	2 ⊙	0	WNW 5 W 7 WNW 5
13	106.8	107.8	106.4	107.0	−2.7	−1.2	−3.3	−2.6	−0.7	−4.7	82	72	88	81	0.9	1.6	0.6	1.0	10	3 ⊙	10	WNW 8 WNW 3 SW 5
14	103.6	103.9	105.7	104.4	−1.4	−0.2	−0.3	−0.6	0.5	−3.3	90	88	100	93	0.5	0.7	0.0	0.4	10	10 •	10 *	SW 4 WSW 3 SW 3
15	108.6	108.9	106.6	108.0	0.1	−0.8	−3.6	−2.0	0.6	−3.6	94	92	97	94	0.4	0.5	0.2	0.4	10	10	10	NW 4 W 4 WSW 5
16	102.0	100.4	99.8	100.7	−4.4	−2.1	−0.8	−2.0	−0.8	−6.2	96	92	91	93	0.2	0.4	0.5	0.4	10	10 *	10	WSW 4 WSW 4 NW 4
17	103.8	105.4	111.1	106.8	−6.2	−8.0	−13.0	−10.0	−0.5	−13.1	75	78	76	76	1.0	0.7	0.5	0.7	9	0 ⊙	0	NNE 5 NNE 6 N 3
18	114.9	116.4	116.0	115.8	−16.0	−10.3	−13.5	−13.3	−9.4	−16.1	91	77	88	85	0.2	0.6	0.3	0.4	0	0 ⊙	0	NNW 4 NW 3 N 5
19	115.4	111.1	109.2	111.2	−10.4	−7.2	−6.3	−7.6	−5.9	−15.6	84	77	86	82	0.4	0.8	0.5	0.6	10	10 △	10	NW 3 NW 2 NNW 4
20	106.4	105.0	103.0	104.8	−6.6	−4.1	−5.5	−5.4	−3.5	−6.7	86	84	90	87	0.5	0.7	0.4	0.5	10	10	10	NNW 5 NW 3 NNW 2
21	100.7	99.9	98.7	99.8	−15.4	−10.5	−13.4	−13.2	−5.4	−16.4	91	80	84	85	0.2	0.5	0.4	0.4	0	0	0	ESE 3 ESE 1 SE 2
22	95.7	93.8	91.6	93.7	−15.2	−9.4	−7.6	−10.0	−6.0	−15.7	86	82	87	85	0.3	0.5	0.4	0.4	6	8	8	SE 2 S 2 SW 2
23	88.4	88.1	91.7	89.4	−6.4	−5.7	−14.2	−10.1	−5.0	−14.3	94	90	87	90	0.2	0.4	0.3	0.3	10	10	0	SW 4 N 3 N 2
24	92.0	91.4	89.9	91.1	−15.8	−10.6	−11.4	−12.3	−8.1	−17.2	86	80	86	84	0.3	0.5	0.4	0.4	2	8	10	WSW 2 SW 2 SSW 1
25	87.1	88.1	92.7	89.3	−8.8	−8.6	−15.0	−11.8	−7.8	−15.1	92	77	91	87	0.3	0.7	0.2	0.4	10	9 ⊙	0	N 2 NE 6 NNE 5
26	98.6	102.6	106.0	102.4	−19.7	−13.8	−15.0	−15.9	−12.4	−20.5	83	96	87	89	0.2	0.1	0.2	0.2	0	1 ⊙	0	N 2 NNW 2 N 3
27	109.7	110.4	109.3	109.8	−19.2	−10.5	−12.0	−13.4	−8.1	−20.3	83	70	60	71	0.2	0.8	1.0	0.7	0	0 ⊙	0	N 1 S 1 SSE 4
28	106.9	103.7	100.2	103.6	−19.1	−7.2	−9.0	−11.1	−2.7	−19.3	83	60	76	73	0.2	1.4	0.7	0.8	0	0 ⊙	1	SSE 2 SSW 1 SSW 3
29	97.0	98.0	98.7	97.9	−10.3	−1.6	−3.3	−4.6	0.1	−11.1	84	71	81	79	0.4	1.5	0.9	0.9	0	10	2	SSW 4 SW 7 SW 6
30	92.3	88.0	85.1	88.5	−6.1	1.4	0.2	−1.1	2.0	−7.0	89	63	71	74	0.4	2.5	1.8	1.6	2	8 ⊙	10	SSW 6 SSW 6 SSW 7
31	85.0	80.1	77.5	80.9	−0.4	0.8	1.1	0.6	1.7	−0.6	94	83	98	92	0.3	1.2	0.1	0.5	10 △	10 •	10 •	SW 5 SSW 3 SW 5
M	96.3	96.1	96.3	96.2	−6.3	−2.8	−4.7	−4.6	−1.2	−8.0	90	81	88	86	0.4	1.0	0.5	0.6	6.4	6.3	5.6	3.4 3.5 3.5

Luty – Février

1	81.1	77.6	73.9	77.5	1.6	3.0	2.4	2.4	3.4	0.3	89	81	95	88	0.8	1.5	0.4	0.9	10	9	10	WSW 4 SSW 3 SSW 5
2	75.2	74.1	71.6	73.6	0.8	2.6	0.2	1.0	4.2	−0.2	94	79	88	87	0.4	1.6	0.7	0.9	10	9	2	WSW 5 SW 3 WSW 2
3	70.4	69.9	75.2	71.8	−2.2	−0.3	−0.1	−0.7	0.8	−2.4	100	98	100	99	0.0	0.2	0.0	0.1	10 =	10	10 *	ESE 2 S 1 W 4
4	82.2	84.0	81.5	82.6	−1.0	0.7	−2.1	−1.1	1.0	−2.8	83	73	92	83	1.0	1.7	0.4	1.0	9	8 ⊙	0	WNW 4 W 4 W 3
5	83.0	87.3	94.6	88.3	−5.2	0.4	−1.2	−1.8	0.8	−5.4	95	71	78	81	0.2	1.9	1.2	1.1	2	5 ⊙	10	SSW 2 SE 1 NW 5
6	98.5	97.8	93.9	96.7	−2.8	1.0	−2.8	−1.8	2.0	−4.3	82	51	80	71	0.9	3.2	1.0	1.7	9	1 ⊙	0	WSW 1 SSW 4 SSE 3
7	87.7	87.2	87.3	87.4	−1.7	−0.1	−1.0	−1.0	0.6	−5.5	82	82	89	84	1.0	1.1	0.7	0.9	10	10 *	9	S 3 SW 5 SW 5
8	87.6	89.6	93.9	90.4	−2.2	2.1	1.1	0.5	3.7	−2.5	91	87	90	89	0.5	0.9	0.6	0.7	9	9	10	WSW 4 WNW 5 W 4
9	93.9	92.9	88.0	92.3	−0.8	2.8	−0.7	0.2	3.4	−1.0	95	76	97	89	0.3	1.9	0.2	0.8	10	9	10 *	WNW 3 SSW 3 S 3
10	88.1	92.2	100.7	93.7	0.3	1.6	−0.1	0.4	2.6	−1.3	96	96	96	96	0.2	0.3	0.3	0.3	10 • =	10 •	10	SSW 3 NW 3 NNW 3
11	99.3	95.0	89.2	94.5	−1.0	2.1	1.4	1.0	2.6	−1.2	92	95	85	90	0.5	0.4	1.1	0.7	3	9	10	WNW 1 S 4 SW 5
12	85.5	86.1	91.8	87.8	0.2	2.3	0.1	0.7	4.8	−0.1	98	95	98	97	0.1	0.4	0.2	0.2	10 =	10	10 =	SW 4 SW 2 SW 2
13	96.8	98.5	100.5	98.6	1.2	2.6	0.6	1.2	3.4	−0.3	100	89	98	96	0.0	0.8	0.1	0.3	10 =	9	10	WSW 4 WNW 2 NW 2
14	104.5	106.5	106.3	105.8	−0.2	2.2	−0.6	0.2	3.2	−0.8	86	64	88	79	0.8	2.6	0.7	1.4	9	7 ⊙	0	N 2 WSW 3 SW 1
15	105.2	106.5	106.3	106.1	−2.5	1.9	1.1	0.4	3.6	−2.9	95	85	87	89	0.3	1.0	0.9	0.7	1	9	0	SW 4 SW 5 SW 6
16	105.5	107.4	110.1	107.7	0.6	3.4	3.5	2.8	4.9	−0.1	94	95	98	95	0.4	0.5	0.1	0.3	9	10	10	SW 5 WSW 2 WNW 4
17	111.4	112.0	111.5	111.6	1.6	3.2	2.8	2.6	4.2	1.3	94	90	96	93	0.4	0.8	0.3	0.5	10	10 •	10	W 4 W 5 W 2
18	109.7	108.5	107.1	108.4	1.5	3.3	4.4	3.9	8.0	1.0	98	91	87	92	0.1	0.8	1.1	0.7	10 =	0	0	WSW 3 SW 4 W 3
19	104.7	105.5	105.9	105.4	−0.4	1.3	3.1	1.8	5.6	−0.6	96	94	95	95	0.2	0.4	0.4	0.3	0	10	10 =	SW 5 WSW 5 WNW 5
20	107.3	109.7	111.6	109.5	1.8	3.7	2.4	2.6	4.2	1.4	94	90	95	93	0.4	0.8	0.4	0.5	10 •	10	10 •	NW 3 WSW 2 WSW 2
21	112.5	112.2	111.6	112.1	1.8	5.2	1.5	2.5	6.2	1.3	89	75	91	85	0.8	2.2	0.6	1.2	10	6 ⊙	0	W 2 SW 2 C 0
22	111.7	112.0	111.4	111.7	0.4	6.1	1.8	2.5	6.7	−1.1	96	65	91	85	0.3	3.5	0.7	1.5	10	4	10	WNW 1 WNW 1 ESE 2
23	110.1	109.3	107.8	109.1	0.3	1.9	0.8	1.0	2.6	0.0	96	85	90	90	0.2	1.0	0.7	0.6	0	10	10	C 0 SSE 4 ESE 1
24	107.7	108.0	108.7	108.1	−0.2	0.7	−0.3	0.0	1.3	−0.5	88	86	82	85	0.7	0.9	1.1	0.9	10	10	10	ESE 1 C 0 SSW 1
25	110.1	111.2	112.1	111.1	−1.6	−0.4	−1.2	−1.1	0.9	−1.9	83	78	83	81	0.9	1.3	1.0	1.1	10	10	3	E 4 ESE 5 SE 4
26	111.9	112.6	112.6	112.4	−3.0	3.9	−1.1	−0.3	5.6	−3.2	88	59	85	77	0.6	3.3	0.8	1.6	0	0 ⊙	0	SE 4 S 4 SSW 3
27	111.1	108.8	104.7	108.2	−3.2	5.7	1.3	1.4	7.8	−3.7	95	54	83	77	0.2	4.3	1.1	1.9	0	2 ⊙	8	SSW 2 SSW 6 SSW 4
28	97.2	91.7	88.0	92.3	0.8	7.6	3.3	3.8	8.7	0.4	81	61	75	72	1.3	4.0	1.9	2.4	10	9	10 •	SW 4 SW 8 SW 8
29																						
30																						
31																						
M	98.3	98.4	98.5	98.4	−0.5	2.6	0.8	0.9	3.8	−1.3	92	80	90	87	0.5	1.5	0.7	0.9	7.9	7.7	6.9	3.0 3.4 3.4

DNI	WILGOTNOŚĆ WZGLĘDNA v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	1	–	≡0–1 10⁰⁰–4⁴⁵ = –24. V° 3⁵⁰–24
2	6	1.0	1	–	✳° 10²⁵–13¹⁵ 15⁴². = 0⁰⁰–24. V° 0⁰⁰–10⁰⁰
3	6	.	3	–	= 0⁰⁰–⁵⁰ ≡'–5³⁰ ≡°–6³⁰ = –13⁴⁵. ◡ 23³⁰–24
4	7	0.0	pł.	–	= 22³⁰–24. ◡ 0⁰⁰–⁴⁰
5	6	3.9	.	–	•° 2⁴⁸–3³⁷. 8⁴⁷–16⁴². = 0⁰⁰–17⁴⁵ ≡0–1 p = – np
6	6	.	pł.	–	✳1 6¹⁵–²⁰. = 0⁰⁰–24. ⌴° 21⁰⁰–24
7	7	.	pł.	–	= 0⁰⁰–9³⁰. 14⁵⁰–24. ⌴0–1 0⁰⁰–11⁰⁰
8	6	0.4	pł.	–	= 0⁰⁰–24. ⌴° na – 10⁰⁰
9	7	.	1	–	✳° 0⁴⁵ na – 3⁵⁴. = 0⁰⁰–9³⁰ 21¹⁰–24. ⌴° 22⁰⁰–24
10	6	.	1	–	= 0⁰⁰–20¹⁵ ≡0–1 –24. ⌴° 0⁰⁰–11⁰⁰. ◡ 4¹⁵–5⁴⁰
11	6	1.0	1	–	≡1–0 0⁰⁰–2⁵⁰ = –24
12	7	0.0	2	–	✳° 1⁴³–5⁵⁰ ✳▽ 9⁰¹–⁰⁵. 9²¹–²⁵ 14³⁵–15⁰⁵. 15¹⁰–³⁷. = 0⁰⁰–9³⁰
13	7	0.8	2	–	= 20¹⁵–24
14	6	6.0	2	–	△ 4¹⁰–5²⁰ ◉° 6³⁰ ◉° ◉° 11¹⁵–14⁰² △–14⁰⁷ ✳0–1 –24. = 0⁰⁰–24. ∞ 4⁴⁵–14⁰⁷
15	6	.	7	–	✳° 0⁰⁰–2⁵⁰. = 0⁰⁰–24
16	6	0.4	7	–	✳° 12³⁰ 13⁰⁰. 13³⁰ 14⁴⁰–15³⁰. = 0⁰⁰–23³⁰
17	7	0.0	7	–	✳▽° 16⁴⁸–17⁰⁸
18	7	.	7	–	
19	6	0.0	7	–	△ 10⁵⁰–14⁵⁵. = 8³⁰–24
20	6	0.0	7	–	△ 8¹⁵–10¹⁰ ✳–11²⁰ △ 13⁴⁵–16¹⁵ ✳ 16³⁰–17¹⁰. = 0⁰⁰–24
21	6	.	7	–	= 0⁰⁰–24
22	6	.	7	–	= 0⁰⁰–24. ⊕ 11²⁵–12⁰⁰
23	6	.	6	–	= 0⁰⁰–24
24	6	0.0	7	–	✳ 8³⁰ 10²⁵. = 17¹⁵–24
25	7	0.0	6	–	✳° 8⁵⁰–9⁰⁸. = 0⁰⁰–11³⁰. 21³⁰–24
26	6	.	6	–	= 0⁰⁰–24
27	6	.	6	–	= 0⁰⁰–14¹⁵. 16³⁰–19³⁰
28	7	.	6	–	= 1⁵⁰–12²⁰
29	7	.	6	–	= 18³⁰–24
30	7	0.5	6	–	△ 17¹⁰–⁴⁵. = 0⁰⁰–9³⁰ 17²⁰–24
31	6	3.3	5	–	△ 4⁴⁵–6³⁵ ◉ 6⁴⁰–7³⁰ •° 12²⁵ 22⁴⁰. = 0⁰⁰–24. ∞ 6⁴⁰–12¹⁵
Σ	–	17.3	–	–	UWAGI.

Luty – Février

1	6	4.1	2	–	•° 15⁵⁰ 16⁰⁵. ✳–16²⁰ •°–19⁵⁵. = 0⁰⁰–24
2	6	.	pł.	–	= 0⁰⁰–24. ⊕ 8⁴⁵–10⁵⁵
3	6	2.2	pł.	–	△ 14⁴⁸–15²⁰ ✳0–1 20³⁵. = 0⁰⁰–2⁴⁰ ≡2–0 –8⁵⁰ = –24. ⌴° 1⁰⁰–12⁰⁰
4	7	.	3	–	= 0⁰⁰–9¹⁵ 19³⁰–24
5	7	.	2	–	= 0⁰⁰–11³⁰ 18¹⁵–24
6	7	.	2	–	= 0⁰⁰–3³⁰
7	6	0.0	1	–	✳° 12³⁰–14⁵³. = 2¹⁵–24. ◡ 2³⁰–3²⁰
8	6	0.2	pł.	–	✳▽0–1 8¹⁵–³⁴. = 0⁰⁰–24
9	7	4.6	pł.	–	△ 19⁵⁰–20²⁵ ✳0–1 –24 = 0⁰⁰–11¹⁵. 16³⁰–24
10	6	1.9	3	–	✳0–1 0⁰⁰–2⁴⁸ •°–10¹⁵ 12⁵⁰ • 14⁴⁸ 15⁵⁰ ✳° 16⁵⁰ 18³⁵ •° 20¹⁵. = 0⁰⁰–6²⁰ ≡0–1 8⁵⁰ = –24
11	6	3.1	1	–	= 0⁰⁰–24
12	6	.	1	–	•° 0⁵⁰–3⁵⁰ ✳° 5³⁰ = 0⁰⁰–5⁴⁵ ≡0–1 8⁵⁰ = –16⁴⁵ ≡0–1 –24
13	6	2.1	pł.	–	•° 10⁴⁵ 11¹⁰ 15⁵⁰ 16¹⁵ ••–17³⁰ ✳•–18¹⁰ ✳°–19³⁰ ✳° 19⁴⁰ 20¹⁰. ≡0–2 0⁰⁰–8⁴⁰ = –13³⁰. 15¹⁵–24
14	7	.	pł.	–	= 0⁰⁰–5³⁰
15	6	.	.	–	= 5¹⁰–24. ⌴° 2⁰⁰–9⁰⁰
16	5	.	.	–	= 0⁰⁰–24
17	6	0.2	.	–	•° 10⁵⁰ 13⁴⁰. 20¹⁵ 22⁴⁵. = 0⁰⁰–24
18	6	.	.	–	= 0⁰⁰–⁴⁰ ≡0–1 11⁵⁰ = –23⁴⁵ ≡2–24
19	5	0.5	.	–	•° 17⁴⁵–24. ≡2–0 0⁰⁰–2⁵⁰ = –18¹⁵ ≡0–1 20⁴⁵ = –24. ⌴° 2⁰⁰–9⁰⁰
20	6	0.0	.	–	•° 0⁰⁰–⁵⁰ 1⁵⁵ 7⁰⁵ 15⁵⁰ 16³⁰–18²⁵. 19⁴⁵ 24. = 0⁰⁰–24
21	7	0.0	.	–	•° 0⁰⁰ 2⁵⁰ 7⁴² 8⁰⁵. = 0⁰⁰–10³⁰. 17⁴⁵–24. ⌴° 23⁰⁰–24
22	6	0.0	.	–	•° 22⁵⁰–24. = 0⁰⁰–24. ⌴° 0⁰⁰–2⁰⁰ ⌴° 3⁰⁰–8⁰⁰
23	6	.	.	–	•° 0⁰⁰ 5⁴⁵. = 0⁰⁰–24
24	6	.	.	–	= 0⁰⁰–24
25	7	.	.	–	= 0⁰⁰–11¹⁵. 19¹⁰–24. ⌴° 23⁰⁰–24
26	7	.	.	–	= 0⁰⁰–11³⁰. 20¹⁵–24. ⌴° 0⁰⁰–9⁰⁰ 22⁵⁰–24
27	7	.	.	–	= 0⁰⁰–10¹⁵. 17³⁰–24. ⌴0–1 0⁰⁰–6⁰⁰
28	7	0.1	.	–	•° 18²⁰–²⁵. 20³⁰–21³⁵. 23⁴⁵–24. = 0⁰⁰–7⁵⁰. ⩥ a. ◡ 1⁵⁰–5¹⁰
29					
30					
31					
Σ	–	19.0	–	–	UWAGI.

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — Marzec – Mars 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.8	95.4	98.3	94.5	2.0	6.5	2.4	3.5	7.0	1.8	89	66	91	82	0.8	3.2	0.7	1.6	10		9	SW 5	W 7	WNW 5
2	102.1	102.6	102.7	102.5	1.2	5.1	2.2	2.7	6.0	0.9	92	70	75	79	0.5	2.6	1.8	1.6	10	10	9	W 5	WSW 5	WNW 6
3	103.4	105.7	107.6	105.6	0.5	5.2	2.7	2.7	6.8	0.1	90	65	74	76	0.6	3.2	1.9	1.9	9	9	10	WSW 1	SW 1	SW 1
4	109.2	110.7	111.5	110.4	1.6	5.6	4.5	3.6	6.2	1.4	93	98	87	93	0.6	0.1	1.1	0.6	10	10 =	8	C 0	WSW 1	NW 5
5	107.5	107.4	109.2	108.0	2.0	5.9	2.7	3.5	6.3	1.4	93	82	86	87	0.6	1.7	1.0	1.1	10	10	5	SW 7	WNW 8	WNW 5
6	109.4	109.1	107.8	108.8	0.5	6.5	3.0	3.2	8.3	−0.1	96	72	91	86	0.2	2.7	0.7	1.2	0	9	0	WSW 5	WNW 5	NW 5
7	104.8	102.7	102.8	103.4	1.7	8.9	7.1	6.2	11.9	1.4	98	75	78	84	0.1	2.9	2.2	1.7	10	9 ⊙	0	SW 6	W 7	NW 5
8	107.1	108.2	106.1	107.1	2.1	10.8	6.1	6.5	12.5	1.7	84	52	80	72	1.2	6.5	1.8	3.1	5 ⊙	0 ⊙	0	WNW 5	W 6	WNW 4
9	105.6	104.0	103.0	104.2	5.6	12.5	8.9	9.0	13.9	4.6	89	57	75	74	1.0	6.5	2.9	3.4	10	2 ⊙	0	W 4	WNW 4	WNW 5
10	102.7	102.0	99.1	101.3	4.8	13.8	11.1	10.2	17.6	3.9	87	63	65	72	1.1	5.9	4.6	5.9	9 ⊙	9 ⊙	0	WNW 5	WSW 4	WSW 2
11	96.7	97.6	98.8	97.7	3.2	14.4	8.5	8.6	14.7	3.0	84	51	76	70	1.2	8.1	2.7	4.0	1 ⊙	4 ⊙	10	WSW 2	W 7	NW 5
12	97.5	94.7	86.9	93.0	7.3	9.5	10.2	9.3	10.8	7.1	86	65	67	73	1.5	4.2	4.0	3.2	10	10	10	WSW 6	W 8	SW 9
13	78.7	82.2	87.0	82.6	7.1	7.5	2.4	4.8	12.5	2.2	67	53	79	66	3.5	4.9	1.6	3.3	2 ⊙	9	0	W 10	WNW 14	NW 6
14	89.7	89.6	89.6	89.6	1.2	7.8	4.9	4.7	8.5	0.6	79	43	92	71	1.4	6.0	0.7	2.7	8 ⊙	6 ⊙	10	WNW 5	WNW 6	W 5
15	87.8	90.1	94.9	90.9	7.6	10.7	7.1	8.1	13.4	4.7	90	61	73	75	1.0	5.1	2.8	3.0	10	8 ⊙	0	W 9	NW 10	WSW 5
16	94.2	91.1	95.5	92.9	6.8	9.7	7.2	7.7	11.7	5.2	94	69	69	77	0.6	3.7	3.2	2.5	10 •	10	0	WSW 5	W 9	NW 9
17	99.4	97.7	94.2	97.1	3.7	12.2	6.8	7.4	14.0	3.1	90	56	72	73	0.8	6.2	2.7	3.2	3 ⊙	6 ⊙	2	NW 4	WNW 7	WSW 4
18	86.0	81.1	79.5	82.2	3.9	18.8	11.1	11.2	19.4	3.0	78	35	84	65	1.8	14.4	2.1	6.1	6 ⊙	4 ⊙	9 •	SW 5	SW 7	WSW 5
19	79.8	80.3	82.1	80.7	5.4	6.7	1.2	3.6	11.3	1.0	87	54	94	78	1.2	4.5	0.4	2.0	10	10	10 ⁂	WSW 3	W 6	NW 4
20	86.9	87.0	82.9	85.6	−1.7	1.4	−1.4	−0.8	3.0	−1.9	84	60	70	71	0.9	2.8	1.7	1.8	7 ⊙	8 ⊙	3	NW 4	WNW 5	SW 3
21	73.4	72.2	74.1	73.2	1.2	2.5	2.1	2.0	6.2	−1.8	75	93	87	85	1.7	0.5	0.9	1.0	10	10	10	SSW 9	SW 9	WSW 7
22	81.8	86.5	90.8	86.4	0.4	1.9	−1.1	0.0	3.6	−1.3	90	76	81	82	0.6	1.7	1.1	1.1	10	7 *	5	NW 6	NW 6	WNW 3
23	88.2	89.1	90.5	89.3	−1.4	3.1	4.3	2.6	5.0	−3.4	88	91	92	90	0.6	0.6	0.7	0.6	10 *	10	10 •	SW 4	W 3	WNW 6
24	91.6	91.5	92.2	91.8	3.5	8.3	6.1	6.5	9.0	4.1	86	69	79	78	1.2	3.5	2.0	2.2	10	9	0	WSW 8	W 12	W 6
25	93.6	94.3	96.2	94.7	5.4	7.5	4.8	5.6	8.2	4.7	87	79	89	85	1.2	2.2	1.0	1.5	9	9	4	W 4	W 9	W 4
26	96.4	95.7	86.9	92.3	3.2	10.6	5.9	6.4	11.4	2.1	98	51	71	73	0.2	6.2	2.7	3.0	9	9	8	WSW 5	WSW 7	SW 6
27	81.8	83.3	82.7	82.6	6.5	8.0	2.8	5.0	8.9	1.7	89	42	59	63	1.0	6.2	3.1	3.4	10 •	6 ⊙	1	WSW 6	W 10	WSW 8
28	84.5	84.9	84.4	84.6	0.0	3.7	0.7	1.5	4.3	−0.9	69	59	81	70	1.9	3.3	1.2	2.1	7 ⊙	6 ⊙	10	W 9	W 7	WSW 5
29	88.3	87.4	85.8	87.2	−1.9	3.4	2.9	1.8	4.0	−2.2	87	78	95	87	0.7	1.7	0.4	0.9	2 ⊙	10	10 •	WSW 4	WSW 7	WSW 8
30	84.0	83.4	81.6	83.0	4.6	7.5	6.7	6.4	8.1	2.8	81	72	82	78	1.7	3.0	1.7	2.1	9	10	10	WSW 7	WSW 10	SW 5
31	78.1	84.3	84.3	82.2	8.1	5.6	3.4	5.1	8.3	3.2	86	61	91	79	1.3	3.6	0.7	1.9	10	10	9	WSW 8	SW 4	SW 2
M	93.0	93.2	93.1	93.1	3.1	7.7	4.8	5.1	9.4	1.7	87	65	80	77	1.1	4.1	1.8	2.3	7.9	7.9	5.3	5.1	7.1	4.8

Kwiecień – Avril

1	87.5	86.5	80.5	84.8	0.8	5.9	10.1	6.7	10.6	0.3	62	50	68	60	2.5	4.7	4.0	3.7	0 ⊙	10	10 •	W 7	WSW 5	WSW 2
2	85.4	87.3	86.7	86.5	3.7	8.3	5.1	5.6	10.2	3.2	82	44	89	72	1.5	6.2	1.0	2.9	10	7 ⊙	10 •	WSW 6	WNW 6	W 1
3	80.3	81.4	85.8	82.5	7.4	11.8	6.9	8.2	13.3	4.3	91	76	81	83	0.9	3.3	1.8	2.0	10 •	8 ⊙	2	SW 4	WSW 6	NW 5
4	84.0	85.1	91.5	86.9	5.6	13.2	5.9	7.2	13.3	2.6	97	65	77	80	0.5	5.3	2.1	2.6	10	10	0	SSW 1	WSW 9	C 0
5	92.7	90.6	89.4	90.9	4.7	14.9	13.4	11.6	20.1	4.5	90	70	70	77	0.8	5.0	4.7	3.5	10 •	0 ⊙	0	E 2	SSE 3	SSW 5
6	90.3	91.1	90.9	90.8	9.1	21.4	16.1	15.7	23.2	8.6	81	40	59	60	2.2	15.2	7.5	8.3	7 ⊙	4 ⊙	0	SW 3	SW 5	SW 3
7	90.5	89.2	88.7	89.5	10.4	23.2	18.0	17.4	24.2	8.7	77	34	54	55	2.9	18.6	9.4	10.3	0	1 ⊙	0	C 0	SW 5	SW 2
8	88.0	86.4	86.6	87.0	10.6	18.6	9.7	12.2	19.5	9.5	90	61	86	79	1.3	8.3	1.7	3.8	10	9	10	SW 2	W 3	NNW 7
9	92.8	94.5	97.1	94.8	3.8	6.7	2.8	4.0	9.9	2.6	73	46	65	61	2.1	5.3	2.6	3.3	2 ⊙	7 ⊙	0	W 7	NW 9	NW 1
10	97.7	94.6	90.8	94.4	0.8	7.7	5.9	4.1	8.8	−1.1	69	30	56	52	2.0	7.3	3.6	4.3	8	10 ⊙	0	NW 1	ENE 4	ENE 2
11	87.0	86.0	88.3	87.1	3.5	13.4	7.7	8.1	14.8	3.1	58	44	65	55	3.2	8.7	3.9	5.3	9	2 ⊙	0	E 3	E 1	ENE 4
12	93.1	93.0	93.8	94.6	2.3	10.3	6.3	6.4	12.4	1.3	77	37	59	58	1.7	7.9	4.0	4.5	5	6	0	NW 4	NNW 3	NE 1
13	93.1	91.3	91.1	91.8	3.4	17.4	12.0	11.2	20.3	2.1	76	41	72	63	1.9	11.7	4.0	5.9	10	1 ⊙	0	SE 2	SW 5	C 0
14	91.3	90.9	89.1	90.4	9.3	21.0	15.3	15.2	22.6	7.3	72	40	50	54	3.2	14.9	8.7	8.9	1 ⊙	0 ⊙	0	SW 4	SW 5	SW 1
15	89.8	89.3	88.9	89.3	11.2	23.4	17.3	17.3	25.1	7.9	62	22	50	45	5.1	22.4	9.9	12.5	0 •	1 ⊙	0	SSW 1	WSW 5	SW 2
16	88.9	87.8	87.8	88.2	12.4	20.4	12.9	14.6	20.6	10.8	74	42	70	62	3.7	13.8	4.4	7.3	9	9	10	SW 1	SW 2	SE 1
17	88.3	88.8	89.9	89.0	9.3	15.6	12.8	12.6	16.8	8.2	93	69	79	80	0.8	5.5	3.1	3.1	3	8	10	WSW 2	W 4	W 3
18	90.7	89.6	88.3	89.5	10.2	18.4	14.8	14.6	20.1	8.1	96	59	77	77	0.4	8.7	3.8	4.3	2 ⊙	6 ⊙	10	C 0	WSW 1	NE 1
19	89.8	91.3	91.5	90.9	10.3	17.0	11.4	12.5	17.8	9.2	88	53	70	70	1.4	9.2	4.1	4.9	8	7 ⊙	3	NNW 1	E 3	NNW 3
20	93.7	93.8	97.7	95.7	5.6	11.2	6.7	7.6	13.0	4.8	74	49	55	59	2.4	6.8	4.4	4.5	8	8 ⊙	2	E 6	ENE 5	NE 4
21	99.1	98.2	96.4	97.9	5.0	12.8	7.1	8.0	14.0	1.7	67	32	48	49	2.8	10.1	5.2	6.0	0 ⊙	0 ⊙	0	NE 5	ESE 6	E 2
22	94.2	91.6	88.8	91.5	5.8	15.7	10.8	10.8	17.4	3.0	67	34	48	50	3.0	11.8	6.7	7.2	0 ⊙	0 ⊙	0	ESE 2	SSE 6	SE 4
23	87.5	86.6	86.5	86.8	6.5	16.5	10.4	10.9	17.8	3.1	69	35	40	48	3.0	12.0	7.6	7.5	0 ⊙	0 ⊙	0	SE 5	E 6	ESE 6
24	87.5	88.7	88.9	88.4	7.3	10.3	8.9	8.8	11.8	5.1	73	57	67	66	2.7	5.4	3.8	4.0	3 ⊙	9	10	ESE 5	E 8	E 7
25	90.0	90.4	90.2	90.2	7.1	11.7	10.1	9.8	13.1	4.9	77	60	66	68	2.3	5.3	4.3	4.0	10	9	8	E 7	SE 9	ENE 5
26	88.1	86.9	85.8	86.9	7.3	14.9	12.2	11.6	17.2	6.9	77	55	65	66	2.3	7.3	5.0	4.9	10	8 ⊙	3	ENE 5	E 5	E 2
27	86.6	86.4	86.6	86.5	8.6	15.6	11.6	11.8	16.3	5.3	73	41	62	59	3.0	10.3	5.1	6.2	3 ⊙	4 ⊙	3	NE 2	NE 3	NE 1
28	86.6	86.3	85.9	86.3	10.2	18.1	12.2	13.2	20.0	8.7	77	33	64	58	2.8	14.0	5.1	7.3	10	7 ⊙	1	NW 3	N 1	N 1
29	87.1	88.2	90.0	88.4	8.6	16.3	10.8	11.6	19.0	5.8	85	53	55	64	1.7	8.8	3.9	5.5	3 ⊙	8	8 ·	C 0	E 5	E 4
30	87.8	85.1	85.2	86.0	9.1	19.3	11.2	12.8	20.0	7.7	65	37	65	56	4.1	14.3	4.7	7.7	1 ⊙	4 ⊙	10	ESE 5	ENE 9	SE 6
31																								
M	89.6	89.4	89.4	89.5	6.9	15.0	10.3	10.7	16.8	5.3	77	47	64	63	2.3	9.6	4.7	5.5	5.4	5.4	5.7	5.1	4.9	5.1

Sandomierz $H_s = 202\,m$ $H_b = 200{,}3\,m$ $h_w = 20{,}1\,m$ **Marzec – Mars 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	7	0.5	.	–	● 0⁰⁰–05 ▽ 15³⁵–41 18³⁵–45 19⁴⁵–20⁰⁷. = 0⁰⁰–6¹⁵
2	7	.	.	–	= 0³⁰–2³⁰ 5³⁰–11³⁰ 23¹⁰–24
3	7	.	.	–	= 0⁰⁰–9³⁰ 22³⁰–24
4	2	0.2	.	–	● 7³²–8⁰³ ● 8⁰⁰–12¹⁵. = 0⁰⁰–8²⁵ = 0-1 14⁴⁵ = –24. ⌓ 23²⁵–24
5	6	0.0	.	–	● 14⁵⁵–15⁴⁰. = 0⁰⁰–24. ⌒ 22⁰⁰–24. ⌓ 0⁰⁰–20
6	7	.	.	–	= 0⁰⁰–12¹⁵ 20²⁰–24. ⌒ 1 1⁰⁰–8⁰⁰
7	6	.	.	–	= 0⁰⁰–13³⁰ 17⁴⁵–24
8	7	.	.	–	= 0⁰⁰–9³⁰ 21⁴⁵–24. ⌒ 0 5⁰⁰–7⁰⁰
9	7	.	.	–	= 0⁰⁰–10¹⁰. ≫ 11²⁵–15³⁰
10	7	.	.	–	
11	7	.	.	–	= 3¹⁰–9¹⁵
12	6	2.4	.	–	● 0 12⁴⁸–13²⁰ 14¹⁵ 23¹⁵–24. = 1⁰⁰ 15³⁰. ≫ 17³⁰ 18⁴⁵ 20¹⁰ 24
13	8	0.5	.	–	● 0⁰⁰–13⁷. 2⁵³ 5³⁵ ⨯ 16³⁵–45 17⁵⁵–18⁰⁶ ▽ 18⁵⁰–19¹⁵. ≫, ⩓ 0⁰⁰–7²⁰ ≫ 8³⁰–9²⁰ ≫, ⩓ 10⁴⁰–16³⁵ ≫ 18⁴⁰ 19²⁵
14	8	0.3	.	–	● 16³⁵ 18³⁵ ● 21¹⁰ 24. = 17⁵⁰–24
15	8	0.0	.	–	● 0⁰⁰ 3²⁰ 7⁰⁵. 35 ≫ 4⁴⁵ 6¹⁰ 10⁴⁰ 11³⁵ 13⁵⁰ 14¹⁵. = 0⁰⁰–1¹⁰
16	7	0.0	.	–	● 5⁵⁰ 6⁴⁵ ▽ 17⁵⁴. 18⁰⁸. ≫ 18⁰³–30. 20³⁵–21¹⁰. = 5⁵⁰–8¹⁵
17	7	.	.	–	⊕ 12¹⁵–13³⁰
18	7	2.6	.	–	● 1 19⁵⁰ 20⁴⁵. 21⁴⁸ 22¹⁰ 23²⁰ 24. = 19⁴⁰–24
19	7	0.0	.	–	▽ 0-1 0⁰⁰–15. ● 0²⁰ 1⁴⁵ 2⁴⁰ ▽ 17⁵⁰–53 ● 19⁵⁵–20²⁵ ✳ 0–20⁵⁵. = na, np
20	7	0.3	.	–	▽ 0 4⁵¹–5⁰⁷ 6⁰⁵–07 10²⁴–31 12¹⁵–18 ⨺ 1 ✳. ⨺ 1-0 12⁴⁴–13⁰⁵
21	6	3.6	.	–	✳ 0-1 6⁴¹ 11³⁵ ✳ – 12¹⁵ ▽ 12⁵⁵–13⁰⁵ ● 0 ⨺ 15⁰³ 17⁵⁵ (K) 16²⁵. ≫ p. = a–p
22	7	0.9	pż.	–	✳ 2-1 2⁵⁵ 3⁰⁹ ⨺ 1 ✳. ✳ 1 5³³–49 ▽ 1-0 ⨺ 1 8⁵⁰ 14³⁶. = 8²⁰–9³⁰
23	6	0.8	1	–	✳ 3⁵³ 9⁰⁵. ● 10²² 11⁵³ ● 19²⁵–20⁴⁵. = 3³⁰–24. ⌓ 1⁰⁰–4⁰⁰
24	7	2.1	.	–	● 8⁵⁵ 9³⁰ ● 14⁵¹ 15⁰³ 16³⁰–17⁰⁵. = 0⁰⁰ 5⁶⁰ 19¹⁰–24. ≫ 10⁴⁰–13³⁰
25	7	0.3	.	–	● 0-1 0⁰³–53 ▽ 11⁰⁰ 15¹⁷. = 0⁰⁰–8¹⁵. ≫ 9³⁰–12¹⁵
26	7	0.5	.	–	= 3¹⁵–11³⁰. ▽ 20¹⁵–21³⁰
27	8	0.0	.	–	● 3⁵⁰ 6⁴⁵ ● 7⁵²–8¹² ✳ 0 12⁵³–58. = 0¹⁵ 7⁴⁵. ≫ ⩓ 11¹⁵ 15²⁰ ≫ p. ⊕ 10⁴⁵–11²⁰
28	8	2.7	.	–	✳ 2-2 9³⁸ 13⁰² ⨺ 1 14⁰⁵ ▽ 15²⁰ ✳ 1-0 17²² 18⁰⁵. ⌒ 20⁰⁵–40
29	6	0.8	2	–	✳ 0 0⁵⁰–2⁴⁰ ✳ 0-1 9⁰³–10¹⁵ 10³⁰ ✳. ● 0 11¹⁰. ▽. ● 0 14⁵³ 24. = na, a, p. ≫ 13²⁵–14³⁵
30	7	0.8	.	–	● 0⁰⁰ 2⁴⁵. 10⁵² 11²⁰ ▽ 1 13¹⁵–27. = na–a, p. ≫ 10³⁰–12⁴⁵. 13⁵⁰–14³⁰
31	7	0.9	.	–	● 0⁰⁴⁰ 1⁵⁰ ▽ 6⁴⁴ 10²⁹ ● 0 10³⁵. 45. 21⁵⁰–23³⁵. = na, p–24
Σ	–	20.2	–	–	UWAGI:

Kwiecień – Avril

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	7	1.4	.	–	● 13⁵¹ 15¹⁵. 18⁵⁰ 24. = 0⁰⁰–4³⁰. ≫ 8⁴⁰–9³⁵. 16⁴⁵ 18²⁰. 20²⁰ 21¹⁵
2	8	6.4	.	–	● 0⁰⁰. 1⁴⁷. 5⁴⁰ 6¹⁴. 11⁵⁵ 23⁴⁰. = 18³⁰–24
3	7	7.0	.	–	● 1-0 0⁴⁸–3⁴⁰ ● 6⁴⁰ 7⁴⁸ ▽ 0-1 10⁵³ 11⁴⁷ ▽ 0-2 13⁵⁰. 14¹⁰. = 0⁰⁰–8⁴⁰
4	7	3.7	.	–	● 6⁵² 7¹⁸–8²⁰ 9²⁵ 11³⁵. = 3³⁰ 12¹⁵ 21¹⁵–24
5	6	0.4	.	–	● 2³⁰–3²⁰ 6⁵⁰. 10³². 10⁵⁰ 11¹⁵. = 0⁰⁰–13³⁰
6	8	.	.	–	
7	7	0.0	.	–	= 4⁵⁰–8³⁰. ⌒ 1 5⁰⁰–9⁰⁰
8	7	3.9	.	–	▽ 6⁴⁵–50 9³²–39 ▽ 0-2 17¹⁰. 18⁴⁰ ▽ 0 23⁵⁵–24. (K) 17⁰⁸–18³⁵ SSE–N. = 1³⁰–10⁴⁰. ⌒ 0 na–a
9	8	.	.	–	▽ 0 0⁰⁰–12¹. ≫ 14⁵⁰–15¹⁵
10	8	.	.	–	= 1³⁰–8²⁰. ⌓ 0 4⁰⁰–7⁰⁰
11	7	.	.	–	
12	8	.	.	–	⌒ 0 3⁰⁰–9⁰⁰
13	7	.	.	–	= 4⁵⁰–8³⁰ 21³⁰–24. ⌒ 0 21⁰⁰–24
14	7	.	.	–	= 0⁰⁰–10¹⁵. ⌒ 0 0⁰⁰–9⁰⁰ 22⁰⁰–24
15	7	.	.	–	= 3³⁰–6³⁰. ⌒ 0 0⁰⁰–8⁰⁰
16	7	16.4	.	–	▽ 0 10⁵⁰ 13¹⁷ ▽ 0-1 13⁴⁶. 16⁵⁴–17³⁶. 19³⁵ 23⁴⁰. (K) 13¹⁷–45 N-SE-S. 16²⁵–18⁰⁵ S–N. 18³²–20²⁵ S-NNE (K) 0 20²⁴–28 NNE. 20⁴²–21⁴⁹ SSE
17	7	.	.	–	⌒ 0-1 np. 16.IV: (K) 0–22⁰⁰ (K) 0–22³⁰ N. = na–9³⁰
18	7	.	.	–	= 0⁴⁵–8⁴⁰. ⌒ 1-2 0⁰⁰–10⁰⁰ ⌒ 0 np
19	7	.	.	–	= 2⁵⁵²–8³⁰. ⌒ 0-1 0⁰⁰–11⁰⁰. ⌒ 0 20⁰⁰–24
20	7	.	.	–	⌒ 0 0⁰⁰–10⁰⁰. ⊕ 10⁵⁰–12¹⁵
21	8	.	.	–	⌒ 0 2⁰⁰–9⁰⁰
22	8	.	.	–	
23	7	.	.	–	
24	8	.	.	–	
25	7	0.3	.	–	
26	7	0.1	.	–	● 0 3⁴⁵ 6²⁵ 7⁵³ 9⁴⁰
27	8	.	.	–	⌒ 1 3⁰⁰–10⁰⁰
28	8	0.0	.	–	▽ 0 15⁴⁵–46. ⌒ 0 20⁰⁰–24
29	7	0.8	.	–	▽ 0 12⁵²–13²⁵. 13²⁰–27. ⌒ 0-1 0⁰⁰–9⁰⁰
30	7	.	.	–	
31					
Σ	–	40.4	–	–	UWAGI:

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ Maj – Mai 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	85.1	87.2	88.9	87.1	9.3	11.2	10.3	10.3	12.0	8.9	78	75	82	78	2.6	3.6	2.2	2.8	10	10	10	Σ 3	SE 1	SSE 1
2	89.9	90.2	89.6	89.9	8.0	13.3	12.0	11.1	14.9	6.4	92	66	76	78	0.9	5.2	3.3	3.1	9	10	1	C 0	C 0	C 0
3	88.6	88.2	88.6	88.5	10.2	19.3	13.1	13.9	20.6	7.0	86	49	75	70	1.7	11.4	3.8	5.6	0 ⊙	6 ⊙	9	C 0	WSW 2	SW 1
4	91.1	92.4	93.8	92.4	12.0	13.1	11.2	11.9	16.5	10.4	86	78	85	83	2.0	3.3	2.0	2.4	8	9 (R)	1	W 3	C 0	WSW 1
5	96.1	95.9	94.8	95.6	6.3	19.2	14.9	13.8	20.1	4.4	100	47	55	67	0.0	11.8	7.5	6.4	10 ≡	6 ⊙	6	C 0	SSW 3	S 1
6	92.6	91.6	92.6	92.3	11.2	21.8	15.6	16.0	22.8	9.4	78	45	96	73	2.9	14.5	0.7	6.0	8	4 ⊙	10	S 1	SSW 5	NW 1
7	93.8	92.3	87.9	91.3	11.6	15.0	13.8	13.6	17.1	11.4	100	83	91	91	0.0	2.9	1.5	1.5	10 •	9	10	C 0	SW 1	SW 2
8	90.2	88.6	88.4	89.1	9.6	12.8	7.6	9.4	14.6	7.4	82	69	91	81	2.2	4.6	0.9	2.6	1 ⊙	8 ⊙	0	WSW 5	W 7	W 2
9	86.8	84.7	83.1	84.9	6.8	9.9	7.4	7.9	12.2	4.6	90	72	94	85	1.0	3.4	0.6	1.7	10	10	9	WSW 6	SW 5	WSW 2
10	83.8	84.8	86.8	85.1	8.5	10.6	7.2	8.4	12.5	6.9	86	75	88	83	1.5	3.2	1.2	2.0	6 ⊙	10 •	9	WSW 5	W 8	W 5
11	88.6	90.1	92.2	90.3	7.3	8.5	7.6	7.8	10.2	5.8	84	80	89	84	1.6	2.3	1.2	1.7	10	10	10	WNW 6	NW 5	NW 5
12	91.8	91.1	91.2	91.4	5.9	5.9	5.9	5.4	8.7	3.7	92	86	82	87	0.7	1.3	1.7	1.2	10	10	4	NNW 7	NW 6	WNW 5
13	92.0	91.4	90.5	91.3	4.5	11.4	9.5	8.7	13.3	2.0	97	61	73	77	0.3	5.3	3.3	3.0	10	7 ⊙	9	W 1	WSW 6	SW 2
14	88.8	88.7	87.5	88.3	7.0	9.0	7.9	8.0	12.7	5.6	88	89	94	90	1.2	1.3	0.6	1.0	9	10 •	10	SW 5	SW 3	SW 3
15	88.0	88.2	89.1	88.4	4.5	11.2	7.8	7.8	12.8	2.7	98	62	89	83	0.1	5.1	1.2	2.1	10 ≡	8	8	SW 4	W 7	WNW 3
16	90.3	89.6	88.9	89.6	6.5	10.4	6.8	7.6	13.5	3.8	87	63	84	78	1.3	4.7	1.6	2.5	10	9 •	2	W 4	W 4	C 0
17	88.5	88.9	90.5	89.3	7.5	15.7	9.8	10.7	16.1	4.2	86	46	84	72	1.5	9.6	1.9	4.3	4 ⊙	7 ⊙	10	NW 1	NW 5	NW 3
18	91.5	92.1	92.1	91.9	7.5	11.6	7.0	8.3	13.6	6.6	86	62	75	74	1.5	5.1	2.4	3.0	9	9 ⊙	4	NNW 4	N 5	N 1
19	91.4	91.2	90.3	91.0	7.8	13.4	10.9	10.8	15.7	4.4	80	44	63	62	2.1	8.7	4.7	5.2	9	8 ⊙	1	C 0	NW 1	C 0
20	88.8	86.2	84.0	86.3	10.2	17.8	14.4	14.2	19.4	5.9	72	42	63	59	3.4	11.8	6.1	7.1	0	4 ⊙	6	C 0	SE 3	SE 3
21	84.2	84.7	85.4	84.8	12.6	14.7	11.2	12.4	16.9	10.6	74	81	91	82	3.7	3.1	1.2	2.7	9	10 •	10	NNE 1	SE 3	NW 1
22	85.2	86.1	86.9	86.1	11.0	13.1	9.7	10.9	16.5	8.0	89	75	63	76	1.5	3.8	4.4	3.2	4 ⊙	10	6	NW 4	N 6	NW 1
23	88.9	89.7	89.9	89.5	11.2	16.2	12.2	13.0	17.6	7.9	66	38	61	55	4.5	11.4	5.6	7.2	4 ⊙	6 ⊙	8	NNW 2	NNW 3	C 0
24	91.2	91.7	91.5	91.5	10.4	18.3	14.4	14.4	19.6	8.1	80	55	75	65	2.6	13.7	4.1	6.8	7 ⊙	9 ⊙	10	SW 1	SW 3	NW 1
25	92.3	91.2	89.6	91.0	11.8	19.6	13.7	14.7	20.8	8.1	74	46	70	63	3.6	12.4	4.7	6.9	0 ⊙	6 ⊙	1	NNW 1	NW 3	N 1
26	89.4	88.7	87.3	88.5	12.8	21.8	16.7	17.0	22.4	9.8	80	40	61	60	2.9	15.6	7.3	8.6	9	8 ⊙	3	N 1	SSW 3	SE 1
27	87.0	86.3	85.9	86.4	13.1	23.2	17.5	17.8	24.8	9.6	75	45	71	64	3.8	15.8	5.9	8.5	0 ⊙	0 ⊙	5	S 1	S 3	N 2
28	86.3	85.3	85.5	85.7	15.7	22.5	14.7	16.9	24.5	10.7	75	54	84	71	4.4	12.4	2.7	6.5	1	7 ⊙ (R)	9	SSE 2	SSE 4	W 2
29	83.7	78.8	74.6	79.0	13.1	23.2	18.4	18.3	25.5	11.8	96	50	76	74	0.6	14.2	5.1	6.6	10	4 ⊙	10 •	NNE 4	ESE 5	SSE 2
30	76.5	79.0	80.5	78.7	13.7	17.1	12.7	14.0	19.6	12.5	92	67	93	84	1.3	6.3	1.1	2.9	10	8 ⊙	10 •	SW 4	W 3	WNW 2
31	83.1	83.7	83.9	83.6	11.5	17.2	14.2	14.3	19.4	10.7	87	54	68	70	1.9	9.0	5.1	5.3	9	1 ⊙	1	WSW 3	SW 5	C 0
M	88.6	88.3	88.1	88.3	9.6	15.1	11.5	11.9	17.0	7.4	85	61	79	75	1.9	7.6	3.1	4.2	7.0	7.5	6.5	2.5	3.8	1.7

Czerwiec – Juin

1	83.9	83.6	82.5	83.3	13.8	23.9	19.4	19.1	25.8	8.8	77	37	65	60	5.7	18.5	7.8	10.0	0	1 ⊙	1	SSW 1	SSW 3	SSW 1
2	82.8	82.3	82.5	82.5	16.4	26.4	18.6	20.0	27.5	13.6	81	41	79	67	3.4	20.2	4.5	9.4	6 ⊙	3 ⊙	10	SW 1	SW 2	S 1
3	82.9	82.5	84.4	83.3	18.6	26.4	16.0	19.2	27.0	13.8	75	42	92	70	5.3	19.8	1.6	8.9	1 ⊙	6 ⊙	8	S 1	S 3	NNW 1
4	85.9	85.9	87.8	86.5	16.7	24.4	17.2	18.9	26.2	14.0	93	51	87	77	1.4	15.1	2.6	6.4	7 ⊙	6 ⊙	7	NW 2	NW 1	NE 3
5	90.1	91.6	92.2	91.3	16.2	22.4	18.0	18.6	23.9	13.4	94	54	66	71	1.2	12.4	6.9	6.8	9	6 ⊙	8	NE 4	SE 5	E 3
6	92.4	91.9	90.1	91.5	17.6	18.4	17.7	17.8	20.1	15.0	80	81	84	82	4.0	4.1	3.2	3.8	8	10	8	E 5	E 7	ESE 3
7	88.6	87.6	86.7	87.6	17.1	24.6	16.8	18.8	25.1	15.0	88	53	85	75	2.4	14.5	3.3	6.7	8	8 ⊙	10	SE 2	S 4	SW 3
8	87.2	87.9	88.4	87.8	15.2	23.0	17.0	18.0	25.2	13.4	96	64	85	82	0.8	10.2	3.0	4.7	10	6 ⊙	10	SSW 1	S 2	W 2
9	89.3	89.2	88.9	89.1	16.2	24.7	17.0	18.7	25.8	13.1	92	49	81	74	1.6	16.0	3.8	7.1	0 ⊙	4 ⊙	5	NW 1	WSW 2	C 0
10	90.3	89.9	89.8	90.0	17.3	26.7	18.5	20.2	27.6	13.1	87	37	74	66	2.6	21.9	5.5	10.0	0	4 ⊙	10	S 2	SSE 4	SE 1
11	89.8	88.9	88.1	88.9	15.1	23.9	16.0	17.8	25.8	12.5	88	50	87	75	2.1	14.7	2.3	6.4	7	5 ⊙	7	SSE 3	SW 1	WNW 2
12	87.9	87.2	86.7	87.3	16.0	17.8	16.5	16.7	21.1	15.1	96	99	88	94	0.8	0.2	2.4	1.1	10	8 (R)	9	W 1	NW 2	NNW 2
13	87.0	85.7	83.3	85.3	13.4	21.0	17.8	17.5	22.3	13.0	99	64	76	80	0.2	8.9	5.0	4.7	10 •	6 ⊙	10	WSW 2	SSW 2	SW 1
14	83.0	84.5	87.8	85.1	14.4	18.5	14.2	15.3	19.1	13.7	97	67	78	81	0.6	7.0	3.6	3.7	10	9 •	7	SW 1	WSW 9	WSW 3
15	89.7	91.9	92.6	91.4	13.3	15.8	12.6	13.6	17.6	12.0	90	56	74	73	1.6	7.9	3.7	4.4	10 •	8 ⊙	0	WSW 7	W 7	W 2
16	94.9	94.5	95.2	94.9	12.6	17.2	15.2	14.0	19.0	8.5	80	52	82	71	2.9	9.4	2.8	5.0	1 ⊙	8	0	WSW 3	WSW 2	WSW 1
17	96.4	96.2	95.9	96.2	11.8	21.0	17.2	16.8	22.6	7.5	85	46	54	62	2.0	13.4	9.0	8.1	0	7 ⊙	2	WSW 1	W 3	W 1
18	96.3	94.9	92.6	94.6	14.0	24.2	19.6	19.4	25.7	10.3	77	44	71	64	3.7	17.0	6.7	9.1	8 ⊙	3 ⊙	0	W 1	SW 3	WSW 1
19	93.0	93.7	97.0	94.6	17.8	26.0	16.8	19.4	26.4	13.4	81	64	82	76	3.8	12.2	3.3	6.5	0 ⊙	7 ⊙	9	WSW 4	NW 1	NW 3
20	101.1	101.4	101.6	101.4	14.6	20.3	13.4	15.4	21.3	11.6	70	39	67	59	5.0	14.6	5.2	8.3	0 ⊙	4 ⊙	0	NW 1	NW 4	N 1
21	101.2	98.7	97.2	99.0	14.6	21.3	17.2	17.6	24.1	9.0	65	37	65	56	5.8	15.9	6.9	9.5	0	2 ⊙	1	N 1	WSW 1	WSW 1
22	102.8	100.5	95.2	99.5	11.3	19.8	18.4	17.0	23.9	10.0	87	49	68	68	1.9	11.7	6.8	6.8	10	0 ⊙	1	NNW 2	SE 2	S 1
23	91.5	93.7	94.9	93.4	16.0	21.6	18.2	18.3	24.1	15.4	98	63	69	77	0.4	9.3	6.4	5.4	10 •	8 ⊙	1	C 0	WNW 4	WNW 2
24	96.1	95.6	97.0	96.2	16.0	23.6	17.6	18.7	25.8	11.2	80	48	72	67	3.6	15.2	5.7	8.2	5 ⊙	8 ⊙	3	WSW 4	W 5	WNW 2
25	95.6	95.3	91.1	93.3	16.1	27.2	21.4	21.5	29.3	11.7	84	43	70	66	2.9	19.8	7.8	10.2	3 ⊙	4 ⊙	1	WSW 4	WSW 4	NW 1
26	90.8	89.0	90.2	90.0	19.2	30.8	18.0	21.3	31.2	14.7	77	37	94	69	5.0	27.8	1.2	11.3	1 ⊙	3 ⊙	10	WSW 4	SW 4	W 3
27	88.3	86.8	87.0	87.4	19.6	30.6	19.0	22.0	31.3	16.7	84	39	83	69	3.6	26.7	3.8	11.4	0 ⊙	1 ⊙	10 • R	SW 2	SSW 6	W 6
28	88.4	96.8	102.1	95.8	17.7	12.8	13.3	14.3	19.2	12.6	99	89	72	87	0.2	1.6	4.3	2.0	10 •	10 •	3	WNW 3	NW 5	WNW 3
29	104.4	104.0	104.1	104.2	15.0	19.0	15.6	16.3	21.3	9.8	73	56	77	69	4.5	9.6	4.1	6.1	2 ⊙	8 ⊙	10	NW 3	WNW 5	N 2
30	104.2	103.3	101.3	103.0	16.6	21.8	18.4	18.8	23.3	14.1	71	54	73	67	3.3	11.9	3.3	7.6	0 ⊙	4 ⊙	10	NW 3	N 1	N 1
31																								
M	91.9	91.8	91.8	91.8	15.7	22.3	17.0	18.0	24.3	12.3	85	54	77	72	2.8	13.6	4.6	7.0	4.9	5.6	5.4	2.3	3.3	1.9

Sandomierz $H_s = 202\,m$ $H_s = 200{,}3\,m$ $h_w = 20{,}1\,m$ **Maj – Mai 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	⌒ 21^{00} – 24
2	6	.	.	–	= 0^{15} – 20^{00}. ⌒ 0^{00} – 6^{00}, 22^{00} – 24
3	7	0.0	.	–	= 0^{30} – 7^{30} ⌒ 1 1^{00} – 9^{00}
4	7	2.5	.	–	▽ 1^{53} – 2^{01} 12^{42} – 13^{30} 14^{03} – 40, (K) 11^{53} – 13^{25} – 14^{05} S-E-W K 14^{05}–30 W-E. = na – a
5	7	.	.	–	= 1^{00} – 2^{50} ≡ 0-2 7^{45} = – 9^{45}
6	7	9.1	.	–	● ▽ 15^{05} 18^{15}. = 18^{15} – 24
7	6	4.0	.	–	● 0-1 3^{12} – 10^{30} 10^{55} ▽ 18^{59} – 19^{20} 23^{54} – 24. = 0^{00} – 13^{35}
8	7	4.7	.	–	▽ 0^{00} – 18 11^{27} – 47 ● 0-1 13^{17} – 14^{10} 16^{10} – 44. K 11^{40} – 47 WSW – E 13^{41} – 14^{10} WSW – E. = np. ≫ 13^{20}–35
9	7	5.2	.	–	● ▽ 9^{50} – 10^{16} ▽ 0-2 12^{45} – 13^{15} ▲ 12^{54}–55 ▽ 13^{43} – 19^{35}. (K) 10^{50} – 11^{38} S K 12^{45} – 13^{40} S W – N – NE (K) – 14^{50} SW – NE.
10	7	1.0	.	–	▽ 5^{30} – 24. = na **[9.V: = 0^{00} – 11^{20}. 20^{30} – 24**
11	7	0.0	.	–	▽ ⌒ 0^{00} – 06 10^{07} – 12 ● ⌒ 10^{50} – 11^{20}
12	7	2.5	.	–	● ⌒ 7^{40} – 11^{10} ● ▽ 12^{50} – 13^{02} ● ⌒ 13^{15} – 14^{20} 14^{45}. = 4^{15} – 11^{30}
13	7	0.4	.	–	= 3^{40} – 10^{45} ⌒ ⌒ 20^{00} – 24
14	6	5.1	.	–	● ▽ 6^{25}–30 9^{52} – 55 ● ⌒ 11^{15} 14^{25} ▽ 15^{35} – 19^{15} ● ⌒ 19^{25} – 20^{25}. = 0^{30} – 24. ⌒ ⌒ 0^{00} – 6^{00}
15	7	2.7	.	–	● ▽ 1-0 14^{15} 20^{28}. = 0^{00} – 3^{45} ≡ 0-2 7^{45} = – 10^{50}
16	8	0.0	.	–	▽ 10^{13} – 14^{02}. = 3^{30} – 8^{20}. ⌒ ⌒ 20^{00} – 24
17	7	.	.	–	= 0^{00} – 7^{50}. 20^{20} – 24. ⌒ 0-1 0^{00} – 9^{00} ⌒ ⌒ 23^{00} – 24
18	7	0.0	.	–	● 10^{57}–59. = 0^{00} – 7^{15}. ⌒ ⌒ 0^{00} – 9^{00} ⌒ 0-1 19^{00} – 24
19	7	.	.	–	= 1^{30} – 8^{30} ⌒ 1-0 0^{00} – 9^{00} ⌒ ⌒ 19^{00} – 24
20	8	0.0	.	–	● ▽ 21^{50} – 22^{05}. = 3^{15} – 6^{10}. ⌒ 0-1 0^{00} – 9^{00}
21	6	0.4	.	–	● 8^{55}. 10^{10} – 11^{30} 12^{45} ▽ 17^{52} – 18^{23} ● ⌒ 18^{44} – 19^{05}. 19^{15}–18. = na – p
22	7	.	.	–	= na – a
23	8	.	.	–	⌒ 20^{00} – 24
24	7	.	.	–	⌒ 0^{00} – 9^{00}. ⊕ 11^{45} – 14^{20}
25	7	.	.	–	= 1^{50} – 8^{50}. ⌒ ⌒ 20^{00} – 24
26	7	.	.	–	= 0^{30} – 10^{15}. ⌒ 0-1 0^{00} – 8^{00}
27	7	.	.	–	= 22^{15} – 24 ⌒ ⌒ 3^{00} – 9^{00}
28	7	3.7	.	–	● ▽ 15^{51} – 16^{08} ● 0-1 17^{03} – 18^{37}. (K) 13^{30} – 14^{25} NE – N – NNW K 16^{25} – 19^{05} S – N. = 0^{00} – 8^{30}. ⌒ ⌒ 20^{0} – 7^{00}
29	7	2.9	.	–	▽ 0-1 20^{29} – 23^{50}. = 1^{00} – 11^{30}
30	7	9.3	.	–	● ▽ ⌒ 2^{48} – 3^{08} 17^{45} – 18^{03} ● 0-1 20^{15} – 23^{20}. = 1^{45} – 8^{20}. np
31	7	.	.	–	= 0^{00} – 9^{15}. ⌒ ⌒ 21^{00} – 24
Σ	–	53.1	–	–	UWAGI.

Czerwiec – Juin

1	8	.	.	–	= 0^{20} – 7^{45}. ⌒ ⌒ 0^{00} – 8^{00}, 23^{00} – 24
2	7	.	.	–	= 23^{30} – 24. ⌒ 0-1 0^{00} – 9^{00} ⌒ ⌒ 23^{00} – 24
3	7	1.4	.	–	● ▽ 14^{35}–48 18^{55} 20^{09}. K 18^{50} – 19^{38} NNE – NNW. = 0^{00} – 6^{45}. np ⌒ 0-1 na
4	7	0.5	.	–	● ▽ 11^{35}–53 15^{43} 17^{36}. K 15^{45} – 17^{05} NNE – WNW. = 0^{00} – 9^{30}. np
5	7	.	.	–	= 0^{00} – 10^{10}. ⌒ 0-1 3^{00} – 8^{00}
6	7	0.0	.	–	● ▽ 13^{55} 14^{03}. = 2^{30} – 11^{15} ⌒ 0-1 0^{00} – 8^{00}
7	7	2.2	.	–	● 0-1 14^{57} – 15^{12} 15^{59} – 16^{07} 19^{45}–48. K 15^{15}–40. = 0^{30} – 9^{15}. 23^{50} – 24
8	7	.	.	–	(K) 17^{30} – 20^{20}. = 0^{00} – 9^{15}. 20^{30} – 24. ⌒ ⌒ 4^{00} – 7^{00}
9	7	.	.	–	(K) 18^{35}. 19^{40} SSE – SSW. = 0^{00} – 10^{30}. 22^{30} – 24. ⌒ ⌒ 2^{00} – 8^{00}
10	7	1.1	.	–	● ▽ 16^{30}–52. K 16^{25} – 17^{20} SSE – NW (K) – 18^{20} N. = 0^{00} – 8^{30}. ⌒ 0-1 2^{00} – 9^{00}
11	7	0.0	.	–	(K) 15^{10} – 17^{00} ENE – S = 3^{50} 9^{30}. ⌒ ⌒ 5^{00} 9^{00}
12	7	26.6	.	–	● 7^{33}–45 ▽ 0-2 9^{55} 13^{13} ▽ ● 15^{04}–35 ● ▽ ● 21^{04} 24. (K) 12^{40}–50 W K 1 13^{30} W – NE (K) 14^{00} NE. 15^{20} 16^{05} N. = 2^{00} 11^{30} 21^{15}–24
13	7	2.9	.	–	● 0^{00} 8^{60} 22^{45} 23^{05} – 24. = 0^{00} – 13^{15} – 23^{05} 24
14	7	3.2	.	–	● 0^{00}–45 3^{30} – 5^{30} 8^{45} ▽ 13^{34} – 47. = 0^{00} – 10^{15}
15	7	0.0	.	–	▽ ● 0^{45} 8^{10}. = 0^{30} – 10^{20} ⌒ ⌒ 22^{00} – 24
16	7	.	.	–	⌒ 0-1 0^{00} – 9^{00} ⌒ ⌒ 23^{00} – 24
17	7	.	.	–	= 5^{10} – 9^{30}. ⌒ 0-1 0^{00} – 8^{00}. 22^{00} – 24
18	7	.	.	–	⌒ 1-2 0^{00} – 9^{00} ⌒ ⌒ 23^{00} – 24
19	7	0.0	.	–	● ▽ 14^{10}–24. = 3^{15} – 8^{45}. ⌒ 0-1 0^{00} – 9^{00}
20	7	.	.	–	= 0^{50} – 9^{15}. ⌒ ⌒ 21^{00} – 24
21	7	.	.	–	⌒ 0-1 0^{00} – 9^{00}
22	7	3.6	.	–	= 3^{15} – 8^{30}
23	7	3.8	.	–	● 5^{50} 6^{30} – 9^{20} ▽ 2-0 9^{20}–26. = 4^{30} – 12^{30}. ⌒ ⌒ 22^{00} – 24
24	7	.	.	–	= 4^{15} – 9^{30} ⌒ ⌒ 0^{00} – 9^{00} 23^{30} – 24
25	7	.	.	–	= 4^{15} – 7^{15}. ⌒ 0-1 0^{00} – 9^{00}
26	7	23.2	.	–	● ▽ 0-1 16^{35} – 18^{15}. K 16^{25} – 18^{40} SW – NE. = 20^{15} – 24. ⌒ ⌒ 2^{00} – 8^{00}
27	7	16.7	.	–	● ▽ 0-1 20^{56} – 23^{03}. K 20^{50} – 22^{15} W – E (K) – 23^{30} N – E – S 23^{48} – 24 WSW – E. = na – a, np. ≫ 20^{05}–10
28	6	3.3	.	–	● ▽ 0-1 5^{07} 10^{10}. ⌒ 10^{15} 14^{20}. (K) 0^{00} – 3^{30} WSW – S – E K 5^{30} – 6^{35} WSW – W – N. = 0^{00} – 14^{20}
29	7	.	.	–	⌒ ⌒ 3^{00} – 8^{00}
30	7	.	.	–	⌒ ⌒ 21^{00} – 24
31					
Σ	–	78.3	–	–	UWAGI.

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ **Lipiec – Juillet 1961**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.7	101.0	99.9	100.9	18.2	25.7	18.6	20.3	26.6	15.8	75	46	72	64	5.3	17.9	6.1	9.8	0 ⊙	2 ⊙	2	NW 1	NW 1	N 1
2	100.5	99.6	97.7	99.3	19.2	26.1	20.8	21.7	28.3	12.9	71	45	67	61	6.4	18.6	8.0	11.0	0 ⊙	0 ⊙	0	NNW 1	NNW 3	C 0
3	97.4	95.7	92.6	95.2	18.8	29.3	25.3	25.7	30.2	15.9	71	40	47	53	6.3	24.5	15.0	15.3	0 ⊙	1 ⊙	0	WSW 1	SW 3	SW 2
4	90.1	87.5	84.6	87.4	19.5	28.3	20.2	22.6	29.7	16.3	81	51	84	72	4.3	18.9	5.8	9.0	0 ⊙	1 ⊙	9	SW 2	WSW 2	SSW 2
5	89.5	90.6	92.0	90.7	15.4	19.2	14.6	16.0	20.4	14.2	79	57	74	70	3.7	9.6	4.3	5.9	8	9 ⊙	9	WNW 3	WNW 3	W 1
6	93.6	95.4	97.0	95.3	12.4	13.7	12.6	12.8	17.0	8.1	78	73	73	75	3.2	4.2	3.9	3.8	1 ⊙	8	10	WSW 1	W 7	W 3
7	97.8	97.8	98.0	97.9	11.7	17.6	15.2	15.9	17.9	8.8	85	58	76	73	2.0	8.4	3.7	4.7	9	8 ⊙	8	W 3	W 3	WNW 1
8	98.1	97.2	94.6	96.6	12.2	18.8	14.6	15.0	21.8	8.3	78	43	58	60	3.2	12.4	7.0	7.5	6 ⊙	8 ⊙	1	W 1	NW 4	C 0
9	90.2	86.7	88.1	88.3	13.7	22.0	13.6	15.7	24.4	10.4	72	41	95	69	4.4	15.7	1.1	7.1	0 ⊙	8 ⊙	10 •	SW 1	SW 4	W 2
10	88.7	88.4	89.7	88.9	12.6	19.2	12.9	14.4	20.3	10.3	88	44	89	74	0.7	12.3	1.6	4.9	3 ⊙	7 ⊙	8	W 3	WNW 6	WSW 3
11	92.3	92.6	91.7	92.2	13.2	19.3	16.6	16.4	21.3	8.9	74	41	60	58	4.0	15.3	7.5	8.3	3 ⊙	8 ⊙	8	W 3	SW 4	WSW 2
12	89.1	87.5	85.3	87.3	13.0	21.5	22.4	19.8	27.0	11.0	80	70	74	75	3.0	7.8	7.2	6.0	9	2 ⊙	10	SSW 2	S 4	WNW 1
13	82.4	78.6	77.3	79.4	17.6	27.2	17.5	20.0	28.9	14.5	88	53	95	79	2.4	16.9	1.0	6.8	2 ⊙	2 ⊙	10 • R	SSW 1	SSW 9	W 2
14	82.0	85.3	88.0	85.1	14.8	17.3	14.1	15.1	19.1	12.9	89	52	73	71	1.8	9.4	4.4	5.2	4 ⊙	9	1	SW 4	W 7	W 1
15	89.3	88.8	89.7	89.2	13.7	25.8	17.8	18.3	25.2	10.8	83	49	80	71	2.7	14.9	4.0	7.2	9	6 ⊙	1	SW 2	SW 5	W 1
16	84.9	86.5	87.0	86.1	14.3	18.7	15.3	15.9	21.6	13.9	92	75	81	82	1.3	6.0	3.4	3.6	10 •	9	1	NE 2	WSW 12	C 0
17	85.9	84.8	85.6	85.4	15.2	22.8	15.0	17.0	25.7	12.5	85	52	78	72	2.6	13.3	3.6	6.5	6 ⊙	8 ⊙	7	WSW 2	SW 4	W 2
18	85.3	85.2	85.4	85.3	12.4	16.8	14.2	14.4	19.3	8.4	81	63	82	75	2.7	7.1	2.9	4.2	0	8 ⊙	0	WSW 4	W 4	W 1
19	86.2	85.9	86.5	86.2	12.0	20.7	13.8	15.1	21.5	9.3	90	52	86	76	1.3	11.7	2.2	5.1	7	8 ⊙	0	WNW 1	SW 3	C 0
20	87.2	88.0	87.2	87.5	14.2	19.5	15.6	16.2	20.5	9.9	83	55	82	73	2.7	10.2	3.2	5.4	4 ⊙	10	10	WSW 2	SW 4	WSW 3
21	89.3	89.3	89.9	89.5	14.8	20.1	14.6	16.0	20.5	11.2	83	55	95	77	2.9	10.5	1.1	4.8	3 ⊙	8 ⊙	10	WSW 2	WSW 8	W 2
22	89.1	89.1	89.8	89.3	13.1	18.8	14.0	15.0	19.8	12.1	92	59	90	80	1.3	8.8	1.6	3.9	10	9	6	WSW 6	W 6	W 1
23	92.0	92.6	93.9	92.8	13.7	18.4	14.8	15.4	20.5	11.5	91	60	76	76	1.5	8.5	4.0	4.7	2	9 ⊙	2	SW 3	SW 4	NW 1
24	96.4	96.9	99.4	97.6	13.2	17.6	13.7	14.6	19.7	9.6	91	61	65	72	1.4	7.9	5.5	4.9	10	9	8	SW 1	WNW 2	WNW 2
25	101.2	101.5	100.4	101.0	13.3	16.7	13.1	14.0	17.7	10.4	77	51	77	68	3.5	9.4	3.5	5.5	9	9	4	NW 3	WNW 4	W 2
26	99.0	97.1	92.9	96.3	13.3	19.4	17.6	17.0	22.3	11.2	81	50	63	65	3.0	11.2	7.3	7.2	8 ⊙	8 ⊙	8	W 2	SW 5	SW 1
27	88.8	86.3	85.7	86.9	15.0	25.6	21.2	20.8	27.3	11.8	75	40	62	59	4.1	19.7	9.6	11.1	2 ⊙	8	9	SW 4	WSW 8	WSW 3
28	84.7	83.1	82.9	83.6	18.0	26.6	18.2	20.2	28.1	15.8	89	46	95	77	2.2	18.7	1.1	7.3	5 ⊙	8 ⊙	9	WNW 2	SW 6	SW 1
29	82.2	88.7	91.1	87.3	15.4	13.1	14.2	14.2	18.6	12.4	98	94	93	95	0.4	0.9	1.1	0.8	10	10 •	10	WNW 1	NW 5	WNW 1
30	90.1	88.1	89.1	89.1	12.6	12.8	12.6	12.6	14.3	12.3	98	100	99	99	0.4	0.0	0.2	0.2	10 •	10 •	10 •	N 4	N 4	W 3
31	88.6	91.3	94.1	91.3	12.0	16.5	13.0	13.6	17.5	11.2	99	67	93	86	0.2	6.2	1.1	2.5	10	9	9	SW 3	SW 8	SW 3
M	90.8	90.6	90.6	90.7	14.5	20.4	15.9	16.7	22.3	11.6	84	56	78	73	2.7	11.4	4.2	6.1	5.2	7.1	6.1	2.3	5.0	1.6

Sierpień – Août

1	95.0	95.2	95.0	95.1	13.0	18.7	15.9	14.9	20.8	11.1	85	44	81	70	2.3	12.0	3.0	5.8	9	5 ⊙	0	SW 3	WSW 8	SW 1
2	94.6	92.7	91.3	92.9	13.8	24.7	20.0	19.6	26.5	9.9	81	38	62	60	3.0	19.3	8.8	10.4	0	0 ⊙	2	WSW 1	SW 1	S 3
3	91.7	92.3	95.6	93.2	16.4	23.2	16.6	18.2	24.1	13.4	83	61	89	78	3.0	11.1	2.2	5.4	9	6 ⊙	10	S 1	NW 2	NW 1
4	97.8	96.6	94.9	96.4	13.8	20.3	16.4	16.7	21.8	10.7	78	45	70	64	3.6	13.2	5.6	7.5	0 ⊙	7 ⊙	9	NW 2	W 2	WSW 1
5	94.2	94.0	93.4	93.9	16.3	21.8	17.5	18.3	24.2	14.4	75	60	79	71	4.5	10.3	4.2	6.3	8 ⊙	7 ⊙	1	WSW 2	WSW 4	W 2
6	92.7	91.1	89.8	91.2	16.8	29.6	25.0	23.1	30.3	13.5	86	40	68	65	2.7	24.8	9.1	12.2	1 ⊙	1 ⊙	2	WSW 1	SW 5	SSW 1
7	89.3	88.8	90.8	89.6	19.6	29.7	20.4	22.5	30.8	16.4	79	36	78	64	4.7	26.7	5.3	12.2	1 ⊙	2 ⊙	6	S 1	W 2	N 3
8	95.7	95.6	95.7	95.0	15.8	19.4	17.3	17.4	21.8	15.3	89	63	87	80	1.9	8.4	2.6	4.3	10	10	9 • R	N 2	NE 3	NE 1
9	94.9	96.1	96.1	95.7	17.4	28.8	22.5	22.8	29.6	14.3	96	51	83	77	0.9	19.3	4.5	8.2	3 ⊙	3 ⊙	3	C 0	WNW 1	C 0
10	96.6	95.8	92.2	94.9	19.8	26.9	24.2	23.8	29.5	19.0	98	68	87	84	0.5	11.2	4.1	5.3	9 ⊙	• 3 ⊙	0	NE 1	SSE 4	E 2
11	90.6	88.3	92.1	90.3	22.8	31.9	20.6	24.0	33.3	19.6	80	44	89	71	5.4	26.4	2.6	11.5	0 ⊙	6 ⊙	5	C 0	SSW 2	W 3
12	93.5	92.3	88.5	91.4	18.1	21.4	17.2	18.5	24.0	16.4	94	73	98	88	1.3	6.9	0.4	2.9	9	9	10 •	W 3	WSW 2	ENE 4
13	90.3	94.4	97.2	94.0	13.9	13.8	11.6	12.7	17.5	10.7	99	92	94	95	0.2	1.3	0.8	0.8	10 •	10 •	2	NW 4	NW 4	WSW 2
14	98.2	97.5	95.1	96.9	11.2	17.3	13.4	13.8	19.9	8.2	97	57	83	79	0.3	8.5	2.7	3.8	8	9	1	W 2	SW 3	C 0
15	92.9	89.9	89.3	90.7	11.0	20.2	15.3	15.4	21.6	9.6	97	58	82	79	0.3	10.0	3.2	4.5	0	8	8	SW 1	SSW 3	W 1
16	88.0	88.0	87.1	87.7	13.8	13.9	12.5	13.7	17.5	11.5	88	69	89	82	2.0	5.6	1.5	3.0	9	10	8	SW 3	WSW 5	WSW 2
17	85.7	84.5	84.0	84.7	11.2	17.0	13.0	13.6	18.0	9.0	83	53	80	72	2.3	9.2	3.0	4.8	4 ⊙	10	4	WSW 2	WSW 5	C 0
18	83.6	83.1	83.8	83.5	11.2	15.2	13.0	13.1	18.3	9.3	86	65	81	77	1.8	6.0	2.8	3.5	6	10	8	NW 5	WNW 7	WNW 5
19	84.9	85.6	83.7	84.1	12.1	17.8	15.3	15.1	19.5	10.4	83	56	77	72	2.3	9.1	4.1	5.2	4 ⊙	9	1	WSW 6	WSW 8	SW 5
20	84.6	85.4	88.4	86.1	15.6	14.5	11.6	12.8	18.2	11.3	92	81	93	89	1.3	3.1	1.0	1.8	10	10	8	SW 4	WSW 5	WSW 4
21	90.9	91.4	91.2	91.2	11.3	17.4	15.6	15.0	18.9	9.9	93	67	84	81	1.0	6.6	2.8	3.5	10	8 ⊙	10	WSW 5	WSW 9	SW 5
22	89.5	86.9	84.2	86.9	13.6	23.5	17.4	18.0	25.2	11.0	80	46	72	66	3.2	15.7	5.7	8.2	0 ⊙	0 ⊙	8	SW 2	SW 9	WSW 4
23	87.2	87.2	89.7	88.0	13.4	18.4	12.1	14.0	18.6	12.1	87	57	93	79	2.0	9.1	1.0	4.0	10	8 ⊙	9	W 4	W 4	W 3
24	91.6	92.7	94.2	92.8	10.8	17.0	11.8	12.8	17.5	9.3	89	51	80	73	1.3	9.3	2.8	4.6	9	7 ⊙	9	W 3	W 7	W 2
25	94.3	94.2	95.1	94.5	11.3	19.8	14.7	15.1	20.6	9.9	94	48	87	76	0.8	11.9	2.2	5.0	10	7 ⊙	10	WSW 2	WSW 7	W 3
26	96.0	97.8	98.7	97.5	12.4	17.1	14.4	14.6	18.9	11.4	99	79	92	90	0.2	4.1	1.3	1.9	10 •	10	10	SSW 1	NNW 2	SW 1
27	99.3	99.0	99.4	99.2	14.6	24.4	17.6	18.6	24.6	14.1	98	54	86	79	0.4	14.2	2.8	5.8	9	8	0	C 0	W 3	NNW 1
28	100.4	101.0	101.8	101.1	16.4	23.0	15.0	17.4	23.7	13.9	91	60	65	72	1.7	11.2	5.9	6.3	8	8 ⊙	3	NW 3	W 2	NW 4
29	101.4	100.0	98.9	100.1	12.8	22.0	16.2	16.8	22.7	11.1	91	54	79	75	1.4	12.2	3.8	5.8	2	8 ⊙	3	W 2	NNW 5	NNE 1
30	100.6	101.3	102.0	101.3	12.0	18.9	12.7	14.1	19.9	9.4	90	45	75	70	1.3	11.9	3.7	5.6	2 ⊙	2 ⊙	0	NNW 3	N 3	N 1
31	103.9	104.7	105.3	104.7	11.4	21.0	16.1	16.2	22.5	9.7	85	49	72	68	2.3	12.8	5.1	6.7	7	2 ⊙	0	NW 4	NNE 1	N 1
M	93.2	92.9	93.0	93.0	14.2	21.0	16.1	16.8	22.6	12.1	89	57	82	76	1.9	11.7	3.5	5.7	6.0	6.5	5.1	2.4	4.1	2.4

Sandomierz $H_s = 202\ m$ $H_b = 200{,}3\ m$ $h_w = 20{,}1\ m$ **Lipiec – Juillet 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	OPAD ŚNIEGU s	USŁONECZNIENIE	POGODA
1	7	.	.	–	⌒ 0 00–8 00 21 00–24
2	7	.	.	–	⌒ 0-1 0 00–8 00 ⌒ 0 22 00–24
3	7	.	.	–	⌒ 1 na–a ⌒ 0 21 00–24
4	7	0.3	.	–	• 0 18 29–31 19 14–15 ⌒ 0 0 00–6 00 ↖ 22 40–24 E-S
5	7	.	.	–	▽ 0 1 48–2 06 4 48–5 35 ↖ 0 0 00–1 15 E-S . = 1 30–7 15
6	7	0.0	.	–	▽ 0 12 48–13 13 . ⌒ 0 2 00–8 00
7	7	0.0	.	–	▽ 0 12 44–45 13 07–08 . = 4 30–8 45
8	7	.	.	–	= 4 20–7 10 . ⌒ 0 0 00–7 00 . 21 00–24
9	8	1.0	.	–	• 0 19 38–21 42 . = 21 40–24 . ⌒ 0-1 0 00–9 00
10	7	0.1	.	–	▽ 0 17 15–16 17 32–36 = 0 00 7 45–22 10–24
11	7	.	.	–	= 0 00–5 15 . ⌒ 0 2 00–9 00 23 00–24
12	7	5.8	.	–	• 0 8 33–9 15 • 0 9 18–11 33 . = 4 30–12 20 . ↖ 0 9 30–45 W-E (↖) 0–11 30
13	7	6.3	.	–	▽ 0-1 20 01–08 ▽ 0-2 20 37–21 20 . ↖ 19 50–22 10 W-NE . = 20 30–24 . ≫–≡ 20 24–47
14	7	.	.	–	= 0 00–4 15 . ⌒ 0 22 00–24
15	7	1.3	.	–	⌒ 0-1 0 00–9 00 21 00–24
16	7	0.0	.	–	▽ 0 5 45–6 48 • 0 7 07–8 17 . = 3 20–9 45 . ≫–≡ 10 25–13 45 . ⌒ 1 na ⌒ 0 np
17	7	.	.	–	= 1 15–9 30 . ⌒ 0-1 0 00–9 00 . ⌒ 0 22 00–24
18	7	.	.	–	= 4 30–9 10 . ⌒ 0-1 0 00–9 00 . 21 00–24
19	7	.	.	–	= 1 30–11 15 21 10–24 . ⌒ 1 0 00–9 00 ⌒ 0 21 00–24
20	7	0.0	.	–	• 0 13 44–14 08 . = 0 00–3 45 = 0-2 6 40–9 30 . 21 40–24 . ⌒ 0-1 0 00–3 00 ⌒ 1 8 00–10 00
21	7	0.6	.	–	▽ 0 20 48–21 13 . = 0 00–8 40 20 30–24
22	7	5.1	.	–	▽ 0 7 10–22 ▽ 0-2 14 24–18 39 (↖) 0 15 47–16 45 SW-N ↖ 0 18 08–19 15 NW-NE . = 0 00–11 30 . 21 15–24
23	7	.	.	–	= 0 00–8 15 . ⌒ 0 22 00–24
24	7	0.0	.	–	▽ 0 11 52–12 01 . = 3 10–10 15 . ⌒ 0-1 0 00–10 00
25	7	.	.	–	⌒ 0 np
26	7	.	.	–	= 1 30–7 10 . ⌒ 0 0 00–4 00 . ◡ 23 45–24
27	7	1.6	.	–	▽ 0 23 55–24 . ≫ 1 4 10–15 20 . ◡ 0 0 00–1 20
28	7	4.4	.	–	▽ 0 0 00–03 0 08–12 • 0-2 17 28–51 ▽ 0 19 04–12 19 22–36 . ≫ 12 35–13 40 . = na–a , np
29	7	15.8	.	–	• 0-1 1 35–2 04 • 0-1 6 15–8 50 13 47 • 1 4 52–24 . = 0 00–p , np
30	6	18.6	.	–	• 0 0 00–2 15 3 05 • 0-1 9 10 10 07–12 35 13 00–14 20 • 1-0 19 25 • 0 20 17–23 32 = na–p . np
31	7	0.7	.	–	• 0 3 06–5 25 • 0–7 23 • 0 8 53–11 05 ▽ 1 4 33…42 . 19 50–21 10 . = 0 00–11 30 . np
Σ	–	61.6	–	–	UWAGI.

Sierpień – Août

1	7	.	.	–	= 0 00–10 30 . ⌒ 0 21 00–24
2	7	.	.	–	= 2 00–11 30 . ⌒ 0-2 0 00–11 00
3	7	0.4	.	–	• 0 20 02–20 25–22 46 . = 3 50–10 45 . 20 10–24 . ⌒ 0 2 00–10 00
4	7	0.0	.	–	• 0 19 55–20 25 . = 0 00–7 45
5	7	.	.	–	⌒ 0 23 00–24
6	7	.	.	–	= 0 50–7 15 . ⌒ 0-2 0 00–10 00 ⌒ 0 23 00–24
7	7	0.7	.	–	⌒ 0-1 0 00–10 00
8	7	4.6	.	–	• 0 4 48–5 35 5 58–7 55 10 30 ▽ 1-0 20 57–21 40 . ↖ 0 20 57–21 25 (↖) 0–22 40 SSE-NE . = na–a , np
9	7	10.0	.	–	(↖) 0 23 35–24 SSE-NNE . = 0 00–12 30
10	7	.	.	–	▽ 0 0 55–2 10 2 58–3 40 • 1–5 25 . (↖) 0 0 00–1 40 SSE-NNE ↖ 0 2 55–3 30 ↖ 1–5 42 S-NNE ▽ 0-1 2 58–5 25 . = na–a
11	7	0.0	.	–	▽ 0 16 27–29 (↖) 0 16 20–45 NW-NE . = 0 00–8 15 22 20–24 . ⌒ 0-1 np
12	7	19.5	.	–	▽ 0 10 24–26 13 42–20 32 ▽ 2-0 21 07 ▽ 0-1 21 23–22 27 (↖) 0 18 45–22 46 . = 0 00–a . np . ⌒ 1 0 00–10 24
13	6	11.2	.	–	▽ 0 0 15–1 10 • 0 1 15–4 20 5 30 • 0–6 15 7 10 • 0-1 12 10 • 0 18 50 . = 0 00–24
14	7	.	.	–	= 0 00–9 15 22 30–24 . ⌒ 1 21 00–24
15	7	0.4	.	–	▽ 0 13 55–14 07 . = 0 00–9 30 . 20 15–24 . ⌒ 0-2 0 00–11 00
16	7	.	.	–	= 0 00–9 20 21 10–24 . ⌒ 0 20 00–24
17	7	.	.	–	= 0 00–6 45 . ⌒ 0-1 0 00–10 00 ⌒ 0 21 00–24
18	7	.	.	–	= 4 30–8 45 . ⌒ 0 0 00–9 00
19	7	0.0	.	–	▽ 0 10 50–11 05 • 0 23 49–24 . ≫ 10 35–11 15 . 16 05–17 20 . = 9 30–13 15
20	7	2.8	.	–	• 0 0 00…37 ▽ 0 13 12–21 18 = 1 30–8 10
21	7	.	.	–	≫ 13 15–14 40 . = 1 30–13 15 .
22	7	2.2	.	–	▽ 0-1 21 42–55 ▽ 0 21 57–22 40 . ↖ 0 21 55–23 10 S-E-N . ⌒ 0 5 00–8 00
23	7	0.8	.	–	• 0 4 40–5 05 ▽ 0 13 38–19 48 . = 0 30–9 15
24	7	.	.	–	
25	6	0.6	.	–	= 2 20–14 38 . 22 40–24 . ⌒ 0 2 00–4 00 . ⌒ 22 50–23 30
26	6	1.3	.	–	• 0 6 50–7 12–8 40 • 0 15 46–16 03 . = 0 00–24
27	7	.	.	–	▽ 0 6 28–34 . = 0 00–11 15 . ⌒ 0-1 21 00–24
28	7	.	.	–	= 7 15–10 40 . ⌒ 1-0 0 00–10 00
29	7	.	.	–	⌒ 0 3 00–10 00
30	7	.	.	–	= 4 30–8 30 . ⌒ 0-1 3 00–10 00 ⌒ 0 21 00–24
31	7	.	.	–	⌒ 0-1 0 00–10 00 . 20 00–24
Σ	–	54.5	–	–	UWAGI.

Sandomierz $\varphi = 50°41'$ $\lambda = 21°45'$ **Wrzesień – Septembre 1961**

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	106.5	105.8	105.1	105.1	14.1	25.4	18.3	19.0	26.9	11.5	89	44	72	68	1.8	18.3	5.8	8.6	0 ⊙	1 ⊙	0	NNW 1	WSW 1	WSW 1
2	101.5	99.5	96.4	99.1	15.2	27.1	21.0	20.6	28.3	11.4	95	48	58	67	0.7	18.7	10.5	10.0	1 ⊙	0 ⊙	0	C 0	SW 3	SW 1
3	94.4	92.8	89.8	92.3	14.2	27.3	19.1	19.9	28.4	13.0	86	36	65	62	2.4	23.3	7.7	11.1	0 ⊙	0 ⊙	0	SW 3	SSW 5	SW 1
4	88.4	88.8	90.9	89.4	14.6	18.2	17.0	16.7	24.6	12.6	76	73	99	85	4.0	5.6	0.2	3.3	3 ⊙	10 •	7	WSW 3	WNW 4	WNW 1
5	91.3	91.0	88.4	90.2	15.3	18.5	17.8	16.8	23.5	11.8	99	86	94	93	0.2	2.9	1.2	1.4	0	10	0	C 0	SE 1	SSE 1
6	85.2	84.4	85.5	85.0	15.7	25.8	17.4	19.1	26.5	13.9	82	42	90	71	3.2	19.4	2.1	8.2	7 ⊙	9 ⊙	0	SE 2	WSW 7	WSW 1
7	84.7	84.5	85.6	84.9	15.1	23.4	16.2	17.7	24.9	14.4	100	53	85	79	0.0	13.5	2.7	5.4	10 •	6 ⊙	10	SW 1	SW 6	WSW 4
8	87.0	87.6	88.4	87.7	12.2	16.4	13.3	13.8	17.3	11.5	80	48	69	66	2.9	9.6	4.8	5.8	1 ⊙	8	10	WSW 5	W 7	W 6
9	89.6	91.2	91.5	90.8	11.4	15.0	13.3	13.2	16.8	10.8	94	64	85	81	0.9	6.0	2.3	3.1	10	10	0	W 4	NW 4	W 2
10	92.3	93.8	94.7	93.6	11.4	13.8	12.0	12.3	15.8	10.8	88	75	84	82	1.7	3.9	2.2	2.6	10	10	10	W 3	NW 5	WNW 3
11	94.3	94.7	94.1	94.4	11.0	14.0	12.2	12.4	15.0	10.4	96	71	86	84	0.5	4.6	2.0	2.4	10	10	10	W 2	W 4	WSW 2
12	92.8	91.6	90.7	91.7	10.2	18.8	15.6	15.0	20.0	9.1	88	49	68	68	1.4	11.2	5.7	6.1	9	6 ⊙	10	WSW 3	SW 6	WSW 5
13	92.0	93.1	94.0	93.0	12.0	17.1	14.6	14.6	19.0	11.3	95	68	79	81	0.7	6.2	3.4	3.4	10	9	10	SW 2	W 2	NW 1
14	91.7	90.2	89.2	90.4	12.3	22.4	16.8	17.1	22.7	11.3	90	51	85	75	1.4	13.2	2.9	5.8	9	10	0	C 0	SW 5	WSW 1
15	90.1	94.9	98.2	94.4	15.6	17.4	11.6	14.0	18.6	11.1	85	60	84	76	2.6	7.9	2.1	4.2	5	6 ⊙	1	WSW 7	NW 6	W 4
16	99.4	99.2	99.2	99.3	11.8	19.5	17.9	16.8	23.4	8.9	87	64	78	76	1.8	8.3	4.4	4.8	10	7 ⊙	1	WSW 3	WSW 4	W 1
17	100.5	100.2	99.1	99.9	12.1	25.8	19.7	19.3	27.9	10.8	99	49	72	73	0.1	16.8	6.3	7.7	0 ≡	0 ⊙	0	S 1	SSW 3	S 1
18	98.7	97.2	96.5	97.5	13.0	27.5	21.0	20.6	28.7	11.0	99	35	77	70	0.2	25.8	5.8	9.9	3 ⊙	3 ⊙	0	SW 1	WSW 7	NW 2
19	98.1	97.9	98.4	98.1	16.2	21.7	12.7	15.8	22.2	12.7	90	30	69	65	1.7	18.1	4.6	8.1	9	0 ⊙	0	NNE 4	NNW 3	N 3
20	99.7	100.0	100.3	100.0	7.7	17.9	10.7	11.8	18.7	6.4	95	49	76	73	0.7	10.3	3.1	4.8	0 ⊙	1 ⊙	0	NW 3	NE 3	NE 3
21	101.5	101.9	103.3	102.2	8.0	16.6	8.3	10.3	17.4	6.3	89	42	75	69	1.2	11.1	2.8	5.0	0 ⊙	0 ⊙	0	NE 1	ENE 3	NNE 1
22	105.0	105.4	106.2	105.5	5.5	15.9	8.2	9.4	17.4	3.7	75	44	66	62	2.2	10.2	3.7	5.4	0 ⊙	0 ⊙	0	NE 1	ENE 3	E 1
23	105.8	104.2	102.1	104.0	5.4	17.2	9.8	10.6	18.4	2.8	60	31	59	50	3.6	13.5	4.9	7.3	0 ⊙	1 ⊙	0	E 3	ENE 4	ENE 2
24	100.5	100.2	99.3	100.0	5.0	19.6	13.7	13.0	21.7	4.1	83	39	63	62	1.5	14.0	5.9	7.1	0 ⊙	2 ⊙	0	E 1	S 3	SSW 1
25	98.9	98.4	98.0	98.4	5.5	22.6	14.4	14.2	23.6	4.3	89	33	65	62	1.0	18.4	5.8	8.4	0 ⊙	0 ⊙	1	SSW 1	SSW 3	SW 2
26	100.0	99.9	97.8	99.2	12.6	16.7	15.6	14.1	18.0	11.0	92	72	79	81	1.2	5.4	3.4	3.3	9	9 ⊙	10	NW 3	WNW 1	WSW 1
27	95.8	95.0	95.5	95.4	9.4	17.3	12.0	12.7	17.7	8.8	89	66	84	80	1.3	6.7	2.2	3.4	8	8	9	NE 1	N 2	NNE 1
28	96.9	97.3	98.8	97.7	6.4	18.1	10.2	11.2	18.9	5.3	97	46	73	72	0.3	11.3	3.3	5.0	0 ⊙	2 ⊙	2	NNW 1	E 1	ENE 1
29	99.4	98.8	98.3	98.9	6.8	18.0	10.4	11.4	19.0	5.9	88	46	72	69	1.2	11.0	3.5	5.2	6 ⊙	1 ⊙	0	E 2	SE 3	ENE 1
30	98.8	96.9	96.9	97.5	7.8	17.2	10.6	11.6	18.5	6.4	90	47	74	70	1.1	10.4	3.4	5.0	9	9	9	E 2	SE 3	E 3
31																								
M	96.0	95.9	95.7	95.9	11.0	19.7	14.3	14.8	21.3	9.4	89	52	76	72	1.4	11.8	4.0	5.7	4.6	4.9	3.3	2.1	3.8	2.0

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1	97.9	98.6	100.0	98.8	6.3	11.8	11.1	10.1	13.0	5.2	95	73	88	85	0.4	3.8	1.6	1.9	10	9	10	ENE 4	ENE 6	NE 4
2	101.8	103.2	104.1	103.0	10.8	15.5	12.0	12.6	17.0	9.2	89	64	73	75	1.5	6.4	3.8	3.9	10	8	0	ENE 4	E 6	NE 4
3	105.1	104.6	104.8	104.8	7.2	17.9	11.0	11.8	18.6	6.6	93	51	79	74	0.8	10.1	2.7	4.5	0 ⊙	3 ⊙	0	NE 2	E 6	E 3
4	105.0	104.1	103.5	104.2	7.6	19.2	11.3	12.4	19.8	6.9	97	40	63	67	0.3	13.2	5.0	6.2	0 ⊙	1 ⊙	0	E 3	SE 7	E 3
5	103.6	103.0	103.3	103.3	6.9	18.8	10.9	11.9	20.0	6.2	87	42	65	65	1.3	12.6	4.6	6.2	0 ⊙	0 ⊙	0	E 2	ESE 3	SE 3
6	102.9	101.4	98.7	101.0	6.0	19.0	10.0	11.2	19.7	5.2	88	47	72	69	1.2	11.6	3.5	5.4	0	0 ⊙	0	E 1	E 4	E 3
7	96.0	93.5	91.8	93.8	5.6	17.2	12.0	11.7	17.6	5.1	86	45	54	61	1.3	11.2	6.5	6.5	0 ⊙	0 ⊙	4	E 2	SE 5	SE 6
8	90.7	89.7	91.5	90.6	5.6	16.5	10.3	10.7	17.3	5.4	78	44	63	62	2.0	10.6	4.7	5.8	4 ⊙	3 ⊙	3	ESE 5	ESE 5	SE 2
9	97.1	100.6	104.6	100.8	4.8	17.4	11.4	11.2	17.8	4.2	95	61	86	81	0.4	7.7	1.8	3.3	2	3 ⊙	10	ESE 2	NW 2	NNW 3
10	107.0	107.8	107.4	107.4	7.5	14.8	12.0	11.6	15.7	6.4	96	71	91	86	0.5	4.8	1.2	2.2	8	9	10	NNW 3	N 2	SE 2
11	106.1	104.9	103.7	104.9	5.3	17.6	9.0	10.2	18.3	4.8	95	45	64	67	0.4	11.4	4.1	5.3	0	0 ⊙	0	E 2	E 5	E 1
12	102.4	101.4	100.9	101.6	3.1	17.4	11.2	10.7	18.2	2.7	68	55	84	69	2.5	9.0	2.1	4.5	0	2 ⊙	0	SE 1	SE 2	NW 3
13	101.6	102.4	102.7	102.2	9.8	15.0	7.0	9.7	15.2	6.8	81	53	85	73	2.3	7.9	1.4	3.9	9	6 ⊙	2	E 4	NNW 3	NW 3
14	101.3	100.2	98.6	100.0	6.0	10.2	8.2	8.2	10.4	4.8	94	64	96	85	0.6	4.5	0.5	1.9	10	10	10	NW 3	WNW 3	W 4
15	99.6	99.6	98.0	99.1	9.6	11.4	9.9	10.2	12.0	8.1	99	88	84	90	0.2	1.7	1.9	1.3	9	10	10	NW 2	WNW 2	WSW 4
16	96.9	96.1	95.4	95.5	8.6	10.8	7.0	8.4	12.9	7.0	82	70	93	82	2.0	3.9	0.7	2.2	10	10	1	WNW 4	W 3	S 1
17	91.1	87.7	82.2	87.0	4.2	13.9	10.8	9.9	16.0	3.9	97	66	81	81	0.2	5.4	2.5	2.7	2 ≡	9	1	SW 1	SSW 4	S 2
18	74.4	73.8	73.0	74.4	13.9	15.9	15.1	15.0	17.0	8.5	58	44	49	50	6.7	10.2	8.8	8.6	9 •	10	10	SSW 3	S 6	SE 4
19	76.3	78.3	81.7	78.8	14.0	21.6	16.1	17.0	23.3	12.3	52	41	61	51	7.7	15.3	7.2	10.1	10	3 ⊙	0	SE 6	SE 6	SE 4
20	85.3	86.2	86.8	86.1	9.3	20.8	13.9	14.3	21.1	9.3	92	55	85	77	1.0	11.2	2.3	4.8	1 ⊙	0 ⊙	0	E 4	E 5	E 2
21	89.2	91.8	96.7	92.6	10.7	16.1	9.2	11.3	17.5	8.9	92	63	92	82	1.0	6.9	0.9	2.9	9	7 ⊙	1	ESE 3	SE 7	SSE 2
22	98.5	100.7	101.9	100.4	9.2	10.4	7.6	8.7	10.8	7.3	93	76	65	78	0.8	3.0	3.6	2.5	10	10	8	SE 1	SE 3	ESE 3
23	102.9	102.9	102.9	102.9	3.2	12.2	8.2	8.0	13.2	2.9	76	54	62	64	1.9	6.3	4.2	4.2	4	6 ⊙	2	E 3	SE 2	SE 4
24	103.3	102.7	100.8	102.3	1.8	15.8	9.4	9.1	16.8	1.7	87	49	78	71	0.9	9.1	2.6	4.2	4 ⊙	5 ⊙	10	SE 3	SW 3	S 2
25	98.8	97.0	97.0	97.6	3.6	16.0	8.8	9.3	17.3	3.2	93	48	78	73	0.3	9.6	2.4	4.2	2 ⊙	3 ⊙	8	SSE 2	S 3	S 3
26	95.5	95.0	94.1	94.9	5.0	13.7	8.8	9.1	14.5	4.6	89	54	73	72	1.0	7.2	3.0	3.7	7	9	1	S 3	S 3	SSW 1
27	92.5	91.3	90.5	91.5	4.4	15.7	10.6	10.3	16.2	4.2	80	54	48	54	1.7	11.8	6.7	6.7	9	9	3	SSW 1	SSW 7	SSW 2
28	90.6	90.0	88.6	89.7	4.9	19.2	11.3	11.7	19.8	4.7	67	38	59	55	2.9	13.7	5.4	7.3	0 ⊙	0 ⊙	0	E 2	SE 3	C 0
29	88.1	87.3	89.4	88.3	4.0	14.6	10.8	10.0	16.4	2.9	95	60	96	85	0.3	6.7	0.3	2.6	3	8	10	SSE 1	S 2	WSW 4
30	93.2	93.2	94.1	93.5	8.6	10.2	8.9	9.2	10.9	8.3	92	82	89	88	1.0	2.2	1.2	1.5	10	10	10	WNW 1	WSW 1	NNW 1
31	94.9	95.8	96.2	95.6	7.2	11.4	7.4	8.4	12.3	6.8	97	79	90	89	0.3	2.8	1.0	1.4	10 •	6 ⊙	0	NW 1	SW 3	SW 3
M	96.4	96.3	96.3	96.3	6.9	15.4	10.4	10.8	16.4	6.0	86	57	76	73	1.3	8.1	3.2	4.3	5.2	5.3	4.0	2.6	4.1	2.8

Sandomierz $H_s = 202\ m$ $H_b = 200{,}3\ m$ $h_w = 20{,}1\ m$ **Wrzesień – Septembre 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	⌒ 1 0⁰⁰–9⁰⁰ ⌒ ° 20⁰⁰–24
2	7	.	.	–	⌒ 0-1 0⁰⁰–9⁰⁰
3	8	.	.	–	⌒ ° 2⁰⁰–8⁰⁰
4	7	1.2	.	–	⌒ ●▽ 0-1 13⁰¹–43 , (↖) 13³² E ; = 21⁴⁵–24 , ⌒ ° 2¹⁰⁰–23⁰⁰
5	5	0.0	.	–	● ° 11¹⁸…⁴⁵ = 0⁰⁰–8³⁰ ≡ ° –9⁵⁰ = –24 , ⌒ ¹ 0⁰⁰–8³⁰ ⌒ ° 21⁰⁰–24
6	7	0.0	.	–	= 0⁰⁰ 24 , ⌒ 0-1 0⁰⁰–10⁰⁰
7	7	1.1	.	–	● ° 6⁴⁵…⁵⁸ 7³² 8⁰² ●▽ 19¹⁵–⁵⁰ , 20³⁷–⁴⁴ , = 0⁰⁰–7³⁰ ≡ ° –8⁴⁰ = a, np ⌒ ° na
8	7	0.0	.	–	●▽ 14⁰⁵–¹⁵ » 10⁰⁵–13¹⁵ = 0⁰⁰–7¹⁵
9	7	0.0	.	–	●▽ ° 3⁰³–⁰⁵ , = 7¹⁵–12¹⁵
10	7	0.0	.	–	● ° 4⁴⁵ 5⁰³ 8⁴⁰ 9³⁸ ●▽ ° 14³⁸–⁴² , = 8⁴⁰–11⁵⁰
11	7	.	.	–	● ° 5⁵⁰ 6⁴⁰ , = 0³⁰–10³⁰ , 21¹⁵–24
12	7	0.0	.	–	● ° 23¹³…⁴⁰ , = 0⁰⁰–9¹⁵ , 20³⁰–24 , ⌒ ° 1⁰⁰–8⁰⁰
13	7	0.0	.	–	● ° 9⁴⁰ 10⁴² , = 0⁰⁰–13²⁰ , ⌒ ° 3⁰⁰–8⁰⁰
14	7	6.4	.	–	= 4¹⁰–10⁵⁰
15	7	.	.	–	●▽ 0-1 0¹⁵ 1⁰⁵ ●▽ ° 2⁴⁷–3¹⁰ , (↖) ° 0¹⁵–⁵⁰ E–SSE , ⌒ 21⁰⁰–24
16	7	.	.	–	= 6³⁰–10⁵⁰ , 22¹⁵–24 , ⌒ 0-1 0⁰⁰–9⁰⁰ 21⁰⁰–24
17	7	.	.	–	= 0⁰⁰–4⁴⁵ ≡ 0-1 7⁵⁰ = –9¹⁵ , ⌒ ° 0⁰⁰–4⁰⁰ ⌒ ° 21⁰⁰–24
18	8	.	.	–	= 4⁵⁰–10³⁰ , 23³⁰–24 , ⌒ 0-2 0⁰⁰–10⁰⁰ ⌒ ° 22⁰⁰–24
19	7	.	.	–	= 0⁰⁰–9⁵⁰ , ⌒ 0-1 0⁰⁰–9⁰⁰ ⌒ ° 21⁰⁰–24
20	7	.	.	–	= 5³⁰–9⁵⁰ ⌒ 0-1 0⁰⁰–10⁰⁰
21	7	.	.	–	⌒ 0-1 6⁰⁰–10⁰⁰ ⌒ ° 21⁰⁰–24
22	7	.	.	–	⌒ 0-1 0⁰⁰–10⁰⁰ ⌊ ° 6⁰⁰–7⁰⁰
23	7	.	.	–	⌊ ° 5⁰⁰–7⁰⁰
24	7	.	.	–	⌒ ° 22⁸⁰–24
25	7	0.6	.	–	= 1³⁰–10⁵⁰ , ⌒ 0-1 0⁰⁰–10⁰⁰
26	6	.	.	–	●▽ ° 3⁴²–⁴⁷ , = 0³⁰–24
27	7	.	.	–	= 0⁰⁰–13¹⁵ 20¹⁵–24 , ⌒ ° 20⁰⁰–24
28	7	.	.	–	= 0⁰⁰–11⁶⁰ , ⌒ 0-2 0⁰⁰–10⁰⁰ ⌒ ° 21⁰⁰–24
29	7	.	.	–	⌒ 0-1 0⁰⁰–11⁰⁰ , ▽ 2⁴⁰–5³⁰
30	7	.	.	–	= 0⁰⁰–9³⁰ , ⌒ ° 6⁰⁰–9⁰⁰
31					
Σ	–	9.3	–	–	UWAGI.

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1	6	.	.	–	= 4¹⁵ 15⁶⁰ , ⌒ 0-1 2⁰⁰–8⁰⁰
2	6	.	.	–	= 1⁵⁰–12⁴⁰
3	7	.	.	–	= 3³⁰–9¹⁵ , ⌒ ° 2⁰⁰–8⁰⁰ 21⁰⁰–23⁰⁰
4	7	.	.	–	= 0³⁰–9³⁰ , ⌒ 1-2 0⁰⁰–9⁰⁰
5	7	.	.	–	= 5³⁰–10¹⁵ , ⌒ ° 5⁰⁰–9⁰⁰
6	7	.	.	–	⌒ ° 2⁰⁰–8⁰⁰
7	7	.	.	–	= 5⁵⁰–9³⁰
8	7	.	.	–	= 3³⁰–6²⁰
9	7	.	.	–	= 3⁴⁰–8⁵⁰ 21¹⁵–24 , ⌒ ° 5⁰⁰–8⁰⁰ , 21⁰⁰–23⁰⁰
10	6	.	.	–	= 0⁰⁰–24 , ⌒ 1-2 0⁰⁰–9⁰⁰
11	7	.	.	–	= 0⁰⁰–9⁴⁵ , ⌒ 0-2 2⁰⁰–11⁰⁰
12	7	.	.	–	= 21⁴⁰–24 , ⌒ ° 22⁰⁰–24
13	7	.	.	–	= 0⁰⁰–9³⁰ , ⌒ ° 0⁰⁰–4⁰⁰
14	7	4.0	.	–	● ° 12⁴⁰ 13³⁰–16¹⁰ 18³⁸ ● ° 21⁵⁰–22¹³ ● ° –22⁴⁵ , = na – a, p – 24
15	6	0.4	.	–	● ° 0⁴⁷–1¹⁰ ● ° 8⁴⁵ 9¹⁰ ●▽ 12³⁵–⁴¹ = 0⁰⁰–24
16	7	.	.	–	= 0⁰⁰–9⁵⁰ , 18³⁰–24 , ⌒ ° 20⁰⁰–24
17	6	0.1	.	–	= 0⁰⁰–6¹⁰ ≡ 1-0 7²⁰ = –24 , ⌒ ° 0⁰⁰–6¹⁰
18	7	.	.	–	● ° 3⁵⁰ 6³⁵ , = 0⁰⁰–6³⁵
19	7	.	.	–	
20	7	.	.	–	= 5³⁰–9⁵⁰ , ⌒ ° 1⁰⁰–8⁰⁰
21	7	.	.	–	= 20³⁰–24 , ⌒ ° 20⁰⁰–24
22	6	.	.	–	= 0⁰⁰–13¹⁰ , ⌒ ° 0⁰⁰–8⁰⁰ , ▽ 19³⁵–20⁴⁵
23	7	.	.	–	⊕ 11⁴⁰–12¹⁰
24	7	.	.	–	= 5³⁰–8³⁰ , ⌒ 1⁰⁰–9⁰⁰ , ▽ 18⁴⁵–24
25	7	.	.	–	= 22⁰⁰–24 , ⌒ ° 4⁰⁰–9⁰⁰ , ▽ 0⁰⁰–2³⁰
26	7	.	.	–	= 4³⁰–12¹⁵ , ⌒ ° 0⁰⁰–9⁰⁰ , ▽ 3⁴⁵–4²⁰ ⊕ 11²⁰–12¹⁰
27	7	.	.	–	⌒ ° 4⁰⁰–9⁰⁰ , ▽ 0³⁵–5¹⁵
28	7	.	.	–	
29	7	0.8	.	–	● ° 14⁵² 15⁴⁵–16³⁰ 17¹⁰–18⁴⁰ 19¹⁷…³⁴ , 21³⁰ 22²⁵ , = 6¹⁰–12¹⁵ , p – 24 ⌒ ° 6⁰⁰–10⁰⁰
30	7	4.9	.	–	● ° 22⁴⁵–24 , = 0⁰⁰–12²⁰ , 17³⁰–24
31	7	0.5	.	–	● ° 0⁰⁰–7²⁵ , = 0⁰⁰–10⁴⁵ , 16³⁰–24
Σ	–	30.7	–	–	UWAGI.

Sandomierz — $\varphi = 50°41'$ — $\lambda = 21°45'$ — Listopad – Novembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	97.6	98.3	98.5	98.1	7.6	12.6	8.3	9.2	13.1	5.8	84	56	92	77	1.6	6.5	1.0	3.0	9	9	10 •	SW 6	WSW 7	SW 6
2	100.9	100.2	96.0	99.0	6.1	10.6	5.5	6.9	12.1	5.2	92	67	91	85	0.7	4.3	0.8	1.9	6	6	0	WSW 3	WSW 3	SSW 2
3	89.9	87.5	87.5	88.3	5.2	14.3	6.8	8.3	14.5	3.6	92	44	81	72	0.7	9.2	1.9	3.9	7	6 ⊙	0	SW 1	SW 7	SW 2
4	85.9	86.0	85.6	85.8	3.4	6.4	4.8	4.8	7.1	3.4	95	91	95	93	0.5	0.9	0.4	0.6	5	10 •	10 •	SSW 1	C 0	W 8
5	85.1	84.7	90.1	86.0	4.4	6.3	4.0	4.7	6.8	3.6	98	97	100	98	0.2	0.2	0.0	0.1	10 ⁹	10 •	10 =	NNE 5	NE 3	SSE 1
6	89.6	88.7	87.8	88.7	7.0	10.5	10.0	9.4	10.8	3.9	100	94	99	98	0.0	0.8	0.2	0.3	10	10	10 ⁹	NNE 2	ENE 4	ESE 4
7	85.4	85.4	86.1	85.6	10.8	11.8	9.2	10.2	12.2	9.1	89	80	88	86	1.5	2.8	1.4	1.9	10	10	10	E 3	SE 5	E 3
8	84.4	86.3	87.0	85.9	8.0	8.0	6.8	7.4	9.6	6.6	97	92	99	96	0.3	0.9	0.2	0.5	10 ⁹	10	10 ⁹	SE 2	SW 2	SW 1
9	86.7	86.1	85.5	86.1	5.6	9.5	4.1	5.8	10.0	3.9	92	69	95	85	0.7	3.7	0.4	1.6	10	7 ⊙	0	S 2	SSW 6	S 2
10	82.7	83.3	84.1	83.4	4.4	10.4	8.8	8.1	10.5	2.7	97	83	90	90	0.3	2.1	1.1	1.2	8	10	10	SE 1	SSE 3	SSE 3
11	85.2	84.4	86.4	84.7	7.0	7.6	7.8	7.6	9.0	6.9	96	96	93	95	0.4	0.4	0.8	0.5	10 •	10 •	10	SE 3	SE 5	SE 2
12	85.7	87.2	89.2	87.4	6.6	7.8	7.2	7.2	8.2	6.4	96	96	96	96	0.4	0.5	0.5	0.5	10 •	10	10	ESE 3	ESE 2	E 2
13	89.2	87.6	85.0	87.3	6.6	5.8	7.3	6.8	7.7	5.2	98	92	97	96	0.1	0.7	0.3	0.4	10 ⁹	10	10 •	ESE 5	E 5	E 4
14	78.7	84.3	91.8	84.9	9.4	3.8	0.1	3.4	9.6	0.0	93	88	94	92	0.8	0.9	0.4	0.7	10 •	10 •	10	SW 4	WNW 5	NW 3
15	93.6	94.8	96.0	94.8	-0.5	-0.9	-0.6	-0.6	0.2	-1.4	90	93	93	92	0.6	0.4	0.4	0.5	10	10 ⁹	10	N 2	NNE 3	W 2
16	96.0	94.8	92.3	94.4	-0.1	0.5	0.9	0.6	1.1	-0.9	92	84	96	91	0.5	1.0	0.2	0.6	10	10	10	SW 2	SW 2	WSW 2
17	88.6	86.7	86.9	87.4	0.9	3.4	4.4	3.3	4.5	0.6	85	83	89	86	1.0	1.5	1.0	1.2	10	10	10	WSW 6	W 7	W 4
18	85.5	85.2	86.6	85.8	3.1	3.7	1.5	2.4	5.1	1.0	86	85	91	87	1.0	1.2	0.6	0.9	10	9	5	W 6	W 5	W 4
19	89.1	90.9	97.7	92.6	0.4	2.4	-0.1	0.6	2.6	-0.4	90	84	67	80	0.6	1.2	2.0	1.3	10	10 *	9	W 5	WNW 6	N 6
20	103.8	107.1	111.8	107.6	-1.9	0.1	-2.4	-1.6	0.7	-2.7	81	71	82	78	1.0	1.8	0.9	1.2	10	8 ⊙	2	NW 3	NNW 4	WNW 3
21	111.2	109.0	105.3	108.5	-5.0	0.3	-1.1	-1.7	1.1	-5.5	90	77	77	81	0.4	1.4	1.3	1.0	4	10 ⊙	10	SW 2	WSW 3	SW 4
22	101.8	100.4	98.2	100.1	-4.5	2.8	0.0	-0.4	4.0	-5.0	88	62	78	76	0.5	2.9	1.3	1.6	3	1 ⊙	0	SW 1	SSW 2	WSW 3
23	95.4	95.8	92.3	95.8	-5.1	1.7	-1.9	-1.8	3.7	-5.7	88	70	79	79	0.5	2.0	1.1	1.2	0	1 ⊙	1	SW 3	SSW 3	S 2
24	93.7	94.3	95.5	94.5	-5.0	1.7	1.2	-0.2	3.1	-5.6	90	69	81	80	0.4	2.1	1.3	1.3	0	6 ⊙	9	SW 1	SW 2	SW 4
25	94.1	92.9	91.7	92.9	0.2	1.6	0.8	0.8	2.0	-1.2	92	96	94	94	0.5	0.3	0.4	0.4	9	10	10	E 2	ESE 1	SW 2
26	90.3	88.6	86.1	88.3	0.8	6.4	1.6	2.6	6.7	0.1	98	82	98	93	0.2	1.7	0.2	0.7	10	1 ⊙	0	SW 1	SSE 1	SE 1
27	81.5	79.0	78.5	79.7	2.7	6.2	7.4	5.9	9.0	1.3	95	92	93	93	0.4	0.7	0.8	0.6	8	10	10	SSE 2	SSE 2	SW 3
28	85.8	86.5	91.0	87.1	5.0	4.7	3.6	4.2	7.6	3.3	95	94	97	95	0.4	0.5	0.3	0.4	10	10	10	W 2	SW 2	ESE 1
29	95.3	92.8	95.3	93.1	3.4	4.4	3.6	3.8	5.7	3.0	97	95	88	93	0.3	0.5	0.9	0.6	10	10	2	SE 1	SSE 2	WSW 2
30	88.0	87.6	84.4	86.7	-0.5	4.6	3.0	2.5	5.6	-1.4	94	74	83	84	0.4	2.2	1.3	1.3	5	6	9	C 0	SW 4	SW 3
31																								
M	90.4	90.3	90.9	90.6	2.9	5.6	3.8	4.0	6.8	1.5	92	82	90	88	0.6	1.8	0.8	1.1	8.1	8.3	7.2	2.7	3.5	3.0

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1	77.0	76.6	78.7	77.4	6.5	9.2	9.6	8.7	10.3	2.7	75	72	74	74	2.5	3.2	3.2	3.0	10	9	10	SW 10	WSW 9	SW 7
2	77.1	74.4	75.9	75.8	7.2	12.2	9.4	9.6	13.0	6.5	78	66	71	72	2.2	4.8	3.4	3.5	2	8	9	SW 5	SW 6	SW 6
3	87.2	88.6	87.0	87.6	0.8	5.0	3.0	3.0	9.6	0.1	85	64	77	75	1.2	3.1	1.7	2.0	2	4 ⊙	2	SW 4	SW 3	SSW 1
4	85.3	85.0	90.6	86.4	4.5	9.4	8.8	7.9	11.1	1.1	87	78	86	84	1.1	2.6	1.5	1.7	10 •	10	10	SSW 3	SW 5	WSW 2
5	88.6	88.2	87.1	88.0	10.2	14.4	9.0	10.6	14.9	7.1	81	69	86	79	2.4	5.1	1.6	3.0	10 •	9	0	SW 5	SW 7	SW 2
6	85.7	86.9	90.8	87.8	9.4	2.8	0.2	3.2	10.9	0.0	91	91	98	93	1.1	0.7	0.1	0.6	10	10 •	10 *	SW 2	W 9	NW 3
7	88.4	88.2	90.9	89.2	-0.2	0.0	-0.3	-0.2	0.6	-0.6	98	96	98	97	0.1	0.2	0.2	0.2	10 *	10 *	10 *	N 1	N 4	N 3
8	93.1	94.3	95.8	94.4	-1.9	-1.1	-1.9	-1.7	0.1	-3.9	90	81	87	86	0.5	1.0	0.7	0.7	10	10	10	NW 2	WNW 1	W 2
9	97.1	97.9	96.6	97.2	-4.1	-6.1	-4.5	-4.8	-1.5	-9.7	89	92	91	91	0.5	0.3	0.4	0.4	7	5 =	10	WSW 3	C 0	SE 1
10	95.1	91.9	90.8	91.9	-6.1	-1.6	-1.9	-2.9	-0.9	-7.3	92	82	92	89	0.3	1.0	0.4	0.6	10	4 ⊙	10	SE 1	SE 2	SE 2
11	86.5	80.9	72.3	79.9	-0.6	1.4	0.8	0.6	1.6	-2.1	92	85	96	91	0.4	1.0	0.3	0.6	8	10	10	SSW 2	SSW 4	SSW 7
12	76.8	82.0	86.2	81.7	0.9	0.7	0.2	0.5	2.7	-0.1	98	96	96	97	0.1	0.2	0.3	0.2	10	10	10	NW 3	NNW 3	N 2
13	94.0	98.4	102.2	98.2	-5.2	-5.1	-7.0	-5.6	0.3	-7.0	85	66	72	74	0.8	1.4	1.0	1.1	10	3 ⊙	0	NNE 6	N 5	N 5
14	102.0	100.2	99.7	100.6	-10.7	-7.5	-9.3	-9.2	-6.5	-11.5	80	51	70	67	0.5	1.7	0.9	1.0	0	1	9	NW 3	NNW 8	NNW 8
15	94.5	93.8	98.6	95.6	-8.7	-11.7	-14.1	-12.2	-8.4	-15.0	83	82	83	83	0.5	0.4	0.3	0.4	10 *	9	5 ↔	NW 6	NNE 6	N 5
16	106.5	111.4	116.9	111.6	-17.1	-13.7	-16.1	-15.8	-13.0	-17.7	90	75	81	79	0.3	0.5	0.3	0.4	1	0	0	NE 4	NNE 3	NNW 2
17	117.8	115.7	113.8	115.8	-18.7	-11.3	-8.7	-11.8	-8.5	-19.5	84	90	83	86	0.2	0.3	0.5	0.3	8	10 *	10	NW 4	NW 4	N 4
18	112.5	111.7	110.3	111.5	-5.0	-5.9	-4.2	-4.3	-5.6	-9.5	88	87	82	86	0.5	0.6	0.8	0.6	10	10 ⁂	10	N 4	NNW 4	WNW 3
19	107.2	105.5	103.5	105.4	-5.4	-4.3	-2.4	-3.6	-2.2	-6.0	85	84	91	87	0.6	0.7	0.4	0.6	10	10	10	W 4	WSW 2	NW 4
20	100.3	94.1	86.4	93.6	-1.7	-2.0	-0.2	-1.0	-0.1	-2.8	88	85	90	88	0.7	0.8	0.6	0.7	10	10	10 *	W 5	WSW 7	W 4
21	84.2	84.9	89.5	86.2	-1.5	-2.1	-6.4	-4.1	0.9	-7.6	90	79	83	84	0.5	1.1	0.6	0.7	10 *	8	0	NW 2	NW 10	WNW 6
22	87.7	81.7	83.2	84.2	-11.9	-5.5	-9.3	-9.0	-4.5	-12.7	89	92	85	89	0.3	0.3	0.4	0.3	3	10 *	6	SW 4	SW 4	NW 2
23	87.6	90.4	92.0	90.0	-10.8	-8.3	-15.1	-12.4	-7.6	-15.9	87	77	86	83	0.4	0.7	0.3	0.5	10	0 ⊙	9	NW 2	WNW 2	SW 3
24	94.6	98.3	95.3	94.1	-11.6	-8.6	-14.4	-12.2	-8.1	-15.9	86	74	87	82	0.4	0.8	0.3	0.5	10	9	0	C 0	SW 1	C 0
25	90.8	89.4	88.3	89.5	-18.5	-16.1	-20.9	-19.1	-14.2	-21.0	84	81	82	82	0.2	0.3	0.2	0.2	0	2 ⊙	0	NNE 1	E 2	SSE 1
26	87.7	86.1	84.0	85.9	-25.7	-16.5	-15.1	-18.1	-13.3	-26.4	78	90	86	85	0.2	0.2	0.3	0.2	0	2 ⊙	10	S 2	C 0	SE 1
27	85.9	88.3	90.9	88.4	-11.7	-12.5	-13.2	-12.6	-9.5	-15.1	89	85	84	86	0.3	0.4	0.4	0.4	4	3 ⊙	10	WSW 1	NE 1	NNE 4
28	88.3	86.6	86.9	87.3	-12.3	-7.1	-4.1	-6.9	-4.1	-15.8	85	82	84	84	0.4	0.6	0.7	0.6	10	10	10	NE 4	E 3	E 1
29	87.3	87.7	88.8	87.9	-3.9	-0.1	-5.7	-2.8	0.5	-4.6	92	73	94	87	0.4	1.6	0.3	0.8	10	1 ⊙	10 =	E 1	S 1	S 1
30	86.2	85.9	87.2	86.4	-2.7	0.6	-1.5	-1.3	1.9	-4.5	93	82	91	89	0.3	1.2	0.5	0.7	0	1 ⊙	0	ESE 2	SE 2	SE 2
31	86.3	86.0	83.9	85.4	-1.2	3.2	0.2	0.6	4.7	-2.8	91	86	98	92	0.3	1.1	0.1	0.5	1	9	0 =	SE 3	SE 1	SE 1
M	91.5	91.2	91.7	91.5	-5.0	-2.8	-4.3	-4.1	-0.7	-7.7	87	80	86	84	0.7	1.2	0.7	0.9	7.0	6.7	6.8	3.2	3.8	3.1

Sandomierz $H_s = 202\ m$ $H_b = 200{,}3\ m$ $h_w = 20{,}1\ m$ **Listopad – Novembre 1961**

DNI	WILGOTNOŚĆ %	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.8	.	-	●° 15⁵⁰ 16⁴⁰ 19⁴⁰..50 20²⁰..21⁴⁰ = 0⁰⁰—9⁴⁵, 19⁴⁰—24
2	7	.	.	-	= 0⁰⁰—12¹⁵, 16³⁰—24, ⌒° 22⁰⁰—24
3	7	.	.	-	= 0⁰⁰—9⁵⁰, 22³⁰—24, ⌒ 0-2 0⁰⁰—8⁰⁰, ☋ 4⁵⁰—6⁰⁰
4	6	2.2	.	-	▽°9⁴⁵-⁵⁰, ●° 10⁴⁷..24, = 0⁰⁰—24, ⌒° 2⁰⁰—4⁰⁰
5	5	1.5	.	-	●° 0⁰⁰ 2¹² ●° 5¹⁰—6³⁰ 7⁴⁰ ●° 8⁵⁰ 9⁴⁵ ●° 10⁵⁰ ●° 13⁴⁰, = na, a, p ≡°a, p—24
6	6	0.1	.	-	●° 3⁵⁰ 5¹⁵—6¹⁰, 12⁴³ 13³⁵ 16⁵⁰ 20¹⁵, 20⁵⁰, ≡° 0⁰⁰—2⁴⁰ = —24
7	7	0.5	.	-	●° 21⁴⁵—22¹⁰ ●° 22³⁰—24, = 0⁰⁰—12¹⁵, 18³⁰—24
8	6	0.8	.	-	●° 0-1 7⁰⁰—14⁰, 4⁵⁰—8³⁰ ●° 17⁴⁵ 18¹⁵ ●° 0-1 20¹² 22⁴⁰, = 0⁰⁰—24
9	7	.	.	-	= 0⁰⁰—10³⁰, 21¹⁵—24, ⌒° 21⁰⁰—24
10	6	+ 1.6	.	-	●° 9³⁵ 17⁴⁵, 20⁵⁰ 22³⁰ ●° 23⁴⁰, = 0⁰⁰—24, ⌒° 0⁰⁰—9⁰⁰
11	6	14.0	.	-	●° 1⁴⁵ 6⁴⁰ ●° 0-1 7⁴³ 11¹⁵ 11²⁵—15²⁸, = 0⁰⁰—24
12	6	2.2	.	-	●° 0-1 1⁴⁵—8⁴⁵, = 0⁰⁰—10²⁰, 12³⁰—14²⁸, 19³⁰—24
13	6	17.2	.	-	●° 3²⁰—6⁵², 13³⁵ 14⁴⁵ ●° 16¹⁴—20⁴⁵, 21³⁰—24, = 0⁰⁰—24
14	7	0.9	.	-	●° 0-1 0⁰⁰—2¹⁰ 3³⁰—5²⁰ 7¹⁰ ●° 9²⁰—11⁴⁰ ●°, ●°, ✳° 17⁴⁰, = na, p—24
15	6	0.0	.	-	●° 10⁴⁹ 15⁵⁰, = 0⁰⁰—24
16	6	0.0	.	-	●° 19⁴⁰..20²⁰, 20⁴³ 22⁴⁰, = 0⁰⁰—24
17	6	0.4	.	-	= 0⁰⁰—24
18	7	0.5	.	-	●° 5¹⁵..45 ●° 10¹⁰—39 15²⁵-⁵⁰ ▽° 16³⁵—55, = na, a, p—24
19	7	1.6	.	-	✳ 0-1 ▽ ✳° ▽ ✳° 7⁴⁸ 9⁰⁸ ▽ 0-2 ✳ 12³⁵ ▽° —13¹⁵ ✳ 0-1 13¹⁸—14⁰⁶ ▽° 19⁵⁵—20⁰⁴, = 0⁰⁰—12¹⁵ ⌴ 0-1 na—a
20	7	0.0	1	-	✳° ▽ 5²⁵-⁴⁵ ✳° 7²⁸..⁴⁰ ✳° 18³⁵-⁴² ⌴° 21⁰⁰—24
21	6	.	.	-	= 0¹⁵—24, ⌴ 0-1 0⁰⁰—11⁰⁰, ▽ 0⁴⁵—4²⁰, 18⁴⁰-⁴⁵ ▽☋—22³⁰
22	7	.	.	-	= 0⁰⁰—12¹⁵, 18³⁰—24, ⌴° 2⁰⁰—9⁰⁰, 22⁰⁰—24, ☋ 1⁰⁰—4²⁰
23	7	.	.	-	= 0⁰⁰—12¹⁵, 15³⁰—24, ⌴ 0-1 0⁰⁰—11⁰⁰, 20⁰⁰—24
24	6	.	.	-	= 0⁰⁰—13⁴⁰, 22³⁰—24, ⌴ 1-0 0⁰⁰—12⁰⁰
25	6	0.7	.	-	●° 8⁴⁸ 9⁴⁰—10³⁰ 11³⁵, = 0⁰⁰—24
26	4	.	.	-	= 0⁰⁰—4⁴⁵ ≡ 1-0 11³⁰ = —24
27	6	2.7	.	-	●° 17⁴⁵-⁵⁰, 18⁴⁰ 19¹⁰—20²⁵, 21³⁸ 23⁴⁵, = 0⁰⁰—24
28	6	0.1	.	-	●° 13⁵⁰ 15⁴⁰, = 0⁰⁰—13⁴⁵ ≡°—15⁵⁰ = —18⁵⁰ ≡°—19²⁰ = —24
29	6	.	.	-	= 0⁰⁰—24
30	6	.	.	-	= 0⁰⁰—8⁵⁰ ≡ 0-1 10¹⁵, ⌴° 1⁰⁰—10⁰⁰
31					
Σ	—	47.8	—	-	UWAGI:

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1	7	0.3	.	-	●° 7³⁴—8⁴⁹, = 0⁰⁰—1³⁰, ≫ 5³⁰—9³⁰ 14⁴⁰—15²⁰
2	8	0.2	.	-	✳° ▽ 9²³-²⁵, 11²³—⁴⁰, 11⁵¹—12⁰³, 21⁵⁰—22¹², ≫ 21⁵¹—22⁴⁰
3	7	0.3	.	-	
4	6	1.6	.	-	●° 4⁴⁵ 5³⁰ ▽° 6³⁰—7⁰² ▽ 0-1 7³⁹—8⁰², = 1⁴⁰—24
5	7	0.3	.	-	●° 6³² 8¹⁰, = 0⁰⁰—3³⁰, 21¹⁵—24
6	6	10.3	.	-	●° 9⁰⁴ 13³⁵ ✳° —14⁰⁵ ✳° —17¹⁰..22²⁰ ●° 24, = 0⁰⁰—24, ≫ 11⁴⁵—12¹⁰
7	5	11.7	2	-	●° 0⁰⁰..³⁰ ✳° —2³⁰ 5⁵⁰—17²⁰, 17³⁵ 20⁴⁵, = 0⁰⁰—24
8	6	.	9	-	= 0⁰⁰—24
9	2	.	9	-	= 0⁰⁰—9¹⁵ ≡ 0-2 19⁵⁵ = —24
10	7	.	9	-	= 0⁰⁰—8³⁰, 19²⁰—24
11	6	4.1	8	-	✳ 0-1 13⁴⁸—15⁴², △ 16⁴², 16¹² △ ✳° —16¹⁴ ✳ 1-0 18³⁸ ●° —20²⁵ ●° 21⁴⁵, 22¹⁵, = 0⁰⁰—24
12	6	0.2	5	-	● 18¹⁵—22¹⁵, = 0⁰⁰—24
13	6	1.1	5	-	✳° 1³⁸ 3⁴⁰, 8⁵⁰ 9³⁰—10⁴⁵, 11⁵⁵ 12¹⁰ ✳ 0 14⁵⁰—15³³, 16⁴⁸—18²², = 0⁰⁰—13⁴⁰
14	7	1.9	5	-	
15	6	3.8	8	-	✳° 2⁵⁰ 3⁴⁵—7⁴⁵ ● 1-0 10²², 16⁴⁵ 17⁴⁰ ✳° 18³⁰—19¹², ↔ 19⁴⁰—24, = 2⁵⁰—24
16	6	.	10	-	↔ 0⁰¹—1¹⁰, = 0⁰⁰—24
17	6	0.0	9	-	✳° 8⁵⁰ 17²⁰, = 0⁰⁰—24
18	6	0.3	11	-	✳° 8²⁵ 9⁰⁵ △—13³⁵, = 0⁰⁰—24
19	6	0.7	11	-	△ 7⁵⁰ 17²⁵ ✳° 14⁴⁶, 15¹⁰—16²⁵, = 0⁰⁰—24
20	6	1.4	10	-	△ 1⁴⁵—3¹⁰ ✳ 0-1 △ ✳° 12³⁵—15⁴⁰ ✳°, ✳△° 17⁴⁰—20⁴⁰ △ 21¹²—22⁵², ●° 23¹⁰—24, = 0⁰⁰—24
21	7	0.6	13	-	●° 0⁰⁰-³⁵ ✳° 5⁴⁵—7²⁵ ✳ 0-1 7³⁷ 11⁵⁰, = 0⁰⁰—12¹⁵, ≫ 11¹⁰—12⁴⁵
22	6	3.1	12	-	✳° 8⁵² 16³⁵ ✳° 23⁴⁵—24, = 8³⁰—20¹⁵
23	7	0.1	14	-	▽ 0⁰⁰-¹⁰ ✳° 22⁵⁰—24, = 21⁴⁵—24
24	6	0.2	15	-	✳° 0⁰⁰-³⁰ 7⁴⁸—8³⁰ 11⁵⁰, = 0⁰⁰—24
25	6	.	15	-	= 0⁰⁰—24
26	6	.	15	-	= 0⁰⁰—24
27	6	.	14	-	= 0⁰⁰—24
28	6	.	14	-	= 0⁰⁰—24
29	6	.	13	-	= 0⁰⁰—20³⁰ ≡ 0-1 22⁴⁰ = —24, V° 20³⁰—24
30	6	.	13	-	= 0⁰⁰—24, V° 0⁰⁰—10⁰⁰
31	6	.	13	-	= 0⁰⁰—13²⁰, 17³⁰—20³⁰ ≡ 0-1 24
Σ	—	42.2	—	-	UWAGI:

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Styczeń - Janvier 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	89.6	91.1	91.6	90.8	-3.1	-2.0	-2.7	-2.2	1.4	-5.6	99	96	100	98	0.0	0.2	0.0	0.1	10	10	10	C 0	ENE 1	C 0
2	89.6	87.6	85.3	87.5	-3.2	-0.6	-2.3	-2.1	0.5	-3.5	99	97	100	99	0.0	0.2	0.0	0.1	10	10	10	C 0	C 0	C 0
3	78.4	74.0	75.4	75.9	-7.0	3.9	6.6	2.5	7.7	-7.7	99	69	69	79	0.0	2.6	2.9	1.8	4	8	10	C 0	E 3	SSW 2
4	75.0	74.4	76.8	75.4	4.3	7.4	3.9	4.9	10.0	3.6	77	66	85	76	1.9	3.5	1.2	2.2	9	9	10	ENE 2	ENE 1	C 0
5	77.6	80.2	86.9	81.6	1.7	3.1	3.1	2.8	5.2	1.1	94	95	74	87	0.4	0.5	1.9	0.9	10	10	10	W 1	SW 1	SW 2
6	90.8	90.4	87.9	89.7	0.6	4.7	-0.4	1.1	5.6	-0.9	98	59	78	78	0.1	3.5	1.3	1.6	5	0	3	C 0	SSE 1	ESE 3
7	85.9	85.8	86.7	86.1	-2.4	1.2	0.4	-0.1	2.2	-3.7	93	81	87	87	0.3	1.3	0.8	0.8	3	10	3	C 0	C 0	WNW 1
8	87.9	87.6	86.0	87.2	1.7	3.9	2.3	2.6	5.1	0.0	90	65	82	79	0.6	2.8	1.3	1.6	10	5	9	SW 3	SSW 3	C 0
9	85.8	86.3	86.7	86.3	2.7	3.9	-0.6	1.8	6.6	-0.7	77	60	92	76	1.7	3.8	0.4	2.0	9	8	3	SSW 3	SSW 3	C 0
10	87.3	85.6	87.3	86.7	-0.4	2.4	-1.3	-0.2	2.7	-2.2	92	89	100	94	0.5	0.8	0.1	0.5	10	10	5	C 0	WSW 1	C 0
11	87.3	88.5	92.1	89.3	-5.9	2.9	2.0	0.8	3.5	-4.5	96	81	82	86	0.2	1.4	1.3	1.0	2	5	10	C 0	ENE 1	WNW 1
12	98.0	100.1	103.9	100.7	-0.7	0.0	-1.4	-0.9	2.2	-1.5	89	62	88	80	0.6	2.3	0.6	1.2	10	7	10	W 4	SW 5	SW 5
13	106.2	105.7	105.7	105.2	-1.7	-0.6	-2.1	-1.6	0.1	-2.1	71	72	96	80	1.6	1.7	0.2	1.2	10	6	10	WNW 4	SSW 5	SW 1
14	101.7	101.3	104.2	102.4	-0.1	3.2	0.4	1.0	5.3	-2.1	78	50	88	72	1.3	3.9	0.8	2.0	10	10	10	SW 3	W 5	SW 3
15	106.4	106.6	104.5	105.8	0.3	0.8	-1.7	-0.6	1.4	-1.8	96	96	96	96	0.2	0.3	0.2	0.2	10	10	10	C 0	NW 1	NW 1
16	99.8	99.3	99.0	99.4	-4.4	-3.9	-2.5	-3.3	-1.3	-5.8	91	89	100	93	0.4	0.5	0.0	0.3	10	10	10	WSW 3	WSW 1	WSW 3
17	101.0	103.4	108.3	104.2	-5.5	-6.3	-9.0	-7.0	-0.7	-9.3	83	68	92	81	0.8	1.2	0.3	0.8	9	3	8	N 4	N 4	N 3
18	112.8	114.0	113.7	113.5	-14.5	-9.6	-14.3	-13.2	-8.4	-15.4	87	69	87	81	0.3	0.9	0.3	0.5	3	3	5	NNE 1	C 0	N 1
19	110.7	108.1	106.7	108.5	-15.2	-8.0	-6.8	-9.2	-6.5	-16.8	91	69	77	79	0.2	1.0	0.8	0.7	9	9	10	C 0	NE 1	NE 1
20	103.7	101.5	99.2	101.5	-8.3	-2.5	-7.9	-6.6	-1.4	-9.6	78	78	93	83	0.7	1.1	0.2	0.7	3	2	6	C 0	ESE 2	NE 1
21	96.1	94.9	94.6	95.2	-11.6	-6.2	-11.3	-10.1	-5.3	-13.0	95	78	90	87	0.2	0.8	0.3	0.4	4	0	4	C 0	NNE 3	NNE 1
22	92.0	90.0	88.5	90.2	-12.4	-4.3	-9.0	-8.7	-3.2	-14.4	89	84	89	87	0.3	0.7	0.4	0.5	9	9	4	C 0	C 0	C 0
23	85.3	84.8	87.5	85.9	-5.7	-2.9	-5.9	-5.1	-1.6	-9.8	95	95	89	93	0.2	0.2	0.4	0.3	10	10	10	C 0	C 0	NE 3
24	88.7	88.1	86.9	87.9	-12.0	-10.4	-13.7	-12.4	-5.8	-13.7	82	80	88	83	0.4	0.5	0.3	0.4	10	0	4	NE 2	NE 2	ENE 1
25	85.3	85.8	88.3	85.3	-10.9	-8.4	-10.8	-10.2	-7.5	-14.8	87	89	87	88	0.4	0.3	0.4	0.4	10	10	10	E 4	E 4	NNE 8
26	94.4	97.7	102.0	98.0	-17.8	-13.7	-16.3	-16.0	-10.7	-18.1	90	88	85	88	0.2	0.3	0.2	0.2	4	1	0	E 4	NE 3	NNE 1
27	105.9	106.1	105.9	106.0	-20.8	-13.0	-15.3	-16.1	-10.5	-21.1	75	92	86	84	0.3	0.2	0.3	0.3	10	0	0	C 0	NE 2	NNE 3
28	102.9	99.8	96.3	99.7	-19.4	-8.6	-12.4	-13.2	-6.3	-19.6	83	92	93	89	0.2	0.3	0.2	0.2	10	10	0	C 0	NNE 1	C 0
29	94.5	96.2	95.7	95.5	-14.0	0.9	-4.7	-5.6	2.2	-15.6	83	85	98	89	0.3	1.0	0.1	0.5	8	10	0	C 0	W 2	C 0
30	89.1	84.4	83.3	85.6	-7.4	8.2	5.4	2.9	8.6	-8.9	93	42	69	68	0.2	6.4	2.8	3.1	4	9	10	C 0	SW 8	SW 3
31	81.9	76.0	78.3	78.8	4.6	6.0	6.1	5.7	9.1	3.3	82	83	83	83	1.5	1.6	1.6	1.6	10	10	10	SW 2	SSW 1	W 5
M	93.2	92.7	93.3	93.1	-6.0	-1.4	-3.9	-3.8	0.3	-7.5	88	78	88	85	0.5	1.5	0.7	0.9	7.9	6.9	6.9	1.3	1.9	1.6

Luty - Février

1	78.5	72.3	72.2	74.4	0.8	4.7	2.7	2.7	6.2	0.6	96	70	91	86	0.3	2.5	0.6	1.1	10	10	10	C 0	NE 2	WSW 5
2	73.1	70.6	67.8	70.5	1.9	5.5	-0.3	1.7	5.6	-0.5	84	56	90	77	1.2	3.9	0.6	1.9	10	8	5	WSW 1	SSW 1	SSW 1
3	66.7	68.5	74.8	70.0	0.6	1.7	0.9	1.0	1.9	-1.1	84	83	87	85	1.0	1.1	0.9	1.0	10	10	10	C 0	WSW 5	WSW 3
4	81.3	82.0	78.2	80.5	0.0	1.5	-1.2	-0.2	2.7	-1.3	96	61	85	81	0.2	2.6	0.8	1.2	10	5	4	WSW 2	SW 4	SSE 1
5	79.9	85.0	93.7	86.2	-2.3	0.6	-1.8	-1.3	1.7	-2.3	98	90	86	91	0.1	0.6	0.8	0.5	10	10	8	C 0	WNW 1	WNW 2
6	95.6	95.3	88.9	92.6	-4.7	0.5	-1.1	-1.6	2.3	-5.9	93	52	73	73	0.3	3.0	1.6	1.6	0	3	9	C 0	E 2	ESE 1
7	83.9	84.0	84.9	84.3	-2.7	2.1	2.5	1.1	3.8	-5.0	86	73	77	79	0.7	1.9	1.7	1.4	8	10	10	C 0	SSW 2	WSW 2
8	86.1	88.9	92.7	89.2	1.5	3.2	2.1	2.2	3.7	-0.7	92	86	95	90	0.5	1.1	0.5	0.7	10	10	10	SW 1	SW 1	WSW 5
9	92.9	88.6	85.8	88.4	-0.1	4.7	2.3	2.3	3.0	-0.5	94	54	95	81	0.4	3.9	0.4	1.6	5	10	10	C 0	SSE 3	SW 2
10	87.3	92.6	99.6	93.2	3.7	3.0	1.8	2.6	4.7	1.6	97	91	85	91	0.3	0.7	1.1	0.7	10	10	10	SW 5	WSW 3	WNW 4
11	96.0	90.3	86.6	91.0	1.1	6.5	3.9	3.8	7.1	0.6	89	66	72	76	0.7	3.3	2.3	2.1	10	9	10	C 0	SSW 2	WSW 1
12	82.7	82.6	89.3	84.9	1.1	5.9	3.2	3.4	6.4	1.0	98	82	93	91	0.1	1.7	0.5	0.8	10	8	8	WNW 1	C 0	WSW 1
13	94.7	96.2	97.8	96.2	3.1	4.8	3.0	3.5	5.1	2.1	91	78	90	86	0.6	1.9	0.8	1.1	10	10	10	SW 1	WSW 4	SW 1
14	101.0	102.8	102.7	102.2	0.6	3.7	-0.2	1.0	5.1	-0.3	92	73	92	86	0.5	2.2	0.5	1.1	10	7	3	NNE 1	ENE 2	C 0
15	102.6	103.8	104.2	103.5	-0.6	6.8	3.1	3.1	9.4	-2.4	92	72	86	83	0.4	2.7	1.0	1.4	10	7	0	C 0	WSW 1	SW 2
16	104.2	106.0	108.4	106.2	3.0	4.7	4.7	4.3	5.0	-0.1	83	95	97	92	1.3	0.4	0.2	0.6	9	10	10	SW 2	WSW 1	W 5
17	109.8	110.0	109.7	109.8	3.8	5.5	5.1	4.9	5.7	3.5	97	89	84	90	0.3	1.0	1.4	0.9	10	10	10	WNW 5	WSW 2	W 2
18	107.7	108.4	104.8	106.3	-0.8	10.9	3.4	4.2	13.5	-1.4	100	58	90	83	0.0	5.5	0.8	2.1	10	0	0	C 0	SW 5	SW 1
19	103.9	103.7	103.8	103.8	0.1	2.7	4.8	3.1	4.9	-0.4	100	88	89	92	0.0	0.9	1.0	0.6	10	10	10	SW 5	SSW 1	WNW 1
20	104.9	106.6	109.2	106.9	0.9	4.3	3.3	3.0	4.9	0.6	98	92	93	94	0.1	0.7	0.5	0.4	10	10	10	SW 2	SSW 2	WNW 3
21	108.8	108.4	108.6	108.6	2.2	6.6	4.6	4.5	7.8	2.1	95	68	85	83	0.4	3.1	1.3	1.6	10	5	10	NNE 1	NE 2	C 0
22	108.7	107.7	107.1	107.8	-0.6	6.4	1.9	2.4	7.3	-0.8	100	60	84	81	0.0	3.8	1.2	1.7	4	4	0	C 0	E 3	E 2
23	105.6	104.8	104.1	104.8	2.2	3.3	1.8	2.3	4.6	1.0	87	78	93	86	1.0	1.7	0.6	1.1	10	9	10	NNE 3	NNE 2	NE 2
24	104.1	104.4	104.5	104.3	1.1	2.0	0.8	1.2	2.4	0.7	96	87	90	91	0.2	0.9	0.7	0.6	10	10	10	E 1	E 1	C 0
25	104.9	106.3	106.9	106.1	-0.4	0.2	-0.9	-0.5	1.2	-1.0	96	86	92	91	0.2	0.9	0.3	0.5	10	10	0	ENE 2	ENE 3	ENE 3
26	108.0	109.0	109.4	108.8	-1.9	0.3	-0.4	-0.6	2.0	-2.7	100	87	96	94	0.0	0.8	0.2	0.3	10	9	9	WSW 1	C 0	ENE 1
27	107.3	105.2	101.8	104.8	-4.3	8.1	4.3	3.1	10.8	-4.8	98	55	77	77	0.1	4.8	1.9	2.3	3	3	9	C 0	SW 2	SW 1
28	94.4	88.1	86.8	89.8	0.3	14.1	6.9	7.1	14.3	0.2	98	45	78	74	0.1	8.8	2.2	3.7	8	8	10	C 0	S 3	WSW 3
29																								
30																								
31																								
M	95.5	95.3	95.8	95.5	0.4	4.4	2.2	2.3	5.5	-0.3	94	74	87	85	0.4	2.4	1.0	1.3	8.8	8.0	8.2	1.1	2.1	1.7

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$ Styczeń – Janvier 1961

DNI	WIATR DZIAŁANIE V	OPAD R	GRUBŚNIEGU h	USŁONECZNIENIE	POGODA
1	3	0.0	5	-	* na *°a, II, ≡°I, II, ≡² III
2	3	1.3	5	-	*°8^{30}–II, ≡°I, ≡¹ ok 8^{00} ≡°II ≡² III
3	8	.	5	-	≡° V¹ I
4	8	5.8	2	-	▽ ok 13^{40}, = III
5	3	4.9	pł.	-	•¹⁻⁰ na, I ok 8^{10}, ok 11^{20} 12^{05-33}, ≡°I, II
6	7	.	pł.	-	= na – ok 8^{10}
7	3	1.2	pł.	-	≡°I, II, III, ⌴°, ⌵ I
8	6	.	1	-	* na *°I, = I
9	8	.	pł.	-	= I, ≡° III, ⌴° III
10	3	0.0	pł.	-	*°7^{45}–ok 7^{55}, ≡°I, II, III; ⌴°I ⌴¹ III
11	5	0.4	pł.	-	≡°I, = II ≡° III, V° I
12	4	0.0	pł.	-	* na *°I–8^{45}, 13^{00-05}, 15^{01-04}, = I, II, III
13	7	.	pł.	-	≡° III
14	5	4.1	pł.	-	*¹ 20^{12-23}, I, np, = I, II ≡° III
15	5	0.0	6	-	*¹ na, ≡¹I, = II ≡°I
16	5	0.0	5	-	△°a, II *° ok 18^{00}, ≡°I, = II ≡° III
17	7	0.0	5	-	*°8^{53}–11^{18}, ⊕ II
18	5	.	4	-	≡°I, ok 11^{30} = II ≡° III, ⌴°I, III
19	5	.	4	-	≡°I, = II, ⌴¹ I
20	7	.	4	-	≡°I, = III
21	5	.	5	-	= I, II, III, ⌴¹ I
22	3	0.4	5	-	= I, ≡° II, III, ⌴°I
23	3	1.4	4	-	* na *°7^{15}–8^{22} *¹ 10^{45}–II, 12^{50}–14^{25}, ≡°I, II ≡ III
24	4	.	7	-	≡°I, a = II, III
25	5	0.2	7	-	*°ok 9^{00} II *¹ 12^{50}–13^{30} *°p, = I, II, III
26	5	.	7	-	= I, II ≡° III
27	3	.	7	-	≡ ok 6^{35} ≡¹I ≡¹⁻⁰a ≡° II, III
28	2	.	6	-	≡¹I, II, III, ⌴°I
29	3	.	6	-	≡¹I ≡° II, III, ⌴¹I, III
30	8	0.2	6	-	≡°I ≡°, = a–10^{50}, ⌴¹I
31	4	2.2	pł.	-	•6^{00}–I, ok 7^{10} •¹ ok 11^{30}–ok 14^{00}, = I, II
Σ	–	22.1	–	-	UWAGI: Ciśnienie powietrza w ciągu całego roku jest za niskie przeciętnie o ok. 0,4 mb. W ciągu całego roku uwagi dotyczące mgły są niepewne.

Luty – Février

1	5	5.9	.	-	•⁰⁻¹ 12^{31}–p, p, III, ≡°I, = II, III
2	7	0.0	.	-	* n, = I, III, ⌴° III, ⌵ III
3	5	0.8	pł.	-	*⁰⁻² 6^{35}–ok 10^{00} *° 12^{17}–p, p, = I, II, III
4	7	0.0	1	-	*°I, 6^{47}–8^{05} *⁰⁻¹ 8^{30}–ok 9^{30}, ≡°I, ⌴° III
5	4	1.4	pł.	-	*¹ 7^{05}–9^{40} *⁰⁻¹ ok 13^{30}–16^{40}, = I, II, III, ⌴°I
6	7	.	2	-	≡°I, = III
7	4	0.0	1	-	⛆¹ 9^{02-07}, ≡°I, ≡° = a – ok 8^{00} = II, III
8	4	0.9	pł.	-	*°na * ok 9^{00} •⁰⁻¹ a – ok 11^{30} •°p, ≡°I, = II, III
9	7	3.6	.	-	•⁰⁻¹ 14^{05}–np, = I, II, ⌴°I
10	5	0.9	.	-	• na, I • ¹⁻⁰ 9^{18}–a •– ok 13^{45}, ≡°I ≡° = a = II III
11	7	2.1	.	-	≡°I
12	6	1.0	.	-	• na, ≡°I, III
13	5	0.1	.	-	• na •°12^{50}–13^{45}, ≡°I, =, ≡°a = II ≡°III
14	7	.	.	-	= I, III, ⌴° III
15	6	.	.	-	≡°I ≡°III, ⌴¹I ⌴° III
16	3	0.0	.	-	• ok 11^{00}, 13^{00}, = I ≡° =a ≡°II, III
17	4	.	.	-	≡°I = II ≡° III
18	5	.	.	-	≡² na, I ≡²⁻⁰ a – 10^{40} ≡° III, ⌴°I, III
19	4	6.7	.	-	• 19^{57}–20^{15}, ≡¹I = II, III
20	5	0.0	0	-	•° * na •°I, a – ok 8^{00}, ≡°I = II ≡° III
21	6	.	.	-	= I, 10^{40}, III
22	6	.	.	-	≡°I, ok 11^{30}, ⌴° III
23	7	.	.	-	= I, III
24	5	.	.	-	≡°I = II, III
25	5	.	.	-	= I, II, III, ⌴¹ III
26	4	.	.	-	≡¹I = II ≡° III, ⌴²I ⌴° III
27	5	0.0	.	-	▽p, ≡°I, = ≡ a = II, III, ⌴²I
28	7	3.2	.	-	•° ok 16^{00} •⁰⁻² p •² III, ≡ I, a, ⌴°I
29					
30					
31					
Σ	–	26.6	–	-	UWAGI:

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Marzec – Mars 1961

Dzień	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D, v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	89.8	91.5	96.9	92.7	3.1	5.1	3.2	3.8	7.0	2.8	90	76	90	85	0.8	2.1	0.8	1.2	10	7 ⊙	10	SW 1	WSW 6	WSW 2
2	100.3	100.6	100.9	100.6	3.1	6.0	4.2	4.4	7.1	2.7	90	69	74	78	0.8	3.0	2.1	2.0	9	8	10	SW 4	SW 6	NW 1
3	99.8	102.4	105.1	102.4	2.6	6.9	5.7	5.2	8.6	1.8	82	70	85	79	1.3	3.0	1.5	1.9	10 ≡	9	10 ● ≡	C 0	WSW 2	C 0
4	106.4	108.7	109.3	108.1	4.9	7.6	5.7	6.0	7.7	4.1	98	79	83	87	0.2	2.2	1.6	1.3	10 ● ≡	10	9	WSW 1	WSW 2	W 1
5	107.8	106.6	107.6	107.3	3.5	9.3	6.6	6.5	10.2	2.6	88	62	79	76	0.9	4.4	2.0	2.4	9	10 ⊙	10	W 5	WSW 6	NW 2
6	107.8	107.2	106.6	107.2	3.8	8.6	6.0	6.1	10.1	3.2	90	65	79	77	0.8	4.2	2.0	2.5	10 ≡	9 ⊙	0	SW 1	WSW 2	W 3
7	103.3	101.1	102.4	102.3	1.1	11.7	9.1	7.8	12.9	0.5	92	56	67	72	0.5	6.1	3.8	3.5	5 ⊙ ≡	9 ⊙	0 ≡	WSW 1	SW 6	WSW 2
8	106.6	106.4	105.8	106.3	1.1	11.3	8.6	7.4	12.6	1.0	98	59	68	75	0.1	5.4	3.6	3.0	7 ≡	1 ⊙	0	C 0	WSW 5	SW 3
9	105.7	104.3	103.0	104.3	4.5	12.8	10.7	9.7	14.2	4.3	84	59	61	68	1.3	6.0	5.1	4.1	9 ⊙	2 ⊙	0	SW 5	WSW 4	WSW 3
10	102.4	99.9	96.9	99.7	6.0	17.2	10.1	10.8	19.7	4.2	70	30	81	60	2.9	13.7	2.4	6.3	3 ⊙	0 ⊙	0 ≡	WSW 1	SSW 2	C 0
11	96.0	96.1	97.8	96.6	5.9	15.7	10.7	10.8	16.0	4.9	74	47	66	62	2.4	9.4	4.5	5.4	3 ⊙	6 ⊙	10	C 0	WSW 3	WSW 3
12	96.7	94.1	86.3	92.4	8.4	11.9	11.1	10.6	13.7	8.0	73	50	64	62	3.0	6.9	4.8	4.9	10	10	7	WSW 5	SW 5	SW 2
13	80.3	82.7	87.1	83.4	8.6	9.0	6.4	7.6	14.4	6.2	63	51	55	56	4.2	5.7	4.3	4.7	8 ⊙	9 ⊙	10	W 8	W 5	WNW 6
14	88.6	88.7	89.0	88.8	3.8	4.4	8.0	6.0	8.0	3.3	64	89	97	83	2.9	1.0	0.3	1.4	9	10 ●	10 ●	W 4	W 3	W 3
15	89.5	90.9	94.7	91.7	7.9	11.4	10.0	9.8	13.2	7.5	93	64	74	77	0.7	4.9	3.2	2.9	10 ●	9 ⊙	5	WSW 4	W 5	WSW 5
16	94.4	91.2	95.9	93.2	8.7	13.7	9.5	10.4	14.2	7.6	80	49	58	62	2.2	8.0	5.0	5.1	9	8 ⊙	0	WSW 4	WNW 9	NW 7
17	97.4	96.4	92.4	95.4	4.9	12.6	9.6	9.2	15.1	4.4	86	55	63	68	1.3	6.6	4.5	4.1	1 ⊙	9 ⊙	0	WSW 1	WSW 6	SW 1
18	83.4	79.1	76.9	79.8	3.7	20.3	11.9	12.0	20.6	3.0	88	29	76	64	1.0	16.9	3.3	7.1	2 ⊙ ≡	4 ⊙	3	C 0	W 7	WNW 3
19	78.3	78.7	81.1	79.4	5.1	7.0	3.9	5.0	11.9	3.3	86	55	95	79	1.3	4.5	0.4	2.1	10	8 ⊙	10	SSW 1	W 3	NNW 7
20	84.9	84.3	79.3	82.8	-0.5	3.7	2.9	2.2	5.6	-0.8	63	41	52	52	2.2	4.7	3.6	3.5	8 ⊙	4 ⊙	9	NW 2	WNW 4	SSW 2
21	70.4	70.0	75.4	71.3	3.1	4.3	1.8	2.8	7.5	1.2	71	69	89	76	2.2	2.6	0.8	1.9	10	10 ⊙	7	SSW 4	WSW 5	SW 4
22	81.2	85.9	89.3	85.5	1.1	2.6	-0.3	0.8	3.3	-0.5	87	58	100	82	0.9	3.1	0.0	1.3	9 *	7	7	W 3	WNW 5	SW 2
23	86.8	88.5	90.8	88.7	0.0	3.7	5.7	3.8	5.8	-1.7	100	85	82	89	0.0	1.2	1.7	1.0	10 *	10	10 ●	SW 2	WSW 5	WSW 3
24	91.7	91.6	92.1	91.8	6.3	7.9	7.9	7.5	9.3	5.0	78	71	71	73	2.1	3.1	3.1	2.8	6 ⊙	10	10	WSW 3	WSW 4	WSW 4
25	93.3	93.6	95.5	94.1	6.7	9.8	8.1	8.2	10.6	6.1	82	67	79	76	1.7	4.0	2.3	2.7	10 ●	10 ●	10 ●	W 3	WSW 3	WSW 3
26	94.2	91.6	84.5	90.1	6.1	10.4	8.0	8.1	12.4	5.5	85	58	59	67	1.4	5.3	4.4	3.7	9 ⊙	10	10	SW 1	SSW 3	SSW 3
27	81.2	82.4	82.7	82.1	7.4	8.7	2.9	5.5	10.9	2.8	84	34	71	63	1.6	7.3	2.2	3.7	10	7	2	SW 3	WNW 4	W 3
28	84.1	84.9	84.9	84.6	-0.5	3.0	1.0	1.1	5.4	-1.0	88	71	90	83	0.7	2.2	0.7	1.2	9 *	10 *	10 *	WSW 6	W 8	WSW 4
29	86.4	85.3	84.9	85.5	0.6	5.0	4.8	3.8	5.6	-0.1	92	72	90	85	0.5	2.4	0.8	1.2	10 *	10 ●	10 ●	SW 3	SW 5	WSW 3
30	82.6	82.3	79.1	81.3	5.3	7.7	8.7	7.6	8.9	3.4	74	76	71	74	2.3	2.5	3.3	2.7	9 ⊙	10	10	SW 5	SSW 3	SW 3
31	77.3	82.5	81.9	80.6	10.1	4.2	4.9	6.0	10.2	3.3	76	88	87	84	3.0	0.9	1.1	1.7	10 ●	10 ●	10	SW 2	NW 1	C 0
M	91.9	91.9	92.0	91.9	4.4	8.8	6.7	6.6	10.7	3.2	83	61	76	73	1.5	4.9	2.6	3.0	8.2	7.9	6.7	2.7	4.4	2.8

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1	86.6	82.6	80.4	83.2	2.2	9.6	10.7	8.3	12.3	1.8	51	49	68	56	3.6	6.1	4.2	4.6	0 ⊙	9	10 ●	W 6	SW 4	SW 4
2	84.4	85.3	82.6	84.1	4.1	8.2	6.3	6.2	10.9	4.1	88	65	88	80	1.0	3.9	1.1	2.0	10 ●	9	9	SSW 4	SSW 4	E 2
3	78.5	79.9	82.9	80.4	6.3	13.6	9.3	9.6	15.0	4.6	97	56	87	80	0.2	6.8	1.6	2.9	10 ●	8	10 ●	C 0	SW 8	SW 1
4	81.0	83.9	88.2	84.4	8.8	14.7	9.6	10.7	15.1	4.1	80	64	89	78	2.3	6.0	1.3	3.2	10 ⊙	9	9	WSW 2	SW 5	C 0
5	87.9	86.2	86.6	86.9	7.0	19.2	14.5	13.8	22.3	6.6	91	58	60	70	0.9	9.2	6.7	5.6	10	3 ⊙	0	NE 1	E 1	SW 1
6	87.1	87.5	87.1	87.2	9.1	23.9	16.1	16.3	24.8	7.4	89	28	60	59	1.3	21.3	7.4	10.0	5 ≡	3 ⊙	0	C 0	SSW 1	ESE 1
7	87.4	86.4	86.9	86.9	10.6	24.6	17.7	17.6	25.7	7.4	80	30	60	57	2.6	21.5	8.1	10.7	0 ⊙	1 ⊙	5	C 0	SW 2	WSW 1
8	85.9	85.6	87.5	85.7	13.4	21.8	11.0	14.3	23.3	10.7	75	47	75	66	3.8	13.9	3.2	7.0	8	3 ⊙	10	C 0	W 4	WNW 6
9	91.7	92.6	94.1	92.8	5.6	9.3	3.8	5.6	11.1	3.8	66	43	67	59	3.1	6.7	2.6	4.1	7 ⊙	7 ⊙	2	SW 2	WNW 8	C 0
10	95.2	89.6	86.3	89.7	0.3	9.3	6.6	5.8	9.8	-1.8	82	36	51	56	1.1	7.5	4.7	4.4	4 ⊙	9 ⊙	10	E 1	NE 5	NE 5
11	85.2	82.5	85.7	85.8	4.7	14.7	10.3	10.0	16.1	4.1	74	45	55	57	2.1	9.1	5.8	5.7	9	4 ⊙	8	NE 1	ENE 1	WNW 5
12	90.3	91.9	92.1	91.4	4.6	12.3	8.4	8.4	13.9	2.8	67	36	61	55	2.9	9.1	4.3	5.4	9 ⊙	4 ⊙	0	C 0	NE 1	ENE 1
13	90.3	88.8	88.7	89.3	5.1	20.0	12.9	12.7	21.3	2.1	76	39	75	63	2.1	14.2	5.8	6.7	3 ⊙	1 ⊙	0 ≡	C 0	SSW 4	W 1
14	88.3	86.8	85.5	86.9	8.7	22.9	15.6	15.7	24.8	6.7	89	25	34	56	1.2	20.8	8.1	10.0	0 ≡ ⊙	2 ⊙	0	C 0	SSE 2	S 1
15	86.1	85.7	86.2	86.0	12.3	23.3	18.7	18.8	26.4	7.7	60	19	41	40	5.8	26.1	12.7	14.9	0 ⊙	2 ⊙	4	C 0	SW 3	S 1
16	85.4	85.8	85.1	84.8	13.3	21.3	15.1	15.2	23.2	11.1	70	36	62	56	4.7	16.2	5.8	8.9	4 ⊙	8 ⊙	3	C 0	S 5	WNW 2
17	85.7	85.9	87.1	86.2	12.0	16.7	13.0	12.7	17.4	10.3	72	58	87	72	4.0	8.0	1.6	4.5	9 ⊙	7 ⊙	0	WSW 1	NNE 2	ENE 1
18	87.3	85.6	85.3	86.1	7.0	18.9	14.3	13.6	20.6	5.9	100	48	74	74	0.0	11.3	4.3	5.2	10 ≡ ⊙	8 ⊙	10	C 0	NNE 3	SW 2
19	87.6	88.1	88.8	88.2	12.3	17.0	12.5	13.6	18.6	10.3	75	52	70	66	3.3	9.4	4.4	5.8	9 ⊙	6 ⊙	5	C 0	NE 5	NNW 5
20	90.9	91.9	94.2	92.3	7.0	13.7	8.5	9.4	15.2	6.3	69	43	44	52	3.1	8.9	6.3	6.1	6 ⊙	8 ⊙	8	NNE 1	ENE 4	NE 2
21	94.2	92.5	90.5	92.4	4.6	13.7	9.3	9.2	15.3	1.0	70	40	50	53	2.6	9.5	5.8	6.0	1 ⊙	1 ⊙	0	E 2	ESE 6	NE 5
22	88.5	85.0	83.6	85.7	6.1	18.7	10.3	11.4	19.8	1.7	72	32	70	58	2.7	14.8	5.8	7.1	0 ⊙	0 ⊙	3	NE 1	ESE 6	E 1
23	82.1	80.4	80.2	80.9	9.0	18.7	11.7	12.8	19.8	5.8	72	27	50	50	3.2	15.8	6.8	8.6	0 ⊙	0 ⊙	0	NE 3	E 9	ENE 7
24	81.6	82.6	83.9	82.7	7.0	13.3	9.4	9.8	15.2	4.2	77	51	70	66	2.3	7.6	3.6	4.5	0 ⊙	4 ⊙	10	NNE 3	NE 10	E 9
25	84.8	85.4	85.8	85.3	7.9	10.7	10.2	9.8	11.7	7.7	79	68	67	71	2.2	4.2	4.0	3.5	10	10	8	ENE 5	ENE 8	E 9
26	83.2	81.8	81.7	82.2	8.3	13.3	13.3	12.6	16.0	6.3	80	59	70	70	2.3	7.2	4.7	4.7	5 ⊙	9	10	ENE 6	ENE 6	NE 3
27	82.3	82.7	84.2	83.1	9.1	13.3	11.7	12.0	17.1	7.9	81	51	69	67	2.2	8.7	4.2	5.0	9 ⊙	8 ⊙	5	NE 2	NE 6	ENE 1
28	84.3	83.4	83.3	83.7	10.6	17.1	12.0	12.9	19.1	6.4	80	41	79	67	2.6	11.6	3.0	5.7	6 ⊙	8 ⊙	7	ENE 1	SE 1	C 0
29	83.3	83.0	84.2	83.5	9.9	19.8	13.2	14.0	20.7	8.3	84	33	65	61	1.9	15.3	5.3	7.6	8 ⊙	8	9	C 0	ESE 2	ENE 5
30	82.7	80.1	80.4	81.1	8.4	20.2	12.0	13.2	20.7	4.9	78	40	63	60	2.4	14.3	5.2	7.3	2 ⊙	7 ⊙	10	NE 4	ENE 7	NE 5
31																								
M	86.2	85.5	86.0	85.9	7.9	16.7	11.5	11.9	18.1	5.7	77	44	66	62	2.5	11.5	4.8	6.3	5.9	5.5	5.5	1.5	4.4	2.9

Kraków, Obserw. Astr. UJ $H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$ Marzec – Mars 1961

DNI	WIATR DZIAŁ NDSC v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁOCZNIENIE	POGODA
1	4	1.4	.	–	• ° 11^{45}– ok. 12^{00}, p., =→, a, II, III
2	6	0.0	.	–	• ° 12$^{52-53}$ △ –12^{56}, =, III
3	5	4.8	.	–	• ° 17$^{02-08}$ 20$^{15-34}$, I, n, ≡°, a = II ≡° III
4	5	0.1	.	–	• na, I, a – ok. 10^{00}, ≡¹ I ≡$^{0-1}$, = – ok. 10^{20}, = II
5	6	.	.	–	= I, III
6	5	.	.	–	≡° I = II, III
7	5	.	.	–	≡° I ≡, = a = II ≡° III, ⌣¹ I
8	5	.	.	–	≡° I = II, III, ⌣° I
9	5	.	.	–	= I, II, III
10	7	.	.	–	= I ≡ III
11	5	.	.	–	= I, II, III, ⌒° I
12	7	1.2	.	–	• ° 12$^{18-45}$, = I
13	7	0.0	.	–	• na, p
14	7	1.8	.	–	• ° 10^{55}– n, = III
15	6	0.1	.	–	• na • I – ok. 9^{15}, = I
16	6	0.0	.	–	• ▽ 17$^{30-33}$, = I
17	6	.	.	–	= ⌒° I
18	7	4.3	.	–	• ¹ 19^{00} 20$^{14-25}$, (R) 20$^{00-25}$, ≡¹ ⌒¹ I
19	7	0.1	.	–	• na • ▽ ok. 10^{30}, ok 14^{30}, 16$^{15-20}$
20	7	.	.	–	
21	7	5.4	.	–	* 8^{25} • ° ok 10^{00}, 12^{25} *¹ 12^{42} 13^{02} • ° 17$^{00-12}$ *¹ 17^{39} • ° ok 19^{00}
22	7	0.5	pł.	–	*° 6^{40}– ok 8^{30}, ok 11^{45} ▽ p., = I, III, ∪ 18^{50}
23	5	0.5	1	–	* na *¹ I *° – ok. 8^{00} • a • ° ok 13^{00} • ok 19^{00}– n, = I, II, III
24	5	0.1	.	–	= I, II, III
25	7	1.2	.	–	• $^{1-0}$ 6^{15}– 7^{30} • ° 12^{34} 13^{30} • $^{0-1}$ ok. 18^{00} • III, = I III, ∪ 18^{50}
26	7	1.0	.	–	= I
27	8	0.4	.	–	• ° na – 6^{30} • ¹ 7$^{25-50}$ 8$^{10-30}$ *, • ° p, = I, III
28	4	2.4	.	–	* $^{0-2}$ 6^{20} 17^{30} *¹ 20^{27}– n
29	6	2.1	pł.	–	* na *¹ I *$^{1-2}$– ok. 9^{00} • 12^{30}– III; *¹ I, = I, III
30	7	1.1	.	–	• I, ok. 10^{00}, 12^{30} I • ° ok. 13^{00}, = III, ∪ 21^{15}
31	6	6.4	.	–	• $^{1-2}$ 6^{30}... ok. 14^{00}, = III
Σ	–	34.9	–	–	UWAGI

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1	7	6.1	.	–	▽ 11^{45} • ° 18^{30}– 20^{50}
2	7	2.2	.	–	• ° na – 6^{50}, 16^{20}– 19^{00}, np
3	8	0.2	.	–	• ¹ 6$^{31-35}$ • ° 8^{00}– p • ¹ ok 14^{00} • III
4	8	0.8	.	–	• ¹ 9^{37}– ok. 10^{30}, 14$^{18-34}$, = III
5	7	0.2	.	–	• ° 7$^{15-40}$, = I III ⌒° III
6	8	.	.	–	≡° I =, ≡ a – ok. 8^{30} ⌒¹ I, III
7	8	.	.	–	= ⌒$^{0-2}$ I, III
8	7	1.3	.	–	• ¹ 15^{49}– 17^{08} • ° 18$^{38-44}$, (R) 15$^{45-52}$, 16^{48}, 17^{07}, = ⌒ I
9	7	.	.	–	⌒° III
10	8	.	.	–	= III, ⌣ I, ⊕ 11^{30}, II
11	6	.	.	–	⌒° I
12	8	.	.	–	= I, ok. 8^{45}, ⌒ I III
13	7	.	.	–	= I, ok. 9^{40} ≡° III ⌒¹ I ⌒° III
14	8	.	.	–	≡, = I – a = III, ⌒¹ I ⌒° III
15	8	.	.	–	≡, ⌒¹ I
16	9	0.0	.	–	• ▽ ok. 7^{30}, ⌒° I, ⌒ 17$^{33-56}$
17	7	.	.	–	(R) 16^{58}, =, ⌒° III
18	7	.	.	–	≡¹, ⌒² I ≡¹, = – ok. 7^{50}
19	7	.	.	–	=, ⌒° I
20	8	.	.	–	⌒° I
21	8	.	.	–	= III, ⌒¹ I
22	8	.	.	–	⌒° I
23	9	.	.	–	⌒° I
24	8	.	.	–	▽ II
25	8	.	.	–	
26	7	0.0	.	–	• ° 15^{50}– 17^{50}
27	7	.	.	–	
28	7	.	.	–	=, ⌒° I, II
29	7	.	.	–	= ⌒¹ I
30	8	.	.	–	
31					
Σ	–	10.8	–	–	UWAGI

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Maj – Mai 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	82.0	84.6	86.1	84.2	9.5	10.4	10.6	10.3	12.0	8.2	83	85	85	84	2.1	1.9	2.0	2.0	10	10 •	10	N 3	NNE 1	NNE 1
2	86.8	86.6	86.4	86.6	10.1	15.5	11.1	12.0	17.2	8.2	85	57	79	74	2.0	7.6	2.8	4.1	10	9 ⊙	9	C 0	SE 1	E 1
3	85.9	84.6	86.7	85.7	8.5	20.9	12.6	13.6	21.2	5.0	85	42	87	71	1.7	14.4	1.9	6.0	8 ⊙	8 ⊙	10	C 0	SSE 2	SW 2
4	89.4	90.6	91.1	90.4	11.4	11.9	11.0	11.3	17.0	10.7	90	85	91	88	1.4	2.3	1.1	1.6	9	9 • ☈	8 =	WSW 1	W 1	SW 1
5	92.4	91.2	90.3	91.3	9.0	20.6	16.9	15.8	21.8	5.0	88	47	63	66	1.4	12.9	7.2	7.2	0	7 ⊙	9	C 0	E 3	C 0
6	88.8	87.7	90.8	89.1	13.0	24.7	15.9	17.4	25.1	8.7	81	42	87	70	2.8	18.1	2.3	7.7	9	9	10 •	C 0	SW 4	W 1
7	90.8	88.7	85.6	88.4	12.6	18.6	16.5	16.0	20.4	12.2	96	64	66	75	0.5	7.8	6.4	4.9	10 •	6 ⊙	7	C 0	ESE 2	WSW 1
8	88.8	87.5	87.4	87.9	10.2	12.8	9.0	10.2	16.5	7.0	80	70	84	78	2.5	4.4	1.9	2.9	3 ⊙	7	10	S 1	WSW 1	SW 7
9	85.0	82.1	81.7	82.9	9.0	13.5	8.4	9.8	13.9	6.9	76	51	83	70	2.8	7.6	1.8	4.1	9 ⊙	7 ⊙	10	WSW 4	WSW 7	SSW 4
10	83.1	84.7	86.3	84.7	8.4	9.3	8.3	8.6	12.2	7.5	87	83	87	86	1.4	2.0	1.4	1.6	10 •	9 ⊙	9	SW 2	W 5	W 4
11	87.7	87.9	90.4	88.7	7.4	11.7	8.3	8.9	13.2	6.9	87	62	84	78	1.3	5.1	1.7	2.7	10 •	8	10	W 1	NW 4	N 1
12	91.6	90.2	89.4	90.4	4.0	8.5	7.4	6.8	10.1	3.8	80	64	83	76	1.6	4.0	1.8	2.5	10	10	9	NW 2	W 5	C 0
13	90.4	88.6	88.0	89.0	6.1	13.7	10.2	10.0	15.2	5.0	69	44	65	66	1.0	8.7	4.3	4.7	10	7 ⊙	9	WSW 3	SSW 4	SW 1
14	86.0	84.8	84.9	85.2	10.3	12.9	8.0	9.8	14.8	7.8	75	77	99	84	3.1	3.5	0.1	2.2	10	9 ⊙	5	WNW 3	SSW 3	WNW 1
15	86.1	86.5	87.5	86.6	7.0	9.5	8.7	8.5	12.6	4.7	81	85	84	83	1.9	2.1	1.8	1.9	8 ⊙	8	9	W 3	W 2	SSW 2
16	88.0	86.6	86.0	86.9	7.5	12.7	9.0	9.6	13.8	5.8	84	56	79	73	1.7	6.5	2.5	3.6	8 ⊙	9	10	W 1	W 1	W 1
17	85.9	87.2	89.6	87.6	7.9	10.6	8.9	9.1	13.2	6.3	90	73	82	82	1.0	3.5	2.0	2.2	9	9	10	WSW 1	NW 4	NW 1
18	90.5	90.0	89.7	90.1	8.7	12.5	10.4	10.5	14.2	8.4	82	51	71	68	1.9	7.1	3.6	4.2	8	7 ⊙	10	NNW 3	NW 4	W 1
19	88.7	87.8	86.0	87.5	9.5	16.1	11.7	12.2	17.7	7.9	82	47	72	67	2.2	9.7	3.7	5.2	9	4 ⊙	4	WSW 1	NNW 3	NNE 1
20	85.2	82.3	81.1	82.9	10.1	16.7	13.1	13.2	18.7	4.8	79	46	62	62	2.6	10.2	5.8	6.2	0 ⊙	6 ⊙	8	C 0	NE 3	NNW 1
21	80.8	81.2	83.0	81.7	12.0	15.7	11.5	12.7	16.8	8.5	76	59	93	76	3.3	7.2	1.0	3.8	8 ⊙	10	10	ESE 2	ENE 7	ENE 1
22	83.3	83.1	84.9	83.8	12.3	16.3	12.7	13.5	16.9	9.0	83	66	64	71	2.4	6.3	5.4	4.7	4 ⊙	9	9	C 0	N 3	NNW 1
23	86.5	86.5	87.2	86.7	11.2	15.9	12.4	13.0	18.4	6.8	65	31	57	51	4.7	12.6	6.2	7.8	3 ⊙	4 ⊙	3	C 0	NNW 3	NNW 1
24	88.9	88.8	89.3	89.0	9.9	18.5	13.7	14.0	19.7	6.3	81	36	75	64	2.4	13.6	3.9	6.6	9 ⊙	8	9	WNW 2	W 1	C 0
25	89.5	87.4	86.4	87.8	12.1	19.5	14.7	15.2	21.3	8.6	77	50	80	69	3.2	11.3	3.3	5.9	2 ⊙	8 ⊙	10	NW 1	WNW 1	WNW 1
26	86.4	85.5	84.2	85.4	12.3	21.6	16.5	16.7	22.8	8.8	81	41	72	65	2.7	15.3	5.4	7.8	8 ⊙	5 ⊙	9	WNW 1	ESE 1	C 0
27	83.6	82.3	82.1	82.7	13.9	18.9	14.7	15.6	23.4	10.1	78	65	89	77	3.6	7.7	1.8	4.4	4 ⊙	8	9	C 0	WNW 2	C 0
28	82.7	81.9	84.2	82.9	13.8	21.3	12.3	14.9	23.9	11.6	91	61	90	81	1.5	9.9	1.4	4.3	10	9 ⊙	10	WNW 1	W 4	WSW 2
29	79.8	73.0	71.2	74.7	10.9	20.0	16.7	16.1	22.7	7.6	96	74	94	88	0.5	6.2	1.2	2.6	10	5 ⊙	10 •	NE 4	ENE 6	ENE 1
30	75.0	76.5	79.3	76.9	12.1	15.7	11.5	12.7	17.2	10.5	80	59	81	73	2.8	7.2	2.7	4.2	6 ⊙	7 ⊙	10	W 4	WNW 5	WSW 1
31	80.7	80.2	80.5	80.5	11.1	18.5	15.2	15.0	19.8	7.0	72	49	74	65	3.7	10.9	4.4	6.3	3 ⊙	5 ⊙	9	C 0	E 3	ENE 1
M	86.1	85.4	85.7	85.7	10.1	15.6	11.9	12.4	17.5	7.6	83	59	79	74	2.2	8.0	3.0	4.4	7.3	7.6	8.8	1.4	3.0	1.3

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1	80.1	79.3	78.7	79.4	14.9	24.8	18.7	19.3	25.8	8.6	74	36	80	63	4.3	20.1	4.4	9.6	0 ⊙	1 ⊙	4	C 0	ENE 3	C 0
2	79.2	78.9	79.4	79.2	17.3	26.2	17.7	19.7	27.8	14.0	80	28	82	63	3.9	24.5	3.6	10.7	5	9 ⊙	6	C 0	SW 4	C 0
3	78.9	79.3	81.5	79.9	18.3	24.0	17.8	19.5	24.9	13.0	71	53	80	68	6.0	13.9	4.0	8.0	1 ⊙	6' ⊙	10	N 1	ENE 3	WSW 1
4	83.1	82.4	84.5	83.3	16.7	22.8	16.9	18.3	24.6	14.7	88	63	90	80	2.4	10.3	1.9	4.9	10 •	7 ⊙	6	C 0	ENE 1	C 0
5	86.8	88.0	89.3	88.0	15.6	18.2	17.5	17.2	22.0	13.5	92	83	75	83	1.3	3.5	4.9	3.2	10	7 ⊙	10	C 0	E 2	ENE 1
6	87.8	85.9	85.1	86.3	15.5	22.4	16.9	17.9	23.5	13.3	89	63	97	83	1.9	10.0	0.6	4.2	10	6 ⊙	10 •	ENE 4	ENE 5	ENE 2
7	84.7	83.3	82.8	83.6	16.7	24.2	17.3	18.9	24.9	14.7	90	58	90	79	2.0	12.6	2.0	5.5	9 ⊙	9	10	C 0	ENE 4	E 1
8	83.9	84.2	85.8	84.6	15.8	22.7	17.6	18.4	24.4	13.3	93	59	88	80	1.3	11.3	2.4	5.0	8	9 •	10	C 0	NE 1	C 0
9	86.4	86.1	86.1	86.2	17.0	21.1	17.1	18.1	23.7	14.8	90	67	94	84	2.0	8.3	1.2	3.8	10	9	10	W 1	NW 1	E 1
10	86.6	85.7	86.9	86.4	15.9	25.0	16.0	17.7	25.4	12.1	100	52	88	80	0.0	15.2	2.1	5.8	10 =	6 ⊙	9	C 0	E 1	S 1
11	87.3	86.5	86.4	86.7	14.5	21.8	18.0	18.1	22.3	11.8	93	67	79	80	1.1	8.5	4.2	4.6	10 ⊙	10 ⊙	10	SSW 1	W 2	W 3
12	85.8	85.0	85.0	85.3	15.1	19.0	15.9	16.5	20.3	14.9	98	69	90	86	0.4	6.8	1.8	3.0	10 •	10 ⊙	10 • ☈	C 0	SSW 1	WSW 1
13	84.5	81.8	80.6	82.3	14.6	21.4	16.3	17.2	22.4	10.7	81	51	85	72	3.1	12.6	2.7	6.1	1 ⊙	7 ⊙	10 •	WSW 1	SSE 1	C 0
14	80.9	84.1	86.7	83.9	16.4	14.9	13.1	14.4	19.7	12.6	73	68	87	76	5.1	5.3	1.9	4.1	9 ⊙	10	9	W 5	W 5	WSW 2
15	89.1	89.5	90.6	89.7	13.3	16.9	13.4	14.2	18.1	11.8	82	57	81	73	2.8	8.2	3.0	4.7	9	9	10 •	WSW 4	WSW 4	SW 1
16	93.0	91.7	92.7	92.5	12.7	18.8	14.4	15.1	20.0	10.0	67	47	75	62	4.9	11.5	4.4	6.9	0 ⊙	3 ⊙	2	W 2	WNW 2	NW 1
17	94.0	93.4	93.4	93.6	13.4	21.6	16.4	17.0	23.2	7.4	77	59	69	62	3.5	15.9	5.8	8.4	2 ⊙	4 ⊙	3	SW 2	WNW 4	C 0
18	93.5	91.8	90.5	91.9	14.3	25.5	19.5	19.7	27.2	9.5	74	39	75	63	4.3	20.0	5.7	10.0	3 ⊙	1 ⊙	0	C 0	SW 5	C 0
19	91.3	91.1	95.9	92.8	20.1	28.5	16.9	20.6	28.9	13.4	68	43	81	64	7.4	22.1	3.7	11.1	0 ⊙	5 ⊙	9	C 0	S 3	SW 1
20	98.6	98.7	99.0	98.8	15.8	20.3	15.3	16.7	21.5	13.6	61	42	59	54	6.9	13.9	7.2	9.3	9 ⊙	7 ⊙	0	WNW 2	WNW 1	NNW 1
21	97.3	94.6	94.8	95.6	13.6	25.0	18.3	18.3	25.2	7.2	71	44	57	57	4.5	15.7	9.0	9.7	0 ⊙	3 ⊙	0	ENE 1	WNW 3	WSW 1
22	98.6	95.4	90.7	94.9	14.1	22.8	19.8	19.1	25.6	11.0	76	54	77	69	3.9	12.7	5.3	7.3	0 ⊙	0 ⊙	10	NNE 2	ENE 4	C 0
23	89.6	91.8	92.9	91.4	17.9	25.7	17.4	19.1	25.2	16.3	86	41	77	68	2.8	17.3	4.6	8.2	7 ⊙	7 ⊙	4	SW 2	WNW 6	W 1
24	93.6	93.2	94.9	93.9	16.2	25.6	18.7	19.8	27.2	11.1	78	59	72	63	4.0	20.1	6.2	10.1	5 ⊙	8 ⊙	5	C 0	SW 5	WSW 1
25	93.2	90.5	88.7	90.8	18.9	29.4	22.1	23.1	30.9	12.0	66	33	62	54	7.5	27.5	10.1	15.0	0 ⊙	1 ⊙	0	WSW 1	SW 5	C 0
26	87.6	86.4	86.7	86.9	22.9	30.8	18.9	22.9	32.7	15.1	64	42	92	66	9.9	25.9	1.7	12.5	3 ⊙	7⊙(☈)	10	C 0	W 1	ENE 1
27	84.2	82.4	83.2	83.3	20.1	32.2	19.9	25.0	33.5	15.5	85	33	91	70	3.5	32.4	2.0	12.6	0 ⊙	2 ⊙	10	NE 2	WNW 2	ESE 1
28	90.0	95.2	100.7	95.3	15.0	16.8	14.9	15.4	20.0	14.2	88	63	66	72	2.0	7.0	5.7	4.9	10 •	8	8	W 5	W 4	W 2
29	102.4	101.3	101.5	101.7	13.0	20.1	16.0	16.3	21.7	10.0	77	52	72	67	3.5	11.3	5.1	6.6	1 ⊙	5 ⊙	6	SW 3	WNW 4	NNW 1
30	101.6	100.5	99.0	100.4	15.5	22.2	17.5	18.2	23.7	10.3	75	46	82	68	4.4	14.5	3.6	7.5	0 ⊙	3 ⊙	0	NW 1	NNW 2	C 0
31																								
M	89.1	88.6	89.1	88.9	16.0	22.9	17.2	18.3	24.5	12.4	80	51	80	70	3.7	14.6	4.0	7.4	5.1	5.0	6.7	1.3	3.0	0.8

Kraków, Obserw. Astr. UJ $H_s = 206\ m$ $H_t = 219{,}8\ m$ $h_w = 10\ m$ Maj – Mai 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	–	• 12³⁸–⁴²
2	6	.	.	–	= //
3	7	6.4	.	–	• 13²⁸ 14⁴⁵ 18³⁰–19¹⁵, (K) 14⁰⁴ 16¹⁶, = I, III, ⌒ I
4	6	2.8	.	–	•¹⁻² 3³⁰–4³⁰ •⁰⁻² 10⁴⁰–14⁰⁰ K° 10⁵³ 11³⁴ NE–NW, (K)° – 11⁵⁷ K² 12³⁵ W K¹ II, = I ≡° III
5	7	.	.	–	= I, III
6	8	16.1	.	–	• ° 16³⁸–18¹⁵, p – III •² np, = ⌒° I
7	7	1.5	.	–	• ¹ na, I, a •² 22⁰⁰ – ok 23⁰⁰, = I, ⌒° III
8	7	8.0	.	–	▲° 11 13–15 •⁰⁻² 10⁵⁷ 11³² 14⁰⁰ 18⁰⁰ ▲° 15⁴⁸–⁴⁹, 15⁵¹–⁵³ (K)⁰⁻¹ 10⁴⁰– K¹ 11¹⁷⁻²² NNE–N–NNW, K¹ 14⁰⁴⁻¹⁶, 15⁴³–16⁰⁰ ESE–ENE, ⌒ 18⁴³⁻⁴⁶
9	7	2.6	.	–	•° 9⁵³ 10³² •¹ 11⁴⁵–⁵⁰ •² p
10	6	1.9	.	–	• ¹ 6¹⁵–7³⁰ •² 8¹²–²² ok 12⁰⁰ •° ok 14⁰⁰ •² 17²⁰, 17³⁰, ok 22⁰⁰⁻¹⁵
11	7	2.5	.	–	• I ▽ 10⁴⁵ •¹ 18³⁰–19⁰¹ • np
12	7	0.0	.	–	• ° 13¹⁰, = III
13	7	.	.	–	= I
14	7	14.7	.	–	• ¹ 8⁵⁰–10⁴⁰ 11²⁰–⁴⁰ 14⁰³⁻³⁵ 17³⁵–18³⁰ K² 14⁰¹ K¹ 17⁵⁶ W, = III, ⌒° I
15	6	1.9	.	–	• ² na •¹⁻² 12¹²–³⁰ •¹ 14⁰⁰–ok 15⁴⁰, = I, III
16	7	0.1	.	–	• ° 18²⁷⁻³⁸, = ≈ I
17	6	1.4	.	–	• ¹ 15⁵⁰–16⁴⁰ ok 23⁰⁰–23²⁰, K° 15³⁵, ≈ II
18	7	.	.	–	
19	7	0.0	.	–	• ¹ 6⁵⁰–7⁰¹, = I
20	7	.	.	–	=, ⌒ ¹ I, ∪ III
21	7	4.2	.	–	▽° ok 12²⁵ ok 14⁰⁰ •¹⁻² 15³²–20²⁰
22	7	0.6	.	–	• ° ok 13⁰⁰, 13⁴⁴–⁴⁸, (K) 13⁴⁵, = I
23	8	.	.	–	⌒° I
24	8	.	.	–	= I, III, ⌒° I
25	7	.	.	–	= I, ⌒° III
26	7	.	.	–	= I, III, ⌒ ¹ I
27	7	0.5	.	–	•² 11¹¹–²⁹, K⁰⁻¹ 11¹⁴–⁵⁴ SW–NW (K) 12⁰⁷ = na – 9⁴⁵ ⌒° ≈ I
28	7	19.9	.	–	• ° 7⁵⁴–8⁰¹ ▽° 11⁴⁰ •⁰⁻² p ▲° 16³⁰⁻³⁶, (K), K¹⁻² 15⁵⁴–18¹³, = I, III
29	7	24.3	.	–	•¹⁻² 16²⁵–17¹⁶ ▲² 17⁰⁵⁻¹⁰ •⁰⁻¹ ok 20³⁰–24, (K), K¹⁻² 16⁴⁸–17²⁴, = I, III
30	7	4.5	.	–	• ¹ 0⁰⁰–2²⁰, 17³²–19¹⁰
31	8	.	.	–	⌒° III
Σ	–	113.9	–	–	UWAGI:

Czerwiec – Juin

1	8	.	.	–	⌒ ¹ I ⌒° III
2	8	.	.	–	(K) 14²⁸ S–15⁰⁰ SE, ⌒ ¹ I, III
3	8	0.0	.	–	= I, ⌒ ¹ I ⌒° III
4	7	5.8	.	–	• ° na, I •⁰⁻² 17²¹–18⁴⁰, (K) SE 17³⁸– K¹ 18²⁸–(K) E 18⁴⁴, = I
5	7	1.3	.	–	• ³ 15⁴⁰–16⁰⁰
6	7	1.4	.	–	• ° 14⁵⁵–15⁴⁰, ok 18⁰⁰ ok 21³⁰ (K) 15⁰⁹–18³³ SE, = III
7	7	0.1	.	–	• ° 14⁰⁵–ok 15³⁰ (K) 14³³ SW K¹ 14⁴⁷ 14⁵⁹, = I
8	7	2.2	.	–	• ² 13³⁵⁻⁵⁰ 14⁵⁹–15⁰⁵, (K) K² 14²¹–15⁰¹, = I
9	4	2.3	.	–	• na •² 14²⁰⁻⁵⁰ •¹ ok 17⁰⁰, K¹ 14¹⁸–15⁰¹ SW, = I, II, III, ≈ II
10	7	0.0	.	–	• ° K° 15⁴⁹–⁵⁵ ≡²⁻¹ na – 8²⁰ = – 8⁴⁵, ⌒ ¹ I
11	5	0.4	.	–	• na, (K), K¹ 16³⁶– ok 18⁰⁰ WSW, = I, II
12	6	3.3	.	–	• ¹ 7²– ok 10⁰⁰ • ° 14³³⁻⁴⁰ •¹ 15³³–16⁴⁰ •⁰⁻² 21¹⁰–21⁴⁴, K¹ II WSW, = I, III
13	8	7.1	.	–	•¹⁻² 20⁵²–21⁵⁰ •² 22⁵⁸–23⁵⁰, = I
14	7	1.0	.	–	• ° 3³⁰–13²⁰⁻³⁰ •¹ 19³⁰–⁴⁰, 20¹⁷–³³
15	7	0.0	.	–	• ° III, = III
16	7	.	.	–	= ≈ I, ⌒° I III
17	6	.	.	–	= I, ⌒ ¹ I, III
18	7	.	.	–	= I, ⌒ ¹ I ⌒° III
19	6	.	.	–	⌒ ° I
20	8	.	.	–	
21	7	.	.	–	= III, ⌒° I
22	7	2.4	.	–	= III, ⌒° I
23	7	.	.	–	•²⁻¹ 2⁵⁰–5¹⁰, = na – ok 9²⁰
24	6	.	.	–	= I, III, ⌒ ¹ I
25	7	.	.	–	
26	7	3.8	.	–	•⁰⁻² 14⁰⁰⁻²⁵ •¹⁻² 16⁰⁰–20²⁰ (K) 13³⁸ W K¹ 14¹⁸ SE 14³⁶ SE 17⁵⁵ = I, III, ≈ I
27	8	34.4	.	–	•²⁻¹ 17²⁰–20¹⁰ ▲¹ 17²⁰⁻²⁴ ▲² 23³¹⁻³³ •² 23³⁰⁻⁴⁰, K 17¹⁶⁻²⁵ NW, 19⁰⁸⁻³⁰ N, 23⁰⁵–⁴⁵ SW, ≫ ok 17⁰⁰
28	7	5.4	.	–	• ² na, I •¹ 9³⁰–11¹⁰, = I
29	6	.	.	–	= ⌒° I
30	7	.	.	–	= I, ⌒ ² I ⌒ ¹ ≈ III
31					
Σ	–	70.9	–	–	UWAGI:

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	99.2	99.2	96.5	98.3	16.7	25.7	20.1	20.6	26.8	12.2	79	45	73	66	4.1	18.1	6.4	9.5	0 ⊙	1 ⊙	3	WNW 1	NW 1	C 0
2	96.9	96.1	94.4	95.8	18.9	26.5	20.6	21.6	27.9	12.4	75	41	74	63	5.3	20.5	6.3	10.7	0 ⊙	0 ⊙	0	C 0	N 3	C 0
3	94.4	92.4	89.6	92.1	19.3	29.8	24.0	24.3	31.7	13.1	65	28	67	53	7.8	30.0	9.8	15.9	1 ⊙	0 ⊙	0	C 0	WNW 1	C 0
4	88.0	84.6	83.1	85.2	20.2	29.0	21.6	23.1	30.9	16.3	70	41	72	61	7.1	23.6	7.2	12.6	2 ⊙	1 ⊙	10 •	SW 1	W 4	SSW 1
5	87.7	88.3	89.1	88.4	15.7	18.1	14.2	15.6	21.7	14.2	77	50	78	68	4.1	10.4	3.6	6.0	7 ⊙	10 ⊙	5	W 3	WSW 4	C 0
6	90.9	93.0	94.6	92.8	12.7	14.9	13.5	13.6	17.7	8.7	73	55	63	64	3.9	7.5	5.7	5.7	9	9	7	C 0	WSW 7	WSW 1
7	95.4	95.4	95.5	95.4	13.3	16.2	11.7	13.2	18.5	10.5	71	55	88	71	4.5	8.6	1.6	4.9	9	9 ⊙	3	W 3	NW 4	C 0
8	95.4	94.1	91.1	93.5	10.7	20.1	15.1	15.2	21.8	7.3	91	43	72	69	1.2	13.3	4.8	6.4	8 ⊙	9	2	WNW 2	SSE 2	C 0
9	87.3	84.2	86.3	85.9	14.5	22.2	14.3	16.3	22.9	8.6	76	47	82	68	3.9	14.1	2.9	7.0	9 ⊙	10	6	C 0	SSW 5	W 4
10	87.4	86.5	87.9	87.3	13.7	18.3	15.3	15.6	20.4	10.4	80	50	61	64	3.2	10.4	6.9	6.8	3 ⊙	10	7	WSW 3	WSW 6	WSW 2
11	90.3	90.0	88.4	89.6	13.6	19.5	16.9	16.7	22.4	9.8	68	46	84	66	5.0	12.4	3.1	6.8	2 ⊙	10	0	SSW 1	SW 3	C 0
12	85.0	83.7	81.8	83.5	17.7	24.6	20.5	20.9	29.3	13.8	75	59	81	72	5.1	12.9	4.6	7.5	8	5 ⊙	1	C 0	E 2	C 0
13	77.2	74.2	74.2	75.2	19.6	29.6	17.3	21.0	30.3	14.0	75	38	85	66	5.7	25.9	2.9	11.5	1 ⊙	6 ⊙	9	NE 1	SSW 6	W 2
14	81.2	83.1	84.9	83.1	15.9	18.9	15.3	16.4	20.1	13.6	65	42	65	57	6.3	12.7	6.2	8.4	9	4 ⊙	3	WSW 6	SW 7	C 0
15	85.5	86.3	86.0	85.9	15.8	24.2	18.8	19.4	24.9	11.8	80	49	80	70	3.5	15.5	4.3	7.8	8	8 ⊙	4	C 0	SW 4	C 0
16	81.7	84.7	84.0	83.5	16.1	20.3	17.6	17.9	22.2	14.6	96	57	72	75	0.8	10.2	5.7	5.6	10 •	4 ⊙	4	C 0	WSW 6	W 1
17	83.7	83.0	83.1	83.3	15.9	17.4	15.4	16.0	22.1	14.2	80	79	67	75	3.6	4.2	5.8	4.5	8 ⊙	10 • ☈	0	C 0	WSW 3	SW 1
18	83.1	82.7	82.8	82.9	13.9	19.1	14.5	15.5	20.3	10.6	74	50	82	69	4.1	11.1	2.9	6.0	10	7 ⊙	2	SW 1	W 6	C 0
19	83.5	82.8	84.0	83.4	13.7	18.7	16.3	16.2	21.3	10.9	84	64	72	73	2.5	7.9	5.3	5.2	7 ⊙	8 ⊙	8 • ☈	WSW 1	SSW 2	SW 9
20	84.7	85.1	86.2	85.3	13.3	16.2	14.7	15.2	20.0	9.5	88	72	93	84	1.8	5.8	1.1	2.9	10	10	9	C 0	SE 1	WSW 1
21	87.4	87.6	88.2	87.7	13.5	18.6	15.4	15.8	19.2	10.6	88	66	84	79	1.8	7.5	2.8	4.0	10 ⊙	10	10 •	C 0	WSW 4	WSW 1
22	88.0	88.0	88.4	88.1	14.1	17.2	13.4	14.5	19.0	12.3	84	69	95	83	2.5	6.2	0.7	3.1	10 •	8	7	WSW 1	WSW 3	SSW 1
23	89.6	89.7	91.7	90.3	14.6	19.3	16.3	16.6	21.9	12.5	89	58	72	73	1.8	9.5	5.3	5.5	10	7	7	C 0	NNW 1	NW 2
24	94.1	95.8	98.0	96.0	14.1	17.2	15.1	15.4	19.2	12.9	82	61	63	69	2.9	7.6	6.3	5.6	5 ⊙	10	10	WSW 2	W 3	NW 1
25	99.2	99.1	99.0	99.1	13.0	15.6	14.0	14.2	16.7	12.0	81	60	77	73	2.8	7.1	3.7	4.5	10	10	10	SSW 1	SW 4	WSW 1
26	96.8	95.8	89.7	93.4	13.3	21.3	16.8	17.0	23.5	11.3	74	44	79	66	4.0	14.2	4.1	7.4	0 ⊙	2 ⊙	8	SW 1	S 1	SE 1
27	86.0	84.1	83.3	84.5	18.1	27.5	19.5	21.2	28.3	11.1	73	41	89	68	5.6	21.7	2.4	9.9	3 ⊙	8 ⊙	9	SE 1	SW 5	C 0
28	81.2	80.4	79.4	80.3	18.4	25.7	20.0	21.0	27.3	16.6	86	53	75	71	2.9	15.5	5.8	8.1	10	9 ⊙	10	C 0	WSW 4	W 1
29	81.1	87.5	89.3	86.0	16.6	14.8	13.1	14.4	20.4	12.6	95	82	89	89	1.0	3.1	1.6	1.9	10 •	10	10 •	W 2	SW 2	SW 1
30	88.8	89.6	90.2	89.5	12.1	13.2	11.5	12.1	14.2	11.2	93	83	94	90	1.0	2.6	0.9	1.5	10 •	10 •	10 •	NW 3	NW 2	C 0
31	87.8	90.1	92.4	90.1	12.0	15.2	13.0	13.3	16.2	11.2	96	87	96	93	0.5	2.3	0.6	1.1	10 •	10 ⊙	10 •	SW 4	SW 3	SW 2
M	88.3	88.2	88.2	88.2	15.2	20.6	16.3	17.1	22.6	12.0	80	55	78	71	3.6	12.0	4.2	6.6	6.7	7.3	5.9	1.2	3.5	1.1

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1	92.4	92.0	91.8	92.1	14.3	20.2	14.9	16.1	22.0	10.2	80	46	85	70	3.2	12.8	2.9	6.3	6 ⊙	4 ⊙	0	SSW 2	W 6	C 0
2	90.6	88.5	88.2	89.1	14.7	26.0	20.4	20.4	27.3	8.8	78	43	76	66	3.6	19.1	5.9	9.5	0 ⊙	2 ⊙	3	C 0	SSE 2	WSW 1
3	89.8	90.0	94.0	91.3	15.7	22.2	17.5	18.2	22.9	14.0	90	64	70	75	1.7	9.7	6.1	5.8	9 ⊙	10 ⊙	10	SW 1	WSW 2	WNW 1
4	9[illegible].4	93.5	92.3	93.7	12.8	20.5	18.1	17.4	22.0	9.8	89	43	63	65	1.6	13.8	7.7	7.7	1 ⊙	3 ⊙	9	C 0	SW 2	C 0
5	92.2	91.5	90.1	91.3	17.3	23.6	18.1	19.3	24.8	15.4	70	53	90	71	5.8	13.5	2.1	7.1	10	7 ⊙	1	C 0	SW 4	C 0
6	89.0	87.3	86.4	87.6	19.1	30.6	22.4	23.6	31.8	13.0	77	39	74	63	5.0	26.7	7.0	12.9	0 ⊙	1 ⊙	1	C 0	SE 1	C 0
7	86.1	85.2	89.2	86.8	20.4	30.4	21.5	23.4	31.7	15.0	75	40	79	65	6.1	26.2	5.4	12.6	1 ⊙	3 ⊙	9	C 0	SSW 1	C 0
8	92.4	90.6	90.9	91.3	16.5	20.0	19.1	18.7	22.8	15.6	94	69	86	83	1.2	7.2	3.2	3.9	10 •	10	0	NNE 1	NNE 5	C 0
9	92.2	92.6	93.1	92.6	19.0	28.1	23.7	23.6	30.6	14.9	85	58	78	74	3.4	15.7	6.6	8.6	8 ⊙	8 ⊙	10 •	C 0	C 0	ESE 2
10	92.7	91.0	87.9	90.5	20.8	28.3	24.5	24.5	29.8	19.1	99	68	94	87	0.3	12.2	1.8	4.8	2 ⊙	2 ⊙	0	NNE 3	WNW 3	NNE 1
11	87.7	84.8	90.3	87.6	22.2	32.7	20.6	24.0	33.2	18.9	82	44	85	70	5.0	27.5	3.7	12.1	0 ⊙	9 ⊙	4	NNW 1	SSW 2	SW 1
12	90.4	88.2	88.7	89.1	17.6	23.6	15.7	18.2	24.7	15.6	94	67	91	84	1.2	9.5	1.5	4.1	10 •	5 ⊙	10 •	C 0	E 3	NW 2
13	90.1	93.2	96.3	93.2	14.1	14.3	12.9	13.6	15.9	12.8	95	82	91	89	0.7	2.9	1.4	1.7	10 •	10	0	NW 2	NW 3	WSW 2
14	95.4	93.7	91.9	93.7	11.3	18.1	12.8	13.8	19.2	8.9	91	56	89	79	1.2	9.2	1.6	4.0	0 ⊙	7 ⊙	5	SW 1	NNE 2	C 0
15	88.6	87.5	86.5	87.5	12.4	20.0	15.5	15.8	21.5	8.8	86	58	76	73	2.0	9.8	4.3	5.4	9 ⊙	8 ⊙	9	SSW 1	S 3	SW 1
16	85.2	85.9	85.3	85.5	14.4	13.9	13.9	14.0	17.4	11.3	80	85	64	76	3.2	2.3	5.7	3.7	10	10	9	SW 2	W 1	WSW 4
17	83.2	81.2	81.2	81.9	13.0	19.3	14.4	15.3	19.6	9.5	73	40	67	60	4.1	13.5	5.5	7.7	5 ⊙	3 ⊙	2	WSW 2	WSW 2	NNW 1
18	83.5	85.2	84.5	83.7	12.0	16.9	11.8	13.1	17.8	10.0	83	54	89	75	2.3	8.7	1.5	4.2	9 ⊙	7 ⊙	6	W 3	WSW 7	SSW 3
19	83.3	81.9	81.5	82.2	12.6	19.1	16.0	15.9	20.2	11.0	80	56	78	71	2.9	9.8	4.0	5.6	10	10	10 •	SSW 4	SSW 7	SSW 3
20	82.9	83.9	88.0	84.9	14.7	17.6	13.0	14.6	18.1	12.4	79	61	83	74	3.4	7.9	2.6	4.6	10	10 ⊙	8	SW 1	W 6	WSW 4
21	89.4	89.3	89.3	89.3	13.4	20.2	15.3	16.0	21.3	10.7	83	58	78	73	2.7	10.0	3.9	5.5	10	4 ⊙	0	SW 2	SW 4	SSW 1
22	86.9	84.1	83.7	84.9	14.1	25.4	15.7	17.7	25.7	9.8	82	40	84	69	2.9	19.5	2.8	8.4	0 ⊙	8 ⊙	10	C 0	SW 5	SW 1
23	85.5	86.6	88.6	86.9	14.2	14.9	13.3	13.9	17.5	12.4	77	77	91	82	3.8	3.8	1.4	3.0	8 ⊙	10 •	9	WSW 5	S 3	WSW 2
24	91.4	91.3	92.5	91.7	11.9	17.4	12.9	13.8	17.8	9.7	84	51	87	74	2.1	9.8	1.9	4.6	8 ⊙	9	10	W 4	WSW 2	WSW 1
25	92.0	92.4	93.8	92.7	12.3	20.2	15.7	16.0	21.5	9.8	94	54	87	78	0.9	11.0	2.2	4.7	9	3 ⊙	5	C 0	SSW 6	SW 1
26	94.3	95.2	95.8	95.1	15.3	21.1	16.9	17.6	23.0	12.0	82	60	89	77	3.2	10.1	2.1	5.1	3 ⊙	5 ⊙	10	W 1	W 4	NW 2
27	96.4	96.5	97.2	96.7	15.8	25.6	18.7	19.7	26.6	12.6	91	48	88	76	1.5	17.2	2.5	7.1	4 ⊙	5 ⊙	2	C 0	W 4	SW 2
28	98.4	99.4	100.4	99.4	16.2	23.4	16.7	18.2	24.4	14.8	88	72	81	80	2.1	8.1	3.7	4.6	9	9 ⊙	7	W 2	WNW 3	WNW 1
29	99.9	97.3	96.4	97.9	12.6	22.7	16.5	17.1	24.7	10.7	89	54	78	74	1.6	12.8	4.3	6.2	1 ⊙	0 ⊙	3	SW 1	SW 3	NW 2
30	97.8	98.1	98.9	98.3	13.9	20.5	15.3	16.2	22.1	10.5	87	43	71	67	2.2	13.7	5.1	7.0	7 ⊙	6 ⊙	4	C 0	NW 1	N 1
31	101.1	101.9	103.0	102.0	10.8	21.3	15.2	15.6	22.8	7.7	90	47	87	75	1.4	13.5	2.3	5.7	1 ⊙	7 ⊙	0	C 0	N 3	NNE 2
M	90.8	90.3	90.9	90.7	15.0	21.9	16.7	17.6	23.2	12.1	85	56	82	74	2.7	12.5	3.6	6.3	5.8	6.3	5.4	1.5	3.2	1.4

Kraków, Obserw. Astr. UJ $H_s = 206\ m$ $H_b = 219{,}8\ m$ $h_w = 10\ m$ Lipiec – Juillet 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	-	= /, ⌒¹ ≈ III
2	7	.	.	-	= / ≈ III, ⌒¹ /, III
3	7	.	.	-	= / ⌒¹ /, III
4	6	5.7	.	-	•⁰ 15²⁵– ok. 16⁵⁰ •⁰⁻² ok. 21⁰⁰ 24, (K), K¹ 16³⁹– 17²¹, = ⌒¹ /
5	7	.	.	-	•² 0⁰⁰– ok. 0³⁰ ⌒⁰ III
6	7	0.0	.	-	▽⁰ 10³⁰– ok. 11⁰⁰, ⌒¹ /
7	6	.	.	-	= /, ⌒⁰ III
8	7	.	.	-	⌒¹ /, III
9	7	2.7	.	-	•²⁻¹ 15⁵⁵– 17⁰⁵, = ⌒¹ /
10	7	0.6	.	-	▽⁰ 12²³ •² 16¹²⁻²⁰, (K) K¹ 16¹²⁻³⁷ SE-E, ⌒⁰ /
11	7	.	.	-	⌒⁰ /, III
12	8	.	.	-	= / ≈ III, ⌒¹ / ⌒⁰ III
13	7	14.1	.	-	•²⁻¹ 18¹⁵– 19³⁵, K⁰⁻¹ 18²¹– 19¹⁵, ≫ 18²⁰⁻⁴⁰, ⌒² /
14	8	0.0	.	-	⌒¹ III
15	8	8.3	.	-	▽ na
16	8	0.0	.	-	•²⁻⁰ ok. 2⁵⁰– 8⁰⁰, ⌒⁰ III
17	7	9.1	.	-	•² 13⁰⁵⁻⁵⁰ ▽ 16⁰⁰, 17⁰⁰, 17⁴⁵, (K), K² 13⁰⁰– 14⁰⁰ SW
18	7	.	.	-	⌒² ≈ III
19	7	0.8	.	-	▽ 13⁰⁰– //, •⁰ 21³⁵– 22¹⁵ (K) 12³²– 13⁰² SW–S K⁰⁻¹ 16²⁸⁻⁴² SW (K) III– 22⁰⁰ W, = ⌒² /
20	7	7.4	.	-	•¹ 8²² 9⁰⁷ •⁰ 10²⁵⁻³⁷ •²⁻¹ 17³⁰– ok. 18³⁰, K¹⁻² 17³⁰⁻³⁸ SSW, = /, III
21	7	5.6	.	-	•²⁻⁰ 16¹⁰– ok. 22⁰⁰, = /
22	8	8.2	.	-	•¹ 7³⁰⁻⁵⁰ ▽ 12³⁰ •¹⁻² 14⁴⁵– 15¹⁰ •² 17²⁰⁻⁴², K 14⁴⁰– 15¹⁰, 17²⁰⁻⁴²
23	8	.	.	-	= /
24	7	.	.	-	= /
25	7	.	.	-	= /
26	8	.	.	-	= /
27	7	0.0	.	-	•⁰ ok. 20⁰⁰, = ⌒¹ /
28	8	21.5	.	-	•⁰ 11⁰⁶⁻¹⁹, 17⁴⁵ •² 22⁵⁰– 24, = /
29	6	10.5	.	-	•² 0⁰⁰– ok. 10¹⁰ •¹⁻² ok. 21⁰⁰– 24, = III
30	7	21.8	.	-	•⁰⁻² na, a, p, np
31	8	11.8	.	-	•⁰⁻² na, a, p, np; = /, III
Σ	—	126.1	—	-	UWAGI:

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1	7	.	.	-	= ⌒² III
2	8	.	.	-	= /, ⌒² / ⌒¹ III
3	5	0.0	.	-	•⁰ 19⁵⁵– 20⁰⁵, = /, II, III
4	7	0.0	.	-	▽ 18¹⁵, = ⌒² /
5	7	.	.	-	⌒¹ III
6	8	.	.	-	= /, ⌒² /, III
7	7	1.5	.	-	= ⌒² /
8	7	0.1	.	-	•¹ 5¹⁰– ok. 8³⁰, ⌒¹ III
9	7	4.2	.	-	•⁰ III, (K) 23⁰⁰ SE, = ≈ /, ⌒¹ /
10	7	.	.	-	•²⁻⁰ 1⁵⁵– 2²⁰, K⁰ 1⁴⁰– 2⁰⁵, = /, III
11	7	0.0	.	-	•⁰ ok. 16³⁰, = ⌒² /
12	7	27.1	.	-	•⁰⁻¹ 7³⁵ 8⁴⁰ •⁰ 10⁰⁰– ok. 10³⁰ •⁰⁻² 17⁵² 24, = /
13	7	21.6	.	-	•⁰⁻² 0⁰⁰– 13¹⁰ •¹ 15⁵⁰– 16⁰⁰ •? 18¹⁰⁻²⁵, = /
14	7	0.0	.	-	▽⁰ a, = /, III, ⌒¹ III
15	7	.	.	-	= /, ⌒² / ⌒⁰ III
16	7	0.3	.	-	•¹ 12³⁶– 13²⁰, ⌒¹ /
17	7	.	.	-	
18	7	2.8	.	-	•¹⁻⁰ 11¹⁴⁻³³ ▽⁰ 14⁴⁰ 15⁰⁵ •¹⁻⁰ 16⁴¹⁻⁵⁷ •²⁻⁰ 19³⁴⁻⁵³, = /
19	8	0.3	.	-	•⁰ ok. 9¹⁵ •⁰⁻¹ 18³⁰– 19¹⁵ • ⁰ 21³⁸⁻⁴², ok. 22⁰⁰
20	8	4.0	.	-	•¹ 14⁴⁵– 15²⁸ •⁰ 16¹⁰⁻²¹, 16⁴⁵⁻⁴⁸ •²⁻¹ 17⁰⁷⁻¹⁹, ⌒ 16⁴²⁻⁵¹
21	8	.	.	-	
22	8	0.5	.	-	•⁰ 20¹²⁻³⁸, K⁰ 20¹⁵⁻⁴⁵ N, = ⌒¹ /
23	7	6.4	.	-	•⁰⁻¹ 11³⁸⁻⁵³ •² 12¹⁸⁻²⁰ ok. 13¹⁵ •²⁻¹ 14⁵⁰– 16⁴⁰, (K) ok. 12⁰⁰
24	7	.	.	-	= /
25	7	0.0	.	-	= ⌒¹ /
26	7	.	.	-	= ⌒¹ /, III
27	8	.	.	-	= ⌒¹ /, III
28	5	.	.	-	= //; ⌒⁰ /
29	6	.	.	-	= /; ⌒¹ / ⌒⁰ III
30	7	.	.	-	= ⌒¹ /, III
31	7	.	.	-	
Σ	—	68.8	—	-	UWAGI:

Kraków, Obserw. Astr. UJ — $\varphi = 50°04'$ — $\lambda = 19°58'$ — Wrzesień – Septembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	103.7	102.8	100.3	102.3	12.8	24.0	17.0	17.7	25.5	9.8	89	47	85	74	1.6	15.8	3.0	6.8	0 ⊙	1 ⊙	0	NNE 1	ENE 1	C 0
2	98.3	96.3	95.5	96.0	14.1	27.7	18.3	19.6	29.3	10.7	92	39	86	72	1.3	22.5	2.8	8.9	0 ⊙	0 ⊙	0	NE 1	SSW 1	C 0
3	91.3	89.3	87.5	89.4	14.3	28.4	17.2	19.3	29.2	10.6	90	32	76	66	1.6	26.3	4.7	10.9	0 ⊙	1 ⊙	1	C 0	SW 2	C 0
4	86.5	87.1	88.8	87.5	15.5	25.8	17.3	19.0	26.8	11.7	74	48	86	69	4.6	17.3	2.7	8.2	7 ⊙	4 ⊙	5	C 0	SW 4	C 0
5	88.1	87.2	84.2	86.5	14.2	25.4	19.2	19.5	27.3	12.4	97	58	85	80	0.6	13.5	3.4	5.8	10	1 ⊙	6	C 0	E 1	C 0
6	81.5	82.4	83.1	82.3	16.4	21.8	16.1	17.6	24.5	14.0	84	67	96	82	2.8	8.7	0.8	4.1	9 ⊙	9	5	C 0	W 4	C 0
7	82.1	82.0	83.5	82.5	15.9	24.7	15.6	18.0	25.1	13.6	98	47	84	76	0.4	16.4	2.8	6.5	9 ⊙	4 ⊙	10	C 0	SW 4	SSW 1
8	85.8	85.5	87.8	86.4	12.9	17.5	13.9	14.6	18.5	11.5	69	41	69	60	4.6	11.7	4.9	7.1	3 ⊙	9 ⊙	9	SW 4	W 8	WSW 4
9	88.4	89.7	90.7	89.6	12.2	15.5	13.7	13.8	16.2	11.5	94	77	81	84	0.9	4.1	3.0	2.7	10 ●	10	9	W 1	WSW 2	WSW 1
10	91.3	92.3	93.0	92.2	12.1	13.0	12.2	12.4	14.8	11.6	87	73	82	81	1.8	4.1	2.5	2.8	10	10	9	W 2	WSW 3	WSW 2
11	92.7	92.3	91.3	92.1	11.2	15.2	9.6	11.4	15.6	9.2	94	67	95	85	0.8	5.6	0.7	2.4	10	10	7	C 0	SW 2	C 0
12	89.9	89.0	89.3	89.4	7.3	19.7	15.8	14.6	21.0	5.1	99	50	78	76	0.1	11.5	3.9	5.2	0 ⊙	8 ⊙	7	C 0	W 2	W 3
13	89.9	90.6	91.2	90.6	12.3	19.9	13.7	14.9	20.5	11.4	93	55	90	79	1.0	10.4	1.6	4.3	10	7 ⊙	9	C 0	WNW 4	C 0
14	88.1	87.7	86.2	87.3	11.7	25.3	16.9	17.7	25.7	10.2	94	43	86	74	0.8	18.2	2.7	7.2	8 ⊙	6 ⊙	3	C 0	WNW 8	C 0
15	90.9	94.3	97.2	94.1	14.8	17.9	11.1	13.7	19.5	10.7	73	49	88	70	4.5	10.5	1.6	5.5	4 ⊙	8	3	W 5	W 4	C 0
16	97.4	96.4	95.9	96.6	11.4	23.6	15.2	16.4	24.9	8.2	86	49	93	76	1.8	14.8	1.2	5.9	6 ⊙	2 ⊙	0 =	C 0	WNW 2	C 0
17	96.9	95.8	95.2	96.0	10.7	27.6	16.7	17.9	29.3	9.6	97	45	90	77	0.4	20.2	2.0	7.5	0 ⊙	4 ⊙	0	C 0	NNW 1	C 0
18	95.9	95.1	95.1	95.4	12.0	28.5	17.5	18.9	29.5	9.6	93	35	84	71	1.0	25.3	3.2	9.8	3 ⊙	7 ⊙	1	C 0	WSW 4	WSW 1
19	95.0	95.4	95.2	95.2	16.3	22.3	13.7	16.5	23.6	13.4	89	59	59	69	2.1	11.1	6.5	6.6	10 =	4 ⊙	0	C 0	W 3	NNW 2
20	96.1	96.3	96.5	96.3	8.7	18.7	11.5	12.6	19.0	6.2	92	44	79	72	0.9	12.2	2.8	5.3	0 ⊙	0 ⊙	0	N 1	NE 5	ENE 1
21	97.3	97.3	99.0	97.9	5.3	17.5	10.6	11.0	18.0	4.0	100	47	65	71	0.1	10.7	4.4	5.1	0 ⊙	0 ⊙	0	NE 1	ENE 4	NE 2
22	100.4	100.9	101.3	100.9	4.0	16.8	8.9	9.6	17.9	1.8	93	42	77	71	0.5	11.1	2.6	4.7	0 ⊙	0 ⊙	0	ENE 1	ENE 4	NE 1
23	100.7	99.4	96.9	99.0	4.1	17.0	10.8	10.7	19.3	1.5	83	39	64	62	1.4	11.9	4.6	6.0	1 ⊙	2 ⊙	0	NE 1	ENE 3	NE 1
24	96.8	96.1	95.7	96.2	4.5	22.1	10.4	11.8	23.8	3.0	92	31	85	69	0.7	16.3	1.9	7.0	0 ⊙	0 ⊙	0	C 0	WSW 1	SW 1
25	95.4	94.6	96.0	95.3	6.5	23.9	12.9	14.0	24.9	5.9	96	32	80	69	0.5	20.2	2.9	7.9	0 =⊙	0 ⊙	5	C 0	WSW 2	W 1
26	97.5	96.4	94.3	96.1	13.9	18.7	14.0	15.2	19.2	11.6	95	69	95	86	0.7	6.7	0.7	2.7	10 =	10	10 =	C 0	E 1	E 1
27	92.6	91.7	92.2	92.2	12.1	15.7	13.4	13.6	17.0	10.8	100	89	94	94	0.0	1.9	0.9	0.9	10 =	10	10 =	NNW 3	WSW 1	W 1
28	93.3	94.0	94.9	94.1	11.2	13.4	10.7	11.5	16.8	10.4	100	91	96	96	0.0	1.4	0.5	0.6	10 =	10	3	ENE 1	NNE 3	NE 1
29	95.3	94.3	93.6	94.4	7.6	18.5	12.9	13.0	20.0	6.3	100	49	81	77	0.0	10.9	2.8	4.6	10 =	2	10 ●	E 3	E 5	ENE 3
30	93.7	92.5	91.0	92.4	10.6	12.7	13.2	12.4	13.8	9.9	91	84	80	85	1.2	2.4	3.0	2.2	10 =	10	10	NNE 3	NE 3	NNE 5
31																								
M	93.1	92.8	92.7	92.9	11.2	20.6	14.0	15.0	21.9	9.2	91	53	83	76	1.3	12.5	2.7	5.5	5.3	5.0	4.4	0.9	3.1	1.1

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1	92.1	93.1	96.0	93.7	7.2	13.0	9.4	9.8	14.4	7.0	91	68	84	81	0.9	4.8	1.9	2.5	9 ⊙	5 ⊙	3	NE 6	NE 8	NE 4
2	96.9	97.9	98.9	97.9	10.9	14.7	10.9	11.8	15.8	7.3	91	67	85	81	1.1	5.5	1.9	2.8	9	8	2	NE 5	NE 7	E 2
3	100.1	98.7	98.9	99.2	7.2	17.6	11.1	11.8	18.5	6.3	97	51	77	75	0.3	9.8	3.1	4.4	4 ⊙	3 ⊙	0	ENE 1	E 7	ENE 3
4	99.0	97.9	97.6	98.2	7.3	19.4	10.4	11.9	19.8	5.9	87	42	82	70	1.3	13.0	2.2	5.5	0 ⊙	0 ⊙	0	NE 1	ESE 5	ENE 1
5	98.1	97.8	98.3	98.1	5.6	19.7	12.2	12.4	20.3	4.4	94	46	74	71	0.6	12.4	3.7	5.6	2 ⊙	3 ⊙	7	C 0	E 1	ENE 1
6	98.2	95.6	92.6	95.5	4.9	20.6	11.4	12.1	20.6	4.4	98	42	76	72	0.2	14.0	3.3	5.8	4 ⊙	1 ⊙	0	C 0	ENE 4	E 1
7	88.4	86.0	85.1	86.5	8.1	18.1	12.6	12.8	18.8	5.6	78	43	63	61	2.4	11.8	5.4	6.5	0 ⊙	5 ⊙	2	ENE 3	E 6	ENE 2
8	83.9	82.3	86.5	84.2	9.5	20.4	10.8	12.9	20.8	7.1	75	40	80	65	3.0	14.4	2.6	6.7	4 ⊙	9 ⊙	0	NE 1	ENE 3	C 0
9	95.2	98.5	101.9	98.5	9.3	16.3	9.3	11.0	17.5	7.5	91	62	96	83	1.1	7.0	0.5	2.9	9 ⊙	9	5 =	S 1	W 3	C 0
10	104.3	104.1	102.8	103.7	5.5	16.3	8.8	9.8	17.1	4.6	98	60	95	84	0.1	7.4	0.6	2.7	4 =⊙	4 ⊙	0	C 0	NE 1	ENE 1
11	101.8	100.9	99.6	100.8	7.4	12.3	8.4	9.1	15.9	4.8	100	80	97	92	0.0	2.9	0.3	1.1	10 =	0 ⊙	0 =	E 3	ENE 1	ENE 1
12	99.1	98.2	99.0	98.8	3.9	19.8	13.7	12.8	19.9	3.7	100	54	86	80	0.0	10.6	2.2	4.3	0 =⊙	9 ⊙	9	C 0	WSW 3	WNW 1
13	99.9	100.8	100.9	100.5	8.7	12.5	9.7	10.2	14.5	8.5	93	77	77	82	0.7	3.4	2.8	2.3	10	9	7	NW 1	SSW 1	NW 1
14	100.1	99.1	97.8	99.0	6.9	11.9	9.6	9.5	12.3	6.4	92	57	84	78	0.7	6.0	1.9	2.9	9	9 ⊙	10	SW 1	WSW 3	W 3
15	98.3	98.1	96.5	97.6	9.9	12.1	10.8	10.9	12.4	9.5	93	80	85	87	0.6	2.8	2.0	1.8	10 ●	10	10	WSW 1	WSW 3	WSW 1
16	94.6	92.7	90.6	92.6	9.5	16.5	8.3	10.6	18.1	8.2	84	52	94	77	1.9	9.0	0.7	3.9	9	2 ⊙	0 =	WSW 1	WSW 3	C 0
17	88.8	84.1	77.0	83.3	4.8	17.5	8.3	9.7	19.2	4.6	100	56	96	84	0.0	8.8	0.5	3.1	8 =⊙	7 ⊙	9 =	C 0	SSW 3	ENE 1
18	68.2	67.8	68.4	68.1	13.5	17.1	14.7	15.0	17.5	7.6	75	56	66	66	3.9	8.5	5.7	6.0	10	9	8	E 3	ESE 2	ESE 3
19	70.2	73.2	75.7	73.0	16.0	20.0	17.2	17.6	21.9	14.2	60	50	69	60	7.4	11.6	6.2	8.4	9 ⊙	9	9 ●	ESE 3	SE 4	E 1
20	80.1	81.1	81.1	80.8	13.5	17.6	14.5	15.0	20.4	10.6	76	72	77	75	3.7	5.7	3.8	4.4	9	8	9	WSW 1	C 0	NNE 3
21	82.4	86.7	91.8	87.0	12.1	18.1	9.1	12.1	18.9	8.6	84	40	67	64	2.2	12.5	3.8	6.2	9 ●	4	2	ENE 2	SE 3	SW 1
22	95.2	96.0	96.4	95.9	0.6	9.4	9.6	7.3	9.8	0.6	100	87	97	95	0.0	1.6	0.4	0.7	10 =	10	9	C 0	NE 4	ENE 3
23	97.6	97.7	98.5	97.9	5.6	13.9	9.3	9.5	14.6	5.5	100	77	96	91	0.0	3.7	0.5	1.4	10 =	8	8 =	C 0	ENE 2	NE 1
24	99.1	98.0	97.2	98.1	2.4	17.4	8.0	9.0	18.4	2.0	100	50	92	81	0.0	10.0	0.9	3.6	6 =⊙	7 ⊙	4 =	C 0	S 1	SSW 1
25	94.3	93.4	93.2	93.6	0.8	18.5	9.3	9.5	18.9	0.8	100	41	83	75	0.0	12.6	2.0	4.9	1 =⊙	5 ⊙	9 =	C 0	WSW 1	C 0
26	91.5	91.3	90.1	91.0	5.5	13.7	7.0	8.3	14.9	5.0	95	60	93	83	0.4	6.4	0.7	2.5	7 =	9	8 =	C 0	C 0	C 0
27	87.8	87.1	86.3	87.1	3.6	15.8	9.2	9.4	17.4	3.1	97	57	77	77	0.3	7.8	2.6	3.6	9 =	9	9	C 0	ENE 1	C 0
28	86.5	85.9	85.0	85.8	3.6	18.5	10.7	10.9	19.5	3.4	80	51	84	72	1.6	10.5	2.1	4.7	2 =⊙	1 ⊙	0	C 0	NNE 3	WNW 2
29	84.9	84.4	87.8	85.7	4.5	15.7	9.8	10.0	15.8	4.4	100	67	95	87	0.0	5.8	0.6	2.1	9 =	10	10	C 0	W 1	WSW 3
30	90.1	90.0	90.2	90.1	8.9	11.2	9.1	9.6	11.5	8.8	99	85	95	93	0.2	2.0	0.7	1.0	10	10	10 ●	C 0	E 1	NE 2
31	92.1	93.6	94.7	93.5	8.5	12.8	9.6	10.1	13.5	8.1	99	85	74	86	0.2	2.3	3.2	1.9	10 =	4 ⊙	5	C 0	WSW 2	WSW 2
M	92.2	92.0	92.1	92.1	7.3	16.1	10.4	11.0	17.1	6.1	91	60	84	78	1.1	7.9	2.2	3.7	6.8	6.3	5.5	1.2	2.9	1.5

Kraków, Obserw. Astr. UJ $H_s = 206\ m$ $H_b = 219{,}8\ m$ $h_w = 10\ m$ **Wrzesień – Septembre 1961**

DNI	WI. DZIAŁ. NOŚC. v	OPAD R	GRUB. ŚNIE. GU h	USŁO. NECZ. NIENIE	P O G O D A
1	8	.	.	–	= 1; ⌒² 1, III
2	8	.	.	–	= 1, III; ⌒ 1
3	8	.	.	–	⌒² 1 ⌒¹ III
4	7	1.1	.	–	•¹⁻² 15⁵⁰–16⁰³, (K) 15⁵⁰ NW K⁰⁻² 16⁴²; ᴨᴨ ⌒² 1
5	7	0.0	.	–	= 1, ⌒¹ III
6	6	2.8	.	–	▽ 7⁰⁰⁻¹⁰ ▽° 13²⁰⁻³⁰ •⁰⁻² 14⁰⁰⁻²⁵ •² 15³⁵⁻⁴⁵, = 1
7	8	0.2	.	–	•¹ 1⁴⁰–2²⁰ •¹⁻⁰ 4¹⁰–5¹⁰ •° 16⁰⁵⁻²⁰ •⁰⁻¹ 21⁰⁵⁻²⁰, ≡² na. = 1
8	8	1.1	.	–	≫ a
9	7	0.0	.	–	•¹ ok. 3⁰⁰–3¹⁵ • na. 1 • 14⁰⁰⁻²⁰, = 1.
10	7	0.4	.	–	• 9⁰⁰⁻¹⁵ •° 13⁰⁵⁻²⁰, = 1
11	7	.	.	–	•° ok. 3⁴⁵–6⁵⁰, = 1, III, ⌒° III
12	7	0.0	.	–	▽° 21⁰²⁻¹⁵, = 1, III; ᴨᴨ ⌒² 1
13	7	.	.	–	= ⌒° 1 III
14	7	1.4	.	–	•¹⁻⁰ 23⁵⁰–24; = 1; ⌒¹ 1 ⌒° III
15	8	.	.	–	•⁰⁻¹ 0⁰⁰–2³⁰, ⌒° III
16	7	.	.	–	= 1 ≡° III, ⌒¹ 1, III
17	8	.	.	–	≡¹⁻⁰ na – ok. 7⁰⁰ = –7³⁰, ⌒² 1
18	8	.	.	–	= ⌒¹ 1
19	7	.	.	–	≡° 1, ⌒° 1, III
20	8	.	.	–	⌒² 1
21	8	.	.	–	= 1 = III, ᴨᴨ ⌒¹ 1
22	8	.	.	–	= 1, III; ⌒° 1
23	7	.	.	–	= ⌒ 1 ⌒° III
24	7	.	.	–	= 1, ⌒¹ 1 ⌒° III
25	7	.	.	–	≡° ᴨᴨ 1 = III, ⌒¹ 1
26	5	3.1	.	–	•¹ 18⁰⁵⁻⁴⁰ •² 18⁵⁰–19¹⁵, (K) 18⁰⁰ K⁰⁻¹ 19⁰⁷⁻⁴⁰, ≡° 1 = II ≡° III
27	4	0.0	.	–	•° a, ≡² 1 = II ≡° III
28	4	.	.	–	≡² 1 = II, III; ⌒¹ III
29	8	7.0	.	–	•° 18¹⁶⁻²⁸ •¹ 18⁴¹⁻⁵² •⁰⁻¹ 21³⁵–23³⁰, K¹ ok. 21⁰⁸ K² 22⁰⁷ NW, ≡² 1
30	5	0.1	.	–	•° 3³⁰⁻⁵⁰, p, ≡° 1 = II, III
31					
Σ	–	17.2	–	–	UWAGI.

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1	7	.	.	–	= ⌒° 1
2	7	.	.	–	= ⌒° 1
3	8	.	.	–	= 1
4	8	.	.	–	= III, ⌒² 1 ⌒° III
5	7	.	.	–	= 1 = III; ⌒¹ 1
6	8	.	.	–	= 1; ⌒¹ 1 ⌒° III
7	8	.	.	–	⌒° 1
8	8	.	.	–	⌒° 1 III
9	7	0.0	.	–	•° ok. 15⁰⁰, = 1 ≡° III; ⌒¹ 1 ⌒° III
10	5	.	.	–	≡° 1 = II, III, ⌒¹ 1, III
11	4	.	.	–	≡¹ 1 = II ≡° III, ⌒¹ 1, III
12	7	.	.	–	≡° 1 = III; ⌒° III
13	5	.	.	–	= 1, II; ⌒°
14	7	0.0	.	–	•° ok. 15⁰⁰–20⁰⁰, = 1
15	4	0.0	.	–	• na – ok. 10⁰⁰, = 1, II III
16	5	.	.	–	= 1 II ≡° III; ᴨᴨ 1; ⌒¹ III
17	7	.	.	–	= 1 II ≡° III; ᴨᴨ 1; ⌒¹ III
18	8	0.0	.	–	▽ 13³⁰, ok. 14³⁰
19	8	0.0	.	–	• III
20	4	0.0	.	–	ᴨᴨ 1, II; ⌒° 1 .
21	8	.	.	–	▽ 6¹⁵–1; ⌒° III
22	6	0.0	.	–	▽° ok. 17³⁰, ≡² ⌒ 1
23	6	.	.	–	≡¹ 1 ≡° III, ᴨᴨ III; ⌒° 1 ⌒¹ III
24	8	.	.	–	≡° 1 ≡° III, ⌒° 1 ⌒° III
25	7	.	.	–	≡ 1 ≡° III; ⌒° 1 ⌒ III
26	4	.	.	–	≡° 1 = II ≡° III, ⌒° 1, III
27	8	.	.	–	≡° 1 = II, ⌒° 1
28	7	.	.	–	≡° 1 = III; ᴨᴨ III; ⌒° III
29	5	1.0	.	–	•° 13⁴⁰–15²⁰, ≡° 1 = II, III; ⌒¹ 1
30	5	4.6	.	–	•⁰⁻⁷ ok. 19⁰⁰–24; = 1, II, III
31	4	.	.	–	•° 0⁰⁰–6³⁰; ≡° 1 = II
Σ	–	5.6	–	–	UWAGI.

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58' — Listopad – Novembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	96.2	96.3	97.3	96.6	7.8	12.7	9.6	9.9	13.4	7.3	80	58	89	76	2.1	6.2	1.3	3.2	7 ⊙	9	10 •	WSW 3	W 7	WSW 3
2	99.2	96.7	91.4	95.8	8.6	12.4	5.8	8.2	13.1	5.5	89	63	95	82	1.3	5.3	0.4	2.3	5	2 ⊙	3 =	WSW 1	WNW 1	C 0
3	86.7	84.5	83.7	85.0	3.6	16.1	9.7	9.8	16.4	2.1	97	40	64	67	0.3	11.0	4.3	5.2	7 =⊙	4 ⊙	9	C 0	SW 3	SW 1
4	82.9	83.2	84.3	83.5	5.8	6.8	2.6	4.4	10.1	2.4	88	91	93	91	1.1	0.9	0.6	0.9	10	10 •	10 •	WSW 1	C 0	NNW 3
5	81.4	83.2	87.9	84.2	0.9	1.4	1.5	1.3	2.9	0.8	96	98	98	97	0.2	0.2	0.1	0.2	10 ✳	10	10 =	NNW 2	W 1	W 2
6	86.8	84.7	82.8	84.8	1.5	2.6	4.7	3.4	4.8	1.5	100	100	100	100	0.0	0.0	0.0	0.0	10 ₉ =	10 ₉ =	10 ₉ =	WSW 1	C 0	SW 1
7	80.2	79.2	80.8	80.1	8.1	15.8	7.5	9.2	14.2	4.5	100	79	100	93	0.0	3.4	0.0	1.1	10 =	7	10 =	E 6	E 4	C 0
8	82.5	83.8	83.8	83.4	5.3	6.3	4.8	5.3	7.8	4.7	95	89	82	89	0.4	1.0	1.5	1.0	10 •	10	10	WSW 2	WSW 2	SW 1
9	82.8	81.9	80.3	81.7	0.5	8.9	4.6	4.6	10.4	0.1	98	80	93	90	0.1	2.3	0.6	1.0	1 =	7 ⊙	8	C 0	C 0	ENE 1
10	78.2	78.5	79.5	78.7	5.6	14.7	9.1	9.6	14.8	3.0	94	59	99	84	0.6	6.9	0.2	2.6	10	9	10 ₉ =	ENE 1	S 2	SSW 1
11	78.8	79.7	80.9	79.8	7.7	10.1	7.9	8.4	11.4	7.4	100	91	96	96	0.0	1.2	0.4	0.5	10 • =	9 •	10	C 0	ENE 1	NNE 2
12	82.1	83.1	84.1	83.1	7.7	8.5	7.6	7.8	9.4	7.2	100	96	100	99	0.0	0.5	0.0	0.2	10	10 =	10 =	C 0	NE 1	NE 3
13	82.8	81.2	79.1	81.0	7.3	10.0	9.2	8.9	10.4	6.1	97	92	97	95	0.3	1.0	0.3	0.5	10	10	10 ₉	ENE 7	NE 5	NE 2
14	79.0	84.3	89.1	84.1	8.8	4.7	2.2	4.5	9.3	2.0	95	84	93	91	0.6	1.3	0.6	0.8	10 •	10	10 ✳	SW 3	W 4	WNW 2
15	90.6	91.9	93.4	92.0	0.7	1.6	0.8	1.0	2.4	0.5	98	81	88	89	0.1	1.3	0.8	0.7	10 ₉	10	10	N 1	NNW 3	NNW 2
16	93.0	92.0	89.1	91.4	1.3	1.9	2.7	2.2	2.7	0.6	87	85	86	86	0.9	1.0	1.0	1.0	10	10	10	C 0	WNW 2	WSW 2
17	87.5	86.8	86.2	86.8	2.3	4.6	4.7	4.1	5.0	1.8	87	81	94	87	0.9	1.7	0.5	1.0	10	10	10	SW 2	WSW 4	SW 3
18	84.7	85.7	85.5	85.3	4.2	4.4	4.1	4.2	5.2	3.3	75	74	88	79	2.0	2.2	1.0	1.7	10	10	8	WNW 4	WSW 4	WSW 4
19	86.9	90.6	96.3	91.3	1.3	3.0	1.7	1.9	4.2	1.3	91	83	81	85	0.6	1.3	1.3	1.1	10	9 ✳	10	WSW 3	W 5	WNW 4
20	101.9	105.4	109.1	105.5	-0.3	1.7	-0.8	0.0	2.1	-0.8	90	65	81	79	0.6	2.4	1.1	1.4	10 ✳	2 ⊙	2	NNW 2	NNW 5	NNW 1
21	108.8	106.3	102.4	105.8	-3.7	1.7	-0.7	-0.8	2.9	-4.3	80	37	79	65	0.9	4.3	1.2	2.1	2	4 ⊙	8	C 0	WSW 2	WSW 1
22	99.4	97.6	94.6	97.2	-2.6	5.6	-1.2	0.2	7.0	-2.8	89	58	97	75	0.6	5.7	0.2	2.2	5 =	1 ⊙	0 =	C 0	SW 1	SW 1
23	91.7	89.9	89.4	90.3	-4.4	2.6	-0.7	-0.8	3.6	-5.0	96	68	90	85	0.2	2.4	0.6	1.1	2 =	5 =	0 =	C 0	C 0	WSW 1
24	91.4	91.5	91.5	91.5	-3.7	5.2	1.7	1.2	6.3	-4.6	94	60	80	78	0.3	3.5	1.4	1.7	4 =	0 ⊙	9 =	C 0	WSW 1	C 0
25	91.1	90.1	88.5	89.9	1.2	3.4	3.6	3.0	4.1	0.1	94	88	88	90	0.4	0.9	0.9	0.7	10 • =	10 =	10 =	C 0	SW 1	SW 1
26	87.9	84.5	80.9	84.4	0.0	2.3	-0.3	0.4	4.3	-0.4	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =⊙	10 =	C 0	C 0	C 0
27	76.9	74.5	76.2	75.9	0.3	7.7	7.6	5.8	8.3	-1.3	100	84	89	91	0.0	1.6	1.2	0.9	9 =	9	10 =	C 0	NNE 1	NNW 3
28	81.9	83.9	86.9	84.2	6.3	8.4	3.5	5.4	8.5	3.4	89	83	97	90	1.0	1.8	0.2	1.0	4 =	9	5 =	C 0	WSW 1	C 0
29	89.1	89.6	90.3	89.7	2.1	6.2	3.1	3.6	7.8	1.9	100	88	91	93	0.0	1.2	0.6	0.6	10 ₉ =	7 =	2 =	C 0	C 0	WSW 1
30	85.7	86.2	82.2	84.7	-1.4	6.5	5.0	3.6	7.2	-2.6	100	68	75	81	0.0	3.1	2.2	1.8	8 =	7 ⊙	6	C 0	SW 3	SW 3
31																								
M	87.6	87.6	87.6	87.6	2.8	6.5	4.1	4.4	7.7	1.5	93	77	90	87	0.5	2.5	0.8	1.3	8.1	7.7	8.0	1.3	2.1	1.6

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1	75.7	75.8	77.3	76.3	7.4	11.1	11.1	10.2	11.4	3.5	76	68	72	72	2.5	4.2	3.7	3.5	10 •	9	8	WSW 6	SW 10	SW 5
2	74.8	72.3	74.0	73.7	11.9	16.5	11.1	12.6	17.3	9.4	69	48	66	61	4.3	9.9	4.5	6.2	9	7 ⊙	10	SW 6	SSW 6	SW 5
3	85.1	84.9	83.3	84.4	2.4	5.2	1.8	2.8	11.7	0.9	79	73	93	82	1.6	2.3	0.6	1.5	3	6 =	0 =	SW 1	WSW 1	SW 1
4	79.8	82.8	86.8	83.1	3.7	13.7	8.7	8.7	14.0	0.3	88	62	86	79	1.0	6.0	1.5	2.8	8 • =	7 ⊙	5	C 0	SSW 6	SW 1
5	86.1	85.3	84.0	85.1	14.2	17.5	12.4	14.1	18.2	6.1	71	54	68	64	4.8	9.1	4.7	6.2	9	6	2	SSW 7	SW 1	SSW 2
6	85.1	86.4	88.5	86.0	9.3	3.9	0.0	3.3	12.5	0.0	93	90	96	93	0.8	0.8	0.2	0.6	10 •	10 •	10 ✳	C 0	W 3	N 1
7	85.1	86.3	89.6	87.0	-0.2	0.1	0.3	0.1	0.5	-0.6	100	100	98	99	0.0	0.0	0.1	0.0	10 ✳ =	10 ✳	10	C 0	N 3	NNW 2
8	91.9	92.2	94.1	92.7	-0.7	0.3	-1.3	-0.8	0.4	-2.4	93	89	93	92	0.4	0.7	0.4	0.5	10	4 ⊙	10	C 0	WSW 3	WSW 3
9	94.1	93.4	91.3	92.9	-5.6	-5.0	-9.4	-6.8	-1.1	-9.4	95	93	98	95	0.2	0.4	0.1	0.2	10 =	4 ⊙	9	C 0	C 0	NE 1
10	89.3	88.2	87.6	88.4	-9.1	-5.4	-1.5	-5.9	-1.2	-9.8	98	94	88	93	0.1	0.3	0.7	0.4	10 =	10 =	10 =	C 0	C 0	N 1
11	82.7	76.2	71.3	76.7	-5.6	0.7	4.7	1.6	4.8	-4.0	97	90	95	94	0.2	0.6	0.4	0.4	7 =	10 • =	10 •	C 0	C 0	W 2
12	76.3	79.5	82.9	79.6	6.5	5.1	2.0	3.9	7.0	2.0	96	98	93	96	0.5	0.2	0.6	0.4	10 •	10	10 ✳	WSW 7	NNW 3	NE 2
13	91.8	97.4	100.2	96.5	-0.5	-3.9	-5.5	-3.8	2.2	-5.5	90	87	85	87	0.6	0.6	0.6	0.6	10	8 ✳ ⊙	4	NW 3	NW 5	NW 2
14	100.6	99.7	100.9	100.4	-9.4	-7.1	-9.4	-8.8	-5.4	-9.5	91	74	66	77	0.3	0.9	1.0	0.7	2	1 ⊙	0	C 0	NNW 4	NW 1
15	95.5	91.1	96.9	94.5	-5.8	-4.7	-14.1	-9.7	-4.0	-14.1	87	53	87	89	0.5	0.3	0.3	0.4	10 ✳	10 ✳	10 ✳	W 4	NNW 12	N 1
16	102.9	107.4	111.8	107.4	-14.8	-14.7	-12.9	-13.8	-12.8	-15.5	87	78	92	86	0.3	0.4	0.2	0.3	8	9 ⊙	10	NE 5	NE 4	NE 6
17	114.5	114.8	112.2	113.8	-17.3	-15.4	-11.4	-13.4	-11.3	-17.3	85	76	86	82	0.2	0.5	0.4	0.4	10 ✳ =	9 ✳ ⊙	10 ✳ =	C 0	C 0	SW 1
18	111.0	110.7	109.4	110.4	-9.3	-4.4	-5.4	-6.1	-4.2	-11.4	95	65	85	82	0.2	1.5	0.6	0.8	10 ✳ =	8 ✳	10	SSW 2	NNW 2	WNW 2
19	107.2	105.3	103.5	105.3	-8.8	-6.5	-5.3	-5.5	-5.3	-9.0	92	91	97	93	0.3	0.3	0.1	0.2	10 =	10 ✳	10	SW 5	SSW 4	SW 3
20	99.6	95.7	87.0	93.4	-2.9	-1.1	0.3	-0.8	0.7	-3.3	95	95	96	95	0.2	0.4	0.2	0.3	10 =	10	10 ⚠	SW 3	SW 8	WSW 4
21	84.8	85.5	89.4	86.6	0.8	-0.9	-3.4	-1.7	1.6	-4.7	77	91	81	83	1.5	0.5	0.9	1.0	9	4	2	SW 4	NW 8	W 2
22	86.2	78.8	81.7	82.2	-6.1	-2.2	-4.6	-4.4	-1.5	-7.5	81	98	81	87	0.7	0.1	0.8	0.5	9	10	9	W 1	SW 5	C 0
23	86.2	88.8	90.8	88.6	-7.6	-7.8	-10.7	-9.2	-4.5	-10.7	87	84	94	88	0.4	0.5	0.2	0.4	10	3	7	W 2	NNW 2	W 2
24	92.1	90.7	88.8	90.5	-13.2	-11.0	-14.5	-13.5	-10.3	-15.1	100	86	87	91	0.0	0.4	0.5	0.2	10 =	0 ⊙	9 =	SSW 1	SSW 1	NE 1
25	87.2	85.9	84.8	86.0	-19.4	-18.7	-22.2	-20.6	-14.4	-23.1	89	78	81	83	0.1	0.3	0.2	0.2	2	0 ⊙	0	E 1	E 1	C 0
26	84.5	82.2	81.5	82.7	-25.4	-16.8	-13.4	-17.2	-13.4	-25.7	98	80	80	86	0.0	0.3	0.4	0.2	3 =	0 =⊙	10 =	C 0	C 0	C 0
27	83.3	84.1	85.6	84.3	-8.8	-5.7	-11.0	-9.1	-5.4	-13.4	86	84	90	87	0.4	0.6	0.3	0.4	10 =	5 ⊙	10 =	C 0	ENE 1	NE 6
28	83.4	83.1	83.1	83.2	-10.0	-7.6	-9.2	-9.0	-6.4	-11.0	87	93	95	92	0.4	0.2	0.2	0.3	10	10	7 =	E 4	ENE 2	NE 1
29	83.7	84.2	84.7	84.2	-7.3	-4.9	-10.5	-8.3	-4.9	-10.6	96	88	94	93	0.1	0.5	0.2	0.3	10 =	0 =⊙	10 =	C 0	C 0	C 0
30	82.6	82.4	83.1	82.7	-5.3	-2.0	-5.6	-4.6	-1.5	-10.5	98	98	95	97	0.1	0.1	0.2	0.1	10 =	4 =⊙	5 =	C 0	C 0	C 0
31	83.4	82.7	80.3	82.1	-5.4	0.0	-2.7	-2.7	0.1	-6.3	98	100	100	99	0.1	0.0	0.0	0.0	10 =	10 =	10 =	C 0	C 0	C 0
M	89.2	88.8	89.2	89.1	-4.5	-2.1	-4.2	-3.8	-0.1	-7.4	89	84	88	87	0.7	1.4	0.8	1.0	8.7	6.6	7.6	2.0	3.1	2.3

Kraków, Obserw. Astr. UJ $H_s = 206$ m $H_b = 219{,}8$ m $h_w = 10$ m Listopad - Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ GU h	USŁONECZNIENIE	POGODA
1	7	0.5	.	-	$\bullet^{0}$ ok 18^{00} – np, = III
2	6	.	.	-	= I ≡^{0} III, ⌓^{2} III
3	8	.	.	-	≡^{0} I
4	4	18.0	.	-	$\bullet^{0-1}$ ok 9^{00} – II, p, III, = I, II
5	4	5.8	pł.	-	*^{1} na, I *^{0} a, p – ok 17^{00}, = I, II ≡^{0} III
6	3	1.8	.	-	• na, I, a, II, p, III, ≡^{0} I, II ≡^{2} III
7	8	7.5	.	-	• p, ≡^{0} I ≡^{2} III
8	4	2.2	.	-	• na $\bullet^{0}$ I $\bullet^{0-1}$ 9^{00} $\bullet^{0}$ p, = I, II, III
9	5	.	.	-	≡^{0} I ≡$^{2-0}$ ok 8^{30} – 11^{00} = – 11^{20} II, ⌓^{0} I ⌓^{2} III
10	8	7.4	.	-	$\bullet^{0}$ 7^{30} – 8^{30} ▽^{0} 13^{00-30} $\bullet^{0-1}$ ok 15^{00} •, III, ≡^{1} III
11	5	5.2	.	-	$\bullet^{1-0}$ na – ok 9^{00} $\bullet^{0}$ 11^{45} – II, ≡^{0} I = II, III
12	3	0.0	.	-	• na • p, = I ≡$^{2-1}$ ok 8^{30} – ok 10^{30} ≡^{0} II, III
13	5	14.7	.	-	•• p • III, = I, II, III
14	5	0.8	.	-	• na •^{1} I – ok 8^{00} • p *^{0} III, = I, II
15	6	0.2	.	-	• na, I • * p, = I
16	4	0.0	.	-	= I, II, III
17	5	0.0	.	-	▽^{0} na $\bullet^{0}$ 10^{00}, p, np, = I, II III
18	7	0.3	.	-	$\bullet^{0}$ 15^{00-45}, = I, III
19	5	0.2	.	-	*^{0} 12^{30-40}, ok 15^{40}, ≡ I, II
20	7	0.2	1	-	*^{0} na, I ✳ 7^{15} *^{1} 7^{20-40}
21	7	.	pł.	-	= I, II, ⌓^{1} I
22	5	.	pł.	-	≡^{0} I = II ≡^{0} III, ⌓^{0} I
23	3	.	pł.	-	≡^{1} I ≡^{0} II, III, ⌓^{2} I ⌓^{3} III
24	4	1.5	pł.	-	≡^{0} I = II ≡^{0} III, ⌓^{2} I, ∪ 21^{00} – 22^{00}
25	3	0.1	.	-	$\bullet^{0}$ na, I, a – ok 8^{00}, p, ≡^{0} I, II, III
26	3	.	.	-	≡^{2} I ≡$^{2-0}$ a – ok 14^{00} ≡^{2} III, ⌓^{0} I
27	4	0.1	.	-	$\bullet^{0}$ ok 17^{00}, 20^{58} 21^{12}, ≡^{0} I = II ≡^{0} III
28	4	0.3	.	-	≡^{0} I = II ≡^{0} III
29	3	.	.	-	$\bullet^{0}$, • na •, I, ≡^{2} I ≡^{0} II, III
30	6	0.2	.	-	• p, ≡^{1} I, ⌓^{2} I
31					
Σ	–	67.0	–	-	UWAGI

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1	8	0.8	.	-	$\bullet^{0}$ 2^{00} – 3^{00}, 6^{27}, I, a, 14^{00} – ok 15^{00}
2	8	.	.	-	
3	3	0.0	.	-	= I ≡^{0} II, III
4	6	0.1	.	-	$\bullet^{0-1}$ 6^{15} – a, ≡^{0} I
5	9	0.6	.	-	▽ na
6	5	27.4	.	-	$\bullet^{0}$ na $\bullet^{0-1}$ a $\bullet^{1}$ II, 13^{30} *^{1}, *$^{1-2}$ p – n, ≡^{0} 7^{20} – ok 8^{30}
7	4	5.6	17	-	*^{1} na, I *$^{1-2}$ a *^{0} II, p – ok 19^{00}, ≡^{0} I = II
8	4	.	16	-	= I, II, III
9	4	.	12	-	≡^{0} I ≡$^{0-2}$ ok 7^{40} = ok 9^{30}, II = III, ⌓^{1} I V III
10	3	.	10	-	≡^{1} I, II, III, V^{0} I, II
11	3	16.6	10	-	$\bullet^{1}$ ok 11^{00} – a, II $\bullet^{0-1}$ p $\bullet^{0}$ III, ≡^{0} I ≡^{0} II = III, ⌓^{0} I
12	4	6.2	.	-	• na $\bullet^{1}$ I, a – ok 12^{20} •, * p *III *, * n, = I, II, III
13	7	0.0	1	-	⛬^{0} ok 12^{00} – 12^{30} *^{0} II * p
14	6	0.1	2	-	= I, V^{0} I
15	3	3.2	2	-	*^{1} na *$^{0-2}$ ok 11^{00} *^{2} *↔ II *^{1} p *^{2} III, ≫ 12^{30-40}, = I, III
16	6	0.6	11	-	*^{0} p, = III
17	5	0.7	8	-	*^{0} na, I, a, II *p *^{1} III, ≡^{0} I = II ≡^{0} III
18	5	0.6	10	-	* na *^{0} I *^{1} a *^{0} II, ≡^{0} I
19	4	0.2	9	-	*^{0} a, II, 14^{00} – 16^{00}, ≡^{0} I = II, III
20	6	0.4	8	-	⛬ * na •, ⛬ p ⛬ III ∿ np, ≡^{0} I = III
21	6	0.8	6	-	⛬^{2} 7^{00} *^{2} – 7^{40} *↔ ≫ 11^{45} – 12^{05} *↔ 15^{05-15} ⛬^{2} *^{2} p, ∪ ok 20^{00}
22	4	2.8	8	-	*$^{0-1}$ a *$^{2-0}$ p, = II, ⌓^{0} I, ∪ III
23	7	0.2	15	-	*^{0} 9^{45} – 10^{00} = I
24	8	0.7	14	-	*^{1} a – 10^{15} *^{0} p, ≡^{0} I, III, ⌓^{0} III
25	4	.	15	-	= I, II, III, ⌓^{1} I V^{1} III
26	2	.	12	-	≡^{0} I ≡^{1} II ≡^{0} III, V^{0} I, II
27	4	.	12	-	≡^{0} I = II ≡^{0} III
28	4	.	12	-	= I, II ≡^{0} III
29	2	.	12	-	≡^{1} I, II ≡^{2} III
30	3	.	11	-	≡^{2} I ≡^{0} II, III, V^{1} I, II
31	1	.	11	-	≡^{2} I, II, III, V^{1}
Σ	–	67.6	–	-	UWAGI

Przemyśl — φ = 49°48' — λ = 22°46' — Styczeń – Janvier 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			POGODA N			KIERUNEK I PRĘDKOŚĆ WIATRU D, v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	88.8	89.4	90.9	89.7	-9.0	-1.2	-1.2	-5.2	-0.4	-11.1	95	95	91	94	0.2	0.3	0.5	0.3	8	8	10	C 0	C 0	C 0
2	89.2	87.6	84.2	87.0	-1.3	-0.1	-0.4	-0.6	0.4	-2.0	97	100	100	99	0.2	0.0	0.0	0.1	10	10 *	10	C 0	C 0	NE 1
3	80.2	77.3	77.1	78.2	-1.2	8.4	8.0	5.8	8.7	-2.0	99	65	67	77	0.1	3.8	3.5	2.5	8	5 ⊙	8	C 0	SW 4	SW 5
4	78.2	77.3	77.9	77.8	4.7	7.0	0.7	3.5	8.5	0.6	81	75	92	85	1.6	2.4	0.5	1.5	8	8	10	SSE 2	SSE 2	SE 2
5	76.9	76.8	85.7	79.8	1.9	6.2	1.0	2.5	7.6	0.4	87	80	96	88	0.9	1.9	0.3	1.0	9	8	3	SE 1	E 1	W 2
6	89.4	90.6	89.5	89.8	2.4	2.9	0.0	1.5	4.5	-0.4	84	74	82	80	1.2	1.9	1.1	1.4	8	1	0	WNW 2	W 4	C 0
7	86.9	85.8	86.0	86.2	-1.3	3.4	2.2	1.6	5.2	-1.9	85	86	82	84	0.9	1.1	1.3	1.1	4	8	0	NW 1	C 0	SW 1
8	86.8	86.9	86.3	86.7	1.8	4.6	0.2	1.7	4.8	-0.6	80	69	80	74	1.5	3.1	1.2	1.9	8	0	0	W 2	W 3	W 1
9	85.0	85.7	86.5	85.7	1.7	5.4	-1.0	1.5	5.4	-1.1	76	62	91	76	1.6	3.5	0.5	1.9	9	3 ⊙	0	W 3	W 1	C 0
10	86.4	86.7	87.6	86.9	-2.9	0.7	-3.0	-2.0	1.6	-3.6	95	86	97	93	0.2	0.9	0.1	0.4	8	0	10 =	C 0	C 0	C 0
11	88.2	88.5	90.8	89.2	-6.2	0.6	-0.1	-1.4	1.2	-6.4	94	92	82	89	0.2	0.5	1.1	0.6	10 =	0	0	C 0	NW 1	W 1
12	92.7	96.5	98.7	96.0	0.7	-1.2	-1.4	-0.8	1.1	-2.3	92	82	80	85	0.5	1.0	1.1	0.9	10 *	8	10	W 3	W 6	WNW 7
13	101.0	102.2	102.3	101.8	-2.2	-1.4	-4.6	-3.2	-1.3	-4.7	76	72	91	80	1.2	1.5	0.4	1.0	10 *	9	10	WNW 5	WNW 7	WNW 1
14	99.7	99.4	100.3	99.8	-0.4	1.8	0.5	0.6	1.8	-5.0	70	55	71	65	1.7	3.3	1.8	2.3	10	9	10	W 3	WNW 5	WNW 3
15	102.9	103.9	101.7	102.8	-0.3	0.2	-1.7	-0.9	0.5	-1.8	96	88	88	91	0.3	0.7	0.7	0.6	10	10	10	WNW 1	NW 4	NW 2
16	96.9	95.6	94.1	95.5	-5.8	-3.8	-2.0	-2.9	-1.6	-5.3	92	92	94	93	0.4	0.4	0.4	0.4	10	10 ≙	10	NW 3	WNW 4	WNW 5
17	97.0	98.2	103.3	99.5	-6.8	-9.1	-12.4	-10.2	-1.4	-12.6	75	82	70	76	0.9	0.5	0.7	0.7	8	0 ⊙	0	N 7	NW 7	NNW 6
18	108.8	109.9	110.3	109.7	-15.5	-10.7	-14.6	-13.8	-10.7	-16.0	77	70	83	77	0.4	0.8	0.3	0.5	0	0 ⊙	0	WNW 4	NW 6	W 2
19	107.3	104.9	103.7	105.3	-13.0	-8.3	-8.3	-9.5	-7.7	-15.8	76	72	92	80	0.5	0.9	0.2	0.5	10	9 *	10 *	W 3	W 4	W 2
20	100.7	99.7	98.0	99.5	-5.5	-5.5	-13.6	-9.6	-5.3	-13.7	95	82	88	88	0.2	0.7	0.3	0.4	10	1 ⊙	0	NW 4	NNE 1	C 0
21	95.7	94.9	93.5	94.7	-19.2	-13.8	-15.8	-16.2	-12.5	-20.5	89	92	86	89	0.1	0.2	0.3	0.2	0	0 ⊙	2	C 0	NW 1	C 0
22	91.2	89.7	87.6	89.5	-15.1	-3.5	-4.7	-7.0	-3.2	-18.7	86	63	64	71	0.3	1.7	1.5	1.2	9	9	2	C 0	W 3	W 4
23	83.7	82.3	85.2	83.7	-3.4	-3.6	-8.5	-6.0	-3.3	-8.6	70	87	89	82	1.4	0.6	0.3	0.8	10	10 *	10	W 5	W 4	NNW 3
24	86.8	86.2	84.8	85.9	-13.2	-7.7	-14.3	-12.4	-6.9	-14.5	88	70	87	82	0.3	1.0	0.3	0.5	10	0 ⊙	0	N 1	C 0	C 0
25	81.7	81.8	85.7	83.1	-15.0	-9.3	-10.5	-11.3	-6.4	-16.8	91	85	84	87	0.2	0.4	0.4	0.3	10	9 *	10 *	C 0	N 3	NE 7
26	92.9	96.4	100.5	96.6	-17.8	-14.5	-18.7	-17.4	-10.4	-19.4	90	78	78	82	0.2	0.4	0.3	0.3	3	0 ⊙	0	NNE 1	N 2	C 0
27	104.5	105.2	104.6	104.8	-23.2	-15.5	-16.1	-17.2	-12.2	-23.9	88	76	81	82	0.1	0.5	0.3	0.3	0 ⊙	0 ⊙	0	C 0	C 0	C 0
28	102.4	99.7	96.8	99.6	-19.5	-1.8	-5.1	-7.9	3.2	-21.0	89	61	46	65	0.1	2.1	2.2	1.5	0 ⊙	1 ⊙	0	WNW 2	C 0	C 0
29	95.5	94.2	95.3	94.3	-1.6	3.8	-0.5	0.5	3.8	-7.2	41	42	58	47	3.2	4.7	2.5	3.5	0	2 ⊙	0	W 2	W 4	W 4
30	90.2	87.3	82.4	86.6	0.3	4.2	2.0	2.1	4.5	-2.3	71	43	66	60	1.8	4.7	2.5	3.0	2	5 ⊙	10	SW 9	SW 7	SW 9
31	82.4	77.6	74.4	78.1	2.0	4.0	4.3	3.6	4.5	1.4	71	61	72	68	2.1	3.2	2.3	2.5	7	9	10	W 4	SW 5	SW 7
M	91.9	91.6	91.8	91.8	-5.9	-1.8	-4.5	-4.2	-0.6	-8.3	84	75	82	80	0.8	1.6	0.9	1.1	7.1	4.9	4.7	2.2	2.9	2.4

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1	77.7	75.9	70.9	74.2	2.6	5.6	3.1	3.6	6.3	2.3	82	72	81	78	1.3	2.5	1.4	1.7	10	10	10	N 1	SW 4	C 0
2	71.0	69.9	67.5	69.5	1.7	1.2	0.3	0.9	3.2	0.1	94	94	98	95	0.4	0.4	0.1	0.3	10 ●	10 *	6	W 1	WNW 1	C 0
3	66.1	65.5	70.4	67.3	-2.6	2.2	1.3	0.6	3.3	-3.2	98	75	79	84	0.1	1.8	1.4	1.1	2	10	10	C 0	W 4	W 7
4	77.4	79.1	78.0	78.2	0.2	0.7	-0.8	-0.2	1.6	-0.9	89	71	91	84	0.7	1.8	0.5	1.0	10	6	0	W 3	WNW 5	C 0
5	78.5	82.0	88.1	82.9	-2.6	1.1	-0.4	-0.6	1.3	-3.2	89	68	84	80	0.6	2.1	0.9	1.2	9	9	9	NE 1	E 1	NW 4
6	95.9	93.7	91.2	92.9	-4.2	0.1	-3.2	-2.6	1.3	-4.3	87	67	86	80	0.6	2.1	0.7	1.1	9	1 ⊙	0	NW 1	WNW 1	SE 2
7	84.7	83.4	83.2	83.8	-0.9	0.8	-0.9	-0.5	0.9	-5.0	75	64	89	76	1.4	2.4	0.6	1.5	8	10	10 *	SW 3	WSW 4	WSW 1
8	83.7	85.6	89.4	86.2	-0.3	1.5	1.2	1.0	2.0	-1.0	78	80	90	83	1.3	1.4	0.7	1.1	10	9	10	W 5	W 4	W 1
9	91.2	89.6	84.9	88.6	0.4	4.5	1.2	1.8	4.5	0.1	92	57	68	72	0.5	3.6	2.2	2.1	5	2 ⊙	10	W 2	W 3	SW 1
10	84.6	87.3	93.7	88.5	0.1	1.6	0.9	0.9	2.0	-0.2	98	93	87	93	0.2	0.6	0.9	0.6	10 *	10 ≋	10 *	W 5	W 4	NW 7
11	95.5	91.3	86.3	91.0	-0.3	2.6	2.6	1.9	4.0	-0.5	98	75	77	83	0.2	1.9	1.7	1.3	10	9	8	NW 3	W 2	W 4
12	82.1	81.7	85.8	83.2	2.5	3.0	1.9	2.5	3.3	1.8	84	86	87	86	1.2	1.1	0.9	1.1	10	10	10	W 2	W 2	W 1
13	91.0	93.7	94.9	93.2	1.1	2.2	0.6	1.1	2.7	0.5	96	96	98	97	0.2	0.3	0.1	0.2	10 ≋	10 ●	10 *	WNW 3	WNW 2	NW 2
14	98.8	101.3	102.2	100.8	0.3	1.4	-1.4	-0.3	1.6	-1.6	74	65	89	76	1.6	2.4	0.6	1.5	10	9	0	NW 2	NW 2	C 0
15	101.3	102.0	102.5	101.9	-3.2	4.9	1.3	1.1	5.4	-4.1	79	59	79	72	1.0	3.6	1.4	2.0	1	0 ⊙	0	W 3	WNW 4	W 3
16	101.4	102.5	104.8	102.9	2.3	3.6	2.8	2.9	5.5	0.8	80	86	100	89	1.4	1.1	0.0	0.8	8	10 ●	10 =	W 4	W 7	W 2
17	105.6	106.9	106.5	106.3	1.9	2.8	2.7	2.5	4.0	1.6	94	93	100	96	0.4	0.6	0.0	0.3	10	10	10 ●	WNW 5	W 7	WNW 1
18	104.8	103.8	102.4	103.6	1.9	9.6	5.2	5.5	10.7	1.4	96	60	70	75	0.3	4.8	2.6	2.6	10	0 ⊙	0	W 3	W 4	W 4
19	100.7	100.4	101.3	100.8	1.8	7.7	4.0	4.4	7.8	1.3	82	63	85	77	1.3	3.9	1.2	2.1	0	5 ⊙	10	W 3	W 6	W 1
20	102.2	104.1	107.1	104.5	2.0	2.9	2.7	2.6	4.9	1.8	100	95	88	94	0.0	0.4	0.9	0.4	10	10 ●	10	W 2	WNW 3	C 0
21	107.8	107.7	107.2	107.6	1.8	5.2	2.6	3.0	5.2	1.4	95	75	77	82	0.6	2.2	1.7	1.5	10	10	9	C 0	W 5	W 1
22	106.8	106.7	106.0	106.5	2.2	5.4	3.1	3.4	5.5	2.0	78	69	90	79	1.6	2.8	0.8	1.7	10	9	10	W 1	W 3	N 1
23	104.8	103.9	102.5	103.7	1.1	2.1	1.2	1.4	3.1	0.9	94	87	92	91	0.4	0.9	0.5	0.6	10	10	10	ENE 5	E 4	ENE 1
24	102.5	103.1	103.5	103.0	0.1	0.1	-0.7	-0.3	2.0	-0.8	94	84	81	86	0.4	1.0	1.1	0.8	10	10	10	C 0	WNW 1	C 0
25	104.7	105.2	107.1	105.7	-1.7	-0.6	-1.8	-1.5	0.2	-1.9	84	79	83	82	0.9	1.2	0.9	1.0	10	10	0	C 0	E 4	E 4
26	107.5	108.0	108.7	108.1	-4.2	5.0	-0.3	0.0	6.5	-4.5	96	55	78	76	0.2	3.9	1.4	1.8	0 ⊙	0 ⊙	0	C 0	ENE 2	C 0
27	107.6	105.1	101.6	104.8	-3.0	7.1	1.7	1.9	7.9	-3.5	93	47	70	70	0.4	5.4	2.0	2.6	0 ⊙	0 ⊙	3	C 0	W 3	W 3
28	94.4	89.2	84.1	89.2	1.3	8.8	4.8	4.9	8.8	1.0	72	50	56	59	1.9	5.6	3.8	3.8	2	5 ⊙	10	W 3	SW 7	SW 7
29																								
30																								
31																								
M	95.8	95.8	94.0	95.9	0.1	3.3	1.3	1.5	4.1	-0.6	88	74	84	82	0.8	2.2	1.1	1.4	7.6	7.3	7.0	2.1	3.5	2.1

Przemyśl $H_s = 237\,m$ $H_b = 238{,}9\,m$ $h_w = 20{,}6\,m$ **Styczeń – Janvier 1961**

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	5	.	12	-	$\equiv^{2}\ 0^{00}-1^{50}\ =-24$
2	4	7.3	10	-	$*^{0}\ 10^{15}-12^{52}\ *^{0-1}\ 14^{31}-19^{40}.\ =\ 0^{00}-24$
3	7	.	21	-	$=\ 0^{00}-10^{45}$
4	8	.	12	-	
5	5	1.1	7	-	$\triangledown^{0}\ 14^{00}-15^{08}.\ =\ 8^{10}-13^{36}$
6	7	0.1	5	-	$*^{0}\ 8^{20-30}\ \bullet^{0}-9^{05}.\ \smile^{0}\ 20^{00}-24$
7	5	.	5	-	$=\ a.\ p.\ \smile^{0}\ 0^{00}-9^{00}$
8	7	.	pż.	-	$=\ 18^{15}-21^{30}.\ \smile^{0}\ 3^{00}-9^{00}$
9	6	.	pż.	-	$=\ 11^{16}-24$
10	5	.	pż.	-	$=\ 0^{00}-14^{44}\ \equiv^{2}-24.\ \smile^{0}\ 1^{00}-11^{00}$
11	5	0.5	pż.	-	$\equiv^{2-1}\ 0^{00}-7^{40}\ =-21^{30}.\ \triangledown^{0}\ 5^{40}-7^{15}$
12	7	0.0	1	-	$*^{0}\ 3^{40}-7^{05}\ \triangledown^{0}\ 8^{34-50}\ *^{0}-10^{55}\ \triangledown^{0}\ 11^{50}-12^{00}$
13	7	0.0	1	-	$*^{0}\ 5^{50}-11^{20}$
14	7	3.0	1	-	
15	6	.	5	-	$*^{0-1}\ 1^{10}-6^{20}.\ =\ 1^{00}-13^{35}.\ 23^{10}-24$
16	5	0.1	5	-	$\triangle^{0}\ 10^{40}-19^{10}.\ =\ 0^{00}-22^{10}$
17	8	0.0	5	-	$\triangledown^{0}\ 3^{40}-4^{20}.\ 5^{38}-6^{20}\ *^{0}\ 8^{45}-9^{20}\ \triangledown^{0}-10^{45}.\ 15^{20-35},\ 16^{25-40}$
18	6	0.0	6	-	$\leftrightarrow\ 10^{32}-11^{51}.\ =\ 10^{45}-17^{20}.\ \smile^{0}\ 19^{00}-24$
19	6	1.4	6	-	$*^{0}\ 10^{40}-24.\ \smile^{0}\ 0^{00}-9^{00}$
20	8	.	7	-	$*^{0}\ 0^{00}-5^{45}.\ =\ 6^{50}-8^{40}.\ \smile^{0}\ 17^{00}-24$
21	6	0.0	7	-	$\leftrightarrow\ 9^{35-40}\ 10^{50}-11^{10}.\ =\ 1^{30}-24.\ \smile^{1-2}\ 0^{00}-9^{00}\ \smile^{0}\ 19^{00}-24$
22	7	.	7	-	$=\ 0^{00}-11^{30}.\ \smile^{0}\ 0^{00}-12^{00}$
23	6	0.9	6	-	$*^{0}\ 7^{04}.\ 14^{50}-21^{40}-24.\ =\ 8^{40}-19^{30}$
24	6	0.0	10	-	$*^{0}\ 0^{00}-6^{20}.\ 7^{40}-9^{15}\ \leftrightarrow\ 9^{28}-10^{00}.\ =\ 1^{00}-24$
25	6	0.0	10	-	$*^{0}\ 6^{50}-10^{35}.\ 11^{50}-24.\ =\ 0^{00}-24$
26	6	.	10	-	$*^{0}\ 3^{40}-4^{05}.\ =\ 4^{10}-24.\ \smile^{0}\ 1^{00}-11^{00}\ \smile^{1}\ 20^{00}-24$
27	6	.	10	-	$=\ 0^{00}-24.\ \smile^{1}\ 0^{00}-9^{00}$
28	5	.	10	-	$=\ 0^{00}-11^{10}\ \infty-13^{20}$
29	7	.	9	-	
30	7	0.0	9	-	$\triangle\ 20^{10-20}\ *^{0}-21^{05}$
31	7	2.2	5	-	$\bullet^{0}\ 13^{40}-15^{50}.\ 21^{36}-22^{52}$
Σ	—	16.6	—	-	UWAGI.

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1	6	0.0	4	-	$=\ 6^{10}-19^{30}$
2	5	1.7	pż.	-	$\bullet^{0}\ 6^{20}\ 7^{40}\ \bullet^{0}-8^{10}.\ \bullet^{0}\ 10^{20-26}\ \bullet^{0}-14^{06}\ \bullet^{0}\ 16^{19}\ 17^{10}.\ =\ 6^{10}-24.\ \varphi\ 21^{45}-22^{20}$
3	5	0.0	pż.	-	$=\ 0^{00}-11^{40}.\ \smile\ na-a$
4	5	0.0	pż.	-	$\triangledown^{0}\ 0^{36}-1^{10}\ *^{0}\ 7^{45}-8^{15}\ \triangledown\ 11^{02}-12^{15}.\ =\ na-a,\ p-np$
5	7	.	pż.	-	$=\ 17^{30}-24$
6	8	.	pż.	-	
7	7	0.1	pż.	-	$\triangle\ 14^{45}-16^{45}\ *^{0}\ 17^{10}-24.\ =\ 14^{10}-24$
8	7	1.3	1	-	$*^{0}\ 0^{00}-1^{10}\ \triangledown^{0}\ 11^{12-24}\ \bullet^{0}\ 15^{14}\ 16^{38}\ *^{0}\ 23^{35}-24.\ =\ na.\ \oplus\ a$
9	7	1.3	1	-	$*^{0}\ 0^{00}-4^{10}\ =\ 0^{00}-10^{40}$
10	5	4.9	5	-	$*^{0}\ 2^{45}-11^{30}\ \bullet-12^{50}\ \bullet^{0}-13^{40}\ *^{0}\ 15^{10}-16^{45}\ \bullet^{0}-17^{50}\ *^{0}\ 19^{35}-24.\ =\ na-24$
11	7	.	1	-	$*^{0}\ 0^{00}-4^{20}.\ =\ 0^{00}-11^{10}$
12	6	0.6	pż.	-	$\bullet^{0}\ 10^{15}-12^{20}\ 13^{05}\ 16^{20}.\ =\ 10^{10}-24$
13	5	2.1	.	-	$\bullet^{0}\ 5^{10}-6^{20}\ \bullet^{0}-8^{24}\ \bullet^{0}-8^{45}.\ 11^{40}-12^{50}\ \triangle^{0}\ 14^{48}-15^{05}\ *^{0}\ 17^{46}-22^{45}.\ =\ 0^{00}-24$
14	8	.	pż.	-	$=\ 0^{00}-4^{20}$
15	7	.	.	-	$=\ 16^{25}-20^{10}.\ \smile^{0}\ 0^{00}-8^{00}$
16	6	0.1	.	-	$\bullet^{0}\ 11^{40}-13^{35}.\ =\ 11^{30}-10^{45}\ \equiv^{0}-23^{30}\ =-24.\ \smile^{0}\ 2^{00}-9^{00}$
17	6	0.1	.	-	$\bullet\ 2^{50}-4^{30}.\ 5^{30}-6^{10}.\ 7^{38}-11^{16}.\ 14^{40}-15^{10}.\ 17^{38}-22^{40}.\ =\ 0^{00}-24$
18	7	.	.	-	$=\ 0^{00}-10^{40}$
19	7	0.0	.	-	$\bullet^{0}\ 15^{40}-18^{35}.\ 21^{38}-24.\ =\ 14^{15}-24$
20	5	0.0	.	-	$\bullet^{0}\ 0^{00}-1^{40}.\ 2^{40}-4^{10}.\ p.\ =\ 0^{00}-20^{20}$
21	7	.	.	-	$=\ 6^{20}-10^{28}$
22	6	.	.	-	$=\ 6^{10}-24$
23	6	.	.	-	$=\ 0^{00}-24$
24	6	.	.	-	$=\ 0^{00}-20^{15}.\ 23^{58}-24$
25	6	.	.	-	$=\ 0^{00}-12^{50}$
26	7	.	.	-	$=\ 2^{20}-11^{40}.\ \smile^{0}\ 1^{00}-9^{00}$
27	7	.	.	-	$=\ 5^{20}-9^{15}.\ \smile^{0}\ 0^{00}-8^{00}$
28	7	0.5	.	-	$\bullet^{0}\ 22^{40}-24$
29					
30					
31					
Σ	—	12.7	—	-	UWAGI.

Przemyśl — $\varphi = 49°48'$ — $\lambda = 22°46'$ — Marzec – Mars 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	87.8	89.4	93.2	90.1	2.2	4.3	2.5	2.9	6.4	1.9	89	85	89	88	0.8	1.2	0.8	0.9	10	10	6	C 0	W 3	W 2
2	97.5	98.6	98.7	98.3	1.1	5.0	1.7	2.4	5.7	1.1	94	60	90	81	0.4	3.5	0.6	1.5	8	9	9	W 2	WNW 4	C 0
3	98.8	100.6	102.8	100.7	0.8	4.0	1.8	2.1	5.0	0.7	90	85	85	87	0.7	1.2	1.1	1.0	9	8	3	W 1	NW 2	NW 1
4	104.3	105.6	106.1	105.3	0.2	4.8	3.9	3.2	5.0	-1.1	96	76	97	90	0.3	2.0	0.3	0.9	10	10	10	NW 1	NW 1	WNW 2
5	105.9	102.2	103.5	103.2	4.2	8.6	4.3	5.4	8.9	2.5	85	60	85	77	1.2	4.5	1.2	2.3	10	8	2	W 6	W 9	W 6
6	104.1	104.2	102.7	103.7	3.3	7.1	4.1	4.6	8.0	3.1	83	64	85	77	1.3	3.6	1.2	2.0	9	5	0	WNW 4	WNW 6	WNW 3
7	100.2	97.5	97.7	98.5	2.3	11.1	7.6	7.2	11.6	1.8	91	58	77	75	0.6	5.5	2.3	2.8	8	8 ⊙	4	W 4	W 7	WNW 4
8	102.5	103.2	101.2	102.3	1.8	10.2	7.0	6.5	11.3	1.7	93	46	75	71	0.6	6.7	2.4	3.2	2	1 ⊙	0	W 3	WNW 7	WNW 3
9	100.5	98.7	98.4	99.2	5.5	10.8	11.0	9.6	12.8	4.8	88	66	67	74	1.1	4.5	4.3	3.3	10	3 ⊙	10	WNW 5	NW 8	WNW 5
10	98.1	97.6	95.2	97.0	6.1	14.8	8.1	9.3	16.7	5.5	77	51	83	70	2.1	8.2	1.8	4.0	2 ⊙	5 ⊙	0	W 4	W 6	W 1
11	93.0	92.9	95.9	93.9	9.6	15.5	11.3	11.9	15.6	4.6	63	48	63	58	4.5	9.2	5.0	6.2	7	5	10	WNW 5	WNW 7	W 5
12	93.1	91.1	83.6	89.3	8.3	10.3	11.8	10.6	11.9	8.0	79	55	56	63	2.3	5.8	6.1	4.7	10	9	8	W 4	W 7	W 6
13	74.5	77.0	81.2	77.6	7.8	8.0	2.6	5.2	13.1	1.5	80	51	79	70	2.1	5.2	1.6	3.0	8	10	10	WNW 8	WNW 10	NW 6
14	84.2	84.3	84.8	84.4	1.8	6.6	5.0	4.6	7.7	1.7	69	58	86	64	2.2	6.0	1.2	3.1	6	3	10	W 6	WNW 6	W 4
15	85.5	84.5	89.5	85.8	8.4	11.1	9.6	9.7	12.4	4.5	85	60	58	68	1.6	5.2	5.1	4.0	10	9	0	W 7	W 10	W 7
16	90.6	86.2	87.8	88.2	7.8	11.8	7.5	8.6	12.1	5.9	82	59	75	72	2.0	9.6	2.7	5.4	9	9	0	W 5	W 10	NW 9
17	94.4	93.5	90.5	92.8	5.1	11.2	8.6	8.4	12.5	4.8	86	57	61	68	1.3	5.7	4.4	3.8	3 ⊙	6 ⊙	0	WNW 5	W 6	W 3
18	83.1	78.6	75.5	79.1	9.0	18.4	14.7	14.2	19.1	6.8	57	30	47	45	5.0	14.8	8.8	9.5	3	3 ⊙	0	W 5	SW 7	SW 4
19	75.2	76.8	76.9	76.3	6.7	3.9	3.7	4.5	14.7	2.4	67	92	88	82	3.3	0.7	1.0	1.7	10	10 •	0	NW 5	W 3	W 2
20	81.2	81.7	80.0	81.0	-0.6	1.0	-2.0	-0.9	4.0	-2.1	85	59	73	72	0.9	2.8	1.5	1.7	9 ⚹	8	0	NW 6	WNW 5	NW 1
21	71.3	69.6	69.8	70.2	2.8	4.7	3.7	3.7	5.4	-2.6	59	65	62	62	3.1	2.9	3.1	3.0	10	10	0	SW 6	SW 8	SW 5
22	76.2	80.5	85.8	80.8	1.4	3.7	-1.0	0.8	4.9	-1.3	79	56	85	73	1.4	3.6	0.9	2.0	9	6	2	W 4	NW 5	WNW 2
23	85.4	85.2	86.8	85.8	-2.7	1.2	2.8	1.0	2.8	-4.3	84	81	86	84	0.8	1.3	1.1	1.1	9	10 ✳	10	WNW 1	W 4	W 4
24	88.1	88.1	87.9	88.0	4.9	7.0	7.3	6.6	7.9	2.8	87	69	72	76	1.1	3.1	2.9	2.4	9	10	10	W 4	W 5	W 6
25	89.2	89.8	91.8	90.3	6.6	8.8	5.2	6.4	9.5	5.1	82	60	81	74	1.7	4.5	1.6	2.6	9	10	7	W 5	W 6	W 2
26	92.4	89.2	83.8	88.5	5.2	11.0	9.0	8.6	12.9	4.4	90	52	58	67	0.8	6.3	4.8	4.0	3 ⊙	9	0	W 1	WSW 5	W 2
27	78.0	79.3	79.1	78.8	9.0	6.8	3.7	5.8	9.9	3.7	65	46	56	55	4.2	5.3	3.6	4.4	10 •	10	1	W 5	W 6	WNW 3
28	80.8	81.4	81.0	81.1	0.0	1.3	1.0	0.8	3.8	-2.0	76	76	92	81	1.3	1.6	0.5	1.2	6 ✳	4	10 ✳	WNW 5	W 6	W 5
29	83.8	84.2	82.6	83.5	0.0	4.6	4.2	3.2	5.7	-0.2	82	65	80	76	1.1	3.0	1.6	1.9	8	9	10 •	WNW 5	W 5	W 5
30	81.7	80.2	79.0	80.3	5.3	11.9	7.8	8.2	12.0	3.0	77	50	82	70	2.1	6.9	2.0	3.7	2	10	10	SW 5	SW 6	W 2
31	75.3	76.5	80.2	78.0	8.4	4.1	3.8	5.0	10.7	2.3	85	92	95	91	1.6	0.7	0.4	0.9	10 •	10 •	10	W 3	NW 7	C 0
M	88.8	88.7	88.7	88.7	4.3	7.9	5.6	5.8	9.7	2.3	81	62	76	73	1.7	4.6	2.4	2.9	7.7	7.6	4.9	4.2	6.0	3.5

Kwiecień – Avril

1	83.6	82.2	77.5	81.2	2.1	10.2	10.8	8.5	12.4	1.8	57	39	56	51	3.0	7.5	5.7	5.4	1 ⊙	10	10	W 6	WSW 7	SW 8
2	81.4	83.4	82.2	82.3	4.2	7.6	7.2	6.6	10.9	3.3	90	71	80	80	0.8	3.0	2.1	2.0	10	9	10	W 4	W 5	C 0
3	77.4	77.4	80.9	78.6	9.9	13.8	8.7	10.3	15.7	5.0	89	64	85	79	1.3	5.7	1.6	2.9	10 •	9	0	W 3	WNW 6	C 0
4	81.5	81.1	86.9	83.2	5.2	16.7	10.2	10.6	18.4	2.3	98	50	87	78	0.1	9.6	1.6	3.8	1	9	8	C 0	SW 5	NW 1
5	88.0	87.2	86.6	87.3	7.2	15.2	13.4	12.3	21.3	6.6	93	79	70	81	0.8	3.7	4.7	3.1	10	7	0	N 1	NNE 1	SW 1
6	86.9	87.5	87.5	87.3	13.6	22.9	15.5	16.9	24.0	10.8	66	39	60	55	5.4	17.1	7.0	9.8	6	1 ⊙	0	C 0	W 4	C 0
7	87.2	85.7	85.5	86.1	13.3	24.8	18.5	18.8	25.0	10.5	69	32	54	52	4.8	21.3	9.8	12.0	0 ⊙	1 ⊙	0	SW 1	SW 10	SW 2
8	84.1	81.0	80.6	81.9	15.2	23.2	13.6	16.4	23.3	11.4	65	49	85	66	6.0	14.4	2.3	7.6	3 ⊙	4 ⊙	10 ↖	W 3	W 2	W 6
9	87.9	88.6	92.1	89.5	5.4	8.5	3.0	5.0	13.9	3.0	74	57	67	66	2.4	4.7	2.5	3.2	7 ⊙	6	0	W 6	WNW 7	NW 2
10	92.6	89.6	85.8	89.3	-0.8	8.8	5.9	5.0	8.9	-3.2	94	58	58	63	0.4	7.0	3.9	3.8	0 ⊙	8	10	NW 1	E 4	NE 3
11	82.4	81.5	82.2	82.0	4.4	11.9	9.7	8.9	14.1	4.0	82	61	70	71	1.5	5.3	3.5	3.4	9	5	0	N 1	N 2	N 3
12	86.3	89.1	91.3	88.9	3.8	10.4	6.3	6.7	10.9	1.0	75	46	66	62	2.0	5.8	3.2	3.7	9	8	0	C 0	NNW 3	C 0
13	89.3	87.8	87.2	88.1	1.3	18.3	13.4	11.6	19.8	-0.7	94	38	56	63	0.4	13.3	6.8	6.8	10	3 ⊙	0	W 1	WNW 3	W 2
14	87.4	86.8	85.8	86.7	10.0	22.8	15.4	15.9	23.8	7.8	72	23	46	47	3.5	21.4	9.5	11.5	0 ⊙	0 ⊙	0	W 2	SW 4	C 0
15	85.9	85.4	85.6	85.6	13.1	25.2	18.8	19.0	25.3	6.4	58	26	47	44	6.4	25.6	11.3	13.8	0 ⊙	3 ⊙	0	NW 1	WSW 7	C 0
16	85.4	83.5	83.3	84.1	13.6	21.8	14.3	16.0	22.4	10.9	79	40	58	59	3.4	15.6	6.8	8.6	9	9	8	SW 1	SW 3	W 4
17	84.5	84.0	85.1	84.5	8.3	18.3	12.4	12.9	19.3	4.8	92	46	85	74	1.0	11.6	2.2	4.9	0 ⊙	5 ⊙	0	NW 1	WNW 5	C 0
18	86.0	85.7	83.3	85.0	8.3	19.6	14.3	14.2	20.7	5.3	96	53	80	76	0.3	10.7	3.2	4.8	7	8	10	W 2	NW 1	C 0
19	84.4	85.6	85.8	85.3	12.2	17.3	13.0	13.9	17.7	11.3	98	69	68	78	0.3	6.2	4.8	3.8	9	9	10	NW 2	NE 1	N 3
20	86.3	88.4	91.9	88.9	8.3	13.3	7.0	9.0	14.2	6.9	84	55	60	66	1.7	7.0	4.0	4.2	9	8	5	N 5	NE 7	N 4
21	93.3	93.4	92.4	93.0	4.2	11.8	7.3	7.8	13.1	0.3	84	45	61	63	1.3	7.6	4.0	4.3	2 ⊙	1 ⊙	0	NE 2	ENE 9	E 3
22	90.8	87.8	85.0	87.9	4.2	16.2	9.8	10.0	17.0	0.6	75	43	63	60	2.0	10.6	4.3	5.7	0 ⊙	0 ⊙	0	ESE 1	E 5	E 4
23	84.1	82.2	81.7	82.7	5.4	15.6	8.3	9.3	16.3	2.0	86	35	62	61	1.3	11.3	4.2	5.7	0 ⊙	0 ⊙	0	E 2	ENE 8	E 6
24	82.7	82.9	83.7	83.1	7.0	10.0	8.3	8.4	10.7	4.7	78	69	79	75	2.2	5.8	2.3	2.8	9	9	10	E 7	E 9	E 9
25	84.4	84.6	84.6	84.3	6.8	9.4	10.3	9.2	10.9	6.4	86	76	69	77	1.3	2.8	3.9	2.7	10	10	10	E 7	E 9	NE 5
26	82.8	81.6	81.1	81.8	8.4	16.0	10.2	11.2	17.0	7.2	78	54	78	70	2.4	8.4	2.7	4.5	10	8	0	ENE 2	E 6	E 2
27	81.1	81.0	81.7	81.3	7.3	13.2	8.2	9.3	14.3	3.3	84	57	82	74	1.7	6.6	2.0	3.4	3 ⊙	9	2	NE 3	NNE 5	NNE 1
28	81.6	81.1	81.4	81.4	6.9	17.1	9.8	10.9	18.3	3.8	91	37	74	67	0.8	12.4	3.1	5.4	9	7	0	WNW 3	NW 2	NW 1
29	82.7	82.7	84.3	83.3	6.3	19.9	11.4	12.2	20.3	2.7	91	30	69	63	0.8	16.2	4.2	7.1	0 ⊙	5 ⊙	1	W 2	NE 3	NE 3
30	83.1	80.7	79.9	81.2	8.9	15.8	9.3	10.9	17.0	6.3	81	60	84	75	2.2	7.1	1.9	3.7	8	10	10	NE 3	SE 10	E 7
31																								
M	85.2	84.6	84.8	84.9	7.3	15.9	10.8	11.2	17.2	4.9	82	49	69	67	2.1	10.8	4.3	5.3	5.4	6.0	3.8	3.4	5.0	2.7

Przemyśl — $H_s = 237\,m$ — $H_b = 238{,}9\,m$ — $h_w = 20{,}6\,m$ — Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	0.0	.	-	●● $^{0}2^{50}-3^{30}$ ▽$^{0}15^{34}-48$; = $1^{30}-6^{20}$
2	7	0.0	.	-	✳ $^{0}21^{40}-22^{20}$; = $11^{40}-12^{15}$
3	6	0.6	.	-	●▽ $^{0}10^{25}-58$; = $5^{30}-10^{15}$ $12^{10}-24$
4	6	0.2	.	-	● $^{0-1}13^{40}-19^{10}$; = $0^{00}-24$ ⌣ $^{0}0^{00}-7^{00}$
5	7	0.0	.	-	● $^{0}16^{20}$ 17^{15} ; = $0^{00}-9^{40}$
6	7	.	.	-	= $5^{30}-8^{30}$
7	6	.	.	-	= $4^{40}-9^{30}$; ∞ $11^{15}-18^{40}$ =-24
8	8	.	.	-	= $0^{00}-8^{20}$ $17^{40}-22^{20}$
9	7	.	.	-	= $11^{12}-12^{10}$
10	6	.	.	-	= $5^{20}-7^{40}$ ∞ $11^{10}-19^{30}$ =-24 ; ⌓ $22^{00}-24$
11	7	.	.	-	= $0^{00}-1^{30}$; ⌒ $^{0}0^{00}-2^{00}$
12	7	3.4	.	-	= $2^{50}-10^{20}$ ∞ $10^{20}-11^{30}$
13	8	0.5	.	-	● $^{0}3^{35}-4^{15}$ $5^{10}-6^{20}$ ●▽ $^{0}18^{25}-19^{40}$ ✳▽ $^{0}19^{50}-20^{20}$; ≫ $12^{15}-16^{30}$
14	8	0.3	.	-	● $^{0}22^{45}-24$; = $22^{50}-24$
15	8	0.1	.	-	● $^{0}0^{00}-30$ ● $^{0}7^{25}-50$ $8^{40}-9^{55}$; = $0^{00}-1^{50}$; ≫ $11^{10}-14^{30}$
16	7	1.0	.	-	● $^{0}6^{45}-7^{50}$ ▽ $^{0}19^{10}-30$; ↖ $^{1}19^{10}-45$; ≫ $11^{15}-14^{30}$
17	7	.	.	-	
18	8	.	.	-	
19	6	3.6	.	-	● $^{0}7^{55}-13^{40}$; = $7^{30}-21^{20}$
20	8	0.0	.	-	⚹ $6^{20}-40$ $7^{30}-35$ ✳▽ $^{0}9^{55}-10^{05}$ ⌣ $^{0}20^{00}-24$
21	8	.	.	-	⌣ $^{0}0^{00}-5^{00}$
22	7	0.6	.	-	✳▽ $^{0}7^{05}-8^{12}$ $8^{40}-9^{00}$ ✳▽ $^{0}11^{41}-14^{21}$ ⚹ $^{0-1}15^{34}-16^{30}$ ✳▽ $^{0-1}17^{50}$
23	7	0.3	2	-	✳ $^{0}8^{20}-14^{30}$ ● $^{0}17^{45}-19^{10}$; = $17^{15}-21^{30}$
24	7	0.0	.	-	● $^{0}1^{06}$ 2^{30} $15^{25}-16^{15}$ ● $^{0}19^{40}-20^{10}$; = $2^{42}-5^{35}$; $21^{40}-24$
25	7	0.0	.	-	● $^{0}0^{50}-1^{20}$; $3^{50}-4^{40}$ ▽ $^{0}15^{03}-10$; = $0^{00}-9^{40}$
26	8	0.0	.	-	
27	7	0.6	.	-	● $^{0}6^{05}-8^{40}$ $9^{20}-11^{22}$
28	8	3.7	p2.	-	✳▽ $^{0-2}1^{50}$ 2^{10}
29	8	0.7	3	-	✳▽ $^{0}0^{40}-4^{20}$ ● $^{0}13^{45}-14^{15}$; 20^{25} 24
30	8	0.4	.	-	● $^{0}0^{00}-2^{35}$; $14^{31}-15^{20}$ 16^{10} 17^{28} ; ⊕ $^{0}12^{10}-13^{00}$
31	6	5.0	.	-	● $^{0}4^{05}$ 9^{55} ● $^{0-1}10^{05}-17^{15}$
Σ	—	21.0	—	-	UWAGI.

Kwiecień – Avril

1	8	3.0	.	-	● $^{0}21^{45}$ 22^{20} ; 23^{35-55} ≫ $7^{30}-10^{20}$; $13^{20}-15^{40}$
2	8	6.3	.	-	● $^{0}0^{05}-5^{20}$; $20^{35}-22^{20}$
3	8	3.6	.	-	● $^{0-1}4^{5}-9^{10}$
4	8	0.3	.	-	▽ $^{0}12^{50}$ 13^{50} ; ≡ $^{0}3^{50}-4^{40}$
5	7	.	.	-	● $^{0}5^{50}$ 6^{06} ; = $4^{20}-5^{10}$; $6^{12}-12^{20}$; ⌒ $^{1}20^{00}-24$
6	8	.	.	-	⌒ $^{1}0^{00}-9^{00}$; $22^{00}-24$
7	8	.	.	-	≫ 12^{15} 13^{40} ; ⌒ $^{0}0^{00}-7^{00}$
8	8	2.6	.	-	▽ $^{0}13^{48}$ 14^{15} ; $18^{45}-19^{28}$; ↖ $^{0}13^{35}$ 14^{40} S-E ; $18^{40}-20^{34}$
9	8	.	.	-	▽ $^{0}0^{28}-46$
10	8	.	.	-	⌣ $^{0}3^{00}-7^{00}$; ⊕ $^{1}11^{20}-15^{06}$
11	7	0.0	.	-	● $^{0}7^{40}-8^{10}$; ⌒ $^{0}21^{00}-24$
12	8	.	.	-	⌒ $^{0}0^{00}-7^{00}$; $21^{00}-24$
13	8	.	.	-	⌒ $^{2}0^{00}-8^{00}$; ⊕ $^{1}5^{40}-8^{20}$
14	8	.	.	-	
15	8	.0.4	.	-	↖ $^{0}23^{50}-24$
16	8	0.6	.	-	▽ $^{0}0^{03}-30$ $13^{02}-20$; 14^{45} 15^{10} ; ↖ $^{0}0^{00}-45$ $12^{45}-13^{50}$ SW-NE ; $14^{40}-15^{50}$ SW-NE
17	8	.	.	-	⌒ $^{2-0}1^{00}-9^{00}$ ⌒ $^{0}20^{00}-24$
18	8	1.4	.	-	● $^{0}23^{40}-24$; = $0^{30}-8^{28}$; ⌒ $^{2}0^{00}-8^{00}$
19	7	.	.	-	● $^{0}0^{00}-4^{50}$
20	8	.	.	-	
21	8	.	.	-	⌒ $^{0}3^{00}-7^{00}$
22	8	.	.	-	⌣ $^{0}4^{00}-5^{00}$
23	8	.	.	-	⌣ $^{0}4^{00}-6^{00}$
24	8	.	.	-	
25	8	0.2	.	-	
26	8	.	.	-	● $^{0}1^{20}-2^{10}$ ● $^{0}3^{25}-45$
27	8	.	.	-	= $^{1-0}3^{50}-5^{40}$ = - 6^{20} ; ⌒ $^{0}20^{00}-24$
28	7	.	.	-	
29	8	.	.	-	= $1^{40}-8^{20}$ ⌒ $^{2}1^{00}-8^{00}$
30	7	.	.	-	≫ $12^{20}-13^{30}$; $14^{35}-15^{20}$; ⊕ $^{0}10^{26}-12^{25}$
31					
Σ	—	18.6	—	-	UWAGI.

Przemyśl — φ = 49°48' — λ = 22°46' — Maj - Mai 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	79.7	81.4	83.7	81.6	8.5	10.2	9.7	9.5	10.5	8.0	97	91	91	93	0.3	1.1	1.1	0.8	10	10	10	E 4	NE 5	NNE 2
2	84.5	84.9	84.4	84.6	9.6	15.6	12.6	12.6	17.4	8.3	96	66	82	81	0.5	6.0	2.6	3.0	10	8	8	N 2	SW 2	C 0
3	84.3	83.7	84.6	84.2	8.4	18.8	12.4	13.0	20.0	5.3	100	55	88	81	0.0	9.7	1.7	3.8	1 ≡ ⊙	6 ⊙	2	NW 1	NE 2	W 1
4	86.3	87.9	89.0	87.7	11.5	12.2	10.7	11.5	14.2	7.0	90	98	99	96	1.4	0.3	0.2	0.6	8	10 • ₹	0	W 3	NW 2	C 0
5	91.7	91.9	90.9	91.5	6.9	18.2	13.1	12.8	19.0	4.3	100	54	72	75	0.0	9.5	4.3	4.6	0 ≡	4 ⊙	0	WNW 2	E 3	C 0
6	89.8	88.5	87.7	88.7	12.4	21.4	18.0	17.4	25.5	6.9	81	50	68	66	2.7	12.8	6.5	7.3	5	9	10	C 0	SW 5	SW 1
7	88.8	88.2	84.2	87.1	13.0	15.3	13.2	13.2	18.5	12.7	100	95	94	96	0.0	1.1	0.9	0.7	10	10 •	10	NW 1	NW 1	C 0
8	85.7	84.7	84.2	84.9	9.7	14.3	7.9	10.0	16.2	7.8	84	59	80	74	1.9	6.6	2.0	3.5	9	8	3	W 3	W 4	W 4
9	83.2	80.9	79.9	81.3	8.8	11.5	7.6	8.9	13.8	5.3	80	63	97	80	2.3	5.0	0.3	2.5	9	9	8	W 3	W 4	W 1
10	80.4	81.1	82.5	81.3	8.6	9.5	8.3	8.7	12.9	6.5	89	91	84	88	1.3	1.1	1.7	1.4	8	9	9	W 4	W 3	W 3
11	84.3	85.0	86.2	85.2	7.3	10.9	8.0	8.6	11.3	4.8	87	67	84	79	1.3	4.3	1.6	2.4	10	8	10	WNW 3	NW 3	NNW 5
12	85.2	85.2	86.6	85.7	5.9	5.0	5.4	5.4	8.1	4.3	85	90	94	90	1.4	0.8	0.6	0.9	10	10	10 •	NW 7	NW 7	W 2
13	87.7	87.5	87.5	87.6	6.4	11.8	8.4	8.8	12.5	3.2	88	57	70	72	1.1	5.9	3.3	3.4	9	9	2	W 2	W 4	C 0
14	85.8	84.8	83.0	84.5	11.2	14.5	8.2	10.5	16.5	5.6	60	51	86	66	5.3	8.1	1.5	5.0	9	8	10	WSW 5	SW 7	NW 7
15	83.3	84.2	84.8	84.1	6.2	12.3	7.8	8.5	13.6	4.1	98	64	83	82	0.2	5.1	1.8	2.4	10 ≡	6	1	WNW 2	WNW 3	WNW 1
16	85.3	85.1	84.6	85.0	8.4	11.7	6.9	8.5	13.5	5.3	83	54	80	72	1.8	6.2	2.0	3.3	4 ⊙	8	0	W 3	NW 4	C 0
17	84.0	84.5	85.3	84.6	6.2	9.6	10.4	9.2	14.8	1.0	95	87	80	87	0.5	1.6	2.6	1.6	1	8 •	10	W 1	W 3	NW 2
18	86.1	86.6	87.1	86.6	8.8	11.3	7.7	8.9	12.3	7.5	93	65	89	82	0.8	4.7	1.2	2.2	10	9	5	NW 5	NW 5	C 0
19	86.4	86.1	85.8	86.1	7.4	14.0	9.3	10.0	15.5	2.2	88	52	78	73	1.2	7.7	2.6	3.8	2	6 ⊙	1	NW 2	NW 3	W 1
20	84.3	80.2	78.9	81.1	6.6	19.2	13.9	13.4	20.4	2.4	94	41	60	65	0.5	13.0	6.4	6.6	0 ⊙	7 ⊙	4	NW 1	SE 4	NE 1
21	78.7	78.5	79.6	78.9	10.4	13.8	11.0	11.6	14.7	9.1	95	81	91	89	0.6	3.0	1.1	1.6	10 •	10	10 •	NNE 3	NNE 1	NE 1
22	79.8	79.0	80.9	79.9	10.8	14.4	11.2	11.9	16.9	9.1	92	75	71	79	1.0	4.1	3.9	3.0	9	9 •	4	NW 1	NW 6	NW 5
23	83.6	84.8	85.3	84.6	9.9	13.7	8.7	10.2	15.3	6.5	79	51	85	72	2.5	7.6	1.6	3.9	7	8	0	NW 1	NW 5	C 0
24	86.9	87.2	87.3	87.1	9.6	16.5	11.8	12.4	17.7	2.8	82	41	80	68	2.2	11.0	2.8	5.3	3 ⊙	8	8	W 1	C 0	NW 1
25	87.5	86.4	85.1	86.3	11.4	17.3	11.9	13.1	18.7	9.1	80	61	84	75	2.7	7.6	2.1	4.1	8	9	3	WNW 2	C 0	C 0
26	85.1	84.4	83.2	84.2	11.3	21.3	14.9	15.6	22.1	6.8	84	39	63	62	2.2	15.3	6.2	7.9	2 ⊙	4 ⊙	1	C 0	N 3	C 0
27	83.1	82.3	81.9	82.4	14.2	23.0	15.0	16.8	24.0	6.8	75	43	75	64	4.1	16.1	4.1	8.1	9	5	0	C 0	W 2	C 0
28	82.7	82.3	81.1	82.0	13.2	15.8	14.9	14.7	22.0	10.3	88	84	94	89	1.8	2.8	0.9	1.8	9	9 (₹)	2	C 0	N 1	C 0
29	79.3	74.1	69.6	74.3	13.2	23.6	17.1	17.8	24.7	11.7	94	52	82	76	0.9	14.0	3.5	6.1	10	2 ⊙	9	NW 1	E 7	W 1
30	72.0	73.7	75.2	73.6	16.2	18.1	14.8	16.0	20.0	14.1	92	73	73	79	1.6	5.6	4.5	3.9	9	9	2	C 0	NW 5	WNW 1
31	78.7	79.0	79.5	79.1	11.8	18.0	14.6	14.8	20.0	9.4	81	56	76	71	2.6	9.1	4.0	5.2	6	8	9	W 3	NW 1	C 0
M	84.0	83.7	83.5	83.7	9.8	14.9	11.1	11.7	16.8	6.7	88	65	82	78	1.5	6.7	2.6	3.6	7.0	7.8	5.2	2.1	3.3	1.3

Czerwiec - Juin

1	79.7	79.0	78.7	79.1	16.7	25.3	18.8	19.4	25.4	7.4	73	45	66	61	5.2	15.6	7.3	9.4	0 ⊙	3 ⊙	1	C 0	W 2	C 0
2	78.6	78.3	78.3	78.4	19.2	22.0	16.3	18.4	24.7	13.8	73	68	82	74	6.0	8.3	3.2	5.8	3 ⊙	9 • ₹	2	C 0	W 4	C 0
3	78.3	78.1	79.8	78.7	15.4	23.2	14.1	16.7	25.0	11.3	92	65	95	84	1.3	10.0	0.7	4.0	8	3	8	WNW 2	WNW 4	C 0
4	80.6	80.5	81.8	81.0	15.2	17.0	14.7	15.4	22.8	12.0	94	83	97	91	1.0	3.4	0.3	1.6	3 ⊙	9 • ₹	4	W 1	NW 5	N 1
5	84.3	86.0	87.1	85.8	15.8	20.8	15.3	16.8	22.3	13.0	96	67	94	86	0.7	8.2	1.0	3.3	10	9	9	N 2	NE 4	NE 2
6	86.9	86.3	85.6	86.3	15.9	19.1	16.3	17.0	19.3	14.2	96	78	90	88	0.8	4.8	2.0	2.5	10	10	9	ENE 3	SE 8	ENE 3
7	84.7	83.3	82.8	83.7	16.0	21.3	15.6	17.2	22.7	14.0	92	70	91	84	1.6	7.8	1.3	3.6	9	8	4	ENE 1	ENE 4	C 0
8	83.7	83.7	83.4	83.6	17.4	18.8	17.2	17.6	24.2	14.9	83	69	89	80	3.4	6.7	2.2	4.1	9	7	4	C 0	WNW 5	W 1
9	84.5	84.3	84.8	84.5	17.5	24.6	17.4	19.2	25.4	12.8	84	54	85	74	3.2	14.3	3.0	6.8	0 ⊙	4 ⊙	1	W 2	NE 2	C 0
10	85.6	85.3	85.5	85.5	15.2	25.7	17.0	18.7	26.0	11.3	91	46	75	71	1.5	17.9	4.9	8.1	0	6	3	W 1	E 3	C 0
11	85.2	84.0	83.3	84.2	16.3	25.1	15.9	18.3	25.5	11.8	80	46	90	72	3.6	17.0	1.8	7.5	7	4 ⊙	5	SW 1	SW 2	C 0
12	83.3	82.3	82.3	82.6	15.9	21.1	16.9	17.7	22.2	13.4	90	65	94	83	1.8	8.7	1.2	3.9	9	6 ⊙	10	W 2	NW 4	W 1
13	82.4	81.8	80.3	81.5	13.9	19.5	17.1	16.9	21.0	13.5	95	67	84	82	0.7	7.5	3.2	3.8	10 •	5	7	WNW 2	WNW 2	C 0
14	78.9	80.5	84.3	81.2	15.3	17.9	12.6	14.6	18.0	12.6	96	80	91	89	0.8	4.0	1.4	2.1	10 •	9	0	E 1	C 0	W 1
15	86.2	87.5	88.0	87.2	14.0	17.5	15.1	15.4	18.7	10.4	82	58	74	71	2.9	8.4	4.4	5.2	9	6	10	W 3	W 3	C 0
16	89.8	89.7	90.2	89.9	15.6	17.4	13.4	14.4	19.0	11.4	74	50	70	65	4.0	10.0	4.7	6.2	0 ⊙	2 ⊙	0	WNW 1	WNW 5	C 0
17	91.9	92.1	91.6	91.9	13.3	19.8	14.6	15.6	21.5	8.3	79	52	79	70	3.2	11.2	3.4	5.9	0 ⊙	4 ⊙	0	W 2	NW 3	C 0
18	91.9	91.1	89.0	90.7	12.8	23.3	19.8	18.9	25.5	9.3	88	45	68	67	1.8	15.6	7.3	8.2	4 ⊙	9	0	W 1	W 2	C 0
19	89.5	89.4	90.7	89.9	19.6	28.4	20.8	22.4	29.0	16.2	68	51	86	68	7.3	19.0	3.4	9.9	0 ⊙	3 ⊙	10	W 3	W 4	NW 3
20	95.6	96.1	96.2	96.0	16.1	19.4	15.7	16.7	20.8	14.9	67	43	64	58	6.0	12.8	6.4	8.4	2	6	7	NW 5	NW 4	NNW 3
21	96.4	95.6	93.1	94.4	13.1	21.8	18.1	17.8	23.4	7.9	82	52	79	71	2.8	12.7	4.5	6.7	0	2	8	C 0	SE 3	N 1
22	97.5	96.2	92.0	95.2	14.6	21.1	17.8	17.8	23.4	12.6	81	61	79	74	5.1	9.7	4.2	5.7	1 ⊙	0 ⊙	0	W 2	W 1	C 0
23	87.3	89.3	90.6	89.1	16.6	20.7	18.1	18.4	22.6	13.6	79	73	73	76	4.1	6.5	5.3	5.3	10 •	8	0	W 4	NW 5	NW 1
24	91.9	91.4	92.1	91.8	16.8	25.3	19.1	20.1	26.0	13.3	84	49	61	65	3.1	16.3	8.7	9.4	0	6	3	WNW 1	WNW 5	NW 2
25	92.1	90.2	87.3	89.9	16.6	27.3	22.8	22.4	28.7	11.1	85	43	60	63	2.9	20.7	11.1	11.6	0 ⊙	2 ⊙	0	WNW 1	W 3	W 1
26	87.1	86.0	85.9	86.3	25.6	29.7	20.3	25.3	30.6	19.2	69	33	82	68	9.0	19.4	4.4	10.9	0 ⊙	4 ⊙	8	W 1	SW 6	NW 1
27	84.9	84.1	82.6	83.9	22.1	31.1	24.3	25.6	24.3	15.8	73	34	54	54	7.3	30.0	14.2	17.2	0 ⊙	1 ⊙	6	NW 1	SSW 7	SW 1
28	83.4	91.6	97.0	90.7	22.3	14.3	12.2	15.3	25.1	12.1	80	94	85	86	5.4	0.9	2.2	2.8	4	10 •	0	W 3	WNW 5	WNW 3
29	99.3	99.2	98.4	99.0	15.4	18.2	16.2	16.0	19.6	8.7	80	58	76	71	3.2	8.8	4.4	5.3	1	10	10	W 3	NW 4	NW 4
30	99.9	98.3	96.6	98.3	14.4	20.3	16.9	17.2	22.3	13.2	89	57	74	73	1.8	10.3	5.0	5.8	10	7	0	NW 1	NW 3	C 0
31																								
M	87.4	87.3	87.3	87.3	16.3	21.8	17.0	18.0	23.3	12.3	83	59	80	74	3.3	11.6	4.2	6.4	4.3	5.7	4.3	1.7	3.8	1.0

Przemyśl

$H_1 = 237\,m$ $H_2 = 238.9\,m$ $h_w = 20.6\,m$

Maj – Mai 1961

DNI	WIDZIALNOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	7	.	.	–	= 5²⁵–7⁴⁰, 23⁵⁰–24
2	7	.	.	–	= 0⁰⁰–7²⁰
3	7	0.0	.	–	•° 11⁰³–15, = 1³⁰–3⁴⁵ ≡⁰⁻¹–6⁵⁰ = –8³⁰ np; ⌒⁰⁻¹ na–a, np
4	6	7.0	.	–	▽° 7⁰² 8⁴⁰ 10³⁰–⁴⁰ •° 10⁵² 11¹⁰ ▽¹⁻⁰ 11³⁰–13⁴⁰ •° 14⁴⁵–⁵⁸; ↖° 11³⁰–12⁴⁰, = na, a, p, np; ⌒¹ na
5	8	.	.	–	= 0⁰⁰–2⁵⁰ ≡⁰⁻¹–4⁴⁵ = –5²⁰ ≡°–7³⁰ = –8⁴⁵
6	8	0.5	.	–	•° 23⁰⁶ 24, = 3⁴⁰–4²⁰, ⌒¹ 1⁰⁰–8⁰⁰
7	6	12.9	.	–	•° 0⁰⁰–¹⁰ 4¹⁰ 5⁰⁵ •° 5²⁰–6⁰⁴ 7²⁰–8⁴⁰ •⁰⁻¹–12⁵⁰ ▽° 21⁰⁵–³⁰, = na, a
8	7	5.2	.	–	▽° 1³⁵ 2⁴⁰ 13⁴³–⁴⁷ 14¹⁹–15¹³; ↖° 14⁰⁰–15¹⁶ NW–SE
9	8	2.7	.	–	▽° 7⁵⁰ 10²⁰, ↖° 18⁵⁰–19²⁵
10	8	1.0	.	–	▽° 0¹⁵–³⁶, 12⁰¹ 16¹⁷, 22⁰²–¹⁵
11	8	0.0	.	–	▽° 11⁰⁰–⁰⁶
12	7	0.0	.	–	•° 20²⁰ 21⁰⁶ = 3³⁰–6²⁰
13	8	.	.	–	= 19⁴⁰–24, ⌒¹ 20⁰⁰–24
14	8	8.2	.	–	▽¹⁻² 21¹⁵–23⁴⁵, = 0⁰⁰–3⁵⁰, ⌒¹ 0⁰⁰–9⁰⁰
15	7	0.0	.	–	▽° 11⁵⁰–12⁰⁵, = 3¹⁰–⁴⁵ ≡°–7¹⁰ = –7²⁰, 19⁴⁰–24
16	7	0.1	.	–	= 0⁰⁰–4⁴⁰, ⌒¹ 1⁰⁰–7⁰⁰, ⌒° 20⁰⁰–24
17	7	0.7	.	–	▽° 5³⁰–6¹⁰, 11¹⁸–³⁷, 12¹⁰–⁴², = na, a, np, ⌒° na
18	7	0.0	.	–	•° 4³⁰–⁴⁵ 5²⁰ 6¹⁵ ▽° 11⁴⁰–12¹⁰, = 0⁰⁰–4²⁰, 6²⁰–10¹⁵
19	8	.	.	–	= 1³⁰–7⁴⁰ 19⁴⁰–24
20	7	0.5	.	–	= 0⁰⁰–3³⁵, 6⁰⁵–9⁴⁰, ⌒² 1⁰⁰–9⁰⁰
21	7	9.4	.	–	•° 4⁴⁰ 9³⁵ ▽¹ 12⁴⁵–13¹³ 13⁴⁰–14²⁰ •° 17⁴⁰ 22²⁰, = na–a, np
22	7	10.0	.	–	▽⁰⁻² 10⁵⁵ 15⁴⁵, ↖¹ 13⁵²–⁴⁰ ↖° 15¹⁰–²⁵, = 0⁰⁰–8⁴⁵
23	8	.	.	–	⌒¹ 20⁰⁰–24
24	8	.	.	–	= 3³⁰–4⁵⁰, ⌒¹ 0⁰⁰–7⁰⁰
25	7	0.0	.	–	▽° 12⁵⁵–13¹⁰, = 18³⁰–24, ⌒¹ 1⁰⁰–7⁰⁰ ⌒° 20⁰⁰–24
26	8	.	.	–	= 0⁰⁰–7¹⁰, ⌒² 0⁰⁰–9⁰⁰ ⌒¹ 19⁰⁰–24
27	7	0.2	.	–	▽° 15⁴⁰–16²⁰ (↖)° 12⁵⁵–16⁴⁰, ⌒¹ 0⁰⁰–8⁰⁰
28	7	33.6	.	–	▽²⁻⁰ 12¹⁰–⁵⁵ ▲¹ 12⁷⁵–⁷⁸ ▽²⁻¹ 14⁵⁰–15¹⁰ ▽° 15⁴⁰–16²⁰ ↖¹ 11⁴⁵–16⁵⁰ S–NE, = na–a, np; ⌒¹ 2⁰⁰–9⁰⁰
29	7	1.9	.	–	= 2³⁰–11³⁶, ⌒° 21⁰⁰–24
30	7	1.2	.	–	•⁰⁻¹ 0⁰⁵–1⁵² ▽° 14⁰⁵–⁴⁵ 16³⁵–⁴⁰, = 6⁴⁰–8³⁰, 23²⁰–24
31	7	.	.	–	= 0⁰⁰–10³⁰, ⌒² 2⁰⁰–9⁰⁰
Σ	–	75.1	–	–	UWAGI.

Czerwiec – Juin

1	8	.	.	–	= 0⁰⁰–2²⁰, ⌒² 0⁰⁰–7⁰⁰
2	7	10.0	.	–	▽° 11⁴⁰–⁵⁵, ▽⁰⁻² 13²⁵–15²⁰ ▽° 15⁵⁰–16⁰⁵, (↖) 10⁵⁵–13²⁰ ↖¹–15³⁰, = 4³⁰–7²⁰
3	8	10.3	.	–	▽° 8⁵⁰ 9²⁰ ▽¹ 15²⁰ 19²⁰, ↖¹ 14⁵⁰–18⁴⁰, = 2⁰⁰–4²⁰ np
4	7	13.6	.	–	▽° 13¹⁰–³⁵ 16¹⁵–³⁰ ▽°–19²⁰ ↖° 13⁰⁶–18⁴⁵, = 0⁰⁰–⁵⁰ ≡° 2⁴⁰ = na, np
5	7	5.6	.	–	▽²⁻⁰ 10⁰⁰–11²⁰ ▽¹⁻⁰ 18¹⁵–20⁴⁰, = 0⁰⁰–9⁴⁰, a, np
6	7	.	.	–	= na–a
7	8	1.3	.	–	▽° 14²⁵–⁵⁰, 16⁴⁵–17⁵⁰, 18³⁵–19⁴⁵, ↖° 14¹⁵–15⁵⁰, = 3³⁰–9⁴⁰, ⌒¹ 3⁰⁰–7⁰⁰
8	8	.	.	–	▽° 0⁵⁷–1⁴⁰, (↖) 13¹⁰–14⁴⁰, ⌒° 20⁰⁰–24
9	8	.	.	–	⌒¹ 0⁰⁰–9⁰⁰, 21⁰⁰–24
10	7	.	.	–	= 2³⁰–3⁴⁰ ≡°–7²⁰ = –8¹⁵, ↖° 13⁵⁰–15⁴⁰ ⌒² 0⁰⁰–9⁰⁰ ⌒¹ np
11	8	4.0	.	–	▽¹⁻⁰ 14⁵⁵–16⁰⁰, ↖° 14³¹–16⁴⁵ E–SW, ⌒¹ 0⁰⁰–9⁰⁰
12	7	7.9	.	–	•° 8¹⁵–⁴⁰ ▽° 16⁴⁰–18⁴⁵ •° 21³⁵ 22¹⁵, ↖° 16⁴⁰–18⁴⁵ SW–NE, = 4²⁰–8²⁰, 19³⁵–24
13	7	2.9	.	–	•° 2¹⁰–9²⁰, = 0⁰⁰–9³⁰, ⌒¹ 22⁰⁰–24
14	7	5.4	.	–	•⁰⁻¹ 6²⁵–11²⁰ 14⁴⁰ 16⁰⁵ •° 17⁵⁰–18¹⁰, = 6⁴⁰–13²⁰, ⌒¹ 0⁰⁰–6²⁵
15	7	.	.	–	= 5⁴⁰–7²⁰, 20³⁰–24, ⌒° 23⁰⁰–24
16	7	.	.	–	= 0⁰⁰–8¹⁰, 20³⁰–24, ⌒¹ 0⁰⁰–8⁰⁰, 21⁰⁰–24
17	8	.	.	–	= 0⁰⁰–7⁴⁰, ⌒¹ 0⁰⁰–9⁰⁰, 21⁰⁰–24
18	7	.	.	–	= 3²⁰–9³⁰, ⌒¹⁻² 0⁰⁰–9⁰⁰ ⌒° 21⁰⁰–24
19	7	0.0	.	–	▽° 21⁵⁰–22⁰⁵, ⌒¹ 0⁰⁰–7⁰⁰
20	8	.	.	–	
21	8	.	.	–	= 5⁵⁰–8⁰⁵, ⌒° 23⁰⁰–24
22	7	0.0	.	–	⌒° 0⁰⁰–7⁰⁰
23	7	4.6	.	–	▽° 7²⁰–8¹⁶ •⁰⁻¹–10¹⁵, = 3⁴⁰–6²⁵, a, np, ⌒° 21⁰⁰–24
24	7	.	.	–	= 0⁰⁰–11⁴⁰ ∞ 18¹⁰–19⁴⁰, ⌒° 0⁰⁰–8⁰⁰
25	7	.	.	–	= 3²⁰–9⁴⁰, ⌒° 20⁰⁰–8⁰⁰
26	8	.	.	–	
27	8	0.0	.	–	(↖)° 23¹⁵–24, ⌒° 0⁰⁰–9⁰⁰
28	7	5.3	.	–	▽° 12⁵–⁴⁰ ▽¹⁻⁰ 9³⁰–10⁰⁵, 10³⁵–12⁰⁵ •°–14⁴⁰, 16³⁵ 17¹⁵, (↖)ᵁ 0⁰⁰–1⁴⁰, ↖° 9²⁵–10³⁰
29	8	.	.	–	
30	8	.	.	–	⌒° 21⁰⁰–24
31					
Σ	–	70.9	–	–	UWAGI.

Przemyśl — φ = 49°48' — λ = 22°46' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P − 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	96.7	96.0	94.7	95.8	16.1	24.7	19.7	20.0	25.6	11.7	81	47	61	63	3.4	16.4	9.0	9.6	2 ⊙	5	2	W 2	NNW 4	NW 3
2	95.2	94.7	95.3	94.4	17.0	25.1	19.5	20.3	27.2	12.0	79	40	74	64	4.1	19.1	5.9	9.7	0 ⊙	0 ⊙	0	WNW 2	NW 2	C 0
3	95.1	92.0	88.8	91.3	19.0	27.9	18.8	21.1	29.4	12.4	72	56	75	60	6.2	24.0	5.9	12.0	0 ⊙	1 ⊙	0	W 2	NW 3	C 0
4	86.3	82.8	81.2	83.4	20.7	30.8	21.2	23.5	31.3	13.8	70	38	73	60	7.4	27.3	6.9	13.9	2 ⊙	1 ⊙	10	W 2	WSW 4	WNW 4
5	85.0	85.9	87.4	86.1	16.4	18.8	13.9	15.8	21.2	13.8	74	59	76	70	4.7	8.8	3.9	5.8	10	10	10 •	NW 5	WNW 2	NW 5
6	88.8	89.4	92.8	90.3	13.4	18.4	12.2	14.0	19.5	9.4	85	43	72	67	2.3	12.1	4.0	6.1	1 ⊙	9	1	WNW 1	WNW 4	C 0
7	93.8	93.1	93.1	93.3	12.6	17.3	14.5	14.7	19.6	7.3	76	59	61	65	3.6	8.1	6.5	6.1	4 ⊙	8	9	W 3	WNW 4	NW 1
8	93.1	92.0	90.1	91.7	13.2	19.8	14.3	15.4	20.7	11.3	86	47	70	68	2.1	12.3	5.0	6.5	5	5 ⊙	0	NW 1	N 2	C 0
9	86.0	82.4	83.4	83.9	13.0	24.1	14.9	16.7	25.0	7.1	80	35	77	64	3.0	19.6	3.8	8.8	0 ⊙	5	9	NW 1	W 3	W 4
10	84.0	84.4	85.4	84.6	13.7	18.2	12.5	14.2	20.4	10.9	86	55	90	77	2.2	9.3	1.4	4.3	4 ⊙	9	9	W 5	W 4	W 3
11	88.3	88.8	87.9	88.3	13.2	18.7	16.0	16.0	21.0	9.1	78	51	61	63	3.3	10.6	7.2	7.0	1 ⊙	7	8	W 4	W 3	C 0
12	85.8	84.2	81.8	83.9	15.5	24.4	21.1	20.5	27.5	9.7	77	54	60	64	4.1	14.2	10.1	9.5	7	9	0	C 0	SW 1	W 1
13	79.0	75.7	73.9	76.2	20.3	28.7	21.4	23.0	29.6	14.9	69	41	66	59	7.2	23.1	8.6	13.0	3 ⊙	2 ⊙	10 ☇	W 1	SW 6	W 14
14	78.0	81.3	84.1	81.1	17.2	15.4	13.5	14.9	21.4	13.1	81	85	84	83	3.7	3.0	2.3	3.1	9	10 •	0	W 4	WNW 3	C 0
15	85.4	85.3	85.4	85.4	16.3	23.6	19.8	19.9	25.3	8.8	74	44	63	60	4.7	16.4	8.5	9.9	2 ⊙	2 ⊙	6	W 2	WSW 6	C 0
16	82.1	80.7	82.2	81.7	16.6	25.7	17.1	19.1	26.6	12.9	73	49	86	69	5.2	16.8	2.8	8.3	9	3 ⊙	9	C 0	W 5	NW 3
17	82.2	81.3	81.0	81.5	14.9	21.0	13.0	16.3	23.2	13.7	91	53	95	79	1.5	11.7	1.1	4.8	9	7	2	WNW 2	SW 1	W 2
18	81.5	80.7	80.9	81.0	12.8	19.1	14.1	15.0	20.0	11.7	84	50	80	71	2.4	11.1	3.2	5.6	5 ⊙	7	0	W 2	NW 5	WNW 1
19	81.9	81.2	81.9	81.7	12.2	21.7	13.4	15.2	22.7	7.7	94	49	82	75	0.9	13.3	2.8	5.7	9	5	1	W 1	WNW 2	C 0
20	83.3	83.7	82.9	83.3	12.8	19.4	14.4	15.2	21.1	8.2	91	63	94	83	1.4	8.4	0.9	3.6	8	10	10 •	W 2	W 5	C 0
21	84.8	85.5	85.7	85.3	14.5	18.2	13.6	15.0	21.1	12.3	86	65	92	81	2.4	7.3	1.3	3.7	0 ⊙	9	10 •	W 5	NW 5	WNW 1
22	85.5	85.4	86.4	85.8	15.1	18.6	14.0	15.4	20.6	12.6	86	62	84	77	2.5	8.2	2.5	4.4	5	5 (☇)	1	W 2	W 4	C 0
23	87.8	87.7	88.6	88.0	13.6	20.0	17.5	17.2	21.5	10.6	91	55	67	71	1.5	10.5	6.6	6.2	0	9	9	W 1	NNE 3	NW 1
24	91.4	92.3	94.2	92.6	13.9	18.2	15.2	15.6	19.1	13.6	85	66	65	71	2.3	7.1	6.3	5.2	9	10	9	W 1	NW 1	NW 3
25	96.1	96.4	95.9	96.1	13.2	16.7	12.3	13.6	18.2	11.3	80	54	74	69	3.0	8.7	3.7	5.1	5	7	2	WNW 1	NW 3	NW 1
26	94.9	93.4	89.9	92.7	12.5	19.4	14.9	15.4	20.9	9.3	85	50	73	69	2.2	11.2	4.5	6.0	9	9	0	WSW 1	SW 1	C 0
27	85.7	85.7	82.3	83.9	18.4	26.2	22.4	22.4	26.8	10.7	55	42	57	51	9.6	19.9	11.6	13.7	0 ⊙	5 ◔	9	W 5	WSW 5	SW 3
28	80.9	80.4	79.1	80.1	20.9	27.8	21.1	22.7	28.7	17.7	72	48	72	64	6.8	19.5	7.0	11.1	7	7	3	W 1	SW 5	W 1
29	77.5	82.2	86.2	82.0	19.6	18.1	12.8	15.8	21.1	12.5	79	84	95	86	4.9	3.3	0.7	3.0	6	10	10	W 6	W 5	WNW 3
30	83.4	82.9	85.5	83.9	11.8	16.5	11.9	13.0	17.1	11.2	96	82	94	91	0.5	3.5	0.8	1.6	10	9	10 •	NW 2	NW 2	W 5
31	86.4	88.5	90.7	88.5	12.1	18.1	13.2	14.2	19.8	11.1	93	60	85	79	1.0	8.3	2.3	3.9	10	7	1	W 1	WSW 5	C 0
M	86.6	86.5	86.3	86.4	15.2	21.3	16.0	17.1	23.0	11.4	81	54	76	70	3.6	12.7	4.8	7.0	4.9	6.5	5.2	2.2	3.5	1.9

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1	91.8	91.3	90.8	91.3	15.7	21.4	15.7	16.6	22.3	10.6	89	48	81	73	1.8	13.3	3.4	6.2	2 ⊙	4 ⊙	2	W 1	WSW 3	C 0
2	90.4	88.7	87.6	88.9	14.4	25.4	18.2	19.0	25.6	9.0	88	47	70	68	2.0	17.0	6.2	8.4	0 ⊙	2 ⊙	0	W 1	SSE 4	C 0
3	87.4	87.0	90.4	88.3	14.6	24.3	16.6	18.0	24.9	10.9	90	61	85	78	1.6	11.8	3.3	5.6	1 ⊙	6	10	C 0	NW 5	NW 4
4	93.0	92.0	90.7	91.9	14.8	19.2	15.1	16.0	20.7	14.3	80	48	89	72	3.3	11.4	1.9	5.5	7	5 ⊙	3	NW 5	NW 4	C 0
5	90.3	90.3	89.8	90.1	15.5	21.0	17.0	17.6	23.8	13.5	83	63	89	78	3.0	9.1	2.2	4.8	9	9	10	NW 2	WNW 3	W 1
6	89.2	88.0	87.0	88.1	17.6	28.5	22.3	22.7	29.0	13.4	87	47	66	67	2.6	20.7	9.1	10.8	0 ⊙	1 ⊙	1	C 0	SW 6	W 1
7	86.1	85.4	85.4	85.6	21.3	30.3	24.3	25.0	30.5	16.8	68	41	66	58	8.1	25.4	10.2	14.6	1 ⊙	0 ⊙	0	W 1	SW 5	C 0
8	90.6	89.8	89.0	89.8	19.1	25.1	22.3	22.2	26.3	17.4	85	63	84	77	3.4	11.6	4.2	6.4	9	5	7	WNW 2	N 2	NE 1
9	90.4	91.2	91.5	91.0	20.6	28.1	25.0	25.7	29.6	16.4	88	52	82	74	2.8	18.3	5.1	8.7	0 ⊙	1 ⊙	3	W 4	C 0	N 1
10	91.9	91.7	88.9	90.8	21.3	28.3	25.1	25.0	30.7	18.9	88	64	61	71	3.0	13.8	12.5	9.8	4	0 ⊙	0	N 4	ENE 6	C 0
11	87.0	85.4	86.7	86.4	24.1	33.4	24.9	26.8	33.5	19.6	71	36	71	59	8.8	33.1	9.0	17.0	0 ⊙	0 ⊙	10 ☇	E 1	SW 7	WNW 7
12	88.9	87.7	82.5	86.4	19.2	24.3	19.3	20.5	25.5	17.6	93	63	94	83	1.5	11.3	1.3	4.7	8	5 ⊙	3	W 2	N 2	C 0
13	85.1	87.7	92.5	88.4	16.2	14.4	12.4	13.8	19.3	12.4	95	94	94	94	1.0	0.9	0.9	0.9	10	10 •	10	NW 1	NW 7	NW 1
14	93.6	92.7	90.9	92.4	12.0	18.4	14.6	14.9	19.5	9.6	91	55	77	74	1.2	9.6	3.8	4.9	1 ⊙	5	0	W 2	N 2	NW 1
15	89.1	86.7	86.0	87.3	11.3	22.1	15.1	15.9	23.2	8.0	93	45	89	76	1.0	14.6	1.9	5.8	0 ⊙	2 ⊙	10 •	NW 1	NW 2	W 1
16	84.3	82.6	83.7	83.5	12.8	20.4	11.6	14.1	21.4	10.6	94	59	90	81	0.9	9.9	1.3	4.0	3	9	10 •	WNW 2	W 1	W 2
17	82.2	80.5	79.0	80.6	11.4	16.4	12.1	13.0	17.4	8.9	89	67	88	81	1.5	6.2	1.7	3.1	7 ⊙	10	0	WNW 1	WNW 2	C 0
18	78.0	77.9	78.9	78.3	11.7	15.4	13.1	13.3	16.8	10.3	80	65	85	77	2.8	6.2	2.3	3.8	9	9	2	NW 7	NW 7	W 6
19	81.4	80.9	80.2	80.8	12.9	20.4	16.9	16.8	21.0	12.2	78	54	64	65	5.3	11.0	7.0	7.1	5	7 ⊙	10	W 4	SW 7	SW 1
20	81.3	82.2	84.7	82.7	14.5	15.2	12.4	13.6	19.0	12.3	90	87	86	88	1.6	2.3	2.0	2.0	9 •	10	8	WNW 1	W 3	W 5
21	87.7	88.3	88.0	88.0	12.4	16.1	14.8	14.5	19.5	10.2	85	73	82	80	2.2	4.9	3.1	3.4	8	7	0	W 2	W 5	C 0
22	86.7	84.2	81.3	84.1	15.8	24.3	18.9	19.5	24.4	11.1	74	44	56	58	4.6	17.0	9.5	10.4	2 ⊙	4 ⊙	6	W 2	SW 7	SW 2
23	82.7	83.3	85.4	83.8	14.4	16.8	12.8	14.2	19.4	12.8	94	67	84	82	0.9	6.3	2.4	3.2	10 •	9	8	W 1	W 3	W 6
24	87.6	88.4	89.6	88.5	11.7	15.1	12.1	12.8	17.1	10.5	84	53	83	73	2.1	8.2	2.3	4.2	8	9	1	W 5	WNW 7	NW 2
25	90.6	90.7	91.0	90.8	12.6	19.4	15.9	16.0	20.4	10.0	67	56	75	73	1.9	9.9	4.5	5.4	9	8	10	WNW 2	SW 4	W 2
26	92.0	92.6	94.3	93.0	14.3	19.2	15.6	16.2	21.0	11.6	88	69	95	84	2.0	6.8	0.9	3.2	9	9	8	WNW 1	W 6	C 0
27	95.1	95.0	95.1	95.1	14.9	23.6	17.1	18.2	24.6	13.6	91	53	86	77	1.5	13.5	2.8	5.9	8	3 ⊙	0	C 0	W 3	C 0
28	95.5	96.2	96.5	96.1	17.0	24.3	17.0	18.8	24.4	13.6	85	61	78	74	3.4	11.8	4.3	6.5	1	4	0	W 4	NW 5	NW 2
29	96.8	95.4	93.8	95.3	13.6	20.2	17.8	17.4	21.3	12.2	85	59	66	70	2.3	9.8	6.9	6.3	9	8	10	WNW 3	NW 6	NW 4
30	95.3	95.7	96.8	95.9	13.0	19.2	13.7	14.9	19.7	10.8	87	43	69	66	1.9	12.7	4.9	6.5	1 ⊙	3 ⊙	0	NW 2	NNW 6	NW 1
31	98.7	99.5	100.1	99.4	10.3	19.5	16.3	15.7	20.6	7.8	90	46	79	72	1.3	12.4	4.1	5.9	1 ⊙	4 ⊙	9	W 2	NW 4	NW 1
M	89.1	88.7	88.6	88.8	15.1	21.6	16.9	17.6	23.0	12.5	86	58	79	74	2.6	12.0	4.4	6.3	4.9	5.4	4.9	2.1	4.2	1.7

Przemyśl — $H_s = 237\,m$ — $H_b = 238{,}9\,m$ — $h_w = 20{,}6\,m$ — Lipiec - Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU L	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌒ 0 00–8 00 , 23 00–24
2	8	.	.	–	⌒ 0 00–6 00 , 22 00–24
3	8	.	.	–	⌒ 0 00–9 00
4	7	.	.	–	☾ 22 40–24 , ∞ 12 20–14 40
5	7	1.1	.	–	• 0 19 50–24 , ☾ 0 00–30
6	7	0.8	.	–	• 0 0 00–40 ▽ 0 15 32–16 15 , ☈ 0 15 34–16 25 S–N
7	7	.	.	–	
8	7	.	.	–	= 6 20–8 40 , 20 15–24 , ⌒ 0 22 00–24
9	7	0.6	.	–	• 0 22 20–24 , = 0 00–8 40 , ⌒ 1 0 00–8 00
10	7	0.9	.	–	• 0 0 00–1 50 ▽ 0 17 40–44 , 19 32–20 10 , = 3 15–7 40
11	8	.	.	–	= 3 20–6 50
12	7	.	.	–	= 4 50–7 40 , ⌒ 0 3 00–7 00
13	8	1.4	.	–	▽ 0 21 45–22 50 , ☈ 0 21 27–22 35 , ≫ – ≫ 21 07–22 15
14	7	1.4	.	–	• 0 12 35–16 20
15	8	.	.	–	
16	8	4.9	.	–	▽ 0 15 15–30 17 20–35 , ☈ 0 14 50–17 40 , ⌒ 0 2 00–7 00
17	8	4.6	.	–	▽ 0 0 40–3 20 • 0 4 40–7 25 ▽ 1 17 10–18 15 , ☈ 0 16 45–18 20 S–N
18	8	.	.	–	= 20 30–24 , ⌒ 0 21 00–24
19	7	.	.	–	= 0 00–4 50 ≡ 0 6 45 — — 9 20 , ⌒ 1 na ⌒ 0 np
20	8	10.6	.	–	• 0 11 55–12 10 16 40–17 15 19 20–23 40 , ⌒ 0 0 00–8 00
21	7	4.5	.	–	• 0 0 25–2 45 ▽ 0 16 15–25 ▽ 0-1 20 03–21 50 , ☈ 0 20 05–21 25 , = na – a , np
22	7	1.3	.	–	▽ 0 9 50–10 20 11 55–12 03 ▽ 1 16 20–30 17 05–20 , ☈ 0 12 05–13 40 WSW–SE , = na – a
23	7	.	.	–	= 4 50–8 25 , ⌒ 1 2 00–8 00
24	6	.	.	–	= 2 20–10 20
25	8	.	.	–	
26	7	.	.	–	
27	7	0.0	.	–	
28	7	.	.	–	▽ 0 4 40–50
29	7	28.7	.	–	▽ 1 10 25–50 • 0 13 50–14 35 15 50–24 , = 7 20–8 50 , 12 40–14 35 , 18 20–24 , ⌒ 2 00–6 00
30	8	11.5	.	–	▽ 1-0 1 50–3 40 • 0-1 7 25 , 8 05–11 25 • 0 17 15–40 , 20 10–24 , ☈ 0 1 50–3 40 , = a
31	8	.	.	–	• 0-1 0 00–2 15
Σ	–	72.3	–	–	UWAGI.

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1	7	.	.	–	= 4 50–7 20 20 30–24 , ⌒ 1 2 00–8 00 21 00–24
2	7	.	.	–	= 0 00–9 30 , ⌒ 1 0 00–9 00 ⌒ 0 21 00–24
3	7	14.6	.	–	▽ 2-1 18 02–19 15 ▽ 0 19 40–20 05 , ☈ 1 17 45–20 40 , = na – a , p – 24 , ⌒ 0-2 0 00–9 00
4	8	.	.	–	= 0 00–6 40 , ⌒ 1 21 00–24 , ⊕ 0 15 40–16 25
5	7	.	.	–	= 20 16–24 , ⌒ 1 0 00–9 00 , 21 00–24
6	8	.	.	–	= 0 00–9 10 , ⌒ 1 0 00–9 00 ⌒ 0 22 00–24
7	8	.	.	–	⌒ 0 0 00–9 00
8	7	.	.	–	= 19 30–24
9	7	.	.	–	= 0 00–9 50 , 23 20–24 , ☾ 22 15–24 , ⌒ 0 4 00–8 00
10	7	.	.	–	☾ 0 00–1 40 , = 0 00–8 36
11	7	1.9	.	–	▽ 0 21 50–58 22 17–27 23 15–36 , ☾ 20 30–24
12	7	16.0	.	–	▽ 2 18 43–19 18 , ☈ 0 0 00–36 ☈ 1 18 20–19 35 , = 4 20–8 40 19 05–24
13	7	5.9	.	–	▽ 3 40–5 20 • 0-1 10 42–14 40 • 0 14 45–15 16 • 0 16 25–19 07..40 , (☈) 0 0 20–1 35 , = 0 00-36 , 8 46–16 32
14	8	.	.	–	= 2 00–5 50 , ⌒ 0 23 00–24
15	8	1.0	.	–	▽ 0 18 30–19 10 • 0 20 50–22 20 , = 2 00–8 30 , ⌒ 0-2 0 00–8 00
16	7	4.1	.	–	• 0 14 06–22 25 , = 0 20–2 45 ≡ 0 6 50 — — 9 25 , np
17	7	.	.	–	= 0 00–8 30 , 21 20–24 , ⌒ 0 21 00–24
18	7	0.2	.	–	▽ 0-1 11 50–14 04 , = 0 00–5 40 , ⌒ 1 0 00–6 00
19	7	0.2	.	–	▽ 0 3 40–50 4 50–5 05
20	7	4.8	.	–	▽ 0 6 30–50 7 20–38 • 0 12 02–13 20 ▽ 1-0 16 20–17 20
21	7	.	.	–	▽ 0 0 10–22 , ⌒ 1 19 00–24
22	8	0.8	.	–	⌒ 1 0 00–9 00
23	7	0.0	.	–	▽ 0 3 20–4 40 , 7 25–8 10
24	8	.	.	–	= 4 20–8 35
25	6	0.0	.	–	▽ 0 22 45–23 08 , = 2 00–13 10
26	6	0.3	.	–	▽ 1 16 30–50 , = 0 30–8 30 , 12 20–24
27	7	.	.	–	= 0 00–10 40 , ⌒ 1 21 00–24
28	6	0.2	.	–	▽ 0 14 12–19 , 16 15–19 , = 0 30–14 10 , 19 35–22 40 , ⌒ 1 0 00–9 00
29	8	.	.	–	
30	8	.	.	–	⌒ 1 2 00–9 00 ⌒ 0 21 00–24
31	8	.	.	–	⌒ 0-1 0 00–9 00
Σ	–	48.0	–	–	UWAGI.

Przemyśl — φ = 49°48' — λ = 22°46' — Wrzesień – Septembre 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA Nw			KIERUNEK i PRĘDKOŚĆ WIATRU Dv		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	101.7	101.3	98.7	100.6	13.2	25.2	16.7	17.4	24.9	11.5	87	51	84	74	2.0	14.0	3.1	6.4	1 ⊙	1 ⊙	0	WNW 2	NW 2	NW 2
2	97.4	95.8	92.8	95.3	13.2	26.7	17.4	18.7	28.0	10.3	95	57	72	67	1.1	21.9	5.5	9.5	0 ⊙	0 ⊙	0	WNW 2	W 3	W 2
3	90.4	89.3	86.8	88.8	15.8	28.0	20.2	21.0	28.4	12.8	75	36	54	55	4.4	24.3	11.0	13.2	0 ⊙	2 ⊙	0	W 3	SW 5	W 4
4	84.9	85.1	86.0	85.3	18.4	22.8	17.4	19.0	26.4	17.1	56	50	72	59	9.3	13.9	5.5	9.6	1 ⊙	8	0	W 4	W 5	W 3
5	86.9	86.6	84.8	86.1	13.6	25.9	17.1	18.4	26.8	11.8	94	50	76	73	0.9	16.7	4.7	7.4	7	2 ⊙	0	W 1	SW 2	C 0
6	82.0	81.5	81.9	81.8	17.3	26.4	19.0	20.4	27.0	14.8	79	40	84	68	4.1	20.7	5.6	9.5	4 ⊙	8	10	C 0	SSW 8	W 3
7	80.5	80.2	81.5	80.7	15.6	25.6	16.5	18.6	26.3	13.3	98	50	95	81	0.4	16.5	1.0	6.0	2	5 ⊙	10 •	NW 1	SW 4	C 0
8	83.3	83.7	84.5	83.8	13.0	18.3	13.2	14.4	18.8	12.8	94	50	72	72	0.9	10.4	4.3	5.2	10	6 ⊙	4	W 5	W 5	C 0
9	85.5	86.4	87.5	86.5	11.9	16.2	12.3	13.2	16.6	10.7	95	67	92	85	0.7	6.2	1.2	2.7	8	9	10	W 3	WSW 6	W 2
10	87.8	88.6	89.8	88.7	11.8	15.4	12.0	12.8	15.6	11.6	87	61	83	77	1.8	6.9	2.3	3.7	10	9	10	W 3	WNW 6	W 3
11	90.1	90.3	90.1	90.2	11.0	15.7	11.8	12.1	14.8	10.3	89	75	82	81	1.5	4.2	2.5	2.7	9	10	10	W 2	W 4	W 1
12	89.2	88.1	87.4	88.2	8.8	20.8	15.0	14.9	21.1	7.3	95	59	60	65	0.6	15.1	6.7	7.5	1	2 ⊙	4	C 0	SW 6	SW 1
13	88.1	88.9	89.9	89.0	13.0	18.4	14.4	15.0	19.3	12.0	93	61	90	81	1.1	8.4	1.6	3.7	10	7	10	W 1	W 5	C 0
14	88.5	86.6	85.9	87.0	12.0	24.3	19.1	18.6	25.7	10.0	94	41	66	67	0.8	17.8	7.5	8.7	9	8 ⊙	4	W 1	SW 7	SW 1
15	86.3	89.9	93.3	89.8	16.8	18.6	12.2	15.0	19.1	12.0	80	49	73	67	3.9	10.9	3.8	6.2	7	4	0	W 7	W 7	W 2
16	95.2	95.1	95.1	95.1	10.2	19.2	14.0	14.4	20.1	8.0	90	57	91	79	1.2	9.4	1.5	4.0	8	9	0	W 2	W 2	W 1
17	96.4	95.7	95.5	95.9	9.3	26.6	19.5	18.7	27.9	8.0	99	48	75	75	0.1	18.2	6.1	8.1	0	0 ⊙	0	W 1	SE 2	C 0
18	94.3	93.0	92.6	93.3	18.8	29.5	19.7	21.9	30.0	11.5	61	29	64	52	8.4	29.3	8.3	15.3	1 ⊙	2 ⊙	0	SW 3	WSW 6	W 1
19	93.0	92.6	93.9	93.2	17.2	20.7	13.3	16.1	22.3	13.2	89	72	60	74	2.2	7.0	6.1	5.1	10	2 ⊙	0	W 1	W 5	NW 1
20	94.1	94.9	94.9	94.6	6.2	17.8	10.6	11.5	18.4	4.7	97	50	74	74	0.3	10.3	3.4	4.7	2	4 ⊙	0	W 2	NE 4	NE 2
21	95.7	95.9	98.0	96.5	5.4	16.2	8.2	9.5	16.2	3.4	97	47	73	72	0.3	9.7	3.0	4.3	0 ⊙	1 ⊙	0	NE 2	ENE 4	NE 1
22	99.5	100.1	100.9	100.2	1.6	15.3	7.4	7.9	15.7	0.4	96	57	65	65	0.3	10.9	3.8	5.0	0 ⊙	0 ⊙	0	C 0	E 4	NE 2
23	100.5	99.5	98.0	99.3	2.0	17.6	10.0	9.9	18.3	-0.1	85	51	65	60	1.1	13.9	4.4	6.5	0	1 ⊙	0	C 0	E 7	C 0
24	96.6	95.6	95.2	95.8	2.8	21.2	10.6	11.3	22.4	1.2	95	55	80	69	0.6	16.9	2.6	6.7	1 ⊙	1 ⊙	0	C 0	E 1	C 0
25	94.9	94.3	94.2	94.5	4.4	23.2	16.1	15.0	23.5	2.9	93	32	44	56	0.6	19.4	10.2	10.1	0 ⊙	0 ⊙	1	SW 1	SW 4	WSW 3
26	95.2	95.7	95.8	94.9	13.0	16.6	13.6	14.2	17.5	11.3	67	78	94	80	4.9	4.3	0.9	3.4	10	10	10	W 1	SW 2	C 0
27	91.2	90.1	90.0	90.4	11.9	18.6	14.3	14.8	19.6	11.4	95	65	90	83	0.7	7.4	1.6	3.2	7	5	8	SW 1	WSW 2	C 0
28	91.5	92.5	93.5	92.5	11.0	14.7	10.9	11.9	17.0	10.4	100	80	91	90	0.0	3.3	1.1	1.5	10 ≡	7	0	C 0	NW 2	C 0
29	94.4	94.2	93.7	94.1	4.7	16.3	9.4	10.0	17.6	2.9	100	60	85	81	0.0	7.4	2.0	3.1	10	8	0	C 0	ESE 3	C 0
30	93.7	91.9	91.8	92.5	4.6	17.8	10.6	10.9	17.8	4.3	98	48	82	76	0.2	10.6	2.3	4.4	2	8	8	C 0	ESE 7	E 1
31																								
M	91.6	91.5	91.4	91.5	11.0	20.5	14.1	14.9	21.4	9.1	89	51	76	72	1.8	12.9	4.1	6.5	4.7	4.6	5.3	1.6	4.2	1.2

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1	92.3	92.3	94.5	93.0	4.2	15.6	10.9	9.9	15.9	3.8	100	65	89	85	0.0	3.5	1.4	2.3	10 ≡	8	10	NE 1	NE 5	NE 4
2	96.4	97.8	98.5	97.6	11.0	15.0	10.2	11.6	16.8	9.6	91	69	87	82	1.1	5.2	1.6	2.6	10	8	0	ENE 6	E 7	E 2
3	100.0	99.7	100.1	99.9	5.6	16.1	9.8	10.3	16.9	4.9	97	58	91	82	0.3	7.7	1.1	3.0	0 ⊙	5 ⊙	0	E 2	ESE 7	ESE 1
4	100.5	99.3	99.1	99.6	5.6	18.3	11.8	11.9	18.9	4.8	100	44	65	70	0.0	11.6	4.9	5.5	10 ≡	0 ⊙	0	C 0	ESE 7	E 1
5	99.4	98.3	98.6	98.8	4.2	19.1	10.7	11.2	19.9	3.4	93	40	70	68	0.5	13.2	3.9	5.9	0	0 ⊙	0	C 0	ESE 4	C 0
6	98.6	97.1	94.7	96.8	4.0	18.6	11.8	11.6	19.3	2.3	93	49	71	71	0.5	10.9	3.9	5.1	0 ⊙	0 ⊙	0	C 0	E 1	E 3
7	92.6	89.6	82.5	90.2	4.2	17.0	10.8	10.7	17.3	3.2	92	47	62	67	0.6	10.2	5.0	5.3	0	0	0	E 1	SE 5	SE 4
8	87.2	86.2	86.9	86.8	5.6	16.0	9.6	9.7	17.3	2.6	93	45	67	68	0.5	10.0	4.0	4.8	2	2 ⊙	0	E 1	ESE 5	E 1
9	92.2	93.5	93.8	93.5	3.4	16.2	10.2	10.0	16.4	2.9	93	53	81	76	0.5	8.6	2.4	3.8	1 ⊙	0 ⊙	8	C 0	NNW 4	C 0
10	101.7	102.8	102.5	102.3	8.4	13.8	7.9	9.5	15.4	7.7	92	65	96	84	0.9	5.6	0.4	2.3	10	1 ⊙	0	C 0	N 2	C 0
11	101.8	100.4	99.8	100.7	2.6	17.1	9.0	9.4	18.1	1.9	100	49	64	71	0.0	9.9	4.1	4.7	0 ≡	0 ⊙	0	N 1	E 4	C 0
12	98.3	97.2	96.4	97.3	0.6	17.8	8.8	9.0	18.3	0.2	98	50	54	67	0.1	10.1	5.2	5.1	0 ⊙	0 ⊙	0	C 0	SE 3	C 0
13	96.1	97.3	96.9	96.8	4.2	9.9	10.3	8.7	12.8	0.9	97	93	66	85	0.2	0.8	4.2	1.7	8	10	9	C 0	W 3	NW 5
14	96.2	95.1	94.2	95.2	7.0	9.6	8.0	8.2	10.3	5.5	81	67	89	79	1.9	4.0	1.2	2.4	9	10	10 •	W 2	W 4	W 4
15	94.6	94.7	93.8	94.4	8.9	11.0	10.4	10.2	11.9	7.5	96	90	86	91	0.5	1.3	1.8	1.2	8	10	10	W 5	WNW 5	W 5
16	92.4	92.1	89.8	91.4	10.0	11.6	6.8	8.8	13.1	6.5	81	69	94	81	2.4	4.2	0.6	2.4	10	8 ⊙	0	W 2	W 4	C 0
17	87.4	84.0	79.2	83.5	6.4	18.0	10.8	11.5	19.2	1.9	92	48	78	73	0.7	10.7	3.0	4.8	5 ○	8	2	C 0	S 4	C 0
18	72.8	71.8	72.2	72.3	14.4	16.2	13.1	14.2	17.1	9.9	55	44	60	53	7.5	10.2	6.1	7.9	8	10	9	SE 5	SE 4	SSE 2
19	74.2	75.0	78.6	75.9	10.3	24.7	13.9	15.7	24.8	10.2	69	34	70	58	3.9	20.6	4.7	9.7	8	4 ⊙	0	SSE 1	SE 7	C 0
20	81.6	82.0	82.3	82.0	9.6	18.8	14.2	14.2	19.7	7.8	87	60	80	76	1.6	8.6	3.2	4.5	0 ⊙	0 ⊙	0	SE 1	ESE 6	E 4
21	86.1	88.2	92.1	88.8	11.0	18.8	10.4	12.6	19.0	10.2	92	45	91	75	1.0	12.4	1.1	4.8	10 •	5	10	SSW 1	S 6	E 4
22	93.3	95.5	97.2	95.3	9.3	10.9	7.8	9.0	11.9	7.4	92	77	71	80	0.9	5.0	3.1	2.3	10	10	7	E 5	SE 5	E 5
23	98.6	98.9	99.3	98.9	1.2	13.0	7.2	7.2	13.6	0.3	90	51	66	69	0.7	7.3	3.3	3.8	1 ⊙	2 ⊙	0	C 0	SE 2	SE 1
24	99.8	98.7	97.8	98.8	2.1	18.1	8.7	9.4	18.2	1.7	91	44	77	71	0.6	11.6	2.5	4.9	3 ⊙	2 ⊙	0	C 0	SSW 3	C 0
25	95.7	94.2	93.8	94.6	4.7	17.4	8.3	9.7	18.0	4.1	90	44	74	69	0.8	11.2	2.9	5.0	4 ⊙	2 ⊙	6	C 0	SSW 5	C 0
26	92.1	91.0	91.2	91.4	2.0	18.3	11.2	10.7	19.4	1.0	96	32	55	61	0.3	14.3	6.0	6.9	7	7	2	C 0	SW 4	SW 1
27	89.6	88.6	87.6	88.6	2.4	20.2	11.1	11.2	20.5	1.5	84	25	41	50	1.2	17.9	7.8	9.0	5 ⊙	7 ⊙	5	C 0	SSW 3	S 1
28	87.3	86.0	85.0	86.1	5.9	22.4	9.2	11.7	22.5	3.5	67	26	69	54	3.1	20.0	5.6	8.9	0 ⊙	0 ⊙	0	C 0	S 3	SE 1
29	84.4	85.2	85.3	84.3	1.8	16.7	12.0	10.6	19.6	0.4	94	50	81	75	0.4	9.6	2.7	4.2	8 ⊙	5 ⊙	10 •	SE 1	SE 1	W 2
30	88.4	88.9	88.6	88.6	9.2	12.0	9.7	10.2	12.4	8.8	89	74	88	84	1.2	3.6	1.4	2.1	10	8	10 •	C 0	W 1	N 1
31	88.3	91.2	93.0	90.8	7.9	9.3	6.8	7.7	10.3	6.4	99	91	93	94	0.1	1.1	0.8	0.7	10 •	10	0	N 5	NW 3	W 2
M	92.3	92.0	92.1	92.1	6.0	16.0	10.0	10.5	16.9	4.6	90	55	75	73	1.1	9.1	3.2	4.5	5.4	4.5	5.4	1.2	4.0	1.6

Przemyśl — $H_s = 237\ m$ — $H_h = 238{,}9\ m$ — $h_w = 20{,}6\ m$ — Wrzesień – Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌒¹ 21⁰⁰–24
2	8	.	.	–	= 6²⁰–8⁴⁰, ⌒¹ 0⁰⁰–9⁰⁰
3	8	.	.	–	
4	8	0.1	.	–	▽• 14²⁵–15⁰⁷
5	6	.	.	–	= 2²⁰–14²⁵, ⌒° 2⁰⁰–9⁰⁰ 21⁰⁰–24
6	8	0.7	.	–	▽• 19⁰⁰–07, 21⁵⁶–22⁰⁵, 22²⁵–23¹², K° 21²⁰–22⁴⁰ SW, ⌒¹ 0⁰⁰–9⁰⁰
7	8	3.9	.	–	▽• 18¹⁰–15 18³⁵–45 ▽•¹⁻⁰ 21³⁰–22⁰⁷, = 3⁴⁰–8²⁰
8	8	0.5	.	–	▽• 1⁵⁰–4³⁰
9	7	0.0	.	–	•° 6⁵⁰–7¹⁰ ▽° 14¹⁰–³⁵, = 5³⁰–13²⁰, 18³⁰–24
10	8	0.0	.	–	•° 6⁵⁰ 7⁰⁶, 19³⁵ 20⁰⁰, = 0⁰⁰–5¹⁰
11	7	0.0	.	–	▽• 10⁵⁶–11⁰⁰, = 3³⁰–7²⁰, 18⁴⁴–24
12	8	1.0	.	–	= 0⁰⁰–9³⁰
13	7	.	.	–	•° 2¹²–3⁰⁰, = 3⁰⁰–11²⁰, 18⁴⁰–24
14	7	0.7	.	–	= 0⁰⁰–9¹⁷, ⌒° 4⁰⁰–9⁰⁰
15	8	.	.	–	▽• 1²⁰–40 •° 2²⁰–45
16	7	.	.	–	= 21²⁰–24, ⌒° 2⁰⁰–8⁰⁰, 21⁰⁰–24
17	8	.	.	–	= 0⁰⁰–10²⁵, ⌒¹ 0⁰⁰–9⁰⁰ ⌒° 22⁰⁰
18	8	.	.	–	⌒² 2⁰⁰–9⁰⁰ ⌒° 21⁰⁰–24
19	7	.	.	–	= 5²⁰–11⁴⁰, ⌒° 0⁰⁰–7⁰⁰
20	8	.	.	–	= 8¹⁰–9⁴⁰, ⌒⁰⁻² 2⁰⁰–10⁰⁰
21	8	.	.	–	= 4³⁰–9⁴⁰, ⌒⁰⁻¹ 2⁰⁰–9⁰⁰ ⌒° 22⁰⁰–24
22	8	.	.	–	= 3²⁰–10³⁰, ⌒⁰⁻¹ 0⁰⁰–5⁰⁰ ⌒° 23⁰⁰–24, ⌴° 6⁰⁰–8⁰⁰
23	8	.	.	–	= 7⁴⁵–9³⁶, ⌒° 0⁰⁰–4⁰⁰ ⌴° 8⁰⁰
24	8	.	.	–	= 5⁴⁰–9³⁰, ⌒° 2⁰⁰–7⁰⁰ 21⁰⁰–24
25	7	.	.	–	= 6⁴⁰–10²⁰, ⌒⁰⁻¹ 0⁰⁰–8⁰⁰
26	5	2.8	.	–	•° 9³⁴ 10⁰⁶, 22¹⁵–²⁵ 23⁴⁵–24, = 7²⁰–24
27	6	0.6	.	–	•° 4⁵⁰–5⁴⁵ ▽• 20⁴⁰ 21⁰², = 0⁰⁰–24
28	6	.	.	–	= 0⁰⁰–40 ≡⁰⁻² 10⁵⁰ = –24
29	6	.	.	–	= 0⁰⁰ 4⁴⁵ ≡° 5⁴⁰ = –6²⁰ ≡² 11³⁵ = a–p, np, ⌒° 21⁰⁰–24
30	7	.	.	–	= 0⁰⁰–11²⁰, ⌒¹ 0⁰⁰–10⁰⁰
31					
Σ	–	10.3	–	–	UWAGI.

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1	7	.	.	–	= 1⁰⁰–4⁴⁰ ≡⁰⁻² 8⁵⁰ = –11⁴⁰, ⌒⁰⁻¹ 2⁰⁰–10⁰⁰
2	7	.	.	–	= 5⁴⁵–8¹⁵, ⌒° 22⁰⁰–24
3	7	.	.	–	= 3⁴⁰–10³⁰, ⌒¹ 0⁰⁰–9⁰⁰ 21⁰⁰–24
4	7	.	.	–	= 1⁰⁰–5⁵⁰ ≡⁰⁻² 5⁵⁰–8³⁵ = –9³⁰, ⌒² 0⁰⁰–5⁰⁰
5	7	.	.	–	= 1⁴⁰–9²⁵, 20⁴⁰–24 ⌒¹ 1⁰⁰–10⁰⁰ ⌒° 20⁰⁰–24
6	7	.	.	–	= 0⁰⁰–11¹⁰, ⌒° 0⁰⁰–9⁰⁰
7	7	.	.	–	= 5²⁰–9⁴⁰
8	7	.	.	–	= 4²⁰–9³⁰ ⌒° 4⁰⁰–8⁰⁰, 22⁰⁰–24
9	6	.	.	–	= 6²⁰–11¹⁰ ∞–17⁴⁰, ⌒° 0⁰⁰–9⁰⁰
10	7	.	.	–	= 2⁴⁰–12¹⁰, 15⁴⁰–21⁴⁰ ≡° 22¹⁰ ≡¹–23²⁰ ≡²–24 ⌒¹ 20⁰⁰–24
11	7	.	.	–	= ² 0⁰⁰ 6²⁰ ≡° 7⁵⁰ = –10³⁰, ⌒²⁻¹ 0⁰⁰–8⁰⁰ ⌒° 23⁰⁰–24
12	7	.	.	–	= 2²⁰–10⁴⁰, ⌒° 0⁰⁰–4⁰⁰ ⌴° 5⁰⁰–7⁰⁰
13	6	0.0	.	–	•° 10²⁰–48 = 4³⁰–14²⁸
14	7	2.2	.	–	•° 14¹⁰–15²⁰ 16⁴⁵–17¹⁰, 20²⁰–22⁰⁵ 23⁴⁰–24, = 23⁴⁰–24
15	7	0.0	.	–	•° 0⁰⁰–3⁰⁰ ▽• 11³⁰–45, = 0⁰⁰–5¹⁰, 15³⁰–24
16	6	.	.	–	= 5²⁰–24, ⌒¹ 20⁰⁰–24
17	7	.	.	–	= 0⁰⁰–8²⁵, ⌒¹ 0⁰⁰–8⁰⁰
18	7	.	.	–	
19	7	.	.	–	
20	7	0.1	.	–	= 6¹⁰–9³⁰ ⌒° 2⁰⁰–8⁰⁰
21	7	0.1	.	–	•° 6²⁸ 7⁰⁶, 7²⁰ 9⁰⁰, = 2²⁰–9²⁰, ⌒⁰⁻¹ 0⁰⁰–6⁰⁰
22	7	0.0	.	–	•° 9⁴⁰ 10⁰⁵, = 1⁴⁰–7⁴⁰
23	7	.	.	–	= 6²⁰–10³⁰
24	8	.	.	–	= 3⁴⁰–10⁴⁰, ⌒° 2⁰⁰–7⁰⁰
25	7	.	.	–	= 5⁴⁰–9⁴⁰, ⌴° 4⁰⁰–8⁰⁰
26	8	.	.	–	= 6¹⁵–9⁴⁰, ⌴° 4⁰⁰–7⁰⁰
27	8	.	.	–	⌴° 4⁰⁰–7⁰⁰
28	8	.	.	–	= 16⁴⁵–24 ⌒° 22⁰⁰–24
29	6	0.4	.	–	•° 18⁴⁵ 19¹⁰ 20²⁰–21⁴⁰, = 0⁰⁰–11²⁰ ∞–12⁴⁰, ⌒° 1⁰⁰–3⁰⁰ ⌴° 4⁰⁰–7⁰⁰
30	7	1.6?	.	–	•° 20²⁵–23⁴⁰ •¹–24, = 20⁵⁰–24
31	6	2.9	.	–	•¹ 0⁰⁰–30 •° 10⁴⁰, 11⁴⁵–12¹⁰, = 0⁰⁰–13¹⁵
Σ	–	7.3?	–	–	UWAGI.

Przemyśl — φ = 49°48' — λ = 22°46' — Listopad – Novembre 1961

Dni	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N			POGODA			KIERUNEK i PRĘDKOŚĆ WIATRU D, v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III	I	II	III
1	94.0	94.5	95.4	94.6	8.7	14.9	8.6	10.2	15.1	6.2	77	50	80	69	2.5	8.4	2.3	4.4	8	3 ⊙	10 •	W 1	SW 7	W 2
2	97.1	96.6	92.8	95.5	7.4	12.0	5.2	7.4	12.0	4.5	96	65	92	84	0.5	4.9	0.7	2.0	8	8 ⊙	0	W 2	SW 2	C 0
3	86.6	85.2	83.5	85.1	8.9	15.8	10.4	11.4	15.9	2.8	76	43	65	61	2.8	10.2	4.4	5.8	4 ⊙	2 ⊙	0	SW 1	SW 6	SW 5
4	81.9	80.7	79.1	80.6	10.0	11.2	7.2	8.9	12.4	6.4	67	71	90	76	4.1	3.9	1.1	3.0	8	6	10	S 2	NE 4	C 0
5	77.5	79.9	85.0	80.8	4.4	6.2	4.3	4.8	7.2	4.1	98	97	92	96	0.2	0.3	0.7	0.4	10	10	10	WNW 1	NW 1	W 2
6	83.7	83.0	82.8	83.2	4.2	7.2	10.6	8.2	10.7	3.2	100	100	95	98	0.0	0.0	0.7	0.2	10 ⁹ =	10 ⁹ ≡	10	W 1	NW 1	E 5
7	81.4	81.0	80.9	81.1	10.9	11.5	8.2	9.7	11.7	8.1	90	85	94	90	1.3	2.0	0.6	1.3	10	10	10 ⁹	E 6	E 5	E 6
8	80.3	82.1	82.8	81.7	8.0	9.3	7.1	7.9	9.8	7.0	92	83	85	87	0.9	2.0	1.5	1.5	9	9	10	E 2	SW 3	SW 1
9	82.9	82.8	82.2	82.6	7.0	10.9	5.4	7.2	12.1	4.9	80	61	94	78	2.0	5.0	0.6	2.5	8	10	10	SE 1	SE 4	C 0
10	80.0	80.1	80.6	80.2	8.4	12.4	9.3	9.8	12.8	5.4	87	68	92	82	1.4	4.7	0.9	2.3	3	9	0	S 2	S 3	C 0
11	79.5	80.4	81.8	80.6	7.2	8.0	8.2	7.9	8.2	6.5	97	90	92	93	0.3	1.0	0.9	0.7	10	10	10	SSE 2	ESE 3	E 3
12	81.7	82.6	84.2	82.8	7.2	10.1	8.1	8.4	10.6	6.7	100	90	96	95	0.0	1.3	0.5	0.6	10 •	5	0	E 2	SE 1	E 3
13	84.1	82.9	80.5	82.5	8.3	9.6	10.0	9.5	10.6	7.0	99	89	100	96	0.2	1.3	0.0	0.5	10 ⁹ =	10	10	E 4	E 2	E 1
14	75.8	78.5	85.9	80.1	9.2	12.0	1.7	6.2	12.6	1.9	95	72	85	84	0.6	4.0	1.0	1.9	8	9	10	S 3	WSW 6	NW 6
15	87.6	89.2	91.1	89.3	-0.2	-0.6	-1.1	-0.8	1.7	-1.3	100	95	93	96	0.0	0.3	0.4	0.2	10 ⁹	10	10	NW 3	NNW 4	W 1
16	91.6	90.2	87.8	89.9	-0.2	1.8	2.3	1.6	2.6	-1.3	92	76	87	85	0.5	1.7	0.9	1.0	10	10	10	W 2	W 1	C 0
17	84.7	82.9	83.1	83.6	2.9	5.2	4.2	4.1	5.4	2.0	91	72	93	85	0.6	2.4	0.5	1.2	10	10	10	W 1	W 4	W 2
18	81.4	81.0	81.6	81.3	4.6	3.2	3.4	3.6	4.9	2.4	84	83	76	81	1.4	1.5	1.9	1.5	10	10	3	W 4	W 5	W 4
19	84.2	85.7	91.5	87.1	1.3	0.6	0.0	0.5	3.4	0.0	89	98	79	89	0.8	0.1	1.3	0.7	10	10 ✳	9	W 3	W 2	NW 4
20	97.8	100.7	105.9	101.5	-2.4	-0.8	-1.7	-1.6	0.0	-3.4	87	77	92	85	0.7	1.3	0.4	0.8	10 ✳	10	9	NW 4	NNW 4	NW 4
21	106.2	104.4	100.8	103.8	-3.8	0.3	-0.7	-1.2	0.4	-4.1	92	68	77	79	0.4	2.0	1.3	1.2	9	9	10	W 1	W 3	W 2
22	97.6	95.8	93.6	95.7	-1.6	3.0	0.3	0.5	4.0	-2.5	82	51	60	64	1.0	3.8	2.4	2.4	3	4	0	W 2	W 3	W 2
23	91.1	89.5	88.1	89.6	-2.7	5.2	-1.6	-0.2	5.6	-4.5	78	51	80	70	1.1	4.3	1.0	2.1	0	0 ⊙	0	W 1	W 1	C 0
24	89.4	89.9	91.2	90.2	-3.4	8.0	2.3	2.3	8.5	-4.7	79	49	77	68	1.0	5.5	1.7	2.7	0	1 ⊙	6	C 0	WSW 2	W 1
25	89.9	88.4	87.2	88.5	-0.4	4.2	4.2	3.0	4.6	-1.4	98	80	97	92	0.1	1.6	0.2	0.6	4	10 •	10 =	C 0	C 0	C 0
26	86.0	84.8	82.6	84.5	2.3	6.4	5.0	4.7	7.3	1.8	98	87	90	92	0.1	1.3	0.8	0.7	10 ≡	6 ⊙	4	C 0	S 2	C 0
27	77.6	75.3	74.3	75.7	5.8	13.3	11.1	10.3	14.2	3.5	89	63	89	80	1.0	5.6	1.5	2.7	4	9	10	S 1	SW 5	WSW 3
28	78.8	81.5	85.8	82.0	8.4	6.6	5.3	6.4	11.2	5.1	92	82	98	91	0.9	1.7	0.1	0.9	10	10	10	W 3	W 4	C 0
29	88.6	88.7	89.2	88.8	4.6	7.2	5.8	5.8	7.8	4.2	97	86	95	93	0.3	1.5	0.4	0.7	10	6	10	E 2	E 2	C 0
30	84.9	83.8	81.7	83.5	-1.9	8.4	5.2	4.2	8.4	-2.2	98	65	72	78	0.1	3.8	2.4	2.1	2 =	4 ⊙	4	N 1	W 4	C 0
31																								
M	86.1	86.1	86.4	86.2	4.1	7.4	4.9	5.3	8.4	2.3	90	75	87	84	0.9	2.9	1.1	1.6	7.6	7.7	7.2	1.9	3.1	1.9

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1	74.5	74.9	76.1	75.2	7.0	8.6	8.5	8.2	9.7	4.5	67	69	77	71	3.3	3.5	2.6	3.1	8	10	10	SW 7	SW 7	WSW 5
2	74.5	73.1	73.7	73.8	10.6	14.0	11.0	11.6	14.6	8.3	64	47	66	59	4.6	8.5	4.5	5.9	2	5 ⊙	2	SW 7	S 7	SW 6
3	85.6	84.9	83.8	84.1	3.5	7.0	5.3	5.3	11.0	1.0	70	52	83	68	2.3	4.8	1.5	2.9	4	2	10	W 3	W 1	C 0
4	79.5	81.5	87.1	82.7	10.8	12.4	11.0	11.3	12.9	5.9	70	64	71	68	3.9	5.2	3.8	4.3	9	8	10	SW 8	SW 4	W 2
5	86.2	86.1	84.1	85.5	12.5	16.4	14.0	14.2	16.5	9.0	68	50	61	60	4.7	9.3	6.2	6.7	9	6	0	WSW 4	WSW 7	SW 8
6	81.5	80.4	85.6	82.5	11.2	13.6	0.6	6.5	14.1	0.5	77	65	96	79	3.1	5.5	0.3	3.0	9	9	10 ✳	SW 5	SW 4	NW 6
7	81.6	81.5	84.5	82.5	0.0	0.1	0.3	0.2	0.0	-0.1	100	96	95	96	0.0	0.3	0.4	0.2	10 ✳	10 ✳	10	NE 4	N 5	NNW 4
8	86.8	88.7	91.1	88.9	-0.6	-1.2	-2.0	-1.4	0.3	-2.0	97	95	89	94	0.2	0.3	0.6	0.4	10 ✳	10	10	NNW 6	NW 5	C 0
9	92.4	93.2	92.1	92.6	-5.0	-2.5	-7.3	-5.5	-2.0	-7.3	93	82	90	88	0.3	0.9	0.3	0.5	0	1 ⊙	0	W 1	W 1	C 0
10	89.9	88.2	87.0	88.4	-8.3	-1.4	-3.5	-4.2	-0.6	-12.0	83	86	94	88	0.5	0.8	0.3	0.5	9	8	2	SW 1	SW 2	C 0
11	83.5	78.2	69.8	77.2	2.5	3.2	1.7	2.3	3.9	-4.2	77	74	85	79	1.7	2.0	1.0	1.6	8	9	10 •	S 3	SW 6	WSW 6
12	71.3	76.1	80.5	76.0	3.1	1.8	0.5	1.5	3.3	0.5	98	96	100	98	0.1	0.3	0.0	0.1	10 •	10	10 ⁹	WSW 2	W 3	NW 3
13	86.6	91.5	95.1	91.1	-1.8	-5.6	-6.4	-5.0	0.5	-7.0	96	85	75	85	0.2	0.6	0.9	0.6	10 ✳	10 ✳	9 ✳	N 5	NNW 6	NNW 5
14	95.3	95.8	93.5	94.2	-11.1	-8.3	-10.2	-10.0	-6.4	-11.9	76	57	74	69	0.6	1.4	0.7	0.9	0	2	8	NW 4	NW 5	NW 7
15	88.2	87.8	92.2	89.4	-8.9	-11.1	-15.6	-12.8	-8.8	-16.1	86	83	81	83	0.4	0.4	0.3	0.4	10 ✳	10 ✳	0	W 7	NW 5	N 3
16	99.6	103.8	109.7	104.4	-18.2	-12.1	-14.9	-15.0	-11.7	-18.5	84	89	87	87	0.2	0.3	0.3	0.3	10	10 ✳	2	N 1	NE 2	NE 3
17	112.3	109.5	107.0	109.6	-21.6	-13.9	-10.2	-14.0	-10.2	-22.9	89	71	84	81	0.1	0.6	0.4	0.4	2	3 ✳	10 ✳	ENE 1	W 2	NW 4
18	106.0	105.5	104.9	105.5	-6.4	-4.3	-4.2	-4.8	-4.1	-10.6	86	91	91	89	0.5	0.4	0.4	0.4	10	10 ✳	10	N 4	NW 4	NW 5
19	102.2	100.3	98.4	100.3	-6.1	-4.5	-5.4	-4.4	-5.4	-6.4	92	86	92	90	0.3	0.6	0.4	0.4	10	10 ⛆	10	W 6	W 6	W 5
20	95.5	90.4	82.2	89.4	-2.5	-1.2	-0.4	-1.1	-0.4	-3.9	93	84	92	90	0.4	0.9	0.5	0.6	10	10	10 ✳	W 4	W 7	W 6
21	79.0	78.2	84.2	80.5	-0.9	-1.2	-5.8	-3.4	0.6	-6.4	85	80	61	75	0.8	1.1	1.5	1.1	10 ✳	9 ✳	0	WNW 3	NW 7	WNW 5
22	83.4	77.7	77.7	79.6	-5.8	-4.4	-5.4	-5.2	-4.0	-8.4	84	81	92	86	0.6	0.8	0.3	0.6	5	10 ✳	10 ✳	W 4	WSW 7	W 5
23	81.9	85.0	87.7	84.9	-9.1	-8.9	-13.5	-11.2	-5.3	-13.9	85	73	84	81	0.4	0.8	0.4	0.5	10 ✳	8	0	NW 7	WNW 4	C 0
24	89.6	89.4	88.0	89.0	-13.1	-10.6	-18.6	-15.2	-10.2	-18.7	84	80	95	86	0.4	0.5	0.1	0.3	10 ✳	2 ⊙	0 =	W 2	C 0	C 0
25	85.4	84.1	83.3	84.3	-20.6	-17.9	-21.9	-20.6	-17.6	-25.5	89	84	81	85	0.1	0.2	0.2	0.2	10	0 ⊙	0	C 0	C 0	C 0
26	83.2	81.8	80.1	81.7	-24.8	-13.3	-15.1	-17.1	-10.4	-25.5	79	68	86	78	0.2	0.7	0.3	0.4	0	0 ⊙	0	C 0	W 1	C 0
27	81.1	82.9	84.6	82.9	-9.2	-5.5	-7.3	-7.3	-5.4	-15.2	88	82	88	86	0.4	0.7	0.4	0.5	10	9	10	C 0	C 0	NE 3
28	82.6	81.5	82.4	82.2	-7.6	-4.4	-3.8	-4.9	-5.7	-8.1	87	86	87	87	0.4	0.6	0.6	0.5	10	10	10	E 3	E 6	E 3
29	82.5	83.2	84.4	83.4	-1.9	0.5	0.6	0.0	0.8	-3.8	96	90	96	94	0.2	0.6	0.3	0.4	10	10	10	E 1	E 2	C 0
30	83.1	82.4	83.9	83.1	-3.6	0.1	1.2	-0.3	3.5	-4.8	92	85	92	89	0.4	1.1	0.5	0.7	10 =	9	0	C 0	E 1	C 0
31	83.4	83.0	80.1	82.2	5.0	5.3	4.8	5.0	6.7	0.0	84	80	84	83	1.4	1.8	1.4	1.5	5	10	0	C 0	SSE 2	C 0
M	86.7	86.4	86.9	86.7	-3.9	-1.6	-3.5	-3.1	-0.2	-7.2	84	78	85	82	1.1	1.8	1.0	1.3	7.7	7.4	5.9	3.3	3.8	3.0

Przemyśl

$H_s = 237\ m$ $H_b = 238{,}9\ m$ $h_w = 20{,}6\ m$ Listopad - Novembre 1961

DNI	WIDZIALNOŚĆ	OPAD R	GRUBOŚĆ ŚNIEGU s	USŁONECZNIENIE	POGODA
1	8	4.5	.	–	• 20 20 – 24
2	7	.	.	–	• 0 00 – 1 45 . = 5 20 – 11 25 16 12 – 24 . ⌒ 1 20 00 – 24
3	8	.	.	–	= 0 00 – 2 30 . ⌒ 1 0 00 – 7 00
4	7	.	.	–	= 20 20 – 24
5	6	1.9	.	–	• 10 06 – 11 20 • 22 40 – 24 . = 0 00 – 24
6	1	1.1	.	–	• 0-2 0 00 – 13 40 • 19 40 – 20 00 . = 0 00 – 6 20 ≡ 7 30 = – 8 10 ≡ 0-2 – 13 50 = – 24
7	8	0.1	.	–	• 20 10 – 22 45 • – 23 35 . = 0 00 – 5 10 = 17 30 – 24
8	8	0.1	.	–	• 9 40 – 12 35
9	7	.	.	–	⌒ 22 00 – 24
10	7	0.1	.	–	• 9 45 – 11 25 16 40 17 28 . = 17 30 – 24 . ⌒ 0 00 – 7 00
11	6	4.0	.	–	• 10 40 11 21 . 13 32-38 . 14 12-21 . = 0 00 – 24 . ⌒ 0 00 – 7 00
12	7	2.3	.	–	• 0 40 – 9 35 . = 0 00 – 8 40 19 30 – 23 40 ≡ 0 – 24 . ⌒ 1 20 00 – 24
13	6	3.2	.	–	• 6 10 – 10 15 • 15 45 – 24 . ≡ 0 00 – 9 50 = – 10 20 . ⌒ 1 0 00 – 6 10
14	8	0.4	.	–	• 0 00 – 1 40 ▽ 0 7 50 – 8 45 . = 1 00 – 6 12 . ⌒ 1 6 48 – 7 08
15	7	0.0	.	–	• 3 20 – 7 10 = 3 10 – 9 40 . 14 35 – 15 05
16	6	.	.	–	= 1 00 – 5 20 . 8 20 – 24
17	6	0.5	.	–	• 17 10 – 55 19 14 – 45 = 0 00 – 13 10 . 14 40 – 24
18	6	0.7	.	–	• 0 9 30 – 10 05 . = 0 00 – 10 20 . 12 30 – 13 30
19	5	5.4	.	–	▽ 0-1 8 21 – 10 40 * 0-1 . 16 08
20	8	0.1	1	–	* 0 3 25 – 7 20 8 10 – 9 20 ▽ 0 – 10 40 . 17 20 – 18 15 . = 8 20 – 9 35
21	7	.	1	–	= 7 40 – 9 20 . ⌓ 0 19 00 – 22 40
22	7	.	pł.	–	
23	6	.	pł.	–	= 7 20 – 24
24	6	.	pł.	–	∞ 10 28 – 17 30 . ⌴ 0 0 00 – 9 00
25	4	2.2	pł.	–	• 0 11 45 – 17 20 . = 1 20 – 12 40 ≡ 1-0 14 40 – 17 30 = – 18 40 ≡ 0-1 – 24 . ⌴ 0 1 00 – 8 00
26	5	0.4	.	–	≡ 0-1 0 00 – 10 40 = – 24
27	8	2.3	.	–	• 0 15-50 ▽ 1 18 25 – 19 40 . = 0 00 – 1 00
28	6	0.0	.	–	= 5 30 – 24
29	6	0.2	.	–	• 0 1 40 – 3 25 ▽ 0 17 33-50 . = 0 00 – 24
30	7	.	.	–	= 0 00 – 3 50 ≡ 0-1 – 8 45 = – 12 15 . 15 40 – 20 10 . ⌴ 1 4 00 – 9 00
31					
Σ	–	29.5	–	–	UWAGI.

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1	8	.	.	–	
2	8	.	.	–	
3	7	.	.	–	
4	8	0.0	.	–	• 0 ▽ 8 55 – 9 06
5	8	0.3	.	–	• 0 ▽ 7 15 – 8 40
6	8	2.9	.	–	• 0 ▽ 8 45 – 9 10 14 25 – 16 15 • 0 – 18 20 • 0 * 19 21 * 0 – 24
7	4	5.9	1	–	* 0 0 00 – 18 40
8	6	0.7	8	–	* 0 1 35 – 11 32 . 12 22 – 15 40 . = 11 30 – 17 20 . 20 20 – 24
9	5	.	8	–	= 0 00 – 24
10	6	0.0	8	–	= 0 00 – 23 40
11	8	5.6	7	–	* 0 3 40 – 4 04 • 0 15 45 – 16 38 • 0 – 17 15 * 0 – 19 50 • 0 * – 20 10 • 0 – 21 35 • 0 23 40 – 24 . = 17 30 – 20 20
12	6	1.9	pł.	–	• 0 0 00 – 2 20 • 0 3 10 – 7 12 10 18-40 • 0 * – 11 19 • 0 13 40 – 16 42 . 19 10 – 22 30 . = a-np
13	6	0.8	2	–	* 0 2 40 – 21 10 . = 0 00 – 14 30
14	8	0.7	5	–	* 0 17 40 – 18 15 . 21 18 – 24 . = 5 50 – 6 10
15	5	3.1	6	–	* 0 0 00 – 13 40 17 35 – 20 10 23 35 – 24 . = 13 40 – 14 20 . ⊹ 1 50 – 12 40
16	5	0.0	11	–	* 0 0 00 – 2 35 . 5 50 – 6 40 . 7 40 – 14 18 . = 2 35 – 14 20 . 15 45 – 17 10
17	6	0.3	13	–	* 0 8 25 – 20 35 . = 2 30 – 24
18	6	0.3	14	–	* 0 7 40 – 18 30 . = 0 00 – 2 30 . 6 10 – 7 15 . 8 45 – 24
19	5	0.4	15	–	△ 0 10 35 – 11 40 . 12 20 – 13 35
20	6	7.1	16	–	△ 0 2 20 – 6 10 * 0 15 00 – 24 ⊹ 16 45 – 24 . = 0 00 – 13 36
21	7	0.3	24	–	* 0 0 00 – 2 35 . 4 40 – 9 40 ▽ 0 11 55 – 45 . 12 02 – 40 ⊹ 0 00 – 45 . 12 40 – 15 50
22	6	4.7	28	–	* 0-1 12 00 – 21 26 * 0 22 40 – 24 . = 6 15 – 8 20 . ⊹ 12 40 – 20 45
23	7	0.0	29	–	* 0 0 00 – 2 20 . 3 40 – 6 40 . 13 50 – 14 15 . = 9 15 – 11 20
24	6	0.2	29	–	* 0 5 50 – 10 45 . 11 12 – 12 10 . = 15 50 – 19 45 ≡ 1-0 – 24
25	6	.	29	–	= 0 00 – 4 50 = – 24
26	6	.	29	–	= 0 00 – 24
27	5	0.0	29	–	* 0 21 40 – 24 . = 0 00 – 24
28	6	0.0	28	–	* 0 0 00 – 3 20 . = 0 00 – 24
29	5	1.1	22	–	⌒ 0 6 35 – 10 50 . = 0 00 – 24
30	5	.	17	–	= 0 00 – 1 50 ≡ 0 – 3 40 = – 6 20 ≡ 1-0 9 50 = – 24
31	7	.	16	–	= 0 00 – 6 45 . 14 20 – 20 20
Σ	–	37.3	–	–	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Styczeń – Janvier 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	17.6	18.9	20.0	18.8	-5.7	-1.5	-5.9	-4.2	-0.7	-9.0	92	84	81	86	0.4	0.9	0.7	0.7	10	10	3	C 0	C 0	SE 2
2	16.9	14.7	13.4	15.0	-5.5	-2.2	-6.3	-5.0	-1.9	-9.9	87	85	94	89	0.5	0.8	0.2	0.5	10	10 *	10 =	SE 2	ENE 1	C 0
3	8.4	3.6	6.7	6.2	-8.1	4.6	4.9	1.6	8.5	-11.6	87	53	63	68	0.4	4.0	3.2	2.5	3	8	9	NE 1	SSW 10	S 7
4	5.1	5.7	6.7	5.8	7.1	6.4	5.8	6.3	7.6	4.2	47	61	65	58	5.4	3.7	3.2	4.1	8	9 •	9 •	SSW 5	WSW 5	SW 4
5	7.0	10.8	16.6	11.5	0.4	0.5	-1.9	-0.7	5.8	-3.9	94	92	83	90	0.4	0.5	0.9	0.6	10 *	10 *	7	C 0	C 0	SW 1
6	19.6	19.1	15.8	18.2	-3.2	-1.1	-1.2	-1.7	-0.3	-5.5	81	71	62	71	0.9	1.7	2.1	1.6	1	0 ⊙	0	SSW 1	S 1	SE 4
7	13.7	14.6	16.3	14.9	1.0	0.2	-6.0	-2.7	2.7	-6.4	64	84	89	79	2.4	1.0	0.4	1.3	4	10	3	S 3	SE 2	ESE 1
8	17.1	16.3	14.6	16.0	-0.8	1.9	0.2	0.4	2.6	-7.3	83	63	73	73	1.0	2.6	1.7	1.8	9	7 ⊙	10 *	NE 2	SE 3	SW 1
9	15.5	16.0	16.3	15.9	-1.6	1.0	-6.2	-3.2	2.6	-7.2	88	81	84	84	0.6	1.3	0.6	0.8	4	3 ⊙	1	C 0	NE 1	SW 1
10	16.2	16.3	16.4	16.3	-4.3	-0.2	-6.6	-4.3	0.1	-7.6	84	80	86	83	0.7	1.2	0.5	0.8	8	6 ⊙	2	C 0	ENE 1	C 0
11	16.5	17.2	21.0	18.2	-10.6	-0.3	-5.1	-5.3	-0.2	-11.0	80	70	88	79	0.5	1.8	0.5	0.9	4	8 ⊙	8	C 0	C 0	C 0
12	24.5	26.9	29.9	27.1	-2.7	-6.4	-6.6	-5.6	-1.0	-7.9	91	68	78	79	0.5	1.2	0.8	0.8	10 ⛬	8	10 *	NE 2	W 3	C 0
13	31.5	30.9	30.6	31.0	-7.3	-2.7	-7.9	-6.4	-1.9	-10.4	76	62	67	68	0.8	1.9	1.1	1.3	9	0 ⊙	0	C 0	SW 1	SE 2
14	29.4	28.8	30.5	29.6	-4.7	-0.6	-2.9	-2.8	-0.4	-9.3	81	70	73	75	0.8	1.8	1.3	1.3	10	9	4	C 0	C 0	C 0
15	32.3	32.1	30.5	31.6	-3.1	1.3	-8.4	-4.6	1.7	-8.9	86	71	80	79	0.7	1.9	0.6	1.1	9	1 ⊙	0	E 2	E 2	C 0
16	26.1	24.0	25.3	25.1	-7.8	1.5	-7.0	-5.1	3.8	-10.2	75	43	82	66	0.9	4.3	0.6	1.9	0	0 ⊙	10	C 0	E 2	C 0
17	25.8	27.2	31.0	28.0	-6.1	-7.7	-12.3	-9.6	-4.3	-16.1	68	70	63	67	1.2	1.0	0.9	1.0	9	1 ⊙	9 ⛬	C 0	NE 2	E 3
18	35.2	36.0	36.0	35.7	-21.3	-9.7	-17.7	-16.6	-9.4	-22.4	74	53	68	65	0.3	1.4	0.5	0.7	0	0 ⊙	0	NE 2	E 2	C 0
19	33.7	31.7	31.0	32.1	-17.8	-7.2	-7.7	-10.1	-6.3	-19.8	57	55	79	64	0.6	1.6	0.7	1.0	2	9	10	S 2	E 1	C 0
20	28.4	26.3	24.5	26.4	-9.8	-2.5	-12.1	-9.1	-1.8	-13.1	85	55	78	73	0.4	2.3	0.5	1.1	6	0 ⊙	0	C 0	ENE 1	SE 1
21	21.2	20.0	20.1	20.4	-14.1	-5.7	-11.5	-10.7	-5.4	-14.7	70	57	65	64	0.6	1.7	0.9	1.1	1	4 ⊙	2	SW 1	NE 1	C 0
22	18.7	17.4	16.5	17.5	-13.5	-5.2	-11.3	-10.5	-4.4	-14.1	68	65	83	72	0.7	1.4	0.4	0.8	2	8 ⊙	3	ESE 2	ENE 1	C 0
23	12.8	11.4	12.8	12.3	-7.5	-3.9	-4.6	-5.2	-3.9	-11.8	84	80	88	84	0.5	0.9	0.5	0.6	10 *	10 *	10 ⛬	C 0	SSE 1	ESE 1
24	13.5	12.3	10.6	12.1	-7.4	-6.6	-7.5	-7.2	-4.6	-8.2	87	88	87	87	0.4	0.4	0.4	0.4	10	3	10 *	ESE 1	C 0	C 0
25	7.7	7.7	11.7	9.0	-10.5	-8.6	-14.6	-12.1	-7.5	-15.1	70	68	69	69	0.8	1.0	0.6	0.8	10	4 ⊙	0 *	SSE 1	ENE 5	E 3
26	16.9	20.4	25.3	20.9	-20.3	-8.8	-16.2	-15.4	-6.0	-22.2	76	41	76	64	0.3	1.9	0.4	0.9	0	0 ○	0	E 2	NE 2	C 0
27	29.6	30.0	30.6	30.1	-16.3	-3.4	-13.1	-11.5	-1.4	-17.7	71	32	76	60	0.5	3.2	0.5	1.4	0	0 ○	0	C 0	E 1	ESE 1
28	29.3	27.4	24.1	26.9	-15.1	-2.2	-12.4	-10.5	-1.5	-16.1	73	33	66	57	0.5	3.5	0.8	1.6	0	0 ○	0	C 0	C 0	C 0
29	25.2	24.8	24.6	24.2	-14.7	-0.1	-4.2	-5.8	1.6	-15.6	69	75	84	76	0.6	1.6	0.7	1.0	1	9	0	C 0	W 2	C 0
30	20.2	16.4	13.5	16.7	-9.2	5.2	6.9	2.4	8.1	-11.2	82	25	52	53	0.5	6.5	4.7	5.9	6	9	10	SE 1	WSW 2	WNW 5
31	12.6	7.4	10.3	10.1	-0.2	4.2	2.9	2.4	7.4	-0.2	90	76	84	83	0.6	1.9	1.2	1.2	10	10 •	10 •	C 0	WSW 5	W 7
M	20.2	19.7	20.4	20.1	-7.7	-1.9	-6.3	-5.6	-0.3	-10.9	78	65	76	73	0.8	2.0	1.0	1.3	5.7	5.4	4.8	1.0	1.9	1.4

Luty – Février

1	8.4	2.1	2.6	4.4	-1.2	4.7	1.4	1.6	6.5	-1.3	84	55	74	71	0.9	3.8	1.8	2.2	10	10	10	SE 3	SW 6	NW 3
2	3.2	0.7	98.1	0.7	-1.3	0.4	-5.0	-2.7	1.9	-5.8	86	72	85	80	0.8	1.8	0.7	1.1	10	6 ⊙	3	SW 2	S 2	SW 2
3	96.9	98.9	3.7	99.8	-2.7	-0.6	-5.1	-2.4	0.6	-7.0	80	81	81	81	1.0	1.1	0.9	1.0	10	10 ⛬ *	9	C 0	WSW 7	C 0
4	10.1	10.7	6.9	9.2	-4.2	-3.5	-10.8	-7.3	-2.7	-12.8	79	78	80	79	0.9	1.0	0.5	0.8	10 *	9 *	0	W 4	SE 1	ESE 1
5	7.6	12.2	20.1	13.3	-7.6	-2.4	-5.1	-5.0	-1.8	-13.3	82	78	85	82	0.6	1.1	0.6	0.8	10	9 *	10 *	ESE 1	ENE 2	NE 3
6	22.6	21.1	18.1	20.6	-16.1	-2.4	-8.1	-8.7	-0.2	-17.2	76	51	81	69	0.4	2.3	0.6	1.2	0	2 ⊙	8	C 0	C 0	C 0
7	13.8	13.3	14.2	13.8	-7.0	-0.6	-1.0	-2.4	1.0	-11.3	82	81	81	81	0.6	1.1	1.1	0.9	9	9	10	SE 1	SW 3	SW 3
8	15.4	18.0	21.3	18.2	-1.2	-0.3	-1.6	-1.2	-0.4	-3.3	84	86	86	85	0.9	0.9	0.7	0.8	10 *	10 *	10 ⛬	W 2	W 4	WSW 2
9	21.3	17.6	14.0	17.6	-8.1	0.0	-2.7	-3.4	0.3	-9.3	78	71	91	80	0.7	1.8	0.5	1.0	8	10	10 *	SE 1	SW 1	C 0
10	17.4	21.8	27.0	22.1	1.0	-0.3	-1.5	-0.6	1.1	-3.3	90	88	90	89	0.7	0.8	0.3	0.7	10	10 *	10 •	SW 2	W 4	W 5
11	24.2	20.2	16.7	20.4	-3.9	3.0	-0.3	-0.3	3.4	-4.2	85	77	88	83	0.7	1.8	0.7	1.1	8	3 ⊙	10	WSW 2	C 0	C 0
12	11.8	11.3	18.0	13.8	-0.7	0.9	0.2	0.2	1.0	-2.6	89	83	96	90	0.6	1.0	0.3	0.6	9	10 *	10	C 0	W 1	E 1
13	25.3	25.1	26.0	24.9	0.2	0.2	-1.1	-0.4	0.3	-1.1	92	83	87	87	0.3	1.1	0.8	0.8	10	9	9	W 2	NW 2	NW 1
14	28.2	29.8	30.8	29.6	-1.8	1.7	-4.9	-2.3	3.0	-5.6	88	70	78	79	0.7	2.0	0.9	1.2	10	4 ⊙	1	C 0	C 0	C 0
15	31.0	32.0	33.1	32.0	-9.0	3.6	-3.7	-3.2	5.2	-9.6	82	49	92	74	0.3	4.0	0.4	1.6	6	0 ⊙	0	S 1	E 2	C 0
16	33.1	34.1	35.8	34.3	1.3	2.3	1.3	1.6	4.7	-6.2	73	91	92	85	1.8	0.6	0.3	1.0	10	10 •	10	SE 2	NW 2	SW 1
17	37.3	37.3	37.1	37.4	-2.3	3.9	-2.3	-0.8	6.3	-5.4	93	76	80	83	0.4	1.9	1.1	1.1	4	6 ⊙	0	SW 1	SW 1	SE 2
18	36.1	35.6	34.3	35.4	-4.0	11.7	-0.3	1.7	13.3	-4.6	77	30	63	57	1.0	9.6	2.1	4.2	1	0 ⊙	0	C 0	C 0	C 0
19	31.9	31.1	32.1	31.7	-4.9	9.3	2.0	2.1	9.9	-5.3	83	44	83	70	0.7	6.7	1.2	2.9	0	1 ⊙	9	C 0	SW 1	ESE 1
20	32.4	33.9	33.3	33.9	0.1	1.3	-0.3	0.2	2.0	-0.3	92	83	90	89	0.3	1.0	0.6	0.7	10 *	10	10	ENE 1	E 1	C 0
21	33.6	36.2	33.9	33.9	-1.2	0.0	0.3	0.0	1.3	-1.2	89	84	79	84	0.6	1.0	1.3	1.0	8	10	10	C 0	NE 2	E 1
22	33.6	34.7	33.9	34.7	-3.9	2.3	-4.4	-3.1	3.0	-6.4	89	62	89	80	0.4	2.7	0.3	1.2	1	8 ⊙	1	C 0	ENE 1	C 0
23	32.1	31.2	31.0	31.4	-9.0	3.2	-4.4	-3.6	4.1	-9.1	86	53	77	72	0.4	3.7	1.0	1.7	2	1 ⊙	0	C 0	ENE 1	ESE 1
24	30.3	30.6	31.1	30.7	-7.8	3.0	-3.9	-3.2	3.3	-8.7	84	55	87	75	0.3	3.4	0.6	1.3	0	0	0	C 0	ENE 2	C 0
25	31.8	32.1	33.3	32.3	-6.3	5.8	-2.3	-1.3	6.6	-7.3	89	46	83	73	0.4	3.0	0.8	2.1	0	0 ⊙	0	C 0	NE 2	C 0
26	34.1	33.0	36.0	33.0	-7.3	1.4	-4.0	-3.3	2.3	-8.0	84	74	87	82	0.3	1.8	0.6	1.0	0	0 ⊙	9	C 0	ENE 2	C 0
27	33.3	34.0	31.3	33.6	-9.3	4.0	-0.9	-1.8	5.4	-9.8	82	62	89	78	0.3	3.1	0.6	1.4	0	1 ○	8	C 0	NE 2	C 0
28	24.4	19.6	16.9	20.3	-3.3	3.3	1.8	1.4	6.3	-3.8	90	61	86	79	0.3	3.4	1.0	1.6	8	8 ⊙	10 •	C 0	ESE 2	C 0
29																								
30																								
31																								
M	25.8	25.6	24.1	25.8	-4.4	2.1	-2.3	-1.7	3.2	-6.3	85	69	84	79	0.7	2.3	0.8	1.3	6.2	6.0	6.3	0.9	1.9	1.0

Zakopane — $H_s = 844\,m$ — $H_b = 838{,}2\,m$ — $h_w = 17{,}7\,m$ — Styczeń - Janvier 1961

DNI	WIATR DZIAŁ.	WIATR NOŚĆ v	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	6	0.0	10	–	☀°6⁵⁵ 9⁰³, = 9²⁰ – 19³⁵ ☂¹ 23³⁰ – 24
2	5	0.6	9	–	☀° 7²⁵ – 16⁵¹, ≡° 0²⁰ 1⁴⁰ = a, p ≡³⁻° 20²⁷ – 24, V° np, ☂¹ na
3	9	0.0	9	–	•° 19⁵¹ – 21⁴⁸, ≡° 0⁰⁰⁻²⁶, ⩓ 11³⁰ – 12³⁰ ⩓ – ⩔ – 16⁴⁰ ¹ ⩔ – 17⁴⁰, V° 0⁰⁰⁻²⁶
4	8	9.3	pż.	–	•° 12³⁰ – 17⁴⁵, 20⁴⁵ – 23⁴⁰ •° – 24
5	7	7.9	1	–	•°0⁰⁰ 5⁴⁰ ☀⁰⁻¹ – 13¹⁰, = 0⁴⁰ – 12³⁰
6	9	.	9	–	△° 0⁵⁰ – 2¹⁰
7	8	0.0	8	–	⌴⁰⁻¹ 19⁰⁰ – 24
8	9	0.0	5	–	▽° 1¹⁵ – 3⁰⁷ ☀° 19⁵⁰ 22³⁰ – 23⁴⁵, ⌴¹ 0⁰⁰ – 11⁰⁰
9	8	.	5	–	
10	7	.	4	–	⌴° 21⁰⁰ – 24
11	8	0.2	4	–	⌴⁰⁻¹ 0⁰⁰ – 8⁰⁰ ⊕° 9⁰⁰ – 30
12	8	1.9	4	–	☀° △° 3⁴² 11⁴⁵ ☀° ▽ 11⁴⁸ 15²⁰ ☀° 18⁵⁰ 20⁵⁰ – 23⁴⁵
13	8	.	8	–	
14	7	.	7	–	= 14³⁰ – 15¹⁰ 17²⁰ – 18³⁰
15	8	.	7	–	⌴° 19⁰⁰ – 24
16	8	0.0	6	–	⌴° 0⁰⁰ – 9⁰⁰
17	8	0.0	5	–	☀° 0⁵⁵ 5¹⁰, 9⁴⁵ – 10²⁵ △° 20³⁵ – 22²⁰, ⌴¹ 23⁰⁰ – 24
18	9	.	5	–	
19	8	.	5	–	
20	8	.	4	–	
21	7	.	4	–	⌴¹ na – / ⌴° 20⁰⁰ – 24
22	8	0.6	4	–	⌴⁰⁻¹ 0⁰⁰ – 12⁰⁰ ⌴° 20⁰⁰ – 24
23	6	0.5	6	–	☀° 3⁵⁷ – 20³⁰ △ – 21¹⁵ ⟷ – 24, = 7¹⁵ – 12¹⁵, ⌴° 0⁰⁰ – 3⁰⁰
24	5	0.1	7	–	⟷ 0⁰⁰ 1¹⁰ ☀° 20⁴⁵ – 24, = 6¹⁵ – 7¹⁵ ≡° – 10⁴³ V° 8¹⁵ – 10⁴³
25	8	0.0	8	–	☀° 0⁰⁰ – 2⁵⁰ 18⁴⁵ – 21²⁰, = 0⁰⁰ – 6³⁰, ⌴¹ 19⁰⁰ – 22⁰⁰
26	7	.	8	–	⌴⁰⁻¹ 0⁰⁰ – 12⁰⁰ ⌴° 18⁰⁰ – 24
27	7	.	8	–	⌴° 0⁰⁰ – 10²⁰, 19⁰⁰ – 24
28	7	.	7	–	⌴° 0⁰⁰ – 9⁰⁰
29	8	.	7	–	⌴° 0⁰⁰ – 9⁰⁰, 22⁰⁰ – 24
30	9	.	6	–	– 7³⁰ – 12¹⁰, ⌴¹ 0⁰⁰ – 12⁰⁰
31	6	0.6	4	–	•° 10⁰⁰ 11⁴⁰, 12⁴⁰ – 13⁴⁵ •° ▽ 15¹⁵–22 •¹ ▽ 19⁴⁵ – 20⁵⁰, = a, p
Σ	–	21.7	–	–	UWAGI: W ciągu całego roku uwagi o silnych wiatrach są niepewne.

Luty – Février

1	6	1.7	pż.	–	•°☀° 11⁴⁰ – 15³⁰ ☀° – 16¹⁰ •° – 17⁴⁵ ☀°△° 20⁴⁰ – 24, ⌴° 3⁰⁰ – 9⁰⁰, ☂¹ 3⁰⁰ – 5²⁰ ⊕° 9¹⁵ – 10⁴⁰
2	8	0.0	3	–	☀° 0⁰⁰ 4⁴⁰ ⊕¹ 9³⁵ 11¹⁵ ☂ °21¹⁰ – 23³⁰
3	6	2.5	2	–	△ 6⁴⁵ 7²⁵ ☀° – 9³⁰ 10²⁵ ▽⁰⁻¹ ☀ 11³⁰ – 13⁴⁰ ☀° ▽ ☀° △° 14⁴⁵ 24, = a, ☂ na
4	7	0.2	5	–	☀° 0⁰⁰ 12³⁰ ☀° ▽ – 13³⁵, ⌴° 19⁰⁰ – 24 ☂¹ 23¹⁵ – 24
5	6	3.9	6	–	☀° 11⁴⁰ 12⁴⁵ ☀° ▽ 12⁵⁰ – 14²⁰ ☀⁰⁻¹ 14³⁰ – 23¹⁰ 24, ⌴° 0⁰⁰ – 9⁰⁰, ☂¹ a
6	9	.	10	–	☀° 0⁰⁰ – 2⁴⁰, ⌴¹ na ⌴° 18⁰⁰ – 24
7	7	0.1	9	–	☀° 8⁵⁵, 10⁰⁷ △° – 10²⁰ ☀° 11⁰⁶, = a, ⌴¹ 0⁰⁰ – 9⁰⁰
8	7	1.4	8	–	☀⁰⁻² 6³⁵ – 7³⁷ ☀⁰⁻² – 6⁴⁰ △° 20²⁰ – 21¹⁰ ▽° – 22¹⁵
9	7	9.4	9	–	☀° 0⁴⁵ 1¹⁸ – 13⁴⁵ 14¹⁰ – 14²⁰ 16³⁰ △° – 17⁴⁰ ☀⁰⁻¹ – 24
10	6	3.5	20	–	☀° 0⁰⁰ – 2³⁰, 3³⁰ •° – 5²⁰ 6⁴⁰ △° 8⁵⁴ – 12¹⁵ ☀° – 13²⁵ △ – 19⁴⁵ ☯ ∼ – 24, = a
11	7	2.3	17	–	☯° ∼ 0⁰⁰ 3³⁰
12	6	2.8	20	–	☀⁰⁻¹ 3³⁸ – 5²⁵ ☀° 11⁵⁰ – 12¹⁰ 12²⁰ – 13⁵⁸ •° – 14¹⁵ ☀° – 17⁴⁵, ≡¹⁻⁰ 8²⁰ – 9¹⁵ = a – 24
13	7	0.1	21	–	△° 6⁰⁵ – 40 ☯ △ 7²⁰ – 8⁵⁵ ☀° ▽ 15⁵³ – 17⁴⁵, = 0⁰⁰ – 6¹⁰
14	9	.	20	–	= 6¹⁵ – 8²⁰ ⌴° 19⁰⁰ – 24
15	8	.	20	–	⌴° 0⁰⁰ – 8⁰⁰, 19⁰⁰ – 24
16	7	0.6	15	–	•° 10⁴⁰ 11¹⁰, 11¹⁵ – 12²⁵ •° – 17²⁰, = a, p – 24, ⌴° na, ⌓° 1¹⁵ – 3³⁰
17	7	.	14	–	⌴¹ na – / ⌴° 22⁰⁰ – 24
18	9	.	10	–	⌴° 0⁰⁰ – 9⁰⁰
19	9	0.5	8	–	= 18³⁰ – 20¹⁵ np, ⌴° 1⁰⁰ – 9⁰⁰
20	6	0.8	5	–	•° 0⁵⁰ 3²⁵ •° 6⁴⁵ – 7¹⁵ ☀° – 8⁵⁰ △ 9³⁰ – 10⁴⁵ •° 13⁵⁵ 14⁴⁰, = 0⁰⁰ – 24
21	6	.	5	–	= 0⁰⁰ – 20⁴⁰
22	7	.	5	–	⌴° 3⁰⁰ – 8⁰⁰, 21⁰⁰ – 24
23	7	.	5	–	≡² 2⁴⁵ – 4⁴⁷ = a, ⌴° 0⁰⁰ – 2⁰⁰ V° 2⁴⁵ – 4⁴⁷ ⌴° 5⁰⁰ – 8⁰⁰, 19⁴⁰ – 24
24	6	.	5	–	– 10¹⁵ – 15³⁰ ⌴° 0⁰⁰ – 9⁰⁰
25	8	.	4	–	♏ 9⁵ – 10³⁰, ⌴° na – 8⁴⁰, 20⁰⁰ – 24
26	7	.	3	–	⌴¹ 0⁰⁰ – 9⁰⁰ 18⁰⁰ – 21⁰⁰
27	8	.	3	–	⌴° 1⁰⁰ – 8⁰⁰ 19⁰⁰ – 24
28	7	7.5	2	–	•° 19⁴⁰ 21²⁰ •⁰⁻⁰ – 23⁴⁵ ☀° – 24, = 6³⁰ – 7⁴⁰, 18³⁰ – 24, ⌴° na – a
29					
30					
31					
Σ	–	37.3	–	–	UWAGI: Dnia 2.II.1961 r. w terminie III oraz dnia 3 w terminach I, II i w średniej dziennej ciśnienie powietrza wynosi 800 mb + wartość podana w tablicy.

Zakopane — φ = 49°18' — λ = 19°57' — Marzec – Mars 1961

DNI	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	19.0	20.4	25.0	21.5	-1.5	1.6	-0.1	0.0	2.2	-1.5	90	72	84	82	0.5	1.9	1.0	1.1	10	7	9	C 0	WNW 3	SE 2
2	28.9	29.5	28.7	29.0	-1.2	0.9	-0.4	-0.3	1.9	-1.7	82	71	70	74	1.0	1.9	1.8	1.6	9	9 *	9	SW 2	SW 3	SSW 2
3	28.1	30.5	32.6	30.4	-1.2	2.4	0.4	0.5	2.6	-4.4	76	64	81	74	1.3	2.6	1.2	1.7	9	9	10 *	WSW 2	C 0	ESE 1
4	34.1	36.0	37.3	35.8	0.4	1.3	1.0	0.9	1.7	0.3	92	92	92	92	0.5	0.5	0.5	0.5	10 *	10 •	10	C 0	C 0	C 0
5	35.9	35.7	35.6	35.7	-1.5	7.7	2.8	3.0	7.8	-1.8	82	31	77	63	1.0	7.3	1.7	3.3	8	9 ⊙	10	SW 2	W 3	SE 1
6	35.6	35.2	34.5	35.1	0.2	6.1	0.4	1.8	7.7	-0.2	80	57	84	74	1.2	4.1	1.0	2.1	9	8 ○	3	C 0	ENE 2	C 0
7	32.0	30.6	32.2	31.6	1.7	10.5	3.1	4.6	11.9	-2.0	54	41	64	53	3.2	7.5	2.7	4.5	6	8 ⊙	5	C 0	C 0	SE 3
8	33.9	34.9	35.6	34.8	-0.4	10.2	2.4	3.6	10.4	-0.4	90	37	62	63	0.6	7.8	2.8	3.7	3 ○	5 ○	2	ESE 1	NE 1	SW 2
9	34.9	34.0	33.4	34.1	2.5	8.7	3.5	4.6	11.1	0.3	74	61	63	66	1.8	4.4	2.9	3.0	9	2 ○	0	NNW 2	W 4	S 2
10	32.2	29.7	28.2	30.0	3.0	15.2	3.3	6.2	15.5	1.2	85	44	79	69	1.1	9.8	1.6	4.2	3 ○	1 ⊙	0	C 0	ENE 1	S 1
11	27.1	26.9	28.3	27.4	4.2	11.0	6.8	7.2	11.9	1.8	65	43	72	60	2.8	7.4	2.8	4.3	4	8	10	SW 1	WNW 4	NW 4
12	26.7	24.5	19.8	23.7	4.4	8.6	9.6	8.0	10.1	3.8	64	52	49	55	3.0	5.5	6.1	4.9	10	8 ○	8	WNW 3	W 5	SW 5
13	11.8	13.7	16.8	14.1	5.2	4.4	2.3	3.6	10.9	2.3	85	53	66	68	1.3	4.0	2.4	2.6	10	9	9	W 4	W 5	WSW 6
14	18.3	17.9	19.8	18.7	0.5	2.4	4.4	2.9	4.4	0.5	72	85	93	83	1.8	1.1	0.6	1.2	9	10 *	10 •	WNW 4	W 2	C 0
15	20.8	22.7	26.2	23.2	3.6	5.8	5.5	5.1	7.8	3.2	91	77	67	78	0.7	2.1	2.9	1.9	10 •	9	5	W 4	SW 7	SSE 2
16	25.5	22.8	23.7	24.0	4.6	9.8	6.1	6.6	10.7	3.8	86	58	80	75	1.2	5.0	1.9	2.7	10	9	10 •	WNW 5	WSW 4	WSW 6
17	27.3	26.6	23.7	25.9	1.2	11.1	3.8	5.0	12.4	0.7	79	32	55	55	1.4	8.9	3.6	4.6	5 ○	7 ⊙	1	C 0	SW 2	SW 1
18	16.4	13.2	9.5	13.0	0.1	15.2	12.5	10.1	15.6	-1.1	72	30	40	47	1.8	12.2	8.8	7.6	7	5 ⊙	2	C 0	WSW 5	SSW 5
19	8.3	8.8	10.2	9.1	1.4	1.4	-0.4	0.5	12.5	-0.4	94	76	86	85	0.4	1.7	0.8	1.0	10 •	10	8	C 0	NW 3	SE 1
20	12.8	13.0	9.0	11.6	-5.2	-1.5	-1.9	-2.6	0.6	-5.5	77	60	65	67	0.9	2.3	1.9	1.7	7 * ○	4 ⊙	9	NE 1	NE 4	WSW 4
21	0.9	0.9	4.6	2.1	-0.1	0.1	-0.6	-0.3	1.6	-3.7	86	86	72	81	0.9	0.9	1.7	1.2	10 *	10 *	9	WSW 4	W 6	WSW 4
22	9.8	13.8	17.2	13.6	-3.3	-3.4	-7.2	-5.3	-0.7	-7.2	81	83	85	83	0.9	0.8	0.5	0.7	10 *	10 ⚠ *	7	NE 2	NNW 2	WSW 4
23	16.4	17.9	20.9	18.4	-3.7	0.2	0.5	-0.6	0.6	-9.6	85	88	89	87	0.7	0.8	0.7	0.7	10 *	10 *	10 *	SW 2	W 3	SE 3
24	22.2	22.3	23.0	22.5	1.7	3.6	2.6	2.6	4.2	0.5	79	68	78	75	1.4	2.5	1.6	1.8	10 ⚠	10	10	W 1	WNW 3	SW 2
25	23.2	24.4	25.5	24.4	1.9	3.7	2.4	2.6	4.7	1.8	88	73	88	83	0.8	2.2	0.9	1.3	10 •	9	10	S 3	WSW 3	SW 1
26	23.6	21.8	16.5	20.6	1.5	5.8	5.0	4.3	7.2	1.2	90	56	49	65	0.7	4.0	4.4	3.0	4 ○	10	7	C 0	NNW 4	W 3
27	12.3	12.9	12.3	12.5	5.0	0.7	-0.3	1.3	8.1	-1.0	70	88	63	74	2.6	0.8	2.3	1.9	10 •	10 *	4	W 4	SW 3	W 3
28	12.8	14.3	13.8	13.6	-4.7	-5.1	-5.2	-5.6	-0.2	-6.1	91	84	92	89	0.4	0.8	0.3	0.5	10 *	10 *	10 *	WSW 4	WNW 8	W 5
29	16.0	15.1	15.7	15.6	-5.6	1.4	1.1	0.0	1.6	-4.2	85	72	83	80	0.7	2.0	1.1	1.3	10	10	10	SW 2	W 4	NW 4
30	13.6	13.1	10.5	12.4	2.6	5.3	5.8	4.9	7.2	1.1	58	64	65	62	3.1	3.2	3.2	3.2	2 ○	9	10	W 6	WNW 7	SW 2
31	9.3	11.3	11.8	10.8	6.4	4.1	4.4	4.8	7.7	4.1	71	86	81	79	2.7	1.1	1.6	1.8	10 •	10 •	10 •	W 4	ESE 1	NW 2
M	21.6	21.8	22.0	21.8	0.8	4.9	2.4	2.6	6.8	-0.8	80	64	73	72	1.4	3.8	2.2	2.5	8.2	8.2	7.3	2.0	3.3	2.6

Kwiecień – Avril

1	16.3	14.2	12.6	14.4	0.3	7.9	6.8	5.4	7.9	-0.2	69	48	68	62	1.9	5.5	3.2	3.5	1 ○	7 ○	10 •	WNW 3	W 8	WSW 5
2	13.7	14.3	13.3	13.8	2.1	7.6	5.2	5.0	10.1	1.7	93	73	81	82	0.5	2.8	1.7	1.7	10 • *	10	8	ENE 2	N 3	C 0
3	10.2	12.1	14.2	12.2	5.4	9.5	6.1	6.8	10.5	2.7	92	55	87	78	0.8	5.3	1.7	2.6	9	9	9 •	C 0	WSW 6	SW 2
4	13.5	15.8	18.8	16.0	9.2	11.4	7.6	9.0	13.0	2.0	50	51	80	60	5.8	6.5	2.1	4.8	8 ○	9	9	SW 7	WNW 7	C 0
5	18.7	18.4	19.3	18.8	5.5	16.5	10.0	10.5	17.1	3.2	84	38	62	61	1.4	11.6	4.8	5.9	8	2 ⊙	0	C 0	S 5	ESE 1
6	20.0	19.8	20.1	20.0	5.9	19.1	14.5	13.5	19.7	3.0	74	24	48	49	2.4	16.8	8.6	9.3	2 ○	1 ⊙	0	ENE 1	ESE 1	S 4
7	18.9	19.4	20.1	19.5	11.1	20.2	11.1	13.4	21.2	6.6	59	28	65	51	5.4	17.1	4.7	9.1	0 ○	0 ⊙	0	NE 3	SW 3	SW 1
8	18.8	16.3	17.9	17.7	10.7	19.0	7.9	11.4	19.7	7.1	66	40	93	66	4.4	13.3	0.7	6.1	6	6 ⊙	10	SW 1	SW 5	NW 3
9	21.1	22.1	22.4	21.9	0.4	5.8	0.8	2.0	7.9	0.3	82	50	75	69	1.2	4.6	1.7	2.5	9	6 ⊙	3	NE 3	N 3	ESE 1
10	20.9	17.4	15.6	18.0	-2.0	8.7	5.8	4.6	10.2	-4.6	83	38	65	62	0.9	6.9	3.2	3.7	0 ⊙	8 ⊙	10	C 0	E 2	C 0
11	13.2	13.0	15.7	14.0	5.6	14.2	7.7	8.8	14.3	4.9	76	48	80	68	2.1	8.4	2.1	4.2	9	7 ⊙	10	C 0	NNE 3	C 0
12	18.8	20.6	22.2	20.5	1.6	10.0	2.1	4.0	11.1	0.3	93	44	79	72	0.6	6.8	1.4	2.9	8 ○	3 ⊙	0	C 0	ESE 3	SE 2
13	21.1	20.4	21.1	20.9	5.9	16.1	8.3	9.6	16.9	-0.8	48	34	70	51	4.8	12.1	3.4	6.8	7	4 ⊙	0	C 0	SW 3	SE 1
14	20.2	19.2	18.2	19.2	6.2	18.5	11.5	11.9	19.1	2.0	80	20	43	48	1.9	17.1	7.7	8.9	8 ⊙	8 ⊙	0	C 0	SSE 5	E 2
15	18.3	18.5	18.8	18.5	14.3	19.1	10.5	13.6	19.3	4.7	31	25	76	44	11.4	16.6	5.1	10.4	0 ⊙	3 ⊙	4	SW 3	SSW 6	C 0
16	18.1	16.5	16.9	17.2	12.8	14.3	5.9	9.7	16.2	5.7	51	45	89	62	7.3	9.1	1.1	5.8	9 •	6 •	0	SW 4	SSW 7	C 0
17	17.1	17.0	18.2	17.4	6.4	14.7	7.9	9.2	15.2	1.3	76	49	90	72	2.3	8.5	1.1	4.0	1 ○	9	0	E 1	NNE 3	C 0
18	18.0	16.9	16.6	17.2	5.7	15.6	9.0	9.8	16.0	2.3	83	48	90	74	1.6	9.2	1.2	4.0	6 ⊙	8 ○	10	E 1	NE 2	C 0
19	18.0	19.2	18.5	18.6	8.6	11.3	8.7	9.3	12.2	7.6	90	68	93	84	1.2	4.3	0.7	2.1	10	9	10 •	C 0	E 2	C 0
20	18.9	21.0	22.7	20.9	6.0	9.5	5.5	6.6	10.5	5.3	84	49	67	67	1.5	6.0	2.9	3.5	10	9	5	N 1	NE 3	E 3
21	22.3	21.2	20.7	21.4	0.7	12.3	4.1	5.3	14.0	-1.9	85	33	73	64	1.0	9.6	2.2	4.3	2 ⊙	0 ⊙	0	C 0	E 3	C 0
22	18.7	16.0	14.4	16.4	4.5	14.5	9.0	9.2	15.0	-0.9	67	40	49	52	2.7	9.9	5.9	6.2	0 ⊙	2 ⊙	1	ENE 1	NE 2	SE 7
23	12.2	10.9	11.0	11.4	7.0	14.9	5.8	8.4	15.6	3.4	62	29	60	50	3.8	12.1	3.7	6.5	2 ⊙	2 ⊙	0	NE 2	SE 4	C 0
24	11.2	10.8	12.3	11.4	6.0	13.3	5.4	7.5	13.7	-0.5	62	47	79	63	3.7	8.2	1.9	4.6	0 ⊙	4 ⊙	3	C 0	ENE 4	C 0
25	13.8	13.9	15.0	14.2	0.6	10.6	5.9	5.8	11.1	-0.2	96	65	77	79	0.3	4.5	2.2	2.3	10 ▬	3 ⊙	10	C 0	NE 3	NE 3
26	13.1	11.9	12.3	12.4	5.1	13.9	8.8	9.2	14.6	1.1	79	54	91	75	1.9	7.4	1.0	3.4	6	8	9	C 0	ENE 2	C 0
27	12.6	12.7	14.9	13.4	8.7	13.2	8.5	9.7	14.2	6.0	83	51	87	74	1.8	7.4	1.4	3.5	9	9	10	C 0	NE 2	C 0
28	15.1	14.7	14.4	14.7	5.4	12.1	6.9	7.8	12.1	1.9	88	52	83	74	1.1	6.8	1.6	3.2	9	9	8	C 0	ENE 1	E 2
29	14.4	15.0	14.9	14.8	6.3	10.9	7.1	7.8	13.9	3.2	83	58	67	69	1.6	5.3	3.4	3.4	7	8	4	C 0	SE 6	SE 1
30	12.7	11.3	10.8	11.6	6.2	13.2	7.1	8.4	14.6	0.7	74	50	88	71	2.5	7.6	1.2	5.8	10	10	10	ESE 1	E 4	C 0
31																								
M	16.7	16.4	16.8	16.6	5.7	13.3	7.4	8.4	14.2	2.3	75	45	75	65	2.7	8.9	2.7	4.8	5.9	6.0	5.1	1.1	3.7	1.3

Zakopane — $H_s = 844$ m — $H_b = 838{,}2$ m — $h_w = 17{,}7$ m — Marzec – Mars 1961

DNI	WI. DZIAŁ-NOŚĆ v	OPAD R	GRUB ŚNIE-GU h	USŁO-NECZ-NIENIE	P O G O D A
1	8	0.5	6	–	✳⁰ 0⁰⁰–6³⁰ ✳⁰ 8¹⁰–⁴² ▽⁰·¹ 8⁵⁷–9¹⁸, 17¹¹–³³, 18⁰⁵–²⁸ ✳⁰ np., = na
2	8	0.0	5	–	▽⁰ 10³² 13¹³
3	8	2.4	3	–	✳⁰ 19⁴⁸ 23¹⁰–24
4	5	3.8	2	–	✳⁰·¹ 0¹⁵–2⁴² 3⁰⁶–11⁵⁰ ●⁰–12²⁰ ●⁰–15¹⁰, 17⁰⁷–18⁴⁷, = p, 18⁵⁰–21⁵⁰
5	9	.	3	–	⊕⁰ 10¹⁵ 16¹⁰
6	8	.	2	–	— 3²⁰–7⁴⁰
7	9	.	pł.	–	⌴⁰ 1⁰⁰–8⁰⁰ 20⁰⁰–24
8	9	.	pł.	–	⌴⁰ 0⁰⁰–8⁰⁰
9	9	.	pł.	–	
10	9	.	pł.	–	⌒⁰ 0⁰⁰–8⁰⁰ ⌴⁰ 22⁰⁰–24
11	8	.	pł.	–	⌴⁰ 0⁰⁰–8⁰⁰
12	8	2.8	.	–	●⁰ 23⁴⁵ 24
13	9	6.7	.	–	●⁰ 0⁰⁰ 1²⁰, 3³⁰ 4¹⁵ ●⁰·¹–8¹⁰ △⁰ 21¹⁰, » na
14	6	11.2	.	–	△⁰ 0²⁰–1¹⁵ ✳ 8⁵⁸–13²⁰ ●⁰–15²⁵ ●¹–16⁰⁸ ●⁰–24, = a, p
15	7	1.5	.	–	●⁰ 0⁰⁰–⁴⁵ 3⁵⁰–11²⁰
16	8	0.0	.	–	●⁰ 5¹⁴–6²⁰ ▽⁰ 20¹⁰–21⁰⁵
17	9	.	.	–	
18	9	3.5	.	–	⌴⁰ 3⁰⁰–8⁰⁰
19	8	7.5	.	–	▽⁰ ●⁰ ✳⁰ 4⁵² 10⁵⁰ ✳⁰ 18⁵⁵–19¹⁰ ✳¹ ▽¹ 21²⁵–24, = na – a, ⌴⁰ p – np
20	9	0.0	9	–	▽¹ 0⁰⁰–10 △¹ ▽¹ 1¹⁵ ✳⁰·¹ 4³⁰ 5⁴⁵ ▽⁰ 9³⁰
21	6	3.6	5	–	▽⁰ 2⁵⁵–4¹⁵ 6⁴⁵–7¹⁵ ✳⁰ 12³⁰–13⁵⁵ ▽¹ 18⁴²–19¹⁴
22	5	4.8	10	–	✳⁰·¹ 1¹⁰–4⁵⁰ 5⁰⁵–6¹² ▽⁰·¹ 7¹⁸–⁴⁰, 8¹⁰–20¹⁵ ⌅¹ 12²⁰–13⁰⁷
23	6	1.8	18	–	✳⁰ 4⁵¹ 7¹⁵–10¹⁵ 12⁴⁸–13¹² △⁰ 17⁵⁰–18²⁰ ✳⁰–21¹⁵ ●⁰–21³⁵
24	7	0.8	7	–	●⁰ ✳⁰ 0²⁰–3³⁰ ⌅⁰ 6¹⁵–7⁰⁷ ●⁰ ✳⁰–8⁵⁰ ●⁰–9²⁰, 15⁰⁵ ³⁰ ●⁰ 16⁴² 19¹⁵
25	7	3.1	4	–	●⁰ 0⁴⁰–5²⁰ ⌅⁰ 6³⁰–³⁵ ✳⁰–6⁵⁰ ●⁰–8⁴⁰ ▽⁰·¹ 14²⁵–15¹¹, 15²³–16¹⁷ ●⁰ 18⁴³ 20³⁵
26	8	0.0	pł.	–	» 23⁴²–24, ▽⁰ 20¹⁵–22²⁰
27	7	6.2	.	–	●⁰ 5⁵⁵ 7¹⁰, 9¹⁵ 10⁰² ●⁰ ✳–11²⁰ ✳⁰–12²² 13³⁰ ✳⁰ 16⁰⁵–17³⁰, » na
28	5	4.0	10	–	▽⁰·¹ ✳⁰·¹ 0⁰⁰ 24, ✳ ⅄¹ 9³⁵–10⁴⁴, 12²⁰–⁵⁰
29	8	0.3	15	–	✳⁰ 0⁰⁰–4⁴⁵, 5²⁰ 7³⁰–8⁴⁰ ▽⁰ 13⁵⁰–15⁴⁸, 16³⁵–17⁴⁵
30	8	0.1	10	–	✳⁰ 1⁰⁰ 18
31	7	5.2	pł.	–	▽⁰·²·¹ 4³⁵ 13¹⁷ ✳¹ 13²⁴ ✳² 13³⁵ ▽⁰–15²⁰ ●⁰ 17³⁵ 18²⁵, 19³⁵–21⁴⁰ ▽⁺⁰ 22²⁰–23¹⁶
Σ	–	69.8	–	–	UWAGI.

Kwiecień – Avril

1	9	1.1	.	–	●⁰ 16⁴⁵–17⁰⁷ ●⁰ 20¹⁵ 22²⁵ 23¹⁸–24
2	8	3.5	.	–	●⁰ 0⁰⁰ 6²⁵ ✳¹ 6⁴⁵ ▽⁰·¹–8¹⁰ ✳¹–8³⁵ ▽⁰–8⁴⁵, 9²²–⁴⁰, = 6¹⁵–8³⁵
3	8	0.2	.	–	▽⁰ 0⁴² 2¹⁴ 8⁰³–²⁵, 11³⁰ 14³⁸ ●⁰ 19²⁵·⁴⁰ ▽⁰–21¹⁵
4	9	0.1	.	–	●⁰ 10⁰⁶–²³ ▽ 18
5	9	.	.	–	
6	9	.	.	–	⌒⁰·¹ 1⁰⁰–7⁰⁰
7	9	0.0	.	–	
8	9	10.1	.	–	●⁰ 5⁵⁰–6⁰⁰ ▽⁰·² 17⁴²–20²⁰ ●⁰ 23⁰⁶ 24, (↘)⁰ 17⁴⁰–18³⁰ NW–SE, = np
9	9	.	.	–	●⁰ 0⁰⁰ ¹² ●¹·⁰–2¹⁵, = 0⁰⁰–6¹⁰
10	9	.	.	–	⌴⁰·¹ 0⁰⁰–7⁰⁰
11	8	0.0	.	–	●⁰ 14⁵⁰–15²⁵ 17¹⁰–³⁰
12	9	.	.	–	⌒² 0⁰⁰–8⁰⁰ ⌴⁰ 23⁰⁰–24
13	8	.	.	–	⌴⁰ 0⁰⁰–6⁰⁰ ⌒⁰·¹ np
14	9	.	.	–	⌒¹·² 0⁰⁰–7⁰⁰
15	9	0.2	.	–	●⁰ 19³⁵–20¹⁵ 21²⁵–24 » 11¹⁰–14³⁰, ⌒⁰ 3⁰⁰–7⁰⁰
16	9	2.2	.	–	●⁰ 0⁰⁰–1¹⁵ ▽⁰·¹ 6³⁰ 19¹⁵
17	9	.	.	–	⌒⁰·¹ 20⁰⁰–24
18	8	0.9	.	–	●⁰ 15⁰⁵ 20³⁵ ⌒¹·² 0⁰⁰–7⁰⁰
19	7	5.8	.	–	●⁰ 8⁰⁵–10¹⁰ ●⁰ 14³⁵–15¹⁵ ●⁰·¹ 17⁵⁰ 23⁴⁵, = na – a
20	9	.	.	–	⌒¹ 22⁰⁰–24
21	9	.	.	–	⌴⁰ 0⁰⁰–7⁰⁰ ⌒⁰·¹ 20⁰⁰–24
22	9	.	.	–	⌒¹ na ⌴¹ na
23	9	.	.	–	
24	9	.	.	–	⌴⁰ na, np
25	8	.	.	–	≡¹ 3³⁵–7⁴⁰ — 7⁵⁵ ⌴⁰ na
26	9	4.8	.	–	▽⁰·² 15⁴⁵ 19³⁵, ⌒⁰ na
27	8	0.8	.	–	▽⁰·¹ 19¹⁰–⁴⁸
28	8	0.0	.	–	▽⁰ 8²³–⁴³ 13⁰⁵–¹³, 14¹³–³³, ⌒¹ na – 9⁰⁰
29	8	0.0	.	–	●⁰ 13⁰⁸–¹⁶
30	9	0.8	.	–	●⁰ 14⁴⁵–17⁴⁰ 18²⁰ 19²⁰, ⌒¹ na ⌴¹ – na, ▽⁰ 20²⁵–21³⁵
31					
Σ	–	30.5	–	–	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Maj – Mai 1961

Dni	CIŚNIENIE P = 900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	11.7	14.7	16.2	14.2	6.8	5.9	6.4	6.4	7.2	5.4	91	94	88	91	0.9	0.6	1.2	0.9	10	10 =	10	C 0	E 1	S 2
2	16.9	17.5	17.5	17.3	5.6	9.9	4.3	6.0	11.7	4.0	90	64	88	81	0.9	4.4	1.0	2.1	10	10	0	C 0	ENE 1	C 0
3	16.7	16.7	18.4	17.3	9.2	12.6	8.0	9.4	15.0	1.2	72	60	91	74	3.2	5.8	0.9	3.3	7 ⊙	9	7	SE 2	C 0	C 0
4	20.4	21.8	22.4	21.5	7.1	8.9	5.3	6.6	12.3	5.1	88	87	87	87	1.2	1.4	1.2	1.3	9	9	1	E 1	SE 1	SW 1
5	23.2	22.8	22.6	22.9	7.9	16.3	9.9	11.0	17.3	1.2	67	46	79	64	3.7	10.0	2.6	5.4	1 ⊙	9	3	C 0	ENE 2	C 0
6	21.2	20.9	21.7	21.3	10.5	20.1	11.8	13.6	20.5	4.3	77	45	92	71	2.9	15.1	1.0	5.7	10	8 ⊙	10	C 0	ENE 3	NNW 1
7	21.4	20.4	18.2	20.0	10.0	14.9	11.9	12.2	16.6	9.1	96	68	62	75	0.5	5.3	5.1	3.6	10 •	7 ⊙	4	C 0	WSW 2	SSW 3
8	20.3	17.9	18.2	18.8	6.8	10.5	5.4	7.0	12.3	4.9	62	47	67	59	3.8	6.6	3.0	4.5	8	6	4	SW 4	W 6	WNW 2
9	16.0	15.3	15.1	14.1	5.2	8.8	2.8	4.9	9.2	2.2	67	47	90	68	2.9	6.0	0.7	3.2	9	7	10	WSW 4	WNW 6	WSW 1
10	13.9	16.1	17.2	15.7	4.0	4.8	3.0	3.7	5.8	2.3	88	85	89	87	1.0	1.3	0.8	1.0	10 •	10 •	10	W 2	SW 3	SW 1
11	17.5	17.9	19.6	18.3	2.9	3.4	3.2	3.2	6.3	1.9	87	86	89	87	0.9	1.1	0.8	0.9	10	9 •	10 •	C 0	NW 2	C 0
12	20.3	20.4	19.5	20.1	0.8	2.2	1.0	1.2	3.8	0.8	87	76	90	84	0.9	1.7	0.7	1.1	10 *	10	8	NNE 2	NNW 2	C 0
13	19.9	18.8	19.1	19.3	3.0	8.8	3.0	4.4	10.0	-1.4	70	47	73	65	2.3	6.0	2.0	3.4	2 ⊙	8	1	SW 1	NNE 1	C 0
14	17.1	15.7	17.2	16.7	6.1	10.0	4.0	6.0	12.6	0.9	73	63	86	74	2.6	4.6	1.1	2.8	9	9 ⊙	10 • R	NE 3	SW 4	NW 5
15	16.1	17.4	18.0	17.2	4.1	7.1	5.2	5.4	9.2	-0.7	78	58	85	74	1.8	4.2	1.3	2.4	7	9	10	SE 1	NW 3	ESE 1
16	17.5	16.8	17.0	17.1	3.7	9.2	5.0	5.7	9.7	3.0	78	53	79	70	1.8	5.5	1.8	3.0	10	8	7	NE 1	NNE 3	C 0
17	15.7	17.5	19.4	17.5	3.5	3.3	2.5	3.0	6.9	1.1	79	89	93	87	1.6	0.8	0.5	1.0	10 •	10 •	10	C 0	ENE 2	C 0
18	20.1	20.6	20.6	20.4	3.8	6.6	3.8	4.5	6.8	0.2	95	63	84	81	0.4	3.6	1.2	1.7	10	10 •	9	ENE 1	NW 1	C 0
19	18.8	18.9	18.4	18.7	8.0	9.9	5.9	7.4	11.0	2.0	69	60	81	70	3.3	4.9	1.8	3.3	3 ⊙	9	9	C 0	NNE 2	C 0
20	15.6	13.2	12.5	13.8	7.2	12.5	6.6	8.2	13.9	1.9	70	50	77	66	3.1	7.3	2.2	4.2	2 ⊙	9	6	C 0	E 1	WSW 2
21	11.1	11.5	12.6	11.7	7.6	9.9	8.1	8.4	12.1	3.3	81	79	96	85	1.9	2.6	0.5	1.7	9	10 •	10 •	NE 1	ENE 5	C 0
22	13.8	14.1	15.8	14.6	7.3	9.6	6.8	7.6	12.2	6.2	95	76	92	87	0.7	2.9	0.8	1.5	10	9	9	E 1	C 0	C 0
23	16.8	17.2	18.4	17.5	6.7	12.7	6.8	8.2	13.7	3.2	69	42	76	62	3.0	8.5	2.4	4.6	6	3	4	NE 2	NE 3	E 1
24	19.3	19.9	21.0	20.1	8.0	13.2	8.4	9.5	14.0	4.4	72	46	79	66	3.0	8.1	2.3	4.5	10	6	9	C 0	E 2	C 0
25	20.3	19.0	18.2	19.2	10.4	15.4	10.5	11.7	16.6	4.2	69	45	82	65	3.9	9.6	2.3	5.3	8	7	4	C 0	NE 3	C 0
26	17.8	17.3	16.8	17.3	10.7	17.1	12.0	13.0	18.5	5.5	77	44	73	65	3.0	11.0	3.9	6.0	9 ⊙	8 ⊙	10	C 0	ESE 2	C 0
27	16.1	15.5	14.9	15.5	12.8	17.3	13.4	14.2	18.9	6.8	67	48	64	60	4.9	10.2	5.5	6.9	6 ⊙	9 R	10	C 0	SSE 2	ESE 1
28	14.8	14.1	14.9	14.6	12.3	17.4	12.1	13.5	18.2	9.6	80	53	91	75	2.9	9.4	1.3	4.5	9	9	9	C 0	SSE 6	C 0
29	9.7	5.0	4.2	6.3	11.5	17.9	14.1	14.4	20.1	9.8	85	46	69	67	2.1	11.1	5.1	6.1	8	10	10 •	C 0	SSE 3	C 0
30	6.4	7.9	10.5	8.3	9.1	11.7	6.8	8.6	14.3	6.7	92	84	85	87	1.0	2.2	1.5	1.6	10	8 ⊙	10	SSE 2	ENE 2	SE 1
31	11.5	11.7	13.0	12.1	8.6	15.1	9.3	10.6	18.4	2.6	70	50	75	65	3.4	8.6	3.0	5.0	2 ⊙	5 ⊙	1	ENE 2	E 3	WSW 1
M	16.7	16.5	17.0	16.7	7.1	11.1	7.0	8.0	12.7	3.6	79	61	82	74	2.2	5.8	1.9	3.3	7.9	8.4	7.3	1.0	2.5	0.7

Czerwiec – Juin

1	12.5	12.1	12.2	12.3	19.9	20.9	15.6	16.2	21.4	4.2	65	41	57	54	5.2	14.6	7.6	9.1	0 ⊙	4 ⊙	6	E 1	E 1	E 1
2	12.2	13.5	12.7	12.8	17.8	12.6	11.3	13.2	21.3	9.6	47	95	89	76	10.8	1.1	1.6	4.5	1	10 • R	10	C 0	E 2	C 0
3	12.0	12.4	14.2	12.9	11.3	16.0	13.1	13.4	19.1	6.7	89	81	86	85	1.6	3.5	2.2	2.4	9	8	10	C 0	SW 3	SSE 2
4	15.0	15.0	16.6	15.5	13.2	15.3	13.1	13.7	19.2	10.8	87	87	95	90	2.0	2.3	0.7	1.7	9	7 • ⊙	10 •	C 0	NE 2	C 0
5	18.0	18.5	19.6	18.7	12.1	16.9	11.1	12.8	17.6	10.4	95	78	93	89	0.7	4.3	0.9	2.0	10	9	3	C 0	SE 4	C 0
6	18.8	17.7	16.9	17.8	11.9	18.0	12.9	13.9	18.4	7.1	90	65	93	83	1.4	7.1	1.2	3.2	8	9	10	C 0	NE 2	C 0
7	16.8	16.6	15.6	16.3	12.7	17.0	13.1	14.0	17.8	9.4	95	69	89	84	0.7	6.0	1.7	2.8	8	9	9	C 0	E 2	C 0
8	16.7	17.7	18.9	17.8	14.2	15.7	12.6	13.8	19.1	9.2	83	78	94	85	2.8	4.0	1.0	2.6	4 ⊙	10	10	C 0	NE 4	SW 2
9	18.6	19.0	18.5	18.7	14.4	15.6	11.7	13.4	18.3	7.4	79	73	92	81	3.5	4.8	1.0	3.1	1 ⊙	9	6	NE 2	E 2	C 0
10	18.6	19.2	19.1	19.0	14.9	15.3	11.6	13.4	19.9	7.3	78	79	94	84	3.7	3.8	0.9	2.8	4 ⊙	9 (R)	5	C 0	SW 2	C 0
11	18.6	18.9	18.2	18.6	13.3	13.0	12.3	12.7	16.9	8.8	85	93	93	90	2.4	1.2	1.1	1.6	8	10 • R	8	C 0	C 0	C 0
12	17.2	17.8	17.5	17.5	13.7	12.4	10.9	12.0	14.7	10.8	87	95	92	91	2.1	0.7	1.0	1.3	10	10 •	10	C 0	C 0	C 0
13	16.4	14.5	12.7	14.5	12.1	17.6	14.6	14.7	17.7	6.9	76	55	72	68	3.4	9.1	4.6	5.7	1 ⊙	9	10	C 0	E 1	S 1
14	13.2	16.5	18.9	16.2	12.2	12.3	9.8	11.0	15.3	9.7	77	74	80	77	3.3	3.8	2.4	3.2	7	10	7	SW 4	W 7	C 0
15	20.7	21.1	21.6	21.1	8.0	13.9	9.9	10.4	14.7	6.9	84	61	84	76	1.7	6.3	2.0	3.3	10	9	9	SW 3	NNW 5	C 0
16	22.4	22.3	24.3	23.0	9.9	15.9	8.4	10.6	17.8	4.9	72	45	86	68	3.5	9.9	1.5	5.0	2 ⊙	1 ⊙	0	NW 4	N 5	C 0
17	24.9	24.9	26.0	25.3	11.7	17.5	12.2	13.4	19.3	3.5	64	50	80	65	4.8	10.0	2.9	5.9	1 ⊙	6 ⊙	3	C 0	NE 4	C 0
18	25.6	24.5	24.4	24.8	13.8	21.9	15.3	16.6	22.4	5.9	67	47	71	62	5.2	13.9	5.1	8.1	5 ⊙	5 ⊙	0	C 0	WNW 3	SW 1
19	24.6	24.4	26.9	25.3	18.9	24.6	14.8	18.3	25.5	10.7	62	42	96	67	8.1	18.1	0.7	9.0	1 ⊙	1 ⊙	10	SW 1	N 3	C 0
20	28.8	29.4	29.4	29.2	12.0	16.0	12.0	13.0	16.7	11.6	81	49	74	68	2.7	9.4	3.7	5.3	10	5 ⊙	8	NE 1	NE 3	C 0
21	28.1	26.1	27.6	27.3	11.2	19.8	15.1	15.3	21.3	4.3	71	43	72	62	3.9	13.3	4.8	7.3	1 ⊙	3 ⊙	7	C 0	ENE 4	C 0
22	29.0	27.5	24.2	26.9	12.3	21.3	15.4	16.1	22.7	6.2	72	52	73	66	4.1	12.2	4.8	7.0	0 ⊙	5 ⊙	10	C 0	NE 2	NE 1
23	22.2	24.3	26.0	24.2	14.9	19.3	13.2	15.2	20.0	13.0	91	56	81	76	1.5	9.6	2.9	4.7	9	4 ⊙	1	NE 3	WNW 5	C 0
24	26.0	26.3	27.8	26.7	16.4	21.4	13.5	16.2	22.1	9.4	67	47	74	63	6.1	13.7	4.1	8.0	1 ⊙	8 ⊙	1	SW 2	NW 6	SW 2
25	25.9	24.1	23.1	24.4	15.5	25.1	16.5	18.4	26.4	6.1	65	42	57	55	6.2	18.6	8.2	11.0	2	1 ⊙	0	C 0	SW 3	C 0
26	21.9	20.4	20.2	20.8	18.8	26.4	16.3	19.4	27.0	10.0	60	31	85	59	8.7	23.7	2.8	11.7	5 ⊙	8 ⊙	5	C 0	SW 6	C 0
27	17.6	17.8	17.3	17.6	25.9	26.7	19.5	22.4	27.5	15.8	45	38	76	52	17.0	21.9	5.5	14.8	1 ⊙	2 ⊙	9	NE 1	SSE 6	C 0
28	21.4	27.2	31.6	26.7	13.0	10.4	9.6	10.6	22.2	9.5	94	84	85	87	0.9	2.0	2.1	1.7	10 •	10 •	9	SW 3	W 4	C 0
29	33.0	32.7	32.2	32.6	10.8	14.7	10.4	11.6	17.1	4.9	66	53	84	68	4.4	7.9	2.0	4.8	7 ⊙	9	8	C 0	N 3	ESE 1
30	32.2	31.2	31.0	31.5	13.5	18.6	12.3	14.2	20.2	7.6	71	53	85	69	4.5	9.9	2.4	5.6	2 ⊙	1 ⊙	0	NE 1	ENE 3	C 0
31																								
M	21.0	21.1	21.5	21.2	13.7	17.7	12.9	14.3	20.0	8.2	75	62	83	73	4.2	8.9	2.8	5.3	4.9	6.7	6.5	0.9	3.2	0.4

Zakopane — $H_s = 844\,m$ — $H_b = 838{,}2\,m$ — $h_w = 17{,}7\,m$ — Maj – Mai 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	3	0.5	•	–	●°146 3³⁵ ●°10¹⁰ 12³⁵ 15⁵⁵ 17⁵⁰. 21³⁵–22¹⁰. = 7¹⁵–9³⁰ ≡°–13⁴⁰ = –24
2	8	.	•	–	= 0⁰⁰–4³⁰ ⌒⁰ 20⁰⁰–24
3	7	2.1	•	–	●▽⁰⁻¹ 9⁴⁸. 19⁰⁴. ↖° 10¹⁷–⁴⁵ S–SE. 19⁰⁸–⁴⁵ SW–SE. ⌒¹ na. ⌒° na
4	8	4.3	•	–	●▽° 1⁴⁶–2⁰⁴ ●▽⁰⁻¹ 4¹⁴⁵–5²² 5³¹ ●▽⁰⁻² 9¹⁵ 12³⁵ ▲¹ 9¹⁷⁻²⁰
5	8	.	•	–	⌒¹ 1⁰⁰–3⁰⁰ ⌒° –5⁰⁰
6	8	24.3	•	–	●▽⁰⁻¹ 18¹³–20²⁰ 21¹⁵–24. ⌒¹ na–8³⁰
7	8	8.5	•	–	●▽⁰⁻² 0⁰⁰ 1²⁸. ●¹⁻⁰ 9³³ ●▽⁰⁻¹ 22⁴⁰ 24
8	9	2.2	•	–	●▽¹⁻⁰ 0⁰⁰–44 ●▽° 11⁴¹–45 ●▽⁰⁻² 13¹⁰–⁵⁸ ●▽° 14⁴⁵ 15⁰⁵ △ 14⁵² 15⁰⁰. (↖)° 16²⁵–45
9	9	13.0	•	–	●▽° 6⁵⁶ 7⁰² 9²⁵–³³ ✱° 9³⁸ ●▽° 14⁰⁹ ●▽⁰⁻² 15¹⁰–⁴⁰. 19¹⁸–20³⁵. 21³⁰–22⁴⁵. ↖° 16¹³–¹⁷ W–NW
10	7	6.8	•	–	●▽° 2³⁰ 3¹⁵ ●▽⁰⁻¹ 4³⁵–5³⁵ 6⁴⁰–7⁴⁰ ●▽⁰⁻¹ 8³⁰–22³³
11	7	10.5	•	–	●▽° 1³⁵–3⁴⁵ 8⁵⁸ 11⁴⁸ ▲² 12¹⁶–²⁸ ●▽° 21³⁷ ✱¹⁻⁰ 22⁴³ ●▽° –22⁴⁸
12	7	0.2	•	–	●▽° 0⁴⁰ 1⁰⁷ ▲¹ 1¹³ ●¹⁻⁰ 2⁰⁵ 3¹⁸ 5³⁵ ✱⁰⁻¹ –10²⁵ ●▽° 14⁵⁰ 15¹⁵. 16¹⁵⁻²⁰
13	9	.	•	–	⌒° na
14	8	8.6	•	–	●▽° 11³³–12²⁸ 15²⁶ 20¹⁹ ●▽² 21⁰² ●▽² 21¹⁶ ●▽¹⁻⁰ –21²⁵. ↖¹ 20³⁰–21⁰⁷ E–SW
15	8	0.3	•	–	●▽° 10⁵² 16⁴⁸
16	9	0.5	•	–	●▽¹ 10⁵⁰–⁵³ ▲ ●▽° –10⁵⁶ ●▽° 16²⁷
17	6	23.1	•	–	●▽° 5⁴⁶ 8¹⁵ ●▽⁰⁻¹ 11²⁵ 14⁵⁰ 15⁵⁰ 16¹⁰ ●▽⁰⁻² 16²⁰–18³⁰ ●▽⁰⁻¹ 19¹⁵–20⁴⁰ ●▽° 21²³–22¹⁰ ✱–22²² ✱°–22³⁰ ●¹–23⁴⁰
18	8	0.2	•	–	●▽° 0¹⁸ 7¹⁸ ●▽° 12¹³ 17²⁸. = 5³⁰–7³⁰
19	8	.	•	–	●▽° 3¹⁵ 25
20	9	.	•	–	⌒² 4⁰⁰–8⁰⁰ ⌒¹ 22⁰⁰–24
21	8	5.5	•	–	●▽⁰⁻¹ 12¹⁰–15²⁰ ●▽° 15⁴⁰–16⁰³ ●▽⁰⁻¹ 16³² 24
22	8	12.3	•	–	●▽° 0⁰⁰–6⁴⁸ ●▽⁰⁻¹ 11⁴⁷. 19³¹. ↖° 13¹⁰–⁵⁵ SE–SW ↖¹ 14¹⁰⁻²¹ (↖)°–14⁴⁸ E–N. = 4³⁰–8³⁰
23	9	.	•	–	= 0²⁰–3¹⁵ ⌒° 20⁰⁰–24
24	9	.	•	–	⌒° 0⁰⁰–9⁰⁰. 21⁰⁰–24
25	7	.	•	–	⌒⁰⁻¹ na
26	7	.	•	–	= na. ⌒² na–9⁰⁰ ⌒¹ 21⁰⁰–24
27	7	0.0	•	–	●▽° 12⁵¹–13¹² 15³⁵–⁵¹ ●° 22³²–⁴⁵. (↖)° 12⁴⁰–⁵¹ ↖°–13¹⁴ (↖)°–13³⁰ W–NE. ⌒² na–a
28	9	0.1	•	–	●▽° 15⁴⁵–16¹⁵ 18⁵⁵–19⁰⁵. = 21¹⁵–24
29	7	10.2	•	–	●▽⁰⁻² 14⁰⁰–15³³ ●▽¹ 21²⁵–22¹⁰ ●¹⁻⁰–24. = 0⁰⁰–7¹⁵
30	7	2.0	•	–	●° 0⁰⁰⁻¹⁵ ●°2⁴⁰–3²⁰ ●°–3⁴⁵ ●▽⁰⁻¹ 12⁰² 17¹⁵. = 6²⁰–12⁴⁵. 21³⁰–24
31	8	.	•	–	= 0⁰⁰–2⁴⁵. ⌒¹ 5⁰⁰–7⁰⁰ ⌒° 21⁰⁰–24
Σ	—	135.2	—	–	UWAGI

Czerwiec – Juin

1	9	.	•	–	⌒¹⁻² 0⁰⁰–6⁰⁰ ⌒° np
2	6	37.6	•	–	●▽⁰⁻² 13¹³–16¹⁵. ↖²⊥° 13¹⁴–15⁰³ SE–SW. ⌒⁰⁻¹ 0⁰⁰–9⁰⁰
3	8	0.3	•	–	●▽° 11¹³ 13³⁹. 19⁴⁶–20¹⁴ ●° ●° 22¹⁸–23⁵⁰. (↖)° 12⁰⁷–⁴⁵ NW
4	8	12.2	•	–	●▽⁰⁻² 12⁵² 13⁰² ●▽° 21⁰²–⁴⁴. ↖⁰⁻¹ p S–W
5	7	0.7	•	–	●▽° 13¹⁸–19⁰⁵ = 4⁴⁰–10³⁰
6	9	5.5	•	–	●▽⁰⁻² 11⁴⁵–12⁰² 15¹²–⁵⁰ 17⁵⁸–19⁴⁵ ●▽° 20⁴⁵–22³⁰. ↖¹ 15¹²–³⁰ S–SW. ⌒° 0⁰⁰–8⁰⁰
7	8	3.8	•	–	●▽⁰⁻¹ 5⁵⁰–7¹⁵. 10⁵⁷–12⁴⁴ ●▽° 15⁰¹–¹⁰ ●⁰⁻¹ 16²⁰ 19⁰⁸. ↖° 11²⁵–12⁴⁵ SW–S. = 3³³–5³⁰. ⌒° 18⁵²–19¹⁰
8	8	0.6	•	–	●▽° 5²⁵–³⁵. 12⁴⁸–13¹⁵. 18⁴⁸ 23⁰⁵. (↖)° 12¹⁵–12⁴⁵
9	9	.	•	–	(↖)° 11⁴⁵–13²⁰. ⌒² p–np
10	8	0.3	•	–	●▽° 12²⁰–13⁰⁶. (↖)° 11³⁰–12³⁰ ↖°–13³⁰ (↖)°–14⁴⁵ SE–SW. ⌒² na ⌒¹ np
11	6	10.1	•	–	●▽⁰⁻² 11⁰¹ 14³⁰. ●°–15³⁰. ↖⁰⁻² 12³⁰–15³⁰. ⌒¹ 0⁰⁰–8⁴⁰
12	6	16.4	•	–	●▽° 2³⁵ 4⁵² 9⁰¹–²². ●° 10⁰²–²⁰ ●°–10⁵³. ●° 11⁰⁵–12¹⁰ ●▽²⁻⁰ 15²⁰ ●▽° 17¹⁰–⁵⁰. 22⁴²–⁴⁸. ↖¹ 12¹¹–²⁰ SE–SW. = 1⁵–16³⁰. 21³⁰–22³⁰
13	9	15.3	•	–	●▽° 0³⁵–⁵⁰. 20⁵⁷–21¹⁰ 23⁴⁰–24
14	8	1.4	•	–	●▽⁰⁻² 0⁰⁰–2²⁰ ●▽ 12¹⁵–³⁸. 13⁵⁰–14⁰⁰
15	7	.	•	–	●⁰⁻¹ 2⁴² 6⁴⁰
16	8	.	•	–	⌒° na ⌒¹ 22⁰⁰–24
17	8	.	•	–	⌒¹ 0⁰⁰–9⁰⁰ ⌒° 22⁰⁰–24
18	8	.	•	–	⌒⁰⁻¹ 0⁰⁰–9⁰⁰
19	8	0.0	•	–	●° 18⁵³ 19¹⁵. = 18¹⁵–24. ⌒° na–9⁰⁰
20	8	.	•	–	= na. ⌒° np
21	8	.	•	–	⌒⁰⁻¹ 0⁰⁰–9⁰⁰
22	7	12.4	•	–	⌒° na–9⁰⁰
23	8	0.0	•	–	●▽⁰⁻¹ 2¹⁵–5³⁰ ●▽° 10⁵⁵–11³⁰. (↖)° 1⁵⁵–2⁰³ W ↖¹ 3¹⁷–4³⁰ S–SW. ⌒¹ 22⁰⁰–24
24	8	.	•	–	⌒⁺² 0⁰⁰–6⁰⁰
25	9	.	•	–	⌒⁰⁻¹ 0⁰⁰–9⁰⁰ ⌒¹ 21⁰⁰–24
26	9	.	•	–	⌒² 2⁰⁰–9⁰⁰ ⌒¹ 23⁰⁰–24. ⌒¹ 21¹⁰–22¹⁵
27	8	16.5	•	–	(↖)° 18³⁰–19²⁰ SE. ⌒¹ 0⁰⁰–9⁰⁰
28	7	4.9	•	–	●▽⁰⁻² 1³². 15⁴⁹. (↖) 2¹⁵ ↖ 21⁷–²²
29	9	.	•	–	⌒² 0⁰⁰–9⁰⁰ ⌒° 21⁰⁰–24
30	9	.	•	–	⌒⁰⁻¹ 0⁰⁰–9⁰⁰. 21⁰⁰–24
31					
Σ	—	138.0	—	–	UWAGI

Zakopane — φ = 49°18' — λ = 19°57' — Lipiec - Juillet 1961

DNI	CIŚNIENIE P−900				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	30.4	29.9	29.4	29.9	15.3	22.5	15.7	17.5	25.6	7.1	70	49	78	66	5.3	14.0	4.0	7.8	0 ⊙	2 ⊙	1	E 1	ENE 3	C 0
2	29.1	28.6	28.1	28.6	15.8	23.8	15.1	17.4	24.5	8.1	70	40	80	63	5.3	17.7	5.6	8.9	0 ⊙	3 ⊙	0	C 0	ENE 2	C 0
3	27.6	25.9	24.3	25.9	17.4	25.9	17.0	19.5	27.0	8.9	66	55	72	58	6.8	21.4	5.4	11.2	0 ⊙	1 ⊙	2	C 0	NE 4	E 1
4	21.5	18.4	16.7	18.9	20.1	25.5	17.0	19.9	27.1	11.7	61	45	81	62	9.1	17.9	3.8	10.3	0 ⊙	5 ⊙	10	ENE 1	WNW 4	C 0
5	19.3	20.0	21.5	20.3	15.0	12.9	8.9	10.9	17.8	8.9	69	77	83	76	4.6	3.5	1.9	3.3	8 ⊙	10 •	6	WNW 3	NE 1	C 0
6	21.9	23.5	26.2	23.9	10.4	15.1	7.6	9.7	14.3	3.4	64	71	84	73	4.6	4.3	1.6	3.5	7	6 ⊙	3	NE 4	WSW 5	C 0
7	25.9	25.0	26.1	26.0	10.0	15.9	11.1	11.5	14.3	2.5	65	51	75	64	4.3	7.9	3.3	5.2	3 ⊙	9	9	ENE 1	N 3	C 0
8	25.3	24.6	23.0	24.3	10.7	15.2	10.0	11.5	16.2	6.0	72	55	83	70	3.6	7.9	2.1	4.5	2 ⊙	7	8	C 0	NE 1	C 0
9	18.9	16.5	18.9	18.1	12.5	17.2	10.6	12.7	18.5	6.7	73	51	82	69	4.0	9.7	2.3	5.3	2 ⊙	10	10 •	C 0	WSW 3	ESE 1
10	19.3	18.7	20.2	19.4	10.9	16.2	10.2	11.9	17.7	8.4	75	54	92	74	3.3	8.5	1.0	4.3	9	9	10 •	WSW 3	WNW 5	WNW 4
11	21.9	21.7	21.7	21.8	10.3	17.5	12.3	13.1	19.0	5.6	68	75	81	75	4.0	4.8	2.8	3.9	3 ⊙	8	1	NE 3	WNW 5	C 0
12	18.2	17.5	16.1	17.3	13.4	22.7	17.3	17.8	25.9	6.8	78	41	77	65	3.4	16.4	4.5	8.1	8	5 ⊙	3	C 0	NE 2	C 0
13	11.4	9.5	8.1	9.7	19.5	22.2	15.4	17.1	25.0	11.0	57	52	94	68	9.8	13.0	0.9	7.9	3 ⊙	3 ⊙	8	SSE 5	SSE 7	C 0
14	14.0	15.8	18.0	15.9	11.9	14.0	8.2	10.6	15.8	7.9	78	54	76	69	3.0	7.4	2.6	4.3	9	7 ⊙	1	SW 2	SW 6	C 0
15	18.4	19.2	19.1	18.9	15.1	19.5	16.5	16.4	21.0	6.7	64	50	70	61	5.4	11.4	5.7	7.5	7	8	9	NE 2	NNE 2	ENE 2
16	14.5	17.0	17.1	16.2	17.1	17.8	11.8	14.6	19.6	11.7	59	59	82	67	8.0	8.2	2.5	6.2	4 ⊙	5	8	NNW 5	W 5	SW 1
17	15.6	14.7	15.9	15.4	13.3	17.0	10.6	12.9	18.2	10.1	80	56	72	69	3.1	8.6	3.6	5.1	1 ⊙	8	2	C 0	WNW 3	C 0
18	15.4	15.0	15.2	15.2	11.1	15.2	11.7	12.4	17.0	5.5	67	58	83	69	4.4	7.4	2.4	4.7	7	9	9	WNW 4	WNW 3	C 0
19	15.6	15.1	16.4	15.7	10.4	15.2	10.3	11.6	17.2	8.2	91	59	94	81	1.2	7.2	0.8	3.1	9	9	9	C 0	NW 1	SW 1
20	16.7	17.4	18.5	17.5	9.3	11.9	9.9	10.2	12.4	6.1	95	91	93	93	0.6	1.2	0.9	0.9	10	10 •	9	C 0	SE 1	C 0
21	19.7	20.5	20.1	20.1	11.6	15.7	11.5	12.1	16.7	7.2	82	74	77	78	2.5	4.1	3.2	3.3	5	8	9	SE 2	SW 2	SE 2
22	19.3	19.2	20.4	19.6	11.0	15.7	11.0	12.2	17.4	9.5	82	60	91	78	2.3	7.1	1.2	3.5	9	9	9 •	W 2	WNW 3	C 0
23	20.6	21.1	23.0	21.6	10.2	14.7	13.0	12.7	16.7	5.3	91	78	82	84	1.1	3.7	2.7	2.5	1 ⊙	9	10	C 0	NE 1	SE 2
24	25.3	25.9	28.3	26.5	9.9	13.3	10.8	11.2	14.6	9.6	93	70	80	81	0.9	4.6	2.7	2.7	10 ⚲	10	10 •	C 0	NE 1	C 0
25	29.2	29.5	29.0	29.2	9.5	11.7	10.0	10.3	12.1	8.6	75	67	79	74	3.0	4.5	2.6	3.4	10	10	10	C 0	ENE 1	C 0
26	27.6	25.7	22.8	25.4	9.5	17.2	11.2	12.2	19.2	4.7	75	46	85	68	3.0	10.6	2.4	5.3	8	3 ⊙	1	C 0	NE 2	SE 2
27	19.8	18.0	17.4	18.4	15.0	24.2	18.5	19.0	25.2	6.9	76	36	54	55	4.0	19.5	9.7	11.1	1 ○	7 ⊙	8	C 0	NNW 4	ESE 1
28	15.2	14.2	12.4	14.0	16.1	25.8	16.5	18.2	25.1	8.2	77	41	88	69	4.3	17.3	2.5	8.0	8	7	9 •	C 0	SW 2	S 2
29	13.1	18.8	20.6	17.5	13.3	10.1	8.3	10.0	20.8	8.1	98	91	99	96	0.4	1.2	0.2	0.6	10 •	10 •	10 •	C 0	NE 2	C 0
30	18.6	20.7	20.8	20.0	7.9	7.4	7.2	7.4	8.7	6.9	99	93	96	96	0.1	0.8	0.5	0.5	10 •	10 •	10 •	C 0	NE 3	NNE 1
31	19.8	21.9	24.6	22.1	8.1	13.0	8.8	9.7	14.4	6.9	94	69	93	85	0.6	4.6	0.8	2.0	9	9	6	SE 2	NW 6	C 0
M	20.3	20.3	20.6	20.4	12.5	16.9	12.0	13.4	18.7	7.5	76	60	82	73	3.7	8.9	2.7	5.3	5.6	7.3	6.8	1.5	3.0	0.6

Sierpień - Août

1	24.2	23.7	24.3	24.1	11.6	18.5	9.7	12.4	19.3	6.7	71	46	88	68	4.0	11.5	1.5	5.7	8	4 ⊙	0	NW 2	NW 4	C 0
2	23.1	21.7	21.5	22.1	12.0	21.4	13.4	15.0	22.4	4.9	75	52	89	72	3.5	12.4	1.7	5.9	1 ⊙	4 ○	3	C 0	NE 2	C 0
3	21.7	22.0	25.7	23.1	14.6	18.5	11.5	14.0	19.6	10.1	82	70	94	82	3.0	6.5	0.9	3.5	10	10 •	10 •	ESE 1	ESE 2	C 0
4	25.8	25.0	25.0	25.3	10.7	14.3	11.9	12.2	16.4	10.0	87	71	85	81	1.7	4.8	2.0	2.8	9	9	7	C 0	NE 1	SW 1
5	24.3	24.5	23.9	24.2	13.8	19.4	13.3	15.0	20.7	11.4	76	60	87	74	3.8	8.8	2.0	4.9	10	8 ⊙	0	SW 1	SW 3	C 0
6	22.9	21.9	21.4	22.1	15.4	25.6	16.1	18.3	26.5	8.1	79	51	82	71	3.8	15.9	3.3	7.7	0 ⊙	1 ⊙	0	C 0	E 2	ESE 1
7	19.4	19.7	22.3	20.5	17.4	26.9	19.5	20.8	26.9	10.4	72	37	80	63	5.7	22.3	4.4	10.8	4 ⊙	2 ⊙	9	E 1	ESE 3	C 0
8	22.9	22.2	23.9	23.0	16.5	25.3	17.1	18.3	24.1	15.9	86	67	90	81	2.8	9.5	2.1	4.8	8	8	0	NE 3	NE 3	ESE 1
9	25.5	25.9	26.4	25.9	19.1	26.7	19.3	21.1	27.5	14.1	70	51	88	70	6.8	17.2	2.7	8.9	2 ⊙	6 ⊙	10 (⚲)	SE 3	NE 2	E 1
10	25.6	24.5	22.6	24.2	17.4	28.5	22.2	22.6	28.7	13.7	93	44	62	66	1.6	21.8	10.1	11.2	2 ⊙	3 ⊙	0	C 0	SSE 3	S 3
11	21.5	19.4	23.2	21.4	23.8	29.9	18.5	22.7	30.0	15.8	51	31	81	54	14.3	29.3	4.0	15.9	0 ⊙	3 ⊙	0	W 3	SW 6	ESE 2
12	22.2	20.3	20.6	21.0	14.7	20.8	13.3	15.5	21.9	12.4	94	68	93	85	0.9	7.7	1.2	3.3	9	9	10 ⚲	C 0	SSE 1	ESE 2
13	21.1	24.4	26.4	24.0	10.3	9.2	8.5	9.1	13.3	7.7	97	95	95	95	0.3	0.6	0.8	0.6	10 ⚲	10 •	10	C 0	NW 2	SW 1
14	25.8	25.1	25.9	24.9	6.4	13.4	10.5	10.2	14.8	5.4	92	66	89	82	0.8	5.1	1.4	2.4	0 ⊙	6 ⊙	6	C 0	SE 1	C 0
15	21.7	19.8	19.2	20.2	10.9	16.8	11.2	12.5	18.6	4.9	75	56	80	70	3.3	8.4	2.7	4.8	1 ⊙	8 ⊙	9	C 0	NW 6	C 0
16	17.5	17.0	17.3	17.3	9.9	13.3	8.9	10.2	15.1	6.5	84	69	76	76	2.0	4.8	2.8	3.2	10	9	9	ENE 1	NW 5	W 5
17	14.5	12.9	13.1	13.5	6.4	12.6	9.3	9.4	15.1	3.8	82	59	85	75	1.8	6.0	1.8	3.2	9	9	9	SW 1	C 0	C 0
18	14.2	15.7	17.2	15.7	7.7	9.3	8.3	8.4	11.7	7.2	91	84	88	88	0.9	1.9	1.3	1.4	10 •	10 •	10 •	C 0	SW 4	SSE 2
19	16.1	15.3	15.3	15.6	9.5	14.2	13.9	13.9	15.9	5.9	75	59	51	62	3.0	6.6	8.9	6.2	8	9	10	SW 2	SW 3	SW 7
20	15.1	17.0	20.6	17.6	11.6	10.9	9.3	10.3	15.9	9.2	77	79	82	79	3.1	2.8	2.1	2.7	10	10	3	W 1	WNW 3	C 0
21	21.9	22.3	22.1	22.1	11.0	15.8	8.4	10.9	16.3	8.1	72	56	91	73	3.8	8.0	0.9	4.2	9	7 ⊙	1	W 2	W 6	SE 1
22	19.9	17.8	16.9	18.2	9.6	19.2	15.1	14.8	21.7	4.7	87	46	68	67	1.7	12.1	5.4	6.4	3	8	10 • ⚲	C 0	SW 3	WNW 7
23	17.2	18.3	21.4	19.0	10.1	11.3	8.1	9.4	15.0	7.2	83	79	87	83	2.2	2.9	1.4	2.2	7	9	10 • ⚲	W 3	WSW 3	SW 6
24	22.6	23.2	24.0	23.3	7.5	10.9	9.5	9.4	12.0	6.7	91	64	88	81	1.0	4.5	1.5	2.5	9 •	9	10	SW 3	SW 4	C 0
25	23.9	24.3	25.7	24.6	10.1	15.9	11.4	11.7	16.6	9.1	86	62	89	79	1.9	6.1	1.6	3.2	10	9	8	WSW 1	W 4	SSW 2
26	26.6	27.6	28.6	27.6	12.5	17.2	10.9	12.9	18.1	7.8	81	58	87	75	2.8	8.4	1.7	4.3	8	8 ⊙	4	NNE 2	W 5	C 0
27	29.2	29.2	30.3	29.6	14.3	21.0	14.2	15.9	21.6	9.1	76	54	81	70	4.0	11.4	3.1	6.2	3 ⊙	8 ⊙	6	SE 1	WSW 3	SE 1
28	30.3	30.7	31.6	30.9	13.3	22.0	15.1	16.4	22.1	10.3	91	62	85	79	1.5	9.9	3.1	4.8	2 ⊙	5 ⊙	10	C 0	NE 2	C 0
29	30.7	29.9	28.7	29.8	10.0	19.9	11.3	13.1	20.2	6.9	78	46	81	68	2.8	12.3	2.5	5.9	0 ⊙	8 ⊙	3	C 0	W 1	C 0
30	28.3	29.0	30.2	29.2	9.9	17.3	8.9	11.3	18.2	6.4	92	49	93	78	1.0	10.1	0.8	4.0	3 ⊙	4 ⊙	0	C 0	NE 4	C 0
31	31.1	32.6	34.2	32.6	7.8	17.3	8.7	10.7	18.4	4.1	91	51	91	78	1.0	9.7	0.9	3.9	0 ⊙	1 ⊙	0	C 0	E 4	C 0
M	22.8	22.7	23.5	23.0	12.1	18.1	12.6	13.8	19.4	8.5	82	59	84	75	2.9	9.7	2.6	5.1	5.6	6.9	5.7	1.0	3.0	1.3

Zakopane — $H_s = 844\ m$ — $H_b = 838{,}2\ m$ — $h_w = 17{,}7\ m$ — Lipiec - Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰
2	9	.	.	–	⌒ 1 na – 9⁰⁰; 23⁰⁰–24
3	9	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰ ⌒ 0 np.
4	8	6.5	.	–	●▽ 0 16³⁸–⁵² ●▽ 0-2 18⁰⁰–¹⁷ ●▽ 0-1 22⁰⁰–23²¹ (K) 0 17⁵⁵ K 0 18⁰⁰–¹⁷ (K) 0 18²⁰ W-NE (K) 0 21⁴⁵–22¹⁰ K 1 –22³⁸ (K) 1 –23⁰⁰ W-NE, 23³⁰–³⁰ S-SE; ≫ 22⁰⁰–¹⁴
5	8	0.7	.	–	●▽ 0 11⁴⁰–14⁴⁵, 16¹⁸–²²; ⌒ 1 0⁰⁰–24
6	9	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰, 21⁰⁰–24
7	8	0.0	.	–	● 0 22⁴³–23²⁵; ⌒ 2 0⁰⁰–9⁰⁰
8	8	.	.	–	⌒ 1 23⁰⁰–24
9	8	0.7	.	–	●▽ 0 14⁵⁰–15⁰⁵ ● 0 15¹³ 17¹⁸ 18³⁸…⁴⁵ 21²⁶…⁴⁵; = na; ⌒ 1 0⁰⁰–9⁰⁰
10	8	5.8	.	–	●▽ 0 13⁵³–14⁰⁷ 17⁰⁵–²⁰ ●▽ 1 –18⁰² ● 0 –18³³ ●▽ 0-2 21³⁴–22¹⁰; K 0 17¹⁹–⁴⁵ NW-SE
11	8	.	.	–	⌒ 0 22⁰⁰–24
12	9	.	.	–	⌒ 0-2 0⁰⁰–9⁰⁰
13	9	11.4	.	–	●▽ 0-2 17⁵⁸–19¹² 19³⁵–20⁰³; (K) 0 17⁴⁶–⁵⁶ K 0-1 –18²⁰ (K) 0 –18³⁵ W-E K 0 18⁵⁰–19¹⁵, ≫ 7³⁰ 17¹⁵ ≪ 18⁰⁸–²⁰
14	9	0.0	.	–	●▽ 0 5⁴⁹–6¹¹ ● 0 10²⁵…⁴⁵; ⌒ 0-1 20⁰⁰–24
15	9	7.2	.	–	⌒ 1 0⁰⁰–7⁰⁰
16	9	1.1	.	–	●▽ 0-2 3⁰⁵–4⁴⁵, 5⁰⁸–⁵³; K 1-2 3³⁰–4⁰⁰ (K) 1 –4³⁰ SW-NE, ≫ – ≪ 2⁴⁰–5⁵⁰
17	9	0.0	.	–	● 0-1 1⁰⁵–2⁴⁵; ●▽ 0 12³⁵–⁴⁶; ⌒ 1 23⁰⁰–24
18	8	.	.	–	⌒ 0 22⁰⁰–24
19	8	7.7	.	–	●▽ 0-2 10⁵⁵–18⁴⁴ (K) 0 6¹⁵–²⁰ NE K 0 11⁰⁵–⁴⁵ W-SE 14⁵¹–15⁴⁵ SW-SE, = 4³⁰–6³⁰, 19³⁰–21¹⁵; ⌒ 1 0⁰⁰–9⁰⁰
20	6	17.1	.	–	● 0 0⁰²–11⁰⁵ ● 0-2 13¹⁸–19¹⁸ ● 0 20¹⁵…³⁵; = 12³⁰–13⁴⁰
21	8	0.7	.	–	●▽ 0 11⁰¹–⁰³ 12¹⁹–²⁰, 17³⁶–⁴⁷ ●▽ 1 23⁰⁹–¹⁵ ●▽ 0 23¹⁷–³¹; = 1³⁰–4³⁰
22	8	2.4	.	–	●▽ 0-1 0⁰²–⁵⁷ ●▽ 0-2 21²¹–22⁰³
23	8	3.3	.	–	●▽ 0 13²⁰–⁴⁵ ●▽ 0-2 16¹⁵–17¹⁰, = 22³⁰–24
24	8	0.0	.	–	● 0 0²⁵…⁴⁰ ● 0 1³⁰…8⁰⁵ ● 0 21³⁰…⁴⁵; = 0⁰⁰–8⁴⁵
25	7	.	.	–	
26	8	.	.	–	⌒ 1 23⁰⁰–24
27	9	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰
28	8	15.3	.	–	● 0 20⁴⁸–21¹⁰ ●▽ 0-1 21²⁷–⁴⁵ ●▽ 0-2 22⁴⁵–⁵³
29	7	49.0	.	–	●▽ 2-0 3⁴⁹–4⁴⁵ ● 0-1 6¹⁰–24
30	7	39.4	.	–	● 0-2 0⁰⁰–24
31	9	0.9	.	–	● 0-1 0⁰⁰–6²⁸ ●▽ 0 14⁴⁵–⁵² ●▽ 0-1 17⁴⁷–19²⁵
Σ	–	169.2	–	–	UWAGI.

Sierpień – Août

1	9	.	.	–	⌒ 1 21⁰⁰–24
2	9	.	.	–	= 3³⁰–4³⁰, ⌒ 2 0⁰⁰–9⁰⁰ ⌒ 0-1 20⁰⁰–24
3	6	16.5	.	–	●▽ 0-2 11³⁵–22⁵³, K 2 14⁰⁵–¹⁵, ⌒ 1 0⁰⁰–8⁰⁰, ⊕ 0 7¹⁰–8²⁰
4	7	.	.	–	●▽ 0 0³⁸–2⁰⁵
5	9	.	.	–	⌒ 1 22⁰⁰–24
6	9	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰ ⌒ 0-1 20⁰⁰–24
7	8	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰
8	8	.	.	–	
9	9	0.1	.	–	●▽ 0 21¹⁸–³⁵, (K) 0 21³⁵–22³⁰ W, ⌒ 2 n–a
10	7	.	.	–	K 2 1²⁵–3¹⁵; = 1⁵⁰–4³⁰
11	9	1.5	.	–	≫ 0¹⁰–1³⁰ 10⁴⁵ 12²⁰ ⌒ 0-1 20⁰⁰–24
12	8	21.2	.	–	●▽ 3 7¹⁰–²⁵ ●▽ 2-0 7²⁰ 10¹⁰ ●▽ 0 15⁴²–16⁰⁵ 19⁰⁰ 20⁰⁵ ● 0 21¹⁵–22²⁷ ●▽ 0-2 22²⁷–23⁵³, K 0 15⁵⁸–16⁴⁵ W-SE (K) 2 23¹⁵–⁴⁵ SE-S
13	6	22.8	.	–	●▽ 0-2 0¹³–2⁰⁰, 2²⁰–7³⁰ ●● 1 –9⁰¹ ● 0-2 –16⁴², K 1 0⁰⁸–1³⁰ SW, = 4⁴⁵–11³⁰
14	8	.	.	–	
15	9	.	.	–	⌒ 2 2⁰⁰–10⁰⁰ ⌒ 0 22⁰⁰–24
16	8	0.0	.	–	●▽ 0 8⁰⁵…¹⁷ 9³⁸–11²⁵, 12⁴⁸–13¹⁵ ⌒ 0 0⁰⁰–10⁰⁰
17	8	2.7	.	–	●▽ 0 15²⁵–16⁵² 20³³–⁴⁵ ⌒ 1 0⁰⁰–9⁰⁰
18	6	10.8	.	–	●▽ 0-2 0¹⁹–2¹⁰ ● 0 6³⁵, 7¹⁵–10³⁹, 13³⁵ 19⁵⁷ ●▽ 1-0 19⁵⁷, 22⁴⁵, K 0 0²⁰–1³⁰ SW-SE, = 10³⁰–22¹⁵
19	8	0.6	.	–	●▽ 1-0 22⁴³–23⁰⁵
20	7	1.2	.	–	●▽ 0 2⁴⁵–3²⁵ ● 0 8²³…10⁰⁸ ●▽ 0-1 13⁰⁵–14³³, 16⁰⁸–²³
21	9	.	.	–	⌒ 1 21⁰⁰–24
22	9	6.8	.	–	●▽ 0-2 21⁴⁰–23²⁰ ●▽ 0 23⁴⁰–24, K 1-0 21⁴⁰–23¹⁰ ⌒ 0-2 0⁰⁰–10⁰⁰
23	8	16.7	.	–	●▽ 0 0⁰⁰–⁰⁵ ●▽ 0-2 8²⁵–23⁰⁵ ▲ 0 17⁵⁷–⁵⁸, K 0 15¹¹–⁴⁵ K 1 17⁴⁸–19³⁰ NE-NW, 21³⁴–22⁰⁰
24	8	0.1	.	–	●▽ 1 0¹⁹–⁴⁰ ●▽ 1-0 7⁰⁹–⁴⁵ 16⁴⁸ 17⁰⁵ = 21¹⁵–24
25	8	0.1	.	–	● 0 5⁴⁵ 6⁰⁷ ●▽ 0 21¹⁸–²⁵; = 0⁰⁰–7¹⁵
26	8	.	.	–	⌒ 1 na – 1 ⌒ 1-2 np.
27	9	.	.	–	⌒ 2 0⁰⁰–8⁰⁰ ⌒ 0 20⁰⁰–24
28	8	.	.	–	⌒ 0-2 0⁰⁰–10⁰⁰
29	9	.	.	–	⌒ 0-2 0⁰⁰–7⁰⁰ ⌒ 0 21⁰⁰–24; ⊕ 0 13²⁰–³⁰
30	9	.	.	–	⌒ 0-1 0⁰⁰–9⁰⁰ ⌒ 1 20⁰⁰–24
31	9	.	.	–	⌒ 1-2 0⁰⁰–9⁰⁰ ⌒ 2 p–n
Σ	–	101.1	–	–	UWAGI.

Zakopane — φ = 49°18' — λ = 19°57' — Wrzesień – Septembre 1961

DNI	CIŚNIENIE P − 900 + I	II	III	Dies	TEMPERATURA T I	II	III	Dies	Max	Min	WILGOTNOŚĆ WZGL. U I	II	III	Dies	NIEDOSYT WILGOTNOŚCI Δ I	II	III	Dies	ZACHMURZENIE i POGODA N,w I	II	III	KIERUNEK i PRĘDKOŚĆ WIATRU D,v I	II	III
1	34.4	33.7	32.6	33.6	9.0	21.6	11.7	15.5	22.5	5.9	93	48	94	78	0.8	13.5	0.9	5.0	0 ⊙	1 ⊙	0	C 0	NE 2	C 0
2	30.7	29.5	27.5	29.2	11.5	23.5	10.9	14.2	23.7	8.0	90	49	86	75	1.4	14.7	1.8	6.0	0 ⊙	4 ⊙	0	C 0	WSW 3	C 0
3	24.5	25.0	21.5	23.0	10.5	23.3	11.7	14.3	24.0	6.5	85	28	75	62	2.0	20.5	3.6	8.7	0 ⊙	2 ⊙	0	C 0	SE 3	C 0
4	20.8	21.1	22.1	21.3	10.8	20.5	12.5	14.1	22.2	6.4	81	51	87	73	2.5	12.0	2.0	5.5	10	7 ⊙	0	C 0	WSW 3	SE 1
5	21.1	20.2	17.7	19.7	10.9	25.2	17.8	17.4	24.2	8.8	87	45	59	63	1.7	15.9	8.2	8.6	1 ⊙	5 ⊙	2	C 0	E 3	ESE 2
6	15.0	15.4	16.1	15.5	18.8	22.4	12.5	16.6	22.4	12.4	51	48	94	64	10.8	14.2	0.9	8.6	4 ⊙	6 ⊙	3	SSW 6	S 7	C 0
7	15.2	15.2	17.3	15.9	11.4	19.6	13.3	14.4	21.3	9.8	98	53	75	75	0.4	10.7	3.9	5.0	9	9	10	C 0	C 0	WSW 1
8	17.5	18.2	19.6	18.4	8.4	13.0	10.2	10.4	14.0	8.0	71	44	71	62	3.2	8.4	3.6	5.1	5	4 ⊙	8	SW 1	NW 6	WNW 4
9	20.3	21.8	22.3	21.5	8.9	10.1	9.4	9.4	12.7	7.8	85	89	89	87	1.9	1.4	1.3	1.5	10	10	10	NE 1	N 1	NE 1
10	22.1	23.3	23.8	23.1	7.6	7.9	6.9	7.3	9.3	6.7	90	87	92	90	1.1	1.3	0.7	1.0	10	10 ●	10	SE 1	NNE 2	C 0
11	23.4	23.2	22.3	23.0	6.9	9.6	4.0	6.1	10.1	3.8	91	79	93	88	0.9	2.7	0.5	1.4	10	10	10	C 0	NE 1	C 0
12	21.5	21.1	21.4	21.3	3.1	17.5	10.9	10.6	17.7	0.4	97	48	74	73	0.2	10.5	3.4	4.7	0	8	10	C 0	NNE 2	ESE 1
13	21.8	22.7	22.9	22.5	9.4	15.7	7.7	10.1	16.8	6.7	74	51	91	72	3.1	8.8	0.9	4.3	10	7	2	SE 1	WSW 4	C 0
14	21.2	21.3	20.4	21.0	6.6	21.0	19.8	16.8	22.5	4.8	95	47	53	64	0.7	13.3	11.0	8.3	8 ⊙	9 ⊙	9	C 0	SW 6	SW 6
15	22.9	23.5	23.1	23.3	12.8	15.3	8.2	11.1	20.1	8.0	77	48	88	71	3.5	9.0	1.3	4.6	9	1 ⊙	0	SW 5	WNW 5	W 1
16	29.0	28.6	28.7	28.8	7.5	21.0	11.4	12.8	22.3	4.7	80	57	85	74	2.1	10.8	2.1	5.0	6	2 ⊙	0	SE 2	NE 1	C 0
17	29.3	29.3	29.6	29.5	8.7	25.5	12.0	14.6	25.9	5.7	83	37	80	67	1.8	20.5	2.9	8.4	0 ⊙	0 ⊙	0	C 0	ENE 2	C 0
18	28.9	28.2	28.7	28.6	10.4	25.0	11.4	14.6	26.6	6.4	75	43	71	63	3.2	18.1	4.0	8.4	2 ⊙	6 ⊙	0	C 0	C 0	SE 1
19	27.0	26.8	25.8	26.5	11.0	19.8	15.1	15.2	22.6	8.5	80	70	89	80	2.6	6.9	2.0	3.8	0 ⊙	5	8	C 0	NE 2	C 0
20	25.7	25.8	26.1	25.9	5.8	16.9	6.5	8.8	17.5	3.5	94	42	89	75	0.6	11.1	1.0	4.2	0 ⊙	0 ⊙	0	C 0	NE 3	C 0
21	26.2	26.5	28.7	27.1	4.0	15.9	4.9	7.4	16.4	0.9	92	48	91	77	0.6	9.6	0.8	3.7	0 ⊙	0 ⊙	0	C 0	NE 3	C 0
22	29.3	29.7	30.7	29.9	1.6	17.8	3.8	6.8	18.2	-1.0	92	26	86	68	0.6	15.1	1.1	5.6	0 ⊙	0 ⊙	0	C 0	NE 2	C 0
23	29.8	29.2	28.9	29.3	1.4	17.9	5.9	7.8	18.2	-1.4	80	38	80	66	1.5	12.6	1.9	5.3	0 ⊙	3 ⊙	0	C 0	ENE 1	C 0
24	28.2	27.7	28.0	28.0	3.6	17.4	6.8	8.6	18.4	1.8	91	55	81	69	0.7	12.9	1.9	5.2	0 ⊙	0 ⊙	0	C 0	C 0	C 0
25	27.7	27.4	28.6	27.9	4.5	19.6	9.2	10.6	19.7	1.9	85	36	64	62	1.2	14.8	4.2	6.7	0 ⊙	1 ⊙	5	C 0	NNW 2	C 0
26	27.9	27.1	25.8	26.9	9.8	18.8	11.7	13.0	19.9	6.2	89	55	95	80	1.3	9.8	0.6	3.9	10	7 ⊙	9	C 0	NE 1	C 0
27	25.6	22.1	23.6	23.1	8.7	16.3	11.9	12.2	17.7	8.1	96	68	91	85	0.4	5.9	1.2	2.5	6	6 ⊙	10	C 0	WNW 1	C 0
28	24.1	24.1	25.5	24.6	5.7	18.0	6.4	9.1	18.8	5.3	95	53	89	79	0.5	9.5	1.0	3.7	10	1 ⊙	0	C 0	NE 1	C 0
29	25.3	25.0	25.2	25.2	6.8	20.1	13.6	13.5	20.8	4.8	94	59	85	79	0.6	9.6	2.4	4.2	2 ⊙	4 ⊙	7	C 0	NNE 1	C 0
30	24.7	22.9	21.6	23.1	11.2	17.7	12.6	13.5	17.8	10.4	95	75	88	85	0.9	4.8	1.8	2.5	9	10	4	NE 1	C 0	C 0
31																								
M	24.6	24.5	24.7	24.6	8.2	18.4	10.3	11.8	19.5	5.6	86	52	85	74	1.8	10.9	2.4	5.0	4.4	4.6	3.6	0.5	2.3	0.6

Październik – Octobre

1	20.4	21.1	24.2	21.9	11.3	15.0	5.8	9.5	15.2	4.3	95	46	80	74	0.7	9.1	1.9	3.9	10	3 ⊙	0	C 0	ENE 3	NW 3
2	25.7	26.2	28.3	26.7	5.0	13.6	4.2	6.8	14.8	0.8	88	52	92	77	1.0	7.4	0.6	3.0	8	1 ⊙	0	C 0	NE 4	E 1
3	28.4	27.8	28.4	28.2	1.8	16.8	4.5	6.9	17.2	-0.2	95	43	86	74	0.6	13.0	1.1	4.2	1 ⊙	1 ⊙	0	C 0	W 2	NE 1
4	28.5	27.7	28.3	28.1	1.4	16.1	5.6	7.2	16.8	0.2	92	41	76	70	0.6	10.9	2.1	4.5	1 ⊙	4 ⊙	4	C 0	NE 2	NW 1
5	28.3	28.4	29.3	28.7	4.2	15.7	6.7	8.3	16.2	2.7	88	53	86	76	0.9	8.4	1.3	3.5	7 ⊙	3 ⊙	1	C 0	NE 2	C 0
6	28.4	26.3	25.5	26.1	3.4	15.5	12.8	11.1	16.9	2.2	95	53	52	66	0.5	8.3	7.1	5.3	3 ⊙	3 ⊙	0	C 0	NE 2	SSE 5
7	18.3	17.1	16.0	17.2	11.3	14.6	13.7	13.3	15.5	6.0	46	40	46	44	7.2	10.0	8.4	8.5	4 ⊙	7	6	NE 2	SSE 6	SW 4
8	14.7	15.0	18.8	16.2	12.3	18.4	8.6	12.0	19.1	8.3	61	40	81	61	5.7	12.6	2.2	6.8	8 ⊙	7 ⊙	0	SE 2	SW 3	NE 1
9	26.2	28.8	32.0	29.0	3.3	12.3	3.9	9.4	13.4	4.2	92	74	88	85	0.7	3.8	1.3	2.0	9	10	10	C 0	E 2	ESE 1
10	33.3	33.4	32.9	33.3	1.3	13.9	3.0	5.4	14.8	0.8	94	56	95	81	0.4	7.0	0.6	2.7	3 ⊙	2 ⊙	0	SE 1	E 2	C 0
11	31.1	30.6	30.6	30.8	2.2	17.0	5.4	7.3	17.3	1.3	96	49	92	79	0.3	9.9	0.7	3.6	0 ⊙	0 ⊙	0	C 0	E 2	C 0
12	29.9	29.2	29.7	29.6	3.3	14.2	10.9	9.8	15.1	2.1	95	64	84	81	0.4	5.8	2.1	2.8	0 ⊙	9	10	C 0	ENE 1	C 0
13	29.2	29.6	30.3	29.8	7.6	7.1	5.4	6.4	10.9	5.1	91	93	92	92	0.9	0.8	0.8	0.8	10	10 ●	10	NE 1	NE 1	C 0
14	29.3	28.8	28.4	28.9	5.6	6.8	4.4	4.8	7.4	2.9	89	63	90	81	0.8	3.3	0.9	1.7	9	9	10 ●	C 0	E 1	C 0
15	28.1	27.8	26.6	27.5	5.6	9.2	6.9	7.2	9.7	4.1	95	82	86	88	0.4	2.0	1.3	1.2	10	10	10	C 0	NW 2	NW 2
16	25.0	23.2	22.3	23.6	-0.7	16.0	3.8	5.7	16.4	-0.9	98	43	83	75	0.1	10.3	1.4	3.9	10 ≈	1 ⊙	1	C 0	NNE 3	C 0
17	20.1	16.2	9.3	15.3	2.1	14.9	12.6	10.6	16.1	0.9	88	45	52	62	0.8	9.2	7.1	5.7	8	7 ⊙	10	C 0	WSW 3	WNW 6
18	1.1	0.0	0.7	0.6	10.6	12.3	12.9	12.2	13.2	8.7	69	54	58	60	4.1	6.6	6.2	5.6	9	9 ●	9	SSE 7	S 7	SSW 6
19	3.4	3.9	9.0	6.1	13.9	16.0	16.3	15.7	17.3	12.2	64	36	50	57	5.8	8.0	9.3	7.7	10 ●	9	8	WSW 4	SE 3	S 4
20	11.6	12.6	12.8	12.3	14.4	16.8	13.6	14.6	18.2	11.1	57	46	67	57	7.0	10.4	5.2	7.3	9	9	9	S 2	E 2	SE 1
21	13.2	18.8	22.6	18.2	10.9	10.3	3.8	7.2	13.6	3.6	45	47	74	55	7.1	6.6	2.0	5.2	7	3 ⊙	3	SSE 4	SSW 8	NE 1
22	24.3	25.0	25.8	25.0	0.3	9.8	3.6	4.4	10.4	-0.9	90	59	91	80	0.6	5.0	0.7	2.1	10	9	4	C 0	E 1	C 0
23	27.4	27.7	28.8	28.0	5.1	10.0	4.6	6.1	10.7	2.2	95	77	91	88	0.4	2.9	0.7	1.3	10	8	2	C 0	NE 3	S 1
24	29.4	29.3	28.5	29.1	1.0	12.4	2.5	4.6	12.6	0.0	92	54	91	79	0.5	6.5	0.6	2.5	8	7	0	C 0	ENE 2	C 0
25	26.0	25.3	25.1	25.5	-1.6	12.7	4.2	4.9	15.3	-1.9	95	52	89	78	0.3	7.1	0.8	2.7	1	6 ⊙	9	C 0	SW 1	C 0
26	22.5	22.3	22.0	22.3	1.0	9.8	2.6	4.0	11.1	0.2	90	63	93	82	0.7	4.6	0.6	2.0	8	9	8	ESE 1	NE 1	C 0
27	18.5	18.7	18.1	18.4	2.1	14.4	6.2	7.2	15.0	0.3	88	46	74	69	0.8	8.9	2.5	4.1	9	9	3	ESE 1	NE 1	SW 1
28	17.9	18.0	17.3	17.8	5.2	16.3	5.6	8.2	16.4	3.8	84	53	92	76	1.4	8.8	0.8	3.7	4	0 ⊙	0	NE 3	NE 1	C 0
29	17.0	16.2	18.6	17.3	4.7	12.3	7.3	8.0	13.2	2.4	92	70	92	85	0.7	4.3	0.8	1.9	9	10 ●	7	E 1	N 2	C 0
30	20.0	19.4	19.3	19.6	2.8	7.7	6.8	6.0	8.3	2.2	91	81	92	88	0.7	2.0	0.8	1.2	9	10	10 ●	C 0	E 1	C 0
31	22.2	24.0	26.1	24.1	4.7	9.3	4.1	5.6	9.6	2.3	92	61	73	75	0.7	4.6	2.2	2.5	10	3 ⊙	2	C 0	W 3	C 0
M	22.6	22.7	23.1	22.8	5.1	13.1	7.0	8.0	14.1	2.9	85	57	80	74	1.7	7.0	2.4	3.7	6.9	6.1	4.7	0.9	2.6	1.3

Zakopane $H_s = 844\ m$ $H_b = 838{,}2\ m$ $h_w = 17{,}7\ m$ **Wrzesień - Septembre 1961**

DNI	WIDZIALNOŚĆ v	OPAD R	GŁĘBOKOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	-	$^{2}0^{00}$ a $^{1}21^{00}$ 24
2	9	.	.	-	(K) $^{0}16^{50}$ 17^{40} S-NW. $^{1-2}0^{00}$ 6^{00} $^{0-1}21^{00}$ 24
3	9	.	.	-	$^{1-2}0^{00}$ a
4	8	0.0	.	-	$^{0}8^{30}$ 55 . $^{0-2}0^{00}$ a $^{1}21^{00}$ 24
5	7	.	.	-	^{2} n a $^{1}21^{00}$ 24
6	9	6.1	.	-	$^{0-2}16^{37}$ 17^{48} $^{4}15$. $^{0}0^{00}$ 100
7	9	3.3	.	-	$^{0}140$ 215 $^{0}20^{30}$ 50 $^{0-1}22^{30}$ 24 . $^{2}5^{50}$ 6^{45}
8	9	0.8	.	-	$^{0-1}0^{00}$ 135 $^{0}23^{10}$ 30
9	7	3.8	.	-	$^{0}115$ 237 $^{0}4^{05}$ 40 720 32 $^{0}745$ 8^{05} ^{0} 1735 , $^{0}2^{102}$ 11
10	7	0.9	.	-	$^{0-1}3^{17}$ 6^{18} $^{0}11^{58}$ 12^{45} $^{0}13^{20}$ 14^{15} 17^{10} 18^{30} ^{1} 18^{40} $^{0}22^{20}$ 23^{30} . = 4^{30} 5^{45}
11	8	.	.	-	$^{1-2}20^{00}$ 24
12	9	.	.	-	= 21^{30} 22^{30} $^{2}0^{00}$ 4^{00} ^{3} 7^{00}
13	9	.	.	-	$^{0}200$ 9^{00} $^{1}7^{10}$ 30
14	9	1.9	.	-	$^{0}2^{155}$ 22^{15} $^{1}23^{13}$ 25 ^{0} 23^{42} . ^{0} na
15	9	.	.	-	$^{0}145$. 50 320 28
16	9	.	.	-	^{0} p np
17	9	.	.	-	^{1} na 1 $^{1-2}20^{00}$ 24
18	9	.	.	-	$^{2}0^{00}$ a $^{0-1}20^{00}$ 24
19	8	.	.	-	= 19^{30} 24 . $^{1-2}0^{00}$ 0^{00}
20	9	.	.	-	= 0^{00} 30 . ^{2} na 10^{00} $^{0-1}19^{00}$ 24
21	9	.	.	-	$^{1-2}0^{00}$ 4^{00} ^{1} 7^{00} $^{0-1}19^{00}$ 24
22	9	.	.	-	$^{1}0^{00}$ 100 $^{0-2}$ 900
23	9	.	.	-	$^{1}0^{00}$ 100 $^{0-2}$ 100 8^{00} $^{0-1}19^{00}$ 24
24	9	.	.	-	$^{1-2}0^{00}$ 10^{00} $^{0-2}19^{00}$ 24
25	8	0.0	.	-	$^{2}0^{00}$ 4^{00} $^{1-0}$ 4^{00} 8^{00}
26	8	7.4	.	-	$^{0}5^{50}$ 6^{40} $^{0-2}18^{01}$ 24 (K) $^{0}18^{23}$ 20^{30} W-E. = 7^{00} 8^{15}
27	7	.	.	-	$^{0}0^{08}$ 55 . = 18^{40} 22^{30} 23^{30} 24 . ^{0} 22^{00} 24
28	6	0.0	.	-	$^{0}8^{03}$ 50 = na a $^{0}8^{03}$ 35 = a p . $^{0-2}0^{00}$ 8^{00}
29	8	0.0	.	-	$^{0}19^{08}$ 17 (K) $^{0}22^{25}$ 28^{30} E. = 20^{40} 24 . $^{1-2}0^{00}$ 10^{00}
30	7	0.0	.	-	$^{0}12^{50}$ 13^{25} . 18^{08} 19^{15} . = 0^{00} 1^{30}
31					
Σ	—	24.2	—	-	UWAGI:

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1	8	.	.	-	= 5^{11} 8^{20}
2	9	.	.	-	$^{0-2}0^{00}$ 8^{00} $^{1-2}19^{00}$ 24
3	9	.	.	-	$^{0-1}0^{00}$ 7^{00} $^{0-1}20^{00}$ 24
4	8	.	.	-	$^{0}0^{00}$ 8^{00}
5	8	.	.	-	$^{0}0^{00}$ 3^{00} ^{0} 5^{00} $^{1}18^{00}$ 24
6	9	.	.	-	$^{1-2}0^{00}$ 4^{00} ^{1} 7^{00}
7	9	.	.	-	
8	9	.	.	-	$^{0}23^{00}$ 24 . $^{0}17^{00}$ 16^{00}
9	8	0.0	.	-	$^{0}17^{50}$ 18^{10} = 18^{30} 23^{20} $^{0}0^{00}$ 8^{00} 23^{30} 24
10	8	.	.	-	= 0^{45} 3^{45} = ^{0} 4^{45} . $^{0}0^{00}$ 5^{00} ^{0} 8^{00} $^{1}19^{00}$ 24
11	8	.	.	-	$^{0-2}0^{00}$ 7^{00} $^{0}19^{00}$ 24
12	8	1.7	.	-	= 18^{25} 24 . $^{1}1^{00}$ 10^{00}
13	6	5.1	.	-	$^{0}0^{40}$ 107 ^{0} 137 $^{0}2^{06}$ 5^{35} 6^{25} 9^{40} ^{0} 13^{40} 14^{40} . = 0^{00} 103
14	8	6.4	.	-	$^{0}17^{38}$ 18^{45} $^{0}20^{10}$ 45 ^{0} 24 = 3^{30} 5^{15}
15	9	1.0	.	-	$^{0}0^{00}$ 6^{35} 7^{04} 15 ^{0} 8^{35} 9^{48} 10^{43} . = 7^{40} 8^{30} = ^{0} 23^{45} 24
16	9	.	.	-	= $^{0-2}0^{00}$ 7^{12} $^{0-1}18^{00}$ 22^{00} ^{0} 24
17	8	14.8	.	-	$^{0}22^{25}$ 23^{15} ^{2} 20^{30} 24 . $^{0-1}0^{00}$ 8^{00}
18	7	18.7	.	-	$^{0-1}0^{35}$ 9^{25} 12^{15} 18^{42} $^{2}0^{00}$ 24 . $^{1}9^{48}$ 55
19	8	1.4	.	-	$^{0}0^{30}$ 35 5^{35} 21^{46} ^{2} n . $^{1}9^{15}$ 10^{30} 15^{25} 16^{20}
20	9	2.1	.	-	$^{0}3^{33}$ 4^{17} $^{0-1}20^{02}$ 23^{30}
21	9	.	.	-	$^{0}2^{20}$ 3^{20} $^{0}20^{00}$ 23^{00} ^{0} 24 ^{2} 10^{00} 12^{00}
22	8	0.4	.	-	$^{0}15^{38}$ 17^{45} $^{0-1}0^{00}$ 7^{00} $^{0}6^{38}$ 7^{30}
23	6	.	.	-	$^{0}5^{40}$ 6^{12} $^{0}20^{00}$ 24
24	9	.	.	-	$^{0-1}0^{00}$ 8^{00} $^{0}18^{00}$ 20^{00} $^{0-1}$ 24 . $^{0}12^{30}$ 13^{00}
25	8	.	.	-	< 19^{38} $^{1-2}0^{00}$ 7^{00} $^{0-1}20^{00}$ 24
26	7	.	.	-	$^{1}0^{00}$ 2^{00} ^{0} 8^{00} $^{1}19^{00}$ 20^{00} ^{0} 24
27	9	.	.	-	$^{0-2}0^{00}$ 8^{00} $^{0}19^{00}$ 24
28	9	.	.	-	$^{0}0^{00}$ 10^{00} $^{0-1}18^{00}$ 24
29	8	0.9	.	-	$^{0}12^{40}$ 13^{30} 14^{35} 17^{00} $^{1}0^{00}$ 6^{00}
30	7	16.6	.	-	$^{0-1}17^{40}$ 18^{10} 24 . = 2^{15} 3^{40} 13^{15} 24
31	8	1.8	.	-	$^{0-1}0^{00}$ 8^{40} . = 0^{00} 8^{30} $^{1}18^{00}$ 24
Σ	—	70.9	—	-	UWAGI:

Zakopane — φ = 49°18' — λ = 19°57' — Listopad – Novembre 1961

DNI	CIŚNIENIE P−900 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	26.7	26.5	27.4	26.9	4.6	11.1	6.5	7.2	11.5	2.5	66	57	69	64	2.9	5.8	3.0	3.9	9	6 ⊙	10 •	WSW 5	E 2	WSW 5
2	28.7	26.5	25.0	26.1	5.1	9.0	1.1	4.1	9.8	0.9	85	64	92	80	1.3	4.2	0.5	2.0	8	2 ⊙	0	SE 1	E 1	C 0
3	18.2	16.2	15.8	16.7	-0.1	14.8	1.4	4.4	15.1	-0.5	90	25	78	64	0.7	12.5	1.6	4.9	7	4 ⊙	0	ESE 1	SSW 3	C 0
4	13.4	12.4	12.9	12.9	0.3	0.5	-0.3	0.0	3.0	-0.5	90	94	100	95	0.6	0.3	0.0	0.3	9	10 *	10 *	C 0	C 0	C 0
5	10.5	12.2	16.3	13.0	-2.1	-1.0	-1.3	-1.5	-0.3	-2.3	94	87	92	91	0.3	0.8	0.4	0.5	10 *	10 ₉ *	10	C 0	C 0	C 0
6	14.8	12.9	12.6	13.4	0.3	2.0	1.9	1.6	2.6	-1.7	90	91	96	92	0.6	0.7	0.3	0.5	10	10 ≡	10 •	C 0	C 0	C 0
7	9.8	10.3	11.7	10.6	4.3	8.1	3.4	4.8	9.8	1.6	97	80	95	90	0.3	2.2	0.3	1.0	9 •	6 ⊙	10	SE 2	C 0	C 0
8	12.3	13.3	13.9	13.2	2.2	3.8	2.0	2.5	4.3	2.1	96	95	98	96	0.3	0.4	0.2	0.3	10	10 ₉	10 ₉ ≡	C 0	C 0	C 0
9	12.4	12.6	12.4	12.5	-0.1	5.2	1.2	1.9	6.8	-0.3	98	70	94	87	0.2	2.6	0.4	1.1	10 —	4 ⊙	10	C 0	NE 2	SW 1
10	9.7	10.1	10.7	10.2	9.3	11.4	7.3	8.9	11.6	1.2	61	54	81	65	4.7	6.2	1.9	4.3	9	9 ⊙	10	NE 3	SW 3	NE 1
11	8.8	10.1	11.6	10.2	5.6	7.1	5.4	5.9	7.3	5.1	92	92	94	93	0.8	0.8	0.6	0.7	10	9	10	C 0	NE 2	C 0
12	12.7	13.1	14.3	13.4	1.2	9.0	0.3	2.8	9.4	0.4	96	76	98	90	0.3	2.8	0.1	1.1	4	6 ⊙	10 ≡	C 0	NE 3	SW 1
13	12.3	11.0	10.2	11.2	2.2	11.7	7.6	7.3	11.7	0.2	90	60	94	81	0.7	3.3	0.6	2.3	9	10 •	10 •	NE 3	ESE 4	SSE 2
14	10.6	13.1	17.0	13.6	3.3	8.3	1.1	4.0	8.3	1.0	82	62	96	80	1.6	4.3	0.2	2.0	10	3 ⊙	10 ₉ ≡	SSE 2	WNW 4	C 0
15	17.3	18.8	20.9	19.1	-0.7	-0.3	-1.8	-1.2	1.1	-2.0	98	96	96	97	0.1	0.3	0.3	0.2	10 ≡	10	10	ENE 1	ENE 2	C 0
16	20.7	19.3	17.9	19.3	-2.3	1.0	0.7	0.0	1.6	-2.6	93	89	92	91	0.4	0.8	0.3	0.6	10 ≡	10	10	C 0	ENE 1	NE 1
17	15.9	15.3	16.3	16.0	0.6	2.2	1.4	1.4	2.9	0.6	90	64	83	79	0.7	2.6	1.2	1.3	10	10	10	W 1	SE 2	WNW 3
18	14.8	14.3	15.2	14.8	0.1	-0.1	0.0	0.0	1.4	-0.3	88	92	86	89	0.8	0.3	0.8	0.7	10	10 ⁂	10 * ⁂	WNW 3	NW 3	SSW 3
19	17.6	19.1	24.3	20.3	-1.3	-1.3	-2.8	-2.2	0.1	-3.0	74	84	62	80	1.3	0.9	0.9	1.1	10 ⁂	10 ⁂	10	WSW 2	WSW 4	C 0
20	28.1	31.3	35.2	31.3	-3.1	-3.6	-4.3	-4.4	-1.3	-5.4	90	69	74	78	0.4	1.3	1.1	1.0	10 *	3 ⊙	9	C 0	C 0	NE 1
21	34.9	32.8	30.6	32.8	-11.1	1.0	-3.6	-4.3	1.2	-12.7	83	54	76	71	0.4	3.1	1.1	1.3	2	9 ⊙	2	SW 1	ESE 1	SE 1
22	27.9	25.8	24.7	26.1	-4.6	8.0	-3.3	-0.8	8.2	-3.3	81	42	74	66	0.8	6.3	1.3	2.8	9	6 ⊙	1	C 0	C 0	C 0
23	21.0	19.1	18.3	19.3	-3.4	3.8	-4.3	-2.0	7.4	-6.0	82	44	82	69	0.7	3.1	0.8	2.2	2	1 ⊙	0	C 0	C 0	C 0
24	20.0	20.8	21.6	20.8	-3.7	8.2	-0.3	0.4	8.3	-7.6	84	37	73	65	0.6	6.9	1.6	3.0	9	2	8	C 0	C 0	SSW 1
25	20.1	18.7	18.2	19.0	1.0	3.2	-1.1	0.3	3.3	-1.9	77	80	94	84	1.6	1.3	0.3	1.1	10	10	7	SW 2	C 0	C 0
26	15.8	14.2	11.8	13.9	-0.8	0.2	0.4	0.0	0.9	-1.6	96	98	92	95	0.3	0.1	0.3	0.3	6	10 ≡	6	C 0	ENE 2	SW 1
27	7.1	6.2	8.8	7.4	10.1	13.0	4.2	7.9	13.9	0.3	63	58	93	71	4.6	6.3	0.3	3.8	7	8	6	SSW 4	SSW 3	C 0
28	12.3	13.9	16.7	14.4	3.9	6.4	0.3	3.3	6.9	0.3	83	80	96	86	1.6	1.9	0.2	1.2	9	10	10	C 0	C 0	C 0
29	18.3	19.4	20.1	19.3	1.2	4.8	-0.6	1.2	5.8	-0.7	94	83	87	89	0.4	1.3	0.7	0.8	9	8	3	C 0	E 1	C 0
30	15.9	16.1	13.7	15.2	-3.8	3.3	-1.0	-0.1	3.8	-4.1	89	48	83	74	0.3	4.6	0.9	2.0	1	9 ⊙	0	C 0	WNW 6	ESE 1
31																								
M	17.0	16.9	17.3	17.1	0.3	5.2	0.7	1.8	6.0	-1.4	86	71	88	82	1.0	3.1	0.8	1.6	8.3	7.6	7.4	1.0	1.8	0.7

Grudzień – Décembre

1	7.4	8.6	10.1	8.7	6.9	8.8	8.1	8.0	9.0	-1.4	58	61	64	61	4.1	4.4	3.9	4.1	7	7	7	WSW 7	NW 8	W 6
2	7.7	5.3	7.6	6.9	10.4	13.1	9.1	10.4	14.0	5.3	54	35	55	48	5.7	9.8	5.3	6.9	3	1	1	SW 8	SW 8	NW 6
3	14.8	14.5	13.9	14.4	-1.7	3.1	-2.0	-0.6	9.1	-2.6	89	57	89	78	0.6	3.3	0.6	1.5	2	9	3	C 0	C 0	C 0
4	11.8	15.6	19.2	15.5	9.3	10.9	4.9	7.3	11.5	-2.1	48	37	71	59	6.1	3.3	2.3	4.7	8	7	0	SW 6	W 7	ESE 1
5	19.6	18.0	16.9	18.2	13.7	18.2	5.6	10.8	18.4	2.6	54	34	89	59	7.2	13.7	1.0	7.3	10	5 ⊙	9	WSW 2	SW 4	C 0
6	13.8	13.0	16.0	14.3	5.1	2.2	-3.6	0.0	8.0	-3.6	92	90	90	91	0.7	0.7	0.3	0.6	9	10 •	10 *	C 0	ENE 1	C 0
7	12.0	12.9	16.2	13.7	-3.8	-2.9	-3.2	-3.3	-2.8	-4.2	89	88	93	91	0.3	0.3	0.2	0.4	10 *	10 *	10 ₉	C 0	NE 1	C 0
8	18.1	19.4	21.4	19.6	-4.3	-4.3	-7.0	-5.6	-3.0	-7.6	91	79	80	83	0.4	0.9	0.7	0.7	10 *	9 *	10	W 1	C 0	C 0
9	21.3	20.8	19.8	20.6	-14.2	-3.2	-12.6	-10.6	-1.0	-15.2	83	72	85	80	0.3	1.3	0.4	0.7	3	8 ⊙	0	C 0	C 0	C 0
10	18.3	17.2	17.6	17.7	-13.4	-3.3	-7.7	-8.1	-2.6	-15.3	80	74	81	78	0.4	1.2	0.6	0.7	3	9 ⊙	2	C 0	C 0	C 0
11	13.8	8.3	4.2	8.8	-8.1	-2.6	3.4	-1.0	3.3	-9.0	84	87	84	85	0.3	0.7	1.2	0.8	4	10 *	10 •	C 0	C 0	C 0
12	8.1	10.2	11.7	10.0	2.4	2.3	2.6	2.3	4.2	2.2	93	91	93	93	0.6	0.6	0.4	0.3	10 •	10 •	10 •	SW 2	W 2	C 0
13	18.1	22.4	25.3	21.9	-1.8	-3.8	-9.6	-6.7	2.6	-11.3	83	79	69	77	0.9	0.8	0.9	0.9	10 *	9 *	9	NE 2	NE 4	NE 2
14	24.7	24.3	23.6	24.9	-17.3	-10.6	-14.6	-14.3	-9.6	-18.0	79	47	69	65	0.3	1.4	0.6	0.8	0	0 ⊙	6	C 0	C 0	ENE 2
15	22.3	17.6	18.8	19.6	-11.1	-9.2	-13.7	-12.3	-8.4	-17.0	72	83	77	78	0.7	0.4	0.4	0.3	10 *	10 *	10 *	C 0	WSW 4	W 2
16	24.0	27.4	32.6	28.0	-19.9	-17.6	-17.4	-18.1	-13.0	-21.3	70	68	74	71	0.4	0.3	0.4	0.4	7 *	9 ⚠ ⊙	9 ⚠	ENE 1	E 4	ENE 2
17	33.4	33.2	33.9	34.8	-19.2	-12.0	-12.7	-14.2	-10.4	-21.7	71	60	77	69	0.4	1.0	0.3	0.6	1	3 ⊙	10 *	C 0	ENE 2	NE 2
18	34.9	34.1	34.0	34.3	-9.7	-6.7	-9.1	-8.6	-6.7	-12.9	78	72	82	77	0.6	1.0	0.3	0.7	10 *	10 *	10 *	E 3	ENE 1	SE 1
19	31.9	31.3	29.8	31.0	-7.8	-3.2	-3.7	-3.1	-3.3	-9.4	87	88	87	87	0.4	0.3	0.6	0.3	10 —	10 ⚠	10	C 0	C 0	C 0
20	26.7	21.7	16.2	21.3	-3.1	-3.1	-2.8	-3.4	-0.6	-7.3	80	72	88	80	0.8	1.3	0.6	0.9	10	10	10 *	C 0	SW 3	SW 3
21	13.6	13.1	16.8	14.3	-2.7	-4.1	-7.9	-5.6	-2.1	-7.9	82	84	73	80	0.9	0.7	0.9	0.8	10 * ⚠	10 *	10 *	SE 3	SW 2	E 2
22	14.1	8.3	8.3	10.2	-12.1	-4.1	-6.9	-7.3	-2.6	-12.6	70	82	77	76	0.7	0.8	0.8	0.8	6	10 *	10 *	C 0	W 4	NW 2
23	11.6	13.7	13.6	13.6	-11.2	-11.3	-20.9	-16.1	-6.9	-22.6	79	72	73	73	0.3	0.7	0.3	0.3	9	9 *	0	C 0	C 0	C 0
24	13.9	14.3	13.2	14.3	-22.1	-12.3	-22.9	-20.1	-10.9	-23.7	66	66	81	71	0.4	0.8	0.2	0.3	0	0 ⊙	0	C 0	C 0	C 0
25	10.7	10.0	10.8	10.3	-23.7	-9.2	-19.2	-17.8	-7.6	-24.3	80	64	77	74	0.2	1.1	0.3	0.3	0	0 ⊙	0	C 0	C 0	C 0
26	10.3	9.4	8.0	9.3	-20.0	-8.1	-11.8	-12.9	-7.4	-21.7	83	66	78	76	0.2	1.2	0.3	0.6	0	3 ⊙	10	C 0	C 0	NE 2
27	9.1	10.0	10.3	9.8	-9.6	-7.2	-7.8	-8.1	-7.1	-13.0	78	74	81	78	0.6	0.9	0.6	0.7	10 *	7 ⊙	10	C 0	C 0	C 0
28	9.1	9.3	11.4	10.0	-8.4	-2.4	-8.1	-6.3	-1.3	-11.3	83	63	87	78	0.3	1.8	0.4	0.9	10	1 ⊙	0	C 0	C 0	C 0
29	12.3	13.1	14.0	13.1	-3.2	0.3	-3.0	-3.2	2.9	-9.2	92	78	90	87	0.3	1.4	0.4	0.7	3	2 ⊙	1	C 0	C 0	C 0
30	12.3	11.7	13.2	12.4	8.3	9.1	3.3	7.2	10.3	-3.3	96	96	62	98	3.0	3.1	3.3	4.3	2	7 ⊙	2	NE 3	NE 1	NE 3
31	12.3	12.6	11.1	12.1	2.1	2.8	-0.3	1.0	7.6	-0.7	79	80	92	84	1.4	1.3	0.3	1.1	6	9 ⊙	6	NE 2	ENE 1	C 0
M	16.7	16.3	16.9	16.6	-6.2	-2.4	-6.2	-5.2	-0.3	-10.4	77	70	80	76	1.4	2.1	1.0	1.3	6.3	6.9	6.3	1.3	1.8	1.2

Zakopane — $H_s = 844$ m — $H_b = 838{,}2$ m — $h_w = 17{,}7$ m — Listopad - Novembre 1961

DNI	WIATR	OPAD	ORIENTACJA	USŁONECZNIENIE	POGODA
1	9	0.3	.	-	
2	8	.	.	-	
3	9	.	.	-	
4	5	47.9	.	-	
5	6	11.2	32	-	
6	5	3.1	27	-	
7	8	8.7	20	-	
8	5	0.5	11	-	
9	8	.	6	-	
10	8	8.6	2	-	
11	7	9.8	.	-	
12	8	.	.	-	
13	8	6.8	.	-	
14	8	0.2	.	-	
15	5	.	.	-	
16	6	.	.	-	
17	8	0.0	.	-	
18	6	0.5	.	-	
19	7	3.2	1	-	
20	8	0.8	7	-	
21	7	.	8	-	
22	9	.	6	-	
23	6	.	4	-	
24	6	.	3	-	
25	7	0.9	3	-	
26	1	.	2	-	
27	9	.	pz.	-	
28	7	0.4	.	-	
29	7	0.0	.	-	
30	9	.	.	-	
31					
Σ	—	102.9	—	-	UWAGI

Grudzień - Décembre

DNI	WIATR	OPAD	ORIENTACJA	USŁONECZNIENIE	POGODA
1	9	0.1	.	-	
2	9	0.0	.	-	
3	8	0.0	.	-	
4	9	0.0	.	-	
5	9	.	.	-	
6	6	29.1	.	-	
7	6	9.1	32	-	
8	6	0.2	40	-	
9	8	.	35	-	
10	9	.	32	-	
11	6	12.2	29	-	
12	7	15.0	19	-	
13	7	0.3	5	-	
14	9	0.6	6	-	
15	5	7.7	6	-	
16	7	0.2	27	-	
17	8	0.3	20	-	
18	8	0.2	22	-	
19	6	0.4	22	-	
20	8	7.9	19	-	
21	6	4.5	26	-	
22	6	2.0	40	-	
23	7	0.2	42	-	
24	7	.	42	-	
25	8	.	40	-	
26	9	0.0	40	-	
27	6	0.1	37	-	
28	7	.	37	-	
29	8	.	33	-	
30	9	.	29	-	
31	8	.	25	-	
Σ	—	90.1	—	-	UWAGI

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Styczeń – Janvier 1961

DNI	CIŚNIENIE P − 700				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	91.9	92.6	92.8	92.4	-7.1	-8.4	-10.9	-9.3	-6.4	-10.9	96	95	94	95	0.1	0.2	0.2	0.2	10	10 ≡	9	SW 2	SW 3	S 3
2	90.5	89.3	88.2	89.3	-9.0	-9.0	-6.5	-7.8	-6.4	-11.0	95	95	97	96	0.2	0.2	0.1	0.2	10 *△ ≡	10 *△ ≡	9	SSE12	S 11	S 7
3	85.7	83.5	82.4	83.9	-6.9	-6.5	-4.2	-5.4	-4.1	-7.5	91	97	96	95	0.3	0.1	0.2	0.2	9	9	10 * ≡	SSE16	SSE22	SW 18
4	81.1	82.9	84.2	82.7	-3.6	-3.2	-2.8	-3.1	-2.6	-4.2	97	97	97	97	0.2	0.1	0.1	0.1	9	10 ≡	10 * ≡	SSE12	S 19	SE 13
5	83.3	86.4	90.5	86.7	-3.7	-6.9	-8.9	-7.1	-2.8	-9.0	97	96	95	96	0.2	0.1	0.2	0.2	10 * ≡	10 * △	10 △	S 8	WNW 5	SE 6
6	92.6	93.1	89.4	91.7	-11.4	-9.6	-10.0	-10.2	-8.9	-11.5	93	76	84	84	0.2	0.7	0.4	0.4	4	1 ⊙	2	WSW 7	SSE11	SE 19
7	88.3	89.3	90.8	89.5	-9.3	-8.8	-8.9	-9.0	-7.4	-10.5	95	95	86	92	0.2	0.2	0.4	0.3	5	10 ≡	1	SSE16	SSW10	SSE11
8	90.8	90.5	88.1	89.8	-10.3	-9.8	-9.1	-9.6	-8.8	-10.8	94	94	95	94	0.2	0.2	0.2	0.2	5	7 ⊙	10 *△ ≡	SW 9	S 10	SSE17
9	90.2	90.8	90.7	90.6	-8.8	-8.7	-9.0	-8.9	-7.9	-9.6	95	98	82	92	0.2	0.1	0.5	0.3	9	8	3	W 4	S 7	SSE 3
10	90.5	90.7	90.8	90.7	-8.0	-7.9	-8.7	-8.3	-6.6	-9.9	90	96	56	81	0.3	0.1	1.4	0.6	5	10 ≡	0	SW 3	SSE 4	S 4
11	90.7	91.4	94.6	92.2	-8.0	-7.6	-5.6	-6.7	-5.4	-10.1	67	96	97	87	1.1	0.1	0.1	0.4	5	9	10 ≡	SSE13	S 12	SSE10
12	96.6	96.7	98.8	97.4	-9.1	-13.8	-15.8	-13.6	-5.5	-16.5	95	96	95	95	0.2	0.1	0.1	0.1	10 ≡	10 * ≡	10 * ≡	WSW 5	N 4	N 5
13	100.6	102.3	102.9	101.9	-14.3	-11.2	-6.7	-9.7	-6.7	-17.6	96	73	15	61	0.1	0.7	3.1	1.3	0	1 ⊙	1	NNE 9	NNE 4	N 6
14	103.5	103.0	102.9	103.1	-1.7	-2.9	-5.6	-4.0	-1.0	-6.7	96	88	95	93	0.2	0.6	0.2	0.3	9	8	7	N 1	SSE 7	S 3
15	104.4	105.1	104.1	104.5	-6.1	-6.4	-4.4	-5.3	-3.6	-9.2	66	28	31	42	1.3	2.5	2.9	2.2	9	1 ⊙	1	NNE13	NNE 5	NNE 4
16	100.1	98.5	96.2	98.3	-6.7	-6.1	-10.1	-8.2	-3.2	-10.4	21	58	94	58	2.7	1.6	0.2	1.5	1	1 ⊙	10 ≡	N 6	N 5	N 9
17	95.3	96.0	95.9	95.7	-15.4	-14.9	-22.5	-18.8	-9.8	-25.7	95	31	96	74	0.1	1.3	0.0	0.5	10 *△ ≡	0 ○	10 △ ≡	N 9	N 14	NNE13
18	100.8	102.7	103.2	102.2	-18.6	-18.5	-15.2	-16.9	-14.9	-25.5	26	84	25	45	1.0	0.2	1.4	0.9	0	1 ⊙	0	NNE 5	N 7	NNE 6
19	102.5	101.6	101.0	101.7	-14.2	-12.1	-11.7	-12.4	-11.7	-16.5	20	74	95	62	1.6	0.6	0.2	0.8	2	9	10 *△	NE 4	N 5	NNE 6
20	98.6	97.5	95.5	97.2	-12.7	-12.1	-12.8	-12.6	-10.6	-14.2	92	74	58	75	0.2	0.6	1.0	0.6	7	1 ⊙	0	N 6	NE 3	NNE 4
21	92.6	92.1	91.8	92.2	-13.9	-13.0	-13.3	-13.4	-11.1	-14.6	96	57	80	78	0.1	1.0	0.4	0.5	1	1 ⊙	1	NNE 4	N 2	N 2
22	91.3	90.7	89.9	90.6	-8.9	-9.2	-10.0	-9.5	-8.3	-13.5	47	54	59	53	1.7	1.4	1.2	1.4	3	5 ⊙	5	NNE 1	SSW 4	SW 5
23	86.9	86.0	86.4	86.4	-8.6	-8.2	-9.2	-8.8	-8.1	-10.6	95	98	98	97	0.2	0.1	0.1	0.1	10 *△ ≡	10 * ≡	10	W 2	WNW 4	NW 3
24	86.5	86.5	84.7	85.9	-10.7	-9.0	-9.0	-9.4	-8.2	-11.1	97	98	98	98	0.1	0.1	0.1	0.1	1	3 ⊙	9 *	W 1	WSW 2	C 0
25	81.0	80.3	82.3	81.2	-10.0	-10.0	-13.0	-11.5	-8.3	-14.8	94	94	66	85	0.2	0.2	0.8	0.4	10 *	4 ⊙	1	NW 1	NNE 1	NE 4
26	87.5	92.1	96.6	92.1	-12.4	-9.7	-10.6	-10.8	-7.8	-14.4	26	38	20	28	1.7	1.8	2.2	1.9	0	0 ⊙	0	E 5	S 1	NE 4
27	100.3	102.2	102.8	101.8	-11.9	-7.8	-6.4	-8.1	-6.0	-12.2	29	29	17	25	1.7	2.4	3.1	2.4	0	0 ⊙	0	NNE 4	C 0	E 2
28	102.0	101.2	98.1	100.4	-5.8	-4.8	-5.2	-5.2	-4.3	-7.6	16	20	15	17	3.3	3.4	3.5	3.4	1	1 ⊙	2	S 8	SSE12	SE 17
29	96.9	98.8	99.0	98.2	-5.0	-5.4	-5.8	-4.5	-2.9	-7.1	31	98	70	66	2.9	0.1	1.3	1.4	1	8 ⊙	7	SSE16	SW 3	SW 2
30	95.8	95.0	90.6	93.1	-6.0	-4.0	-4.9	-5.0	-2.7	-6.1	51	46	95	64	1.9	2.5	0.2	1.5	5	8 ⊙	10	S 12	S 16	S 20
31	89.3	85.1	86.4	86.9	-3.8	-3.3	-4.0	-3.8	-1.7	-5.0	96	97	96	96	0.2	0.1	0.2	0.2	10 *△ ≡	10 * ≡	10 * ≡	SSE16	SSW13	W 12
M	93.2	93.3	93.3	93.3	-9.1	-8.7	-9.0	-9.0	-6.6	-11.6	74	76	74	75	0.8	0.8	0.8	0.8	5.5	5.7	5.7	7.4	7.3	7.7

Luty – Février

1	84.9	78.9	79.3	81.0	-7.2	-5.4	-6.9	-6.6	-4.0	-8.6	67	95	94	85	1.1	0.2	0.2	0.5	10	10 * ≡	10 * ≡	SSW13	SE 19	NW 4
2	78.8	77.1	74.2	76.7	-9.3	-7.6	-11.4	-9.9	-6.3	-11.7	91	96	93	93	0.3	0.1	0.2	0.2	10 * ≡	8	6	N 5	S 3	S 12
3	74.0	75.0	78.5	75.8	-8.2	-9.3	-11.8	-10.3	-6.0	-12.1	95	95	97	96	0.2	0.2	0.1	0.2	10 * △	10 * ≡	10 *	W 4	WNW 9	NNW 2
4	83.1	84.0	80.8	82.6	-12.8	-11.3	-14.3	-13.2	-9.6	-14.8	92	95	96	94	0.2	0.2	0.1	0.2	10 *	9 *	2	WNW 7	WNW 5	SSE 9
5	81.1	85.7	91.1	86.0	-12.4	-9.0	-12.8	-11.8	-9.0	-14.4	93	95	92	93	0.2	0.2	0.2	0.2	10	10 *	10 * ≡	SSE 9	C 0	N 6
6	93.5	94.1	92.5	93.4	-15.2	-11.5	-7.6	-10.5	-5.7	-16.6	82	72	82	79	0.3	0.7	0.6	0.5	1	4 ⊙	4	N 2	WNW 3	S 4
7	89.7	89.1	88.8	89.2	-2.6	-6.0	-8.8	-6.6	-2.0	-9.2	85	97	95	92	0.8	0.1	0.2	0.4	7	10 △ ≡	10 ≡	WSW 7	WNW 6	NW 4
8	89.5	91.6	94.2	91.8	-8.6	-9.1	-9.7	-9.3	-8.3	-10.2	95	95	94	95	0.2	0.2	0.2	0.2	10 * ≡	10 * ≡	10 △ ≡	NNW 4	NW 7	NW 6
9	94.4	91.9	89.7	92.0	-11.3	-9.3	-4.6	-7.4	-3.8	-11.9	90	95	98	94	0.3	0.2	0.1	0.2	8	10 *	10 * ≡	W 3	S 10	WNW 8
10	92.0	95.3	98.9	95.4	-6.1	-7.6	-9.1	-8.0	-4.5	-9.4	97	96	95	96	0.1	0.1	0.2	0.1	10 * ≡	10 △ ≡	10 △ ≡	NNW 7	NNW 3	NNW 6
11	97.9	95.9	95.0	95.6	-8.8	-5.7	-3.4	-4.8	-2.3	-9.9	95	75	78	83	0.2	1.1	1.0	0.8	9	6 ⊙	10	NNW 3	WSW 5	W 11
12	88.1	87.2	91.9	89.1	-6.8	-5.1	-6.9	-6.4	-3.2	-8.0	96	98	96	97	0.1	0.1	0.1	0.1	7	10 *△ ≡	10 △ ≡	NNW 3	S 2	N 5
13	96.5	98.0	98.8	97.8	-7.2	-7.6	-8.8	-8.1	-6.7	-9.3	96	96	95	96	0.1	0.1	0.2	0.1	10 *△ ≡	10 *△ ≡	10 * ≡	N 5	N 3	N 4
14	99.7	102.4	104.2	102.1	-9.7	-6.8	-5.1	-6.7	-5.1	-10.4	94	96	13	68	0.2	0.1	3.6	1.3	10 ≡	9	1	N 6	NNE 4	NNE 4
15	106.2	107.5	109.4	107.7	0.0	1.8	1.4	1.2	2.5	-5.2	25	24	44	31	4.6	5.3	3.9	4.6	7	1 ○	0	NNW 3	WNW 4	N 5
16	108.6	108.2	108.8	108.5	-0.6	-5.9	-5.8	-4.0	1.4	-6.1	69	96	95	87	1.8	0.2	0.2	0.7	9	10 △ ≡	0	NW 6	WNW 3	N 4
17	111.1	112.6	112.4	112.0	-0.2	0.6	0.8	0.5	1.4	-5.9	48	39	26	38	3.2	3.9	4.8	4.0	3	8	1	NE 4	N 6	NNE 9
18	111.9	112.3	111.5	111.9	0.8	3.1	2.9	2.4	3.6	0.5	21	25	17	21	5.1	5.7	6.2	5.7	1	0 ⊙	0	N 5	N 4	N 3
19	107.8	107.3	106.9	107.3	1.1	-0.2	-3.9	-1.7	3.2	-4.0	24	45	92	54	5.0	3.3	0.4	2.9	1	1 ○	8	WSW 4	W 2	NW 2
20	104.9	106.6	108.1	106.5	-6.6	-4.7	-4.7	-5.2	-5.2	-7.2	97	98	91	95	0.1	0.1	0.4	0.2	10 *△ ≡	10 ≡	1	NNE 4	NE 2	ENE 2
21	107.9	108.6	108.9	108.5	-5.0	-4.7	-1.3	-3.1	-0.5	-7.3	68	88	25	60	1.3	0.5	4.2	2.0	1	0 ⊙	0	SE 4	SSE 6	SSE 1
22	108.4	108.7	107.6	108.2	-1.0	3.5	-0.8	0.2	3.6	-5.2	16	29	27	24	4.8	5.5	4.2	4.8	2	7 ⊙	4	ENE 2	C 0	C 0
23	106.3	106.1	105.3	105.9	-2.1	-1.2	-1.4	-1.5	1.2	-3.5	28	44	27	33	3.7	3.1	4.0	3.6	5	2 ○	0	C 0	SSE 3	SSE 2
24	104.7	105.4	105.9	105.3	-2.3	-0.1	-2.4	-1.8	0.9	-2.7	59	48	59	55	2.2	3.2	2.1	2.5	0	1 ⊙	0	SE 2	SSE 2	C 0
25	106.4	107.1	107.9	107.1	-3.0	-1.5	-1.2	-1.7	0.8	-3.4	22	56	22	33	3.7	2.4	4.4	3.5	1	1 ⊙	0	S 2	SSW 4	S 3
26	108.5	109.1	109.5	109.0	-1.5	-1.0	0.2	-0.5	0.6	-3.6	14	56	15	22	4.7	3.7	5.2	4.5	0	0 ⊙	0	C 0	SW 3	WSW 2
27	108.9	109.2	107.2	108.4	-2.9	0.0	-1.1	-1.3	1.0	-2.9	28	85	91	67	3.5	1.1	0.5	1.7	0	4 ⊙	9	NNE 3	N 1	WNW 2
28	101.2	96.8	95.8	97.3	-1.2	0.6	-1.4	-0.8	1.5	-3.3	99	80	92	90	0.1	1.3	0.4	0.6	8	9	10 *△	SSW 8	SSW14	WSW 8
29																								
30																								
31																								
M	98.1	98.3	98.3	98.3	-5.4	-4.2	-5.0	-4.9	-2.2	-7.7	67	74	69	70	1.7	1.5	1.7	1.6	6.1	6.4	5.2	4.5	4.8	4.6

DNI	WYDZIELNOŚĆ	OPAD	GRUBOŚĆ ŚNIEGU	USŁONECZNIENIE	POGODA
1	0	1.9	60	-	
2	0	3.0	61	-	
3	9	4.5	64	-	
4	0	11.8	60	-	
5	6	8.6	69	-	
6	9	.	79	-	
7	1	1.7	75	-	
8	8	1.6	76	-	
9	8	.	78	-	
10	1	.	76	-	
11	9	1.2	73	-	
12	0	2.7	75	-	
13	9	0.0	82	-	
14	9	0.0	79	-	
15	9	.	75	-	
16	9	1.2	74	-	
17	9	0.7	72	-	
18	9	.	71	-	
19	9	0.1	69	-	
20	9	.	67	-	
21	9	.	64	-	
22	9	0.5	65	-	
23	1	1.1	65	-	
24	9	0.2	67	-	
25	9	0.0	66	-	
26	9	.	64	-	
27	9	.	61	-	
28	9	.	60	-	
29	5	0.0	56	-	
30	9	0.0	50	-	
31	0	4.1	48	-	
Σ	—	44.9	—	-	UWAGI:

Luty - Février

DNI	WYDZIELNOŚĆ	OPAD	GRUBOŚĆ ŚNIEGU	USŁONECZNIENIE	POGODA
1	0	3.2	51	-	
2	9	0.9	51	-	
3	0	6.9	50	-	
4	6	1.0	59	-	
5	6	16.0	61	-	
6	9	.	90	-	
7	0	0.6	83	-	
8	0	8.2	79	-	
9	8	7.8	96	-	
10	0	10.0	106	-	
11	9	3.8	110	-	
12	0	4.3	113	-	
13	1	5.4	118	-	
14	9	.	124	-	
15	9	.	120	-	
16	0	2.2	116	-	
17	9	.	118	-	
18	9	.	116	-	
19	9	0.5	106	-	
20	0	0.4	101	-	
21	9	.	102	-	
22	9	.	101	-	
23	9	.	96	-	
24	9	.	95	-	
25	9	.	92	-	
26	9	.	90	-	
27	9	.	89	-	
28	9	8.8	85	-	
29					
30					
31					
Σ	—	80.0	—	-	UWAGI:

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Marzec – Mars 1961

DNI	CIŚNIENIE P − 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI A				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	95.2	94.4	97.9	95.2	-8.6	-8.4	-8.7	-8.6	-1.1	-9.2	92	95	95	94	0.5	0.2	0.2	0.2	10 *△ =	9	10 =	NNW 4	NW 4	N 3
2	100.7	102.3	101.4	101.5	-10.0	-8.5	-9.9	-9.6	-7.8	-10.5	94	95	94	94	0.2	0.2	0.2	0.2	10 =	10 △	9	NNE 4	NW 2	WNW 2
3	100.9	103.4	105.1	103.1	-9.9	-6.5	-7.2	-7.7	-5.6	-11.0	94	97	96	96	0.2	0.1	0.1	0.1	9	10 *	10 * =	N 2	NNE 3	NE 4
4	106.5	108.6	109.9	108.3	-6.2	-4.7	-6.0	-5.7	-4.2	-7.3	97	98	97	97	0.1	0.1	0.1	0.1	10 * =	10 *△ =	10 =	NNE 5	NNE 4	NNE 5
5	109.3	110.2	108.7	109.4	-6.4	-5.1	-4.8	-4.8	-2.7	-9.2	84	48	98	77	0.6	2.5	0.1	1.1	8	8 ⊙	10 △ =	NNE 5	NW 7	NNE 6
6	108.0	109.8	110.2	109.3	-4.3	-0.9	0.6	-1.0	1.1	-9.0	25	32	44	33	3.5	3.9	3.6	3.7	4 ⊙	8 ⊙	4	NE 9	NE 8	NE 7
7	108.5	107.5	107.4	107.8	0.9	0.3	-2.4	-0.9	1.7	-2.6	56	60	57	58	2.9	2.5	2.2	2.5	6	8 ○	4	N 6	WNW 5	NNE 9
8	108.1	109.9	110.5	109.5	-4.5	-1.2	-2.2	-2.5	-0.3	-6.2	79	42	51	57	0.9	3.2	2.5	2.2	2 ○	5 ⊙	1	NE 8	NNE 9	NNE13
9	109.0	109.8	109.2	109.3	-4.0	-0.9	-0.6	-1.5	0.1	-5.0	96	99	95	97	0.2	0.0	0.3	0.2	10 =	9	6	NNE 8	NNE 5	NNE10
10	109.0	108.7	106.2	108.0	1.5	6.1	2.5	3.2	6.3	-0.7	80	49	76	68	1.4	4.7	1.9	2.7	3 ⊙	1 ○	1	NE 6	SSE 1	SSW 5
11	103.9	104.0	103.9	103.9	-1.2	-0.4	-1.9	-1.4	2.5	-2.7	76	80	100	85	1.4	1.2	0.0	0.9	7 ⊙	6 ○	10 =	WNW 8	WNW 7	NNW 8
12	101.7	101.2	98.4	100.4	-5.0	-0.6	1.7	-0.6	2.0	-5.2	98	99	76	91	0.1	0.0	1.7	0.6	10 =	9	9	NNW 8	NNW 8	WNW15
13	88.9	89.3	91.1	89.8	-2.0	-6.6	-6.9	-5.6	2.1	-7.4	98	94	99	97	0.1	0.2	0.0	0.1	10 * =	9	10 =	NW 16	N 12	NNE12
14	92.2	93.4	96.0	93.9	-8.4	-4.3	-1.9	-4.1	-1.9	-10.2	95	96	98	96	0.2	0.2	0.1	0.2	10 =	10 *△ =	10 *△ =	N 10	N 7	N 7
15	96.0	98.6	101.5	98.7	-5.4	-3.1	-5.5	-5.4	-1.6	-5.7	97	99	99	98	0.2	0.0	0.0	0.1	10 *△ =	10 △ =	10 △ =	N 11	N 12	N 9
16	100.8	100.0	98.5	99.8	-2.5	-1.4	-3.1	-2.5	-1.3	-4.7	100	99	97	99	0.0	0.1	0.1	0.1	10 • =	10 *	10 * =	NNW11	N 12	N 16
17	101.7	103.7	101.1	102.2	-6.0	-1.6	-1.2	-2.5	-0.7	-7.3	92	71	50	71	0.3	1.6	2.8	1.6	6 ⊙	9 ⊙	2	NNE 8	N 6	NW 5
18	95.6	95.7	90.1	93.1	0.9	3.6	1.9	2.1	4.3	-1.8	41	43	76	53	3.8	4.5	1.7	3.3	8 ⊙	7 ⊙	6	SW 10	WSW 8	SW 13
19	85.7	84.9	85.2	85.3	-5.7	-7.5	-9.2	-7.4	2.0	-10.1	97	96	95	96	0.2	0.1	0.2	0.2	10 * △	10 △	10 =	WNW 9	W 3	NW 4
20	85.1	86.2	85.9	85.1	-14.0	-12.7	-11.5	-12.4	-8.6	-14.8	100	88	90	93	0.0	0.3	0.3	0.2	10 * =	5 ○	10 *	NNE 5	NW 4	SW 10
21	75.7	76.7	79.6	77.3	-10.1	-9.0	-10.1	-9.8	-8.6	-12.1	94	95	94	94	0.2	0.2	0.2	0.2	10 * =	10 * =	10 *	SW 21	WSW13	WNW 9
22	83.1	86.1	89.0	86.1	-11.9	-11.3	-14.3	-13.0	-10.1	-14.4	93	93	96	94	0.2	0.2	0.1	0.2	10 * =	10 * =	N 5	NNE 7	NNW 2
23	89.7	92.0	94.9	92.2	-9.0	-7.1	-6.3	-7.2	-6.3	-15.4	95	96	97	96	0.2	0.1	0.1	0.1	10 *△ =	10 *△ =	10 △ =	N 7	NNE 7	NNE 9
24	96.0	97.3	97.8	97.3	-6.1	-5.0	-5.3	-5.4	-4.4	-6.8	97	98	98	98	0.1	0.1	0.1	0.1	10 △ =	10 =	10 △ =	N 7	WNW 8	N 8
25	97.7	98.9	100.0	98.9	-5.5	-4.8	-4.6	-4.9	-4.2	-6.0	97	98	98	98	0.1	0.1	0.1	0.1	10 △ =	10 △ =	10 △ =	N 8	NNW 9	NNE 9
26	98.9	97.3	94.0	96.7	-5.2	-4.9	-4.5	-4.8	-4.3	-5.9	93	98	77	89	0.3	0.1	1.0	0.5	8	10 △	7	WNW 6	SSW 7	WSW10
27	89.4	88.6	87.3	88.4	-5.6	-6.9	-10.1	-7.7	-2.8	-10.5	97	96	91	95	0.2	0.1	0.3	0.2	10 *△ =	10 *△ =	7 *	W 10	WNW13	NNW16
28	85.1	87.3	87.4	86.6	-13.9	-12.3	-11.2	-12.2	-9.6	-14.5	96	93	93	94	0.1	0.2	0.2	0.2	10 * =	10 * =	10 *△ =	NW 17	NW 17	WNW18
29	88.9	89.9	91.0	89.9	-11.5	-8.5	-5.7	-7.8	-5.5	-13.4	95	95	97	95	0.2	0.2	0.1	0.2	10 *△ =	10 △	10 *△ =	NW 12	W 9	NW 9
30	89.5	90.4	88.5	89.5	-7.0	-5.4	-5.2	-4.2	-3.0	-7.3	96	97	97	97	0.1	0.2	0.1	0.1	5 ⊙	10	10 △ =	W 11	W 10	SSW12
31	87.3	88.4	88.8	88.2	-2.2	-1.8	-3.0	-2.5	-1.5	-4.0	98	98	97	98	0.1	0.1	0.1	0.1	10 * △	10 * ⚹	10 *	WNW11	W 9	WNW10
M	96.3	97.2	97.2	96.9	-5.9	-4.4	-4.9	-5.0	-2.4	-8.0	88	85	88	87	0.6	0.9	0.7	0.7	8.6	8.8	8.3	8.6	7.6	8.8

Kwiecień – Avril

1	90.6	91.2	90.1	90.6	-10.2	-4.0	-2.4	-4.8	-2.0	-10.9	59	91	98	83	1.2	0.4	0.1	0.6	3 ⊙	9	10 * =	NW 13	WNW11	WSW10
2	90.2	92.1	91.3	91.2	-2.2	-1.6	-0.9	-1.4	-0.6	-5.0	98	98	99	98	0.1	0.1	0.0	0.1	10 *	10	10 △ =	WNW10	W 9	SSW10
3	89.0	90.3	92.0	90.4	-1.0	-1.6	-1.8	-1.6	-0.3	-2.3	99	98	98	98	0.1	0.1	0.1	0.1	10 =	9	8 △	WSW 6	WSW 6	WSW 6
4	91.9	94.0	96.8	94.2	-1.6	-0.4	0.0	-0.5	0.4	-2.6	96	98	100	98	0.2	0.1	0.0	0.1	8 ⊙	9	10 ⚹	SSW 9	SW 10	WSW 4
5	97.2	98.5	98.8	98.2	0.7	3.0	2.1	2.0	3.9	-0.3	92	80	92	88	0.5	1.7	0.7	1.0	9	6 ⊙	4	S 10	S 10	SSW12
6	99.6	100.8	100.0	100.1	2.1	6.3	3.7	4.0	6.7	1.2	87	55	87	76	1.0	4.2	1.0	2.1	4 ⊙	1 ⊙	1	SSW 8	SSE 5	SSE14
7	98.3	101.1	101.4	100.3	4.3	7.6	7.3	6.6	9.5	1.8	72	51	60	61	2.4	5.1	4.1	3.9	1 ⊙	1 ⊙	2	SSE17	WSW 2	SW 4
8	99.5	98.0	96.1	97.9	6.5	7.0	0.8	3.8	7.8	0.5	63	65	100	76	3.6	3.4	0.0	2.3	8	8 ⊙ (R)	10 =	WSW 5	W 7	WNW10
9	95.0	97.0	97.0	96.3	-8.6	-4.2	-5.0	-5.7	0.8	-9.2	92	98	29	73	0.3	0.1	3.0	1.1	8 ○	8	0	NE 6	NNE 3	N 3
10	95.7	95.0	95.1	94.6	-2.4	0.1	-0.4	-0.8	0.9	-5.0	9	47	100	52	4.7	3.3	0.0	2.7	1 ○	7 ⊙	10 =	SW 3	WSW 6	SSW 8
11	91.8	92.7	93.7	92.7	-0.3	1.9	-0.6	0.0	2.2	-1.8	100	88	99	96	0.0	0.8	0.0	0.3	9	9	10 =	WSW 3	NW 2	NE 4
12	94.5	97.5	99.3	97.1	-3.2	-0.1	-0.2	-0.9	1.0	-4.2	65	78	70	71	1.6	1.4	1.8	1.6	9	4 ⊙	0	NNE 7	NNE 1	NW 2
13	98.9	100.3	100.4	99.9	1.4	5.7	3.1	3.3	7.5	-0.3	47	64	80	64	3.6	3.4	1.6	2.9	8	6	1	WNW 4	C 0	S 2
14	99.2	99.6	98.1	99.0	4.2	6.3	3.3	4.4	7.7	1.1	26	36	62	41	6.1	6.2	3.0	5.1	7 ⊙	6 ⊙	0	SSW 5	SW 8	SSW16
15	98.2	99.0	98.6	98.6	3.6	7.0	3.7	4.5	7.2	2.5	60	53	78	64	3.2	4.7	1.8	3.2	1 ⊙	5 ⊙	6	S 13	WSW10	S 8
16	97.1	95.7	95.4	96.1	0.7	2.5	-0.6	0.5	4.1	-1.4	98	98	95	97	0.1	0.1	0.3	0.2	9 ⚹	9 • ⚹	1	SW 10	SW 15	SW 10
17	95.4	96.5	97.2	96.4	0.3	3.7	1.8	1.9	4.8	-1.1	64	81	88	78	2.2	1.6	0.9	1.6	2 ⊙	9	2	SW 4	C 0	NE 2
18	96.7	96.9	95.7	96.4	1.5	5.1	2.0	2.6	5.7	0.2	74	78	98	83	1.8	1.9	0.2	1.3	8 ⊙	8	10 •	S 5	W 1	C 0
19	96.1	97.4	96.6	96.7	1.1	1.1	1.1	1.1	2.0	0.2	100	100	100	100	0.0	0.0	0.0	0.0	9	10 • =	10 *△ =	NE 4	ENE 4	NE 7
20	95.8	97.9	98.7	97.5	-1.8	-1.4	-3.3	-2.4	1.1	-4.4	98	97	65	87	0.1	0.2	1.7	0.7	10 =	9	3	ENE 8	ENE 6	ENE 4
21	98.4	99.4	99.0	98.9	1.8	3.3	-1.2	0.7	4.5	-3.7	50	57	80	56	4.9	3.2	1.1	3.1	3 ⊙	1 ⊙	0	C 0	WNW 1	WSW 5
22	95.9	95.7	92.6	94.7	-2.1	3.1	-1.9	-0.7	4.4	-3.9	81	63	98	81	1.0	2.8	0.1	1.3	0 ⊙	4 ⊙	7	SSW10	WSW 7	SW 15
23	90.7	91.2	90.1	90.7	-0.2	3.3	0.6	1.1	4.8	-3.3	94	61	46	67	0.1	2.9	3.5	2.2	6 ⊙	2 ⊙	0	S 8	SSE 7	S 15
24	89.9	90.5	91.0	90.5	-1.0	4.4	0.6	1.2	4.5	-2.2	77	73	85	78	1.4	2.3	0.9	1.5	1 ○	6 ⊙	5	S 4	ENE 3	SSE 1
25	91.6	92.5	92.6	92.2	0.6	3.4	2.0	2.0	4.8	-1.4	90	94	58	81	0.7	0.4	3.0	1.4	6 ⊙	9	3	NE 4	NE 1	ENE 2
26	92.0	91.8	91.9	91.9	0.9	2.9	2.0	2.0	4.3	-1.2	98	96	96	97	0.1	0.2	0.3	0.2	6	9 •	8	NE 1	SSW 3	SSE 3
27	91.4	92.3	93.2	92.3	0.9	2.1	0.4	1.0	3.5	0.4	100	98	100	99	0.0	0.1	0.0	0.0	10 =	10	10 =	ENE 5	ENE 3	NE 2
28	92.9	93.6	93.4	93.3	-1.6	0.7	-0.1	-0.3	1.6	-1.9	86	88	90	88	0.8	0.8	0.7	0.8	9	10 *	8	WSW 3	S 2	S 3
29	92.9	94.2	93.7	93.6	-0.2	-0.4	0.8	0.2	3.3	-1.2	96	100	80	92	0.3	0.0	1.3	0.5	9 ⊙	10 *⚹ =	2	SW 8	SSE 6	S 10
30	91.9	91.2	89.9	91.0	2.0	3.1	0.4	1.5	4.2	-0.4	68	76	94	79	2.3	1.9	0.4	1.5	10	10	10 △	SE 4	E 2	0 0
31																								
M	94.6	95.3	95.3	95.1	-0.1	2.3	0.6	0.8	3.7	-1.9	77	79	84	80	1.3	1.8	1.1	1.3	6.3	7.1	5.4	6.6	5.0	6.3

Kasprowy Wierch — $H_s = 1991\,m$ — $H_b = 1988{,}8\,m$ — $h_w = 15{,}4\,m$ — Marzec – Mars 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	P O G O D A
1	7	2.4	93	-	
2	6	0.2	97	-	
3	7	5.2	94	-	
4	0	10.4	104	-	
5	9	0.3	120	-	
6	9	.	115	-	
7	9	.	110	-	
8	9	.	106	-	
9	7	.	103	-	
10	9	.	101	-	
11	8	0.1	95	-	
12	8	2.6	92	-	
13	9	6.9	96	-	
14	0	21.3	97	-	
15	0	8.1	115	-	
16	7	1.2	121	-	
17	9	.	122	-	
18	9	1.2	115	-	
19	6	9.5	107	-	
20	9	2.3	122	-	
21	0	8.0	118	-	[19.III: 23[15] 24]
22	0	16.7	142	-	
23	0	10.4	175	-	
24	0	6.5	191	-	
25	0	9.4	195	-	
26	7	1.6	205	-	
27	0	11.5	192	-	
28	1	10.7	203	-	
29	7	6.0	228	-	
30	8	3.6	220	-	
31	6	10.2	216	-	
Σ	—	166.3	—	-	UWAGI [31.III: ☩ 0-1 0[00]-24]

Kwiecień – Avril

1	9	7.8	204	-	
2	7	3.7	202	-	
3	8	0.4	198	-	
4	8	0.0	189	-	
5	8	.	174	-	
6	9	.	160	-	
7	9	0.0	145	-	
8	9	7.1	123	-	
9	9	.	105	-	
10	9	0.0	103	-	
11	8	3.2	95	-	
12	9	.	83	-	
13	8	.	71	-	
14	9	.	70	-	
15	9	0.2	63	-	
16	9	3.8	55	-	
17	9	.	53	-	
18	8	7.1	51	-	
19	0	8.2	44	-	
20	8	.	41	-	
21	9	.	39	-	
22	9	.	36	-	
23	9	.	34	-	
24	9	.	31	-	
25	8	.	29	-	
26	7	0.5	26	-	
27	7	0.6	24	-	
28	8	0.5	22	-	
29	1	3.0	pł.	-	
30	8	0.9	pł.	-	
31					
Σ	—	47.0	—	-	UWAGI

Kasprowy Wierch $\varphi = 49°14'$ $\lambda = 19°59'$ Maj - Mai 1961

DNI	CIŚNIENIE P − 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE I POGODA N,w			KIERUNEK I PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	89.8	92.1	95.4	91.8	-0.3	-0.1	-1.1	-0.6	0.8	-1.3	100	100	99	100	0.0	0.0	0.1	0.0	10 =	10 ● =	10 =	NNE 5	NNE 2	N 1
2	93.6	95.3	95.8	94.9	-2.0	0.9	0.7	0.1	2.7	-2.5	98	100	75	91	0.1	0.0	1.6	0.6	10 ● =	10 =	1	NNE 5	NNE 1	NNE 2
3	95.4	96.2	96.9	96.2	0.6	3.2	2.0	2.0	3.6	0.0	98	84	85	89	0.1	1.2	1.1	0.8	9	9 ●	7	N 2	SSW 3	W 4
4	97.8	99.3	100.4	99.2	-0.2	0.1	0.6	0.3	3.3	-0.9	100	100	85	95	0.0	0.0	0.9	0.3	10 ⚹ =	10 ⚹ =	0	NNW 2	NNW 5	ENE 4
5	101.3	102.5	102.6	102.1	1.6	7.3	3.5	4.0	8.2	-0.1	64	69	97	77	2.5	5.2	0.2	2.0	1 ☉	7 ☉	4	C 0	SSE 1	SSW 8
6	100.9	102.3	102.0	101.7	3.2	8.3	5.7	5.7	9.3	2.3	98	74	100	91	0.2	2.9	0.0	1.0	10	9	10	SSW 4	S 6	SSW 4
7	100.2	100.1	97.8	99.4	3.7	5.0	3.1	3.7	6.6	2.9	100	98	87	95	0.0	0.1	1.0	0.4	10 ●	9	4	SW 5	NW 5	W 8
8	96.8	95.8	94.7	95.8	-3.3	0.4	-3.3	-2.4	3.5	-4.0	92	79	92	88	0.4	1.3	0.4	0.7	9	8	7	N 7	WNW 5	NNW 9
9	92.5	91.2	90.2	91.3	-4.7	-2.2	-3.2	-3.3	-1.6	-5.1	98	87	97	94	0.1	0.7	0.1	0.3	10 ⚹	9 ⚹	10 ⚹ =	NW 7	WNW 6	WNW 12
10	90.4	92.4	93.1	92.0	-4.3	-3.1	-3.8	-3.8	-2.8	-4.9	96	97	96	96	0.2	0.1	0.2	0.2	10 =	10 ⚹ =	10 ⚹ =	NW 7	N 6	NNW 7
11	92.7	93.4	94.9	93.7	-4.7	-2.9	-4.1	-4.0	-2.1	-5.6	98	97	96	97	0.1	0.1	0.2	0.1	10 ⚹ =	9 ⚹	10 ⚹ ☾ =	NNE 3	NNE 5	NNE 6
12	94.0	94.4	94.6	94.3	-6.6	-4.6	-6.2	-5.9	-3.7	-7.0	97	98	97	97	0.1	0.1	0.1	0.1	10 ⚹ ☾ =	10 ⚹ =	10	NNE 5	NNE 7	NNE 6
13	94.9	95.7	95.8	95.5	-6.0	-2.8	-4.0	-4.2	-1.6	-7.5	92	88	89	90	0.3	0.6	0.5	0.5	2 ☉	9	4	C 0	WSW 4	S 7
14	94.3	93.3	93.0	93.5	-2.5	-1.5	-1.8	-1.9	-1.0	-4.3	98	99	98	98	0.1	0.1	0.1	0.1	10 =	10 ⚹ =	10 ⚹ ☾ =	SSW 9	SW 13	W 6
15	92.2	94.1	94.7	93.7	-5.1	-1.5	-3.2	-3.2	-1.1	-6.5	77	96	97	90	0.9	0.2	0.1	0.4	2 ☉	10 ● =	10 △ =	N 2	N 2	NW 1
16	93.8	94.0	94.0	93.9	-4.6	-1.3	-3.2	-3.1	-0.9	-5.3	96	99	92	96	0.2	0.1	0.3	0.2	9	9 ⚹	5 ⚹	WNW 3	NNW 2	W 3
17	92.2	93.3	95.2	93.6	-3.2	-2.1	-3.1	-2.9	-0.4	-4.7	97	98	97	97	0.1	0.1	0.1	0.1	10 △ =	10 ⚹ △ =	10 ⚹ △ =	SSW 2	NNE 3	NNE 5
18	95.8	96.4	96.7	96.3	-3.2	-2.7	-4.4	-3.7	-2.6	-4.5	97	97	96	97	0.1	0.1	0.2	0.1	10 ⚹ =	10 ⚹ ☾ =	9	NNE 5	NNE 5	NNE 6
19	95.9	96.5	96.3	96.2	-1.9	-1.3	-1.0	-1.3	0.0	-4.8	98	99	97	98	0.1	0.1	0.2	0.1	7 ☉	10 ⚹ ☾	8	NNE 3	NNW 2	C 0
20	95.6	92.6	91.8	92.7	-0.2	0.3	0.8	0.4	2.0	-1.5	84	94	86	88	1.0	0.4	1.0	0.8	2 ☉	9 ⚹ ☾	4	NE 1	NE 1	E 3
21	90.2	90.0	90.9	90.4	0.5	0.4	0.5	0.5	1.2	-0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 ⚹ △ =	10 ⚹ ☾ =	NE 6	NE 7	NE 7
22	91.6	92.9	93.3	92.6	-0.2	-0.1	-0.9	-0.5	0.7	-1.0	100	100	99	100	0.0	0.0	0.0	0.0	10 ● △ =	10 ⚹ =	10 △ =	NE 7	NE 8	NNE 8
23	93.6	95.7	96.9	95.4	-3.1	0.4	-0.4	-0.9	2.3	-3.6	97	83	90	90	0.1	1.1	0.6	0.6	7 ☉	4 ☉	3	NNE 3	NNE 2	NE 1
24	97.4	98.7	99.2	98.4	-0.1	2.0	0.9	0.9	3.0	-0.9	92	85	92	90	0.6	1.1	0.5	0.7	9	9	8	WSW 1	NNE 1	NNE 3
25	99.0	99.1	98.4	98.8	1.6	4.3	3.2	3.1	5.5	0.5	91	73	100	88	0.7	2.3	0.0	1.0	9 ☉	9	10 =	NNE 3	NNE 2	ENE 3
26	97.5	98.2	97.3	97.7	3.3	5.6	4.2	4.4	7.1	2.4	79	70	89	79	1.6	2.6	0.8	1.7	9 ☉	9	9	N 2	C 0	SSW 5
27	96.7	96.5	95.6	96.3	4.2	4.5	4.3	4.3	7.6	3.7	87	90	94	90	1.0	0.8	0.4	0.7	8	10 ● ☾	10	S 6	SSE 7	S 9
28	95.0	95.4	95.3	95.2	3.8	5.1	4.4	4.4	6.1	2.9	100	100	91	97	0.0	0.0	0.8	0.3	10 =	9	6	S 10	WSW 7	S 5
29	90.8	87.8	86.5	88.4	4.6	6.2	4.2	5.8	8.4	2.7	96	90	100	95	0.3	0.9	0.0	0.4	9 ●	9 ●	10 ● =	SSE 7	SSE 11	SW 8
30	86.8	88.2	88.7	87.9	3.4	2.2	0.0	1.4	4.2	-0.2	88	96	100	95	0.9	0.3	0.0	0.4	7 ☉	8	10 =	S 2	SW 7	C 0
31	89.8	92.1	93.3	91.7	-2.3	3.3	3.2	2.4	6.3	-2.9	96	64	96	85	0.3	3.2	0.3	1.3	3 ☉	6 ☉	3	SW 3	WSW 7	SSW 9
M	94.4	95.0	95.1	94.8	-0.9	1.1	-0.1	0.0	2.4	-2.0	94	90	94	93	0.4	0.8	0.4	0.5	8.1	9.0	7.3	4.4	4.5	5.2

Czerwiec - Juin

1	93.8	94.8	94.2	94.3	5.1	7.6	5.7	6.0	10.0	2.5	66	79	100	82	3.0	2.1	0.0	1.7	1 ☉	8	9	S 5	SSW 7	SW 10
2	93.7	95.0	94.5	94.4	6.5	7.4	6.7	6.8	10.1	4.1	81	85	74	80	1.8	1.6	2.5	2.0	3 ☉	9 ● △ ☾	9	SW 13	NNE 5	NE 6
3	93.1	94.2	94.9	94.1	6.6	6.9	5.8	6.3	8.4	4.6	84	97	100	94	1.5	0.3	0.0	0.6	9	10	10 ●	ESE 4	NW 1	NNE 3
4	95.5	96.3	97.2	96.4	5.2	7.1	5.8	6.0	8.6	4.5	100	100	95	98	0.0	0.0	0.3	0.2	10 ●	10 = (☾)	9	NE 2	E 2	E 3
5	97.8	99.3	99.8	99.0	5.3	8.1	6.0	6.4	8.2	4.4	100	100	95	98	0.0	0.0	0.3	0.2	10	10 =	6	ENE 6	C 0	E 1
6	99.3	99.2	98.4	99.0	6.8	9.1	6.0	7.0	9.8	4.6	79	89	87	85	2.1	1.4	1.3	1.6	8	9 ●	9 ●	S 2	S 4	SSE 7
7	97.9	97.7	96.3	97.4	5.9	6.3	5.3	5.8	8.1	4.4	88	99	100	96	1.1	0.2	0.0	0.4	8	10	10 =	SSE 5	SSW 4	SSW 5
8	97.2	98.7	99.2	98.4	5.4	8.0	6.7	6.7	8.7	4.3	97	87	95	93	0.3	1.3	0.3	0.7	7 ☉	9	10	SSW 6	SW 2	C 0
9	99.2	100.1	99.8	99.7	7.0	8.9	6.7	7.3	9.8	5.8	92	83	95	90	0.8	2.0	0.3	1.1	3 ☉	10 (☾)	6	ESE 1	SE 2	S 5
10	99.3	100.3	100.1	100.0	7.3	6.8	6.0	6.6	10.3	4.9	73	94	87	85	2.8	0.7	1.3	1.6	6 ☉	9 ● ☾	9	SSE 3	WSW 6	SSE 5
11	99.2	99.3	98.3	99.1	7.0	5.1	6.3	6.2	8.2	4.7	72	89	96	86	2.8	0.9	0.3	1.3	9 ☉	10 ● △ ☾	10	SSE 3	NW 1	C 0
12	97.6	97.8	97.3	97.6	6.3	5.2	3.9	4.9	7.0	3.8	93	100	100	98	0.3	0.0	0.0	0.2	9	10 ●	10	SSW 4	NNW 2	NNW 2
13	96.2	93.7	93.7	95.2	3.2	6.4	5.3	5.2	7.3	1.9	72	71	100	81	2.2	2.8	0.0	1.7	3	9	10 ● =	C 0	WSW 4	SW 10
14	93.3	93.6	97.3	95.3	3.0	2.3	1.7	2.2	5.3	1.0	100	96	98	98	0.0	0.3	0.2	0.2	10 =	10	9	W 5	W 2	WNW 6
15	98.4	99.8	100.2	99.3	0.6	2.4	2.4	2.0	4.0	-0.1	100	94	69	88	0.0	0.3	2.3	0.9	10 ● ☾ =	9	8	NW 3	W 3	WNW 2
16	100.2	101.9	102.8	101.6	1.7	7.0	3.1	3.7	8.6	-0.6	28	70	92	63	5.0	3.0	0.3	2.8	0 ☉	5 ☉	2	W 2	NNE 3	NNE 1
17	103.1	104.9	105.2	104.4	4.3	7.3	5.9	6.0	10.1	1.9	65	81	90	79	2.9	2.0	0.9	1.9	2 ☉	9 ☉	7	S 1	NW 2	N 1
18	105.2	106.0	105.6	105.6	6.2	11.3	9.0	8.9	14.4	4.3	61	70	83	71	3.7	4.0	2.0	3.2	7 ☉	7 ☉	3	NNE 1	W 1	C 0
19	105.9	107.0	107.2	106.7	9.3	15.3	9.4	10.8	15.6	7.9	83	63	100	82	2.0	6.6	0.0	2.9	2 ☉	6 ☉	10	C 0	NNE 4	WNW 4
20	106.6	107.8	107.6	107.3	4.3	5.7	3.2	4.1	9.4	3.0	100	90	91	94	0.0	0.9	0.7	0.5	10 =	9	9	NNE 4	NNE 5	NE 4
21	106.5	106.8	107.4	106.9	4.9	10.6	6.4	7.1	12.4	2.0	93	73	90	85	0.6	3.4	0.9	1.6	6 ☉	5 ☉	7	NW 2	NNW 1	NNE 2
22	108.4	108.5	105.7	107.5	6.6	11.2	8.3	8.6	13.0	4.1	74	68	91	78	2.5	4.3	1.1	2.6	2 ☉	8	10	NNE 2	W 4	SSW 11
23	102.5	105.2	106.3	104.7	6.7	7.9	6.6	7.0	9.2	6.0	97	89	91	92	0.3	1.1	0.9	0.8	9	8	7	NNW 6	NNW 5	WNW 5
24	106.4	107.8	108.4	107.5	6.6	12.3	8.1	8.8	13.6	5.6	81	53	75	70	1.8	6.7	2.7	3.7	6	9 ☉	6	W 2	NW 4	NNE 3
25	107.7	107.3	105.7	106.9	10.4	14.1	11.7	12.0	17.1	7.7	69	59	70	66	3.9	6.6	4.2	4.9	3 ☉	4 ☉	2	NW 3	W 5	SW 7
26	104.7	104.6	102.8	104.0	11.9	14.6	11.9	12.6	16.3	10.1	72	57	73	67	3.9	7.1	3.7	4.9	3 ☉	7 ☉	6	SSW 7	SW 8	SSW 9
27	101.1	101.9	100.5	101.2	12.5	15.5	12.5	13.2	16.7	10.7	67	62	95	75	4.8	6.8	0.8	4.1	3 ☉	3 ☉	9	SSE 10	WSW 10	SW 7
28	101.1	104.3	107.8	104.3	7.0	3.0	0.8	2.9	12.3	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 ● =	10 ● =	10 =	N 3	N 4	NNE 7
29	108.9	110.4	110.1	109.8	0.0	4.6	3.8	3.0	7.3	-0.6	100	93	100	98	0.0	0.6	0.0	0.2	9	9	10 =	NE 7	NNE 2	NNE 6
30	109.9	110.7	110.3	110.3	6.6	9.6	6.7	7.4	12.1	2.6	74	82	84	80	2.3	2.2	1.3	2.1	2 ☉	7	1	NE 4	NNE 2	ENE 3
31																								
M	101.0	102.0	101.8	101.6	6.0	8.3	6.3	6.7	10.4	4.0	82	82	91	85	1.8	2.3	1.0	1.7	6.1	8.3	7.8	3.9	3.3	4.5

Kasprowy Wierch — $H_s = 1991\ m$ — $H_b = 1988{,}8\ m$ — $h_w = 15{,}4\ m$ — Maj - Mai 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	0	2.4	,1	-	
2	0	0.0	pł.	-	
3	6	8.7	pł.	-	
4	0	2.6	2	-	
5	8	.	pł.	-	
6	8	28.9	pł.	-	
7	7	4.2	pł.	-	
8	8	0.9	pł.	-	
9	8	6.5	pł.	-	
10	0	15.6	6	-	
11	6	21.8	20	-	
12	0	1.0	47	-	
13	8	0.6	50	-	
14	0	12.8	48	-	
15	0	1.3	58	-	
16	7	0.7	57	-	
17	0	(35.9)	55	-	
18	0	1.6	92	-	
19	7	0.0	86	-	
20	8	0.0	81	-	
21	0	9.0	79	-	
22	0	9.0	74	-	
23	8	.	72	-	
24	8	.	63	-	
25	7	.	53	-	
26	7	0.0	45	-	
27	7	1.0	35	-	
28	8	1.7	pł.	-	
29	8	15.6	pł.	-	
30	7	4.1	pł.	-	
31	8	.	pł.	-	
Σ	—	185.9	—	-	UWAGI.

Czerwiec - Juin

1	8	.	pł.	-	
2	6	16.9	pł.	-	
3	5	2.0	pł.	-	
4	1	5.6	pł.	-	
5	0	5.7	pł.	-	
6	7	5.6	pł.	-	
7	8	10.8	pł.	-	
8	8	0.8	pł.	-	
9	8	13.9	pł.	-	
10	8	2.6	pł.	-	
11	7	15.6	.	-	
12	6	15.7	.	-	
13	9	18.9	.	-	
14	8	4.3	.	-	
15	7	0.0	.	-	
16	8	.	.	-	
17	7	.	.	-	
18	8	.	.	-	
19	8	2.2	.	-	
20	8	.	.	-	
21	8	.	.	-	
22	8	19.0	.	-	
23	7	0.7	.	-	
24	8	.	.	-	
25	8	.	.	-	
26	8	.	.	-	
27	8	18.6	.	-	
28	0	3.4	.	-	
29	8	.	.	-	
30	8	.	.	-	
31					
Σ	—	162.3	—	-	UWAGI.

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Lipiec – Juillet 1961

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N.w			KIERUNEK i PRĘDKOŚĆ WIATRU D.v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	110.2	111.1	110.4	110.6	9.9	13.3	8.8	10.2	15.1	6.0	58	56	93	69	5.1	6.7	0.8	4.2	1 ⊙	3 ⊙	5	NE 3	NNE 3	NE 3
2	109.5	110.2	110.0	109.9	9.1	15.0	12.1	12.1	16.5	7.1	70	55	61	62	3.4	7.5	5.4	5.4	1 ⊙	4 ⊙	1	NE 3	NNE 2	C 0
3	109.1	108.8	107.2	108.4	11.6	16.6	12.8	13.4	18.5	10.7	52	46	73	57	6.5	10.4	4.0	7.0	1 ⊙	2 ⊙	3	C 0	N 3	NW 4
4	104.7	103.0	100.0	102.6	12.1	16.1	11.9	13.0	17.4	10.7	56	54	63	58	6.2	8.4	5.1	6.6	1 ⊙	8	10 (R)	NW 3	SW 3	SSW 8
5	98.8	98.9	99.5	99.1	3.1	3.3	0.8	2.0	11.9	0.6	87	97	100	95	1.0	0.2	0.0	0.4	9 ⊙	10 •	8	WNW 3	SW 5	NW 2
6	99.6	101.3	103.3	101.4	0.0	1.9	0.2	0.6	3.0	-1.3	78	71	87	79	1.4	2.0	0.8	1.4	6 ⊙	8	2	WNW 4	NNW 3	NW 3
7	103.2	104.2	104.0	103.8	0.5	3.0	2.2	2.0	5.1	-1.5	75	82	100	86	1.6	1.4	0.0	1.0	3 ⊙	10	10 =	NNE 1	NNW 1	WSW 1
8	103.2	103.8	102.6	103.2	1.5	5.0	4.2	3.7	6.4	0.8	98	89	89	92	0.1	0.9	0.8	0.6	5 ⊙	10	7	S 1	C 0	SW 2
9	98.9	97.6	97.5	98.0	3.8	6.2	1.9	3.4	8.4	1.6	82	64	100	82	1.4	3.4	0.0	1.6	4 ⊙	10	10•Δ=	SW 5	SW 6	NNE 7
10	97.6	98.8	98.9	98.4	1.1	4.6	3.2	3.0	5.9	0.6	100	83	100	94	0.0	1.5	0.0	0.5	10	9	10 •	NNW 5	WSW 6	NW 7
11	100.1	101.8	102.4	101.4	1.0	6.8	7.1	5.5	9.0	-1.0	71	77	77	75	2.0	2.3	2.3	2.2	4 ⊙	9	1	WNW 8	WSW 2	WSW 4
12	100.4	100.2	98.7	99.8	7.5	11.0	9.1	9.2	13.7	6.0	97	76	100	91	0.3	3.1	0.0	1.1	9	7 ⊙	10 =	S 10	SSW 6	S 5
13	93.1	92.5	89.6	91.7	8.0	9.9	5.9	7.4	13.0	4.5	99	94	100	98	0.1	0.7	0.0	0.3	9	8	10 =	S 13	S 13	SW 8
14	93.1	95.1	97.6	95.3	1.9	3.0	3.4	2.9	5.9	0.4	100	70	63	78	0.0	2.3	2.9	1.7	10 • =	7 ⊙	2	WNW 7	WNW 8	SW 7
15	98.7	101.0	100.6	100.1	5.3	9.0	7.7	7.4	10.2	2.9	82	83	97	87	1.6	2.0	0.4	1.3	7 ⊙	9	9	SW 11	SSW 2	SSW 6
16	95.4	98.2	97.6	97.1	5.7	9.5	5.3	6.4	11.3	5.1	98	90	95	94	0.2	1.2	0.5	0.6	9	6 ⊙	9	SW 12	SSW 5	NNE 2
17	95.9	96.3	95.7	96.0	4.6	6.2	3.2	4.3	8.3	2.8	80	84	73	79	1.7	1.5	2.1	1.8	4 ⊙	9 •	5	C 0	SW 7	WNW 5
18	94.5	95.2	95.5	95.1	1.6	5.0	3.9	3.6	6.7	0.2	93	83	100	92	0.6	1.4	0.0	0.7	7 ⊙	9 •	10 =	NNW 5	NNE 1	WSW 2
19	95.0	95.5	96.6	95.7	3.0	4.0	4.0	3.8	5.4	1.3	96	87	94	92	0.3	1.0	0.4	0.6	8	8	8	S 3	W 3	SW 6
20	96.9	96.9	97.9	97.2	4.5	5.0	2.8	3.8	5.1	2.0	96	100	100	99	0.3	0.0	0.0	0.1	9	10 • =	10 =	SW 3	WSW 2	WNW 8
21	98.8	99.9	99.4	99.4	2.4	3.7	3.6	3.3	6.1	1.4	100	100	96	99	0.0	0.0	0.3	0.1	9 ⊙	9 • ☽	9	NNW 4	W 6	WNW 7
22	98.4	99.3	99.5	99.1	2.4	4.7	3.7	3.6	6.3	1.8	98	95	100	98	0.2	0.4	0.0	0.2	10	9	10 • =	WNW 7	SSE 2	NNE 5
23	99.7	101.0	102.4	101.0	4.0	5.9	5.1	5.0	7.4	2.7	84	100	100	95	1.3	0.0	0.0	0.4	2 ⊙	10	10 • =	SSW 3	WSW 1	N 4
24	103.0	104.4	105.8	104.4	2.7	3.7	2.7	3.0	5.1	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 • ☽ =	10	10 =	NNE 4	WNW 1	C 0
25	105.7	106.9	106.2	106.3	1.8	3.3	3.2	2.9	4.7	1.3	98	96	98	97	0.2	0.3	0.2	0.2	5 ⊙	9	10 =	WSW 2	WNW 2	SW 7
26	104.7	105.3	105.5	104.5	-0.3	8.4	7.7	5.9	9.1	-0.9	98	73	59	77	0.2	3.0	4.3	2.5	7 ⊙	5	3	NE 2	NNE 2	W 7
27	101.3	101.4	100.4	101.0	7.7	13.4	10.7	10.6	14.9	6.7	78	57	64	66	2.3	6.6	4.6	4.5	1 ⊙	8 ⊙	6	SW 5	S 6	SSW11
28	98.4	97.5	95.8	97.2	10.6	12.1	10.7	11.0	13.4	8.7	65	62	84	70	4.5	5.3	2.1	4.0	8 ⊙	7	10 •	SSW 9	WSW11	SW 9
29	94.4	97.4	98.3	96.7	6.7	3.6	0.6	2.9	10.8	0.2	100	100	100	100	0.0	0.0	0.0	0.0	10 •	10 • =	10 ☀ =	WNW 3	NNE 4	NNE 8
30	96.0	97.5	98.4	97.3	-0.1	0.2	0.0	0.0	0.9	-1.1	100	100	100	100	0.0	0.0	0.0	0.0	10 * =	10 * =	10 ☀ =	NNE11	NNE10	NNE 4
31	98.0	100.7	102.9	100.5	1.0	2.6	1.9	1.8	3.0	-0.2	100	100	98	99	0.0	0.0	0.1	0.0	10 • =	10	10	WNW 5	WNW 2	NW 6
M	99.9	100.7	100.6	100.4	4.3	7.0	5.2	5.4	9.0	2.6	87	81	89	86	1.4	2.4	1.2	1.7	6.4	8.2	7.7	5.0	4.1	5.1

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1	102.6	103.8	104.3	103.6	2.1	5.6	5.6	4.7	8.3	1.1	96	77	80	84	0.3	2.0	1.8	1.4	9 ⊙	6 ⊙	1	SSW 6	SW 7	SW 6
2	103.3	103.5	103.1	103.3	7.6	12.5	9.7	9.9	13.5	4.1	40	76	88	68	6.2	3.5	1.5	3.7	1 ⊙	7 ⊙	3	SSW 5	NW 2	C 0
3	102.5	103.2	104.4	103.4	7.8	8.0	5.2	6.6	10.0	4.9	94	97	100	97	0.7	0.3	0.0	0.3	9	10 •	10 • =	C 0	C 0	NNE 3
4	103.9	104.0	104.4	104.1	4.7	5.6	4.8	5.0	6.9	2.0	100	98	98	99	0.0	0.2	0.1	0.1	5 ⊙	9	9	S 1	WSW 5	WSW 1
5	104.3	105.4	105.3	105.0	5.6	8.6	9.5	8.3	11.1	3.8	96	83	76	85	0.3	2.0	2.8	1.7	9	9	1	WSW 4	NW 6	WSW 5
6	104.8	105.5	104.8	105.0	10.2	14.6	13.1	12.8	16.8	8.5	77	65	67	70	2.8	5.9	4.9	4.5	1 ⊙	4 ⊙	2	SSW 5	WSW 6	SSW 7
7	102.7	103.8	104.8	103.8	10.8	15.2	12.2	12.6	17.0	9.4	73	64	83	73	3.5	6.4	2.4	4.1	4 ⊙	3 ⊙	7	SSW10	SW 6	SSW 1
8	104.2	105.5	106.8	105.5	10.4	14.4	12.8	12.6	15.4	9.7	100	79	89	89	0.0	3.5	1.6	1.7	10 =	8	1	SW 7	WSW 6	SW 4
9	108.1	109.6	109.1	108.9	13.2	15.6	14.3	14.4	17.4	11.9	69	78	83	77	4.6	3.9	2.9	3.8	7 ⊙	8	8 (R)	SW 4	WNW 1	SSW 6
10	108.6	109.1	107.0	108.2	14.2	16.8	15.0	15.2	18.5	13.1	83	65	80	76	2.9	6.7	3.3	4.3	5 ⊙	5 ⊙	1	S 6	WSW 6	S 12
11	105.1	104.5	105.4	105.0	14.8	18.0	14.9	15.6	18.8	13.7	67	47	35	50	5.6	10.7	10.9	9.1	1 ⊙	4 ⊙	1	S 14	SW 14	WSW 7
12	103.8	102.7	101.5	102.7	11.6	13.1	9.7	11.0	14.9	8.5	57	88	100	82	3.7	1.7	0.0	2.5	10	9	10 • =	S 4	WSW10	NNE 1
13	99.7	101.7	103.8	101.7	4.1	2.6	0.7	2.0	9.9	0.1	100	100	100	100	0.0	0.0	0.0	0.0	10 • ☽ =	10 ☔ =	10 =	NNE 6	NNE 7	NNE 5
14	103.1	103.7	102.9	103.2	3.5	5.2	3.2	3.8	7.0	-1.1	51	88	97	79	3.8	1.0	0.3	1.7	1 ⊙	8 ⊙	7	S 2	SW 3	SSW 1
15	101.2	100.4	99.3	100.3	3.5	6.9	4.2	4.7	8.1	2.4	79	65	82	75	1.6	3.4	1.5	2.2	3 ⊙	8	9	WNW 2	WSW 6	WSW 7
16	97.2	96.7	95.9	96.6	3.2	3.4	0.1	1.7	5.2	-0.2	91	98	98	96	0.7	0.1	0.2	0.3	9	10	10	SSW 5	SSW 4	NNW 8
17	93.2	92.5	92.4	92.7	-0.1	3.0	1.1	1.3	4.9	-1.4	92	96	100	96	0.6	0.3	0.0	0.3	8	10 =	10•Δ=	S 4	NE 1	NNE 5
18	92.1	93.7	94.9	93.6	0.1	0.1	0.7	0.4	1.3	-0.6	100	100	100	100	0.0	0.0	0.0	0.0	10•Δ=	10 ☆ =	10 ☀ =	NNE 8	NNE 8	NNE 6
19	94.9	95.6	95.8	95.4	1.4	3.2	4.9	3.6	5.1	-0.5	93	100	96	96	0.6	0.0	0.4	0.3	9	9	9 •	W 8	SW 9	WSW10
20	95.1	96.0	98.9	96.7	4.9	2.6	1.4	2.6	5.5	0.9	63	100	89	84	3.3	0.0	0.8	1.4	10	10 • =	9	WSW10	W 5	NNW 8
21	100.6	101.9	101.7	101.4	2.5	5.9	3.5	3.8	6.8	0.7	77	76	98	84	1.7	2.2	0.1	1.3	9	8	1	WNW 8	W 5	SSW 9
22	100.3	99.4	98.1	99.3	6.4	7.6	7.4	7.2	9.6	3.5	70	82	86	79	2.8	1.8	1.4	2.0	3 ⊙	8	9 (R)	SW 8	SW 16	SW 7
23	96.4	97.5	99.0	97.6	1.7	1.6	0.0	0.8	7.4	-0.4	91	100	100	97	0.7	0.0	0.0	0.2	9	10 • =	10Δ☔=	WNW 6	WNW 6	NNE 9
24	99.4	100.9	102.4	100.9	-0.4	0.1	2.3	1.1	2.5	-1.6	100	100	100	100	0.0	0.0	0.0	0.0	10 Δ =	10	10 =	NNW 8	NNE 8	NNW 6
25	102.1	103.5	104.9	103.5	2.4	3.4	4.5	3.7	5.0	1.9	100	92	100	97	0.0	0.6	0.0	0.2	10 ☽ =	10	10 =	WSW 3	WSW 5	NW 9
26	105.7	107.5	108.2	107.1	4.8	6.7	5.9	5.8	8.4	1.5	88	91	100	93	1.0	0.9	0.0	0.6	8	8	7	WNW 7	NW 5	NW 5
27	108.9	110.3	110.7	110.0	6.8	10.4	8.7	8.6	11.2	5.7	77	64	97	79	2.3	4.5	0.5	2.4	4 ⊙	6 ⊙	6	NNW 3	NNW 3	NW 3
28	110.6	111.8	111.1	111.2	8.1	11.6	6.8	8.3	12.4	6.8	97	81	99	92	0.4	2.6	0.2	1.1	6	8	10 =	NNE 2	NNE 2	NNE 4
29	109.7	110.0	108.1	109.3	7.0	10.4	5.9	7.3	11.2	4.2	61	56	98	72	3.9	5.9	0.2	3.3	2 ⊙	7 ⊙	7	NE 9	NNE 4	NNE 6
30	106.7	108.5	108.8	108.0	5.6	8.7	4.7	5.9	10.1	4.0	70	75	86	76	2.6	3.0	1.1	2.2	3 ⊙	4 ⊙	0	NNE 6	NNE 5	NE 4
31	109.1	111.2	112.3	110.9	6.8	9.3	5.3	6.7	9.4	3.2	20	65	92	59	7.9	4.0	0.7	4.2	0 ⊙	1 ⊙	1	NE 6	NNE 5	NE 6
M	102.6	103.3	103.6	103.2	6.0	8.1	6.4	6.7	10.0	3.9	80	82	90	84	2.1	2.5	1.3	2.0	6.3	7.6	6.4	5.7	5.6	5.5

Kasprowy Wierch — $H_s = 1991\ m$ — $H_b = 1988{,}8\ m$ — $h_w = 15{,}4\ m$ — Lipiec – Juillet 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	8	.	.	–	
2	8	.	.	–	
3	8	.	.	–	
4	8	4.1	.	–	
5	7	1.7	.	–	
6	8	0.0	.	–	
7	8	.	.	–	
8	7	.	.	–	
9	8	1.8	.	–	
10	7	4.2	.	–	
11	8	.	.	–	
12	8	.	.	–	
13	7	16.1	.	–	
14	9	0.3	.	–	
15	9	10.0	.	–	
16	8	3.6	.	–	
17	9	0.3	.	–	
18	7	2.6	.	–	
19	8	6.1	.	–	
20	0	14.4	.	–	
21	7	2.0	.	–	
22	8	0.7	.	–	
23	7	7.6	.	–	
24	5	0.3	.	–	
25	7	.	.	–	
26	8	.	.	–	
27	8	0.2	.	–	
28	8	4.6	.	–	
29	0	44.3	.	–	
30	0	43.4	5	–	
31	8	0.5	10	–	
Σ	–	168.8	–	–	UWAGI:

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1	8	.	5	–	
2	8	.	.	–	
3	7	8.3	.	–	
4	7	.	.	–	
5	8	.	.	–	
6	9	.	.	–	
7	8	.	.	–	
8	8	.	.	–	
9	8	0.0	.	–	
10	8	.	.	–	
11	9	0.2	.	–	
12	8	22.0	.	–	
13	0	24.2	.	–	
14	8	.	.	–	
15	8	.	.	–	
16	7	3.2	.	–	
17	1	6.5	.	–	
18	0	9.8	1	–	
19	7	2.9	.	–	
20	0	3.6	.	–	
21	8	.	.	–	
22	9	5.4	.	–	
23	0	12.4	.	–	
24	6	1.8	2	–	
25	8	0.5	pż.	–	
26	8	.	.	–	
27	8	.	.	–	
28	8	.	.	–	
29	8	.	.	–	
30	9	.	.	–	
31	9	.	.	–	
Σ	–	100.8	–	–	UWAGI:

Kasprowy Wierch $\varphi = 49°14'$ $\lambda = 19°59'$ **Wrzesień – Septembre 1961**

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE i POGODA N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	113.0	114.4	113.3	113.6	9.4	13.1	10.7	11.0	14.5	4.9	55	72	60	62	5.3	4.2	5.2	4.9	1 ⊙	2 ⊙	1	ENE 7	E 2	W 1
2	111.4	111.1	108.9	110.5	11.1	10.3	9.9	10.3	13.6	8.9	49	62	55	56	6.6	4.7	5.5	5.6	0 ⊙	7 •	0	NE 1	SW 1	SSW 4
3	105.6	105.4	103.6	104.9	8.6	11.4	8.4	9.2	12.6	7.9	61	54	66	60	4.3	6.1	3.6	4.7	0 ⊙	3 ⊙	0	S 5	WSW 6	SSW 8
4	102.2	103.0	103.6	102.9	9.3	11.4	8.7	9.5	12.1	7.4	53	70	71	65	5.5	4.0	3.3	4.3	9 •	9	1	WNW 9	NW 4	N 2
5	102.6	103.2	100.8	102.2	9.5	13.7	9.9	10.8	14.9	7.9	39	66	83	63	7.4	5.4	2.2	5.0	2 ⊙	8	2	WSW 2	WSW 2	SSW 10
6	95.8	98.0	97.9	97.2	8.9	9.7	7.4	8.4	10.6	7.4	79	84	90	84	2.4	2.0	1.0	1.8	4 ⊙	8	3	SW 16	SW 15	SSW 9
7	96.3	97.4	97.8	97.2	6.9	9.6	5.4	6.8	11.1	4.8	73	73	89	78	2.7	3.2	1.0	2.3	9 ⊙	9	10	SW 7	S 3	WNW 9
8	96.0	96.9	97.8	96.9	1.6	3.7	0.9	1.8	5.4	0.3	38	62	100	67	4.4	3.1	0.0	2.5	7 ⊙	4 ⊙	10 =	WNW 9	WSW 6	WNW 9
9	98.4	100.0	100.4	99.6	1.2	1.6	1.8	1.6	1.9	0.3	100	100	100	100	0.0	0.0	0.0	0.0	10 • =	10 9 =	10 =	NNE 6	NW 6	N 6
10	99.5	100.4	100.8	100.2	-0.8	0.1	-0.1	-0.2	1.8	-1.4	99	100	100	100	0.0	0.0	0.0	0.0	10 =	10 • =	10 9 =	N 6	NNE 3	N 2
11	100.2	100.9	100.4	100.5	-0.7	2.4	1.4	1.1	2.9	-1.2	99	100	100	100	0.0	0.0	0.0	0.0	10 =	10 =	8	N 2	WSW 2	SSW 7
12	99.8	101.2	101.1	100.7	5.4	7.8	4.6	5.6	9.1	0.3	16	65	82	54	7.6	3.7	1.6	4.3	1 ⊙	6 ⊙	10	W 4	WSW 1	W 6
13	100.6	102.3	102.5	101.9	3.2	6.5	4.4	4.6	8.0	2.1	82	71	89	81	1.5	2.8	0.9	1.7	9	7 ⊙	1	WNW 4	NNW 2	SSW 10
14	102.3	103.5	102.5	102.8	8.0	11.6	9.3	9.6	13.1	4.5	61	64	85	70	4.1	4.8	1.8	3.6	7 ⊙	8	10	SSW 11	WNW 7	W 10
15	101.9	104.3	106.0	104.1	3.5	5.2	2.4	3.4	10.4	2.0	98	49	100	82	0.1	5.5	0.0	1.9	9	3 ⊙	10 =	NNW 10	NW 8	NNE 5
16	107.8	109.5	109.9	109.1	6.0	11.8	12.9	10.9	13.7	1.8	95	66	25	61	0.5	4.7	11.4	5.5	8	1 ⊙	1	NE 6	NNE 4	NE 3
17	110.9	112.2	112.2	111.8	14.4	16.3	13.7	14.5	17.1	12.9	28	30	37	32	11.9	12.9	9.9	11.6	1 ⊙	0 ⊙	0	C 0	WSW 5	SSW 6
18	110.8	111.4	110.5	110.9	15.6	17.4	13.6	14.6	18.4	11.4	24	24	29	26	12.0	15.1	11.1	12.7	2 ⊙	3 ⊙	1	SSW 9	SW 6	W 1
19	108.6	108.2	106.6	107.8	10.5	12.7	9.8	10.7	15.4	7.8	57	93	67	72	5.5	1.1	4.0	3.5	1 ⊙	10 =	1	NNW 2	NNE 3	NNW 3
20	104.5	105.7	105.1	105.1	9.5	10.7	7.1	8.6	11.4	6.8	4	54	71	43	11.4	6.0	2.9	6.8	0 ⊙	1 ⊙	1	ENE 5	ESE 1	NNE 1
21	104.3	106.0	106.8	105.7	6.7	10.7	6.7	7.7	11.5	5.1	21	59	9	30	7.8	5.2	9.0	7.3	0 ⊙	0 ⊙	0	NE 4	SE 2	NE 4
22	107.7	109.1	109.3	108.7	8.3	10.5	7.6	8.5	11.7	6.6	4	28	11	14	10.5	9.0	8.4	9.3	0 ⊙	0 ⊙	0	ENE 3	ESE 2	ENE 3
23	108.2	108.7	109.0	108.3	7.8	10.5	5.5	7.3	11.8	5.3	0	49	45	31	10.6	6.5	4.9	7.3	1 ⊙	4 ⊙	0	NE 3	SW 2	SSW 1
24	106.4	107.3	107.0	106.9	6.2	8.6	4.4	5.9	9.5	4.3	17	42	75	45	7.9	6.6	2.2	5.6	0 ⊙	0 ⊙	0	S 3	SW 3	C 0
25	106.2	107.5	108.1	107.3	3.5	9.4	6.1	6.3	10.8	2.7	59	50	46	52	3.1	5.9	5.0	4.7	0 ⊙	1 ⊙	3	SSW 5	NW 2	N 3
26	107.4	107.4	105.0	106.6	6.5	8.9	5.6	6.6	9.1	5.5	89	75	97	87	1.1	2.9	0.3	1.4	10	7	10	WNW 5	WNW 4	SW 7
27	102.9	102.8	102.4	102.7	5.0	6.8	4.2	5.0	8.5	3.7	81	90	100	90	1.6	1.0	0.0	0.9	7 ⊙	8	10 =	WSW 2	NW 3	SW 3
28	102.6	104.2	105.1	104.0	4.8	8.7	6.1	6.4	9.2	3.5	42	65	58	55	5.0	3.8	5.9	4.2	1 ⊙	1 ⊙	1	NNE 4	NW 1	NNW 3
29	105.2	106.0	105.9	105.7	5.9	10.5	8.1	8.2	10.8	4.4	100	83	94	92	0.0	2.2	0.7	1.0	7	5 ⊙	7 (R)	N 3	NW 3	NNW 3
30	105.2	104.6	103.2	104.3	8.1	9.9	9.8	9.4	10.3	7.2	94	67	57	73	0.7	4.0	5.0	3.2	9	10 •	10	NNE 1	NW 2	NNW 1
31																								
M	104.2	105.1	104.8	104.7	6.7	9.4	6.9	7.5	10.7	4.8	57	66	70	64	4.7	4.5	5.5	4.2	4.5	5.2	4.4	5.1	3.6	4.7

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1	100.7	100.7	101.7	101.0	7.4	7.6	4.7	6.1	9.8	3.4	100	58	24	61	0.0	4.4	6.5	3.6	10	3 ⊙	0	NNE 3	E 4	ESE 2
2	102.8	104.7	106.0	104.5	6.7	7.1	2.0	4.4	8.9	1.2	27	74	81	61	7.2	2.6	1.4	3.7	1 ⊙	1 ⊙	0	C 0	SW 1	SSW 4
3	105.6	106.4	106.2	106.1	2.4	4.9	1.5	2.6	6.9	0.2	66	67	80	71	2.6	2.9	1.4	2.3	1 ⊙	1 ⊙	0	SSE 4	WSW 6	SSW 9
4	105.7	106.4	106.1	106.1	1.0	5.4	1.7	2.4	6.3	-1.4	65	64	81	70	2.3	3.2	1.3	2.3	1 ⊙	3 ⊙	5	S 8	SW 5	SSW 12
5	106.5	107.4	107.8	107.2	2.8	4.0	2.6	3.0	5.0	1.0	94	89	96	93	0.5	0.9	0.3	0.6	8 ⊙	7	1	SSW 9	WSW 7	SSW 7
6	106.3	105.7	102.1	104.7	2.3	4.3	1.5	2.4	5.9	0.8	82	70	88	80	1.3	2.5	0.8	1.5	2 ⊙	2 ⊙	1	S 2	WSW 6	SW 12
7	97.2	96.7	96.3	96.7	0.8	3.7	3.0	2.6	5.0	0.0	88	76	87	84	0.8	2.0	1.0	1.3	4	6 ⊙	6	SW 16	SSW 13	SSW 11
8	95.2	96.6	98.8	96.9	3.2	8.1	5.3	5.5	8.5	1.7	94	68	75	79	0.4	3.4	2.2	2.0	9	8 ⊙	4	S 16	S 7	SSW 9
9	103.7	106.7	109.0	106.5	3.4	7.0	3.7	4.4	7.4	2.1	88	86	97	90	0.9	1.4	0.3	0.9	8	9	3	C 0	SSW 2	NNE 4
10	110.0	111.2	110.7	110.6	5.1	8.6	6.5	6.7	9.3	2.1	29	72	18	40	6.3	3.2	8.0	5.8	3 ⊙	2 ⊙	0	NE 3	WSW 1	NE 2
11	109.3	109.7	109.1	109.4	6.8	8.7	5.6	6.7	9.5	4.7	22	60	75	52	7.8	4.4	2.2	4.8	1 ⊙	1 ⊙	0	S 2	SW 4	ESE 1
12	107.7	107.8	107.0	107.5	4.1	5.1	3.0	3.8	6.5	2.8	77	100	100	92	2.0	0.0	0.0	0.7	1 ⊙	10 =	10 =	NE 3	N 1	NNE 7
13	105.3	105.7	105.4	105.5	0.3	0.9	-2.9	-1.2	3.0	-3.5	100	100	97	99	0.0	0.0	0.1	0.0	10 • =	10 9 =	10 =	NNE 6	NNE 3	NNE 8
14	103.9	104.0	102.9	103.6	-4.2	-2.8	-2.8	-3.2	-2.4	-5.1	96	97	97	97	0.2	0.1	0.1	0.1	10 =	10 △ =	10 △ =	NNE 7	NNE 5	NNE 7
15	103.9	104.7	104.3	104.3	-0.7	0.6	4.0	2.0	4.7	-5.2	99	96	41	79	0.0	0.3	4.7	1.7	10 • 9 =	9 ⊙	1	NNE 8	SSW 1	WNW 5
16	103.0	103.1	101.5	102.5	4.3	6.5	4.6	5.0	7.0	3.1	45	43	45	44	4.5	5.7	4.7	5.0	0 ⊙	4 ⊙	5	NW 6	WNW 3	SSW 4
17	99.2	96.3	88.9	94.8	3.4	4.0	1.5	2.6	5.4	1.0	56	82	100	79	3.4	1.5	0.0	1.6	8 ⊙	8	10	SW 2	SW 9	SSW 18
18	80.2	78.8	79.6	79.5	1.3	1.4	2.9	2.1	3.0	0.6	100	100	100	100	0.0	0.0	0.0	0.0	10 * =	10 • =	10 =	SSW 24	SSW 22	SE 19
19	83.3	85.7	87.5	85.5	4.1	4.7	5.2	4.8	6.8	2.9	100	100	95	98	0.0	0.0	0.4	0.1	10 • 9 =	10 •	10	SSW 16	SSW 17	SSW 23
20	91.7	93.1	93.4	92.7	4.3	5.2	5.2	5.0	6.9	3.8	93	82	83	86	0.6	1.6	1.4	1.2	10	9	10 •	S 14	SSE 10	SSE 16
21	92.0	94.9	99.4	95.4	0.8	-2.2	-2.0	-1.4	5.4	-5.5	72	96	77	82	1.8	0.2	1.5	1.1	8	6	2	SE 14	S 14	SSW 8
22	101.3	102.7	103.1	102.4	0.8	1.7	0.7	1.0	3.1	-2.9	54	98	96	83	3.0	0.1	0.3	1.1	10	10	4	SSE 1	W 1	SSW 5
23	104.6	104.9	105.5	105.0	0.3	0.2	-0.2	0.0	1.2	-0.8	100	100	100	100	0.0	0.0	0.0	0.0	10 * =	10 * =	10 =	S 4	SSW 9	S 9
24	106.0	107.0	105.9	106.3	-1.2	0.5	4.1	1.9	4.4	-1.9	99	100	40	80	0.1	0.0	4.9	1.7	10 =	5	1	S 10	S 7	S 8
25	103.7	104.3	104.5	104.2	4.6	6.7	7.1	6.4	7.5	1.1	39	41	13	31	5.2	5.8	8.7	6.6	1 ⊙	8 ⊙	9	S 12	S 11	S 6
26	102.0	101.4	101.6	101.7	5.4	4.0	6.1	5.4	8.1	4.0	3	41	30	25	8.7	4.7	6.6	6.7	7	9	7	SSE 12	SSE 8	SSE 11
27	98.8	99.0	97.9	98.6	3.5	6.1	4.5	4.6	7.1	2.5	70	72	90	77	2.3	2.6	0.8	1.9	9	9 ⊙	6	SSE 9	SSW 12	SSW 16
28	98.4	99.1	97.8	98.4	3.9	8.7	6.8	6.6	8.8	2.9	96	61	53	70	0.3	4.3	4.6	3.1	6	1 ⊙	0	S 12	S 11	SSE 7
29	96.2	95.9	96.6	96.2	3.8	3.4	1.1	2.4	7.5	0.6	84	100	91	92	1.3	0.0	0.6	0.6	9	10 •	2	S 7	SW 4	SW 4
30	97.2	97.3	96.4	97.0	0.0	0.2	-0.8	-0.4	1.3	-1.4	81	100	99	93	1.1	0.0	0.0	0.4	7	10 =	10 * △ =	SSW 5	SW 2	W 2
31	97.7	100.6	102.6	100.3	-2.4	-2.0	-1.8	-2.0	-0.8	-3.2	98	100	85	94	0.1	0.0	1.2	0.4	10 * =	2 ⊙	8	NNE 2	N 1	NW 10
M	100.6	101.2	101.1	101.0	2.5	3.9	2.7	3.0	5.7	0.5	75	80	73	77	2.1	1.9	2.1	2.0	6.6	6.5	4.9	7.6	6.7	8.6

Kasprowy Wierch — $H_s = 1991\,m$ — $H_b = 1988{,}8\,m$ — $h_w = 15{,}4\,m$ — Wrzesień – Septembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	.	.	–	(m) na–a., ○ na–p., ( ) 0^{00}–20^{00}
2	9	3.4	.	–	●^{0}12$^{35-45}$ ▲$^{0-1}$13^{05}–14^{00} 14^{24}–15^{05} 16$^{08-43}$ (K)^{0}14^{02} SW (pojed. grzmot) K^{0}16^{35}–17^{15} W-NW; Σ^{0}p., ( )7^{45}–14^{40}, 17^{20}–19^{30}
3	9	0.0	.	–	(m) na–9^{30}, ○ na–p., ( ) 6^{30}–24
4	8	0.3	.	–	●^{0}7^{12} 9^{25} ◠^{0}23^{00}–24 ○ a..p. ⊕12^{40} 13^{30}, ( )^{00}–8^{00}
5	7	.	.	–	◠^{0}0^{00}–6^{00}, ≫10^{35}–24 (por. 22), ○ na..p
6	8	6.0	.	–	●$^{0-1}$16^{32}–17^{20}, ≡ 16^{50}–18^{20} ≡^{2}–19^{20}, ≫ ◝^{00}–10^{45}, 13^{20}–15^{40}, 22^{35}–24 (por. 27), Σ^{1} 17$^{05-50}$ (K)^{0}17^{30}–18^{15} E, ○ na..p ◯a
7	9	4.2	.	–	●$^{0-1}$0^{35} 1^{30}–20$^{15-25}$ 22^{22}–24, ≡ ≡^{2}0^{25}–4^{40} (m) 4^{30}–9^{40}, ≡ 10^{40}–20^{35}, ≫ 1^{00}–3^{30} 22^{30}–24 (por. 25), ○ na..p., ( )7^{20}–12^{00}
8	9	1.4	.	–	●^{0}0^{00} 1^{50}–23^{35}–24, ≡ ≡^{2}8^{05} 9^{15} 20^{20}–24, ≫ 0^{00}–5^{40} 18^{35}–20^{00} (por. 20), ○ na..p ◎^{0}8^{05}–9^{15}, ( ) 6^{30}–8^{20}
9	0	7.3	.	–	●^{0} $^{0-1}$ ○ ●$^{0-1}$0^{00}–14^{30}, 16^{25}–17^{15}, 19^{30} 21^{20}, ≡ ≡ 0^{00}–24
10	0	3.2	.	–	●$^{0-2}$ ◠ $^{0-1}$ ●^{0}3^{00}–6^{30}, 8^{50}–10^{20}, 13^{30}–24, V^{0} Vᴖ ^{0}–6^{50} 13^{30}–20^{30} 21^{30}–24, ≡^{2}0^{00}–24
11	0	0.0	.	–	◠ ●^{0}0^{00}–4^{20}, 10^{15} 11^{30}, Vᴖ ^{0}V^{0}0^{00}–10^{30}, ≡ ≡ 0^{00}–6^{00}, 18^{14}–19^{20}, 20^{35}–24, m, (m) 16^{10} np., ○ p., ◎^{0}17^{30} 18^{30} ⊕$^{0-1}$18$^{15-50}$
12	8	.	.	–	≡ 0$^{00-20}$ (m) na. ≡ 22^{30}–24, ○ na–p ⊕^{0}6^{40} 7^{15}
13	8	.	.	–	≡ 0$^{00-30}$ 1^{20} 3^{15}, ≫ 21$^{05-45}$, ○ a..p
14	8	5.4	.	–	●^{0}22^{27}–24, ≡ 23^{35}–24, ≫ 1^{45} 9^{20} 11^{35}–24 (por. 19), ○ na..p ⊕^{0}7^{15} 8^{30} 9^{00} 10^{00} 11$^{25-50}$, ◯a
15	8	.	.	–	●^{0}0^{00} 4^{40}, ≡ ≡^{2}0^{00} 8^{35}, 10^{15}–11^{20} 18^{35}–22^{30}, ≫ 0$^{00-30}$ 3^{40} 7^{45} (por. 19), ○ a..p
16	9	.	.	–	◟^{0}0^{15} 1^{00} S., ○ a..p ◡^{0}21^{15}–22^{30}, ( ) 5^{30}–6^{30}, 7^{00}–24
17	9	.	.	–	⊙ na–p., ( ) 1^{00}–24
18	9	.	.	–	≫ 11^{20} 15^{25}, ○ na–p., ( ) 0^{00}–24
19	1	.	.	–	≡ ≡^{2}13^{10} 21^{10} m 16^{45}–24, ○ na–p. ◎$^{1-2}$ 15^{25} 18^{10}, ( )0^{00}–5^{00}
20	9	.	.	–	m 0^{00}–1^{30} (m) 1^{30}–8^{30}, ○ na–p., ( ) 4^{30}–24
21	9	.	.	–	(m) na–a., ○ na–p. zielony promień 18^{36}, ( ) 0^{00}–24
22	9	.	.	–	(m) na–a., ○ na–p.; ( ) 0^{00}–24
23	9	.	.	–	○ na–p. zielony promień 18^{27}, ( ) 0^{00}–15^{30}, 21^{30}–24
24	9	.	.	–	○ na–p., ( ) 0^{00}–15^{00}
25	8	0.4	.	–	○ na–p
26	7	8.7	.	–	●$^{0-1}$5^{46} 7^{25} 18$^{10-25}$ 19^{30} 20^{15} 22^{15}–24, (K)^{0}17^{02} 18^{15}–20^{15} W-NE, NW, ≫ 22^{00} 23^{40}, ○ a..p
27	8	0.0	.	–	●$^{0-1}$0^{02}–3^{10} 16$^{50-55}$, ≡ ≡^{2}11^{15} 22^{30}, ○ na..p ◎ 16$^{45-52}$
28	9	.	.	–	◡^{1}4^{00} 7^{50}, (m) 5^{30}–11^{30}, ○ na–p., ( ) 5^{30}–14^{00}
29	8	.	.	–	≡ ≡^{2}6^{40}–8^{20}, 22^{15} 23^{45}, (K)^{0}21^{19} 23^{30} NE, ○ a..p
30	8	0.3	.	–	●^{0}11^{53}–14^{04}, 17^{36}–19^{05}, ◟^{0}4^{40}–6^{30} NE-E
31					
Σ	–	40.6	–	–	UWAGI.

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1	9	.	.	–	≡ 4^{30}–6^{45} m 6^{50}–10^{50} ≡ 7^{40} 13^{30} (m) 23^{30}–24, ○ a..p ( ) 12^{30}–24
2	9	.	.	–	◡^{0}20^{30}–24, (m) 0^{00}–14^{00}, ○ na–p., ( ) 0^{00}–14^{00}
3	9	.	.	–	◡^{0}0^{00}–6^{00}, 23^{00}–24, m, (m) 3^{30} a., ≫ 21^{05}–24, ○ na–p.; ( ) 8^{30}–12^{15}
4	9	.	.	–	◡$^{0-1}$0^{00} 3^{20} 5^{45} 9^{00} V^{0} 13^{20} 5^{45} ≡ 3^{20} 5^{45} 6$^{05-10}$, ≫ 0^{00} 3^{40} 10^{30}–24, ○ na–p ψ^{1} 3^{20} na. ⊕^{0}16^{00} 17^{20} ◎^{0}6$^{08-20}$, ( )2^{15} 3^{20}, 5^{30} 13^{00}
5	8	.	.	–	◠ 17^{40}–23^{30}, ◡^{1}23^{30}–24, ≡ 19^{15}–20^{35}, ≫ 0^{00} 2^{30}, 7^{30}–8^{45}, ○ na..p
6	8	.	.	–	◡^{1}0^{00}–8^{45}, ≫ 18^{50}–24 (por. 19), ○ na–p
7	8	0.0	.	–	✳^{0}5^{00} 0^{40} ≫ ◝^{00}–24 (por. 28), ○ a..p
8	8	.	.	–	≫ 0^{00} 11^{30} (por. 26), ○ a..p ⊕$^{0-1}$11^{25} 16^{10}
9	8	0.0	.	–	●^{0}10^{15} 11^{15}, 17^{45} 18^{10}, ≡ ≡^{2} 15^{20} 16^{30} 22^{30} 23^{30} m 16^{30}–23^{30}, ◠$^{0-1}$2^{40} 7^{00}, ○ p...
10	9	.	.	–	(m), m 0^{00}–19^{30}, ○ na–p., ( ) 2^{30}–14^{00} 22^{30}–24
11	9	.	.	–	◠$^{0-1}$0^{00} 23^{00} ◡^{0}23^{00}–24 (m) 2^{00} a., ○ na–p., ( ) 0^{00} 13^{15}
12	0	7.4	.	–	●● 23^{45}–24, ◡$^{0-1}$0^{00} 8^{20}, ≡ ≡^{2}8^{05}–24, ○ na–a..p ◎^{1}7^{45} 9^{30}
13	0	4.1	.	–	●● ● $^{0-1}$ ●^{0}0^{00} 15^{30} V^{0} 15^{45}–24, ≡ ≡^{2}0^{00}–24
14	0	12.5	.	–	✳ ◠ △ ◡ ^{0}17^{30} 18^{45} 20^{15}–24, V$^{0-2}$ Vᴖ ^{0}0^{00}–24, ≡ ≡^{2}0^{00}–24
15	7	1.1	1	–	✳^{0} ◠ ^{0} ●^{0}0^{00} 1^{15}, 11^{15}...35 V^{0} 0^{00}–2^{00} ◡^{2} 2^{00} 11^{15}, ≡ ≡^{2} 0^{00} 14^{30} m (m) 12^{04}–24, ○ p., ⊕^{0}12$^{13-36}$ ◎^{2}p. 16^{15}, ( ) 14^{15}–24
16	9	.	1	–	m 1^{00} 11^{10}, ○ na–p ⊕$^{0-1}$12^{00} 15^{20} ◡^{1}20^{10} 21^{15}, ( ) 0^{00}–24
17	8	25.1	pł.	–	●^{0}22^{45}–24, ≡ ≡^{2}17^{30} 18^{45} 20^{30}–24, ≫ 13^{30} 17^{20} 18^{20}–24 (por. 32), ○ na..p ; ( ) 0^{00}–6^{50}
18	0	22.3	.	–	●$^{0-1}$ ✳^{0}0^{00} 10^{45}, ≡ ≡^{2}11^{00}–24, ≫ 0^{00}–24 (por. do 60 m/sek.)
19	7	2.2	.	–	◠ ●$^{0-1}$ 3^{00} 8^{50} 9^{35} 15^{35} 18^{15} 20^{10} 21^{05} 21^{13} 22^{40} 23^{30}, ≡ ≡^{2} 0^{00} 15^{45}, ≫ 0^{00}–24 (por. 40), ◠ ^{1,0}8^{55} 9^{00}, 10$^{15-30}$, 11^{20}–12^{00}, 13^{20} 16^{30}
20	9	6.8	.	–	●^{0}4^{00} 5^{15}, 15^{50} 18^{25}, 19^{00} 23^{15}, ≡ 21^{45} 23^{30}, ≫ 1^{00}–8^{40}, 12^{30} 21^{30} (por. 34), ○ p..., ( ) 10^{20}–14^{20}
21	9	.	.	–	●^{0}2^{30} 3^{50}, ≡ ≡^{2}7^{50} 12^{10}, ≫ 4^{25} 15^{30} (por. 28), V^{0} 11^{45} 12^{10} ◡^{0}20^{00} 22^{30}, ○ a..p ◎^{1}a., ( ) 5^{20}–7^{40}
22	9	1.3	.	–	●^{0}14^{50} 16^{10} ✳^{0} 16^{45} V^{0} 21^{45}–24, ≡ ≡ 12$^{05-30}$ m 18^{30}–21^{45}, ≡ ≡^{2} 21^{45} 22^{30}, ≡ 22^{30}–24, ○ a..., ⊕^{0}7^{30}–8^{30}, ( )7^{00} 23^{45}
23	0	1.8	.	–	●● ✳ ●● ◠ ✳$^{0-1}$ ✳^{0}5^{30} 13^{14} V^{0} 0$^{00-30}$ 16^{25}–24, ≡ ≡^{2} 0^{00}–24
24	9	.	.	–	V$^{0-2}$ 1^{00} 9^{30}, ≡ ≡^{2} 0^{00} 17^{30} m 17^{30}–24, ≫ 0^{15} 7^{30}–22^{25}–24 (por. 17), ○ a..p., ( ) 9^{30} 13^{30}, 16^{20}–24
25	9	.	.	–	m 0^{00} 7^{00}, ≫ 0^{00} 7^{15} 8^{30} 14^{30}, ○ a..p ⊕ ◠a..p ψ^{0}22^{40} 23^{30}, ( ) 0^{00}–24
26	9	.	.	–	≫ 5^{30} 12^{30} 14^{30}–24 (por. 20), ○ a..p ◡^{0}20^{05}–24 ψ^{1}0^{30} 2^{20} 20^{05} 23^{30}, ( ) 0^{00}–24
27	9	.	.	–	≫ ◝^{00}–6^{20} 7^{20} 14^{30}–16^{50}–24 (por. 29), ○ a..p ◡^{1}0^{00} 5^{20} ◯a ψ^{0}20^{00}–24, ( ) 0^{00}–24
28	9	.	.	–	≡ 1^{40} 7^{35} 5^{10} 8^{40}, ≫ ◝^{00}–14^{30} (por. 25), ⊙ a..p ψ ◡^{1}0^{00} na. ◎^{0}7^{30} 8^{10} ◠^{0}18^{20}–22^{30}, ( ) 0^{00}–24
29	7	1.5	.	–	△^{0}7^{42} 8^{10} ●^{0}9^{10} 17^{50}, ≡ ≡^{2}6^{30} 7^{10} 10^{25} 20^{00}, m 20^{20} 22^{40} ≡ 22^{40} 23^{15} ○ a. ψ^{1}22^{40}–23^{25} ( ) 0^{00}–6^{30}
30	1	13.0	.	–	●△ ● ✳△ ●$^{0-1}$ ✳ ^{0}△ ●^{0}15^{40}–24, ◡$^{0-1}$4^{10}–7^{45}, m (m) 2^{40} 10^{40}, ≡ ≡^{2} 10^{40}–15^{30} 16^{35}–24, ○ a...; ( ) 6^{30}–8^{30}
31	9	2.9	15	–	✳△$^{0-1}$, △^{0}0^{00} 10^{45}, V^{0} 1^{30} 11^{11}, ≡ ≡^{2} 0^{00}–10^{22} ≡ 10^{22}–11^{11}, ≫ 20^{30}–24, ✳^{0}20^{15}–24, ○ a..p., ( ) 23^{30}–24
Σ	–	102.0	–	–	UWAGI.

Kasprowy Wierch — φ = 49°14' — λ = 19°59' — Listopad – Novembre 1961

DNI	CIŚNIENIE P = 700 +				TEMPERATURA T						WILGOTNOŚĆ WZGL. U				NIEDOSYT WILGOTNOŚCI Δ				ZACHMURZENIE N,w			KIERUNEK i PRĘDKOŚĆ WIATRU D,v		
	I	II	III	Dies	I	II	III	Dies	Max	Min	I	II	III	Dies	I	II	III	Dies	I	II	III	I	II	III
1	103.6	104.2	104.3	104.0	2.3	2.2	1.8	2.0	4.7	-2.8	65	70	90	75	2.5	2.2	0.7	1.8	8	8 ⊙	10 •	WNW 4	S 11	WSW 4
2	104.2	103.7	101.0	103.0	-2.4	1.8	1.8	0.8	4.2	-5.9	69	58	86	71	1.6	3.0	1.0	1.9	6	3 ⊙	0	NNW 5	SSW 7	SSW15
3	96.5	95.4	94.2	95.4	0.6	2.4	-1.0	0.2	2.8	-2.7	58	46	73	52	4.0	3.9	1.6	3.2	5	6 ⊙	2	SW 17	SW 16	S 6
4	90.9	88.8	87.8	89.2	-2.8	-2.9	-6.1	-4.5	0.2	-6.4	73	97	97	89	1.4	0.1	0.1	0.5	9	10 * △=	10 △ =	SE 5	WSW 9	NNE 8
5	85.4	87.2	92.1	88.2	-2.2	-2.0	-0.1	-1.1	-0.1	-8.2	98	98	86	94	0.1	0.1	0.9	0.4	10 * =	10 △ =	9	SSW 5	SSW 6	SE 3
6	92.0	92.3	92.2	92.2	1.1	3.3	3.4	2.8	5.6	-2.0	88	100	100	96	0.8	0.0	0.0	0.3	9	10 •	10 •	ESE10	SE 5	SSE 8
7	89.0	89.6	90.8	89.8	1.6	0.1	0.0	0.4	3.6	-0.6	100	100	96	99	0.0	0.0	0.5	0.2	10 •	9	10	SSE14	SSE11	SE 2
8	90.2	90.3	90.9	90.5	-1.1	-2.1	-3.5	-2.6	0.0	-3.8	99	98	97	98	0.1	0.1	0.1	0.1	10 * △ =	10 △ =	4	SSE 5	SW 8	SW 4
9	89.3	90.4	90.5	90.1	-4.3	-2.1	-3.5	-3.4	-0.6	-5.6	96	98	97	97	0.2	0.1	0.1	0.1	10 =	7 ⊙	8	SSW12	SSW10	SSW11
10	87.9	88.3	89.4	88.5	-0.5	0.0	0.0	-0.1	0.1	-3.9	100	100	100	100	0.0	0.0	0.0	0.0	10 △ =	10 △ =	10 △ =	SSE16	S 13	SSW14
11	87.5	88.6	90.2	88.7	-0.5	-0.7	-0.6	-0.6	0.1	-1.8	100	99	99	99	0.0	0.0	0.0	0.0	10 △ =	10	10 * =	SSE10	SSW11	SE 2
12	90.5	91.4	92.4	91.4	-2.2	-0.8	-2.0	-1.8	-0.5	-2.7	96	99	89	95	0.2	0.0	0.6	0.3	1	8 ⊙	4	SW 4	SSW10	S 10
13	91.4	90.3	89.6	90.4	0.4	1.5	0.3	0.6	2.6	-2.0	100	100	100	100	0.0	0.0	0.0	0.0	9 •	10	10 * =	SSE12	S 7	SSE 5
14	88.6	91.3	95.0	91.0	-2.1	-0.9	-2.8	-2.2	0.3	-2.9	98	97	100	98	0.1	0.2	0.0	0.1	10 △ =	2 ⊙	10 =	W 7	W 4	N 3
15	92.7	93.9	95.4	94.0	-3.8	-3.9	-2.5	-3.2	-1.6	-5.6	99	96	30	75	0.1	0.2	3.6	1.3	6	5 ⊙	4	NE 4	ENE 2	NE 4
16	96.2	95.3	93.7	95.1	0.3	-0.3	-0.1	0.0	1.5	-3.1	21	47	45	38	4.9	3.2	3.3	3.8	7	9	10	W 3	SSW 4	W 3
17	91.2	90.9	91.4	91.2	-3.7	-7.1	-6.4	-5.9	1.2	-7.8	55	99	97	84	2.1	0.0	0.1	0.7	5	10 △ =	10 △ =	WNW 3	N 5	N 4
18	89.4	89.3	89.7	89.5	-8.0	-8.9	-8.1	-8.3	-6.4	-9.4	96	95	95	95	0.1	0.2	0.2	0.2	10 =	10 △ =	10 △ =	NNW 4	NW 5	N 5
19	90.5	91.9	95.1	92.5	-10.6	-10.4	-11.3	-10.9	-7.9	-11.6	94	94	93	94	0.2	0.2	0.2	0.2	10 △ =	10 * △ =	N 6	NNE 7	NNE 9	
20	97.8	100.9	104.2	101.0	-13.6	-12.5	-13.9	-13.5	-11.3	-14.2	96	96	96	96	0.1	0.1	0.1	0.1	10 * △ =	9 *	10 * =	NNE 8	NNE 7	NNE 7
21	105.9	106.5	105.4	105.9	-9.0	-4.2	-2.6	-4.6	-2.5	-14.2	25	46	58	43	2.0	2.4	2.1	2.2	3	9	10	NE 5	W 3	NNW 6
22	103.3	102.8	101.8	102.6	-3.4	1.6	3.1	1.1	3.4	-4.1	38	29	12	26	2.9	4.9	6.7	4.8	10	7 ⊙	4	N 7	NNE 3	WNW 3
23	98.9	97.7	96.0	97.5	3.3	3.4	4.4	3.9	5.1	2.7	21	18	14	18	6.2	6.4	7.2	6.6	1	1 ⊙	1	S 8	SSW11	WSW 5
24	97.6	98.8	98.9	98.4	0.9	4.0	2.3	2.4	5.5	0.3	19	29	23	24	5.3	5.7	5.5	5.5	8	3 ⊙	7	NNE 4	SSE 2	SSW 8
25	97.1	95.8	95.5	96.1	-1.1	-1.6	-1.5	-1.4	2.4	-2.6	95	98	96	96	0.3	0.1	0.2	0.2	10 =	10 * =	5	SSW10	SW 7	NNW 1
26	95.6	92.1	88.8	91.5	-1.3	-0.7	-1.7	-1.4	-0.6	-2.6	80	99	98	92	1.1	0.0	0.1	0.4	5	9	10 =	W 2	S 8	SSE13
27	86.6	86.2	87.8	86.9	0.4	2.4	1.5	1.4	2.5	-1.7	100	100	100	100	0.0	0.0	0.0	0.0	10 =	10 • =	8	S 17	S 19	WSW13
28	90.6	91.2	93.1	91.6	-1.1	-0.6	-2.7	-1.8	2.8	-3.1	99	89	95	94	0.1	0.6	0.2	0.3	10 =	9 *	9	W 4	WSW 3	SSW 7
29	95.1	95.8	96.1	95.7	-3.3	-3.4	-3.4	-4.4	-2.0	-5.6	92	92	90	91	0.4	0.4	0.4	0.4	9	10	3	W 7	SW 6	SW 5
30	92.9	93.3	91.3	92.5	0.9	0.0	-1.3	-0.4	1.6	-5.4	65	47	58	57	2.3	3.3	2.4	2.7	5	9	4	W 13	W 14	WSW10
31																								
M	93.5	93.8	94.1	93.8	-2.2	-1.4	-2.0	-1.9	0.5	-4.6	77	81	80	79	1.3	1.2	1.3	1.3	7.9	8.1	7.4	7.7	7.8	6.6

Grudzień – Décembre

1	86.1	87.8	89.3	87.7	-2.5	-0.3	-1.2	-1.3	0.1	-5.4	98	98	99	98	0.1	0.2	0.1	0.1	10 =	8 ⊙	10 =	SW 14	W 17	SSW 9
2	87.5	85.4	87.0	86.6	-0.1	0.4	0.1	0.1	0.7	-2.5	100	96	94	97	0.0	0.3	0.4	0.2	10 =	2 ⊙	4	SW 14	SSW13	SW 11
3	90.4	91.5	91.5	91.1	-5.1	-3.1	-4.2	-4.2	0.3	-7.1	30	90	94	71	2.9	0.5	0.3	1.2	2	10	5	WNW 6	SSW12	S 10
4	90.4	93.9	97.4	93.9	-1.7	0.0	-0.3	-0.6	0.5	-4.5	98	100	96	98	0.1	0.0	0.3	0.1	7	7	2	SSW14	W 11	SSW12
5	99.1	98.7	96.4	98.1	3.0	5.7	0.5	2.4	5.7	-0.3	100	63	100	88	0.0	3.4	0.0	1.1	10	3 ⊙	10 =	SSW12	S 14	SSW12
6	93.3	91.1	88.5	91.0	1.1	-3.3	-11.5	-6.3	1.5	-11.8	98	97	97	97	0.1	0.1	0.1	0.1	9	10 △ =	10 * =	SE 3	NNE 5	NNE 7
7	85.0	85.6	88.0	86.2	-11.8	-11.3	-11.2	-11.4	-11.0	-12.0	97	93	93	94	0.1	0.2	0.2	0.2	10 * =	10 * =	10 * =	NE 8	NE 6	NNE 5
8	90.0	90.9	92.3	91.1	-12.0	-12.6	-13.6	-13.0	-10.9	-14.4	97	92	92	94	0.1	0.2	0.2	0.2	10 * =	10 * =	0	NNE 9	NNE 6	NNE 9
9	94.1	95.3	94.5	94.6	-9.7	-6.6	-6.6	-7.4	-6.3	-14.0	43	20	18	27	1.6	2.9	3.0	2.5	2	8 ⊙	1	C 0	SSW 5	SSW12
10	95.4	92.8	92.5	92.9	-5.9	-4.5	-5.8	-4.0	-1.8	-7.0	8	19	94	40	4.2	3.6	0.3	2.7	4	8 ⊙	2	SSW 5	SW 4	W 4
11	90.2	85.2	82.6	86.0	-4.8	-5.5	-2.0	-3.6	-0.6	-5.9	98	97	98	98	0.1	0.1	0.1	0.1	3	10 * △ =	10 * =	SSW 7	SSW15	NW 13
12	84.9	87.2	88.3	86.8	-5.0	-2.6	-5.1	-5.0	-1.8	-5.5	97	98	99	98	0.1	0.1	0.0	0.1	10 * △ =	10 * =	10 * =	NNW11	N 8	WNW 6
13	91.0	92.6	93.1	92.2	-8.6	-12.2	-19.1	-14.8	-3.1	-19.2	98	96	95	96	0.1	0.1	0.1	0.1	10 * △ =	10 * △ =	3	N 9	NNE 8	NE 9
14	92.3	91.5	91.0	91.6	-20.9	-20.5	-24.0	-22.4	-18.9	-24.1	89	89	97	92	0.1	0.1	0.0	0.1	0	1 ⊙	10 * =	NE 12	NNE12	NNE10
15	89.9	87.4	84.8	87.4	-20.9	-18.1	-23.6	-21.6	-16.6	-24.9	96	95	97	96	0.1	0.1	0.0	0.1	10 * △ =	10 △ =	10 △ =	NNE13	N 11	NNE 9
16	87.3	92.5	97.4	92.4	-27.7	-21.2	-18.6	-21.5	-18.4	-28.0	89	96	95	95	0.1	0.0	0.1	0.1	8 △	4 ⊙	1	NNE11	ENE 8	E 6
17	101.7	101.5	100.5	101.2	-17.4	-17.7	-17.4	-17.5	-14.8	-18.8	95	95	95	95	0.1	0.1	0.1	0.1	1	3 ⊙	10 * △ =	ENE 9	NE 11	NNE14
18	101.1	101.6	103.0	101.9	-18.0	-16.0	-10.0	-13.5	-10.0	-18.9	95	100	85	93	0.1	0.0	0.4	0.2	4	9 *	0	NE 11	NNE15	ENE10
19	101.9	101.4	100.6	101.3	-8.3	-10.1	-10.0	-9.6	-8.1	-11.2	95	94	94	94	0.2	0.2	0.2	0.2	10 =	10 △ =	10 =	ENE 8	NE 6	NE 7
20	98.3	95.9	89.5	94.6	-11.5	-10.0	-10.3	-10.5	-5.7	-12.2	79	66	97	81	0.5	1.0	0.1	0.5	6	10	10 * =	NE 7	NNW 4	N 10
21	85.8	85.4	86.3	85.8	-11.0	-12.4	-16.8	-14.2	-9.7	-17.0	97	96	95	96	0.1	0.1	0.1	0.1	10 * =	10 * =	10 * =	NNE12	N 12	N 12
22	85.4	82.3	80.2	82.6	-17.9	-12.0	-13.8	-14.4	-11.2	-18.8	95	95	100	96	0.1	0.2	0.0	0.1	8	10 * =	10 * =	NNW 8	WNW14	N 7
23	81.1	82.6	84.6	82.8	-19.6	-19.4	-19.3	-19.4	-15.8	-20.9	95	95	77	89	0.1	0.1	0.3	0.2	10 * =	4 ⊙	0	NNE 6	NE 8	ENE 6
24	85.5	85.1	84.0	84.9	-19.2	-15.3	-14.8	-15.5	-11.8	-19.7	89	80	65	78	0.1	0.4	0.7	0.4	1	1 ⊙	1	NE 5	C 0	SE 1
25	85.2	85.1	85.1	85.1	-12.4	-9.5	-13.0	-12.0	-8.1	-15.6	50	67	55	51	1.6	1.0	0.9	1.2	1	1 ⊙	0	E 4	ENE 1	SW 1
26	84.0	85.3	82.2	85.2	-10.4	-11.8	-8.5	-9.8	-6.3	-13.3	63	97	63	74	1.0	0.1	1.2	0.8	0	7 ⊙	9	S 7	SSW10	SSW12
27	82.6	84.2	85.2	84.0	-6.5	-4.5	-4.9	-5.2	-3.9	-12.0	97	96	98	97	0.1	0.2	0.1	0.1	10 * =	7 ⊙	9	SSW 7	WSW 2	SSW 4
28	85.2	85.7	87.1	86.0	-4.8	-3.9	-4.0	-4.2	-3.4	-5.4	85	99	91	92	0.6	0.1	0.4	0.4	9 *	7	10	S 8	S 8	S 7
29	88.4	89.7	91.3	89.8	-3.3	-2.0	-1.3	-2.0	-0.8	-4.9	97	87	99	94	0.1	0.7	0.1	0.3	10	3	10 =	SSW 4	SSW 9	SSW12
30	90.5	90.7	91.6	90.9	-0.8	-0.6	-1.6	-1.2	-0.3	-1.9	99	99	98	99	0.0	0.0	0.1	0.0	8	10 =	10 △ =	SSW14	SSE14	SSW12
31	89.9	91.1	89.2	90.1	-5.4	-3.3	-1.3	-2.3	-1.4	-4.0	97	94	99	97	0.2	0.3	0.1	0.2	10 =	8	10 △ =	SSW17	SW 3	S 13
M	90.0	90.1	90.1	90.1	-9.3	-8.3	-9.3	-9.2	-6.1	-12.2	85	87	89	87	0.5	0.5	0.3	0.4	6.9	7.1	6.7	8.9	8.6	8.8

Kasprowy Wierch — $H_s = 1991\,m$ — $H_g = 1988{,}8\,m$ — $h_w = 15{,}4\,m$ — Listopad – Novembre 1961

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	0.5	11	-	
2	9	.	8	-	
3	9	.	8	-	
4	0	26.1	5	-	
5	0	14.5	41	-	
6	7	14.5	50	-	
7	8	8.1	37	-	
8	0	1.5	40	-	
9	8	3.8	32	-	
10	0	15.6	30	-	
11	7	11.4	33	-	
12	9	0.0	41	-	
13	5	18.8	36	-	
14	9	0.0	45	-	
15	9	.	45	-	
16	9	.	42	-	
17	0	0.8	40	-	
18	0	2.1	41	-	
19	0	20.4	43	-	
20	7	4.8	75	-	
21	9	.	78	-	
22	9	.	75	-	
23	9	.	71	-	
24	9	.	65	-	
25	0	2.8	59	-	
26	9	4.0	57	-	
27	0	3.3	50	-	
28	8	1.3	42	-	
29	8	0.1	41	-	
30	9	.	40	-	
31					
Σ	—	154.6	—	-	UWAGI.

Grudzień – Décembre

DNI	WIDZIALNOŚĆ V	OPAD R	GRUBOŚĆ ŚNIEGU h	USŁONECZNIENIE	POGODA
1	9	0.9	38	-	
2	9	0.8	36	-	
3	9	0.0	34	-	
4	9	1.0	33	-	
5	9	1.1	26	-	
6	0	24.7	25	-	
7	0	9.3	64	-	
8	0	1.6	71	-	
9	9	.	74	-	
10	9	0.3	71	-	
11	0	12.9	68	-	
12	0	19.5	72	-	
13	0	3.8	95	-	
14	9	4.2	97	-	
15	0	9.3	98	-	
16	4	1.2	110	-	
17	9	4.4	110	-	
18	5	1.1	113	-	
19	0	1.5	110	-	
20	9	14.2	111	-	
21	0	17.8	127	-	
22	0	6.4	146	-	
23	9	0.8	151	-	
24	9	.	149	-	
25	9	.	148	-	
26	9	0.1	143	-	
27	9	0.2	140	-	
28	9	0.2	135	-	
29	9	.	135	-	
30	0	0.8	131	-	
31	9	0.7	125	-	
Σ	—	138.8	—	-	UWAGI.

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1961

TABLICA II

WYNIKI MIESIĘCZNE I ROCZNE SPOSTRZEŻEŃ METEOROLOGICZNYCH

RÉSULTATS MENSUELS ET ANNUELS
DES OBSERVATIONS MÉTÉOROLOGIQUES

Rozewie

$\varphi = 54°50'$ $\lambda = 18°20'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o\,m}$	$\overline{\text{Max}}$	$\overline{\text{Min}}$	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.4	-3.0	5.5	29, 30	-11.0	25	-1.4	0.4	-0.7	-0.6	4.7	5.1	4.9	4.9	81	79	80	80	1.0	1.2	1.1	1.1	6.8	6.6	6.5	6.6
II	–	–	–	–	4.2	0.3	12.7	18	-5.5	5	1.4	3.2	1.8	2.0	6.3	6.8	6.3	6.5	92	88	90	90	0.5	1.0	0.7	0.7	8.2	7.9	7.0	7.7
III	–	–	–	–	7.0	1.9	13.5	10	-4.3	20	3.4	5.5	4.4	4.4	6.9	7.2	7.0	7.0	88	80	84	84	1.0	1.9	1.4	1.4	7.4	5.5	4.2	5.7
IV	–	–	–	–	10.0	3.4	21.4	7	-1.6	10	5.9	7.9	6.3	6.6	7.5	7.8	7.5	7.6	80	72	78	77	2.0	3.1	2.3	2.5	4.5	3.8	2.1	3.5
V	–	–	–	–	11.9	6.6	19.1	5	0.9	2	9.0	10.4	8.3	9.0	9.9	10.4	9.7	10.0	86	83	88	86	1.7	2.4	1.3	1.8	6.5	6.8	5.9	6.4
VI	–	–	–	–	19.3	12.6	29.3	27	8.0	22	15.4	17.5	14.6	15.5	14.3	14.3	14.1	14.2	82	72	84	80	3.3	6.1	2.7	4.0	4.2	3.6	5.1	4.3
VII	–	–	–	–	18.7	11.8	28.9	3	7.8	6	14.7	16.7	14.3	15.0	14.5	14.4	14.3	14.4	87	76	88	84	2.3	4.8	2.0	3.0	7.2	7.5	6.7	7.1
VIII	–	–	–	–	18.4	12.2	24.8	6	9.8	4	14.3	16.7	14.1	14.8	14.7	14.8	14.7	14.7	90	78	91	86	1.6	4.3	1.5	2.5	7.0	6.4	6.4	6.6
IX	–	–	–	–	17.7	11.3	27.1	17	6.6	27	13.1	16.5	13.8	14.3	12.9	13.9	13.4	13.4	84	74	84	81	2.4	5.0	2.4	3.3	5.0	4.3	3.8	4.4
X	–	–	–	–	13.6	8.9	19.3	10	4.0	31	10.1	12.6	10.9	11.1	11.2	11.6	11.6	11.5	90	80	89	86	1.2	3.0	1.5	1.9	5.7	6.2	4.1	5.3
XI	–	–	–	–	7.1	3.3	11.5	2	-1.4	23	4.7	6.1	5.1	5.2	7.5	7.7	7.7	7.6	86	81	86	84	1.2	1.9	1.2	1.4	7.8	7.9	7.1	7.6
XII	–	–	–	–	1.8	-3.2	12.5	5	-13.3	29	-1.1	-0.1	-1.0	-0.8	5.1	5.3	5.0	5.1	84	82	84	83	0.9	1.1	0.9	1.0	6.6	6.5	7.2	6.8
Rok	–	–	–	–	10.9	5.5	29.3	27.VI	-13.3	29.XII	7.5	9.4	7.7	8.1	9.6	9.9	9.7	9.7	86	79	86	84	1.6	3.0	1.6	2.1	6.4	6.1	5.5	6.0

Łeba

$\varphi = 54°46'$ $\lambda = 17°34'$

I	–	–	–	–	1.5	-3.3	6.4	30	-10.2	26	-1.7	0.7	-0.9	-0.7	4.8	5.1	4.9	4.9	83	77	82	81	0.8	1.4	1.0	1.1	7.6	7.2	6.7	7.2
II	–	–	–	–	4.8	0.5	12.6	18	-5.3	6	1.6	4.0	2.3	2.6	6.4	6.9	6.5	6.6	92	84	90	89	0.5	1.4	0.8	0.9	8.0	8.1	8.5	8.2
III	–	–	–	–	7.5	2.6	15.3	10	-4.2	20	3.9	6.2	4.7	4.9	7.2	7.5	7.3	7.3	89	79	84	84	1.0	2.1	1.4	1.5	8.3	6.9	6.9	7.4
IV	–	–	–	–	12.3	2.8	23.9	14	-3.1	10	6.4	10.5	6.7	7.6	7.7	8.0	7.9	7.9	79	63	79	74	2.2	5.5	2.3	3.3	5.2	4.6	3.3	4.4
V	–	–	–	–	13.0	6.2	23.3	5	-1.3	2	9.6	11.3	9.0	9.7	10.1	10.4	9.9	10.1	85	78	85	83	1.9	3.2	1.8	2.3	7.1	6.9	6.8	6.9
VI	–	–	–	–	20.4	12.6	29.7	27	7.7	22	16.2	18.6	15.4	16.4	14.7	14.2	14.4	14.4	80	68	82	77	3.9	7.7	3.2	4.9	5.2	5.2	6.0	5.4
VII	–	–	–	–	19.0	12.0	32.6	3	7.2	2	14.9	17.6	15.0	15.6	14.8	16.0	14.8	15.2	87	75	86	83	2.2	5.9	2.0	3.4	8.0	7.6	8.0	7.9
VIII	–	–	–	–	18.5	12.6	23.3	6	9.7	4	14.6	17.1	14.6	15.2	14.9	15.3	14.8	15.0	89	78	89	85	1.8	4.3	1.8	2.6	7.9	7.5	6.6	7.3
IX	–	–	–	–	18.5	10.2	27.3	1	4.4	24,25,27	12.3	17.8	12.8	13.9	13.0	14.2	13.0	13.4	89	70	88	82	1.6	6.4	2.0	3.3	5.1	5.3	4.2	4.9
X	–	–	–	–	15.0	8.6	20.1	6	3.3	30	10.2	14.3	11.1	11.7	11.3	12.0	11.6	11.6	90	75	88	84	1.2	4.4	1.7	2.4	6.2	6.5	3.9	5.5
XI	–	–	–	–	7.4	2.8	11.8	2	-4.8	23	4.8	6.4	5.0	5.3	7.8	7.8	7.5	7.7	88	81	85	85	1.0	1.9	1.4	1.4	8.9	8.2	6.6	7.9
XII	–	–	–	–	2.0	-3.7	12.7	5	-13.6	17	-1.1	-0.1	-1.0	-0.8	5.1	5.4	5.1	5.2	85	83	85	84	0.8	1.1	0.9	0.9	7.5	7.5	6.3	7.1
Rok	–	–	–	–	11.7	5.3	32.6	3.VII	-13.6	17.XII	7.6	10.4	7.9	8.4	9.8	10.2	9.8	9.9	86	76	85	82	1.6	3.8	1.7	2.4	7.1	6.8	6.2	6.7

Puck

$\varphi = 54°43'$ $\lambda = 18°25'$

I	–	–	–	–	1.5	-2.7	6.2	31	-11.7	26	-1.3	-0.5	-0.5	-0.4	4.9	5.2	5.1	5.1	83	79	82	81	0.9	1.3	1.0	1.1	8.5	8.1	6.6	7.7
II	–	–	–	–	5.1	0.8	15.3	18	-6.0	5	1.9	4.2	2.6	2.8	6.3	6.8	6.6	6.6	89	82	88	86	0.8	1.6	0.9	1.1	8.9	9.0	8.3	8.7
III	–	–	–	–	8.6	2.6	15.8	10	-4.6	20	4.5	7.2	5.2	5.5	7.0	6.9	7.2	7.0	82	68	80	77	1.5	3.5	1.8	2.4	8.3	6.8	7.7	7.6
IV	–	–	–	–	11.5	3.6	24.1	7	-1.8	2, 11	7.0	9.9	7.6	8.0	8.0	8.7	8.5	8.4	78	70	80	76	2.3	4.1	2.2	2.9	4.5	4.7	4.1	4.4
V	–	–	–	–	13.1	6.8	20.1	5	1.4	2, 13	10.1	11.6	9.5	10.2	10.4	10.9	10.3	10.5	84	80	86	83	2.1	3.0	1.7	2.3	7.5	7.6	7.4	7.5
VI	–	–	–	–	21.2	12.7	29.4	27	9.1	24	16.8	19.7	16.2	17.2	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.1	6.0	4.7
VII	–	–	–	–	19.6	12.2	28.9	3	9.1	6	15.3	18.0	15.2	15.9	15.2	16.0	15.2	15.5	87	78	88	84	2.3	5.0	2.2	3.2	7.6	8.1	8.8	8.2
VIII	–	–	–	–	19.5	12.4	26.9	6	9.7	26	14.4	18.1	15.1	15.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.4	9.2	8.5
IX	–	–	–	–	18.7	10.6	28.4	17	4.4	28	12.3	17.6	14.6	14.8	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.0	6.0	5.4
X	–	–	–	–	14.4	8.9	18.2	11	4.6	31	10.7	13.4	11.7	11.9	11.6	12.8	12.0	12.1	89	83	87	86	1.4	2.7	1.8	2.0	7.0	7.0	6.1	6.7
XI	–	–	–	–	7.1	3.2	11.6	1	-3.7	23	4.8	6.2	5.0	5.2	7.7	8.1	7.7	7.8	88	84	87	86	1.1	1.5	1.2	1.3	8.5	8.7	8.7	8.6
XII	–	–	–	–	1.8	-3.5	13.3	5	-14.2	28	-0.9	-0.1	-1.2	-0.8	4.9	5.3	4.9	5.0	80	81	81	81	1.1	1.2	1.0	1.1	7.8	7.5	7.3	7.5
Rok	–	–	–	–	11.8	5.6	29.4	27.VI	-14.2	28.XII	8.0	10.5	8.4	8.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.1	7.2	7.2

Poraj

$\varphi = 54°40'$ $\lambda = 17°36'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8.2	1.3	16.7	10	-8.3	20	3.8	6.8	4.7	5.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	14.1	0.8	22.9	14	-7.2	2	6.4	12.3	5.9	7.6	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.2	4.6	4.4
V	–	–	–	–	14.2	4.9	24.1	30	-3.4	2	9.7	12.9	8.4	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.5	6.7
VI	–	–	–	–	21.4	10.6	28.9	27	4.3	22	16.4	20.4	15.3	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	5.6	5.7
VII	–	–	–	–	19.5	10.8	31.7	3	5.0	1	14.7	17.8	14.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	7.3	7.2
VIII	–	–	–	–	18.9	11.0	24.3	6	6.5	26	14.9	17.7	13.7	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.2	7.1	6.7
IX	–	–	–	–	18.9	7.8	28.1	17	-0.3	23, 24	11.7	17.7	12.2	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.8	6.0	5.4
X	–	–	–	–	15.0	7.2	19.6	5, 6	1.5	30	10.0	14.2	10.3	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	6.1	6.3
XI	–	–	–	–	7.4	1.8	12.3	3	-7.7	23, 24	4.0	6.9	4.3	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	6.6	6.9
XII	–	–	–	–	1.7	-5.2	13.0	5	-16.4	17, 24	-1.6	0.1	-1.7	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.3	6.9
Rok	–	–	–	–	–	–	31.7	3.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Rozewie

$H_s = 54\,m$ $h_w = 19\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%D, %nD]																		OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	≥ 10	≥ 15	●	●	≥ 0.1	≥ 1.0	≥ 10.0	≡	▦	≋
I	3	6.0	6	4.9	3.5	4.3	1.5	9.0	2.1	4.4	36.5	5.3	13	7.5	4.5	7.0	4	5.3	30.0	6.2	5	2	8	22	·	7	·	3	12	16	8	·	4	14	·
II	1	6.0	1	3.0	1	3.0	6.5	3.5	12.5	6.4	21.5	5.4	29	6.1	9.5	5.7	2	5.5	37.2	22.4	28	·	·	8	·	6	·	1	13	15	6	1	18^2	4	·
III	4.5	6.7	1.5	6.7	·	·	·	·	3	4.3	12.5	6.0	52.5	11.3	19	11.7	·	10.1	27.7	8.0	12	·	·	6	·	27	13	3	6	12	6	·	6^2	3	·
IV	3.5	4.4	12.5	3.1	14.5	3.0	18	3.8	7	5.6	9.5	3.4	11	4.6	9	6.3	5	3.8	3.7	1.1	4	·	·	7	·	3	1	12	2	6	1	·	5^2	·	2
V	8	4.0	12	3.6	5	3.3	7.5	3.1	4.5	3.7	13.5	3.3	18	5.0	15.5	4.1	9	3.5	51.8	9.8	3	·	·	·	·	1	·	4	9	12	11	·	10^2	·	3
VI	1	1.0	3	1.7	7	2.4	14.5	3.0	4	4.2	8.5	3.5	30	6.6	18	7.0	4	4.9	22.4	11.2	14	·	·	·	2	6	1	7	3	9	5	1	4^2	·	3
VII	1	1.0	3	5.7	0.5	1.0	5.5	3.0	4.5	2.3	32	4.5	22	5.0	12.5	4.4	12	3.8	186.3	56.6	13	·	·	·	2	1	·	2	10	19	11	4	2^2	·	6
VIII	1.5	4.0	2.5	1.6	0.5	1.0	3.5	2.4	2.5	2.2	23.5	3.8	30.5	6.2	18.5	5.8	10	4.4	75.4	19.2	19	·	·	·	·	4	·	·	7	17	14	3	4	·	1
IX	1	1.0	7	3.0	4	3.2	13.5	3.2	11.5	4.2	15	3.4	20	4.4	12	5.5	6	3.7	34.2	12.1	14	·	·	·	2	·	·	9	5	7	6	2	3	·	3
X	·	·	·	·	3	6.8	3.1	5.7	17.5	5.9	25	4.1	8.5	5.1	7	6.3	1	5.3	37.5	14.5	18	·	·	·	·	3	1	6	8	14	8	1	3	✓	1
XI	8	6.4	10	6.8	7.5	8.2	7	6.6	11.5	3.6	23	5.5	14.5	6.6	5.5	9.0	3	6.0	31.4	9.9	11	·	·	6	·	9	1	1	18	15	9	·	7	·	·
XII	5	8.2	16	8.3	3	3.7	4.5	5.4	17	4.4	29.5	6.6	11	11.2	7	9.8	·	7.2	47.8	18.2	2	5	8	20	·	12	5	·	10	17	10	1	6	11	·
Rok	37.5	4.1	74.5	4.0	49.5	3.3	113	4.1	116.5	4.3	250	4.6	260	6.6	138	6.9	56	5.3	585.4	56.6	13.VII	7	16	69	6	79	22	48	103	159	95	13	72^2	32	19

Łeba

$H_s = 2\,m$ $h_w = 21\,m$

I	1	6.0	4.5	5.0	1.5	5.7	6	4.6	40.5	3.7	29	4.4	6	3.4	1.5	2.3	3	4.1	43.4	9.1	30	1	7	24	·	2	·	1	13	17	14	·	1	12	·
II	4	2.2	·	·	1	5.0	5	3.7	22.5	3.7	31	3.3	13.5	3.3	3	3.7	4	3.3	56.2	27.2	28	·	·	7	·	1	·	1	19	17	10	1	6	2	·
III	2	6.0	·	·	·	·	·	·	3	2.5	42.5	5.7	38	6.1	7.5	5.5	·	5.8	24.0	5.6	29	·	·	3	·	7	·	1	14	13	7	·	4	1	·
IV	2.5	3.4	10.5	3.8	14	3.3	13.5	4.4	14.5	2.8	12.5	2.8	15	3.0	2.5	3.2	5	3.1	8.9	3.7	4	·	·	8	·	1	·	7	2	8	2	·	4	·	2
V	11.5	4.1	12.5	3.1	3.5	3.7	1	4.0	10.5	3.3	21	3.1	20	3.4	8	3.9	5	3.3	62.1	9.8	15	·	·	1	·	1	·	2	13	18	12	·	2	·	3
VI	3.5	2.1	9.5	2.4	6.5	2.5	7.5	3.2	1.5	2.0	17	3.2	34	4.8	3.5	3.3	7	3.3	52.8	30.1	10	·	·	·	5	2	·	6	7	8	8	1	3	·	3
VII	1.5	2.0	·	·	3.5	3.4	0.5	6.0	8	2.2	40	4.2	23.5	3.7	9	2.6	7	3.4	117.6	35.0	13	·	·	·	3	1	·	2	18	21	16	3	·	·	6
VIII	·	·	2	2.0	1.5	1.0	1.5	1.0	7.5	3.1	29	3.4	38	4.0	5.5	2.4	8	3.2	101.4	34.6	22	·	·	·	·	1	·	·	14	20	16	1	2	·	1
IX	2.5	1.8	3.5	3.0	4.5	4.4	11.5	3.3	14	2.0	19	2.2	25.5	4.0	2.5	5.2	7	2.9	61.8	21.6	7	·	·	·	2	·	·	9	6	11	9	3	2	·	3
X	·	·	·	·	8	3.6	2.5	4.9	2.7	3.1	20.5	3.4	9.5	4.4	1	4.0	2	3.8	39.2	10.5	18	·	·	·	·	3	·	7	8	14	10	1	2	·	·
XI	8.5	4.2	5.5	5.9	7.5	5.9	8	2.9	16.5	2.0	22.5	5.0	8.5	4.5	7	4.2	6	3.9	33.7	6.3	30	·	·	6	·	2	·	1	17	15	9	·	4	·	·
XII	13	6.0	4.5	4.1	6	3.9	2.5	2.2	21.5	2.1	29.5	4.9	10	6.2	5	3.5	1	4.3	47.0	12.6	2	6	8	22	·	5	·	·	11	19	8	1	·	18	·
Rok	50	3.2	52.5	2.4	57.5	3.5	82	3.4	187	2.7	313.5	3.8	241.5	4.2	56	3.6	55	3.7	648.1	35.0	13.VII	7	15	71	10	26	·	37	142	181	121	11	30	33	18

Puck

$H_s = 1\,m$ $h_w = 14\,m$

I	1.5	2.0	5.5	4.4	4	4.2	11	4.3	1	2.0	29.5	4.6	8	5.6	3.5	5.1	29	3.1	32.2	6.5	29	2	10	20	·	3	2	1	18	12	12	·	2	7	·
II	·	·	1	4.0	3	3.0	12	3.1	1.5	3.7	22.5	3.0	14	3.1	15	4.1	15	2.7	41.8	24.7	28	·	·	7	·	1	·	·	21	8	8	1	3	3	·
III	·	·	1	6.0	·	·	·	·	·	·	9	2.6	6.5	9.1	16	9.7	2	8.4	31.8	12.0	29	·	·	3	·	17	10	1	17	9	5	1	·	·	·
IV	5	3.8	15	4.8	8	2.1	20	4.0	·	·	3	3.7	13	3.0	3	1.0	23	2.9	3.8	2.8	5	·	·	4	·	2	·	11	6	2	2	·	4	·	·
V	6	4.2	14	3.8	6	1.7	7	3.0	·	·	18	1.7	9	4.7	10	5.0	23	2.5	82.3	25.8	14	·	·	·	·	2	·	3	16	15	13	2	5	·	2
VI	·	·	5	1.6	10	2.0	12	2.8	3	2.3	10	3.5	28	7.4	7	4.7	15	3.8	46.6	38.6	14	·	·	·	3	9	2	6	5	5	3	1	2	·	3
VII	3	5.7	3	2.0	4	4.5	5	2.4	·	·	4.1	3.1	11	3.6	7	4.3	19	2.7	119.2	33.0	13	·	·	·	2	3	1	2	20	15	13	4	·	·	4
VIII	1	2.0	2	2.5	2	1.5	4	1.8	1	3.0	24	2.8	31	5.6	6	6.3	22	3.2	63.9	18.2	22	·	·	·	2	10	·	·	22	15	13	1	1	·	2
IX	·	·	2	2.5	8	2.9	13	4.1	2	3.5	18	3.6	13	4.5	5	4.4	29	2.6	51.4	19.6	8	·	·	·	3	4	·	9	10	6	5	3	·	·	·
X	·	·	·	·	3	5.0	3.8	4.9	2	4.0	15	2.4	6	7.7	4	4.5	25	3.3	36.4	17.0	18	·	·	·	·	4	·	5	14	12	8	1	·	·	·
XI	7	6.6	7	7.6	10	9.2	7	2.1	·	·	15	4.5	15	3.5	5	9.0	24	4.1	41.7	10.6	11	·	·	5	·	6	1	·	20	15	12	1	6	·	·
XII	9	7.1	12	1.1	1	2.0	13	2.8	·	·	31	4.5	12	8.1	3	6.7	12	5.3	37.1	12.4	2	6	10	21	·	12	3	·	16	10	8	1	5	13	
Rok	32.5	2.6	67.5	3.4	59	3.2	142	2.9	10.5	1.5	236	3.3	225	5.5	84.5	5.4	238	3.7	588.2	38.6	14.VI	8	20	60	10	73	19	38	185	124	102	16	28	23	11^2

Poraj

$H_s = 5\,m$ $h_w = 10\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	7	4.6	·	·	·	·	·	0.5	3.0	18	3.8	38	5.0	24.5	5.8	5	4.7	31.3	8.5	22	·	·	8	·	5	·	·	·	10	8		4	–	–		
IV	3	2.5	2.5	2.2	12.5	2.9	21	3.5	11	3.4	6.5	3.7	11.5	3.0	9	3.1	13	2.7	11.8	5.5	5	·	·	11	·	·	·	·	·	4	3	·	3	·	–	
V	18	3.7	10.5	2.9	7	2.8	3	1.3	6.5	3.0	13.5	2.7	12.5	2.6	12	2.9	10	2.6	64.6	12.0	15	·	·	2	·	·	·	·	7	14	13	1	1	·	–	
VI	4.5	1.4	4	2.8	7.5	1.5	11.5	2.2	3.5	2.7	5.5	3.2	2.2	3.7	13.5	3.3	18	2.3	49.7	17.9	10	·	·	·	9	·	·	·	2	10	9	2	3	·	–	
VII	5	2.6	0.5	1.0	5	2.5	2.5	1.6	8.5	3.2	25.5	3.5	19.5	3.0	13.5	2.0	13	2.5	162.4	33.4	13	·	·	·	3	·	·	·	5	23	19	5	4	·	–	
VIII	2	1.8	1.5	1.3	1	1.5	5	3.1	5.5	3.5	20	3.4	2.6	3.4	14	3.4	18	2.7	95.0	15.3	22, 23	·	·	·	·	·	·	·	4	21	17	2	1	·	–	
IX	2.5	1.4	0.5	1.0	10.5	2.1	10	3.0	5.5	2.9	8.5	1.9	1.5	2.5	11.5	2.1	2.6	1.7	71.7	19.7	7	·	·	2	2	·	·	·	4	12	10	2	7	·	–	
X	3	4.3	1	3.0	9	3.1	22.5	3.3	1.5	3.5	12	3.3	8	2.6	5.5	3.5	17	2.7	40.6	8.7	18	·	·	·	·	·	·	·	9	11	9	·	3	·	–	
XI	8.5	4.2	4.5	4.2	6.5	4.9	8	3.1	11	2.6	17	4.0	9	3.2	5.5	3.6	20	2.9	32.3	5.7	11	·	·	9	·	1	·	·	10	15	10	·	5	–	–	
XII	9.5	6.7	2.5	5.8	4.5	2.8	9.5	2.6	16.5	2.8	18	5.2	12	5.2	6.5	3.7	14	3.7	–	–	–	6	10	22	·	3	2	·	6	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Hel

$\varphi = 54°36'$ $\lambda = 18°49'$ **1961**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1017.7	1044.4	995.1	1018.0	1.6	−2.1	5.0	16	−11.5	25	−0.9	0.6	0.0	−0.1	5.1	5.3	5.4	5.3	85	80	84	83	0.8	1.2	0.9	1.0	7.4	7.6	7.0	7.3
II	1019.0	1037.5	989.6	1019.3	4.0	0.4	11.3	18	−2.5	14	1.5	3.2	2.9	2.2	6.5	6.8	6.6	6.6	96	88	93	92	0.3	1.0	0.5	0.6	8.2	8.1	8.1	8.1
III	1012.1	1032.7	986.1	1012.4	8.0	1.8	15.4	10	−3.0	20	3.9	6.8	4.4	4.9	7.2	7.1	7.2	7.2	88	72	86	82	1.0	2.9	1.2	1.7	7.8	6.7	4.5	6.3
IV	1013.4	1027.3	1003.1	1013.7	12.0	2.7	20.6	7	−4.4	12	5.7	11.0	5.8	7.1	7.9	8.3	7.9	8.0	85	62	85	77	1.4	5.3	1.5	2.7	5.1	3.9	2.5	3.8
V	1011.3	1020.0	999.8	1011.6	13.7	6.0	19.7	30	−0.1	2	9.3	12.1	8.2	9.4	10.5	11.0	10.0	10.5	89	78	91	86	1.3	3.4	1.0	1.9	6.8	7.5	6.4	6.9
VI	1013.4	1025.7	1002.5	1013.7	22.0	12.7	26.3	27	7.2	1	16.2	20.9	15.6	17.1	15.1	15.5	15.1	15.2	82	62	85	76	3.4	9.6	2.7	5.2	4.6	3.6	5.1	4.4
VII	1010.4	1026.2	993.5	1010.7	20.4	12.5	29.8	3	7.5	17	15.2	18.5	15.0	15.9	15.0	15.8	14.8	15.2	87	75	86	83	2.3	6.0	2.4	3.6	7.7	7.4	7.1	7.4
VIII	1013.0	1029.0	999.5	1013.3	19.7	13.1	26.0	6	8.8	31	14.8	18.3	14.6	15.6	15.1	15.7	14.9	15.2	89	75	89	84	1.8	5.6	1.8	3.1	7.2	7.0	6.9	7.0
IX	1017.4	1031.6	999.4	1017.7	19.0	10.5	26.7	1	3.8	24	12.7	18.1	13.6	14.5	13.5	14.3	13.5	13.8	91	69	86	82	1.4	6.8	2.3	3.5	4.3	4.5	4.0	4.3
X	1018.0	1032.9	991.1	1018.3	14.4	9.9	18.4	5	6.8	30	10.6	13.8	11.8	12.0	11.6	12.5	12.1	12.1	91	79	87	86	1.2	3.4	1.8	2.1	6.1	6.5	4.6	5.7
XI	1013.2	1034.8	992.3	1013.5	7.4	3.9	11.7	1	−3.3	28	5.3	6.4	5.3	5.8	8.0	8.1	8.0	8.0	88	83	85	85	1.1	1.7	1.4	1.4	8.6	8.3	7.8	8.2
XII	1013.7	1046.7	983.5	1014.0	1.9	−2.3	11.1	5	−12.0	28	−0.3	0.5	−0.3	−0.1	5.3	5.4	5.3	5.3	86	81	85	84	0.3	1.2	0.9	1.0	8.1	7.6	7.9	7.9
Rok	1014.4	1046.7	983.5	1014.7	12.0	5.8	29.8	3. VII	−12.0	28. XII	7.8	10.8	8.0	8.6	10.1	10.5	10.1	10.2	88	75	87	83	1.4	4.0	1.5	2.3	6.8	6.6	6.0	6.5

Ustka

$\varphi = 54°35'$ $\lambda = 16°52'$

I	1016.4	1043.3	993.3	1017.5	1.6	−3.0	6.1	29, 30	−12.7	26	−1.5	0.8	−0.8	−0.6	4.3	4.8	4.5	4.5	73	70	73	72	1.4	1.8	1.5	1.6	6.7	7.0	6.4	6.7
II	1018.1	1036.3	987.8	1019.2	5.2	1.0	13.4	18	−3.1	6	1.9	4.0	2.8	2.9	6.0	6.5	6.3	6.3	95	80	83	83	1.0	1.8	1.3	1.4	8.4	7.9	7.8	8.0
III	1012.8	1033.1	985.5	1013.9	7.3	2.8	17.0	10	−2.5	20	3.8	5.7	4.8	4.8	6.7	6.8	6.8	6.8	82	74	78	78	1.4	2.5	1.9	1.9	8.4	6.7	6.5	7.2
IV	1012.2	1025.5	1001.9	1013.2	12.5	3.9	24.5	14	−1.3	11	6.3	10.5	7.4	7.9	7.2	7.6	7.4	7.4	74	62	71	69	2.7	5.9	3.2	3.9	4.2	4.8	3.1	4.0
V	1011.0	1021.2	998.6	1012.0	12.5	7.2	21.8	5	1.7	2	9.5	10.9	9.3	9.7	10.3	10.5	10.1	10.3	86	81	86	84	1.7	2.7	1.7	2.0	7.3	6.7	5.5	6.5
VI	1012.9	1026.8	1001.4	1013.9	20.0	12.8	28.8	27	8.0	22	15.6	17.1	15.7	16.0	14.4	14.1	14.3	14.3	81	73	80	78	3.5	5.7	3.8	4.3	5.6	5.5	4.7	5.3
VII	1009.7	1025.5	993.3	1010.7	18.6	12.6	31.8	3	8.2	6	15.0	16.9	15.1	15.5	14.8	14.7	14.6	14.7	87	77	85	83	2.4	4.9	2.7	3.3	7.8	7.2	6.5	7.2
VIII	1012.5	1027.9	999.1	1013.6	17.9	12.8	24.2	10	9.9	31	14.5	16.7	14.8	15.2	14.7	15.5	14.8	15.0	89	82	87	86	1.9	3.6	2.2	2.6	8.1	7.5	6.6	7.4
IX	1016.4	1029.3	998.6	1017.4	18.3	10.8	27.3	1	4.6	25	12.4	17.6	13.4	14.2	13.1	13.7	13.2	13.3	89	68	85	81	1.6	6.7	2.4	3.6	4.8	4.7	3.9	4.5
X	1016.1	1030.1	987.7	1017.1	14.9	8.9	19.8	6	4.6	31	10.0	14.3	11.2	11.7	11.0	11.3	11.3	11.2	89	70	85	81	1.4	5.3	2.1	2.9	6.4	6.3	3.8	5.5
XI	1012.2	1035.0	990.2	1013.2	7.2	3.2	11.8	1	−4.7	23	4.8	6.8	4.8	5.3	7.7	7.8	7.5	7.7	88	78	85	84	1.1	2.2	1.3	1.5	8.4	7.6	7.3	7.8
XII	1013.3	1046.2	981.1	1014.4	1.8	−3.3	13.4	5	−16.0	28	−1.3	0.0	−0.9	−0.8	5.1	5.4	5.1	5.2	84	81	84	83	0.9	1.2	1.0	1.0	6.6	7.4	6.5	6.8
Rok	1013.6	1046.2	981.1	1014.6	11.5	5.8	31.8	3. VII	−16.0	28. XII	7.6	10.1	8.1	8.5	9.6	9.9	9.7	9.7	84	75	82	80	1.8	3.7	2.1	2.5	6.9	6.6	5.7	6.4

Ustka – Wydma

$\varphi = 54°35'$ $\lambda = 16°52'$

I	–	–	–	–	1.6	−3.1	5.6	31	−12.2	25	−1.6	0.6	−0.8	−0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	5.1	1.0	13.7	18	−2.7	6	1.9	3.8	2.7	2.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	7.2	2.6	17.0	10	−2.7	20	3.8	5.6	4.7	4.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	12.6	3.6	25.0	14	−1.4	11	6.4	10.1	7.2	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	12.4	7.0	22.3	5	1.9	2	9.5	10.5	9.3	9.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	19.9	12.7	29.6	27	8.4	22	15.5	16.8	15.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	18.8	12.4	32.6	3	8.1	6	14.9	16.9	15.1	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	17.8	12.7	24.3	10	10.0	4, 31	14.5	16.6	14.7	15.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.3	10.8	27.7	1	4.7	25	12.5	17.6	13.4	14.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.9	8.8	20.3	6	4.6	31	9.9	14.4	11.2	11.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.1	3.2	11.8	1	−4.4	23	5.0	6.7	5.0	5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1.8	−3.2	13.3	5	−16.2	28	−1.2	0.0	−0.8	−0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	11.5	5.7	32.6	3. VII	−16.2	28. XII	7.6	10.0	8.1	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lębork

$\varphi = 54°33'$ $\lambda = 17°45'$

I	1014.9	1041.3	992.6	1017.6	1.5	−4.0	6.5	29	−13.4	26	−2.0	0.5	−1.6	−1.2	4.6	4.8	4.7	4.7	81	72	80	78	0.9	1.7	1.1	1.2	7.6	7.9	6.9	7.5
II	1016.3	1034.8	986.6	1019.1	5.0	0.4	14.5	18	−6.4	4	1.5	4.1	2.4	2.6	6.2	6.7	6.3	6.4	90	81	87	86	0.7	1.7	1.0	1.1	8.8	8.5	8.6	8.6
III	1010.7	1030.8	983.7	1013.4	8.3	2.0	17.1	10	−6.3	20	3.8	6.8	4.6	5.0	7.0	7.1	7.1	7.1	86	72	82	80	1.2	3.0	1.5	1.9	8.9	7.7	7.2	7.9
IV	1010.5	1024.1	1000.2	1013.2	14.3	2.5	24.9	14	−5.7	2	6.0	12.7	7.5	8.4	7.5	7.3	7.4	7.4	78	49	71	66	2.3	8.4	3.4	4.7	5.0	5.3	3.3	4.5
V	1008.9	1018.5	996.5	1011.6	14.8	5.5	24.3	30	−3.1	2	9.2	13.1	8.9	10.0	10.4	10.5	10.2	10.4	88	71	88	82	1.4	4.9	1.5	2.6	7.4	7.7	5.8	7.0
VI	1011.0	1023.7	998.8	1013.6	22.2	11.6	29.4	27	6.6	22	16.2	21.0	16.1	17.4	14.9	13.7	14.5	14.4	81	57	79	72	3.6	11.9	3.9	6.5	5.6	6.5	6.2	6.1
VII	1007.9	1023.7	993.3	1010.5	19.7	11.5	31.6	3	5.5	2	14.6	18.0	14.8	15.6	14.4	14.2	14.6	14.4	87	71	86	81	2.3	7.1	2.4	3.9	8.4	8.3	7.8	8.2
VIII	1010.7	1026.0	996.6	1013.4	19.1	11.5	25.1	6	8.3	4	13.9	17.8	14.0	14.9	14.4	14.3	14.4	14.4	90	70	90	83	1.6	6.4	1.7	3.2	8.1	8.8	6.4	7.8
IX	1014.7	1027.6	997.2	1017.4	19.2	8.6	28.4	17	0.8	25	10.6	18.2	12.3	13.4	12.2	12.8	12.8	12.6	92	62	88	81	1.2	8.6	1.8	3.9	5.5	5.3	4.2	5.0
X	1014.7	1028.9	986.7	1017.4	15.1	7.9	19.9	5, 6	1.7	30	9.7	14.3	10.8	11.4	10.8	11.4	11.1	11.1	89	70	85	81	1.4	5.2	2.0	2.9	6.8	6.6	5.0	6.1
XI	1010.5	1032.5	988.7	1013.2	6.9	1.5	11.6	1	−6.2	23	3.6	6.1	4.4	4.6	7.4	7.6	7.3	7.4	91	80	86	86	0.8	2.0	1.2	1.3	8.4	8.1	7.3	7.9
XII	1011.3	1044.9	983.6	1014.0	1.2	−5.3	13.5	5	−17.0	28	−2.2	−0.2	−2.2	−1.7	4.8	5.0	4.7	4.8	84	76	82	81	0.9	1.4	1.0	1.1	7.9	7.5	7.1	7.5
Rok	1011.8	1044.9	983.6	1014.5	12.3	4.5	31.6	3. VII	−17.0	28. XII	7.1	11.0	7.7	8.4	9.6	9.6	9.6	9.6	86	69	84	80	1.5	5.2	1.9	2.9	7.4	7.4	6.3	7.0

Hel

$H_s = 1\,m$ $H_b = 2{,}6\,m$ $h_w = 24\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%, ∑=0)																	Średnia prędkość	OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C					Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ -10°	Max ≤ 0°	Min 0° ≤	Max ≥ 25°	≥ 6 ∧ <	≥ 15	●	●	≥ 0,1 ∧ < 1,0	≥ 1,0 ∧ < 10,0	≥ 10,0	≡	▦	n/o
I	2	6,2	5,5	4,7	4	4,5	3,5	8,9	24	4,0	34	4,6	10,5	6,2	6,5	5,1	3	4,7	23,2	4,7	24	2	9	15	·	7	·	1	17	15	8	·	·	7	·
II	1,5	5,0	1,5	5,0	0,5	3,0	6,5	5,1	21	6,1	15	3,7	16,5	3,9	10,5	4,6	11	4,1	40,2	13,6	28	·	·	9	·	3	·	1	17	14	8	1	6	1	·
III	4	5,5	·	·	·	·	·	·	5	3,8	11	7,0	42	7,3	28	7,9	3	6,9	28,4	7,5	29	·	·	5	·	19	4	2	9	14	8	·	1	2	·
IV	7	2,6	14,5	4,0	15,5	4,1	13,5	3,5	7	3,5	5	3,1	9,5	3,6	9	5,3	9	3,4	6,6	2,4	4	·	·	6	·	3	·	10	3	7	3	·	2	·	1
V	15	3,3	7,5	4,2	5	3,0	9	2,9	8,5	3,1	8	2,9	12,5	2,9	16,5	4,3	11	3,0	90,1	23,0	14	·	·	1	·	1	·	1	13	16	14	4	3	·	4
VI	2,5	2,8	10	3,0	6,5	2,8	4	2,2	1,5	2,7	4	4,0	27	5,4	12,5	5,0	22	3,3	43,6	25,9	14	·	·	·	6	1	·	8	4	8	6	1	1	·	4
VII	1,5	2,7	2	4,2	7	4,1	3	2,5	11,5	3,2	18,5	4,6	26	5,1	6,5	5,2	17	3,6	114,0	28,0	13	·	·	·	2	3	·	2	17	21	15	4	·	·	7
VIII	·	·	1,5	2,0	3,5	2,9	2,5	1,8	6	3,2	19	4,4	33,5	6,6	12	5,3	15	4,4	84,3	16,6	1	·	·	·	1	8	·	·	10	19	13	3	1	·	5
IX	1,5	3,3	4	3,1	16	3,7	11	4,3	7,5	3,6	9,5	3,8	18	5,3	8,5	5,5	14	3,7	41,6	18,9	14	·	·	·	3	4	·	9	6	9	6	1	·	·	1
X	·	·	·	·	13	6,3	25,5	6,9	22	5,1	13	5,2	8	6,1	6,5	5,7	5	5,6	31,2	12,2	18	·	·	·	·	10	·	5	12	12	8	1	·	·	·
XI	5,5	5,5	5,5	6,6	9,5	8,7	10	6,4	10	4,8	16,5	6,8	19	6,0	10	6,6	4	6,2	33,8	9,2	11	·	·	3	·	13	·	1	19	16	8	·	1	·	·
XII	5	8,6	10	7,0	3	3,5	5	5,5	16,5	6,2	15	6,7	23,5	8,1	13	6,0	2	6,7	45,8	12,4	2	2	11	18	·	15	1	·	16	15	13	1	3	16	·
Rok	45,5	3,8	6,2	3,6	83,5	3,9	93,5	4,2	140,5	4,1	168,5	4,7	246	5,5	139,5	5,5	116	4,6	582,8	28,0	13.VII	4	20	57	12	87	5	40	143	166	110	16	18	26	22

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Ustka

$H_s = 6\,m$ $H_b = 8{,}1\,m$ $h_w = 19{,}8\,m$ anemometr, $18\,m$ wiatromierz Wilda

I	·	·	2	6,5	9	3,1	3	6,3	34	3,4	32,5	5,3	35	7,6	9	5,1	·	4,5	40,6	7,4	29	3	9	17	·	2	·	6	13	15	12	·	5	10	·
II	2	7,0	1	4,0	1	3,0	·	·	21	5,2	26	3,7	15	4,7	11	5,2	7	4,2	53,0	18,8	28	·	·	8	·	·	·	1	20	18	10	1	9	5	·
III	3	7,7	1	5,0	·	·	·	·	2	6,0	19	4,9	50,5	8,2	17,5	7,1	·	7,2	34,3	6,0	29	·	·	3	·	14	2	1	10	14	10	·	9	1	·
IV	2	4,5	12	3,8	8	2,9	12	4,8	19	3,2	11	2,9	10,5	5,4	10,5	4,1	5	3,6	11,5	3,6	1	·	·	6	·	2	·	11	4	8	4	·	5	1	1
V	11	4,8	15	4,9	3	5,0	1	5,0	5	3,4	17,5	3,7	17,5	5,1	18	4,4	5	4,3	84,7	25,2	3	·	·	·	·	2	·	1	9	16	10	3	6	·	3
VI	1	3,0	17,5	3,3	3,5	2,6	2	3,0	5	2,9	13	3,9	26	6,7	20	6,0	2	4,8	43,7	14,7	10	·	·	·	4	4	·	6	7	12	9	1	2	·	5
VII	3,5	5,1	·	·	·	·	1	6,0	7	2,4	34	4,7	24	6,2	22,5	5,2	1	5,0	141,3	34,6	13	·	·	·	3	3	·	3	15	23	16	2	·	·	5
VIII	2	1,5	·	·	1	3,0	·	·	6	2,2	30	3,9	34	5,6	18	5,7	2	4,6	61,7	8,9	16	·	·	·	·	4	·	1	14	23	17	·	2	·	4
IX	1	2,0	6	3,2	3,5	2,1	14,5	4,0	11	3,5	18	3,2	15	5,3	19	6,3	2	4,3	50,6	31,2	7	·	·	·	2	2	·	9	6	8	6	1	2	·	1
X	·	·	2	3,5	3	3,3	20,5	4,9	23,5	4,0	31	3,9	5	6,0	7	6,3	1	4,4	26,9	4,3	19	·	·	·	·	1	·	6	10	12	9	·	·	·	·
XI	9,5	5,3	5,5	4,7	7,5	5,9	8,5	3,9	12	2,8	31,5	4,7	5	7,1	9,5	5,7	1	4,7	30,4	7,2	30	·	·	6	·	3	·	1	18	14	11	·	4	·	·
XII	9,5	8,8	3	7,2	7,5	3,8	4,5	4,0	19	4,4	31,5	6,2	7	8,0	11	7,7	·	6,1	51,2	9,0	2	6	10	18	·	13	5	2	13	16	13	·	3	17	·
Rok	44,5	4,1	6,5	3,8	4,7	2,9	6,7	3,5	164,5	3,6	295	4,2	213	6,3	173	5,7	26	4,8	628,9	34,6	13.VII	9	19	58	9	50	7	48	139	179	127	8	47	34	19

Uwaga. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru.

Ustka – Wydma

$H_s = 7\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	2	9	19	·	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	8	·	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	3	·	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	7	·	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	·	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	5	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	3	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	·	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	1	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	·	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	6	·	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5	8	18	·	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7	17	61	9	–	–	–	–	–	–	–	–	–	–

Lębork

$H_s = 18\,m$ $H_b = 21{,}8\,m$ $h_w = 12\,m$

I	1	2,5	8	1,4	6,5	1,5	13	2,2	22	1,6	21,5	3,0	15	3,0	3	1,8	3	2,2	32,9	9,6	30	5	9	18	·	·	·	2	18	14	9	·	2	8	·
II	0,5	2,0	1	2,0	1,5	2,3	13,5	1,9	10	2,7	20,5	2,3	32,5	2,2	3,5	2,9	1	2,2	48,1	24,3	28	·	·	8	·	·	·	1	20	14	9	1	3	4	·
III	3,5	4,3	·	·	·	·	·	·	3	2,7	10	2,2	66	4,2	10,5	4,6	·	4,0	33,5	9,4	29	·	·	6	·	1	·	1	16	14	6	·	1	4	·
IV	1	2,0	7,5	2,3	23,5	2,2	14,5	2,4	3	2,2	8	1,9	17	2,2	11,5	2,8	4	2,2	4,7	1,3	1	·	·	10	·	·	·	8	3	6	3	·	2	2	2
V	9	2,3	9,5	1,8	8	2,1	6	2,1	3,5	2,3	11,5	1,8	20,5	2,4	18	2,2	7	2,0	86,7	20,5	14	·	·	2	·	·	·	·	12	17	14	2	3	·	2
VI	·	·	7	1,5	12,5	1,5	7	2,3	4,5	2,7	7	2,7	34	3,0	9	3,3	4	2,4	52,1	18,6	14	·	·	·	10	·	·	2	8	10	7	1	·	·	4
VII	1,5	2,0	3	1,3	2,5	1,8	4	1,8	4	1,9	36,5	2,7	25,5	2,5	15	1,5	1	2,2	108,7	32,4	31	·	·	·	4	·	·	2	24	24	15	4	·	·	8
VIII	·	·	·	·	3	1,0	5	1,0	6	2,0	26	2,5	38,5	2,4	13,5	2,6	1	2,3	74,5	15,8	22	·	·	·	1	·	·	·	18	19	14	1	1	·	2
IX	5	1,0	1	3,0	10,5	2,2	11	1,9	4,5	2,1	15,5	1,7	27	2,0	3,5	2,7	12	1,7	59,1	13,3	7	·	·	·	3	·	·	7	9	11	9	3	4	·	2
X	·		1,5	1,0	12,5	2,0	25,5	1,9	11,5	2,3	19	2,4	14	2,3	3	3,2	6	2,0	30,3	7,5	18	·	·	·	·	·	·	5	11	11	8	·	3	·	·
XI	4,5	2,7	6,5	2,5	16,5	2,3	11	1,2	5,5	1,5	16,5	4,0	16	3,1	5,5	2,1	8	2,4	34,2	5,7	30	·	·	9	·	·	·	1	17	17	9	·	5	·	·
XII	5,5	3,0	1,0	2,0	9,5	1,8	11,5	1,1	9,5	1,4	24,5	3,0	13,5	4,2	7	2,0	2	2,5	47,6	15,8	2	8	11	23	·	3	1	·	14	16	10	1	1	19	·
Rok	31,5	1,8	5,5	1,6	111,5	1,7	122	1,6	87	2,1	216,5	2,5	319,5	2,8	103	2,5	49	2,3	612,4	32,4	31. VII	13	20	76	18	4	1	29	170	173	113	13	25	37	20

Gdynia

$\varphi = 54°31'$ $\lambda = 18°34'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnio				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1015.9	1042.3	993.8	1017.8	1.9	−2.0	6.2	31	−8.6	25	−1.1	0.8	−0.1	−0.1	4.7	5.0	5.0	4.9	79	74	78	77	1.1	1.6	1.3	1.3	7.9	7.8	7.8	7.8
II	1017.5	1035.7	988.9	1019.4	5.2	1.2	16.2	18	−2.8	6	2.1	3.8	2.7	2.8	6.5	6.6	6.5	6.5	90	82	87	86	0.8	1.6	1.0	1.1	9.1	8.4	7.9	8.5
III	1010.6	1031.0	985.6	1012.4	9.2	3.3	17.8	10	−2.9	20	4.8	7.6	5.8	6.0	6.9	6.6	7.0	6.8	79	63	75	72	1.9	4.1	2.4	2.8	7.9	7.2	5.3	6.8
IV	1011.7	1025.7	1001.7	1013.5	11.5	4.4	23.9	7	−1.2	11	6.5	9.1	7.6	7.7	7.6	8.0	7.8	7.8	77	69	74	73	2.4	4.1	2.8	3.1	4.9	5.2	3.6	4.6
V	1009.8	1018.2	999.1	1011.6	13.2	7.5	18.4	30	2.4	2	9.7	11.2	9.4	9.9	9.9	10.3	9.8	10.0	82	77	83	81	2.2	3.2	2.0	2.5	7.9	7.8	6.8	7.5
VI	1011.8	1024.0	1001.3	1013.5	21.1	13.9	27.5	25	9.1	1	16.2	19.4	16.6	17.2	14.3	14.4	14.8	14.5	77	65	78	73	4.3	8.4	4.3	5.7	4.9	5.3	5.7	5.3
VII	1008.9	1024.6	993.9	1010.6	19.4	13.0	32.8	3	9.4	6	15.3	17.7	15.8	16.2	14.2	14.8	14.5	14.5	82	72	80	78	3.3	5.8	3.6	4.2	7.5	8.1	7.5	7.7
VIII	1011.5	1027.2	998.8	1013.2	19.1	13.3	26.8	6	11.4	26, 30	14.9	17.9	15.2	15.8	14.5	14.5	14.6	14.5	85	71	85	80	2.6	6.3	2.7	3.9	7.6	7.5	6.8	7.3
IX	1015.7	1029.2	998.8	1017.4	18.5	11.8	28.7	17	5.8	24	13.4	17.5	14.5	15.0	13.2	13.6	13.5	13.4	84	68	81	78	2.5	6.8	3.2	4.2	4.7	5.3	4.5	4.8
X	1016.3	1030.7	999.1	1018.1	14.4	9.6	18.4	10	5.7	23	10.5	13.3	11.9	11.9	11.3	11.7	11.9	11.6	88	77	85	83	1.5	3.7	2.1	2.4	6.8	7.0	5.2	6.3
XI	1011.1	1032.7	990.1	1012.9	7.3	3.8	11.8	1	−1.0	23	5.1	6.5	5.5	5.6	7.6	7.8	7.6	7.7	85	80	83	83	1.4	2.0	1.6	1.7	8.8	8.3	7.7	8.3
XII	1011.7	1044.5	981.7	1013.6	1.8	−2.9	13.3	5	−14.4	28	−0.7	0.3	−0.9	−0.6	5.1	5.1	4.9	5.0	81	76	81	79	1.1	1.5	1.1	1.2	8.0	7.8	6.8	7.5
Rok	1012.7	1044.5	981.7	1014.5	11.9	6.4	32.8	3.VII	−14.4	28.XII	8.1	10.4	8.7	9.0	9.6	9.9	9.8	9.8	82	73	81	79	2.1	4.1	2.3	2.8	7.2	7.1	6.3	6.9

Słupsk

$\varphi = 54°28'$ $\lambda = 17°01'$

I	–	–	–	–	1.6	−3.5	6.5	29	−12.2	25	−2.0	0.9	−1.3	−0.9	4.6	5.1	4.7	4.8	82	74	79	78	0.9	1.6	1.1	1.2	6.9	6.5	6.1	6.5
II	–	–	–	–	5.3	0.7	13.8	18	−5.1	5	1.7	4.4	2.6	2.8	6.3	6.8	6.5	6.5	90	82	87	86	0.7	1.7	1.0	1.1	8.4	8.3	8.6	8.4
III	–	–	–	–	8.3	2.7	17.6	10	−4.1	20	4.0	6.9	4.8	5.1	6.8	7.4	7.2	7.1	82	74	83	80	1.4	2.7	1.5	1.9	7.9	7.1	6.2	7.1
IV	–	–	–	–	14.6	3.5	24.5	14	−2.2	12	6.5	13.2	7.9	8.9	7.1	7.0	7.5	7.2	72	46	70	63	2.7	9.2	3.5	5.1	4.3	4.1	2.5	3.6
V	–	–	–	–	14.9	6.4	25.3	30	0.6	13	9.8	13.7	9.2	10.5	9.8	9.9	9.7	9.8	80	64	83	76	2.5	6.2	2.1	3.6	7.6	6.8	5.7	6.7
VI	–	–	–	–	22.8	12.1	29.3	27	7.3	22	16.6	21.1	16.3	17.5	14.4	13.1	14.3	13.9	76	54	78	69	4.7	12.7	4.4	7.3	5.2	5.0	4.9	5.0
VII	–	–	–	–	19.5	11.5	32.3	3	6.4	1	14.6	18.1	14.5	15.5	14.1	14.0	14.4	14.2	84	69	83	79	2.7	7.5	2.2	4.1	8.1	7.3	7.7	7.7
VIII	–	–	–	–	19.2	11.8	26.3	31	8.6	13	14.2	17.8	14.3	15.2	14.4	14.4	14.3	14.4	88	71	88	82	1.9	6.4	2.0	3.4	7.6	8.1	6.3	7.3
IX	–	–	–	–	19.5	9.3	28.8	17	1.9	25	11.5	18.7	12.8	14.0	12.6	13.4	12.9	13.0	89	61	86	79	1.5	7.7	2.1	3.8	4.9	5.3	3.8	4.7
X	–	–	–	–	15.3	8.0	20.3	10	3.3	30	9.7	14.6	10.7	11.4	10.4	10.9	10.7	10.7	86	66	83	78	1.7	5.9	2.4	3.3	6.5	5.8	4.8	5.7
XI	–	–	–	–	7.2	2.2	11.9	2	−7.3	23	4.0	6.6	4.1	4.7	7.3	7.4	7.0	7.2	87	75	83	82	1.1	2.4	1.5	1.7	8.9	7.5	7.5	8.0
XII	–	–	–	–	1.4	−5.0	13.7	5	−19.6	26	−2.4	0.1	−1.8	−1.5	4.7	5.1	4.7	4.8	83	77	82	81	0.9	1.5	1.0	1.1	7.5	7.3	6.8	7.2
Rok	–	–	–	–	12.5	5.0	32.3	3. VII	−19.6	26. XII	7.4	11.3	7.8	8.6	9.4	9.5	9.5	9.5	83	68	82	78	1.9	5.5	2.1	3.2	7.0	6.6	5.9	6.5

Darłowo

$\varphi = 54°27'$ $\lambda = 16°23'$

I	–	–	–	–	1.4	−3.5	6.0	29	−12.9	25, 26	−1.9	0.5	−1.1	−0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.9	6.7	6.7
II	–	–	–	–	4.7	0.6	12.3	18	−4.9	5	2.0	3.8	2.2	2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	8.0	8.0
III	–	–	–	–	6.7	2.7	14.8	10	−1.3	20	3.8	5.2	4.5	4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.1	5.3	6.9	6.5
IV	–	–	–	–	12.7	3.3	24.8	14	−2.8	8	6.5	10.7	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.0	3.6	3.9
V	–	–	–	–	13.0	6.8	21.0	5	0.7	13	9.6	10.8	9.2	9.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.0	7.4	7.0
VI	–	–	–	–	20.0	12.6	28.9	27	7.0	22	15.4	17.1	15.6	15.9	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.2	5.7	5.2
VII	–	–	–	–	18.5	12.5	31.8	13	8.0	6	15.1	17.1	15.0	15.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.9	7.8	7.6
VIII	–	–	–	–	17.8	13.0	25.4	10	9.9	4	14.8	16.4	15.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	7.0	7.0
IX	–	–	–	–	16.8	10.9	27.1	1	4.2	24	12.5	17.4	13.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	3.1	4.1	4.0
X	–	–	–	–	14.8	8.6	20.3	6	4.0	30	9.8	14.1	10.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.3	5.6	5.7
XI	–	–	–	–	7.3	3.3	11.8	2	−4.9	23	4.9	6.4	5.0	5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	8.1	8.1
XII	–	–	–	–	–	−3.6	13.3	5	−17.8	28	−1.6	−0.2	−0.8	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.2	7.8
Rok	–	–	–	–	–	5.6	31.8	13.VII	−17.8	28. XII	7.6	9.9	8.0	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.0	6.4	6.5

Gdańsk – Nowy Port

$\varphi = 54°24'$ $\lambda = 18°40'$

I	–	–	–	–	1.4	−3.4	5.7	31	−11.7	26	−2.0	0.6	−1.1	−0.9	4.7	5.3	5.0	5.0	83	79	84	82	0.8	1.2	0.8	0.9	7.6	6.9	6.4	7.0
II	–	–	–	–	4.8	0.7	15.7	18	−4.5	5	1.6	3.7	2.3	2.5	6.4	6.7	6.5	6.5	93	84	89	89	0.5	1.5	0.8	0.9	8.3	7.7	8.0	8.0
III	–	–	–	–	9.0	2.8	17.9	10	−3.9	20, 21	4.7	7.8	5.6	5.9	6.7	6.4	6.8	6.6	78	61	74	71	2.0	4.5	2.5	3.0	6.8	5.6	5.1	5.8
IV	–	–	–	–	12.3	3.9	24.5	7	−1.5	2	6.4	11.0	7.6	8.2	7.4	8.0	7.9	7.8	75	61	74	70	2.6	6.0	2.9	3.8	4.2	5.1	2.9	4.1
V	–	–	–	–	13.8	2.0	22.1	30	2.2	2	9.6	12.2	9.3	10.1	9.9	10.2	9.9	10.0	82	73	84	80	2.2	4.3	2.0	2.8	6.8	7.5	5.8	6.1
VI	–	–	–	–	21.8	13.4	29.0	26, 27	8.2	1	16.5	20.2	16.5	17.4	14.6	14.5	14.5	14.5	77	62	77	72	4.3	9.7	4.5	6.2	4.1	4.1	5.2	4.5
VII	–	–	–	–	19.8	12.4	33.9	3	8.7	6	15.3	18.3	15.3	16.0	14.2	14.3	14.3	14.3	82	69	82	78	3.3	7.2	3.2	4.6	7.7	7.3	6.9	7.3
VIII	–	–	–	–	19.7	12.6	28.0	6	10.7	4	14.6	18.6	14.8	15.7	14.3	14.0	14.5	14.3	86	66	86	79	2.4	7.9	2.4	4.2	6.8	7.3	6.0	6.7
IX	–	–	–	–	19.0	10.5	28.6	17	4.0	28	12.1	18.4	13.9	14.6	12.6	13.5	13.1	13.1	88	64	81	78	1.9	8.1	3.0	4.5	4.0	4.7	3.5	4.1
X	–	–	–	–	14.7	7.6	19.5	6	3.0	31	8.8	14.1	11.0	11.2	10.2	11.4	11.1	10.9	90	72	84	82	1.2	4.9	2.1	2.7	5.6	5.9	3.4	5.0
XI	–	–	–	–	7.0	2.8	11.9	1	−4.9	23	4.3	6.2	5.0	5.1	7.5	8.0	7.5	7.7	89	83	84	85	1.0	1.6	1.4	1.3	8.5	7.9	7.2	7.9
XII	–	–	–	–	1.2	−4.3	13.4	5	−18.5	28	−2.0	−0.3	−1.7	−1.4	4.6	4.9	4.8	4.8	81	77	82	80	1.1	1.5	1.0	1.2	6.5	6.1	6.5	6.4
Rok	–	–	–	–	12.0	5.5	33.9	3.VII	−18.5	28. XII	7.5	10.9	8.2	8.7	9.4	9.8	9.7	9.6	84	71	82	79	1.9	4.9	2.2	3.0	6.4	6.3	5.6	6.1

Gdynia $H_s = 2 m$ $H_b = 14{,}5 m$ $h_w = $ 25 m anemograf / 12,5 m wiatromierz Wilda **1961**

MIESIĄC	ROZKŁAD WIATRU $^nD, ^vmD$ N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	v>15	◉	●	Opad R ≥0.1	R≥1.0	R≥10.0	≡	⊞	R
I	3.5	6.9	3	7.3	3	6.5	25	9.2	22.5	5.6	30	4.3	19.5	4.2	8	5.6	1	5.1	25.8	6.2	30	·	7	17	·	5	·	1	19	15	8	·	3	6	·
II	1	2.0	1	6.0	·	·	5.5	6.1	23.5	6.3	16.5	3.9	19.5	3.8	14	4.8	3	4.7	36.3	17.0	28	·	·	7	·	8	·	·	19	12	8	1	3	·	·
III	1	9.0	·	·	·	·	·	·	3	5.7	6.5	7.6	56	6.8	25.5	8.2	1	7.2	36.8	7.8	12	·	·	4	·	24	2	2	9	13	10	·	·	2	·
IV	7	4.2	7	5.6	9.5	6.2	14	4.8	17	4.4	9	4.2	13.5	4.1	12	4.5	1	4.6	9.2	2.6	4	·	·	4	·	8	·	9	3	9	3	·	5	·	1
V	16	4.1	3.5	4.9	4	3.5	6.5	4.5	9.5	4.5	12	4.4	17	4.1	20.5	4.3	4	4.1	57.2	17.5	14	·	·	·	·	1	·	1	13	19	12	1	3	·	3
VI	5.5	4.3	4	3.2	4.5	4.8	7	3.6	8	4.1	9.5	3.6	30	5.3	15.5	5.4	6	4.4	40.5	19.2	14	·	·	·	5	6	1	4	6	10	6	1	·	·	6
VII	3.5	4.6	2.5	3.2	4	4.5	6	3.8	12	3.0	32	4.3	23.5	4.7	6.5	4.8	3	4.1	114.6	30.1	31	·	·	·	1	7	·	1	18	24	15	4	·	·	7
VIII	3.5	2.6	·	·	0.5	4.0	4	4.4	5.5	3.6	28	3.7	37.5	4.8	13	5.4	1	4.3	86.1	24.5	23	·	·	·	2	4	·	·	12	18	15	2	·	·	2
IX	1	4.5	1.5	4.3	11	4.3	12	6.6	10	6.2	16.5	3.7	23	3.6	9	4.8	6	4.3	25.8	12.4	14	·	·	·	2	5	·	8	7	10	5	1	·	·	·
X	·	·	·	·	2	5.7	23	7.8	34.5	6.6	13	4.6	11.5	5.2	7	4.9	2	6.2	41.0	20.4	18	·	·	·	·	16	·	5	13	12	8	1	1	·	·
XI	4.5	6.0	5	8.2	5	9.4	12	9.5	9	5.0	21.5	5.1	23.5	4.3	8.5	4.9	1	5.8	40.7	16.7	11	·	·	4	·	12	1	1	21	18	8	1	7	·	·
XII	4	8.0	6.5	9.8	1.5	7.7	3	5.7	22.5	5.6	20	6.0	22.5	6.5	13	5.5	·	6.3	43.1	14.9	2	5	9	18	·	18	3	·	15	13	11	1	4	17	·
Rok	50.5	4.7	34	4.4	45	4.7	95.5	5.5	177	5.0	214.5	4.6	297	4.8	152.5	5.3	29	5.1	557.1	30.1	31. VII	5	16	54	10	114	7	32	155	173	109	13	26	25	19

Uwaga. Obserwacji nad wiatrem w terminach klimatologicznych dokonywano za pomocą wiatromierza Wilda, w czasie między terminami – za pomocą anemografu.

Słupsk $H_s = 16 m$ $h_w = 17 m$

I	3	1.0	0.5	1.0	3	1.3	5	2.8	28	1.7	12	3.9	1.5	1.0	1	1.0	39	1.3	54.8	15.4	30	5	10	19	·	1	·	6	15	15	10	2	2	10	·
II	2	1.5	1	2.0		·	5	2.6	28.5	2.0	15	2.3	10.5	2.0		·	22	1.6	62.9	23.6	28	·	·	8	·	·	·	1	20	18	9	2	3	4	·
III	2	5.0	·	·	·	·	·		5	4.0	28.5	5.1	42.5	6.4	4	4.0	11	5.0	49.4	11.5	29	·	·	4	·	9	5	1	11	14	12	2	4	2	·
IV	·	·	12.5	2.0	10	2.8	11.5	3.5	5	2.5	7	2.1	5	3.0	4	3.4	35	1.6	12.5	6.2	1	·	·	7	·	1	·	12	2	5	4	·	1	1	1
V	14	2.0	6	1.8	1	2.0	5	3.4	5	1.4	13	2.4	9	2.6	10	2.1	30	1.5	90.2	24.3	14	·	·	·	1	·	·	2	12	15	11	4	·	·	2
VI	·	·	3	2.7	13	1.6	2	5.0	5.5	1.8	17	3.7	21.5	4.2	1	1.0	27	2.3	49.0	11.2	10	·	·	·	11	4	2	4	4	11	9	1	·	·	1
VII	1	1.0	·	·	0.5	1.0	2.5	2.8	14	2.0	23.5	2.2	14	2.0	1.5	1.3	36	1.3	167.3	41.8	31	·	·	·	3	·	·	2	22	24	20	4	·	·	3
VIII	·	·	·	·	1.5	1.0	0.5	1.0	5.5	1.8	26	2.1	17.5	3.0	4	1.8	38	1.3	122.2	34.9	22	·	·	·	2	·	·	·	13	20	17	4	1	·	2
IX	1	1.0	1	4.0	8.5	2.6	6.5	2.2	3	1.3	17	2.0	6	3.0	2	1.5	45	1.1	105.5	36.1	7	·	·	·	3	·	·	10	7	12	11	3	2	·	3
X	·	·	1	2.5	14.5	2.8	16.5	2.8	13	2.5	10	2.2	4	2.4	2	2.5	32	1.7	38.4	9.6	31.	·	·	·	·	1	·	7	12	12	8	·	2	·	·
XI	4	1.6	6	4.6	8.5	1.6	7	1.5	6.5	3.1	19	3.0	4	2.8	3	2.2	32	1.7	35.1	12.2	30	·	·	8	·	1	·	1	18	14	10	1	4	·	·
XII	7.5	3.3	6.5	1.4	0.5	2.0	8	1.7	21.5	2.2	17	3.6	5.5	5.6	3.5	1.6	23	2.1	63.1	16.6	2	9	10	23	·	3	·	·	10	14	10	1	1	15	1
Rok	34.5	1.4	37.5	1.8	61	1.6	69.5	2.4	140.5	2.2	205	2.9	141	3.2	36	1.9	370	1.9	850.4	41.8	31. VII	14	20	69	20	19	7	46	146	174	131	24	20	32	13

Darłowo $H_s = 3 m$ $h_w = 23 m$

I	3	3.2	6.5	2.8	14	2.2	18	2.6	25.5	4.1	16	5.9	5.5	6.6	4.5	4.7	·	3.9	43.8	8.5	30	3	10	18	·	3	·	4	14	—	11		3	6	—
II	3.5	4.6	1.5	3.3	3	4.3	9	2.8	21	4.1	23	4.2	18	5.3	2	5.0	3	4.1	57.0	22.8	28	·	·	8	·	1	·	1	17	—	10	1	13	4	—
III	5	9.7	·	·	·	·		·	3	7.0	23	6.6	57.5	9.3	4.5	9.0		8.6	42.1	10.6	31	·	·	2	·	15	5	1	9	—	10	1	8	·	—
IV	4.5	2.4	14.5	3.5	27.5	2.8	11.5	2.8	4	2.7	13	3.9	9.5	4.9	5.5	4.5	·	3.4	6.2	3.2	17	·	·	7	·	1	·	10	5	—	2	·	5	·	—
V	18.5	5.5	14.5	4.7	5.5	2.4	3	2.3	6	2.3	19	3.9	19	4.8	25	5.3	·	4.4	76.1	30.0	13	·	·	·	·	1	·	2	15	—	11	1	—	·	—
VI	3	4.3	14.5	3.1	11.5	1.3	4	1.5	6	2.7	20.5	5.6	27	8.2	1.5	3.7	2	4.9	47.9	13.6	10	·	·	·	4	6	3	4	6	—	9	1	2	·	—
VII	2.5	7.8	3	5.3	4.5	2.6	5.5	1.7	16	3.3	27	3.8	26	9.1	4.5	7.4	4	5.2	161.0	50.2	31	·	·	·	3	8	·	2	17	—	19	5	2	·	—
VIII	1	3.0	0.5	2.0	1.5	1.3	3	2.7	16.5	2.9	27.5	5.7	32	6.6	3	9.2	8	4.9	88.8	25.0	15	·	·	·	1	7	·	1	9	—	16	3	1	·	—
IX	3.5	1.9	5.5	2.5	18.5	2.4	12.5	2.8	7.5	2.0	17	6.1	17.5	6.7	5	4.7	3	4.0	65.7	25.4	7	·	·	·	1	2	·	11	3	—	8	3	2	·	—
X	0.5	3.0	3	4.6	16	3.3	29	3.5	19.5	3.8	12.5	3.9	11	6.8	1.5	6.3	·	4.0	18.9	4.3	19	·	·	·	·	1	·	9	12	—	6	·	1	·	—
XI	9.5	5.8	10	5.0	18.5	3.4	8.5	2.4	13.5	4.2	16.5	9.0	8	5.1	4.5	7.3	1	5.2	29.4	8.4	30	·	·	4	·	6	3	·	19	—	10		3	·	—
XII	9	10.6	5.5	3.8	11	2.0	16.5	2.6	17	3.5	19.5	9.2	9	9.0	5.5	5.0	·	5.7	52.2	—	—	7	—	19	—	11	3	·	13	—	7		—	8	—
Rok	63.5	5.2	79	3.4	131.5	2.3	120.5	2.3	155.5	3.6	234.5	5.6	240	6.9	49.5	6.0	21	4.9	689.1	50.2	31. VII	10	—	58	—	62	14	45	139	—	119	15	—	18	—

Gdańsk - Nowy Port $H_s = 7 m$ $h_w = 13 m$

I	3	4.8	3	5.0	3	3.7	14	3.2	21	2.9	17.5	3.7	8.5	5.5	11	4.0	12	3.2	15.0	3.7	30	3	8	20	·	3	1	1	14	13	6	·	·	—	·
II	2.5	2.6	1.5	4.3	0.5	1.0	10.5	3.9	19.5	5.0	12	3.3	16.5	3.3	15	4.5	6	3.7	31.3	11.2	28	·	·	10	·	2	·	1	17	12	7	1	9	—	·
III	1	12.0	·	·	·	·	·	·	6	2.0	14	6.4	50.5	8.0	19.5	8.3	2	7.3	17.8	3.9	29	·	·	7	·	24	5	4	7	11	6	·	1	—	·
IV	11	5.4	11.5	3.4	11	3.9	14	3.1	7.5	4.3	4	3.4	8	4.2	9	4.9	14	3.4	6.9	1.5	4	·	·	3	·	3	·	11	3	8	5	·	—	·	2
V	18.5	4.5	8.5	4.1	3.5	1.9	4	2.8	9	3.6	10.5	3.8	11.5	3.0	16.5	4.6	11	3.4	63.2	20.5	6	·	·	·	·	4	·	2	11	16	13	1	6	·	4
VI	7.5	3.3	6	2.6	8.5	1.5	7	2.4	4	2.0	7	4.6	28	4.6	10	4.6	12	3.2	94.5	36.2	14	·	·	·	7	2	2	7	4	9	6	4	—	·	6
VII	3.5	3.9	0.5	5.0	3.5	3.0	7	2.1	10	2.6	28.5	3.6	14	4.1	4	4.5	22	2.7	94.9	24.0	31	·	·	·	1	1	·	2	14	20	15	3	—	·	7
VIII	1.5	1.3	2.5	2.2	2	2.0	3.5	2.1	7.5	3.7	20	3.6	35	4.2	10	4.4	11	3.3	74.0	15.5	23	·	·	·	2	2	1	·	7	18	12	4	—	·	3
IX	2	4.0	4	2.5	7	2.4	9.5	3.2	9	2.5	9.5	3.2	18.5	3.9	5.5	3.9	25	2.4	26.3	11.8	14	·	·	·	3	·	·	10	3	9	4	1	—	·	·
X	·	·	0.5	1.0	10.5	2.7	26.5	2.9	19.5	2.9	11.5	3.2	8	3.1	6.5	3.8	10	2.7	39.9	22.7	18	·	·	·	·	·	·	7	5	10	7	1	—	·	·
XI	5	7.4	5.5	8.5	10	6.7	10.5	2.5	13	2.9	13.5	5.3	19	4.0	6.5	5.9	7	4.5	32.8	16.8	11	·	·	6	·	8	2	2	18	12	9	1	—	·	·
XII	8	11.1	6	6.8	1	5.0	14.5	4.2	17	3.2	15.5	5.3	16.5	6.5	10.5	5.9	4	5.4	34.8	10.0	2	6	9	22	·	14	3	2	13	13	9	·	—	—	·
Rok	53.5	5.8	49.5	3.8	60.5	2.8	121	2.7	143	3.1	163.5	4.1	234	4.5	124	4.9	136	3.8	531.4	36.2	14. VI	9	17	68	13	63	14	49	116	151	99	16	—	—	22

Gdańsk – Wrzeszcz $\varphi = 54°23'$ m $\lambda = 18°36'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1016.4	1042.8	994.2	1018.0	1.4	−3.6	5.9	31	−11.8	25	−1.9	0.3	−1.1	−1.0	4.6	4.9	4.9	4.8	82	75	81	79	0.9	1.5	1.0	1.1	7.0	7.4	6.6	7.0
II	1017.8	1036.2	989.0	1019.4	5.0	0.6	16.1	18	−5.2	5	1.8	3.8	2.4	2.6	6.4	6.6	6.5	6.5	92	82	88	87	0.6	1.6	0.9	1.0	8.0	8.4	8.1	8.2
III	1011.3	1031.4	985.3	1012.8	9.3	2.8	18.6	10	−3.4	20	4.6	7.8	5.5	5.8	6.9	6.6	7.0	6.8	81	63	77	74	1.7	4.2	2.2	2.7	7.1	6.8	4.7	6.2
IV	1012.1	1026.0	1001.8	1013.6	13.3	3.6	24.3	7	−3.0	2	6.5	11.6	7.7	8.4	7.4	7.4	7.6	7.5	75	54	72	67	2.7	7.1	3.3	4.4	4.8	4.9	3.3	4.3
V	1010.2	1017.4	998.4	1011.7	14.1	6.6	22.0	5	1.3	2	9.8	12.8	9.2	10.2	10.0	10.1	9.9	10.0	82	70	85	79	2.2	5.1	1.9	3.1	6.9	8.0	6.0	7.0
VI	1012.3	1024.4	1001.2	1013.8	22.5	13.3	29.6	27	7.8	1	16.6	21.0	16.7	17.8	14.0	13.4	14.2	13.9	74	55	75	68	5.9	12.0	5.0	7.3	4.5	4.7	4.9	4.7
VII	1009.4	1025.1	993.2	1010.9	20.2	12.5	33.1	3	8.9	6	15.2	18.5	15.5	16.2	14.0	14.0	14.1	14.0	81	67	80	76	3.4	7.8	3.6	4.9	7.3	8.0	7.3	7.5
VIII	1012.0	1027.9	998.5	1013.5	19.7	12.5	27.3	6	10.5	4	14.7	18.5	14.6	15.6	14.3	13.7	14.4	14.1	86	65	86	79	2.4	7.9	2.4	4.2	7.3	7.8	6.2	7.1
IX	1016.2	1029.6	998.8	1017.7	19.4	10.4	28.8	17	3.1	24	12.1	16.6	13.4	14.4	12.6	12.6	12.7	12.6	87	59	82	76	2.0	9.3	2.9	4.7	4.8	4.7	4.1	4.5
X	1016.8	1031.2	989.8	1016.3	14.9	7.8	19.6	4, 5, 10	3.3	23	9.0	14.0	10.9	11.2	10.3	11.2	11.2	10.9	89	71	86	82	1.3	5.0	1.9	2.7	6.2	6.6	4.0	5.6
XI	1012.0	1033.7	991.9	1013.6	6.9	2.5	11.7	1	−4.6	23	4.1	6.0	4.9	5.0	7.4	7.6	7.4	7.5	88	81	84	84	1.0	1.8	1.4	1.4	8.4	8.4	7.2	8.0
XII	1012.7	1045.7	983.1	1014.3	1.3	−4.7	13.7	5	−17.5	28	−1.8	−0.5	−2.1	−1.6	4.8	5.0	4.7	4.8	82	79	82	81	1.0	1.3	1.0	1.1	6.8	7.2	6.3	6.8
Rok	1013.3	1045.7	983.1	1014.8	12.3	5.4	33.1	3. VII	−17.5	28. XII	7.6	11.0	8.1	8.7	9.4	9.4	9.6	9.5	83	68	82	78	2.0	5.4	2.3	3.2	6.6	6.9	5.7	6.4

Gdańsk – Siedlce $\varphi = 54°21'$ $\lambda = 18°36'$

I	–	–	–	–	−0.9	−4.1	5.2	31	−13.3	26	−2.4	−0.1	−1.8	−1.5	4.6	5.0	4.8	4.8	84	79	84	82	0.7	1.2	0.8	0.9	6.9	7.9	6.5	7.1
II	–	–	–	–	4.5	0.2	15.7	18	−5.2	6	1.2	3.3	2.0	2.1	6.3	6.7	6.5	6.5	94	86	92	91	0.4	1.3	0.6	0.8	8.1	8.8	7.9	8.3
III	–	–	–	–	8.9	2.3	18.0	10	−4.7	20	4.1	7.5	5.0	5.4	6.9	6.8	7.1	6.9	84	65	81	77	1.4	3.8	1.8	2.3	7.9	6.7	4.0	6.2
IV	–	–	–	–	13.9	3.7	23.6	7	−3.5	2	6.4	12.1	7.5	8.4	7.4	7.5	8.0	7.6	75	53	75	68	2.6	7.4	2.9	4.3	5.1	5.5	2.7	4.4
V	–	–	–	–	14.6	6.4	21.8	5	1.7	2	9.7	13.1	8.8	10.1	10.2	10.3	10.0	10.2	84	69	87	80	2.0	5.2	1.8	3.0	7.0	8.3	6.5	7.3
VI	–	–	–	–	22.8	12.9	29.4	27	8.1	1	16.7	21.3	16.1	17.6	14.6	14.3	14.4	14.4	76	57	78	70	4.6	11.6	4.1	6.8	4.9	5.8	4.9	5.2
VII	–	–	–	–	20.5	11.7	33.4	3	7.4	6	15.3	18.5	14.6	15.8	14.5	15.0	14.4	14.6	84	72	86	91	3.0	6.9	2.4	4.1	8.0	8.1	8.6	8.2
VIII	–	–	–	–	19.8	12.1	27.4	6	9.5	18	14.3	18.3	13.9	15.1	14.5	14.8	14.4	14.6	89	71	90	83	1.8	6.6	1.6	3.3	8.6	8.4	6.5	7.8
IX	–	–	–	–	19.4	9.8	28.8	2	4.2	22	11.9	18.5	12.6	13.9	12.8	13.5	12.9	13.1	90	63	87	80	1.6	8.3	1.9	3.9	4.9	5.0	3.7	4.5
X	–	–	–	–	14.5	7.2	18.9	10	2.5	23	8.4	13.6	10.0	10.5	10.6	11.7	11.1	11.1	95	76	90	87	0.6	4.1	1.2	2.0	6.3	6.9	2.9	5.4
XI	–	–	–	–	6.5	2.1	11.2	1	−4.4	23	3.6	5.5	4.2	4.4	7.5	7.8	7.6	7.6	93	85	90	89	0.6	1.4	0.8	0.9	8.9	8.6	6.5	8.0
XII	–	–	–	–	0.7	−5.4	12.6	5	−19.3	28	−2.7	−1.2	−2.7	−2.3	4.7	4.9	4.6	4.7	85	80	83	83	0.7	1.1	0.8	0.9	6.5	7.9	5.0	6.5
Rok	–	–	–	–	12.2	4.9	33.4	3. VII	−19.3	28. XII	8.2	10.9	7.5	8.3	9.6	9.9	9.6	9.7	86	71	85	81	1.7	4.9	1.7	2.8	6.9	7.3	5.5	6.6

Kamienica Królewska $\varphi = 54°23'$ $\lambda = 17°54'$

I	–	–	–	–	−0.1	−5.0	4.9	30	−17.8	25	−3.5	−1.0	−2.7	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	7.6	7.9
II	–	–	–	–	3.7	−0.6	13.6	18	−8.9	4	0.3	2.8	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.7	9.2	8.7	9.2
III	–	–	–	–	7.2	1.3	17.1	10	−5.9	20	2.9	5.8	3.4	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.3	6.7	7.5
IV	–	–	–	–	13.6	2.8	24.1	7	−7.9	2	6.1	12.2	6.5	7.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.6	3.7	4.4
V	–	–	–	–	14.5	5.6	24.1	30	0.1	13	9.0	13.0	8.1	9.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.7	7.6	7.3
VI	–	–	–	–	22.2	11.6	28.5	27	6.7	22	16.3	20.7	15.0	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	5.9	5.8
VII	–	–	–	–	19.0	10.4	32.4	3	6.0	1	14.0	17.5	13.3	14.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	8.0	8.1
VIII	–	–	–	–	18.4	10.8	25.6	6	7.4	4	13.4	17.2	13.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.6	6.9	7.5
IX	–	–	–	–	18.8	9.0	27.5	2	2.3	24	11.7	17.8	12.2	13.5	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.3	4.3	4.7
X	–	–	–	–	14.3	7.6	19.1	5, 6	1.6	31	8.9	13.3	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.7	5.5	5.9
XI	–	–	–	–	6.0	1.4	10.1	1, 2, 3	−4.9	23	2.8	4.7	3.4	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.6	8.1	8.5
XII	–	–	–	–	−0.2	−6.2	12.1	5	−19.8	17	−3.7	−1.6	−3.4	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	6.5	7.1
Rok	–	–	–	–	11.4	4.1	32.4	3. VII	−19.8	17. XII	6.5	10.2	6.6	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	6.6	7.0

Krynica Morska $\varphi = 54°23'$ $\lambda = 19°27'$

I	–	–	–	–	0.7	−3.7	5.6	4	−13.2	26	−2.4	−0.3	−1.4	−1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	6.3	6.9
II	–	–	–	–	3.5	−0.1	10.2	18	−5.3	6	0.7	2.4	1.4	1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.6	8.3	8.3
III	–	–	–	–	8.0	2.3	17.0	10	−2.0	20	3.6	6.6	4.7	4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.6	5.8	7.0
IV	–	–	–	–	12.6	4.5	22.7	7	−1.0	2	6.8	11.1	7.0	8.0	–	–	–	–	–	–	–	–	–	–	–	–	3.9	3.9	2.9	3.6
V	–	–	–	–	14.7	6.6	25.5	30	3.2	2	9.8	12.8	9.3	10.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	7.4	7.3
VI	–	–	–	–	22.6	13.3	28.6	10	8.9	22	16.7	20.7	16.5	17.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.4	4.4	4.5
VII	–	–	–	–	20.4	12.1	30.5	3	8.8	28	14.9	18.7	15.4	16.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.0	7.8	7.7
VIII	–	–	–	–	19.5	12.1	27.6	6	9.3	5	14.6	18.3	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.6	6.5	6.9
IX	–	–	–	–	19.3	10.9	26.6	2	5.7	24	12.8	18.2	13.9	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.4	4.2	4.2
X	–	–	–	–	14.7	9.0	18.2	4	5.0	23	9.8	14.0	11.5	11.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	6.5	6.7
XI	–	–	–	–	6.3	3.0	11.4	1	−1.4	24, 29	3.9	5.4	4.4	4.5	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.1	8.0	8.4
XII	–	–	–	–	0.7	−5.0	9.8	2	−16.4	28	−2.5	−1.1	−1.9	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	8.1	7.9
Rok	–	–	–	–	11.9	5.4	30.5	3. VII	−16.4	28. XII	7.4	10.6	8.0	8.5	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.5	6.4	6.6

Gdańsk - Wrzeszcz

$H_s = 13\,m$ $H_b = 12{,}4\,m$ $h_w = 15{,}5\,m$ **1961**

MIESIĄC	ROZKŁAD WIATRU [%D, %nD]																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v				Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	n ≥ 10	n ≥ 15	●	●	n ≥ 0.1	n ≥ 1.0	n ≥ 10.0	≡	▦	≋
I	25	52	5	46	1	4.0	85	34	24	36	165	49	75	63	7	46	21	34	21.1	4.4	30	4	9	20	·	1	·	2	14	15	8	·	·	13	·
II	2	42	2	32	·	·	11	35	235	39	115	31	185	42	75	54	8	36	34.9	14.7	28	·	·	8	·	2	·	1	18	12	6	1	2	2	·
III	25	24	·	·	·	·	05	30	45	46	155	66	46	86	17	81	7	23	19.4	4.0	12, 29	·	·	4	·	17	4	4	9	10	8	·	·	2	·
IV	9	46	15	42	35	50	165	31	65	27	4	50	85	53	6	51	22	31	8.9	2.1	1	·	·	5	·	2	·	8	2	8	4	·	2	1	2
V	19	59	115	48	2	25	15	37	75	33	14	60	9	35	85	49	20	37	46.7	10.4	6	·	·	·	·	1	·	1	11	16	12	2	1	·	2
VI	75	29	10	38	3	22	35	41	3	37	14	49	26	63	5	54	18	39	56.4	14.6	14	·	·	·	9	4	·	7	3	10	7	2	·	·	6
VII	25	50	4	32	1	45	2	25	165	31	335	49	105	56	4	56	19	35	86.0	24.4	31	·	·	·	3	1	·	1	15	19	12	2	·	·	5
VIII	2	35	3	27	·	·	1	20	13	31	265	48	205	60	11	40	16	38	73.0	12.0	10, 23	·	·	·	2	2	·	·	11	21	13	3	1	·	2
IX	2	30	55	35	3	32	85	19	65	42	17	47	105	59	8	52	29	29	33.5	11.7	14	·	·	·	3	1	·	9	5	9	5	2	·	·	·
X	·	·	1	40	4	26	22	35	225	36	115	41	7	62	4	60	21	31	41.6	23.0	18	·	·	·	·	1	·	5	9	12	8	1	1	·	·
XI	45	81	8	71	8	56	85	37	11	44	185	57	10	52	65	58	15	46	36.3	18.0	11	·	·	6	·	5	·	1	17	16	8	1	6	·	·
XII	55	11	7	76	·	·	105	21	175	27	24	69	11	70	75	61	10	51	44.8	11.7	2	6	10	22	·	10	5	1	12	14	11	1	3	18	·
Rok	59	42	72	41	25.5	25	93	30	156	36	206.5	50	185	58	92	55	206	40	502.6	24.4	31.VII	10	19	65	17	47	9	40	126	162	102	15	16	36	17

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Gdańsk - Siedlce

$H_s = 72\,m$ $h_w = 10\,m$

I	2	60	3	43	2	30	15	17	205	33	165	57	115	50	11	58	25	34	19.6	4.5	30	3	10	21	·	2	·	2	15	13	8	·	·	11	·
II	2	40	1	30	·	·	35	20	20	54	95	32	215	46	85	50	18	35	33.0	14.6	28	·	·	11	·	4	·	1	20	11	7	1	4	4	·
III	5	62	·	·	·	·	·	·	2	70	45	53	355	72	41	86	5	73	24.5	5.2	12	·	·	6	·	13	·	1	8	11	8	·	·	1	·
IV	14	46	9	44	85	43	115	37	18	33	7	44	65	42	75	45	8	37	10.8	2.2	8	·	·	6	·	1	·	8	3	9	6	·	1	·	2
V	30	49	95	52	3	38	25	28	65	44	115	48	85	47	65	52	15	40	64.6	11.5	3	·	·	·	·	1	·	2	14	16	14	2	1	·	2
VI	75	37	135	45	55	43	4	31	55	35	2	45	26	58	18	66	8	47	41.0	9.3	27	·	·	·	9	2	·	6	7	12	10	·	·	·	7
VII	4	28	2	30	35	47	15	10	10	29	185	48	315	37	6	45	16	32	80.3	25.0	31	·	·	·	3	·	·	1	22	17	14	2	·	·	6
VIII	15	43	15	30	·	·	3	33	7	37	11	46	27	48	14	48	28	32	80.6	12.6	6	·	·	·	2	·	·	·	16	22	15	3	·	·	2
IX	25	28	35	17	45	36	95	33	9	47	95	38	19	44	145	52	22	32	33.4	14.4	14	·	·	·	3	·	·	11	6	9	7	1	·	·	·
X	2	70	1	40	2	35	15	43	29	43	7	53	45	47	105	49	22	35	45.7	22.0	18	·	·	·	·	·	·	6	8	12	9	1	3	·	·
XI	85	51	6	57	45	57	85	46	9	29	10	68	19	42	85	51	16	40	43.8	14.4	11	·	·	8	·	1	·	1	18	17	12	1	3	·	·
XII	7	111	2	45	4	102	2	15	17	39	12	52	195	65	155	56	14	51	59.2	12.1	2	7	11	22	·	8	1	3	11	14	12	1	1	17	·
Rok	86	52	52	36	37.5	36	585	26	1535	41	119	49	230	50	161.5	55	197	41	536.5	25.0	31.VII	10	21	74	17	32	1	42	148	163	122	12	13	33	19

Kamienica Królewska

$H_s = 160\,m$ $h_w = 11\,m$

I	8	24	3	30	2	35	2	25	48	48	20	68	7	44	2	40	1	48	34.1	10.1	30	8	10	24	·	3	1	·	19	13	7	1	–	–	–
II	2	40							39	57	12	35	17	30	10	44	4	44	43.6	21.4	28	·	1	12	·	3	·	·	24	18	11	1	–	–	–
III	6	25	·	·					8	40	27	80	35	48	12	67	5	56	55.7	10.9	12	·	·	9	·	9	4	1	15	16	8	1	–	–	–
IV	10	30	6	30	16	29	5	68	24	50	6	32	16	34	2	10	5	36	8.9	3.6	5	·	·	9	·	1	1	6	3	7	2	·	–	–	–
V	27	24	5	32	5	32	4	42	14	46	6	40	22	36	3	20	7	30	84.5	25.3	14	·	·	·	·	1	·	·	15	13	13	1	–	·	–
VI	7	30	3	27	5	22	11	38	10	42	6	40	33	41	9	59	6	37	91.9	27.8	15	·	·	·	11	5	1	4	9	8	8	4	–	·	–
VII	11	17	·	·	·	·	4	62	23	37	17	49	28	42	11	30	9	36	89.2	20.8	18	·	·	·	4	3	·	2	19	21	14	3	–	·	–
VIII	8	39			·	·	·	·	23	40	14	43	28	41	11	30	9	36	154.8	45.6	1	·	·	·	1	1	·	1	15	18	17	7	–	·	–
IX	10	24	1	30	7	30	8	36	23	43	7	59	23	36	3	43	8	35	64.7	21.6	7	·	·	·	4	·	·	9	7	8	7	3	–	·	–
X	3	27	1	60	6	48	7	56	55	51	6	42	7	53	3	30	5	47	26.9	9.2	18	·	·	·	·	5	·	6	13	11	8	·	–	·	–
XI	9	26	2	40	2	40	3	47	23	42	19	44	18	40	2	35	12	35	38.8	7.5	30	·	·	9	·	5	·	·	23	14	11	·	–	·	–
XII	13	44	6	32	1	10	3	20	39	63	11	80	10	53	2	20	8	51	47.4	11.5	2	9	14	24	·	7	2	·	11	14	12	1	–	–	–
Rok	114	29	27	23	44	20	47	33	329	47	151	51	244	42	63	36	76	41	741.5	45.6	1.VIII	17	25	87	20	13	9	29	173	161	116	22	–	–	–

Krynica Morska

$H_s = 4\,m$ $h_w = 17\,m$

I	25	76	6	50	7	27	6	70	45	50	38	68	13	49	7	59	9	53	11.3	4.6	30	4	11	16	·	6	1	4	17	9	4	·	·	–	·
II	05	20	15	27	·	·	·	·	75	65	385	53	145	43	105	50	11	44	21.7	7.8	11	·	·	10	·	2	·	3	22	10	5	·	4	–	–
III	35	119	·	·	·	·	·	·	·	·	12	80	355	69	40	90	2	80	14.3	2.7	29	·	·	4	·	15	4	3	16	11	6	·	–	–	–
IV	14	41	10	54	9	36	18	53	3	33	8	33	15	50	125	50	14	39	17.8	5.8	17	·	·	2	·	1	·	15	6	9	7	·	–	·	–
V	15	39	10	34	6	40	5	42	2	55	205	53	11	58	115	50	12	41	74.4	21.4	7	·	·	·	1	1	·	4	18	14	10	2	·	·	–
VI	5	34	11	31	4	32	7	47	3	27	185	50	155	76	14	57	12	44	94.0	49.1	14	·	·	·	10	3	·	8	6	8	5	2	·	·	–
VII	2	20	05	20	1	45	05	70	2	60	44	62	145	67	65	50	22	46	143.4	29.8	13	·	·	·	2	5	·	11	20	20	17	4	1	·	–
VIII	1	20	1	20	15	23	05	30	1	20	315	55	28	52	125	61	16	44	119.4	18.7	10	·	·	·	1	3	·	3	13	20	16	5	1	·	–
IX	4	24	55	40	75	27	115	29	25	30	15	41	245	48	75	43	12	34	48.3	32.3	14	·	·	·	3	·	·	12	8	6	6	1	·	·	–
X	15	70	·	·	11	61	325	53	65	35	205	32	7	41	7	46	7	43	27.8	7.2	29	·	·	·	·	1	·	7	17	8	8	·	2	·	–
XI	35	30	5	59	135	70	105	51	3	58	225	47	115	54	85	65	12	48	25.8	4.4	10	·	·	5	·	4	·	1	22	12	9	·	–	·	–
XII	45	54	12	66	8	66	45	21	75	39	325	62	14	71	8	89	2	61	12.2	3.1	2	7	11	21	·	5	2	·	19	13	3	·	1	–	–
Rok	57	46	62.5	33	68.5	36	96	39	42.5	39	301.5	53	190.5	56	145.5	59	131	48	610.4	49.1	14.VI	11	22	58	17	46	7	61	184	140	96	14	–	–	–

Czarna Dąbrówka — φ = 54°21' — λ = 17°34' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA t								ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
									Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.1	−5.6	5.0	29,30	−17.1	26	−3.1	−0.4	−2.4	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.9	7.3	7.3
II	–	–	–	–	3.7	−0.7	12.6	18	−11.8	5	0.8	3.1	1.5	1.7	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.0	8.3	8.5
III	–	–	–	–	7.0	1.3	16.4	10	−8.6	20	3.1	6.1	3.9	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.6	7.2	7.9
IV	–	–	–	–	13.2	2.6	22.6	7	−8.2	2	6.1	12.7	6.5	8.0	–	–	–	–	–	–	–	–	–	–	–	–	4.3	3.7	3.2	3.7
V	–	–	–	–	13.8	5.1	24.1	30	−2.5	2	9.2	13.1	8.2	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.7	5.6	6.3
VI	–	–	–	–	21.3	11.6	28.4	3	6.3	22	16.5	20.6	15.6	17.1	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.3	5.3	5.1
VII	–	–	–	–	18.3	10.6	31.0	3	5.2	1	14.1	17.4	13.6	14.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.3	8.5	8.4
VIII	–	–	–	–	17.9	10.9	24.9	6	8.0	4	13.1	17.1	13.2	14.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	7.8	8.2
IX	–	–	–	–	18.2	8.9	28.4	17	1.6	24	11.3	17.9	12.0	13.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.7	3.8	4.7
X	–	–	–	–	14.0	7.9	18.4	10	2.7	31	9.3	13.7	10.3	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.4	4.7	5.6
XI	–	–	–	–	6.0	1.6	11.0	1	−5.9	23	3.2	5.6	3.4	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.8	7.8	8.1
XII	–	–	–	–	−0.1	−6.2	11.4	5	−18.4	17, 26	−3.4	−1.3	−3.3	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.8	7.7	7.8
Rok	–	–	–	–	11.1	4.0	31.0	3.VII	−18.4	17.26.XII	6.7	10.5	6.9	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	6.4	6.8

Świbno - Ujście Wisły — φ = 54°21' — λ = 18°56'

I	–	–	–	–	1.4	−4.1	4.8	31	−16.5	26	−2.5	−0.1	−1.5	−1.4	4.7	5.1	4.9	4.9	87	80	85	84	0.6	1.1	0.8	0.8	7.4	7.6	6.9	7.3
II	–	–	–	–	4.1	0.1	15.1	18	−4.9	5	1.0	2.8	1.8	1.8	6.3	6.7	6.5	6.5	95	89	92	92	0.4	0.9	0.6	0.6	8.4	8.5	8.8	8.6
III	–	–	–	–	8.1	2.3	17.7	10	−4.4	20	4.0	6.5	5.0	5.1	7.1	7.2	7.3	7.2	87	75	82	81	1.1	2.6	1.6	1.8	8.3	6.6	5.8	6.9
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Świbno — φ = 54°20' — λ = 18°56'

I	–	–	–	–	1.0	−4.0	4.8	31	−13.6	26	−2.6	0.0	−1.8	−1.6	4.6	5.2	4.8	4.9	86	82	79	82	0.6	1.0	0.8	0.8	8.1	8.1	7.2	7.8
II	–	–	–	–	4.3	−0.2	14.3	18	−5.0	5	0.8	3.2	1.7	1.8	6.2	7.0	6.4	6.5	94	91	92	92	0.4	0.7	0.5	0.5	9.3	8.7	8.5	8.8
III	–	–	–	–	8.9	2.2	18.0	10	−5.5	20	3.9	7.6	5.0	5.4	7.2	7.3	7.4	7.3	88	70	84	81	1.0	3.4	1.5	2.0	7.9	6.9	6.7	7.2
IV	–	–	–	–	12.3	3.7	24.2	7	−1.2	10	6.6	11.2	7.7	8.3	7.7	7.9	8.2	7.9	79	60	77	72	2.2	6.1	2.6	3.6	4.6	4.7	2.9	4.1
V	–	–	–	–	13.8	6.6	21.4	30	1.7	13	9.7	12.6	9.6	10.4	10.6	10.4	10.1	10.4	88	72	84	81	1.5	4.5	1.9	2.7	7.3	8.0	6.5	7.3
VI	–	–	–	–	22.5	12.8	28.7	27	6.8	22	16.6	20.4	16.9	17.7	15.0	14.7	15.3	15.0	79	62	79	73	4.0	9.8	4.1	6.0	4.8	5.1	5.5	5.1
VII	–	–	–	–	20.0	11.3	32.9	3	7.8	6	14.6	18.0	15.0	15.6	14.8	14.9	14.8	14.8	88	72	86	82	2.0	6.2	2.4	3.5	7.4	7.8	7.8	7.7
VIII	–	–	–	–	20.6	11.9	27.4	6	8.2	18	14.1	18.1	14.4	15.2	14.8	14.6	14.8	14.7	91	71	90	84	1.4	6.4	1.7	3.2	7.0	7.6	6.7	7.1
IX	–	–	–	–	19.0	10.2	28.1	2	4.4	25	11.7	17.9	13.4	14.1	12.7	13.6	13.5	13.3	90	66	87	81	1.4	7.4	2.1	3.6	4.6	4.8	3.5	4.3
X	–	–	–	–	14.6	7.8	18.8	4	3.2	31	8.8	13.6	10.4	10.8	10.4	12.0	11.0	11.1	92	77	87	85	1.0	3.8	1.7	2.2	6.0	6.4	4.0	5.4
XI	–	–	–	–	6.7	2.3	11.8	1	−4.6	23	3.6	5.5	4.1	4.3	7.4	7.6	7.4	7.5	92	83	89	88	0.7	1.6	1.0	1.1	8.9	8.5	7.2	8.2
XII	–	–	–	–	1.1	−5.5	12.9	5	−19.1	28	−2.9	−1.1	−2.8	−2.4	4.8	5.1	4.7	4.9	87	83	86	85	0.6	1.0	0.8	0.8	7.7	6.7	6.3	6.9
Rok	–	–	–	–	12.1	4.9	32.9	3.VII	−19.1	28.XII	7.1	10.6	7.8	8.3	9.7	10.0	9.9	9.9	88	74	85	82	1.4	4.3	1.8	2.5	7.0	6.9	6.1	6.7

Kartuzy — φ = 54°20' — λ = 18°12'

I	–	–	–	–	−0.4	−4.6	4.0	31	−16.1	26	−3.3	−1.1	−2.7	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	6.2	7.0
II	–	–	–	–	3.1	−0.7	13.8	18	−9.6	5	0.4	2.0	1.1	1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.9	8.1	8.7
III	–	–	–	–	7.0	1.6	16.2	10	−5.8	20	2.9	5.8	3.8	4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.4	5.4	7.2
IV	–	–	–	–	12.7	2.9	23.1	7	−3.1	2	5.4	11.4	6.7	7.6	7.4	7.8	7.8	7.7	81	59	78	73	1.9	6.5	2.4	3.6	4.3	4.9	3.0	4.1
V	–	–	–	–	13.7	5.6	23.0	30	0.7	2	8.7	12.1	8.1	9.2	9.7	10.4	9.7	9.9	85	74	89	83	1.7	4.1	1.3	2.4	6.5	8.5	6.0	7.0
VI	–	–	–	–	21.5	12.0	27.8	27	7.1	1	14.4	20.0	15.4	16.3	13.8	13.2	14.0	13.8	84	57	79	73	2.8	10.8	3.7	5.8	4.8	5.7	5.6	5.4
VII	–	–	–	–	18.7	10.8	31.8	3	7.2	6	12.8	17.1	14.1	14.5	13.4	13.9	14.1	13.8	91	74	88	84	1.4	6.2	2.2	3.3	7.8	7.9	7.4	7.7
VIII	–	–	–	–	18.2	11.0	25.3	6	9.6	4	12.4	16.6	13.5	14.0	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	6.8	7.7
IX	–	–	–	–	18.0	9.2	27.3	17	3.4	24	10.5	17.0	12.1	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.1	3.6	4.7
X	–	–	–	–	13.6	7.5	18.3	5, 6	3.3	31	8.4	12.6	9.9	10.2	10.3	10.9	10.7	10.8	93	76	88	86	0.8	3.8	1.5	2.1	7.8	6.4	4.5	6.0
XI	–	–	–	–	5.3	1.4	9.9	3	−4.7	23	2.9	4.4	3.3	3.5	7.1	7.2	7.1	7.1	93	85	90	89	0.5	1.3	0.8	0.9	9.2	8.8	8.6	8.9
XII	–	–	–	–	−0.6	−5.6	10.9	5	−18.0	17	−3.4	−1.9	−3.4	−3.0	4.6	5.0	4.5	4.7	88	86	87	87	0.5	0.7	0.6	0.6	8.2	8.2	6.9	7.8
Rok	–	–	–	–	10.9	4.3	31.8	3.VII	−18.0	17.XII	6.0	9.7	6.8	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.3	6.0	6.8

Czarna Dąbrówka — $H_s = 120\,m$ — $h_w = 12\,m$ — 1961

MIESIĄC	ROZKŁAD WIATRU (%D, %nD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	Wiatr v ≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	■	⊞	R ≥10
I	3	3.7	4	2.5	5	3.4	9	4.3	28	4.0	33	5.4	7	3.4	4	3.2	·	4.3	32.4	10.7	30	8	11	28	·	3	·	6	19	10	7	1	–	–	·
II	·	·	·	·	·	·	9	6.8	18	5.5	33	3.9	15	3.8	9	4.6	·	4.6	42.2	17.5	28	1	1	10	·	4	·	1	19	15	8	1	–	–	·
III	1	14.0	·	·	·	·	·	·	2	8.5	12	4.5	46	9.1	32	8.7	·	8.4	53.4	12.8	31	·	·	8	·	17	8	1	15	15	10	1	–	–	·
IV	6	2.3	2	3.0	15	3.4	25	5.0	11	4.6	7	4.0	13	5.0	11	5.5	·	4.5	12.6	4.9	1	·	·	9	·	4	1	12	3	4	3	·	–	·	1
V	15	2.8	2	3.0	4	3.0	2	4.5	8	4.1	17	3.6	18	3.6	27	3.1	·	3.4	83.9	23.4	14	·	·	2	·	·	·	4	13	15	13	2	–	·	1
VI	1	2.0	5	2.6	10	2.9	6	3.0	5	4.6	13	3.8	31	6.0	19	6.5	·	4.9	86.9	23.6	14	·	·	·	6	8	1	6	5	9	7	3	–	·	3
VII	·	·	·	·	·	·	1	2.0	7	4.0	42	4.6	28	4.0	15	4.6	·	4.3	94.4	27.0	13	·	·	·	3	1	·	2	23	26	17	2	–	·	9
VIII	2	4.0	·	·	3	5.0	1	3.0	2	4.5	33	4.0	38	4.6	14	5.6	·	4.4	137.5	17.5	21	·	·	·	·	3	·	1	20	21	15	5	–	·	3
IX	7	2.7	·	·	3	3.3	13	5.0	15	4.0	22	3.4	21	4.5	8	4.2	1	4.0	98.3	23.3	29	·	·	·	3	3	·	9	7	14	9	3	–	·	1
X	·	·	·	·	1	3.0	32	6.0	26	4.3	18	4.0	8	5.0	7	6.0	1	4.1	29.5	6.5	18	·	·	·	·	3	·	7	12	9	9	·	–	·	·
XI	3	3.0	3	4.0	7	4.0	13	4.4	8	3.5	40	4.7	8	3.4	8	3.5	·	4.2	42.3	10.2	30	·	·	8	·	2	·	2	19	17	13	1	–	–	·
XII	6	3.3	5	3.0	3	3.3	15	5.8	14	3.8	28	5.9	7	5.9	15	5.1	·	5.0	52.2	18.8	2	11	13	25	·	6	1	·	18	13	13	1	–	–	·
Rok	44	3.2	21	1.5	51	2.6	126	4.2	144	4.6	298	4.3	240	4.9	169	5.0	2	4.7	766.6	27.0	13.VIII	20	25	90	12	54	11	51	173	168	124	20	–	–	18

Świbno - Ujście Wisły — $H_s = 5\,m$ — $h_w = 12\,m$

I	1.5	8.3	6	6.8	3.5	6.9	12.5	6.0	28	4.8	27.5	4.3	5	5.5	7	10.4	2	5.6	11.7	2.9	11	4	11	20	·	8	·	1	15	12	4			5	·
II	2.5	5.0	1	4.5	2.5	4.4	9	4.3	21	6.3	20.5	4.9	19	5.9	5.5	5.2	3	5.3	41.4	12.3	28	·	·	11	·	4	1	1	18	11	7	1	6	·	·
III	3	9.5	·	·	·	·	·	·	5	6.1	16	7.0	42.5	9.6	26.5	9.9	·	9.0	13.4	4.0	21	·	·	3	·	23	7	1	12	10	7	·	1	·	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Świbno — $H_s = 3\,m$ — $h_w = 10\,m$

I	3	7.2	3	6.8	2	3.0	5	6.4	10.5	4.4	44	3.0	16	3.2	3.5	8.6	6	3.6	16.5	4.0	11	6	11	19	·	2	·	·	16	12	7	·	2	5	·
II	·	·	·	·	·	·	5	3.0	8	8.1	29.5	2.8	26	2.2	3.5	5.6	12	2.9	42.6	11.3	28	·	·	12	·	2	2	·	19	15	9	1	5	·	·
III	1.5	11.0	·	·		·	·	·	1.5	8.3	18	6.8	53	6.1	14	9.0	5	6.4	16.4	3.9	21	·	·	6	·	10	6	·	9	10	6	·	·	·	·
IV	13.5	6.4	6	5.8	7.5	5.7	8.5	5.9	6	3.5	10	3.2	17	3.7	15.5	4.5	6	4.4	17.2	8.7	17	·	·	5	·	2	·	8	2	9	7	·	1	·	2
V	13	5.7	3.5	5.3	1	5.0	3	5.8	6.5	4.9	14	3.7	23.5	2.7	25.5	5.0	3	4.2	73.5	17.6	6	·	·	·	·	·	·	2	14	15	13	3	2	·	5
VI	11	6.3	4	5.0	2	3.5	4	3.2	4	4.2	13.5	3.9	36.5	4.0	12	5.0	3	4.3	29.6	10.0	14	·	·	·	7	2	·	6	5	8	7	1	·	·	6
VII	2	4.5	·	·	2	7.0	·	·	4	4.8	30	4.0	38.5	2.6	8.5	4.2	8	3.2	123.5	23.5	31	·	·	·	2	·	·	·	18	21	15	5	1	·	6
VIII	2	2.5	·	·	1	4.0	·	·	5	3.1	26	4.1	38	3.2	9	3.6	12	3.0	88.2	26.1	6	·	·	·	2	·	·	·	9	18	13	2	3	·	4
IX	3.5	2.1	12.5	3.7	10.5	3.2	8.5	4.6	11	3.5	9.5	4.4	14.5	3.4	5	3.6	15	3.0	31.3	16.4	14	·	·	·	3	·	·	6	5	7	5	1	1	·	·
X	0.5	3.0	2	2.0	18.5	4.6	23.5	5.4	22	4.0	7.5	3.7	5.5	2.5	6.5	4.8	7	4.0	34.6	11.4	18	·	·	·	·	4	·	6	9	12	9	1	4	·	·
XI	3	9.8	5	9.5	17	5.8	10	4.4	15.5	3.1	10	5.4	11	3.8	5.5	8.0	13	4.4	37.9	9.5	11	·	·	7	·	5	·	1	19	14	9	·	5	·	·
XII	4	10.6	5.5	7.4	6.5	3.5	13.5	4.4	16.5	4.3	19	5.1	16	4.8	5	6.9	7	4.8	32.9	9.4	23	7	9	24	·	4	·	3	14	13	8	·	4	16	·
Rok	57	5.8	41.5	3.8	68	3.8	81	3.6	110.5	4.7	231	4.2	295.5	3.5	113.5	5.7	97	4.0	544.2	26.1	6.VIII	13	20	73	14	31	8	32	139	154	108	14	28	21	23

Kartuzy — $H_s = 220\,m$ — $h_w = 10\,m$

I	·	·	2	2.0	1	1.0	7	1.8	8	2.2	55	2.4	10	2.8	6	3.3	4	2.3	33.2	11.2	30	6	13	26	·	·	·	5	17	10	6	1	7	21	–
II	·	·	1	1.0	·	·	4	2.5	5	1.8	48	2.1	17	2.9	6	4.0	3	2.3	38.3	14.0	28	·	2	16	·	·	·	·	20	14	9	1	12	7	–
III	1	3.0	·	·	·	·	·	·	·	·	28	3.8	38	5.0	26	5.9	·	4.8	41.6	11.9	29	·	·	8	·	·	·	1	15	13	7	1	5	4	–
IV	·	·	6	2.3	6	2.3	13	2.7	11	2.3	29	2.1	11	1.9	7	3.0	7	2.1	15.9	4.0	1	·	·	8	·	·	·	8	4	8	6	·	2	3	–
V	9	3.7	7	2.7	·	·	3	3.0	9	1.9	31	2.5	18	3.1	14	3.4	2	2.8	64.2	18.2	14	·	·	·	·	·	·	·	13	14	11	1	3	·	–
VI	1	1.0	4	1.5	1	1.0	4	4.0	4	2.0	29	3.5	27	3.2	11	3.3	9	2.7	58.1	20.6	14	·	·	·	6	2	·	4	6	11	8	2	1	·	–
VII	·		·	·	·	·	·	·	3	3.0	51	2.5	21	2.5	7	3.0	11	2.3	137.0	30.4	17	·	·	·	4	·	·	2	16	23	21	4	2	·	–
VIII	·	·	·	·	·	·	2	1.0	·	·	43	2.5	31	3.0	8	3.7	9	2.5	86.2	18.2	7	·	·	·	1	·	·	1	14	18	15	1	1	·	–
IX	1	2.0	1	3.0	·	·	2	2.0	9	2.3	32	1.8	21	2.4	5	2.2	19	1.7	56.2	17.4	14	·	·	·	4	·	·	10	6	11	7	2	3	·	–
X	·	·	·	·	2	2.0	4	1.5	17	1.8	56	1.6	6	3.0	6	4.0	2	1.8	35.9	11.9	18	·	·	·	·	·	·	4	12	11	8	1	5	·	–
XI	8	2.5	2	3.0	3	3.0	5	1.4	11	1.5	27	3.1	19	2.6	4	3.2	11	2.3	50.1	12.8	11	·	·	9	·	·	·	1	25	17	13	2	10	·	–
XII	8	2.0	4	2.0	·	·	2	1.0	5	1.0	35	2.8	17	2.6	11	3.4	11	2.3	38.7	11.7	2	9	14	25	·	·	·	·	15	13	9	1	7	17	–
Rok	28	1.6	27	1.5	13	0.8	46	1.7	82	1.6	464	2.6	236	2.9	111	3.5	88	2.5	655.4	30.4	17.VII	15	29	92	15	2	·	36	163	163	120	17	58	52	–

Tolkmicko

$\varphi = 54°19'$ $\lambda = 19°32'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
										Średnia																		
	P_m	Max	Min	$P_{n.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.2	-3.7	6.6	5	-14.8	26	-2.2	0.0	-1.2	-1.2	4.5	4.8	4.7	4.7	80	75	79	78	1.0	1.4	1.1	1.2	6.3	7.2	7.4	7.0
II	–	–	–	–	4.5	0.3	14.0	18	-4.0	5	1.3	3.1	2.3	2.2	6.1	6.6	6.4	6.4	91	86	88	88	0.6	1.1	0.9	0.9	7.9	8.6	8.3	8.3
III	–	–	–	–	8.2	2.1	16.8	10	-3.9	20	3.8	6.6	5.0	5.1	7.0	7.3	7.2	7.2	86	75	81	80	1.2	2.6	1.8	1.9	8.0	6.5	6.0	6.8
IV	–	–	–	–	13.3	3.6	24.0	7	-3.8	2	6.7	11.4	8.2	8.6	7.7	8.5	8.0	8.1	77	62	73	71	2.5	5.8	3.3	3.9	4.2	4.8	3.8	4.3
V	–	–	–	–	14.6	7.0	25.6	30	2.2	2	10.3	13.0	9.7	10.7	10.4	10.8	10.3	10.5	83	73	86	81	2.3	4.7	1.8	2.9	6.7	7.8	6.2	6.9
VI	–	–	–	–	22.3	13.9	30.1	27	7.8	22	17.0	20.6	17.1	18.0	15.1	15.9	15.3	15.4	78	66	79	74	4.4	8.9	4.4	5.9	5.1	5.2	6.3	5.5
VII	–	–	–	–	20.4	12.3	31.3	3	8.9	6	15.1	18.6	15.3	16.1	14.9	15.4	15.0	15.1	87	72	86	82	2.4	6.5	2.6	3.8	7.2	7.9	7.7	7.6
VIII	–	–	–	–	19.3	12.4	27.3	6	9.3	18	14.7	18.3	14.7	15.6	14.8	15.3	14.7	14.9	88	73	87	83	2.0	6.0	2.1	3.4	7.4	6.9	7.4	7.2
IX	–	–	–	–	19.2	10.7	28.3	2	5.7	27	12.4	18.1	13.4	14.3	12.9	14.3	13.3	13.5	88	68	85	80	1.8	7.0	2.4	3.7	4.0	4.6	4.1	4.2
X	–	–	–	–	15.2	8.3	19.8	4	3.0	23	9.1	14.3	11.4	11.6	10.5	12.0	11.2	11.2	90	74	83	82	1.2	4.5	2.4	2.7	5.7	6.4	5.1	5.7
XI	–	–	–	–	6.4	2.3	11.3	3	-3.8	24	3.6	5.4	4.3	4.4	7.3	7.6	7.4	7.4	90	83	87	87	0.8	1.6	1.1	1.2	8.7	8.1	8.0	8.3
XII	–	–	–	–	0.7	-5.8	13.4	5	-16.6	27	-2.5	-1.2	-2.4	-2.1	4.7	5.0	4.7	4.8	85	81	83	83	0.8	1.1	0.9	0.9	7.5	7.0	6.7	7.1
Rok	–	–	–	–	12.1	5.3	31.3	3.VII	-16.6	27.XII	7.4	10.7	8.2	8.6	9.7	10.3	9.8	9.9	85	74	83	81	1.8	4.3	2.1	2.7	6.6	6.8	6.4	6.6

Gołdap

$\varphi = 54°19'$ $\lambda = 22°19'$

I	–	–	–	–	–	-6.2	–	–	-20.4	26	-3.7	-1.9	-3.1	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	9.2	7.7	8.5
II	–	–	–	–	2.4	-1.6	8.4	15	-10.3	5	-0.4	1.3	0.4	0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.6	8.3	7.8	8.6
III	–	–	–	–	6.7	-0.1	14.0	10	-6.1	23	2.0	5.0	2.3	2.9	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.5	5.1	7.5
IV	–	–	–	–	13.0	1.1	23.4	7	-5.4	2	5.2	11.9	6.0	7.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.6	2.9	4.2
V	–	–	–	–	16.0	6.6	25.6	30	-0.6	23	9.8	14.4	10.2	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.8	7.7	7.5
VI	–	–	–	–	22.3	11.2	29.1	27	6.9	21	16.4	20.5	15.4	16.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.0	5.6	6.0
VII	–	–	–	–	20.3	10.9	28.4	3	7.1	16	14.6	19.1	14.1	15.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	6.8	7.2
VIII	–	–	–	–	19.4	10.7	27.5	6	6.1	30, 31	13.5	18.1	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.2	7.5	7.6
IX	–	–	–	–	18.2	6.6	27.0	3	0.1	24	10.3	17.0	10.5	12.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	4.6	3.3	4.8
X	–	–	–	–	13.5	5.5	18.0	4	-0.2	23	7.4	12.7	8.9	9.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.0	5.5	6.4
XI	–	–	–	–	4.7	0.4	10.9	2	-5.8	29	2.3	3.9	2.7	2.9	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.9	8.5	8.7
XII	–	–	–	–	-1.3	-8.2	11.2	5	-23.2	27	-5.3	-3.1	-4.5	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	5.9	7.5
Rok	–	–	–	–	–	3.1	29.1	27.VI	-23.2	27.XII	6.0	9.9	6.4	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	6.2	7.0

Hopowo

$\varphi = 54°16'$ $\lambda = 18°14'$

I	–	–	–	–	-0.8	-5.6	3.8	31	-16.0	26	-4.3	-1.7	-2.9	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.7	7.1	7.5
II	–	–	–	–	3.0	-1.0	13.6	18	-8.5	5	-0.1	1.7	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.7	8.5	8.8
III	–	–	–	–	6.9	0.6	17.0	10	-5.9	20	2.5	5.5	2.3	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.3	7.3	7.7
IV	–	–	–	–	12.5	2.0	22.4	7	-5.0	2	5.6	11.4	5.1	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.3	5.5	5.3
V	–	–	–	–	12.6	5.0	21.9	30	-1.9	2	8.4	12.1	6.8	8.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.1	6.7	7.2
VI	–	–	–	–	21.3	11.6	27.6	27	6.1	1	15.3	20.5	15.0	16.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.8	5.8	5.4
VII	–	–	–	–	18.7	10.8	31.4	3	6.6	6	13.6	17.0	13.3	14.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.8	7.1	7.6
VIII	–	–	–	–	18.0	11.0	25.5	6	8.8	30	12.9	16.7	12.3	13.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.0	6.7	7.5
IX	–	–	–	–	17.4	9.2	26.8	2	3.2	24	10.9	16.8	11.1	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	4.8	5.4
X	–	–	–	–	13.0	6.9	17.9	6	3.7	31	8.2	12.3	8.5	9.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.8	6.0	6.6
XI	–	–	–	–	5.2	1.1	9.9	1	-4.3	23	2.3	4.2	2.6	2.9	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.5	8.4	8.6
XII	–	–	–	–	-0.5	-6.2	11.0	5	-19.4	17	-4.2	-2.2	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.4	6.9	7.5
Rok	–	–	–	–	10.6	3.8	31.4	3.VII	-19.4	17.XII	5.9	9.5	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	6.7	7.1

Bartoszyce

$\varphi = 54°15'$ $\lambda = 20°48'$

I	–	–	–	–	0.3	-5.2	6.4	5	-18.9	25, 26	-3.4	-0.9	-2.1	-2.1	4.5	4.9	4.8	4.7	87	81	86	85	0.6	1.0	0.7	0.8	7.1	7.3	6.7	7.0
II	–	–	–	–	3.6	-0.5	11.3	18	-6.3	5	0.6	2.8	1.6	1.6	6.0	6.6	6.3	6.3	94	87	91	91	0.4	1.1	0.6	0.7	9.3	7.8	7.8	8.3
III	–	–	–	–	8.0	0.8	15.7	10	-4.2	20	3.1	6.3	3.7	4.2	6.8	6.6	6.8	6.7	89	69	84	81	0.9	3.1	1.4	1.8	8.2	7.2	4.4	6.6
IV	–	–	–	–	14.0	1.4	23.0	7	-3.8	2	5.4	12.5	7.3	8.1	7.3	7.2	7.7	7.4	80	50	73	68	1.9	8.2	3.0	4.4	4.7	4.7	3.2	4.2
V	–	–	–	–	16.3	6.0	25.0	30	0.7	2	9.6	14.4	10.1	11.0	10.4	11.6	10.7	10.9	86	64	85	78	1.7	6.4	1.9	3.3	7.5	7.9	7.4	7.6
VI	–	–	–	–	22.6	11.2	30.4	27	7.4	21	15.8	21.2	15.5	17.0	14.9	14.7	15.1	14.9	83	59	85	76	3.2	11.1	2.5	5.6	6.1	6.1	6.2	6.1
VII	–	–	–	–	20.2	10.9	29.8	3	7.1	16	14.3	18.6	14.7	15.6	14.4	14.4	14.8	14.5	89	68	89	82	1.9	7.5	2.0	3.8	7.5	7.4	7.8	7.6
VIII	–	–	–	–	19.3	11.0	27.6	6	6.9	31	13.8	18.4	14.0	15.0	14.4	14.7	14.6	14.6	91	70	91	84	1.5	6.7	1.4	3.2	7.5	7.2	7.2	7.3
IX	–	–	–	–	19.0	7.5	27.4	17	-1.1	24	10.2	17.9	11.7	12.9	12.0	13.4	12.7	12.7	93	65	90	83	1.0	7.5	1.3	3.3	5.0	5.0	3.5	4.5
X	–	–	–	–	14.3	6.5	19.2	4	1.7	23	8.0	13.5	9.9	10.3	10.1	11.5	10.6	10.7	93	75	87	85	0.8	4.2	1.7	2.2	7.2	6.2	5.5	6.3
XI	–	–	–	–	5.6	1.2	11.1	3	-5.7	29	2.9	4.6	3.4	3.6	7.2	7.5	7.5	7.4	93	87	93	91	0.6	1.2	0.6	0.8	8.5	8.2	7.5	8.1
XII	–	–	–	–	-0.4	-7.7	13.1	5, 6	-22.8	27	-4.1	-2.2	-4.6	-3.9	4.4	4.9	4.2	4.5	83	83	81	82	0.7	0.9	0.9	0.8	7.5	6.5	4.2	6.1
Rok	–	–	–	–	11.9	3.6	30.4	27.VI	-22.8	27.XII	6.4	10.6	7.1	7.8	9.4	9.8	9.6	9.6	88	72	86	82	1.3	4.9	1.5	2.6	7.2	6.8	6.0	6.7

Tolkmicko $H_s = 1 m$ $h_w = 19 m$ 1961

MIESIĄC	ROZKŁAD WIATRU (D, ¥mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◑	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	1.5	6.3	2.5	7.0	7	5.0	10	5.6	14	7.1	44.5	6.3	6.5	6.0	4	11.2	3	6.3	22.2	10.3	30	4	10	18	·	—	—	4	15	11	5	1	·	5	·
II	0.5	4.0	3	3.0	1	5.0	3	4.0	23.5	6.9	38.5	4.9	12	4.6	0.5	4.0	2	5.2	39.1	11.6	11	·	·	8	·	—	—	2	20	13	7	1	5	1	·
III	1	1.2	·	·	·	·	·	·	·	·	29.5	9.2	50.5	9.3	12	1.2	·	9.6	23.8	6.0	20	·	·	5	·	—	—	1	11	13	9	·	2	2	·
IV	7.5	4.4	8	7.8	7.5	7.0	22.5	6.1	7	4.6	10	6.5	11	5.3	11.5	7.7	5	5.9	20.3	8.4	17	·	·	5	·	—	—	11	5	8	6	·	·	·	1
V	17.5	6.4	9	5.1	5	5.2	6.5	6.0	5.5	5.1	22	5.0	9.5	6.1	14	7.1	4	5.6	116.8	32.2	7	·	·	·	1	—	—	1	11	16	12	3	·	·	5
VI	7.5	4.7	7.5	3.7	7.5	3.8	13	5.0	3	3.3	18.5	6.0	18	6.5	12	9.0	3	5.6	96.2	52.5	14	·	·	·	9	—	—	5	6	11	7	3	·	·	4
VII	2	3.5	5	3.2	2	5.5	6.5	4.8	6	4.5	50	5.6	16.5	5.4	2	5.5	3	5.1	135.2	30.0	13	·	·	·	2	—	—	1	13	21	18	4	·	·	6
VIII	·	·	5	2.4	·	·	2	3.5	5	4.0	47.5	6.4	20.5	6.8	7	6.7	6	5.7	130.6	29.0	6	·	·	·	2	—	—	·	12	20	18	3	·	·	6
IX	3	3.7	2	4.5	13	3.8	13	5.8	12	4.2	23	6.3	18	5.2	4	6.0	2	5.1	50.4	21.7	14	·	·	·	3	—	—	10	4	6	4	2	·	·	2
X	·	·	·	·	0.5	6.0	41.5	7.2	16	5.5	22	5.0	5	7.2	6	6.3	2	6.2	24.3	4.6	26	·	·	·	·	—	—	6	9	10	9	·	·	·	·
XI	1	7.0	7.5	7.3	14.5	5.8	11.5	6.0	5	3.0	37.5	7.1	5	5.0	6	7.7	2	6.3	34.6	5.4	18	·	·	10	·	—	—	1	19	13	10	·	3	1	·
XII	4	8.0	7	8.8	9.5	5.9	3.5	4.4	12.5	4.2	41.5	7.9	6.5	10.6	5.5	8.4	3	7.1	35.1	5.9	23	9	13	21	·	—	—	2	12	15	8	·	·	16	·
Rok	45.5	4.1	56.5	4.4	67.5	4.4	133	4.9	109.5	4.4	384.5	6.4	179	6.5	84.5	6.7	35	6.1[2]	728.6	52.5	14.VI	13	23	67	17	—	—	44	137	157	113	17	10	25	24

Gołdap $H_s = 150 m$ $h_w = 15,5 m$

I	5.5	3.3	2	1.5	5.5	1.8	12	2.3	8	2.8	12	4.0	15	3.1	12	2.4	21	2.2	41.2	17.7	30	7	—	28	·	·	·	1	20	18	8	1	6	26	—
II	1	2.0	·	·	7.5	2.5	4.5	3.3	16.5	3.3	18	3.7	14	2.1	5.5	2.0	17	2.3	32.8	7.4	28	1	2	18	·	1	·	·	21	15	8	·	9	11	—
III	1	2.0	·	·	·	·	1	4.0	6	6.2	21.5	4.6	26	3.3	27.5	5.8	10	4.2	64.2	17.3	12	·	·	13	·	6	1	·	13	15	14	2	3	2	—
IV	8	3.1	4.5	1.8	14	2.7	6.5	3.1	7	5.0	9.5	3.7	6.5	3.8	10	3.5	24	2.3	27.4	7.2	5	·	·	12	·	3	·	13	7	9	7	·	3	1	—
V	9.5	2.6	1.5	2.0	2.5	3.2	4	3.5	11	2.1	7.5	2.5	14	2.4	11	3.0	32	1.7	98.5	18.2	6	·	·	1	3	·	·	·	15	18	16	3	2	·	—
VI	·	·	2	2.0	6.5	2.4	6.5	2.5	5.5	2.4	15	2.4	18.5	3.3	4	3.4	32	1.8	105.6	54.5	12	·	·	·	8	·	·	2	10	11	11	2	4	·	—
VII	·	·	1	1.0	1	2.0	5.5	2.6	12	2.5	21.5	2.2	18	2.3	8	1.6	26	1.6	76.5	14.6	30	·	·	·	3	·	·	2	11	19	17	1	·	·	—
VIII	2	4.0	2	1.5	0.5	1.0	3	3.2	6.5	2.5	15	2.6	20.5	3.1	10.5	3.5	33	1.9	71.3	11.8	7, 22	·	·	·	2	·	·	1	15	17	15	2	1	·	—
IX	0.5	3.0	1.5	1.0	5	1.8	4.5	1.7	4	2.2	7.5	2.5	19	2.4	7	2.4	41	1.2	61.4	17.1	13	·	·	·	3	·	·	9	8	9	9	1	4	·	—
X	·	·	1	2.0	14	3.6	31	4.5	17	2.9	8	1.8	3.5	3.3	3.5	3.9	15	3.0	17.0	7.6	29	·	·	1	·	3	·	5	13	7	6	·	9	·	—
XI	5	3.7	2.5	1.8	16	5.7	10	4.0	8.5	3.5	14	3.0	8	2.9	12	3.6	14	3.2	38.4	10.6	30	·	1	14	·	2	·	·	24	10	8	1	9	4	—
XII	8.5	3.9	3	3.3	9	3.3	9	3.6	11	3.5	20.5	4.7	7.5	2.8	7.5	3.7	17	3.1	36.8	7.8	20	12	17	27	·	3	1	·	13	14	10	·	1	23	—
Rok	41	2.3	21	1.5	81.5	2.5	97.5	3.2	113	3.2	170	3.1	170.5	2.9	118.5	3.2	282	2.4	671.1	54.5	12. VI	20	—	114	19	18	2	33	170	162	129	13	51	67	—

Hopowo $H_s = 220 m$ $h_w = 12 m$

I	2.5	3.8	2	3.0	2	3.0	4	3.2	18	4.9	41.5	5.1	4	4.5	7	4.0	12	4.1	26.5	8.5	30	8	17	29	·	1	·	2	18	16	6	·	—	9	·
II	1.5	4.3	·	·	·	·	6	5.3	17	5.9	22	4.5	15	4.4	8.5	5.1	14	4.1	34.4	15.8	28	·	3	17	·	1	·	1	23	8	6	1	—	6	·
III	1	12.0	·	·	·	·	·	·	·	·	27	5.7	33	6.5	30	7.9	2	6.7	37.5	6.7	12	·	·	10	·	8	1	1	16	14	8	·	—	3	·
IV	0.5	3.0	12	4.2	4.5	4.2	13.5	4.4	11.5	4.6	13.5	5.0	9.5	5.5	8	4.6	17	3.8	12.1	2.8	6	·	·	9	·	1	·	5	6	9	7	·	—	1	1
V	3	5.5	9.5	3.9	2.5	4.2	2	4.5	8.5	5.1	23.5	4.4	12.5	3.6	12.5	4.0	19	3.4	70.9	18.6	14	·	·	1	·	·	·	·	13	16	12	2	—	·	4
VI	2	3.0	3	2.3	1.5	2.3	5.5	3.9	5	5.2	19	5.0	20.5	5.4	11.5	4.5	22	3.6	69.3	26.6	16	·	·	·	5	1	·	3	5	9	6	3	—	·	8
VII	2	4.5	0.5	3.0	0.5	3.0	0.5	5.0	10	4.6	44	4.4	13	4.3	4.5	3.9	18	3.5	126.6	34.1	13	·	·	·	4	·	·	2	16	25	18	3	—	·	11
VIII	1	3.0	1	3.0	·	·	0.5	1.0	6.5	4.4	37	4.7	16.5	4.7	8.5	4.2	22	3.5	96.1	20.3	10	·	·	·	1	·	·	·	13	22	19	1	—	·	4
IX	·	·	2	2.0	·	·	6.5	3.5	11	5.2	25	4.2	11.5	5.4	3	5.8	31	3.0	39.4	15.6	14	·	·	·	3	1	·	8	9	9	8	1	—	·	3
X	·	·	1.5	3.0	2	3.0	18	4.2	23.5	5.4	20.5	4.9	4	5.2	4.5	6.7	19	3.8	27.7	11.3	18	·	·	·	·	·	·	4	14	12	8	1	—	·	·
XI	3.5	4.1	7	4.6	2	4.5	8.5	4.3	10.5	5.1	21.5	5.6	7.5	5.4	8.5	4.9	21	3.9	44.8	15.7	11	·	·	11	·	1	·	1	22	16	7	2	—	·	·
XII	2	7.0	6.5	4.8	0.5	3.0	5.5	4.6	11	5.8	30	6.0	10	5.8	8.5	4.1	19	4.4	54.2	13.3	4	9	14	26	·	3	1	1	19	14	11	1	—	18	·
Rok	19	4.2	45	2.8	15.5	2.3	70.5	3.7	132.5	4.7	324.5	5.0	157	5.1	115	4.9	216	4.0	639.5	34.1	13.VII	17	34	103	13	17	2	28	174	170	116	15	—	37	31

Bartoszyce $H_s = 60 m$ $h_w = 13 m$

I	3	3.0	5	1.8	·	·	10.5	1.9	13	1.7	28	2.9	12	2.0	7.5	2.9	14	2.0	18.9	11.7	30	7	12	25	·	·	·	1	13	12	3	1	—	—	—
II	1	2.0	·	·	·	·	6	2.3	11	2.3	27	2.4	23	2.2	5	1.6	11	2.0	27.0	9.4	27	·	2	14	·	·	·	·	20	11	5	·	5	—	—
III	1	3.5	·	·	·	·	1	3.0	6	3.2	23.5	3.2	35.5	3.7	24	4.9	2	3.7	32.1	10.0	12	·	·	11	·	1	1	·	11	16	8	1	2	—	—
IV	4	1.9	10	2.9	15.5	2.1	6.5	2.0	5	2.4	11	2.4	10	2.4	13	2.6	15	2.0	14.7	4.5	5	·	·	12	·	1	·	12	6	11	6	·	1	—	—
V	9	1.7	3	1.3	1	3.0	7.5	1.9	5.5	2.4	17	2.1	6	2.3	32	2.2	12	1.9	62.3	13.9	7	·	·	·	1	·	·	·	14	15	11	1	·	·	—
VI	·	·	8	1.5	5	1.4	6.5	2.9	3	2.2	16	2.7	21	3.3	8.5	2.9	22	2.0	68.9	22.1	16	·	·	·	8	·	·	2	8	15	11	1	1	·	—
VII	2	1.5	1	2.0	1.5	2.7	2.5	2.6	11	2.3	40	2.1	10.5	2.0	7.5	1.5	17	1.7	84.0	13.6	22	·	·	·	3	·	·	1	14	27	16	1	2	·	—
VIII	4	1.4	1.5	2.3	3	1.0	·	·	4.5	2.2	34.5	2.5	23.5	2.6	10	2.0	12	2.1	78.8	14.4	23	·	·	·	1	·	·	·	10	20	13	3	·	·	—
IX	3	1.7	2	1.0	8.5	2.1	3.5	1.7	4.5	1.9	16	2.5	16.5	2.3	8	1.5	28	1.6	38.0	13.7	14	·	·	2	4	·	·	8	3	9	5	1	—	·	—
X	1	1.5	6	1.2	10	2.2	22.5	2.6	15	2.1	9.5	1.8	4	1.5	6	2.5	19	1.7	20.0	6.7	29	·	·	·	·	·	·	4	10	10	6	·	5	·	—
XI	9.5	1.8	2.5	2.0	11	2.7	9.5	2.1	7	2.1	26	2.6	7.5	2.8	5	1.4	12	2.1	43.5	9.5	18	·	·	14	·	·	·	·	18	16	9	·	5	—	—
XII	10.5	4.3	4	1.6	·	·	9.5	1.4	7	1.6	29	3.5	10.5	2.3	6.5	2.2	16	2.3	29.3	7.3	4	11	14	25	·	1	·	4	8	12	8	·	·	—	—
Rok	48	2.0	43	1.5	55.5	1.4	85.5	2.0	92.5	2.2	277.5	2.6	180	2.4	133	2.4	180	2.1	517.5	22.1	16.VI	18	28	103	17	3	1	32	135	174	101	9	—	—	—

Nowy Dwór Gdański — φ = 54°13' — λ = 19°08' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.9	−4.7	5.1	4	−15.5	26	−3.0	−0.2	−2.3	−2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.7	6.3	7.2
II	–	–	–	–	4.2	0.0	13.9	18	−4.5	5,6	0.9	3.4	1.6	1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.4	8.5	8.6
III	–	–	–	–	9.6	1.8	18.2	10	−5.6	20	4.0	8.4	4.5	5.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.3	5.2	6.1
IV	–	–	–	–	14.8	3.0	24.6	7	−2.4[9]	21[2]	7.3	13.4	7.1	8.7	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.4	4.3	4.3
V	–	–	–	–	15.6	6.6	26.3	30	2.6	2	10.4	14.0	9.2	10.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	7.2	7.2
VI	–	–	–	–	23.8	12.8	30.2	27	7.1	1	17.3	22.7	16.0	18.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.9	6.1	5.1
VII	–	–	–	–	20.9	11.4	32.6	3	8.0	16	15.2	19.4	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	8.1	7.8
VIII	–	–	–	–	20.3	11.6	28.6	6	8.8	4	14.6	19.2	14.1	15.5	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.9	6.7	6.6
IX	–	–	–	–	20.0	9.7	29.0	2	3.9	28	11.8	19.2	12.9	14.2	–	–	–	–	–	–	–	–	–	–	–	–	3.9	3.7	3.6	3.7
X	–	–	–	–	15.3	7.4	19.8	4	3.2	23	9.0	14.5	10.0	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.9	4.2	5.3
XI	–	–	–	–	6.4	2.0	11.0	3	−5.0	23	3.3	6.6	3.8	4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.7	8.1	8.5
XII	–	–	–	–	0.5	−6.4	12.9	5	−21.0	28	−3.5	−1.3	−3.5	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.8	6.6	7.0
Rok	–	–	–	–	12.7	4.6	32.6	3. VII	−21.0	28. XII	7.3	11.5	7.3	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	6.2	6.4

Koszalin — φ = 54°12' — λ = 16°10'

I	1012.9	1039.1	988.7	1017.2	1.1	−4.1	5.7	29	−14.8	27	−2.5	0.1	−1.7	−1.4	4.6	5.1	4.8	4.8	83	78	83	81	0.8	1.2	0.8	0.9	7.2	6.8	6.5	6.8
II	1014.7	1032.0	984.7	1019.0	5.0	0.3	12.2	18	−4.4	5	1.5	3.7	2.2	2.4	6.5	7.1	6.8	6.8	95	89	94	93	0.4	0.9	0.4	0.6	8.8	8.4	8.0	8.4
III	1010.5	1030.6	982.2	1014.7	8.0	2.2	16.2	10	−3.8	20	3.5	6.5	4.6	4.8	7.2	7.5	7.3	7.3	91	77	86	85	0.7	2.4	1.3	1.5	8.7	8.0	7.4	8.0
IV	1008.3	1020.7	998.1	1012.4	14.0	3.2	24.0	14	−2.6	10	6.3	12.2	7.8	8.5	7.5	7.7	7.7	7.6	77	56	73	69	2.4	7.5	3.4	4.4	5.2	6.0	4.6	5.3
V	1007.6	1018.0	993.2	1011.7	14.2	5.8	24.3	30	0.5	13	9.1	12.5	9.0	9.9	10.2	10.3	9.8	10.1	88	72	85	82	1.5	4.6	1.9	2.7	7.5	7.7	7.1	7.4
VI	1009.7	1023.4	997.8	1013.7	21.3	11.5	28.8	2	6.1	22	15.5	19.7	15.5	16.6	14.4	13.7	14.5	14.2	82	61	83	75	3.3	9.9	3.4	5.5	6.2	6.6	6.1	6.3
VII	1006.6	1022.4	991.1	1010.7	18.8	11.3	31.4	3	6.0	1	14.1	17.3	14.0	14.8	14.5	14.2	14.3	14.3	90	74	89	84	1.7	6.2	1.8	3.2	8.6	7.9	7.5	8.0
VIII	1009.6	1023.9	996.7	1013.7	18.2	10.8	25.6	31	7.5	8	13.7	16.7	13.6	14.4	14.7	14.9	14.2	14.6	93	79	91	88	1.1	4.4	1.5	2.3	7.6	8.0	6.1	7.2
IX	1012.9	1025.1	995.7	1017.0	19.0	10.0	26.9	17	3.4	24	11.8	17.9	13.3	14.1	12.8	13.5	13.4	13.2	90	66	86	81	1.4	7.2	2.1	3.6	5.1	5.1	4.8	5.0
X	1012.3	1025.7	983.2	1016.4	14.5	8.0	20.4	6	3.4	31	9.4	13.9	10.5	11.1	10.6	11.1	11.0	10.9	90	72	87	83	1.2	5.0	1.9	2.7	7.1	6.8	4.1	6.0
XI	1008.9	1031.9	987.6	1013.1	6.6	2.2	11.6	1	−4.4	22	3.8	5.7	4.0	4.4	7.6	7.8	7.4	7.6	92	84	89	88	0.6	1.5	0.9	1.0	8.5	8.2	8.3	8.3
XII	1010.1	1043.0	978.7	1014.4	1.1	−4.9	13.5	5	−18.6	26	−2.7	−1.1	−2.3	−2.1	4.8	5.3	4.9	5.0	87	85	87	86	0.7	0.9	0.7	0.8	7.6	7.2	6.4	7.1
Rok	1010.3	1043.0	978.7	1014.4	11.8	4.7	31.4	3. VII	−18.6	26. XII	7.0	10.4	7.5	8.1	9.6	9.8	9.7	9.7	88	74	86	83	1.3	4.3	1.7	2.4	7.3	7.2	6.4	7.0

Kołobrzeg – Wydma — φ = 54°11' — λ = 15°33'

I	–	–	–	–	1.6	−3.4	5.8	30	−13.5	27	−1.9	0.8	−1.0	−0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.4	6.7
II	–	–	–	–	5.4	0.7	12.6	18	−3.1	5	2.0	4.2	2.6	2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.4	7.9	8.3
III	–	–	–	–	7.6	2.7	16.9	10	−2.8	20	4.0	5.9	5.1	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	7.3	7.8
IV	–	–	–	–	12.4	4.0	24.6	14	−1.0	10	6.7	10.3	8.0	8.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.0	5.2	5.6
V	–	–	–	–	12.8	7.5	22.0	26	3.4	13	9.7	10.9	9.8	10.1	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.9	7.3	7.7
VI	–	–	–	–	19.9	12.6	26.1	25	7.8	22	15.6	17.3	15.5	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.5	5.9	6.1
VII	–	–	–	–	18.9	12.7	30.1	3	8.8	6	14.8	17.4	15.1	15.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	7.4	7.8
VIII	–	–	–	–	18.1	12.5	23.9	10	9.9	8, 14	14.6	16.8	15.0	15.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.9	7.5
IX	–	–	–	–	18.9	11.5	27.2	1	6.2	24	12.8	17.8	14.6	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.2	4.6	4.9
X	–	–	–	–	14.8	8.8	21.3	6	3.9	31	9.7	14.2	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	5.1	6.0
XI	–	–	–	–	7.1	3.2	12.0	1	−5.0	23	4.8	6.5	4.9	5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.3	8.4	8.5
XII	–	–	–	–	1.6	−3.7	13.5	5	−16.4	28	−1.8	−0.1	−1.0	−1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.9	6.8	7.1
Rok	–	–	–	–	11.6	5.8	30.1	3 VII	−16.4	28. XII	7.6	10.2	8.3	8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	6.6	7.0

Kołobrzeg — φ = 54°11' — λ = 15°35'

I	1016.5	1043.0	991.5	1017.3	1.7	−3.4	6.3	29	−13.8	25, 26	−2.0	0.8	−1.2	−0.9	4.8	5.2	4.9	5.0	84	76	83	81	0.7	1.5	0.9	1.0	6.9	6.7	6.3	6.6
II	1018.5	1035.9	987.9	1019.3	5.6	0.8	13.2	18	−4.9	5	2.0	4.2	2.7	2.9	6.6	7.1	6.8	6.8	93	87	92	91	0.5	1.3	0.6	0.8	8.6	8.5	7.8	8.3
III	1014.6	1034.8	985.5	1015.3	8.1	2.8	16.8	10	−2.8	20	3.9	6.4	5.3	5.2	7.2	7.4	7.4	7.3	88	77	82	82	1.0	2.5	1.6	1.7	8.6	7.6	7.3	7.8
IV	1011.9	1024.1	1000.9	1012.6	12.7	3.9	24.6	14	−1.5	10	6.5	10.9	7.6	8.2	7.6	7.7	8.1	7.8	77	62	77	72	2.3	6.2	2.8	3.8	5.7	6.0	5.2	5.6
V	1011.4	1022.2	997.6	1012.1	13.2	7.0	21.8	26	2.7	13	9.6	11.4	9.6	10.0	10.4	10.5	10.1	10.3	87	78	84	83	1.6	3.3	2.0	2.3	8.0	7.7	7.2	7.6
VI	1013.4	1027.2	1001.3	1014.1	20.2	12.4	26.5	25	8.0	22	15.6	18.1	15.5	16.1	14.5	14.3	14.5	14.4	81	70	83	78	3.4	6.8	3.3	4.5	6.0	6.6	5.9	6.2
VII	1010.2	1025.9	994.8	1010.9	19.1	12.4	31.1	3	7.4	1	14.7	17.6	14.9	15.5	14.5	14.7	14.4	14.5	87	73	85	82	2.4	5.8	2.6	3.6	8.4	7.7	7.4	7.8
VIII	1013.2	1027.7	999.8	1013.9	18.5	12.2	24.5	10	9.7	14	14.4	17.1	14.8	15.3	14.7	15.2	14.7	14.9	89	75	87	84	1.8	4.5	2.2	2.8	7.6	8.0	6.9	7.5
IX	1016.5	1028.8	999.2	1017.2	19.2	10.9	22.6	1	4.6	24	12.4	18.0	13.9	14.6	13.1	14.6	13.7	13.8	89	70	85	81	1.6	6.5	2.4	3.5	4.9	5.1	4.8	4.9
X	1015.7	1029.0	985.8	1016.4	14.9	8.4	21.1	6	3.8	31	9.7	14.2	10.6	11.3	10.7	11.6	11.3	11.2	89	73	88	83	1.3	4.9	1.6	2.6	6.5	6.4	5.1	6.0
XI	1012.6	1036.2	991.1	1013.3	7.3	2.8	12.2	1	−6.3	23	4.3	6.5	4.7	5.0	7.7	7.9	7.6	7.7	90	80	87	86	0.9	1.9	1.2	1.3	8.7	8.1	8.2	8.3
XII	1013.8	1047.4	981.2	1014.6	1.7	−3.8	13.7	5	−17.0	26	−2.0	−0.1	−1.1	−1.1	4.3	5.3	4.9	5.0	83	81	80	81	0.9	1.2	1.2	1.1	7.4	7.0	7.0	7.1
Rok	1014.0	1047.4	981.2	1014.7	11.8	5.5	31.1	3. VII	−17.0	26. XII	7.4	10.4	8.1	8.5	9.7	10.1	9.9	9.9	86	75	84	82	1.5	3.9	1.9	2.4	7.3	7.1	6.6	7.0

Nowy Dwór Gdański $H_s = 0\ m$ $h_w = 13\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU ⁿD, ᵛmD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		◔	●	Opad R			≡	⊠	R ⊘
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15			R ≥ 0.1	R ≥ 1.0	R ≥ 10.0			
I	1	2.0	9	2.8	14	1.4	14	2.0	21.5	2.4	19.5	1.9	3	2.0	5	2.4	6	1.9	21.6	5.9	11	7	11	22	·	·	·	·	14	11	5	·	1	—	
II	5	1.8	3	2.3	6	1.8	20.5	2.3	14.5	2.3	7.5	1.6	13.5	2.0	8	2.4	6	2.0	42.8	14.2	9	·	·	10	·	·	·	1	21	9	7	2	7	—	·
III	1.5	3.0	·	·	·	·	1	3.0	5	2.6	22	2.6	31.5	2.8	29	3.9	3	3.0	17.1	5.7	21	·	·	6	·	1	·	1	8	10	6	·	1	—	·
IV	13	2.0	15	2.3	20	2.5	10	3.1	3	2.3	6	1.8	3	2.0	11	2.9	9	2.0	10.8	2.4	18	·	·	8	·	·	·	8	3	7	6	·	1	·	1
V	20	3.0	11.5	1.9	8	2.1	11.5	1.6	5.5	3.0	9	2.7	5.5	2.1	17	2.8	5	2.3	112.8	35.4	7	·	·	·	1	·	·	1	12	16	15	4	·	·	5
VI	7	2.6	11	1.7	15.5	1.5	5.5	1.8	6	1.4	5.5	2.5	23	2.0	10.5	2.3	6	1.8	47.9	21.1	14	·	·	·	12	·	·	5	5	9	6	1	·	·	5
VII	8	1.4	9	1.4	3	2.7	8	1.7	9	2.6	28.5	2.5	22.5	2.0	·	·	5	2.0	138.5	33.2	13	·	·	·	3	·	·	2	19	23	19	4	1	·	8
VIII	6	1.2	3	1.0	3	1.3	2	3.0	12	1.3	21	2.0	30.5	1.8	8.5	2.0	7	1.6	108.4	27.5	10	·	·	·	3	·	·	1	8	22	17	3	·	·	3
IX	4.5	1.2	9	1.9	15	1.9	7	2.7	4.5	1.8	14	2.5	14.5	1.9	6.5	2.2	15	1.7	35.6	23.5	14	·	·	·	4	·	·	12	2	7	4	1	3	·	1
X	1	3.0	4.5	1.6	33	2.6	17	2.5	14.5	2.0	6	2.3	10	1.8	3	2.2	4	2.2	27.7	7.1	25	·	·	·	·	·	·	8	10	10	6	·	6	·	·
XI	2.5	5.8	12.5	3.6	17.5	2.6	7	1.7	18.5	2.4	18	2.4	5.5	1.7	6.5	2.1	2	2.5	39.0	8.5	18	·	·	8	·	·	·	1	21	16	8	·	5	—	·
XII	4	8.0	12	4.2	13.5	1.6	15.5	2.2	8	2.4	22.5	2.5	6	2.0	9.5	3.4	2	2.8	41.9	9.1	23	10	12	24	·	2	·	2	12	12	8	·	2	—	·
Rok	73.5	2.9	99.5	2.1	148.5	1.8	119	2.3	122	2.2	179.5	2.3	168.5	2.0	114.5	2.4	70	2.2	644.1	35.4	7.V	17	23	78	23	3	·	42	135	152	107	15	27	—	23

Koszalin $H_s = 33\ m$ $H_b = 33{,}9\ m$ $h_w = 13{,}5\ m$

I	3	2.3	2.5	3.0	4.5	2.8	29	4.5	24.5	5.1	19	4.8	3	3.7	5.5	3.4	2	4.3	38.7	7.7	30	3	10	23	·	3	·	5	18	16	12	·	7	7	·
II	2	5.8	1	3.0	0.5	2.0	15	5.4	23	4.8	17.5	3.5	17	3.9	7	5.1	1	4.4	60.9	20.9	28	·	·	10	·	1	·	1	19	15	10	3	12	3	·
III	4	6.8	·	·	·	·	·	·	7	4.1	26.5	6.7	47	7.6	8.5	6.5	·	6.9	38.5	7.4	29	·	·	7	·	13	2	·	17	15	13	·	8	1	·
IV	8	3.1	5.5	4.6	12.5	4.3	27.5	4.5	7	4.6	6.5	2.9	10.5	3.6	7.5	3.9	5	3.8	9.2	1.8	17	·	·	8	·	1	·	5	5	9	5	·	2	1	1
V	20	4.2	5.5	4.7	0.5	1.0	9.5	3.8	5	4.8	14.5	5.7	14.5	4.3	17.5	3.8	6	4.1	64.6	11.8	28	·	·	·	·	·	·	·	16	20	12	1	4	·	3
VI	6	2.6	2.5	1.8	5	3.4	10.5	3.0	10	3.4	11	5.7	32.5	5.1	9.5	2.6	3	4.0	49.1	12.2	10	·	·	·	7	1	·	1	7	11	10	1	5	·	6
VII	3	2.5	0.5	2.0	2	4.5	8	3.8	11.5	4.2	32.5	5.0	18	4.4	12.5	4.1	5	4.2	146.2	50.7	31	·	·	·	3	4	·	2	20	27	20	4	2	·	8
VIII	2.5	1.8	0.5	1.0	0.5	1.0	7.5	3.2	14	3.9	23	4.2	30	4.9	9	3.6	6	3.9	109.8	30.2	19	·	·	·	1	1	·	2	12	21	13	3	7	·	2
IX	5.5	1.7	3	2.7	3.5	3.0	26	4.3	7	4.3	15.5	4.5	11.5	4.2	8	4.1	10	3.6	99.9	46.3	7	·	·	·	2	·	·	9	9	10	8	2	2	·	3
X	·	·	·	·	9	4.2	36.5	5.4	28	4.3	7	5.4	9	3.6	3.5	4.6	·	4.7	31.2	6.2	26	·	·	·	·		·	5	11	12	9	·	2	·	·
XI	5.5	2.9	9.5	4.2	6	4.1	12.5	3.3	21.5	4.5	21.5	5.8	4.5	6.0	4	5.5	5	4.3	40.6	11.6	10	·	·	7	·	2	·	1	20	16	9	2	6	·	·
XII	8.5	2.3	6.5	3.2	4.5	2.0	19.5	4.4	21.5	5.2	20	7.3	7.5	6.4	3	1.7	2	5.2	46.2	12.1	2	9	10	23	·	7	3	3	14	14	7	1	5	9	·
Rok	68	3.4	37	2.5	48.5	2.7	201.5	3.8	180	4.4	214.5	5.1	205	4.8	95.5	4.1	45	4.4	734.9	50.7	31.VII	12	20	78	13	33	5	34	168	186	128	17	62	21	23

Kołobrzeg – Wydma $H_s = 5\ m$ $h_w = 11\ m$

I	2	2.5	2.5	4.8	10.5	3.4	22.5	3.5	25.5	4.3	21	5.3	3.5	4.9	5.5	4.4	·	4.2	39.1	9.1	4	3	9	19	·	—	—	6	17	15	11	·	—	6	—
II	1.5	5.7	2.5	4.6	4	2.1	11.5	4.7	20.5	4.4	21	4.1	20	3.9	3	4.2	·	4.2	54.9	15.5	28	·	·	8	·	—	—	·	17	18	10	1	—	2	—
III	2.5	8.4	·	·	·	·	0.5	3.0	7.5	4.3	32.5	6.5	44	7.4	6	7.5	·	6.8	31.4	4.8	29	·	·	3	·	—	—	·	19	17	12	·	—	·	—
IV	4.5	3.3	19.5	5.1	15	4.4	15	4.0	7	3.1	8.5	3.2	11.5	3.8	9	3.8	·	4.1	4.6	2.2	1	·	·	3	·	—	—	3	4	8	1	·	—	·	—
V	15	5.4	12.5	6.1	2	3.2	5	2.8	16	3.4	13.5	4.3	15	4.0	14	4.7	·	4.5	71.1	11.1	28	·	·	·	·	—	—	·	19	19	14	1	—	·	—
VI	9	2.8	13.5	3.3	3	2.7	3.5	3.0	7	3.2	18.5	5.1	27	5.7	6.5	4.5	2	4.3	46.3	11.2	10	·	·	·	3	—	—	2	4	10	7	2	—	·	—
VII	3	3.5	2	2.8	2.5	4.6	5	2.3	26	4.6	27	4.9	22.5	6.5	4	7.0	1	5.0	154.3	28.4	31	·	·	·	3	—	—	2	15	22	17	5	—	·	—
VIII	3.5	1.6	6	2.0	1	2.0	3	2.0	26.5	3.7	21.5	4.6	26	6.3	3.5	5.6	2	4.4	135.0	48.9	19	·	·	·	·	—	—	2	15	22	21	3	—	·	—
IX	3	2.5	8	2.8	11	3.7	18.5	3.0	14	3.2	13	5.0	18	6.0	4.5	5.0	·	4.1	77.0	40.4	7	·	·	·	2	—	—	8	7	11	7	2	—	·	—
X	·	·	1	3.0	19.5	4.5	20	3.6	33.5	4.0	9.5	4.7	9.5	3.8	·	·	·	4.1	31.4	5.4	26	·	·	·	·	—	—	6	11	12	9	·	—	·	—
XI	6.5	7.7	12	6.4	10.5	3.5	9.5	3.0	26	4.4	15	5.0	3	7.2	7.5	6.4	·	5.0	25.1	8.0	30	·	·	4	·	—	—	1	21	14	8	·	—	·	—
XII	9.5	8.5	5.5	6.9	11.5	3.8	15	3.5	27	5.3	14.5	5.9	7.5	7.2	2.5	5.8	·	5.5	46.5	8.6	11	8	8	18	·	—	—	3	14	13	10	·	—	16	—
Rok	60	4.3	85	4.0	90.5	3.2	129	3.2	236.5	4.0	215.5	4.9	207.5	5.6	66	4.9	5	4.7	716.7	48.9	19.VIII	11	17	55	8	—	—	33	163	181	127	14	—	24	—

Kołobrzeg $H_s = 3\ m$ $H_b = 5{,}4\ m$ $h_w =$ 22 anemometr, 13 wiatromierz Wilda

I	2.5	3.0	1.5	5.0	12	3.4	19.5	4.1	23.5	3.9	24.5	5.0	4	4.2	5.5	4.5	·	4.2	32.6	8.2	4	3	8	18	·	1	·	6	15	16	10	·	3	6	·
II	1	7.0	2	5.5	4	2.5	12	4.8	14.5	4.1	20.5	4.7	25.5	4.2	4.5	3.7	·	4.3	50.5	14.9	28	·	·	7	·	·	·	·	18	18	10	1	11	2	·
III	4	6.5	·	·	·	·	·	·	4.5	4.0	16	5.4	62	7.0	6.5	6.7	·	6.5	34.2	5.4	29	·	·	2	·	13	·	·	18	17	10	·	9	·	·
IV	5.5	3.7	16	5.1	17	3.8	18	4.9	5	3.5	8.5	2.9	12	3.7	8	2.7	·	4.0	5.8	2.1	1	·	·	6	·	1	·	3	5	7	1	·	5	·	·
V	13.5	4.8	16	5.5	3.5	1.3	6.5	2.7	10.5	2.6	15	3.8	18.5	4.5	10.5	4.0	·	4.1	76.5	12.0	28	·	·	·	·		·	·	19	21	14	1	3	·	3
VI	8.5	2.9	10.5	3.7	8.5	2.4	3	2.2	6.5	3.3	17	4.4	27	5.7	6	4.5	3	4.1	60.0	24.8	10	·	·	·	3	·	·	2	4	11	8	2	3	·	6
VII	2	1.5	3.5	2.7	2.5	4.6	5.5	2.7	15.5	3.5	35.5	4.4	21	5.6	6.5	4.3	1	4.2	141.4	30.9	31	·		·	3	1	·	2	18	24	17	6	2	·	6
VIII	3.5	2.1	4.5	2.1	3.5	1.6	2.5	2.2	15	2.8	29.5	4.0	28	5.2	4.5	4.8	2	3.8	116.1	42.3	19	·		·	·	·		2	15	21	20	2	1	·	2
IX	2	2.5	4.5	3.6	16	3.3	15.5	3.0	9.5	2.7	18.5	4.2	15.5	5.5	6.5	3.3	2	3.7	70.8	35.2	7		·	·	2	·	·	8	6	12	7	2	2	·	1
X	0.5	1.0	0.5	1.0	23	4.8	15.5	4.5	28	3.5	17	4.0	8.5	4.1	·	·	·	4.1	27.8	5.0	26	·	·	·		·	·	6	11	12	9	·	1	·	·
XI	6	6.7	11	5.1	10.5	3.5	9.5	3.4	16.5	4.2	26	5.3	3.5	4.6	5	5.7	2	4.6	26.8	6.8	30	·		5		1	·	2	20	19	8	·	5	·	·
XII	9	2.3	4.5	5.3	12	4.0	17	3.6	18	4.8	24.5	5.9	5.5	7.0	2.5	4.8	·	5.2	45.3	7.4	4	8	8	20	·	5	1	3	15	16	9	·	2	16	·
Rok	58	4.1	74.5	3.7	112.5	2.9	123.5	3.2	167	3.6	252.5	4.5	231	5.1	66	4.1	10	4.4	602.8	42.3	19.VIII	11	16	58	8	22	1	34	164	194	123	14	47	24	18

Uwaga. Kierunki wiatru – wg wiatromierza Wilda, prędkości wg anemometru.

Żelisławki

$\varphi = 54°10'$ $\lambda = 18°39'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	−4.6	5.0	31	−15.7	26	−3.2	−0.5	−2.3	−2.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	5.9	6.1
II	–	–	–	–	4.0	0.1	15.1	13	−5.4	5	0.9	2.0	1.7	1.8	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.6	7.9	8.5
III	–	–	–	–	8.8	1.8	17.2	10	−5.0	20	3.5	7.4	4.5	5.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.7	4.0	5.4
IV	–	–	–	–	14.0	2.5	23.6	7	−4.0	11	5.8	12.3	6.5	7.8	–	–	–	–	–	–	–	–	–	–	–	–	3.6	3.9	3.0	3.5
V	–	–	–	–	15.0	5.7	24.0	30	0.7	13	9.3	13.4	9.6	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.7	6.3	7.1
VI	–	–	–	–	23.0	12.0	28.1	27	6.3	1	15.8	21.5	16.1	17.4	–	–	–	–	–	–	–	–	–	–	–	–	3.5	4.7	5.1	4.4
VII	–	–	–	–	20.4	11.3	32.8	3	7.4	4	14.6	18.4	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.5	7.5	7.3
VIII	–	–	–	–	19.7	11.5	27.4	6	8.6	4	14.0	18.3	13.9	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	6.5	6.9
IX	–	–	–	–	19.5	9.2	28.4	17	1.8	24	11.3	18.3	12.5	13.6	–	–	–	–	–	–	–	–	–	–	–	–	3.9	3.9	3.5	3.8
X	–	–	–	–	14.6	6.8	19.5	5	2.6	23	8.1	13.7	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.4	3.6	5.2
XI	–	–	–	–	6.0	1.8	10.8	1	−4.4	23	3.0	5.0	2.7	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.9	7.9	8.2
XII	–	–	–	–	0.1	−6.4	13.1	5	−19.1	17	−3.4	−1.6	−3.5	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.5	5.7	6.6
Rok	–	–	–	–	12.1	4.3	32.8	3.VII	−19.1	17.XII	6.8	10.7	7.2	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	5.6	6.1

Elbląg

$\varphi = 54°10'$ $\lambda = 19°26'$

I	1013.0	1039.4	991.8	1018.5	0.3	−4.5	5.6	5	−16.8	26	−3.2	−0.6	−2.1	−2.0	4.5	4.8	4.7	4.7	86	77	83	82	0.6	1.2	0.9	0.9	7.1	8.3	6.7	7.4
II	1014.5	1032.0	986.7	1020.0	3.9	−0.2	11.7	18	−4.6	5	0.7	2.7	1.7	1.7	6.0	6.6	6.4	6.3	94	88	91	91	0.4	0.9	0.6	0.6	8.5	8.8	8.6	8.6
III	1007.7	1028.9	981.4	1013.1	8.6	1.3	17.1	10	−8.1	20	3.2	7.1	4.5	4.8	6.9	6.8	7.0	6.9	88	69	82	80	0.9	3.4	1.6	2.0	8.6	7.6	6.5	7.6
IV	1008.0	1020.9	997.5	1013.3	14.1	4.1	22.9	7	−3.5	2	6.4	12.6	8.3	8.9	7.0	7.4	7.3	7.2	72	50	66	63	2.9	8.0	4.1	5.0	4.7	5.5	4.3	4.8
V	1006.0	1013.4	994.1	1011.3	15.1	6.8	25.5	30	2.5	2	9.5	13.5	9.6	10.6	10.2	10.3	10.1	10.2	85	67	84	79	1.9	5.6	2.1	3.2	7.3	7.8	6.6	7.2
VI	1008.3	1021.0	997.5	1013.4	22.9	13.3	29.2	27	6.8	22	16.7	21.8	17.2	18.2	14.4	13.8	14.4	14.2	76	54	74	68	5.0	13.0	5.5	7.8	5.6	6.3	5.6	5.8
VII	1005.8	1020.6	990.3	1011.0	20.1	11.5	30.7	3	7.4	6	14.2	18.3	15.0	15.6	14.2	14.6	14.5	14.4	88	70	85	81	2.2	7.0	2.8	4.0	8.0	8.0	7.8	7.9
VIII	1008.4	1023.9	995.1	1013.6	19.2	11.4	27.8	6	8.4	18	13.7	18.0	13.9	14.9	14.4	15.0	14.2	14.5	91	73	89	84	1.4	6.1	1.8	3.1	8.2	8.4	7.1	7.9
IX	1012.4	1026.1	995.7	1017.6	16.9	9.9	27.2	2	3.4	27	12.1	18.1	13.1	14.1	12.3	13.3	12.8	12.8	85	64	83	77	2.1	8.0	2.5	4.2	5.2	5.2	4.0	4.8
X	1013.3	1026.9	987.0	1018.6	14.7	8.1	19.5	4	3.5	14	9.0	13.9	11.2	11.3	10.1	11.4	10.6	10.7	88	72	81	80	1.4	4.7	2.8	3.0	6.3	6.8	5.4	6.2
XI	1008.2	1029.6	990.0	1013.6	6.0	1.7	11.2	3, 8	−4.8	20	3.1	5.1	3.8	4.0	7.0	7.2	7.2	7.1	89	81	88	86	0.8	1.7	1.0	1.2	9.0	8.7	8.5	8.7
XII	1009.1	1041.9	980.3	1014.7	−0.2	−6.6	13.0	5	−19.2	27	−3.8	−2.0	−3.6	−3.2	4.5	4.9	4.5	4.6	85	81	85	84	0.7	1.0	0.8	0.8	8.0	7.5	5.8	7.1
Rok	1009.6	1041.9	980.3	1014.9	12.0	4.7	30.7	3.VII	−19.2	27.XII	6.8	10.7	7.7	8.2	9.3	9.7	9.5	9.5	86	70	83	80	1.7	5.0	2.2	3.0	7.2	7.4	6.4	7.0

Płocko

$\varphi = 54°09'$ $\lambda = 16°50'$

I	–	–	–	–	0.3	−5.4	5.3	29	−18.0	26	−3.6	−1.0	−2.7	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.5	6.4	7.0
II	–	–	–	–	4.5	−0.6	14.2	18	−12.4	5	0.9	3.7	1.9	2.1	–	–	–	–	–	–	–	–	–	–	–	–	9.1	6.9	7.7	7.9
III	–	–	–	–	7.6	1.2	17.5	10	−5.7	20	3.2	6.5	4.2	4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.0	7.5	7.6
IV	–	–	–	–	14.1	2.1	23.0	14	−3.9	11	6.5	12.8	7.6	8.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.6	5.3	5.0
V	–	–	–	–	14.2	4.7	25.0	30	−0.8	13	9.1	12.9	8.7	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	7.6	7.1
VI	–	–	–	–	21.6	11.6	27.2	2	7.3	1	15.7	20.5	15.7	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.4	7.2	5.8
VII	–	–	–	–	18.8	11.1	30.6	3	7.4	2	14.2	17.5	14.0	14.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.7	8.0	7.8
VIII	–	–	–	–	18.6	11.2	29.9	6	8.4	26	13.8	17.8	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.2	7.6	6.9
IX	–	–	–	–	19.0	8.2	27.4	17	0.4	24	11.8	18.4	12.3	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.5	5.4	5.1
X	–	–	–	–	14.1	7.0	19.2	6	3.8	23, 30	10.1	13.6	10.5	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.1	6.5	6.6
XI	–	–	–	–	6.2	1.5	10.5	1, 2, 3	−6.6	23	3.5	5.8	4.0	4.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.9	7.2	8.0
XII	–	–	–	–	0.2	−5.9	11.4	5	−21.8	17	−3.7	−2.2	−2.7	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.6	7.4
Rok	–	–	–	–	11.6	3.9	30.6	3.VII	−21.8	17.XII	6.8	10.5	7.3	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.4	7.0	6.9

Kościerzyna

$\varphi = 54°08'$ $\lambda = 17°58'$

I	–	–	–	–	−0.3	−5.5	4.3	30	−19.1	26	−3.8	−1.2	−2.9	−2.7	4.3	4.8	4.6	4.6	85	82	85	84	0.6	1.0	0.7	0.8	8.0	7.6	6.7	7.3
II	–	–	–	–	3.5	−1.0	15.1	18	−11.7	5	0.4	2.6	1.1	1.3	5.9	6.5	6.1	6.2	92	88	92	91	0.5	1.0	0.6	0.7	9.7	9.0	8.2	9.0
III	–	–	–	–	7.8	1.1	16.9	10	−6.0	20	3.1	6.5	3.9	4.4	6.8	6.6	6.7	6.7	87	69	83	80	1.0	3.3	1.4	1.9	8.6	7.3	6.2	7.4
IV	–	–	–	–	13.4	2.6	22.8	7	−5.0	2	5.9	12.0	6.7	7.8	7.1	6.8	7.2	7.0	75	49	72	65	2.5	8.0	3.0	4.5	4.4	5.1	2.7	4.0
V	–	–	–	–	14.3	5.4	23.5	30	0.2	2	9.2	13.0	7.9	9.5	9.5	9.5	9.1	9.4	81	65	84	77	2.3	5.8	1.7	3.3	7.0	6.6	5.5	7.0
VI	–	–	–	–	22.0	11.5	30.0	27	6.1	1, 22	15.7	20.7	15.4	16.8	13.9	12.9	13.6	13.5	78	54	78	70	4.2	12.1	4.1	6.8	5.2	5.6	5.8	5.5
VII	–	–	–	–	18.6	10.6	30.8	3	5.4	1	13.6	16.7	13.8	14.5	13.8	13.8	13.7	13.8	88	74	86	83	1.9	5.9	2.2	3.3	8.8	8.3	8.2	8.4
VIII	–	–	–	–	18.2	10.8	25.3	6	7.9	14	13.1	16.9	13.3	14.2	13.9	14.0	13.7	13.9	92	73	90	85	1.3	5.6	1.6	2.8	8.3	7.8	5.9	7.3
IX	–	–	–	–	18.4	8.6	27.2	2	2.4	24	10.8	17.2	11.8	12.9	12.2	13.1	12.4	12.6	92	67	87	82	1.0	7.1	1.8	3.3	5.3	5.3	3.7	4.8
X	–	–	–	–	13.5	7.2	18.2	5	2.1	30	8.3	12.6	9.7	10.1	10.1	11.0	10.5	10.5	92	76	87	95	0.9	3.8	1.6	2.1	7.2	7.2	4.2	6.2
XI	–	–	–	–	5.4	1.1	9.8	1	−7.2	23	2.6	3.8	3.2	3.2	7.0	7.2	7.0	7.1	92	83	88	88	0.6	1.5	0.9	1.0	8.9	8.5	7.9	8.4
XII	–	–	–	–	−0.6	−6.6	11.9	5	−20.1	26	−3.7	−1.9	−3.9	−3.4	4.4	4.8	4.4	4.5	86	84	87	86	0.6	0.9	0.6	0.7	7.9	7.6	5.9	7.1
Rok	–	–	–	–	11.2	3.8	30.8	3.VII	−20.1	26.XII	6.3	9.9	6.7	7.4	9.1	8.2	9.1	9.1	87	72	85	81	1.4	4.7	1.7	2.6	7.4	7.3	5.9	6.9

Żelistawki

$H_s = 68\ m$ $h_w = 12\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%D, *mD)																		OPAD R			LICZBA DNI (n)											
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v				Opad R				
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max≥25°	≥10	≥15	●	●	≥0.1	≥1.0	≥10.0	≡	▦	≋
I	25	34	15	30	65	23	55	30	18	34	25	48	12	56	6	70	16	36	21.0	70	31	7	11	24	·	2	·	5	12	11	6	·	·	5	·
II	15	37	1	20	·	·	4	48	205	42	22	40	25	55	3	47	7	41	26.8	110	28	·	·	10	·	5	·	1	19	7	7	1	4	3	·
III	15	63	·	·	·	·	·	·	35	53	19	76	44	91	23	108	2	89	17.0	39	27	·	·	10	·	21	8	5	8	9	7	·	·	3	·
IV	85	22	45	44	45	39	135	39	65	30	13	46	95	37	9	68	21	32	13.3	49	1	·	·	8	·	2	·	11	3	6	5	·	2	1	1
V	14	39	5	28	15	17	15	23	65	30	165	39	125	60	165	45	19	33	53.6	144	6	·	·	·	·	1	·	3	13	14	13	1	2	·	2
VI	14	26	05	20	15	27	35	29	5	25	55	34	365	59	75	50	16	37	55.2	123	7	·	·	·	10	5	·	8	6	10	8	2	·	·	4
VII	35	26	2	25	2	35	·	·	5	23	29	40	225	52	5	43	19	34	77.0	140	31	·	·	·	4	4	·	2	17	18	17	2	·	·	4
VIII	25	24	·	·	1	10	1	20	8	28	185	39	41	52	5	45	16	37	52.9	143	10	·	·	·	2	3	·	1	13	16	9	2	1	·	2
IX	15	20	35	20	4	30	4	26	65	31	9	35	265	47	6	52	29	27	23.2	148	14	·	·	·	4	1	·	14	5	8	5	1	·	·	·
X	05	30	·	·	15	27	195	32	15	25	175	29	105	51	45	41	24	25	37.0	181	18	·	·	·	·	·	·	8	9	10	9	1	4	·	·
XI	2	85	6	37	7	39	8	30	115	29	25	56	85	54	4	80	18	38	43.3	155	11	·	·	9	·	4	·	3	20	16	11	1	5	·	·
XII	25	54	2	25	4	50	55	24	7	37	305	59	155	73	10	58	16	46	36.9	63	2	12	13	23	·	8	3	3	14	11	9	·	2	18	·
Rok	545	38	26	21	335	25	66	25	113	32	2305	45	269	57	385	59	203	40	457.2	181	18.X	19	24	84	20	56	11	64	139	136	106	11	20	30	137

Elbląg

$H_s = 38\ m$ $H_b = 42{,}8\ m$ $h_w = 14{,}5\ m$ anemometr; $14\ m$ wiatromierz Wilda

I	7	37	9	39	6	29	285	46	25	48	7	40	25	24	5	33	3	41	18.2	46	30	7	12	23	·	2	·	4	17	12	6	·	·	9	·
II	55	25	1	30	25	36	195	45	26	46	95	29	3	32	9	27	8	35	47.0	149	11	·	·	11	·	1	·	1	22	11	9	2	11	3	·
III	85	55	1	20	1	10	3	32	75	43	18	44	205	55	325	50	1	48	23.0	53	3	·	·	8	·	6	1	·	15	8	7	·	5	2	·
IV	11	39	145	59	215	51	165	57	85	34	3	37	5	49	8	64	2	50	29.1	90	17	·	·	6	·	9	·	7	3	7	6	·	2	2	2
V	25	43	10	36	9	46	65	47	10	42	95	45	6	36	15	46	2	42	92.9	162	7	·	·	·	1	1	·	1	14	14	11	6	2	·	6
VI	8	36	7	50	13	42	9	48	55	40	13	33	14	37	185	40	2	39	88.7	344	14	·	·	·	10	2	·	5	7	10	7	5	1	·	8
VII	3	33	3	30	75	45	75	33	18	36	185	31	195	30	13	20	3	30	166.6	245	13	·	·	·	3	·	·	1	20	21	20	5	1	·	9
VIII	12	27	3	17	2	20	5	29	14	31	185	37	17	31	185	27	3	29	91.4	125	6	·	·	·	1	·	·	1	17	16	15	3	4	·	2
IX	8	17	95	25	11	43	145	43	75	43	115	23	13	29	15	28	·	32	68.5	402	14	·	·	·	4	2	·	7	7	6	6	1	·	·	3
X	15	20	1	20	205	60	275	59	195	43	65	42	2	42	115	29	3	48	36.9	109	26	·	·	·	·	2	·	6	15	10	9	1	1		
XI	75	58	55	55	9	22	185	45	155	37	135	49	105	35	9	33	1	46	31.8	51	10	·	·	8	·	2	·	1	24	11	8	·	6	2	·
XII	75	53	13	53	2	20	21	44	155	38	135	53	55	49	9	28	6	42	39.0	83	20	10	13	23	·	4	1	2	14	13	8	·	2	14	·
Rok	1045	37	775	40	105	40	177	44	1725	40	142	39	1185	37	164	35	34	40	733.1	402	14.IX	17	25	79	19	31	2	36	175	139	112	23	35	32	29

Uwaga. Kierunki wiatru – wg wiatromierza Wilda, prędkości – wg anemometru.

Płocko

$H_s = 125\ m$ $h_w = 14\ m$

I	35	24	11	15	1	10	21	27	30	26	18	38	4	20	25	18	2	26	35.6	102	29	9	12	25	·	1	·	–	–	14	12	1	1	7	–
II	15	40	6	27	·	·	2	25	22	24	24	29	17	26	45	31	7	25	96.0	394	28	1	·	10	·	·	·	–	–	9	9	4	5	4	–
III	2	25	1	20	·	·	·	·	3	48	25	54	36	51	22	44	4	47	70.0	155	28	·	·	10	·	6	·	–	–	15	12	2	2	4	–
IV	9	19	13	28	9	18	13	37	9	26	8	33	9	31	10	20	10	24	23.9	144	1	·	·	11	·	·	·	–	–	6	4	1	·	1	–
V	185	14	55	22	1	20	4	18	7	26	15	31	18	22	24	21	·	23	100.3	180	30	·	·	1	1	·	·	–	–	15	13	4	·	·	–
VI	35	17	4	15	4	12	5	24	45	23	215	40	28	25	105	30	9	25	81.7	344	14	·	·	·	9	·	·	–	–	11	9	3	·	·	–
VII	3	30	1	20	·	·	4	12	125	21	40	41	185	29	7	27	7	30	206.6	494	31	·	·	·	4	·	·	–	–	26	21	6	1	·	–
VIII	3	13	·	·	1	10	4	20	135	29	345	34	24	39	6	25	7	30	105.9	289	19	·	·	·	2	·	·	–	–	20	16	1	3	·	–
IX	12	18	6	22	4	20	11	28	115	28	215	29	13	28	8	25	3	25	80.0	222	14	·	·	·	3	·	·	–	–	11	9	3	2	·	–
X	·	·	3	37	10	51	155	42	26	45	205	50	10	44	3	50	5	44	32.9	50	23	·	·	·	·	3	·	–	–	11	9	·	1	·	–
XI	5	36	5	56	4	52	12	56	215	27	235	44	9	38	8	37	2	40	24.1	60	10	·	·	7	·	1	·	–	–	12	7	·	3	·	–
XII	7	30	11	32	3	37	11	35	14	49	23	55	10	57	14	39	·	44	70.2	178	1	9	14	25	·	4	·	–	–	12	10	2	·	19	–
Rok	68	22	665	24	37	19	1025	27	1745	31	2745	40	1965	34	1195	31	56	32	927.2	494	31.VII	19	26	89	19	15	·	–	–	162	131	27	10	35	–

Kościerzyna

$H_s = 180\ m$ $h_w = 12\ m$

I	4	30	4	35	·	·	1	80	15	63	35	28	30	15	125	19	5	23	28.4	97	30	7	12	26	·	·	·	1	17	14	8	·	10	10	·
II	2	10	·	·	05	10	05	10	6	67	235	27	30	17	175	24	4	24	44.5	125	28	1	1	13	·	·	·	1	22	20	9	1	17	6	·
III	·	·	·	·	·	·	·	·	·	·	8	80	50	50	34	50	1	52	51.4	86	12	·	·	10	·	9	1	1	15	17	10	·	4	4	·
IV	8	15	12	35	6	43	13	38	1	30	2	21	175	16	165	23	9	24	18.7	61	1	·	·	10	·	·	·	7	2	10	6	·	1	4	1
V	9	26	6	43	1	10	·	·	1	70	8	38	335	17	245	20	10	21	72.4	132	14	·	·	·	·	·	·	·	12	14	13	2	2	·	4
VI	5	16	4	40	1	50	2	40	1	30	6	47	41	28	23	24	7	27	93.4	362	10	·	·	·	9	2	·	4	6	11	8	4	1	·	8
VII	1	10	1	10	·	·	1	30	·	·	4	58	595	21	185	14	8	19	173.1	337	17	·	·	·	4	1	·	2	22	23	19	5	1	·	10
VIII	3	10	1	30	·	·	·	·	·	·	5	46	62	20	17	18	5	20	124.2	248	6	·	·	·	1	·	·	1	13	24	19	3	5	·	5
IX	3	10	4	45	·	·	3	37	·	·	10	38	265	17	335	15	10	18	70.6	186	29	·	·	·	3	·	·	12	7	11	10	3	2	·	2
X	1	10	4	30	6	30	18	31	2	50	23	33	12	20	22	14	5	25	32.5	99	18	·	·	·	·	·	·	4	12	11	9	·	6	·	·
XI	3	17	10	60	3	63	5	18	1	30	105	44	255	24	22	15	10	26	41.6	78	30	·	·	14	·	·	·	3	21	18	12	·	8	·	·
XII	4	30	6	33	1	30	5	14	3	23	275	32	185	36	23	16	5	26	31.9	76	4	11	15	24	·	1	·	1	13	14	7	·	6	9	·
Rok	43	15	52	30	185	20	485	25	165	30	1675	41	406	23	264	21	79	25	782.7	362	10.VI	19	28	97	17	13	1	37	162	187	130	18	63	33	30

Lidzbark Warmiński

$\varphi = 54°08'$ $\lambda = 20°36'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.2	−5.7	6.1	5	−20.8	26	−4.1	−1.9	−2.9	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.1	7.2	7.3
II	–	–	–	–	3.2	−0.7	10.8	18	−6.8	5	0.3	2.5	1.1	1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.0	7.8	8.3
III	–	–	–	–	7.9	0.7	15.2	10	−4.7	20	2.8	6.5	3.6	4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.0	6.0	6.3
IV	–	–	–	–	14.0	1.8	23.2	7	−4.6	2	6.1	12.5	7.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	4.3	3.8	3.4	3.8
V	–	–	–	–	15.9	6.3	26.2	30	0.4	2	9.9	14.7	9.8	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	6.4	7.1
VI	–	–	–	–	23.2	11.8	31.3	27	6.4	1	15.7	21.4	16.4	17.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	5.1	5.5
VII	–	–	–	–	20.7	11.4	31.1	3	8.2	16	14.2	18.4	15.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	7.9	7.6
VIII	–	–	–	–	19.4	11.1	27.8	6	7.1	18	13.4	18.2	13.8	14.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.6	7.0	7.3
IX	–	–	–	–	19.2	8.4	27.8	17	0.9	24	9.9	17.7	12.2	13.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	4.5	3.9	4.8
X	–	–	–	–	14.5	2.2	19.7	4	2.2	23	8.1	13.2	10.2	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.0	6.5	6.6
XI	–	–	–	–	5.3	1.4	10.9	3	−4.7	24	2.4	4.0	3.1	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.6	8.4	8.6
XII	–	–	–	–	−0.8	−7.7	13.4	5	−23.9	27	−4.8	−2.9	−4.7	−4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.0	5.8	6.5
Rok	–	–	–	–	11.9	3.8	31.3	27.VI	−23.9	27.XII	6.2	10.4	7.1	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.4	6.3	6.7

Ornela

$\varphi = 54°07'$ $\lambda = 20°07'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	19.3	8.3	27.8	2	1.0	24	10.6	18.0	12.1	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.9	4.1	4.8
X	–	–	–	–	14.3	7.0	19.1	4	2.6	10	8.0	13.5	10.3	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.7	5.8	6.7
XI	–	–	–	–	5.9	1.3	10.4	3	−5.2	20	2.6	4.5	3.4	3.5	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.1	8.1	8.5
XII	–	–	–	–	−0.4	−2.7	13.5	5	−26.3	23	−4.7	−2.5	−4.3	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.4	4.7	6.3
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kętrzyn

$\varphi = 54°06'$ $\lambda = 21°21'$

I	1005.1	1029.7	983.4	1018.9	−0.3	−4.7	5.4	4	−18.4	26	−3.6	−1.6	−2.4	−2.5	4.4	4.7	4.7	4.6	86	81	86	84	0.6	1.0	0.7	0.8	7.9	8.2	7.7	7.9
II	1006.8	1024.4	980.3	1020.3	3.0	−0.7	11.0	18	−5.9	5	0.2	2.0	1.0	1.0	5.7	6.3	6.0	6.0	91	88	89	89	0.5	0.9	0.6	0.7	9.4	8.2	8.0	8.5
III	998.8	1019.9	977.0	1012.1	7.8	0.4	15.6	10	−5.4	20	2.7	5.7	3.2	3.7	6.6	6.7	6.5	6.6	88	73	83	81	0.9	2.6	1.4	1.6	8.5	8.1	5.8	7.5
IV	1000.6	1012.5	987.1	1013.7	13.7	2.8	23.5	7	−3.5	2	5.5	12.2	7.5	8.2	7.1	6.9	7.4	7.1	77	49	70	65	2.3	8.3	3.4	4.7	4.9	4.7	3.6	4.4
V	998.4	1006.3	987.7	1011.3	16.0	6.7	24.8	30	1.9	19	9.5	14.2	10.1	11.0	10.4	10.7	10.7	10.6	87	66	86	80	1.7	5.7	1.8	3.1	7.4	7.6	7.2	7.4
VI	1001.1	1012.7	991.5	1013.8	22.5	12.0	30.3	27	7.5	22	16.0	20.8	15.9	17.2	15.0	14.7	14.8	14.8	82	61	82	75	3.4	10.4	3.5	5.8	5.5	5.7	4.7	5.3
VII	998.7	1013.3	983.9	1011.5	20.3	11.3	29.8	3	7.9	6	14.3	18.7	14.8	15.6	14.3	14.2	14.5	14.3	88	67	86	80	2.1	7.8	2.5	4.1	6.9	7.5	6.5	7.0
VIII	1000.8	1016.0	987.8	1013.6	19.3	11.1	27.9	6	8.2	18,26,31	13.6	17.8	13.8	14.8	14.2	14.6	14.0	14.3	91	72	88	84	1.5	6.2	1.9	3.2	7.3	7.7	6.8	7.3
IX	1005.0	1019.1	987.5	1017.8	18.6	8.7	27.5	2	3.5	23	10.9	17.5	12.0	13.1	12.1	13.0	12.5	12.5	91	64	88	81	1.2	7.5	1.7	3.5	4.9	4.8	3.5	4.4
X	1006.9	1020.4	982.5	1020.0	14.1	6.7	18.7	4	1.7	23	7.8	13.3	10.0	10.3	9.6	10.9	10.1	10.2	90	72	82	81	1.1	4.6	2.3	2.7	7.0	6.3	5.0	6.1
XI	1000.7	1020.6	984.9	1014.0	5.1	1.1	10.7	3	−5.6	20	2.4	4.2	3.1	3.2	6.9	7.3	7.1	7.1	92	87	90	90	0.6	1.1	0.8	0.8	8.7	8.5	8.1	8.4
XII	1000.8	1032.1	974.2	1014.5	−1.0	−7.1	12.3	5	−21.2	27	−4.6	−2.7	−4.4	−4.0	4.2	4.6	4.3	4.4	88	82	87	86	0.6	0.9	0.7	0.7	7.2	6.2	5.1	6.2
Rok	1002.0	1032.1	974.2	1015.1	11.6	4.0	30.3	27.VI	−21.2	27.XII	6.2	10.2	7.0	7.6	9.2	9.6	9.4	9.4	88	72	85	82	1.4	4.8	1.8	2.7	7.1	7.0	6.0	6.7

Sumałki

$\varphi = 54°06'$ $\lambda = 22°57'$

I	997.1	1020.7	976.3	1018.8	−1.4	−6.6	4.0	4	−20.4	26	−4.3	−2.9	−3.7	−3.6	4.3	4.6	4.5	4.5	91	88	90	90	0.4	0.5	0.4	0.4	8.6	8.8	8.1	8.5
II	998.9	1016.7	973.6	1020.3	1.9	−2.0	7.2	18	−11.7	5	−0.8	0.8	−0.1	0.0	5.5	5.8	5.8	5.7	94	90	94	93	0.3	0.7	0.3	0.4	9.5	8.7	8.1	8.8
III	989.7	1010.5	968.6	1010.7	6.9	0.7	14.1	10	−4.7	20, 23	1.8	5.3	2.5	3.0	6.2	6.7	6.1	6.3	87	74	83	81	0.9	2.4	1.3	1.5	9.3	8.5	6.1	8.0
IV	992.8	1005.9	977.2	1013.4	13.1	1.5	23.0	7	−3.5	2	4.7	11.6	6.3	7.2	6.9	6.8	7.2	7.0	79	51	73	68	1.9	7.8	2.7	4.1	5.0	5.6	3.8	4.8
V	990.3	998.8	981.6	1010.6	16.0	7.0	26.0	30	1.7	23	9.8	14.5	10.6	11.4	10.3	10.0	10.8	10.4	85	62	84	77	2.0	7.3	2.3	3.9	7.8	8.3	7.1	7.7
VI	993.5	1004.0	984.8	1013.5	22.4	11.9	29.9	27	6.8	21	16.0	20.6	16.0	17.2	14.8	13.6	14.5	14.3	81	58	79	73	3.6	11.2	4.0	6.3	6.4	7.3	5.5	6.4
VII	991.2	1004.8	978.8	1011.2	20.7	11.1	28.5	3	6.8	6	14.4	18.8	15.0	15.8	14.1	13.0	14.0	13.7	86	62	82	77	2.3	9.1	3.3	4.9	7.3	8.3	7.3	7.6
VIII	992.9	1007.8	978.6	1012.9	19.9	11.1	27.9	6	5.8	18	13.5	18.4	14.1	15.0	13.9	13.7	14.2	13.9	90	65	88	81	1.7	7.8	2.0	3.8	8.8	8.1	6.5	7.5
IX	997.2	1011.2	979.7	1017.6	18.0	7.9	27.8	3	0.4	24	10.0	17.0	11.2	12.4	11.7	12.3	12.0	12.0	93	63	88	81	0.9	7.6	1.7	3.4	6.6	6.2	3.5	5.4
X	1000.3	1013.1	978.3	1021.0	13.2	5.5	17.9	4	−0.8	23	6.5	12.2	8.5	9.0	9.0	10.1	9.6	9.6	92	72	86	83	0.7	4.3	1.6	2.2	7.6	7.0	4.9	6.5
XI	993.2	1011.6	978.1	1014.3	4.4	0.4	10.6	2	−6.6	24	1.9	3.3	2.5	2.6	6.8	7.1	7.0	7.0	94	89	93	92	0.4	0.9	0.5	0.6	9.1	9.1	8.3	8.8
XII	992.6	1023.3	965.8	1014.2	−1.8	−7.6	11.4	5	−23.5	27	−5.3	−3.5	−4.7	−4.6	4.1	4.5	4.2	4.3	90	85	89	88	0.5	0.7	0.6	0.6	8.1	7.6	5.7	7.1
Rok	994.1	1023.3	965.8	1014.9	11.1	3.4	29.9	27.VI	−23.5	27.XII	5.7	9.7	6.5	7.1	9.0	9.0	9.2	9.1	88	72	86	82	1.3	5.0	1.7	2.7	7.8	7.8	6.2	7.3

Lidzbark Warmiński

$H_s = 90\,m$ $h_w = 13\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%D, %nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min ≤ -10°	Max ≤ 0°	Min < 0°	Max ≥ 25°	Wiatr ≥ 10 m/s	≥ 15 m/s	Opad R ≥ 0.1 mm	≥ 1.0 mm	≥ 10.0 mm	▬	≋	≈
I	6	3.5	3.5	3.4	2	4.5	20	4.3	20.5	4.2	27	4.9	5.5	2.5	1.5	4.7	7	3.8	25.1	14.4	30	6	12	26	·	1	·	2	17	–	4	1	4	9	·
II	3	4.2	·	·	2.5	3.6	18.5	3.5	17.5	5.5	22	3.6	13.5	4.2	6	2.2	1	4.0	38.3	12.1	27	·	2	16	·	1	·	1	16	–	5	3	4	·	·
III	·	·	·	·	0.5	7.0	2.5	4.6	2.5	3.6	4.3	6.5	3.5	8.3	9.5	6.1	·	7.0	38.3	9.1	12	·	·	11	·	14	3	3	10	–	10	·	–	·	·
IV	5.5	4.2	14.5	3.6	14.5	4.1	13.5	4.2	8	5.6	6.5	3.3	13.5	3.9	12	5.2	2	4.1	19.9	9.1	5	·	·	11	·	4	·	11	4	–	4	·	·	·	2
V	12.5	3.1	7	3.4	4.5	4.1	7.5	3.8	8.5	3.3	23.5	4.1	6.5	4.8	22	3.4	1	3.7	82.3	21.7	15	·	·	·	1	·	·	·	11	–	14	2	·	·	6
VI	2	1.5	12.5	2.0	8.5	3.6	11	4.0	6	4.9	17	4.6	18.5	6.0	9.5	3.4	5	3.9	91.9	30.2	8	·	·	·	13	·	·	4	8	–	11	2	1	·	5
VII	4	2.0	3.5	2.7	1.2	2.7	6	2.2	19	4.0	2.6	4.1	13	3.0	6.5	2.3	3	3.2	135.3	24.1	22	·	·	·	5	1	·	1	16	–	20	4	·	·	3
VIII	5.5	1.7	2	2.5	2	3.0	2.5	4.6	14.5	4.4	43.5	5.1	15	3.6	4	2.5	4	4.1	97.8	18.3	22	·	·	·	2	·	·	1	12	–	17	3	1	·	2
IX	6	2.5	9	2.2	6.5	3.3	8	2.8	9	2.6	21.5	4.3	8	3.7	3	2.3	19	2.5	41.7	17.8	14	·	·	·	4	1	·	8	6	–	5	2	3	·	1
X	·	·	1.2	2.3	1.2	4.7	2.1	4.7	1.6	5.1	2.5	3.4	6	2.6	·	·	1	4.0	17.4	6.2	29	·	·	·	·	3	·	5	13	–	6	·	4	·	·
XI	3	3.0	8	4.5	11	5.1	14	3.4	14	3.4	27.5	4.3	4.5	3.7	4	3.2	4	3.8	46.0	9.6	10	·	2	13	·	·	·	1	22	–	10	·	–	·	·
XII	8	5.6	8	3.5	1	1.0	1.7	3.3	1.0	3.6	3.5.5	4.6	6.5	3.5	4	3.4	3	3.9	36.5	15.8	4	11	14	25	·	4	1	4	10	–	6	2	–	17	·
Rok	55.5	2.6	8.0	2.5	7.7	3.9	141.5	3.8	145.5	4.2	3.18	4.4	145.5	4.2	8.2	3.2	5.0	4.0	670.5	30.2	8.VI	17	3.0	102	2.5	2.9	4	41	145	–	112	19	–	2.6	19

Ornota

$H_s = 70\,m$ $h_w = 14\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51.9	20.0	14	·	·	·	4	–	–	5	3	9	5	3	1	·	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.0	8.4	29	·	·	·	·	–	–	4	13	10	7	·	6	·	·
XI	5	2.1	8	2.9	18.5	3.5	15	2.4	11	2.5	20	6.0	7.5	2.4	2	5.2	3	3.4	38.6	6.4	30	·	·	10	·	·	·	1	19	14	11	·	6	·	·
XII	6	6.5	7	3.3	4	2.8	18.5	3.8	10.5	4.1	20	6.8	16	4.5	2	4.0	9	4.3	28.8[2]	10.0	4	11	13	24	·	4	1	3	9	11	7	1	2	10	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kętrzyn

$H_a = 110\,m$ $H_b = 107.4\,m$ $h_w = 11\,m$

I	5.5	3.2	4.5	2.3	·	·	13.5	3.6	20.5	3.5	17.5	4.5	15	2.7	6.5	2.5	10	3.0	18.0	7.2	30	6	12	25	·	·	·	1	18	11	5	·	3	14	·
II	1	3.0	2	2.0	1	3.0	16	3.9	16	3.5	23	2.8	12	2.5	7	2.9	6	2.9	35.7	12.4	28	·	2	18	·	·	·	·	20	9	7	2	10	8	·
III	1	3.0	·	·	·	·	1	6.0	2	2.5	22.5	5.3	4.5	5.3	17.5	5.4	4	5.1	32.9	8.7	12	·	·	12	·	6	·	1	15	16	11	·	3	6	·
IV	4.5	1.4	1.1	3.9	1.1	4.3	19.5	4.6	4.5	3.7	9	3.8	10	3.2	11.5	3.6	9	3.4	14.5	5.2	5	·	·	11	·	1	·	11	8	6	6	·	4	2	3
V	9.5	2.7	1	1.0	5	2.8	10	4.2	6	2.8	13	3.5	17	3.1	17.5	3.6	14	2.8	92.6	19.0	7	·	·	·	·	·	·	1	15	17	13	5	3	·	7
VI	3	1.7	4.5	1.7	8	2.8	12	3.8	3.5	3.9	13.5	3.4	24.5	4.0	9	3.6	12	3.0	87.4	32.5	27	·	·	·	9	·	·	6	7	14	10	2	2	·	5
VII	4	1.0	2	1.0	2	4.8	5.5	4.2	9.5	2.8	34	2.7	18.5	2.7	3.5	3.0	14	2.3	116.3	23.6	18	·	·	·	3	·	·	1	13	21	16	4	3	·	7
VIII	3	1.0	2	1.0	1.5	2.3	2	4.5	8	3.4	24.5	3.3	26.5	3.6	13.5	2.0	12	2.7	84.2	16.2	7	·	·	·	2	·	·	1	12	20	16	3	1	·	4
IX	3	2.5	2	4.5	8.5	3.1	12.5	3.6	3.5	2.7	15.5	3.5	19	3.7	5	3.8	21	2.7	30.2	14.4	14	·	·	·	4	·	·	11	7	7	5	1	4	·	1
X	·	·	1	1.0	8	4.1	3.8	5.9	19	2.8	8	2.9	8.5	3.7	2.5	2.4	8	4.0	23.4	8.2	25	·	·	·	·	1	·	5	11	7	5	·	8	·	·
XI	7.5	2.7	3.5	5.9	6.5	6.2	15	5.7	13.5	2.8	21	4.8	9.5	4.2	4.5	2.0	9	3.9	46.3	8.1	18	·	2	14	·	·	·	1	21	13	10	·	6	3	·
XII	8.5	4.4	7	4.2	1.5	2.0	10	4.6	14	4.5	22.5	3.9	15	5.0	6.5	2.9	8	3.9	27.7	6.4	4	12	16	27	·	2	·	4	9	13	6	·	5	22	·
Rok	50.5	2.2	40.5	2.4	5.3	3.0	155	4.6	120	3.2	224	3.7	220.5	3.6	104.5	3.1	127	3.3	609.2	32.5	27.VI	18	3.2	107	18	10	·	43	156	154	110	17	52	55	27

Suwałki

$H_s = 165\,m$ $H_b = 169.6\,m$ $h_w = 13\,m$

I	8	4.5	3.5	5.4	1.5	3.0	9.5	4.0	17.5	4.8	2.5	4.8	10	4.2	8	4.7	9	4.2	32.4	13.1	30	10	13	30	·	2	·	·	24	17	7	2	8	29	·
II	0.5	4.0	2	2.5	3	4.2	7	4.9	14.5	5.3	2.4	5.1	15	4.5	7	2.2	11	4.0	26.1	11.1	28	1	7	19	·	2	·	1	22	12	5	1	16	13	·
III	1	4.0	·	·	·	·	0.5	10.0	2.5	6.8	29.5	6.2	42.5	6.0	16	7.6	1	6.3	55.9	14.6	12	·	·	13	·	2.0	2	·	16	18	12	1	2	3	·
IV	5.5	4.8	5.5	5.3	1.7	4.5	13	5.8	11.5	4.9	6	4.8	13.5	5.1	11	5.6	7	4.7	20.7	6.4	7	·	·	11	·	9	1	6	6	10	5	·	3	2	1
V	9	4.6	7	2.4	5.5	3.8	8.5	4.6	11.5	4.4	16	3.5	13	3.8	15.5	3.7	7	3.6	89.2	15.3	6	·	·	·	3	2	·	·	14	16	12	3	6	·	3
VI	3	2.5	8.5	2.4	8	4.0	8	5.6	9.5	4.7	13.5	5.0	25.5	5.0	5	4.7	9	4.1	84.7	20.5	12	·	·	·	9	4	·	2	9	13	11	4	·	·	7
VII	2	4.2	1	5.0	4	4.2	3	4.2	13	4.5	33.5	4.4	19.5	4.5	10	2.6	7	3.9	63.8	21.3	30	·	·	·	3	1	·	1	18	18	10	2	5	·	5
VIII	2.5	2.6	3.5	2.1	3	4.5	1.5	6.0	11	5.0	23.5	5.4	33	4.9	12	3.0	3	4.5	69.5	19.3	12	·	·	·	2	6	·	1	15	19	14	2	2	·	6
IX	5	4.0	3	4.0	9	3.3	5	2.6	3	4.7	21	4.9	19.5	3.4	6.5	4.1	18	3.2	48.1	20.7	6	·	·	·	5	4	·	5	7	9	6	2	8	·	2
X	·	·	5	3.2	11.5	4.5	29.5	7.2	21	3.7	12	4.3	10	3.2	1	2.5	3	4.8	6.5	3.1	26	·	·	1	·	9	·	3	13	6	2	·	7	·	·
XI	4.5	5.2	3.5	5.7	12	6.8	11.5	6.9	9.5	5.5	24	4.6	10	4.8	5	4.4	10	4.8	42.7	10.3	30	·	3	16	·	6	·	·	21	13	11	1	9	4	·
XII	7	8.1	6	5.4	2	3.2	8	4.7	15	4.0	27	5.9	11.5	4.7	10.5	4.4	6	4.9	39.5	11.4	2	12	17	27	·	9	·	2	12	13	6	2	5	21	·
Rok	4.9	4.9	4.8.5	3.6	7.6.5	3.8	10.5	5.5	13.9.5	4.9	2.5.5	4.9	2.2.3	4.5	10.7.5	4.1	8.1	4.4	5.8.4.1	2.1.3	3.0.VII	2.3	4.0	11.7	2.2	7.4	3	2.1	1.7.7	1.6.4	1.0.1	2.0	7.1	7.2	2.4

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Sejny

$\varphi = 54°06'$ $\lambda = 23°21'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	+1.2	−7.1	4.0	4	−25.8	25	−4.0	−2.3	−4.2	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.2	7.0	7.9
II	–	–	–	–	2.1	−1.9	7.1	18	−9.4	5	−0.8	1.2	−0.1	0.0	–	–	–	–	–	–	–	–	–	–	–	+	8.6	7.5	7.9	8.0
III	–	–	–	–	7.1	−0.1	14.8	10	−5.7	23	1.9	5.6	2.4	3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.5	6.0	6.8
IV	–	–	–	–	13.0	1.2	23.2	7, 15	−4.4	21	4.6	11.9	6.2	7.2	–	–	–	–	–	–	–	–	–	–	–	–	3.4	4.5	2.7	3.5
V	–	–	–	–	16.5	6.1	25.7	28, 30	−0.1	23	9.8	14.9	10.6	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	6.7	6.8
VI	–	–	–	–	22.6	10.7	30.1	27	5.2	21	16.2	20.9	15.4	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.0	4.8	5.4
VII	–	–	–	–	20.9	10.3	28.9	3	6.4	12	14.5	19.5	14.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	6.2	6.4
VIII	–	–	–	–	20.2	10.3	27.3	6	5.8	18	13.5	18.8	13.7	14.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	6.5	6.6
IX	–	–	–	–	18.4	6.0	28.1	3	−1.8	24	9.5	17.1	10.2	11.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.3	3.6	4.8
X	–	–	–	–	13.5	4.9	17.8	4	−1.2	23	6.5	12.6	8.3	8.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.9	3.8	5.6
XI	–	–	–	–	4.8	0.1	11.0	2	−8.4	29	2.0	3.6	2.2	2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.0	7.2	8.0
XII	–	–	–	–	−1.5	−8.8	11.8	5	−26.1	24	−5.4	−3.3	−5.2	−4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.3	5.3	6.4
Rok	–	–	–	–	11.4	2.6	30.1	27.VII	−26.1	24.XII	5.7	10.1	6.2	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	5.6	6.3

Tczew

$\varphi = 54°05'$ $\lambda = 18°48'$

I	–	–	–	–	1.0	−3.7	5.3	30	−12.4	26	−2.4	0.1	−1.4	−1.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.8	5.2	6.0
II	–	–	–	–	4.6	0.4	15.0	18	−3.2	6	1.5	3.7	2.6	2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	7.6	8.1
III	–	–	–	–	9.5	2.8	18.4	10	−3.5	20	4.3	8.3	5.3	5.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.2	4.1	4.8
IV	–	–	–	–	14.9	3.7	23.8	7	−1.7	11	7.2	13.7	7.6	9.0	–	–	–	–	–	–	–	–	–	–	–	–	4.0	3.4	4.1	3.9
V	–	–	–	–	15.3	6.8	24.6	30	3.2	2	10.3	14.2	9.6	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.9	5.8	6.7
VI	–	–	–	–	23.7	13.4	29.1	27	8.4	1	15.9	22.1	16.9	18.0	–	–	–	–	–	–	–	–	–	–	–	–	3.6	4.3	3.8	3.9
VII	–	–	–	–	20.8	12.1	33.1	3	7.8	6	14.2	19.1	15.2	15.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.7	6.7	7.3
VIII	–	–	–	–	20.2	12.3	28.6	6	9.6	14	13.6	18.8	15.1	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	4.4	6.0
IX	–	–	–	–	20.2	10.1	29.4	2	0.9	25	11.3	19.0	13.5	14.3	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.2	3.5	3.8
X	–	–	–	–	14.9	7.4	18.9	5, 6, 10	3.6	23	8.6	14.3	10.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.0	3.1	4.2
XI	–	–	–	–	6.5	2.8	11.4	3	−5.5	23	3.6	5.6	4.1	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	7.2	7.5
XII	–	–	–	–	0.6	−5.4	13.6	5	−18.6	28	−3.2	−1.2	−2.8	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	5.5	6.1
Rok	–	–	–	–	12.7	5.2	33.1	3.VII	−18.6	28.XII	7.1	11.5	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.1	5.1	5.7

Rosnowo

$\varphi = 54°04'$ $\lambda = 16°18'$

I	–	–	–	–	−1.1	−4.9	6.2	30	−18.7	26	−3.0	0.5	−2.1	−1.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.0	6.1	6.1
II	–	–	–	–	5.2	0.3	13.5	18	−7.8	5	1.4	4.4	2.4	2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.9	8.0
III	–	–	–	–	8.4	2.2	17.5	10	−5.5	20	3.7	7.3	4.7	5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.9	6.4	7.0
IV	–	–	–	–	14.9	3.0	24.8	14	−3.9	10	5.9	13.3	7.0	8.3	–	–	–	–	–	–	–	–	–	–	–	–	3.4	3.7	3.9	3.7
V	–	–	–	–	15.0	5.9	25.0	30	0.5	13	8.5	13.4	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	6.5	6.8
VI	–	–	–	–	22.3	11.7	28.2	2	6.3	22	14.9	20.4	15.5	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.8	4.0	4.7
VII	–	–	–	–	19.5	11.4	32.5	3	4.7	1	13.6	17.8	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	7.0	7.7
VIII	–	–	–	–	19.1	11.2	27.8	31	7.7	14	12.9	17.6	14.2	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.6	5.8	6.7
IX	–	–	–	–	19.7	9.2	28.7	17	2.3	25	10.2	18.5	13.4	13.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.1	3.8	4.2
X	–	–	–	–	14.9	8.3	20.2	10	3.2	14	9.3	14.3	10.8	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.9	4.1	5.7
XI	–	–	–	–	6.8	1.9	11.6	2	−8.2	23	3.5	6.0	3.8	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.5	7.8	8.0
XII	–	–	–	–	0.7	−6.0	13.8	5	−20.2	26	−3.2	−0.9	−3.0	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	5.8	6.3
Rok	–	–	–	–	12.3	4.5	32.5	3. VII	−20.2	26.XII	6.5	11.0	7.5	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	5.8	6.2

Stare Pole

$\varphi = 54°04'$ $\lambda = 19°13'$

I	–	–	–	–	0.5	−5.1	5.8	4	−18.3	26	−3.4	−0.5	−2.4	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	5.5	6.7
II	–	–	–	–	4.0	0.2	12.8	18	−4.3	5	0.9	3.0	2.0	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.5	7.9	8.4
III	–	–	–	–	9.2	1.6	17.7	10	−6.5	20	3.6	7.7	4.8	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.5	4.9	6.1
IV	–	–	–	–	14.6	2.8	23.2	7	−4.0	2	5.7	13.2	7.0	8.2	–	–	–	–	–	–	–	–	–	–	–	–	4.2	3.5	2.7	3.5
V	–	–	–	–	15.2	6.4	25.5	30	1.5	2	9.7	13.7	9.2	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.2	7.5	7.2
VI	–	–	–	–	23.2	12.5	29.3	27	7.0	1	16.2	22.0	16.6	17.8	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.8	5.4	5.0
VII	–	–	–	–	20.2	11.2	31.3	3	6.8	1	14.4	18.6	14.9	15.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	8.0	7.6
VIII	–	–	–	–	19.7	11.5	27.8	6	8.4	14	14.0	18.5	14.2	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	6.6	7.1
IX	–	–	–	–	19.6	9.2	28.3	2	1.9	24	11.2	18.7	12.5	13.7	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.4	3.7	4.1
X	–	–	–	–	14.9	7.4	19.5	4	2.9	23	8.5	14.2	10.5	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.3	4.2	5.9
XI	–	–	–	–	6.1	1.6	10.6	1, 3	−5.9	23	3.2	5.2	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.5	8.3	8.6
XII	–	–	–	–	0.0	−6.7	13.7	5	−20.3	28	−3.6	−1.7	−3.8	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	6.7	6.4	7.2
Rok	–	–	–	–	12.3	4.4	31.3	3. VII	−20.3	28.XII	6.7	11.0	7.4	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	5.9	6.4

Sejny — $H_s = 130$ m — $h_w = 12$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość
I	10	4.6	1.5	3.0	4.5	4.1	11	3.8	20	4.8	14	4.5	11	4.5	15	3.1	6	4.0
II	3	2.0	·	·	1	4.0	9.5	5.4	19	5.0	14	3.7	14	2.9	4.5	2.9	19	3.1
III	·	·	·	·	·	·	2	7.5	7.5	6.0	30	7.5	26	6.1	20.5	6.6	7	6.2
IV	3.5	4.4	7	4.1	13.5	5.1	14	4.6	5	3.8	7.5	3.8	8	6.2	13.5	3.3	18	3.6
V	5	2.2	3.5	3.1	7	3.8	10.5	3.5	11	4.0	8	4.1	8	3.6	23	2.8	17	2.7
VI	2	1.5	4	2.5	10	3.2	8.5	3.2	11	4.6	11	4.8	19.5	4.9	5	2.9	19	3.2
VII	1	2.0	3	2.3	2	4.5	4	4.8	16	4.1	25	4.1	13	4.0	4	2.2	25	2.9
VIII	6.5	2.6	1.5	3.0	1.5	3.0	2	7.0	19	5.8	14	6.5	14.5	4.6	14	3.2	20	3.8
IX	6	3.0	6	3.9	4.5	2.1	1.5	2.0	7	5.2	9	4.9	19	3.6	14	4.2	23	2.9
X	·	·	1	3.0	24	5.6	21.5	6.0	17	2.7	1	6.0	5.5	4.0	1	4.0	22	3.7
XI	5.5	2.7	3.5	5.1	18.5	8.8	4.5	4.2	14	3.0	10.5	4.9	12.5	4.1	7	4.1	14	4.3
XII	12	5.1	0.5	8.1	10	4.2	4	4.1	15	3.7	10.5	6.9	18.5	5.2	7.5	4.8	15	4.1
Rok	54.5	2.5	31.5	3.2	96.5	4.0	93	4.7	161.5	4.4	154.5	5.1	169.5	4.5	129	3.7	205	3.7

MIESIĄC	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	▦	R
I	30.6	8.3	5	9	13	29	·	2	·	2	19	9	7	·	3	—	—
II	22.1	6.1	28	·	6	22	·	1	·	1	17	8	6	·	7	—	—
III	38.6	9.5	12	·	·	13	·	12	1	·	10	15	11	·	3	—	—
IV	20.1	5.5	7	·	·	12	·	2	1	13	4	10	6	·	3	—	—
V	64.5	15.0	1	·	·	1	2	·	·	·	8	12	12	1	1	·	—
VI	90.1	42.5	28	·	·	·	7	3	·	2	3	12	6	3	1	·	—
VII	86.2	22.0	28	·	·	·	3	·	·	3	11	17	13	3	2	·	—
VIII	42.4	7.8	22	·	·	·	2	4	·	2	7	16	11	·	1	·	—
IX	35.0	13.0	14	·	·	3	5	2	·	6	7	8	7	1	13	·	—
X	6.7	2.8	26	·	·	1	·	3	·	5	8	5	2	·	8	·	—
XI	29.4	6.6	8	·	3	17	·	3	·	·	17	12	10	·	4	—	—
XII	38.5	11.3	2	13	16	27	·	5	·	2	10	12	9	2	3	—	—
Rok	504.2	42.5	28.VI	22	38	125	19	37	2	36	121	136	100	10	49	—	—

Tczew — $H_s = 10$ m — $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość
I	0.5	3.0	6.5	2.2	2.5	3.6	8	4.4	24	1.7	22.5	2.4	3	2.3	8	2.5	18	2.0
II	6	1.9	1.5	1.0	·	·	9.5	2.3	27	2.1	16	2.4	12	2.3	6	1.7	6	2.0
III	5	6.6	·		·	·	·	·	1.5	2.7	19	3.9	26	4.7	39.5	6.5	2	5.3
IV	12	3.8	11.5	3.4	7	2.6	18	3.4	9	1.4	7	2.4	3.5	1.4	10	3.0	12	2.5
V	20.5	4.0	8.5	2.2	3.5	6.9	7	2.3	8.5	1.9	13	2.2	6	3.2	16	3.5	10	2.8
VI	3.5	3.1	3.5	2.6	5	1.4	3	3.0	6.5	1.2	19	2.5	16	3.6	11.5	3.0	22	2.0
VII	3	2.0	1	3.0	1	2.0	2.5	4.6	20.5	1.5	27	2.5	14	3.1	6	1.9	18	1.9
VIII	2.5	1.8	1	1.0	0.5	1.0	2.5	1.0	11.5	1.5	28	2.8	21	2.6	12	2.8	14	2.1
IX	3	1.7	5	1.5	4.5	2.2	10.5	2.0	9	1.3	14.5	1.8	8	2.8	6.5	3.7	29	1.4
X	0.5	2.0	·	·	7.5	2.4	20	2.4	29	1.8	10	2.0	6	3.8	4	4.4	16	2.2
XI	6.5	3.5	5.5	3.2	5.5	3.8	10	2.6	9.5	2.0	25.5	2.2	5.5	2.2	3	2.2	19	2.0
XII	2.5	8.0	6.5	6.0	5	2.2	4	1.8	14.5	1.7	29.5	3.4	14	3.3	7	3.1	10	2.9
Rok	65.5	3.9	50.5	2.2	42	2.3	95	2.5	170.5	1.7	231	2.5	135	2.9	129.5	3.2	176	2.4

MIESIĄC	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	▦	R
I	13.0	5.0	30	3	11	19	·	1	·	—	—	9	4	·	5	—	·
II	25.0	7.5	28	·	·	10	·	·	·	—	—	11	6	·	7	—	·
III	12.6	2.7	3	·	·	5	·	10	3	—	—	10	5	·	1	—	·
IV	14.1	7.1	7	·	·	5	·	1	·	—	—	8	4	·	1	·	1
V	68.5	26.3	7	·	·	·	·	3	1	—	—	15	11	2	1	·	6
VI	79.4	25.0	7	·	·	·	13	·	·	—	—	12	9	1	·	·	9
VII	107.5	16.7	13	·	·	·	4	·	·	—	—	24	18	4	2	·	3
VIII	87.5	28.9	10	·	·	·	3	·	·	—	—	19	11	2	3	·	2
IX	27.1	18.4	14	·	·	·	4	·	·	—	—	8	2	1	6	·	·
X	33.0	11.1	18	·	·	·	·	1	·	—	—	11	10	1	5	·	·
XI	39.9	16.1	11	·	·	5	·	·	·	—	—	17	10	1	4	·	·
XII	22.9	5.7	4	11	12	23	·	3	1	—	—	14	9	·	4	11	·
Rok	530.5	28.9	10.VIII	14	23	87	24	19	5	—	—	158	99	12	39	—	21

Rosnowo — $H_s = 62$ m — $h_w = 12$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość
I	·	·	2	1.0	3	2.3	19.5	2.3	17	1.7	14.5	3.6	3	2.7	7	1.9	27	1.7
II		·	·	·	1	1.0	17	2.8	9.5	2.4	11.5	2.7	21.5	3.0	2.5	4.6	21	2.1
III	3	3.0	·	·	·	·	·	·	3.5	4.3	13	4.0	58.5	5.8	7	3.9	8	4.8
IV	3	1.7	6	1.7	24	3.6	8	4.2	6	2.1	4	2.2	8	3.2	5	4.0	26	2.2
V	11.5	3.2	7	1.3	4.5	2.1	5.5	3.0	3	3.3	14	3.0	8	2.8	11.5	3.3	28	2.0
VI	0.5	5.0	·	·	9	2.4	3	3.3	8	1.5	7.5	3.5	28.5	4.1	4.5	3.0	29	2.3
VII	2	1.5	·	·	2	2.0	5	2.2	4.5	2.2	30	2.9	22.5	2.6	6	3.7	21	2.1
VIII	0.5	4.0	1	1.0	1	3.0	1	1.0	6	2.2	21	3.3	19.5	4.2	6	4.8	37	2.2
IX	·	·	·	·	6.5	2.8	12	3.6	1.5	1.3	10.5	3.0	9.5	3.9	3	2.3	47	1.5
X	·	·	·	·	15	4.8	30	3.7	7	2.9	3	4.3	10	3.0	1	3.0	27	2.7
XI	4	1.2	4	4.0	9	4.0	8	2.4	6	3.9	16	4.0	7	4.6	3	2.0	33	2.2
XII	8.5	2.3	4.5	1.9	3	2.7	18	2.2	5	3.2	22	4.0	9	3.2	2	2.0	21	2.2
Rok	33	1.8	24.5	0.9	78	2.6	127	2.6	77	2.6	167	3.4	205	3.6	58.5	3.2	325	2.3

MIESIĄC	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	▦	R
I	38.1	9.9	30	7	10	17	·	·	·	8	14	13	10	·	3	—	—
II	64.2	19.5	28	·	·	10	·	·	·	1	18	15	10	3	7	—	—
III	61.5	13.9	29	·	·	5	·	7	1	2	15	20	15	1	4	—	—
IV	12.4	2.8	5	·	·	8	·	1	·	12	6	9	5	·	3	—	—
V	91.4	10.8	16	·	·	·	·	·	·	4	14	17	13	3	·	·	—
VI	46.2	12.2	15	·	·	·	11	·	·	6	4	12	8	1	1	·	—
VII	200.2	55.2	31	·	·	·	4	·	·	3	17	28	21	4	2	·	—
VIII	123.7	16.7	3	·	·	·	1	1	·	3	12	24	20	4	4	·	—
IX	89.6	44.8	7	·	·	·	3	·	·	12	8	11	11	2	5	·	—
X	34.4	6.0	31	·	·	·	·	1	·	7	12	10	9	·	2	·	—
XI	47.6	12.9	30	·	·	7	·	·	·	2	20	14	11	1	6	—	—
XII	49.9	10.7	2	9	12	22	·	1	·	4	11	13	9	1	5	—	—
Rok	859.2	55.2	31.VII	16	22	69	19	11	1	64	151	186	142	20	42	—	—

Stare Pole — $H_s = 3$ m — $h_w = 11{,}5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość
I	3	2.3	2	2.5	2	1.0	8	2.5	23	2.7	30	3.6	8	3.1	5	4.2	12	2.7
II	2	5.0	2	1.5	·	·	7	3.1	22.5	4.2	19	3.2	18.5	3.8	5	1.8	3	3.4
III	1	9.0	·	·	·	·	·	·	2	3.0	31	5.2	34	7.9	24	9.2	1	7.1
IV	11	5.9	6	2.5	26	3.3	12	3.5	4	2.2	10	2.7	7	4.9	5	5.8	9	3.4
V	23	6.0	4	5.5	4	1.2	7	2.0	7	1.6	13	2.6	8	4.4	14	2.7	13	3.0
VI	7	1.6	7	3.9	13	2.4	1	4.0	5	2.4	19	3.0	21	5.5	9	6.2	8	3.5
VII	5	2.2	5	1.2	5	3.8	·	·	11	1.7	33	3.6	21	4.3	1	2.0	12	2.9
VIII	6	1.5	·	·	3	1.0	5	1.0	8	2.8	26	3.2	33	3.8	3	4.3	9	2.8
IX	1	1.0	2	1.5	22	1.7	3	2.3	13	2.5	12	2.6	20	2.6	2	7.0	15	2.0
X	2	3.0	1	1.0	19	3.0	20	3.8	17	1.8	18	3.6	7	3.6	2	6.5	7	2.9
XI	4	3.2	3	1.3	13	6.3	11	1.8	13	1.7	25	5.0	5	4.0	7	4.1	9	3.5
XII	6	9.5	10	3.8	4	1.0	5	1.4	21	2.0	24	5.0	13	6.5	4	8.8	6	4.1
Rok	71	4.0	42	2.1	111	2.1	79	2.1	151.5	2.4	260	3.6	195.5	4.5	81	5.2	104	3.4

MIESIĄC	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◎	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	▦	R
I	19.2	5.6	11	8	11	21		4	·	3	13	11	5	·	5	6	—
II	37.7	10.8	11	·	·	10	·	2	·	1	19	12	7	1	18	·	—
III	14.9	2.5	21	·	·	7	·	12	4	2	8	13	8	·	—	3	—
IV	15.8	6.2	7	·	·	10	·	6	2	10	1	7	6	·	3	1	—
V	87.1	18.2	7	·	·	·	1	3	·	1	11	17	13	2	3	·	—
VI	71.7	26.3	14	·	·	·	12	7	2	6	6	11	7	3	1	·	—
VII	145.1	21.2	21	·	·	·	3	3	·	3	14	25	21	6	5	·	—
VIII	68.6	10.8	3	·	·	·	2	1	·	1	11	19	17	2	4	·	—
IX	30.2	14.8	14	·	·		4	2	·	13	4	8	4	1	2	·	—
X	24.8	7.8	26	·	·	·	·	6	·	6	10	10	9	·	12	·	—
XI	33.0	7.2	19	·	·	9	·	5	·	1	21	16	10	·	8	·	—
XII	35.9	6.4	4	11	14	24	·	7	3	2	13	13	9	·	3	11	—
Rok	584.0	26.3	14.VI	19	25	81	22	58	11	49	131	162	116	15	—	21	—

Giżycko

$\varphi = 54°03'$ $\lambda = 21°46'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dlse	I	II	III	Dlse	I	II	III	Dlse	I	II	III	Dlse	I	II	III	Dlse
I	–	–	–	–	-0.6	-5.1	5.2	4, 5	-16.3	25	-3.7	-1.9	-2.5	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	75	81	82	79
II	–	–	–	–	2.5	-1.0	9.8	18	-7.8	5	0.0	1.4	0.7	0.7	–	–	–	–	–	–	–	–	–	–	–	–	97	90	80	89
III	–	–	–	–	7.0	0.8	13.4	10	-3.7	20	2.3	5.3	3.4	3.6	–	–	–	–	–	–	–	–	–	–	–	–	88	78	56	74
IV	–	–	–	–	13.1	2.8	23.5	7	-4.5	2	5.1	11.7	7.4	7.9	–	–	–	–	–	–	–	–	–	–	–	–	47	43	32	41
V	–	–	–	–	15.6	7.5	24.9	28	3.3	23	9.5	14.0	10.5	11.1	–	–	–	–	–	–	–	–	–	–	–	–	75	75	75	75
VI	–	–	–	–	22.0	13.0	29.8	27	9.1	22	15.9	20.4	16.4	17.3	–	–	–	–	–	–	–	–	–	–	–	–	57	60	54	57
VII	–	–	–	–	19.9	11.8	28.7	3	9.0	6	14.2	18.2	15.0	15.6	–	–	–	–	–	–	–	–	–	–	–	–	72	76	75	74
VIII	–	–	–	–	18.9	11.8	27.4	6	8.8	18	13.6	17.5	14.2	14.9	–	–	–	–	–	–	–	–	–	–	–	–	75	75	69	73
IX	–	–	–	–	18.0	9.3	26.8	3	4.0	28	11.0	16.9	12.4	13.2	–	–	–	–	–	–	–	–	–	–	–	–	49	51	34	45
X	–	–	–	–	13.2	6.9	18.4	4	1.1	23	7.6	12.6	9.7	9.9	–	–	–	–	–	–	–	–	–	–	–	–	71	62	47	60
XI	–	–	–	–	5.0	1.3	10.7	2	-4.7	24	2.6	4.0	3.2	3.2	–	–	–	–	–	–	–	–	–	–	–	–	93	85	89	89
XII	–	–	–	–	-1.4	-7.1	12.1	5	-22.0	27	-4.9	-2.9	-4.5	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	75	64	53	64
Rok	–	–	–	–	11.1	4.3	29.8	27. VI	-22.0	27. XII	6.1	9.8	7.2	7.6	–	–	–	–	–	–	–	–	–	–	–	–	73	70	62	68

Olecko

$\varphi = 54°03'$ $\lambda = 22°30'$

I	996.3	1019.7	975.3	1019.0	-1.4	-6.3	4.5	4	-18.1	26	-4.4	-2.8	-3.3	-3.4	4.3	4.6	4.6	4.5	92	87	91	90	0.3	0.6	0.4	0.4	9.1	8.7	8.6	8.8
II	998.2	1015.6	972.7	1020.7	1.8	-1.6	8.0	18	-8.9	5	-0.8	0.6	0.2	0.0	5.6	5.9	5.9	5.8	96	92	95	94	0.2	0.5	0.3	0.3	9.8	8.8	8.5	9.0
III	989.4	1009.7	969.2	1011.4	6.7	0.3	14.1	10	-4.4	20, 23	1.9	5.2	2.6	3.1	6.4	6.5	6.3	6.4	91	74	84	83	0.6	2.5	1.2	1.4	9.1	8.3	6.7	8.0
IV	992.1	1005.2	977.3	1013.8	12.7	2.2	22.8	7	-4.7	2	4.7	11.2	7.2	7.6	6.8	6.7	7.3	6.9	77	51	70	66	2.0	7.3	3.3	4.2	5.1	5.4	4.4	5.0
V	989.8	998.4	980.0	1011.2	15.6	6.9	25.2	28	2.0	15	9.5	14.2	10.7	11.3	10.3	9.8	10.6	10.2	85	62	82	76	1.9	7.0	2.6	3.8	7.4	8.1	8.2	7.9
VI	993.0	1003.8	983.1	1014.0	21.9	12.2	29.1	27	7.5	21	15.7	20.1	16.3	17.1	14.3	13.2	13.5	13.7	80	57	74	70	3.8	11.0	5.4	6.7	6.3	6.8	5.6	6.2
VII	990.6	1004.3	977.6	1011.6	19.9	11.3	28.6	3	7.1	6	13.8	18.3	14.9	15.5	14.0	13.3	14.1	13.8	89	64	83	79	1.8	8.2	3.1	4.4	6.7	7.3	7.5	7.2
VIII	992.4	1007.4	978.8	1013.5	19.2	11.1	27.2	6	7.2	18	13.2	17.8	14.0	14.8	13.7	13.7	14.2	13.9	90	68	88	82	1.5	6.9	1.9	3.4	7.7	7.4	7.1	7.4
IX	996.7	1010.4	978.3	1018.1	17.5	8.4	26.6	3	2.3	24, 28	10.1	16.5	11.8	12.6	11.9	12.5	12.4	12.3	94	66	88	83	0.7	6.9	1.8	3.1	6.4	5.8	4.3	5.5
X	999.3	1012.3	976.9	1021.1	12.8	5.9	17.9	4	0.3	23	6.9	11.6	9.0	9.1	9.2	10.1	9.7	9.7	91	75	84	83	0.8	3.8	1.8	2.1	7.7	7.2	5.7	6.9
XI	992.5	1011.2	976.9	1014.6	4.5	0.7	10.7	2	-4.8	24	2.1	3.3	2.6	2.6	6.9	7.1	7.1	7.0	95	89	93	92	0.4	0.9	0.6	0.6	9.6	8.9	9.0	9.2
XII	992.0	1022.3	965.7	1014.7	-2.0	-7.7	11.6	5	-23.3	27	-5.3	-3.6	-5.0	-4.7	4.1	4.5	4.2	4.3	90	86	88	88	0.5	0.7	0.6	0.6	7.9	7.4	6.6	7.3
Rok	993.5	1022.3	965.7	1015.3	10.8	3.6	29.1	27. VI	-23.3	27. XII	5.6	9.4	6.8	7.2	9.0	9.0	9.2	9.1	89	73	85	82	1.2	4.7	1.9	2.6	7.7	7.5	6.8	7.3

Małbark

$\varphi = 54°02'$ $\lambda = 19°02'$

I	–	–	–	–	0.8	-5.2	6.3	4	-17.6	26	-3.0	-0.4	-2.3	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	5.7	6.5
II	–	–	–	–	4.4	0.0	13.9	18	-4.6	5	1.0	3.0	2.2	2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.8	7.6	8.3
III	–	–	–	–	9.4	1.8	18.0	10	-5.1	20	3.7	7.7	5.0	5.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.8	5.1	6.3
IV	–	–	–	–	14.9	3.2	23.0	7, 14	-2.6	2	6.6	13.4	7.7	8.8	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.0	3.3	3.8
V	–	–	–	–	15.4	5.7	25.0	30	0.6	2	9.7	13.8	9.1	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	6.6	6.9
VI	–	–	–	–	23.4	12.6	29.0	27	8.1	21	16.2	21.9	16.8	17.9	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.5	5.3	5.2
VII	–	–	–	–	20.5	11.2	32.5	3	6.7	1	14.5	18.5	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.0	7.7	7.7
VIII	–	–	–	–	21.3	11.5	28.0	6	8.7	31	13.9	18.5	14.3	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	6.2	7.0
IX	–	–	–	–	20.0	9.0	29.2	2	1.0	24, 25, 28	11.3	18.7	12.2	13.6	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.0	3.7	4.3
X	–	–	–	–	15.1	7.2	20.0	4	2.6	23	8.5	14.3	10.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	4.5	6.2
XI	–	–	–	–	6.2	1.6	10.9	1, 2	-6.1	23	3.1	5.1	3.8	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.4	7.6	8.4
XII	–	–	–	–	0.1	-7.1	14.1	5	-23.8	28	-3.7	-1.7	-3.7	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.4	5.5	6.6
Rok	–	–	–	–	12.6	4.3	32.5	3. VII	-23.8	28. XII	6.8	11.1	7.5	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	5.7	6.4

Dziwnów

$\varphi = 54°01'$ $\lambda = 14°44'$

I	1015.8	1042.2	989.1	1016.7	1.6	-3.1	6.4	30	-12.9	27	-1.8	0.6	-0.8	-0.7	5.0	5.3	5.2	5.2	86	79	84	83	0.6	1.2	0.8	0.9	7.3	6.7	6.1	6.7
II	1017.8	1035.4	987.4	1018.7	5.9	0.6	11.7	18	-4.5	5	1.8	4.1	3.0	3.0	6.8	7.6	7.2	7.2	97	92	95	95	0.2	0.8	0.4	0.5	8.9	8.1	7.2	8.1
III	1014.8	1035.0	985.5	1015.6	8.3	3.2	16.9	10	-2.2	21	4.4	6.4	5.4	5.4	7.6	7.7	7.8	7.7	91	81	87	86	0.8	2.0	1.2	1.3	7.9	7.2	6.0	7.0
IV	1011.1	1022.6	999.4	1011.9	12.8	5.0	24.4	14	-1.2	1	7.2	10.9	8.5	8.8	8.5	9.0	9.1	8.9	82	72	82	79	1.9	4.9	2.4	3.1	4.8	4.8	4.9	4.8
V	1011.1	1022.2	996.8	1011.9	13.2	8.3	22.0	26	4.6	2	10.0	11.5	10.4	10.5	10.9	11.2	10.8	11.0	88	83	85	85	1.4	2.6	1.9	2.0	7.1	7.0	7.1	7.1
VI	1013.1	1027.0	1001.8	1013.9	20.0	13.4	27.5	26	10.4	22	15.6	17.8	16.2	16.4	15.1	14.9	15.2	15.1	85	74	83	81	2.8	5.8	3.3	4.0	5.7	5.8	5.3	5.6
VII	1009.9	1025.2	993.8	1010.7	19.3	13.7	30.4	3	10.5	6	15.2	17.6	15.8	16.1	14.8	14.7	14.9	14.8	85	73	83	80	2.6	5.7	3.2	3.8	7.6	7.3	8.0	7.6
VIII	1013.0	1027.0	999.5	1013.8	18.5	13.1	23.9	10	10.7	16	14.8	17.3	15.9	16.0	15.3	15.5	15.4	15.4	91	78	85	85	1.6	4.4	2.7	2.9	7.4	6.8	5.8	6.7
IX	1015.9	1027.7	999.6	1016.7	19.6	12.2	26.8	17	6.5	27	13.2	18.4	15.1	15.4	13.9	14.8	15.0	14.6	90	70	86	82	1.5	6.7	2.5	3.6	4.1	4.1	3.1	3.8
X	1014.7	1028.8	983.7	1015.5	15.0	9.3	21.6	6	6.1	31	10.0	14.2	11.4	11.8	11.4	12.3	12.0	11.9	92	77	89	86	1.0	4.1	1.6	2.2	5.3	6.0	4.4	5.4
XI	1012.1	1035.5	990.3	1012.9	7.2	3.8	12.3	1	-3.4	22	5.0	6.4	5.2	5.4	8.1	8.2	8.0	8.1	91	84	89	88	0.8	1.5	1.0	1.1	8.3	7.9	8.0	8.1
XII	1013.4	1046.2	980.8	1014.3	1.9	-3.8	13.2	5	-18.2	26	-1.8	-0.1	-0.8	-0.9	5.1	5.5	5.3	5.3	87	83	86	85	0.8	1.0	1.0	0.9	7.4	6.3	6.6	6.8
Rok	1013.6	1046.2	980.8	1014.4	11.9	6.3	30.4	3. VII	-18.2	26. XII	7.8	10.4	8.8	9.0	10.2	10.6	10.5	10.4	89	79	86	85	1.3	3.4	1.8	2.2	6.8	6.5	6.0	6.5

Giżycko $H_s = 132$ m $h_w = 12,5$ m 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	v >15	◔	●	Opad R ≥0.1	R ≥1.0	R ≥10.0	≡	⊠	R
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n																	
I	10	4.2	2	4.0	·	·	21	3.9	19	3.8	18	3.9	10	3.5	12	3.2	1	3.7	24.7	10.2	5	6	12	27	·	1	·	2	18	11	5	1	3	10	·
II	1	2.0	1	3.0	1	3.0	21	4.5	14	3.5	16	2.7	16	2.3	6	3.7	8	3.0	25.9	7.2	28	·	1	18	·	·	·	·	21	8	5	·	7	8	·
III	2	4.5	·	·	·	·	2	4.5	5	3.0	27	4.6	33	5.2	22	6.1	2	5.0	30.2	11.0	12	·	·	11	·	4	2	·	15	14	9	1	2	2	·
IV	4	3.0	9	4.1	16	3.5	25	3.4	5	3.2	6	2.8	6	2.7	13	3.9	6	3.2	19.4	4.0	1	·	·	9	·	·	·	12	6	8	7	·	2	2	1
V	6	3.2	5	3.0	5	2.6	12	3.1	13	2.3	12	3.1	9	2.4	25	3.6	6	2.8	70.7	13.0	6	·	·	·	·	·	·	·	15	17	13	1	1	·	4
VI	2	2.0	8	2.1	13	2.2	16	2.9	2	2.5	19	4.3	21	3.0	5	3.2	4	2.9	87.5	24.0	16	·	·	·	5	·	·	4	10	15	13	3	1	·	7
VII	5	1.8	1	1.0	3	4.0	6	4.2	17	2.2	36	3.1	12	2.7	4	2.8	9	2.6	94.3	21.2	16	·	·	·	3	·	·	1	13	18	14	4	·	·	3
VIII	2	1.5	·	·	4	1.5	1	1.0	10	3.9	28	3.6	25	3.8	9	2.3	14	2.9	58.9	10.8	22	·	·	·	2	·	·	1	13	20	15	2	·	·	5
IX	5	2.4	2	1.5	14	2.1	15	2.0	7	2.0	13	4.5	19	3.1	3	1.7	12	2.3	42.9	14.6	14	·	·	·	3	·	·	10	8	11	7	2	3	·	1
X	·	·	·	·	28	5.0	29	4.9	15	3.1	7	3.3	7	3.7	3	4.7	4	4.2	10.1	2.6	29	·	·	·	·	·	·	5	11	6	5	·	7	·	·
XI	9	2.8	3	4.3	9	8.0	19	4.2	11	3.6	18	4.4	11	4.2	4	4.8	6	4.2	38.5	7.0	8, 30	·	·	11	·	1	·	·	23	12	10	·	4	·	·
XII	5	7.2	8	5.1	3	3.0	18	3.9	10	2.7	18	4.3	11	3.7	11	3.7	9	3.6	28.0	7.8	2	12	16	27	·	3	·	3	12	9	6	·	2	20	·
Rok	51	2.9	39	2.3	96	2.9	185	3.5	128	3.0	218	3.7	180	3.4	117	3.6	81	3.4	531.1	24.0	16.VI	18	29	103	13	9	2	38	165	149	109	14	32	42	21

Olecko $H_s = 181$ m $H_b = 177,7$ m $h_w =$ 12 m I–VII, 13 m VIII–XII

I	14.5	3.6	3.5	3.6	11	3.2	8	3.4	10.5	4.0	16.5	4.3	13.5	4.3	15.5	2.7	·	3.6	26.9	11.1	5	11	14	29	·	·	·	·	25	14	6	1	7	30	·
II	1	3.0	3	1.7	7	2.0	10	3.4	15	4.3	5	2.7	24	3.0	19	2.6	·	3.0	25.9	11.2	28	·	8	19	·	·	·	·	22	12	5	1	11	15	·
III	0.5	6.0	·	·	·	·	1	4.0	4	3.9	10	5.0	43	6.2	34.5	5.1	·	5.6	41.3	12.7	12	·	·	12	·	7	1	·	17	21	10	1	2	2	·
IV	9.5	3.2	14	3.1	17	3.2	3	5.0	5	3.1	2.5	3.8	9.5	3.7	29.5	3.1	·	3.3	16.8	5.6	5	·	·	10	·	1	·	7	7	8	5	·	2	2	1
V	8	2.4	1.5	2.7	7.5	2.7	2	3.5	5	4.0	3.5	3.9	12	3.6	53.5	2.6	·	2.9	92.9	21.4	10	·	·	·	1	·	·	·	17	17	13	4	2	·	4
VI	4.5	2.1	11	2.6	8	2.6	4	4.4	3	4.1	7	3.4	24.5	4.1	28	2.7	·	3.2	61.6	15.7	16	·	·	·	4	·	·	2	11	10	8	2	·	·	7
VII	2	2.0	2.5	2.0	1.5	2.0	2.5	4.4	3.5	2.9	16	3.6	38	2.8	27	1.8		2.7	78.3	18.3	30	·	·	·	3	·	·	1	11	18	13	2	1	·	5
VIII	1	2.0	·	·	2	3.0	4	3.2	7.5	3.1	23.5	4.5	33.5	5.4	21.5	3.4		4.3	57.0	10.2	22	·	·	·	2	4	·	1	14	20	11	2	1	·	5
IX	1.5	3.3	6	2.5	9.5	2.5	8.5	3.2	6.5	3.4	17	3.4	25.5	4.0	10.5	3.6	5	3.2	51.5	14.0	14	·	·	·	3	·	·	6	9	9	6	2	3	·	1
X	·	·	0.5	4.0	12.5	3.1	51	4.5	8	3.6	10	3.0	9	4.8	2	2.0	·	4.0	11.7	4.6	26	·	·	·	·	1	·	4	15	12	4	·	18	·	·
XI	0.5	3.0	10	3.1	7	4.4	11	3.7	19	3.3	16.5	3.8	18	4.7	7	4.4	1	3.8	47.5	13.4	10	·	3	15	·	·	·	·	24	17	10	1	12	·	·
XII	8	8.0	7.5	4.9	3.5	3.3	9	4.0	15	3.4	22.5	4.9	14.5	5.5	13	4.6	·	4.8	42.9	12.8	2	12	19	27	·	7	·	1	12	17	7	2	2	19	·
Rok	51	3.2	59.5	2.5	86.5	2.7	114	3.9	102	3.6	150	3.9	265	4.3	261	3.2	6	3.7	554.3	21.4	10.V	23	44	112	13	20	1	22	184	175	98	18	61	68	23

Malbork $H_s = 20$ m $h_w = 11$ m

I	1	1.0	·	·	6	2.2	18	4.4	38	4.9	1	1.0	7	3.8	2	2.5	20	3.4	17.0	8.0	30	8	10	26	·	1	·	1	14	8	3	·	·	—	·
II	2	3.0	·	·	5	3.6	3	4.7	38	4.8	6	3.7	13	3.6	·	·	17	3.4	33.3	15.0	28	·	·	13	·	·	·	1	19	11	6	1	5	—	·
III	·	·	·	·	3	2.3	1	1.0	23	5.0	5	4.4	43	5.3	11	5.5	7	4.7	13.8	4.0	21	·	·	9	·	2	·	1	10	9	6	·	1	—	·
IV	10	3.1	2	4.0	15	4.1	12	6.0	9	4.9	3	2.7	7	4.3	4	4.2	28	3.0	20.5	7.5	7	·	·	7	·	·	·	9	3	7	5	·	·	—	1
V	17	4.4	4	3.2	3	2.3	6	5.8	18	4.7	6	4.2	7	3.9	12	4.2	20	3.4	102.2	25.0	7	·	·	·	·	·	·	1	12	15	13	4	·	·	7
VI	8	2.8	1	1.0	15	3.9	8	4.0	9	4.3	6	4.8	20	4.9	3	4.3	20	3.2	103.0	30.0	5	·	·	·	11	·	·	6	6	9	9	5	·	·	6
VII	4	2.5	·	·	4	2.8	6	4.3	32	4.7	3	5.0	17	5.2	3	2.0	24	3.3	105.5	13.0	9	·	·	·	3	·	·	2	19	23	21	3	·	·	8
VIII	2	2.5	·	·	2	3.0	4	2.8	29	5.0	3	5.0	23	4.1	2	4.0	28	3.0	63.0	14.0	6	·	·	·	1	·	·	1	9	17	16	1	1	·	5
IX	1	1.0	·	·	11	3.5	7	4.6	14	4.6	2	2.0	12	4.6	5	3.8	38	2.4	24.5	15.0	14	·	·	·	4	·	·	12	8	4	4	·	·	·	2
X	·	·	·	·	26	4.5	13	6.0	20	5.2	3	4.0	7	3.6	4	3.5	20	3.8	30.4	7.5	26	·	·	·	·	·	·	6	13	10	7	·	1	·	·
XI	6	3.3	1	1.0	15	5.2	8	4.2	22	5.7	4	5.2	5	4.6	7	5.0	22	3.8	46.5	11.0	19	·	·	8	·	·	·	1	21	18	14	1	4	—	·
XII	7	4.4	2	4.0	3	3.0	12	4.2	30	5.4	2	5.0	13	4.4	5	4.2	19	3.7	32.5	6.0	4	12	14	24	·	·	·	3	11	13	10	·	1	—	
Rok	58	2.3	10	1.1	108	3.4	98	4.3	282	4.9	44	3.9	174	4.4	58	3.6	263	3.4	592.2	30.0	5.VI	20	24	87	19	3	·	44	145	144	114	15	13	—	29

Dziwnów $H_s = 7$ m $H_b = 7,1$ m $h_w = 13$ m

I	0.5	4.0	2.5	2.0	7	2.3	17.5	3.3	35.5	3.1	15.5	4.6	6	2.6	6.5	5.4	2	3.4	22.5	8.9	10	3	9	18	·	1	·	7	15	14	7	·	3	4	·
II	·	·	3.5	6.3	2.5	2.6	11	3.7	26.5	3.7	22	3.4	11.5	4.6	4	5.4	3	3.8	53.3	12.5	28	·	·	8	·	2	·	·	20	13	10	2	11	4	·
III	2.5	12.0	·	·	·	·	·	·	6.5	3.5	26.5	5.4	47	2.4	10.5	9.7	·	7.0	29.8	5.6	22	·	·	3	·	11	4	2	13	13	10	·	8	·	·
IV	1.5	2.0	17	5.6	12	4.2	18.5	3.3	10	2.4	5.5	3.8	6.5	5.5	13	5.0	6	4.0	11.7	2.5	17	·	·	2	·	4	·	5	4	7	6	·	4	·	3
V	13	7.8	15	6.6	2.5	3.4	8.5	3.4	5.5	2.3	9	5.3	15.5	5.8	14	4.8	10	4.9	69.2	16.0	26	·	·	·	·	11	·	2	14	22	13	2	·	·	5
VI	2.5	2.6	14	4.8	4.5	3.2	6.5	2.4	7	3.3	10.5	4.3	30.5	7.1	10.5	5.2	4	4.9	95.6	27.4	9	·	·	·	4	4	1	3	5	11	8	5	2	·	5
VII	0.5	1.0	3	3.0	4	2.5	3.5	3.3	14.5	3.0	29.5	5.0	25	7.4	11	9.0	2	5.5	106.3	29.0	31	·	·	·	3	10	1	2	14	21	13	4	·	·	3
VIII	0.5	3.0	1	4.0	4.5	2.3	4	1.8	15.5	2.7	25.5	5.0	30	7.3	11	5.2	1	4.9	72.1	17.4	19	·	·	·	·	6	1	2	9	18	16	1	·	·	3
IX	·	·	5	3.4	8.5	2.4	20.5	2.6	17	2.7	11	3.8	15.5	6.5	10.5	5.7	2	3.8	32.5	14.9	7	·	·	·	1	5	·	12	5	8	6	2	1	·	3
X	1	4.0	·	·	9.5	4.4	32.5	3.9	30.5	4.0	7.5	4.2	8	5.3	4	4.7	·	4.1	28.9	5.1	20	·	·	·	·	·	·	8	9	10	9	·	1	·	·
XI	6	7.2	9.5	5.9	14	4.4	9	3.3	21.5	4.0	14.5	5.4	7	8.3	6.5	7.2	2	5.1	20.5	7.1	30	·	·	3	·	5	·	2	21	11	6	·	3	·	·
XII	9	10.1	1.5	2.3	8.5	3.7	22.5	3.0	24	3.8	11.5	7.7	12.5	8.5	3.5	6.7	·	5.5	36.2	11.1	11	7	9	19	·	11	·	2	10	13	7	1	1	13	·
Rok	37	4.5	72	4.1	77.5	3.0	164	2.8	214	3.2	188.5	4.8	215	6.4	105	6.2	32	4.7	589.6	29.0	31.VII	10	19	53	8	70	7	47	139	161	111	17	34	21	22

Siejnik — φ = 54°01' — λ = 22°29' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.4	-6.7	3.6	4	-18.2	26	-4.7	-2.3	-3.6	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	7.5	7.9
II	–	–	–	–	2.0	-1.7	8.0	18	-8.7	5	-0.7	1.1	0.4	0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.9	7.9	8.3
III	–	–	–	–	6.7	0.3	13.9	10	-4.8	20	2.2	5.7	2.9	3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.1	5.4	6.8
IV	–	–	–	–	12.9	2.1	23.8	7	-4.9	2	5.1	11.8	6.9	7.7	–	–	–	–	–	–	1	–	–	–	–	–	3.3	4.2	3.0	3.5
V	–	–	–	–	16.0	7.1	25.1	30	2.0	15	10.4	14.7	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	22.4	12.2	29.3	27	7.4	21	16.2	20.9	15.8	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.4	11.0	29.2	3	7.3	6	14.4	18.9	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.1	6.1	6.0
VIII	–	–	–	–	20.2	11.2	28.0	6	7.2	18	13.7	18.7	13.9	15.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	18.2	8.5	27.5	3	2.8	28	10.4	17.2	11.9	12.8	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.1	4.6	4.3
X	–	–	–	–	13.2	5.8	18.1	4	0.6	23	6.8	12.4	8.5	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	4.9	5.9	5.6
XI	–	–	–	–	4.4	0.4	10.9	2	-5.5	24	2.2	3.6	2.6	2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.0	8.7	8.5
XII	–	–	–	–	-2.2	-8.0	11.3	5	-24.0	27	-5.7	-3.5	-5.1	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.2	6.4	6.7
Rok	–	–	–	–	11.1	3.5	29.3	27 VI	-24.0	27 XII	5.9	9.9	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Miastko — φ = 54°00' — λ = 16°58'

I	–	–	–	–	0.2	-5.5	5.1	31	-18.9	26	-3.9	-0.6	-3.0	-2.6	4.2	4.5	4.4	4.4	81	73	81	78	0.8	1.5	0.8	1.0	7.0	6.5	5.8	6.4
II	–	–	–	–	4.1	-0.6	14.2	18	-10.0	5	0.5	3.3	1.6	1.8	5.9	6.6	6.3	6.3	91	84	91	89	0.5	1.2	0.6	0.8	9.2	8.6	8.1	8.6
III	–	–	–	–	8.1	1.8	17.0	10	-7.2	20	3.2	7.0	4.2	4.6	6.8	7.1	7.3	7.1	87	71	87	82	1.1	3.1	1.2	1.8	7.9	6.6	6.5	7.0
IV	–	–	–	–	14.3	3.0	23.9	14	-3.5	2. 10	5.5	13.1	7.6	8.4	6.9	7.3	7.5	7.2	74	49	71	65	2.6	8.8	3.4	4.9	3.6	4.1	4.2	4.0
V	–	–	–	–	14.6	5.6	24.0	30	-0.3	13	8.4	13.2	8.8	9.8	9.7	9.8	9.6	9.7	87	66	84	79	1.4	5.9	1.8	3.0	6.8	7.9	5.3	6.7
VI	–	–	–	–	22.2	11.6	28.1	2	6.0	1	13.5	20.5	16.0	16.5	13.6	13.3	14.3	13.7	85	56	79	73	2.0	11.4	4.1	5.8	4.5	5.4	5.0	5.0
VII	–	–	–	–	19.0	11.2	31.3	3	4.9	1	13.0	17.6	14.3	14.8	13.6	13.7	14.0	13.8	90	70	86	82	1.5	6.6	2.4	3.5	7.4	7.4	6.4	7.1
VIII	–	–	–	–	18.8	11.1	26.2	31	7.7	4	13.0	17.8	13.9	14.6	13.8	14.4	14.1	14.1	92	71	88	84	1.3	6.5	1.9	3.2	6.6	7.1	5.4	6.4
IX	–	–	–	–	19.4	8.4	28.3	2	0.2	24	11.1	18.4	12.3	13.5	12.2	12.8	12.8	12.6	90	61	87	79	1.4	9.0	1.9	4.1	4.7	4.1	4.1	4.3
X	–	–	–	–	14.2	7.7	19.5	11	3.0	31	8.8	13.6	10.2	10.7	10.2	10.6	10.6	10.5	89	69	86	81	1.2	5.1	1.9	2.7	6.2	5.7	5.3	5.7
XI	–	–	–	–	5.8	1.2	10.4	1	-7.8	23	2.8	5.1	3.3	3.6	6.9	7.0	7.0	7.0	98	78	88	85	0.9	2.0	0.9	1.3	8.8	8.1	7.8	8.2
XII	–	–	–	–	-0.7	-2.0	12.0	5	-23.0	17	-4.3	-1.6	-4.0	-3.5	4.4	4.6	4.4	4.5	83	76	83	81	0.7	1.3	0.7	0.9	7.0	6.4	7.1	6.8
Rok	–	–	–	–	11.7	4.0	31.3	3.VII	-23.0	17.XII	6.0	10.6	7.1	7.7	9.0	9.3	9.4	9.2	86	69	84	80	1.3	5.2	1.8	2.8	6.6	6.5	5.9	6.3

Radostowo — φ = 53°59' — λ = 18°45'

I	–	–	–	–	0.3	-5.0	5.6	30	-17.2	26	-3.5	-0.6	-2.7	-2.4	4.4	4.9	4.7	4.7	86	81	87	85	0.6	1.1	0.6	0.8	7.3	7.6	5.9	6.9
II	–	–	–	–	4.0	-0.1	14.3	18	-5.5	5	0.8	3.1	1.9	1.9	5.9	6.6	6.4	6.3	90	85	90	88	0.6	1.2	0.7	0.8	8.5	8.8	7.6	8.3
III	–	–	–	–	9.3	2.1	17.5	10	-4.7	20	3.8	8.1	5.0	5.5	6.8	6.6	6.9	6.8	84	61	78	74	1.4	4.4	1.9	2.6	8.4	7.3	5.5	7.1
IV	–	–	–	–	14.3	2.5	23.0	7	-3.3	12	5.8	12.9	6.9	8.1	7.4	7.3	7.6	7.4	78	48	75	67	2.2	8.4	2.8	4.5	5.1	5.5	3.5	4.7
V	–	–	–	–	15.2	5.5	24.3	30	0.9	23	9.7	13.7	9.0	10.4	10.2	10.1	10.1	10.1	84	65	88	79	2.0	5.9	1.5	3.1	7.6	8.8	7.5	8.0
VI	–	–	–	–	23.2	11.7	29.9	27	6.1	1	16.3	21.7	15.7	17.4	15.1	14.4	15.1	14.9	81	56	84	74	3.6	11.8	2.9	6.1	5.1	6.5	6.5	6.0
VII	–	–	–	–	20.2	10.9	32.4	3	6.4	8	14.5	18.4	14.5	15.5	14.5	14.6	14.8	14.6	88	70	89	82	2.1	7.2	1.8	3.7	8.4	8.5	8.3	8.4
VIII	–	–	–	–	19.7	10.9	28.1	6	7.4	4	13.9	18.5	14.0	15.1	14.2	14.8	14.4	14.5	89	70	89	83	1.7	6.9	1.7	3.4	7.7	8.2	5.9	7.3
IX	–	–	–	–	19.8	8.7	29.0	2	0.6	24	10.7	18.7	12.3	13.5	12.1	13.9	12.7	12.9	91	65	87	81	1.2	8.3	1.9	3.8	4.9	5.7	3.9	4.8
X	–	–	–	–	14.5	6.6	19.7	5	2.2	31	8.0	14.0	9.9	10.4	10.2	11.9	11.0	11.0	95	76	90	87	0.6	4.3	1.3	2.1	7.0	7.6	3.7	6.1
XI	–	–	–	–	5.9	1.7	10.6	1	-5.6	23	3.0	5.1	3.6	3.8	7.2	7.6	7.3	7.4	92	84	90	89	0.6	1.4	0.8	0.9	9.0	8.6	7.7	8.4
XII	–	–	–	–	0.0	-6.9	13.4	5	-22.2	28	-3.9	-1.6	-3.8	-3.3	4.4	4.9	4.4	4.6	84	82	86	84	0.7	1.1	0.8	0.9	8.0	7.7	4.9	6.9
Rok	–	–	–	–	12.2	4.0	32.4	3.VII	-22.2	28.XII	6.6	11.0	7.2	8.0	9.4	9.8	9.6	9.6	87	70	86	81	1.4	5.2	1.6	2.7	7.2	7.6	5.9	6.9

Międzyzdroje — φ = 53°56' — λ = 14°27'

I	–	–	–	–	1.1	-3.6	6.0	30	-13.1	27	-1.9	0.3	-1.4	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.8	6.1	7.5
II	–	–	–	–	6.3	0.6	11.9	18	-4.9	5	2.1	4.6	3.2	3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.8	7.2	8.0
III	–	–	–	–	8.5	2.5	17.5	10	-3.0	20	4.3	7.2	5.3	5.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	14.6	4.6	24.9	14	-1.1	9. 10	7.6	12.5	8.3	9.2	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.4	4.0	4.2
V	–	–	–	–	14.3	6.9	21.9	26	3.2	29	10.0	12.9	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.5	7.4	7.8
VI	–	–	–	–	21.4	12.7	27.9	26	7.8	20	15.9	19.5	15.7	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.5	4.5	5.5
VII	–	–	–	–	20.0	12.4	31.4	2	9.7	1	15.0	18.3	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.3	7.7	7.7
VIII	–	–	–	–	19.1	11.9	26.4	31	8.3	24	14.4	17.9	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.3	7.3	7.0
IX	–	–	–	–	20.1	11.4	27.6	1	4.7	27	13.2	19.1	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	2.9	2.9	3.4
X	–	–	–	–	15.0	8.6	21.6	6	5.2	31	10.1	14.4	11.3	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.7	4.5	5.6
XI	–	–	–	–	6.8	2.9	11.9	1	-4.6	22	4.5	6.0	4.8	5.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1.4	-4.2	13.3	5	-17.6	26	-2.0	0.3	-1.5	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.4	5.6	31.4	2.VII	-17.6	26.XII	7.8	11.1	8.3	8.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Siejnik — $H_s = 170$ m — $h_w = 12$ m — 1961

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD}: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v > 10	v > 15	⊙	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R K
I	4	3.2	4	3.5	·	·	10	2.8	20	3.7	25	3.9	9	4.9	19	4.0	2	3.7	44.4	15.6	5	11	16	29	·	2	·	1	17	18	9	2	6	29	—
II	·	·	·	·	3	1.7	1	3.0	28	5.6	32.5	3.7	14	3.8	2.5	1.8	3	4.1	39.1	13.1	28	·	8	22	·	3	·	1	18	10	7	2	14	13	—
III	0.5	4.0	·	·	·	·	·	·	2.5	4.2	25	4.7	52.5	4.4	7.5	7.3	5	4.4	66.4	16.5	12	·	·	11	·	6	·	3	14	17	13	1	4	·	—
IV	6.5	3.0	6.5	3.1	14.5	3.5	15	3.3	5	1.8	14	2.7	17.5	2.3	5	3.9	6	2.6	27.9	9.9	7	·	·	10	·	2	·	14	6	8	6	·	3	·	—
V	2	3.0	1	2.0	3	3.7	12	4.7	9	4.6	20	3.6	15	3.4	20	3.4	11	3.3	102.1	23.5	10	·	·	·	1	2	·	—	—	17	14	3	1	·	—
VI	1	1.0	7	2.9	6	3.0	9	3.2	9	4.9	27	4.1	16	5.3	·	·	15	3.4	83.0	22.2	16	·	·	·	6	1	·	—	—	12	10	3	·	·	—
VII	4	3.0	·	·	2.5	4.8	1.5	6.0	4	4.0	52	4.1	12	3.4	1	2.0	16	3.2	93.7	22.7	30	·	·	·	3	·	·	3	9	16	13	3	4	·	—
VIII	·	·	·	·	2	3.0	·	·	7	5.4	45.5	5.3	22.5	4.5	5	3.2	11	4.3	63.1	10.7	22	·	·	·	2	4	·	—	—	18	12	2	1	·	—
IX	1	3.0	4	2.8	4	2.8	4	2.8	7	5.6	23	4.2	17	3.9	4	2.0	26	2.7	49.1	13.4	14	·	·	·	5	2	·	8	6	7	6	2	7	·	—
X	·	·	6	2.7	6	5.7	26	7.0	30	3.8	16	3.4	2	3.0	1	5.0	6	4.4	12.7	4.4	26	·	·	·	·	5	·	5	10	9	4	·	12	·	—
XI	4.5	4.6	7	4.4	3	5.3	12	5.5	19	3.6	18	4.5	13	4.9	8.5	3.7	5	4.2	60.1	15.0	10	·	5	15	·	2	1	·	19	14	10	2	13	·	—
XII	4	3.5	4	4.8	1	2.0	8	3.5	19	3.7	26	5.5	14	4.1	14	8.0	3	4.8	51.0	14.0	2	13	17	28	·	4	1	2	15	11	7	2	9	20	—
Rok	27.5	2.4	39.5	2.2	45	3.0	98.5	3.5	159.5	4.2	324	4.1	204.5	4.0	87.5	3.7	109	3.8	692.6	23.5	10.V	24	46	115	17	33	2	—	—	157	111	22	74	62	—

Miastko — $H_s = 145$ m — $h_w = 11$ m

I	·	·	1	1.0	3	1.7	5	1.6	34	2.4	15	2.3	13	1.8	6	2.3	16	1.8	44.2	16.5	30	9	11	23	·	1	·	5	14	16	10	1	—	10	·
II	·	·	·	·	2	2.0	2	2.0	29	2.5	9	2.1	25	2.1	8	2.1	9	2.0	52.2	12.5	28	·	·	13	·	·	·	1	22	16	8	1	—	3	·
III	·	·	·	·	·	·	·	·	2	2.5	10	4.9	52	3.9	25	4.2	4	3.9	68.1	15.6	27	·	·	8	·	4	·	2	11	17	9	2	—	5	
IV	1	2.0	4	2.5	8	1.6	17	2.6	15	2.6	7	2.0	8	2.9	9	2.6	21	1.9	19.0	6.0	17	·	·	8	·	—	·	9	3	8	7	·	—	4	1
V	6	2.3	·	·	2	3.0	1	2.0	12	1.8	8	3.4	32	2.0	18	2.6	14	2.0	68.4	11.5	3	·	·	1	·		·	1	13	15	13	1	—	·	4
VI	·	·	1	2.0	·	·	4	1.2	13	1.8	7	2.7	45	2.4	·	·	20	1.8	71.8	13.9	14	·	·	·	10	·	·	6	5	16	12	3	—	·	5
VII	·	·	·	·	·	·	2	1.0	15	1.6	22	2.5	39	1.9	2	2.5	13	1.8	167.1	41.5	31	·	·	·	4	·	·	2	11	24	17	6	—	·	6
VIII	·	·	·	·	·	·	1	3.0	7	2.4	17	1.7	48	2.4	1	2.0	19	1.8	87.6	11.0	20	·	·	·	2	·	·	1	8	20	17	1	—	·	1
IX	·	·	·	·	2	2.5	6	2.7	8	1.8	8	2.1	36	1.9	·	·	30	1.3	59.3	27.5	7	·	·	·	4	·	·	10	10	10	4	2	—	·	2
X	·	·	·	·	3	2.3	12	2.2	26	2.2	16	1.7	16	1.7	6	2.8	14	1.7	30.0	6.9	17	·	·	·	·	·	·	8	11	10	7	·	—	·	·
XI	1	1.0	3	2.3	3	2.7	5	1.8	11	1.9	16	1.9	22	2.7	10	2.0	19	1.7	33.3	15.3	30	·	·	10	·	·	·	2	20	17	7	1	—	·	·
XII	2	1.5	2	1.5	5	1.8	6	2.0	18	1.9	11	3.4	24	2.5	6	1.8	19	1.8	43.8	9.8	4	10	15	25	·	·	·	3	16	13	9	·	—	16	·
Rok	10	0.6	11	0.8	28	1.5	61	1.8	190	2.1	146	2.6	360	2.4	91	2.1	198	2.0	744.8	41.5	31. VII	19	26	88	20	5	·	50	144	182	120	18	—	38	19

Radostowo — $H_s = 40$ m — $h_w = 15$ m

I	3	3.3	4.5	4.0	3.5	3.4	4	4.2	22.5	4.2	30.5	4.0	6.5	3.7	25	3.4	16	3.3	14.8	5.0	30	8	11	23	·	3	·	2	13	9	5	·	·	12	·
II	3.5	3.7	3.5	4.0	·	·	3.5	5.9	24	4.6	19	3.6	18	3.1	4.5	1.8	8	3.5	31.3	9.4	28	·	·	11	·	2	·	1	19	9	7	·	4	6	·
III	2	4.0	1	6.0	·	·	·	·	1.5	3.0	26.5	5.6	43.5	5.4	17.5	5.2	1	5.3	15.6	2.5	12, 29	·	·	7	·	5	·	·	13	12	7	·	1	3	·
IV	11.5	4.0	14.5	4.9	9	3.8	12.5	5.2	5.5	2.6	7.5	3.2	12.5	2.8	4	3.0	13	3.4	16.1	4.8	7	·	·	10	·	2	·	7	4	11	6	·	·	2	2
V	21.5	4.5	12	2.9	4	3.4	1.5	4.3	7	3.7	17	3.6	10	2.4	9	2.5	11	3.1	62.2	14.8	6	·	·	·	·	·	·	·	17	16	13	3	1	·	3
VI	7	3.7	14	2.0	1.5	3.0	6.5	1.9	6.5	2.2	11	4.5	26.5	3.7	10	2.8	7	2.9	76.5	21.0	14	·	·	·	10	·	·	3	6	10	7	5	·	·	7
VII	8	2.2	3.5	2.1	3.5	4.0	·	·	11	3.1	37	3.4	21.5	2.7	4.5	2.4	4	2.9	101.1	14.1	21	·	·	·	3	1	·	1	22	23	17	3	·	·	6
VIII	7.5	2.9	1.5	1.7	1	2.0	1.5	1.0	8.5	3.8	31	3.8	28.5	3.4	6.5	2.5	7	3.1	83.3	22.5	6	·	·	·	3	·	·	1	10	18	13	2	1	·	3
IX	5	2.2	8	2.7	2.5	2.2	12	2.2	9	3.1	19	4.2	17	3.0	5.5	2.6	12	2.6	25.3	14.0	14	·	·	·	4	2	·	10	8	10	3	1	·	·	·
X	0.5	1.0	4	3.2	5	3.6	20.5	3.4	22	3.8	17	3.2	8	2.8	8	2.2	8	3.0	43.2	20.8	18	·	·	·	·	1	·	7	11	12	9	1	8	·	·
XI	6.5	3.8	10.5	5.2	6	5.3	6.5	3.5	8.5	3.8	29.5	4.1	10.5	3.9	6	2.3	6	3.8	22.9	7.0	19	·	·	8	·	1	·	1	20	15	8	·	5	·	·
XII	6	6.4	8.5	4.4	1.5	1.7	3.5	2.4	17.5	3.5	27.5	5.1	13	4.2	8.5	2.7	7	3.9	25.4	6.0	4	12	13	25	·	4	·	3	11	12	8	·	3	18	·
Rok	82	3.5	85.5	3.6	37.5	2.7	72	2.8	143.5	3.4	272.5	4.0	215.5	3.4	86.5	2.8	100	3.4	522.7	22.5	6.VIII	20	24	84	20	21	·	36	154	157	103	15	23	41	21

Międzyzdroje — $H_s = 10$ m — $h_w = 14$ m

I	3	3.7	·	·	9.5	2.9	40	3.0	19.5	3.0	10	5.2	6.5	3.2	4.5	3.9	·	3.3	29.5	12.5	10	3	8	22	·	1	·		17	8	7	1	—	—	—
II	2.5	1.4	3	2.0	8	2.6	17.5	3.7	23	3.1	8.5	2.1	10.5	3.0	11	2.5	·	2.9	40.6	8.0	10	·	·	6	·	·	·		15	12	10	·	—	—	—
III	4	5.0	·	·	·	·	3	1.7	5.5	3.5	11	4.1	43	6.5	26.5	5.8	·	5.6	22.7	4.2	22	·	·	2	·	5	3	—	—	10	7	·	—	—	—
IV	6.5	2.8	14	2.8	38	3.0	10.5	2.9	5	2.6	1.5	3.0	4.5	4.3	10	2.2	·	2.9	23.7	7.3	2	·	·	3	·	·	·	11	3	7	6	·	·	·	—
V	19	3.3	18	3.1	4.5	2.1	12.5	2.9	4.5	1.8	7.	2.3	10	3.9	17.5	3.2	·	3.1	76.8	12.0	26	·	·	·	·	·	·	·	19	19	15	3	—	·	—
VI	8	3.8	11	2.4	11	2.5	4.5	2.3	2.5	2.6	3	4.3	20.5	4.6	21.5	4.1	8	3.3	70.6	24.2	9	·	·	·	5	·	·	4	8	9	8	2	—	·	—
VII	7.5	3.1	5	1.4	7	2.0	2	2.5	11	2.1	8.5	2.5	31	3.6	18	4.6	3	3.1	63.3	18.6	31	·	·	·	4	1	·	2	18	16	13	2	—	·	—
VIII	6	2.4	·	·	10	2.6	5	2.2	11.5	2.9	8.5	3.9	29	2.8	20	2.8	3	2.8	75.7	14.3	3	·	·	·	1	·	·	4	14	18	18	1	1	·	—
IX	6	1.3	9.5	1.8	21.5	2.7	9.5	2.5	11.5	2.6	4.5	2.3	7.5	3.0	13	4.5	7	2.5	21.8	9.9	15	·	·	·	2	·	·	15	5	7	6	·	·	·	—
X	·	·	0.5	3.0	28	3.3	41.5	3.4	4.5	3.7	3.5	4.7	5.5	5.0	9.5	4.7	·	3.6	25.0	5.5	24	·	·	·	·	·	·	8	10	11	6	·	1	·	—
XI	7.5	3.7	15	2.9	27	2.8	11.5	2.6	7	4.0	12.5	4.5	3	6.0	5.5	7.0	1	3.5	15.2	8.4	30	·	·	3	·	·	·	—	—	5	3	·	4	—	—
XII	9	6.8	3	3.7	15	1.9	20	3.4	13.5	3.5	13.5	4.2	15	4.8	4	6.0	·	3.8	23.3	7.0	5	8	11	20	·	·	·	—	—	8	6	·	2	—	—
Rok	79	3.8	79	1.9	179.5	2.4	177.5	2.8	119	3.0	92	3.6	186	4.2	161	4.3	22	3.4	488.2	24.2	9 VI	11	19	56	12	7	3	—	—	130	105	9	—	—	—

Świnoujście

$\varphi = 53°55'$ $\lambda = 14°14'$ **1961**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnie																	
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.2	-3.1	6.6	30	-13.8	27	-1.8	0.3	-0.8	-0.8	4.8	5.1	5.0	5.0	84	77	81	81	0.8	1.3	1.0	1.0	6.5	6.3	5.4	6.1
II	–	–	–	–	6.3	0.8	12.8	27	-3.5	6	1.9	4.5	3.3	3.2	6.6	7.4	7.1	7.0	93	87	91	90	0.5	1.2	0.7	0.8	8.1	7.9	6.9	7.6
III	–	–	–	–	9.7	3.1	17.1	10	-2.4	20	4.3	8.1	5.9	6.0	7.3	7.4	7.5	7.4	86	68	80	78	1.2	3.7	1.9	2.3	7.1	7.2	5.8	6.7
IV	–	–	–	–	13.3	5.2	25.0	14	-0.6	1, 11	7.3	11.2	8.9	9.1	8.0	8.1	8.3	8.1	76	63	73	71	2.5	6.1	3.5	4.0	4.6	5.1	4.4	4.7
V	–	–	–	–	13.4	7.5	21.8	26	3.6	29	9.7	11.6	9.9	10.3	10.4	10.5	10.3	10.4	86	77	84	82	1.7	3.4	2.0	2.4	7.4	7.5	6.1	7.0
VI	–	–	–	–	20.6	12.5	28.2	26	8.7	20	15.2	18.5	16.1	16.5	14.2	13.5	14.2	14.0	82	65	78	75	3.2	8.2	4.3	5.2	5.1	6.0	5.0	5.3
VII	–	–	–	–	19.8	12.7	30.9	3	10.4	6	14.8	17.3	15.3	15.7	14.3	14.2	14.4	14.3	85	72	83	80	2.7	6.9	3.1	3.9	7.0	8.0	7.1	7.3
VIII	–	–	–	–	19.6	12.1	24.1	9	9.5	8	14.0	17.6	14.8	15.3	14.5	14.5	14.5	14.5	90	73	86	83	1.6	5.8	2.4	3.3	7.0	7.3	5.3	6.5
IX	–	–	–	–	19.5	11.8	27.8	1, 17	4.7	27	12.9	18.4	14.9	15.3	13.5	13.9	14.2	13.9	89	65	83	79	1.7	7.6	2.7	4.0	4.9	4.3	3.1	4.1
X	–	–	–	–	15.0	8.9	20.6	6	5.4	31	9.8	14.0	11.3	11.6	10.5	11.0	11.3	10.9	87	70	84	80	1.6	5.3	2.3	3.1	6.1	6.5	5.0	5.9
XI	–	–	–	–	7.0	3.4	12.2	1	-3.5	22	4.7	6.2	4.9	5.2	7.8	7.9	7.7	7.8	90	82	87	86	0.9	1.8	1.1	1.3	8.0	7.7	6.9	7.5
XII	–	–	–	–	1.6	-4.0	13.4	5	-17.5	26	-2.1	0.0	-1.0	-1.0	4.8	5.2	5.0	5.0	84	79	83	82	0.9	1.3	1.1	1.1	6.5	6.3	7.1	6.6
Rok	–	–	–	–	12.2	5.9	30.9	3. VII	-17.5	26. XII	7.6	10.6	8.6	8.8	9.7	9.9	10.0	9.9	86	73	83	81	1.6	4.3	2.2	2.7	6.5	6.7	5.7	6.3

Gryfice

$\varphi = 53°55'$ $\lambda = 15°13'$

I	–	–	–	–	0.6	-4.1	5.9	29	-14.8	27	-2.8	0.1	-2.0	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.3	5.8	6.4
II	–	–	–	–	5.8	0.3	11.7	18	-4.7	5	1.7	4.5	2.5	2.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.8	7.6	8.1
III	–	–	–	–	9.0	2.6	17.1	10	-3.9	20	3.8	7.9	5.1	5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.5	6.5	7.1
IV	–	–	–	–	14.8	3.8	25.4	14	-1.9	10	6.4	13.3	7.4	8.6	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.8	5.4	4.7
V	–	–	–	–	14.9	6.6	23.0	30	2.4	13	9.2	13.4	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.6	6.9
VI	–	–	–	–	22.7	11.6	28.8	2	7.0	22	15.7	21.1	15.5	17.0	–	–	–	–	–	–	–	–	–	–	–	–	4.0	5.3	5.4	4.9
VII	–	–	–	–	20.3	11.8	32.4	3	7.4	1	14.5	18.6	14.5	15.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.8	8.0	7.8
VIII	–	–	–	–	19.5	11.5	26.6	31	8.6	8	13.7	18.1	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	4.9	6.5
IX	–	–	–	–	20.0	9.8	27.4	1	3.0	24	11.2	19.4	13.2	14.2	–	–	–	–	–	–	–	–	–	–	–	–	4.0	3.6	3.1	3.6
X	–	–	–	–	14.8	7.7	20.6	6	3.1	31	9.1	14.2	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.9	4.5	5.4
XI	–	–	–	–	6.5	2.1	11.4	1	-5.8	23	3.5	6.0	3.8	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.2	7.2	7.9
XII	–	–	–	–	0.5	-5.5	13.8	5	-19.6	26	-3.0	-1.0	-2.7	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.0	7.5	6.6
Rok	–	–	–	–	12.4	4.8	32.4	3. VII	-19.6	26. XII	6.9	11.3	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.3	6.0	6.3

Wirty

$\varphi = 53°54'$ $\lambda = 18°23'$

I	–	–	–	–	-0.2	-4.7	4.7	30, 31	-17.8	26	-3.8	-0.7	-2.1	-2.2	4.4	5.1	4.8	4.8	88	85	88	87	0.5	0.9	0.6	0.6	7.3	6.5	6.5	6.8
II	–	–	–	–	3.8	-0.2	15.3	18	-2.6	5	0.7	3.1	1.6	1.8	6.0	6.8	6.3	6.4	92	88	92	91	0.5	1.0	0.6	0.7	9.1	8.0	9.0	8.7
III	–	–	–	–	8.9	2.2	18.3	10	-5.8	20	3.6	7.6	4.9	5.2	7.1	7.4	7.6	7.4	88	71	87	82	1.0	3.4	1.2	1.9	7.2	5.5	4.7	5.8
IV	–	–	–	–	13.9	2.7	23.3	14	-3.5	12	6.2	12.8	8.4	9.0	–	–	–	–	–	–	–	–	–	–	–	–	3.6	3.4	2.6	3.2
V	–	–	–	–	15.5	5.2	24.3	30	-0.4	1, 2	9.4	14.0	9.9	10.8	10.2	11.2	10.7	10.7	86	71	87	81	1.7	5.1	1.8	2.9	7.5	8.2	6.7	7.5
VI	–	–	–	–	23.3	12.0	28.4	27	6.3	22	15.9	21.8	16.8	17.8	14.8	14.4	14.7	14.6	81	56	77	71	3.6	12.2	4.6	6.8	4.0	3.7	3.4	3.7
VII	–	–	–	–	20.2	11.1	31.9	3	5.8	1	14.0	18.7	15.0	15.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.3	8.5	8.0
VIII	–	–	–	–	19.8	10.7	27.5	6	7.3	5^2	13.7	18.0	14.5	15.2	14.2	14.9	14.6	14.6	91	73	88	84	1.5	6.0	2.0	3.2	6.8	7.2	4.8	6.3
IX	–	–	–	–	19.3	8.4	28.4	2, 17	1.1	25.27.28	10.5	18.3	12.7	13.6	12.1	13.3	13.7	13.0	92	63	91	82	1.1	8.4	1.5	3.7	3.2	3.2	2.9	3.1
X	–	–	–	–	14.7	6.5	18.8	12	4.2	1, 23	8.8	14.0	9.9	10.6	10.6	12.2	11.1	11.3	93	77	91	87	0.8	4.0	1.2	2.0	6.1	4.8	2.6	4.5
XI	–	–	–	–	5.8	0.7	9.8	1, 2	-7.1	23	2.6	5.3	3.2	3.6	7.1	7.7	7.1	7.3	93	86	91	90	0.5	1.3	0.6	0.8	8.8	8.0	6.6	7.8
XII	–	–	–	–	-0.7	-6.6	12.8	5	-20.6	17	-4.6	-2.0	-3.6	-3.4	4.3	5.0	4.6	4.6	89	86	89	88	0.5	0.8	0.5	0.6	6.7	5.9	4.4	5.7
Rok	–	–	–	–	12.0	4.0	31.9	3. VII	-20.6	17. XII	6.4	10.9	7.6	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	5.2	5.9

Jazy

$\varphi = 53°53'$ $\lambda = 23°22'$

I	–	–	–	–	-1.1	-6.7	5.3	4	-23.0	25	-4.6	-2.3	-3.9	-3.7	4.2	4.7	4.5	4.5	89	86	89	86	0.4	0.7	0.4	0.5	8.3	8.5	7.7	8.1
II	–	–	–	–	2.5	-2.0	8.0	18	-7.9	5	-0.7	1.6	0.1	0.3	5.6	6.0	5.8	5.8	95	86	93	91	0.3	1.0	0.4	0.6	9.2	8.2	8.1	8.5
III	–	–	–	–	7.3	-0.2	16.0	10	-6.8	23	2.1	5.9	2.8	3.4	6.2	6.5	6.3	6.3	86	70	84	80	1.0	3.1	1.2	1.8	8.7	7.3	6.0	7.3
IV	–	–	–	–	13.4	0.4	23.9	7	-5.4	21	4.9	12.3	5.7	7.2	6.8	6.6	7.0	6.8	77	47	74	66	2.1	8.8	2.7	4.5	4.0	4.6	3.7	4.1
V	–	–	–	–	16.7	5.6	26.8	30	-1.1	23	10.1	15.3	9.8	11.2	10.6	9.9	10.4	10.3	86	58	86	77	2.1	8.4	2.0	4.1	7.0	7.0	7.0	7.0
VI	–	–	–	–	22.8	10.6	31.6	27	4.6	21	16.9	20.9	15.8	17.4	14.6	12.9	13.6	13.7	77	55	77	70	4.9	12.6	4.8	7.4	6.3	6.8	6.0	6.4
VII	–	–	–	–	21.1	10.6	29.4	3	5.8	12	14.7	19.5	15.0	16.0	14.0	13.3	14.0	13.8	94	60	82	75	2.9	9.8	3.3	5.3	6.7	6.7	6.9	6.8
VIII	–	–	–	–	20.2	10.9	28.7	6	6.1	18	14.0	18.8	14.0	15.2	13.9	13.5	14.1	13.8	87	63	88	79	2.1	8.6	2.1	4.3	7.7	6.8	6.7	7.1
IX	–	–	–	–	18.4	6.7	28.9	3	-1.9	23, 24	9.4	17.4	10.6	12.0	11.6	12.2	11.7	11.8	94	62	90	82	0.8	8.4	1.5	3.6	6.0	5.5	3.7	5.1
X	–	–	–	–	13.7	4.9	17.8	4	-1.5	23	6.2	13.0	8.9	9.2	8.8	9.9	9.4	9.4	92	67	83	81	0.8	5.2	2.1	2.7	6.6	6.0	5.3	6.0
XI	–	–	–	–	4.4	-0.3	10.8	2	-8.5	29	1.6	3.3	1.7	2.1	6.6	7.2	6.6	6.8	93	90	97	97	0.5	0.8	0.6	0.6	8.7	8.7	8.5	8.6
XII	–	–	–	–	-1.5	-8.2	12.5	5	-28.0	27	-5.7	-3.2	-5.1	-4.8	4.3	4.7	4.3	4.3	90	85	88	88	0.4	0.6	0.5	0.5	8.1	7.2	5.6	7.0
Rok	–	–	–	–	11.5	2.7	31.6	27. VI	-28.0	27. XII	5.7	10.2	6.3	7.1	8.9	9.0	9.0	9.0	89	69	86	81	1.5	5.7	1.8	3.8	7.3	6.9	6.3	6.8

Świnoujście $H_s = 6\,m$ $h_w = 20\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (nD, vmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	v>15	◉	●	Opad R ≥0.1	R≥1.0	R≥10.0	═	⊞	R/⊡
I	2	3.0	1	3.0	7	3.9	26.5	4.0	23.5	3.6	17.5	4.1	9	3.3	5.5	4.5	1	3.8	24.2	10.5	10	2	10	19	·	2	·	9	16	14	6	1	5	7	·
II	·	·	6	3.0	4	1.9	8.5	4.8	16.5	4.1	23.5	2.7	19	3.4	6.5	3.8	·	3.4	48.6	10.5	28	·	·	7	·	2	·	·	17	15	9	1	13	1	·
III	2.5	1.5	·	·	·	·	·	·	1	2.0	25.5	4.4	51.5	5.3	12.5	6.9	·	5.5	34.3	6.2	29	·	·	4	·	10	3	3	11	14	10	·	4	2	·
IV	8	2.8	20	5.0	10.5	4.1	21	4.1	4.5	2.8	9	2.6	8.5	3.4	8.5	4.1	·	3.9	32.7	12.6	28	·	·	2	·	5	3	6	5	8	5	1	3	·	2
V	18.5	5.4	16	5.2	4.5	3.0	7.5	3.3	25	3.4	13	3.0	18	3.6	12	6.0	1	4.3	76.4	15.4	7	·	·	·	·	8	·	·	14	20	17	3	1	·	5
VI	9	4.7	10	2.5	6	2.8	6	2.4	5	1.6	13	3.4	28	4.4	12	4.0	1	3.6	45.2	11.2	27	·	·	·	3	·	·	3	4	11	10	1	2	·	5
VII	1	2.0	3	3.7	3	1.3	1.5	4.3	5	2.8	33	3.5	34.5	3.6	11	4.9	1	3.5	75.3	21.1	11	·	·	·	3	1	·	2	13	24	13	2	·	·	3
VIII	3.5	1.4	3.5	1.9	3	1.8	4.5	2.7	5.5	3.0	27.5	3.1	32.5	3.6	11	3.3	2	3.0	74.6	14.3	3	·	·	·	·	·	·	3	9	23	18	1	1	·	4
IX	2	2.0	9	2.6	6.5	4.2	16.5	3.2	11	3.0	16	3.0	16.5	3.7	10.5	3.7	2	3.2	34.4	11.3	14	·	·	·	3	·	·	12	6	9	7	1	1	·	2
X	1.5	6.3	0.5	3.0	8	5.1	27	4.7	23.5	3.2	22.5	3.0	7	2.4	3	4.3	·	3.8	36.7	10.9	20	·	·	·	·	·	·	6	10	11	7	1	4	·	·
XI	3	4.3	14.5	6.4	7.5	4.7	7.5	3.1	10.5	3.0	28.5	3.8	13.5	3.8	5	5.2	·	4.2	25.0	8.8	30	·	·	4	·	3	2	2	17	9	6	·	4	·	·
XII	9	2.4	1.5	5.3	7	4.2	18	3.7	17.5	3.6	26	4.6	12	4.5	2	5.0	·	4.5	46.2	10.3	11	7	10	19	·	2	·	2	13	13	8	1	7	15	·
Rok	60	3.4	85	3.5	67	3.1	144.5	3.4	126	3.0	255	3.4	250	3.8	99.5	4.6	8	3.9	553.6	21.1	11.VII	9	20	55	9	33	8	48	135	171	116	13	45	25	21

Gryfice $H_s = 40\,m$ $h_w = 14\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R/⊡
I	·	·	·	·	5	1.6	2	2.0	12.5	2.1	13.5	2.7	10.5	2.9	3.5	3.4	46	1.3	40.5	6.8	30	4	11	23	·	-	·	8	17	16	11	·	5	2	·
II	3	6.6	1	3.0	1	1.0	1	3.0	6	1.5	12.5	1.9	25	1.8	3.5	1.6	31	1.3	59.5	13.3	28	·	·	10	·	1	·	1	19	13	12	3	11	1	·
III	3	5.5	·	·	·	·	·	·	2	2.2	8.5	3.8	60.5	8.1	10	6.0	9	6.5	52.5	9.2	29	·	·	4	·	13	5	1	13	16	12	·	5	1	·
IV	6.5	2.3	7	2.2	14.5	2.3	2.5	1.4	3	2.0	5.5	1.8	10	2.8	5	3.5	36	1.4	22.6	7.5	28	·	·	7	1	1	·	8	7	8	8	·	2	·	2
V	13.5	3.7	7.5	5.6	2	2.0	·	·	3	2.7	10	2.0	19.5	5.3	7.5	3.0	30	2.7	85.7	15.1	3	·	·	·	·	4	·	4	15	19	16	3	1	·	3
VI	5	2.8	2	1.0	6	1.7	1	1.0	2	2.0	4.5	2.0	32.5	4.8	9	2.7	28	2.5	66.6	24.6	14	·	·	·	8	2	·	6	4	11	9	2	1	·	5
VII	0.5	2.0	·	·	2	2.5	·	·	1	1.5	11	2.5	37	4.3	13.5	3.6	28	2.6	161.3	68.0	31	·	·	·	4	2	1	2	18	23	14	5	2	·	4
VIII	·	·	1	5.0	1	1.0	·	·	2	2.0	10	1.9	33.5	4.0	25	5.0	43	1.8	88.4	16.0	22	·	·	·	1	2	·	4	9	21	18	1	3	·	3
IX	1	2.0	·	·	5	1.2	5	1.6	2	1.5	6	1.5	21.5	4.0	3.5	1.6	46	1.3	55.7	25.2	7	·	·	·	4	·	·	14	6	9	8	2	6	·	1
X	1	2.0	0.5	2.0	14.5	2.7	·	·	9.5	2.4	18.5	2.5	15	4.9	4	3.6	30	2.2	40.0	8.0	26	·	·	·	·	2	·	7	10	11	8	·	3	·	·
XI	1.5	4.0	6.5	3.2	12	5.9	0.5	4.0	2.5	1.8	15	2.9	21	5.0	3	2.8	28	2.9	28.1	10.0	30	·	·	6	·	5	·	3	20	12	7	1	9	·	·
XII	6	5.7	1	2.0	5	3.2	·	·	11.5	1.8	14	3.8	15.5	6.4	1	3.0	39	2.4	49.5	9.6	4, 11	8	12	24	·	3		4	15	13	11	·	4	15	·
Rok	41	3.0	26.5	2.0	68	2.1	12	1.1	57	2.0	129	2.4	301.5	4.5	66	3.3	394	2.4	750.4	68.0	31.VII	12	23	74	18	35	6	62	153	172	134	17	52	19	18

Wirty $H_s = 121\,m$ $h_w = 13\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R/⊡
I	·	·	7	1.6	2	1.0	14	1.1	6	1.2	29	1.7	7	1.1	1	3.0	27	1.0	29.4	13.6	11	6	12	23	·	·	·	—	—	6	4	1	5	4^2	·
II	1	1.0	1	1.0	·	·	8	1.0	9	1.2	29	1.3	16	2.0	1	1.0	19	1.1	38.8	14.8	9	·	1	13	·	·	·	—	—	12	5	1	14	4^2	·
III	·	·	·	·	·	·	·	·	4	4.0	33	3.1	42	3.4	10	5.1	4	3.3	36.8	10.2	20	·	·	7	·	3	·	—	—	13	10	1	3	1^2	·
IV	·	·	8	1.9	4	2.0	19	1.7	8	3.0	16	2.2	9	1.9	13	2.3	13	1.8	24.8	20	2	·	·	7	·	-	·	—	—	7	7	·	1	3^2	2
V	9	1.6	11	1.0	2	1.0	12	1.3	2	1.5	17	1.5	9	1.7	7	1.7	24	1.1	64.9	13.6	6	·	·	2	·	·	·	—	—	14	10	3	2	·	3
VI	·	·	4	1.5	4	1.5	7	2.1	1	1.0	21	3.0	22	2.3	3	4.0	28	1.7	63.3	25.2	10	·	·	·	13	·	·	—	—	7	6	1	·	·	6
VII	1	1.0	1	1.0	1	2.0	1	1.0	5	1.0	44	1.7	25	2.0	2	1.5	13	1.5	119.1	17.2	13	·	·	·	4	·	·	—	—	17	16	5	2	·	5
VIII	1	1.0	1	1.0	1	1.0	1	1.0	2	1.0	34	1.7	28	2.1	1	1.0	24	1.3	93.1	26.1	6	·	·	·	1	·	·	—	—	20	15	2	5	·	3
IX	·	·	·	·	2	1.0	13	1.1	7	1.0	21	1.2	10	2.0	1	1.0	36	0.8	35.3	16.8	14	·	·	·	4	·	·	—	—	9	6	1	12	·	1
X	·	·	·	·	7	1.1	34	1.4	5	1.0	12	1.0	4	1.0	·	·	31	0.8	35.5	19.4	18	·	·	·	·	·	·	—	—	12	6	1	17	·	·
XI	·	·	5	1.0	8	1.6	8	1.2	2	1.0	19	1.2	11	1.1	3	1.7	34	0.8	28.7	14.4	11	·	·	10	·	·	·	—	—	11	5	1	14	1	·
XII	·	·	7	1.6	4	1.0	6	1.3	3	1.0	24	2.0	7	1.3	11	1.8	31	1.1	35.2	10.6	4	11	16	26	·	·	·	—	—	11	7	1	9	18	·
Rok	12	0.4	45	1.0	35	1.1	123	1.2	54	1.5	299	1.8	190	1.8	53	2.0	284	1.4	604.9	26.1	6.VIII	17	29	88	22	3	·	—	—	139	97	18	84	31^2	20

Jazy $H_s = 120\,m$ $h_w = 15\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R/⊡
I	11.5	3.4	1.5	3.3	0.5	4.0	15	2.5	15	2.5	19.5	3.2	7	2.8	10	2.4	13	2.4	38.3	8.2	30	10	13	28	·	·	·	1	19	13	10	·	3	—	—
II	2	1.5	1	2.0	1.5	1.3	12.5	2.0	15	3.0	14	2.1	14	2.3	8	2.2	16	1.9	33.4	12.8	28	·	4	21	·	·	·	1	22	9	6	1	8	—	—
III	·	·	·	·	·	·	1.5	4.3	6.5	2.8	28.5	3.5	37.5	3.3	16	5.7	3	3.6	45.6	11.2	12	·	·	15	·	1	1	·	15	17	11	1	1	—	—
IV	7	3.2	6	2.3	8	2.4	11.5	2.8	7	3.1	8	2.8	8	3.0	11.5	3.7	23	2.2	26.9	9.2	5	·	·	14	·	1	·	11	6	8	6	·	2	—	—
V	7	3.7	2.5	1.8	8	2.3	7.5	3.3	6.5	2.8	7	2.3	13	2.7	15.5	2.4	26	1.9	57.2	17.0	4	·	·	1	3	·	·	·	11	12	9	2	4	·	—
VI	3	2.8	3.5	2.1	4.5	2.8	10.5	2.2	14.5	2.2	16	2.2	23.5	2.9	6.5	2.5	8	2.3	98.2	24.3	27	·	·	·	13	·	·	2	12	13	11	4	8	·	—
VII	1.5	2.0	1	2.5	3	2.7	7	2.4	14	2.4	27	2.7	24.5	2.4	3	2.7	12	2.2	71.8	16.4	28	·	·	·	3	·	·	2	11	15	10	3	·	·	—
VIII	2.5	2.2	1.5	1.0	·	·	3.5	2.6	9.5	2.6	22	3.1	23	2.8	14	2.4	17	2.2	35.6	7.7	11	·	·	·	2	·	·	·	11	16	10	·	1	·	—
IX	4	2.6	1.5	1.0	3.5	2.1	4	1.8	7.5	2.5	15.5	2.5	20	2.9	6	3.0	28	1.8	36.6	13.5	14	·	·	4	5	·	·	7	7	7	7	1	12	·	—
X	·	·	4	2.2	19	3.4	26	3.4	12.5	2.8	3.5	3.1	8	2.1	1	2.5	19	2.4	9.4	4.2	26	·	·	2	·	·	·	4	11	4	2	·	8	·	—
XI	6	3.3	11.5	3.6	14.5	3.8	6.5	2.5	6.5	2.1	20.5	2.5	7.5	3.1	2	1.8	15	2.5	64.0	22.5	10	·	5	17	·	·	·	·	20	14	11	1	5	—	—
XII	11	4.4	3.5	2.7	2.5	3.4	11.5	2.6	8.5	2.8	20	4.1	11.5	2.9	6.5	3.8	18	2.8	51.1	22.2	2	12	17	27	·	1	·	1	11	10	10	1	·	—	—
Rok	55.5	2.4	37.5	2.0	66	2.4	117	2.7	123	2.6	201.5	2.8	197.5	2.8	100	2.9	198	2.4	568.1	24.3	27.VI	22	39	129	26	3	1	29	156	138	103	14	52	—	—

Biskupiec

$\varphi = 53°52'$ $\lambda = 20°57'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.5	-5.8	5.0	5	-21.3	26	-4.2	-1.5	-3.0	-2.9	4.1	4.5	4.5	4.4	82	77	83	81	0.7	1.1	0.7	0.8	–	–	–	–
II	–	–	–	–	2.8	-0.8	11.4	18	-5.7	5	0.0	2.3	0.9	1.0	5.7	6.3	5.9	6.0	92	87	89	89	0.5	0.9	0.7	0.7	–	–	–	–
III	–	–	–	–	7.6	0.6	15.8	10	-4.1	20	2.7	6.1	3.1	3.8	6.5	6.8	6.5	6.6	87	72	85	81	1.0	2.8	1.2	1.7	–	–	–	–
IV	–	–	–	–	13.9	2.0	23.2	7	-6.5	2	5.5	12.6	6.8	7.9	7.0	7.3	7.5	7.3	76	51	74	67	2.3	8.2	2.8	4.4	–	–	–	–
V	–	–	–	–	15.8	6.3	23.7	30	0.7	19	9.4	14.5	10.0	11.0	10.0	10.7	10.7	10.5	84	65	86	78	2.0	6.3	1.8	3.4	–	–	–	–
VI	–	–	–	–	22.8	11.5	30.4	27	6.2	1	15.9	21.7	15.5	17.2	14.8	13.8	14.8	14.5	82	54	84	73	3.5	12.8	3.1	6.5	–	–	–	–
VII	–	–	–	–	20.2	10.1	29.9	3	7.4	17	14.0	19.0	14.2	15.4	13.8	14.4	14.3	14.2	87	67	88	81	2.2	8.2	2.0	4.1	–	–	–	–
VIII	–	–	–	–	19.3	10.4	27.9	6	6.2	31	13.4	18.3	13.5	14.7	14.1	15.0	14.1	14.4	91	72	90	84	1.4	6.5	1.5	3.1	–	–	–	–
IX	–	–	–	–	18.8	7.4	27.6	17	0.6	28	10.9	18.1	11.2	12.8	11.9	12.7	12.0	12.2	89	61	89	80	1.4	8.5	1.6	3.8	–	–	–	–
X	–	–	–	–	13.9	6.2	18.7	4	1.0	23	7.6	13.4	9.5	10.0	9.4	10.6	9.8	9.9	89	70	82	80	1.1	5.0	2.2	2.8	–	–	–	–
XI	–	–	–	–	4.7	0.4	10.4	3	-6.0	24	2.0	3.9	2.6	2.8	6.7	7.0	6.7	6.8	91	85	89	88	0.6	1.2	0.8	0.9	–	–	–	–
XII	–	–	–	–	-1.5	-8.5	1.3.2	5	-26.3	27	-5.5	-3.0	-5.2	-4.7	3.9	4.3	4.0	4.1	78	77	79	78	0.8	1.2	0.8	0.9	–	–	–	–
Rok	–	–	–	–	11.5	3.3	30.4	27 VI	-26.3	27 XII	6.0	10.4	6.6	7.4	9.0	9.4	9.2	9.2	86	70	85	80	1.5	5.2	1.6	2.8	–	–	–	–

Augustów

$\varphi = 53°51'$ $\lambda = 23°00'$

I	–	–	–	–	-1.0	-6.5	6.2	4	-21.6	26	-4.4	-2.1	-3.5	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.6	8.4	8.4
II	–	–	–	–	2.2	-1.5	8.1	18	-5.8	14	-0.4	1.2	0.3	0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.9	8.8	7.6	8.8
III	–	–	–	–	7.5	0.5	15.2	10	-4.6	20	2.2	6.0	2.9	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.1	5.1	6.9
IV	–	–	–	–	13.8	3.2	23.8	14	-4.0	11	5.3	12.4	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	3.9	4.2	4.0	4.0
V	–	–	–	–	16.6	7.0	26.6	29	2.1	15	9.8	15.2	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	7.3	7.4
VI	–	–	–	–	23.0	12.3	30.8	27	6.7	21	16.6	21.1	17.0	17.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.0	5.4	5.6
VII	–	–	–	–	21.0	11.4	29.4	3	8.0	6	14.6	19.6	15.5	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.4	6.7	6.8
VIII	–	–	–	–	20.5	11.4	28.6	6	6.8	18	13.9	19.3	14.7	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.3	6.0	6.6
IX	–	–	–	–	19.0	8.1	28.4	3	0.1	24	9.9	17.8	11.6	12.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.3	3.4	4.9
X	–	–	–	–	14.1	6.1	20.1	4	0.2	23	6.9	13.1	9.1	9.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.7	4.0	5.6
XI	–	–	–	–	4.8	0.9	11.9	2	-5.6	29	2.2	3.7	2.7	2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.6	8.5	8.5
XII	–	–	–	–	-1.5	-7.5	12.5	5	-24.7	27	-5.3	-3.0	-4.7	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	5.4	6.5
Rok	–	–	–	–	11.7	3.8	30.8	27 VI	-24.7	27 XII	5.9	10.4	7.0	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.0	6.7

Mikołajki

$\varphi = 53°47'$ $\lambda = 21°35'$

I	1001.8	1026.1	981.2	1018.4	-0.3	-5.0	5.3	4	-18.9	26	-3.4	-1.4	-2.3	-2.4	4.6	4.7	4.8	4.7	90	81	88	86	0.4	0.9	0.6	0.6	7.8	8.1	7.3	7.7
II	1003.7	1020.8	977.6	1020.3	2.8	-1.0	11.7	18	-5.5	5	0.1	2.0	1.0	1.0	5.9	6.2	6.1	6.1	95	88	92	92	0.3	0.9	0.5	0.6	9.0	8.2	7.8	8.3
III	995.7	1016.7	974.0	1012.0	7.7	1.0	15.4	10	-3.9	20	2.8	6.2	3.9	4.2	6.7	6.5	6.6	6.6	89	69	81	80	0.9	3.1	1.6	1.9	8.5	7.4	5.5	7.1
IV	997.3	1010.4	983.7	1013.3	13.5	3.2	22.8	7	-3.6	2	5.6	12.2	7.7	8.3	7.1	6.8	7.6	7.2	77	49	70	65	2.3	8.3	3.3	4.6	4.9	4.8	4.0	4.6
V	995.0	1003.6	984.5	1010.8	15.7	7.5	24.5	28	3.2	15	9.9	14.3	10.7	11.4	10.5	10.3	10.8	10.5	85	63	83	77	1.9	6.6	2.3	3.6	7.5	7.6	6.6	7.2
VI	998.0	1010.0	989.3	1013.5	22.4	13.2	29.7	27	9.0	1	16.2	21.0	16.8	17.7	14.9	14.8	15.0	14.9	81	57	78	72	3.7	11.4	4.4	6.5	6.2	6.0	4.8	5.7
VII	995.7	1010.1	981.0	1011.3	20.1	11.9	29.5	3	8.2	6	14.1	18.5	15.1	15.7	13.9	13.5	14.4	13.9	86	66	84	79	2.3	8.2	3.1	4.5	7.2	7.4	7.1	7.2
VIII	997.8	1013.0	985.2	1013.4	19.3	12.1	27.9	6	9.4	14	13.7	18.0	14.6	15.2	13.9	14.0	14.4	14.1	89	69	86	81	1.8	6.9	2.4	3.7	7.1	7.4	6.2	6.9
IX	1001.9	1015.4	985.5	1017.6	18.4	9.6	27.6	2	3.4	24	11.2	17.4	13.0	13.6	12.3	12.5	12.8	12.5	91	63	84	79	1.3	7.9	2.4	3.9	4.9	5.0	3.7	4.5
X	1004.0	1016.9	980.2	1020.0	13.5	7.1	18.4	4	2.4	23	7.9	12.6	10.1	10.2	9.6	10.5	10.0	10.0	89	73	81	81	1.1	4.3	2.4	2.6	7.1	6.3	5.2	6.2
XI	997.6	1012.7	982.3	1013.8	5.0	1.4	10.9	2	-4.8	24	2.5	3.9	3.1	3.2	6.9	7.1	7.2	7.1	93	86	90	90	0.6	1.2	0.8	0.9	9.0	8.6	8.1	8.6
XII	997.7	1028.5	971.7	1014.4	-1.2	-6.9	12.5	5	-22.1	27	-4.7	-2.8	-4.2	-4.0	4.2	4.6	4.3	4.4	87	82	86	85	0.7	1.0	0.7	0.8	7.0	6.7	4.7	6.1
Rok	998.8	1028.5	971.7	1014.8	11.4	4.5	29.7	27 VI	-22.1	27 XII	6.3	10.2	7.5	7.9	9.2	9.3	9.5	9.3	88	70	84	81	1.4	5.1	2.0	2.8	7.2	7.0	5.9	6.7

Resko

$\varphi = 53°46'$ $\lambda = 15°25'$

I	1010.9	1032.0	986.1	1018.1	1.0	-4.4	6.1	29	-17.0	27	-2.8	0.4	-2.0	-1.6	4.6	5.2	4.8	4.9	85	79	85	83	0.6	1.2	0.7	0.8	6.5	6.5	5.8	6.3
II	1013.0	1030.3	983.3	1020.1	5.7	0.3	12.2	18	-6.7	5	1.6	4.4	2.7	2.8	6.5	7.3	6.9	6.9	94	87	92	91	0.4	1.2	0.6	0.7	8.8	8.4	7.6	8.3
III	1009.6	1029.3	980.6	1016.6	9.2	2.4	17.4	10	-4.6	20	3.8	7.7	5.1	5.4	7.2	7.5	7.4	7.4	89	71	84	81	1.0	3.3	1.5	1.9	8.7	7.6	6.2	7.5
IV	1006.0	1017.5	994.7	1012.9	14.8	3.8	24.9	14	-3.0	10	6.5	13.3	8.6	9.2	7.7	8.3	8.5	8.2	78	55	75	69	2.3	9.0	3.1	4.5	4.8	5.4	4.6	4.9
V	1005.8	1016.5	990.8	1012.7	14.9	6.3	25.0	30	0.3	13	9.0	13.4	9.5	10.4	10.1	10.5	10.2	10.3	88	69	85	81	1.5	5.1	1.8	2.8	7.5	8.0	7.0	7.5
VI	1008.1	1021.8	995.8	1014.8	22.4	11.4	28.2	5	6.8	22	15.5	20.8	15.8	17.0	14.5	14.2	14.9	14.5	82	59	83	75	3.3	11.1	3.3	5.9	4.5	6.6	5.1	5.4
VII	1005.1	1020.4	989.4	1011.8	19.7	11.7	31.7	3	5.5	1	14.0	18.2	14.5	15.3	14.3	14.2	14.4	14.3	89	70	87	82	1.9	7.4	2.3	3.9	8.1	8.0	7.4	7.8
VIII	1008.1	1021.9	994.8	1014.9	19.4	11.3	26.3	31	7.5	8	13.5	17.9	13.9	14.8	14.7	15.0	14.6	14.8	95	74	92	87	0.8	5.9	1.4	2.7	7.9	7.7	5.5	7.0
IX	1011.2	1022.8	995.2	1018.0	20.0	9.5	27.8	17	0.7	27	11.1	19.1	12.8	14.0	12.7	13.9	13.4	13.3	94	63	89	82	0.9	8.7	1.7	3.9	5.8	4.5	3.3	4.5
X	1010.2	1023.6	980.3	1017.1	14.8	7.7	20.6	6	2.3	14	9.2	14.1	10.3	11.0	10.5	11.2	11.2	11.0	90	71	89	83	1.3	5.2	1.5	2.7	7.1	6.2	4.7	6.0
XI	1007.1	1030.3	987.2	1014.0	6.5	1.6	11.4	2	-6.2	23	3.0	5.8	3.5	4.0	7.3	7.8	7.4	7.5	94	83	92	90	0.5	1.6	0.7	0.9	8.7	8.4	7.2	8.1
XII	1008.4	1041.2	977.4	1015.6	0.3	-6.4	13.6	5	-21.2	26	-3.6	-1.1	-3.1	-2.7	4.7	5.1	4.7	4.8	88	82	86	85	0.6	1.1	0.8	0.8	7.0	6.3	6.0	6.4
Rok	1008.6	1041.2	977.4	1015.5	12.4	4.6	31.7	3 VII	-21.2	26 XII	6.7	11.2	7.6	8.3	9.6	10.0	9.8	9.8	89	72	87	83	1.3	5.0	1.6	2.6	7.1	7.0	5.9	6.7

Uwaga. Ciśnienie powietrza jest za wysokie przeciętnie o ok. 0,5 mb.

Biskupiec

$H_s = 160\,m$ $h_w = 14\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU °/₀																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		●	●	Opad R			≡	▦	≥R
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min<-10°	Max<0°	Min<0°	Max>25°	>10	>15			≥0.1	≥1.0	≥10.0			
I	11	17	·	·	1	1.0	10	3.0	13	18	30	3.3	13	1.7	15	17	·	24	21.9	9.1	30	7	12	27	·	1	·	—	—	14	5	·	5	10	·
II	1	2.0	3	2.0	·	·	6	2.3	13	3.5	30	2.6	23	2.0	8	1.8	·	24	24.8	5.9	27	·	3	17	·	·	·	—	—	11	6	·	10	1	·
III	·	·	·	·	·	·	1	5.0	1	3.0	25	5.8	35	4.6	31	5.3	·	5.1	38.6	10.6	12	·	·	10	·	5	1	—	—	14	7	1	4	4	·
IV	7	2.1	10	2.3	16	3.8	7	5.3	2	2.5	16	2.9	13	2.1	19	2.9	·	3.0	23.0	6.6	5	·	·	10	·	1	·	—	—	10	7	·	2	2	1
V	3	2.3	10	1.8	8	2.1	4	2.5	4	2.8	21	2.6	14	2.2	29	3.2	·	2.6	99.7	18.8	27	·	·	·	·	·	·	—	—	15	14	3	1	·	7
VI	4	1.2	12	2.1	9	1.7	3	4.0	4	2.5	22	4.0	18	3.9	18	2.6	·	3.0	85.2	16.4	27	·	·	·	10	·	·	—	—	13	10	3	1	·	5
VII	3	1.0	1	1.0	3	3.0	4	2.5	3	1.3	41	2.8	28	2.2	10	1.6	·	2.4	122.3	22.4	31	·	·	·	3	·	·	—	—	20	18	4	2	·	5
VIII	4	2.2	2	2.0	3	2.0	·	·	4	4.8	27	3.2	31	2.5	22	2.5	·	2.7	90.9	13.4	7	·	·	·	2	·	·	—	—	18	18	2	1	·	4
IX	6	1.7	8	2.4	12	2.1	7	2.9	2	2.5	14	3.0	23	2.5	18	2.1	·	2.4	34.3	13.4	14	·	·	·	4	·	·	—	—	6	5	1	4	·	2
X	·	·	4	2.5	18	4.1	24	3.8	13	3.1	16	3.0	12	2.9	6	2.8	·	3.4	15.4	5.8	29	·	·	·	·	·	·	—	—	9	5	·	10	·	·
XI	7	2.0	5	3.6	12	4.7	13	3.8	9	3.3	25	4.2	10	3.6	6	3.5	3	3.7	48.2	8.9	30	·	2	14	·	·	·	—	—	16	11	·	5	4	·
XII	9	2.8	3	4.7	4	1.8	6	4.2	9	1.9	26	3.9	18	3.7	14	2.5	4	3.1	40.7	7.0	2	11	14	26	·	2	·	—	—	12	11	·	4	19	·
Rok	55	1.6	58	2.0	86	2.2	85	3.3	77	2.8	293	3.4	238	2.8	196	2.7	7	3.0	645.0	22.4	31.VII	18	31	104	19	9	1	—	—	158	117	14	49	40	24

Uwaga. W miesiącach I–X obserwator nie notował cisz.

Augustów

$H_s = 130\,m$ $h_w = 17\,m$

I	15	1.7	1	2.0	2	2.0	5	2.4	20	2.2	10	2.4	2	1.5	1	2.0	37	1.3	34.1	6.8	11	12	13	30	·	·	·	1	20	11	11	·	3	27	—
II	1	2.0	2	1.0	1	2.0	5	1.3	24.5	1.5	14.5	1.5	0.5	1.0	2.5	1.8	33	0.9	32.0	13.0	28	·	5	20	·	·	·	·	22	4	4	2	15	7	—
III	8.5	2.6	·	·	·	·	1	3.0	2	1.2	20	3.4	12.5	5.0	23	3.2	26	2.6	35.0	10.3	12	·	·	11	·	1	·		9	15	10	1	7	1	—
IV	5.5	2.4	5.5	2.9	10	3.2	8	3.3	4.5	2.4	6.5	2.9	7	2.7	10	4.0	33	1.9	24.4	8.2	5	·	·	9	·	1	·	1.2	6	9	7		1	2	—
V	3	2.2	2	2.2	5.5	2.2	10	3.1	5.5	1.7	5	3.2	11.5	2.5	13.5	2.6	37	1.5	65.6	11.1	6	·	·	·	3	·	·	·	13	14	10	1	1	·	—
VI	1	1.0	5	2.6	3	2.7	12.5	3.3	4	3.4	10.6	2.7	19	3.4	7	3.4	28	2.0	87.1	27.2	8	·	·	·	12	·	·	3	8	11	9	3	·	·	—
VII	3	2.3	0.5	3.0	0.5	6.0	2	5.3	10	3.0	30.5	3.7	19	3.9	6.5	2.8	21	2.8	73.4	20.1	30	·	·	·	3	·	·	3	13	17	14	2	·	·	—
VIII	3.5	1.3	2.5	2.0	0.5	2.0	·	·	10	4.0	30	4.7	20	3.5	20.5	3.0	6	3.5	33.5	6.7	11	·	·	·	3	·	·	4	10	17	9	·	1	·	—
IX	0.5	1.0	1	2.0	2	2.2	3.5	1.9	3.5	3.7	11	3.3	16	2.4	9.5	2.3	43	1.4	46.7	11.7	14	·	·	·	5	·	·	7	9	7	7	3	5	·	—
X	0.5	3.0	4	3.0	11.5	3.9	26	3.3	14.5	2.3	6.5	2.8	5	3.4	3	1.7	22	2.3	92	3.2	26	·	·	·	·	·	·	4	9	5	5	·	10	·	—
XI	6	2.9	·	·	2	2.0	12	2.4	3	1.8	24.5	2.9	14.5	3.1	6	2.8	22	2.0	45.7	12.1	11	·	1	16	·	·	·	·	21	13	9	1	2	·	—
XII	10.5	2.8	3	5.0	3	4.0	8.5	3.1	7.5	2.7	20	3.6	13.5	3.3	11	2.9	16	2.7	36.4	12.1	2	13	16	27	·	·	·	3	11	9	7	1	1	20	—
Rok	58	2.1	26.5	2.1	41	2.7	93.5	2.7	109	2.5	189	3.1	140.5	3.0	113.5	2.7	324	2.1	523.1	27.2	8.VI	25	35	113	26	2	·	37	151	132	102	14	46	57	—

Mikołajki

$H_s = 127\,m$ $H_b = 131{,}1\,m$ $h_w = 12\,m$

I	8.5	3.6	3.5	3.0		·	7.5	3.5	24.5	3.7	21	3.2	10	3.7	8	2.9	10	3.1	38.8	14.0	5	6	12	26	·	·	·	1	18	13	7	2	4	15	·
II	2	2.2	0.5	3.0	3	3.2	14	3.6	21.5	4.3	13	2.5	17	2.7	5	3.1	8	3.0	25.3	8.0	11	·	1	18	·	·	·	1	20	10	4	·	11	10	·
III	0.5	7.0	·	·	0.5	9.0	0.5	9.0	8	3.8	25.5	4.8	45	5.5	10	8.7	3	5.4	33.0	6.8	30	·	·	11	·	9	1	·	10	13	8	·	3	3	·
IV	7	3.4	5	2.2	19	3.9	10.5	5.1	5.5	3.1	9	2.7	13	3.4	11	4.0	10	3.3	13.8	3.6	7	·	·	9	·	3	·	10	7	7	5	·	4	2	2
V	5	3.3	3.5	1.9	6.5	3.2	9	3.4	10	2.5	13	2.2	13.5	3.0	21.5	4.8	11	2.9	65.2	13.4	10	·	·	·	·	2	·	·	10	16	13	1	4	·	6
VI	2	1.8	3.5	1.6	14	2.5	8.5	3.6	8.5	3.9	16.5	3.4	17	4.0	10	3.7	10	3.0	98.0	31.5	15	·	·	·	8	2	1	4	7	16	11	3	2	·	10
VII	2.5	2.2	·	·	5.5	2.3	7	3.6	17	3.5	26.5	2.6	15	3.3	5.5	2.2	14	2.5	85.3	14.1	16	·	·	·	3	6	·	2	13	22	18	2	4	·	6
VIII	1	2.0	·	·	1.5	1.0	4	4.5	14.5	4.4	27.5	3.3	24	4.5	13.5	3.0	7	3.5	72.5	17.2	7	·	·	·	2	3	·	10	1	20	14	1	1	·	7
IX	4.5	1.9	3	1.8	13.5	2.2	6.5	4.0	7.5	3.2	18.5	3.3	20.5	4.3	7	3.3	9	2.9	26.3	11.0	14	·	·	·	3	2	1	8	5	7	5	1	7	·	2
X	1	2.0	1.5	1.7	19.5	4.2	31	5.0	21	3.1	8	3.4	7	2.3	2	3.8	2	3.8	7.7	2.5	2.9	·	·	·	·	3	·	5	13	6	4	·	9	·	·
XI	7	3.0	2.5	3.0	8.5	6.6	15	4.9	15	2.7	18.5	3.9	10	3.8	7.5	2.7	6	3.7	44.8	8.3	5	·	2	11	·	3	·	1	21	13	10	·	8	3	·
XII	11.5	4.9	5.5	3.5	1.5	3.0	11.5	4.0	14	3.2	19	3.9	18.5	4.2	5.5	4.6	6	3.8	35.7	12.0	2	11	15	27	·	5	1	3	10	10	6	1	4	20	·
Rok	52.5	3.1	28.5	1.8	93	3.4	125	4.5	167	3.4	216	3.3	210.5	3.7	106.5	3.9	96	3.4	547.4	31.5	15.VI	17	30	102	16	38	4	45	135	153	105	11	61	53	33

Resko

$H_s = 55\,m$ $H_b = 56{,}2\,m$ $h_w = 11\,m$

I	1.5	2.3	1.5	1.7	5.5	1.5	20.5	2.8	2.3	3.0	14	2.3	7.5	2.3	2.5	3.4	17	2.1	47.5	18.3	3.0	5	11	20	·	·	·	8	15	12	8	1	4	7	·
II	1	3.8	0.5	1.0	2.5	1.8	12	3.5	16.5	2.5	17	2.3	18.5	2.1	5	1.9	11	2.1	63.0	17.1	9	·	·	10	·	·	·	·	16	14	9	4	10	4	·
III	1.5	6.0	·	·	·	·	0.5	2.0	3	2.2	14.5	3.6	49.5	4.0	16	3.6	8	3.5	62.2	10.6	2.9	·	·	7	·	2	2	1	15	19	14	2	6	2	·
IV	3	1.0	6.5	1.4	2.0	2.7	18.5	3.6	4.5	2.4	7	1.9	8.5	2.4	6	1.9	16	2.1	41.1	22.4	2.7	·	·	6	·	·	·	6	5	9	7	1	1	1	3
V	12.5	2.5	6.5	2.4	1.5	1.0	10	2.2	6.5	2.5	12	2.1	17	2.6	11	2.7	16	2.0	94.5	10.7	8	·	·	·	·	·	·	·	16	18	17	2	2	·	6
VI	2.5	1.0	3	1.3	2.5	1.8	6	2.5	8.5	2.1	10.5	2.4	24	3.1	8	2.5	25	1.8	57.7	14.1	14	·	·	·	8	·	·	2	2	14	10	3	3	·	7
VII	1	1.0	0.5	1.0	1	1.0	2	2.0	12	2.3	26	2.7	30.5	2.8	7	2.7	13	2.2	141.6	48.7	31	·	·	·	4	1	·	2	19	25	18	3	1	·	6
VIII	·	·	·	·	·	·	4	1.8	10	2.1	17	2.4	29	2.9	4	3.6	29	1.8	141.1	22.0	19	·	·	·	1	·	·	2	10	22	20	5	4	·	6
IX	·	·	·	·	3	1.5	15.5	2.4	10.5	1.4	15	2.4	12	3.1	3	2.2	31	1.5	39.4	19.8	7	·	·	·	4	·	·	10	6	11	8	1	5	·	1
X	·	·	·	·	1.0	2.5	28.5	3.6	14.5	3.0	11	2.7	6.5	1.7	1.5	2.7	21	2.3	61.5	16.1	3.1	·	·	·	·	·	·	6	11	12	9	2	3	·	·
XI	2	1.5	5	2.9	8.5	3.1	7	1.6	11	2.4	21	2.8	7.5	2.5	1	3.0	27	1.8	26.9	10.6	30	·	·	9	·	·	·	1	19	13	8	1	6	·	·
XII	4.5	2.6	2.5	1.8	2	1.5	15.5	2.4	12	2.0	20	3.3	10.5	2.9	4	2.4	22	2.0	50.8	10.2	11	9	12	23	·	2	1	3	13	14	10	1	3	17	·
Rok	29.5	1.7	26	1.1	56.5	1.5	140	2.5	132	2.3	185	2.6	221	2.7	69	2.7	236	2.1	827.3	48.7	31.VII	14	23	75	17	5	3	41	147	183	138	26	48	31	29

Świdwin

$\varphi = 53°46'$ $\lambda = 15°46'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	0.6	-4.8	5.4	29	-16.9	26	-3.2	-0.3	-2.4	-2.1	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.0	5.3	6.0
II	—	—	—	—	5.1	-1.2	12.4	18	-6.1	4	0.8	3.6	1.9	2.0	—	—	—	—	—	—	—	—	—	—	—	—	9.2	8.1	7.8	8.4
III	—	—	—	—	8.4	1.8	16.2	10	-4.8	20	3.3	7.0	4.4	4.8	—	—	—	—	—	—	—	—	—	—	—	—	8.2	7.2	5.9	7.1
IV	—	—	—	—	14.7	3.5	22.4	7	-3.5	10	6.4	12.5	8.1	8.8	—	—	—	—	—	—	—	—	—	—	—	—	4.2	5.4	5.1	4.9
V	—	—	—	—	15.1	6.2	24.6	30	1.2	13	9.6	10.0	9.1	9.4	—	—	—	—	—	—	—	—	—	—	—	—	7.1	8.0	7.1	7.4
VI	—	—	—	—	22.1	11.5	27.3	2	7.3	22	15.5	19.9	15.4	16.6	—	—	—	—	—	—	—	—	—	—	—	—	6.9	7.0	5.8	6.6
VII	—	—	—	—	19.5	11.2	30.5	3	7.6	6	13.9	17.4	14.0	14.8	—	—	—	—	—	—	—	—	—	—	—	—	8.3	7.9	8.3	8.1
VIII	—	—	—	—	19.0	10.6	25.9	31	7.3	8	13.8	17.4	13.6	14.6	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.7	5.7	6.3
IX	—	—	—	—	19.8	9.1	27.6	1	0.5	27	11.0	18.6	12.8	13.8	—	—	—	—	—	—	—	—	—	—	—	—	4.1	3.6	3.3	3.7
X	—	—	—	—	14.5	7.7	20.6	6	3.0	30	9.2	13.5	10.0	10.7	—	—	—	—	—	—	—	—	—	—	—	—	7.2	6.1	5.2	6.2
XI	—	—	—	—	6.1	1.6	10.9	2	-5.1	22	2.9	5.0	3.3	3.6	—	—	—	—	—	—	—	—	—	—	—	—	8.6	8.6	8.0	8.4
XII	—	—	—	—	0.0	-6.6	13.5	5	-24.2	27	-3.8	-1.8	-3.6	-3.2	—	—	—	—	—	—	—	—	—	—	—	—	7.3	6.3	5.7	6.4
Rok	—	—	—	—	12.1	4.2	30.5	3.VII	-24.2	27.XII	6.6	10.2	7.2	7.8	—	—	—	—	—	—	—	—	—	—	—	—	7.0	6.7	6.1	6.6

Potczyn-Zdrój

$\varphi = 53°46'$ $\lambda = 16°06'$

I	—	—	—	—	1.0	-4.4	5.9	29	-17.4	26	-2.9	0.1	-2.2	-1.8	4.6	5.3	4.8	4.9	86	83	85	84	0.6	1.0	0.7	0.8	—	—	—	—
II	—	—	—	—	5.4	0.0	13.4	18	-6.5	5	1.3	4.3	2.2	2.5	6.3	7.4	6.6	6.8	92	88	91	91	0.5	1.1	0.7	0.8	—	—	—	—
III	—	—	—	—	9.0	2.3	18.1	10	-3.0	22	3.9	7.9	4.9	5.4	7.2	7.5	7.7	7.5	88	70	87	82	1.0	3.4	1.2	1.9	—	—	—	—
IV	—	—	—	—	14.8	3.4	24.8	7	-3.2	10	7.0	13.4	8.2	9.2	7.7	8.6	8.1	8.1	76	57	75	69	2.7	7.7	3.1	4.5	5.6	5.5	6.0	5.7
V	—	—	—	—	15.3	6.0	25.0	30	0.2	13	9.8	13.7	9.1	10.4	10.0	10.7	9.3	10.0	82	69	81	77	2.2	5.5	2.4	3.4	7.1	6.8	7.1	7.0
VI	—	—	—	—	22.8	11.1	27.8	2	6.5	22	15.5	20.8	15.3	16.7	14.1	14.1	15.1	14.4	81	59	86	75	3.6	11.0	2.5	5.7	4.7	5.5	5.3	5.2
VII	—	—	—	—	19.6	11.4	31.5	3	5.3	1	14.2	18.0	14.0	15.0	14.1	14.3	14.4	14.2	87	71	90	83	2.2	7.0	1.7	3.6	8.4	7.6	8.1	8.0
VIII	—	—	—	—	19.4	11.2	26.1	31	9.0	4	14.0	18.2	13.7	14.9	14.6	15.3	14.7	14.9	91	74	93	86	1.5	5.9	1.2	2.9	6.8	6.7	6.5	6.7
IX	—	—	—	—	19.8	9.0	28.3	2	-0.1	24	11.2	19.0	11.8	13.5	12.5	14.1	13.0	13.2	92	64	92	83	1.2	8.5	1.2	3.6	5.8	4.1	4.2	4.7
X	—	—	—	—	14.5	7.3	19.9	6	2.2	31	9.3	14.0	10.4	11.0	10.8	11.5	11.2	11.2	93	73	89	85	0.9	4.7	1.6	2.4	8.0	5.8	6.2	6.7
XI	—	—	—	—	6.6	1.8	11.3	2	-6.5	23	3.2	5.8	3.6	4.0	7.2	7.7	7.5	7.5	91	83	92	89	0.7	1.6	0.7	1.0	8.6	7.9	8.0	8.2
XII	—	—	—	—	0.4	-6.4	13.8	5	-21.6	26	-3.4	-1.2	-3.3	-2.8	4.8	5.0	4.8	4.9	87	82	88	86	0.6	1.0	0.5	0.7	6.9	5.4	6.2	6.2
Rok	—	—	—	—	12.4	4.4	31.5	3.VII	-21.6	26.XII	6.9	11.2	7.3	8.2	9.5	10.1	9.8	9.8	87	73	87	82	1.5	4.9	1.5	2.6	—	—	—	—

Olsztyn - Dajtki

$\varphi = 53°46'$ $\lambda = 20°25'$

I	1001.4	1026.0	980.7	1018.7	-0.3	-6.0	6.1	4	-21.9	26	-4.3	-1.4	-2.9	-2.9	4.4	4.8	4.8	4.7	91	83	89	88	0.4	0.8	0.5	0.6	7.0	7.9	7.3	7.4
II	1003.2	1020.2	976.4	1020.6	3.3	-0.8	13.0	18	-6.8	5	0.3	2.3	1.2	1.2	6.1	6.5	6.3	6.3	96	90	93	93	0.2	0.8	0.5	0.5	9.2	8.6	8.2	8.7
III	996.0	1016.8	971.9	1012.9	8.4	0.8	16.1	10	-5.5	20	2.9	6.5	3.9	4.3	6.8	6.6	6.8	6.7	89	68	83	80	0.9	3.3	1.5	1.9	8.1	8.0	4.9	7.0
IV	996.6	1009.6	985.7	1013.3	14.0	2.1	23.4	7	-4.7	2	5.4	12.6	7.6	8.3	7.3	7.0	7.8	7.4	79	49	73	67	2.1	8.5	3.2	4.6	5.4	5.6	4.6	5.2
V	994.6	1002.1	983.2	1011.1	16.0	6.2	23.6	27	-0.4	19	9.3	14.2	10.0	10.9	10.4	11.0	10.8	10.7	88	67	87	81	1.6	5.7	1.8	3.0	7.2	8.0	7.0	7.4
VI	997.5	1009.6	986.9	1013.6	23.0	12.1	31.0	27	6.1	1	16.2	21.7	16.4	17.6	15.0	13.9	14.9	14.6	82	55	80	72	3.5	12.7	4.0	6.7	6.1	6.6	5.6	6.1
VII	995.1	1009.8	978.9	1011.3	20.2	11.2	30.8	3	7.4	1	13.9	18.5	14.8	15.5	14.2	13.9	14.3	14.1	89	67	85	80	1.8	6.0	2.8	4.2	7.6	7.8	7.1	7.5
VIII	992.5	1012.7	984.5	1013.9	19.1	10.9	27.7	6	7.2	31	13.3	17.8	14.0	14.8	14.2	14.6	14.3	14.4	92	72	88	84	1.2	6.3	1.7	3.1	7.8	7.7	6.5	7.3
IX	1001.4	1014.3	985.1	1017.8	19.0	8.2	27.8	17	0.0	24	10.3	17.9	11.9	13.0	12.0	13.0	12.6	12.5	94	63	89	82	0.9	8.1	1.6	3.5	5.2	5.0	3.2	4.5
X	1002.6	1015.5	977.9	1019.2	14.3	6.9	19.2	4	2.0	10	7.9	13.4	10.0	10.3	9.9	11.2	10.4	10.5	92	74	85	84	0.8	4.4	1.9	2.4	6.5	6.7	4.5	5.9
XI	996.9	1017.7	980.7	1013.8	5.1	0.6	10.3	3	-7.4	23	2.3	4.1	2.9	3.1	7.1	7.4	7.3	7.3	95	89	93	92	0.3	1.0	0.5	0.6	8.9	8.3	7.7	8.3
XII	997.4	1028.1	971.0	1014.7	-0.9	-7.6	13.2	6	-26.0	27	-4.8	-2.8	-4.3	-4.0	4.3	4.7	4.4	4.5	87	84	88	86	0.6	0.9	0.7	0.7	7.2	7.0	5.1	6.4
Rok	998.4	1028.1	971.0	1015.1	11.8	3.7	31.0	27.VI	-26.0	27.XII	6.1	10.4	7.1	7.7	9.3	9.6	9.6	9.5	90	72	86	83	1.2	5.0	1.7	2.6	7.2	7.3	6.0	6.8

Kwidzyń

$\varphi = 53°44'$ $\lambda = 18°55'$

I	—	—	—	—	1.1	-4.8	6.4	4	-16.0	26	-3.6	-0.3	-2.1	-2.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	4.4	-0.2	10.0	18	-7.7	5	0.7	3.2	2.2	2.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	10.2	1.6	17.1	10	-5.6	20	3.5	8.2	5.0	5.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	15.2	—	23.2	7, 14	—	—	6.2	13.4	8.9	9.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	16.3	—	24.8	30	—	—	9.9	14.7	10.4	11.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	23.8	—	29.6	27	—	—	15.9	22.5	18.0	18.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	20.5	10.8	32.1	3	6.4	1	14.1	18.3	15.8	16.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	19.7	10.8	28.1	6	8.0	4,14,18,26	13.3	18.4	15.5	15.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.7	8.8	28.1	2	1.0	24,28	10.5	18.8	13.6	14.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	15.2	7.5	20.2	5	2.5	14	8.7	14.5	11.3	11.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	6.0	2.8	11.0	7	-7.4	23	3.1	5.0	3.8	3.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	0.3	-7.1	13.6	5	-23.3	28	-3.8	-1.6	-3.7	-3.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	12.7	—	32.1	3.VII	-23.3	28.XII	6.5	11.3	8.2	8.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Świdwin

$H_s = 94\,m$ $h_w = 12{,}4\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%D, vmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min <-10°	Max <0°	Min <0°	Max >25°	Wiatr v >10	>15	●	●	Opad R >0.1	>1.0	>10.0	≡	⊠	≈
I	2	2.5	2.5	4.2	8.5	2.1	19	3.0	25.5	3.6	12.5	4.2	5.5	2.5	3.5	2.1	3.4	2.8	31.0	8.3	30	5	9	27	·	1	·	9	13	12	8	·	1	2	·
II	1.5	5.0	1.5	1.0	1	5.0	2.5	3.0	2.2	3.8	1.7	3.5	1.5	2.3	7	2.3	1.2	2.7	54.5	12.5	9	·	·	12	·	·	·	·	18	14	11	3	7	·	·
III	2	7.0	·	·	·	·	·	·	2	6.5	2.1	7.5	40.5	7.6	22.5	6.0	5	6.7	45.6	11.0	29	·	·	8	·	1.4	6	3	11	19	13	1	2	·	·
IV	4	4.0	1.1	3.8	1.1	3.5	2.4	3.7	4	2.2	1.0	3.3	6.5	5.5	1.5	5.0	1.8	3.0	20.2	6.2	7	·	·	6	·	·	·	8	8	11	6	·	1	·	3
V	1.2	3.2	10.5	3.9	5	2.6	8.5	3.1	10.5	4.0	13.5	4.9	1.0	3.7	1.2	3.0	1.1	3.2	79.5	16.4	5	·	·	·	·	·	·	2	16	17	15	3	·	·	2
VI	1.0	3.1	4	3.0	5	2.6	10.5	2.7	4.5	1.9	1.0	4.2	20.5	5.5	11.5	3.5	1.4	3.2	68.4	16.3	7	·	·	·	9	1	1	1	9	11	10	3	—	·	6
VII	2	1.0	·	·	1	5.0	1.5	1.7	1.0	3.0	2.2.5	5.4	3.1	3.6	1.1	4.6	1.4	3.4	112.1	45.0	31	·	·	·	4	1	·	1	20	23	18	2	·	·	1
VIII	2	2.0	·	·	·	·	3	2.3	9	3.7	2.4	3.7	2.2	3.7	1.2	2.8	2.1	2.7	118.6	20.0	19	·	·	·	1	·	·	4	11	19	18	4	·	·	2
IX	·	·	2	1.0	6	1.7	16.5	2.5	9	2.4	1.4	3.1	1.0	3.7	8.5	2.6	2.4	2.0	37.0	16.2	7	·	·	·	4	·	·	12	4	9	6	1	—	·	1
X	·	·	·	·	6.5	3.9	3.2	4.2	1.9	3.2	12.5	4.1	6	3.0	5	2.6	1.2	3.3	34.0	6.3	31	·	·	·	·	·	·	7	13	12	9	·	—	·	·
XI	2	2.5	7.5	3.0	1.0	4.8	7	1.4	1.0	3.2	2.4	4.8	5	3.4	5.5	2.8	1.9	2.9	28.5	9.0	30	·	·	8	·	1	1	2	22	13	10	·	—	·	·
XII	7	4.7	2	1.0	3	3.7	1.7	2.2	12.5	2.8	2.6	5.6	6.5	4.0	4	1.5	1.5	3.2	54.0	23.4	22	10	13	25	·	1	1	4	12	7	6	1	—	10	·
Rok	44.5	2.9	41	1.7	57	2.9	146.5	2.5	138	3.4	207	4.5	178	4.0	104	3.2	179	3.3	688.4	45.0	31.VII	15	22	86	18	19	9	53	157	167	130	18	—	12	15

Połczyn-Zdrój

$H_s = 50\,m$ $h_w = 14{,}5\,m$

I	·	·	·	·	1.4	2.1	1.2	2.7	1.0	2.1	2.5	3.4	7	2.1	3	3.7	2.2	2.1	28.8	8.5	30	6	10	19	·	·	·	—	—	13	10	·	·	—	—
II	1	4.0	·	·	·	·	2	3.0	1.0	2.4	3.2	3.2	6	3.2	1.1	2.4	2.2	2.2	46.1	11.1	9	·	·	14	·	·	·	—	—	11	8	1	4	—	—
III	·	·	·	·	·	·	1	4.0	·	·	2.6	4.4	3.8	4.4	2.2	5.2	6	4.3	46.8	8.1	27	·	·	7	·	·	·	—	—	17	12	·	2	—	—
IV	·	·	2	1.0	1.2	3.0	2.0	3.0	1.3	1.8	7	2.0	6	1.8	1.4	2.6	1.6	2.0	24.9	7.8	28	·	·	9	·	·	·	1	7	8	6	·	·	·	—
V	·	·	·	·	2	3.5	1	3.0	1.0	1.1	1.4	2.1	1.5	2.5	4.0	2.9	1.1	2.2	79.7	14.9	5	·	·	·	·	·	·	·	8	17	13	3	·	·	—
VI	·	·	·	·	·	·	6	2.5	1.1	1.3	3.4	2.8	6	2.0	1.2	4.8	2.1	2.2	72.4	17.6	13	·	·	·	1.1	·	·	3	3	12	10	3	·	·	—
VII	·	·	·	·	·	·	2	1.5	1.0	2.2	5.0	2.7	1.3	2.8	6	4.0	1.2	2.4	152.5	55.2	31	·	·	·	4	·	·	1	19	21	17	4	·	·	—
VIII	·	·	·	·	·	·	6	2.3	3	1.7	3.3	3.2	2.4	3.4	4	3.0	2.3	2.3	116.5	16.7	19	·	·	·	3	·	·	2	12	23	20	2	1	·	—
IX	·	·	·	·	·	·	1.0	2.2	6	2.5	2.4	2.6	1.7	3.4	1	2.0	3.2	1.8	42.1	18.2	7	·	·	1	4	·	·	6	6	8	7	1	6	·	—
X	1	1.0	2	2.5	6	4.0	1.6	3.3	1.8	2.4	1.8	2.6	7	2.6	1	3.0	2.4	2.1	31.0	7.1	31	·	·	·	·	·	·	1	13	11	9	·	3	·	—
XI	3	1.3	1	6.0	4	3.5	1.7	2.6	3	3.3	2.5	3.1	5	1.8	6	1.8	2.6	1.9	28.6	10.4	30	·	·	8	·	·	·	1	19	13	10	1	—	·	—
XII	·	·	9	2.1	6	3.2	9	4.0	6	2.2	2.9	3.0	·	·	7	3.4	2.7	2.1	41.9	10.9	4	10	12	22	·	·	·	2	7	8	6	1	—	16	—
Rok	5	0.5	1.4	1.0	44	1.6	102	2.8	100	1.9	3.17	2.9	144	2.5	127	3.2	2.42	2.3	711.3	55.2	31.VII	16	22	80	22	·	·	—	—	162	128	16	—	—	—

Olsztyn - Dajtki

$H_s = 133\,m$ $H_b = 135{,}4\,m$ $h_w = 12\,m$

I	4	4.0	7	3.1	·	·	1.2	1.5	17.5	2.9	2.8	3.1	9	2.3	5.5	2.9	1.0	2.5	20.1	7.9	30	9	13	26	·	·	·	3	16	12	8	·	6	17	·
II	1	3.0	0.5	3.0	2.5	1.4	1.0.5	1.7	16	3.3	2.4	2.8	14.5	3.0	1.0	2.7	5	2.6	28.1	7.1	28	·	2	17	·	·	·	1	20	17	7	·	14	7	·
III	·	·	1	2.0	·	·	·	·	4	3.5	23.5	4.1	44	4.8	19.5	2.1	1	4.5	32.1	7.1	12	·	·	11	·	1	·	1	9	17	8	·	4	4	·
IV	7.5	2.9	1.0	2.9	2.2	3.5	9	3.7	9	1.5	12	2.8	8	4.2	11.5	3.3	1	3.1	16.3	6.8	5	·	·	11	·	1	·	8	8	7	5	·	5	3	2
V	10.5	3.1	4.5	2.3	9	2.1	6.5	2.2	8.5	2.6	24	2.5	9	3.3	17	3.8	4	2.7	77.6	18.2	28	·	·	1	·	·	·	·	12	17	14	3	5	·	4
VI	5	1.5	1.0	2.2	15.5	2.1	5.5	2.6	9	2.2	1.3	2.9	25.5	3.7	5.5	3.4	1	2.8	99.2	24.7	7	·	·	·	12	·	·	4	8	14	10	5	2	·	7
VII	4	2.0	1	1.0	6	2.1	3	2.3	7.5	2.1	43.5	2.7	14	3.0	7	1.6	7	2.3	125.2	23.0	13	·	·	·	3	·	·	1	16	21	17	5	3	·	7
VIII	5	2.2	0.5	4.0	3	1.0	1	1.0	7.5	2.9	3.3	3.0	2.7	3.6	1.3	3.0	3	2.9	91.7	16.1	1	·	·	·	2	·	·	1	13	20	14	3	3	·	3
IX	5	1.8	2.5	2.2	8.5	2.5	6	2.7	8.5	2.2	19.5	2.6	12.5	3.3	8.5	3.2	1.4	2.3	43.9	15.9	14	·	·	·	4	·	·	9	5	7	6	2	3	·	1
X	·	·	1	2.0	24.5	3.6	17.5	4.0	18.5	2.6	13.5	2.6	10	3.5	5	3.6	3	3.2	27.6	9.4	29	·	·	·	·	·	·	5	10	8	7	·	11	·	·
XI	10	3.0	3	3.7	12	5.7	10	3.0	12.5	2.7	22.5	3.5	11	4.0	3	3.2	6	3.4	42.4	6.5	5	·	·	13	·	·	·	1	19	18	11	·	8	·	·
XII	7.5	4.6	5.5	4.8	4	2.0	6.5	2.9	15.5	2.9	24	4.6	17	4.6	4	3.4	9	3.6	32.0	7.0	4	12	14	25	·	1	·	4	13	12	7	·	7	21	·
Rok	59.5	2.3	46.5	2.8	107	2.2	87.5	2.3	134	2.6	280.5	3.1	206.5	3.6	109.5	3.0	64	3.0	636.2	24.7	7.VI	21	29	104	21	3	·	38	149	170	114	18	71	52	24

Uwaga. Kierunki i prędkości wiatru — wg anemometru.

Kwidzyń

$H_s = 15\,m$ $h_w = 13\,m$

I	·	·	1.3	1.5	1	3.0	1.5	2.5	4.0	3.6	2.2	4.6	0.5	8.0	0.5	8.0	1	2.9	12.5	6.9	30	7	9	20	·	2	·	—	—	6	2	·	·	—	·
II	1.5	1.7	3.5	1.9	·	·	1.2	2.8	3.9.5	2.4	1.9	2.4	6.5	2.8	2	2.0	·	2.6	31.9	10.2	27	·	·	13	·	1	·	—	—	8	6	1	3	—	·
III	·	·	·	·	·	·	1	0.5	2.3.5	2.3	30.5	2.9	32	4.5	6	3.0	·	3.2	12.0	2.6	20	·	·	6	·	4	·	—	—	10	6	·	1	—	·
IV	4	1.5	8	1.8	1.3	2.4	2.2	1.5	8	1.5	15	1.9	10	2.2	6	2.7	4	1.8	18.7	4.8	5	·	·	—	·	·	·	—	—	11	6	·	1	·	2
V	1.4	2.0	6	1.3	8	1.5	2	1.0	16	1.4	17	1.9	11	1.5	1.3	1.8	6	1.6	57.3	16.5	6	·	·	—	·	·	·	—	—	13	11	2	·	·	2
VI	2.5	1.0	6	1.0	4.5	1.9	1.2	1.1	13.5	1.7	12.5	1.8	15	2.2	2	1.0	2.2	1.2	39.7	9.6	14	·	·	—	15	·	·	—	—	9	8	·	·	·	5
VII	1	1.0	·	·	0.5	3.0	5.5	1.2	29	1.6	26.5	1.9	10	2.2	2.5	1.8	1.8	1.4	71.6	12.6	31	·	·	·	4	·	·	—	—	21	18	1	·	·	8
VIII	1	1.0	2	1.0	1	1.0	2	1.0	24.5	2.1	25	3.1	14.5	3.3	3	1.0	2.0	2.0	50.5	11.1	3	·	·	·	3	·	·	—	—	20	11	1	2	·	4
IX	·	·	3	2.3	6	1.5	1.1	2.0	15.5	1.3	15	2.9	10.5	1.9	7	2.3	2.2	1.5	44.5	17.2	14	·	·	·	4	·	·	—	—	7	7	2	·	·	2
X	1	1.0	3.5	3.0	13.5	3.0	3.5	2.5	14	1.9	8	2.9	2.5	1.4	2.5	3.4	1.3	2.2	31.5	8.2	18	·	·	·	·	·	·	—	—	10	8	·	—	·	·
XI	1.5	4.3	7.5	1.9	8.5	2.2	18.5	1.3	13.5	1.4	20	3.8	1.5	1.7	4	2.5	1.4	1.9	32.6	14.7	11	·	·	8	·	·	·	—	—	11	7	1	·	·	·
XII	3	3.3	8	1.9	3.5	2.1	29.5	1.7	17	2.8	13	4.8	5.5	3.4	6.5	2.2	7	2.5	24.9	5.6	4	12	14	25	·	·	·	—	—	9	8	·	·	—	·
Rok	29.5	1.4	60.5	1.5	60.5	1.8	165.5	1.6	254	2.0	223.5	2.9	119.5	2.9	55	2.6	12.7	2.1	427.7	17.2	14.IX	19	23	—	26	7	·	—	—	135	98	8	—	—	23

Prabuty

$\varphi = 53°44'$ $\lambda = 19°13'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max obs.	Data	Min obs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.4	-5.9	5.2	4	-20.0	26	-4.2	-1.2	-3.0	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	5.9	6.7
II	–	–	–	–	3.4	-0.6	12.7	18	-5.2	5	0.4	2.2	1.1	1.2	6.1	6.4	6.2	6.3	96	90	93	93	0.3	0.8	0.5	0.5	9.0	8.4	8.7	8.7
III	–	–	–	–	9.3	1.6	16.9	10	-5.0	20	3.3	7.7	4.3	4.9	6.9	6.7	7.1	6.9	89	65	84	79	1.0	4.1	1.4	2.2	7.7	6.5	4.5	6.2
IV	–	–	–	–	14.7	2.8	23.4	7	-2.8	11	6.2	12.5	7.3	8.3	7.6	7.6	8.2	7.8	78	53	78	70	2.3	7.8	2.5	4.2	4.4	4.7	2.1	3.7
V	–	–	–	–	15.3	6.1	24.4	30	1.7	23	9.5	13.4	8.9	10.2	10.2	10.7	10.2	10.4	85	70	89	81	1.9	5.0	1.3	2.7	6.7	7.8	5.3	6.6
VI	–	–	–	–	23.7	12.4	30.8	27	6.6	1	15.6	21.8	16.6	17.6	14.3	13.0	14.8	14.0	81	51	78	70	3.6	13.7	4.4	7.2	4.3	5.2	3.8	4.4
VII	–	–	–	–	20.0	11.0	31.9	3	6.1	1	14.4	18.0	14.4	15.3	14.0	13.9	14.3	14.1	85	69	87	80	2.6	7.4	2.2	4.1	7.4	2.5	6.8	7.2
VIII	–	–	–	–	19.6	11.4	28.2	6	8.1	14. 18	12.7	17.9	14.0	14.6	13.5	14.5	14.3	14.1	92	72	89	84	1.2	6.3	1.8	3.1	6.3	7.2	5.3	6.3
IX	–	–	–	–	19.8	9.0	28.6	2	1.7	28	10.2	18.3	12.3	13.3	11.7	13.0	12.7	12.5	92	61	87	80	1.1	8.5	1.9	3.8	4.1	4.8	2.0	3.6
X	–	–	–	–	14.8	7.1	19.2	5	3.2	23	8.7	13.7	10.2	10.7	9.9	11.1	10.3	10.4	88	72	84	81	1.4	4.9	2.2	2.8	6.8	6.0	4.4	5.7
XI	–	–	–	–	5.6	1.1	10.4	7. 8	-6.5	23	2.6	4.5	3.3	3.4	7.1	7.3	7.2	7.2	93	84	90	89	0.5	1.3	0.8	0.9	9.0	7.8	7.0	7.9
XII	–	–	–	–	-0.5	-7.0	13.8	6	-20.4	26	-4.2	-2.3	-3.9	-3.6	4.4	4.8	4.2	4.5	83	83	82	83	0.7	0.9	1.0	0.9	7.1	6.5	6.4	6.7
Rok	–	–	–	–	12.1	4.1	31.9	3.VII	-20.4	26.XII	6.3	10.5	7.1	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	5.2	6.2

Szczecinek

$\varphi = 53°43'$ $\lambda = 16°41'$

I	1000.2	1025.9	977.7	1018.3	0.3	-5.2	5.3	29	-19.7	26	-3.6	-0.5	-2.6	-2.3	4.6	5.1	4.8	4.8	90	82	88	87	0.4	0.9	0.6	0.6	6.6	6.7	5.9	6.4
II	1002.2	1018.8	973.4	1020.1	4.5	-0.3	12.9	18	-7.1	5	0.9	3.3	2.0	2.0	6.3	7.0	6.7	6.7	96	90	94	93	0.2	0.9	0.4	0.5	9.0	8.8	8.1	8.6
III	997.8	1017.4	970.1	1015.4	8.3	2.3	17.6	10	-4.0	20	3.5	7.2	4.6	5.0	7.3	7.3	7.4	7.3	91	72	87	83	0.7	3.1	1.2	1.7	8.8	8.2	6.7	7.9
IV	995.5	1007.3	984.7	1012.9	14.3	3.2	23.6	14	-3.2	10. 11	5.8	12.7	8.2	8.7	7.8	8.5	8.5	8.3	82	58	76	72	1.8	7.1	2.8	3.9	5.4	5.6	4.7	5.2
V	994.8	1004.5	981.5	1012.0	14.9	6.2	24.4	30	-0.1	2	9.4	13.1	9.5	10.4	10.2	10.7	10.1	10.3	86	72	84	81	1.7	4.8	2.0	2.8	7.1	8.7	6.9	7.6
VI	997.3	1010.7	985.0	1014.1	22.3	12.0	27.4	26	8.4	22	15.7	20.5	16.2	17.2	14.7	14.3	14.9	14.6	78	60	80	73	3.4	10.4	3.8	5.9	4.9	6.6	5.4	5.6
VII	994.6	1009.6	979.0	1011.5	19.3	11.8	31.8	3	4.0	1	14.1	17.7	14.5	15.2	14.3	14.5	14.6	14.5	89	73	88	83	1.9	6.5	2.0	3.5	8.6	8.1	7.2	8.0
VIII	997.5	1012.0	984.6	1014.5	19.0	11.7	26.2	31	8.9	30	13.7	17.6	14.1	14.9	14.8	15.2	14.8	14.9	94	76	91	87	0.9	5.4	1.4	2.6	7.7	8.0	5.5	7.1
IX	1000.7	1012.4	984.7	1017.8	19.4	8.5	28.6	2	0.3	25	10.7	18.8	12.7	13.7	12.6	13.6	13.3	13.2	95	62	88	82	0.8	8.7	1.9	3.8	4.9	4.7	4.0	4.5
X	1000.2	1012.7	971.7	1017.5	14.1	8.0	19.8	6	3.6	14	8.9	13.5	10.4	10.8	10.7	11.4	11.1	11.1	93	74	88	85	0.8	4.3	1.6	2.2	7.1	6.9	5.1	6.4
XI	996.3	1018.6	977.0	1014.0	6.0	1.7	10.7	2	-8.4	23	3.0	5.3	3.5	3.8	7.4	7.6	7.4	7.5	95	85	92	91	0.4	1.4	0.7	0.8	9.0	8.4	8.2	8.5
XII	997.3	1029.0	968.0	1015.4	-0.2	-6.5	13.3	5	-22.5	26	-4.0	-1.4	-3.6	-3.2	4.7	5.2	4.6	4.8	90	86	89	88	0.5	0.8	0.6	0.6	6.7	7.4	6.5	6.9
Rok	997.9	1029.0	968.0	1015.3	11.9	4.4	31.8	3.VII	-22.5	26. XII	6.5	10.6	7.5	8.0	9.6	10.0	9.8	9.8	90	74	87	84	1.1	4.5	1.6	2.4	7.2	7.3	6.2	6.9

Ślinice

$\varphi = 53°43'$ $\lambda = 18°11'$

I	–	–	–	–	0.4	-6.3	4.8	31	-21.0	26	-4.9	-0.9	-3.6	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	5.9	6.7
II	–	–	–	–	4.4	-0.5	15.3	18	-7.4	5	0.5	3.2	1.3	1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.2	7.8	8.4
III	–	–	–	–	9.3	1.5	18.2	10	-6.4	20	3.2	7.7	4.3	4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	6.0	6.9
IV	–	–	–	–	15.1	2.5	24.7	14	-5.0	11	5.7	13.4	7.2	8.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.0	3.5	4.3
V	–	–	–	–	16.3	5.5	25.7	30	0.5	13	9.4	14.6	9.3	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	8.4	7.5	7.6
VI	–	–	–	–	24.4	11.5	29.6	10	5.4	1	16.2	22.7	16.8	18.1	–	–	–	–	–	–	–	–	–	–	–	–	4.2	6.0	5.1	5.1
VII	–	–	–	–	20.7	11.0	33.2	3	6.4	1	14.2	18.7	14.7	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.0	7.7	7.7
VIII	–	–	–	–	20.3	11.1	28.6	6	7.3	14	13.3	18.6	14.2	15.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.6	5.8	7.0
IX	–	–	–	–	20.5	8.2	30.1	2. 3	0.1	28	10.0	19.0	12.2	13.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.9	3.8	4.4
X	–	–	–	–	14.6	6.9	19.5	5. 6	2.6	31	8.1	13.7	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	4.2	5.8
XI	–	–	–	–	6.0	0.8	10.2	2	-9.8	23	2.4	4.8	2.8	3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.3	7.9	8.5
XII	–	–	–	–	0.1	-7.2	13.5	5	-21.3	17	-3.9	-1.6	-4.4	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.5	5.4	6.5
Rok	–	–	–	–	12.7	3.8	33.2	3.VII	-21.3	17.XII	6.2	11.2	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.0	5.9	6.6

Chojnice

$\varphi = 53°42'$ $\lambda = 17°33'$

I	996.2	1021.6	974.6	1018.7	-0.2	-5.0	5.5	30	-17.6	26	-3.8	-1.2	-2.6	-2.6	5.4	4.8	4.6	4.6	89	82	85	85	0.4	0.9	0.7	0.7	6.7	7.1	6.3	6.7
II	998.1	1015.0	969.3	1020.3	3.7	-0.1	11.8	18	-6.7	5	0.6	2.7	1.3	1.5	6.1	6.8	6.3	6.4	95	90	93	93	0.3	0.8	0.4	0.5	9.3	9.0	7.8	8.7
III	–	–	–	–	8.2	1.7	16.5	10	-5.2	20	3.1	7.0	4.0	4.5	7.0	7.1	7.2	7.1	91	71	87	83	0.7	3.2	1.1	1.7	8.9	8.2	6.8	8.0
IV	–	–	–	–	14.1	3.6	23.2	14	-2.0	2. 10	5.7	12.6	7.9	8.5	7.4	7.8	7.9	7.7	79	54	72	68	2.0	7.7	3.2	4.3	4.9	5.7	4.5	5.0
V	–	–	–	–	15.4	6.1	24.9	30	0.6	2	9.0	13.7	9.3	10.4	9.8	10.1	9.8	9.9	85	65	83	78	1.8	6.0	2.1	3.3	7.5	8.5	6.0	7.3
VI	993.3	1006.1	981.4	1014.1	22.6	12.0	27.9	2	6.2	22	15.7	21.0	16.1	17.2	14.3	13.6	14.2	14.0	80	56	78	71	3.8	12.0	4.4	6.7	5.3	6.7	5.7	5.9
VII	990.6	1005.3	974.6	1011.6	19.3	10.6	31.6	3	5.3	6	13.7	17.6	14.1	14.9	14.3	14.2	14.3	14.3	90	73	88	84	1.6	6.6	2.0	3.4	8.4	8.3	7.4	8.0
VIII	993.4	1008.1	979.9	1014.5	18.9	10.9	26.4	6	7.0	14	13.2	17.5	13.5	14.4	14.4	14.9	14.2	14.5	94	75	91	87	0.9	5.5	1.5	2.6	8.8	8.5	6.4	7.8
IX	996.8	1008.9	981.1	1018.0	19.1	9.3	27.2	2	2.4	27	10.9	18.2	12.4	13.5	12.6	13.8	13.1	13.2	94	66	89	83	0.8	7.6	1.6	3.3	4.4	5.0	4.4	4.6
X	996.6	1008.9	969.1	1018.1	13.7	7.4	18.4	5	2.3	31	8.4	12.9	9.8	10.2	10.5	11.4	10.8	10.9	95	77	89	87	0.6	3.7	1.4	1.9	7.6	7.3	5.1	6.7
XI	992.1	1014.1	974.1	1013.9	5.5	1.2	9.8	1	-5.4	23	2.7	4.7	3.0	3.4	7.1	7.4	7.0	7.2	92	85	91	89	0.6	1.3	0.7	0.9	9.2	8.6	8.1	8.6
XII	992.9	1023.8	964.8	1015.2	-0.9	-6.5	12.4	5	-19.0	26	-4.0	-2.0	-4.0	-3.5	4.4	4.9	4.3	4.5	86	85	85	85	0.6	0.8	0.7	0.7	6.7	7.0	5.7	6.5
Rok	–	–	–	–	11.6	4.3	31.6	3.VII	-19.0	26.XII	6.3	10.4	7.1	7.7	9.4	9.7	9.5	9.5	89	73	86	83	1.2	4.7	1.6	2.5	7.3	7.5	6.2	7.0

Prabuty $H_s = 98\,m$ $h_w = 12\,m$ 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	4	2.4	5	3.4	2	2.5	1	3.0	13	4.2	27	4.0	15	2.4	13	2.3	13	2.8	25.4	11.7	11	10	12	24	·	2	·	4	15	12	2	2	4	—	·
II	5	2.2	1.5	2.0	1	2.0	3	4.3	12.5	6.5	23.5	3.9	17	2.0	12.5	3.1	8	3.2	43.1	10.7	11	·	1	16	·	3	·	·	20	12	7	1	17	—	·
III	5	3.2	·	·	·	·	·	·	1	10.0	14	5.9	45	4.1	23	4.3	5	4.2	23.6	4.5	20	·	·	9	·	6	2	2	10	15	10	·	4	—	·
IV	10	1.6	15	3.6	5.5	4.0	9.5	5.8	8	4.1	8	2.9	11	2.5	9	1.6	14	2.7	19.8	5.7	1	·	·	10	·	2	·	9	3	8	7	·	5	·	2
V	25	4.4	4	3.2	1	4.0	2	3.0	5.5	4.5	20.5	4.1	12	3.1	6	2.2	17	3.1	89.2	19.5	6	·	·	·	·	1		1	11	15	14	2	4	·	6
VI	10	1.6	7	2.1	4	2.8	5.5	3.5	9.5	3.4	10	4.8	30	3.3	7	2.6	7	2.9	54.9	26.0	15		·	·	12	·	·	7	2	8	8	2	2	·	5
VII	7	2.0	·	·	1	3.0	2	3.5	3	3.0	28	3.6	28	3.0	11	2.7	13	2.7	101.0	21.2	28	·		·	3	·	·	2	15	20	16	3	·	·	7
VIII	4	1.5	·	·	·	·		·	2	2.0	29	3.6	34	2.3	12	2.2	12	2.4	66.7	11.0	1		·	·	3	1	·	2	7	21	16	1	9	·	5
IX	5	2.0	3	2.0	5	3.4	3	4.0	5.5	3.4	14.5	4.7	29	2.1	6	1.5	19	2.2	45.1	24.5	14	·	·		4	1		11	4	10	5	2	3	·	3
X	1	3.0	·	·	12	3.1	2.5	6.2	12	4.0	20	4.2	9	2.0	5	2.2	9	3.8	27.0	6.2	24	·	·	·	·	1		5	9	9	7	·	7	·	·
XI	8	2.7	7	5.9	7	3.9	7	3.6	6	2.8	20	4.1	17	2.9	9	3.3	9	3.3	38.5	8.0	11		1	13	·	·	·	·	17	15	11	·	9	1	·
XII	6	4.5	10	4.2	·	·	·	·	14.5	3.1	24.5	5.0	19	5.6	10	2.0	9	3.9	33.1	6.8	4	12	14	24		4	1	6	10	12	9	·	8	16	·
Rok	90	2.6	52.5	2.2	38.5	2.4	58	3.1	92.5	4.2	239	4.2	266	2.9	123.5	2.5	135	3.1	562.4	26.0	15. VI	22	28	96	22	21	3	49	123	157	112	13	72	—	28

Szczecinek $H_s = 137\,m$ $H_b = 142{,}6\,m$ $h_w = 12\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	0.5	2.0	5.5	2.4	4	2.4	7	3.4	30.5	2.7	25.5	3.7	9.5	2.2	4.5	2.1	6	2.7	35.6	14.0	30	8	11	24	·	·	·	6	12	15	8	1	4	11	·
II	1.5	5.3	·	·	·	·	5.5	3.5	19.5	3.2	28.5	2.6	14	3.4	8	3.2	7	2.8	42.1	9.4	27	·	·	12	·	·	·	1	20	18	8	·	14	3	·
III	0.5	7.0	·	·	·	·	·	·	2	4.8	24	4.0	49	4.7	16.5	5.3	1	4.6	47.0	11.0	29	·	·	4	·	3		1	18	20	13	1	4	4	·
IV	2	1.0	7	2.6	12.5	3.1	18	3.3	9	2.4	11	2.3	9.5	2.5	8	2.8	13	2.4	16.3	3.0	8	·	·	7	·	·	·	6	7	10	6	·	·	4	1
V	13.5	3.7	8.5	3.4	1.5	2.0	3	3.5	10.5	2.8	16	3.1	14	3.1	18	3.4	8	3.0	67.5	15.6	5	·	·	1	·	·	·	·	13	15	10	2	1	·	6
VI	3	2.3	·	·	3	2.7	6.5	3.8	7.5	3.1	16.5	3.1	27	4.7	7.5	3.8	19	3.0	43.8	8.6	15	·	·	·	9	·	·	2	5	14	10	·	1	·	8
VII	2	1.0	·	·	2	2.5	2	3.5	7	3.1	43	3.7	24.5	3.3	8.5	3.6	4	3.3	137.0	39.3	31	·	·	·	4	·	·	2	21	25	20	5	1	·	5
VIII	1	1.5	2	3.2	3	1.7	2	3.3	4	3.7	32	3.2	27	3.7	5	4.2	17	2.8	78.7	17.2	19	·	·	·	2	·	·	1	8	21	15	2	5	·	2
IX	0.5	3.0	·	·	3	1.0	15	3.2	9	2.2	22	2.8	18	3.2	2.5	3.6	20	2.2	37.3	16.6	7	·	·	·	4	·	·	10	8	10	5	2	6	·	3
X	·	·		·	7	4.1	19.5	4.0	26.5	3.8	20.5	2.9	11	2.5	3.5	3.5	5	3.3	31.0	6.6	31	·	·	·	·	·	·	5	11	13	9	·	5	·	·
XI	2.5	3.8	7.5	5.8	6.5	5.0	3.5	2.7	14	2.5	27	4.0	12.5	2.8	5.5	3.2	11	3.2	25.9	8.2	30		·	7	·	·	·	2	21	16	8	·	8	·	·
XII	3	6.5	8.5	2.5	5.5	1.5	4.5	2.2	18.5	2.1	20	4.5	20.5	3.7	5.5	3.4	7	3.0	34.1	7.4	4	10	13	24	·	5	·	3	15	14	7	·	8	19	·
Rok	30	3.1	39	1.7	48	2.2	86.5	3.0	158	3.0	286	3.3	236.5	3.3	93	3.5	118	3.0	596.3	39.3	31. VII	18	24	79	19	8	·	39	159	191	119	13	57	41	25

Śliwice $H_s = 115\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	2	2.5	7.5	1.9	3.5	2.7	16.5	1.5	23	1.7	27.5	2.6	6.5	2.7	1.5	2.0	5	2.0	26.0	13.5	30	11	10	27	·	·		3	14	10	6	1	—	9	·
II	1	2.0	3	2.0	1	1.0	10	2.0	25	2.5	20	1.8	16	3.0	6	1.5	2	2.2	39.2	9.8	27		·	13	·	1	·	1	18	12	8	·	7	4	
III	·	·	·	·	·	·	·	·	6	2.6	36.5	3.1	30.5	4.4	20	5.5		4.0	32.5	11.2	27	·	·	8	·	8	·	2	15	11	7	1	1	3	·
IV	4	1.8	15	2.3	6	3.7	28.5	2.0	9	1.8	12	1.7	9.5	3.0	2	4.0	4	2.1	18.0	7.6	1	·	·	9	·	·	·	8	2	7	5	·	·	·	2
V	12	2.6	9	2.9	2	2.0	7	2.8	13.5	1.7	24.5	2.2	15	2.7	6	2.8	4	2.3	62.8	18.0	6		·	·	1	1		·	12	13	10	2	·	·	7
VI	3	1.7	4	2.1	3	1.5	11.5	2.0	10	1.3	32.5	2.1	17.5	2.8	4.5	3.6	4	2.1	40.4	13.7	14	·	·		14	·		4	4	10	7	1	·	·	8
VII	·	·	2	1.5	·	·	6	1.5	6	1.1	67	1.6	8	2.5	2	2.5	2	1.6	118.5	23.8	31	·	·	·	5			2	17	21	15	4	·		7
VIII	3	1.0	4	1.5	1	1.0	2	1.5	9.5	1.2	52	1.7	15.5	2.5	1	3.0	5	1.6	63.5	14.7	1	·	·	·	3	·	·	1	12	22	15	2	3	·	3
IX	2	1.5	5	1.4	7	1.7	13	1.5	7.5	1.3	37	1.6	12.5	2.4	·	·	6	1.6	47.0	16.2	14	·	·	·	4	·		12	6	10	9	1	4	·	5
X	·	·	·	·	3	1.3	32	2.0	26	1.3	20.5	1.8	5.5	2.4	3	2.7	3	1.7	37.6	12.2	18	·	·	·	·			7	10	13	9	1	5	·	·
XI	4	2.2	9.5	3.0	6.5	3.0	15	1.6	8	1.6	36	2.4	4	1.2	4	2.0	3	2.1	26.7	5.5	8	·		12	·	·		2	23	12	11	·	7	·	·
XII	4	3.0	5	1.6	9	1.3	11	1.5	13	1.3	31	3.4	11	2.0	6	2.7	3	2.2	33.3	2.4	2	11	13	25	·	2	·	2	15	12	8	·	2	14	
Rok	35	1.5	64	1.7	42	1.6	152.5	1.7	156.5	1.6	396.5	2.2	151.5	2.6	56	2.7	41	2.1	545.5	23.8	31. VII	22	23	94	27	12	·	44	148	153	110	13	—	30	32

Chojnice $H_s = 172\,m$ $H_b = 177{,}2\,m$ $h_w = 12{,}5\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◉	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	1.5	2.3	6.5	2.6	6.5	2.4	19.5	2.4	19	2.5	22	5.2	10.5	3.1	7.5	3.6	·	3.3	24.5	9.3	30	6	11	23		3	·	3	15	14	6		9	15	
II	2	3.5	1	3.0	0.5	2.0	15.5	3.4	9.5	3.6	19	4.2	16	4.1	13.5	3.4	7	3.4	35.8	8.7	28	·		10		2		1	21	14	7	·	14	5	·
III	1	6.0	·	·	·	·		·	·	·	12.5	5.2	32.5	6.7	40	6.7	2	6.4	25.6	4.7	29	·		9		17	2	1	18	17	10		6	4	
IV	1	2.5	13	2.8	23.5	3.1	17.5	3.3	4	2.1	7.5	3.5	5	5.5	14.5	3.2	4	3.2	25.9	5.6	28	·	·	7		3	1	7	7	11	8		1	5	1
V	17.5	3.5	13	2.6	2.5	1.6	4.5	3.0	9	3.3	14	4.5	15	4.0	12.5	4.3	5	2.4	59.2	13.6	5	·		·	·	·	·		13	14	9	3	3	·	4
VI	1	3.0	9.5	2.4	11.5	3.0	8	3.7	4	3.0	10.5	4.8	27	5.4	16.5	3.8	2	4.0	90.7	47.1	7	·	·		10	3	·	3	8	13	10	2			9
VII	·	·	-	·	2.5	3.2	5.5	2.4	5.5	1.9	37.5	4.2	27.5	4.2	9.5	3.4	5	3.6	145.9	27.1	13	·	·	·	4	1	·	2	19	25	18	5	1		8
VIII	1	1.5	3.5	1.7	1	3.0	4	1.8	3	2.3	32.5	3.6	27	4.4	12	4.0	9	3.3	77.9	19.7	6	·		·	2	3		1	15	22	14	3	3		2
IX	·	·	5	1.2	18.5	2.9	9	2.8	4.5	2.2	18	3.6	18	3.9	10	2.8	7	2.9	30.2	10.9	14	·		·	4	1		11	9	11	6	1	2	·	1
X	0.5	6.0	1.5	1.0	20.5	4.1	22	3.3	16	2.6	15	3.5	4.5	3.1	10	4.0	3	3.3	40.4	11.6	19	·	·	·	·	·		5	14	11	9	1	9	·	·
XI	5	1.5	11	4.4	10	3.6	7	2.7	5.5	3.2	23.5	4.6	12.5	3.8	7.5	2.9	8	3.4	26.0	4.9	17	·	·	11	·	2		1	20	19	9	·	10	·	·
XII	1.5	1.7	8.5	2.9	6	1.7	14	2.5	6.5	1.7	20	5.7	14	6.8	17.5	4.5	5	4.0	26.8	2.4	4	11	16	25	·	7	1	5	14	12	5	·	7	14	
Rok	32	2.6	72.5	2.0	103	2.6	126.5	2.6	86.5	2.4	232	4.4	214.5	4.6	171	3.9	57	3.6	607.9	47.1	7. VI	17	27	85	20	42	4	40	173	183	111	15	65	43	25

Ostróda — φ = 53°42' — λ = 19°58' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.2	−5.7	5.9	4, 5	−20.9	26	−4.3	−1.3	−2.8	−2.8	4.3	4.7	4.6	4.5	86	80	84	83	0.5	1.0	0.7	0.7	6.5	6.8	5.8	6.4
II	–	–	–	–	3.0	−0.4	10.7	18	−3.5	5	0.6	2.2	1.3	1.4	5.8	6.3	6.0	6.0	90	86	88	88	0.6	1.0	0.8	0.8	8.7	8.4	8.2	8.4
III	–	–	–	–	8.3	1.3	16.3	10	−6.7	20	3.1	6.7	4.2	4.6	6.5	6.5	6.7	6.6	85	68	81	78	1.2	3.5	1.7	2.1	7.6	6.3	6.0	6.6
IV	–	–	–	–	14.5	3.4	23.0	7	−2.5	12	6.0	13.2	8.2	8.9	7.2	7.2	7.7	7.4	75	47	69	64	2.5	8.9	3.6	5.0	3.8	3.9	3.5	3.7
V	–	–	–	–	16.2	6.6	24.5	30	1.7	19, 23	9.7	14.3	10.2	11.1	10.4	11.0	10.6	10.7	86	67	85	79	1.8	5.9	2.1	3.3	7.2	7.1	6.6	7.0
VI	–	–	–	–	24.0	12.6	31.9	27	6.9	21	16.2	22.1	16.6	17.9	14.8	14.2	14.6	14.5	80	54	77	70	3.8	13.0	4.5	7.1	5.8	4.8	4.8	5.1
VII	–	–	–	–	20.3	11.3	31.4	3	7.4	6	14.4	18.6	14.7	15.6	14.1	14.7	14.0	14.3	86	69	84	79	2.4	7.3	3.0	4.2	8.0	6.9	8.0	7.6
VIII	–	–	–	–	19.4	11.1	28.2	6	8.0	14	13.6	17.7	14.5	15.1	13.7	14.6	14.3	14.2	88	73	86	82	2.0	6.1	2.4	3.5	7.2	6.5	5.9	6.5
IX	–	–	–	–	19.4	8.8	27.6	3	1.7	24	10.8	18.3	12.4	13.5	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.4	4.8	4.8
X	–	–	–	–	14.8	6.9	19.5	4	2.5	23	8.2	14.0	10.3	10.7	9.7	11.3	10.3	10.4	89	72	82	81	1.3	4.9	2.4	2.9	7.2	5.5	5.5	6.1
XI	–	–	–	–	5.5	1.1	10.7	3	−6.1	23	2.5	4.3	3.1	3.2	6.9	7.5	7.0	7.1	91	88	88	89	0.6	1.0	0.9	0.8	8.5	8.3	7.8	8.2
XII	–	–	–	–	−0.7	−7.3	13.2	5	−24.3	27	−4.7	−2.8	−4.4	−4.1	4.2	4.6	4.2	4.3	83	79	82	81	0.7	1.0	0.8	0.8	7.7	6.3	5.2	6.4
Rok	–	–	–	–	12.0	4.1	31.9	27. VI	−24.3	27. XII	6.3	10.6	7.4	7.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	6.0	6.4

Trzebież — φ = 53°40' — λ = 14°31'

I	–	–	–	–	1.2	−3.6	6.7	30	−15.0	27	−2.3	0.3	−1.3	−1.2	5.0	5.3	5.2	5.2	90	80	88	86	0.5	1.2	0.6	0.8	6.7	6.3	5.9	6.3
II	–	–	–	–	6.7	0.6	13.0	27	−3.6	5	1.9	5.3	3.2	3.4	6.8	7.8	7.3	7.3	96	87	94	92	0.3	1.3	0.5	0.7	9.0	8.0	8.2	8.4
III	–	–	–	–	10.0	2.7	17.7	10	−4.5	20	4.4	8.3	6.0	6.2	7.5	7.7	7.9	7.7	88	70	84	81	1.1	3.6	1.6	2.1	8.6	7.8	6.0	7.5
IV	–	–	–	–	14.2	5.2	24.8	14	−1.2	1	7.3	12.4	9.6	9.7	8.3	9.0	9.0	8.8	79	63	75	72	2.2	6.2	3.3	3.9	5.1	5.7	4.8	5.2
V	–	–	–	–	14.3	6.9	22.0	5	3.2	29	9.6	12.7	10.1	10.6	10.5	11.2	10.6	10.8	87	76	85	83	1.5	3.7	1.9	2.4	7.7	7.7	6.8	7.4
VI	–	–	–	–	21.3	11.8	27.9	26	7.7	22	15.7	19.8	16.2	17.0	14.7	14.9	15.2	14.9	82	65	82	76	3.5	8.4	3.5	5.1	4.7	6.3	4.1	5.0
VII	–	–	–	–	19.7	11.5	31.6	3	8.3	1, 6	14.6	17.9	15.0	15.6	14.7	14.7	14.6	14.7	88	71	86	82	2.0	6.1	2.7	3.6	7.0	8.0	6.6	7.2
VIII	–	–	–	–	19.6	11.0	25.8	31	8.0	8	13.8	17.8	14.5	15.1	14.7	15.4	14.8	15.0	93	76	89	86	1.2	5.2	1.9	2.8	6.9	7.4	5.7	6.7
IX	–	–	–	–	20.0	10.3	28.3	17	0.8	27	12.0	19.0	14.0	14.8	13.3	14.8	14.3	14.1	93	67	88	83	1.1	7.5	2.0	3.5	3.8	4.3	2.8	3.6
X	–	–	–	–	15.0	7.8	21.7	6	3.3	14	9.3	14.3	10.7	11.2	10.7	11.5	11.5	11.2	92	71	89	84	1.1	5.1	1.6	2.6	5.4	5.5	4.9	5.3
XI	–	–	–	–	6.8	1.8	12.3	1	−6.4	22	3.6	6.1	4.2	4.5	7.6	8.1	7.7	7.8	94	85	91	90	0.6	1.5	0.8	1.0	8.0	7.4	6.8	7.4
XII	–	–	–	–	1.0	−5.3	14.8	5	−20.8	26	−2.9	−0.5	−2.1	−1.9	5.0	5.5	5.1	5.2	91	85	90	89	0.5	0.9	0.6	0.7	6.1	5.8	6.2	6.0
Rok	–	–	–	–	12.5	5.1	31.6	3. VII	−20.8	26. XII	7.2	11.1	8.3	8.7	9.9	10.5	10.3	10.2	89	75	87	84	1.3	4.2	1.8	2.4	6.6	6.7	5.7	6.3

Nowogard — φ = 53°40' — λ = 15°07'

I	–	–	–	–	0.8	−4.9	6.1	29	−16.1	26, 27	−2.8	0.0	−2.3	−1.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	5.9	−0.2	12.1	27	−5.3	5	1.5	4.5	2.4	2.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	9.3	2.0	17.2	10	−3.7	20	4.0	8.1	5.3	5.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.0	4.1	24.8	14	−1.0	1	7.2	13.5	8.9	9.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	14.6	6.4	22.7	26	1.6	29	9.4	13.2	9.5	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	22.7	11.7	27.7	5, 10	6.3	22	16.2	20.9	15.8	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.1	11.7	31.2	2, 3	7.3	1	14.4	18.3	14.6	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.1	11.0	26.9	31	7.5	8	13.7	18.2	13.8	14.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.7	9.8	28.4	2	1.0	27	11.8	19.6	12.8	14.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.0	7.5	21.7	6	2.9	31	9.1	14.2	10.1	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.6	1.5	11.1	1, 2, 3	−6.6	22	3.0	5.8	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	0.8	−6.1	13.7	5	−19.5	17	−3.8	−1.3	−3.0	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.6	4.5	31.2	2.3. VII	−19.5	17. XII	7.0	11.2	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biebrza — φ = 53°39' — λ = 22°36'

I	–	–	–	–	−1.2	−7.0	5.5	4	−23.2	26	−4.9	−2.2	−3.4	−3.5	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.7	7.6	8.4
II	–	–	–	–	2.4	−2.1	11.9	18	−7.4	5	−0.5	1.3	0.1	0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.0	9.0	9.2
III	–	–	–	–	7.8	−0.1	15.5	10	−7.1	20	2.0	6.8	3.2	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.5	7.9	8.0
IV	–	–	–	–	13.6	0.4	24.0	15	−5.6	11	4.8	12.6	5.9	7.3	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.2	4.1	4.8
V	–	–	–	–	16.6	5.8	25.6	30	−0.5	15	9.8	15.1	9.7	11.1	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.4	7.9
VI	–	–	–	–	23.0	10.8	28.8	10	4.3	21	15.5	21.6	15.4	17.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.2	6.2	6.6
VII	–	–	–	–	20.8	10.1	29.4	2	4.9	6	14.1	19.7	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	7.5	7.4
VIII	–	–	–	–	20.2	10.6	28.3	6	3.1	18	13.5	19.0	13.5	14.9	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.2	7.0	7.5
IX	–	–	–	–	19.3	5.4	27.8	3	−3.7	24	9.8	18.1	10.5	12.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.7	4.4	5.6
X	–	–	–	–	13.9	5.1	19.1	4	−0.6	23	6.6	12.9	8.7	9.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.5	5.5	6.3
XI	–	–	–	–	4.7	0.7	12.2	2	−8.5	29	2.0	3.7	2.7	2.8	–	–	–	–	–	–	–	–	–	–	–	–	9.2	9.1	8.4	8.9
XII	–	–	–	–	−1.6	−9.3	13.5	5	−27.1	27	−5.5	−3.0	−5.5	−4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.0	4.8	6.3
Rok	–	–	–	–	11.6	2.5	29.4	2. VII	−27.1	27. XII	5.6	10.5	6.3	7.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	6.6	7.2

Ostróda

$H_s = 106\,m$ $h_w = 10\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (fD, fmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Max<-10°	Max<0°	Min<0°	Min>25°	Wiatr v ≥10	v ≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	≋	⊞	≈
I	3.5	2.0	3	2.3	3.5	2.9	11.5	3.9	5.5	2.6	38	5.1	13	4.1	5	4.2	10	3.8	13.5	9.2	30	8	12	25	.	1	1	3	12	6	3	.	3	2	.
II	.	.	1	4.0	0.5	5.0	15.5	4.2	11	3.2	26.5	3.8	25.5	3.4	3	3.0	1	3.6	25.0	6.2	11	.	.	16	.	.	.	1	18	10	7	.	10	.	.
III	.	.	.	.	.	.	.	.	0.5	3.0	26.5	4.1	5.4	5.5	12	6.2	.	5.2	23.9	6.4	28	.	.	10	.	3	.	2	11	12	8	.	3	.	.
IV	2.5	3.0	6.5	2.5	16.5	3.6	18	4.2	4	2.4	22	3.2	9	5.4	8.5	4.8	3	3.6	16.8	4.8	1	.	.	9	.	3	1	8	3	9	4	.	1	5	2
V	3	3.0	1	2.0	5	3.3	9	3.5	9	3.9	22	3.3	28.5	3.4	14.5	4.1	1	3.5	58.1	11.2	6	.	.	.	.	.	.	.	10	18	12	1	1	.	5
VI	3.5	2.9	1	3.0	11	3.0	12.5	2.6	7	3.4	22	3.7	26	4.4	4	3.1	3	3.4	48.8	14.6	14	.	.	.	13	.	.	4	5	8	6	2	.	.	5
VII	.	.	1	2.0	0.5	7.0	4.5	2.8	8	2.2	39.5	3.8	34.5	3.2	3	3.8	2	3.3	103.1	16.7	13	.	.	.	4	.	.	.	13	22	18	3	1	.	5
VIII	3	2.3	4	2.2	1.5	2.0	0.5	2.0	5.5	3.6	36	4.0	29.5	4.0	9	2.3	4	3.5	86.3	20.4	2	.	.	.	2	.	.	.	11	17	15	2	1	.	1
IX	1.5	2.0	5	2.8	5	3.0	11.5	3.0	6.5	2.6	28.5	3.5	20	3.3	4	3.0	8	2.9	32.2	12.8	14	.	.	.	4	.	.	7	5	6	5	2	2	.	1
X	.	.	.	.	13.5	3.9	38.5	3.6	14.5	3.0	15	2.8	8.5	3.1	1	4.5	2	3.3	7.7[2]	2.1	18, 24	.	.	.	.	.	.	3	6	6	3	.	4	.	.
XI	3.5	2.0	7	2.8	6.5	4.3	16	3.2	12.5	3.4	25.5	3.1	10.5	3.4	3.5	2.0	5	3.0	50.8	9.6	19	.	1	13	.	.	.	1	19	12	9	.	6	.	.
XII	8	3.4	4	1.8	1	2.0	1.3	2.8	5	2.0	3.4	3.2	16	4.3	7	3.8	5	3.1	32.9	10.2	4	10	13	24	.	1	.	3	12	11	7	1	3	–	.
Rok	28.5	1.7	33.5	2.1	64.5	3.3	150.5	3.0	89	2.9	335.5	3.6	27.5	4.0	74.5	3.7	44	3.5	499.1[2]	20.4	2. VIII	18	26	97	23	8	2	32	125	137	97	11	35	–	19

Trzebież

$H_s = 1\,m$ $h_w = 18\,m$

I	2.5	4.4	3.5	2.7	7	4.1	19.5	5.0	18.5	4.1	19.5	5.8	11	2.7	7.5	5.4	4	4.3	35.3	9.4	10	3	10	21	.	3	.	9	17	14	9	.	2	5	.
II	0.5	10.0	1.5	3.0	2	3.2	10.5	5.1	9.5	4.3	24	4.7	14.5	3.2	15.5	3.2	6	3.8	47.6	10.3	27	.	.	9	.	3	.	.	18	13	9	1	8	1	.
III	1.5	1.5	.	.	.	.	.	.	.	.	16	7.1	50.5	6.7	24	7.5	1	7.0	38.9	6.8	20	.	.	7	.	11	2	2	16	16	11	.	2	2	.
IV	10	4.9	10	3.8	9	5.1	29.5	5.2	5.5	4.2	7	4.4	4.5	3.3	12.5	5.1	2	4.7	34.1	13.3	28	.	.	1	.	2	.	6	7	9	7	1	.	.	1
V	2.1	6.4	8	6.3	1	4.0	9	4.2	4	4.8	14	3.5	16.5	4.2	17.5	6.4	2	5.1	105.6	17.9	30	.	.	.	.	5	.	1	15	21	19	4	.	.	4
VI	10.5	4.4	8	3.1	1	3.0	4	3.2	6.5	4.2	13	4.9	25	5.8	18	5.0	4	4.6	54.9	15.7	13	.	.	.	4	2	.	3	4	8	7	3	1	.	1
VII	1.5	2.7	4	1.8	1	6.0	2	3.5	0.5	6.0	3.6	4.7	3.2	4.8	10	7.0	6	4.5	74.6	14.2	31	.	.	.	3	3	.	2	13	17	13	4	.	.	1
VIII	4.5	2.4	0.5	4.0	.	.	6.5	2.8	3.5	4.6	21.5	5.4	32.5	4.3	14	4.6	10	4.0	75.0	14.3	11	.	.	.	1	1	.	2	9	19	16	1	2	.	2
IX	2	2.2	1.5	2.7	3	3.3	2.5	3.7	4.5	4.3	16	4.3	15	4.4	9	4.2	14	3.4	36.4	19.2	7	.	.	.	3	.	.	13	5	7	5	1	2	.	1
X	1	5.0	.	.	4	6.6	3.1	5.9	1.7	4.8	15	4.4	9	5.2	7	3.9	9	4.7	41.1	15.0	20	.	.	.	.	2	.	8	9	8	7	1	2	.	.
XI	4.5	5.0	6	6.8	9.5	6.5	9.5	2.4	8.5	3.4	21.5	5.4	12.5	5.4	3	3.0	15	4.1	24.7	7.8	30	.	.	6	.	2	.	3	18	11	9	.	5	.	.
XII	4	9.2	2	8.5	5.5	5.3	13	3.9	14	4.3	24	6.0	12.5	5.3	4	5.4	14	4.6	57.2	16.0	11	9	12	21	.	2	2	6	12	14	9	2	5	15	.
Rok	63.5	4.8	4.5	3.6	43	3.9	159.5	3.7	92	4.1	227.5	5.0	235.5	4.6	142	5.1	87	4.6	625.4	19.2	7. IX	12	22	65	11	36	4	55	143	157	121	18	29	23	10[2]

Nowogard

$H_s = 60\,m$ $h_w = 11\,m$

I	1	4.0	4	1.0	4	2.5	16	1.8	23	3.7	22	3.5	9	1.4	9	3.4	5	2.7	43.6	7.0	29	6	9	26	.	.	.	–	–	15	12	.	2	3	.
II	1	1.0	.	.	.	.	.	.	3.0	2.8	4.0	2.5	1.3	1.3	.	.	.	2.4	63.2	12.5	9	.	.	14	.	.	.	–	–	16	9	3	–	1	.
III	2	2.0	.	.	.	.	.	.	8	2.9	2.8	4.8	3.6	2.8	1.8	4.9	1	3.8	53.6	9.5	28	.	.	8	.	1	.	–	–	15	13	.	–	.	.
IV	3	4.7	.	.	1	2.0	2.3	5.4	2.2	4.0	10	3.1	1.8	2.6	11	3.3	2	3.8	26.0	7.0	1	.	.	3	.	.	.	–	–	11	7	.	.	.	1
V	2.5	3.5	3	2.3	2	5.0	3	4.3	1.5	3.4	1.5	3.6	1.5	3.4	10	3.8	5	3.4	123.2	25.0	9	.	.	.	.	.	.	–	–	20	18	4	2	.	4
VI	5	1.6	1	1.0	2	1.0	5	2.2	1.6	1.9	11	2.2	2.5	2.0	8	2.1	17	1.6	72.0	22.5	14	.	.	.	10	.	.	–	–	9	8	2	.	.	3
VII	1	1.0	1	1.0	2	1.0	1	3.0	2.4	2.8	1.5	2.2	4.0	2.1	6	2.0	3	2.2	111.8	27.5	9	.	.	.	4	.	.	–	–	22	16	3	.	.	3
VIII	2	1.0	.	.	.	.	2	1.0	1.4	3.0	2.1	2.6	3.7	1.8	1.1	2.5	6	2.0	120.7	26.5	3	.	.	.	2	.	.	–	–	22	20	2	.	.	4
IX	8	1.2	.	.	2	1.0	1.6	2.5	2.4	2.0	1.4	1.6	1.4	1.9	4	1.8	8	1.7	32.7	10.3	14	.	.	.	5	.	.	–	–	9	6	1	.	.	1
X	2	1.0	.	.	1	1.0	2.8	4.6	3.5	3.1	1.5	2.7	7	1.4	4	1.0	1	3.2	47.2	13.5	31	.	.	.	.	.	.	–	–	9	8	1	7	.	.
XI	11	2.4	3.5	2.7	5	5.0	9	2.6	17.5	2.5	20.5	3.4	11.5	3.0	3	1.7	9	2.6	31.9	9.0	30	.	.	7	.	.	.	–	–	16	10	.	7	.	.
XII	7.5	1.7	1	3.0	6	1.2	4	2.2	3.3	2.8	2.1	3.5	11.5	1.9	1	1.0	8	2.4	59.3	11.0	4	9	12	23	.	.	.	–	–	18	14	2	3	–	.
Rok	68.5	2.1	13.5	0.9	25	1.6	107	2.5	261.5	2.9	232.5	3.0	237	2.1	85	2.3	65	2.6	785.2	27.5	9. VII	15	21	81	21	1	.	–	–	182	141	18	–	–	16

Biebrza

$H_s = 1.17\,m$ $h_w = 12\,m$ I–IX, $13\,m$ X–XII

I	1.4	1.2	3	2.0	2	1.0	4	1.8	16.5	1.3	19.5	1.8	5	1.0	11	1.7	18	1.2	37.3	12.4	5	11	13	29[2]	.	.	.	–	–	15	9	1	1	29	–
II	9	1.6	3	1.0	4	1.0	8	1.9	7	1.9	9	1.6	9	1.7	7	1.0	28	1.0	24.4	5.6	27	.	5	22[2]	.	.	.	–	–	10	5	.	12	1[2]	–
III	5	2.6	.	.	1	1.0	1	4.0	.	.	1.5	3.5	3.6	5.1	2.1	5.3	14	3.9	25.0	6.4	12	.	.	14	.	4	1	–	–	11	7	.	3	2	–
IV	14	1.6	2	3.0	19	2.9	3	3.3	1	4.0	4	2.8	6	6.0	5	2.2	36	1.7	34.4	11.2	4	.	.	13	.	1	1	–	–	11	7	1	2	2	–
V	11	4.0	2	4.0	10	2.5	2	2.5	3	2.3	4	4.8	12	3.2	8	2.1	41	1.8	63.3	14.1	6	.	.	2	1	1	1	–	–	16	11	2	2	.	–
VI	7	1.0	2	1.5	3	1.3	.	.	2	2.5	7	3.7	2.2	3.3	8	1.9	39	1.5	110.9	23.2	28	.	.	.	11	1	.	–	–	14	10	6	1	.	–
VII	1	2.0	.	.	.	.	.	.	1	7.0	2	4.5	4.5	2.8	8	2.5	36	1.8	120.1	37.4	16	.	.	.	3	.	.	–	–	17	12	4	3	.	–
VIII	4	1.8	.	.	.	.	1	2.0	2	2.5	9	3.1	3.0	2.7	6	2.2	41	1.5	42.0	9.4	21	.	.	.	2	1	.	–	–	11	8	.	1	.	–
IX	2	1.5	1	1.0	3	2.0	4	1.8	4	1.2	8	3.8	11	2.1	9	3.0	48	1.1	27.5	14.6	14	.	.	7	4	.	.	–	–	6	6	1	6	.	–
X	.	.	.	.	1.0	1.8	2.9	3.3	8	2.6	12	2.9	6	1.7	.	.	2.8	1.9	6.7	3.0	26	.	.	1	.	.	.	–	–	4	3	.	10	.	–
XI	1	2.0	3	1.3	9	3.6	15	2.3	8	2.4	8	2.8	6	3.3	10	2.3	30	1.7	42.9	10.7	10	.	4	16	.	.	.	–	–	15	9	1	6	.	–
XII	10	7.6	3	4.3	2	2.5	10.5	4.8	19.5	4.4	17	5.2	12	5.2	4	5.0	15	4.3	23.2	8.0	2	11	16	27	.	5	3	–	–	9	5	.	1	17	–
Rok	7.6	2.2	1.9	1.5	63	1.6	77.5	2.3	72	2.7	114.5	3.4	200	3.2	97	2.4	374	2.0	552.7	37.4	16. VII	22	38	131[2]	21	13	6	–	–	139	92	16	48	51[2]	–

Pisz

$\varphi = 53°38'$ $\lambda = 21°48'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
										Średnia																		
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.5	−6.2	5.6	4	−22.7	26	−4.2	−1.5	−3.2	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.4	8.5	8.5
II	–	–	–	–	3.0	−1.2	13.3	18	−6.9	5	−0.2	2.4	0.7	0.9	–	–	–	–	–	–	–	–	–	–	–	–	9.4	9.1	8.5	9.0
III	–	–	–	–	8.6	0.3	17.4	10	−5.9	20	2.5	6.8	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.6	6.4	7.5
IV	–	–	–	–	14.7	1.9	24.2	15	−5.7	21	5.6	13.3	7.4	8.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	4.4	5.2
V	–	–	–	–	16.9	6.3	26.6	28	0.7	23	9.9	15.4	10.0	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.8	8.0	7.9
VI	–	–	–	–	23.5	11.3	31.8	27	5.7	2	16.1	22.0	16.2	17.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	6.3	6.5
VII	–	–	–	–	21.1	10.5	31.5	3	6.6	6	14.1	19.5	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.7	8.2	7.8
VIII	–	–	–	–	20.3	11.1	29.1	6	5.5	18	13.8	19.0	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	7.5	7.6
IX	–	–	–	–	19.5	6.6	28.8	3	−2.0	24	9.5	18.6	11.0	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	5.2	5.5
X	–	–	–	–	14.2	6.1	19.8	4	1.0	23	7.3	13.6	9.3	9.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	7.2[3]	7.3[3]
XI	–	–	–	–	4.9	0.3	11.6	2	−8.1	24	2.1	4.1	2.6	2.8	–	–	–	–	–	–	–	–	–	–	–	–	9.5	9.0	8.3	8.9
XII	–	–	–	–	−1.1	−8.0	13.3	5	−26.2	27	−5.2	−2.5	−5.0	−4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.3	6.4	7.2
Rok	–	–	–	–	12.1	3.2	31.8	27.VI	−26.2	27.XII	5.9	10.9	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7[3]	7.4[3]	7.1[3]	7.4[2]

Różanystok

$\varphi = 53°38'$ $\lambda = 23°24'$

I	–	–	–	–	−1.9	−6.3	5.0	4	−19.0	26	−4.5	−2.8	−3.8	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.2	8.1	8.2
II	–	–	–	–	1.7	−1.5	7.4	18	−4.7	7	−0.8	0.7	0.1	0.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.6	8.4	8.7
III	–	–	–	–	6.9	0.5	14.7	10	−3.9	20	1.8	5.4	2.8	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	5.8	7.6
IV	–	–	–	–	13.2	2.3	23.0	15	−2.7	21	5.1	11.8	7.3	7.9	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.6	3.7	4.3
V	–	–	–	–	16.2	7.2	25.5	30	1.0	15	9.7	15.3	10.8	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	7.4	7.5
VI	–	–	–	–	22.4	11.8	29.6	27	6.3	21	16.0	20.1	16.4	17.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	5.9	6.2
VII	–	–	–	–	21.2	10.8	28.1	3	8.0	7	14.8	19.6	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.9	7.0	6.9
VIII	–	–	–	–	20.5	11.4	28.7	6	7.3	30	13.8	19.1	14.5	15.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	6.6	7.3
IX	–	–	–	–	18.2	8.0	28.1	3	0.5	22	10.2	16.9	12.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.6	3.9	4.9
X	–	–	–	–	13.7	5.9	17.7	4	−0.5	23	6.4	12.7	9.0	9.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	5.3	6.4
XI	–	–	–	–	4.4	0.1	11.7	2	−5.3	21	1.9	3.5	2.3	2.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.6	8.2
XII	–	–	–	–	−2.0	−8.0	12.7	5	−21.7	27	−5.4	−3.7	−5.1	−4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.3	5.5	6.7
Rok	–	–	–	–	11.2	3.5	29.6	27.VI	−21.7	27.XII	5.8	9.9	6.8	7.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.2	6.3	6.9

Szczytno

$\varphi = 53°34'$ $\lambda = 21°02'$

I	–	–	–	–	−0.5	−6.6	5.5	4	−21.8	26	−4.5	−1.5	−3.7	−3.4	4.2	4.6	4.5	4.4	8.7	8.1	8.8	9.5	0.5	1.0	0.5	0.7	7.8	7.7	6.8	7.4
II	–	–	–	–	2.8	−1.2	11.5	18	−5.3	5	−0.1	2.1	0.6	0.8	5.7	6.2	6.0	6.0	9.3	8.6	9.2	9.0	0.4	1.1	0.5	0.7	9.6	8.3	7.4	8.4
III	–	–	–	–	8.3	0.3	16.8	10	−5.9	20	2.9	6.9	3.3	4.1	6.5	6.5	6.5	6.5	8.5	6.7	8.3[3]	7.8	1.2	3.6	1.3	2.0	7.6	6.5	3.6[3]	5.9[3]
IV	–	–	–	–	14.2	1.7	24.5	7	−5.3	2, 11	5.8	13.1	6.4	7.9	7.1	7.3	7.6	7.3	7.5	5.0	7.6	6.7	2.5	8.7	2.5	4.6	4.4	4.3	2.6	3.8
V	–	–	–	–	16.5	5.7	25.1	27	−0.7	19	10.2	15.2	9.5	11.1	10.4	10.6	10.5	10.5	9.3	6.2	8.7	7.7	2.3	7.3	1.7	3.8	6.2	6.5	5.6	6.1
VI	–	–	–	–	23.3	10.9	30.3	27	5.2	1	17.1	22.3	14.9	17.3	15.1	14.5	14.3	14.6	7.8	5.5	8.4	7.2	4.6	13.1	2.8	6.8	5.1	4.7	4.8	4.9
VII	–	–	–	–	20.5	9.5	30.5	3	5.2	6	14.5	18.9	13.9	15.3	14.2	14.5	13.8	14.2	8.7	6.8	8.7	8.1	2.4	7.9	2.2	4.2	7.4	7.4	6.8	7.2
VIII	–	–	–	–	19.7	10.2	28.6	6	5.1	14	14.4	18.8	13.7	15.2	14.6	15.0	13.9	14.5	8.8	6.9	8.8	8.2	2.1	7.1	2.0	3.7	6.4	6.0	5.7	6.0
IX	–	–	–	–	18.8	6.6	27.4	2	−1.2	24	10.3	18.2	11.1	12.7	–	–	–	–	–	–	–	–	–	–	–	–	5.2	3.9	3.2	4.1
X	–	–	–	–	14.0	5.7	18.6	4	−0.5	13	7.4	13.3	9.5	9.9	9.2	10.6	9.7	9.8	8.9	7.0	8.1	8.0	1.2	4.9	2.4	2.8	6.2	5.1	3.8	5.0
XI	–	–	–	–	4.8	−0.1	11.5	2	−9.0	23	1.9	3.8	2.3	2.6	6.8	7.2	6.9	7.0	9.3	8.8	9.1	9.1	0.5	1.0	0.6	0.7	8.5	8.0	6.3	7.6
XII	–	–	–	–	−1.6	−9.0	13.1	5	−27.4	27	−5.7	−3.2	−5.7	−5.1	4.1	4.4	4.0	4.2	8.2	7.9	8.0	8.0	0.7	1.0	0.7	0.8	7.2	6.0	4.4	5.9
Rok	–	–	–	–	11.7	2.8	30.5	3.VII	−27.4	27.XII	6.2	10.7	6.3	7.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	5.1[3]	6.0[2]

Szczuczyn

$\varphi = 53°34'$ $\lambda = 22°17'$

I	–	–	–	–	−0.9	−6.5	5.4	4	−20.2	26	−4.6	−2.4	−3.4	−3.4	4.3	4.6	4.5	4.5	9.0	8.5	8.8	8.8	0.4	0.7	0.5	0.5	7.8	8.3	8.1	8.1
II	–	–	–	–	2.6	−1.5	11.0	18	−5.4	5	−0.4	1.5	0.5	0.5	5.7	6.2	5.9	5.9	9.4	9.0	9.3	9.2	0.3	0.7	0.5	0.5	9.4	8.7	7.6	8.6
III	–	–	–	–	8.1	0.5	16.6	10	−4.5	20	2.3	6.2	3.3	3.8	6.5	6.8	6.5	6.6	8.9	7.1	8.2	8.1	0.8	3.0	1.4	1.7	8.8	7.8	5.8	7.5
IV	–	–	–	–	14.0	1.5	23.5	7	−5.0	2	5.1	12.5	7.3	8.0	7.1	7.2	8.0	7.4	7.8	4.8	7.5	6.7	2.1	8.3	2.6	4.3	4.9	4.9	3.3	4.4
V	–	–	–	–	16.7	6.9	25.8	29	1.7	5	9.9	15.0	10.5	11.5	10.5	10.3	10.7	10.5	8.5	6.1	8.4	7.7	1.9	7.4	2.3	3.9	7.9	8.3	6.7	7.6
VI	–	–	–	–	23.1	11.4	31.3	27	5.6	21	15.9	21.4	16.1	17.4	14.5	13.6	14.6	14.2	8.0	5.5	8.0	7.2	3.8	12.7	3.8	6.8	6.1	6.6	6.3	6.3
VII	–	–	–	–	20.9	10.8	30.2	3	6.4	6	14.4	19.1	14.7	15.7	14.0	13.7	14.5	14.1	8.6	6.3	8.6	7.8	2.5	9.1	2.4	4.7	7.2	8.1	7.9	7.7
VIII	–	–	–	–	20.1	11.0	29.5	6	6.2	18	13.7	18.8	14.5	15.4	14.0	13.8	14.1	14.0	8.9	6.4	8.5	7.9	1.8	8.3	2.6	4.2	7.6	8.0	6.0	7.2
IX	–	–	–	–	18.9	7.6	28.8	3	−1.2	24	9.8	17.8	11.4	12.6	11.5	12.1	12.1	11.9	9.2	5.9	8.7	7.9	1.1	9.0	1.8	4.0	6.3	5.5	3.1	5.0
X	–	–	–	–	13.6	5.0	19.1	4	−1.6	23	6.2	12.7	8.6	9.0	8.8	10.2	9.5	9.5	9.2	7.0	8.4	8.2	0.8	4.7	1.9	2.5	7.5	7.1	4.8	6.5
XI	–	–	–	–	4.7	0.5	10.8	2	−7.0	24	2.1	3.8	2.6	2.8	6.9	7.2	7.0	7.0	9.3	8.7	9.2	9.1	0.5	1.1	0.7	0.8	9.2	8.9	8.2	8.8
XII	–	–	–	–	−1.8	−8.0	13.4	5	−24.8	27	−5.3	−3.1	−5.0	−4.6	4.1	4.6	4.2	4.3	8.4	8.2	8.5	8.4	0.7	0.9	0.6	0.7	8.2	7.3	5.9	7.1
Rok	–	–	–	–	11.7	3.3	31.3	27.VI	−24.8	27.XII	5.8	10.3	6.3	7.4	9.0	9.2	9.3	9.2	8.8	7.0	8.5	8.1	1.4	5.5	1.8	2.9	7.6	7.5	6.1	7.1

Pisz — H_s = 118 m — h_w = 14 m — 1961

ROZKŁAD WIATRU (n_D, v_{mD}) · OPAD R · LICZBA DNI (n)

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Temp. Min < -10°	Temp. Max < 0°	Temp. Min < 0°	Temp. Max > 25°	Wiatr v > 10	Wiatr v > 15	◉	●	Opad R ≥ 0.1	Opad R ≥ 1.0	Opad R ≥ 10.0	≡	⊞	R ⊛
I	15.5	1.6	2.5	3.4	3.5	1.3	11	2.0	21.5	1.9	13.5	2.8	12	1.9	8.5	1.6	5	1.9	35.6	10.7	5	10	12	28	·	·	·	—	—	15	8	1	—	16	·
II	4	1.0	1	1.0	12.5	1.2	7.5	1.9	17	2.5	6	1.8	18	1.6	11	1.2	7	1.5	25.8	8.6	28	·	2	18	·	·	·	—	—	13	6	·	—	5	·
III	7	2.1	2	1.5	2	1.0	·	·	5	2.7	7	2.9	42	2.9	28	3.1	·	2.8	33.9	7.0	29	·	·	12	·	2	·	—	—	15	10	·	—	4	·
IV	18.5	1.5	7	1.4	28	1.8	9.5	2.1	25	2.0	5	1.8	7.5	1.5	10	2.7	2	1.8	22.9	10.4	7	·	·	9	·	·	·	—	—	7	4	1	—	2	2
V	22.5	1.7	6.5	1.1	11	1.2	5	1.6	9	1.6	4.5	1.7	14.5	1.7	11	2.0	9	1.5	74.7	15.2	21	·	·	·	3	·	·	—	—	19	13	3	—	·	3
VI	6.5	1.3	10	1.4	13	1.3	6	1.8	7.5	1.3	6	2.2	14.5	2.0	9.5	2.0	17	1.3	151.6	71.0	12	·	·	·	11	·	·	—	—	16	11	2	—	·	8
VII	5	1.4	3	1.6	6	1.2	4.5	1.2	12.5	1.7	15	1.6	25.5	1.6	10.5	1.4	11	1.4	124.8	26.5	22	·	·	·	4	·	·	—	—	23	17	5	—	·	3
VIII	10	1.2	2.5	1.0	3.5	1.3	1	1.0	6	2.7	14	1.4	34.5	2.0	12.5	2.0	9	1.6	54.3	11.5	6	·	·	·	2	·	·	—	—	18	12	1	—	·	5
IX	7.5	1.5	15.5	1.2	9.5	1.1	3.5	1.3	10	1.0	4.5	2.6	23	1.5	4.5	1.0	12	1.2	45.4	13.1	7	·	·	4	5	·	·	—	—	9	7	2	—	·	1
X	4	1.2	4	1.0	25.5	1.9	22.5	2.2	19	1.7	3.5	2.1	3.5	2.4	8	2.0	3	1.8	13.1	3.5	9, 14	·	·	·	·	·	·	—	—	8	5	·	—	·	·
XI	11	1.6	7	1.4	17.5	3.2	16.5	2.0	9.5	2.1	5.5	2.5	19	2.0	3	1.3	1	2.1	47.5	6.6	30	·	2	14	·	·	·	—	—	17	10	·	—	3	·
XII	18.5	2.2	7	2.8	4	1.5	4.5	1.4	19.5	1.5	5.5	2.2	22.5	2.3	6.5	1.8	5	1.9	35.8	8.2	4	11	15	27	·	1	·	—	—	12	8	·	—	20	2
Rok	130	1.5	68	1.6	136	1.5	91.5	1.5	139	1.8	90	2.1	236.5	2.0	123	1.8	81	1.7	665.4	71.0	12. VI	21	31	112	25	3	·	—	—	172	111	15	—	50	22

Różanystok — H_s = 160 m — h_w = 12 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Temp. Min < -10°	Temp. Max < 0°	Temp. Min < 0°	Temp. Max > 25°	Wiatr v > 10	Wiatr v > 15	◉	●	Opad R ≥ 0.1	Opad R ≥ 1.0	Opad R ≥ 10.0	≡	⊞	R ⊛
I	10	5.6	2.5	5.4	2	3.5	6	3.6	22.5	5.3	24.5	6.2	11.5	6.3	11	4.5	3	5.3	15.8	4.3	5	9	15	28	·	8	·	·	19	13	6	·	4	23	—
II	4.5	2.8	2	2.0	2	4.0	2	1.2	26	5.6	25	4.6	13.5	4.6	8	3.8	1	4.5	14.0	5.0	28	·	7	20	·	1	·	1	19	7	4	·	9	2	—
III	·	·	·	·	·	·	0.5	8.0	6.5	6.1	30	8.9	41	7.8	15	10.1	·	8.4	32.1	6.7	12	·	·	11	·	16	4	·	14	15	10	·	2	2	—
IV	5.5	4.5	10.5	3.7	11	4.5	6.5	4.0	16	3.5	10	5.4	12	5.2	13.5	3.6	5	4.0	22.0	6.7	7	·	·	8	·	1	1	7	6	8	7	·	1	·	—
V	8	4.7	4	3.8	9	3.4	4.5	4.0	19.5	3.2	13.5	3.2	20	3.7	12.5	3.4	2	3.7	53.8	16.0	30	·	·	·	2	1	·	·	15	14	10	1	2	·	—
VI	6.5	3.1	4.5	3.0	5.5	4.2	8.5	2.9	15.5	3.5	19.5	4.6	21	4.8	8	3.4	1	3.9	79.7	17.7	16	·	·	·	9	·	·	·	7	13	11	3	·	·	—
VII	15.5	3.5	11	3.4	9	3.6	·	·	2.5	9.0	16	4.0	16	5.6	19	4.3	4	4.1	75.4	18.0	19	·	·	·	3	4	·	·	10	13	9	3	3	·	—
VIII	11	4.5	5	4.3	2	3.0	2.5	6.4	6.5	4.8	30	6.4	24.5	4.9	10.5	5.2	1	5.3	58.0	13.3	20	·	·	·	3	4	·	·	10	15	12	2	·	·	—
IX	7.5	3.4	0.5	3.0	6	2.8	2.5	1.4	9	2.1	30.5	6.1	19.5	4.5	9.5	3.5	5	4.2	35.7	12.6	14	·	·	·	3	2	1	9	8	9	7	1	4	·	—
X	5.5	3.4	4	4.9	15.5	5.3	22	5.7	24	4.4	6	5.8	14	4.1	·	·	2	4.8	5.3	2.8	26	·	·	1	·	3	·	4	11	5	2	·	5	·	—
XI	4.5	6.9	5	4.8	16	7.4	4	5.8	18	4.3	22.5	7.5	14	5.7	4	4.5	2	6.0	36.8	6.8	10	·	4	15	·	8	·	·	20	17	10	·	3	3	—
XII	10.5	8.0	5.5	5.3	4.5	3.8	4.5	4.4	18	5.0	20.5	8.9	19.5	6.2	8	5.4	2	6.3	24.4	6.6	2	12	18	27	·	9	2	1	13	9	6	·	1	21	—
Rok	89	4.2	54.5	3.6	82.5	3.8	63.5	4.0	184	4.7	248	6.0	226.5	5.3	119	4.3	28	5.0	453.0	18.0	19. VII	21	44	110	20	57	8	22	152	138	94	10	34	51	—

Szczytno — H_s = 144 m — h_w = 15 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Temp. Min < -10°	Temp. Max < 0°	Temp. Min < 0°	Temp. Max > 25°	Wiatr v > 10	Wiatr v > 15	◉	●	Opad R ≥ 0.1	Opad R ≥ 1.0	Opad R ≥ 10.0	≡	⊞	R ⊛
I	16.5	2.3	6.5	1.2	·	·	7	3.1	18.5	3.2	24	3.5	11.5	2.7	6	2.2	3	2.8	23.8	7.3	30	12	12	27	·	1	1	3	18	12	7	·	9	16	·
II	1.5	2.0	0.5	2.0	1	2.0	2	3.0	16	4.0	17.5	3.5	26.5	2.3	10	2.4	9	2.6	23.2	5.8	11	·	3	21	·	1	·	1	20	10	7	·	17	4	·
III	1	5.5	·	·	·	·	·	·	2	4.5	12	8.2	39	6.6	31	7.7	8	6.5	26.7	5.9	29	·	·	13	·	12	10	3	9	17	7	·	5	3	·
IV	8	3.7	5.5	2.3	8	3.9	19.5	3.5	8	2.9	9.5	2.4	17	2.5	10.5	6.5	4	3.3	26.3	11.7	7	·	·	11	·	6	2	11	5	8	6	1	5	3	1
V	6	5.8	6.5	3.5	2	4.5	4	3.0	7	4.0	9.5	3.2	29	3.4	28	3.0	1	3.4	62.1	16.2	10	·	·	1	1	·	·	2	9	15	11	2	1	·	4
VI	3	2.7	4.5	3.2	2.5	2.6	13.5	3.1	6	3.6	12	3.2	24	3.9	23.5	3.3	1	3.4	135.0	31.2	7	·	·	·	11	3	2	8	7	14	12	6	3	·	6
VII	4	2.5	·	·	·	·	5	3.2	1.5	2.0	9.5	3.3	48	2.9	23	3.0	2	2.9	106.7	22.7	16	·	·	·	3	3	·	1	15	22	15	3	2	·	5
VIII	4.5	2.9	7	2.1	·	·	1	4.0	1.5	4.7	11	3.4	29.5	2.8	34.5	3.2	4	2.9	91.4	21.3	7	·	·	·	2	1	1	5	10	19	16	1	3	·	1
IX	5.5	2.2	3.5	2.0	4	2.5	12.5	2.6	5.5	3.1	11	2.5	28	2.9	16	3.3	4	2.7	43.4	23.7	14	·	·	4	5	1	1	12	7	8	6	1	11	·	·
X	·	·	2	2.5	9.5	2.9	38	4.2	20	3.2	8.5	3.2	10	3.2	4	3.6	1	3.5	12.5	4.3	29	·	·	1	·	·	·	8	9	10	5	·	14	·	·
XI	8.5	2.2	6	3.5	9	4.4	10	3.9	11	2.4	12.5	2.4	27	3.3	4	1.6	2	3.0	52.9	8.1	5	·	2	13	·	2	·	2	18	18	10	·	15	·	·
XII	13	4.9	2.5	1.0	3	2.0	5.5	4.7	12	2.3	15.5	4.6	25.5	4.1	7	2.6	9	3.4	38.2	11.6	4	13	16	27	·	4	3	6	12	12	9	1	8	21	·
Rok	71.5	3.1	44.5	1.9	39	2.1	118	3.2	109	3.3	152.5	3.6	315	3.4	197.5	3.5	48	3.4	647.2	31.2	7. VI	25	33	118	22	34[2]	20[2]	62	139	165	111	15	93	47	17

Szczuczyn — H_s = 130 m — h_w = 15 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Temp. Min < -10°	Temp. Max < 0°	Temp. Min < 0°	Temp. Max > 25°	Wiatr v > 10	Wiatr v > 15	◉	●	Opad R ≥ 0.1	Opad R ≥ 1.0	Opad R ≥ 10.0	≡	⊞	R ⊛
I	7.5	3.3	6	2.8	1.5	2.7	17.5	3.7	16	4.9	20	5.9	13	4.7	9.5	3.1	2	4.3	28.7	11.6	5	11	12	29	·	2	1	·	19	16	5	1	7	28	·
II	0.5	1.0	1	2.5	3.5	2.3	9	4.5	20	4.2	18	4.3	18.5	3.6	5.5	3.5	8	3.5	16.3	4.2	11	·	5	19	·	·	·	·	20	10	5	·	15	2	·
III	·	·	·	·	·	·	1	10.0	4	5.6	27	7.6	44	7.0	16	7.2	1	7.2	22.9	5.8	30	·	·	11	·	15	6	·	16	16	5	·	2	1	·
IV	7	3.1	8.5	4.0	14.5	4.3	13	4.8	5	2.7	11	4.9	15.5	3.8	10.5	4.6	5	3.9	23.9	8.0	7	·	·	11	·	3	1	10	7	11	7	·	4	3	1
V	9	2.9	5	2.3	2	3.5	9	4.4	7	4.4	15	3.7	20	3.6	15	2.9	11	3.1	89.9	18.7	15	·	·	·	3	1	·	·	14	21	13	4	·	·	3
VI	2	1.2	7.5	2.6	10.5	2.4	7	3.3	6.5	3.2	19	5.2	20.5	4.1	9	3.1	8	3.4	80.4	13.2	11	·	·	·	11	3	·	3	10	15	13	4	·	·	8
VII	2	2.0	3.5	3.3	3.5	2.7	4	3.5	11	3.8	37.5	3.9	22	3.2	3.5	2.3	6	3.3	93.9	26.2	30	·	·	·	3	2	1	1	17	18	12	4	3	·	6
VIII	3.5	2.4	1.5	3.0	0.5	3.0	·	·	11.5	4.5	32	4.9	26.5	3.8	9.5	3.7	8	3.9	45.0	7.4	23	·	·	·	2	2	·	1	12	17	12	·	2	·	4
IX	4.5	2.2	5	2.5	5.5	2.2	5	2.6	2.5	4.4	19	5.2	20.5	4.5	6	2.8	22	3.0	30.4	17.9	14	·	·	2	5	1	·	6	7	7	5	1	4	·	3
X	·	·	4	2.5	20.5	3.7	31.5	4.7	10	3.2	7	4.6	11.5	2.3	2.5	2.4	6	3.7	5.5	2.6	26	·	·	1	·	3	·	5	12	5	2	·	11	·	·
XI	5.5	3.2	5	4.1	4.3	7.2	15	3.2	10.5	3.5	17	6.0	12	4.3	5	2.8	7	4.3	41.7	9.6	8	·	4	14	·	4	·	·	21	18	10	·	8	·	·
XII	6.5	5.6	5.5	3.2	1.5	3.3	12	4.0	13	3.7	19	8.2	16	5.3	12.5	3.4	7	4.7	29.4	9.2	2	11	16	26	·	7	2	2	15	17	6	·	6	20	·
Rok	48	2.2	52.5	2.7	76.5	3.1	124	4.1	117	4.0	241.5	5.4	240	4.2	104.5	3.5	91	4.0	508.0	26.2	30. VII	22	37	113	24	43	11	28	170	171	95	14	62	54	25

Kamień Krajeński — φ = 53°32' — λ = 17°31' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.1	−6.0	4.8	30	−19.8	26	−4.3	−1.2	−3.4	−3.1	—	—	—	—	—	—	—	—	—	—	—	—	6.6	6.8	5.3	6.2
II	—	—	—	—	3.9	−1.1	12.4	18	−7.5	5	0.2	2.8	1.1	1.3	—	—	—	—	—	—	—	—	—	—	—	—	9.2	9.0	7.1	8.4
III	—	—	—	—	8.6	1.3	16.9	10	−6.7	20	3.3	7.1	4.3	4.8	—	—	—	—	—	—	—	—	—	—	—	—	8.0	6.1	5.8	6.6
IV	—	—	—	—	14.1	2.6	23.4	14	−3.6	10	5.9	12.5	7.5	8.4	—	—	—	—	—	—	—	—	—	—	—	—	4.2	4.9	4.2	4.4
V	—	—	—	—	15.2	5.5	23.5	30	−0.4	13	9.1	13.5	9.7	10.5	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.7	5.9	6.6
VI	—	—	—	—	22.8	11.2	27.9	26	4.9	22	15.3	20.6	15.8	16.9	—	—	—	—	—	—	—	—	—	—	—	—	3.9	5.0	4.3	4.4
VII	—	—	—	—	19.9	10.4	32.1	3	4.7	1	13.7	17.6	14.3	15.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.5	7.2	7.7
VIII	—	—	—	—	19.7	10.5	27.4	6	6.4	14	13.2	17.2	14.6	14.9	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.3	5.9	6.8
IX	—	—	—	—	19.6	8.3	28.3	2	0.6	25	10.6	18.1	13.0	13.7	—	—	—	—	—	—	—	—	—	—	—	—	4.3	3.8	3.1	3.7
X	—	—	—	—	14.1	6.8	18.9	5, 6	2.1	31	8.2	13.1	10.0	10.3	—	—	—	—	—	—	—	—	—	—	—	—	7.7	6.2	4.6	6.2
XI	—	—	—	—	5.9	0.9	10.5	2	−8.2	23	2.6	4.6	3.1	3.4	—	—	—	—	—	—	—	—	—	—	—	—	9.0	8.6	8.2	8.6
XII	—	—	—	—	−0.7	−7.4	13.4	5	−20.5	26	−4.2	−2.3	−4.5	−3.9	—	—	—	—	—	—	÷	—	—	—	—	—	7.2	6.7	5.4	6.4
Rok	—	—	—	—	11.9	3.6	32.1	3. VII	−20.5	26. XII	6.1	10.3	7.1	7.6	—	—	—	—	—	—	—	—	—	—	—	—	6.8	6.6	5.6	6.3

Grudziądz — φ = 53°30' — λ = 18°46'

I	—	—	—	—	0.6	−4.5	5.7	4	−16.7	26	−3.2	−0.2	−1.9	−1.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	4.3	−0.2	11.1	18	−5.5	6	1.3	3.5	1.9	2.2	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	9.9	2.3	17.5	10	−4.1	20	4.3	8.6	5.6	6.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	6.6	6.6	7.2
IV	—	—	—	—	15.4	4.2	23.8	14	−1.9	10	7.2	13.9	8.6	9.6	—	—	—	—	—	—	—	—	—	—	—	—	4.6	4.5	3.2	4.1
V	—	—	—	—	16.7	6.9	24.4	30	2.7	13	10.1	15.1	10.7	11.6	—	—	—	—	—	—	—	—	—	—	—	—	6.6	7.6	6.3	6.8
VI	—	—	—	—	25.3	13.2	33.1	27	7.8	22	17.4	23.3	18.7	19.5	—	—	—	—	—	—	—	—	—	—	—	—	4.4	5.0	5.4	4.9
VII	—	—	—	—	21.6	12.2	33.3	3	9.0	8	14.9	19.4	15.9	16.5	14.1	14.3	15.0	14.5	83	66	83	77	3.0	9.1	3.4	5.2	7.1	7.5	6.4	7.0
VIII	—	—	—	—	20.9	11.8	29.1	6	8.5	14	13.9	19.0	15.1	15.8	14.4	14.8	15.0	14.7	91	68	87	82	1.6	7.6	2.3	3.8	7.3	7.6	5.2	6.7
IX	—	—	—	—	20.8	9.7	28.8	17	3.6	28	11.0	19.4	13.4	14.3	—	—	—	—	—	—	—	—	—	—	—	—	4.4	4.3	4.0	4.2
X	—	—	—	—	15.3	7.6	20.2	5	4.3	13, 14, 31	8.4	14.4	10.7	11.0	10.2	11.5	10.9	10.9	91	71	85	82	1.0	5.1	2.1	2.7	7.2	6.1	5.4	6.2
XI	—	—	—	—	5.9	1.5	11.7	2	−6.2	23	3.1	4.9	3.4	3.7	7.3	7.6	7.4	7.4	93	86	93	91	0.6	1.3	0.6	0.8	8.9	7.8	6.9	7.9
XII	—	—	—	—	0.1	−6.2	14.2	5	−18.9	17	−3.4	−1.6	−3.2	−2.8	4.7	5.0	4.6	4.8	88	82	87	86	0.6	1.0	0.8	0.8	7.2	6.2	5.9	6.4
Rok	—	—	—	—	13.1	4.9	33.3	3. VII	−18.9	17. XII	7.1	11.6	8.2	8.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Osowiec — φ = 53°29' — λ = 22°39'

I	—	—	—	—	−1.0	−6.3	5.6	4	−19.3	25	−4.7	−2.1	−3.3	−3.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	2.3	−1.2	10.5	18	−4.7	5	−0.3	1.9	0.7	0.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	7.4	0.6	15.3	10	(−4.8)	20	2.4	6.4	3.6	4.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	13.9	2.9	23.4	15	−3.2	2, 3, 11	5.5	12.5	7.9	8.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	16.8	6.6	26.6	28	1.6	12, 15	10.0	15.1	10.7	11.7	—	—	—	—	—	—	—	—	—	—	—	—	6.5	5.4	7.5	6.5
VI	—	—	—	—	23.3	11.7	30.5	27	5.6	21	16.2	21.6	16.2	17.6	—	—	—	—	—	—	—	—	—	—	—	—	5.2	5.0	7.0	5.7
VII	—	—	—	—	20.9	10.6	30.1	3	6.4	6	14.5	19.6	15.4	16.2	—	—	—	—	—	—	—	—	—	—	—	—	6.9	6.8	8.3	7.3
VIII	—	—	—	—	20.5	10.8	29.8	6	5.3	18	14.0	19.6	15.5	16.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	19.3	6.4	28.2	2	−1.6	24	9.9	18.6	11.8	13.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	14.5	5.2	19.1	4	−1.5	23	7.0	14.0	9.0	9.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	4.7	0.2	11.5	2	−7.8	29	2.0	3.9	2.2	2.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	−1.8	−7.8	13.5	5	−25.2	27	−5.4	−2.9	−5.1	−4.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	11.7	3.3	30.5	27. VI	−25.2	27. XII	5.9	10.7	7.0	7.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Szczecin-Niebuszewo — φ = 53°28' — λ = 14°33'

I	—	—	—	—	0.9	−4.0	6.5	30	−15.3	27	−2.6	0.2	−1.5	−1.4	4.8	5.0	5.0	4.9	88	77	85	83	0.6	1.3	0.7	0.9	6.9	6.6	5.8	6.4
II	—	—	—	—	6.5	1.0	12.8	27	−3.7	5	2.1	5.1	3.2	3.4	6.8	7.5	7.2	7.2	95	86	93	91	0.4	1.4	0.6	0.8	9.0	8.1	6.9	8.0
III	—	—	—	—	9.7	2.6	17.0	10	−4.2	20	4.2	8.5	5.5	5.9	7.5	7.3	7.6	7.5	90	66	83	83	0.9	4.1	1.6	2.2	8.5	7.8	5.8	7.4
IV	—	—	—	—	14.8	5.1	24.9	14	−1.0	1	7.3	13.3	9.1	9.7	8.2	8.3	8.6	8.4	79	55	73	69	2.3	7.8	3.3	4.5	5.7	5.8	5.1	5.5
V	—	—	—	—	14.5	7.1	22.5	26	3.8	29	9.4	13.1	9.5	10.4	10.1	10.1	10.2	10.1	85	68	85	79	1.7	5.3	1.8	2.9	8.0	7.9	6.8	7.6
VI	—	—	—	—	22.0	12.1	27.6	26	7.7	20, 22	15.7	20.4	16.2	17.1	14.1	13.6	14.2	14.0	78	57	77	71	4.0	11.0	4.5	6.5	4.5	6.4	4.6	5.2
VII	—	—	—	—	19.6	12.2	31.9	3	8.7	6	14.6	18.1	14.9	15.6	14.3	13.5	14.1	14.0	86	67	84	79	2.5	8.0	3.0	4.5	7.6	7.9	7.2	7.6
VIII	—	—	—	—	19.6	11.8	26.0	31	8.3	24	14.2	18.2	14.8	15.5	14.7	14.5	15.0	14.8	91	69	87	82	1.6	6.7	2.3	3.5	7.5	7.5	5.8	6.9
IX	—	—	—	—	20.3	11.0	28.2	2	4.3	27	12.8	19.5	14.0	15.1	13.4	14.4	13.8	13.5	89	63	81	78	1.6	9.0	2.5	4.4	3.7	4.4	3.4	3.8
X	—	—	—	—	15.0	8.3	21.0	6	4.2	31	9.3	14.0	10.9	11.3	10.6	11.0	11.3	11.0	90	70	87	82	1.2	5.3	1.9	2.8	6.2	6.1	5.0	5.8
XI	—	—	—	—	6.5	1.9	11.7	1	−5.4	23	3.2	5.7	3.8	4.1	7.4	7.6	7.4	7.5	93	82	90	88	0.6	1.7	0.8	1.0	8.7	7.9	6.8	7.8
XII	—	—	—	—	1.1	−5.2	14.3	5	−18.8	26	−2.6	−0.6	−2.0	−1.8	5.0	5.2	5.0	5.1	89	82	87	86	0.6	1.2	0.8	0.9	6.9	6.7	6.9	6.8
Rok	—	—	—	—	12.5	5.3	31.9	3. VII	−18.8	26. XII	7.3	11.3	8.2	8.8	9.7	9.8	10.0	9.8	88	78	84	81	1.5	5.2	2.0	2.9	6.9	6.9	5.8	6.5

Kamień Krajeński $H_s = 124 m$ $h_w = 12 m$ 1961

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	⊙	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	ꝶ
I	3	1.0	11	1.6	·	·	5	2.2	17	1.1	21	2.2	6	1.2	8	1.4	22	1.2	25.0	8.6	30	11	13	29	·	·	·	5	15	12	7	·	—	—	·
II	1	2.0	·	·	3	1.0	12	1.3	11	2.2	16	1.3	19	1.4	12	1.4	10	1.3	42.2	12.7	27	·	·	18	·	·	·	1	18	19	6	1	12	—	·
III	·	·	·	·	·	·	·	·	1	4.0	5	4.8	40	3.8	44	4.8	3	4.2	39.1	6.2	29	·	·	9	·	7	1	2	12	18	10	·	3	—	·
IV	7	1.1	12	2.8	25	2.5	8	2.6	4	1.2	5	1.0	10	3.0	9	2.7	10	2.1	30.7	6.6	27	·	·	10	·	·	·	9	4	13	8	·	·	—	2
V	18	2.1	10	1.5	5	1.2	2	1.0	7	2.3	9	1.8	16	1.9	15	2.8	11	1.8	53.9	10.7	7	·	·	1	·	·	·	1	7	14	12	1	2	·	3
VI	4	1.8	4	1.0	11	1.6	1	1.0	5	1.4	6	2.0	29	2.8	12	2.2	18	1.7	65.8	20.3	14	·	·	·	10	1	·	5	4	11	8	3	1	·	8
VII	3	1.3	·	·	3	1.0	1	4.0	5	1.4	17	1.8	38	2.1	8	1.2	18	1.5	144.8	38.0	31	·	·	·	3	·	·	2	16	25	19	4	·	·	6
VIII	4	1.0	1	2.0	1	1.0	1	2.0	3	2.0	15	1.7	39	2.1	9	1.8	20	1.5	62.8	14.8	10	·	·	·	2	·	·	3	10	21	13	1	3	·	3
IX	1	1.0	5	1.0	11	1.9	4	2.8	3	1.3	7	2.3	25	2.3	10	1.7	24	1.5	44.9	17.9	5	·	·	·	4	·	·	14	5	9	5	2	2	·	2
X	2	1.0	2	1.5	26	3.0	14	1.6	7	1.6	13	2.5	6	1.0	10	2.7	13	2.0	37.8	9.0	19	·	·	·	·	·	·	5	11	13	9	·	9	·	·
XI	8	1.9	8	5.8	8	3.2	6	1.2	1	1.0	16	3.5	16	2.6	7	3.0	20	2.4	28.9	6.4	30	·	·	14	·	·	·	2	22	20	12	·	—	—	·
XII	8	4.5	10	1.9	5	1.4	4	1.5	13	1.3	10	3.8	21	3.7	12	2.5	10	2.5	29.1	9.4	4	11	15	28	·	1	·	3	12	11	5	·	—	—	·
Rok	59	1.6	63	1.6	98	1.5	58	1.8	77	1.7	140	2.4	265	2.3	156	2.4	179	2.0	605.0	38.0	31.VII	22	28	104	19	9	1	52	136	186	114	12	—	—	24

Grudziądz $H_s = 40 m$ $h_w = 12,5 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	⊙	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	ꝶ
I	3	2.7	1	4.0	11.5	2.3	21	2.7	12.5	2.3	29	3.3	7	3.1	6	2.7	2	2.8	26.3	11.0	30	6	11	23	·	·	·	—	—	10	7	1	5	10	·
II	4	3.9	2	2.2	9	2.9	15	3.6	22.5	4.1	16.5	3.1	10	2.9	3	1.7	2	3.3	18.8	3.8	11, 28	·	·	15	·	1	1	—	—	9	7	·	11	1	·
III	2.5	4.8	·	·	·	·	·	·	6.5	2.2	29	3.2	46	4.2	8	4.9	1	3.8	31.5	10.0	27	·	·	6	·	4	·	1	16	14	9	1	·	2	·
IV	4	3.0	6	3.7	22	3.7	19.5	3.7	17	3.1	7.5	2.8	8	3.9	4	2.8	2	3.4	37.6	11.6	7	·	·	6	·	·	·	11	2	8	8	1	·	·	1
V	2.5	2.0	9	2.8	10.5	2.0	5.5	2.1	18	2.8	13	3.3	7	3.0	7.5	3.7	20	2.2	67.3	21.8	6	·	·	·	·	·	·	2	13	11	11	2	·		4
VI	1	2.0	3	3.0	13.5	1.1	7	2.9	14.5	2.1	26.5	2.4	11.5	3.9	1	2.0	12	2.1	30.4	7.9	14	·	·	·	17	·	·	6	4	8	7	·	·	·	3
VII	1	1.0	6	1.0	4	1.0	7.5	1.3	17	1.6	36	2.2	10	3.8	3.5	1.6	8	1.8	123.1	30.4	31	·	·	·	5	·	·	2	14	20	18	3	·	·	7
VIII	·	·	1	1.0	6	2.0	5.5	1.5	17.5	2.3	39	3.1	14.5	3.6	5.5	2.3	4	2.7	40.8	5.5	11	·	·	·	4	·	·	1	11	15	13	·	1	·	3
IX	1	1.0	0.5	1.0	13	2.2	9	1.9	18	1.7	21.5	2.1	9	1.9	·	·	18	1.6	34.2	15.3	14	·	·	·	6	·	·	11	5	6	6	1	2	·	1
X	1.5	1.0	·	·	15	3.3	27	3.7	14	2.3	10	4.8	2.5	3.8	2	3.5	21	2.7	33.1	9.6	18	·	·	·	·	·	·	4	9	10	10	·	9	·	·
XI	4.5	2.0	3.5	5.6	10	5.8	14.5	3.3	15	3.2	16	4.6	3.5	2.7	4	4.1	19	3.1	44.0	18.3	11	·	·	10	·	1		1	18	10	9	1	6	·	·
XII	2.5	3.2	4	2.9	11.5	2.7	17	2.3	18.5	2.6	24	4.4	6	3.2	6.5	2.4	3	3.0	29.6	9.9	4	9	14	24	·	1	·	3	13	10	9	·	2	13	·
Rok	27.5	2.2	36	2.3	126	2.4	148.5	2.4	191	2.5	268	3.3	135	3.3	51	2.6	112	2.7	516.7	30.4	31. VII	15	25	84	32	7	1	—	—	131	114	10	36	26	19

Osowiec $H_s = 110 m$ $h_w = 11 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	⊙	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	ꝶ
I	9.5	2.1	·	·	2	2.0	21	1.9	13	2.9	11	4.3	17	2.5	9.5	2.4	10	2.3	34.4	13.5	6	13	13	28		1	·	—	—	10	7	1	2	27	—
II	2	2.0	1	1.0	5	1.8	17	3.6	16.5	3.1	19.5	2.3	10	3.1	2	2.5	11	2.5	17.8	6.2	11	·	3	20	·	1	·	—	—	11	4		11	1	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39.6	11.6	30	·	·	12	·	—	—	—	—	9	8	1	—	2	—
IV	16.5	2.6	19	2.7	7.5	3.8	9	2.4	2	5.0	12.5	1.9	7	2.8	12.5	4.8	4	2.8	21.2	7.8	7	·	·	8	·	2	·	—	—	7	7	·	1	2	—
V	9	2.5	7	1.1	4.5	1.4	19.5	2.6	7	2.0	21	3.0	13.5	3.4	11.5	2.0	·	2.5	54.7	10.5	10	·	·	·	4	·	·	·	8	11	11	2	1	·	—
VI	4.5	2.4	14.5	1.6	13.5	2.0	5.5	2.0	18	2.5	18.5	4.3	11	3.5	0.5	4.0	4	2.6	122.6	40.3	11	·	·	·	12	·	·	2	10	17	16	3	·	·	—
VII	·	·	4	4.1	2	5.2	8	3.1	33	3.2	29	3.2	6	3.5	2	2.0	9	3.0	87.6	34.5	30	·	·	·	3	1	·	1	15	15	11	3	3	·	—
VIII	4	2.2	·	·	1	4.0	11	4.6	14.5	3.9	26.5	3.4	15	3.2	6	4.0	15	3.0	46.0	7.8	11	·	·	·	2	1	·	—	—	14	9	·	3	·	—
IX	4.5	3.0	4	2.8	2	1.5	4	2.2	7.5	3.7	19.5	2.5	6	2.7	3.5	1.8	39	1.5	32.8	8.1	6	·	·	3	5	·	·	—	—	10	6	·	5	·	—
X	·	·	15	2.1	12	4.0	34	3.4	4.5	3.3	13.5	1.3		·	·	·	14	2.5	7.0	5.5	26	·	·	1	·	·	·	—	—	4	1	·	6	·	—
XI	5.5	2.9	14	2.4	8	4.1	18.5	2.3	12	2.5	4.5	5.1	9	4.1	5.5	3.7	13	2.6	45.5	8.9	10	·	5	17	·	·	·	—	—	19	12	·	11		—
XII	10.5	4.7	5.5	2.6	1	2.0	26	2.5	10.5	3.0	11.5	4.0	9	4.3	9	2.4	10	2.9	26.8	5.6	4	12	16	24	·	3	·	—	—	15	9	·	3	20	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	536.0	40.3	11.VI	25	37	113	26	—	—	—	—	142	101	10	—	50	—

Szczecin – Niebuszewo $H_s = 69 m$ $h_w = 10 m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	⊙	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	ꝶ
I	·	·	4.5	3.2	13.5	2.9	21.5	3.3	16.5	2.8	16.5	4.3	6.5	2.5	3	3.5	11	2.9	38.1	7.1	4	3	10	20	·	·	·	9	17	13	10	·	4	7	·
II	·	·	·	·	7	2.9	10	4.0	17.5	3.4	18.5	3.6	18	2.7	8	2.8	5	3.1	56.4	12.0	27	·	·	9	·	·	·	·	16	15	9	2	7	2	·
III	3	6.7	·	·	·	·	·	·	15	6.0	18.5	4.4	56	4.9	13	5.2	1	4.9	42.9	7.5	30	·	·	6	·	4	·	1	14	18	11	·	4	1	·
IV	2	3.3	10.5	3.0	20	3.8	14	4.8	6.5	3.3	9.5	3.6	9.5	3.7	9	2.4	4	3.4	23.4	8.4	14	·	·	1	·	·	·	7	7	10	6	·	2	1	3
V	24	4.1	8.5	2.8	6.5	1.9	5.5	4.3	6	2.6	8.5	3.2	20.5	3.3	13.5	3.5	·	3.4	128.9	23.9	29	·	·	·	·	·	·	·	16	22	18	3	·	·	8
VI	4.5	3.1	10.5	2.3	8	2.4	3.5	3.3	6	3.1	17	3.6	27.5	1.9	11	3.3	2	3.2	53.6	21.3	13	·	·	·	5	·	·	1	3	9	4	2	·	·	5
VII		·	3	2.7	3.5	2.3	1	4.0	10	3.8	31	4.0	35	3.3	5.5	3.6	4	3.4	109.2	20.3	18	·	·	·	3	·	·	2	18	19	15	4	·	·	6
VIII	4	2.0	1.5	2.7	3	2.2	6.5	2.5	6	4.0	31	3.8	28	3.5	2	2.2	11	3.0	126.3	20.9	3	·	·	·	1	·	·	3	12	20	14	6	1	·	3
IX	8.5	2.0	·	·	16.5	3.2	13	2.7	11.5	3.3	14.5	3.4	14	3.3	2	3.0	11	2.7	31.0	13.9	7	·	·	·	4	·	·	13	6	6	4	1	2	·	2
X	1	3.5	1.5	3.3	21	5.1	14.5	5.1	28	3.7	12.5	3.6	5.5	2.7	6	2.6	3	4.0	41.7	11.3	20	·	·	·	·	2	·	8	11	10	8	1	2	·	·
XI	10	2.2	11.5	3.8	7	3.6	6	3.5	10.5	4.1	21.5	4.0	8	3.0	3.5	3.4	12	3.1	26.4	6.0	30	·	·	7	·	·	·	3	17	15	9	·	7	·	·
XII	6.5	3.5	0.5	4.0	9	2.5	18	2.3	6.5	2.8	20.5	4.8	18.5	3.8	4.5	3.3	9	3.1	55.7	14.5	4	9	11	21	·	1	·	3	16	15	9	3	2	16	·
Rok	68.5	2.5	52	2.3	114	2.7	113.5	3.3	126.5	3.6	219.5	3.9	267	3.4	81	3.2	73	3.4	733.6	23.9	29. V	12	21	64	13	7	·	50	153	172	117	22	31	27	27

Szczecin – Dąbie

$\varphi = 53°24'$ $\lambda = 14°37'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max obs.	Data	Min obs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1016.1	1042.0	989.9	1017.0	1.3	−4.2	6.9	30	−17.8	26	−2.7	0.4	−1.6	−1.4	4.7	5.2	5.0	5.0	86	78	85	83	0.7	1.3	0.8	0.9	6.6	6.6	5.6	6.3
II	1018.3	1035.9	989.0	1019.2	6.9	0.8	13.1	28	−5.5	5	2.1	5.7	3.4	3.6	6.7	7.6	7.1	7.1	94	83	90	89	0.5	1.7	0.8	1.0	8.5	7.9	6.9	7.8
III	1015.9	1035.0	986.3	1016.7	10.3	2.9	17.4	10	−3.2	20	4.4	8.8	6.2	6.4	7.5	7.4	7.7	7.5	89	66	81	79	1.0	4.1	2.0	2.4	8.3	7.5	5.9	7.2
IV	1010.8	1022.3	999.2	1011.6	15.2	4.6	25.0	14	−0.6	1	7.0	13.7	9.5	9.9	8.4	8.8	8.8	8.7	82	56	73	70	1.9	7.8	3.5	4.4	5.7	5.9	5.4	5.7
V	1011.1	1022.1	996.4	1011.9	15.5	7.3	22.6	26	1.6	29	9.5	14.0	10.2	11.0	10.4	10.7	10.7	10.6	87	68	85	80	1.5	5.6	1.9	3.0	8.0	8.2	6.7	7.6
VI	1013.3	1027.7	1000.7	1014.1	22.8	12.3	28.1	25	6.5	22	15.6	20.9	16.7	17.5	14.4	14.6	14.8	14.6	81	59	78	73	3.5	10.6	4.3	6.1	5.2	6.3	5.1	5.5
VII	1010.6	1025.1	995.0	1011.4	20.4	12.7	32.0	3	8.5	1	14.5	18.8	15.5	16.1	14.5	13.8	14.3	14.2	88	65	81	78	2.1	8.6	3.6	4.8	7.8	7.8	7.2	7.6
VIII	1013.5	1026.7	1000.9	1014.3	20.2	12.1	26.4	31	8.5	8	13.9	18.7	15.1	15.7	14.5	15.0	14.8	14.8	91	70	86	82	1.5	6.9	2.5	3.6	7.8	7.7	5.8	7.1
IX	1016.0	1027.3	1000.4	1016.8	20.8	10.4	28.3	2	0.5	27	11.8	19.8	13.9	14.8	13.1	14.5	13.8	13.8	93	62	85	80	1.1	9.1	2.4	4.2	4.4	4.5	3.6	4.2
X	1014.8	1029.3	984.0	1015.6	15.4	8.0	21.7	6	3.9	31	9.1	14.4	11.1	11.4	10.5	11.2	11.4	11.0	90	69	86	82	1.2	5.5	2.0	2.9	5.9	6.2	5.5	5.9
XI	1012.4	1035.8	993.2	1013.3	6.9	1.7	12.0	2	−8.4	22	3.1	6.3	4.0	4.4	7.3	7.9	7.5	7.6	92	82	90	88	0.6	1.7	0.9	1.1	8.5	8.0	6.8	7.8
XII	1013.9	1046.5	982.9	1014.8	1.5	−5.7	14.9	5	−22.3	26	−2.7	−0.2	−2.1	−1.8	4.9	5.2	5.0	5.0	87	80	86	84	0.7	1.4	0.9	1.0	6.8	6.6	6.7	6.7
Rok	1013.9	1046.5	982.9	1014.7	13.1	5.2	32.0	3.VII	−22.3	26.XII	7.1	11.8	8.5	9.0	9.7	10.2	10.1	10.0	88	70	84	81	1.4	5.4	2.1	3.0	7.0	6.9	5.9	6.6

Wierzchowo

$\varphi = 53°27'$ $\lambda = 16°06'$

I	–	–	–	–	0.1	−5.5	5.5	29	−18.6	26	−3.8	−0.4	−2.7	−2.4	4.4	4.8	4.6	4.6	86	77	84	82	0.5	1.2	0.7	0.8	6.5	6.1	5.5	6.0
II	–	–	–	–	4.5	0.2	10.6	18	−5.6	5	1.0	3.8	2.0	2.2	6.2	7.2	6.7	6.7	94	90	94	93	0.4	0.8	0.4	0.5	–	–	–	–
III	–	–	–	–	8.3	1.5	17.8	10	−5.5	20	3.6	7.5	4.3	4.9	7.3	7.6	7.5	7.5	90	73	89	84	0.8	3.1	1.0	1.6	8.1	6.2	6.4	6.9
IV	–	–	–	–	13.9	3.0	23.2	14	−3.8	10	6.4	12.7	7.4	8.5	8.1	8.5	8.5	8.4	81	58	80	73	1.9	7.1	2.3	3.8	4.7	4.5	3.5	4.2
V	–	–	–	–	14.4	5.3	22.5	30	−0.4	13	9.4	13.1	8.9	10.1	10.3	10.9	10.0	10.4	87	73	87	82	1.7	4.4	1.5	2.5	6.7	6.7	5.5	6.3
VI	–	–	–	–	21.8	10.8	27.1	26	5.3	22	15.9	20.0	15.3	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.6	4.2	4.9
VII	–	–	–	–	19.0	11.0	30.8	3	5.2	1	14.0	17.5	13.8	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.4	6.4	6.8
VIII	–	–	–	–	19.2	10.7	26.1	6	6.8	8, 14	14.0	17.6	13.7	14.8	14.8	15.6	14.7	15.0	92	78	93	88	1.4	5.0	1.2	2.5	6.7	6.4	5.2	6.1
IX	–	–	–	–	19.6	8.6	27.9	2	−0.2	27	11.6	18.7	12.2	13.6	12.7	14.2	13.1	13.3	91	67	91	83	1.4	7.9	1.4	3.6	3.8	3.7	2.9	3.5
X	–	–	–	–	14.0	7.0	20.0	6	2.4	31	9.1	13.4	9.8	10.5	10.6	11.3	10.9	10.9	91	76	90	86	1.1	4.1	1.3	2.2	6.9	5.6	4.8	5.8
XI	–	–	–	–	5.8	1.3	11.0	2	−7.4	23	2.9	5.2	3.2	3.6	7.2	7.6	7.3	7.4	93	85	92	90	0.5	1.4	0.6	0.8	8.6	7.5	7.0	7.7
XII	–	–	–	–	−0.3	−2.0	14.0	5	−21.3	27	−4.0	−1.4	−3.8	−3.2	4.7	5.0	4.5	4.7	88	83	87	86	0.5	1.0	0.6	0.7	7.3	6.1	6.8	6.7
Rok	–	–	–	–	11.7	3.9	30.8	3.VII	−21.3	27.XII	6.7	10.6	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Jastrowie

$\varphi = 53°25'$ $\lambda = 16°48'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.1	10.2	28.0	6	6.2	4	13.0	18.0	13.5	14.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	29.0	2	–	–	10.5	18.7	12.6	13.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.7	6.9	22.5	11	1.5	31	8.9	13.5	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.2	6.5	5.9
XI	–	–	–	–	6.1	1.1	11.3	2	−9.5	23	2.6	5.0	3.1	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.4	8.0	7.9
XII	–	–	–	–	–	−7.5	13.1	5	−22.0	26	−4.3	−1.9	−4.5	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.5	7.4	7.1
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kołno

$\varphi = 53°25'$ $\lambda = 21°56'$

I	–	–	–	–	−0.4	−6.7	5.6	4	−23.0	26	−4.8	−2.0	−3.6	−3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.9	7.5
II	–	–	–	–	3.0	−1.3	12.5	18	−5.4	6	−0.3	1.8	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.6	8.2	8.7
III	–	–	–	–	8.9	0.0	17.0	10	−5.4	20	2.0	6.7	3.3	3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.3	5.6	7.6
IV	–	–	–	–	14.6	2.6	23.9	15	−4.5	10	5.5	13.0	7.7	8.5	–	–	–	–	–	–	–	–	–	–	–	–	4.2	3.0	2.7	3.3
V	–	–	–	–	17.4	6.7	25.6	28	1.5	23	10.0	15.6	10.5	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	6.5	7.2
VI	–	–	–	–	23.3	12.3	31.3	27	7.1	21	16.1	21.9	15.9	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.6	5.6	5.2
VII	–	–	–	–	20.9	10.4	30.4	3	6.2	6	14.2	19.2	14.9	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.3	6.9	6.7
VIII	–	–	–	–	20.1	11.6	29.3	6	6.5	18	14.0	19.0	14.9	15.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.1	6.3	7.0
IX	–	–	–	–	19.3	8.1	28.0	3	1.7	28	9.7	18.3	12.1	13.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	3.4	2.9	3.6
X	–	–	–	–	14.0	6.1	19.1	4	0.3	23	7.2	13.3	9.5	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.2	4.2	4.9
XI	–	–	–	–	4.8	0.5	11.8	3	−6.4	23	2.2	4.0	2.7	2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.8	8.0	8.5
XII	–	–	–	–	−1.6	−8.2	14.6	5	−24.8	27	−5.0	−3.3	−4.9	−4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	4.9	6.6
Rok	–	–	–	–	12.0	3.5	31.3	27.VI	−24.8	27.XII	5.9	10.6	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	5.7	6.4

Szczecin – Dąbie

$H_s = 1\ m$ $H_b = 6{,}9\ m$ $h_w = 20\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%, ‰] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Min<0°	Max<0°	Max>25°	Wiatr v >10	>15	●	●	Opad R ≥0,1	≥1,0	≥10,0	≡	▦	≋
I	1	4.0	-	-	7	3.0	19.5	4.0	11	4.5	3.2	4.5	4.5	2.1	3	4.7	15	3.5	35.9	5.9	13	5	10	20	-	-	-	9	15	14	12	-	3	7	-
II	2	3.5	1	3.0	2	2.5	11	4.5	9	5.2	2.9	4.4	9	3.6	11	2.7	10	3.6	56.0	13.8	11	-	-	9	-	-	-	-	17	15	9	2	6	2	-
III	6	4.8	0.5	2.0	-	-	-	-	-	-	1.8	4.9	43.5	5.6	18	6.0	7	5.1	44.6	7.3	29	-	-	3	-	4	-	1	15	18	12	-	3	-	-
IV	8	2.5	1.2	3.4	11.5	4.0	2.0	5.4	6	5.4	12.5	3.9	8	3.8	8	2.1	4	3.8	26.7	7.7	14	-	-	3	-	2	-	6	8	9	6	-	3	1	2
V	13.5	4.9	1.1	3.5	3.5	2.1	3.5	5.6	3	6.0	1.3	3.7	2.1	3.8	10.5	3.7	14	3.4	127.5	20.8	29	-	-	-	-	-	-	-	15	21	19	5	4	-	8
VI	5	2.8	2	1.8	8.5	2.6	4	4.9	6	5.2	1.8	4.1	2.6	4.3	13.5	4.3	7	3.7	62.2	26.3	13	-	-	-	8	-	-	1	4	10	7	2	1	-	5
VII	2	5.0	-	-	3.5	2.9	2.5	5.2	2	6.0	3.4	4.6	3.7	4.0	6	4.9	6	4.1	88.8	14.3	21	-	-	-	3	-	-	2	17	18	15	2	1	-	5
VIII	3	1.3	2	3.0	1	1.0	4.5	3.4	4	3.5	2.6.5	4.1	2.2	4.2	7	5.1	13	3.4	67.0	17.6	3	-	-	-	1	-	-	2	14	21	16	1	4	-	2
IX	2.5	1.8	2	1.8	8.5	3.3	15.5	4.4	12	4.4	19.5	3.9	11.5	4.3	3.5	3.9	15	3.3	21.8	8.6	14	-	-	-	6	1	-	11	8	7	5	-	8	-	1
X	0.5	1.0	-	-	10.5	5.4	20.5	7.2	15	6.2	2.9	4.2	7	3.3	4.5	3.6	6	4.9	38.7	13.5	20	-	-	-	-	4	-	7	12	10	8	1	5	-	-
XI	3.5	3.3	12.5	2.7	9	4.4	3	2.8	6	4.6	2.4.5	4.4	11	3.9	1.5	2.0	19	3.1	26.4	6.2	13	-	-	7	-	1	-	2	18	14	8	-	8	-	-
XII	5	3.9	3	3.3	6.5	2.3	10	2.7	6.5	2.6	2.6.5	4.2	2.2.5	4.0	3	2.0	10	3.2	47.7	10.6	4	9	11	20	-	2	-	4	14	13	10	2	3	16	-
Rok	5.2	3.2	4.6	2.0	7.1.5	2.8	11.4	4.2	8.0.5	4.5	2.9.2.5	4.2	2.2.3	3.9	8.9.5	3.8	12.6	3.8	663.3	26.3	13.VI	14	21	62	18	14	-	45	157	170	126	15	49	26	23

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Wierzchowo

$H_s = 140\ m$ $h_w = 13\ m$

I	1	4.5	5.5	3.2	6.5	2.8	16.5	3.4	30.5	3.8	17.5	4.5	7.5	4.2	1	5.5	7	3.5	36.4	9.7	29	9	11	23	-	2	1	9	14	11	9	-	8	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	41.5	14.7	27	-	1	13	-	-	-	-	-	-	-	-	-	-	-	-
III	4.5	4.6	-	-	-	-	-	-	0.5	1.0	7	5.4	4.6	6.4	3.3	6.2	2	6.0	30.7	6.6	27	-	-	7	-	12	3	3	10	11	8	-	5	-	-
IV	10.5	3.1	3.5	3.6	14.5	4.1	23.5	4.8	9	5.2	6	3.3	4	2.9	11	3.3	8	3.7	12.5	4.7	8	-	-	9	-	1	-	9	4	7	3	-	2	-	-
V	2.3	4.0	8	4.1	5	3.0	7.5	2.7	8	3.2	11	3.8	15	3.5	11.5	2.9	4	3.4	85.5	16.7	5	-	-	1	-	1	-	2	5	15	12	3	-	-	-
VI	11	3.1	2	1.5	5.5	2.5	11	2.7	8.5	2.7	6	3.2	20.5	4.0	17.5	4.0	8	3.1	62.5	53.5	31	-	-	-	7	-	-	3	2	11	11	2	-	-	-
VII	8.5	3.3	1.5	1.7	1	1.5	7	3.0	5.5	2.6	2.4.5	3.5	2.7.5	3.1	17.5	3.3	-	3.2	142.2	16.5	13	-	-	-	4	1	-	2	7	19	18	4	1	-	-
VIII	9	2.3	1	1.0	-	-	-	-	9	2.7	2.2.5	3.3	20	3.7	2.2.5	3.4	9	2.9	95.4	21.5	10	-	-	-	3	-	-	3	6	17	15	4	1	-	-
IX	6.5	1.3	0.5	4.0	9	2.5	15.5	2.7	8.5	2.8	13.5	3.1	17	3.2	13.5	2.8	6	2.6	28.3	6.8	7	-	-	1	4	-	-	14	5	7	6	-	2	-	-
X	15	3.0	-	-	12.5	4.5	23	4.0	19.5	3.7	19	3.1	5.5	2.6	7	3.1	5	3.4	40.8	11.5	31	-	-	-	-	1	-	6	11	10	9	1	1	-	-
XI	8	2.1	6	4.8	7.5	4.4	15.5	3.1	9.5	2.0	19	3.7	10.5	3.9	9	2.7	5	3.1	32.4	12.6	30	-	-	8	-	2	-	1	16	14	10	1	6	-	-
XII	6.5	3.5	2	3.5	6.5	3.0	10.5	3.0	13	2.5	20	3.8	16.5	3.8	9	2.9	9	3.0	34.1	11.7	4	10	13	26	-	1	-	2	14	9	6	1	8	-	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	642.3	53.5	31.VII	19	25	88	18	-	-	-	-	-	-	-	-	-	-

Jastrowie

$H_s = 120\ m$

I	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
III	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IV	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	77.2	13.8	10	-	-	-	3	-	-	-	-	20	13	3	-	-	-
IX	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	46.0	15.2	5	-	-	-	4	-	-	-	-	9	7	2	-	-	1
X	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	40.4	9.3	17	-	-	-	-	-	-	5	9	13	9	-	1	-	-
XI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	29.8	5.0	27	-	-	7	-	-	-	4	21	17	10	-	5	-	-
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	32.3	7.6	1	10	-	25	-	-	-	1	16	12	6	-	3	21	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Kołna

$H_s = 128\ m$ $h_w = 13\ m$ (I–V), $16.5\ m$ (VI–XII)

I	12	6.3	3	2.7	6	2.5	8	3.4	20.5	4.1	12.5	6.8	11	5.3	10	5.3	10	4.4	33.2	12.3	5	11	11	30	-	3	1	-	-	15	8	1	1	27	-
II	4	2.7	-	-	-	-	9.5	3.9	20.5	5.2	12.5	3.5	8.5	3.8	4	3.5	20	3.1	19.5	5.8	11	-	2	20	-	2	-	-	-	11	7	-	11	3	-
III	25	10.0	2	7.5	3	5.7	3	6.2	5.5	3.3	30	7.6	20	7.2	19	5.4	8	6.2	26.3	6.2	30	-	-	15	-	8	5	-	-	14	9	-	5	-	-
IV	12	3.5	6.5	3.5	17	3.9	12.5	4.8	9	3.8	1.5	8.3	10	5.4	9.5	4.3	12	3.7	30.2	10.9	7	-	-	11	-	4	-	-	-	8	6	1	2	2	1
V	8	6.1	2	2.5	4	2.5	10	4.6	11	4.5	11.5	3.8	13	3.8	18.5	3.5	15	3.4	107.9	22.0	10	-	-	-	2	1	-	-	16	14	5	2	-	4
VI	9.5	4.2	1	3.0	6.5	3.9	11.5	3.6	6	4.5	17	4.5	21.5	5.1	12	5.0	5	4.3	64.8	13.3	22	-	-	-	11	2	-	-	-	11	10	2	1	-	7
VII	8	4.7	3	4.2	0.5	3.0	5	9.2	7.5	3.9	26	4.6	14.5	4.6	17.5	4.5	11	4.2	91.5	22.4	28	-	-	-	3	2	1	-	-	20	14	3	1	-	2
VIII	2	2.5	1	3.0	1	3.0	1	5.0	4	5.9	28	5.1	33	4.9	17	4.3	6	4.5	61.9	11.8	27	-	-	-	2	3	-	-	-	16	14	1	2	-	3
IX	9	3.8	1	2.0	5	2.6	10.5	3.0	3.5	3.3	13	5.8	11.5	4.4	13.5	5.7	23	3.3	54.0	27.9	14	-	-	-	5	4	-	-	-	8	7	1	9	-	2
X	1	2.0	4	5.0	2.5	4.1	3.0	7.2	25.5	3.8	2	2.5	3.5	6.7	8.5	3.8	11	4.6	7.2	3.0	29	-	-	-	-	5	1	-	-	5	3	-	9	-	-
XI	10	9.3	3	10.7	11	7.0	9	4.9	10	3.7	13	6.2	22	6.5	3	3.0	9	5.7	42.1	8.0	8	-	2	14	-	9	1	-	-	16	10	-	4	1	-
XII	17.5	7.2	3	15.0	3	3.6	12	3.9	9	4.3	12.5	8.4	17	5.3	11	3.9	8	5.4	19.5	5.0	4	11	17	27	-	9	5	-	-	12	5	-	5	16	-
Rok	9.5.5	5.2	2.8.5	4.9	6.4.5	3.6	12.2	5.0	13.2	4.2	18.4.5	5.6	18.5.5	5.2	14.3.5	4.4	13.8	4.4	55.8.1	27.9	14.IX	22	32	117	23	52	14	-	-	152	107	14	52	49	19

Sokółka

$\varphi = 53°24'$ $\lambda = 23°30'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−1.9	−7.3	6.5	4	−24.0	26	−5.4	−3.0	−4.3	−4.2	4.3	4.6	4.5	4.5	96	88	94	93	0.1	0.6	0.2	0.3	7.5	7.6	7.7	7.6
II	–	–	–	–	1.9	−2.1	7.9	18	−6.2	6	−1.2	0.9	−0.3	−0.2	5.5	6.1	5.8	5.8	96	93	96	95	0.2	0.4	0.3	0.3	9.3	8.6	8.4	8.8
III	–	–	–	–	6.9	0.2	15.2	10	−4.8	20	1.6	5.3	2.7	3.1	6.5	7.0	6.5	6.7	93	78	86	86	0.5	2.2	1.1	1.3	8.4	7.7	5.9	7.3
IV	–	–	–	–	13.6	2.2	24.2	7	−5.2	2	5.1	12.1	7.4	8.0	7.3	7.4	7.9	7.5	81	53	76	70	1.8	7.8	2.7	4.1	4.4	4.4	2.9	3.9
V	–	–	–	–	16.7	6.9	26.0	30	2.0	23	10.1	15.4	10.7	11.7	10.5	10.7	10.8	10.7	84	62	83	76	2.2	7.4	2.4	4.0	6.3	6.9	6.6	6.6
VI	–	–	–	–	22.8	12.2	31.1	27	5.4	21	16.1	21.0	16.5	17.5	14.6	14.1	14.5	14.4	80	58	77	72	3.8	11.5	4.5	6.6	4.7	5.6	5.3	5.2
VII	–	–	–	–	21.1	11.3	29.0	3	7.7	7	14.3	19.3	15.3	16.0	14.0	13.8	14.1	14.0	86	63	82	77	2.4	9.0	3.5	5.0	6.0	6.8	6.5	6.4
VIII	–	–	–	–	20.4	11.6	28.9	6	7.4	18, 30	13.6	19.3	14.5	15.5	14.0	14.6	14.3	14.3	90	65	86	80	1.7	8.2	2.4	4.1	6.8	6.3	5.2	6.1
IX	–	–	–	–	18.4	7.9	27.7	3	1.1	22	9.8	17.3	11.8	12.7	11.4	12.6	12.0	12.0	91	64	85	80	1.1	7.9	2.0	3.7	5.6	5.3	2.7	4.5
X	–	–	–	–	13.7	5.4	18.2	4	−0.7	23	6.2	12.9	8.9	9.2	8.7	9.9	9.3	9.3	90	67	81	79	0.9	5.2	2.1	2.7	6.9	5.6	4.5	5.7
XI	–	–	–	–	4.3	0.3	11.0	2	−5.7	24	1.8	3.4	2.1	2.4	6.8	7.1	6.8	6.9	95	89	92	92	0.4	1.0	0.6	0.7	9.2	8.3	7.7	8.4
XII	–	–	–	–	−2.1	−8.5	13.1	5	−23.8	27	−5.5	−3.6	−5.2	−4.9	4.3	4.5	4.3	4.4	90	85	88	88	0.4	0.8	0.5	0.6	8.5	6.8	5.3	6.9
Rok	–	–	–	–	11.3	3.3	31.1	27 VI	−24.0	26. I	5.5	10.0	6.7	7.2	9.0	9.4	9.2	9.2	89	72	86	82	1.3	5.2	1.9	2.8	7.0	6.7	5.7	6.5

Zawodzie

$\varphi = 53°23'$ $\lambda = 21°24'$

I	–	–	–	–	−0.4	−6.5	4.7	4, 5	−21.4	26	−4.5	−1.5	−3.5	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	7.7	7.8
II	–	–	–	–	3.0	−1.4	12.9	18	−6.0	5	−0.2	2.4	0.6	0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.0	7.9	8.4
III	–	–	–	–	8.9	0.3	16.9	10	−6.2	20	2.6	7.1	3.3	4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.5	5.3	7.2
IV	–	–	–	–	14.4	1.5	24.0	7	−5.7	11	6.0	12.9	6.8	8.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.6	4.1	5.1
V	–	–	–	–	16.7	5.9	25.0	28	0.3	19	10.1	15.5	9.8	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	7.7	7.6
VI	–	–	–	–	23.1	11.1	32.5	27	5.9	1	16.2	22.4	15.6	17.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	5.6	5.9
VII	–	–	–	–	20.9	9.9	30.5	3	5.2	6	14.3	19.1	14.3	15.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.9	7.5	7.5
VIII	–	–	–	–	20.0	10.8	28.5	6	5.8	31	14.0	18.8	14.0	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	6.5	7.2
IX	–	–	–	–	19.3	7.1	28.0	2, 17	−0.4	23	9.5	18.4	10.9	12.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.7	4.3	4.6
X	–	–	–	–	14.0	5.5	19.0	4	0.6	28	7.0	13.4	9.3	9.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.3	4.9	5.7
XI	–	–	–	–	5.0	0.0	12.2	3	−9.5	23	2.1	4.1	2.4	2.8	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.2	7.7	8.4
XII	–	–	–	–	−1.4	−8.4	14.4	5	−25.6	27	−5.5	−2.9	−5.2	−4.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	5.6	6.6
Rok	–	–	–	–	12.0	3.0	32.5	27 VI	−25.6	27 XII	6.0	10.8	6.5	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.9	6.2	6.8

Płusza

$\varphi = 53°22'$ $\lambda = 16°48'$

I	–	–	–	–	0.4	−6.3	6.1	29	−20.1	27	−4.2	−0.2	−3.2	−2.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.8	5.6	6.0
II	–	–	–	–	4.6	−0.8	12.5	18	−6.8	5	1.0	3.8	1.7	2.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	7.3	8.2
III	–	–	–	–	9.3	1.8	17.7	10	−8.3	20	3.7	8.2	4.6	5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.9	5.6	6.9
IV	–	–	–	–	14.6	3.1	22.7	7	−4.4	10	6.3	12.8	8.1	8.8	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.4	4.5	4.8
V	–	–	–	–	15.4	5.0	22.7	5	−1.5	13	9.8	13.7	9.0	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.3	6.1	6.8
VI	–	–	–	–	22.8	11.1	28.4	26	3.2	22	16.1	21.5	15.8	17.3	–	–	–	–	–	–	–	–	–	–	–	–	4.1	5.9	4.6	4.9
VII	–	–	–	–	20.1	10.6	32.6	3	3.7	1	14.3	18.5	14.4	15.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.9	7.3	7.9
VIII	–	–	–	–	19.9	10.1	28.6	6	5.1	14	13.5	18.5	14.1	15.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	6.3	6.9
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–		–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Nidzica

$\varphi = 53°22'$ $\lambda = 20°25'$

I	–	–	–	–	−1.0	−6.5	5.1	4, 5	−22.4	26	−4.8	−1.7	−3.5	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.5	7.2	7.6
II	–	–	–	–	2.2	−1.7	10.4	18	−6.4	5	−0.4	1.8	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.6	8.0	8.6
III	–	–	–	–	7.7	0.6	15.1	10	−5.1	20	2.7	6.5	3.4	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.7	5.0	6.7
IV	–	–	–	–	13.5	2.4	22.4	7	−4.2	10	6.0	12.4	7.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.4	4.0	4.8
V	–	–	–	–	15.7	5.4	23.9	28	−0.9	19	9.9	14.5	9.6	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	6.3	6.9
VI	–	–	–	–	22.7	11.4	30.4	27	4.7	21	17.0	21.5	15.8	17.5	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	5.8	5.7
VII	–	–	–	–	20.3	9.8	30.0	3	5.1	6	14.4	18.6	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.9	7.9	7.9
VIII	–	–	–	–	19.3	10.8	27.9	6	6.0	14	13.6	19.0	13.9	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.4	7.0	7.3
IX	–	–	–	–	18.9	7.5	26.8	2	0.0	27	10.3	18.3	11.4	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.8	3.5	4.4
X	–	–	–	–	13.8	5.8	19.0	4	0.8	13	7.8	13.3	9.0	9.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.7	4.8	5.7
XI	–	–	–	–	4.9	0.4	10.6	4	−8.5	23	2.0	4.0	2.3	2.6	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.1	7.6	8.3
XII	–	–	–	–	−1.7	−8.8	13.2	5	−22.6	27	−5.5	−3.4	−5.4	−4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.6	5.7	6.7
Rok	–	–	–	–	11.4	3.1	30.4	27 VI	−22.6	27 XII	6.1	10.3	6.5	7.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	6.1	6.7

Sokółka $H_s = 180\,m$ $h_w = 17\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU ºD, ºmD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	v>15	◐	●	Opad R ≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	17	4.6	3	1.7	1.5	4.7	15.5	4.6	14.5	6.3	15	6.2	18.5	5.2	8	3.8	·	5.1	29.5	5.8	12	11	16	31	·	3	·	2	16	19	7	·	3	25	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	9.8	3.6	1	·	6	26	·	—	—	(1)	(22)	7²	4²	·	12	15	·
III	3	2.7	·	·	1	2.0	1	7.0	6.5	6.9	13	6.3	46	7.5	22.5	8.0	·	7.2	56.9	12.9	30	·	·	13	·	15	1	·	15	20	11	1	3	3	·
IV	11	3.8	7	4.0	19	4.6	13.5	5.9	3	3.2	11	4.6	9	5.7	16	3.7	·	4.6	25.6	7.0	7	·	·	11	·	3	1	11	5	10	9	·	2	3	2
V	21.5	3.3	4.5	3.0	17	3.5	4	4.8	7	3.4	5	2.6	11.5	3.0	17.5	2.6	5	3.0	61.7	12.3	30	·	·	·	2	1	1	3	10	18	13	1	4	·	3
VI	6.5	2.2	9	3.0	15.5	4.5	7.5	4.3	7	5.1	7.5	5.5	16.5	5.2	20.5	5.5	·	4.7	88.1	23.1	28	·	·	·	10	3	1	5	5	16	15	2	·	·	8
VII	5	2.9	4	3.4	4	4.5	3	3.3	7	5.4	11	5.5	38	5.3	21	3.1	·	4.5	88.9	37.0	28	·	·	·	3	3	·	2	9	13	7	2	4	·	4
VIII	8	3.5	3.5	2.9	2	2.0	2	2.5	8.5	6.5	12.5	6.7	35	5.0	21.5	5.2	·	5.1	60.4	11.5	10	·	·	·	3	6	·	·	5	17	12	1	1	·	6
IX	10	2.5	13.5	2.3	4.5	4.7	4	2.5	1.5	3.3	11.5	6.0	20	4.8	23	4.7	2	4.0	49.7	23.0	14	·	·	·	4	3	2	9	5	8	6	2	6	·	2
X	4	2.0	10	4.3	14.5	6.9	30.5	7.2	11	5.0	4	3.9	8.5	4.4	10.5	3.2	·	5.5	6.0	2.9	14	·		1	·	5	·	7	9	5	2	·	10	·	·
XI	6.5	4.1	4.5	4.6	15.5	7.9	18.5	5.2	6	4.3	8	5.3	18.5	6.3	12.5	3.6	·	5.5	37.6	5.8	10	·	5	16	·	6	·	·	19	21	9	·	6	7	·
XII	20	5.3	5	3.9	6	5.0	11.5	4.0	9.5	3.8	13	7.1	15.5	6.6	12.5	5.4	·	5.4	27.5	5.5	20	12	17	27	·	6	2	4	14	19	7	·	4	21	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	541.7	37.0	28.VII	23	44	125	22	—	—	44	134	173²	102²	9	55	74	25

Zawodzie $H_s = 122\,m$ $h_w = 12\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	9	1.6	6	1.7	3	2.7	12	2.0	16	2.0	18.5	3.4	9.5	3.4	6	2.3	13	2.1	31.7	7.6	5	10	12	28	·	·	·	2	16	15	8	·	4	14	·
II	2.5	1.4	2	2.5	1.5	2.3	8	2.6	18	2.8	18.5	2.3	19	2.4	2.5	1.4	12	2.1	18.9	8.3	11	·	1	22	·	·	·	·	18	16	4	·	8	1	·
III	·	·	·	·	·	·	0.5	5.0	2	3.0	24.5	4.8	53	4.0	13	4.5	·	4.2	19.7	5.0	29	·	·	13	·	5	·	·	12	12	6	·	2	2	·
IV	2.5	1.2	10.5	2.5	10.5	3.5	16.5	3.2	4.5	2.6	10	2.8	13	3.3	9.5	3.2	13	2.6	27.8	11.8	7	·	·	12	·	·	·	7	7	9	7	1	3	·	1
V	6.5	2.5	3	2.2	6.5	2.1	7.5	2.5	6.5	2.2	18.5	2.7	14.5	3.4	15	3.1	15	2.3	92.8	13.0	6	·	·	·	1	·	·	·	15	18	15	4	·	·	4
VI	1.5	2.3	3.5	3.0	8	2.7	8	2.1	5.5	1.9	24	2.7	24.5	3.3	7	2.3	8	2.5	102.6	27.4	8	·		·	11	·	·	3	8	15	10	3	2	·	7
VII	2.5	2.2	1	2.0	3.5	2.3	4	2.6	4.5	2.1	36	2.4	26.5	2.8	12	2.1	3	2.4	89.4	22.5	28	·	·	·	3	·	·	1	17	20	14	3	·	·	4
VIII	3.5	1.9	4	1.9	1	1.5	·	·	4	2.2	32.5	2.9	33.5	3.1	7.5	2.1	7	2.6	64.3	11.5	6, 20	·	·	·	2	·	·	2	13	18	13	2	·	·	2
IX	3.5	1.8	6.5	2.1	12.5	1.6	1.5	1.0	4	1.6	17.5	2.5	24	3.2	6.5	2.0	14	2.0	47.6	30.5	14	·	·	1	5	·	·	12	7	7	5	1	3	·	2
X	·	·	4.5	2.3	25	2.6	26	2.8	14	2.1	10.5	2.5	8	2.8	2	2.5	3	2.5	9.1	2.6	9	·	·	·	·	·		6	11	8	3	·	7	·	·
XI	11.5	3.0	5.5	4.5	13	3.5	7	1.9	8.5	2.9	24	2.7	13	3.2	5.5	2.6	2	2.9	50.1	7.5	10	·	2	14	·	·	·	·	20	20	11	·	6	·	·
XII	9.5	2.7	7	2.9	3	2.3	8.5	1.9	11.5	1.5	22	2.8	22.5	3.0	5	2.4	4	2.4	27.4	7.3	2	11	14	28		·	·	5	13	14	8	·	4	20	·
Rok	52.5	1.7	53.5	2.3	87.5	2.3	99.5	2.3	99	2.2	256.5	2.9	261	3.2	91.5	2.5	94	2.6	581.4	30.5	14.IX	21	29	118	22	5	·	38	157	172	104	14	39	37	20

Płusza $H_s = 95\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40.0	12.8	30	12	12	24	·	—	—	8	14	14	11	1	2	—	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	43.5	13.0	9	·	·	19	·	—	—	1	16	11	8	2	7	—	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	50.6	6.8	22	·	·	8	·	—	—	2	11	17	15	·	4	—	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	32.7	10.0	28	·	·	7	·	—	—	8	7	9	9	1	·	—	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	74.4	10.5	5	·	·	1		—	—	1	14	17	13	2	·	·	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	43.5	14.0	7	·	·	·	10	—	—	6	5	9	6	1	·	·	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	157.8	57.0	31	·	·	·	4	—	—	2	16	19	19	4	1	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	70.3	13.5	6	·	·	·	3	—	—	2	10	17	14	1	·	·	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	34.9	12.2	5	—	—	—	—	—	—	—	—	8	6	2	—	—	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39.0	10.4	17	—	—	—	—	—	—	—	—	12	9	1	—	—	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	39.7	10.0	30	—	—	—	—	—	—	—	—	12	7	1	—	—	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	31.1	10.6	4	—	—	—	—	—	—	—	—	12	7	1	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	657.5	57.0	31.VII	—	—	—	—	—	—	—	—	157	124	17	—	—	—

Nidzica $H_s = 170\,m$ $h_w = 13\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	6.5	2.1	5	2.8	1	1.0	12.5	3.6	9.5	2.7	24.5	4.1	2.5	3.4	11.5	3.4	20	2.6	36.3	5.8	30	9	13	29	·	·	·	2	15	13	10	·	4	—	
II	1	2.0	2.5	2.2	0.5	3.0	17	3.3	6.5	5.5	19	3.3	5.5	2.4	15	2.4	17	2.5	30.8	5.6	9	·	4	25	·	1	·	1	19	11	10	·	12	—	·
III	·	·	·	·	·	·	·	·	·	·	16.5	4.7	34	4.6	36.5	5.2	6	4.5	40.5	11.2	30	·		11	·	4	1	1	10	13	11	1	2	—	
IV	4	2.8	4	2.6	6.5	2.7	19	3.4	5	2.6	8	2.7	5.5	3.2	11	4.3	27	2.3	27.8	11.6	7	·	·	11	·	1	·	9	6	8	7	1	—	·	1
V	10	3.0	5	3.0	3	1.3	5	3.8	8.5	3.5	14	4.3	5.5	3.4	14	3.4	28	2.4	58.8	16.5	7	·	·	2	·	·			9	12	12	2	—	·	3
VI	1	2.0	·	·	6	2.2	13	3.8	7.5	3.9	12	4.7	14.5	3.9	17	4.1	19	3.1	83.9	31.4	8		·	·	10	·		2	5	9	9	3	·	·	3
VII	3.5	2.6	1.5	2.7	1	2.0	3	4.7	8.5	3.4	37	3.8	17.5	4.1	7	3.6	14	3.2	100.0	17.4	16	·	·	·	3	·		1	18	17	16	3	·	·	3
VIII	3	2.7	3	2.0	2	1.5	·	·	4.5	3.3	38	4.1	10.5	3.9	18	3.5	14	3.1	121.7	35.4	10	·		·	2			1	11	20	20	2	·	·	4
IX	5	2.2	2	2.0	3	2.0	6.5	3.1	5	2.5	18.5	4.4	8.5	3.4	9.5	3.0	32	2.1	36.2	17.9	14	·		·	4	·		10	7	7	5	1	4	·	1
X	0.5	3.0	2.5	3.2	11.5	3.5	29	4.3	13	3.9	10.5	2.4	2.5	4.8	4.5	2.5	19	3.0	15.9	8.5	29	·		·	·	·	·	4	7	7	4	·	—	·	
XI	14	3.0	6	4.0	6	3.8	11	3.3	8.5	3.0	17.5	5.0	4.5	3.0	7.5	3.0	15	3.0	61.3	9.4	29		1	13	·		·	·	19	15	12	·	—		·
XII	11	4.0	4	2.6	·	·	5	3.0	7.5	2.7	27.5	4.5	6.5	3.0	16.5	2.8	15	3.0	49.9	9.7	2	12	17	27	·	2	·	5	15	8	8	·	—	—	
Rok	59.5	2.4	35.5	2.3	40.5	1.9	121	3.0	84	3.1	243	4.0	112.5	3.6	168	3.4	226	2.9	663.1	35.4	10.VIII	21	35	118	19	8	1	36	141	140	124	13	—	—	15²

Lipki

$\varphi = 53°21'$ $\lambda = 14°58'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.8	-4.0	6.2	30	-14.6	27	-2.7	0.0	-2.1	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	6.4	6.8
II	–	–	–	–	6.4	0.4	12.8	28	-4.4	5, 6	2.0	5.3	2.8	3.2	6.6	7.6	6.9	7.0	93	85	92	90	0.5	1.4	0.6	0.8	9.5	7.6	7.2	8.1
III	–	–	–	–	9.7	2.1	17.3	10	-3.3	20	4.2	8.4	5.4	5.8	7.2	7.8	7.6	7.5	87	71	86	81	1.2	3.4	1.4	2.0	9.2	7.2	6.7	7.7
IV	–	–	–	–	15.0	4.5	25.2	14	-0.7	11	7.7	13.6	9.3	10.0	8.4	8.8	8.9	8.7	78	57	75	70	2.4	7.7	3.2	4.4	5.8	5.2	5.3	5.4
V	–	–	–	–	15.0	6.7	21.9	26	(2.0)	29	9.5	13.4	9.8	10.6	10.4	10.7	10.3	10.5	87	70	85	81	1.5	5.0	1.9	2.8	8.0	6.5	8.5	7.7
VI	–	–	–	–	22.3	11.9	27.0	25, 26	8.6	13	15.7	20.6	16.0	17.1	14.5	15.0	14.7	14.7	81	62	81	75	3.5	9.9	3.7	5.7	4.9	5.9	4.9	5.2
VII	–	–	–	–	20.0	12.0	31.6	3	8.7	6	14.4	18.2	14.8	15.6	14.3	15.0	14.5	14.6	87	71	85	81	2.3	6.7	2.6	3.9	7.9	7.3	7.8	7.7
VIII	–	–	–	–	20.1	11.4	26.2	31	7.6	8	14.0	18.7	14.6	15.5	14.5	14.7	14.6	14.6	90	69	87	82	1.6	7.2	2.2	3.7	–	–	–	–
IX	–	–	–	–	20.6	10.1	28.5	2	0.9	27	11.7	19.8	13.8	14.8	12.6	13.6	13.4	13.2	89	60	84	78	1.5	10.0	2.5	4.7	–	–	–	–
X	–	–	–	–	14.9	7.8	21.4	6	2.5	14	9.1	14.3	10.7	11.2	10.1	10.9	11.0	10.7	88	68	86	81	1.5	5.8	2.0	3.1	5.9	5.1	4.7	5.2
XI	–	–	–	–	6.6	1.6	11.9	2	-6.4	22	3.0	5.8	3.7	4.0	7.1	7.6	7.3	7.3	91	82	90	88	0.7	1.7	0.8	1.1	8.2	7.3	7.7	7.7
XII	–	–	–	–	0.7	-6.3	13.8	5	-22.5	26	-3.5	-1.0	-2.9	-2.6	4.8	5.3	5.0	5.0	86	86	89	87	0.6	1.0	0.6	0.7	7.1	6.1	7.3	6.8
Rok	–	–	–	–	12.7	4.8	31.6	3.VII	-22.5	26.XII	7.1	11.4	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wałcz

$\varphi = 53°17'$ $\lambda = 16°28'$

I	1004.0	1029.4	981.2	1018.4	0.3	-4.8	5.8	29	-16.5	26	-3.6	-0.4	-2.4	-2.2	4.4	4.8	4.7	4.6	86	76	84	82	0.6	1.3	0.7	0.9	6.7	6.1	5.6	6.1
II	1006.0	1022.8	976.8	1020.3	4.9	0.1	12.3	18	-5.9	5	1.2	3.7	2.4	2.4	6.2	6.8	6.6	6.5	93	84	90	89	0.5	1.3	0.8	0.9	9.0	8.5	7.5	8.3
III	1002.0	1021.5	973.5	1016.0	9.1	2.3	18.3	10	-4.6	20	3.8	8.1	4.9	5.4	7.2	7.2	7.4	7.3	89	67	84	80	1.0	3.9	1.4	2.1	8.6	7.8	6.2	7.5
IV	998.6	1011.1	988.0	1012.4	14.9	4.2	24.0	14	-2.0	10	6.1	13.2	9.0	9.3	7.8	8.3	8.6	8.2	81	55	73	70	1.9	7.8	3.3	4.3	5.4	5.5	4.4	5.1
V	998.1	1007.8	984.6	1011.9	15.4	6.3	21.7	26	1.5	13	9.4	13.8	10.1	10.8	9.9	10.7	10.1	10.2	84	69	81	78	2.0	5.4	2.4	3.3	7.0	8.5	5.9	7.1
VI	1000.8	1014.4	988.2	1014.2	22.8	12.0	28.8	26	7.6	22	15.9	21.2	16.6	17.6	14.1	13.9	14.8	14.3	78	56	78	71	4.1	11.9	4.3	6.8	5.6	6.7	4.8	5.7
VII	998.2	1012.9	982.9	1011.7	19.7	11.7	32.4	3	7.6	1	14.0	18.3	14.9	15.5	13.9	14.1	14.0	14.0	87	69	83	80	2.2	7.8	3.1	4.4	8.5	8.3	7.8	8.2
VIII	1001.1	1015.7	988.5	1014.6	19.8	11.4	27.4	6	7.6	14	13.6	18.4	14.6	15.3	14.1	14.6	14.8	14.5	90	70	88	83	1.5	7.1	2.1	3.6	7.9	7.7	6.2	7.3
IX	1004.1	1015.6	989.0	1017.7	20.3	9.2	29.6	2	1.1	25	10.9	19.5	12.9	14.0	12.1	13.5	13.3	13.0	90	59	87	79	1.4	9.9	2.0	4.4	4.6	4.6	3.3	4.2
X	1003.4	1016.0	975.7	1017.2	14.5	7.5	20.5	6	3.4	31	8.7	13.7	10.5	10.8	10.1	10.9	10.9	10.6	89	70	86	82	1.2	5.1	1.9	2.7	7.2	6.6	5.3	6.4
XI	999.7	1022.6	982.3	1013.8	6.1	1.7	11.4	2	-8.1	23	3.1	5.4	3.6	3.9	7.1	7.2	7.1	7.1	90	80	88	86	0.8	1.8	1.0	1.2	9.1	8.8	8.1	8.7
XII	1001.1	1033.7	972.2	1015.6	-0.2	-6.6	14.1	5	-20.7	26	-3.7	-1.5	-3.9	-3.2	4.6	4.8	4.3	4.6	85	81	84	83	0.7	1.2	0.8	0.9	6.9	7.1	5.0	6.3
Rok	1001.4	1033.7	972.2	1015.3	12.3	4.6	32.4	3.VII	-20.7	26.XII	6.6	11.1	7.8	8.3	9.3	9.7	9.7	9.6	87	70	84	80	1.5	5.4	2.0	3.0	7.2	7.2	5.8	6.7

Lidzbark

$\varphi = 53°16'$ $\lambda = 19°50'$

I	–	–	–	–	-0.5	-5.9	5.1	4	-21.0	26	-4.5	-1.5	-3.4	-3.2	4.3	4.7	4.5	4.5	88	80	87	85	0.4	0.9	0.5	0.6	7.9	7.6	7.4	7.6
II	–	–	–	–	3.2	-1.0	11.2	18	-5.5	5	0.3	1.9	0.7	0.9	6.1	6.4	6.2	6.2	97	91	95	94	0.2	0.7	0.3	0.4	9.3	8.5	9.1	9.0
III	–	–	–	–	8.4	0.7	15.5	10	-6.8	20	3.0	6.6	3.8	4.3	6.9	6.8	6.9	6.9	90	70	86	82	0.8	3.2	1.2	1.7	8.3	6.9	7.4	7.5
IV	–	–	–	–	13.9	2.9	23.2	7	-3.2	10	6.6	12.3	7.8	8.5	7.4	7.4	8.0	7.6	73	51	73	66	2.7	7.7	3.0	4.5	5.1	5.8	5.0	5.3
V	–	–	–	–	15.7	6.2	23.5	28	0.9	19	9.7	13.9	9.7	10.8	10.0	10.2	10.4	10.2	82	64	85	77	2.3	6.1	1.9	3.4	7.4	8.4	7.3	7.7
VI	–	–	–	–	23.4	12.1	32.5	27	5.5	1	16.4	21.8	16.4	17.8	14.8	12.7	14.7	14.0	79	49	79	69	4.1	14.3	4.1	7.5	5.3	5.6	5.8	5.6
VII	–	–	–	–	20.5	10.6	32.3	3	6.7	6	13.9	18.8	15.0	15.7	13.9	12.9	14.0	13.6	87	61	82	77	2.3	9.5	3.3	5.0	7.3	7.7	8.4	7.9
VIII	–	–	–	–	19.6	11.0	28.3	6	6.9	30	13.4	17.8	14.9	15.2	13.9	14.4	14.7	14.3	91	71	86	83	1.5	6.5	2.5	3.5	7.3	7.4	7.7	7.5
IX	–	–	–	–	19.1	8.5	27.6	17	1.0	28	10.9	17.7	13.2	14.0	12.1	12.8	13.1	12.7	91	62	86	80	1.3	8.0	2.3	3.9	4.5	3.2	3.5	3.7
X	–	–	–	–	13.6	6.3	19.1	4	1.8	10	8.2	12.8	9.6	10.0	9.8	10.6	10.0	10.1	89	71	83	81	1.2	4.7	2.0	2.7	6.9	6.7	6.5	6.7
XI	–	–	–	–	4.9	0.6	10.5	3	-8.2	23	2.2	3.8	2.7	2.8	7.0	7.2	7.0	7.1	94	87	91	91	0.4	1.1	0.7	0.7	9.1	8.2	8.1	8.5
XII	–	–	–	–	-1.2	-7.7	14.1	5	-26.6	27	-4.9	-3.2	-4.5	-4.3	4.4	4.3	4.3	4.3	84	76	84	81	0.6	1.1	0.7	0.8	7.2	6.7	7.0	7.0
Rok	–	–	–	–	11.7	3.7	32.5	27.VI	-26.6	27.XII	6.3	10.2	7.2	7.7	9.2	9.2	9.5	9.3	87	69	85	80	1.5	5.3	1.9	2.9	7.1	6.9	6.9	7.0

Kisielnica

$\varphi = 53°15'$ $\lambda = 22°07'$

I	–	–	–	–	-1.2	-7.0	5.7	4	-24.9	26	-5.0	-2.4	-3.7	-3.7	4.1	4.5	4.4	4.3	87	82	86	85	0.5	0.9	0.6	0.7	7.3	7.5	7.4	7.4
II	–	–	–	–	2.2	-1.3	10.2	18	-4.9	6	-0.3	1.6	0.4	0.5	5.6	5.9	5.8	5.8	93	86	92	90	0.4	1.1	0.5	0.7	9.5	8.3	8.2	8.7
III	–	–	–	–	7.4	0.2	14.9	10	-5.5	20	2.1	6.5	3.3	3.8	6.5	6.9	6.7	6.7	90	70	85	82	0.7	3.1	1.2	1.7	8.2	7.3	5.9	7.1
IV	–	–	–	–	13.3	2.3	23.0	15	-3.7	21	5.8	12.5	7.2	8.2	7.3	7.5	7.7	7.5	77	51	74	67	2.2	7.9	2.9	4.3	4.6	4.7	2.9	4.1
V	–	–	–	–	16.1	6.5	25.1	28, 29	0.6	15	10.3	15.4	10.4	11.6	10.6	10.1	10.9	10.5	83	59	85	76	2.2	8.0	2.0	4.1	7.7	7.8	5.9	7.1
VI	–	–	–	–	23.1	11.8	30.8	27	6.1	1	16.3	21.7	16.2	17.6	14.7	14.0	14.4	14.4	79	55	78	71	4.1	12.6	4.3	7.0	5.8	6.4	5.8	5.7
VII	–	–	–	–	20.6	10.2	29.8	3	5.3	6	14.2	18.8	14.6	15.6	14.0	13.6	13.9	13.8	86	64	84	78	2.3	8.6	3.0	4.6	6.7	7.9	7.5	7.4
VIII	–	–	–	–	20.2	11.4	29.5	6	6.6	18	13.8	19.2	14.4	15.4	14.2	14.0	14.3	14.2	90	63	87	80	1.7	8.5	2.2	4.1	7.5	6.8	5.9	6.7
IX	–	–	–	–	19.3	7.5	29.0	2	1.2	23, 27	10.3	18.2	11.2	12.7	11.6	12.3	12.0	12.0	91	58	88	79	1.2	9.3	1.6	4.0	4.9	4.3	2.7	4.0
X	–	–	–	–	14.1	5.5	19.0	4	0.2	23	6.9	13.1	9.2	9.6	9.0	10.2	9.5	9.6	90	69	81	80	1.0	5.2	2.3	2.8	6.4	5.0	4.4	5.3
XI	–	–	–	–	4.8	0.4	10.8	2, 3	-5.9	23, 24	2.0	3.8	2.4	2.6	6.7	7.1	6.9	6.9	92	87	92	90	0.6	1.2	0.6	0.8	8.8	8.3	7.6	8.2
XII	–	–	–	–	-1.5	-8.7	13.8	5	-24.9	27	-5.5	-3.5	-5.5	-5.0	4.1	4.3	4.1	4.2	86	79	84	83	0.6	1.0	0.7	0.8	8.1	6.2	4.7	6.3
Rok	–	–	–	–	11.5	3.2	30.8	27.VI	-24.9	26.I, 27.XII	5.9	10.4	6.7	7.4	9.0	9.2	9.2	9.1	87	69	85	80	1.5	5.6	1.8	3.0	7.1	6.6	5.7	6.5

Lipki $H_s = 30\,m$ $h_w = 10\,m$ 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	⊠	R f0
I	2.5	1.8	4.5	2.3	13	1.7	24.5	1.9	25	1.9	15	2.1	5	2.4	3.5	2.1	·	2.0	44.6	11.2	30	4	11	22	·	·	·	7	16	8	6	1	9	?	·
II	2	1.0	3.5	2.1	5	2.2	13.5	2.5	18.5	2.1	18	2.6	12	2.1	11.5	2.0	·	2.2	51.7	11.5	27	·	·	12	·	·	·	·	15	9	8	2	14	·	·
III	0.5	3.0	1	2.0	1	4.0	·	·	7.5	2.2	21.5	5.4	33	3.8	28.5	2.7	·	3.7	46.6	6.5	30	·	·	6	·	4	·	·	17	16	13	·	13	·	
IV	8	2.9	10.5	2.4	26.5	3.4	10	4.1	11.5	3.3	9	2.3	2.5	4.2	12	2.8	·	3.1	13.0	4.8	7	·	·	3	1	·	·	3	6	4	4	·	5	·	·
V	19	4.3	2	2.6	1	5.0	6	4.0	10	3.4	10.5	3.7	17.5	4.3	13	4.9	14	3.5	98.9	11.7	7	·	·	·	·	·	·	·	13	21	18	2	·	·	6
VI	7	3.0	2.5	3.4	8.5	3.2	5	4.3	7	3.5	13.5	4.1	28	5.4	5.5	4.7	13	3.7	48.3	15.8	13	·	·	·	8	2	·	4	3	9	6	3	·	·	5
VII	·	·	1.5	2.7	3	3.2	1	4.0	11	3.8	35	4.0	25.5	4.1	3	4.8	13	3.4	95.0	13.1	18	·	·	·	3	·	·	3	17	20	17	4	1	·	4
VIII	2	2.5	·	·	3	2.0	5	2.3	11	3.0	24.5	4.4	22.5	5.1	6	3.2	19	3.2	59.1	11.5	10	·	·	·	2	·	·	—	—	19	12	2	5	·	2
IX	2.5	2.4	0.5	2.0	16	3.8	15.5	3.6	11.5	3.2	12.5	4.2	13.5	5.0	5	2.9	13	3.3	22.9	8.1	14	·	·	·	5	1	·	—	—	5	4	·	4	·	2
X	1	2.0	1	4.0	18.5	5.6	22.5	4.8	21.5	3.6	9	4.2	5	3.7	5.5	2.8	9	4.0	24.2	12.7	20	·	·	·	·	1	·	8	13	7	5	1	6	·	·
XI	7.5	3.5	5.5	4.6	14	3.8	7	3.6	13	4.4	14.5	5.1	7.5	4.9	2	3.7	19	3.4	34.0	8.4	13	·	·	8	·	·	·	5	20	11	8	·	9	·	·
XII	1	4.0	1	4.5	16	2.9	15	3.4	13	3.8	16.5	6.4	14.5	3.7	8	3.6	8	3.7	46.0	13.4	4	9	12	21	·	2	·	2	15	9	8	2	5	10	·
Rok	53	2.5	33.5	2.7	125.5	3.4	125	3.2	160.5	3.2	199.5	4.0	186.5	4.1	103.5	3.4	108	3.3	584.3	17.7	7.V	13	23	72	19	10	·	—	—	138	109	17	71	10?	19

Wałcz $H_s = 111\,m$ $H_b = 113{,}8\,m$ $h_w = 23\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	⊠	R f0
I	5	1.2	4	2.1	20.5	1.7	6.5	2.1	12.5	1.9	23.5	2.6	8	1.7	5	1.4	8	1.8	39.3	12.5	30	7	12	22	·	·	·	8	14	14	10	1	·	·	·
II	3	1.0	6	1.7	7	2.6	4	4.8	13.5	2.0	15	2.0	25.5	2.3	7	2.3	3	2.2	51.0	19.0	9	·	·	14	·	1	·	1	19	12	8	1	7	2	·
III	·	·	·	·	·	·	·	·	2.5	4.0	18.5	4.2	66	4.3	5	3.0	1	4.2	55.4	11.0	29	·	·	5	·	10	·	1	13	20	12	1	1	2	·
IV	5	1.9	20.5	2.4	18.5	2.9	2	3.0	6	1.2	9	2.1	14	1.9	11	1.7	4	2.1	31.4	5.4	8	·	·	5	·	1	·	7	6	11	11	·	·	·	1
V	5	2.2	3.5	2.0	8	2.1	1	2.0	2.5	3.2	14	2.9	33	2.0	23	2.1	3	2.2	97.8	19.8	5	·	·	·	·	·	·	1	15	17	15	4	·	·	3
VI	1	1.0	5	1.6	7	2.4	4	2.8	0.5	2.0	16	3.0	35	2.7	14.5	1.1	7	2.2	57.4	20.1	4	·	·	·	9	·	·	3	6	12	7	2	·	·	4
VII	·	·	1.5	1.7	2.5	2.6	·	·	6.5	1.8	42.5	2.5	31	2.2	4	1.6	5	2.2	129.3	46.1	31	·	·	·	4	·	·	2	20	22	19	2	·	·	5
VIII	1.5	1.7	·	·	1	2.0	1	2.0	2	1.5	30	2.4	46	2.3	4.5	1.4	7	2.1	73.5	17.4	6	·	·	·	3	·	·	1	12	22	12	1	·	·	4
IX	3	1.8	12.5	2.2	3.5	3.3	2.5	1.0	3.5	2.7	14.5	3.0	27.5	2.0	3	1.0	20	1.7	30.7	11.4	7	·	·	·	5	·	·	13	8	11	6	2	·	·	2
X	2	1.0	17	3.3	18	3.0	6.5	1.9	8	2.6	13.5	2.1	21	1.7	1	1.0	6	2.2	37.5	9.6	17	·	·	·	·	·	·	6	13	13	8	·	·	·	·
XI	6.5	1.9	10.5	3.8	5.5	1.5	1	1.0	4	2.4	20.5	3.3	21	2.0	14	1.6	7	2.3	31.8	11.9	30	·	·	8	·	·	·	1	21	16	6	1	2	·	·
XII	5	1.2	6	1.5	6	1.7	8	1.8	6	1.4	17.5	3.8	25.5	2.5	10	1.7	9	2.1	47.7	14.3	4	10	14	23	·	1	·	6	13	15	9	1	·	17	·
Rok	37	1.2	86.5	1.9	97.5	2.2	36.5	1.9	67.5	2.2	234.5	2.8	353.5	2.3	102	1.7	80	2.3	682.8	46.1	31.VII	17	26	77	21	13		50	160	185	123	16	10	21	19

Lidzbark $H_s = 150\,m$ $h_w = 11\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	⊠	R f0
I	3.5	2.0	3.5	1.7	1	4.0	11.5	3.0	18.5	2.9	21	3.2	9	2.3	3	2.0	22	2.2	11.6	4.6	11	10	12	26	·	1	·	1	18	8	4	·	—	10	—
II	0.5	1.0	·	·	1	3.0	15.5	2.8	15.5	3.4	24	2.9	12.5	3.1	1	2.0	14	2.5	20.2	6.9	11	·	4	21	·	1	·	·	22	12	6	·	—	6	—
III	12	5.9	9.5	5.9	·	·	1	2.0	4	2.2	25	4.3	26	4.5	8.5	4.2	7	4.3	19.2	3.7	29	·	·	12	·	5	·	·	16	15	8	·	5	·	—
IV	4.5	2.1	6	2.2	11.5	3.3	20	4.4	6	2.2	9.5	1.9	5.5	4.0	7	2.8	20	2.5	34.6	14.2	7	·	·	10	·	1	·	8	7	13	10	1	·	2	—
V	7	2.1	4	2.5	5	1.6	6.5	2.8	10.5	3.3	14.5	1.8	18	1.9	10.5	2.0	17	1.8	68.9	30.9	7	·	·	·	·	·	·	·	13	15	13	1	2	·	—
VI	·	·	0.5	2.0	8.5	2.8	12	2.8	9.5	2.5	21.5	2.9	18	3.1	·	·	20	2.2	28.4	6.7	12	·	·	·	12	·	·	2	7	8	7	·	1	·	—
VII	2	2.0	1.5	1.0	0.5	1.0	5.5	4.0	11.5	2.0	33	3.5	13.5	3.2	2.5	2.0	23	2.3	83.0	15.0	13	·	·	·	4	1	·	2	19	20	14	3	1	·	—
VIII	·	·	1	1.0	2	1.0	1	1.0	7.5	2.1	37	4.5	20	2.7	1.5	2.0	23	2.6	77.5	18.0	2	·	·	·	2	2	·	1	13	17	14	2	4	·	—
IX	1	4.0	·	·	12.5	2.3	6.5	3.3	13.5	2.1	25	3.3	15	4.4	1.5	3.0	15	2.6	38.8	14.7	14	·	·	·	4	1	·	12	5	9	7	1	3	·	—
X	·	·	0.5	1.0	16	5.0	30.5	4.2	18.5	2.8	8.5	2.7	8.5	3.2	0.5	2.0	10	3.4	14.9	6.2	29	·	·	·	·	3	·	5	15	7	5	·	10	·	—
XI	5.5	3.4	4.5	3.5	12.5	4.5	11	2.8	9.5	2.6	21	3.8	6.5	2.8	3.5	2.4	16	2.8	43.8	8.2	27	·	1	14	·	·	·	1	22	13	11	·	9	·	—
XII	5.5	4.3	6	3.5	0.5	3.0	7.5	2.2	11.5	3.4	25	4.1	14	3.9	2	1.0	21	2.8	30.1	10.4	2	12	14	27	·	3	·	5	17	10	7	1	10	22	—
Rok	41.5	2.2	37	2.0	71	2.6	128.5	2.9	136	2.6	265	3.2	166.5	3.3	41.5	2.1	208	2.7	471.0	30.9	7.V	22	31	110	22	18	·	37	174	147	106	9	—	40	—

Kisielnica $H_s = 140\,m$ $h_w = 18\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	⊠	R f0
I	8.5	3.9	8	1.6	3.5	2.1	16	3.7	10.5	3.2	27	3.8	13	3.0	6.5	4.3	·	3.4	37.3	10.0	5	11	12	29	·	·	·	2	15	13	9	1	4	29	·
II	·	·	6	2.2	4.5	2.6	13.5	2.9	16.5	3.8	20	2.8	15.5	4.0	6	2.2	2	3.1	18.1	5.0	11	·	4	21	·	·	·	·	20	11	9	·	6	7	·
III	·	·	·	·	·	·	1	5.0	4	5.1	36.5	5.3	40.5	5.8	11	5.6	1	5.5	30.0	8.5	30	·	·	13	·	11	1	2	15	12	9	·	4	2	·
IV	8	3.2	8.5	4.6	12.5	4.8	23	3.1	3	2.3	15	3.3	7	4.3	9	3.8	4	3.5	25.0	8.8	7	·	·	11	·	1	·	11	5	10	7	·	1	3	2
V	6	3.0	4.5	3.6	5.5	3.8	9.5	4.3	6.5	3.6	11	2.8	23	2.9	17	3.6	10	3.0	64.4	13.1	10	·	·	·	2	·	·	·	10	14	14	2	1	·	1
VI	2	1.5	6.5	2.4	17.5	2.9	8.5	2.6	7	2.8	18	2.9	23	4.4	5.5	3.5	2	3.1	99.8	34.0	8	·	·	·	10	·	·	4	9	9	8	5	·	·	4
VII	3.5	2.0	5.5	3.2	5.5	2.3	1.5	6.3	9.5	3.8	29.5	2.9	27	3.1	5	3.4	6	2.9	78.6	21.7	30	·	·	·	3	·	·	1	11	15	15	3	1	·	1
VIII	5.5	1.4	4	2.0	·	·	2	1.5	4	2.0	28	3.4	36	3.6	11.5	3.5	2	3.1	62.3	12.9	15	·	·	·	2	1	·	1	10	14	13	2	2	·	4
IX	2.5	1.8	15.5	2.3	11	2.3	4	2.5	1.5	1.7	16	2.9	26.5	3.5	6	2.7	7	2.6	44.7	26.0	14	·	·	·	5	1	·	11	4	6	6	1	5	·	2
X	0.5	1.0	5	2.2	20.5	3.6	29.5	3.8	2.5	3.3	10	2.4	6.5	2.6	5.5	3.0	8	3.0	9.0	4.3	26	·	·	·	·	·	·	8	8	3	3	·	8	·	·
XI	4.5	3.4	5.5	5.1	13.5	7.0	12	2.8	8.5	2.5	15	3.3	18	3.1	6	2.8	7	3.5	46.2	8.0	8	·	2	15	·	3	1	1	20	14	11	·	7	·	·
XII	9.5	5.7	10.5	3.6	5	3.6	13.5	3.1	8	3.2	15	4.3	21	3.6	7.5	4.3	3	3.8	29.2	9.7	20	11	15	26	·	3	·	5	13	10	7	·	3	20	·
Rok	50.5	2.2	78.5	2.7	99	2.9	134	3.5	86.5	3.1	240	3.3	257	3.7	96.5	3.6	52	3.4	544.6	34.0	8.VI	22	33	115	22	20	2	46	140	131	111	14	42	61	14

Kopna Góra

$\varphi = 53°15'$ $\lambda = 23°29'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−1.1	−7.7	8.3	4	−28.2	26	−5.6	−2.3	−4.4	−4.2	4.3	4.6	4.4	4.4	92	85	91	89	0.3	0.8	0.3	0.5	7.8	8.0	2.6	7.8
II	–	–	–	–	2.4	−2.3	9.3	18	−9.0	6	−0.9	1.5	−0.2	0.0	5.4	6.0	5.8	5.7	95	88	94	92	0.3	0.9	0.4	0.5	9.1	8.0	7.5	8.2
III	–	–	–	–	7.7	−0.2	16.3	10	−7.4	23	1.6	6.2	2.9	3.4	6.4	6.8	6.5	6.6	91	72	85	83	0.6	3.0	1.2	1.6	8.5	7.0	5.7	7.1
IV	–	–	–	–	14.1	1.0	24.0	7, 15	−6.2	11	5.0	12.7	7.0	7.9	7.2	6.8	7.8	7.3	80	47	77	68	1.9	8.9	2.6	4.5	4.1	4.0	3.2	3.8
V	–	–	–	–	17.1	6.0	27.0	30	−0.7	23	10.2	15.7	10.4	11.7	10.5	10.0	10.8	10.4	84	58	85	76	2.3	8.6	2.2	4.4	6.5	6.6	6.2	6.4
VI	–	–	–	–	23.4	10.8	31.8	27	2.4	21	16.2	21.2	16.4	17.6	14.8	14.2	15.0	14.7	82	59	81	74	3.8	11.9	4.0	6.6	5.1	5.7	4.3	5.0
VII	–	–	–	–	21.3	10.5	29.5	3	6.4	6	14.4	19.4	14.9	15.9	14.1	13.7	14.7	14.2	86	62	86	78	2.4	9.3	2.6	4.8	5.3	7.0	6.3	6.2
VIII	–	–	–	–	20.7	11.2	29.0	6	4.7	18	13.8	19.5	14.3	15.5	14.1	14.1	14.7	14.3	89	63	89	80	1.8	9.0	1.8	4.2	6.7	6.0	4.8	5.8
IX	–	–	–	–	19.2	6.2	28.3	3	−2.4	23	9.8	18.1	10.7	12.1	11.1	12.4	12.0	11.8	94	60	91	82	0.8	9.1	1.4	3.8	5.7	4.3	3.0	4.3
X	–	–	–	–	14.4	5.2	18.9	4	0.0	23	6.2	13.4	9.4	9.6	8.6	10.0	9.4	9.3	89	66	80	78	1.0	5.5	2.5	3.0	6.7	5.3	4.5	5.5
XI	–	–	–	–	4.8	0.1	11.8	2	−8.0	24	1.9	3.7	2.2	2.5	6.8	7.3	6.9	7.0	94	89	93	92	0.4	1.0	0.6	0.7	9.1	8.5	8.4	8.7
XII	–	–	–	–	−1.3	−9.0	12.8	5	−25.7	27	−5.8	−3.0	−5.5	−5.0	4.3	4.7	4.3	4.4	90	84	89	88	0.4	0.8	0.5	0.6	7.7	7.3	5.8	6.8
Rok	–	–	–	–	11.9	26	31.8	27.VI	−28.2	26. I	5.5	10.5	6.5	7.2	9.0	9.2	9.4	9.2	89	69	87	82	1.3	5.7	1.7	2.9	6.9	6.5	5.6	6.3

Drawno

$\varphi = 53°13'$ $\lambda = 15°46'$

I	–	–	–	–	0.8	−5.0	6.3	29	−15.9	27	−3.6	0.0	−2.3	−2.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	5.1	−0.5	11.5	28	−5.5	5	1.8	3.9	2.1	2.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	9.1	2.3	17.9	10	−4.8	20	4.5	8.1	4.8	5.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.0	4.5	23.9	14	−1.1	1	7.6	13.7	8.9	9.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.1	6.8	21.7	26	3.4	12	10.5	13.6	10.0	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	22.5	12.3	28.1	26	7.6	22	16.4	20.7	16.7	17.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	19.8	12.1	31.7	3	8.6	6, 30	14.6	18.4	14.7	15.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.2	11.8	27.5	27	8.2	8	14.3	18.6	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.4	9.8	28.5	2	2.0	27	12.2	19.5	13.7	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.5	7.4	20.6	6	1.2	31	9.3	13.9	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.3	1.6	12.2	2	−6.1	22, 23	3.2	5.6	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	0.0	−7.0	13.9	5	−22.5	26	−3.7	−1.4	−3.6	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.4	4.7	31.7	3.VII	−22.5	26. XII	7.3	11.2	7.8	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kańczewice

$\varphi = 53°11'$ $\lambda = 18°33'$

I	–	–	–	–	−0.3	−5.0	5.1	4	−16.0	26	−3.8	−1.2	−2.8	−2.6	4.3	4.9	4.6	4.6	84	83	85	84	0.6	0.8	0.6	0.7	7.2	7.4	5.7	6.8
II	–	–	–	–	3.0	−0.5	9.8	28	−5.1	6	0.6	2.4	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	9.0	1.5	16.8	10	−5.6	20	3.6	7.5	4.7	5.1	7.4	7.6	7.5	7.5	92	74	87	84	0.7	3.1	1.3	1.7	7.9	5.9	5.7	6.5
IV	–	–	–	–	14.2	3.8	24.2	7	−1.9	10	6.2	12.5	8.5	8.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.0	4.4	4.7
V	–	–	–	–	15.7	6.2	22.8	26, 27	1.4	13	9.5	13.7	9.7	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.5	7.2	7.6
VI	–	–	–	–	23.5	11.9	31.7	27	5.9	22	15.5	21.9	16.8	17.8	–	–	–	–	–	–	–	–	–	–	–	–	4.1	5.0	5.3	4.8
VII	–	–	–	–	20.4	11.0	31.9	3	6.0	1	14.4	17.9	14.4	15.3	14.6	14.3	14.7	14.5	89	71	89	83	2.0	7.1	2.0	3.7	7.5	7.5	8.7	7.9
VIII	–	–	–	–	19.9	11.0	28.4	6	7.4	14	13.7	18.2	14.1	15.0	14.6	14.6	14.7	14.6	92	70	91	84	1.3	6.8	1.6	3.2	7.4	6.4	6.5	6.8
IX	–	–	–	–	19.8	8.8	28.1	2	1.8	25	11.5	18.6	12.8	13.9	12.3	13.6	12.9	12.9	89	63	86	79	1.6	9.4	2.1	4.0	4.6	5.0	4.5	4.7
X	–	–	–	–	14.4	7.0	18.7	5, 6	2.2	14	8.1	13.4	10.2	10.5	10.2	11.4	11.0	10.9	93	75	88	85	0.7	4.2	1.5	2.1	7.2	6.5	5.2	6.3
XI	–	–	–	–	5.5	1.1	10.8	2	−5.2	23	2.4	4.6	2.8	3.2	7.2	7.7	7.4	7.4	97	90	96	94	0.2	0.9	0.3	0.5	8.2	7.8	7.9	8.0
XII	–	–	–	–	−0.4	−7.1	14.6	5	−19.1	28	−4.2	−2.1	−4.2	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.0	7.5	7.8
Rok	–	–	–	–	12.1	4.1	31.9	3. VII	−19.1	28.XII	6.5	10.6	7.4	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wyrzysk

$\varphi = 53°09'$ $\lambda = 17°16'$

I	–	–	–	–	0.5	–	5.8	29	–	–	−3.8	−0.2	−2.7	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.8	5.2	5.9
II	–	–	–	–	4.8	–	11.7	28	–	–	1.1	3.7	1.8	2.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.1	7.3	8.1
III	–	–	–	–	9.7	2.1	18.3	10	−5.4	20	3.7	8.7	4.5	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	5.9	6.2	6.6
IV	–	–	–	–	14.9	4.3	24.5	7	−1.1	10	6.5	13.6	8.3	9.2	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.5	3.3	3.9
V	–	–	–	–	15.9	5.9	21.5	26	0.5	13	10.2	14.5	9.5	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.4	12.1	28.9	26	6.1	22	16.5	22.0	15.7	17.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.6	11.7	33.1	3	7.9	6	14.5	19.0	13.9	15.3	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.2	7.0	7.1
VIII	–	–	–	–	20.3	11.5	28.5	6	6.9	14	14.1	19.2	14.0	15.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.5	9.2	28.5	1–3, 17	2.2	28	11.9	19.7	12.4	14.1	–	–	–	–	–	–	–	–	–	–	–	–	3.1	3.5	2.6	3.1
X	–	–	–	–	14.6	7.3	20.5	6	1.7	31	8.6	14.1	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.1	4.3	5.4
XI	–	–	–	–	6.2	1.5	11.5	2	−8.3	23	2.7	5.4	3.1	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	7.6	8.1
XII	–	–	–	–	−0.2	−6.8	14.5	5	−20.5	26	−3.8	−1.4	−4.2	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.3	4.8	5.4
Rok	–	–	–	–	12.6	–	33.1	3.VII	–	–	6.8	11.5	7.2	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kopna Góra — $H_s = 160$ m — $h_w = 15$ m — 1961

MIESIĄC	ROZKŁAD WIATRU °D, v=D — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) Temperatura T — Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v — v > 10	v > 15	◔	●	Opad R — R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	℞
I	13	2.8	1	5.0	2.5	2.8	12.5	3.2	18	2.6	18.5	3.2	6.5	3.4	11	2.1	10	2.6	36.7	6.6	12, 31	12	13	28	·	·	·	1	16	21	9	·	4	23	·
II	2	2.0	2	2.0	3	3.0	8	3.2	14.5	4.2	17.5	3.0	13.5	2.8	6.5	2.1	17	2.5	20.0	5.6	11	·	6	21	·	·	·	1	19	14	5	·	12	15	·
III	1	2.0	·	·	·	·	1	4.0	4	3.2	40	4.9	28.5	5.0	10.5	4.7	8	4.3	59.6	14.9	30	·	·	15	·	3	·	1	15	20	12	1	4	2	·
IV	9.5	2.7	4	2.8	15.5	3.3	8	3.1	9.5	3.3	8.5	2.9	8.5	3.3	9.5	3.5	17	2.6	20.8	4.1	4	·	·	13	·	1	1	12	5	8	8	·	4	3	1
V	8	3.1	1	3.0	11	3.9	6	3.0	9.5	2.4	13.5	2.7	12.5	1.9	9.5	2.9	22	2.2	65.4	12.5	16	·	·	2	3	·	·	3	10	18	12	1	3	·	6
VI	3	2.0	3	3.8	17.5	3.0	8	1.9	11.5	2.5	13	2.7	20	3.1	7	2.1	7	2.5	69.9	12.8	28	·	·	·	13	1	·	6	7	18	13	2	1	·	7
VII	4	3.2	·	·	4.5	2.0	1.5	2.7	14.5	2.7	31.5	3.4	13.5	3.3	2.5	2.8	21	2.4	102.2	29.6	28	·	·	·	4	·	·	3	9	14	8	4	3	·	4
VIII	7	4.1	2	3.0	·	·	·	·	13.5	2.9	27	3.9	18.5	2.9	6	2.8	19	2.7	82.9	19.5	10	·	·	·	3	·	·	3	7	16	14	2	2	·	7
IX	8.5	2.1	1.5	1.6	6.5	2.2	2	2.0	9.5	3.3	12.5	3.2	16	2.8	8.5	2.4	25	2.0	37.4	18.3	14	·	·	4	5	·	·	9	5	8	6	1	6	·	3
X	·	·	3.5	2.9	22.5	4.6	21	4.0	20.5	2.8	2.5	3.0	8.5	1.8	1.5	2.0	13	3.0	10.1	5.9	14	·	·	·	·	·	·	·	·	5	3	·	11	·	·
XI	6	3.0	2.5	3.2	18.5	4.1	10	3.0	8	3.1	21	3.2	7	2.6	2	2.5	15	2.7	47.2	8.9	10	·	3	17	·	·	·	·	22	20	11	·	10	·	·
XII	13	4.2	3.5	5.1	4.5	2.6	10	2.9	15.5	2.5	16.5	4.2	10	2.6	8	2.9	12	2.9	37.4	8.7	20	12	17	27	·	·	·	4	14	18	10	·	1	20	·
Rok	75	2.6	24	2.7	106	2.6	88	2.8	148.5	3.0	222	3.4	163	3.0	82.5	2.7	186	2.7	589.6	29.6	28. VII	24	39	127	28	5	1	43	129	180	111	11	61	63	28

Drawno — $H_s = 82$ m

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40.9	9.6	30	6	10	25	·	—	—	—	—	17	9	·	·	·	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	64.9	12.2	9	·	·	19	·	—	—	—	—	18	11	3	·	1	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	51.2	10.2	29	·	·	6	·	—	—	—	—	13	11	1	5	1	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	23.8	5.7	1	·	·	4		—	—	—	—	8	7	·	3	·	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	68.2	16.5	7	·	·	·	·	—	—	—	—	18	13	1	3	·	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	85.8	20.1	14	·	·	·	10	—	—	—	—	12	11	4	1	·	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	116.9	42.0	31	·	·	·	4	—	—	—	—	23	16	1	—	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	57.0	10.7	10	·	·	·	3	—	—	—	—	21	18	1	1	·	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	36.1	10.1	14	·	·	·	4	—	—	—	—	7	6	1	—	·	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	35.6	6.6	23	·	·	·	·	—	—	—	—	13	9	·	18	·	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	44.3	14.5	30	·	·	7	·	—	—	—	—	16	11	2	4	·	—
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	51.5	17.2	11	9	13	24	·	—	—	—	—	12	5	3	2	19	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	676.2	42.0	31. VII	15	23	85	21	—	—	—	—	178	127	17	—	21	—

Kończewice — $H_s = 94$ m — $h_w = 12$ m

I	2	2.5	9.5	2.7	3.5	1.0	13.5	1.9	15.5	1.2	23.5	2.5	9	2.7	7.5	3.5	9	2.1	22.6	11.6	30	8	12	24	·	·	·	5	14	11	5	1	6	3	·
II	11	1.2	4	1.0	6	1.0	3.5	3.6	15	2.2	14.5	2.1	22	2.4	6	2.0	2	1.9	28.1	13.2	8	·	·	17	·	1	1	—	—	12	6	1	22	5	·
III	5	5.6	·	·	·	·	·	·	1	3.0	3	2.3	58.5	4.7	23.5	4.9	2	4.6	17.8	5.7	30	·	·	10	·	3	·	2	13	13	6	·	4	3	·
IV	11	2.5	7.5	2.2	29	2.5	5	3.8	4	2.0	3.5	2.1	10.5	2.9	11.5	2.7	8	2.4	37.2	11.7	29	·		7	·	·	·	11	7	10	7	1	—	1	6
V	26	2.2	5	1.8	7	1.3	2	2.0	3.5	3.0	6.5	3.3	24	2.3	10	1.6	9	2.0	83.2	21.1	6	·	·	·	·	·	·	2	15	15	11	2	3	·	7
VI	3	1.7	13	1.2	7.5	1.5	3	2.7	6	1.8	5.5	2.8	22.5	2.6	19.5	3.3	10	2.1	30.7	10.2	11	·	·	·	11	·	·	8	5	7	5	1	1	·	8
VII	2	1.5	1	1.0	1.5	2.3	4	1.8	8.5	2.5	19.5	3.2	26	3.6	7.5	2.9	23	2.3	175.5	50.3	31	·	·	·	4	·	·	2	18	23	19	5	7	·	12
VIII	2.5	1.0	2	3.0	2.5	1.8	0.5	1.0	1.5	1.0	20	2.6	27.5	3.9	10.5	3.0	26	2.2	52.8	10.3	11	·	·	·	1	1	·	2	12	15	13	1	8	·	4
IX	1.5	1.7	6.5	1.3	10	1.7	6	2.2	5	2.2	12	2.9	20	2.8	8	4.1	21	2.0	30.0	12.3	14	·	·	·	4	2	·	13	9	8	5	1	10	·	2
X	1	2.0	4	1.2	21	2.4	15	3.1	8.5	1.4	10.5	1.9	8	2.0	4	3.5	21	1.8	39.5	16.2	18	·	·	·	·	·	·	4	10	13	10	1	14	·	·
XI	10.5	2.0	8	3.8	9	3.7	8	2.8	3.5	2.7	19.5	4.1	13	3.7	4.5	1.4	14	2.8	44.2	8.4	27	·	·	14	·	1	·	2	20	16	11	·	11	1	·
XII	10	4.3	6	3.5	2	2.5	7	1.7	6.5	1.9	13.5	4.1	21.5	3.6	14.5	3.2	12	2.9	26.9	8.4	11	11	15	25	·	2	·	·	15	6	6	·	11	11	·
Rok	85.5	2.4	66.5	1.9	99	1.8	67.5	2.2	78.5	2.1	151.5	2.8	262.5	3.1	127	3.0	157	2.4	588.5	50.3	31. VII	19	27	97	20	10	1	—	—	149	104	14	—	24	39

Wyrzysk — $H_s = 90$ m — $h_w = 12$ m

I	6	1.3	2	2.0	8	2.6	1	4.0	14	3.4	5	3.2	25	3.2	7	2.1	25	2.1	33.5	11.5	30	—	11	—	·	1	·	—	—	12	9	1	2	·	
II	14	1.9	·	·	3	1.7	5	3.2	11	3.8	7	3.7	23	3.4	8	2.1	13	2.5	39.4	14.0	9	—	·	—	·	1	·	—	—	13	7	1	7	·	·
III	12	3.8	1	7.0	·	·	1	3.0	·	·	2	6.0	36	5.8	38	6.4	3	5.6	43.2	9.0	30	·	·	7	·	8	·	—	—	14	12	·	·	—	·
IV	7	3.3	7	2.6	8	3.2	18	4.7	16	4.2	4	3.8	11	3.1	10	3.4	9	3.4	57.4	14.5	28	·	·	7	·	·	·	—	—	11	9	2	·	·	2
V	20	2.8	2	5.0	3	2.0	·	·	10	3.1	3	3.7	18	2.8	16	4.1	21	2.5	60.8	9.0	5	·	·	·	·	1	·	—	—	17	15	·	·	·	4
VI	2	2.0	·	·	6	3.7	3	3.7	15	2.5	4	3.2	27	4.1	10	2.7	23	2.5	54.7	18.5	4	·	·	·	10	1	·	—	—	11	10	2	·	·	6
VII	2	4.0	1	1.0	·	·	1	3.0	3	1.7	10	3.2	54	3.3	6	3.7	16	2.7	165.9	75.0	31	·	·		4	3	·	—	—	23	19	3	·	·	4
VIII	7	1.4	1	3.0	3	3.0	·	·	1	4.0	7	3.0	34	3.9	12	3.8	28	2.4	70.0	10.0	7, 10	·		·	3	1	·	—	—	19	18	2	·	·	3
IX	3	2.3	·	·	7	3.4	7	3.7	4	3.2	6	2.3	23	3.4	1	7.0	39	1.9	24.4	11.0	14	·	·	·	5	2	·	—	—	7	4	1	·	·	2
X	2	1.0	·	·	4	2.0	22	4.3	16	3.1	9	3.8	10	2.4	5	2.0	25	2.4	34.7	7.5	18, 19	·	·	·	·	·	·	—	—	9	9	·	2	·	·
XI	10	2.9	2	6.0	6	7.8	6	2.7	7	1.9	4	3.5	26	3.8	3	3.3	26	2.7	27.2	9.5	30	·	·	8	·	1	·	—	—	12	6	·	7	·	·
XII	11	2.2	2	1.5	4	2.5	3	4.3	13	2.1	4	5.5	18	2.9	14	2.4	24	2.0	26.3	9.0	4	10	16	24	·	·	·	—	—	10	7	·	1	—	·
Rok	86	2.4	18	2.3	52	2.7	67	3.0	110	2.8	65	3.7	305	3.5	130	3.6	252	2.7	632.5	75.0	31. VII	—	27	—	22	19	·	—	—	158	125	12	19	—	21

Bydgoszcz, IMiUZ — φ = 53°08' — λ = 18°01' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.6	-5.0	5.7	4	-17.1	26	-3.9	-0.5	-2.4	-2.3	4.5	4.8	4.7	4.7	89	77	84	83	0.5	1.3	0.8	0.9	7.1	6.6	5.2	6.3
II	–	–	–	–	4.8	0.3	11.4	18	-3.9	5	1.3	3.6	2.3	2.4	6.3	6.7	6.5	6.5	93	84	90	89	0.5	1.3	0.8	0.9	9.8	8.9	6.4	8.3
III	–	–	–	–	9.8	2.8	17.7	10	-4.5	20	4.0	8.1	5.7	5.9	6.9	6.7	7.1	6.9	84	62	78	75	1.4	4.4	2.2	2.7	8.5	7.3	5.6	7.1
IV	–	–	–	–	14.8	4.3	24.3	7	-2.3	10	6.1	13.1	9.3	9.4	7.6	8.0	8.6	8.1	79	54	70	68	2.0	8.0	3.5	4.5	5.2	5.3	3.6	4.7
V	–	–	–	–	16.0	7.1	21.1	30	3.2	12	9.5	14.0	11.0	11.4	9.8	9.9	10.2	10.0	82	63	79	75	2.3	6.4	3.0	3.9	7.1	9.1	6.0	7.4
VI	–	–	–	–	23.9	13.3	30.0	27	7.5	22	16.4	17.0	18.2	16.7	14.0	12.5	14.6	13.7	75	48	70	64	4.8	14.6	6.6	8.7	4.4	5.0	5.6	5.0
VII	–	–	–	–	20.8	12.5	33.0	3	8.0	6	14.6	18.7	15.8	16.2	13.8	13.2	13.9	13.6	83	64	78	75	3.0	9.2	4.3	5.5	7.6	8.5	7.6	7.9
VIII	–	–	–	–	20.3	12.2	28.3	6	8.5	14	13.7	18.5	15.4	15.8	14.1	13.9	14.8	14.3	89	66	84	80	1.8	7.8	2.9	4.2	7.6	7.7	4.2	6.5
IX	–	–	–	–	20.3	9.3	28.9	2	1.6	28	10.8	19.2	13.3	14.2	12.0	12.9	13.1	12.7	90	58	84	77	1.3	10.0	2.6	4.6	5.8	4.7	3.5	4.7
X	–	–	–	–	14.9	7.6	20.1	6	3.2	31	8.4	14.1	10.6	10.9	10.1	11.2	11.0	10.8	91	71	86	83	1.0	5.0	1.8	2.6	7.6	6.5	5.0	6.4
XI	–	–	–	–	6.2	1.9	11.4	2	-8.3	23	3.0	5.2	3.6	3.8	7.2	7.5	7.4	7.4	92	83	91	89	0.7	1.5	0.8	1.0	9.2	8.6	8.2	8.7
XII	–	–	–	–	0.1	-6.2	15.2	5	-19.0	26	-3.7	-1.5	-3.5	-3.0	4.7	4.8	4.5	4.7	88	80	86	85	0.6	1.3	0.8	0.9	7.4	6.4	5.3	6.4
Rok	–	–	–	–	12.7	5.0	33.0	3.VII	-19.0	26.XII	6.7	11.2	8.3	8.6	9.2	9.3	9.7	9.4	86	68	82	79	1.7	5.9	2.5	3.4	7.3	7.0	5.5	6.6

Bydgoszcz — φ = 53°07' — λ = 17°58'

I	1010.1	1035.5	987.8	1019.1	0.5	-6.2	5.5	31	-21.4	26	-4.6	-0.5	-2.9	-2.7	4.4	5.0	4.7	4.7	88	81	86	85	0.4	1.0	0.6	0.7	6.5	6.9	6.4	6.6
II	1011.8	1027.9	983.8	1020.6	4.7	-0.5	11.8	18	-4.0	5	0.9	3.6	1.5	1.9	6.3	6.9	6.5	6.6	95	87	93	92	0.3	1.1	0.5	0.6	9.5	8.7	7.0	8.4
III	1006.9	1026.5	980.3	1015.6	9.7	1.8	17.9	10	-6.4	20	3.6	8.1	5.1	5.5	7.0	7.0	7.3	7.1	88	66	82	79	1.0	4.0	1.7	2.2	8.4	7.4	5.7	7.2
IV	1004.4	1015.9	994.3	1013.0	15.0	3.7	24.5	7	-5.0	10	6.2	13.2	8.8	9.2	7.8	8.5	8.6	8.3	84	57	73	71	2.0	7.7	3.2	4.3	5.2	5.3	4.1	4.9
V	1003.4	1011.5	990.1	1011.8	16.1	6.0	21.7	26	1.0	12	9.5	14.1	10.3	11.0	10.1	10.7	10.3	10.4	84	67	82	78	2.2	5.7	2.4	3.4	6.9	8.7	5.9	7.2
VI	1006.0	1019.1	993.9	1014.4	24.2	11.9	31.2	27	4.5	22	16.6	22.5	17.3	18.4	14.7	13.5	15.0	14.4	77	50	76	68	4.6	14.4	5.2	8.1	4.7	5.7	5.2	5.2
VII	1003.6	1018.3	988.1	1012.0	21.1	11.2	34.2	3	6.4	1	14.9	19.0	15.0	16.0	14.4	14.3	14.2	14.3	85	67	84	79	2.7	8.6	3.1	4.8	7.9	8.0	7.0	7.6
VIII	1006.4	1020.6	993.5	1014.8	20.5	11.0	29.5	6	6.0	14	13.8	18.3	14.5	15.3	14.6	14.6	14.8	14.7	92	70	89	84	1.3	6.9	1.9	3.4	7.7	7.9	4.9	6.8
IX	1009.7	1021.3	995.7	1018.2	20.4	8.4	29.2	2	0.3	27	11.0	19.4	12.6	13.9	12.5	14.2	13.1	13.3	93	63	89	82	1.0	8.9	1.8	3.9	4.6	4.6	3.8	4.3
X	1009.6	1021.6	982.1	1018.2	15.0	6.7	20.2	6	1.6	13	8.0	14.2	10.2	10.6	10.0	11.5	10.9	10.8	93	72	88	84	0.8	4.9	1.6	2.4	7.1	6.9	5.2	6.4
XI	1005.4	1027.5	989.7	1014.2	6.0	1.1	11.6	2	-9.4	23	2.6	5.1	3.1	3.5	7.2	7.8	7.4	7.5	95	87	93	92	0.4	1.2	0.5	0.7	9.0	8.7	8.4	8.7
XII	1006.7	1037.5	979.7	1015.8	-0.2	-7.2	15.0	5	-22.2	27	-4.2	-1.5	-3.8	-3.3	4.6	5.0	4.5	4.7	87	83	86	85	0.6	1.0	0.7	0.8	7.0	6.5	5.3	6.3
Rok	1007.0	1037.5	979.7	1015.7	12.8	4.0	34.2	3.VII	-22.2	27.XII	6.5	11.3	7.6	8.2	9.5	9.9	9.8	9.7	88	71	85	81	1.4	5.4	1.9	2.9	7.0	7.1	5.7	6.6

Mława — φ = 53°07' — λ = 20°22'

I	1001.0	1025.0	981.6	1019.6	-0.4	-6.9	5.6	4	-21.2	26	-4.4	-1.6	-3.4	-3.2	4.2	4.6	4.4	4.4	85	78	85	83	0.6	1.1	0.6	0.8	7.4	7.7	7.1	7.4
II	1002.8	1019.1	975.9	1021.3	3.1	-1.2	12.0	18	-4.2	5	0.1	2.1	0.8	1.0	5.8	6.2	6.0	6.0	93	87	91	90	0.4	0.9	0.6	0.6	8.9	8.8	7.4	8.4
III	996.0	1016.1	971.4	1014.1	8.9	0.9	16.4	10	-4.5	20	2.6	7.0	4.2	4.5	6.6	6.6	6.7	6.6	88	65	80	78	0.9	3.7	1.7	2.1	8.2	7.9	5.1	7.1
IV	995.6	1007.9	984.4	1013.4	14.7	3.1	24.0	7	-3.7	10	5.4	12.6	8.2	8.6	7.5	8.0	8.3	7.9	81	54	73	69	1.7	7.6	3.0	4.1	5.8	5.9	3.9	5.2
V	993.9	1001.2	982.2	1011.5	16.8	6.5	24.5	28	1.1	19	9.8	15.2	10.7	11.6	10.4	10.6	11.0	10.7	86	61	84	77	1.8	7.2	2.1	3.7	7.1	8.5	6.8	7.5
VI	996.9	1009.4	986.3	1014.1	23.9	12.6	32.6	27	6.6	1, 21	16.5	22.7	17.3	18.4	15.4	13.9	15.1	14.8	82	51	76	70	3.6	14.4	4.9	7.6	5.7	6.4	5.0	5.7
VII	994.7	1008.8	977.8	1012.0	21.2	10.8	31.8	3	6.9	6	14.0	19.4	15.3	16.0	14.0	14.0	14.4	14.1	87	64	86	79	2.2	9.3	3.3	4.9	7.4	8.2	7.4	7.7
VIII	997.3	1012.0	984.8	1014.6	20.1	11.1	28.8	6	7.0	4, 14	13.5	18.6	14.6	15.3	14.5	15.0	15.0	14.8	93	70	89	84	1.0	7.0	1.8	3.3	8.2	8.6	6.3	7.7
IX	1008.9	1013.4	986.8	1018.4	19.7	8.5	28.6	2	1.4	25	10.2	18.6	12.1	13.2	12.1	13.6	13.1	12.9	95	63	91	83	0.6	8.4	1.6	3.5	5.1	5.1	2.8	4.3
X	1001.9	1013.8	976.5	1019.7	14.7	6.1	19.5	5	1.7	10	7.3	13.5	9.6	10.0	9.4	11.0	9.9	10.1	91	72	83	82	1.0	4.8	2.2	2.7	6.5	6.5	4.1	5.7
XI	996.2	1017.7	982.3	1014.5	5.3	0.7	11.5	3	-7.9	23	1.9	4.0	2.7	2.8	6.8	7.3	7.1	7.1	94	88	92	91	0.4	1.0	0.6	0.7	8.9	8.5	8.0	8.5
XII	996.9	1027.1	972.5	1015.6	-1.1	-8.2	14.9	5	-26.4	27	-5.4	-3.3	-4.9	-4.6	4.2	4.5	4.2	4.3	86	81	85	84	0.5	1.0	0.7	0.7	7.0	7.2	4.9	6.4
Rok	997.8	1027.1	972.4	1015.6	12.2	3.8	32.6	27.VI	-26.4	27.XII	6.0	10.7	7.3	7.8	9.2	9.6	9.6	9.5	88	70	85	81	1.2	5.5	1.9	2.9	7.2	7.4	5.7	6.8

Białystok — φ = 53°07' — λ = 23°11'

I	1002.1	1024.2	981.4	1020.2	-1.2	-6.9	6.3	4	-23.0	25	-5.0	-2.1	-4.0	-3.8	4.2	4.6	4.3	4.4	88	82	86	85	0.5	0.9	0.6	0.7	7.1	8.1	8.1	7.8
II	1004.1	1021.6	978.2	1021.9	2.5	-1.8	9.0	18	-9.0	6	-0.9	1.2	0.1	0.1	5.6	6.0	5.9	5.8	95	90	94	93	0.2	0.7	0.4	0.4	9.1	8.9	7.9	8.6
III	995.5	1016.3	975.2	1013.1	7.8	0.8	15.8	10	-4.2	20	2.1	6.0	3.7	3.8	6.5	6.9	6.6	6.7	90	73	82	82	0.7	2.7	1.5	1.6	8.5	7.9	5.3	7.2
IV	996.8	1009.7	983.0	1014.0	14.5	2.7	24.3	15	-3.3	11	5.6	12.8	8.0	8.6	7.3	7.4	8.0	7.6	78	50	72	67	2.2	8.3	3.2	4.6	5.1	5.4	3.4	4.6
V	994.6	1003.0	984.3	1011.5	17.5	6.9	27.2	29	2.1	23	10.4	15.4	11.0	12.0	10.6	10.4	10.7	10.6	84	61	82	76	2.3	7.9	2.7	4.3	6.9	8.0	6.5	7.1
VI	997.9	1009.3	988.8	1014.5	23.9	12.0	31.9	27	5.2	21	16.2	21.5	17.2	18.0	14.9	14.3	14.8	14.7	81	58	75	71	3.7	12.1	5.1	7.0	5.3	6.6	5.1	5.7
VII	995.7	1008.6	982.3	1012.4	21.2	10.9	30.0	3	7.3	6	14.6	19.3	15.4	16.2	14.5	14.1	14.8	14.5	87	64	85	79	2.2	8.8	2.9	4.6	5.1	7.8	6.6	6.5
VIII	997.8	1011.9	985.2	1014.5	20.8	11.6	29.5	6	5.8	18	13.7	19.3	14.8	15.6	14.3	14.5	14.8	14.5	91	65	88	81	1.6	8.5	2.2	4.1	7.6	7.5	6.2	7.1
IX	1001.7	1015.0	987.5	1018.7	19.4	7.7	28.1	3	-0.6	24	9.3	18.2	11.7	12.7	11.6	13.1	12.4	12.4	95	62	88	82	0.6	8.5	1.8	3.6	4.8	5.5	3.4	4.6
X	1004.6	1016.1	982.6	1021.7	14.3	4.9	19.4	4	-0.8	23	6.1	13.4	8.9	9.3	8.7	10.4	9.6	9.6	91	68	83	81	0.8	5.2	2.8	2.7	6.4	6.6	5.4	6.1
XI	997.5	1017.6	985.6	1015.2	4.9	0.5	11.6	2, 3	-5.8	24	2.1	3.8	2.5	2.7	6.8	7.4	7.0	7.1	94	90	93	92	0.5	0.9	0.6	0.7	9.4	8.5	8.5	8.8
XII	997.3	1027.2	974.3	1015.4	-1.5	-8.6	13.8	5	-23.5	28	-5.4	-3.2	-5.1	-4.7	4.3	4.8	4.3	4.5	91	89	90	90	0.4	0.6	0.5	0.5	8.6	7.7	5.0	7.1
Rok	998.8	1027.2	974.3	1016.0	12.0	3.4	31.9	27.VI	-23.5	28.XII	5.7	10.5	7.0	7.6	9.1	9.5	9.4	9.3	89	71	85	82	1.3	5.4	2.0	2.9	7.0	7.1	6.0	6.8

Bydgoszcz, IMiUZ — $H_s = 47\,m$ — $h_w = 10\,m$ — 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	●	●	R ≥ 0,1	R ≥ 1,0	R ≥ 10,0	≡	▦	FR
I	.	.	3.5	1.9	10.5	1.8	5.5	2.1	15.5	2.1	1.4	1.8	1.3	2.2	1	1.0	30	1.3	24.9	10.3	30	9	11	22	.	.	.	6	14	13	8	1	7	4	.
II	1	2.0	.	.	7	2.0	4.5	1.9	11	2.1	14.5	2.7	2.4	2.2	3	2.7	19	1.8	29.3	10.6	9	.	.	13	.	.	.	.	17	15	6	1	11	1	.
III	1	4.0	0.5	1.0	0.5	1.0	.	.	2	4.5	3	3.7	7.5	3.4	12.5	4.0	2	3.4	29.9	5.7	30	.	.	5	.	1	.	2	15	17	11	.	4	3	.
IV	5.5	1.4	7	1.7	24.5	2.2	9.5	2.6	4.5	2.4	4	2.0	6.5	2.7	2.5	2.6	26	1.6	37.4	8.4	7	.	.	5	.	.	.	9	7	12	10	.	2	1	3
V	12.5	1.8	6.5	1.6	4	1.6	1	2.0	2.5	2.8	9.5	3.3	23.5	2.1	3.5	1.9	30	1.5	62.3	12.8	6	.	.	.	.	.	.	.	13	13	11	3	2	.	5
VI	5.5	1.8	3	1.7	10.5	2.5	1.5	3.0	6	1.7	4	3.5	31.5	2.4	8	2.4	20	1.8	37.1	8.9	4	.	.	.	13	.	.	5	3	10	9	.	.	.	6
VII	2	2.5	.	.	2.5	1.6	1	2.5	6	2.0	15.5	2.6	4.1.5	2.7	3.5	2.3	21	2.0	152.6	62.2	31	.	.	.	5	.	.	2	16	21	15	3	.	.	9
VIII	1	4.0	.	.	7	1.2	1.5	1.3	3	1.7	14.5	2.3	3.4.5	2.6	4.5	3.2	27	1.7	56.5	15.4	22	.	.	.	3	.	.	2	7	19	11	1	4	.	2
IX	.	.	1	2.0	12.5	2.1	1.5	2.3	3.5	2.7	9.5	2.2	2.9.5	2.7	0.5	3.0	27	1.7	27.6	8.9	14	.	.	.	4	.	.	9	7	12	5	.	3	.	3
X	.	.	.	.	2.6	2.8	10	2.6	13	2.0	3.5	3.8	15	2.3	2.5	4.0	23	2.0	35.7	9.2	18	.	.	.	.	.	.	3	10	13	8	.	13	.	.
XI	5.5	2.2	5	4.8	15.5	2.7	3	1.8	10	1.8	10	3.4	17.5	2.9	0.5	2.0	23	2.1	32.6	9.1	27	.	.	6	.	.	.	1	21	20	7	.	12	.	.
XII	4	4.0	6	2.2	7.5	1.6	3.5	2.0	7.5	1.8	13	4.6	22.5	2.5	2	2.8	27	2.0	29.4	8.0	4	11	14	23	.	1	.	4	14	14	6	.	8	18	.
Rok	38	2.0	32.5	1.4	133	1.9	42.5	2.0	84.5	2.3	115	3.0	330.5	2.6	44	2.7	275	1.9	560.3	62.2	31.VII	20	25	74	25	2	.	43	144	179	107	9	66	27	28

Bydgoszcz — $H_s = 70\,m$ — $H_b = 70{,}5\,m$ — $h_w = 14\,m$

I	2	3.2	3.5	3.6	8.5	2.4	10	2.3	18.5	2.4	18.5	3.8	14	3.1	8	2.8	10	2.6	23.6	9.6	30	11	12	24	.	1	.	5	17	12	8	.	.	9	.
II	3.5	3.1	.	.	1.5	1.3	10	3.5	12	4.4	20	4.4	16	3.2	14	4.2	7	3.6	31.8	10.1	9	.	.	16	.	1	.	.	18	14	6	1	8	3	.
III	5	5.7	1	3.0	.	.	.	.	.	.	10	4.4	44	5.8	33	5.5	.	5.5	31.7	6.6	30	.	.	9	.	7	1	2	14	15	11	.	2	3	.
IV	7.5	3.3	9	3.7	13	3.9	24	4.3	6.5	3.2	5	3.3	10.5	3.6	7.5	3.2	7	3.5	39.5	8.7	28	.	.	9	.	1	.	9	7	13	9	.	.	2	2
V	19.5	3.6	12	4.3	5	3.8	3.5	2.4	6.5	3.8	13.5	4.0	23.5	4.0	3.5	4.6	6	3.6	67.8	13.9	16	.	.	.	.	.	.	.	13	13	12	3	1	.	3
VI	8.5	4.4	2	2.5	10	4.0	9	3.1	8	4.8	9	5.1	28.5	4.2	11	4.9	4	4.1	31.0	8.3	14	.	.	.	11	5	.	3	4	9	9	.	2	.	6
VII	5.5	2.5	2.5	1.4	1	2.0	3	2.0	5	2.8	17	4.3	46	4.2	8	3.8	5	3.6	183.5	61.2	31	.	.	.	5	3	1	2	15	21	19	6	.	.	9
VIII	6.5	2.2	1	1.0	2.5	4.6	2.5	3.0	2	3.5	15.5	4.5	31	4.0	20	3.5	12	3.3	52.9	12.8	22	.	.	.	3	1	.	1	10	19	12	1	7	.	3
IX	1.5	1.7	1.5	4.0	17.5	2.7	10	3.5	4	4.5	9	3.9	18.5	3.6	14	4.4	14	3.0	27.8	10.4	14	.	.	.	5	1	.	12	8	9	5	1	3	.	4
X	.	.	.	.	9	3.7	25.5	4.5	18.5	4.2	14.5	3.9	55	3.5	10	3.6	10	3.6	33.0	9.4	18	.	.	.	.	1	.	4	11	12	8	.	5	.	.
XI	7	2.9	8	3.9	6.5	5.8	14	4.2	3	2.8	11	6.6	18.5	3.6	5	3.8	17	3.5	39.3	8.8	27	.	.	7	.	1	.	1	22	17	8	.	7	.	.
XII	5	4.6	10.5	3.6	3	3.0	6.5	3.7	10	2.8	16	4.9	21	5.2	14	3.8	7	3.9	27.7	8.0	11	12	15	25	.	3	.	4	13	12	6	.	5	18	.
Rok	71.5	3.1	51	2.6	77.5	3.1	118	3.0	94	3.3	159	4.4	277	4.0	148	4.0	99	3.6	589.6	61.2	31.VII	23	27	90	24	25	2	43	152	166	113	12	40	35	27

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Mława — $H_s = 141\,m$ — $H_b = 145{,}8\,m$ — $h_w = 13\,m$

I	6	2.5	7.5	1.8	4.5	1.9	11	2.2	18	2.2	17	2.9	7	2.1	5	3.6	17	2.0	21.1	4.8	30	9	13	26	.	.	.	2	17	13	6	.	4	22	.
II	1.5	1.3	1	1.0	3	1.3	14	2.8	17.5	2.9	15	2.9	18	1.9	8	1.5	6	2.2	24.5	6.4	11	.	3	22	.	1	.	2	19	15	9	.	8	9	.
III	0.5	1.0	.	.	.	.	.	.	2	5.0	23	3.9	49.5	4.6	16	3.6	2	4.2	28.1	6.4	30	.	.	10	.	1	.	.	11	13	8	.	3	5	.
IV	4	2.1	13	2.3	21.5	3.6	16.5	2.6	4	2.0	6	2.6	5.5	2.7	8.5	3.4	11	2.5	38.4	12.1	7	.	.	8	.	.	.	7	7	14	13	1	.	4	3
V	11.5	3.3	5	2.6	9	1.3	8	2.8	7.5	2.8	19.5	2.6	12.5	2.3	16	3.9	4	2.7	46.5	11.0	7	.	.	.	.	.	.	.	9	14	11	1	1	.	5
VI	3.5	1.0	9	2.3	11.5	3.0	10	3.2	5.5	2.8	15.5	2.9	22.5	3.4	8.5	2.9	4	2.8	45.0	20.5	27	.	.	.	14	.	.	2	6	10	8	2	1	.	5
VII	5.5	1.5	3.5	1.6	4	3.8	2.5	1.8	11.5	1.6	40	2.7	14.5	3.7	5.5	1.8	6	2.4	87.1	13.3	30	.	.	.	5	.	.	2	16	16	12	5	1	.	3
VIII	3.5	1.1	4	2.0	3	1.7	2.5	1.2	11	2.8	29.5	3.0	23	2.8	11.5	2.2	5	2.5	104.7	20.4	7	.	.	.	2	.	.	1	14	18	13	3	2	.	7
IX	4.5	1.9	11	1.8	14.5	2.4	3	2.0	11	1.6	13	3.5	14.5	3.1	5.5	2.1	13	2.1	47.3	16.9	14	.	.	.	5	.	.	10	7	11	6	2	1	.	2
X	2.5	1.0	6.5	2.7	3.4.5	3.4	20	2.7	9	1.8	4.5	2.7	6	2.8	7	2.4	3	2.8	11.5	4.2	18	.	.	.	.	.	.	6	8	7	3	.	4	.	.
XI	12.5	3.0	6	4.8	17.5	3.8	7	2.4	7.5	1.7	17.5	3.0	11.5	3.0	2.5	2.6	8	2.8	52.6	9.3	5	.	1	12	.	.	.	1	22	17	12	.	7	.	.
XII	9.5	3.1	7	2.9	3.5	3.1	13	2.0	6	2.3	23	3.8	12	3.0	9	2.8	10	2.7	33.0	5.7	2	11	14	25	.	2	2	4	12	16	8	.	3	21	.
Rok	65	1.9	73.5	2.2	126.5	2.4	107.5	2.1	110.5	2.5	223.5	3.0	196.5	3.0	103	2.7	89	2.6	539.8	20.5	27.VI	20	31	103	26	4	2	37	148	164	109	14	35	61	25

Białystok — $H_s = 139\,m$ — $H_b = 140{,}8\,m$ — $h_w = 11\,m$

I	8	4.2	.	.	.	.	13.5	3.9	20	3.5	15	4.5	12.5	3.0	10	3.2	14	3.2	41.9	7.8	11	12	13	28	.	1	.	1	17	18	10	.	5	23	.
II	1	2.0	1	1.0	2.5	2.8	9.5	4.2	17	4.6	7.5	3.1	17	2.8	5.5	2.9	2.3	2.5	20.9	6.4	11	.	5	19	.	.	.	1	20	14	5	.	15	14	.
III	0.5	3.0	.	.	.	.	1	7.0	6	3.5	19.5	4.4	46.5	4.5	15.5	5.5	4	4.4	48.1	11.4	21	.	.	11	.	2	.	1	14	21	9	1	2	4	.
IV	4.5	3.8	7	3.7	12	3.3	14	4.2	10.5	3.4	6.5	3.5	8	4.1	9.5	4.5	18	3.1	27.0	6.4	7	.	.	8	.	2	.	8	6	10	8	.	2	2	2
V	1.5	5.3	3	3.3	3.5	2.9	13.5	2.9	6.5	4.2	13	2.6	13.5	3.2	15.5	3.4	21	2.5	39.2	8.8	1	.	.	.	4	.	.	.	12	16	12	.	3	.	4
VI	1	2.0	3.5	2.7	10	3.0	10.5	2.4	10	2.3	12.5	3.2	20.5	3.6	8	4.4	14	2.7	80.9	23.1	28	.	.	.	13	.	.	2	8	15	13	1	3	.	7
VII	4	2.4	1	4.0	4	2.0	3	4.5	15.5	3.0	16.5	3.1	32	3.2	4	3.4	13	2.7	92.6	30.4	28	.	.	.	4	.	.	3	10	16	9	2	1	.	4
VIII	1.5	2.3	1	1.0	2	3.0	1	1.0	12	3.5	2.5	3.4	24.5	3.3	17	3.2	9	3.0	79.7	19.8	10	.	.	.	4	.	.	.	13	16	12	1	.	.	6
IX	2	2.0	3.5	1.8	5.5	2.5	3	2.3	5.5	3.3	14.5	3.0	18	3.1	9	3.4	29	2.0	35.5	13.7	14	.	.	2	5	.	.	10	6	7	7	1	5	.	1
X	1	3.0	1.5	3.0	9	3.9	3.5	4.5	16	3.6	3.5	2.6	9	3.3	4	2.4	14	3.4	64	3.0	25.29	.	.	1	.	.	.	6	12	3	2	.	8	.	.
XI	4.5	4.0	3.5	4.4	15	4.8	13.5	3.2	11	2.8	10	4.2	15	4.1	7.5	4.1	10	3.5	44.2	8.0	8	.	3	15	.	.	.	.	22	14	11	.	5	.	.
XII	12.5	4.6	2	5.5	0.5	2.0	11	4.0	10.5	3.0	6.5	5.5	18	4.6	5	4.5	27	3.1	28.1	6.3	4	11	16	26	.	3	.	2	13	11	9	.	4	20	.
Rok	42	3.2	27	2.5	64	2.5	128.5	3.7	142.5	3.4	150	3.6	234.5	3.6	110.5	3.7	196	3.0	544.5	30.4	28.VII	23	37	110	30	8	.	34	153	161	107	6	53	63	24

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Przelewice

$\varphi = 53°06'$ $\lambda = 15°05'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.6	−4.6	5.8	29	−16.7	26	−3.2	−0.2	−2.1	−1.9	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.3	5.8	6.1
II	–	–	–	–	6.1	0.6	12.8	28	−5.9	5	1.7	5.1	2.7	3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	7.2	7.7
III	–	–	–	–	9.6	2.8	17.7	10	−3.8	20	4.2	8.1	5.3	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	5.7	6.7
IV	–	–	–	–	15.3	4.6	25.1	14	−1.2	11	7.1	13.9	8.7	9.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.4	4.7	5.2
V	–	–	–	–	15.2	6.9	22.6	26	3.9	13, 18	9.5	13.7	9.6	10.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	6.5	7.7
VI	–	–	–	–	22.5	11.7	28.8	26	8.3	20	15.9	20.3	15.7	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.3	3.7	5.1
VII	–	–	–	–	20.2	12.1	31.8	3	8.3	6	14.6	18.6	14.7	15.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.2	8.1	8.3
VIII	–	–	–	–	20.5	11.9	26.9	6	8.8	8	14.3	19.1	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	6.0	6.7
IX	–	–	–	–	20.7	10.7	28.9	2	4.1	27	12.4	19.5	13.7	14.8	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.2	3.5	3.9
X	–	–	–	–	15.1	7.8	21.5	6	3.9	31	8.8	14.1	10.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.7	4.6	5.4
XI	–	–	–	–	6.4	1.8	12.5	2	−4.9	22	2.9	5.7	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.7	7.1	7.8
XII	–	–	–	–	0.6	−6.7	13.7	5	−21.7	26	−3.5	−1.2	−3.1	−2.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.7	5.0	31.8	3. VII	−21.7	26. XII	7.1	11.4	7.8	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Ostrołęka

$\varphi = 53°05'$ $\lambda = 21°34'$

I	1007.0	1030.8	987.6	1019.3	−0.4	−5.8	5.5	4	−22.0	26	−4.3	−1.4	−3.1	−3.0	4.3	4.7	4.6	4.5	87	81	86	85	0.5	1.0	0.6	0.7	7.4	7.7	6.9	7.3
II	1008.7	1025.4	982.6	1020.8	3.1	−1.1	13.4	18	−7.5	5	0.1	2.4	0.7	1.0	6.2	6.2	5.9	6.1	94	85	88	89	0.4	1.2	0.6	0.7	9.1	8.2	7.7	8.3
III	1001.0	1021.5	979.1	1012.9	9.1	1.1	16.9	10	−4.7	20	2.6	7.3	4.0	4.5	6.7	7.1	6.8	6.9	90	69	82	80	0.8	3.5	1.5	1.9	7.9	7.8	5.5	7.1
IV	1001.4	1014.0	989.8	1013.1	15.0	3.5	23.5	7	−3.5	10	6.0	13.3	8.6	9.1	7.8	7.8	8.1	7.9	81	51	70	67	1.9	8.5	3.5	4.6	5.2	5.8	4.4	5.1
V	999.3	1007.6	987.8	1010.9	17.5	7.4	26.3	28	2.3	23	10.1	16.0	11.0	12.1	10.9	10.7	11.4	11.0	87	59	86	77	1.7	8.2	2.0	4.0	7.8	8.1	7.1	7.7
VI	1002.3	1014.6	992.1	1013.7	24.1	12.6	32.3	27	6.6	21	16.5	22.5	17.2	18.3	15.2	13.8	15.0	14.7	81	52	76	70	3.8	14.3	4.9	7.7	5.5	6.1	5.6	5.7
VII	1000.3	1014.3	984.2	1011.8	21.6	11.0	31.0	3	7.0	6	14.3	19.9	15.4	16.2	14.2	14.0	14.5	14.2	87	61	83	77	2.2	9.8	3.2	5.1	7.2	7.9	6.8	7.3
VIII	1002.6	1017.1	990.2	1014.1	20.9	11.6	30.0	6	7.4	18	13.9	19.3	15.0	15.8	14.4	14.6	14.7	14.6	90	66	86	81	1.6	8.4	2.5	4.2	7.4	7.8	6.6	7.3
IX	1006.4	1019.3	992.1	1018.0	20.1	8.5	28.4	2	1.3	25	10.1	19.1	12.2	13.4	11.7	12.6	12.8	12.4	92	57	88	79	1.1	10.2	1.8	4.4	4.9	4.8	3.0	4.2
X	1008.2	1020.1	983.9	1020.0	14.8	5.9	20.1	4	0.8	23	7.0	13.9	9.7	10.1	9.1	10.3	9.8	9.7	90	67	81	79	7.1	5.8	2.4	3.1	6.5	6.4	4.3	5.7
XI	1002.2	1023.3	988.4	1014.1	5.1	0.6	11.3	3	−8.6	23	2.7	4.1	2.7	3.0	6.9	7.3	7.0	7.1	93	86	91	90	0.5	1.2	0.7	0.8	9.3	8.6	7.4	8.4
XII	1002.6	1032.8	978.7	1014.9	−1.2	−7.6	15.3	5	−25.3	27	−4.7	−2.7	−4.6	−4.2	4.3	4.6	4.3	4.4	86	80	86	84	0.6	1.1	0.7	0.8	7.7	6.6	5.4	6.6
Rok	1003.5	1030.8	978.7	1015.3	12.5	4.0	32.3	27. VI	−25.3	27. XII	6.2	11.1	7.4	8.0	9.3	9.5	9.6	9.5	88	68	84	80	1.4	6.1	2.0	3.2	7.2	7.2	5.9	6.8

Toruń – Wrzosy

$\varphi = 53°03'$ $\lambda = 18°35'$

I	1010.6	1035.8	989.4	1019.6	0.3	−6.0	6.3	4	−21.0	26	−4.6	−0.4	−3.2	−2.8	4.3	4.9	4.6	4.6	88	78	86	84	0.5	1.2	0.7	0.8	7.3	7.3	5.5	6.7
II	1012.4	1028.6	984.5	1021.2	4.4	0.0	12.5	18	−4.9	22	1.1	3.4	1.9	2.1	6.4	6.8	6.5	6.6	96	86	88	90	0.3	1.1	0.6	0.7	9.5	9.1	6.8	8.5
III	1006.9	1026.8	980.8	1015.6	9.6	2.3	17.9	10	−6.8	20	3.7	8.2	5.2	5.6	6.9	6.7	7.2	6.9	86	63	81	77	1.2	4.4	1.8	2.5	8.7	7.8	5.7	7.4
IV	1004.7	1016.4	994.1	1013.2	15.0	3.9	25.2	7	−4.1	10	6.6	13.3	8.7	9.3	7.8	8.4	8.6	8.3	78	54	74	69	2.3	8.0	3.0	4.4	5.5	5.8	3.9	5.1
V	1003.5	1011.6	990.6	1011.9	16.5	6.3	22.1	5	1.1	13	9.9	14.6	10.4	11.3	10.3	10.5	10.5	10.4	84	64	83	77	2.1	6.5	2.3	3.6	7.5	9.3	6.6	7.8
VI	1006.1	1019.7	994.5	1014.5	24.4	12.3	32.6	27	6.3	21	16.9	22.8	17.3	18.6	14.5	13.2	14.7	14.1	75	49	74	66	5.0	15.3	5.3	8.5	5.5	6.6	6.1	6.1
VII	1004.0	1018.5	987.6	1012.3	21.2	11.7	33.9	3	7.0	1	15.0	19.0	15.3	16.2	13.8	13.6	14.1	13.8	81	64	81	75	3.4	9.5	3.6	5.5	7.7	8.6	7.0	7.8
VIII	1006.7	1021.2	993.3	1015.1	20.5	11.6	29.8	6	6.8	14	13.9	18.9	14.9	15.6	14.4	14.5	14.7	14.5	90	67	86	81	1.6	7.9	2.5	4.0	8.2	7.7	5.8	7.2
IX	1010.0	1022.1	995.9	1018.5	20.3	8.8	29.6	2	0.1	28	11.2	19.3	12.7	14.0	12.1	13.1	12.7	12.6	89	58	84	77	1.5	10.1	2.4	4.7	4.8	5.4	4.3	4.8
X	1010.2	1022.4	983.0	1018.8	15.0	2.1	19.8	5	2.9	10	8.2	14.2	10.5	10.8	10.0	11.4	10.6	10.7	91	71	84	82	1.0	5.1	2.2	2.8	6.8	7.2	5.1	6.4
XI	1005.6	1028.2	990.4	1014.4	6.0	1.5	11.8	3	−8.7	23	2.8	5.3	3.4	3.7	7.2	7.8	7.4	7.5	93	87	92	91	0.5	1.2	0.7	0.8	9.2	9.0	8.4	8.9
XII	1007.0	1038.5	982.3	1016.1	−0.3	−7.0	15.6	5	−22.6	27	−4.0	−1.5	−3.9	−3.3	4.7	4.9	4.4	4.7	88	82	85	85	0.6	1.2	0.8	0.9	7.6	7.0	5.6	6.7
Rok	1007.3	1038.5	980.8	1016.0	12.7	4.4	33.9	3. VII	−22.6	27. XII	6.7	11.4	7.8	8.4	9.4	9.6	9.7	9.6	87	69	83	80	1.7	6.0	2.2	3.3	7.4	7.6	5.9	7.0

Przasnysz

$\varphi = 53°01'$ $\lambda = 20°53'$

I	–	–	–	–	−0.7	−5.6	4.5	4	−18.4	26	−4.2	−1.0	−3.1	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	8.5	8.5
II	–	–	–	–	2.5	−0.8	9.6	18	−4.6	6	0.2	2.2	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8.5	1.1	15.4	10	−3.2	20	3.2	7.7	3.8	4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	14.4	2.8	22.3	7	−2.3	11	6.6	13.2	7.7	8.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.6	6.5	25.1	27, 28	1.0	20	10.2	15.7	10.1	11.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.4	12.0	31.7	27	6.0	21	16.1	22.3	15.3	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.0	10.0	30.8	3	4.6	8	14.4	19.6	14.5	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	19.9	10.2	28.8	6	6.5	8	14.0	18.8	15.2	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	19.6	8.5	28.1	2	0.9	24	10.1	18.8	12.3	13.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.2	5.4	19.2	4	1.0	23	7.4	13.1	8.9	9.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.6	6.1	6.1
XI	–	–	–	–	4.9	0.7	11.2	3	−8.3	23	2.0	4.5	2.6	2.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.1	8.2	8.5
XII	–	–	–	–	−1.2	−7.2	14.9	5	−25.1	27	−4.9	−2.4	−4.3	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.4	6.9	7.0
Rok	–	–	–	–	11.9	3.6	31.7	27. VI	−25.1	27. XII	6.3	11.0	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Przelewice

$H_s = 60\ m$ $h_w = 10\ m$

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	⩛
I	·	·	1	2.0	10	2.4	28.5	2.8	18	3.6	22.5	3.3	4.5	2.3	1.5	3.0	7	2.8	29.4	5.5	30	6	10	21	·		·	9	12	15	9		3	1	·
II	·	·	0.5	2.0	5	3.0	9	3.4	18.5	3.6	30.5	3.1	13.5	2.7	2	2.0	5	2.9	41.1	9.0	11	·		9	·		·	1	17	11	8	·	6		·
III	2	2.0	·	·	·	·	·	·	4.5	2.2	37	4.5	41	4.6	7.5	4.1	1	4.3	44.9	8.6	30	·		3			·	3	11	16	12	·	1	·	·
IV	5	1.2	3.5	2.7	22.5	3.4	15	2.5	10	2.6	9.5	2.4	9.5	3.3	3	1.3	12	2.4	24.5	5.4	27			3	1		·	10	11	12	7	·	·	·	1
V	7.5	2.4	3	3.2	3	1.8	5.5	3.9	12	2.5	24	2.9	18	2.7	9	2.0	11	2.4	134.8	18.0	21	·	·	·	·	·	·	·	14	22	20	6	·	·	7
VI	1	3.0	1.5	2.7	7	1.5	10	2.7	7	2.5	28	2.2	19	2.8	3.5	2.0	13	2.0	91.6	42.2	13	·	·	·	7	·	·	5	5	9	7	3	·		4
VII	·	·	1	2.0	2.5	1.4	0.5	1.0	17	2.1	52	2.4	9.5	2.5	1.5	3.0	9	2.1	117.9	20.5	21	·		·	4		·	2	23	22	17	4	·	·	2
VIII	1	2.0	·	·	1	2.0	4	1.5	13.5	1.7	49.5	2.6	8	3.4	4	3.1	12	2.2	57.8	16.1	10			·	3	·	·	3	14	20	10	2	1		2
IX	1	2.5	3.5	1.4	8	1.9	13	2.5	15.5	2.0	29.5	2.7	7.5	1.9		·	12	2.0	20.2	7.2	14	·		·	6	·	·	11	5	9	4		·	·	1
X	·	·	1	3.0	15.5	3.6	22	4.0	22.5	2.9	21	2.8	4	1.5	·	·	7	3.0	32.8	16.6	20			·	·	·		8	10	9	7	1	2	·	·
XI	0.5	4.0	9.5	3.0	7.5	4.6	11	2.7	12.5	3.0	26.5	4.0	9.5	2.4	2	1.8	11	2.9	39.7	19.3	13		·	8	·	2	·	2	19	14	8	1	7	·	·
XII	2	1.2	2	3.5	6	2.7	16	2.5	19	2.1	22	4.5	16.5	4.5	4.5	1.6	5	3.1	54.3	13.5	11	10	15	22	·	2	·	—	—	9	7	—	—	15	·
Rok	20	1.5	26.5	2.1	88	2.4	134.5	2.5	170	2.6	352	3.1	160.5	2.9	38.5	2.0	105	2.7	689.0	42.2	13.VI	16	25	66	21	4		—	—	168	116	—	—	16	17

Ostrołęka

$H_s = 95\ m$ $H_b = 96{,}3\ m$ $h_w = 13\ m$

I	5	2.7	8.5	2.6	2	1.5	12	1.4	12	2.4	24	2.8	5.5	3.0	7	2.7	17	2.0	31.2	11.8	5	10	12	27	·	1	·	3	17	18	8	1	7	19	·
II	2.5	1.6	2	1.5	2.5	1.4	11.5	1.8	15.5	2.8	11.5	2.9	15	1.9	10.5	1.4	13	1.8	18.7	5.7	11	·	2	18	·	1	·		20	14	6	·	9	9	·
III	5	3.3	·	·	·	·	·	·	2.5	4.0	14	4.0	31.5	4.4	37	4.1	3	4.0	24.9	8.4	30	·	·	10	·	5	2	1	12	11	6		2	2	·
IV	6.5	2.6	9	2.7	15.5	2.9	17	2.8	3.5	2.4	7.5	2.2	9	3.2	7	4.4	15	2.4	20.2	6.4	7	·	·	7	·	1	·	6	9	9	6	·	2	3	2
V	18	3.6	4.5	2.2	4	2.1	11.5	2.4	7	2.6	11	3.6	7.5	3.3	7.5	1.9	22	2.2	65.0	13.6	10	·	·		3	·		·	14	18	11	3	·	·	2
VI	1.5	5.0	1	1.0	10.5	2.2	14	2.4	6.5	1.8	11	2.9	15.5	3.5	11	3.0	19	2.2	85.4	21.6	8	·	·	·	14	1	·	4	8	13	10	3	1	·	8
VII	7.5	2.1	1	3.0	2.5	1.8	2.5	4.6	8.5	2.0	25.5	2.6	17.5	3.0	5	2.7	23	2.0	76.9	20.3	30	·	·	·	3	1	·	2	15	20	12	2	3	·	6
VIII	6.5	1.7	3	2.0	2	2.0	1.5	2.7	7	2.8	20	3.2	20.5	2.7	16.5	2.5	16	2.2	50.0	8.1	10	·	·	·	3	1	·	·	16	19	12		1	·	4
IX	4	1.6	5.5	1.5	6.5	2.5	12.5	1.7	3	2.5	11.5	2.4	19.5	2.9	4.5	2.8	23	1.8	30.6	8.4	14	·	·		5	·	·	11	5	11	6		6		1
X	0.5	2.0	0.5	2.0	9.5	2.7	30.5	3.6	15	2.5	6	2.6	5.5	3.1	3.5	1.3	22	2.3	10.5	3.8	29	·	·	·	·	·	·	5	8	6	4		7	·	·
XI	7	3.4	7.5	3.4	10.5	4.5	12	2.5	6	2.7	10	3.3	18.5	2.5	25	2.8	16	2.6	47.1	7.0	27	·	2	14	·	·	·	·	20	16	14	·	7	·	·
XII	9	3.4	10.5	2.8	2.5	1.2	4.5	2.3	11.5	1.7	13.5	3.3	18	3.4	7.5	2.1	16	2.3	24.9	7.6	4	10	14	25	·	1	·	5	16	13	7	·	6	18	·
Rok	73	2.8	53	2.1	68	2.1	129.5	2.4	98	2.5	165.5	3.0	183.5	3.1	119.5	2.6	205	2.3	485.4	21.6	8.VI	20	30	101	28	12	2	37	160	168	102	9	51	51	23

Toruń - Wrzosy

$H_s = 69\ m$ $H_b = 70{,}2\ m$ $h_w = 12\ m$

I	1	5.0	7	3.1	4.5	2.9	22.5	2.2	12.5	2.2	22	3.2	8.5	3.0	4	3.4	11	2.4	20.8	5.7	30	11	11	24		·	·	5	15	13	5	·	3	10	
II	2	3.0	2	1.8	2.5	3.0	19	3.2	12.5	3.0	17.5	2.5	12	3.3	9.5	2.9	7	2.7	28.8	10.6	9	·	·	13	·	1	1	·	18	15	7	1	13	5	·
III	·	·	·	·		·	·		3	3.2	23	4.1	43	4.9	20	4.8	4	4.4	31.9	6.7	30	·	·	6	·	9	1	·	15	17	10	·	4	4	·
IV	7	3.6	12	3.4	18.5	4.2	16.5	3.4	5	2.7	6.5	2.6	6	3.2	11.5	2.6	7	3.1	33.6	11.3	7	·	·	6	1	1	·	9	7	11	9	1	·	3	3
V	13	3.5	6	3.8	5	2.6	5.5	2.5	6	2.3	15	2.8	14	2.6	17.5	3.1	11	2.6	61.5	16.6	6	·	·	·	·	·	·	·	14	14	11	2	4	·	7
VI	3	1.8	5.5	2.5	10	3.0	11	2.9	5.5	3.4	11	3.0	22	3.1	15	3.4	7	2.8	50.7	9.9	11	·	·	·	12	·	·	3	8	10	9	·	1	·	8
VII	2.5	1.6	0.5	1.0	2	4.2	6.5	2.8	12.5	2.2	24.5	2.7	29	2.7	10.5	2.3	5	2.5	144.9	50.4	31	·	·	·	4	·	·	1	18	20	18	4	1	·	9
VIII	2	1.5	1.5	2.7	2.5	3.2	3.5	2.7	8	2.5	25.5	3.1	27.5	2.5	11.5	2.2	11	2.4	74.0	15.8	7	·	·	·	4	·	·	1	13	19	15	2	8	·	7
IX	1.5	2.3	4.5	2.0	12	3.3	10.5	3.3	8	1.6	19	2.7	14.5	3.2	7	2.7	13	2.4	28.5	9.8	14	·	·	·	5	·	·	11	8	9	5	·	2	·	1
X	·	·	2.5	3.2	20	4.6	26	3.5	16.5	2.4	7.5	3.1	7.5	2.4	5	2.3	8	3.0	30.3	10.5	18	·	·	·	·	1	·	5	13	11	8	1	11		·
XI	8	2.4	5.5	6.3	12	4.0	12.5	2.4	7	2.5	19.5	3.3	10.5	3.7	5	2.8	10	3.0	35.3	6.1	27	·	·	7	·	·	·	1	24	13	9	·	7	1	·
XII	4	2.4	7.5	3.9	6	3.3	14.5	2.2	11.5	2.6	15.5	3.6	21	3.5	9	3.6	4	3.0	26.9	8.3	11	11	14	24	·	1	·	4	12	12	6	·	5	20	·
Rok	44	2.3	54.5	2.8	95	3.2	148	2.6	108	2.6	206.5	3.1	215.5	3.2	125.5	3.0	98	2.9	567.2	50.4	31.VII	22	25	80	26	13	2	40	165	164	112	11	59	43	35

Przasnysz

$H_s = 120\ m$ $h_w = 14\ m$

I	4.5	1.9	14.5	1.7	2	1.0	7	1.3	15	2.1	21	2.8	16	2.5	2	3.0	11	1.9	13.1	4.9	31	8	12	29	·	·	·		20	10	4	·	2	10	·
II	·	·	·	·	1	2.0	5	2.6	14.5	2.3	16.5	1.7	33.5	1.6	3.5	1.9	10	1.6	18.9	6.7	11	·	3	18	·	·	·	—	—	9	4		2	7	·
III	·	·	·	·	·	·	·	·	·	·	8.5	2.8	69	3.3	12.5	2.8	3	3.1	15.8	6.9	31	·	·	10	·	·	·	—	—	9	3	·	1	2	·
IV	5	1.2	4	2.0	13.5	1.7	15	3.1	3.5	1.3	6	2.2	18.5	2.2	12.5	1.6	12	1.8	24.7	6.2	16	·	·	6	·	·	·	—	—	10	7	·	·	2	1
V	8	2.1	·		4	1.8	6	1.5	11.5	1.5	21.5	1.8	15	2.4	17	2.2	10	1.7	60.6	11.9	28	·	·	·	2	·	·	—	—	15	14	1	1	·	3
VI	2.5	1.4	·		5	2.4	14	2.0	8	2.6	10	2.2	34	2.2	11.5	1.8	5	2.0	22.5	8.4	7	·	·	·	13	·	·	—	—	10	5	·	·	·	5
VII	2	2.5	2	2.5	·	·	·	·	·	·	28.5	2.0	39.5	1.9	8	1.5	13	1.7	65.7	22.0	16	·	·	·	5	·	·	—	—	9	8	2	·	·	1
VIII	7	1.6	·	·	2	1.5	1	3.0	1	1.0	9	2.9	44.5	2.7	20.5	1.7	8	2.1	64.9	21.2	12	·	·	·	2	·	·	—	—	16	9	2	·	·	2
IX	1	1.0	7	1.4	15	1.2	1	2.0	·	·	5	2.0	27	2.6	17	1.5	17	1.5	17.7	9.3	14	·	·	·	5	·	·	—	—	6	4	·	·	·	1
X	3	2.0	2	1.0	23.5	2.1	14	2.7	16.5	1.6	9	2.1	5	2.4	5	1.8	15	1.7	6.3	3.0	18	·		·	·	·	·	1	8	5	2	·	6	·	·
XI	9	1.8	5	2.6	10	3.9	8	3.0	3.5	3.0	7.5	1.8	32	2.6	5	2.2	10	2.3	35.6	8.3	4	·	2	11	·	·	·	·	19	14	8	·	7	·	·
XII	8	2.5	9	1.7	1	2.0	4	1.5	12	1.9	9.5	3.9	32.5	2.7	3	2.0	14	2.1	14.8	5.8	4	10	14	24	·	·	·	·	13	8	5	·	—	15	·
Rok	50	1.5	43.5	1.1	77	1.6	75	1.9	85.5	1.4	152	2.4	366.5	2.4	117.5	2.0	128	2.0	360.6	22.0	16.VII	18	31	98	27	·	·	—	—	121	73	5	—	36	13²

Chodzież — φ = 52°59' — λ = 16°54' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	−6.0	7.4	31	−18.7	26	−4.3	−0.3	−3.5	−2.9	4.2	5.2	4.3	4.6	83	84	83	83	0.6	0.9	0.7	0.7	5.8	5.9	5.0	5.6
II	–	–	–	–	5.2	−0.4	12.5	18	−4.8	5	1.3	3.9	1.8	2.2	6.1	6.8	6.2	6.4	90	84	88	87	0.7	1.4	0.9	1.0	9.4	8.6	7.0	8.3
III	–	–	–	–	9.6	2.1	18.5	10	−5.9	20	4.2	8.5	4.4	5.4	7.2	7.4	7.2	7.3	86	68	86	80	1.2	4.0	1.3	2.2	7.6	6.3	6.0	6.6
IV	–	–	–	–	15.1	3.9	25.6	7	−3.8	11	7.2	13.8	8.0	9.2	7.9	8.8	8.8	8.5	76	56	80	71	2.6	8.0	2.4	4.3	4.8	4.2	3.8	4.3
V	–	–	–	–	15.7	6.1	21.7	26	1.4	13	10.0	14.0	9.2	10.6	10.1	10.6	10.1	10.3	82	68	86	79	2.4	6.0	1.7	3.4	7.2	7.8	5.3	6.8
VI	–	–	–	–	23.3	12.3	29.4	26	7.2	22	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	2.7	4.4	3.5	3.5
VII	–	–	–	–	20.4	11.8	33.8	3	7.2	6	14.4	18.5	14.1	15.3	13.9	14.4	14.0	14.1	84	69	87	80	2.7	7.8	2.2	4.2	7.3	7.8	7.4	7.6
VIII	–	–	–	–	20.3	11.6	29.1	6	7.8	4	14.1	18.6	13.7	15.0	14.4	14.7	13.7	13.3	89	70	87	82	1.9	7.2	2.1	3.7	6.3	6.8	3.9	5.7
IX	–	–	–	–	20.6	9.4	29.1	2	0.6	24	12.5	19.8	13.2	14.7	12.8	13.2	12.7	12.9	86	57	83	75	2.1	10.4	2.6	5.0	3.6	3.9	3.9	3.8
X	–	–	–	–	14.6	7.5	22.0	6	2.2	31	9.2	13.9	10.2	10.9	10.5	11.3	10.5	10.8	90	73	84	82	1.2	4.9	2.0	2.7	7.2	5.9	4.9	6.0
XI	–	–	–	–	6.1	1.1	11.8	2	−8.8	23	2.8	5.3	2.9	3.5	6.9	7.4	6.9	7.1	90	82	89	87	0.8	1.7	0.8	1.1	9.0	7.7	7.5	8.1
XII	–	–	–	–	−0.8	−7.2	14.6	5	−20.5	26	−4.2	−2.0	−4.8	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.0	5.1	6.1
Rok	–	–	–	–	12.5	4.4	33.8	3.VII	−20.5	26.XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	5.3	6.0

Trzcińsko-Zdrój — φ = 52°58' — λ = 14°36'

I	–	–	–	–	0.7	−4.8	5.6	29,30	−21.0	26	−3.4	0.0	−2.4	−2.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.3	6.0	6.5
II	–	–	–	–	6.8	0.8	13.0	28	−4.3	5	2.3	5.8	3.3	3.7	6.9	7.8	7.2	7.3	94	84	92	90	0.4	1.7	0.6	0.9	9.9	8.5	6.6	8.3
III	–	–	–	–	9.6	2.5	17.0	17	−4.7	20	4.3	8.7	5.6	6.0	7.4	7.9	7.9	7.7	88	71	86	82	1.1	3.6	1.4	2.0	8.4	7.2	5.7	7.1
IV	–	–	–	–	15.1	4.8	25.1	14	−0.9	1	7.2	14.0	9.2	9.9	8.6	9.0	9.3	9.0	83	57	78	73	1.8	7.8	2.6	4.1	5.8	6.1	4.2	5.4
V	–	–	–	–	14.9	6.8	22.8	26	2.6	16	9.5	13.8	9.8	10.7	10.5	10.4	10.6	10.5	88	67	88	81	1.5	5.7	1.5	2.9	8.5	8.3	7.1	8.0
VI	–	–	–	–	22.5	11.7	28.5	26	7.2	20	15.8	20.8	16.3	17.3	14.4	14.5	15.2	14.7	80	60	82	74	3.7	10.5	3.6	6.3	5.7	6.8	6.3	6.3
VII	–	–	–	–	20.1	11.9	31.7	3	8.2	6	14.4	18.0	15.3	15.8	14.4	13.8	14.4	14.2	88	69	82	80	2.2	7.7	3.3	4.4	8.5	8.4	8.8	8.6
VIII	–	–	–	–	20.1	11.6	26.3	31	7.8	24	14.1	18.9	15.2	15.8	14.7	15.3	15.3	15.1	91	70	88	83	1.6	7.0	2.1	3.6	7.9	7.5	6.5	7.3
IX	–	–	–	–	20.7	10.1	29.3	2	2.3	27	12.1	19.8	13.8	14.9	14.7	14.4	14.2	14.0	91	62	88	80	1.3	9.4	2.0	4.2	5.0	4.7	3.5	4.4
X	–	–	–	–	15.2	7.8	21.3	6	1.6	14	8.9	14.5	10.6	11.2	13.3	11.2	11.0	10.9	91	69	86	82	1.1	5.6	1.9	2.9	7.1	6.2	4.8	6.0
XI	–	–	–	–	6.4	1.4	12.6	2	−5.2	22	2.9	5.8	3.6	4.0	10.4	7.9	7.4	7.5	91	84	92	89	0.7	1.5	0.7	1.0	9.0	8.2	6.4	7.9
XII	–	–	–	–	0.8	−6.1	14.1	5	−21.5	26	−2.9	−0.8	−2.6	−2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.0	6.8	7.4
Rok	–	–	–	–	12.7	4.9	31.7	3.VII	−21.5	26.XII	7.1	11.6	8.1	8.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	6.1	6.9

Wądołki Borowe — φ = 52°57' — λ = 22°13'

I	–	–	–	–	−1.0	−7.6	6.8	4	−26.0	26	−5.4	−2.6	−4.0	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.9	7.4	7.6
II	–	–	–	–	2.4	−2.0	11.2	18	−13.4	6	−0.4	1.6	0.2	0.4	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.4	7.3	8.3
III	–	–	–	–	8.3	0.7	15.5	10	−4.8	20	2.2	6.7	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	5.4	6.8
IV	–	–	–	–	14.2	3.0	23.5	15	−3.8	10	5.9	12.8	7.5	8.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.2	3.1	4.2
V	–	–	–	–	16.7	6.5	25.7	29	0.7	15	10.1	15.4	10.4	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.6	5.7	6.5
VI	–	–	–	–	23.5	11.4	32.3	27	4.6	21	16.3	21.8	16.3	17.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.6	5.7	5.7
VII	–	–	–	–	20.9	10.1	30.3	3	5.2	6	14.3	19.0	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.8	6.6	7.1
VIII	–	–	–	–	20.5	11.4	29.9	6	7.6	14	13.9	19.0	14.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.1	6.8
IX	–	–	–	–	19.2	7.6	28.3	3	−0.3	24	10.1	18.0	11.7	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.3	3.0	4.2
X	–	–	–	–	14.1	5.1	18.3	19	0.6	23	6.6	13.3	9.5	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.8	4.3	5.6
XI	–	–	–	–	4.8	0.5	11.4	3	−8.8	23	2.1	3.9	2.5	2.7	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.6	8.1	8.6
XII	–	–	–	–	−1.7	–	14.6	5	–	–	−4.8	−3.3	−5.1	−4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	5.3	6.9
Rok	–	–	–	–	11.8	–	32.3	27.VI	–	–	5.9	10.5	6.8	7.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.8	5.7	6.5

Krzyż — φ = 52°53' — λ = 16°01'

I	–	–	–	–	0.7	−5.9	5.7	30	−19.8	27	−4.3	0.0	−3.1	−2.6	4.5	5.0	4.4	4.6	82	78	80	80	0.7	1.3	0.8	0.9	6.0	6.1	5.9	6.0
II	–	–	–	–	5.7	−0.2	12.9	28	−4.5	5,6	1.5	4.4	2.0	2.4	6.3	7.1	6.5	6.6	91	84	90	88	0.6	1.4	0.7	0.9	8.8	8.6	7.9	8.4
III	–	–	–	–	9.6	2.1	18.9	10	−6.2	20	3.8	8.7	5.2	5.7	7.1	7.3	7.5	7.3	86	66	83	78	1.2	4.3	1.5	2.3	7.9	7.3	6.1	7.1
IV	–	–	–	–	15.2	3.8	24.5	14	−3.1	10	6.3	13.7	8.6	9.3	8.0	8.5	8.8	8.4	82	55	76	71	1.8	8.2	2.6	4.2	5.6	5.5	3.5	4.9
V	–	–	–	–	15.6	6.0	22.9	26	0.5	13	9.4	13.5	10.1	10.8	10.3	10.4	10.1	10.3	86	69	82	79	1.7	5.4	2.4	3.2	7.8	9.3	6.5	7.9
VI	–	–	–	–	23.2	11.0	29.7	26	6.7	13	15.7	21.3	16.5	17.5	14.4	13.6	14.7	14.2	80	55	79	71	3.6	12.0	4.2	6.6	5.4	6.4	5.8	5.9
VII	–	–	–	–	20.5	11.7	33.3	3	7.4	6,17	14.2	18.7	14.9	15.7	14.1	13.6	13.9	13.9	86	65	83	78	2.3	9.0	3.2	4.8	8.3	8.2	7.9	8.1
VIII	–	–	–	–	20.9	11.0	28.3	6	5.5	4	13.6	19.0	14.7	15.5	14.4	14.3	14.7	14.5	91	66	87	81	1.4	8.2	2.2	3.9	7.6	7.5	5.1	6.7
IX	–	–	–	–	21.1	8.5	29.7	2	−0.6	25	10.8	20.0	12.1	13.8	12.1	13.1	12.6	12.6	91	56	87	78	1.2	11.0	1.9	4.7	5.1	4.9	2.8	4.3
X	–	–	–	–	15.2	6.5	21.5	6	2.3	31	8.4	14.4	9.9	10.6	10.2	11.0	10.6	10.6	93	68	87	83	0.8	5.8	1.7	2.8	7.5	5.8	5.4	6.2
XI	–	–	–	–	6.3	1.4	12.9	2	−6.6	22	2.8	5.6	3.3	3.8	6.9	7.7	7.2	7.3	90	84	89	88	0.8	1.5	0.9	1.1	8.4	8.4	7.2	8.0
XII	–	–	–	–	0.4	−7.5	15.3	5	−24.0	26	−4.0	−1.1	−4.1	−3.3	4.7	5.1	4.6	4.8	88	82	86	85	0.6	1.2	0.7	0.8	6.7	6.5	6.0	6.4
Rok	–	–	–	–	12.9	4.0	33.3	3.VII	−24.0	26.XII	6.5	11.5	7.5	8.2	9.4	9.7	9.8	9.6	87	69	84	80	1.4	5.8	1.9	3.0	7.1	7.0	5.8	6.6

Chodzież

$H_s = 100$ m $h_w = 12$ m **1961**

MIESIĄC	ROZKŁAD WIATRU (nD, vnD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	Wiatr v > 15	⊙	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	·	·	0.5	3.0	8	1.2	5.5	1.5	13.5	1.5	11.5	2.6	6	1.2	4	1.5	44	0.9	33.6	10.2	30	10	13	25	·	·	·	10	11	13	7	1	2	2	·
II	1	1.0	·	·	1	1.0	7.5	1.3	10.5	1.4	20.5	1.4	5	1.4	3.5	1.9	35	0.8	28.8	9.6	9	·	·	17	·	·	·	1	17	15	9	·	6	·	·
III	·	·	·	·	·	·	·	·	4	4.1	25	2.6	24.5	3.8	22.5	3.2	17	2.6	44.6	10.8	20	·	·	9	·	2	·	4	14	19	14	1	2	3	·
IV	1	1.0	3	1.0	20	2.8	17	2.2	6.5	1.9	8.5	1.6	8.5	1.8	2.5	1.2	23	1.6	42.3	9.9	7	·	·	7	1	·	·	11	5	10	10	·	2	2	3
V	2.5	1.8	5.5	2.4	6	1.9	5.5	1.0	13	1.9	20	2.3	9.5	1.7	14	2.2	17	1.6	71.0	14.5	5	·	·	·	·	·	·	1	10	16	12	2	2	·	4
VI	1	1.0	1.5	1.0	2.5	1.4	7	1.9	7.5	1.4	11	1.3	20.5	1.8	11	2.2	28	1.2	51.6	16.8	4	·	·	·	11	·	·	12	2	9	8	2	1	·	6
VII	1	1.0	·	·	1	1.0	3.5	1.7	3	2.0	24	1.6	21.5	1.6	12	1.3	27	1.1	215.3	62.1	31	·	·	·	4	·	·	2	18	25	18	7	·	·	8
VIII	1	1.0	·	·	1	1.0	2.5	1.2	7	1.4	29	1.7	18	2.1	4.5	2.1	30	1.2	81.6	10.8	6, 10	·	·	·	3	·	·	4	8	18	14	2	2	·	7
IX	·	·	1	1.0	10.5	2.0	9.5	1.7	12.5	1.6	22	2.4	18.5	2.2	5	2.6	11	1.8	36.9	20.8	5	·	·	·	5	·	·	15	4	8	4	1	1	·	2
X	·	·	·	·	9	3.1	18	2.6	28.5	1.9	12	2.0	5	1.7	6.5	1.8	14	1.9	31.4	5.5	23	·	·	·	·	·	·	7	11	12	9	·	3	·	·
XI	3	1.0	5	2.1	9	2.7	5.5	2.2	3.5	1.4	13	2.4	11	1.9	4	1.4	36	1.2	36.9	12.0	30	·	·	8	·	·	·	1	19	15	9	1	9	·	·
XII	2	4.5	4	1.2	5	1.4	6	1.2	6	1.0	14.5	3.1	8	2.9	7.5	1.7	40	1.2	46.8	14.8	11	12	16	25	·	·	·	6	13	10	8	3	2	20	·
Rok	12.5	1.0	20.5	1.0	73	1.6	87.5	1.5	115.5	1.8	211	2.1	156	2.0	97	1.9	322	1.4	720.8	62.1	31. VII	22	29	91	24	2	·	74	132	170	122	20	32	27	30

Trzcińsko-Zdrój

$H_s = 60$ m $h_w = 11$ m

I	1	5.0	3.5	3.0	13	2.0	19.5	2.6	21.5	2.6	10	3.0	7	1.6	4.5	3.2	13	2.2	27.6	6.2	30	7	10	22	·	·	·	–	–	13	8	·	6	8	·
II	0.5	3.0	·	·	7.5	2.9	7	3.6	18	2.7	12	2.8	14.5	3.0	11.5	3.1	13	2.5	42.9	9.2	8			9	·	·	·	–	–	10	8	·	6	·	·
III	2	3.2	·	·	·	·	·	·	1	4.0	11	5.0	54	5.2	15	5.4	10	4.6	38.8	8.9	30		·	7	·	4	·	–	–	13	8	·	7	·	·
IV	10.5	2.7	6	1.8	24	2.6	8.5	3.6	8.5	2.7	5	2.3	5	4.0	7.5	2.8	15	2.3	18.2	4.0	1.7			1	1	·	·	–	–	11	6	·	2	·	2
V	18.5	3.0	5.5	2.2	2.5	2.2	5.5	2.8	9.5	2.3	7	2.9	17.5	3.8	16	3.3	11	2.7	99.1	11.8	29		·		·	·	·	–	–	19	17	3	·	·	4
VI	4.5	2.4	5.5	1.4	7.5	2.3	6	1.9	7	3.0	8.5	2.4	24.5	4.2	15.5	3.3	11	2.7	47.1	10.6	13		·	·	7	·	·	–	–	6	5	3	·	·	4
VII	·	·	5.5	1.3	2	1.8	2	2.0	7.5	2.3	20.5	3.0	42	3.3	7.5	3.9	6	2.8	136.2	21.6	31		·	·	3	·	·	–	–	17	13	6	·	·	3
VIII	2	2.2	5	1.4	4	1.1	4	1.1	5	1.9	15	2.5	35.5	3.3	9.5	4.5	13	2.5	53.6	11.2	10	·	·	·	2	·	·	–	–	16	12	1	3	·	4
IX	2.5	1.8	2.5	1.4	11.5	2.3	14	1.8	11.5	1.6	7.5	3.1	16.5	3.5	5	2.0	19	1.9	15.7	4.0	14	·		·	6		·	–	–	7	5	·	1	·	1
X	3	2.2	0.5	2.0	18	3.4	25.5	3.5	21	2.7	6.5	3.0	8.5	3.4	5	2.2	5	2.9	28.7	13.3	20	·	·	·	·	·	·	–	–	8	7	1	6	·	·
XI	5	1.9	12	2.2	6.5	2.3	4.5	2.3	11	2.6	20	3.6	12.5	3.8	4.5	4.0	14	2.5	35.6	17.1	13		·	8	·	·	·	–	–	13	8	1	9	·	·
XII	4.5	2.8	2	1.2	11.5	2.1	14	2.0	10.5	2.1	16.5	4.1	16.5	3.4	6.5	3.7	11	2.5	28.2	13.3	11	9	12	21	·	1	·	–	–	7	5	1	4	10	·
Rok	54	2.5	48	1.5	108	2.1	110.5	2.3	132	2.5	139.5	3.1	254	3.5	108	3.4	141	2.7	571.7	21.6	31. VII	16	22	68	19	5	·	–	–	140	102	16	44	18	18

Wądołki Borowe

$H_s = 130$ m $h_w = 12$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.9	10.7	5	12	12	29	·	–	–	·	15	13	10	1	4	28	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	13.2	3.0	1, 4	1	4	19	·	–	–	·	17	15	4	·	11	9	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.2	6.0	30	·		11	·	–	–	1	8	14	7	·	3	2	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	16.9	4.5	8	·	·	6	·	–	–	10	4	11	6	·	1	3	2
V	12	3.4	1.5	1.3	7	3.9	10.5	3.6	14	3.5	9	3.6	11.5	4.1	10.5	4.7	17	3.1	39.6	10.1	7	·	·	·	2	·	·	·	6	14	8	1	1	·	1
VI	2	2.0	3.5	2.9	9	3.7	19	2.7	12.5	2.9	10	4.4	22	4.5	7	4.9	5	3.5	57.4	20.4	27	·	·	·	10	2	·	2	4	12	11	1	1	·	5
VII	2.5	3.4	3	4.2	1.5	2.0	5.5	3.5	23	3.4	28.5	3.6	14.5	4.5	6.5	2.5	8	3.3	86.6	24.7	30	·	·	·	3	2	·	2	10	15	11	3	2	·	3
VIII	4	3.5	1	2.0	2	2.5	2	1.5	13	4.6	28	4.7	23	4.2	7	3.3	13	3.6	67.1	20.2	10	·	·	·	4	1	·	·	11	14	11	2	·	·	3
IX	2.5	2.6	6	2.5	8.5	2.7	6.5	2.5	7.5	2.7	16	5.0	19	4.8	3	4.3	21	3.0	45.6	16.0	7	·	·	·	5	1	·	11	5	10	6	2	2	·	2
X	1	4.0	2	2.8	17	4.9	39	5.0	14	3.4	2	3.0	12	4.1	4	3.1	2	4.3	6.5	3.6	29	·	·	·	·	2	·	6	10	5	2	·	9	·	·
XI	3	3.5	6.5	5.8	10.5	6.0	14.5	4.3	15	3.6	13	5.8	12.5	5.2	7	4.1	8	4.4	36.2	4.7	27	·	3	15	·	3	·	1	23	21	9	·	4	·	·
XII	10	5.0	4.5	5.1	2	4.5	10.5	4.9	15	3.8	12.5	4.0	24	5.7	8.5	3.7	6	4.4	18.8	7.8	4	–	16	–	·	3	1	2	16	14	6	·	2	21	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	446.0	24.7	30. VII	–	35	–	24	–	–	35	129	158	91	10	40	63	16

Krzyż

$H_s = 31$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41.7	12.6	30	10	11	23	·	–	–	8	13	14	11	1	2	4	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.3	11.5	11	·	1	14	·	–	–	·	17	11	8	1	10	4	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	55.1	13.9	29	·	·	5	·	–	–	1	11	16	12	2	5	1	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39.3	8.0	8	·	·	6	·	–	–	7	7	9	8	·	2	1	3
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	78.1	11.4	16	·	·	·	·	–	–	·	15	19	14	2	3	·	3
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36.1	13.8	4	·	·	·	10	–	–	3	7	9	5	2	2		4
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	143.7	40.5	31	·	·	·	5	–	–	2	21	21	16	5	·		3
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44.3	7.2	22	·	·	·	3	–	–	1	10	19	13	·	2	·	2
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	21.6	8.2	14	·	·	3	6	–	–	11	5	6	5	·	7	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29.8	5.6	23	·	·	·		–	–	6	12	12	9	·	9	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.8	12.8	13	·	·	7	·	–	–	2	19	16	10	2	6	·	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52.3	18.2	11	10	16	23	·	–	–	3	14	10	6	3	2	19	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	627.9	40.5	31. VII	20	28	81	24	–	–	44	151	162	117	18	50	29	16

Ciechocinek — φ = 52°53' — λ = 18°48' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
									Średnie																			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	−4.9	6.0	4	−17.3	26	−3.9	−0.5	−2.5	−2.4	4.6	5.1	4.9	4.9	93	82	91	89	0.3	1.0	0.5	0.6	7.1	7.2	5.3	6.5
II	–	–	–	–	4.6	0.2	11.9	18	−3.4	5, 6	1.2	3.4	1.8	2.0	6.3	6.6	6.5	6.5	95	84	92	90	0.4	1.3	0.6	0.8	9.2	8.4	7.6	8.4
III	–	–	–	–	10.4	2.2	17.1	10	−4.7	20	3.8	8.3	5.6	5.8	7.0	6.9	7.4	7.1	86	64	81	77	1.2	4.2	1.9	2.4	7.6	6.7	6.0	6.8
IV	–	–	–	–	15.5	4.4	25.5	7	−2.5	10	6.6	13.6	9.1	9.6	8.1	9.1	9.0	8.7	81	57	76	71	2.0	7.5	2.9	4.1	4.6	5.3	4.3	4.7
V	–	–	–	–	17.0	7.0	22.6	27	2.9	12, 23	9.9	15.1	11.1	11.8	10.5	10.9	11.0	10.8	86	64	83	78	1.9	6.7	2.4	3.7	6.7	8.5	6.6	7.3
VI	–	–	–	–	24.7	12.9	33.2	27	7.0	23	17.1	22.9	17.5	18.8	14.9	14.8	15.7	15.1	76	54	78	69	4.9	13.8	4.6	7.8	4.0	5.0	4.5	4.5
VII	–	–	–	–	21.6	12.0	33.7	3	8.2	6	15.1	19.3	15.3	16.2	14.4	14.4	14.6	14.5	85	66	84	78	2.9	9.0	3.2	5.0	7.3	7.9	6.5	7.2
VIII	–	–	–	–	20.9	11.8	29.9	6	7.1	14	14.1	19.4	15.1	15.9	14.9	16.0	15.5	15.5	92	71	90	84	1.4	7.0	1.8	3.4	7.0	7.0	5.3	6.4
IX	–	–	–	–	20.4	8.8	29.2	2	0.5	29	10.9	19.4	13.1	14.1	12.3	14.2	13.5	13.3	91	62	87	80	1.3	9.0	2.0	4.1	4.3	4.6	3.7	4.2
X	–	–	–	–	14.8	7.0	19.1	10	2.0	31	8.3	14.2	10.5	10.9	10.0	12.0	10.8	10.9	90	75	85	83	1.1	4.3	2.0	2.5	6.7	6.8	5.0	6.2
XI	–	–	–	–	6.1	1.5	12.1	3	−7.7	24	3.0	5.4	3.5	3.8	7.2	7.8	7.5	7.5	93	86	92	90	0.6	1.3	0.7	0.9	8.6	8.7	7.7	8.3
XII	–	–	–	–	−0.2	−6.6	16.1	5	−20.6	26, 27	−3.6	−1.6	−3.8	−3.2	4.8	5.0	4.5	4.8	89	83	87	86	0.6	1.1	0.7	0.8	7.7	6.2	5.6	6.5
Rok	–	–	–	–	13.0	4.7	33.7	3.VII	−20.6	26,27.XII	6.9	11.6	8.0	8.6	9.6	10.2	10.1	10.0	88	71	86	82	1.6	5.5	1.9	3.0	6.7	6.9	5.7	6.4

Kabylec — φ = 52°51' — λ = 17°12'

I	–	–	–	–	0.7	−5.3	5.5	29	−17.2	27	−4.5	−0.2	−2.6	−2.5	4.3	5.3	4.8	4.8	87	85	87	86	0.5	0.8	0.5	0.6	5.9	6.6	5.7	6.1
II	–	–	–	–	4.8	0.1	11.7	18	−3.1	5	1.0	3.9	2.1	2.3	6.3	7.1	6.7	6.7	94	87	93	91	0.4	1.1	0.5	0.7	8.8	8.3	6.6	7.9
III	–	–	–	–	9.3	2.1	17.2	10	−6.2	20	3.5	8.0	4.6	5.2	7.3	8.0	7.6	7.6	92	74	88	88	0.8	3.1	1.0	1.6	8.5	7.5	5.3	7.1
IV	–	–	–	–	14.9	4.2	24.3	7	−2.4	10	7.1	13.8	8.9	9.7	8.7	9.7	9.3	9.2	83	61	79	74	1.8	7.0	2.5	3.8	5.2	5.5	3.4	4.7
V	–	–	–	–	15.5	6.5	21.7	26	0.5	13	9.9	14.0	9.7	10.8	10.7	11.8	11.0	11.2	87	75	91	84	1.7	4.6	1.2	2.5	7.0	8.4	5.9	7.1
VI	–	–	–	–	23.1	12.2	27.9	26	5.8	22	16.5	21.6	16.6	17.8	15.2	14.8	16.1	15.4	81	58	85	75	3.8	11.5	3.1	6.0	4.6	6.0	5.3	5.3
VII	–	–	–	–	20.3	11.9	33.1	3	7.3	6	14.7	18.5	15.0	15.8	14.8	15.0	15.0	14.9	89	73	87	83	2.1	7.2	2.4	3.9	8.1	8.6	8.1	8.3
VIII	–	–	–	–	20.4	11.8	28.9	6	7.4	4	14.0	19.0	14.8	15.6	14.9	15.3	15.4	15.2	93	70	90	84	1.2	7.1	1.7	3.3	7.5	7.9	5.3	6.9
IX	–	–	–	–	20.6	9.9	29.9	2	1.5	27	11.9	19.7	13.7	14.8	13.0	14.2	13.9	13.7	91	62	88	80	1.4	9.4	2.1	4.3	4.3	4.6	3.2	4.0
X	–	–	–	–	14.8	7.4	21.2	6	2.3	13, 14	8.8	14.2	10.1	10.8	10.5	11.8	11.1	11.1	92	74	89	85	0.9	4.7	1.4	2.3	6.9	6.0	5.1	6.0
XI	–	–	–	–	6.2	1.7	12.4	2	−6.6	23	2.7	5.4	3.3	3.7	7.2	7.8	7.5	7.5	94	86	94	91	0.4	1.3	0.5	0.7	8.3	8.1	7.3	7.9
XII	–	–	–	–	−0.5	−7.7	14.8	5	−22.4	26	−5.1	−2.0	−4.4	−4.0	4.5	5.1	4.5	4.7	91	88	90	90	0.4	0.8	0.5	0.6	6.0	6.4	6.0	6.1
Rok	–	–	–	–	12.5	4.6	33.1	3.VII	−22.4	26, XII	6.7	11.3	7.6	8.3	9.8	10.5	10.2	10.2	90	74	88	84	1.3	4.9	1.4	2.5	6.8	7.0	5.6	6.5

Więcławice — φ = 52°51' — λ = 18°19'

I	–	–	–	–	0.2	−5.0	5.0	4, 31	−16.3	26	−4.1	−0.9	−2.9	−2.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.2	6.5	6.6
II	–	–	–	–	4.2	0.0	10.2	18	−3.3	6	0.8	3.1	1.6	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.6	7.8	7.9
III	–	–	–	–	9.1	2.4	15.1	10	−4.7	20	3.6	7.6	4.9	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.5	6.8	6.5
IV	–	–	–	–	14.5	4.2	23.9	7	−1.7	11	6.8	13.1	8.8	9.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.3	4.9	4.6
V	–	–	–	–	15.7	6.6	21.3	26	0.3	13	10.2	14.3	10.8	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	6.5	6.6
VI	–	–	–	–	23.3	12.4	31.1	27	6.7	22	16.3	21.8	17.0	18.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	3.8	4.6	4.3
VII	–	–	–	–	20.5	11.6	32.1	3	7.8	6	14.4	18.5	15.1	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.8	7.0	6.8
VIII	–	–	–	–	20.0	11.7	28.4	6	7.4	4	13.9	18.7	15.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.6	6.8
IX	–	–	–	–	19.5	9.5	28.0	2	2.9	27	11.4	18.9	14.2	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.2	5.6	5.2
X	–	–	–	–	14.5	7.2	19.1	5	2.5	31	8.1	13.7	10.2	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.2	5.9	5.9
XI	–	–	–	–	5.7	1.8	11.5	2	−4.7	24	2.6	5.0	3.1	3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	7.6	7.6
XII	–	–	–	–	−0.6	−6.0	14.4	5	−19.3	26	−3.9	−2.3	−3.8	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.5	5.9	6.0
Rok	–	–	–	–	12.2	4.7	32.1	3.VII	−19.3	26.XII	6.7	11.0	7.9	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.9	6.3	6.2

Szepietowo — φ = 52°51' — λ = 22°33'

I	–	–	–	–	−1.5	−6.6	5.8	4	−21.8	26	−5.3	−2.8	−4.0	−4.0	4.1	4.4	4.3	4.3	87	83	86	85	0.5	0.8	0.6	0.6	7.3	7.9	7.3	7.5
II	–	–	–	–	2.2	−1.9	9.3	18	−9.5	7	−0.6	1.3	0.2	0.3	5.4	6.1	5.8	5.8	92	90	92	91	0.4	0.7	0.4	0.5	9.0	8.2	6.8	8.0
III	–	–	–	–	7.7	1.2	14.3	18	−2.4	23	2.2	5.8	3.8	3.9	6.6	7.7	7.1	7.1	92	82	88	87	0.6	1.8	1.0	1.1	7.7	7.7	5.5	7.0
IV	–	–	–	–	14.6	3.4	23.5	15	−2.4	10, 11	5.6	12.5	8.3	8.7	8.0	8.9	9.0	8.6	85	60	79	75	1.4	6.4	2.5	3.4	4.6	4.9	3.7	4.4
V	–	–	–	–	16.7	7.2	28.1	29	3.0	15, 23	10.1	14.9	10.9	11.7	10.7	11.1	11.0	10.9	86	66	84	79	1.9	6.6	2.4	3.7	7.2	7.2	7.2	7.2
VI	–	–	–	–	23.3	12.5	31.9	27	8.0	21	16.3	21.2	17.0	17.9	14.8	14.4	15.0	14.7	80	59	77	72	4.2	11.5	4.7	6.8	5.8	6.0	6.1	5.8
VII	–	–	–	–	20.8	11.4	30.0	3	8.5	6	14.3	18.6	15.3	15.9	14.0	13.9	14.2	14.0	86	66	82	78	2.5	8.1	3.4	4.7	5.9	7.4	6.9	6.7
VIII	–	–	–	–	20.7	12.0	29.5	6	8.1	18	13.7	19.1	15.1	15.8	14.2	14.4	14.8	14.5	89	65	86	80	1.7	8.4	2.6	4.2	6.7	7.0	6.6	6.8
IX	–	–	–	–	19.5	8.9	28.1	3	2.0	22	10.2	18.1	12.6	13.4	11.6	12.6	12.7	12.3	91	60	86	79	1.3	8.8	2.3	4.1	5.3	4.3	3.6	4.4
X	–	–	–	–	14.3	5.4	19.0	4	−0.2	23	6.2	13.4	9.4	9.6	8.6	10.1	9.6	9.4	89	67	81	79	1.1	5.4	2.3	2.9	6.6	5.6	4.6	5.6
XI	–	–	–	–	4.7	0.5	11.5	3	−8.7	23	1.8	3.7	2.4	2.6	6.8	7.4	6.9	7.0	93	91	91	92	0.5	0.9	0.7	0.7	9.2	8.6	7.7	8.5
XII	–	–	–	–	−1.7	−7.9	14.1	5	−22.3	26	−5.9	−3.2	−5.0	−4.6	4.2	4.5	4.2	4.3	83	80	81	81	0.5	0.9	0.6	0.7	8.4	7.0	5.5	7.0
Rok	–	–	–	–	11.8	3.8	31.9	27.VI	−22.3	26.XII	5.8	10.2	7.2	7.6	9.1	9.6	9.6	9.4	88	72	84	81	1.4	5.0	2.0	2.8	7.0	6.8	6.0	6.6

Ciechocinek — $H_s = 44\ m$ — $h_w = 14\ m$ — 1961

MIESIĄC	ROZKŁAD WIATRU °D. %D																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	n ≥ 10 m/s	n ≥ 15 m/s	●	●	n ≥ 0.1	n ≥ 1.0	n ≥ 10.0	▬	▦	ZR
I	5	1.7	10.5	2.7	11.5	2.9	10.5	2.1	9.5	2.3	20	3.3	14	2.4	6	2.6	6	2.5	19.2	5.0	30	9	11	23	·	·	·	5	15	12	6	·	1	7	·
II	6	1.4	4	1.5	7	1.7	10	2.4	8.5	2.8	19.5	2.7	14	3.0	10	2.0	5	2.2	27.9	9.1	9	·	·	12	·	1	·	·	18	14	7	·	7	5	·
III	0.5	1.0	·	·	·	·	·	·	·	·	12.5	4.6	58	4.9	20	4.2	2	4.6	31.8	9.0	30	·	·	5	·	6	3	2	14	16	9	·	3	3	·
IV	4.5	1.6	24.5	3.0	19.5	4.3	4	2.9	4	2.6	3.5	2.7	13.5	3.3	9.5	2.6	7	2.9	39.8	6.7	7	·	·	4	2	1	·	8	6	13	11	·	1	1	4
V	18.5	2.2	13	2.3	2	3.2	3	2.5	6	1.8	8	2.4	19	2.5	15.5	2.0	8	2.1	53.7	9.4	15	·	·	·	·	·	·	·	14	15	11	·	3	·	3
VI	5.5	1.0	10.5	2.6	7.5	2.6	5	1.8	2	4.5	11	3.1	25.5	3.4	15	2.3	8	2.5	30.9	13.7	4	·	·	·	13	·	·	7	4	12	5	1	·	·	8
VII	3	1.0	1.5	1.0	1.5	1.7	0.5	1.0	7.5	1.9	24.5	2.6	34	2.6	6.5	2.1	14	2.0	149.0	42.2	31	·	·	·	6	·	·	2	15	20	15	4	·	·	7
VIII	5	1.7	3.5	1.7	2.5	1.2	·	·	6	1.7	18	3.1	34	2.5	14	2.0	10	2.1	69.4	16.3	2	·	·	·	5	·	·	2	11	19	12	1	4	·	7
IX	5	1.1	16.5	2.0	8.5	2.5	1	1.0	0.5	1.0	10.5	2.3	23.5	2.7	9.5	2.1	15	1.9	19.6	6.8	29	·	·	·	5	·	·	12	8	8	5	·	2	·	2
X	2.5	2.0	10	2.0	27.5	4.0	12	1.9	6	2.0	10	1.7	6.5	3.0	7.5	1.9	11	2.4	21.3	6.4	29	·	·	·	·	·	·	5	11	11	5	·	6	·	·
XI	8.5	2.5	9.5	3.3	16	4.0	4.5	2.2	4	1.5	15	4.2	16.5	2.8	5	1.8	11	2.8	42.8	7.4	11	·	·	9	·	·	·	2	21	18	9	·	6	·	·
XII	9.5	1.6	8.5	4.0	9	2.1	5	1.2	7	1.4	17	4.0	19	2.8	14	2.4	4	2.6	26.5	7.7	11	10	14	24	·	1	1	3	11	11	6	·	1	18	·
Rok	73.5	1.6	112	2.2	112.5	2.5	55.5	1.6	61	2.0	169.5	3.1	277.5	3.0	132.5	2.3	101	2.6	531.9	42.2	31.VII	19	25	77	31	9	4	48	148	169	101	6	34	34	31

Kobylec — $H_s = 90\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	18.0	5.3	30	8	11	24	·	–	–	9	16	9	5	·	7	7	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	22.3	8.7	9		·	14		–	–	1	16	14	7	·	14	1	
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	42.9	11.9	30	·		5	·	–	–	2	13	15	9	1	5	2[2]	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32.9	5.7	8	·	·	5	·	–	–	8	6	10	8	·	·	2	3
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	76.0	12.7	5	·	·	·	·	–	–	1	11	14	13	2	·	·	4
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.1	16.2	4	·		·	10	–	–	4	7	9	9	2	1	·	6
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	201.4	68.0	31	·		·	5	–	–	2	20	21	20	7	·	·	5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	61.3	12.6	2			·	3	–	–	2	9	15	13	1	6	·	3
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	12.7	6.7	14			·	4	–	–	10	6	3	2	·	3	·	2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25.7	5.8	19			·	·	–	–	7	13	7	6	·	10	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	26.7	6.5	13	·	·	8	·	–	–	2	17	9	7	·	10	·	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44.2	13.5	11	13	15	24	·	–	–	6	12	7	7	2	6	19	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	611.2	68.0	31.VII	21	26	80	22	–	–	54	146	133	106	15	62	31[2]	23

Więcławice — $H_s = 90\ m$ — $h_w = 22\ m$

I	·	·	7	2.9	4	1.8	16	2.7	14	1.9	29	2.9	10	2.4	7	2.4	6	2.4	22.8	6.4	30	8	12	24	·	·	·	–	–	10	6	·	·	–	·
II	1	4.0	3	1.0	2	2.0	8	3.2	6	3.2	33	2.6	22	2.9	6	2.0	3	2.6	23.6	7.6	9	·	·	13	·	1	·	–	–	11	8	·	7	–	·
III	·	·	·	·	·	·	·	·	·	·	12	3.6	52	5.1	27	5.1	2	4.8	33.8	12.2	30	·	·	5	·	5	·	–	–	15	9	1	2	–	·
IV	4	2.5	8	4.0	15	4.3	14	3.5	2	2.0	9	2.9	16	3.1	11	2.0	11	2.9	51.3	12.0	7	·	·	5	·	·	·	–	–	13	12	1	1	–	3
V	6	2.8	7	2.0	3	2.0	4	1.5	4	2.2	10	2.1	31	2.8	18	2.3	10	2.2	82.0	12.0	6.16	·	·	·	·	·	·	–	–	14	13	3	1	·	5
VI	4	2.2	·	·	11	2.2	6	1.8	10	2.0	15	1.8	30	3.2	7	1.6	7	2.2	49.1	19.5	4	·	·	·	9	1	1	–	–	7	7	1	·	·	6
VII	·	·	·	·	2	2.0	2	2.0	4	1.5	26	2.9	45	2.9	8	2.4	6	2.6	210.1	82.0	31	·	·	·	5	·	·	–	–	18	17	4	·	·	6
VIII	1	1.0	2	1.0	2	2.5	2	1.5	2	1.5	26	1.6	37	2.6	7	2.3	14	1.8	79.6	14.0	22	·	·	·	2	·	·	–	–	11	11	3	3	·	6
IX	3	1.3	2	1.5	13	2.3	11	1.9	8	1.6	19	2.2	21	2.7	5	2.2	8	2.0	24.3	10.0	14	·	·	·	4	·	·	–	–	6	3	1	·	·	·
X	·	·	·	·	16	3.4	23	2.5	7	2.0	19	2.0	15	2.2	3	2.7	10	2.2	29.3	11.3	18	·	·	·	·	·	·	–	–	8	6	1	3	·	·
XI	2	1.0	7	2.1	15	4.0	6	2.1	3	1.7	13	2.4	17	3.0	11	1.9	16	2.2	43.4	6.5	27	·	·	8	·	·	·	–	–	15	11	·	7	·	
XII	5	2.8	4	4.2	11	2.7	3	2.0	1	2.0	28	2.7	20	3.9	7	2.6	14	2.6	23.7	8.5	11	10	14	24	·	1	·	–	–	5	5	·	2	–	·
Rok	26	1.5	40	1.6	94	2.4	95	2.1	61	1.8	239	2.5	316	3.1	117	2.5	107	2.5	673.0	82.0	31. VII	18	26	79	20	8	1	–	–	133	108	15	26	–	26

Szepietowo — $H_s = 150\ m$ — $h_w = 14\ m$

I	11	3.9	3	2.0	2.5	2.0	16.5	2.7	12	3.2	17	3.9	17	3.8	14	3.7	·	3.4	47.9	10.6	5	11	12	29	·	2	·	1	17	13	9	2	·	25	·
II	1	2.5	3	2.0	5	2.0	11.5	3.5	15	3.6	13	2.9	25	3.3	7.5	2.3	3	3.0	14.9	6.4	11	·	5	20	·	1	·	1	17	10	4	·	10	12	·
III	0.5	3.0	·	·	·	·	·	·	1	12.0	15.5	4.1	68.5	6.9	6.5	5.5	1	6.3	26.1	10.3	30	·	·	12	·	12	1	·	13	11	6	1	3	·	·
IV	4	4.2	3	2.3	16	2.6	14	3.5	3	4.3	15	3.0	17	4.0	15	2.9	3	3.1	23.1	8.7	16	·	·	7	·	3	·	9	4	11	6	·	2	·	2
V	4	4.0	·	·	5	3.0	8	2.4	12.5	3.4	16	2.7	33.5	2.5	9	2.8	5	2.6	58.5	12.0	11	·	·	·	3	·	·	·	13	12	10	1	1	·	1
VI	2	2.0	·	·	14	2.5	16	3.2	15	2.1	17.5	3.2	20.5	3.9	1	2.0	4	2.9	63.2	17.2	27	·	·	·	10	·	·	1	10	13	11	1	·	·	8
VII	6	2.5	1	2.0	5.5	2.7	7.5	4.6	18.5	2.9	26	2.9	21.5	2.9	3	1.7	4	2.8	79.8	32.7	30	·	·	·	3	·	·	3	12	11	9	2	·	·	4
VIII	1.5	2.3	0.5	2.0	2.5	2.4	4	4.5	12	2.5	31.5	4.0	30.5	3.1	8.5	2.6	2	3.2	67.2	42.6	10	·	·	·	5	·	·	1	10	13	8	1	1	·	1
IX	2	2.5	2.5	2.2	14.5	2.0	6	1.8	6.5	3.0	16	3.1	32	3.3	7.5	2.3	3	2.7	21.6	7.9	14	·		·	5	1	·	9	7	6	4	·	5	·	1
X	2	2.0	·	·	14	2.6	35.5	4.1	17.5	3.0	9	2.5	14	3.0	·	·	1	3.3	6.0	3.3	29	·	·	1	·	1	·	6	8	3	2	·	9	·	·
XI	7.5	3.5	2.5	3.0	10	3.6	16	3.8	18	2.0	5.5	3.4	25	3.1	2.5	2.8	3	3.0	43.7	9.0	8	·	2	16	·	1	·	1	21	15	11	·	10	·	·
XII	10	5.0	5.5	2.3	·	·	13.5	2.9	19.5	2.2	9	3.8	26	4.2	8.5	3.2	1	3.4	20.0	6.6	4	11	16	25	·	2	·	3	17	11	6	·	3	20	·
Rok	51.5	3.1	21	1.5	89	2.1	148.5	3.1	150.5	3.7	191	3.3	330.5	3.7	83	2.6	30	3.3	472.0	42.6	10.VIII	22	35	110	26	23	4	35	149	129	86	8	44	57	17

Głodowo — φ = 52°50' — λ = 19°15' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	—	—	—	—	−0.2	−5.7	6.4	4	−18.5	26	−4.3	−1.1	−3.5	−3.1	—	—	—	—	—	—	—	—	—	—	—	—	7.3	7.5	5.8	6.9
II	—	—	—	—	3.6	−0.4	10.7	18	−3.8	6	0.6	2.8	1.0	1.4	—	—	—	—	—	—	—	—	—	—	—	—	9.8	8.5	7.1	8.5
III	—	—	—	—	8.6	1.6	15.4	10	−5.0	20	3.5	7.5	4.6	5.0	—	—	—	—	—	—	—	—	—	—	—	—	8.5	7.0	6.2	7.2
IV	—	—	—	—	14.4	3.7	23.5	7	−3.5	10	7.7	13.4	8.0	9.3	—	—	—	—	—	—	—	—	—	—	—	—	5.0	5.0	4.2	4.7
V	—	—	—	—	15.9	5.9	22.5	27	0.9	23	10.3	14.3	9.8	11.0	—	—	—	—	—	—	—	—	—	—	—	—	7.2	8.9	5.8	7.3
VI	—	—	—	—	23.3	11.9	31.5	27	4.4	22	17.3	22.1	16.2	18.0	—	—	—	—	—	—	—	—	—	—	—	—	4.4	5.9	5.8	5.4
VII	—	—	—	—	20.7	10.6	32.2	3	7.6	6	14.6	19.3	14.0	15.5	—	—	—	—	—	—	—	—	—	—	—	—	7.1	8.0	7.0	7.4
VIII	—	—	—	—	20.1	11.6	29.1	6	7.4	30	14.2	18.8	14.7	15.6	—	—	—	—	—	—	—	—	—	—	—	—	8.1	7.4	6.2	7.2
IX	—	—	—	—	19.6	9.4	29.3	2	1.7	27	12.5	18.9	12.8	14.2	—	—	—	—	—	—	—	—	—	—	—	—	3.9	4.4	4.4	4.2
X	—	—	—	—	14.5	6.6	18.5	4	2.6	31	8.9	14.0	9.9	10.7	—	—	—	—	—	—	—	—	—	—	—	—	6.5	6.5	4.7	5.9
XI	—	—	—	—	5.5	1.3	11.6	3	−7.0	23	2.5	4.8	2.8	3.2	—	—	—	—	—	—	—	—	—	—	—	—	8.7	8.5	7.4	8.2
XII	—	—	—	—	−0.8	−7.1	15.6	5	−23.2	27	−4.4	−2.3	−4.4	−3.8	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.6	5.2	6.9
Rok	—	—	—	—	12.1	4.1	32.2	3.VII	−23.2	27.XII	7.0	11.0	7.2	8.1	—	—	—	—	—	—	—	—	—	—	—	—	7.0	7.1	5.8	6.6

Inowrocław — φ = 52°48' — λ = 18°14'

I	—	—	—	—	0.4	−4.7	5.5	4	−15.8	26	−3.3	−0.1	−2.4	−2.0	4.5	4.8	4.7	4.7	85	75	85	82	0.6	1.4	0.7	0.9	7.0	7.0	5.8	6.6
II	—	—	—	—	4.7	0.2	11.7	18	−2.8	6	1.7	4.0	2.0	2.4	6.4	6.9	6.6	6.6	92	84	93	90	0.6	1.4	0.5	0.8	9.3	8.9	6.4	8.2
III	—	—	—	—	9.9	2.4	18.0	10	−5.9	20	4.3	8.9	5.1	5.8	7.3	7.7	7.6	7.5	87	68	86	80	1.1	3.9	1.3	2.1	8.6	7.7	5.8	7.4
IV	—	—	—	—	15.2	4.8	25.0	7	−0.4	2, 10	7.2	14.0	9.2	9.9	8.6	9.6	9.5	9.2	82	59	80	74	1.9	7.3	2.5	3.9	5.6	5.7	4.2	5.2
V	—	—	—	—	16.1	7.1	21.8	27	1.2	13	10.5	14.8	10.2	11.4	10.9	11.6	10.6	11.0	85	69	84	79	1.9	5.6	2.0	3.2	7.2	9.1	5.3	7.2
VI	—	—	—	—	23.8	12.8	30.4	27	7.1	22	16.9	22.9	16.4	18.2	16.0	16.0	15.9	16.0	83	57	85	75	3.4	12.6	2.9	6.3	5.4	5.9	4.4	5.2
VII	—	—	—	—	20.9	12.2	32.9	3	8.1	7	14.8	19.4	14.6	15.8	14.7	14.7	14.5	14.6	87	67	87	80	2.4	8.8	2.3	4.5	7.7	8.4	6.6	7.6
VIII	—	—	—	—	20.8	12.1	29.4	6	8.1	4	14.1	19.6	15.0	15.9	14.8	16.3	15.4	15.5	92	72	90	85	1.4	6.9	1.9	3.4	7.7	7.7	4.7	6.7
IX	—	—	—	—	20.6	10.2	29.1	2	5.1	27	12.0	19.8	13.8	14.8	12.3	13.9	13.2	13.1	86	60	82	76	2.0	9.8	2.9	4.9	4.8	4.6	3.2	4.2
X	—	—	—	—	14.9	7.4	19.5	6,10	2.8	31	8.6	14.3	10.3	10.9	10.2	12.1	11.0	11.1	90	75	88	84	1.1	4.5	1.5	2.4	7.4	6.3	4.5	6.1
XI	—	—	—	—	6.0	1.9	12.1	2	−5.2	23	3.2	5.5	3.4	3.9	7.2	7.6	7.3	7.3	91	83	91	88	0.7	1.6	0.7	1.0	9.0	8.7	7.4	8.4
XII	—	—	—	—	−0.4	−6.3	15.5	5	−18.8	26,27	−3.2	−1.7	−3.6	−3.0	4.8	4.8	4.6	4.7	86	78	85	83	0.6	1.2	0.6	0.8	7.6	7.2	6.0	6.9
Rok	—	—	—	—	12.7	5.0	32.9	3.VII	−18.8	26,27.XII	7.2	11.8	7.8	8.6	9.8	10.5	10.1	10.1	87	71	86	81	1.5	5.4	1.6	2.8	7.3	7.3	5.4	6.7

Bielsk Podlaski — φ = 52°47' — λ = 23°11'

I	—	—	—	—	−1.6	−7.6	5.9	4	−26.7	25	−5.7	−2.6	−4.5	−4.3	—	—	—	—	—	—	—	—	—	—	—	—	7.7	7.9	7.2	7.6
II	—	—	—	—	2.1	−2.0	8.7	18	−9.3	5	−0.7	1.4	0.2	0.3	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.8	7.5	8.4
III	—	—	—	—	8.0	1.0	15.4	10	−3.6	20	2.4	6.6	3.9	4.2	—	—	—	—	—	—	—	—	—	—	—	—	8.8	8.2	7.1	8.0
IV	—	—	—	—	14.3	3.5	23.6	15	−2.6	10	5.9	13.3	8.3	8.9	—	—	—	—	—	—	—	—	—	—	—	—	6.1	5.8	4.3	5.4
V	—	—	—	—	17.2	7.1	25.9	28.29	3.0	16	10.7	15.7	10.9	12.1	—	—	—	—	—	—	—	—	—	—	—	—	7.6	7.6	6.7	7.3
VI	—	—	—	—	23.5	11.8	30.9	27	5.6	21	16.5	21.7	16.6	17.8	—	—	—	—	—	—	—	—	—	—	—	—	6.2	7.1	6.2	6.5
VII	—	—	—	—	21.0	11.2	28.9	13	7.3	6	14.8	19.4	15.2	16.1	—	—	—	—	—	—	—	—	—	—	—	—	6.5	7.5	7.0	7.0
VIII	—	—	—	—	20.8	11.7	29.5	7	7.1	18	14.1	19.7	15.1	16.0	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.3	6.3	7.0
IX	—	—	—	—	19.6	7.9	27.7	3	−0.3	24	9.7	18.4	11.7	12.9	—	—	—	—	—	—	—	—	—	—	—	—	5.5	5.0	4.3	4.9
X	—	—	—	—	14.6	5.1	18.4	28	0.2	23	6.4	13.9	9.2	9.7	—	—	—	—	—	—	—	—	—	—	—	—	6.7	6.3	4.9	6.0
XI	—	—	—	—	4.8	0.7	11.8	3	−6.0	24	2.1	4.1	2.6	2.8	—	—	—	—	—	—	—	—	—	—	—	—	9.7	8.8	8.4	9.0
XII	—	—	—	—	−1.6	−8.0	14.0	5	−21.8	27	−5.3	−3.0	−4.8	−4.5	—	—	—	—	—	—	—	—	—	—	—	—	8.4	7.7	5.3	7.1
Rok	—	—	—	—	11.9	3.5	30.9	27.VI	−26.7	25.I	5.9	10.7	7.0	7.6	—	—	—	—	—	—	—	—	—	—	—	—	7.5	7.3	6.3	7.0

Gorzów Wlkp. — φ = 52°44' — λ = 15°15'

I	1010.6	1035.7	986.4	1018.3	0.7	−5.0	6.7	29	−17.5	27	−3.5	−0.5	−2.1	−2.0	4.7	5.1	4.9	4.9	92	82	88	87	0.4	1.0	0.6	0.7	6.8	6.7	6.1	6.5
II	1013.0	1029.8	983.4	1020.5	6.6	0.9	13.0	28	−4.3	6	2.1	4.7	3.3	3.4	6.8	7.4	7.2	7.1	95	86	92	91	0.4	1.3	0.7	0.8	8.4	8.0	7.1	7.8
III	1010.4	1029.3	981.4	1017.9	10.0	2.6	18.0	10	−4.5	20	3.8	8.4	6.0	6.0	7.4	7.6	7.8	7.6	91	69	83	81	0.8	3.7	1.8	1.8	8.1	7.6	5.5	7.1
IV	1004.6	1015.2	994.4	1011.8	15.4	5.3	24.7	14	−0.7	1	6.4	13.6	10.4	10.2	8.5	9.4	9.4	9.1	86	60	72	73	1.4	7.1	3.6	4.0	6.6	6.1	3.9	5.5
V	1005.1	1015.2	990.3	1012.4	15.4	7.1	23.0	26	3.8	18	9.0	13.6	10.5	10.9	10.6	11.0	10.8	10.8	91	72	84	82	1.0	4.9	2.1	2.7	7.9	8.5	6.8	7.7
VI	1007.5	1021.9	994.0	1014.7	22.6	12.5	28.8	26	7.5	22	14.9	21.0	17.5	17.7	14.9	15.6	15.7	15.4	88	63	78	76	2.2	9.8	4.5	5.5	4.8	6.3	4.9	5.3
VII	1005.4	1018.8	990.4	1012.6	20.2	12.2	32.6	3	7.9	6	13.8	18.3	15.5	15.8	14.5	14.1	14.6	14.4	91	69	83	81	1.5	7.8	3.3	4.2	8.8	8.0	8.0	8.3
VIII	1008.1	1021.2	996.1	1015.3	20.6	12.1	27.8	6	8.3	4	13.6	19.0	15.7	16.0	14.6	15.0	15.4	15.0	93	69	86	83	1.1	7.4	2.6	3.7	7.7	7.3	5.8	6.9
IX	1010.4	1021.0	995.7	1017.6	21.3	10.4	30.4	2	3.1	27	11.4	19.8	14.9	15.2	13.0	14.1	13.8	13.6	94	61	80	78	0.8	9.7	3.6	4.7	4.3	5.1	3.9	4.4
X	1009.4	1023.1	979.2	1016.7	15.4	8.0	22.2	6	3.2	31	8.6	14.2	10.9	11.2	10.5	11.6	11.4	11.2	94	73	88	85	0.8	5.1	1.7	2.5	6.6	6.0	5.2	5.9
XI	1006.6	1029.7	990.5	1014.1	6.2	1.6	13.0	2	−6.3	22	2.6	5.2	3.8	3.8	7.1	7.8	7.6	7.5	95	86	92	91	0.4	1.3	0.6	0.8	8.4	8.3	7.1	7.9
XII	1008.2	1040.0	980.2	1015.9	0.7	−5.8	15.3	5	−19.9	26	−3.3	−1.1	−2.7	−2.4	5.0	5.2	4.9	5.0	91	84	88	88	0.5	1.1	0.7	0.8	7.0	6.9	6.3	6.7
Rok	1008.3	1040.0	979.2	1015.7	12.9	5.2	32.6	3.VII	−19.9	26.XII	6.6	11.4	8.6	8.8	9.8	10.3	10.3	10.1	92	73	84	83	0.9	5.8	2.3	2.7	7.1	7.1	5.9	6.7

Głodowo

$H_s = 129\ m$ $h_w = 10\ m$ 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < −10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	·	·	4	4.0	7	3.1	8.5	5.6	21	2.0	22	3.8	15	3.9	6.5	2.5	9	3.1	13.4	3.6	30	11	12	28	·	1	·	4	13	6	6	·	6	10	·
II	·	·	·	·	·	·	17	3.2	13.5	4.2	19.5	3.6	29	4.0	5	2.8	·	3.7	34.8	10.6	9	·	1	17	·	1	1	·	17	12	7	1	12	5	·
III	0.5	4.0	·	·	1	4.0	·	·	1	5.0	9	5.7	66	6.6	12.5	8.2	3	6.5	35.2	10.4	30	·	·	9	·	8	1	1	15	13	9	1	4	2	·
IV	4	3.8	2	4.0	26	5.3	21.5	3.8	4.5	2.9	5	4.0	13.5	3.4	3.5	4.6	10	3.7	35.6	8.4	15	·	·	7	·	1	·	9	9	12	10	·	2	1	3
V	7	3.0	1	3.0	4	3.5	12	2.8	4	2.2	15.5	3.5	27.5	3.8	13	3.7	9	3.1	52.1	9.6	7	·	·	·	·	·	·	·	12	13	11	·	1	·	4
VI	3	1.3	3	2.7	7	2.9	11	1.9	9	1.9	15	2.5	25	4.0	10	3.3	7	2.7	35.1	6.6	14	·	·	·	10	·	·	2	4	12	10	·	1	·	2
VII	4	1.8	·	·	1	1.0	1	6.0	8	1.9	27.5	3.1	38.5	4.3	3	4.3	10	3.1	181.1	61.3	31	·	·	·	5	·	·	2	16	18	17	6	1	·	5
VIII	5	2.0	1	2.0	4	2.2	1	2.0	12	1.8	27	3.6	32	3.4	4	2.8	7	2.8	82.6	14.2	6	·	·	·	3	·	·	1	14	17	16	3	4	·	4
IX	1	2.0	3	1.3	15	2.4	11.5	2.7	13.5	1.4	11	2.5	25	3.4	1	1.0	9	2.3	37.6	11.3	14	·	·	·	5	·	·	12	5	10	6	2	3	·	2
X	·	·	·	·	16	3.7	24.5	3.6	24.5	2.3	8	3.6	8	3.6	5	2.2	7	2.9	17.2	3.7	29	·	·	·	·	·	·	6	10	10	6	·	9	·	·
XI	5	2.4	7	5.4	14	6.4	11	2.8	5	2.4	18.5	3.1	23.5	4.3	2	3.0	4	3.9	65.9	16.0	11	·	1	10	·	1	–	2	21	20	12	1	–	·	·
XII	5	2.6	6	3.5	3	1.7	10.5	4.3	14	1.8	16.5	6.3	24	4.0	9	3.2	5	3.6	31.5	8.7	1	11	14	24	·		·	1	11	15	5	·	5	15	·
Rok	34.5	1.9	27	2.2	98	3.0	129.5	3.2	130	2.5	194.5	3.8	327	4.1	74.5	3.5	80	3.4	622.1	61.3	31.VII	22	28	95	23	12	2	40	147	158	115	14	–	33	20

Inowrocław

$H_s = 90\ m$ $h_w = 15\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < −10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	0.5	2.0	9	2.8	6.5	2.1	26	2.5	10	2.6	25.5	3.9	7	2.6	8.5	2.5	·	2.9	8.4	1.7	31	7	11	23	·	1	-	6	15	11	4	·	1	2	·
II	3.5	2.7	·	·	·	·	17.5	2.9	13.5	3.6	22.5	2.5	18	2.9	9	2.4	·	2.9	17.6	4.2	11	·	·	13	·	1	1	1	17	10	7	·	7	1	·
III	·	·	·	·	·	·	·	·	0.5	5.0	17.5	4.2	53.5	5.1	21.5	5.0	·	4.9	23.5	5.6	30	·	·	6	·	7	2	1	15	13	10	·	2	1	·
IV	3	3.0	7	2.5	15.5	3.4	22.5	4.2	7	2.6	8.5	3.9	15	2.3	11.5	2.8	·	3.2	61.0	38.4	16	·	·	2	·	·	·	6	9	11	8	1	1	1	3
V	11	2.8	14.5	2.5	4	2.8	5.5	2.3	6	2.5	18	2.6	20.5	3.0	13.5	2.7	·	2.7	72.1	9.6	14	·	·	·	·	·	·	·	12	18	13	·	1	·	3
VI	1	1.0	2	1.5	8.5	1.8	12.5	2.4	4.5	2.6	14	2.9	30	3.2	9.5	1.9	8	2.4	35.7	9.8	7	·	·	·	9	·	·	2	5	10	7	·	·	·	7
VII	1	2.0	0.5	2.0	1.5	2.7	2	3.0	5.5	2.4	37	3.2	30.5	2.5	11	3.0	4	2.8	165.8	52.7	31	·	·	·	5	·	·	2	15	19	15	5	·	·	6
VIII	4.5	1.3	1.5	1.3	3.5	1.4	4.5	2.9	4	2.6	39.5	3.6	25.5	3.0	10	2.2	·	3.0	69.1	12.3	23	·	·	·	5	·	·	2	9	16	13	1	1	·	5
IX	2.5	1.2	7	2.0	15	3.3	13.5	3.8	6.5	1.8	22	3.1	20.5	2.4	3	2.5	·	2.8	13.6	8.5	14	·	·	·	6	·	·	11	6	8	3	·	1	·	1
X	0.5	1.0	1.5	2.3	12	4.0	33.5	5.1	15.5	3.9	14	4.0	6	2.4	10	2.7	·	4.1	26.8	10.8	18	·	·	·	·	3	·	4	10	10	6	1	3	·	·
XI	6.5	3.8	6.5	3.7	10	4.2	10.5	3.0	7.5	2.3	25	4.1	18	2.7	6	2.5	·	3.4	32.8	4.7	27	·	·	9	·	4	·	2	21	18	10	·	4	·	·
XII	5	2.6	8	3.2	2	2.5	5.5	3.5	12.5	2.5	28	4.1	21	3.5	11	2.9	·	3.4	32.3	6.3	2	10	14	24	·	3	·	·	14	11	7	·	1	18	·
Rok	39	2.0	57.5	2.0	78.5	2.4	153.5	3.0	93	2.9	271.5	3.5	265.5	3.0	124.5	2.8	12	3.2	558.7	52.7	31.VII	17	25	77	25	19	3	37	148	155	103	8	22	23	25

Bielsk Podlaski

$H_s = 145\ m$ $h_w = 12,5\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < −10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	3	1.2	2	5.0	2	1.0	12	3.2	18	3.0	27	4.1	13.5	3.1	10.5	3.2	5	3.2	43.8	11.6	12	13	13	28	·	1	·	3	4	20	9	2	·	20	
II	0.5	1.0	3.5	1.6	2	1.5	13	3.9	15	3.1	23	2.2	14.5	2.5	5.5	1.9	7	2.4	23.9	6.8	5	·	6	19	·	·	·	1	17	12	7	·	7	4	·
III	1.5	5.7	·	·	·	·	1	1.0	4	4.9	25.5	5.3	49.5	5.5	9.5	9.0	2	5.6	36.0	12.0	30	·	·	11	·	8	1	·	17	15	8	1	2	·	-
IV	5.5	2.5	9	2.8	10	3.4	16	5.2	3	2.7	18.5	3.1	12	4.0	12	2.8	4	3.4	44.6	27.2	16	·	·	6	·	3	1	5	7	11	7	1	1	·	2
V	4	2.0	1.5	3.0	6.5	1.9	11.5	2.6	7.5	3.3	14.5	2.6	24	2.5	11.5	2.6	12	2.2	57.6	12.9	7	·	·	·	2	·	·	·	11	16	10	3	·	·	3
VI	·	·	5	1.4	10.5	1.9	13.5	3.1	4.5	1.6	22	3.0	14.5	3.0	9	2.3	11	2.3	90.0	33.2	12	·	·	·	12	·	·	·	9	16	14	3	·	·	6
VII	3	3.0	1	1.0	1	3.0	3	3.0	8	3.6	30	2.7	31	2.4	9	1.1	7	2.3	110.3	28.3	30	·	·	·	4	·	·	1	11	13	8	5	·	·	3
VIII	0.5	3.0	3	2.0	·	·	1	1.0	5	2.6	30	3.7	29.5	2.5	15	2.7	9	2.6	66.8	15.1	10	·	·	·	5	·	·	1	12	17	13	2	·	·	4
IX	8	1.1	8.5	1.7	1.5	2.3	2.5	2.6	2.5	3.4	21	3.0	21.5	3.2	10.5	1.9	14	2.2	34.5	9.8	6	·	·	2	6	·	·	11	7	10	7	·	6	·	2
X	·	·	9	2.6	17	3.6	26.5	5.4	10.5	2.9	8	2.9	7	2.4	8	1.9	7	3.4	6.1	3.4	29	·	·	·	·	3	1	4	9	2	2	·	7	·	-
XI	3.5	2.7	6.5	3.3	13	4.0	17.5	3.4	7	2.3	16	4.1	14	2.8	5.5	2.1	7	3.0	45.0	12.2	8	·	1	16	·	1	·	·	22	17	8	1	6	·	-
XII	10.5	3.1	4	2.2	3	2.7	8	2.8	13.5	2.6	16	4.6	17.5	3.4	14.5	3.6	6	3.1	34.7	7.8	20	11	16	25	·	2	·	3	14	20	8	·	1	21	-
Rok	40	2.1	53	2.2	66.5	2.1	125.5	3.1	98.5	3.0	251.5	3.4	248.5	3.1	120.5	2.9	91	3.0	593.3	33.2	12.VI	24	36	107	29	18	3	29	140	169	101	18	30	45	20

Gorzów Wlkp.

$H_s = 65\ m$ $H_b = 59,7\ m$ $h_w = 12\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < −10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	2	3.0	3	2.0	26	3.3	20	3.0	6	2.5	17	2.5	11.5	2.4	7.5	2.5	·	2.8	35.6	8.2	30	8	10	23	·	·	·	7	17	15	11	·	4	11	·
II	4	1.8	1.5	1.7	11.5	2.7	12.5	2.3	3.5	1.9	14.5	2.4	15.5	2.1	20	2.4	1	2.3	37.4	7.4	9	·	·	8	·	·	·	1	15	16	10	·	7	3	·
III	9.5	2.6	0.5	3.0	·	·	·	·	0.5	5.0	3.5	5.1	39.5	4.1	39.5	4.1	·	4.0	47.9	11.1	30		·	5		5	4	2	11	18	12	1	3	1	·
IV	13	2.9	9	2.3	29	3.9	13.5	4.4	3	2.0	7.5	1.1	4.5	1.8	9.5	2.3	1	3.1	60.1	22.3	27	·	·	1	·	2	·	7	7	12	10	1	3	·	3
V	30	2.8	9.5	2.5	4	2.5	5	2.2	3.5	2.9	5.5	2.5	20	2.6	15.5	2.8	·	2.7	83.0	11.9	9	·	·	·		·	·	·	16	20	16	2	1	·	3
VI	17.5	2.0	4	1.8	13.5	2.1	5.5	2.8	1	2.5	1.5	3.7	15	3.0	32	2.4	·	2.4	54.9	14.4	10	·	·	·	9	·	·	3	4	10	7	2	·	·	5
VII	3.5	1.9	8.5	1.2	3	3.0	1	1.0	1	2.0	10	3.2	36.5	2.9	29.5	2.4	·	2.5	105.2	19.1	6	·	·	·	4	·	·	1	22	22	19	3	2	·	4
VIII	8.5	1.7	3	1.8	3	2.0	4.5	2.1	2	1.8	9	3.1	37	2.5	26	2.2	·	2.3	52.3	12.1	10	·	·	·	4	·	·	3	14	17	13	1	2	·	3
IX	9	1.8	6.5	1.8	22	2.5	9	2.3	5.5	2.3	6	2.2	15	2.3	17	2.7	·	2.3	25.8	8.8	14	·	·	·	6	1	1	10	8	11	5	·	·	·	2
X	4.5	2.2	1.5	2.0	24.5	3.7	15.5	3.6	5.5	2.8	17.5	1.9	12	2.1	12	1.8	·	2.7	46.6	12.5	20	·	·	·	·	·	·	5	11	12	11	1	5	·	·
XI	11	1.6	17	2.1	16.5	4.2	6.5	2.6	2	2.0	10	3.4	16	2.9	10	2.4	1	2.7	57.4	19.2	30	·	·	8	·	2	2	2	17	16	9	2	9	·	·
XII	8	2.8	7.5	2.5	21	2.5	14.5	2.1	3.5	2.0	7.5	6.2	22	3.7	9	3.2	·	3.1	43.2	14.0	1	9	14	23	·	3	·	5	15	13	7	2	5	15	·
Rok	120.5	2.3	71.5	2.1	174	2.7	107.5	2.4	37	2.5	109.5	3.1	244.5	2.7	227.5	2.6	3	2.7	649.4	22.3	27.IV	17	24	68	23	13	7	46	157	182	130	15	41	30	20

Kołuda Wielka — φ = 52°44' — λ = 18°09' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	−5.8	4.8	4	−19.8	26	−4.2	−0.6	−2.9	−2.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	5.4	6.2
II	–	–	–	–	4.5	−0.5	11.3	18	−3.3	5, 6	0.8	3.6	1.4	1.8	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.6	6.6	8.2
III	–	–	–	–	9.3	2.0	17.9	10	−4.4	20	3.6	8.1	4.9	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.1	6.5	7.5
IV	–	–	–	–	15.6	4.3	25.6	7	−1.4	1	7.4	14.1	9.0	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.7	5.1	5.6
V	–	–	–	–	16.9	7.1	22.5	26	2.0	13	10.3	14.9	10.4	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.9	7.4	7.7
VI	–	–	–	–	24.3	12.6	31.9	27	6.2	22	15.7	22.3	17.0	18.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.8	4.6	5.3
VII	–	–	–	–	21.5	11.9	33.8	3	7.2	6	14.5	19.3	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.1	7.1	7.5
VIII	–	–	–	–	21.2	11.7	29.9	6	7.7	4	13.8	19.5	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	6.8	7.1
IX	–	–	–	–	21.0	8.9	30.2	2	2.3	24	10.7	19.9	12.6	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.1	3.5	4.3
X	–	–	–	–	15.2	6.3	20.6	10	2.6	31	8.1	14.3	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.0	4.9	5.6
XI	–	–	–	–	5.9	1.5	11.9	2	−6.6	23	2.4	5.4	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	9.0	9.3	8.0	8.8
XII	–	–	–	–	0.2	–	15.7	5	–	–	−3.6	−1.6	−3.9	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	5.4	6.5
Rok	–	–	–	–	13.0	–	33.8	3. VII	–	–	6.6	11.6	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.2	5.9	6.7

Puttusk — φ = 52°42' — λ = 21°06'

I	–	–	–	–	0.4	−5.7	4.6	4	−21.3	26	−4.4	−1.7	−3.3	−3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	6.5	7.0
II	–	–	–	–	3.3	−0.6	11.5	18	−3.3	5	0.4	2.5	0.9	1.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.0	7.4	8.2
III	–	–	–	–	9.0	1.7	16.8	10	−2.9	3	3.1	7.0	4.6	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.1	4.7	6.6
IV	–	–	–	–	15.4	3.9	24.2	14	−2.1	11	6.2	13.6	9.1	9.5	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.9	3.9	4.4
V	–	–	–	–	17.5	7.7	26.7	28	3.2	15	10.1	15.9	11.6	12.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.9	6.1	6.6
VI	–	–	–	–	24.4	12.5	33.1	27	6.0	21	16.4	22.5	17.4	18.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.5	5.0	5.3
VII	–	–	–	–	21.7	11.3	31.7	3	7.3	6	14.2	19.7	15.9	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.4	6.4	6.6
VIII	–	–	–	–	21.2	12.1	30.5	6	7.5	31	14.3	19.7	15.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.9	5.8	6.3
IX	–	–	–	–	20.4	8.6	28.7	3	0.6	25	9.7	19.4	12.6	13.7	–	–	–	–	–	–	–	–	–	–	–	–	4.6	3.6	2.7	3.6
X	–	–	–	–	15.1	5.6	21.4	19	2.1	29	7.3	14.1	9.8	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.0	3.3	5.1
XI	–	–	–	–	5.6	0.8	12.3	3	−8.0	23	2.3	4.5	2.9	3.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.5	7.7	8.1
XII	–	–	–	–	−0.8	−7.0	15.4	5	−23.4	26	−4.6	−2.6	−4.1	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.6	5.0	6.4
Rok	–	–	–	–	12.7	4.2	33.1	27. VI	−23.4	26. XII	6.2	11.2	7.7	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.4	6.2

Białowieża — φ = 52°42' — λ = 23°51'

I	999.8	1020.5	979.3	1020.8	−1.5	−8.0	7.0	4	−24.9	26	−5.9	−2.6	−4.6	−4.4	4.0	4.4	4.3	4.2	89	83	89	87	0.4	0.8	0.4	0.5	7.6	7.9	8.2	7.9
II	1001.9	1019.0	976.1	1022.6	2.3	−2.6	6.8	15	−8.7	6	−1.2	1.2	−0.1	0.0	5.4	6.9	5.6	5.6	95	88	92	92	0.3	0.9	0.5	0.6	9.2	9.0	7.7	8.6
III	993.2	1013.9	972.6	1013.4	7.7	0.0	16.5	18	−6.5	23	1.8	6.0	3.7	3.8	6.2	6.6	6.5	6.4	88	70	82	80	0.9	3.1	1.6	1.9	9.1	8.3	6.0	7.8
IV	994.5	1006.9	982.0	1014.4	14.0	2.0	23.7	15	−5.2	11	5.4	12.6	7.0	8.0	7.6	7.7	8.1	7.8	81	52	78	70	1.7	7.8	2.3	3.9	6.1	4.3	3.4	4.6
V	992.2	1000.5	982.2	1011.8	16.5	5.7	25.8	30	0.3	19	9.9	15.3	10.1	11.4	10.4	10.1	10.6	10.4	85	59	85	76	2.0	8.0	2.1	4.0	7.1	7.8	5.1	6.7
VI	995.8	1006.7	987.3	1015.0	23.2	10.8	31.4	27	4.2	21	16.2	20.9	16.1	17.3	14.5	14.0	14.2	14.2	79	58	78	72	4.1	11.5	4.4	6.7	5.1	6.3	4.9	5.4
VII	993.7	1005.8	980.4	1013.1	21.3	11.0	28.8	13	7.4	6, 20	14.9	19.5	15.4	16.3	13.9	13.3	14.0	13.7	82	59	80	74	3.1	9.9	3.7	5.6	5.6	7.8	6.1	6.5
VIII	995.6	1009.1	982.1	1015.0	20.8	11.6	29.5	7	5.9	18	13.9	19.6	14.8	15.8	13.9	13.9	14.8	14.2	87	61	87	78	2.2	9.6	2.3	4.7	7.9	7.0	5.8	6.9
IX	999.5	1012.3	986.6	1019.3	19.0	7.1	28.3	3	−1.7	23	9.1	17.7	11.0	12.2	11.0	12.1	12.0	11.7	91	60	99	80	1.1	8.8	1.7	3.9	5.6	5.3	3.2	4.7
X	1002.5	1013.5	981.5	1022.5	14.3	4.0	18.3	4	−2.1	23	5.5	13.6	8.6	9.1	8.1	9.4	8.7	8.7	88	62	78	76	1.1	6.4	2.6	3.4	7.0	5.9	3.7	5.5
XI	995.3	1014.4	982.8	1015.6	4.5	0.1	12.3	3	−7.6	24	1.9	3.8	2.3	2.6	6.7	7.1	6.7	6.8	93	87	91	90	0.5	1.2	0.7	0.8	9.6	9.2	8.3	9.0
XII	994.9	1024.3	973.3	1015.8	−1.7	−9.1	13.7	5	−25.7	27	−5.9	−3.2	−5.1	−4.8	4.1	4.6	4.3	4.3	88	84	88	87	0.5	0.9	0.5	0.6	8.6	7.7	5.9	7.4
Rok	996.6	1024.3	972.6	1016.6	11.7	2.7	31.4	27. VI	−25.7	27. XII	5.5	10.4	6.6	7.3	8.8	9.1	9.2	9.0	87	69	85	80	1.5	5.7	1.9	3.0	7.4	7.2	5.7	6.8

Łagiewniki — φ = 52°40' — λ = 18°19'

I	–	–	–	–	0.2	−4.9	5.0	4	−15.7	27	−3.7	−0.6	−2.7	−2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	4.5	−0.2	11.1	18	−3.0	6, 7	1.4	3.7	1.8	2.2	6.6	7.1	6.6	6.8	97	89	94	93	0.3	1.0	0.5	0.6	–	–	–	–
III	–	–	–	–	9.2	2.4	16.8	10	−4.2	20	4.6	8.1	5.0	5.7	7.5	7.4	7.5	7.5	88	69	85	81	1.2	3.6	1.4	2.1	–	–	–	–
IV	–	–	–	–	14.5	4.5	24.6	7	−1.2	1	7.6	13.5	8.9	9.7	8.5	8.8	8.9	8.7	80	57	76	71	2.4	7.7	3.0	4.4	–	–	–	–
V	–	–	–	–	16.3	6.9	23.1	5	0.8	13	10.9	14.6	10.6	11.7	10.7	10.4	10.6	10.6	82	64	83	76	2.5	6.6	2.4	3.8	–	–	–	–
VI	–	–	–	–	23.8	12.3	31.1	27	6.6	22	17.0	22.4	17.1	18.4	15.2	14.2	15.4	14.9	78	53	78	70	4.3	13.5	4.5	7.4	–	–	–	–
VII	–	–	–	–	20.9	11.6	33.1	3	8.1	6	15.1	18.8	14.7	15.8	14.3	13.9	14.0	14.1	83	66	83	77	3.0	8.7	3.0	4.9	–	–	–	–
VIII	–	–	–	–	20.8	11.9	29.1	6	7.9	14	14.6	19.5	15.4	16.2	15.0	15.2	14.9	15.0	90	68	85	81	1.8	7.9	2.8	4.2	–	–	–	–
IX	–	–	–	–	20.4	9.4	28.7	2	2.3	27	12.3	19.2	13.2	14.5	13.0	14.0	12.7	13.2	89	63	82	78	1.7	9.5	2.6	4.6	–	–	–	–
X	–	–	–	–	15.2	6.9	19.8	6	1.6	31	8.7	14.4	10.0	10.8	10.3	11.8	10.7	10.9	91	73	87	84	1.1	4.8	1.6	2.5	–	–	–	–
XI	–	–	–	–	6.1	1.8	11.4	3	−5.9	23	3.0	5.4	3.5	3.8	7.6	7.8	7.4	7.6	93	86	92	90	0.5	1.3	0.7	0.8	–	–	–	–
XII	–	–	–	–	−0.1	−6.8	16.0	5	−20.5	26	−3.3	−1.3	−3.7	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.6	4.6	33.1	3. VII	−20.5	26. XII	7.4	11.5	7.8	8.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kołuda Wielka

$H_s = 85\,m$ $h_w = 12\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%, ‰D) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min ≤ -10°	Max ≤ 0°	Max ≤ 0°	Max ≥ 25°	Wiatr v ≥ 10	≥ 15	●	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	▬	▩	≋
I	1	2.0	8	1.9	3	1.3	8	2.3	25	2.4	8	2.4	12	2.8	1	3.0	27	1.7	19.9	5.3	31	10	10	7	·	·	·	7	14	9	6	·	·	3	–
II	2	1.5	·	·	4	1.8	1	1.0	24	27	9	2.9	14	3.6	5	2.2	25	2.0	26.4	7.6	9	·	·	17	·	1	1	1	18	11	8	·	4	2	–
III	1	1.0	·	·	·	·	·	·	·	·	14	8.9	57	6.6	9	4.3	12	5.8	29.6	8.0	30	·	·	7	·	8	5	2	17	11	9	·	2	2	–
IV	12.5	2.0	2.5	1.8	14	2.4	5	2.0	6	1.7	2	3.0	6	3.3	14	2.6	28	1.6	35.2	9.5	16	·	·	3	1	·	·	4	12	11	10	·	·	2	–
V	12	1.7	8	1.8	2	2.0	2	2.0	6	2.2	6	1.8	22	2.2	11	2.3	24	1.5	61.9	14.2	6	·	·	·	·	·	·	·	18	14	11	1	1	·	–
VI	1	2.0	2	2.5	3	2.7	1	1.0	6.5	1.9	2.5	2.2	29	1.9	8	2.1	37	1.2	41.4	18.0	7	·	·	·	12	·	·	6	10	10	7	1	·	·	–
VII	·	·	·	·	·	·	·	·	6.5	2.4	9.5	2.1	42	2.0	4	3.2	31	1.4	151.2	69.4	31	·	·	·	6	1	·	2	15	14	13	4	·	·	–
VIII	1	2.0	4	3.9	1	3.5	1	1.0	5	2.0	9.5	2.2	30	2.2	11.5	2.7	30	1.6	63.4	11.5	7	·	·	·	5	·	·	3	15	14	13	2	2	·	–
IX	0.5	2.0	1	2.0	9	1.8	1	2.0	9.5	1.9	9.5	2.4	17	2.1	5.5	2.4	37	1.2	16.3	10.2	14	·	·	·	5	·	·	12	9	9	3	1	2	·	–
X	2.5	1.8	4.5	2.6	10	2.6	20	1.6	21	2.2	2	2.0	4	1.8	4	2.0	25	1.5	32.0	10.0	19	·	·	·	·	·	·	9	14	10	7	1	·	·	–
XI	5	2.0	1	2.0	10	3.7	1	1.0	4.5	2.0	17.5	2.7	6	2.3	7	1.7	38	1.5	31.8	7.3	13	·	·	6	·	·	·	1	23	13	8	·	3	·	–
XII	4	2.1	4	1.6	0.5	1.0	4	1.5	9	1.6	19	2.7	19.5	2.2	11	2.3	22	1.6	32.6	7.6	1	–	15	–	·	·	·	·	17	11	7	·	–	19	–
Rok	42.5	1.7	35	1.7	56.5	1.9	44	1.3	123	1.9	108.5	2.9	258.5	2.8	91	2.6	336	1.9	541.7	69.4	31.VII	–	25	–	29	10	6	47	182	137	102	10	–	28	–

Puttusk

$H_s = 80\,m$ $h_w = 12\,m$

I	13	3.2	10.5	2.6	0.5	3.0	7	3.4	6.5	5.6	26	4.0	11	4.1	4.5	6.0	14	3.3	35.5	9.0	31	9	12	27	·	–	–	5	17	14	9	·	–	19	·
II	0.5	3.0	0.5	3.0	0.5	3.0	6.5	6.1	16	5.9	13	4.2	32	3.0	4	3.8	11	3.6	15.1	3.4	11	·	2	18	·	–	–	1	19	11	6	·	–	6	·
III	·	·	·	·	·	·	·	·	1	9.0	13	10.1	49.5	7.8	28.5	7.3	1	8.0	28.4	6.0	16	·	·	8	·	–	–	·	8	12	9	·	–	2	·
IV	6	2.5	7.5	3.9	8	6.4	14	6.9	2.5	4.0	10.5	4.5	17.5	5.2	11	5.4	13	4.4	26.3	6.6	16	·	·	5	·	–	–	9	7	8	7	·	–	1	2
V	7.5	4.7	·	·	6	3.6	5	5.1	4	5.0	18.5	4.0	21.5	4.1	21.5	4.8	9	4.0	88.1	25.4	1	·	·	·	3	–	–	·	6	15	12	2	–	·	6
VI	0.5	2.0	3	4.3	4.5	4.4	11	5.1	9	4.1	18	5.7	19	5.6	14	4.7	11	4.5	34.2	13.9	22	·	·	·	14	–	–	3	4	10	7	1	–	·	7
VII	4	3.8	0.5	1.0	0.5	2.0	3.5	9.1	6	5.7	31.5	4.8	29.5	4.7	7.5	3.5	10	4.3	61.9	15.0	28	·	·	·	5	–	–	3	1	16	10	2	–	·	5
VIII	4.5	2.8	2	3.5	0.5	5.0	1.5	4.3	4	7.9	28.5	6.4	24.5	5.1	15.5	3.8	12	4.6	58.0	30.0	10	·	·	·	4	–	–	2	9	12	7	1	–	·	4
IX	3	3.3	4.5	2.8	8	3.6	8	4.4	2.5	4.1	16.5	5.9	20.5	4.7	10	5.6	17	3.9	20.8	7.8	14	·	·	·	5	–	–	11	4	7	4	·	–	·	1
X	1	4.0	5	3.6	16.5	6.6	29	6.4	13.5	4.9	6.5	5.0	7.5	4.6	7	4.4	7	5.2	5.6	2.5	29	·	·	·	·	–	–	7	7	5	3	·	–	·	·
XI	7	6.1	6	8.1	5	8.0	11.5	6.5	8.5	4.5	18.5	5.5	21.5	5.5	4	5.0	8	5.4	46.3	10.0	4	·	1	11	·	–	–	1	20	17	10	1	–	·	·
XII	8.5	8.6	6.5	7.9	2	4.0	14	4.5	4.5	5.1	21	5.3	23	7.6	7.5	8.5	6	6.1	25.5	5.6	1	9	14	26	·	–	–	5	14	13	6	·	–	19	·
Rok	55.5	3.7	46	3.4	52	4.1	111	5.2	78	5.5	221.5	5.4	277	5.2	135	5.2	119	4.8	445.7	30.0	10.VIII	18	29	95	31	–	–	47	116	140	90	7	–	47	25

Białowieża

$H_s = 163\,m$ $H_b = 163{,}7\,m$ $h_w = 18{,}7\,m$

I	9.5	3.6	4	4.9	5.5	1.6	13	1.9	15	2.3	19	4.0	8.5	2.4	12.5	3.1	6	2.8	32.5	9.5	31	13	13	30	·	2	·	3	19	17	9	·	6	25	·
II	3	1.5	1.5	1.7	4.5	2.3	11.5	2.3	12	3.6	17	2.8	11.5	3.2	11	3.0	12	2.4	19.0	6.7	28	·	4	22	·	·	·	1	19	12	3	·	14	16	·
III	0.5	5.0	0.5	5.0	·	·	0.5	6.0	5	4.1	22.5	5.2	35.5	6.0	27.5	21	1	6.0	44.8	13.1	30	·	·	16	·	10	3	1	15	19	9	1	5	1	·
IV	6	2.0	3.5	3.0	16	3.4	18.5	4.1	7.5	2.6	9	3.9	5.5	4.4	10	5.0	14	3.1	31.8	17.1	16	·	·	9	·	2	1	11	5	8	7	1	2	1	1
V	6	3.0	2.5	2.0	7.5	2.9	10.5	2.3	7.5	3.1	15.5	2.4	11	2.9	16.5	3.5	16	2.4	77.9	13.8	1	·	·	·	2	·	·	3	11	17	13	1	3	·	6
VI	3	1.7	3	2.2	9.5	3.2	10	2.6	12	2.4	16	3.3	15	3.3	13.5	2.8	8	2.6	60.1	14.8	28	·	·	·	11	·	·	4	6	12	12	1	2	·	9
VII	2	1.7	4	2.1	2	2.2	3.5	2.9	8.5	4.0	30.5	3.3	25	3.4	7.5	3.1	10	2.9	56.9	22.5	30	·	·	·	4	·	·	3	10	12	5	5	3	·	8
VIII	6	2.3	0.5	4.0	1.5	1.0	2.5	1.0	11	3.1	27	4.1	19.5	4.2	18	3.9	7	3.4	94.7	35.2	10	·	·	·	6	2	1	2	11	17	10	3	3	·	6
IX	5	1.8	6	1.9	9.5	2.6	11	1.7	4.5	2.3	13	4.1	13.5	5.3	11.5	3.4	16	2.6	32.5	11.7	6	·	·	3	5	1	1	11	6	7	5	2	11	·	2
X	·	·	2	1.8	12	4.5	35.5	5.2	15.5	2.9	2	3.8	4.5	3.3	8.5	3.3	13	3.6	2.9	2.0	29	·	·	1	·	5	·	7	8	2	1	·	10	·	·
XI	5.5	2.1	3	2.7	11.5	4.5	23.5	4.7	7.5	2.0	13.5	3.5	11.5	4.2	8	3.1	6	3.5	49.5	11.8	12	·	4	15	·	3	·	·	23	18	9	1	7	2	·
XII	11.5	4.4	3.5	6.0	6.5	3.5	13	2.2	9	2.2	17.5	4.7	13	4.3	15	4.2	4	3.7	27.4	6.0	1	11	16	28	·	2	1	2	15	19	9	·	5	21	·
Rok	58	2.4	34	3.1	86	2.6	153	3.1	115	2.9	202.5	3.8	174	3.9	159.5	3.8	113	3.2	530.0	35.2	10.VIII	24	37	124	28	27	7	48	148	160	92	13	71	66	32

Łagiewniki

$H_s = 80\,m$ $h_w = 10\,m$

I	2	4.0	11.5	2.1	6	1.9	12.5	1.8	10	1.3	15	1.7	8.5	2.1	8.5	1.8	19	1.5	17.2	7.0	31	8	11	23	·	·	·	–	–	6	5	·	–	–	·
II	5.5	1.7	3	2.3	2.5	2.8	11.5	1.5	7	2.0	11	2.1	16	2.1	11.5	2.6	16	1.7	30.7	9.2	9	·	·	16	·	·	·	–	–	7	7	·	–	–	·
III	2.5	4.0	·	·	·	·	·	·	0.5	2.0	26.5	3.2	57.5	3.1	4	5.4	2	3.2	27.4	9.6	30	·	·	5	·	·	·	–	–	11	11	·	11	–	·
IV	12	1.5	12.5	2.2	11.5	2.0	17	2.3	1	1.0	7	2.0	5	1.4	9	2.3	15	1.6	41.3	12.8	16	·	·	4	·	·	·	–	–	10	10	1	2	·	2
V	17	1.9	7.5	2.1	3	2.0	1	1.0	3	1.0	12	2.8	16	1.8	14.5	1.8	19	1.6	52.7	15.3	6	·	·	·	·	1	·	–	–	13	9	1	3	·	2
VI	2	2.0	4	1.8	6	1.5	2.5	2.2	2	1.2	4	2.4	24	2.1	13.5	2.7	32	1.4	22.1	7.0	13	·	·	·	11	·	·	–	–	7	4	·	·	·	7
VII	3	2.7	·	·	2.5	1.0	5.5	1.4	2	1.5	9	2.4	39	2.1	11	2.3	21	1.6	176.6	66.2	31	·	·	·	5	·	·	–	–	18	17	4	2	·	5
VIII	2	2.5	·	·	0.5	2.0	0.5	2.0	4.5	2.0	33.5	2.2	11.5	2.6	12.5	2.4	28	1.6	112.9	16.0	11	·	·	·	5	·	·	–	–	17	14	5	·	·	4
IX	3	2.0	·	·	12	1.3	7	1.6	1	2.5	10	1.6	19	2.3	3	2.7	35	1.1	27.0	14.7	14	·	·	·	6	·	·	–	–	6	3	1	·	·	1
X	·	·	2.5	2.2	19.5	2.0	9.5	2.0	6.5	1.2	9	1.6	15	1.6	9	2.1	22	1.4	32.6	13.2	29	·	·	·	·	·	·	–	–	6	4	2	4	·	·
XI	8	2.6	2.5	2.2	10	2.6	1.5	2.3	1	1.0	30	1.9	12	1.9	3	1.3	22	1.5	36.6	9.5	13	·	·	9	·	·	·	–	–	8	7	·	–	–	·
XII	9	2.7	6.5	1.7	5.5	1.6	11.5	1.1	12.5	1.6	23	2.1	12.5	2.6	7.5	2.2	5	1.9	30.3	9.4	11	9	14	24	·	·	·	–	–	7	6	·	9	–	·
Rok	66	2.3	50	1.4	79	1.7	80	1.6	51	1.5	190	2.2	236	2.1	107	2.5	236	1.7	607.4	66.2	31.VII	17	25	81	27	1	·	–	–	116	97	14	–	–	21

Wieniec – Zdrój

$\varphi = 52°40'$ $\lambda = 19°00'$

MIESIĄC	CIŚNIENIE P				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.1	–6.1	5.7	4	–20.3	26	–4.1	–0.6	–3.5	–3.0	4.4	4.7	4.5	4.5	88	76	86	83	0.5	1.3	0.6	0.8	7.3	6.3	5.1	6.2
II	–	–	–	–	4.3	0.3	9.9	28	–3.5	22	1.1	3.9	1.5	2.0	6.3	6.9	6.2	6.2	94	89	94	92	0.4	0.9	0.5	0.6	8.5	7.6	6.5	7.5
III	–	–	–	–	9.1	1.9	16.6	10	–4.8	20	3.9	8.1	4.8	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	5.3	6.8
IV	–	–	–	–	14.8	4.0	24.7	7	–3.6	10	7.2	13.7	8.8	9.6	8.6	9.2	9.2	9.0	82	58	79	73	2.0	7.5	2.6	4.0	4.0	4.5	4.3	4.3
V	–	–	–	–	16.5	6.5	22.7	27	0.4	13	9.6	15.4	10.5	11.5	10.2	10.9	10.9	10.7	85	63	85	78	1.9	7.0	2.1	3.7	6.9	6.9	6.7	6.8
VI	–	–	–	–	23.9	12.2	32.7	27	5.0	1 , 21	16.6	22.8	17.0	18.4	14.7	14.2	14.9	14.6	78	53	77	69	4.4	14.2	4.6	7.7	4.6	5.1	4.5	4.7
VII	–	–	–	–	21.0	10.9	33.7	3	7.3	30	15.1	19.5	14.8	16.0	14.6	15.4	14.3	14.8	85	70	86	80	2.8	8.3	2.8	4.6	6.7	7.8	6.5	7.0
VIII	–	–	–	–	20.5	11.5	30.3	6	6.7	14	14.4	19.2	14.7	15.8	15.3	16.3	15.5	15.7	93	73	92	86	1.3	6.5	1.6	3.1	7.1	6.1	5.2	6.1
IX	–	–	–	–	20.2	8.6	28.8	2	0.1	24	11.5	19.5	12.4	14.0	12.6	14.1	13.5	13.4	91	62	91	81	1.3	8.9	1.4	3.9	3.8	4.3	3.8	4.0
X	–	–	–	–	15.0	6.5	19.7	6	2.0	13,14	8.3	14.2	10.2	10.7	10.1	12.0	10.9	11.0	91	75	88	85	1.0	4.5	1.6	2.4	6.8	7.2	5.8	6.6
XI	–	–	–	–	5.9	1.4	11.6	3, 7	–7.6	23	2.7	5.1	3.2	3.6	7.3	8.2	7.5	7.7	94	91	94	93	0.4	0.8	0.5	0.6	8.4	8.6	7.7	8.2
XII	–	–	–	–	–1.0	–6.8	15.7	5	–23.0	27	–4.0	–1.7	–4.0	–3.4	4.5	4.8	4.5	4.6	88	82	88	86	0.6	1.1	0.8	0.8	7.7	7.1	5.5	6.8
Rok	–	–	–	–	12.5	4.2	33.7	3.VII	–23.0	27.XII	6.9	11.6	7.5	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.6	6.3

Nur

$\varphi = 52°40'$ $\lambda = 22°19'$

I	–	–	–	–	–1.0	–7.3	7.3	4	–25.0	26	–5.3	–2.2	–4.2	–4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	7.3	7.3
II	–	–	–	–	3.1	–1.5	10.4	18	–8.1	5	–0.2	2.3	0.7	0.9	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.4	7.9	8.6
III	–	–	–	–	8.6	1.0	16.5	10	–3.3	23	2.7	6.9	4.1	4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.4	5.5	6.6
IV	–	–	–	–	15.1	3.5	24.7	15	–3.1	11	6.1	13.5	8.2	9.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.5	3.8	4.2
V	–	–	–	–	17.4	6.9	26.2	28	1.8	15	10.1	15.9	11.0	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	6.0	6.7
VI	–	–	–	–	24.2	12.1	32.6	27	5.3	21	16.4	22.4	17.0	18.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.4	5.9	5.6
VII	–	–	–	–	21.7	11.1	31.6	3	7.1	6	14.8	19.7	15.2	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.4	7.1	6.8
VIII	–	–	–	–	21.3	11.8	30.1	6	8.3	31	14.0	20.0	15.4	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	6.5	6.5
IX	–	–	–	–	20.2	8.0	28.4	3	–0.3	23	10.0	18.5	12.0	13.1	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.0	3.6	4.2
X	–	–	–	–	15.2	5.2	20.0	4, 5	1.4	23	6.5	14.4	9.4	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.5	4.6	5.2
XI	–	–	–	–	5.3	0.7	12.8	3	–7.3	23	2.4	4.3	2.7	3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.9	8.0	8.5
XII	–	–	–	–	–1.2	–7.8	14.2	5	–22.9	26,27	–4.5	–2.6	–4.5	–4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.0	6.7	7.4
Rok	–	–	–	–	12.5	3.6	32.6	27.VI	–25.0	26.1	6.1	11.1	7.2	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.6	6.1	6.5

Posiwietne

$\varphi = 52°38'$ $\lambda = 20°23'$

I	–	–	–	–	–0.5	–6.4	5.6	4	–22.3	26	–4.4	–1.5	–3.2	–3.1	4.3	4.8	4.5	4.5	88	83	86	86	0.5	0.9	0.6	0.7	7.5	7.3	6.0	6.9
II	–	–	–	–	3.3	–0.5	9.8	18	–3.9	5	0.5	2.5	1.3	1.4	6.0	6.4	6.2	6.2	94	86	92	91	0.4	1.1	0.6	0.7	8.4	8.0	7.6	8.0
III	–	–	–	–	8.9	1.7	16.3	10	–3.0	20	3.4	7.3	4.7	5.0	6.7	7.1	7.2	7.0	85	69	85	80	1.2	3.4	1.5	2.0	7.5	7.6	5.2	6.8
IV	–	–	–	–	14.9	3.7	23.5	7	–2.9	10	6.6	13.3	8.8	9.4	7.8	8.3	8.6	8.2	77	54	73	68	2.3	7.8	3.1	4.4	4.5	5.0	2.9	4.1
V	–	–	–	–	16.7	6.6	24.7	27	0.6	17	10.0	14.9	10.9	11.7	10.4	10.4	10.7	10.5	83	62	81	75	2.1	7.1	2.7	4.0	6.5	7.1	6.0	6.5
VI	–	–	–	–	23.8	12.3	31.7	27	4.6	21	16.5	22.1	16.8	18.0	15.0	14.0	15.1	14.7	79	53	79	70	4.0	13.2	4.3	7.2	4.2	5.2	4.4	4.6
VII	–	–	–	–	21.1	11.0	31.6	3	7.5	6	14.5	19.5	15.1	16.0	14.0	13.5	14.1	13.9	84	62	82	76	2.7	9.7	3.4	5.3	6.7	7.3	5.7	6.6
VIII	–	–	–	–	20.4	11.8	30.2	6	7.2	31	14.3	19.1	15.2	16.0	14.6	15.1	15.1	14.9	89	69	86	81	1.9	7.4	2.5	4.0	6.6	6.8	5.5	6.3
IX	–	–	–	–	19.8	8.5	28.1	2	–0.1	28	10.5	18.9	12.5	13.6	11.8	13.1	12.8	12.6	90	59	86	78	1.5	9.4	2.1	4.3	4.5	4.0	3.0	3.8
X	–	–	–	–	14.8	5.7	19.7	4	1.6	31	7.3	13.9	9.8	10.2	9.2	10.8	9.8	9.9	90	69	81	80	1.1	5.3	2.4	2.9	5.4	5.5	3.4	4.8
XI	–	–	–	–	5.6	0.9	12.1	3	–8.6	23	2.4	4.7	3.1	3.3	7.0	7.4	7.3	7.2	93	85	92	90	0.5	1.3	0.6	0.8	8.4	8.3	7.5	8.1
XII	–	–	–	–	–1.1	–7.3	14.7	5	–24.2	27	–4.5	–3.0	–4.1	–3.9	4.6	4.8	4.5	4.6	91	87	90	89	0.5	0.8	0.5	0.6	7.9	7.0	5.5	6.8
Rok	–	–	–	–	12.3	4.0	31.7	27.VI	–24.2	27.XII	6.4	11.0	7.6	8.2	9.3	9.6	9.7	9.5	87	70	84	80	1.6	5.6	2.0	3.1	6.5	6.6	5.2	6.1

Szamotuły

$\varphi = 52°37'$ $\lambda = 16°34'$

I	–	–	–	–	0.5	–5.0	6.3	29, 30, 31	–16.0	26	–4.0	–0.3	–2.6	–2.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.6	6.2	6.0
II	–	–	–	–	5.9	0.4	12.4	28	–3.6	5	1.5	4.7	2.5	2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.4	6.7	7.6
III	–	–	–	–	10.1	2.6	18.7	10	–5.0	20	4.1	8.6	5.5	5.9	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.5	5.5	6.7
IV	–	–	–	–	15.7	5.0	25.5	7	–1.0	10	7.0	14.1	9.9	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.7	4.1	5.1
V	–	–	–	–	15.9	7.0	22.1	26	2.7	12	9.7	14.2	10.7	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.5	7.1
VI	–	–	–	–	23.7	12.4	29.4	25	7.4	22	16.1	22.3	17.1	18.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.9	5.2	5.0
VII	–	–	–	–	20.8	12.3	33.6	3	7.2	6	15.0	19.0	15.6	16.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	7.1	7.0
VIII	–	–	–	–	21.0	12.1	29.8	6	7.9	8	14.2	19.4	15.4	16.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.9	5.6	6.2
IX	–	–	–	–	21.3	9.8	30.0	2	1.8	24	12.1	20.0	14.4	15.2	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.1	3.6	3.9
X	–	–	–	–	15.1	7.7	21.5	6	1.7	31	9.0	14.4	10.8	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.7	4.7	5.6
XI	–	–	–	–	6.6	1.6	12.8	3	–6.8	23	2.4	5.6	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.5	8.3	8.5
XII	–	–	–	–	0.1	–7.0	15.3	5	–22.4	27	–4.3	–1.4	–3.8	–3.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.4	6.6
Rok	–	–	–	–	13.1	4.9	33.6	3.VII	–22.4	27.XII	6.9	11.7	8.3	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.3	5.8	6.3

Wieniec - Zdrój

H_s = 82 m — h_w = 13 m I–VI, 14 m VII–XII

MIESIĄC	ROZKŁAD WIATRU (n, v) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◐	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	ℝ
I	6.5	1.4	1	3.5	4.5	1.7	11.5	1.3	15	1.2	23.5	1.5	8.5	1.6	6.5	1.5	16	1.2	19.0	7.2	31	11	12	24			·	7	12	7	5	·	3	–	–
II	2.5	1.0	·	·	1	1.0	8.5	1.4	8	1.6	9	1.8	30.5	1.3	6.5	1.3	18	1.1	34.1	8.8	9			20	·	·		·	13	12	9	·	12	--	–
III	4	2.2	·	·	·	·	·	·	·	·	1	4.0	60	2.5	20	3.0	8	2.4	42.0	9.8	30			8	·	·	·	1	12	13	10	·	5	–	–
IV	5	1.4	1	3.0	11	2.1	14	2.3	11	1.5	·	·	17	1.5	5	1.6	26	1.3	56.9	10.7	26	·		7		·	·	12	7	12	9	·	7	·	–
V	7.5	1.6	·	·	8	1.4	5.5	2.0	7.5	2.1	18	1.8	21.5	1.1	15	1.7	10	1.4	40.5	6.4	6		·	·	·	·		·	7	14	12	·	7	·	–
VI	·	·	3	1.0	10	1.4	3	1.3	7	1.4	13	1.5	39.5	1.9	6.5	1.5	8	1.5	21.9	4.7	14	·		·	11			4	4	11	6		·	·	–
VII	1	1.0	·	·	·	·	2	1.0	7	2.1	36	2.0	35.5	1.7	2.5	1.8	9	1.6	149.7	31.7	31	·	·	·	7		·	4	15	17	15	5	6	·	–
VIII	2	2.5	·		2	2.0	1	1.0	3	1.3	21	1.9	39	1.7	12	1.5	13	1.5	90.3	17.5	11			·	4	·		2	8	19	13	7	5	·	–
IX	4	1.0	4	1.2	15	1.5	3	1.7	8	1.1	15	1.7	31	1.8	3	1.0	7	1.5	40.0	16.1	14		·	·	5	·	·	13	8	8	6	2	2	·	–
X	5	1.0	·	·	7	2.7	22	2.8	30	1.5	10	1.2	7	2.0	3	2.0	9	1.7	20.3	8.6	7	·	·	·	·	·	·	5	15	7	4	·	–	·	–
XI	5	1.4	4	1.2	9	2.6	1	1.0	10	1.8	8	2.2	9	1.9	1	1.0	43	1.0	71.7	13.4	11	·	·	9	·	·	·	2	20	16	14	2	15	·	–
XII	7	1.7	1	3.0	7	1.3	4	1.5	6	1.9	7	2.1	16	1.7	6	1.7	39	1.0	28.2	8.4	1	9	17	24	·	·	·	3	12	12	7	·	3	15	–
Rok	49.5	1.4	14	1.1	74.5	1.5	75.5	1.4	112.5	1.5	161.5	1.8	314.5	1.7	87	1.6	206	1.4	614.6	31.7	31.VII	20	29	92	27	·	·	53	133	148	110	16	–	–	–

Nur

H_s = 110 m — h_w = 13 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	ℝ
I	6	3.7	3	1.0	1.5	1.0	19.5	2.6	8	2.2	14	2.0	11	1.5	5	2.4	25	1.5	45.6	10.6	5	12	12	30	·	2	·	3	16	15	10	2	1	27	·
II	1.5	1.7	3.5	1.6	4	1.0	21.5	1.5	3	4.3	8.5	2.8	10	1.6	7	2.8	25	1.4	20.7	5.5	1		2	18	·	1	·	·	20	13	5		8	10	·
III	3	6.5	·	·	·	·	1	3.0	3.5	3.6	19.5	4.3	38	3.7	21	5.1	7	3.9	36.5	19.0	30	·	·	11	·	5	1	3	12	13	9	1	3	2	·
IV	8.5	1.2	11.5	1.4	15	1.7	15	2.0	3.5	1.4	4.5	2.8	8	4.1	4	3.8	20	1.6	32.0	10.5	16			5		1	·	10	7	10	9	1	1	1	2
V	9	2.7	1	1.0	8	1.0	8	1.2	4	1.4	8	1.3	9	1.9	15	1.8	31	1.1	56.0	14.1	1	·	·	·	3	1	·	2	11	17	14	2	1	·	3
VI	2.5	3.2	2	1.5	6.5	1.8	14.5	1.2	5	1.7	10.5	2.7	13	2.2	7	2.4	29	1.3	45.0	9.5	8	·	·	·	13	·	·	2	6	12	7	·	1	·	7
VII	1.5	2.3	4	1.8	0.5	1.0	5.5	1.4	6.5	1.6	20	1.8	19	1.7	7	2.4	29	1.2	108.2	30.0	30		·	·	5			3	16	15	12	4	1	·	2
VIII	4.5	1.3	1	3.0	3	1.0	·	·	9.5	2.4	16	2.5	17.5	1.7	12.5	1.5	29	1.3	72.3	26.7	10	·		·	7	·	·	2	10	13	9	2	·	·	2
IX	5.5	2.0	5	1.9	5.5	1.1	6.5	1.6	5.5	1.1	11.5	3.2	12	1.7	8.5	2.4	30	1.4	34.2	7.8	12	·	·	1	5	1	·	13	8	11	7	·	2	·	2
X	1.5	2.6	6.5	1.2	14	2.6	25.5	3.0	8.5	1.5	5	1.5	6.5	2.0	4.5	2.9	21	1.8	4.9	3.5	29	·		·		·	·	8	9	2	2	·	7	·	
XI	6.5	2.5	4.5	3.0	13.5	2.6	12.5	1.7	5	1.2	13.5	2.6	13	2.0	2.5	1.0	19	1.7	58.6	9.3	12	·	2	14	·	·	·	1	20	15	11	·	5	·	
XII	12	6.9	2.5	4.0	4	1.4	11.5	1.3	8.5	1.4	14	4.4	10.5	1.5	12	3.5	18	2.6	28.4	7.2	1	11	14	26	·	4	3	4	18	14	7	·	·	21	·
Rok	62	3.0	44.5	1.8	75.5	1.4	141	1.7	70.5	2.0	145	2.7	167.5	2.1	106	2.7	283	1.7	542.4	30.0	30.VII	23	30	105	33	15	4	51	153	150	102	12	30	61	18

Poświętne

H_s = 101 m — h_w = 14 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	ℝ
I	9	2.6	13.5	2.8	2.5	2.0	6.5	3.4	15.5	2.6	22.5	4.1	15.5	4.1	8	4.4	·	3.4	26.6	10.0	31	11	13	27	·	1	·	4	15	14	8	1	3	10	
II	2.5	1.6	3.5	2.3	1	2.0	12	2.6	11	4.6	19	4.0	19	4.3	16	4.0	·	3.8	20.9	9.5	9	·	2	18	·	1	1	2	17	12	4	·	6	5	·
III	1	6.5		·	·	·	·	·		·	5	6.9	45	6.9	42	8.1	·	7.5	24.1	9.8	30	·	·	8		13	7	1	9	14	7	·	1	2	
IV	7	2.1	17	2.3	16	4.3	14	5.1	4	3.5	7	3.7	9.5	5.2	10.5	5.9	5	3.8	45.1	9.8	26	·	·	6	·	4	2	11	5	12	10	·	·	1	3
V	15	4.1	3.5	5.7	11	2.7	5.5	2.0	7	4.0	16	3.6	13	4.6	18	3.6	4	3.6	41.3	11.2	1	·	·	·	·	2	·	1	8	16	9	1	·	·	7
VI	6	1.8	8.5	2.6	10.5	3.5	8.5	3.8	8.5	2.7	14	4.0	16.5	5.0	16.5	3.9	1	3.6	36.0	18.2	22	·	·	·	13	3	·	4	4	12	6	1	·	·	12
VII	8.5	2.4	1.5	2.3	2.5	2.0	1.5	3.3	9	2.7	26.5	4.4	30	4.2	12.5	3.4	1	3.7	104.0	24.4	16	·	·	·	4	3	2	3	9	15	10	5	·	·	7
VIII	5.5	3.1	3.5	1.7	2.5	3.2	1	1.0	3	3.7	25	4.0	28	4.4	23.5	3.4	1	3.7	77.0	35.9	10	·	·	·	3	·	·	·	10	16	13	1	·	·	8
IX	2.5	1.6	8.5	1.7	17	2.4	7.5	3.0	0.5	4.0	13	3.8	23.5	4.2	14.5	4.4	3	3.3	21.1	10.0	14	·		1	5	2	·	12	6	5	3	1	–	·	2
X	0.5	1.0	5.5	3.1	20.5	4.1	24	4.4	15.5	3.6	8	4.1	7	3.6	9	3.4	3	3.9	12.4	3.6	18	·	·	·	·	3	·	9	7	8	6	·	–	·	·
XI	12	3.1	7	5.2	16	5.1	9.5	2.5	5.5	3.1	10.5	3.5	22.5	5.3	5	3.9	2	4.1	55.9	8.5	5	·	1	11	·	6	·	2	18	18	13	·	8	·	·
XII	9	7.4	11	4.2	6.5	3.3	7.5	2.7	7	2.2	17	6.0	22	4.7	11	4.5	2	4.6	24.9	7.1	1	10	14	24	·	6	1	4	14	14	5	·	3	16	
Rok	78.5	3.1	83	2.8	106	2.9	97.5	2.8	86.5	3.1	183.5	4.3	251.5	4.7	186.5	4.4	22	4.1	489.3	35.9	10.VIII	21	30	95	25	44	13	53	122	156	94	10	–	34	39

Szamotuły

H_s = 70 m — h_w = 17,5 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	ℝ
I	7	1.6	10	1.9	14	2.0	14	1.7	16	1.8	14	2.5	6	1.7	5	1.4	7	1.7	31.1	6.4	30	9	12	22	·	·	·	5	11	11	10	·	–	19	·
II	6	1.5	7	1.7	9	2.1	11	2.2	8	2.4	17	2.0	9	2.2	13	1.9	4	1.9	37.1	15.7	9	·	·	12	·	·	·	1	14	12	9	1	–	1	·
III	1	1.0	1	2.0	·	·	·	·	·	·	8	2.4	57	3.5	25	3.2	1	3.3	52.6	14.6	30	·	·	4	·	5	2	1	10	16	15	1	–	·	
IV	13	1.6	7	1.9	25	2.8	9	2.6	5	3.0	6	1.8	10	2.2	12	1.8	3	2.2	98.2	32.6	26	·	·	3	1	·	·	6	5	13	11	2	–	·	4
V	26	1.8	12	1.4	4	1.8	3	2.7	4	1.8	10	2.8	9	2.7	22	2.3	3	2.0	87.4	20.4	5	·	·	·	·	·	·	·	8	19	16	2	–	·	6
VI	13	1.4	10	1.6	7	2.1	2	2.0	5	2.2	8	2.9	12	3.2	25	2.4	8	2.1	31.8	10.2	7	·	·	·	11	·	·	5	3	7	6	1	–	·	7
VII	1	1.0	1	2.0	1	2.0	2	2.5	3	2.0	15	2.8	43	2.7	23	2.0	4	2.3	167.1	57.0	31	·	·	·	5		·	2	10	19	16	5	–	·	3
VIII	8	1.4	2	1.5	4	1.5	3	2.0	·	·	17	2.6	30	2.7	22	1.7	7	2.0	63.6	8.6	10	·	·	·	4	·	·	2	6	15	11	·	–	·	2
IX	7	1.3	6	1.3	15	2.1	5	1.8	1	1.0	10	2.3	24	2.4	9	1.7	13	1.7	40.4	22.2	5	·	·	·	6	·	·	11	2	5	3	2	–	·	2
X	4	1.2	4	2.0	23	3.0	11	2.0	6	1.8	15	2.5	3	1.3	13	1.9	14	2.0	20.7	4.2	20, 31	·	·	·	·	·	·	5	8	8	7	·	–	·	·
XI	4	2.2	9	2.3	9.5	2.9	1.5	2.0	10	1.5	17	2.2	20	2.4	15	1.5	4	2.0	44.1	17.6	13		·	8	·	·	·	1	21	11	7	1	–		·
XII	4	1.5	13	1.8	3	2.3	6	1.5	11	1.4	10	1.9	25	2.7	14	1.8	7	1.8	47.5	11.2	1	11	16	24	·	·	·	2	13	14	9	1	–	20	·
Rok	94	1.5	82	1.8	114.5	2.0	67.5	1.9	69	1.6	147	2.4	248	2.5	198	2.0	75	2.1	721.6	57.0	31.VII	20	28	73	27	5	2	41	111	150	120	16	–	40	24

Przebędowo

$\varphi = 52°35'$ $\lambda = 17°01'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.3	−5.3	5.4	4	−17.3	27	−4.1	−0.6	−2.8	−2.6	4.4	4.9	4.6	4.6	87	79	85	84	0.5	1.1	0.6	0.7	6.5	5.2	5.9	5.9
II	–	–	–	–	5.3	−0.2	11.4	18	−4.4	5	1.4	4.1	2.3	2.5	6.5	7.2	6.7	6.8	95	87	93	92	0.3	1.1	0.6	0.7	8.6	7.7	7.7	8.0
III	–	–	–	–	9.6	2.3	17.5	10	−6.5	20	3.9	8.1	5.2	5.6	7.1	7.1	7.4	7.2	88	67	83	79	1.1	4.0	1.6	2.2	6.9	6.1	6.1	6.4
IV	–	–	–	–	15.1	4.4	25.2	7	−1.5	10	7.1	13.6	9.4	9.9	8.4	8.8	9.2	8.8	81	57	76	71	2.0	7.7	3.0	4.2	4.8	4.4	4.1	4.4
V	–	–	–	–	15.4	6.3	21.5	26	1.1	13	9.8	13.7	10.4	11.1	10.5	10.6	10.3	10.5	86	68	83	79	1.9	5.5	2.2	3.2	7.5	8.1	5.4	7.0
VI	–	–	–	–	23.0	11.9	28.0	25, 26	6.1	22	16.3	21.2	16.6	17.7	15.1	14.3	15.5	15.0	81	57	82	73	3.7	11.5	3.7	6.3	4.8	4.8	3.4	4.3
VII	–	–	–	–	20.3	11.9	32.8	3	7.4	6	14.5	18.5	15.6	16.0	14.4	14.6	14.6	14.5	87	70	83	80	2.3	7.6	3.6	4.5	7.5	7.4	7.4	7.4
VIII	–	–	–	–	20.4	11.7	29.0	6	7.5	4	13.9	18.6	15.4	15.8	14.8	14.4	15.3	14.8	93	68	87	83	1.2	7.6	2.3	3.7	7.9	7.8	7.1	7.6
IX	–	–	–	–	20.6	9.9	29.0	2	3.5	24	12.0	19.6	14.0	14.9	12.6	12.7	13.3	12.9	88	56	82	75	1.7	10.8	3.0	5.2	4.5	3.8	4.3	4.2
X	–	–	–	–	14.7	7.4	21.4	6	1.5	13	8.6	13.9	10.3	10.8	10.2	10.9	10.5	10.5	91	70	84	82	1.1	5.2	2.1	2.8	6.4	5.1	4.7	5.4
XI	–	–	–	–	6.1	1.5	12.0	2	−7.0	23	2.7	5.4	3.2	3.6	7.3	7.8	7.5	7.5	95	86	94	92	0.4	1.3	0.5	0.7	8.4	8.3	7.1	7.9
XII	–	–	–	–	−0.1	−7.7	14.9	5	−26.4	27	−4.2	−1.9	−3.8	−3.4	4.7	5.0	4.5	4.7	90	84	85	86	0.5	1.0	0.8	0.8	7.3	6.8	6.3	6.8
Rok	–	–	–	–	12.6	4.5	32.8	3.VII	−26.4	27.XII	6.8	11.2	8.0	8.5	9.7	9.9	10.0	9.9	88	71	85	81	1.4	5.4	2.0	2.9	6.8	6.3	5.8	6.3

Wyszków

$\varphi = 52°35'$ $\lambda = 21°27'$

I	–	–	–	–	−0.5	−6.6	6.8	4	−23.0	26	−5.0	−1.6	−3.7	−3.5	4.3	4.9	4.6	4.6	90	84	90	88	0.3	0.8	0.4	0.5	7.1	7.3	6.3	6.9
II	–	–	–	–	3.4	−1.3	11.6	18	−9.2	6	0.2	2.6	0.5	1.0	6.1	6.4	6.1	6.2	96	86	95	92	0.2	1.1	0.4	0.6	9.3	8.3	7.6	8.4
III	–	–	–	–	9.5	0.5	17.0	10	−3.2	23	2.8	7.5	4.1	4.6	6.8	7.0	7.0	6.9	87	68	85	80	0.8	3.7	1.3	1.9	8.0	7.6	5.9	7.2
IV	–	–	–	–	15.4	3.1	24.5	7	−4.7	10	6.6	13.9	8.4	9.3	7.8	8.2	8.6	8.2	79	52	76	69	2.2	8.7	2.9	4.6	4.6	5.2	3.3	4.4
V	–	–	–	–	17.4	6.7	26.4	28	1.0	15	10.8	15.9	10.7	12.0	11.0	10.8	11.6	11.1	84	60	87	77	2.3	7.9	1.8	4.0	6.9	7.0	6.6	6.8
VI	–	–	–	–	24.3	11.8	34.6	27	6.1	21	16.8	22.7	16.2	18.0	15.5	14.7	15.3	15.2	81	54	82	72	3.8	13.6	3.5	7.0	5.1	5.8	5.6	5.5
VII	–	–	–	–	21.9	10.6	32.6	3	6.7	6	14.8	20.3	15.1	16.3	14.4	14.2	15.0	14.5	85	61	87	77	2.6	10.3	2.5	5.1	7.1	7.6	7.5	7.4
VIII	–	–	–	–	21.3	11.0	30.9	6	6.4	18	14.7	20.2	14.9	16.2	14.9	15.0	14.8	14.9	88	64	87	80	2.1	9.3	2.4	4.5	7.0	7.5	5.9	6.8
IX	–	–	–	–	20.4	8.1	29.7	2	1.2	25, 28	11.0	19.4	12.1	13.7	12.3	13.1	13.0	12.8	92	58	89	80	1.1	10.2	1.6	4.3	4.0	3.4	2.9	3.4
X	–	–	–	–	15.2	5.2	21.8	9	1.1	31	6.8	14.4	9.8	10.2	8.9	10.3	9.8	9.7	89	63	81	78	1.1	6.5	2.6	3.4	5.9	5.3	3.9	5.0
XI	–	–	–	–	5.9	0.3	13.0	3	−7.6	23, 24	2.4	4.9	2.8	3.2	7.1	7.6	7.2	7.3	94	86	93	91	0.4	1.4	0.5	0.8	8.4	7.9	7.3	7.9
XII	–	–	–	–	−0.6	−8.1	15.3	5	−25.3	26	−4.7	−2.5	−4.6	−4.1	4.4	4.8	4.5	4.6	86	80	88	85	0.6	1.0	0.4	0.7	8.4	6.7	5.7	6.9
Rok	–	–	–	–	12.8	3.4	34.6	27.VI	−25.3	26.XII	6.4	11.5	7.2	8.1	9.5	9.8	9.8	9.7	88	68	87	81	1.5	6.2	1.7	3.1	6.8	6.6	5.7	6.4

Gorzyń

$\varphi = 52°34'$ $\lambda = 15°54'$

I	–	–	–	–	0.3	−5.6	7.2	29	−18.6	26	−4.0	−0.6	−2.7	−2.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.8	5.7	6.0
II	–	–	–	–	6.5	0.6	13.1	15, 28	−4.1	6	2.0	5.1	3.0	3.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.7	7.0	7.6
III	–	–	–	–	10.1	2.9	19.4	10	−5.1	20	4.4	8.5	5.9	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.7	6.3	6.9
IV	–	–	–	–	15.5	5.1	25.4	7	−0.8	1, 10	7.5	14.1	9.6	10.2	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.2	4.2	4.7
V	–	–	–	–	15.7	6.8	22.2	26	3.0	18	9.9	13.8	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.8	6.7	7.3
VI	–	–	–	–	23.2	12.4	29.9	26	8.0	22	16.2	21.5	17.1	18.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.0	4.7	4.8
VII	–	–	–	–	20.6	12.6	33.8	3	8.4	6	15.0	19.0	15.4	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	7.2	7.4
VIII	–	–	–	–	20.5	12.5	29.4	6	8.0	8	14.4	19.0	15.7	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	5.1	6.2
IX	–	–	–	–	21.0	10.4	30.4	3	1.6	27	12.4	20.1	14.3	15.3	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.1	3.6	3.8
X	–	–	–	–	15.5	7.6	21.6	6	1.8	31	9.1	14.7	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.1	5.2	5.3
XI	–	–	–	–	6.5	1.5	13.2	2	−6.1	21, 22	2.9	5.7	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	7.3	7.6
XII	–	–	–	–	0.6	−6.2	16.1	5	−20.8	26	−3.1	−1.0	−3.2	−2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	6.0	6.5
Rok	–	–	–	–	13.0	5.0	33.8	3.VII	−20.8	26.XII	7.2	11.7	8.4	8.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	5.8	6.2

Trzemeszno

$\varphi = 52°34'$ $\lambda = 17°49'$

I	–	–	–	–	0.4	−4.8	5.8	4	−15.7	27	−3.9	−0.6	−2.6	−2.4	4.5	5.0	4.7	4.7	87	80	87	85	0.5	1.0	0.6	0.7	6.8	6.5	6.6	6.6
II	–	–	–	–	5.0	0.1	11.8	18	−3.6	6	1.2	3.9	2.2	2.4	6.4	7.0	6.6	6.7	95	87	92	91	0.4	1.1	0.6	0.7	8.7	8.5	6.2	7.8
III	–	–	–	–	9.5	2.3	17.4	10	−5.1	20	3.9	8.2	5.0	5.5	7.3	7.4	7.4	7.4	90	69	84	81	0.9	3.7	1.5	2.0	8.2	7.9	6.1	7.4
IV	–	–	–	–	15.4	5.1	24.8	7	−0.8	1	7.3	14.0	9.4	10.0	8.7	9.1	9.3	9.0	83	57	77	72	1.8	7.8	2.9	4.2	5.5	6.3	4.1	5.3
V	–	–	–	–	16.3	7.1	22.1	26	1.9	13	10.6	14.6	10.6	11.6	10.7	11.0	11.0	10.9	84	67	85	79	2.2	6.0	2.0	3.4	8.0	8.9	7.0	8.0
VI	–	–	–	–	24.2	13.0	31.2	27	7.1	22	17.6	22.9	16.9	18.6	14.9	14.7	15.7	15.1	74	54	81	70	5.5	13.9	3.8	7.7	6.0	7.1	6.4	6.5
VII	–	–	–	–	21.2	12.3	33.8	3	7.7	6	15.7	19.6	15.1	16.4	14.4	14.4	14.5	14.4	81	65	85	77	3.8	9.5	2.9	5.4	8.4	8.5	8.1	8.3
VIII	–	–	–	–	21.0	12.2	29.9	6	9.4	4	14.9	19.4	15.0	16.1	15.2	15.8	15.4	15.5	89	71	89	83	1.9	7.3	1.9	3.7	7.8	8.2	5.5	7.2
IX	–	–	–	–	20.7	10.4	29.8	2	4.8	27	12.3	19.8	13.8	14.9	13.0	14.0	13.7	13.6	89	60	85	78	1.8	9.7	2.4	4.6	4.7	5.1	4.1	4.6
X	–	–	–	–	14.8	7.5	20.3	6	2.3	31	8.6	14.0	10.4	10.8	10.3	11.5	11.1	11.0	91	73	88	84	1.0	4.7	1.5	2.4	7.1	6.8	5.2	6.4
XI	–	–	–	–	6.2	2.0	11.8	2	−5.1	23	2.9	5.4	3.4	3.8	7.3	8.0	7.6	7.6	95	88	94	92	0.4	1.1	0.5	0.7	9.1	8.8	8.3	8.7
XII	–	–	–	–	−0.3	−6.7	15.3	5	−20.1	27	−3.7	−1.7	−3.8	−3.2	4.8	5.2	4.6	4.9	88	87	87	87	0.5	0.8	0.6	0.6	7.6	7.6	6.7	7.3
Rok	–	–	–	–	12.9	5.0	33.8	3.VII	−20.1	27.XII	7.3	11.6	8.0	8.7	9.8	10.3	10.1	10.1	87	72	86	82	1.7	5.6	1.8	3.0	7.3	7.5	6.2	7.0

Przebędowo $H_s = 82\ m$ $h_w = 11\ m$ 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	OPAD R Max	OPAD R Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v > 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	=	⊞	R
I	2	3.5	6	2.3	10	2.0	20.5	2.4	27.5	3.9	12	3.3	8	3.6	·	·	7	2.9	25.3	6.8	31	9	11	22	·	·	·	8	12	14	7	·	6	5	·
II	1.5	4.0	4	3.4	6.5	2.2	9	3.7	20.5	4.3	11	3.9	12	4.9	6.5	3.1	13	3.3	24.5	10.6	9	·	·	15	·	1	·	·	17	11	7	1	8	·	·
III	1	5.0	·	·	·	·	·	·	5	3.8	32	6.2	45	5.5	7	4.0	3	5.4	28.3	11.1	30	·	·	5	·	5	1	1	8	15	8	1	5	·	·
IV	7	3.1	11	2.7	18	3.5	8	2.9	8	4.1	17.5	2.9	1.5	5.0	8	4.0	11	2.9	31.1	12.0	15	·	·	5	1	·	·	9	6	9	7	1	2	·	4
V	9.5	3.6	4.5	3.3	4	1.2	5	2.2	11.5	2.7	20	3.8	10.5	2.9	21	3.9	7	3.1	77.9	14.5	5	·	·	·	·	1	·	·	10	18	12	2	·	·	3
VI	3	2.7	1.5	1.0	9.5	2.3	10	3.0	8	2.2	22	3.6	17	4.7	4	2.2	15	2.8	76.0	26.3	7	·	·	·	10	·	·	6	4	7	5	3	1	·	5
VII	7.5	2.5	1.5	1.0	2	2.0	6	3.8	11.5	2.4	38	4.0	17.5	3.9	7	4.6	2	3.5	170.3	48.3	31	·	·	·	5	·	·	1	15	18	16	4	1	·	5
VIII	2	2.5	4	2.0	1	3.0	3.5	2.9	12.5	3.2	34	4.4	17.5	4.3	9.5	3.6	9	3.5	76.5	32.1	10	·	·	·	4	·	·	·	17	14	13	1	4	·	3
IX	4	1.1	3	2.2	13.5	2.4	4.5	2.3	14	2.6	25.5	3.6	8	3.8	4.5	2.9	13	2.5	22.8	15.4	14	·	·	·	6	·	·	11	7	2	2	1	·	·	1
X	2.5	2.6	4.5	2.3	13.5	2.6	22.5	3.9	20.5	3.2	12.5	2.5	6.5	4.3	5.5	3.6	5	3.1	19.6	4.2	29	·	·	·	·	1	·	9	11	9	6	·	7	·	·
XI	9.5	3.8	9	4.2	9	2.6	6.5	2.4	12	3.7	20.5	4.4	10	3.9	2.5	2.8	11	3.3	27.6	10.2	13	·	·	8	·	·	·	2	20	12	6	1	7	·	·
XII	2.5	2.8	12.5	1.9	3	2.0	10.5	2.8	15	4.5	18	4.8	9.5	4.9	8	4.6	14	3.3	37.3	20.8	11	13	15	24	·	1	·	3	15	9	5	1	10	16	·
Rok	52	3.1	61.5	2.2	90	2.2	106	2.7	166	3.4	263	4.0	163	4.3	83.5	3.3	110	3.3	617.2	48.3	31.VII	22	26	79	26	9	1	50	142	138	94	16	51	21	21

Wyszków $H_s = 96\ m$ $h_w = 13\ m$

I	5.5	3.5	8.5	1.8	1	1.0	13	2.2	18.5	1.7	9.5	2.2	11	3.6	12	2.9	14	2.1	30.0	9.5	31	12	13	27	·	·	·	5	15	17	8	·	1	20	·
II	·	·	2	1.0	4	1.8	17	2.4	10	2.0	18	1.9	7	2.7	5	1.8	21	1.6	13.9	2.0	1, 11	·	1	18	·	·	·	1	20	15	8	·	—	3	·
III	1	5.0	·	·	·	·	1	5.0	6.5	4.2	36	4.5	27	6.2	14.5	5.9	7	4.9	25.8	9.2	30	·	·	12	·	5	2	3	15	10	7	·	2	·	1
IV	3.5	2.1	7.5	2.9	13.5	2.5	16.5	4.9	7	1.4	5	5.0	5	4.8	10	3.0	22	2.6	33.6	12.0	16	·	·	6	·	1	·	12	7	10	9	1	·	·	3
V	4	3.2	1	3.0	7	1.9	12.5	1.9	4	1.8	11	2.5	5.5	3.3	17	3.6	31	1.8	65.2	10.6	1	·	·	·	2	·	·	·	10	16	16	1	·	·	5
VI	·	·	3.5	1.0	15	1.4	5.5	2.2	4	2.0	13.5	2.8	13	3.2	9.5	3.0	26	1.7	48.0	19.2	27	·	·	·	14	·	·	4	8	13	9	1	·	·	7
VII	3	2.3	3	1.0	2	3.0	5.5	2.7	4.5	1.8	29	2.1	9	3.0	7	2.6	30	1.5	82.6	22.4	28	·	·	·	7	·	·	2	16	16	15	2	1	·	2
VIII	4	2.0	1	1.0	·	·	4.5	2.1	5.5	2.4	24.5	2.6	11	2.6	13.5	2.7	29	1.7	56.6	18.5	10	·	·	·	5	·	·	3	10	14	8	1	·	·	2
IX	2.5	2.2	7	2.0	14.5	2.2	4	1.8	3	1.3	10	3.2	14.5	3.4	4.5	2.7	30	1.7	28.8	11.3	14	·	·	·	5	·	·	13	5	8	6	1	2	·	1
X	2	3.0	1	1.0	22.5	3.8	23	3.3	1.5	2.3	8.5	2.4	4	2.6	1.5	2.1	29	2.2	6.9	4.5	29	·	·	·	·	·	·	8	7	5	2	·	7	·	·
XI	5.5	3.4	3.5	6.8	16.5	3.4	6	2.5	5.5	1.8	17	2.6	6.5	2.3	9.5	2.8	20	2.3	63.0	8.2	11	·	1	14	·	·	·	1	18	18	15	·	4	·	·
XII	7.5	3.8	8	2.8	5	2.8	6	2.2	5	1.8	14.5	2.4	17	3.4	11	3.4	19	2.3	26.7	5.8	1	10	14	26	·	·	·	4	15	14	6	·	2	17	·
Rok	38.5	2.5	46	2.0	101	2.0	114.5	2.8	75	2.0	196.5	2.8	130.5	3.4	115	3.0	278	2.2	481.1	22.4	28.VII	22	29	103	33	6	2	56	146	156	109	7	—	40	21

Gorzyń $H_s = 60\ m$ $h_w = 15\ m$

I	·	·	0.5	4.0	18.5	2.6	14	2.7	20	3.6	15	3.5	12.5	2.3	15	2.7	11	2.6	38.0	8.7	14	10	10	23	·	·	·	6	13	16	10	·	1	15	·
II	1.5	2.0	0.5	5.0	5	3.6	11	4.1	13.5	3.6	12.5	4.2	15	3.1	16	2.2	9	3.0	31.8	9.6	9	·	·	11	·	1	·	1	12	14	6	·	10	2	·
III	·	·	1	3.0	·	·	·	·	1	7.0	11	4.3	65	4.4	13	4.2	2	4.3	56.5	14.3	30	·	·	4	·	3	2	1	11	16	11	2	4	·	·
IV	2.5	2.4	7.5	2.3	25	3.7	12	3.8	7	2.1	5.5	1.9	9	3.1	9.5	2.5	12	2.6	42.2	9.6	7	·	·	3	1	·	·	8	4	11	9	·	2	·	3
V	6.5	2.2	6	2.2	3.5	1.4	8.5	3.6	2.5	3.4	11.5	3.0	24	3.1	21.5	2.5	9	2.5	91.8	15.8	5	·	·	·	·	·	·	·	13	20	14	4	·	·	8
VI	2.5	1.4	4.5	2.5	4.5	3.0	9	2.6	1.5	2.3	6	3.1	37	2.7	8	2.7	17	2.2	35.3	11.7	4	·	·	·	12	·	·	5	4	8	6	1	·	·	4
VII	·	·	·	·	0.5	2.0	2.5	1.6	3.5	3.0	22	2.5	50.5	2.4	7	2.3	7	2.2	121.3	21.7	31	·	·	·	5	·	·	2	13	20	17	4	·	·	5
VIII	·	·	·	·	3	2.0	3	2.3	4	2.5	20	2.6	43.5	2.4	8.5	1.6	11	2.1	60.2	20.4	10	·	·	·	4	·	·	2	8	18	11	1	1	·	2
IX	·	·	·	·	16	2.4	11.5	3.2	12	1.8	14	2.6	22.5	2.7	2	2.2	12	2.2	37.6	14.7	3	·	·	·	7	·	·	11	5	8	5	2	·	·	3
X	2	1.0	·		19	5.1	22.5	3.4	19	2.9	7.5	3.3	7	2.5	3	2.3	13	3.0	25.1	5.3	23	·	·	·	·	·	·	7	9	12	9	·	3	·	·
XI	2	1.5	7	3.6	9.5	4.1	16.5	1.9	3	2.3	23	3.0	11	3.3	7	2.1	11	2.5	39.4	16.9	13	·	·	9	·	·	·	1	17	15	6	1	7	·	·
XII	1	4.0	5	2.6	6.5	2.5	12	3.0	14.5	3.4	13	4.3	19.5	3.2	10.5	3.2	11	2.9	47.4	16.1	11	9	13	23	·	2	·	5	13	15	6	2	2	10	·
Rok	18	1.2	32	2.1	111	2.7	122.5	2.7	101.5	3.2	161	3.2	316.5	2.9	107.5	2.5	125	2.7	626.6	21.7	31.VII	19	23	73	29	6	2	49	122	173	110	17	30	27	25

Trzemeszno $H_s = 105\ m$ $h_w = 15{,}4\ m$

I	1	1.0	8.5	1.9	12	1.4	16	1.4	16.5	1.9	18.5	2.8	13.5	2.4	7	2.1	·	2.0	26.0	8.0	31	7	11	22	·	·	·	6	16	13	6	·	·	16	·
II	2	1.8	2.5	1.0	5	1.5	6	1.3	16	2.0	17.5	2.6	20.5	2.5	14.5	2.7	·	2.3	29.3	9.3	9	·	·	12	·	1	·	1	14	14	8	·	7	2	·
III	1.5	4.0	0.5	2.0	·	·	·	·	·	·	12	3.5	49	5.0	30	4.9	·	4.7	33.9	10.6	30	·	·	5	·	3	1	1	16	15	7	1	4	2	·
IV	4.5	1.4	16.5	1.6	19	2.9	10.5	2.4	4	1.9	10.5	1.6	14	2.3	11	3.2	·	2.3	60.1	26.9	28	·	·	1	·	·	·	5	7	10	9	2	1	·	4
V	14.5	1.4	15	1.9	3.5	1.1	4	1.4	7	1.6	12	1.8	21	2.2	16	1.7	·	1.8	72.8	8.5	30	·	·	·	·	·	·	·	18	19	14	·	1	·	5
VI	4	1.5	5	2.0	14.5	1.3	3.5	1.3	8.5	1.9	7	1.2	26.5	2.1	21	1.8	·	1.8	31.5	10.0	10	·	·	·	12	·	·	·	6	13	6	1	·	·	5
VII	4	1.0	1	1.0	·	·	0.5	3.0	7	2.1	16.5	2.1	46	2.2	18	2.1	·	2.1	184.3	62.6	31	·	·	·	6	·	·	·	21	20	18	3	·	·	6
VIII	3.5	1.0	1	1.0	8.5	1.0	3.5	1.6	4	1.2	21	2.0	31.5	2.3	20	1.6	·	1.8	103.9	43.7	10	·	·	·	5	·	·	1	11	15	12	2	4	·	2
IX	4.5	1.0	2.5	1.2	22.5	1.3	6.5	1.8	9	1.7	12	2.0	21	2.3	11	2.0	1	1.7	20.5	14.4	14	·	·	·	7	·	·	10	7	5	4	1	·	·	·
X	0.5	1.0	2.5	2.2	17.5	2.5	21.5	2.3	19	1.5	11.5	1.6	10	2.0	9.5	2.0	1	2.0	31.2	11.0	19	·	·	·	·	·	·	2	11	11	5	1	4	·	·
XI	4	1.5	12.5	2.2	11.5	2.9	4	1.2	7.5	1.5	21	2.3	20	2.4	9.5	2.3	·	2.2	35.8	12.1	13	·	·	8	·	·	·	1	23	19	8	1	8	·	·
XII	4	1.9	12	1.3	6	1.8	12	1.1	15	1.6	13.5	4.4	17	2.8	13.5	3.1	·	2.4	31.0	10.1	11	9	16	24	·	·	·	2	15	11	9	1	6	20	·
Rok	46	1.5	79.5	1.6	120	1.5	88	1.6	113.5	1.6	173	2.3	290	2.5	181	2.5	2	2.3	660.3	62.6	31.VII	16	27	72	30	4	1	29	165	165	106	13	35	40	22

Gniezno

$\varphi = 52°33'$ $\lambda = 17°36'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	−5.4	5.4	4	−17.6	26	−4.2	−0.8	−3.1	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.0	5.1	6.1
II	–	–	–	–	5.3	0.1	12.3	18	−3.6	6	1.3	3.8	2.3	2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.0	6.4	7.8
III	–	–	–	–	9.5	2.4	17.7	10	−4.8	20	3.6	7.8	5.2	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	5.3	6.9
IV	–	–	–	–	15.4	4.5	24.9	7	−1.2	10	6.9	13.9	9.2	9.8	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.6	3.9	4.8
V	–	–	–	–	16.1	6.8	22.4	26	1.7	12	9.9	14.1	10.2	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	9.3	5.9	7.6
VI	–	–	–	–	23.9	12.6	28.9	25, 26	6.7	22	16.5	22.4	16.6	18.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.6	4.7	5.8
VII	–	–	–	–	20.9	12.1	33.0	3	7.7	6	14.7	18.8	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.4	7.6	8.0
VIII	–	–	–	–	20.6	12.1	29.3	6	8.4	18	13.8	18.9	15.0	15.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	5.9	7.2
IX	–	–	–	–	20.8	9.8	29.4	2	2.6	24	11.4	19.8	13.1	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.7	2.4	3.7
X	–	–	–	–	15.1	7.3	22.9	5	3.4	13	8.0	13.8	9.9	10.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.7	4.5	5.8
XI	–	–	–	–	6.0	1.8	12.2	2	−5.5	23	2.7	5.2	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.5	7.7	8.4
XII	–	–	–	–	−0.3	−7.4	15.6	5	−21.5	26	−4.3	−2.3	−4.2	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	5.9	6.8
Rok	–	–	–	–	12.8	4.7	33.0	3.VII	−21.5	26.XII	6.7	11.3	7.7	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.1	5.4	6.6

Krzemień

$\varphi = 52°33'$ $\lambda = 22°30'$

I	–	–	–	–	−0.9	−6.9	6.9	4	−24.8	26	−4.9	−2.2	−4.0	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	6.2	6.8
II	–	–	–	–	3.0	−1.3	10.8	18	−5.4	6	0.0	2.1	0.9	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.2	7.3	7.8
III	–	–	–	–	8.7	1.1	15.9	10	−4.1	20	2.8	7.1	4.3	4.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.6	5.5	6.0
IV	–	–	–	–	14.8	3.7	24.5	15	−3.5	10	6.6	13.3	8.2	9.1	–	–	–	–	–	–	–	–	–	–	–	–	4.3	3.6	3.1	3.7
V	–	–	–	–	16.5	7.0	25.4	28	1.2	15	10.9	15.2	10.8	12.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.4	4.7	5.0
VI	–	–	–	–	23.5	11.7	32.3	27	5.8	21	16.7	22.2	17.6	18.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.3	11.0	30.3	3	7.0	6	15.6	19.9	15.0	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.8	6.6	6.3
VIII	–	–	–	–	20.9	12.2	30.4	6	7.8	31	15.3	19.9	15.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	19.7	8.2	28.7	3	0.4	24, 28	10.6	19.0	12.5	13.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	14.8	5.1	18.9	4, 28	0.6	23	7.3	14.3	9.6	10.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	5.3	0.6	12.4	3	−6.8	24	2.7	3.6	2.8	3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.9	6.8	7.8
XII	–	–	–	–	−0.9	−8.0	14.9	5	−23.6	26	4.5	2.5	4.7	4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.6	5.5	6.9
Rok	–	–	–	–	12.2	3.7	32.3	27.VI	−24.8	26.I	6.6	11.0	7.4	8.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Płock – Radziwie

$\varphi = 52°32'$ $\lambda = 19°40'$

I	1012.2	1037.0	991.9	1020.4	0.2	−6.0	6.3	4	−19.6	26	−4.2	−0.8	−2.8	−2.6	4.3	4.8	4.5	4.5	86	78	83	82	0.6	1.2	0.8	0.9	6.9	7.5	5.6	6.7
II	1013.8	1029.3	985.8	1021.8	4.2	−0.1	12.1	18	−3.6	6	0.9	3.5	1.6	1.9	6.2	6.6	6.3	6.4	94	84	91	90	0.4	1.4	0.6	0.8	8.9	7.9	7.8	8.2
III	1008.0	1027.9	983.2	1015.9	9.5	2.3	17.2	10	−3.4	20	3.7	7.6	5.3	5.5	7.0	7.2	7.3	7.2	87	69	81	79	1.1	3.6	1.8	2.2	8.6	7.7	6.6	7.6
IV	1005.7	1016.6	995.5	1013.5	15.7	4.8	24.5	7	−2.8	10	6.7	14.0	9.8	10.1	8.3	9.0	9.4	8.9	82	56	75	71	1.8	7.9	3.2	4.3	5.3	5.3	4.0	4.9
V	1004.4	1011.4	990.9	1012.1	17.2	6.8	23.8	27	0.2	19	9.8	15.3	11.2	11.9	11.0	11.3	11.7	11.3	89	66	87	81	1.3	6.6	1.9	3.3	7.2	7.5	7.3	7.3
VI	1007.2	1020.4	996.5	1014.8	24.3	13.0	32.9	27	6.3	22	16.6	22.9	17.8	18.8	16.3	16.4	17.3	16.7	86	60	84	77	2.8	12.1	3.3	6.1	5.0	6.1	5.7	5.6
VII	1005.3	1018.6	988.7	1013.0	21.5	11.7	32.8	3	7.6	6	14.6	19.6	15.6	16.4	14.7	14.9	15.4	15.0	88	67	86	80	2.0	8.8	2.6	4.5	7.4	7.9	6.3	7.2
VIII	1008.0	1022.2	995.6	1015.7	21.2	12.1	30.3	6	7.8	4	14.0	19.5	15.6	16.2	15.0	15.3	16.0	15.4	93	68	89	83	1.2	7.9	2.1	3.7	7.7	7.3	6.0	7.0
IX	1011.3	1023.3	998.4	1019.0	20.5	9.4	29.5	2	1.4	28	11.1	19.4	13.6	14.4	12.5	13.6	13.7	13.3	92	60	86	79	1.2	9.7	2.2	4.4	4.9	5.0	3.0	4.3
X	1011.7	1023.9	985.4	1019.5	15.4	6.8	20.8	5	2.7	14	7.9	14.5	10.7	11.0	9.8	11.8	10.9	10.8	92	73	86	84	1.0	4.9	2.0	2.6	6.8	6.7	4.8	6.1
XI	1006.9	1029.2	994.4	1014.8	6.0	1.5	12.8	3	6.0	23	2.8	5.1	3.6	3.8	7.3	7.8	7.5	7.5	94	87	92	91	0.5	1.2	0.7	0.8	8.3	8.6	8.3	8.4
XII	1008.3	1038.9	984.0	1016.5	−0.5	−6.5	15.4	5	−22.1	27	−4.0	−2.1	−3.6	−3.3	4.5	4.8	4.6	4.6	86	82	88	85	0.7	1.1	0.6	0.8	7.8	7.2	6.6	7.2
Rok	1008.6	1038.9	983.2	1016.5	12.9	4.6	32.9	27.VI	−22.1	27.XII	6.7	11.5	8.2	8.6	9.7	10.3	10.4	10.1	89	71	86	82	1.2	5.5	1.8	2.8	7.1	7.1	6.0	6.7

Przybroda

$\varphi = 52°31'$ $\lambda = 16°40'$

I	–	–	–	–	0.1	−5.6	5.6	30	−17.4	26	−4.3	−0.8	−2.8	−2.7	4.1	4.7	4.4	4.4	81	74	81	79	0.8	1.2	0.9	1.0	6.0	5.3	6.2	5.8
II	–	–	–	–	5.6	0.2	11.5	28	−3.5	6	1.6	4.4	2.3	2.6	6.3	7.2	6.5	6.7	91	84	90	88	0.6	1.3	0.7	0.9	8.1	7.9	6.0	7.3
III	–	–	–	–	9.5	2.0	18.4	10	−5.6	20	3.9	8.2	4.9	5.5	7.1	7.5	7.4	7.3	86	70	84	80	1.2	3.7	1.4	2.1	8.2	7.0	5.2	6.8
IV	–	–	–	–	15.1	4.5	24.7	7	−1.1	10	7.2	13.6	9.5	10.0	8.3	8.8	9.1	8.7	79	57	75	70	2.2	7.6	3.1	4.3	5.4	5.2	3.9	4.8
V	–	–	–	–	15.5	6.6	22.1	26	2.5	13	10.0	13.7	10.1	11.0	10.5	10.2	10.6	10.4	85	67	85	79	1.9	5.7	1.9	3.2	7.9	8.1	5.7	7.2
VI	–	–	–	–	22.9	11.9	28.2	26	6.9	22	16.4	21.6	16.1	17.6	14.4	13.3	14.8	14.1	77	52	80	70	4.4	13.0	3.8	7.0	5.1	4.8	5.1	5.0
VII	–	–	–	–	20.6	11.8	31.8	3	7.2	6	14.9	18.9	14.8	15.8	14.3	13.3	14.4	14.0	84	63	86	78	3.0	9.4	2.6	5.0	7.8	7.6	7.8	7.7
VIII	–	–	–	–	20.6	12.0	28.6	6	8.1	4	14.5	19.0	15.1	15.9	14.7	14.8	15.0	14.8	88	66	87	80	2.0	7.8	2.3	4.0	7.4	6.6	4.4	6.1
IX	–	–	–	–	20.7	9.9	29.7	2	2.6	24	12.0	19.7	14.0	14.9	12.5	12.9	12.9	12.8	87	56	80	74	1.9	10.6	3.5	5.4	4.4	4.1	4.0	4.2
X	–	–	–	–	14.7	7.4	21.3	6	2.0	31	8.8	14.0	10.3	10.8	10.1	11.1	10.6	10.6	89	71	85	82	1.3	5.2	2.1	2.9	6.3	5.6	4.3	5.4
XI	–	–	–	–	6.2	1.6	12.1	2	−6.4	23	2.9	5.6	3.4	3.8	7.0	7.6	7.1	7.2	89	82	89	87	0.8	1.7	0.9	1.1	8.7	8.3	6.0	7.7
XII	–	–	–	–	0.1	−6.9	15.1	5	−22.7	27	−3.8	−1.7	−3.9	−3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.1	6.0	6.9
Rok	–	–	–	–	12.6	4.6	31.8	3.VII	−22.7	27.XII	7.0	11.4	7.8	8.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	5.4	6.3

Gniezno

$H_s = 110\ m$ $h_w = 10\ m$ **1961**

MIESIĄC	ROZKŁAD WIATRU [%D, %cD]																		OPAD R			LICZBA DNI (n)											
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v		G	●	Opad R			≡	▥	≋
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max≥25°	≥10	≥15			≥0.1	≥1.0	≥10.0			
I	0.5	3.0	7	3.7	2.5	3.0	13	1.3	30	1.5	19.5	1.7	8	1.7	4.5	2.1	8	1.7	29.2	9.8	31	9	11	24	·	·	·	8	13	13	7	·	5	12	·
II	1	1.5	2	3.0	1.5	1.7	10	1.8	21.5	2.1	17.5	1.8	18	3.0	7.5	3.7	5	2.2	33.6	12.4	9	·	·	12	·	1	·	·	14	14	7	1	9	1	·
III	0.5	5.0	1	3.0	1	1.0	·	·	·	·	18.5	4.8	53	4.9	18	5.4	1	4.9	39.2	11.2	30	·	·	5	·	10	4	3	15	13	9	1	3	2	·
IV	6	2.3	10	2.7	18.5	4.7	15	3.0	5	1.4	10	1.4	8	2.7	7.5	2.1	10	2.6	32.8	9.5	16	·	·	5	·	·	·	7	7	10	7	·	2	1	4
V	9.5	1.8	10.5	3.1	3	1.3	1.5	1.0	10	1.0	16.5	1.8	18.5	2.5	13.5	2.2	10	1.8	80.5	14.8	5	·	·	·	·	1	1	·	12	18	15	2	·	·	3
VI	3.5	1.0	3.5	1.3	8	2.4	9.5	2.2	10	1.7	12	2.5	23.5	2.4	8	1.5	12	1.8	66.3	29.0	8	·	·	·	13	·	·	4	7	12	5	3	2	·	5
VII	0.5	1.0	·	·	·	·	1	1.0	6	1.3	22	2.0	38	2.5	8.5	3.5	17	1.9	223.3	62.0	31	·	·	·	5	·	·	2	20	18	17	6	·	·	7
VIII	3	2.0	·	·	4	1.2	0.5	1.0	3.5	1.4	24.5	1.9	31.5	2.8	2	1.0	24	1.6	96.9	36.5	10	·	·	·	5	1	1	1	13	16	13	3	3	·	2
IX	1	1.0	·	·	9.5	1.6	9.5	1.8	3.5	1.6	21	1.9	14.5	2.3	2	1.0	29	1.3	23.4	17.3	14	·	·	·	7	1	·	13	5	4	3	1	3	·	3
X	0.5	1.0	1	1.0	15.5	3.2	12	2.5	16.5	1.8	11	2.1	10	1.5	3.5	1.6	23	1.7	36.8	15.3	19	·	·	·	·	1	·	6	10	9	5	1	4	·	·
XI	6	3.0	8.5	3.5	8.5	3.8	2	1.0	7	2.1	22	3.0	10	3.6	4	2.4	22	2.3	37.4	9.9	13	·	·	10	·	2	·	2	21	13	9	·	7	·	·
XII	7.5	2.1	6.5	1.6	4.5	1.7	1	2.0	16.5	1.3	13.5	4.2	20.5	2.8	6	3.9	17	2.1	40.6	16.1	11	12	15	25	·	3	·	2	15	13	9	1	7	20	·
Rok	39.5	2.1	50	1.9	76.5	2.1	75	1.6	129.5	1.4	208	2.4	253.5	2.7	85	2.5	178	2.2	740.0	62.0	31.VII	21	26	81	30	20	6	48	152	153	106	13	45	36	24

Krzemień

$H_s = 111\ m$ $h_w = 10\ m$

I	4.5	5.7	2	3.2	0.5	2.0	12	3.2	12.5	3.6	15	3.5	16	3.2	6.5	3.0	24	2.6	26.1	8.9	31	12	12	29	·	1	·	4	14	11	6	·	1	19	·
II	·	·	1	5.0	2.5	4.2	9.5	2.9	11	3.1	6	2.0	15.5	2.7	2.5	3.2	36	1.7	11.0	3.0	28	·	1	20	·	·	·	·	17	11	3	·	5	4	·
III	·	·	·	·	·	·	·	·	3	4.7	20	5.0	44.5	4.9	10.5	3.9	15	4.0	26.3	13.6	30	·	·	12	·	4	·	4	9	13	6	1	3	1	·
IV	4.5	3.4	3	3.2	15.5	4.5	9	4.3	3	3.0	7.5	3.4	7.5	5.3	5	4.0	35	2.5	37.1	21.1	16	·	·	5	·	1	·	13	5	8	7	1	·	·	1
V	1	6.0	2	4.0	7	3.4	8	2.3	4	3.4	5	2.1	11.5	2.2	9.5	3.2	45	1.5	64.3	15.2	1	·	·	·	1	·	·	5	7	14	12	1	·	·	1
VI	·	·	0.5	3.0	4	2.5	8	2.1	11.5	2.4	15.5	2.4	13	3.0	3.5	2.9	34	1.6	23.9	4.6	21	·	·	·	9	·	·	—	—	10	7	·	·	·	1
VII	·	·	4	3.9	1.5	3.0	4.5	4.2	3.5	3.7	22	3.4	22	3.2	1.5	3.0	34	2.2	137.9	36.5	28	·	·	·	5	·	·	4	14	13	11	5	·	·	4
VIII	1.5	3.3	·	·	2.5	3.0	1	2.5	4.5	3.9	21.5	3.6	19.5	3.5	10.5	3.0	32	2.3	61.1	20.0	11	·	·	·	5	·	·	—	—	14	11	3	·	·	4
IX	1	4.0	2	3.8	8.5	3.0	3.5	1.6	2	2.5	13	3.6	14.5	2.8	4.5	1.6	41	1.6	25.6	8.3	12	·	·	·	6	1	·	—	—	10	6	·	2	·	·
X	·	·	3.5	2.4	19.5	4.4	21.5	4.3	11	2.8	5.5	3.4	7	3.1	1	2.0	24	2.8	4.7	3.5	29	·	·	·	·	·	·	—	—	2	2	·	6	·	·
XI	5	3.2	4	5.2	12	6.5	7.5	4.3	3.5	2.4	10	4.6	13	4.1	2	4.5	33	2.9	55.7	10.3	12	·	2	15	·	·	·	·	17	15	12	2	6	·	·
XII	8.5	4.5	2	2.2	2.5	4.0	8	3.2	7.5	3.1	11.5	5.7	16.5	3.8	13.5	4.4	23	3.1	16.2	5.4	1	11	15	26	·	1	·	3	5	10	5	·	1	21	·
Rok	26	2.5	24	3.0	76	3.4	92.5	2.9	77	3.2	152.5	3.6	200.5	3.5	70.5	3.2	376	2.4	489.9	36.5	28.VII	23	30	107	26	8	·	—	—	131	88	13	24	46	11[2]

Płock - Radziwie

$H_s = 63\ m$ $H_s = 63{,}8\ m$ $h_w = 14\ m$

I	4	2.8	3.5	3.1	3	3.3	15	3.9	13.5	2.4	18	3.4	15	3.2	2	3.5	19	2.6	19.1	9.9	31	12	12	26	·	·	·	4	14	12	4	·	2	16	·
II	·	·	·	·	·	·	17	3.3	10.5	2.9	20.5	2.8	24	2.8	4	2.5	8	2.6	21.9	7.2	9	·	·	15	·	1	1	·	17	13	6	·	12	5	·
III	·	·	·	·	0.5	3.0	0.5	3.0	1	3.5	19.5	5.7	61	6.1	6.5	5.7	4	5.6	34.0	11.2	30	·	·	5	·	7	·	·	17	16	8	1	4	1	·
IV	3	4.5	4.5	4.8	17.5	4.8	19	4.8	9.5	2.2	5.5	2.7	16	3.9	7	4.2	8	3.7	28.4	6.4	16	·	·	3	·	1	·	10	7	11	9	·	2	2	3
V	7	4.3	5	3.6	4	3.4	8.5	3.5	8	3.5	16	3.0	17.5	2.7	13	4.7	14	2.9	52.1	13.7	27	·	·	·	·	·	·	·	13	14	11	1	2	·	5
VI	1	1.0	1	5.0	5.5	3.9	13.5	3.4	10.5	2.5	17.5	3.9	25	4.0	3	4.3	13	3.1	61.1	29.0	8	·	·	·	13	2	·	2	4	12	10	1	·	·	10
VII	1.5	1.7	3.5	1.7	1.5	2.0	3	2.0	5	2.5	32	3.6	35.5	3.9	4	2.9	7	3.2	129.9	35.4	13	·	·	·	7	1	·	3	11	17	11	5	1	·	5
VIII	1	2.0	·	·	1	3.0	3	2.6	5	1.6	29	3.8	40	3.8	3	4.7	11	3.2	73.7	15.5	11	·	·	·	6	·	·	1	10	16	13	3	2	·	8
IX	1.5	4.0	1	3.0	14	2.5	9.5	3.9	4.5	2.7	15	2.8	27	3.8	25	2.8	15	2.7	31.2	13.9	14	·	·	·	5	·	·	9	5	7	4	1	2	·	1
X	·	·	0.5	5.0	30.5	4.5	27.5	3.8	6.5	2.9	6.5	3.1	7.5	4.0	5	2.8	9	3.5	13.7	5.5	29	·	·	·	·	·	·	4	9	8	4	·	6	·	·
XI	8	2.5	4.5	2.9	13	5.5	16	2.6	4	2.9	14.5	4.6	13	4.0	3	2.3	14	3.2	76.6	16.1	11	·	·	8	·	·	·	1	21	20	16	2	3	·	·
XII	5.5	4.2	6	3.4	7.5	3.5	17	3.0	4	2.5	16.5	4.7	21.5	4.1	11	3.4	4	3.6	24.3	8.5	1	8	14	24	·	·	·	4	18	11	5	·	6	16	·
Rok	32.5	2.2	29.5	2.7	98	3.3	149.5	3.3	82	2.7	210.5	3.7	303	3.9	64	3.6	126	3.3	566.0	35.4	13.VII	20	26	81	31	12	1	38	146	157	101	44	42	40	32

Przybroda

$H_s = 88\ m$ $h_w = 10\ m$

I	1	3.0	9.5	2.7	15	3.0	19.5	2.6	22	3.7	12.5	3.3	8.5	3.5	2	3.0	3	3.0	27.4	7.4	14	9	11	24	·	·	·	7	12	11	10	·	2	15	·
II	0.5	3.0	2.5	3.0	9	3.2	10.5	3.3	19.5	3.6	15	3.3	17	4.4	5	3.9	5	3.4	27.0	11.9	9	·	·	13	·	·	·	1	12	11	6	1	7	3	·
III	1	6.0	·	·	·	·	·	·	4.5	4.3	22	5.4	57	5.3	6.5	4.4	2	5.1	47.0	14.1	30	·	·	5	·	4	·	2	13	17	10	1	3	·	·
IV	8.5	2.7	11	3.8	19.5	4.0	10.5	3.0	7.5	3.1	7.5	3.1	8.5	4.1	9	2.8	8	3.1	83.0	24.5	15	·	·	4	·	·	·	10	8	13	11	3	3	·	5
V	1.5	3.2	8	2.6	5	2.7	5	2.6	5	2.8	20	3.4	15.5	3.1	14.5	3.3	5	2.9	66.0	16.8	5	·	·	·	·	·	·	·	11	17	13	1	1	·	2
VI	4	2.1	4	2.1	10	2.8	5.5	2.6	10	2.6	12	2.8	27	3.9	2.5	1.8	1.5	2.5	33.8	18.4	10	·	·	·	9	·	·	2	5	6	4	1	·	·	2
VII	0.5	2.0	1	2.0	1	2.5	4.5	2.8	10	2.6	32	4.2	30	3.7	6	3.5	8	3.3	138.7	44.5	31	·	·	·	5	·	·	1	17	17	15	3	·	·	2
VIII	4	2.1	1	3.0	2.5	2.6	5.5	2.5	12.5	3.4	27	3.9	18	4.1	6.5	2.9	1.6	2.9	89.7	46.9	10	·	·	·	4	·	·	2	6	13	11	1	1	·	2
IX	1.5	1.7	4.5	1.9	16.5	3.2	7	2.5	14	3.1	15.5	3.9	11	4.2	4	2.8	1.6	2.7	24.0	14.9	14	·	·	·	5	·	·	12	6	5	2	1	·	·	2
X	1	3.0	0.5	4.0	24	4.8	10	3.5	18.5	3.1	25	4.1	9	3.1	4.5	3.7	1.8	3.1	19.7	5.4	29	·	·	·	·	·	·	9	9	9	7	·	3	·	·
XI	10	2.6	10	3.4	6	3.3	3	2.3	12	3.5	26	3.7	9	3.9	7	2.3	7	3.1	29.8	13.2	13	·	·	7	·	·	·	2	15	9	5	1	7	·	·
XII	7	2.7	9.5	2.9	6.5	3.3	12.5	2.9	9.5	3.7	14.5	5.0	16.5	4.3	10	3.4	7	3.4	45.5	15.8	11	10	16	24	·	·	·	2	13	11	8	2	4	—	·
Rok	54	2.8	61.5	2.6	115	3.0	93.5	2.6	145	3.3	211.5	3.8	227	4.0	77.5	3.2	110	3.2	631.6	46.9	10.VIII	19	27	77	23	4	·	50	127	139	102	15	31	—	15[2]

Wieliszew — φ = 52°27' — λ = 20°58' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.1	-6.2	6.7	5	-22.3	26	-4.1	-1.5	-3.1	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	4.0	-0.6	11.1	28	-6.2	5	0.7	2.6	1.1	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	9.3	1.5	16.8	10	-2.4	3	3.6	7.2	5.1	5.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.5	4.4	23.9	7	-3.8	10	7.1	13.7	9.7	10.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.3	7.0	26.1	27	1.9	13, 17	10.5	15.4	11.3	12.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	24.1	12.4	33.6	27	6.5	21	16.2	22.2	17.0	18.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	11.0	32.1	3	6.5	6	14.1	19.6	15.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.3	11.5	30.9	6	7.3	31	14.5	19.8	15.7	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.7	8.8	29.1	3	1.6	28	11.1	19.2	14.0	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.3	5.2	22.4	19	0.9	30	7.4	14.3	10.0	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.2	0.5	13.4	3	-8.5	23	2.3	4.7	3.3	3.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-0.2	-7.3	15.6	5	-24.0	26	-4.2	-2.2	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.9	4.0	33.6	27.VI	-24.0	26.XII	6.6	11.2	8.0	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Poznań-Sołacz — φ = 52°26' — λ = 16°54'

I	–	–	–	–	0.4	-5.1	5.8	4	-15.8	26,27	-3.9	-0.6	-2.8	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	6.0	0.1	12.5	18	-3.1	6	1.6	4.6	2.7	2.9	6.2	7.0	6.5	6.6	90	81	87	86	0.7	1.6	1.0	1.1	–	–	–	–
III	–	–	–	–	9.9	2.4	18.3	10	-6.5	20	3.9	8.1	5.5	5.8	6.9	7.1	7.1	7.0	85	66	77	76	1.3	4.0	2.3	2.5	–	–	–	–
IV	–	–	–	–	15.5	5.3	24.9	7	-1.3	10	7.0	14.0	10.0	10.2	8.2	9.2	9.4	8.9	80	57	74	70	2.1	7.8	3.3	4.4	–	–	–	–
V	–	–	–	–	15.8	6.9	22.3	26	2.8	13	9.6	14.1	10.7	11.3	10.3	10.7	10.9	10.6	86	68	85	80	1.8	5.7	2.1	3.2	–	–	–	–
VI	–	–	–	–	23.6	12.5	29.1	25	6.5	22	16.6	22.1	17.2	18.3	14.5	13.6	15.5	14.5	76	51	79	69	4.7	13.3	4.5	7.5	–	–	–	–
VII	–	–	–	–	20.7	12.3	33.0	3	7.7	6	14.8	19.1	15.5	16.2	13.7	13.4	14.2	13.8	81	63	81	75	3.4	9.6	3.6	5.5	–	–	–	–
VIII	–	–	–	–	20.9	12.1	31.8	6	8.3	4, 18	14.1	19.3	15.1	15.9	14.4	14.7	15.1	14.7	89	66	87	81	1.9	8.3	2.2	4.1	–	–	–	–
IX	–	–	–	–	21.0	9.8	30.0	2	3.1	24	11.7	20.1	13.7	14.8	12.2	13.5	13.4	13.0	87	57	84	76	1.9	10.6	2.5	5.0	–	–	–	–
X	–	–	–	–	15.1	7.6	22.0	6	1.8	13	8.7	14.4	10.3	10.9	10.0	11.1	10.7	10.6	88	69	86	81	1.4	5.6	2.0	3.0	–	–	–	–
XI	–	–	–	–	6.5	1.7	12.7	2	-7.3	23	2.9	5.8	3.6	4.0	7.0	7.5	7.3	7.3	91	80	90	87	0.7	1.9	0.9	1.2	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	33.0	3. VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Poznań-Ławica — φ = 52°25' — λ = 16°50'

I	1007.7	1032.8	984.8	1019.5	0.2	-5.8	5.4	9, 30	-16.5	26	-4.4	-0.8	-2.9	-2.8	4.3	4.8	4.5	4.5	86	78	84	83	0.5	1.2	0.7	0.8	6.0	6.1	6.4	6.2
II	1009.9	1026.3	980.6	1021.5	5.8	0.2	12.6	18	-4.0	6	1.4	4.5	2.6	2.8	6.4	6.9	6.6	6.6	93	82	90	88	0.5	1.6	0.8	1.0	8.2	7.6	6.9	7.6
III	1006.5	1025.8	979.0	1018.0	9.9	2.2	18.6	10	-6.7	20	3.8	8.1	5.1	5.5	7.0	7.2	7.3	7.2	86	67	82	78	1.2	4.0	1.7	2.3	8.2	8.0	5.6	7.3
IV	1001.5	1012.4	990.7	1012.7	15.5	5.0	25.1	7	-1.1	10	6.8	13.9	9.9	10.1	8.1	8.7	9.0	8.6	80	55	72	69	2.0	8.2	3.7	4.6	5.7	6.0	3.9	5.2
V	1001.5	1010.4	986.7	1012.6	15.8	6.9	22.4	26	2.2	13	9.6	14.0	10.7	11.2	10.3	10.2	10.5	10.3	85	65	82	77	1.8	6.2	2.5	3.5	8.0	8.6	5.8	7.5
VI	1004.2	1018.2	992.1	1015.1	23.5	12.3	29.6	25	6.8	22	16.3	22.0	17.1	18.1	14.0	13.0	15.0	14.0	75	49	76	67	4.8	14.0	4.8	7.9	4.9	6.0	5.3	5.4
VII	1002.3	1015.3	986.2	1013.3	21.0	12.2	34.0	3	6.9	6	14.6	19.2	15.5	16.2	14.3	14.1	14.8	14.4	86	65	84	78	2.6	9.1	3.2	5.0	7.8	8.1	7.3	7.7
VIII	1005.1	1018.6	992.5	1016.2	20.9	11.9	30.2	6	7.6	4, 18	13.8	19.3	15.2	15.9	14.5	15.1	15.3	15.0	91	68	88	82	1.4	7.9	2.1	3.8	7.5	7.7	5.3	6.8
IX	1007.5	1018.2	993.9	1018.6	21.0	10.2	30.3	2	3.8	24	11.6	20.0	14.1	15.0	12.4	13.3	13.4	13.0	89	57	82	76	1.6	10.9	2.9	5.1	4.4	4.4	4.2	4.3
X	1006.9	1019.3	978.4	1018.2	15.1	7.6	22.2	6	1.9	13	8.4	14.4	10.3	10.8	9.9	10.9	10.5	10.4	89	68	84	80	1.3	5.9	2.2	3.1	6.4	6.1	4.8	5.8
XI	1003.2	1026.2	989.1	1014.7	6.4	1.3	12.6	2	-7.0	23	2.7	5.6	3.2	3.7	7.0	7.6	7.2	7.3	91	82	91	88	0.7	1.7	0.7	1.0	8.9	8.6	7.0	8.2
XII	1004.9	1035.6	979.0	1016.7	0.1	-7.2	15.0	5	-23.4	26	-4.1	-1.8	-3.8	-3.4	4.5	4.9	4.5	4.6	85	82	84	84	0.7	1.1	0.9	0.9	7.1	7.2	6.8	7.0
Rok	1005.1	1035.6	978.4	1016.5	12.9	4.7	34.0	3.VII	-23.4	26.XII	6.7	11.5	8.1	8.6	9.4	9.7	9.9	9.7	86	68	83	79	1.6	6.0	2.2	3.3	6.9	7.0	5.8	6.6

Nowy Dwór Mazowiecki — φ = 52°26' — λ = 20°43'

I	–	–	–	–	-0.1	-5.6	6.3	4	-20.1	26	-4.2	-1.1	-2.9	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.7	6.9
II	–	–	–	–	3.6	-0.3	10.6	18	-3.7	5, 6	0.6	2.8	1.5	1.6	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.2	7.6	8.4
III	–	–	–	–	9.2	2.1	17.0	10	-2.2	20	3.5	7.4	5.3	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	5.9	7.1
IV	–	–	–	–	15.7	4.6	24.4	7	-1.1	10	6.5	14.2	9.6	10.0	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.1	3.2	3.8
V	–	–	–	–	17.4	7.8	26.3	27	3.3	13, 15	10.2	15.6	11.8	12.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.6	8.4	7.4
VI	–	–	–	–	24.2	13.4	33.0	27	7.6	21	16.6	22.5	17.8	18.7	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.4	6.6	5.9
VII	–	–	–	–	21.7	11.9	32.1	3	8.2	6	14.5	19.9	16.2	16.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	7.6	7.4
VIII	–	–	–	–	21.3	12.6	30.8	6	8.1	2	14.4	19.9	16.0	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.9	7.9	7.0
IX	–	–	–	–	20.8	9.4	29.0	3	2.7	24	10.6	19.8	13.3	14.2	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.0	4.3	4.3
X	–	–	–	–	15.7	–	21.9	20	1.6	31	7.1	14.6	10.2	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.6	6.6	6.2
XI	–	–	–	–	6.0	1.1	13.5	3	-8.3	23	2.4	5.0	3.4	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.9	8.2	8.6
XII	–	–	–	–	-0.4	–	16.0	5	-23.6	26	-4.2	-2.3	-3.8	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.4	6.5	6.7
Rok	–	–	–	–	12.9	–	33.0	27.VI	-23.6	26.XII	6.5	11.5	8.2	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	6.6	6.6

Wieliszew $H_s = 78\,m$ $h_w = 13\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (ⁿD, ᵛmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v ≥10	v >15	◉	●	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	R ϖ
I	3.5	4.4	6.5	4.5	6	2.7	16.5	3.6	10.5	3.9	20	4.2	8	3.8	2	4.2	20	3.1	34.7	11.4	31	11	12	26	·	1	·	—	—	13	8	1	3	18	·
II	1.5	2.3	2.5	3.0	1	2.5	10	4.2	11.5	4.1	18.5	3.4	14	3.6	·	·	25	2.6	18.0	3.7	9	·	·	19	·	·	·	—	—	11	8	·	7	6	·
III	1.5	4.3	·	·	·	·	·	·	4	6.1	26.5	5.9	37.5	5.5	14.5	6.0	9	5.2	31.4	7.3	21	·	·	9	·	6	·	—	—	19	6	·	1	4	·
IV	5.5	3.5	8	3.9	20	3.8	12	4.7	6.5	3.7	8	4.5	7.5	5.6	4.5	4.7	18	3.4	45.5	25.4	16	·	·	2	·	1	·	—	—	10	8	1	·	·	2
V	5.5	4.1	1.5	4.7	8	3.3	5	2.8	6.5	4.5	13	3.5	12.5	4.4	9	3.6	32	2.5	33.0	11.1	28	·	·	·	2	·	·	—	—	13	9	1	·	·	3
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	41.2	8.8	22	·	·	·	13	—	—	—	—	13	11	·	1	·	9
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	60.7	13.1	29	·	·	·	5	—	—	—	—	18	11	2	1	·	6
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	59.3	19.6	12	·	·	·	6	—	—	—	—	13	7	2	·	·	4
IX	1	3.0	4	2.9	16	3.0	7	2.6	4	3.0	15.5	3.7	15.5	4.1	3	3.2	24	2.4	24.0	9.5	6	·	·	·	5	·	·	—	—	6	4	·	3	·	2
X	0.5	1.0	4.5	4.3	23.5	3.7	17	4.5	14.5	4.1	7.5	3.5	7	4.4	3.5	3.1	15	3.4	5.8	2.4	29	·	·	·	·	·	·	—	—	5	3	·	4	·	·
XI	9	3.7	5	6.3	13	5.6	9.5	2.8	10	3.5	14	4.7	15	4.1	5.5	2.9	9	3.8	47.2	9.3	4	·	1	13	·	1	·	—	—	16	12	·	4	·	·
XII	11.5	7.2	5.5	4.8	4.5	3.8	6	3.5	13	3.5	18.5	5.0	18.5	3.9	9.5	3.9	6	4.2	17.4	4.5	1	10	14	25	·	2	1	—	—	11	6	·	5	18	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	418.2	25.4	16.IV	21	27	94	31	—	—	—	—	148	93	7	29	46	26

Poznań - Sołacz $H_s = 71\,m$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	32.2	8.8	14	8	11	24	·	—	—	—	—	11	10	·	·	—	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	35.3	14.2	9	·	·	12	·	—	—	—	—	13	9	1	2	—	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	42.8	9.2	30	·	·	5	·	—	—	—	—	17	12	·	·	—	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	66.5	28.0	15	·	·	2	·	—	—	—	—	11	10	1	2	·	1
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	88.8	22.0	5	·	·	·	·	—	—	—	—	20	17	2	1	·	3
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	69.9	37.4	10	·	·	·	13	—	—	—	—	6	6	2	·	·	4
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	141.4	56.2	31	·	·	·	5	—	—	—	—	21	17	2	·	·	5
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	48.4	8.5	11	·	·	·	5	—	—	—	—	17	12	·	·	·	2
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	45.0	17.8	3	·	·	·	7	—	—	—	—	7	4	2	·	·	2
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	26.4	6.1	29	·	·	·	·	—	—	—	—	14	8	·	6	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	36.4	15.5	13	·		7	·	—	—	—	—	14	6	1	1	—	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	·	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	56.2	31.VII	—	—	—	30	—	—	—	—	—	—	—	—	—	—

Poznań-Ławica $H_s = 86\,m$ $H_b = 92.1\,m$ $h_w = 13\,m$

I	0.5	3.0	2.5	4.2	10	4.0	21.5	2.9	25	3.9	14	4.5	7.5	5.2	4.5	4.1	12	3.4	31.0	8.8	14	10	11	25	·	1	·	7	14	15	6	·	6	21	·
II	1	4.5	1	3.5	9	2.9	13	3.4	18.5	4.5	15	3.8	12.5	5.5	10	5.0	4	4.0	41.0	16.8	9	·	·	12	·	2	·	2	15	13	10	1	11	1	·
III	2	5.0	1	5.0	·	·	·	·	4	5.0	27	6.1	49.5	7.3	9.5	7.1	·	6.7	43.6	10.4	30	·	·	5	·	18	4	·	14	17	11	1	4	1	·
IV	5	3.5	5.5	4.7	24.5	4.9	16.5	4.0	6	4.6	8.5	2.9	5	7.3	9	4.0	10	3.9	85.0	30.0	15	·	·	2	1	4	·	7	9	12	10	3	2	·	3
V	13.5	4.8	7	5.6	3.5	2.3	8	2.6	7.5	4.1	16.5	5.3	17	5.4	15	5.4	5	4.6	105.0	23.4	5	·	·	·	·	6	2	·	13	19	19	3	3	·	7
VI	6.5	3.1	3	5.8	11	3.7	9.5	3.0	7.5	3.6	16.5	4.2	22	5.9	10	5.8	4	4.3	101.5	38.7	10	·	·	·	12	5	·	2	5	9	6	3	1	·	7
VII	1	3.0	0.5	1.0	2.5	3.0	4	3.0	12.5	3.2	32	4.6	26.5	6.3	10	5.4	4	4.6	132.5	48.9	31	·	·	·	5	6	·	2	17	20	17	2	·	·	7
VIII	3.5	3.7	1.5	3.0	3	3.0	4.5	2.2	12.5	4.0	28.5	4.9	23	5.7	10.5	4.3	6	4.3	49.9	7.4	11	·	·	·	4	7	1	1	9	15	12	·	5	·	2
IX	4	3.8	4	1.6	20.5	3.7	15	3.0	13	3.8	15	4.9	13	6.5	3.5	4.6	2	4.1	52.0	19.8	14	·	·	·	6	5	·	11	8	8	4	3	2	·	2
X	3	4.3	·	·	19.5	5.3	20	4.2	19	4.1	13	3.5	6.5	4.7	6	4.5	6	4.1	25.4	5.4	29	·	·	·	·	2	·	7	10	12	9	·	7	·	·
XI	7	5.0	7	5.3	12.5	6.6	8	2.2	8	2.8	26.5	4.9	11	5.1	7	5.3	3	4.6	36.5	14.7	13	·	·	8	·	5	·	1	17	15	7	1	7	·	·
XII	5	5.0	8.5	3.5	8	4.1	11	3.2	13	3.3	11.5	6.0	18	5.8	12	5.0	6	4.3	49.1	17.1	11	12	15	24	·	8	·	2	15	16	9	1	7	19	·
Rok	52	4.1	41.5	3.6	124	3.6	131	2.8	142	3.9	224	4.6	211.5	5.9	107	5.0	62	4.4	752.5	48.9	31.VII	22	26	76	28	69	7	42	146	171	120	18	55	42	28

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Nowy Dwór Mazowiecki $H_s = 70\,m$ $h_w = 13\,m$

I	5	2.5	5	1.8	3.5	1.1	9.5	1.5	21.5	1.2	22.5	1.3	8.5	1.8	9.5	1.5	8	1.3	29.1	10.0	31	9	13	26	·	·	·	6	18	12	8	1	8	21	·
II	3	1.3	0.5	2.0	3	1.3	12	1.2	19	1.4	14	1.3	11.5	1.2	6	1.0	15	1.0	19.8	7.1	9	·	2	16	·	·	·	·	17	7	7	·	14	6	·
III	·	·	·	·	·	·	·	·	8	1.8	38.5	2.7	32	3.3	13.5	4.0	1	3.0	25.7	9.6	30	·	·	8	·	1	1	1	14	13	6	·	5	2	·
IV	5.6	1.4	5.5	2.1	11.5	1.7	17.5	2.1	7.5	1.4	7	1.9	7.5	2.7	10	3.2	18	1.7	25.7	6.5	8	·	·	2	·	1	1	13	8	11	7	·	2	1	2
V	4.5	2.6	3.5	1.7	2.5	1.2	5.5	1.4	11	1.7	15.5	1.8	11	2.1	17.5	2.1	22	1.4	56.0	7.8	7	·	·	·	2	·	·	·	18	17	14	·	·	·	6
VI	·	·	4	1.2	4.5	1.4	12.5	1.6	13	1.7	14	1.8	16	1.8	7	2.1	19	1.4	52.3	11.2	11	·	·	·	15	·	·	2	8	14	12	1	2	·	8
VII	1	2.5	1	1.0	1.5	1.0	3.5	2.3	9.5	1.5	36	1.4	12	1.6	6.5	1.7	22	1.2	71.4	18.5	28	·	·	·	7	·	·	3	17	20	13	2	3	·	2
VIII	1.5	1.0	2	1.0	1.5	1.0	2	1.0	9	1.2	30.5	1.5	15	1.4	10.5	1.6	21	1.1	45.9	18.2	10	·	·	·	5	·	·	1	14	13	11	1	1	·	2
IX	0.5	2.0	2	1.2	6	1.4	6.5	1.4	5.5	1.2	22	1.5	12.5	1.8	5	1.6	30	1.0	29.7	11.5	14	·	·	·	5	·	·	8	4	6	4	1	2	·	2
X	·	·	0.5	3.0	12	2.1	21	2.6	13.5	2.6	5.5	2.4	3.5	3.0	6	3.6	31	1.7	7.0	2.8	29	·	·	·	·	·	·	5	13	6	3	·	10	·	·
XI	8.5	3.6	5	2.1	8.5	3.2	10	1.8	7.5	1.7	18.5	2.0	8.5	2.4	6.5	2.3	17	1.9	64.1	12.3	4	·	1	10	·	·	·	1	24	16	14	1	12	·	·
XII	9	5.9	4.5	3.6	2.5	1.6	4.5	1.2	6	1.8	13.5	2.2	15.5	2.6	9.5	4.3	28	2.2	20.2	6.8	11	—	14	—	·	3	·	6	17	9	5	·	5	20	·
Rok	38.5	1.9	33.5	1.7	57	1.4	104.5	1.5	131	1.6	237.5	1.8	153.5	2.1	107.5	2.4	232	1.6	446.9	18.5	28.VII	—	30	—	34	5	2	46	172	144	104	7	64	50	22

Siemiatycze

$\varphi = 52°26'$ $\lambda = 22°52'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−1.8	−7.2	7.4	4	−24.4	26	−5.1	−2.7	−4.4	−4.2	4.2	4.6	4.3	4.4	89	86	88	88	0.4	0.7	0.4	0.5	7.5	7.4	6.1	7.0
II	–	–	–	–	2.3	−1.6	8.8	18	−5.4	6	−0.3	1.8	0.5	0.6	5.5	6.2	5.8	5.8	91	89	91	90	0.5	0.8	0.6	0.6	9.0	8.4	6.2	7.9
III	–	–	–	–	8.1	0.5	15.7	10	−3.5	20	2.5	6.7	4.0	4.3	6.6	7.1	7.0	6.9	89	72	85	82	0.9	2.9	1.3	1.7	8.0	7.3	6.1	7.1
IV	–	–	–	–	15.1	3.6	24.3	15	−4.5	10	6.5	13.5	8.8	9.4	7.7	8.2	8.2	8.0	76	53	71	67	2.3	8.3	3.6	4.7	5.5	5.5	3.7	4.9
V	–	–	–	–	17.2	7.0	26.4	29	1.9	19	10.3	15.8	11.1	12.1	10.9	10.8	11.1	10.9	86	62	84	77	1.9	8.0	2.4	4.1	6.9	7.0	6.3	6.7
VI	–	–	–	–	24.1	12.5	33.6	27	6.7	21	17.0	22.5	17.4	18.5	15.3	14.3	14.8	14.8	79	55	75	70	4.3	13.8	5.3	7.8	5.5	6.2	6.1	5.9
VII	–	–	–	–	22.2	11.3	31.3	3	6.7	6	15.5	20.1	15.9	16.9	14.4	14.2	14.5	14.4	82	60	81	74	3.4	10.5	3.8	5.9	5.3	7.2	6.7	6.4
VIII	–	–	–	–	21.7	12.2	31.5	7	8.5	18, 31	14.7	20.2	15.5	16.5	14.8	15.0	15.3	15.0	88	64	86	79	2.1	10.4	2.6	5.0	6.1	6.5	5.5	6.0
IX	–	–	–	–	20.1	8.7	29.8	3	1.9	23, 28	10.7	19.3	12.7	13.9	12.2	12.9	13.1	12.7	92	57	87	79	1.1	10.3	2.0	4.5	4.6	3.5	2.1	3.4
X	–	–	–	–	15.0	5.4	19.8	4	0.3	23	6.8	14.2	9.8	10.1	8.9	10.0	9.5	9.5	89	63	78	77	1.1	6.4	2.7	3.4	6.1	5.0	3.5	4.9
XI	–	–	–	–	5.1	0.9	12.7	3	−7.1	23	2.5	4.4	2.8	3.1	7.1	7.7	7.0	7.3	93	90	92	92	0.5	1.0	0.7	0.7	9.2	8.8	7.2	8.4
XII	–	–	–	–	1.3	−7.5	14.5	5	−22.1	27	−4.6	−2.8	−4.6	−4.2	4.3	4.8	4.4	4.5	86	84	87	86	0.6	0.8	0.6	0.7	8.9	7.6	5.7	7.4
Rok	–	–	–	–	12.3	3.9	33.6	27.VI	−24.4	26.I	6.4	11.1	7.5	8.1	9.3	9.6	9.6	9.5	87	70	84	80	1.6	6.2	2.2	3.3	6.9	6.7	5.4	6.3

Legionowo

$\varphi = 52°24'$ $\lambda = 20°58'$

I	1007.3	1030.4	988.6	1020.7	−0.1	−6.2	6.8	4	−21.0	26	−4.5	−1.5	−3.2	−3.1	4.4	4.8	4.7	4.6	92	83	90	88	0.4	0.9	0.5	0.6	7.5	7.2	6.6	7.1
II	1009.1	1025.0	982.1	1022.3	3.7	−0.5	10.6	18	−4.5	5	0.5	2.7	1.3	1.4	6.0	6.4	6.2	6.2	94	86	92	91	0.4	1.1	0.6	0.7	9.1	8.3	7.6	8.3
III	1002.7	1022.4	980.0	1015.5	9.4	2.0	17.4	10	−2.3	23	3.3	7.1	5.1	5.1	6.8	6.9	7.1	6.9	88	69	80	79	1.1	3.5	1.9	2.2	8.8	7.8	5.3	7.3
IV	1001.2	1013.3	990.2	1013.8	15.5	4.1	24.4	15	−3.0	10	6.6	14.0	9.5	9.9	7.9	7.6	8.3	7.9	79	47	67	64	2.1	9.4	4.0	5.2	5.7	5.7	3.6	5.0
V	999.7	1007.2	986.7	1012.2	17.3	7.1	26.4	27	2.6	15	10.3	15.5	11.7	12.3	10.4	9.6	10.8	10.3	82	56	78	72	2.4	8.6	3.3	4.8	7.4	7.7	6.7	7.3
VI	1002.7	1015.2	992.6	1014.9	24.2	12.5	33.7	27	5.9	21	16.6	21.9	17.7	18.5	14.7	13.5	14.9	14.4	77	54	73	68	4.4	13.4	5.6	7.8	5.3	6.6	4.8	5.6
VII	1001.0	1013.7	985.8	1013.3	21.5	11.5	31.6	3	7.5	20	14.5	19.8	16.2	16.7	13.9	13.1	14.4	13.8	84	59	79	74	2.8	10.8	4.3	6.0	7.0	7.9	6.7	7.2
VIII	1003.4	1017.1	991.7	1015.7	21.1	12.4	30.9	6	8.1	18	14.5	19.8	16.2	16.7	14.4	14.1	15.1	14.5	87	62	81	77	2.3	9.7	3.7	5.2	6.7	7.5	5.2	6.5
IX	1006.7	1018.7	993.6	1019.3	20.2	9.2	28.7	2, 3	1.5	23	10.8	19.4	13.7	14.4	12.0	12.5	13.1	12.5	90	55	82	76	1.4	10.7	2.9	5.0	4.9	4.8	2.8	4.2
X	1007.7	1019.7	983.1	1020.4	15.2	5.5	22.3	19	0.3	31	6.9	14.3	10.3	10.4	9.1	10.3	9.9	9.8	91	64	80	78	1.0	6.4	2.8	3.4	6.5	6.0	4.1	5.5
XI	1002.2	1023.9	990.5	1015.1	5.9	0.9	13.2	3	−9.5	23	2.3	4.9	3.3	3.5	7.1	7.6	7.4	7.4	96	87	93	92	0.4	1.3	0.6	0.8	7.8	8.5	6.8	7.7
XII	1003.1	1032.4	980.7	1016.5	−0.6	−6.7	15.4	5	−23.3	26	−4.4	−2.4	−3.7	−3.6	4.5	4.8	4.6	4.6	89	83	90	87	0.6	1.1	0.6	0.8	7.5	7.5	5.6	6.9
Rok	1003.9	1032.4	980.0	1016.7	12.8	4.3	33.7	27.VI	−23.3	26.XII	6.4	11.3	8.2	8.5	9.3	9.3	9.7	9.4	87	67	82	79	1.6	6.4	2.6	3.5	7.0	7.1	5.5	6.5

Słubice

$\varphi = 52°21'$ $\lambda = 14°36'$

I	1014.9	1038.7	990.0	1017.7	1.4	−5.6	7.8	30	−23.3	27	−3.6	0.1	−2.3	−2.0	4.7	4.9	4.8	4.8	89	74	84	82	0.6	1.5	0.9	1.0	5.7	6.4	5.3	5.8
II	1017.5	1034.1	987.7	1020.4	8.0	0.9	14.7	15	−4.3	6	2.5	6.6	3.9	4.2	6.8	7.5	7.3	7.2	91	76	89	85	0.7	2.5	0.9	1.4	7.7	7.3	6.3	7.1
III	1015.8	1034.0	986.7	1018.6	10.9	2.7	18.4	10	−6.0	20	4.1	9.1	6.5	6.6	7.4	7.5	7.6	7.5	88	65	78	77	1.1	4.4	2.3	2.6	7.0	7.0	5.6	6.5
IV	1008.6	1020.3	999.1	1011.3	16.3	4.9	26.2	14	−0.4	1	7.5	14.6	9.9	10.5	8.9	9.3	9.5	9.2	84	57	76	72	1.7	8.1	3.0	4.3	5.5	5.2	5.1	5.3
V	1009.8	1019.7	996.6	1012.5	15.6	6.7	24.0	26	2.2	18	9.4	13.9	10.3	11.0	10.5	10.5	10.8	10.6	88	67	85	80	1.4	5.8	1.9	3.0	7.9	8.1	6.1	7.4
VI	1012.0	1026.8	997.9	1014.8	23.3	12.2	30.0	26	6.1	22	15.6	21.6	17.0	17.8	14.4	13.8	15.0	14.4	81	54	77	71	3.5	12.4	4.7	6.9	4.8	5.8	4.8	5.1
VII	1010.1	1022.8	994.5	1012.7	20.9	12.5	32.5	3	8.2	17	14.5	18.7	15.9	16.2	14.1	13.1	14.1	13.8	85	63	78	75	2.6	9.3	4.3	5.4	8.1	7.9	7.7	7.9
VIII	1012.9	1025.5	1001.0	1015.5	21.3	11.9	28.7	6	6.7	8	14.2	19.6	15.7	16.3	14.7	14.7	15.0	14.8	91	65	83	80	1.6	8.6	3.4	4.5	6.7	6.9	5.2	6.3
IX	1014.7	1024.7	999.7	1017.3	22.0	9.6	30.4	2, 17	−1.4	24	11.1	20.8	14.4	15.2	12.9	14.4	13.9	13.7	95	59	84	79	0.8	10.9	2.8	4.8	3.8	4.4	3.2	3.8
X	1013.5	1028.1	983.0	1016.2	16.2	6.8	23.1	6	1.3	14	8.4	15.3	10.7	11.3	10.1	11.2	10.8	10.7	92	66	85	81	1.1	6.5	2.2	3.3	5.6	5.3	5.5	5.5
XI	1011.3	1034.5	996.0	1014.1	6.9	1.1	14.1	2	−8.4	22	2.4	5.8	3.4	3.8	7.1	8.1	7.4	7.5	94	86	93	91	0.5	1.3	0.7	0.8	7.2	8.4	6.6	7.4
XII	1013.2	1044.4	986.4	1016.0	1.6	−6.0	15.8	5	−21.2	26	−2.9	−0.2	−2.4	−2.0	5.2	5.4	5.0	5.2	89	82	87	86	0.7	1.3	0.9	1.0	6.3	6.6	6.4	6.4
Rok	1012.9	1044.4	983.0	1015.6	13.7	4.8	32.5	3.VII	−23.3	27.I	6.9	12.2	8.6	9.1	9.7	10.0	10.1	9.9	89	68	83	80	1.4	6.0	2.3	3.2	6.4	6.6	5.6	6.2

Paproć

$\varphi = 52°19'$ $\lambda = 16°08'$

I	–	–	–	–	0.6	−6.1	6.5	30	−19.3	27	−4.3	−0.6	−3.2	−2.8	4.3	4.7	4.5	4.5	85	75	84	81	0.6	1.4	0.7	0.9	–	–	–	–
II	–	–	–	–	6.6	0.1	12.7	15	−4.5	6	1.7	5.1	2.8	3.1	6.5	7.2	6.9	6.9	92	82	92	89	0.6	1.8	0.7	1.0	7.4	6.9	6.8	7.0
III	–	–	–	–	10.3	1.9	19.2	10	−6.9	20	3.6	8.8	5.3	5.8	7.1	7.5	7.4	7.3	89	67	82	79	1.0	4.2	1.7	2.3	7.6	5.7	5.4	6.2
IV	–	–	–	–	15.9	4.8	25.3	7	−1.3	1	7.3	14.0	9.6	10.1	8.6	9.7	9.5	9.3	82	61	78	74	1.8	7.1	2.8	3.9	4.4	4.8	3.3	4.2
V	–	–	–	–	16.0	6.7	22.2	5, 26	1.1	13	9.6	13.7	10.6	11.1	10.6	10.4	10.8	10.6	88	68	84	80	1.5	5.6	2.3	3.1	6.8	7.9	6.0	6.9
VI	–	–	–	–	23.2	11.5	29.2	26	4.5	22	16.2	21.5	17.1	18.0	14.7	14.2	15.2	14.7	79	55	78	71	4.1	11.5	4.6	6.7	3.6	4.1	4.9	4.2
VII	–	–	–	–	20.8	11.7	32.6	3	7.5	8	14.7	19.9	15.0	15.9	14.5	14.2	14.4	14.4	86	66	85	79	2.6	8.5	2.8	4.6	7.4	7.7	6.5	7.2
VIII	–	–	–	–	21.0	11.2	30.0	6	5.8	4	14.0	19.4	14.8	15.8	14.8	15.2	15.1	15.0	92	68	88	83	1.4	8.0	2.0	3.8	6.2	6.2	4.1	5.5
IX	–	–	–	–	21.0	9.3	30.3	2	1.4	24	11.4	20.1	13.5	14.6	12.6	14.3	13.3	13.4	92	60	85	79	1.1	10.0	2.4	4.5	3.7	3.7	3.5	3.6
X	–	–	–	–	15.8	6.7	21.8	10	−0.7	13	8.0	14.7	9.7	10.5	9.9	11.5	10.6	10.7	92	70	89	84	1.0	5.6	1.6	2.7	5.3	4.7	4.9	5.0
XI	–	–	–	–	6.6	1.0	13.2	2	−9.1	23	2.2	5.8	3.2	3.6	6.9	7.7	7.3	7.3	92	83	92	89	0.6	1.7	0.6	1.0	7.1	7.3	6.1	6.8
XII	–	–	–	–	0.8	−7.1	16.2	5	−23.7	26	−4.0	−1.0	−3.6	−3.0	4.8	5.0	4.7	4.8	89	79	87	85	0.6	1.4	0.7	0.9	6.6	6.2	5.9	6.2
Rok	–	–	–	–	13.2	4.3	32.6	3.VII	−23.7	26.XII	6.7	11.7	7.9	8.6	9.6	10.1	10.0	9.9	88	70	85	81	1.4	5.6	1.9	3.0	–	–	–	–

Siemiatycze $H_s = 145\,m$ $h_w = 16\,m$ **1961**

MIESIĄC	ROZKŁAD WIATRU n, v																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v		◔	●	Opad R			≡	⊞	ℝ
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15			R ≥ 0.1	R ≥ 1.0	R ≥ 10.0			
I	18.5	1.4	3.5	1.3	7.5	2.0	7	1.3	21.5	2.1	15	2.0	8	1.7	9	1.8	3	1.7	52.4	13.0	4	13	15	28	·	·	·	2	14	16	11	2	3	24	·
II	1	1.0	1	3.0	4	1.5	10.5	2.0	15	2.3	16.5	1.3	15.5	1.2	11.5	1.1	9	1.4	16.9	5.8	28	·	2	20	·	·	·	1	17	16	4	·	15	10	·
III	·	·	·	·	·	·	1	3.0	9	2.1	18	4.0	36.5	3.4	24.5	3.2	4	3.3	34.0	10.8	30	·	·	13	·	3	2	1	11	22	8	1	9	1	·
IV	10	1.5	9.5	1.4	21	3.3	5	1.8	11.5	1.8	5.5	1.9	7	5.5	11.5	2.3	9	2.3	30.7	11.7	16	·	·	6	·	1	1	10	7	7	6	1	2	·	1
V	6	1.6	1	2.0	10.5	1.7	13.5	1.2	8	1.1	8.5	2.0	20	1.8	12.5	1.7	13	1.4	86.3	21.2	7	·	·	·	3	·	·	1	10	17	14	2	1	·	1
VI	3.5	1.0	12	1.6	14.5	1.5	9.5	1.3	3	1.0	21	1.9	13.5	1.6	7	1.2	6	1.4	54.7	16.4	12	·	·	·	14	·	·	3	9	12	8	1	·	·	3
VII	9.5	1.1	1.5	1.0	6	1.3	5	1.5	12.5	1.8	18	1.6	29.5	2.0	7	1.7	4	1.6	122.9	42.3	19	·	·	·	7	·	·	3	10	12	10	4	·	·	3
VIII	1.5	1.0	3	1.0	3	1.0	1.5	1.0	12	1.3	21	2.3	30	2.0	15	1.5	6	1.7	117.5	26.2	11	·	·	·	6	·	·	4	7	18	13	5	1	·	4
IX	1	1.0	8.5	1.1	11.5	1.7	5	1.4	7.5	1.3	17	1.8	21.5	1.9	8	1.4	10	1.4	46.7	12.6	14	·	·	·	6	·	·	13	4	11	8	2	7	·	1
X	1	1.0	7	2.9	22	2.5	31.5	2.7	6	1.9	7	1.3	10	2.0	6.5	1.9	2	2.3	7.0	3.5	14	·	·	·	·	2	2	7	7	3	2	·	8	·	·
XI	3	1.7	7.5	1.7	20.5	3.0	13.5	1.8	11.5	1.5	12.5	2.4	11.5	1.8	7	1.7	3	2.0	66.5	12.1	12	·	1	16	·	·	·	·	21	19	12	1	10	·	·
XII	10.5	1.8	4	2.2	9.5	2.0	13.5	1.3	9	1.7	13.5	3.9	13.5	2.8	18.5	1.7	1	2.2	27.9	9.2	1	12	16	25	·	·	·	2	17	18	6	·	3	20	·
Rok	65.5	1.2	58.5	1.6	130	1.8	116.5	1.7	126.5	1.7	173.5	2.2	216.5	2.3	138	1.8	70	1.9	663.5	42.3	19 VII	25	34	108	36	6	5	47	134	171	102	19	59	55	13

Legionowo $H_s = 93\,m$ $H_b = 103{,}7\,m$ $h_w = 10\,m$

I	5	3.0	5	4.1	3	2.2	12	2.5	19.5	3.2	22	4.3	15.5	3.5	6	3.1	5	3.2	29.8	11.9	31	10	13	26	·	1	·	4	15	16	8	1	4	20	·
II	·	·	1.5	3.0	5.5	2.5	11	3.1	16.5	4.5	17.5	3.4	18	4.0	3	2.3	11	3.0	17.8	6.5	9	·	1	18	·	1	·	1	19	11	6	·	11	6	·
III	·	·	·	·		·	·	·	4	6.1	30.5	5.7	47	6.8	8.5	5.0	3	6.0	31.3	12.2	30	·	·	11	·	15	1	·	11	16	7	1	4	5	·
IV	2.5	3.0	8	3.2	27.5	4.2	9.5	4.1	5.5	3.4	9.5	4.7	13	6.1	5.5	2.5	9	3.9	26.2	5.3	2	·	·	5	·	4	·	9	8	11	9	·	·	1	2
V	4.5	2.9	6	2.5	10.5	2.2	6.5	3.2	12	2.9	15	3.3	14	3.2	12.5	2.7	12	2.5	31.4	7.2	7	·	·	·	2	2	·	·	10	16	9	·	·	·	5
VI	2	4.2	3	4.2	10	2.8	8	2.5	9	2.8	18	3.6	22	4.3	2	4.5	16	2.9	78.5	21.2	23	·	·	·	15	1	1	1	3	15	11	3	1	·	9
VII	0.5	3.0	3	1.8	3	3.2	5	4.4	12	3.7	40.5	4.2	17	4.1	7	3.0	5	3.7	74.2	24.7	28	·	·	·	6	1	·	3	14	18	11	2	2	·	4
VIII	2.5	1.8	0.5	3.0	3	4.0	2	1.5	7.5	2.3	30.5	4.2	29	4.0	7	3.1	11	3.3	75.5	25.9	12	·	·	·	6	1	·	2	9	14	8	3	1	·	3
IX	3	2.0	9	1.9	13.5	2.1	5.5	2.5	6.5	2.5	20.5	3.4	19.5	3.9	3.5	3.0	9	2.7	27.5	11.1	14	·	·	·	5	1	·	10	4	4	3	1	1	·	·
X	·	·	2	3.2	30.5	3.9	21	4.3	17	3.1	5	3.4	8	4.0	3.5	1.7	6	3.5	5.6	2.0	29	·	·	·	·	1	·	7	10	4	3	·	7	·	·
XI	3	4.3	7	4.0	11.5	5.8	12	3.2	9.5	3.8	18	5.0	16.5	3.8	4.5	3.7	8	3.9	58.4	12.3	4	·	2	11	·	1	·	1	17	15	10	2	7	·	·
XII	7	4.9	7.5	4.5	4.5	3.1	6	2.6	9	2.9	20	5.9	18	3.9	8	4.3	13	3.7	15.8	5.1	11	9	14	24	·	5	·	2	14	14	4	·	4	18	·
Rok	30	2.4	52.5	3.0	122.5	3.0	98.5	2.8	128	3.4	247	4.3	237.5	4.3	71	3.2	108	3.5	472.0	25.9	12 VIII	19	30	95	34	34	2	40	134	154	89	13	42	50	23

Słubice $H_s = 20\,m$ $H_b = 22{,}2\,m$ $h_w = 10\,m$

I	1	1.0	2	4.0	5.5	2.9	6.5	2.6	17.5	2.4	28	4.3	12.5	2.8	5	3.3	15	2.8	42.4	6.9	14	10	9	19	·	1	·	8	12	17	11	·	4	15	·
II	0.5	5.0	·	·	5	2.1	5.5	2.6	13	3.2	26.5	4.3	13.5	4.7	11	4.2	9	3.5	21.8	6.2	9	·	·	9	·	4	·	3	16	13	6	·	5	·	·
III	2	5.2	·		·				1.5	4.3	15.5	3.9	49.5	5.7	19.5	4.9	5	4.9	46.4	16.4	30	·	·	7	·	9	·	4	11	16	10	1	5	·	·
IV	10.5	2.5	10.5	2.2	14.5	2.4	11.5	3.6	5.5	2.7	11	3.0	12.5	2.8	6	3.0	8	2.5	39.5	9.7	7	·	·	1	1	·	·	9	9	9	8	·	3	·	2
V	17.5	3.5	2.5	3.4	1	2.0		·	5	3.0	16	3.4	20	3.9	20	3.4	11	3.1	143.3	38.9	29	·	·	·	·	2	·	·	16	23	19	4	1	·	7
VI	5	2.5	2	1.5	6	1.8	3	2.8	9	1.7	10.5	2.6	20.5	4.4	20	4.2	14	2.8	23.9	7.0	12	·	·	·	10	1	·	3	3	7	7		·	·	7
VII	1	1.0	·	·	1	2.0	1	3.0	3	1.5	32.5	3.2	36.5	3.9	12	3.6	6	3.2	68.4	8.3	21	·	·	·	4	4	1	2	19	17	14	·	·	·	6
VIII	2.5	3.2	2	1.2	3	1.7	3.5	2.0	4.5	1.9	26	3.2	33.5	4.0	11	3.8	7	3.1	64.2	15.3	16	·	·		5	2	·	5	11	15	11	2	1	·	3
IX	1.5	1.7	2.5	1.8	10.5	2.0	3.5	2.7	12	1.8	16.5	2.3	16.5	4.4	3	4.7	24	2.0	25.7	6.6	5	·	·	·	8	2	2	14	7	8	6	·	3	·	2
X	1.5	3.3	0.5	4.0	15	4.2	9	4.6	22	2.7	22.5	2.6	5.5	3.3	2	4.0	15	2.7	49.0	19.8	20	·	·	·	·	1	·	6	10	12	7	2	2	·	·
XI	4.5	2.4	7.5	2.5	10.5	4.4	3.5	1.1	8	2.2	22.5	3.4	14.5	3.8	4	2.9	15	2.7	57.0	23.1	13	·	·	9	·	3	·	2	14	16	9	1	6	·	·
XII	4.5	4.8	5	2.6	9	2.4	2.5	2.2	13.5	2.5	22	3.9	16.5	5.1	5	3.9	15	3.1	35.3	12.6	1	8	11	21	·	5	·	5	14	11	7	1	4	12	·
Rok	52	3.0	34.5	1.9	81	2.3	49.5	2.3	114.5	2.5	249.5	3.3	251.5	4.1	118.5	3.8	144	3.0	616.9	38.9	29.V	18	20	66	28	34	3	61	142	164	115	11	34	27	27

Paproć $H_s = 75\,m$ $h_w = 11\,m$

I	·	·	2	1.5	21	2.0	21	1.6	13.5	2.1	17	2.6	11.5	2.1	2	1.8	5	1.9	38.2	13.2	14	11	11	24	·	·	·	–	–	14	8	1	2	17	·
II	2	2.5	·	·	10.5	2.9	15	2.3	8.5	1.8	13.5	2.9	20.5	2.1	10	3.1	4	2.4	29.6	11.0	9	·	·	13	·	·	·	–	–	16	9	1	8	1	·
III	0.5	3.0	0.5	3.0	·	·	·	·	0.5	1.0	19	3.9	52	4.1	9.5	3.8	11	3.5	44.8	10.9	30	·	·	9	·	6	·	–	–	17	13	1	7	·	·
IV	5.5	2.0	9	2.9	29.5	3.0	11.5	2.8	5	1.8	3	1.7	9.5	2.4	12	1.9	5	2.4	48.6	9.0	15	·	·	2	1	·	·	–	–	12	10	·	1	·	3
V	10.5	2.5	7.5	2.5	8	1.8	2	1.5	7	1.9	19.5	2.9	15.5	2.5	19	2.7	4	2.4	106.1	25.6	5	·	·	·	·	·	·	–	–	21	20	3	2	·	7
VI	2	2.0	4	1.9	10	2.0	5	2.2	2	3.0	10	1.8	32.5	2.7	9.5	2.1	15	1.9	46.1	23.2	4	·	·	·	9	·	·	–	–	7	5	1	·	·	2
VII	1	1.0	1	1.0	2	2.5	1	1.0	5	1.8	34.5	2.5	29	2.2	9.5	2.1	10	2.0	87.1	20.6	31	·	·	·	5	·	·	–	–	19	15	3	·	·	3
VIII	4	1.8	2	1.8	3	1.8	3	1.3	3	2.0	29	2.3	25	2.2	7	1.7	17	1.7	48.7	12.3	6	·	·	·	4	·	·	–	–	17	12	1	10	·	2
IX	0.5	1.0	2	2.8	21.5	2.1	2	1.8	2.5	2.6	19	2.2	11.5	2.2	5	2.4	26	1.5	41.3	20.6	5	·	·	·	7	·	·	–	–	8	5	2	6	·	2
X	2.5	2.6	1.5	4.3	25	3.0	13	1.9	14	1.6	14.5	1.4	3.5	2.3	4	1.8	15	1.8	23.0	4.6	29	·	·	1	·	·	·	–	–	13	8	·	12	·	·
XI	8	1.5	10	2.7	8	3.2	5	1.2	5.5	1.7	17.5	2.0	11	1.9	5	2.4	20	1.7	35.6	18.3	13	·	·	9	·	·	·	–	–	14	6	1	11	·	·
XII	3.5	1.6	12.5	1.6	6	1.7	10	1.7	8.5	1.8	18	3.0	7.5	2.5	5	2.6	22	1.6	55.8	17.2	11	9	13	23	·	·	·	–	–	15	11	2	2	17	·
Rok	40	1.8	52	2.2	144.5	2.2	88.5	1.6	75	1.9	214.5	2.4	229	2.4	97.5	2.4	154	2.1	604.9	25.6	5.V	20	24	81	26	6	·	–	–	173	122	16	61	35	19

Ostrowy — φ = 52°18' — λ = 19°10' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.4	-5.9	6.0	4	-19.0	26	-4.4	-1.4	-3.3	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.3	6.3	6.6
II	–	–	–	–	4.4	0.0	11.1	18	-3.6	6	0.8	3.3	1.8	1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	6.8	8.0	7.8
III	–	–	–	–	9.2	2.2	16.3	10	-3.6	20	3.3	7.2	5.2	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	6.9	7.0
IV	–	–	–	–	15.3	4.4	24.6	7	-1.4	1	6.5	13.5	9.1	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	4.2	5.5	5.2
V	–	–	–	–	16.6	6.5	23.0	27	0.1	13	9.6	14.9	10.7	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	7.2	6.6
VI	–	–	–	–	23.3	12.6	27.7	25	5.9	21	16.2	21.9	16.8	17.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.7	11.2	32.0	3	6.8	6	14.3	18.9	14.4	15.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.9	11.9	29.7	6	6.5	30	14.0	19.1	14.9	15.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.4	9.1	28.6	17	1.3	28	10.9	19.0	12.3	13.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.0	–	19.4	6	–	–	7.7	13.7	10.2	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.1	1.4	12.1	3	-6.3	23	2.4	4.6	3.3	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.2	8.4	8.3
XII	–	–	–	–	-0.6	-6.8	15.4	5	-21.3	26	-4.1	-2.6	-4.3	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.1	7.3	7.5
Rok	–	–	–	–	12.6	–	32.0	3.VII	-21.3	26.XII	6.4	11.0	7.6	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Słupca — φ = 52°17' — λ = 17°52'

I	–	–	–	–	0.0	-5.3	5.8	4	-16.9	27	-4.5	-1.1	-3.2	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.6	5.6	5.8
II	–	–	–	–	5.1	0.0	10.8	18	-3.5	6	1.1	4.1	1.7	2.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.7	6.2	7.6
III	–	–	–	–	9.4	2.1	17.2	10	-3.3	20	3.6	8.0	5.0	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.6	5.7	7.0
IV	–	–	–	–	15.3	4.9	24.5	7	-0.5	1	6.9	13.9	9.4	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.7	4.4	4.7
V	–	–	–	–	16.0	6.7	21.6	26	2.0	12, 13	10.0	14.6	10.5	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.1	5.8	7.0
VI	–	–	–	–	23.5	12.3	29.4	27	6.1	22	16.4	22.2	16.5	17.9	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.6	4.7	4.8
VII	–	–	–	–	20.6	11.6	32.5	3	7.8	6	14.7	18.9	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.1	7.0	7.7
VIII	–	–	–	–	20.7	11.9	29.7	6	7.8	18	14.6	19.4	14.9	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	4.9	6.5
IX	–	–	–	–	20.7	9.8	29.2	2	3.8	25	11.9	20.0	13.5	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.0	3.8	4.3
X	–	–	–	–	15.1	6.8	21.1	6	2.2	13	8.0	14.5	9.9	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	4.5	5.7
XI	–	–	–	–	6.0	1.7	12.4	2, 3	-6.2	23	2.8	5.2	3.0	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.4	6.8	7.9
XII	–	–	–	–	-0.6	-6.9	15.1	5	-21.4	26	-3.9	-2.1	-4.3	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.0	6.4	7.2
Rok	–	–	–	–	12.6	4.6	32.5	3.VII	-21.4	26.XII	6.8	11.5	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	5.5	6.4

Warszawa - Bielany — φ = 52°17' — λ = 20°58'

I	1007.3	1030.4	989.0	1020.7	-0.1	-5.2	6.9	4	-18.1	26	-4.0	-1.4	-2.6	-2.6	4.2	4.6	4.5	4.4	85	79	82	82	0.7	1.1	0.9	0.9	7.6	7.4	6.8	7.3
II	1009.2	1024.5	981.8	1022.4	3.7	0.2	10.1	18	-4.2	6	0.8	2.8	1.7	1.8	5.9	6.3	6.1	6.1	90	84	87	87	0.6	1.2	0.9	0.9	9.0	8.4	7.2	8.2
III	1002.8	1022.6	979.7	1015.7	9.2	2.4	16.5	10	-1.8	20	3.4	7.3	5.4	5.4	6.8	7.1	7.1	7.0	87	70	78	78	1.2	3.4	2.1	2.2	9.1	7.9	5.9	7.6
IV	1001.4	1013.1	990.0	1014.1	15.6	5.1	24.1	15	-1.5	10	7.0	13.9	10.3	10.4	8.0	8.2	8.5	8.2	77	51	65	64	2.4	8.6	4.6	5.2	5.5	5.7	3.4	4.9
V	999.7	1007.4	986.2	1012.3	17.2	8.1	26.1	27	4.1	13	10.4	15.6	12.1	12.5	10.3	9.7	10.7	10.2	81	56	76	71	2.6	8.6	3.7	5.0	7.2	8.0	6.3	7.2
VI	1002.8	1015.2	992.5	1015.1	23.9	13.7	33.4	27	9.0	21	16.5	22.2	18.1	18.7	14.8	13.4	14.5	14.2	79	52	70	67	4.2	13.9	6.5	8.2	5.2	7.1	5.0	5.8
VII	1001.0	1013.8	984.9	1013.4	21.2	12.6	31.5	3	8.8	6	14.8	19.6	16.2	16.7	13.9	13.6	14.1	13.9	83	61	77	74	3.1	9.9	4.6	5.9	7.0	8.2	6.1	7.1
VIII	1003.7	1017.5	992.0	1016.1	21.1	13.0	30.7	6	8.9	30	14.6	19.7	16.3	16.7	14.4	14.3	15.1	14.6	86	63	81	77	2.5	9.3	3.8	5.2	6.6	7.4	5.6	6.5
IX	1006.8	1018.7	993.5	1019.4	20.2	10.4	29.0	3	2.2	24	11.7	19.1	14.1	14.8	12.0	12.1	12.9	12.3	86	55	78	73	2.2	10.7	3.7	5.5	5.1	5.0	3.4	4.5
X	1007.7	1020.1	983.1	1020.4	15.2	7.1	22.3	19	3.4	29	7.9	14.3	11.1	11.1	9.0	9.8	9.6	9.5	85	62	74	74	1.8	6.8	3.7	4.1	6.3	6.5	3.5	5.4
XI	1002.3	1024.0	990.4	1015.3	6.1	1.7	12.9	3	-6.2	23	2.6	5.1	4.0	3.9	7.1	7.4	7.3	7.3	92	83	88	88	0.6	1.6	1.0	1.1	8.4	8.7	7.4	8.2
XII	1003.1	1033.0	981.1	1016.5	-0.4	-6.0	15.4	5	-20.1	26	-3.7	-2.2	-3.2	-3.1	4.5	4.7	4.5	4.6	84	80	85	83	0.9	1.2	0.8	1.0	8.1	7.5	6.5	7.4
Rok	1004.0	1033.0	979.7	1016.8	12.7	5.3	33.4	27.VI	-20.1	26.XII	6.8	11.3	8.6	8.8	9.2	9.3	9.6	9.4	85	66	78	76	1.9	6.4	3.0	3.8	7.1	7.3	5.6	6.7

Warszawa, Inst. Geogr. UW — φ = 52°14' — λ = 21°01'

I	–	–	–	–	0.0	-4.8	6.8	4	-15.6	26	-3.5	-1.1	-2.2	-2.2	4.2	4.6	4.5	4.4	82	76	79	79	0.8	1.3	1.1	1.1	7.9	8.4	6.9	7.7
II	–	–	–	–	3.9	0.5	9.2	18	-3.3	6	1.2	3.1	2.2	2.2	6.0	6.4	6.2	6.2	89	84	87	87	0.8	1.3	1.0	1.0	9.2	8.4	7.7	8.4
III	–	–	–	–	9.2	2.9	15.9	18	-1.4	20	3.9	7.4	6.0	5.8	6.9	7.3	7.2	7.1	85	70	76	77	1.3	3.3	2.4	2.3	9.7	8.6	6.2	8.2
IV	–	–	–	–	15.7	5.5	24.2	15	-0.1	1	7.2	14.4	11.2	11.0	8.2	8.7	9.0	8.6	78	51	64	64	2.3	8.6	4.9	5.3	6.4	6.0	3.3	5.2
V	–	–	–	–	17.3	9.0	25.8	27	4.8	13	10.5	16.0	12.8	13.0	11.0	11.2	11.4	11.2	85	62	77	75	1.9	7.5	3.7	4.4	7.7	8.2	6.5	7.5
VI	–	–	–	–	24.0	14.7	33.1	27	10.7	21	16.8	22.6	18.9	19.3	15.7	15.3	16.0	15.7	82	57	73	71	3.5	12.7	6.1	7.4	6.2	7.3	6.0	6.5
VII	–	–	–	–	21.3	13.4	31.0	3	10.0	6	15.1	19.9	17.1	17.3	14.8	15.2	15.3	15.1	86	67	79	77	2.6	8.7	4.6	5.3	8.0	8.6	7.4	8.0
VIII	–	–	–	–	20.9	13.8	30.9	6	9.1	30	14.9	19.9	17.1	17.2	14.4	14.9	15.3	14.9	84	64	78	75	2.8	9.0	4.5	5.4	6.2	7.5	5.3	6.3
IX	–	–	–	–	20.1	11.3	29.3	3	4.8	23	12.1	19.2	15.1	15.4	12.2	12.8	13.2	12.7	85	57	76	73	2.4	10.2	4.4	5.7	6.3	5.3	3.3	5.0
X	–	–	–	–	15.1	7.3	22.2	19	3.5	31	7.9	14.3	11.5	11.3	9.5	10.7	10.6	10.3	89	67	78	78	1.3	5.8	3.1	3.4	7.0	7.2	4.4	6.2
XI	–	–	–	–	6.2	2.1	13.0	3	-5.1	23	3.2	5.2	4.4	4.3	7.3	7.7	7.6	7.5	93	85	88	89	0.6	1.4	1.0	1.0	9.0	9.3	7.8	8.7
XII	–	–	–	–	-0.1	-5.5	15.6	5	-20.6	26	-3.2	-1.9	-2.8	-2.7	4.7	4.8	4.7	4.7	85	79	85	83	0.9	1.3	0.8	1.0	8.0	7.6	6.9	7.5
Rok	–	–	–	–	12.8	5.8	33.1	27.VI	-20.6	26.XII	7.2	11.6	9.3	9.4	9.6	10.0	10.1	9.9	85	68	78	77	1.8	5.9	3.1	3.6	7.6	7.7	6.0	7.1

Ostrowy $H_s = 120\ m$ $h_w = 11\ m$ **1961**

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	⊼
I	1	4.0	10	3.0	9	3.0	17	2.7	27	3.2	12.5	5.6	6	3.5	3.5	3.4	7	3.2	18.0	8.9	31	11	11	27	·	·	·	–	–	6	4	·	2	–	·
II	4	3.8	3.5	3.0	5	2.7	9.5	3.4	24	4.2	19.5	4.0	7.5	4.4	7	3.9	4	3.7	21.7	6.1	9	·	·	16	·	1	·	–	–	11	6	·	9	–	·
III	9	3.5	1.5	2.0	0.5	2.0	0.5	2.0	9	5.2	22	5.5	31.5	5.8	19	5.4	·	5.3	38.3	18.5	30	·	·	9	·	3	·	–	–	11	7	1	7	–	·
IV	6	4.4	15.5	2.9	26	4.3	12.5	3.9	8.5	4.4	4	4.4	5.5	5.1	3	5.7	9	3.7	23.5	4.7	3	·	·	2	·	·	·	–	–	9	6	·	1	–	3
V	7.5	3.8	13.5	3.3	18.5	2.7	12.5	2.6	12.5	3.6	11	3.7	6.5	4.7	2	4.0	9	3.0	49.2	14.7	30	·	·	·	·	·	·	–	–	13	10	1	2	·	5
VI	1	3.0	13.5	2.7	13	2.7	10.5	2.6	9	2.7	16.5	3.9	10.5	4.6	2	3.5	14	2.7	31.0	16.4	4	·	·	·	10	·	·	–	–	6	3	1	·	·	7
VII	2	3.2	5.5	2.4	3.5	2.4	2.5	3.8	21	2.5	25	3.0	22.5	4.4	3	4.3	8	3.0	119.6	28.6	31	·	·	·	7	·	·	–	–	16	14	4	·	·	4
VIII	2.5	3.4	4.5	2.2	10.5	2.5	3.5	2.7	19.5	3.0	12.5	3.8	24	4.0	7	3.0	9	2.9	103.9	40.1	10	·	·	·	4	·	·	–	–	16	10	4	·	·	5
IX	2.5	1.8	25	1.8	25	3.0	5	3.5	16.5	2.9	9	3.0	15	4.3	2.5	3.8	12	2.8	17.1	6.7	14	·	·	·	5		·	–	–	8	3	·	1	·	1
X	·	·	8	3.9	26.5	4.2	2	3.5	22	3.8	17.5	3.6	9	3.8	7	3.0	1	3.8	16.5	5.0	18	·	·	·		·	·	–	–	7	4	·	1	·	
XI	10.5	3.1	5.5	4.5	12	4.2	4	3.1	16	2.7	15	4.3	23	3.8	2	2.5	2	3.6	57.4	12.7	13	·	·	9	·	·	·	·	19	17	11	1	4	·	
XII	9.5	4.0	5	3.1	7	3.2	4.5	3.0	9	4.3	21.5	4.1	24	3.9	12.5	3.4	·	3.8	19.4	6.7	11	10	17	24	·	1	·	·	14	7	6	·	1	–	
Rok	55.5	3.2	88.5	2.9	156.5	3.1	84	3.1	194	3.5	186	4.1	185	4.4	70.5	3.8	75	3.5	515.6	40.1	10.VIII	21	28	86	26	5	·	–	–	127	84	12	28	–	25

Słupca $H_s = 90\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.3	9.1	14	10	11	25	·	–	–	6	15	9	4	·	2	–	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	31.8	11.6	9	·	·	12	·	–	–	1	14	15	9	1	5	–	
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.8	13.4	30	·	·	5	·	–	–	2	14	17	12	1	1	–	1
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	66.4	37.4	16	·	·	2	·	–	–	10	7	11	10	1	1	·	2
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	56.1	12.3	16	·	·	·	·	–	–	·	10	18	11	1	1	·	2
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52.1	13.2	11	·	·	·	10	–	–	4	5	10	8	2	·	·	8
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	184.2	60.1	31	·	·	·	6	–	–	3	18	20	17	4	·	·	6
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	102.9	24.6	11	·	·	·	5	–	–	4	11	14	10	3	1	·	7
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	10.9	5.8	14	·	·	·	7	–	–	12	7	6	2	·	·	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36.2	13.3	18	·	·	·	·	–	–	8	10	10	4	2	2	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41.1	15.2	13	·	·	8	·	–	–	3	19	20	9	1	6	·	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.5	22.0	11	10	16	24	·	–	–	3	13	11	6	1	2	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	691.3	60.1	31.VII	20	27	76	28	–	–	56	143	161	102	17	21	–	27

Warszawa - Bielany $H_s = 101\ m$ $H_b = 104.7\ m$ $h_w = 16\ m$

I	8.5	3.2	5	2.8	1	4.5	8.5	3.6	20	2.9	19	3.9	16	2.9	7	3.0	8	3.0	27.9	9.7	31	9	13	25	·		·	2	16	15	6	·	2	22	·
II	0.5	3.0	1.5	3.0	2	3.2	14.5	2.9	16	3.6	14	3.3	21	3.6	8.5	2.6	6	3.0	15.2	3.8	28	·	·	11	·	·	·	1	19	10	5	·	6	5	·
III	·	·	·	·	·	·	·	·	1	6.0	26	5.1	55	5.2	10	6.0	1	5.2	33.4	16.1	30	·	·	6	·	6	·	·	15	16	6	1	4	3	1
IV	3.5	3.6	4	4.4	16.5	5.4	12	5.1	4.5	3.3	7.5	3.5	12.5	5.0	5.5	4.3	24	3.4	28.4	5.6	15	·	·	4	·	3	·	9	6	10	8	·	1	1	1
V	6	4.0	2.5	3.2	6.5	4.2	7.5	2.9	5.5	3.0	12.5	3.8	13.5	3.0	11	2.8	28	2.3	48.3	16.9	7	·	·	·	2	·	·	·	12	18	11	1	·	·	3
VI	0.5	2.0	5	3.6	7.5	5.1	8	3.8	2.5	2.8	11.5	3.6	22	3.8	5	3.9	28	2.7	64.6	15.5	27	·	·	·	13	1	·	2	4	15	9	3	·	·	9
VII	0.5	2.0	1.5	1.0	3	3.2	3.5	6.0	8	3.3	29.5	3.4	23.5	3.4	5.5	2.6	18	2.7	79.9	19.9	28	·	·	·	7	·	·	1	14	20	14	2	1	·	4
VIII	4.5	2.1	1.5	2.3	1	2.0	4	2.2	3.5	2.4	23.5	3.7	31.5	3.8	6.5	2.3	17	2.7	58.1	16.7	10	·	·	·	5	·	·	2	9	15	9	2	1	·	4
IX	2	1.8	4	2.2	13.5	3.0	7.5	2.9	3	2.5	19	3.2	19	4.1	9	3.4	13	2.8	22.8	11.1	14	·	·	·	5	·	·	8	6	7	3	1	1	·	·
X	1.5	2.7	1.5	2.7	22	4.6	27	5.3	12	2.9	6.5	2.2	12	2.9	3.5	2.9	7	3.7	7.1	2.2	14	·	·	·	·	·	·	6	8	7	3	·	7	·	·
XI	4.5	2.8	7.5	4.5	10	5.8	13	4.2	8.5	2.6	15.5	3.9	20.5	3.3	7.5	2.6	3	3.6	63.3	11.5	12	·	1	10	·	·	·	1	20	17	11	2	7	1	·
XII	6	3.2	10	3.3	3.5	4.3	6	3.4	15.5	2.5	13	4.8	24.5	4.4	9.5	4.1	5	3.6	20.0	5.7	11	8	14	23	·	1	·	2	15	16	6	·	4	17	·
Rok	38	2.5	44	2.8	86.5	3.8	111.5	3.5	100	3.2	197.5	3.7	271	3.8	88.5	3.4	158	3.2	469.0	19.9	28.VII	17	28	79	32	11	·	34	144	166	91	12	34	49	22

Warszawa, Inst. Geogr. UW $H_s = 108\ m$ $h_w = 20\ m$

I	7.5	1.9	5	1.8	3.5	2.3	18.5	2.5	22.5	3.2	20.5	3.5	10	2.9	2.5	4.0	3	2.8	24.5	7.5	31	8	13	25	·	1	·	1	20	14	7	·	1	11	·
II	2	2.0	·	·	4.5	2.4	16.5	2.4	23	3.1	23.5	3.0	10	3.6	2.5	3.0	2	2.9	13.9	4.4	28	·	·	10	·	·	·	1	20	9	5	·	9	7	·
III	1	2.0	·	·	1	4.0	1	4.0	6.5	3.7	33	4.2	42	4.8	8.5	4.2	·	4.4	26.3	13.1	30	·	·	5	·	–	–	·	17	14	6	1	3	·	1
IV	4.5	2.8	8	1.3	25.5	3.2	9	3.6	10	2.9	9.5	3.3	9.5	3.5	5	2.2	9	2.7	28.1	6.7	2	·	·	1	·	–	–	6	8	8	7	·	·	1	1
V	3.5	2.6	4.5	1.6	11.5	2.3	10.5	2.6	11.5	2.8	15	2.6	16.5	3.3	12	2.7	8	2.4	51.0	11.9	7	·	·	·	1	1	·	·	11	14	9	2	·	·	7
VI	2	3.0	3.5	2.7	9.5	3.7	12.5	3.2	21	3.0	21.5	2.6	13	3.5	2	1.2	5	2.9	69.1	24.8	27	·	·	·	13	·	·	·	7	12	9	2	·	·	10
VII	2.5	3.4	2.5	1.8	3.5	1.3	9	3.4	25.5	2.8	31.5	3.2	15	3.2	2.5	3.0	1	3.0	90.1	23.0	28	·	·	·	7	–	–	1	17	16	12	3	·	·	7
VIII	4	2.1	3	1.0	3	1.3	3.5	2.9	24.5	2.3	27.5	3.2	19	2.7	5.5	2.4	3	2.5	62.8	20.7	11	·	·	·	5	·	·	·	7	14	10	2	1	·	3
IX	1.5	1.7	3	2.3	18	2.3	8.5	2.5	17	2.6	26	2.9	10.5	3.4	3.5	2.4	2	2.6	18.6	8.3	14	·	·	·	5	–	–	6	5	5	3	·	·	·	
X	0.5	2.0	4	3.0	23	3.3	30.5	3.4	16	2.6	9.5	2.6	7	3.4	0.5	6.0	2	3.0	4.8	2.3	29	·	·	·	·	–	–	5	10	4	3	·	6	·	·
XI	4	3.8	7.5	3.3	12.5	3.2	17.5	2.7	16	3.2	17	3.7	9	2.9	5.5	2.2	1	3.1	60.7	11.5	13	·	1	8	·	–	–	1	22	15	11	2	5	·	·
XII	8	3.0	5	3.3	12	3.5	12	2.9	15	3.3	16.5	3.8	19	3.6	4.5	3.2	1	3.4	17.7	5.4	11	8	14	23	·	–	–	2	17	11	5	·	4	17	·
Rok	41	2.5	46	1.8	127.5	2.7	149	3.0	208.5	3.0	251	3.2	180.5	3.4	54.5	3.0	37	3.0	467.6	24.8	27.VI	16	28	72	31	–	–	23	161	136	87	12	29	36	29

Warszawa, Obserw. Astr. UW — φ = 52°13' — λ = 21°02' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE $N_{m\,c.}$			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1005.6	1028.6	986.8	1020.3	0.1	−5.6	6.5	4	−17.1	26	−4.2	−1.3	−2.9	−2.8	4.5	4.8	4.7	4.7	90	81	88	86	0.4	1.0	0.6	0.7	7.7	7.6	6.8	7.4
II	1007.5	1023.0	980.3	1022.0	3.8	0.1	9.1	18	−3.7	6	0.7	2.8	1.7	1.7	6.1	6.5	6.4	6.3	93	87	91	90	0.4	1.0	0.6	0.7	9.2	8.1	7.0	8.1
III	1001.1	1020.8	977.7	1015.3	9.1	2.5	16.0	18	−1.7	20	3.6	7.3	5.5	5.5	7.1	7.6	7.5	7.4	89	75	82	82	0.9	2.9	1.8	1.9	9.5	6.8	5.8	7.4
IV	999.4	1011.0	989.0	1013.4	16.1	5.0	25.1	15	−1.5	10	7.2	14.6	10.1	10.5	8.4	9.1	9.2	8.9	81	54	72	69	2.0	8.5	3.7	4.7	5.3	4.5	3.3	4.4
V	997.9	1005.7	985.0	1011.8	17.7	8.2	26.1	27	4.1	15	10.0	16.3	12.1	12.6	10.7	10.6	11.1	10.8	86	58	78	74	1.9	8.6	3.3	4.6	7.6	8.3	6.6	7.5
VI	1001.1	1013.6	990.7	1014.7	24.1	13.6	33.4	27	9.1	21	16.2	22.7	17.7	18.6	15.4	14.7	15.1	15.1	83	54	74	70	3.2	13.6	5.4	7.4	4.3	6.3	3.5	4.7
VII	999.2	1011.3	984.5	1012.9	21.5	12.6	31.4	3	9.1	6	14.7	20.1	16.3	16.8	14.4	14.8	15.0	14.7	86	65	81	77	2.5	9.4	3.7	5.2	7.1	8.2	6.5	7.3
VIII	1001.8	1015.7	990.4	1015.5	21.8	12.9	31.1	6	9.1	30	14.3	20.1	16.3	16.8	14.5	15.4	15.3	15.1	88	65	82	78	2.0	8.9	3.4	4.8	4.9	7.2	5.3	5.8
IX	1005.1	1016.9	992.2	1019.0	21.0	10.4	30.0	3	2.6	23	11.3	20.0	14.1	14.9	12.3	13.6	13.2	13.0	90	59	81	77	1.6	10.5	3.3	5.1	4.1	4.0	2.1	3.4
X	1006.0	1018.3	981.5	1020.1	15.3	6.3	22.0	19	1.8	31	7.0	14.7	10.5	10.7	9.5	11.7	10.7	10.6	94	71	84	83	0.7	5.3	2.2	2.7	6.3	6.3	3.0	5.2
XI	1000.4	1022.5	988.4	1014.7	6.2	1.6	13.0	3	−6.5	23	2.7	5.1	3.8	3.8	7.2	7.8	7.5	7.5	94	88	91	91	0.5	1.2	0.8	0.8	8.6	8.6	7.0	8.1
XII	1001.3	1031.0	979.6	1016.0	−0.1	−6.1	15.5	5	−22.1	26	−3.7	−2.1	−3.4	−3.2	4.9	5.0	4.6	4.8	88	84	86	86	0.5	1.0	0.7	0.7	8.1	7.3	7.2	7.5
Rok	1002.2	1031.0	977.7	1016.3	13.0	5.1	33.4	27.VI	−22.1	26.XII	6.6	11.7	8.5	8.8	9.6	10.1	10.0	9.9	88	70	82	80	1.4	6.0	2.5	3.3	6.9	6.9	5.3	6.4

Warszawa, Stacja Pomp Rzeczn. — φ = 52°13' — λ = 21°03'

I	–	–	–	–	−0.1	−5.5	6.3	4	−18.8	26	−4.3	−1.4	−2.9	−2.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	3.9	−0.3	10.0	18	−2.8	6	0.6	3.0	1.5	1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	9.2	2.7	16.2	10	−1.6	20	3.9	7.6	5.5	5.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.7	4.7	24.9	15	−1.8	10	7.3	14.5	9.8	10.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.4	7.9	27.4	27	2.2	15	10.7	15.8	12.2	12.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.8	13.7	34.0	27	7.9	1	16.9	22.4	17.7	18.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.4	12.3	31.6	3	7.5	6	15.4	20.0	16.3	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	20.9	12.9	31.1	6	9.0	15, 30	14.8	20.0	16.1	16.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.3	9.9	29.4	3	2.7	23	11.7	19.6	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.3	5.5	22.3	19	0.8	31	7.2	14.8	9.6	10.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.3	1.4	13.2	3	−7.1	23	2.7	5.2	3.9	3.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	−0.3	−6.3	15.6	5	−22.7	26	−3.4	−2.1	−3.4	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.8	4.9	34.0	27.VI	−22.7	26.XII	7.0	11.6	8.3	8.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Warszawa – Okęcie — φ = 52°09' — λ = 20°59'

I	1006.4	1029.2	987.4	1020.1	−0.4	−6.3	6.1	4	−19.0	26	−4.4	−1.4	−3.2	−3.1	4.2	4.7	4.5	4.5	87	79	85	84	0.5	1.1	0.7	0.8	7.6	7.2	6.5	7.1
II	1008.2	1023.4	981.0	1021.6	3.5	−0.3	9.6	18	−4.6	5	0.6	2.7	1.3	1.5	5.9	6.5	6.1	6.2	92	87	90	90	0.5	1.0	0.7	0.7	9.0	8.5	7.4	8.3
III	1002.3	1021.4	979.3	1015.4	9.0	2.0	15.8	10	−2.2	20	3.5	7.3	5.1	5.3	6.9	7.4	7.2	7.2	86	72	81	80	1.2	3.1	1.8	2.0	8.8	7.7	6.4	7.6
IV	1000.7	1012.3	990.4	1013.6	15.7	4.3	24.6	15	−3.1	10	6.8	14.5	9.2	9.9	8.1	8.4	8.6	8.4	80	50	71	67	2.0	9.0	3.5	4.8	5.9	5.3	3.7	5.0
V	999.2	1007.0	986.6	1012.0	17.0	6.9	25.1	29	1.4	15	10.2	15.6	11.3	12.1	10.6	10.3	11.0	10.6	84	59	81	75	2.0	8.1	2.7	4.3	7.2	7.7	6.8	7.2
VI	1002.3	1014.8	992.2	1014.9	23.6	12.0	32.4	27	5.2	21	16.3	22.0	16.4	17.8	15.4	14.7	15.3	15.1	83	56	82	74	3.2	12.3	3.5	6.3	5.5	6.7	5.8	6.0
VII	1000.5	1013.1	985.8	1013.2	21.2	11.1	30.5	3	6.9	6	14.7	19.7	15.2	16.2	14.4	14.1	14.7	14.4	86	62	85	78	2.5	9.6	2.8	5.0	6.9	7.5	6.2	6.9
VIII	1003.1	1016.7	991.8	1015.8	21.0	12.1	31.1	6	8.0	30, 31	14.5	19.7	15.3	16.2	14.8	15.0	15.2	15.0	89	66	87	81	1.9	8.6	2.4	4.3	6.0	7.2	6.0	6.4
IX	1006.3	1018.0	993.7	1019.1	20.4	8.8	29.9	2, 3	1.2	23	11.2	19.5	12.7	14.0	12.2	13.0	12.9	12.7	90	58	85	78	1.4	10.4	2.2	4.7	5.1	4.6	3.6	4.4
X	1007.2	1019.1	982.7	1020.2	15.4	5.1	22.3	19	0.2	31	6.8	14.6	9.6	10.2	8.9	10.3	9.6	9.6	89	63	80	77	1.2	6.6	2.6	3.5	6.3	6.5	4.1	5.6
XI	1001.7	1023.4	989.7	1014.9	6.0	1.1	13.2	3	−7.9	23	2.4	5.2	3.4	3.6	7.1	7.7	7.4	7.4	94	85	91	90	0.5	1.5	0.7	0.9	8.6	8.6	7.8	8.3
XII	1002.7	1031.8	981.1	1016.3	−0.5	−6.3	15.4	5	−23.5	26	−4.0	−2.4	−3.6	−3.4	4.5	4.8	4.5	4.6	87	82	88	86	0.7	1.1	0.7	0.8	8.1	7.3	7.0	7.5
Rok	1003.4	1031.8	979.3	1016.4	12.7	4.2	32.4	27.VI	−23.5	26.XII	6.6	11.4	7.7	8.4	9.4	9.7	9.8	9.6	87	68	84	80	1.5	6.0	2.0	3.2	7.1	7.1	5.9	6.7

Uwaga. Ciśnienie powietrza w styczniu i lutym jest za niskie przeciętnie o około 0.5 mb.

Jeziory — φ = 52°16' — λ = 16°48'

I	–	–	–	–	0.1	−6.2	5.4	9	−18.3	26	−4.8	−0.9	−3.5	−3.2	4.3	4.8	4.6	4.6	90	79	87	85	0.4	1.1	0.6	0.7	5.7	5.1	5.3	5.4
II	–	–	–	–	6.1	−0.1	12.5	18	−5.1	6	1.4	4.9	2.4	2.8	6.4	7.1	6.7	6.7	94	82	92	89	0.4	1.7	0.6	0.9	8.1	7.4	6.7	7.4
III	–	–	–	–	9.7	2.2	18.8	10	−6.6	20	3.8	8.4	5.2	5.6	7.0	7.5	7.5	7.3	87	69	84	80	1.2	3.9	1.5	2.2	7.8	7.1	4.8	6.6
IV	–	–	–	–	15.7	5.1	25.2	6	−0.9	10	7.2	14.2	9.4	10.0	8.3	9.0	9.2	8.8	80	56	76	71	2.1	8.2	3.1	4.5	5.2	5.2	3.2	4.5
V	–	–	–	–	15.7	6.6	22.1	26	2.2	13, 16	9.9	14.1	10.1	11.0	10.6	10.7	10.8	10.7	87	68	87	81	1.7	5.8	1.7	3.1	7.1	8.6	4.6	6.8
VI	–	–	–	–	23.4	12.0	29.8	26	6.4	22	16.6	21.9	15.9	17.6	15.2	14.4	15.6	15.1	80	55	85	73	3.9	12.5	2.7	6.4	3.4	4.8	4.4	4.2
VII	–	–	–	–	20.7	11.9	32.3	3	7.9	6, 11	14.7	19.0	14.7	15.8	14.7	14.4	14.6	14.6	88	68	87	81	2.2	8.5	2.4	4.4	7.3	7.4	6.7	7.1
VIII	–	–	–	–	20.8	11.8	29.3	6	7.4	4	14.3	19.2	14.6	15.7	15.0	15.6	15.2	15.3	92	71	91	85	1.5	7.2	1.6	3.4	6.7	6.7	4.8	6.1
IX	–	–	–	–	21.0	10.2	29.3	2	4.4	24	11.9	19.9	13.5	14.7	12.9	13.9	14.1	13.6	90	60	90	80	1.4	10.1	1.6	4.4	4.2	4.3	4.1	4.2
X	–	–	–	–	15.1	7.2	21.3	6	1.4	13	8.4	14.5	10.0	10.7	10.2	11.5	10.7	10.8	92	72	87	84	1.1	5.3	1.7	2.7	5.7	5.2	4.1	5.0
XI	–	–	–	–	6.3	1.5	12.8	2	−6.6	22	2.7	5.6	3.3	3.7	7.1	7.7	7.4	7.3	93	84	93	90	0.6	1.5	0.6	0.9	8.1	8.4	7.0	7.8
XII	–	–	–	–	0.3	−6.8	15.8	5	−22.8	26	−4.1	−1.5	−3.5	−3.2	4.7	5.1	4.7	4.8	87	83	87	86	0.6	1.1	0.7	0.8	7.1	7.0	6.5	6.9
Rok	–	–	–	–	12.9	4.6	32.3	3.VII	−22.8	26.XII	6.8	11.6	7.7	8.4	9.7	10.1	10.1	10.0	88	71	87	82	1.4	5.6	1.6	2.9	6.9	6.4	5.2	6.0

Warszawa, Obserw. Astr. UW — $H_s = 110$ m — $H_b = 114{,}8$ m — $h_w = 25$ m — 1961

MIESIĄC	ROZKŁAD WIATRU °/D, °/mD																		OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr				Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	> 10	> 15	●	●	≥ 0.1	≥ 1.0	≥ 10.0	■	▦	ΣR
I	5	1.4	8	1.3	2	1.0	6	1.0	12.5	1.1	18.5	1.3	11	2.3	7	2.7	23	1.3	34.3	10.2	31	9	12	25	·	·	·	5	18	15	10	1	–	19	·
II	1.5	1.7	3	1.0	·	·	6	1.0	19	1.0	11.5	1.3	14.5	1.6	8.5	1.1	28	0.9	19.4	6.7	28	·	·	13	·	·	·	1	19	12	5	·	–	7	·
III	1	3.0	·	·	·	·	·	·	0.5	3.0	14.5	2.7	5.0	3.0	2.3	2.9	4	2.8	33.9	17.8	30	·	·	5	·	·	·	1	14	17	5	1	–	2	·
IV	5	1.0	2	1.0	1	3.0	16	2.0	13	1.6	7	2.1	11	2.3	2	2.0	33	1.2	31.5	8.2	17	·	·	2	1	·	·	11	5	9	7	·	–	1	1
V	5	1.0	4	1.5	2	1.0	5	1.0	10	1.2	9	1.0	20	1.4	10	1.6	28	0.9	49.4	10.6	7	·	·	·	2	·	·	1	16	15	12	1	–	·	5
VI	·	·	·	·	2	1.0	8	1.3	13	1.3	9	2.3	24	2.0	5	2.6	29	1.2	86.3	35.2	27	·	·	·	13	·	·	7	2	16	9	3	–	·	9
VII	6	1.0	·	·	·	·	·	·	10	1.4	16	1.1	30	1.6	3	1.0	28	1.0	110.0	30.8	28	·	·	·	6	·	·	2	16	19	14	4	–	·	5
VIII	5	1.4	1	1.0	·	·	1	1.0	3	1.7	21	2.1	32	2.2	3	1.0	27	1.4	62.0	19.5	11	·	·	·	6	·	·	4	8	17	12	2	–	·	3
IX	2	1.0	1	1.0	1	1.0	11	1.2	5	1.4	10	1.4	22	2.0	7	1.6	31	1.0	19.0	7.9	14	·	·	·	5	·	·	13	3	8	3	·	–	·	·
X	·	·	·	·	1	1.0	30	1.9	30	1.6	4	1.0	9	2.3	6	3.0	13	1.6	5.9	2.7	29	·	·	·	·	·	·	7	4	4	2	·	–	·	·
XI	8	1.8	6	2.3	3	1.7	16	1.4	9	1.2	8	2.0	21	2.3	2	2.0	17	1.5	80.5	13.9	13	·	·	10	·	·	·	2	20	19	13	4	–	·	·
XII	9	2.1	8	1.2	2	1.0	2	1.0	9	1.2	9	2.6	22	1.6	5	1.8	27	1.2	25.2	8.1	1	8	13	23	·	·	·	2	18	17	6	·	–	18	·
Rok	47.5	1.3	33	0.9	14	0.9	101	1.1	134	1.5	137.5	1.7	266.5	2.0	81.5	1.9	280	1.3	557.4	35.2	27.VI	17	25	78	33	·	·	56	143	168	98	16	–	47	23

Warszawa, Stacja Pomp Rzeczn. — $H_s = 85$ m — $h_w = 14$ m

I	9	2.7	8	2.0	2	1.0	13	2.4	18	1.8	15.5	3.6	12	2.9	6.5	2.2	9	2.3	32.2	9.9	31	9	12	28	·	·	·	–	–	13	9	·	1	6	–
II	7.5	1.6	1.5	2.0	3.5	1.0	11	2.1	17	2.1	15	2.6	19	3.1	5.5	3.6	4	2.3	20.2	6.8	28	·	·	19	·	·	·	–	–	12	5	·	6	7	–
III	1.5	2.0	·	·	·	·	·	·	4.5	2.1	15.5	3.8	5.6	4.6	13.5	3.7	2	4.0	30.5	17.1	30	·	·	6	·	2	·	–	–	14	4	1	3	4	–
IV	10	2.2	6	1.7	21.5	3.4	16	3.4	4	1.9	7.5	2.1	9.5	4.3	5.5	2.9	10	2.6	27.4	6.7	2	·	·	2	·	1	·	–	–	8	7	·	1	1	–
V	6.5	2.7	3	2.0	5.5	2.2	12	2.2	5	1.4	9.5	1.9	20.5	2.2	1.4	2.4	17	1.8	47.6	10.6	7	·	·	·	2	·	·	–	–	12	9	1	·	·	–
VI	4	1.0	2	3.2	1.1	2.7	12.5	2.3	3	2.0	13.5	2.3	27.5	3.3	6.5	2.2	10	2.3	84.7	23.5	27	·	·	·	12	·	·	–	–	16	10	3	1	·	–
VII	2	2.2	0.5	1.0	3	1.3	5.5	2.6	5.5	1.7	22.5	2.7	3.7	2.9	5	1.7	12	2.3	106.3	32.3	28	·	·	·	6	·	·	–	–	21	15	2	·	·	–
VIII	6	1.8	2.5	1.6	3.5	1.0	1.5	1.0	1.5	1.7	18.5	3.0	41.5	2.6	9	1.9	9	2.2	63.1	19.9	11	·	·	·	5	·	·	–	–	15	10	2	1	·	–
IX	6.5	1.4	3	1.5	1.1	1.9	5	1.4	4.5	1.3	10	2.2	27	2.9	4	3.4	19	1.8	16.8	6.8	14	·	·	·	5	·	·	–	–	6	3	·	1	·	–
X	1.5	1.0	1.5	1.7	2.3	3.1	27.5	2.9	5	1.5	6	2.4	9.5	2.5	5	2.2	14	2.3	4.1	2.2	29	·	·	·	·	·	·	–	–	4	2	·	6	·	–
XI	12.5	2.6	6	3.2	10.5	3.7	11.5	1.9	7	1.4	15.5	2.4	17	2.9	4	1.5	6	2.4	68.8	13.0	13	·	·	10	·	·	·	–	–	14	13	3	8	·	–
XII	12	4.0	5.5	3.2	5	3.1	7.5	2.1	12.5	1.5	12	4.5	25	3.6	7.5	4.1	6	3.1	18.2	6.1	11	8	14	22	·	1	·	–	–	11	5	·	3	19	–
Rok	79	2.1	39.5	1.9	99.5	2.0	123	2.0	87.5	1.7	161	2.8	301.5	3.2	86	2.6	118	2.4	519.9	32.3	28.VII	17	26	87	30	4	·	–	–	146	92	12	31	37	–

Warszawa - Okęcie — $H_s = 106$ m — $H_b = 106{,}9$ m — $h_w = 8{,}8$ m

I	3.5	4.3	6	3.9	2	3.2	15.5	3.1	18.5	3.1	14	4.2	10.5	4.8	11	3.3	12	3.2	26.3	8.5	31	11	13	26	·	·	·	4	17	13	9	·	4	20	·
II	2	2.5	1	1.5	2	1.8	13	3.2	18	2.9	10.5	3.7	15.5	3.7	6	3.7	16	2.6	16.3	4.7	28	·	·	16	·	1	·	1	19	12	4	·	11	3	·
III	0.5	5.0	·	·	·	·	·	·	4	4.2	13.5	5.6	53.5	6.5	19.5	6.1	2	6.0	25.8	12.5	30	·	·	9	·	10	·	·	12	15	6	1	4	2	1
IV	2.5	2.8	7.5	4.3	18.5	4.1	16.5	4.2	10.5	2.5	6	3.2	13.5	5.5	10	4.2	5	3.8	24.5	6.9	2	·	·	3	·	2	·	7	5	7	6	·	3	1	2
V	5	4.2	3.5	3.1	8	3.4	8.5	3.0	10	3.5	10	2.9	23.5	4.1	17.5	4.0	7	3.4	39.4	8.4	7	·	·	·	2	2	·	·	11	18	11	·	·	·	6
VI	1	3.5	2	2.5	1.5	3.4	10.5	3.1	10	2.8	17.5	3.5	27.5	4.4	4.5	3.9	2	3.6	81.9	28.2	27	·	·	·	11	2	·	1	4	17	12	3	1	·	12
VII	3	4.2	1	1.0	3.5	1.6	6	4.0	12	3.2	24.5	3.8	30	4.4	7	3.3	6	3.5	88.2	28.2	28	·	·	·	6	1	·	2	11	17	11	2	2	·	9
VIII	3.5	1.3	1.5	3.7	2.5	3.0	3	1.8	13.5	2.4	25.5	4.5	29	4.1	11.5	3.6	3	3.6	61.2	16.6	10	·	·	·	5	·	·	1	6	15	11	2	3	·	4
IX	0.5	2.0	5.5	2.6	1.4	3.0	7	2.7	9	2.3	18.5	3.7	21.5	4.6	6	4.1	8	3.2	15.8	7.0	14	·	·	·	5	·	·	8	5	7	3	·	2	·	1
X	0.5	4.0	3.5	4.0	2.4	4.2	27.5	4.5	15	3.3	3	4.5	10	4.5	4.5	4.3	5	4.0	6.9	3.0	1.4	·	·	·	1	·	·	7	8	7	2	·	8	·	·
XI	8.5	3.6	5	6.2	13.5	5.4	13.5	3.8	11.5	2.9	13.5	4.8	15.5	4.9	7	3.1	2	4.3	71.5	12.8	4	·	2	10	·	1	·	1	22	21	13	2	6	·	·
XII	5.5	5.7	6	5.5	5.5	3.8	10	3.7	14	3.3	12.5	5.6	22.5	4.9	16	5.2	1	4.7	20.6	8.2	11	9	14	24	·	3	·	3	18	15	4	·	6	17	·
Rok	3.6	3.6	42.5	3.2	19.85	3.1	13.1	3.1	14.6	3.0	16.9	4.2	27.2.5	4.7	120.5	4.1	69	3.8	478.4	28.2	27.VI, 28.VII	20	29	88	29	23	·	35	138	164	92	10	50	43	35

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Jeziory — $H_s = 84$ m — $h_w = 15$ m

I	·	·	1.8	1.2	6	1.5	17	1.2	14	1.4	3.2	1.4	1	2.0	4	1.2	1	1.3	35.7	8.8	14, 31	12	11	25	·	·	·	8	13	12	8	·	7	19	·
II	·	·	1	1.0	5	2.0	13	1.5	11	1.3	4.1	1.8	7	1.4	6	1.5	·	1.6	28.3	13.1	9	·	·	14	·	·	·	2	14	13	7	1	14	·	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	39.8	11.6	3.0	·	·	7	·	–	–	2	11	15	8	1	6	1	·
IV	6	1.5	11	2.1	10	1.8	21	1.7	6	1.8	19	1.2	7	1.3	10	1.4	·	1.6	88.9	28.0	16	·	·	2	1	·	·	10	6	12	11	3	3	·	4
V	·	·	10	1.6	3	1.3	10	1.4	2	2.5	37	1.4	12	1.1	18	1.5	1	1.4	99.5	26.1	29	·	·	·	·	·	·	2	8	18	15	2	3	·	7
VI	2	2.0	3	2.0	1	2.0	16	1.3	4	1.2	44	1.2	12	1.4	6	1.1	2	1.3	49.3	23.0	10	·	·	·	9	·	·	10	6	8	7	1	1	·	7
VII	·	·	·	·	·	·	4	1.2	5	1.2	63	1.5	19	1.4	1	1.0	1	1.4	127.6	44.3	31	·	·	·	5	·	·	2	13	21	16	5	4	·	8
VIII	1	1.0	4	1.2	1	2.0	6	1.0	2	1.0	54	1.3	22	1.5	2	1.0	1	1.3	64.5	16.8	20	·	·	·	3	·	·	4	9	10	9	3	6	·	6
IX	5	1.2	9	1.7	7	1.1	10	1.7	5	1.0	43	1.4	11	1.5	·	·	·	1.4	35.9	19.0	5	·	·	·	7	·	·	11	8	6	4	2	3	·	2
X	·	·	9	3.0	5	2.8	21	1.8	6	1.0	44	1.2	5	1.0	3	1.3	·	1.6	23.8	6.1	29	·	·	·	·	·	·	9	8	9	8	·	12	·	·
XI	1	1.0	19	2.1	5	1.4	8	1.0	1	1.0	44	1.3	5	1.0	7	1.0	·	1.4	35.7	19.5	13	·	·	10	·	·	·	4	19	15	5	1	13	·	·
XII	2	1.5	10	1.2	7	1.1	19	1.1	3	1.0	30	1.6	7	1.4	14	1.3	1	1.3	52.8	21.1	11	10	15	24	·	·	·	3	15	13	9	1	10	16	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	681.8	44.3	31.VII	22	26	82	25	–	–	67	130	152	107	18	82	36	34

Świebodzin

$\varphi = 52°15'$ $\lambda = 15°32'$ **1961**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o\,m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dius	I	II	III	Dies	I	II	III	Dies	I	II	III	Dias
I	–	–	–	–	0.3	−6.8	6.8	29	−23.5	27	−4.6	−0.9	−3.9	−3.3	4.5	5.2	4.7	4.8	91	86	91	89	0.3	0.8	0.4	0.5	6.9	6.2	5.4	6.2
II	–	–	–	–	7.2	0.5	14.0	15	−4.5	6	2.0	5.5	3.1	3.4	6.8	7.7	7.2	7.2	96	85	94	92	0.3	1.5	0.5	0.8	8.6	7.2	6.1	7.3
III	–	–	–	–	10.4	2.4	19.4	10	−5.8	20	3.6	9.0	5.5	5.9	7.5	8.2	7.8	7.8	93	72	86	84	0.6	3.7	1.5	1.9	7.8	6.8	5.9	6.8
IV	–	–	–	–	16.0	5.0	27.1	6	−0.7	1	7.3	14.4	9.6	10.2	9.2	10.6	10.3	10.0	88	65	85	79	1.2	6.8	2.0	3.3	4.8	5.4	3.3	4.5
V	–	–	–	–	15.8	7.1	23.9	26	3.0	13	9.6	14.1	10.5	11.2	10.6	11.6	11.4	11.2	88	73	89	82	1.4	4.9	1.5	2.6	7.0	8.2	5.6	6.9
VI	–	–	–	–	23.2	11.8	30.2	26	7.2	21	15.7	22.1	17.0	18.0	14.9	15.6	16.4	15.6	83	59	84	75	3.1	11.5	3.2	5.9	4.4	5.5	4.4	4.8
VII	–	–	–	–	20.5	12.2	32.9	3	8.7	6, 8	14.7	19.1	15.5	16.2	14.4	14.5	15.0	14.6	86	68	85	80	2.5	8.6	2.9	4.7	7.7	7.6	7.0	7.4
VIII	–	–	–	–	21.3	11.9	30.4	6	7.8	4	14.0	19.6	15.3	16.0	14.8	15.8	15.9	15.5	92	70	91	84	1.3	7.6	2.0	3.6	6.6	7.1	4.2	6.0
IX	–	–	–	–	21.8	9.9	31.0	2	1.3	24	11.4	20.6	13.5	14.8	–	–	–	–	–	–	–	–	–	–	–	–	3.9	4.4	3.4	3.9
X	–	–	–	–	16.3	7.2	22.9	6	2.2	31	8.1	15.3	10.4	11.0	10.1	12.0	11.2	11.1	94	70	89	84	0.8	5.7	1.6	2.7	5.0	5.3	5.0	5.1
XI	–	–	–	–	6.9	1.4	13.2	2	−6.7	23	2.5	5.7	3.4	3.8	7.1	8.0	7.5	7.5	94	87	94	92	0.4	1.2	0.5	0.7	7.6	7.9	6.6	7.4
XII	–	–	–	–	1.3	−6.6	16.2	5	−22.3	26	−3.4	−1.2	−3.3	−2.8	5.0	5.0	4.7	4.9	89	82	87	86	0.6	1.2	1.0	0.9	6.5	6.2	6.0	6.2
Rok	–	–	–	–	13.4	4.7	32.9	3.VII	−23.5	27.I	6.7	11.9	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	5.2	6.0

Zbąszyń

$\varphi = 52°15'$ $\lambda = 15°56'$

I	–	–	–	–	0.4	–	6.7	30	–	–	−4.5	−0.8	−3.3	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.4	6.5	6.2
II	–	–	–	–	6.7	–	12.6	15	–	–	1.7	5.3	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.6	7.6	8.1
III	–	–	–	–	10.3	2.5	19.4	10	−4.7	20	4.0	8.9	5.5	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.4	6.9	7.4
IV	–	–	–	–	16.4	5.0	25.1	14	−0.5	1, 10	7.5	14.6	9.6	10.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.5	6.0	5.5
V	–	–	–	–	16.0	7.2	23.3	26	3.2	12, 25	9.8	13.8	10.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.4	7.4	7.8
VI	–	–	–	–	23.6	12.1	29.8	26	5.4	22	16.0	22.1	17.5	18.3	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.5	5.6	5.1
VII	–	–	–	–	21.1	12.5	32.9	3	8.4	6	14.8	19.2	15.6	16.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.6	8.7	8.4
VIII	–	–	–	–	21.0	12.2	29.9	6	7.2	4	14.2	19.6	15.8	16.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.4	7.0	7.2
IX	–	–	–	–	21.7	9.8	30.4	2	2.3	24	12.1	20.7	14.2	15.3	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.8	4.4	4.6
X	–	–	–	–	15.9	7.1	22.5	6	1.4	13	8.1	15.1	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.5	5.0	5.6
XI	–	–	–	–	6.5	1.3	13.3	2	−7.4	23	2.5	5.7	3.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.3	7.8	8.1
XII	–	–	–	–	0.7	−6.5	15.7	5	−23.3	26	−3.8	−1.0	−3.4	−2.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.9	7.1	7.0
Rok	–	–	–	–	13.4	–	32.9	3.VII	–	–	6.9	11.9	8.3	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.9	6.7	6.8

Kórnik

$\varphi = 52°15'$ $\lambda = 17°06'$

I	–	–	–	–	0.1	−6.6	6.2	9	−20.2	27	−5.1	−1.4	−4.1	−3.7	4.2	4.7	4.5	4.5	90	80	88	86	0.4	1.1	0.5	0.7	6.1	5.9	5.6	5.9
II	–	–	–	–	6.2	0.3	12.4	18	−3.7	6	1.4	4.6	2.5	2.8	6.4	6.9	6.7	6.7	94	82	91	89	0.5	1.6	0.7	0.9	9.1	7.7	6.0	7.6
III	–	–	–	–	10.0	2.6	17.5	10	−5.6	20	3.9	8.2	5.7	5.9	7.0	7.3	7.3	7.2	86	69	79	78	1.2	3.9	2.1	2.4	7.7	7.4	5.7	6.9
IV	–	–	–	–	15.7	5.0	26.0	7	−0.6	1	6.8	13.8	9.1	9.7	8.3	8.6	9.5	8.8	82	55	80	72	1.9	7.8	2.4	4.0	5.4	5.5	3.8	4.9
V	–	–	–	–	15.9	7.0	22.0	26	2.7	12	9.6	13.8	10.6	11.2	10.3	10.3	10.9	10.5	86	67	84	79	1.8	5.8	2.1	3.2	7.6	8.5	5.9	7.3
VI	–	–	–	–	23.4	12.3	29.3	26	6.3	22	16.1	21.7	16.7	17.8	14.6	13.6	15.2	14.5	79	53	80	71	3.9	12.8	4.0	6.9	4.7	5.4	4.7	4.9
VII	–	–	–	–	21.1	12.1	33.2	3	7.9	6	14.8	19.1	15.1	16.0	13.9	13.3	14.1	13.8	83	63	83	76	3.1	9.9	3.3	5.4	8.1	8.1	8.6	8.3
VIII	–	–	–	–	21.2	12.2	31.0	6	7.9	14	14.3	19.2	15.3	16.0	14.6	14.5	15.1	14.7	89	66	86	80	1.9	8.4	2.5	4.3	7.2	6.7	5.4	6.4
IX	–	–	–	–	21.0	9.8	30.2	2	3.5	24	11.7	19.8	13.8	14.8	12.3	12.9	13.2	12.8	88	56	83	76	1.7	10.8	2.8	5.1	4.2	4.4	3.1	3.9
X	–	–	–	–	15.3	7.2	22.2	6	2.1	13	8.0	14.3	10.0	10.6	10.0	10.9	10.6	10.5	92	68	86	82	0.9	5.6	1.8	2.8	6.4	5.8	5.2	5.8
XI	–	–	–	–	6.3	1.5	12.9	2	−6.4	23	2.7	5.4	3.1	3.6	7.1	7.8	7.4	7.4	93	86	94	91	0.6	1.4	0.5	0.8	8.9	8.3	7.1	8.1
XII	–	–	–	–	−0.1	−7.3	15.7	5	−23.8	26	−4.3	−2.1	−4.0	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	7.0	7.2
Rok	–	–	–	–	13.0	4.7	33.2	3.VII	−23.8	26.XII	6.7	11.4	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	5.7	6.4

Sinołęka

$\varphi = 52°13'$ $\lambda = 21°55$

I	–	–	–	–	−1.1	−6.1	6.6	4	−20.5	26	−5.0	−2.4	−3.9	−3.8	4.0	4.3	4.3	4.2	86	78	85	83	0.5	1.1	0.6	0.7	7.1	7.0	6.0	6.7
II	–	–	–	–	2.8	−1.1	9.6	18	−5.5	6	−0.1	1.8	0.8	0.8	5.6	6.1	5.9	5.9	92	87	90	90	0.5	1.0	0.6	0.7	8.6	8.3	6.8	7.9
III	–	–	–	–	8.4	1.5	16.2	10	−2.2	23	2.8	6.4	4.5	4.6	6.5	6.9	6.9	6.8	86	72	81	80	1.1	2.9	1.7	1.9	7.9	7.2	4.5	6.5
IV	–	–	–	–	15.0	3.7	24.2	15	−3.8	10	6.1	13.5	9.0	9.4	7.5	7.5	7.9	7.6	77	48	67	64	2.2	8.9	4.0	5.0	4.9	4.0	2.3	3.7
V	–	–	–	–	16.9	7.0	25.7	29	1.6	15	10.0	15.2	10.9	11.8	9.6	9.8	10.7	10.0	82	58	82	74	2.3	8.2	2.5	4.3	7.2	7.8	5.7	6.9
VI	–	–	–	–	23.5	12.0	32.0	27	5.5	21	16.0	22.0	16.9	17.9	14.5	13.9	14.3	14.2	79	54	74	69	3.9	13.3	5.1	7.4	5.0	5.9	5.1	5.3
VII	–	–	–	–	21.4	11.5	30.4	3	7.8	9	14.6	19.5	15.7	16.4	13.7	13.0	14.1	13.6	82	59	79	73	3.1	10.3	4.0	5.8	5.1	7.1	6.3	6.2
VIII	–	–	–	–	20.9	12.0	30.4	6	8.5	31	14.2	19.6	15.6	16.2	13.9	13.7	14.6	14.1	85	61	82	76	2.6	9.8	3.4	5.3	6.2	6.4	5.4	6.0
IX	–	–	–	–	19.8	8.9	28.7	3	0.4	23	10.8	18.8	12.9	13.8	11.4	11.6	12.5	11.8	86	53	82	74	2.0	10.9	2.8	5.2	4.8	3.7	2.7	3.7
X	–	–	–	–	15.2	5.2	22.2	19	0.2	31	6.6	14.2	9.8	10.1	8.5	9.2	9.2	9.0	86	58	76	73	1.5	7.3	3.1	4.0	5.3	5.5	3.5	4.8
XI	–	–	–	–	5.6	0.9	13.4	3	−8.8	23	2.2	4.6	3.1	3.2	6.8	7.3	7.1	7.1	91	84	91	89	0.7	1.5	0.8	1.0	8.6	8.8	7.3	8.2
XII	–	–	–	–	−1.0	−7.1	15.0	5	−23.7	26	−4.7	−2.8	−4.2	−4.0	4.2	4.6	4.4	4.4	85	82	86	84	0.8	1.1	0.7	0.9	8.4	7.3	5.8	7.2
Rok	–	–	–	–	12.3	4.0	32.0	27.VI	−23.7	26.XII	6.1	10.9	7.6	8.0	8.8	9.0	9.3	9.0	85	66	81	77	1.8	6.4	2.4	3.5	6.6	6.6	5.1	6.1

Świebodzin $H_s = 78$ m $h_w = 12$ m 1961

MIESIĄC	ROZKŁAD WIATRU ($^{0}/_{0}$, m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v v>10	v>15	◔	◐	Opad R R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	1	2.0	6.5	2.9	23.5	1.9	4.5	2.7	14	3.0	23	3.6	10.5	3.3	·	·	10	2.5	37.0	8.0	31	12	10	22	·	·	·	7	16	15	8	·	5	18	·
II	·	·	0.5	1.0	9	2.2	3.5	3.0	7	2.9	18.5	3.7	24	3.1	5.5	2.4	16	2.5	17.8	5.0	9	·	·	12	·	·	·	3	14	13	5	·	9	2	·
III	1.5	5.7	·	·	·	·	·	·	·	·	14	5.4	63	4.8	7.5	4.1	7	4.5	56.7	18.0	28	·	·	6	·	2	·	3	13	16	11	2	7	·	1
IV	15	2.7	12	3.4	13.5	3.9	8.5	3.7	3	1.7	9.5	2.5	13.5	2.9	4	3.8	11	2.8	59.4	21.3	27	·	·	1	1	·	·	10	7	12	10	1	3	·	1
V	13.5	2.7	2.5	2.2	1.5	3.3	1.5	3.7	7	2.2	14.5	3.8	19.5	3.4	22	2.6	11	2.6	115.3	21.2	5	·	·	·	·	·	·	1	14	23	16	4	·	·	6
VI	7.5	1.9	5.5	1.4	6.5	1.3	5	2.3	3	4.2	11.5	2.7	31	4.0	7	3.4	13	2.6	49.0	13.5	3	·	·	·	10	·	·	7	6	11	9	1	1	·	5
VII	2.5	1.0	2	1.0	0.5	1.0	2.5	3.2	6.5	2.2	34	3.3	34	3.4	3	2.8	8	2.8	73.1	15.5	6	·	·	·	5	2	·	2	13	16	12	2	·	·	5
VIII	5.5	2.4	2.5	1.6	1	3.0	2	1.5	1.5	5.0	18.5	3.0	38	3.0	8	2.9	16	2.4	50.0	8.3	16	·	·	·	6	·	·	4	7	17	11	·	—	·	6
IX	8	1.8	7.5	2.0	10.5	1.7	3.5	1.9	8	1.2	13.5	3.0	23	2.9	1	4.0	15	1.9	31.3	11.6	14	·	·	·	8	·	·	13	8	11	6	1	—	·	4
X	2.5	1.8	2.5	6.0	17	4.0	9.5	3.7	18	2.5	13.5	1.8	18	2.2	2	1.0	10	2.5	41.7	17.2	20	·	·	·	·	·	·	7	10	9	8	1	7	·	1
XI	12.5	2.6	9.5	4.3	3	4.5	1	1.0	12	1.8	18.5	3.2	16	4.3	2.5	4.0	15	2.8	46.0	25.2	13	·	·	7	·	·	·	3	18	16	8	1	6	·	·
XII	2.5	2.0	5.5	3.9	13	2.2	2	1.8	8.5	2.2	13.5	5.7	21.5	4.4	7.5	3.3	19	2.9	49.4	15.0	11	10	13	23	·	2	·	5	14	17	9	2	·	15	·
Rok	72	2.2	56.5	2.5	99	2.4	43.5	2.4	88.5	2.4	202.5	3.5	312	3.5	70	2.9	151	2.7	626.7	25.2	13.XI	22	23	71	30	6	·	65	140	176	113	15	—	35	31

Zbąszyń $H_s = 57$ m $h_w = 11$ m

I	1	1.0	6	2.5	15	1.8	18.5	1.9	21	2.6	10.5	3.4	7.5	2.8	3.5	2.9	10	2.2	33.1	9.0	14	—	10	—	·	·	·	—	—	12	8	·	1	15	·
II	2	2.2	·	·	9.5	2.6	17.5	2.0	16.5	2.4	16	3.0	9	3.2	8.5	3.5	5	2.5	24.7	11.2	9	—	·	—	·	1	·	—	—	13	8	1	7		·
III	·	·	·	·	·	·	2	1.8	4.5	2.1	22.5	4.8	51.5	6.1	3.5	5.4	9	4.9	39.9	12.8	30	·	·	7	·	9	·	—	—	16	10	1	3		·
IV	8.5	2.2	6	2.6	26.5	2.9	13	2.7	7	1.5	9.5	2.3	6	3.5	7.5	3.1	6	2.5	51.4	10.2	1	·	·	2	1	·		—	—	11	10	1	1	·	3
V	10	2.2	4	2.4	2.5	2.4	6	2.0	9.5	2.4	19	3.0	14.5	3.8	16.5	2.7	11	2.5	113.1	31.8	5	·	·		·	1		—	—	20	15	2	·	·	7
VI	6	1.2	1.5	1.7	11.5	2.0	7	1.6	3	2.0	16	2.6	25.5	3.4	8.5	2.5	11	2.2	79.6	49.0	4	·	·	·	11	·	·	—	—	9	8	1	·	·	3
VII	1.5	2.3	1	1.0	2	1.5	5	1.4	11	2.3	29	3.0	30.5	3.7	6	2.7	7	2.7	85.1	12.8	6		·	·	5	·	·	—	—	18	15	3			3
VIII	0.5	2.0	1.5	1.0	3	1.7	9	1.6	5.5	2.5	28.5	3.1	24.5	2.9	5.5	2.0	15	2.2	54.6	15.7	6	·			4	·	·	—	—	19	11	1	·	·	3
IX	2.5	2.4	4	1.5	20	2.4	5.5	1.9	15	2.4	14	3.0	13.5	3.1	2.5	2.8	13	2.2	24.9	11.5	14	·		·	7	·	·	—	—	5	4	1	—		2
X	1	1.0	·	·	27.5	3.8	19	2.2	11.5	2.2	7	2.1	6	2.9	5	3.2	16	2.4	27.9	6.2	17	·	·	·	·	1	·	—	—	11	8	·	·	·	·
XI	8	2.2	3	3.7	14	2.9	8.5	1.8	10	2.6	18.5	3.6	11	4.1	8	3.1	9	2.7	38.7	22.2	13	·	·	7	·	·	·	—	—	12	6	1	—	·	·
XII	9.5	2.5	4	1.8	3	2.3	10.5	1.7	7	2.8	14	3.9	17	4.4	4	3.0	14	2.6	52.7	16.1	11	9	14	23	·	·	·	—	—	13	10	2	·	16	·
Rok	50.5	1.8	31	1.5	144.5	2.2	121.5	1.9	121.5	2.5	204.5	3.2	216.5	3.7	79	3.1	126	2.6	625.7	49.0	4.VI	—	24	—	28	12	·	—	—	159	113	14	—	31	21

Kórnik $H_s = 77$ m $h_w = 16$ m

I	·	·	2	2.0	7.5	2.1	29.5	2.6	11	3.4	21	4.5	11.5	3.7	2.5	4.4	8	3.0	33.2	8.8	14	12	11	25	·	3		8	14	14	7	·	3	21	·
II	1.5	6.3	·	·	3.5	2.1	12.5	4.2	11.5	4.0	23.5	3.9	13	4.6	9.5	4.7	9	3.7	36.1	16.1	9	·	·	13	·	3	1	1	13	13	8	1	7	1	·
III	·	·	·	·	·	·	·	·	·	·	28.5	5.7	57.5	5.6	6	8.1	1	5.8	50.7	11.6	30	·	·	6	·	12	1	2	13	17	11	1	2	1	·
IV	7.5	3.0	2	3.8	17.5	5.2	14	4.9	7	5.2	10	2.9	9	5.3	8	4.9	15	3.8	126.9	67.7	16	·	·	2	1	7	1	10	7	11	10	3		·	4
V	12	5.0	5	3.0	0.5	2.0	7.5	1.3	6	3.3	21	3.5	13	4.0	13	4.0	15	3.0	87.5	15.1	29	·		·	·	1	·	·	13	19	14	3	·	·	5
VI	2.5	1.4	1	1.0	6.5	3.0	6.5	2.4	4	2.2	20	3.0	20.5	3.8	10	3.5	19	2.5	50.0	20.7	14	·	·	·	9	2	·	5	6	10	5	2	·	·	5
VII	0.5	1.0	0.5	1.0	1.5	2.3	0.5	1.0	6	3.0	26	3.2	32	4.0	9	3.2	17	2.8	116.1	43.9	31	·		·	5	1	·	2	24	19	15	1	·	·	7
VIII	1.5	2.7	1	2.0	1	4.0	4	2.4	3	2.8	32	3.5	21.5	3.6	8	2.8	21	2.6	66.2	14.5	11	·	·		5	·	·	2	8	13	10	3	3	·	5
IX	2.5	1.8	0.5	1.0	14	2.8	10	3.0	3.5	1.7	20	2.8	14.5	3.7	4	3.9	21	2.3	26.9	11.3	12	·	·	·	7	·	·	12	6	7	3	2	1	·	2
X	1	3.0	0.5	1.0	17	5.0	17	3.8	12	4.1	14	2.9	8.5	2.6	4	2.6	19	3.0	24.5	6.5	19	·	·	·	·	1	1	7	12	9	8	·	4	·	·
XI	3.5	4.1	8.5	6.2	9	6.8	5	2.0	2	1.5	27	3.9	3.5	3.7	8.5	2.8	23	3.2	31.7	16.1	13		·	7	·	4	1	2	19	13	5	1	9	·	·
XII	4.5	3.0	8.5	3.0	3.5	3.3	7	2.9	9	3.4	13	7.3	19	4.4	7.5	4.1	21	3.3	46.5	23.2	11	9	15	24	·	4	1	2	15	12	10	1	5	19	·
Rok	37	2.6	29.5	2.0	81.5	3.2	113.5	2.5	75	2.9	256	3.9	223.5	4.1	90	4.1	189	3.2	696.3	67.7	16.IV	21	26	77	27	38	6	53	150	157	106	18	34	42	28

Sinołęka $H_s = 160$ m $h_w = 11$ m

I	10	2.5	6	3.4	·	·	14.5	2.3	20.5	2.6	13	3.7	15.5	3.2	8.5	3.8	5	2.8	28.8	9.5	31	12	13	29	·	1	·	4	14	13	8	·	·	22[z]	—
II	5	2.0	1	2.0	2	2.5	11.5	3.0	18.5	3.5	11.5	2.0	21	3.0	6.5	3.3	7	2.7	13.3	3.4	1, 28	·	2	18	·	·	·	·	16	10	5	·	7	8	—
III	1	5.0	·	·	·	·	·	·	3	5.2	15	4.8	45.5	4.8	24.5	5.7	4	4.8	20.6	8.9	30	·	·	9	·	3	1	1	9	13	5	·	2	1	—
IV	8	2.6	5	3.1	14.5	4.0	18.5	4.3	6.5	2.5	7	2.1	10.5	5.8	5	4.9	15	3.2	18.5	7.4	2	·	·	6	·	2	·	10	3	8	5	·	1	·	—
V	3	1.7	0.5	1.0	7	2.1	13	1.8	7.5	2.0	8	1.8	12.5	3.1	20.5	2.4	21	1.7	57.8	11.3	28	·	·	·	2	·	·	·	11	14	10	2	·	·	—
VI	1.5	1.0	2	2.2	10	2.1	12.5	1.9	9	2.3	8	2.8	22.5	3.8	12.5	2.8	12	2.4	65.3	22.1	4	·		·	10	1	·	1	5	12	8	2	1	·	—
VII	3.5	1.3	·	·	2	1.0	3	3.0	11	3.2	16.5	2.0	27.5	2.3	12.5	2.3	17	1.9	89.0	23.3	28	·		·	5	1	1	3	9	15	13	3	1	·	—
VIII	5.5	1.2	1.5	1.7	2	2.0	1	1.0	11.5	2.2	19	2.8	23.5	3.0	17	2.8	12	2.3	52.8	14.0	22	·		·	5	2	2	2	6	12	9	2	·	·	—
IX	2	2.2	5.5	1.6	10.5	1.5	5	1.9	6	1.9	11.5	2.5	19.5	3.5	5	2.8	25	1.8	12.4	6.0	14	·	·	·	5	·	·	13	6	5	4	·	3	·	—
X	2	1.5	0.5	1.0	19	2.5	32.5	3.6	9.5	2.7	25	4.6	7	2.1	8	2.4	12	2.6	4.1	2.1	29	·	·	·	·	1	·	7	4	4	2	·	6	·	—
XI	5	3.4	5.5	2.2	9.5	5.2	16	2.7	8	3.2	10	3.2	14.5	3.6	6.5	2.9	15	2.8	66.4	11.0	12	·	2	13	·	1	·	1	20	18	12	2	4	2	—
XII	13.5	4.1	4.5	2.6	3.5	3.1	6	2.8	9.5	2.7	10	5.0	20.5	3.3	14.5	4.3	11	3.2	19.4	7.5	1	9	15	24	·	1	·	3	14	10	4	·	3	20	—
Rok	60	2.4	32	1.7	80	2.2	133.5	2.4	120.5	2.8	132	3.1	240	3.5	141	3.4	196	2.7	448.4	23.3	28.VII	21	32	99	27	13	4	45	117	134	85	11	28	53[?]	—

Pętkowo

$\varphi = 52°12'$ $\lambda = 17°15'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.3	−6.4	5.6	9	−19.0	27	−5.0	−1.2	−3.6	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.5	5.3	5.7
II	–	–	–	–	5.7	0.1	12.3	18	−4.2	6	1.4	4.7	2.5	2.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	5.7	7.3
III	–	–	–	–	9.8	2.1	17.9	10	−5.8	20	3.9	8.0	5.5	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	4.7	6.6
IV	–	–	–	–	15.7	5.0	25.3	7	−0.7	1	7.5	14.1	9.5	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.1	3.9	4.8
V	–	–	–	–	15.9	6.9	21.6	26	2.0	12	9.9	14.0	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.0	6.5	7.2
VI	–	–	–	–	23.5	12.3	28.9	26	6.1	22	16.1	21.9	17.2	18.1	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.9	4.2	4.3
VII	–	–	–	–	21.0	12.1	31.9	3	7.5	11	15.0	19.5	15.3	16.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	6.9	7.1
VIII	–	–	–	–	20.9	11.9	30.1	6	7.5	4, 18	14.4	19.4	15.2	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	6.0	6.5
IX	–	–	–	–	21.1	9.8	29.5	2	3.6	24	12.2	20.3	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.2	3.5	3.8
X	–	–	–	–	15.5	7.1	22.6	6	2.0	31	8.4	14.8	9.9	10.8	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.4	4.4	5.1
XI	–	–	–	–	6.4	1.8	14.1	3	−5.5	23	2.7	5.6	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.2	6.9	7.9
XII	–	–	–	–	−0.1	−7.2	15.4	5	−23.4	26	−4.2	−1.9	−3.8	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	5.6	6.8
Rok	–	–	–	–	12.9	4.6	31.9	3.VII	−23.4	26.XII	6.9	11.6	8.1	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	5.3	6.1

Koło

$\varphi = 52°12'$ $\lambda = 18°38'$

I	–	–	–	–	0.1	−5.7	6.4	4	−17.2	27	−4.4	−1.4	−2.9	−2.9	4.2	4.6	4.4	4.4	8.5	7.9	8.2	8.2	0.7	1.1	0.9	0.9	6.9	6.9	5.3	6.4
II	–	–	–	–	5.0	0.0	12.2	18	−3.8	6	1.2	3.8	2.1	2.3	6.3	6.8	6.5	6.5	9.3	8.4	9.0	8.9	0.5	1.4	0.7	0.9	8.6	7.9	6.9	7.8
III	–	–	–	–	9.6	2.4	17.5	10	−4.6	20	3.7	7.5	5.4	5.5	7.0	7.4	7.3	7.2	8.7	7.2	8.1	8.0	1.1	3.2	1.9	2.1	7.9	7.7	5.6	7.1
IV	–	–	–	–	16.3	4.9	25.3	7	−1.2	1, 10	7.2	14.5	9.9	10.4	8.3	8.7	9.0	8.7	8.0	5.3	7.1	6.8	2.1	8.8	3.7	4.9	6.0	5.0	4.0	5.0
V	–	–	–	–	16.7	7.0	22.4	26	2.5	12, 13	9.6	15.0	10.9	11.6	10.3	10.3	10.9	10.5	8.6	6.1	8.3	7.7	1.7	7.2	2.3	3.7	7.9	8.3	6.5	7.6
VI	–	–	–	–	24.3	12.5	32.3	27	6.3	22	16.5	22.7	17.3	18.4	15.2	14.1	15.7	15.0	8.0	5.2	7.9	7.0	3.8	14.1	4.3	7.4	4.8	6.5	5.4	5.6
VII	–	–	–	–	21.2	11.4	34.4	3	8.1	7	14.7	19.5	15.2	16.1	14.0	13.8	14.1	14.0	8.4	6.3	8.3	7.7	2.8	9.9	3.3	5.3	7.1	8.1	6.1	7.1
VIII	–	–	–	–	21.3	12.3	30.4	6	8.4	30	14.2	19.8	15.9	16.4	14.7	15.1	15.7	15.2	9.0	6.5	9.6	8.0	1.7	8.5	2.5	4.3	7.1	7.6	6.0	6.9
IX	–	–	–	–	21.0	9.3	30.4	2	2.8	24	10.7	19.9	13.4	14.4	12.3	13.3	13.3	13.0	9.3	5.7	8.5	7.8	0.9	10.6	2.3	4.6	4.7	4.8	4.1	4.5
X	–	–	–	–	15.5	6.8	21.8	6	2.7	31	7.9	14.6	10.3	10.8	9.8	11.3	10.7	10.6	9.2	6.9	8.6	8.2	0.9	5.6	1.9	2.8	7.1	7.4	3.9	6.1
XI	–	–	–	–	6.2	1.7	12.6	7	−6.2	23	2.8	5.2	3.5	3.8	7.1	7.6	7.4	7.4	9.3	8.4	9.2	9.0	0.5	1.4	0.7	0.9	8.2	8.7	7.6	8.2
XII	–	–	–	–	−0.5	−7.2	15.9	5	−22.8	17	−3.9	−2.0	−4.0	−3.5	4.6	4.7	4.4	4.6	8.4	7.9	8.5	8.3	0.9	1.3	0.7	1.0	7.4	7.4	5.2	6.7
Rok	–	–	–	–	13.1	4.6	34.4	3.VII	−22.8	17.XII	6.7	11.6	8.1	8.6	9.5	9.8	10.0	9.8	8.7	6.8	8.4	8.0	1.5	6.1	2.1	3.2	7.0	7.2	5.6	6.6

Niepokalanów

$\varphi = 52°12'$ $\lambda = 20°25'$

I	–	–	–	–	0.3	−5.8	6.2	4	−18.7	26	−4.1	−1.0	−3.2	−2.9	4.2	4.7	4.5	4.5	8.5	8.0	8.6	8.4	0.6	1.1	0.6	0.8	6.7	6.8	5.6	6.4
II	–	–	–	–	4.4	−0.1	11.0	18	−4.2	6	0.8	3.2	1.4	1.7	6.0	6.5	6.1	6.2	9.1	8.4	9.0	8.8	0.5	1.3	0.7	0.8	8.9	7.5	7.2	7.9
III	–	–	–	–	9.7	2.2	17.8	10	−2.3	20	3.7	7.6	5.3	5.5	6.9	7.4	7.2	7.2	8.6	7.1	8.0	7.9	1.2	3.3	1.9	2.1	7.8	7.5	5.9	7.1
IV	–	–	–	–	16.1	4.3	25.2	7	−2.7	10	7.0	14.3	9.2	9.9	8.1	8.7	9.0	8.6	7.8	5.3	7.5	6.9	2.2	8.5	3.1	4.6	5.1	4.6	3.4	4.4
V	–	–	–	–	17.5	6.9	26.0	27	1.9	19	10.4	15.7	11.1	12.1	10.6	10.6	11.0	10.7	8.3	6.0	8.3	7.5	2.2	7.8	2.4	4.1	6.4	6.7	6.2	6.4
VI	–	–	–	–	24.4	12.3	32.8	27	6.0	21	16.1	22.6	16.9	18.1	15.5	15.1	15.9	15.5	8.4	5.6	8.2	7.4	3.0	12.9	3.6	6.5	4.0	4.7	4.3	4.3
VII	–	–	–	–	21.5	11.2	31.8	3	8.0	6	14.6	19.5	15.2	16.1	14.6	14.5	14.9	14.7	8.7	6.5	8.6	7.9	2.2	8.8	2.6	4.5	6.9	7.1	5.6	6.5
VIII	–	–	–	–	21.5	12.2	31.1	6	6.9	30	14.4	20.0	15.4	16.3	14.8	15.4	15.7	15.3	9.0	6.6	8.9	8.2	1.8	8.5	2.1	4.1	5.9	6.5	5.2	5.9
IX	–	–	–	–	21.0	9.2	30.3	17	1.8	24	10.6	19.8	13.0	14.1	12.0	14.0	13.4	13.1	9.2	6.0	8.7	8.0	1.2	9.7	2.0	4.3	3.9	3.5	3.2	3.5
X	–	–	–	–	15.8	5.9	22.1	20	1.8	31	7.5	15.0	10.0	10.6	9.2	10.7	9.8	9.9	8.8	6.4	8.0	7.7	1.3	6.6	2.6	3.5	5.7	5.8	3.7	5.1
XI	–	–	–	–	6.4	1.4	13.9	3	−7.0	23	2.7	5.5	3.6	3.8	6.9	7.5	7.3	7.2	9.1	8.2	9.0	8.8	0.7	1.8	0.8	1.1	7.9	8.1	7.3	7.8
XII	–	–	–	–	0.0	−6.9	16.0	5	−23.7	26	−3.9	−1.9	−3.9	−3.4	4.7	4.8	4.3	4.6	8.6	8.0	8.2	8.3	0.7	1.3	0.9	1.0	7.8	6.9	5.7	6.8
Rok	–	–	–	–	13.2	4.4	32.8	27.VI	−23.7	26.XII	6.6	11.7	7.8	8.5	9.5	10.0	9.9	9.8	8.7	6.8	8.4	8.0	1.5	6.0	1.9	3.1	6.4	6.3	5.3	6.0

Łosice

$\varphi = 52°12'$ $\lambda = 22°43'$

I	–	–	–	–	−1.8	−7.6	6.3	4	−24.6	26	−5.5	−3.0	−4.7	−4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	7.0	7.3
II	–	–	–	–	2.5	−1.5	9.3	18	−5.5	6	−0.4	1.8	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.0	6.9	8.0
III	–	–	–	–	8.8	1.0	17.1	18	−3.4	20	2.5	6.8	4.0	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.3	5.1	6.9
IV	–	–	–	–	15.7	3.9	24.6	16	−3.2	10	6.4	13.8	8.4	9.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.2	3.0	4.5
V	–	–	–	–	17.2	6.8	26.5	29	2.5	15	10.7	15.4	10.9	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.1	6.5	7.5
VI	–	–	–	–	24.2	11.8	32.1	27	5.9	21	16.8	22.1	16.5	18.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	5.3	6.2
VII	–	–	–	–	22.9	11.2	33.5	3	6.1	6	15.8	20.5	15.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.9	6.4	6.7
VIII	–	–	–	–	21.8	11.9	30.5	7	8.2	25	14.4	20.2	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.3	6.9
IX	–	–	–	–	20.7	8.5	30.0	3	1.0	23	11.0	19.6	13.1	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.0	2.9	4.4
X	–	–	–	–	15.8	5.0	20.1	4	0.4	23	6.8	14.7	9.9	10.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.7	4.0	5.3
XI	–	–	–	–	5.5	0.9	13.4	3	−6.9	23	2.3	4.6	2.9	3.2	–	–	–	–	–	–	–	–	–	–	–	–	9.4	9.2	8.0	8.9
XII	–	–	–	–	−0.8	−7.2	15.5	5	−20.7	26	−4.6	−3.1	−4.4	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.5	6.4	7.6
Rok	–	–	–	–	12.7	3.7	33.5	3.VII	−24.6	26.I	6.4	11.1	7.3	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	5.6	6.7

Pętkowo $H_s = 86$ m $h_w = 13{,}5$ m 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr		○	●	Opad R			≡	⊠	R
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15			R ≥ 0.1	R ≥ 1.0	R ≥ 10.0			
I	2.5	3.6	5	4.1	21	2.9	16.5	2.9	22	3.5	18.5	5.0	5.5	4.6	1	2.0	1	3.6	28.6	8.1	14	12	11	26	·	1	·	7	9	9	7	·	9	15	·
II	3	3.0	2	1.5	10	3.2	13.5	3.8	18	4.6	19.5	4.2	11	4.4	6	2.7	1	3.9	25.2	13.6	9	·	·	12	·	2	1	2	14	6	5	1	16	·	·
III	3	3.7	·	·	·	·	·	·	2.5	2.6	28	6.7	47.5	8.4	12	4.0	·	7.0	42.9	10.9	30	·	·	6	·	13	4	2	11	14	10	1	7	·	·
IV	11.5	3.3	10	5.4	22	6.6	13.5	6.4	4	3.1	14	3.5	8.5	3.5	3.5	5.0	3	4.8	63.3	18.6	16	·	·	2	1	6	·	8	7	10	9	2	5	·	3
V	17	3.5	9	4.0	7.5	2.5	6	3.5	14	3.6	14.5	4.4	15	6.0	8	4.6	2	4.0	77.3	12.4	5	·	·	·	·	2	·	·	12	18	13	3	2	·	6
VI	4	2.4	3.5	4.1	13.5	3.1	10.5	3.4	9	2.7	16.5	3.7	25.5	5.6	5.5	3.3	2	3.9	48.2	17.9	10	·	·	·	11	2	·	4	4	7	7	1	1	·	6
VII	2.5	2.4	0.5	3.0	5.5	3.2	3.5	3.0	14.5	3.4	32.5	5.2	29	5.8	4	2.9	1	4.7	126.9	47.4	31	·	·	·	5	7	·	2	9	16	14	3	1	·	4
VIII	4	3.5	4.5	3.9	4.5	2.3	4.5	3.4	10.5	3.1	30.5	5.2	26.5	4.5	5	3.0	3	4.1	71.5	17.6	11	·	·	·	4	3	1	3	11	12	10	3	8	·	2
IX	6	2.2	6	2.5	20.5	3.4	12.5	2.8	12	3.0	17	4.4	12.5	5.5	2.5	2.6	1	3.5	12.8	5.4	5	·	·	·	7	2	·	14	8	5	3	·	5	·	2
X	3	2.3	1.5	1.3	23	6.2	21	4.8	18.5	3.7	11.5	3.5	8	2.9	5.5	2.4	1	4.2	27.0	8.9	19	·	·	·	·	5	·	9	9	8	6	·	12	·	·
XI	5.5	3.9	10.5	6.0	11.5	3.4	10	1.8	5.5	2.7	29	5.2	9	3.2	4	2.8	5	3.8	29.2	13.4	13	·	·	7	·	4	1	2	18	10	8	1	13	·	·
XII	6.5	2.9	10	3.1	8.5	3.7	10.5	2.6	12.5	3.0	13.5	5.5	20	5.1	6.5	4.2	5	3.8	41.6	19.0	11	10	16	24	·	2	·	4	15	11	9	1	12	16	·
Rok	68.5	3.1	62.5	3.2	147.5	3.4	122	3.2	143	3.2	245	4.7	218	5.0	63.5	3.3	25	4.3	594.5	47.4	31.VII	22	27	77	28	49	7	57	127	126	101	16	91	31	23

Koło $H_s = 95$ m $h_w = 11$ m

I	3.5	1.9	2.5	1.8	9.5	1.8	10.5	1.8	11.5	1.6	19	3.4	7.5	1.6	4	3.4	25	1.7	25.9	11.5	31	11	11	24	·	·	·	7	14	8	5	1	5	19	·
II	·	·	1	1.0	9.5	1.6	10	1.6	12.5	2.8	11	2.0	19.5	2.9	6.5	3.8	14	2.0	25.9	11.1	9	·	·	12	·	1	·	·	16	10	5	1	9	2	·
III	·	·	·	·	1	1.0	·	·	·	·	15.5	3.6	56	4.8	15.5	4.7	5	4.3	46.4	15.8	30	·		6	·	5	1	1	15	15	12	1	5	3	
IV	1	2.0	5.5	2.8	27	2.5	12.5	2.0	4.5	1.4	5.5	1.8	10	3.2	6	3.7	18	2.0	25.9	4.8	2	·		2	1	1	1	6	7	9	8	·	1	·	2
V	7.5	2.1	3	3.0	8	1.4	6.5	1.0	5	2.3	12	2.5	15.5	2.8	12.5	3.3	23	1.8	51.2	10.0	21	·	·	·	·	·	·	·	15	15	12	1	4	·	4
VI	1	1.5	4	2.0	11	2.4	5.5	1.8	7	1.9	9	2.1	24	3.6	6.5	3.7	22	2.1	70.6	26.4	8	·	·	·	14	·	·	1	6	10	8	3	1	·	9
VII	·	·	1	1.0	·	·	5	1.6	3.5	1.6	18	2.8	34	3.3	2.5	2.0	29	1.9	133.1	55.4	31	·	·	·	7	·	·	2	13	17	15	3	·	·	6
VIII	2	1.5	0.5	2.0	3	1.8	2.5	1.4	5	1.2	14.5	2.9	30	3.6	6.5	3.4	29	2.0	66.1	13.3	11		·	·	5	·	·	1	11	14	11	2	3	·	7
IX	2.5	2.0	1	1.0	16	1.7	8.5	2.4	5.5	1.5	4.5	2.4	21.5	3.4	0.5	2.0	30	1.6	15.4	9.7	14	·	·	·	7	·	·	10	9	7	5	·	2	·	3
X	1.5	2.7	2	1.5	24.5	2.7	14	2.3	11	1.9	7.5	2.3	7.5	2.5	4	2.5	21	2.0	27.4	9.7	18	·	·	·	·	·	·	4	8	9	4	·	5	·	
XI	4	2.0	5	2.6	16.5	3.3	5	1.3	8	1.4	14	2.5	11.5	3.7	5	2.3	21	2.4	58.8	16.7	13	·	·	8	·	·	·	1	20	20	11	1	7		·
XII	3.5	2.6	7	2.4	4	3.0	7	1.4	6.5	1.2	9.5	5.7	24	3.3	9.5	2.9	22	2.3	28.5	9.6	11	12	15	24	·	3	·	4	13	12	6	·	6	19	·
Rok	26.5	1.5	32.5	1.8	130	1.9	87	1.6	80	1.6	140	2.8	261	3.2	79	3.1	259	2.2	575.2	55.4	31.VII	23	26	76	34	10	2	37	147	146	102	13	48	43	31

Niepokalanów $H_s = 92$ m $h_w = 24{,}5$ m

I	5	2.0	6.5	2.6	11.5	2.3	6	4.0	9	2.7	22	4.2	20.5	2.9	9.5	3.4	3	3.1	28.2	9.8	31	8	12	26	·	1	·	6	12	16	8	·	8	12	·
II	2.5	2.6	·	·	1	1.0	11.5	3.3	13.5	2.9	14.5	4.2	19	3.6	17	3.6	5	3.3	20.4	6.0	9	·	·	14	·	1	·	·	13	14	5	·	9	1	·
III	1.5	3.3	·	·	·	·	·	·	·	·	8	6.6	45	5.9	36.5	6.4	2	6.0	36.4	17.5	30	·	·	8	·	5	·	2	10	14	9	1	4	1	·
IV	4.5	3.4	5.5	3.5	9.5	5.1	19.5	4.6	7	4.9	4.5	4.1	11	4.7	14.5	5.3	14	3.9	26.8	6.7	2	·	·	5	1	1		10	6	8	6	·	2	1	2
V	11.5	3.8	8	4.5	5	3.2	3	3.7	3	4.3	3	5.2	19.5	4.6	28	4.3	12	3.7	67.9	16.1	7	·	·	·	2	·	·	·	9	18	11	2	-	·	6
VI	1	4.0	1	1.0	7	3.4	11	4.5	10	2.8	10	3.5	28.5	4.1	14.5	3.4	7	3.4	65.9	21.1	27		·	·	13	·	·	4	2	15	13	1	2	·	8
VII	3	3.0	·	·	·	·	1.5	4.3	5	2.7	16.5	3.8	45.5	4.1	10.5	3.6	11	3.4	111.8	30.8	28	·	·	·	7	·	·	3	13	18	12	4	·	·	9
VIII	4	3.8	2	4.5	·	·		·	2	2.8	16.5	3.8	31.5	5.1	19	4.2	18	3.6	76.9	23.8	10	-	·		5		-	2	5	16	10	2	2		4
IX	5.5	2.9	6	3.3	7	3.1	4	3.8	4.5	3.2	12	3.8	19	5.4	11	4.5	21	3.2	25.2	13.2	14	·	·		6	1	-	11	4	8	3	1	·	·	2
X	2	2.5	1	7.0	5.5	4.1	39	4.5	13	4.0	10.5	3.6	6	4.1	7	4.6	9	3.8	8.1	3.6	29	·	·	·	·	·	·	4	5	6	2	·	8	·	·
XI	8	3.6	5.5	3.5	6.5	5.7	19.5	3.5	11	2.0	11	3.9	18	4.9	7.5	4.1	3	3.7	67.5	13.4	4	·	1	8	·	·	·	2	21	20	11	3	6	1	·
XII	13	4.2	3.5	4.0	8	2.1	9	2.6	6.5	2.8	8	4.9	23.5	5.1	20.5	4.0	1	4.0	23.2	9.1	11	9	14	24	·	·	·	2	12	14	6	·	2	16	
Rok	61.5	3.3	39	2.8	61	2.5	124	3.2	84.5	2.9	136.5	4.3	287	4.5	195.5	4.3	106	3.8	558.3	30.8	28.VII	17	27	85	34	9	·	46	112	167	96	14	43	32	31

Łosice $H_s = 153$ m $h_w = 14$ m

I	7	4.2	4.5	3.3	0.5	2.0	22.5	5.1	31.5	4.6	13	3.6	9	4.3	4	3.2	1	4.4	26.3	8.4	31	13	15	27	·	2		3	18	14	6	·	·	25	·
II	·	·	·	·	2.5	2.8	17	4.4	30	3.9	18	3.5	6.5	3.4	3	2.3	7	3.5	12.4	4.6	1	·	1	18	·	·	·	1	18	9	4	·	4	4	
III	·	·	·	·	·	·	1	7.5	11	5.1	31.5	5.0	45	5.4	4.5	5.5	·	5.2	17.5	7.4	30	·	·	11	·	4	·	·	12	11	6	·	·	·	1
IV	3	4.0	5.5	3.7	11	6.0	22.5	5.8	20	2.9	12	4.3	7	5.6	6	3.1	3	4.4	23.7	9.2	2	·	·	6	·	5	·	8	5	6	6	·	·	1	1
V	1.5	3.0	·	·	5.5	4.3	14.5	3.9	25.5	2.4	26	3.0	9	2.7	5	3.8	6	2.9	71.5	12.6	7	·	·	·	3	·		·	14	14	13	2	·		5
VI	2	2.0	·	·	7	4.1	22	4.0	22	3.4	30.5	3.3	4.5	2.8	1	3.0	1	3.5	36.3	11.8	28	·	·	·	12	·	·	1	7	11	7	1	·		6
VII	1.5	3.0	0.5	3.0	1.5	2.3	7.5	3.8	28.5	3.2	45	3.4	4	3.6	2.5	3.6	2	3.3	59.4	29.2	30	·	·	·	8	·	·	3	10	12	7	2	·	·	3
VIII	1	3.0	·	·	1	3.0	7	2.5	22.5	3.1	44	3.7	13	3.9	2.5	2.2	2	3.4	38.2	10.3	15	·	·		7	·	·	·	10	15	7	1		·	4
IX	1	4.0	·	·	15	4.2	11.5	3.4	20	3.2	23	4.5	15.5	3.1	1	3.0	3	3.6	18.8	4.5	6	·	·	·	6	1	·	10	6	9	6		2	·	2
X	·	·	0.5	4.0	27.5	6.4	34	7.1	11.5	3.6	9.5	2.4	7	3.0	1	1.0	2	5.4	4.2	2.4	29	·	·	·	·	5	2	5	7	2	2	·	5	·	·
XI	5	3.8	3.5	4.1	14.5	6.6	18	4.6	16	2.4	20.5	4.6	8	4.4	3.5	5.0	1	4.4	58.4	12.0	14	·	1	15	·	·	·	1	24	15	10	2	2	2	·
XII	6	4.2	1	4.5	4	4.6	18	3.1	11	5.0	26	4.4	9.5	3.5	10.5	4.0	7	3.8	15.6	4.5	1	11	15	25	·	1	·	1	19	12	5	·	1	24	·
Rok	28	2.6	15.5	1.9	90	3.9	195.5	4.6	249.5	3.6	299	3.8	138	3.8	44.5	3.3	35	4.0	382.3	29.2	30.VII	24	32	102	36	18	2	33	150	130	79	8	14	56	22

Siedlce

$\varphi = 52°11'$ $\lambda = 22°16'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1001.6	1023.3	981.7	1020.7	−0.9	−7.1	6.5	4	−21.5	26	−5.2	−2.5	−4.1	−4.0	4.1	4.6	4.3	4.3	89	85	88	87	0.4	0.8	0.5	0.6	7.0	7.5	6.7	7.1
II	1003.5	1019.5	976.6	1022.4	2.9	−1.1	10.7	18	−4.9	6	−0.2	2.0	0.7	0.8	5.6	6.2	5.9	5.9	93	87	91	90	0.4	1.0	0.6	0.7	9.0	8.3	7.8	8.4
III	996.5	1016.1	975.2	1015.0	8.4	1.0	16.6	18	−3.1	20	2.4	6.7	4.0	4.3	6.6	7.4	7.0	7.0	90	75	86	84	0.8	2.6	1.2	1.5	8.3	7.9	6.0	7.4
IV	995.7	1007.6	983.9	1013.8	15.5	3.5	24.9	15	−4.3	10	6.3	14.0	8.6	9.3	8.1	8.8	8.9	8.6	84	55	77	72	1.7	8.1	2.7	4.2	6.1	5.6	3.6	5.1
V	993.6	1002.3	981.6	1011.7	17.0	6.6	26.0	29	1.7	15	10.2	15.3	10.8	11.8	10.9	10.9	11.4	11.1	86	64	87	79	1.8	7.2	1.9	3.6	7.7	7.9	6.3	7.3
VI	997.3	1009.5	987.6	1014.9	23.9	11.7	32.3	27	4.0	21	16.3	22.1	16.6	17.9	15.6	15.7	15.6	15.6	84	60	82	75	3.0	11.7	3.5	6.1	5.6	6.5	5.6	5.9
VII	995.5	1008.0	980.0	1013.2	22.0	10.9	31.1	3	6.4	6	15.0	20.3	15.3	16.5	14.5	14.3	14.7	14.5	85	61	84	77	2.7	10.2	3.0	5.3	6.6	7.4	6.9	7.0
VIII	997.8	1011.1	986.2	1015.5	21.4	11.8	30.7	6	6.7	31	14.4	20.1	15.4	16.3	14.6	15.3	15.0	15.0	89	66	85	80	2.0	9.0	2.8	4.6	6.8	7.3	6.3	6.8
IX	1001.2	1013.3	988.5	1019.1	20.5	7.5	29.2	3	−1.1	23	10.1	19.4	12.1	13.4	12.0	13.2	12.8	12.7	94	58	88	80	1.0	10.1	1.8	4.3	5.1	4.8	3.3	4.4
X	1002.9	1014.4	979.8	1021.0	15.8	4.9	22.6	19	−0.1	31	6.6	14.9	9.5	10.1	8.7	10.0	9.5	9.4	89	60	79	76	1.2	7.3	2.6	3.7	6.6	6.3	4.0	5.6
XI	996.6	1017.5	984.2	1015.1	5.6	0.8	13.7	3	−8.1	23	2.4	4.8	2.9	3.3	7.2	7.6	7.2	7.3	95	86	93	91	0.4	1.3	0.6	0.8	9.2	8.9	7.4	8.5
XII	997.0	1025.6	976.4	1016.0	−1.0	−7.6	14.8	5	−22.8	26	−4.8	−2.7	−4.2	−4.0	4.5	4.8	4.6	4.6	90	85	91	89	0.5	0.9	0.5	0.6	8.5	7.3	6.2	7.3
Rok	998.3	1025.6	975.2	1016.5	12.6	3.6	32.3	27.VI	−22.8	26.XII	6.1	11.2	7.3	8.0	9.4	9.9	9.7	9.7	89	70	86	82	1.3	5.8	1.8	3.0	7.2	7.1	5.8	6.7

Reguły

$\varphi = 52°10'$ $\lambda = 20°51'$

I	–	–	–	–	0.2	−7.2	5.7	4	−19.4	26	−4.5	−1.6	−3.4	−3.2	4.4	5.0	4.6	4.7	89	87	89	88	0.4	0.7	0.4	0.5	7.2	7.0	6.7	7.0
II	–	–	–	–	3.6	−0.5	9.6	18	−4.7	6	0.6	2.7	1.3	1.5	6.2	6.9	6.5	6.5	96	92	97	95	0.2	0.6	0.2	0.3	9.1	8.6	7.2	8.3
III	–	–	–	–	9.0	1.9	16.1	18	−2.2	29	3.4	7.1	5.0	5.1	7.2	7.8	7.7	7.6	92	77	87	85	0.7	2.6	1.3	1.5	8.8	8.1	5.9	7.6
IV	–	–	–	–	15.7	4.0	24.2	7, 15	−3.4	10	6.6	14.3	8.8	9.7	8.5	8.8	9.2	8.8	85	53	79	72	1.5	8.4	2.5	4.1	5.3	4.6	3.6	4.5
V	–	–	–	–	17.0	6.5	25.3	27	1.0	15	10.2	15.7	11.0	12.0	10.8	10.6	11.3	10.9	87	60	85	77	1.8	7.8	2.1	3.9	7.3	7.9	6.7	7.3
VI	–	–	–	–	23.9	11.8	32.3	27	5.4	21	16.4	22.1	16.1	17.7	15.4	15.3	15.5	15.4	83	58	84	75	3.4	11.9	3.0	6.1	4.9	7.0	6.0	6.0
VII	–	–	–	–	21.3	11.1	30.8	3	7.6	9	14.6	20.0	15.0	16.1	14.4	14.4	14.8	14.5	86	63	87	79	2.4	9.6	2.4	4.8	7.4	7.9	6.9	7.4
VIII	–	–	–	–	21.1	12.0	31.3	6	6.7	31	14.6	19.8	15.2	16.2	15.0	15.5	15.4	15.3	89	67	88	81	1.9	8.2	2.2	4.1	6.6	7.1	5.7	6.5
IX	–	–	–	–	20.5	8.6	29.8	3	0.6	23	11.1	19.6	12.4	13.9	12.4	13.4	13.3	13.0	92	59	90	80	1.3	10.2	1.6	4.4	4.4	4.2	3.5	4.0
X	–	–	–	–	15.5	5.0	22.0	20	0.5	31	7.2	14.6	9.6	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.1	4.5	5.6
XI	–	–	–	–	5.9	1.2	12.9	3	−7.8	23	2.5	5.2	3.4	3.6	7.3	8.1	7.7	7.7	97	90	96	94	0.2	1.0	0.4	0.5	9.3	8.6	7.4	8.1
XII	–	–	–	–	−0.6	−6.9	15.6	5	−24.0	26	−4.0	−2.2	−3.9	−3.5	4.8	5.2	4.7	4.9	92	89	92	91	0.5	0.7	0.4	0.5	8.5	7.5	6.9	7.6
Rok	–	–	–	–	12.8	4.0	32.3	27.VI	−24.0	26.XII	6.6	11.4	7.5	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	5.9	6.6

Brwinów

$\varphi = 52°08'$ $\lambda = 20°43'$

I	1007.8	1030.8	988.3	1020.4	0.0	−6.0	6.5	5	−20.4	26	−4.2	−1.6	−3.1	−3.0	4.3	4.6	4.4	4.4	87	79	84	83	0.6	1.1	0.8	0.8	7.2	7.1	6.1	6.9
II	1009.5	1024.8	981.5	1021.9	4.1	−0.2	10.5	18	−4.8	6	0.6	2.8	1.3	1.5	5.9	6.4	6.1	6.1	92	85	90	89	0.5	1.2	0.7	0.8	8.8	8.1	7.4	8.1
III	1003.6	1023.0	979.5	1015.7	9.3	2.1	16.3	10	−1.8	20	3.4	7.2	5.1	5.2	6.9	7.4	7.3	7.2	88	73	82	81	1.1	3.0	1.7	1.9	8.7	7.8	5.6	7.4
IV	1001.3	1013.1	991.2	1013.2	15.8	4.6	24.5	7	−3.5	10	6.9	14.0	9.2	9.8	8.0	8.5	9.0	8.5	78	53	75	69	2.3	8.4	3.1	4.6	5.3	4.8	3.6	4.6
V	999.9	1007.6	986.7	1011.7	17.1	6.9	25.9	27	1.7	19	9.9	15.2	10.9	11.7	10.7	10.6	11.2	10.8	87	62	85	78	2.0	7.3	2.1	3.8	7.0	7.3	6.7	7.0
VI	1003.1	1015.8	992.7	1014.7	23.8	12.5	32.7	27	5.7	21	16.1	22.1	16.5	17.8	15.4	15.1	15.8	15.4	84	58	84	75	3.1	12.1	3.2	6.1	5.0	6.1	5.3	5.5
VII	1001.3	1013.2	985.3	1013.0	21.2	11.7	31.2	3	7.7	6	14.5	19.5	15.2	16.1	14.4	14.6	14.7	14.6	87	66	85	79	2.2	8.7	2.9	4.6	7.0	7.8	6.4	7.1
VIII	1003.9	1017.6	992.1	1015.6	21.3	12.4	31.0	6	7.3	31	14.4	19.7	15.6	16.3	14.7	15.4	15.4	15.2	89	67	87	81	2.0	8.2	2.6	4.3	6.1	6.8	5.5	6.1
IX	1007.1	1018.7	994.0	1019.0	20.7	9.3	29.0	2, 3	0.8	23	11.0	19.4	12.8	14.0	12.0	13.4	13.3	12.9	88	59	88	79	1.6	9.9	2.0	4.5	4.6	4.0	3.6	4.1
X	1007.8	1019.9	982.4	1019.9	15.7	6.3	22.2	20	2.2	29	7.4	14.6	10.5	10.8	9.1	10.5	10.0	9.9	88	65	79	77	1.3	6.4	2.9	3.5	6.2	6.2	3.7	5.4
XI	1002.5	1024.7	990.2	1014.7	6.3	1.5	13.4	3	−7.7	23	2.7	5.2	3.7	3.8	7.1	7.6	7.4	7.4	93	84	90	89	0.6	1.6	0.9	1.0	8.2	8.7	7.4	8.1
XII	1003.6	1033.2	981.1	1016.2	0.0	−6.5	15.7	5	−21.7	26	−4.0	−2.1	−3.5	−3.3	4.6	4.8	4.5	4.6	86	80	87	84	0.8	1.2	0.8	0.9	8.2	7.7	5.8	7.2
Rok	1004.3	1033.2	979.5	1016.3	12.9	4.6	32.7	27.VI	−21.7	26.XII	6.6	11.3	7.8	8.4	9.4	9.9	9.8	9.7	87	69	85	80	1.5	5.8	2.0	3.1	6.9	6.9	5.6	6.5

Wielichowo

$\varphi = 52°07'$ $\lambda = 16°21'$

I	–	–	–	–	0.1	−6.9	5.8	30	−21.5	28	−4.9	−1.2	−3.7	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	5.2	5.8
II	–	–	–	–	6.6	−0.1	13.2	18	−5.0	6	1.5	5.4	2.8	3.1	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.2	6.2	7.5
III	–	–	–	–	10.3	1.7	19.2	10	−8.4	20	3.3	8.6	5.4	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	4.5	6.5
IV	–	–	–	–	15.9	4.9	25.6	7	−2.1	1	7.1	14.0	9.5	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.4	3.9	4.8
V	–	–	–	–	15.8	6.6	22.3	26	2.2	13	9.7	13.7	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.1	5.8	7.1
VI	–	–	–	–	23.4	11.3	29.8	25	4.7	22	16.2	21.8	16.6	17.8	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.2	5.7	5.1
VII	–	–	–	–	20.8	11.5	32.7	3	7.1	6, 8	14.6	19.2	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.1	7.6	7.8
VIII	–	–	–	–	20.9	11.1	30.2	6	5.8	4	14.0	19.3	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	4.7	6.3
IX	–	–	–	–	21.1	9.4	30.0	2	2.5	25	11.4	20.1	13.3	14.5	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.6	3.0	4.0
X	–	–	–	–	15.5	6.6	21.7	5, 6	−0.3	13	7.9	14.8	9.5	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.7	4.3	5.5
XI	–	–	–	–	6.4	0.9	13.3	2	−8.0	23	2.2	5.7	3.1	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.2	6.9	7.8
XII	–	–	–	–	0.5	−7.3	15.8	5	−24.6	26	−4.3	−1.5	−3.7	−3.3	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	5.5	6.8
Rok	–	–	–	–	13.1	4.1	32.7	3. VII	−24.6	26.XII	6.6	11.7	7.7	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.6	5.3	6.2

Siedlce

$H_s = 146\ m$ $H_b = 149{,}1\ m$ $h_w = 13\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%D, %mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n Temperatura T Min ≤ 10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	≥ 10	≥ 100	≡	▦	R ≥ 10
I	6.5	3.3	8.5	1.9	1	2.0	1.9	2.9	18.5	3.8	19.5	4.1	13.5	4.4	5.5	3.6	1	3.5	32.7	7.5	31	12	13	29	·	1	·	4	15	15	8	·	·	24	·
II	1	1.0	2	2.2	4.5	2.0	15.5	2.9	18	3.8	15.5	3.0	18	3.0	6.5	2.6	3	3.0	14.1	4.6	1	·	2	20	·	·	·	·	18	13	3	·	1.1	4	·
III	·	·	·	·	·	·	·	·	5	5.2	26.5	5.0	45.5	5.3	15	5.8	1	5.2	24.6	7.4	30	·	·	11	·	5	1	1	12	15	8	·	3	2	·
IV	9	2.2	8	3.9	20	3.7	13.5	4.0	6.5	2.8	12	3.3	10	5.4	7	3.6	4	3.5	28.7	7.7	2	·	·	7	·	2	·	7	6	8	7	·	3	1	1
V	5	2.3	5.5	3.3	9	2.7	11	2.7	8.5	3.2	16.5	2.1	14.5	3.6	17	4.1	6	2.9	78.3	19.4	7	·	·	·	3	1	1	·	15	13	11	2	2	·	5
VI	·	·	7.5	3.0	10.5	2.0	17	2.9	7	3.3	18	3.3	21	3.6	7	3.8	2	3.1	43.4	6.2	27	·	·	·	11	·	·	3	7	16	13	·	·	·	7
VII	7	1.8	3	2.2	2	3.0	4.5	3.4	11.5	3.4	29	4.1	25.5	2.9	4.5	3.0	6	3.1	75.3	23.9	28	·	·	·	6	·	·	3	13	16	10	2	·	·	4
VIII	3.5	2.0	1.5	2.0	2.5	1.6	2	2.2	10	3.2	27.5	5.1	24	3.4	13	3.0	9	3.4	47.8	12.6	10	·	·	·	6	3	3	2	10	15	12	2	1	·	5
IX	3	1.3	5.5	2.4	11.5	2.4	2	2.5	9	3.0	18	4.8	17	4.4	5	3.5	19	2.8	12.8	3.4	14	·	·	2	6	2	·	10	7	9	3	·	2	·	1
X	1.5	2.3	0.5	0.3	21.5	3.4	30.5	3.4	14	3.8	4.5	3.8	6.5	4.2	5	2.6	9	3.1	4.4	2.2	14	·	·	1	·	·	·	6	10	3	2	·	3	·	·
XI	8	4.1	5	3.7	10.5	4.9	18.5	3.0	8.5	2.8	14	4.8	13	3.6	5.5	3.8	7	3.5	63.9	11.8	14	·	1	14	·	·	·	1	20	20	12	2	6	2	·
XII	13	5.7	5.5	2.1	5	2.9	14	2.9	17.5	3.0	18	5.3	15	3.1	6	5.8	5	3.8	20.6	5.3	11	10	16	25	·	6	1	2	17	14	6	·	5	20	·
Rok	57.5	2.2	52.5	2.2	98	2.6	147.5	2.7	128	3.4	219	4.1	223.5	3.9	97	3.8	72	3.4	446.6	23.9	28.VII	22	32	109	32	20	6	39	150	157	95	8	42	53	23

Reguły

$H_s = 98\ m$ $h_w = 12\ m$ (I–VII) $14.5\ m$ (VIII–XII)

I	8	1.9	4	2.4	6	2.6	19	1.8	15	1.9	20.5	2.9	9	2.6	8.5	2.2	3	2.2	44.1	10.5	31	11	12	26	·	·	·	3	14	15	11	1	7	23	·
II	2.5	1.0	0.5	1.0	1	1.5	17	2.2	12.5	2.9	14	2.5	13.5	2.8	5	2.5	18	2.0	20.9	4.9	9	·	·	17	·	·	·	1	18	15	5	·	9	1	·
III	·	·	·	·	1	7.0	0.5	2.0	1.5	2.7	27.5	3.7	48.5	3.8	11	3.6	3	3.6	34.5	15.9	30	·	·	7	·	1	·	·	13	14	5	1	4	·	·
IV	4	2.6	3.5	1.4	18.5	2.8	13	3.4	3	1.7	6	3.4	11	2.9	8	2.6	23	2.1	28.3	6.8	2	·	·	4	·	·	·	9	8	10	8	·	3	·	2
V	6	2.8	2.5	1.0	7	1.6	8.5	2.0	3.5	3.0	12.5	1.6	15	2.4	20	2.2	18	1.7	45.2	14.1	7	·	·	·	1	·	·	·	11	17	13	1	1	·	6
VI	1	2.0	4.5	1.2	4.5	2.1	13	1.7	5	1.5	12.5	1.3	23.5	2.1	5	1.9	21	1.4	64.5	17.9	27	·	·	·	12	·	·	1	5	15	12	1	3	·	10
VII	4.5	1.8	0.5	1.0	2.5	3.0	3	3.0	7	2.8	29.5	2.1	21	2.3	4	3.0	21	1.8	91.5	24.1	28	·	·	·	6	·	·	3	17	18	14	2	1	·	5
VIII	5.5	1.7	1	2.0	·	·	3.5	2.1	12	1.5	17	2.3	26	2.3	11	1.7	17	1.7	63.7	21.2	10	·	·	·	5	·	·	1	8	15	12	2	4	·	3
IX	4.5	1.3	2.5	1.8	12	1.9	14	1.9	6.5	1.8	13	2.0	30.5	2.5	2	2.5	5	2.0	23.3	7.7	12	·	·	·	5	·	·	10	6	7	3	·	7	·	1
X	1	1.0	1	2.0	22.5	3.3	29.5	3.6	11	2.0	3.5	1.9	10.5	2.3	4	1.8	10	2.6	7.6	2.8	14	·	·	·	·	·	·	5	7	4	3	·	9	·	·
XI	7	2.6	6	3.3	11.5	3.3	16.5	2.3	6.5	1.9	10.5	3.6	20	3.6	9	2.2	3	2.8	80.7	14.4	13	·	2	9	·	·	·	2	20	20	13	3	5	·	·
XII	9	4.2	4.5	2.4	2	3.0	14	2.3	11	2.0	11.5	4.5	27.5	4.1	13.5	3.5	·	3.5	32.1	11.0	11	9	14	23	·	1	·	3	17	14	7	1	5	16	·
Rok	5.3	1.9	30.5	1.6	88.5	2.7	151.5	2.4	94.5	2.1	178	2.6	256	2.8	101	2.5	142	2.3	536.4	24.1	28.VII	20	28	86	29	2	·	38	144	164	106	12	58	40	27

Brwinów

$H_s = 96\ m$ $H_b = 98{,}0\ m$ $h_w = 11\ m$

I	4.5	2.2	4	2.4	3	2.5	1.9	2.7	14.5	3.7	19.5	4.4	11.5	3.5	3	4.0	14	2.9	25.6	9.5	31	10	13	25	·	1	·	5	16	11	7	·	2	18	·
II	2.5	2.4	0.5	2.0	4.5	2.3	13	3.0	11.5	4.0	20.5	3.6	16	3.3	4.5	2.3	11	2.9	17.0	4.5	1.9	·	·	15	·	1	·	·	18	11	4	·	10	1	·
III	·	·	·	·	·	·	1.5	5.7	2.6	5.6	52.5	5.3	·	·	10	6.4	3	5.3	29.0	14.3	30	·	·	8	·	6	3	·	15	12	5	1	4	·	·
IV	1.5	3.7	5	3.0	16	3.5	16	4.8	4	3.0	8	4.1	14	4.4	8.5	2.5	17	3.1	25.6	6.3	2	·	·	3	·	1	1	7	6	11	7	·	·	·	3
V	5.5	2.3	1.5	1.7	8	1.9	9	2.4	3.5	3.3	12	3.7	21	3.0	15.5	4.0	17	2.5	51.8	13.7	7	·	·	·	1	·	·	·	10	17	13	1	·	·	2
VI	·	·	1	2.0	12.5	2.8	12	3.1	6	2.4	17	2.9	21.5	3.3	5	3.0	15	2.5	81.3	14.6	10	·	·	·	11	·	·	2	5	15	13	4	1	·	8
VII	1	4.0	1	2.0	0.5	2.0	5.5	2.5	8	2.7	23	4.0	32.5	3.3	5.5	2.9	16	2.8	117.1	30.0	30	·	·	·	6	·	·	2	15	18	13	4	1	·	5
VIII	1.5	2.3	·	·	1.5	3.0	4.5	2.1	6	2.5	27	3.8	27	2.9	9.5	3.2	16	2.6	61.2	19.5	10	·	·	·	5	·	·	2	6	15	9	2	1	·	3
IX	·	·	·	·	16.5	2.5	6.5	2.9	5.5	2.6	15.5	3.9	20	3.7	6	4.1	20	2.6	19.6	6.4	12	·	·	·	5	1	·	11	6	8	4	·	·	·	1
X	·	·	·	·	3.0	3.7	2.5	4.2	12.5	2.4	5.5	4.0	9	2.7	4	2.2	7	3.2	5.3	2.1	29	·	·	·	·	·	·	6	6	3	3	·	7	·	·
XI	8	2.7	3.5	3.9	14	4.0	13	2.7	6.5	2.7	20.5	4.3	10	3.7	5.5	2.4	9	3.2	73.4	16.0	4	·	1	8	·	·	·	2	20	19	11	2	4	·	·
XII	7.5	3.2	2.5	2.8	2	2.5	12.5	2.5	9	2.9	17.5	5.7	24	3.6	10	3.8	8	3.4	23.1	9.5	11	8	14	23	·	2	·	3	16	12	5	·	1	17	·
Rok	3.2	1.9	19	1.6	108.5	2.6	137.5	3.2	113	3.2	238.5	4.1	206.5	3.1	87	3.4	153	3.1	530.0	30.0	30.VII	18	28	82	28	12	4	40	139	152	94	14	31	36	22

Wielichowo

$H_s = 65\ m$ $h_w = 10\ m$

I	·	·	1.5	1.7	18.5	2.1	9.5	1.7	9.5	2.7	24.5	2.7	9.5	2.7	3	2.0	17	1.9	32.8	10.8	14	12	11	23	·	·	·	8	12	11	7	1	·	17	·
II	1	2.0	1	1.0	5.5	2.3	9.5	2.3	15.5	2.1	22	2.6	13.5	3.5	8	2.2	8	2.3	22.8	10.7	9	·	·	16	·	·	·	1	15	12	7	1	5	·	·
III	1.5	2.3	·	·	·	·	·	·	·	·	15	2.7	53.5	4.5	10	3.7	13	3.5	39.4	13.5	30	·	·	9	·	2	·	2	9	16	8	1	3	·	·
IV	2.5	1.8	7.5	1.9	2.7	2.9	12.5	3.0	6	2.2	8	1.6	6.5	3.2	4	1.8	16	2.1	69.4	17.8	15	·	·	2	1	·	·	10	9	10	9	3	1	·	4
V	10	2.0	8	2.2	3.5	2.4	7	2.4	6.5	1.3	12.5	2.9	17.5	3.5	7	2.4	21	2.0	104.6	21.0	29	·	·	·	·	·	·	2	11	20	16	3	·	·	5
VI	5	1.5	5	1.6	8.5	1.9	10.5	1.4	3	2.5	5.5	1.9	21	2.5	4.5	1.8	27	1.4	34.8	15.1	4	·	·	·	9	·	·	7	6	10	6	1	·	·	6
VII	0.5	1.0	3	1.0	·	·	4.5	1.4	8.5	1.4	23.5	2.2	26.5	2.1	3.5	1.7	23	1.5	80.4	22.1	31	·	·	·	5	·	·	2	17	19	14	1	·	·	4
VIII	4.5	1.4	2	1.0	1.5	2.0	1.5	2.7	2.5	1.6	22.5	1.8	21.5	2.1	4	1.6	33	1.2	53.4	10.9	22	·	·	·	4	·	·	2	7	17	11	1	3	·	5
IX	1	1.0	4	1.6	16	1.8	2	3.0	4.5	2.2	10	1.6	15.5	2.2	2	1.3	35	1.2	49.8	31.6	5	·	·	·	7	·	·	12	5	9	5	1	1	·	3
X	1.5	3.0	2.5	3.2	2.0	2.7	1.8	2.1	9	2.1	6	2.2	3.5	2.9	3.5	1.9	29	1.7	19.8	6.0	29	·	·	1	·	·	·	7	10	13	7	·	5	·	·
XI	6	1.6	10	3.6	5.5	4.2	1.5	3.0	3.5	2.0	16	3.1	9.5	2.5	5	2.0	33	1.8	37.3	20.9	13	·	·	10	·	·	·	1	19	12	6	1	6	·	·
XII	5	1.4	6	2.1	13	2.2	10.5	1.5	3.5	1.3	10	4.8	18	3.1	7	1.8	20	2.0	41.9	11.9	11	11	14	24	·	·	·	4	15	11	10	1	·	15	·
Rok	38.5	1.6	90.5	1.7	119	2.8	87	2.0	72	1.8	175.5	2.5	216	2.9	61.5	2.0	275	1.9	586.4	31.6	5.IX	23	25	85	26	2	·	58	135	160	106	15	24	32	27

Łowicz

$\varphi = 52°07'$ $\lambda = 19°56'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA t					Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.1	−6.5	5.9	4	−20.3	27	−4.4	−1.5	−3.3	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	6.2	7.2
II	–	–	–	–	4.6	−0.1	11.6	18	−4.8	6	1.0	3.4	1.5	1.8	–	–	–	–	–	–	–	–	–	–	–	–	9.9	8.4	8.1	8.8
III	–	–	–	–	9.5	2.3	17.6	10	−3.3	20	3.7	7.4	5.4	5.5	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.4	6.7	8.1
IV	–	–	–	–	15.7	4.6	25.4	7	−2.3	10	7.4	14.3	9.6	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.4	4.3	5.3
V	–	–	–	–	16.9	7.0	24.4	27	1.5	19	10.4	15.2	10.9	11.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.2	7.3	7.9
VI	–	–	–	–	23.7	12.5	32.5	27	6.9	21	16.6	21.9	16.9	18.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.8	6.0	6.0
VII	–	–	–	–	21.5	11.7	33.7	3	8.1	6	15.2	19.1	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	4.3[2]	5.2	6.7	5.4[2]
VIII	–	–	–	–	21.4	12.6	31.2	6	7.6	30	14.9	19.8	16.1	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.6	5.9	6.2
IX	–	–	–	–	20.5	9.4	29.8	2	2.2	23	11.5	19.4	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.0	4.0	4.6
X	–	–	–	–	15.8	5.9	21.5	20	2.4	10	8.1	14.9	10.2	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.6	4.8	6.2
XI	–	–	–	–	6.5	1.2	12.9	3	−6.4	23	2.9	5.3	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.8	7.7	8.3
XII	–	–	–	–	0.1	–	16.3	5	–	–	−3.5	−2.0	−3.5	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.3	6.5	7.6
Rok	–	–	–	–	13.0	–	33.7	3.VII	–	–	7.0	11.4	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.2	6.8

Świder

$\varphi = 52°07'$ $\lambda = 21°15'$

I	–	–	–	–	−0.4	−6.8	7.3	4	−22.9	26	−5.1	−1.4	−4.0	−3.6	4.1	4.5	4.3	4.3	86	76	84	82	0.5	1.2	0.7	0.8	7.3	7.8	7.0	7.4
II	–	–	–	–	3.7	−0.7	10.0	18	−5.5	5	0.2	2.8	0.9	1.2	5.7	6.3	5.9	6.0	91	83	90	88	0.5	1.3	0.7	0.8	9.2	8.5	8.1	8.6
III	–	–	–	–	9.6	1.3	17.6	18	−3.6	23	3.3	7.7	4.7	5.1	6.7	7.0	7.1	6.9	86	67	82	78	1.2	3.8	1.7	2.2	9.1	7.8	5.8	7.6
IV	–	–	–	–	16.3	3.6	25.7	15	−5.9	10	6.7	15.2	8.4	9.7	7.9	7.7	8.3	8.0	78	44	72	65	2.2	10.6	3.2	5.3	5.9	4.7	2.7	4.4
V	–	–	–	–	17.9	6.5	26.5	27	1.4	17	10.3	16.4	10.8	12.1	10.8	10.1	10.9	10.6	85	56	84	75	2.0	9.3	2.3	4.5	7.1	7.7	6.0	6.9
VI	–	–	–	–	24.4	11.8	34.0	27	4.2	21	16.8	23.0	16.6	18.2	15.4	14.0	15.1	14.8	81	51	79	70	3.9	14.7	4.0	7.5	5.5	6.4	5.5	5.8
VII	–	–	–	–	21.8	11.3	31.3	3	6.5	6	14.9	20.2	15.3	16.4	14.0	13.6	14.4	14.0	83	59	83	75	3.2	10.8	3.2	5.7	7.3	7.8	6.4	7.2
VIII	–	–	–	–	21.7	11.9	31.6	6	5.8	31	14.3	20.5	15.3	16.4	14.4	14.5	15.0	14.6	88	60	86	78	2.0	10.3	2.6	5.0	5.9	7.3	5.6	6.3
IX	–	–	–	–	21.1	8.3	30.2	3	0.3	23	10.4	20.2	12.4	13.8	11.8	12.3	12.6	12.2	92	58	86	77	1.2	12.1	2.1	5.1	5.8	4.8	2.7	4.4
X	–	–	–	–	16.0	5.6	23.5	19	0.7	29	7.2	15.1	10.3	10.7	8.8	10.0	9.4	9.4	86	60	76	74	1.6	7.6	3.4	4.2	6.6	6.6	4.0	5.7
XI	–	–	–	–	6.3	1.0	13.8	3	−7.9	23	2.5	5.4	3.4	3.7	7.1	7.6	7.3	7.3	93	83	91	89	0.5	1.6	0.8	1.0	9.5	9.1	7.8	8.8
XII	–	–	–	–	−0.1	−7.1	15.7	5	−23.6	17	−4.2	−1.8	−3.8	−3.4	4.4	4.6	4.4	4.5	84	76	85	82	0.8	1.5	0.8	1.0	8.5	7.2	6.4	7.4
Rok	–	–	–	–	13.2	3.9	34.0	27.VI	−23.6	17.XII	6.4	11.9	7.5	8.3	9.3	9.4	9.6	9.4	86	64	83	78	1.6	7.1	2.1	3.6	7.3	7.1	5.7	6.7

Śrem

$\varphi = 52°05'$ $\lambda = 17°01'$

I	–	–	–	–	0.0	−6.9	6.0	9	−20.9	27	−5.1	−1.2	−3.9	−3.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.9	5.8	6.0
II	–	–	–	–	6.3	0.3	12.4	18	−3.6	6	1.4	4.9	2.8	3.0	–	–	–	–	–	–	–	–	–	–	–	–	9.4	7.2	6.0	7.5
III	–	–	–	–	10.2	2.1	18.2	10	−6.1	20	3.9	8.5	5.2	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	5.8	7.0
IV	–	–	–	–	16.0	5.1	25.4	7	−0.7	1	7.1	14.3	9.5	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.4	4.1	5.2
V	–	–	–	–	16.2	7.0	22.9	26	2.7	12, 13	9.7	14.1	10.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.5	7.3	7.9
VI	–	–	–	–	23.7	11.7	29.0	26	5.5	22	16.4	21.7	16.4	17.7	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.7	4.4	4.9
VII	–	–	–	–	21.3	11.8	32.7	3	7.4	6	14.9	19.5	15.1	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	8.0	7.7
VIII	–	–	–	–	21.2	11.8	30.9	6	7.6	4	14.2	19.6	15.1	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.9	5.3	6.3
IX	–	–	–	–	21.3	9.7	29.8	2	3.3	24	11.5	20.2	14.1	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.7	3.7	4.4
X	–	–	–	–	15.7	7.3	22.1	6	2.0	31	8.2	14.7	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.0	5.1	6.0
XI	–	–	–	–	6.3	1.5	13.0	2	−6.7	23	2.7	5.6	3.3	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.9	8.3
XII	–	–	–	–	0.1	−2.2	15.3	5	−23.1	27	−4.3	−1.8	−3.8	−3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.6	6.9
Rok	–	–	–	–	13.2	4.5	32.7	3.VII	−23.1	27.XII	6.7	11.7	7.9	8.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	5.8	6.5

Topola - Błonie

$\varphi = 52°05'$ $\lambda = 19°11'$

I	–	–	–	–	−0.3	−6.5	6.9	4	−20.2	26	−5.1	−1.4	−3.7	−3.5	4.3	4.8	4.6	4.6	91	83	90	88	0.3	0.9	0.4	0.5	6.5	6.8	4.7	6.0
II	–	–	–	–	4.6	−0.4	11.2	18	−3.9	6	0.7	3.5	1.4	1.8	6.2	6.8	6.5	6.5	96	87	95	93	0.2	1.1	0.4	0.6	9.2	7.2	7.1	7.8
III	–	–	–	–	9.2	1.5	17.6	10	−4.6	20	3.0	7.3	4.8	5.0	7.2	7.8	7.5	7.5	93	77	87	86	0.6	2.7	1.3	1.5	8.0	7.2	6.6	7.3
IV	–	–	–	–	16.1	3.8	25.4	7	−2.9	10	6.7	14.6	8.9	9.8	8.7	9.3	9.3	9.1	86	56	80	74	1.4	8.2	2.4	4.0	4.8	3.9	3.9	4.2
V	–	–	–	–	17.2	6.6	24.0	27	1.0	13	9.5	15.4	10.6	11.5	10.8	11.6	11.1	11.2	90	67	86	81	1.2	6.4	1.9	3.2	6.7	7.0	7.0	6.9
VI	–	–	–	–	24.1	11.7	31.4	27	6.0	21	16.2	22.6	16.5	18.0	16.2	16.2	15.8	16.1	87	60	84	77	2.4	11.7	3.2	5.8	4.4	4.7	5.2	4.8
VII	–	–	–	–	21.1	10.7	31.9	3	6.4	8	14.3	19.8	14.7	15.9	14.6	15.0	14.5	14.7	90	67	87	81	1.8	8.8	2.4	4.3	6.8	6.7	5.8	6.4
VIII	–	–	–	–	21.4	11.9	31.1	6	7.4	30	14.1	19.7	15.3	16.1	15.2	16.1	15.9	15.7	94	70	90	85	1.1	7.4	1.8	3.4	6.3	6.5	6.6	6.5
IX	–	–	–	–	20.7	8.9	28.6	17	2.3	24	10.9	19.8	12.8	14.1	12.6	14.6	13.4	13.5	95	64	89	83	0.8	9.2	1.7	3.9	4.2	3.8	3.2	3.7
X	–	–	–	–	–	6.2	–	–	2.1	14	7.4	14.5	9.8	10.4	9.8	12.0	10.9	10.9	95	73	90	86	0.6	4.8	1.3	2.2	6.5	6.1	5.1	5.9
XI	–	–	–	–	–	1.4	–	–	−5.6	23	2.5	5.3	3.4	3.6	7.3	8.1	7.6	7.7	97	89	96	94	0.3	1.0	0.4	0.6	7.8	8.0	8.1	8.0
XII	–	–	–	–	−0.7	−6.4	15.0	5	−20.8	26	−4.0	−2.4	−3.9	−3.6	4.7	4.9	4.6	4.7	90	86	88	88	0.6	0.9	0.6	0.7	8.0	7.4	6.3	7.2
Rok	–	–	–	–	–	4.1	31.9	3.VII	−20.8	26.XII	6.4	11.6	7.6	8.3	9.8	10.6	10.1	10.2	92	73	89	85	0.9	5.3	1.5	2.6	6.6	6.3	5.8	6.2

Łowicz — $H_s = 95$ m — $h_w =$ 12 m I–VI, 14 m VII–XII — 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R > 0.1	R > 1.0	R > 10.0	≡	⊞	R/▽
I	2	4.5	9	1.3	0.5	2.0	16	1.8	24	1.9	9.5	2.4	7	1.7	1	3.0	24	1.4	17.8	7.4	31	9	12	25	·	·	·	2	15	10	6	·	5	—	·
II	1	2.0	·	·	7	2.0	16	1.8	18.5	1.6	5	4.1	13.5	1.4	5	1.4	18	1.4	21.2	5.4	1	·	·	14	·	1	1	·	20	14	7	·	8	—	·
III	·	·	·	·	·	·	1	1.0	6	3.0	20.5	4.0	46.5	2.9	14	3.7	5	3.1	25.0	8.3	30	·	·	7	·	4	2	·	17	16	5	·	4	—	·
IV	3.5	1.3	8	2.0	21.5	2.8	10.5	3.3	7.5	1.5	2	2.0	11	1.0	11	2.3	15	1.9	21.8	5.7	16	·	·	3	1	1	1	6	10	8	4	·	6	—	3
V	11	1.8	2	1.5	2	1.5	12	1.8	10	1.6	10	1.4	13	1.5	19	1.6	14	1.3	55.9	12.8	30	·	·	·		·	·	·	18	15	10	2	·	—	7
VI	3	1.3	1	3.0	7.5	1.4	14.5	1.3	6	1.0	9	1.3	26	1.7	10	1.8	13	1.3	68.4	23.0	7	·	·	·	11	2	·	1	6	13	11	2	3	—	10
VII	3	1.5	1	1.0	1	1.0	0.5	1.0	17	2.0	5.5	2.5	47	2.5	10	2.2	8	2.1	116.4	25.6	28			·	6	·	·	4	10	17	17	4	1	—	1
VIII	2.5	1.8	·	·	3.5	3.4	1.5	2.7	13.5	2.3	22.5	3.6	30.5	2.4	11	2.9	8	2.5	65.6	35.7	10		·	·	5	2	·	3	8	14	6	2	2	—	1
IX	5	1.2	2	1.5	12.5	1.1	9	1.2	5	1.3	11.5	1.6	22	2.2	7	1.7	16	1.3	34.1	14.3	14	·	·	·	6	·	·	8	7	8	6	1	6	—	2
X	·	·	1	1.0	13.5	2.0	36.5	1.7	10	1.7	8	1.9	8.5	1.5	5.5	1.9	10	1.5	8.7	4.3	29	·	·	·	·	1	·	3	10	6	3	·	11	—	·
XI	7	1.4	4	2.4	13	1.3	11	1.0	6	1.0	10	2.6	19	2.0	5	1.2	15	1.4	72.0	15.5	13	·	·	11	·	1	·	1	21	15	12	3	8	—	·
XII	10	1.7	10.5	1.3	4	3.8	7	1.7	10.5	1.4	12	4.7	24.5	2.1	13.5	1.8	1	2.2	15.7	6.6	11	—	15	—	·	3	·	1	17	7	3	·	6	—	·
Rok	48	1.5	38.5	1.2	86	1.9	135.5	1.7	134	1.7	125.5	2.7	268.5	1.9	112	2.1	147	1.8	522.6	35.7	10.VIII	—	27	—	29	15	4	29	159	143	90	14	60	—	24

Świder — $H_s = 94$ m — $h_w = 16{,}9$ m

I	8	2.2	1	2.0	-	-	12	2.2	31	2.1	9.5	2.4	8.5	2.4	10	2.2	13	1.9	42.5	17.1	31	12	13	26	·	·	·	4	18	16	8	1	4	22	·
II	2.5	1.2	0.5	2.0	2	1.0	15	1.9	22	2.8	8	2.4	14	2.2	9	2.1	11	2.0	22.4	6.2	28	·	·	18	·	·	·	1	21	13	6	·	11	5	·
III	2.5	1.6	·	·	·	·	0.5	3.0	2.5	2.8	17	3.7	43.5	3.7	23	3.6	4	3.5	25.5	8.9	30	·	·	11	·	·	·	·	16	15	7	·	5	2	1
IV	4	1.6	7.5	2.5	13.5	3.0	18.5	3.0	10.5	2.6	5.5	3.3	11	3.8	7.5	3.4	12	2.6	35.3	11.8	17	·	·	5	1	·	·	9	5	8	7	1	3	1	2
V	10	2.4	4.5	1.4	6	1.7	9.5	2.3	13.5	2.3	8.5	2.1	10.5	2.4	14.5	2.4	16	1.8	49.6	8.0	28	·	·	·	3	·	·	·	9	16	11	·	·	·	3
VI	2.5	4.0	5	2.0	9.5	2.2	12	2.4	14.5	2.0	11	2.4	18.5	2.7	7	3.0	10	2.2	77.2	21.5	27	·	·	·	13	·		1	5	16	12	2	·	·	11
VII	4	2.8	0.5	3.0	3	1.7	9	2.6	12	2.2	24	3.1	23.5	2.6	5	2.9	12	2.3	90.5	19.3	28	·	·	·	7	·	·	2	14	17	16	2	1	·	8
VIII	1.5	1.0	1.5	2.0	0.5	2.0	7.5	2.7	9.5	1.9	15	3.4	22.5	2.9	15	2.7	20	2.2	58.6	15.4	10	·	·	·	7	·	·	3	7	15	9	1	1	·	4
IX	3.5	1.9	5	1.4	7	2.1	8.5	2.1	8	1.7	9.5	3.8	17	2.9	3.5	2.4	28	1.7	18.6	6.0	14	·	·	·	6	·	·	9	6	6	4	·	1	·	1
X	1	2.0	1.5	2.4	17	2.9	36.5	3.1	9.5	2.6	4	3.0	7.5	2.4	4	2.1	12	2.5	5.4	3.7	29	·	·	·	·	·	·	7	11	5	2	·	5	·	·
XI	10	2.4	6	2.7	8	3.2	20	2.6	8	2.1	8.5	3.6	12	3.0	5.5	2.2	12	2.4	80.9	13.4	5	·	1	10	·	·	·	·	22	19	12	4	9	·	·
XII	14	2.6	1.5	1.3	4.5	2.2	10	2.2	15	2.3	8.5	3.4	21	2.7	13.5	2.8	5	2.5	24.9	6.3	11	9	14	26	·	·	·	2	16	16	6	·	1	20	·
Rok	63.5	2.1	34.5	1.9	71	1.8	159	2.5	156	2.3	129	3.0	209.5	2.8	117.5	2.6	155	2.3	531.4	21.5	27.VI	21	28	96	37	·	·	38	150	162	100	11	41	50	30

Uwaga. Kierunki i prędkości wiatru – wg anemografu.

Śrem — $H_s = 85$ m — $h_w = 10$ m

I	2	1.0	16.5	1.3	6.5	1.2	8.5	1.5	18.5	2.2	11.5	1.9	5	2.5	6.5	1.5	18	1.4	31.5	10.1	14	12	11	23	·	·	·	7	14	10	6	1	3	20	·
II	3	1.0	3.5	1.0	9.5	1.4	4.5	1.8	12.5	2.5	13	2.4	14.5	3.3	11.5	1.7	12	1.8	23.1	9.2	9	·	·	13	·	·	·	1	15	12	6	·	7	2	·
III	1.5	2.3	·	·	·	·	·	·	2.5	1.6	23.5	4.0	46	4.6	16.5	2.5	3	3.8	39.3	13.6	30	·	·	6	·	1	·	3	16	13	9	1	1	2	·
IV	4.5	1.0	16	2.0	17	2.3	7.5	1.5	2.5	1.6	5.5	1.5	9.5	2.9	8.5	1.6	19	1.6	119.7	39.8	16	·	·	2	1	·	·	7	10	9	9	4	·	·	3
V	19	1.3	2.5	1.0	2.5	1.0	5	1.2	4	1.2	11.5	1.9	15	2.3	16.5	2.4	17	1.5	108.0	20.7	29	·	·	·	·	·	·	·	17	19	17	2	·	·	4
VI	4	1.2	5.5	1.2	7.5	1.4	5	1.4	2.5	1.4	6.5	2.1	24.5	3.1	9.5	1.4	25	1.5	36.5	15.4	10	·	·	·	12	·	·	4	6	10	8	1	·	·	6
VII	1	1.0	1.5	1.0	0.5	0.1	5	1.4	9	1.2	21.5	2.6	34.5	2.3	6	2.5	14	1.8	104.6	43.8	31	·	·	·	5	·	·	2	18	19	12	3	·	·	1
VIII	3.5	1.0	5.5	2.1	1.5	1.7	2	1.0	7	1.9	22.5	2.6	17	2.8	5	2.6	29	1.6	66.0	16.2	11	·	·	·	5	·	·	2	8	10	8	4	5	·	3
IX	3	1.0	15	1.3	11	1.7	2.5	1.4	6	1.1	16.5	2.1	12.5	2.7	0.5	4.0	23	1.4	8.6	3.5	5	·	·	·	7	·	·	10	7	7	2	·	2	·	2
X	4	1.2	10	1.8	16	2.3	7.5	1.4	15.5	1.7	5	2.4	4	2.2	6	1.5	25	1.4	21.9	5.5	19	·	·	·	·	·	·	6	13	8	8	·	5	·	·
XI	10	1.6	15.5	1.8	2	1.0	2	1.0	4.5	2.1	17.5	3.0	6.5	2.7	6	1.2	26	1.5	35.9	19.5	13	·	·	9	·	·	·	2	21	13	8	1	7	·	·
XII	6	1.0	7.5	1.1	6	2.0	5	1.1	9	1.9	12	4.0	13	3.1	10.5	2.8	24	1.8	41.4	15.0	11	10	13	23	·	·	·	4	15	12	10	1	2	20	·
Rok	61.5	1.2	99	1.3	80	1.3	54.5	1.2	93.5	1.7	166.5	2.5	202	2.9	103	2.1	235	1.8	636.5	43.8	31.VII	22	24	76	30	1	·	48	160	142	103	18	32	44	19

Topola – Błonie — $H_s = 109$ m — $h_w =$ 10 m I–X, 12 m XI–XII

I	1	7.0	6.5	2.5	14.5	1.2	3	2.0	11.5	1.9	32.5	3.5	11.5	2.5	3.5	3.1	9	2.4	25.3	9.9	31	12	11	24	·	1	·	6	9	9	5	·	4	19	·
II	2.5	2.8	0.5	2.0	3.5	2.4	5	1.9	6.5	2.9	28.5	2.9	19	2.9	8.5	2.4	10	2.3	22.6	8.7	9	·	·	18	·	1	·	·	13	12	7	·	11	·	·
III	0.5	6.0	·	·	·	·	·	·	·	·	13	6.9	48	6.4	28.5	6.5	3	6.3	45.4	13.3	30	·	·	9	·	8	2	2	14	15	12	1	4	1	·
IV	0.5	2.0	8.5	2.4	17.5	2.8	13	3.2	2	3.0	15	2.7	8.5	4.1	9	3.3	16	2.5	21.2	7.2	2	·	·	5	1	1	·	10	4	8	6	·	1	·	2
V	8	2.8	11	2.2	1	1.0	2.5	1.7	1.5	1.7	25	2.6	21	3.5	22	3.0	1	2.8	47.7	10.2	7	·	·	·	·	1	1	·	13	14	11	1	2	·	5
VI	4	1.4	9.5	2.1	6.5	3.4	3	2.2	2.5	2.4	16	2.8	24	3.2	20.5	3.1	4	2.7	104.5	36.8	7	·	·	·	12	1	1	4	3	12	10	3	3	·	9
VII	0.5	1.0	·	·	·	·	1	1.0	1.5	3.0	38.5	4.0	26.5	3.2	17	2.5	8	3.1	145.1	54.1	31	·	·	·	7	2	·	3	9	17	13	4	·	·	8
VIII	4.5	2.1	1.5	2.7	1.5	3.0	2	2.2	1.5	1.0	28.5	4.4	30.5	3.9	11	3.2	12	3.3	105.4	36.6	10	·	·	·	5	1	·	2	8	14	12	4	·	·	6
IX	5	1.7	5	1.5	8	2.0	7.5	2.4	2	2.0	14	3.6	18	2.9	12.5	2.4	18	2.1	39.1	15.5	14	·	·	·	7	·	·	15	5	8	6	1	1	·	2
X	1.5	2.3	·	·	19	2.9	17.5	2.6	8.5	2.7	19.5	3.2	9.5	2.9	6.5	2.5	11	2.5	17.7	5.7	7	·	·	·	·	·	·	4	9	9	3	·	10	·	·
XI	9.5	2.7	6	5.1	9.5	3.1	3	2.7	4	1.6	21	3.5	16	4.5	4	2.6	17	2.8	79.6	26.4	13	·	·	9	·	1	·	1	19	16	13	1	7	·	·
XII	7.5	4.9	8	4.2	3	4.8	5.5	1.7	13.5	5.0	16.5	5.8	13.5	4.7	12.5	4.4	13	4.0	26.1	8.8	11	9	16	25	·	5	·	3	15	11	6	·	6	16	·
Rok	45	3.1	56.5	2.1	84	2.2	63	2.0	55	2.3	268	3.8	246	3.7	155.5	3.2	122	3.1	679.7	54.1	31.VII	21	27	90	32	22	4	50	121	145	104	15	49	36	32

Terespol

$\varphi = 52°05'$ $\lambda = 23°37'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnio																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1003.4	1023.6	982.1	1020.8	-1.5	-8.2	6.0	4	-24.0	26	-5.9	-3.1	-4.7	-4.6	4.0	4.5	4.3	4.3	91	86	90	89	0.4	0.7	0.4	0.5	7.5	7.5	7.0	7.3
II	1005.4	1022.2	978.6	1022.5	2.6	-1.4	8.8	18	-4.8	7	-0.6	1.7	0.5	0.5	5.6	6.0	5.8	5.8	95	86	91	91	0.3	1.0	0.6	0.6	8.9	8.4	7.1	8.1
III	997.5	1017.7	978.1	1014.3	8.2	0.8	17.3	18	-4.1	23	2.7	6.4	4.2	4.2	6.6	7.0	7.0	6.7	89	72	85	82	0.9	3.0	1.4	1.8	9.1	8.0	5.6	7.6
IV	997.4	1009.4	984.5	1013.8	15.4	3.7	25.0	16	-2.6	10	6.1	13.8	8.9	9.4	7.7	7.9	8.3	8.0	80	50	70	67	1.9	8.8	3.5	4.7	6.0	5.6	3.0	4.9
V	995.2	1003.8	983.7	1011.5	17.4	6.8	26.2	28	2.5	19	10.5	15.6	11.6	12.3	10.8	10.3	11.0	10.7	84	60	81	75	2.2	8.7	2.9	4.4	6.8	7.5	5.5	6.6
VI	998.8	1010.3	990.0	1014.7	24.1	12.0	32.3	27	5.8	21	16.6	22.2	17.5	18.5	14.6	14.1	14.6	14.4	77	55	73	68	4.6	13.4	5.7	7.9	4.8	6.5	5.1	5.5
VII	996.9	1008.9	983.3	1012.8	23.0	11.6	30.7	3	7.8	9	15.4	20.9	16.5	17.3	14.1	13.4	13.9	13.8	81	55	74	70	3.5	12.0	5.1	6.9	5.3	7.2	6.2	6.2
VIII	998.9	1012.2	988.1	1014.9	22.1	12.0	30.3	7	7.5	31	14.4	20.5	15.8	16.6	14.6	14.4	14.9	14.6	89	60	84	78	2.0	10.6	3.1	5.2	6.9	7.4	5.8	6.7
IX	1002.6	1015.3	990.6	1018.8	20.6	7.7	29.6	3	-1.3	23	10.0	19.2	12.7	13.7	11.8	12.3	12.4	12.1	93	56	82	77	1.0	10.9	2.9	4.9	4.3	5.2	2.8	4.1
X	1005.2	1015.9	984.0	1021.6	15.5	4.7	20.6	19	-0.8	23	5.9	14.5	9.4	9.8	8.8	10.0	9.5	9.4	93	62	81	79	0.7	6.8	2.3	3.3	6.6	5.9	4.4	5.6
XI	998.3	1018.4	985.2	1015.1	5.2	0.5	13.7	3	-7.6	23	2.1	4.5	2.6	3.0	7.1	7.6	7.2	7.3	96	88	94	93	0.3	1.3	0.4	0.7	9.2	9.5	7.4	8.7
XII	998.3	1027.1	978.4	1015.6	-1.4	-7.9	14.5	5	-23.2	27	-4.9	-3.1	-4.5	-4.3	4.5	4.8	4.5	4.6	91	87	91	90	0.4	0.8	0.5	0.6	8.7	7.6	7.0	7.8
Rok	999.8	1027.1	978.1	1016.3	12.6	3.5	32.5	27.VI	-24.0	26.I	6.0	11.1	7.5	8.0	9.2	9.4	9.4	9.3	88	68	83	80	1.5	6.5	2.4	3.5	7.0	7.2	5.6	6.6

Młochów

$\varphi = 52°03'$ $\lambda = 20°47'$

I	–	–	–	–	-0.3	-6.4	5.9	5	-20.3	26	-4.6	-1.8	-3.1	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	5.4	6.8
II	–	–	–	–	3.8	-0.3	11.2	18	-5.4	6	0.5	2.6	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.9	7.0	8.4
III	–	–	–	–	9.0	2.1	16.5	10	-2.5	20	3.4	7.0	5.2	5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.7	5.3	7.2
IV	–	–	–	–	15.6	4.4	24.5	15	-3.1	10	7.1	13.9	8.9	9.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.3	3.6	4.8
V	–	–	–	–	16.8	6.9	25.4	27	1.0	19	10.1	15.0	10.1	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.2	6.2	7.3
VI	–	–	–	–	23.6	12.3	32.4	27	6.5	21	16.4	21.7	16.2	17.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	7.0	5.7	6.0
VII	–	–	–	–	21.1	11.5	30.7	3	7.5	6	14.6	19.4	14.9	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.8	6.8	7.4
VIII	–	–	–	–	21.1	12.5	30.7	6	7.7	31	15.1	19.4	15.5	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.7	5.6	6.6
IX	–	–	–	–	20.4	9.7	28.9	2	1.2	23	11.2	19.3	13.2	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.9	3.3	4.6
X	–	–	–	–	15.6	5.9	21.9	19, 20	2.2	23	7.2	14.6	10.4	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	4.3	6.2
XI	–	–	–	–	6.1	1.2	13.2	3	-6.6	23	2.5	5.0	3.4	3.6	–	–	–	–	–	–	–	–	–	–	–	–	9.1	9.1	6.9	8.4
XII	–	–	–	–	-0.3	-6.9	15.4	5	-22.5	26	-4.1	-2.4	-3.9	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.8	6.7	7.8
Rok	–	–	–	–	12.7	4.4	32.4	27.VI	-22.5	26.XII	6.6	11.1	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	5.6	6.8

Trzebiechów

$\varphi = 52°01'$ $\lambda = 15°44'$

I	–	–	–	–	–	–	–	–	–	–	-4.8	-0.4	-3.8	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.0	5.6	6.2
II	–	–	–	–	–	–	–	–	–	–	1.9	6.2	3.3	3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.4	5.5	6.9
III	–	–	–	–	–	–	–	–	–	–	4.3	9.0	5.6	6.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.1	4.9	6.7
IV	–	–	–	–	–	–	–	–	–	–	8.3	15.1	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.6	4.8	5.1
V	–	–	–	–	–	–	–	–	–	–	10.3	14.2	10.4	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	8.3	6.6	7.3
VI	–	–	–	–	–	–	–	–	–	–	15.7	22.2	17.1	18.0	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.7	5.2	4.6
VII	–	–	–	–	21.7	11.9	34.8	3	8.1	8	15.0	19.5	15.6	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.8	11.9	31.2	6	7.9	14	14.3	19.8	15.7	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	22.3	9.7	31.6	2	2.4	25	12.0	20.8	14.6	15.5	–	–	–	–	–	–	–	–	–	–	–	–	3.6	3.6	2.8	3.3
X	–	–	–	–	16.5	6.9	23.0	5, 6	1.1	31	8.2	15.5	11.0	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.3	–	13.4	2	–	–	2.4	5.8	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.3	6.0	7.3
XII	–	–	–	–	–	–	–	–	–	–	-3.8	-1.2	-2.9	-2.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.4	5.6	5.8
Rok	–	–	–	–	–	–	–	–	–	–	7.0	12.2	8.4	9.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Biała Podlaska

$\varphi = 52°01'$ $\lambda = 23°08'$

I	–	–	–	–	-1.3	-8.0	7.2	4	-23.5	26	-5.7	-2.5	-4.9	-4.5	3.9	4.3	4.1	4.1	88	78	86	84	0.5	1.1	0.5	0.7	7.7	7.3	6.6	7.2
II	–	–	–	–	2.7	-1.5	8.4	18	-4.7	7	-0.6	1.7	0.5	0.5	5.5	5.8	5.6	5.6	94	83	88	88	0.4	1.2	0.8	0.8	9.3	8.4	7.4	8.4
III	–	–	–	–	8.3	1.4	17.2	18	-3.7	23	2.6	6.5	4.4	4.5	6.2	6.9	6.7	6.6	85	71	80	79	1.1	3.1	1.8	2.0	9.0	8.3	5.5	7.6
IV	–	–	–	–	15.8	3.5	25.1	15	-3.4	10	6.3	13.9	8.5	9.3	7.9	9.0	8.7	8.5	80	55	75	70	1.9	8.1	2.8	4.3	6.6	5.9	3.1	5.2
V	–	–	–	–	17.3	6.6	26.2	28, 29	1.8	5	10.5	15.4	10.9	11.9	11.1	11.6	11.6	11.4	87	68	88	81	1.9	6.6	1.7	3.4	7.8	8.3	6.8	7.6
VI	–	–	–	–	24.4	11.9	32.9	27	5.3	21	16.8	22.5	16.9	18.3	15.8	16.4	16.0	16.1	82	62	83	76	3.6	11.6	3.5	6.2	6.5	7.0	6.3	6.6
VII	–	–	–	–	22.7	11.4	30.7	3	7.1	6, 9	15.4	21.0	15.9	17.1	14.7	15.2	15.3	15.1	83	62	84	76	3.1	10.3	3.8	5.5	5.6	7.4	6.7	6.6
VIII	–	–	–	–	22.3	12.1	31.5	11	7.6	31	14.7	20.6	15.7	16.7	14.8	15.9	15.8	15.5	88	66	88	81	2.1	9.3	2.3	4.6	7.2	7.2	5.9	6.8
IX	–	–	–	–	21.3	8.0	30.9	3	-1.6	23	10.2	20.3	12.7	14.0	11.7	13.2	12.6	12.5	90	55	83	76	1.3	11.5	2.7	5.2	5.1	5.3	3.0	4.5
X	–	–	–	–	15.8	4.8	21.0	19	-0.4	12	6.4	15.0	9.6	10.1	8.6	9.9	9.6	9.4	88	59	80	76	1.2	7.5	2.4	3.7	7.1	5.7	4.3	5.7
XI	–	–	–	–	5.5	0.8	14.0	3	-7.7	23	2.4	4.7	2.8	3.2	6.9	7.2	7.1	7.1	92	83	92	89	0.6	0.5	0.7	0.6	9.9	9.1	8.0	9.0
XII	–	–	–	–	-1.1	-7.7	14.8	5	-22.8	27	-4.6	-2.8	-4.4	-4.1	4.4	4.8	4.5	4.6	86	83	88	86	0.6	0.9	0.6	0.7	9.2	8.4	6.5	8.0
Rok	–	–	–	–	12.8	3.6	32.9	27.VI	-23.5	26.I	6.2	11.4	7.4	8.1	9.3	10.0	9.8	9.7	87	69	85	80	1.5	6.8	1.9	3.1	7.6	7.6	5.8	6.9

Terespol

$H_s = 133\,m$ $H_b = 135{,}0\,m$ $h_w = 12{,}5\,m$ **1961**

MIESIĄC	ROZKŁAD WIATRU (fD, vmD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min <-10°	Max <0°	Min <0°	Max ≥25°	Wiatr v ≥10	v ≥15	●	●	Opad R ≥0.1	≥1.0	≥10.0	≡	≡	≋
I	16	3.1	4.5	2.3	0.5	3.0	1.5	2.8	16.5	2.8	12	3.4	10.5	3.2	11	4.1	7	2.9	24.4	7.6	31	13	13	28		·	·	2	18	14	5	·	1	26	·
II	5.5	1.4	4	2.4	6	2.4	5	2.7	14.5	3.5	6.5	2.5	18	2.1	21.5	2.5	3	2.5	4.1	1.6	11	·	2	19	·	·	·	1	18	10	2	·	5	8	·
III	1.5	5.0	·	·	·	·	·	·	3.5	3.9	13.5	4.8	36.5	5.3	36	4.3	2	4.7	18.0	3.3	30	·	·	9	·	3	·	·	14	16	7	·	2	2	·
IV	17	2.1	9	3.7	16	3.3	9	4.7	7	2.4	9.5	2.5	11.5	3.7	11	2.3		3.0	25.0	8.5	2	·	·	4	·	·	·	7	5	8	5	·	1	·	·
V	11	2.0	3.5	2.0	8.5	2.8	8.5	2.0	6.5	3.4	10.5	2.1	14.5	2.2	26	2.5	4	2.3	39.6	8.4	16	·	·	·	3	·	·	2	11	14	11	·	2	·	4
VI	2.5	1.8	6.5	3.2	12	2.5	8.5	2.7	9	2.2	7.5	2.0	22.5	2.2	18.5	2.6	3	2.4	53.5	13.2	12	·	·	·	13	·	·	3	5	12	7	2	·	·	7
VII	8	1.9	2	3.0	·	·	2	2.5	8	3.0	13	2.4	26.5	2.8	26.5	2.1	7	2.3	47.6	31.6	30	·	·	·	7	·	·	3	6	11	4	1	·	·	5
VIII	8	2.4	2	2.0	·	·	·	·	9.5	2.7	17.5	2.6	17.5	3.1	28.5	2.9	10	2.5	70.4	34.0	3	·	·	·	7	·	·	1	9	15	8	2	1	·	4
IX	1.5	1.9	1.0	2.3	7	1.7	0.5	1.0	3	4.0	12.5	2.4	10.5	4.0	25.5	2.5	6	2.4	10.4	4.4	12	·	·	1	6	·	·	11	6	6	2	·	4	·	1
X	1	3.0	7.5	3.5	22.5	3.9	27.5	3.9	15.5	2.4	1	2.5	4	2.9	13	2.7	1	3.4	2.4	0.9	29	·	·	2	·	·	·	4	8	3	·	·	5	·	·
XI	1.0	3.4	4.5	3.6	16.5	4.8	11.5	4.0	7.5	2.7	5.5	3.0	24	2.5	7.5	2.4	3	3.3	67.7	15.5	14	·	2	16	·	·	·	·	20	17	10	2	10	3	·
XII	18.5	4.3	5	3.4	3	4.0	1.3	2.5	12	2.2	8.5	4.5	11.5	3.3	16.5	3.5	5	3.2	28.8	5.8	1	11	16	26	·	·	·	1	17	17	7	·	3	24	·
Rok	114	2.7	58.5	2.6	92	2.4	100.5	2.4	112.5	2.9	117.5	2.9	207.5	3.1	241.5	2.9	51	2.9	391.9	34.0	3.VIII	24	33	105	36	3	·	35	137	143	68	7	34	63	21

Młochów

$H_s = 141\,m$ $h_w = 12{,}5\,m$

I	1	7.0	5.5	2.6	2	2.8	14.5	2.7	21	3.5	24	4.9	10.5	4.9	3.5	3.7	1.1	3.5	23.6	9.2	31	12	13	25	·	2	·	5	16	12	7		3	19	·
II	1	3.5	·	·	5.5	2.4	10.5	1.6	2.2	4.0	2.4	4.4	11	5.2	3	3.2	7	3.5	18.4	5.9	9	·	·	15	·	·	·	·	18	10	4	·	6	2	·
III	·	·	·	·	·	·	·	·	1.5	5.7	4.0	6.4	4.1	2.0	7.5	9.3	3	6.7	21.5	6.9	30	·	·	9	·	8	2	·	13	16	7	·	3	·	·
IV	2	5.0	5	4.1	16	4.4	14.5	3.8	8	4.2	11	5.2	12.5	5.7	5	6.7	16	3.9	20.3	5.9	2	·	·	5	·	1	1	6	7	9	5	·	2	1	2
V	3	4.0	2.5	1.6	7	2.9	10	2.9	9.5	3.1	19.5	3.9	14.5	4.3	11	4.5	16	3.0	50.7	5.3	7.8	·	·	·	1	1	·	·	11	16	14	·	·	·	5
VI	1	3.5	0.5	5.0	14	2.8	12	2.8	8.5	2.2	27	3.9	15.5	4.0	5.5	4.4	6	3.3	64.1	19.4	27	·	·	·	12	·	·	3	6	15	13	1	·	·	8
VII	2	2.0	0.5	1.0	2	2.5	3.5	2.9	15	3.1	42.5	4.0	12.5	3.6	7	2.9	8	3.3	80.0	19.8	28	·	·	·	6	·	·	1	15	17	11	2	·	·	7
VIII	3	3.3	·	·	4	2.2	2.5	1.8	10	3.0	3.9	4.3	15	4.3	10.5	3.4	9	3.5	84.6	28.0	10	·	·	·	5	·	·	1	8	11	6	3	1	·	2
IX	1.5	2.7	2.5	1.8	10.5	3.0	10.5	2.8	10.5	3.8	19.5	4.6	16.5	4.8	2.5	5.4	1.6	3.2	17.5	5.5	12	·	·	·	5	1	·	10	6	8	5	·	1	·	·
X	·	·	3	2.8	2.4	3.8	2.3	3.6	16.5	3.8	8.5	3.6	7.5	4.6	4.5	3.9	6	3.5	4.5	1.8	29	·	·	·	·	·	·	2	8	4	2	·	6	·	·
XI	1.1	3.4	5	4.8	1.3	6.0	1.5	2.2	7	3.8	2.1	4.8	9.5	4.3	3.5	4.0	5	4.0	74.2	18.0	13	·	2	9	·	1	·	·	20	19	11	2	4	1	·
XII	3.5	6.0	7.5	5.7	5	5.0	7.5	2.0	1.2	3.2	27.5	5.4	18	4.9	8	4.4	4	4.4	20.2	10.3	11	9	15	24	·	2	·	1	17	9	4	1	5	17	·
Rok	2.9	3.4	3.2	2.4	10.3	3.2	123.5	2.4	141.5	3.6	303.5	4.6	18.4	4.8	71.5	4.6	107	3.8	479.6	28.0	10.VIII	21	30	87	29	16	3	29	145	146	89	9	31	40	24

Trzebiechów

$H_s = 55\,m$ $h_w = 10{,}4\,m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	38.6	8.3	14	–	–	–	–	–	–	–	–	–	10	·	–	15	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	13.8	5.4	8	–	–	–	–	–	–	–	–	–	4	·	–	·	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.1	15.2	30	–	–	–	–	–	–	–	–	–	12	1	–	·	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	46.5	11.2	1	–	–	–	–	–	–	–	–	–	8	1	–	·	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	96.7	21.6	5	–	–	–	–	–	–	–	–	–	15	3	–	·	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	30.6	16.1	4	–	–	–	–	–	–	–	–	–	6	1	–	·	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	81.3	18.0	17	·	·	·	7	–	–	–	–	–	12	3	–	·	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.0	8.5	6	·	·	·	7	–	–	–	–	–	9	·	–	·	–
IX	3.5	1.6	0.5	1.0	7.5	2.3	5.5	1.9	4	3.1	6	3.4	21.5	3.7	5.5	4.1	36	1.9	13.6	4.0	5	·	·	·	8	·	·	–	–	–	5	·	–	·	–
X	1	4.5	1	3.0	6.5	4.0	17.5	3.9	7	2.3	7	2.4	12.5	3.6	2.5	5.0	3.8	2.1	46.0	24.0	20	·	·	·	·	1	·	–	–	–	8	1	–	·	–
XI	3	3.2	6	2.6	9	4.4	2	2.2	·	·	7.5	3.3	2.3	3.6	3.5	4.7	3.6	2.2	41.0	20.4	13	–	·	·	·	·	·	–	–	–	7	1	–	·	–
XII	1	4.0	5	2.8	3	2.8	3.5	1.7	2	1.5	8	3.6	2.8	4.2	5.5	6.9	3.7	2.4	40.8	9.5	11	–	–	–	·	2	·	–	–	–	9	·	–	15	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	541.0	24.0	20.X	–	–	–	–	–	–	–	–	–	105	11	–	30	–

Biała Podlaska

$H_s = 145\,m$ $h_w = 12\,m$

I	9	2.8	3	1.8	1.5	2.0	1.9	2.1	14.5	2.2	18.5	2.3	12	2.7	13.5	2.6	2	2.3	29.1	8.7	31	13	13	28	·	1	·	3	15	18	8	·	4	26	·
II	2	1.0	2.5	1.6	2	2.5	6.5	2.4	12.5	2.6	16.5	1.7	19.5	1.5	3.5	1.0	1.9	1.4	11.6	4.9	1	·	3	19	·	·	·	·	21	12	3	·	8	12	·
III	·	·	·	·	·	·	1	3.0	4	2.5	1.7	3.2	43.5	3.4	17.5	4.2	10	3.1	20.0	3.0	30	·	·	6	·	·	·	·	16	15	10	·	2	·	1
IV	1.5	1.7	4.5	2.0	13.5	3.3	8	3.8	5	1.3	9	2.1	9	4.6	5.5	2.0	3.4	1.8	23.1	11.0	2	·	·	6	·	·	·	5	3	6	5	1	1	·	·
V	2	3.5	2	1.8	5	2.3	7	1.9	3	2.8	3	1.7	1.6	2.6	10	1.9	4.5	1.2	48.9	8.5	7	·	·	·	2	·	·	·	14	15	10	·	1	·	·
VI	2	1.5	3	3.3	9	2.9	7.5	1.9	4.5	2.4	11	2.4	16	2.8	4	2.3	3.3	1.6	70.2	29.2	12	·	·	·	14	·	·	·	8	9	9	2	1	·	7
VII	1	1.5	1	1.5	1	5.0	6.5	2.6	8.5	3.5	12.5	2.9	22.5	3.0	6	2.7	3.4	1.9	63.7	28.0	30	·	·	·	7	·	·	3	9	10	9	2	1	·	6
VIII	1	1.0	·	·	·	·	1	3.0	5.5	3.8	1.8	3.6	21.5	3.7	1.4	4.0	3.2	2.4	19.8	3.8	7	·	·	·	8	1	·	·	10	16	6	·	·	·	2
IX	3.5	2.4	3	2.3	2	3.0	1.5	3.7	5	2.3	9	5.7	14.5	3.9	6.5	4.5	4.5	1.9	12.2	4.7	14	·	·	1	7	·	·	10	5	5	3	·	2	·	1
X	·	·	4	3.4	17.5	5.4	24.5	5.2	5.5	4.0	1.5	4.0	7	4.0	4	3.0	2.9	3.3	6.3	3.9	14	·	·	1	·	2	·	6	9	4	2	·	7	·	·
XI	6	3.1	3.5	4.9	14.5	5.4	9.5	3.8	4	3.6	11.5	3.7	10.5	3.7	2.5	2.8	2.8	2.8	71.0	15.4	12	·	1	14	·	·	·	·	23	21	11	2	7	3	·
XII	8	4.4	2.5	4.4	5	2.9	8.5	2.7	5.5	3.3	1.2	5.7	12.5	3.9	11	4.2	2.8	2.8	34.5	7.3	1	11	15	26	·	·	·	·	18	20	9	·	4	24	·
Rok	3.6	1.9	2.9	2.2	7.1	2.9	100.5	3.0	77.5	2.9	139.5	3.2	204.5	3.3	9.8	2.9	33.8	2.2	410.4	29.2	12.VI	24	32	101	38	4	·	27	151	151	85	7	38	65	17

Skierniewice

$\varphi = 51°58'$ $\lambda = 20°10'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1004.0	1026.6	985.0	1020.6	−0.4	−6.6	5.5	4,5	−19.2	27	−4.9	−1.9	−3.8	−3.6	4.2	4.6	4.5	4.4	89	81	88	86	0.5	1.0	0.6	0.7	6.7	6.2	6.1	6.3
II	1006.1	1021.1	978.2	1022.4	4.3	−0.4	11.7	18	−5.9	6	1.0	3.1	1.5	1.8	6.2	6.6	6.3	6.4	94	86	92	91	0.4	1.2	0.6	0.7	9.1	8.0	6.4	7.8
III	1000.8	1020.2	976.7	1016.7	9.3	2.7	17.5	10	−2.2	20	4.0	7.2	5.6	5.6	7.2	7.2	7.3	7.2	84	71	80	78	1.1	3.3	1.9	2.1	8.4	8.0	6.1	7.5
IV	997.8	1008.8	987.6	1013.5	15.8	4.5	24.7	15	−2.6	10	7.0	14.3	9.1	9.9	8.3	8.5	8.9	8.6	80	52	75	69	2.0	8.9	3.1	4.7	5.1	4.6	3.7	4.5
V	996.8	1004.0	983.8	1012.4	16.9	6.9	25.0	27	1.2	19	9.9	15.3	10.9	11.8	10.2	10.3	10.9	10.5	82	60	83	75	2.2	7.8	2.3	4.1	7.0	7.9	7.0	7.3
VI	999.9	1013.1	989.5	1015.2	23.6	12.2	31.8	27	6.5	21	16.3	21.5	16.5	17.7	15.3	14.9	15.4	15.2	82	59	82	74	3.4	11.3	3.5	6.1	4.6	5.9	5.4	5.3
VII	998.2	1010.4	982.2	1013.6	20.8	11.3	30.9	3	7.4	8	14.6	19.2	14.8	15.8	14.1	13.6	14.5	14.1	85	62	85	77	2.7	9.4	2.6	4.9	7.3	8.1	6.4	7.3
VIII	1000.8	1014.4	989.5	1016.2	21.2	12.4	30.6	6	8.3	30,31	14.5	19.8	15.5	16.3	15.1	16.0	16.0	15.7	90	70	90	83	1.7	7.7	1.9	3.8	6.5	7.3	5.9	6.6
IX	1003.7	1015.0	991.2	1019.3	20.3	9.3	29.6	2	1.2	24	10.9	19.7	13.3	14.3	11.9	12.3	12.9	12.3	89	54	83	75	1.6	11.3	2.8	5.0	4.9	4.0	3.6	4.2
X	1004.0	1016.1	978.6	1019.8	16.0	6.0	22.2	20	1.6	31	7.9	15.0	10.4	10.8	9.4	10.2	9.6	9.7	88	61	78	76	1.3	7.2	3.1	3.9	6.8	6.2	4.4	5.8
XI	998.9	1021.1	987.2	1014.8	6.1	1.5	12.9	3	−6.3	23	2.8	5.2	3.6	3.8	7.2	7.6	7.5	7.4	93	85	92	90	0.5	1.5	0.6	0.9	8.5	8.7	7.7	8.3
XII	1000.1	1029.0	978.4	1016.6	−0.3	−6.2	15.8	5	−21.9	26	−3.7	−2.1	−3.6	−3.2	4.8	4.8	4.5	4.7	88	82	88	86	0.6	1.1	0.7	0.8	8.6	7.2	7.0	7.6
Rok	1000.9	1029.0	976.7	1016.3	12.8	4.5	31.8	27.VI	−21.9	26.XII	6.7	11.4	7.8	8.4	9.5	9.7	9.9	9.7	87	69	85	80	1.5	6.0	2.0	3.2	7.0	6.9	5.8	6.5

Zielona Góra

$\varphi = 51°56'$ $\lambda = 15°30'$

I	997.1	1020.2	974.0	1019.2	0.3	−5.6	6.8	30,31	−18.0	27	−3.8	−1.0	−2.7	−2.6	4.4	4.7	4.6	4.6	87	78	85	83	0.6	1.2	0.7	0.8	6.4	6.8	5.5	6.2
II	1000.1	1016.6	970.1	1021.8	7.1	1.2	14.8	15	−4.9	6	2.2	5.4	3.7	3.8	6.6	7.0	7.0	6.9	91	78	87	85	0.7	2.2	1.1	1.3	7.5	7.6	6.0	7.0
III	998.1	1016.5	970.2	1019.6	10.1	3.2	19.6	10	−4.1	20	4.2	8.1	6.2	6.2	7.1	7.4	7.3	7.3	86	70	76	77	1.3	3.9	2.6	2.6	8.0	8.2	5.9	7.4
IV	991.3	1002.2	981.8	1012.3	16.0	6.1	24.9	7	−1.2	1	7.7	14.2	10.6	10.8	8.6	8.9	8.8	8.8	80	56	68	68	2.3	8.1	4.5	5.0	6.6	6.3	4.6	5.8
V	992.2	1001.5	978.4	1013.2	15.1	7.5	22.5	26	3.2	16	9.2	13.1	10.8	11.0	10.0	10.4	10.5	10.3	86	71	81	79	1.8	5.1	2.7	3.2	8.2	8.3	7.0	7.8
VI	995.0	1009.4	981.9	1015.5	23.0	13.1	29.7	25	8.2	15	15.4	21.0	17.6	17.9	14.0	13.7	14.4	14.0	80	56	72	69	3.7	11.6	6.0	7.1	5.1	6.2	5.6	5.6
VII	993.2	1005.6	978.0	1013.9	20.4	12.7	33.3	3	8.1	6	14.3	18.4	15.5	15.9	13.4	12.9	13.7	13.3	83	63	78	75	3.2	9.3	4.4	5.6	7.9	8.3	7.8	8.0
VIII	995.9	1008.4	984.0	1016.6	20.6	12.7	29.9	6	8.0	17	14.3	19.0	16.0	16.3	14.2	14.7	14.9	14.6	87	68	81	79	2.3	7.9	3.5	4.6	7.3	7.5	5.7	6.8
IX	997.7	1007.8	983.9	1018.4	21.4	12.1	29.9	2	6.3	24	13.0	20.0	15.8	16.2	12.8	13.7	13.5	13.3	84	60	74	73	2.5	10.6	5.0	6.0	4.7	4.9	3.8	4.5
X	996.4	1009.7	967.7	1017.4	15.5	7.9	22.5	6	3.7	31	8.6	14.7	10.9	11.3	9.8	10.5	10.5	10.3	88	64	81	78	1.5	6.7	2.6	3.6	6.9	6.7	5.1	6.2
XI	993.3	1016.0	980.3	1014.9	6.1	1.9	12.4	2	−2.6	21	2.6	5.3	3.8	3.9	6.9	7.5	7.3	7.2	92	84	89	88	0.6	1.5	0.9	1.0	8.2	8.7	7.7	8.2
XII	994.8	1024.1	970.7	1016.9	0.6	−5.7	15.4	5	−17.9	17	−3.2	−1.2	−2.9	−2.6	4.9	5.0	4.6	4.8	88	82	85	85	0.7	1.3	1.0	1.0	7.0	7.3	6.3	6.9
Rok	995.4	1024.1	967.7	1016.6	13.0	5.6	33.3	3.VII	−18.0	27.I	7.0	11.4	8.8	9.0	9.4	9.7	9.8	9.6	86	69	80	78	1.8	5.8	2.9	3.5	7.0	7.2	5.9	6.7

Pleszew

$\varphi = 51°54'$ $\lambda = 17°47'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.8	12.3	29.8	27	6.6	22	16.5	21.8	16.6	17.9	–	–	–	–	–	–	–	–	–	–	–	–	3.2	5.1	3.7	4.0
VII	–	–	–	–	20.9	12.1	33.2	3	9.5	11	14.9	19.3	14.9	16.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	7.6	7.6
VIII	–	–	–	–	21.5	12.4	30.5	6	6.7	24	14.5	19.8	15.4	16.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.7	6.5	6.7
IX	–	–	–	–	21.4	9.8	29.7	2	1.7	24	11.8	20.3	13.6	14.8	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.3	4.3	4.4
X	–	–	–	–	15.6	7.2	22.3	6	2.5	31	8.4	14.7	10.2	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.6	5.8	5.9
XI	–	–	–	–	6.2	–	12.8	3	–	–	2.7	5.3	3.4	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.1	8.0	8.2
XII	–	–	–	–	−0.3	–	15.9	5	–	–	−4.0	−2.1	−4.0	−3.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	33.2	3.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Leszno - Strzyżewice

$\varphi = 51°50'$ $\lambda = 16°32'$

I	–	–	–	–	0.7	−7.0	6.4	4	−21.6	28	−4.8	−1.0	−3.5	−3.2	4.3	4.7	4.5	4.5	89	78	87	85	0.5	1.3	0.7	0.8	6.2	6.5	6.1	6.3
II	–	–	–	–	7.0	0.0	13.6	18	−4.5	6	1.5	5.4	3.0	3.2	6.4	7.2	6.9	6.8	93	79	90	87	0.5	2.0	0.8	1.1	8.0	6.9	5.9	6.9
III	–	–	–	–	10.8	1.7	19.6	10	−6.7	20	3.5	8.9	5.3	5.8	7.1	7.8	7.4	7.4	90	69	82	80	0.9	4.1	1.8	2.3	7.7	8.5	5.5	7.2
IV	–	–	–	–	16.5	5.2	26.3	7	−2.4	1	7.7	14.5	9.7	10.4	9.0	9.8	9.7	9.5	83	60	79	74	1.8	7.6	2.7	4.0	6.5	6.6	5.0	6.0
V	–	–	–	–	16.0	6.5	22.9	26	1.8	16	9.8	13.9	10.8	11.3	10.8	10.9	11.2	11.0	89	70	86	82	1.5	5.3	1.9	2.9	7.4	8.4	7.3	7.7
VI	–	–	–	–	23.6	10.8	29.4	25	4.1	22	15.9	21.8	16.5	17.7	15.2	14.6	15.9	15.2	83	56	84	74	3.1	12.0	3.2	6.1	5.3	5.7	5.1	5.4
VII	–	–	–	–	21.4	11.1	33.4	3	6.5	8	14.7	19.5	15.1	16.1	14.3	13.7	14.5	14.2	85	62	85	77	2.7	9.9	3.0	5.2	7.6	8.0	6.2	7.9
VIII	–	–	–	–	21.5	10.7	31.2	6	5.9	14	14.3	19.7	14.9	16.0	15.1	15.5	15.4	15.3	92	68	90	83	1.4	8.0	1.8	3.7	7.7	7.7	6.2	7.2
IX	–	–	–	–	21.8	9.5	30.1	17	0.6	24	11.7	20.5	14.1	15.1	12.8	14.0	13.6	13.5	91	59	83	78	1.3	10.9	2.8	5.0	4.7	5.0	3.6	4.4
X	–	–	–	–	16.1	6.7	22.1	5	0.3	13	8.2	15.0	9.8	10.7	10.0	11.2	10.4	10.5	92	68	86	82	1.0	6.2	1.8	3.0	6.7	6.7	4.5	6.0
XI	–	–	–	–	6.5	1.1	13.6	3	−8.1	23	2.3	5.7	3.2	3.6	6.9	7.7	7.4	7.3	93	82	94	90	0.6	1.7	0.5	0.9	8.6	9.1	7.8	8.5
XII	–	–	–	–	0.6	−7.6	16.6	5	−25.5	26	−4.3	−1.4	−3.8	−3.3	4.7	5.8	4.7	4.8	89	81	88	86	0.7	1.3	0.8	0.9	6.9	6.8	6.5	6.7
Rok	–	–	–	–	13.5	4.1	33.4	3.VII	−25.5	26.XII	6.7	11.9	7.9	8.6	9.7	10.2	10.1	10.0	89	69	86	81	1.3	5.9	1.8	3.0	6.9	7.2	6.0	6.7

Skierniewice

$H_s = 128\ m$ $H_b = 129{,}5\ m$ $h_w = 8{,}3\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °D. °mD																		OPAD R			LICZBA DNI (n)															
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max<-10°	Max<0°	Min<0°	Max>25	v>10	v>15	●	●	0,1≤R<1	1≤R<10	10≤R<100	R≥100	≡	⊞	≋
I	4	2.6	5	2.8	2.5	3.4	1.0	3.0	2.1	3.3	2.0	3.7	14.5	2.7	6	2.5	1.0	2.8	20.7	8.9	31	11	12	25		·	·	5	13	10	4	·	3	18	·
II	2	2.2	1.5	2.3	4	3.6	1.3	3.5	1.8	3.4	1.6	3.2	21.5	3.7	8	3.1	½	3.4	21.3	5.9	1	·	·	19		1	·	·	15	13	5	·	5	3	·
III	·	·	·	·	·	·	·	·	2	1.5	20.5	5.9	6.0	5.4	10.5	6.3	·	5.5	18.9	3.4	12	·	·	5	·	10	1	1	13	12	9	·	2	1	·
IV	1.5	2.0	1.0	4.0	12.5	4.6	14.5	4.9	7.5	3.0	9.5	3.3	12	4.8	10.5	4.1	7	3.9	23.1	6.9	2	·	·	4	·	3	·	9	7	7	5	·	1	·	1
V	4.5	3.2	4	2.2	5	2.0	7.5	2.6	10.5	2.7	17.5	3.0	22.5	2.9	18.5	3.5	3	2.9	67.0	13.3	28	·	·	·	·	·	·	·	16	16	13	1	·	·	5
VI	0.5	3.0	6.5	1.6	10.5	4.2	9.5	3.5	6.5	2.6	10.5	2.9	28.5	3.2	16.5	3.6	1	3.2	88.3	15.8	27	·	·	·	10	1	·	3	4	13	11	5	2	·	9
VII	0.5	2.0	0.5	4.0	3.5	2.0	3	3.3	9	2.7	28	3.4	30	3.4	9.5	3.4	9	3.0	124.6	26.5	28	·	·	·	6	·	·	2	14	15	13	4	·	·	8
VIII	3.5	3.0	2	2.7	2	3.7	2.5	3.2	9.5	3.5	28	3.5	32	3.1	11.5	2.9	2	3.2	42.7	14.4	12	·	·	·	5	·	·	2	10	11	7	2	1	·	1
IX	0.5	3.0	6	1.7	16.5	2.5	7	3.8	12.5	2.5	12.5	3.2	21.5	4.2	4.5	2.3	9	2.8	18.5	5.8	14	·	·	·	5	1	·	10	6	6	6	·	1	·	1
X	·	·	3	1.7	1.8	5.0	2.8.5	5.0	15.5	3.3	8	3.4	14.5	3.0	3.5	3.7	2	4.0	8.6	4.0	29	·	·	·	·	2	·	5	6	3	2	·	1	·	·
XI	6.5	2.8	3.5	5.0	1.2	5.4	10.5	3.4	11	2.5	21.5	2.9	15.5	3.8	8.5	2.8	1	3.4	85.3	19.0	13	·	1	8	·	1	·	1	20	18	13	3	3	1	·
XII	5	3.7	7.5	5.3	3.5	4.7	8	2.4	17.5	2.4	13.5	4.0	27	4.0	11	4.1	·	3.7	15.7	8.1	11	8	15	23	·	3	1	·	15	9	4	·	·	16	·
Rok	28.5	2.3	49.5	2.8	95	3.4	114	3.2	140.5	2.8	205.5	3.5	299.5	3.7	118.5	3.5	44	3.5	534.7	26.5	28 VII	19	28	84	26	22	2	38	139	133	92	15	19	39	25

Zielona Góra

$H_s = 180\ m$ $H_b = 173{,}8\ m$ $h_w =$ 12 m, 17 m anemometr wiatromierz Wilda

I	·	·	3.5	2.1	14.5	3.8	1.5	4.0	18.5	3.9	28.5	4.0	6.5	3.6	4.5	2.3	2	3.7	42.9	12.0	14	11	14	23	·	·	·	7	15	15	3	2	8	22	·
II	1.5	1.3	·	·	5	3.2	6.5	3.6	13.5	3.8	20.5	3.9	21.5	3.8	12.5	3.1	3	3.5	23.4	5.1	9	·	·	9	·	·	·	4	13	14	10	·	11	3	·
III	1.5	1.0	·	·	·	·	·	·	·	·	18.5	4.6	5.3	4.5	2.0	3.3	·	4.2	48.4	13.8	30	·	·	5	·	4	·	1	17	18	12	1	6	2	·
IV	8	2.2	5.5	3.2	2.4	4.3	7.5	4.7	10	2.8	6.5	3.8	18.5	3.3	9	2.5	1	3.5	38.4	9.8	1	·	·	1	·	·	·	6	8	7	6	·	5	·	3
V	11	2.5	3	3.5	0.5	2.0	3.5	2.9	3	2.8	18.5	3.5	2.6	3.2	27.5	2.7	·	3.0	132.8	25.0	29	·	·	·	·	·	·	·	18	23	21	3	6	·	7
VI	2	1.5	3	2.0	8.5	2.6	4.5	2.8	9.5	2.9	13	3.2	26.5	3.5	18	2.8	5	2.8	129.4	30.0	4	·	·	·	7	·	·	1	6	11	7	2	3	·	5
VII	1	3.0	·	·	·	·	4	2.5	7.5	2.8	30.5	3.2	42.5	3.5	7.5	3.3	·	3.3	67.1	10.4	30	·	·	·	4	·	·	2	17	19	17	1	·	·	4
VIII	4	2.2	0.5	3.0	1.5	3.0	6	2.8	10	2.9	25	3.8	37	3.3	8	2.0	1	3.1	54.1	16.7	6	·	·	·	4	1	·	2	13	17	11	1	6	·	6
IX	2.5	2.8	·	·	16.5	4.0	17.5	3.7	12.5	3.1	21	3.5	18	3.8	2	3.2	·	3.6	21.5	3.5	5, 14	·	·	·	8	·	·	11	8	12	9	·	5	·	4
X	0.5	3.0	0.5	3.0	12.5	5.2	2.2	3.9	19.5	3.5	17	3.4	11	3.2	8	2.6	2	3.6	45.1	24.0	20	·	·	·	·	·	·	4	11	9	7	1	5	·	·
XI	3	2.0	6.5	3.2	13	3.6	8	2.8	12.5	3.1	25	4.2	13	3.6	6	3.1	3	3.4	53.8	25.0	13	·	·	8	·	·	·	2	20	17	8	1	13	·	·
XII	5	2.9	1.5	2.7	1.4	2.8	9	2.8	15.5	3.4	20	4.7	17.5	4.5	9.5	2.7	1	3.6	51.6	14.2	11	9	14	22	·	2	·	5	13	19	10	2	8	20	·
Rok	4.0	2.0	24	1.9	110	2.9	103.5	3.0	132	2.9	244	3.8	291	3.6	132.5	2.8	18	3.4	708.5	80.0	4. VI	20	28	68	23	7	·	45	159	181	127	14	76	47	29

Uwaga. Kierunki wiatru - wg wiatromierza Wilda, prędkości - wg anemometru

Pleszew

$H_s = 120\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.5	13.1	22	·	·	·	12	–	–	11	4	11	8	1	9	·	8
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	140.4	36.7	31	·	·	·	6	–	–	3	17	18	15	5	6	·	4
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	98.7	22.1	11	·	·	·	6	–	–	3	13	14	13	3	6	·	5
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	93	31	14	·	·	·	7	–	–	13	10	6	4	·	11	·	2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	30.8	11.8	18	·	·	·	·	–	–	7	12	7	4	2	11	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.8	17.3	13	–	·	–	·	–	–	2	20	16	8	1	7	·	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.3	13.7	11	–	15	–	·	–	–	–	–	15	9	1	3	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Leszno - Strzyżewice

$H_s = 91\ m$ $h_w =$ 11,3 m, 14,2 m anemometr wiatromierz Wilda

I	0.5	3.0	5	3.8	25.5	3.1	14.5	3.1	15.5	4.1	14.5	3.9	9	3.4	3.5	3.6	5	3.3	36.2	11.4	31	12	12	24	·	·	·	7	13	16	8	1	3	19	·
II	2	2.8	·	·	1.3	3.2	1.1	3.3	15.5	3.5	10.5	4.7	17	4.2	1.4	4.2	1	3.8	27.1	13.0	9	·	·	14	·	3	1	4	15	14	6	1	6	2	·
III	0.5	4.0	·	·	·	·	1	2.0	2.5	2.4	21.5	5.6	54.5	6.1	1.2	4.8	1	5.6	44.1	14.2	30	·	·	8	·	12	·	1	13	17	12	1	3	1	·
IV	6.5	3.3	1.4	4.1	22.5	4.6	13.5	3.2	5.5	3.3	5.5	3.6	10	4.9	9.5	3.6	3	3.8	62.4	24.2	27	·	·	1	1	1	·	5	10	9	8	1	2	·	4
V	11.5	3.7	5.5	4.6	7	2.6	3	3.3	7.5	2.5	16.5	4.5	16.5	4.6	24.5	3.7	1	3.8	77.2	14.3	29	·	·	·	·	4	·	1	19	19	16	2	3	·	8
VI	3	2.7	1.0	2.6	1.0	3.4	9.5	2.8	1	2.0	18	3.4	22	4.3	14.5	3.4	2	3.4	57.8	22.7	10	·	·	·	11	3	·	5	6	9	8	2	4	·	9
VII	0.5	2.0	1	2.0	2.5	2.4	2.5	3.8	9.5	2.6	31	4.8	35	4.0	8	3.9	3	3.9	92.2	28.0	31	·	·	·	7	6	·	2	20	18	14	2	1	·	7
VIII	4.5	2.8	2.5	1.4	6	2.6	6	2.7	6.5	3.8	30.5	4.5	28	4.0	5	4.2	4	3.7	76.2	20.5	6	·	·	·	4	5	·	1	13	14	11	2	8	·	5
IX	4	2.5	5.5	3.0	19	3.4	11.5	2.8	11	3.1	15.5	4.3	18	4.2	2.5	2.8	3	3.4	14.4	6.4	5	·	·	·	8	2	·	12	7	6	5	·	2	·	2
X	4.5	2.6	2	4.5	25.5	4.2	18	3.7	12.5	3.7	9	4.0	13.5	2.6	6	2.8	2	3.5	19.7	4.6	20	·	·	·	·	3	·	5	11	10	7	·	10	·	·
XI	8.5	4.1	1.2	4.9	7.5	3.9	1.4	2.0	2.5	4.2	19.5	5.1	15.5	4.0	5.5	4.5	5	3.8	42.4	23.8	13	·	·	8	·	4	·	1	22	14	9	1	10	·	·
XII	3	3.0	1.0	3.8	9	3.4	17.5	2.7	8.5	3.6	12.5	5.5	1.9	5.2	8.5	4.2	5	3.9	45.2	16.4	11	12	13	25	·	4	·	5	13	14	9	1	5	18	·
Rok	4.9	3.0	67.5	2.9	147.5	3.1	122	3.0	9.8	3.2	204.5	4.5	258	4.3	113.5	3.8	35	3.8	594.9	28.0	31 VII	24	25	80	31	47	1	49	162	160	113	14	57	40	35

Uwaga. Kierunki wiatru - wg wiatromierza Wilda, prędkości wg anemometru.

Bełsk

$\varphi = 51°50'$ $\lambda = 20°48'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.0	-7.8	5.0	4	-23.7	26	-5.5	-2.4	-4.6	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.6	5.7	6.7
II	–	–	–	–	3.5	-1.0	11.4	18	-7.4	6	0.0	2.5	0.8	1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	7.1	8.1
III	–	–	–	–	8.8	1.9	16.9	10	-2.8	20	3.0	7.1	4.7	4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.8	6.9	7.8
IV	–	–	–	–	15.2	3.3	26.4	7	-7.1	10	6.5	13.6	8.1	9.1	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.1	4.2	5.1
V	–	–	–	–	16.6	5.0	24.6	27	-0.7	19	9.8	14.8	9.3	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.9	7.2	7.5
VI	–	–	–	–	23.0	10.9	31.8	27	2.2	21	15.7	21.3	15.1	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.7	6.7	6.4
VII	–	–	–	–	20.7	10.1	30.0	3	4.7	9	14.2	19.1	13.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.4	6.6	7.3
VIII	–	–	–	–	20.7	11.4	30.4	6	5.3	31	14.1	19.3	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.9	6.7	7.2
IX	–	–	–	–	20.1	7.8	28.9	2	-2.2	22	10.6	18.8	11.6	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.5	3.9	4.5
X	–	–	–	–	15.3	4.6	21.9	20	-0.2	31	6.6	14.5	9.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.8	4.7	6.1
XI	–	–	–	–	5.8	0.9	13.2	3	-8.0	23	2.2	4.7	3.1	3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	9.1	8.0	8.7
XII	–	–	–	–	-0.6	-7.3	14.9	5	-23.6	26	-4.3	-2.8	-4.4	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.9	6.4	7.6
Rok	–	–	–	–	12.3	3.3	31.8	27 VI	-23.7	26. I	6.1	10.9	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	6.2	6.9

Strzelna

$\varphi = 51°49'$ $\lambda = 19°54'$

I	–	–	–	–	-0.5	-7.4	6.5	4	-21.1	26	-5.7	-2.0	-4.7	-4.3	4.1	4.7	4.4	4.4	91	84	91	88	03	08	04	05	–	–	–	–
II	–	–	–	–	4.6	-0.9	12.6	18	-6.1	6	0.4	3.2	0.9	1.4	6.2	6.8	6.3	6.4	97	88	96	94	02	1.0	03	05	9.4	7.5	6.7	7.9
III	–	–	–	–	9.3	2.2	18.2	10	-3.3	20	3.2	6.9	5.0	5.0	7.0	7.4	7.4	7.3	91	75	85	84	08	2.9	1.5	1.7	7.0	6.7	5.4	6.4
IV	–	–	–	–	15.9	3.6	24.8	7	-3.5	10	6.5	14.1	8.6	9.4	8.3	8.5	8.7	8.5	84	53	76	71	1.6	8.4	3.0	4.3	–	–	–	–
V	–	–	–	–	17.1	5.9	26.1	27	-0.1	19	9.6	14.8	9.8	11.0	10.3	10.3	10.6	10.4	85	62	87	78	1.9	7.1	1.8	3.6	–	–	–	–
VI	–	–	–	–	23.5	11.5	31.4	27	5.0	21	16.3	21.4	15.9	17.4	15.0	14.6	15.3	15.0	81	58	84	74	3.7	11.6	2.9	6.1	4.2	5.0	4.2	4.5
VII	–	–	–	–	20.7	10.0	30.9	3	5.5	8	14.0	18.5	13.7	15.0	14.0	13.5	14.2	13.9	87	66	90	81	2.2	8.5	1.7	4.1	8.0	8.2	5.3	7.2
VIII	–	–	–	–	21.0	11.6	30.2	6	6.5	4	14.1	19.4	14.7	15.7	14.6	15.1	15.1	14.9	90	65	89	81	1.7	8.2	1.8	3.9	–	–	–	–
IX	–	–	–	–	20.4	8.7	28.9	2	1.9	22	10.7	19.1	12.5	13.7	11.9	13.0	12.8	12.6	90	58	87	78	1.4	9.9	2.0	4.4	4.2	3.7	2.9	3.6
X	–	–	–	–	15.5	5.6	20.5	20	1.5	31	7.2	14.3	9.5	10.1	9.3	10.6	9.8	9.9	91	66	83	80	1.0	6.1	2.3	3.1	–	–	–	–
XI	–	–	–	–	6.1	0.9	12.7	7	-7.7	23	2.1	4.7	2.8	3.1	7.1	7.6	7.3	7.3	96	88	94	93	0.3	1.2	0.5	0.7	7.7	8.0	7.0	7.6
XII	–	–	–	–	-0.6	-6.9	15.6	5	-22.8	26	-4.3	-2.6	-4.1	-3.8	4.6	4.9	4.5	4.7	89	87	91	89	0.5	0.8	0.5	0.6	8.4	6.9	5.3	6.9
Rok	–	–	–	–	12.8	3.7	31.4	27 VI	-22.8	26 XII	6.2	11.0	7.0	7.8	9.4	9.8	9.7	9.6	89	71	88	83	1.3	5.5	1.6	2.8	–	–	–	–

Żelechów

$\varphi = 51°49'$ $\lambda = 21°54'$

I	–	–	–	–	-0.9	-8.1	7.1	4	-23.4	26	-5.7	-2.7	-4.9	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.8	5.3	6.2
II	–	–	–	–	3.2	-1.3	10.6	18	-5.4	5	-0.4	2.1	0.6	0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.9	8.0
III	–	–	–	–	8.5	1.4	16.3	18	-2.5	20	2.6	6.9	4.3	4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.7	5.2	7.2
IV	–	–	–	–	15.6	3.4	25.3	16	-4.4	10	6.8	14.6	8.8	9.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.2	2.8	4.2
V	–	–	–	–	17.4	6.1	26.2	27	1.0	17	10.2	16.1	10.4	11.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	5.3	6.3
VI	–	–	–	–	23.5	11.6	31.4	27	5.0	21	16.4	21.8	16.1	17.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.8	6.3	6.1
VII	–	–	–	–	21.9	10.7	30.8	3	6.3	6	14.9	20.2	15.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.2	6.6	6.7
VIII	–	–	–	–	21.4	11.8	31.2	7	6.6	31	14.5	20.6	15.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.7	5.7	6.1
IX	–	–	–	–	20.8	8.1	30.2	3	-1.7	23	10.0	19.9	12.3	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.2	3.3	4.3
X	–	–	–	–	15.5	5.4	23.0	19	0.8	29	7.0	14.8	9.8	10.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.8	2.9	4.3
XI	–	–	–	–	5.9	1.2	14.3	3	-7.1	23	2.5	5.1	3.4	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.5	7.8	8.4
XII	–	–	–	–	-0.9	-7.5	15.3	5	-22.8	26	-4.7	-2.7	-4.0	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.6	6.5	7.6
Rok	–	–	–	–	12.7	3.6	31.4	27 VI	-23.4	26. I	6.2	11.4	7.2	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.4	5.5	6.3

Radzyń Podlaski

$\varphi = 51°48'$ $\lambda = 22°38'$

I	–	–	–	–	-1.4	-8.5	6.4	4	-24.8	26	-5.9	-2.5	-5.4	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	5.7	6.1
II	–	–	–	–	2.7	-1.3	10.1	18	-5.0	6	-0.6	2.2	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	8.0	8.1
III	–	–	–	–	8.9	1.1	18.3	18	-2.5	23	2.7	7.0	4.2	4.5	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	5.5	7.4
IV	–	–	–	–	15.9	3.2	25.3	15	-4.1	10	6.6	14.4	9.3	9.4	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.7	2.9	4.1
V	–	–	–	–	17.5	5.8	25.9	29	0.7	13	10.4	16.2	10.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.3	6.2	6.7
VI	–	–	–	–	24.8	10.4	32.8	27	4.3	21	16.9	23.0	15.3	17.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.3	4.7	5.2
VII	–	–	–	–	23.2	10.0	31.7	3	4.8	6	15.5	21.4	14.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.5	7.3	5.5	6.1
VIII	–	–	–	–	23.1	10.8	31.8	7	5.0	31	15.1	21.8	14.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.7	5.4	6.1
IX	–	–	–	–	22.4	7.2	31.6	2, 18	-1.8	23	10.5	21.2	12.0	13.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.0	3.5	4.1
X	–	–	–	–	16.0	4.6	22.3	19	1.0	23	6.6	15.4	9.4	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.6	3.5	4.7
XI	–	–	–	–	5.9	0.8	14.8	3	-8.0	23	2.4	5.1	3.0	3.4	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.7	7.8	8.2
XII	–	–	–	–	-1.1	-8.0	14.9	5	-22.1	27	-4.7	-2.9	-4.5	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.1	6.2	7.5
Rok	–	–	–	–	13.2	3.0	32.8	27 VI	-24.8	26. I	6.3	11.9	6.8	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.4	6.2

Bełsk

$H_s = 180\ m$ $h_w = 10\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%D, %nD]																	OPAD R			LICZBA DNI (n)										
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		●	●	Opad R			≥	≥	R ≥ 10
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	≥ 10	≥ 15			≥ 0.1	≥ 1.0	≥ 10.0			
I	3.5	2.6	4	2.6	2	2.0	12	2.3	13	2.5	23.5	2.8	12	2.0	6	1.5	17	2.0	32.8	7.2	31	12	13	27		1	-	3	13	20	6	-	4	20	-
II	2.5	1.4	2	2.0	5	1.5	9	2.1	14.5	2.1	18	3.1	15	3.0	5	2.2	13	2.1	18.7	7.3	1	-	1	19	-	-	-	-	16	11	6	-	10	10	-
III	1.5	7.3	-	-	-	-	-	-	3	3.5	21	4.6	51	3.5	12.5	3.8	4	3.7	26.3	5.5	21	-	-	8	-	5	1	-	17	16	9	-	6	3	1
IV	4	2.0	5.5	3.1	17	4.5	14	5.3	4.5	2.4	11.5	2.6	12.5	4.4	5	4.4	16	3.3	21.5	7.3	2	-	-	6	1	3	-	6	6	6	5	-	1	-	1
V	3.5	3.4	2.5	2.0	7	1.6	5.5	1.5	2	1.2	14	2.9	17.5	2.8	11	3.3	30	1.7	58.8	10.2	7	-	-	1	-	1	-	-	14	16	12	1	-	-	4
VI	-	-	0.5	1.0	10	2.3	6	3.6	4	3.0	13.5	2.5	18	3.6	5	3.0	33	1.9	91.5	30.8	7	-	-	-	8	1	1	-	6	14	9	3	1	-	8
VII	2	3.0	1	2.5	0.5	3.0	7.5	2.6	9	2.7	31	3.3	18.5	3.6	3.5	3.3	20	2.6	100.6	26.7	31	-	-	-	7	-	-	2	15	15	12	2	-	-	8
VIII	5	1.7	1.5	1.3	3	2.0	2.5	2.4	6	1.9	26	3.2	25	2.8	6	2.0	18	2.3	76.9	36.9	12	-	-	-	5	-	-	1	12	14	6	2	1	-	2
IX	0.5	1.0	1.5	2.7	3.5	2.6	5.5	2.7	8	1.9	20	2.6	21	3.0	2	3.0	28	1.8	19.0	9.6	6	-	-	3	6	1	-	11	5	4	3	-	1	-	-
X	1	2.0	3.5	2.3	17	4.1	22	4.2	10.5	2.6	10	3.4	13	3.2	2	3.8	14	3.0	6.8	3.4	29	-	-	1	-	2	-	4	11	5	2	-	3	-	-
XI	5.5	4.0	3	5.7	10	4.8	10.5	2.7	7	1.8	16.5	3.0	16	3.1	6.5	2.1	15	2.7	86.4	28.5	13	-	2	10	-	-	-	-	22	16	12	3	7	2	-
XII	4	3.1	5.5	3.8	3.5	3.3	5.5	2.1	10	2.2	14.5	3.9	18.5	2.6	13.5	3.4	18	2.5	19.7	9.5	11	10	15	26	-	2	-	-	16	14	4	-	4	17	-
Rok	33	2.6	30.5	2.4	78.5	2.6	100	2.6	91.5	2.3	219.5	3.2	238	3.1	78	3.1	226	2.5	560.0	36.9	12.VIII	22	31	101	27	16	2	27	153	151	86	11	38	52	24

Strzelna

$H_s = 194\ m$ $h_w = 18\ m$

I	5	2.7	3.5	2.6	5	2.2	14.5	2.0	22	2.4	12	4.0	9	2.2	7	3.2	17	2.2	22.8	8.4	31	13	14	27	-	-	-	-	-	9	5	-	-	2.0	-
II	5	2.2	2	1.5	4	1.0	7	2.9	17	3.1	14.5	3.8	5	2.8	17.5	2.8	12	2.5	26.6	7.5	9	-	-	18	-	-	-	-	14	16	8	-	-	7	-
III	1	4.0	-	-	-	-	-	-	1	1.0	13.5	5.7	42.5	6.5	32	5.1	3	5.6	38.2	5.8	12	-	-	8	-	5	4	3	9	19	12	-	-	3	-
IV	4	2.0	5	3.2	22	3.4	13	4.5	7.5	3.2	6	3.5	11.5	4.2	7	4.7	14	3.1	39.4	13.8	16	-	-	5	-	2	-	-	-	10	7	1	-	-	2
V	17	4.1	4	3.2	3	1.7	2	4.0	13.5	3.0	10	4.5	12.5	3.9	14	4.9	17	3.2	73.7	12.2	21	-	-	1	1	-	-	-	-	15	11	3	1	-	7
VI	6.5	5.2	1.5	2.0	13.5	3.8	8	4.5	7	5.0	7	4.0	18	5.7	18.5	3.5	10	3.9	117.1	61.0	11	-	-	-	9	1	-	6	5	11	9	4	3[3]	-	8
VII	9	2.4	3.5	2.1	1	1.5	1.5	2.0	5.5	3.5	17.5	4.3	25	3.9	23	3.5	7	3.3	196.5	33.3	28	-	-	-	6	-	-	3	14	16	12	8			8
VIII	5	3.0	1	4.0	2	4.0	1	2.0	5.5	3.8	20.5	4.7	19	4.2	17	4.3	22	3.2	53.2	16.2	10	-	-	-	5	1	-	-	-	13	10	1	5	-	3
IX	1	1.0	4	2.2	13	2.7	8	3.5	4	3.2	10	3.2	15	3.9	13	4.0	22	2.6	17.9	6.3	29	-	-	-	6	-	-	13	4	7	5	-	3	-	1
X	1	1.0	3.5	2.3	23.5	3.1	18	4.1	8.5	3.6	4.5	2.0	4	2.8	11	3.0	19	2.5	11.9	4.9	14	-	-	-	-	-	-	-	-	4	3	-	10	-	-
XI	8	2.8	8	2.6	17	2.6	2	1.5	10.5	2.3	14	3.4	5.5	3.3	6	2.7	19	2.2	116.3	32.0	13	-	-	10	-	-	-	4	20	19	13	3	10	1	-
XII	8.5	3.3	7	2.3	7	1.4	4	1.2	15	2.8	10.5	4.5	3.5	1.7	16.5	2.3	21	2.0	23.4	7.9	11	10	15	26	-	-	-	2	13	12	6		6	16	-
Rok	6.9	2.8	4.3	2.3	11.1	2.3	7.9	2.7	11.7	3.1	14.0	4.0	17.05	3.8	18.25	3.7	18.3	3.0	737.0	61.0	11.VI	23	29	95	27	9	4	-	-	151	101	20	-	47	29

Żelechów

$H_s = 175\ m$ $h_w = 10{,}5\ m$ I-V, $14{,}5\ m$ VI-XII

I	3	3.7	3	3.7	-	-	13	3.5	22	3.8	22	3.8	8	6.0	16	4.3	6	3.8	37.7	8.6	30	12	12	29	-	1	-	8	15	12	11	-	-	21	-
II	1	3.0	2	2.0	7	3.4	7	3.6	20	4.1	23	3.3	13	4.3	5	3.6	6	3.4	20.9	8.0	1	-	1	19	-	-	-	3	20	9	5	-	-	6[2]	-
III	-	-	-	-	-	-	-	-	2	5.0	29	6.6	42	5.5	18	7.1	2	6.0	37.8	10.0	30	-	-	9	-	6	1	-	13	15	10	1	-	-	-
IV	1	1.0	7	5.9	10	4.8	18	6.1	6	3.5	14	4.4	10	6.3	15	4.0	9	4.5	29.7	12.0	2	-	-	5	2	4	1	10	5	6	6	1	-	-	2
V	-	-	7	3.0	1	2.0	7	4.4	14	2.8	17	3.7	12	4.1	31	4.5	4	3.7	67.4	11.2	28	-	-	-	3	1	-	1	7	15	13	2	-	-	6
VI	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	99.3	28.8	4	-	-	-	11	-	-	1	8	16	14	3	-	-	10
VII	-	-	-	-	-	-	1	3.0	5	4.8	33	4.2	32	3.2	20	3.1	2	3.5	85.0	21.7	30	-	-	-	8	-	-	3	13	20	15	3	-	-	9
VIII	2	2.5	1	2.0	-	-	1	5.0	1	7.0	35	4.7	16	4.4	28	3.8	9	3.8	35.1	5.5	22	-	-	-	6	1	-	4	8	14	13	-	-	-	5
IX	1	1.0	2	2.0	1	5.0	4	3.5	2	4.5	37	4.3	18	5.5	19	3.2	6	4.0	9.0	4.5	14	-	-	2	7	3	2	12	8	5	3	-	-	-	-
X	-	-	2	4.5	7	5.6	28	9.0	5	4.4	27	4.0	11	2.9	9	4.0	4	5.5	37	23	14	-	-	-	-	6	4	11	5	3	2	-	-	-	-
XI	1	3.0	8	7.0	4	5.8	13	5.1	3	4.0	31	4.1	12	3.9	16	4.4	2	4.5	89.1	20.6	15	-	1	12	-	4	-	2	21	16	10	4	-	-	-
XII	5	4.2	1	5.0	4	6.0	5	4.2	7	2.6	27	6.7	19	4.7	25	6.2	-	5.5	27.9	13.5	11	10	15	25	-	10	2	3	20	12	4	1	-	25	-
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	542.6	28.8	4.VI	22	29	101	37	36	10	58	143	143	106	15	-	52	32

Radzyń Podlaski

$H_s = 151\ m$ $h_w = 13\ m$

I	9	4.8	3	2.0	13	2.2	7	2.6	4	3.5	11	4.0	16	3.4	9	2.0	21	2.4	29.3	5.8	5.31	13	13	29	-	1	-	3	11	14	9	-	1	2.5	-
II	4	1.2	2	2.0	3	2.3	7	3.3	8	3.9	7	3.9	18	2.2	5	2.8	30	1.8	5.7	1.8	1	-	3	19	-	-	-	-	21	14	1	-	11	4	-
III	5	1.8	-	-	-	-	-	-	3	4.3	8	5.0	47	5.4	26	5.7	4	5.0	19.5	4.5	21	-	-	11	-	6	1	1	13	17	8	-	3	3	-
IV	14	2.4	3	4.3	28	4.4	2	5.5	3	4.0	4	3.0	13	5.9	6	3.7	17	3.4	33.5	10.4	17	-	-	6	1	3	-	9	3	7	7	1	3	-	2
V	27	2.3	3	2.3	10	2.5	1	4.0	2	3.0	1	3.0	13	3.2	14	3.8	22	2.2	43.7	8.6	30	-	-	-	3	1	-	2	10	16	13	-	4	-	-
VI	8	2.1	6	2.8	16	2.9	2	1.5	3	4.7	2	3.5	26	3.5	12	3.2	15	2.6	48.9	26.0	28	-	-	-	15	-	-	5	3	12	5	1	-	-	9
VII	9	2.8	-	-	1	3.0	1	5.0	8	5.2	6	3.0	15	3.2	30	2.8	23	2.5	59.1	21.4	30	-	-	-	9	-	-	3	4	15	7	2	1	-	5
VIII	16	2.4	1	3.0	-	-	-	-	4	2.8	5	3.6	17	4.1	35	2.9	15	2.6	23.3	4.4	13	-	-	-	10	-	-	3	5	14	9	-	2	-	6
IX	9	2.7	12	2.1	12	2.4	-	-	2	2.0	3	4.0	23	3.7	13	3.4	16	2.5	10.3	4.3	14	-	-	3	9	-	-	12	6	6	4	-	4	-	-
X	9	1.9	8	3.5	33	3.8	17	5.6	7	3.9	5	2.6	1	2.0	4	2.0	9	3.4	6.8	4.6	14	-	-	-	-	2	-	8	7	2	2	-	6	-	-
XI	12	2.4	25	10.8	17.5	3.8	5	2.0	1	2.0	4	3.5	13	3.3	8	3.2	27	2.4	67.9	14.7	14	-	1	13	-	2	-	2	22	17	12	3	5	-	-
XII	21	6.0	25	3.6	11	2.3	1	3.0	3	3.0	8	3.8	15	3.3	8.5	3.4	23	3.0	30.6	5.6	1	11	17	27	-	3	-	3	16	14	10	-	4	-	-
Rok	14.3	2.7	4.3	3.0	144.5	2.5	4.3	2.7	4.8	3.5	6.4	3.6	217	3.6	170.5	3.2	222	2.8	378.6	26.0	28.VI	24	34	108	47	18	1	51	121	148	87	7	40	56	22

Puczniew — φ = 51°47' — λ = 19°05' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{m.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	−0.7	−7.7	7.1	4	−23.6	26	−5.7	−1.9	−4.5	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.5	5.9	6.6
II	–	–	–	–	4.7	−0.1	11.7	18	−4.6	6	0.8	3.4	1.8	2.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.4	6.1	7.5
III	–	–	–	–	9.0	1.8	17.6	10	−4.3	20	3.3	7.0	5.2	5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.9	6.3	7.6
IV	–	–	–	–	15.8	4.1	24.4	7	−3.4	10	7.4	14.3	8.9	9.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	4.6	5.5	5.4
V	–	–	–	–	16.8	6.7	22.0	5	2.1	19, 23	9.7	14.6	10.4	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	8.6	6.9	7.6
VI	–	–	–	–	23.9	12.0	32.0	27	5.3	21	16.2	21.6	17.0	18.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	7.7	6.4	6.5
VII	–	–	–	–	20.5	11.2	32.0	3	5.6	8	14.4	18.8	15.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.5	7.0	7.7
VIII	–	–	–	–	20.9	12.1	30.1	6	7.7	30	14.2	19.4	15.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.6	6.5	7.0
IX	–	–	–	–	20.6	9.5	29.3	2	2.4	24	11.6	19.5	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.2	3.8	4.4
X	–	–	–	–	15.6	6.5	20.1	6	2.3	14	8.0	14.5	10.0	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.0	4.0	6.1
XI	–	–	–	–	6.5	1.8	13.1	7	−5.2	23	2.8	5.5	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.6	8.0	8.3
XII	–	–	–	–	−0.3	−2.2	15.5	5	−23.6	17	−4.0	−2.2	−4.0	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	6.6	7.3
Rok	–	–	–	–	12.8	4.2	32.0	27.VI, 3.VII	−23.6	26.I, 17.XII	6.6	11.2	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	6.1	6.8

Warka — φ = 51°47' — λ = 21°12'

I	–	–	–	–	−0.4	−7.7	7.1	4	−23.9	26	−5.3	−1.7	−4.3	−3.9	4.0	4.6	4.3	4.3	8.5	7.8	8.6	8.3	0.6	1.2	0.6	0.8	6.6	6.5	5.8	6.3
II	–	–	–	–	4.1	−0.4	10.9	18	−4.7	6	0.3	3.2	1.4	1.6	5.7	6.4	6.1	6.1	8.9	8.3	8.9	8.7	0.7	1.4	0.8	1.0	8.6	8.0	7.2	7.9
III	–	–	–	–	9.3	1.8	17.3	10	−2.1	20, 23	3.5	7.7	5.2	5.4	6.9	7.4	7.4	7.2	8.7	7.0	8.2	8.0	1.1	3.4	1.8	2.1	8.3	7.6	6.1	7.3
IV	–	–	–	–	16.4	3.7	25.8	15	−3.8	10	6.6	14.9	9.3	10.0	8.1	8.5	8.4	8.3	8.1	5.0	7.1	6.7	1.9	9.4	3.6	5.0	5.5	4.8	3.6	4.6
V	–	–	–	–	18.1	6.2	26.8	27	0.6	19	9.8	16.4	10.7	11.9	10.6	10.6	11.0	10.7	8.7	5.8	8.5	7.7	1.7	8.6	2.1	4.1	6.9	7.4	5.7	6.7
VI	–	–	–	–	24.2	11.6	32.8	27	4.1	21	16.1	22.4	16.3	17.8	15.5	15.3	15.4	15.4	8.4	5.7	8.3	7.5	3.0	12.5	3.3	6.3	5.2	6.3	5.5	5.7
VII	–	–	–	–	22.1	10.7	31.8	3	6.8	9	14.5	20.3	15.0	16.2	14.4	14.7	14.7	14.6	8.7	6.3	8.8	7.9	2.2	9.7	2.6	4.8	6.2	7.8	6.3	6.8
VIII	–	–	–	–	22.2	11.8	31.3	6	5.6	31	14.4	20.6	15.4	16.4	14.9	15.4	15.6	15.3	9.0	6.3	8.6	8.0	1.7	9.6	2.2	4.5	5.3	7.4	5.8	6.2
IX	–	–	–	–	21.8	8.2	30.3	2	−0.5	23	10.3	20.4	12.4	13.9	11.7	13.0	13.0	12.6	9.1	5.5	8.7	7.8	1.3	11.8	1.9	5.0	4.0	4.4	2.9	3.8
X	–	–	–	–	16.4	5.0	23.0	19	0.3	29	6.5	15.6	9.5	10.3	8.9	10.5	9.5	9.6	9.1	6.1	8.1	7.8	1.0	7.6	2.6	3.7	5.1	5.8	3.4	4.8
XI	–	–	–	–	6.3	1.2	14.5	3	−8.3	23	2.6	5.3	3.5	3.7	7.1	7.8	7.5	7.5	9.3	8.6	9.2	9.0	0.5	1.4	0.6	0.8	8.5	8.1	8.1	8.2
XII	–	–	–	–	−0.1	−7.7	15.7	5	−24.7	26	−4.2	−2.1	−4.1	−3.6	4.5	4.7	4.6	4.6	8.4	8.0	8.8	8.4	0.8	1.3	0.6	0.9	8.0	7.2	6.6	7.3
Rok	–	–	–	–	13.4	3.7	32.8	27.VI	−24.7	26.XII	6.3	11.9	7.5	8.3	9.4	9.9	9.8	9.7	8.7	6.7	8.5	8.0	1.4	6.5	1.9	3.3	6.5	6.8	5.6	6.3

Wisznice — φ = 51°47' — λ = 23°13'

I	–	–	–	–	−1.2	−8.3	7.3	4	−24.0	26	−5.9	−2.8	−4.9	−4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.9	6.2	6.9
II	–	–	–	–	2.8	−1.2	8.8	18	−4.3	7	−0.6	1.9	0.4	0.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.9	7.9	8.1
III	–	–	–	–	8.1	1.1	18.0	18	−3.1	20	2.3	6.5	4.1	4.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.0	3.5	25.1	15	−4.0	10	6.4	14.1	9.3	9.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.4	6.1	26.5	28	2.0	5	10.4	15.4	11.2	12.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	24.2	11.1	33.3	27	4.3	21	16.8	22.6	16.4	18.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	23.2	10.7	31.1	3	6.1	6	15.7	21.1	16.3	17.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.5	11.6	31.5	7	6.3	31	15.3	20.5	16.3	17.1	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.5	6.6	5.8
IX	–	–	–	–	21.5	7.4	30.7	3	−1.7	23	10.2	19.8	13.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	3.0	2.9	3.6
X	–	–	–	–	16.1	5.1	21.4	19	0.1	23	6.8	19.0	10.1	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	5.9	0.8	14.3	3	−8.1	23	2.4	4.9	3.1	3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.9	8.0	8.5
XII	–	–	–	–	−1.4	−8.4	13.9	5	−22.0	27	−5.1	−2.8	−5.5	−4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	6.9	7.7
Rok	–	–	–	–	12.9	3.3	33.3	27.VI	−24.0	26. I	6.2	11.4	7.6	8.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kalisz — φ = 51°44' — λ = 18°05'

I	1001.7	1025.8	979.8	1020.1	−0.5	−7.1	7.2	4	−21.7	27	−5.6	−2.0	−4.2	−4.0	4.2	4.8	4.4	4.5	9.2	8.5	9.0	8.9	0.4	0.8	0.5	0.6	5.9	5.9	4.9	5.6
II	1004.1	1020.0	975.2	1022.1	5.4	−0.1	12.6	18	−4.3	6	0.8	4.0	1.9	2.2	6.3	7.1	6.5	6.6	9.6	8.7	9.2	9.2	0.3	1.1	0.5	0.6	8.8	7.7	5.8	7.3
III	1000.5	1019.1	975.2	1018.2	9.5	2.1	18.2	10	−4.3	20	3.3	7.6	5.4	5.4	7.0	7.7	7.4	7.4	8.9	7.4	8.2	8.2	0.9	3.0	1.7	1.9	8.2	7.7	5.7	7.2
IV	995.2	1005.3	984.9	1012.5	16.0	4.7	24.6	7	−1.0	10	7.1	14.4	9.8	10.3	8.9	9.4	9.4	9.2	8.6	5.7	7.6	7.3	1.4	7.9	3.1	4.1	5.8	5.1	4.9	5.3
V	995.2	1002.8	981.3	1012.5	16.3	6.9	21.8	27	2.2	12, 13	9.5	14.3	10.6	11.2	10.4	10.6	11.2	10.7	8.7	6.6	8.8	8.0	1.6	6.1	1.7	3.1	7.0	7.9	6.9	7.3
VI	998.2	1012.0	987.1	1015.1	23.3	11.8	30.3	27	5.5	22	15.9	21.3	16.5	17.6	15.2	15.1	15.7	15.3	8.4	6.0	8.3	7.6	3.0	10.9	3.3	5.7	5.1	6.4	5.1	5.5
VII	996.7	1009.0	981.3	1013.6	20.7	11.4	32.4	3	7.2	8	14.5	18.3	14.7	15.7	14.0	14.1	14.2	14.1	9.5	6.7	8.5	7.9	2.7	8.6	2.9	4.7	7.3	7.7	7.0	7.3
VIII	999.3	1012.7	987.8	1016.3	21.3	12.1	30.3	6	7.5	14	14.2	19.5	15.5	16.2	15.0	15.6	15.9	15.5	9.1	6.9	8.9	8.3	1.5	7.7	2.1	3.8	7.3	7.3	6.0	6.9
IX	1001.8	1012.7	989.3	1019.0	21.0	9.4	29.2	2	2.7	24	11.4	19.8	13.4	14.5	12.5	13.7	13.4	13.2	9.1	6.0	8.6	7.9	1.2	10.0	2.2	4.5	4.4	5.1	3.3	4.3
X	1001.2	1013.6	973.7	1018.6	15.4	6.8	21.8	6	2.2	31	7.8	14.4	10.0	10.6	10.0	11.5	11.0	10.8	9.6	7.2	9.0	8.5	0.7	5.2	1.3	2.4	6.9	6.7	4.6	6.1
XI	997.0	1019.9	985.1	1014.7	6.2	1.3	12.7	2	−4.8	22, 23	2.5	5.2	3.2	3.5	7.1	7.7	7.5	7.4	9.4	8.6	9.5	9.2	0.4	1.4	0.4	0.7	8.5	8.6	6.6	7.9
XII	998.6	1028.2	976.1	1017.0	−0.6	−7.1	15.8	5	−24.3	26	−4.6	−2.5	−4.2	−3.8	4.7	4.9	4.6	4.7	9.2	8.6	9.1	9.0	0.5	0.9	0.5	0.6	7.2	6.9	6.1	6.7
Rok	999.1	1028.2	973.7	1016.6	12.8	4.4	32.4	3.VII	−24.3	26.XII	6.4	11.2	7.7	8.2	9.6	10.2	10.1	10.0	9.0	7.2	8.7	8.3	1.2	5.3	1.7	2.7	6.9	6.9	5.6	6.5

Puczniew

$H_s = 142\ m$ $h_w = 10\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%D, ∑D] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min ≤ -10°	Max < 0°	Min < 0°	Max ≥ 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	≥ 1.0	≥ 10.0	≡	⊞	∑R
I	2.5	2.6	10.5	1.8	6	2.0	9.5	2.5	21	3.0	16.5	3.2	8.5	2.2	0.5	5.0	18	2.1	21.1	9.4	14	12	11	2.5	·	·	·	2	11	8	4	·	–	–	·
II	2	2.5	·	·	1	3.0	1.3	2.7	20.5	3.7	15.5	3.4	14.5	3.1	5.5	3.5	12	2.8	29.5	11.0	9	·	·	13	·	1	·	1	14	14	9	1	–	·	·
III	·	·	·	·	·	·	·	·	1.5	3.7	2.4	4.6	46.5	5.3	1.4	5.8	7	4.8	28.5	6.6	29	·	·	8	·	5	·	·	17	14	10	·	–	·	·
IV	1.5	1.7	4.5	3.4	25.5	4.4	9.5	3.7	6	2.5	9	4.4	12	3.4	4	5.0	18	3.1	26.0	5.6	2,8	·	·	3	·	·	·	4	7	8	7	·	–	·	2
V	5.5	4.0	6	4.2	1.5	1.7	3.5	3.0	5.5	2.4	14.5	3.2	20	3.3	13.5	4.1	23	2.6	46.3	9.9	8	·	·	·	·	·	·	·	13	15	11	·	–	·	3
VI	·	·	4	2.8	5	3.9	8	3.0	9	2.7	11	2.4	26	4.1	6	3.8	21	2.6	59.4	36.6	8	·	·	·	12	·	·	1	10	8	6	1	6	·	6
VII	5	2.0	0.5	3.0	1	1.0	·	·	6.5	2.4	29.5	3.6	25.5	3.8	11	2.6	14	2.8	156.0	43.9	31	·	·	·	7	1	·	3	17	18	16	5	2	·	7
VIII	3.5	1.8	2	3.0	2.5	5.8	2.5	1.0	4	2.1	2.8	3.8	20.5	3.6	1.4	2.9	16	2.8	85.1	41.0	10	·	·	·	5	2	·	2	13	18	13	2	15	·	6
IX	3.5	1.9	3	2.5	13.5	2.0	12	3.0	12	1.8	12.5	3.6	17	3.2	5.5	1.9	11	2.3	22.3	6.6	14	·	·	·	7	1	·	12	9	5	5	·	16	·	·
X	1.5	1.7	·	·	2.1.5	4.4	2.2	3.6	2.0	2.4	9.5	2.6	7.5	2.9	6	2.8	5	3.1	16.2	6.4	18	·	·	·	·	·	·	3	9	8	4	·	16	·	·
XI	10	3.4	5	5.9	9.5	5.3	7.5	2.2	6.5	2.1	2.3	3.8	11.5	3.0	6	4.0	11	3.2	53.0	12.1[2]	5	·	·	9	·	2	·	1	20	–	–	–	12	·	·
XII	5	5.1	8	4.0	2	5.8	6	4.4	10.5	3.5	16	4.9	21.5	4.2	12	4.7	12	3.8	25.4	12.2	11	10	15	24	·	1	·	4	17	11	5	1	5	20	·
Rok	40	2.2	43.5	2.6	8.9	3.3	9.3.5	2.4	123	2.7	209	3.6	231	3.5	9.8	3.8	168	3.0	568.8	43.9	31.VII	22	2.6	8.2	3.1	13	·	3.3	157	–	–	–	–	–	2.4

Warka

$H_s = 120\ m$ $h_w = 13\ m$

I	3	1.8	0.5	2.0	1.5	1.0	7	1.5	8	2.1	18.5	2.5	10.5	3.5	10	2.8	3.4	1.6	31.1	7.5	31	12	1.1	2.8	·	·	·	6	14	13	6	·	2	2.4	·
II	0.5	2.0	·	·	0.5	1.0	9	1.9	9.5	3.1	15.5	2.2	20.5	3.0	4.5	2.2	2.4	1.8	13.8	4.7	9	·	·	15	·	·	·	-1	19	9	4	·	4	2	·
III	·	·	·	·	·	·	·	·	1	6.0	1.0	4.0	52.5	5.8	20.5	6.4	9	5.2	16.8	2.7	21,29,30	·	·	8	·	9	5	2	13	15	8	·	1	1	·
IV	2	1.2	3	3.0	13.5	2.7	17.5	3.5	2.5	2.4	7	2.6	12.5	5.4	6	3.6	2.6	2.5	31.6	8.7	16	·	·	4	1	1	1	8	7	7	7	·	·	·	2
V	2	2.5	4.5	1.7	5	2.0	3.5	1.3	7	1.9	5	1.4	19	2.5	18	3.1	2.9	1.6	46.1	8.7	7	·	·	·	3	1	·	1	8	16	8	·	·	·	3
VI	1	6.0	2.5	2.4	5.5	2.5	5.5	1.8	4.5	1.8	14.5	2.0	20	2.6	13.5	3.3	2.3	1.9	88.4	25.2	27	·	·	·	12	·	·	3	6	14	12	3	·	·	10
VII	2	4.0	·	·	3	2.3	1	1.0	5	2.8	1.4	2.3	38.5	2.6	8.5	2.6	2.1	2.0	89.2	23.6	30	·	·	·	7	1	·	3	12	15	11	3	1	·	8
VIII	3	1.5	2	1.2	1	2.0	·	·	2.5	1.2	1.7	2.2	2.8	3.1	16.5	2.8	2.3	1.9	46.7	16.2	10	·	·	·	8	1	1	2	10	13	8	2	1	·	2
IX	1	2.0	2.5	1.4	9	1.4	4	1.7	3.5	1.0	13.5	2.7	12	2.8	8.5	3.8	3.6	1.5	7.7	3.0	6	·	·	1	8	·	·	1.4	5	6	3	·	1	·	·
X	·	·	·	·	1.1	2.5	30.5	3.0	1.2	2.7	8.5	1.6	8	4.1	6	2.0	1.7	2.3	3.0	1.9	1.4	·	·	·	·	·	·	9	6	2	2	·	5	·	·
XI	6.5	2.6	3	3.0	8.5	3.2	1.3	2.4	5	1.6	1.3	3.1	14.5	3.5	4.5	3.8	2.2	2.2	86.0	19.1	13	·	·	11	·	·	·	2	23	22	13	4	6	1	·
XII	7.5	3.1	5	2.7	·	·	11.5	2.0	4.5	1.1	15.5	4.4	16	2.7	13	3.4	2.0	2.4	23.3	9.6	11	10	14	24	·	1	1	3	17	12	6	·	2	20	
Rok	28.5	2.2	23	1.4	58.5	1.7	102.5	1.7	65	2.3	152	2.6	252	3.5	129.5	3.3	284	2.2	483.7	25.2	27.VI	22	2.5	91	39	14	8	54	140	144	88	12	23	48	2.5

Wisznice

$H_s = 152\ m$ $h_w = 13\ m$

I	8	2.5	2	1.5	11.5	1.8	13.5	2.1	18.5	2.7	8.5	2.6	18	3.8	3	3.3	1.0	2.4	21.6	9.5	31	13	13	2.9	·	·	·	2	15	15	4	·	·	2.2	–
II	·	·	1.5	2.0	8.5	1.4	8.5	2.1	20	2.2	10.5	2.0	23.5	2.4	2.5	1.8	9	1.9	7.1	2.5	12	·	2	1.8	·	·	·	·	20	12	3	·	11	·	–
III	1	5.0	·	·	·	·	0.5	3.0	4.5	4.1	1.7	5.1	57.5	5.5	11.5	5.3	1	5.3	23.0	8.8	21	·	·	10	·	6	1	–	–	16	4	·	3	2	–
IV	9	1.7	9	2.0	14.5	2.8	10	3.6	13.5	2.1	11	2.0	15	4.6	2	2.2	6	2.6	25.6	8.2	2	·	·	8	1	3	·	–	–	6	6	·	1	·	–
V	9	1.8	4	1.2	13.5	2.0	7	1.6	5.5	1.6	13.5	2.8	21	2.1	8.5	2.9	1.1	1.9	40.1	7.0	3	·	·	·	3	·	·	–	–	15	12	·	2	·	–
VI	3	2.3	2.5	1.8	19.5	1.7	6.5	2.4	9	2.4	11	2.4	26	2.9	4.1	2.8	3.5	2.6	9	2.5	66.7	28.6	30	·	·	·	8	·	·	–	–	9	8	1	·	·	–
VII	5	2.3	1	2.5	·	·	1.0	2.7	3	2.3	20.5	2.9	41	2.8	3.5	2.6	9	2.5	66.7	28.6	30	·	·	·	8	·	·	–	–	12	9	3	1	·	–
VIII	2.5	2.8	·	·	·	·	4.5	2.1	3	1.8	2.3	3.8	3.9	3.4	1.0	3.6	1.1	3.0	35.4	10.0	13	·	·	·	8	1	·	2	6	14	9	1	3	·	–
IX	4	2.0	3	2.3	11.5	2.4	4	1.9	6.5	1.9	2.0	3.9	14	4.4	4	3.5	2.3	2.4	17.2	7.5	14	·	·	4	8	2	1	10	3	4	4	·	7	·	–
X	3	2.3	5	2.5	24.5	3.4	3.1	3.1	9	3.2	1.5	2.3	6.5	2.8	3.5	2.3	9	2.8	4.0	2.8	14	·	·	·	·	·	·	–	–	2	2	·	8	·	–
XI	8	2.4	1.5	4.3	19	4.3	11	2.7	16.5	2.2	12	4.6	11	4.3	2	4.5	9	3.1	42.6	12.5	8	·	1	14	·	·	·	1	23	16	9	2	7	·	–
XII	16.5	4.2	4	2.9	8	2.6	8	1.8	14	2.9	11.5	3.8	13	4.6	16	3.4	2	3.4	29.1	8.4	1	11	20	26	·	1	·	2	18	12	5	·	·	24	–
Rok	69	2.4	33.5	1.9	130.5	1.9	114.5	2.4	123	2.4	160	3.2	285.5	3.6	71	3.2	108	2.8	358.5	28.6	30.VII	24	36	109	40	13	1	–	–	133	75	7	43	48	–

Kalisz

$H_s = 140\ m$ $H_p = 143,1\ m$ $h_w = 15\ m$

I	2.5	1.8	7.5	2.7	4	2.0	1.8	2.3	2.5	2.6	1.5	3.4	10	2.6	4	2.1	7	2.4	20.5	8.6	14	11	12	2.7	·	·	·	7	11	10	5	·	3	2.1	·
II	1.5	2.7	·	·	2	1.5	14.5	2.9	18.5	3.2	12.5	3.1	17	3.6	11	2.9	7	2.8	31.4	12.6	9	·	·	14	·	1	1	1	14	13	8	1	6	1	·
III	·	·	·	·	·	·	0.5	1.0	3.5	3.4	22.5	4.6	52	5.5	13.5	4.2	1	4.9	31.0	6.8	29	·	·	7	·	6	2	1	13	15	8	·	4	3	·
IV	5	2.2	9.5	3.3	21.5	3.7	12.5	2.8	6	2.4	9.5	3.0	12.5	3.1	6.5	3.8	7	2.9	31.7	9.3	16	·	·	2	·	·	·	4	9	9	6	·	1	·	4
V	11.5	2.8	3	3.0	3	1.7	4	1.9	5.5	2.0	18.5	3.4	17.5	3.2	16	3.0	14	2.5	77.2	28.2	29	·	·	·	·	·	·	1	12	13	10	1	1	·	6
VI	1	1.0	6	1.3	7.5	2.5	6	1.2	7	1.9	13	3.0	24	3.1	13.5	2.7	12	2.2	50.0	16.4	7	·	·	·	10	·	·	3	6	11	8	1	1	·	8
VII	2	1.5	0.5	1.0	0.5	1.0	3.5	1.1	10.5	2.0	31	3.5	29	4.0	8	2.4	8	2.9	134.9	31.7	31	·	·	·	7	·	·	3	15	19	15	6	·	·	7
VIII	3.5	1.3	4.5	1.3	2.5	2.8	3.5	1.0	3	3.5	32	3.6	26.5	3.5	8.5	2.5	9	2.9	58.1	16.0	11	·	·	·	5	·	·	1	9	17	9	1	3	·	5
IX	4	1.5	2.5	1.4	16	2.2	11	2.2	10	1.6	20	2.6	15	3.3	3.5	3.1	8	2.2	11.5	4.2	14	·	·	·	7	·	·	10	6	7	3	·	1	·	2
X	1.5	1.3	2	4.2	16.5	4.1	18.5	3.3	2.2	3.0	6.5	2.8	7	3.0	8	2.8	11	2.9	28.7	8.4	18	·	·	·	·	·	·	5	10	6	5	·	5	·	·
XI	3.5	3.1	4.5	4.2	11.5	3.5	5	2.3	1.5	2.3	18.5	3.3	11.5	3.2	8.5	2.4	12	2.6	56.5	28.1	13	·	·	9	·	1	·	1	15	14	8	1	7	·	·
XII	6.5	2.8	7.5	2.7	3.5	3.1	9	2.2	13.5	2.7	13	5.5	15.5	4.1	15.5	3.1	9	3.1	33.9	15.5	11	11	15	23	·	2	·	3	12	11	8	1	5	19	·
Rok	47.5	1.8	47.5	2.1	88.5	2.3	10.6	2.0	139.5	2.6	212	3.5	237.5	3.5	116.5	2.9	105	2.8	565.4	31.7	31.VII	22	2.7	8.2	2.9	10	3	4.0	132	145	93	12	37	44	3.2

Łódź - Lublinek

$\varphi = 51°44'$ $\lambda = 19°24'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	996.1	1019.4	976.5	1020.1	-0.2	-7.6	7.7	4	-21.3	18	-5.5	-2.1	-4.1	-3.9	4.1	4.6	4.4	4.4	89	83	88	87	0.5	0.9	0.6	0.7	7.5	6.9	5.6	6.7
II	998.4	1013.5	970.1	1021.8	5.2	-0.6	11.8	18	-6.1	6	0.6	3.4	1.5	1.8	6.1	6.6	6.3	6.3	94	84	93	90	0.3	1.3	0.5	0.7	9.0	8.2	6.4	7.9
III	993.9	1012.2	969.8	1017.1	9.4	1.6	18.2	10	-4.9	20	2.8	6.7	4.7	4.7	6.8	7.1	7.3	7.1	90	73	85	83	0.9	3.0	1.4	1.8	9.0	8.3	6.1	7.8
IV	989.9	1000.1	980.1	1012.5	16.2	4.6	25.2	7	-1.3	10	7.1	14.0	9.4	10.0	8.2	8.3	8.4	8.3	79	52	70	67	2.1	8.7	3.8	4.9	6.5	5.7	4.2	5.5
V	989.3	995.6	975.8	1011.8	17.1	6.6	24.0	27	2.0	23	9.6	14.5	10.6	11.3	10.2	10.0	10.5	10.2	85	61	82	76	1.9	7.0	2.6	3.8	7.0	8.2	7.0	7.4
VI	992.4	1005.3	982.4	1014.4	24.0	11.7	33.3	27	5.2	22	16.1	21.6	16.6	17.7	14.6	13.4	14.6	14.2	79	53	77	70	4.0	13.1	4.5	7.2	5.7	6.5	5.7	6.0
VII	990.8	1002.7	975.2	1013.0	21.4	10.6	32.8	3	4.7	8	14.0	18.7	14.7	15.5	13.5	12.9	13.6	13.3	84	61	82	76	3.0	9.6	3.4	5.3	7.5	8.2	6.1	7.3
VIII	993.4	1006.8	982.2	1015.7	21.5	11.8	30.8	6	7.6	30	14.0	19.2	15.3	16.0	14.3	14.2	15.0	14.5	89	64	85	79	2.0	8.6	2.7	4.4	6.5	7.9	6.2	6.9
IX	996.1	1007.2	983.8	1018.6	21.0	9.6	30.2	2	3.5	22	11.3	19.1	13.7	14.4	11.8	12.4	12.6	12.3	87	57	79	74	1.8	10.6	3.4	5.3	5.5	4.7	3.9	4.7
X	995.9	1007.9	969.9	1018.7	16.2	6.5	21.1	6	0.1	10	7.6	14.2	10.3	10.6	9.3	10.2	10.0	9.8	89	64	81	78	1.3	6.3	2.7	3.4	7.4	7.4	4.4	6.4
XI	991.1	1013.2	979.3	1014.2	6.9	1.2	13.7	7	-6.8	23	2.3	5.0	3.3	3.5	7.0	7.5	7.3	7.3	94	84	92	90	0.5	1.5	0.6	0.9	8.2	8.8	8.1	8.4
XII	992.3	1021.1	971.3	1016.1	0.1	-7.3	14.9	5	-23.2	26	-4.3	-2.6	-4.2	-3.8	4.6	4.7	4.4	4.6	88	84	89	87	0.6	1.0	0.6	0.7	7.9	7.5	6.2	7.2
Rok	993.3	1021.1	969.8	1016.2	13.2	4.1	33.3	27.VI	-23.2	26.XII	6.3	11.0	7.6	8.1	9.2	9.3	9.5	9.3	87	68	84	80	1.6	6.0	2.2	3.3	7.3	7.4	5.8	6.8

Uwaga: Ciśnienie powietrza jest za niskie przeciętnie o ok. 0,6 mb

Łódź - Ruda Pabianicka

$\varphi = 51°42'$ $\lambda = 19°27'$

I	–	–	–	–	-0.9	-8.7	6.8	4	-23.8	27	-6.2	-2.0	-5.0	-4.6	3.9	4.4	4.1	4.1	87	79	86	84	0.5	1.1	0.6	0.7	8.2	7.0	5.3	6.8
II	–	–	–	–	4.7	-0.8	11.9	18	-6.2	6	0.5	3.5	1.1	1.6	6.0	6.5	6.1	6.2	93	83	91	89	0.4	1.4	0.6	0.8	9.4	7.9	7.2	8.2
III	–	–	–	–	8.9	1.9	17.5	10	-3.5	20	3.0	7.1	4.9	5.0	6.7	7.2	7.2	7.0	88	72	83	81	0.9	3.2	1.6	1.9	8.6	8.1	6.2	7.6
IV	–	–	–	–	16.3	4.2	25.1	7	-3.0	10	7.0	14.7	8.9	9.9	8.2	8.5	8.6	8.4	80	51	74	68	2.1	9.2	3.1	4.8	6.3	5.7	4.2	5.4
V	–	–	–	–	17.2	6.2	24.6	27	0.7	19	9.7	15.1	10.2	11.3	10.2	10.3	10.7	10.4	84	60	86	77	2.0	7.4	1.9	3.8	7.3	8.4	7.0	7.6
VI	–	–	–	–	23.8	11.4	32.9	27	5.5	21	16.1	21.8	15.9	17.4	14.9	14.5	15.2	14.9	81	57	83	74	3.6	12.3	3.1	6.3	5.5	7.1	5.8	6.1
VII	–	–	–	–	21.0	10.5	33.4	3	4.5	8	14.0	19.1	14.1	15.3	13.8	13.5	14.0	13.8	86	63	86	78	2.4	9.6	2.4	4.8	7.3	8.3	5.8	7.1
VIII	–	–	–	–	21.2	11.6	31.1	6	6.6	4	14.1	19.6	14.7	15.8	14.6	14.8	15.1	14.8	90	65	99	81	1.8	8.7	2.0	4.2	6.5	8.0	6.4	7.0
IX	–	–	–	–	20.7	8.8	29.8	2	1.8	24	11.0	19.6	12.7	14.0	11.7	13.1	12.8	12.5	88	58	85	77	1.7	10.6	2.2	4.8	6.0	5.0	4.0	5.0
X	–	–	–	–	15.4	5.7	20.4	6	1.1	31	7.2	14.3	9.4	10.1	9.2	10.7	9.9	9.9	90	67	84	80	1.4	5.8	2.1	3.0	7.6	7.1	4.0	6.2
XI	–	–	–	–	6.2	1.2	13.0	7	-7.0	22	2.3	5.1	3.1	3.4	6.9	7.4	7.2	7.2	93	83	92	89	0.6	1.6	0.7	1.0	9.0	8.6	7.8	8.5
XII	–	–	–	–	-0.3	-7.4	14.4	5	-23.6	26	-4.6	-2.5	-4.3	-3.9	4.4	4.7	4.4	4.5	86	82	87	85	0.7	1.1	0.7	0.8	8.9	7.7	6.4	7.7
Rok	–	–	–	–	12.8	3.7	33.4	3.VII	-23.6	27.I	6.2	11.3	7.1	7.9	9.2	9.6	9.6	9.5	87	68	86	80	1.5	6.0	1.8	3.1	7.6	7.4	5.8	6.9

Smolice

$\varphi = 51°42'$ $\lambda = 17°11'$

I	–	–	–	–	0.1	-6.9	7.3	4	-20.8	27	-5.1	-0.8	-3.6	-3.3	4.1	4.8	4.5	4.6	86	78	86	83	0.6	1.3	0.7	0.9	5.9	5.7	6.0	5.9
II	–	–	–	–	6.4	0.4	14.9	18	-3.5	6	1.5	5.4	2.7	3.1	6.4	7.3	6.8	6.8	93	81	90	88	0.5	1.8	0.8	1.0	8.7	7.1	5.2	7.0
III	–	–	–	–	10.2	2.3	18.5	10	-4.5	20	3.8	8.7	5.8	6.0	7.1	7.4	7.5	7.3	88	67	81	79	1.0	4.2	2.0	2.4	8.0	7.5	5.6	7.0
IV	–	–	–	–	16.2	5.0	25.3	7	-1.1	1	8.2	14.7	9.7	10.6	9.3	9.3	9.5	9.4	83	56	78	72	1.8	8.3	2.9	4.3	5.3	5.4	3.8	4.8
V	–	–	–	–	16.0	6.8	22.2	26	2.5	12	10.4	14.4	10.6	11.5	10.9	11.1	11.3	11.1	87	69	87	81	1.8	5.6	1.7	3.0	7.5	8.1	6.3	7.3
VI	–	–	–	–	23.2	11.6	28.3	25	5.5	22	16.2	21.5	16.3	17.6	15.6	14.9	16.0	15.5	84	58	86	76	3.0	11.3	2.7	5.7	5.2	6.0	4.1	5.1
VII	–	–	–	–	21.3	11.1	31.1	3	6.1	8	15.0	19.6	14.7	16.0	14.1	13.7	14.6	14.1	83	62	87	77	3.3	10.1	2.4	5.3	7.1	7.7	7.6	7.5
VIII	–	–	–	–	21.4	11.6	31.3	6	7.2	14	14.8	20.1	15.7	16.6	15.1	15.1	15.5	15.2	89	65	86	80	1.9	9.1	2.7	4.6	7.3	7.2	5.2	6.6
IX	–	–	–	–	21.6	9.8	29.8	2.17	3.8	25	12.2	20.5	14.0	15.2	12.8	13.0	13.5	13.1	89	54	83	75	1.7	11.8	2.8	5.4	4.6	5.2	3.2	4.3
X	–	–	–	–	15.9	7.1	22.0	5	0.5	13	8.2	15.1	10.5	11.1	10.2	11.3	11.0	10.8	93	68	87	83	0.9	6.2	1.8	3.0	6.7	6.5	4.6	5.9
XI	–	–	–	–	6.4	1.4	12.9	2	-5.3	23	2.6	5.6	3.5	3.8	7.0	7.8	7.5	7.4	93	85	93	90	0.5	1.5	0.6	0.9	8.3	8.6	6.8	7.9
XII	–	–	–	–	0.1	-6.8	15.1	5	-23.6	27	-3.9	-1.6	-3.7	-3.2	4.6	5.0	4.5	4.7	84	81	84	83	0.9	1.2	0.9	1.0	7.5	6.3	6.4	6.7
Rok	–	–	–	–	13.2	4.4	31.3	6.VIII	-23.6	27.XII	7.0	11.9	8.0	8.8	9.8	10.1	10.2	10.0	88	69	86	81	1.5	6.0	1.8	3.1	6.8	6.8	5.4	6.3

Głogów

$\varphi = 51°39'$ $\lambda = 16°06'$

I	–	–	–	–	0.3	-6.4	6.5	9	-21.8	27	-4.4	-0.8	-3.3	-3.0	4.4	4.8	4.8	4.7	88	80	89	86	0.5	1.3	0.6	0.8	7.0	5.9	6.6	6.5
II	–	–	–	–	7.4	0.9	14.3	15	-3.6	26	2.0	6.1	3.5	3.8	6.5	7.6	7.0	7.0	91	81	88	87	0.7	2.0	1.0	1.2	7.4	7.0	5.5	6.6
III	–	–	–	–	10.6	3.0	20.2	10	-4.3	20	4.5	9.0	6.2	6.5	7.4	7.9	7.5	7.6	87	69	79	78	1.2	3.7	2.2	2.4	7.6	7.4	6.1	7.0
IV	–	–	–	–	16.6	5.7	25.6	7	-0.8	1	8.7	15.4	10.3	11.2	9.3	9.7	9.5	9.5	82	56	75	71	2.2	8.6	3.4	4.7	5.6	5.2	4.5	5.1
V	–	–	–	–	15.7	7.5	23.0	26	3.5	16	10.1	13.9	11.0	11.5	10.6	10.6	11.0	10.7	86	68	84	79	1.9	5.6	2.3	3.3	8.1	8.3	7.5	8.0
VI	–	–	–	–	23.3	12.6	29.7	25	8.1	16, 22	16.0	21.5	16.5	17.6	14.6	14.6	15.0	14.7	80	57	80	72	3.8	11.4	3.9	6.4	5.0	6.1	5.6	5.6
VII	–	–	–	–	21.0	12.2	32.8	3	7.8	6	15.2	19.5	14.8	16.1	14.1	13.2	13.8	13.7	81	60	82	74	3.5	10.4	3.4	5.8	7.7	7.9	8.2	7.9
VIII	–	–	–	–	21.7	12.5	31.3	6	8.0	14	14.9	20.1	15.7	16.6	14.5	15.3	15.2	15.0	85	65	84	78	2.7	8.9	2.9	4.8	7.5	7.2	6.1	6.9
IX	–	–	–	–	22.0	10.7	30.8	2	3.2	24	12.8	20.9	14.9	15.9	13.0	13.9	13.6	13.5	87	58	79	75	2.2	11.8	3.8	5.9	5.3	5.4	3.3	4.7
X	–	–	–	–	16.2	7.2	22.3	5	3.5	30	8.9	15.4	10.3	11.2	10.0	10.6	10.5	10.4	88	62	84	78	1.5	7.3	2.1	3.7	6.8	6.3	5.2	6.1
XI	–	–	–	–	6.6	1.7	13.4	2	-5.4	22	2.9	5.7	3.8	4.0	7.0	7.7	7.4	7.4	91	83	90	88	0.8	1.6	0.8	1.1	8.6	8.1	7.3	8.0
XII	–	–	–	–	0.7	-6.4	16.1	5	-23.1	26	-3.4	-1.3	-3.4	-2.9	4.8	5.0	4.7	4.8	85	80	85	83	0.9	1.3	0.8	1.0	7.1	6.5	5.6	6.4
Rok	–	–	–	–	13.5	5.1	32.8	3.VII	-23.1	26.XII	7.4	12.1	8.4	9.1	9.7	10.1	10.0	9.9	86	68	83	79	1.8	6.2	2.3	3.4	7.0	6.8	6.0	6.6

Łódź - Lublinek

$H_s = 187 m$ $H_b = 187,7 m$ $h_w = 11 m$ **1961**

MIESIĄC	Rozkład wiatru N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Temperatura Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	⌈⌉
I	3	4.0	7.5	3.1	10.5	2.1	13	3.2	16	4.7	17	5.2	11	4.5	3	3.2	12	3.5	22.4	10.4	31	13	12	26	·	1	·	4	14	11	4	1	8	21	·
II	1.5	3.7	0.5	1.0	5.5	2.3	11.5	2.7	16.5	4.0	15.5	4.6	13.5	4.7	10.5	4.0	9	3.5	30.1	9.5	9	·	·	18	·	1	·	1	16	18	9	·	8	5	·
III	·	·	·	·	·	·	·	·	2	6.2	18.5	5.9	53.5	6.2	14	6.6	5	5.9	36.4	6.9	29	·	·	8	·	14	3	·	15	17	10		6	5	·
IV	3.5	3.6	4	3.9	30.5	5.0	12	5.1	7.5	5.2	6.5	3.2	12.5	5.1	6.5	4.5	7	4.4	39.0	7.0	28	·	·	2	1	5	·	5	6	10	9	·	4	·	2
V	11	3.7	5	3.1	10.5	2.7	5	3.2	5.5	4.4	14.5	4.5	14.5	4.9	10	5.0	17	3.3	54.0	8.5	8	·	·	·	·	3	1	1	13	17	11	·	1	·	6
VI	0.5	5.0	2.5	1.4	10	4.1	9.5	2.5	6.5	2.8	12.5	3.7	25	4.5	11.5	3.3	12	3.2	27.6	16.4	4	·	·		11	1	·	3	5	9	7	1	2	·	8
VII	2	1.8	2.5	2.6	6	1.7	3	2.3	7.5	3.2	18.5	4.9	32.5	4.6	7	3.4	14	3.4	160.4	39.8	31	·	·		7	3	·	2	14	20	15	5	·	·	8
VIII	2.5	2.2	1	3.0	4.5	3.4	4.5	4.3	8	2.9	25.5	4.8	27	4.5	7	3.7	13	3.6	79.8	31.2	10	·		·	5	4	1	2	12	18	13	2	3	·	5
IX	1.5	3.3	2	5.2	22	3.0	8	3.4	7.5	2.9	16.5	4.2	17	5.1	4.5	4.2	11	3.4	21.2	4.9	29	·	·	·	6	1	·	9	10	9	6	·	1	·	2
X	·	·	0.5	2.0	27.5	5.3	23	5.3	10	4.4	8.5	3.8	8	4.4	5.5	3.4	10	4.3	10.2	3.7	29	·		·	·	5	·	3	9	8	3	·	8	·	·
XI	8	4.9	2.5	6.0	17.5	5.2	6.5	2.7	8.5	3.2	17	4.9	15	4.6	5	4.0	10	4.0	84.5	22.2	13	·	·	9	·	4	·	1	20	19	12	2	6	2	·
XII	8.5	4.8	6.5	5.7	8.5	3.6	8	2.3	14.5	3.6	13	7.3	19.5	4.1	11.5	4.4	3	4.4	28.1	10.4	11	11	13	26	·	5	·	3	15	13	5	1	7	19	·
Rok	42	3.1	34.5	3.1	153	3.2	104	3.1	110	4.0	183.5	4.8	249	4.8	96	4.1	123	3.9	593.7	39.8	31.VII	24	25	89	30	47	5	34	149	169	104	12	54	52	31

Łódź - Ruda Pabianicka

$H_s = 181 m$ $h_w = 18 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	⌈⌉
I	3	3.5	3	2.8	17	2.4	21	3.3	11.5	3.8	20	4.6	10.5	4.3	1	3.0	6	3.4	26.6	10.8	31	13	12	30	·	1	·	–	–	15	4	1	–	23	·
II	0.5	1.0	1	3.0	7.5	3.7	11	3.9	13.5	3.7	16.5	4.6	18.5	4.1	6.5	3.9	9	3.6	30.4	10.3	9	·	·	20	·	1	·	–	–	18	9	1	–	3	·
III	·	·	·	·	0.5	1.0	0.5	1.0	1	3.0	26	6.3	54	5.7	9	4.6	2	5.6	45.8	8.2	30	·	·	7	·	6	·	–	–	20	13	·	–	5	·
IV	0.5	1.0	6	3.3	32	5.4	8.5	4.6	6.5	3.9	7	3.9	14.5	5.4	1	4.5	14	4.1	31.8	6.1	2	·	·	2	1	2	·	–	–	10	7	·	–	·	2
V	4.5	3.2	7	2.9	12	1.8	5	4.2	2	3.5	15	4.4	19	3.6	14.5	3.5	14	2.9	73.6	28.8	27	·	·	·	·	5	·	–	–	15	11	1	–	·	6
VI	1	1.0	2	2.8	13	3.1	12.5	2.8	6	1.8	10	3.4	26	3.9	5.5	3.8	14	2.8	65.3	41.4	4	·	·	·	12	·	·	–	–	10	8	1	–	·	7
VII	1	3.0	0.5	4.0	4	2.5	2	2.0	6.5	2.5	26.5	3.7	31.5	3.7	3	2.7	18	2.8	183.2	35.0	31		·	·	7	1	·	–	–	21	15	5	–	·	8
VIII	2	1.5	3	2.3	3.5	3.6	6	2.2	3.5	2.6	32	4.1	25.5	3.6	5.5	3.2	12	3.1	69.1	26.5	10	·	·		5	1	·	–	–	15	10	2	–	·	2
IX	1.5	1.0	6.5	1.9	22	2.4	8	3.3	6	2.8	13	3.9	19	3.7	4	3.1	10	2.7	22.8	7.4	29		·	·	6	·	·	–	–	7	5	·	–	·	2
X	·	·	1.5	4.7	29.5	4.4	23	4.9	10.5	3.0	7.5	2.8	8	4.4	3	3.7	10	3.8	11.3	4.0	18	·	·	·	·	1	·	–	–	10	4	·	–	·	·
XI	6	3.2	1.5	4.0	16	5.3	7	3.3	5.5	3.0	20	4.7	15	4.0	8	2.9	11	3.6	90.5	22.3	13	·	·	10	·	2	·	–	–	24	12	3	–	2	·
XII	6	4.0	5	3.0	8.5	4.0	11	3.0	10.5	2.7	12.5	5.7	22	4.0	13.5	3.9	4	3.7	33.5	11.0	11	11	14	25	·	2	·	–	–	19	8	1	–	19	·
Rok	26	1.9	37	2.9	165.5	3.3	115.5	3.2	83	3.0	206	4.3	263.5	4.2	74.5	3.6	124	3.5	683.9	41.4	4.VI	24	26	94	31	22		–	–	184	106	15	–	52	27

Smolice

$H_s = 107 m$ $h_w = 15 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	⌈⌉
I	·	·	9.5	3.2	16.5	2.3	13	3.2	15.5	2.7	21	3.3	7.5	1.7	·	·	10	2.5	34.7	12.1	31	12	13	23	·	·	·	6	12	11	7	1	2	18	·
II	0.5	3.0	2	5.5	6	3.3	12.5	2.7	12	4.4	17.5	3.2	17.5	2.8	8	2.2	8	2.9	38.5	18.4	9	·	·	12	·			2	12	14	8	1	10	1	·
III	1.5	2.0	·	·	·	·	·	·	1	4.0	23	3.7	44	3.9	19.5	4.0	4	3.7	36.4	7.3	30	·	·	6		·	·	1	13	18	10	·	5	·	·
IV	5.5	1.7	6.5	2.3	22	3.2	9	3.8	9	2.8	8	3.1	7.5	2.5	12.5	2.3	10	2.5	48.8	15.5	16	·	·	1	1	·	·	9	6	10	8	1	·	·	4
V	7	3.0	3.5	2.9	4.5	2.0	5	1.4	2	3.0	13.5	2.7	17	2.9	15.5	2.8	25	2.0	96.6	33.1	29	·		·	·	·	·	2	12	19	17	1	·	·	3
VI	4	2.5	4	1.2	10	1.9	7	2.4	2	2.5	11.5	1.7	22.5	2.4	6	3.0	23	1.6	114.8	23.3	4	·	·	·	9	·	·	4	5	13	11	5	2	·	7
VII	2	1.5	·	·	3	2.0	2	3.0	6	1.8	16	2.6	35	3.2	6	2.5	23	2.2	124.8	46.5	31	·	·	·	7	·	·	2	13	21	14	4	·		4
VIII	1	1.0	2	1.0	4	1.8	2	2.0	9	2.7	23.5	2.5	16.5	2.4	9	2.0	26	1.7	59.0	24.2	11	·	·	·	4	·	·	1	10	15	13	1	7	·	4
IX	2.5	2.4	9.5	1.9	11	2.2	8.5	3.6	9	2.5	14.5	2.2	9	2.9	5	2.4	21	1.9	10.9	3.8	14	·	·	·	7	·	·	9	6	7	3	·	1	·	3
X	3	3.0	2	2.5	21.5	3.4	15.5	3.3	11.5	3.1	7	2.6	6.5	2.2	6	1.8	20	2.3	31.0	7.3	18	·	·	·	·	·	·	5	10	10	6	·	5	·	·
XI	3.5	2.9	9.5	3.2	8	3.1	7	1.4	6.5	3.7	14	2.4	10	1.9	5.5	2.4	26	1.8	55.5	26.9	13	·	·	8	·		·	2	19	14	8	1	7	·	·
XII	4	2.1	9.5	2.1	8.5	2.3	4.5	2.2	8.5	2.8	13.5	4.0	13	3.1	12.5	3.0	19	2.3	43.2	14.9	11	9	14	24	·	·	·	5	14	12	9	1	6	15	·
Rok	34.5	2.1	58	2.2	115	2.3	86	2.4	92	3.0	183	2.8	206	2.7	105.5	2.4	215	2.3	694.2	46.5	31.VII	21	27	74	28	·	·	48	132	164	114	16	45	34	23

Głogów

$H_s = 112 m$ $h_w = 10 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	⌈⌉
I	1	1.0	5.5	2.4	17.5	1.3	4	3.2	6	4.2	23	3.5	12	3.1	7	2.9	17	2.3	28.1	12.1	14	12	13	22	·	·		6	15	11	8	1	1	19	·
II	3	3.2	2.5	1.8	10	2.4	4	2.0	1.5	1.3	13.5	6.0	16	4.1	17.5	3.8	16	3.1	22.1	8.3	1	·	·	11	·	1	·	4	13	12	7	·	3	4[2]	·
III	·	·	·	·	·	·	·	·	·	·	6.5	6.3	41.5	5.9	39	5.0	6	5.2	28.3	5.8	30	·	·	4	·	5	1	4	16	14	10	·	1	·	·
IV	9.5	2.5	16	2.7	11	3.7	10	4.2	3	5.7	5.5	3.0	13	2.9	12	3.7	10	2.9	39.5	7.6	1	·	·	2	1	·	·	7	9	10	8	·	·	·	4
V	3.5	2.1	1	3.0	3	1.3	4	3.5	2	5.5	4	6.4	25	4.0	42.5	3.5	8	3.4	149.4	52.3	1	·	·	·	·	2	·	1	18	18	18	4	·	·	5
VI	4	2.0	6	2.0	3.5	2.0	3	3.2	0.5	5.0	2	5.0	22.5	3.2	35.5	3.3	13	2.7	72.6	21.7	10	·	·	·	10	1	·	7	8	9	9	3	·	·	8
VII	0.5	4.0	1	3.0	·	·	·	·	1	2.0	19	3.6	44	3.4	19.5	3.0	8	3.0	67.1	11.2	30	·	·	·	5	·	·	2	20	18	13	1	·	·	3
VIII	5.5	2.5	1.5	1.3	0.5	2.0	3	1.7	3	3.7	13	4.7	28	3.4	19.5	3.3	19	2.7	67.5	21.1	6	·	·	·	5	1	·	3	12	13	12	2		·	2
IX	3	1.3	7	2.1	9	1.9	1	1.0	3	3.3	15	3.9	18	3.4	9	2.8	25	2.1	21.3	13.7	5	·	·	·	8	·	·	11	7	10	4	1	4	·	3
X	1	2.0	0.5	5.0	16.5	3.9	15	3.7	6	2.7	14.5	3.6	11.5	2.3	13	2.1	15	2.7	38.6	21.5	20	·	·	·	·	1	·	4	12	10	6	1	4	·	·
XI	6	3.2	6.5	3.6	6	3.7	2	5.0	·	·	8.5	6.5	21	4.0	18	3.2	22	3.0	35.2	16.8	13	·	·	7	·	2	·	2	19	11	7	1	5	·	·
XII	1.5	3.7	12.5	2.7	6	2.6	5.5	2.2	2.5	3.0	15.5	6.9	20.5	5.7	16	4.3	13	3.9	42.5	8.5	11	10	15	23	·	3	1	5	13	13	11	·	·	18	·
Rok	38.5	2.3	60	2.5	83	2.1	51.5	2.5	28.5	3.0	140	5.0	273	3.8	248.5	3.4	172	3.1	612.2	52.3	1.V	22	28	69	29	16	2	56	162	149	113	14	18	41[2]	25

Ostrów Wlkp. — φ = 51°39' — λ = 17°49' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.3	-6.5	9.8	4	-20.5	26	-4.7	-0.6	-3.4	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	5.4	5.6
II	–	–	–	–	6.2	0.2	13.7	18	-4.1	6	1.4	5.4	2.7	3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.1	6.1	7.0
III	–	–	–	–	9.9	2.5	19.0	10	-4.7	20	4.1	8.5	5.9	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	6.0	7.1
IV	–	–	–	–	16.8	5.4	25.9	7	-1.6	10	8.2	15.5	10.3	11.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.1	4.5	5.0
V	–	–	–	–	16.6	7.3	23.7	5	2.5	12	10.3	15.0	11.1	11.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.1	8.2	7.9
VI	–	–	–	–	23.8	12.4	30.3	27	6.7	21	16.8	22.4	16.9	18.2	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.3	5.3	5.4
VII	–	–	–	–	21.1	12.0	33.6	3	7.8	8	15.1	19.8	15.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	7.9	7.6
VIII	–	–	–	–	21.8	12.5	31.6	6	7.6	14	14.7	20.3	15.7	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.6	6.1	6.8
IX	–	–	–	–	21.9	10.2	30.7	2	2.1	24	12.5	21.0	14.1	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.5	4.5	4.6
X	–	–	–	–	16.3	7.3	22.2	6	1.8	13	8.3	15.4	10.7	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	4.7	5.8
XI	–	–	–	–	–	–	13.1	2	–	–	2.7	5.6	3.9	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.4	7.2	7.9
XII	–	–	–	–	0.3	-7.0	16.0	5	-26.3	27	-4.2	-1.3	-3.5	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.6	6.6	6.8
Rok	–	–	–	–	–	–	33.6	3.VII	-26.3	27.XII	7.1	12.2	8.3	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.7	6.0	6.4

Żary — φ = 51°38' — λ = 15°08'

I	–	–	–	–	0.7	-6.2	7.2	30	-20.2	27	-3.9	-0.5	-2.9	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.3	5.8	6.3
II	–	–	–	–	7.4	0.8	15.4	15	-4.1	6	2.2	6.2	3.2	3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	6.3	6.8
III	–	–	–	–	10.5	2.0	17.7	17	-6.5	20	3.7	8.9	5.9	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.2	6.2	7.0
IV	–	–	–	–	17.0	5.2	25.6	14	-1.4	1	8.3	15.3	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.4	4.5	5.2
V	–	–	–	–	15.5	6.8	24.1	26	2.9	18	9.5	13.5	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.1	6.5	7.2
VI	–	–	–	–	23.4	11.7	30.0	25	6.0	1	15.6	21.7	16.2	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.5	5.3	5.2
VII	–	–	–	–	20.9	11.3	34.1	3	7.8	8	14.6	18.9	15.1	15.9	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	7.4	7.5
VIII	–	–	–	–	21.1	11.9	31.0	6	7.2	14	14.3	19.3	15.3	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	4.6	5.9
IX	–	–	–	–	22.0	11.0	30.3	3	3.1	23	12.5	21.0	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.2	4.1	4.2
X	–	–	–	–	16.2	6.6	24.3	6	1.0	16	8.2	15.5	9.9	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.7	4.3	5.4
XI	–	–	–	–	6.6	1.3	12.8	2	-6.8	22	2.7	5.8	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	7.7	8.0
XII	–	–	–	–	1.1	-6.7	15.6	5	-20.2	26	-3.4	-1.0	-3.1	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.2	5.2	6.4
Rok	–	–	–	–	13.5	4.6	34.1	3.VII	-20.2	27.I, 26.XII	7.0	12.0	8.2	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	5.7	6.3

Nowe Miasto n. P. — φ = 51°37' — λ = 20°35'

I	–	–	–	–	-0.6	-8.6	6.3	4	-22.2	27	-5.9	-2.3	-4.6	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.1	5.9	7.0
II	–	–	–	–	4.3	-1.0	11.2	18	-7.4	6	0.2	2.9	1.0	1.3	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.5	6.3	8.0
III	–	–	–	–	8.8	1.8	16.6	18	-2.8	20	3.3	7.2	5.0	5.1	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.8	5.9	7.6
IV	–	–	–	–	15.5	4.4	24.7	7	-2.1	10	6.4	14.8	9.4	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	4.5	3.7	4.9
V	–	–	–	–	17.0	6.6	25.7	27	1.6	19	9.2	15.6	11.0	11.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	6.3	7.0
VI	–	–	–	–	23.9	11.8	33.0	27	5.4	21	15.9	22.5	17.2	18.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.6	5.2	5.3
VII	–	–	–	–	21.5	11.4	31.7	3	7.0	6	14.2	19.6	15.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	5.9	6.8
VIII	–	–	–	–	21.4	12.2	30.7	6	8.5	31	14.3	20.1	16.0	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.6	5.7	5.9
IX	–	–	–	–	20.7	9.0	29.2	3, 17	-0.1	23	10.4	19.9	13.6	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	3.5	3.3	3.9
X	–	–	–	–	16.1	5.5	23.4	20	0.9	10	6.6	15.4	10.4	10.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.2	4.0	5.6
XI	–	–	–	–	6.2	1.2	13.7	3	-7.0	23	2.4	4.9	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.1	7.2	8.2
XII	–	–	–	–	-0.5	-7.3	15.6	5	-24.1	26	-4.2	-2.4	-4.1	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.6	5.8	6.8
Rok	–	–	–	–	12.9	3.9	33.0	27.VI	-24.1	26.XII	6.1	11.5	7.8	8.3	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.6	5.4	6.4

Sieradz — φ = 51°36' — λ = 18°44'

I	–	–	–	–	-0.6	-7.5	7.1	4	-23.0	26	-5.5	-1.7	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	5.2	4.4	5.8
II	–	–	–	–	5.1	0.0	12.1	18	-5.5	6	0.8	4.3	1.6	2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.6	6.3	6.1	7.0
III	–	–	–	–	9.3	2.1	18.1	10	-4.0	20	3.7	7.8	5.0	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.7	5.5	6.8
IV	–	–	–	–	16.5	4.9	25.0	7	-0.4	1	7.9	15.3	9.4	10.5	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.4	4.1	4.6
V	–	–	–	–	17.1	7.0	23.0	27	2.3	12	10.3	15.3	10.3	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	6.5	6.6
VI	–	–	–	–	23.8	11.8	31.3	27	6.1	22	17.0	22.1	16.0	17.8	–	–	–	–	–	–	–	–	–	–	–	–	3.3	4.8	4.9	4.3
VII	–	–	–	–	21.2	11.3	32.5	3	6.7	6	15.2	19.5	14.4	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.7	5.9	6.2
VIII	–	–	–	–	21.4	11.9	30.7	6	8.1	4, 14	15.0	20.0	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.0	4.9	5.4
IX	–	–	–	–	21.1	9.5	29.8	2	0.9	24	12.1	20.2	13.5	14.8	–	–	–	–	–	–	–	–	–	–	–	–	3.8	3.2	3.7	3.6
X	–	–	–	–	15.6	6.9	21.4	6	2.6	22	8.3	14.5	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.6	1.7	12.7	2	-5.0	22, 23	2.7	5.5	3.3	3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.1	7.0
XII	–	–	–	–	-0.1	-7.2	14.7	5	-24.6	26	-4.9	-2.5	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	13.1	4.4	32.5	3.VII	-24.6	26.XII	6.9	11.7	7.9	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Ostrów Wlkp. — $H_s = 126\ m$ — $h_w = 11\ m$ — 1961

MIESIĄC	ROZKŁAD WIATRU (%D, %nD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD Suma	OPAD Max	OPAD Data	Temperatura T Min<-10°	Temperatura T Max<0°	Temperatura T Min<0°	Temperatura T Max>25°	Wiatr v ≥10	Wiatr v ≥15	LICZBA DNI (n) G	G	Opad R ≥0.1	Opad R ≥1.0	Opad R ≥10.0	▬	▦	R ≥0
I	·	·	4.5	3.5	9	2.9	11.5	2.8	21	4.0	13.5	3.4	3	4.3	4.5	3.1	26	2.5	27.8	11.1	14	12	13	22	·	·	·	9	9	12	6	1	2	23	·
II	5	3.9	1	1.0	1	3.0	1.4	2.6	13.5	3.3	1.4	3.0	7	2.1	5.5	4.2	23	2.2	27.4	12.3	9	·	·	12	·	1	·	3	15	14	6	1	8	1	·
III	5.5	5.5	·	·	·	·	·	·	5	4.3	16.5	3.5	27.5	4.5	28.5	5.2	10	4.1	35.4	6.1	30	·	·	7	·	4	·	3	14	13	9	·	4	1	·
IV	1	6.0	3.5	4.6	20.5	4.2	17	3.1	7.5	2.3	8.5	3.5	4	4.2	9	3.6	19	2.9	39.2	17.5	16	·	·	2	1	·	·	8	10	9	5	1	·	·	4
V	9	3.4	6	2.4	4	3.1	2.5	3.0	6	2.8	16.5	2.9	7	2.9	9	3.1	33	1.9	75.4	30.7	29	·	·	·	·	·	·	1	20	21	12	1	·	·	3
VI	3	2.3	2	3.2	6	3.0	7.5	3.2	8	2.4	12	2.9	7.5	3.6	8	3.6	36	1.8	59.0	17.1	10	·	·	·	11	·	·	5	8	11	9	3	2	·	8
VII	0.5	2.0	·	·	1	2.0	1.5	3.7	14.5	2.5	28.5	2.9	14.5	4.2	7.5	4.1	25	2.4	120.3	40.7	31	·	·	·	7	·	·	2	18	21	15	4	·	·	5
VIII	1	2.0	0.5	1.0	3.5	1.3	5	1.6	7.5	3.5	2.5	3.8	10.5	4.2	7	2.6	33	2.1	59.0	15.8	11	·	·	·	7	1	·	2	12	18	11	1	2	·	5
IX	1.5	2.3	1	1.0	1.4	2.8	6.5	3.5	13	2.4	9.5	3.1	7	4.4	4.5	2.8	33	1.9	20.2	6.9	26	·	·	·	8	·	·	11	7	8	5	·	2	·	4
X	5	3.4	0.5	3.0	13.5	4.2	19.5	3.4	16.5	3.2	10.5	2.9	2	3.0	1.5	3.7	24	2.6	28.4	10.2	18	·	·	·	·	·	·	5	9	9	4	1	4	·	·
XI	4	2.9	7	3.9	8.5	3.9	4	2.8	10.5	2.7	17.5	3.9	4.5	2.3	5	2.9	29	2.3	60.0	29.6	13	·	·	—	·	·	·	2	21	15	11	1	5	·	·
XII	5.5	2.9	7	2.4	5.5	2.6	7.5	2.3	10.5	2.2	16.5	5.6	6	4.2	15.5	2.5	19	2.6	36.6	11.6	11	11	14	23	·	2	·	4	13	12	8	1	10	16	·
Rok	41	3.0	33	2.2	86.5	2.8	96.5	2.7	133.5	3.0	188.5	3.4	100.5	3.7	105.5	3.4	310	2.4	568.7	40.7	31.VII	23	27	—	34	8	·	55	156	163	101	15	39	41	29

Żary — $H_s = 162\ m$ — $h_w = 20\ m$

I	1	1.0	1.5	4.0	13	4.8	20	3.5	25	6.1	21	6.3	6	6.2	15	3.3	4	5.0	44.4	12.1	14	11	11	23	·	5	2	6	14	18	10	1	5	19	·
II	0.5	4.0	·	·	4	2.5	6.5	3.0	1.5	7.6	22	5.8	23.6	5.5	7.5	5.3	5	5.3	46.2	10.6	9	·	·	10	·	8	·	5	13	14	10	1	9	4	·
III	1.5	5.0	·	·	·	·	·	·	·	·	23.5	5.2	45.5	6.5	21.5	7.9	1	6.4	56.8	13.8	28	·	·	7	·	14	6	4	16	16	12	1	8	2	·
IV	3	2.8	5	4.4	17	3.7	12.5	4.4	6	3.9	8.5	4.1	19.5	4.0	13.5	3.1	5	3.6	48.2	18.1	2	·	·	1	1	1	·	7	9	6	6	2	3	·	·
V	6.5	4.7	7	3.6	0.5	7.0	2.5	3.6	6.5	4.0	13.5	5.0	28	5.0	20.5	4.6	8	4.3	155.6	36.5	29	·	·	·	·	5	2	1	11	21	17	4	·	·	4
VI	2	3.5	2.5	4.2	6	2.2	5	2.8	8	3.8	15.5	3.7	29	4.3	16	3.8	6	3.5	50.0	19.6	4	·	·	·	10	2	·	5	6	13	10	1	3	·	5
VII	1	7.5	0.5	2.0	3.5	2.3	2	3.2	7	3.4	33.5	4.0	36.5	5.3	8	6.2	1	4.5	56.5	7.9	30	·	·	·	4	6	1	2	16	18	16	·	·	·	1
VIII	2.5	3.4	0.5	4.0	2.5	3.4	3.5	4.9	9	3.7	32.5	4.6	24	4.5	8.5	3.3	10	3.8	66.4	19.4	6	·	·	·	7	5	1	4	8	17	12	2	5	·	1
IX	0.5	2.0	1.5	2.3	18.5	2.7	6.5	3.0	1.5	4.1	22	3.7	17	4.4	6	3.2	3	3.4	61.1	45.9	4	·	·	·	9	1	1	13	6	13	6	1	5	·	2
X	2	2.0	1	6.0	11.5	5.1	14.5	4.2	25.5	4.2	12	4.3	16.5	2.9	5	3.5	5	3.8	36.8	11.9	20	·	·	·	·	4	·	6	8	9	7	1	8	·	·
XI	6.5	3.8	7	3.3	8.5	5.9	3	4.8	18.5	3.2	19	4.0	13.5	4.4	6	4.2	8	3.7	53.2	22.2	13	·	·	9	·	4	2	2	20	15	8	2	9	·	·
XII	1.5	4.7	2	3.5	13.5	3.3	10.5	3.3	13.5	4.1	15.5	6.1	25.5	4.7	7	7.6	4	4.5	64.8	18.7	11	12	12	22	·	3	2	6	12	14	11	2	5	14	·
Rok	28.5	3.7	28.5	3.1	98.5	3.6	86.5	3.4	14.9	4.0	238.5	4.7	284.5	4.8	121	4.7	69	4.3	740.0	45.9	4. IX	23	23	72	31	58	17	61	139	174	125	18	60	39	13

Nowe Miasto n. P. — $H_s = 155\ m$ — $h_w = 13{,}5\ m$

I	3.5	2.6	7.5	2.3	9.5	2.5	9	2.6	15.5	2.8	21	2.1	18	2.2	9	2.7	·	2.4	28.8	7.8	31	13	10	29	·	·	·	4	16	12	5	·	1	24	·
II	2.5	2.0	·	·	3	1.8	6.5	1.9	20	2.9	18	2.6	15.5	2.7	13.5	2.7	5	2.4	27.6	8.5	1	·	·	19	·	·	·	·	16	12	6	·	3	8	·
III	4.5	8.3	·	·	·	·	·	·	0.5	3.0	20.5	4.2	40	6.0	27.5	6.6	·	5.8	27.7	5.5	21	·	·	8	·	9	6	1	15	13	9	·	2	5	·
IV	4	1.0	2.5	3.8	18.5	5.7	10.5	4.2	1	1.5	21.5	3.0	14	4.8	18	4.7	·	4.2	25.6	6.6	2	·	·	4	·	6	5	6	7	7	6	·	2	·	2
V	5	4.2	5	1.7	8	2.2	3.5	2.0	7	2.5	11	2.9	25	2.6	26.5	3.6	2	2.8	44.0	16.2	28	·	·	·	1	2	1	2	14	16	10	1	1	·	3
VI	2.5	1.6	7.5	2.3	5.5	1.7	13	3.3	6	2.4	14.5	3.4	29	2.7	12	1.9	·	2.6	61.9	21.5	27	·	·	·	12	4	·	2	6	11	11	2	2	·	10
VII	4	3.1	9.5	2.6	15.5	2.5	9	1.9	3	3.7	18	2.5	20	2.3	10	3.0	4	2.4	128.8	28.4	30	·	·	·	7	1	·	4	14	18	16	5	·	·	11
VIII	3.5	2.7	7	2.9	12	2.3	9.5	3.2	3.5	2.3	14.5	3.8	26.5	3.4	13.5	2.7	3	3.0	53.0	12.2	10	·	·	·	5	1	1	4	8	12	9	3	1	·	4
IX	9.5	1.8	4	1.8	11.5	1.9	11	2.4	4.5	1.7	10.5	2.1	21.5	2.6	17.5	2.9	·	2.3	21.8	13.2	6	·	·	1	6	·	·	16	5	7	4	1	—	·	1
X	·	·	2.5	1.0	20.5	2.5	30.5	2.7	10	1.8	9	1.4	10.5	1.7	10	1.7	·	2.1	6.3	3.6	14	·	·	·	·	·	·	5	8	4	3	·	2	·	·
XI	2	1.0	4	1.8	18	1.9	12	1.2	7	1.0	18	1.7	17	1.5	8	1.4	4	1.5	100.7	32.0	13	·	2	11	·	·	·	·	19	15	10	5	1	·	·
XII	4.5	4.1	8	3.5	3.5	1.0	7	1.0	13.5	1.3	22.5	1.6	17.5	3.4	16.5	2.5	·	2.3	22.4	10.0	10	10	13	25	·	1	1	3	15	10	6	1	·	19	·
Rok	45.5	2.7	57.5	2.0	125.5	2.2	121.5	2.2	91.5	2.2	199	2.6	254.5	3.0	182	3.0	19	2.8	548.6	32.0	13.XI	23	25	97	31	24	14	47	143	137	95	18	—	56	31

Sieradz — $H_s = 137\ m$ — $h_w = 14\ m$

I	1	1.0	1	2.0	12	3.8	10	1.9	38.5	4.4	4.5	2.0	11	4.1	·	·	15	3.1	21.6	9.8	14	12	11	26	·	4	1	—	—	6	4	·	·	18	·
II	·	·	·	·	5	1.2	3	3.7	32	3.6	6	4.0	25	4.3	1	4.0	12	3.2	33.8	12.1	9	·	·	13	·	2	1	—	—	15	9	1	5	·	·
III	·	·	·	·	·	·	1	1.0	12	5.1	12	5.1	6.7	8.0	·	·	1	7.1	24.1	7.4	29	·	·	10	·	15	2	—	—	13	8	·	2	·	·
IV	·	·	·	·	2.4	4.3	10	3.5	20	1.8	6	3.2	14	4.6	2	5.0	14	3.0	27.3	8.4	8	·	·	2	·	·	·	—	—	6	5	·	1	·	2
V	6.5	1.9	1	4.0	4	2.5	·	·	18	2.2	11	3.9	31.5	3.7	3	2.8	18	2.5	67.6	21.1	27	·	·	·	·	·	·	—	—	11	10	1	·	·	4
VI	·	·	·	·	11	2.5	6.5	2.1	2.8	1.8	6.5	3.7	2.5	4.2	1	1.0	12	2.5	53.3	23.2	8	·	·	·	10	1	·	—	—	9	8	1	·	·	7
VII	8	1.3	1	2.0	5	3.0	0.5	1.0	13.5	1.8	11	3.5	3.7	5.7	4	4.4	13	3.4	184.5	62.3	31	·	·	·	7	3	·	—	—	18	15	4	·	·	7
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	56.4	9.7	12	·	·	·	5	—	—	—	—	14	12	·	·	·	4
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	25.1	8.8	6	·	·	·	6	—	—	—	—	5	4	·	1	·	1
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	23.7	8.6	7	·	·	·	·	—	—	—	—	5	3	·	4	·	·
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	48.8	19.1	13	·	·	8	·	—	—	—	—	14	9	1	2	·	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	37.2	14.6	11	12	13	23	·	—	—	—	—	11	7	1	·	16	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	603.4	62.3	31.VII	24	24	82	28	—	—	—	—	127	94	9	15	34	25

Sabieszyn

$\varphi = 51°36'$ $\lambda = 22°10'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.0	-8.0	6.8	4	-23.6	26	-5.7	-2.8	-4.6	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.5	5.1	6.4
II	–	–	–	–	3.0	-1.0	9.8	18	-4.5	6	-0.4	2.0	0.7	0.8	5.4	6.1	5.8	5.8	9.1	8.6	8.9	8.9	0.5	1.0	0.7	0.7	8.1	8.0	7.1	7.7
III	–	–	–	–	8.5	1.2	17.8	18	-3.1	23	2.8	6.7	4.6	4.7	6.5	6.8	6.8	6.7	8.6	7.0	7.9	7.8	1.1	3.3	1.9	2.1	7.7	8.0	5.4	7.0
IV	–	–	–	–	15.2	4.4	24.3	15	-3.7	10	6.5	13.9	9.3	9.8	7.7	8.0	8.0	7.9	7.7	5.0	6.6	6.4	2.2	8.6	4.2	5.0	6.1	4.5	2.4	4.3
V	–	–	–	–	16.6	7.1	23.9	27, 29	1.4	13	9.9	15.1	11.2	11.8	10.4	10.1	10.6	10.4	8.5	6.0	7.9	7.5	2.0	7.6	3.0	4.2	7.8	7.6	6.4	7.3
VI	–	–	–	–	23.3	12.3	30.8	27	7.6	21	15.8	21.5	16.9	17.8	14.8	14.1	14.5	14.5	8.2	5.6	7.5	7.1	3.3	12.1	5.0	6.8	6.4	6.1	7.1	6.5
VII	–	–	–	–	21.9	11.5	30.3	3	7.2	6	14.5	20.1	15.5	16.4	14.1	12.7	13.7	13.5	8.5	5.5	7.8	7.3	2.6	11.6	4.2	6.1	6.3	7.7	6.4	6.8
VIII	–	–	–	–	21.5	12.4	30.1	7	7.0	31	14.4	20.1	15.8	16.5	14.4	13.9	15.0	14.4	8.7	5.9	8.2	7.6	2.3	10.4	3.4	5.4	6.6	7.7	5.9	6.7
IX	–	–	–	–	20.6	9.1	29.1	2, 3	1.1	23	10.5	19.6	13.6	14.3	11.6	11.1	12.3	11.7	8.9	4.9	7.7	7.2	1.5	12.6	3.7	5.9	5.2	4.8	2.8	4.3
X	–	–	–	–	15.6	5.6	22.9	19	0.9	24	6.6	14.8	10.2	10.4	8.4	9.1	9.1	8.9	8.6	5.5	7.3	7.1	1.5	8.0	3.5	4.3	6.1	5.3	3.8	5.1
XI	–	–	–	–	5.9	1.2	14.7	3	-7.3	23	2.4	5.0	3.4	3.6	6.9	7.5	7.3	7.2	9.2	8.4	9.1	8.9	0.7	1.5	0.8	1.0	9.0	8.9	8.2	8.7
XII	–	–	–	–	-0.9	-7.5	1.4.9	5	-22.0	26	-4.6	-2.8	-4.1	-3.9	4.4	4.7	4.4	4.5	8.4	8.2	8.5	8.4	0.7	1.0	0.7	0.8	8.3	7.7	6.9	7.6
Rok	–	–	–	–	12.5	4.0	30.8	27.VI	-23.6	26.1	6.1	11.1	7.7	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.9	5.6	6.5

Szprotawa

$\varphi = 51°34'$ $\lambda = 15°32'$

I	–	–	–	–	0.5	-7.1	7.0	3.1	-22.7	27	-4.7	-0.4	-3.5	-3.0	4.3	4.7	4.5	4.5	8.7	7.5	8.7	8.3	0.6	1.6	0.7	1.0	7.1	6.5	6.3	6.6
II	–	–	–	–	7.6	0.1	15.0	15	-5.6	6	1.9	6.4	2.8	3.5	6.4	7.3	6.7	6.8	8.9	7.7	8.9	8.5	0.8	2.4	0.9	1.4	7.9	6.5	5.5	6.6
III	–	–	–	–	11.0	2.1	20.4	10	-7.6	20	3.8	9.4	5.8	6.2	6.9	7.5	7.2	7.2	8.6	6.5	7.8	7.6	1.3	4.8	2.2	2.8	8.4	7.7	6.0	7.4
IV	–	–	–	–	17.0	5.3	25.4	7, 14	-1.3	1	8.3	15.8	10.4	11.2	9.1	9.3	9.5	9.3	8.2	5.3	7.4	7.0	2.1	9.4	3.5	5.0	6.0	5.7	4.7	5.5
V	–	–	–	–	16.0	7.2	23.4	26	2.8	18	9.5	14.1	10.2	11.0	10.4	10.3	10.7	10.5	8.7	6.6	8.6	8.0	1.6	6.3	1.9	3.3	7.8	8.8	7.6	8.1
VI	–	–	–	–	23.2	11.6	30.0	25	6.5	17	15.4	21.9	16.1	17.4	14.4	14.6	15.3	14.8	8.2	5.6	8.3	7.4	3.3	12.3	3.2	6.3	5.4	6.0	5.6	5.7
VII	–	–	–	–	21.0	11.5	33.1	3	5.7	8	14.9	19.6	15.0	16.1	13.8	13.2	13.9	13.6	8.2	5.9	8.1	7.4	3.4	10.7	3.5	5.9	7.6	8.4	7.0	7.7
VIII	–	–	–	–	21.5	11.8	31.0	6	6.3	14	14.3	19.9	15.2	16.2	14.7	15.1	15.3	15.0	8.9	6.7	8.7	8.1	1.8	9.2	2.2	4.4	6.7	7.1	4.2	6.0
IX	–	–	–	–	22.5	10.0	31.6	17	3.3	24	11.9	21.4	14.0	15.3	12.8	14.4	13.8	13.7	9.0	5.8	8.5	7.8	1.4	12.3	2.6	5.4	4.6	4.1	3.4	4.0
X	–	–	–	–	16.7	6.0	23.9	5	0.9	16	7.7	16.0	9.7	10.8	9.5	11.1	10.3	10.3	9.0	6.2	8.6	7.9	1.3	7.5	2.0	3.6	6.8	6.5	4.8	6.0
XI	–	–	–	–	6.7	1.0	12.8	2	-8.2	23	2.1	6.0	3.2	3.6	6.7	7.6	7.2	7.2	9.1	8.0	9.2	8.8	0.6	1.9	0.7	1.1	8.2	7.9	7.7	7.9
XII	–	–	–	–	1.1	-7.2	16.0	5	-23.3	26	-3.7	-0.7	-3.6	-2.9	4.8	5.1	4.7	4.9	8.5	7.7	8.5	8.2	0.9	1.5	0.9	1.1	7.3	6.3	5.9	6.5
Rok	–	–	–	–	13.7	4.4	33.1	3.VII	-23.3	26.XII	6.8	12.4	7.9	8.8	9.5	10.0	9.9	9.8	8.7	6.6	8.4	7.9	1.6	6.7	2.0	3.4	7.0	6.8	5.7	6.5

Włodawa I

$\varphi = 51°33'$ $\lambda = 23°33'$

I	–	–	–	–	-1.6	-8.8	6.2	4	-23.7	26	-6.2	-2.9	-5.3	-4.9	3.9	4.3	4.1	4.1	8.7	8.1	8.9	8.6	0.5	0.9	0.5	0.6	7.4	7.4	6.0	6.9
II	–	–	–	–	3.0	-1.1	8.8	18	-5.6	7	-0.6	2.2	0.7	0.8	5.6	6.0	5.9	5.8	9.4	8.3	9.1	8.9	0.3	1.3	0.6	0.7	8.4	8.4	8.0	8.3
III	–	–	–	–	8.4	1.3	18.0	18	-4.4	23	2.9	6.8	4.6	4.7	6.7	6.9	7.1	6.9	8.9	6.9	8.3	8.0	0.9	3.3	1.6	1.9	9.0	8.1	5.5	7.5
IV	–	–	–	–	15.9	4.1	24.7	15	-3.1	10	6.8	14.4	9.2	9.9	7.9	7.8	8.5	8.1	7.7	4.7	7.1	6.5	2.3	9.5	3.4	5.1	5.6	6.0	3.0	4.9
V	–	–	–	–	17.3	6.9	26.0	29	2.8	17	10.6	15.9	11.2	12.2	10.5	10.2	11.1	10.6	8.2	5.8	8.3	7.4	2.6	8.6	2.5	4.6	6.7	7.8	5.2	6.6
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Włodawa II

$\varphi = 51°33'$ $\lambda = 23°33'$

I	998.6	1017.8	978.0	1021.3	-2.0	-9.4	5.4	4	-24.7	26	-6.5	-3.4	-5.7	-5.3	3.9	4.3	4.1	4.1	8.8	8.3	9.1	8.7	0.4	0.8	0.3	0.5	7.4	7.5	6.1	7.0
II	1000.7	1017.0	973.6	1022.9	2.6	-1.5	8.7	18	-5.6	7	-0.7	1.8	0.5	0.5	5.5	5.9	5.9	5.8	9.4	8.5	9.1	9.0	0.3	1.1	0.6	0.7	8.4	8.5	7.9	8.3
III	993.4	1012.8	974.9	1015.2	8.0	1.1	17.7	18	-4.6	23	2.7	6.5	4.4	4.5	6.8	6.9	7.1	6.9	9.0	7.2	8.4	8.2	0.8	3.0	1.4	1.7	9.0	8.2	5.5	7.6
IV	992.6	1003.8	981.5	1013.8	15.6	3.8	24.0	15	-3.2	10	6.4	14.2	8.9	9.6	7.8	8.3	8.7	8.3	7.9	5.1	7.4	6.8	2.0	8.6	3.0	4.5	5.8	6.2	3.2	5.1
V	990.7	999.1	979.1	1011.8	16.9	6.4	25.7	28, 29	1.8	17	10.2	15.6	10.9	11.9	10.7	10.6	11.3	10.9	8.6	6.1	8.6	7.8	2.0	7.7	2.0	3.3	6.7	7.8	5.2	6.6
VI	994.3	1006.0	985.6	1015.0	24.1	11.4	32.0	27	5.4	21	16.5	22.2	16.6	18.0	15.0	15.0	15.2	15.1	7.9	5.8	8.0	7.2	4.0	12.5	3.9	6.8	4.7	6.8	5.6	5.7
VII	992.6	1004.0	978.8	1013.3	23.1	11.2	30.8	4	7.5	19	15.3	21.2	15.8	17.0	14.3	14.2	14.5	14.3	8.3	5.8	8.1	7.4	3.3	11.8	3.6	6.2	5.9	7.1	5.9	6.3
VIII	994.8	1007.3	981.8	1015.6	22.1	12.0	31.7	11	7.4	30	14.6	20.7	15.9	16.8	14.9	15.1	15.4	15.1	8.9	6.2	8.5	7.9	1.9	10.2	3.0	5.0	6.3	7.2	5.3	6.3
IX	998.2	1010.1	986.4	1019.3	20.9	7.8	29.3	3, 18	-1.7	23	10.0	19.6	13.0	13.9	12.0	13.1	13.1	12.7	9.5	5.8	8.5	7.9	0.8	10.7	2.3	4.6	4.9	4.8	3.0	4.2
X	1000.3	1010.5	979.6	1021.7	15.6	5.0	20.8	19	-0.1	23	6.3	14.8	9.4	10.0	8.8	9.5	9.4	9.2	9.0	5.8	7.9	7.6	1.0	7.6	2.5	3.7	6.1	5.7	4.3	5.4
XI	993.5	1013.2	980.7	1015.3	5.7	1.0	14.3	3	-7.3	23	2.3	4.8	2.9	3.2	7.0	7.4	7.2	7.2	9.4	8.5	9.3	9.1	0.5	1.6	0.6	0.9	9.1	9.1	6.9	8.4
XII	993.6	1020.8	975.8	1016.0	-1.4	-8.4	14.0	5	-22.1	26	-4.9	-3.2	-4.7	-4.4	4.5	4.8	4.5	4.6	9.1	8.7	9.1	9.0	0.4	0.8	0.4	0.5	8.8	7.5	7.1	7.8
Rok	995.3	1020.8	973.6	1016.8	12.6	3.4	32.0	27.VI	-24.7	26.1	6.0	11.2	7.3	8.0	9.3	9.6	9.7	9.5	8.8	6.8	8.5	8.0	1.4	6.4	2.0	3.3	6.9	7.2	5.5	6.5

Sobieszyn — H_s = 159 m — h_w = 13 m

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	☉	●	Opad R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	3	1.3	6	1.1	6	1.0	8	1.1	10	1.4	25	2.1	18.5	2.2	6.5	1.6	10	1.5	23.0	5.5	31	12	14	28	·	·	·	4	10	13	6	·	–	26	·
II	1.5	1.0	1	1.0	5.5	1.7	7	1.7	14.5	1.5	20.5	1.7	25.5	1.8	0.5	1.0	8	1.5	10.0	2.7	11	·	1	18	·	·	·	1	18	12	4	·	–	5	·
III	·	·	·	·	·	·	0.5	2.0	2.5	3.2	20	3.8	59.5	3.9	6.5	4.2	4	3.7	29.9	8.8	28	·	·	10	·	2	·	1	10	15	7	·	–	4	·
IV	3.5	1.6	6.5	2.0	15	3.1	11.5	3.7	2.5	1.4	13.5	1.6	15.5	3.9	5	1.8	17	2.2	22.9	6.1	2	·	·	1	·	·	·	7	4	6	5	·	–	·	2
V	5	1.4	2	2.0	7	1.7	7	1.7	8.5	1.4	6.5	1.2	23.5	1.8	6.5	1.7	27	1.2	57.2	9.5	14	·	·	·	·	·	·	·	12	17	12	·	–	·	5
VI	2	1.0	3.5	1.6	10.5	1.2	4	1.4	7	1.3	10	1.4	28	1.6	4	1.0	21	1.1	50.6	11.0	4	·	·	·	10	·	·	1	11	15	8	1	–	·	11
VII	4.5	1.2	0.5	1.0	·	·	2.5	1.8	7	2.3	29.5	2.2	25.5	2.0	0.5	1.0	23	1.5	55.1	14.6	30	·	·	·	8	·	·	2	8	12	10	2	–	·	7
VIII	6	1.0	1	1.0	2	1.0	·	·	4.5	1.6	27.5	2.3	24.5	2.0	5.5	1.1	22	1.4	40.1	10.1	20	·	·	·	6	2	·	1	9	14	10	1	–	·	5
IX	1	1.0	9.5	1.0	11	1.2	1.5	1.0	1	1.0	28	2.5	16.5	2.1	3.5	1.3	18	1.4	12.4	6.2	14	·	·	·	7	·	·	12	5	6	4	·	–	·	·
X	1	1.0	0.5	3.0	31	2.3	14.5	3.6	10	2.4	7	1.7	11	1.7	1	1.0	17	1.9	7.7	4.1	14	·	·	·	·	·	·	8	8	3	2	·	–	·	·
XI	7	1.7	7	2.3	20	2.4	4	1.8	4.5	1.3	14.5	2.0	18	2.7	4	1.0	11	1.9	79.7	22.5	13	·	1	13	·	·	·	1	23	18	11	3	–	3	·
XII	10.5	2.1	4.5	2.6	10	1.7	6.5	1.0	3	1.0	21.5	2.6	18.5	2.6	10.5	2.4	8	2.0	28.1	6.3	11	11	16	25	·	·	·	1	17	14	8	·	–	24	·
Rok	45	1.2	42	1.6	118	1.4	67	1.7	75	1.6	223.5	2.1	284.5	2.4	54	1.6	186	1.8	416.7	22.5	13.XI	23	32	95	31	4	·	39	135	145	87	7	–	62	30

Szprotawa — H_s = 122 m — h_w = 14,5 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	☉	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	·	·	0.5	8.0	10.5	4.5	8.5	2.0	7.5	1.7	24	4.8	3	4.8	1	7.0	38	2.3	32.0	11.5	14	12	12	26	·	2	·	5	15	16	4	1	5	19	·
II	0.5	2.0	·	·	2.5	2.2	4.5	1.7	5	2.3	26	4.1	13	3.9	5.5	3.5	27	2.4	30.3	8.4	9	·	·	15	·	1	·	4	13	13	7	·	10	4	·
III	·	·	·	·	·	·	·	·	0.5	4.0	30	4.9	27.5	5.8	14	4.5	21	4.0	41.9	8.8	28	·	·	9	·	6	1	2	18	14	12	·	11	1	·
IV	1.5	3.0	6	2.5	18	2.8	15	3.3	3	2.0	16	2.9	4	3.1	4.5	2.6	22	2.2	41.0	12.9	2	·	·	1	2	·	·	6	10	6	6	1	4	·	1
V	3	1.8	3.5	3.1	·	·	3.5	2.9	3.5	1.4	24	4.1	10	3.5	9.5	2.2	36	2.0	110.6	29.3	29	·	·	·	·	2	·	1	17	23	18	2	·	·	8
VI	·	·	·	·	6	2.2	5	1.5	2	1.0	19.5	3.3	14.5	3.5	7	3.0	36	1.8	97.1	25.9	10	·	·	·	11	1	·	3	7	15	10	3	5	·	6
VII	·	·	·	·	2	1.5	1	2.0	1.5	2.0	40	3.5	21	3.4	1.5	2.0	26	2.4	74.8	16.6	30	·	·	·	4	·	·	2	19	20	13	2	·	·	2
VIII	·	·	·	·	2.5	1.0	2.5	1.8	9	1.9	23.5	2.4	17	2.3	0.5	2.0	38	1.3	60.5	15.6	6	·	·	·	7	·	·	4	9	19	12	2	2	·	2
IX	·	·	3	1.8	13	3.0	3	1.8	6	2.8	13.5	2.4	11.5	2.3	1	2.0	39	1.4	21.1	7.7	4	·	·	·	9	·	·	11	6	11	4	·	3	·	2
X	·	·	·	·	11.5	4.7	12.5	3.4	7	2.4	17	3.2	1.5	3.0	3.5	1.9	40	1.9	39.9	14.8	20	·	·	·	·	·	·	5	11	9	8	1	2	·	·
XI	1	2.0	7.5	4.6	7.5	5.1	1	1.5	5.5	2.3	22	3.9	5.5	3.2	3	2.7	37	2.2	35.8	13.5	13	·	·	9	·	2	·	2	20	15	6	1	8	·	·
XII	0.5	4.0	3.5	2.5	8	3.0	5.5	2.1	4	2.8	25	4.8	11	4.0	5.5	4.0	30	2.6	54.7	18.6	11	12	12	23	·	2	2	5	14	16	9	1	6	17	·
Rok	6.5	1.1	24	1.9	81.5	2.5	62	2.0	54.5	2.2	280.5	3.7	139.5	3.6	56.5	3.1	390	2.2	639.7	29.3	29.V	24	24	83	33	16	3	50	159	177	109	14	56	41	21

Włodawa I — H_s = 174 m — h_w = 13 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	☉	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	7	3.3	3	2.7	3.5	1.6	22	2.5	11.5	2.7	18	3.5	10.5	4.4	13.5	3.9	4	3.0	21.0	8.6	31	13	15	28	·	2	·	2	15	15	5	·	–	31	–
II	2.5	1.2	3.5	1.7	3	1.7	15.5	2.5	12	2.7	16	2.2	18	3.0	12.5	2.4	1	2.4	5.7	1.4	1	·	3	16	·	·	·	1	20	12	3	·	–	8	–
III	·	·	·	·	·	·	1	8.0	2.5	3.0	16	4.7	41.5	5.3	31	5.4	1	5.1	19.9	4.0	21	·	·	7	·	1	·	·	13	17	7	·	–	1	–
IV	5	1.8	8	2.6	13.5	3.5	18	3.6	5.5	2.4	13	3.3	6	5.3	15	2.9	6	3.0	26.0	6.0	2, 16	·	·	5	·	2	·	6	5	6	6	·	–	·	–
V	8	2.0	1	1.0	8	1.8	11	2.7	9	1.8	9	2.2	17	2.9	17	2.3	13	2.0	65.1	26.0	4	·		·	3	·	·	1	9	16	9	1	–	·	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Włodawa II — H_s = 175 m — H_b = 175,9 m — h_w = 13 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	☉	●	R > 0.1	R > 1.0	R > 10.0	≡	⊞	R
I	6	4.3	3	2.3	3.5	1.9	18.5	2.5	13.5	2.8	21.5	4.4	12.5	5.4	11.5	4.5	3	3.6	19.0	6.6	31	13	16	30	·	2		2	14	14	6	·	3	31	·
II	3.5	1.0	2.5	1.0	2.5	2.4	12.5	3.1	10.5	3.6	18.5	3.1	21	3.4	12	2.8	1	3.0	5.4	1.4	1	·	4	19	·	·		1	20	13	2	·	6	7	·
III	1	1.0	·	·	·	·	·	·	2	4.2	18	5.0	41.5	6.1	29.5	6.6	1	5.9	17.9	3.5	21	·	·	9	·	9	·		13	17	7	·	1	1	·
IV	6	1.2	8	2.8	13.5	3.9	14.5	4.8	6.5	2.5	12	3.7	9	5.4	13.5	2.9	7	3.3	25.2	6.3	8	·	·	6	·	4	·	5	6	6	6	·	1	·	2
V	6	2.0	1	1.0	8	2.2	10.5	3.0	10	2.2	9	3.2	16.5	3.6	21	2.6	11	2.4	49.7	10.4	4	·	·	·	2	·	·	1	9	16	9	1	1	·	3
VI	1	1.0	9.5	2.4	10.5	2.1	5.5	3.6	7	3.1	12.5	2.1	22	3.3	12	3.0	10	2.5	40.4	5.8	27	·	·	·	9	·	·	2	7	13	10	·	·	·	9
VII	4	2.2	1	1.0	1	1.0	3.5	3.3	12	3.5	10.5	3.4	39	3.5	12	3.4	10	3.0	73.5	33.8	30	·	·	·	9	1	1	3	9	12	8	3	·	·	5
VIII	5	2.4	·	·	3	1.3		·	8	2.3	21	4.0	24.5	4.1	15.5	3.2	16	3.0	54.2	13.6	9	·	·	·	7	·	·	2	10	16	7	2	·		3
IX	5.5	1.6	6	1.8	9.5	2.1	5.5	2.4	4	2.0	12.5	3.6	31	4.4	5	3.5	11	2.9	11.3	5.9	14	·	·	3	7	·	·	11	4	8	3	·	4	·	·
X	0.5	5.0	4.5	3.6	18	4.0	32.5	4.5	11	3.2	4.5	3.2	8.5	4.2	5.5	2.5	8	3.7	5.5	2.4	14	·	·	1	·		·	7	7	5	2	·	5	·	·
XI	1.5	4.7	3	4.3	12.5	5.6	19	4.0	7.5	2.1	14.5	3.2	19	4.8	6	4.7	7	3.8	55.9	13.3	12	·	2	14	·	·		1	20	17	10	2	5	2	·
XII	10.5	4.0	4	3.2	6.5	3.0	12.5	2.8	8.5	3.4	13	5.3	18.5	4.8	17.5	4.7	2	4.0	38.1	10.1	7	12	17	27	·	1		1	14	19	8	1	3	25	·
Rok	50.5	2.5	42.5	2.0	88.5	2.5	134.5	2.8	100.5	2.9	167.5	3.7	263	4.4	161	3.7	87	3.4	396.1	33.8	30.VII	25	39	109	34	17	1	36	133	156	78	9	29	66	22

Wińsko — φ = 51°28' — λ = 16°37' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	−6.2	7.6	4	−20.1	26, 27	−4.4	−1.0	−3.0	−2.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.5	5.8	5.8
II	–	–	–	–	6.8	0.6	13.7	18	−4.9	6	1.6	5.4	3.4	3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.3	5.6	6.2
III	–	–	–	–	10.2	2.0	19.7	10	−5.2	20	3.8	8.4	6.1	6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.3	5.2	6.5
IV	–	–	–	–	16.4	5.6	25.3	7	−1.9	1	8.2	15.1	11.1	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.6	5.2	5.1
V	–	–	–	–	15.6	7.2	23.3	26	2.6	12	9.6	13.5	11.1	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	6.9	7.3
VI	–	–	–	–	22.9	12.2	28.2	25	7.4	16	15.2	21.1	17.6	17.9	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.4	3.7	4.4
VII	–	–	–	–	20.5	11.9	32.0	3	7.4	6	14.5	18.5	15.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.5	6.3	6.9
VIII	–	–	–	–	21.5	12.5	30.9	6	8.1	17	14.6	19.5	16.6	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.9	5.2	6.1
IX	–	–	–	–	21.8	11.3	29.9	2, 3	3.4	23	12.8	20.6	15.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.3	3.6	4.2
X	–	–	–	–	15.9	7.5	21.8	6	4.3	23	8.8	14.7	10.7	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	4.1	5.5
XI	–	–	–	–	6.6	1.5	13.6	2	−3.7	21	2.8	5.6	3.7	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	6.5	7.6
XII	–	–	–	–	0.4	−6.9	15.9	5	−20.3	17, 26	−3.6	−1.4	−3.6	−3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.0	4.8	6.0
Rok	–	–	–	–	13.2	4.9	32.0	3.VII	−20.3	17,26.XII	7.0	11.7	8.8	9.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	5.2	6.0

Grabownica — φ = 51°28' — λ = 17°27'

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.5	4.2	25.1	7	−3.2	10	8.1	15.1	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.5	3.9	4.4
V	–	–	–	–	16.1	6.1	22.5	26	2.0	12	10.1	14.3	10.4	11.3	11.0	10.9	11.1	11.0	89	68	88	82	15	5.8	1.6	3.0	7.0	6.5	5.3	6.3
VI	–	–	–	–	–	10.6	–	–	4.3	22	16.5	21.6	16.1	17.6	15.7	15.7	15.4	15.6	83	62	84	76	3.4	10.2	2.9	5.5	3.6	4.1	4.4	4.0
VII	–	–	–	–	20.6	10.9	32.0	3	6.6	8	14.6	19.3	14.4	15.7	14.2	14.8	14.1	14.4	85	67	86	79	2.7	8.4	2.6	4.6	5.8	6.1	6.2	6.0
VIII	–	–	–	–	21.3	11.5	31.2	6	6.5	14	14.8	19.9	15.3	16.3	15.2	15.6	15.4	15.4	89	67	88	81	1.8	8.2	2.3	4.1	5.1	6.1	5.4	5.5
IX	–	–	–	–	21.5	9.2	29.8	2	−0.5	24	11.8	20.3	13.3	14.7	12.7	14.0	13.4	13.4	90	59	87	79	1.7	10.7	2.2	4.9	3.5	3.8	3.0	3.4
X	–	–	–	–	15.7	6.3	21.7	6	1.0	22	8.3	14.9	9.4	10.5	10.2	11.8	10.7	10.9	91	71	91	84	1.0	5.5	1.1	2.5	6.5	5.5	4.0	5.3
XI	–	–	–	–	6.7	1.2	12.8	2	−6.9	23	2.6	5.9	3.1	3.7	7.1	8.0	7.5	7.5	94	85	95	91	0.5	1.4	0.4	0.8	8.0	7.8	7.3	7.7
XII	–	–	–	–	0.1	−8.6	16.9	5	−25.0	26	−4.9	−1.4	−4.0	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.0	5.0	5.7
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Osiny — φ = 51°28' — λ = 22°04'

I	–	–	–	–	−1.1	−7.9	6.8	4	−28.3	26	−5.6	−2.5	−4.8	−4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.5	5.5	6.5
II	–	–	–	–	3.2	−0.8	10.9	18	−5.1	6	0.0	2.3	0.9	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.1	7.4	8.0
III	–	–	–	–	9.1	1.7	18.2	18	−2.5	23	3.3	7.2	4.7	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.0	6.2	7.5
IV	–	–	–	–	15.8	4.1	24.6	15	−3.5	10	7.5	14.1	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.2	4.1	5.0
V	–	–	–	–	16.9	6.6	25.4	29	1.0	15	10.3	15.2	11.2	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.7	6.3	6.9
VI	–	–	–	–	23.6	11.8	30.9	27	5.3	21	16.3	21.9	16.5	17.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.5	7.3	6.5
VII	–	–	–	–	22.2	10.8	30.7	3	6.1	6	15.1	20.3	15.0	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	7.3	7.2
VIII	–	–	–	–	22.3	12.1	31.3	11	5.7	30	14.6	20.7	15.7	16.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	6.9	7.0
IX	–	–	–	–	20.9	9.0	29.9	3	1.1	22	11.5	19.6	13.6	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.9	3.9	4.7
X	–	–	–	–	16.0	5.9	23.4	19	2.1	14, 24	7.4	15.0	10.2	10.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.5	4.0	5.2
XI	–	–	–	–	6.6	1.5	15.0	3	−6.4	23	3.0	5.6	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.8	8.4	8.9
XII	–	–	–	–	−0.6	−7.0	14.9	5	−22.5	25	−4.6	−2.6	−3.9	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.9	7.8	8.2
Rok	–	–	–	–	12.9	4.0	31.3	11.VIII	−22.5	25.XII	6.6	11.4	7.6	8.3	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.3	6.8

Nowa Wieś — φ = 51°27' — λ = 22°45'

I	–	–	–	–	−1.5	−8.4	5.9	4	−22.9	26	−5.7	−2.8	−5.3	−4.8	4.0	4.4	4.1	4.2	87	83	89	86	0.5	0.9	0.4	0.6	7.5	6.8	5.1	6.5
II	–	–	–	–	2.8	−1.1	9.1	18	−5.3	7	−0.2	2.0	0.8	0.8	5.6	6.1	5.8	5.8	91	86	90	89	0.5	1.1	0.7	0.8	8.4	8.5	7.8	8.2
III	–	–	–	–	8.2	1.6	17.9	18	−2.6	23	3.1	6.6	4.6	4.7	6.5	6.8	6.9	6.7	85	70	80	78	1.2	3.2	1.8	2.1	8.9	8.0	5.6	7.5
IV	–	–	–	–	15.5	3.5	23.9	15	−3.8	10	6.9	14.1	8.9	9.7	7.6	7.8	8.0	7.8	74	48	68	63	2.7	9.0	3.8	5.2	5.6	5.2	2.3	4.4
V	–	–	–	–	16.8	6.3	25.6	29	1.8	13	10.1	15.0	10.7	11.6	10.5	10.1	10.7	10.4	84	61	83	76	2.1	7.7	2.4	4.1	7.1	8.5	5.9	7.2
VI	–	–	–	–	23.5	11.5	31.0	27	4.5	21	16.3	22.0	15.8	17.5	14.8	14.7	14.6	14.7	80	57	81	73	3.9	12.3	3.6	6.6	5.4	6.9	5.8	6.0
VII	–	–	–	–	22.1	11.0	30.2	3	7.2	9, 20	15.0	20.4	15.6	16.6	14.1	13.6	13.9	13.9	83	58	79	73	3.2	10.9	4.2	6.1	5.4	7.8	6.9	6.7
VIII	–	–	–	–	21.9	11.7	31.7	11	5.9	30	14.6	20.6	15.4	16.5	14.4	14.1	14.6	14.4	86	58	83	76	2.5	11.0	3.3	5.6	6.4	6.9	6.0	6.4
IX	–	–	–	–	20.6	8.7	28.8	3	−0.5	23	11.0	19.6	13.0	14.2	11.6	11.2	12.0	11.6	86	50	78	71	1.9	12.6	3.6	6.0	5.0	4.7	2.9	4.2
X	–	–	–	–	15.7	4.9	22.4	19	−0.3	24	6.6	15.2	9.9	10.4	8.5	8.9	9.2	8.9	86	53	74	71	1.4	8.6	3.2	4.4	6.4	5.6	4.1	5.3
XI	–	–	–	–	6.1	1.5	14.2	3	−6.8	23	2.9	5.3	3.6	3.8	7.0	7.4	7.4	7.3	90	82	89	87	0.8	1.8	0.8	1.1	9.4	9.1	8.4	9.0
XII	–	–	–	–	−0.9	−7.1	14.5	5	−20.6	26	−4.5	−2.8	−4.3	−4.0	4.2	4.5	4.3	4.3	80	78	83	80	0.9	1.2	0.8	1.0	8.3	8.0	6.9	7.7
Rok	–	–	–	–	12.6	3.7	31.7	11.VIII	−22.9	26. I	6.3	11.3	7.4	8.1	9.1	9.1	9.3	9.2	84	65	81	77	1.8	6.7	2.4	3.6	7.0	7.2	5.6	6.6

Wirsko

$H_s = 180\ m$ $h_w = 14\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T			Wiatr v				Opad R				
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max≥25°	≥10	≥15	●	●	≥0.1	≥1.0	≥10.0	■	▦	R R
I	1	1.0	5.5	2.5	20.5	2.8	9	3.4	21.5	4.8	13.5	3.8	18	3.1	2	4.0	2	3.4	40.3	11.8	31	11	12	22	-	2	-	7	12	12	7	1	1	18	-
II	4.5	1.4	1	5.0	6	2.2	9	3.2	15	3.3	14	3.3	24	4.5	10.5	4.2	-	3.6	24.7	8.1	9	-	-	9	-	2	1	6	12	15	8	-	7	3	
III	1	1.0	-	-	-	-	-	-	-	-	6	5.2	6.3	6.7	2.3	4.3	-	5.9	24.0	5.6	14	-	-	9	-	11	2	2	11	13	10	-	4	-	-
IV	8	1.6	17.5	2.2	16.5	2.2	7	4.2	8	2.9	6	2.7	15.5	3.5	10.5	3.3	1	2.7	77.8	28.6	15	-	-	2	1	1	-	8	9	12	10	1	3	-	5
V	11.5	2.3	2	2.0	4	1.8	1.5	2.7	4	1.9	3.5	1.6	27.5	3.9	3.3	3.3	6	2.9	84.7	14.3	29	-	-	-	-	1	-	1	14	21	14	1	1	-	4
VI	7	1.5	8	1.8	3	2.3	6.5	2.1	5.5	2.8	5	2.4	2.9	3.3	2.2	2.9	4	2.6	80.7	25.4	22	-	-	-	8	1	-	5	2	15	11	2	3	-	7
VII	1	1.0	4	1.0	-	-	2	2.0	4	1.2	7	2.3	5.7	3.7	1.6	3.6	2	3.2	88.7	16.1	13	-	-	-	6	-	-	2	11	22	14	2	-	-	3
VIII	6	1.7	3	1.0	4	2.2	2	1.0	3	2.7	9.5	1.8	4.7	3.5	16.5	2.7	2	2.8	48.5	27.5	11	-	-	-	7	1	-	4	8	14	10	1	2	-	2
IX	3.5	1.6	14.5	2.2	12.5	2.6	3	2.8	12	2.4	10	2.7	20	4.0	14.5	3.6	-	3.0	22.2	5.9	14	-	-	-	8	1	-	10	8	8	5	-	2	-	3
X	5	1.7	6	1.7	17	3.6	9.5	3.6	16.5	4.2	13	2.7	5.5	3.3	16.5	2.9	4	3.1	33.7	11.2	20	-	-	-	-	-	-	6	9	12	7	1	4	-	1
XI	8.5	3.0	5	1.6	5	3.8	10	2.8	2	2.0	12	2.8	25.5	3.5	13	3.0	9	2.7	39.5	13.1	13	-	-	12	-	1	1	3	18	11	11	1	12	-	-
XII	3	2.7	8	1.6	11.5	1.9	7.5	2.9	9.5	3.0	13.5	4.3	20.5	4.7	17.5	3.2	2	3.3	43.3	14.4	11	11	13	23	-	1	✓	6	10	10	8	1	7	16	-
Rok	6.0	1.7	74.5	1.9	100	2.1	67	2.6	101	2.6	113	3.0	352.5	4.0	195	3.4	32	3.3	608.1	28.6	15.IV	22	25	77	30	22	4	60	124	165	115	11	46	37	25

Grabownica

$H_s = 119\ m$ $h_w = 12\ m$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.6	9.1	1	-	-	4	1	–	–	9	7	12	9	-	-	-	5
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	66.4	18.2	29	-	-	-	-	–	–	3	9	20	16	1	-	-	5
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.7	12.2	12	-	-	-	–	–	–	9	6	14	12	1	-	-	8
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	125.1	41.2	31	-	-	-	5	–	–	3	8	19	15	4	-	-	2
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	71.8	28.5	10	-	-	-	4	–	–	5	11	16	11	2	-	-	4
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25.5	13.5	26	-	-	1	7	–	–	14	4	6	5	1	7	-	2
X	1	2.0	-	-	5	4.6	7	4.9	1.9	3.0	11	2.4	5	1.0	3	2.0	4.2	1.6	34.6	12.7	19	-	-	-	-	1	-	8	6	7	7	1	4	-	-
XI	7.5	1.8	6.5	5.4	2	5.0	3	2.5	4.5	2.7	9.5	2.8	12	1.8	8	2.4	3.7	1.6	85.6	30.2	14	-	-	10	-	-	-	4	2.0	13	12	3	–	-	-
XII	6	2.2	5.5	2.5	2.5	2.8	4	2.4	7.5	2.5	14.5	3.9	16	2.4	13	3.6	2.4	2.2	46.9	15.2	11	13	14	23	-	-	-	10	13	10	8	2	3	–	-
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	41.2	31.VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Osiny

$H_s = 153\ m$ $h_w = 13\ m$

I	4.5	1.9	5	2.8	2.5	2.4	17.5	2.9	16	5.1	19	4.3	13.5	4.6	7	2.1	8	3.4	23.4	5.1	31	12	13	27	-	2		3	13	13	7		1	16	-
II	4	2.1	0.5	1.0	2	3.5	14.5	3.8	19.5	4.2	14.5	4.0	18.5	4.1	1.5	2.7	9	3.5	14.8	6.4	11	-	1	17	-	1		2	19	12	5	-	10	-	
III	-	-	-	-	-	-	0.5	4.0	5.5	5.6	12.5	6.1	6.0	6.3	12.5	7.0	2	6.2	21.5	4.2	21	-	-	11	-	9	1	-	13	18	8	-	4	-	1
IV	4.5	3.8	9	4.0	12.5	5.6	20	5.2	7.5	4.9	10	4.3	16	5.2	6.5	3.4	4	4.6	24.2	8.0	8	-	-	3	-	1	-	6	6	6	5	-	1	-	1
V	4	3.8	5	3.8	8.5	2.1	13	3.0	11	3.2	9	3.6	21.5	3.8	14	3.6	7	3.1	55.1	19.5	3	-	-	-	1	-	-	-	12	17	12	1	1	-	5
VI	-	-	4.5	3.3	8.5	3.3	14	3.5	9	3.3	11	4.8	23.5	3.6	6.5	4.3	13	3.2	88.3	26.8	4	-	-	-	8	-	-	1	10	14	10	3	1	-	10
VII	5	1.8	2	1.5	1.5	2.0	2.5	1.8	11.5	4.7	23	4.3	32.5	4.0	7	4.0	8	3.6	64.4	19.7	30	-	-	-	8	-	-	3	13	14	10	2	-	-	5
VIII	3	2.3	2	2.0	2	2.0	2	3.2	15.5	3.8	14	3.6	32.5	4.5	15	3.7	7	3.6	52.5	20.1	9	-	-	-	7	-	-	1	10	12	9	2	1	-	6
IX	3	2.0	4	1.8	1.5	2.1	9.5	2.4	9	3.2	13.5	4.4	21	5.2	8	3.6	7	3.3	18.4	8.8	14	-	-	-	7	1	-	11	8	7	5	-	2	-	
X	0.5	3.0	4	2.2	18.5	4.8	34.5	5.0	11	4.5	5	2.9	7	3.4	8.5	2.6	4	4.1	6.5	3.8	14	-	-	-	-	-	-	7	7	12	2	-	5	-	
XI	7	4.2	5.5	4.1	11	3.9	20	3.7	7	3.4	10	4.4	15.5	4.6	7	3.4	7	3.7	63.6	20.1	13	-	1	11	-	-	-	1	23	16	10	2	7	-	
XII	6	4.9	4.5	4.0	-	-	10.5	3.0	14	3.4	16.5	4.8	18.5	3.9	18	3.7	5	3.7	34.0	10.2	11	10	17	24	-	2		-	21	13	8	1	6	23	
Rok	41.5	2.5	46	2.5	82	2.6	158.5	3.5	136.5	4.1	158	4.3	280	4.4	111.5	3.7	81	3.8	466.7	26.8	4.VI	22	32	93	31	16	1	35	155	144	91	11	39	39	28

Nowa Wieś

$H_s = 179\ m$ $h_w = 16\ m$

I	4.5	3.3	3	2.7	2	3.0	16.5	2.0	15.5	2.6	21	3.2	15	3.9	7.5	3.2	8	2.7	19.4	6.0	3.1	12	13	28	-	-		4	10	11	5	-	1	25	-
II	4	1.8	-	-	4	1.8	10	2.2	17	2.6	14.5	2.4	20.5	2.5	9	2.3	5	2.2	4.8	1.5	1.1	-	1	17	-	-	-	-	2.0	9	3	-	6	4	-
III	-	-	-	-	-	-	-	-	3	4.2	21.5	3.4	55.5	4.6	9	5.7	4	4.2	23.1	2.9	2.1	-	-	8	-	2	-	1	13	15	10	-	1	1	2
IV	2	1.5	5.5	3.8	17	4.4	16	3.5	4	2.8	14.5	2.6	12.5	4.0	5.5	4.0	13	3.1	25.3	7.3	8	-	-	5	-	-	-	7	4	6	6	-	1	-	2
V	4.5	3.0	1.5	2.3	7.5	2.4	8	2.3	6.5	2.2	13	1.8	20.5	3.2	10.5	2.7	21	2.0	51.2	16.3	3.0	-	-	-	2	-	-	1	10	16	14	1	1	-	2
VI	-	-	1	5.0	13	2.5	10	1.6	9	2.7	15	2.0	25	3.0	7	2.2	10	2.2	67.8	15.5	4	-	-	-	8	-	-	1	8	15	12	2	-	-	9
VII	3	2.0	0.5	1.0	-	-	4	1.5	8.5	2.5	20	2.7	33.5	2.4	6.5	2.2	17	2.0	47.6	11.7	2.9	-	-	-	7	-	-	2	10	16	9	3	-	-	3
VIII	1	2.0	1	3.0	2	1.5	5	1.8	2.5	2.6	2.4	2.9	31.5	3.1	11	3.0	10	2.5	38.7	7.2	9	-	-	-	6	-	-	1	10	13	8	-	1	-	2
IX	1.5	1.7	3	2.2	13	2.3	12	2.0	6.5	2.2	17	2.4	21	3.6	3	2.7	13	2.2	14.3	6.7	1.4	-	-	1	7	-	-	12	5	8	4	-	1	-	-
X	1	2.0	1	3.5	2.5	3.8	2.8	3.5	1.2	3.0	5.5	1.8	7.5	3.3	6	2.5	7	3.1	2.8	1.4	2.9	-	-	2	-	-	-	7	9	3	2	-	5	-	-
XI	5	3.1	1	3.5	15.5	4.4	16	3.2	6.5	1.9	16.5	3.3	12.5	3.8	6	3.5	11	3.0	53.6	16.0	13	-	1	12	-	-	-	1	24	17	10	2	4	-	-
XII	13.5	3.6	2.5	2.8	6	3.7	12	1.8	7	3.1	14.5	3.6	18	3.7	11.5	5.2	8	3.2	30.4	2.8	6	10	19	25	-	1	-	2	17	15	7	-	1	24	-
Rok	4.0	2.8	2.0	2.5	10.5	2.5	13.75	2.1	10.3	2.7	19.7	2.7	27.3	3.4	9.2.5	3.3	12.7	2.7	379.0	16.3	30.V	22	34	98	30	3	-	39	140	144	90	8	22	54	20

Ostrzeszów

$\varphi = 51°26'$ $\lambda = 17°56'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.0	−6.3	10.0	4	−19.4	27	−4.5	−1.0	−3.4	−3.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.1	5.3	5.4
II	–	–	–	–	6.0	0.4	13.8	18	−4.0	6	1.2	5.0	2.7	2.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.8	6.0	6.8
III	–	–	–	–	9.8	1.8	18.8	10	−6.1	20	3.9	8.4	5.4	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.7	6.3	7.0
IV	–	–	–	–	16.7	5.8	25.7	7	−0.8	1	8.6	15.3	10.2	11.1	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.0	4.5	5.0
V	–	–	–	–	16.1	7.2	22.7	26	2.0	12	10.3	14.4	10.5	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.5	6.9	7.5
VI	–	–	–	–	23.3	12.2	29.8	27	6.5	17, 22	16.5	21.5	16.4	17.7	–	–	–	–	–	–	–	–	–	–	–	–	4.2	6.6	3.9	4.9
VII	–	–	–	–	20.9	12.0	33.1	3	7.4	8	15.3	19.2	14.9	16.1	–	–	–	–	–	–	–	–	–	–	–	–	6.9	8.1	7.1	7.4
VIII	–	–	–	–	21.5	12.3	31.9	6	7.3	14	15.1	20.0	15.6	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.0	6.1	6.5
IX	–	–	–	–	21.5	10.6	30.3	2	4.2	24	12.7	19.9	14.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.0	2.8	3.8
X	–	–	–	–	15.5	7.1	21.5	6	1.6	13	8.2	14.8	10.3	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.4	4.8	5.8
XI	–	–	–	–	6.4	1.7	12.5	2	−4.2	21, 22	2.6	5.4	3.4	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.3	6.2	7.5
XII	–	–	–	–	0.1	−7.1	15.4	5	−21.6	27	−4.3	−2.1	−4.0	−3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.2	6.2	6.7
Rok	–	–	–	–	13.2	4.8	33.1	3.VII	−21.6	27.XII	7.1	11.7	8.0	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.6	5.5	6.2

Zawałocze

$\varphi = 51°26'$ $\lambda = 23°34'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2.5	−1.8	7.3	18	−8.5	7	−0.5	2.1	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.9	7.8	7.7
III	–	–	–	–	7.4	1.1	16.9	18	−3.9	23	3.0	6.8	4.2	4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.0	3.5	24.9	15	−4.5	10	7.0	14.9	8.2	9.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.2	4.7	4.9
V	–	–	–	–	17.5	6.5	26.1	28, 29	1.5	20	10.4	15.7	10.5	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.8	7.3	7.1
VI	–	–	–	–	24.5	11.3	31.7	27	5.0	21	16.9	22.1	16.3	17.9	15.5	15.8	15.9	15.7	80	62	86	76	4.0	11.6	2.9	6.2	–	–	–	–
VII	–	–	–	–	24.1	10.8	31.2	3	6.1	17	15.4	21.7	15.8	17.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.7	6.5	6.5
VIII	–	–	–	–	22.8	11.6	33.0	1.1	5.2	31	14.8	21.1	15.9	16.9	15.4	15.8	15.7	15.6	91	65	88	81	1.7	9.7	2.6	4.7	5.7	6.0	5.6	5.8
IX	–	–	–	–	20.9	7.3	29.5	3	−2.3	23	9.7	19.1	12.1	13.2	11.6	13.5	12.9	12.7	93	62	88	81	1.1	9.6	2.1	4.3	4.7	3.7	3.0	3.8
X	–	–	–	–	15.8	4.8	21.2	20	−0.1	23	6.2	15.0	9.4	10.0	9.0	10.4	9.8	9.7	93	62	82	79	0.7	7.0	2.1	3.3	5.7	4.6	3.8	4.7
XI	–	–	–	–	6.4	0.7	14.7	3	−10.3	23	2.4	5.0	3.1	3.4	7.3	8.0	7.6	7.6	96	90	96	94	0.4	1.1	0.4	0.6	8.8	8.6	7.3	8.2
XII	–	–	–	–	−1.0	−8.4	14.2	5	−24.9	17	−5.1	−2.8	−4.7	−4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.0	7.1	7.6
Rok	–	–	–	–	–	–	33.0	11.VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Piotrków Trybunalski

$\varphi = 51°25'$ $\lambda = 19°42'$

I	–	–	–	–	−0.4	−7.1	6.1	4	−19.6	27	−5.5	−1.3	−4.1	−3.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	4.7	−0.6	11.6	18	−10.2	6	0.5	4.0	1.3	1.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8.7	2.4	18.1	10	−3.0	20	3.6	7.3	4.8	5.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.4	5.3	25.1	7, 15	−1.0	10	7.9	15.4	10.0	10.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.8	7.2	25.1	27	2.9	19	10.2	15.4	11.1	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.4	6.8	6.9
VI	–	–	–	–	23.9	12.6	32.1	27	7.1	21	16.4	22.5	17.1	18.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	7.4	5.6	6.0
VII	–	–	–	–	21.0	11.5	32.1	3	8.3	8, 20	14.5	19.6	15.3	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	6.3	7.1
VIII	–	–	–	–	21.4	11.5	31.1	6	7.5	17, 18	14.5	19.9	15.7	16.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.9	5.9	6.7
IX	–	–	–	–	20.8	9.4	29.3	2	2.3	22	11.0	19.6	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.8	6.0	20.4	6	1.7	10	7.2	14.8	10.3	10.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.1	4.7	6.0
XI	–	–	–	–	5.8	1.2	12.9	3, 7	−6.0	21, 22	2.4	5.1	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.7	6.4	7.4
XII	–	–	–	–	−0.6	−6.9	14.9	5	−24.1	26	−4.7	−2.8	−4.2	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.9	4.4	32.1	27.VI, 3.VII	−24.1	26.XII	6.5	11.6	7.9	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Radom

$\varphi = 51°25'$ $\lambda = 21°07'$

I	–	–	–	–	−0.7	−7.7	6.0	4, 5	−22.5	27	−5.8	−2.2	−4.2	−4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.2	6.6	6.7
II	–	–	–	–	4.1	−0.4	10.8	18	−6.7	5	0.4	3.1	1.5	1.6	5.9	6.9	6.5	6.4	9.2	8.9	9.5	9.2	0.5	0.9	0.4	0.6	8.9	7.5	8.1	8.2
III	–	–	–	–	9.0	2.5	18.2	18	−2.4	20	3.8	7.7	5.3	5.5	7.2	7.9	7.9	7.7	8.9	7.4	8.8	9.0	1.0	2.9	1.2	1.7	–	–	–	–
IV	–	–	–	–	15.9	5.2	24.8	15	−1.2	10	7.6	14.4	11.0	11.0	8.5	8.7	9.2	8.8	8.0	5.3	6.8	6.7	2.2	8.5	4.5	5.1	–	–	–	–
V	–	–	–	–	17.4	7.1	25.3	27	2.0	19	10.5	15.3	12.9	12.9	10.6	10.5	11.3	10.8	8.3	6.2	7.6	7.4	2.4	7.5	3.9	4.6	7.1	7.5	6.2	6.9
VI	–	–	–	–	23.7	12.7	32.3	27	6.2	21	15.7	22.5	18.9	19.0	15.3	15.0	15.2	15.2	8.5	5.6	7.0	7.0	2.8	12.4	6.8	7.3	5.8	6.1	5.7	5.9
VII	–	–	–	–	21.7	11.4	30.8	3	7.0	6	14.9	19.9	16.4	16.9	14.1	13.7	14.5	14.1	8.3	6.0	7.8	7.4	3.1	10.4	4.6	6.0	5.9	6.8	7.2	6.6
VIII	–	–	–	–	21.6	12.1	30.5	6	7.7	6	14.0	20.2	17.1	17.1	14.5	15.0	15.6	15.0	9.0	6.2	7.9	7.7	1.7	9.7	4.3	5.2	5.7	7.6	6.6	6.6
IX	–	–	–	–	21.2	9.7	29.8	2	1.3	24	10.9	19.9	15.4	15.4	11.7	13.0	13.1	12.6	8.9	5.5	7.3	7.2	1.8	11.2	4.9	6.0	–	–	–	–
X	–	–	–	–	16.3	5.9	23.0	19, 20	1.8	10	7.2	15.7	10.5	11.0	9.0	9.8	9.8	9.5	8.8	5.6	7.6	7.3	1.4	8.3	3.2	4.3	5.6	5.7	4.4	5.2
XI	–	–	–	–	6.6	1.5	14.7	3	−5.2	23	2.9	5.4	3.6	3.9	7.2	7.5	7.4	7.4	9.2	8.2	9.2	8.9	0.6	1.8	0.7	1.0	8.6	8.3	7.6	8.2
XII	–	–	–	–	−0.4	−7.1	12.0	5	−23.5	25	−4.5	−2.3	−4.2	−3.8	4.5	4.9	4.3	4.6	8.5	8.2	8.6	8.4	0.7	1.1	0.6	0.8	8.3	7.4	7.2	7.6
Rok	–	–	–	–	13.0	4.4	32.3	27.VI	−23.5	25.XII	6.5	11.6	8.7	8.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Ostrzeszów *H_s = 198 m* *h_w = 12 m* *1961*

MIESIĄC	ROZKŁAD WIATRU °D, °mD: N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R: Suma	Max	Data	LICZBA DNI (n): Temperatura T: Min < −10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v > 10	v > 15	◑	●	Opad R: R > 0.1	R > 1.0	R > 10.0	≡	⊞	ƹ
I	·	·	6	4.2	7	1.9	17.5	2.4	27	3.9	15	2.7	6.5	3.5	1	5.5	13	2.8	28.1	7.2	14	12	12	23	·		·	10	13	12	8	·	6	12	·
II	·	·		·	4.5	3.7	9.5	3.5	24	4.1	13.5	3.2	21.5	3.6	3	4.5	8	3.4	37.6	14.5	9	·	·	14	·	1	·	3	13	15	9	1	12	·	·
III	·	·		·	·	·	·	·	4.5	3.6	20.5	4.3	55.5	5.6	8.5	7.6	4	5.2	34.0	6.9	21	·	·	8	·	5	·	3	14	15	9	·	5	·?	·
IV	1.5	2.3	6	4.5	21.5	5.2	9	3.6	7.5	3.8	13.5	2.9	12	3.8	3	5.7	16	3.4	45.2	15.3	8	·	·	1	1	·		9	8	10	7	2	3	·	3
V	4.5	2.9	2.5	1.8	2	1.8	4.5	2.0	8	2.2	15	2.8	24	3.6	11.5	4.3	21	2.4	80.3	23.0	29	·	·	·	·	·	·	2	16	21	13	3	2		5
VI	2	1.0	1	3.0	6.5	2.8	7	2.4	15.5	2.4	9	2.6	28	3.6	8	3.2	13	2.5	45.5	16.2	22	·	·	·	9	·	·	4	5	11	9	1	4		4
VII	2.5	2.6	·	·	0.5	1.0	2.5	2.6	3.5	4.3	23.5	3.4	43.5	3.4	9	3.5	8	3.1	151.0	45.5	31	·	·	·	7	·	·	3	16	16	16	4	7	·	3
VIII	2.5	2.0	1.5	1.3	2	3.5	5	3.0	3	2.2	26	4.0	26	3.9	9	2.9	18	2.9	60.0	16.3	11	·	·	·	7	·	·	3	11	16	11	2	3	·	4
IX	0.5	2.0	1.5	2.7	13.5	2.7	7.5	2.9	8	2.4	21	2.8	19.5	3.8	3.5	2.9	15	2.5	26.1	15.4	26		·	·	9	·	·	14	5	7	4	1	4	·	1
X	·	·	·	·	12	4.8	19.5	3.7	13	2.4	21.5	3.1	9	3.2	7	3.4	11	3.0	31.3	11.8	18	·	·	·	·	·	·	5	9	6	5	2	9	·	·
XI	10.5	2.7	0.5	3.0	8.5	4.9	8	2.9	12	2.3	16	3.8	22	2.8	2.5	4.0	10	2.8	61.2	28.8	13		·	9	·	2	·	1	15	13	10	1	10	·	·
XII	6	2.5	9	3.4	9	2.3	13.5	2.9	9.5	2.5	16	5.0	23	3.5	4	5.5	3	3.4	42.2	13.4	11	13	14	23	·	2	·	3	13	12	8	1	5	12	·
Rok	30	1.5	28	2.0	87	2.9	103.5	2.7	135.5	3.0	210.5	3.4	290.5	3.7	70	4.4	140	3.1	642.5	45.5	31.VII	25	26	78	33	10	·	60	138	154	109	18	70	24?	20

Zawołocze *H_s = 165 m* *h_w = 12 m*

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	0.5	2.0	·	·	·	·	14	3.1	10.5	2.7	15.5	2.5	18	2.8	2.5	2.6	23	2.0	9.5	2.3	1	·	2	18	·	·	·	2	16	11	3	·	–	–	·
III		·	·	·	·	·	·	·	4.5	2.6	18	3.4	43	3.3	21.5	3.0	6	3.0	24.8	4.5	21	·	·	9	·	·	·	–	–	16	13	·	–	–	1
IV	5	2.4	6.5	2.4	17.5	3.0	13.5	3.7	5.5	2.5	11	2.3	11.5	3.4	4.5	4.6	15	2.5	44.9	22.0	16	·	·	5		1	·	5	4	6	6	1	–	·	2
V	3	2.7		·	4.5	2.6	7.5	2.6	8.5	2.8	7	3.1	24	3.0	14.5	2.9	24	2.1	53.7	20.8	30	·	·	·	3	·	·	·	14	17	8	1	–	·	4
VI	·	·	3	4.3	5	2.9	12	3.2	7.5	2.5	14	2.3	20.5	2.4	5	2.6	23	2.0	71.1	14.9	23	·	·	·	12	·	·	–	–	11	10	2	–	·	7
VII	1.5	3.0	1	2.0	1	2.0	4.5	2.7	10	2.2	25.5	3.1	26.5	3.1	5	2.9	18	2.4	78.3	36.5	30	·	·	·	12	·	·	1	9	13	12	2	–	·	3
VIII	·	·	·	·	·	·	2.5	1.0	4.5	1.4	28	3.1	23	3.0	8	2.6	27	2.0	49.1	21.5	9	·	·	·	8	·	·	1	4	12	7	2	–	·	
IX	0.5	2.0	2	2.0	4	1.9	6	1.9	3.5	2.7	15.5	3.0	14	3.7	0.5	7.0	44	1.5	15.9	4.4	14	·	·	2	7	·	·	11	1	8	5	·	–	·	·
X	0.5	2.0	2	2.5	16.5	3.3	31.5	3.4	12.5	2.9	3.5	3.1	5.5	2.2	1	2.5	20	2.5	7.4	3.1	31	·	·	1	·	·	·	8	6	5	2	·	–	·	·
XI	3	2.8	1.5	4.3	8.5	2.8	15	2.9	5.5	2.2	12.5	3.0	12.5	2.5	3.5	2.9	28	1.9	66.0	13.6	12	1	2	14	·	·	·	1	20	14	12	3	–	–	·
XII	11.5	3.3	1	4.0	2	2.5	12	2.1	6.5	3.1	15	5.4	12.5	4.7	8.5	5.9	24	3.0	–	–	–	12	18	26	·	3	·	1	15	–	–	–	–	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	36.5	30.VII	–	–	–	42	–	–	–	–	–	–	–	–	–	–

Piotrków Trybunalski *H_s = 200 m* *h_w = 16 m I–VII, 13,5 m VIII–XII*

I	20.5	2.5	4.5	2.6	8.5	2.5	6.5	3.6	18	2.9	8.5	3.0	15.5	3.0	5	3.0	6	2.6	31.0	9.8	24	13	10	25	·	·	·	–	–	12	8	·	2	17	·
II	9.5	2.5	4	2.8	8	2.6	4.5	3.0	21	2.7	7.5	3.0	17	3.1	8.5	3.3	4	2.7	44.9	9.5	1	1	1	13	·	·	·	–	–	13	12	·	3	6	·
III	6	2.5	2.5	3.2	1.5	4.0	1	3.5	1.5	4.3	10	4.0	59.5	4.2	10	4.6	1	3.1	51.4	7.9	29	·	·	6	·	·	·	–	–	16	14	·	2	·	·
IV	10.5	3.0	4	4.2	24.5	3.2	8.5	3.5	11	2.9	2.5	4.0	12	3.6	10	3.1	7	3.0	28.7	9.9	8	·	·	1	2	·	·	–	–	7	6	·	·	·	1
V	23	2.8	10	2.8	5.5	3.2	2	4.0	2.5	3.0	6	4.7	18.5	4.4	19.5	3.4	6	3.2	59.2	3.8	3	·	·	·	1	·	·	·	10	16	14	·	·	·	4
VI	15.5	2.4	10	2.6	7	2.8	2.5	3.8	4.5	3.0	9	4.5	13	3.8	15.5	3.7	13	2.8	44.8	18.8	27	·	·	·	12	·	·	2	6	11	10	1	·	·	4
VII	7	2.6	1	2.0	4.5	2.7	4	2.9	4	2.8	14	4.2	23	3.8	28.5	3.4	7	3.2	236.9	69.0	13	·	·	·	7	1	1	3	15	19	16	7	·	·	4
VIII	6	2.7	0.5	3.0	1.5	1.7	2.5	2.6	7	3.4	19	3.6	36.5	3.5	15	3.0	5	3.1	45.5	11.9	10	·	·	·	6	·	·	3	11	15	10	1	·	·	3
IX	6.5	1.2	3	2.3	11.5	2.7	8.5	3.2	5	3.0	13.5	3.2	23	4.2	11	3.3	8	2.9	11.4	2.9	26	·	·	·	7	·	·	–	–	7	5	·	–	·	1
X	0.5	2.0	4.5	2.9	19.5	3.8	15.5	6.2	12.5	3.6	13	3.8	10	2.4	12.5	3.1	5	3.6	6.3	1.6	14	·	·	·	·	3	·	2	8	6	4	·	–	·	·
XI	10	3.2	7.5	3.4	7	4.1	4.5	3.2	6.5	3.3	21	2.8	22	2.8	11.5	2.9	·	3.1	60.8	18.0	13	·	·	9	·	·	·	3	18	15	15	1	18	·	·
XII	10.5	3.4	7	4.6	2	4.0	3	2.0	10.5	2.8	20	4.2	13	3.5	18	2.7	9	3.1	41.4	18.0	11	11	15	24	·	·	·	–	–	9	9	1	8	–	·
Rok	125.5	2.6	58.5	3.0	101	3.1	63	3.5	104	3.1	144	3.8	263	3.5	165	3.3	71	3.0	662.3	69.0	13.VII	25	26	78	35	4	1	–	–	146	123	11	–	–	17?

Radom *H_s = 178 m* *h_w = 13 m*

I	8	4.6	·	·	1	4.0	24	2.6	26	3.2	10	3.4	22	3.5	2	4.0	·	3.3	27.4	7.3	5	12	14	27	·	·	·	2	12	9	6	·	–	19	–
II	2	3.0	·	·	·	·	15	2.7	24	3.2	15	2.9	24	3.2	3	2.7	1	3.0	16.7	4.4	9	·	1	14	·	·	·	1	17	9	6	·	–	5	–
III	·	·	·	·	·	·	·	·	3	6.0	18	5.3	64	5.1	8	4.9	·	5.2	28.9	7.3	21	·	·	6	·	3	·	·	18	13	8	·	·	·	–
IV	6	3.2	2	2.5	25	4.2	10	4.1	7	2.0	15	3.5	16	3.4	8	4.1	1	3.6	32.6	12.0	8	·	·	2	·	·	·	4	5	6	6	1	1	·	–
V	9	3.0	3	3.3	7	3.6	13	2.7	7	3.1	14	3.4	22	3.5	18	4.0	·	3.4	30.6	7.8	8	·	·	·	·	·	·	·	8	11	8	·	·	·	–
VI	6	2.2	2	2.0	13	3.3	11	3.0	10	2.5	13	2.5	27	2.8	7	3.3	1	2.8	59.7	21.0	27	·	·	·	10	·	·	1	7	11	10	1	·	·	–
VII	5	3.8	·	·	3	3.0	2	2.0	10	3.0	16	2.6	47	2.3	10	3.0	·	2.6	96.3	25.0	30	·	·	·	7	·	·	2	12	13	12	3	·	·	–
VIII	8	2.8	·	·	3	2.0	1	1.0	12	2.9	18	2.8	37	2.6	14	2.9	·	2.7	35.1	12.0	20	·	·	·	7	·	·	2	9	7	6	1	1	·	–
IX	8	1.8	8	1.6	7	1.9	7	2.1	8	1.9	17	2.6	27	2.7	7	2.6	1	2.3	10.0	5.2	14	·	·		8	·	·	7	12	5	3	·	2	·	–
X	2	1.5	5	2.6	25	4.0	32	4.2	3	3.3	8.5	3.1	8.5	3.2	4	3.8	5	3.5	4.6	4.4	14	·	·	·	·	1	·	8	8	3	1	·	2	·	–
XI	5.5	3.4	4	3.9	7.5	3.5	13.5	2.3	12.5	2.0	21	3.3	14.5	3.3	9.5	3.5	2	3.0	92.6	29.4	13	·	2	9	·	1	·	2	20	19	14	3	3	·	–
XII	9.5	6.5	2.5	2.6	3	2.7	16	2.1	9	2.1	20.5	5.0	22	3.1	10.5	5.2	·	3.8	24.0	7.6	11	10	13	27	·	4	·	2	20	12	7	·	1	16	–
Rok	69	3.0	26.5	1.5	94.5	2.7	144.5	2.4	131.5	2.9	186	3.4	331	3.2	101	3.7	11	3.3	458.5	29.4	13.XI	22	30	85	32	9	·	31	148	118	87	9	–	40	–

Puławy

$\varphi = 51°25'$ $\lambda = 21°58'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnio																	
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	1001.1	1021.9	981.9	1021.0	−0.8	−7.3	8.4	4	−20.6	27	−5.1	−2.2	−4.3	−4.0	4.1	4.6	4.4	4.4	87	81	89	86	0.5	1.0	0.5	0.7	6.8	6.3	5.4	6.2
II	1003.1	1018.1	975.9	1022.6	3.5	−0.5	11.0	18	−4.9	5	−0.1	2.7	0.9	1.1	5.7	6.3	6.0	6.0	93	86	91	90	0.4	1.1	0.6	0.7	7.5	7.9	7.2	7.5
III	997.0	1016.2	976.6	1016.1	9.0	1.9	18.6	18	−2.7	23	3.3	7.4	5.1	5.2	6.9	7.1	7.2	7.1	88	70	82	80	1.0	3.5	1.7	2.1	8.0	7.6	5.5	7.0
IV	994.6	1005.5	984.4	1013.4	16.1	4.7	25.2	15	−3.1	10	7.4	14.7	9.8	10.4	7.9	8.0	8.3	8.1	75	48	67	63	2.7	9.6	4.1	5.5	5.6	4.8	2.7	4.4
V	993.1	1001.2	980.6	1011.8	17.3	7.4	26.0	27	2.2	17	10.3	15.8	11.5	12.3	10.5	9.8	10.9	10.4	83	56	80	73	2.3	8.9	3.0	4.7	6.7	7.3	5.3	6.4
VI	996.7	1009.7	987.7	1014.9	23.9	12.4	31.4	27	6.1	21	16.5	22.3	17.2	18.3	15.3	14.6	15.1	15.0	81	55	76	71	3.7	12.9	4.7	7.1	4.9	5.9	5.9	5.6
VII	995.1	1006.7	981.3	1013.4	22.2	11.3	30.6	3	8.1	6, 11	15.0	20.4	15.8	16.8	14.0	13.2	14.3	13.8	82	56	80	73	3.2	11.6	3.8	6.2	5.3	6.9	5.3	5.8
VIII	997.5	1010.4	986.9	1015.8	22.1	12.5	31.4	11	6.8	31	14.7	20.9	16.1	17.0	14.8	14.6	15.5	15.0	87	59	83	76	2.2	11.0	3.2	5.5	5.8	7.0	6.6	6.5
IX	1000.6	1011.7	988.7	1019.4	21.1	9.3	29.8	2	1.2	23	11.0	20.0	13.6	14.6	11.7	11.5	12.7	12.0	87	50	79	72	1.8	12.7	3.2	5.9	4.9	4.9	2.3	4.0
X	1001.6	1013.0	979.0	1020.5	16.2	6.5	23.7	19	3.3	29	7.4	15.2	10.4	10.8	8.7	9.6	9.5	9.3	84	57	75	72	1.8	8.0	3.3	4.4	5.7	5.5	3.5	4.9
XI	995.7	1016.7	983.3	1014.9	6.7	2.0	15.3	3	−7.2	23	3.1	5.7	4.0	4.2	7.3	7.6	7.6	7.5	92	82	91	88	0.7	1.9	0.8	1.1	8.5	8.6	8.5	8.5
XII	996.4	1023.9	977.4	1016.2	−0.3	−6.9	15.1	5	−23.3	26	−4.5	−2.4	−3.7	−3.6	4.6	4.8	4.8	4.7	89	83	90	87	0.6	1.1	0.5	0.7	8.2	7.6	7.5	7.8
Rok	997.7	1023.9	975.9	1016.6	13.1	4.4	31.4	27.VI, 11.VII	−23.3	26.XII	6.6	11.7	8.0	8.6	9.3	9.3	9.7	9.4	86	65	82	78	1.7	6.9	2.4	3.7	6.5	6.7	5.5	6.2

Sulejów

$\varphi = 51°22'$ $\lambda = 19°53'$

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	17.2	5.6	24.8	27	0.0	19	9.4	15.3	10.3	11.3	—	—	—	—	—	—	—	—	—	—	—	—	6.1	6.6	4.7	5.8
VI	—	—	—	—	23.9	10.1	32.8	27	3.5	21	15.1	21.9	16.0	17.2	—	—	—	—	—	—	—	—	—	—	—	—	4.3	6.0	5.3	5.2
VII	—	—	—	—	20.7	10.0	31.8	3	3.9	8, 9	14.3	19.5	14.6	15.8	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.9	6.3	7.1
VIII	—	—	—	—	21.3	10.9	29.7	6	6.5	30, 31	14.8	20.1	14.9	16.2	—	—	—	—	—	—	—	—	—	—	—	—	4.7	6.6	4.0	5.1
IX	—	—	—	—	20.8	7.4	28.8	3	−0.5	23, 25	10.8	19.7	13.0	14.1	—	—	—	—	—	—	—	—	—	—	—	—	3.9	3.3	2.7	3.3
X	—	—	—	—	15.8	5.5	22.2	20	1.2	22	7.3	15.2	9.1	10.2	—	—	—	—	—	—	—	—	—	—	—	—	5.8	6.0	2.7	4.8
XI	—	—	—	—	6.3	0.7	13.4	3	−6.2	23	2.3	5.1	2.9	3.3	—	—	—	—	—	—	—	—	—	—	—	—	7.8	7.9	7.5	7.7
XII	—	—	—	—	−0.4	−8.4	15.3	5	−26.4	26	−4.9	−2.5	−4.7	−4.2	—	—	—	—	—	—	—	—	—	—	—	—	7.2	7.0	5.4	6.5
Rok	—	—	—	—	—	—	32.8	27.VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Szczerców

$\varphi = 51°20'$ $\lambda = 19°07'$

I	—	—	—	—	0.0	−8.2	6.6	4	−21.7	28	−5.1	−1.1	−4.5	−3.8	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	5.5	−1.5	12.7	18	−5.9	5	0.8	4.7	1.4	2.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	9.7	—	19.0	10	—	—	3.8	8.6	5.0	5.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	17.3	4.8	25.9	7	−2.5	10	8.8	16.6	8.7	10.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	17.9	6.4	25.4	27	2.3	12	10.6	16.3	10.0	11.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	24.3	11.2	32.9	27	5.8	21	16.6	22.9	15.4	17.6	—	—	—	—	—	—	—	—	—	—	—	—	5.4	5.3	5.5	5.4
VII	—	—	—	—	21.4	10.8	33.0	3	6.9	12	15.1	20.0	14.4	16.0	—	—	—	—	—	—	—	—	—	—	—	—	7.1	7.9	6.9	7.3
VIII	—	—	—	—	22.0	11.0	31.4	6	5.1	15	14.8	20.9	15.3	16.6	—	—	—	—	—	—	—	—	—	—	—	—	6.0	6.4	5.7	6.0
IX	—	—	—	—	21.9	9.0	30.8	17	0.8	24	10.8	21.1	13.1	14.5	—	—	—	—	—	—	—	—	—	—	—	—	5.8	4.2	5.3	5.1
X	—	—	—	—	16.6	6.4	21.9	6	2.0	22	8.7	16.1	9.7	11.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	7.0	1.2	13.8	3	−7.4	23	2.9	6.0	3.3	4.0	—	—	—	—	—	—	—	—	—	—	—	—	8.4	8.3	8.2	8.3
XII	—	—	—	—	0.1	−7.7	14.8	5	−24.2	26	−3.9	−1.6	−4.0	−3.4	—	—	—	—	—	—	—	—	—	—	—	—	8.9	7.3	7.5	7.9
Rok	—	—	—	—	13.6	—	33.0	3.VII	−24.2	26.XII	7.0	12.5	7.3	8.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Oborniki Śląskie

$\varphi = 51°18'$ $\lambda = 16°35'$

I	—	—	—	—	0.7	−6.0	8.1	4	−17.5	27	−4.2	−0.5	−3.2	−2.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	6.8	−0.1	13.8	18	−6.4	6	1.0	5.6	2.6	2.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	10.9	2.5	20.0	10	−4.7	20	4.3	9.5	6.1	6.5	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	17.2	5.9	26.4	7	−1.5	1	8.2	16.1	9.9	11.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	—	—	—	—	16.5	7.0	23.5	26	2.5	16	9.3	14.6	9.8	10.9	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VI	—	—	—	—	23.5	11.8	29.3	25	6.0	16	15.0	22.1	15.7	17.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VII	—	—	—	—	21.1	11.0	33.8	3	6.3	11	14.3	19.6	14.3	15.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
VIII	—	—	—	—	21.2	11.3	31.2	6	7.1	17	13.9	19.8	14.6	15.7	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IX	—	—	—	—	21.9	10.9	30.5	17	5.5	24	12.3	20.5	14.4	15.4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
X	—	—	—	—	15.3	7.1	22.2	5, 6	1.3	22	8.1	14.7	9.9	10.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XI	—	—	—	—	6.3	0.8	13.4	2	−4.9	21, 22	2.0	5.1	2.6	3.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
XII	—	—	—	—	0.3	−6.7	15.3	5	−21.2	26	−3.7	−1.3	−3.7	−3.1	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Rok	—	—	—	—	13.2	4.6	33.8	3.VII	−21.2	26.XII	6.7	12.2	7.8	8.6	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Puławy $H_s = 142$ m $H_b = 155{,}2$ m $h_w = 12$ m

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v > 10	v > 15	◉	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R
I	2.5	2.0	3.5	1.4	6	1.2	6.5	1.2	19.5	1.6	10	1.8	6	1.6	17	1.6	22	1.2	24.5	7.4	31	11	13	27	·	1	·	5	13	11	7	·	2	25	·
II	2.5	1.4	0.5	2.0	6.5	1.2	9.5	1.4	15.5	1.7	4	1.2	7	1.6	12.5	1.2	26	1.0	14.7	3.4	11	·	1	18	·	·	·	3	17	13	6	·	11	7	·
III	0.5	1.0	·	·	·	·	2	1.2	3	1.5	12	2.4	35.5	2.8	29	3.6	11	2.6	23.1	5.5	21	·	·	8	·	3	1	1	10	19	6	·	2	2	1
IV	4	1.5	5	1.9	17	2.5	12.5	2.1	7.5	1.3	2.5	1.6	9	3.1	10.5	2.9	22	1.8	24.2	7.9	8	·	·	2	1	2	·	7	4	6	6	·	1	·	2
V	5.5	1.7	1.5	2.3	8.5	1.5	4	1.5	4.5	1.3	5	1.6	14	1.4	15	2.3	35	1.1	34.0	6.2	9	·	·	·	2	1	·	1	9	16	10	·	3	·	5
VI	3.5	1.1	3.5	1.1	7	1.9	10	1.4	10.5	1.4	4.5	2.1	11	1.7	13	1.8	27	1.1	68.0	18.0	3	·	·	·	10	1	·	2	7	14	9	2	·	·	10
VII	1	1.0	0.5	1.0	0.5	2.0	3	1.3	6.5	1.5	9	1.8	18.5	1.9	13	1.8	41	1.0	71.1	22.8	30	·	·	·	8	2	1	3	5	14	11	2	1	·	6
VIII	4	1.9	·	·	1	1.0	1	1.0	4	1.5	11	1.9	17.5	1.5	11.5	1.9	43	0.9	43.2	13.5	9	·	·	·	6	·	·	1	9	12	7	1	3	·	3
IX	0.5	1.0	3.5	1.0	10	1.4	6	1.4	6	1.5	7.5	1.5	15.5	1.9	9	2.3	32	1.1	11.9	7.2	14	·	·	·	8	·	·	11	5	5	2	·	4	·	·
X	1	1.5	·	·	22.5	2.0	23.5	2.9	11	2.0	2	1.0	2	1.8	12	1.4	19	1.7	5.1	2.4	29	·	·	·	·	·	·	9	7	3	2	·	8	·	·
XI	6	1.5	3	1.7	12	2.4	10	1.8	9	1.3	3	1.5	15.5	1.9	7.5	1.7	24	1.3	56.5	18.1	13	·	1	11	·	·	·	2	21	19	9	2	6	·	·
XII	10	3.0	1	1.5	5.5	1.5	7.5	1.3	9	1.3	6	2.2	14	1.7	21	2.1	19	1.5	37.7	10.8	11	10	15	23	·	·	·	2	17	14	9	1	5	25	·
Rok	41	1.6	22	1.2	96.5	1.6	95.5	1.5	106	1.5	76.5	1.7	165.5	1.9	171	2.0	321	1.4	414.0	22.8	13. VII	21	30	89	35	10	2	47	124	146	84	8	46	59	27

Sulejów $H_s = 186$ m $h_w = 14$ m

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
V	·		1	2.0	0.5	1.0	10.5	1.5	2·	1.0	11	2.1	16	2.3	11	2.6	41	1.2	25.9	4.4	9	·	·	·	·	·	·	4	7	13	9	·	·	·	4
VI	2	2.0	·	·	5	2.2	8	2.4	3	2.0	4.5	2.6	22	3.3	5.5	3.2	40	1.6	50.6	25.0	27	·	·		10	·	·	4	6	14	8	1	·	·	8
VII	2	3.0	·	·	·	·	2	2.5	6	2.7	19	3.5	34	3.5	8	2.9	22	2.5	175.2	41.9	31	·	·	·	6	·	·	3	13	16	13	7	·	·	6
VIII	2	2.5	·	·	3	3.0	·	·	8	2.9	14	4.6	32	3.9	5	3.6	29	2.6	67.5	46.2	12	·	·	·	6	·		5	5	10	8	1	·	·	3
IX	4	1.8	7	2.0	7	2.1	8	2.9	7	1.7	21	3.0	15	4.0	3	2.0	18	2.2	19.3	10.5	29	·	·	·	7	·	·	13	3	7	3	1	—	·	·
X	·	·	1	3.0	9	3.6	35	2.9	7.5	3.0	6.5	2.4	8	3.1	7	2.3	19	2.3	5.2	1.8	29	·	·	·	·	·	·	6	6	5	3	·	6	·	·
XI	6	2.1	2.5	2.4	6.5	3.4	13.5	2.0	7	2.5	16.5	3.6	12.5	3.5	5.5	3.8	20	2.3	97.4	29.2	4	·		12	·	·	·	3	20	20	13	3	—	1²	·
XII	6.5	3.5	2.5	2.6	4.5	2.3	10	1.7	12.5	2.9	11	5.7	16.5	4.0	16.5	2.4	13	2.8	30.5	13.4	11	12	15	26	·	2	·	4	13	12	8	1	—	20	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	46.2	12. VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Szczerców $H_s = 160$ m

I	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	16.5	8.1	14	12	11	25	·	—	—	—	—	8	5	·	1	4	·
II	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	47.0	13.5	1	·	·	20	·	—	—	—	—	12	10	2	7	5	·
III	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	40.0	7.8	29	·	·	—	·	—	—	—	—	14	12	·	3	2	·
IV	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	35.8	11.9	8	·	·	3	2	—	—	—	—	8	7	1	1	·	—
V	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	69.8	10.1	8	·	·	·	1	—	—	—	—	16	13	1	1	·	—
VI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	44.3	8.2	8	·	·	·	12	—	—	—	—	11	9	·	1	·	—
VII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	219.4	55.0	31	·	·	·	7	—	—	—	—	21	14	6	·	·	—
VIII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	53.3	13.0	12	·	·	·	7	—	—	—	—	13	10	2	·	·	—
IX	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	12.5	3.8	29.	·	·	·	8	—	—	—	—	5	5	·	2	·	—
X	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	8.2	3.0	29	·	·	·	·	—	—	—	—	4	4		8	·	—
XI	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	71.4	20.5	13	·	·	7	·	—	—	—	—	14	12	3	7	2	·
XII	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	48.5	15.0	11	11	13	23	·	—	—	—	—	14	8	2	1	17	·
Rok	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	666.7	55.0	31. VII	23	24	—	37	—	—	—	—	140	109	17	32	30	—

Oborniki Śląskie $H_s = 180$ m $h_w = 22$ m

I	2	2.0	3.5	1.6	3	1.7	22.5	2.1	11.5	2.5	7.5	1.7	3	3.2	9	1.4	31	1.4	30.5	11.4	14	9	12	25	·	·	·	—	—	12	9	1	2	20	·
II	5	2.2	1	5.0	4	1.8	6	2.5	6	1.3	6.5	2.3	4	1.4	9.5	2.5	42	1.1	21.7	6.9	2	·	·	14	·	·	·	—	—	7	4	·	1	2	·
III	10.5	2.8	10	3.1	2.5	2.4	1	1.0	1	2.0	4	4.2	8.5	4.6	26.5	2.8	29	2.2	44.4	16.1	29	·	·	5	·	·	·	—	—	11	7	1	·	1	·
IV	6	2.9	10	2.3	12.5	2.7	10.5	2.4	5.5	1.7	0.5	2.0	2	1.5	12	2.8	31	1.6	45.6	14.6	16	·	·	2	2	·	·	—	—	8	6	3	1	·	1
V	14	2.0	10.5	2.3	9.5	2.5	0.5	1.0	2	3.0	5	2.9	6.5	3.2	14	2.5	31	1.6	93.3	24.8	29	·	·	·	·	1	·	—	—	21	18	2	·	·	4
VI	15.5	1.5	10.5	1.6	6	2.4	7.5	2.3	4.5	2.6	1	1.0	5.5	2.5	12.5	2.5	27	1.4	50.4	24.6	10	·	·	·	11	·	·	—	—	12	8	1	·	·	7
VII	4	1.9	7.5	1.5	7	1.9	5.5	1.8	0.5	1.0	2	2.2	20.5	2.8	31	2.7	15	2.0	111.4	23.4	28	·	·	·	8	·	·	—	—	22	18	4	·	·	5
VIII	7.5	2.9	4.5	1.3	8	1.9	3.5	3.3	2	2.5	7	2.7	9.5	3.3	19	2.8	35	1.7	58.6	15.7	10	·	·	·	4	·	·	—	—	17	12	2	1	·	2
IX	9	1.6	14.5	2.4	18	2.2	13.5	2.3	2	1.8	4.5	2.0	7.5	1.9	5	2.2	16	1.7	25.2	6.9	14	·	·	·	8	·	·	—	—	8	5	·	1	·	2
X	6	2.1	9	2.8	20.5	3.1	28	2.7	25	2.4	1	2.0	2.5	2.2	11.5	1.8	12	2.3	39.9	7.8	18	·	·	·	·	·	·	—	—	9	8	·	—	·	1
XI	9	2.1	8.5	2.3	10	2.0	12.5	1.8	0.5	3.0	9	2.1	10	2.1	16.5	1.8	14	1.7	53.4	12.1	13	·	·	12	·	·	·	—	—	17	13	1	7	·	·
XII	10	2.4	15.5	2.0	8.5	2.1	·	·	2.5	1.6	8.5	2.5	3.5	2.3	24.5	2.7	20	1.8	72.3	16.4	11	11	13	24	·	·	·	—	—	17	14	2	1	16	·
Rok	98.5	2.2	102	2.4	109.5	2.2	111	1.9	40.5	2.5	56.5	2.3	83	2.6	191	2.4	303	1.7	646.7	24.8	29 V	20	25	82	33	1	·	—	—	161	122	17	—	39	22

Krasnik Dolny — φ = 51°17' — λ = 15°36' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA				ŚREDNI NIEDOSYT WILGOTNOŚCI				ŚREDNIE ZACHMURZENIE			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.3	-7.5	16.8	30	-23.1	27,28	-4.7	-0.4	-3.7	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.7	6.1	6.5
II	–	–	–	–	7.5	0.2	15.4	18	-4.1	26	2.0	6.3	2.8	3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	5.2	6.3
III	–	–	–	–	10.6	2.7	18.8	10	-3.7	20	4.2	9.2	5.8	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	7.2	7.3
IV	–	–	–	–	16.5	5.9	24.9	7	0.6	10	8.4	15.1	10.0	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	4.7	5.5
V	–	–	–	–	15.1	6.8	21.8	5	2.2	12	9.7	13.3	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.7	7.2	8.0
VI	–	–	–	–	22.6	11.0	28.7	25	5.8	16	15.3	20.6	16.0	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.7	5.1	5.4
VII	–	–	–	–	20.6	11.3	31.6	3	4.9	8	15.0	19.0	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.5	6.7	7.1
VIII	–	–	–	–	21.5	11.4	30.6	6	4.4	14	14.6	19.6	15.0	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.5	3.7	5.6
IX	–	–	–	–	22.1	9.6	31.0	17	2.4	24	12.4	20.8	14.4	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.0	4.1	4.8
X	–	–	–	–	16.2	6.3	23.7	5	0.7	16	8.1	15.3	10.1	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.4	3.9	5.2
XI	–	–	–	–	7.1	1.2	12.9	2	-6.7	23	2.4	6.1	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	6.2	7.2
XII	–	–	–	–	1.0	-7.3	16.3	5	-22.0	17	-3.7	-0.9	-4.2	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.4	5.1	6.7
Rok	–	–	–	–	13.5	4.3	31.6	3.VII	-23.1	27,28.1	7.0	12.0	7.9	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.6	5.4	6.3

Nałęczów — φ = 51°17' — λ = 22°13'

I	–	–	–	–	-0.8	-8.9	7.2	4	-24.3	27	-5.9	-2.4	-5.5	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.4	5.6	6.5
II	–	–	–	–	3.4	-4.6	10.9	18	-8.8	5	-0.5	2.4	0.4	0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.1	6.8	7.6
III	–	–	–	–	8.6	1.1	18.6	18	-3.1	23	3.0	7.0	4.4	4.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.8	5.9	7.1
IV	–	–	–	–	16.1	3.1	24.0	7	-5.2	10	7.8	14.5	7.5	9.3	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.5	4.0	4.4
V	–	–	–	–	16.9	4.9	25.4	29	-0.4	17,19	10.5	15.3	9.7	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	6.1	6.8
VI	–	–	–	–	23.5	9.8	31.5	27	4.8	17,21	15.7	21.8	14.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.0	5.1	5.5
VII	–	–	–	–	21.3	9.2	30.5	3	4.1	6	14.3	20.0	13.7	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	7.0	5.9	6.0
VIII	–	–	–	–	22.1	10.6	31.8	11	3.7	30	14.4	20.5	14.3	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.6	6.1	6.1
IX	–	–	–	–	20.9	6.2	29.2	2	-3.6	23	9.9	19.9	10.8	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.6	3.1	4.2
X	–	–	–	–	16.4	4.3	23.8	19	0.3	11,29	6.2	15.3	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.3	4.2	5.0
XI	–	–	–	–	6.9	1.2	14.7	3	-8.9	23	2.9	5.7	3.5	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.5	8.1
XII	–	–	–	–	-0.3	-8.0	14.4	5	-24.2	23,25	-5.1	-2.4	-4.6	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	7.3	7.4
Rok					12.9	2.7	31.8	11.VIII	-24.3	27.1	6.3	11.5	6.5	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	5.6	6.2

Motycz — φ = 51°15' — λ = 22°25'

I	–	–	–	–	-1.8	-8.0	6.4	4	-20.0	26	-5.6	-2.9	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2.4	-1.4	9.2	18	-6.5	5	-0.4	1.9	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8.0	1.7	17.9	18	-2.4	20	3.0	6.4	4.5	4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	15.2	4.4	23.4	15	-2.6	10	7.3	13.7	9.0	9.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.0	6.6	24.1	27	2.2	19	10.3	14.6	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.1	11.6	31.3	27	7.5	17	16.4	21.3	15.4	17.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.8	10.6	30.1	3	5.6	6	14.7	19.9	14.8	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.7	11.9	31.7	11	6.7	31	14.6	20.2	15.1	16.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.3	8.2	28.9	2	-1.8	23	10.7	19.4	12.6	13.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.5	5.2	23.1	19	1.0	11	7.2	14.8	9.8	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.1	1.3	14.0	3	-5.5	23	2.9	5.3	3.6	3.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.2	-7.8	14.3	5	-21.3	25	-4.8	-3.0	-4.2	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok					12.3	3.7	31.7	11.VIII	-21.3	25.XII	6.4	11.0	7.2	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lublin — φ = 51°14' — λ = 22°34'

I	998.9	1018.8	978.8	1021.6	-1.0	-7.9	8.1	4	-23.3	27	-5.5	-2.2	-4.9	-4.4	4.0	4.4	4.1	4.2	87	80	86	84	0.5	1.1	0.6	0.7	7.5	6.6	5.6	6.6
II	1000.9	1016.1	972.9	1023.1	3.2	-1.3	10.4	18	-8.3	5	-0.4	2.4	0.8	0.9	5.6	6.1	5.8	5.8	94	84	90	89	0.4	1.2	0.7	0.8	7.9	8.1	8.0	8.0
III	994.7	1013.4	974.7	1016.5	8.8	1.5	19.0	18	-2.7	23	3.2	6.8	4.5	4.8	7.1	7.1	7.3	7.2	92	72	86	83	0.7	3.1	1.3	1.7	8.3	8.0	6.0	7.4
IV	992.6	1003.3	982.4	1013.8	16.1	3.9	25.3	15	-4.5	10	-6.7	14.7	9.4	10.0	8.2	8.3	8.6	8.4	81	49	71	67	1.9	9.2	3.4	4.8	5.5	5.4	2.6	4.5
V	991.0	999.1	978.7	1012.1	17.1	6.1	26.0	29	0.8	17	10.1	15.3	11.4	12.0	10.9	10.4	11.3	10.9	87	62	83	77	1.7	7.7	2.5	4.0	7.2	7.9	6.6	7.2
VI	994.5	1006.8	985.5	1015.2	24.3	11.2	32.7	27	4.4	21	16.4	22.3	16.9	18.1	15.6	15.0	15.7	15.4	83	57	81	74	3.2	12.7	3.7	6.5	4.5	6.3	5.5	5.4
VII	993.2	1004.5	978.3	1014.1	22.3	10.2	30.4	3	5.3	9	14.6	20.5	15.7	16.6	14.7	14.2	15.2	14.7	88	60	85	78	2.2	10.8	3.0	5.3	5.6	7.2	6.0	6.3
VIII	995.4	1008.1	984.1	1016.3	22.6	11.4	33.3	11	4.1	31	14.4	20.9	15.6	16.6	15.4	15.5	16.0	15.6	93	63	89	82	1.3	10.4	2.2	4.6	5.7	7.0	5.5	6.1
IX	998.5	1009.7	986.9	1019.8	21.2	7.4	29.3	2,3	-2.2	23	9.9	20.2	12.1	13.6	11.7	11.9	12.7	12.1	94	51	88	78	0.9	12.6	1.8	5.1	5.3	4.6	3.4	4.4
X	999.7	1010.8	978.0	1021.2	16.4	5.3	23.5	19	0.5	24	6.5	15.6	10.2	10.6	8.9	9.8	9.9	9.5	90	57	79	75	1.1	8.3	2.7	4.0	5.5	5.7	4.3	5.2
XI	993.5	1014.2	980.7	1015.3	6.9	1.6	15.0	3	-7.3	23	3.8	5.9	3.8	4.1	7.4	7.9	7.7	7.7	95	83	92	90	0.5	1.7	0.6	0.9	8.6	8.8	8.2	8.5
XII	994.0	1021.1	975.0	1016.4	-0.5	-7.3	14.0	5	-22.4	26	-4.2	-2.3	-4.2	-3.7	4.7	5.0	4.7	4.8	91	85	92	89	0.5	1.0	0.4	0.6	7.8	7.7	7.3	7.6
Rok	995.6	1021.1	972.9	1017.2	13.1	3.5	33.3	11.VIII	-23.3	27.1	6.2	11.7	7.6	8.3	9.5	9.6	9.9	9.7	90	67	85	81	1.2	6.6	1.9	3.2	6.6	6.9	5.8	6.4

Kraśnik Dolny $H_s = 180 m$ $h_w = 10,8 m$ 1961

MIESIĄC	ROZKŁAD WIATRU °D, v°mD N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	·	·	4.5	3.3	15	3.3	1.5	1.3	6.5	2.7	20	4.9	14.5	3.8	1	5.0	30	2.6	23.1	7.4	14	12	12	26	·	1	·	6	15	11	6	·	1	16	·
II	2.5	1.8	·	·	8	1.8	2.5	4.2	2	1.2	23	3.7	25.5	3.9	3.5	6.4	17	2.8	29.9	8.9	9	·	·	11	·	4	·	5	12	14	7	·	5	3	·
III	1	12.0	·	·	·	·	·	·	1	3.0	15.5	5.6	54	6.4	7.5	4.9	14	5.2	45.1	8.2	30	·	·	6	·	7	2	3	15	16	13	·	5	1	·
IV	3.5	2.4	1.5	3.3	21.5	3.7	8	3.8	4.5	2.0	12.5	2.4	14	3.3	4.5	2.3	20	2.4	65.0	13.6	2	·	·	·	·	·	·	6	10	10	8	4	3	·	4
V	2	2.0	1	1.5	2.5	2.8	1.5	3.7	2.5	2.4	14	3.0	35.5	2.9	6	2.0	28	1.9	128.5	37.0	29	·	·	·	·	·	·	·	17	18	18	2	1	·	4
VI	1.5	1.0	1.5	2.3	5	4.0	3	3.0	3.5	1.6	10.5	4.0	24.5	3.9	4.5	2.9	36	2.1	98.6	59.7	10	·	·	·	6	·	·	4	8	12	11	1	10	·	7
VII	·	·	·	·	1.5	3.0	8.5	3.6	3	6.2	24.5	4.3	36.5	4.4	2	3.0	17	3.5	75.2	25.8	30	·	·	·	4	2	·	3	16	15	12	3		·	1
VIII	2	1.5	·	·	5.5	3.5	1.5	2.7	3	9.3	21	4.4	28.5	4.2	4.5	1.9	27	2.9	47.3	15.4	11	·	·	·	6	3	1	4	6	14	12	1	5	·	5
IX	1	3.0	2.5	2.6	16	2.7	3.5	1.3	3.5	3.0	15	3.1	16	3.6	2.5	3.4	30	2.0	32.8	13.8	5	·	·	·	9	1	1	9	10	6	5	1	3	·	3
X	2	1.0	2.5	2.6	21	4.9	5.5	2.7	7	2.0	10	3.6	9	1.6	2	1.0	34	2.1	38.9	14.5	20	·	·	·	·	1	·	4	7	8	6	1	7	·	
XI	3	1.5	4	1.5	10.5	4.2	1	1.5	2	4.0	11	4.4	25.5	3.6	6	1.7	27	2.4	24.3	8.7	13	·	·	9	·	·	·	1	16	14	6	·	5	·	·
XII	·	·	5	1.6	13.5	1.4	0.5	1.0	3.5	2.4	14	6.1	26	3.8	6.5	2.3	24	2.6	36.2	15.0	11	12	13	23	·	2	·	4	12	12	7	1	·	15	·
Rok	18.5	2.2	22.5	1.6	120	2.9	37	2.2	42	3.3	191	4.1	309.5	3.8	50.5	3.1	304	2.7	644.9	59.7	10.VI	24	25	75	25	21	4	49	144	150	111	14	45	35	24

Nałęczów $H_s = 166 m$ $h_w = 15 m$

I	1	3.0	2	4.0	2.5	1.4	18	2.3	16.5	4.4	8.5	4.2	10	4.0	12.5	3.4	22	2.6	31.7	7.2	31	11	13	26	·		·	4	12	14	10	·	·	22	·
II	2.5	1.4	0.5	1.0	6	2.6	16.5	3.5	13.5	4.3	10	2.5	17	2.9	5	2.3	13	2.6	12.4	3.1	9	·	1	20	·	·	·	2	15	9	6	·	–	5	·
III	·	·	·	·	·	·	·	·	6.5	6.5	10.5	5.3	54	5.9	15	6.4	7	5.5	41.2	9.0	28	·	·	12	·	2		1	11	15	11	·	–	·	1
IV	1.5	3.7	4	2.8	20.5	3.9	11.5	5.0	9	2.9	6.5	4.4	11	5.9	6	5.3	20	3.4	25.8	9.7	8	·	·	5	·	1	·	6	4	6	3	·	·	·	2
V	5.5	2.8	2	3.0	8	2.9	10	3.4	4	5.0	6.5	4.2	14	3.9	18	3.2	25	2.5	77.5	15.4	10	·	·	2	1	·	·	·	11	16	13	2	–	·	3
VI	·	·	2.5	2.6	8	3.0	13.5	2.8	5.5	2.5	6	2.4	14.5	3.7	13	2.7	27	2.1	137.8	45.7	4	·	·	·	9	·	·	4	5	12	10	5	–	·	9
VII	3	1.7	·	·	·	·	6	3.5	10.5	3.9	18	4.3	16.5	4.2	11	3.4	28	2.7	122.1	29.0	30	·	·	·	8	·	·	3	4	13	13	4	–	·	7
VIII	3	2.3	·	·	·	·	4.5	1.0	9	3.6	14.5	4.6	20.5	4.1	14.5	4.2	27	2.8	74.8	30.5	12	·	·	·	6	2	·	·	7	14	10	2	–	·	5
IX	·	·	3	3.8	6	2.9	1.5	3.7	8.5	3.8	16	4.5	13	5.0	6	4.4	36	2.6	14.3	6.5	14	·	·	5	7	·	·	9	4	5	4	·	–	·	·
X	·	·	3.5	3.3	23.5	4.1	26.5	4.2	5	3.2	2.5	2.8	8	3.5	4	5.5	20	3.2	7.7	6.7	14	·	·	·	·	1	·	9	6	2	1	·	–	·	·
XI	1.5	3.7	4	2.9	14.5	2.7	11.5	2.3	12	2.6	12.5	3.2	10.5	3.2	8.5	2.4	15	2.3	56.8	17.2	13	·	·	11	·	·	·	2	18	15	12	2	2	·	·
XII	6.5	2.4	3	1.5	5.5	1.6	14	1.7	10	3.3	7.5	3.9	11.5	2.7	16	3.3	19	2.1	47.5	9.3	7	11	16	25	·	·	·	3	16	16	11	·	2	25	·
Rok	24.5	1.8	24.5	2.1	94.5	2.1	133.5	2.8	110	3.8	119	3.9	200.5	4.1	129.5	3.9	259	2.9	649.6	45.7	4.VI	22	30	106	31	6	·	43	113	137	104	15	–	52	27

Motycz $H_s = 213 m$ $h_w = $ 10 m I–VIII, 14 m IX–XII

I	4.5	2.9	4.5	2.9	2	2.2	11.5	3.4	16.5	3.2	26	3.3	13.5	4.3	9.5	3.6	5	3.3	15.3	5.7	31	11	16	28	·	·	·	–	–	8	5	·	4	27	
II	2	1.2	0.5	1.0	3.5	2.6	11.5	3.6	14.5	3.3	20.5	3.1	19	2.9	6.5	2.7	6	2.8	12.2	2.9	9	·	1	18	·	·	·	–	–	9	6	·	10	13	
III	·	·	·	·	·	·	·	·	4	3.4	16.5	4.5	52.5	5.7	18	6.1	2	5.4	31.6	7.4	12	·	·	8	·	4	·	–	–	19	10	·	2	4	1
IV	6	2.5	4.5	5.2	17	5.2	13.5	5.4	9	3.5	12.5	3.2	13	3.8	7.5	4.7	7	4.0	35.4	9.9	8	·	·	4	·	2	·	–	–	6	4	·	·	·	2
V	8	2.8	1.5	3.7	7	3.3	11.5	2.6	10.5	2.8	9	3.2	18.5	3.3	15	3.6	12	2.7	43.9	7.8	30	·	·	·	·	·	·	–	–	14	10	·	1	·	7
VI	2.5	2.2	3	2.2	10.5	3.3	10.5	2.7	10	2.4	13	2.8	23	3.0	9.5	3.0	8	2.6	65.9	18.5	4	·	·		8	·	·	–	–	11	10	3	·	·	9
VII	3.5	3.7	1	3.5	0.5	1.0	3.5	3.4	13.5	3.1	20.5	3.0	31.5	3.3	7	3.3	12	2.8	57.1	17.2	30	·	·		7	1	1	–	–	13	10	2	·	·	9
VIII	3	3.5	1	3.0	3	2.0	3	2.3	10.5	3.1	19	3.2	32.5	3.5	16	3.5	5	3.1	36.2	10.6	12	·	·		5	1	·	–	–	10	7	2	1	·	6
IX	3	1.7	2.5	2.6	13.5	3.4	5.5	3.0	8	2.7	23	3.0	19.5	4.0	7	3.3	8	3.0	8.9	2.3	10	·	·	2	7	·	·	–	–	8	4	·	4	·	·
X	1.5	3.0	1.5	3.7	17.5	5.0	27.5	6.0	18.5	4.0	8	3.0	10	3.2	4.5	4.0	4	4.3	4.6	2.8	14	·	·	·	·	·	·	–	–	2	2		6	·	·
XI	5.5	4.9	2	5.0	13	6.1	13	4.4	12.5	3.4	14.5	3.8	18.5	4.4	8	5.1	3	4.4	46.3	14.5	13	·	2	13	·	·		–	–	15	8	2	5	·	
XII	9.5	6.5	4.5	4.7	5	3.5	6.5	3.4	16	3.6	14	4.6	20	4.5	14.5	5.0	3	4.4	25.5	9.9	6	10	19	26	·	·		–	–	10	6	·	5	25	·
Rok	49	2.9	26.5	3.1	92.5	3.1	117.5	3.4	143.5	3.2	196.5	3.4	271.5	3.8	123	4.0	75	3.6	382.9	18.5	4.VI	21	38	99	27	8	1	–	–	125	82	9	38	69	34

Lublin $H_s = 171 m$ $H_b = 176,7 m$ $h_w = 10 m$

I	7	3.6	3.5	4.4	7.5	4.7	10.5	2.5	16.5	3.2	28	3.8	9.5	4.4	6.5	3.1	4	3.2	20.7	7.3	31	12	13	27	·	4	·	3	11	16	5	·	5	25	·
II	3	2.7	·	·	5.5	2.6	13	3.1	15	3.6	18.5	2.9	19	2.9	4	2.1	6	2.8	11.3	2.7	9	·	1	19	·	·	·	1	18	14	4	·	9	5	·
III	·	·	·	·	·	·	·	·	5	3.2	31.5	5.2	49	5.5	4.5	7.2	3	5.2	38.0	6.3	28	·	·	8	·	14	3	1	13	18	12	·	3	3	1
IV	9.5	2.2	8.5	4.3	17	4.4	9.5	4.8	9	2.7	14.5	4.0	10	4.5	7	3.9	5	3.7	38.0	11.0	8	·	·	4	1	8	1	6	3	6	5	2	1	·	2
V	7	2.2	4	2.8	5	3.6	11	3.3	12	3.0	18	3.1	14	4.0	15	3.8	7	3.1	44.5	10.1	4	·	·	·	3	2	·	·	13	17	13	1	4	·	4
VI	1	2.0	4.5	2.6	15.5	3.0	6.5	3.0	7.5	3.0	20	3.4	18.5	2.6	7.5	3.0	9	2.7	56.4	12.2	27	·	·	·	12	1	·	2	5	15	12	1	·	·	10
VII	5.5	3.1	0.5	6.0	·	·	1	3.0	14	3.3	32.5	3.8	18.5	2.6	3	2.7	18	2.7	65.2	19.6	30	·	·	·	8	5	1	3	7	17	11	2	·	·	7
VIII	2	3.0	1	1.0	2.5	2.6	0.5	1.0	7.5	3.1	25	4.3	31.5	3.3	9	2.6	14	2.9	31.3	9.1	13	·	·	·	8	2	·	2	7	15	5	·	1	·	3
IX	4.5	1.2	6	2.2	9.5	2.5	3.5	3.1	7.5	2.8	25	4.0	13.5	3.2	2.5	4.8	18	2.6	10.0	3.3	6	·	·	1	8	2	·	11	9	11	4	·	3	·	·
X	1.5	1.0	7.5	3.2	21.5	3.8	21	4.0	17.5	3.2	5.5	3.6	6.5	2.3	4	2.4	8	3.1	4.7	2.7	14	·	·	·	·	6	1	8	9	5	2	·	6	·	·
XI	3.5	4.7	6	3.5	13.5	4.5	6	3.4	14.5	2.6	27	3.7	6.5	3.8	7	3.9	6	3.4	59.6	17.6	13	·	1	12	·	2	·	1	21	20	12	2	6	·	·
XII	12	3.9	0.5	3.0	6	2.5	4	2.2	15	2.9	18	5.5	15	3.3	12.5	4.8	10	3.5	41.9	9.8	7	10	16	26	·	6	1	1	16	18	8	·	7	25	·
Rok	56.5	2.5	42	2.8	103.5	2.6	86.5	2.8	141	3.0	263.5	3.9	211.5	3.5	82.5	3.7	108	3.2	421.6	19.6	30.VII	22	31	97	40	52	7	39	132	172	93	8	45	58	27

Felin

$\varphi = 51°14'$ $\lambda = 22°38'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.7	–	6.4	4	–	–	-5.6	-2.7	-5.0	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.4	4.2	5.8
II	–	–	–	–	2.8	–	9.3	18	–	–	-0.5	2.0	0.5	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.2	7.9	8.1
III	–	–	–	–	8.0	–	17.8	18	–	–	3.0	6.6	4.6	4.7	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.7	5.8	7.1
IV	–	–	–	–	15.3	–	23.4	15	–	–	6.9	14.3	9.5	10.0	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.8	3.6	4.1
V	–	–	–	–	16.5	–	24.9	27,29	–	–	10.2	15.1	11.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.5	5.7	6.6
VI	–	–	–	–	23.6	–	31.6	26	–	–	16.5	21.8	17.1	18.1	–	–	–	–	–	–	–	–	–	–	–	–	3.6	5.8	4.7	4.7
VII	–	–	–	–	22.2	–	29.9	3	–	–	14.9	20.4	15.9	16.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.7	6.0	5.9
VIII	–	–	–	–	22.1	–	32.3	11	–	–	14.9	20.6	16.2	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	6.1	5.9
IX	–	–	–	–	20.7	–	29.0	2	–	–	10.8	19.7	13.6	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.4	3.0	4.1
X	–	–	–	–	15.9	–	23.0	19	–	–	7.6	15.2	10.2	10.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.5	3.8	4.8
XI	–	–	–	–	6.4	–	14.3	3	–	–	3.4	5.6	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	7.8	8.2
XII	–	–	–	–	-1.0	–	14.1	5	–	–	-4.3	-2.7	-4.1	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.7	7.6	7.7
Rok	–	–	–	–	12.6	–	32.3	11.VIII	–	–	6.5	11.3	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	5.5	6.1

Legnica

$\varphi = 51°13'$ $\lambda = 16°10'$

I	1003.2	1026.5	980.3	1019.3	1.2	-6.4	8.7	30	-23.3	27	-4.5	-0.5	-2.9	-2.7	4.3	4.8	4.6	4.6	8.7	7.7	8.4	8.3	0.7	1.6	1.0	1.1	6.3	6.5	6.5	6.4
II	1006.1	1022.2	975.5	1022.0	7.9	0.4	13.6	15	-4.0	18	2.1	6.0	3.4	3.7	6.5	7.4	6.9	6.9	9.1	7.9	8.8	8.6	0.7	2.1	1.0	1.3	7.4	7.2	5.2	6.6
III	1004.1	1022.1	977.7	1019.7	11.4	3.5	20.4	10	-3.1	20	5.0	9.5	6.8	7.0	7.3	7.8	7.6	7.6	8.3	6.6	7.6	7.5	1.6	4.4	2.6	2.9	7.0	7.4	5.9	6.8
IV	996.6	1007.4	988.1	1011.8	17.1	5.3	26.1	6	-1.6	10	8.1	15.7	10.5	11.2	9.8	9.9	10.4	10.0	8.8	5.6	8.1	7.5	1.3	8.6	2.6	4.2	5.8	5.6	4.8	5.4
V	997.7	1006.1	984.0	1012.9	16.0	7.6	22.3	26	4.3	18	10.0	14.2	10.9	11.5	11.0	10.8	11.4	11.1	8.9	6.7	8.7	8.1	1.5	5.8	1.7	3.0	7.9	8.1	7.2	7.7
VI	1000.3	1014.7	987.1	1015.2	23.2	11.5	29.6	25	5.6	17	15.4	21.3	16.6	17.5	15.3	15.4	16.3	15.7	8.7	6.1	8.6	7.8	2.4	10.4	2.8	5.2	5.5	5.5	5.1	5.4
VII	999.1	1011.4	983.2	1014.1	21.4	11.6	32.4	3	5.3	8	15.0	19.6	15.3	16.3	14.7	13.8	14.6	14.4	8.5	6.2	8.4	7.7	2.6	9.9	3.0	5.2	7.1	7.4	6.4	7.0
VIII	1001.7	1013.8	990.2	1016.7	22.2	11.9	32.1	6	7.1	4	14.8	20.3	15.8	16.7	15.1	15.2	15.6	15.3	8.9	6.4	8.6	8.0	1.9	9.2	2.5	4.5	6.8	7.1	4.6	6.2
IX	1003.3	1013.4	990.5	1018.3	22.7	10.1	31.1	3	1.0	24	11.8	21.2	14.4	15.4	12.9	14.2	14.3	13.8	9.2	5.8	8.6	7.9	1.4	12.0	2.6	5.3	5.2	4.9	4.1	4.7
X	1002.1	1014.8	974.0	1017.3	16.6	6.7	23.2	6	0.2	16	8.2	15.5	10.5	11.2	9.9	11.5	10.8	10.7	9.1	6.7	8.5	8.1	1.2	6.6	2.1	3.3	6.6	7.2	4.7	6.2
XI	999.0	1021.8	986.5	1014.7	7.2	1.5	14.3	2	-7.3	23	2.4	6.0	3.6	3.9	7.0	7.9	7.5	7.5	9.4	8.4	9.3	9.0	0.6	1.7	0.6	1.0	8.5	8.1	7.1	7.9
XII	1000.8	1029.9	978.4	1016.9	1.3	-7.4	17.5	5	-24.7	26	-3.6	-0.9	-3.8	-3.0	4.8	5.3	4.7	4.9	8.7	8.2	8.7	8.5	1.0	1.6	0.9	1.2	6.8	7.0	5.3	6.4
Rok	1001.2	1029.9	974.0	1016.6	14.0	4.7	32.4	3.VII	-24.7	26.XII	7.1	12.3	8.4	9.0	9.9	10.3	10.4	10.2	8.9	6.9	8.5	8.1	1.4	6.2	2.0	3.2	6.7	6.8	5.6	6.4

Wieluń

$\varphi = 51°13'$ $\lambda = 18°35'$

I	995.3	1018.7	974.3	1020.7	-0.3	-7.6	9.2	4	-22.8	27	-5.1	-1.6	-4.3	-3.8	4.0	4.6	4.3	4.3	8.5	7.8	8.6	8.3	0.7	1.3	0.7	0.9	6.6	6.0	5.6	6.1
II	997.4	1013.3	969.0	1022.2	5.4	-0.3	13.6	18	-7.3	6	0.8	4.3	1.8	2.2	6.0	6.8	6.3	6.4	9.3	8.1	9.0	8.8	0.5	1.7	0.7	1.0	9.0	7.1	5.5	7.2
III	994.2	1012.5	969.3	1018.5	9.8	2.2	18.9	10	-4.6	20	3.5	8.0	5.2	5.5	6.8	7.2	7.3	7.1	8.5	6.8	8.2	7.8	1.2	3.9	1.8	2.3	8.5	8.3	6.5	7.8
IV	988.6	998.4	979.1	1012.5	17.2	4.9	25.6	7	-4.6	10	7.9	15.6	9.7	10.7	8.8	9.3	9.0	9.0	8.0	5.3	7.4	6.9	2.2	9.3	3.3	4.9	5.5	4.7	4.3	4.8
V	988.6	995.9	974.0	1012.4	17.2	6.8	23.3	5,27	2.6	12	10.1	15.5	10.3	11.6	10.6	10.6	11.0	10.7	8.5	6.1	8.7	7.8	1.9	7.4	1.7	3.7	6.7	7.6	6.2	6.8
VI	991.7	1005.5	980.7	1015.0	23.8	11.8	31.2	27	6.4	16	16.2	21.8	15.9	17.4	15.0	15.1	15.1	15.1	8.1	5.8	8.3	7.4	3.6	11.8	3.1	6.2	4.9	6.1	5.9	5.6
VII	990.5	1002.2	975.4	1013.9	21.2	11.3	32.5	3	6.6	8	14.7	19.3	14.6	15.8	14.2	14.0	13.9	14.0	8.4	6.4	8.3	7.7	2.9	9.4	3.1	5.1	6.4	7.8	6.8	7.0
VIII	993.2	1006.0	982.7	1016.7	21.8	12.1	31.2	6	7.6	31	14.5	20.4	15.0	16.2	14.7	15.5	15.2	15.1	8.8	6.4	8.8	8.0	2.1	9.1	2.2	4.5	6.5	7.6	4.9	6.3
IX	995.3	1006.2	982.9	1018.9	21.3	9.5	29.9	2	0.9	24	11.7	20.3	13.4	14.7	12.2	13.7	13.0	13.0	8.7	5.8	8.3	7.6	2.0	10.9	2.7	5.2	5.7	4.4	2.8	4.3
X	994.6	1007.0	967.3	1018.6	15.8	7.0	21.5	6	2.8	22	8.1	14.8	10.4	10.9	9.8	11.1	10.5	10.5	9.1	6.7	8.3	8.0	1.1	6.0	2.2	3.1	7.4	7.0	4.3	6.2
XI	990.3	1012.8	977.6	1014.7	6.8	1.4	13.3	7	-4.7	23	2.8	5.7	3.4	3.8	7.0	7.6	7.3	7.3	9.1	8.1	9.1	8.8	0.6	1.9	0.7	1.1	8.6	8.7	7.5	8.3
XII	991.7	1019.8	971.4	1016.9	0.0	-7.4	15.2	5	-23.7	26	-3.8	-1.8	-4.0	-3.4	4.7	4.9	4.5	4.7	8.6	8.1	8.6	8.4	0.7	1.3	0.7	0.9	7.5	7.4	6.5	7.1
Rok	992.6	1019.8	967.3	1016.7	13.3	4.3	32.5	3.VII	-23.7	26.XII	6.8	11.9	7.6	8.5	9.5	10.0	9.8	9.8	8.6	6.8	8.5	8.0	1.6	6.2	1.9	3.2	6.9	6.9	5.6	6.5

Siemianice

$\varphi = 51°11'$ $\lambda = 18°09'$

I	–	–	–	–	-0.4	-7.4	10.3	4	-23.2	27	-5.4	-1.9	-4.5	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.9	5.9	6.2
II	–	–	–	–	5.4	-0.1	11.0	18	-4.6	6	0.6	4.1	1.7	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.1	5.0	6.8
III	–	–	–	–	9.8	2.1	18.9	10	-4.3	20	3.2	7.9	5.1	5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.3	6.0	7.2
IV	–	–	–	–	16.3	5.0	25.1	7	-1.3	10	7.7	15.2	9.9	10.7	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.5	4.7	4.9
V	–	–	–	–	16.4	6.8	22.5	27	2.5	12	9.8	14.6	10.2	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.5	6.6	7.1
VI	–	–	–	–	23.3	11.8	30.1	27	6.4	22	16.1	21.2	16.2	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.3	5.4	5.5
VII	–	–	–	–	21.1	11.3	32.0	3	5.5	8	14.5	19.2	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.7	7.3	7.3
VIII	–	–	–	–	21.4	12.0	31.1	6	7.6	14	14.5	19.8	15.5	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	5.9	6.3
IX	–	–	–	–	21.3	9.6	30.0	2	1.1	23	11.4	20.0	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.4	4.2	4.6
X	–	–	–	–	15.6	7.0	21.5	6	1.8	22	8.1	14.7	10.5	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	4.8	6.3
XI	–	–	–	–	6.7	1.5	12.7	7	-4.2	22	2.6	5.5	3.4	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.5	7.3	8.0
XII	–	–	–	–	0.1	-7.1	14.7	5	-23.3	26	-4.1	-2.0	-3.5	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.8	6.3	7.0
Rok	–	–	–	–	13.1	4.4	32.0	3.VII	-23.3	26.XII	6.6	11.5	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	5.8	6.4

Felin H_s = 215 m h_w = 10 m 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	6	2.7	4.5	2.9	1	2.0	1	2.0	14.5	3.5	11.5	4.5	8	2.9	4.5	2.8	42	4.8	13.3	3.9	14	–	15	–	·	2	1	3	10	–	5	·	–	22	–
II	1.5	2.7	·	·	·	·	1	4.0	10	2.0	16	3.1	5.5	2.1	4	2.6	46	1.1	8.4	2.8	9	–	·	–	·	·	·	2	19	–	3	·	–	1	–
III	0.5	1.0	1	1.0	·	·	·	·	2.5	1.0	27	3.3	45.5	4.3	3.5	1.6	13	3.2	29.4	5.8	12	–	·	–	·	1	·	1	13	–	10	·	·	·	–
IV	·	·	6	1.7	6	1.7	8	2.5	10	1.4	9	3.0	6.5	4.2	3.5	4.7	41	1.4	33.8	11.0	8	–	·	–	·	3	·	9	4	–	6	1	·	·	–
V	4	3.4	0.5	2.0	1	1.0	5	1.2	5	1.8	7	4.4	6.5	2.4	6	2.5	58	1.0	45.1	12.5	30	–	·	–	·	·	·	2	12	–	11	1	·	·	–
VI	1.5	1.3	2.5	1.6	7	1.1	3	1.7	3	1.7	9	2.3	5	1.0	2	4.0	57	0.6	37.7	6.5	14	–	·	–	8	·	·	6	4	–	11	·	·	·	–
VII	2	1.0	·	·	2	3.5	·	·	3	2.0	24	1.5	17	1.7	1	1.0	44	0.9	64.9	20.6	30	–	·	–	8	·	·	3	6	–	12	2	·	·	–
VIII	0.5	6.0	·	·	3	1.7	0.5	1.0	7.5	1.0	24	1.9	15.5	2.3	4	2.2	38	1.1	36.7	17.7	12	–	·	–	6	·	·	3	7	–	6	1	·	·	–
IX	·	·	2	1.0	2	1.0	·	·	6.5	2.0	10.5	1.1	13.5	2.8	3.5	1.4	52	0.8	10.2	2.7	14	–	·	–	7	·	·	13	5	–	5	·	–	·	–
X	·	·	5	1.4	5	1.0	15.5	2.3	13	2.4	11.5	1.7	3.5	2.3	5.5	1.8	34	1.2	5.2	2.9	14	–	·	–	·	·	·	9	7	–	2	·	–	·	–
XI	10	2.0	2	1.8	9	3.1	7	2.6	18	2.2	9	2.4	18.5	2.2	6.5	2.4	10	2.0	48.0	18.2	13	–	·	–	·	·	·	2	21	–	8	1	5	·	–
XII	24.5	3.7	1.5	8.7	4.5	4.0	·	·	13.5	4.4	11	4.9	20.5	1.9	4.5	1.1	13	3.0	30.7	9.3	6	–	19	–	·	4	·	3	19	–	6	·	3	25	–
Rok	50.5	2.0	25	1.8	40.5	1.7	41	1.2	106.5	2.1	169.5	2.8	165.5	2.5	48.5	2.3	448	1.5	363.4	20.6	30.VII	–	34	–	29	10	1	56	127	–	85	6	–	48	–

Legnica H_s = 121 m H_b = 126,3 m h_w = 12 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	·	·	4	3.1	11.5	3.1	15.5	2.4	49.5	2.9	40.5	2.4	14	2.3	7	2.0	11	2.3	26.1	7.5	14	11	12	22	·	2	1	5	13	13	7	·	5	15	·
II	1.5	3.3	·	·	0.5	6.0	11.5	2.4	14	2.5	6.5	3.0	22.5	3.0	15.5	3.0	12	2.4	28.0	9.7	9	·	·	12	·	1	·	5	14	16	6	·	3	1	·
III	1.5	3.3	·	·	·	·	·	·	0.5	4.0	4	3.6	56	3.8	27	4.1	4	3.7	32.1	8.7	28	·	·	4	·	2	·	2	11	15	11	·	·	1	1
IV	2.5	1.0	4.5	1.9	12	3.4	15.5	3.4	6.5	2.8	5.5	2.0	12.5	2.4	17	2.3	14	2.3	87.7	23.5	8	·	·	2	2	·	·	5	9	10	10	3	1	·	6
V	2	3.5	6	2.0	1	1.0	1	5.0	7	1.7	1.5	3.3	37.5	2.8	32	2.3	5	2.4	88.8	19.2	29	·	·	·	·	·	·	1	20	20	16	2	·	·	7
VI	·	·	2.5	2.2	4.5	1.9	8	2.0	4	2.5	1.5	1.3	29	2.8	24.5	2.8	16	2.1	61.0	16.3	7	·	·	·	6	·	·	6	3	15	9	2	2	·	9
VII	1	1.0	·	·	1.5	3.7	4.5	1.7	3	1.3	11	2.0	44.5	2.9	16.5	2.9	11	2.3	69.8	15.9	30	·	·	·	9	1	·	2	14	17	12	3	·	·	5
VIII	·	·	1	2.0	2	2.0	2.5	3.0	4	1.2	11	2.3	36	2.7	18.5	2.5	18	2.0	50.5	27.3	11	·	·	·	7	·	·	1	7	14	7	1	1	·	4
IX	2	1.2	4.5	1.2	10.5	2.2	9	2.4	8.5	2.2	5	1.5	20.5	2.9	13	2.6	17	1.9	24.5	6.3	5	·	·	·	9	1	·	10	7	8	7	·	4	·	3
X	1	1.0	2	1.0	6	4.2	20.5	3.6	17	3.4	3.5	3.9	7	2.8	17	1.8	19	2.4	40.5	12.4	20	·	·	·	·	1	·	5	12	8	5	1	4	·	·
XI	3	2.5	8.5	1.5	7	3.6	4.5	3.0	5	2.9	5	3.1	16	2.8	17	2.5	24	1.9	40.5	12.8	13	·	·	8	·	·	·	1	16	14	8	2	9	·	·
XII	3.5	2.4	8	2.7	2.5	3.4	11	2.8	7	3.2	6.5	3.0	25.5	3.6	13	4.0	16	2.7	41.6	10.1	12	11	13	22	·	·	·	5	13	14	9	1	3	16	·
Rok	18	1.6	41	1.5	59	2.9	103.5	2.6	96	2.6	71.5	2.6	321	2.9	218	2.7	167	2.4	591.1	27.3	11.VIII	22	25	70	33	8	1	48	139	164	107	15	32	33	35

Wieluń H_s = 195 m H_b = 198,4 m h_w = 11 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	5	0.9	5	2.2	11.5	1.5	15	2.1	23.5	3.5	20	2.8	6	2.2	7	1.7	·	2.5	46.5	9.0	14	12	13	26	·	3	·	6	13	7	4	·	4	21	·
II	2.5	1.8	·	·	3.5	1.7	8.5	2.1	20.5	2.8	20	2.8	19.5	2.7	8.5	2.2	1	2.5	37.3	12.4	9	·	·	14	·	2	·	1	14	18	7	1	9	7	·
III	·	·	·	·	·	·	·	·	1	3.0	22.5	3.9	53.5	4.2	15	4.0	1	4.0	35.6	7.6	21	·	·	8	·	4	·	1	17	15	10	·	4	5	2
IV	1.5	1.0	7	2.4	28	3.5	7	3.2	11.5	2.4	9	2.9	17	2.4	9	2.7	·	2.9	38.7	16.8	8	·	·	4	3	·	·	6	4	7	5	2	1	·	5
V	8	3.1	6	2.3	5	1.4	3.5	2.3	8	2.3	11.5	3.3	25	2.7	26	2.4	·	2.6	76.1	22.3	29	·	·	·	·	·	·	3	10	16	13	1	1	·	6
VI	3	1.0	4.5	1.9	6.5	2.2	6	1.8	7.5	2.1	8	2.2	32.5	2.3	21	1.9	1	2.0	39.7	12.7	27	·	·	·	11	·	·	4	5	15	12	1	1	·	9
VII	2	1.0	·	·	3	1.7	1	4.0	6	2.1	18.5	2.4	48	3.1	14.5	1.8	·	2.6	172.9	33.5	31	·	·	·	7	·	·	3	13	20	17	5	·	·	5
VIII	0.5	2.0	2.5	1.6	3.5	2.6	2	1.2	8.5	2.2	20.5	3.4	36	3.2	18.5	1.8	1	2.7	53.4	11.3	10	·	·	·	5	2	·	1	9	13	8	3	3	·	5
IX	3	1.3	2	1.8	23.5	2.1	5	2.3	14.5	2.2	16	2.6	49.5	2.7	6.5	1.6	·	2.3	46.1	6.0	6	·	·	·	7	·	·	9	7	7	4	·	3	·	2
X	3.5	1.0	2	2.5	28	3.2	14	2.7	13.5	3.6	12	3.1	42.5	1.8	6.5	2.6	1	2.8	15.7	5.9	7	·	·	·	·	1	·	4	9	6	5	·	5	·	·
XI	13	1.7	3	3.8	10	2.7	9	1.8	11.5	2.0	17.5	2.5	20	2.2	6	1.8	·	2.2	73.8	32.7	13	·	·	10	·	·	·	1	18	19	12	1	8	4	·
XII	8	2.1	7.5	1.7	10	2.1	6	1.8	17	3.3	13	4.8	20	2.4	40.5	3.2	1	2.8	44.9	12.2	11	11	13	25	·	4	·	2	15	17	9	1	2	20	·
Rok	50	1.4	39.5	1.7	132.5	2.1	77	1.9	143	2.6	188.5	3.1	309.5	2.7	149	2.3	6	2.7	620.7	33.5	31.VII	23	26	87	33	16	·	41	134	160	106	15	41	57	34

Siemianice H_s = 182 m h_w = 10 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◑	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	1	4.0	6.5	4.6	8.5	4.0	7.5	4.4	20.5	4.2	23.5	3.8	8	4.6	4.5	3.4	13	3.5	16.9	8.4	14	12	13	24	·	·	·	6	15	10	3	·	3	20	·
II	1.5	2.0	1	3.5	4.5	4.3	6	3.8	16.5	3.4	20	3.4	18	5.2	9.5	6.6	7	3.9	32.1	16.4	9	·	·	16	·	3	1	3	12	14	6	1	7	3	·
III	1	7.5	·	·	·	·	0.5	4.0	2	3.0	23.5	5.1	49.5	7.4	15.5	8.1	1	6.8	29.3	7.9	14	·	·	7	·	17	5	1	14	14	9	·	4	4	·
IV	4	3.1	10.5	5.4	17	5.3	9.5	5.2	8	2.9	10	3.1	11.5	4.6	11.5	4.6	8	4.1	37.5	16.3	8	·	·	3	1	3	·	5	8	7	7	1	2	·	3
V	5	4.3	9	3.7	·	·	1	3.0	6	2.9	11	3.9	28.5	4.8	15.5	4.2	17	3.4	62.7	23.0	29	·	·	·	·	2	·	2	12	13	11	1	·	·	5
VI	6.5	3.5	3.5	4.4	1	4.0	7.5	2.6	6.5	2.1	14.5	2.5	29	4.9	11.5	5.1	10	3.5	71.3	21.7	8	·	·	·	10	2	·	2	4	14	11	3	·	·	10
VII	1	2.0	1.5	1.7	1	1.0	3.5	4.3	5	3.1	21	3.6	39	4.3	16	4.8	5	3.9	163.3	47.8	31	·	·	·	7	2	·	3	10	18	13	4	·	·	6
VIII	2.5	3.0	3.5	3.3	1	4.0	3	4.3	4.5	3.8	31	4.4	19.5	6.2	17	4.4	11	4.2	53.6	11.4	11	·	·	·	5	4	·	3	7	13	10	1	1	·	6
IX	1.5	3.7	12.5	3.5	8.5	4.0	5.5	3.3	7.5	2.5	17.5	3.3	20	4.9	8	4.7	9	3.5	17.5	6.6	26	·	·	·	7	1	·	10	9	7	5	·	4	·	1
X	1	2.0	3	5.0	12	6.1	18.5	4.4	23.5	3.6	13	3.1	7	3.5	9	4.7	6	3.9	27.3	11.3	18	·	·	·	·	3	·	4	9	7	4	1	8	·	·
XI	6.5	4.7	5.6	6.8	5	5.6	5	3.7	14	2.7	23	3.3	42.5	4.2	11.5	4.7	7	3.7	71.3	40.7	13	·	·	8	·	1	·	1	19	13	10	1	9	1	·
XII	9	6.6	7	4.4	2.5	4.4	7.5	3.1	10	3.4	16.5	5.0	16	5.3	13.5	6.8	11	4.5	43.7	12.9	11	12	14	24	·	6	1	1	13	14	11	1	9	20	·
Rok	40.5	3.9	63.5	3.9	61	3.6	75	3.8	124	3.1	224.5	3.7	258.5	5.0	143	5.2	105	4.1	626.5	47.8	31.VII	24	27	82	30	44	7	41	132	144	100	14	47	48	31

Opole Lubelskie

$\varphi = 51°09'$ $\lambda = 21°59'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.8	-8.6	8.5	4	-23.6	27	-4.9	-1.9	-4.3	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.6	5.1	5.9
II	–	–	–	–	3.7	-0.8	11.5	18	-6.5	5	0.3	3.2	1.3	1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.7	7.3	8.0
III	–	–	–	–	9.4	2.0	19.4	18	-2.3	23	4.0	8.1	5.1	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	5.2	6.3
IV	–	–	–	–	16.5	4.4	25.2	15	-4.5	10	8.7	15.4	9.4	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.5	6.6	26.0	27	0.9	19	11.1	15.9	10.9	12.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	24.7	11.9	32.2	27	4.9	21	16.7	23.0	16.6	18.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.6	11.2	31.6	3	6.6	6	15.2	20.5	15.5	16.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.6	12.3	34.0	11	5.0	31	14.7	21.3	16.1	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.3	8.3	30.2	2	-0.7	23	10.8	20.5	13.2	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.1	3.1	3.9
X	–	–	–	–	16.6	6.1	24.2	19	2.3	14	7.6	16.0	10.5	11.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.5	4.4	5.1
XI	–	–	–	–	7.0	1.8	14.6	3	-7.6	23	3.9	6.4	4.2	4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.0	8.2	8.1
XII	–	–	–	–	-0.4	-7.7	14.4	5	-24.1	26	-4.2	-2.0	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.3	6.5	7.4
Rok	–	–	–	–	13.4	4.0	34.0	11.VIII	-24.1	26.XII	7.0	12.2	7.9	8.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Zgorzelec

$\varphi = 51°08'$ $\lambda = 15°02'$

I	994.5	1013.0	968.5	1019.1	0.8	-5.1	6.0	31	-18.8	27	-3.2	0.0	-2.3	-1.9	4.4	4.8	4.6	4.6	85	76	83	81	0.8	1.5	0.9	1.1	6.5	6.6	6.4	6.5
II	995.3	1011.5	963.9	1022.5	6.5	0.7	11.4	18	-7.6	6	2.1	5.4	3.0	3.4	6.3	7.0	6.6	6.6	88	78	86	84	0.9	2.1	1.1	1.4	7.0	6.8	5.2	6.3
III	994.3	1012.1	966.7	1021.2	10.5	2.8	18.3	17	-4.7	20	4.0	8.9	6.0	6.2	7.1	8.0	7.7	7.6	86	70	82	79	1.2	3.9	1.9	2.3	8.3	8.5	6.5	7.8
IV	985.6	996.7	976.3	1011.8	16.5	6.1	25.2	7	-0.4	1	8.5	15.3	10.7	11.3	9.5	10.3	10.1	10.0	85	60	77	74	1.8	7.7	3.1	4.2	6.1	6.1	4.5	5.6
V	987.4	996.3	975.4	1013.7	14.8	7.3	22.8	26	3.8	12	9.2	12.8	10.3	10.6	10.4	10.7	10.8	10.6	89	73	86	83	1.3	4.5	1.9	2.6	8.5	8.7	7.0	8.0
VI	990.2	1004.7	976.2	1016.0	22.4	11.4	29.2	25	6.0	16	14.7	20.8	16.5	17.1	14.9	16.4	15.8	15.7	88	67	83	79	2.0	8.5	3.3	4.6	6.4	6.1	5.2	5.9
VII	988.9	1001.0	972.9	1014.8	20.5	11.5	31.3	3	7.1	8	14.2	19.0	15.0	15.8	14.5	14.6	14.7	14.6	88	66	85	80	2.0	8.3	2.8	4.4	7.5	7.7	7.0	7.4
VIII	991.5	1002.9	979.7	1017.4	20.9	11.8	29.6	6	6.9	14	13.8	19.7	15.5	16.1	14.6	16.8	15.5	15.6	92	74	87	84	1.4	6.8	2.4	3.5	7.5	7.2	4.7	6.5
IX	992.6	1002.6	979.6	1018.5	22.3	11.1	29.1	2	3.4	23	12.6	21.2	15.1	16.0	12.9	14.8	14.4	14.0	87	60	83	77	2.3	11.3	2.9	5.5	5.6	4.8	3.3	4.6
X	990.9	1004.6	961.9	1017.2	15.5	7.1	22.9	6	2.2	23	8.6	14.6	10.1	10.8	10.0	11.2	10.5	10.6	90	69	85	81	1.6	5.8	2.0	3.1	6.1	6.7	4.0	5.6
XI	988.0	1010.2	975.9	1015.0	6.3	1.6	11.4	3	-6.3	21	2.8	5.3	3.7	3.9	6.8	7.3	7.1	7.0	89	82	88	86	0.8	1.6	1.0	1.1	8.1	7.2	6.9	7.4
XII	989.7	1016.9	967.9	1017.4	1.5	-6.3	15.2	5	-21.5	25	-3.3	-0.9	-2.7	-2.4	4.9	5.2	5.2	5.1	87	82	87	85	0.8	1.3	0.8	1.0	7.6	7.0	6.2	6.9
Rok	990.5	1016.9	961.9	1017.0	13.2	5.0	31.3	3.VII	-21.5	25.XII	7.0	11.8	8.4	8.9	9.7	10.6	10.2	10.2	88	71	84	81	1.4	5.3	2.0	2.9	7.1	7.0	5.6	6.6

Wrocław - Gądów Mały

$\varphi = 51°08'$ $\lambda = 16°59'$

I	1004.3	1028.0	981.7	1019.4	1.2	-6.3	9.7	4	-19.7	27	-4.3	-0.4	-2.7	-2.5	4.2	4.7	4.5	4.5	87	76	85	83	0.7	1.6	0.9	1.1	6.2	6.5	6.8	6.5
II	1007.0	1022.6	975.9	1021.9	7.5	-0.8	13.1	15	-6.9	6	1.2	5.8	2.7	3.1	6.2	6.8	6.6	6.5	91	75	88	85	0.6	2.5	1.0	1.4	7.0	6.8	5.5	6.4
III	1004.6	1022.5	978.8	1019.2	11.4	2.0	20.1	10	-5.9	20	3.9	9.3	5.9	6.2	7.0	7.4	7.5	7.3	85	64	80	76	1.3	4.6	2.1	2.7	7.9	7.5	6.3	7.2
IV	997.5	1007.9	988.8	1018.8	17.6	5.1	25.6	7	-1.5	10	8.4	16.1	10.8	11.5	9.4	9.7	9.9	9.7	83	53	75	70	1.8	9.3	3.4	4.8	6.3	6.1	5.0	5.8
V	998.3	1006.8	984.2	1012.6	16.8	6.3	23.3	26	2.3	13	9.9	14.7	10.7	11.5	10.7	10.9	11.0	10.9	87	66	86	80	1.7	6.2	2.1	3.3	7.5	7.9	7.4	7.6
VI	1001.0	1015.3	982.4	1015.0	23.7	10.7	29.7	25	4.4	22	15.5	21.4	16.6	17.5	14.7	15.0	15.7	15.1	83	59	82	75	3.1	11.0	3.5	5.9	5.7	5.8	5.3	5.6
VII	999.9	1011.9	984.1	1014.0	21.8	10.8	32.9	3	3.6	8	14.8	19.4	15.1	16.1	13.8	13.2	13.9	13.6	82	60	81	74	3.2	10.4	3.5	5.7	7.0	7.3	7.2	7.2
VIII	1002.5	1015.1	991.5	1016.6	22.3	10.8	31.5	6	5.1	4	14.5	20.2	15.3	16.3	15.0	15.6	15.5	15.4	90	66	88	81	1.7	8.7	2.2	4.2	6.8	7.5	6.0	6.8
IX	1004.2	1015.1	991.9	1018.3	22.4	9.4	30.2	2,17	2.3	25	11.8	21.1	14.4	15.4	13.0	13.7	13.9	13.5	92	55	84	77	1.1	12.2	2.8	5.4	5.6	5.1	3.8	4.8
X	1003.3	1015.9	975.1	1017.7	16.5	6.4	23.4	6	1.4	14	8.2	15.2	10.2	11.0	10.1	11.5	10.9	10.8	93	68	88	83	0.9	6.1	1.8	2.9	7.0	7.2	4.0	6.1
XI	999.8	1023.0	987.5	1014.6	7.2	0.8	13.0	2	-8.6	23	2.4	6.1	3.3	3.8	7.1	7.9	7.5	7.5	94	83	93	90	0.5	1.6	0.6	0.9	8.4	8.4	7.2	8.0
XII	1001.6	1030.8	979.9	1016.8	0.9	-7.7	16.4	5	-24.4	26	-4.0	-4.0	-3.7	-3.9	4.8	5.2	4.7	4.9	89	81	87	86	0.8	1.4	0.8	1.0	7.6	6.5	5.8	6.6
Rok	1002.0	1030.8	975.1	1016.5	14.1	4.0	32.9	3.VII	-24.4	26.XII	6.9	12.3	8.2	8.9	9.7	10.4	10.1	10.0	88	67	85	80	1.4	6.3	2.1	3.3	6.9	6.9	5.9	6.6

Czarniecka Góra

$\varphi = 51°08'$ $\lambda = 20°31'$

I	–	–	–	–	-0.1	-8.5	5.9	4,5,5,30	-26.2	26	-6.2	-1.6	-4.9	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	3.8	-1.8	8.9	28	-9.4	6	-0.1	2.9	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8.6	–	17.9	18	–	–	2.8	7.1	4.9	4.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.1	4.2	24.9	7,15	-1.5	10,21	6.9	15.0	8.7	9.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.1	6.6	25.1	27	2.1	25	9.3	15.5	10.9	11.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.6	11.7	31.5	27	5.0	21	15.4	22.6	16.6	17.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.1	10.3	31.2	3	5.9	20	13.9	19.9	15.4	16.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.6	10.4	30.1	6,11	5.3	30	13.7	20.5	16.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.0	6.9	29.0	17	-1.4	23	9.9	20.2	13.3	14.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	16.1	4.7	23.0	20	-0.4	14	6.7	15.5	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.4	-0.1	12.4	7	-10.4	21,23	2.3	5.5	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-0.6	-8.6	15.4	5	-25.8	26	-5.2	-2.3	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12.9	–	31.5	27.VI	-26.2	26.I	5.8	11.7	7.5	8.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Opale Lubelskie

H_s = 149 m h_w = 12,5 m

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◔	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	[illegible]
I	8	2.8	4	2.8	2	3.5	9	3.9	23	4.7	9	5.6	14	2.9	24	3.3	·	3.8	18.6	5.0	14	12	13	29	·	3	·	8	12	14	4	·	·	23	·
II	4	4.2	1	3.0	2	2.0	12	2.8	18	3.8	7	2.6	17	4.8	23	3.0	·	2.8	49.5	3.8	28	·	1	17	·	1	·	3	19	14	6	·	11	1	
III	3	3.3		·	·	·	·	·	2	5.5	6	5.0	32	4.7	50	5.1	·	4.9	20.9	3.8	18	·	·	7	·	5	·	6	10	17	8	·	3	1	
IV	8	2.8	6	4.0	17	4.5	13	6.2	5	3.2	7	2.7	11	3.9	23	3.0	·	3.9	32.6	41.8	8	·	·	2	1	·	·	–	–	8	4	2	·		
V	10	2.8	2	2.5	6	3.8	13	2.3	14	3.1	2	4.0	18	3.1	28	3.1	··	3.0	28.8	5.6	7	·	·	·	3	·	·	–	–	15	8	·	1	·	
VI	4	2.5	1	2.0	13	3.5	10	3.5	7	4.1	10	3.2	16	3.2	29	4.0	·	3.5	53.2	9.4	27	·	·	·	14	·	·	–	–	15	13	·	·	·	·
VII	5	2.8	3	2.0	3	2.3	1	2.0	10	3.5	14	3.6	29	3.5	28	3.3	·	3.3	95.5	23.7	30	·	·	·	8	1	1	–	–	16	12	3	·	·	
VIII	6	3.3	3	3.3	5	1.6	1	1.0	8	2.9	9	4.4	28	3.1	33	2.9	·	3.0	39.5	10.7	13	·	·	·	8	·	·	–	–	13	9	2	1	·	·
IX	3	4.7	11	2.5	11	4.7	5	2.6	12	4.8	15	3.4	18	2.7	15	4.0		2.7	6.6	3.4	14	·	·	2	8	·	·	13	7	6	2	·	2	·	·
X	2	5.0	12	3.6	15	3.2	27	4.3	12	3.9	7	4.1	9	5.0	9	4.1		4.0	4.8	3.6	14	·	·	·		1	·	7	7	2	2	·	1	·	·
XI	7	2.3	6	2.3	8	3.0	16	2.5	9	2.6	8	2.1	19	2.4	17	2.8	·	2.5	59.6	18.3	13	·	·	10	·	·	·	2	18	16	10	2	2	·	
XII	12	3.8	7	3.3	5	2.0	8	2.0	16	4.2	4	6.2	13	3.8	28	3.9	·	3.7	46.6	12.6	11	11	15	24	·	2	·	3	16	20	9	2	1	23	
Rok	72	2.9	56	2.6	87	2.6	115	2.8	136	3.6	98	3.9	224	3.3	307	3.5	·	3.4	426.2	23.7	30.VII	23	29	91	42	13	1	–	–	156	87	11	22	48*	

Uwaga. Obserwator nie notował cisz.

Zgorzelec

H_s = 219 m H_b = 217,9 m h_w = 18,3 m

I	2.5	1.0	9	3.0	5	5.4	·	·	9	3.0	54	4.1	4	2.2	15	4.0	8	3.4	30.1	40.1	31	8	9	21	·	2	·	6	13	12	5	1	·	18	·
II	2.5	2.6	0.5	1.0	·	·	·	·	6	3.3	44.5	4.2	10	3.9	6.5	3.6	14	3.3	56.2	21.4	9	·	·	7	·	2	·	5	13	15	11	1	1	4	
III	2	2.5	·	·	·	·	·	·	2.5	1.4	29	3.3	38.5	3.6	6	3.7	15	2.9	66.4	16.6	30	·	·	4	·	·	·	2	18	19	15	1	·	2	
IV	5	2.5	10	3.0	13.5	3.3	5.5	2.0	10	2.5	21.5	2.6	11.5	3.5	3	2.5	10	2.5	62.5	15.2	2	·	·	1	1	·	·	5	11	10	9	3	·	·	5
V	14	2.7	8.5	2.2	4	4.1	3	2.3	1	1.0	22	2.5	20	2.8	15.5	2.3	5	2.5	141.4	33.0	29	·	·	·	·	·	·	·	20	24	20	3	·	·	5
VI	6	2.3	0.5	2.0	4	3.0	3.5	2.6	7	1.8	24	3.2	19	2.5	16	2.2	10	2.3	57.1	23.6	3	·	·	·	7	·	·	3	9	12	8	1	·	·	6
VII	1	4.0	·	·	4	1.2	2	2.0	6	1.9	22.5	3.3	43	3.0	10.5	3.0	4	2.8	71.6	46.9	30	·	·	·	4	·	·	2	16	18	15	2	·	·	2
VIII	3	2.7	1	3.0	4	1.9	1	1.5	9.5	2.6	44.5	3.0	14	3.0	10	3.0	6	2.7	43.9	7.8	11	·	·	·	7	1	·	2	9	22	14	·	·	·	5
IX	2	2.0	6	4.6	6.5	3.8	3.5	2.0	11.5	4.0	32.5	3.6	10.5	3.1	5.5	2.7	12	3.0	17.3	3.5	14	·	·	·	10	·	·	9	6	12	7	·	·	·	2
X	3	1.0	2	4.0	11	5.5	6	4.0	8.5	6.5	36.5	4.0	4	1.9	6	2.4	16	3.4	30.2	8.3	21	·	·	·	·	4	·	5	8	9	7	·	·	·	·
XI	6	2.8	7	3.2	6	5.2	1	4.0	10	3.3	42	4.3	5.5	3.0	4.5	2.4	8	3.5	33.7	9.8	30	·	·	8	·	2	·	3	17	16	6	·	·	·	
XII	5	2.4	5.5	2.9	4.5	2.9	1	1.0	6.5	7.2	31.5	5.4	16	2.9	9	3.8	14	3.6	50.9	21.6	11	10	12	23	·	4	·	4	15	16	8	1	·	14	1
Rok	52	2.4	50	2.4	62.5	3.0	26.5	1.8	87.5	3.2	404.5	3.6	196	3.0	94	2.7	122	3.0	661.3	33.0	29.V	18	21	64	29	15	·	46	155	185	125	13	1	38	26

Wrocław - Gądów Mały

H_s = 116 m H_b = 118,6 m h_w = 20 m

I	1.5	2.3	8.5	2.4	18	3.1	14	4.4	21	5.3	15	4.2	7.5	3.9	3.5	4.9	4	3.9	24.8	6.6	31	10	12	24	·	2	2	6	15	11	5	·	8	15	
II	3.5	2.9	·	·	5.5	2.5	18.5	3.2	17.5	3.9	7	4.5	18	4.8	7	4.0	7	3.5	39.7	12.2	9	·	·	17	·	2	·	4	11	13	8	1	7	3	
III	2.5	3.0	·	·	·	·	0.5	1.0	4.5	3.0	18	5.1	48.5	6.1	18	4.3	1	5.2	28.2	7.4	14	·	·	8	·	11	·	2	15	14	11	·	7	2	1
IV	8.5	1.5	17	2.3	12	3.5	13.5	4.1	8.5	3.5	6	5.2	12.5	4.0	3	2.8	9	3.0	64.3	22.1	8	·	·	2	2	1	1	4	12	11	10	2	4	·	6
V	7	2.4	5.5	2.1	2	2.2	2.5	2.8	7.5	3.1	11.5	3.6	31	4.0	18	3.0	8	3.0	68.6	11.8	29	·	·	·	·	4	1	1	16	18	15	2	5	·	3
VI	2	1.2	3	1.3	2.5	2.2	12.5	2.3	8.5	2.6	9	2.8	27	3.9	11.5	3.2	14	2.6	89.2	56.4	10	·	·	·	11	·	·	3	3	12	8	2	5	·	8
VII	1	2.0	1	1.0	1.5	3.0	2	3.5	13	2.5	16	3.7	42	5.0	6.5	3.7	10	3.7	90.5	24.3	15	·	·	·	8	2	·	2	15	16	15	2	2	·	5
VIII	0.5	3.0	3	1.8	4	1.8	5	1.9	10.5	2.7	18.5	4.8	31	4.0	7.5	2.8	13	3.1	78.9	30.2	10	·	·	·	6	3	·	1	13	14	9	2	9	·	5
IX	1	1.5	9.5	4.7	18	4.9	9.5	2.2	12	3.0	10.5	3.9	18	4.2	15	5.0	10	2.6	14.1	4.2	26	·	·	·	8	·	·	9	7	11	5	·	5	·	2
X	2	2.8	1.5	2.7	23	3.4	16	4.2	16.5	4.4	11.5	3.0	7.5	2.4	6	2.7	9	3.2	39.6	13.6	20	·	·	·	·	2	·	4	9	9	6	2	8	·	·
XI	6	2.0	6.5	2.7	12	2.2	8	2.8	11.5	3.4	10	4.6	14.5	3.9	9.5	2.9	12	2.7	39.4	8.4	13	·	·	10	·	1	·	1	19	14	13	·	9	·	
XII	4	2.1	9	2.2	6.5	1.8	14	2.4	11.5	4.7	4.5	7.4	24	4.7	12.5	3.1	7	3.4	43.5	9.7	12	12	13	24	·	3	·	4	13	14	9	·	4	15	·
Rok	39.5	2.2	64.5	1.7	105	2.3	116	2.9	142.5	3.5	137.5	4.4	281.5	4.2	104.5	3.5	104	3.3	620.8	56.4	10.VI	22	25	85	35	31	4	41	148	157	114	13	73	35	30

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Czarniecka Góra

H_s = 256 m h_w = 10 m

I	1	5.0	10	2.9	·	·	·		22	4.5	5	5.8	23	3.0	20	2.3	12	3.0	32.6	8.3	4	12	14	28	·	·	·	–	–	–	8	·	5	–	
II	·		·	·	·	·	·				17	4.6	26	2.5	27	3.1	14	2.7	50.7	16.0	1	·	·	21	·	·	·	–	–	–	9	3	14	–	
III	7	2.7		·	·	·		·	3	5.7	11	6.2	31	5.6	35	6.7	6	5.5	58.0	12.0	12	–	·	–	·	11	2	–	–	–	15	1	6	–	
IV	4	3.8	8	2.9	12	4.7	15	3.9	10	4.0	8	3.0	12	4.2	14	2.7	7	3.4	31.5	40.5	8	·	·	4		1	·	–	–	–	6	·	2	·	2
V	17	2.4	15	3.0	6	3.3	5	2.6	6	3.0	4	4.2	14	3.1	18	2.9	8	2.7	69.5	25.0	27	·	·	·	1		·	–	–	–	13	1	3	·	2
VI		·	·	·	10	3.1	16	3.2	10	3.2	7	4.4	22	3.4	14	3.3	11	3.0	117.6	32.1	27	·	·	·	10		·	–	–	–	14	4	3	·	9
VII	4	3.5	·	·		·		·	1	4.0	23	4.6	28	3.6	24	3.0	13	3.2	122.5	33.6	30	·	·	·	8	3	1	–	–	–	15	4	3	·	3
VIII	14	3.8	·	·	·	·			·	·	12	3.8	29	3.9	27	3.4	11	3.3	53.2	10.2	12,23	·	·	·	5	2	·	–	–	–	10	2	7	·	2
IX	1	5.0	5	2.2	15	2.5	9	2.9	·	·	6	5.2	17	3.5	22	3.3	15	2.7	44.2	4.3	14	·		1	7	2	·	–	–	–	7	·	6	·	
X	3	3.3	13	2.4	14	2.4	28.5	4.8	14.5	4.3	7	4.3	4	3.8	-		9	3.5	8.5	4.3	14	·	·	1	·	2	·	–	–	–	4	·	6	·	
XI	12	2.9	·	·	9	2.7	10	3.5	14	2.3	11	4.3	21	3.6	2	2.5	11	2.8	90.4	17.5	13	2	·	11	·	·	·	–	–	–	12	4	8	–	
XII	17	3.2	4	5.5	7	2.1	4	3.8	10	2.5	20	4.7	10	3.8	7	2.0	14	3.0	63.7	11.5	11	12	15	24	·	1	·	–	–	–	14	1	2	–	
Rok	80	3.0	56	1.8	73	1.7	87.5	2.1	90.6	2.8	134	4.6	237	3.7	210	2.9	131	3.2	712.4	33.5	30.VII	–	29	–	31	22	3	–	–	–	127	20	65	–	18

Pszczela Wola

$\varphi = 51°07'$ $\lambda = 22°31'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOT. NOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.5	-8.2	7.4	4	-21.8	27	-5.7	-2.4	-5.4	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	5.2	6.2
II	–	–	–	–	2.9	-0.9	9.4	18	-4.8	5	-0.2	2.5	0.6	0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	7.0	7.7
III	–	–	–	–	8.8	1.5	18.7	18	-2.2	23	3.1	7.3	4.4	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.3	5.9	7.4
IV	–	–	–	–	16.2	4.0	24.3	15	-3.5	10	6.9	14.8	8.1	9.5	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	3.1	4.4
V	–	–	–	–	17.1	6.1	25.6	29	0.6	17	10.3	15.6	10.1	11.5	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	5.5	6.5
VI	–	–	–	–	23.8	11.1	30.9	27	3.6	21	16.2	21.9	15.4	17.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.7	5.9	5.9
VII	–	–	–	–	22.5	9.9	29.8	3	6.4	8,9	15.4	20.9	15.2	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.0	5.7	6.2
VIII	–	–	–	–	22.3	11.6	32.7	11	4.7	31	14.7	21.2	15.0	16.5	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.6	5.7	6.2
IX	–	–	–	–	20.9	7.5	29.2	2	-3.2	23	10.4	20.1	12.5	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.7	3.6	4.5
X	–	–	–	–	16.1	5.2	23.2	19	0.6	11	6.9	15.4	9.4	10.3	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.4	4.5	5.2
XI	–	–	–	–	6.7	1.3	14.4	3	-6.1	23	3.2	5.9	3.6	4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.7	7.1	8.1
XII	–	–	–	–	-0.6	-7.5	14.9	5	-22.4	25	-4.5	-2.4	-4.2	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.2	8.2	8.1
Rok	–	–	–	–	12.9	3.5	32.7	11.VIII	-22.4	25.XII	6.4	11.7	7.1	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	5.6	6.4

Chełm Lubelski

$\varphi = 51°07'$ $\lambda = 23°30'$

I	994.7	1013.3	975.0	1021.8	-2.2	-9.1	4.3	4	-24.0	21	-6.4	-3.5	-5.7	-5.3	3.7	4.1	3.9	3.9	89	82	88	86	0.4	0.9	0.5	0.6	6.8	7.3	5.1	6.4
II	996.9	1012.5	969.8	1023.3	2.4	-1.4	8.8	18	-5.6	7	-0.8	1.5	0.4	0.4	5.4	5.9	5.7	5.7	93	86	90	90	0.4	1.0	0.6	0.7	7.6	8.3	7.7	7.9
III	990.3	1008.9	971.9	1016.2	8.2	1.1	18.3	18	-4.4	23	2.7	6.3	4.0	4.2	6.8	6.8	7.1	6.9	90	72	86	83	0.8	3.1	1.2	1.7	8.3	8.1	4.3	6.9
IV	988.7	999.2	978.8	1014.0	15.8	4.4	24.2	7	-3.6	10	6.8	14.1	9.4	9.9	8.0	8.4	8.6	8.3	79	51	71	67	2.2	8.3	3.7	4.7	4.8	5.6	3.1	4.5
V	987.0	995.1	975.7	1012.1	16.7	6.9	25.0	29	1.9	19	10.3	15.1	10.8	11.8	10.6	10.3	11.0	10.6	8.4	6.1	8.4	7.6	2.2	7.6	2.4	4.1	6.9	7.5	5.6	6.7
VI	990.6	1002.1	981.9	1015.3	23.2	11.6	30.7	27	6.1	21	16.1	21.3	16.3	17.5	14.9	14.6	14.8	14.8	8.1	5.9	8.0	7.3	3.6	11.4	4.0	6.3	4.3	6.3	4.3	5.0
VII	989.1	1000.0	975.7	1014.0	22.5	11.5	30.1	3	8.0	20	14.9	20.6	15.4	16.6	14.2	13.6	14.5	14.1	8.4	5.7	8.3	7.5	3.0	11.3	3.2	5.8	5.7	6.6	5.1	5.8
VIII	991.3	1003.3	978.9	1016.2	22.1	12.2	32.7	11	6.4	31	14.7	20.4	15.8	16.7	14.7	14.2	14.7	14.5	8.7	6.0	8.1	7.6	2.3	10.6	3.6	5.5	5.5	6.6	5.4	5.8
IX	994.5	1005.7	983.3	1019.6	20.4	8.8	28.7	6	-1.0	23	10.7	19.1	13.0	14.0	11.6	11.9	12.3	11.9	8.8	5.4	8.0	7.4	1.7	11.0	3.1	5.3	4.4	4.4	2.6	3.8
X	996.2	1006.6	976.5	1021.7	15.5	5.3	24.0	19	-0.6	23	6.5	14.6	9.4	10.0	8.5	9.2	9.0	8.9	8.7	5.7	7.6	7.3	1.3	7.7	2.8	3.9	5.6	4.9	3.5	4.7
XI	989.6	1008.8	977.4	1015.5	6.2	1.2	14.4	3	-6.1	23	2.5	5.2	3.5	3.7	7.0	7.5	7.4	7.3	9.2	8.3	9.1	8.9	0.6	1.7	0.7	1.0	8.7	8.7	7.8	8.4
XII	989.6	1015.7	972.8	1016.3	-1.1	-7.8	14.4	5	-21.3	26	-4.9	-3.0	-4.6	-4.3	4.3	4.6	4.4	4.4	8.7	8.4	8.7	8.6	0.6	1.0	0.6	0.7	8.3	7.6	6.8	7.6
Rok	991.5	1015.7	971.9	1017.1	12.5	3.7	32.7	11.VIII	-24.0	21.I	6.1	11.0	7.3	7.9	9.1	9.3	9.4	9.3	8.7	6.7	8.3	7.9	1.6	6.3	2.2	3.4	6.4	6.8	5.1	6.1

Grabowiec

$\varphi = 51°06'$ $\lambda = 21°23'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.2	10.7	29.9	3	6.0	6	14.8	19.9	14.5	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.2	6.2	6.4
VIII	–	–	–	–	21.9	11.1	31.5	11	6.4	31	14.9	20.7	15.0	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.7	6.0	6.0
IX	–	–	–	–	20.8	7.6	29.1	2	-1.3	23	10.7	19.6	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.3	3.3	4.4
X	–	–	–	–	16.2	5.1	22.9	20	1.4	10	7.0	15.4	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.4	4.2	5.3
XI	–	–	–	–	6.5	0.9	14.8	3	-6.7	23	2.8	5.5	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.9	8.3	8.8
XII	–	–	–	–	–	-7.7	–	–	-23.0	26	-4.8	-2.9	-4.2	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	8.3	7.9
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Namysłów

$\varphi = 51°05'$ $\lambda = 17°43'$

I	–	–	–	–	0.0	-7.4	10.3	4	-21.5	27	-5.8	-4.1	-4.4	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	6.3	0.0	12.3	15	-4.8	6	0.6	5.6	2.3	2.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	10.8	2.0	19.8	10	-5.5	20	2.9	9.8	5.5	5.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	17.7	5.5	26.8	7	-1.1	10	8.1	16.7	10.4	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.3	5.1	5.4
V	–	–	–	–	17.4	6.8	24.6	27	2.7	23	10.3	15.8	10.4	11.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	7.8	7.5
VI	–	–	–	–	24.1	11.2	31.0	27	5.0	21	15.7	22.5	15.8	17.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.6	6.3	5.7
VII	–	–	–	–	21.7	11.0	32.8	3	5.5	11	15.0	20.1	14.6	16.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	7.9	7.7
VIII	–	–	–	–	22.3	11.5	32.0	6	7.0	4	14.5	21.2	15.2	16.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.7	6.1	6.6
IX	–	–	–	–	22.7	9.3	31.2	2	0.7	24	12.5	21.6	13.4	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.4	4.3	4.7
X	–	–	–	–	16.8	6.1	23.4	6	0.6	14	8.3	15.9	10.1	11.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.3	1.3	12.8	2	-5.0	22	2.0	6.4	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	0.4	-7.1	16.3	5	-24.6	25	-4.4	-1.1	-3.3	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	14.0	4.2	32.8	3.VII	-24.6	25.XII	6.6	12.8	7.8	8.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Pszczela Wola H_s = 195 m h_w = 18 m 1961

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr v≥10	Wiatr v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	⊼
I	3	1.8	4	1.8	1	1.0	3.5	2.1	19.5	2.1	18	1.9	17	1.9	3	1.8	24	1.4	45.7	4.4	31	12	14	27	·	·	·	5	10	9	4	·	2	22	–
II	·	·	1	1.0	4.5	1.1	8.5	1.1	22	1.9	13	1.2	17	1.0	1	1.0	17	1.1	13.5	4.1	11	·	1	17	·	·	·	2	18	8	4	·	6	6	–
III	·	·	·	·	·	·	·	·	4.5	1.9	15.5	2.4	63	2.5	5	2.9	5	2.3	37.6	9.7	28	·	·	9	·	·	·	1	14	15	8	·	4	3	–
IV	2	2.0	7	1.8	9	2.5	6	3.4	12.5	1.6	13.5	1.4	12.5	2.8	3.5	1.7	24	1.6	42.5	11.8	1	·	·	3	·	·	·	6	4	6	6	2	·	·	–
V	·	·	·	·	3	1.0	6.5	2.0	11.5	1.5	5.5	1.0	24.5	1.4	9	1.2	33	0.9	53.2	10.1	9	·	·	·	2	·	·	·	9	16	14	1	·	·	–
VI	·	·	1.5	3.0	6.5	2.2	8.5	2.0	6.5	1.6	3.5	1.6	24.5	1.9	2	1.5	37	1.1	37.4	10.3	11	·	·	·	11	·	·	2	8	9	6	1	·	·	–
VII	3	1.3	1	1.0	·	·	1	1.0	7.5	2.0	13.5	2.0	27.5	1.3	5.5	1.4	34	1.0	71.8	20.8	29	·	·	·	8	·	·	4	7	15	11	3	·	·	–
VIII	·	·	·	·	1	2.0	·	·	7	1.4	16	1.9	35	2.1	3	1.8	31	1.3	34.9	13.4	12	·	·	·	6	·	·	2	6	14	7	1	1	·	–
IX	0.5	2.0	2.5	1.2	3	1.7	5	1.6	7	1.2	16.5	2.0	16.5	1.8	3	1.3	36	1.0	11.0	5.0	14	·	·	3	8	·	·	11	5	7	2	·	2	·	–
X	0.5	3.0	3	1.7	15	2.9	19	2.7	11.5	2.0	1	2.0	7.5	1.7	0.5	3.0	35	1.5	4.4	2.2	14	·	·	·	·	·	·	8	7	4	2	·	6	·	–
XI	3	1.8	5.5	2.2	9.5	2.7	9	1.7	10	1.7	5.5	1.7	23	1.8	1.5	1.0	23	1.4	36.9	13.3	13	·	1	12	·	·	·	2	20	10	7	1	3	·	–
XII	7.5	2.5	5	1.1	1	2.0	5.5	1.4	11.5	1.7	13	2.5	7.5	2.2	15	2.0	27	1.3	21.1	7.2	7	10	17	25	·	·	·	1	18	10	6	·	1	23	–
Rok	19.5	1.2	30.5	1.2	53.5	1.6	72.5	1.6	131	1.7	134.5	1.8	275.5	1.9	52	1.7	326	1.3	380.0	20.8	29.VII	22	33	96	35	·	·	44	126	123	77	9	25	54	–

Chełm Lubelski H_s = 208 m H_b = 209,6 m h_w = 12 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr v≥10	Wiatr v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	⊼
I	5	3.2	4.5	2.9	5	2.0	26.5	3.2	16.5	3.1	18	6.0	7	6.0	9.5	4.9	1	4.0	13.5	5.1	31	13	16	31	·	2	1	3	10	13	5	·	4	31	:
II	3	2.7	2	2.2	3.5	2.4	20	3.7	15.5	3.3	13	4.3	11	4.4	7	4.1	9	3.3	6.0	0.9	28	·	3	17	·	·	·	1	17	12	·	·	6	7	·
III	3	4.7	·	·	·	·	1	1.0	8.5	3.5	24	6.4	36.5	6.8	18	7.4	2	6.2	28.7	6.1	18	·	·	10	·	12	1	1	8	18	11	·	1	1	1
IV	3	3.5	5.5	3.5	19.5	4.2	24	4.2	11.5	3.5	6.5	6.4	6.5	6.7	6.5	6.6	7	4.2	48.4	16.1	16	·	·	2	·	6	·	6	4	10	5	3	1	·	2
V	3.5	3.4	1	4.0	17	2.4	22	2.8	11.5	3.6	13.5	4.3	8.5	5.5	8	4.1	8	3.2	53.7	22.1	30	·	·	·	·	·	·	1	12	15	7	2	1	·	2
VI	4	3.2	2.5	3.0	11	2.7	27.5	3.0	9.5	2.5	12.5	4.7	10	4.9	4	3.8	9	3.1	85.3	47.1	12	·	·	·	8	·	·	2	2	12	10	3	·	·	9
VII	2	2.8	2	1.8	3	2.0	16.5	2.6	29	2.9	16.5	4.5	12	4.9	6	2.8	6	3.2	81.7	22.5	30	·	·	·	8	2	1	3	8	13	9	3	1	·	7
VIII	5.5	4.5	3	2.7	5	2.2	13.5	2.5	17	3.7	18.5	5.0	16	5.2	10.5	4.1	4	3.9	53.7	23.3	12	·	·	·	7	2	·	3	9	11	6	2	1	·	4
IX	·	·	6	2.2	17	2.2	12.5	2.0	17	2.5	12	5.5	17.5	4.8	4	5.0	4	3.2	9.4	5.4	14	·	·	1	7	3	·	14	6	7	3	·	3	·	1
X	4	2.8	1	2.0	14	3.6	54	4.7	8	3.9	2.5	4.4	6.5	4.4	3	3.3	·	4.3	8.2	4.1	31	·	·	1	·	1	·	10	8	4	3	·	6	·	·
XI	2	2.0	2.5	3.6	10	4.4	29	4.3	16.5	3.0	13.5	6.1	12	5.0	3.5	4.9	1	4.3	43.0	11.9	13	·	2	13	·	·	·	1	20	17	9	1	7	1	·
XII	12.5	4.4	10	3.0	6	3.8	17	3.3	11	3.0	17.5	6.3	8	5.7	7	4.4	4	4.1	32.3	9.2	7	11	18	25	·	4	·	1	17	14	7	·	4	25	·
Rok	47.5	3.1	40	2.6	111	2.7	263.5	3.1	171.5	3.2	168	5.3	151.5	5.4	87	4.6	55	3.9	463.9	23.3	12.VIII	24	39	100	30	32	3	46	121	146	75	14	35	65	26

Grabowiec H_s = 210 m h_w = 15 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr v≥10	Wiatr v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	⊼
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	2.5	5.6	3.5	4.0	0.5	1.0	3.5	2.5	10	3.2	14	3.0	35	3.3	12	3.5	12	2.8	130.2	30.5	30	·	·	·	8	1	1	3	9	14	13	5	·	·	5
VIII	3	3.2	2	4.8	1.5	4.0	·	·	8	3.8	16	4.0	25.5	3.1	19	3.2	18	2.8	38.6	12.0	12	·	·	·	6	·	·	3	7	12	10	1	1	·	2
IX	·	·	1.5	2.7	10.5	1.9	4	2.4	11	2.3	10.5	4.1	16.5	4.1	7	4.2	29	2.2	6.9	3.5	14	·	·	2	7	·	·	10	7	6	2	·	3	·	·
X	2	2.2	3.5	2.3	12	2.3	24	5.1	20	4.0	8	2.8	8	3.9	6.5	3.5	9	3.4	3.4	2.2	14	·	·	·	·	2	·	6	6	2	2	·	2	·	·
XI	8.5	4.0	1.5	3.0	7	4.9	9.5	3.4	20	2.8	9	2.8	14.5	3.7	8	3.4	12	3.0	64.0	13.1	4	·	1	10	·	·	·	1	22	13	13	2	6	·	·
XII	7.5	6.1	3.5	3.7	4	2.2	8.5	2.8	17	4.0	9.5	4.8	15	4.7	18	4.8	10	3.9	39.3	14.8	6	10	–	25	·	2	·	2	20	11	8	2	4	22	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Namysłów H_s = 151 m h_w = 12,6 m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	Temp. Min<-10°	Temp. Max<0°	Temp. Min<0°	Temp. Max>25°	Wiatr v≥10	Wiatr v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	≡	⊞	⊼
I	2	1.5	5.5	2.0	10.5	1.4	10	1.8	13	2.1	19.5	1.9	12.5	1.8	6	2.1	14	1.6	21.3	8.1	14	11	12	27	·	·	·	–	–	11	6	·	1	20	:
II	0.5	1.0	·	·	2.5	1.2	13.5	1.7	9	2.1	14.5	2.4	17	2.3	20	2.5	7	2.0	41.9	17.8	9	·	·	14	·	1	1	–	–	15	10	1	5	1	
III	0.5	3.0	·	·				·	1.5	2.7	9.5	4.3	57.5	4.3	20	5.4	4	4.3	29.1	7.5	14	·	·	8	·	11	2	–	–	15	10	·	4	1	
IV	·	·	3	2.3	20	2.0	20.5	2.3	8	1.2	6	2.1	13.5	2.8	10	2.4	9	2.0	42.2	23.6	8	·	·	1	2	·	·	–	–	9	7	1	1	·	3
V	1	2.0	2.5	2.0	3	1.2	10	1.4	5.5	1.3	10	2.1	17	2.0	25	2.2	19	1.5	65.5	25.2	29	·	·	·	·	1	1	–	–	15	10	1	1	·	2
VI	·	·	1	1.0	4	1.8	11.5	1.4	6.5	1.4	11.5	1.8	26	1.9	12.5	2.4	17	1.5	58.4	18.0	3	·	·	·	11	·	·	–	–	11	9	2	1	·	5
VII	·	·	·	·	·	·	3	2.3	6.5	1.3	20	1.9	37.5	2.2	14	4.0	12	2.1	116.0	31.1	28	·	·	·	7	1	·	–	–	19	14	3	2	·	6
VIII	·	·	1	1.0	·	·	3	1.0	10	1.6	28.5	2.0	19.5	2.3	16	2.7	15	1.8	73.9	19.6	9	·	·	·	6	·	·	–	–	15	11	2	1	·	5
IX	·		1.5	1.7	18	2.2	8.5	1.4	14.5	1.1	9.5	1.3	16	1.8	5	1.8	17	1.3	18.5	5.8	6	·	·	·	8	·	·	–	–	7	4	·	2	·	
X	0.5	3.0	3.5	1.9	13.5	1.9	35	2.2	3.5	1.0	9.5	1.5	6	2.1	8.5	1.9	13	1.7	39.0	14.2	19	·	·	·	·	·	·	–	–	7	5	2	10	·	·
XI	4	1.5	3	2.0	10.5	1.8	6	1.9	5	2.1	26	2.0	14.5	1.7	9	1.9	12	1.6	58.3	27.9	13	·	·	7	·	·	·	–	–	16	10	1	4	·	·
XII	1.5	2.3	5	2.7	10.5	1.9	18	1.6	6	2.4	13	4.3	13.5	2.5	15.5	3.1	10	2.3	51.5	12.4	11	11	13	24	·	2	·	–	–	13	10	1	2	16	·
Rok	10	1.2	26	1.4	92.5	1.3	139	1.6	89	1.7	177.5	2.3	250.5	2.3	161.5	2.7	149	2.0	615.6	31.1	28.VII	22	25	81	34	16	4	–	–	153	106	14	34	38	21

Przedbórz

$\varphi = 51°05'$ $\lambda = 19°53'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.7	-8.6	6.8	4	-23.3	27	-6.7	-2.1	-5.2	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	5.0	5.3	6.3
II	–	–	–	–	4.6	-0.8	12.3	18	-5.4	6	0.2	3.5	1.0	1.4	–	–	–	–	–	–	–	–	–	–	–	–	10.0	7.2	8.0	8.3
III	–	–	–	–	8.9	2.1	18.6	10	-3.4	20	3.1	7.4	5.1	5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.8	6.9	6.5	7.4
IV	–	–	–	–	16.7	4.5	25.2	7	-3.4	10	7.4	15.5	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.2	4.7	4.8
V	–	–	–	–	17.5	6.3	25.4	31	0.8	19	9.3	16.0	10.7	11.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.1	6.5	7.0
VI	–	–	–	–	23.7	11.5	31.6	27	5.4	21	16.1	22.1	16.2	17.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.3	4.1	4.7
VII	–	–	–	–	20.7	11.2	30.6	3	5.8	8	14.3	19.2	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	6.6	7.1
VIII	–	–	–	–	21.3	11.9	29.7	6	6.7	30	14.4	20.1	15.3	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.3	5.8	6.0
IX	–	–	–	–	20.9	8.7	28.8	17	-0.8	24	11.1	19.6	13.5	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.1	3.8	3.7	4.2
X	–	–	–	–	16.5	6.4	22.5	20	4.9	31	8.1	15.4	10.4	11.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.7	3.7	4.5
XI	–	–	–	–	6.7	–	13.9	3	–	–	2.2	5.2	3.3	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.3	7.7	8.3
XII	–	–	–	–	-0.6	-8.3	16.5	5	-25.1	26	-5.2	-2.7	-4.9	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	6.7	7.7
Rok	–	–	–	–	13.0	–	31.6	27.VI	-25.1	26.XII	6.2	11.6	7.4	8.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	5.8	6.4

Laskowice Oławskie

$\varphi = 51°03'$ $\lambda = 17°21'$

I	–	–	–	–	0.5	-6.9	10.1	4	-22.2	27	-4.8	-0.3	-3.6	-3.1	4.1	4.7	4.3	4.4	84	74	82	80	0.8	1.6	0.9	1.1	6.1	6.4	6.6	6.4
II	–	–	–	–	6.7	-0.3	12.2	15	-6.3	6	1.0	5.5	2.4	2.8	6.1	6.9	6.5	6.5	92	76	89	86	0.6	2.2	0.8	1.2	7.6	6.5	5.0	6.4
III	–	–	–	–	10.8	2.7	19.8	10	-3.6	20	4.3	9.2	6.0	6.4	6.9	7.6	7.3	7.3	82	66	80	76	1.8	4.3	2.2	2.7	7.7	7.1	5.7	6.8
IV	–	–	–	–	17.3	5.2	25.8	7	-1.8	10	8.6	16.4	10.3	11.4	9.6	10.2	10.0	9.9	84	54	79	72	1.8	9.1	2.8	4.6	5.8	5.5	5.2	5.5
V	–	–	–	–	16.7	6.9	23.0	26	2.6	12	10.3	15.2	10.6	11.7	10.9	10.7	11.1	10.9	87	62	86	78	1.7	7.0	1.9	3.5	7.8	7.5	7.5	7.6
VI	–	–	–	–	23.0	11.4	28.8	25	5.7	21	16.1	21.7	16.4	17.6	15.2	15.0	15.6	15.3	83	59	83	75	3.2	11.4	3.4	6.0	5.0	6.1	4.5	5.2
VII	–	–	–	–	21.4	11.5	32.3	3	4.5	8	15.2	20.0	15.3	16.4	14.1	13.1	14.0	13.7	81	58	80	73	3.4	10.8	3.7	6.0	6.6	7.2	6.5	6.8
VIII	–	–	–	–	22.0	11.9	31.3	6	6.2	14	15.0	20.6	15.8	16.8	14.9	15.2	15.4	15.2	87	63	85	78	2.4	9.7	2.9	5.0	6.9	7.3	6.2	6.8
IX	–	–	–	–	21.8	9.6	29.9	2	2.6	24	12.0	21.1	14.0	15.3	12.6	13.6	13.4	13.2	89	55	82	75	1.7	12.2	2.9	5.6	5.0	4.6	4.1	4.6
X	–	–	–	–	16.2	6.3	21.9	5,6	1.4	13	7.7	15.5	9.9	10.8	9.6	11.0	10.4	10.3	91	64	86	80	1.1	7.0	1.9	3.3	7.4	6.8	5.1	6.4
XI	–	–	–	–	6.9	1.3	13.0	2	-5.9	22	2.7	6.1	3.7	4.0	7.0	7.7	7.4	7.4	91	80	91	87	0.7	1.9	0.8	1.1	8.4	8.4	7.7	8.2
XII	–	–	–	–	0.4	-7.1	17.0	5	-22.6	25	-4.3	-1.3	-3.7	-3.2	4.6	5.0	4.7	4.8	86	81	86	84	0.8	1.4	0.8	1.0	7.0	6.2	5.3	6.2
Rok	–	–	–	–	13.6	4.4	32.3	3.VII	-22.6	25.XII	7.0	12.5	8.1	8.9	9.6	10.1	10.0	9.9	86	66	84	79	1.6	6.6	2.1	3.4	6.8	6.6	5.8	6.4

Suchedniów

$\varphi = 51°03'$ $\lambda = 20°50'$

I	–	–	–	–	-0.4	-9.3	6.8	4	-24.6	26	-6.4	-1.7	-5.5	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.4	4.8	6.0
II	–	–	–	–	4.1	-1.8	12.5	18	-9.3	5	-0.4	3.2	0.5	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	6.9	7.8
III	–	–	–	–	9.2	–	19.5	10	–	–	3.2	7.6	4.6	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	6.2	7.3
IV	–	–	–	–	16.1	–	25.5	15	–	–	6.8	14.8	7.5	9.2	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.6	3.6	4.2
V	–	–	–	–	17.1	–	25.2	27	–	–	9.8	15.3	9.5	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.4	6.8	7.1
VI	–	–	–	–	23.7	10.2	32.0	27	3.0	21	16.5	21.9	15.4	17.3	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.9	5.0	5.2
VII	–	–	–	–	21.8	9.4	31.4	3	3.9	6	14.8	20.2	14.1	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.8	5.9	6.2
VIII	–	–	–	–	22.1	10.9	31.4	11	3.9	31	14.6	20.9	14.3	16.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.6	4.3	5.7
IX	–	–	–	–	21.1	6.7	30.1	3	-2.6	22,23	9.9	19.9	11.0	13.0	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.6	4.2	4.6
X	–	–	–	–	16.0	3.9	22.7	20	-0.7	6	5.8	15.1	9.1	9.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.3	3.0	4.5
XI	–	–	–	–	6.8	-0.9	14.6	3	-9.4	23	2.3	5.8	3.2	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.6	6.5	7.5
XII	–	–	–	–	-0.5	-8.9	15.9	5	-26.9	26	-5.4	-2.2	-5.4	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	6.8	6.5	7.1
Rok	–	–	–	–	13.1	–	32.0	27.VI	-26.9	26.XII	6.0	11.7	6.5	7.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.4	5.3	6.1

Krasnystaw

$\varphi = 50°59'$ $\lambda = 23°10'$

I	–	–	–	–	-1.5	-10.3	7.0	4	-25.9	27	-6.5	-2.5	-6.1	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	5.9	4.7	6.0
II	–	–	–	–	3.1	-1.6	8.9	18	-6.5	7	-0.6	2.3	0.6	0.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	7.4	8.1
III	–	–	–	–	8.8	1.1	18.3	18	-3.7	23	3.1	7.2	4.3	4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.1	4.2	6.9
IV	–	–	–	–	16.3	4.1	25.6	7	-4.2	10	7.0	15.1	8.5	9.8	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.7	2.7	4.3
V	–	–	–	–	17.4	6.4	25.6	29	0.6	17	10.3	15.9	10.3	11.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.2	5.2	6.8
VI	–	–	–	–	24.6	10.8	32.2	27	4.9	21	16.6	22.7	16.3	18.0	–	–	–	–	–	–	–	–	–	–	–	–	4.1	6.4	4.4	5.0
VII	–	–	–	–	23.3	10.8	31.5	13	6.4	9	16.4	21.4	15.8	17.4	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.7	6.5	6.6
VIII	–	–	–	–	22.6	11.8	33.1	11	4.9	31	15.7	21.3	15.7	17.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.6	5.6	5.9
IX	–	–	–	–	21.0	7.7	28.6	3	-2.9	23	10.3	20.2	11.9	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.2	3.1	4.6
X	–	–	–	–	16.3	4.8	22.1	19	-1.3	12	6.7	15.5	9.3	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.8	4.3	4.8
XI	–	–	–	–	6.7	1.3	15.6	3	-7.5	23	3.1	5.9	3.4	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.1	7.6	8.2
XII	–	–	–	–	-0.9	-8.9	15.6	5	-23.4	17,25	-4.9	-2.4	-5.0	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.9	7.2	7.8
Rok	–	–	–	–	13.1	3.2	33.1	11.VIII	-25.9	27.1	6.4	11.9	7.1	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	5.2	6.2

Przedbórz

$H_s = 235\,m$ $h_w = 10{,}5\,m$ I-V, $13\,m$ VI-XII 1961

MIESIĄC	ROZKŁAD WIATRU [%D, %nD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min <-10°	Max <0°	Min <0°	Max >25°	Wiatr v >10	>15	●	●	Opad R ≥0.1	≥1.0	≥10.0	▬	▦	≈
I	5	4.4	4	3.8	2	3.5	2.1	4.1	8	2.8	4	3.8	2	2.5	11	3.4	36	2.2	16.5	6.5	14	13	14	28	·	1	·	–	–	6	5	·	2	17	–
II	3	5.0	3	2.7	4	4.0	1.5	3.5	1.0	3.3	2.5	3.2	7	2.4	5	2.4	12	2.8	33.7	10.1	1	·	1	17	·	·	·	–	–	9	8	1	–	1	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	44.7	6.3	12	·	·	7	·	–	–	–	–	18	14	·	3	·	–
IV	1.0	3.4	6	4.7	2.0	5.2	7	4.0	9	3.0	6	3.7	11	4.9	4	4.2	17	3.5	37.0	15.2	8	·	·	4	2	·	·	–	–	6	6	2	1	·	–
V	1.2	3.8	8	2.8	3	3.0	6	3.7	5	2.8	1.3	4.2	1.5	2.7	8	4.0	23	2.6	33.2	5.9	9	·	·	·	1	·	·	–	–	13	11	·	1	·	–
VI	2	2.5	8	3.2	9	3.3	8	3.0	1.3	2.6	1.4.5	4.6	1.6	3.4	6.5	3.5	13	2.9	87.0	37.8	27	·	·	·	9	·	·	–	–	1.4	10	1	3	·	–
VII	1	5.0	·	·	1	3.0	6	3.0	1.8.5	3.6	2.2.5	4.0	2.4	3.5	8	8.5	12	3.2	1.45.2	29.9	31	·	·	·	7	·	·	–	–	1.7	1.5	6	·	·	–
VIII	1.5	4.3	3	3.0	0.5	6.0	4	4.0	1.9.5	3.9	20	3.8	22	4.1	9.5	3.0	13	3.3	52.3	15.7	12	·	·	·	7	·	·	–	–	11	10	2	2	·	–
IX	4	3.0	4	2.2	9	3.6	1.3	3.5	1.7	3.7	1.6.5	3.8	4.1	4.0	1.5	4.7	1.4	3.1	17.4	7.5	6	·	·	3	7	·	·	–	–	5	4	·	3	·	–
X	1	5.0	1	3.0	3.7	6.4	1.4	3.8	1.3	3.0	9	4.0	7	3.7	·	·	11	4.3	2.1	0.8	15	·	·	·	·	2	·	–	–	5	·	·	1.0	·	–
XI	8	2.6	·	·	1.2	4.0	8	2.8	3.2.5	3.4	6.5	3.9	1.1	4.3	2	5.0	1.0	3.2	88.1	17.4	4	·	·	·	·	·	·	–	–	1.7	1.0	4	1.0	1	–
XII	9	4.1	4	4.5	4	1.8	1.1	3.5	1.5	4.7	1.5	4.9	8	4.2	9	4.7	1.8	3.5	37.4	14.8	11	11	15	26	·	2	·	–	–	11	8	1	3	24	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	594.6	37.8	27.VI	24	30	–	33	–	–	–	–	132	101	17	–	43	–

Laskowice Oławskie

$H_s = 135\,m$ $h_w = 13{,}5\,m$

I	0.5	2.0	7	3.4	12.5	3.2	18.5	3.1	23.5	3.7	17.5	3.1	7.5	3.0	4	3.5	2	3.2	49.0	8.7	14	12	11	24	·	·	·	5	12	15	4	·	4	17	·
II	2.5	3.4	0.5	2.0	6	2.1	2.1.5	3.4	1.5.5	3.5	8.5	3.4	1.6.5	3.9	11	4.9	2	3.5	3.5.3	11.9	9	·	·	1.5	·	2	1	4	12	17	9	1	5	4	·
III	5.5	3.5	1	1.0	1	1.0	1	1.0	2.5	2.6	1.8.5	4.5	3.7	5.8	2.6.5	4.8	·	4.9	2.1.1	5.4	14	·	·	6	·	5	1	3	13	14	9	·	2	1	·
IV	8.5	1.8	6	3.2	2.2.5	3.3	1.3.5	4.3	1.2	3.5	9.5	4.0	7.5	3.3	8.5	4.4	2	3.4	7.1.6	2.5.8	8	·	·	1	1	4	·	5	8	10	6	3	1	·	6
V	1.3.5	2.1	4	2.6	2.5	3.2	2.5	2.8	9.5	2.6	1.2.5	2.8	2.0	3.6	2.5.5	3.1	3	2.8	6.5.1	2.5.5	29	·	·	·	·	·	·	2	1.6	1.8	1.2	1	2	·	7
VI	5	2.4	3	2.8	5.5	2.9	9	3.3	1.2.5	2.7	1.1.5	2.3	2.2.5	3.1	1.6	3.3	5	2.8	6.4.3	1.9.1	3	·	·	·	9	1	·	5	5	1.4	1.0	3	2	·	8
VII	4	1.8	1.5	1.7	0.5	3.0	6	3.7	9.5	2.8	1.9.5	3.3	3.9	3.8	1.1	3.7	2	3.4	8.2.3	2.4.6	2.8	·	·	·	7	4	·	3	1.2	1.6	9	2	·	·	3
VIII	2.5	5.2	2	1.0	8	1.9	4.5	2.3	9	3.1	2.1	3.6	2.7	3.4	1.2	3.4	7	3.0	1.0.5.0	4.0.8	1.1	·	·	·	7	4	·	1	1.1	1.4	1.2	3	1	·	5
IX	2	2.0	4.5	1.4	1.7.5	3.6	1.1.5	3.2	1.9	2.4	1.1	3.5	1.4.5	3.8	6	3.6	4	3.0	1.3.2	4.8	26	·	·	·	8	2	·	1.0	6	8	4	·	1	·	2
X	0.5	6.0	·	·	2.0.5	5.0	2.4	3.8	1.6.5	3.3	8.5	4.6	9	2.1	1.0	3.6	4	3.7	4.0.6	1.1.2	20	·	·	·	·	5	·	5	1.4	7	6	2	5	·	·
XI	8.5	3.4	5	4.6	6	5.3	1.2.5	2.8	1.5	3.0	1.6	4.6	1.5	2.9	9	3.7	3	3.5	3.8.1	7.8	5	·	·	9	·	2	·	1	1.8	1.8	1.1	·	6	·	·
XII	5	4.0	8	3.8	3	3.0	1.6	3.4	1.1	3.4	1.2.5	4.7	1.0	6.1	2.3.5	4.5	4	4.0	3.6.8	8.0	11	12	14	22	·	6	·	7	1.3	1.5	1.0	·	4	1.5	·
Rok	5.8	3.1	4.2.5	2.3	1.0.5.5	3.1	1.4.0.5	3.1	1.5.5.5	3.0	1.6.6.5	3.7	2.2.5.5	3.7	1.6.3	3.9	3.8	3.4	5.9.2.4	4.0.8	11.VIII	24	2.5	7.7	3.2	3.5	2	5.1	1.4.0	1.6.6	1.0.2	1.5	3.3	3.7	3.1

Suchedniów

$H_s = 272\,m$ $h_w = 13{,}5\,m$

I	3	2.3	1	2.5	1	2.0	2.5	2.0	1.0	3.6	1.7.5	2.7	1.6.5	2.1	3.5	1.6	3.8	1.5	3.1.8	7.0	5.3.1	11	14	2.8	·	·	·	5	9	12	6	·	·	2.0	·
II	1	3.0	·	·	2.5	1.4	2	1.5	1.2.5	3.1	2.6	3.0	1.7.5	2.5	4.5	3.7	1.8	2.2	2.5.7	5.8	9	·	·	2.0	·	·	·	1	1.7	1.5	9	·	·	3	·
III	0.5	2.0	·	·	1	8.0	2	6.0	1	4.0	1.4.5	4.6	5.2	4.3	1.0	4.6	1.2	3.9	4.5.0	7.0	12	·	·	–	·	2	·	1	1.4	2.0	1.5	·	1	2	·
IV	5	2.9	4	3.9	1.0.5	5.0	4.0	5.0	7	2.9	7.5	3.9	1.3.5	3.6	6.5	2.7	2.6	2.7	3.6.3	1.0.4	1	·	·	–	1	·	·	9	5	7	6	1	·	·	2
V	7.5	2.1	1	3.0	4	2.8	2	2.2	7.5	2.3	6	4.1	2.1	3.0	9	2.4	3.5	1.7	7.8.8	4.5.5	2.8	·	·	–	1	·	·	·	1.4	1.3	1.2	1	·	·	2
VI	0.5	3.0	3	3.7	4	3.4	3	3.0	7.5	2.7	2.5	2.0	3.0	2.7	4.5	2.7	3.5	1.7	9.0.2	2.2.9	8	·	·	·	9	·	·	4	6	1.0	1.0	3	·	·	7
VII	·	–	·	·	0.5	2.0	2.5	4.4	2	3.0	1.8	2.7	3.5.5	2.8	5.5	2.8	2.9	2.0	1.0.9.5	2.3.8	3.0	·	·	·	8	·	·	3	8	1.5	1.3	5	·	·	5
VIII	1.5	2.0	2	3.0	1	3.5	0.5	4.0	1.5	2.0	7	3.6	3.4.5	3.2	6	2.8	3.9	1.8	6.7.8	2.4.6	11	·	·	·	7	·	·	3	7	1.2	1.1	2	·	·	2
IX	2.5	2.6	1.5	3.0	4	2.2	2.5	2.8	2.5	2.4	6.5	2.8	2.2	3.1	2.5	3.2	4.6	1.4	9.6	4.2	14	·	·	3	·	1	1	9	7	5	2	·	2	·	·
X	1	1.5	1	2.0	1.4	3.8	1.2.5	5.2	8.5	6.6	9.5	1.9	1.0.5	2.2	4	2.1	3.2	2.4	5.1	3.4	14	·	·	3	·	1	1	9	7	5	2	·	2	·	·
XI	3	2.0	2.5	2.4	1.0	3.0	5.5	2.6	6	2.6	9.5	2.5	2.3.5	2.1	7	2.2	2.3	1.8	7.8.1	2.0.3	13	·	1	1.2	·	·	·	3	1.8	1.4	1.2	3	2	2	·
XII	9	3.4	3.5	2.3	2	2.0	·	·	4	2.4	1.2.5	3.0	1.7.5	2.9	9.5	3.0	3.5	1.8	3.4.7	1.1.1	11	13	16	2.5	·	·	·	2	1.6	1.6	1.0	1	3	2.2	·
Rok	3.4.5	2.2	1.9.5	2.2	5.4.5	3.3	4.5	3.2	7.0	3.1	1.3.7	3.1	2.9.4	2.9	7.2.5	2.8	3.6.8	2.1	6.1.2.6	4.5.5	2.8.V	24	3.1	–	3.4	3	1	5.2	1.3.1	1.4.9	1.0.9	1.6	9.3	4.9	1.8

Krasnystaw

$H_s = 190\,m$ $h_w = 12\,m$

I	6	1.5	7	1.0	2.5	1.0	1.2	1.3	2.7.5	1.5	1.5.5	2.3	7.5	1.9	1.5	1.7	·	1.6	2.0.8	5.6	14	14	13	3.1	·	·	·	3	1.2	1.2	9	·	4	3.1	·
II	2	1.0	2	1.0	5	1.6	8	1.6	1.5	1.6	1.5.5	1.6	1.9	1.2	1.7.5	1.2	·	1.4	1.6.9	7.0	1	·	·	2.1	·	·	·	2	2.0	9	4	·	1.0	1.1	·
III	1.5	1.0	·	·	·	·	2	1.0	6	2.3	2.2.5	2.2	3.5.5	2.7	2.5.5	2.3	·	2.4	2.6.8	6.2	2.8	·	·	8	·	1	·	3	1.1	1.7	6	·	4	2	1
IV	5	1.8	1.1.5	1.7	1.6	2.3	8	2.6	1.4	1.5	9.5	2.3	1.2	2.5	1.4	1.5	·	2.0	4.4.6	1.2.6	1.6	·	·	3	2	·	·	8	4	6	6	3	2	·	3
V	1.0	1.2	9	1.2	7.5	1.6	4	1.9	1.0.5	1.8	8.5	1.9	1.7.5	1.5	2.6	1.4	·	1.5	3.6.1	1.1.8	1.4	·	·	·	3	·	·	·	1.1	1.3	8	1	2	·	2
VI	3.5	1.1	6	1.4	9.5	1.6	7.5	1.7	1.0	1.3	1.6	2.2	1.2.5	1.7	2.5	1.4	·	1.6	6.3.3	1.0.8	1.4	·	·	·	1.5	·	·	6	3	1.2	1.2	1	·	·	8
VII	1.5	1.3	3	1.0	·	·	1.5	1.3	9.5	1.5	2.7	1.6	2.5.5	1.4	2.5	1.3	·	1.4	8.4.1	2.3.2	2.9	·	·	·	9	·	·	2	1.0	1.9	9	3	·	·	7
VIII	7.5	1.0	0.5	1.0	3.5	1.3	3.5	1.3	3.5	1.1	2.8.5	1.8	1.5	1.7	3.1	1.3	·	1.5	6.6.4	2.6.5	1.2	·	·	·	7	·	·	3	1.0	1.0	6	3	·	·	4
IX	4.5	1.2	1.3.5	1.2	5.5	1.3	8.5	1.2	4.5	1.6	2.3.5	1.7	1.4	1.6	1.6	1.6	·	1.5	1.7.0	1.0.2	1.4	·	·	2	6	·	·	1.0	7	7	5	1	·	·	·
X	2	1.2	8	1.5	2.0.5	2.7	2.5	2.2	1.3.5	1.7	8	1.6	2	1.2	1.4	1.2	·	1.9	1.3.5	7.0	3.0	·	·	1	·	·	·	1.1	9	3	3	·	7	·	·
XI	4	1.6	3	2.5	1.0	2.5	1.2.5	2.2	1.4.5	1.3	1.9	1.7	1.3.5	1.8	1.3.5	1.2	·	1.8	–	–	–	·	·	1.2	·	1	·	1	2.0	–	–	–	–	·	·
XII	1.1	1.8	5.5	1.2	4	1.5	9.5	1.2	1.1	2.1	2.1	2.2	9.5	1.6	2.1.5	1.5	·	1.7	–	–	–	11	18	2.7	·	·	·	1	1.8	–	–	–	4	–	·
Rok	5.8.5	1.3	6.9	1.2	8.4	1.4	4.0.2	1.6	1.3.8.5	1.6	2.1.4.5	1.9	1.8.3.5	1.7	2.4.4	1.5	·	1.7	–	–	–	2.5	3.1	1.0.5	4.2	2	·	5.0	1.3.5	–	–	–	–	–	2.5

Uwaga. Obserwator nie notował ciaz.

Wojcieszów Górny

$\varphi = 50°57'$ $\lambda = 15°55'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.1	-6.6	7.2	31	-18.4	18.27	-4.3	0.1	-2.8	-2.4	4.0	4.4	4.2	4.2	82	68	78	76	0.9	2.0	1.1	1.3	5.5	5.2	5.9	5.5
II	–	–	–	–	6.9	-0.4	14.8	18	-8.3	6	1.2	5.4	2.0	2.6	5.9	6.4	6.1	6.1	88	71	85	81	0.8	2.8	1.1	1.6	6.8	5.9	4.6	5.8
III	–	–	–	–	10.1	2.0	20.1	10	-6.5	20	3.9	8.5	5.7	6.0	6.4	6.7	6.7	6.6	79	63	74	72	1.9	4.8	2.8	3.2	6.0	6.5	5.6	6.0
IV	–	–	–	–	15.9	5.0	24.7	7	-1.0	10	7.5	14.6	8.8	9.9	8.8	9.2	9.3	9.1	83	57	82	74	1.8	8.1	2.2	4.0	5.1	4.8	3.6	4.5
V	–	–	–	–	14.4	5.8	21.8	26	2.0	13	8.6	12.8	8.6	9.6	10.1	10.0	10.1	10.1	89	69	90	83	1.3	5.1	1.2	2.5	7.7	7.6	5.5	6.9
VI	–	–	–	–	21.7	10.2	28.2	25	4.6	17	13.9	20.0	14.5	15.7	13.6	14.3	14.3	14.1	85	62	85	77	2.5	9.5	2.4	4.8	5.1	5.6	4.2	5.0
VII	–	–	–	–	19.4	10.3	30.3	3	4.4	8	13.1	17.8	13.7	14.6	13.0	12.4	12.8	12.7	85	62	82	76	2.3	8.9	3.1	4.8	6.4	7.1	5.2	6.2
VIII	–	–	–	–	20.5	10.4	29.8	6	5.4	14	13.0	19.0	13.9	15.0	13.6	14.7	14.1	14.1	89	67	88	81	1.6	8.1	2.1	3.9	5.5	6.1	3.2	4.9
IX	–	–	–	–	21.4	9.8	27.7	2	2.8	23	11.9	20.3	13.0	14.6	12.1	14.2	13.3	13.2	86	60	87	78	2.1	10.4	4.9	4.8	4.7	3.7	2.8	3.7
X	–	–	–	–	15.1	6.2	21.5	11	1.7	22	8.3	14.1	8.8	10.0	9.2	10.5	9.6	9.8	85	66	85	79	1.9	5.9	1.9	3.2	4.7	4.9	3.1	4.2
XI	–	–	–	–	6.6	0.7	14.3	2	-5.6	21	2.6	5.6	3.1	3.6	6.5	6.9	6.7	6.7	87	75	86	83	1.1	2.4	1.1	1.5	7.3	7.0	5.3	6.5
XII	–	–	–	–	1.3	-7.9	16.3	5	-23.4	17	-3.7	-0.8	-4.1	-3.2	4.5	4.8	4.3	4.5	82	76	79	79	1.1	1.7	1.2	1.3	6.6	5.6	5.4	5.9
Rok	–	–	–	–	12.9	3.8	30.3	3.VII	-23.4	17.XII	6.3	11.4	7.1	8.0	9.0	9.5	9.3	9.3	85	66	83	78	1.6	5.8	1.8	3.1	6.0	5.8	4.5	5.4

Oława – Zwierzyniec

$\varphi = 50°57'$ $\lambda = 17°18'$

I	–	–	–	–	1.0	-6.2	9.9	4	-20.5	27	-4.4	-0.1	-2.9	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.8	5.6	5.7
II	–	–	–	–	6.8	-0.3	12.4	15	-7.1	6	0.9	5.3	2.6	2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.8	6.0	6.3
III	–	–	–	–	11.0	3.1	20.1	10	-3.8	20	4.4	9.3	6.3	6.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	5.7	7.0
IV	–	–	–	–	18.0	6.1	27.4	7	-0.5	10	8.6	16.8	10.9	11.8	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.9	4.6	4.7
V	–	–	–	–	17.0	7.7	23.5	26	2.7	13	10.3	15.2	11.0	11.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.4	7.2	7.3
VI	–	–	–	–	23.4	12.1	29.9	25	6.1	16	15.6	21.6	16.9	17.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.9	5.4	5.5
VII	–	–	–	–	21.9	11.9	33.1	3	6.4	8	15.1	20.0	15.6	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.4	6.9	7.0
VIII	–	–	–	–	22.4	12.4	32.1	6	7.7	14	15.0	20.6	15.9	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.9	5.6	6.7
IX	–	–	–	–	22.6	10.5	30.9	2	3.8	23	12.4	21.4	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.6	4.1	4.7
X	–	–	–	–	16.5	7.0	22.4	6	1.6	22	8.2	15.5	10.4	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.8	3.9	5.6
XI	–	–	–	–	7.1	1.8	13.6	2	-4.8	22	2.9	6.2	4.0	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.0	6.9	7.7
XII	–	–	–	–	0.7	-6.8	17.5	5	-22.2	26	-3.9	-1.0	-3.5	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	5.8	6.5	6.7
Rok					14.0	4.9	33.1	3.VII	-22.2	26.XII	7.1	12.6	8.5	9.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.4	5.7	6.2

Bodzentyn

$\varphi = 50°57'$ $\lambda = 20°57'$

I	–	–	–	–	-1.2	-9.3	6.4	4	-25.3	26	-6.3	-2.3	-5.5	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.7	4.9	6.3
II	–	–	–	–	3.4	-1.1	9.4	18	-7.6	5	-0.2	2.9	1.1	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.9	7.1	7.8
III	–	–	–	–	8.9	1.9	18.3	18	-3.1	20	3.2	7.4	4.8	5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	6.2	6.9
IV	–	–	–	–	16.0	3.9	24.5	15	-3.2	10	8.0	14.6	8.9	10.1	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.7	4.1	4.6
V	–	–	–	–	16.6	5.6	24.2	27	0.8	19	9.9	15.2	9.7	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.6	6.1	6.9
VI	–	–	–	–	23.5	10.7	32.0	27	3.9	21	15.9	22.1	15.2	17.1	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.9	5.4	5.4
VII	–	–	–	–	21.4	10.0	30.5	3	5.5	6	14.7	19.9	14.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	6.1	6.3
VIII	–	–	–	–	21.5	11.0	30.9	11	5.2	31	14.2	20.6	14.7	16.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.3	5.4	6.7
IX	–	–	–	–	21.0	7.4	28.9	3	-3.0	23	9.8	20.0	12.1	13.5	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.5	4.1	4.4
X	–	–	–	–	16.0	4.0	23.1	20	-0.9	10	6.5	15.3	9.0	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.7	3.8	5.0
XI	–	–	–	–	6.7	1.4	14.7	3	-6.0	21	3.0	6.0	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.6	7.0	7.6
XII	–	–	–	–	–	-7.6	–	–	-24.4	26	-4.6	-2.4	-4.5	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.7	7.3	7.3
Rok	–	–	–	–	–	3.1	32.0	27.VI	-25.3	26.I	6.2	11.6	7.0	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	5.6	6.2

Silniczka

$\varphi = 50°55'$ $\lambda = 19°46'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.8	10.0	31.1	3	3.1	8	14.1	19.3	13.9	15.3	13.9	13.1	13.9	13.6	86	60	87	78	2.4	10.1	2.3	4.9	6.8	7.5	6.4	6.9
VIII	–	–	–	–	21.6	11.2	30.2	6	5.0	31	14.1	20.3	14.8	16.0	14.5	14.4	14.9	14.6	89	60	88	79	1.9	10.0	2.2	4.7	5.5	6.7	4.6	5.6
IX	–	–	–	–	20.8	7.2	29.4	17	-1.2	24	11.2	19.9	12.2	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.1	3.4	4.3
X	–	–	–	–	16.4	4.4	22.0	20	-0.8	10	6.9	15.4	8.9	10.0	8.9	10.1	9.5	9.5	89	59	83	77	1.3	7.6	2.2	3.7	6.5	5.8	3.0	5.1
XI	–	–	–	–	6.7	0.8	13.9	7	-8.1	23	2.2	5.7	3.2	3.6	7.0	7.6	7.3	7.3	93	83	91	89	0.5	1.8	0.7	1.0	7.9	7.3	7.2	7.5
XII	–	–	–	–	-0.6	-8.9	17.2	5	-28.9	26	-5.3	-2.6	-5.2	-4.6	4.5	5.0	4.4	4.6	91	88	90	90	0.5	0.9	0.6	0.7	7.5	7.4	5.6	6.8
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Wojcieszów Górny

$H_s = 358$ m — $h_w = 23$ m

MIESIĄC	ROZKŁAD WIATRU °D, %mD — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: v > 10	v > 15	⊙	●	Opad R: R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	2	2.0	5	2.4	14	1.8	1	6.0	14.5	2.4	21.5	3.5	9	2.1	1	2.0	25	1.9	32.4	13.8	14	12	9	27	·	·	·	–	–	13	6	1	4	20	·
II	5	1.8	·	·	·	·	1.5	2.0	4.5	2.0	22	2.4	23	2.5	5	2.4	23	1.7	58.4	18.4	9	·	·	14	·	·	·	–	–	16	11	1	8	5	·
III	5	1.4	·	·	·	·	·	·	1	6.0	27	3.5	24	3.2	23	3.6	13	2.8	55.9	16.7	30	·	·	11	·	·	·	–	–	17	14	1	4	5	·
IV	6	1.3	3	1.7	9	1.7	·	·	10	2.6	8	2.0	4	2.2	6	2.2	44	1.0	61.0	16.4	15	·	·	2	·	·	·	–	–	12	11	1	4	·	7
V	18	1.6	1	1.0	·	·	·	·	9	1.7	9	2.4	8	2.1	8	2.8	40	1.1	116.3	25.7	29	·	·	·	·	·	·	–	–	26	16	4	6	·	4
VI	2	2.0	1	2.0	·	·	1	2.0	15	1.6	8	2.1	7	2.6	19	1.9	37	1.2	71.5	15.8	7	·	·	·	5	·	·	–	–	16	12	2	4	·	7
VII	2	1.5	·	·	1	1.0	·	·	12	2.3	9	2.4	23	2.3	17	2.6	29	1.6	96.0	24.1	28	·	·	·	5	·	·	–	–	18	14	4	3	·	3
VIII	6	1.7	·	·	·	·	·	·	10.5	1.3	11.5	2.8	18	2.0	10	2.4	37	1.2	64.0	23.1	11	·	·	·	4	·	·	–	–	18	16	1	5	·	2
IX	5	1.0	·	·	4	1.5	6	1.8	19	1.8	7	1.9	8	1.9	10	3.0	31	1.3	31.1	8.8	4	·	·	·	8	·	·	–	–	9	6	·	5	·	2
X	2	1.5	1	2.0	1	2.0	6	2.3	20	2.8	10	2.2	4	2.0	5	2.2	44	1.3	37.1	14.8	20	·	·	·	·	·	·	–	–	9	7	1	·	·	·
XI	13	1.5	1	2.0	5	1.8	3	1.7	9	2.3	18	2.3	8	2.0	4	2.5	29	1.4	58.6	21.3	13	·	·	12	·	·	·	–	–	17	7	3	10	·	·
XII	12	1.6	2	2.0	5	1.0	·	·	11	3.0	17	5.1	9	2.8	6	2.3	31	2.0	60.8	28.6	11	12	12	26	·	1	·	–	–	17	7	1	1	19	·
Rok	78	1.6	14	1.1	39	0.9	18.5	1.3	135.5	2.5	168	2.7	145	2.3	114	2.5	383	1.5	743.1	28.6	11.XII	24	21	92	22	1	·	–	–	188	127	20	54	49	25

Oława – Zwierzyniec

$H_s = 137$ m — $h_w = 10$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	⊙	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	·	·	3	1.7	6	1.8	31.5	1.6	7.5	2.1	16	2.1	9	1.6	2	1.0	18	1.4	20.8	5.5	15	12	11	24	·	·	·	7	13	14	8	·	2	17	·
II	1	1.0	·	·	3.5	1.9	29.5	1.9	8	3.1	12	2.4	8.5	2.8	10.5	2.9	11	2.0	33.6	13.6	9	·	·	16	·	1	·	5	11	12	8	1	5	4	·
III	1	5.0	·	·	·	·	·	·	4	1.8	21	2.7	42	3.6	16	3.3	9	2.9	29.4	6.4	14	·	·	4	·	4	1	2	14	16	9	·	1	2	·
IV	4.5	1.7	6.5	1.7	10	2.4	23	2.3	6.5	2.2	12	2.1	4	2.8	7.5	1.7	16	1.8	28.2	7.4	16	·	·	1	2	·	·	8	8	10	7	·	1	·	6
V	12.5	2.0	4.5	1.6	2.5	1.6	3.5	1.4	15	2.7	18.5	2.2	5.5	3.9	24.5	2.4	20	1.8	73.3	17.1	29	·	·	·	·	·	·	2	15	18	13	3	·	·	5
VI	·	·	1	2.0	6	1.6	10.5	1.8	0.5	1.0	8.5	1.7	8	2.8	22.5	2.1	33	1.3	60.8	13.0	22	·	·	·	10	·	·	6	9	14	10	1	1	·	8
VII	0.5	1.0	·	·	·	·	3.5	1.6	4.5	1.7	26.5	2.2	18.5	2.7	14.5	2.5	25	1.7	91.2	25.5	28	·	·	·	8	·	·	3	14	17	12	4	1	·	3
VIII	0.5	3.0	·	·	2.5	1.4	10	1.4	0.5	2.0	19.5	2.5	17	2.6	9	2.3	34	1.4	121.8	46.2	11	·	·	·	7	·	·	2	11	15	11	2	·	·	9
IX	1.5	2.0	7	1.7	8	1.7	15	1.8	2.5	2.4	9	1.9	2.5	1.8	7.5	2.7	37	1.1	17.6	7.6	14	·	·	·	8	·	·	11	8	6	4	·	4	·	·
X	·	·	0.5	5.0	14.5	2.8	19.5	2.4	7	1.9	12.5	2.1	4.5	1.8	4.5	3.1	30	1.6	33.1	11.4	18	·	·	·	·	·	·	7	9	7	5	1	6	·	·
XI	5	1.4	5.5	1.2	2.5	1.8	12.5	1.5	2.5	2.2	12.5	2.8	8	2.6	10.5	1.5	31	1.3	50.1	10.6	5	·	·	8	·	·	·	3	18	16	9	1	8	·	·
XII	6.5	1.5	4.5	1.0	1.5	1.0	19	1.8	3.5	1.9	11.5	3.3	5	2.4	27.5	2.0	14	1.7	43.4	9.5	12	12	14	22	·	·	·	4	14	17	10	·	5	16	·
Rok	33	1.6	32.5	1.3	57	1.5	177.5	1.6	48.5	2.1	179.5	2.3	132.5	2.6	156.5	2.3	278	1.7	603.3	46.2	11.VIII	24	25	75	35	5	1	60	144	162	106	13	34	39	31

Bodzentyn

$H_s = 270$ m — $h_w = 14$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	⊙	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	1	3.5	6	2.5	0.5	6.0	8.5	5.3	9	4.6	20.5	4.8	16	3.6	18.5	3.4	13	3.5	29.2	7.2	5	12	16	28	·	3	·	5	11	11	5		5	25	·
II	1	2.5	0.5	2.0	4	4.6	13	4.0	7.5	4.9	17	4.0	23.5	3.7	14.5	3.2	3	3.7	23.0	6.2	9	·	·	18	·	1	·	1	19	9	7	·	5	6	·
III	·	·	·	·	·	·	·	·	2.5	8.6	34	6.4	32.5	7.1	23	6.9	1	6.7	38.2	8.9	21	·	·	7	·	11	2	1	13	15	10	·	1	5	·
IV	2	3.0	14.5	5.2	11	4.2	11	4.1	3.5	2.9	17.5	5.2	8	4.8	9.5	4.8	13	4.0	42.0	19.7	8	·	·	4	·	3	1	7	6	6	5	2	·	·	1
V	4.5	4.1	5	3.2	6.5	2.7	7	3.7	3	3.8	18.5	3.7	14.5	3.4	18	3.5	16	2.9	55.3	22.2	28	·	·	·	·	·	·	·	9	12	11	1	·	·	3
VI	1	4.0	1.5	3.3	4	2.6	11.5	2.7	10	2.8	20	3.4	14.5	4.1	8.5	4.0	19	2.7	82.8	19.1	26	·	·	·	8	·	·	3	5	15	10	4	·	·	10
VII	1.5	4.3	·	·	·	·	7.5	3.1	5.5	3.4	41.5	3.8	12.5	3.8	5.5	3.5	19	3.0	107.2	24.5	30	·	·	·	7	·	·	4	8	15	13	4	·	·	4
VIII	1.5	4.0	1.5	2.3	3.5	1.7	3	1.8	4	2.5	34	3.8	17	3.4	12.5	3.2	16	2.7	38.5	16.8	12	·	·	·	5	·	·	2	7	11	8	1	1	·	2
IX	0.5	4.0	3	3.5	2.5	3.0	1.5	6.0	0.5	4.0	25.5	3.8	16.5	3.0	7	3.8	33	2.2	13.3	5.8	14	·	·	3	7	·	·	10	6	9	6	·	1	·	·
X	·	·	4.5	3.3	10.5	4.0	20.5	4.2	16	3.7	10	4.2	9.5	3.6	13	3.5	9	3.5	5.2	4.0	14	·	·	4	·	1	·	7	7	4	1	·	3	·	·
XI	5	2.9	1[illegible]	3.1	10	3.1	10	3.6	3	4.2	26	3.9	8	4.4	14	3.8	3	3.5	80.0	24.5	13	·	1	11	·	·	·	4	20	16	12	3	5	·	·
XII	4.5	5.8	2	2.2	1	2.5	7	3.9	5.5	3.5	28	4.0	14.5	3.0	19.5	3.8	11	3.3	48.1	15.3	6	13	–	26	·	·	·	1	14	13	9	2	2	23	·
Rok	22.5	2.7	49.5	2.6	53.5	2.9	100.5	3.5	70	4.1	292.5	4.2	187	4.0	163.5	4.0	156	3.5	562.8	24.5	30.VII,13.XI	25	–	101	27	19	3	45	125	136	97	17	23	59	20

Silniczka

$H_s = 215$ m — $h_w = 14$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	⊙	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	5	2.0	0.5	4.0	3	2.7	5	2.3	7	2.4	21.5	2.8	24.5	3.2	9.5	3.0	17	2.3	146.7	27.7	13	·	·	·	8	·	·	3	13	21	17	7	1	·	7
VIII	6	3.7	1	3.0	2	3.5	4.5	1.6	5	2.4	15.5	2.4	26.5	3.3	8.5	3.3	24	2.2	65.1	15.5	12	·	·	·	7	·	·	4	7	12	11	2	2	·	3
IX	1	3.0	2.5	2.4	11	3.0	7.5	3.1	7.5	4.2	13	3.9	17	3.9	3.5	3.4	27	2.2	24.8	13.9	6	·	·	2	6	·	·	11	8	7	5	1	6	·	4
X	2.5	3.0	·	·	17.5	4.4	27.5	4.5	4	2.2	2.5	1.8	10.5	3.6	4.5	3.6	24	3.0	4.1	3.0	18	·	·	3	·	·	·	5	5	4	1	·	3	·	·
XI	9	4.5	4.5	3.0	11.5	3.8	8	3.2	6.5	2.5	12	2.9	15	4.0	4.5	2.9	22	2.6	79.6	17.8	13	·	·	11	·	·	·	2	16	18	9	3	3	3	·
XII	10.5	4.0	9	3.3	3.5	2.0	8	2.0	8.5	3.5	6.5	4.8	16	4.5	12	4.1	19	3.0	42.3	16.4	11	13	14	25	·	1	·	1	12	16	8	1	7	24	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Świeradów - Zdrój

$\varphi = 50°54'$ $\lambda = 15°20'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnie																			
	P_m	Max	Min	$P_{n.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0,3	-4,7	6,2	31	-16,8	26	-2,8	-0,9	-2,5	-2,2	3,8	3,9	3,8	3,8	71	65	71	69	1,5	2,0	1,5	1,7	5,6	6,3	5,7	5,9
II	–	–	–	–	5,7	0,0	16,8	18	-7,5	6	1,4	4,2	2,2	2,5	5,4	5,8	5,5	5,6	81	73	78	77	1,4	2,8	1,8	2,0	6,7	6,7	5,9	6,4
III	–	–	–	–	8,1	1,8	17,0	10	-5,5	20	3,0	6,8	4,7	4,8	5,9	6,0	6,1	6,0	78	64	73	72	1,8	4,3	2,7	2,9	7,5	7,5	7,4	7,5
IV	–	–	–	–	14,3	5,4	22,0	7	-0,9	1	8,8	13,1	8,7	9,8	8,5	8,4	8,8	8,6	75	57	78	70	3,0	7,3	2,7	4,3	5,7	6,2	5,4	5,8
V	–	–	–	–	12,3	5,4	21,8	26	1,2	13	8,0	10,7	8,0	8,7	9,0	8,6	8,9	8,8	84	69	83	79	2,0	4,7	2,0	2,9	8,5	7,8	7,5	7,9
VI	–	–	–	–	20,1	10,2	25,8	25	4,1	16	14,6	18,4	13,7	15,1	11,8	12,3	12,4	12,2	71	59	79	70	5,3	9,3	3,6	6,1	6,3	5,2	5,3	5,6
VII	–	–	–	–	18,1	10,0	30,6	3	5,9	6	13,6	16,3	12,8	13,9	11,9	10,9	11,7	11,5	77	62	78	72	4,2	8,6	3,5	5,4	7,2	7,1	6,9	7,1
VIII	–	–	–	–	18,7	10,9	28,8	6	6,0	17	13,4	17,5	13,6	14,5	12,6	13,1	12,6	12,8	82	66	80	76	2,9	7,7	3,3	4,6	7,0	6,8	5,5	6,4
IX	–	–	–	–	20,1	11,8	27,5	17	7,2	21	13,6	19,5	14,3	15,4	11,8	12,0	11,9	11,9	77	55	74	69	4,1	11,6	4,8	6,8	5,2	4,5	3,4	4,4
X	–	–	–	–	13,4	7,0	19,6	1	3,1	2	8,7	12,7	9,0	9,8	8,9	9,3	8,9	9,0	79	65	79	74	2,6	5,8	2,7	3,7	5,8	5,7	4,5	5,3
XI	–	–	–	–	5,9	1,3	11,4	22	-3,8	21	2,6	4,6	3,3	3,4	6,0	6,4	6,2	6,2	80	76	80	79	1,5	2,3	1,7	1,8	7,5	7,8	7,5	7,6
XII	–	–	–	–	-0,7	-6,2	13,1	5	-18,7	16	-3,4	-4,1	-3,1	-2,7	4,3	4,6	4,3	4,4	79	73	77	76	1,1	1,7	1,3	1,4	7,1	7,3	5,4	6,6
Rok	–	–	–	–	11,4	4,4	30,6	3.VII	-18,7	16.XII	6,8	10,2	7,1	7,8	8,3	8,4	8,4	8,4	78	65	78	74	2,6	5,7	2,6	3,6	6,7	6,6	5,9	6,4

Jelenia Góra

$\varphi = 50°54'$ $\lambda = 15°48'$

I	976,4	997,0	954,0	1019,8	1,3	-9,2	7,3	31	-29,1	27	-5,8	0,1	-4,0	-3,4	3,8	4,3	4,1	4,1	83	68	82	78	0,9	2,1	1,1	1,4	5,8	6,4	6,9	6,4
II	980,2	996,2	949,0	1022,9	7,6	-1,9	15,0	18	-14,0	6	0,4	6,0	1,7	2,4	5,8	6,6	6,2	6,2	90	71	88	83	0,7	3,0	0,9	1,5	7,5	6,7	5,5	6,6
III	979,0	996,4	952,8	1021,2	10,1	0,8	19,7	10	-5,2	20	2,4	8,3	4,8	5,1	6,3	6,8	6,8	6,6	85	65	80	77	1,2	4,6	2,1	2,6	7,7	7,7	6,9	7,4
IV	971,1	981,3	964,3	1012,1	16,0	4,1	23,7	6,7	-2,5	1	7,2	14,5	9,3	10,1	8,8	9,5	9,3	9,2	85	58	79	74	1,6	7,7	2,7	4,0	6,4	6,7	5,0	6,0
V	972,6	980,7	959,9	1013,6	14,3	5,0	21,5	26	1,4	13	8,6	12,7	8,5	9,6	10,0	9,5	10,0	9,8	89	66	90	82	1,3	5,6	1,3	2,7	8,3	8,7	7,6	8,2
VI	975,7	989,7	962,8	1046,1	21,7	8,7	28,2	25	2,5	17	14,0	19,9	14,6	15,8	13,7	13,4	14,2	13,8	85	58	85	76	2,4	10,4	2,6	5,1	6,4	6,5	5,8	6,2
VII	974,6	986,5	959,0	1015,2	20,0	9,1	30,5	3	2,0	8	13,5	18,2	13,4	14,6	12,8	11,7	12,8	12,4	82	58	83	74	2,9	10,1	2,8	5,3	7,3	7,7	7,1	7,4
VIII	977,2	988,6	966,2	1017,7	20,6	9,4	30,1	6	3,2	14	12,8	18,8	13,8	14,8	13,4	14,3	14,1	13,9	89	66	88	81	1,7	8,2	2,0	4,0	7,0	7,4	5,2	6,5
IX	978,5	988,3	966,7	1019,2	22,2	7,6	29,7	17	-0,2	23	10,0	21,1	12,7	14,1	11,6	13,0	12,9	12,5	92	53	87	77	1,1	13,1	2,1	5,4	5,0	4,8	3,4	4,4
X	976,7	989,9	948,9	1017,9	15,6	4,9	21,8	11	-1,5	30	7,5	14,6	8,7	9,9	8,7	10,3	9,4	9,5	84	63	84	77	2,1	6,7	2,2	3,7	6,7	7,1	3,5	5,8
XI	973,1	995,4	961,1	1015,2	7,0	-0,3	13,7	2	-8,0	21	1,6	6,0	2,6	3,2	6,3	6,9	6,7	6,6	90	74	89	84	0,8	2,6	0,9	1,4	7,7	7,8	7,1	7,5
XII	974,5	1001,2	954,6	1017,6	1,3	-10,1	16,3	5	-28,7	25	-6,0	-1,2	-5,3	-4,4	4,2	4,8	4,3	4,4	84	77	81	81	1,0	1,7	1,2	1,3	7,0	6,6	5,0	6,2
Rok	975,8	1001,2	948,9	1017,3	13,1	2,3	30,5	3.VII	-29,1	27.I	5,5	11,6	6,7	7,7	8,8	9,3	9,2	9,1	86	65	85	79	1,5	6,3	1,8	3,2	6,9	7,0	5,8	6,6

Sabótka

$\varphi = 50°54'$ $\lambda = 16°45'$

I	–	–	–	–	1,2	-5,5	8,7	30	-20,1	27	-2,1	-0,1	-2,0	-1,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	7,0	0,6	13,9	28	-5,5	6	2,7	6,1	3,2	3,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	3,4	–	–	-3,7	20	5,3	9,3	6,8	7,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	6,0	–	–	0,6	1	9,4	15,4	10,9	11,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	7,9	–	–	3,8	12,13	10,4	13,9	10,7	11,4	–	–	–	–	–	–	–	–	–	–	–	–	8,2	7,7	8,3	8,1
VI	–	–	–	–	21,8	12,6	28,1	25	8,0	16	16,3	20,8	16,6	17,6	–	–	–	–	–	–	–	–	–	–	–	–	7,1	6,0	6,5	6,5
VII	–	–	–	–	20,8	12,4	31,7	3	7,7	8	15,7	19,3	15,5	16,5	–	–	–	–	–	–	–	–	–	–	–	–	7,1	7,5	7,8	7,5
VIII	–	–	–	–	21,6	13,2	31,5	6	8,4	14	15,9	20,1	16,6	17,3	–	–	–	–	–	–	–	–	–	–	–	–	6,7	8,0	5,9	6,9
IX	–	–	–	–	22,1	11,4	29,6	2	3,6	23	14,4	21,0	16,8	17,2	–	–	–	–	–	–	–	–	–	–	–	–	6,6	6,6	5,3	6,2
X	–	–	–	–	16,1	7,0	22,4	5	2,1	22	9,4	15,2	10,5	11,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7,2	2,1	13,4	2	-2,3	27	3,8	5,8	4,6	4,7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	1,4	-6,2	17,5	5	-21,7	26	-2,4	-0,7	-2,6	-2,1	–	–	–	–	–	–	–	–	–	–	–	–	9,8	7,7	6,7	8,1
Rok	–	–	–	–	–	5,4	31,7	3.VII	-21,7	26.XII	8,2	12,2	9,0	9,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–		

Olesno

$\varphi = 50°53'$ $\lambda = 18°25'$

I	–	–	–	–	0,2	-6,8	10,5	4	-21,2	27	-4,7	-0,7	-3,7	-3,2	4,1	4,6	4,5	4,4	87	75	86	83	0,6	1,5	0,6	0,9	7,2	6,5	6,1	6,6
II	–	–	–	–	5,2	-0,9	13,6	18	-7,8	6	0,5	4,3	1,4	1,9	6,0	6,5	6,2	6,2	93	79	91	88	0,4	1,9	0,6	1,0	8,6	7,1	5,0	6,9
III	–	–	–	–	9,4	1,3	19,6	10	-5,1	20	3,1	7,7	4,9	5,2	6,8	7,5	7,4	7,2	88	71	85	81	1,0	3,4	1,5	2,0	7,9	7,2	5,9	7,0
IV	–	–	–	–	17,1	5,0	24,9	7	-1,7	10	8,2	16,1	10,1	11,1	8,7	9,2	9,5	9,1	78	51	76	68	2,5	9,9	3,2	5,2	4,3	4,5	3,7	4,2
V	–	–	–	–	16,5	5,8	23,4	26	1,5	23	9,9	15,1	9,8	11,2	10,8	11,4	11,2	11,1	89	68	91	83	1,6	6,3	1,1	3,0	7,2	7,4	6,3	7,0
VI	–	–	–	–	23,1	10,9	30,3	27	5,2	17	15,6	21,0	16,0	17,2	15,1	15,0	15,6	15,2	84	61	86	77	2,9	10,7	2,8	5,5	4,6	6,1	4,7	5,1
VII	–	–	–	–	20,8	10,6	30,7	3	4,3	8	14,4	19,0	14,7	15,7	13,9	14,2	14,4	14,2	85	66	86	79	2,8	8,5	2,6	4,6	6,7	7,3	6,3	6,8
VIII	–	–	–	–	21,5	11,2	30,4	6	6,0	14	14,0	20,0	15,0	16,0	14,6	15,4	15,3	15,1	90	66	89	82	1,7	8,8	2,1	4,2	6,5	7,4	4,0	6,0
IX	–	–	–	–	21,4	9,7	29,7	2	2,4	24	11,6	20,5	13,7	14,9	12,1	13,1	13,0	12,7	87	55	82	75	2,0	11,9	3,8	5,6	5,6	4,0	3,2	4,3
X	–	–	–	–	15,8	6,5	21,3	5	0,4	13	7,9	15,0	10,1	10,8	9,8	10,9	10,5	10,4	91	66	85	81	1,1	6,4	2,0	3,2	6,7	6,5	4,7	6,0
XI	–	–	–	–	7,0	0,9	13,2	10	-5,0	21	2,9	6,1	3,3	3,9	7,1	7,6	7,4	7,4	92	80	93	88	0,7	2,1	0,5	1,1	7,9	8,1	6,8	7,6
XII	–	–	–	–	0,1	-8,0	14,9	5	-23,4	25	-4,0	-1,4	-4,1	-3,4	4,8	5,0	4,6	4,8	86	80	87	84	0,6	1,3	0,6	0,8	7,4	6,5	5,1	6,3
Rok					13,2	3,8	30,7	3.VII	-23,4	25.XII	6,6	11,9	7,6	8,4	9,5	10,0	10,0	9,8	88	68	86	81	1,5	6,1	1,7	3,1	6,7	6,6	5,2	6,2

Świeradów-Zdrój $H_s = 549\,m$ $h_w = 13,5\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%D, m/s) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	◉	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	Π
I	3.5	4.3	4	2.9	3	3.0	8	3.4	33.5	4.6	21.5	3.3	2.5	3.4	3	2.2	14	3.2	61.6	30.1	31	5	11	27	·	2	1	6	11	13	8	1	1	26	
II	4.5	5.7	·	·	2	4.5	2.5	2.4	16.5	4.4	25	3.8	16.5	2.5	9	2.9	11	3.1	135.0	55.2	9	·	2	10	·	2	·	4	13	15	14	3	6	12	
III	0.5	2.0	·	·	·	·			10.5	2.6	23	3.4	23.5	3.2	30.5	3.1	5	3.0	139.6	25.2	30	·	·	8	·	·	·	3	17	18	14	6	2	9	
IV	2	2.5	·	·	2	3.0	6.5	3.4	24.5	3.1	21.5	2.4	14	1.4	6.5	1.6	13	2.1	104.1	19.5	16	·	·	1	·	2	·	3	7	17	11	5	4	·	5
V	2.5	1.4	1.5	1.0	·	·	2	3.5	14.5	2.8	21.5	2.4	19	2.3	19	1.8	13	2.0	261.3	43.2	21	·	·	·	·	·	·	·	15	21	19	9	5	·	6
VI	·		1	2.0	2	1.0	2	1.8	19.5	2.1	22	1.8	18	1.7	13.5	2.1	12	1.6	91.0	21.5	13	·	·	·	3	·	·	2	4	16	12	3	3		8
VII	3	1.3	·	·	·	·	1	5.0	19	2.6	21	2.6	30.5	2.5	11.5	2.4	7	2.3	165.4	53.5	30	·	·	·	4		·	2	13	24	17	5		·	1
VIII	·	·	·	·	·		2	2.0	22	2.2	36.5	2.5	12.5	2.4	9	2.4	11	2.1	99.0	14.4	11		·	·	1	·	·	2	8	24	17	4	3		5
IX	2.5	3.0	·	·	1	1.0	4	1.4	25	3.5	32	2.9	10	2.9	6.5	3.7	9	2.8	33.6	9.5	14		·	·	8	3	·	7	5	11	8		2	·	2
X	1	4.0	·	·	1	3.0	9.5	7.6	34	5.2	24.5	2.8	2	1.2	8	1.4	13	3.7	44.3	42.0	20		·	·	·	7	2	6	8	9	8	1	2	·	
XI	5	1.2	1	1.0	4	2.0	10	5.2	22	5.5	16	3.4	7.5	2.5	13.5	2.1	11	3.2	56.2	15.2	13		2	9	·	7	1		14	20	10	2	3	1	
XII	3	3.2	·	·	·	·	9.5	3.3	23.5	5.1	17.5	4.6	9	3.7	19.5	3.5	11	3.6	102.5	28.3	11	12	16	23	·	3	·	3	14	15	13	4	3	20	1
Rok	24.5	2.1	7.5	0.6	15	1.5	57	3.2	264.5	3.6	282	3.0	165	2.5	149.5	2.4	130	2.7	1293.6	55.2	9.II	17	31	78	16	26	4	38	129	203	151	43	34	68	28

Jelenia Góra $H_s = 342\,m$ $H_b = 343,9\,m$ $h_w = 15\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	Π
I	·	·	5	3.0	19	4.5	22	2.9	3.5	6.0	10	4.6	9	4.8	2.5	4.8	22	3.1	23.5	10.7	14	13	12	26	·	3	·	6	14	13	6	1	2	18	
II	2.5	1.0	2.5	2.0	8	2.1	9	2.7	3	2.7	6.5	4.4	17.5	5.1	9	4.5	26	2.6	56.7	21.3	9	1	·	18	·	·		5	15	17	9	1	6	5	
III	·	·	·	·	·	·	4	1.8	·	·	6.5	6.0	46.5	5.6	20	4.9	16	4.3	45.8	9.4	13	·	·	15	·	5	·	3	17	20	14	·	1	2	
IV	·	·	3.5	4.0	14.5	3.9	14	4.8	1	7.5	4	4.9	7	4.9	11	3.5	35	2.6	62.1	23.2	16	·	·	4	·	1	·	3	9	14	9	1	3	·	6
V	2	2.8	0.5	3.0	4	3.4	5.5	2.2	2	2.5	6.5	3.3	23	4.2	19.5	3.4	30	2.4	151.0	27.3	29	·	·	·	·	·	·	·	20	23	18	5	5	·	3
VI	1.5	2.0	2	1.8	7	3.0	10	2.4	2	3.0	3.5	3.7	14.5	4.6	19.5	3.8	30	2.4	55.9	11.1	10	·	·	·	5	·	·	3	11	14	11	1	2	·	9
VII	1	1.0	2.5	1.8	2.5	2.6	5	2.2	6.5	2.5	7.5	3.9	35.5	4.1	7.5	3.8	25	2.6	104.4	26.0	30	·	·	·	5	1	·	2	15	18	12	3	3	·	3
VIII	1.5	2.0	1.5	2.0	2	3.2	7	1.6	2.5	2.6	9.5	5.1	24	4.3	11	3.9	34	2.4	66.1	24.1	11	·	·	·	5	·	·	3	10	19	15	1	12	·	3
IX	1	1.5	3.5	1.9	9	3.6	13	1.9	4.5	2.5	5.5	4.3	46.5	4.4	11	2.7	26	2.2	28.5	12.2	5	·	·	1	10	·	·	10	4	9	6	1	3	·	2
X	1	2.0	1.5	2.3	12.5	4.9	31.5	4.6	5	4.5	2.5	5.6	8	3.0	7	2.4	24	3.1	46.1	14.2	20	·	·	2	·	3	·	5	9	9	7	1	6	·	
XI	·	·	7.5	2.4	11.5	3.0	8	2.0	·	·	7	4.6	20	3.8	7	3.1	29	2.2	43.8	16.9	13	·	·	14	·	·	·	3	17	15	6	2	5	·	
XII	2.5	3.6	2	4.0	7	3.0	8.5	1.9	1	4.0	10.5	6.8	18.5	5.2	14	3.1	29	2.9	51.3	20.7	11	15	13	25	·	1	·	5	11	15	9	1	3	19	
Rok	13	1.3	32	2.4	97	3.1	137.5	2.6	31	3.2	79.5	4.8	240	4.5	139	3.7	326	2.7	735.2	27.3	29.V	29	25	105	25	14	·	48	152	186	122	18	51	44	26

Sobótka $H_s = 204\,m$ $h_w = 14\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	Π
I	·	·	1.5	4.0	6	2.1	17.5	2.7	40.5	3.0	16	3.7	21	3.1	6.5	3.1	14	2.5	18.3	7.5	14	8	11	23	·	1	·	–	–	8	6	·	1	–	·
II	0.5	3.0	·	·	0.5	2.0	4.5	1.8	8	2.6	17	3.2	27.5	4.5	12	4.7	14	3.2	14.7	6.7	11	·	·	9	·	·	·	–	–	7	4	·	2	–	·
III	·	·	·	·	·	·		·	·	·	11	3.7	47.5	5.1	30.5	5.1	4	4.7	26.2	6.4	29	·	·	6	·	2	·	–	–	10	7	·	·	–	1
IV	3	2.7	1	1.0	7	2.9	19.5	2.3	11	3.0	6.5	3.2	18.5	3.0	10.5	3.1	13	2.4	52.0	18.5	16	·	·	·	–	1	·	–	–	11	9	1	·	·	4
V	3	1.9	5	0.3	1	1.0	4	1.9	3.5	2.4	7.5	2.1	46.5	3.3	19	3.1	8	2.7	61.7	12.9	20	·	·	·	·	·	·	·	17	17	12	2	1	·	4
VI	·	·	1	2.0	3	2.2	5.5	2.3	5.5	3.1	9	2.7	41	3.0	14	3.0	11	2.5	82.2	18.7	3	·	·	·	4	·	·	1	10	13	12	3	·	·	9
VII	·	·	·	·	1	1.0	3.5	2.3	5	3.0	11	2.7	49	3.1	14.5	2.9	9	2.7	103.9	29.7	28	·	·	·	5	·	·	1	16	14	12	4	1	·	3
VIII	·	·	·	·	5	1.9	3.5	2.1	4.5	3.6	14	3.2	45.5	3.0	12.5	3.3	8	2.7	129.2	41.5	11	·	·	·	7	·	·	2	10	14	10	4	1	·	4
IX	0.5	3.0	·	·	8	2.0	12	2.0	12.5	2.3	15	2.9	28.5	2.9	4.5	3.4	9	2.4	21.0	5.8	26	·	·	·	8	·	·	5	10	9	6	·	1	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	45.1	17.3	20	·	·	·	·	–	–	–	–	8	8	1	3	·	
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	65.2	24.6	13	·	·	5	·	–	–	–	–	14	9	2	8	–	
XII	3	1.3	·	·	7	1.7	9.5	2.2	3.5	3.3	7	4.2	31	4.0	14	3.3	18	2.6	34.0	12.3	11	9	12	23	·	1	·	·	16	10	5	1	7	–	
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	653.5	41.5	11.VIII	17	23	66	–	–	–	–	–	135	100	18	25	–	26

Olesno $H_s = 238\,m$ $h_w = 13\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	Π
I	2.5	4.4	3	2.2	10.5	4.9	12	4.5	25	2.9	23.5	4.4	7	3.3	6.5	4.5	3	2.8	21.0	7.3	14	11	12	25	·	2	·	5	15	13	6	·	3	20	·
II	3	2.0	0.5	1.0	4.5	2.1	8.5	1.8	13	2.5	20	3.0	14	2.9	10.5	4.2	10	2.5	49.1	20.1	9	·	1	19	·	1	·	1	12	18	7	1	8	2	
III	0.5	3.0	·	·	·	·	·	·	2	1.5	18.5	2.8	36	4.9	29	6.0	7	4.4	40.2	7.9	14	·	·	10	·	7	·	4	16	17	11	·	5	·	1
IV	6	2.7	4.5	2.0	16	2.4	18	2.4	8.5	1.8	15	2.6	8	3.2	7	3.6	7	2.4	25.6	8.5	1,8	·	·	2	·	·	·	10	5	8	5	·	1	·	3
V	12	2.3	3.5	1.7	4	1.4	4	1.5	4.5	2.4	14.5	2.2	18	3.6	17.5	3.0	15	2.2	85.0	20.4	29	·	·	·	·	·	·	1	11	18	13	2	2	·	5
VI	2	3.8	1	1.0	6	1.7	6.5	4.7	7.5	4.7	17	2.1	15	3.2	16	3.5	19	2.0	106.1	37.0	27	·	·	·	11	·	·	5	7	14	10	3	2	·	9
VII	2.5	3.0	0.5	1.0	0.5	1.0	3.5	1.3	6.5	1.2	27.5	2.7	26.5	3.2	17.5	3.8	8	2.7	145.5	32.8	31		·	·	7	·	·	2	12	21	16	5	1	·	6
VIII	4.5	2.1	1	1.0	1.5	1.3	4	1.6	4.5	2.3	24.5	2.2	21.5	3.3	14.5	4.0	17	2.3	47.7	9.9	12	·	·	·	5	·	·	4	7	16	12	·	2	·	3
IX	2	1.2	1	1.0	12	1.7	15	1.5	12.5	1.8	17.5	2.2	11	2.6	9	3.9	10	1.9	30.1	12.8	6	·	·	·	8	·	·	10	7	7	5	1	3	·	1
X	5.5	2.1	1	2.0	16.5	2.5	16.5	2.2	14	2.9	18.5	3.5	7.5	1.7	3.5	3.9	10	2.4	17.3	5.3	19	·	·	·	·	·	·	4	9	7	5	·	8	·	·
XI	7.5	2.2	3	2.5	8.5	2.6	8	1.8	14	1.9	20	2.2	11	2.9	12	2.7	6	2.2	79.5	28.1	13		·	13	·	·	·	2	16	21	11	2	7	·	
XII	13	2.6	6	1.6	6.5	1.5	6	1.8	12	3.2	19.5	3.6	13.5	3.3	12.5	3.5	4	2.8	50.6	15.9	11	14	13	24	·	·	·	5	11	14	13	1	3	16	
Rok	61	2.4	25	1.4	86.5	1.7	102	1.6	124	2.2	236	2.8	189	3.2	155.5	3.6	116	2.6	697.7	37.0	27.VI	25	26	93	31	10	·	53	128	174	114	15	45	38	28

Cieplice Śl. - Zdrój — φ = 50°52' — λ = 15°41' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.6	-8.9	10.3	3	-23.9	18	-5.9	0.1	-4.1	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	6.0	5.8
II	–	–	–	–	8.0	-2.2	15.9	15	-12.8	6	0.9	6.3	1.6	2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.0	5.8	6.5
III	–	–	–	–	10.0	1.2	20.3	10	-7.3	20	3.0	8.3	5.2	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	7.5	7.5
IV	–	–	–	–	15.8	4.4	24.1	7	-3.4	10	7.6	14.6	9.4	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.5	5.4	5.8
V	–	–	–	–	14.1	4.9	21.2	26	0.2	13	9.0	12.3	8.5	9.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	9.2	7.3	8.3
VI	–	–	–	–	21.8	8.9	28.6	25	3.0	17	14.5	19.7	14.2	15.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.7	6.5	6.4
VII	–	–	–	–	20.0	9.3	31.1	3	2.6	8	14.0	18.2	13.4	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.2	7.6	7.7
VIII	–	–	–	–	20.7	9.2	30.4	6	3.3	4,14	13.4	18.9	13.8	15.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.5	7.3	7.2
IX	–	–	–	–	22.1	7.5	29.6	17	0.3	23,24	10.6	21.1	12.5	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.1	4.9	5.1
X	–	–	–	–	15.5	4.5	22.5	6	-2.8	16	7.5	14.6	8.7	9.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.7	5.2	6.0
XI	–	–	–	–	6.9	-0.9	13.2	2	-8.9	23	1.5	5.7	2.1	2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.8	7.4	7.6
XII	–	–	–	–	1.5	-10.4	16.2	5	-29.2	25	-6.2	-1.7	-5.3	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.0	6.6	6.6
Rok	–	–	–	–	13.2	2.3	31.1	3.VII	-29.2	25.XII	5.8	11.5	6.7	7.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.9	6.5	6.7

Stupia Nowa — φ = 50°52' — λ = 21°05'

I	–	–	–	–	-1.0	-7.6	5.9	4	-22.1	26	-5.3	-2.3	-4.2	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.5	4.8	6.3
II	–	–	–	–	3.6	-0.9	10.8	18	-4.2	5	0.0	2.9	1.1	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.1	7.1	7.9
III	–	–	–	–	8.4	2.0	18.5	18	-4.1	20	3.2	7.1	4.8	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.6	6.9	6.5	7.3
IV	–	–	–	–	15.4	5.2	23.4	7	-1.0	10	8.2	14.1	8.7	9.9	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.4	4.0	4.2
V	–	–	–	–	16.1	6.6	23.9	28	2.0	15	10.1	14.6	10.0	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.3	5.4	6.4
VI	–	–	–	–	23.0	12.1	30.2	27	6.8	21	16.3	21.5	16.1	17.5	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.7	6.6	5.7
VII	–	–	–	–	20.9	11.5	29.7	3	7.0	6	14.9	19.3	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	6.3	6.5
VIII	–	–	–	–	21.2	12.4	30.6	11	8.1	30	14.8	20.1	15.6	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.8	4.5	5.5
IX	–	–	–	–	20.2	10.2	28.2	2	2.1	24	12.6	19.1	14.3	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.0	3.4	4.8
X	–	–	–	–	15.4	6.8	22.0	20	3.6	23	8.6	14.7	10.4	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.3	3.6	5.1
XI	–	–	–	–	6.4	1.4	13.7	3	-5.6	21	3.1	5.4	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.3	7.1	8.2
XII	–	–	–	–	-0.6	-7.2	15.5	5	-23.4	25	-4.6	-2.9	-3.8	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.1	7.3	7.6
Rok	–	–	–	–	12.4	4.4	30.6	11.VIII	-23.4	25.XII	6.8	11.1	7.6	8.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	5.6	6.3

Świdnica — φ = 50°51' — λ = 16°29'

I	–	–	–	–	1.3	-4.9	10.4	31	-18.5	27	-2.8	0.3	-1.8	-1.5	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.2	5.8	6.1
II	–	–	–	–	7.3	1.1	16.6	18	-4.9	6	2.5	5.8	3.6	3.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.2	5.7	6.5
III	–	–	–	–	10.9	2.6	18.3	17	-3.5	20	4.8	9.4	6.5	6.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.9	6.0	6.5
IV	–	–	–	–	16.8	6.4	25.3	7	-0.7	1	9.9	15.8	10.6	11.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.6	5.5	5.7
V	–	–	–	–	15.5	7.2	22.9	26	3.3	13	10.6	13.9	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.9	6.9	7.4
VI	–	–	–	–	22.7	11.9	29.9	25	7.2	21	16.4	20.9	16.1	17.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	4.8	5.6
VII	–	–	–	–	20.7	12.1	31.4	3	7.2	8	15.9	19.4	14.9	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.9	6.8	6.7
VIII	–	–	–	–	21.6	12.1	30.8	6	7.4	14	15.7	20.1	15.4	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.3	5.0	6.1
IX	–	–	–	–	22.4	10.6	30.2	18	4.6	23	14.2	21.2	14.5	16.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.6	4.9	5.1
X	–	–	–	–	16.1	6.8	22.1	5	1.2	16	9.1	15.0	10.4	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.1	4.7	6.0
XI	–	–	–	–	7.4	1.9	12.1	2	-5.1	21	3.2	6.0	4.3	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	6.8	7.4
XII	–	–	–	–	1.7	-6.5	17.3	5	-21.7	17	-2.8	-0.2	-2.7	-2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.6	6.3	7.0
Rok	–	–	–	–	13.7	5.1	31.4	3.VII	-21.7	17.XII	8.1	12.3	8.5	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	5.8	6.4

Kielce — φ = 50°51' — λ = 20°37'

I	987.2	1008.3	969.5	1021.7	-1.0	-9.0	6.0	4	-22.8	27	-6.5	-2.4	-5.6	-5.0	3.9	4.3	4.0	4.1	9.0	7.9	8.8	8.6	0.4	1.1	0.5	0.7	7.0	6.6	5.8	6.5
II	989.5	1003.8	960.8	1023.3	3.5	-1.9	10.6	18	-7.9	6	-0.6	2.3	0.3	0.6	5.6	6.2	5.9	5.9	9.4	8.6	9.3	9.1	0.3	1.1	0.4	0.6	8.8	8.5	7.1	8.1
III	984.9	1002.8	962.3	1018.0	8.8	1.5	18.8	18	-4.2	20	3.0	7.2	4.6	4.8	6.8	6.9	7.1	6.9	8.9	6.9	8.3	8.0	0.9	3.6	1.5	2.0	8.8	8.1	7.4	8.1
IV	980.7	999.2	971.5	1013.1	16.3	4.2	25.1	15	-3.4	10	7.5	14.8	8.6	9.9	7.9	8.1	8.3	8.1	7.5	4.9	7.4	6.6	2.7	9.5	-3.2	5.1	6.2	6.3	4.9	5.8
V	980.0	987.1	966.4	1012.3	17.2	5.4	25.6	27	0.3	15	9.6	14.9	9.8	11.0	10.1	9.6	9.9	9.9	8.4	5.8	8.2	7.5	2.1	7.7	2.5	4.1	7.4	8.3	6.9	7.5
VI	983.5	996.4	973.7	1015.1	23.7	11.1	31.7	27	5.0	21	15.9	21.8	15.6	17.2	14.5	13.8	14.6	14.3	8.0	5.4	8.2	7.2	3.7	12.9	3.3	6.6	5.6	5.8	5.9	5.8
VII	982.3	993.7	966.9	1014.1	21.5	10.3	31.0	3	5.6	8	14.5	19.8	14.4	15.8	13.6	13.1	13.7	13.5	8.2	5.8	8.3	7.4	3.1	10.8	3.0	5.6	6.8	7.7	5.8	6.8
VIII	984.9	997.4	975.0	1016.8	21.9	11.3	31.1	11	5.0	31	14.1	20.4	14.7	16.0	14.5	14.2	14.8	14.5	8.9	5.9	8.7	7.8	1.9	10.7	2.2	4.9	6.9	7.7	5.1	6.6
IX	987.4	998.3	976.0	1019.6	20.8	8.0	29.2	2	0.5	22	11.0	19.3	12.9	14.0	11.8	12.0	12.1	12.0	8.8	5.4	8.0	7.4	1.7	11.2	3.2	5.4	5.2	5.2	3.7	4.7
X	987.3	998.9	963.4	1019.9	15.9	5.3	22.2	20	4.5	10,17	7.1	15.0	10.1	10.6	8.7	9.5	9.3	9.2	8.6	5.7	7.6	7.3	1.6	7.8	3.3	4.2	6.8	6.6	4.7	6.0
XI	981.8	1003.4	970.0	1014.9	6.5	0.8	14.1	3	-8.0	21,23	2.4	5.4	3.1	3.5	7.1	7.6	7.3	7.3	9.3	8.4	9.3	9.0	0.5	1.6	0.6	0.9	8.8	8.7	7.4	8.3
XII	982.8	1009.2	963.2	1017.0	-1.1	-8.3	16.5	5	-25.2	26	-5.3	-2.9	-4.9	-4.5	4.4	4.8	4.5	4.6	8.9	8.6	9.1	8.9	0.5	1.0	0.4	0.6	7.4	7.6	7.5	7.5
Rok	984.4	1009.2	960.8	1017.1	12.8	3.2	31.7	27.VI	-25.2	26.XII	6.1	11.3	7.0	7.8	9.1	9.2	9.3	9.2	8.7	6.6	8.4	7.9	1.6	6.6	2.0	3.4	7.1	7.3	6.0	6.8

Cieplice Śl. - Zdrój

$H_s = 345\ m$ $h_w = 13{,}6\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °/₀																Średnia prędkość	OPAD R			LICZBA DNI (n)										
	N		NE		E		SE		S		SW		W		NW		C		Suma	Max	Data	Temperatura T			Wiatr				Opad R				
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Max<-10°	Max<0°	Min<0°	Max>25°	≥10	≥15		≥0.1	≥1.0	≥10.0		
I	·	·	6.5	2.9	9.5	2.0	4.5	1.4	5.5	6.3	8.5	6.2	8.5	3.5	6	4.2	4.4	2.0	146	10.4	14	13	11	2.6	·	2	2	8	14	8	2	1	10	1.5	·
II	0.5	4.0	2.5	2.4	6	1.7	0.5	3.0	12.5	3.6	8	3.0	1.7	3.9	7	2.3	3.0	2.0	36.3	17.9	9	1	·	1.8	·	1	1	5	14	11	7	1	7	4	·
III	5	1.2	·	·	1	3.0	1	2.0	3	1.3	8	6.9	3.6	6.5	2.5	7.0	1.4	5.8	33.9	5.4	13.30	·	·	1.3	·	9	7	4	17	14	10	·	–	·	·
IV	2	2.5	8	4.6	11	3.5	10	6.3	3.5	4.1	5.5	4.8	6.5	5.8	10.5	4.9	3.3	3.0	43.9	18.2	16	·	·	4	·	4	1	3	8	11	10	1	–	·	6
V	8	3.9	2.5	1.8	3.5	1.3	2.5	3.8	9	3.0	3.5	5.6	18.5	6.3	15.5	3.9	3.0	2.9	113.7	26.1	29	·	·	·	·	3	2	·	20	19	16	4	–	·	3
VI	6	2.9	4.5	2.1	4.5	2.4	8	2.0	8.5	2.1	4	4.4	11	4.2	13.5	4.4	3.0	2.2	73.7	26.7	10	·	·	·	6	1	·	6	15	12	12	1	–	·	7
VII	2	2.8	1.5	1.7	1.5	2.3	3	3.5	1.0	3.4	1.4.5	4.5	21.5	4.0	12	5.0	2.7	2.9	94.4	24.6	30	·	·	·	5	3	1	2	21	14	12	3	·	·	1
VIII	·	·	6	2.7	7	1.6	1	1.0	4	3.5	20	4.3	9	3.9	13	3.9	3.3	2.3	62.9	22.3	11	·	·	·	6	·	·	2	14	13	12	2	1	·	5
IX	3.5	2.3	4.5	2.0	8	2.4	4	2.8	5	4.0	7.5	4.7	3.5	3.4	11	4.6	4.3	1.8	23.6	8.9	14	·	·	·	10	2	·	8	8	9	6	·	6	·	2
X	3	3.3	6.5	2.4	11.5	4.7	12	2.9	14.5	5.2	9.5	13.2	5	3.6	3	3.7	2.8	3.7	40.2	16.8	20	·	·	5	·	6	2	5	12	8	7	1	3	·	·
XI	7	2.1	2	4.5	11	2.4	7	1.3	2	4.0	8	8.9	8.5	4.6	6.5	2.6	3.8	2.2	46.5	22.3	13	·	·	1.7	·	3	1	3	17	12	5	1	·	·	·
XII	2	2.5	3.5	1.4	6.5	2.5	7	2.1	8	2.2	12.5	10.9	9.5	4.0	13	4.9	3.1	3.2	44.8	15.3	11	15	14	2.4	·	4	4	3	13	11	8	2	6	1.9	1
Rok	3.9	2.3	4.8	2.4	8.1	2.5	6.0.5	2.7	8.5.5	3.6	10.9.5	6.4	1.5.4.5	4.5	1.3.6	4.3	3.8.1	2.8	628.5	26.7	10.VI	29	25	10.7	27	38	21	49	173	142	107	17	–	38	23

Słupia Nowa

$H_s = 307\ m$ $h_w = 15\ m$

I	8.5	2.4	1	3.0	·	·	1	4.0	2.9	4.6	2.0	4.9	6	3.9	16.5	2.4	11	3.5	39.5	15.6	31	11	14	2.8	·	2	·	3	12	14	6	1	4	2.5	·
II	0.5	2.0	·	·	1	2.0	3.5	3.9	1.9	5.0	20.5	4.6	1.0	3.0	16.5	3.4	1.3	3.5	55.6	17.3	9	·	·	1.7	·	3	·	1	17	13	8	1	7	1	·
III	1.5	3.0	·	·	·	·	·	·	4.5	5.3	1.7	5.0	3.5	4.0	2.9	4.1	6	4.0	61.0	12.3	29	·	·	6	·	2	·	1	13	17	14	1	1	5	·
IV	3.5	4.1	3	2.8	11	3.1	10	3.7	12.5	2.7	1.7	3.6	10.5	3.1	7.5	3.8	1.5	2.8	52.5	19.4	8	·	·	1	·	·	·	9	2	7	6	2	·	·	2
V	3.5	3.0	1	1.5	3.5	3.4	8	2.6	1.6	3.0	11.5	2.6	1.0	2.8	25.5	3.0	1.4	2.4	102.5	47.8	28	·	·	·	·	·	·	1	8	12	10	2	1	·	4
VI	·	·	·	·	2	3.5	3	3.8	7.5	3.0	14.5	2.8	23.5	2.7	11.5	2.6	2.8	1.9	139.8	32.3	27	·	·	·	7	·	·	4	9	15	15	4	2	·	7
VII	0.5	2.0	1	2.0	·	·	3	4.5	13.5	3.4	21.5	3.0	25.5	2.9	1.0	3.6	1.8	2.5	153.9	46.8	30	·	·	·	7	·	·	1	9	14	11	6	·	·	7
VIII	0.5	3.0	0.5	2.0	0.5	2.0	2	3.0	15.5	2.6	19.5	3.4	22.5	2.7	1.8	2.9	1.4	2.5	60.4	19.3	12	·	·	·	5	1	·	3	7	10	8	1	1	·	2
IX	1	2.0	2.5	1.8	2.5	2.4	4.5	3.4	2.0.5	2.8	2.0	3.5	1.3	3.5	8	2.8	1.8	2.5	20.7	12.6	14	·	·	·	6	·	·	9	5	7	4	1	2	·	2
X	0.5	4.0	1.5	3.3	3.5	2.9	2.3.5	4.7	2.3.5	5.0	1.1	4.0	5	2.8	1.5.5	2.5	9	3.7	10.0	7.8	14	·	·	·	·	1	·	7	7	3	3	·	3	·	·
XI	4.5	4.8	·	·	3.5	3.0	6	2.9	18.5	4.5	1.4.5	5.4	13.5	2.9	13.5	3.3	16	3.3	115.7	31.4	13	·	2	1.0	·	1	1	·	18	16	13	3	11	·	·
XII	1.8	4.3	1	1.0	·	·	·		16	4.7	22.5	4.5	7	3.1	2.0.5	3.9	8	3.8	39.5	15.9	6	10	19	2.5	·	·	·	1	17	16	8	1	2	2.5	·
Rok	4.2.5	2.9	11.5	1.4	2.7.5	1.9	6.4.5	3.0	1.9.6	3.9	2.0.9.5	3.9	1.8.1.5	3.1	1.9.2	3.2	1.7.0	3.0	851.1	47.8	28.V	21	35	8.7	25	10	1	40	124	144	106	23	34	56	24

Świdnica

$H_s = 230\ m$ $h_w = 14\ m$

I	·	·	2	3.0	5.5	1.9	11.5	1.1.9	1.7.5	3.8	2.9	5.8	1.5	1.0	4	5.0	2.2	3.2	20.0	10.2	3	9	10	1.9	·	5	2	7	11	8	4	1	1	10.5	·
II	1	3.0	·	·	·	·	5	2.2	9.5	3.7	3.7.5	6.7	7.5	3.3	9.5	4.1	1.4	4.3	27.2	9.2	9	·	·	7	·	5	3	4	12	16	8	·	1	1.5	·
III	4.5	2.8	·	·	·	·	·	·	0.5	3.0	2.5.5	4.0	4.7.5	4.5	8	3.9	7	3.9	28.8	5.3	30	·	·	8	·	3	3	3	13	19	9	·	·	·	3
IV	5	1.6	5	2.0	9	2.0	1.1.5	3.0	8	4.1	1.1.5	4.1	7.5	1.7	8.5	2.4	2.4	2.0	43.7	14.7	16	·	·	1	1	1	·	4	11	10	8	1	1	·	6
V	5	1.8	1.5	3.0	3.5	2.1	2	2.0	3	3.7	16.5	3.0	14.5	2.7	2.5	2.6	2.2	2.0	84.3	24.6	29	·	·	·	·	·	·	·	11	2.0	16	1	2	·	4
VI	3.5	1.9	3	1.0	3.5	2.1	6.5	1.8	7	2.0	9.5	1.7	2.0.5	2.8	12.5	2.5	2.4	1.7	69.7	26.2	10	·	·	·	9	·	·	2	8	11	9	3	1	·	7
VII	·	·	2	1.0	2	1.5	2	1.5	3	2.7	24.5	3.4	31	2.8	10.5	3.3	1.8	2.4	111.5	23.4	28	·	·	·	5	·	·	2	12	14	10	5	·	·	4
VIII	3	1.3	1	2.0	1	1.0	4	2.8	2.5	2.8	32.5	2.5	21.5	3.3	8.5	1.8	1.9	2.1	81.7	28.0	10	·	·	·	5	·	·	3	9	14	10	2	1	·	2
IX	1.5	1.7	1.5	1.3	7	2.3	8	1.6	9.5	2.1	24	3.2	12.5	4.0	6	2.7	2.0	2.2	11.3	3.9	26	·	·	·	9	·	·	10	8	8	3	·	3	·	3
X	2	3.0	·	·	5.5	4.1	2.1	2.6	12.5	3.7	2.1	4.7	7	3.1	4	3.2	2.0	2.8	36.2	15.3	20	·	·	·	·	1	1	4	9	8	6	1	3	·	·
XI	10.5	2.4	3.5	1.0	4.5	2.2	8.5	1.8	7.5	3.1	2.5.5	4.4	5	3.2	8	3.0	1.7	2.6	45.3	14.5	13	·	·	8	·	1	1	2	16	12	7	2	4	·	·
XII	4	2.5	4	1.9	1.5	2.7	8	1.9	3.5	3.6	32	7.6	13	4.2	12	3.5	1.5	4.2	39.0	12.1	11	11	12	2.1	·	7	3	2	13	17	7	2	·	1.7.3	·
Rok	4.0	1.8	2.3.5	1.4	4.3	1.8	8.8	1.9	8.4	3.2	2.8.9	4.3	1.8.9	3.0	1.1.6.5	3.2	2.2.2	2.8	598.7	28.0	10.VIII	20	22	6.4	29	23	13	43	133	157	97	18	17	28.9	29

Kielce

$H_s = 268\ m$ $H_b = 270{,}1\ m$ $h_w = 21.1\ m$

I	0.5	5.0	4.5	2.4	6	2.6	9	2.8	2.2.5	3.4	20	3.6	1.5.5	2.9	3	2.3	1.2	2.8	28.4	6.2	4	13	14	2.8	·	1	·	3	13	12	6	·	2	2.6	·
II	0.5	1.0	·	·	·	·	4.5	3.2	2.6.5	3.3	17	2.6	2.4	2.7	5.5	2.2	6	2.6	31.1	9.5	9	·	1	2.2	·	1	·	·	17	14	7	·	5	1.2	·
III	0.5	4.0	1	9.0	·	·	·	·	3.5	4.3	16.5	4.7	5.7	4.5	11.5	5.8	3	4.6	40.9	7.6	21	·	·	9	·	3	2	·	20	19	9	·	4	4	·
IV	·	·	3	4.0	14.5	5.4	18	4.4	11	4.0	12	2.8	13	3.3	5.5	3.9	13	3.5	49.6	21.0	8	·	·	4	1	1	·	4	9	7	6	2	·	·	2
V	3.5	1.6	2	1.8	7	3.1	14	2.8	8.5	3.4	12	3.4	25	3.1	15	2.9	6	2.8	36.5	6.2	27	·	·	·	1	·	·	·	14	13	12	·	3	·	4
VI	·	·	1.5	1.7	6	3.8	11	4.0	11.5	3.3	13	3.0	32	3.1	3	1.7	12	2.8	72.8	14.0	3	·	·	·	10	·	·	2	5	14	12	2	1	·	10
VII	·	·	·	·	·	·	3	3.8	5.5	3.7	2.9	3.5	37.5	2.9	5	2.6	1.3	2.7	107.1	35.4	30	·	·	·	8	·	·	2	13	17	14	3	·	·	5
VIII	1	2.0	·	·	4	1.2	2.5	3.8	9	3.7	24	3.6	34.5	2.7	10	2.0	8	2.7	43.2	12.1	12	·	·	·	7	·	·	1	8	9	7	1	1	·	3
IX	0.5	1.0	1	3.0	8	2.6	11.5	2.8	9	3.0	19.5	2.7	27	2.6	5.5	2.4	8	2.4	22.1	7.6	14	·	·	·	5	·	·	9	8	12	6	·	2	·	2
X	·	·	0.5	6.0	14.5	4.0	3.5	3.9	14	3.0	4.5	3.9	13	2.5	3.5	2.1	8	3.2	3.9	2.9	14	·	·	·	·	1	·	5	10	4	1	·	4	·	·
XI	1.5	4.7	1.5	2.3	9.5	4.1	10	2.9	13.5	2.9	22	3.0	14	3.3	11	2.6	7	2.9	79.3	19.7	13	·	1	1.0	·	·	·	·	19	18	11	3	3	1	·
XII	5.5	3.1	2.5	5.6	4.5	3.3	1.0	2.3	14	3.1	14.5	3.8	13.5	2.9	19.5	2.7	9	2.8	58.4	15.9	11	11	18	2.6	·	·	·	2	17	19	11	2	2	2.5	·
Rok	13.5	1.9	17.5	3.0	7.4	2.5	12.8.5	3.1	14.8.5	3.4	2.0.4	3.4	3.0.6	3.0	9.8	2.8	10.5	3.0	573.3	36.4	30.VII	24	34	9.9	32	7	2	28	153	158	102	13	27	68	26

Święty Krzyż — φ = 50°51' — λ = 21°03' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.7	–	3.6	4	–	–	-6.0	-4.4	-5.6	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.5	4.6	5.5
II	–	–	–	–	1.8	-3.0	9.6	18	-7.0	5	-1.7	0.3	-0.7	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	6.2	7.0
III	–	–	–	–	6.0	0.0	16.4	18	-8.7	20	1.3	4.3	2.7	2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.7	6.4	7.3
IV	–	–	–	–	13.5	4.4	22.7	15	-3.0	1	5.8	11.9	8.3	8.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.0	3.8	4.6
V	–	–	–	–	14.1	6.4	22.4	27,28	0.6	12	7.8	12.3	9.0	9.5	9.0	9.2	9.0	9.1	85	65	78	76	4.9	5.7	2.8	3.5	8.2	8.7	6.5	7.8
VI	–	–	–	–	20.9	–	28.5	27	–	–	14.6	19.5	15.1	16.1	13.2	13.3	12.8	13.1	80	59	75	71	3.6	10.0	4.6	6.1	5.2	6.7	7.5	6.5
VII	–	–	–	–	18.8	–	27.7	3	–	–	13.0	17.1	13.6	14.3	12.1	12.5	12.1	12.2	82	65	78	75	3.2	7.6	3.8	4.9	7.7	7.8	6.8	7.4
VIII	–	–	–	–	19.0	11.0	29.2	11	7.1	24	12.9	17.9	14.1	14.8	13.1	13.6	13.2	13.3	87	66	81	78	2.1	7.8	3.2	4.4	5.6	6.5	5.8	6.0
IX	–	–	–	–	18.0	10.1	25.9	2	4.0	23	11.3	16.6	12.7	13.3	10.8	11.7	11.1	11.2	80	63	75	73	2.9	7.8	3.9	4.9	5.0	4.4	3.7	4.4
X	–	–	–	–	13.7	6.1	20.9	20	1.7	23	7.1	12.5	8.8	9.3	8.6	9.1	8.8	8.8	85	64	78	76	1.6	5.8	2.7	3.4	6.5	5.6	4.5	5.5
XI	–	–	–	–	4.9	0.4	11.9	3	-6.5	20	1.7	3.3	2.3	2.4	6.6	7.0	6.9	6.8	94	90	94	93	0.5	1.0	0.5	0.7	8.8	8.3	8.2	8.4
XII	–	–	–	–	-2.6	-8.2	13.7	5	-19.0	16	-5.7	-4.7	-5.4	-5.3	4.8	4.5	4.3	4.3	91	91	93	92	0.3	0.4	0.3	0.3	8.8	7.2	6.5	7.5
Rok	–	–	–	–	10.4	–	29.2	11.VIII	–	–	5.2	8.9	6.2	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	5.9	6.5

Strzyżów — φ = 50°51' — λ = 24°02'

I	–	–	–	–	-1.8	-9.3	3.8	4,9	-23.8	27	-6.4	-3.1	-5.9	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	5.6	5.2	6.3
II	–	–	–	–	2.7	-1.4	9.1	28	-5.9	7	-0.6	2.0	0.4	0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.6	7.5	7.9
III	–	–	–	–	8.4	1.1	18.5	18	-4.2	23	3.2	6.9	3.9	4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.9	5.1	6.5
IV	–	–	–	–	16.2	–	24.9	7	–	–	7.3	14.7	8.5	9.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.5	6.6	25.3	29	1.0	20	10.8	15.9	10.6	12.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	24.0	11.6	31.4	27	6.2	1	16.9	22.2	16.4	18.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	23.6	11.3	31.2	4	5.7	9	15.5	22.0	15.8	17.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.4	12.1	33.0	11	7.9	25	15.0	21.1	16.3	17.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.7	7.7	28.9	18	-3.4	23	10.0	19.8	12.3	13.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15.9	4.4	21.3	28	-1.4	23	6.0	15.1	8.2	9.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6.9	0.9	15.2	3	-7.6	23	2.8	5.9	3.6	4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-0.9	-8.7	16.9	5	-23.7	26	-5.1	-2.7	-5.0	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.8	6.6	7.3
Rok	–	–	–	–	13.0	–	33.0	11.VIII	-23.8	27.1	6.3	11.6	7.1	8.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Szklarska Poręba — φ = 50°50' — λ = 15°32'

I	–	–	–	–	1.2	-7.1	6.8	3	-22.3	26	-4.3	-0.2	-3.5	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.9	5.8	6.1
II	–	–	–	–	6.2	-1.8	16.1	18	-11.9	6	0.6	4.7	0.9	1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	5.9	6.7
III	–	–	–	–	7.8	0.2	16.1	17	-9.1	20	1.9	6.4	3.5	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	6.9	7.9
IV	–	–	–	–	14.1	3.7	21.8	9	-3.3	10	8.1	12.6	7.7	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.0	5.8	6.4
V	–	–	–	–	12.1	4.7	21.3	26	0.6	13	7.9	10.1	7.3	8.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.9	8.0	8.7
VI	–	–	–	–	19.9	8.8	26.0	25	3.2	17	14.3	18.1	13.1	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.6	6.7
VII	–	–	–	–	17.3	8.8	28.0	3	3.0	8	12.8	15.7	11.9	13.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.9	7.5	7.8
VIII	–	–	–	–	18.5	9.2	28.5	6	3.0	14	12.6	16.6	12.7	13.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.4	4.9	6.7
IX	–	–	–	–	20.1	–	28.8	17	–	–	12.4	19.0	12.8	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	4.0	5.1
X	–	–	–	–	13.7	4.6	19.9	11	-1.6	2	7.6	12.4	7.8	8.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.1	4.6	6.2
XI	–	–	–	–	–	–	–	–	–	–	1.4	4.3	2.3	2.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.9	8.0	8.1
XII	–	–	–	–	0.9	-8.8	12.6	5	-23.3	16	-4.7	-4.0	-4.2	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	5.6	6.6
Rok	–	–	–	–	–	–	28.8	17.IX	-23.3	16.XII	5.9	9.9	6.0	7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	6.1	6.9

Lipowa — φ = 50°50' — λ = 21°27'

I	–	–	–	–	-1.3	-8.5	6.0	4	-21.3	27	-5.9	-2.8	-4.8	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.3	6.0	6.8
II	–	–	–	–	3.8	-1.2	12.1	18	-6.9	5	-0.1	2.7	0.6	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.5	8.0	8.4
III	–	–	–	–	8.8	2.0	19.0	18	-2.7	20	3.9	7.2	5.1	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.5	7.4	7.5
IV	–	–	–	–	15.9	4.8	25.0	15	-2.7	10	6.8	14.4	9.3	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.7	4.9	5.6
V	–	–	–	–	16.7	6.2	26.9	28	1.8	13	9.4	15.0	10.4	11.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.3	7.6
VI	–	–	–	–	23.4	10.8	30.3	26	7.1	1	16.1	21.9	16.0	17.5	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.5	6.2	5.4
VII	–	–	–	–	21.8	10.9	30.1	3	6.6	6	15.1	19.9	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.9	7.0	6.1
VIII	–	–	–	–	22.0	12.0	31.5	11	8.1	17,31	14.9	20.8	15.9	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.5	6.2	5.6
IX	–	–	–	–	21.0	8.6	29.0	2	-0.7	22,24	11.5	19.8	13.8	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.5	4.4	4.3
X	–	–	–	–	16.2	4.7	22.0	19	0.3	24	6.5	15.0	9.6	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	5.8	6.0
XI	–	–	–	–	6.9	1.5	15.5	3	-5.7	21	2.9	5.4	3.8	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.9	8.9	8.9
XII	–	–	–	–	-1.2	-7.5	14.0	2	-22.1	26	-5.0	-3.1	-4.5	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.8	7.3	7.8	8.0
Rok	–	–	–	–	12.8	3.7	31.5	11.VIII	-22.1	26.XII	6.3	11.4	7.5	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.6	6.7	6.7

Święty Krzyż

$H_s = 575\,m$ $h_w = 24\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%D, %nD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min ≤ -10°	Max < 0°	Min < 0°	Max ≥ 25°	Wiatr v ≥ 10	v ≥ 15	Opad R ≥ 0,1	≥ 1,0	≥ 10,0	≡	≋	≈
I	6.5	3.0	4	4.0	4.5	3.4	6	5.6	3.3	7.6	8.5	5.3	7.5	3.9	6	2.9	17	4.6	70.2	16.8	31	-	24	-	·	6	4	7	9	15	9	3	-	29	·
II	3	3.5	0.5	1.0	-	-	4	6.0	20.5	6.7	9	6.7	16	4.7	13	3.3	18	4.2	59.8	18.4	9	·	9	27	·	6	3	4	15	14	12	1	-	22	·
III	3	5.7	·	·	·	·	·	·	14.5	8.0	13.5	5.8	3.3	8.7	23	7.2	6	7.1	93.8	15.4	30	·	1	16	·	18	8	1	17	17	14	4	-	8	·
IV	4.5	4.2	6.5	3.4	1.5	5.3	10.5	6.0	19.5	5.7	4.5	6.0	13	4.8	4.5	3.1	12	4.4	93.8	33.4	8	·	·	3	·	6	2	9	6	6	6	3	-	·	2
V	6.5	3.9	2	3.0	4	3.8	4	3.8	14.5	4.5	6.5	4.5	11	2.6	9.5	2.9	35	2.3	187.4	74.8	28	·	·	·	·	1	·	1	14	14	13	6	-	·	1
VI	2	1.5	4	2.5	4.5	3.8	7.5	3.4	18.5	4.7	4	3.9	18.5	2.9	10	2.9	21	2.4	249.3	52.6	27	·	·	·	3	3	1	4	13	17	15	8	-	·	6
VII	4.5	4.4	1	1.0	-	-	1	9.0	24.5	5.5	19.5	4.2	15.5	3.1	12	2.0	15	3.4	296.2	75.9	30	·	·	·	3	5	1	3	19	15	13	8	-	·	3
VIII	6.5	2.2	·	·	·	·	3	3.3	15	3.6	16.5	3.0	13.5	2.5	16.5	3.0	22	2.3	99.8	27.0	12	·	·	·	5	·	·	6	10	14	8	4	-	·	2
IX	4	1.8	6	1.1	8	4.9	7.5	3.1	13.5	2.3	15.5	2.2	9.5	2.5	10	2.9	16	1.8	58.0	23.8	14	·	·	·	3	1	·	10	7	11	9	1	9	·	2
X	7	3.2	3	3.3	5.5	3.0	25.5	9.9	24.5	7.8	7	4.5	6	3.4	10.5	2.8	4	6.2	6.1	4.2	14	·	·	·	·	8	5	4	8	4	2	·	10	·	·
XI	11	6.5	2	2.2	3.5	5.4	8.5	4.9	15	5.9	13.5	7.0	11.5	5.3	11	6.0	14	4.9	94.7	24.8	13	·	4	12	·	8	1	·	21	16	15	3	18	2	·
XII	24	4.2	9.5	9.0	2	5.0	6	7.7	13.5	8.0	11	9.4	6	4.5	7	4.7	14	5.5	58.6	22.5	6	13	20	27	·	9	6	1	16	11	9	1	14	25	·
Rok	8.2.5	3.7	3.8.5	2.5	4.7	2.6	8.3.5	5.2	2.2.6.5	5.9	1.2.9	5.2	1.6.1	4.1	1.3.3	3.6	1.9.4	4.1	1.3.6.7.7	7.5.9	30.VII	-	58	-	14	71	31	50	155	154.5	125.5	42.5	-	86	16

Strzyżów

$H_s = 185\,m$ $h_w =$ 11,5 m I-VIII, 12,5 m IX-XII

I	8	4.1	·	·	5	3.0	13.5	3.3	11.5	3.6	11.5	2.7	12.5	3.1	15	3.1	16	2.7	13.8	8.6	15	13	15	31	·	1	·	3	12	-	3	·	5	-	-
II	3	1.0	1	1.0	3	1.7	14	5.1	14	4.6	8	2.4	13	2.7	13	2.5	15	2.8	12.6	3.4	2,28	·	·	20	·	1	·	2	20	-	4	·	-	-	-
III	1	9.0	·	·	·	·	1	3.0	2	12.0	24	6.1	25	3.8	35	5.5	5	5.1	31.0	5.6	12	·	·	11	·	7	·	2	9	-	9	·	-	-	-
IV	6	2.2	8	4.6	18	5.6	8	8.8	6	3.5	9	5.9	12	2.2	11	3.5	12	4.0	46.1	16.0	8	·	·	-	·	7	·	-	-	-	7	2	1	·	-
V	4	2.0	5	2.0	5.5	4.7	9	3.8	5.5	1.8	16	4.5	8	2.9	19	4.0	21	2.8	41.5	9.2	14	·	·	·	2	·	·	-	-	-	10	·	1	·	-
VI	1	1.0	9	4.1	7	1.9	11.5	3.9	5	3.9	12	3.4	11.5	2.9	24	2.3	9	2.7	51.0	14.8	4	·	·	·	11	1	·	-	-	-	9	3	·	·	-
VII	1	1.0	2	4.0	1	4.0	9	4.7	3	4.7	17	3.2	24	2.4	25	2.8	11	2.7	108.8	42.3	30	·	·	·	9	·	·	-	-	-	12	3	·	·	-
VIII	1	4.0	2	2.5	3	1.3	4	3.8	5	2.8	18	3.6	29	3.1	25	3.3	6	3.0	45.1	21.6	12	·	·	·	8	2	·	-	-	-	7	2	1	·	-
IX	4	2.8	6	1.8	10	1.7	5	2.6	·	·	12	4.0	24	1.9	13	3.2	16	2.1	7.2	4.1	14	·	·	3	5	·	·	-	-	-	2	·	5	·	-
X	2	1.0	9	3.8	25	4.2	29	5.9	5	3.2	1	3.0	5	2.8	9	2.7	8	4.0	7.4	3.4	29	·	·	2	·	6	·	-	-	-	3	·	10	·	-
XI	5	2.4	4	3.0	21	5.0	14	3.7	2	1.0	13	3.6	16	2.8	11	3.3	4	3.4	30.2	5.5	25	·	·	13	·	1	·	-	-	-	8	·	5	-	-
XII	14	4.2	7	3.1	8	2.6	11	2.5	7	2.9	14	6.1	11	3.2	13	3.5	8	3.4	26.2	7.6	11	13	18	25	·	3	·	1	12	-	7	·	3	-	-
Rok	50	2.9	53	2.5	106.5	3.0	129	4.3	66	3.7	155.5	4.0	191	2.8	213	3.3	131	3.2	420.9	42.3	30.VII	26	33	-	35	29	·	-	-	-	81	10	-	-	-

Szklarska Poręba

$H_s = 640\,m$ $h_w = 13\,m$

I	·	·	1	1.0	4	1.0	8	1.6	9.5	3.9	19	4.2	7	2.4	16.5	2.2	28	2.0	66.8	26.1	31	10	9	29	·	2	·	5	9	13	7	2	·	31	·
II	2.5	1.6	·	·	4	1.0	4.5	1.0	14	3.2	13.5	3.5	17	2.6	18.5	3.2	10	2.5	73.4	36.4	9	2	1	20	·	1	1	3	14	13	10	1	1	8	·
III	4	4.2	1	1.0	3.5	1.0	2	1.0	2	1.5	10	3.4	42	4.3	20.5	3.8	8	3.4	132.3	32.7	30	·	2	18	·	·	·	·	20	18	12	5	-	8	·
IV	0.5	1.0	4	1.2	10.5	2.1	7.5	1.8	13.5	3.4	9	1.9	7	1.4	9	1.3	29	1.4	83.3	20.7	3	·	·	6	·	1	·	1	10	12	9	5	1	·	5
V	2	2.0	4	1.2	3.5	1.0	12.5	1.2	12.5	1.8	11.5	3.7	21	3.2	6	3.2	20	1.9	246.9	40.5	27	·	·	·	·	·	·	·	22	20	19	8	4	·	2
VI	·	·	·	·	6	1.7	7	1.2	12.5	1.9	13	2.7	16.5	2.7	4	3.5	31	1.5	120.5	18.5	27	·	·	·	1	·	·	3	14	14	13	6	-	·	5
VII	0.5	1.0	0.5	1.0	1	1.0	6	1.4	10.5	2.0	27	2.4	34	1.9	7.5	2.4	6	1.9	171.3	42.2	30	·	·	·	3	1	·	2	18	22	19	4	·	·	1
VIII	·	·	·	·	0.5	1.0	9.5	1.0	23	1.2	24	1.6	21	1.9	8	1.5	7	1.4	111.3	20.2	11	·	·	·	2	·	·	1	11	20	14	5	1	·	1
IX	1.5	1.3	3.5	1.3	9.5	1.1	9.5	1.5	16	2.1	19.5	2.5	11	2.3	7.5	1.9	12	1.7	39.1	16.1	14	·	·	·	7	1	·	8	7	10	8	1	1	·	3
X	2	1.8	4	2.8	6	2.3	16	3.9	22	6.3	9	5.6	7	3.8	4	2.4	23	3.4	65.6	28.5	17	·	·	1	·	7	2	3	11	8	7	2	2	·	·
XI	0.5	1.0	·	·	3	2.0	13.5	1.6	11.5	1.8	15	5.1	20	2.9	4.5	3.2	22	2.2	75.5	24.2	13	·	-	-	·	3	·	1	20	-	-	2	8	1	·
XII	5	1.6	3	1.3	3	1.3	7	1.3	12	2.8	15.5	6.1	17	3.5	6.5	3.7	24	2.5	155.6	57.0	11	12	17	25	·	3	·	3	13	14	10	5	2	19	1
Rok	18.5	1.3	21	0.9	54.5	1.4	103	1.6	159	2.7	186	3.6	220.5	2.7	112.5	2.7	220	2.2	1341.6	57.0	11.XII	24	-	-	13	19	3	30	169	-	-	46	-	57	18

Lipowa

$H_s = 245\,m$ $h_w = 16,5\,m$

I	9	2.3	7	2.0	2	1.0	5	4.0	2.5	5.8	12.5	3.7	9.5	3.0	9	4.2	14	3.4	136	7.0	14	12	15	31	·	5	2	2	14	8	4	·	·	20	·
II	1	1.0	5	2.0	-	-	8	3.2	24	5.4	10	2.1	14	2.6	12	3.5	10	3.3	14.2	3.8	10	·	·	20	·	6	·	·	20	13	7	·	·	1	·
III	4	2.2	·		·	·	·	·	·	·	10	7.1	44.5	6.6	26.5	6.0	8	5.7	13.5	3.0	29	·	·	7	·	13	4	·	14	16	5	·	·	1	·
IV	4	1.8	3	2.7	21	4.7	11	6.5	14	2.9	12	3.8	10.5	4.8	3.5	5.7	11	3.8	53.3	25.1	8	·	·	2	·	7	·	3	7	8	7	1	-	·	2
V	9	3.1	2	1.0	7	3.4	3.5	4.3	15.5	4.0	8	2.9	20	3.0	11	4.5	17	2.8	28.9	6.5	6	·	·	·	1	4	·	·	14	14	8	·	·	·	3
VI	·	·	1	4.0	4	1.2	13	3.3	15.5	3.1	3.5	1.9	16	3.6	12	2.8	25	2.2	128.9	30.8	7	·	·	·	7	2	·	4	7	14	14	6	·	·	9
VII	2.5	3.2	·	·	·	·	2	3.5	8	3.1	10	2.8	23.5	2.7	19	1.7	28	1.8	77.0	23.8	30	·	·	·	8	2	·	3	4	13	11	2	-	·	6
VIII	4	1.8	·	·	2	1.0	2	2.5	7	2.1	11.5	2.9	27.5	2.8	20	2.1	19	2.0	33.6	12.9	12	·	·	·	6	4	·	3	5	11	8	1	-	·	3
IX	2	1.0	1	1.0	9	1.4	4	2.0	12	2.3	6	1.8	23	2.6	7	1.7	26	1.5	12.6	6.6	14	·	·	2	6	·	·	12	6	5	4	·	-	·	2
X	1	2.0	·	·	7	2.0	3.1	4.7	18	4.1	4	2.8	3	4.7	12	2.1	17	3.1	3.0	3.0	14	·	·	·	·	4	1	2	10	1	1	·	-	·	·
XI	9	3.2	·	·	6	3.8	12.5	3.8	18.5	2.2	13	2.8	18	3.2	7	4.7	6	3.0	52.0	20.0	13	·	·	10	·	1	·	·	24	10	6	2	-	·	·
XII	2.9	5.2	·	·	1	2.0	2	4.0	13.5	3.0	13.5	4.9	3	1.0	22	2.8	9	3.4	29.7	6.0	14	11	16	24	·	5	2	2	20	15	11	·	-	25	·
Rok	9.4.5	2.2	19	1.1	69	1.7	94	3.2	17.1	3.2	11.4	3.3	21.2.5	3.4	161	3.5	190	3.0	460.3	30.8	7.VI	23	31	96	28	53	9	31	145	128	86	12	-	47	25

Częstochowa

$\varphi = 50°49'$ $\lambda = 19°06'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	987.8	1009.4	967.8	1021.2	0.2	-7.2	9.3	4	-19.7	27	-5.2	-1.0	-4.1	-3.6	4.0	4.8	4.2	4.3	88	81	85	85	0.5	1.2	0.7	0.8	7.3	6.4	5.5	6.4
II	990.3	1005.4	960.7	1023.1	5.2	-0.6	15.1	18	-7.8	6	0.6	4.2	1.4	1.9	6.0	6.8	6.1	6.3	93	83	90	89	0.5	1.6	0.7	0.9	9.2	7.6	5.3	7.4
III	986.9	1004.9	962.8	1019.2	9.6	1.9	19.6	10	-4.1	20	3.2	7.5	5.0	5.2	6.8	7.2	7.4	7.1	88	70	84	81	1.0	3.6	1.5	2.0	7.4	7.9	5.9	7.1
IV	981.2	990.3	972.8	1012.6	17.3	5.2	25.7	7	-1.8	10	7.2	15.8	10.1	10.8	8.6	9.4	8.9	9.0	83	53	71	69	1.8	9.3	3.7	4.9	3.9	4.6	4.4	4.3
V	981.1	987.4	966.6	1012.5	17.0	6.5	24.1	27	1.4	12	9.2	15.2	10.7	11.4	10.2	10.8	10.8	10.6	87	62	83	77	1.6	7.1	2.3	3.7	6.8	8.3	7.1	7.4
VI	984.7	998.0	974.1	1015.4	23.9	11.7	32.8	27	6.2	16	15.3	21.4	16.5	17.4	14.7	14.4	15.1	14.7	84	57	80	74	3.0	12.0	3.9	6.3	4.8	6.4	5.0	5.4
VII	983.4	994.9	969.2	1014.3	21.2	11.2	31.5	3	6.6	8	13.9	19.3	14.8	15.7	13.8	14.4	14.0	14.1	86	65	82	78	2.2	9.0	3.1	4.8	6.7	8.0	6.3	7.0
VIII	986.1	999.0	976.0	1017.1	22.1	11.7	31.0	10	7.9	31	13.8	20.3	15.4	16.2	14.4	15.1	15.1	14.9	90	63	85	79	1.6	9.5	2.7	4.6	5.8	7.1	4.5	5.8
IX	988.2	999.3	976.9	1019.5	21.7	9.5	29.3	2	1.9	24	11.2	20.3	13.6	14.7	12.0	12.9	12.9	12.6	88	55	81	75	1.6	11.8	3.0	5.5	5.0	4.4	3.1	4.2
X	987.5	1000.0	961.0	1019.1	16.7	6.8	22.5	6	1.8	22	8.0	15.5	10.4	11.1	9.5	10.5	10.1	10.0	88	61	80	76	1.4	7.4	2.7	3.8	7.3	6.5	3.5	5.8
XI	982.8	1004.9	970.4	1015.1	7.3	1.2	13.8	3	-5.3	22	2.6	6.1	3.3	3.8	7.0	7.7	7.2	7.3	91	81	90	87	0.7	2.0	0.8	1.2	8.0	7.8	7.5	7.8
XII	984.0	1011.1	965.3	1017.3	0.1	-7.5	16.6	5	-23.2	26	-4.4	-4.7	-4.3	-3.7	4.6	5.1	4.4	4.7	87	84	86	86	0.6	1.1	0.7	0.8	6.9	7.2	6.6	6.9
Rok	985.3	1011.1	960.7	1017.2	13.5	4.2	32.8	27.VI	-23.2	26.XII	6.3	11.9	7.7	8.4	9.3	9.9	9.7	9.6	88	68	83	80	1.4	6.3	2.2	3.3	6.6	6.8	5.4	6.3

Szrenica

$\varphi = 50°48'$ $\lambda = 15°31'$

I	858.1	873.7	840.5	-	-3.1	-8.0	1.4	16	-15.9	25	-6.5	-4.8	-5.9	-5.8	2.9	3.1	3.1	3.0	74	73	74	74	0.9	1.2	0.9	1.0	6.7	7.3	6.7	6.9
II	863.7	879.5	834.7	-	1.4	-4.0	10.7	25	-11.6	5	-2.2	-0.4	-1.9	-1.6	4.2	4.7	4.4	4.4	83	83	83	83	1.1	1.5	1.2	1.3	8.0	7.9	7.4	7.8
III	863.3	879.3	837.9	-	1.7	-3.2	11.0	10	-11.4	20	-1.9	0.2	-1.0	-0.9	4.4	5.0	4.7	4.7	83	83	84	83	1.1	1.5	1.1	1.2	8.5	8.7	8.4	8.5
IV	858.2	864.8	848.8	-	8.3	1.5	14.4	9	-7.1	1	4.0	7.0	3.7	4.6	6.7	7.3	7.0	7.0	82	75	87	81	1.7	3.0	1.2	2.0	7.1	8.0	7.1	7.4
V	859.2	864.9	848.3	-	6.0	1.0	15.2	26	-2.4	13	2.8	4.5	2.9	3.3	7.2	7.6	7.3	7.4	95	90	95	93	0.5	1.1	0.4	0.7	9.5	9.1	8.1	8.9
VI	864.5	876.7	852.4	-	13.8	6.7	20.1	25	1.4	16	9.1	12.1	9.3	10.0	10.1	11.3	10.4	10.6	87	81	88	85	1.7	3.1	1.5	2.1	7.2	7.5	6.6	7.1
VII	863.1	875.0	850.4	-	10.9	5.4	21.8	3	0.9	6	7.3	9.5	7.4	7.9	9.7	10.1	9.8	9.9	94	85	94	91	0.8	2.5	0.8	1.4	8.4	8.6	7.7	8.2
VIII	865.5	877.1	854.1	-	12.2	6.7	21.8	10	2.3	16	8.6	10.6	8.9	9.2	10.1	11.3	10.5	10.6	90	89	91	90	1.4	2.1	1.2	1.6	8.0	8.3	6.9	7.7
IX	867.2	876.8	854.0	-	14.6	8.2	22.4	17	2.2	8	10.0	13.3	10.3	11.0	9.3	10.8	9.5	9.9	76	73	77	75	3.4	5.2	3.3	4.0	5.9	5.6	4.3	5.3
X	863.1	876.1	837.2	-	8.0	2.8	15.7	1	-1.1	20,22	4.3	6.5	4.1	4.8	7.4	8.2	7.4	7.7	89	85	90	88	1.1	1.8	1.0	1.3	7.0	7.7	6.0	6.9
XI	857.6	874.8	848.4	-	1.8	-2.4	9.7	23	-9.3	21	-0.8	0.3	-0.7	-0.5	4.8	5.1	5.2	5.0	84	84	89	86	1.1	1.4	0.7	1.1	8.5	8.3	8.3	8.4
XII	856.3	874.4	842.6	-	-3.2	-9.3	6.3	5	-22.3	16	-6.6	-5.3	-6.2	-6.1	3.7	3.9	3.6	3.7	86	85	82	84	0.4	0.6	0.6	0.5	8.3	7.7	6.6	7.5
Rok	861.6	879.5	834.7	-	6.0	0.4	22.4	17.IX	-23.3	16.XII	2.3	4.5	2.6	3.0	6.7	7.4	6.9	7.0	85	82	86	84	1.3	2.1	1.2	1.5	7.8	7.9	7.0	7.6

Szczawno - Zdrój

$\varphi = 50°48'$ $\lambda = 16°16'$

I	-	-	-	-	0.3	-5.8	6.5	4,31	-18.5	26	-3.1	-0.5	-2.6	-2.2	4.2	4.4	4.1	4.2	79	72	76	76	1.1	1.7	1.3	1.4	6.0	6.0	6.3	6.1
II	-	-	-	-	5.5	0.2	16.7	18	-6.7	6	1.5	4.5	2.4	2.7	5.8	6.1	6.1	6.0	85	73	83	80	1.1	2.5	1.3	1.6	6.8	6.2	5.6	6.2
III	-	-	-	-	9.5	2.1	18.3	10	-4.2	20	3.7	8.2	5.5	5.7	6.3	6.8	6.6	6.6	79	63	73	72	1.8	4.5	2.7	3.0	6.8	6.4	5.5	6.2
IV	-	-	-	-	15.6	5.7	23.6	7	-1.5	10	9.4	14.5	9.7	10.8	-	-	-	-	-	-	-	-	-	-	-	-	4.7	5.5	5.2	5.1
V	-	-	-	-	13.9	6.6	20.3	26	1.7	13	9.5	12.3	9.0	10.0	-	-	-	-	-	-	-	-	-	-	-	-	7.8	8.6	7.4	7.9
VI	-	-	-	-	21.4	11.1	27.6	25	5.4	16	15.9	19.9	14.9	16.4	-	-	-	-	-	-	-	-	-	-	-	-	5.3	5.7	4.8	5.3
VII	-	-	-	-	19.3	10.8	29.8	3	6.7	8	14.8	18.0	13.6	15.0	-	-	-	-	-	-	-	-	-	-	-	-	6.6	6.8	6.5	6.6
VIII	-	-	-	-	20.3	11.4	29.1	6	6.4	17	14.9	18.8	14.2	15.5	-	-	-	-	-	-	-	-	-	-	-	-	5.6	7.0	4.3	5.6
IX	-	-	-	-	21.1	11.2	29.1	18	3.3	23	14.1	20.1	14.1	15.6	12.1	12.5	12.4	12.3	75	54	77	69	4.4	11.9	4.2	6.8	4.6	4.7	3.3	4.2
X	-	-	-	-	14.5	7.2	20.8	6	1.9	22	9.3	13.8	9.6	10.6	9.7	9.9	9.5	9.7	82	64	81	76	2.2	6.2	2.6	3.7	5.7	6.4	4.5	5.5
XI	-	-	-	-	6.1	1.5	10.6	2	-4.0	20	2.9	5.2	3.9	4.0	6.5	6.9	6.8	6.7	84	77	83	81	1.1	2.1	1.4	1.5	8.0	8.0	8.2	8.1
XII	-	-	-	-	0.9	-6.6	15.1	5	-21.2	17	-3.4	-0.9	-2.9	-2.5	4.5	4.9	4.5	4.6	83	77	80	80	1.0	1.6	1.2	1.3	7.0	6.6	6.6	6.7
Rok	-	-	-	-	12.4	4.6	29.8	3.VII	-21.2	17.XII	7.5	11.2	7.6	8.5	-	-	-	-	-	-	-	-	-	-	-	-	6.2	6.5	5.7	6.1

Bierutowice

$\varphi = 50°47'$ $\lambda = 15°44'$

I	-	-	-	-	0.2	-6.1	4.5	3	-19.7	25	-3.5	-1.5	-3.1	-2.8	-	-	-	-	-	-	-	-	-	-	-	-	4.5	5.3	4.9	4.9
II	-	-	-	-	4.8	-1.6	15.0	18	-7.6	5,6	0.7	3.0	1.2	1.5	-	-	-	-	-	-	-	-	-	-	-	-	6.2	6.2	5.3	5.9
III	-	-	-	-	6.0	-0.1	15.8	10	-6.2	22	1.7	4.6	2.7	2.9	-	-	-	-	-	-	-	-	-	-	-	-	6.5	6.9	6.8	6.7
IV	-	-	-	-	12.3	4.1	18.3	14	-4.5	1	8.0	10.8	7.2	8.3	-	-	-	-	-	-	-	-	-	-	-	-	4.9	5.7	4.4	5.0
V	-	-	-	-	10.2	4.0	18.2	26	-0.2	13	6.6	8.5	6.3	6.9	-	-	-	-	-	-	-	-	-	-	-	-	8.3	8.8	6.9	8.0
VI	-	-	-	-	17.7	9.7	23.0	27	4.8	16	13.6	16.4	12.7	13.8	-	-	-	-	-	-	-	-	-	-	-	-	4.8	5.4	4.3	4.8
VII	-	-	-	-	16.1	8.8	27.5	2	4.9	6	11.9	14.7	11.4	12.4	-	-	-	-	-	-	-	-	-	-	-	-	6.2	6.5	5.5	6.1
VIII	-	-	-	-	16.8	9.7	25.7	6	4.5	14	12.9	15.4	12.4	13.3	-	-	-	-	-	-	-	-	-	-	-	-	4.9	6.2	4.0	5.0
IX	-	-	-	-	18.0	10.5	26.2	3	5.4	20,21	13.6	17.1	13.1	14.2	-	-	-	-	-	-	-	-	-	-	-	-	3.9	4.1	3.4	3.8
X	-	-	-	-	12.1	5.8	17.8	1	1.5	22	8.2	10.8	7.9	8.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XI	-	-	-	-	5.4	-0.3	10.2	23,24	-5.1	30	1.5	3.5	2.6	2.6	-	-	-	-	-	-	-	-	-	-	-	-	7.2	6.8	6.8	6.7
XII	-	-	-	-	0.0	-6.5	11.4	5	-19.3	16	-3.2	-2.5	-3.6	-3.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	10.0	3.2	27.5	2.VII	-19.7	25.1	6.0	8.4	5.9	6.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Częstochowa

$H_s = 281$ m $H_b = 262{,}7$ m $h_w = 21{,}5$ m **1961**

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v		◑	●	Opad R			≡	⊞	☈
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15			R > 0.1	R > 1.0	R > 10.0			
I	1	1.5	7	4.2	14.5	1.5	8	1.4	25.5	2.1	25.5	2.5	7	2.5	4.5	1.0	·	2.0	47.0	7.1	14	10	11	28	·	·	·	5	14	13	5	·	·	23	·
II	·	·	·	·	1	1.0	6.5	4.2	18.5	1.9	27	2.7	16	2.5	10	1.6	5	2.1	43.7	11.9	9		1	15	·	1	·	1	14	14	10	2	6	5	·
III	·	·		·	·	·		·	·	·	25.5	3.4	54.5	3.1	12	4.8	1	3.4	42.8	7.8	29	·	·	6	·	5	·	3	16	16	11	·	2	3	·
IV	8	1.4	3.5	3.1	20.5	2.6	12.5	1.6	8.5	2.5	15.5	2.5	14	1.8	5.5	2.2	2	2.1	60.0	25.2	28	·	·	2	2	1	·	9	5	10	8	2	·	·	2
V	10.5	2.4	3	2.3	6	2.2	3	1.7	3.5	2.1	15	3.1	23	2.0	27	1.6	2	2.1	62.9	12.3	29	·	·	·	·	·	·	·	15	18	12	2	1	·	5
VI	2.5	2.2	4	1.5	9	2.2	4	2.0	10.5	2.3	11	3.2	28.5	2.6	14.5	2.4	6	2.3	72.2	42.6	27	·	·	·	12	2	2	5	6	13	9	1	·	·	8
VII	5.5	1.2	·	·	1	1.0	·		4.5	3.0	26.5	2.9	40.5	2.5	14	1.3	1	2.4	167.5	42.5	31	·	·	·	7	·	·	3	15	16	9	5	·	·	5
VIII	6	1.8	0.5	2.0	3	1.7	3	1.0	1.5	2.3	24.5	2.9	41.5	2.3	10	1.9	3	2.2	50.1	29.1	12	·	·	·	7	1	1	4	8	10	7	1	·	·	1
IX	2.5	1.2	·	·	14	1.7	6.5	1.5	8.5	1.5	21.5	2.1	23.5	2.1	7.5	1.8	6	1.8	21.0	11.8	6	·	·	·	8	·	·	10	5	7	4	1	1	·	1
X	1	2.0	·	·	13	3.0	18.5	1.7	26.5	2.5	10.5	3.1	10.5	2.0	7	1.9	6	2.2	6.5	1.9	19	·	·	·	·	·	·	3	6	6	3	·	2	·	·
XI	12	1.5	1.5	3.0	5.5	2.6	5.5	1.7	12	1.8	33	2.2	7.5	2.8	8	1.8	5	2.0	76.8	25.6	13	·	·	10	·	·	·	3	18	19	13	2	7	3	·
XII	13.5	2.5	5	2.2	1.5	1.3	2	2.0	15.5	2.0	19.5	3.8	14.5	2.1	13.5	2.6	8	2.4	53.6	12.2	11	12	13	26	·		·	3	15	14	10	2	1	24	·
Rok	62.5	1.5	24.5	1.3	89	1.7	69.5	1.3	135	2.0	255	2.9	281	2.4	133.5	2.1	45	2.2	674.1	42.6	27.VI	22	25	87	36	10	3	49	137	156	101	18	20	58	22

Szrenica

$H_s = 1323$ m $H_b = 1363{,}6$ $h_w = 19{,}8$ m

I	4	8.1	3	8.5	14	8.0	6.5	11.9	21.5	13.3	38.5	12.3	25	10.2	1	13.0	2	11.1	82.4	19.2	30	8	29	31	·	26	21	6	18	18	15	2	22	31	·
II	5	10.9	4	3.5	2.5	2.6	2.5	4.4	15	12.2	22	11.0	18	8.9	13	9.9	2	9.5	71.1	42.9	9	2	15	25	·	24	11	2	18	16	15	1	21	28	·
III	10	9.8	4	7.4	0.5	5.0	·	·	1	14.0	21.5	13.2	31	13.5	25	12.4	·	12.4	106.0	19.7	30	1	12	27	·	31	20	1	22	21	19	4	24	31	·
IV	3	5.2	11	4.8	16	4.6	6	7.1	19	15.8	22	8.6	9	13.2	1	13.0	3	8.9	130.9	36.6	16	·	1	7	·	20	12	1	13	13	10	6	15	8	6
V	10	7.5	14	8.4	7	5.1	0.5	3.0	12.5	10.4	24	9.0	12	8.8	11	7.7	2	8.2	212.7	41.5	27	·		11	·	22	8	·	24	26	23	6	23	13	4
VI	9.5	4.5	10	4.4	13	5.2	3.5	9.4	14	9.4	23.5	7.0	9	7.3	7.5	8.7	·	6.8	106.1	27.1	13	·	·	·	·	20	6	2	13	16	13	3	17	·	9
VII	4	9.5	1.5	3.0	2.5	2.2	1	4.0	7.5	1.4	43.5	10.3	25	8.6	8	9.1	·	9.6	251.5	42.8	28	·	·	·	·	25	12	·	20	24	20	9	24	·	4
VIII	3.5	5.1	6	4.0	3.5	4.0	0.5	7.0	8	9.1	43.5	11.0	21	10.9	7	6.9	·	9.6	142.4	18.7	11	·	·	·	·	23	10	2	17	23	21	6	23	·	2
IX	1	9.0	0.5	2.0	7.5	2.8	11	4.2	10.5	11.1	22.5	11.1	22.5	7.9	14.5	6.6	·	8.0	73.8	25.5	14	·	·	·	·	18	9	8	7	15	8	2	13	·	3
X	3.5	7.0	2.5	7.2	8.5	7.1	23	13.3	22	16.2	9.5	12.1	15.5	9.7	4.5	5.8	4	11.4	82.8	27.9	17	·	·	6	·	23	16	2	15	16	9	2	25	1	·
XI	8	10.2	1.5	8.3	5.5	6.8	14.5	7.3	17.5	12.7	15.5	12.7	11.5	9.7	14	6.6	2	9.6	100.0	27.1	13	·	10	25	·	23	12	·	22	23	14	3	22	17	·
XII	4.5	13.0	17	9.5	10.5	9.3	8	10.1	10	12.8	27	15.5	7.5	12.5	8.5	10.5	·	12.1	130.9	39.1	11	14	21	28	·	26	16	2	15	23	12	5	24	28	1
Rok	66	8.3	75	5.9	91	5.2	77	6.6	158.5	11.5	313	11.2	184.5	10.1	115	9.2	15	9.8	1490.6	42.8	28.VII	25	88	160	·	281	153	26	204	234	179	49	253	157	29

Uwaga. Kierunki i prędkości wiatru – wg anemografu.

Szczawno – Zdrój

$H_s = 415$ m $h_w =$ 11,5 m I–IV; 13 m V–XII

I	2	1.0	1	1.0	3	1.7	·	·	7	5.4	48	4.4	10	2.1	·		22	3.0	18.0	7.0	14	8	12	26	·	4	·	7	11	7	5	·	5	19	·
II	·	·	·	·	·	·	·	·	2	3.0	34	3.4	28	2.9	3	3.0	17	2.5	31.9	9.5	9	·	1	9	·	1	·	6	12	13	9	·	·	6	·
III	·	·	·	·		·	·	·	·	·	13	2.8	53	3.3	·	·	27	2.3	39.0	9.3	30	·	·	8	·	·	·	5	10	16	10	·	3	3	·
IV	2	2.0	5	2.4	5	2.4	2	3.5	2	2.0	14	2.7	14	1.9	4	1.8	42	1.2	51.7	8.9	15	·	·	2	·	·	·	5	7	13	10	·	4	·	5
V	8	1.5	1	2.0	·	·	·	·	5	1.8	10	2.0	18	3.7	16	1.7	35	1.5	111.4	24.2	29	·		·		·		·	18	21	15	3	4	·	6
VI	3	1.0	2	1.0	4	1.5	·	·	7	1.9	9	2.3	14	2.6	13	2.3	38	1.2	54.7	25.0	10	·	·	·	4	·	·	9	9	12	9	1	1	·	3
VII	·	·	2	1.0	·		·	·	4	1.5	13	1.8	39	1.9	7	2.0	28	1.3	115.7	22.7	28	·	·	·	5	·	·	5	16	13	11	5	·	·	1
VIII	4	1.0	·	·	2	1.0	·	·	5	2.6	16	4.2	19	2.3	5	2.4	42	1.5	77.8	17.7	11	·	·	·	4	2	·	4	7	17	12	3	2	·	3
IX	4	1.0	·	·	4	1.8	·	·	17	2.8	10	4.2	14	1.8	1	1.0	40	1.4	31.0	14.0	26	·	·	·	9	1	·	11	6	8	5	1	5	·	5
X	·	·	·	·	7	1.4	4	3.0	10	3.4	22	2.9	7	1.7	·	·	43	1.4	42.7	18.6	20	·	·	·	·	2	·	8	11	8	7	1	2	·	·
XI	4	1.5	2	1.0	4	1.2	·	·	7	2.1	16	3.2	10	2.8	3	1.0	44	1.2	48.7	11.4	13	·	·	9	·	1	1	3	22	13	8	2	9	·	·
XII	3	2.3	·	·	·	·	2	2.0	9	5.4	20	9.0	15	2.7	5	3.2	39	3.2	51.8	22.5	11	11	12	23	·	4	3	6	19	11	6	1	3	19	·
Rok	30	0.9	13	0.7	29	0.9	8	0.7	75	2.7	225	3.6	241	2.5	57	1.5	417	1.8	674.4	25.0	10.VI	19	25	77	22	15	4	69	148	152	107	17	38	47	23

Bierutowice

$H_s = 860$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	51.2	17.0	31	6	10	30	·	–	–	–	–	14	8	2	4	24	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	53.2	13.6	9	·	4	21	·	–	–	–	–	18	13	1	6	23	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	99.9	15.8	21	·	3	16	·	–	–	–	–	20	15	3	3	12	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	77.8	17.1	3	·	·	4	·	–	–	–	–	14	11	5	6	·	7
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	187.6	30.8	29	·	·	1	·	–	–	–	–	20	17	6	9	2	4
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	76.1	23.5	11	·	·	·	·	–	–	–	–	14	13	2	4	·	4
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	138.4	40.4	30	·	·	·	2	–	–	–	–	14	12	3	3	·	1
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	93.3	27.2	11	·	·	·	1	–	–	–	–	18	14	2	1	·	1
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	25.9	9.2	5	·	·	·	1	–	–	–	–	7	5	·	5	·	2
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	68.8	24.6	17	·		·	·	–	–	–	–	10	8	2	6	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	147.3	38.0	5	·	4	14	·	–	–	–	–	18	13	4	12	14	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	130.3	36.4	11	10	14	23	·	–	–	–	–	19	13	4	3	19	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1149.8	40.4	30.VII	16	35	109	4	–	–	–	–	186	142	34	62	814	19

Karpacz

$\varphi = 50°46'$ $\lambda = 15°45'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	932.8	950.5	912.9	-	-0.4	-5.7	5.2	3	-17.2	26	-3.3	-1.5	-3.1	-2.8	3.9	4.0	4.0	4.0	78	71	79	76	1.1	1.6	1.1	1.3	4.7	5.8	5.5	5.3
II	937.2	952.5	907.0	-	4.8	-1.1	14.1	18	-9.0	6	0.8	3.5	1.2	1.7	5.5	5.8	5.7	5.7	84	76	85	82	1.1	2.3	1.1	1.5	6.7	6.5	5.4	6.2
III	936.4	952.3	911.4	-	6.8	0.3	15.0	10	-6.5	20	2.1	5.3	3.4	3.6	5.5	6.1	5.9	5.8	78	70	76	75	1.8	3.2	2.2	2.4	7.5	7.7	6.9	7.4
IV	929.8	937.9	920.5	-	13.1	4.3	21.0	7	-3.6	1	7.7	11.7	7.8	8.8	8.4	8.9	8.7	8.7	80	66	82	76	2.4	5.4	2.2	3.3	5.3	6.3	4.3	5.3
V	931.1	937.5	919.8	-	11.1	4.6	19.3	26	0.3	13	7.3	9.3	7.0	7.6	8.9	9.2	9.0	9.0	87	79	89	85	1.6	2.9	1.2	1.9	8.0	8.7	7.0	7.9
VI	934.7	947.3	923.2	-	18.7	10.0	25.0	25	5.4	16	13.5	16.9	13.2	14.2	12.8	14.2	13.1	13.4	82	74	86	81	3.1	5.5	2.4	3.7	6.2	6.3	5.2	5.9
VII	933.5	944.0	919.6	-	16.6	9.5	27.0	3	5.4	6	12.2	15.1	12.0	12.8	11.7	11.5	11.2	11.5	82	68	80	77	2.9	6.4	3.2	4.2	7.5	6.9	6.5	7.0
VIII	936.0	946.9	926.4	-	17.5	10.2	26.3	6	5.0	14	12.8	16.1	13.1	13.8	12.5	13.1	12.5	12.7	84	72	82	79	2.6	5.8	2.9	3.8	6.8	7.1	5.0	6.3
IX	937.2	946.5	926.1	-	18.2	10.8	25.6	3	6.2	20	13.1	17.6	13.4	14.4	11.6	12.6	11.7	12.0	77	64	76	72	4.0	8.2	4.1	5.4	4.9	4.9	2.3	4.0
X	934.5	947.0	908.3	-	12.1	6.5	18.4	1	2.2	22	8.0	11.1	8.5	9.0	8.7	9.7	8.9	9.1	82	74	81	79	2.2	3.8	2.4	2.8	5.7	6.9	4.0	5.5
XI	930.7	950.4	919.6	-	5.0	0.4	10.2	1	-6.0	21	1.9	3.5	2.8	2.8	6.1	6.4	6.3	6.3	85	81	84	83	1.1	1.7	1.3	1.4	7.5	7.6	7.3	7.5
XII	931.1	953.5	914.7	-	0.2	-6.9	12.3	5	-21.7	16	-3.7	-1.9	-3.3	-3.0	4.5	4.8	4.6	4.6	87	84	86	86	0.8	1.2	1.0	1.0	6.9	6.5	5.3	6.2
Rok	933.8	953.5	907.0	-	10.3	3.6	27.0	3.VII	-21.7	16.XII	6.0	8.9	6.3	6.9	8.3	8.9	8.5	8.6	82	73	82	79	2.1	4.0	2.1	2.7	6.5	6.8	5.4	6.2

Dobrogoszcz

$\varphi = 50°46'$ $\lambda = 17°01'$

I	-	-	-	-	1.1	-6.1	10.3	4	-20.0	27	-3.3	0.3	-2.7	-2.1	-	-	-	-	-	-	-	-	-	-	-	-	6.4	6.0	6.0	6.1
II	-	-	-	-	6.9	0.3	14.2	18	-5.4	6	1.8	5.8	2.8	3.3	-	-	-	-	-	-	-	-	-	-	-	-	7.0	6.2	5.1	6.1
III	-	-	-	-	10.8	2.2	19.7	10	-4.4	20	4.4	9.8	5.9	6.5	-	-	-	-	-	-	-	-	-	-	-	-	7.3	7.1	5.9	6.8
IV	-	-	-	-	17.1	5.1	26.1	7	-1.4	10	8.8	16.1	10.3	11.4	-	-	-	-	-	-	-	-	-	-	-	-	4.9	5.3	5.4	5.2
V	-	-	-	-	16.1	6.8	22.9	26	2.8	13	10.1	14.7	10.4	11.4	-	-	-	-	-	-	-	-	-	-	-	-	7.5	7.5	7.5	7.5
VI	-	-	-	-	22.6	11.0	28.5	25	5.5	16	16.0	20.8	16.0	17.2	-	-	-	-	-	-	-	-	-	-	-	-	6.0	5.8	5.5	5.8
VII	-	-	-	-	21.1	10.9	31.0	3	5.9	8	15.1	19.1	14.9	16.0	-	-	-	-	-	-	-	-	-	-	-	-	6.9	7.8	6.8	7.2
VIII	-	-	-	-	21.7	11.9	31.3	6	7.3	4	15.1	20.2	15.3	16.5	-	-	-	-	-	-	-	-	-	-	-	-	6.5	7.6	5.6	6.5
IX	-	-	-	-	22.6	10.0	30.0	2	4.0	23	13.0	21.4	14.8	16.0	-	-	-	-	-	-	-	-	-	-	-	-	5.4	4.5	4.8	4.9
X	-	-	-	-	16.2	6.6	23.1	6	4.5	16	8.2	15.5	10.4	11.1	-	-	-	-	-	-	-	-	-	-	-	-	7.5	6.2	4.6	6.1
XI	-	-	-	-	7.1	2.2	13.2	2	-2.9	21	3.7	6.1	4.2	4.6	-	-	-	-	-	-	-	-	-	-	-	-	7.8	8.0	6.7	7.5
XII	-	-	-	-	1.4	-7.0	18.2	5	-23.0	26	-2.7	-0.5	-2.7	-2.2	-	-	-	-	-	-	-	-	-	-	-	-	7.5	6.2	5.2	6.3
Rok	-	-	-	-	13.7	4.5	31.3	6.VIII	-23.0	26.XII	7.5	12.4	8.3	9.1	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.5	5.8	6.3

Werbkowice

$\varphi = 50°45'$ $\lambda = 23°46'$

I	-	-	-	-	-2.0	-9.7	4.7	4	-24.6	27	-6.6	-3.2	-6.0	-5.4	-	-	-	-	-	-	-	-	-	-	-	-	8.1	6.4	4.9	6.5
II	-	-	-	-	2.5	-1.6	9.2	28	-6.0	6,7	-0.9	1.7	0.3	0.4	-	-	-	-	-	-	-	-	-	-	-	-	8.1	8.6	7.9	8.2
III	-	-	-	-	7.5	0.9	19.0	18	-4.3	23	2.5	6.8	3.9	4.3	-	-	-	-	-	-	-	-	-	-	-	-	8.3	8.0	4.6	7.0
IV	-	-	-	-	16.5	3.6	25.1	7	-2.8	10	6.7	15.0	8.9	9.9	-	-	-	-	-	-	-	-	-	-	-	-	4.2	5.2	3.3	4.2
V	-	-	-	-	17.8	5.8	26.4	29	0.3	17	10.2	16.1	10.7	11.9	-	-	-	-	-	-	-	-	-	-	-	-	6.5	7.5	6.9	7.0
VI	-	-	-	-	24.0	10.7	31.7	27	5.6	29	16.2	22.1	16.2	17.7	-	-	-	-	-	-	-	-	-	-	-	-	4.1	5.5	4.8	4.8
VII	-	-	-	-	23.4	10.5	31.5	4	5.1	8	14.8	21.7	15.5	16.9	-	-	-	-	-	-	-	-	-	-	-	-	5.7	6.5	6.0	6.1
VIII	-	-	-	-	22.5	11.1	33.1	11	5.2	31	14.3	21.2	15.6	16.7	-	-	-	-	-	-	-	-	-	-	-	-	5.8	6.5	5.3	5.9
IX	-	-	-	-	21.1	7.3	29.0	18	-3.8	23	9.4	19.8	12.5	13.6	-	-	-	-	-	-	-	-	-	-	-	-	5.3	5.0	3.0	4.4
X	-	-	-	-	16.1	3.5	21.4	19	-2.5	12	5.2	15.3	8.7	9.5	-	-	-	-	-	-	-	-	-	-	-	-	7.2	4.7	2.7	4.9
XI	-	-	-	-	6.9	1.1	14.6	3	-6.9	23	2.6	5.9	3.8	4.0	-	-	-	-	-	-	-	-	-	-	-	-	9.1	8.5	8.4	8.7
XII	-	-	-	-	-1.0	-8.8	16.2	5	-24.3	26	-5.0	-2.8	-5.0	-4.4	-	-	-	-	-	-	-	-	-	-	-	-	8.7	8.0	6.9	7.9
Rok	-	-	-	-	12.9	2.9	33.1	11.VIII	-24.6	27.I	5.8	11.6	7.1	7.9	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.7	5.4	6.3

Śnieżka

$\varphi = 50°44'$ $\lambda = 15°44'$

I	831.3	846.7	814.0	-	-4.3	-9.3	1.2	16	-18.3	26	-7.0	-6.6	-6.8	-6.8	2.8	2.9	2.9	2.9	74	74	77	75	0.9	0.9	0.8	0.9	6.1	6.4	6.3	6.3
II	836.8	853.3	808.7	-	-0.2	-4.7	7.2	18	-11.8	6	-2.5	-2.1	-2.5	-2.4	3.7	4.0	4.1	3.9	77	79	81	79	1.6	1.5	1.3	1.5	6.8	7.1	5.9	6.6
III	835.8	852.5	810.4	-	0.3	-4.9	8.5	10	-13.5	20	-3.0	-1.3	-2.2	-2.2	4.0	4.5	4.2	4.2	83	83	83	83	1.1	1.3	1.2	1.2	7.9	8.2	7.7	7.9
IV	832.3	838.9	823.3	-	5.7	0.0	11.9	7	-9.1	1	2.2	4.2	2.6	2.9	5.8	6.8	6.7	6.4	80	83	91	85	1.6	1.6	0.8	1.3	6.7	7.3	6.8	6.9
V	833.0	839.1	823.2	-	3.6	0.0	11.2	26	-4.0	12	1.2	2.3	1.9	1.8	6.4	6.9	6.7	6.7	95	95	94	95	0.4	0.4	0.5	0.4	8.9	9.3	8.6	8.9
VI	838.9	850.6	827.1	-	11.2	5.5	17.0	25	0.3	16	7.1	9.3	8.2	8.2	8.9	9.9	9.9	9.6	88	85	90	88	1.4	2.0	1.2	1.5	6.7	7.2	6.4	6.8
VII	837.0	849.6	825.4	-	8.7	3.9	19.4	2	-1.4	5	5.5	6.7	6.1	6.1	8.6	8.7	8.8	8.7	94	89	93	92	0.8	1.6	0.9	1.1	8.1	8.6	7.7	8.1
VIII	839.8	851.8	828.6	-	10.3	5.5	19.6	10	0.2	16	6.8	8.4	7.6	7.6	9.1	10.2	9.7	9.7	91	92	91	91	1.1	1.3	1.1	1.2	7.8	8.3	6.8	7.6
IX	841.7	851.8	828.3	-	12.4	7.4	20.4	18	0.6	8	9.0	11.0	9.5	9.8	7.8	9.6	8.5	8.6	71	75	74	73	4.0	4.1	3.7	3.9	5.3	5.6	3.9	4.9
X	837.3	850.3	811.6	-	6.4	1.2	12.9	27	-2.9	20,22	3.1	4.8	3.4	3.6	6.4	7.1	6.5	6.7	85	84	86	85	1.5	1.6	1.5	1.5	6.8	7.5	6.0	6.8
XI	831.5	847.8	821.3	-	0.6	-3.3	8.4	23	-10.1	20	-1.2	-0.6	-1.4	-1.2	4.5	4.7	4.6	4.6	82	82	84	83	1.3	1.4	1.0	1.2	8.2	7.9	8.1	8.1
XII	829.2	845.9	816.3	-	-4.1	-10.0	5.2	5	-24.9	16	-7.4	-6.8	-7.2	-7.2	3.3	3.4	3.2	3.3	80	80	80	80	0.6	0.7	0.7	0.7	7.4	7.7	6.8	7.3
Rok	835.4	853.3	808.7	-	4.2	-0.7	20.7	18.IX	-24.9	16.XII	4.2	2.4	1.6	1.7	5.9	6.6	6.3	6.3	83	83	85	84	1.4	1.5	1.2	1.4	7.2	7.6	6.8	7.2

Karpacz

$H_s = 700$ m $H_b = 708,0$ m $h_w = 16$ m

ROZKŁAD WIATRU (%D, %mD) · OPAD R · LICZBA DNI (n)

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	⚡
I	7	2.4	5	2.4	·	·	2.5	6.4	16.5	9.2	3	2.2	1.5	2.7	5.5	3.8	52	2.5	52.4	17.0	31	7	13	28	·	7	2	5	5	14	9	2	2	24	·
II	4.5	2.2	2	4.0	·	·	2.5	3.6	7.5	6.3	6	4.9	6	2.2	16.5	3.7	39	2.0	55.5	15.1	9	·	3	17	·	2	1	7	15	18	14	1	5	14	·
III	9.5	3.2	0.5	4.9	·	·	0.5	2.0	3	5.3	11.5	5.5	18	3.5	28	4.1	22	3.1	92.3	15.4	30	·	2	14	·	5	·	2	17	17	13	3	2	12	·
IV	2.5	1.4	0.5	2.0	1	2.5	8.5	4.5	15	6.5	4	2.1	3	3.7	7.5	3.1	48	2.1	93.5	19.0	3	·	·	4	·	3	2	6	7	15	12	4	3	·	7
V	5	3.3	2.5	2.2	·	·	2.5	4.0	6	5.8	9	2.7	2.5	2.8	15.5	3.5	50	1.6	212.8	30.9	29	·	·	·	·	·	·	·	17	24	18	8	6	1	4
VI	3	2.2	·	·	1	1.0	6	5.8	5.5	3.5	3.5	3.0	3.5	2.6	16.5	3.2	51	1.5	101.6	27.0	10	·	·	·	·	1	·	4	9	17	12	3	7	·	9
VII	5.5	2.6	1	2.0	0.5	2.0	4.5	4.8	4	5.6	8	3.6	19.5	3.4	13	3.8	37	2.2	185.7	35.9	30	·	·	·	2	2	·	2	14	19	14	5	1	·	4
VIII	2	1.5	2.5	1.0	·	·	2	2.0	6	2.6	12.5	3.5	16.5	3.7	10.5	3.4	41	1.8	87.8	21.2	11	·	·	·	1	1	1	2	9	20	15	2	4	·	2
IX	5	4.7	5.5	1.3	1	3.0	2	3.0	11	6.2	10	4.4	6.5	3.6	4	2.0	45	1.9	37.9	10.7	5	·	·	·	1	1	·	10	3	12	7	1	3	·	5
X	1	1.0	0.5	2.0	3	3.8	12.5	8.9	19.5	9.7	1.5	3.7	1.5	3.0	5.5	2.6	48	3.6	79.3	33.2	17	·	·	·	·	9	5	7	10	9	7	3	4	·	·
XI	2	2.0	·	·	0.5	3.0	4.5	5.0	3	8.3	10	4.4	4	3.1	13	2.5	53	1.6	85.4	32.9	13	·	3	12	·	2	·	3	17	20	9	2	8	4	·
XII	1.5	3.3	1.5	1.7	·	·	2.5	10.6	12	5.3	2	8.5	5.5	4.7	17	3.9	51	2.2	128.5	36.6	11	13	16	24	·	4	·	4	10	17	10	5	2	22	·
Rok	48.5	2.2	21.5	1.5	7	1.3	50.5	5.0	109	6.2	81	4.0	88	3.2	152.5	3.3	537	2.2	1212.7	36.6	11.XII	20	37	99	4	37	11	52	133	202	140	39	47	77	31

Dobrogoszcz

$H_s = 175$ m $h_w = 15,5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	⚡
I	2	1.2	6	2.5	6	2.0	9	1.3	49.5	3.0	27	4.4	5	2.1	6.5	2.3	42	2.6	10.5	3.0	14	12	10	24	·	3	2	6	12	9	4	·	1	16	–
II	2	2.2	0.5	1.0	0.5	1.0	5	1.1	28.5	3.9	14	6.6	8	6.8	12.5	5.6	13	4.0	23.1	5.6	9	·	·	11	·	6	1	6	11	12	7	·	1	3	–
III	2.5	3.2	·	·	·		2	3.2	5.5	2.3	13.5	6.1	37.5	5.5	27	7.0	5	5.5	27.3	7.3	14	·	·	7	-	11	1	2	14	13	9	·	·	·	–
IV	9	1.9	7	1.6	9	2.6	13.5	2.5	12	2.8	9.5	4.3	3.5	3.4	11.5	4.4	15	2.5	88.9	42.4	27	·	·	2	2	3		7	9	12	8	2	2	·	–
V	10	2.0	3	1.7	3	2.5	6.5	1.1	8	1.2	12	3.3	15.5	3.6	27	3.6	8	2.6	77.2	33.2	27			·	·	3		1	14	16	14	2	·	·	–
VI	1.5	2.0	3	2.3	7	1.5	4.5	1.3	11	1.3	9.5	2.6	13.5	2.6	22	3.1	48	1.9	121.5	48.9	8	·	·	·	7	·		3	8	14	12	4	·	·	–
VII	0.5	1.0	·	·	5	1.0	6.5	1.6	9.5	1.2	13.5	3.7	30.5	2.6	16.5	2.7	11	2.2	88.1	22.6	28	·	·	·	6	1		2	15	13	10	3	·	·	–
VIII	5.5	1.8	1.5	1.3	4	1.5	6.5	1.3	14	1.7	21	3.1	14	3.0	12.5	2.4	14	2.0	88.3	21.3	11	·	·	·	6	·	·	2	10	15	13	4	·	·	–
IX	1.5	1.0	0.5	1.0	5.5	1.9	8	2.4	15.5	2.3	12	3.8	11	3.7	9	2.3	27	1.9	43.1	4.3	14	·	·	·	9	1	·	10	9	8	6	·	1	·	–
X	1.5	3.0	1	3.0	8.5	5.6	18.5	3.5	26	3.7	10.5	4.3	9.5	1.9	10.5	3.1	7	3.4	46.8	16.9	20	·	·	·	·	5	1	4	10	7	6	2	2	·	–
XI	9	1.8	5	1.5	9	1.3	7	1.2	25	1.8	12.5	5.8	6.5	3.6	10	2.2	6	2.3	57.4	13.0	6	·	·	7	·	2	·	2	16	12	9	2	4	·	–
XII	7.5	2.0	2.5	2.0	1	1.0	9	1.4	16	5.1	15	7.3	7	6.1	23	3.9	12	3.9	26.4	9.6	11	12	13	24	·	7	1	4	11	12	5	·	·	15	–
Rok	52.5	1.9	30	1.5	58.5	1.8	96	1.8	190.5	2.5	170	4.6	161.5	3.7	188	3.6	148	2.9	668.6	48.9	8.VI	24	23	75	30	42	6	49	139	143	103	19	11	34	–

Werbkowice

$H_s = 204$ m $h_w =$ 12 m I–VIII, 14 m IX–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	⚡
I	7.5	2.8	8	2.2	·	·	6	2.2	14.5	2.2	32	2.4	13	2.8	11	2.9	1	2.4	13.0	3.5	2,14	13	16	31	·	·	·	4	12	12	5	·	1	31	·
II	1	2.0	2.5	2.4	4	2.1	15.5	2.6	10.5	2.7	14.5	2.1	21.5	2.6	13.5	2.2	1	2.4	40.2	2.7	12	·	2	20	·	·	·	2	19	13	4	·	4	13	·
III	0.5	3.0	·	·	·	·	2	2.5	2.5	3.6	11	2.9	45	3.9	31	3.9	1	3.7	24.7	3.8	12,18,28	·	·	10	·	2	2	1	11	19	6	·	3	1	·
IV	7.5	2.5	1.5	2.7	8.5	3.1	20.5	3.1	8	2.2	10.5	2.6	21	2.8	10.5	3.0	2	2.7	37.2	13.5	8	·	·	3	1	1	·	7	4	8	7	1	·	·	3
V	24	1.9	4	1.8	1.5	2.7	19.5	2.1	8.5	1.8	4.5	1.7	12	2.7	16	2.5	3	2.1	54.7	24.0	30	·	·	·	3	·	·	2	13	13	10	2	·	·	1
VI	13	1.9	7.5	1.9	6.5	2.0	20	1.8	6.5	1.8	7	2.1	5	2.6	14.5	2.6	10	1.8	52.2	13.3	4	·	·	·	12	·	·	2	6	14	6	3	·	·	4
VII	7	1.7	3.5	2.0	3.5	2.0	12	2.0	8.5	2.1	7.5	2.7	25.5	2.5	24.5	2.0	1	2.1	100.2	36.1	30	·	·	·	10	·	·	4	11	11	9	3	·	·	4
VIII	10	2.4	1.5	2.7	·	·	·	·	11.5	2.4	13	2.6	25	2.7	28	2.4	4	2.4	49.9	17.9	12	·	·	·	7	·	·	4	7	13	6	2	·	·	3
IX	7.5	2.1	10.5	1.9	8.5	2.2	8	1.7	6	2.6	10.5	2.8	19	2.6	12	2.8	9	2.2	5.7	3.4	14	·	·	3	5	1	·	11	8	6	2	·	2	·	1
X	2	3.5	6	2.7	11	2.7	37	3.3	11.6	2.7	5.5	2.7	6	4.5	7	3.7	7	2.9	8.4	5.5	30	·	·	2	·	·	·	7	6	4	2	·	9	·	·
XI	5	4.2	0.5	3.0	11	3.0	17	3.1	11	2.3	14.5	4.3	21.5	4.9	4.5	5.2	5	3.6	34.3	7.6	12	·	1	11	·	1	·	1	23	14	9	·	5	·	·
XII	12.5	6.4	7	2.1	3.5	2.9	6.5	2.0	12	2.2	15.5	5.8	13.5	6.4	13.5	7.4	9	4.5	23.2	6.1	7	12	18	25	·	7	2	·	19	9	5	·	2	25	·
Rok	97.5	2.9	52.5	2.1	58	1.9	164	2.2	110	2.4	146	2.9	228	3.4	186	3.4	53	2.7	410.7	36.1	30.VII	25	37	105	38	12	4	45	139	136	71	11	26	70	16

Śnieżka

$H_s = 1603$ m $H_b = 1610,6$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	⚡
I	7	8.9	4.5	14.7	4.5	11.6	8	6.6	10.5	11.4	33	18.5	16.5	11.0	6	6.9	3	12.8	69.7	10.3	14	7	29	31	·	29	20	9	15	17	16	1	22	31	·
II	15.5	11.6	1	2.5	2.5	8.0	1.5	5.3	5.5	12.9	49	16.6	14.5	13.9	22.5	13.0	2	13.0	124.1	27.5	9	3	15	23	·	25	20	6	14	19	16	3	20	28	·
III	9.5	9.6	·	·	·	·	·	·	1	25.0	13.5	18.1	30.5	14.9	38.5	15.6	·	15.3	133.1	31.9	21	3	17	28	·	31	28	2	18	22	16	4	25	29	·
IV	11	4.8	4.5	7.0	3	3.5	6	6.8	14.5	12.3	18	11.8	25.5	13.9	6.5	4.4	1	10.0	69.7	13.5	30	·	1	14	·	22	13	·	12	15	12	3	22	12	6
V	4.5	9.1	2.5	4.8	0.5	3.0	2	3.2	5.5	4.3	14.5	10.1	27.5	11.1	35	9.1	1	9.2	227.3	31.6	21	·	6	16	·	23	11	·	25	27	18	8	29	17	4
VI	18.5	8.1	2.5	6.0	4	6.8	2	4.8	7	8.2	17.5	8.5	22.5	9.8	16	9.2	1	8.5	93.3	15.6	8	·	·	·	·	27	8	3	13	18	12	3	24	·	6
VII	3	3.0	·	·	·	·	·	·	3	9.0	26.5	11.4	41	10.8	17.5	7.0	2	9.7	181.1	38.2	30	·	·	2	·	25	16	1	22	23	18	6	24	·	4
VIII	6	4.5	·	·	·	·	·	·	3.5	5.7	28	12.9	34.5	10.6	20	9.7	1	10.4	108.4	18.2	12	·	·	·	·	26	16	1	16	22	17	2	24	·	2
IX	5	8.1	1.5	3.7	2.5	4.0	4	5.4	2.5	12.4	24	11.1	34.5	8.4	16	8.6	·	8.9	49.2	8.6	5	·	·	·	·	17	11	8	8	13	11	·	16	·	4
X	12	7.5	1	6.0	2	6.8	10.5	10.6	9	12.7	36.5	17.6	14.5	7.0	7.5	8.0	·	12.3	70.6	23.1	20	·	·	9	·	28	19	3	14	20	9	2	27	1	·
XI	18.5	8.9	2.5	10.8	2.5	4.4	2.5	11.8	16	8.2	20	13.0	14.5	10.3	12.5	9.6	1	10.1	104.9	25.8	13	4	11	25	·	24	13	1	20	22	15	3	24	9	·
XII	14.5	11.3	3.5	10.6	1	8.0	6	9.2	6.5	9.3	29	17.0	11	12.0	21.5	13.0	·	13.2	96.7	17.7	12	16	22	30	·	29	22	3	15	23	16	4	26	26	·
Rok	125	8.0	23.5	5.5	22.5	4.7	42.6	6.3	84.6	11.0	279.5	13.9	287	11.1	218.5	9.5	12	11.1	1325.1	38.2	30.VII	38	101	178	·	299	197	37	192	239	176	39	283	153	26

Zamość — φ = 50°44' — λ = 23°15' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	994,0	1012,7	974,8	1022,1	-1,5	-9,4	6,9	4	-24,1	26	-6,5	-2,8	-5,7	-5,2	3,8	4,3	4,1	4,1	89	81	90	87	0,5	1,0	0,4	0,6	7,1	5,4	4,7	5,7
II	996,0	1011,0	968,6	1023,6	3,0	-1,4	9,4	28	-5,9	6	-0,6	2,2	0,6	0,7	5,5	5,9	5,7	5,7	92	82	89	88	0,4	1,4	0,7	0,8	7,9	7,6	8,1	7,9
III	990,0	1008,0	971,0	1017,0	8,8	1,2	19,4	18	-3,8	23	3,0	6,8	4,4	4,6	6,9	7,0	7,1	7,0	90	70	84	81	0,8	3,2	1,5	1,8	8,4	7,8	5,0	7,1
IV	987,7	997,5	977,9	1014,1	16,6	4,2	25,6	15	-3,0	10	7,4	15,2	9,5	10,4	8,1	8,4	8,9	8,5	77	48	73	66	2,5	9,6	3,3	5,1	4,6	5,0	2,8	4,1
V	986,1	994,0	974,2	1012,3	17,1	6,8	26,0	29	1,5	17	10,0	15,7	11,1	12,0	10,6	10,6	11,2	10,8	86	61	84	77	1,9	8,2	2,2	4,1	6,8	7,1	5,8	6,6
VI	989,7	1001,7	980,8	1015,5	24,4	11,6	32,7	27	6,5	21	16,5	22,2	16,7	18,0	15,0	14,6	15,3	15,0	79	56	80	72	4,0	13,0	3,9	7,0	4,4	6,2	4,4	5,0
VII	988,4	999,1	974,7	1014,3	23,6	11,4	32,0	4	7,1	9	15,2	21,5	15,8	17,1	14,1	13,7	14,7	14,2	82	55	82	73	3,4	12,6	3,6	6,5	4,9	6,4	5,1	5,5
VIII	990,6	1002,3	978,9	1016,5	22,8	12,2	33,8	11	6,6	31	14,6	21,3	16,1	17,0	14,8	14,9	15,6	15,1	88	59	84	77	2,2	11,4	3,1	5,6	5,2	5,7	5,2	5,4
IX	993,6	1004,5	982,8	1019,8	21,1	8,7	29,1	3	-0,4	22,23	10,4	19,8	13,0	14,0	11,6	12,3	12,5	12,1	90	54	82	75	1,5	11,7	2,8	5,3	4,5	4,1	3,3	4,0
X	995,2	1005,3	975,5	1021,8	16,5	4,5	22,5	19	-2,2	12	5,9	15,6	8,9	9,8	8,7	9,9	9,2	9,3	91	58	80	76	0,8	8,1	2,3	3,7	5,3	4,3	3,3	4,3
XI	988,7	1008,1	976,6	1015,8	7,2	1,4	15,3	3	-5,8	23	2,9	6,2	4,1	4,3	7,4	7,9	7,7	7,7	94	82	91	89	0,6	2,0	0,7	1,1	8,5	8,0	7,7	8,1
XII	988,9	1014,2	972,0	1016,8	-0,6	-7,8	17,2	5	-23,0	25	-4,5	-2,4	-4,6	-4,0	4,4	4,9	4,5	4,6	88	85	89	87	0,7	1,1	0,6	0,8	7,9	7,3	6,8	7,3
Rok	990,7	1014,2	968,6	1017,4	13,2	3,6	33,8	11.VIII	-24,1	26.1	6,2	11,8	7,5	8,2	9,2	9,5	9,7	9,5	87	66	84	79	1,6	6,9	2,1	3,5	6,3	6,2	5,2	5,9

Zdanów — φ = 50°43' — λ = 21°33'

I	–	–	–	–	-1,4	-8,7	6,2	4	-20,2	26	-6,4	-3,4	-5,2	-5,0	–	–	–	–	–	–	–	–	–	–	–	–	7,4	6,3	5,5	6,4
II	–	–	–	–	3,2	-1,9	9,2	18	-7,4	5	-0,7	1,9	0,3	0,4	–	–	–	–	–	–	–	–	–	–	–	–	8,7	7,8	6,5	7,7
III	–	–	–	–	8,5	1,3	18,4	18	-2,4	20,21,23	2,8	6,9	4,2	4,5	–	–	–	–	–	–	–	–	–	–	–	–	8,0	7,2	6,0	7,1
IV	–	–	–	–	15,9	4,5	23,5	15	-1,2	10	6,8	14,2	9,4	10,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16,2	6,6	24,9	29	1,5	13	9,7	14,3	10,4	11,2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23,2	11,2	30,8	27	6,5	16	15,6	21,5	15,4	17,0	–	–	–	–	–	–	–	–	–	–	–	–	4,2	4,1	4,9	4,4
VII	–	–	–	–	21,9	10,3	29,3	3	6,1	6	14,5	19,8	14,6	15,9	–	–	–	–	–	–	–	–	–	–	–	–	4,8	6,0	5,5	5,4
VIII	–	–	–	–	22,2	11,6	32,7	11	6,7	17	14,4	20,6	15,1	16,3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20,6	8,9	28,8	2	2,4	24	11,1	19,2	13,7	14,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15,8	–	22,6	19	–	–	6,5	14,7	9,5	10,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6,3	0,7	13,5	3	-5,7	21,23	2,5	5,1	3,1	3,5	–	–	–	–	–	–	–	–	–	–	–	–	9,4	7,9	7,4	8,2
XII	–	–	–	–	-1,3	–	13,8	5	–	–	-5,3	-3,7	-4,5	-4,4	–	–	–	–	–	–	–	–	–	–	–	–	6,9	6,2	6,7	6,6
Rok	–	–	–	–	12,6	–	32,7	11.VIII	–	–	6,0	10,9	7,2	7,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Janów Lubelski — φ = 50°43' — λ = 22°25'

I	–	–	–	–	-1,6	-8,4	6,7	4	-21,1	27	-5,9	-2,2	-5,1	-4,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2,8	-1,4	8,5	28	-6,8	6	-0,2	2,7	0,2	0,7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8,4	1,6	18,9	18	-3,2	23	3,6	7,4	4,4	5,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16,4	4,7	24,9	7,15	-2,2	10	9,0	15,4	9,9	11,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16,1	7,0	24,9	29	1,8	16,17	10,5	15,4	10,9	12,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23,6	11,4	31,8	26	6,2	16,17	16,4	21,8	16,7	17,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21,7	10,7	30,1	3	6,4	8	14,8	20,5	16,0	16,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21,8	11,7	32,8	11	7,4	14	14,9	21,0	16,3	17,1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20,4	9,2	27,9	2,3,18	2,1	23	11,4	19,8	14,2	14,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	15,8	6,0	23,1	19	1,3	23	8,1	15,6	10,3	11,1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	6,6	1,5	13,9	3	-6,8	23	3,3	6,0	4,0	4,3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1,0	-7,2	15,5	5	-20,3	25	-4,3	-2,4	-4,2	-3,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	12,6	3,9	32,8	11.VIII	-21,1	27.1	6,8	11,8	7,8	8,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sokołowsko — φ = 50°41' — λ = 16°14'

I	–	–	–	–	-0,8	-7,9	5,3	31	-24,8	26	-5,9	-4,7	-4,6	-4,2	–	–	–	–	–	–	–	–	–	–	–	–	7,6	7,3	6,2	7,0
II	–	–	–	–	3,3	-1,6	13,1	18	-13,5	6	0,0	2,1	0,5	0,8	–	–	–	–	–	–	–	–	–	–	–	–	9,4	8,8	8,5	8,9
III	–	–	–	–	8,0	-0,2	15,6	10	-6,1	20	4,1	6,5	3,3	3,6	–	–	–	–	–	–	–	–	–	–	–	–	7,8	7,3	6,7	7,3
IV	–	–	–	–	14,6	3,2	22,4	7	-3,2	1	7,3	13,3	7,9	9,1	–	–	–	–	–	–	–	–	–	–	–	–	5,2	6,0	4,8	5,3
V	–	–	–	–	12,8	4,1	21,0	26	-0,8	13	8,0	11,3	7,2	8,4	–	–	–	–	–	–	–	–	–	–	–	–	8,4	8,6	7,3	8,1
VI	–	–	–	–	20,4	8,7	26,2	25	2,5	16	13,9	18,9	12,9	14,6	–	–	–	–	–	–	–	–	–	–	–	–	5,8	6,1	5,5	5,8
VII	–	–	–	–	18,2	8,6	28,8	3	2,1	8	12,5	16,8	12,0	13,3	–	–	–	–	–	–	–	–	–	–	–	–	7,4	7,7	6,6	7,2
VIII	–	–	–	–	19,1	8,8	28,6	10	3,4	14	12,3	17,7	12,3	13,6	–	–	–	–	–	–	–	–	–	–	–	–	7,2	7,4	6,7	7,1
IX	–	–	–	–	20,0	7,6	27,8	18	-1,4	23	10,0	19,0	11,2	12,8	–	–	–	–	–	–	–	–	–	–	–	–	4,9	4,9	4,0	4,6
X	–	–	–	–	12,9	5,4	18,7	5,6	0,1	31	7,2	12,0	8,1	8,8	–	–	–	–	–	–	–	–	–	–	–	–	7,2	6,4	4,5	6,0
XI	–	–	–	–	4,8	-0,2	10,4	12	-7,2	21	1,1	3,4	1,9	2,1	–	–	–	–	–	–	–	–	–	–	–	–	8,5	8,6	8,0	8,4
XII	–	–	–	–	-0,5	-8,4	13,7	5	-24,7	25	-5,2	-2,3	-4,9	-4,3	–	–	–	–	–	–	–	–	–	–	–	–	7,5	7,5	6,3	7,1
Rok	–	–	–	–	11,1	2,3	28,8	3.VII	-24,8	26.1	5,2	9,8	5,6	6,6	–	–	–	–	–	–	–	–	–	–	–	–	7,2	7,2	6,3	6,9

Zamość

$H_s = 219$ m $H_b = 218,8$ m $h_w = 14$ m

MIESIĄC	ROZKŁAD WIATRU °D, v m/s N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v >10	v >15	◐	●	Opad R R>0.1	R>1.0	R>10.0	≡	⊞	R Γ0
I	5.5	2.4	3.5	4.7	3.5	2.4	13.5	1.4	11	3.4	19	4.0	10.5	4.0	17.5	2.3	9	2.6	17.7	4.9	14	13	14	31	·	2	1	5	9	15	5	·	5	29	·
II	1	2.0	1	2.0	2.5	1.8	16.5	2.2	10	3.0	17	2.3	24.5	2.1	4.5	1.7	7	2.1	13.5	3.9	10	·	1	17	·	·	·	2	17	14	4	·	9	11	·
III	·	·	·	·	·	·	·	·	2.5	5.2	26.5	4.8	53	4.1	11	4.1	·	4.3	33.4	12.4	28	·	·	9	·	2	·	2	12	17	8	1	1	1	·
IV	5	2.1	10.5	2.8	19.5	4.9	7	6.6	5	4.0	17.5	3.3	13	2.7	11.5	2.1	1	3.5	43.7	16.7	8	·	·	3	1	2	·	6	3	8	6	1	1	·	2
V	2.5	1.8	3.5	1.9	15.5	2.2	3.5	3.3	6	2.9	12	2.8	19	2.9	25	2.2	6	2.3	51.5	20.1	14	·	·	·	1	·	·	1	9	16	11	1	2	·	5
VI	2	1.0	6	2.1	12	2.1	9.5	1.6	6.5	1.9	14	2.4	21.5	1.7	12.5	2.1	6	1.8	46.6	11.2	13	·	·	·	14	·	·	4	5	15	10	1	2	·	9
VII	1.5	1.7	0.5	2.0	1	3.0	2.5	2.8	9.5	3.0	16.5	2.8	41.5	2.4	10	1.9	10	2.2	90.5	24.0	29	·	·	·	11	·	·	4	5	17	10	4	·	·	6
VIII	0.5	1.0	0.5	1.0	2.5	1.8	5	2.0	6.5	2.9	23	3.7	30.5	3.1	17.5	2.1	7	2.7	48.5	14.4	12	·	·	·	9	2	·	4	6	10	6	2	1	·	5
IX	1	1.0	4.5	1.7	11	2.0	4.5	1.8	2.5	7.0	22	2.2	25	2.5	1.5	2.3	18	1.9	18.1	10.8	6	·	·	2	6	1	1	14	6	9	3	1	4	·	1
X	·	·	2	2.5	28.5	2.6	25.5	3.4	10	3.0	4	3.0	7	2.7	6	2.0	10	2.6	17.5	9.8	30	·	·	1	·	·	·	12	8	4	3	·	7	·	·
XI	5.5	2.5	0.5	2.0	15.5	3.6	11	3.0	6	1.8	15.5	2.7	20	3.0	5	2.7	8	2.6	32.6	8.9	13	·	·	11	·	·	·	2	20	15	8	·	5	·	·
XII	10.5	2.8	5	1.3	5	2.4	8	1.6	6	3.5	15	5.8	18	2.9	15.5	3.4	10	2.9	33.4	7.9	7	12	18	25	·	6	2	1	16	16	8	·	10	25	·
Rok	35	1.5	37.5	1.8	116.5	2.4	109.5	2.5	81.5	3.5	202	3.3	283.5	2.8	137.5	2.2	92	2.6	447.0	24.0	29.VII	25	33	99	42	15	4	57	116	156	82	11	47	66	28

Zdanów

$H_s = 236$ m $h_w = 15$ m

I	11	2.6	4	2.4	·	·	6.5	2.7	17	4.2	16	3.5	6.5	4.4	11	3.7	21	2.7	15.0	6.9	14	12	16	29	·	3	·	4	12	8	4	·	2	26	·
II	3	2.5	·	·	3.5	1.9	7	2.8	13.5	3.6	8	2.7	17	2.3	12	3.1	20	2.1	12.1	4.2	1	·	1	23	·	·	·	1	16	9	5	·	6	3	·
III	2	2.0	1	1.0	0.5	1.0	·	·	0.5	6.0	20	5.4	44	5.6	24	6.0	1	5.5	13.3	2.9	21	·	·	7	·	10	1	2	15	13	6	·	1	·	·
IV	9	3.4	8.5	3.1	18	5.3	8	5.9	6	2.2	9.5	3.7	7	6.3	10	4.6	15	3.7	39.8	12.5	8	·	·	2	·	3	·	–	–	8	6	2	·	·	2
V	14	2.8	5	1.8	6.5	2.0	6.5	2.4	5	3.6	5	3.6	12	4.2	17	4.2	22	2.5	33.0	8.0	6	·	·	·	·	·	·	–	–	15	9	·	3	·	5
VI	7.5	2.6	6	2.0	9	3.8	9	2.6	5.5	3.2	5	3.4	12	3.2	18	3.6	18	2.5	84.7	18.9	4	·	·	·	10	·	·	7	4	13	12	3	·	·	6
VII	2.5	3.2	1.5	3.3	2.5	2.8	0.5	2.0	6	3.7	15	4.1	28.5	3.2	17.5	3.1	19	2.7	83.2	23.1	30	·	·	·	8	·	·	3	6	15	10	3	·	·	5
VIII	9.5	2.9	1	2.0	1.5	4.0	1.5	3.0	3.5	2.6	15.5	4.2	23.5	4.1	14	3.7	23	2.8	47.6	17.4	12	·	·	·	7	3	·	–	–	10	7	1	·	·	2
IX	6	2.8	5.5	2.5	7	3.3	2.5	3.2	3	4.0	8	3.8	22	4.1	11	3.6	25	2.6	15.2	7.1	14	·	·	·	6	·	·	–	–	7	4	·	1	·	1
X	4.5	3.8	4	4.4	18.5	4.8	19.5	6.6	9	4.3	4	3.0	3.5	3.6	9	3.6	21	3.7	6.5	3.5	30	·	·	-	·	6	2	–	–	3	2	·	2	·	·
XI	7	4.3	2.5	4.2	8.5	4.2	8	2.9	4.5	3.1	17.5	2.8	20.5	3.9	5.5	4.0	16	3.0	50.4	18.6	13	·	1	13	·	·	·	·	19	12	9	2	8	·	·
XII	16.5	5.6	2	3.5	1	1.0	6.5	3.1	10	4.2	12	5.3	7.5	5.6	18.5	5.9	19	4.1	36.6	16.0	6	–	18	27	·	2	·	3	13	12	8	1	4	25	·
Rok	92.5	3.2	41	2.5	76.5	2.8	75.5	3.1	82.5	3.7	135.5	3.8	204	4.2	167.5	4.1	220	3.2	437.4	23.1	30.VII	–	36	–	31	27	3	–	–	125	82	12	27	54	21

Janów Lubelski

$H_s = 230$ m $h_w = 20,1$ m

I	15	1.5	·	·	18	1.8	10	3.4	16	1.8	3	1.7	14	2.7	3	1.0	14	1.8	19.1	5.2	31	13	17	29	·	·	·	–	–	9	5	·	–	26	–
II	9	1.2	3	1.7	9	1.6	9	2.3	20	1.8	·	·	17	1.3	1	2.0	16	1.3	13.4	3.9	9	·	2	21	·	·	·	–	–	11	4	·	–	3	–
III	·	·	1	4.0	·	·	5	3.2	33	3.0	16	3.9	29	4.2	4	2.8	5	3.6	47.4	8.5	12	·	·	9	·	5	·	–	–	19	12	·	–	·	–
IV	14	2.0	14	2.2	13	4.7	7	1.1	14	1.9	5	2.8	6	2.5	5	2.4	12	2.2	35.9	14.0	8	·	·	1	·	·	·	–	–	9	6	1	–	·	–
V	2	1.0	8	1.9	12	1.6	3	2.0	13	1.7	12	2.1	25	2.1	4	1.8	14	1.6	48.3	9.0	14	·	·	·	·	·	·	–	–	14	11	·	–	·	–
VI	·	·	1	2.0	22	1.9	2	1.0	11	1.9	4	2.5	26	1.5	3	1.0	21	1.3	44.9	13.5	12	·	·	·	9	·	·	–	–	13	8	1	–	·	–
VII	5	1.8	·	·	4	2.0	7	1.6	22	1.9	11	1.9	24	1.6	4	1.2	16	1.5	91.1	27.0	29	·	·	·	8	·	·	–	–	13	10	4	–	·	–
VIII	2	1.0	4	1.2	6	1.8	9	1.9	22	2.0	12	2.0	23	2.4	5	1.6	10	1.8	69.3	29.5	12	·	·	·	7	·	·	–	–	10	8	2	–	·	–
IX	1	1.0	14	1.6	9	1.9	8	1.4	19	2.2	8	2.2	9	2.0	2	1.0	20	1.5	17.9	10.0	14	·	·	·	6	·	·	–	–	8	3	1	–	·	–
X	10	1.7	15	3.0	35	2.9	5	2.6	10	1.8	1	2.0	12	2.0	·	·	5	2.4	13.1	6.6	30	·	·	·	·	·	·	–	–	5	3	·	–	·	–
XI	2	2.5	9	2.1	15	2.1	7	1.1	19	1.6	12	2.5	16	1.9	3	1.0	7	1.8	39.6	13.5	13	·	2	10	·	·	·	–	–	14	10	1	–	·	–
XII	8	2.1	5	1.4	14	1.3	5	1.8	15	4.0	3	2.3	20	2.5	7	3.1	16	2.0	38.6	11.0	7	12	19	24	·	1	·	–	–	11	8	2	–	25	–
Rok	68	1.3	74	1.8	157	2.0	77	2.0	214	2.1	87	2.2	221	2.2	41	1.6	156	1.9	478.6	29.5	12.VIII	25	40	94	30	6	·	–	–	126	88	12	–	54	–

Sokołowsko

$H_s = 570$ m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	16.1	3.5	14	12	16	29	·	–	–	5	18	12	6	·	1	25	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43.1	14.1	9	2	4	20	·	–	–	1	24	14	12	1	3	16	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	49.2	5.8	21	·	1	19	·	–	–	3	16	17	13	·	2	9	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	47.8	12.7	15	·	·	6	·	–	–	6	7	12	9	1	2	·	6
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	138.7	22.1	29	·	·	1	·	–	–	·	18	23	18	5	2	·	4
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	56.3	25.2	10	·	·	·	1	–	–	3	8	13	9	1	·	·	4
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	115.2	29.1	28	·	·	·	4	–	–	2	15	19	14	3	·	·	1
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	112.1	43.1	12	·	·	·	2	–	–	4	15	17	12	2	·	·	2
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	17.0	4.3	14	·	·	2	4	–	–	9	7	10	6	·	1	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43.0	12.9	20	·	·	·	·	–	–	5	11	9	7	3	3	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	54.3	11.5	5	·	1	14	·	–	–	2	23	17	12	1	8	2	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	62.6	18.2	11	12	16	26	·	–	–	4	16	20	10	1	2	24	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	755.4	43.1	12.VIII	26	38	117	11	–	–	44	178	183	128	18	24	76	18

Grodków — φ = 50°41' — λ = 17°23' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{n.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.4	-6.5	10.6	4	-21.5	27	-4.1	0.2	-3.1	-2.5	4.0	4.9	4.2	4.4	80	76	81	79	1.0	1.6	1.0	1.2	5.3	5.8	5.4	5.5
II	–	–	–	–	6.9	-0.2	13.5	18	-4.4	6	1.1	5.5	2.4	2.8	6.0	6.9	6.4	6.4	90	77	87	85	0.7	2.2	1.0	1.3	7.9	6.1	5.0	6.3
III	–	–	–	–	11.0	2.8	19.5	10	-2.4	20	4.5	9.4	6.2	6.6	6.7	7.4	7.2	7.1	80	63	76	73	1.8	4.8	2.6	3.1	7.8	7.2	6.5	7.2
IV	–	–	–	–	17.6	5.5	26.4	7	-1.1	10	8.8	14.6	10.1	11.4	9.2	9.4	9.4	9.3	80	50	75	68	2.3	10.2	3.2	5.2	4.8	5.3	4.8	5.0
V	–	–	–	–	16.7	7.2	24.1	26	2.4	13	10.5	15.0	10.6	11.7	10.8	10.3	10.9	10.7	85	61	85	77	2.1	7.1	2.1	3.8	7.3	7.3	7.4	7.3
VI	–	–	–	–	23.2	12.3	30.2	27	6.4	21	16.3	21.2	16.3	17.5	14.8	14.6	15.6	15.0	79	59	84	74	4.1	11.2	3.2	6.2	4.9	6.2	5.3	5.5
VII	–	–	–	–	21.4	11.6	32.5	3	5.6	11	15.2	19.8	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	7.0	7.2
VIII	–	–	–	–	22.0	11.9	31.7	6	6.9	4	15.0	20.6	15.4	16.6	14.9	15.7	15.1	15.2	86	65	85	79	2.3	9.2	2.7	4.7	6.6	7.1	5.3	6.3
IX	–	–	–	–	22.5	9.1	30.3	2	4.2	23	12.1	21.5	14.1	15.4	12.5	14.3	13.5	13.4	87	56	83	75	1.9	12.2	3.0	5.7	5.1	4.2	3.0	4.1
X	–	–	–	–	16.7	5.6	22.7	6	1.6	22	7.9	15.7	9.9	10.8	9.7	11.1	10.3	10.4	90	64	85	80	1.1	7.2	2.0	3.4	6.4	6.0	5.1	5.8
XI	–	–	–	–	7.5	1.4	13.7	2	-5.5	21	2.9	6.1	3.6	4.0	6.9	7.6	7.3	7.3	90	80	91	87	0.9	2.0	0.7	1.2	7.4	7.9	6.6	7.3
XII	–	–	–	–	0.9	-6.9	17.7	5	-23.4	26	-3.9	-4.0	-3.7	-3.1	4.6	5.0	4.5	4.7	82	77	81	80	1.0	1.6	0.9	1.2	8.0	6.5	5.7	6.7
Rok	–	–	–	–	14.0	4.5	32.5	3.VII	-23.4	26.XII	7.2	12.6	8.1	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.4	5.6	6.2

Sandomierz — φ = 50°41' — λ = 21°45'

I	996.2	1016.4	977.5	1021.8	-1.2	-8.0	8.0	4	-20.5	26	-6.3	-2.8	-4.7	-4.6	3.4	4.3	4.1	4.1	90	81	88	86	0.4	1.0	0.5	0.6	6.4	6.3	5.6	6.1
II	998.4	1012.6	969.9	1023.5	3.8	-1.3	8.7	28	-5.5	7	-0.5	2.6	0.8	0.9	5.4	5.9	5.8	5.7	92	80	90	87	0.5	1.5	0.7	0.9	7.9	7.7	6.9	7.5
III	993.1	1011.3	972.2	1017.7	9.4	1.7	19.4	18	-3.4	23	3.1	7.7	4.8	5.1	6.7	6.8	7.0	6.8	87	65	80	77	1.1	4.1	1.8	2.3	7.9	7.9	5.5	7.1
IV	989.5	999.1	980.3	1013.5	16.8	5.3	25.1	15	-1.1	10	6.9	15.0	10.5	10.7	7.9	8.1	8.3	8.1	77	47	64	63	2.3	9.6	4.7	5.5	5.4	5.4	3.7	4.8
V	988.3	996.1	974.6	1012.2	17.0	7.4	25.5	29	2.0	13	9.6	15.1	11.5	11.9	10.2	10.2	10.8	10.4	85	61	79	75	1.9	7.6	3.1	4.2	7.0	7.5	6.5	7.0
VI	991.8	1004.4	982.3	1015.3	24.3	12.5	31.3	27	7.5	17	15.7	22.5	17.0	18.0	15.2	14.4	14.9	14.8	85	54	77	72	2.8	13.6	4.6	7.0	4.9	5.6	5.4	5.3
VII	990.7	1001.7	977.3	1014.3	22.3	11.6	30.2	3	8.1	6	14.5	20.4	15.9	16.7	13.9	13.3	14.2	13.8	84	56	78	73	2.7	11.4	4.2	6.1	5.2	7.1	6.1	6.1
VIII	993.0	1005.5	983.1	1016.7	22.6	12.1	33.3	11	8.2	14	14.2	21.0	16.1	16.8	14.6	14.1	15.2	14.6	89	57	82	76	1.9	11.7	3.5	5.7	6.0	6.5	5.1	5.9
IX	995.9	1006.5	984.4	1019.7	21.3	9.4	28.7	18	2.8	23	11.0	19.7	14.3	14.8	11.9	11.9	12.8	12.2	89	52	76	72	1.4	11.8	4.0	5.7	4.6	4.9	3.3	4.3
X	996.3	1007.8	973.8	1020.4	16.4	6.0	23.5	19	1.7	24	6.9	15.4	10.4	10.8	8.7	9.7	9.5	9.3	86	57	76	73	1.5	8.1	3.2	4.3	5.2	5.5	4.0	4.9
XI	990.6	1011.8	978.5	1015.2	6.8	1.5	14.5	3	-5.7	23	2.9	5.6	3.8	4.0	7.2	7.6	7.4	7.4	92	82	90	88	0.6	1.8	0.8	1.1	8.1	8.3	7.2	7.9
XII	991.6	1017.8	972.3	1016.9	-0.7	-7.7	14.9	5	-26.4	26	-5.0	-2.8	-4.3	-4.1	4.3	4.5	4.4	4.4	87	80	86	84	0.7	1.2	0.7	0.9	7.0	6.7	6.8	6.8
Rok	992.9	1017.8	972.2	1017.2	13.2	4.2	33.3	11.VIII	-26.4	26.XII	6.1	11.6	8.0	8.4	9.1	9.2	9.5	9.3	87	64	80	77	1.5	7.0	2.6	3.7	6.3	6.6	5.5	6.1

Opole — φ = 50°40' — λ = 17°58'

I	998.0	1020.5	976.2	1022.8	0.7	-6.7	11.5	4	-21.3	27	-4.5	-0.4	-3.5	-3.0	4.0	4.6	4.2	4.3	82	74	81	79	0.8	1.6	0.9	1.1	6.1	5.9	6.4	6.1
II	1000.6	1015.9	971.4	1022.9	6.4	-0.9	12.4	18	-6.7	6	0.4	5.0	1.9	2.3	5.8	6.6	6.3	6.2	91	76	90	86	0.5	2.2	0.7	1.1	7.5	6.9	5.5	6.6
III	998.2	1015.3	973.1	1020.2	10.7	2.6	20.6	10	-3.5	20	3.9	8.9	5.9	6.2	6.8	7.2	7.3	7.1	83	64	78	75	1.5	4.6	2.2	2.8	8.2	7.6	6.5	7.4
IV	994.3	1000.8	983.2	1012.7	18.1	5.0	27.0	7	-3.4	10	8.1	16.8	10.4	11.4	8.9	9.4	9.4	9.2	80	50	73	68	2.2	10.5	3.6	5.4	4.8	5.4	4.9	5.0
V	994.9	999.3	978.1	1013.2	17.8	6.9	24.2	26	2.4	13	10.0	15.7	10.9	11.9	10.6	10.5	10.6	10.6	86	60	81	76	1.8	7.9	2.7	4.1	7.9	7.9	8.1	8.0
VI	994.7	1008.7	983.2	1015.7	23.9	11.4	30.8	25	5.5	21	16.1	22.0	16.8	17.9	14.9	15.2	15.3	15.1	81	59	80	73	3.6	11.8	4.1	6.5	5.1	6.2	5.6	5.6
VII	993.8	1005.3	978.4	1014.9	22.2	11.5	33.4	3	5.2	8	14.9	20.3	15.7	16.6	13.7	13.8	14.1	13.9	80	59	79	73	3.5	11.1	4.1	6.2	7.2	7.4	6.8	7.1
VIII	996.3	1008.2	986.3	1017.4	22.4	11.7	31.3	6	5.8	14	14.6	20.7	15.8	16.7	14.6	15.6	15.3	15.2	87	64	84	78	2.3	9.4	3.0	4.9	6.8	7.1	4.8	6.2
IX	998.1	1008.8	986.7	1019.3	22.6	9.5	30.5	2	0.2	23	11.7	21.3	14.2	15.4	12.2	13.5	13.0	12.9	87	54	79	73	2.0	12.7	3.5	6.1	5.6	4.3	3.2	4.4
X	997.1	1009.6	970.2	1018.6	16.5	6.8	22.9	6	2.2	10	7.9	15.6	10.6	11.2	9.5	10.7	10.4	10.2	89	62	82	78	1.4	7.5	2.5	3.8	6.5	6.8	5.0	6.1
XI	993.4	1015.4	980.6	1015.5	7.3	4.5	14.6	3	-6.7	22	3.0	6.1	3.5	4.0	7.1	7.5	7.2	7.3	90	79	90	86	0.8	2.1	0.8	1.2	7.9	8.2	6.9	7.7
XII	995.1	1022.5	976.3	1017.8	0.5	-7.2	15.2	2	-26.5	26	-4.1	-1.4	-3.6	-3.2	4.6	5.0	4.6	4.7	85	78	83	82	0.8	1.4	0.9	1.0	7.4	6.7	5.5	6.5
Rok	995.7	1022.5	970.2	1017.4	14.1	4.3	33.4	3.VII	-26.5	26.XII	6.8	12.6	8.2	9.0	9.4	10.0	9.8	9.7	85	65	82	77	1.8	6.9	2.4	3.7	6.8	6.7	5.8	6.4

Lubliniec — φ = 50°40' — λ = 18°41'

I	–	–	–	–	0.3	-6.9	11.4	4	-22.1	27	-5.2	-0.4	-4.0	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	5.1	-0.6	11.0	18	-6.7	6	0.6	4.3	1.3	1.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	9.4	1.9	18.9	10	-2.6	20	3.6	8.3	4.9	5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	17.2	5.5	25.8	7	-1.9	10	9.3	16.4	10.0	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.8	6.5	24.1	26	1.7	15	10.7	15.6	10.1	11.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.5	11.4	29.8	25	5.6	21	16.8	21.8	15.5	17.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.2	10.9	31.4	3	5.5	8	15.2	20.0	14.6	16.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.9	11.4	30.3	6	6.5	14	14.8	20.6	15.0	16.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	21.5	9.8	29.4	2	2.6	24	12.2	20.6	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	16.1	7.0	21.6	5	2.3	10,17	8.5	15.5	10.1	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.2	–	13.1	3	–	–	2.6	6.5	3.7	4.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	0.0	–	14.5	5	–	–	-4.2	-4.1	-3.7	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	13.3	–	31.4	3.VII	–	–	7.1	12.3	7.8	8.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Gradków

$H_s = 176$ m $h_w = 13{,}5$ m **1961**

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	3	2.0	9	2.3	10.5	2.4	7.5	4.9	25	3.0	21	4.0	7.5	3.5	6.5	2.1	3	2.9	10.0	4.6	14	11	12	24	·	1	·	9	9	10	3	·	6	20	·
II	4	2.5	0.5	2.0	2.5	4.6	8	4.9	16.5	2.8	15	2.8	24	3.4	10.5	3.5	3	2.8	34.0	10.6	9	·	·	14	·	·	·	4	10	12	9	1	10	5	·
III	2	4.0	·	·	·	·	0.5	3.0	2	4.8	19	4.3	42.5	3.8	27	4.1	·	3.9	34.7	7.4	28	·	·	5	·	2	·	3	15	14	9	·	·	3	·
IV	11	1.5	5.5	1.5	16	2.6	2.5	2.6	14.5	2.6	14	2.1	7.5	2.9	15	2.9	4	2.3	39.9	12.5	27	·	·	1	1	·	·	9	7	7	6	2	1	·	4
V	10	2.1	2	1.0	2	1.5	1	1.0	3	2.0	15	2.7	23	2.8	31	2.5	6	2.3	50.3	13.6	1	·	·	·	·	1	·	3	14	14	12	1	·	·	2
VI	3.5	2.6	2.5	2.0	2	1.8	6	1.8	8.5	1.9	12.5	1.8	22.5	2.5	21.5	3.3	11	2.2	74.9	26.6	10	·	·	·	8	·	·	6	9	13	10	3	1	·	10
VII	0.5	1.0	1	1.0	·	·	2.5	2.2	8	1.6	21.5	2.6	32	2.6	11.5	2.7	16	2.0	93.5	22.4	28	·	·	·	6	·	·	3	15	15	12	2	·	·	3
VIII	4	1.8	·	·	2.5	1.6	1.5	2.0	5.5	1.8	18	2.9	27	2.5	17.5	2.7	17	2.1	83.5	29.6	17	·	·	·	6	·	·	2	8	17	10	2	3	·	6
IX	3.5	1.6	4.5	1.6	12	1.8	5.5	1.4	9.5	1.4	18	2.4	10	2.4	10	2.9	17	1.7	14.4	5.8	14	·	·	·	9	·	·	13	6	5	4	·	3	·	·
X	1	2.0	4.5	2.3	6	4.2	13.5	2.3	10	3.0	12.5	4.0	8	1.9	13.5	3.0	24	2.2	55.1	21.8	20	·	·	·	·	1	·	2	8	7	5	2	6	·	·
XI	8.5	1.7	15	1.0	6.5	3.5	5	1.7	12	1.7	15	3.7	9	3.5	10.5	3.4	22	2.1	50.0	8.1	6	·	·	7	·	2	·	3	14	16	10	·	6	·	·
XII	8.5	1.8	5.5	2.2	·	·	9	2.1	13.5	2.0	13	4.6	13.5	2.8	22	3.4	8	2.6	42.1	10.0	12	10	13	22	·	1	·	1	11	16	11	1	5	19	·
Rok	59.5	2.0	36.5	1.4	60	1.8	62.5	2.0	128	2.1	194.5	3.2	226.5	2.9	196.5	3.0	131	2.4	582.4	29.6	17.VIII	21	25	73	30	8	·	58	126	146	101	14	41	47	25

Sandomierz

$H_s = 202$ m $H_b = 200{,}3$ m $h_w = 20{,}1$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	12	3.1	2.5	5.6	2.5	2.0	9.5	2.5	15.5	3.5	31	3.6	8	4.3	11	3.5	1	3.5	17.3	6.0	14	12	15	29	·	·	·	5	11	9	5	·	5	26	·
II	1.5	3.0	0.5	2.0	3.5	2.7	6	2.8	11.5	3.3	29.5	3.9	49.5	3.2	9	3.2	3	3.3	19.0	4.6	9	·	·	21	·	1	·	1	14	10	6	·	6	8	·
III	·	·	·	·	·	·	·	·	0.5	9.0	27.5	5.1	42	6.1	22	5.8	1	5.7	20.2	3.6	21	·	·	7	·	11	2	1	11	17	5	·	1	2	1
IV	7	3.2	10	2.8	17	4.4	10	4.6	2.5	2.8	19.5	3.6	10.5	4.9	8.5	3.6	5	3.7	40.4	16.4	16	·	·	1	1	2	1	6	4	10	6	1	·	·	2
V	9	2.9	1	2.5	1.5	2.3	7.5	2.4	8	2.3	18.5	3.2	17	4.1	17.5	3.1	13	2.7	53.1	9.3	30	·	·	·	1	1	·	1	11	14	12	·	2	·	4
VI	7.5	1.4	2	3.5	3.5	4.7	5.5	2.7	11	2.2	20.5	2.6	21	3.1	17	2.4	2	2.6	78.5	26.6	12	·	·	·	15	1	·	4	7	12	11	3	·	·	10
VII	4	2.8	1	2.0	·	·	·	·	3	3.7	32.5	3.5	35.5	3.0	13	2.4	4	3.0	61.6	18.6	30	·	·	·	9	4	2	3	7	13	9	2	1	·	3
VIII	9.5	2.4	4.5	4.8	1	2.0	0.5	4.0	5.5	1.9	25.5	3.5	28	3.6	42.5	3.3	6	2.9	54.5	49.5	12	·	·	·	7	2	·	3	10	12	7	3	·	·	5
IX	5	2.1	9.5	2.3	10	2.1	4.5	2.1	6	2.0	21.5	3.0	20	3.4	40.5	3.0	3	2.6	9.3	6.4	14	·	·	·	6	1	·	11	8	4	3	·	3	·	2
X	4	3.0	4.5	3.8	22.5	3.3	23.5	3.6	13.5	2.9	8.5	2.9	5.5	3.2	10	2.6	1	3.2	10.7	4.9	30	·	·	·	·	·	·	9	7	6	2	·	1	·	·
XI	5	4.6	3	3.3	9.5	3.1	14.5	2.4	9	2.2	29.5	2.9	13.5	4.2	4	3.8	2	3.1	47.8	17.2	13	·	·	10	·	·	·	2	18	17	8	2	5	1	·
XII	13.5	4.1	5.5	3.4	5	1.7	11	1.6	6	2.2	21.5	4.4	10	4.3	16.5	3.8	4	3.4	42.2	11.7	7	11	16	25	·	4	·	3	12	19	9	2	3	25	·
Rok	78	2.7	44	2.8	76	2.4	92.5	2.4	92	3.2	285.5	3.5	230.5	4.0	151.5	3.4	45	3.3	454.6	26.6	12.VI	23	31	93	39	27	5	49	120	143	83	13	27	62	27

Opole

$H_s = 176$ m $H_b = 177{,}9$ m $h_w =$ 13 m I–V, 13.5 m VI–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	1.5	1.0	3.5	3.4	13.5	2.0	15	1.9	44	4.1	2	2.5	5.5	2.5	6	2.7	2	3.1	9.8	3.5	14	11	13	26	·	3	3	6	11	8	3	·	1	18	·
II	0.5	4.0	1	10.0	1.5	2.0	14	2.1	34.5	2.3	9.5	2.0	14	2.9	7	4.1	2	2.6	48.0	18.1	9	·	·	18	·	2	1	4	14	15	8	1	7	5	·
III	2	5.8	·	·	·	·	·	·	5	2.1	24.5	1.9	40.5	4.1	21	4.9	·	3.9	38.4	10.4	14	·	·	6	·	5	1	1	18	16	9	1	2	2	·
IV	2	1.2	6.5	2.5	7	2.9	16	2.2	15	2.4	20	2.9	11.5	2.6	9	2.8	3	2.3	25.4	6.3	16	·	·	1	3	2	2	4	5	7	6	·	1	·	3
V	4	2.2	3.5	3.7	1.5	1.3	2.5	1.8	11	2.0	17.5	2.4	30.5	2.6	21.5	2.5	1	2.4	56.6	27.8	29	·	·	·	·	2	1	·	17	16	8	1	1	·	4
VI	3.5	2.4	0.5	1.0	1.5	1.7	4.5	1.3	13	1.5	15	2.1	28.5	2.5	21.5	2.5	2	2.1	50.1	13.8	27	·	·	·	11	1	·	5	8	14	9	1	5	·	9
VII	0.5	3.0	0.5	3.0	0.5	1.0	0.5	1.0	4	3.5	25.5	2.2	31	1.8	21.5	1.9	9	1.8	97.2	33.9	28	·	·	·	8	·	·	2	12	14	13	4	·	·	4
VIII	3	1.0	1.5	1.3	0.5	2.0	5	2.0	5.5	2.5	27	2.3	25.5	2.2	22	2.0	3	2.0	39.7	9.4	12	·	·	·	7	1	·	2	9	14	10	·	2	·	6
IX	1.5	1.0	4.5	2.3	11.5	1.5	10	2.0	15	2.2	13.5	2.3	18	2.4	9	1.3	7	1.9	15.3	6.1	14	·	·	·	8	1	1	9	8	7	3	·	4	·	·
X	-	-	1.5	4.3	10	4.2	22.5	2.6	26.5	4.1	3.5	3.9	13.5	1.4	11.5	2.4	4	3.0	24.8	9.9	19	·	·	·	·	2	1	5	11	8	4	·	8	·	·
XI	4	2.1	3.5	2.3	3.5	3.4	7	1.5	26.5	2.0	17	2.5	7.5	2.5	19	1.8	2	2.1	48.4	11.2	13	·	·	6	·	·	·	1	15	16	13	1	5	·	·
XII	11.5	2.8	1.5	5.3	·	·	4	4.0	22	3.9	8.5	4.1	15	3.8	25.5	3.1	5	3.3	49.4	12.5	11	11	13	24	·	6	·	2	14	13	9	1	1	19	·
Rok	34	2.2	28	3.3	51	1.8	101	1.9	222	2.7	183.5	2.6	241	2.6	194.5	2.7	40	2.5	503.1	33.9	28.VII	22	26	81	37	25	10	41	142	148	95	10	37	44	26

Lubliniec

$H_s = 256$ m $h_w = 12{,}5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	4.5	2.0	2.5	2.4	14.5	2.3	14	1.9	17.5	3.1	13	3.2	9.5	1.8	2.5	1.4	15	2.1	13.6	4.2	14	11	14	27	·	1	·	–	–	10	5	·	·	21	·
II	5.5	4.3	·	·	2.5	1.0	9	1.8	16.5	3.5	6	4.5	26.5	2.7	5	6.6	13	2.8	57.7	18.8	9	·	·	20	·	3	1	–	–	14	11	2	7	5	·
III	4.5	8.0	·	·	·	·	·	·	8	2.9	15.5	3.4	39.5	4.3	14.5	5.3	11	3.8	54.4	7.9	14	·	·	7	·	6	2	–	–	14	10	·	3	5	·
IV	7	2.4	3	2.5	17	3.1	11.5	3.5	7.5	2.1	4	3.2	14.5	2.7	5.5	4.6	20	2.3	24.9	6.4	8	·	·	1	1	·	·	–	–	7	7	·	·	·	2
V	19.5	2.0	5.5	1.2	7	2.1	2	1.0	4	3.5	6	2.0	32.5	3.0	9.5	2.2	7	2.2	76.8	22.6	27	·	·	·	·	·	·	–	–	17	15	2	·	·	3
VI	11	3.2	3	1.0	9	1.4	8.5	1.5	8.5	1.6	4	1.0	20.5	3.2	10.5	1.9	15	1.8	104.8	28.0	9	·	·	·	10	2	2	–	–	12	10	3	2	·	9
VII	7	2.7	1	1.0	2.5	1.0	2	1.0	14.5	1.2	6.5	1.9	34.5	2.5	5	2.4	20	1.6	147.4	36.2	31	·	·	·	7	1	·	–	–	14	11	5	1	·	2
VIII	4.5	2.1	2	1.0	3.5	1.0	3.5	1.0	8	2.0	16.5	2.3	27	2.5	11	2.9	17	1.8	70.3	30.7	12	·	·	·	8	·	·	–	–	10	8	1	3	·	2
IX	3	1.0	4.5	1.0	12.5	1.2	16.5	1.1	13.5	1.1	12.5	1.8	17.5	1.8	2	1.8	8	1.2	31.3	20.0	26	·	·	·	7	·	·	–	–	6	4	1	1	·	2
X	4	1.2	3	1.3	10.5	1.9	27	1.7	15.5	1.5	6.5	1.2	11.5	1.3	4	1.4	11	1.3	8.8	2.9	17	·	·	·	·	·	·	–	–	5	4	·	7	·	·
XI	9	2.1	7	1.9	11.5	3.0	9.5	1.3	23	1.3	10.5	2.7	13.5	1.9	3	4.3	3	1.9	79.4	27.4	13	–	·	–	·	1	·	–	–	13	12	2	4	2	·
XII	22.5	1.7	5.5	1.3	6.5	1.1	4	1.4	19	2.7	15	3.9	11	2.4	8.5	2.1	1	2.3	61.4	15.8	11	–	13	–	·	·	·	–	–	16	11	1	·	21	·
Rok	102	2.7	37	1.2	97	1.6	107.5	1.4	155.5	2.2	116	2.6	258	2.5	81	3.1	141	2.1	730.8	36.2	31.VII	–	27	–	33	14	5	–	–	138	108	17	28	54	20

Ostroszowice

$\varphi = 50°39'$ $\lambda = 16°38'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.4	-5.4	7.9	4	-18.9	27	-3.5	0.0	-2.6	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.8	6.6	6.2
II	–	–	–	–	6.4	0.1	16.5	18	-9.6	6	4.6	4.9	2.6	2.9	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.6	5.9	6.5
III	–	–	–	–	9.8	2.0	18.3	10	-5.5	20	3.2	8.5	5.6	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	6.4	6.6
IV	–	–	–	–	15.9	5.5	23.9	7	-1.1	10	9.1	14.8	9.6	10.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.6	5.3	5.3
V	–	–	–	–	14.7	6.3	21.4	26	1.4	13	9.5	12.9	9.1	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.0	7.3	7.6
VI	–	–	–	–	21.9	11.5	28.0	25	4.3	16	16.0	19.7	14.9	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.0	4.3	5.3
VII	–	–	–	–	20.4	11.2	30.6	3	6.5	8	14.8	18.6	14.3	15.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.3	6.3	6.8
VIII	–	–	–	–	20.9	11.8	30.0	6	6.5	14	14.4	19.6	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.6	5.1	6.0
IX	–	–	–	–	21.9	10.3	28.9	18	0.9	23	13.3	20.7	14.3	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.6	4.4	4.6
X	–	–	–	–	15.1	6.7	21.0	11	1.4	23	8.3	14.0	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	5.0	6.1
XI	–	–	–	–	6.7	1.8	11.6?	22?	-4.2	21	2.9	5.1	3.9	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.3	8.5	8.2
XII	–	–	–	–	1.4	-6.8	16.8	5	-21.4	25	-3.2	-0.9	-3.1	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.4	6.8	7.0
Rok	–	–	–	–	13.0	4.6	30.6	3.VII	-21.4	25.XII	7.2	11.5	7.8	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	6.0	6.3

Szczekociny

$\varphi = 50°38'$ $\lambda = 19°49'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.5	10.8	30.7	3	4.9	6	14.7	19.4	14.4	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	7.1	6.7
VIII	–	–	–	–	22.0	10.8	30.3	6	4.7	31	14.6	20.8	14.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.9	4.7	5.0
IX	–	–	–	–	21.2	–	30.1	17	–	–	10.8	20.1	12.5	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	3.9	3.2	4.0
X	–	–	–	–	16.3	–	21.9	20	–	–	6.7	15.6	9.1	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.1	4.3	4.2	4.9
XI	–	–	–	–	6.9	–	14.0	3	–	–	2.5	5.9	3.1	3.6	–	–	–	–	–	–	–	–	–	–	–	–	9.4	7.8	8.3	8.5
XII	–	–	–	–	-0.7	-9.1	17.0	5	-23.9	25,26	-5.3	-2.5	-5.8	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	6.7	7.3
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Skroniów

$\varphi = 50°38'$ $\lambda = 20°16'$

I	–	–	–	–	-1.8	-9.4	7.1	4	-23.4	27	-6.7	-2.9	-5.5	-5.2	4.0	4.4	4.2	4.2	94	81	92	89	0.2	0.9	0.4	0.5	7.1	5.7	6.1	6.3
II	–	–	–	–	3.8	-1.1	12.4	18	-5.7	5	-0.1	3.0	1.0	1.2	5.8	6.5	6.1	6.1	94	85	92	90	0.4	1.2	0.6	0.7	9.3	8.5	7.0	8.3
III	–	–	–	–	9.2	2.2	18.9	18	-3.8	20	3.4	7.9	4.8	5.2	7.0	7.1	7.3	7.1	88	68	85	80	1.0	4.0	1.4	2.1	7.9	7.8	6.7	7.5
IV	–	–	–	–	16.5	4.2	25.5	15	-2.8	10	7.3	15.3	9.1	10.2	8.2	8.2	8.5	8.3	79	48	73	67	2.3	10.0	3.4	5.2	5.3	5.3	3.7	4.8
V	–	–	–	–	17.1	6.1	24.6	27	1.6	2	9.5	15.5	10.1	11.3	10.2	9.7	10.3	10.1	85	56	82	74	1.8	8.6	2.3	4.2	7.4	7.7	7.2	7.4
VI	–	–	–	–	23.9	11.2	31.4	26	5.6	16,21	16.0	22.4	15.4	17.3	14.6	13.8	14.9	14.4	80	51	84	72	3.7	14.0	2.8	6.8	4.8	5.7	5.4	5.3
VII	–	–	–	–	21.1	10.9	30.4	3	7.0	6	14.5	19.5	14.5	15.8	13.9	14.1	14.2	14.1	84	63	86	78	2.9	9.3	2.5	4.9	6.8	7.3	6.5	6.9
VIII	–	–	–	–	21.9	11.4	30.9	11	7.5	14	14.4	20.8	14.9	16.2	14.8	14.5	14.8	14.7	88	59	86	78	1.9	10.8	2.5	5.1	5.5	6.7	4.8	5.7
IX	–	–	–	–	21.4	8.4	29.8	2	1.1	24	11.0	20.2	13.2	14.4	11.7	11.7	12.1	11.8	87	50	79	72	1.8	12.9	3.4	6.0	4.9	4.4	4.0	4.4
X	–	–	–	–	16.3	5.0	22.5	20	1.1	24	6.7	15.6	9.4	10.3	8.8	9.5	9.3	9.2	89	55	79	74	1.2	8.4	2.7	4.1	7.0	6.1	4.7	5.9
XI	–	–	–	–	6.8	1.0	14.6	3	-6.0	23	2.4	5.8	3.1	3.6	6.9	7.1	7.3	7.3	92	82	92	89	0.6	1.9	0.6	1.0	8.2	8.1	7.7	8.0
XII	–	–	–	–	-1.1	-8.4	17.1	5	-26.5	26	-5.2	-3.1	-5.3	-4.8	4.3	4.5	4.3	4.4	91	82	90	88	0.5	1.3	0.6	0.8	7.9	7.0	7.7	7.5
Rok	–	–	–	–	12.9	3.5	31.4	26.VI	-26.5	26.XII	6.1	11.7	7.1	8.0	9.2	9.3	9.4	9.3	88	66	85	79	1.5	6.9	1.9	3.4	6.8	6.7	6.0	6.5

Staszów

$\varphi = 50°34'$ $\lambda = 21°10'$

I	–	–	–	–	-0.7	-9.9	7.1	4	-25.1	27	-7.0	-2.2	-5.7	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	5.0	6.1
II	–	–	–	–	4.0	-1.6	9.5	18	-6.1	5	-0.3	3.0	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.2	7.0	8.0
III	–	–	–	–	9.4	1.8	19.8	18	-2.8	29	3.4	8.1	4.8	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.9	6.3	7.3
IV	–	–	–	–	16.9	3.8	25.5	15	-4.8	10	7.0	15.4	8.9	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.5	4.1	5.0
V	–	–	–	–	16.9	5.4	24.9	29	-1.0	13	9.9	15.2	10.1	11.3	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.7	6.7	7.1
VI	–	–	–	–	23.9	10.0	31.8	27	4.1	21	15.6	22.3	15.8	17.4	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.3	4.9	5.1
VII	–	–	–	–	22.0	9.2	29.6	3	4.1	8	14.5	22.0	14.4	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.9	6.1	5.9
VIII	–	–	–	–	22.6	10.6	32.9	11	5.1	31	14.3	21.1	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	4.6	5.4
IX	–	–	–	–	21.1	6.8	28.8	18	-0.5	23	9.7	19.8	12.5	13.6	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.9	3.4	4.2
X	–	–	–	–	16.5	4.0	22.5	19	-2.0	24	6.1	15.6	9.6	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.7	3.6	5.0
XI	–	–	–	–	7.0	0.4	15.0	3	-9.8	23	2.2	6.1	3.3	3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.6	7.1	7.9
XII	–	–	–	–	-4.0	-10.1	15.2	5	-31.6	26	-5.9	-3.0	-5.8	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	7.3	7.4
Rok	–	–	–	–	13.2	2.5	32.9	11.VIII	-31.6	26.XII	6.8	11.8	7.0	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	5.4	6.2

Ostroszowice $H_s = 375\ m$ $h_w = 12{,}5\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	⊕	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	.	.	1.5	3.3	1	9.5	9.5	6.1	14.5	3.4	20	11.3	19	6.5	12.5	3.5	15	5.6	9.5	5.0	31	9	9	21	.	11	8	7	9	9	2	.	3	12	
II		.		.	1	2.0	6	5.6	5	6.3	18	9.8	21	5.4	18	5.0	15	5.4	27.7	7.5	9	.	1	8	.	8	5	5	13	14	8	.	2	5	
III	2	4.8	.	.		.			1	8.0	8.5	4.2	36	6.6	36.5	4.7	9	5.7	25.3	3.7	30	.	.	8	.	9	4	3	11	14	10	.	.	4	
IV	2.5	3.0	2	1.8	4	2.1	13.5	2.6	5	5.7	11	5.1	9.5	5.6	12.5	3.0	30	2.5	33.2	8.1	8	.	.	2	.	4	.	7	9	10	8	.	.	.	5
V	5.5	2.8	.		.	.	3	2.7	1	3.0	8.5	3.9	17.5	3.6	34.5	3.0	23	2.5	84.9	20.4	29	.	.		.	.	.	.	14	19	13	1	1	.	1
VI	6.5	3.2	2	1.5	0.5	2.0	3.5	2.3	3	3.3	9.5	3.3	14	4.3	30	2.2	21	2.2	33.8	6.7	4	.	.	.	5	.		6	4	14	11	.	.	.	7
VII	4.5	1.6		.			0.5	2.0	4	4.1	11	4.8	33.5	4.1	23.5	2.9	16	3.0	75.1	27.2	28	.	.	.	5	2	.	3	15	14	11	2	.	.	1
VIII	3	4.0	.		0.5	2.0	3.5	1.7	1	1.0	7.5	2.9	42	4.8	17.5	2.3	18	3.0	79.1	31.0	11	.	.	.	6	5	.	2	6	15	12	2	.	.	4
IX	.	.		.	0.5	4.0	7	3.1	8.5	3.9	12	4.0	20.5	3.8	15.5	2.6	26	2.5	11.9	3.4	7	.	.	.	9	3	1	10	7	8	5	.	1	.	1
X	.	.			2	2.0	14	3.9	25	3.8	15	7.3	5	5.7	16	2.9	16	3.6	46.7	18.5	20	.	.	.	.	5	2	4	9	7	7	1	.	.	.
XI	4.5	3.3		.	.	.	4	2.2	9	3.1	11	6.9	25.5	3.8	28	3.0	11	3.3	61.3	17.6	13	.	.	7	.	3	2	1	19	17	9	3	5	.	.
XII	7.5	2.5	1	3.0	1	3.0	3	4.3	14.5	3.1	11	7.3	16	8.8	34	2.8	5	4.3	39.8	12.5	11	12	13	23	.	9	4	.	13	19	11	1	.	22	.
Rok	33	2.1	6.5	0.8	10.5	2.2	67.5	3.0	91.5	4.1	143	5.6	259.5	5.2	278.5	3.2	205	3.6	528.3	31.0	11.VIII	21	23	69	25	59	26	48	129	160	107	10	12	43	19

Szczekociny $H_s = 262\ m$ $h_w = 14\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	⊕	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	3	1.3			2	2.0	5	1.6	7	3.4	21.5	4.3	25	4.5	9.5	4.0	20	3.0	116.0	23.0	31	.	.	.	8	3	.	2	10	17	13	5	.	.	6
VIII	1	5.0	1.5	3.6	2.5	2.4	4.5	3.6	7.5	6.0	49.5	5.8	12.5	5.0	11	5.1	33	3.3	49.3	17.3	12	.	.	.	7	3	.	3	4	10	8	1	1	.	3
IX	1	3.0	2	3.5	11	3.6	10.5	3.0	5	3.8	15	5.6	12.5	4.6	3	3.0	30	2.8	21.7	13.3	15	.	.	.	7	1	.	11	4	7	4	1	5	.	2
X	0.5	4.0	6	5.8	23.5	4.2	17.5	5.0	4.5	3.7	6	3.9	5	3.7	5	3.4	24	3.1	26	1.3	15	.	.	.	.	4	.	6	8	4	1	.	6	.	.
XI	4.5	2.8	1.5	5.0	10	4.1	6	2.7	5.5	5.4	14	4.8	7	5.2	6	3.0	35	2.6	77.8	13.2	14	.	.	–	.	.	.	.	24	17	11	2	5	.	.
XII	5.5	3.7	3	4.7	8	2.8	5.5	3.4	8.5	7.8	9	8.7	9	5.8	14.5	4.4	30	3.6	32.3	12.6	7	15	18	28	.	4	1	1	15	10	6	1	.	24	.
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Skroniów $H_s = 256\ m$ $h_w = 16{,}5\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	⊕	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	1	3.0	4	2.4	11	1.9	11	2.8	4.5	1.9	14.5	4.4	15	3.3	8	4.8	24	2.4	23.0	7.9	4	13	15	29	.	2	.	5	13	11	6	.	3	22	.
II	0.5	5.0	.	.	3.5	3.4	10	1.9	7.5	2.5	11.5	2.7	19.5	3.6	43.5	4.6	18	2.6	23.3	7.0	9	.	.	19	.	.	.	.	17	10	6	.	2	5	.
III	0.5	7.0		.	.		.	.	.	.	12.5	6.4	50.5	5.5	25.5	7.3	4	5.9	29.4	4.7	18	.	.	6	.	6	.	.	15	16	12	.	2	3	1
IV	4	2.2	6	4.2	26	4.8	6	4.4	4.5	2.8	5.5	4.9	12.5	4.4	6.5	5.9	19	3.5	49.8	8.1	2	.	.	3	1	1	.	7	4	8	5	.	1	.	3
V	8	2.4	6	2.3	4	2.8	1	2.0	4	2.8	6	3.5	20.5	4.0	17.5	4.1	26	2.5	32.9	9.3	8	.		.	.	.	.	1	16	14	8	.	2	.	4
VI	1	4.0	3.5	2.1	8.5	3.0	7	2.4	4.5	1.9	6.5	1.8	18	3.9	15	4.5	26	2.3	90.8	50.2	11	.	.	.	10	.	.	4	5	10	7	2	1	.	9
VII	2.5	1.6	.	.	1.5	3.0	1.5	3.0	2	2.0	10	4.8	35.5	3.5	15	3.6	25	2.6	125.7	25.1	4	.	.	.	7	1	1	3	11	17	14	4	.	.	7
VIII	3.5	3.3	1	2.0	2	3.5	1.5	4.3	0.5	3.0	15	3.6	28.5	4.2	14	4.0	27	2.8	39.6	15.4	12	.	.	.	6	1	.	3	7	11	8	1	.	.	4
IX	1	5.0	2	2.0	1.5	2.8	4	2.8	.	.	14.5	3.1	23	4.7	6.5	4.8	24	2.7	16.9	7.4	14	.	.	.	8	.	.	10	5	8	3	.	2	.	4
X	0.5	2.0		.	2.5	3.9	25.5	3.4	2.5	4.0	3.5	3.3	8	3.7	9	4.1	19	2.9	2.7	1.2	14	.	.	.	.	.	.	5	9	4	1	.	3	.	.
XI	5	4.4	1	5.0	13.5	4.5	7.5	2.2	3	2.0	11.5	3.9	20.5	4.0	9	3.8	19	3.0	81.7	24.5	11	.	.	14	.	1	.	1	19	17	11	3	3	.	.
XII	11.5	4.3	3.5	2.6	8	2.6	4	1.9	2	2.0	13	6.6	9.5	5.4	17.5	5.2	24	3.4	43.4	16.7	11	13	19	25	.	2	.	1	17	16	7	2	3	24	.
Rok	39	3.4	27	1.9	118	3.0	79	2.6	35	2.1	124	4.1	261	4.2	157	4.7	255	3.0	529.2	50.2	11.VI	26	34	96	32	14	1	40	138	142	88	12	22	54	32

Staszów $H_s = 193\ m$ $h_w = 16{,}2\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	⊕	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R
I	3.5	2.7	4	3.8	2	3.0	12	4.2	9	2.4	3	2.0	11.5	3.4	12	3.1	36	2.0	24.6	6.8	31	13	14	28	.	.	.	5	12	13	6	.	.	20	:
II	.	.	1	2.0	8	2.9	9.5	3.2	12	3.0	5	1.9	12.5	2.7	9	3.8	27	2.0	21.7	6.6	9	.	.	20	.	.	.	1	18	12	6	.	4	3	.
III	.	.	.	.	.	.	1	3.0	2.5	2.8	9.5	4.0	36.5	5.3	30.5	5.0	13	4.2	22.1	4.4	18	.	.	8	.	5	.	1	15	15	9	.	1	2	.
IV	.	.	5	4.6	22	5.8	10	4.4	0.5	1.0	4.5	2.3	10.5	4.8	4.5	4.2	33	3.0	28.3	13.8	18	.	.	4	1	2	.	7	5	8	8	1	.	.	2
V	3.5	4.0	4.5	3.1	6	3.5	9	3.1	2	3.5	2	2.0	14	3.4	9	4.0	43	4.8	50.4	8.6	6	.	.	1	.	1	.	1	13	13	11		1	.	1
VI	1	4.0	2	2.0	7	3.7	13	3.6	1	4.0	3	2.0	9	4.3	14	3.9	40	2.0	139.5	58.0	3	.	.	.	10	.	.	5	4	12	12	3	2	.	9
VII	1	3.0		.	1	3.0	6.5	3.4	3	2.0	9.5	2.1	22	3.2	11	3.7	39	1.8	73.3	23.7	30	.	.	.	8	.	.	4	8	12	9	2	.	.	4
VIII	4	3.0	2	2.0	1	2.0	5	2.6	2.5	2.0	9.5	3.4	17	2.9	15	3.9	37	1.9	54.8	15.5	12	.	.	.	7	.	.	4	8	10	9	3	1	.	1
IX	3	2.7	7	3.3	6	3.3	4	2.5	2	2.0	3.5	2.6	14.5	4.4	8	3.0	42	1.8	17.9	11.2	14	.	.	1	7	1	.	11	7	7	4	1	5	.	1
X	2	4.0	1	4.0	20	4.8	22	6.0	4	3.0		.	4	2.2	6	2.6	34	3.0	5.7	3.7	30	.	.	6	.	2	.	8	8	6	2	.	4	.	.
XI	4	4.0	2.5	4.8	14.5	4.8	4	3.6	.	.	4	2.2	22	3.1	5	3.4	34	2.3	60.3	18.2	11	.	.	13	.	.	.	2	18	18	11	2	8	1	.
XII	6	4.6	9	4.1	3	1.7	2	2.5	4	1.8	6	4.5	3	2.3	21	4.2	39	2.2	48.5	16.2	6	15	16	26	.	.	.	1	15	16	9	2	5	21	.
Rok	28	2.4	38	2.8	90.5	3.2	98	3.5	42.5	2.3	59.5	2.4	176.5	3.5	145	3.7	417	2.3	547.1	58.0	3.VI	28	30	107	33	11	.	50	131	142	96	14	31	47	18

Tarnobrzeg

$\varphi = 50°34'$ $\lambda = 21°40'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.7	-8.9	8.6	4	-23.3	27	-6.7	-2.6	-4.7	-4.7	3.8	4.4	4.2	4.1	91	82	87	87	0.4	1.0	0.6	0.7	6.7	5.9	4.9	5.8
II	–	–	–	–	3.8	-1.4	9.5	28	-6.0	5	-0.5	2.8	0.7	0.9	5.6	5.9	5.9	5.8	94	80	91	88	0.4	1.6	0.6	0.9	8.0	7.4	6.8	7.4
III	–	–	–	–	9.6	1.7	20.0	18	-3.0	23	3.2	7.9	4.8	5.2	6.9	6.8	7.1	6.9	88	65	81	78	0.9	4.2	1.8	2.3	7.5	7.4	6.0	7.0
IV	–	–	–	–	17.2	4.8	25.1	15	-2.2	10	7.0	15.5	10.2	10.7	8.1	8.5	8.7	8.4	79	47	69	65	2.1	9.9	4.1	5.4	5.1	5.2	2.9	4.4
V	–	–	–	–	17.2	7.0	26.1	29	2.0	13	9.6	15.2	11.4	11.9	10.2	10.1	10.9	10.4	85	63	80	76	1.9	7.9	2.8	4.2	6.6	7.3	6.4	6.8
VI	–	–	–	–	24.6	11.8	32.6	26	6.4	21	15.4	23.1	16.9	18.1	15.0	13.5	15.1	14.5	85	48	78	70	2.6	15.5	4.3	7.5	5.3	5.0	5.0	5.1
VII	–	–	–	–	22.5	11.3	30.6	3	7.5	11	14.4	20.6	16.3	16.9	13.8	12.6	14.1	13.5	84	53	76	71	2.7	12.5	4.8	6.7	5.5	6.6	6.5	6.2
VIII	–	–	–	–	23.0	12.0	33.7	11	7.9	15,31	14.1	21.3	16.6	17.2	14.5	13.9	15.2	14.5	88	55	80	74	1.9	12.3	4.1	6.1	5.4	6.2	4.8	5.5
IX	–	–	–	–	24.6	8.7	28.7	3,18	0.4	23	10.2	20.3	14.4	14.8	11.3	11.5	12.5	11.8	91	48	75	72	1.2	13.1	4.3	6.2	4.7	4.6	3.3	4.2
X	–	–	–	–	16.8	5.4	23.1	19	0.3	24	6.8	15.8	10.3	10.8	8.6	9.3	9.5	9.1	88	53	76	72	1.4	9.0	3.2	4.5	5.6	5.5	3.8	5.0
XI	–	–	–	–	7.1	1.2	14.8	3	-7.3	23	3.1	6.0	3.8	4.1	7.4	7.9	7.6	7.6	93	83	92	89	0.6	1.8	0.7	1.0	7.8	8.3	6.9	7.7
XII	–	–	–	–	-0.5	-8.0	15.3	5	-28.8	26	-5.1	-2.7	-4.5	-4.2	4.4	4.7	4.5	4.5	90	85	91	89	0.6	1.1	0.6	0.8	7.6	6.8	5.8	6.7
Rok	–	–	–	–	13.5	3.8	33.7	11.VIII	-28.8	26.XII	6.0	11.9	8.0	8.5	9.1	9.1	9.6	9.3	88	64	81	78	1.4	7.5	2.7	3.9	6.3	6.4	5.3	6.0

Biłgoraj

$\varphi = 50°33'$ $\lambda = 22°43'$

I	–	–	–	–	-1.4	-9.8	7.5	4	-25.5	27	-6.6	-2.0	-5.6	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.3	5.0	5.7
II	–	–	–	–	3.4	-1.8	8.6	28	-6.3	5,6,15	-0.4	3.0	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.4	8.1	7.9
III	–	–	–	–	9.0	0.9	18.6	18	-4.2	23	3.5	8.1	4.8	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	5.5	6.7
IV	–	–	–	–	16.8	3.0	25.1	15	-5.8	10	7.5	15.7	9.7	10.6	–	–	–	–	–	–	–	–	–	–	–	–	3.5	3.9	3.2	3.5
V	–	–	–	–	16.8	5.8	25.6	29	-0.5	17	10.4	15.7	11.0	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.4	5.7	6.4
VI	–	–	–	–	24.1	10.4	32.1	26,27	3.5	21	16.3	22.8	16.9	18.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.5	10.1	31.5	4	5.0	8	14.8	21.2	15.7	16.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	20.7	7.8	29.1	2	0.0	23	10.7	20.1	13.4	14.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	16.1	5.4	23.1	19	0.8	12	7.6	15.6	10.0	10.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.2	1.3	14.3	3	-10.3	23	3.1	6.4	4.1	4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.7	7.9	8.2
XII	–	–	–	–	-0.5	-7.0	15.1	5	-22.0	25	-4.7	-1.8	-4.0	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	6.3	7.1
Rok	–	–	–	–	–	–	–	–	-25.5	27.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Nisko

$\varphi = 50°31'$ $\lambda = 22°09'$

I	–	–	–	–	-0.4	-8.7	7.4	4	-23.5	26	-6.3	-2.2	-4.9	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.4	5.9	6.0
II	–	–	–	–	4.5	-0.9	9.7	18	-4.9	7	0.1	3.4	1.1	1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.2	7.1	7.7
III	–	–	–	–	10.2	2.0	20.6	18	-3.7	23	4.2	8.2	5.1	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.0	6.1	7.2
IV	–	–	–	–	17.8	3.9	26.6	15	-3.9	10	7.4	16.2	10.0	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.1	2.7	4.4
V	–	–	–	–	17.7	6.9	25.7	27	0.4	19	10.5	15.9	10.8	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.2	6.4	7.2
VI	–	–	–	–	25.1	11.5	32.9	26,27	4.5	21	17.1	23.4	16.3	18.3	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.5	5.0	5.4
VII	–	–	–	–	23.6	10.7	32.7	3	5.9	8	15.1	21.3	15.5	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	7.8	6.7	6.6
VIII	–	–	–	–	23.6	11.8	33.5	11	4.3	31	14.9	21.9	16.0	17.2	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.8	5.1	5.4
IX	–	–	–	–	21.8	8.0	29.9	18	-2.0	23	10.9	20.5	13.9	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.6	3.5	4.1
X	–	–	–	–	16.8	5.5	24.2	19	0.6	11	6.8	15.9	9.9	10.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.7	3.0	4.2
XI	–	–	–	–	7.4	1.6	15.0	3	-8.6	23	3.0	6.3	4.0	4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.8	7.1	7.5
XII	–	–	–	–	-0.2	-8.3	14.3	2	-29.7	25	-5.2	-2.1	-4.6	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.1	6.2	6.7
Rok	–	–	–	–	14.0	3.7	33.5	11.VIII	-29.7	25.XII	6.5	12.4	7.7	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.5	5.4	6.0

Karfantów

$\varphi = 50°29'$ $\lambda = 17°36'$

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.4	11.4	31.9	3	5.6	8	15.3	19.5	15.3	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	7.1	7.2
VIII	–	–	–	–	22.1	11.6	30.3	10	8.0	17	15.1	20.4	16.0	16.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.0	4.5	5.8
IX	–	–	–	–	22.5	8.6	31.0	2	0.7	23	12.7	21.3	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	3.9	3.2	4.1
X	–	–	–	–	16.6	5.7	22.4	6,8	0.2	16	7.8	15.6	10.0	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.6	4.3	5.7
XI	–	–	–	–	6.8	1.1	13.4	1	-5.3	23	2.6	6.0	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.1	6.6	7.1
XII	–	–	–	–	0.7	-7.3	18.0	5	-25.6	26	-4.1	-0.9	-3.5	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.4	5.0	6.4
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Tarnobrzeg

H_s = 175 m h_w = 15,2 m

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD}																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	K
I	5.5	1.5	3.5	1.7	2	2.0	3	2.2	15	4.4	19	3.1	14	4.8	6	3.0	25	2.5	21.7	8.1	14	12	14	29	·	–	–	5	11	18	5	·	3	22	·
II	1.5	2.0	4	1.8	2	3.5	2.5	3.2	11.5	4.2	18	3.6	22.5	2.7	3	3.3	19	2.5	20.8	3.5	10	·	·	21	·	–	–	1	14	19	6	·	7	4	·
III	·	·	·	·	·	·	·	·	·	·	15.5	5.5	60.5	7.0	12	8.6	5	6.6	20.7	4.8	13	·	·	6	·	–	–	1	13	15	6	·	1	2	·
IV	7	1.4	5.5	2.1	9	4.8	13.5	6.3	4	4.4	14.5	4.1	14.5	6.8	2	8.5	20	3.8	39.9	21.8	16	·	·	1	1	–	–	6	4	8	7	1	·	·	3
V	5	1.6	1	1.0	2	1.5	7.5	3.1	5.5	3.1	7.5	2.5	15	2.9	8.5	2.4	41	1.5	55.5	11.1	6	·	·	·	3	–	–	·	12	18	12	1	2	·	6
VI	4.5	1.0	1.5	1.7	3.5	4.4	6.5	4.3	7	2.0	6.5	2.5	16.5	3.0	5	2.5	39	1.6	67.7	19.5	26	·	·	·	14	–	–	2	5	13	10	2	1	·	8
VII	3.5	1.7	·	·	1	2.0	·	·	4	3.6	16	3.7	36.5	2.7	5	4.2	27	2.2	55.1	16.3	30	·	·	·	10	–	–	3	8	14	9	2	·	·	5
VIII	3	1.5	3.5	1.6	·	·	1	2.5	3.5	2.1	15.5	3.1	27	3.8	8.5	3.2	31	2.1	58.0	26.5	9	·	·	·	8	–	–	2	6	11	7	1	·	·	6
IX	1.5	1.0	6.5	4.4	7.5	1.7	6	4.3	3.5	1.4	11	2.8	25	4.4	4	4.2	25	2.4	40.9	6.6	14	·	·	·	7	–	–	11	6	5	3	·	6	·	3
X	1.5	1.0	0.5	1.0	7.5	3.7	30.5	4.7	12.5	4.5	6	2.6	7.5	2.3	3	1.8	24	2.9	11.9	8.4	30	·	·	·	·	–	–	9	6	6	2	·	7	·	·
XI	6	1.8	2	2.2	5.5	4.7	13.5	3.6	5	2.6	16.5	3.0	19	3.9	4.5	2.9	18	2.7	61.4	17.0	7	·	·	10	·	–	–	2	18	22	12	3	9	·	·
XII	10	2.9	7	2.9	6	1.8	3	1.7	2.5	4.6	19	5.3	12	5.3	12.5	4.2	21	3.2	44.3	8.8	11	11	15	24	·	–	–	2	13	27	9	·	8	25	·
Rok	49	1.4	35	1.4	46	2.5	87	3.0	74	3.1	165	3.5	270	4.1	74	4.1	295	2.8	467.9	26.5	9.VIII	23	29	91	43	–	–	44	116	176	88	10	44	53	31

Biłgoraj

H_s = 190 m h_w = 19 m

I	5	1.4	1	1.0	7	1.3	21	1.6	6	2.3	14	2.4	4	1.8	16	3.2	19	1.7	13.8	5.8	31	13	16	29	·	1	·	5	10	10	4	·	1	20	–
II	1	2.0	·	·	4	1.0	13	1.8	15	1.3	4	1.5	18	1.8	6	1.5	23	1.2	40.1	4.5	9	·	1	20	·	·	·	·	17	8	3	·	9	·	–
III	·	·	·	·	·	·	1	1.0	4	2.2	14	2.5	56	3.9	13	6.4	5	3.7	27.9	4.3	29	·	·	11	·	6	1	1	13	17	11	·	·	·	–
IV	2	2.0	4	2.0	17.5	3.0	14.5	5.4	9	2.0	4	3.2	8	5.6	4	3.5	27	2.6	23.6	4.6	8	·	·	6	1	3	·	8	2	9	7	·	1	·	–
V	2	1.5	4	3.0	9	1.9	9	1.9	9	2.3	3	1.7	16	2.2	13	2.3	28	1.5	66.6	20.4	14	·	·	1	1	·	·	·	8	14	9	2	1	·	–
VI	5	2.2	·	·	10	2.2	14	1.7	4	2.0	8	2.0	22	2.2	4	2.0	23	1.5	80.1	24.0	3	·	·	·	14	·	·	–	–	12	11	2	·	·	–
VII	3	1.7	·	·	2	1.5	4	1.8	6	2.7	8	2.0	25	2.5	14	2.1	31	1.5	116.2	32.7	20	·	·	·	9	·	·	–	–	13	10	5	·	·	–
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	·	·	·	–	–	–	–	–	–	–	–	–	·	–
IX	4	1.2	3	1.7	6	1.3	6	1.3	13	1.8	8	2.0	15	1.8	1	1.0	34	1.0	40.0	3.0	6,7	·	·	·	6	·	·	–	–	7	3	·	2	·	–
X	2	1.5	1	1.0	30	2.2	26	3.5	8	2.2	·	·	10	1.5	5	2.0	11	2.2	16.5	11.5	30	·	·	·	·	·	·	–	–	6	4	1	·	·	–
XI	3	1.3	5	1.6	7	2.4	18	1.7	7	1.6	8	1.9	18	1.8	6	2.0	18	1.4	39.8	14.2	13	1	·	10	·	·	·	1	20	11	8	2	2	·	–
XII	12	1.8	2	4.0	2	1.5	17	1.5	9	1.9	11	2.7	14	2.5	14	2.9	12	1.9	34.5	11.1	11	10	17	23	·	·	·	2	14	11	7	1	1	17	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24	34	100	–	–	–	–	–	–	–	–	–	37	–

Nisko

H_s = 164 m h_w = 16 m

I	6	2.3	6	2.0	8.5	2.5	19.5	2.3	16.5	2.7	11	4.1	18	2.9	7.5	3.1	·	2.8	20.0	5.0	2,14	12	15	29	·	1	·	5	13	7	6	·	·	24	·
II	2	3.0	·	·	11	1.5	6.5	2.2	18.5	2.2	8.5	2.1	29.5	2.3	8	1.2	·	2.1	20.4	5.0	1,9	·	·	18	·	·	·	2	16	10	6	·	3	2	·
III	·	·	·	·	·	·	4	1.8	7.5	3.3	19.5	4.2	55	5.9	7	6.8	·	5.2	38.2	8.0	21	·	·	9	·	9	3	1	13	15	11	·	3	·	·
IV	2	3.0	5.5	2.1	26	5.7	9	5.0	11	2.3	7.5	3.7	20	3.0	8	3.4	1	3.9	38.0	10.5	18	·	·	2	2	6	·	7	3	8	7	1	1	·	2
V	5.5	2.5	3	1.7	13	1.9	6	2.6	9	2.5	8	2.5	29	2.3	17.5	3.3	2	2.5	65.2	15.0	14	·	·	·	3	1	·	·	13	13	11	1	·	·	4
VI	5.5	1.9	·	·	14	3.4	14.5	2.3	6.5	2.1	8	2.8	25.5	2.6	12	2.2	4	2.5	50.8	20.5	12	·	·	·	15	1	·	4	6	15	9	1	·	·	7
VII	4.5	1.9	·	·	1.	3.0	4.5	2.8	11.5	3.4	16	1.9	37	2.8	15.5	1.9	3	2.4	106.8	23.0	29	·	·	·	9	1	1	3	11	17	12	5	·	·	4
VIII	5.5	1.9	1	3.0	5	2.8	4	1.8	11	2.0	15	3.9	34.5	2.4	14	3.2	3	2.6	74.3	32.0	9	·	·	·	9	·	·	5	9	11	10	2	·	·	4
IX	2.5	1.4	3	1.0	17	2.0	4.5	2.4	13.5	1.4	8	2.0	31	2.6	5.5	2.6	5	2.0	17.5	12.0	6	·	·	2	8	·	·	15	7	3	3	1	2	·	1
X	1	2.0	1.5	1.7	27	4.3	22.5	3.6	16.5	3.7	3.5	2.4	15	2.4	3	3.0	3	3.4	18.6	10.0	30	·	·	·	·	·	·	12	6	4	4	1	2	·	·
XI	1	3.0	0.5	1.0	13.5	4.0	16	2.4	16	1.9	17	2.6	19	2.6	7	3.6	·	2.7	45.4	12.0	13	·	·	10	·	·	·	4	18	13	8	2	2	1	·
XII	6.5	2.5	4	4.0	.7	2.0	13.5	1.9	13	3.1	9.5	2.9	21.5	2.2	17	4.8	1	2.8	51.9	15.0	7	11	16	23	·	1	·	4	12	12	10	2	2	18	·
Rok	42	/2.1	24.5	1.1	143	2.8	124.5	2.6	150.5	2.6	131.5	2.9	335	2.8	122	3.3	22	2.9	547.1	32.0	9.VIII	23	31	93	46	20	4	62	127	128	97	16	15	45	22

Korfantów

H_s = 200 m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	75.4	23.5	15	·	·	·	7	–	–	3	15	11	5	4	3	·	4
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	35.1	7.1	11	·	·	·	5	–	–	3	10	11	10	·	2	·	3
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	43.8	6.0	6	·	·	·	8	–	–	11	5	5	3	·	7	·	·
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27.6	13.2	20	·	·	·	·	–	–	6	8	4	4	1	7	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48.0	8.6	6	·	·	8	·	–	–	3	15	13	10	·	7	1	·
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34.5	10.7	11	11	14	25	·	–	–	3	11	12	7	1	2	5	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Zawiercie

$\varphi = 50°29'$ $\lambda = 19°26'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.9	-7.5	9.5	4	-21.0	18	-5.3	-1.7	-4.5	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	4.0	-1.0	11.1	18	-6.9	6	-0.1	3.2	0.9	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.6	5.8	6.9
III	–	–	–	–	8.7	1.6	18.2	18	-3.9	20	2.9	7.1	4.6	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	5.5	6.6
IV	–	–	–	–	17.0	5.1	24.8	15	-1.4	10,11	8.7	15.4	9.6	10.8	–	–	–	–	–	–	–	–	–	–	–	–	3.0	4.0	3.1	3.4
V	–	–	–	–	16.5	6.2	25.2	27	1.1	2	9.6	15.3	10.2	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.4	5.7	6.1
VI	–	–	–	–	23.8	11.2	32.4	27	4.1	16,17	16.1	21.7	15.8	17.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	20.8	10.9	30.4	3	6.0	6	14.3	18.9	14.2	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.1	7.1	5.0	5.7
VIII	–	–	–	–	21.9	11.2	30.9	10	6.0	14	14.4	20.4	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	32.4	27.VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Otmuchów

$\varphi = 50°28'$ $\lambda = 17°10'$

I	–	–	–	–	1.7	-6.7	11.5	4	-21.7	27	-4.2	0.5	-2.8	-2.3	3.9	4.4	4.3	4.2	78	67	78	74	1.2	2.3	1.3	1.6	6.3	6.5	6.5	6.4
II	–	–	–	–	6.9	-1.1	14.2	18	-8.3	6	0.6	6.0	1.8	2.6	5.7	6.4	5.9	6.0	88	69	84	80	0.8	3.2	1.2	1.7	7.6	6.8	5.4	6.6
III	–	–	–	–	11.0	1.8	20.2	10	-4.1	20	3.5	9.8	5.2	5.9	6.5	6.9	7.0	6.8	82	59	79	73	1.5	5.7	2.1	3.1	7.3	6.8	7.4	7.1
IV	–	–	–	–	17.9	4.3	27.0	7	-1.9	10	8.7	16.8	10.3	11.5	9.2	9.2	9.5	9.3	80	50	75	68	2.3	10.7	3.4	5.5	5.2	6.2	4.7	5.4
V	–	–	–	–	16.4	6.7	23.6	26	1.0	15	10.3	15.1	10.5	11.6	10.4	10.0	10.9	10.4	83	59	85	76	2.3	7.7	2.0	4.0	7.1	7.8	4.9	7.6
VI	–	–	–	–	23.4	10.4	30.5	27	5.7	17	16.1	21.6	15.8	17.3	14.6	14.2	15.3	14.7	79	56	84	73	3.9	12.2	2.9	6.3	4.8	5.6	5.2	5.2
VII	–	–	–	–	21.6	11.0	32.5	3	4.0	8	15.3	20.4	15.5	16.7	13.6	12.8	13.8	13.4	78	54	78	70	4.2	12.0	4.1	6.8	6.6	6.8	7.5	7.0
VIII	–	–	–	–	22.3	11.6	30.8	6	5.6	4	15.3	21.1	16.1	17.2	15.0	15.3	15.2	15.2	85	61	83	76	2.7	10.3	3.4	5.5	6.5	7.0	5.3	6.3
IX	–	–	–	–	23.0	9.0	30.3	17	-0.4	23	12.1	22.0	14.3	15.7	12.3	13.5	13.5	13.1	87	52	82	74	2.4	13.9	3.2	6.5	5.7	4.6	3.2	4.5
X	–	–	–	–	16.7	6.1	23.2	6	-1.0	16	8.0	15.9	10.5	11.2	9.2	10.5	9.9	9.9	86	60	79	75	1.9	8.0	2.9	4.3	7.7	6.2	3.5	5.8
XI	–	–	–	–	7.3	1.2	14.0	2	-5.7	22	2.7	6.2	3.8	4.1	6.6	7.2	7.1	7.0	88	76	87	84	1.0	2.4	1.2	1.5	7.6	8.2	6.6	7.5
XII	–	–	–	–	1.3	-7.6	17.1	5	-25.1	26	-3.3	-0.4	-3.5	-2.7	4.5	4.9	4.3	4.6	80	72	76	76	1.2	2.1	1.3	1.5	8.7	7.1	6.6	7.5
Rok	–	–	–	–	14.1	3.9	32.5	3.VII	-25.1	26.XII	7.1	12.9	8.1	9.0	9.3	9.6	9.7	9.5	83	61	81	75	2.1	7.5	2.4	4.0	6.8	6.6	5.8	6.4

Kudowa - Zdrój

$\varphi = 50°27'$ $\lambda = 16°16'$

I	–	–	–	–	0.7	-6.2	6.7	4	-18.4	27	-4.2	-0.2	-3.3	-2.8	4.2	4.5	4.4	4.4	86	71	86	81	0.7	1.6	0.7	1.0	6.1	6.4	6.1	6.2
II	–	–	–	–	4.1	-1.1	10.3	18	-13.1	6	0.4	3.3	1.0	1.4	6.0	6.4	6.2	6.2	94	87	93	91	0.4	1.4	0.5	0.8	8.9	8.6	8.3	8.6
III	–	–	–	–	9.2	0.3	16.4	10	-6.5	20	1.7	7.7	4.1	4.4	6.5	7.1	7.0	6.9	93	68	86	82	0.6	3.9	1.3	1.9	7.4	7.5	6.2	7.0
IV	–	–	–	–	16.4	4.6	23.7	7	-0.7	10	7.6	15.0	9.7	10.5	9.0	9.1	9.6	9.2	85	56	79	73	1.7	8.6	2.6	4.3	4.8	5.9	4.3	5.0
V	–	–	–	–	14.8	5.5	22.3	26	0.3	15	8.8	13.6	9.0	10.1	10.2	9.7	10.2	10.0	89	63	89	80	1.3	6.3	1.4	3.0	8.4	8.2	6.6	7.7
VI	–	–	–	–	21.9	9.8	27.9	25	2.6	16	14.2	20.1	14.8	16.0	14.2	14.1	14.4	14.2	87	61	85	78	2.2	9.9	2.6	4.9	5.3	5.1	5.1	5.2
VII	–	–	–	–	19.9	9.9	30.3	3	3.8	8	13.0	18.0	13.5	14.5	13.2	12.9	13.2	13.1	87	64	85	79	2.0	8.5	2.6	4.4	7.1	7.0	6.8	7.0
VIII	–	–	–	–	20.7	10.4	29.4	6	4.9	14	13.1	19.2	14.2	15.2	14.1	15.0	14.7	14.6	92	68	90	83	1.2	8.0	1.7	3.6	6.7	6.7	6.1	6.5
IX	–	–	–	–	21.1	8.1	27.5	5	0.9	23	10.1	20.2	12.9	14.0	11.8	13.5	13.2	12.8	93	58	88	80	0.9	11.0	1.9	4.6	5.0	4.7	3.3	4.3
X	–	–	–	–	14.2	5.4	20.3	5	0.2	16	7.6	13.4	8.6	9.6	9.1	10.3	9.6	9.7	88	69	87	81	1.7	5.6	1.8	3.0	6.8	6.6	4.5	6.0
XI	–	–	–	–	5.6	0.5	11.7	12	-7.6	22	1.8	4.6	2.7	3.0	6.6	7.0	7.0	6.9	91	81	92	88	0.6	1.6	0.6	0.9	8.3	8.2	7.8	8.1
XII	–	–	–	–	0.6	-7.7	15.8	5	-23.3	25,26	-4.5	-0.8	-3.8	-3.2	4.6	5.1	4.6	4.8	88	78	85	84	0.6	1.4	0.8	0.9	7.5	7.0	6.4	7.0
Rok	–	–	–	–	12.4	3.3	30.3	3.VII	-23.3	25.26.XII	5.8	11.2	7.0	7.8	9.1	9.6	9.5	9.4	89	69	87	82	1.2	5.6	1.5	2.8	6.9	6.8	6.0	6.6

Góra Św. Anny

$\varphi = 50°27'$ $\lambda = 18°10'$

I	–	–	–	–	-0.3	-6.0	9.7	4	-17.9	27	-4.7	-1.5	-3.2	-3.2	4.1	4.8	4.5	4.5	88	84	88	87	0.5	0.9	0.5	0.6	–	–	–	–
II	–	–	–	–	4.6	-0.7	10.6	18	-6.8	6	0.2	3.4	1.7	1.8	5.8	6.5	6.4	6.2	92	83	92	89	0.5	1.4	0.5	0.8	–	–	–	–
III	–	–	–	–	9.1	2.2	18.5	10	-3.1	20,28	3.8	7.8	4.4	5.1	6.9	7.0	7.6	7.2	86	68	90	81	1.3	4.1	0.9	2.1	–	–	–	–
IV	–	–	–	–	16.9	6.5	25.1	7	-0.9	1	9.3	15.7	9.7	11.1	9.3	9.1	10.3	9.6	78	52	84	71	2.6	9.4	2.0	4.7	–	–	–	–
V	–	–	–	–	16.0	7.3	22.4	26	2.9	12	9.8	14.7	9.6	10.9	10.6	9.7	11.1	10.5	87	60	91	79	1.7	7.4	1.1	3.4	–	–	–	–
VI	–	–	–	–	21.7	12.6	28.5	27	7.3	16	15.4	20.5	15.4	16.7	14.1	14.1	15.2	14.5	80	59	86	75	3.6	10.5	2.5	5.5	–	–	–	–
VII	–	–	–	–	20.0	11.9	29.1	3	8.4	6	14.0	18.4	13.8	15.0	13.6	13.5	14.1	13.7	84	64	88	79	2.7	8.6	2.0	4.4	–	–	–	–
VIII	–	–	–	–	21.1	12.3	28.6	10	8.6	17	14.8	20.0	14.6	16.0	14.2	15.4	14.8	14.8	84	66	89	80	2.9	8.5	2.0	4.5	–	–	–	–
IX	–	–	–	–	20.7	11.3	27.5	18	7.1	22	13.4	19.9	13.9	15.3	12.8	13.0	13.7	13.2	83	57	86	75	2.8	11.0	2.3	5.4	–	–	–	–
X	–	–	–	–	15.3	7.7	20.9	8	4.0	16	10.0	14.3	9.8	11.0	10.3	10.1	10.8	10.4	84	64	89	79	2.1	6.5	1.4	3.3	–	–	–	–
XI	–	–	–	–	6.0	1.2	12.0	3	-3.7	21	2.6	5.0	3.1	3.4	6.9	7.7	7.3	7.3	92	87	94	91	0.6	1.3	0.5	0.8	–	–	–	–
XII	–	–	–	–	-1.0	-7.3	13.2	5	-21.4	25	-4.5	-2.5	-4.4	-4.0	4.5	4.9	4.5	4.6	88	85	89	87	0.6	1.0	0.5	0.7	–	–	–	–
Rok	–	–	–	–	12.5	4.9	29.1	3.VII	-21.4	25.XII	7.0	11.3	7.4	8.3	9.4	9.6	10.0	9.7	86	69	89	81	1.8	5.9	1.4	3.0	–	–	–	–

Zawiercie

$H_s = 335\ m$ $h_w = 12\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU (°D, °mD)																		OPAD R			Temperatura T				Wiatr		LICZBA DNI (n)								
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	> 10 m/s	> 15 m/s	●	●	Opad R ≥ 0,1	Opad R ≥ 1,0	Opad R ≥ 10,0	≡	▤	ZR
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n																		
I	3	1,7	5	1,7	18	2,2	7,5	2,5	20,5	1,9	19,5	2,4	8	1,8	25	1,0	9	1,9	24,8	7,0	4	10	16	28	·	·	·	–	–	11	6	·	–	25	·
II	·	·	·	·	4	2,0	8	1,4	2,2	1,4	17,5	1,7	19,5	1,8	4	1,8	9	1,5	35,3	11,4	1	·	1	19	·	·	·	3	13	9	7	1	–	6	·
III	15	7,0	·	·	·	·	·	·	6	3,8	16,5	3,1	5,5	3,3	6,5	3,8	11	3,0	49,5	10,2	14	·	·	8	·	2	·	3	12	12	8	1	–	4	1
IV	2,5	2,6	11,5	2,0	28,5	6,1	1,5	5,3	14,5	2,5	6	2,9	8,5	3,4	4	2,0	13	3,4	36,9	8,6	1	·	·	3	·	5	·	12	3	6	6	·	–	·	3
V	12,5	2,5	4,5	2,4	6,5	2,0	1,5	1,7	9	3,5	5,5	2,0	2,2	2,6	12,5	2,4	19	2,0	47,5	10,6	29	·	·	·	1	1	1	3	11	12	11	1	–	·	3
VI	3,5	1,0	2,5	1,4	1,6	1,8	2	1,5	7,5	2,3	9,5	1,9	2,4	1,8	1,1	2,4	14	1,6	93,6	48,0	27	·	·	·	11	·	·	–	–	11	9	2	–	·	4
VII	·	·	·	·	·	·	0,5	1,0	10,5	2,0	2,0	2,3	3,8	1,6	4	2,4	20	1,5	138,7	19,6	13	·	·	·	7	·	·	5	8	14	13	7	–	·	1
VIII	4	1,4	0,5	2,0	5	2,2	1	1,0	1,1	1,8	1,6	2,0	3,0	1,9	7,5	1,6	18	1,5	70,1	26,0	12	·	·	·	8	·	·	–	–	12	9	2	–	·	4
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	34,5	14,2	14	–	–	–	–	–	–	–	–	6	3	2	–	–	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	5,4	1,7	19	–	–	·	–	–	–	–	–	5	3	·	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	75,1	22,8	13	–	–	–	–	–	–	–	–	13	11	2	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	52,7	18,0	6	–	–	–	–	–	–	–	–	7	7	2	· –	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	664,1	48,0	27.VI	–	–	–	–	–	–	–	–	118	93	20	–	–	–

Otmuchów

$H_s = 211\ m$ $h_w = 11,6\ m$

I	0,5	3,0	1,2	1,4	7,5	1,6	1,5	2,0	7,5	2,5	1,7	2,3	7	1,7	1,3	2,2	2,7	1,4	55	33	14	10	11	25	·	·	·	6	15	7	1	·	1	1,6	·
II	2	3,5	0,5	1,0	1,5	1,0	1	1,0	2	1,7	8	2,6	2,2	2,0	1,6	2,4	3,1	1,4	26,5	6,1	9	·	·	1,8	·	·	·	5	1,3	1,5	8	·	4	·	·
III	5	2,8	1	5,0	·	·	·	·	·	·	2	1,8	2,4	3,4	4,0	3,9	2,1	2,8	35,0	8,0	14	·	·	11	·	1	·	1	1,5	1,7	9	·	1	2	·
IV	5	1,8	9,5	1,9	11,5	1,8	5,5	1,5	4	1,9	5	2,3	11,5	2,0	9	1,9	2,9	1,3	22,3	5,6	27	·	·	4	2	·	·	7	9	8	6	·	2	·	3
V	9	2,1	7,5	1,3	3,5	1,3	1	1,5	0,5	2,0	6	1,9	1,9,5	1,9	2,9	2,2	1,7	1,6	62,0	22,0	29	·	·	·	·	·	·	1	1,5	1,9	1,3	1	·	·	·
VI	9	1,9	7,5	1,2	8	1,4	2	1,5	1,5	2,7	0,5	2,0	13,5	2,1	1,9	2,1	2,9	1,2	43,0	7,3	8	·	·	·	8	·	·	5	7	1,2	9	·	·	·	5
VII	7	2,7	5	1,3	2,5	1,6	1,5	1,3	1,5	1,3	3,5	2,0	1,4	2,8	3,0	3,5	2,8	1,8	75,0	21,6	28	·	·	·	6	·	·	4	1,7	1,3	9	3	·	·	·
VIII	5	1,4	2,5	1,0	4	1,2	·	·	2,5	1,0	8,5	2,8	2,1,5	2,9	1,8	2,8	3,1	1,7	55,3	11,8	11	·	·	·	6	·	·	2	7	1,5	1,1	2	2	·	5
IX	0,5	4,0	3	1,0	1,1,5	1,5	4	1,9	1,5	1,3	3,5	2,0	8,5	2,5	10,5	3,6	4,1	1,1	23,7	8,5	6	·	·	1	1,0	·	·	1,2	7	8	4	·	6	·	1
X	2,5	1,8	4	2,5	1,1,5	2,5	10,5	3,0	8	2,2	8,5	2,7	12,5	1,9	1,3,5	2,3	2,2	1,8	53,4	19,1	20	·	·	1	·	·	·	4	7	7	7	2	7	·	·
XI	8,5	1,8	2	1,8	4,5	1,2	·	·	2	1,8	4,5	2,2	1,3,5	3,0	2,2	2,2	3,3	1,4	38,0	9,1	4	·	·	9	·	·	·	2	1,6	1,3	9	·	7	·	
XII	5	1,8	3,5	1,7	4,5	1,1	1	3,0	1	3,0	8	3,5	14	3,2	2,7	2,7	2,9	1,8	33,4	6,6	12	12	12	24	·	·	·	1	1,3	1,9	10	·	·	1,9	
Rok	5,9	2,4	5,8	1,8	7,0,5	1,3	2,8	1,4	3,2	1,7	7,5	2,3	1,8,1,5	2,4	2,4,7	2,6	3,4,4	1,6	473,1	22,0	29.V	22	23	93	32	1	·	50	141	153	96	8	30	37	14,2

Kudowa - Zdrój

$H_s = 385\ m$ $h_w = 13,5\ m$

I	1,5	1,7	1,1,5	2,2	9,5	3,2	4,5	2,9	1,2,5	1,6	10,5	1,6	9,5	1,8	0,5	2,0	3,3	1,4	38,3	18,9	31	10	12	26	·	2	·	6	12	12	6	1	3	3	·
II	3	1,0	5	1,2	1	1,0	3,5	1,0	10,5	1,6	1,2	1,2	10,5	1,6	2,5	1,4	3,6	0,8	20,0	4,7	11	1	·	1,4	·	·	·	·	2,1	1,4	5	·	9	4	·
III	4,5	1,0	6	1,0	0,5	1,0	·				4	1,2	4,1	2,0	1,3	1,6	2,4	1,3	44,9	11,9	30	·	·	1,7	·	2	·	3	1,2	1,4	9	1	4	4	·
IV	5,5	1,1	2,1,5	1,6	9	3,6	2	5,5	1,5	2,3	3,5	1,6	1,4,5	2,0	3,5	2,3	2,9	1,4	66,8	29,8	27	·	·	3	·	·	·	6	9	1,2	10	1	2	·	4
V	7	1,1	10	1,8	1	2,0	0,5	3,0	1,5	3,0	1	2,0	2,7	1,7	8	1,5	3,7	1,0	85,2	16,1	9	·	·	·	·	·	·	·	1,6	1,8	1,2	3	2	·	5
VI	4,5	1,0	1,5	2,1	1,5	2,7	1,5	2,3	1	2,5	1	3,0	1,7	1,6	8,5	1,5	4,0	1,0	86,2	2,9,7	22	·	·	·	6	·	·	7	7	1,0	8	2	1	·	6
VII	6	1,3	8	1,4		·	1	1,5	1,5	2,0	2,5	1,8	3,1,5	2,2	7,5	1,9	3,5	1,2	112,9	30,1	28	·	·	·	5	·	·	2	1,2	1,7	1,3	4	3,3	·	3
VIII	6,5	1,3	8	1,5	·		1	2,0	2	1,5	2	2,0	3,1,5	2,0	1,0	1,8	3,2	1,2	111,6	58,8	11	·	·	·	4	·	·	3	1,2	1,6	1,0	3	6	·	2
IX	6	1,5	9,5	1,8	1,5	3,7		·	4,5	2,2	3,5	1,9	1,3,5	2,0	8,5	2,0	4,3	1,0	19,5	9,1	14	·	·	·	8	2	·	10	7	6	4	·	7	·	·
X	5,5	1,7	1,9,5	2,3	5	4,0	5	2,8	1,0	2,4	1,5	2,0	1,3,5	2,0	3	1,8	3,0	1,6	51,4	18,2	17	·	·	·	·	2	·	4	8	7	5	3	5	·	
XI	4,5	1,2	1,0,5	2,0	1	4,0		·	2	1,5	4	2,0	2,9,5	1,6	1,5	1,0	3,7	1,0	31,3	11,4	30	·	·	8	·	1	·	2	2,0	1,3	8	1	5	·	
XII	4,5	1,7	11	1,9	8	2,3	0,5	1,0	4,5	1,6	4	2,4	2,5,5	1,8	4	2,4	3,1	1,3	37,3	14,6	11	13	14	2,5	·	·	·	3	1,5	1,4	8	1	3	1,7	
Rok	5,9	1,3	1,3,5,5	1,7	3,8	2,3	1,9,5	1,8	5,1,5	1,8	4,9,5	1,9	2,6,4,5	1,9	7,0,5	1,8	4,0,7	1,2	705,4	58,8	11.VIII	24	26	93	23	9	·	46	151	153	98	20	50,8	28	20

Góra Św. Anny

$H_s = 370\ m$ $h_w = 16\ m$

I	4	2,0	1,3	2,8	1,7	2,3	1,5	3,1	3,1	6,7	2	1,5	5	2,2	2	1,0	4	3,8	90	32	14	7	16	29	·	5	2	–	–	12	2	·	5	20	·
II	·	·	·	·	9	1,4	2,8	2,9	1,0	4,2	5	1,8	1,3	3,8	7	1,9	1,2	2,5	55,0	25,6	9	·	·	1,7	·	2	·	–	–	1,5	9	2	9	4	·
III	4	1,8	·	·	·	·	·	5	2,0	1,7	4,1	5,7	3,7	7	6,9	3	3,7	43,9	11,2	14	·	·	6	·	5	2	–	–	1,7	11	1	4	4	1
IV	5	2,4	1,2	2,6	2,0	2,9	9	4,5	1,8,5	4,5	5,5	3,9	9,5	3,8	6,5	2,3	4	3,3	13,6	7,8	1	·	·	1	1	7	1	–	–	5	4	·	·	·	2
V	1,4	1,9	4	2,1	3	1,0	2,5	1,4	1,6	2,7	9	2,0	2,6	2,6	1,4,5	2,2	4	2,2	96,5	26,7	29	·	·	·	·	2	·	–	–	1,4	1,2	3	3	·	5
VI	7	2,5	5,5	1,9	8	2,4	5,5	3,0	1,0	1,8	7,5	1,9	2,9,5	2,3	1,6	2,2	1	2,2	100,6	34,1	27	·	·	·	5	·	·	–	–	1,3	9	2	2	·	9
VII	2,5	2,0	4	1,2	1,5	1,3	1,5	2,0	2,7	3,2	1,5,5	4,2	3,3,5	3,0	6,5	3,1	1	3,1	146,5	40,2	13	·	·	·	6	1	·	–	–	1,2	10	3	1	·	3
VIII	4	2,0	5	1,0	4	1,5	8	2,3	1,1,5	3,7	1,1,5	3,0	2,2	2,0	2,5	2,8	2	2,5	52,5	24,5	12	·	·	·	3	3	·	–	–	1,7	10	1	·	·	3
IX	1,5	2,0	8,5	2,5	1,9,5	1,9	1,1	2,2	2,0,5	2,6	7,5	2,4	1,2	3,4	7,5	1,7	2	2,4	31,5	17,9	14	·	·	·	7	1	·	–	–	7	3	1	1	·	1
X	·	·	1	6,0	2,8	3,5	1,2,5	3,2	2,4,5	4,9	7	1,6	1,4	1,9	6	1,7	·	3,4	16,2	8,6	19	·	·	·	·	5	3	–	–	8	4	·	5	·	·
XI	1,1	2,1	1	6,0	8	2,0	1,6,5	1,8	2,7	3,3	4,5	3,1	1,5	3,0	1,8,5	2,6	2	2,5	63,5	15,2	13	·	2	1,2	·	2	·	–	–	1,8	9	3	6	2	·
XII	1,8,5	2,7	1,5	1,3	6	1,2	6,5	2,5	3,0,5	4,8	2,5	8,0	1,5,5	4,5	1,1	3,7	1	3,8	69,8	14,6	11	12	18	2,6	·	4	·	–	–	1,4	12	3	3	2,0	·
Rok	7,1,5	1,8	5,5,6	2,3	1,2,4	1,8	1,1,6	2,4	2,3,1,5	3,7	9,4,5	3,1	2,3,8,5	3,0	1,2,7,5	2,7	3,6	3,0	698,6	40,2	13.VII	1,9	3,6	9,1	2,2	3,7	8	–	–	1,5,2	9,5	1,9	3,9	5,0	2,4

Busko - Zdrój

$\varphi = 50°27'$ $\lambda = 20°43'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnie				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{m.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.4	-8.2	6.6	4	(-24.7)	27	-6.0	-4.9	-4.4	-4.2	4.0	4.5	4.4	4.3	89	79	89	86	0.4	1.1	0.5	0.7	6.3	5.8	5.7	5.9
II	–	–	–	–	4.5	-4.0	11.5	18	-5.5	5	0.0	3.0	1.3	1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.8	6.5	7.7
III	–	–	–	–	9.7	2.1	19.8	18	-2.9	20	3.8	8.1	4.8	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.1	6.3	7.0
IV	–	–	–	–	17.1	5.6	25.7	15	-0.6	10	8.6	15.5	9.9	11.0	8.4	8.6	8.5	8.5	74	49	69	64	3.0	9.7	4.1	5.6	4.4	4.7	2.9	4.0
V	–	–	–	–	17.3	6.6	24.8	27	0.8	15	10.4	15.5	10.8	11.9	10.4	9.9	10.4	10.2	81	57	80	73	2.5	8.4	2.8	4.6	6.5	7.0	5.9	6.5
VI	–	–	–	–	24.3	12.2	33.2	27	6.4	16	15.9	22.7	16.6	18.0	14.9	13.8	14.7	14.5	82	51	78	70	3.3	14.4	4.3	7.3	4.9	5.3	4.9	5.0
VII	–	–	–	–	22.3	11.8	31.2	3	7.5	6	14.6	20.3	15.5	16.5	13.9	13.3	14.2	13.8	82	57	81	73	2.9	11.4	3.7	6.0	5.2	6.5	5.5	5.7
VIII	–	–	–	–	22.6	12.1	32.8	11	8.7	18	14.6	21.3	16.0	17.0	14.8	14.4	15.3	14.8	88	57	83	76	2.0	11.9	3.4	5.8	5.4	5.9	4.5	5.3
IX	–	–	–	–	21.4	9.7	29.4	18	3.5	24,25	11.4	20.1	14.3	15.0	11.9	12.0	12.4	12.1	86	52	75	71	1.9	12.4	4.3	6.2	4.7	5.0	3.3	4.3
X	–	–	–	–	16.7	6.9	24.0	20	3.9	17,22	8.2	16.0	10.6	11.3	9.2	9.6	9.7	9.5	85	54	77	72	1.8	8.9	3.2	4.6	5.6	4.9	3.4	4.6
XI	–	–	–	–	7.1	1.6	14.9	3,7	-6.2	21	3.0	6.1	3.6	4.1	7.2	7.7	7.5	7.5	92	81	92	88	0.6	2.0	0.6	1.1	7.7	7.6	6.1	7.1
XII	–	–	–	–	-0.6	-7.5	17.0	5	-25.9	26	-4.5	-2.7	-4.6	-4.1	4.6	4.8	4.5	4.6	91	92	90	91	0.5	1.2	0.6	0.8	7.8	7.0	7.4	7.4
Rok	–	–	–	–	13.5	4.3	33.2	27.VI	-25.9	26.XII	6.7	12.0	7.9	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.3	5.2	5.9

Tomaszów Lubelski

$\varphi = 50°27'$ $\lambda = 23°25'$

I	–	–	–	–	-1.4	–	6.3	4	–	–	-6.9	-3.1	-6.3	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.3	6.6	7.0
II	–	–	–	–	2.5	-2.4	8.8	28	-9.0	7	-1.2	1.7	0.0	0.1	5.0	5.6	5.4	5.3	87	80	88	85	0.7	1.4	0.7	0.9	8.7	8.1	8.0	8.3
III	–	–	–	–	9.1	0.9	18.2	18	-5.3	21	2.7	6.7	4.3	4.5	6.7	6.9	6.9	6.8	88	71	82	80	0.9	3.2	1.6	1.9	9.1	8.3	6.8	8.1
IV	–	–	–	–	–	3.8	–	–	-2.5	10	7.3	14.5	8.7	9.8	8.1	8.3	8.6	8.3	78	49	75	67	2.4	9.1	2.9	4.8	5.5	6.1	4.0	5.2
V	–	–	–	–	16.9	5.7	25.2	29	-0.3	17	9.9	14.9	10.0	11.2	10.6	10.3	10.7	10.5	86	62	86	78	1.8	7.3	1.9	3.7	7.3	8.0	6.7	7.3
VI	–	–	–	–	23.6	10.8	30.9	26,27	4.6	21	16.6	21.6	15.5	17.3	14.9	14.4	14.9	14.7	78	57	84	73	4.2	12.1	2.9	6.4	4.9	7.2	5.7	5.9
VII	–	–	–	–	23.5	11.1	31.6	4	6.3	19	15.5	21.4	14.8	16.6	14.1	13.7	14.0	13.9	80	55	83	73	3.8	12.5	3.2	6.5	6.2	7.2	5.9	6.4
VIII	–	–	–	–	22.4	11.3	32.7	11	7.2	31	14.9	20.7	15.3	16.6	15.0	15.4	15.3	15.2	88	63	87	79	2.2	9.9	2.4	4.8	6.0	6.9	5.8	6.2
IX	–	–	–	–	20.4	7.9	28.4	18	-3.2	23	10.5	19.0	12.4	13.6	11.6	12.6	12.1	12.1	89	57	83	76	1.5	10.2	2.8	4.8	4.9	5.1	4.2	4.7
X	–	–	–	–	15.6	3.2	20.9	19	-3.9	12	5.1	14.8	7.8	8.9	8.0	9.1	8.7	8.6	90	56	82	76	0.9	8.0	2.0	3.6	6.3	5.5	3.9	5.2
XI	–	–	–	–	7.1	0.7	14.9	3	-6.9	24	3.0	6.0	4.0	4.2	7.2	8.0	7.6	7.6	91	84	90	88	0.6	1.7	0.8	1.0	8.9	6.4	8.4	8.6
XII	–	–	–	–	-0.5	-8.4	15.4	5	-24.8	25	-4.9	-2.7	-4.8	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	7.8	8.2
Rok	–	–	–	–	–	–	32.7	11.VIII	–	–	6.0	11.3	6.8	7.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	6.2	6.8

Kłodzko

$\varphi = 50°26'$ $\lambda = 16°39'$

I	980.5	1001.0	957.5	1020.9	0.1	-6.3	8.5	31	-21.8	27	-4.7	-1.2	-3.3	-3.1	4.1	4.4	4.3	4.3	86	75	84	82	0.7	1.4	0.8	1.0	7.0	6.7	7.2	7.0
II	984.0	999.4	953.3	1023.8	4.8	-4.2	13.2	18	-13.0	6	0.5	3.5	1.3	1.6	5.8	6.4	5.9	6.0	90	81	87	86	0.6	1.5	0.9	1.0	9.0	7.9	6.6	7.8
III	982.0	999.5	956.7	1020.9	10.2	1.0	17.7	10	-6.5	20	2.3	8.6	4.9	5.2	6.4	7.1	7.1	6.9	88	65	81	78	1.0	4.5	1.8	2.4	7.3	7.0	6.8	7.0
IV	974.2	983.3	967.2	1012.4	16.6	4.4	24.0	7	-2.9	10	6.8	15.3	9.9	10.5	8.8	8.9	9.5	9.1	87	52	78	72	1.4	9.1	2.9	4.5	5.7	5.9	5.0	5.5
V	975.3	982.6	962.5	1013.6	15.4	5.7	23.1	26	0.7	13	8.4	13.8	9.5	10.3	10.0	9.6	10.3	10.0	90	62	87	80	1.2	6.6	1.7	3.2	7.8	8.1	7.6	7.8
VI	978.4	992.6	966.1	1016.0	22.2	9.9	28.8	25	3.5	16	14.0	20.5	15.8	16.5	14.1	13.7	14.2	14.0	87	58	79	75	2.2	10.8	4.0	5.7	5.1	6.2	5.5	5.6
VII	977.5	989.0	962.7	1015.1	20.7	9.9	30.5	3	3.2	8	13.3	18.8	14.3	15.2	12.9	12.1	12.9	12.6	84	57	78	73	2.6	10.5	3.7	5.6	6.6	7.0	6.3	6.6
VIII	980.1	994.7	969.7	1017.7	21.3	10.6	29.0	10	4.7	4	13.3	19.7	14.8	15.6	14.0	14.6	14.6	14.4	90	63	86	80	1.6	9.0	2.5	4.4	6.5	7.1	6.5	6.7
IX	981.5	992.4	969.7	1019.4	21.8	8.2	29.8	18	-0.8	23	10.3	20.7	13.5	14.5	11.5	12.5	12.8	12.3	91	53	82	75	1.6	12.6	3.0	5.7	5.3	5.0	4.2	4.8
X	980.1	993.3	952.5	1018.5	14.9	6.0	20.6	5	-0.5	16	7.7	13.9	9.5	10.2	8.9	9.9	9.7	9.5	86	65	83	78	1.9	6.4	2.3	3.5	8.5	7.4	5.0	7.0
XI	976.5	998.4	963.4	1015.5	5.9	0.7	12.2	2	-6.7	21	2.0	4.7	3.0	3.2	6.6	7.1	7.0	6.9	91	82	91	88	0.7	1.6	0.8	1.0	8.1	8.2	7.7	8.0
XII	977.8	1003.5	959.3	1017.9	0.4	-7.7	17.0	5	-26.4	26	-4.5	-1.5	-3.9	-3.4	4.5	4.7	4.5	4.6	87	77	84	83	0.8	1.6	1.0	1.1	8.4	6.8	7.3	7.5
Rok	979.0	1003.5	952.5	1017.7	12.9	3.4	30.5	3.VII	-26.4	26.XII	6.8	11.4	7.4	8.0	9.0	9.2	9.4	9.2	88	68	83	79	1.4	6.3	2.1	3.3	7.1	6.9	6.3	6.8

Świerklaniec

$\varphi = 50°26'$ $\lambda = 18°57'$

I	–	–	–	–	-0.1	-8.0	9.5	4	-23.2	27	-5.6	-0.9	-4.2	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.9	6.7	6.9
II	–	–	–	–	4.5	-0.8	13.2	18	-8.0	6	0.5	3.4	1.4	1.7	–	–	–	–	–	–	–	–	–	–	–	–	9.5	8.8	6.8	8.4
III	–	–	–	–	9.6	2.2	19.1	18	-3.2	20	3.5	7.8	5.5	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.8	6.8	7.5
IV	–	–	–	–	17.4	4.6	25.1	7	-3.4	10	8.0	15.9	10.3	11.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.5	4.1	5.0
V	–	–	–	–	17.2	6.1	23.7	26	1.3	12	9.6	15.3	10.2	11.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.0	7.5	8.0
VI	–	–	–	–	23.8	11.3	31.3	27	4.1	21	16.1	21.9	16.2	17.6	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.1	6.2	5.9
VII	–	–	–	–	21.2	11.3	30.9	3	7.2	11	14.6	19.4	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.6	6.7	7.0
VIII	–	–	–	–	22.0	11.2	30.9	10	5.1	14	14.2	20.5	15.0	16.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.9	4.5	6.2
IX	–	–	–	–	21.8	8.6	28.9	17	1.3	24	11.6	20.4	12.8	14.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.1	2.9	4.7
X	–	–	–	–	16.5	5.4	21.2	6	0.4	22	7.1	15.6	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.1	4.3	6.1
XI	–	–	–	–	7.4	0.7	13.7	3	-6.6	23	2.8	6.1	3.4	3.9	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.0	7.3	8.1
XII	–	–	–	–	0.1	-7.9	15.8	5	-24.4	25	-4.1	-1.4	-4.5	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.4	6.4	7.2
Rok	–	–	–	–	13.4	3.7	31.3	27.VI	-24.4	25.XII	6.5	12.0	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	5.8	6.7

Busko - Zdrój

$H_s = 225\ m$ $h_w = 14\ m$ **1961**

MIESIĄC	ROZKŁAD WIATRU (%D, %wD)																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	10<v<15	v>15	●	≥0.1	≥1.0	≥10.0	▬	▩	≥1
I	2	2,5	5	3,0	11	4,7	15,5	2,4	22,5	3,6	8	3,0	8	3,4	14	3,0	7	2,7	19,5	5,4	14	12	14	28	·	1	·	5	10	9	5	·	3	23	·
II	3	3,3	·	·	6	2,8	4	2,2	20	3,1	15,5	2,2	22,5	2,6	6	2,5	7	2,5	25,0	8,0	9	·	·	18	·	·	·	·	16	11	7	·	10	1	·
III	2	4,0	·	·	·	·	·	·	3	3,7	14	6,4	49,5	4,2	22,5	5,3	2	4,7	29,7	8,0	18	·	·	7	·	9	1	3	12	19	11	·	3	2	1
IV	9,5	4,1	4,5	6,0	18	6,6	16,5	4,9	10	3,2	12	4,5	6	2,2	7,5	4,8	6	4,5	17,4	5,0	3	·	·	1	2	9	·	8	3	9	7	·	·	·	4
V	6	4,6	6	3,7	14,5	2,2	8,5	2,3	9,5	2,4	10	3,4	24,5	3,5	15	3,4	2	3,1	45,8	10,7	28	·	·	·	·	1	·	2	7	15	8	1	·	·	4
VI	8,5	2,4	6,5	3,8	7	3,6	13	4,2	6,5	2,6	7,5	3,2	20,5	2,8	16,5	3,3	4	3,1	87,2	40,6	27	·	·	·	13	·	·	3	3	12	10	3	1	·	12
VII	5	3,6	2	1,0	2	1,5	5,5	2,7	13	2,2	16	3,9	37,5	2,4	8	2,4	4	2,6	83,9	26,2	30	·	·	·	8	3	1	2	7	16	12	4	·	·	7
VIII	8	3,0	5,5	2,0	3	1,3	6,5	2,2	5,5	1,8	23	3,7	22	3,3	14,5	3,7	5	3,0	89,3	27,0	13	·	·	·	7	2	·	5	5	16	11	3	1	·	5
IX	2	3,5	4,5	3,8	18	3,4	9	2,3	5,5	1,5	13,5	3,3	19,5	4,0	6	4,9	12	3,0	11,6	5,5	14	·	·	·	8	2	·	12	7	9	4	·	3	·	1
X	3	4,0	2	4,5	23,5	6,0	3,0	5,1	12,5	5,2	4	3,5	6,5	2,9	7,5	2,1	4	4,6	31,1	4,2	30	·	·	·	·	8	·	7	5	6	1	·	3	·	·
XI	8	3,6	2	2,0	1,5	5,4	13,5	2,9	11,5	2,3	7,5	3,0	21	3,3	6,5	3,8	5	3,3	61,3	17,1	13	·	·	9	·	2	·	2	13	15	10	3	5	·	·
XII	14	3,9	4	6,0	10	3,5	7,5	2,5	6	4,4	14	5,0	11,5	5,4	13	5,2	13	3,8	51,2	19,0	6	10	17	26	·	3	·	2	17	15	6	2	4	24	·
Rok	71	3,5	42	3,0	12,5	3,2	12,9,5	2,8	12,5,5	3,0	14,5	3,8	24,9	3,3	13,7	3,7	71	3,4	524,8	40,6	27.VI	22	31	89	38	40	2	51	105	152	92	16	33	50	34

Tomaszów Lubelski

$H_s = 273\ m$ $h_w = 12\ m$

I	6,5	2,6	2,5	2,8	8	2,6	13,5	2,7	9,5	3,1	19	3,5	14,5	2,9	16,5	2,8	3	2,8	21,1	5,7	31	-	16	-	·	·	·	2	16	13	8	·	-	31	·
II	2	1,0	4,5	2,6	8,5	2,5	1,0	2,6	8	3,5	17	3,8	22	3,0	10	2,6	2	2,9	17,1	5,2	10	·	3	21	·	·	·	1	18	10	4	·	-	17	·
III	0,5	4,0	·	·	·	·	1	4,0	1	3,5	27,5	4,1	5,1	4,0	10	4,2	2	4,0	42,7	7,6	28	·	·	10	·	·	·	·	16	17	11	·	-	1	1
IV	6,5	3,5	5,5	3,4	2,0	4,2	6,5	5,6	9,5	3,8	17	3,4	14,5	3,9	10,5	2,6	·	3,8	24,1	7,5	1	·	·	4	-	·	·	5	5	8	5	·	-	·	1
V	4,5	2,3	6	2,6	11	3,2	6	2,9	7	3,1	8	3,1	25	3,5	24,5	2,8	1	3,0	54,7	17,2	14	·	·	1	-1	·	·	·	11	14	11	1	-	·	·
VI	7	2,6	6,5	3,5	15,5	3,4	5	2,7	7	3,1	8	3,0	18	3,2	22	2,8	1	3,0	70,5	18,0	12	·	·	·	11	·	·	2	9	12	9	2	-	·	5
VII	7	2,4	1	3,0	2	3,0	4	2,2	5	4,2	24	3,5	27,5	2,9	19,5	2,5	3	2,9	93,3	34,3	29	·	·	·	11	·	·	2	11	14	10	4	-	·	1
VIII	9,5	2,6	5	3,0	3	3,3	2	2,5	5,5	3,1	21	3,7	24	3,5	22	2,9	1	3,2	104,1	36,8	9	·	·	·	7	·	·	1	7	11	11	3	-	·	5
IX	6	2,2	14	2,6	5	2,8	3	2,7	3,5	3,0	14,5	3,5	25,5	3,3	13,5	2,9	5	2,8	15,2	5,0	14	·	·	2	7	·	·	12	9	9	4	·	-	·	·
X	2	3,2	1,5	2,8	32,5	3,3	1,3	4,7	5	3,1	4,5	3,2	9,5	2,4	7,5	2,5	4	3,1	10,7	7,0	30	·	·	4	·	·	·	8	9	3	3	·	-	·	·
XI	1	5,0	6,5	2,7	14,5	3,6	13,5	5,0	3	3,5	22	3,7	18,5	2,8	8	2,6	3	3,1	35,5	8,0	12	·	2	12	·	·	·	1	23	16	12	·	-	·	·
XII	6	2,8	6,5	2,7	1,3	2,2	4	1,8	10	3,6	19	3,6	11	3,4	17,5	3,7	6	3,0	34,9	7,0	2,0	12	18	26	·	·	·	1	21	15	8	·	-	23	·
Rok	58,5	2,9	7,3	2,6	13,3	2,8	8,1,5	3,1	7,4	3,4	20,1,5	3,5	26,1	3,2	18,1,5	2,9	3,1	3,1	520,9	36,8	9.VIII	-	3,9	-	-	·	·	35	155	142	96	10	-	72	13?

Kłodzko

$H_s = 316\ m$ $H_b = 320,1\ m$ $h_w = 15\ m$

I	12,5	2,8	4	2,2	1,5	2,3	1,5	5,7	33,5	7,1	7	4,4	5,5	3,7	3,5	3,4	24	3,8	7,6	3,1	31	9	13	25	·	6	3	6	18	10	2	·	3	17	·
II	3	2,0	·	·	·	·	2	3,5	24	5,7	8,5	3,2	14	3,1	9,5	2,5	23	2,9	15,0	5,0	9	1	1	18	·	5	1	·	18	13	4	·	8	4	·
III	2,5	2,4	1	2,5	·	·	·	·	1,5	4,7	6	4,6	34,5	5,1	23,5	3,8	24	3,3	33,7	5,1	30	·	·	13	·	5	·	2	16	17	12	·	1	5	·
IV	6,5	3,2	10,5	3,0	3	2,8	3	3,3	12	7,2	6	4,5	8,5	3,5	11,5	2,1	29	2,7	28,6	8,2	2	·	·	3	·	3	·	4	9	10	7	·	5	·	5
V	15,5	1,8	3,5	2,7	3	2,0	0,5	3,0	8	4,1	6,5	2,9	16	3,9	13	2,5	27	2,1	59,5	15,8	29	·	·	·	·	1	·	·	14	17	13	1	5	·	7
VI	13	1,8	1,5	2,3	2	1,0	0,5	5,0	6,5	2,8	1,5	3,3	21,5	3,7	12,5	2,9	31	1,9	53,0	24,2	8	·	·	·	5	1	·	4	8	12	9	2	4	·	8
VII	2	1,8	-	-	·	·	0,5	4,0	4,5	4,1	1,7	3,5	31,5	4,6	12,5	3,2	25	2,9	76,7	28,8	28	·	·	·	5	2	·	3	12	17	11	3	·	·	3
VIII	3,5	1,7	2	2,5	·	·	·	·	8,5	4,2	1,0	3,6	23,5	3,4	10,5	3,0	35	2,1	65,4	23,3	11	·	·	·	4	1	1	2	9	14	12	1	4	·	5
IX	7	2,7	1	2,0	1	2,0	1,5	4,0	1,3	4,3	7,5	3,1	9	3,3	3	3,0	47	1,6	16,4	8,4	6	·	·	2	9	·	·	10	9	5	3	·	4	·	2
X	5	2,3	4,5	3,4	0,5	6,0	3	5,8	2,7	5,9	5	3,8	6,5	2,5	2,5	3,4	39	2,7	64,4	23,5	20	·	·	1	·	5	1	2	13	7	7	2	8	·	·
XI	12,5	2,0	2	1,5	1	3,0	0,5	6,0	13,5	4,2	8,5	2,9	15,5	2,9	2,5	1,8	34	1,8	34,8	6,2	4	·	·	9	·	·	·	2	19	16	10	·	3	1	·
XII	1,4	2,9	3	2,5	0,5	4,0	1,5	4,7	1,7	5,8	9,5	4,1	9	2,8	8,5	5,1	30	2,8	26,2	6,4	12	12	14	24	·	·	·	·	14	17	~9	·	2	19	·
Rok	9,7	2,3	3,3	2,0	12,5	4,7	14,9	3,8	16,9	5,0	9,3	3,7	19,5	3,5	11,3	3,1	36,8	2,6	48,1,3	28,8	28.VIII	22	28	9,5	25	29	6	35	159	155	99	9	47	46	30

Świerklaniec

$H_s = 284\ m$ $h_w = 17\ m$

I	4	2,6	10,5	2,6	8	3,1	8	2,5	8	3,4	3,7	5,0	10	3,1	7,5	3,3	·	3,8	19,4	5,2	14	11	15	27	·	3	·	3	13	12	5	·	1	26	·
II	0,5	2,0	1,5	1,7	4,5	2,1	1,0	2,1	1,1	4,7	2,9	4,8	17,5	2,9	1,0	4,3	·	3,8	49,2	13,7	9	·	·	18	·	3	·	·	18	15	8	2	7	6	·
III	1,5	4,0	·	·	·	·	·	·	0,5	1,2	1,7	5,7	5,0	5,3	2,4	4,4	·	5,1	58,4	11,5	30	·	·	6	·	6	·	1	19	17	12	1	3	4	1
IV	5	2,4	9,5	2,1	18,5	4,5	1,3	3,3	4	3,1	15,5	5,5	10	5,6	9,5	3,6	5	3,6	41,4	14,7	1	·	·	3	1	1	·	5	3	8	6	1	·	·	4
V	12,5	2,4	3	2,5	4	2,2	5,5	2,6	3	4,0	2,0	4,4	12	4,5	3,0	3,4	3	3,4	55,7	10,3	29	·	·	·	·	1	·	·	17	17	11	1	1	·	5
VI	2,5	1,2	2,5	1,8	1,0	3,1	11,5	2,4	3,5	3,0	1,6	3,7	1,8	3,9	2,3	3,2	3	3,1	122,2	50,8	27	·	·	·	11	1	·	1	6	12	9	3	1	·	9
VII	2	1,5	·	·	·	·	3,5	2,1	4,5	2,9	3,4,5	4,0	2,7,5	3,3	1,4	3,3	7	3,2	21,2,0	45,6	13	·	·	·	7	·	·	·	12	17	13	8	1	·	7
VIII	4,5	1,6	3	2,0	4	1,8	5	2,2	5	3,2	2,8	4,7	2,1	4,3	12,5	2,8	10	3,3	52,1	16,6	12	·	·	·	7	2	·	1	6	13	8	1	3	·	3
IX	3	1,7	6	2,2	1,5	2,7	6,5	2,4	5	1,8	1,9	4,1	2,3	3,0	4,5	1,8	8	2,6	20,9	11,8	14	·	·	·	7	·	·	9	7	7	5	1	6	·	2
X	4,5	1,7	1,5	2,0	21,5	3,7	2,3	3,1	6,5	5,4	1,0	4,4	9	3,8	8	2,9	9	3,1	4,4	1,4	1,7	·	·	·	·	2	·	4	8	7	2	·	9	·	·
XI	5	2,2	5,5	2,3	6	2,4	9	2,1	3,5	2,3	30	4,7	13,5	4,0	11,5	2,9	6	3,3	91,2	32,0	13	·	·	10	·	3	·	·	18	17	12	2	7	2	·
XII	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	52,3	18,4	11	15	14	26	·	-	-	2	15	15	9	1	2	22	·
Rok	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	779,2	50,8	27.VI	24	29	90	83	-	-	26	142	157	100	21	41	60	31

Duszniki - Zdrój

$\varphi = 50°24'$ $\lambda = 16°24'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.3	-7.1	-9.1	31	-21.9	26	-5.0	-1.0	-4.3	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	5.9	6.2
II	–	–	–	–	4.2	-1.4	13.4	18	-11.3	6	0.1	3.7	0.5	1.2	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.2	6.2	7.0
III	–	–	–	–	8.4	0.8	16.4	10	-4.7	20	2.1	7.5	3.4	4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	6.3	7.8
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	13.9	5.3	21.7	27	0.6	15	8.5	13.2	7.7	9.3	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.6	6.3	7.7
VI	–	–	–	–	20.7	10.1	26.9	25	3.1	16	13.4	19.2	13.6	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.8	4.9	5.2
VII	–	–	–	–	18.8	9.4	28.9	3	5.0	8	12.7	17.6	12.2	13.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.4	6.5	6.8
VIII	–	–	–	–	19.9	9.9	27.8	6	4.3	14	13.1	19.1	13.3	14.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	5.3	5.8
IX	–	–	–	–	20.5	8.5	30.4	3	2.4	22	14.0	19.4	12.4	13.8	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.2	3.0	3.7
X	–	–	–	–	13.6	5.7	19.1	6	0.4	22	7.3	13.0	7.9	9.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.1	3.1	5.0
XI	–	–	–	–	5.3	0.3	10.3	2	-6.5	21	1.4	4.9	2.6	2.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.9	7.6	7.6
XII	–	–	–	–	-0.3	-7.9	1.4.8	5	-24.4	26	-5.1	-1.5	-4.6	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.1	6.5	6.6
Rok	–	–	–	–	–	–	30.4	3.IX	-24.4	26.XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Polanica - Zdrój

$\varphi = 50°24'$ $\lambda = 16°30'$

I	–	–	–	–	0.5	-6.3	7.9	31	-20.0	27	-4.8	-0.8	-3.4	-3.1	4.1	4.7	4.3	4.4	87	78	83	83	0.6	1.4	0.9	1.0	6.4	6.8	6.6	6.6
II	–	–	–	–	5.1	-1.3	12.5	18	-11.4	6	0.1	4.0	1.4	1.7	5.7	6.6	6.2	6.2	91	81	91	88	0.5	1.6	0.7	0.9	8.9	7.4	7.1	7.8
III	–	–	–	–	10.0	1.2	18.7	10	-5.4	20	2.6	8.6	4.8	5.2	6.5	6.9	7.0	6.8	88	63	81	77	1.0	4.8	1.8	2.5	7.1	7.1	6.1	6.8
IV	–	–	–	–	16.3	4.3	23.9	6	-2.3	10	7.7	14.9	9.0	10.2	9.0	9.3	9.6	9.3	84	56	83	74	1.8	8.4	2.2	4.1	4.6	5.9	4.7	5.1
V	–	–	–	–	15.2	5.7	22.4	26	0.6	15	9.2	13.6	8.8	10.1	10.4	9.9	10.3	10.2	89	64	90	81	1.4	6.1	1.3	2.9	8.0	8.2	6.9	7.7
VI	–	–	–	–	22.0	9.9	29.1	25	3.8	16	14.5	20.3	14.6	16.0	14.3	13.8	14.4	14.2	85	59	85	77	2.5	10.5	2.4	5.1	5.3	6.1	4.7	5.4
VII	–	–	–	–	20.4	10.0	29.9	3	4.4	8	13.6	18.5	13.7	14.9	13.2	12.8	13.1	13.0	84	61	83	76	2.7	9.0	2.9	4.9	6.5	7.2	5.6	6.4
VIII	–	–	–	–	21.2	10.8	29.6	6	5.3	4	13.6	19.9	14.5	15.6	13.8	14.8	14.5	14.4	87	64	87	79	2.1	9.0	2.4	4.5	6.5	6.2	5.5	6.1
IX	–	–	–	–	21.7	8.7	28.8	18	0.6	23	10.8	20.5	12.9	14.3	12.1	14.2	13.1	13.1	92	60	88	80	1.2	10.7	2.1	4.7	5.1	4.9	3.5	4.5
X	–	–	–	–	14.6	5.9	20.9	5	0.2	30	7.5	13.7	8.8	9.7	9.1	10.5	9.9	9.8	91	69	88	83	1.6	5.7	1.7	3.0	7.3	6.2	3.6	5.7
XI	–	–	–	–	5.7	0.4	12.9	2	-6.6	21	1.8	4.5	2.8	3.0	6.8	7.2	7.2	7.1	94	84	94	91	0.4	1.4	0.5	0.8	8.0	8.4	9.4	7.9
XII	–	–	–	–	0.5	-7.1	17.3	5	-22.8	25	-4.3	-1.5	-3.9	-3.4	5.0	5.4	4.7	4.9	89	82	88	86	0.7	1.3	0.8	0.9	7.8	6.3	5.9	6.7
Rok	–	–	–	–	12.8	3.5	29.9	3.VII	-22.8	25.XII	6.0	11.4	7.0	7.8	9.2	9.6	9.5	9.4	88	68	87	81	1.4	5.8	1.6	2.9	6.8	6.7	5.6	6.4

Wałbrom

$\varphi = 50°23'$ $\lambda = 16°45'$

I	–	–	–	–	-1.2	-9.3	7.1	4	-23.6	18	-6.0	-2.2	-5.2	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.7	5.6	6.1
II	–	–	–	–	3.6	-1.8	12.1	18	-6.9	6	-0.4	2.7	0.6	0.9	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.9	7.4	8.2
III	–	–	–	–	8.6	0.9	18.1	10	-4.4	23	2.6	7.0	4.1	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	7.1	7.6
IV	–	–	–	–	16.0	3.3	23.6	7	-4.0	10	7.4	14.8	8.5	9.8	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.4	2.9	3.8
V	–	–	–	–	16.3	4.4	24.2	27	-0.7	2	9.5	14.4	9.4	10.7	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.2	6.9	7.4
VI	–	–	–	–	23.0	9.6	30.5	27	3.4	21	16.0	21.4	14.7	16.7	–	–	–	–	–	–	–	–	–	–	–	–	4.5	6.0	4.6	5.0
VII	–	–	–	–	20.6	9.0	30.2	3	2.7	8	14.1	18.8	13.2	14.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.7	5.2	6.7
VIII	–	–	–	–	21.3	9.4	29.7	6	4.0	31	13.7	20.2	13.6	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.9	4.4	5.7
IX	–	–	–	–	20.4	6.9	28.7	17	-0.6	24	11.0	19.3	11.6	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.5	4.0	4.5
X	–	–	–	–	15.7	4.4	19.8	20	0.0	28	6.3	15.0	9.2	9.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	4.5	6.0
XI	–	–	–	–	6.6	0.2	14.0	10	-7.4	21	2.2	5.4	2.7	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.5	7.1	7.6
XII	–	–	–	–	-0.9	-9.8	16.9	5	-27.7	26	-5.5	-2.8	-5.4	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	7.0	7.6
Rok	–	–	–	–	12.5	2.3	30.5	27.VI	-27.7	26.XII	5.9	11.2	6.4	7.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	5.6	6.4

Ząbkowice

$\varphi = 50°22'$ $\lambda = 19°17'$

I	–	–	–	–	-0.2	-7.8	10.4	4	-19.4	27	-5.4	-1.1	-4.7	-4.0	3.8	4.1	4.0	4.0	85	72	84	80	0.7	1.7	0.7	1.0	6.6	6.7	5.3	6.2
II	–	–	–	–	4.4	-4.2	13.2	18	-6.9	6	-0.2	3.4	0.9	1.2	5.7	6.1	6.0	5.9	94	79	91	88	0.3	1.8	0.6	0.9	8.9	8.1	7.0	8.0
III	–	–	–	–	9.3	1.3	18.6	10	-3.8	20	2.5	7.6	4.5	4.8	6.7	6.6	7.2	6.8	91	65	85	80	0.7	4.2	1.5	2.1	7.8	8.4	7.1	7.8
IV	–	–	–	–	17.3	4.9	25.3	15	-2.0	10	8.6	15.9	9.6	10.9	8.3	7.9	8.5	8.2	74	45	71	63	3.2	11.0	3.7	6.0	3.9	4.5	3.6	4.0
V	–	–	–	–	16.9	5.7	23.7	6	-0.4	13	9.8	14.9	10.1	11.2	9.9	9.8	10.1	9.9	82	58	81	74	2.5	7.7	2.5	4.2	6.9	8.2	7.7	7.6
VI	–	–	–	–	23.5	11.3	32.8	27	3.6	16	16.1	22.0	15.5	17.3	14.2	13.2	15.0	14.1	78	51	84	71	4.4	13.8	2.8	7.0	4.0	6.1	5.4	5.2
VII	–	–	–	–	20.7	10.9	30.2	3	6.0	6	14.3	18.9	14.1	15.4	13.6	13.2	13.7	13.5	83	62	85	77	3.0	9.6	2.7	5.1	5.8	7.0	6.0	6.2
VIII	–	–	–	–	22.0	11.1	31.1	10	5.3	14	14.2	20.5	14.9	16.1	14.3	14.5	14.9	14.6	87	60	86	78	2.1	10.5	2.4	5.0	5.3	6.4	4.3	5.3
IX	–	–	–	–	21.2	9.3	29.5	17	3.5	22,24	11.9	20.2	13.2	14.6	12.0	11.8	12.4	12.1	84	51	80	72	2.2	12.5	3.0	5.9	4.6	4.5	3.5	4.2
X	–	–	–	–	16.6	6.4	21.5	5	2.6	14	7.6	15.6	10.0	10.8	9.2	10.0	9.9	9.7	88	58	81	76	1.4	8.0	2.5	4.0	5.9	5.5	3.9	5.1
XI	–	–	–	–	7.0	0.8	14.2	3,10	-7.4	21	2.3	6.0	3.2	3.7	6.9	7.4	7.2	7.2	92	78	90	87	0.6	2.3	0.7	1.2	7.9	7.1	7.1	7.4
XII	–	–	–	–	-0.4	-8.0	17.3	5	-25.3	26	-4.6	-2.0	-4.8	-4.0	4.6	4.7	4.3	4.5	89	80	87	85	0.6	1.5	0.7	0.9	6.7	5.9	5.7	6.1
Rok	–	–	–	–	13.2	3.7	32.8	27.VI	-25.3	26.XII	6.4	11.8	7.2	8.2	9.1	9.1	9.4	9.2	86	63	84	78	1.8	7.0	2.0	3.6	6.2	6.5	5.6	6.1

Duszniki - Zdrój H_s = 540 m h_w = 16 m 1961

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◔	●	Opad R > 0.1	R > 1.0	R > 10.0	═	▦	R / R
I	2	2,2	5,5	2,6	2	2,0	·	·	5	5,7	51,5	4,1	4,5	3,3	1,5	4,3	21	3,0	56,4	25,3	31	11	15	29	·	3	·	7	12	15	7	2	3	25	·
II	2,5	2,2	5,5	2,1	2	3,5	2	2,5	6,5	4,0	25	3,2	5	2,3	2,5	4,8	33	1,8	44,8	9,5	9	1	2	21	·	·	·	3	17	17	11	·	4	10	·
III	2	1,5	1,5	2,3	1,5	2,3	·	·	15,5	3,8	47	3,4	2,5	2,2	·	·	23	2,5	81,0	16,6	30	·	·	16	·	1	·	5	18	20	13	1	1	7	·
IV	7,5	2,3	3,5	2,7	3,5	1,7	·	·	6,5	4,1	21,5	2,4	5,5	2,0	3	1,8	39	1,4	89,9	21,0	27	·	·	2	·	·	·	–	–	12	10	3	3	·	1
V	16	2,5	5	3,2	1	1,5	·	·	5	3,9	27	3,6	4,5	2,2	4,5	3,3	33	2,0	118,9	24,2	9	·	·	·	·	1	·	·	14	19	17	3	·	·	5
VI	4	1,4	0,5	1,0	·	·	·	·	3,5	2,0	34,5	2,1	3	1,3	2,5	2,4	42	1,1	103,5	47,2	9	·	·	·	3	·	·	10	9	18	13	5	·	·	4
VII	2	2,0	·	·	1	2,0	1	3,0	3	2,5	33,5	3,0	13	3,2	0,5	3,0	39	1,7	134,5	35,4	28	·	·	·	4	·	·	3	13	22	18	4	·	·	2
VIII	4	2,0	·	·	·	·	·	·	·	·	42	3,0	8	2,8	3	2,0	36	1,8	87,3	26,1	12	·	·	·	2	·	·	4	10	19	18	3	·	·	2
IX	3	1,7	·	·	·	·	·	·	3	2,2	48,5	2,6	3,5	3,4	2	2,0	30	1,7	34,7	14,9	14	·	·	·	5	·	·	12	6	11	7	1	1	·	·
X	2,5	2,0	2	3,3	2	1,8	3,5	3,7	8	6,9	32	3,8	15,5	3,2	5,5	3,8	22	3,0	61,1	17,8	20	·	·	·	·	4	·	6	5	10	6	3	·	·	·
XI	12	2,2	5	2,6	6	2,2	1	2,0	·	·	28	3,8	2,5	4,4	5,5	2,3	30	2,1	80,2	16,4	30	·	·	12	·	·	·	3	19	21	15	2	7	1	·
XII	10	2,0	11	3,6	5,5	4,3	0,5	1,0	1	4,5	28,5	4,0	12	2,2	3,5	5,0	21	2,6	66,7	18,4	11	13	17	26	·	1	·	5	13	20	11	2	1	17	·
Rok	67,5	2,0	39,5	2,0	24,5	1,8	8	1,0	57	3,3	419	3,2	79,5	2,7	31	2,4	369	2,1	959,0	35,4	28.VII	25	34	106	14	10	·	–	–	204	146	29	20	60	14

Polanica - Zdrój H_s = 400 m h_w = 11,3 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	▦	R / R
I	5	2,2	2,5	2,8	3	2,7	6	3,2	10	4,4	45	3,6	7	2,6	6,5	2,3	38	1,9	25,8	13,6	31	10	12	25	·	·	·	6	17	11	6	1	–	18	:
II	0,5	2,0	·	·	3	2,3	3	2,0	3,5	4,6	8	3,5	17,5	3,3	11,5	3,7	37	1,9	23,6	6,0	9	1	1	20	·	1	·	·	18	12	7	·	–	5	·
III	2,5	3,2	·	·	·	·	·	·	·	·	8	5,2	39	3,6	19,5	3,5	24	2,8	49,4	11,4	21	·	·	14	·	·	·	3	9	15	14	1	–	5	·
IV	1,5	3,3	5,5	3,0	4,5	2,9	4	4,2	5,5	4,0	11,5	5,6	10	2,7	2,5	2,0	45	1,9	64,1	17,6	15	·	·	2	·	·	·	7	9	10	7	3	–	·	4
V	4,5	3,0	3	2,3	3	2,0	3	2,3	1	5,0	4	4,0	20,5	2,8	19	2,4	35	1,7	101,0	15,0	27	·	·	·	·	·	·	·	14	17	14	3	–	·	4
VI	3,5	2,3	2	2,0	·	·	2	2,5	1	2,0	25	4,0	15,5	2,7	14,5	2,4	49	1,2	67,8	29,4	8	·	·	·	5	·	·	6	7	11	8	2	–	·	4
VII	1,5	3,0	0,5	2,0	·	·	1	4,0	2,5	3,0	13	4,1	40	2,9	4,5	2,4	30	2,1	69,8	19,6	28	·	·	·	5	·	·	4	12	12	9	3	–	·	2
VIII	1,5	2,0	3	3,0	·	·	0,5	2,0	5,5	3,3	9	3,8	27,5	2,8	6	3,0	40	1,7	62,9	17,3	11	·	·	·	5	·	·	3	9	14	12	1	–	·	5
IX	6	2,3	0,5	3,0	0,5	3,0	1	3,0	2,5	3,4	6,5	3,2	16	2,7	7	2,1	50	1,2	14,5	7,9	14	·	·	·	9	·	·	11	6	7	3	·	–	·	1
X	4,5	2,1	1	3,0	4	2,8	10	4,6	8	3,3	9	4,2	7	2,6	7,5	2,2	42	1,8	56,3	21,2	20	·	·	·	·	·	·	6	10	7	6	3	–	·	·
XI	5	2,2	5	2,4	3	2,3	1	4,0	3	3,2	4	3,1	15,5	2,6	8,5	3,0	45	1,3	44,1	40,1	13	·	·	11	·	·	·	3	20	17	11	1	–	1	·
XII	4	1,2	5,5	3,1	3,5	3,1	1	5,0	3,5	2,0	14,5	5,8	11	3,3	11	2,5	39	2,1	37,6	8,6	11	12	13	24	·	1	·	2	13	13	9	·	–	19	·
Rok	40	2,4	28,5	2,2	24,5	1,8	32,5	3,1	46	3,2	105	4,2	226,5	2,9	118	2,6	474	1,8	613,9	29,4	8.VI	23	26	96	24	2	·	51	144	146	106	18	–	48	20

Walbrom H_s = 373 m h_w = 13,5 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	▦	R / R
I	1	1,0	3	2,0	10,5	1,9	4,5	5,8	3	4,3	20,5	4,9	14,5	3,3	1	3,0	35	2,3	26,7	9,0	4	13	16	28	·	2	·	4	13	13	5	·	–	26	·
II	0,5	1,0	·	·	3	3,3	7,5	3,6	3,5	3,4	15	3,9	26	3,6	2,5	4,2	26	2,5	34,9	6,0	9	·	2	21	·	1	·	1	19	14	10	·	–	5	·
III	0,5	2,0	·	·	·		·	·	0,5	14,0	13	6,4	58	5,6	11	6,2	10	5,2	54,8	9,1	29	·	·	10	·	10	2	1	16	18	13	·	–	4	1
IV	0,5	2,0	4	2,0	28,5	4,8	4,5	3,2	3	4,0	11,5	5,1	11,5	4,3	1,5	4,0	25	3,2	26,5	10,9	1	·	·	4	·	2	·	10	2	8	5	1	–	·	2
V	9	2,5	2	1,0	5	2,8	6	2,8	3	2,3	7	3,6	21	3,5	6	3,6	34	2,0	69,6	43,3	29	·	·	1	·	·	·	·	12	17	13	1	–	·	8
VI	·	·	1	2,0	9	3,1	3	3,0	2	3,0	9	3,2	21,5	3,5	1,5	5,0	43	1,7	100,3	24,6	12	·	·	·	6	·	·	6	5	15	12	3	–	·	12
VII	2,5	2,0	·	·	2	2,0	2	3,5	4	3,2	18	4,1	24	4,0	2,5	3,2	38	2,2	136,2	33,6	30	·	·	·	7	2	1	3	10	18	15	4	–	·	8
VIII	·	·	2	2,5	5	2,8	1	2,0	1	4,0	22	4,4	22	3,3	2	5,5	38	2,2	62,3	26,8	12	·	·	·	6	2	1	3	6	12	9	1	–	·	3
IX	4	2,0	·	·	14	3,8	2	4,0	3	3,3	10	2,8	22	4,0	·	·	35	2,2	14,3	6,0	14	·	·	1	6	1	·	10	8	10	3	·	–	·	2
X	1,5	2,0	·	·	30,5	4,4	9,5	4,6	·	·	11	3,3	14	3,4	1,5	3,3	25	2,9	5,4	2,6	14	·	·	·	·	2	·	5	10	5	3	·	–	·	·
XI	7	3,9	2	1,0	10	5,5	3	4,0	2	4,0	14	4,3	23	3,6	3	3,0	26	2,8	82,6	18,1	13	·	1	15	·	2	·	2	18	17	13	2	–	3	·
XII	11,5	3,7	4	2,0	2	1,5	1	3,0	2	3,0	18	4,8	13	5,5	6,5	2,6	35	2,6	71,3	19,6	11	16	18	27	·	2	·	1	16	17	12	2	–	24	·
Rok	38	1,8	18	1,0	119,5	3,0	44	3,3	27	4,0	169	4,2	270,5	4,0	39	3,6	370	2,6	684,9	33,6	30.VII	29	37	107	25	26	4	46	135	164	113	14	–	62	36

Ząbkowice H_s = 314 m h_w = 14 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R > 0.1	R > 1.0	R > 10.0	═	▦	R / R
I	5,5	1,5	8	2,6	14	2,7	9,5	1,9	8,5	1,2	12	2,9	12,5	2,0	7	1,6	16	1,8	25,2	9,2	4	12	14	28	·	·	·	5	12	13	7	·	4	21	
II	2,5	1,2	1	1,5	4	2,1	7	1,6	4,5	1,9	14,5	2,0	19	2,3	11,5	2,2	20	1,6	43,1	12,4	9	·	·	18	·	·	·	1	18	16	12	1	10	1	·
III	1,5	2,3	·	·	·	·	·	·	1,5	2,0	40	4,4	33	3,3	36	3,2	11	3,0	44,5	8,4	18	·	·	12	·	2	1	1	20	19	11	·	8	2	1
IV	4,5	2,0	10	2,1	26,5	4,5	6,5	4,0	3	1,7	8,5	3,7	11,5	2,3	9,5	3,1	40	3,0	21,8	7,1	1	·	·	3	1	1	·	12	4	6	6	·	·	·	2
V	16	2,2	6,5	1,8	8	1,8	2,5	1,8	1,5	2,3	8	2,8	13	4,4	23,5	2,6	14	2,3	75,3	18,1	29	·	·	2	·	1	·	1	17	16	13	3	5	·	4
VI	8,5	2,1	4,5	1,9	13	2,3	3	2,7	0,5	2,0	4,5	2,0	18	2,5	23	2,4	15	1,9	110,4	47,4	27	·	·	·	9	·	·	6	5	14	10	2	·	·	7
VII	6	1,5	2	1,0	1	3,0	1	2,0	2,5	3,0	12,5	2,4	23,5	2,6	19,5	2,1	25	1,7	166,6	27,7	8	·	·	·	7	1	1	5	8	17	15	7	3	·	6
VIII	6,5	1,6	2,5	1,8	5,5	2,3	1	1,0	1	1,5	12	3,0	21	2,7	21,5	2,3	22	1,8	67,5	28,7	12	·	·	·	7	1	·	5	5	10	9	1	4	·	2
IX	1,5	1,3	4	2,0	21	2,9	10	2,6	·	·	1,5	3,7	24,5	2,7	7,5	1,5	20	2,0	14,9	5,0	14	·	·	·	7	·	·	12	6	8	6	·	8	·	2
X	5,5	1,9	1	1,0	26,5	4,1	16	3,6	2,5	3,4	4,5	2,2	7,5	2,5	9,5	1,8	28	2,5	4,7	1,8	17	·	·	·	·	·	·	5	7	5	3	·	9	·	·
XI	6	1,8	3	1,5	14	2,3	2,5	1,2	1,5	2,0	13,5	2,2	21	2,3	11,5	1,8	17	1,7	79,2	21,5	13	·	·	10	·	·	·	2	16	19	14	2	16	2	·
XII	12,5	2,4	6,5	2,1	7,5	2,1	1	1,0	4	1,1	9	3,6	10,5	2,8	13	3,2	29	1,8	54,1	14,0	11	13	17	26	·	·	·	4	8	15	11	2	2	22	·
Rok	76,5	1,8	49	1,6	141	2,5	60	2,0	31	1,8	110,5	2,9	215	2,7	193	2,3	219	2,1	704,3	47,4	27.VI	25	31	99	31	6	2	59	126	158	117	18	69	48	24

Miechów

$\varphi = 50°22'$ $\lambda = 20°02'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																	
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.2	-9.5	6.0	31	-23.8	27	-6.8	-2.1	-5.6	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	5.6	5.5	6.2
II	–	–	–	–	4.1	-0.7	13.3	18	-5.4	5.6	0.0	3.2	4.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	6.9	8.0
III	–	–	–	–	9.1	2.0	18.4	18	-2.6	20	3.5	7.6	4.9	5.2	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.0	5.4	6.8
IV	–	–	–	–	16.4	3.9	24.5	15	-3.7	10	7.1	15.2	9.2	10.2	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.7	2.8	4.1
V	–	–	–	–	16.4	5.5	23.8	27	4.0	15	9.2	15.0	10.0	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	6.7	6.9
VI	–	–	–	–	23.2	10.2	31.5	27	4.1	17	15.6	21.9	15.3	17.0	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.8	5.8	5.0
VII	–	–	–	–	21.2	9.5	29.2	4	3.5	8	14.1	19.4	14.2	15.5	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	6.2	6.6
VIII	–	–	–	–	21.8	11.6	30.8	11	6.6	2	13.8	20.6	15.0	16.1	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.2	3.8	5.1
IX	–	–	–	–	20.9	7.8	28.8	17	0.4	24	9.9	19.8	12.8	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.3	2.7	4.1
X	–	–	–	–	16.2	4.5	21.9	20	-4.4	24	6.0	15.5	9.2	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.8	3.5	5.2
XI	–	–	–	–	6.9	0.6	14.5	3	-7.7	21	2.2	5.9	3.1	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	6.9	7.4
XII	–	–	–	–	-0.6	-9.0	17.8	5	-27.5	26	-5.5	-2.7	-5.6	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.0	5.8	7.0
Rok	–	–	–	–	12.9	3.0	31.5	27.VI	-27.5	26.XII	5.8	11.6	7.0	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.3	5.2	6.1

Tarnogród

$\varphi = 50°22'$ $\lambda = 22°45'$

I	–	–	–	–	-1.0	-9.5	9.5	4	-23.2	21	-6.4	-2.3	-5.4	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.3	4.5	5.7
II	–	–	–	–	3.5	-0.7	7.6	18	-4.8	7	-0.3	2.5	0.7	0.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.9	7.1	7.9
III	–	–	–	–	8.9	2.1	18.4	18	-2.8	23	3.4	7.2	4.7	5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	6.5	7.0
IV	–	–	–	–	16.7	5.0	24.9	15	-2.5	10	8.7	15.2	9.8	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	16.6	7.0	25.3	29	1.6	17	11.0	15.3	10.8	12.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	23.8	12.3	31.3	27	6.6	21	16.4	22.4	16.3	17.8	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.3	4.5	4.4
VII	–	–	–	–	21.9	11.7	30.7	4	7.1	8	15.4	20.8	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.9	4.5	5.0
VIII	–	–	–	–	22.4	12.3	32.5	11	7.1	31	14.7	21.2	15.8	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.6	3.2	4.3
IX	–	–	–	–	20.4	8.8	28.3	18	-0.9	23	10.8	19.6	13.0	14.1	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.2	3.7	4.0
X	–	–	–	–	16.0	5.7	23.4	19	1.1	17	7.9	15.4	9.3	10.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.4	1.9	14.3	3	-6.8	23	3.6	6.3	4.2	4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.3	7.0	7.3
XII	–	–	–	–	-0.1	-7.7	14.9	5	-24.7	25	-4.8	-2.1	-4.5	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.8	6.1	6.8
Rok	–	–	–	–	13.0	4.1	32.5	11.VIII	-24.7	25.XII	6.7	11.8	7.5	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Lądek - Zdrój

$\varphi = 50°21'$ $\lambda = 16°53'$

I	–	–	–	–	0.1	-6.6	7.3	31	-20.5	27	-5.1	-1.3	-3.6	-3.4	3.8	4.3	4.1	4.1	83	74	82	80	0.8	1.5	0.9	1.1	7.0	6.9	7.4	7.1
II	–	–	–	–	4.5	-1.5	12.3	18	-10.8	6	0.0	3.5	0.9	1.3	5.5	6.2	5.9	5.9	90	79	90	86	0.6	1.8	0.6	1.0	7.8	7.5	6.9	7.4
III	–	–	–	–	9.2	0.5	18.3	10	-2.9	22	2.0	7.4	4.1	4.4	6.1	6.6	6.6	6.4	87	6.5	81	78	1.1	4.2	1.8	2.4	8.4	8.2	6.8	7.8
IV	–	–	–	–	16.0	4.3	23.7	7	-2.7	10	7.4	14.8	9.0	10.0	8.5	8.9	9.0	8.8	82	54	79	72	2.1	8.5	2.7	4.4	5.2	7.1	5.9	6.1
V	–	–	–	–	14.3	5.2	22.0	26	0.3	15	8.3	12.5	8.4	9.4	9.7	9.8	10.2	9.9	89	68	91	83	1.4	5.1	1.1	2.5	8.8	9.5	7.3	8.5
VI	–	–	–	–	21.7	10.3	27.3	27	3.9	16	14.4	19.4	14.6	15.8	13.7	13.6	14.3	13.9	83	61	85	76	3.0	9.3	2.6	5.0	5.5	7.0	6.2	6.2
VII	–	–	–	–	19.7	10.1	30.0	3	5.8	26	13.2	17.9	13.6	14.6	12.7	12.2	12.7	12.5	83	60	81	75	2.8	9.1	3.3	5.1	7.8	8.1	6.8	7.6
VIII	–	–	–	–	20.3	10.8	28.2	6	6.3	17	13.4	18.7	14.0	15.0	13.6	14.4	13.9	14.0	87	66	87	80	2.1	7.8	2.4	4.1	7.0	8.2	7.0	7.4
IX	–	–	–	–	21.0	9.0	27.9	18	0.9	23	11.1	20.0	12.7	14.1	11.6	13.6	12.6	12.6	87	59	85	77	2.2	10.5	2.5	5.1	5.5	5.7	3.5	4.9
X	–	–	–	–	14.2	6.3	19.8	10	1.0	30	7.7	13.2	9.3	9.9	8.9	10.0	9.5	9.5	86	68	82	79	1.9	5.6	2.4	3.3	7.6	7.0	5.5	6.7
XI	–	–	–	–	5.8	0.0	22.2	2,12	-7.5	21	1.7	4.5	2.7	2.9	6.4	6.8	6.7	6.6	90	80	89	86	0.7	1.8	0.9	1.1	8.0	9.0	7.6	8.2
XII	–	–	–	–	0.2	-7.8	17.0	5	-26.5	25	-4.5	-1.8	-3.9	-3.5	4.5	4.6	4.5	4.5	87	77	84	83	0.8	1.6	1.0	1.1	7.6	6.9	6.5	7.0
Rok	–	–	–	–	12.2	3.4	30.0	3.VII	-26.5	25.XII	5.8	10.7	6.8	7.5	8.8	9.2	9.2	9.1	86	68	85	80	1.6	5.6	1.8	3.0	7.2	7.6	6.4	7.1

Bytom

$\varphi = 50°21'$ $\lambda = 18°55'$

I	–	–	–	–	0.4	-5.8	14.3	4	-17.2	18	-4.0	-0.4	-2.8	-2.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	5.4	6.0
II	–	–	–	–	4.9	-0.2	14.0	18	-7.2	6	1.0	4.0	2.1	2.3	5.6	5.9	5.7	5.7	85	74	80	80	1.0	2.3	1.5	1.6	8.6	7.1	5.7	7.1
III	–	–	–	–	9.9	2.2	19.4	18	-3.4	20	3.6	8.0	5.7	5.8	6.6	6.7	7.0	6.8	83	64	76	74	1.4	4.5	2.3	2.7	7.3	6.3	6.2	6.6
IV	–	–	–	–	17.6	4.8	25.3	7	0.5	10	8.4	16.1	11.0	11.6	8.2	8.3	8.6	8.4	73	46	65	61	3.1	10.7	4.9	6.2	3.6	4.3	3.5	3.8
V	–	–	–	–	15.8	6.3	23.5	27	2.1	12	9.8	14.8	10.4	11.4	10.3	10.2	10.8	10.4	85	61	85	77	1.9	7.2	2.1	3.7	7.1	7.6	6.2	7.0
VI	–	–	–	–	23.4	12.0	31.3	27	5.8	16	16.0	21.7	16.5	17.7	14.7	14.0	15.3	14.7	81	55	82	73	3.7	12.4	3.7	6.6	4.2	5.3	4.8	4.8
VII	–	–	–	–	20.2	11.5	31.6	3	7.7	11	14.6	19.0	14.7	15.8	14.0	14.0	14.2	14.1	84	66	85	78	2.9	8.8	2.8	4.8	5.2	7.1	6.0	6.1
VIII	–	–	–	–	21.7	11.8	30.8	10	6.7	14	14.3	20.5	15.3	16.4	14.9	15.0	15.2	15.0	90	62	86	79	1.7	9.8	2.5	4.7	5.2	5.8	2.8	4.6
IX	–	–	–	–	22.0	9.9	29.8	17	3.3	24	12.3	20.5	13.9	15.2	12.8	14.1	13.9	13.6	89	59	87	78	1.8	10.7	2.2	4.9	4.8	4.2	2.7	3.9
X	–	–	–	–	16.8	6.7	21.6	5,6	2.1	10,22	8.2	15.6	10.8	11.4	9.9	11.3	11.0	10.7	91	65	85	80	1.1	6.7	2.1	3.3	6.1	5.3	3.6	5.0
XI	–	–	–	–	7.4	1.8	14.1	3	-3.4	21	3.4	6.1	4.0	4.4	7.5	7.8	7.6	7.6	94	80	85	86	0.5	2.0	0.7	1.1	8.2	7.0	6.4	7.2
XII	–	–	–	–	0.3	-6.7	16.6	5	-22.1	25	-3.6	-1.3	-3.7	-3.1	5.0	5.1	4.8	5.0	92	82	89	88	0.5	1.3	0.6	0.8	7.4	6.8	6.7	7.0
Rok	–	–	–	–	13.4	4.5	31.6	3.VII	-22.1	25.XII	7.0	12.0	8.2	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.1	5.0	5.8

Miechów

$H_s = 292\ m$ $h_w = 16{,}5\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °/0, °/00																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr				Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min < -10°	Max < 0°	Min < 0°	Max > 25°	≥ 10	≥ 15	●	●	≥ 0.1	≥ 1.0	≥ 10.0	≡	▦	ZR
I	2	5.0	5.5	3.6	7.5	2.6	9.5	2.5	5.5	2.8	9	3.6	11	3.6	12	3.5	3.4	2.2	19.2	6.5	4	13	16	29	·	1	·	4	13	11	5	·	7	22	·
II	1	5.0	·	·	3.5	2.7	12	2.8	10	2.6	5.5	3.7	19.5	3.8	13.5	4.0	4.9	2.6	18.9	5.2	9	·	·	16	·	·	·	·	17	12	7	·	5	1	
III	2.5	7.0	·	·	·	·	·	·	0.5	2.0	9.5	6.0	49.5	5.6	28	6.1	3	5.6	26.8	5.2	14	·	·	8	·	8	·	2	13	16	7	·	1	2	1
IV	3	2.3	5	3.8	22.5	4.7	12	4.5	4	2.9	7.5	4.5	12	4.5	7	4.7	17	3.5	30.6	12.9	1	·	·	2	·	3	·	7	2	9	6	1	·	·	2
V	9	4.0	5.5	2.4	8	3.2	5	2.6	2.5	2.6	6	3.3	15.5	3.2	19.5	4.3	22	2.7	77.5	22.7	28	·	·	·	·	·	·	·	13	15	9	2	2	·	6
VI	5.5	2.2	0.5	1.0	1.3	2.5	1.1	2.2	5	2.9	3	3.0	14	4.4	17	4.1	21	2.5	73.6	20.0	12	·	·	·	7	·	·	5	4	15	12	2	1	·	8
VII	1.5	5.0	·	·	1	3.0	2.5	3.0	4.5	2.8	10	3.8	26.5	4.1	19	4.1	28	2.7	78.5	16.7	30	·	·	·	7	3	·	3	12	16	12	3	·	·	4
VIII	2.5	5.4	1.5	2.7	5	2.4	2.5	2.6	3	3.2	13.5	4.4	23.5	4.0	17.5	3.6	24	2.8	64.4	19.2	12	·	·	·	7	3	·	5	6	11	8	4	·	·	3
IX	2.5	3.0	1	3.0	11.5	2.5	10.5	2.4	2	2.5	6.5	4.2	18	4.6	9	3.8	29	2.4	20.3	8.0	29	·	·	·	8	·	·	10	5	7	5	·	4	·	4
X	1	3.0	0.5	4.0	20.5	4.0	25.5	3.6	3.5	4.6	3.5	3.4	6.5	4.5	10	3.6	22	2.9	20	1.3	17	·	·	2	·	·	·	5	6	3	1	·	4	·	·
XI	8.5	3.9	1.5	3.0	10.5	3.8	6.5	3.7	3	2.2	7.5	3.6	20.5	4.4	11	4.5	21	3.0	68.3	16.5	13	·	·	14	·	·	·	2	15	18	11	3	6	3	·
XII	12.5	5.6	5	3.2	8	2.6	5	2.0	3	3.3	8.5	5.5	11	6.0	18	4.4	22	3.4	33.8	14.5	6	16	18	26	·	1	·	2	11	17	4	1	4	24	·
Rok	51.5	4.3	26	2.2	111	2.8	102	2.7	46.5	2.9	90	4.1	227.5	4.4	181.5	4.2	259	3.0	513.9	22.7	28.V	29	34	97	29	19	·	45	117	150	87	16	34	52	28

Tarnogród

$H_s = 217\ m$ $h_w = 15{,}9\ m$

I	3	2.0	2	1.5	·	·	3	1.0	21	1.5	19	2.2	13	2.0	3	2.3	29	1.3	16.4	4.1	31	13	14	30	·	·	·	–	–	10	5	·	9	22	·
II	·	·	·	·	1	1.0	4	1.2	19	1.5	11	2.4	17	1.4	4	1.0	28	1.0	18.4	4.7	10	·	·	16	·	·	·	–	–	12	6	·	16	1	·
III	·	·	·	·	·	·	·	·	·	·	14	3.9	56	3.0	9	3.4	14	2.7	26.9	6.5	29	·	·	8	·	·	·	–	–	12	8	·	10	·	·
IV	4	2.2	2	4.0	16	1.8	8	2.4	5	2.4	6	2.7	10	3.9	·	·	39	1.5	22.5	7.8	18	·	·	4	·	·	·	–	–	8	5	·	·	·	2
V	6	2.2	1	4.0	3	1.3	3	1.3	7	2.0	5	1.4	19	1.8	5	2.2	44	1.0	81.6	28.2	14	·	·	·	1	·	·	–	–	13	12	2	6	·	6
VI	1	1.0	2	1.5	3	1.3	3	1.3	5	1.2	6	1.2	19	1.6	3	1.3	48	0.7	103.3	37.0	4	·	·	·	11	·	·	–	–	13	10	3	3	·	4
VII	·	·	·	·	·	·	·	·	12	1.8	6	1.3	28	2.0	8	1.9	39	1.1	101.3	35.5	29	·	·	·	7	·	·	–	–	15	13	3	·	·	4
VIII	3	1.3	·	·	·	·	1	1.0	3	1.7	12	1.7	24	1.8	9	1.8	41	1.0	127.7	61.4	9	·	·	·	6	·	·	–	–	13	12	4	·	·	5
IX	1	1.0	1	1.0	2	1.5	1	1.0	3	1.7	8	1.5	22	1.9	2	2.5	50	0.8	15.6	7.1	4	·	·	1	6	·	·	–	–	6	3	·	4	·	1
X	1	1.0	2	2.0	10	1.8	16	2.1	14	1.8	2	1.5	9	1.9	2	2.0	37	1.1	9.0	3.2	30	·	·	·	·	·	·	–	–	4	4	·	7	·	·
XI	2	4.0	·	·	7	1.9	8	2.1	10	1.4	7	2.3	23	1.8	5	2.0	28	1.3	31.5	12.6	13	·	1	9	·	·	·	–	–	16	5	1	7	·	·
XII	1.5	2.6	3	1.3	2	3.0	5	1.2	7	2.1	16	4.0	16	1.9	6	2.5	23	1.9	37.8	14.6	11	11	15	25	·	·	·	–	–	13	6	1	6	15	·
Rok	36	1.4	13	1.3	44	1.1	52	1.2	106	1.6	112	2.2	256	2.1	56	1.9	420	1.3	592.0	61.4	9.VIII	24	30	90	31	·	·	–	–	135	89	14	68	38	22

Lądek - Zdrój

$H_s = 460\ m$ $h_w = 13{,}5\ m$

I	1.5	1.3	1.1	1.5	7	1.4	7.5	2.9	23.5	3.2	17.5	3.3	3	1.0	1	1.0	21	2.0	10.5	3.7	31	10	13	27	·	5	3	6	18	10	2	·	2	20	
II	0.5	1.0	·	·	0.5	1.0	8	2.1	19.5	2.1	23.5	1.6	5	1.6	3	1.3	24	1.3	34.2	9.5	9	1	2	19	·	·	·	4	18	15	9	·	2	8	·
III	2.5	1.0	3	1.0	4	1.0	·	·	13.5	2.2	31	2.3	15	2.9	3	1.8	21	1.7	49.1	6.7	14	·	·	16	·	1	·	3	19	17	13	·	·	6	
IV	3.5	1.3	17.5	1.3	7	1.1	11	2.0	12.5	2.7	11.5	2.5	4	1.5	·	·	23	1.4	24.1	6.9	27	·	·	4	·	2	·	3	10	11	8	·	1	·	5
V	5	1.4	10.5	1.1	8.5	1.1	2	1.8	15	1.7	19.5	1.5	6.5	1.3	2	1.0	24	1.0	118.6	20.5	29	·	·	·	·	1	·	·	20	20	16	4	2	·	7
VI	1	2.0	9.5	1.0	9.5	1.0	3.5	1.7	13	1.7	12.5	2.2	3	1.8	·	·	38	0.9	122.8	36.1	8	·	·	·	3	·	·	4	11	15	12	4	2	·	8
VII	0.5	2.0	2	1.0	1	1.0	1	2.0	24	2.1	26.5	2.0	3	2.3	1	1.5	34	1.3	84.8	27.3	28	·	·	·	5	·	·	3	17	14	10	2	·	·	4
VIII	1	2.0	7	1.1	1	1.0	1	1.0	19	1.9	23	1.9	4.5	2.0	0.5	3.0	36	1.1	57.3	10.2	12	·	·	·	2	·	·	3	16	19	14	1	·	·	4
IX	3	1.2	8.5	1.2	4.5	1.2	9.5	1.2	19	1.6	14.5	1.5	2	1.5	·	·	29	1.0	27.0	9.5	14	·	·	·	9	·	·	8	7	9	5	·	1	·	1
X	2	1.0	6.5	1.2	7	1.7	9.5	2.6	23.5	3.2	8	2.4	1	2.0	2.5	1.4	33	1.6	78.4	25.8	18	·	·	·	·	1	·	4	15	9	7	2	4	·	
XI	5	2.1	5	1.0	6	1.2	1.5	2.0	21	2.4	17.5	2.3	3	1.3	3	2.5	28	1.4	69.7	20.0	5	·	·	14	·	·	·	2	21	20	7	2	1	5	·
XII	4.5	1.4	10.5	1.3	6	1.5	6.5	1.0	15.5	4.3	22.5	4.1	2.5	3.4	3	1.2	22	2.2	57.4	9.8	12	14	14	26	·	4	1	4	14	18	14	·	2	23	·
Rok	30	1.5	91	1.1	62	1.2	61	1.7	219	2.4	227.5	2.3	52.5	1.9	19	1.2	333	1.4	731.9	36.1	8.VI	25	29	106	19	14	4	44	186	177	117	15	17	62	29

Bytom

$H_s = 300\ m$ $h_w = 22\ m$

I	2	2.0	6.5	2.8	16.5	2.5	6	1.7	12	2.8	26	3.2	25	1.2	6.5	2.0	15	2.2	19.6	5.2	14	9	14	25	·	·	·	5	7	12	5	·	11	19	·
II	3	1.3	·	·	7.5	1.6	6.5	1.7	7.5	2.9	22.5	3.8	14.5	1.9	6.5	1.7	16	2.1	54.0	17.3	9	·	·	14	·	·	·	1	12	15	11	1	10	4	·
III	0.5	3.0	·	·	·	·	·	·	2.5	4.4	14	3.8	46.5	3.0	19.5	3.5	10	2.9	73.0	14.8	29	·	·	5	·	1	·	5	15	16	13	2	8	5	2
IV	7	1.6	3.5	3.3	2.5	3.2	6.5	2.6	5	2.1	13	3.0	4	1.9	8	2.4	18	2.2	22.8	9.0	1	·	·	·	1	1	1	11	2	7	6	·	·	·	3
V	8	1.9	9.5	2.5	2.5	2.6	1	2.0	3.5	2.9	10	3.2	12	3.6	17.5	2.8	2.9	2.0	64.2	15.3	29	·	·	·	·	3	·	1	10	14	14	1	2	·	8
VI	1.5	2.7	2	2.0	7	2.8	6	2.2	2.5	3.0	6	2.2	18.5	2.3	21.5	2.5	2.5	1.8	128.2	83.9	27	·	·	·	8	1	·	3	4	10	9	3	1	·	10
VII	3.5	1.1	·	·	0.5	4.0	0.5	4.0	1.5	2.3	18	3.3	25.5	2.6	13.5	2.5	3.0	1.9	153.2	42.0	13	·	·	·	7	1	·	2	9	16	13	5	·	·	6
VIII	2.5	3.0	1.5	3.0	2.5	1.8	0.5	1.0	4.5	4.0	14	3.4	22.5	2.4	12	3.0	3.3	1.9	46.7	18.6	12	·	·	·	7	·	·	8	3	10	9	1	·	·	4
IX	1.5	3.7	5.5	2.3	14.5	3.2	1.5	1.7	4	2.5	16	3.3	13.5	2.7	8.5	2.7	2.5	2.1	23.2	8.0	6	·	·	·	7	1	·	12	6	7	5	·	7	·	1
X	1.5	2.0	2.5	1.4	19.5	3.8	4.5	3.2	11	3.0	13.5	4.0	8	1.9	7.5	2.1	2.5	2.3	2.2	1.2	29	·	·	·	·	·	·	5	6	3	1	·	12	·	·
XI	6	1.9	2	2.5	8	2.6	4.5	2.0	3	4.2	27	3.0	10.5	2.0	13	2.1	19	2.0	77.3	26.3	13	·	·	8	·	·	·	2	15	14	12	2	8	2	·
XII	16	1.5	9.5	1.9	5.5	2.5	5.5	2.0	3	4.3	24.5	3.8	8	2.6	13	2.5	9	2.3	55.0	17.6	11	12	13	25	·	·	·	·	11	16	8	1	7	22	·
Rok	52	2.1	42.5	1.8	109	2.6	40	2.0	60	3.0	204.5	3.3	186	2.3	147	2.5	254	2.1	719.4	83.9	27.VI	21	27	77	30	8	1	55	99	140	106	16	66	52	34

Chorzelów

$\varphi = 50°21'$ $\lambda = 21°27'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnio I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.9	-9.4	8.1	4	-25.2	27	-6.7	-2.3	-4.9	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.8	5.4	5.9
II	–	–	–	–	4.0	-1.1	9.3	28	-5.3	5	0.1	3.2	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.8	6.5	7.5
III	–	–	–	–	9.8	1.8	20.6	18	-3.7	23	3.8	8.6	5.2	5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.3	5.8	7.0
IV	–	–	–	–	17.5	4.7	26.0	15	-3.9	10	7.8	16.6	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.2	3.8	4.6
V	–	–	–	–	17.5	6.6	28.0	26	1.4	19	10.3	16.0	11.0	12.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.2	5.8	6.5
VI	–	–	–	–	24.8	11.5	33.5	27	5.5	21	16.2	23.5	16.5	18.2	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.4	5.3	5.1
VII	–	–	–	–	23.0	11.1	31.5	4	6.4	8	15.5	21.5	15.6	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.7	6.1	6.1
VIII	–	–	–	–	23.6	12.2	34.5	11	6.0	31	14.9	22.0	16.2	17.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.8	4.9	5.3
IX	–	–	–	–	21.9	7.9	29.5	18	-2.0	23	10.1	21.0	13.4	14.5	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.8	3.5	4.3
X	–	–	–	–	17.2	5.4	23.5	19	-0.1	12,24	6.7	16.4	10.6	11.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.3	3.3	4.6
XI	–	–	–	–	7.8	1.9	14.3	3	-7.6	23	3.3	6.7	4.2	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	6.9	7.3
XII	–	–	–	–	-0.7	-8.4	14.4	5	-29.8	26	-4.9	-2.5	-4.8	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.8	5.7	6.7
Rok	–	–	–	–	13.8	3.7	34.5	11.VIII	-29.8	26.XII	6.4	12.6	7.8	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.3	5.2	5.9

Prudnik

$\varphi = 50°19'$ $\lambda = 17°34'$

I	–	–	–	–	1.5	-6.4	9.6	4	-20.5	27	-4.5	0.3	-2.8	-2.4	4.1	4.6	4.2	4.3	8.3	7.1	7.9	7.8	0.8	2.0	1.1	1.3	–	–	–	–
II	–	–	–	–	6.8	-0.8	13.1	27	-7.1	6	1.0	5.8	1.9	2.6	5.8	6.8	6.1	6.2	8.8	7.4	8.7	8.3	0.8	2.6	0.9	1.4	6.6	5.7	5.2	5.8
III	–	–	–	–	10.7	1.9	19.0	10	-2.6	20	3.9	9.5	5.0	5.8	6.6	7.3	7.0	7.0	8.2	6.3	8.0	7.5	1.6	5.0	2.0	2.9	6.9	6.3	6.0	6.4
IV	–	–	–	–	17.3	4.8	25.7	7	-2.0	10	9.5	16.1	10.0	11.4	9.0	9.0	9.0	9.0	7.4	5.0	7.4	6.6	3.1	9.9	3.7	5.6	3.6	5.7	4.4	4.6
V	–	–	–	–	16.2	6.1	22.6	26	1.8	15	10.6	14.7	9.8	11.2	10.3	9.8	10.5	10.2	8.1	6.0	8.7	7.6	2.7	7.4	1.7	3.9	6.8	7.4	7.3	7.2
VI	–	–	–	–	22.8	11.0	29.3	25	5.6	16	16.9	20.8	15.2	17.0	14.2	14.6	14.5	14.4	7.4	6.0	8.4	7.3	5.3	10.3	2.7	6.1	4.5	5.2	5.1	4.9
VII	–	–	–	–	21.5	11.0	31.4	3	6.0	11	15.6	19.8	14.2	16.0	14.4	13.4	13.4	13.7	8.0	5.9	8.2	7.4	3.7	10.5	3.1	5.8	6.2	6.6	6.9	6.6
VIII	–	–	–	–	22.0	11.7	30.6	6	7.0	17	15.6	20.6	14.9	16.5	14.9	15.7	14.3	15.0	8.3	6.5	8.3	7.7	3.1	9.1	3.1	5.1	6.5	6.2	4.7	5.8
IX	–	–	–	–	22.0	9.2	29.5	18	0.5	23	11.7	21.2	14.0	15.2	11.9	14.4	12.8	13.0	8.5	5.8	8.0	7.4	2.5	11.7	3.5	5.9	4.1	4.3	3.9	4.1
X	–	–	–	–	16.2	6.0	22.0	11	0.3	16	8.6	15.5	10.1	11.1	9.0	10.1	9.5	9.5	8.2	5.8	7.8	7.3	2.4	8.0	3.1	4.5	5.7	5.2	3.8	4.9
XI	–	–	–	–	7.3	1.0	14.3	1	-4.9	21	2.6	6.3	3.7	4.1	6.5	7.2	6.8	6.8	8.6	7.4	8.4	8.1	1.1	2.5	1.4	1.7	6.9	6.9	6.1	6.6
XII	–	–	–	–	1.3	-7.4	17.9	5	-25.8	26	-3.8	-0.5	-3.0	-2.6	4.4	4.8	4.4	4.5	8.0	7.3	7.7	7.7	1.2	2.1	1.4	1.6	7.2	5.5	6.3	6.3
Rok	–	–	–	–	13.8	4.0	34.4	3.VII	-25.8	26.XII	7.3	12.5	7.8	8.8	9.3	9.8	9.4	9.5	8.2	6.4	8.1	7.6	2.4	6.8	2.3	3.8	–	–	–	–

Sielec

$\varphi = 50°19'$ $\lambda = 20°25'$

I	–	–	–	–	-4.0	-10.2	7.7	4	-24.8	27	-7.1	-2.1	-5.9	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	5.9	5.4	6.5
II	–	–	–	–	4.6	-0.8	12.8	18	-4.9	5	0.5	3.9	1.4	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.1	7.9	8.3
III	–	–	–	–	10.3	2.2	20.2	18	-2.8	20	4.2	8.8	5.2	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.0	6.1	7.3
IV	–	–	–	–	17.5	3.8	26.5	15	-3.8	10	8.1	16.6	9.3	10.8	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.2	3.1	3.9
V	–	–	–	–	17.6	6.0	25.8	27	0.3	15	10.7	16.0	10.2	11.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	6.5	7.0
VI	–	–	–	–	24.6	10.6	33.5	27	4.2	17	16.0	23.1	15.3	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.6	5.6	5.2
VII	–	–	–	–	22.2	10.2	31.9	3	5.0	11	15.0	20.7	14.7	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.4	5.7	6.5
VIII	–	–	–	–	23.1	10.9	32.8	11	5.5	31	14.5	21.8	15.2	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.4	4.1	5.4
IX	–	–	–	–	21.7	7.0	30.2	2	-1.1	22	10.1	20.7	12.5	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.8	3.5	4.2
X	–	–	–	–	16.9	4.0	23.0	19	-1.5	25	7.0	16.2	8.5	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.8	3.9	5.5
XI	–	–	–	–	7.5	0.3	15.6	3	-7.0	24	2.2	6.3	2.8	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.1	7.3	7.8
XII	–	–	–	–	-0.8	-8.8	18.4	5	-26.2	25	-6.3	-3.0	-5.1	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	7.5	7.4
Rok	–	–	–	–	13.7	2.9	33.5	27.VI	-26.2	25.XII	6.2	12.4	7.0	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.5	5.6	6.3

Bystrzyca Kłodzka

$\varphi = 50°18'$ $\lambda = 16°39'$

I	–	–	–	–	-0.1	-6.2	8.0	31	-20.8	27	-4.9	-1.5	-3.5	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.2	7.2	6.9
II	–	–	–	–	4.6	-1.4	13.1	18	-12.8	6	0.3	3.4	1.2	1.5	–	–	–	–	–	–	–	–	–	–	–	–	9.3	7.4	6.8	7.8
III	–	–	–	–	10.2	0.8	18.9	10	-5.7	20	2.3	8.6	4.7	5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.7	6.0	6.8
IV	–	–	–	–	16.6	4.4	24.1	7	-3.5	10	7.9	15.1	9.6	10.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.3	4.6	5.0
V	–	–	–	–	14.9	5.4	22.7	26	-0.1	15	8.8	13.2	8.9	10.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.9	6.7	7.3
VI	–	–	–	–	22.1	10.2	28.7	25	2.6	16	15.0	20.3	15.0	16.3	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.7	5.4	5.3
VII	–	–	–	–	20.6	10.1	30.4	3	3.8	8	14.0	18.8	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.4	6.2	6.8
VIII	–	–	–	–	21.3	10.9	28.5	6	4.5	4	13.9	19.8	14.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.1	5.4	5.9
IX	–	–	–	–	21.8	8.9	28.8	18	-0.9	23	11.1	20.6	13.4	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.3	3.3	4.2
X	–	–	–	–	14.8	5.7	20.1	5,6,8	-0.7	16	7.1	13.6	9.1	9.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.3	4.1	5.5
XI	–	–	–	–	5.9	0.7	11.3	2,12	-6.3	21	2.2	4.6	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	7.3	7.8
XII	–	–	–	–	0.2	-7.1	16.0	5	-25.6	26	-3.9	-1.9	-3.7	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	5.6	6.1	6.9
Rok	–	–	–	–	12.7	3.5	30.4	3.VII	-25.6	26.XII	6.2	11.2	7.2	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	5.8	6.4

Chorzelów

$H_s = 170$ m $h_w = 16$ m **1961**

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R > 0.1	R > 1.0	R > 10.0	≡	⊠	⩘
I	5.5	1.4	6.5	1.6	1.5	1.0	4.5	5.2	29	2.0	7.5	4.1	9	1.8	4.5	2.6	25	1.5	49.2	6.5	14	13	14	29	·	1	·	5	12	10	6	·	3	23	·
II	1	4.0	1	4.0	5	1.2	6	1.2	20.5	2.2	5.5	1.2	20.5	1.1	3.5	1.0	21	1.1	30.4	9.6	9	·	1	17	·	·	·	2	16	12	5	·	7	8	·
III	1	1.0	·	·	1	1.0	·	·	4	2.2	15.5	2.3	41.5	3.5	17	5.0	13	3.0	27.6	5.6	18	·	·	9	·	4	·	·	12	15	8	·	6	1	1
IV	4	3.2	7	1.4	22	2.7	13	2.3	13	1.4	8	2.4	7	3.7	5	3.2	11	2.1	16.7	5.5	16	·	·	2	1	·	·	7	6	6	5	·	1	·	2
V	9	1.9	6	1.8	7	1.7	2.5	1.0	7.5	1.5	13.5	1.7	5.5	1.5	10	4.8	32	1.1	47.6	8.3	28	·	·	·	4	·	·	1	9	15	12	·	2	·	3
VI	2.5	1.2	4	1.2	7	1.6	8.5	1.2	3.5	2.1	6	1.0	7.5	1.8	16	1.7	35	0.9	79.7	19.5	27	·	·	·	16	·	·	4	4	12	11	3	2	·	6
VII	3.5	2.4	·	·	3	1.0	2	2.0	5.5	2.3	16	2.0	16	1.7	11	2.1	36	1.2	63.6	20.0	30	·	·	·	10	·	·	3	9	14	8	2	1	·	4
VIII	8.5	2.0	2	1.5	1	3.0	·	·	7	1.6	12	1.9	19	4.7	11.5	2.8	32	1.3	69.9	20.5	12	·	·	·	8	·	·	5	7	12	8	2	2	·	8
IX	3.5	1.1	5	1.5	5	1.6	5.5	1.4	5	1.2	9	1.4	18	2.1	7	1.3	32	1.0	16.0	9.7	6	·	·	3	10	·	·	11	6	5	4	·	8	·	2
X	3	1.7	2	2.0	22	2.5	14	2.0	14	2.9	6	4.5	1.5	1.7	6.5	1.6	24	1.7	18.4	13.3	30	·	·	2	·	·	·	10	6	4	3	1	5	·	·
XI	5	1.8	2	2.5	15	2.4	5	1.4	11	1.7	14	1.6	13	2.0	4	2.0	21	1.5	44.0	14.3	11	·	·	10	·	·	·	4	17	19	8	2	9	·	
XII	13	2.1	9	2.3	6	1.5	2	2.5	13	2.4	6	3.3	17	2.0	5	2.6	22	1.7	52.2	18.0	6	11	16	25	·	·	·	2	11	18	7	2	3	18	
Rok	59.5	1.7	44.5	1.4	95.5	1.8	63	1.7	133	2.0	119	1.8	175.5	2.0	101	2.3	304	1.5	485.3	20.5	12.VIII	24	31	97	49	5	·	54	115	142	85	12	49	50	26

Prudnik

$H_s = 265$ m $h_w =$ 15,5 m I–IX; 14 m X–XII

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	⩘
I	2	1.2	6	2.1	7.5	1.7	6	2.3	20.5	9.0	7.5	4.1	9.5	4.6	3	3.5	31	3.4	5.8	3.6	14	10	11	28	·	5	3	–	–	8	1	·	2	17	:
II	·	·	2	2.0	5.5	2.9	7.5	3.1	11.5	3.0	2.5	3.8	16	5.0	12	5.3	27	2.8	38.0	11.3	9	·	·	17	·	2	1	8	11	15	9	1	4	2	
III	·	·	·	·	·	·	·	·	4	2.2	11	5.9	48.5	6.4	22.5	6.8	7	5.8	47.6	10.4	14	·	·	8	·	13	4	4	12	18	11	1	·	2	1
IV	10	2.3	9.5	2.8	6.5	3.8	7.5	3.4	15	6.6	7	6.0	7	3.7	13.5	3.1	14	3.4	14.5	5.9	1	·	·	1	1	5	2	7	4	7	3	·	·	·	3
V	8.5	3.5	1	2.0	1	3.0	1	1.0	5	5.3	9	3.1	25	4.0	22.5	3.6	20	2.9	72.2	15.8	29	·	·	·	·	4	4	1	13	19	12	2	2	·	9
VI	8	2.2	1	1.0	2	3.5	6.5	3.3	8	4.9	2.5	3.0	22	3.8	17	3.9	23	2.7	125.1	38.7	8	·	·	·	5	2	·	8	6	13	12	4	1	·	11
VII	4.5	1.7	·	·	2.5	2.6	0.5	5.0	5.5	3.7	13.5	4.5	29.5	3.9	14	3.5	23	2.8	98.4	25.8	15	·	·	·	6	2	·	6	14	15	10	3	·	·	6
VIII	4.5	3.0	1	1.0	2.5	3.8	1.5	2.3	7.5	3.9	16	3.6	19	4.1	15	3.6	29	2.5	58.6	14.9	12	·	·	·	6	1	·	4	8	13	12	1	1	·	5
IX	2	2.0	5	2.2	12.5	3.4	5.5	1.9	11	3.8	12	3.8	8	3.8	4	4.0	30	2.2	26.0	11.9	14	·	·	·	8	1	·	13	6	6	4	2	4	·	2
X	·	·	0.5	4.0	11.5	3.3	18	3.8	23	7.0	4	3.6	10.5	3.1	5.5	5.5	20	3.7	32.2	12.7	20	·	·	·	·	4	·	7	5	7	6	1	4	·	·
XI	2	2.8	6	4.8	3.5	2.3	9.5	2.5	15	3.5	8	3.1	13	4.7	15	3.0	18	2.8	73.8	19.6	4	·	·	8	·	·	·	4	13	19	10	2	5	1	·
XII	7.5	3.2	2	2.5	·	·	7.5	3.3	11.5	3.3	8	6.8	23	5.3	14.5	4.9	19	3.7	48.2	9.7	11	13	13	25	·	4	2	2	9	18	10	·	·	21	
Rok	46	1.8	34	1.8	55	2.5	71	2.7	137.5	4.7	101	4.3	231	4.4	158.5	4.2	261	3.2	640.4	38.7	8.VI	23	24	85	26	43	16	–	–	158	100	17	23	43	37

Sielec

$H_s = 202$ m $h_w = 16{,}7$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	⩘
I	1	2.0	3	2.7	4	1.5	3	5.0	1	2.0	3.5	4.9	12.5	3.6	2	4.2	63	1.0	22.6	7.2	4	14	15	29	·	1	·	4	15	9	6	·	12	20	·
II	·	·	2.5	2.8	3	2.8	2.5	4.6	0.5	1.0	2.5	1.4	12.5	2.5	6.5	3.8	54	1.0	24.1	6.5	9	·	·	15	·	·	·	1	19	10	6	·	14	·	
III	0.5	1.0	·	·	·	·	·	·	·	·	13.5	4.9	46	5.7	7	5.4	26	3.9	14.5	5.2	18	·	·	8	·	5	1	1	15	12	6	·	3	·	1
IV	2	1.5	6	2.7	24	5.5	3	1.5	·	·	11	3.3	7.5	3.1	0.5	6.0	36	2.4	11.0	3.9	1	·	·	3	2	2	·	11	4	5	4	·	1	·	1
V	2	1.5	4	2.2	5.5	3.1	0.5	2.0	2.5	2.6	7	3.1	17	2.5	5.5	1.5	49	1.2	48.1	13.5	6	·	·	·	1	1	·	1	12	16	9	1	6	·	4
VI	1	1.0	1	3.0	10.5	3.8	2.5	3.4	2	3.5	6	2.8	5	4.8	5	4.0	57	1.3	99.6	47.8	27	·	·	·	12	3	·	7	7	13	10	4	4	·	9
VII	·	·	1	1.0	4	3.5	·	·	2	4.5	6	2.6	23.5	3.0	2.5	2.4	54	1.2	76.3	18.0	28	·	·	·	8	2	·	3	10	12	9	4	1	·	3
VIII	0.5	1.0	1.5	2.3	3	2.7	·	·	1	1.0	7	3.1	20.5	3.3	3.5	2.3	56	1.2	63.7	28.4	10	·	·	·	8	·	·	5	8	8	6	2	·	·	1
IX	·	·	·	·	12	3.2	·	·	·	·	9.5	3.9	11.5	4.1	3	1.5	54	1.4	9.7	3.9	29	·	·	2	7	·	·	12	6	6	4	·	7	·	2
X	·	·	·	·	26.5	5.6	11.5	6.2	2	1.0	4.5	3.7	6	2.8	4.5	2.4	38	2.9	2.3	2.0	14	·	·	5	·	6	·	8	9	2	1	·	10	·	·
XI	1	1.0	0.5	5.0	9.5	4.3	1	1.0	1	1.0	10.5	3.6	12	3.5	2.5	4.8	52	1.5	85.2	25.0	11	·	·	13	·	1	·	1	18	14	12	3	15	1	·
XII	1	2.0	4.5	4.7	4.5	2.0	0.5	1.0	1	1.0	8.5	5.1	6	5.3	6	4.4	61	1.5	59.5	22.5	6	15	19	26	·	3	·	4	18	14	8	2	11	23	·
Rok	9	0.9	24	2.2	106.5	3.2	24.5	2.1	13	1.5	89.5	3.5	180	3.7	48.5	3.3	600	1.7	516.6	47.8	27.VI	29	34	101	38	24	1	58	141	121	81	16	84	44	21

Bystrzyca Kłodzka

$H_s = 370$ m $h_w = 12{,}3$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◉	●	R > 0.1	R > 1.0	R > 10.0	≡	⊠	⩘
I	12	3.3	1	2.0	·	·	2.5	3.4	40	6.2	3.5	5.6	·	·	6	3.6	28	3.7	33.7	17.8	31	9	14	23	·	5	1	6	18	14	5	1	1	20	:
II	3.5	4.6	·	·	·	·	4	4.2	34	5.8	7	3.9	5.5	5.4	3	5.0	27	3.6	17.3	4.2	4	2	2	19	·	5	2	1	18	13	6	·	5	5	·
III	6.5	1.8	1	5.0	·	·	3	2.5	9	3.7	12.5	6.7	20	6.8	9	3.6	32	3.3	31.1	6.7	21	·	·	16	·	8	3	2	13	17	9	·	6	4?	·
IV	8.5	3.2	4.5	3.2	1	2.0	3	5.7	28.5	5.8	5	4.0	2.5	6.2	5	2.8	32	3.0	34.0	8.0	3	·	·	4	·	4	1	6	6	10	8	·	5	·	2
V	17	2.9	2	2.0	2	2.0	3	3.7	13.5	3.4	6.5	3.7	8	5.2	6	2.4	35	2.1	73.3	10.1	29	·	·	1	·	·	·	·	10	19	14	1	5	·	6
VI	9.5	2.8	2	1.8	·	·	0.5	9.0	14	3.7	5.5	3.8	7	5.2	5.5	2.8	46	1.8	82.3	30.8	4	·	·	·	5	1	·	6	7	14	10	3	1	·	7
VII	2.5	2.2	1.5	1.7	·	·	3.5	2.4	18.5	3.0	20.5	3.8	11.5	3.2	1	3.0	34	2.0	64.1	26.3	28	·	·	·	5	1	·	3	14	13	9	2	2	·	1
VIII	3	4.0	3	2.0	1.5	2.0	5.5	4.3	18.5	3.9	15	4.4	4.5	4.2	7	4.1	35	2.5	67.4	12.5	6	·	·	·	5	1	·	4	8	15	12	1	3	·	4
IX	4	3.9	0.5	2.0	0.5	1.0	7	2.6	26	3.3	6.5	2.7	3.5	2.9	6	3.7	36	1.9	14.6	10.5	14	·	·	2	8	·	·	10	5	7	3	1	7	·	1
X	8	3.2	3.5	3.6	1	5.5	3.5	9.7	34	7.5	5	6.0	1	2.5	5	3.0	32	4.1	63.0	20.5	18	·	·	2	·	7	2	6	7	8	6	2	10	·	·
XI	13.5	3.0	2	3.3	·	·	4.5	3.8	24.5	4.1	6	3.8	3	2.7	3.5	2.7	33	2.3	47.4	12.1	4			10	·	·	·	3	19	14	9	1	5	1	·
XII	18.5	3.6	1.5	3.3	·	·	1.5	6.7	28.5	6.0	4.5	5.7	4	4.4	8.5	3.9	26	3.5	37.7	7.7	11	12	15	23	·	2	·	1	12	20	11	·	1	20	·
Rok	106.5	3.2	22.5	2.9	6	4.0	41.5	4.8	289	4.7	97.5	4.5	70.5	4.1	65.5	3.4	396	2.8	565.9	30.8	4.VI	23	31	100	23	34	9	48	137	164	102	12	51	50	21

Głuchołazy

$\varphi = 50°18'$ $\lambda = 17°23'$ **1961**

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
					— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.8	-5.8	8.9	31	-17.6	27	-3.7	-0.2	-2.9	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.3	5.4	5.1
II	–	–	–	–	-0.2	-3.2	12.9	27	-7.0	6	1.0	5.4	2.3	2.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.8	5.6	6.0
III	–	–	–	–	10.4	2.5	18.7	18	-2.1	28	4.4	9.1	5.3	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.0	6.3	6.6
IV	–	–	–	–	17.0	5.5	26.3	7	-1.0	1	10.0	16.1	9.7	11.4	–	–	–	–	–	–	–	–	–	–	–	–	3.9	5.6	4.9	4.8
V	–	–	–	–	15.0	6.4	21.6	6	2.1	15	10.4	13.8	9.6	10.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.6	6.7	7.2
VI	–	–	–	–	22.3	11.4	29.8	25	5.9	16	16.4	20.7	14.5	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.3	5.2	5.2
VII	–	–	–	–	21.2	11.4	31.2	3	7.0	8,11	15.4	19.6	14.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	6.2	6.4
VII	–	–	–	–	21.6	12.0	28.7	10	7.6	4	15.2	20.2	14.7	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.2	3.8	5.4
IX	–	–	–	–	22.2	10.5	30.3	2	1.5	23	13.8	21.1	13.8	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.4	3.6	4.4
X	–	–	–	–	16.3	6.3	24.2	9	0.2	16	8.6	15.0	10.1	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.6	4.2	5.3
XI	–	–	–	–	6.8	0.8	13.6	1	-5.0	21	2.8	5.6	3.2	3.7	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.2	5.8	6.6
XII	–	–	–	–	1.0	-6.5	18.6	5	-22.0	25	-3.4	-1.1	-3.0	-2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.0	5.9	6.4
Rok	–	–	–	–	13.4	4.5	31.2	3.VII	-22.0	25.XII	7.6	12.1	7.6	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.8	5.3	5.8

Gliwice

$\varphi = 50°18'$ $\lambda = 18°40'$

I	–	–	–	–	0.2	-6.1	10.0	4	-18.9	27	-4.5	-0.5	-3.2	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.1	6.8	5.8
II	–	–	–	–	5.0	-0.5	12.0	18	-6.3	6	0.6	4.1	1.6	2.0	5.7	6.6	6.2	6.2	8.9	8.1	8.9	8.6	0.7	1.7	0.8	1.1	7.7	6.6	5.4	6.6
III	–	–	–	–	9.8	2.4	19.0	10	-1.9	28	3.4	8.3	5.6	5.7	6.8	7.3	7.5	7.2	8.7	6.7	8.2	7.9	1.1	4.1	1.8	2.3	7.5	6.5	6.6	6.8
IV	–	–	–	–	17.7	5.9	25.0	7	-1.3	1	8.3	16.5	10.8	11.6	8.7	8.8	9.1	8.9	7.8	4.8	7.0	6.5	2.4	10.6	4.0	5.7	3.8	4.1	4.4	4.1
V	–	–	–	–	16.5	6.2	23.6	6	4.3	13	9.6	14.9	10.0	11.1	10.7	11.0	10.8	10.8	8.9	6.6	8.6	8.0	1.4	6.4	2.0	3.3	7.4	8.0	7.7	7.7
VI	–	–	–	–	23.1	11.5	30.4	27	5.5	16	15.7	21.2	16.3	17.4	15.0	14.4	15.2	14.9	8.4	5.9	8.2	7.5	3.1	11.1	3.6	5.9	4.0	5.9	5.7	5.2
VII	–	–	–	–	21.1	11.1	30.6	3	6.7	11	14.7	19.5	14.4	15.8	13.8	13.6	13.7	13.7	8.2	6.1	8.3	7.5	3.2	10.0	3.0	5.4	5.6	7.5	7.3	6.8
VIII	–	–	–	–	22.1	11.8	30.6	10	6.4	14	14.4	20.6	15.6	16.6	14.6	14.9	14.9	14.8	8.8	6.2	8.3	7.8	2.1	9.2	3.2	4.8	5.4	6.1	4.8	5.4
IX	–	–	–	–	21.8	9.8	28.7	2	3.1	22	12.3	20.9	14.0	15.3	12.3	12.8	13.0	12.7	8.5	5.3	8.1	7.3	2.3	12.6	3.2	6.0	4.8	4.1	3.2	4.0
X	–	–	–	–	16.2	6.9	21.6	8	1.9	10	8.0	15.7	10.2	11.0	9.6	10.5	10.4	10.2	9.0	6.0	8.3	7.8	1.2	7.4	2.2	3.6	6.0	5.4	5.2	5.5
XI	–	–	–	–	7.1	1.4	13.5	3	-4.1	23	3.0	6.2	3.6	4.1	7.1	7.7	7.2	7.3	9.1	8.0	8.9	8.7	0.7	2.1	0.9	1.2	8.1	7.7	6.7	7.5
XII	–	–	–	–	0.0	-7.3	15.5	5	-24.2	25	-4.2	-1.5	-4.2	-3.5	4.6	5.1	4.6	4.8	8.7	8.4	8.7	8.6	0.7	1.2	0.6	0.8	7.2	5.8	6.8	6.6
Rok	–	–	–	–	13.4	4.4	30.6	3.VII,10.VIII	-24.2	25.XII	6.8	12.2	7.9	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.1	5.9	6.0

Mielec

$\varphi = 50°18'$ $\lambda = 21°27'$

I	1000.1	1020.6	982.2	1022.0	-0.6	-8.6	8.6	4	-25.0	27	-6.2	-2.1	-4.4	-4.3	3.9	4.3	4.3	4.2	8.8	2.8	8.7	8.4	0.5	1.2	0.6	0.8	6.8	6.4	5.4	6.2
II	1002.3	1016.8	973.4	1023.6	4.2	-0.9	9.3	28	-4.9	26	0.3	3.2	1.3	1.5	5.6	6.1	5.9	5.9	9.0	8.0	8.6	8.5	0.6	1.6	0.9	1.0	8.2	7.9	7.1	7.7
III	997.7	1015.2	976.7	1018.7	9.8	2.2	20.4	18	-2.4	23	4.0	8.2	5.3	5.7	7.0	7.1	7.2	7.1	8.5	6.6	8.0	7.7	1.3	4.2	1.9	2.5	8.4	8.3	5.5	7.4
IV	992.8	1002.1	984.2	1013.3	17.7	4.8	26.1	15	-4.3	10	7.9	16.2	10.4	11.2	8.3	8.6	9.1	8.7	7.6	4.7	7.1	6.5	2.7	10.6	3.9	5.7	5.5	6.0	4.6	5.4
V	992.0	999.5	977.2	1012.5	17.3	6.9	26.5	29	1.0	19	10.2	15.5	11.6	12.2	10.3	10.1	10.8	10.4	8.2	5.8	7.9	7.3	2.4	8.2	3.2	4.6	6.6	8.1	6.7	7.1
VI	995.4	1008.3	985.5	1015.4	25.0	11.6	34.7	27	5.9	21	16.3	23.1	17.4	18.6	14.9	13.2	15.0	14.4	8.0	4.8	7.6	6.8	3.9	15.7	5.0	8.2	5.1	6.1	6.6	5.9
VII	994.3	1005.4	980.7	1014.3	23.1	11.4	31.5	4	7.0	8	15.2	21.1	16.3	17.2	13.6	12.2	14.0	13.3	7.9	5.1	7.6	6.9	3.8	13.6	4.8	7.4	5.8	7.2	7.1	6.7
VIII	996.8	1009.0	987.1	1016.9	23.6	12.6	34.8	11	6.2	31	15.0	21.9	17.0	17.7	14.2	13.6	15.3	14.4	8.2	5.2	7.8	7.1	3.2	13.5	4.5	7.1	5.8	6.2	5.5	5.8
IX	999.5	1010.4	988.0	1019.9	21.9	8.4	29.3	18	-1.3	23	10.4	20.7	14.4	15.0	11.3	11.8	12.2	11.8	8.8	4.9	7.4	7.0	1.8	13.2	4.7	6.6	4.8	5.1	4.2	4.7
X	999.6	1011.3	977.0	1020.2	17.0	6.2	24.4	19	0.6	12	7.7	16.2	11.1	11.5	8.8	9.5	9.4	9.2	8.4	5.3	7.2	7.0	2.0	9.3	4.0	5.1	5.8	5.7	3.5	5.0
XI	994.3	1015.8	982.0	1015.4	7.8	2.1	14.6	3	-8.1	23	3.6	6.7	4.7	4.9	7.5	8.0	7.7	7.7	9.1	8.0	8.7	8.6	0.8	2.1	1.1	1.3	8.1	8.2	7.4	7.9
XII	995.3	1021.8	976.5	1017.1	-0.4	-8.1	15.0	2	-29.2	26	-4.4	-2.2	-4.2	-3.8	4.8	4.7	4.5	4.6	8.6	7.9	8.5	8.3	0.8	1.5	0.9	1.1	7.4	7.3	6.6	7.1
Rok	996.7	1021.8	973.4	1017.5	13.9	4.0	34.8	11.VIII	-29.2	26.XII	6.7	12.4	8.4	9.0	9.1	9.1	9.6	9.3	8.4	6.2	7.9	7.5	2.0	7.9	3.0	4.3	6.5	6.9	5.8	6.4

Olkusz

$\varphi = 50°17'$ $\lambda = 19°34'$

I	–	–	–	–	-0.3	-8.1	8.9	4	-24.2	18	-6.0	-1.4	-4.4	-4.0	3.7	4.2	4.1	4.0	8.5	7.4	8.4	8.1	0.6	1.6	0.8	1.0	–	–	–	–
II	–	–	–	–	4.3	-1.0	13.4	18	-7.8	6	0.0	3.6	1.1	1.4	5.5	6.1	5.9	5.8	8.9	7.7	8.7	8.4	0.7	2.0	0.9	1.2	–	–	–	–
III	–	–	–	–	8.9	2.2	18.8	10	-3.4	20	3.3	7.3	4.9	5.1	6.5	6.8	7.1	6.8	8.4	6.8	8.1	7.8	1.3	3.8	1.8	2.3	–	–	–	–
IV	–	–	–	–	16.9	4.7	24.7	15	-2.8	10	9.2	15.6	9.8	11.1	9.2	10.1	9.0	9.4	7.9	5.8	7.5	7.1	2.8	8.3	3.5	4.9	–	–	–	–
V	–	–	–	–	16.6	5.8	24.7	27	1.8	12	9.9	15.0	10.2	11.3	10.3	11.0	10.4	10.6	8.4	6.3	8.3	7.7	2.1	6.7	2.3	3.7	–	–	–	–
VI	–	–	–	–	23.4	11.3	32.2	27	5.0	16	16.1	21.9	15.9	17.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.0	11.0	30.2	3	4.6	8	14.7	19.0	14.8	15.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	21.7	11.2	30.7	11	5.7	14	14.6	20.0	15.2	16.2	14.1	14.4	14.6	14.4	8.4	6.4	8.3	7.7	2.8	9.8	3.1	5.2	–	–	–	–
IX	–	–	–	–	20.9	8.8	30.0	17	2.1	24	11.8	20.0	13.0	14.4	12.0	13.5	12.4	12.6	8.6	5.9	8.2	7.6	2.1	10.6	2.8	5.2	–	–	–	–
X	–	–	–	–	16.5	5.9	20.2	6,11,28	1.1	25	7.8	15.5	10.0	10.8	9.4	10.3	10.1	9.9	8.9	6.0	8.2	7.7	4.3	7.5	2.3	3.7	–	–	–	–
XI	–	–	–	–	7.3	0.9	14.8	3	-7.1	23	2.7	6.2	3.2	3.8	7.0	7.7	7.2	7.3	9.2	8.1	9.2	8.8	0.2	2.1	0.7	1.2	–	–	–	–
XII	–	–	–	–	-0.3	-7.6	17.8	5	-25.6	26	-4.6	-2.0	-4.6	-4.0	4.6	5.1	4.6	4.8	8.8	8.5	9.0	8.8	0.6	1.1	0.5	0.7	–	–	–	–
Rok	–	–	–	–	13.1	3.7	32.2	27.VI	-25.6	26.XII	6.6	11.7	7.4	8.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Głuchołazy $H_s = 344\ m$ $h_w = 10\ m$ 1961

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	◑	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	1.5	2.0	8	1.5	6.5	1.5	9	2.1	13.5	3.9	13.5	2.4	9.5	1.6	3.5	2.1	28	1.6	6.5	3.3	14	8	13	27	·	1	1	8	8	9	1	·	3	20	·
II	2	2.2	2.5	1.4	1	1.0	2	3.0	14.5	1.9	20.5	2.1	12	1.8	14.5	2.6	15	1.7	40.8	8.4	9	·	·	26	·	1	·	7	12	12	10	·	4	5	·
III	3.5	3.0	1	1.0	·	·	·	·	2.5	3.0	20	3.3	33	1.9	25	3.2	8	2.5	55.2	8.0	14	·	·	5	·	1	·	3	13	19	13	·	2	5	·
IV	1	1.0	6	3.4	5.5	1.8	4.5	3.0	8	3.6	21.5	1.7	11.5	1.3	11	2.6	21	1.7	13.9	4.4	1	·	·	2	1	·	·	8	4	9	5	·	·	·	5
V	4	2.9	1	2.0	3	2.0	·	·	5.5	1.8	17	2.1	32	1.8	19.5	2.3	11	1.8	110.2	24.3	29	·	·	·	·	·	·	2	11	19	16	4	4	·	5
VI	1.5	3.0	3	1.0	1	2.0	3.5	1.7	9	2.1	21.5	1.5	26	1.8	8.5	2.9	16	1.5	163.4	44.0	8	·	·	·	6	·	·	6	7	14	11	5	·	·	10
VII	·	·	1	2.0	1	2.0	4.5	2.4	6.5	1.9	31	1.7	27	2.0	6	2.0	16	1.6	90.9	23.3	28	·	·	·	7	·	·	3	8	14	11	3	·	·	3
VIII	2.5	3.4	1	1.0	1	2.0	2	3.0	14	1.9	32.5	2.1	20.5	1.8	7.5	2.5	12	1.8	54.9	16.4	12	·	·	·	5	·	·	3	6	17	11	2	2	·	6
IX	4.5	1.0	4.5	2.4	3.5	2.9	7	1.1	8.5	2.1	27	1.8	14.5	1.5	5.5	2.5	18	1.5	18.4	7.8	14	·	·	·	9	·	·	10	8	8	4	·	1	·	2
X	2	3.0	4	2.9	4	3.4	9.5	3.9	22	3.2	13.5	2.7	16	1.7	3	2.7	19	2.3	56.5	25.3	20	·	·	·	·	·	·	7	7	12	6	2	4	·	·
XI	3	1.7	2	1.5	3	2.3	7.5	1.9	18	1.7	15	2.4	19	2.2	11.5	2.2	11	1.8	65.9	16.4	4	·	·	9	·	·	·	5	12	17	10	3	10	2	·
XII	4.5	2.6	4	1.8	·	·	3	1.0	9.5	1.9	16.5	2.9	15.5	1.6	16	2.6	24	1.7	62.5	10.0	11	10	13	25	·	·	·	3	11	18	11	1	7	23	·
Rok	27	2.2	38	1.8	29.5	1.7	52.5	1.9	131.5	2.4	249.5	2.2	236.5	1.8	131.5	2.5	199	1.8	739.1	44.0	8.VI	18	26	94	28	3	1	65	107	168	109	20	37	55	31

Gliwice $H_s = 220\ m$ $h_w = 13\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	◑	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	4	1.0	14.5	1.6	2.5	1.0	16	1.2	23.5	1.9	18	4.7	5	2.3	9.5	2.4	·	2.3	14.6	4.6	31	10	15	27	·	·	·	7	11	12	4	·	1	19	:
II	2.5	2.2	·	·	5	1.4	7.5	1.7	16.5	2.0	27	3.4	12.5	2.3	13	2.7	·	2.5	50.9	15.4	9	·	·	17	·	·	·	4	13	14	10	2	7	5	·
III	7.5	2.8	·	·	·	·	·	·	2.5	1.0	21.5	3.2	24.5	3.2	37	3.8	·	3.4	58.7	11.4	18	·	·	6	·	1	·	5	17	17	12	2	1	4	2
IV	9.5	1.9	14.5	1.9	15	2.6	7.5	1.9	7	1.9	24.5	2.3	6	1.8	4	2.0	2	2.1	12.0	5.8	1	·	·	2	·	·	·	9	6	4	2	·	·	·	2
V	22	2.2	12.5	1.6	2.5	1.6	3	1.2	4	1.4	13.5	2.6	14.5	2.8	16	2.2	5	2.1	50.8	11.3	29	·	·	·	·	1	·	1	19	14	11	1	1	·	6
VI	16.5	2.3	13	1.8	13	1.2	10.5	1.5	6	2.2	11	2.4	7	3.7	11	3.7	2	2.2	92.4	30.0	27	·	·	·	7	·	·	5	7	15	10	2	·	·	8
VII	15.5	1.3	4	1.5	3	1.0	6.5	1.5	9.5	2.4	20.5	2.3	17	2.1	16	2.4	1	2.0	115.4	32.8	15	·	·	·	7	1	·	5	15	16	11	3	·	·	4
VIII	13	1.9	5	1.4	5	1.0	9	1.1	6.5	1.5	25	2.8	9.5	2.6	17	2.0	3	2.0	47.9	14.4	12	·	·	·	7	·	·	4	5	14	9	1	·	·	3
IX	3.5	1.9	1.5	2.0	16.5	1.6	11	1.5	11.5	1.9	22.5	2.5	11	2.8	11.5	2.5	1	2.1	18.1	5.5	14	·	·	·	7	·	·	11	6	8	6	·	2	·	2
X	8.5	2.2	0.5	1.0	19.5	2.2	17	1.9	13.5	2.6	16.5	2.8	5.5	2.5	8	3.1	4	2.3	4.2	1.7	17	·	·	·	·	·	·	7	8	5	2	·	1	·	·
XI	15.5	1.8	4.5	1.8	7	1.6	8	1.2	16.5	1.8	26	2.8	3.5	3.7	4	2.6	5	2.0	67.8	30.4	4	·	·	5	·	·	·	2	16	12	9	2	2	2	·
XII	24.5	1.8	7.5	1.9	1.5	1.0	14.5	1.2	7.5	2.7	21	3.3	4	1.9	10.5	3.4	2	2.3	58.9	15.5	11	12	15	25	·	·	·	4	18	14	10	1	1	21	·
Rok	142.5	1.9	77.5	1.4	90.5	1.4	110.5	1.3	124.5	1.9	247	2.9	120	2.6	157.5	2.7	25	2.3	591.7	32.8	15.VII	22	30	82	28	3	·	64	141	145	96	14	16	51	27

Mielec $H_s = 168\ m$ $H_b = 170{,}2\ m$ $h_w = 24\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	◑	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	6	2.8	5	2.0	3	1.5	18	4.4	18	4.8	9.5	2.6	16	2.8	0.5	1.0	17	2.9	16.9	4.9	5	12	15	29	·	3	·	5	12	9	6	·	3	22	·
II	0.5	1.0	4	2.5	6	2.9	13.5	2.9	20	3.8	8.5	2.9	19	3.0	1.5	2.7	11	2.7	26.0	7.9	9	·	·	15	·	1	·	1	17	11	6	·	5	4	·
III		·		·	·	·	1.5	4.0	3.5	6.1	17	4.3	55.5	5.8	9.5	5.7	6	5.1	26.3	4.9	18	·	·	9	·	6	1	1	15	12	8	·	2	·	·
IV	3	4.2	9	2.6	23.5	5.7	14.5	3.8	12	4.0	6.5	4.8	9	5.8	3.5	1.9	9	4.0	14.6	4.8	16	·	·	2	1	5	2	5	8	6	6	·	1	·	2
V	6.5	3.2	4	2.8	7.5	2.7	4	2.2	7.5	3.0	5.5	2.9	22.5	3.4	8.5	2.6	27	2.1	40.6	7.4	14	·	·	·	2	3	1	·	12	14	11	·	6	·	6
VI	0.5	2.0	6.5	2.8	10.5	3.9	13.5	1.9	8.5	2.6	6.5	2.9	18	3.0	6	4.5	20	2.3	73.2	16.0	27	·	·	·	16	1	·	2	9	12	10	3	3	·	10
VII	4	2.9			1	1.0	9.5	3.5	11.5	3.1	16	3.6	31.5	3.5	5.5	3.5	14	2.9	70.4	31.9	30	·	·	·	9	1	·	1	6	12	8	2	·	·	5
VIII	3.5	3.1	8	2.1	2	1.5	8.5	2.5	11.5	2.6	11.5	4.6	23	4.5	8	3.9	17	2.9	71.1	49.7	12	·	·	·	10	1	·	2	8	8	7	4	1	·	6
IX	1.5	2.7	6.5	3.0	12.5	3.2	9	2.1	9.5	2.4	11	2.8	17.5	4.9	0.5	5.0	22	2.5	24.8	15.3	4	·	·	2	7	2	·	9	8	4	4	1	6	·	2
X	4.5	3.0	2.5	4.0	28.5	5.4	19.5	5.4	8.5	6.1	3.5	2.6	8.5	3.1	2.5	4.6	15	4.1	17.7	12.7	30	·	·	·	·	6	·	8	6	4	3	1	5	·	·
XI	4	2.4	2.5	2.8	14	5.5	13.5	4.0	12.5	3.4	14	3.5	14.5	4.4	6	3.4	9	3.6	45.9	13.9	11	·	·	10	·	1	·	1	17	14	8	2	6	·	·
XII	10.5	4.2	11	3.0	2.5	1.8	10.5	3.4	13.5	5.6	9	4.8	12.5	4.0	8.5	4.3	15	3.5	51.2	19.3	6	13	15	24	·	3	·	3	16	14	9	1	4	24	·
Rok	44.5	2.6	59	2.3	111	2.9	136.5	3.3	136.5	4.0	118.5	3.5	247.5	4.0	60.5	3.6	182	3.2	478.7	31.9	30.VII	25	30	91	45	33	4	38	134	120	86	14	42	50	31

Olkusz $H_s = 360\ m$ $h_w = 16{,}5\ m$

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Opad R Max	Opad R Data	T Min<-10°	T Max<0°	T Min<0°	T Max>25°	Wiatr v>10	Wiatr v>15	◑	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	1	2.0	3	1.7	25	2.6	9	1.6	8	3.1	14	2.5	20.5	2.5	3.5	2.9	9	2.2	31.8	12.0	4	13	15	27	·	·	·	–	–	13	8	1	2	24	–
II	·	·	·	·	3.5	1.7	7.5	1.6	11	1.6	6	2.0	31	3.2	8	2.8	17	2.0	39.9	12.4	9	·	1	18	·	1	·	–	–	14	10	1	4	7	–
III	·	·	1	1.0	1	5.0	·	·	2	6.5	22.5	4.6	45.5	4.9	15	4.3	6	4.4	50.2	7.2	28	·	·	7	·	7	·	–	–	14	12	·	2	3	–
IV	7	5.0	1	3.0	37.5	3.8	3.5	2.0	5	2.0	8	4.5	16	3.8	4	2.0	8	3.4	49.2	9.8	1	·	·	2	·	3	1	–	–	7	5	·	·	·	–
V	10.5	2.2	1	2.0	1	2.0	5	1.6	7.5	3.2	4.5	4.7	28.5	3.0	9	2.8	26	2.0	81.5	26.8	6	·	·	·	·	·	·	–	–	19	12	2	·	·	–
VI	4.5	2.7	1	1.0	11	2.6	6	2.0	1	5.0	6	3.7	15	3.7	9.5	2.3	36	1.8	54.8	23.0	27	·	·	·	6	·	·	–	–	13	8	2	·	·	–
VII	1.5	1.7	1	1.0	1	1.0	·	·	19	3.0	15	3.1	15	2.8	3.5	2.7	37	1.7	115.1	32.1	13	·	·	·	8	·	·	–	–	16	14	5	·	·	–
VIII	2.5	1.8	3.5	1.0	6	2.2	·	·	9.5	2.7	16.5	3.0	17	3.3	6	1.9	32	1.8	77.1	25.2	12	·	·	·	7	·	·	–	–	11	11	2	·	·	–
IX	1	2.0	·	·	17.5	3.0	1.5	2.0	3.5	2.6	11.5	2.4	12.5	3.2	3.5	6.1	39	1.7	41.7	4.8	14	·	·	·	7	2	·	–	–	10	4	·	3	·	–
X	0.5	1.0	1.5	2.3	25	3.5	15	2.7	2.5	1.8	11.5	2.2	4	2.5	8	3.0	25	2.1	4.7	1.4	19	·	·	·	·	·	·	–	–	5	3	·	·	·	–
XI	5	2.2	4.5	2.3	9	3.4	5	1.0	5	2.5	16	2.4	21	1.9	8.5	2.2	16	1.8	90.6	26.7	13	·	·	11	·	·	·	–	–	19	11	3	·	1	–
XII	10	3.2	2	2.6	8	2.1	1	2.5	8.5	4.6	9.5	4.2	18	3.4	10	3.0	25	2.5	60.6	19.5	11	13	17	25	·	1	·	–	–	16	7	2	2	24	–
Rok	43.5	2.0	19.5	1.5	145.5	2.7	53.5	1.4	83.5	3.2	141	3.3	244	3.2	88.5	3.0	278	2.3	637.2	32.1	13.VII	26	33	90	28	14	1	–	–	157	105	18	13	59	–

Borusowa

$\varphi = 50°17'$ $\lambda = 20°47'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.0	-9.1	6.4	31	-24.7	28	-6.6	-2.8	-4.8	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	4.2	-0.8	11.8	18	-5.0	5	-0.2	3.2	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.7	8.0	7.6
III	–	–	–	–	9.8	2.6	20.0	18	-2.9	20	3.9	8.3	5.2	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.4	8.8	8.2
IV	–	–	–	–	17.8	4.3	27.9	15	-2.4	10	6.8	15.6	10.2	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.2	7.0	24.8	27	0.6	13	9.7	15.3	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.2	7.6	6.3
VI	–	–	–	–	24.3	11.4	32.8	27	5.5	17	15.5	22.7	16.4	17.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	22.0	10.5	30.3	3	5.3	8	15.0	20.1	15.4	16.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.9	11.9	33.4	11	6.8	31	14.1	21.5	16.2	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	22.0	8.0	29.7	17	0.9	23,24	10.2	20.3	13.9	14.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	17.2	5.6	24.0	20	0.6	24	7.2	16.2	10.2	11.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.7	1.5	15.3	3	-6.2	24	2.7	6.3	3.7	4.1	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.3	7.9	7.6
XII	–	–	–	–	-0.7	-8.6	11.9	5	-27.8	26	-5.1	-2.9	-5.1	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.0	8.0	7.8
Rok	–	–	–	–	13.6	3.7	33.4	11.VIII	-27.8	26.XII	6.1	12.0	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Zakrzów

$\varphi = 50°16'$ $\lambda = 18°09'$

I	–	–	–	–	0.6	-5.8	10.7	4	-19.7	27	-4.4	-0.3	-3.0	-2.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.7	5.3	5.8
II	–	–	–	–	5.8	-0.5	11.9	18	-7.0	6	0.7	4.9	1.8	2.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	6.5	5.8	6.8
III	–	–	–	–	10.7	2.0	19.8	10	-2.4	20	3.5	9.6	5.4	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.1	6.8
IV	–	–	–	–	18.2	4.4	25.7	7	-2.9	10	8.3	17.0	10.4	11.5	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.1	4.1	4.5
V	–	–	–	–	16.9	6.3	23.6	26	1.7	14	10.6	15.4	10.2	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.0	7.2	7.3
VI	–	–	–	–	23.2	11.4	29.3	25	5.2	21	16.3	21.8	15.8	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.8	5.8	5.5
VII	–	–	–	–	21.3	11.1	30.9	3	5.8	8	15.2	19.9	14.7	16.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.5	6.8	7.2
VIII	–	–	–	–	22.1	11.3	29.9	10	6.7	14	15.1	21.0	15.2	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	4.5	5.9
IX	–	–	–	–	22.4	9.1	29.3	18	-0.4	23	12.3	21.1	13.5	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.1	3.1	4.1
X	–	–	–	–	16.7	5.8	21.8	5	0.7	16	9.6	16.0	10.1	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.6	4.1	5.5
XI	–	–	–	–	7.3	1.7	12.6	2	-3.9	21	3.1	6.4	3.9	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.3	6.7	7.8
XII	–	–	–	–	0.7	-6.8	15.9	5	-25.9	26	-4.1	-1.2	-3.0	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.0	7.2	7.4
Rok	–	–	–	–	13.8	4.2	30.9	3.VII	-25.9	26.XII	7.0	12.6	7.9	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.4	5.6	6.2

Leżajsk

$\varphi = 50°15'$ $\lambda = 22°26'$

I	–	–	–	–	-1.1	-8.9	8.4	4	-24.2	27	-6.5	-2.9	-5.2	-5.0	3.5	4.2	3.8	3.8	8.1	7.8	8.2	8.0	0.8	1.1	0.8	0.9	7.2	5.6	5.9	6.2
II	–	–	–	–	4.5	-0.7	10.8	18	-5.4	7	0.0	3.1	1.2	1.4	5.4	6.1	5.9	5.8	8.8	7.9	8.7	8.5	0.7	1.6	0.8	1.0	7.8	7.5	7.7	7.7
III	–	–	–	–	9.9	2.2	18.9	18	-2.9	23	3.8	7.7	5.4	5.6	7.0	7.0	7.2	7.1	8.6	6.7	8.1	7.8	1.2	3.9	2.0	2.4	8.0	8.3	6.1	7.5
IV	–	–	–	–	17.6	4.8	26.0	15	-3.1	10	7.7	15.8	10.6	11.2	8.4	9.0	8.6	8.7	7.8	5.0	6.6	6.5	2.4	9.7	4.5	5.5	4.9	4.9	3.3	4.4
V	–	–	–	–	17.4	7.1	25.7	29	1.6	17	9.9	15.5	11.3	12.0	10.6	10.7	10.8	10.7	8.6	6.2	7.9	7.6	1.7	7.5	3.0	4.1	7.8	8.2	5.6	7.2
VI	–	–	–	–	24.9	12.3	32.5	27	7.0	1	16.6	22.8	17.4	18.6	15.1	14.7	14.7	14.8	8.0	5.4	7.4	6.9	4.0	13.7	5.4	7.7	4.7	5.8	5.6	5.4
VII	–	–	–	–	23.4	11.4	32.5	4	7.6	15	15.3	21.4	16.4	17.3	13.9	13.0	13.8	13.6	7.9	5.3	7.4	6.9	3.8	12.8	5.3	7.3	5.2	6.9	6.2	6.4
VIII	–	–	–	–	23.5	12.6	33.9	11	7.4	15	15.0	21.6	17.1	17.7	14.7	14.4	15.2	14.8	8.5	5.6	7.7	7.3	2.6	12.3	4.7	6.5	5.3	5.9	5.4	5.5
IX	–	–	–	–	21.8	9.0	29.7	18	-0.2	23	10.6	20.3	14.5	15.0	11.6	11.4	12.3	11.8	8.9	4.8	7.3	7.0	1.6	13.1	4.7	6.5	4.7	4.7	4.0	4.5
X	–	–	–	–	16.7	5.4	23.4	19	1.6	12,17	6.4	15.3	10.1	10.5	8.6	9.6	9.2	9.1	8.8	5.7	7.5	7.3	1.2	8.1	3.2	4.2	5.4	4.9	3.0	4.4
XI	–	–	–	–	7.8	1.9	14.8	3	-7.5	23	3.6	6.4	4.5	4.8	7.6	8.1	7.8	7.8	9.2	8.3	9.0	8.8	0.7	1.8	0.9	1.1	7.8	8.1	7.3	7.7
XII	–	–	–	–	-0.3	-7.5	14.7	5	-27.9	25	-4.7	-2.2	-4.1	-3.8	4.3	4.9	4.5	4.6	8.0	8.2	8.5	8.2	0.9	1.2	0.9	1.0	7.7	7.8	6.3	7.3
Rok	–	–	–	–	13.8	4.1	33.9	11.VIII	-27.9	25.XII	6.5	12.0	8.3	8.8	9.2	9.4	9.5	9.4	8.4	6.4	7.9	7.6	1.8	7.2	3.0	4.0	6.4	6.6	5.5	6.2

Katowice

$\varphi = 50°14'$ $\lambda = 19°02'$

I	985.6	1006.6	966.2	1021.8	0.1	-7.4	10.2	4	-19.7	18	-5.1	-0.8	-4.1	-3.5	4.0	4.5	4.2	4.2	8.7	7.5	8.6	8.3	0.6	1.5	0.7	0.9	6.3	6.0	5.4	5.9
II	988.5	1003.4	959.4	1023.9	4.6	-1.2	12.9	18	-7.4	6	0.1	3.6	1.2	1.5	5.7	6.3	5.9	6.0	9.2	8.0	8.8	8.7	0.5	1.8	0.8	1.0	8.4	7.6	6.3	7.4
III	985.4	1002.9	962.1	1020.2	9.5	1.6	19.0	10,18	-3.4	20	3.2	7.7	5.4	5.4	6.9	7.1	7.3	7.1	8.9	6.9	8.1	8.0	0.9	3.9	1.9	2.2	8.0	6.9	7.0	7.3
IV	978.9	987.7	971.6	1012.8	17.2	4.5	24.5	15	-3.8	10	8.1	15.9	10.3	11.2	8.7	8.8	8.8	8.8	7.9	5.0	7.0	6.6	2.3	10.0	4.0	5.4	5.1	5.1	4.8	5.0
V	979.2	985.5	965.0	1013.1	16.4	5.9	23.8	6	0.9	15	9.5	14.6	10.3	11.2	10.2	9.9	10.4	10.2	8.5	6.0	8.3	7.6	1.8	7.2	2.3	3.8	7.3	7.8	7.6	7.6
VI	982.6	996.1	971.8	1014.8	23.1	11.1	31.3	27	3.8	16	16.0	21.4	16.1	17.4	14.4	13.9	14.6	14.3	8.0	5.5	8.0	7.2	4.0	12.2	3.8	6.7	4.7	6.3	5.6	5.5
VII	981.7	992.8	967.6	1015.1	20.8	10.9	30.0	3	6.1	11	14.6	19.1	14.6	15.7	13.5	13.2	13.6	13.4	8.1	6.1	8.1	7.4	3.4	9.8	3.3	5.5	5.8	7.6	6.1	6.5
VIII	984.3	996.3	974.6	1017.9	21.5	11.0	30.1	10	6.0	14	14.1	20.2	15.4	16.3	14.6	14.6	14.6	14.6	8.9	6.4	8.2	7.7	1.8	9.8	3.3	5.0	5.7	6.8	5.3	5.9
IX	986.2	997.0	975.0	1019.9	24.1	8.9	28.6	17	4.6	22	11.6	20.0	13.6	14.7	12.1	12.9	12.6	12.5	8.8	5.6	8.0	7.5	1.9	11.1	3.2	5.4	4.9	4.2	3.5	4.2
X	985.3	997.2	959.4	1019.5	16.3	5.7	21.3	8	0.7	10	7.3	15.4	10.1	10.7	9.5	10.2	10.2	10.0	9.2	6.0	8.2	7.6	0.9	7.5	2.3	3.6	6.8	6.2	4.9	6.0
XI	980.8	1002.2	967.8	1015.7	7.0	0.6	14.4	3	-7.2	21	2.7	6.0	3.1	3.7	7.1	7.3	7.0	7.1	9.3	7.8	9.0	8.7	0.6	2.3	0.8	1.2	8.2	7.7	7.0	7.6
XII	981.9	1006.8	965.0	1017.9	-0.2	-7.7	17.4	5	-23.7	26	-4.3	-1.8	-4.2	-3.6	4.7	4.7	4.5	4.6	8.9	8.1	8.7	8.6	0.6	1.5	0.7	0.9	7.9	7.4	5.9	7.1
Rok	983.4	1006.8	959.4	1018.0	13.1	3.7	31.3	27.VI	-23.7	26.XII	6.5	11.8	7.6	8.4	9.3	9.4	9.5	9.4	8.7	6.6	8.2	7.8	1.6	6.6	2.3	3.6	6.6	6.6	5.8	6.3

Borusowa — $H_s = 170$ m — $h_w = 16$ m — 1961

MIESIĄC	ROZKŁAD WIATRU (%)																		OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	≥ 10	≥ 15			≥ 0.1	≥ 1.0	≥ 10.0			
I	9.5	2.7	4.5	3.0	6.5	1.9	·	·	10.5	3.6	3.5	3.1	1.4	3.6	5.5	3.9	39	1.9	12.1	5.4	14	12	15	28	·	·	·	–	–	5	4	·	4	19	·
II	2.5	1.4	·	·	5	3.0	0.5	4.0	18.5	3.3	3	2.3	24.5	3.5	5	3.4	29	2.3	25.2	6.0	19	·	·	17	·	1	·	·	15	9	7	·	4	3	·
III	1	2.0	·	·	·	·	·	·	1.5	2.0	3	3.8	6.4	6.9	12.5	6.2	11	5.7	20.5	5.6	18	·	·	6	·	15	·	·	22	11	6	·	·	1	1
IV	8.5	3.5	3	3.2	2.0	4.4	3.5	3.6	6	3.2	4.5	1.9	1.6	4.8	1.5	6.0	27	2.8	10.4	3.8	8	·	·	1	1	4	·	–	–	4	4	·	1	·	1
V	6	2.2	3.5	2.3	10.5	2.5	4	2.8	7.5	2.7	1	2.5	2.8	4.0	8.5	3.5	24	2.4	54.9	15.2	6	·	·	·	·	2	·	2	9	13	11	1	3	·	4
VI	2.5	2.8	1.5	1.3	9.5	2.9	2.5	3.4	10.5	3.4	9	3.2	22.5	3.6	7	4.0	25	2.4	78.2	25.1	27	·	·	·	13	2	·	–	–	12	10	3	4	·	7
VII	1.5	2.0	·	·	·	·	2.5	3.2	5.5	3.8	5	2.7	41.5	3.7	4	3.4	33	2.3	103.6	44.0	30	·	·	·	8	2	·	–	–	14	12	3	·	·	6
VIII	3	2.7	1	3.0	2	2.5	·	·	6.5	2.8	8.5	3.2	2.7	3.6	1.3	3.6	32	2.2	51.6	22.0	9	·	·	·	8	1	·	–	–	5	5	3	1	·	4
IX	3.5	2.9	2.5	1.6	1.3	2.5	2.5	2.4	4	3.5	4.5	2.8	24.6	4.3	0.5	4.0	35	2.1	40	–	–	·	·	·	10	2	·	–	–	2	2	·	4	·	2
X	6.5	3.4	1.5	2.3	20.5	2.3	1.8	5.2	1.3	5.5	·	·	8	2.9	2.5	2.4	23	2.9	11.2	8.5	30	·	·	·	·	3	1	8	9	4	2	·	7	·	·
XI	6	2.3	·	·	1.1	2.7	·	·	3	2.0	1.5	3.7	31.5	3.3	2	4.5	35	1.9	59.1	16.6	11	·	·	7	·	·	·	1	17	13	11	2	3	·	·
XII	1.3	3.8	1.5	2.7	5.5	2.5	·	·	6	3.3	4	4.0	19.5	5.5	8.5	4.0	35	2.6	50.8	23.6	6	14	18	24	·	2	1	2	17	8	4	2	–	24	·
Rok	63.5	2.6	1.9	1.6	103.5	2.3	33.5	2.0	92.5	3.3	47.5	2.8	32.1	4.1	70.5	4.1	344	2.6	481.6	44.0	30.VII	26	33	83	40	34	2	–	–	100	78	14	–	47	25

Zakrzów — $H_s = 217$ m — $h_w = 13$ m

I	7	1.5	2.5	1.4	14.5	1.6	2	2.0	39.5	3.3	2	4.5	·	·	1.5	4.0	24	2.0	4.4	3.0	14	10	13	25	·	·	·	7	12	5	1	·	3	15	·
II	4	1.8	·	·	0.5	1.0	3.5	1.9	28.5	3.4	5	2.8	9.5	2.4	6	3.7	27	2.0	36.3	11.6	9	·	·	16	·	·	·	12	2	11	9	1	6	2	
III	3	6.3	·	·	·	·	·	·	6.5	2.3	6.5	3.5	30	3.2	23	3.7	24	2.6	37.7	15.8	14	·	·	9	·	·	·	3	15	13	8	1	·	1	
IV	4	2.5	2	2.0	11.5	2.6	3	2.0	13.5	2.3	3	2.0	8	2.5	5	2.4	40	1.3	21.6	11.1	1	·	·	2	1	·	·	9	6	4	2	2	1	·	1
V	1.4	3.1	3.5	1.9	1.5	1.0	3.5	2.3	12	2.3	13.5	3.1	7	2.7	15	2.8	23	2.0	54.3	18.0	29	·	·	·	·	·	·	1	14	12	10	1	·	·	3
VI	10.5	3.0	0.5	1.0	1	3.0	2	4.0	1.4	2.1	7	2.1	3	3.3	1.6	2.6	36	1.5	102.4	26.7	27	·	·	·	8	·	·	5	9	13	10	4	–	·	11
VII	5	2.3	·	·	·	·	0.5	3.0	1.9	2.9	4.5	2.0	1.0	3.4	1.6	3.0	38	1.7	123.1	24.8	15	·	·	·	7	·	·	3	17	1.4	1.3	4	–	·	2
VIII	7	2.4	2	2.5	2	1.5	1	1.0	23.5	2.4	5.5	2.8	3	2.7	1.4	2.7	35	1.5	46.4	19.2	12	·	·	·	6	·	·	4	8	11	8	1	4	·	2
IX	0.5	4.0	1	2.0	7.5	1.5	2.5	2.6	12.5	2.2	9.5	3.3	·	·	10.5	2.3	46	1.2	12.0	6.1	6	·	·	1	8	·	·	15	7	4	4	·	9	·	
X	8	2.9	·	·	3.5	3.6	1.2	3.0	15.5	2.3	7	3.4	·	·	1.3	3.1	34	1.8	13.7	7.6	19	·	·	·	·	·	·	6	9	5	4	·	9	·	
XI	15.5	2.7	2.5	2.6	1.5	3.0	2	2.8	28.5	2.9	3	3.7	3	3.0	7	3.7	27	2.1	59.2	21.8	4	·	·	7	·	·	·	2	17	15	10	1	2	·	·
XII	15.5	2.7	8	2.4	1	1.0	2.5	5.6	1.7	3.2	8.5	4.3	2	5.5	20.5	3.3	18	2.7	39.1	10.1	11	11	14	24	·	·	·	2	16	9	8	1	·	17	·
Rok	9.4	2.9	2.2	1.3	44.5	1.6	34.5	2.3	230	2.6	75	3.1	75.5	2.4	147.5	3.1	372	1.9	550.2	26.7	27.VII	21	27	84	30	·	·	69	132	116	87	16	–	35	19

Leżajsk — $H_s = 190$ m — $h_w = 15,7$ m

I	3	2.0	3	2.0	8	1.4	1.8	2.6	10.5	3.9	17.5	5.4	1.8	4.9	5	4.2	10	3.4	13.5	3.9	14	13	16	29	·	2	1	6	14	10	4	·	4	25	
II	2	1.0	1	1.0	6.5	2.5	8.5	2.4	16	2.7	17	3.6	22	3.2	4	3.5	7	2.7	13.9	5.7	10	·	·	16	·	·	·	1	17	10	4	·	6	3	·
III	·	·	·	·	·	·	·	·	3.5	4.1	2.5	5.3	59.5	6.2	3	3.0	2	5.7	27.7	6.2	29	·	·	8	·	6	·	1	13	16	7	·	5	1	1
IV	4	1.8	6	2.5	24.5	4.4	6.5	5.1	9	2.8	1.7	4.3	8.5	6.6	3.5	4.0	11	3.7	13.4	5.4	1	·	·	2	1	6	·	7	4	6	4	·	·	·	1
V	8	2.3	1	4.0	12	3.0	6.5	1.7	5	2.9	1.5	3.1	22.5	3.2	1.2	3.0	11	2.6	76.2	26.2	14	·	·	·	2	1	·	·	13	14	9	2	2	·	5
VI	2	1.0	2.5	4.2	10.5	3.0	7	1.3	6	1.7	18.5	3.4	22.5	2.8	10	2.8	11	2.4	44.0	12.7	27	·	·	·	14	·	·	4	8	12	9	1	·	·	11
VII	2.5	1.0	1	2.0	·	·	1	3.0	9	2.7	23.5	3.0	39.5	3.3	6.5	2.4	10	2.7	89.5	33.5	29	·	·	·	10	1	·	3	7	15	8	3	·	·	6
VIII	3.5	2.3	0.5	2.0	5	1.9	2	2.2	7.5	2.9	20.5	3.6	27	3.6	1.6	2.6	11	2.8	56.5	15.0	12	·	·	·	10	·	·	3	6	9	8	3	·	·	7
IX	·	·	2	2.0	1.2	2.0	5	2.3	5.5	4.0	20.5	4.5	20	3.4	4	2.2	21	2.6	19.4	11.1	6	·	·	1	8	1	·	12	8	8	3	1	7	·	2
X	·	·	2	2.5	34.5	4.1	18.5	3.0	5	3.4	8.5	2.9	11	3.5	5.5	1.9	8	3.1	18.3	11.4	30	·	·	·	·	1	·	12	7	6	4	1	8	·	
XI	0.5	1.0	1.5	1.7	12.5	4.4	11.5	3.0	9.5	2.9	2.5	3.7	1.5	3.7	4.5	3.7	10	3.2	36.3	12.3	13	·	·	10	·	·	·	3	17	16	9	1	8	·	
XII	8.5	2.7	2.5	2.4	5	2.1	10.5	2.3	6.5	8.4	1.5	6.6	16.5	3.8	12.5	4.8	16	3.7	40.2	11.4	11	10	15	23	·	4	1	2	17	13	8	1	3	17	
Rok	3.4	1.3	2.3	2.2	130.5	2.4	9.5	2.4	9.3	3.5	22.3	4.1	28.2	4.0	86.5	3.2	128	3.2	448.9	33.5	29.VII	23	31	89	45	22	2	54	131	135	77	13	43	46	33

Katowice — $H_s = 284$ m — $H_b = 284,1$ m — $h_w = 20$ m

I	0.5	3.0	3.5	3.6	13.5	3.8	11	2.9	10.5	3.7	2.9	4.8	1.4	4.3	6	4.4	5	3.9	23.0	7.6	4	11	15	28	·	2	·	7	12	13	7	·	5	22	
II	3.5	3.3	1	1.0	1	2.0	1.1	2.0	8	3.2	2.7	5.0	16.5	4.8	8	3.6	8	3.6	58.0	15.1	9	·	·	17	·	1	·	3	16	15	10	2	11	6	
III	5.5	3.7	·	·	·	·	·	·	0.5	10.0	2.2	6.5	4.0	5.2	2.3	5.6	2	5.5	65.2	11.0	14	·	·	8	·	8	·	2	17	17	14	1	4	5	2
IV	2	3.5	9.5	3.3	16.5	4.9	1.4	3.9	7	3.8	21.5	5.7	7.5	4.1	5	4.3	7	4.2	16.4	6.2	1	·	·	3	·	2	1	6	5	7	4	·	1	·	2
V	11.5	2.8	8	2.7	6	3.6	5.5	2.5	5	2.6	1.6	4.3	17.5	3.9	16.5	4.0	7	3.3	82.3	17.6	27	·	·	·	·	2	·	·	13	17	14	3	5	·	5
VI	8	3.5	6.5	2.1	7.5	3.3	7.5	3.6	8	3.4	1.2	3.3	16.5	4.6	1.8	3.3	6	3.3	103.9	52.9	27	·	·	·	10	1	·	4	5	15	10	3	6	·	8
VII	9	2.9	1.5	1.7	·	·	2	2.2	4.5	3.2	21.5	4.0	3.7	4.4	10.5	3.0	7	3.5	140.7	33.6	13	·	·	·	7	2	·	3	14	18	12	5	·	·	5
VIII	9	2.7	5	2.0	4	2.5	2.5	2.4	2	2.8	2.5	4.9	2.7	4.2	9.5	3.6	9	3.5	70.7	30.8	12	·	·	·	7	2	·	2	9	11	9	1	8	·	4
IX	0.5	2.0	3	2.7	11.5	3.7	9.5	2.9	4	2.8	27.5	4.6	2.1	4.3	6	4.1	7	3.7	25.7	11.5	4	·	·	·	7	1	·	10	7	7	6	1	5	·	1
X	8	4.2	2	3.8	13	4.5	2.4	3.8	9.5	3.6	1.8	4.3	9	4.2	7.5	3.9	7	3.8	36	1.8	29	·	·	·	·	2	·	4	8	7	1	·	10	·	·
XI	8	3.9	4	4.0	3.5	3.7	8.5	3.1	7	2.3	3.2	4.4	15.5	4.1	6.5	3.1	5	3.6	79.3	24.4	4	·	·	10	·	2	·	1	19	19	10	2	7	3	·
XII	6	4.3	15.5	4.2	3.5	3.4	3.5	2.1	6.5	2.6	23.5	5.7	1.1	5.5	10.5	4.4	13	4.0	54.2	16.4	6	13	14	27	·	5	·	3	14	17	7	3	4	24	·
Rok	6.6.5	3.3	5.9.5	2.6	80	3.0	9.9	2.6	7.2.5	3.7	2.7.5	4.8	2.3.2.9	4.5	1.2.7	3.9	8.3	3.8	7.2.3.0	5.2.9	2.7.VI	2.4	2.9	9.3	3.1	3.0	1	4.5	1.3.9	1.6.3	1.0.4	2.1	6.6	6.0	2.7

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Kalbuszowa

$\varphi = 50°14'$ $\lambda = 21°47'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.6	-9.2	9.3	4	-25.6	27	-6.2	-1.9	-5.0	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.1	5.8	6.3
II	–	–	–	–	4.1	-0.8	10.1	18	-4.4	5	0.1	3.1	0.9	1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.6	7.2	7.8
III	–	–	–	–	9.5	2.2	19.5	18	-3.0	23	3.8	7.7	5.1	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.8	8.2	6.9	8.0
IV	–	–	–	–	17.3	4.1	25.6	15	-4.2	10	7.6	15.8	9.1	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.6	4.7	5.4
V	–	–	–	–	16.8	6.2	25.0	29	0.6	19	10.0	15.3	10.5	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.1	6.2	7.3
VI	–	–	–	–	24.3	10.9	32.0	27	4.1	21	16.2	22.8	15.5	17.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.3	6.7	6.2
VII	–	–	–	–	22.5	10.5	31.9	4	5.7	8	15.0	20.5	14.6	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.4	6.7	6.9
VIII	–	–	–	–	23.3	11.9	33.5	11	4.1	31	14.9	21.6	15.9	17.1	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.8	6.3	6.4
IX	–	–	–	–	21.5	7.4	29.0	18	-2.0	23	10.5	20.0	12.5	13.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.4	4.5	5.1
X	–	–	–	–	16.6	5.2	23.3	19	0.1	12	7.3	15.7	9.6	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.2	4.8	5.9
XI	–	–	–	–	7.7	2.2	13.9	3	-6.4	21,24	3.6	6.5	4.5	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	7.9	8.3
XII	–	–	–	–	-0.1	-8.3	13.4	5	-31.1	26	-5.0	-2.0	-4.4	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.5	7.5	7.7
Rok	–	–	–	–	13.6	3.5	33.5	11.VIII	-31.1	26.XII	6.5	12.1	7.4	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.3	6.8

Głubczyce

$\varphi = 50°12'$ $\lambda = 17°49'$

I	–	–	–	–	0.8	-5.7	10.1	4	-18.8	27	-4.4	-0.4	-3.0	-2.7	4.4	4.9	4.7	4.7	91	77	89	86	0.4	1.4	0.5	0.8	–	–	–	–
II	–	–	–	–	5.9	-0.6	12.1	18	-7.4	6	0.8	5.0	1.5	2.2	6.1	6.7	6.4	6.4	94	77	94	88	0.4	2.1	0.5	1.0	–	–	–	–
III	–	–	–	–	11.2	2.0	20.6	10	-3.3	20	3.3	10.0	5.2	5.9	6.8	7.5	7.5	7.3	87	62	85	78	1.1	5.2	1.5	2.6	–	–	–	–
IV	–	–	–	–	17.8	4.8	26.8	7	-3.8	10	8.2	16.6	9.8	11.1	9.1	9.4	9.4	9.3	83	51	77	70	2.1	10.1	3.0	5.1	–	–	–	–
V	–	–	–	–	17.0	6.5	24.1	27	0.9	13	10.0	15.0	10.1	11.3	10.9	10.9	11.1	11.0	88	65	89	81	1.5	6.7	1.5	3.2	–	–	–	–
VI	–	–	–	–	23.3	11.4	29.8	25	5.7	21	15.8	21.6	16.0	17.4	15.0	15.1	16.0	15.4	83	59	88	77	3.1	11.2	2.4	5.6	–	–	–	–
VII	–	–	–	–	21.6	11.1	31.6	3	7.0	26	14.8	19.7	14.5	15.9	13.9	13.7	14.3	14.0	82	61	86	76	3.3	10.1	2.5	5.3	–	–	–	–
VIII	–	–	–	–	22.2	11.5	29.5	6	6.8	4	14.4	20.6	14.9	16.2	14.7	15.1	15.0	14.9	88	62	88	79	2.1	9.8	2.1	4.7	–	–	–	–
IX	–	–	–	–	22.3	9.3	29.8	18	-0.4	23	11.4	21.4	13.5	15.0	12.3	13.8	13.3	13.1	89	56	85	77	1.6	11.8	2.6	5.3	–	–	–	–
X	–	–	–	–	16.4	6.0	23.0	11	0.8	3	7.4	15.2	9.7	10.5	9.1	11.2	10.2	10.2	88	66	65	80	1.3	6.5	1.9	3.2	–	–	–	–
XI	–	–	–	–	7.2	1.5	14.1	1	-4.6	22	2.7	6.1	3.6	4.0	7.0	7.6	7.4	7.3	93	80	91	88	0.5	2.1	0.7	1.1	–	–	–	–
XII	–	–	–	–	0.8	-6.4	15.2	5	-23.1	26	-3.9	-1.2	-3.1	-2.8	4.7	5.0	5.0	4.9	89	79	87	85	0.6	1.4	0.7	0.9	–	–	–	–
Rok	–	–	–	–	13.9	4.3	31.6	3.VII	-23.1	26.XII	6.7	12.5	7.7	8.6	9.5	10.1	10.0	9.9	88	66	87	80	1.5	6.5	1.7	3.2	–	–	–	–

Goszyce

$\varphi = 50°11'$ $\lambda = 20°08'$

I	–	–	–	–	-4.1	-9.3	7.0	4	-23.5	27	-6.9	-2.6	-4.9	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.8	5.0	5.8
II	–	–	–	–	4.5	-0.7	11.8	18,28	-5.4	5	0.0	3.4	1.6	1.6	5.7	6.5	6.2	6.1	92	81	90	88	0.5	1.5	0.7	0.9	8.3	8.1	6.7	7.7
III	–	–	–	–	9.4	2.7	18.7	18	-2.3	23	3.9	7.8	5.6	5.7	7.1	7.5	7.4	7.3	87	71	81	80	1.1	3.4	1.8	2.1	6.5	6.7	5.3	6.2
IV	–	–	–	–	17.0	4.6	25.8	15	-3.7	10	6.9	15.6	10.3	10.8	8.2	9.4	9.3	9.0	81	53	74	69	2.0	9.0	3.5	4.8	3.8	4.5	3.5	3.9
V	–	–	–	–	16.7	6.5	23.9	27	2.8	12,13	8.9	15.1	10.7	11.4	10.1	11.0	10.9	10.7	88	64	84	79	1.4	6.7	2.2	3.4	5.5	6.6	6.3	6.1
VI	–	–	–	–	23.3	11.3	32.0	27	5.8	21	15.4	21.9	16.3	17.5	14.7	14.6	14.9	14.7	84	56	80	73	3.1	12.4	3.8	6.4	3.6	5.1	5.8	4.8
VII	–	–	–	–	21.4	11.3	30.0	3	5.9	8	14.2	19.7	15.4	16.2	13.9	14.0	14.3	14.1	85	62	81	76	2.5	9.8	3.5	5.3	6.1	6.2	6.4	6.2
VIII	–	–	–	–	22.0	12.0	31.0	11	7.3	31	14.3	20.7	16.1	16.8	14.3	14.9	15.2	14.8	86	60	81	76	2.2	10.5	3.5	5.4	5.0	4.8	4.1	4.6
IX	–	–	–	–	20.6	9.0	28.4	17	1.0	22	10.7	19.6	14.6	14.9	11.5	12.5	12.7	12.2	88	56	75	73	1.6	11.0	4.2	5.6	4.1	3.5	3.9	3.8
X	–	–	–	–	15.9	5.5	21.7	20	-0.8	24	6.9	15.2	10.3	10.7	8.7	10.2	9.9	9.6	87	60	79	75	1.5	7.3	2.8	3.9	5.0	4.8	3.2	4.3
XI	–	–	–	–	6.6	0.9	14.6	3	-7.6	23	2.4	5.5	3.3	3.6	6.9	7.5	7.3	7.2	91	82	92	88	0.7	1.9	0.7	1.1	7.3	6.7	5.6	6.5
XII	–	–	–	–	-0.8	-8.6	16.7	5	-26.2	26	-5.2	-2.8	-5.0	-4.5	4.2	4.7	4.1	4.3	84	83	82	83	0.7	1.2	0.8	0.9	7.8	6.5	6.0	6.8
Rok	–	–	–	–	13.0	3.8	32.0	27.VI	-26.2	26.XII	6.0	11.6	7.9	8.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	5.2	5.6

Horyniec

$\varphi = 50°11'$ $\lambda = 23°21'$

I	–	–	–	–	-1.2	-10.4	9.9	4	-25.6	27	-7.1	-2.1	-6.5	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	4.5	5.1	5.7
II	–	–	–	–	2.9	-1.9	9.0	28	-8.8	15	-1.0	2.2	0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.9	7.6	7.9
III	–	–	–	–	8.3	0.8	18.0	18	-6.2	23	2.7	7.3	4.2	4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.4	5.6	7.0
IV	–	–	–	–	16.7	3.3	24.9	7,15	-5.1	10	7.6	15.6	8.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.6	4.1	4.3
V	–	–	–	–	16.7	5.5	25.0	29	-4.0	17	10.4	15.4	9.4	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.5	7.1	7.2
VI	–	–	–	–	23.5	10.4	30.4	27	4.2	29	16.8	22.0	15.1	17.2	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.6	4.2	4.2
VII	–	–	–	–	22.9	9.8	30.6	4	4.7	7	15.3	21.6	14.4	16.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.4	5.4	5.1
VIII	–	–	–	–	22.4	10.7	33.3	11	3.4	31	14.7	21.3	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.0	4.9	4.8
IX	–	–	–	–	20.7	7.0	29.0	18	-1.6	23	10.5	19.9	10.7	13.0	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.1	3.7	4.2
X	–	–	–	–	16.3	3.5	23.2	19	-4.8	13	6.0	15.7	8.3	9.6	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.2	3.0	4.2
XI	–	–	–	–	7.7	0.6	15.2	3	-9.9	23	3.1	6.8	3.8	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.9	8.0	8.2
XII	–	–	–	–	-0.4	-8.9	16.5	5	-23.9	26	-5.1	-1.9	-4.8	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	7.2	7.5
Rok	–	–	–	–	13.0	2.5	33.3	11.VIII	-25.6	27.I	6.2	12.0	6.6	7.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.9	5.5	5.9

Kalbuszowa

$H_s = 208$ m $h_w = 16{,}1$ m 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD																		OPAD R			LICZBA DNI (n)											
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max<-10°	Max<0°	Max<0°	Max>25°	>10	>15		≥0.1	≥1.0	≥10.0			
I	2	2.0	3.5	2.6	2	1.5	9	2.0	26.5	3.8	8.5	2.4	15	2.1	25	3.2	24	2.1	19.6	5.6	14	10	14	29	·	1	·	5	12	13	6	·	1	2.0	·
II	·	·	2	1.0	5.5	2.3	7.5	1.5	20.5	3.6	10	2.2	17.5	1.8	2	1.0	19	1.8	31.4	10.2	10	·	·	20	·	·	·	·	16	12	7	1	2	1	·
III	·	·	·	·	1.5	1.0	0.5	1.0	4.5	5.7	24	3.9	52.5	4.9	5	3.6	5	4.3	34.9	5.7	12	·	·	8	·	4	1	·	14	16	9	·	·	·	·
IV	3	3.3	3.5	3.7	2.2	4.8	6	3.8	10	3.0	10	3.8	8.5	4.4	5	3.0	22	3.0	22.7	8.2	16	·	·	4	1	2	·	5	6	8	5	·	·	·	2
V	3	2.0	3	1.7	6	3.7	4.5	1.8	9.5	2.6	11	3.4	17	2.9	8	2.2	31	1.8	54.1	19.7	14	·	·	·	·	·	·	·	12	15	10	1	1	·	3
VI	1.5	1.3	3	2.7	6.5	4.0	7	1.2	5.5	2.4	14	1.8	19.5	2.3	5	2.5	28	1.6	62.1	11.5	3,9	·	·	·	13	·	·	1	10	13	11	2	1	·	6
VII	1	3.0	·	·	0.5	3.0	1.5	2.7	8.5	2.9	23.5	2.7	19.5	2.0	3.5	2.9	35	1.6	118.1	26.9	29	·	·	·	8	·	·	2	12	16	9	5	·	·	2
VIII	2.5	1.8	3	4.0	1.5	2.3	4.5	1.9	8	3.4	19.5	3.0	19.5	3.5	7.5	2.7	27	2.2	53.2	12.3	12	·	·	·	8	·	·	1	12	14	7	1	1	·	5
IX	0.5	4.0	2.5	2.8	9.5	3.0	1.5	2.3	9	2.6	12	3.2	14	2.9	2	3.2	39	1.7	27.9	13.3	6	·	·	2	7	·	·	10	7	7	4	1	2	·	2
X	1	2.0	3.5	4.0	3.1	3.5	10.5	3.0	12	4.3	5.5	1.9	7	2.4	1.5	4.7	21	2.6	19.2	13.9	30	·	·	·	·	·	·	5	8	6	3	1	1	·	·
XI	3	1.5	1	3.0	12.5	6.2	7	2.5	16	3.3	19	2.7	11.5	3.0	5	2.1	15	2.8	36.0	9.3	13	·	·	7	·	·	·	·	17	16	10	·	2	·	·
XII	8.5	3.6	4.5	2.6	2.5	2.8	2	1.3	23	4.2	7.5	2.9	11.5	3.3	12.5	2.8	21	2.6	54.4	12.1	11	12	15	23	·	·	·	15	14	10	2	1	2.3	·
Rok	2.6	2.0	2.9.5	2.3	10.1	3.2	6.1.5	2.1	153	3.5	164.5	2.8	213	3.0	59.5	2.8	287	2.3	533.9	26.9	29.VII	22	29	93	37	7	1	29	141	150	91	14	12	44	20

Głubczyce

$H_s = 280$ m $h_w = 13$ m

I	3	2.3	·	·	2	2.0	2	1.0	21	5.0	17	5.4	3.5	1.6	0.5	3.0	44	2.3	4.7	4.2	14	8	13	25	·	3	·	-	-	5	1	·	2	2.1	·
II	5	2.0	·	·	·	·	1.5	2.3	20.5	2.8	14	3.8	5	2.0	1	2.0	37	1.6	38.1	8.7	9	·	1	16	·	·	·	-	-	12	9	·	5	4	·
III	8	2.4	1	2.0	·	·	·	·	3	3.5	9	2.8	20.5	3.4	11.5	3.6	40	1.8	32.7	7.3	28	·	·	8	·	1	·	-	-	15	9	·	1	4	·
IV	2	3.5	2.5	2.6	1.5	2.7	4	2.5	2.3	3.0	5	4.0	14	2.8	3	2.5	35	1.8	13.2	6.7	17	·	·	4	1	·	·	-	-	6	3	·	·	·	1
V	5	2.5	·	·	0.5	2.0	1.5	2.0	6.5	3.2	20.5	3.1	14	2.4	6	2.8	39	1.6	79.5	15.5	29	·	·	·	·	·	·	-	-	19	15	2	·	·	5
VI	4.5	2.2	1.5	2.0	1	2.0	4.5	1.8	9.5	2.2	8.5	2.1	8	2.6	5.5	2.7	47	1.1	95.1	28.8	10	·	·	·	9	·	·	-	-	14	11	4	·	·	10
VII	1.5	2.0	·	·	·	·	1.5	2.0	18.5	2.6	9.5	2.9	10.5	2.7	6.5	2.6	45	1.4	131.3	28.6	13	·	·	·	7	·	·	-	-	17	11	5	·	·	6
VIII	2.5	4.6	·	·	0.5	3.0	1.5	3.0	14.5	2.7	17	2.9	6	2.0	3	3.5	48	1.4	39.0	10.0	12	·	·	·	5	·	·	-	-	16	8	1	·	·	1
IX	3.5	1.9	2	1.2	1.5	2.0	2.5	1.4	19	2.2	11.5	2.8	3.5	2.0	0.5	2.0	46	1.1	9.9	5.3	6	·	·	1	10	·	·	-	-	6	2	·	3	·	·
X	0.5	3.0	1	3.0	3.5	2.4	·	·	19.5	3.8	9.5	5.3	11	2.1	1	4.0	47	1.8	37.3	17.8	19	·	·	·	·	·	·	-	-	6	5	1	4	·	·
XI	11.5	1.7	1.5	1.3	·	·	·	·	14	3.0	10	3.6	3.5	1.9	2.5	2.6	47	1.3	55.1	16.7	5	·	·	5	·	·	·	-	-	17	9	1	4	3	·
XII	2.2	3.0	·	·	4	1.0	1	2.0	14.5	5.4	19.5	5.3	6	2.7	2	3.0	24	3.0	42.0	8.0	6	10	13	23	·	1	·	-	-	10	10	·	·	22	·
Rok	6.9	2.6	9.5	1.0	14.5	1.4	20	1.5	183.5	3.3	151	3.7	105.5	2.4	43	2.9	499	1.7	577.9	28.8	10.VI	18	27	82	32	5	·	-	-	143	93	14	19	54	23

Goszyce

$H_s = 260$ m $h_w = 14{,}5$ m

I	3.5	2.1	1.4	1.6	7	3.3	7.5	2.1	12.5	2.5	16	3.4	2	1.5	2.5	1.4	28	1.7	18.1	5.1	4	13	15	28	·	·	·	-	-	12	6	·	4	2.0	·
II	·	·	4	2.9	1.1	1.6	13	1.6	10	1.6	16	3.9	17	3.2	1	2.0	12	2.2	13.4	4.2	9			16	·	·	·	-	-	9	5	·	4	3	·
III	1	2.0	·	·	·	·	·	·	9.5	4.6	3.5	5.2	38.5	5.4	3	2.7	6	4.8	22.4	5.8	18	·	·	6	·	2	·	-	-	15	9	·	1	4	1
IV	2	1.8	1.5	3.1	16.5	4.4	13.5	4.0	9.5	2.3	9	3.8	1.5	2.3	6	5.2	17	3.0	16.6	4.6	2	·	·	1	1	·	·	-	-	8	5	·	1	·	2
V	3.5	3.6	1.0	2.7	4	4.0	9.5	2.2	9.5	2.4	11	3.1	11	3.3	11.5	3.3	23	2.2	70.0	14.7	28	·	·	·	·	·	·	-	-	15	13	2	1	·	5
VI	1	2.0	4	3.4	8	2.8	7	2.4	9.5	2.5	11.5	3.9	11.5	3.1	10.5	2.4	27	2.0	52.2	14.6	27	·	·	·	7	·	·	-	-	12	8	2	3	·	12
VII	2	2.5	1	6.0	1	4.0	1	2.0	17.5	3.1	22.5	3.6	16	3.3	14	2.8	18	2.6	108.6	24.6	30	·	·	·	8	·	·	-	-	15	14	3	·	·	7
VIII	2	3.0	2.5	4.6	3	2.0	4	3.8	7	3.2	13	3.9	24.5	4.2	4	3.8	33	2.5	76.2	39.8	9	·	·	·	6	·	·	-	-	11	5	2	1	·	4
IX	·	·	1.0	3.7	1.1	3.4	3.5	1.7	4	2.6	14.5	4.2	14	3.6	6	4.3	27	2.5	17.7	6.7	29	·	·	·	6	·	·	-	-	7	4	·	6	·	3
X	0.5	1.0	5	5.9	15.5	4.4	1.5	4.3	11.5	3.2	2.5	3.0	4	4.6	8	2.4	31	2.6	4.8	4.2	30	·	·	2	·	1	·	-	-	3	1	·	4	·	·
XI	1.5	2.0	1	4.0	7	4.4	·	·	6	1.2	14.5	3.5	7	2.9	5	3.8	48	1.5	73.0	16.5	4	·	·	11	·	·	·	-	-	16	9	4	5	6	·
XII	1.1.5	3.0	10.5	2.3	2	2.0	·	·	10	3.8	10	5.6	3	3.7	13	3.2	33	2.2	41.3	19.8	11	14	18	25	·	2	·	-	-	11	6	1	4	24	·
Rok	2.8.5	1.9	77	3.4	86	3.0	74	2.0	116.5	2.8	175.5	3.9	150	3.4	84.5	3.1	303	2.5	514.3	39.8	9.VIII	27	33	89	28	5	·	-	-	134	85	14	34	57	34

Horyniec

$H_s = 240$ m $h_w = 12$ m

I	1	3.0	2.5	1.4	1.5	1.3	11	2.7	12	2.9	9.5	4.1	15	3.8	7.5	3.9	33	2.1	14.6	4.5	31	13	16	28	·	1	·	5	9	11	3	·	3	3.1	-
II	·	·	·	·	1.5	1.7	7.5	2.7	9.5	2.4	6.5	2.8	14.5	3.1	2.5	3.0	42	1.4	23.2	7.2	10	·	2	22	·	·	·	1	19	13	7	·	12	17	-
III	·	·	·	·	·	·	1	3.0	1.5	6.0	17	4.0	4.4	4.7	17.5	5.0	12	4.0	20.5	3.6	31	·	·	12	·	2	·	·	13	18	9	·	3	1	-
IV	2.5	4.2	4	3.5	12	3.2	11.5	3.0	8.5	2.2	5	5.0	10.5	6.0	3	6.0	33	2.5	15.3	7.6	1	·	·	2	·	1	1	8	3	7	3	·	·	·	-
V	7.5	2.5	2	2.0	10	1.9	2.5	3.0	3	3.2	7.5	2.7	11	2.8	8.5	2.5	41	1.4	36.5	7.2	9	·	·	3	·	·	·	·	12	16	11	·	3	·	-
VI	3.5	1.7	·	·	8.5	2.5	2.5	2.8	4	2.2	6.5	2.2	10.5	2.5	7.5	2.7	47	1.2	169.0	95.1	2	·	·	·	8	·	·	10	2	13	10	3	1	·	-
VII	6.5	2.8	1	1.5	0.5	2.0	1	2.5	7.5	2.4	8	2.9	15.5	3.2	9	3.1	44	1.5	75.2	35.3	29	·	·	·	10	·	·	4	6	13	9	3	2	·	-
VIII	7.5	2.8	1	2.0	1.5	2.0	3.5	2.3	5	1.9	10	2.5	16.5	2.8	9	2.8	39	1.6	60.2	22.3	12	·	·	·	8	·	·	6	3	15	10	3	4	·	-
IX	1.5	2.7	0.5	2.0	5	2.1	0.5	3.0	2.5	1.8	2	2.2	15	3.3	8	3.7	54	1.2	17.4	7.5	7	·	·	2	7	·	·	12	6	9	6	·	3	·	-
X	1.5	2.7	·	·	2.4.5	2.4	8	2.6	8.5	1.9	1.5	2.3	7.5	2.6	1.5	2.7	40	1.4	10.7	8.3	30	·	·	4	·	·	·	12	7	3	3	·	3	·	-
XI	1	3.0	·	·	7.5	2.6	6.5	1.8	10	2.0	5	2.6	26.5	3.1	2.5	2.8	29	1.8	33.2	5.4	12	·	1	12	·	·	·	2	21	15	11	·	5	·	-
XII	6.5	3.4	4.5	1.9	3.5	2.6	5	2.4	2.5	2.8	7	3.9	17.5	3.1	7.5	2.3	39	1.7	31.0	6.5	11	13	17	25	·	·	·	3	17	17	8	·	5	2.4	-
Rok	3.9	2.4	15.5	1.2	7.9	2.0	60.5	2.6	74.5	2.6	85.5	3.1	20.4	3.4	8.4	3.4	45.5	1.8	506.8	95.1	2.VI	26	36	110	33	4	1	63	118	150	90	9	44	73	-

Trzebinia $\varphi = 50°10'$ $\lambda = 19°28'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	p_m	Max	Min	$p_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	-6.5	9.6	4	-17.0	27	-4.3	-1.0	-3.5	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	5.8	6.4
II	–	–	–	–	4.6	-0.8	13.6	18	-7.0	6	0.1	3.9	1.6	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	6.3	7.4
III	–	–	–	–	9.4	2.2	19.6	10	-2.9	23	3.3	8.1	5.5	5.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	7.1	7.7
IV	–	–	–	–	17.0	6.4	25.0	15	-0.4	1	9.1	16.1	10.8	11.7	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.3	4.0	4.9
V	–	–	–	–	16.6	6.9	23.6	27	2.2	12	9.9	15.4	10.7	11.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	8.1	7.6	7.6
VI	–	–	–	–	23.2	12.4	31.8	27	6.7	16	15.8	22.3	16.3	17.7	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.3	6.1	5.3
VII	–	–	–	–	21.1	11.4	30.0	3	6.8	8	14.8	19.6	15.3	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.4	5.7	5.9
VIII	–	–	–	–	21.8	12.0	30.5	11	7.9	14	15.3	20.7	16.1	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.7	4.8	5.3
IX	–	–	–	–	20.7	10.6	29.2	17	5.4	23	12.5	20.0	14.6	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.4	3.0	4.3
X	–	–	–	–	16.1	7.7	20.0	8	3.3	14	9.5	15.6	10.9	11.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.8	3.7	5.3
XI	–	–	–	–	7.0	1.3	14.6	10	-5.2	21	3.1	6.1	3.5	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.7	6.9	7.1
XII	–	–	–	–	-0.9	-7.2	17.1	5	-21.3	26	-3.7	-2.0	-4.1	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.5	5.9	6.5
Rok	–	–	–	–	13.1	4.7	31.8	27.VI	-21.3	26.XII	7.1	12.1	8.1	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	5.6	6.1

Biały Kościół $\varphi = 50°10'$ $\lambda = 19°50'$

I	–	–	–	–	-0.4	-7.4	7.5	5	-20.3	26	-5.2	-2.0	-4.2	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	4.9	-2.0	12.5	18	-7.0	6	-0.3	3.3	1.5	1.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	6.2	6.9
III	–	–	–	–	9.2	1.0	20.3	18	-4.2	23	3.3	7.5	5.2	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.9	6.2	6.8
IV	–	–	–	–	17.3	5.6	25.1	6	-0.9	1	7.9	15.6	10.0	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.1	4.0	4.4
V	–	–	–	–	16.9	6.9	24.2	6	1.5	12	9.3	14.6	10.6	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.1	6.1	6.2
VI	–	–	–	–	23.3	12.2	31.3	27	6.4	16	16.5	22.0	16.3	17.8	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.1	4.8	4.7
VII	–	–	–	–	21.2	11.1	32.5	2	6.4	6	15.2	19.5	15.6	16.5	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.4	6.5	6.8
VIII	–	–	–	–	21.3	11.9	30.5	11	7.7	14	14.8	20.1	15.6	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.4	5.2	5.2
IX	–	–	–	–	20.1	10.5	28.0	2	3.7	23	12.6	19.2	14.4	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.0	3.6	3.5	4.0
X	–	–	–	–	15.5	6.9	19.8	20	4.2	22	8.3	14.6	10.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.6	4.0	4.6
XI	–	–	–	–	6.6	1.5	14.0	7	-5.4	21	2.7	5.3	3.4	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.9	7.9
XII	–	–	–	–	-0.8	-7.6	15.8	5	-22.2	26	-4.4	-2.7	-3.9	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	6.2	6.6
Rok	–	–	–	–	12.9	4.2	32.5	2.VII	-22.2	26.XII	6.7	11.4	7.9	8.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Garlica Murowana $\varphi = 50°09'$ $\lambda = 19°56'$

I	–	–	–	–	-0.6	-8.3	9.9	4	-18.7	19,26,27	-6.1	-2.3	-4.8	-4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.1	6.6	6.4
II	–	–	–	–	4.4	-1.5	13.2	18	-6.3	7	-0.1	3.4	1.4	1.5	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.5	7.1	7.9
III	–	–	–	–	9.4	2.1	18.9	18	-2.5	23	3.4	7.8	5.1	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.6	6.0	7.2
IV	–	–	–	–	17.0	4.9	25.4	15	-2.0	10	7.4	15.6	10.1	10.8	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.9	3.4	4.3
V	–	–	–	–	16.4	6.1	23.6	6	2.4	15	9.1	14.6	10.6	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.2	7.1	7.1
VI	–	–	–	–	23.1	11.0	31.8	27	5.6	17	15.1	21.5	15.7	17.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	6.1	5.4
VII	–	–	–	–	21.1	10.5	30.0	3	5.9	8	14.1	19.3	14.3	15.5	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.2	6.6	6.6
VIII	–	–	–	–	21.9	11.3	31.1	11	7.3	31	14.2	20.6	15.3	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.5	4.3	5.1
IX	–	–	–	–	20.7	9.0	28.5	17	1.5	23	11.0	19.4	13.3	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.3	2.9	4.2
X	–	–	–	–	16.2	6.1	20.2	19,20	0.6	25	7.3	15.3	10.1	10.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.5	3.5	5.1
XI	–	–	–	–	7.0	1.1	14.8	3	-5.4	21	2.7	5.9	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.4	6.6	7.2
XII	–	–	–	–	-0.5	-8.5	18.0	5	-26.0	26	-5.2	-2.3	-4.8	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.6	6.7	7.2
Rok	–	–	–	–	13.0	3.6	31.8	27.VI	-26.0	26.XII	6.1	11.6	7.5	8.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.3	5.5	6.2

Lubaczów $\varphi = 50°09'$ $\lambda = 23°08'$

I	–	–	–	–	-1.4	-10.9	6.6	4	-27.2	27	-7.2	-2.6	-6.7	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	5.9	5.5	6.7
II	–	–	–	–	3.3	-1.5	9.5	28	-6.3	7	-0.6	2.3	0.4	0.6	5.6	6.4	6.0	6.0	9.5	8.9	9.5	9.3	0.3	0.9	0.3	0.5	9.5	8.5	7.4	8.5
III	–	–	–	–	9.2	1.0	18.7	18	-5.3	23	3.0	7.6	4.5	4.9	7.0	7.3	7.2	7.2	9.2	7.0	8.5	8.2	0.7	3.5	1.5	1.9	8.7	8.5	4.9	7.4
IV	–	–	–	–	17.0	3.7	25.3	15	-4.3	10	6.8	15.4	9.3	10.2	8.4	9.1	9.0	8.8	8.3	5.2	7.6	7.0	1.7	9.2	2.9	4.6	5.9	6.1	3.9	5.3
V	–	–	–	–	17.1	5.5	25.3	29	-0.9	17	9.8	15.7	10.4	11.6	11.2	11.3	11.4	11.3	9.2	6.5	8.9	8.2	1.1	7.2	1.6	3.3	8.1	8.2	6.1	7.5
VI	–	–	–	–	24.1	10.6	31.8	27	4.6	21	16.2	22.3	16.0	17.6	15.8	15.9	16.1	15.9	8.5	6.0	8.8	7.8	2.9	11.8	2.3	5.7	5.2	6.1	6.3	5.9
VII	–	–	–	–	23.2	9.8	31.5	4	5.4	19	14.7	21.5	15.2	16.6	14.6	13.9	14.9	14.5	8.7	5.5	8.6	7.6	2.3	12.4	2.6	5.8	5.5	6.3	6.0	5.9
VIII	–	–	–	–	23.0	10.9	33.7	11	3.0	31	14.3	21.7	15.8	16.9	15.2	15.2	15.8	15.4	9.2	5.9	8.7	7.9	1.4	11.7	2.5	5.2	5.7	6.3	5.2	5.7
IX	–	–	–	–	21.3	6.6	29.5	18	-3.3	23	9.7	20.1	12.1	13.5	11.8	13.1	12.8	12.6	9.5	5.6	8.8	8.0	0.8	11.2	1.7	4.6	5.4	5.6	3.2	4.7
X	–	–	–	–	16.3	3.9	22.3	19	-2.3	13	5.9	15.7	8.8	9.8	8.5	9.7	9.1	9.1	9.1	5.5	8.0	7.5	1.0	8.5	2.4	4.0	6.2	5.7	4.0	5.3
XI	–	–	–	–	7.7	0.7	15.6	3	-9.5	23	3.2	6.8	3.9	4.4	7.7	8.6	7.8	8.0	9.4	8.4	9.4	9.1	0.5	1.7	0.6	0.9	8.7	8.5	7.5	8.2
XII	–	–	–	–	-0.5	-9.2	16.6	5	-32.0	25	-5.0	-2.1	-4.8	-4.2	4.4	5.1	4.6	4.7	8.5	8.6	9.0	8.7	0.6	1.1	0.7	0.8	8.3	8.2	5.7	7.4
Rok	–	–	–	–	13.4	2.6	33.7	11.VIII	-32.0	25.XII	5.9	12.0	7.1	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	5.5	6.6

Trzebinia

$H_s = 320\,m$ $h_w = 14{,}9\,m$ **1961**

MIESIĄC	ROZKŁAD WIATRU (°D, °mD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Min < 0°	Min ≤ 0°	Max ≥ 25°	Wiatr v ≥ 10	v ≥ 15	●	●	Opad R ≥ 0,1	≥ 1,0	≥ 10,0	≡	▦	≈
I	35	1,1	1,5	2,3	2,5	2,1	5	1,8	3	4,3	7	3,2	20,5	1,9	8,5	1,3	1,9	1,7	25,8	14,0	4	10	14	26	·	1	·	7	15	8	6	1	3	16	·
II	1,5	2,3	1	2,0	9,5	1,9	1,5	1,7	1	1,0	4,5	1,8	25	1,9	13	2,1	2,7	1,3	57,1	18,9	9	·	·	14	·	·	·	3	16	16	9	1	8	4	·
III	1,5	4,3	·	·	·	·	·	·	·	·	9,5	6,3	43,5	3,0	34,5	3,8	4	3,5	67,4	10,6	21	·	·	6	·	3	1	1	16	15	13	1	5	4	1
IV	4,5	2,9	5	3,3	24,5	4,7	4	2,5	1,5	1,3	6,5	4,2	13	2,2	9	2,8	2,2	2,6	23,0	7,0	1,8	·	·	2	·	3	2	6	6	6	5	·	·	·	1
V	14,5	1,6	5,5	1,9	8	2,3	·	·	·	·	4,5	2,6	18,5	2,7	19	1,9	2,3	1,6	91,5	24,0	3	·	·	·	·	·	·	·	15	15	14	3	1	·	6
VI	4,5	1,4	·	·	2,0,5	1,6	1,5	1,7	·	·	5	3,2	14	2,4	22,5	2,0	2,2	1,5	86,4	38,0	27	·	·	·	8	·	·	4	5	14	12	1	1	·	6
VII	2,5	3,2	·	·	·	·	1,5	1,0	1,5	1,0	9,5	2,6	36,5	2,8	22,5	2,8	1,9	2,2	133,3	33,5	13	·	·	·	7	·	·	2	5	15	11	5	·	·	4
VIII	7	1,5	1	1,5	8	1,0	1,5	1,0	·	·	9	1,9	31	1,9	15,5	1,8	2,0	1,4	121,7	64,0	9	·	·	·	7	·	·	4	8	10	8	3	2	·	2
IX	2,5	1,2	2,5	3,0	17,5	2,9	4	4,2	0,5	1,0	6	3,3	22	2,8	10	2,3	2,5	2,0	46,2	28,0	4	·	·	·	6	3	·	10	9	8	7	1	3	·	1
X	2,5	1,4	·	·	3,3	4,0	8,5	3,8	2,5	6,6	5,5	2,3	9,5	1,6	9,5	2,1	2,2	2,5	4,1	1,4	1,4	·	·	·	·	3	·	4	8	6	2	·	7	·	·
XI	5,5	1,7	1	2,5	10	2,3	4	4,6	·	·	2,5	3,0	22,5	2,4	27,5	2,1	1,7	1,9	77,9	25,4	13	·	1	9	·	1	·	3	14	17	10	2	11	1	·
XII	2	1,7	1,5	4,3	12,5	3,0	·	·	·	·	6	6,7	6,5	8,2	32,5	3,3	3,2	2,7	58,8	20,2	6	11	18	25	·	4	2	2	11	16	7	2	8	22	·
Rok	52	2,0	19	1,7	168,5	2,2	31,5	1,9	10	1,3	75,5	3,4	262,5	2,8	224	2,4	25,2	2,1	793,2	64,0	9.VIII	21	33	82	28	18	5	46	128	146	104	20	49	47	21

Biały Kościół

$H_s = 400\,m$ $h_w = 18{,}5\,m$

I	·	·	3	1,0	24,5	4,3	7,5	1,1	9	1,0	10,5	1,0	28,5	1,5	·	·	1,0	1,1	84,3	21	4,23	11	16	30	·	·	·	-	-	6	4	·	1	15	·
II	3	1,0	·	·	3	1,0	1,7	1,2	2	1,5	4	1,0	5,4	1,2	·	·	1	1,2	46,1	12,6	2,8	·	1	24	·	·	·	2	9	10	7	2	3	·	·
III	1	1,0	·	·	·	·	·	·	·	·	1	1,0	8,9	4,0	2	10,5	·	4,1	55,2	13,8	1,8	·	·	6	·	3	1	1	16	14	13	1	2	2	1
IV	6	1,0	·	·	2,4	2,6	9	1,9	1	1,0	2,1	1,3	20	2,2	5	2,0	4	1,9	20,4	5,8	8	·	·	2	1	·	·	3	4	7	6	·	·	·	2
V	1,4	1,0	1,1	1,2	1,2	1,4	1,3	1,2	·	·	7	1,4	2,5	2,0	5	2,0	5	1,4	85,1	26,8	2,9	·	·	·	·	·	·	2	8	18	11	2	1	·	8
VI	4	1,2	7	1,3	2,1	1,6	7,5	1,7	9,5	1,4	5	1,2	3,4	1,8	1	3,0	1	1,6	88,8	30,3	11	·	·	·	4	·	·	2	3	13	11	3	1	·	12
VII	1	1,0	·	·	·	·	1,5	2,0	4,5	2,2	2,8	2,1	4,6	2,1	7	2,6	5	2,0	162,5	38,5	1,3	·	·	·	7	·	·	1	9	18	15	6	·	·	7
VIII	5	2,4	·	·	6	1,3	·	·	3	1,0	1,0	1,4	5,1,5	2,1	8,5	2,1	9	1,7	133,2	63,7	9	·	·	·	6	·	·	3	5	9	8	3	1	·	2
IX	3	1,0	·	·	2,7	1,3	·	·	5	1,0	6	1,0	3,9	1,6	·	·	1,0	1,3	12,6	3,4	2,9	·	·	·	5	·	·	1,0	2	8	7	·	5	·	5
X	·	·	0,5	5,0	3,4,5	1,4	1,0	1,4	6	1,2	1,8	1,1	1,3	1,5	8	1,0	3	1,3	4,2	2,8	3,0	·	·	·	·	·	·	3	5	3	2	·	1	·	·
XI	1	2,0	2	1,0	1,9	1,2	1,6	1,4	1	1,0	12,5	3,0	3,5,5	2,1	3	2,0	·	1,9	94,6	27,3	1,3	·	·	11	·	·	·	·	16	12	8	4	4	1	·
XII	10,5	1,3	6,5	1,5	1,6	1,1	·	·	·	·	·	·	4,0	1,9	2	1,0	1,8	1,3	99,3	26,7,4	7	12	20	27	·	·	·	3	13	14	8	5	·	22	·
Rok	48,5	1,1	30	0,9	18,7	1,2	8,1,5	1,0	41	0,9	12,3	1,3	4,7,6,5	2,0	41,5	2,2	6,6	1,7	810,4,3	63,7,4	9.VIII	23	37	100	23	3	1	-	-	132	100	26	19	40	37

Gorlica Murowana

$H_s = 270\,m$ $h_w = 15{,}9\,m$

I	4,5	1,8	1,6	2,6	8,5	2,9	4	4,2	·	·	6	2,8	15,5	3,4	2,5	5,2	3,6	1,9	21,4	5,9	4	13	16	28	·	1	·	5	13	12	6	·	4	2,5	·
II	1	1,0	5	1,6	1,3	2,3	6	2,2	3,5	1,7	8,5	2,0	17,5	2,8	4,5	3,7	2,5	1,7	23,5	6,7	9	·	·	22	·	·	·	1	17	9	5	·	3	·	·
III	3,5	2,7	·	·	·	·	0,5	1,0	1,5	6,3	11,5	4,2	50,5	4,9	16,5	4,6	9	4,2	31,8	5,5	1,8	·	·	6	·	2	·	2	15	16	10	·	·	5	1
IV	6,5	3,0	1,4	2,8	2,2	5,0	7	4,2	1,5	2,0	8,5	3,5	10,5	4,2	3	6,0	1,7	3,3	9,8	3,3	1	·	·	1	1	·	·	9	3	6	4	·	·	·	2
V	12,5	3,1	8	2,6	8	2,8	3,5	2,4	4	2,8	8	3,4	21,5	2,6	8,5	3,2	1,9	2,3	98,9	23,5	2,9	·	·	·	·	·	·	·	11	18	13	4	1	·	10
VI	8,5	1,1	3	1,7	1,5	2,5	7	2,1	2,5	4,4	5,5	2,2	1,9	2,9	7,5	2,3	2,2	1,8	118,6	59,4	2,7	·	·	·	6	·	·	6	9	15	11	2	2	·	11
VII	4	2,6	0,5	3,0	1,5	1,7	2	1,8	1	1,5	1,3	2,7	3,0	3,5	9	2,7	3,2	2,0	101,0	22,3	3,0	·	·	·	7	1	·	3	12	15	12	3	·	·	5
VIII	7,5	2,5	2,5	2,0	3,5	2,3	1	2,0	0,5	1,0	13,5	3,4	2,5	3,0	5,5	3,5	3,4	1,9	100,6	56,2	9	·	·	·	7	·	·	4	7	12	9	3	·	·	3
IX	4	2,5	7,5	2,7	1,1	3,0	3,5	2,7	0,5	2,0	4,5	2,1	2,3,5	4,1	1,5	3,3	3,4	2,1	12,6	3,4	2,6	·	·	·	6	·	·	1,1	7	8	4	·	6	·	2
X	4	2,8	2,5	3,6	2,8,5	3,6	1,1,5	4,3	0,5	1,0	4	2,5	1,0	3,0	5	3,3	2,7	2,5	3,7	3,0	3,0	·	·	·	·	·	·	6	7	3	1	·	2	·	·
XI	7	2,6	3,5	1,4	1,1	3,7	4	1,8	0,5	3,0	9	2,6	2,0,5	3,5	6,5	3,2	2,8	2,1	73,3	18,5	4	·	·	8	·	·	·	3	17	17	9	2	4	1	·
XII	1,7	3,5	9	3,6	3	3,0	·	·	·	·	9	3,9	1,3,5	4,9	9,5	3,7	3,2	2,5	56,9	24,7	6	14	18	27	·	·	·	2	15	10	6	2	1	24	·
Rok	80	2,4	7,1,5	2,3	12,5	2,7	50	2,4	16	2,1	10,1	2,9	25,7	3,6	7,9,5	3,7	3,1,5	2,4	652,1	59,4	27.VI	27	34	92	27	4	·	52	133	141	90	16	23	55	34

Lubaczów

$H_s = 214\,m$ $h_w = 16\,m$

I	5,5	1,8	5	1,6	9	1,2	1,8	2,1	1,1	1,3	7	2,1	1,8	2,8	7,5	2,8	1,2	1,8	15,1	5,6	3,1	14	17	30	·	·	·	·	10	12	4	·	2	29	·
II	4,5	1,6	·	·	4,5	1,2	1,1,5	2,5	12,5	1,8	3,5	1,3	3,1,5	2,2	9	1,4	7	1,8	19,8	5,9	1,0	·	·	20	·	·	·	·	19	14	7	·	6	4	·
III	·	·	·	·	·	·	·	·	2	2,5	8	3,4	6,3	3,9	1,7	3,9	3	3,7	22,7	3,8	2,8	·	·	11	·	2	2	1	13	17	7	·	1	2	1
IV	5	1,6	5	1,2	16,5	3,0	13,5	4,9	7,5	1,4	8,5	1,7	16,5	3,6	11,5	2,7	6	2,7	27,1	7,2	1	·	·	3	1	1	·	6	5	9	6	·	·	·	2
V	3,5	2,0	·	·	1,2	2,0	3	3,0	1,2	2,3	8	1,9	2,7,5	2,4	1,2	2,2	1,5	1,9	48,0	9,7	1,4	·	·	1	1	·	·	·	10	16	11	·	2	·	1
VI	3	2,3	4	1,8	8	2,2	9,5	2,2	8,5	1,8	1,0	2,0	2,7,5	1,7	1,3,5	2,2	6	1,8	71,3	21,7	3,1,2	·	·	·	1,2	·	·	2	4	10	9	2	·	·	5
VII	3	1,0	1	1,0	·	·	1,5	3,0	6,5	2,2	1,0,5	2,0	4,0,5	1,8	2,0	1,6	1,0	1,6	100,5	38,0	2,9	·	·	·	1,0	·	·	2	4	16	11	3	·	·	1
VIII	8	1,9	2	2,5	3,5	1,7	5,5	1,5	4	1,2	11,5	2,3	3,0,5	2,5	2,0	2,4	8	2,0	57,1	14,3	1,2	·	·	·	8	·	·	2	7	14	9	3	1	·	4
IX	1	3,0	2	1,0	9	1,7	5	1,6	3,5	1,9	1,2	2,0	2,6,5	2,3	1,0	2,2	2,1	1,6	20,7	10,8	7	·	·	2	9	·	·	1,0	8	7	5	1	1	·	1
X	4,5	1,7	2	2,0	1,4,5	2,2	3,4,5	3,6	1,4	2,1	2	1,5	6	2,2	6,5	2,1	9	2,4	17,1	11,0	3,0	·	·	4	·	·	·	6	8	3	3	1	2	·	·
XI	3	1,7	1	1,0	1,0	2,3	1,8,5	3,0	5,5	1,0	11,5	1,1	3,0,5	1,8	7	1,7	3	1,9	33,6	5,6	1,2	·	·	12	·	·	·	·	19	13	9	·	2	·	·
XII	1,2	1,8	3	1,3	8	1,8	1,2	1,7	6	2,7	1,4	2,6	1,6	2,2	1,4	2,6	8	2,0	45,5	10,8	1,1	12	16	24	·	·	·	1	16	16	7	1	1	22	·
Rok	53	1,7	25	1,1	95	1,6	132,5	2,4	93	1,8	106,5	2,0	33,4	2,4	14,8	2,3	10,8	2,1	478,5	38,0	29.VII	26	33	107	41	3	2	30	123	147	88	11	18	57	15?

Tychy — φ = 50°08' — λ = 18°59' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	-	-	-	-	0.4	-7.5	10.2	4	-19.9	27	-5.0	-0.6	-3.6	-3.2	-	-	-	-	-	-	-	-	-	-	-	-	8.8	5.5	6.4	6.9
II	-	-	-	-	5.2	-1.3	13.1	18	-9.0	6	0.1	4.2	1.6	1.9	-	-	-	-	-	-	-	-	-	-	-	-	8.1	6.8	7.2	7.4
III	-	-	-	-	9.9	2.2	19.9	10	-2.5	20	3.6	8.1	5.6	5.7	-	-	-	-	-	-	-	-	-	-	-	-	7.7	6.9	7.4	7.3
IV	-	-	-	-	17.8	4.8	25.7	15	-4.9	10	7.7	16.7	11.1	11.6	-	-	-	-	-	-	-	-	-	-	-	-	4.3	4.7	4.9	4.6
V	-	-	-	-	17.1	6.0	23.9	26	1.9	12	9.2	15.7	10.8	11.6	-	-	-	-	-	-	-	-	-	-	-	-	7.4	8.2	8.7	8.1
VI	-	-	-	-	23.7	10.9	32.2	27	5.9	17	15.3	21.9	16.6	17.6	-	-	-	-	-	-	-	-	-	-	-	-	4.7	7.2	5.8	5.9
VII	-	-	-	-	21.5	10.8	31.0	3	5.2	8	14.3	19.7	15.5	16.2	-	-	-	-	-	-	-	-	-	-	-	-	5.6	8.5	6.1	6.7
VIII	-	-	-	-	22.2	11.2	30.6	6	4.8	14	13.7	20.8	15.8	16.5	-	-	-	-	-	-	-	-	-	-	-	-	5.5	7.5	5.9	6.3
IX	-	-	-	-	21.8	8.5	30.2	17	1.1	12	10.6	20.8	13.6	14.6	-	-	-	-	-	-	-	-	-	-	-	-	4.6	4.6	4.4	4.5
X	-	-	-	-	16.7	5.2	22.0	5	-0.4	25	6.8	15.8	10.2	10.8	-	-	-	-	-	-	-	-	-	-	-	-	6.3	5.8	4.9	5.7
XI	-	-	-	-	7.1	-	15.2	3	-	-	2.5	5.9	3.2	3.7	-	-	-	-	-	-	-	-	-	-	-	-	8.2	6.8	8.4	7.8
XII	-	-	-	-	-0.4	-	17.6	5	-	-	-4.7	-2.0	-4.5	-3.9	-	-	-	-	-	-	-	-	-	-	-	-	9.4	6.5	7.8	7.9
Rok	-	-	-	-	13.6	-	32.2	27.VI	-	-	6.2	12.2	8.0	8.6	-	-	-	-	-	-	-	-	-	-	-	-	6.7	6.6	6.5	6.6

Rybnik — φ = 50°06' — λ = 18°33'

I	-	-	-	-	0.7	-5.9	9.9	4	-18.6	27	-4.4	-0.3	-3.1	-2.7	-	-	-	-	-	-	-	-	-	-	-	-	6.8	6.5	6.4	6.6
II	-	-	-	-	5.4	-0.1	12.5	18	-6.1	6	0.6	4.2	2.0	2.2	-	-	-	-	-	-	-	-	-	-	-	-	8.9	7.8	7.3	8.0
III	-	-	-	-	10.5	2.9	19.3	10	-2.2	20	3.9	8.8	6.1	6.2	-	-	-	-	-	-	-	-	-	-	-	-	8.1	6.8	7.1	7.3
IV	-	-	-	-	18.2	5.7	24.8	7,15	-2.0	10	8.9	16.9	11.2	12.0	-	-	-	-	-	-	-	-	-	-	-	-	5.0	5.2	5.7	5.3
V	-	-	-	-	16.8	6.9	23.3	26	2.8	2	9.9	15.0	10.9	11.7	-	-	-	-	-	-	-	-	-	-	-	-	8.0	7.6	8.5	8.0
VI	-	-	-	-	23.3	12.1	30.6	27	6.5	16	15.4	21.2	16.8	17.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VII	-	-	-	-	21.2	11.8	30.4	3	7.0	8	14.6	19.4	15.5	16.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
VIII	-	-	-	-	22.3	12.1	30.6	10	6.8	14	14.2	21.0	16.5	17.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
IX	-	-	-	-	22.0	9.9	29.2	17	2.5	22	11.8	20.8	14.6	15.4	-	-	-	-	-	-	-	-	-	-	-	-	4.6	4.2	4.3	4.4
X	-	-	-	-	16.5	6.5	22.6	6	1.8	22	8.0	15.7	10.7	11.3	-	-	-	-	-	-	-	-	-	-	-	-	7.2	6.0	5.3	6.2
XI	-	-	-	-	7.1	1.9	14.3	3	-3.6	21	3.2	6.4	4.2	4.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
XII	-	-	-	-	0.5	-6.4	16.8	5	-22.4	26	-3.2	-0.9	-3.2	-2.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Rok	-	-	-	-	13.7	4.8	30.6	27.VI,10VII	-22.4	26.XII	6.9	12.4	8.5	9.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Rzeszów-Jasionka — φ = 50°06' — λ = 22°03'

I	996.7	1016.6	978.6	1022.5	-0.9	-9.3	9.3	4.5	-26.4	27	-6.1	-2.1	-4.9	-4.5	3.9	4.5	4.1	4.2	87	81	86	85	0.6	1.1	0.8	0.8	6.9	5.8	5.1	5.9
II	998.8	1012.9	970.6	1024.2	4.0	-1.0	10.8	18	-5.3	5	0.0	3.3	1.0	1.3	5.7	6.2	5.9	5.9	92	79	89	87	0.5	1.6	0.7	0.9	7.9	7.5	6.8	7.4
III	993.8	1011.1	973.5	1018.7	9.5	4.7	17.5	18	-3.4	21	3.7	7.9	4.7	5.2	7.1	7.3	7.2	7.2	88	69	84	80	1.0	3.7	1.6	2.1	8.5	8.0	5.8	7.4
IV	989.5	998.2	981.4	1013.9	17.1	3.9	24.8	15	-3.9	10	7.1	15.6	9.6	10.5	8.6	9.1	9.4	9.0	84	51	77	71	1.8	9.3	2.9	4.7	6.3	6.4	3.8	5.5
V	988.5	996.4	974.3	1012.7	17.0	5.9	25.2	29	0.6	20	9.7	15.3	10.4	11.4	10.9	11.1	11.2	11.1	89	64	87	80	1.3	6.9	1.7	3.3	7.7	7.9	5.5	7.0
VI	991.9	1004.7	982.4	1015.6	24.2	10.8	31.3	27	4.3	21	16.1	22.6	16.1	17.7	15.6	15.0	15.5	15.4	85	56	84	75	2.9	13.0	3.0	6.3	4.9	6.0	5.2	5.4
VII	991.0	1002.0	977.8	1014.8	23.0	10.5	31.8	4	6.1	9	15.2	21.3	15.3	16.8	14.2	13.3	14.9	14.1	82	54	85	74	3.2	12.8	2.7	6.2	5.3	6.6	6.2	6.0
VIII	993.3	1005.4	983.0	1017.1	23.2	11.9	33.4	11	5.9	31	15.1	21.8	16.3	17.4	15.2	15.5	16.4	15.7	88	59	87	78	2.3	11.4	2.8	5.4	5.6	6.0	5.6	5.7
IX	996.1	1006.5	984.7	1020.2	21.7	7.5	29.5	18	-2.1	22	10.6	20.6	12.9	14.2	11.7	12.2	12.2	12.0	90	50	81	74	1.7	12.7	3.0	5.8	4.9	4.8	3.3	4.3
X	996.5	1008.2	975.2	1021.0	16.8	4.4	24.0	19	-0.4	24	6.8	15.7	9.8	10.5	8.8	10.0	9.6	9.5	89	58	80	76	1.4	8.2	2.7	4.1	5.9	5.4	3.7	5.0
XI	991.0	1011.5	979.0	1015.8	8.0	2.2	14.2	3	-5.9	21	3.9	6.9	4.8	5.1	7.7	8.3	7.9	8.0	92	84	88	87	0.7	2.0	1.1	1.3	7.9	8.4	7.4	7.9
XII	991.8	1017.3	973.8	1017.5	-0.3	-8.3	13.6	5	-29.6	26	-4.9	-2.0	-4.3	-3.8	4.6	5.1	4.7	4.8	88	84	88	87	0.7	1.1	0.7	0.8	7.2	7.3	6.2	6.9
Rok	993.2	1017.3	970.6	1017.9	13.6	3.4	33.4	11.VIII	-29.6	26.XII	6.4	12.2	7.6	8.4	9.5	9.8	9.9	9.7	88	66	85	80	1.5	7.0	2.0	3.5	6.6	6.7	5.4	6.2

Racibórz — φ = 50°05' — λ = 18°13'

I	996.7	1018.3	975.2	1021.2	1.2	-5.9	9.8	4	-19.3	27	-4.0	0.0	-2.8	-2.4	4.2	4.5	4.4	4.4	86	71	83	80	0.7	1.9	0.9	1.2	6.7	5.7	5.8	6.1
II	999.6	1014.7	970.0	1023.8	5.9	-0.5	13.1	18	-6.2	6	0.7	4.8	1.9	2.3	5.9	6.4	6.1	6.1	90	75	87	84	0.6	2.2	0.9	1.2	7.7	7.0	5.2	6.6
III	996.9	1015.2	972.9	1020.7	11.4	1.9	21.8	10	-2.0	20	3.6	9.8	5.5	6.1	6.8	6.9	7.4	7.0	86	58	81	75	1.2	5.6	1.9	2.9	7.7	6.3	5.9	6.6
IV	989.4	998.8	982.4	1012.5	18.6	4.9	27.3	7	-1.9	10	7.7	17.3	11.0	11.8	8.8	8.8	9.5	9.0	82	46	72	67	1.9	11.7	3.8	5.8	4.8	5.6	4.3	4.9
V	990.0	997.4	976.2	1013.1	17.7	7.0	24.5	26	2.7	13	9.9	15.9	10.7	11.8	10.2	9.9	10.5	10.2	82	55	83	73	2.2	8.7	2.2	4.4	7.2	7.6	7.3	7.4
VI	993.1	1007.5	981.5	1015.9	23.8	11.6	31.3	27	5.3	21	15.3	21.5	16.7	17.6	14.5	14.4	15.8	14.9	83	58	83	75	3.0	11.7	3.4	6.0	4.9	5.8	5.9	5.5
VII	992.3	1003.7	976.8	1015.1	21.9	11.2	31.8	3	7.4	8	14.6	19.9	14.8	16.0	14.1	14.2	14.8	14.4	84	63	87	78	2.7	9.8	2.3	4.9	6.4	7.1	5.8	6.4
VIII	994.8	1006.9	984.8	1017.7	22.9	11.5	30.6	10	7.3	4	14.4	21.2	15.5	16.6	14.6	15.4	15.4	15.1	88	61	86	78	2.1	10.4	2.5	5.0	5.9	6.7	4.1	5.6
IX	996.6	1007.7	985.4	1019.7	22.7	8.4	29.6	2,18	4.0	23	11.2	21.5	13.3	14.8	12.0	13.3	13.2	12.8	89	53	85	76	1.6	13.1	2.4	5.7	4.8	4.4	3.1	4.1
X	995.5	1008.3	967.9	1018.9	17.1	5.7	23.1	11	0.4	16	7.2	16.0	10.1	10.8	9.3	10.4	10.1	9.9	91	58	82	77	1.0	8.2	2.4	3.9	7.1	6.1	4.2	5.8
XI	991.7	1014.0	978.2	1015.5	7.6	1.4	14.3	3	-4.5	21	2.9	6.5	3.9	4.3	6.9	7.1	7.1	7.0	90	73	86	83	0.8	2.7	1.1	1.5	7.7	7.8	7.0	7.5
XII	993.4	1019.3	976.0	1017.9	1.0	-6.3	17.3	5	-24.1	25	-3.1	-1.0	-3.0	-2.5	4.8	4.8	4.7	4.8	85	76	83	81	0.9	1.8	1.0	1.2	8.1	6.3	6.9	7.1
Rok	994.2	1019.3	967.9	1017.7	14.3	4.2	31.8	3.VII	-24.1	25.XII	6.7	12.8	8.1	8.9	9.3	9.7	9.9	9.6	86	62	83	77	1.6	7.3	2.1	3.7	6.6	6.4	5.5	6.2

Tychy

$H_s = 280\,m$ $h_w = 15{,}5\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25	Wiatr v ≥10	v ≥15	☁	●	Opad R ≥0,1	≥1,0	≥10,0	≡	▦	≈
I	1	3,0	5,5	2,6	12	4,2	4,5	3,3	3	2,7	21	3,3	14	3,4	5	3,6	27	2,4	24,3	9,3	14	11	14	28	·	·	·	1	14	6	–	–	6	17	–
II	1	2,0	·	·	4	2,2	5	3,0	3	2,7	18,5	3,1	13,5	3,6	7	4,8	32	2,0	74,9	22,1	1	·	·	19	·	·	·	2	17	10	8	3	12	2	–
III	·	·	·	·	·	·	·	·	·	·	19	3,6	37	3,5	28	4,9	9	3,6	50,3	9,2	14	·	·	5	·	3	·	2	18	13	13	·	4	1	–
IV	3	2,3	2	3,5	22,5	4,4	6,5	3,0	4	2,8	14	3,4	7	2,6	9	3,3	22	2,7	16,4	7,3	2	·	·	1	2	1	·	9	6	4	4	·	1	·	–
V	6	2,2	6,5	2,8	2	5,0	0,5	2,0	3,5	2,1	4	2,2	22,5	3,0	20	3,7	28	2,2	47,5	8,7	8	·	·	·	·	1	·	·	18	13	12	·	3	·	–
VI	1	2,0	1	2,0	8	2,5	7	3,0	·	·	5,5	3,3	14,5	3,7	13	3,4	40	1,8	74,9	30,5	27	·	·	·	9	·	·	3	10	11	10	1	5	·	–
VII	3	2,0	·	·	·	·	1	3,0	·	·	12,5	2,6	25,5	3,3	14	2,9	37	1,8	115,4	29,5	30	·	·	·	7	·	·	1	11	13	11	4	·	·	–
VIII	2,5	2,0	3	2,3	2	3,0	·	·	·	·	10,5	2,9	21,5	3,0	16,5	2,7	37	1,7	68,8	24,0	12	·	·	·	7	·	·	4	11	9	9	2	2	·	–
IX	·	·	·	·	16,5	2,9	2,5	2,4	·	·	7,5	2,4	16	2,9	7,5	3,5	40	1,6	14,3	7,7	14	·	·	·	7	·	·	10	7	5	4	·	6	·	–
X	4	2,2	0,5	2,0	14,5	4,6	7	3,0	4	2,8	5,5	2,9	7,5	2,8	9	2,7	41	1,8	23	14	2,9	·	·	1	·	·	·	5	10	2	1	·	10	·	–
XI	7	2,0	·	·	6	3,3	·	·	1	3,0	8,5	4,1	17,5	2,8	6	2,8	44	1,5	85,0	30,3	4	·	·	·	·	·	·	·	19	11	10	2	11	2	–
XII	6,5	2,3	4	3,2	1	2,0	2	3,0	·	·	12,5	3,8	11,5	3,3	11,5	3,6	44	1,7	65,6	20,5	6	–	17	–	·	·	·	·	18	11	10	2	7	2,1	–
Rok	3,5	1,8	22,5	1,5	88,5	2,8	36	2,1	18,5	1,3	139	3,1	208	3,2	446,5	3,4	401	2,1	639,7	30,5	27.VI	–	31	–	32	5	·	37	159	108	–	–	67	43	–

Rybnik

$H_s = 243\,m$ $h_w = 11{,}5\,m$

I	2	1,0	1,6	2,4	5	1,2	3	1,0	2	2,0	3,6	4,8	5	1,6	4	1,0	2,0	2,5	12,5	4,1	14	9	14	25	·	3	3	–	–	8	4	·	·	2,0	·
II	·	·	2	1,5	2	1,5	3	3,0	2	1,5	3,8	3,8	13	2,5	3	2,3	2,1	2,3	49,4	13,6	1	·	·	13	·	2	1	–	–	14	9	2	8	4	·
III	·	·	·	·	·	·	·	·	·	·	3,7	4,1	3,7	3,1	10	3,8	9	3,3	56,3	17,6	18	·	·	5	·	2	1	–	–	14	8	2	4	1	2
IV	4	3,0	11	3,6	12	3,8	2	2,0	3	2,7	25,5	3,6	7,5	2,5	7	1,7	18	2,6	7,8	3,3	1	·	·	1	·	4	1	–	–	4	3	·	1	·	·
V	2	2,5	2	4,5	·	·	·	·	1	2,0	2,0	3,4	18,5	2,0	23,5	2,9	26	2,0	49,7	7,9	8	·	·	·	·	·	·	–	–	13	12	·	·	·	6
VI	2	2,0	1	1,0	3	2,0	3	2,0	·	·	2,3	2,7	2,4	2,1	1,3	3,4	21	1,9	140,8	57,4	27	·	·	·	8	1	·	–	–	12	11	5	1	·	8
VII	1	2,0	·	·	0,5	2,0	0,5	2,0	3	4,3	28,5	2,4	28,5	2,2	9	2,1	22	1,8	128,5	36,7	15	·	·	·	7	1	·	–	–	14	14	3	·	·	3
VIII	4,5	1,8	1,5	2,0	1	2,0	·	·	1	1,0	2,4	3,2	2,7	2,5	1,0	1,7	24	1,8	37,8	18,3	12	·	·	·	7	·	·	–	–	10	9	1	·	·	·
IX	3	1,7	1,2	2,8	1	2,0	3	2,0	1	5,0	2,7	2,9	1,2	1,9	6	1,8	2,5	1,8	14,6	6,2	14	·	·	·	7	·	·	–	–	5	4	·	2	·	1
X	3	1,3	8	4,9	12,5	2,2	7,5	2,3	5	2,6	16,5	2,7	11	1,6	6,5	1,6	2,3	1,9	9,9	4,7	1,9	·	·	·	·	2	·	–	–	5	3	·	3	·	·
XI	4	1,0	5	1,2	3	3,0	·	·	2	4,5	29,5	2,4	10,5	1,7	1,3	1,6	2,3	1,5	57,5	16,3	4	·	·	6	·	·	·	–	–	13	10	2	4	2	·
XII	7	2,3	4	1,5	2	1,0	2	1,0	2	1,5	3,1	4,8	9	1,7	2,0	2,1	1,6	2,5	53,9	19,6	11	9	13	24	·	2	1	–	–	12	6	2	1	2,0	·
Rok	3,2,5	1,6	6,2,5	2,1	4,2	1,7	2,4	1,3	2,2	2,3	3,3,6	3,4	2,0,3	2,1	1,2,5	2,2	2,4,8	2,2	6,1,8,7	5,7,1	27.VI	1,8	2,7	7,4	2,9	1,7	7	–	–	1,2,4	9,3	1,7	2,4	4,7	2,0

Rzeszów - Jasionka

$H_s = 200\,m$ $H_b = 201{,}7\,m$ $h_w = 16\,m$

I	2	3,0	7,5	3,9	7,5	2,2	2,5	2,6	2,3	6,4	16	6,6	8,5	4,9	13	5,2	13	4,5	12,3	3,2	14	13	14	28	·	3	·	4	10	11	5	·	1	2,3	·
II	·	·	1	1,0	4,5	3,2	3	2,0	1,2	6,6	2,3	5,6	2,0	4,2	5,5	4,5	1,5	4,0	14,4	4,8	12	·	1	19	·	4	·	1	14	8	6	·	4	2	·
III	3	6,0	·	·	·	·	·	·	3	7,3	10,5	6,5	4,5,5	6,1	2,0	7,6	11	5,8	18,7	4,8	12	·	·	9	·	14	6	·	10	17	5	·	2	1	·
IV	4	3,8	2	4,0	2,3,5	6,3	4,5	6,7	5,5	4,0	11	5,2	11	4,8	4,5	7,3	2,4	4,1	12,4	5,7	8	·	·	3	·	10	1	6	4	5	3	·	2	·	2
V	6,5	2,1	2	1,5	16	2,9	1	2,0	6,5	4,0	4,5	3,1	2,7,5	4,4	11	4,3	18	2,9	55,8	24,6	14	·	·	·	1	4	·	·	8	12	7	1	3	·	3
VI	4,5	3,9	3	2,8	10,5	4,1	6	2,6	1,3	3,5	11	3,4	23	3,7	11	3,8	8	3,3	33,7	6,8	3	·	·	·	11	1	·	1	6	13	10	·	2	·	7
VII	3,5	4,0	1	1,0	3	2,3	3	2,3	1,3	3,2	16	3,6	4,1,5	4,0	1,0	4,3	2	3,6	84,6	28,0	29	·	·	·	9	2	·	2	6	17	9	3	·	·	5
VIII	4,5	4,2	1,5	2,7	7	2,6	2,5	3,0	1,1,5	3,3	18,5	4,0	2,6	4,3	13,5	4,8	8	3,6	66,2	19,3	12	·	·	·	8	2	·	3	5	10	8	4	1	·	6
IX	2,5	1,8	4	3,2	1,6	3,0	1	3,0	8	3,2	17,5	3,4	2,0	4,1	4	4,0	1,7	2,8	10,0	2,9	6	·	·	2	8	2	·	12	6	7	6	·	4	·	1
X	1,5	3,7	6	3,6	4,0	4,7	4,5	4,4	1,4	5,2	5,5	3,8	1,0	3,8	4,5	4,8	7	4,2	21,6	14,2	30	·	·	2	·	2	·	8	6	5	5	1	3	·	·
XI	3	3,0	2,5	5,0	1,5	5,7	6	2,8	1,3,5	4,3	16,5	3,4	23	4,3	7,5	3,9	3	4,1	38,9	9,8	13	·	·	9	·	1	·	1	19	18	10	·	3	2	1
XII	9,5	5,2	5	3,5	1,3	3,2	0,5	3,0	1,3,5	6,3	16,5	5,9	1,4	5,3	1,5	5,3	6	4,8	37,7	12,6	11	12	16	23	·	6	·	3	13	16	7	1	1	2,4	·
Rok	4,4,5	3,4	3,5,5	2,7	1,5,6	3,4	3,4,5	2,9	1,3,6,5	4,8	1,6,6,5	4,5	2,7,0	4,5	1,1,9,5	5,0	1,3,2	4,0	4,0,6,3	2,8,0	29.VII	2,5	3,1	9,5	3,7	5,1	7	4,1	10,7	13,9	8,1	1,0	2,6	5,2	2,5

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Racibórz

$H_s = 189\,m$ $H_b = 192{,}6\,m$ $h_w = 15\,m$ (I–IV), $12{,}5\,m$ (V–XII)

I	7,5	2,2	10,5	2,0	1	2,0	6,5	1,9	3,1	2,5	14,5	3,6	4,5	4,3	3,5	2,9	14	2,1	10,8	4,4	14	8	10	25	·	·	·	5	14	7	3	·	1	1,9	·
II	7	1,6	·	·	0,5	1,0	1,9,5	1,9	2,1,5	2,5	9,5	2,5	5,5	3,1	8,5	3,2	12	2,0	42,2	9,2	9	·	·	17	·	·	·	1	10	14	7	·	7	1	·
III	6,5	2,6	·	·	·	·	2	1,0	8	2,5	9	2,6	17	3,5	3,3,5	3,5	17	2,6	43,7	11,0	18	·	·	9	·	1	·	2	14	15	10	1	1	2	·
IV	8	2,2	10	2,0	12,5	2,0	6,5	2,4	17	2,9	8,5	3,7	4	1,9	3,5	3,4	2,0	2,0	53	2,5	1	·	·	1	3	·	·	7	5	3	2	·	·	·	1
V	14,5	2,3	1,5	2,3	1	2,0	4	1,5	7	2,1	10	2,8	10,5	2,7	2,1,5	2,8	2,3	1,9	80,6	33,1	29	·	·	·	·	·	·	·	13	16	13	2	·	·	6
VI	10	1,3	3	1,7	0,5	1,0	6	1,3	15,5	2,0	9	2,4	7	1,8	1,4	2,5	2,5	1,4	94,3	29,3	27	·	·	·	8	·	·	4	8	12	11	3	2	·	12
VII	5,5	2,5	0,5	1,0	1	1,0	6,5	1,3	17,5	1,8	12,5	2,6	12	2,9	10,5	2,2	2,7	1,6	146,0	54,5	13	·	·	·	7	·	·	4	6	18	14	5	·	·	7
VIII	9,5	2,4	2	2,0	2	1,5	4	1,0	14	2,8	15,5	2,6	8,5	1,9	5,5	2,3	3,2	1,5	37,8	14,3	12	·	·	·	9	·	·	4	4	11	6	2	2	·	2
IX	4	1,9	2,5	2,4	2,5	2,2	9	1,6	17	2,4	11	2,4	2	1,8	6	2,8	3,6	1,3	18,6	7,6	6	·	·	·	10	·	·	11	4	7	5	·	3	·	2
X	4,5	2,0	2	3,5	1,0	3,1	1,1	1,9	14,5	3,3	9	2,8	2	1,8	5	2,2	3,5	1,7	18,4	7,4	19	·	·	·	·	·	·	4	9	5	5	·	5	·	·
XI	1,0	2,4	4,5	1,9	2,9	2,2	1,0	1,8	18	2,2	18,5	2,3	3,5	4,1	8	2,9	1,5	2,0	47,7	11,3	4	·	·	9	·	·	·	1	17	12	8	2	5	2	·
XII	2,6	2,5	3,5	2,0	·	·	1,0,5	1,5	11	3,0	2,0,5	3,1	1,5	3,7	9	2,6	1,1	2,3	54,7	16,0	11	1,0	1,4	2,4	·	·	·	2	1,4	1,5	9	2	1	2,2	·
Rok	1,1,3	2,2	4,0	1,7	3,3,5	1,9	9,5,5	1,6	1,9,2	2,5	1,4,2,6	2,8	7,8	2,5	1,2,8,5	2,8	2,6,7	1,9	6,0,0,1	5,1,5	13.VII	1,8	2,4	8,5	3,7	4	·	4,5	1,1,8	1,3,5	9,3	1,7	2,7	4,6	3,0

Bieruń Stary — φ = 50°05' — λ = 19°05' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T														ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																					
	P_m	Max	Min	$P_{o.m}$	$\overline{Max}$	$\overline{Min}$	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	991.2	1011.9	971.2	1021.6	1.0	−7.2	10.6	4	−19.1	28	−5.1	0.2	−3.9	−3.2	4.1	4.7	4.3	4.4	89	71	87	82	0.6	1.9	0.7	1.1	5.7	5.4	5.4	5.5
II	994.0	1009.3	964.8	1023.9	5.5	−1.1	13.6	18	−8.1	6	0.2	4.8	1.3	1.9	6.0	6.5	6.2	6.2	95	77	91	88	0.3	2.2	0.6	1.0	7.6	7.0	6.3	7.0
III	991.0	1008.4	967.6	1020.3	10.7	1.9	20.7	10	−2.9	20	3.9	9.3	5.2	5.9	7.3	7.2	7.7	7.4	90	63	84	79	0.9	4.9	1.6	2.5	7.0	7.1	6.2	6.8
IV	984.0	992.9	977.1	1012.4	18.9	4.2	26.4	7	−2.0	10	9.0	17.8	9.2	11.3	9.0	9.1	9.2	9.1	77	46	78	67	2.7	11.9	2.7	5.8	4.1	3.8	3.9	3.9
V	984.3	990.9	970.1	1012.7	18.1	5.8	24.8	7	1.5	2	10.6	16.1	9.3	11.3	10.9	10.9	10.9	10.9	84	60	92	79	2.7	8.0	1.0	3.9	7.2	7.0	5.0	6.4
VI	987.6	1001.6	976.8	1015.6	24.4	10.3	31.8	27	4.9	21	16.2	23.2	15.3	17.5	15.5	15.4	15.5	15.5	84	55	89	76	3.2	13.6	2.0	6.3	4.5	5.2	4.7	4.8
VII	986.9	998.0	972.3	1015.1	21.9	10.1	31.3	3	4.5	9	15.3	20.7	14.5	16.2	14.5	15.1	14.8	14.8	83	62	89	78	3.1	10.2	2.0	5.1	5.4	7.0	6.0	6.1
VIII	989.4	1001.5	979.6	1017.7	23.1	10.8	31.0	6	5.4	14	14.8	21.8	14.9	16.6	15.3	16.0	15.6	15.6	90	61	91	81	1.8	10.9	1.7	4.8	5.3	6.5	4.4	5.4
IX	991.3	1002.5	980.3	1019.8	22.3	7.8	30.3	17	1.0	12	10.7	21.1	12.5	14.2	12.3	13.7	13.4	13.1	93	56	91	80	1.1	12.2	1.4	4.9	4.6	4.2	3.3	4.0
X	990.4	1002.7	964.4	1019.3	17.5	5.0	22.3	6	−0.5	25	7.2	16.5	9.1	10.5	9.5	10.8	10.2	10.2	93	59	89	80	0.9	8.3	1.5	3.6	6.8	4.8	3.1	4.9
XI	986.2	1007.9	973.0	1015.7	7.8	0.3	16.9	3	−7.7	23	2.4	6.6	2.6	3.6	7.1	7.7	7.4	7.4	94	78	94	89	0.5	2.4	0.5	1.1	7.8	7.1	7.0	7.3
XII	987.6	1013.4	970.6	1018.0	−0.2	−8.2	18.2	5	−27.1	26	−4.6	−1.4	−4.9	−4.0	4.7	5.0	4.5	4.7	90	83	90	88	0.7	1.4	0.5	0.9	7.6	7.4	6.5	7.1
Rok	988.7	1013.4	964.4	1017.7	14.2	3.3	31.8	27.VI	−27.1	26.XII	6.7	13.1	7.1	8.5	9.7	10.2	10.0	10.0	88	64	89	80	1.5	7.3	1.4	3.4	6.1	6.0	5.2	5.8

Kraków - Czyżyny — φ = 50°05' — λ = 20°01'

I	994.3	1015.5	975.0	1021.5	−0.3	−8.9	8.9	31	−23.2	28	−6.4	−1.6	−4.9	−4.4	3.8	4.3	4.0	4.0	88	74	84	82	0.5	1.6	0.8	1.0	7.7	6.2	5.8	6.6
II	996.7	1011.4	967.2	1023.3	5.3	−1.3	14.1	18	−6.2	6	0.1	4.5	1.6	2.0	5.8	6.3	6.1	6.1	93	76	87	85	0.5	2.3	0.9	1.2	8.8	7.7	7.1	7.9
III	993.1	1010.7	971.0	1019.4	10.3	2.5	20.4	18	−1.7	22,23	4.1	8.7	5.9	6.2	6.9	6.9	7.2	7.0	83	62	77	74	1.5	4.8	2.3	2.9	7.6	7.5	6.2	7.1
IV	987.0	995.6	979.4	1012.6	17.9	4.3	26.0	15	−3.6	10	7.8	16.5	10.3	11.2	8.5	8.7	8.8	8.7	79	47	70	65	2.3	10.8	3.9	5.7	4.9	5.0	4.5	4.8
V	986.8	993.9	972.0	1012.3	17.2	6.5	24.1	6	2.4	3	9.9	15.5	11.0	11.8	10.3	10.6	10.8	10.6	83	60	81	75	2.1	7.6	2.5	4.1	6.9	7.5	7.1	7.2
VI	990.1	1003.9	979.4	1015.2	24.2	11.2	32.9	27	5.9	21	15.8	22.8	16.3	17.8	14.8	14.3	15.3	14.8	82	52	82	72	3.2	14.1	3.3	6.9	4.8	6.0	6.1	5.6
VII	989.4	1000.5	975.1	1014.7	22.0	11.2	31.2	3	5.8	8	14.9	20.3	15.6	16.6	13.9	13.4	14.3	13.9	81	57	80	73	3.3	11.3	3.8	6.1	6.1	7.1	5.7	6.3
VIII	991.9	1004.0	982.3	1017.1	22.8	11.3	32.1	11	6.5	31	14.6	21.6	16.1	17.1	14.7	14.8	15.3	14.9	87	57	82	75	2.2	11.9	3.4	5.8	5.2	6.0	4.7	5.3
IX	994.0	1005.0	982.6	1019.6	21.4	8.3	29.5	17	4.3	24	11.0	20.4	13.4	14.6	12.1	12.7	12.7	12.5	90	54	81	75	1.3	12.2	3.0	5.5	5.2	4.5	3.5	4.4
X	993.4	1005.6	968.6	1019.3	16.9	5.0	21.1	6	−1.1	25	7.0	16.1	9.9	10.7	8.8	10.2	9.6	9.5	88	57	79	75	1.5	8.4	2.8	4.2	6.1	5.9	3.6	5.2
XI	988.8	1010.8	975.8	1015.1	7.5	0.8	16.1	3	−7.1	24	2.5	6.5	3.5	4.0	7.0	7.6	7.2	7.3	92	78	89	86	0.7	2.4	0.9	1.3	7.6	7.6	7.2	7.5
XII	990.2	1016.2	972.7	1017.3	−0.4	−9.0	18.8	5	−29.5	26	−5.1	−2.3	−5.0	−4.4	4.4	4.7	4.2	4.4	87	80	85	84	0.7	1.5	0.8	1.0	7.9	6.6	6.4	7.0
Rok	991.3	1016.2	967.2	1017.3	13.7	3.5	32.9	27.VI	−29.5	26.XII	6.4	12.4	7.8	8.6	9.2	9.5	9.6	9.4	86	63	81	77	1.6	7.4	2.4	3.8	6.6	6.5	5.7	6.3

Kraków - Chełm — φ = 50°04' — λ = 19°51'

I	–	–	–	–	0.4	−9.0	10.5	4	−21.4	28	−5.4	−1.5	−4.0	−3.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.3	4.5	5.5
II	–	–	–	–	5.0	−1.0	13.0	28	−6.9	6	0.2	4.0	2.0	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.9	7.0	7.9
III	–	–	–	–	9.8	3.1	18.9	10,18	−1.4	23	4.2	8.2	6.0	6.1	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.3	6.8	7.4
IV	–	–	–	–	17.5	5.2	25.3	15	−1.3	10	8.0	16.5	11.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	3.7	4.3	3.7	3.9
V	–	–	–	–	16.8	6.9	23.8	27	3.5	12	9.8	15.5	11.2	11.5	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.9	6.9	6.9
VI	–	–	–	–	23.6	11.3	32.1	27	5.7	17	15.5	22.4	16.5	17.7	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.4	5.9	5.3
VII	–	–	–	–	21.6	11.2	31.0	3	6.1	8	14.6	19.9	15.5	16.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.1	7.1	6.8
VIII	–	–	–	–	22.4	11.7	31.8	11	7.2	14	14.4	21.4	15.9	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.5	4.3	5.1
IX	–	–	–	–	21.0	8.8	28.9	17	1.7	22,23	10.7	20.1	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.6	4.0	4.6
X	–	–	–	–	16.4	5.8	21.0	6	−0.3	25	7.3	15.5	10.0	10.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	5.3	4.0	5.6
XI	–	–	–	–	7.1	1.1	15.1	3	−5.8	23	2.8	6.2	3.4	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.1	7.6
XII	–	–	–	–	−0.2	−8.2	17.8	5	−27.8	26	−5.1	−2.3	−4.4	−4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.8	7.0	7.1
Rok	–	–	–	–	13.4	3.9	32.1	27.VI	−27.8	26.XII	6.4	12.2	8.1	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.2	5.7	6.2

Kraków, Obserw. Astr. UJ — φ = 50°04' — λ = 19°58'

I	993.1	1014.0	974.0	1021.3	0.3	−7.5	10.0	4	−21.6	27	−6.0	−1.4	−3.9	−3.8	3.9	4.5	4.3	4.2	88	78	88	85	0.5	1.5	0.7	0.9	7.9	6.9	6.9	7.2
II	995.5	1010.0	966.7	1023.1	5.5	−0.5	14.3	28	−5.9	6	0.4	4.4	2.2	2.3	5.9	6.2	6.3	6.1	94	74	87	85	0.4	2.4	1.0	1.3	8.8	8.0	7.7	8.2
III	991.9	1009.3	970.0	1018.9	10.7	3.2	20.6	18	−1.7	23	4.4	8.8	6.7	6.6	7.0	6.8	7.5	7.1	83	61	76	73	1.5	4.9	2.6	3.0	8.2	7.9	6.7	7.6
IV	985.9	994.2	978.5	1012.3	18.1	5.7	26.4	15	−1.8	10	7.9	16.7	11.5	11.9	8.4	8.2	9.0	8.5	77	44	66	62	2.5	11.5	4.8	6.3	5.5	5.5	5.5	5.5
V	985.7	992.4	971.2	1012.1	17.5	7.6	25.1	6	3.8	12	10.1	15.6	11.9	12.4	10.3	10.3	11.1	10.6	83	59	79	74	2.2	8.0	3.0	4.4	7.3	7.6	8.8	7.9
VI	988.9	1002.4	978.7	1014.9	24.5	12.4	33.5	27	7.2	21	16.0	22.9	17.2	18.3	14.6	14.0	15.7	14.8	80	51	80	70	3.7	14.6	4.0	7.4	5.1	6.0	6.7	5.9
VII	988.2	999.2	974.2	1014.3	22.6	12.0	31.7	3	7.3	8	15.2	20.6	16.3	17.1	13.9	13.1	14.6	13.9	80	55	78	71	3.6	12.0	4.2	6.6	6.7	7.3	5.9	6.6
VIII	990.7	1003.0	981.2	1016.7	23.2	12.1	33.2	11	7.7	31	15.0	21.9	16.7	17.6	14.7	14.7	15.8	15.1	85	56	82	74	2.7	12.5	3.6	6.3	5.8	6.3	5.4	5.8
IX	992.9	1003.7	981.5	1019.2	21.9	9.2	29.5	18	1.5	23	11.2	20.6	14.0	15.0	12.4	12.7	13.5	12.9	91	53	83	76	1.3	12.5	2.7	5.5	5.3	5.0	4.4	4.9
X	992.1	1004.3	967.8	1018.7	17.1	6.1	21.9	19	0.6	22	7.3	16.1	10.4	11.0	9.4	10.7	10.5	10.2	91	60	84	78	1.1	7.9	2.2	3.7	6.8	6.3	5.3	6.1
XI	987.6	1009.1	974.5	1014.8	7.7	1.5	16.4	3	−5.0	23	2.8	6.5	4.1	4.4	7.2	7.6	7.5	7.4	93	77	90	87	0.5	2.5	0.8	1.3	8.1	7.7	8.0	7.9
XII	989.8	1014.8	971.3	1017.2	−0.1	−7.4	18.2	5	−25.7	26	−4.5	−2.1	−4.2	−3.8	4.6	4.9	4.5	4.7	89	84	88	87	0.7	1.4	0.8	1.0	8.7	6.6	7.6	7.6
Rok	990.1	1014.8	966.7	1016.9	14.1	4.5	33.5	27.VI	−25.7	26.XII	6.6	12.6	8.6	9.1	9.4	9.5	10.0	9.6	86	63	82	77	1.7	7.6	2.5	3.9	7.0	6.8	6.6	6.8

Uwaga. Ciśnienie powietrza jest za niskie przeciętnie o ok. 0,4 mb.

Bieruń Stary

$H_s = 236\,m$ $H_b = 239{,}0\,m$ $h_w = 30\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU (%D, %nD) N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v >10	v >15	LICZBA DNI (n) ◔	●	Opad R ≥0.1	≥1.0	≥10.0	≡	▦	≈
I	2	2.0	1.5	4.0	14	2.1	1.5	2.0	1.5	3.0	18	3.1	10	2.4	3.5	1.7	41	1.4	23.2	9.0	4	11	11	28	·	·	·	8	10	11	7	·	2	2.0	·
II	·	·	·	·	3.5	1.7	1.5	1.3	1.5	2.7	20.5	2.7	19	2.9	6	2.6	32	1.5	47.2	14.0	9	·	·	17	·	·	·	3	13	16	7	2	8	4	·
III	·	·	·	·	·	·	·	·	·	·	27.5	3.9	35.5	3.4	17	4.2	13	3.2	49.2	8.5	14	·	·	6	·	·	·	5	15	18	12	·	2	5	1
IV	1.5	2.3	4.5	2.6	2.1	3.3	6	2.8	1.5	2.3	12	4.2	10.5	3.3	3	3.3	30	2.2	23.8	6.7	1	·	·	3	4	1	·	12	4	7	6	·	1	·	3
V	4.5	2.8	3.5	3.0	3	2.0	1	1.0	1	2.0	16.5	3.7	16	3.3	14.5	3.7	33	2.2	64.5	11.3	21	·	·	·	·	·	·	·	10	17	13	1	·	·	8
VI	·	·	3	2.0	4	2.8	1	2.0	0.5	2.0	9.5	3.1	16	3.7	10	3.4	46	1.6	96.1	57.0	27	·	·	·	14	·	·	7	5	12	10	1	2	·	10
VII	·	·	·	·	1	3.0	·	·	1.5	1.7	27	3.4	24	2.8	11.5	2.3	28	2.0	115.3	30.0	30	·	·	·	7	·	·	2	10	15	11	4	·	·	4
VIII	1	1.0	3.5	2.1	3.5	2.4	·	·	·	·	23.5	4.0	11.5	3.0	14	2.4	36	1.9	75.3	26.0	12	·	·	·	9	·	·	5	7	11	7	2	1	·	4
IX	0.5	3.0	5	2.2	6.5	2.8	4	2.9	·	·	12.5	3.0	11.5	2.9	3	2.8	47	1.3	9.8	5.5	14	·	·	·	8	·	·	11	5	7	2	·	4	·	1
X	1	1.5	1	5.5	2.3	2.8	3	2.5	5	3.6	7	3.1	2.5	3.0	5.5	1.7	45	1.5	2.7	1.5	2.9	·	·	1	·	·	·	5	5	3	1	·	9	·	·
XI	1.5	1.3	1	3.0	4	4.5	·	·	·	·	12.5	3.8	7.5	3.1	8.5	1.9	55	1.2	92.3	36.7	4	·	·	10	·	·	·	1	17	14	11	2	4	3	·
XII	4	2.8	1	1.0	3	1.7	·	·	·	·	11.5	6.4	10	3.5	8.5	3.4	55	1.7	68.9	26.0	6	11	15	27	·	2	·	3	12	17	7	3	2	2.4	·
Rok	16	1.4	2.4	2.1	86.5	2.4	18	1.2	12.5	1.4	198	3.7	174	3.1	105	2.8	461	1.8	668.3	57.0	27.VI	22	26	92	42	3	·	62	113	148	94	15	35	56	31

Kraków - Czyżyny

$H_s = 213\,m$ $H_b = 213{,}4\,m$ $h_w = 25\,m$

I	1.3	2.8	1.6	2.6	9.5	4.2	3	3.7	6.5	3.2	5	3.7	1.3	3.5	8	3.8	1.9	2.6	25.5	6.9	4	1.3	1.5	2.8	·	1	·	3	1.3	1.3	6	·	7	2.0	·
II	2.5	2.0	6	2.2	9.5	2.7	3	2.5	5.5	2.4	3.5	4.1	2.5	3.4	1.3	3.4	1.6	2.5	26.9	6.2	1.9	·	·	1.9	·	·	·	·	1.6	1.4	6	·	7	1	·
III	3	4.3	·	·	·	·	·	·	·	·	5	4.4	5.5.5	5.7	2.6.5	4.8	3	5.1	41.0	7.4	31	·	·	7	·	3	·	2	1.5	1.9	1.4	·	2	2	·
IV	4	3.5	7.5	3.3	2.9	4.4	9.5	4.7	2	3.0	6	3.1	1.5	4.2	9	3.8	8	3.7	13.0	7.5	1	·	·	1	3	2	·	8	4	7	3	·	1	·	1
V	10.5	4.4	9.5	2.8	12.5	3.1	3.5	1.4	3	3.2	3	3.7	2.6	3.9	1.5	3.2	1.0	3.1	117.1	18.5	2.9	·	·	·	·	·	·	·	1.1	1.6	1.5	6	2	·	8
VI	5	3.3	5	2.6	1.2	3.1	6	3.2	3	1.8	2.5	3.0	2.5	3.5	2.4.5	3.2	7	2.9	82.2	21.8	2.7	·	·	·	10	2	1	6	9	1.4	1.3	1	2	·	1.1
VII	3.5	4.0	3	2.3	2.5	1.4	4.5	1.8	1	2.5	10.5	2.9	4.0	4.3	2.0	3.2	8	3.2	127.7	2.8.5	3.0	·	·	·	8	·	·	3	8	1.5	1.3	4	·	·	7
VIII	3	4.5	7	3.5	2.5	4.0	1.5	1.3	3.5	1.1	7.5	3.3	3.5	4.0	2.1	3.1	1.2	3.0	67.8	2.9.3	1.2	·	·	·	8	2	·	4	6	1.1	7	2	1	·	3
IX	3.5	2.4	7.5	2.9	1.9.5	3.6	4.5	2.6	0.5	2.0	3	3.5	3.0.5	3.8	1.2	3.2	9	3.1	16.8	4.9	4	·	·	·	8	2	·	1.0	7	9	5	·	7	·	3
X	2	2.2	8.5	2.6	2.7	4.8	1.4.5	4.3	4.5	2.7	3	4.0	1.5	3.3	9.5	2.6	9	3.4	6.8	5.6	3.0	·	·	2	·	·	·	5	5	3	2	·	5	·	·
XI	4.5	4.3	7.5	2.6	1.3.5	4.0	1.5	4.3	1.5	1.3	10.5	3.1	2.6.5	3.9	1.1.5	3.9	1.3	3.2	79.1	24.5	4	·	·	1.0	·	·	·	1	1.7	1.7	1.0	2	1.3	1	·
XII	9	5.6	1.2	3.3	1.0	3.4	2	1.8	1.5	1.7	5.5	4.5	2.8.5	4.5	1.0.5	4.4	1.4	3.6	7.1.4	2.9.8	6	1.5	1.7	2.6	·	2	·	2	1.4	1.9	9	2	1.1	2.4	·
Rok	6.3.5	3.6	8.9.5	2.6	1.4.7.5	3.2	5.3.5	2.6	3.2.5	2.1	6.5	3.6	3.3.0.5	4.0	1.8.0.5	3.6	1.2.8	3.3	675.3	2.9.8	6.XII	2.8	3.2	9.3	3.7	1.4	1	4.4	1.2.5	1.5.7	1.0.3	1.7	5.8	4.8	3.3

Uwaga. Kierunki i prędkości wiatru – wg anemometru.

Kraków - Chełm

$H_s = 225\,m$ $h_w = 17{,}5\,m$

I	2	1.0	1.	5.0	11	3.6	1	1.0	·	·	12	2.4	13	2.1	1	3.5	5.2	1.2	21.1	6.8	4	1.2	1.4	2.7	·	·	·	4	7	1.0	7	·	4	1.7	·
II	·	·	3	1.7	6.5	1.8	1.5	1.7	1	2.0	1.6	3.8	1.9.5	4.4	0.5	5.0	3.6	2.0	23.8	6.1	9	·	·	2.0	·	·	·	·	1.7	1.2	6	·	5	3	·
III	·	·	·	·	·	·	·	·	·	·	2.9	5.9	4.8.5	6.4	8.5	4.9	7	5.6	28.2	4.3	31	·	·	5	·	5	·	2	1.6	1.8	8	·	2	2	1
IV	3.5	2.7	3	3.0	2.9.5	4.3	2.5	4.6	3.5	1.9	8.5	4.5	1.1.5	4.5	2	5.5	2.6	2.9	10.2	4.5	1	·	·	1	1	1	·	1.0	4	5	3	·	·	·	3
V	2	1.0	3	3.0	8	2.5	1	1.0	1	4.0	1.8	3.7	1.8	4.0	7	3.4	3.5	2.1	97.6	1.7.8	2.9	·	·	·	·	·	·	1	1.4	1.6	1.5	4	·	·	7
VI	4	2.0	2	2.0	1.1	2.7	3	2.3	·	·	8	2.9	2.4.5	3.6	4.5	3.0	3.3	1.9	79.5	4.4.6	2.7	·	·	·	7	1	1	6	7	1.4	1.1	1	2	·	1.0
VII	·	·	3.5	1.3	0.5	1.0	·	·	·	·	2.2	4.1	3.5	4.6	6	3.2	2.6	2.9	122.8	2.3.7	2.8	·	·	·	8	1	1	3	1.3	1.5	1.4	4	·	·	7
VIII	·	·	1	3.0	5.5	3.4	0.5	3.0	2	2.0	1.8.5	4.0	2.8.5	5.2	3	2.2	3.4	2.8	68.2	2.6.2	1.2	·	·	·	7	1	·	5	7	1.0	8	2	·	·	4
IX	·	·	2.5	1.8	1.2.5	3.6	·	·	·	·	5	3.7	2.7	4.2	·	·	4.3	2.0	39.5	1.7.0	4	·	·	·	6	1	·	1.1	7	8	5	2	6	·	4
X	·	·	1	4.0	2.2.5	3.5	3.5	1.0	1	2.0	7	3.1	1.2	4.7	1	3.0	4.5	1.8	5.0	3.5	3.0	·	·	1	·	·	·	4	9	4	1	·	6	·	·
XI	2	2.0	·	·	8.5	2.9	0.5	3.0	0.5	5.0	1.9.5	4.4	1.5	6.0	2	5.5	4.2	2.4	7.4.9	1.7.0	4	·	·	1.0	·	·	·	2	1.9	1.8	9	3	1.0	2	·
XII	4	4.2	3.5	4.1	6.5	3.9	·	·	·	·	1.0	6.7	1.9	5.7	4	1.5	4.6	2.6	53.4	2.2.7	6	1.3	1.8	2.6	·	1	·	2	1.5	1.1	5	2	4	2.4	·
Rok	1.7.5	1.1	2.3.5	2.4	1.2.2	2.8	1.3.6	1.5	9	1.4	1.7.3.5	4.1	2.7.1.5	4.6	3.9.5	3.4	4.2.5	2.5	6.2.4.2	4.4.6	2.7.VI	2.5	3.2	9.0	2.9	1.1	2	5.0	1.3.5	1.4.1	9.2	1.8	3.9	4.8	3.6

Kraków, Obserw. Astr. UJ

$H_s = 206\,m$ $H_b = 219{,}8\,m$ $h_w = 10\,m$

I	7.5	2.8	1.4	2.1	7.5	2.7	1.5	2.0	3.5	2.3	1.6	2.7	8.5	2.6	3.5	1.4	3.1	1.6	22.1	5.8	4	1.0	1.3	2.7	·	·	·	1	1.4	1.1	7	·	2.3	2.1	·
II	0.5	1.0	7.5	2.0	9.5	1.9	1.5	1.7	5	1.9	2.6	2.1	1.3.5	2.3	3.5	2.1	1.7	1.7	26.6	6.7	1.9	·	·	1.7	·	·	·	·	1.9	1.1	7	·	2.0	4	·
III	0.5	7.0	·	·	·	·	·	·	3.5	2.6	3.9.5	3.3	3.4	4.0	8.5	3.8	7	3.3	3.4.9	6.4	3.1	·	·	5	·	·	·	1	1.8	1.9	1.2	·	7	1	1
IV	3.5	2.3	2.4.5	3.7	1.5.5	4.3	3.5	2.7	5.5	2.6	1.3.5	3.0	6.5	3.6	2.5	5.2	1.5	3.0	10.8	6.1	1	·	·	1	2	1	·	5	6	6	3	·	4	·	2
V	7.5	1.9	6	2.8	7	2.5	3	1.5	3.5	2.4	1.3	2.7	2.4.5	2.1	1.3.5	2.3	1.5	1.9	113.9	2.4.3	2.9	·	·	·	1	·	·	·	1.8	1.8	1.5	4	1	·	8
VI	3	1.3	8	2.3	1.0	2.0	1	1.0	3.5	1.6	1.4.5	2.6	1.9.5	2.6	8.5	2.0	2.2	1.7	70.9	3.4.4	2.7	·	·	·	1.2	1	·	6	1.1	1.4	1.2	1	1	·	1.1
VII	2	2.2	1	1.0	1	2.0	3.5	1.1	5	2.1	2.7.5	3.1	2.0	2.9	8	1.8	2.5	1.9	126.1	2.1.8	3.0	·	·	·	8	1	·	4	1.1	1.4	1.2	5	·	·	7
VIII	6	2.0	3	2.3	1.5	2.7	2	1.5	7.5	2.9	2.7	2.4	1.7	3.1	9	1.9	2.0	1.9	68.8	2.7.1	1.2	·	·	·	8	·	·	4	1.0	1.1	7	2	·	·	3
IX	5.5	2.4	1.5	2.1	9	2.2	·	·	1	1.0	1.2	2.4	1.6.5	2.9	3	3.3	2.8	1.7	17.2	7.0	2.9	·	·	·	9	1	·	1.0	7	9	6	·	1.0	·	3
X	1	3.0	2.0	2.9	1.9	2.5	4	4.1	3.5	4.3	9.5	1.7	1.0	2.0	3	1.2	2.3	1.8	5.6	4.6	3.0	·	·	·	·	·	·	3	1.1	2	2	·	1.5	·	·
XI	6	2.2	7	2.5	4	3.8	·	·	1.5	1.7	2.2.5	1.9	1.6.5	2.7	6.5	2.8	2.6	1.7	67.0	1.8.0	4	·	·	8	·	·	·	·	1.9	1.9	9	2	1.8	1	·
XII	7	2.6	9	3.1	4	1.9	·	·	4	3.6	22	3.9	1.0.5	2.8	8.5	3.8	2.8	2.3	67.6	2.7.4	6	1.2	1.7	2.4	·	3	·	2	1.7	1.8	6	2	1.8	2.4	·
Rok	5.0	2.6	1.1.5	2.2	8.8	2.4	2.0	1.3	4.7	2.2	2.4.3	2.6	1.9.7	2.8	7.6	2.6	2.5.7	2.0	6.3.1.5	3.4.4	2.7.VI	2.2	3.0	8.2	4.0	7	·	3.6	1.6.1	1.5.2	9.8	1.6	1.1.7	5.1	3.5

Kraków - Nowa Huta

$\varphi = 50°04'$ $\lambda = 20°05'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
										Średnia																		
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.3	-8.8	8.6	4	-24.1	27	-6.8	-2.2	-4.6	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.8	5.3	5.9
II	–	–	–	–	5.0	-4.1	13.6	28	-8.5	6	0.1	4.1	1.8	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	7.6	7.1	7.9
III	–	–	–	–	10.1	2.5	20.3	18	-2.2	23	3.9	8.3	5.7	5.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	5.6	6.8
IV	–	–	–	–	17.7	4.4	25.9	15	-3.2	10	7.4	16.4	10.2	11.0	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.5	3.5	4.1
V	–	–	–	–	17.1	6.8	24.4	6	2.4	3	9.9	15.4	11.0	11.8	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	6.4	6.7
VI	–	–	–	–	24.2	11.1	33.4	27	5.3	21	15.6	22.7	16.2	17.7	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.3	5.3	5.1
VII	–	–	–	–	22.3	10.7	30.9	3	4.7	8	14.7	20.3	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.8	5.3	6.0
VIII	–	–	–	–	22.9	11.0	32.8	11	5.5	31	13.5	21.5	16.0	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.9	3.9	5.0
IX	–	–	–	–	21.4	8.1	29.4	2	0.7	22	10.6	20.1	13.4	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	4.2	2.7	4.2
X	–	–	–	–	17.2	5.0	21.6	6	-1.6	25	6.8	16.1	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.2	3.3	4.8
XI	–	–	–	–	7.6	1.0	16.7	3	-6.9	23	2.3	6.5	3.5	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	6.7	7.3
XII	–	–	–	–	-0.3	-8.6	18.6	5	-27.1	26	-5.3	-2.4	-4.7	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.8	6.6	6.1	7.2
Rok	–	–	–	–	13.7	3.5	33.4	27.VI	-27.1	26.XII	6.1	12.2	7.8	8.5	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.1	5.1	5.9

Dębica

$\varphi = 50°03'$ $\lambda = 21°24'$

I	–	–	–	–	0.0	-7.7	8.7	3	-24.5	27	-4.9	-1.5	-3.8	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.8	6.1	6.6
II	–	–	–	–	4.6	-0.6	11.4	18	-4.4	6	0.7	3.6	1.5	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.6	7.9	8.0
III	–	–	–	–	9.9	2.7	20.9	18	-2.5	23	4.2	8.2	5.6	5.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.9	7.7	8.0
IV	–	–	–	–	17.6	5.0	26.1	15	-3.1	10	7.9	15.9	11.0	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.8	4.4	4.8
V	–	–	–	–	17.2	7.0	24.4	27	2.0	20	9.7	15.5	11.1	11.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	7.1	7.4
VI	–	–	–	–	24.4	11.6	32.2	27	5.4	21	16.4	22.8	16.9	18.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.0	5.2	4.7
VII	–	–	–	–	22.7	11.5	32.2	4	6.6	8	15.1	20.6	15.4	16.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	6.9	6.6
VIII	–	–	–	–	23.6	12.5	34.9	11	5.2	31	15.4	21.7	16.4	17.5	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.2	6.4	5.9
IX	–	–	–	–	22.0	8.5	29.9	18	-0.1	23	11.1	20.7	14.2	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.7	4.5	4.7
X	–	–	–	–	17.2	7.3	23.6	20	1.2	6	8.6	16.1	11.4	11.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.7	4.7	5.1
XI	–	–	–	–	8.5	2.7	15.8	7	-5.0	21	4.3	7.0	5.1	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.4	8.3	7.8
XII	–	–	–	–	0.3	-7.9	14.3	5	-28.6	26	-4.2	-1.4	-4.0	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.5	8.0	8.0
Rok	–	–	–	–	14.0	4.4	34.9	11.VIII	-28.6	26.XII	7.0	12.4	8.4	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.2	6.5	6.5

Tarnów

$\varphi = 50°02'$ $\lambda = 20°59'$

I	995.2	1015.9	977.1	1021.9	0.1	-7.2	8.3	4	-23.3	27	-4.7	-1.2	-3.6	-3.3	3.8	4.1	3.9	3.9	8.0	6.9	7.7	7.5	1.0	1.9	1.3	1.4	7.5	6.2	5.7	6.5
II	997.5	1011.9	968.7	1023.7	4.8	-0.2	12.6	18	-3.6	5.6,26	0.7	3.9	1.6	2.0	5.4	5.8	5.7	5.6	8.4	7.3	8.2	8.0	1.0	2.3	1.2	1.5	8.2	7.7	6.6	7.5
III	993.3	1011.0	972.4	1019.1	10.1	3.0	20.9	18	-2.6	23	4.4	8.6	5.8	6.2	6.8	6.8	7.1	6.9	8.0	6.2	7.7	7.3	1.7	4.8	2.3	2.9	8.2	8.0	7.0	7.7
IV	988.0	996.5	980.3	1013.1	17.4	5.4	25.7	15	-2.3	10	8.7	16.0	10.9	11.6	8.2	8.1	8.6	8.3	7.3	4.5	6.6	6.1	3.3	10.8	4.8	6.3	5.4	6.0	4.4	5.3
V	987.5	994.9	972.8	1012.5	17.0	7.0	24.4	6	2.3	13	10.2	16.4	11.0	11.9	10.2	9.9	10.5	10.2	8.2	5.7	7.9	7.3	2.4	8.3	2.9	4.5	7.1	7.8	6.3	7.1
VI	990.9	1004.1	981.2	1015.6	23.9	12.1	32.5	27	6.3	21	16.5	22.6	16.6	18.1	15.1	14.4	15.0	14.8	8.0	5.4	8.0	7.1	4.0	13.6	4.1	7.2	5.3	5.9	6.1	5.8
VII	990.0	1004.1	976.0	1014.8	22.4	11.5	30.6	3,4	6.6	8	15.6	20.9	15.2	16.7	13.8	12.8	13.9	13.5	7.8	5.4	8.1	7.1	4.1	12.9	3.6	6.9	5.8	7.1	6.2	6.4
VIII	992.5	1004.6	982.8	1017.2	23.4	12.3	34.3	11	6.7	31	15.5	21.8	16.0	17.3	14.8	14.4	15.3	14.8	8.3	5.5	8.3	7.4	3.3	12.8	3.3	6.5	5.9	6.7	4.5	5.7
IX	994.9	1005.7	983.5	1019.9	21.7	8.9	30.2	18	-0.5	23	11.6	20.5	14.2	15.1	11.8	12.3	12.1	12.1	8.5	5.3	7.4	7.1	2.3	12.8	4.4	6.5	5.2	4.9	4.1	4.7
X	994.6	1006.4	971.7	1019.8	16.8	7.4	23.6	20	2.3	22	9.3	16.2	11.2	12.0	9.0	9.7	9.5	9.4	7.9	5.5	7.3	6.9	2.9	9.0	3.9	5.3	6.6	5.6	4.3	5.5
XI	989.6	1011.2	977.4	1016.3	8.2	2.1	16.6	3	-5.5	21	3.6	7.4	4.6	5.0	7.2	7.7	7.4	7.4	8.8	7.4	8.4	8.2	1.0	3.0	1.4	1.8	7.8	8.0	6.9	7.6
XII	990.8	1016.9	972.8	1017.3	0.4	-7.9	16.4	2	-27.6	26	-4.0	-1.9	-3.7	-3.3	4.4	4.6	4.4	4.5	8.2	7.8	8.0	8.0	1.1	1.7	1.3	1.4	7.9	7.1	6.6	7.2
Rok	992.1	1016.9	968.7	1017.5	13.8	4.5	34.3	11.VIII	-27.6	26.XII	7.3	12.5	8.3	9.1	9.2	9.2	9.4	9.3	8.1	6.1	7.8	7.3	2.3	7.8	2.9	4.3	6.7	6.8	5.7	6.4

Jakubowice

$\varphi = 50°01'$ $\lambda = 17°51'$

I	–	–	–	–	0.6	-6.1	11.0	4	-20.8	27	-4.4	-0.6	-3.1	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	4.9	3.6	4.9
II	–	–	–	–	5.5	-0.5	14.1	18	-5.4	6	0.8	4.4	1.6	2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	4.8	6.5
III	–	–	–	–	10.7	1.5	20.1	10	-3.0	20	3.8	9.6	5.7	6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	5.4	6.2
IV	–	–	–	–	17.3	6.2	24.7	7	-2.5	10	8.7	16.3	10.5	11.5	–	–	–	–	–	–	–	–	–	–	–	–	4.2	5.6	3.4	4.4
V	–	–	–	–	16.6	6.7	23.2	26,27	2.4	13	10.3	15.0	10.8	11.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.6	7.5	9.3
VI	–	–	–	–	23.2	10.9	30.5	25	4.0	16	15.7	21.5	16.3	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.0	5.9	5.6	5.2
VII	–	–	–	–	21.4	11.1	30.5	3	5.0	11	14.6	19.6	15.3	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.4	6.4	6.7
VIII	–	–	–	–	22.3	11.4	30.1	10	6.0	4,17	14.9	20.7	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.6	3.6	5.3
IX	–	–	–	–	22.3	9.1	29.3	2	3.2	23	11.9	21.1	14.3	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.8	2.9	4.2
X	–	–	–	–	16.2	6.0	21.8	5	1.7	11	7.6	15.3	9.7	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	3.7	5.3
XI	–	–	–	–	6.6	1.2	12.7	2	-5.6	22	2.6	5.7	3.2	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.9	7.3	7.7
XII	–	–	–	–	0.2	-6.6	15.7	5	-25.1	26	-3.6	-1.7	-3.3	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.6	6.3	7.0
Rok	–	–	–	–	13.6	4.2	30.5	25.VI, 3.VII	-25.1	26.XII	6.9	12.2	8.1	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	5.0	5.9

Kraków – Nowa Huta $H_s = 195\ m$ $h_w = 15,4\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v > 15	◑	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	10.5	2.2	14	1.8	18.5	1.7	·	·	3	2.0	5.5	2.6	20	2.4	3.5	1.9	18	1.7	15.6	4.7	4	13	15	28	·	·	·	6	12	7	6	·	3	19	·
II	3.5	2.7	6	1.5	14.5	1.6	3	1.7	3	2.3	4.5	2.3	38	2.1	4.5	2.0	7	1.8	30.2	9.2	1	·	1	20	·	·	·	·	15	12	8	·	2	2	·
III	·	·	·	·	·	·	·	·	·	·	12.5	4.3	71.5	3.3	7	4.1	2	3.5	29.3	6.5	31	·	·	5	·	1	·	2	13	18	11	·	2	·	1
IV	7.5	1.5	11.5	1.7	30.5	3.0	4	3.2	3.5	2.1	9.5	3.1	15.5	2.3	3	3.5	5	2.4	8.5	4.9	1	·	·	1	2	·	·	8	3	5	2	·	2	·	1
V	8.5	2.2	9.5	1.8	14.5	1.9	1	1.0	4	1.6	4	2.9	34.5	1.9	12	2.6	5	1.9	97.1	17.8	28	·	·	·	·	2	·	·	11	17	16	5	·	·	8
VI	7.5	2.1	3.5	1.7	15.5	1.6	4.5	1.2	3.5	1.0	9	2.2	33	2.1	9.5	2.1	4	1.8	81.2	19.5	4	·	·	·	12	·	·	7	5	15	13	3	1	·	10
VII	6.5	1.5	1	1.0	4	1.0	1	1.5	6.5	1.8	10.5	2.0	48.5	2.5	12	1.7	3	2.0	100.6	20.0	30	·	·	·	8	·	·	3	9	16	14	4	1	·	6
VIII	5	1.8	7.5	2.0	4	2.4	3.5	1.9	2	1.0	11.5	2.0	48.5	2.0	7	2.2	4	1.9	69.1	30.2	12	·	·	·	8	·	·	5	4	8	7	2	2	·	4
IX	4.5	1.9	13.5	2.7	13.5	2.8	0.5	1.0	·	·	9	1.8	37.5	2.0	6.5	2.1	5	2.1	16.8	6.3	4	·	·	·	8	·	·	11	5	5	4	·	5	·	1
X	·	·	9	2.8	37.5	3.0	5.5	4.1	2	2.0	6.5	1.5	23	1.7	3.5	2.6	6	2.4	6.6	6.0	30	·	·	2	·	·	·	4	4	2	1	·	5	·	·
XI	8.5	1.5	6	2.4	12.5	2.4	·	·	2	2.5	7.5	2.1	35	2.5	6.5	2.8	12	2.0	74.5	21.1	4	·	·	9	·	·	·	2	16	14	10	4	4	·	·
XII	9	3.9	5	2.3	17	1.9	1	1.0	·	·	7.5	3.7	32	2.9	9.5	3.9	12	2.5	48.3	22.1	6	14	18	26	·	·	·	2	17	8	4	2	7	23	·
Rok	71	1.8	86.5	1.8	182	1.9	24	1.4	29.5	1.4	97.5	2.5	437	2.3	84.5	2.6	83	2.2	577.8	30.2	12 VIII	27	34	91	38	3	·	50	114	127	96	20	34	44	31

Dębica $H_s = 205\ m$ $h_w = 16,2\ m$

I	3	1.7	8.5	1.6	6.5	2.2	11.5	3.0	30	3.6	12.5	2.1	8.5	3.8	6.5	2.3	6	2.7	16.9	4.9	5	10	14	26	·	·	·	3	13	12	4	·	4	21	·
II	3.5	1.4	1.5	1.7	14	2.1	12	2.7	19	3.0	13	2.7	10.5	2.1	7.5	1.8	3	2.3	20.2	7.4	10	·	·	18	·	1	·	·	16	8	4	·	6	3	·
III	1	2.5	1	2.0	·	·	2	2.0	5	4.4	22	3.2	46	4.5	14	4.2	2	3.9	23.7	5.4	31	·	·	5	·	1	1	1	15	13	8	·	3	2	·
IV	4	2.0	15.5	2.6	22.5	2.8	11	3.0	12.5	2.9	8	3.9	10	4.4	3.5	3.6	3	3.0	50.3	23.3	16	·	·	1	2	·	·	8	5	8	5	2	·	·	2
V	8	1.8	16	1.4	19.5	1.7	3.5	3.4	6.5	4.0	9.5	2.8	14.5	3.3	7.5	2.7	8	2.2	74.2	12.3	14	·	·	·	·	·	·	·	13	14	12	3	4	·	3
VI	4.5	1.8	6.5	2.0	14.5	2.1	15	2.3	8	3.0	2	1.5	17	2.6	9.5	2.9	13	2.1	50.0	12.9	13	·	·	·	10	·	·	4	3	14	10	1	·	·	7
VII	4	1.5	4	1.6	10.5	1.8	11	2.3	8	2.3	8.5	2.4	24	2.5	9	2.8	14	1.9	99.2	21.8	29	·	·	·	9	1	1	3	10	14	11	4	1	·	5
VIII	2.5	2.0	10	1.6	9.5	1.5	7.5	1.7	12	2.5	10	2.8	22	2.9	13.5	2.1	6	2.1	56.5	21.8	12	·	·	·	9	1	·	1	8	11	7	2	·	·	4
IX	2.5	1.4	15	1.7	13	1.8	7.5	2.1	14	2.1	13	2.9	10.5	2.9	5.5	3.8	9	2.1	22.8	13.8	6	·	·	1	9	·	·	11	6	5	4	1	7	·	2
X	3	1.3	11	1.8	24	2.1	20.5	3.5	11.5	3.8	4	1.9	5	2.1	4	1.5	10	2.3	18.1	15.4	30	·	·	·	·	·	·	7	7	4	2	1	5	·	·
XI	7	1.9	8	1.8	8	1.8	10	2.4	19.5	2.6	13	1.9	12.5	2.2	10	1.9	2	2.1	57.5	14.9	11	·	·	9	·	·	·	1	17	17	11	1	6	1	·
XII	11	2.5	8	1.6	6.5	1.8	6	2.4	17.5	3.3	3.5	2.4	14	2.3	19.5	2.9	7	2.4	66.9	27.5	11	12	15	22	·	1	·	1	19	15	9	1	4	23	·
Rok	54	1.8	105	1.8	148.5	1.8	117.5	2.6	163.5	3.1	119	2.5	194.5	3.0	110	2.7	83	2.4	556.3	27.5	11.XII	22	29	82	39	5	2	40	132	135	87	16	40	50	23

Tarnów $H_s = 209\ m$ $H_b = 209,1\ m$ $h_w = 13,6\ m$

I	2	1.0	6	4.3	9	1.6	9	3.2	21	3.2	12	1.9	5.5	3.2	12.5	3.2	16	2.4	16.2	4.8	5	10	14	24	·	1	·	4	14	10	5	·	5	22	·
II	2	2.2	·	·	3.5	1.7	9.5	2.0	17	3.8	7.5	1.6	7	3.6	18.5	2.7	19	2.2	30.6	7.6	28	·	·	15	·	·	·	1	16	13	6	·	5	3	·
III	4.5	2.4	·	·	·	·	1	2.0	2.5	1.8	5	3.6	32	4.4	42	4.5	6	3.9	24.8	7.6	31	·	·	5	·	4	·	1	16	16	9	·	1	2	·
IV	3	2.0	7.5	2.7	17.5	3.0	18.5	3.7	8	2.6	4.5	2.2	8	5.1	8	3.8	15	2.8	21.8	7.2	1	·	·	1	2	4	·	7	9	10	7	·	1	·	2
V	9.5	1.9	5.5	2.5	10	2.5	10.5	2.0	2	2.5	0.5	1.0	12.5	2.5	22.5	2.3	20	1.8	72.5	13.7	6	·	·	·	·	·	·	·	16	14	12	2	2	·	5
VI	6	1.7	3	2.0	5	1.8	15.5	2.6	10.5	1.8	4	1.2	14	2.1	15	2.5	17	1.7	103.9	38.5	7	·	·	·	8	·	·	1	6	11	9	3	2	·	8
VII	6	1.8	1.5	1.0	0.5	1.0	7	1.9	2	2.0	7.5	2.5	22	2.3	22.5	2.5	24	1.7	123.1	47.7	30	·	·	·	9	·	·	3	11	15	11	3	·	·	5
VIII	4	1.4	4.5	1.9	3	2.5	4	1.5	4	1.4	7	2.0	16.5	2.9	19	2.8	31	1.6	61.7	21.0	12	·	·	·	10	·	·	4	6	8	6	2	1	·	3
IX	2	1.5	2	1.5	11	2.0	7.5	2.5	2.5	1.4	4	1.8	14.5	3.3	11.5	2.9	35	1.5	19.6	7.5	6	·	·	1	10	1	·	10	9	7	6	·	4	·	2
X	4	2.0	1.5	2.7	10.5	2.5	24.5	3.7	24	3.9	2	2.2	5	1.8	5.5	1.6	16	2.6	25.5	16.3	30	·	·	·	·	1	·	7	8	7	4	1	3	·	·
XI	7	1.9	2	2.5	5	2.9	16	2.5	10.5	1.9	5	2.0	19	2.7	12.5	2.8	13	2.1	64.5	17.9	4	·	·	8	·	·	·	1	15	15	11	2	4	·	·
XII	11	2.8	7.5	3.5	8.5	1.8	5.5	2.2	11.5	2.7	7.5	3.5	11	3.6	20.5	3.2	10	2.6	52.6	18.4	11	14	16	23	·	3	·	2	17	14	9	2	3	24	·
Rok	61	1.9	41	2.0	83.5	1.9	128.5	2.5	115.5	2.4	66.5	2.1	167	3.1	210	2.9	222	2.2	616.8	47.7	30.VII	24	30	77	39	14	·	41	143	140	95	15	31	51	25

Jakubowice $H_s = 319\ m$ $h_w = 14\ m$

I	11	3.6	4	3.6	·	·	1.5	9.3	26.5	5.6	19	5.2	4	2.5	4	5.4	23	3.7	9.5	4.6	1	7	13	24	·	5	2	9	10	5	3	·	3	16	–
II	3.5	3.3	·	·	·	·	2.5	1.4	27.5	3.9	16	5.0	4.5	2.9	7	5.0	23	3.0	13.6	–	–	·	·	16	·	2	·	2	9	12	7	·	7	1	–
III	4	2.8	2.5	3.0	·	·	1.5	3.7	5	3.6	15.5	4.2	16	3.9	19.5	5.3	29	2.9	28.0	7.6	18	·	·	10	·	·	·	4	10	16	8	·	1	1	–
IV	11.5	2.7	6.5	2.8	10	2.7	3	4.7	16.5	4.2	13	3.3	2	4.0	9.5	4.1	18	2.8	7.5	4.3	1	·	·	1	·	1	·	7	2	4	3	·	·	·	–
V	19	3.1	2.5	1.4	1.5	1.0	0.5	1.0	11	2.7	13	2.4	8	3.8	20.5	3.8	17	2.5	58.1	14.3	29	·	·	·	·	·	·	1	16	15	12	2	·	·	–
VI	20	2.1	2.5	2.2	2.5	1.8	2.5	1.0	8	2.0	9.5	2.2	5	1.8	15	3.9	25	1.8	78.0	27.6	27	·	·	·	7	·	·	6	10	12	10	3			–
VII	7	1.9	3	1.7	1	1.0	·	·	7.5	2.6	15	2.4	14	2.3	14.5	3.1	31	1.6	120.0	32.5	15	·	·	·	6	·	·	4	15	13	10	4	·	·	–
VIII	7	1.8	5	1.0	2.5	1.0	0.5	1.0	8.5	3.0	20.5	2.5	7.5	2.9	14.5	2.3	27	1.6	41.6	17.3	12	·	·	·	8	·	·	5	5	11	8	1	2	·	–
IX	5.5	1.4	2	2.0	5	1.4	3	1.7	17	3.0	9	3.0	4	2.0	7.5	2.6	37	1.4	17.9	6.7	4	·	·	·	9	·	·	12	9	6	5	·	6	·	–
X	4.5	2.9	7	1.9	4.5	3.7	3.5	6.1	21	4.3	12	3.0	4.5	1.9	8	3.3	28	2.4	37.1	15.7	19	·	·	·	·	1	·	7	7	7	4	2	4	·	–
XI	9.5	3.5	0.5	1.0	0.5	1.0	·	·	21	2.8	17	4.1	6	1.5	11.5	4.4	24	2.5	54.8	28.3	4	·	·	6		·		4	19	16	8	1	6	2	–
XII	25.5	4.5	·	·	0.5	5.0	1.5	2.3	10.5	5.7	27	5.2	3	2.0	12	5.3	13	4.2	41.0	12.1	6	10	16	24	·	2^{2}	·	1	13	19	9	1	1	20	–
Rok	128	2.8	35.5	1.7	28	1.6	20	2.7	180	3.6	186.5	3.5	78.5	2.6	143.5	4.0	295	2.5	507.1	32.5	15.VII	17	29	81	30	11^{2}	2	62	125	136	87	14	30	40	–

Ożarńsk

$\varphi = 50°01'$ $\lambda = 22°35'$ **1961**

MIESIĄC	CIŚNIENIE p				TEMPERATURA T											ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max obs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.4	-8.5	8.4	3	-22.2	27	-5.8	-2.9	-4.8	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.3	5.1	5.9
II	–	–	–	–	3.3	-0.8	9.7	18	-5.2	26	-0.2	2.5	0.7	0.9	5.6	6.4	5.9	6.0	9.2	8.8	9.1	9.0	0.5	0.9	0.6	0.7	8.4	7.6	6.5	7.5
III	–	–	–	–	8.8	1.5	18.4	18	-5.3	28	3.3	7.1	4.7	5.0	7.0	7.3	7.1	7.1	9.0	7.2	8.3	8.2	0.9	3.1	1.6	1.9	7.2	7.7	6.0	7.0
IV	–	–	–	–	16.4	5.2	24.0	15	-0.5	1	7.7	15.0	10.1	10.7	8.4	8.7	8.6	8.6	7.8	5.0	6.8	6.6	2.5	9.1	4.1	5.2	4.2	4.7	4.0	4.3
V	–	–	–	–	16.7	7.3	24.6	29	3.3	17,19	9.9	14.8	11.2	11.8	10.5	10.5	10.2	10.4	8.6	6.4	7.7	7.6	1.8	6.9	3.4	4.0	7.5	7.0	5.7	6.7
VI	–	–	–	–	23.3	12.3	30.6	27	7.3	29	16.0	21.7	16.7	17.8	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.2	4.8	4.8
VII	–	–	–	–	22.3	11.7	30.8	4	7.5	7	15.1	20.6	16.0	16.9	14.0	12.7	13.4	13.4	8.2	5.4	7.5	7.0	3.4	12.2	5.2	6.9	5.2	6.3	5.3	5.6
VIII	–	–	–	–	22.8	12.6	33.7	11	7.4	31	15.1	21.1	16.9	17.5	14.6	14.1	14.9	14.5	8.4	5.6	7.6	7.2	3.0	11.8	4.9	6.6	4.7	5.2	5.2	5.0
IX	–	–	–	–	21.1	9.6	28.3	18	-0.6	23	11.6	20.0	14.5	15.2	12.0	12.3	12.2	12.2	8.6	5.4	7.3	7.1	2.2	11.8	4.9	6.3	4.9	4.7	3.5	4.4
X	–	–	–	–	16.2	5.0	23.6	19	0.9	24	6.6	15.3	9.7	10.3	8.4	8.9	8.6	8.6	8.6	5.3	7.1	7.0	1.5	8.8	3.5	4.6	5.6	5.2	3.7	4.8
XI	–	–	–	–	7.4	2.1	14.2	3	-4.7	21	3.7	6.4	4.4	4.7	7.5	8.2	7.6	7.8	9.0	8.4	8.8	8.7	0.8	1.7	1.0	1.2	8.5	8.1	6.5	7.7
XII	–	–	–	–	-0.6	-8.7	14.3	5	-26.5	26	-4.3	-2.5	-4.1	-3.8	4.4	4.6	4.4	4.5	7.9	7.7	7.8	7.8	1.0	1.4	1.0	1.1	8.3	7.9	6.4	7.5
Rok	–	–	–	–	13.0	4.1	33.7	11.VIII	-26.5	26.XII	6.6	11.6	8.0	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.2	5.2	5.9

Jarosław

$\varphi = 50°01'$ $\lambda = 22°42'$

I	–	–	–	–	-1.3	-8.9	8.2	4	-24.0	27	-6.2	-2.8	-5.3	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	8.6	6.0	6.6	7.1
II	–	–	–	–	3.7	-0.4	9.8	18	-3.6	27	0.0	3.0	1.2	1.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.1	7.0	7.9
III	–	–	–	–	9.2	2.3	18.5	18	-2.7	23	3.8	7.6	5.4	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.9	6.2	7.3
IV	–	–	–	–	17.0	5.1	25.1	7,15	-2.4	10	8.0	15.6	10.7	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.1	4.2	5.6
V	–	–	–	–	17.0	7.3	25.5	29	2.3	5	10.1	15.4	11.9	12.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	6.0	6.9
VI	–	–	–	–	24.0	12.3	31.7	26	7.5	1	16.8	22.3	17.5	18.5	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.9	6.1	5.7
VII	–	–	–	–	23.1	11.5	31.7	4	8.5	19	15.6	21.4	16.4	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.0	6.3	5.2
VIII	–	–	–	–	23.1	12.6	34.7	11	8.9	15,31	15.5	21.4	17.3	17.9	–	–	–	–	–	–	–	–	–	–	–	–	3.7	4.2	4.5	4.1
IX	–	–	–	–	21.5	9.2	29.7	18	-0.1	23	11.0	20.5	14.7	15.2	–	–	–	–	–	–	–	–	–	–	–	–	3.8	3.6	3.2	3.5
X	–	–	–	–	16.4	4.8	23.2	19	0.3	13	5.9	15.4	9.9	10.3	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.6	3.5	4.3
XI	–	–	–	–	7.9	1.9	15.3	3	-6.8	23	3.6	6.9	4.7	5.0	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.8	6.5	7.3
XII	–	–	–	–	-0.3	-7.6	16.1	5	-26.3	25	-4.4	-2.0	-4.1	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.2	6.0	7.0
Rok	–	–	–	–	13.4	4.2	34.7	11.VIII	-26.3	25.XII	6.6	12.1	8.4	8.9	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.1	5.5	6.0

Pszczyna

$\varphi = 50°00'$ $\lambda = 18°55'$

I	–	–	–	–	0.3	-7.0	10.6	4	-18.4	27	-4.7	-0.3	-3.8	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.0	5.4	5.2
II	–	–	–	–	5.0	-1.0	13.5	18	-2.0	6	-0.1	4.1	1.0	1.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.8	6.1	6.5
III	–	–	–	–	9.7	2.5	18.6	18	-2.6	20	3.7	8.6	5.5	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.5	5.9	6.6
IV	–	–	–	–	17.5	4.9	24.5	7	-2.0	10	7.8	16.8	9.5	10.9	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.3	3.7	4.2
V	–	–	–	–	16.7	6.5	24.0	27	2.6	12	9.2	15.0	9.9	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.9	5.9	6.3
VI	–	–	–	–	23.9	11.7	32.6	27	6.4	21	14.8	21.6	16.6	17.4	–	–	–	–	–	–	–	–	–	–	–	–	4.0	5.9	5.8	5.2
VII	–	–	–	–	21.9	11.4	30.6	3	6.6	8	14.3	19.6	15.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.1	6.1	5.9
VIII	–	–	–	–	22.8	12.0	30.6	6	6.9	14	14.8	21.0	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.5	4.1	5.1
IX	–	–	–	–	22.0	9.2	29.9	17	1.8	23	12.0	20.4	13.4	14.8	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.1	2.1	3.6
X	–	–	–	–	17.3	5.9	22.6	5	1.0	10	7.4	15.5	9.2	10.3	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	4.3	5.2
XI	–	–	–	–	–	0.8	–	–	-5.3	23	2.4	5.7	2.9	3.5	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	6.1	7.0
XII	–	–	–	–	0.4	-7.6	18.0	5	-24.9	26	-4.3	-1.7	-4.9	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.8	6.6	6.5
Rok	–	–	–	–	–	4.1	32.6	27.VI	-24.9	26.XII	6.4	12.2	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	5.2	5.6

Czernichów

$\varphi = 50°00'$ $\lambda = 19°41'$

I	–	–	–	–	0.7	-8.1	10.0	4	-20.6	28	-6.1	-1.0	-4.3	-3.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.5	5.0	5.5
II	–	–	–	–	5.7	-1.0	14.0	28	-6.3	6	0.1	4.7	1.6	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.7	6.7	7.2
III	–	–	–	–	10.4	2.6	20.5	18	-2.0	28	4.2	9.0	5.7	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	5.7	6.4
IV	–	–	–	–	18.4	4.8	26.9	15	-1.8	10	8.0	17.7	10.6	11.7	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.4	3.8	4.1
V	–	–	–	–	17.7	7.1	25.1	6	3.0	15	9.9	16.3	11.2	12.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.6	6.1	6.5
VI	–	–	–	–	24.5	11.5	33.1	27	6.2	21	15.7	23.3	16.3	17.9	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.3	4.6	4.7
VII	–	–	–	–	22.6	11.4	31.5	3	6.5	8	14.9	20.7	15.4	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.5	5.2	5.6
VIII	–	–	–	–	23.3	11.8	32.7	11	6.7	31	14.8	22.1	15.9	17.2	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.4	3.8	4.8
IX	–	–	–	–	22.1	8.5	30.6	17	1.3	24	10.7	21.1	12.9	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.3	4.2	4.5
X	–	–	–	–	17.3	5.1	21.9	6	-0.7	25	6.2	16.4	9.4	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.2	3.5	5.2
XI	–	–	–	–	7.6	0.5	16.2	3	-6.6	23	2.5	6.5	3.4	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.7	8.0	8.1
XII	–	–	–	–	0.1	–	18.9	5	–	–	-5.1	-1.8	-4.5	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.7	6.9	8.6	8.4
Rok	–	–	–	–	14.2	–	33.1	27.VI	–	–	6.3	12.9	7.8	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.9	5.4	5.9

Ożańsk $H_s = 250$ m $h_w = 20{,}5$ m 1961

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R ꞅ
I	2.5	4.4	·	·	4.5	2.7	9	3.2	7.5	9.7	9.5	7.6	7.5	4.1	14.5	5.2	38	3.2	4.5	1.6	14	12	15	30	·	4	2	·	8	5	3	·	7	18	·
II	·	·	·	·	4.5	3.3	8	3.9	12	5.3	11	4.0	25	4.4	25	4.8	21	3.3	12.6	4.7	10	·	1	16	·	1	·	2	14	11	4	·	6	6	·
III	·	·	·	·	·	·	1	8.0	7	7.7	12.5	6.6	41	7.5	21.5	7.5	10	6.6	16.6	4.5	31	·	·	8	·	13	4	2	13	11	6	·	4	1	1
IV	0.5	2.0	7.5	9.3	14	6.4	7	8.1	9	4.9	8	5.6	6	4.7	11	5.5	27	4.4	11.4	4.5	1	·	·	1	·	8	·	5	2	7	3	·	·	·	4
V	0.5	4.0	4.5	4.0	2	2.8	4.5	3.9	6	4.0	9.5	4.6	21.5	4.8	5.5	4.7	39	2.6	71.7	20.8	14	·	·	·	·	2	·	·	6	15	13	2	1	·	4
VI	·	·	0.5	4.0	8	5.0	6	3.8	7	2.9	6.5	3.8	20	4.6	·	·	42	2.3	89.5	40.8	3	·	·	·	7	3	·	6	4	12	10	2	1	·	5
VII	·	·	·	·	0.5	2.0	4.5	3.8	4.5	4.4	20.5	5.5	21	5.9	·	·	42	3.0	93.8	33.0	29	·	·	·	8	5	·	2	3	15	13	3	·	·	2
VIII	·	·	1	3.0	2	4.5	4.5	3.1	2.5	4.8	23	4.8	22	5.4	1	3.0	37	2.9	38.0	13.9	12	·	·	-	7	2	·	4	3	12	8	1	·	·	5
IX	·	·	2	4.0	7	3.4	3	4.0	3	5.7	24	4.9	12	5.1	·	·	39	2.7	17.3	7.7	7	·	·	1	6	4	·	11	5	8	6	·	2	·	1
X	·	·	2	5.0	16.5	7.1	26.5	6.3	6.5	4.2	9.5	4.3	5.5	4.4	0.5	2.0	26	4.2	21.3	14.0	30	·	·	·	·	4	1	9	6	6	5	1	4	·	·
XI	·	·	0.5	6.0	10.5	7.6	8.5	5.1	5	5.4	14.5	5.3	18.5	4.8	3.5	5.2	29	3.7	25.7	6.0	11	·	2	9	·	5	2	1	17	14	7	·	1	·	·
XII	3	4.7	1	2.0	5.5	4.5	6	4.0	8.5	7.6	11	9.4	18.5	5.3	10.5	4.5	29	4.1	20.9	5.6	11	13	17	24	·	9	·	·	14	10	6	·	1	18	·
Rok	6.5	1.3	19	3.1	75	4.1	88.5	4.8	78.5	5.6	159.5	5.5	218.5	5.1	70.5	3.5	379	3.6	423.3	40.8	3.VI	25	35	89	28	60	9	42	95	126	84	9	27	43	22

Jarosław $H_s = 204$ m $h_w = 19$ m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R ꞅ
I	7	1.0	2	7.0	·	·	28	1.6	3	1.7	19	6.7	2	2.0	21	4.2	11	3.1	10.5	2.4	2	14	17	30	·	3	2	1	13	10	4	·	19	18	:
II	2	1.5	·	·	·	·	19	1.8	6	5.2	17	2.1	24	3.0	11	1.6	5	2.3	13.6	6.7	10	·	1	12	·	1	·	1	16	11	3	·	20	·	·
III	2	9.0	·	·	·	·	1	1.0	·	·	24	5.3	33	5.9	30	8.2	3	6.3	22.9	5.4	12	·	·	8	·	14	5	1	11	13	7	·	16	·	1
IV	3	3.0	3	1.3	4	2.2	32	6.9	5	2.6	21	3.5	8	2.1	10	4.9	4	4.4	15.2	5.5	1	·	·	2	2	9	3	4	5	5	4	·	2	·	3
V	8	1.0	·	·	·	·	27	2.0	10	2.0	10	1.9	17	1.5	14	3.1	7	1.8	43.5	9.2	9	·	·	·	1	·	·	·	13	14	11	·	11	·	7
VI	·	·	·	·	9	1.7	16	1.8	8	1.8	28	2.0	15	1.9	8	1.6	6	1.7	76.6	37.5	3	·	·	·	12	·	·	3	7	10	9	2	11	·	5
VII	·	·	·	·	·	·	5	1.2	·	·	33	1.7	27	2.1	19	1.5	9	1.6	98.0	39.6	29	·	·	·	9	·	·	2	4	14	11	2	·	·	6
VIII	3	4.0	·	·	1	1.0	3	1.3	·	·	33	2.2	17	2.6	27	1.7	9	1.9	37.7	10.5	12	·	·	·	8	·	·	6	4	11	8	1	·	·	2
IX	·	·	1	1.0	1	1.0	13	2.2	3	1.3	13	3.9	24	2.7	19	3.7	16	2.5	20.0	7.3	7	·	·	1	8	2	·	13	4	10	7	·	14	·	2
X	2	3.5	·	·	3	4.0	52	3.8	8	2.0	5	3.0	8	2.2	8	3.6	7	3.2	27.8	15.5	30	·	·	·	·	·	·	11	7	6	5	1	11	·	·
XI	3	3.0	·	·	·	·	22	3.9	8	1.8	19	2.8	21	2.1	13	4.2	4	2.9	37.4	7.2	11	·	·	9	·	1	·	2	16	16	11	·	19	·	·
XII	10.5	3.3	·	·	2	1.5	10	2.9	3	4.2	17	6.5	11	1.1	23.5	4.0	16	3.3	36.5	8.0	7	11	16	24	·	2	·	1	14	13	7	·	2	23	·
Rok	40.5	2.4	6	0.8	20	1.0	228	2.5	54	1.9	239	3.5	207	2.4	203.5	3.5	97	2.9	439.7	39.6	29.VII	25	34	86	40	32	10	45	114	133	87	6	125	41	26

Pszczyna $H_s = 270$ m $h_w = 18$ m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R ꞅ
I	1	2.0	8	1.4	20	2.0	1	1.0	8.5	2.1	32	1.8	11.5	1.4	3	1.7	8	1.6	25.8	8.8	4	11	11	26	·	·	·	10	11	7	7	·	4	11	·
II	·	·	·	·	·	·	4	1.0	8	1.1	36	1.5	13	1.2	6	1.3	17	1.0	52.2	20.0	9	·	2	17	·	·	·	3	12	10	8	2	12	2	·
III	1	2.0	·	·	·	·	·	·	·	·	22	1.9	42	1.3	17	1.6	11	1.3	44.8	11.0	14	·	·	5	·	1	·	2	12	13	11	1	1	·	1
IV	1	1.0	5	1.0	25	1.9	6	1.2	7	1.4	18	1.3	9	1.3	6	1.5	13	1.3	36.0	7.2	1,28	·	·	1	·	·	·	10	4	9	8	·	1	·	1
V	11	1.0	6	1.2	3	1.0	5	1.2	7	1.1	17	1.5	15	1.4	8	1.5	21	1.0	54.2	11.6	21	·	·	·	·	·	·	·	9	14	14	1	2	·	8
VI	6	1.0	1	1.0	7	1.4	10	1.1	7	1.1	21	1.3	16	1.5	12	1.2	10	1.1	61.0	12.2	4	·	·	·	10	·	·	3	6	10	10	2	3	-	8
VII	7	1.0	·	·	2	1.0	2	1.0	4	1.0	34.5	1.6	19.5	1.5	13	1.5	11	1.3	106.0	21.2	15	·	·	·	7	·	·	4	8	12	12	5	·	·	6
VIII	·	·	3	1.0	6	1.0	·	·	5	1.4	37	1.8	12	1.3	11	1.4	19	1.2	52.8	21.4	12	·	·	·	9	1	·	4	5	8	6	2	1	·	3
IX	1	1.0	1	1.0	17	1.5	5	1.0	13	1.2	21	1.6	13	1.4	6	1.7	13	1.2	9.6	5.0	14	·	·	·	7	1	1	12	4	3	3	·	4	·	2
X	4.5	2.0	0.5	2.0	5	2.8	17	2.1	15	3.2	29	2.1	2	3.0	4	1.5	16	1.9	20	1.0	7,29	·	·	·	·	·	·	7	6	2	2	·	7	·	·
XI	5	1.6	3.5	1.0	4.5	1.7	7.5	1.1	7.5	1.4	29.5	1.7	14.5	1.6	7	1.1	11	1.3	83.7	30.0	4	·	–	8	–	·	·	3	15	10	10	3	10	3	·
XII	12	1.5	7	1.6	14	1.4	2	1.0	·	·	29	2.5	10	1.6	3	1.7	16	1.5	55.5	21.2	6	14	15	25	·	2	1	4	12	9	7	2	4	23	·
Rok	49.5	1.2	35	0.9	103.5	1.3	59.5	1.0	82	1.2	326	1.7	177.5	1.5	96	1.5	166	1.3	583.6	30.0	4.XI	25	–	82	–	5	2	62	104	107	98	18	49	39	29

Czernichów $H_s = 218$ m $h_w = 16$ m

Miesiąc	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad Suma	Opad Max	Opad Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊞	R ꞅ
I	1.5	1.7	8	3.9	12	3.4	1.5	2.3	3.5	1.4	5.5	3.6	11.5	3.0	3.5	2.1	46	1.6	23.3	8.9	4	12	13	27	·	1	·	7	9	14	4	·	–	23	·
II	1	1.0	7	2.1	5	1.9	0.5	2.0	2	2.0	6.5	3.5	22.5	3.2	2.5	1.8	37	1.5	36.8	11.8	9	·	·	19	·	·	·	3	14	15	9	1	–	3	·
III	0.5	4.0	·	·	·	·	·	·	·	·	25	4.7	44.5	4.2	9	3.9	14	3.7	49.5	7.9	14	·	·	6	·	3	·	4	14	16	14	·	–	3	1
IV	1	2.0	7	3.8	23.5	4.8	1.5	4.0	2	3.5	8.5	6.1	9.5	2.6	4	3.9	33	2.7	14.6	8.3	1	·	·	1	4	1	·	10	5	6	4	·	–	·	3
V	2	1.5	3	3.0	6	3.5	3	1.7	0.5	3.0	7	2.9	18.5	2.8	9	2.6	44	1.5	83.5	16.7	6	·	·	·	1	·	·	4	10	19	15	3	–	·	12
VI	0.5	2.0	1.5	2.0	12.5	2.7	2	1.0	1	4.0	6	3.4	19.5	2.7	5	2.3	42	1.4	75.0	27.4	27	·	·	·	14	·	·	7	4	13	11	3	–	·	10
VII	1	1.0	·	·	3	1.0	·	·	1	1.0	8	3.6	29	3.1	5	2.7	46	1.5	121.8	27.3	28	·	·	·	8	1	1	5	8	15	12	6	–	·	8
VIII	·	·	4	2.4	3	1.8	·	·	1	1.5	13.5	2.5	22.5	3.4	2	1.2	47	1.4	75.1	40.6	12	·	·	·	10	·	·	6	5	11	8	2	–	·	4
IX	1	1.0	8	3.1	9	3.2	1	1.0	·	·	5.5	3.4	16.5	3.2	2	3.8	47	1.5	11.4	3.2	26	·	·	·	10	·	·	12	9	8	5	·	5	·	3
X	0.5	1.0	5	4.2	16	3.9	4	2.6	6.5	3.7	2	3.2	11	2.9	3	2.3	45	1.8	8.8	6.1	30	·	·	1	·	·	·	3	6	6	2	·	11	·	·
XI	11	2.1	3	2.0	6	4.3	·	·	0.5	2.0	4.5	4.7	18.5	3.1	8.5	2.5	38	1.7	82.2	29.1	4	·	·	10	·	·	·	1	19	20	11	3	12	4	·
XII	10.5	3.5	11	3.3	5	3.4	·	·	1	7.0	10	6.9	16.5	5.6	4	4.9	35	3.0	66.8	19.0	6	–	16	–	·	2	·	·	17	25	9	2	14	22	·
Rok	30.6	1.7	57.6	2.5	101	2.8	13.5	1.2	19	2.4	102	4.0	240	3.3	57.5	2.8	474	1.9	648.8	40.6	12.VIII	–	29	–	47	8	1	62	120	168	104	20	–	55	41

Wieliczka — φ = 50°00' — λ = 20°03' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.3	-8.0	9.3	4	-21.6	27	-5.3	-1.0	-3.8	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	5.4	-0.4	13.7	28	-5.4	6	0.8	4.6	2.2	2.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	10.1	3.3	20.2	18	-1.7	23	4.7	8.8	6.3	6.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	17.8	5.2	26.2	15	-2.4	10	8.1	17.0	10.7	11.6	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.8	5.0	5.4
V	–	–	–	–	17.1	7.5	24.4	6	3.4	12	10.4	15.7	11.2	12.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	8.2	7.8
VI	–	–	–	–	23.9	12.2	32.8	27	5.9	21	16.9	22.5	16.6	18.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.3	6.4	6.2
VII	–	–	–	–	22.1	12.1	30.8	3	6.6	8	16.2	20.5	15.6	17.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	22.8	12.7	32.8	11	6.7	31	15.9	21.8	16.4	17.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	5.9	6.3
IX	–	–	–	–	21.8	9.5	30.4	17	0.9	23	11.8	20.8	14.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.3	4.6	5.2
X	–	–	–	–	17.2	5.5	22.4	8	-0.2	22	7.3	16.7	11.0	11.5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	7.7	1.4	17.0	3	-5.1	23	2.9	7.0	4.2	4.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	0.0	-8.4	20.0	5	-26.9	26	-4.9	-1.7	-4.8	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	13.8	4.4	32.8	27.VI,1,IV	-26.9	26.XII	7.1	12.7	8.3	9.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Bochnia - Chodenice — φ = 49°59' — λ = 20°24'

I	–	–	–	–	0.6	-8.7	8.9	4	-25.5	27	-6.5	-1.6	-4.4	-4.2	3.7	4.1	4.1	4.0	87	72	83	81	0.7	1.8	1.0	1.2	7.3	5.9	5.8	6.3
II	–	–	–	–	5.4	-4.2	14.2	28	-5.4	27	0.5	4.5	1.5	2.0	5.7	6.2	6.1	6.0	89	74	89	84	0.7	2.5	0.8	1.3	8.0	7.7	6.8	7.5
III	–	–	–	–	10.2	2.5	20.4	18	-2.3	23	4.4	8.7	5.7	6.1	7.0	7.4	7.3	7.2	83	67	80	77	1.6	4.3	2.0	2.6	8.0	7.8	6.2	7.3
IV	–	–	–	–	17.6	2.7	25.7	15	-4.4	10	8.1	16.5	10.0	11.2	8.8	8.7	9.0	8.8	80	47	74	67	2.3	10.7	3.7	5.6	5.0	5.1	4.0	4.7
V	–	–	–	–	17.0	6.2	24.7	6	0.5	3	10.3	15.4	10.4	11.6	10.6	10.6	10.8	10.7	84	61	85	77	2.1	7.5	2.0	3.9	7.4	7.5	7.1	7.3
VI	–	–	–	–	24.1	10.6	32.9	27	4.5	21	16.4	22.7	15.9	17.7	15.3	14.9	15.1	15.1	82	54	84	73	3.6	13.3	3.1	6.7	4.8	5.7	5.4	5.3
VII	–	–	–	–	21.9	10.9	30.4	3	5.0	8	15.7	20.3	15.0	16.5	14.0	13.5	14.2	13.9	78	58	83	73	4.1	11.3	3.2	6.2	6.4	7.0	5.5	6.3
VIII	–	–	–	–	22.7	11.6	33.5	11	5.0	31	15.2	21.7	15.6	17.0	14.7	14.9	15.4	15.0	84	57	85	75	2.9	12.1	2.8	5.9	5.5	5.5	4.2	5.1
IX	–	–	–	–	21.0	7.4	28.9	2	-2.1	23	10.7	20.5	12.7	14.2	12.1	12.9	12.7	12.6	92	55	86	78	1.3	12.0	2.3	5.2	5.3	4.7	3.2	4.4
X	–	–	–	–	17.0	4.7	22.4	20	-2.0	22	7.4	16.5	9.6	10.8	9.0	10.3	9.7	9.7	87	57	82	75	1.7	8.8	2.5	4.3	6.6	5.6	3.5	5.2
XI	–	–	–	–	7.9	0.4	16.6	3	-7.2	23	2.5	7.1	3.5	4.2	6.9	8.1	7.4	7.5	91	79	91	87	0.7	2.4	0.7	1.3	7.8	7.4	7.2	7.5
XII	–	–	–	–	-0.6	-9.0	18.5	5	-30.0	26	-5.0	-2.3	-5.4	-4.5	4.3	4.7	4.2	4.4	85	81	87	84	1.1	1.5	0.9	1.2	7.7	7.5	6.3	7.2
Rok	–	–	–	–	13.7	3.2	33.5	11.VIII	-30.0	26.XII	6.6	12.5	7.5	8.5	9.3	9.7	9.7	9.6	85	64	84	78	1.9	7.4	2.1	3.8	6.6	6.4	5.4	6.1

Libertów — φ = 49°58' — λ = 19°53'

I	–	–	–	–	-0.1	-7.2	9.7	4	-20.3	26	-5.4	-1.7	-3.7	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.5	5.3	6.3
II	–	–	–	–	4.5	-0.5	13.5	28	-6.9	6	0.5	3.4	1.9	1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.2	6.8	7.4
III	–	–	–	–	9.1	2.8	18.9	18	-2.5	28	4.0	7.4	5.7	5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.2	5.7	7.2
IV	–	–	–	–	16.5	6.2	24.2	15	-0.6	10	8.1	15.1	10.9	11.3	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.2	3.8	4.3
V	–	–	–	–	15.9	7.9	22.9	6	2.8	12	9.6	14.5	11.1	11.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.6	6.7	6.9
VI	–	–	–	–	22.8	13.0	31.1	27	9.7	21,29	15.5	21.2	17.0	17.7	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.5	6.0	5.4
VII	–	–	–	–	20.9	12.5	29.2	3	8.7	8	14.6	19.1	16.1	16.5	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.9	5.7	5.7
VIII	–	–	–	–	21.5	13.1	31.3	11	8.4	14	14.9	20.4	17.0	17.3	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.8	3.9	4.7
IX	–	–	–	–	20.4	11.1	27.9	17	1.2	23	12.4	19.1	15.4	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	3.5	2.5	3.6
X	–	–	–	–	16.0	7.0	20.0	20	0.5	22	8.4	15.0	11.3	11.5	–	–	–	–	–	–	–	–	–	–	–	–	5.3	4.2	3.0	4.2
XI	–	–	–	–	6.6	1.7	15.5	3	-4.6	21	2.8	5.7	4.0	4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	6.5	7.0
XII	–	–	–	–	-0.5	-7.5	17.3	5	-20.3	25	-5.0	-2.2	-4.1	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.0	4.9	6.6
Rok	–	–	–	–	12.8	5.0	31.3	11.VIII	-20.3	26,1,25XII	6.7	11.4	8.6	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.8	5.1	5.8

Jastrzębie - Zdrój — φ = 49°57' — λ = 18°34'

I	–	–	–	–	1.3	-6.5	11.9	4	-17.8	27	-4.2	0.2	-3.3	-2.6	4.2	4.6	4.3	4.4	86	70	83	80	0.6	2.0	0.8	1.1	6.9	5.7	5.9	6.2
II	–	–	–	–	5.5	-1.1	12.1	18	-9.3	6	0.1	4.5	1.5	1.9	5.8	6.3	6.1	6.1	92	76	89	86	0.5	2.2	0.7	1.1	8.6	6.6	6.4	7.2
III	–	–	–	–	11.0	1.5	19.6	10,18	-2.6	20	3.6	9.0	5.4	5.8	6.9	7.1	7.3	7.1	87	62	82	77	1.2	4.8	1.9	2.6	8.0	6.6	6.1	6.9
IV	–	–	–	–	18.7	4.7	25.1	15	-4.4	10	8.5	17.3	10.2	11.6	8.9	9.0	9.7	9.2	80	47	78	68	2.4	11.5	2.9	5.6	5.3	4.8	4.5	4.9
V	–	–	–	–	17.9	6.1	24.5	26	1.5	2,15	9.9	15.7	9.9	11.4	10.8	11.0	10.8	10.9	88	62	88	80	1.5	7.4	1.5	3.5	7.2	7.1	7.6	7.3
VI	–	–	–	–	24.2	10.6	32.6	27	5.3	21	15.6	21.6	15.6	17.1	14.7	14.7	15.6	15.0	83	58	88	76	3.2	11.5	2.4	5.7	4.9	5.5	5.8	5.4
VII	–	–	–	–	21.4	10.8	29.9	3	6.0	11	14.7	19.8	14.3	15.8	14.6	14.7	15.0	14.8	87	64	92	81	2.4	9.0	1.4	4.3	5.9	6.9	6.3	6.4
VIII	–	–	–	–	22.2	10.9	29.5	6	5.6	14	14.6	20.8	14.8	16.2	15.7	16.9	15.6	16.1	93	68	87	83	1.2	8.4	1.6	3.7	6.1	6.4	4.0	5.5
IX	–	–	–	–	–	7.7	30.0	17	0.6	23	11.0	20.9	12.5	14.2	12.0	15.0	12.8	13.3	99	60	88	82	1.5	10.3	1.8	4.5	3.7	4.5	3.9	4.0
X	–	–	–	–	–	5.0	–	–	0.4	16,22,25	6.8	16.1	9.3	10.4	9.2	11.4	10.1	10.2	92	63	86	80	0.9	7.1	1.8	3.3	7.0	5.2	4.3	5.5
XI	–	–	–	–	6.9	1.1	14.6	3	-5.0	21	2.8	6.2	3.3	3.9	7.0	7.8	7.2	7.3	91	82	91	88	0.7	1.9	0.8	1.1	7.5	7.2	7.0	7.2
XII	–	–	–	–	0.3	-7.7	17.8	5	-25.2	26	-3.9	-1.0	-4.0	-3.2	4.5	5.2	4.3	4.7	81	80	81	81	1.0	1.4	1.0	1.1	8.0	6.1	7.1	7.1
Rok	–	–	–	–	–	3.6	32.6	27.VI	-25.2	26.XII	6.6	12.6	7.5	8.5	9.5	10.3	9.9	9.9	88	66	86	80	1.4	6.5	1.6	3.2	6.6	6.0	5.7	6.1

Wieliczka

$H_s = 225\ m$ $h_w = 20{,}4\ m$ **1961**

MIESIĄC	ROZKŁAD WIATRU [%D, vmD]																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr			Opad R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	> 10	> 15		0.1 ≤ R < 1.0	1.0 ≤ R < 10.0	R ≥ 10.0			ΣR
I	3	1,2	13,5	1,7	13,5	1,2	3,5	1,1	13	3,2	24,5	1,7	7	4,5	3	2,3	12	1,8	17,8	5,0	4	14	15	27	·	2	1	–	–	9	6	·	10	19	·
II	1,5	1,0	5	1,2	11,5	1,3	6,5	1,7	17,5	1,9	26	2,7	6	3,2	1	1,0	9	1,9	28,7	5,8	19	·	·	12	·	·	·	–	–	14	8	·	7	3	·
III	2,5	2,8	·	·	·	·	·	·	1,7	3,0	4,5	4,2	18,5	5,1	7	4,4	3	4,0	36,6	7,0	18	·	·	5	·	3	1	–	–	15	11	·	2	2	·
IV	·	·	1,2	3,2	3,0	1,6	5,5	1,0	13,5	2,6	15,5	3,4	4,5	2,0	1	4,5	8	2,2	23,4	19,4	1	·	·	3	2	3	1	7	6	4	3	1	1	·	2
V	4	2,2	10,5	1,7	6,5	1,4	5	1,6	8,5	2,2	3,1	2,1	1,4	2,1	3,5	1,9	10	1,8	111,8	20,3	6	·	·	·	·	·	·	15	18	15	4	·	·	8	
VI	3	1,3	5	1,6	7,5	1,4	9,5	1,5	2,3	2,1	28,5	1,9	7,5	2,4	1	4,0	5	1,8	93,0	24,6	12	·	·	·	10	2	2	1	8	15	12	2	3	·	8
VII	3	1,2	2	1,2	1,5	1,3	2,5	1,2	14,5	3,2	4,2	2,9	1,3	3,7	7,5	1,9	7	2,6	112,2	19,3	30	·	·	·	9	4	2	–	–	16	12	6	·	·	4
VIII	1	1,0	3	2,0	8	1,8	1	2,5	1,6	2,6	3,2	3,0	1,6	2,8	4	2,5	12	2,3	73,6	30,4	12	·	·	·	8	4	1	1	9	8	7	3	1	·	3
IX	0,5	1,0	1,2	1,6	1,6	1,4	3,5	1,3	1,2	1,4	27,5	2,4	1,0	3,3	0,5	1,0	8	1,8	22,4	10,5	26	·	·	·	8	2	2	9	8	9	4	1	6	·	3
X	1	1,5	9,5	1,7	2,7	2,0	1,1	3,0	1,1	1,3	16,5	1,7	5	1,9	4	2,4	8	1,8	8,6	6,4	30	·	·	1	·	·	·	–	–	4	2	·	9	·	·
XI	1,5	3,0	1,0	1,7	6	1,5	6	1,2	6,5	2,5	3,3	1,7	1,6	2,6	7	1,3	4	1,8	74,8	25,9	4	·	·	10	·	1	·	–	–	16	10	2	14	1	·
XII	5	2,0	1,2	1,5	8	1,2	1,5	2,3	9	3,7	2,2	3,6	1,3	3,0	8,5	3,0	14	2,4	74,5	30,4	6	15	17	26	·	1	·	–	–	15	8	3	12	24	·
Rok	26	1,5	94,5	1,6	135,5	1,3	55,5	1,5	161,5	2,5	343,5	2,6	130,5	3,0	48	2,5	100	2,2	677,4	30,4	12 VIII, 6 XII	29	32	84	37	22	10	–	–	143	98	22	65	49	28

Bochnia - Chodenice

$H_s = 200\ m$ $h_w = 14{,}9\ m$

I	3,5	2,4	15,5	1,7	1,5	2,3	1,5	4,0	1,1	2,7	1,7	4,6	2,6	2,4	1,4	2,5	3	2,7	15,3	4,7	5	14	15	26	·	2	1	5	13	10	4	·	5	20	·
II	5,5	1,2	3,5	2,0	5,5	2,1	5,5	2,1	8	1,8	1,5	2,6	3,3	2,9	1	2,6	1	2,4	19,9	4,7	9	·	·	18	·	·	·	2	14	15	7	·	3	2	·
III	2	4,2	·	·	·	·	·	·	·	·	1,5,5	4,2	5,9	5,8	1,6,5	5,6	·	5,5	25,4	6,8	31	·	·	6	·	8	3	1	12	16	9	·	1	2	·
IV	6,5	1,8	8	2,4	2,3,5	3,0	10,5	3,4	4	2,2	11,5	3,3	1,8	3,4	7	5,1	1	3,1	13,8	4,5	1	·	·	5	1	1	·	8	6	9	4	·	1	·	2
V	4	2,1	8,5	2,2	10,5	2,0	5	1,3	4	2,1	10,5	2,0	3,2	3,5	1,6,5	2,9	2	2,6	78,7	19,2	6	·	·	·	·	·	·	1	15	17	14	2	2	·	9
VI	5	1,9	3	1,5	7,5	2,3	5	2,9	7,5	2,0	8,5	1,7	3,7	2,7	12,5	2,7	4	2,3	121,2	34,4	11	·	·	·	9	·	·	8	7	13	11	4	·	·	10
VII	1	1,5	1	2,0	2	1,0	2,5	2,0	4	2,6	10,5	2,5	4,8	3,1	2,0	2,2	4	2,6	110,1	31,6	30	·	·	·	8	1	1	3	11	16	13	3	·	·	8
VIII	7	1,5	7,5	2,1	0,5	1,0	6,5	1,3	1	1,0	7	3,9	3,8,5	3,0	2,4	3,0	1	2,7	64,4	20,6	12	·	·	·	7	·	·	7	7	8	6	2	·	·	4
IX	2,5	1,6	8,5	1,6	1,1	2,0	6	1,8	·	·	2,5	2,4	3,5,5	2,7	1,9	2,8	5	2,3	31,5	15,1	4	·	·	2	6	·	·	11	6	7	3	1	5	·	2
X	1	1,5	7,5	1,9	17,5	1,9	1,9	3,8	12,5	3,8	1,0	1,8	1,8,5	2,0	7	1,5	·	2,5	18,0	10,5	30	·	·	1	·	·	·	6	8	6	4	1	2	·	·
XI	5	1,5	0,5	1,0	8,5	1,7	1,0	1,4	8,5	1,4	1,4	2,0	3,7	2,5	6,5	3,2	·	2,1	66,3	19,3	4	·	·	11	·	·	·	3	16	16	11	2	4	1	·
XII	7,5	3,1	9	2,0	7,5	1,3	2,5	1,4	2	4,2	10,5	6,0	3,3,5	3,3	1,2,5	3,4	8	3,0	53,6	25,5	6	15	18	26	·	3	·	3	15	13	6	2	5	24	·
Rok	50,5	2,0	72,5	1,7	95,5	1,7	7,4	2,1	62,5	2,0	132,5	3,1	4,1,6	3,1	1,6,2,5	3,1	2,9	2,8	618,2	34,4	11.VI	29	33	95	31	15	5	58	130	146	92	17	28	49	35

Libertów

$H_s = 320\ m$ $h_w = 15{,}9\ m$

I	5,5	2,1	6,5	1,2	1,6	2,0	5	2,0	9,5	2,4	12,5	3,1	2,4	2,0	1,0	1,3	4	2,0	18,3	5,9	4	11	14	24	·	·	·	3	10	7	6	·	7	–	·
II	4,5	1,0	4,5	1,4	5	1,6	5	1,6	12,5	1,9	1,1	2,1	3,9,5	2,5	2	1,0	·	2,1	32,6	7,8	19	·	1	15	·	·	·	2	14	12	11	·	7	–	·
III	0,5	1,0	·	·	·	·	·	·	5	5,8	1,2	4,2	6,8	4,4	7,5	4,7	·	4,4	54,1	8,7	3	·	·	5	·	3	·	2	14	17	14	·	4	–	·
IV	3	1,3	15,5	2,2	2,1,5	2,9	5	2,0	9,5	3,5	12,5	3,0	1,8	2,7	2	1,5	3	2,6	11,9	5,6	1	·	·	1	·	1	·	9	4	6	3	·	2	·	2
V	8	1,9	6	2,2	6	2,5	6,5	1,1	9,5	1,7	10,5	2,4	3,6,5	2,1	4	2,0	6	1,9	93,8	17,2	6	·	·	·	·	·	·	1	10	17	15	2	·	·	7
VI	7	1,1	8	1,2	14	1,4	7	1,4	3	2,3	8	1,4	3,4	1,7	8	1,2	1	1,5	176,5	60,0	9	·	·	·	5	·	·	5	9	14	14	5	1	·	8
VII	5,5	1,4	1	1,0	2	1,0	2	1,0	11	2,0	10	1,8	4,9	2,5	8,5	1,8	4	2,0	114,1	20,0	28	·	·	·	8	·	·	4	8	14	13	5	·	·	6
VIII	7	1,1	5	1,2	6	1,5	3	1,3	12	2,9	16	2,4	3,7	2,3	6	1,3	1	2,1	51,3	30,6	12	·	·	·	6	·	·	8	4	7	5	1	2	·	3
IX	5,5	1,0	11,5	1,7	14	1,7	1	1,0	12	1,2	5	1,4	3,3,5	1,9	2,5	1,0	5	1,5	21,2	11,6	26	·	·	·	5	·	·	13	5	5	3	1	4	·	3
X	3	1,3	7	1,6	2,5,5	1,8	1,4	2,0	7	2,1	5,5	2,1	2,6	1,7	3	1,3	2	1,8	9,4	7,6	30	·	·	·	·	·	·	11	6	3	2	·	7	·	·
XI	10	2,1	7	2,4	6	1,8	5	1,8	10	2,4	4,5	3,0	4,4,5	2,6	3	2,0	·	2,4	40,0	10,5	4	·	·	9	·	·	·	3	15	13	8	1	10	–	·
XII	12,5	3,4	7,5	2,8	12,5	1,7	4,5	2,0	8	5,1	8,5	5,4	3,4,5	3,1	5	3,4	·	3,3	56,9	20,3	6	14	18	27	·	·	·	3	13	13	6	3	6	–	·
Rok	72	1,6	79,5	1,6	128,5	1,7	58	1,4	109	2,8	116	2,7	444,5	2,5	61,5	1,9	26	2,3	680,1	60,0	9.VI	25	33	81	24	4	·	64	112	128	100	18	50	–	29

Jastrzębie - Zdrój

$H_s = 227\ m$ $h_w = 12{,}5\ m$

I	·	·	2,2	2,0	7	2,9	5	1,1	4	1,6	14	3,2	19,5	2,6	5,5	1,8	16	1,9	13,7	5,9	4	10	12	28	·	·	·	5	11	9	5	·	·	27	·
II	3	1,0	2	1,5	7,5	1,3	2	1,0	6	1,4	19	3,2	17,5	2,1	7	1,5	20	1,6	93,3	34,8	9	·	·	19	·	·	·	2	12	15	13	2	6	2	·
III	0,5	2,0	·	·	·	·	1	1,0	1,5	1,0	1,5	4,2	3,6	3,2	2,6	2,2	1,3	2,5	72,3	17,4	14	·	·	12	·	·	·	1	13	18	9	2	1	2	1
IV	2,5	1,8	18,5	1,9	1,0	2,3	1,1	1,3	5	1,1	1,0	2,2	9	3,9	1,4	1,3	1,0	1,8	9,3	3,2	1	·	·	1	1	1	·	6	5	5	4	·	1	·	1
V	6,5	1,2	7,5	1,5	2,5	1,6	·	·	3	1,0	7,5	2,9	15,5	2,5	3,0,5	1,7	2,0	1,5	76,5	19,4	29	·	·	·	·	·	·	·	9	16	15	2	1	·	3
VI	1,5	1,7	2,5	1,6	7	1,4	3	1,2	2	1,0	9	2,2	6	2,2	3,0	1,5	2,9	1,1	95,1	39,2	27	·	·	·	11	·	·	5	6	12	9	4	2	·	6
VII	0,5	1,0	5	1,0	0,5	1,0	2	1,0	2	1,0	6	3,0	3,0	2,6	1,6	1,3	3,1	1,4	124,6	36,2	15	·	·	·	7	·	·	3	7	15	14	4	·	·	4
VIII	2,5	1,0	2	1,5	1	1,0	0,5	1,0	2,5	1,0	1,4	2,6	1,9	2,3	2,2,5	1,5	2,9	1,3	60,2	24,3	12	·	·	·	7	·	·	3	3	13	10	2	·	·	1
IX	1,5	1,0	7	2,1	9	2,2	·	·	2	1,0	9,5	2,2	2,4	2,7	4,0	1,2	2,7	1,5	15,1	6,4	14	·	·	·	6	·	·	13	4	6	2	·	3	·	1
X	5,5	1,8	1,6	1,8	1,6	1,5	6,5	1,8	2	1,5	8	2,0	7,5	2,2	1,1,5	1,5	2,0	1,4	7,7	2,9	1,9	·	·	·	·	·	·	2	7	7	3	·	5	·	·
XI	8	1,0	5,5	1,5	2,5	2,2	3	1,0	1	1,0	1,5,5	2,7	1,4,5	1,5	2,3	1,3	1,7	1,3	72,7	36,0	4	·	·	8	·	·	·	2	15	16	10	2	6	4	·
XII	4,5	1,0	1,9	1,4	4,5	1,0	3,5	1,3	2	3,5	1,6	3,0	1,0	2,8	1,7,5	1,4	1,6	1,6	63,1	16,8	11	10	14	25	·	·	·	3	12	12	10	3	4	22	·
Rok	36,5	1,2	1,0,7	1,5	6,2,5	1,5	3,7,5	1,0	33	1,3	1,4,3,5	2,8	2,0,8,5	2,6	2,1,3,5	1,5	2,4,8	1,6	70,36	39,2	27.VI	20	26	93	32	1	·	45	104	144	104	21	29	57	17

Goczałkowice

$\varphi = 49°57'$ $\lambda = 18°55$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	-7.3	11.2	4	-19.2	27	-4.7	-0.7	-3.6	-3.2	4.1	4.7	4.4	4.4	86	77	85	83	0.7	1.5	0.9	1.0	6.3	5.3	4.8	5.5
II	–	–	–	–	4.5	-1.5	12.0	18	-9.6	6	0.1	3.4	1.0	1.4	5.7	6.2	6.0	6.0	92	81	91	88	0.5	1.7	0.6	0.9	8.0	6.5	6.0	6.8
III	–	–	–	–	9.6	2.1	18.2	10	-2.3	20	4.0	7.8	5.5	5.7	7.1	7.2	7.6	7.3	89	69	84	80	1.2	3.7	1.6	2.2	7.6	6.1	6.2	6.6
IV	–	–	–	–	16.9	4.7	24.2	6	-2.3	10	8.5	15.7	9.9	11.0	8.8	9.2	9.5	9.2	78	52	77	69	2.7	9.1	3.0	4.9	4.5	4.4	3.7	4.2
V	–	–	–	–	16.4	6.9	22.6	27	2.9	12	10.0	15.0	10.7	11.6	10.2	10.5	10.7	10.5	83	62	82	76	2.3	7.1	2.3	3.9	6.6	6.9	6.7	6.7
VI	–	–	–	–	23.0	11.7	30.2	27	5.7	21	15.4	20.9	16.6	17.4	14.4	15.1	15.5	15.0	82	62	82	75	3.2	10.1	3.6	5.6	3.9	5.0	5.1	4.7
VII	–	–	–	–	21.0	12.2	30.9	2	6.9	8	15.0	19.1	15.9	16.5	13.4	13.6	14.3	13.8	79	63	79	74	3.9	9.2	4.0	5.7	5.5	6.1	6.3	6.0
VIII	–	–	–	–	21.5	12.5	29.1	10	6.7	31	15.3	20.1	16.6	17.2	14.9	15.4	15.5	15.3	85	65	81	77	2.8	8.7	3.7	5.1	5.4	4.4	4.5	4.8
IX	–	–	–	–	21.2	9.2	28.4	5	1.2	22	12.0	19.8	14.3	15.1	11.8	13.8	13.3	13.0	83	60	80	74	2.7	10.0	3.6	5.4	4.2	3.9	3.0	3.7
X	–	–	–	–	16.1	5.8	21.2	6	0.9	22	8.6	15.4	10.4	11.2	9.7	10.4	10.3	10.1	88	60	82	77	1.6	7.3	2.5	3.8	6.2	5.2	3.4	4.9
XI	–	–	–	–	6.8	0.9	14.2	3	-4.6	21	3.0	5.6	3.6	4.0	7.0	7.4	7.2	7.2	90	80	90	87	0.8	2.0	0.9	1.2	7.5	7.2	7.3	7.3
XII	–	–	–	–	0.0	-8.4	16.2	5	-26.6	26	-4.6	-2.3	-4.2	-3.8	4.4	4.8	4.3	4.5	84	83	82	83	0.9	1.2	1.0	1.0	7.4	6.8	6.5	6.9
Rok	–	–	–	–	13.1	4.1	30.9	2.VII	-26.6	26.XII	6.9	11.6	8.1	8.7	9.3	9.9	9.9	9.7	85	68	83	79	1.9	6.0	2.3	3.4	6.1	5.6	5.3	5.7

Wadowice

$\varphi = 49°53'$ $\lambda = 19°31'$

I	–	–	–	–	0.8	-7.5	12.2	4	-18.7	27	-4.4	-0.6	-3.8	-3.2	4.0	4.4	4.1	4.2	84	74	83	80	0.9	1.9	1.0	1.3	7.1	6.4	5.2	6.2
II	–	–	–	–	5.6	-1.3	13.9	28	-9.2	6	-0.1	4.4	1.5	1.8	5.5	6.1	5.9	5.8	90	74	86	83	0.6	2.4	1.0	1.3	8.5	7.1	7.2	7.6
III	–	–	–	–	10.1	2.5	19.6	18	-1.8	23	4.2	8.1	6.3	6.2	6.7	6.7	7.0	6.8	81	63	74	73	1.8	4.5	2.7	3.0	8.4	7.7	6.2	7.4
IV	–	–	–	–	17.6	5.2	25.5	15	-1.5	10	8.9	16.4	10.1	11.4	8.5	8.5	9.2	8.7	73	47	74	65	3.3	10.8	3.4	5.8	5.7	5.3	4.5	5.2
V	–	–	–	–	16.9	6.6	23.9	6	2.8	15	10.2	15.2	10.7	11.7	10.1	9.9	10.7	10.2	81	58	83	74	2.6	8.0	2.3	4.3	7.7	7.8	7.7	7.7
VI	–	–	–	–	23.4	11.2	32.0	27	6.5	21	16.3	21.4	15.7	17.3	14.5	13.8	15.2	14.5	78	55	85	73	4.3	12.3	2.7	6.4	5.4	6.4	7.0	6.3
VII	–	–	–	–	21.8	11.0	30.2	3	6.0	8	15.0	19.7	15.1	16.2	13.3	13.5	14.0	13.6	78	60	81	73	4.0	10.6	3.5	6.0	6.5	7.5	7.0	7.0
VIII	–	–	–	–	22.2	11.7	32.0	11	6.8	14	15.1	21.1	15.5	16.8	14.0	14.2	15.1	14.4	80	56	84	73	3.5	11.9	2.9	6.1	6.5	6.7	4.6	5.9
IX	–	–	–	–	21.5	8.9	30.6	17	1.8	23	11.5	20.6	13.2	14.6	11.6	12.6	12.8	12.3	84	53	83	73	2.4	12.4	2.7	5.8	5.3	5.1	3.8	4.7
X	–	–	–	–	16.7	5.5	21.1	8	0.8	25	7.0	16.0	9.0	10.2	9.2	10.0	9.9	9.7	90	57	86	78	1.1	8.5	1.7	3.8	7.1	6.5	4.7	6.1
XI	–	–	–	–	7.2	0.5	15.5	3	-6.7	24	2.5	6.2	3.2	3.8	6.7	7.2	7.0	7.0	89	76	89	85	4.0	2.6	0.9	1.5	8.4	8.3	7.6	8.1
XII	–	–	–	–	0.2	-8.6	19.8	5	-27.2	26	-5.2	-2.0	-4.8	-4.2	4.2	4.7	4.2	4.4	83	81	84	83	1.1	1.6	1.1	1.3	8.3	7.9	6.6	7.6
Rok	–	–	–	–	13.7	3.8	32.0	27.VI, 11.VII	-27.2	26.XII	6.8	12.2	7.6	8.6	9.0	9.3	9.6	9.3	83	63	83	76	2.2	7.3	2.2	3.9	7.1	6.9	6.0	6.7

Żarnowa

$\varphi = 49°52'$ $\lambda = 21°50'$

I	–	–	–	–	-0.6	-7.6	9.6	4	-25.4	27	-4.6	-2.0	-4.1	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.2	5.4	6.3
II	–	–	–	–	3.6	-0.8	11.1	18	-4.9	6	0.2	2.9	1.1	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.5	7.0	7.6
III	–	–	–	–	9.5	2.6	17.8	10	-3.4	23	4.0	7.9	5.5	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.2	5.1	6.6
IV	–	–	–	–	17.0	4.3	24.2	15	-3.3	10	7.0	15.8	10.4	10.9	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.0	3.4	4.3
V	–	–	–	–	16.8	6.8	24.5	29	1.7	20	9.4	15.5	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	8.3	6.8	5.4	6.8
VI	–	–	–	–	24.0	10.9	31.5	27	5.1	21	15.2	22.4	15.8	17.3	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.2	4.7	5.0
VII	–	–	–	–	22.5	10.4	31.0	4	5.6	7	14.4	21.0	14.7	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.3	6.0	6.0
VIII	–	–	–	–	22.8	11.7	32.4	11	5.3	31	14.5	21.5	16.3	17.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.7	4.6	5.5
IX	–	–	–	–	21.2	8.1	28.3	17,18	0.6	22	10.7	19.8	13.0	14.1	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.4	2.9	4.1
X	–	–	–	–	16.6	6.8	24.9	20	0.7	12	8.4	16.0	11.0	11.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.8	2.9	4.4
XI	–	–	–	–	8.1	2.9	15.8	7	-6.2	21	4.5	7.0	5.2	5.5	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.2	6.5	7.3
XII	–	–	–	–	0.1	-7.6	12.3	6	-32.2	25	-4.2	-1.4	-3.4	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	6.8	7.2
Rok	–	–	–	–	13.5	4.0	32.4	11.VIII	-32.2	25.XII	6.6	12.2	8.0	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.1	5.1	5.9

Ochaby

$\varphi = 49°51'$ $\lambda = 18°46'$

I	–	–	–	–	1.1	-6.0	11.5	4	-18.3	27	-3.9	0.1	-2.6	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.1	5.9	6.2
II	–	–	–	–	5.3	-0.7	13.1	18	-10.3	6	0.4	4.5	1.5	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.0	6.2	7.1
III	–	–	–	–	10.1	1.7	19.9	10	-3.4	29	4.0	8.6	5.7	6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	5.9	6.9
IV	–	–	–	–	17.5	5.4	24.7	6,15	-1.4	10	9.5	16.6	10.8	11.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.3	3.8	4.9
V	–	–	–	–	16.4	6.8	24.5	6	2.0	2	10.0	15.1	10.2	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	7.1	7.3
VI	–	–	–	–	23.0	11.4	31.0	27	5.4	21	16.3	21.4	15.8	17.3	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.0	5.8	5.5
VII	–	–	–	–	21.1	11.5	30.4	3	6.0	8	15.4	19.4	15.1	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.5	6.4	6.7
VIII	–	–	–	–	22.0	12.2	30.4	6	6.6	31	15.5	20.8	15.7	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.0	5.0	5.6
IX	–	–	–	–	21.6	8.7	29.4	17	0.1	23	11.8	20.7	13.6	14.9	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.5	2.8	3.8
X	–	–	–	–	16.5	5.9	21.8	6	0.3	11	8.1	15.9	10.2	11.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.9	4.5	5.8
XI	–	–	–	–	7.1	0.6	15.3	3	-5.3	23	2.9	6.3	3.2	3.9	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.0	7.1	7.8
XII	–	–	–	–	0.6	-8.2	18.6	5	-28.0	25	-4.5	-1.5	-4.2	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.7	7.5	7.6
Rok	–	–	–	–	13.5	4.1	31.0	27.VI	-28.0	25.XII	7.1	12.3	7.9	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	5.7	6.3

1961

Goczałkowice

$H_s = 260$ m $h_w = 10$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	═	⊠	R
I	2.5	3.4	15	2.5	9	5.2	·	·	10	6.4	17.5	6.7	12	4.0	4	2.1	23	3.6	17.6	4.3	4	11	12	26	·	3	2	6	10	9	6	·	3	17	·
II	1	5.0	2	4.5	·	·	1.5	1.0	1	2.5	17.5	4.1	21	3.6	8	2.8	32	2.2	45.8	10.4	9	·	1	20	·	1	1	4	15	16	8	1	13	2	·
III	0.5	5.0	·	·	·	·	·	·	0.5	7.0	24	7.5	41	4.9	17	5.4	10	5.2	30.0	7.5	14	·	·	5	·	11	5	3	14	16	7	·	2	3	1
IV	3	1.3	13	3.8	15	3.4	·	·	1.5	6.0	13	4.7	11.5	3.7	3	2.3	30	2.5	10.7	3.8	4	·	·	1	·	4	2	10	2	6	3	·	1	·	2
V	6	3.2	3	3.3	3	3.3	·	·	1	5.0	9	5.9	21	3.7	11	2.9	39	2.2	64.1	13.6	6	·	·	·	·	2	·	·	10	16	13	1	5	·	9
VI	3.5	2.9	1.5	1.7	7.5	2.9	1.5	1.3	2	3.5	9.5	4.0	21	2.9	9.5	3.3	34	1.9	115.5	40.5	27	·	·	·	7	1	·	7	5	11	11	2	2	·	11
VII	3	2.3	·	·	1	2.5	1	2.5	2.5	2.4	9.5	5.2	34	5.4	7	2.7	35	2.9	91.9	28.4	30	·	·	·	6	1	·	4	10	15	11	3	·	·	3
VIII	1	1.0	4	2.2	4	2.0	·	·	4	6.9	17.5	4.6	17.5	4.9	9	2.7	36	2.5	86.0	27.6	9	·	·	·	5	4	·	7	4	9	6	4	3	·	2
IX	1	1.5	8	2.6	3	4.7	·	·	1.5	1.0	10	5.9	15.5	3.6	5	3.4	46	1.9	13.7	7.6	26	·	·	·	6	·	·	13	3	5	3	·	5	·	1
X	1	4.0	12.5	4.0	14.5	4.2	1	3.0	3.5	9.6	10.5	6.0	6	4.5	6	2.5	38	2.8	1.7	1.1	29	·	·	·	·	3	·	4	7	3	1	·	7	·	·
XI	4	2.5	8.5	2.4	1	4.0	·	·	5	6.7	12.5	5.1	15.5	4.4	0.5	2.0	43	2.2	82.5	38.6	4	·	·	13	·	2	1	2	16	10	7	3	7	3	·
XII	7.5	3.4	16	2.9	3	2.3	·	·	3.5	10.3	15.5	9.5	12	6.5	6.5	3.2	29	3.9	60.6	28.1	6	15	17	26	·	6	4	3	15	11	6	3	4	21	·
Rok	34	3.0	83.5	2.5	61	2.9	5	0.6	36	5.6	166	5.8	228	4.3	86.5	2.9	395	2.8	620.1	40.5	27.VI	26	30	91	24	38	15	63	111	127	82	17	52	46	29

Wadowice

$H_s = 260$ m $h_w = 21{,}4$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	═	⊠	R
I	1	1.0	5.5	1.6	20.5	1.8	10.5	1.4	10.5	3.4	15	2.9	12	1.6	3	1.0	15	1.8	21.3	10.2	4	11	14	27	·	2	·	6	14	10	4	1	4	22	·
II	7	1.0	2	1.0	7	1.0	10.5	1.0	12.5	1.0	13	2.5	49.5	2.0	1.5	1.3	11	1.3	39.3	13.3	9	·	·	19	·	·	·	2	18	13	10	1	6	5	·
III	1	1.0	1	1.0	·	·	3.5	1.0	1.5	1.0	30.5	4.1	45.5	3.9	2	5.5	8	3.4	50.2	10.2	14	·	·	7	·	3	·	1	16	16	13	1	1	1	1
IV	5	1.0	6	1.7	23	2.3	11	1.2	10.5	1.5	12	3.6	11	3.0	5.5	1.8	6	2.2	23.1	5.7	4	·	·	1	1	3	·	8	5	8	7	·	·	·	4
V	1	2.0	3	2.0	6	2.2	5	1.0	13	1.3	49.5	1.7	26	2.3	4.5	2.6	15	1.6	89.2	19.0	6	·	·	·	·	·	·	·	15	20	15	1	2	·	7
VI	·	·	1.5	2.0	9.5	2.2	2.5	1.0	28	1.1	13	1.6	23.5	2.3	2	2.0	10	1.5	75.9	17.3	27	·	·	·	8	1	·	3	10	15	13	3	·	·	10
VII	1	1.0	·	·	·	·	·	·	28.5	1.0	30	1.6	25	2.4	2.5	1.2	6	1.5	122.5	26.8	28	·	·	·	8	1	·	2	13	16	13	5	·	·	8
VIII	3	1.3	2	2.0	6	1.2	10	1.3	14	1.1	23	2.0	28.5	2.1	0.5	2.0	6	1.6	105.2	50.8	12	·	·	·	7	·	·	3	6	10	8	3	1	·	3
IX	1	1.0	4	1.8	13	1.8	16.5	1.1	13.5	1.1	10.5	2.1	17	2.9	4.5	1.8	10	1.6	23.6	17.6	26	·	·	·	6	·	·	10	9	5	4	1	3	·	2
X	3	1.0	4	1.8	22	2.0	15	1.1	13	1.8	7	1.3	13.5	2.0	0.5	3.0	15	1.4	14.9	9.8	30	·	·	·	·	·	·	2	8	8	4	·	4	·	·
XI	2	1.0	4	1.0	6	1.2	12	1.0	9	1.1	13	2.2	18.5	2.2	5.5	1.2	20	1.2	86.6	37.4	4	·	·	9	·	·	·	·	18	17	10	2	8	3	·
XII	4	1.0	2	1.0	13	1.1	4	1.0	12.5	1.6	19.5	4.7	18.5	2.0	7.5	1.5	12	2.0	79.8	34.9	6	14	17	27	·	2	·	1	17	18	9	2	4	23	·
Rok	29	1.0	35	1.7	126	1.4	100.5	1.0	166.5	1.4	206	2.5	258.5	2.4	39.5	2.1	134	1.8	731.6	50.8	12.VIII	25	31	90	30	12	·	38	149	156	110	20	33	54	35

Żarnowa

$H_s = 256$ m $h_w = 18{,}3$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	═	⊠	R
I	17.5	3.8	1	2.0	8	2.0	7	2.7	42	5.5	5	3.2	9	2.7	2.5	4.0	1	4.1	21.6	4.8	14	10	14	24	·	5	2	3	10	8	7	·	·	23	–
II	13	4.9	2	3.0	7	2.9	6	2.5	31.5	4.0	7.5	3.5	9	2.4	4	2.8	4	3.1	23.7	8.5	10	·	1	17	·	1	·		13	10	6	·	·	1	–
III	10.5	4.3	3	2.7	6	1.7	1	5.0	12	5.9	11	3.7	26	5.5	22.5	5.8	1	4.9	27.8	6.4	31	·	·	6	·	4	2	1	8	13	8		1	1	–
IV	19.5	2.7	14.5	3.0	16	5.4	5	2.6	13.5	4.4	5.5	9.5	4	5.5	4	4.4	8	3.9	11.0	3.0	1,29	·	·	2	·	5	1	8	3	5	5	·	·	·	–
V	23.5	2.1	12.5	2.4	4	4.0	4.5	3.4	13.5	3.2	4.5	5.7	12	3.2	9.5	3.5	9	2.7	73.6	18.1	14	·	·	·	·	1	·	1	7	14	11	3	3	·	–
VI	15	3.0	9	2.0	11.5	3.4	15.5	2.6	9	4.6	9.5	3.7	7.5	3.5	9	2.9	4	3.0	24.2	4.4	12	·	·	·	9	1	·	1	3	12	10	·	1	·	–
VII	17	2.1	6	1.3	7	1.4	10.5	3.4	17	3.9	6.5	4.4	11	3.7	8	4.6	10	2.8	112.2	30.7	29	·	·	·	9	1	·	2	4	15	12	3	·	·	–
VIII	18	2.7	10.5	2.0	7	2.4	7	1.9	14.5	4.2	8.5	3.6	13	3.2	6.5	4.2	8	2.8	57.8	14.1	12	·	·	·	9	2	·	5	5	12	8	3	2	·	–
IX	11	2.1	14	2.4	7	2.1	8.5	2.1	21.5	2.7	6	4.0	6.5	2.1	7.5	3.1	8	2.3	25.5	6.8	14	·	·	·	8	·	·	12	5	6	4	·	3	·	–
X	11	2.3	8	4.1	8.5	3.0	16.5	3.0	34.5	4.6	4.5	3.9	1.5	4.3	4.5	3.3	4	3.6	24.4	14.2	30	·	·	·	·	4	·	10	3	6	4	1	2	·	–
XI	16	2.5	2.5	4.0	5.5	2.8	3.5	3.9	41.5	3.4	4	3.2	9	3.0	4	3.5	4	2.9	28.4	6.8	13	·	·	8	·	·	·	2	16	14	8	·	1	·	–
XII	25	2.8	8.5	2.6	5	1.6	4	3.8	24	5.6	4	5.0	4	4.5	14.5	3.3	4	3.6	57.8	18.5	11	12	15	23	·	2	·	1	16	14	10	1	·	24	–
Rok	197	2.7	91.5	2.4	92.5	2.7	89	3.1	274.5	4.3	76.5	4.4	112.5	3.6	96.5	3.8	65	3.3	488.0	30.7	29.VII	22	30	80	35	26	5	46	93	129	93	11	13	49	–

Ochaby

$H_s = 270$ m $h_w = 18$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Opad R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	◐	●	R≥0.1	R≥1.0	R≥10.0	═	⊠	R
I	4	3.4	15	3.8	5	4.1	2.5	2.6	16	6.4	22.5	4.9	4	2.4	4	3.6	20	3.6	19.1	11.4	4	10	11	22	·	5	·	7	13	10	4	1	4	6	·
II	1	2.0	0.5	3.0	1.5	1.0	4.5	2.0	21.5	3.8	23	3.9	9	3.3	2	3.2	21	2.6	61.2	16.1	9	1	·	12	·	·	·	3	16	14	9	1	11	3	·
III	1.5	5.3	·	·	·	·	·	·	7	3.5	29	5.0	22.5	4.9	12	5.1	21	3.8	45.2	9.5	14	·	·	5	·	4	·	3	15	16	11	·	1	3	1
IV	3.5	3.4	12	4.4	6.5	4.6	·	·	12	4.2	13	5.0	6.5	5.8	2.5	3.6	34	2.9	14.2	7.8	1	·	·	1	·	5	1	6	3	8	3	·	1	·	3
V	8.5	2.3	3	2.7	3	4.0	0.5	4.0	6	3.3	16.5	4.5	11.5	4.1	11	3.7	33	2.4	93.1	18.2	6	·	·	·	·	4	·	·	11	17	12	4	2	·	8
VI	2.5	4.2	4.5	2.4	5.5	2.5	4.5	1.8	8.5	2.6	9.5	3.2	12	3.3	10	4.2	33	2.0	138.4	67.4	27	·	·	·	7	2	·	5	6	14	10	5	3	·	12
VII	2.5	1.4	2	1.0	·	·	1.5	1.0	11	3.0	23.5	4.1	16.5	3.4	6	1.9	30	2.2	93.5	22.6	30	·	·	·	7	3	1	4	12	16	14	3	·	·	10
VIII	2	2.0	4	2.5	3	3.3	·	·	8.5	3.7	28.5	3.8	15.5	3.5	5.5	2.7	26	2.5	70.7	23.4	12	·	·	·	7	4	·	4	5	9	6	2	2	·	4
IX	3.5	1.4	9.5	3.6	2.5	3.6	·	·	8	3.1	17.5	4.1	10.5	3.6	4.5	2.8	34	2.2	8.1	5.6	14	·	·	·	7	2	·	13	4	7	2	·	4	·	4
X	3	3.2	8.5	3.6	9	4.0	2	2.2	15	5.2	6.5	4.8	8	3.4	1	2.5	40	2.4	6.7	2.1	29	·	·	·	·	5	·	5	8	8	3	·	7	·	·
XI	5	2.6	1.5	3.3	3.5	3.3	0.5	7.0	9.5	3.1	17.5	3.5	8	4.3	2.5	3.0	42	1.8	91.1	49.2	4	·	·	12	·	1	·	1	18	17	8	2	9	5	·
XII	8.5	2.8	6	3.4	2.5	2.8	1	1.5	7.5	5.4	19	5.9	4	6.9	5.5	4.1	39	2.8	76.7	37.4	6	12	15	25	·	7	·	3	18	15	7	3	9	22	·
Rok	45.5	2.8	66.5	2.8	42	2.8	17	1.8	130.5	3.9	226	4.4	128	4.1	66.5	3.4	373	2.5	718.0	67.4	27.VI	23	26	77	28	42	2	54	129	151	89	21	53	[illegible]	42

Porąbka

$\varphi = 49°49'$ $\lambda = 19°13'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.4	-5.1	11.7	4	-21.3	26	-3.4	-0.2	-2.1	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.8	5.2	5.6
II	–	–	–	–	5.4	-0.9	12.2	18	-10.3	6	0.3	4.0	1.6	1.9	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	6.3	6.5
III	–	–	–	–	10.4	2.8	19.4	18	-3.5	23	4.1	8.1	6.0	6.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.6	7.0	7.6
IV	–	–	–	–	17.7	5.9	25.4	7	-1.2	10	8.6	16.3	9.9	11.2	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.3	3.4	4.4
V	–	–	–	–	17.0	6.9	24.9	27	2.5	15	9.7	14.7	10.2	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.7	7.6	7.9
VI	–	–	–	–	23.3	11.7	31.4	27	6.7	22	14.9	20.9	15.4	16.6	–	–	–	–	–	–	–	–	–	–	–	–	4.4	7.0	5.9	5.8
VII	–	–	–	–	21.7	11.6	30.4	3,12	6.7	8	14.2	19.2	14.7	15.7	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.7	7.1	6.9
VIII	–	–	–	–	22.3	12.0	31.9	11	7.2	14	14.2	20.7	15.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.1	5.4	6.2
IX	–	–	–	–	22.0	9.8	31.1	17	2.8	22,23	11.4	20.9	13.3	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.6	3.1	4.0
X	–	–	–	–	16.9	7.1	21.9	6	3.4	10	8.5	15.9	10.6	11.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.4	3.5	5.4
XI	–	–	–	–	7.6	4.9	15.3	3	-5.5	21	3.2	6.3	3.8	4.3	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	6.9	7.5
XII	–	–	–	–	0.7	-7.5	17.9	5	-28.4	25	-4.4	-1.8	-3.5	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.7	6.9	7.3
Rok	–	–	–	–	13.9	4.7	31.9	11.VIII	-28.4	25.XII	6.8	12.1	7.9	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.8	5.7	6.3

Myślenice

$\varphi = 49°49'$ $\lambda = 19°56'$

I	–	–	–	–	1.0	-6.9	13.0	4	-20.7	26	-4.5	-0.2	-3.1	-2.7	3.9	4.1	4.1	4.0	81	66	80	76	1.0	2.4	1.2	1.5	6.2	6.1	5.3	5.9
II	–	–	–	–	5.8	-0.8	14.4	18	-9.3	6	0.3	5.0	1.8	2.2	5.6	5.8	6.2	5.9	89	68	89	82	0.8	3.2	0.8	1.6	7.1	6.8	7.0	7.0
III	–	–	–	–	10.4	2.5	20.6	18	-3.9	23	4.2	8.9	6.0	6.3	6.8	6.4	7.0	6.7	83	58	76	72	1.6	5.5	2.6	3.2	8.0	7.3	6.2	7.2
IV	–	–	–	–	17.7	5.3	25.8	7	-1.9	10	7.8	16.8	10.0	11.2	8.6	7.2	9.4	8.4	80	39	76	65	2.4	12.6	3.1	6.0	4.1	5.2	4.1	4.5
V	–	–	–	–	17.1	6.8	24.6	6	2.4	15	9.8	15.6	10.1	11.4	10.2	9.7	11.1	10.3	84	57	89	77	2.1	8.3	1.5	4.0	6.5	7.2	6.8	6.8
VI	–	–	–	–	23.5	11.5	32.2	27	6.8	21	14.6	21.3	15.3	16.6	14.2	15.4	15.1	14.9	85	62	86	78	2.6	10.5	2.4	5.2	4.7	5.9	5.9	5.5
VII	–	–	–	–	21.5	11.4	29.3	3	7.9	25	13.9	20.0	14.3	15.6	13.2	14.7	14.2	14.0	83	64	87	78	3.0	9.7	2.3	5.0	5.5	6.4	6.1	6.0
VIII	–	–	–	–	22.6	12.4	33.5	11	8.0	14	14.3	21.4	15.0	16.4	13.9	15.8	15.0	14.9	84	63	86	78	2.8	10.8	2.4	5.3	5.1	5.6	4.6	5.1
IX	–	–	–	–	22.0	9.5	31.7	17	1.2	23	10.9	21.0	12.9	14.4	11.3	13.7	12.7	12.6	85	57	85	76	2.1	12.0	2.4	5.5	3.7	3.7	3.0	3.5
X	–	–	–	–	17.5	6.5	23.8	28	1.6	22	7.8	16.4	10.1	11.1	9.0	10.5	10.0	9.8	85	58	81	75	1.8	8.3	2.5	4.2	5.7	5.5	3.8	5.0
XI	–	–	–	–	8.4	1.2	17.4	3	-5.6	21	2.8	7.2	3.7	4.4	6.6	7.4	7.1	7.0	87	74	88	83	1.1	3.2	1.0	1.8	6.6	7.0	6.8	6.8
XII	–	–	–	–	1.0	-7.8	19.5	5	-28.6	25	-4.4	-1.5	-4.0	-3.5	4.6	4.5	4.4	4.5	87	74	85	82	1.0	2.1	1.2	1.4	7.0	6.3	6.2	6.5
Rok	–	–	–	–	14.0	4.3	33.5	11.VIII	-28.6	25.XII	6.5	12.7	7.7	8.6	9.0	9.6	9.7	9.4	84	62	84	77	1.9	7.4	2.0	3.8	5.8	6.1	5.5	5.8

Aleksandrowice

$\varphi = 49°48'$ $\lambda = 19°00'$

I	970.7	990.1	951.5	1021.2	0.6	-5.6	10.5	4	-17.3	26	-3.6	-0.6	-2.6	-2.4	4.0	4.3	4.2	4.2	81	72	79	77	1.1	1.9	1.2	1.4	6.4	6.1	5.7	6.1
II	974.1	988.9	946.0	1024.2	4.8	-1.6	12.8	18	-9.9	6	0.1	3.6	1.2	1.5	5.5	6.2	5.7	5.8	88	79	86	84	0.8	1.9	1.0	1.2	7.9	6.7	5.9	6.8
III	971.7	988.3	949.4	1020.7	9.2	2.1	18.2	18	-3.7	23	3.6	7.4	5.6	5.6	6.7	6.8	6.9	6.8	84	67	76	76	1.5	4.1	2.5	2.7	8.4	7.8	6.9	7.7
IV	965.0	973.1	958.8	1012.7	16.2	5.9	23.3	7	-1.1	10	9.3	15.3	10.7	11.5	8.4	8.9	8.8	8.7	73	52	70	65	3.7	9.1	4.3	5.7	6.0	6.1	4.1	5.4
V	965.5	971.5	951.8	1013.4	15.7	6.3	22.7	6	1.4	15	9.4	14.0	9.9	10.8	10.0	10.2	9.9	10.0	84	64	81	76	2.1	6.5	2.6	3.7	8.0	7.9	7.4	7.8
VI	968.9	982.4	958.4	1015.9	22.1	11.4	29.4	27	6.1	16	15.9	19.8	15.4	16.6	14.0	14.6	13.9	14.2	78	64	80	74	4.4	9.1	3.8	5.8	5.5	6.8	6.3	6.2
VII	968.3	979.1	954.5	1015.4	20.4	11.1	29.2	3	6.5	8	14.7	18.5	14.8	15.7	13.0	13.0	12.9	13.0	78	63	77	73	4.0	9.1	4.2	5.8	6.1	7.4	6.8	6.8
VIII	970.8	982.4	961.2	1017.9	21.1	11.9	30.0	11	5.5	14	15.1	19.9	15.6	16.6	14.2	14.9	14.0	14.4	82	63	79	75	3.3	9.2	4.2	5.6	5.9	7.0	5.5	6.1
IX	972.5	983.0	961.8	1020.0	20.6	9.6	28.6	17	2.1	22	12.9	19.8	13.8	15.1	11.7	13.1	12.2	12.3	78	57	77	71	3.6	10.7	3.9	6.1	4.6	5.0	3.4	4.3
X	971.1	982.8	946.0	1019.2	15.8	6.9	21.6	8	2.9	10	9.4	14.8	10.7	11.4	9.5	10.2	9.7	9.8	82	62	76	73	2.5	6.9	3.3	4.2	6.8	6.8	4.6	6.1
XI	966.6	987.3	954.2	1015.7	6.7	0.7	13.7	27	-6.9	21	3.0	5.5	3.5	3.9	6.7	7.1	6.9	6.9	86	79	86	84	1.3	2.2	1.2	1.6	8.4	8.1	6.6	7.7
XII	967.4	990.2	952.0	1017.8	0.5	-7.4	18.3	5	-25.4	25	-4.3	-2.2	-3.1	-3.2	4.5	4.8	4.7	4.7	87	84	85	85	0.9	1.3	1.1	1.1	7.0	7.4	7.2	7.2
Rok	969.4	990.2	946.0	1017.8	12.8	4.3	30.0	11.VIII	-25.4	25.XII	7.1	11.3	8.0	8.6	9.0	9.5	9.2	9.2	82	67	79	76	2.4	6.0	2.8	3.7	6.8	6.9	5.9	6.5

Leskowiec

$\varphi = 49°48'$ $\lambda = 19°27'$

I	–	–	–	–	-1.7	-7.0	7.0	4	-18.3	18	-4.9	-3.4	-4.5	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.7	5.7	5.8
II	–	–	–	–	2.5	-2.6	13.1	18	-8.6	6	-0.7	1.2	-0.5	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.5	6.1	6.3
III	–	–	–	–	5.1	-0.9	15.6	10	-7.6	23	1.1	3.5	2.0	2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.5	8.4	8.1
IV	–	–	–	–	13.5	4.6	21.6	7	-3.2	1	7.5	12.3	7.7	8.8	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.8	5.2	5.3
V	–	–	–	–	12.6	5.2	19.9	27	-1.5	12	7.5	11.0	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.4	8.0	7.7
VI	–	–	–	–	19.1	10.9	27.2	27	6.1	29	14.1	16.6	14.0	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.9	7.0	6.4
VII	–	–	–	–	17.3	10.1	26.0	3	5.1	6	12.5	15.3	12.5	13.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.2	7.4	6.9
VIII	–	–	–	–	18.1	10.2	28.3	11	6.4	18	13.3	16.5	13.4	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.7	6.5	6.4
IX	–	–	–	–	17.8	10.5	26.8	17	4.9	22	12.8	16.5	13.2	13.9	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.2	5.0	4.8
X	–	–	–	–	13.1	6.8	18.4	8	2.3	14	8.5	11.4	8.7	9.3	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.9	6.0	6.1
XI	–	–	–	–	5.5	-0.3	10.9	27	-7.5	21	2.3	4.1	2.2	2.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.0	6.9	7.0
XII	–	–	–	–	-1.4	-8.1	15.0	5	-23.1	16	-5.1	-3.3	-4.9	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	7.3	7.2
Rok	–	–	–	–	10.1	3.3	28.3	11.VIII	-23.1	16.XII	5.7	8.5	6.0	6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.6	6.6	6.5

Porąbka

$H_s = 315\ m$ $h_w = 13{,}5\ m$ **1961**

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	●	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	13.3	3.3	2	6	11	25	·	–	–	7	9	8	5	·	1	9	·
II	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	65.8	18.7	9	·	·	15	·	–	–	5	15	14	10	2	8	5	·
III	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	68.5	43.0	14	·	·	6	·	–	–	2	19	18	14	1	1	4	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	42.8	13.6	18	·	·	1	1	–	–	11	4	10	7	2	·	·	4
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	118.1	26.6	6	·	·	·	·	–	–	·	20	19	15	3	1	·	6
VI	8.5	2.3	5.5	4.0	1	4.0	2	2.0	8	2.1	31	2.9	10	2.1	10	1.9	14	2.0	166.7	53.8	27	·	·	·	9	·	·	5	8	16	13	4	3	·	9
VII	10	1.7	2	1.5	·	·	2.5	2.6	16.5	2.8	31.5	3.2	9.5	2.3	7	1.6	44	2.2	132.0	22.5	30	·	·	·	8	·	·	3	12	17	15	7	·	·	6
VIII	5.5	2.7	1.5	2.7	·	·	3.5	4.9	12.5	4.1	44.5	2.7	9.5	2.7	6	1.7	40	2.5	124.4	35.5	12	·	·	·	7	1	1	4	11	12	8	5	·	·	3
IX	4.5	1.4	2.5	4.2	·	·	8	1.8	20	3.5	33	3.1	3	3.0	3	3.0	16	2.5	48.7	10.0	26	·	·	·	8	·	·	14	6	9	4	1	1	·	2
X	12	2.8	4	3.0	·	·	4	3.2	18	6.4	32	3.9	7	2.7	2	2.5	14	3.5	14.8	7.7	30	·	·	·	·	3	3	6	8	8	4	·	3	·	·
XI	6	1.7	2	4.0	2	3.0	2	6.5	8	5.5	36	2.8	7	1.9	5	2.2	22	2.2	85.5	41.4	4	·	·	6	·	2	1	3	16	13	9	2	5	5	·
XII	20	1.6	·	·	·	·	6.6	4.4	18.5	5.7	24	5.4	7	3.4	4	2.2	43	3.5	97.3	33.3	6	12	14	24	·	6	4	3	16	13	11	4	7	24	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	947.9	53.8	27.VI	18	25	77	33	–	–	63	144	157	115	31	30	47	30

Myślenice

$H_s = 295\ m$ $h_w = 16{,}8\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	●	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	9.5	2.0	1	3.0	0.5	3.0	·	·	9	6.6	35.5	3.8	12.5	4.4	3	2.3	22	3.0	25.5	8.6	5	9	11	26	·	3	1	5	10	10	6	·	·	20	:
II	3	2.3	·	·	·	·	·	·	25	5.2	41	2.8	7.5	2.5	3	1.7	27	4.9	51.4	15.0	9	·	1	16	·	·	·	3	14	14	9	2	5	6	·
III	·	·	1	1.0	1	2.0	·	·	10	4.0	36.5	3.3	12.5	2.4	·	·	32	2.1	68.4	9.0	14	·	·	5	·	2	·	2	16	19	15	·	1	3	·
IV	4.5	2.8	8.5	2.9	2	1.7	2	1.5	5	2.9	26.5	3.5	9.5	3.5	3	2.0	29	2.1	40.2	11.7	17	·	·	1	1	1	·	8	4	7	6	1	·	·	3
V	5.5	1.9	1.5	2.3	·	·	·	·	4.5	2.2	22.5	2.1	11	2.2	3	1.7	45	1.1	177.8	43.2	29	·	·	·	·	·	·	4	14	19	16	5	3	·	4
VI	4	1.8	1	1.0	·	·	0.5	5.0	0.5	5.0	34	2.8	14	2.0	6	1.7	30	1.6	186.8	37.9	26	·	·	·	9	·	·	6	8	14	14	8	·	·	8
VII	1	3.0	·	·	·	·	·	·	1.5	5.3	33.5	2.5	20.5	2.4	4.5	1.6	32	1.6	123.1	25.4	30	·	·	·	8	1	·	3	11	15	14	5	·	·	6
VIII	4.5	1.8	·	·	·	·	·	·	6	3.6	33	2.6	16.5	2.1	2	1.5	31	1.6	56.9	25.4	12	·	·	·	7	·	·	8	6	12	8	2	2	·	4
IX	8	1.4	0.5	3.0	·	·	·	·	3.5	3.3	39	2.8	17	2.2	5	1.7	47	2.0	13.7	4.2	29	·	·	·	11	1	·	13	4	8	6	·	1	·	3
X	6	2.0	3	1.7	0.5	3.0	1.5	3.3	6.5	4.0	31.5	2.7	8	1.9	1	1.0	35	1.6	21.5	12.2	30	·	·	·	·	·	·	8	7	6	5	1	1	·	·
XI	1	2.0	1	2.0	·	·	·	·	2.5	3.2	42.5	2.8	4.5	1.7	1.5	3.0	37	1.6	67.5	29.8	4	·	·	8	·	1	·	6	15	17	9	1	·	4	·
XII	3	2.0	·	·	0.5	1.0	0.5	1.0	5	4.5	35.5	4.0	9.5	4.5	6	1.5	33	2.4	119.7	38.4	11	11	13	25	·	3	·	5	14	15	9	4	1	24	·
Rok	50	1.9	17.5	1.4	4.5	0.9	4.5	0.9	56.5	4.2	411	3.0	143	2.6	38	1.6	370	1.9	952.5	43.2	29.V	20	25	81	36	12	1	71	123	156	117	29	14	57	28

Aleksandrowice

$H_s = 398\ m$ $H_b = 403{,}4\ m$ $h_w = 20\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	●	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	2	3.8	11	3.0	15.5	4.9	11	3.7	6.5	5.4	22.5	9.5	7.5	4.7	6	4.4	11	5.0	24.0	15.3	4	9	12	25	·	10	5	5	10	10	3	1	1	11	·
II	3	2.2	2	2.0	3.5	2.0	11.5	3.4	8.5	3.9	14	5.5	22.5	4.6	7	4.1	12	3.6	61.5	12.7	9	·	·	19	·	5	·	2	13	15	10	2	8	6	·
III	4.5	4.0	·	·	0.5	1.0	2.5	3.0	2	2.5	16	6.9	45.5	6.1	21	5.9	1	5.9	73.3	12.6	14	·	·	6	·	10	·	1	20	18	13	3	2	4	1
IV	3.5	2.9	3	5.3	20.5	4.9	21.5	4.1	8	6.9	12	7.7	10	6.2	6.5	4.5	5	5.0	36.7	15.3	1	·	·	1	·	14	4	5	4	8	7	1	·	·	3
V	2	3.0	4.5	2.8	6.5	4.4	5.5	2.5	3.5	4.0	18	4.6	22	4.5	17	3.9	14	3.5	132.2	24.0	6	·	·	·	·	3	1	·	15	17	16	5	2	·	7
VI	4	2.8	2.5	2.2	5.5	3.0	16	2.7	5.5	6.0	12.5	4.2	12	4.2	12	4.1	20	2.9	197.4	82.4	27	·	·	·	5	4	·	4	7	15	14	5	2	·	11
VII	4.5	3.6	2.5	1.8	3	2.0	6.5	2.8	5	4.0	18	5.0	35	5.4	9.5	2.9	9	4.0	150.3	32.0	30	·	·	·	7	6	1	2	10	16	14	6	·	·	8
VIII	4.5	1.9	1	2.0	6.5	3.6	3.5	2.6	4.5	5.1	20	5.9	30.5	5.9	9.5	3.7	13	4.3	88.5	40.0	12	·	·	·	5	9	·	1	8	11	7	4	2	·	4
IX	2	2.0	4.5	3.4	12.5	4.3	18	3.0	5.5	1.9	15.5	5.3	14.5	5.0	5.5	4.5	12	3.5	13.0	6.3	14	·	·	·	5	5	1	13	7	7	4	·	1	·	1
X	15	2.0	4.5	4.7	15.5	4.5	19	5.7	9	7.2	8	6.9	9	3.7	6.5	2.3	20	4.0	14.8	6.4	14	·	·	·	·	10	2	3	9	6	5	·	7	·	·
XI	3.5	2.6	3	2.2	5.5	3.5	11	2.7	5.5	6.2	12.5	7.0	17.5	4.9	9.5	2.6	22	3.3	106.1	47.4	4	·	1	12	·	6	1	1	15	14	10	3	6	9	·
XII	9	2.4	8	1.8	8	3.4	8	2.6	6	7.2	15	9.1	18	6.6	4	3.1	17	4.2	98.6	36.6	6	11	17	25	·	9	5	3	16	18	12	4	11	24	·
Rok	44	2.8	46.5	2.6	103	3.5	134	3.2	69.5	5.0	184	6.5	244	5.2	114	3.8	156	4.1	996.4	82.4	27.VI	20	30	88	22	91	20	40	134	155	115	34	42	54	35

Leskowiec

$H_s = 870\ m$ $h_w = 16\ m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	●	●	R≥0.1	R≥1.0	R≥10.0	≡	⊠	R
I	3	4.2	2.5	4.0	2	7.5	24.5	4.4	35	10.8	11	5.7	7.5	4.4	2.5	4.6	5	6.8	34.3	13.8	4	7	18	30	·	11	7	3	6	9	7	1	9	31	:
II	3.5	2.9	1	2.0	·	·	8	4.1	19.5	7.0	17.5	4.4	17	6.4	7.5	9.2	10	5.2	66.9	15.2	10	·	7	25	·	9	3	3	10	12	12	2	16	24	·
III	4	6.6	3	4.0	1	14.0	4.5	7.1	9	8.9	11.5	5.8	40	10.7	16	9.2	4	8.7	119.1	18.4	14	·	4	21	·	18	9	·	20	20	19	2	14	17	1
IV	9.5	2.5	11.5	4.0	11	5.0	11.5	5.2	28.5	6.9	8	5.2	3	5.7	5	4.8	2	5.2	45.9	13.8	18	·	·	4	·	8	1	4	5	7	7	1	4	1	2
V	6	3.4	9	5.1	3	4.7	4.5	2.8	18	5.0	6.5	4.8	13.5	5.6	20.5	5.4	12	4.3	130.7	30.6	6	·	·	1	·	6	1	·	13	20	16	4	14	·	6
VI	5.5	3.2	3.5	2.1	6	4.2	7.5	5.1	19.5	6.2	7	4.0	17.5	7.2	14.5	5.5	9	4.9	154.3	47.3	27	·	·	·	2	9	2	·	11	15	14	6	8	·	9
VII	4	2.5	1.5	4.7	3.5	2.6	18.5	5.2	11.5	6.1	5.5	5.0	14	4.5	19.5	4.8	15	4.1	175.8	35.6	28	·	·	·	2	7	2	3	10	16	15	8	8	·	5
VIII	9	4.4	10.5	3.1	2	7.0	14	4.1	12.5	5.7	5.5	6.8	14	3.6	20.5	5.6	5	4.5	123.5	54.0	12	·	·	·	5	7	·	1	10	12	9	4	8	·	3
IX	3.5	2.1	13	4.3	7	5.9	10.5	6.2	12.5	6.3	7.5	3.8	11	3.1	15	5.2	10	4.3	20.0	6.2	26	·	·	·	1	7	3	9	5	8	7	·	6	·	1
X	1	4.0	4	6.8	12	4.1	15	5.9	28.5	8.0	6.5	4.6	8	3.1	6	7.3	12	5.3	30.9	12.2	14	·	·	·	·	12	4	3	8	8	5	2	10	·	·
XI	9	2.8	4	3.2	1	5.0	13.5	5.0	22	4.9	3.5	2.1	15	4.1	10	3.9	12	3.6	94.3	35.4	4	·	6	14	·	4	1	·	14	16	12	3	13	7	·
XII	5.5	3.6	8	4.1	5	3.2	5	13.4	24	8.6	5	12.8	8	6.5	15.5	6.3	17	5.9	143.2	41.2	6	13	17	24	·	14	7	2	16	15	14	6	16	24	·
Rok	63.5	3.5	71.5	4.0	53.5	5.3	137	5.7	240.5	7.0	95	5.4	168.5	5.4	152.5	6.0	113	5.2	1138.9	54.0	12.VIII	20	52	119	10	118	40	28	128	158	137	39	126	104	27

Dynów

$\varphi = 49°48'$ $\lambda = 22°14'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.8	-8.2	9.8	4	-25.1	27	-6.0	-1.6	-4.4	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.6	6.0	6.3
II	–	–	–	–	3.3	-1.2	10.2	18	-5.6	5	-0.2	2.9	0.9	1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.5	7.6	7.6
III	–	–	–	–	9.1	2.1	17.0	18	-3.9	23	4.0	7.8	5.2	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.5	7.0	7.1
IV	–	–	–	–	16.7	4.3	24.4	16	-3.9	10	7.5	16.0	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.5	5.0	5.3
V	–	–	–	–	16.8	6.4	24.6	29	0.3	20	9.9	15.8	10.5	11.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.3	6.7	6.9
VI	–	–	–	–	23.8	11.2	30.6	27	5.9	21	15.4	22.2	16.2	17.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.7	6.2	5.9
VII	–	–	–	–	22.5	11.0	31.1	4	6.4	7	14.8	21.6	15.1	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.6	6.4	5.8
VIII	–	–	–	–	22.8	11.9	33.0	11	5.7	31	14.9	21.7	16.3	17.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.4	5.9	5.4
IX	–	–	–	–	21.2	7.9	29.8	18	-2.0	22	10.7	20.8	13.3	14.5	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.6	3.6	4.3
X	–	–	–	–	16.4	5.5	24.0	19	-1.8	12	7.4	16.0	10.4	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.1	4.5	4.4	5.0
XI	–	–	–	–	8.1	2.8	13.7	7	-5.1	21	4.5	7.3	5.3	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.7	7.4	7.6
XII	–	–	–	–	-0.3	-7.1	13.7	5	-26.8	25	-4.5	-1.9	-3.4	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.1	7.3	7.5
Rok	–	–	–	–	13.3	3.9	33.0	11.VIII	-26.8	25.XII	6.5	12.4	8.0	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	6.1	6.2

Przemyśl

$\varphi = 49°48'$ $\lambda = 22°46'$

I	991.8	1010.3	974.4	1022.3	-0.6	-8.3	8.7	3	-23.9	27	-5.9	-1.8	-4.5	-4.2	3.7	4.3	3.9	4.0	84	75	82	80	0.8	1.6	0.9	1.1	7.1	4.9	4.7	5.6
II	993.9	1008.7	965.5	1023.8	4.1	-0.6	10.7	18	-5.0	7	0.1	3.3	1.3	1.5	5.5	5.7	5.6	5.6	88	74	84	82	0.8	2.2	1.1	1.4	7.6	7.3	7.0	7.3
III	988.7	1006.1	969.6	1018.0	9.7	2.3	19.1	18	-4.3	23	4.3	7.9	5.6	5.8	6.8	6.5	6.9	6.7	81	62	76	73	1.7	4.6	2.4	2.9	7.7	7.6	4.9	6.7
IV	984.9	993.4	977.4	1013.5	17.2	4.9	25.3	15	-3.2	10	7.5	15.9	10.8	11.2	8.6	8.8	9.0	8.8	82	49	69	67	2.1	10.0	4.3	5.5	5.4	6.0	3.8	5.1
V	983.7	991.9	969.6	1012.2	16.8	6.7	24.7	29	1.0	17	9.8	14.9	11.1	11.7	10.8	10.8	10.9	10.8	88	65	82	78	1.5	6.7	2.6	3.6	7.0	7.8	5.2	6.7
VI	987.3	999.9	978.1	1015.3	23.5	12.5	30.6	26	7.4	1	16.3	21.8	17.0	18.0	15.9	15.3	15.4	15.4	83	59	80	74	3.3	11.6	4.2	6.4	4.3	5.7	4.3	4.8
VII	986.4	996.7	975.7	1014.5	23.0	11.4	31.3	4	7.3	7	15.2	21.3	16.0	17.1	14.0	13.4	13.8	13.7	81	54	76	70	3.6	12.7	4.8	7.0	4.9	6.5	5.2	5.5
VIII	988.8	1000.1	977.9	1016.8	23.0	12.5	33.5	11	7.8	31	15.1	21.6	16.9	17.6	15.0	14.8	15.5	15.1	86	58	79	74	2.6	12.0	4.4	6.3	4.9	5.4	4.9	5.1
IX	991.5	1001.7	980.2	1019.9	21.4	9.1	30.0	18	-0.1	23	11.0	20.5	14.1	14.9	11.9	12.1	12.4	12.1	89	51	76	72	1.8	12.9	4.1	6.3	4.7	4.6	3.3	4.2
X	992.1	1002.8	971.8	1021.0	16.9	4.6	24.8	19	0.1	23	6.0	16.0	10.0	10.5	8.5	9.5	9.2	9.1	90	55	75	73	1.1	9.1	3.2	4.5	5.4	4.5	3.4	4.4
XI	986.2	1006.2	974.3	1015.5	8.4	2.3	16.9	3	-4.7	24	4.1	7.4	4.9	5.3	7.6	7.8	7.8	7.7	90	75	87	84	0.9	2.9	1.1	1.6	7.6	7.7	7.2	7.5
XII	986.7	1012.3	969.8	1017.0	-0.2	-7.2	16.5	5	-25.5	25,26	-3.9	-1.6	-3.5	-3.1	4.8	4.7	4.6	4.6	84	78	85	82	1.1	1.8	1.0	1.3	7.7	7.4	5.9	7.0
Rok	988.5	1012.3	965.5	1017.5	13.6	4.2	33.5	11.VIII	-25.5	25,26.XII	6.6	12.3	8.3	8.9	9.4	9.5	9.6	9.5	86	63	79	76	1.8	7.3	2.8	4.0	6.2	6.3	5.0	5.8

Międzybrodzie Bialskie

$\varphi = 49°47'$ $\lambda = 19°12'$

I	–	–	–	–	1.1	-5.0	10.9	4	-17.9	26	-3.2	-0.3	-1.9	-1.8	3.9	4.1	4.3	4.1	75	66	74	72	1.3	2.2	1.4	1.6	6.7	6.3	6.1	6.4
II	–	–	–	–	4.8	-1.4	11.6	18	-13.9	6	-0.3	3.6	1.3	1.5	5.3	5.8	5.8	5.6	86	73	86	82	0.9	2.2	1.0	1.4	6.5	6.3	7.1	6.6
III	–	–	–	–	10.0	2.4	19.1	18	-3.8	23	4.0	7.6	5.5	5.6	6.4	6.5	6.7	6.5	79	63	75	72	1.8	4.4	2.5	2.9	7.9	6.7	7.6	7.4
IV	–	–	–	–	16.9	5.5	24.5	7	0.2	10	9.1	15.9	10.1	11.3	8.6	8.4	9.0	8.7	73	48	72	64	3.3	10.2	3.6	5.7	4.7	5.4	5.8	5.3
V	–	–	–	–	16.2	6.3	23.4	27	2.2	15	10.2	14.7	9.9	11.2	9.7	9.5	9.9	9.7	77	58	81	72	3.0	7.8	2.5	4.4	7.5	7.5	8.2	7.7
VI	–	–	–	–	22.6	11.2	30.3	27	6.1	21	15.4	20.0	15.4	16.6	13.8	14.9	14.3	14.2	80	62	81	74	3.9	9.6	3.4	5.6	4.9	6.8	7.0	6.2
VII	–	–	–	–	–	10.8	29.5	3	5.8	8	14.6	19.3	15.0	16.0	12.7	13.3	13.3	13.1	76	60	78	71	4.2	9.7	4.0	6.0	6.1	7.2	6.6	6.6
VIII	–	–	–	–	–	11.9	–	–	6.5	14	14.3	20.8	15.9	16.7	13.5	14.2	14.6	14.1	82	58	80	73	3.2	11.4	3.8	6.1	6.1	6.4	6.3	6.3
IX	–	–	–	–	20.9	9.2	29.7	17	1.2	22	10.9	20.2	14.0	14.8	11.0	13.2	13.2	12.5	84	57	82	74	2.5	11.3	3.1	5.6	4.4	4.8	5.2	4.8
X	–	–	–	–	16.3	6.6	22.1	8	1.4	11	8.5	15.9	10.5	11.2	9.2	10.4	10.1	9.8	84	58	80	74	2.1	7.8	2.7	4.2	6.1	5.5	6.1	5.9
XI	–	–	–	–	7.5	1.6	15.0	3	-5.3	23	3.5	6.6	3.8	4.4	6.6	7.4	6.9	7.0	82	75	85	81	1.5	2.7	1.3	1.8	7.2	7.0	7.6	7.3
XII	–	–	–	–	0.8	-7.7	17.2	5	-28.6	25	-4.3	-0.9	-3.2	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.9	7.6	7.4
Rok	–	–	–	–	–	4.3	–	–	-28.6	25.XII	6.9	11.9	8.0	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.4	6.8	6.5

Ciężkowice

$\varphi = 49°47'$ $\lambda = 20°58'$

I	–	–	–	–	0.2	-8.1	9.2	4	-24.9	27	-5.7	-1.2	-4.1	-3.8	4.0	4.4	4.4	4.3	88	74	84	82	0.5	1.5	0.8	0.9	7.0	6.5	5.4	6.3
II	–	–	–	–	4.8	-1.1	12.7	18	-8.1	5	0.0	3.8	1.1	1.5	5.6	6.0	5.9	5.8	91	76	88	85	0.6	2.1	0.9	1.2	8.3	7.9	6.6	7.6
III	–	–	–	–	10.0	2.6	20.7	18	-1.8	7	4.1	8.2	5.8	6.0	7.0	7.0	7.3	7.1	85	66	79	77	1.3	4.4	2.2	2.6	8.1	8.2	6.5	7.6
IV	–	–	–	–	17.6	4.0	26.3	15	-2.7	10	5.9	16.1	10.3	10.6	7.9	9.0	9.4	8.8	85	50	74	70	1.5	10.1	3.4	5.0	6.0	6.4	5.1	5.8
V	–	–	–	–	17.1	6.8	25.2	6	1.3	3	8.9	15.7	10.6	11.4	10.3	10.8	11.3	10.8	90	61	88	80	1.2	7.7	1.7	3.5	7.0	8.0	6.7	7.2
VI	–	–	–	–	24.0	11.1	31.9	27	5.7	21	14.4	22.5	15.7	17.1	15.1	15.5	15.7	15.4	91	58	88	79	1.5	12.5	2.3	5.4	5.5	6.7	5.8	6.0
VII	–	–	–	–	22.2	10.6	30.9	4	5.6	7	13.8	20.6	14.8	16.0	14.0	13.9	14.7	14.2	89	58	87	78	1.9	11.3	2.4	5.2	6.0	7.1	6.2	6.4
VIII	–	–	–	–	23.4	11.7	34.6	11	5.7	31	13.8	21.8	16.3	17.0	14.4	15.5	16.0	15.3	90	59	86	78	1.8	11.7	2.9	5.5	5.5	7.2	5.6	6.1
IX	–	–	–	–	21.4	8.0	30.4	18	-1.9	23	9.3	20.1	12.4	13.6	10.9	13.1	12.5	12.2	91	57	86	78	1.4	11.3	2.3	5.0	5.5	4.9	2.9	4.4
X	–	–	–	–	16.4	5.9	23.1	20	-0.2	22	7.5	15.7	10.0	10.8	8.7	10.2	9.7	9.5	85	59	80	75	2.0	8.0	2.8	4.3	6.7	5.7	4.2	5.5
XI	–	–	–	–	8.2	1.8	16.3	3	-5.5	21	3.3	7.1	4.3	4.8	7.0	7.7	7.4	7.4	87	75	87	83	1.1	2.8	1.2	1.7	8.0	7.1	6.8	7.3
XII	–	–	–	–	0.2	-7.4	15.9	2	-30.0	26	-4.3	-1.4	-3.9	-3.4	4.5	4.7	4.4	4.5	81	75	78	78	0.9	1.7	1.1	1.2	7.5	6.4	6.9	6.9
Rok	–	–	–	–	13.8	3.8	34.6	11.VIII	-30.0	26.XII	5.9	12.4	7.8	8.5	9.1	9.8	9.9	9.6	88	64	84	79	1.3	7.1	2.0	3.5	6.8	6.8	5.7	6.4

Dynów

$H_s = 276$ m $h_w = 17,5$ m

MIESIĄC	ROZKŁAD WIATRU N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temperatura Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	═	⊞	R (snow)
I	2	1.5	4	2.2	1	1.0	·	·	11	6.2	38	6.7	2	5.0	12	2.6	23	4.1	13.5	3.9	14	11	14	28	·	6	3	3	11	9	6	·	·	–	·
II	·	·	2	1.5	·	·	3	1.3	9	7.6	32	4.8	11	1.2	10	2.1	17	3.1	15.4	4.1	10	·	1	18	·	6	·	2	15	10	6	·	1	–	·
III	2	2.0	·	·	·	·	·	·	4	2.0	23	3.7	30	3.6	21	5.0	16	3.3	33.4	6.2	31	·	·	7	·	5	·	·	9	12	9	·	·	–	·
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	17.6	9.1	2	·	·	3	·	–	–	3	5	5	5	·	·	·	2
V	1	1.0	2	2.0	3	2.3	3	1.7	2	4.0	15	3.2	16	2.4	16	2.4	35	1.6	52.5	14.0	14	·	·	·	·	1	·	·	8	13	10	2	·	·	3
VI	2	4.0	1	1.0	·	·	5	3.6	8	2.4	20	2.6	4	1.5	16	2.8	34	1.6	77.0	19.7	3	·	·	·	9	·	·	·	5	15	13	2	1	·	8
VII	2	1.5	1	1.0	1	1.0	·	·	8	3.1	28	2.7	9	2.4	13	2.5	31	1.7	118.3	49.6	29	·	·	·	8	·	·	2	5	15	12	3	·	·	3
VIII	3	2.3	1	3.0	2	1.0	·	·	4	4.2	31	2.3	6	2.3	13	2.1	33	1.5	57.4	24.1	12	·	·	·	7	·	·	3	6	11	8	1	2	·	2
IX	1	1.0	1	4.0	4	3.8	2	2.5	5	2.2	26	2.8	9	2.0	5	2.0	37	1.5	26.1	8.3	7	·	·	2	8	·	·	11	7	7	7	·	4	·	2
X	2	2.0	·	·	9	2.6	9	5.1	10	10.6	18	3.6	3	1.0	11	1.8	31	2.9	27.6	19.1	30	·	·	1	·	7	1	6	6	5	4	1	2	·	·
XI	2	2.0	·	·	9	1.7	·	·	3	2.7	35	4.1	13	2.1	14	2.4	14	2.6	33.8	8.0	13	·	1	8	·	2	·	1	17	15	11	·	·	–	·
XII	21	2.4	3	3.0	5	2.0	·	·	·	·	30	8.2	3	1.0	13	2.8	18	3.8	69.6	22.2	11	11	15	23	·	7	2	1	15	12	12	2	1	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	542.2	49.6	29.VII	22	31	90	32	–	–	32	109	129	103	11	11	–	20

Przemyśl

$H_s = 237$ m $H_b = 238,9$ m $h_w = 20,6$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R (snow)
I	6	3.1	3	3.0	1	1.0	3	1.7	1	2.0	8	5.9	29	3.2	16	3.5	26	2.5	16.6	7.3	2	12	14	28	·	·	·	6	12	9	5	·	3	27	·
II	1	1.0	2.5	1.6	5.5	2.9	1	2.0	·	·	6	4.1	43	3.1	12	2.8	13	2.5	12.7	4.9	10	·	·	14	·	·	·	3	16	10	5	·	1	5	·
III	·	·	·	·	·	·	·	·	·	·	7.5	5.8	59.5	4.7	23	4.5	3	4.6	21.0	5.0	31	·	·	7	·	3	·	1	10	15	5	·	·	2	1
IV	9	2.7	12	3.6	16	5.6	15	7.0	·	·	10	4.2	18.5	3.7	12	2.1	11	3.4	18.6	6.3	2	·	·	2	1	3	·	7	7	9	5	·	2	·	2
V	6	2.1	5.5	1.8	3	4.7	1	4.0	·	·	4.5	3.9	25	2.6	28	3.1	20	2.2	75.1	13.6	28	·	·	·	·	·	·	1	9	16	11	3	3	·	6
VI	4.5	1.4	5	2.7	4	2.4	2	5.5	0.5	7.0	4.5	3.0	29	2.4	21.5	3.1	19	2.2	70.9	13.6	4			·	10	·	·	6	4	11	11	3	2	·	10
VII	2	2.8	0.5	3.0	·	·	·	·	·	·	8.5	3.2	43	3.2	25	2.6	14	2.5	72.3	28.7	29	·	·	·	10	1	1	2	5	13	10	3	1	·	7
VIII	5	2.2	1.5	2.7	1.5	2.7	0.5	4.0	0.5	4.0	8.5	4.6	33.5	2.8	28	3.2	14	2.6	48.0	16.0	12	·	·	·	8	·	·	7	7	12	7	2	1	·	3
IX	·	·	5.5	2.4	5.5	3.6	2	3.5	0.5	8.0	14.5	3.4	37	2.8	6	2.0	49	2.3	10.3	3.9	7	·	·	1	9	·	·	10	5	8	3	·	2	·	1
X	4.5	2.4	3.5	3.7	17.5	3.3	17	3.3	7	3.1	4	2.8	11.5	2.7	3	3.8	25	2.3	7.3?	2.9?	31?	·	·	·	·	·	·	11	8	6	3	·	4	·	·
XI	2	2.5	1	4.0	13.5	3.3	4	2.1	6.5	2.2	9.5	3.7	30	2.3	8.5	3.2	15	2.3	29.5	5.4	19	·	·	9	·	·	·	1	16	18	9	·	6	2	·
XII	7	4.1	4.5	2.8	6.5	2.5	0.5	2.0	2.5	4.4	15	5.2	22.5	3.9	15.5	5.1	19	3.4	37.3	7.1	20	11	16	23	·	·	·	2	15	17	8	·	3	24	·
Rok	47	2.0	44.5	2.6	74	2.7	32.5	2.9	18.5	2.6	100.5	4.2	381.5	3.1	198.5	3.2	198	2.7	419.6	28.7	29.VII	23	30	84	38	7	1	57	114	144	82	11	28	60	30

Międzybrodzie Bialskie

$H_s = 320$ m $h_w = 10$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R (snow)
I	5.5	5.6	15	3.5	1	4.0	21	4.6	29	7.8	·	·	·	·	4.5	4.4	17	4.7	23.5	6.4	4	8	11	25	·	3	1	6	11	13	7	·	3	6	·
II	4.5	3.7	1	5.0	·	·	13	5.9	23	6.9	0.5	3.0	6.5	3.9	4.5	4.3	31	3.6	53.0	12.5	9	1	·	15	·	6	1	4	16	14	13	2	7	5	·
III	7	4.6	2	2.0	1	4.0	18.5	4.0	15.5	5.6	1	4.0	12.5	5.2	14.5	5.4	21	3.8	65.4	14.0	14	·	·	6	·	2	·	1	13	19	17	1	·	1	·
IV	12	5.2	5.5	2.7	·	·	18	5.8	12.5	6.6	2.5	6.4	6	4.3	5.5	4.0	28	3.7	32.2	19.0	18	·	·	·	·	3	·	5	6	7	7	1	1	·	4
V	14	3.8	2.5	3.8	3	2.0	13.5	3.8	11.5	5.1	1.5	4.0	2.5	2.0	6.5	4.1	38	2.3	107.2	25.0	6	·	·	·	·	·	·	·	13	17	13	3	2	·	6
VI	13.5	4.9	2	3.5	·	·	14	4.1	7	4.4	1	4.0	4	3.2	6.5	4.3	42	2.3	221.7	53.6	10	·	·	·	5	·	·	·	9	15	14	6	4	·	11
VII	4.5	2.9	3.5	2.0	1	3.0	31.5	4.6	5.5	4.1	·	·	5	3.0	8	4.4	34	2.6	135.4	22.4	30	·	·	·	–	3	1	·	7	16	14	8	·	·	7
VIII	7	5.6	5	3.0	1	2.0	21	4.8	7	5.6	1	7.0	4	4.2	4	4.2	43	2.5	117.8	34.0	12	·	·	·	–	2	·	1	9	11	8	4	4	·	3
IX	10	4.9	2	7.0	·	·	12	4.8	11	4.4	1	5.0	6	3.6	8	3.3	42	2.4	16.1	10.3	26	·	·	·	5	1	·	9	7	9	3	1	3	·	1
X	10	4.1	6.5	4.2	·	·	21	6.0	14	8.9	·	·	1	4.0	6.5	3.7	34	3.7	15.7	8.0	30	·	·	·	·	6	5	5	7	8	3	·	7	·	
XI	9.5	4.2	2	2.5	0.5	4.0	21	5.5	9	6.0	·	·	1	4.0	15	3.3	32	3.0	77.7	34.3	4	·	·	6	·	4	·	·	14	12	8	2	6	3	·
XII	11	5.9	3	3.3	·	·	21	6.2	14	10.1	·	·	1	7.0	15	5.8	28	4.7	89.1	16.8	12	11	15	25	·	6	1	2	16	19	17	3	4	21	·
Rok	108.5	4.6	50	3.5	7.5	1.6	226.5	5.0	159	6.3	8.5	2.8	49.5	3.7	96.5	4.3	390	3.3	954.8	53.6	10.VI	20	26	77	–	36	9	33	128	160	124	31	41	36	32

Ciężkowice

$H_s = 280$ m $h_w = 15,9$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	◔	●	R≥0.1	R≥1.0	R≥10.0	═	⊞	R (snow)
I	2	1.2	4.5	1.7	0.5	1.0	2	1.8	12.5	1.6	7.5	1.2	5	1.6	3	1.8	59	0.6	17.7	5.4	5	10	14	28	·	·	·	4	12	14	6	·	–	21	·
II	·	·	·	·	·	·	2.5	1.8	13	1.3	7	1.2	14	1.5	1.5	1.3	46	0.6	29.4	7.2	28	·	·	17	·	·	·	1	15	16	8	·	–	9	·
III	·	·	·	·	·	·	·	·	6	1.5	14.5	1.3	36.5	2.0	9	2.6	27	1.8	40.4	6.4	23	·	·	9	·	·	·	1	18	19	13	·	–	1	·
IV	3	1.2	3	1.5	11	2.0	6	1.7	6	1.1	4.5	1.3	3	1.8	3.5	2.7	50	0.7	34.0	9.6	29	·	·	3	2	·	·	6	8	12	11	·	–	·	4
V	1	1.0	1.5	1.0	4.5	1.7	1	1.0	1.5	1.7	8.5	1.2	11.5	1.2	3.5	1.4	60	0.5	118.1	25.6	17	·	·	·	1	1	·	·	13	17	12	6	–	·	6
VI	1	1.0	0.5	1.0	1.5	1.0	1	1.0	8.5	1.2	4.5	1.1	6	2.1	2	1.5	65	0.4	64.9	14.8	7	·	·	·	12	1	·	3	8	11	9	3	–	·	8
VII	·	·	1	1.0	·	·	2.5	1.4	5.5	1.3	10.5	1.3	9.5	1.7	3	1.8	61	0.5	119.4	29.0	30	·	·	·	9	3	1	3	10	17	16	2	–	·	7
VIII	·	·	1	1.0	·	·	1	1.5	3	1.3	8.5	1.2	12.5	2.0	1	1.0	66	0.5	58.9	21.8	12	·	·	·	10	1	·	3	9	11	8	2	–	·	4
IX	·	·	·	·	3	1.3	1.5	1.0	3	1.0	10.5	1.2	2.5	1.8	0.5	3.0	69	0.3	37.4	20.8	6	·	·	2	10	·	·	9	6	10	5	1	–	·	2
X	·	·	0.5	0.5	2.5	1.8	7.5	1.7	18.5	1.4	·	·	6.5	1.4	0.5	2.0	57	0.6	29.9	15.0	30	·	·	1	·	·	·	4	8	9	6	1	–	·	·
XI	0.5	2.0	·	·	·	·	3.5	1.3	13	1.2	11	1.3	9.5	1.4	1.5	1.3	51	0.6	59.9	15.1	4	·	·	10	·	·	·	2	16	18	11	1	–	·	·
XII	8	1.9	4.5	1.0	1	1.0	1	1.0	15.5	1.9	7	1.9	13	1.5	4	2.2	42	0.9	84.2	21.4	12	9	14	23	·	2	1	3	15	16	13	2	–	24	·
Rok	15.5	0.7	10.5	0.7	24	0.8	29.5	1.3	106	1.4	94	1.2	129.5	1.7	33	1.9	653	0.7	694.2	29.0	30.VII	19	28	93	44	8	2	39	138	170	118	18	–	55	31

Rożnów

$\varphi = 49°46'$ $\lambda = 20°41'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T																							
											Średnie				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.4	-6.6	9.4	4	-22.2	27	-4.5	-1.0	-3.3	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.1	7.2	6.9
II	–	–	–	–	5.1	-0.9	11.9	18	-7.9	6	0.1	3.9	1.5	1.8	5.3	5.7	5.4	5.5	8.4	7.1	7.9	7.8	1.0	2.5	1.5	1.7	8.0	7.4	7.0	7.5
III	–	–	–	–	10.0	2.9	21.0	18	-2.3	23	4.3	8.4	6.1	6.2	6.5	6.7	7.0	6.7	7.8	6.2	7.4	7.1	2.0	4.7	2.7	3.1	8.7	7.8	6.8	7.8
IV	–	–	–	–	17.2	5.9	25.4	15	-1.8	10	8.3	15.8	10.7	11.4	8.0	8.8	8.9	8.6	7.3	4.9	6.8	6.3	3.2	9.9	4.4	5.8	5.3	5.7	5.8	5.6
V	–	–	–	–	16.4	7.8	24.5	6	3.1	12	9.7	14.7	11.1	11.6	10.2	10.3	11.0	10.5	8.4	6.3	8.2	7.6	2.0	7.0	2.5	3.8	7.6	7.5	7.0	7.4
VI	–	–	–	–	23.1	12.8	32.1	27	7.6	21	15.7	21.6	16.8	17.7	14.6	14.6	15.3	14.8	8.2	5.8	8.0	7.3	3.4	11.8	4.6	6.6	5.5	5.7	6.4	5.9
VII	–	–	–	–	21.8	12.1	31.0	3	7.6	6	15.0	20.0	15.6	16.6	13.5	13.2	14.6	13.8	7.9	5.8	8.2	7.3	3.9	11.1	3.4	6.1	5.9	7.4	6.6	6.6
VIII	–	–	–	–	22.8	13.3	33.6	11	8.3	31	15.1	21.2	17.0	17.6	14.2	15.3	15.6	15.0	8.2	6.1	8.0	7.4	3.3	11.0	4.1	6.1	5.9	5.8	6.5	6.1
IX	–	–	–	–	21.5	10.6	30.5	17	2.2	23	11.9	20.6	14.5	15.4	12.1	12.8	13.6	12.8	8.5	5.4	8.2	7.4	2.3	12.3	3.3	6.0	6.4	4.7	4.3	5.1
X	–	–	–	–	16.3	8.5	22.0	20	2.0	22	9.3	15.7	11.7	12.1	9.6	10.3	10.1	10.0	8.2	5.9	7.4	7.2	2.2	7.9	3.8	4.6	6.2	5.2	4.1	5.2
XI	–	–	–	–	8.1	2.1	15.6	1	-5.3	22	3.5	7.0	4.2	4.7	7.1	8.0	7.5	7.5	8.9	8.0	8.8	8.6	1.0	2.4	1.0	1.5	7.7	6.9	7.3	7.3
XII	–	–	–	–	0.4	-6.9	16.9	2	-26.0	26	-3.9	-1.5	-3.5	-3.1	4.7	4.9	4.4	4.7	8.3	7.5	7.8	7.9	0.8	1.7	1.2	1.2	7.8	7.2	7.7	7.6
Rok	–	–	–	–	13.6	5.1	33.6	11.VIII	-26.0	26.XII	7.0	12.2	8.5	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	6.4	6.6

Cieszyn

$\varphi = 49°45'$ $\lambda = 18°38'$

I	–	–	–	–	1.4	-5.5	11.0	4	-18.3	27	-3.6	0.0	-2.3	-2.0	4.1	4.6	4.3	4.3	8.1	7.2	7.9	7.7	1.0	1.8	1.2	1.3	7.0	6.8	5.4	6.4
II	–	–	–	–	5.4	-1.2	16.0	18	-8.9	6	0.1	4.5	1.2	1.8	5.7	6.6	6.1	6.1	9.2	7.9	9.1	8.7	0.5	2.0	0.6	1.0	7.9	7.8	6.3	7.3
III	–	–	–	–	10.7	1.7	20.2	18	-2.8	20	3.5	8.8	5.6	5.9	6.9	7.5	7.5	7.3	8.8	6.7	8.2	7.9	1.1	4.3	1.8	2.4	8.2	7.7	6.5	7.5
IV	–	–	–	–	18.3	6.4	25.4	7,8	-1.5	10	9.1	17.1	11.2	12.2	8.8	9.2	9.4	9.1	7.6	4.8	7.1	6.5	3.0	11.0	4.2	6.1	4.9	5.2	4.6	4.9
V	–	–	–	–	17.0	7.3	23.9	6	2.6	15	9.7	15.4	10.7	11.6	10.5	11.2	11.1	10.9	8.7	6.5	8.6	7.9	1.7	7.0	2.0	3.6	7.7	8.3	7.9	8.0
VI	–	–	–	–	23.5	12.3	30.9	27	6.7	21	16.1	21.7	16.4	17.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.8	6.3	5.7
VII	–	–	–	–	21.9	11.3	30.7	3	6.3	8	14.9	20.3	15.0	16.3	14.1	15.9	15.0	15.0	8.3	6.8	8.7	7.9	3.2	8.7	3.0	5.0	6.8	7.0	6.0	6.6
VIII	–	–	–	–	22.7	12.2	30.9	6	7.4	14	14.5	21.3	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	5.4	6.1
IX	–	–	–	–	22.7	10.0	30.5	17,18	2.0	23	11.8	21.5	14.6	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.0	3.2	4.3
X	–	–	–	–	17.1	7.2	22.6	5,8	2.3	10	9.4	16.2	10.6	11.7	9.9	10.9	10.3	10.4	8.5	6.1	8.0	7.5	2.1	7.9	2.8	4.3	7.2	6.4	4.4	6.0
XI	–	–	–	–	7.7	1.2	16.5	3	-4.1	21	2.8	6.9	3.6	4.2	7.1	7.6	7.4	7.4	9.3	7.7	9.2	8.7	0.7	2.7	0.7	1.4	8.7	8.1	7.6	8.1
XII	–	–	–	–	1.0	-6.9	18.3	5	-26.3	25	-3.9	-1.0	-3.4	-2.9	4.4	4.9	4.6	4.6	7.8	7.8	8.0	7.9	1.2	1.7	1.0	1.3	7.6	7.5	6.4	7.2
Rok	–	–	–	–	14.1	4.7	30.9	27.VI, 6.VIII	-26.3	25.XII	7.0	12.7	8.2	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.8	5.8	6.5

Cieszyn - Bobrek

$\varphi = 49°45'$ $\lambda = 18°39'$

I	–	–	–	–	1.4	-5.9	10.5	4	-18.8	27	-3.5	0.2	-2.4	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.2	5.5	6.1
II	–	–	–	–	5.3	-1.5	14.7	18	-14.7	6	0.0	4.6	1.2	1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	6.2	6.9
III	–	–	–	–	10.5	1.5	19.7	18	-2.6	23	3.4	8.7	5.4	5.7	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	6.6	7.4
IV	–	–	–	–	17.7	5.0	25.2	7	-3.0	10	9.9	16.9	10.2	11.8	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.0	4.9	5.4
V	–	–	–	–	17.0	6.1	24.5	6	0.2	2	10.0	15.2	9.8	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.0	7.7	7.8
VI	–	–	–	–	23.5	10.9	31.5	27	4.7	21	16.4	21.6	15.1	17.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.6	5.6	5.8
VII	–	–	–	–	22.0	10.7	30.5	3	5.2	8	15.4	20.2	14.5	16.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	6.3	6.8
VIII	–	–	–	–	22.8	11.6	31.1	6	6.1	31	15.3	21.4	15.4	16.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.5	5.1	5.9
IX	–	–	–	–	22.4	8.2	30.5	17	-0.1	23	11.8	21.3	13.0	14.8	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.9	3.3	4.1
X	–	–	–	–	16.7	6.1	22.6	8	0.7	10	8.5	15.8	9.9	11.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.0	4.3	5.7
XI	–	–	–	–	7.5	0.9	15.7	3	-5.1	21,23	2.7	6.7	3.3	4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.7	7.1	7.7
XII	–	–	–	–	0.8	-8.1	18.1	5	-29.7	25	-4.5	-1.1	-4.0	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.1	7.3	7.5
Rok	–	–	–	–	14.0	3.8	31.5	27.VI	-29.7	25.XII	7.1	12.6	7.6	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.7	5.8	6.4

Klimczak

$\varphi = 49°44'$ $\lambda = 19°00'$

I	–	–	–	–	-2.6	-8.4	5.1	4	-21.3	18	-5.7	-3.8	-5.8	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.5	4.9	5.3
II	–	–	–	–	0.9	-3.9	11.1	18	-9.8	6	-2.1	-0.3	-2.1	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	3.4	-1.9	14.2	10	-7.8	29	-0.3	2.0	0.8	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.8	6.6	7.0
IV	–	–	–	–	12.2	3.4	20.0	7	-5.7	1	6.0	11.0	6.4	7.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.0	3.0	3.9
V	–	–	–	–	9.1	3.8	17.5	6	-2.5	12	5.9	7.7	5.9	6.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.5	6.6	6.9
VI	–	–	–	–	17.4	9.5	24.6	25	5.1	17	11.9	15.3	11.8	12.7	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.2	5.6	4.9
VII	–	–	–	–	14.9	7.8	24.1	3	4.0	6	10.0	13.3	10.3	11.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.2	5.4	5.5
VIII	–	–	–	–	15.8	8.8	25.9	10	4.2	17	10.7	14.5	11.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	16.5	9.2	24.4	3	3.8	12	10.5	14.0	11.8	12.0	–	–	–	–	–	–	–	–	–	–	–	–	3.9	3.4	2.4	3.2
X	–	–	–	–	11.6	–	16.9	8	–	–	7.2	10.3	7.4	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.2	3.8	5.0
XI	–	–	–	–	4.5	–	10.9	12	–	–	0.3	2.1	0.3	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.3	6.0	6.4
XII	–	–	–	–	-2.5	–	11.8	5	–	–	-7.1	-4.8	-6.5	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.8	6.6	6.8
Rok	–	–	–	–	8.4	–	25.9	10.VIII	–	–	3.9	6.8	4.3	4.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Rozinów

$H_s = 300\,m$ $h_w = 20\,m$ 1961

MIESIĄC	ROZKŁAD WIATRU °D. *mD																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	n>10 m/s	n>15 m/s	●	●	n≥0.1	n≥1.0	n≥10.0	≡	⊞	≋
I	1	1.0	1	3.0	6	1.3	21	2.5	17	3.0	6	4.0	7	4.4	10	3.0	24	2.2	21.6	8.5	5	10	14	26	·	1	·	4	13	15	6	·	3	29	·
II	1	1.0	·	·	1.5	3.7	15.5	1.3	10	1.2	18	2.6	12	2.6	10	2.8	18	1.7	23.9	8.0	9	·	·	18	·	1	·	2	14	13	7	·	8	5	·
III	1	3.0	·	·	·	·	2	1.5	2	5.0	28	3.3	33	5.0	20	4.0	7	3.8	25.7	4.7	31	·	·	8	·	4	1	·	16	16	9	·	5	4	·
IV	3	3.0	4.5	1.4	10.5	2.6	30.5	2.6	15.5	2.7	7	2.7	5	4.0	2	2.0	12	2.2	19.1	5.4	1	·	·	1	1	1	·	5	7	10	7	·	·	·	4
V	11.5	1.3	4	1.0	7	1.0	24.5	1.2	10.5	2.6	3	1.7	5	4.8	14.5	2.7	13	1.6	75.5	22.7	6	·	·	·	·	·	·	·	13	17	11	1	5	·	7
VI	10	1.3	2	1.0	4	1.1	26.5	1.5	11.5	2.0	1	2.0	7	4.1	16	2.4	13	1.7	111.7	24.5	7	·	·	·	7	·	·	1	7	13	11	5	2	·	8
VII	8	1.5	1	1.0	4	1.0	19.5	1.5	14.5	3.6	6.5	1.3	5.5	2.5	19	2.2	15	1.8	103.7	29.6	30	·	·	·	8	1	1	2	10	20	13	2	·	·	7
VIII	7.5	9.4	3	1.3	4.5	1.0	27	1.4	11.5	2.3	4	2.0	9	1.8	18.5	2.2	8	1.6	65.2	22.3	12	·	·	·	9	·	·	1	9	10	9	2	·	·	3
IX	1	1.0	2	1.0	2	2.0	40.5	1.3	9.5	1.5	4.5	1.9	11.5	2.5	5	5.8	14	1.6	17.0	5.4	6	·	·	·	8	1	1	6	5	8	4	·	8	·	3
X	4	2.0	·	·	3.5	4.0	44	2.7	17.5	6.0	3	1.0	1	1.0	8	2.3	12	2.9	30.6	17.5	30	·	·	·	·	4	1	7	5	8	6	1	4	·	·
XI	5	1.4	2	1.5	2	1.5	29.5	1.8	12	3.6	3	1.7	10	4.2	7.5	2.6	19	2.0	63.6	19.4	4	·	·	9	·	·	·	1	15	14	10	2	9	1	·
XII	9.5	2.2	3.5	1.0	1.5	1.0	11	1.6	21	3.6	7	1.4	6.5	3.9	19	4.4	14	2.6	73.3	20.9	6	9	16	23	·	1	·	1	13	14	10	3	·	24	
Rok	62.5	1.7	23	1.0	46.5	1.7	291.5	1.7	162.5	3.1	89	2.1	112.5	3.4	148.5	3.0	169	2.1	630.8	29.6	30.VII	19	30	85	38	14	4	30	127	158	103	16	44	63	32

Cieszyn

$H_s = 300\,m$ $h_w = 15{,}8\,m$

I	6	1.2	5	1.3	3.5	1.0	17.5	1.9	28.5	1.8	10.5	2.1	1.5	1.0	7.5	1.2	13	1.4	160	9.3	4	9	12	25	·	·	·	6	14	10	3	·	·	2	·
II	·	·	2	1.0	·	·	10	1.4	38	1.3	22.5	1.4	2.5	1.0	4	1.2	5	1.2	65.3	18.6	9	·	·	21	·	·	·	2	13	13	11	1	2	1	·
III	2	1.0	·	·	·	·	4	1.5	38	1.6	29.5	1.4	9	1.4	4.5	1.4	6	1.4	57.1	14.6	14	·	·	10	·	·	·	1	19	15	11	1	1	1	·
IV	1.5	1.3	6.5	1.5	5	1.3	20	1.2	22.5	1.3	13	1.8	3	1.0	5.5	1.8	13	1.2	28.8	11.1	18	·	·	1	4	·	·	5	1	7	7	1	·	·	2
V	1.0	1.6	5.5	1.0	2.5	1.0	7.5	1.5	17	1.5	18	1.6	4	1.0	9.5	1.0	19	1.1	110.3	27.9	6	·	·	·	·	·	·	·	20	18	13	2	·	·	32
VI	2	1.8	8	1.4	4	1.0	11.5	1.2	25	1.4	12	1.5	1.5	1.3	6	1.6	20	1.1	235.8	57.5	27	·	·	·	9	1	·	4	8	16	13	6	2	·	92
VII	2	1.0	1	1.0	2	1.0	8.5	1.6	36.5	1.8	17.5	1.4	4.5	1.3	6	1.0	15	1.3	128.6	24.1	31	·	·	·	8	·	·	2	11	15	12	5	·	·	23
VIII	6	1.0	0.5	1.0	·	·	6	1.3	31.5	1.6	21	2.0	5	1.2	6	1.2	17	1.3	81.9	26.1	12	·	·	·	7	·	·	3	6	11	6	3	1	·	12
IX	6	2.2	7.5	1.3	2.5	1.0	10.5	1.5	17	1.5	11.5	2.5	3	2.3	4	1.8	28	1.2	14.7	4.9	26	·	·	·	8	·	·	11	5	9	4	·	2	·	2
X	5	1.6	1.2	1.6	3	1.2	16	1.8	17	2.2	6.5	2.3	1.5	2.3	3	1.0	29	1.3	10.8	3.5	20	·	·	·	·	·	·	4	9	7	4	·	2	·	·
XI	2.5	1.0	3	1.0	0.5	1.0	2.5	1.8	26.5	1.4	19	1.3	3	1.2	6	1.0	27	0.9	97.2	59.2	4	·	·	7	·	·	·	·	19	17	10	2	2	4	·
XII	1.0	1.1	6	1.2	1	1.0	4.5	1.8	23	1.5	16	2.1	5	1.4	10.5	1.1	17	1.2	88.9	29.3	6	10	15	25	·	·	·	4	17	17	11	3	2	23	·
Rok	5.3	1.2	5.7	1.1	2.4	0.8	118.5	1.5	320.5	1.6	197	1.8	43.5	1.4	72.5	1.3	209	1.2	935.4	59.2	4.XI	19	27	89	36	1	·	42	142	155	105	24	44	31	192

Cieszyn - Bobrek

$H_s = 300\,m$ $h_w = 14\,m$

I	2	2.0	2.2	1.7	5.5	2.6	8	5.9	25.5	4.2	12	2.1	5.5	1.7	4.5	1.0	8	2.7	14.6	9.1	4	11	12	24	·	2	·	5	9	11	3	·	·	3	·
II	1.5	1.0	2.5	1.2	1	1.5	6.5	4.1	20.5	3.3	11.5	1.9	11.5	1.5	11	1.3	18	1.8	69.1	18.9	9	1	·	18	·	·	·	2	13	14	13	1	6	2	·
III	4	1.5	·	·	·	·	·	·	4.5	1.7	27	4.5	29	2.7	14.5	2.3	14	2.7	51.4	11.9	14	·	·	12	·	·	·	1	16	18	10	1	1	4	1
IV	3.5	1.7	2.1	2.6	5	2.0	6.5	2.5	11	3.2	17	4.1	4.5	3.7	8.5	1.6	13	2.5	27.9	7.6	18	·	·	2	1	·	·	4	4	8	7	·	·	·	2
V	13.5	2.1	10	2.2	2.5	1.2	4.5	2.9	4	2.0	15	3.5	16.5	3.1	14	1.9	13	2.2	104.3	25.2	6	·	·	·	·	1	·	·	17	19	15	2	·	·	9
VI	4	2.5	9	2.3	3	1.5	2.5	1.8	11.5	2.3	14.5	2.8	15	2.7	12.5	1.7	18	1.9	231.9	71.3	27	·	·	·	9	·	·	3	7	17	13	7	·	·	15
VII	5.5	1.4	3	2.0	·	·	1	3.0	11	3.0	25.5	3.8	21	2.8	9	1.6	17	2.3	132.3	32.0	31	·	·	·	8	·	·	3	10	14	12	5	·	·	9
VIII	3.5	2.0	5.5	2.0	2	1.0	1	2.5	8	2.8	22	3.7	18.5	2.8	8.5	1.2	24	2.0	73.6	25.2	12	·	·	·	9	·	·	3	7	9	6	2	·	·	5
IX	4.5	1.6	10	2.2	1	3.0	4.5	2.3	7	3.3	17	3.9	11	2.2	6	2.0	29	1.9	15.9	7.2	26	·	·	1	8	·	·	12	6	8	4	·	1	·	2
X	5.5	1.4	14	2.8	2.5	2.2	13.5	4.3	19	3.8	6	2.8	6	2.6	4.5	1.8	22	2.4	13.8	4.7	20	·	·	·	·	·	·	5	7	6	5	·	2	·	·
XI	9.5	1.3	7.5	1.5	3	1.3	3	2.5	11.5	3.2	17.5	2.1	15.5	1.5	7.5	1.1	15	1.6	93.0	52.9	4	·	·	12	·	·	·	·	16	16	8	2	6	5	·
XII	13.5	1.5	14	1.6	4.5	1.0	1.5	2.7	14	3.8	13	3.8	10	2.5	10.5	1.6	12	2.1	89.6	29.5	6	14	16	26	·	·	·	3	15	19	10	3	2	23	
Rok	70.5	1.7	118.5	1.8	30	1.4	52.5	2.9	147.5	3.0	198	3.2	164	2.5	111	1.6	203	2.2	917.4	71.3	27.VI	26	28	95	35	3	·	41	127	159	106	23	18	37	43

Klimczak

$H_s = 1010\,m$ $h_w = 16\,m$

I	18	8.1	3	4.3	1	4.0	·	·	38	11.6	·	·	8	3.8	·	·	25	4.8	29.3	11.3	4	7	26	31	·	11	10	–	–	9	7	1	10	31	·
II	13	6.0	·	·	·	·	·	·	33	6.8	1	5.0	7	6.9	1	9.0	29	4.3	36.5	8.1	3	·	12	28	·	4	2	–	–	13	12	·	15	28	
III	42	7.7	·	·	·	·	·	·	28	10.1	2	9.0	11	5.4	·	·	10	7.4	97.9	20.0	14	·	10	21	·	12	5	–	–	15	14	1	18	28	·
IV	13	4.5	7	2.9	1	2.0	·	·	39	5.2	·	·	1	5.0	·	·	29	3.2	71.7	38.1	18	·	·	4	·	1	1	–	–	8	8	1	6	4	2
V	28	3.6	1	4.0	·	·	·	·	32	5.0	·	·	4	5.8	·	·	28	3.1	130.1	18.9	10	·	·	2	·	1	1	–	–	14	14	6	15	·	4
VI	11	4.4	2	4.0	5	2.8	·	·	39	3.8	·	·	3	2.3	·	·	30	2.5	213.6	102.4	27	·	·	·	·	·	·	–	–	12	10	3	5	·	8
VII	13	4.2	·	·	1	3.0	·	·	44	6.5	4	4.0	6	5.0	·	·	25	4.2	175.6	37.6	30	·	·	·	·	4	1	–	–	15	13	8	8	·	6
VIII	17	3.8	0.5	4.0	1.5	3.3	·	·	56	5.3	·	·	5	5.4	·	·	11	4.4	113.1	32.9	12	·	·	·	1	3	1	–	–	13	12	3	6	·	5
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	29.5	8.2	26	·	·	·	·	–	–	–	–	8	7	·	–	·	–
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	23.5	7.6	14	–	·	·	·	–	–	–	–	8	7	·	10	·	·
XI	5	7.0	·	·	·	·	·	·	44	7.6	10.5	7.2	0.5	1.0	1	6.0	29	5.0	60.7	25.0	4	–	5	–	·	12	4	–	–	12	9	2	18	11	·
XII	22	6.1	2	3.0	1	2.0	·	·	38.5	9.2	2.5	9.0	·	·	8	4.0	19	5.9	107.1	27.9	11	–	20	–	·	8	5	–	–	14	13	3	16	25	
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1088.6	102.4	27.VI	–	73	–	1	–	–	–	–	144	126	28	–	127	–

Maków Podhalański — φ = 49°44' — λ = 19°40' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{m.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	1.5	-8.7	12.3	4	-19.4	27	-5.7	0.6	-4.5	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.0	5.0	5.4
II	–	–	–	–	5.8	-2.8	15.5	18	-12.7	6	-1.5	4.5	0.3	0.9	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.6	5.5	6.0
III	–	–	–	–	10.2	0.8	21.4	10	-6.8	23	2.7	8.6	4.6	5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.5	6.4	6.9
IV	–	–	–	–	17.7	4.0	24.9	15	-1.9	10	7.6	16.8	9.5	10.8	–	–	–	–	–	–	–	–	–	–	–	–	3.9	3.8	3.2	3.6
V	–	–	–	–	16.5	6.3	24.4	29	2.3	15	9.1	15.2	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.7	7.2	6.8
VI	–	–	–	–	23.4	10.7	31.3	27	5.5	1	15.2	21.3	15.3	16.8	–	–	–	–	–	–	–	–	–	–	–	–	3.9	5.0	5.3	4.7
VII	–	–	–	–	21.5	10.2	30.3	3	5.3	8,25	14.2	20.0	14.7	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.4	6.7	6.1
VIII	–	–	–	–	22.7	10.9	33.3	11	6.3	14,31	13.5	21.5	15.1	16.3	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.9	4.4	4.8
IX	–	–	–	–	22.2	7.9	31.3	17	-0.9	23	10.2	21.4	12.6	14.2	–	–	–	–	–	–	–	–	–	–	–	–	3.7	3.5	3.2	3.5
X	–	–	–	–	17.7	4.6	22.9	28	0.1	25	7.0	16.8	9.0	10.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.5	4.0	4.8
XI	–	–	–	–	8.3	0.1	16.3	3	-8.8	21	2.3	7.5	3.0	4.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.2	6.8	7.0
XII	–	–	–	–	0.6	-9.3	17.4	2,5	-29.7	25	-5.8	-0.8	-4.8	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.5	5.7	6.0
Rok	–	–	–	–	14.0	2.9	33.3	11.VIII	-29.7	25.XII	5.7	12.8	7.1	8.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.3	5.3	5.5

Biecz — φ = 49°44' — λ = 21°15'

I	–	–	–	–	-0.7	-8.2	8.2	4	-24.9	27	-5.4	-2.1	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.1	6.0	6.0
II	–	–	–	–	4.0	-1.5	13.3	18	-6.9	5	-0.2	3.1	0.7	1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	6.1	6.7
III	–	–	–	–	9.7	2.0	19.4	18	-3.4	23	3.9	8.0	5.3	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	5.8	7.0
IV	–	–	–	–	17.4	3.6	25.5	7	-3.9	10	6.8	15.9	9.8	10.6	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.6	3.5	4.5
V	–	–	–	–	16.9	5.9	25.9	5	0.9	13	9.6	15.3	9.9	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	5.2	6.1
VI	–	–	–	–	23.8	10.5	31.7	27	5.0	21	15.1	22.2	15.5	17.1	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.7	4.9	4.7
VII	–	–	–	–	22.2	10.1	32.9	2	5.1	7	14.1	20.1	14.2	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.3	5.8	5.7
VIII	–	–	–	–	23.1	11.1	33.5	11	5.2	31	14.1	21.6	15.5	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.2	3.8	4.7
IX	–	–	–	–	21.3	7.0	29.9	17	-2.5	23	9.4	20.2	12.1	13.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.1	2.6	3.8
X	–	–	–	–	16.5	6.1	24.4	20	0.0	22	8.0	15.7	9.9	10.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.8	2.7	4.4
XI	–	–	–	–	7.8	1.8	15.9	7	-6.1	21	3.2	6.7	4.6	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	6.5	6.8
XII	–	–	–	–	0.1	-8.0	12.7	4	-31.9	26	-4.5	-1.8	-4.0	-3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	6.1	6.8
Rok	–	–	–	–	13.5	3.4	33.5	11.VIII	-31.9	26.XII	6.2	12.1	7.4	8.3	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.8	4.9	5.6

Jasło — φ = 49°44' — λ = 21°28'

I	–	–	–	–	-0.8	-7.8	9.0	4	-24.3	27	-5.4	-2.2	-4.3	-4.0	3.7	4.0	3.9	3.9	7.8	7.1	7.8	7.6	0.9	1.6	1.1	1.2	6.6	5.4	5.2	5.7
II	–	–	–	–	4.0	-1.1	12.8	18	-3.8	5	-0.1	2.9	0.7	1.0	5.3	5.7	5.4	5.5	8.7	7.6	8.4	8.2	0.8	1.9	1.0	1.2	7.9	6.7	6.0	6.9
III	–	–	–	–	9.9	2.6	18.1	10	-3.6	23	3.9	8.3	5.5	5.8	6.7	6.8	7.0	6.8	8.2	6.3	7.8	7.4	1.6	4.5	2.2	2.8	7.5	7.2	5.6	6.8
IV	–	–	–	–	17.9	4.5	25.5	15	-3.4	10	7.4	16.5	10.7	11.3	7.9	8.1	8.8	8.3	7.6	4.3	6.8	6.2	2.6	11.4	4.3	6.1	4.4	5.1	3.4	4.3
V	–	–	–	–	17.6	6.8	24.2	29	1.7	3	9.4	16.0	11.2	12.0	10.2	10.3	10.8	10.4	8.6	5.8	8.0	7.5	1.8	8.5	2.7	4.3	6.9	6.1	5.7	6.2
VI	–	–	–	–	24.4	11.7	31.1	26	6.0	21	15.2	22.6	16.8	17.8	14.8	15.2	15.5	15.2	8.5	5.7	8.1	7.4	2.6	12.9	3.8	6.4	4.6	4.1	5.3	4.7
VII	–	–	–	–	23.0	11.1	31.5	4	5.4	7	14.1	21.5	15.8	16.8	13.6	13.3	14.6	13.8	8.4	5.4	8.1	7.3	2.7	13.2	3.7	6.5	4.9	5.4	6.5	5.6
VIII	–	–	–	–	23.6	11.9	34.0	11	5.9	31	14.1	22.0	16.6	17.3	14.4	15.0	15.8	15.1	8.9	5.8	8.2	7.6	2.1	12.4	3.6	6.0	5.2	5.0	4.8	5.0
IX	–	–	–	–	21.7	8.0	31.0	18	-1.8	23	9.6	20.4	13.6	14.3	11.1	14.2	12.8	12.7	9.1	6.0	8.1	7.7	1.3	10.6	3.1	5.0	4.6	4.0	2.3	3.6
X	–	–	–	–	16.6	6.9	24.6	20	1.6	12	8.2	15.7	10.9	11.4	8.7	9.7	9.6	9.3	8.1	5.6	7.5	7.1	2.4	8.5	3.6	4.8	5.1	4.0	2.8	4.0
XI	–	–	–	–	7.9	2.2	15.9	7	-5.4	21	3.6	6.6	4.7	4.9	7.0	7.7	7.5	7.5	8.6	7.7	8.5	8.3	1.0	2.4	1.3	1.6	8.1	7.1	5.9	7.0
XII	–	–	–	–	0.0	-7.1	12.9	4	-31.0	26	-4.2	-1.6	-3.5	-3.2	4.5	4.7	4.5	4.6	8.1	7.7	8.0	7.9	1.0	1.5	1.1	1.2	7.3	6.8	5.5	6.5
Rok	–	–	–	–	13.8	4.1	34.0	11.VIII	-31.0	26.XII	6.3	12.4	8.2	8.8	9.0	9.6	9.7	9.4	8.4	6.2	7.9	7.5	1.7	7.4	2.6	3.9	6.1	5.6	4.9	5.5

Tęgoborze — φ = 49°43' — λ = 20°39'

I	–	–	–	–	0.5	-6.7	9.7	4	-22.0	27	-4.4	-0.9	-3.1	-2.9	4.0	4.3	4.2	4.2	8.3	7.2	8.1	7.9	0.9	1.7	1.1	1.2	7.4	6.0	5.8	6.4
II	–	–	–	–	4.9	-1.0	11.9	18	-8.3	6	0.2	3.5	1.3	1.6	5.5	5.9	5.7	5.7	8.8	7.5	8.5	8.3	0.8	2.0	1.0	1.3	8.0	7.1	6.4	7.2
III	–	–	–	–	10.9	3.0	21.1	18	-3.0	23	4.5	9.2	6.1	6.5	7.0	7.3	7.5	7.3	8.3	6.3	7.9	7.5	1.6	4.9	2.2	2.9	7.9	7.5	6.1	7.2
IV	–	–	–	–	17.3	6.0	25.8	7,15	-0.5	10	8.1	16.0	11.0	11.5	8.4	9.2	9.2	8.9	7.7	5.1	7.0	6.6	2.6	9.6	4.2	5.5	4.9	5.3	4.4	4.9
V	–	–	–	–	16.8	7.6	23.3	6	3.5	13,14	10.0	14.9	11.0	11.7	10.3	10.3	11.1	10.6	8.3	6.2	8.4	7.6	2.2	7.2	2.3	3.9	7.5	7.5	6.2	7.1
VI	–	–	–	–	23.3	12.7	30.1	27	8.3	17	15.6	21.6	16.8	17.7	14.9	14.9	15.4	15.1	8.3	5.8	8.0	7.4	3.1	11.4	3.9	6.1	5.1	6.5	5.8	5.8
VII	–	–	–	–	21.8	11.9	29.8	4	8.1	6	15.0	20.2	15.4	16.5	13.8	13.5	14.7	14.0	8.1	5.8	8.3	7.4	3.5	11.0	3.1	5.9	5.7	7.4	6.4	6.5
VIII	–	–	–	–	23.4	12.9	34.1	11	8.4	31	15.4	21.8	16.4	17.5	14.8	15.6	15.9	15.4	8.3	5.9	8.4	7.5	3.0	11.5	3.1	5.9	5.7	6.0	5.0	5.6
IX	–	–	–	–	21.7	10.1	30.4	18	2.1	23	12.2	20.5	14.3	15.3	11.8	13.4	13.3	12.8	8.2	5.6	8.1	7.3	2.8	11.4	3.2	5.8	5.0	4.6	3.9	4.5
X	–	–	–	–	16.3	7.7	21.1	20	3.0	22	9.5	15.4	11.5	12.0	9.5	10.5	10.2	10.1	8.1	6.1	7.6	7.3	2.6	7.3	3.5	4.5	6.3	5.4	5.3	5.7
XI	–	–	–	–	8.4	2.4	16.3	1	-4.0	21	3.9	7.2	4.7	5.1	7.3	8.0	7.6	7.6	8.8	7.9	8.7	8.5	1.1	2.6	1.2	1.6	7.6	6.9	6.9	7.1
XII	–	–	–	–	0.6	-6.9	16.1	2	-26.4	25	-3.8	-1.3	-3.4	-3.0	4.8	5.4	4.9	5.0	8.5	8.4	8.6	8.5	0.8	1.2	0.8	0.9	8.1	7.6	7.3	7.7
Rok	–	–	–	–	13.8	5.0	34.1	11.VIII	-26.4	25.XII	7.2	12.3	8.5	9.1	9.3	9.9	10.0	9.7	8.3	6.5	8.1	7.6	2.1	6.8	2.5	3.8	6.6	6.5	5.8	6.3

Maków Podhalański $H_s = 350\,m$ $h_w = 18\,m$ 1961

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temp. Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	═	⊞	R 10
I	·	·	7	2.1	11	1.3	4.5	1.2	7	2.6	7.5	2.7	2	3.0	4	2.5	50	1.0	30.0	7.8	5	12	12	30	·	·	·	7	10	9	9	·	4	–	·
II	2	2.2	1	1.0	8	1.4	12	1.0	7	1.0	5	1.6	7	2.3	2	2.8	40	0.8	51.8	11.9	9	1	1	22	·	·	·	8	13	14	13	1	14	–	·
III	3.5	3.0	·	·	3	1.0	4	1.0	6.5	1.2	16	2.1	12	2.6	12	3.0	36	1.4	71.3	13.3	14	·	·	11	·	·	·	4	15	18	14	1	6	–	·
IV	1	1.0	2	3.5	10	2.1	10	2.1	6	1.8	5	1.6	4	2.0	2	3.5	50	0.9	27.1	13.4	18	·	·	1	·	·	·	12	2	7	5	1	3	·	2
V	·	·	1	2.0	8	3.1	2.5	2.8	6.5	2.2	8	2.8	8	4.8	·	·	59	1.2	138.6	32.2	6	·	·	·	·	·	·	2	12	19	16	4	10	·	3
VI	2.5	4.2	1	3.0	4.5	3.9	6.5	2.5	8.5	2.4	4	4.0	4	2.5	4	5.2	55	1.3	127.9	26.7	4	·	·	·	10	·	·	9	6	13	13	5	4	·	5
VII	·	·	·	·	8	3.2	7.5	2.1	8.5	3.9	12	5.4	7	5.3	2	6.5	48	2.0	119.4	26.4	28	·	·	·	8	·	·	4	10	15	14	3	5	·	2
VIII	3	3.0	1	3.0	8	2.8	4	2.2	10	3.6	8	6.2	5	4.4	3	4.3	51	1.8	66.7	24.2	12	·	·	·	9	1	·	6	7	8	8	2	7	·	3
IX	0.5	8.0	2	3.5	17	3.6	6	2.3	2	3.0	9	4.2	3	4.7	0.5	8.0	50	1.7	13.6	4.1	14	·	·	1	8	·	·	14	5	7	6	·	5	·	1
X	4	3.5	2	10.0	15	3.5	5.5	6.2	5.5	4.7	1	3.0	1	2.0	2	2.0	57	1.7	21.6	8.8	30	·	·	·	·	1	·	8	8	6	4	·	10	·	·
XI	1.5	3.7	·		3	4.3	10	4.6	4	4.1	5	3.8	7	5.3	2.5	4.6	67	1.6	63.1	20.2	4	·	·	8	·	·	·	5	17	11	11	1	14	–	·
XII	6	3.2	1	5.0	5	2.6	·	·	3	3.3	5	7.2	13	5.5	7	7.1	53	2.2	99.5	35.7	6	14	15	27	·	4	·	4	12	13	11	4	3	–	·
Rok	24	2.6	18	2.8	100.5	2.7	72.5	2.3	74.5	2.8	85.5	3.7	73	3.7	41	4.1	606	1.5	828.6	35.7	6.XII	27	28	100	35	6	·	83	117	140	124	22	85	–	16

Biecz $H_s = 260\,m$ $h_w = 16{,}1\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temp. Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	═	⊞	R 10
I	4	3.8	5	3.8	1	2.0	·	·	18	4.9	28	4.4	7	2.0	11	3.5	19	3.2	20.5	8.0	31	10	14	28	·	3	·	4	10	10	6	·	2	22	·
II	·	·	1	1.0	1	3.0	·	·	10	4.3	19	4.4	7	3.0	12	2.3	34	2.1	22.6	6.2	9	·	1	18	·	·	·	1	13	11	7	·	3	1	
III	3	2.7	·	·	·	·	·	·	1	6.0	9	4.2	29	4.0	38	5.0	43	3.8	22.8	3.5	31	·	·	8	·	4	·	3	12	15	8	·	1	1	·
IV	2	5.0	3	4.0	13	4.8	4	3.8	9	4.3	10	3.3	6	2.7	8	5.0	35	2.5	11.9	3.5	1	·	·	3	2	2	·	9	6	7	5	·	·	·	2
V	14	3.6	3	4.0	3	3.3	1	4.0	6	5.0	4	2.2	8	3.2	11	4.5	43	2.1	83.1	17.0	7	·	·	·	1	·	·	1	7	13	11	4	1	·	3
VI	1	3.0	2	4.0	8	3.0	2	4.0	12	2.3	4	3.0	7	3.4	11	2.5	43	1.5	64.3	14.2	7	·	·	·	10	·	·	10	6	13	10	1	·	·	7
VII	5	3.8	·	·	2	2.0	·	·	7	5.1	4	4.8	5	3.0	19	3.8	51	1.8	153.5	29.2	20	·	·	·	9	·	·	5	10	17	14	5	·	·	6
VIII	4	2.5	1	5.0	·	·	2	2.5	6	5.2	5	2.6	17	4.2	15	3.6	43	2.0	49.2	20.3	12	·	·	·	9	1	·	8	5	11	8	2	·	·	2
IX	1	5.0	2	5.5	4	3.0	·	·	3	2.3	5	3.2	6	3.5	9	3.9	60	1.2	13.4	3.9	7	·	·	3	8	·	·	13	6	7	5	·	4	·	2
X	2	4.0	2	2.0	5	4.0	5	5.4	30	5.2	6	3.2	1	6.0	10	3.5	32	3.0	32.8	17.3	30	·	·	·	·	4	·	11	6	6	5	1	4	·	·
XI	3	3.3	2	2.0	4	2.3	1	2.0	15	4.9	7	5.0	16	3.0	15	3.0	27	2.5	51.6	11.0	11	·	·	8	·	·	·	5	15	13	10	2	3	·	·
XII	12	5.1	·	·	1	2.0	1	2.0	12	5.3	14	4.8	4	4.3	21	3.8	28	3.2	55.5	24.5	11	12	15	23	·	4	·	3	14	14	7	1	3	24	·
Rok	51	3.5	21	2.6	42	2.4	16	2.0	129	4.6	115	3.8	113	3.5	180	3.7	428	2.4	581.2	29.2	20.VII	22	30	91	39	18	·	73	110	137	96	16	21	48	22

Jasło $H_s = 240\,m$ $h_w = 15{,}8\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temp. Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	═	⊞	R 10
I	3.5	2.4	2	3.0	0.5	1.0	3	3.7	4.5	6.4	·	·	7.5	2.5	10.5	3.1	21	3.9	47.2	4.7	5,14	10	15	26	·	2	·	5	9	12	5	·	2	23	·
II	0.5	1.0	2.5	2.0	3.5	2.0	1	1.0	29	6.8	1	3.0	6	3.3	6.5	3.8	34	3.1	28.1	7.6	9	·	1	20	·	3	·	2	13	11	7	·	3	4	·
III	·	·	·	·	1	4.0	0.5	1.0	6.5	6.1	5.5	2.6	42.5	4.6	23	5.3	14	4.0	37.0	6.1	31	·	·	7	·	5	·	2	12	21	13	·	2	·	·
IV	2	2.8	7	2.4	16	4.4	5.5	3.5	17.5	4.5	5.5	3.5	6.5	5.0	7	2.8	24	2.9	7.4	2.8	1	·	·	3	1	·	·	9	5	7	3	·	·	·	1
V	8	2.2	4.5	2.6	3.5	3.0	3.5	3.6	6.5	6.1	0.5	7.0	23	2.9	21.5	2.7	22	2.4	99.3	25.4	29	·	·	·	·	·	·	3	9	16	13	4	3	·	2
VI	3	1.7	7.5	1.4	9	2.3	6	3.0	8	4.1	2.5	1.0	12	2.3	13	2.3	29	1.6	77.8	27.5	11	·	·	·	9	·	·	6	3	14	11	2	·	·	6
VII	2	2.0	2.5	2.0	2	1.5	2	3.5	14	5.8	4	2.0	14.5	2.6	14	3.1	38	2.0	104.9	34.2	29	·	·	·	9	·	·	4	8	20	17	3	·	·	4
VIII	2	3.0	2.5	2.2	1.5	3.0	6	1.6	11.5	4.3	1.5	2.0	19.5	3.4	11.5	3.5	37	2.0	55.8	19.8	12	·	·	·	11	·	·	3	4	11	8	2	3	·	3
IX	2	1.5	8	2.4	1	2.5	4.5	2.4	3	5.7	7	2.4	10	2.6	8.5	2.8	46	1.3	34.3	17.0	4	·	·	2	9	·	·	13	3	9	7	1	4	·	3
X	2	1.2	7.5	1.5	12	3.7	6.5	3.6	30.5	5.8	·	·	3.5	1.9	11	2.7	20	3.2	28.1	16.9	30	·	·	·	·	3	·	11	4	7	6	1	2	·	·
XI	2	2.2	1	1.0	7	1.7	3	2.0	33	5.0	1	1.0	15	2.8	15	2.2	13	2.9	41.6	12.8	11	·	·	9	·	1	·	3	14	16	10	1	2	·	·
XII	11.5	2.4	1	2.0	5	2.2	3.5	3.7	25.5	7.2	1	4.5	7	3.9	22.5	3.8	16	3.8	65.8	17.9	11	10	14	21	·	4	·	4	12	17	10	1	3	24	·
Rok	38.5	1.9	46	1.9	61	2.4	45	2.7	230	5.6	29.5	2.4	167	3.2	164	3.2	314	2.8	597.3	34.2	29.VII	20	30	88	39	18	·	65	96	161	110	15	24	51	19

Tęgoborze $H_s = 272\,m$ $h_w = 17{,}6\,m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Temp. Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	◔	●	Opad R≥0.1	R≥1.0	R≥10.0	═	⊞	R 10
I	2	2.0	·	·	·	·	4	2.5	28	3.3	2	6.0	3	2.3	2	2.5	52	1.4	49.1	8.2	5	9	13	26	·	·	·	4	10	10	4	·		19	·
II	·	·	·	·	3	2.0	5	2.6	14	3.2	·	·	1	1.0	·	·	61	0.8	18.7	6.4	9	·	·	17	·	·	·	2	12	9	4	·	5	2	·
III	·	·	·	·	·	·	4	3.2	1	1.0	11	3.0	19	2.0	12	2.6	46	1.2	38.1	6.1	12	·	·	6	·	·	·	2	13	16	13	·	2	·	·
IV	·	·	2	3.5	15	4.2	5	3.2	25.5	2.8	4.5	3.8	4	2.2	6	1.5	28	2.1	23.5	8.5	18	·	·	1	2	·	·	8	5	8	6	·	·	·	3
V	1	1.0	·	·	8	2.2	1	2.0	22	2.5	3	3.0	7	1.6	1	3.0	50	1.1	85.8	23.7	6	·	·	·	·	·	·	·	14	16	13	2	·	·	2
VI	1	2.0	1	2.0	3	1.7	5	3.2	23	2.4	2	3.5	4	2.2	1	2.0	50	1.1	90.2	18.1	27	·	-	·	8	·	·	3	7	12	11	4	·	·	7
VII	·	·	·	·	2	2.0	1	3.0	29	2.7	1	3.0	12	1.6	1	2.0	47	1.2	102.0	26.7	29	·	·	·	8	·	·	3	11	15	12	5	·	·	5
VIII	2	2.0	·	·	1	1.0	1	2.0	24	1.9	2	3.5	11	2.3	1	3.0	51	0.9	84.2	34.6	12	·	·	·	8	·	·	6	4	8	8	3	·	·	1
IX	·	·	2	1.5	4	2.2	5	1.8	24	2.0	1	2.0	7	2.0	·	·	47	0.9	20.8	11.9	26	·	·	·	8	·	·	10	5	6	4	1	4	·	3
X	·	·	2	3.5	7	3.7	7	4.9	35	2.8	3	3.3	3	1.0	·	·	36	1.9	30.2	18.5	30	·	·	·	·	·	·	5	7	6	5	1	3	·	·
XI	1	1.0	1	2.0	1	4.0	1	4.0	28	3.4	3	1.7	6	1.3	·	·	49	1.3	66.9	23.5	4	·	·	5	·	·	·	1	14	12	10	2	5	·	·
XII	6	1.7	·	·	1	1.0	·	·	17	2.8	5	4.0	6	3.2	1	3.0	57	1.1	107.4	31.3	11	9	15	23	·	·	·	2	18	13	12	3	·	23	
Rok	13	0.8	8	1.0	45	2.0	39	2.7	270.5	2.6	37.5	3.1	83	1.9	25	1.6	574	1.2	686.9	34.6	12.VIII	18	28	78	34	·	·	46	120	131	102	21	19	44	21

Limanowa — φ = 49°42' — λ = 20°25' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	2.2	-10.9	8.2	4	-24.4	26	-6.4	-4.2	-5.7	-4.8	3.8	4.2	3.9	4.0	88	73	87	83	0.5	1.7	0.6	0.9	7.2	6.3	6.1	6.5
II	–	–	–	–	4.7	-2.9	14.4	18	-13.3	6	-1.4	3.2	0.0	0.4	5.1	6.0	5.6	5.6	91	78	90	86	0.5	1.9	0.6	1.0	7.9	7.2	7.0	7.4
III	–	–	–	–	9.2	0.9	19.4	18	-7.1	23	2.8	7.5	4.3	4.7	6.3	6.6	6.7	6.5	83	65	81	76	1.4	4.2	1.8	2.5	9.1	8.1	7.1	8.1
IV	–	–	–	–	16.8	2.5	25.0	15	-4.7	10	8.0	15.4	8.1	9.9	8.4	8.7	8.8	8.6	77	50	81	69	2.6	9.4	2.1	4.7	6.2	6.2	5.4	5.9
V	–	–	–	–	15.9	4.5	24.2	6	-0.5	15	9.1	14.0	7.9	9.7	10.4	10.3	10.4	10.4	89	65	95	83	1.4	6.3	0.5	2.7	8.4	8.8	7.5	8.2
VI	–	–	–	–	22.9	9.1	31.6	27	3.7	21	15.3	20.3	13.6	15.7	14.7	14.5	14.8	14.7	84	62	94	80	2.8	10.2	0.9	4.6	5.9	8.0	7.5	7.1
VII	–	–	–	–	21.1	8.2	29.4	3	3.2	6	14.4	19.2	12.5	14.6	13.4	13.0	13.5	13.3	81	60	92	78	3.3	10.2	1.2	4.9	6.5	7.9	7.2	7.2
VIII	–	–	–	–	22.2	9.3	33.3	11	3.2	31	13.7	20.8	13.5	15.4	14.2	15.0	14.4	14.5	89	60	92	80	1.9	10.7	1.4	4.7	6.3	7.5	6.3	6.7
IX	–	–	–	–	21.6	6.0	29.9	17	-1.8	22	9.5	20.4	9.9	12.4	11.3	12.7	11.6	11.8	93	54	93	80	1.0	12.2	1.0	4.7	5.3	5.1	4.3	4.9
X	–	–	–	–	16.4	4.2	21.3	11,20	-1.3	22	6.5	15.7	7.7	9.4	8.8	10.4	9.3	9.5	90	59	89	79	1.2	7.9	1.4	3.5	6.5	5.9	5.1	5.8
XI	–	–	–	–	7.7	-0.2	17.0	3	-9.7	21	1.8	6.7	2.6	3.4	6.6	7.5	6.9	7.0	91	76	90	86	0.6	2.7	0.8	1.4	8.2	7.4	7.4	7.7
XII	–	–	–	–	0.4	-9.9	17.2	5	-30.1	24	-5.3	-1.5	-4.5	-4.0	4.3	5.1	4.4	4.6	86	81	85	84	1.0	1.3	0.9	1.1	8.0	7.7	7.4	7.7
Rok	–	–	–	–	13.4	1.7	33.3	11.VIII	-30.1	24.XII	5.7	11.7	5.8	7.2	8.9	9.5	9.2	9.2	87	65	89	80	1.5	6.6	1.1	3.1	7.1	7.2	6.5	6.9

Żywiec - Sporysz — φ = 49°41' — λ = 19°13'

I	–	–	–	–	1.2	-6.6	11.7	4	-17.9	27	-4.1	0.2	-2.9	-2.4	3.9	4.3	4.1	4.1	80	67	78	75	1.0	2.1	1.2	1.4	6.0	5.6	5.0	5.5
II	–	–	–	–	5.1	-2.0	13.8	18	-16.0	6	-0.7	4.2	0.9	1.3	5.3	6.2	5.7	5.7	89	75	87	84	0.7	2.2	0.9	1.3	6.8	5.8	6.1	6.2
III	–	–	–	–	9.8	1.5	20.5	10	-5.7	23	3.3	8.0	5.1	5.4	6.6	6.5	7.0	6.7	85	63	80	76	1.3	4.7	2.1	2.7	8.0	7.2	6.3	7.2
IV	–	–	–	–	17.7	4.6	25.1	7	-2.6	10	7.8	16.8	10.0	11.2	8.6	8.7	9.7	9.0	80	47	79	69	2.2	11.1	2.7	5.3	5.1	5.6	4.2	5.0
V	–	–	–	–	16.8	6.5	25.3	27	2.1	15	9.4	15.3	10.2	11.3	10.0	9.9	10.6	10.2	84	58	84	75	1.9	8.3	2.1	4.1	7.0	7.8	6.8	7.2
VI	–	–	–	–	23.2	10.5	31.2	27	5.6	21	14.8	20.9	15.2	16.5	14.2	14.6	15.2	14.7	84	60	87	77	4.9	6.5	5.3	5.6	4.9	6.5	5.3	5.6
VII	–	–	–	–	21.4	10.4	30.9	3	4.8	8	14.2	19.4	14.5	15.6	13.2	13.7	14.2	13.7	81	62	86	76	3.3	9.8	2.5	5.2	5.5	7.0	6.1	6.2
VIII	–	–	–	–	22.5	10.9	32.7	10	5.6	14	13.9	21.2	14.8	16.2	13.9	14.8	14.9	14.5	87	59	87	78	2.2	11.3	2.2	5.2	5.8	6.6	4.5	5.6
IX	–	–	–	–	22.2	7.4	29.6	17	-0.4	23	9.9	21.2	12.8	14.2	11.2	13.5	12.8	12.5	90	55	86	77	1.5	12.1	2.3	5.3	4.2	4.1	3.2	3.8
X	–	–	–	–	17.2	5.1	22.7	8	-0.5	11	6.9	16.5	9.5	10.6	9.1	10.2	9.8	9.7	91	55	83	76	1.1	8.9	2.3	4.1	6.8	6.3	4.6	5.9
XI	–	–	–	–	7.9	0.5	14.2	12,27	-7.5	21	2.5	7.0	3.5	4.1	6.6	7.1	6.9	6.9	88	71	86	82	1.0	3.2	1.2	1.8	8.2	7.7	7.1	7.7
XII	–	–	–	–	-0.1	-8.4	15.8	5	-31.0	25	-5.5	-1.5	-4.2	-3.8	4.4	4.9	4.5	4.6	84	80	85	83	0.8	1.5	0.8	1.0	7.3	6.8	6.8	7.0
Rok	–	–	–	–	13.7	3.4	32.7	10.VIII	-31.0	25.XII	6.0	12.4	7.4	8.3	8.9	9.5	9.6	9.3	85	63	84	77	1.8	6.8	2.1	3.6	6.3	6.4	5.5	6.1

Krosno — φ = 49°41' — λ = 21°45'

I	–	–	–	–	-1.2	-8.4	9.5	4	-25.4	27	-4.7	-2.9	-4.5	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.4	6.5	6.9
II	–	–	–	–	3.1	-1.8	9.5	18	-5.5	4,5,6	-0.3	2.5	0.6	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.2	7.3	7.7
III	–	–	–	–	9.5	1.6	17.3	10	-5.6	23	3.6	7.6	5.4	5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.3	6.9	7.2
IV	–	–	–	–	16.9	4.2	23.6	7	-4.5	10	7.2	15.5	10.7	11.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.5	4.7	4.6
V	–	–	–	–	16.7	5.9	23.7	29	1.1	20	9.0	14.9	10.8	11.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	7.6	7.4
VI	–	–	–	–	23.6	11.0	30.8	27	5.5	17,21,29	15.1	21.3	18.2	18.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.3	5.5	4.9
VII	–	–	–	–	22.1	10.5	30.3	4	4.4	7	14.2	20.4	16.4	16.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.2	6.7	5.6
VIII	–	–	–	–	22.8	11.1	32.8	11	4.9	31	13.8	21.3	17.1	17.3	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.5	6.7	5.3
IX	–	–	–	–	20.7	7.7	27.7	2,17,18	-2.3	23	9.8	19.7	14.0	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	3.8	4.6	4.3
X	–	–	–	–	16.1	-5.8	24.0	20	0.6	23	8.1	15.0	10.7	11.1	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.3	3.8	4.3
XI	–	–	–	–	7.5	1.5	15.8	7	-7.4	21	3.7	6.2	4.3	4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.3	6.7	7.3
XII	–	–	–	–	-0.4	-8.6	11.6	5	-29.4	26	-4.3	-2.5	-3.5	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.4	7.3	7.7
Rok	–	–	–	–	13.1	3.4	32.8	11.VIII	-29.4	26.XII	6.3	11.6	8.4	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	6.2	6.1

Bircza — φ = 49°41' — λ = 22°29'

I	–	–	–	–	-0.4	-8.8	10.5	4	-25.6	27	-5.5	-1.3	-4.6	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.4	4.0	5.4
II	–	–	–	–	3.2	-1.6	10.3	18	-7.7	15	-0.5	2.7	0.6	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	6.5	7.1
III	–	–	–	–	9.0	1.6	16.7	18	-5.2	23	3.8	7.4	4.9	5.2	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.6	5.7	7.1
IV	–	–	–	–	16.4	3.7	23.8	8,15	-4.6	10	7.0	15.2	9.6	10.4	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.3	3.4	4.5
V	–	–	–	–	16.4	5.5	23.8	29	-0.2	17	9.6	14.6	10.0	11.0	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.8	5.8	6.6
VI	–	–	–	–	23.1	10.3	30.4	27	4.7	29	15.5	21.0	15.7	17.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.5	5.5	5.2
VII	–	–	–	–	22.2	9.8	30.4	4	4.1	7	14.5	20.6	14.7	16.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.9	5.6	5.7
VIII	–	–	–	–	22.5	10.9	32.9	11	3.8	31	14.5	21.1	15.8	16.8	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.2	5.4	5.2
IX	–	–	–	–	20.8	7.5	29.4	17,18	-3.0	23	10.5	19.8	12.8	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.7	3.4	4.2
X	–	–	–	–	16.2	4.6	23.8	19	-0.7	12	7.0	15.5	9.8	10.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	4.1	4.2	4.7
XI	–	–	–	–	8.2	2.2	14.4	3	-5.6	21	4.3	7.2	4.9	5.3	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.5	7.0	7.5
XII	–	–	–	–	0.3	-7.6	15.9	5	-27.7	25	-3.9	-1.2	-3.2	-2.9	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.4	5.6	7.0
Rok	–	–	–	–	13.2	3.2	32.9	11.VIII	-27.7	25.XII	6.4	11.9	7.6	8.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.0	5.2	5.8

Limanowa

$H_s = 440\ m$ — $h_w = 16\ m$

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} — N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R — Suma	Max	Data	LICZBA DNI (n) — Temperatura T: Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v: ≥ 10	> 15	◔	●	Opad R: ≥ 0.1	≥ 1.0	≥ 10.0	═	⊞	⊓
I	3.5	2.4	1.5	2.0	3.5	2.7	36	3.0	14.5	2.4	2	3.7	10	3.6	13	2.8	9	2.6	16.2	6.2	5	16	14	29	·	·		4	11	12	5	·	2	30	·
II	2	2.8	2	3.0	5	4.2	20.5	3.2	7	2.2	9.5	2.1	13	3.4	20	3.2	1.5	3.0	34.5	13.5	9	1	1	23	·	1	·	2	15	13	9	1	4	10	·
III	5	3.5	·	·	1	3.0	0.5	3.0	4	2.2	4.5	4.2	34.5	5.1	40.5	4.6	3	4.5	42.5	6.9	14	·	·	11	·	5	·	1	17	18	14	·	·	4	·
IV	7	2.1	4	2.2	7.5	2.7	28.5	2.9	7.5	3.0	4.5	2.4	13	3.8	9	3.4	9	2.7	49.0	7.4	8	·	·	5	·	1	·	5	7	7	5	·	·	·	3
V	10	2.8	1	3.0	3.5	3.0	9.5	2.9	1.5	2.0	6	2.6	11.5	3.0	32	2.9	18	2.3	118.7	25.2	28	·	·	2	·	1	·	·	19	19	15	3	2	·	7
VI	3.5	2.6	2.5	1.8	6	3.2	17	2.8	9.5	3.3	5	2.7	7	3.4	21.5	2.9	18	2.4	112.0	27.2	11	·	·	·	7	·	·	·	12	16	14	3	1	·	12
VII	9	2.5	1	3.0	1.5	3.0	7	3.4	4	2.1	3	2.5	11.5	3.0	36	2.8	20	2.2	102.4	29.6	29	·	·	·	8	·	·	3	15	16	12	2	·	·	2
VIII	5.5	2.3	1	3.0	2.5	2.8	10.5	2.4	2	2.8	3.5	2.0	13	3.3	37	2.8	18	2.2	58.9	17.7	12	·	·	·	9	·	·	1	11	9	8	3	1	·	5
IX	3	2.2	2	2.0	7	2.3	17	2.1	4	1.9	3	2.5	10	2.8	22	2.9	22	1.9	33.5	15.4	29	·	·	2	7	·	·	10	8	10	5	1	2	·	4
X	1	3.0	2	1.0	8	2.8	38	3.5	9.5	4.3	5.5	2.2	6	2.0	12	2.4	11	2.8	29.1	14.4	30	·	·	2	·	·	·	5	9	8	5	1	3	·	·
XI	1	2.0	1.5	2.3	3	3.0	23	2.7	7.5	2.3	9	2.5	10.5	3.5	26.5	2.8	8	2.5	67.7	25.7	4	·	·	14	·		·	1	16	17	8	1	8	5	·
XII	3.5	3.6	4	1.8	5.5	3.5	20	2.9	2.5	2.2	7.5	3.1	15	5.2	30	4.1	5	3.5	88.9	22.2	6	15	17	26	·	4	·	1	13	16	11	4	2	24	·
Rok	54	2.6	22.5	2.1	54	3.0	227.5	2.9	73.5	2.6	63	2.7	155	3.5	299.5	3.1	146	2.7	723.4	29.6	29.VII	32	32	114	31	12	·	33	153	161	111	19	25	73	33

Żywiec - Sporysz

$H_s = 360\ m$ — $h_w = 20{,}6\ m$

I	4.5	1.3	8.5	1.6	5.5	1.4	8.5	1.5	12.5	3.6	17.5	4.3	2	1.2	4	1.4	33	1.8	25.1	15.5	4	9	11	27	·	2	·	7	11	8	5	1	1	13	:
II	0.5	1.0	·	·	3	1.2	4	1.1	9	1.9	14	4.4	7.5	1.4	4	1.5	42	1.2	55.4	42.2	9	1	1	20	·	·	·	6	15	15	11	2	9	11	·
III	1	3.5	1	1.0	4	1.2	·	·	5.5	2.0	25.5	2.3	18.5	2.1	13.5	2.5	24	1.6	80.3	18.6	14	·	·	8	·	·	·	1	16	19	14	2	1	5	1
IV	1.5	1.0	8	2.1	7.5	1.9	3	1.8	6	2.2	9	2.3	2	2.5	5	2.0	48	1.0	76.7	55.6	18	·	·	1	1	·	·	8	3	11	8	1	3	·	2
V	5.5	1.0	2.5	2.2	2	1.5	1.5	1.3	3	1.3	12.5	2.3	9	1.9	11	1.8	46	0.9	98.7	28.6	6	·	·	·	1	1	1	1	10	17	13	5	·	·	8
VI	2	1.0	2.5	1.0	3	1.0	4.5	1.0	3	1.2	6	1.7	4.5	1.3	10.5	1.7	54	0.5	157.2	33.8	27	·	·	·	8	·	·	3	7	15	13	6	·	·	12
VII	2.5	1.4	·	·	2	1.0	4.5	1.0	7.5	1.8	15	2.0	7.5	1.7	7	1.4	47	0.8	159.7	37.5	28	·	·	·	8	1	1	3	11	14	11	8	·	·	6
VIII	1	2.0	2	1.0	2	1.0	1	1.0	5.5	2.2	20.5	2.0	9.5	1.8	7.5	1.7	44	1.0	68.8	26.0	12	·	·	·	9	·	·	4	8	11	5	3	2	·	4
IX	1	1.0	1.5	2.3	3	2.0	3.5	1.0	9	1.4	11.5	2.0	6	2.1	3.5	2.4	51	0.8	11.4	5.8	14	·	·	2	8	·	·	12	4	10	3	·	4	·	2
X	·	·	3	2.0	8.5	1.8	9	2.3	8	2.1	8	1.8	4.5	1.8	4	1.8	48	1.0	16.2	9.6	30	·	·	1	·	·	·	4	7	10	3	·	3	·	·
XI	0.5	1.0	·	·	1	1.0	7	1.4	7	1.5	14.5	2.7	4	2.1	6	1.4	50	0.9	71.5	32.5	4	·	·	7	·	1	·	1	16	14	9	2	5	7	·
XII	2.5	1.0	6	1.7	1.5	1.3	4	2.2	9	3.2	12.5	4.7	5.5	2.6	6	2.3	46	1.5	95.2	38.3	6	12	16	26	·	1	·	1	15	14	12	3	1	23	·
Rok	19.5	1.3	35	1.2	43	1.4	50.5	1.3	85	2.0	166.5	2.7	80.5	1.9	82	1.8	533	1.1	916.2	55.6	18.IV	22	28	92	35	6	2	51	123	158	107	33	29	59	35

Krosno

$H_s = 282\ m$ — $h_w = 15\ m$

I	5	2.2	1	1.0	4	1.8	10	5.2	41	7.5	7	3.7	16	3.9	2	5.5	7	5.2	12.8	3.7	14	10	16	28	·	7	1	2	12	9	4	·	3	23	–
II	4	1.2	0.5	2.0	3	1.3	14.5	5.2	24.5	6.1	2	4.5	15.5	3.2	2	2.2	18	3.5	11.0	4.5	10	·	1	21	·	4	·	·	17	11	3	·	6	5	–
III	0.5	5.0	·	·	3	1.7	4.5	6.2	6.5	8.3	5	3.4	48	4.6	13.5	4.9	12	4.2	26.4	4.6	31	·	·	9	·	6	·	1	13	18	9	·	2	1	–
IV	2	2.5	9.5	3.0	48.5	3.9	11.5	3.0	12.5	5.0	3	3.7	19	3.5	2	3.0	12	3.2	21.9	8.7	8	·	·	2	·	·	·	7	5	7	6	·	·	·	–
V	11.5	2.7	5	2.6	10.5	2.4	3.5	2.3	14	4.6	2.5	2.4	13.5	3.9	15.5	3.4	17	2.7	98.5	23.7	29	·	·	·	·		·	·	14	16	12	4	1	·	–
VI	1	4.0	6	3.5	5	2.0	8.5	2.7	8.5	3.6	3	2.3	25	2.3	7	2.4	26	1.9	77.5	21.0	27	·	·	·	7	·	·	4	5	13	11	2	1	·	–
VII	4	2.5	2	2.5	1	2.0	8	2.9	18	4.4	1.5	5.0	27	2.9	13.5	4.0	18	2.8	102.0	37.9	29		·	·	8	3	1	3	5	16	10	3	1	·	–
VIII	6	1.2	2	3.5	3	2.7	5.5	4.3	22.5	4.4	5	3.0	10	2.4	19	4.1	20	2.8	86.5	37.9	12	·	·	·	7	2	·	4	5	14	12	2	2	·	–
IX	5.5	2.7	5	3.6	18	2.5	7	3.0	22	4.2	5	2.2	3	5.0	10.5	4.8	14	3.0	32.3	9.5	7	·	·	2	6	·	·	11	6	12	8	·	5	·	–
X	3	2.8	5.5	3.5	11.5	3.7	18	4.0	25	5.1	·	·	5	1.8	9	4.2	46	3.4	32.0	18.8	30	·	·	·		2	·	11	5	6	6	1	3	·	–
XI	5	3.9	1	3.0	5	3.4	16	5.1	29.5	5.0	0.5	2.0	13.5	4.4	8.5	4.6	11	4.1	43.7	10.3	7	·	·	8	·	1	·	1	14	14	10	1	5	1	–
XII	11	4.4	·	·	5	2.0	4.5	6.0	25.5	10.0	3	1.7	24	4.0	9	5.6	11	5.3	40.0	15.5	11	13	14	23	·	8	3	1	17	13	6	1	4	25	–
Rok	58.5	2.9	37.5	2.4	87.5	2.4	111.5	4.2	249.5	5.7	37.5	2.8	219.5	3.5	111.5	4.1	182	3.5	584.6	37.9	29.VII, 12.VIII	23	31	93	28	33	5	45	118	149	97	14	33	55	–

Bircza

$H_s = 300\ m$ — $h_w = 16\ m$

I	3.5	2.4	2	4.0	3.5	2.4	1.5	2.3	6.5	3.9	28.5	3.5	12.5	3.5	6	2.8	29	2.3	20.1	6.2	31	11	13	29	·	2	·	4	8	8	5	·	·	23	–
II	·	·	0.5	1.0	5.5	2.6	2.5	2.6	6	4.2	18	3.5	21	3.5	4.5	1.8	26	2.3	18.1	8.3	13		1	17	·	1	·	3	12	8	4	·	1	5	–
III	2.5	2.6	·	·	·	·		·	2.5	6.2	15	4.2	40.5	4.8	17.5	4.2	15	3.8	28.5	6.1	31		·	8	·	3	·	1	11	11	10	·	·	2	–
IV	3	4.0	3	3.3	16.5	8.3	8.5	4.8	5	1.7	12.5	4.6	9.5	5.1	4	3.2	28	3.6	13.1	4.5	8		·	5		8	2	4	7	6	6		·	·	–
V	4.5	3.0	5.5	1.9	6.5	2.3	3.5	3.4	5.5	2.1	9.5	3.3	12.5	3.5	13.5	2.4	32	1.8	62.0	18.7	7	·	·	1	·	·	·	·	9	14	11	2	2	·	–
VI	4	2.4	2	1.0	8.5	3.5	2	2.0	7	2.0	10	2.6	11.5	3.0	12	1.8	33	1.6	88.4	14.9	12	·	·	·	5	·	·	3	4	14	12	3	3	·	–
VII	5	1.2	·	·	·	·	·	·	4	1.2	18	3.4	22.5	3.1	18.5	2.1	25	2.0	89.6	28.8	29	·	·	·	8	·	·	2	6	13	13	3	·	·	–
VIII	6	1.8	1	2.0	3	4.3	·	·	5	3.7	11	2.8	17.5	4.0	11.5	2.7	38	1.9	40.1	16.8	12	·	·	·	7	·	·	3	4	13	7	1	4	·	–
IX	1.5	2.3	1	4.0	9.5	4.1	0.5	6.0	2.5	5.0	11.5	3.7	26	3.3	3.5	1.6	34	2.2	16.7	4.3	27	·	·	2	7	·	·	11	5	6	6	·	3	·	–
X	1.5	1.7	4.5	2.8	17	5.8	15	4.1	10.5	4.0	10	3.6	8.5	2.0	6	2.6	20	3.1	23.1	14.2	30	·	·	1	·	4	·	9	5	5	3	1	2	·	–
XI	1	2.0	0.5	7.0	4.5	5.4	10	3.6	7	4.1	22.5	2.7	19.5	3.9	10	3.8	15	3.0	22.1	6.5	11	·	·	10	·	·	·	2	14	9	7	·	·	·	–
XII	7	3.0	3	4.0	4.5	4.0	0.5	3.0	12.5	4.8	17.5	4.9	14	4.0	8	4.0	26	3.1	67.2	20.9	11	11	14	24	·	2	·	1	14	14	10	2	·	25	–
Rok	39.5	2.2	23	2.6	79	3.6	44	2.6	74	3.6	184	3.6	216.5	3.6	115	2.8	321	2.6	489.0	28.8	29.VII	22	28	97	27	20	2	43	99	121	94	12	15	55	–

Mszana Dolna

$\varphi = 49°40'$ $\lambda = 20°05'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.3	-8.7	9.9	4	-21.3	18	-6.1	-0.5	-4.9	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.5	5.8	5.9
II	–	–	–	–	4.5	-2.5	12.4	18	-13.3	6	-1.3	3.6	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.4	7.0	6.9
III	–	–	–	–	8.8	1.2	19.3	10	-5.2	23	2.8	7.8	4.2	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	6.8	7.7
IV	–	–	–	–	16.9	3.5	24.6	15	-3.5	10	7.3	16.2	9.3	10.5	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.2	4.6	5.2
V	–	–	–	–	16.0	5.8	23.4	27	0.7	15	9.0	14.7	9.2	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.8	8.2	8.2
VI	–	–	–	–	22.6	9.9	31.2	27	4.1	21	14.8	20.6	14.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	7.7	7.0	6.5
VII	–	–	–	–	20.9	9.1	30.0	3	4.5	25,26	13.7	19.4	13.5	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.4	7.2	6.8
VIII	–	–	–	–	21.9	10.2	32.2	11	3.6	31	13.4	20.6	14.8	15.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.2	5.1	5.6
IX	–	–	–	–	21.4	6.7	29.9	17	-3.0	23	9.4	20.7	11.4	13.2	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.9	4.2	4.6
X	–	–	–	–	16.8	4.2	21.5	8,11	-1.5	22	6.2	16.0	8.9	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	4.5	5.4
XI	–	–	–	–	8.2	0.2	14.9	7	-7.4	21,22	2.0	7.1	2.8	3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.1	7.6	7.6
XII	–	–	–	–	-0.4	-10.0	16.9	5	-33.2	25	-6.5	-2.1	-5.5	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.9	6.9	7.1
Rok	–	–	–	–	13.2	2.5	32.2	11.VIII	-33.2	25.XII	5.4	12.0	6.6	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	6.2	6.4

Wisła

$\varphi = 49°39'$ $\lambda = 18°52'$

I	–	–	–	–	0.1	-6.4	9.0	4	-18.7	26	-4.8	-0.9	-3.4	-3.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.1	5.2	5.7
II	–	–	–	–	3.9	-2.5	10.7	18	-17.4	6	-1.1	3.3	0.2	0.6	5.3	6.4	5.7	5.8	9.1	8.3	9.2	8.9	0.5	1.4	0.5	0.8	7.0	6.4	6.5	6.6
III	–	–	–	–	8.9	0.5	19.4	10	-7.0	23	2.1	7.6	3.9	4.4	6.5	7.2	7.0	6.9	9.1	7.1	8.6	8.3	0.8	3.7	1.3	1.9	7.9	5.8	7.0	6.9
IV	–	–	–	–	16.7	4.0	24.0	7	-3.1	10	8.0	15.7	8.8	10.3	8.8	10.0	9.5	9.4	8.1	5.6	8.4	7.4	2.2	8.5	2.0	4.2	4.0	5.0	4.1	4.4
V	–	–	–	–	15.3	5.5	22.9	27	2.0	15	8.9	14.1	9.2	10.4	9.8	10.3	10.4	10.2	8.6	6.5	8.9	8.0	1.9	6.4	1.4	3.2	7.2	7.5	7.6	7.4
VI	–	–	–	–	21.7	10.3	29.0	25,27	5.2	21	14.5	19.6	14.9	16.0	13.9	14.6	15.0	14.5	8.4	6.5	8.8	7.9	2.9	8.9	2.2	4.7	4.2	6.2	5.6	5.3
VII	–	–	–	–	20.4	9.6	29.0	3	4.5	8	13.5	19.1	14.1	15.2	12.7	14.4	13.8	13.6	8.2	6.6	8.5	7.8	3.1	8.4	2.5	4.7	4.9	6.8	5.5	5.7
VIII	–	–	–	–	21.0	10.7	31.8	10	4.6	14	13.2	20.1	14.5	15.6	13.2	14.6	14.8	14.2	8.6	6.2	8.8	7.9	2.4	10.0	2.1	4.8	4.9	6.0	5.5	5.5
IX	–	–	–	–	21.1	7.3	27.6	18	0.8	22	9.8	20.2	12.6	13.8	11.1	13.7	13.3	12.7	9.0	5.8	9.0	7.9	1.4	10.7	1.6	4.6	3.0	4.4	3.4	3.6
X	–	–	–	–	16.0	5.3	21.4	8	0.7	10,22	7.2	15.4	8.4	9.8	9.2	11.0	9.9	10.0	9.0	6.3	8.9	8.1	1.3	6.8	1.3	3.1	5.8	5.4	4.4	5.2
XI	–	–	–	–	7.2	0.8	13.7	12	-7.1	21	2.7	6.5	2.9	3.8	6.9	7.6	7.0	7.2	9.1	7.9	9.2	8.7	0.8	2.4	0.6	1.3	7.5	7.1	6.8	7.1
XII	–	–	–	–	-0.5	-8.3	14.7	5	-27.8	25	-5.0	-2.0	-4.3	-3.9	4.7	5.2	4.6	4.6	8.5	8.5	8.5	8.5	0.5	1.1	0.7	0.8	7.2	6.8	6.8	6.9
Rok	–	–	–	–	12.6	3.1	31.8	10.VIII	-27.8	25.XII	5.8	11.6	6.8	7.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.1	5.7	5.9

Lubań Wielki

$\varphi = 49°39'$ $\lambda = 19°59'$

I	–	–	–	–	-3.0	-8.0	5.2	4	-18.8	18	-6.2	-4.5	-5.7	-5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.3	6.1	6.6
II	–	–	–	–	1.2	-3.9	11.0	18	-10.8	6	-2.6	0.0	-1.9	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	6.4	6.6
III	–	–	–	–	3.9	-1.7	15.3	18	-8.9	23	-0.6	2.3	0.9	0.9	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.5	7.8	8.5
IV	–	–	–	–	12.4	3.7	20.9	15	-3.6	1	5.8	11.3	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.6	5.5	6.2
V	–	–	–	–	11.5	4.2	19.7	6	-2.2	12	6.1	9.5	6.6	7.2	–	–	–	–	–	–	–	–	–	–	–	–	8.3	8.7	8.5	8.5
VI	–	–	–	–	18.3	10.0	27.3	27	5.5	29	12.9	16.4	12.9	13.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	8.3	7.5	7.3
VII	–	–	–	–	16.5	8.8	26.3	4	4.9	6	11.2	14.4	11.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	8.2	8.1	7.7
VIII	–	–	–	–	17.0	9.3	27.8	11	4.9	17	11.2	15.6	12.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.4	6.3	7.4
IX	–	–	–	–	16.8	9.1	25.0	18	3.9	12	10.9	15.6	11.9	12.6	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.0	4.2	5.0
X	–	–	–	–	12.2	5.7	17.2	8	2.2	14	7.0	11.2	7.8	8.4	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.8	5.4	6.5
XI	–	–	–	–	4.8	-0.8	10.3	3,7	-9.3	21	1.2	3.3	1.6	1.9	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.6	7.8	8.2
XII	–	–	–	–	-2.7	-8.7	12.6	5	-21.9	16	-5.9	-4.8	-5.9	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.1	7.3	7.7
Rok	–	–	–	–	9.1	2.3	27.8	11.VIII	-21.9	16.XII	4.2	7.5	4.9	5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.6	6.7	7.2

Zawoja

$\varphi = 49°37'$ $\lambda = 19°31'$

I	–	–	–	–	0.0	-7.7	8.2	4	-20.0	18	-4.7	-1.7	-4.2	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.5	4.7	5.3
II	–	–	–	–	4.1	-3.6	13.1	18	-13.1	6	-1.7	2.9	-0.4	0.1	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.7	6.1	5.7
III	–	–	–	–	7.2	-0.3	16.9	10	-7.7	23	2.0	5.1	3.5	3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.2	7.2	7.5
IV	–	–	–	–	14.7	3.9	21.9	7	-4.1	10	8.3	13.4	8.3	9.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.0	4.1	4.9
V	–	–	–	–	13.7	4.5	20.9	27	-0.8	13	8.5	12.0	8.1	9.2	–	–	–	–	–	–	–	–	–	–	–	–	6.5	7.2	7.8	7.2
VI	–	–	–	–	20.4	9.6	27.7	27	4.5	16	14.9	18.3	13.9	15.2	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.5	5.7	5.7
VII	–	–	–	–	18.7	8.9	27.0	3	4.0	8	13.8	17.2	12.8	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.0	5.9	5.8
VIII	–	–	–	–	19.6	10.0	29.2	11	3.8	14	13.9	18.5	13.7	15.0	–	–	–	–	–	–	–	–	–	–	–	–	4.7	6.2	5.4	5.4
IX	–	–	–	–	19.6	8.0	27.7	17	1.3	22	11.7	17.9	11.8	13.3	–	–	–	–	–	–	–	–	–	–	–	–	3.4	4.2	4.0	3.9
X	–	–	–	–	14.8	5.5	19.7	11	0.3	16,22	8.7	13.4	8.7	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.7	4.4	5.3
XI	–	–	–	–	6.9	-0.4	12.7	3	-10.7	21	2.4	5.4	2.4	3.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.9	7.2	7.0
XII	–	–	–	–	-0.1	-7.8	17.4	5	-21.2	17	-4.4	-2.4	-4.1	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	6.9	6.7
Rok	–	–	–	–	11.6	2.6	29.2	11.VIII	-21.2	17.XII	6.1	10.0	6.2	7.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.1	5.8	5.9

Uwaga. W ciągu całego roku obserwacje w III terminie dokonywano o 1 godzinę za wcześnie.

Mszana Dolna

$H_s = 410\ m$ $h_w = 16\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min<-10°	Max<0°	Min<0°	Max>25°	Wiatr v≥10	v≥15	Opad R ≥0.1	≥1.0	≥10.0	≥1	≥5	≥10
I	5.5	1.8	4	2.6	2.5	1.8	2	2.0	6.5	3.8	16.5	3.5	2	2.5	7	1.6	4.7	1.4	171	5.5	5	10	12	28	·	2	·	6	10	8	5	·	·	31
II	4	2.5	0.5	1.0	1.5	1.3	1.5	1.7	5.5	2.9	8.5	2.8	1.2	1.9	8.5	1.9	4.2	1.1	384	110	9	1	1	19	·	·	·	5	15	14	9	1	2	10
III	6.5	4.7	·	·	·	·	1	1.0	2.5	4.4	22.5	3.8	4.9	3.3	17.5	4.3	2.4	2.9	567	89	14	·	·	7	·	1	1	2	18	21	16	·	1	5	·
IV	1.2	2.2	6.5	3.5	8	3.4	1.5	2.3	3.5	2.0	11.5	3.3	5.5	4.0	7.5	2.8	3.4	1.9	131	41	8	·	·	3	·	·	·	7	8	6	5	·	·	·	2
V	6.5	1.7	3	2.7	0.5	5.0	0.5	5.0	3	3.2	5.5	2.5	1.0	2.8	1.6	2.6	4.8	1.3	1375	364	6	·	·	·	·	·	·	·	21	20	18	4	·	·	3
VI	4	3.0	1	1.0	3.5	2.0	2	2.5	1.5	2.3	5	2.4	7	2.2	1.6	1.9	5.0	1.0	1342	278	6	·	·	·	7	·	·	1	12	15	12	6	·	·	8
VII	6.5	1.2	1	2.0	0.5	3.0	0.5	2.0	2.5	2.2	8	2.9	1.3	2.8	2.1	1.7	4.0	1.2	1384	342	29	·	·	·	8	1	·	3	12	15	11	5	·	·	4
VIII	5	1.8	2.5	2.0	1	1.5	·	·	4	2.4	9.5	2.3	1.4.5	2.0	1.8.5	2.1	3.8	1.2	662	212	12	·	·	·	7	·	·	5	9	9	7	3	1	·	4
IX	7	1.4	3.5	1.9	1.5	1.7	1	2.0	3.5	2.9	7	3.4	7.5	2.7	1.4	2.4	4.5	1.2	276	109	29	·	·	2	7	·	·	12	6	9	5	1	·	·	1
X	4	1.9	4	4.4	6.5	4.0	6	3.7	5	2.6	11	3.1	7	2.7	10.5	2.2	3.9	1.7	301	166	30	·	·	2	·	·	·	6	7	5	5	1	·	·	·
XI	3.5	2.4	1.5	1.0	2.5	2.0	4.5	2.2	3.5	1.7	11.5	3.0	3	3.3	1.6	1.9	4.4	1.2	629	203	4	·	·	11	·	·	·	2	16	13	12	2	1	6	·
XII	5.5	1.9	3	2.3	3	2.0	3	1.7	4.5	5.0	1.4	4.4	4.5	5.0	1.4.5	2.5	4.1	1.8	1051	351	11	1.4	1.6	2.7	·	·	·	4	1.5	1.4	11	3	·	2.5	·
Rok	7.0	2.2	3.0.5	2.0	3.1	2.3	2.3.5	2.2	4.5.5	3.0	1.3.0.5	3.1	1.0.5	2.9	1.6.7	2.3	4.9.2	1.5	8273	364	6.V	2.5	2.9	9.9	2.9	4	1	5.3	1.4.9	1.4.9	1.1.6	2.6	5	7.7	2.2

Wisła

$H_s = 430\ m$ $h_w = 14{,}5\ m$

I	4	1.8	2	1.5	2	1.0	1.5.5	2.8	3.8.5	2.9	·	·	2	2.0	2.2	2.0	7	2.3	281	200	4	1.0	1.4	2.5	·	·	·	8	1.2	1.1	6	1	1	3.0	·
II	1.1	1.5	·	·	·	·	1.8.5	2.4	2.5.5	2.5	·	·	·	·	2.0	1.9	9	1.9	961	196	9	1	·	2.4	·	·	·	5	1.5	1.4	1.4	3	5	2.0	·
III	7	2.1	·	·	1	1.0	1.2	1.4	2.1	2.5	·	·	8	2.1	4.0	2.6	4	2.2	1186	183	30	·	·	1.3	·	·	·	3	1.6	1.9	1.8	3	2	9	·
IV	9.5	1.6	·	·	4	1.2	9.5	1.8	4.5.5	2.1	·	·	3	2.0	1.3.5	2.5	5	1.9	649	172	18	·	·	2	·	·	·	10	6	1.0	1.0	3	·	·	2
V	9.5	2.0	3	1.7	3	1.7	6	1.8	2.7	2.4	·	·	0.5	2.0	3.9	2.4	5	2.2	1195	230	6	·	·	·	·	·	·	1	1.8	2.0	1.7	5	3	·	4
VI	3	2.3	·	·	6	1.2	9	1.6	3.6	2.3	·	·	1	1.0	3.1	2.1	4	2.0	2074	510	27	·	·	·	4	·	·	7	7	1.5	1.4	7	3	·	1.0
VII	9.5	1.9	·	·	5	1.8	9	1.6	2.7	2.3	·	·	9	2.0	2.9.5	2.2	4	2.0	1637	320	13	·	·	·	8	1	·	4	7	1.7	1.4	7	·	·	5
VIII	1.3	1.5	·	·	6	1.0	4	1.8	3.1	2.3	·	·	6	1.8	2.8	1.9	5	1.8	829	250	13	·	·	·	5	·	·	6	1.1	1.5	9	3	·	·	3
IX	6.5	2.0	2	1.5	1.0	1.1	9.5	1.4	3.3	2.2	0.5	1.0	3	3.3	1.9.5	2.1	6	1.8	163	5.0	1.4	·	·	·	5	·	·	1.6	7	9	5	·	·	·	1
X	5.5	1.8	1	3.0	9	1.0	1.4.5	2.0	4.2	2.9	0.5	3.0	·	·	1.6.5	2.0	4	2.2	253	5.1	1.4	·	·	·	·	·	·	7	9	8	6	·	3	·	·
XI	5	2.4	·	·	·	·	1.6	2.3	3.7	2.5	·	·	·	·	2.8	2.4	4	2.3	584	240	4	·	·	·	8	·	·	4	1.7	1.3	1.1	2	5	5	·
XII	6.5	2.1	·	·	6	1.0	1.6	2.6	2.4	3.2	·	·	0.5	2.0	3.8	2.5	2	2.5	1459	368	11	1.3	1.8	2.4	·	·	·	4	1.7	1.7	1.3	5	·	2.2	·
Rok	9.0	1.9	8	0.6	5.2	1.0	1.3.9.5	2.0	3.8.7.5	2.5	1	0.3	3.3	1.5	3.2.5	2.2	5.9	2.1	1127.1	510	27.VI	2.4	3.2	9.6	2.2	1	·	7.5	1.4.2	1.6.8	1.3.7	3.9	2.2	8.6	2.5

Lubań Wielki

$H_s = 1023\ m$ $h_w = 15{,}1\ m$

I	1.0	4.0	1	3.0	7	5.9	·	·	3.5	1.3.9	4.9.5	9.3	3	2.3	1.2	3.4	7	6.9	200	64	5	6	2.4	3.0	·	1.0	6	4	1.3	1.2	6	·	1.1	3.1	·
II	·	·	1	3.0	1	4.0	1	2.0	5.5	6.9	3.5	6.1	1.6	3.3	1.3.5	3.9	1.2	4.3	549	89	9	1	1.3	2.5	·	4	1	5	1.5	1.5	1.3	·	1.4	2.8	·
III	0.5	5.0	·	·	·	·	·	·	0.5	1.0	2.5.5	9.7	2.3.5	6.3	3.8	6.9	5	7.2	888	159	14	·	8	2.1	·	1.1	8	1	2.2	2.2	1.9	2	1.8	2.5	·
IV	1.3.5	4.5	3.5	4.6	2	6.0	1	6.0	5.5	4.8	3.5	7.1	7	4.4	1.6.5	3.3	6	5.1	220	51	8	·	·	5	·	6	2	5	1.1	9	7	·	4	2	2
V	5.5	4.3	0.5	9.0	1.5	6.3	1	7.0	1.5	4.3	2.1	5.7	1.5	4.4	3.2	3.9	1.5	3.9	1505	366	6	·	·	3	·	1	·	1	2.3	2.2	1.8	5	1.9	·	7
VI	6	2.7	3	4.3	1	5.0	1	5.0	5	4.0	1.8.5	4.7	1.7.5	3.5	3.4	3.5	4	3.6	1383	349	6	·	·	·	2	1	1	·	1.3	1.5	1.1	5	8	·	1.0
VII	1.5	3.7	1	3.0	·	·	·	·	2.5	6.4	2.1.5	7.7	2.8	4.4	2.9.5	3.8	9	4.5	1663	434	30	·	·	·	2	4	1	2	1.9	1.7	1.4	4	9	·	4
VIII	7	4.7	0.5	7.0	·	·	·	·	·	·	3.2	8.2	1.9.5	3.9	2.9	4.3	5	5.4	935	240	9	·	·	·	2	4	2	1	1.5	1.8	8	3	8	·	4
IX	3.5	4.7	2	7.0	5	7.4	·	·	2	3.0	3.1.5	7.3	2.3.5	5.3	1.4.5	2.9	8	5.2	239	50	9	·	·	·	·	6	4	1.0	8	1.2	8	·	4	·	2
X	2.5	4.6	3.5	5.3	6	7.3	·	·	2.0.5	8.7	2.4.5	7.9	1.1	3.4	1.5	4.8	1.0	6.0	392	154	30	·	·	·	·	6	4	5	1.2	1.1	6	2	6	·	·
XI	1	5.0	·	·	2	5.0	1	6.0	6.5	1.0.7	3.6.5	1.0.0	1.7	4.2	1.5	4.5	1.1	6.6	680	214	4	·	8	1.7	·	1.0	8	1	1.9	1.6	1.3	2	1.5	9	·
XII	8.5	6.1	6	5.3	2	7.0	1	9.0	4	1.2.9	3.6	1.4.5	9.5	6.7	2.0	3.5	6	8.8	1193	260	6	1.4	1.9	2.8	·	1.4	1.1	2	1.8	2.0	1.3	4	1.4	2.5	·
Rok	5.9.5	4.1	2.2	4.3	2.7.5	4.5	6	2.9	5.7	7.5	3.6.6.5	8.2	1.8.9.5	4.3	2.6.9	4.1	9.8	5.6	9787	434	30.VII	2.1	7.2	1.2.9	6	7.7	4.8	3.7	1.8.8	1.8.9	1.3.6	2.7	1.3.0	1.2.0	2.9

Zawoja

$H_s = 670\ m$ $h_w = 18\ m$

I	6	1.5	4.5	1.2	2.5	1.0	1.0	1.4	1.1.5	7.2	1.1.5	4.7	3	1.5	4	1.8	4.0	1.9	231	111	4	1.1	1.4	2.9	·	5	3	7	6	1.0	6	1	1	2.8	·
II	4.5	1.6	1	1.0	·	·	1.2	1.2	1.1	2.7	1.2	1.8	1.5	2.7	3	1.3	3.9	1.0	599	160	9	1	2	2.5	·	1	·	7	9	1.5	1.0	1	·	2.7	·
III	5	3.8	1	1.0	1	1.0	3	1.5	2.3.5	3.3	1.8	4.5	1.0.5	2.9	8	2.1	2.3	2.5	1076	340	14	·	·	1.4	·	3	1	1	1.8	2.2	1.7	2	1	1.3	·
IV	1.0	2.2	0.5	1.0	3	1.0	5.5	2.8	1.5.5	3.4	9.5	3.4	2	1.5	5	1.5	3.9	1.5	537	127	18	·	·	5	·	·	·	7	3	1.2	8	1	·	·	2
V	6	1.8	5	1.9	2	1.0	3.5	2.1	4.5	2.8	8	2.6	1.0	1.6	3	1.7	5.1	0.9	1482	349	6	·	·	1	·	·	·	·	1.3	2.1	1.4	5	3	·	6
VI	5	1.2	2.5	1.0	·	·	·	·	7	2.2	8.5	2.1	9	1.3	7	1.3	5.1	0.7	1339	273	4	·	·	·	3	·	·	3	8	1.5	1.4	5	1	·	6
VII	1.5	1.7	2	1.5	2	1.0	0.5	2.0	1.2	3.4	1.4.5	4.6	8.5	1.4	4	1.6	4.8	1.0	1456	286	29	·	·	·	2	·	·	4	5	1.8	1.5	5	·	·	3
VIII	5	1.4	0.5	2.0	·	·	0.5	1.0	1.1.5	3.3	2.3	2.2	3	1.0	4.5	1.6	4.5	1.1	889	237	12	·	·	·	5	1	·	4	7	1.5	1.0	4	·	·	2
IX	6.5	2.2	3.5	1.1	3	1.0	5.5	1.4	1.0.5	2.4	1.6	1.9	3.5	1.4	1.5	1.0	4.0	1.0	202	5.9	9	·	·	·	2	·	·	1.4	6	9	6	·	·	·	1
X	2.5	1.6	3.5	1.3	6.5	1.1	1.4.5	1.9	1.5.5	5.0	1.2.5	2.2	2.5	1.8	4.5	2.0	3.1	1.7	263	120	30	·	·	·	·	4	2	7	7	1.0	5	1	3	·	·
XI	3.5	1.4	2	1.5	1	1.0	3	2.0	1.3.5	3.8	8.5	2.5	7	1.6	4.5	1.3	4.7	1.2	101.7	51.6	4	1	2	1.7	·	3	1	2	1.6	1.5	9	3	5	1.0	·
XII	1.0.5	2.4	1.5	1.7	·	·	3	1.0	6	6.8	1.6.5	5.5	6	1.6	4.5	1.4	4.5	1.9	126.7	39.0	6	1.3	1.8	2.5	·	7	2	2	1.5	1.7	1.1	6	1	2.4	·
Rok	6.6	1.9	2.7.5	1.4	2.1	0.7	6.1	1.5	1.4.2	3.9	1.5.8.5	2.9	6.6.5	1.7	5.3.5	1.6	4.9.8	1.4	10358	51.6	4.XI	2.6	3.6	1.1.6	1.2	2.4	9	5.8	1.1.3	1.7.9	1.2.5	3.3	1.5	1.0.2	2.0

Uwaga. W okresie 1.1. – 8.IV. obserwacje nad wiatrem prowadzano za pomocą skali Beauforta.

Nowy Sącz

$\varphi = 49°37'$ $\lambda = 20°42'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	P_{om}	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	984,4	1004,6	966,4	1021,9	0,8	-7,6	10,5	4	-20,9	27	-5,3	-0,7	-3,5	-3,2	3,7	4,3	4,0	4,0	83	71	78	77	0,9	1,9	1,2	1,3	6,8	6,4	5,7	6,3
II	987,0	1001,0	958,0	1023,9	5,4	-1,9	13,7	18	-11,0	6	-0,7	4,0	0,9	1,3	5,3	5,7	5,6	5,5	90	71	86	82	0,6	2,5	1,0	1,4	8,4	6,7	6,3	7,1
III	983,4	1000,5	961,5	1019,6	10,4	2,3	20,4	18	-3,7	23	3,7	8,5	5,6	5,8	6,8	6,7	7,1	6,9	84	62	78	75	1,4	4,9	2,2	2,8	8,0	8,0	6,5	7,5
IV	977,5	985,8	970,4	1012,7	18,2	4,1	26,0	7,15	-2,7	10	6,3	16,5	11,2	11,3	8,3	8,7	9,3	8,8	86	47	69	67	1,4	10,7	4,3	5,5	6,0	6,1	4,5	5,5
V	977,2	985,2	962,3	1012,3	17,1	6,9	25,2	6	0,8	3	9,1	15,2	11,3	11,7	10,3	10,0	11,0	10,4	88	59	81	76	1,4	8,0	2,7	4,0	7,6	8,4	7,2	7,7
VI	980,7	993,7	970,6	1015,3	23,9	11,3	32,5	27	6,3	21	14,4	22,1	17,2	17,7	14,4	14,2	15,3	14,6	88	55	78	74	2,1	13,3	4,6	6,7	5,4	6,4	6,9	6,2
VII	980,0	991,2	965,6	1014,8	21,9	10,9	31,1	4	6,6	7	13,8	20,2	15,7	16,4	13,3	13,3	14,6	13,7	84	57	81	74	2,7	11,2	3,5	5,8	5,9	7,4	7,1	6,8
VIII	982,6	995,0	972,1	1017,4	23,2	11,6	34,4	11	5,8	31	13,6	21,7	16,5	17,1	14,2	14,9	15,8	15,0	90	57	83	77	1,8	12,2	3,4	5,8	5,8	6,7	5,7	6,1
IX	984,9	998,3	973,5	1020,1	22,1	7,7	31,1	18	-2,6	23	9,5	20,9	13,6	14,4	11,1	12,7	13,0	12,3	92	52	83	76	1,3	12,9	2,9	5,7	5,5	4,9	3,7	4,7
X	984,1	996,1	960,4	1019,6	17,2	6,0	22,2	20	0,5	22	7,7	16,1	10,8	11,4	9,1	10,3	10,0	9,8	87	58	79	75	1,7	8,3	3,1	4,4	7,0	6,0	4,9	6,0
XI	979,1	1000,2	966,8	1015,4	8,5	1,3	16,3	3	-6,1	24	2,8	7,5	4,1	4,6	6,9	7,7	7,3	7,3	90	74	87	84	0,9	3,1	1,1	1,7	8,2	7,6	7,3	7,7
XII	980,1	1005,3	963,9	1017,6	0,5	-8,6	17,4	5	-30,3	26	-4,9	-1,7	-4,3	-3,8	4,4	4,8	4,5	4,6	84	79	85	83	0,9	1,7	0,9	1,2	7,1	7,6	7,2	7,3
Rok	981,8	1005,3	958,0	1017,6	14,1	3,7	34,4	11.VIII	-30,3	26.XII	5,8	12,5	8,3	8,7	9,0	9,4	9,8	9,4	87	62	81	77	1,4	7,6	2,6	3,9	6,8	6,8	6,1	6,6

Istebna - Kubalonka

$\varphi = 49°36'$ $\lambda = 18°54'$

I	–	–	–	–	-1,5	-7,1	6,6	4	-16,2	18,26	-5,2	-2,8	-4,5	-4,2	–	–	–	–	–	–	–	–	–	–	–	–	6,0	5,8	6,2	6,0
II	–	–	–	–	1,4	-3,0	10,4	18	-10,3	6	-1,8	0,7	-1,3	-0,9	–	–	–	–	–	–	–	–	–	–	–	–	8,2	6,5	7,4	7,4
III	–	–	–	–	6,2	-0,3	15,4	18	-7,1	23	0,9	4,2	2,6	2,6	–	–	–	–	–	–	–	–	–	–	–	–	8,2	6,4	7,3	7,3
IV	–	–	–	–	14,6	4,8	21,3	7	-1,6	10	7,6	13,2	8,1	9,2	–	–	–	–	–	–	–	–	–	–	–	–	4,0	4,2	3,5	3,9
V	–	–	–	–	13,1	5,1	21,1	27	0,6	12	7,4	11,8	7,8	8,7	–	–	–	–	–	–	–	–	–	–	–	–	7,0	6,9	6,5	6,8
VI	–	–	–	–	19,8	10,7	27,0	27	6,2	29	13,5	18,3	13,5	14,7	–	–	–	–	–	–	–	–	–	–	–	–	4,3	5,3	4,2	4,6
VII	–	–	–	–	17,9	9,8	27,0	3	5,5	11	11,8	16,3	12,5	13,3	–	–	–	–	–	–	–	–	–	–	–	–	5,4	6,4	4,6	5,5
VIII	–	–	–	–	18,9	10,5	28,8	10	5,4	14	12,7	17,8	13,5	14,4	–	–	–	–	–	–	–	–	–	–	–	–	4,4	5,1	4,1	4,5
IX	–	–	–	–	19,1	10,1	25,3	17,18	4,8	12	11,6	18,0	13,1	14,0	–	–	–	–	–	–	–	–	–	–	–	–	3,4	3,9	3,1	3,5
X	–	–	–	–	13,6	6,5	18,3	8	3,8	15	8,3	12,7	8,5	9,5	–	–	–	–	–	–	–	–	–	–	–	–	6,3	4,8	4,1	5,1
XI	–	–	–	–	5,0	-0,1	11,1	12	-7,6	21	1,6	3,9	1,9	2,3	–	–	–	–	–	–	–	–	–	–	–	–	8,1	6,8	6,8	7,2
XII	–	–	–	–	-1,9	-7,9	10,7	5	-20,1	16	-5,1	-3,7	-4,9	-4,6	–	–	–	–	–	–	–	–	–	–	–	–	7,7	7,2	6,8	7,2
Rok	–	–	–	–	10,5	3,3	28,8	10.VIII	-20,1	16.XII	5,3	9,2	5,9	6,6	–	–	–	–	–	–	–	–	–	–	–	–	6,1	5,8	5,4	5,8

Istebna - Stecówka

$\varphi = 49°35'$ $\lambda = 18°57'$

I	–	–	–	–	-2,1	-7,2	6,6	4	-17,3	18	-5,8	-2,8	-5,1	-4,7	–	–	–	–	–	–	–	–	–	–	–	–	7,0	6,7	5,8	6,5
II	–	–	–	–	1,0	-3,1	9,5	18	-11,1	6	-2,3	0,2	-1,4	-1,2	–	–	–	–	–	–	–	–	–	–	–	–	8,4	7,6	6,8	7,6
III	–	–	–	–	5,5	-0,3	15,5	10	-6,9	23	0,5	4,1	2,5	2,4	–	–	–	–	–	–	–	–	–	–	–	–	8,5	7,1	7,0	7,5
IV	–	–	–	–	14,1	5,0	21,0	7	-2,0	1	7,4	12,8	7,8	9,0	–	–	–	–	–	–	–	–	–	–	–	–	5,3	6,3	3,5	5,0
V	–	–	–	–	12,4	4,6	20,7	27	0,1	12,13,15	7,3	11,2	7,5	8,4	–	–	–	–	–	–	–	–	–	–	–	–	7,9	8,1	6,6	7,5
VI	–	–	–	–	19,2	10,2	26,2	27	4,7	16	13,4	17,5	13,4	14,4	–	–	–	–	–	–	–	–	–	–	–	–	4,9	6,4	5,7	5,7
VII	–	–	–	–	17,5	9,1	26,6	3	4,4	11	11,6	15,5	12,2	12,9	–	–	–	–	–	–	–	–	–	–	–	–	6,6	8,0	5,6	6,7
VIII	–	–	–	–	19,3	9,8	28,9	11	4,6	13	12,8	18,0	13,1	14,8	–	–	–	–	–	–	–	–	–	–	–	–	4,8	6,0	4,9	5,2
IX	–	–	–	–	19,0	9,2	25,6	17	3,5	12	11,5	17,6	12,7	13,6	–	–	–	–	–	–	–	–	–	–	–	–	3,5	4,3	2,8	3,5
X	–	–	–	–	13,9	6,6	18,7	8	2,8	15	8,3	12,7	8,8	9,6	–	–	–	–	–	–	–	–	–	–	–	–	6,6	6,0	4,4	5,7
XI	–	–	–	–	5,4	-0,2	11,0	12	-9,1	21	1,7	3,5	1,9	2,2	–	–	–	–	–	–	–	–	–	–	–	–	8,6	7,9	6,4	7,6
XII	–	–	–	–	-2,0	-8,2	11,1	5	-20,4	16	-5,7	-4,1	-5,1	-5,0	–	–	–	–	–	–	–	–	–	–	–	–	8,0	7,9	6,6	7,5
Rok	–	–	–	–	10,3	3,0	28,9	11.VIII	-20,4	16.XII	5,1	8,8	5,7	6,3	–	–	–	–	–	–	–	–	–	–	–	–	6,7	6,9	5,5	6,4

Istebna - Zadzie

$\varphi = 49°34'$ $\lambda = 18°56'$

I	–	–	–	–	-1,0	-10,9	8,0	4	-23,1	18	-8,1	-2,0	-6,4	-5,7	–	–	–	–	–	–	–	–	–	–	–	–	6,8	6,7	6,6	6,7
II	–	–	–	–	2,0	-6,7	5,5	18	-24,1	6	-2,4	1,1	-2,8	-1,7	–	–	–	–	–	–	–	–	–	–	–	–	8,7	6,1	6,7	7,2
III	–	–	–	–	6,9	-2,5	16,0	18	-13,0	23	0,4	5,6	0,9	2,0	–	–	–	–	–	–	–	–	–	–	–	–	8,1	6,6	6,9	7,2
IV	–	–	–	–	15,8	1,0	23,2	7	-4,6	10	6,6	14,8	5,4	8,0	–	–	–	–	–	–	–	–	–	–	–	–	3,8	5,4	3,4	4,2
V	–	–	–	–	14,7	3,2	22,6	27	-0,7	13	8,2	13,2	7,0	8,8	–	–	–	–	–	–	–	–	–	–	–	–	7,4	7,8	5,6	6,9
VI	–	–	–	–	21,0	7,9	28,1	27	2,6	29	14,0	19,5	12,4	14,6	–	–	–	–	–	–	–	–	–	–	–	–	4,9	5,9	4,9	5,2
VII	–	–	–	–	19,2	7,0	28,1	3	1,5	26	12,7	17,8	11,4	13,3	–	–	–	–	–	–	–	–	–	–	–	–	5,9	7,2	4,9	6,0
VIII	–	–	–	–	20,0	7,8	29,8	10	2,3	14	13,0	19,1	11,9	14,0	–	–	–	–	–	–	–	–	–	–	–	–	5,1	5,3	4,8	5,1
IX	–	–	–	–	20,1	4,7	26,0	2	-1,8	23	8,6	19,4	9,7	11,9	–	–	–	–	–	–	–	–	–	–	–	–	3,9	3,9	2,8	3,5
X	–	–	–	–	14,7	2,5	19,2	6	-2,3	10	6,8	13,9	6,4	8,4	–	–	–	–	–	–	–	–	–	–	–	–	7,2	5,8	4,8	5,9
XI	–	–	–	–	5,3	-2,1	11,7	3	-13,2	21	0,4	4,1	0,2	1,2	–	–	–	–	–	–	–	–	–	–	–	–	8,5	7,8	7,2	7,8
XII	–	–	–	–	-1,9	-12,0	11,5	5	-35,0	25	-7,6	-3,8	-7,3	-6,5	–	–	–	–	–	–	–	–	–	–	–	–	7,9	7,3	7,0	7,4
Rok	–	–	–	–	11,4	0,0	29,8	10.VIII	-35,0	25.XII	4,4	10,2	4,1	5,7	–	–	–	–	–	–	–	–	–	–	–	–	6,5	6,3	5,5	6,1

Nowy Sącz — $H_s = 292\ m$ — $H_b = 295{,}4\ m$ — $h_w = 16{,}5\ m$ — 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD																			OPAD R			LICZBA DNI (n)																
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość					Temperatura T				Wiatr				Opad R								
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 35°	≥ 10	≥ 15			≥ 0,1	≥ 1,0	≥ 10,0					
I	1	8,0	8,5	2,3	3,5	2,4	5	2,2	2,0	3,2	10,5	3,0	2,5	3,8	3	1,7	3,9	1,7	14,3	6,4	5	10	13	29	·	4	·	5	10	11	5	·	3	16	·				
II	2	4,0	2	4,0	1	6,0	1,5	2,3	11,5	2,9	4,5	3,7	5	3,0	2,5	3,4	5,4	1,2	27,6	8,8	9	1	·	19	·	1	·	3	14	12	7	·	2	8	·				
III	3	2,8	·	·	·	·	0,5	1,0	2	4,2	2,0	5,0	32,5	5,2	10	4,6	2,5	3,6	34,1	4,2	14,18	·	·	9	·	12	4	3	18	18	11	·	·	3	·				
IV	5,5	1,5	5,5	2,9	6	3,2	3	3,2	8,5	3,5	3,5	6,9	7,5	3,5	1,5	8,0	4,9	1,6	4,5	1,2	8	·	·	2	2	6	3	6	7	6	1	·	1	·	2				
V	12,5	3,4	3,5	1,9	2,5	4,4	1	2,0	5	2,5	4	4,6	11	4,4	2,5	3,4	5,1	1,6	106,5	18,2	6	·	·	·	1	2	1	·	16	16	13	3	3	·	6				
VI	5	2,0	2,5	2,0	3,5	2,6	5	1,6	9,5	2,6	1,5	2,7	8,5	4,1	3,5	5,9	5,1	1,3	95,7	21,6	6	·	·	·	11	1	·	1	10	12	11	4	2	·	10				
VII	9	2,0	1,5	3,3	·	·	·	·	5,5	5,0	7,5	3,1	1,0	4,1	6,5	3,1	5,3	1,5	159,3	32,0	29	·	·	·	8	2	1	2	10	19	14	6	·	·	4				
VIII	9	2,9	3	2,7	·	·	·	·	1,3	2,8	10,5	4,1	10,5	4,7	7	4,2	4,0	2,1	79,2	30,1	9	·	·	·	9	4	·	4	10	10	8	3	4	·	5				
IX	2	3,0	5	2,2	7	1,3	0,5	2,0	8	3,6	3,5	4,3	7,5	6,9	0,5	6,0	5,6	1,4	24,3	11,3	26	·	·	2	0	3	·	10	8	6	3	1	6	·	4				
X	6,5	3,0	2,5	4,0	5	2,5	1,0	3,4	21,5	3,1	1,5	2,3	3	3,2	2	1,8	4,1	1,7	29,9	14,7	30	·	·	·	·	1	·	4	9	8	7	1	5	·	·				
XI	7,5	2,1	1	1,0	0,5	1,0	4,5	1,4	15,5	2,2	2,5	3,2	7	5,1	1,5	4,0	5,0	1,2	65,0	26,7	4	·	·	9	·	·	·	1	16	14	8	1	8	3	·				
XII	1,2	2,5	2	1,8	·	·	2,5	3,2	12,5	3,2	8,5	5,9	6,5	5,9	1,1	5,1	3,8	2,4	77,3	23,0	11	12	15	24	·	6	2	2	18	17	11	2	5	2,5	·				
Rok	7,5	3,1	3,7	2,3	2,9	2,0	33,5	1,9	132,5	3,2	7,8	4,1	111,5	4,5	51,5	4,3	54,7	1,8	717,7	32,0	29.VII	23	28	94	40	42	11	41	146	149	99	21	39	55	31				

Istebna - Kubalonka — $H_s = 800\ m$ — $h_w = 25{,}6\ m$

I	7,5	2,3	7	2,4	·	·	5	4,7	3,8	4,5	1,3	2,8	·	·	2,5	1,8	2,0	2,9	36,6	19,0	4	8	26	30	·	2	1	7	13	12	7	1	6	30	·				
II	4,5	1,8	2	1,2	1	1,0	3,5	2,1	33,5	3,0	1,1	2,7	1	2,0	6,5	1,3	2,1	1,9	77,7	15,4	9	1	9	28	·	·	·	2	17	14	13	1	1,5	2,8	·				
III	1,2	1,8	2	2,0	·	·	·	·	9	3,4	11,5	2,9	12,5	2,6	1,8	2,4	2,8	1,8	142,9	19,0	14	·	2	16	·	·	·	3	17	21	20	6	9	2,3	·				
IV	8,5	1,9	6,5	2,8	3,5	1,4	4,5	3,3	25,5	3,1	18,5	2,6	2	3,0	6	1,8	1,5	2,2	60,6	20,2	18	·	·	3	·	·	·	1,2	1	8	7	3	1	2	3				
V	13,5	1,9	5,5	1,1	·	·	3	2,3	1,6	3,5	1,4	2,8	3	2,0	2,1	2,1	1,7	2,0	153,8	47,1	6	·	·	·	·	·	·	4	13	2,0	1,4	5	1,0	·	4				
VI	1,1,5	1,4	1	1,5	1	1,5	·	·	2,0,5	2,5	1,5	2,5	6,5	1,5	2,5,5	1,8	9	1,8	231,0	62,6	27	·	·	·	3	·	·	6	4	16	15	6	4	·	11				
VII	1,0	2,1	·	·	·	·	0,5	5,0	11,5	3,3	28,5	1,8	1,0	1,3	16,5	1,5	1,6	1,5	176,9	26,6	30	·	·	·	3	1	·	6	7	15	14	9	5	·	6				
VIII	9	1,7	2,5	2,2	·	·	1	4,0	1,5	3,3	2,5,5	1,9	6,5	2,0	13,5	1,9	2,0	1,7	95,4	28,2	12	·	·	·	5	·	·	8	7	15	10	4	1	·	5				
IX	1	6,0	5	1,2	·	·	·	·	1,9	2,8	2,2	2,3	4	2,4	3	2,3	3,6	1,5	21,8	5,3	14	·	·	·	3	·	·	1,5	4	10	7	·	4	·	1				
X	3,5	1,0	3	2,3	2	3,8	7	4,9	4,1	5,0	1,2	2,3	3	2,2	10,5	1,8	1,1	3,3	40,3	8,1	30	·	·	·	·	2	1	6	8	9	8	·	5	·	·				
XI	5,5	1,7	·	·	·	·	8	1,6	3,1,5	3,0	16,5	2,7	1	2,0	13,5	2,3	1,4	2,2	88,9	46,1	4	·	4	15	·	·	·	4	16	14	10	2	1,3	7	·				
XII	2,4	3,2	2,5	1,0	·	·	0,5	1,0	2,6,5	3,3	12,5	3,4	2,5	1,8	12,5	2,8	1,2	2,7	155,0	37,8	6	14	20	27	·	·	·	3	16	19	14	6	16	2,5	·				
Rok	1,1,0,5	2,2	3,7	1,5	7,5	0,6	3,3	2,4	2,8,7	3,4	2,0,0.	2,6	5,2	1,9	1,4,9	2,0	2,1,9	2,1	1,2,8,0,9	6,2,6	27.VI	23	6,1	1,1,9	1,4	5	2	7,6	1,2,3	1,7,3	1,3,9	4,3	8,9	1,1,5	3,0				

Istebna - Stecówka — $H_s = 750\ m$ — $h_w = 12{,}5\ m$

I	9	1,9	8	2,8	7	2,4	3	2,0	5,5	4,4	4,5,5	3,3	3	1,7	7	2,3	5	2,8	4,3,0	2,1,0	4	8	2,7	3,0	·	·	·	6	1,6	1,3	7	1	4	3,1	·				
II	9,5	1,6	2,5	1,6	1	2,0	·	·	6,5	3,6	4,3,5	2,6	4	1,5	9	2,0	8	2,2	1,1,9,1	2,5,4	9	1	1,1	2,8	·	·	·	3	1,7	1,7	1,4	2	7	2,8	·				
III	1,0	2,0	·	·	·	·	·	·	1	2,0	2,4,5	3,3	1,9	2,2	3,0,5	2,5	8	2,4	1,6,4,1	3,2,0	14	·	4	1,7	·	·	·	2	1,9	2,3	2,0	8	7	2,4	·				
IV	5,5	2,5	1,1,5	2,0	1,5	2,6	6	3,3	1,5	3,7	2,2,5	2,4	5,5	2,5	4	1,8	5	2,5	6,2,4	2,3,6	18	·	·	3	·	1	·	6	4	8	7	3	1	2	2				
V	2,1	1,6	8,5	1,9	1	2,0	3	1,7	3,5	2,3	2,6,5	2,9	8	2,1	1,6,5	1,9	5	2,0	1,3,4,5	3,6,3	6	·	·	·	·	·	·	·	1,3	1,9	1,4	4	8	·	5				
VI	2,5,5	1,7	6	1,7	1,0	1,8	2	2,0	5,5	2,7	1,8,5	2,4	7	1,7	1,1,5	2,1	4	1,9	2,1,3,2	5,7,6	27	·	·	·	3	·	·	5	1,0	1,5	1,5	8	5	·	9				
VII	1,4,5	1,3	8	1,4	1,5	2,3	·	·	5	3,8	3,9,5	2,3	8,5	1,8	1,2	2,2	4	2,0	1,8,6,2	2,5,1	30	·	·	·	3	·	·	3	1,3	1,5	1,3	9	2	·	4				
VIII	4,5	2,1	10,5	1,5	2,5	1,0	0,5	1,0	9,5	3,1	3,5,5	2,6	7,5	2,9	1,7,5	2,5	5	2,3	9,1,8	2,1,7	12,3	·	·	·	6	1	·	8	8	1,4	1,1	3	4	·	2				
IX	8	1,8	1,2	2,2	6	2,2	3	2,3	1,4	2,5	2,9	2,4	6	1,8	7	1,7	5	2,1	2,6,5	6,7	9	·	·	·	1	·	·	1,6	4	1,0	7	·	4	·	1				
X	8	1,7	7	1,9	1,6,5	2,5	1,7	3,7	1,7,5	4,4	2,1	3,4	2	2,0	4	2,2	·	3,2	3,7,8	8,6	30	·	·	·	·	1	·	5	9	1,0	9	·	4	·	·				
XI	1,3	1,9	1	1,0	5,5	2,0	6,5	2,8	1,4,5	2,6	2,9,5	2,2	5	1,0	1,0	1,8	5	2,0	8,1,2	3,5,5	4	·	6	1,5	·	·	·	1	1,7	1,5	9	3	1,1	8	·				
XII	3,3,5	2,1	6	1,7	1	5,0	2	2,8	7,5	2,8	2,5,4	3,3	4	1,5	6,5	3,3	7	2,4	1,5,6,0	3,1,0	6	1,3	2,0	2,6	·	·	·	2	1,6	2,1	1,4	7	5	2,5	·				
Rok	1,6,2	1,8	8,1	1,6	6,7	2,2	4,3	1,8	1,0,5	3,2	3,6,1	2,8	7,9,5	1,9	1,3,5,5	2,2	6,1	2,3	1,3,1,5,8	5,7,6	27.VI	22	6,8	1,1,9	1,3	3	·	5,7	1,4,6	1,8,0	1,4,0	4,8	6,2	1,1,8	2,3				

Istebna-Zadzie — $H_s = 580\ m$ — $h_w = 19\ m$

I	2	3,0	3	2,3	·	·	0,5	1,0	6,5	3,2	1,8,5	2,9	5,5	2,2	4	1,8	5,3	1,2	4,0,4	2,2,6	4	1,6	1,6	3,0	·	·	·	4	1,5	1,0	6	1	1	3,1	·				
II	·	·	·	·	·	·	·	·	1,5	2,3	1,0,5	2,0	·	·	6	2,2	6,6	0,5	9,8,1	2,9,2	9	8	7	2,8	·	·	·	2	1,5	1,6	1,4	2	4	2,8	·				
III	4	3,0	1	1,0	·	·	·	·	4	2,8	1,7	2,7	1,0	2,2	1,6	2,9	4,1	1,5	1,1,0,6	1,8,6	14	3	1	2,1	·	·	·	1	1,7	2,0	1,6	4	3	2,0	·				
IV	7	2,0	2,5	2,2	4,5	2,3	5	2,8	5	3,6	1,6	3,2	8,5	2,2	4,5	1,6	3,7	1,5	5,1,1	1,9,2	18	·	·	1,2	·	·	·	8	3	1,0	6	2	1	·	3				
V	9	1,9	0,5	2,0	2	2,0	·	·	7,5	2,1	1,0,5	3,1	1,3	2,3	1,8,5	2,1	3,2	1,5	1,0,5,9	3,4,0	6	·	·	2	·	·	·	·	1,1	1,7	1,5	4	1	·	6				
VI	1,0	1,8	2	1,5	1	3,0	2,5	1,0	1,5	1,0	8,5	2,0	1,5	1,8	7,5	1,9	4,2	1,0	1,9,0,0	4,9,6	27	·	·	·	4	·	·	7	6	1,6	1,4	6	8	·	1,1				
VII	0,5	2,0	1	1,0	·	·	0,5	3,0	4	1,9	1,6	1,9	1,4,5	1,6	6,5	1,5	5,0	0,8	1,7,4,0	2,8,3	4	·	·	·	5	·	·	2	8	1,8	1,3	8	·	·	7				
VIII	2	1,5	·	·	1	2,0	·	·	3,5	2,4	1,1,5	3,3	1,4	2,0	1,0	1,6	5,1	1,0	6,8,5	1,6,7	12	·	·	·	6	·	·	7	6	1,1	1,0	2	·	·	2				
IX	3	1,3	·	·	4	2,2	·	·	4	2,0	9	2,8	5	2,0	4	2,0	6,1	0,7	1,9,8	6,3	9	·	·	5	5	·	·	1,5	6	7	6	·	5	·	2				
X	7,5	2,1	5	1,6	6,5	2,2	4	3,4	8,5	4,4	1,1,5	2,7	2,5	3,4	6,5	2,0	4,1	1,5	3,8,7	7,5	30	·	·	8	·	·	·	5	9	9	8	·	4	·	·				
XI	5,5	1,5	1,5	1,7	·	·	·	·	5	3,0	1,1,5	2,2	3	1,8	8,5	1,8	5,5	0,8	7,1,7	3,0,5	4	4	1	1,9	·	·	·	3	1,8	1,0	8	2	8	1,0	·				
XII	1,0,5	2,0	3	2,5	·	·	·	·	2	3,5	1,2	2,5	3,5	3,6	1,2	2,0	5,0	1,1	1,3,4,3	3,7,7	11	1,7	1,9	2,8	·	·	·	4	1,8	1,7	1,1	4	4	2,5	·				
Rok	6,1	1,8	1,9,5	1,3	1,9	1,1	1,2,5	0,9	5,3	2,7	1,5,3,5	2,6	9,4,5	2,1	1,0,4	2,0	5,7,9	1,1	1,1,0,3,1	4,9,6	27.VI	4,8	4,4	1,5,3	2,0	·	·	5,8	1,3,2	1,6,1	1,2,7	3,5	3,9	1,1,4	3,1				

Rabka

$\varphi = 49°36'$ $\lambda = 19°58'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T					Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	953.2	971.4	936.3	–	0.3	-8.4	9.4	4	-20.8	18	-5.9	-1.0	-4.8	-4.1	3.7	3.9	3.8	3.8	86	66	84	79	0.6	2.0	0.8	1.1	7.0	6.0	5.3	6.1
II	956.5	971.0	928.8	–	4.7	-3.2	12.1	18	-13.6	6	-2.0	3.2	-0.4	0.1	4.9	5.6	5.4	5.3	91	73	90	85	0.5	2.3	0.6	1.1	7.2	6.2	6.4	6.6
III	953.9	970.6	932.7	–	8.3	0.5	18.4	10,18	-8.7	23	1.8	6.5	3.5	3.8	6.2	6.3	6.5	6.3	89	66	83	79	0.8	3.8	1.5	2.0	8.3	7.7	6.6	7.5
IV	948.1	955.2	941.7	–	16.5	3.7	23.9	7	-3.3	10	5.7	15.2	9.3	9.9	8.0	8.5	8.8	8.4	86	50	75	70	4.3	9.4	3.1	4.6	5.7	5.9	4.3	5.3
V	948.1	955.1	934.7	–	15.4	5.7	22.5	29	0.4	15	8.2	13.6	9.2	10.0	9.5	9.6	10.1	9.7	87	62	85	78	4.5	6.6	4.8	3.3	7.2	8.4	7.9	7.8
VI	952.1	964.7	942.3	–	22.2	10.1	31.0	27	5.0	21	13.9	20.2	15.1	16.1	13.7	13.7	14.2	13.9	86	60	83	76	2.4	10.6	3.1	5.4	5.1	7.0	6.5	6.2
VII	951.4	961.8	938.1	–	20.5	9.4	30.0	4	4.7	6	12.7	18.8	14.0	14.9	12.6	12.5	13.3	12.8	85	59	83	76	2.4	10.2	2.9	5.2	6.1	7.5	7.2	6.9
VIII	953.9	965.6	944.0	–	21.3	10.3	31.8	11	4.9	31	12.5	19.9	14.2	15.2	13.0	13.4	14.2	13.5	89	58	86	78	1.8	11.1	2.5	5.1	6.4	7.1	5.2	6.2
IX	955.7	966.0	945.5	–	21.2	7.5	29.6	17	-0.6	23	8.9	20.1	12.2	13.4	10.5	11.9	11.9	11.3	91	52	83	75	1.3	12.4	2.6	5.4	4.5	4.7	3.7	4.3
X	954.4	965.6	931.1	–	16.4	4.4	21.5	19	-0.4	22	6.1	15.4	8.7	9.7	8.5	9.4	9.2	9.0	90	55	82	76	1.1	8.5	2.2	3.9	6.4	5.8	4.3	5.5
XI	949.2	968.7	937.9	–	7.7	0.1	14.6	7	-8.4	21	1.8	6.4	2.5	3.3	6.5	7.0	6.6	6.7	90	73	89	84	0.8	3.0	0.8	1.5	8.1	7.5	6.9	7.5
XII	949.6	971.3	935.4	–	-0.6	-8.8	16.4	5	-27.6	25	-6.1	-2.3	-5.4	-4.8	4.2	4.7	4.2	4.4	88	80	89	86	0.7	1.3	0.6	0.9	7.0	7.3	6.5	6.9
Rok	952.2	971.4	928.8	–	12.8	2.6	31.8	11.VIII	-27.6	25.XII	4.8	11.3	6.5	7.3	8.4	8.9	9.0	8.8	88	63	84	78	1.3	6.8	1.9	3.3	6.6	6.8	5.9	6.4

Brzezna

$\varphi = 49°36'$ $\lambda = 20°37'$

I	–	–	–	–	0.8	-7.3	10.7	4	-21.0	27	-5.1	-1.0	-3.6	-3.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.7	6.6	6.8
II	–	–	–	–	5.2	-1.9	13.5	18	-9.9	6	-0.7	3.8	0.8	1.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.2	6.9	6.9
III	–	–	–	–	10.4	2.3	20.3	18	-2.5	22,23	3.7	8.6	5.3	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	6.7	7.3
IV	–	–	–	–	17.9	4.4	25.5	15	-3.0	10	7.0	16.5	10.5	11.1	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.9	4.7	5.4
V	–	–	–	–	17.1	6.4	25.5	6	1.5	3	9.8	15.4	10.4	11.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.8	8.1	8.0
VI	–	–	–	–	24.1	10.7	32.4	26	5.6	21	15.4	22.5	16.0	17.5	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.3	7.1	6.1
VII	–	–	–	–	22.4	10.5	31.8	4	5.8	6,7	14.5	20.8	14.8	16.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.3	7.5	6.9
VIII	–	–	–	–	23.3	11.3	34.1	11	5.8	31	14.2	22.3	15.9	17.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.4	6.2	6.2
IX	–	–	–	–	22.7	8.1	32.9	18	-1.7	23	10.1	21.7	13.0	14.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.1	4.1	4.4
X	–	–	–	–	17.1	6.4	22.5	20	0.4	22	8.0	16.5	10.4	11.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.0	4.9	5.3
XI	–	–	–	–	8.4	1.3	18.1	3	-6.4	21,22,24	2.6	7.5	4.0	4.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.8	7.5	7.2
XII	–	–	–	–	0.8	-8.3	16.0	5	-30.5	26	-4.9	-2.1	-4.8	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.3	7.6
Rok	–	–	–	–	14.2	3.7	34.1	11.VIII	-30.5	26.XII	6.2	12.7	7.7	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.5	6.5	6.5

Płaszkowa

$\varphi = 49°36'$ $\lambda = 20°53'$

I	–	–	–	–	-0.8	-7.9	8.2	4	-18.7	18,27	-5.3	-2.3	-4.6	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.5	6.3	6.5
II	–	–	–	–	3.7	-2.6	11.9	18	-9.1	6	-1.2	2.5	0.0	0.3	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.6	6.9	7.2
III	–	–	–	–	8.6	1.6	18.4	18	-5.5	23	3.1	6.3	4.7	4.7	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.5	7.4	8.2
IV	–	–	–	–	15.4	5.1	23.6	15	-1.9	10	7.9	14.1	9.7	10.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.2	4.7	5.5
V	–	–	–	–	14.9	6.8	22.0	29	1.3	15	9.0	12.9	9.9	10.5	–	–	–	–	–	–	–	–	–	–	–	–	7.7	8.4	7.4	7.8
VI	–	–	–	–	22.1	11.7	29.4	26	6.4	29	15.5	20.6	15.7	16.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.4	6.4	6.1
VII	–	–	–	–	20.7	11.0	29.6	4	6.7	7	14.7	19.1	14.7	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.8	6.9	6.8
VIII	–	–	–	–	21.4	12.0	32.2	11	6.8	14	14.7	20.1	15.7	16.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.2	6.2	6.4
IX	–	–	–	–	20.1	9.6	29.6	18	0.9	22	11.7	18.9	14.1	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.0	3.8	4.6
X	–	–	–	–	14.9	7.0	20.2	19,20	1.7	22	8.6	13.8	10.2	10.7	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.9	4.5	5.5
XI	–	–	–	–	7.0	1.1	13.0	1	-7.4	21	2.9	5.7	3.4	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.6	7.1	7.7
XII	–	–	–	–	-0.5	-7.5	15.4	5	-26.2	25	-4.1	-2.2	-4.1	-3.5	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.7	7.8
Rok	–	–	–	–	12.3	4.0	32.2	11.VIII	-26.2	25.XII	6.5	10.8	7.4	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.0	6.3	6.7

Babia Góra

$\varphi = 49°35'$ $\lambda = 19°31'$

I	–	–	–	–	-3.7	-8.7	2.8	4	-19.9	18	-6.4	-5.3	-6.1	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	5.9	5.8	6.3
II	–	–	–	–	-0.7	-5.1	7.3	27	-12.2	6	-3.0	-2.6	-3.2	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	5.7	5.7	6.2
III	–	–	–	–	2.7	-2.7	11.8	18	-9.2	22,23	-1.3	0.9	-0.1	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.2	7.8	7.7	8.2
IV	–	–	–	–	9.8	2.3	16.9	15	-4.9	1,9,10	5.4	7.8	4.6	5.6	–	–	–	–	–	–	–	–	–	–	–	–	3.6	4.0	4.8	4.1
V	–	–	–	–	9.4	2.8	16.9	27	-2.6	12	5.2	7.9	4.9	5.7	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.6	7.1	7.4
VI	–	–	–	–	16.4	8.2	23.9	27	2.7	29	11.8	14.2	10.8	11.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.6	6.7	6.4
VII	–	–	–	–	14.9	7.2	24.4	3	3.0	7	10.4	12.5	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.7	7.7	6.9
VIII	–	–	–	–	15.4	8.0	26.4	11	3.5	14	10.8	14.2	10.8	11.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	7.3	6.6
IX	–	–	–	–	15.7	7.6	22.9	17	2.9	12	9.7	14.6	10.0	11.1	–	–	–	–	–	–	–	–	–	–	–	–	4.9	4.8	4.1	4.6
X	–	–	–	–	11.4	3.4	16.9	6	–	–	6.7	9.6	6.8	7.5	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	5.2	5.5
XI	–	–	–	–	3.3	-1.5	9.3	13	-11.4	21	0.9	1.8	0.7	1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.9	7.9	7.2	7.7
XII	–	–	–	–	-2.4	-9.6	11.4	15	-23.7	16	-6.0	-5.2	-6.1	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.7	7.9	7.8
Rok	–	–	–	–	7.7	1.0	26.4	11.VIII	-23.7	16.XII	3.7	5.9	3.6	4.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.4	6.4	6.5

Rabka

$H_s = 512\ m$ $H_b = 552{,}5\ m$ $h_w = 18\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °/0, °/00																	OPAD R			LICZBA DNI (n)										
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość													
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Temperatura T Min < -10°	Max < 0°	Min < 0°	Max ≥ 25°	Wiatr v ≥ 10	v ≥ 15	●	●	Opad R ≥ 0,1	≥ 1,0	≥ 10,0	≡	▦	R 12
I	1	2,0	9,5	2,7	4,5	2,6	4	1,9	13	2,8	24	4,2	2	1,5	2	3,0	33	2,1	185	74	5	11	12	28	·	4	1	4	12	11	4	·	·	30	·
II	0,5	2,0	·	·	·	·	2	2,2	14	3,3	17	1,9	14	1,9	6,5	1,8	30	1,4	57,7	17,7	9	1	1	23	·	1	·	4	14	15	12	2	2	20	·
III	1	10,0	·	·	·	·	1,5	3,0	8,5	2,5	27,5	3,6	22,5	3,6	12	3,9	20	2,8	72,7	14,5	14	·	·	10	·	6	4	1	17	21	16	1	·	8	·
IV	5	2,5	11	3,8	3	3,7	5	2,6	9	2,7	17,5	4,5	7	2,4	4,5	2,4	28	2,3	18,1	6,7	8	·	·	2	·	7	3	6	6	7	7	·	·	·	2
V	4	1,2	5	1,6	2	4,0	6	1,2	9,5	1,5	20	2,2	16	2,0	8,5	3,2	22	1,6	118,8	31,5	6	·	·	·	·	4	2	·	18	21	17	3	·	·	8
VI	3	1,7	7	2,3	2	1,5	2,5	1,8	12,5	1,8	14	2,0	12,5	2,2	3,5	2,7	33	1,3	121,8	43,7	6	·	·	·	5	1	1	1	8	12	12	3	·	·	11
VII	·	·	7	1,6	·	·	5,5	1,4	8	2,0	22	2,5	17	2,3	7,5	2,7	26	1,6	133,0	30,5	30	·	·	·	7	1	1	3	13	16	15	4	·	·	7
VIII	2,5	1,8	5,5	1,9	1	1,0	1,5	1,7	11	1,4	22	3,3	8	2,0	11,5	1,7	30	1,5	56,2	18,7	12	·	·	·	6	3	·	1	7	10	7	2	1	·	6
IX	3	2,3	7	2,0	·		6	1,5	10	1,6	23	2,9	9	2,7	4	2,1	28	1,6	137	42	9	·	·	2	5	2	·	10	5	8	6	·	2	·	2
X	4,5	2,3	4,5	4,2	4	1,8	6,5	3,1	18	3,8	10,5	2,4	10,5	1,8	5,5	1,9	29	1,9	253	131	30	·	·	1	·	2	1	4	8	8	3	1	1	·	·
XI	·	·	2,5	2,0	0,5	2,0	0,5	4,0	6,5	2,2	20	2,6	14	1,9	10	2,0	36	1,4	71,5	32,1	4	·	1	14	·	2	·	1	17	17	9	1	4	3	·
XII	6,5	2,3	4	1,5	1	1,0	1,5	1,7	14,5	3,1	14	6,4	13	1,9	6,5	2,3	32	2,1	114,5	31,2	11	13	19	26	·	5	1	3	15	20	11	4	2	25	·
Rok	3,1	2,3	6,3	2,0	1,8	1,5	42,5	2,2	134,5	2,4	231,5	3,2	145,5	2,2	8,2	2,5	347	1,8	821,6	43,7	6.VI	25	33	106	23	38	14	38	140	166	119	21	12	86	36

Brzezna

$H_s = 320\ m$ $h_w = 16\ m$

I	16	2,0	8	1,9	·	·	4	6,2	36	4,3	5	9,8	8	2,0	1	3,0	15	3,2	134	6,5	5	9	13	28	·	3	2	3	10	9	4	·	–	5	·
II	11	1,9	2	2,0	1	3,0	2,5	6,2	35,5	4,1	1	2,0	4	3,0	14	2,1	13	2,8	28,4	8,5	9	·	1	19	·	1	·	3	12	11	7	·	–	4	·
III	9	2,8	·	·	·	·	·	·	4	3,8	6	5,2	29	4,4	23	4,6	22	3,3	37,9	6,1	14	·	·	8	·	2	1	2	15	19	12	·	–	3	·
IV	2,0	3,2	4	3,2	·	·	6	4,8	10	4,3	4	6,2	9	2,5	5	2,6	32	2,3	78	2,8	30	·	·	2	2	2	·	5	6	6	3	·	–	·	2
V	1,0	2,5	1	3,0	1	3,0	3	3,0	6	2,3	·	·	10	3,4	11	5,2	51	1,6	90,8	24,0	6	·	·	1	·	·	·	1	19	15	13	4	–	·	5
VI	8	2,6	5,5	1,9	1	1,0	3,5	2,7	12	3,5	1,5	2,3	5	4,2	17,5	1,8	36	1,6	66,9	16,0	6	·	·	·	10	·	·	2	10	12	11	2	–	·	10
VII	6,5	1,8	3,5	2,5	3	1,7	·	·	11	2,5	11	2,5	2	1,0	2,4	2,2	32	1,5	126,6	30,5	29	·	·	·	9	·	·	2	13	16	14	4	–	·	5
VIII	1,1	2,4	0,5	1,0	0,5	1,0	3	1,7	6	3,0	1,7	3,0	1	1,0	1,8	2,7	36	1,6	53,1	21,0	13	·	·	·	10	·	·	3	10	9	8	2	–	·	3
IX	10,5	1,6	7,5	1,7	·	·	·	·	6	1,8	1,0	3,2	8	2,8	3	3,7	45	1,2	15,9	6,8	29	·	·	2	10	·	·	11	7	9	3	·	–	·	1
X	10,5	2,0	3,5	2,1	2,5	1,0	4	3,1	36,5	4,2	1	1,0	1	3,0	7	3,0	27	2,4	25,6	17,0	30	·	·	·	·	·	·	6	8	8	4	1	–	·	·
XI	9	1,4	·	·	·	·	1	2,5	26	3,4	3	2,3	6	3,0	13	2,2	32	1,8	68,3	20,2	4	·	·	7	·	·	·	2	14	13	9	2	–	2	·
XII	1,8	3,2	·	·	·	·	1	1,0	15,5	4,0	17,5	4,2	3	4,3	13	2,2	25	2,5	56,4	16,0	11	10	16	24	·	1	·	2	17	13	10	2	–	2,5	·
Rok	13,9,5	2,3	35,5	1,6	9	0,9	28	2,6	204,5	3,4	77	3,5	86	2,9	149,5	2,9	366	2,2	591,1	30,5	29.VII	19	30	90	42	9	3	42	141	140	98	17	–	3,9	2,6

Ptaszkowa

$H_s = 522\ m$ $h_w = 15{,}1\ m$

I	1	4,0	1,1	2,1	1,5	1,8	7	3,1	18,5	6,4	11,5	3,4	1,5	2,0	5	3,2	9	3,0	17,5	6,7	5	12	16	29	·	4	1	5	14	10	6	·	–	2,9	·
II	·	·	3	1,7	1,9	1,8	3	5,0	11	5,2	13	3,4	2,6	3,2	2	2,0	7	2,9	39,9	10,7	9	·	2	24	·	1	·	3	15	14	10	1	–	1,3	·
III	·	·	·	·	·	·	·	·	3	5,0	3,3	5,0	5,3	5,9	4	6,8	·	5,6	53,7	10,2	14	·	·	7	·	3	3	·	22	19	17	1	1	8	·
IV	5	3,2	8	3,1	1,7	2,4	7	5,3	8	4,0	2,0	2,9	1,6	4,3	2	2,5	7	3,1	11,3	3,7	1	·	·	3	·	5	·	6	8	10	4	·	1	·	2
V	5	3,4	2	2,0	5	2,4	2	6,0	1,3	3,8	1,5	2,5	2,6	3,8	1,2	3,4	1,3	2,9	107,2	20,7	6	·	·	·	·	·	·	·	15	18	15	5	–	·	3
VI	1	1,0	6	2,7	4	2,8	8,5	3,4	8	5,1	2,0,5	3,0	1,8	2,8	7	2,6	1,7	2,6	63,0	15,0	13	·	·	·	4	·	·	2	6	15	11	1	–	·	8
VII	3	2,7	1	5,0	1	1,0	3	5,0	8	4,6	3,5	3,2	2,3	2,5	1,3	2,5	6	2,9	122,8	39,7	30	·	·	·	6	·	·	2	8	13	12	4	·	·	6
VIII	3	3,3	3	3,3	4	2,0	2	2,0	5	5,0	3,0	3,9	3,1	3,6	4	4,0	1,1	3,2	95,9	25,6	12	·	·	·	6	·	·	3	10	12	9	4	·	·	3
IX	4	3,0	2	2,5	1,3	2,5	1	3,0	8	4,6	2,4	3,4	2,3	3,6	2	2,5	1,3	2,9	18,3	4,6	6	·	·	·	6	·	·	1,1	6	1,1	6	·	1	·	3
X	3	2,7	2	2,5	1,5	3,3	2,7	5,8	1,1	4,9	1,1	3,0	6	5,2	6	2,8	1,2	3,8	43,6	19,5	30	·	·	·	·	2	1	7	8	9	8	1	5	·	·
XI	3	2,0	1	1,0	9	2,7	1,1	4,1	1,2	6,0	1,3	2,6	2,5	3,3	8	2,5	8	3,2	67,8	22,2	4	·	·	1,0	·	1	·	1	16	13	11	1	7	7	·
XII	6	4,3	1	2,0	8	2,4	1	3,0	1,1	6,0	1,4	5,0	2,5	4,1	1,9	4,4	8	4,0	117,5	40,6	11	10	18	25	·	4	·	1	18	17	13	3	5,4	2,5	·
Rok	3,4	2,5	4,0	2,3	1,1,0	2,1	72,5	3,8	1,16,5	5,0	2,4,0	3,4	2,8,7	3,7	8,4	3,3	1,1,1	3,3	757,9	40,6	11.XII	22	36	98	22	20	5	41	146	161	122	21	–	8,2	2,5

Babia Góra

$H_s = 1180\ m$ $h_w = 17{,}5\ m$

I	·	·	·	·	6	1,8	4	3,0	2,0	3,0	1,4	3,2	3	1,7	·	·	46	1,4	34,6	11,5	4	12	26	31	·	·	·	4	10	6	6	1	9	3,1	·
II	7	2,4	3	5,3	·	·	·	·	5	2,6	·	·	10	2,7	·	·	5,9	0,9	73,5	17,0	9	1	18	28	·	·	·	6	13	12	11	1	15	2,8	·
III	1	1,0	·	·	·	·	·	·	2	3,0	4	2,9	4,2	3,0	3	4,3	41	1,7	171,5	27,1	14	·	11	25	·	1	·	1	21	19	19	6	22	3,1	·
IV	2	4,0	·	·	·	·	·	·	7	2,0	·	·	1,9	2,2	·	·	6,2	0,7	35,5	14,2	18	·	·	5	·	·	·	1,3	7	6	6	1	10	8	1
V	3	1,7	2	1,5	·	·	3	2,3	1,0	2,6	3	2,3	1,9	2,2	7	1,7	46	1,1	124,7	22,3	6	·	·	3	·	·	·	1	14	17	16	4	20	·	·
VI	·	·	·	·	2	1,5	·	·	1,3	2,9	1,2	1,8	1,3,5	1,6	6,5	1,6	43	1,1	164,2	41,8	11	·	·	·	·	·	·	1	11	15	15	4	13	·	9
VII	4	1,2	·	·	1	2,0	·	·	4	2,5	7	1,9	2,0	1,9	4	2,0	53	0,8	189,4	36,3	28	·	·	·	·	·	·	3	12	14	14	8	13	·	2
VIII	2	1,0	·	·	·	·	4	3,5	8	3,7	6	3,2	2,8	2,5	5	1,8	40	1,6	126,7	35,5	12	·	·	·	1	·	·	2	11	11	11	4	12	·	2
IX	·	·	1	4,0	·	·	2	4,0	9	3,4	9	2,8	1,9	2,2	1	4,0	49	1,3	26,9	6,4	6	·	·	·	·	·	·	9	6	8	6	·	8	·	·
X	1	2,0	2	3,0	3	1,7	11	2,7	1,2	5,0	6	2,7	2	2,0	3	1,7	53	1,4	41,5	19,3	30	·	·	·	·	·	·	3	8	7	7	1	8	·	·
XI	·	·	·	·	1	2,0	4	3,0	2,6	3,3	1,0	3,3	6	1,8	·	·	43	1,6	128,2	40,4	4	1	8	17	·	·	·	1	18	12	12	4	18	1,0	·
XII	·	·	·	·	·	·	0,5	2,0	1,4,5	3,4	8	3,1	5	5,2	8	2,2	57	1,2	173,4	47,3	6	15	18	26	·	·	·	2	19	12	11	6	11	2,5	·
Rok	2,0	1,1	8	1,2	1,3	0,8	2,8,5	1,7	1,3,0,5	3,1	7,9	2,2	1,8,6,5	2,2	3,7,5	1,6	5,9,2	1,2	1,2,9,0,1	47,3	6.XII	29	8,1	1,3,5	1	1	·	4,6	1,5,0	1,3,9	1,3,4	4,0	1,5,9	1,3,3	1,4,2

Kamienica — φ = 49°35' — λ = 20°21' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnie				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.7	-9.4	9.2	4	-20.8	27	-6.5	-0.8	-5.0	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.1	5.3	6.0
II	–	–	–	–	4.8	-3.6	11.6	18	-15.8	6	-2.0	3.5	0.0	0.4	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.0	6.9	7.2
III	–	–	–	–	9.6	1.1	19.7	10	-8.4	23	2.8	7.5	4.7	4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.7	6.4	6.9
IV	–	–	–	–	16.8	2.8	24.7	7	-3.6	10	6.5	15.6	7.9	9.5	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.6	3.9	4.8
V	–	–	–	–	16.1	4.9	23.7	6	-0.4	3,15	8.9	14.3	8.6	10.1	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.5	6.3	7.0
VI	–	–	–	–	22.8	9.1	31.8	27	3.7	17	14.6	20.5	14.3	15.9	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.6	6.2	5.8
VII	–	–	–	–	21.4	8.5	31.3	4	2.5	7	13.7	19.7	13.3	15.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.9	6.3	6.2
VIII	–	–	–	–	22.2	9.3	33.3	11	4.1	31	13.3	20.5	14.2	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.0	4.3	5.3
IX	–	–	–	–	21.7	5.9	30.2	17	-3.2	23	8.9	20.5	11.4	13.0	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.5	3.4	4.3
X	–	–	–	–	16.0	4.0	21.1	20	-0.8	22	5.9	15.3	7.9	9.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.3	4.2	5.1
XI	–	–	–	–	7.5	-0.4	15.6	3	-9.7	21	1.1	6.4	2.2	3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.6	6.7	6.9
XII	–	–	–	–	-0.3	-9.9	17.7	2	-32.4	25	-6.4	-2.4	-5.8	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	5.9	6.4
Rok	–	–	–	–	13.3	1.9	33.3	11.VIII	-32.4	25.XII	5.1	11.7	6.1	7.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.2	5.5	6.0

Raba Wyżna — φ = 49°34' — λ = 19°53'

I	–	–	–	–	-0.1	-7.7	9.3	4	-20.2	18	-5.2	-1.5	-4.2	-3.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.1	5.1	5.4
II	–	–	–	–	4.3	-2.7	10.9	18	-12.6	6	-1.3	3.2	-0.1	0.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.0	5.9	5.9
III	–	–	–	–	8.7	0.8	18.5	10	-8.0	23	2.6	6.9	3.9	4.3	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.8	6.6	6.8
IV	–	–	–	–	16.5	4.1	23.9	7	-3.4	10	7.2	15.6	9.4	10.4	–	–	–	–	–	–	–	–	–	–	–	–	4.1	5.2	4.4	4.6
V	–	–	–	–	15.4	6.0	22.3	27	0.7	13	9.1	13.8	9.1	10.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.2	6.5	6.5
VI	–	–	–	–	21.9	10.0	30.9	27	5.5	17,21	15.0	20.4	14.9	16.3	–	–	–	–	–	–	–	–	–	–	–	–	4.1	6.3	5.3	5.2
VII	–	–	–	–	20.3	9.9	29.9	4	5.1	7	14.2	18.8	13.8	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.4	6.7	6.1
VIII	–	–	–	–	21.2	11.4	31.9	11	7.5	17	13.5	20.0	14.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.5	4.3	4.9
IX	–	–	–	–	21.0	8.0	28.9	17	0.0	23	11.0	20.3	12.6	14.1	–	–	–	–	–	–	–	–	–	–	–	–	3.9	4.2	4.0	4.0
X	–	–	–	–	15.9	4.8	20.7	8	0.9	22	7.0	15.2	8.9	10.0	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.0	3.6	4.8
XI	–	–	–	–	6.7	0.2	13.7	3	-8.5	21	1.9	5.5	2.5	3.1	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.6	6.6	6.7
XII	–	–	–	–	-0.8	-8.2	18.0	5	-25.4	25	-5.7	-2.6	-4.7	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.3	6.2	6.3
Rok	–	–	–	–	12.6	3.0	31.9	11.VIII	-25.4	25.XII	5.8	11.3	6.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.8	5.4	5.6

Iwonicz-Zdrój — φ = 49°34' — λ = 21°48'

I	971.3	990.0	954.4	1022.2	-1.7	-7.5	9.8	4	-22.2	18	-5.3	-3.3	-4.6	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.1	4.5	5.7
II	974.1	987.6	945.6	1024.4	1.9	-2.1	6.3	18	-7.0	6	-0.9	1.1	-0.5	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	6.3	7.3
III	970.1	985.6	949.8	1019.2	8.5	1.6	16.9	10	-5.4	23	3.1	6.8	4.6	4.8	6.9	7.4	7.2	7.2	8.9	7.5	8.4	8.3	0.9	2.9	1.5	1.8	7.4	7.9	5.5	6.9
IV	965.4	972.8	958.0	1013.2	16.5	4.8	23.5	15	-3.5	10	8.4	15.3	9.5	10.7	9.2	10.3	9.8	9.8	8.1	5.9	8.2	7.4	2.2	7.6	2.4	4.1	4.7	5.6	3.7	4.7
V	964.8	972.4	951.8	1012.5	16.1	6.3	23.0	29	2.0	13	9.7	14.3	9.6	10.8	10.9	11.4	11.2	11.2	9.0	7.1	9.3	8.5	1.3	5.5	1.0	2.6	7.6	7.3	5.6	6.8
VI	968.7	981.0	959.4	1015.6	23.0	11.3	29.8	27	6.3	21	16.0	21.3	15.2	16.9	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.2	4.8	5.3
VII	968.0	978.3	955.0	1015.0	21.6	10.9	30.7	4	5.5	7	15.0	20.0	14.0	15.8	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.7	6.0	6.3
VIII	970.2	981.8	960.4	1017.4	22.1	11.6	32.0	11	6.3	31	14.5	20.6	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.0	4.4	5.3
IX	972.5	982.5	962.0	1020.2	20.2	9.3	27.7	17	0.4	23	11.6	19.2	12.6	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.6	3.0	4.0
X	972.2	983.3	952.2	1020.4	15.3	7.1	23.4	20	2.3	11,22	8.6	14.7	10.1	10.9	9.7	11.1	10.5	10.7	8.7	6.7	8.5	8.0	1.6	6.0	2.0	3.2	5.2	4.7	3.4	4.4
XI	966.8	986.3	956.3	1015.8	7.0	1.9	15.6	7	-6.9	21	3.6	5.9	4.3	4.5	7.5	8.0	7.8	7.8	9.3	8.3	9.1	8.9	0.6	1.7	0.8	1.0	7.9	7.9	6.7	7.5
XII	966.7	989.2	953.4	1017.2	-1.0	-6.8	10.9	5,6	-24.4	25	-3.9	-2.5	-3.6	-3.4	4.7	4.8	4.9	4.8	8.9	8.3	9.0	8.7	0.6	1.0	0.6	0.7	7.9	7.1	7.0	7.3
Rok	969.2	990.0	945.6	1017.8	12.5	4.0	32.0	11.VIII	-24.4	25.XII	6.7	11.1	7.2	8.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.4	5.1	6.0

Sanok — φ = 49°34' — λ = 22°12'

I	–	–	–	–	-0.3	-8.9	10.7	4	-26.7	27	-6.0	-1.6	-4.8	-4.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.0	7.4	7.4
II	–	–	–	–	3.7	-1.4	11.5	18	-4.9	5	-0.4	2.6	0.5	0.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.7	8.1
III	–	–	–	–	9.5	1.2	17.6	10	-5.4	23	3.3	7.3	4.8	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	9.0	7.8	8.5
IV	–	–	–	–	17.7	3.5	24.6	8	-5.4	10	7.1	16.0	9.8	10.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	17.6	5.7	25.8	29	1.5	20	9.4	15.6	10.3	11.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	24.4	10.9	30.2	27	5.9	21	15.4	21.9	15.6	17.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	23.0	10.3	30.6	3,4	5.6	7	14.1	20.9	14.5	16.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	23.7	10.8	32.8	11	3.8	31	14.3	21.6	15.5	16.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	22.1	7.4	30.0	17	-2.0	23	10.5	20.4	12.3	13.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	17.2	-	26.0	20	–	–	7.0	16.1	9.3	10.4	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.2	4.4	5.5
XI	–	–	–	–	8.8	-	16.3	7	–	–	3.7	7.4	4.8	5.8	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.9	8.3	8.7
XII	–	–	–	–	0.1	-	13.1	5	–	–	-4.5	-1.5	-3.7	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	14.0	-	32.8	11.VIII	–	–	6.2	12.2	7.4	8.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Kamienica

$H_s = 460\ m$ $h_w = 21\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °D, %D																		OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T			Wiatr v			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min<-10°	Max<0°	Min<0°	Max>25°	v>10	v>15	●	●	R≥0.1	R≥1.0	R≥10.0	≡	⊡	R≥50
I	2	1.5	7.5	2.1	1	2.0	1.5	2.7	3.5	2.6	13.5	3.0	12	3.2	22	2.2	30	1.7	127	43	5	12	13	30	·	2	·	4	9	8	5	·	3	23	·
II	3	1.5	5.5	1.5	1.5	1.7	4	1.2	8	1.0	1.5	1.0	2.5	3.8	44	2.0	14	1.5	336	100	9	1	·	22	·	·	·	1	14	11	8	1	1	8	·
III	·	·	·	·	·	·	·	·	2	1.5	12.5	5.2	29.5	4.2	40	3.8	9	3.7	381	88	14	·	·	9	·	4	2	2	11	15	13	·	·	4	·
IV	2	2.0	7	2.8	4.5	3.0	7	3.1	1	4.0	5.5	7.4	15	4.0	9	2.5	39	2.1	139	64	8	·	·	3	·	3	·	7	4	8	4	·	·	·	1
V	5.5	2.8	2.5	3.4	1	3.5	3.5	4.6	2.5	2.4	5.5	3.0	20.5	3.3	20	2.3	32	1.9	963	220	6	·	·	2	·	·	·	·	13	17	14	3	1	·	6
VI	1.5	3.0	2.5	2.6	5.5	2.5	5	3.4	2.5	2.8	8	2.1	21.5	2.9	14.5	1.9	29	1.7	789	166	12	·	·	·	6	·	·	·	8	12	11	4	·	·	10
VII	3	2.0	2.5	1.8	2.5	2.0	2.5	1.6	4	2.6	1.5	3.0	18.5	2.4	16	2.6	29	1.8	962	297	29	·	·	·	8	1	1	2	7	14	11	3	·	·	6
VIII	2.5	2.8	1.5	2.3	3.5	3.1	4.5	2.4	1.5	1.7	6.5	2.8	13.5	3.7	24.5	3.2	35	2.0	676	178	3	·	·	·	8	2	1	4	4	8	7	3	·	·	5
IX	3	4.0	2	2.5	3	3.2	3	2.3	5.5	2.2	8.5	4.7	11	3.6	11	2.6	43	1.7	354	271	29	·	·	3	7	1	·	12	5	8	5	1	5	·	2
X	·	·	4	2.5	3.5	4.3	2.0	3.8	5.5	3.0	6	1.8	16	2.7	4	2.2	34	2.0	288	170	30	·	·	3	·	1	·	6	6	7	5	1	2	·	·
XI	4.5	1.8	3	2.2	1	2.5	3	2.2	4.5	1.9	6.5	2.2	18	2.8	23.5	2.1	26	1.6	544	160	4	·	·	13	·	1	·	3	13	17	10	1	3	6	·
XII	2.5	1.8	1	1.0	1	2.0	1	3.0	3	4.5	10	4.7	13.5	3.3	32	2.4	29	2.1	1069	393	11	15	17	27	·	2	·	3	12	15	9	4	1	25	·
Rok	29.5	1.9	39	2.1	28	2.5	55	2.5	43.5	2.5	99	3.4	191.5	3.3	260.5	2.5	349	2.0	6628	393	11.XII	28	30	112	29	17	4	44	106	140	102	21	16	68	30

Raba Wyżna

$H_s = 600\ m$ $h_w = 16\ m$

I	1	1.0	8	1.0	1	1.0	3.2	1.2	1.6	2.2	1.0	2.8	·	·	6	1.3	19	1.3	209	55	4	1.0	1.4	2.8	·	·	·	7	8	7	5	·	·	2.9	·
II	·	·	·	·	3	1.0	3.4	1.3	5.5	1.9	6.5	1.5	2	4.0	7	1.0	2.6	0.9	349	8.0	20	1	2	2.1	·	·	·	6	1.0	11	9	·	5	1.7	·
III	2	1.0	1	1.0	·	·	9.5	1.0	1.1	2.3	2.4.5	2.0	7	1.9	2.4	2.0	1.4	1.6	637	165	14	·	·	9	·	·	·	5	1.6	19	15	1	1	6	·
IV	1	1.0	1.3	1.3	8	1.0	2.1.5	1.3	1.9.5	1.5	8	2.5	1	1.0	8	1.2	1.0	1.3	156	3.5	2	·	·	3	·	·	·	8	5	7	7	·	·	·	2
V	8	1.0	1.0	1.0	1	1.0	1.1.5	1.2	1.3.5	1.3	8	1.8	9	1.0	1.8	1.3	1.4	1.0	973	350	6	·	·	·	·	·	·	2	1.0	1.8	1.4	2	2	·	4
VI	8	1.2	3	1.0	3	1.0	1.8	1.1	9.5	1.1	1.0.5	1.7	1	1.0	1.0	1.2	2.7	0.9	1219	390	9	·	·	·	4	·	·	4	7	1.2	1.2	3	·	·	1.1
VII	1	1.0	2	1.0	4	1.0	1.0	1.0	1.2	1.4	2.2	1.5	4	1.5	1.4	1.0	2.4	0.9	1242	290	29	·	·	·	7	·	·	4	8	1.6	1.5	5	1	·	5
VIII	3.5	1.0	1.5	1.0	·	·	1.3.5	1.0	1.0.5	1.7	1.5	1.9	6	1.7	1.4	1.3	2.9	1.0	579	193	12	·	·	·	6	·	·	8	3	1.1	8	2	1	·	5
IX	2.5	1.0	5.5	1.0	2	1.0	2.0	1.1	1.2	1.3	9	1.7	3	2.3	5	1.4	3.1	0.9	100	4.0	9	·	·	·	5	·	·	1.1	3	6	5	·	3	·	2
X	2	1.0	6	1.0	4	1.0	2.9	1.3	6	1.0	4	2.0	·	·	2	1.0	4.0	0.7	267	150	30	·	·	·	·	·	·	6	6	7	3	1	5	·	·
XI	3	1.0	1	1.0	1	1.0	2.4	1.1	7.5	1.7	1.0.5	2.0	3	1.0	8	1.0	3.2	0.8	768	320	4	·	2	1.3	·	·	·	5	1.6	1.1	9	2	6	8	·
XII	·	·	·	·	·	·	2.0	1.4	1.2.5	2.2	8.5	5.2	1	3.0	1.8	1.1	3.3	1.3	1128	290	11	1.2	1.8	2.6	·	·	·	6	1.3	1.5	1.2	4	·	2.5	·
Rok	3.2	0.8	5.1	0.9	2.7	0.8	2.4.3	1.2	1.3.5.5	1.6	1.3.6.5	2.2	3.7	1.3	1.3.4	1.2	2.9.9	1.0	7628	390	9.VI	2.3	3.6	1.0.0	2.2	·	·	7.2	1.0.5	1.4.0	1.1.4	2.0	2.4	8.5	2.9

Iwonicz-Zdrój

$H_s = 410\ m$ $H_b = 403,3\ m$ $h_w = 16,2\ m$

I	3.5	2.4	1	1.0	·	·	·	·	3.9	6.9	1.2	3.5	2.5	2.2	4	2.0	3.1	3.6	2.2.5	1.1.0	5	1.1	1.7	2.8	·	6	3	5	9	9	6	1	2	2.3	·
II	·	·	·	·	·	·	0.5	3.0	2.8.5	5.0	1.6	3.7	·	·	4	2.5	3.5	2.5	1.5.8	5.1	1.0	·	4	2.3	·	1	1	2	1.4	9	5	·	7	1.2	·
III	0.5	2.0	·	·	·	·	·	·	1.6.5	3.0	1.4	2.3	1.4.5	2.3	2.3.5	2.9	2.4	2.0	3.8.1	6.4	1.9	·	·	1.0	·	·	·	2	1.3	1.6	1.3	·	2	4	·
IV	4.5	1.8	9.5	3.8	4.5	1.6	1	1.5	1.7.5	2.7	1.4.5	3.2	2	1.2	2.5	4.2	3.4	1.8	1.4.0	5.6	1.6	·	·	3	·	1	·	7	4	7	6	·	·	·	3
V	1.0	1.2	3.5	1.7	·	·	1	5.0	9	3.8	5	1.9	4.5	1.7	8	1.9	5.2	1.0	7.7.1	1.6.1	7	·	·	·	·	·	·	2	1.1	1.5	1.4	2	3	·	4
VI	1.0	1.8	2.5	2.2	4	1.8	1	1.5	1.2	2.4	1.4.5	3.1	2.5	1.8	5.5	1.6	3.8	1.3	7.8.5	1.7.8	6	·	·	·	7	·	·	2	6	1.5	1.2	2	1	·	6
VII	8	1.4	·	·	·	·	1	3.0	1.2	4.2	8	2.8	4	1.0	1.0	1.8	5.0	1.2	1.1.0.1	4.2.2	2.9	·	·	·	7	1	·	2	1.1	1.5	1.0	3	1	·	3
VIII	9	1.6	1	2.0	·	·	·	·	1.7.5	2.8	1.4.5	2.1	2.5	2.2	6.5	2.5	4.2	1.3	4.9.4	1.1.8	1.3	·	·	·	7	·	·	3	6	1.2	1.0	2	1	·	3
IX	4.5	1.6	5	2.5	·	·	1	5.0	1.6	3.0	8.5	1.8	3.5	1.7	4.5	2.1	4.7	1.2	2.8.9	6.8	2.6	·	·	·	6	·	·	1.2	4	1.1	8	·	4	·	2
X	3	1.2	5	2.9	2.5	3.0	3.5	2.1	3.7	4.5	8	3.0	0.5	1.0	4.5	1.8	2.9	2.5	3.3.4	1.9.7	3.0	·	·	·	·	2	·	1.2	8	6	6	1	6	·	·
XI	4	1.3	2.5	2.2	1	1.0	3.5	2.4	2.6	5.7	1.6	2.6	3	1.2	6	2.2	2.8	2.5	4.0.6	9.8	7	·	2	9	·	2	·	3	1.8	1.4	9	·	6	3	·
XII	1.1	2.0	0.5	2.0	1	1.0	·	·	3.0	4.9	3	6.7	2	1.8	1.0.5	2.2	3.5	2.3	6.8.4	1.6.7	7	1.0	1.8	2.5	·	3	·	3	1.8	1.5	1.2	3	3	2.4	·
Rok	6.8	1.5	3.0.5	1.7	1.3	0.7	1.2.5	2.0	2.6.1	4.1	1.3.4	3.1	4.1.5	1.5	8.9.5	2.3	4.4.5	1.9	5.7.7.8	4.2.2	2.9.VII	2.1	4.1	9.8	2.7	1.6	4	5.5	1.2.2	1.4.4	1.1.1	1.4	3.6	6.6	2.1

Sanok

$H_s = 314\ m$ $h_w = 16\ m$

I	7	3.6	·	·	6	8.3	1.5	5.5	1.7	6.2	·	·	7	5.3	2	2.0	3.9	3.4	1.6.0	5.7	5	1.2	1.5	2.7	·	2	2	–	–	1.0	6	·	1	2.3	–
II	2	2.0	·	·	5	3.4	9	3.2	1.9	5.3	1	3.0	7	4.1	1	5.0	4.0	2.4	1.1.5	3.8	1.3	·	1	1.7	·	·	·	–	–	1.2	4	·	·	6	–
III	·	·	·	·	1	3.0	1	3.0	1.2	5.7	1	7.0	3.5	8.8	4	8.8	3.9	4.6	2.2.3	5.3	1.9	·	·	9	·	7	6	–	–	1.3	7	·	2	2	–
IV	2	3.0	9	7.1	1.3	4.5	7	3.0	1.0	1.0.0	1	5.0	6	6.0	2	7.0	4.0	3.6	8.1	3.0	3	·	·	4	·	5	4	–	–	6	4	·	·	·	–
V	8	4.0	3	3.7	3	3.0	1.1	4.1	6	7.5	·	·	1.8	5.4	5	3.4	3.9	2.8	3.7.2	1.0.0	1.4	·	·	·	1	3	3	–	–	1.0	9	1	·	·	–
VI	1	3.0	4	4.0	·	·	1.5	3.1	7	4.6	·	·	1.1	3.7	2	5.0	5.0	1.7	8.4.7	2.1.1	9	·	·	·	1.1	1	·	–	–	1.4	1.3	4	1	·	–
VII	·	·	6	2.3	4	4.0	1.3	3.6	9	7.3	2	5.0	1.5	4.9	2	3.0	4.2	2.5	9.4.4	3.2.2	2.9	·	·	·	9	1	1	–	–	1.1	9	4	·	·	–
VIII	4	3.0	·	·	2	3.0	7	3.9	1.4	5.3	·	·	1.3	5.2	2	3.0	5.1	2.1	4.9.0	1.8.0	3	·	·	·	1.1	·	·	–	–	1.2	8	1	·	·	–
IX	2	2.0	5	3.4	4	3.0	9	3.2	1.2.5	5.6	1.5	5.7	1.1	4.5	1	3.0	4.4	2.1	1.8.7	8.6	2.6	·	·	2	9	·	·	–	–	7	5	·	1	·	–
X	·	·	4	5.5	7	3.9	2.3	4.7	1.5	6.1	·	·	7	5.3	2	4.0	3.5	3.2	2.0.2	1.2.3	3.0	–	–	–	1	1	1	–	–	5	4	1	·	·	–
XI	·	·	1	3.0	3	5.7	7	5.0	1.8	4.7	·	·	1.4	5.4	6	3.7	4.1	2.6	3.1.2	9.9	2.5	–	–	–	·	·	·	–	–	1.1	8	·	·	·	–
XII	1.0	4.4	2	6.0	3	3.7	9	3.4	1.9	9.7	·	·	1.0	6.4	9	4.5	3.1	4.2	5.3.9	1.1.2	7	–	1.5	–	·	4	3	–	–	1.5	1.1	2	1	2.5	–
Rok	3.6	2.1	3.4	2.9	5.1	3.8	1.2.6	3.8	1.5.8.5	6.5	6.5	2.1	1.5.4	5.4	3.8	4.4	4.9.1	2.9	4.4.7.2	3.2.2	2.9.VII	–	3.1	–	4.2	2.4	2.0	–	–	1.2.6	8.8	1.3	6	5.6	–

Starćowa

$\varphi = 49°33'$ $\lambda = 19°32'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.0	-7.8	6.4	4	-18.4	18	-5.9	-2.6	-5.1	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.0	5.8	6.1
II	–	–	–	–	2.3	-4.4	10.8	18	-13.3	6	-3.3	1.2	-2.2	-1.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	6.0	6.0
III	–	–	–	–	5.5	-1.2	15.0	18	-9.4	23	0.1	4.0	1.6	1.8	–	–	–	–	–	–	–	–	–	–	–	–	8.0	7.7	7.3	7.7
IV	–	–	–	–	13.7	2.7	20.8	7	-3.3	10	6.6	12.6	5.7	7.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.5	4.4	5.0
V	–	–	–	–	12.4	3.9	20.6	27	-1.5	13	7.0	11.2	6.6	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.7	6.8	7.2
VI	–	–	–	–	19.4	8.9	26.2	27	4.5	16	13.2	17.6	12.1	13.8	–	–	–	–	–	–	–	–	–	–	–	–	5.1	7.1	5.6	5.9
VII	–	–	–	–	17.4	8.0	26.6	3	3.7	6	11.7	16.3	11.1	12.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.1	6.7	6.6
VIII	–	–	–	–	19.0	9.4	28.4	11	3.9	14	12.0	17.7	12.3	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.0	4.9	5.5
IX	–	–	–	–	18.9	8.4	26.3	17	2.7	22	10.4	17.8	11.4	12.8	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.5	4.0	4.2
X	–	–	–	–	13.5	5.2	18.6	11	1.2	22	7.2	12.4	7.8	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.9	5.1	5.7
XI	–	–	–	–	5.8	-0.6	11.1	3	-9.7	21	1.1	4.1	1.6	2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.0	6.4	7.0
XII	–	–	–	–	-1.0	-8.3	14.7	5	-21.5	16	-5.6	-3.1	-5.1	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.6	7.1	6.9
Rok	–	–	–	–	10.5	2.0	28.4	11.VIII	-21.5	16.XII	4.5	9.1	4.8	5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.4	5.8	6.1

Obidowa

$\varphi = 49°33'$ $\lambda = 19°58'$

I	–	–	–	–	-2.3	-8.5	6.8	4	-18.8	18	-6.8	-4.1	-5.3	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	6.2	6.7
II	–	–	–	–	1.3	-4.2	10.1	18	-13.1	6	-3.1	0.0	-1.2	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.7	6.0	6.8
III	–	–	–	–	5.5	-0.3	16.0	10	-7.2	23	0.8	4.0	2.6	2.5	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.3	7.4	8.3
IV	–	–	–	–	13.9	3.9	21.3	15	-1.9	10	5.6	12.6	8.3	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.5	4.9	5.9
V	–	–	–	–	12.5	5.0	19.2	27	-1.1	12	6.3	11.2	8.1	8.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.8	7.8	8.2
VI	–	–	–	–	19.3	10.2	27.9	27	5.8	17	12.4	18.1	14.2	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.3	6.7	6.5
VII	–	–	–	–	17.8	9.6	26.3	3,4	6.2	6	11.4	16.1	12.9	13.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.3	8.0	7.3
VIII	–	–	–	–	18.7	10.2	29.1	11	4.8	18	11.8	17.1	13.7	14.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.5	6.2	6.7
IX	–	–	–	–	18.3	8.9	25.9	17	1.9	22	9.9	17.1	12.8	13.2	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.3	3.8	4.7
X	–	–	–	–	13.6	5.6	18.5	8	1.2	22	6.9	12.4	8.6	9.1	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.1	4.8	6.0
XI	–	–	–	–	5.1	-0.8	11.1	3,7	-9.7	21	1.3	3.6	1.7	2.1	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.8	7.0	7.7
XII	–	–	–	–	-2.7	-9.3	12.6	5	-22.9	25	-6.4	-4.8	-6.1	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.1	7.0	7.1
Rok	–	–	–	–	10.1	2.5	29.1	11.VIII	-22.9	25.XII	4.2	8.6	5.9	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.1	6.3	6.8

Turbacz

$\varphi = 49°33'$ $\lambda = 20°07'$

I	–	–	–	–	-2.8	-9.5	5.1	4	-22.5	18	-6.9	-4.1	-6.6	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.7	5.7	5.9
II	–	–	–	–	0.6	-5.2	8.5	18	-13.3	6	-3.3	-0.4	-2.9	-2.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.0	6.3
III	–	–	–	–	2.1	-3.5	14.1	10	-10.3	23	-2.1	0.6	-0.8	-0.8	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.9	7.2	8.1
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	9.3	1.8	16.8	6	-3.3	13	4.4	8.1	4.5	5.4	–	–	–	–	–	–	–	–	–	–	–	–	8.2	8.2	7.2	7.9
VI	–	–	–	–	16.7	7.7	25.0	27	3.4	29	11.1	14.6	10.7	11.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.6	7.2	6.5
VII	–	–	–	–	15.5	5.8	24.4	4	2.0	7	9.5	13.9	9.8	10.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.6	7.3	6.8
VIII	–	–	–	–	15.7	–	28.4	11	–	–	10.2	14.4	10.6	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.9	4.5	4.8	5.1
IX	–	–	–	–	16.0	6.5	23.9	17	2.5	11	10.0	14.8	10.6	11.5	–	–	–	–	–	–	–	–	–	–	–	–	4.1	4.5	3.3	4.0
X	–	–	–	–	10.9	3.8	15.3	11,28	0.0	14	5.6	10.0	5.9	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.4	4.4	5.1
XI	–	–	–	–	4.3	-2.3	11.7	23	-11.6	21	0.2	3.1	0.4	1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.3	6.7	7.2
XII	–	–	–	–	-2.8	-10.1	12.7	5	-24.9	16	-7.0	-4.4	-6.8	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	6.4	6.5
Rok	–	–	–	–	–	–	28.4	11.VIII	-24.9	16.XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Łącko

$\varphi = 49°33'$ $\lambda = 20°26'$

I	–	–	–	–	0.9	-7.4	10.4	4	-19.2	27	-4.8	-0.5	-3.4	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	5.7	4.7	5.8
II	–	–	–	–	5.0	-2.0	11.0	18	-9.8	6	-0.7	4.1	1.1	1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	5.5	6.3	6.4
III	–	–	–	–	9.9	2.1	19.8	18	-4.7	23	3.8	8.4	5.5	5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.0	5.9	6.8
IV	–	–	–	–	17.5	3.1	25.0	15	-2.7	10	6.3	16.4	9.6	10.5	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.5	4.1	4.7
V	–	–	–	–	16.3	6.0	24.2	6	1.6	15	9.1	15.1	9.7	10.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	8.1	6.3	7.1
VI	–	–	–	–	23.1	10.2	31.0	26	4.1	21	14.0	21.0	15.2	16.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.1	5.7	5.6
VII	–	–	–	–	21.6	9.7	31.7	4	4.4	7	13.7	20.2	14.2	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.5	7.0	6.9	6.5
VIII	–	–	–	–	22.6	10.5	33.9	11	5.4	31	13.6	21.2	14.9	16.2	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.7	5.1	5.2
IX	–	–	–	–	21.8	7.0	30.9	18	-3.2	23	9.6	20.9	11.8	13.5	–	–	–	–	–	–	–	–	–	–	–	–	4.7	3.5	3.2	3.8
X	–	–	–	–	16.5	4.5	22.2	20	-0.2	4	6.3	15.8	9.5	10.3	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.0	3.9	4.9
XI	–	–	–	–	8.3	0.1	16.4	3	-8.0	24	1.8	7.1	3.0	3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.6	6.4	6.7	6.9
XII	–	–	–	–	0.3	-9.4	17.8	2	-29.0	25	-5.3	-4.6	-4.7	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.1	6.2	6.7
Rok	–	–	–	–	13.6	2.9	33.9	11.VIII	-29.0	25.XII	5.6	12.3	7.2	8.1	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.0	5.4	5.9

Stańcowa $H_s = 850 m$ $h_w = 18.5 m$ 1961

MIESIĄC	ROZKŁAD WIATRU $^nD, ^vmD$																		OPAD R			LICZBA DNI (n)													
	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Temperatura T: Min < -10°	Max < 0°	Min ≤ 0°	Max > 25°	Wiatr v > 10	v > 15	◉	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	▬	⊞	R
I	.	.	11	2.1	11	2.1	2	2.0	.	.	38	2.7	12	2.4	19	4.6	.	2.3	32.2	12.2	4	9	20	30	.	1	1	5	13	11	6	1	.	31	
II	10	1.6	1	1.0	.	.	.	.	.	.	18	2.2	41	1.4	13	2.3	1	1.7	74.0	23.7	9	1	7	28	.	.	.	6	12	16	12	1	1	28	.
III	2	1.0	.	.	.	.	.	.	.	.	18	2.4	48	2.8	20	4.2	5	2.8	156.6	33.0	14	.	4	19	.	3	.	1	20	22	20	5	2	22	.
IV	11	1.0	12	1.8	11	2.4	2	2.0	1	5.0	28	2.5	12	2.1	10	4.4	3	2.0	43.3	11.0	26	.	.	3	.		.	6	4	10	8	2	2	2	3
V	22	1.5	6	1.8	8	1.4	.	.	1	3.0	23	2.1	14	1.7	13	4.8	6	1.7	132.9	30.2	6	.	.	3	.	.	.		14	18	13	6		.	6
VI	12	1.8	4	1.8	3	1.7	1	1.0	5	1.6	34	1.5	16	1.7	1	1.0	14	1.3	177.8	36.7	4	.	.		2	.	.	2	10	16	13	6	1		12
VII	1	3.0	12	1.1	1	1.0	.	.	3	1.3	45	2.4	18	2.1	11	1.5	2	2.0	171.8	30.8	28	.	.	.	2	.	.	2	8	17	16	6	.	.	5
VIII	9	1.8	3	1.3	1	3.0	4	2.5	4	3.0	39	2.7	23	1.3	5	2.6	5	2.1	94.2	26.3	23	.		.	6	1	.	6	8	17	11	4		.	3
IX	9	1.0	18	1.2	4	1.2	.	.	3	1.0	26	2.3	18	1.4	6	1.2	6	1.5	20.7	6.3	9	.	.		1		.	13	7	10	7	.		.	1
X	3	1.0	14	1.3	6	2.5	3	1.0	2	1.5	28	2.3	13	1.9	13	1.5	11	1.6	30.7	11.2	14	.	.	.		.	.	5	8	10	8	2	2	.	
XI	3	1.3	.	.	3	1.0	.	.	.	.	24	1.6	42	1.5	8	2.1	10	1.4	76.6	16.9	4	.	3	17	.	.		2	13	17	12	2	5	8	
XII	14	2.8	16	1.8	4	2.5	1	1.0	.	.	25	2.7	19	1.9	8	3.0	6	2.2	153.7	52.3	11	13	17	25	.	.		3	14	22	15	5	.	25	
Rok	96	1.5	97	1.3	52	1.6	13	0.8	19	1.4	346	2.3	276	1.8	127	2.0	69	1.9	1164.5	52.3	11.XII	23	51	125	11	5	1	51	131	186	141	40	13	116	30

Obidowa $H_s = 800 m$ $h_w = 20.5 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min ≤ 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	▬	⊞	R
I	43	3.1				.	2	2.0	47	3.7	10	9.0	1	4.0	1	2.0	19	3.4	15.1	4.3	5	12	25	30	.	2	2	4	15	10	5	.	6	30	–
II	13	2.9	.		1	2.0	1.5	2.0	40.5	2.9	8	3.8	3	2.7	3	2.0	14	2.5	31.6	6.3	8	2	8	27	.	.	.	4	14	15	11	.	10	23	–
III	10.5	2.6	.	.	.	.	.	.	40.5	3.3	25.5	3.9	24	3.4	6.5	3.8	16	2.9	49.0	17.8	14	.	5	16	.	.	.	1	20	20	14	1	3	13	–
IV	12	2.5	2	3.0	8	2.9	16	2.5	25.5	2.5	9.5	4.4	2	3.0	3	3.3	12	2.5	12.9	4.8	8	.	.	3	.	.	.	7	12	7	4	.	3	.	–
V	22	2.4	2	2.0	3	2.3	10.5	2.0	15.5	2.5	17	3.3	6	3.0	1	2.0	16	2.2	117.7	31.3	6	.	.	1	.	.	.	1	21	20	15	2	10	.	–
VI	11	2.6	2	2.5	3	2.0	9	2.1	26.5	2.4	6.5	2.8	4	2.5	4	2.2	24	4.8	134.3	26.0	8	.		.	2	.	.	2	9	12	12	4	2	.	–
VII	11	2.5	2	2.5	4	2.0	4	2.0	17	2.5	28	3.4	6	3.2	5	2.8	16	2.4	155.3	43.1	30	.	.	.	3	.	.	2	15	16	15	5	2	.	–
VIII	9	2.4	1	2.0	1	2.0	3	2.0	30	2.7	25	3.3	2	2.0	5	2.4	17	2.3	98.9	32.0	3	.	.	.	5	.	.	2	12	11	10	4	2	.	–
IX	4	2.5		.	6	2.2	3.5	2.7	36.5	2.6	14	3.6	4	4.0	4	2.2	18	2.2	15.9	5.0	9	.	.	.	3		.	12	8	9	6	.	2	.	–
X	13	2.4	.	.	10	3.2	30	2.7	19	3.0	10	3.5	1	3.0	1	2.0	9	2.6	34.5	20.0	30	.	.	.	.		.	5	11	7	4	1	5	.	–
XI	21	2.9	.	.	2	4.0	2	2.5	40	2.9	12	7.0	5	2.8	.	.	8	3.2	47.8	14.3	4	.	5	17	.	2	2	2	19	13	10	1	8	5	–
XII	31	3.1	.	.	3	2.0	3	3.0	32.5	4.9	7.5	9.6	2	2.0	.	.	14	3.7	72.0	17.4	6	14	19	27	.	5	5	4	16	16	11	2	5	25	–
Rok	170.5	2.7	9	1.0	41	2.0	84.5	2.1	340.5	3.0	173	4.8	60	3.0	33.5	2.1	183	2.6	785.0	43.1	30.VII	28	62	121	13	9	9	46	172	156	117	20	58	96	–

Turbacz $H_s = 1308 m$ $h_w = 18 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min ≤ 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	▬	⊞	R
I	6.5	2.5	10	2.9	2	6.5	0.5	7.0	11	6.3	19.5	6.5	16	3.9	12.5	3.8	15	4.0	23.7	7.0	5	12	23	31	.	4	2	5	11	12	10	.	15	31	–
II	5	3.3	0.5	1.0	2.5	1.6	4.5	2.0	3	1.3	14.5	4.1	19	3.2	18	3.4	17	2.6	81.9	14.0	9	2	16	28	.	2	.	7	14	13	13	4	16	28	–
III	1.5	6.3	.	.	.	.	.	.	5.5	4.8	9	3.6	19	2.7	52	5.3	6	4.2	135.5	28.4	14	1	11	27	.	4	2	2	20	20	18	5	25	26	–
IV	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	27.0	11.0	8	–	–	–	–	–	–	–	–	10	7	1	–	–	–
V	17.5	2.4	3	4.0	.		2	4.2	8.5	3.1	14	2.8	11.5	2.7	18.5	2.6	18	2.2	190.9	54.0	6	.	.	10	.	1	.	.	16	22	20	6	16	.	–
VI	4.5	2.2	2	2.0	1	8.0	7	4.2	11	2.0	6.5	2.8	9.5	2.2	15.5	3.5	33	4.9	149.9	21.0	13	.	.	.	.	2	1	.	8	15	13	8	5	.	–
VII	12	3.1	3.5	2.6	1	2.0	15	4.3	8.5	4.2	16.5	2.5	12.5	2.8	21.5	2.6	16	2.4	201.5	56.0	29	.	.	.	.	2	.	1	12	13	12	5	14	.	–
VIII	7.5	3.5	.	.	2	1.0	1	2.0	7	3.7	17	3.1	21	2.9	23.5	3.4	14	2.7	121.0	30.0	12	–	.	–	2	1	.	4	6	14	13	5	15	.	–
IX	3.5	2.7	5.5	3.0	3.5	2.1	2.5	2.2	11.5	2.5	17.5	2.9	17	2.4	16	3.8	13	2.4	51.8	9.5	9	.	.	.	.	3	.	13	5	10	10		7	.	–
X	6	4.2	3.5	2.3	3.5	4.6	21.5	7.4	21.5	4.3	9	3.3	7.5	4.5	11.5	5.2	9	4.5	60.8	24.2	30	.	.	.	.	10	2	7	8	7	6	2	13	.	–
XI	10.5	4.0	.	.	0.5	1.0	6	6.2	10.5	5.9	15.5	7.4	19.5	4.3	14.5	4.1	13	4.4	90.6	38.0	4	1	8	19	.	9	2	1	17	14	12	3	20	8	–
XII	15	4.7	3	12.2	2	16.0	8	6.4	10.5	6.9	16.5	11.5	9	6.3	24	5.4	5	6.8	174.5	36.3	6	17	18	28	.	13	6	3	13	14	12	8	16	26	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	1309.1	56.0	29.VII	–	–	–	–	–	–	–	–	164	146	47	–	–	–

Łącko $H_s = 360 m$ $h_w = 16 m$

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min ≤ 0°	Max > 25°	v > 10	v > 15	◉	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	▬	⊞	R
I	3	3.3	3.5	1.7	6.5	2.2	1	1.0	17.5	2.3	13	3.7	30.5	2.0	9	1.8	9	2.1	40.8	5.6	5	8	13	28		1	1	5	7	9	4	.	.	8	
II	.	.	4	1.2	2.5	1.4	15	1.0	7	1.7	11	2.0	35	1.9	9	1.7	14	1.5	46.0	4.9	28	.	.	20	.	.	.	3	12	9	6	.	2	2	
III	1	9.0	.	.	.	.	1	1.0	15	1.0	13	2.4	52.5	2.5	22	2.4	2	2.4	32.3	7.2	14	.	.	8	.	.	.	4	13	18	10	.	.	4	
IV	3	2.0	15.5	2.3	11.5	2.1	1	3.0	4	1.8	10	2.1	22	2.6	10	2.0	13	1.9	11.5	4.2	8,19	.	.	4	.	.	.	7	5	6	3	.	.	.	1
V	11.5	1.9	5	1.7	8.5	1.8	1	1.0	6.5	1.9	4.5	1.6	36	2.0	4	1.8	16	1.5	94.5	22.7	6	.	.	.	.	.	.	.	10	14	13	2	2	.	3
VI	6.5	1.5	2.5	1.8	8	1.8	2	2.2	10	1.7	8	1.6	32.5	1.8	6.5	1.2	14	1.5	89.4	18.7	11	.	.	.	8	.	.	1	7	12	9	5	1	.	8
VII	11	1.7	4.5	1.9	6.5	1.2	.	.	3	3.3	7	2.0	32.5	2.1	17.5	2.1	11	1.8	101.2	34.4	29	.	.	.	8	1	1	3	9	13	10	2	.	.	1
VIII	5	1.4	3.5	1.3	3.5	1.0	.	.	4.5	1.4	14.5	2.2	35	2.1	11	1.5	16	1.5	104.7	30.3	3	.	.	.	7	.	.	6	4	8	6	4	1	.	2
IX	4	1.1	6	1.4	4.5	1.2	1	1.0	9	2.0	8.5	2.4	22.5	1.8	12.5	1.8	22	1.3	20.0	14.0	29	.	.	2	7	.	.	12	4	5	3	1	2	.	1
X	2.5	1.0	5.5	1.9	7.5	3.1	13.5	3.1	10	2.8	16.5	2.5	19	1.7	7.5	1.5	11	2.1	24.0	20.1	30	.	.	1	.	1	.	7	5	4	2	1	3	.	.
XI	2	1.0	2	1.0	2.5	1.0	3	1.0	9.5	1.7	12.5	2.0	25.5	1.9	6	1.7	27	1.2	57.8	22.3	4	.	.	11	.	.	.	4	14	13	9	1	5	3	
XII	4.5	2.4	2	1.5	4	1.5	.		2	1.5	11	2.7	39.5	2.8	12	1.9	18	2.0	63.0	17.3	11	14	16	26	.	2	.	4	15	11	8	2	2	24	.
Rok	54	2.2	54	1.5	65.5	1.5	25	1.2	84.5	1.9	129.5	2.3	382.5	2.1	127	1.8	173	1.7	625.2	34.4	29.VII	22	29	100	30	5	2	56	105	122	83	18	18	41	16?

Stary Sącz — φ = 49°33' — λ = 20°39' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
											Średnia																			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.2	-6.9	11.3	4	-21.0	27	-4.8	-1.1	-3.5	-3.2	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	4.1	5.3
II	–	–	–	–	4.5	-1.7	13.0	18	-10.0	6	-0.6	3.5	0.5	1.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	6.3	6.3
III	–	–	–	–	10.2	2.1	20.1	18	-4.3	23	3.7	8.3	5.3	5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.0	6.7	6.9
IV	–	–	–	–	17.7	4.1	25.3	7,15	-3.7	10	7.6	16.4	9.7	10.8	–	–	–	–	–	–	–	–	–	–	–	–	3.5	5.3	4.8	4.5
V	–	–	–	–	16.7	6.5	23.5	29	1.2	15	9.8	15.2	9.9	11.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	8.1	6.3	7.0
VI	–	–	–	–	24.5	10.7	31.3	27	4.9	17,21	14.3	22.1	15.3	16.8	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.8	3.5	4.3
VII	–	–	–	–	22.3	10.3	31.8	4	3.5	7	14.2	20.8	14.2	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.6	7.3	6.6	6.1
VIII	–	–	–	–	23.1	11.2	34.6	11	4.4	31	14.3	21.8	15.3	16.7	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.9	4.6	5.2
IX	–	–	–	–	22.3	8.1	31.6	18	-3.0	23	9.8	21.3	13.0	14.3	–	–	–	–	–	–	–	–	–	–	–	–	4.5	4.1	3.6	4.1
X	–	–	–	–	16.7	6.1	22.5	20	-0.5	22	8.3	16.1	10.5	11.4	–	–	–	–	–	–	–	–	–	–	–	–	5.2	3.8	3.2	4.1
XI	–	–	–	–	8.0	1.9	15.5	3	-5.6	21	3.5	7.1	4.2	4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.3	6.2	6.4
XII	–	–	–	–	0.2	-8.1	17.4	2	-29.1	26	-4.7	-1.2	-3.8	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.2	5.5	6.3
Rok	–	–	–	–	13.9	3.7	34.6	11.VIII	-29.1	26.XII	6.3	12.5	7.6	8.5	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.0	5.1	5.6

Rymanów-Zdrój — φ = 49°33' — λ = 21°51'

I	–	–	–	–	-1.7	-8.0	9.9	4	-23.7	27	-5.7	-3.2	-5.0	-4.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.0	6.5	6.4
II	–	–	–	–	2.0	-2.1	6.6	18	-6.4	15	-0.9	1.2	-0.4	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	8.9	1.2	16.8	10	-7.5	23	3.2	7.2	4.3	4.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	16.8	3.0	23.2	15	-5.6	10	8.4	15.2	8.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	15.8	4.5	23.5	29	-0.1	20	10.1	13.8	8.4	10.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.0	5.5	6.6
VI	–	–	–	–	22.8	9.5	29.9	27	4.2	21	14.9	20.7	13.6	15.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	21.3	9.6	29.9	4	3.3	7	13.4	19.2	13.1	14.7	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.7	6.2	5.8
VIII	–	–	–	–	22.1	10.2	31.9	11	3.8	31	13.4	20.3	14.2	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.5	4.8	5.2
IX	–	–	–	–	20.3	7.2	26.9	17,18	-1.9	23	10.8	19.4	10.5	12.8	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.2	2.2	3.5
X	–	–	–	–	15.5	5.3	24.5	20	-0.4	22	8.2	15.0	8.7	10.2	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.2	3.0	4.1
XI	–	–	–	–	7.2	1.2	15.6	7	-8.9	21	3.4	5.9	4.0	4.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	7.0	6.9
XII	–	–	–	–	-0.7	-7.5	11.5	5	-25.6	24	-4.4	-2.3	-4.0	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	7.2	7.2	7.0	7.1
Rok	–	–	–	–	12.5	2.8	31.9	11.VIII	-25.6	24.XII	6.2	11.0	6.3	7.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Pilsko — φ = 49°32' — λ = 19°19'

I	–	–	–	–	-3.8	-8.8	1.3	4	-18.3	18	-6.4	-5.2	-6.4	-6.1	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	0.8	-4.6	8.8	18	-14.3	6	-2.5	-1.3	-2.2	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	2.1	-2.8	12.3	10	-10.2	23	-1.5	0.4	-0.7	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.7	7.1	7.8
IV	–	–	–	–	9.7	–	17.9	15	–	–	5.1	7.7	5.4	5.9	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.1	5.2	5.0
V	–	–	–	–	8.3	2.2	16.1	27,28	-3.9	13	4.4	7.1	5.0	5.4	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.0	6.7	6.8
VI	–	–	–	–	16.0	7.7	22.9	27	3.7	17	11.2	14.2	10.6	11.6	–	–	–	–	–	–	–	–	–	–	–	–	4.5	6.0	5.0	5.2
VII	–	–	–	–	13.3	6.6	21.3	3	2.1	7	9.1	11.9	9.3	9.9	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.0	5.9	5.9
VIII	–	–	–	–	13.9	7.7	24.3	11	3.2	1,24	10.2	12.9	10.3	10.9	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.4	5.3	6.2
IX	–	–	–	–	–	7.9	–	–	5.0	12	10.2	13.2	10.6	11.3	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.8	4.7	4.7
X	–	–	–	–	–	3.9	–	–	0.1	13	6.2	8.5	6.5	6.9	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.4	3.6	4.1
XI	–	–	–	–	3.5	-2.0	8.2	7,24	-11.5	21	0.6	1.3	0.5	0.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.9	6.3	6.6
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.2	6.9	7.2
Rok	–	–	–	–	–	–	24.3	11.VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Sieniawa — φ = 49°32' — λ = 19°55'

I	–	–	–	–	-0.7	-10.0	8.6	4	-24.3	18	-7.1	-1.9	-5.9	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.3	5.8	5.9
II	–	–	–	–	3.3	-4.9	8.9	19	-15.9	6	-2.8	2.2	-1.6	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	7.6	5.0	6.0	6.2
III	–	–	–	–	7.6	-0.8	17.8	10	-9.2	22	1.1	5.8	2.5	3.0	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	6.6	7.2
IV	–	–	–	–	15.8	2.1	22.6	7	-4.4	10	6.1	14.7	7.6	9.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	4.5	4.5	4.9
V	–	–	–	–	14.4	4.1	21.1	6,27,29	-1.2	13	7.9	12.8	7.8	9.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.4	7.7	7.0
VI	–	–	–	–	21.1	8.4	29.6	27	3.1	21	13.8	19.3	12.7	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	6.4	5.9
VII	–	–	–	–	19.5	7.4	28.5	4	2.1	7	12.9	18.1	12.3	13.9	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.8	6.9	6.6
VIII	–	–	–	–	20.4	9.0	30.9	11	3.3	14	12.6	19.0	12.6	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.8	5.4	5.7
IX	–	–	–	–	20.3	6.2	27.9	17	-1.5	23	9.1	19.3	10.3	12.2	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.0	3.8	4.0
X	–	–	–	–	15.3	3.5	19.7	8	-1.3	22	6.2	14.6	9.6	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.4	4.3	5.4
XI	–	–	–	–	6.1	-0.9	12.8	3	-10.8	21	1.0	4.8	4.8	2.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.9	7.3	7.4
XII	–	–	–	–	-1.7	-10.4	15.9	5	-29.1	25	-7.0	-3.5	-6.3	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.5	6.9	6.7
Rok	–	–	–	–	11.8	1.1	30.9	11.VIII	-29.1	25.XII	4.5	10.4	5.1	6.3	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.8	6.0	6.1

Stary Sącz $H_s = 320\ m$ $h_w =$ 18 m I–II, 22 m IV–XII 1961

MIESIĄC	ROZKŁAD WIATRU (N)		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	OPAD R			LICZBA DNI (n): Temperatura T				Wiatr v		◔	●	Opad R			≡	⊠	R
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15			R ≥ 0.1	R ≥ 1.0	R ≥ 10.0			
I	10	32	3	30	·	·		·	455	118	05	20	·	·	·	·	34	62	7.0	61	5	8	13	28	·	14?	10?	7	9	6	1	·	2	13	·
II	1	20	3	23	·	·	05	100	355	102	1	50	15	20	25	28	39	47	14.7	55	28	·	1	23	·	13?	2	5	11	8	6	·	2	9	·
III	45	34	·		·	·	·	·	45	62	35	46	11	34	155	50	54	19	29.5	95	29	·		9	·	4	·	4	17	13	6	·	2	3	·
IV	45	20	45	29	05	120	·	·	25	77	3	43	55	48	1	25	46	29	7.1	46	1	·		2	2	7	·	9	4	3	2	·	·	·	2
V	5	32	1	10		·	·	·	11	64	1	30	6	30	2	60	67	13	106.6	234	6		·			1	·	1	12	19	15	3	1	·	8
VI	4	31	2	32	·	·	·	·	15	43	·	·	1	50	3	33	65	11	47.7	115	13	·	·	·	8	1	·	7	4	13	11	1	·		10
VII	65	21	·	·	·	·		·	15	74	35	30	3	30	3	33	62	17	114.8	329	30	·	·	·	9	3	1	3	10	13	12	4	·	·	4
VIII	85	24	·	·		·	·		14	41	2	62	35	36	3	30	62	12	52.1	150	12	·	·		8	·		4	7	9	8	3	1	·	3
IX	5	20	·	·		·	05	10	175	37	2	55	15	50	15	30	62	11	21.2	10.1	6	·		2	8	1	·	12	5	8	3	1	5	·	2
X	3	20	2	30	·	·	·	·	42	77	1	100	1	10	·	·	44	37	24.9	16.1	30	·	·	1	·	8?	3?	10	4	7	4	1	4	·	·
XI	3	17	1	10		·	1	80	29	115	1	10	2	25	2	40	51	41	57.4	22.7	4	·		7	·	10?	6?	7	16	13	9	1	5	5	·
XII	65	21	05	10			15	74	265	112	15	37	5	27	45	56	47	39	69.2	22.8	6	11	17	24	·	10?	6?	5	13	12	8	3	1	25	·
Rok	615	24	17	14	05	10	35	22	2805	77	20	40	41	30	38	32	633	28	552.1	329	30.VII	19	31	96	35	72?	28?	74	112	124	85	17	23	55	29

Rymanów-Zdrój $H_s = 360\ m$ $h_w =$ 18 m

I	105	25	55	25		·	4	10	295	61	245	50	·	·	2	25	17	38	19.0	63	14	11	18	30	·	4	1	6	14	11	4	·	–	–	:
II	45	10	05	10		·	2	10	27	39	25	42	·		7	11	18	27	11.0	3.0	8	·	4	21	·	1	·	–	–	9	4		–	–	·
III	235	26	15	17	·		15	10	145	39	16	28	·	·	6	16	30	19	26.0	5.8	31	·	·	10	·	1		–	–	15	9	·	–	–	·
IV	35	36	175	28		·	15	37	215	38	20	36		·		·	26	25	7.5	2.1	19	·		6	·	·	·	–	–	6	4		–	·	1
V	145	13	85	23		·	25	26	105	34	6	33	·	·	7	14	44	12	69.4	13.4	7	·		1	·		·	1	12	14	12	3	–	·	3
VI	13	17	95	18	·	·	05	10	125	26	12	25	1	10	35	13	38	12	70.3	23.9	27			·	5	·	·	–	–	14	10	2	–	·	9
VII	11	12	2	10		·	3	17	135	26	95	27			5	15	49	10	133.7	52.6	29		·	·	7	·	·	3	8	15	14	4	–		5
VIII	125	18	5	21		·	65	12	22	32	15	35	05	10	25	14	29	18	56.7	19.1	12		·	·	8	1	·	5	8	14	8	2	–	·	3
IX	55	10	75	14	2	10	05	10	24	25	155	21		·	10	11	25	14	36.9	11.0	7		·	2	6	·	·	13	4	10	7	1	–	·	2
X	65	16	55	15	·	·	10	18	305	31	175	29	·	·	3	20	20	20	31.7	20.0	30	·	·	1	·	·	·	14	6	6	5	1	–	·	·
XI	10	16	·	·		·	15	13	305	33	175	29		·	3	12	14	21	39.4	13.1	7	·	3	10	·	·	·	5	18	14	10	1	–	–	·
XII	16	16	105	11		·		·	17	46	21	43	·	·	35	10	25	22	73.5	19.0	11	9	17	27	·	2	·	3	15	15	12	4	–	–	·
Rok	131	18	735	16	2	01	47	14	253	36	1995	33	15	02	525	13	335	20	575.1	52.6	29.VII	20	42	108	26	9	1	–	–	143	98	18	–	–	23

Pilsko $H_s = 1270\ m$ $h_w =$ 13 m

I	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24.0	19.5	4	11	26	30		–	–	–	–	5	4	1	5	27	–
II	3	10	·			·	105	12	365	21	26	25	45	19	45	43	2	21	47.4?	10.0	19	2	14	27	·	·	·	10	9	9	9	1	11	28	–
III	1	10	·	·		·	·	·	35	13	365	37	435	27	55	16	3	29	–	–	–	1	13	25		·	·	3	20	–	–	–	19	31	–
IV	·	·	4	10	14	17	55	26	27	39	24	25	8	21	35	16	4	26	–	–	–	–			–		·	6	7	–	–	–	5	5	–
V	16	17	135	19	25	18	·	·	215	21	18	30	135	16	4	18	4	20	126.3	33.6	6			8		·	·	4	13	18	17	5	13	5	–
VI	1	20	3	17	4	12		·	33	21	245	20	8	25	45	17	12	18	162.6	48.0	4	·		·		·		5	7	10	10	5	4	·	–
VII	35	20	45	20	3	17	·	·	10	56	46	28	17	16	2	10	7	25	191.9	42.0	28	·		·	·	1	1	7	13	10	10	8	5	·	–
VIII	2	20	5	12	8	16		·	17	28	475	21	85	22	·	·	5	21	–	–	–	·		·	·	·	·	5	10	–	–	–	11	·	–
IX	·	·	·	·	9	21	9	19	30	24	26	26	10	18	2	10	4	22	22.4	7.8	10	·	–	·	–	·	·	12	10	6	5	·	3	·	–
X	3	20	35	24	45	50	9	37	50	49	22	25	·	·	·	·	1	40	36.8	12.4	14	·	–	·	–	1	1	11	6	7	7	2	8	·	–
XI	2	15	2	15	·	·	55	17	40	30	245	34	95	14	15	23	5	26	63.4	28.0	13	1	6	18	·	·		3	14	8	8	2	12	8	–
XII	125	16	85	31	4	36	4	29	235	34	20	53	165	27	3	20	1	33	–	–	–	–	–	–	–	2	·	3	17	–	–	–	11	26	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	107	130	–

Sieniawa $H_s = 578\ m$ $h_w =$ 16 m

I	·	·	10	10	16	12	19	12	85	26	135	33	5	14	4	18	17	14	21.7	8.5	5	13	17	29	·	·	·	5	8	10	3		4	31	
II	·	·	7	14	17	14	12	14	45	23	125	15	15	13	3	10	13	12	42.2	9.2	9	3	4	27	·	·		4	11	14	12		5	23	
III	·		1	10	·	·	·	·	6	20	38	19	31	20	11	15	6	18	66.0	16.6	14		·	17	·	·	·	3	17	21	16	1	1	8	
IV	25	12	10	16	18	21	12	12	55	12	165	22	10	14	45	10	11	15	19.9	6.4	8	·	·	8		·	·	9	5	5	5	·	1	·	1
V	3	10	4	15	4	10	9	13	25	18	185	18	315	13	115	14	9	13	95.6	32.8	6	·	·	2	·		·	3	11	18	14	2	4		3
VI	1	10	3	13	7	13	155	16	7	13	145	16	22	12	11	10	9	12	120.7	20.6	4	·	·	·	4	·	·	2	8	15	13	4	5	·	7
VII	5	10	4	12	5	12	2	18	1	15	23	16	24	14	15	13	14	12	133.4	35.8	29	·	·	·	6	1	1	3	12	18	14	5	·	·	2
VIII	·	·	3	10	6	13	4	12	·	·	28	14	27	17	15	11	10	13	69.9	22.8	12	·		·	6	·	·	3	7	13	9	2	3		4
IX	5	10	15	11	6	10	·	·	8	15	255	17	125	12	5	10	13	11	14.3	4.6	9	·	·	2	4	·	·	11	6	7	5	·	2	·	1
X	·	·	5	12	23	17	30	15	2	10	9	17	9	14	7	11	8	14	29.0	13.8	30	·	·	1		·		5	8	7	3	2	5	·	·
XI	·		1	10	11	10	17	11	6	16	22	14	135	15	85	12	11	11	76.7	32.8	4	1	1	16	·	·	·	2	16	15	11	1	3	8	·
XII	2	10	19	11	5	14	10	12	55	28	165	22	23	13	3	17	9	14	112.5	30.6	11	14	18	27	·	·	·	4	12	19	11	4	2	25	·
Rok	185	05	82	12	118	12	1305	11	565	16	2375	19	2235	14	985	13	130	13	801.9	35.8	29.VII	31	40	129	20	1	1	54	121	162	116	21	35	95	18

Zwardoń

$\varphi = 49°30'$ $\lambda = 18°59'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.3	-8.7	8.2	4	-19.9	18	-6.5	-2.6	-5.5	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	6.4	5.9	6.1	6.1
II	–	–	–	–	2.1	-4.5	10.1	18	-16.5	6	-2.5	0.8	-1.4	-1.1	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.0	6.8	7.2
III	–	–	–	–	6.9	-1.4	15.6	10	-10.5	23	0.3	4.5	2.4	2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.0	6.4	6.5	7.0
IV	–	–	–	–	14.9	3.0	21.6	7	-3.0	10	5.2	13.6	8.0	8.7	–	–	–	–	–	–	–	–	–	–	–	–	3.1	5.0	3.8	4.0
V	–	–	–	–	13.8	4.0	22.1	27	-0.5	13	7.1	12.0	7.7	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.6	6.8	7.0
VI	–	–	–	–	20.2	8.9	27.3	26	4.2	28	13.2	18.5	13.0	14.4	–	–	–	–	–	–	–	–	–	–	–	–	4.0	5.7	5.0	4.9
VII	–	–	–	–	18.6	8.0	27.3	3	1.9	26	11.8	16.8	12.3	13.3	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.5	5.2	5.5
VIII	–	–	–	–	19.7	9.0	29.5	10	3.0	14	12.0	18.1	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	5.2	5.1
IX	–	–	–	–	19.8	7.1	26.3	17	1.1	22,23	8.8	18.4	11.5	12.6	–	–	–	–	–	–	–	–	–	–	–	–	3.2	3.6	2.7	3.2
X	–	–	–	–	14.4	4.7	19.7	8	0.0	10	6.9	13.1	7.8	8.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	4.1	4.2	4.6
XI	–	–	–	–	5.6	-0.6	12.4	7	-10.8	21	1.2	4.3	1.8	2.3	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.7	6.3	6.9
XII	–	–	–	–	-1.7	-9.1	11.7	5	-24.6	25	-6.1	-4.1	-5.6	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.7	7.1	7.1
Rok	–	–	–	–	11.1	1.7	29.5	10.VIII	-24.6	25.XII	4.3	9.4	5.4	6.1	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.8	5.5	5.7

Nowy Targ

$\varphi = 49°29'$ $\lambda = 20°02'$

I	–	–	–	–	-1.2	-11.3	10.0	4	-24.4	27	-8.5	-2.5	-6.7	-6.1	3.2	3.9	3.4	3.5	8.7	7.2	8.2	8.0	0.4	1.4	0.7	0.8	6.3	4.9	4.8	5.3
II	–	–	–	–	2.9	-6.3	7.4	19	-19.4	6	-4.4	1.5	-1.8	-1.6	4.3	5.4	5.0	4.9	9.2	7.9	9.0	8.6	0.3	1.6	0.5	0.8	7.2	5.3	5.9	6.1
III	–	–	–	–	7.8	-0.5	18.6	10	-12.1	23	1.0	6.0	2.6	3.0	6.0	6.8	6.5	6.4	9.0	7.2	8.7	8.3	0.7	3.0	1.1	1.6	7.2	6.6	6.6	6.8
IV	–	–	–	–	16.2	1.6	22.6	15	-2.2	10	4.7	15.0	8.2	9.0	7.3	8.5	8.7	8.2	8.5	5.1	8.0	7.2	1.3	9.1	2.3	4.2	4.4	5.3	4.9	4.9
V	–	–	–	–	15.1	4.4	22.4	27	-1.0	3	7.2	13.2	8.4	9.3	9.0	9.3	9.7	9.3	8.7	6.3	8.7	7.9	1.4	6.4	1.5	3.1	6.5	7.8	6.5	6.9
VI	–	–	–	–	22.1	8.1	30.2	27	2.5	1	12.3	19.8	14.0	15.0	13.0	13.9	14.0	13.6	9.0	6.2	8.7	8.0	1.4	9.6	2.1	4.4	5.1	5.8	5.6	5.5
VII	–	–	–	–	20.4	7.2	29.2	3	1.2	7	11.4	18.6	13.1	14.0	12.2	12.9	13.4	12.8	9.0	6.0	8.6	7.9	1.4	9.6	2.0	4.3	4.5	4.5	6.0	5.0
VIII	–	–	–	–	21.3	8.3	31.8	11	2.5	31	10.9	19.9	13.2	14.3	12.6	13.9	14.0	13.5	9.5	6.0	9.1	8.2	0.7	10.5	1.5	4.2	5.4	5.2	5.5	5.4
IX	–	–	–	–	21.0	4.9	28.5	17	-3.5	23	6.8	19.8	11.1	12.2	9.7	12.2	12.0	11.3	9.5	5.3	8.9	7.9	0.5	11.7	1.5	4.6	4.3	4.2	3.8	4.1
X	–	–	–	–	15.3	2.3	19.7	20	-4.1	25	4.1	14.4	7.2	8.2	7.6	9.6	9.1	8.8	9.1	5.9	8.9	8.0	1.0	7.1	1.3	3.1	6.6	5.7	4.4	5.6
XI	–	–	–	–	5.7	-1.5	14.6	3	-13.0	21	0.2	4.9	1.0	1.8	6.1	6.8	6.3	6.4	9.3	7.8	9.2	8.8	0.5	2.2	0.6	1.1	7.5	6.7	7.1	7.1
XII	–	–	–	–	-2.6	-12.3	14.5	5	-35.4	26	-8.7	-4.6	-8.1	-7.4	3.5	4.0	3.7	3.7	8.5	8.0	8.8	8.4	0.6	1.1	0.5	0.7	6.6	6.0	7.7	6.8
Rok	–	–	–	–	12.0	0.4	31.8	11.VIII	-35.4	26.XII	3.1	10.5	5.2	6.0	7.9	8.9	8.8	8.5	9.0	6.6	8.7	8.1	0.8	6.1	1.3	2.7	6.0	5.7	5.7	5.8

Jabłonka

$\varphi = 49°28'$ $\lambda = 19°43'$

I	–	–	–	–	-1.7	-11.6	8.2	4	-25.6	18	-7.8	-3.0	-7.1	-6.2	3.4	3.9	3.3	3.5	8.5	7.6	8.2	8.1	0.5	1.2	0.7	0.8	6.6	5.9	5.8	6.1
II	–	–	–	–	2.3	-5.6	7.0	19	-19.3	6	-3.4	1.1	-1.8	-1.5	4.5	5.2	4.9	4.9	9.0	7.8	8.9	8.6	0.5	1.5	0.6	0.9	8.6	6.4	6.5	7.2
III	–	–	–	–	7.3	-0.9	17.2	10	-11.7	23	0.8	5.8	2.9	3.1	5.9	6.2	6.1	6.1	9.0	6.9	8.1	8.0	0.7	3.4	1.6	1.9	7.8	7.5	6.4	7.2
IV	–	–	–	–	15.5	1.5	22.3	7	-3.9	10	4.7	14.4	7.7	8.6	7.4	8.0	8.7	8.0	8.5	5.0	8.2	7.2	1.3	8.9	1.9	4.0	5.2	5.4	4.3	5.0
V	–	–	–	–	14.4	4.0	21.5	6	-1.8	13	7.6	13.1	8.6	9.5	8.9	8.8	9.4	9.0	8.4	5.9	8.3	7.5	1.7	6.8	2.0	3.5	7.3	8.0	7.4	7.6
VI	–	–	–	–	21.1	8.0	29.0	27	2.4	29	12.7	19.6	13.7	14.9	12.6	13.6	13.5	13.2	8.6	6.1	8.5	7.7	2.1	9.9	2.3	4.8	6.7	6.6	5.6	6.3
VII	–	–	–	–	19.6	7.2	29.4	3	1.3	7	11.8	17.9	12.9	13.9	12.0	11.9	12.9	12.3	8.5	5.9	8.6	7.7	2.1	9.4	2.2	4.6	6.4	7.2	6.9	6.8
VIII	–	–	–	–	20.2	8.2	30.2	11	2.9	15,31	11.5	18.9	12.7	14.0	12.6	13.5	13.4	13.2	9.2	6.2	9.0	8.1	1.2	9.4	1.5	4.0	6.8	6.4	4.2	5.8
IX	–	–	–	–	20.3	4.3	27.8	17	-4.2	23	6.9	19.0	10.3	11.6	9.7	12.1	11.5	11.1	9.5	5.5	9.0	8.0	0.6	10.4	1.3	4.1	6.2	4.0	3.2	4.5
X	–	–	–	–	14.7	2.0	19.4	19	-4.2	22	4.3	13.7	7.0	8.0	7.8	9.3	8.6	8.6	9.2	6.0	8.6	7.9	0.9	6.6	1.6	3.0	8.1	5.7	4.4	6.1
XI	–	–	–	–	5.5	–	12.1	3	–	–	0.3	4.6	1.4	1.9	6.1	7.1	6.5	6.6	9.4	8.2	9.3	9.0	0.4	1.7	0.5	0.9	8.0	7.4	7.1	7.5
XII	–	–	–	–	-2.8	–	14.6	5	–	–	-8.2	-5.1	-8.1	-7.4	3.9	4.3	3.8	4.0	9.2	8.9	9.1	9.1	0.4	0.8	0.4	0.5	7.9	7.2	6.5	7.2
Rok	–	–	–	–	11.4	–	30.2	11.VIII	–	–	3.4	10.0	5.0	5.9	7.9	8.7	8.6	8.4	8.9	6.7	8.6	8.1	1.0	5.8	1.4	2.7	7.1	6.5	5.7	6.4

Maniowy

$\varphi = 49°28'$ $\lambda = 20°15'$

I	–	–	–	–	-0.8	-10.5	8.6	4	-23.0	27	-8.0	-3.0	-6.0	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.4	6.3	6.4
II	–	–	–	–	3.2	-6.1	8.1	28	-20.3	6	-3.9	1.2	-2.0	-1.7	–	–	–	–	–	–	–	–	–	–	–	–	9.3	7.0	6.7	7.8
III	–	–	–	–	8.5	0.3	19.2	10	-7.5	23	1.5	6.8	3.1	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.8	7.2	7.8
IV	–	–	–	–	17.0	2.0	24.2	15	-2.5	10	4.8	15.5	8.7	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.7	4.6	5.5
V	–	–	–	–	15.8	4.6	23.3	6	-0.6	15	7.2	14.0	8.8	9.7	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	7.6	7.9
VI	–	–	–	–	22.5	8.2	31.5	27	3.3	21	12.5	20.2	14.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.7	7.1	6.9
VII	–	–	–	–	20.6	7.6	29.2	4	1.3	6	11.8	18.9	13.1	14.2	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.6	7.4	7.1
VIII	–	–	–	–	21.8	8.8	33.0	11	4.0	17,22	10.9	20.2	13.3	14.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	7.0	5.3	7.0
IX	–	–	–	–	21.3	5.1	30.0	17	-4.2	23	6.8	20.1	11.0	12.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	4.4	4.2	5.2
X	–	–	–	–	15.6	3.2	21.0	20	-3.5	22	5.0	14.5	7.8	8.8	–	–	–	–	–	–	–	–	–	–	–	–	7.7	5.6	4.6	6.0
XI	–	–	–	–	6.2	-1.1	15.4	3	-11.0	23,24	0.2	4.9	1.4	2.0	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.4	7.7	7.9
XII	–	–	–	–	-2.8	-12.4	15.3	2	-35.5	26	-9.0	-5.1	-8.2	-7.6	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.3	8.4	8.1
Rok	–	–	–	–	12.4	0.8	33.0	11.VIII	-35.5	26.XII	3.3	10.7	5.5	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.6	6.4	6.9

Zwardoń

H_s = 690 m h_w = 16 m

MIESIĄC	ROZKŁAD WIATRU n_D, v_{mD} N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	●	●	Opad R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	7	3.0	15	3.2	4.5	2.6	·	·	19	3.8	30.5	3.4	3	2.3	3	2.0	11	2.9	37.9	19.4	4	11	17	30	·	·	·	8	15	13	7	1	5	29	
II	6.5	3.4	·	·	0.5	2.0	2	2.2	15.5	4.4	26	3.3	15.5	2.6	12	2.5	6	3.0	76.1	16.8	9	1	7	27	·	·	·	2	15	14	13	3	18	28	·
III	4	3.5	·	·	·	·	·	·	19	4.0	18	3.3	25.5	3.0	15.5	2.9	11	2.9	108.3	25.6	14	1	1	20	·	·	·	5	18	19	19	2	12	26	·
IV	7	3.6	15.5	3.0	3	2.2	5.5	2.5	16.5	3.4	20.5	3.0	2.5	2.8	4.5	2.7	15	2.5	53.5	28.6	18	·	·	5	·	·	·	13	4	10	8	1	2	1	2
V	20	3.0	14.5	2.6	3	2.5	2.5	3.0	13.5	3.4	14.5	3.3	9.5	3.0	7.5	3.3	8	2.8	122.2	40.2	6	·	·	1	·	·	·	2	14	18	14	4	11	·	6
VI	14.5	2.5	7	3.1	11.5	2.3	1.5	1.7	10	3.5	15.5	3.8	16.5	2.9	5.5	2.7	8	2.7	249.5	65.0	27	·	·	·	4	·	·	7	4	15	14	9	9	·	10
VII	7.5	3.1	3.5	2.6	·	·	·	·	20	3.9	21	3.3	21.5	2.8	12.5	2.5	7	2.9	150.3	23.4	15	·	·	·	5	·	·	6	9	15	13	6	11	·	6
VIII	8.5	3.3	4.5	2.7	2	3.0	·	·	13.5	4.1	22.5	3.5	23.5	2.6	10.5	2.3	8	2.8	57.6	17.4	12	·	·	·	6	·	·	7	8	13	10	2	12	·	1
IX	3	3.0	9	2.9	2.5	2.0	2.5	2.0	22	3.2	14	3.8	9.5	2.5	8.5	2.3	19	2.4	23.7	5.4	9	·	·	·	3	·	·	15	3	7	7	·	12	·	1
X	4	4.0	10.5	2.4	5.5	2.9	12.5	3.7	22.5	3.7	18	3.0	8	2.4	3	2.0	9	2.8	40.6	11.3	30	·	·	·	·	·	·	9	8	8	8	2	7	·	·
XI	4	2.8	11	3.6	5	2.6	7	2.5	18.5	3.3	25.5	3.4	8.5	2.8	2.5	4.0	8	2.9	67.5	29.7	4	1	3	17	·	·	·	4	18	12	10	2	17	10	·
XII	18.5	2.7	14.5	3.4	4.5	4.1	·	·	14	4.3	17.5	3.1	6.5	2.6	6.5	3.2	11	2.9	116.5	30.6	6	14	19	26	·	·	·	6	20	18	12	5	9	25	·
Rok	104.5	3.2	105	2.5	42	2.2	33.5	1.5	204	3.8	243.5	3.4	150	2.7	91.5	2.7	121	2.8	1103.7	65.0	27.VI	28	47	126	18	·	·	84	136	162	135	37	125?	119	26

Nowy Targ

H_s = 600 m h_w = 22 m I–X, 21,5 m XI–XII

I	5	1.8	12	1.2	18	2.3	1	2.0	·	·	4	3.4	49	2.6	7	2.0	27	1.5	41.9	5.3	5	15	19	30	·	2	·	–	–	10	4	·	2	31	·
II	1.5	1.0	7	1.1	13	1.3	·	·	·	·	2	1.0	19.5	1.8	15	1.2	26	1.0	53.7	18.7	9	6	5	26	·	·	·	–	–	14	11	1	3	21?	·
III	4	1.2	1	1.0	1	1.0	·	·	0.5	9.0	12	7.0	44.5	4.4	20	2.5	10	3.7	60.9	15.6	14	1	·	15	·	5	1	–	–	18	17	1	·	8?	·
IV	5.5	1.5	11.5	1.1	29.5	2.8	·	·	0.5	5.0	6.5	5.5	10	2.6	16.5	1.6	10	2.2	21.1	6.0	19	·	·	8	·	2	·	8	8	9	5	·	1	·	1
V	11.5	1.6	7	1.1	10	2.7	1	1.0	2	1.0	3	2.0	23.5	3.8	19	2.0	16	2.0	114.8	28.8	6	·	·	2	·	2	·	1	9	19	18	2	1	·	3
VI	11	1.1	3	1.3	15.5	1.6	2.5	1.0	2.5	2.2	2.5	3.2	26	1.9	13	1.3	14	1.6	105.1	17.7	13	·	·	·	5	·	·	4	9	13	12	6	1	·	2
VII	12	1.3	4	1.0	2	1.0	·	·	1	3.0	2	2.8	30.5	2.3	31.5	1.7	10	1.7	113.1	34.9	29	·	·	·	8	·	·	3	2	14	13	3	·	·	2
VIII	11.5	1.5	3.5	1.0	3	2.0	1	1.0	·	·	1.5	2.0	32	2.8	18.5	1.6	22	1.6	78.8	19.5	12,23	·	·	·	7	·	·	6	7	13	9	4	3	·	5
IX	7	1.3	12.5	1.3	9.5	1.6	·	·	·	·	3	8.7	15.5	3.8	17.5	1.4	25	1.6	19.5	6.5	9	·	·	5	5	2	1	14	7	8	6	·	7	·	1
X	7.5	1.0	9.5	1.4	29.5	3.4	2	3.0	·	·	2	4.5	9	2.0	12.5	1.2	21	1.8	36.0	16.8	30	·	·	13	·	1	·	–	–	4	4	2	6	·	·
XI	4	1.4	3.5	1.0	20	2.0	3	1.0	·	·	0.5	10.0	15.5	2.4	14.5	1.4	29	1.3	65.1	21.2	4	4	2	16	·	1	·	–	–	13	11	2	3	6?	·
XII	5.5	1.0	3	1.3	7	1.0	1	1.0	·	·	5	6.4	24.5	2.3	21	1.7	26	1.5	90.8	26.5	11	17	22	27	·	·	·	–	–	16	9	4	4	25	·
Rok	86	1.3	77.5	1.2	158	1.9	11.5	0.8	6.5	1.7	44	4.7	269.5	2.7	206	1.6	236	1.8	770.8	34.9	29.VII	43	48	142	25	15	2	–	–	151	119	25	31	91?	14?

Jabłonka

H_s = 620 m h_w = 19,2 m

I	7.5	2.0	8.5	2.4	3.5	1.6	1.5	2.0	4.5	3.4	23	5.4	0.5	3.0	2	2.0	42	2.0	18.4	6.6	4	17	18	29	·	5	1	4	8	10	5	·	4	30	·
II	2.5	1.4	2.5	1.8	2	1.5	1	1.0	3	2.3	27	2.9	4	2.8	3	1.0	39	1.3	28.2	7.1	9	4	4	27	·	·	·	1	13	14	8	·	7	17	·
III	2.5	3.0	0.5	1.0	0.5	1.0	–	·	3	3.0	44	3.6	8.5	4.4	7	4.4	27	2.6	63.9	12.0	14	1	·	19	·	1	·	1	16	22	18	1	1	6	·
IV	3	2.5	19	2.8	3	3.3	2.5	2.2	·	·	23.5	3.9	2.5	1.8	2.5	4.0	34	2.0	33.0	6.0	8	·	·	10	·	1	·	7	7	10	7	·	1	·	1
V	7	2.5	8.5	2.4	3	3.7	2	2.0	2	2.0	20	3.6	4.5	3.8	5	2.9	41	1.7	110.4	36.7	6	·	·	4	·	2	·	1	16	20	15	2	2	·	7
VI	6	2.8	6.5	2.0	3	2.8	0.5	1.0	3	1.7	17.5	2.8	4.5	4.0	4	1.9	48	1.2	115.8	36.7	8	·	·	·	5	·	·	2	9	17	12	3	6	·	11
VII	5.5	1.5	3.5	1.9	·	·	0.5	1.0	1	2.0	29.5	3.8	5.5	3.1	3.5	2.1	44	1.7	121.9	27.4	29	·	·	·	6	1	1	2	11	15	13	5	4	·	5
VIII	6	3.9	5	2.6	2	1.2	1	1.0	·	·	33	3.7	3	5.2	1	1.0	42	1.9	89.0	20.9	9	·	·	·	5	3	·	2	6	13	9	5	6	·	6
IX	1.5	2.3	6	1.8	4	1.4	2.5	1.0	2	2.0	19.5	3.2	3	3.0	1.5	2.3	50	1.1	14.3	4.3	14	·	·	5	4	1	·	8	6	12	6	·	11	·	1
X	2	2.5	14	1.9	9	2.1	1.5	1.7	8	3.6	11.5	4.7	5	3.0	·	·	42	1.6	23.6	14.0	30	·	·	10	·	1	·	2	9	15	5	1	5	·	·
XI	7	1.5	8	1.2	6	1.5	·	·	1	4.0	19.5	3.3	5	3.5	1.5	3.3	42	1.3	63.8	23.4	4	–	2	–	·	·	·	2	18	17	8	2	6	4	·
XII	16.5	3.1	17.5	2.7	4	2.0	·	·	1.5	7.0	20.5	4.7	1.5	2.3	2.5	4.2	29	2.4	71.9	24.1	11	–	21	–	·	2	·	2	14	18	9	2	4	25	·
Rok	67	2.4	99.5	2.0	40	1.8	13	1.1	29	2.6	288.5	3.8	44.5	3.3	33.5	2.4	480	1.7	754.2	36.7	6.V, 8.VI	–	45	–	20	17	2	34	133	183	115	21	57	82	31

Maniowy

H_s = 520 m h_w = 16,7 m

I	0.5	6.0	3.5	3.1	31.5	2.0	1	1.0	·	·	·	·	47.5	2.8	2	4.2	37	1.5	44.2	6.2	5	16	18	30	·	·	·	4	13	12	4	·	4	21	·
II	·	·	·	·	12.5	2.0	0.5	7.0	·	·	·	·	34.5	2.1	4.5	3.3	32	1.4	39.4	12.8	9	7	3	26	·	·	·	1	15	11	8	1	8	20	·
III	·	·	·	·	2	1.5	·	·	·	·	·	·	55	4.1	25	3.6	11	3.4	73.6	23.7	14	·	·	12	·	2	·	1	18	21	16	1	1	4	·
IV	2	3.0	9.5	3.7	27.5	3.4	3	6.5	·	·	0.5	4.0	15.5	3.9	5	3.0	27	2.6	15.2	6.8	8	·	·	5	·	3	·	6	7	10	4	·	4	·	1
V	6	3.3	4.5	2.0	8	2.5	1.5	4.3	1.5	3.7	0.5	3.0	38	2.4	12	2.7	21	2.0	106.3	22.0	6	·	·	2	·	1	·	·	17	21	14	3	4	·	·
VI	5.5	1.8	4.5	2.9	14.5	2.0	1	4.0	1	1.0	·	·	28	2.7	8.5	2.8	27	1.7	78.8	17.6	4	·	·	·	4	2	2	·	12	13	8	4	6	·	4
VII	6	1.8	1	2.0	6	1.0	2	5.0	·	·	0.5	2.0	39	2.3	11.5	2.8	27	1.6	128.9	34.0	29	·	·	·	7	1	1	2	11	17	12	5	4	·	6
VIII	3.5	2.9	4	4.2	8	1.4	1	2.0	·	·	0.5	4.0	30	3.4	14	3.2	32	2.0	57.8	15.8	12	·	·	·	7	1	·	·	10	21	7	3	14	·	5
IX	4.5	2.9	6.5	3.5	3	2.3	·	·	·	·	·	·	23.5	3.2	7.5	2.8	45	1.5	33.3	14.0	29	·	·	4	5	·	·	5	7	14	5	1	14	·	1
X	3.5	2.0	5.5	3.8	20	5.0	12.5	7.7	·	·	·	·	13.5	2.3	6	2.5	32	2.9	22.5	16.2	30	·	·	8	·	2	·	4	11	16	3	1	10	·	·
XI	1.5	4.3	1	3.0	17.5	3.8	1	6.5	0.5	4.0	0.5	4.0	26	3.2	6	3.1	36	2.1	70.7	29.0	4	4	1	16	·	1	·	·	16	19	9	2	8	6	·
XII	3.5	2.3	2	1.5	9	4.1	·	·	·	·	2	4.5	31.5	3.4	10	4.0	35	1.9	82.9	28.1	11	16	22	27	·	1	·	·	18	16	10	3	9	25	·
Rok	36.5	2.5	42	2.5	159.5	2.3	23.5	3.7	3	0.7	4.5	1.8	352	3.0	112	3.2	362	2.0	723.6	34.0	29.VII	43	44	130	23	14	3	23	155	191	100	24	86	76	17

Przehyba — φ = 49°28' — λ = 20°34' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnia I	Średnia II	Średnia III	Średnia Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-3.7	-8.4	2.0	4	-19.5	18	-6.8	-5.1	-6.2	-6.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.8	8.2	7.8
II	–	–	–	–	0.2	-4.4	11.1	18	-12.8	6	-3.0	-0.7	-2.6	-2.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.3	6.0	6.7
III	–	–	–	–	2.7	-1.8	11.7	10	-8.7	22,23	-0.6	1.6	0.1	0.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.5	7.2	8.2
IV	–	–	–	–	11.0	3.7	18.3	7	-4.0	9,10	5.1	9.6	5.8	6.6	–	–	–	–	–	–	–	–	–	–	–	–	5.4	6.5	5.2	5.7
V	–	–	–	–	9.6	4.0	17.4	6	-2.1	12	5.4	8.3	5.7	6.3	–	–	–	–	–	–	–	–	–	–	–	–	9.0	9.0	9.1	9.0
VI	–	–	–	–	16.5	9.9	24.0	27	5.0	29	11.8	15.5	11.7	12.7	–	–	–	–	–	–	–	–	–	–	–	–	7.3	8.4	8.3	8.0
VII	–	–	–	–	15.1	8.2	23.8	4	4.5	6	10.1	13.7	10.4	11.2	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.4	8.1	8.0
VIII	–	–	–	–	16.3	8.6	26.3	11	4.3	24	10.7	14.9	11.3	12.0	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.3	7.7	7.8
IX	–	–	–	–	15.8	8.7	25.0	18	4.1	11	10.5	14.6	11.2	11.9	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.2	4.8	5.5
X	–	–	–	–	10.1	4.6	15.6	20	1.6	14	5.7	9.2	6.3	6.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.3	6.1	6.8
XI	–	–	–	–	3.4	-1.1	9.6	24	-9.5	21	0.7	2.7	0.5	1.1	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.9	7.6	8.6
XII	–	–	–	–	-3.9	-8.9	10.3	5	-22.6	16	-6.5	-5.3	-6.6	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	8.0	8.2	7.0	7.7
Rok	–	–	–	–	7.8	1.9	26.3	11.VIII	-22.6	16.XII	3.6	6.6	4.0	4.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.9	7.1	7.5

Lesko — φ = 49°28' — λ = 22°20'

I	–	–	–	–	-0.5	-8.5	10.3	4	-23.2	27	-5.9	-1.7	-4.4	-4.1	3.7	4.0	3.8	3.8	8.2	6.9	7.9	7.7	0.8	1.8	1.0	1.2	6.4	6.1	5.0	5.8
II	–	–	–	–	3.1	-2.0	10.5	18	-9.1	15	-1.0	2.3	0.2	0.4	4.9	5.4	5.2	5.2	8.6	7.4	8.4	8.1	0.8	1.9	1.0	1.2	7.9	6.5	7.5	7.3
III	–	–	–	–	8.7	1.5	16.3	18	-6.4	23	3.5	6.7	5.1	5.1	6.5	6.4	6.6	6.5	8.2	6.6	7.6	7.5	1.5	3.8	2.4	2.6	8.5	7.8	6.6	7.6
IV	–	–	–	–	16.9	4.0	23.6	8,15	-3.4	10	7.0	15.5	10.1	10.7	8.1	8.4	8.6	8.4	8.0	4.8	7.0	6.6	2.3	9.8	4.0	5.4	5.3	5.8	4.1	5.1
V	–	–	–	–	16.3	6.0	25.2	29	1.7	20	8.5	14.5	10.5	11.0	9.8	9.7	10.4	10.0	8.7	6.0	8.2	7.6	1.5	7.4	2.6	3.8	7.2	7.7	5.6	6.8
VI	–	–	–	–	22.9	10.8	29.9	27	5.6	29	14.3	20.7	16.2	16.8	14.5	14.8	15.2	14.8	8.8	6.2	8.3	7.8	2.1	10.1	3.5	5.2	5.0	6.0	5.2	5.4
VII	–	–	–	–	21.9	10.2	30.6	4	4.6	7	13.3	20.0	15.1	15.9	13.2	13.1	13.9	13.4	8.6	5.7	8.1	7.5	2.4	11.1	3.6	5.7	6.1	6.0	5.7	5.9
VIII	–	–	–	–	22.6	11.4	32.9	11	4.7	31	13.6	20.9	16.1	16.7	14.0	14.6	15.1	14.6	8.9	5.9	8.2	7.7	1.9	11.1	3.6	5.5	4.9	5.1	5.6	5.2
IX	–	–	–	–	21.5	8.1	29.2	17	-0.8	23	9.8	20.1	13.5	14.2	11.0	11.9	11.9	11.6	8.9	5.1	7.5	7.2	1.7	12.4	3.9	6.0	4.5	3.9	3.1	3.8
X	–	–	–	–	16.9	5.2	26.1	20	0.5	11	6.9	16.0	10.0	10.7	8.4	9.4	9.2	9.0	8.5	5.5	7.6	7.2	1.9	9.3	3.3	4.8	5.3	4.9	3.5	4.6
XI	–	–	–	–	8.6	1.5	16.8	7	-8.2	23	3.6	7.2	4.6	5.0	7.1	7.3	7.3	7.2	8.6	7.1	8.3	8.0	1.2	3.4	1.5	2.0	7.8	7.8	6.9	7.5
XII	–	–	–	–	-0.3	-7.1	14.2	5	-29.3	25	-4.2	-2.1	-3.2	-3.2	4.6	4.7	4.6	4.6	8.6	7.8	8.4	8.3	0.9	1.5	1.0	1.1	7.8	7.9	7.0	7.6
Rok	–	–	–	–	13.2	3.4	32.9	11.VIII	-29.3	25.XII	5.8	11.7	7.8	8.3	8.8	9.1	9.3	9.1	8.6	6.2	8.0	7.6	1.6	7.0	2.6	3.7	6.4	6.3	5.5	6.1

Czarny Dunajec — φ = 49°27' — λ = 19°51'

I	–	–	–	–	-1.9	-10.9	9.0	4	-23.4	18,19	-7.5	-3.3	-5.9	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.5	6.1	6.7
II	–	–	–	–	2.3	-5.3	7.3	28	-17.7	6	-3.5	0.9	-1.5	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.9	6.3	6.3	6.8
III	–	–	–	–	7.1	-0.6	17.4	18	-9.4	23	1.1	5.7	3.0	3.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.5	6.8	7.9
IV	–	–	–	–	15.5	2.6	22.2	7,14	-3.2	10	5.2	14.6	8.3	9.1	–	–	–	–	–	–	–	–	–	–	–	–	5.8	6.0	4.5	5.4
V	–	–	–	–	14.1	4.2	21.3	6	-0.8	13	7.3	13.0	8.6	9.4	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.8	8.0	8.2
VI	–	–	–	–	21.0	8.9	30.5	27	4.0	17	13.1	19.3	14.3	15.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.1	8.5	7.1
VII	–	–	–	–	19.6	8.1	28.8	4	3.2	7	12.0	18.3	13.4	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	7.3	8.0	7.2
VIII	–	–	–	–	20.5	8.7	31.6	11	2.5	14	11.5	19.2	13.8	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.2	5.6	6.3
IX	–	–	–	–	20.2	5.9	26.9	17	-2.4	22	8.1	19.2	11.8	12.7	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.0	3.6	4.6
X	–	–	–	–	14.8	3.0	19.6	19	-2.8	24	4.8	13.9	7.7	8.5	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.3	5.1	6.4
XI	–	–	–	–	5.1	-1.7	12.7	3	-13.2	21	0.0	4.1	1.1	1.5	–	–	–	–	–	–	–	–	–	–	–	–	8.7	7.8	8.7	8.4
XII	–	–	–	–	-2.7	-10.7	14.9	5	-30.5	25	-7.6	-6.0	-7.1	-6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	7.4	7.9	7.3
Rok	–	–	–	–	11.3	1.0	31.6	11.VIII	-30.5	25.XII	3.7	10.0	5.6	6.2	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.0	6.6	6.9

Krościenko — φ = 49°27' — λ = 20°25'

I	–	–	–	–	-0.1	-9.5	9.4	4	-21.7	26	-6.8	-1.6	-5.3	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	4.5	5.6	5.5
II	–	–	–	–	3.8	-4.5	9.2	19	-16.6	6	-2.7	2.7	-1.3	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	7.2	5.6	6.5	6.4
III	–	–	–	–	8.8	0.1	19.8	10	-7.1	23	1.7	7.5	3.1	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.4	6.1	6.9
IV	–	–	–	–	17.2	2.0	24.6	15	-4.3	10	5.5	16.1	7.9	9.4	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.9	3.7	4.3
V	–	–	–	–	16.2	4.5	23.6	6	-0.9	13	8.2	14.8	8.4	10.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.9	5.7	6.4
VI	–	–	–	–	23.1	8.8	30.8	27	3.4	21	13.8	20.7	14.0	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.6	5.2	5.1
VII	–	–	–	–	21.5	8.7	30.3	3	2.9	7	12.9	19.5	12.8	14.5	–	–	–	–	–	–	–	–	–	–	–	–	4.6	6.8	5.8	5.7
VIII	–	–	–	–	22.8	9.2	34.1	11	3.2	31	12.4	21.3	13.4	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.9	4.4	5.1
IX	–	–	–	–	21.8	5.9	30.5	17	-3.3	23	8.3	21.0	10.3	12.5	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.0	3.2	3.8
X	–	–	–	–	16.2	3.9	22.3	20	-1.1	22	6.2	15.3	7.6	9.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.1	3.6	4.9
XI	–	–	–	–	6.9	-0.6	14.6	3	-10.9	21	1.4	6.3	2.0	2.9	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.5	6.5	6.7
XII	–	–	–	–	-1.1	-10.6	15.1	5	-31.8	25	-7.0	-2.8	-5.9	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	6.3	6.5	6.3
Rok	–	–	–	–	13.1	1.5	34.1	11.VIII	-31.8	25.XII	4.5	11.7	5.6	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.8	5.2	5.6

Przehyba

$H_s = 1175\ m$ $h_w = 13{,}5\ m$ **1961**

MIESIĄC	ROZKŁAD WIATRU (%D, %mD)																		OPAD R			LICZBA DNI (n)													
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość				Temperatura T				Wiatr v			Opad R					
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 35°	v > 10	v > 15	●	≥ 0,1	≥ 1,0	≥ 10,0	≥ 100	≡	▤	≈
I	6	4,5	6	3,0	·	·	·	·	25,5	5,2	22,5	4,5	·	·	3,3	4,0	·	4,4	9,6	3,4	12	8	26	30	·	·	·	3	22	5	4	·	–	31	·
II	4,5	3,4	·	·	1	3,0	·	·	2,2	3,6	3,3	3,8	6,5	3,3	1,6	3,4	1	3,6	3,4,0	5,4	3	1	15	26	·	·	·	4	14	14	11	·	–	28	·
III	4	11,2	·	·	·	·	·	·	7	8,7	3,4,5	6,5	28,5	6,2	1,9	8,2	·	7,1	59,2	14,0	14	·	12	22	·	7	·	·	23	17	13	1	–	20	·
IV	1,5	4,4	3	2,7	0,5	4,0	3,5	8,3	3,3	6,3	12	9,8	7	4,0	1,6	3,1	·	5,6	17,0	7,4	8	·	·	4	·	3	·	7	6	6	4	·	–	2	1
V	6,5	3,3	·	·	·	·	·	·	21,5	4,4	32,5	6,0	11	4,4	20,5	4,6	1	4,9	160,3	26,4	17	·	·	3	·	·	·	·	26	17	17	6	–	·	·
VI	7,5	8,6	·	·	1	7,0	·	·	26,5	7,7	16,5	6,5	6,5	6,3	3,0	4,2	2	6,1	105,7	13,4	11	·	·	·	·	4	·	·	16	16	14	4	–	·	10
VII	14,5	4,2	·	·	·	·	1	4,0	25,5	7,2	27	5,2	6	4,2	1,9	5,0	·	5,5	171,1	54,2	30	·	·	·	·	3	1	·	17	16	15	4	–	·	4
VIII	1,7	3,9	3,5	3,4	·	·	0,5	7,0	1,8	5,3	3,0,5	4,0	1,0	3,1	12,5	4,7	1	4,2	98,7	29,0	12	·	·	·	3	2	1	·	18	15	12	4	–	·	4
IX	1,2	4,2	7	4,9	1,5	2,0	1,5	2,0	12,5	5,1	2,9	4,2	1,6,5	3,3	9	3,4	1	4,0	33,7	14,0	29	·	·	·	·	1	·	7	9	8	6	1	–	·	2
X	11,5	5,1	1	7,0	1	4,0	4	5,5	5,7,5	9,8	6,5	4,2	1,5	4,3	1,0	6,6	·	8,1	58,5	12,6	30	·	·	·	·	12	7	2	13	11	8	2	–	·	·
XI	4,5	4,4	·	·	1,5	3,7	4	4,4	4,0	6,6	2,3,5	3,8	8	3,2	8,5	3,3	·	5,0	74,6	15,2	4	·	7	16	·	4	·	1	20	15	10	2	–	8	·
XII	12,5	8,7	2	6,5	2	3,0	2	2,0	3,3	6,3	10,5	6,3	2,5	2,0	28,5	4,8	·	5,9	87,8	23,1	6	13	22	28	·	11	1	2	19	16	14	3	–	26	·
Rok	115,5	5,5	22,5	2,3	8,5	2,2	16,5	2,8	32,2	6,4	27,8	5,4	10,4	3,7	22,2	4,6	6	5,4	910,2	54,2	30.VII	22	82	129	3	47	10	26	203	156	128	27	–	115	21

Lesko

$H_s = 386\ m$ $h_w = 17{,}6\ m$

I	3	4,0	·	·	3	2,3	0,5	7,0	3,1,5	5,5	8	2,2	3,5	2,1	5,5	2,6	3,8	2,5	155	4,2	5,14	11	13	29	·	7	3,1	4	11	12	5	·	2	23	·
II	2	1,5	·	·	3	4,0	1	1,0	18,5	5,2	11,5	2,4	6	1,9	6	2,4	3,6	1,9	19,8	3,1	13	·	1	18	·	2	·	2	15	16	6	·	6	16	·
III	1	4,0	·	·	·	·	·	·	1,8	5,5	7,5	4,0	2,1,5	3,8	2,7	4,0	1,8	3,5	23,1	5,0	19	·	·	9	·	3	·	1	17	16	9	·	2	1	·
IV	2,5	2,0	5	3,6	14,5	3,3	3,5	2,0	18,5	4,1	6	5,2	4	2,4	4	2,1	3,2	2,3	25,3	9,2	18	·	·	4	·	·	·	5	5	9	5	·	·	·	3
V	3	2,8	4,5	1,9	7	2,9	2,5	1,6	12	3,4	9	2,2	9	3,3	7	2,9	3,9	1,6	49,8	10,4	14	·	·	·	1	·	·	·	11	15	8	1	5	·	4
VI	1,5	2,0	4	2,5	7	1,9	1,5	1,7	11	3,3	11,5	3,2	10	2,0	5,5	2,2	3,8	1,5	98,8	16,3	14	·	·	·	4	·	·	5	8	13	13	5	10	·	12
VII	2	1,5	3	1,3	·	·	·	·	1,6,5	3,9	11,5	3,0	6,5	2,5	17,5	2,2	3,6	1,8	69,6	28,0	29	·	·	·	9	·	·	2	7	14	9	3	3	·	5
VIII	6,5	2,5	2	2,5	4	1,6	4	2,1	13,5	4,0	21	4,1	10,5	3,8	12,5	3,6	1,9	2,8	37,9	12,8	12	·	·	·	8	1	·	3	4	13	7	1	6	·	4
IX	·	·	4	2,5	13,5	1,8	4	1,6	8	4,3	11	4,2	11	2,6	7,5	2,1	3,1	1,8	16,5	4,9	26	·	·	2	8	·	·	13	3	9	5	·	4	·	3
X	2	2,8	1	3,5	1,5	1,8	13,5	3,0	15,5	4,9	4	3,5	4,5	4,7	6,5	2,5	3,1	2,2	23,5	12,8	30	·	·	·	1	3	·	11	7	7	4	1	3	·	·
XI	5,5	3,0	1	5,0	·	·	12,5	3,6	20,5	4,4	13,5	3,2	10	3,6	7	3,4	2,0	2,9	155	3,0	19	·	1	11	·	3	·	1	18	14	6	·	5	3	·
XII	8,0	3,5	3,5	2,6	7,5	1,9	7,5	4,3	1,9	7,4	7	5,4	8,5	2,8	11	3,4	2,1	3,5	51,5	11,7	7	11	17	24	·	7	3,2	1	18	17	11	1	3	25	·
Rok	3,7	2,5	2,8	2,1	7,4,5	1,5	5,0,5	2,3	2,0,2,5	4,6	1,2,1,5	3,6	1,0,5	3,0	1,1,7	2,8	3,5,9	2,4	4,4,6,8	2,8,0	29.VIII	22	32	97	31	26	6,2	48	124	155	88	12	49	68	31

Czarny Dunajec

$H_s = 676\ m$ $h_w = 18{,}0\ m$

I	3,5	3,1	6,5	2,3	4,5	3,2	0,5	6,0	1	4,0	12,5	3,6	13,5	3,5	2	2,5	4,9	1,6	214	8,4	5	15	20	30	·	1	·	4	13	9	4	·	2	31	·
II	1,5	3,7	1	3,0	1	2,5	2	1,8	1,5	1,0	12,5	2,6	14	3,6	2,5	3,0	4,8	1,3	303	7,0	9	2	4	27	·	·	·	2	13	13	9	·	6	27	·
III	2,5	4,8	0,5	3,0	·	·	·	·	0,5	1,0	2,9,5	3,6	3,5,5	4,0	4,5	6,3	2,0	3,1	68,0	12,8	14	·	1	13	·	1	1	1	20	19	18	1	·	9	·
IV	4,5	2,8	6,5	3,4	1,3	2,6	2	2,5	2,5	1,6	10,5	2,9	9,5	4,4	2,5	5,6	3,9	1,8	28,5	7,0	19	·	·	4	·	1	·	8	9	11	8	·	2	·	1
V	9,5	2,8	1,0	2,2	2,5	4,2	0,5	1,0	1,5	2,7	11,5	3,7	1,4	3,2	5,5	3,4	3,8	1,8	112,8	35,0	6	·	·	2	·	2	1	2	23	17	13	4	3	·	8
VI	4,5	2,3	8,5	2,4	7	2,1	2	1,5	1,5	3,3	6,5	3,4	13,5	2,7	4,5	2,6	4,2	1,4	141,2	30,3	11	·	·	·	4	·	·	2	15	15	11	6	3	·	11
VII	9,5	1,4	5,5	1,4	·	·	·	·	·	·	15,5	3,2	18,5	3,7	7	2,7	3,7	1,7	143,8	37,0	29	·	·	·	5	1	1	2	15	15	12	5	1	·	7
VIII	4,5	2,4	5	2,3	3	2,0	·	·	1	1,0	14,5	3,4	19	3,4	6	3,8	4,0	1,8	106,7	37,2	3	·	·	·	6	3	2	3	8	10	8	5	3	·	6
IX	2,5	2,0	3	2,5	6,5	2,1	0,5	1,0	0,5	1,0	14,5	3,3	11,5	3,1	3	2,0	4,8	1,3	14,2	5,0	6	·	·	2	4	·	·	10	8	6	4	·	5	·	2
X	2,5	5,2	3	2,0	16,5	2,8	3,5	4,0	4,5	4,7	5	3,5	5	3,1	2	2,8	5,1	1,5	29,8	19,0	30	·	·	6	·	1	1	4	12	8	2	1	7	·	·
XI	3,5	2,1	3,5	3,0	4	1,5	·	·	·	·	6,5	3,2	18	3,3	1,5	5,7	5,3	1,3	71,4	24,4	4	2	3	17	·	1	1	1	21	14	10	3	8	11	·
XII	10	4,3	7	3,0	1	1,0	·	·	·	·	11,5	4,5	11,5	5,0	5	5,4	4,7	2,2	70,4	19,7	6	15	20	27	·	3	·	2	16	18	12	2	4	25	·
Rok	5,8,5	3,1	6,0	2,5	5,9	2,0	1,1	1,5	1,4,5	1,7	1,5,0,5	3,4	1,8,3,5	3,6	4,6	3,8	5,1,2	1,7	8,3,8,5	3,7,2	3.VIII	3,4	4,8	1,2,8	1,9	1,4	7	4,1	1,7,3	1,5,5	1,1,1	2,7	4,4	1,0,3	3,5

Krościenko

$H_s = 440\ m$ $h_w = 24{,}2\ m$

I	0,5	1,0	1,1	1,5	3,5	1,4	6	1,7	·	·	15,5	1,5	9,5	1,7	1	1,0	4,6	0,8	17,4	6,5	5	13	15	30	·	·	·	4	8	8	7	·	4	–	·
II	2	1,0	6	1,2	8,5	1,1	2,5	1,8	1	1,0	2,4	1,4	1,0	1,2	·	·	3,0	0,8	33,2	10,1	9	1	2	25	·	·	·	4	12	9	7	1	9	–	·
III	2,5	1,0	1,5	1,0	·	·	·	·	1	1,0	2,7,5	2,8	2,7	2,1	0,5	1,0	3,3	1,3	83,6	15,2	28	·	·	14	·	·	·	4	15	17	14	2	6	–	·
IV	2	3,5	9,5	1,3	11,5	1,3	4	1,0	2	1,0	7	2,0	9	2,6	·	·	4,5	0,9	12,3	5,2	8	·	·	4	·	1	·	8	3	6	3	·	1	–	1
V	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	115,9	21,9	17	·	·	3	·	·	·	·	9	17	16	3	7	·	7
VI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	95,7	17,5	9	·	·	·	8	–	–	2	5	13	10	3	4	·	13
VII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	124,8	35,4	29	·	·	·	8	–	–	3	7	15	13	4	4	·	5
VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	48,1	17,2	12	·	·	·	8	–	–	4	5	10	6	1	7	·	4
IX	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	32,5	19,6	29	·	·	3	7	–	–	12	3	6	5	1	12	·	3
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	24,3	14,4	30	·	·	1	·	–	–	5	5	10	5	1	11	·	·
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	79,6	38,4	4	2	·	10	·	–	–	4	13	13	9	1	13	–	·
XII	1	1,0	7,5	1,6	4,5	1,5	2	2,0	·	·	19,5	2,1	17,5	2,0	1	2,0	4,0	1,1	126,6	28,7	11	14	18	28	·	·	·	3	13	18	11	4	11	–	·
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	794,0	38,4	4.XI	30	35	118	31	–	–	53	98	142	106	21	89	–	33

Brzegi Dolne

$\varphi = 49°27'$ $\lambda = 22°38'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.8	-11.6	10.6	4	-29.7	27	-6.7	-1.8	-6.8	-5.5	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.0	5.2	6.1
II	–	–	–	–	2.9	-4.1	10.7	18	-15.0	15	-2.3	2.0	-1.0	-0.6	–	–	–	–	–	–	–	–	–	–	–	–	8.2	7.1	7.1	7.5
III	–	–	–	–	8.4	-0.1	15.7	10	-7.7	23	2.7	6.5	3.5	4.0	–	–	–	–	–	–	–	–	–	–	–	–	9.0	8.2	5.6	7.6
IV	–	–	–	–	15.9	0.9	23.7	8	-6.1	10	6.0	14.6	7.4	8.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	7.0	4.2	5.5
V	–	–	–	–	15.7	3.4	23.6	29	-1.7	17	8.3	14.2	7.6	9.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.2	4.9	6.9
VI	–	–	–	–	22.6	8.3	29.3	27	3.1	17	14.6	20.7	13.5	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.2	5.4	5.6
VII	–	–	–	–	21.3	7.5	29.1	4	0.7	7	13.6	19.6	12.5	14.6	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.9	5.0	6.0
VIII	–	–	–	–	21.8	8.7	31.1	11	3.9	17	13.3	20.5	13.7	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.3	5.4	5.6
IX	–	–	–	–	20.2	4.0	28.8	17	-6.0	23	8.4	19.4	8.9	11.4	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.9	2.8	4.0
X	–	–	–	–	16.2	0.8	23.7	20	-5.3	13	4.1	15.6	6.0	7.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.9	3.2	4.4
XI	–	–	–	–	8.1	0.0	13.9	7,12	-10.1	23	3.1	6.7	3.4	4.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.4	6.8	7.9
XII	–	–	–	–	-0.5	-10.1	13.2	5	-31.9	25	-5.9	-2.1	-5.2	-4.6	–	–	–	–	–	–	–	–	–	–	–	–	8.7	8.5	7.2	8.1
Rok	–	–	–	–	12.6	0.6	31.1	11.VIII	-31.9	25.XII	4.9	11.3	5.3	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.9	5.2	6.3

Czarsztyn

$\varphi = 49°26'$ $\lambda = 20°19'$

I	–	–	–	–	-0.9	-10.4	9.0	4	-23.1	27	-7.8	-3.0	-5.8	-5.6	–	–	–	–	–	–	–	–	–	–	–	–	7.1	4.3	5.1	5.5
II	–	–	–	–	3.3	-5.3	9.0	19	-16.2	6	-3.5	1.8	-1.6	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	8.6	5.6	5.7	6.6
III	–	–	–	–	8.4	0.0	18.8	10	-6.3	23	1.2	6.8	3.3	3.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.3	6.5	7.2
IV	–	–	–	–	16.6	1.9	23.6	15	-3.3	10	4.3	15.8	9.0	9.5	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.9	4.5	4.9
V	–	–	–	–	15.2	4.1	22.1	6	-0.4	13	7.3	14.1	8.6	9.6	–	–	–	–	–	–	–	–	–	–	–	–	8.1	7.8	8.5	7.5
VI	–	–	–	–	22.1	8.2	30.5	26	3.4	1	12.0	20.5	14.2	15.2	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.3	6.4	6.3
VII	–	–	–	–	20.5	8.1	29.0	3	1.9	7	11.4	19.7	13.0	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.0	7.2	6.8	6.7
VIII	–	–	–	–	21.7	9.0	32.5	11	4.6	17	11.2	21.1	13.4	14.8	–	–	–	–	–	–	–	–	–	–	–	–	8.7	6.1	4.8	6.5
IX	–	–	–	–	21.1	5.8	28.8	17	-3.4	23	7.2	20.5	11.5	12.7	–	–	–	–	–	–	–	–	–	–	–	–	6.7	3.8	4.0	4.8
X	–	–	–	–	15.8	3.9	20.5	20	-2.7	22	5.7	14.9	8.9	9.6	–	–	–	–	–	–	–	–	–	–	–	–	6.9	5.0	4.0	5.3
XI	–	–	–	–	6.2	-1.1	15.1	3	-11.7	23,24	0.3	5.3	1.6	2.2	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.1	7.0	7.5
XII	–	–	–	–	-2.3	-12.0	14.9	2	-33.8	26	-8.8	-4.4	-7.5	-7.0	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.4	7.4	6.9
Rok	–	–	–	–	12.3	1.0	32.5	11.VIII	-33.8	26.XII	3.4	11.1	5.7	6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.0	5.7	6.3

Czarsztyn - Nadzamcze

$\varphi = 49°26'$ $\lambda = 20°20'$

I	–	–	–	–	-2.3	-9.6	5.4	4	-22.0	27	-8.3	-3.3	-5.9	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.4	5.7	5.7
II	–	–	–	–	1.4	-4.7	9.1	19	-13.2	6	-4.0	0.8	-1.9	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	6.4	5.8	6.7
III	–	–	–	–	6.6	-0.3	17.2	18	-6.8	23	0.6	5.6	2.5	2.8	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	6.6	6.9
IV	–	–	–	–	15.2	4.0	22.7	15	-3.1	10	4.8	14.4	8.5	9.0	–	–	–	–	–	–	–	–	–	–	–	–	4.3	5.6	4.9	4.9
V	–	–	–	–	13.9	4.9	21.9	6	-0.7	15	6.4	12.7	8.4	9.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.3	7.0	6.9
VI	–	–	–	–	20.6	9.4	29.2	27	4.4	17	12.0	18.9	14.4	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.3	6.3	5.4	5.7
VII	–	–	–	–	19.7	8.7	28.2	3	3.2	7	10.9	18.1	13.1	13.8	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.8	5.8	5.4
VIII	–	–	–	–	20.8	9.3	32.2	11	5.0	31	10.6	19.3	13.7	14.3	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.9	5.2	5.8
IX	–	–	–	–	20.1	6.6	28.2	17	-1.4	23	7.8	19.0	12.1	12.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	4.4	4.3	4.7
X	–	–	–	–	14.7	4.6	19.6	20	-1.4	22	5.7	13.4	8.3	8.9	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.0	4.5	5.1
XI	–	–	–	–	5.3	–	13.6	3	–	–	0.3	4.6	1.3	1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.7	7.3	7.1
XII	–	–	–	–	-2.7	–	15.8	5	–	–	-8.3	-4.8	-6.6	-6.6	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.2	6.9	6.4
Rok	–	–	–	–	11.1	–	32.2	11.VIII	–	–	3.2	9.9	5.7	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.0	5.8	5.9

Szczawnica

$\varphi = 49°26'$ $\lambda = 20°29'$

I	–	–	–	–	-0.9	-8.8	9.0	4	-19.6	27	-6.6	-1.5	-5.8	-4.9	3.9	4.4	3.9	4.0	9.5	7.9	9.0	8.8	0.2	1.2	0.4	0.6	6.5	4.5	5.9	5.6
II	–	–	–	–	2.8	-4.3	7.5	28	-14.9	6	-2.7	2.1	-1.7	-1.0	4.9	5.5	5.0	5.1	9.5	7.7	9.2	8.8	0.2	1.8	0.4	0.8	7.6	6.2	6.5	6.8
III	–	–	–	–	7.8	0.2	19.9	18	-6.8	23	1.4	7.3	2.7	3.5	6.6	7.8	6.8	7.1	9.6	7.6	9.0	8.7	0.3	2.9	0.8	1.3	7.8	7.1	6.8	7.2
IV	–	–	–	–	16.9	2.9	26.8	7	-3.7	10	4.8	16.0	8.4	9.4	8.2	10.4	9.8	9.5	9.3	5.7	8.8	7.9	0.6	8.8	1.5	3.6	4.5	4.9	4.3	4.6
V	–	–	–	–	15.0	5.1	21.8	6	-0.4	13	7.6	14.2	8.6	9.8	9.9	10.6	10.2	10.2	9.4	6.5	9.0	8.3	0.7	6.1	1.2	2.7	7.1	7.0	7.0	7.0
VI	–	–	–	–	22.0	10.1	30.1	27	4.5	17	12.5	20.5	14.8	15.6	13.8	15.2	14.4	14.5	9.4	6.4	8.6	8.1	0.9	9.6	2.6	4.4	5.1	5.3	6.0	5.5
VII	–	–	–	–	20.2	9.4	30.0	4	3.7	7	11.5	19.5	14.3	14.9	12.9	14.2	13.7	13.6	9.4	6.4	8.4	8.1	0.8	9.2	2.8	4.3	4.9	6.5	6.7	6.0
VIII	–	–	–	–	22.1	9.8	32.3	11	4.7	31	11.2	20.6	15.1	15.5	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.6	4.8	5.4
IX	–	–	–	–	21.4	6.9	29.0	17	-2.1	23	7.9	20.5	12.7	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	4.1	3.2	4.1
X	–	–	–	–	15.2	5.4	21.1	20	-0.3	22	6.7	14.7	8.8	9.8	8.9	10.2	9.7	9.6	9.0	6.2	8.6	7.9	1.2	6.8	1.7	3.2	6.3	5.1	4.1	5.2
XI	–	–	–	–	6.6	0.1	14.6	3	-9.2	21	1.7	6.1	2.0	3.0	6.6	7.5	6.6	6.9	9.2	7.8	9.1	8.7	0.6	2.3	0.7	1.2	8.2	7.0	7.0	7.4
XII	–	–	–	–	-1.2	-9.6	15.0	5	-28.4	26	-6.4	-2.5	-5.8	-5.1	4.3	4.8	4.2	4.4	9.3	8.2	9.0	8.8	0.3	1.1	0.4	0.6	6.8	6.4	7.1	6.8
Rok	–	–	–	–	12.3	2.3	32.3	11.VIII	-28.4	26.XII	4.1	11.5	6.2	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.8	5.8	6.0

Brzegi Dolne H_s = 420 m h_w = 17 m 1961

ROZKŁAD WIATRU ⁰D, ᵛmD · OPAD R · LICZBA DNI (n): Temperatura T, Wiatr v, Opad R

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	2	2.5	5.5	2.1	·	·	2.5	3.0	18.5	3.0	19.5	3.2	5.5	2.3	1.5	2.3	38	1.7	15.7	4.2	19	13	13	29	·	·	·	5	10	9	7	·	2	23	·
II	1	1.0	1.5	2.0	4.5	1.6	3	1.7	6.5	2.2	18	4.0	11.5	1.9	5	1.7	33	1.6	26.3	6.6	13	5	2	22	·	·	·	2	15	15	9	·	1	19	·
III	1	1.0	·	·	·	·	·	·	6	3.7	15.5	3.8	39	3.6	8.5	3.9	23	2.7	41.7	7.0	31	·	·	14	·	1	·	1	13	18	12	·	2	3	·
IV	·	·	7	2.1	14.5	3.3	6.5	2.7	5	2.6	10	4.8	6.5	3.1	2.5	2.4	38	1.9	17.8	7.9	8	·	·	11	·	·	·	4	6	8	4	·	·	·	3
V	0.5	1.0	5	1.8	5.5	2.1	4.5	1.8	6	2.9	12.5	2.4	11.5	2.3	6.5	2.4	41	1.3	56.1	14.5	27	·	·	5	·	·	·	·	9	15	8	2	4	·	4
VI	3.5	2.1	2	3.0	3	1.0	2	1.0	6.5	1.9	7.5	2.5	10	2.3	8.5	2.5	47	1.0	110.5	22.0	11	·	·	·	5	·	·	2	8	15	11	6	6	·	5
VII	1.5	1.3	2	1.5	2	1.0	1	2.5	3.5	3.0	15	3.3	14	1.9	9	2.1	45	1.2	81.1	27.8	29	·	·	·	8	·	·	2	7	14	10	3	1	·	3
VIII	2	2.0	2.5	2.0	4.5	1.4	0.5	1.0	2.5	1.8	19	2.2	9.5	2.9	6.5	2.4	46	1.1	28.0	8.4	12	·	·	·	6	·	·	3	9	10	8	·	2	·	1
IX	1	3.0	2	1.5	7	1.7	1	5.0	5.5	2.4	10.5	2.8	15	2.2	2	1.5	46	1.1	20.0	7.2	26	·	·	7	6	·	·	14	6	9	6	·	4	·	2
X	4	1.6	2	2.8	6.5	2.7	6.5	1.7	7.5	3.1	4	2.2	7.5	1.5	4	1.5	51	1.0	21.0	9.9	30	·	·	16	·	·	·	12	8	7	4	·	5	·	·
XI	3	2.0	1	1.0	·	·	1.5	1.3	13	2.3	13	3.2	12.5	1.7	7	1.6	39	1.2	22.7	7.8	19	1	2	14	·	·	·	2	19	12	7	·	5	6	·
XII	8	1.7	·	·	5.5	1.6	0.5	2.0	17	4.9	3.5	5.0	14.5	2.4	8	2.7	36	2.0	65.2	12.8	7	15	18	25	·	1	·	1	21	16	13	2	1	25	·
Rok	27.5	1.6	30.5	1.6	53	1.4	29.5	2.0	97.5	2.8	148	3.3	157	2.3	69	2.2	483	1.5	506.1	27.8	29.VII	34	35	143	25	2	·	48	131	148	99	13	33	76	18?

Czorsztyn H_s = 496 m h_w = 24 m (I–III), 18.4 m (IV–XII)

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	1	2.0	·	·	8	2.4	1	3.0	·	·	·	·	6	2.3	1	1.0	76	0.4	13.8	6.7	5	14	18	31	·	·	·	8	9	8	3	·	3	21	–
II	·	·	·	·	·	·	·	·	·	·	·	·	2	4.5	3	2.7	79	0.2	36.0	12.6	9	3	4	25	·	·	·	3	13	12	7	1	9	19	–
III	·	·	·	·	·	·	·	·	·	·	1	4.0	10.5	3.2	25.5	2.7	56	1.1	58.8	13.5	14	·	·	15	·	·	·	4	15	18	17	1	5	7	–
IV	1.5	3.0	4.5	2.8	9.5	2.5	4	2.9	2.5	2.2	0.5	2.0	3	2.8	9.5	3.1	55	1.1	9.1	4.9	8	·	·	6	·	·	·	9	6	5	2	·	4	·	–
V	1	1.5	2.5	1.8	4	2.2	2	2.2	0.5	1.0	·	·	11	2.4	8	1.7	64	0.6	80.6	18.5	6	·	·	1	·	·	·	2	16	16	12	1	3	·	–
VI	·	·	4	2.0	3	2.3	2	3.5	·	·	1	3.0	8.5	3.1	8.5	2.4	63	0.8	62.8	40.7	13	·	·	·	4	·	·	1	12	14	10	2	4	·	–
VII	1	3.0	2	1.0	0.5	1.0	2	4.5	1	2.0	0.5	1.0	7	3.4	12	3.1	67	0.8	108.5	33.0	29	·	·	·	7	·	·	2	11	16	12	3	2	·	–
VIII	0.5	3.0	2.5	1.8	3	2.0	0.5	2.0	0.5	2.0	·	·	16	3.5	2	2.8	68	0.8	57.4	18.0	3	·	·	·	8	·	·	1	10	7	5	2	9	·	–
IX	·	·	0.5	5.0	1.5	3.0	1	3.0	1	2.0	3.5	2.3	9.5	3.5	5	2.4	68	0.7	24.8	12.0	29	·	·	4	6	·	·	7	6	5	5	1	11	·	–
X	·	·	0.5	2.0	12.5	3.7	20	6.6	2	4.2	·	·	1.5	1.7	4.5	4.1	52	2.2	18.3	14.2	30	·	·	6	·	2	·	7	6	5	3	1	10	·	–
XI	·	·	3.5	3.4	5.5	3.7	3.5	4.1	1.5	2.0	·	·	8.5	3.6	5.5	3.9	62	1.1	99.2	45.5	4	4	1	15	·	·	·	3	16	17	11	2	6	10	–
XII	·	·	2	2.0	1	2.0		·	0.5	4.0	2.5	4.8	2	6.0	18	3.9	67	1.1	96.9	38.3	11	17	22	31	·	·	·	4	14	15	10	3	3	25	–
Rok	5	1.0	22	1.8	48.5	2.1	36	2.6	9.5	1.6	9	4.2	85.5	3.3	102.5	2.8	777	0.9	666.2	45.5	4.XI	38	45	134	25	2	·	51	134	138	97	17	69	82	–

Czorsztyn-Nadzamcze H_s = 650 m h_w = 16,6 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	6	1.2	25	1.7	13	3.8	7	9.0	1	2.0	2	1.5	6	6.2	12	2.7	21	2.5	16.2	5.4	5	13	20	30	·	3	2	4	8	8	3	·	6	29	·
II	5	1.2	20	1.4	9	1.8	1	7.0	·	·	1	8.0	28	3.5	6	2.2	14	2.1	29.4	10.2	9	1	7	28	·	·	·	1	12	10	8	1	7	23	·
III	·	·	·	·	1	3.0	·	·	·	·	10	12.2	60	7.5	17	3.8	5	6.9	67.1	19.2	14	·	3	18	·	21	8	2	12	15	12	1	8	9	·
IV	7	1.1	17	2.9	14	3.2	6	7.8	1	4.0	2	11.5	15	5.9	9	3.3	19	3.3	13.0	6.1	8	·	·	4	·	9	4	3	2	8	4	·	2	·	1
V	6	1.3	12	1.6	9	2.6	4	5.2	·	·	3	2.7	21	4.5	23	4.0	15	2.8	97.0	22.4	6	·	·	1	·	5	1	·	7	17	14	3	4	·	3
VI	6	1.2	16	1.8	9	3.9	5	8.6	·	·	4	5.8	25	3.6	10	2.0	15	2.7	68.9	11.3	7	·	·	·	4	8	·	·	3	14	11	2	3	·	9
VII	6	1.5	12	1.9	1	1.0	3	14.3	·	·	2.5	10.2	21.5	5.2	25	2.4	22	2.9	124.6	38.2	29	·	·	·	4	·	3	2	4	15	12	3	6	·	6
VIII	7	1.8	12	3.0	5	1.6	3	6.0	·	·	4	9.5	34	4.4	12	2.7	16	3.2	56.3	17.8	12	·	·	·	6	9	3	2	5	10	8	2	7	·	3
IX	6	1.5	18	1.6	5	1.2	·	·	·	·	2	10.0	25	4.5	8	4.2	26	2.3	30.5	13.2	29	·	·	2	4	5	2	8	7	5	5	1	11	·	1
X	7	1.3	25	2.2	19.5	7.4	11.5	14.6	1	20.0	·	·	9	4.0	6	2.5	14	4.8	26.6	15.7	30	·	·	3	·	11	7	4	5	7	5	1	4	·	·
XI	3	1.0	15	1.5	14	3.6	4	7.8	·	·	4	2.5	20	4.6	16	2.1	14	2.6	68.3	30.3	4	–	3	–	·	5	·	3	12	12	8	1	9	11	·
XII	5	1.0	8	1.5	7	2.1	3	2.0	·	·	·	·	29.5	5.7	13.5	4.6	27	2.9	69.0	23.0	6,11	–	21	–	·	7	2	2	11	12	7	2	3	25	·
Rok	64	1.2	180	1.8	106.5	2.9	47.5	6.9	3	2.2	34.5	6.2	294	5.0	157.5	3.0	208	3.2	666.9	38.2	29.VII	–	54	–	18	83	32	31	88	133	97	17	70	97	23

Szczawnica H_s = 500 m h_w = 32 m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v > 10	v > 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊠	R
I	5	4.7	6.5	2.1	20	1.8	18.5	4.7	·	·	5.5	2.4	11.5	2.0	20	2.0	6	2.4	15.3	7.1	5	13	17	30	·	1	1	5	7	10	4	·	1	14	·
II	9.5	1.4	15	2.0	13	2.0	6	4.6	·	·	3	2.0	5.5	1.8	23	1.9	9	1.8	28.4	6.2	9	1	5	27	·	1	1	1	13	13	10	·	4	13	·
III	3.5	1.3	6	1.2	6.5	2.6	1.5	1.7	1.5	2.3	9	4.8	24	2.4	40	2.5	1	2.5	55.7	9.8	14	·	·	15	·	1	·	4	16	19	15	·	2	8	·
IV	14	2.0	14.5	1.9	22	2.1	13	2.8	2	2.5	2	6.0	16.5	1.6	4	1.5	2	2.1	9.3	3.1	1,8	·	·	3	1	·	·	8	5	8	4	·	1	·	1
V	13	2.0	11	1.5	12.5	1.8	4.5	3.8	4	2.2	4.5	4.2	16	1.9	24.5	2.1	3	2.1	117.3	24.3	17	·	·	1	·	1	·	2	11	20	16	4	2	·	5
VI	13.5	1.7	10	1.6	10.5	2.1	8.5	2.7	4	2.5	3	4.0	8	2.1	21.5	1.9	11	1.8	123.9	24.0	10	·	·	·	4	·	·	3	7	15	12	5	3	·	11
VII	13.5	1.6	11	1.5	7	1.6	6	3.5	2	2.5	3	3.0	20	2.8	28.5	2.4	2	2.3	122.2	37.5	30	·	·	·	8	·	·	3	8	17	12	5	·	·	5
VIII	19	1.5	5	2.0	11	2.3	7	1.9	6	3.8	7.5	3.8	11	2.6	21.5	2.5	5	2.3	63.6	19.2	12	·	·	·	8	·	·	5	8	12	7	3	3	·	3
IX	9	1.2	23.5	1.5	13.5	1.9	8	2.9	5	2.2	5	2.4	9	2.1	12	2.9	5	1.9	35.1	20.0	29	·	·	2	6	·	·	12	4	9	5	1	6	·	1
X	1	1.0	10.5	2.1	31	2.8	16.5	6.2	7	5.3	2	3.0	14.5	2.3	10.5	2.3	·	3.4	27.3	13.2	30	·	·	1	·	3	1	5	7	11	5	1	4	·	·
XI	9	1.8	6	1.7	19	2.4	13	3.8	5	2.6	1	2.0	18	2.1	14	2.8	5	2.3	71.8	22.0	4	·	1	14	·	1	·	2	16	14	10	2	8	4	·
XII	3	2.0	9	1.6	15	2.3	7	2.0	2	5.0	2	2.0	17.5	1.8	31.5	3.1	6	2.3	86.1	17.9	6	12	20	28	·	1	·	6	14	19	12	3	·	25	·
Rok	113	1.6	128	1.7	181	2.1	109.5	3.4	38.5	2.6	47.5	3.3	171.5	2.1	251	2.3	55	2.3	756.0	37.5	30.VII	26	43	121	27	9	3	56	116	167	112	24	34	64	26

Piwniczna

$\varphi = 49°26'$ $\lambda = 20°42'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T												ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	Średnie I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	0.0	-7.7	9.8	4	-19.9	27	-5.7	-1.9	-4.4	-4.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	6.2	6.4	6.7
II	–	–	–	–	4.2	-3.4	10.7	18	-16.7	6	-2.1	2.9	-0.7	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	9.0	6.1	6.9	7.3
III	–	–	–	–	10.3	4.2	20.5	18	-5.7	23	2.9	8.1	4.1	4.8	–	–	–	–	–	–	–	–	–	–	–	–	8.5	7.5	6.5	7.5
IV	–	–	–	–	17.6	3.5	25.4	7	-3.0	10	6.0	16.6	8.9	10.1	–	–	–	–	–	–	–	–	–	–	–	–	4.9	5.2	3.6	4.6
V	–	–	–	–	16.5	5.9	24.3	29	-0.1	13	8.8	14.7	9.8	10.8	–	–	–	–	–	–	–	–	–	–	–	–	9.2	8.7	6.9	8.3
VI	–	–	–	–	23.6	10.7	32.4	27	5.5	21	15.2	21.8	15.0	16.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.4	5.2	5.6
VII	–	–	–	–	22.0	10.1	31.6	4	4.7	7	13.8	20.2	14.1	15.6	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.4	5.9	6.4
VIII	–	–	–	–	23.1	10.8	33.9	11	5.5	31	13.5	21.8	14.9	16.3	–	–	–	–	–	–	–	–	–	–	–	–	6.7	5.9	4.5	5.7
IX	–	–	–	–	22.4	7.3	30.4	18	-1.5	23	9.4	21.2	11.9	13.6	–	–	–	–	–	–	–	–	–	–	–	–	6.5	4.2	4.7	5.1
X	–	–	–	–	17.0	5.3	22.1	19	0.9	22	7.1	15.4	8.9	10.1	–	–	–	–	–	–	–	–	–	–	–	–	6.8	5.0	4.5	5.4
XI	–	–	–	–	8.2	1.1	15.8	3	-8.0	24	2.7	6.4	3.1	3.8	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.3	7.1	7.6
XII	–	–	–	–	-0.1	-8.4	15.3	2	-28.3	25	-5.4	-2.2	-4.7	-4.2	–	–	–	–	–	–	–	–	–	–	–	–	6.7	6.6	7.4	6.9
Rok	–	–	–	–	13.7	3.0	33.9	11.VIII	-28.3	25.XII	5.5	12.1	6.7	7.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.4	5.8	6.4

Krynica

$\varphi = 49°26'$ $\lambda = 20°58'$

I	947.0	963.8	932.5	–	-1.6	-9.2	6.4	4	-19.2	19	-6.8	-3.4	-5.8	-5.4	3.6	4.0	3.8	3.8	9.0	7.9	8.8	8.6	0.4	1.0	0.5	0.6	6.9	6.6	6.4	6.6
II	950.2	963.2	923.3	–	2.4	-4.6	12.4	18	-13.6	6	-3.3	0.6	-1.7	-1.5	4.6	5.3	5.0	5.0	9.4	8.3	9.2	9.0	0.3	1.2	0.4	0.6	8.7	7.3	6.7	7.6
III	946.8	963.0	925.9	–	8.1	-0.1	18.3	18	-8.8	23	1.5	5.8	3.2	3.4	6.0	6.3	6.5	6.3	8.7	6.9	8.4	8.0	0.9	3.4	1.4	1.9	7.6	7.9	6.0	7.2
IV	942.3	948.6	936.1	–	15.6	2.7	21.8	15	-4.4	10	5.1	14.0	8.0	8.8	7.7	8.5	8.5	8.2	8.6	5.3	7.9	7.3	1.3	8.1	2.4	3.9	4.7	5.4	3.7	4.6
V	941.8	949.2	929.3	–	14.6	4.5	22.2	29	-1.1	13	7.5	12.7	8.5	9.3	9.1	9.2	9.6	9.3	8.7	6.3	8.5	7.8	1.4	6.0	1.7	3.0	7.1	8.1	6.7	7.3
VI	946.0	957.7	937.1	–	21.7	9.5	28.6	27	5.0	17	13.1	19.8	14.1	15.3	13.3	13.0	13.5	13.3	8.7	5.8	8.4	7.6	1.9	10.7	2.8	5.1	5.0	6.4	6.5	6.0
VII	945.2	955.5	931.7	–	20.3	8.9	29.7	3	4.1	7	11.8	18.2	13.2	14.1	12.1	11.8	12.8	12.2	8.7	5.8	8.4	7.6	1.9	9.9	2.6	4.8	5.4	7.1	6.7	6.4
VIII	947.8	959.3	937.9	–	21.4	9.5	31.3	11	4.6	31	11.6	19.6	14.0	14.8	12.6	13.5	14.1	13.4	9.1	5.9	8.7	7.9	1.4	10.4	2.2	4.7	5.4	5.7	5.8	5.6
IX	949.8	960.0	939.6	–	20.4	6.6	28.9	18	-1.9	23	8.2	19.1	11.1	12.4	10.1	11.1	11.3	10.8	9.2	5.1	8.4	7.6	1.1	11.7	2.2	5.0	4.0	4.1	3.5	3.9
X	948.7	959.0	927.4	–	14.7	4.8	20.9	20	0.2	22	6.1	13.3	8.5	9.1	8.3	8.9	8.9	8.7	8.8	6.0	8.1	7.6	1.3	6.6	2.4	3.4	5.4	5.3	4.4	5.0
XI	943.1	961.7	933.1	–	5.9	0.1	13.3	7	-10.6	24	4.6	4.9	2.2	2.7	6.6	7.3	6.8	6.9	9.2	8.2	9.2	8.9	0.6	1.8	0.6	1.0	8.9	7.8	7.4	8.0
XII	942.7	962.6	929.6	–	-1.5	-8.8	12.4	2	-28.0	25	-6.2	-2.9	-5.3	-4.9	4.2	4.7	4.3	4.4	9.0	8.3	8.8	8.7	0.5	1.0	0.5	0.7	6.8	7.3	7.3	7.1
Rok	946.0	963.8	923.3	–	11.8	2.0	31.3	11.VIII	-28.0	25.XII	4.2	10.1	5.8	6.5	8.2	8.6	8.8	8.5	8.9	6.6	8.6	8.0	1.1	5.9	1.6	2.9	6.3	6.6	5.9	6.3

Krynica - Góra Parkowa

$\varphi = 49°25'$ $\lambda = 20°58'$

I	–	–	–	–	-2.6	-8.4	5.4	4	-18.4	18	-6.8	-4.1	-6.1	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.1	6.8	6.7	6.9
II	–	–	–	–	1.2	-4.1	13.3	18	-10.6	6	-3.3	0.2	-2.2	-1.9	–	–	–	–	–	–	–	–	–	–	–	–	9.1	7.2	7.4	7.9
III	–	–	–	–	7.3	-0.1	18.0	18	-6.0	22	1.1	5.2	2.8	3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	7.6	5.9	7.3
IV	–	–	–	–	15.1	4.2	22.5	8	-2.8	10	6.2	13.7	8.2	9.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.1	3.7	5.1
V	–	–	–	–	14.1	5.2	21.1	29	0.3	13	7.7	12.1	8.2	9.0	–	–	–	–	–	–	–	–	–	–	–	–	7.4	8.5	6.3	7.4
VI	–	–	–	–	21.1	10.5	27.6	27	6.5	29	13.7	19.3	14.1	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.9	6.1	6.2
VII	–	–	–	–	19.7	9.8	29.2	4	5.6	6	12.2	17.6	13.0	14.0	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.4	6.5	6.7
VIII	–	–	–	–	20.8	10.5	30.1	11	5.8	14,17	12.5	19.2	14.0	14.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.2	4.9	5.7
IX	–	–	–	–	20.5	9.0	28.4	18	1.8	23	10.4	18.7	12.7	13.6	–	–	–	–	–	–	–	–	–	–	–	–	4.7	4.8	3.6	4.4
X	–	–	–	–	14.1	5.9	19.7	20	2.3	17	6.9	12.6	9.1	9.4	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.3	4.3	5.3
XI	–	–	–	–	5.2	0.1	12.1	7	-7.7	23	1.4	4.2	1.9	2.4	–	–	–	–	–	–	–	–	–	–	–	–	9.3	8.1	7.5	8.3
XII	–	–	–	–	-2.1	-8.3	12.0	2	-21.3	25	-5.9	-3.7	-5.5	-5.1	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.3	7.4	7.4
Rok	–	–	–	–	11.2	2.9	30.1	11.VIII	-21.3	25.XII	4.7	9.6	5.8	6.5	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.8	5.9	6.5

Wysowa

$\varphi = 49°26'$ $\lambda = 21°11'$

I	–	–	–	–	-2.9	-8.8	6.1	5	-22.5	19	-6.7	-4.0	-5.6	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.4	6.5	7.5	7.1
II	–	–	–	–	0.8	-4.0	4.8	18	-16.1	6	-2.4	0.2	-1.7	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	9.0	7.4	8.5	8.3
III	–	–	–	–	8.2	-0.4	16.9	10	-12.5	23	2.2	6.8	3.2	3.8	–	–	–	–	–	–	–	–	–	–	–	–	7.0	7.2	6.4	6.9
IV	–	–	–	–	16.1	2.0	22.9	7,15	-7.1	10	7.5	14.9	7.5	9.4	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.0	4.1	4.5
V	–	–	–	–	15.3	3.8	22.5	29	-2.1	13	9.3	13.8	7.8	9.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	7.0	5.9	6.5
VI	–	–	–	–	22.3	8.5	29.2	27	2.5	17	14.9	20.9	13.3	15.6	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.4	5.9	5.3
VII	–	–	–	–	21.0	8.0	29.5	3	4.1	7	13.6	19.0	12.0	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.0	5.9	6.2
VIII	–	–	–	–	21.6	8.7	31.3	11	2.3	31	13.8	20.2	13.2	15.1	–	–	–	–	–	–	–	–	–	–	–	–	5.5	5.8	4.7	5.2
IX	–	–	–	–	19.8	5.8	25.9	18	-5.0	23	9.7	18.9	9.6	12.0	–	–	–	–	–	–	–	–	–	–	–	–	4.4	3.9	3.6	4.0
X	–	–	–	–	14.3	4.5	20.4	20	-1.7	22	7.4	13.4	7.9	9.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.0	3.8	4.9
XI	–	–	–	–	5.3	0.4	12.5	7	-11.7	21	2.3	4.4	2.7	3.0	–	–	–	–	–	–	–	–	–	–	–	–	8.9	8.0	8.5	8.5
XII	–	–	–	–	-1.8	-8.8	10.0	2	-29.7	24	-6.1	-3.3	-5.0	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.7	7.5	7.6	7.6
Rok	–	–	–	–	11.7	1.6	31.3	11.VIII	-29.7	24.XII	5.5	10.4	5.4	6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.3	6.0	6.2

Piwniczna

$H_s = 380$ m — $h_w =$ 16 m (I–VIII), 17,4 m (IX–XII) — 1961

MIESIĄC	ROZKŁAD WIATRU [%D, %mD]																Średnia prędkość	OPAD R			LICZBA DNI (n)											
	N		NE		E		SE		S		SW		W		NW		C				Temperatura T				Wiatr v			Opad R				
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Max<-10°	Max<0°	Min<0°	Max>25°	v≥10	v≥15	●	●	R≥0.1	R≥10	R≥100	≡	⊞	R≥50
I	·	·	3	2,7	2,3	2,3	15	3,8	·	·	1	1,0	2,3	2,1	4	3,2	24	1,9	15,6	6,0	5	10	14	30	·	·	·	5	14	11	5	·	1	2,2	·
II	3	2,7	2	2,5	1,8	2,2	9	3,1	·	·	2	1,5	2,0	2,0	1	3,0	29	1,5	37,1	9,2	9	1	1	24	·	·	·	2	12	13	8	·	4	1,3	·
III	1	2,0	·	·	2	3,5	3	2,0	·	·	5	2,8	5,7	2,7	3	1,3	22	2,0	44,9	7,8	14	·	·	10	·	·	·	2	17	21	13	·	1	6	·
IV	·	·	2	2,0	1,2	2,9	5	2,5	1	4,0	1	3,0	3,0	2,3	4	3,5	35	1,6	9,5	3,8	1	·	·	3	1	·	·	7	5	6	3	·	·	·	1
V	·	·	1	2,0	8	2,2	3	2,7	1	2,0	2	2,5	3,5	2,1	3	2,7	40	1,3	120,7	29,2	17	·	·	1	·	·	·	·	18	19	1,8	3	9	·	6
VI	·	·	4	2,5	9	2,0	2	1,5	3	1,3	2	2,0	2,6	1,9	1	1,0	43	1,0	78,1	29,6	12	·	·	·	8	·	·	3	7	16	1,0	2	4	·	1,0
VII	·	·	·	·	2	1,5	5	2,8	1	1,0	6	1,8	2,8	1,9	3	2,3	48	0,9	104,8	31,0	30	·	·	·	8	·	·	4	10	15	11	4	4	·	5
VIII	·	·	·	·	6	2,3	11	2,0	2	1,0	9	1,9	2,2	2,0	1	2,0	42	1,1	60,4	32,2	12	·	·	·	9	·	·	4	8	10	7	1	5	·	4
IX	·	·	·	·	6	2,7	·	·	3	1,7	7	1,4	2,1	1,7	1	3,0	52	0,8	17,5	8,2	29	·	·	2	10	·	·	8	7	8	4	·	10	·	2
X	·	·	·	·	9	2,4	2,4	3,0	4	1,8	3	1,7	1,0	1,1	·	·	43	1,3	29,0	14,4	30	·	·	·	·	·	·	8	10	10	4	1	8	·	·
XI	·	·	·	·	1	2,0	2,3	2,1	2	1,0	7	1,6	2,1	1,7	1	1,0	35	1,1	68,9	17,6	4	·	·	7	·	·	·	2	16	14	9	3	7	6	·
XII	·	·	·	·	6	2,3	9	2,3	4	2,0	8	1,5	2,9	3,0	6	3,2	34	1,7	87,3	18,1	6	12	16	25	·	·	·	4	15	15	11	3	2	2,5	·
Rok	4	0,4	1,2	1,0	10,2	2,4	10,9	2,3	2,1	1,3	5,3	1,9	3,2,2	2,0	2,8	2,2	444	1,4	673,8	32,2	12.VIII	2,3	3,1	10,2	3,6	·	·	49	139	158	103	17	55	7,2	28

Krynica

$H_s = 613$ m — $H_b = 609,6$ m — $h_w = 18$ m

I	12,5	3,3	0,5	5,0	·	·	2,0	3,0	28,5	3,5	4,5	7,3	2	3,0	8	3,6	20	2,7	174	6,4	5	14	20	30	·	1	·	4	15	13	7	·	1	2,6	·
II	0,5	3,0	·	·	0,5	3,0	10,5	3,1	26,5	2,1	5,5	2,1	5,5	5,4	9	2,3	26	1,8	385	139	9	2	4	28	·	·	·	3	15	15	9	1	8	2,7	·
III	4,5	1,7	·	·	·	·	3	3,0	10	2,7	11	4,5	2,2	5,7	22,5	3,4	20	3,2	49,9	7,0	14	·	·	15	·	·	·	3	13	20	14	·	·	11	·
IV	9,5	2,1	0,5	2,0	·	·	1,0	2,2	17,5	3,3	6	3,2	2	6,0	11,5	2,7	33	1,8	9,5	3,5	8	·	·	4	·	·	·	8	6	7	3	·	1	·	1
V	12,5	2,5	1	1,0	·	·	6,5	2,4	10,5	3,3	7	3,0	10,5	3,8	1,9	2,7	26	2,1	79,7	18,5	17	·	·	1	·	·	·	1	12	18	13	2	1	·	4
VI	12,5	2,3	6	1,8	·	·	1,0	2,2	13,5	3,0	4,5	3,4	3,5	4,1	9	2,9	31	1,8	100,3	32,6	9	·	·	·	4	·	·	3	7	12	1,0	4	3	·	1,0
VII	14,5	1,9	1,5	2,3	·	·	7	2,0	1,6	2,8	6	2,7	6	4,0	1,1	3,6	31	1,8	107,4	22,8	29	·	·	·	6	1	·	3	8	1,9	1,3	3	·	·	5
VIII	8,5	2,5	1,1	1,0	0,5	1,0	11,5	2,7	1,8	3,2	10,5	2,7	3	4,3	1,3	3,0	27	2,1	67,2	11,1	3	·	·	·	7	·	·	5	7	11	11	1	3	·	4
IX	5	1,9	3	1,8	·	·	3	3,3	15,5	3,1	6,5	3,5	4,5	3,7	9,5	2,7	43	1,5	12,7	3,2	6	·	·	1	4	·	·	12	5	1,0	6	·	1	·	1
X	2,5	3,4	·	·	3	4,3	2,6	4,1	1,0	3,3	7	4,9	5	3,6	10,5	2,9	29	2,6	40,5	19,1	30	·	·	·	·	·	·	8	8	9	8	1	2	·	·
XI	11,5	2,7	1	1,0	0,5	3,0	1,5	2,3	3,0	2,9	3,5	3,0	2	3,0	11,5	3,6	1,5	2,4	68,2	13,0	11	1	2,1	2,2	·	·	·	1	2,0	1,5	9	2	7	9	·
XII	2,9	4,0	2,5	1,8	·	·	4,5	2,1	1,9	3,0	7,5	3,7	3,5	8,3	9	3,7	18	3,0	104,0	25,3	11	1,3	2,0	2,6	·	2	·	4	1,6	1,9	1,2	6	2	2,5	·
Rok	12,3	2,6	1,7	1,5	4,5	0,9	12,7	2,7	2,1,5	3,0	7,6,5	3,7	6,9,5	4,6	1,4,3,5	3,1	3,1,9	2,2	69,5,3	32,6	9.VI	3,0	4,6	11,7	2,1	4	·	55	132	168	115	20	29	9,8	2,5

Krynica - Góra Parkowa

$H_s = 740$ m — $h_w = 20,4$ m

I	1,9	3,1	1,1	2,2	·	·	4,5	3,1	4,7	3,6	4,5	2,4	1	2,0	6	3,4	·	3,2	14,0	5,4	5	12	2,5	30	·	1	1	4	14	11	3	·	6	2,9	-
II	10,5	2,5	4,5	1,9	·	·	9	2,9	3,9,5	2,6	6,5	2,5	·	·	1,2	3,3	2	2,6	34,8	11,4	9	1	1,1	28	·	1	·	1	1,6	12	8	1	12	2,8	-
III	16,5	4,0	1	5,5	·	·	0,5	7,0	12,5	3,7	1,8	3,2	9,5	2,5	3,5	4,8	·	4,0	43,7	8,1	2,8	·	·	1,4	·	5	1	3	1,6	2,0	1,3	·	3	1,1	-
IV	13,5	2,1	1,6	2,5	2	1,8	16,5	2,4	2,3	3,5	1,2	2,7	0,5	3,0	6,5	6,5	·	3,0	9,9	3,0	8	·	·	4	·	·	·	6	6	1,1	4	·	2	·	-
V	3,4	3,1	10,5	2,2	·	·	3,5	3,4	1,5	4,1	9,5	2,9	6,5	3,0	1,3	2,7	1	3,1	75,1	17,4	1,7	·	·	·	4	·	2	·	1,1	1,8	1,2	2	6	·	-
VI	22,5	2,5	1,3	2,5	1,5	2,7	7,5	2,6	2,2,5	2,5	8	3,2	6	2,0	8	2,9	1	2,6	90,5	26,1	9	·	·	·	4	·	·	1	7	1,3	8	4	2	·	-
VII	3,1	3,2	9,5	1,8	1	2,0	0,5	2,0	2,0,5	3,9	1,4	2,7	4	2,5	12,5	3,0	·	3,1	107,1	24,4	2,9	·	·	·	3	3	1	2	8	1,8	1,3	3	3	·	-
VIII	2,1,5	3,2	5,5	2,1	1	1,0	4,5	2,1	2,2,5	3,5	1,7	3,0	3,5	2,4	1,6,5	2,9	1	3,0	57,9	10,7	3	·	·	·	6	2	1	5	7	1,3	1,0	1	2	·	-
IX	10,5	2,2	1,9,5	2,3	·	·	9,5	2,2	2,4	2,6	1,3,5	3,1	1	3,0	1,2	2,7	·	2,5	10,3	3,2	6	·	·	·	4	·	·	1,1	7	8	4	·	2	·	-
X	14,5	3,2	8,5	3,3	1,5	2,7	10,5	3,1	4,5,5	5,4	6	2,9	1	1,0	4,5	2,6	1	4,1	39,0	19,5	3,0	·	·	·	·	3	·	8	9	1,0	7	1	5	·	-
XI	2,0	3,5	0,5	1,0	·	·	7,5	2,5	4,4	3,0	1,1,5	3,1	3	2,3	3,5	3,9	·	3,1	68,0	12,2	5	·	3	1,3	·	·	·	·	2,0	1,4	9	3	1,4	6	-
XII	3,1,5	5,0	7	2,3	·	·	·	·	3,5	3,9	4	3,2	·	·	1,5,5	5,4	·	4,4	92,2	20,8	11	1,2	2,0	2,6	·	2	1	1	1,6	1,8	1,0	5	4	2,5	-
Rok	2,4,5	3,1	10,6,5	2,5	7	0,8	7,4	2,8	3,5,1	3,5	1,2,4,5	2,9	3,6	2,0	1,4,5	3,7	6	3,2	64,2,5	26,1	9.VI	2,5	5,9	11,5	1,7	1,9	5	4,2	1,3,7	1,6,6	1,0,1	2,0	6,1	9,9	-

Wysowa

$H_s = 525$ m — $h_w = 25,5$ m

I	8	4,5	·	·	·	·	4,2	5,9	1,7	3,4	·	·	·	·	2,2	3,7	4	4,6	21,4	7,3	5	1,4	2,5	30	·	7	·	5	1,7	1,5	5	·	2	2,9	·
II	5	3,4	·	·	·	·	3,7	4,1	1,6	3,3	·	·	3	1,3	1,2	3,1	1,1	3,1	33,9	10,4	9	2	1,0	2,6	·	·	·	1	1,8	1,5	1,1	1	1,1	2,7	·
III	3	3,0	·	·	·	·	4	4,2	8,5	2,1	3,5	2,9	1,1	3,4	5,4	3,9	9	3,3	41,4	6,7	3,1	1	·	1,4	·	3	1	4	1,2	1,9	1,6	·	1	7	1
IV	1,2	1,9	2	4,8	3,5	2,1	2,9	3,2	1,1	2,5	3	3,7	0,5	1,0,0	1,4	3,7	1,5	2,5	9,1	2,3	8	·	·	9	·	2	·	9	7	8	5	·	·	·	2
V	9,5	1,8	2	2,0	·	·	8,5	4,4	7,5	3,6	·	·	7,5	2,0	3,2	2,6	2,6	2,0	86,5	16,3	3	·	·	4	·	·	·	1	7	2,0	1,2	2	·	·	1
VI	5,5	3,0	2	2,0	1	1,0	16,5	3,7	1,4,5	3,3	4	2,8	1	5,0	2,0,5	3,5	2,5	2,4	89,9	28,9	1,3	·	·	·	6	·	·	3	5	1,8	1,2	3	1	·	1,0
VII	9	4,1	·	·	2	3,5	1,0	5,5	1,1	5,1	2	3,0	0,5	1,0	3,7,5	3,3	2,1	3,1	106,4	29,7	2,9	·	·	·	6	1	1	2	8	1,7	1,5	4	·	·	3
VIII	2,5	3,6	·	·	1	5,0	1,0,5	4,2	8	3,6	6	2,0	3,5	2,6	2,8,5	3,4	3,3	2,2	110,7	56,5	9	·	·	·	7	·	·	4	7	1,4	1,0	2	·	·	3
IX	9	2,2	0,5	4,0	0,5	4,0	1,6,5	3,5	7,5	3,1	·	·	3,5	2,6	1,3,5	2,7	3,7	1,7	19,1	5,0	6	·	·	3	4	·	·	1,3	6	1,0	8	·	3	·	1
X	3	2,2	1,5	4,7	0,5	4,0	4,2	6,5	1,1	4,8	·	·	·	·	1,4	3,5	2,1	4,2	39,0	18,3	30	·	·	3	·	6	1	9	8	1,0	7	1	2	·	·
XI	10,5	2,8	·	·	·	·	2,9,5	4,0	2,6,5	4,1	1,5	3,3	1,5	2,7	1,5,5	3,8	5	3,6	57,8	12,4	1,1	1	4	1,1	·	1	·	1	1,9	1,8	1,0	2	7	6	·
XII	10,6	7,2	·	·	·	·	2,2,5	5,6	1,2,5	3,6	2	3,2	·	·	2,7,5	6,5	1,8	4,6	76,8	20,9	1,1	1,2	2,0	2,5	·	3	·	1	1,8	2,3	1,0	3	3	2,5	·
Rok	8,7,5	3,3	8	1,5	8,5	1,6	2,7,0	4,6	1,5,1	3,5	2,2	1,7	3,2	2,6	2,9,1	3,6	2,2,5	3,1	69,2,0	56,5	9.VIII	3,0	5,9	1,2,5	2,3	2,3	3	5,3	1,3,2	1,8,7	1,2,1	1,8	3,0	9,4	2,1

Barwinek

$\varphi = 49°26'$ $\lambda = 21°41'$ 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	P_{0m}	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-25	-92	76	4	-248	27	-66	-39	-59	-56	–	–	–	–	–	–	–	–	–	–	–	–	83	71	74	76
II	–	–	–	–	07	-37	36	27	-103	15	-18	-02	-16	-13	–	–	–	–	–	–	–	–	–	–	–	–	90	91	83	88
III	–	–	–	–	82	-01	169	10	-99	23	24	64	33	38	–	–	–	–	–	–	–	–	–	–	–	–	86	82	72	80
IV	–	–	–	–	161	19	221	15	-50	10	69	149	72	90	–	–	–	–	–	–	–	–	–	–	–	–	49	55	41	48
V	–	–	–	–	154	37	237	29	-12	13	87	139	77	95	–	–	–	–	–	–	–	–	–	–	–	–	76	75	74	75
VI	–	–	–	–	220	82	291	27	25	21	148	208	128	153	–	–	–	–	–	–	–	–	–	–	–	–	58	58	63	60
VII	–	–	–	–	208	83	289	3	11	7	140	193	123	145	–	–	–	–	–	–	–	–	–	–	–	–	62	63	65	63
VIII	–	–	–	–	214	92	312	11	15	31	135	202	139	154	–	–	–	–	–	–	–	–	–	–	–	–	51	50	56	52
IX	–	–	–	–	197	53	265	18	-43	23	103	190	105	126	–	–	–	–	–	–	–	–	–	–	–	–	54	49	43	49
X	–	–	–	–	147	43	221	20	-17	22	77	140	82	95	–	–	–	–	–	–	–	–	–	–	–	–	55	54	46	52
XI	–	–	–	–	61	08	131	7	-114	21	24	49	36	36	–	–	–	–	–	–	–	–	–	–	–	–	92	88	83	88
XII	–	–	–	–	-14	-82	103	5	-300	25	-50	-34	-46	-44	–	–	–	–	–	–	–	–	–	–	–	–	87	84	84	85
Rok	–	–	–	–	118	17	312	11.VIII	-300	25.XII	56	105	56	68	–	–	–	–	–	–	–	–	–	–	–	–	70	68	65	68

Myczkowce

$\varphi = 49°26'$ $\lambda = 22°25'$

I	–	–	–	–	-01	-	103	4	–	–	-65	-14	-49	-44	–	–	–	–	–	–	–	–	–	–	–	–	63	55	47	55
II	–	–	–	–	37	-30	104	18	-108	15	-18	27	00	02	–	–	–	–	–	–	–	–	–	–	–	–	78	68	67	71
III	–	–	–	–	89	09	169	18	-71	23	32	68	49	50	–	–	–	–	–	–	–	–	–	–	–	–	80	82	62	75
IV	–	–	–	–	171	32	234	7,8,15	-42	10	69	159	95	104	–	–	–	–	–	–	–	–	–	–	–	–	39	53	34	42
V	–	–	–	–	166	52	254	29	11	17,20,21	83	150	95	106	–	–	–	–	–	–	–	–	–	–	–	–	71	74	56	67
VI	–	–	–	–	234	105	299	27,28	55	17	135	218	157	167	–	–	–	–	–	–	–	–	–	–	–	–	49	52	48	50
VII	–	–	–	–	221	96	299	4	45	7,8	129	203	151	158	–	–	–	–	–	–	–	–	–	–	–	–	58	57	44	53
VIII	–	–	–	–	226	110	323	11	43	31	128	212	167	168	–	–	–	–	–	–	–	–	–	–	–	–	53	51	57	54
IX	–	–	–	–	213	77	289	17,18	-02	22,23	92	204	135	142	–	–	–	–	–	–	–	–	–	–	–	–	45	39	27	37
X	–	–	–	–	170	45	259	20	05	13,17,24	66	164	91	103	–	–	–	–	–	–	–	–	–	–	–	–	50	44	30	41
XI	–	–	–	–	88	11	179	1	-88	23	34	75	42	48	–	–	–	–	–	–	–	–	–	–	–	–	84	77	69	77
XII	–	–	–	–	02	-77	139	5	-326	25	-43	-15	-32	-30	–	–	–	–	–	–	–	–	–	–	–	–	81	83	65	76
Rok	–	–	–	–	135	-	323	11.VIII	-326	25.XII	54	121	75	81	–	–	–	–	–	–	–	–	–	–	–	–	63	61	50	58

Jaworzyna Krynicka

$\varphi = 49°25'$ $\lambda = 20°54'$

I	–	–	–	–	-35	-90	29	4	-192	18	-66	-53	-62	-61	–	–	–	–	–	–	–	–	–	–	–	–	65	63	63	64
II	–	–	–	–	08	-43	112	18	-106	6	-27	-07	-22	-20	–	–	–	–	–	–	–	–	–	–	–	–	70	64	58	64
III	–	–	–	–	44	-12	146	18	-70	23	01	26	14	14	–	–	–	–	–	–	–	–	–	–	–	–	88	84	64	79
IV	–	–	–	–	123	35	196	7	-40	10	63	109	65	76	–	–	–	–	–	–	–	–	–	–	–	–	62	59	48	56
V	–	–	–	–	114	46	188	27	-12	12	70	97	68	76	–	–	–	–	–	–	–	–	–	–	–	–	83	88	75	82
VI	–	–	–	–	183	99	251	27	47	1	133	170	128	140	–	–	–	–	–	–	–	–	–	–	–	–	62	72	72	69
VII	–	–	–	–	168	87	256	3	53	6	119	153	115	126	–	–	–	–	–	–	–	–	–	–	–	–	63	69	69	67
VIII	–	–	–	–	180	96	273	11	50	17	121	165	128	136	–	–	–	–	–	–	–	–	–	–	–	–	68	66	55	63
IX	–	–	–	–	169	89	250	18	34	22	111	160	115	125	–	–	–	–	–	–	–	–	–	–	–	–	47	46	37	43
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	273	11.VIII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Żegiestów-Zdrój

$\varphi = 49°22'$ $\lambda = 20°49'$

I	–	–	–	–	-06	-76	89	4	-204	27	-57	-18	-45	-41	–	–	–	–	–	–	–	–	–	–	–	–	77	72	76	75
II	–	–	–	–	33	-35	112	18	-154	6	-22	22	-10	-05	–	–	–	–	–	–	–	–	–	–	–	–	96	74	80	83
III	–	–	–	–	94	08	198	10	-63	23	25	77	37	44	–	–	–	–	–	–	–	–	–	–	–	–	86	80	72	79
IV	–	–	–	–	176	30	255	7	-38	10	49	161	86	96	–	–	–	–	–	–	–	–	–	–	–	–	58	58	50	55
V	–	–	–	–	164	56	238	6	-05	13	80	147	92	103	–	–	–	–	–	–	–	–	–	–	–	–	95	92	74	87
VI	–	–	–	–	234	105	304	27	56	21	130	216	148	161	–	–	–	–	–	–	–	–	–	–	–	–	77	62	63	67
VII	–	–	–	–	218	99	317	3	49	7	121	201	140	150	–	–	–	–	–	–	–	–	–	–	–	–	66	78	73	72
VIII	–	–	–	–	228	104	330	11	55	31	119	214	145	156	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	222	68	302	18	-22	23	80	214	119	133	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	161	53	219	20	02	22	67	152	89	99	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	67	09	136	3	-96	24	22	61	29	35	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-08	-88	146	2	-292	26	-61	-23	-48	-45	–	–	–	–	–	–	–	–	–	–	–	–	78	77	77	77
Rok	–	–	–	–	132	28	330	11.VIII	-292	26.XII	46	119	65	74	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Barwinek

$H_s = 420$ m

$h_w = 16$ m

1961

MIESIĄC	ROZKŁAD WIATRU °D, %D																	OPAD R			LICZBA DNI (n)												
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość	Suma	Max	Data	Temperatura T				Wiatr v				Opad R				
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n					Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	> 10 m/s	> 15 m/s	●	●	≥ 0,1 mm	≥ 1,0 mm	≥ 10,0 mm	≡	▦	≋
I	15,5	2,4	0,5	3,0	1	1,0	6,5	4,0	3,8	4,1	13,5	3,9	·	·	1,8	2,5	·	3,5	34,7	8,9	5	13	22	30	·	2	1	2	19	15	4,0	·	–	–	–
II	5,5	1,1	·	·	·	·	4,5	2,0	28,5	3,6	24,5	2,0	2,5	1,6	16,5	2,1	2	2,4	31,3	9,0	9	1	11	26	·	·	·	·	20	17	10	·	–	–	–
III	4,5	2,8	·	·	·	·	4,5	2,3	16,5	3,0	13,5	1,8	12	1,8	4,2	3,0	·	2,6	32,3	5,4	31	·	1	15	·	·	·	·	17	18	13	·	–	–	–
IV	1,8	2,8	7,5	2,2	3	2,0	6,5	1,6	2,6	3,0	11,5	3,0	4	1,8	11,5	1,8	2	2,5	7,6	3,2	3	·	·	9	·	·	·	7	7	6	3	·	–	–	–
V	18,5	1,8	6	1,6	2	1,2	4	2,1	1,4	3,0	1,0	1,8	2	1,2	3,5,5	1,8	2	1,9	6,1,0	1,0,4	7	·	·	4	·	·	·	·	12	1,8	1,0	2	–	–	–
VI	1,8,5	1,8	2	1,8	2,5	2,0	4,5	1,6	3,2,5	2,2	9	1,7	2,5	1,4	1,8,5	1,4	·	1,8	7,2,9	1,9,7	1,3	·	·	·	5	·	·	·	7	1,6	1,1	2	–	–	–
VII	2,5	2,1	2,5	1,0	·	·	4	1,9	1,7	2,0	1,8	2,8	2	1,0	2,2,5	1,2	2	1,9	1,1,9,2	3,8,0	2,9	·	·	·	6	·	·	1	9	2,1	1,4	3	–	–	–
VIII	1,4	2,3	2	2,0	·	·	4	3,9	1,7	2,9	2,3	1,8	4	1,2	2,0	1,6	9	1,9	5,2,1	1,1,8	1,6	·	·	·	7	·	·	5	6	1,3	1,0	1	–	–	–
IX	1,4,5	1,9	3	1,3	2	1,5	1	1,0	2,5	2,2	1,0	2,0	5,5	1,3	2,1	1,3	8	1,6	1,2,8	3,3	2,6	·	·	4	3	·	·	9	8	1,0	5	·	–	–	–
X	1,4,5	2,1	3,5	2,7	2,5	1,0	1,1,5	3,2	4,5,5	4,1	6	2,5	0,5	3,0	9	2,5	·	3,3	2,9,7	1,4,4	3,0	·	·	4	·	·	·	6	7	9	5	1	–	–	–
XI	1,7,5	2,1	·	·	·	·	2,5	2,6	4,4,5	2,7	1,1	3,0	8	1,6	6,5	3,5	·	2,6	5,9,7	1,2,3	1,1	1	3	1,0	·	·	·	·	2,4	1,8	1,5	2	–	–	–
XII	4,4,5	3,0	·	·	·	·	·	·	3,0	5,2	8	3,1	2	1,0	8,5	2,7	·	3,7	1,2,2,3	3,9,1	1,1	1,3	2,0	2,5	·	·	·	·	2,0	2,6	1,4	4	–	–	–
Rok	2,1,0,5	2,2	2,6	1,3	1,3	0,7	5,3,5	2,2	3,3,4,5	3,2	1,5,8	2,4	4,5	1,4	2,2,9,5	2,1	2,5	2,5	6,3,5,6	3,9,1	1,1.XII	2,8	5,7	1,2,7	2,1	2	1	3,0	1,5,6	1,8,7	1,2,0	1,5	–	–	–

Myczkowce

$H_s = 410$ m

$h_w = 20,5$ m

I	·	·	1	7,0	4	2,2	4	3,2	2,5	2,7	2	1,5	·	·	4	3,8	5,3	1,2	2,1,8	4,4	1,4	–	1,3	–	·	·	·	8	7	9	8	·	–	2,3	–
II	·	·	3	1,7	·	·	2	2,5	9	3,0	7	2,1	7	2,7	·	·	5,6	0,8	2,5,3	7,0	1,3	1	1	2,0	·	·	·	2	1,4	1,0	8	·	–	1,8	–
III	·	·	·	·	·	·	·	·	7	2,9	1,2	2,9	3,7	3,4	1,3	4,2	2,4	2,5	2,1,4	4,6	3,1	·	·	1,2	·	1	·	3	1,6	1,0	8	·	–	2	–
IV	1	2,0	·	·	1,0	2,2	5	1,8	7	2,9	9	3,0	4	6,5	1	6,0	5,3	1,2	2,1,2	9,0	1,8	·	·	5	·	·	·	1,0	7	5	3	·	–	·	–
V	3	3,7	1	1,0	4	1,2	1	3,0	1	4,0	3	3,0	1,1	3,3	7	2,9	6,2	1,0	5,7,8	1,9,0	2,9	·	·	·	1	·	·	·	1,0	1,0	6	3	–	·	–
VI	·	·	·	·	2	2,0	3	4,7	1	3,0	·	·	7	2,4	4	3,2	7,3	0,6	1,1,0,2	2,0,0	9	·	·	·	6	·	·	5	4	1,1	1,1	6	–	·	–
VII	2	2,5	·	·	·	·	2	2,5	4	5,2	1,0	4,2	6	3,5	7	2,6	6,2	1,2	9,1,6	3,9,4	2,9	·	·	·	8	1	1	2	6	1,2	1,0	3	–	·	–
VIII	8	2,9	·	·	·	·	3	2,0	6	3,5	7	2,9	·	·	1,3	3,8	5,6	1,3	4,0,0	9,8	1,6	·	·	·	9	·	·	5	7	1,1	1,0	·	–	·	–
IX	2	2,0	2	1,5	2	1,5	1	1,0	2	2,0	1,1	3,8	6	2,7	7	3,9	5,7	1,1	1,8,5	6,7	2,6	·	·	2	6	·	·	1,2	2	8	6	·	–	·	–
X	·	·	1	3,0	3	2,3	7	2,6	6	2,8	7	5,0	5	3,4	5	3,6	5,9	1,2	2,7,7	1,3,5	3,0	·	·	·	1	·	·	1,2	5	5	4	1	–	·	–
XI	2	3,5	·	·	1	2,0	4	5,2	1,0	4,5	1,1	4,0	1,3	4,5	3	4,0	4,6	2,1	1,4,1	3,5	1,1	·	1	1,1	·	·	·	1	1,8	6	6	·	–	4	–
XII	1	5,0	·	·	1	2,0	5	3,0	5	3,4	1,2	6,0	3	5,3	1,7	5,1	4,9	2,3	5,9,4	1,5,7	7	1,2	1,5	2,2	·	1	·	2	1,8	1,4	8	2	–	2,5	–
Rok	1,9	1,8	8	1,2	2,7	1,3	3,7	2,6	8,3	3,3	9,1	3,2	9,9	3,1	8,1	3,6	6,5,0	1,4	5,0,9,0	3,9,4	2,9.VII	–	3,0	–	3,1	3	1	6,2	1,1,4	1,1,1	8,8	1,5	–	7,2	–

Jaworzyna Krynicka

$H_s = 995$ m

$h_w = 15$ m (I-VII), $15,7$ m (VIII-XII)

I	12,5	5,0	3	2,3	7	2,4	1	3,0	2,5	4,6	2,6,5	4,9	1,6,5	4,2	1,5	4,0	9	3,9	1,8,2	7,1	5	1,2	2,0	3,0	·	2	·	4	1,4	1,8	4	·	9	3,1	·
II	1,5	2,3	·	·	·	·	·	·	3	5,2	3,4	3,3	1,1,5	3,7	1,9	3,7	1,5	2,9	4,5,3	1,6,2	9	1	1,4	2,6	·	2	·	7	1,4	1,4	1,1	1	1,0	2,8	·
III	4	3,0	·	·	·	·	·	·	1	5,0	1,3	4,9	3,9,5	5,6	3,4,5	9,2	1	6,6	6,7,0	1,4,4	1,4	·	7	1,9	·	1,3	7	·	1,7	2,2	1,4	1	3	2,8	·
IV	3,5	3,6	1,8	2,7	8	2,2	6	1,0	5	2,2	2,5	3,0	1,2	4,0	5,5	4,4	7	2,7	1,2,3	3,6	2,8	·	·	4	·	1	1	4	6	7	4	·	2	2	·
V	1,3	1,5	1,0	2,8	1	3,0	·	·	3	2,3	1,8,5	2,4	7,5	4,5	1,9,5	3,7	1,3	2,6	1,3,4,0	2,3,6	1,7	·	·	1	·	·	·	·	1,9	2,4	1,8	5	6	·	4
VI	7	2,4	9,5	2,6	4,5	1,8	3,5	1,3	3	2,3	2,7,5	2,7	1,0,5	3,7	1,3,5	3,8	1,1	2,5	1,2,7,3	3,9,0	1,2	·	·	·	1	·	·	·	6	1,4	1,1	5	3	·	7
VII	8,5	2,4	2	2,0	·	·	·	·	·	·	3,0	2,8	1,9,5	4,3	2,0	4,8	1,3	3,1	1,2,4,5	3,2,2	3,0	·	·	·	2	1	1	2	1,3	1,6	1,6	3	·	·	3
VIII	4	3,0	1,1	3,2	2	3,0	7,5	2,9	2	1,5	3,6,5	3,5	1,3	4,3	1,1	5,7	6	3,5	5,1,6	9,6	3	·	·	·	4	3	1	3	1,0	1,2	1,0	·	1	·	2
IX	1,4	3,0	1,1	3,6	1	1,0	4,5	3,2	8	1,5	2,2,5	2,4	2,0	3,6	9	3,4	1,0	2,6	3,1,6	8,3	1,0	·	·	·	·	·	·	9	5	1,1	7	·	·	·	1
X	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Żegiestów-Zdrój

$H_s = 440$ m

$h_w = 16,1$ m

I	8,5	1,5	1,0	3,0	1,1,5	2,5	3,5	1,7	1,9,5	1,9	4,5	1,4	1,8,5	2,2	1	1,0	1,6	1,8	1,0,1	5,6	5	1,0	1,7	2,9	·	·	·	4	1,8	8	4	·	2	1,3	·
II	1,5,5	1,3	3	2,0	2,5	1,6	3,5	2,0	1,7	2,0	5	1,6	1,9,5	1,8	1	5,0	1,7	1,4	3,2,2	1,0,8	9	1	2	2,6	·	·	·	1	1,8	1,4	8	1	4	1,7	·
III	1,2,5	1,7	1,1,5	2,0	2	2,0	2	2,0	1,5	3,7	8	3,7	4,3,5	3,8	7	3,0	5	2,9	4,4,6	1,1,0	1,4	·	·	1,1	·	·	·	3	2,0	1,8	1,2	1	1	6	·
IV	7,5	2,1	1,1,5	2,2	1,3,5	1,8	4	1,6	1,5	2,9	6	3,2	1,2,5	3,6	3	1,7	1,7	2,0	4,0	1,9	3,0	·	·	3	1	·	·	8	1,1	4	1	·	1	·	·
V	6,5	2,0	1,0,5	2,2	4,5	2,3	3	2,3	8,5	2,5	1,2	2,5	2,7,5	2,8	7,5	2,3	1,3	2,1	8,0,4	2,4,7	1,7	·	·	1	·	·	·	·	2,3	1,8	1,3	1	6	·	4
VI	9,5	1,4	8	1,9	6,5	1,8	5,5	1,7	8	2,7	6,5	2,5	1,6,5	2,2	6,5	3,1	2,3	1,6	8,3,7	2,0,3	7	·	·	·	8	·	·	3	1,0	1,3	9	3	7	·	8
VII	7	1,9	1,0	1,8	7,5	1,6	3	2,3	5	2,3	1,0,5	2,6	2,3	2,7	5	1,9	2,2	1,7	8,8,8	2,5,1	2,9	·	·	·	8	·	·	3	1,6	1,8	1,6	3	4	·	5
VIII	5,5	1,5	2,5	1,6	5	1,8	4	1,5	9	2,4	1,4,5	2,6	1,7	2,3	7,5	1,8	2,8	1,5	3,7,7	9,4	3	·	·	·	9	·	·	–	–	1,2	9	·	1,0	·	2
IX	3,5	1,1	7	1,7	3,5	2,3	2,5	2,2	1,2	2,8	7	2,1	2,1,5	2,3	5	2,3	2,8	1,5	1,6,7	6,8	2,9	·	·	3	7	·	·	–	–	1,0	4	·	1,8	·	·
X	4,5	2,4	6,5	2,6	6	2,2	4	3,1	2,0,5	3,5	8,5	2,7	1,4,5	1,8	2,5	1,8	2,6	1,9	2,7,1	1,4,0	3,0	·	·	·	·	·	·	–	–	9	4	1	1,0	·	·
XI	5,5	1,4	7	1,6	2,5	2,4	5	2,2	1,0,5	2,1	9,5	2,1	2,7	2,5	6	2,1	1,7	1,8	6,2,0	1,4,5	4	·	1	9	·	·	·	–	–	1,6	9	3	4	8	·
XII	1,2	2,0	5,5	2,4	1	2,5	1,5	3,0	9	2,6	6	2,3	4,0	2,6	4	2,9	1,4	2,1	6,7,2	1,1,3	6	1,3	1,8	2,5	·	·	·	3	2,1	1,7	1,0	4	1	2,5	·
Rok	9,8	1,7	9,3	2,1	6,6	2,1	4,1,5	2,1	1,3,5,5	2,6	9,8	2,4	2,8,1	2,6	5,6	2,4	2,2,6	1,9	5,5,4,5	2,5,1	2,9.VII	2,4	3,8	1,0,7	3,3	·	·	–	–	1,5,7	9,9	1,7	6,8	6,9	1,9

Bukowina Tatrzańska — φ = 49°21' — λ = 20°07' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.6	-9.1	8.0	4	-20.5	18	-6.5	-3.6	-5.3	-5.2	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.0	5.5	5.4
II	–	–	–	–	2.0	-4.4	12.6	18	-11.1	6	-2.8	0.3	-1.2	-1.2	–	–	–	–	–	–	–	–	–	–	–	–	6.0	5.4	5.9	5.8
III	–	–	–	–	5.8	-0.4	15.1	10	-8.1	23	1.2	3.7	2.8	2.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	6.9	7.3
IV	–	–	–	–	13.7	3.9	20.3	15	-3.0	10	6.7	12.6	7.8	8.7	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.1	4.6	5.0
V	–	–	–	–	12.2	4.8	19.2	6,28	-0.3	12	7.2	10.7	7.7	8.3	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.9	7.0	6.9
VI	–	–	–	–	19.3	10.3	28.3	27	6.4	16	13.7	17.2	14.0	14.7	–	–	–	–	–	–	–	–	–	–	–	–	4.9	6.2	6.8	6.0
VII	–	–	–	–	17.9	9.6	26.3	4	5.8	7	12.7	16.3	12.8	13.6	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.6	6.9	6.2
VIII	–	–	–	–	18.6	10.2	29.3	11	5.6	14	13.0	17.3	13.5	14.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.2	6.9	6.0
IX	–	–	–	–	18.3	9.4	25.5	17	3.9	22	11.6	17.2	12.5	13.4	–	–	–	–	–	–	–	–	–	–	–	–	4.2	3.5	4.0	3.9
X	–	–	–	–	13.1	5.3	17.5	8	0.5	16	6.7	11.8	8.3	8.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.3	4.0	5.0
XI	–	–	–	–	5.0	-0.9	11.5	27	-9.5	21	1.2	3.8	1.3	1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.3	7.1	6.6	7.0
XII	–	–	–	–	-1.3	-8.5	17.2	5	-21.3	16	-5.3	-3.7	-5.5	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.0	6.4	6.3
Rok	–	–	–	–	10.2	2.5	29.3	11.VIII	-21.3	16.XII	5.0	8.6	5.7	6.2	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.9	6.0	5.9

Muszyna — φ = 49°21' — λ = 20°53'

I	966.0	983.9	950.2	1022.2	0.0	-8.2	8.2	4	-20.4	27	-6.0	-1.8	-4.6	-4.2	3.8	4.2	4.0	4.0	8.8	7.4	8.5	8.2	0.5	1.4	0.7	0.9	6.9	6.3	6.8	6.7
II	966.8	982.3	941.3	1024.5	3.6	-3.8	11.2	18	-15.5	6	-2.3	2.2	-1.1	-0.6	4.8	5.3	5.1	5.1	9.1	7.4	9.0	8.5	0.5	2.0	0.6	1.0	9.2	7.1	7.0	7.8
III	964.9	981.8	944.4	1019.4	9.4	0.4	20.0	18	-7.5	23	2.2	7.8	3.3	4.2	6.1	6.0	6.6	6.2	8.4	5.9	8.5	7.6	1.2	5.1	1.3	2.5	7.4	7.6	6.2	7.1
IV	959.7	966.7	953.3	1012.9	17.1	2.2	24.0	7	-4.0	10	4.9	15.5	8.7	9.4	7.4	7.6	8.6	7.9	8.5	4.4	7.6	6.8	1.4	10.6	2.8	4.9	5.5	5.5	4.1	5.0
V	959.2	967.0	946.2	1012.2	16.1	4.8	22.9	6	-1.2	13	7.9	14.4	9.1	10.1	9.6	10.0	10.4	10.0	8.9	6.2	8.8	8.0	1.3	6.9	1.4	3.2	8.8	8.1	6.8	7.9
VI	963.2	975.4	954.3	1015.3	23.0	9.5	30.0	27	4.4	21	13.2	21.0	14.7	15.9	13.9	13.7	14.7	14.1	9.1	5.7	8.7	7.8	1.5	11.8	2.2	5.2	5.3	5.6	5.7	5.5
VII	962.5	973.4	948.9	1014.8	21.7	9.1	30.6	4	3.5	7	12.6	19.6	13.8	15.0	12.9	12.4	13.7	13.0	8.8	5.7	8.6	7.7	1.9	11.2	2.3	5.1	5.6	7.3	6.4	6.4
VIII	965.1	976.9	954.9	1017.4	22.2	9.5	32.3	11	3.2	31	11.8	20.8	14.3	15.3	13.2	14.0	14.8	14.0	9.4	5.7	8.9	8.0	1.0	11.6	1.9	4.8	7.4	6.0	4.2	5.9
IX	967.3	978.1	956.5	1020.3	21.7	5.6	30.3	18	-3.5	23	7.4	20.7	14.0	12.5	9.8	11.5	11.5	10.9	9.3	4.8	8.6	7.6	1.0	13.6	1.9	5.5	7.0	4.2	3.0	4.7
X	966.6	977.1	944.9	1020.2	15.7	4.2	21.6	19	-0.9	6	6.2	14.6	8.2	9.3	8.1	9.1	9.0	8.7	8.6	5.6	8.4	7.5	1.7	7.9	2.2	3.9	7.1	5.4	4.3	5.6
XI	961.2	980.9	950.7	1015.6	6.7	0.5	13.5	1	-10.2	24	1.9	5.9	2.5	3.2	6.6	7.2	6.8	6.9	9.1	7.6	9.0	8.6	0.7	2.5	0.8	1.3	9.0	7.4	8.1	8.2
XII	961.5	982.8	948.1	1017.7	-1.0	-9.8	12.6	5	-31.0	25	-6.5	-2.7	-5.3	-5.0	4.1	4.6	4.3	4.3	8.6	7.8	8.5	8.3	0.6	1.4	0.7	0.9	6.3	7.4	7.0	6.9
Rok	963.8	983.9	941.3	1017.7	13.0	2.0	32.3	11.VIII	-31.0	25.XII	4.4	11.5	6.2	7.1	8.4	8.8	9.1	8.8	8.9	6.2	8.6	7.9	1.1	7.2	1.6	3.3	7.1	6.5	5.8	6.5

Witów — φ = 49°20' — λ = 19°50'

I	–	–	–	–	-0.6	-11.6	8.8	31	-22.8	18	-8.1	-2.2	-6.9	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	5.3	5.6	5.1	5.3
II	–	–	–	–	2.8	-6.6	10.8	18	-17.3	6	-4.2	1.2	-2.2	-1.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.9	5.9	5.9
III	–	–	–	–	6.7	-1.3	16.1	18	-10.8	23	0.7	4.8	2.3	2.5	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	7.3	7.4
IV	–	–	–	–	14.3	4.7	21.4	7	-4.8	10	5.4	13.3	6.7	8.0	–	–	–	–	–	–	–	–	–	–	–	–	5.0	5.7	4.8	5.2
V	–	–	–	–	12.9	3.5	21.2	6	-1.5	13	7.2	11.4	6.8	8.0	–	–	–	–	–	–	–	–	–	–	–	–	7.1	7.9	6.6	7.2
VI	–	–	–	–	19.6	8.0	28.4	27	3.7	17	13.7	18.1	12.4	14.2	–	–	–	–	–	–	–	–	–	–	–	–	5.2	7.2	6.4	6.3
VII	–	–	–	–	18.6	7.6	27.4	4	2.0	7	12.7	17.3	11.9	13.4	–	–	–	–	–	–	–	–	–	–	–	–	5.8	7.1	6.3	6.4
VIII	–	–	–	–	19.5	8.7	30.0	11	3.6	14,17	12.4	18.1	12.2	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.6	5.5	5.9
IX	–	–	–	–	19.5	6.0	27.7	18	-0.8	23	8.6	18.7	10.4	12.0	–	–	–	–	–	–	–	–	–	–	–	–	3.8	4.3	3.8	4.0
X	–	–	–	–	14.1	2.7	19.3	8	-1.9	25	5.1	12.9	6.8	7.9	–	–	–	–	–	–	–	–	–	–	–	–	6.1	5.6	4.7	5.5
XI	–	–	–	–	5.6	-1.9	14.7	3	-12.0	21	0.4	4.7	0.6	1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.1	7.6	7.5
XII	–	–	–	–	-1.2	-10.7	18.6	5	-26.0	25	-7.1	-3.1	-6.9	-6.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.5	7.1	6.7
Rok	–	–	–	–	11.0	0.5	30.0	11.VIII	-26.0	25.XII	3.9	9.6	4.5	5.6	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.4	5.9	6.1

Poronin — φ = 49°20' — λ = 20°02'

I	–	–	–	–	-0.4	-14.3	9.0	4	-26.1	26	-10.2	-2.3	-8.4	-7.3	–	–	–	–	–	–	–	–	–	–	–	–	4.4	4.6	4.9	4.6
II	–	–	–	–	3.5	-9.1	11.2	18	-20.9	6	-6.8	2.3	-3.8	-3.0	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.6	6.4	5.6
III	–	–	–	–	6.9	-2.3	16.3	18	-14.7	23	-0.1	5.1	1.3	1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.3	7.1	7.3
IV	–	–	–	–	14.7	-0.1	21.5	7	-6.5	10	4.6	13.7	5.9	7.5	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.8	4.7	4.7
V	–	–	–	–	13.3	2.4	21.6	6	-3.2	15	6.6	11.6	6.0	7.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	8.6	7.0	7.7
VI	–	–	–	–	20.2	5.7	28.5	26	0.3	17	13.4	18.3	11.5	13.7	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.8	5.2	5.7
VII	–	–	–	–	18.8	6.0	28.1	4	-0.9	7	12.3	17.3	11.0	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.8	6.9	6.5
VIII	–	–	–	–	19.8	6.9	30.3	11	0.9	31	11.3	18.5	11.7	13.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.1	4.7	5.3
IX	–	–	–	–	19.9	3.0	26.6	17	-4.6	23	6.8	18.9	8.7	10.8	–	–	–	–	–	–	–	–	–	–	–	–	4.3	4.2	4.3	4.3
X	–	–	–	–	14.5	0.9	19.1	8	-4.4	25	3.6	13.5	5.3	6.9	–	–	–	–	–	–	–	–	–	–	–	–	5.1	4.8	4.4	4.8
XI	–	–	–	–	5.7	-3.0	15.2	3	-15.5	21	-0.7	4.6	-0.5	0.7	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.6	7.4	7.2
XII	–	–	–	–	-0.9	-13.0	17.5	5	-32.3	25	-8.2	-3.3	-7.6	-6.7	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.1	6.8	6.4
Rok	–	–	–	–	11.3	-1.4	30.3	11.VIII	-32.3	23.XII	2.7	9.8	3.4	4.8	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.0	5.8	5.8

Bukowina Tatrzańska $H_s = 880$ m $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R̄
I	2	1.8	0.5	2.0	5	3.0	6.5	1.9	3	3.7	14	3.3	8.5	3.8	4.5	2.1	49	1.4	42.9	5.6	4	10	20	30	·	·	·	8	11	10	3	·	1	31	·
II	6	4.7	·	·	1	2.0	1	1.0	3.5	1.9	14.5	3.9	10.5	4.8	6.5	4.0	41	1.8	28.6	9.9	9	1	8	27	·	1	·	8	12	13	8	·	1	28	·
III	·	·	·	·	·	·	·	·	·	·	52.5	4.8	31	5.9	3.5	7.6	6	5.0	44.4	16.1	14	·	3	15	·	3	1	5	20	18	14	1		15	·
IV	6.5	3.5	9	2.7	9.5	2.7	2.5	3.0	4	1.8	15	4.1	9	5.9	4.5	3.7	30	2.4	17.0	7.3	8	·	·	4	·	2	·	8	6	10	5	·	1	·	1
V	4.5	2.5	3	1.7	2	3.5	2	4.0	2	3.5	23.5	3.3	24.5	3.8	7.5	3.2	24	2.5	109.7	23.1	6	·	·	1	·	·	·	·	11	18	15	3	·	·	3
VI	3.5	1.9	5.5	1.7	3	3.2	6	1.9	4.5	1.9	19	2.6	13.5	4.5	13	2.7	22	2.1	115.4	17.6	12	·	·	·	2	·	·	1	10	15	13	6	·	·	8
VII	2.5	1.4	·	·	2.5	1.6	2	2.2	2	1.8	18	3.3	31.5	4.0	13.5	2.4	21	2.5	151.7	42.4	29	·	·	·	3	1	·	13	11	19	15	5	·	·	4
VIII	4.5	1.1	2	1.8	1	2.5	·	·	3	2.0	27	3.2	26	4.5	5.5	2.4	24	2.5	74.3	17.2	12	·	·	·	5	·	·	7	9	12	7	3	·	·	5
IX	5	2.0	2	3.0	4	2.2	4.5	2.7	3	2.3	23	3.3	11	4.6	6.5	2.5	31	2.1	46.9	5.2	9	·			1	·	·	11	3	9	6	·	1	·	3
X	5.5	2.6	7.5	3.7	4.5	5.6	4.5	4.1	1.5	3.7	10.5	3.0	8.5	2.9	11.5	2.5	39	1.9	35.1	16.6	30	·	·	·	·	·	·	8	7	11	6	1	3	·	·
XI	4	1.8	1.5	3.7	4.5	2.8	2	1.5	1.5	2.3	13.5	3.3	12.5	3.6	4.5	2.0	46	1.4	74.6	31.1	4	·	4	18	·	·	·	3	15	17	8	2	7	12	·
XII	2	2.2	2	1.8	2.5	2.8	2	1.5	0.5	3.0	20.5	5.0	22	5.5	1.5	4.7	40	2.8	64.9	17.0	6	12	19	28	·	4	·	2	11	19	9	3	2	25	·
Rok	46	1.9	33	1.8	39.5	2.7	33	2.0	28.5	2.3	251	3.6	208.5	4.5	82.5	3.3	373	2.4	745.5	42.4	29.VII	23	54	123	11	11	1	74	126	171	109	24	16	111	24

Muszyna $H_s = 445$ m $H_b = 447{,}1$ m $h_w = 21{,}2$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R̄
I	7.5	2.6	10.5	2.0	1	2.0	4	1.5	4	2.2	20	2.9	7	1.6	·	·	39	1.4	9.7	5.3	5	11	13	28	·	1	·	4	15	9	3	·	·	11	·
II	1	2.0	5	2.2	·	·	3	1.0	2	1.5	9	2.2	6	1.2	2	3.0	56	0.6	22.7	9.4	9	1	1	24	·	·	·	1	15	13	5	·	5	14	·
III	9	2.4	8	3.4	·	·	2	2.0	3	2.0	30	3.2	5	2.4	4	2.5	32	1.9	39.2	10.9	14	·	·	14	·	·	·	4	14	16	10	1	1	6	·
IV	9	2.2	16	2.1	1	2.0	4	2.8	1	2.0	19	4.0	2	1.5	·	·	38	1.6	8.6	2.2	16	·	·	5	·	1	·	6	7	8	4	·	3	·	1
V	10	1.6	8.5	3.2	1.5	1.7	0.5	1.0	3.5	1.6	12.5	4.0	16.5	1.8	3	1.3	37	1.5	63.5	14.2	17	·	·	2	·	·	·	·	17	16	12	2	7	·	4
VI	8	1.5	11	2.2	1	1.0	·	·	4	1.8	18	3.2	7	2.0	4	1.2	37	1.3	95.9	17.9	12	·	·	·	7	·	·	2	6	14	9	5	2	·	10
VII	15	1.4	9	2.1	1	1.0	·	·	2	1.5	10	4.3	15	2.0	3	1.0	38	1.3	109.1	31.6	29	·	·	·	8	1	·	2	12	17	15	2	·	·	6
VIII	7	1.7	9	2.9	4	1.5	2	2.5	1	9.0	10	3.4	13	1.6	7	1.9	40	1.4	52.6	14.3	3	·	·	·	7	·	·	5	10	14	10	1	9	·	3
IX	7	1.4	12	1.9	3	3.0	5	2.0	·	·	13	2.8	6	1.7	3	1.0	41	1.1	13.5	6.1	29	·	·	4	8	·	·	6	8	7	3	·	12	·	·
X	5	1.4	14	2.2	2	1.5	9	1.8	2	2.5	25	3.6	4	1.8	1	1.0	31	1.7	28.0	18.8	30	·	·	2	·	1		6	10	8	3	1	9	·	·
XI	5	1.4	6	4.7	·	·	3	1.3	2	3.0	23	3.0	9	1.9	3	1.0	39	1.3	63.0	14.9	4	1	2	11	·	·	·	1	19	13	9	2	7	7	·
XII	13	1.9	12	2.0	3	1.3	2	2.0	2	2.0	18	4.4	8	1.6	2	1.0	33	1.7	65.3	20.2	11	14	18	27	·	·	·	5	15	17	10	3	1	25	·
Rok	96.5	1.8	121	2.3	17.5	1.2	34.5	1.5	26.5	2.4	207.5	3.4	98.5	1.8	32	1.2	461	1.4	571.1	31.6	29.VII	27	34	117	30	4	·	42	148	152	93	17	56	63	24

Witów $H_s = 835$ m $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R̄
I	0.5	1.0	0.5	1.0	2	3.0	2	1.2	3.5	3.3	14	4.2	6	2.8	2.5	1.2	62	1.1	19.8	8.0	4	19	17	30	·	3	·	6	8	8	4	·	3	31	·
II	0.5	2.0	·	·	·	·	3.5	1.0	7.5	1.4	12	1.7	13	2.8	6.5	1.2	41	0.9	24.5	6.8	28	4	3	28	·	·	·	5	11	12	10	·	4	26	·
III	0.5	1.0	·	·	·	·	0.5	2.0	3.5	1.9	21.5	3.8	32.5	2.5	12.5	2.1	22	2.1	65.8	8.3	14	1	1	21	·	2	·	2	16	18	16	·	1	13	·
IV	3	1.3	11.5	2.7	2	3.0	3	2.3	2.5	2.2	16	3.7	1.5	2.7	7.5	2.2	43	1.5	26.3	7.3	8	·	·	9	·	1	·	5	4	11	8	·	·	·	1
V	5	1.7	8.5	1.2	1.5	1.0	3	3.0	5	1.7	10.5	2.1	8.5	3.6	14	2.3	37	1.4	130.3	24.6	6	·	·	2	·	·	·	·	13	19	15	5	·	·	5
VI	4.5	2.2	7.5	2.6	·	·	7	1.8	4	2.5	16.5	2.6	6	2.3	8.5	2.8	36	1.5	132.3	21.4	13	·	·	·	3	·	·	·	8	15	12	6	·	·	8
VII	4.5	1.6	4	1.8	·	·	3	1.0	3.5	1.7	28.5	3.3	8	3.8	8.5	2.1	33	1.8	151.8	46.0	29	·	·	·	3	1	·	2	8	13	12	5	·	·	2
VIII	3.5	1.6	7	1.9	2	3.0	2.5	1.8	5	1.3	29.5	3.1	8	2.1	11.5	1.6	24	1.7	94.7	24.0	12	·	·	·	5	1	·	3	8	12	10	4	·	·	3
IX	2	1.5	5	1.9	·	·	3	1.3	7.5	1.2	22.5	2.2	7.5	2.3	10.5	1.4	32	1.2	18.6	3.8	9,26	·	·	1	3	·	·	12	2	8	7	·	·	·	1
X	3	1.7	4.5	1.2	1.5	1.7	11	3.1	10	2.4	10.5	3.9	3.5	2.0	7	1.5	42	1.4	38.4	18.4	30	·	·	5	·	2	·	4	8	13	6	1	2	-	·
XI	1	1.0	·	·	·	·	3	2.0	8.5	1.4	17.5	2.1	4.5	1.1	13.5	1.5	42	0.9	92.5	44.2	4	1	3	22	·	1	·	·	18	13	9	1	10	13	·
XII	3	2.3	5.5	1.9	3	2.7	3.5	1.0	4.5	1.1	16.5	6.3	4	3.2	3	2.3	50	1.7	91.4	28.7	6	14	19	27	·	4	·	2	12	16	9	4	1	25	·
Rok	31	1.6	54	1.4	12	1.2	45	1.8	65	1.8	215.5	3.2	103	2.6	105.5	1.8	464	1.4	886.4	46.0	29.VII	39	43	145	14	15	·	41	116	158	118	26	21	108	20

Poronin $H_s = 800$ m $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◔	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	≡	⊞	R̄
I	1.5	1.3	10	1.2	27	1.2	6.5	1.4	1	1.0	3.5	5.3	7.5	2.1	1	2.0	35	1.0	19.2	10.4	4	24	17	30	·	1	·	9	6	6	3	1	2	30	·
II	3.5	1.0	6	1.2	21.5	1.0	2	1.0	·	·	2.5	1.6	16	1.4	0.5	1.0	32	0.7	31.5	8.5	9	12	4	28	·	·	·	6	9	13	10	·	1	25	·
III	0.5	3.0	1.5	1.3	10.5	1.1	·	·	0.5	3.0	13.5	3.0	4.5	2.3	2.5	1.4	19	1.8	44.9	8.3	14	2	1	23	·	·	·	4	19	19	10	·	2	13	·
IV	4.5	1.7	10	2.2	20.5	1.4	3.5	2.0	7.5	1.5	4	2.8	12.5	2.5	2.5	2.4	25	1.4	17.6	5.4	8	·	·	17	·	·	·	9	5	10	7	·	1	·	1
V	6.5	1.0	5.5	1.0	14	1.1	1.5	2.0	1	1.0	5.5	1.8	21.5	2.0	6.5	1.3	31	1.0	119.5	24.6	6	·	·	6	·	·	·	·	17	18	14	4	1	·	1
VI	3.5	1.9	5	1.6	18.5	1.2	4	1.5	1.5	2.3	10	2.0	15.5	1.9	1	5.0	31	1.1	152.1	26.0	8	·	·	·	4	·	·	4	11	16	12	7	1	·	10
VII	4	1.2	1.5	2.0	11.5	1.0	2	1.5	2.5	2.6	5	3.0	32	1.9	4.5	1.2	30	1.2	148.4	41.6	29	·	·	1	4	1	·	3	13	15	14	5	·	·	5
VIII	4.5	1.0	1.5	1.0	14.5	1.2	3.5	1.6	5	1.4	11.5	2.3	17	1.6	4.5	1.7	31	1.0	77.5	21.3	12	·	·	·	6	·	·	7	6	12	9	3	·	·	3
IX	8	1.1	7.5	1.2	9	1.1	1	2.0	4.5	1.8	6	2.4	15	2.3	3	1.0	36	1.0	18.3	6.2	6	·	·	6	3	-	·	11	5	8	5	·	3	·	3
X	3	1.3	6	1.7	15	1.3	4	2.0	4.5	3.3	8.5	2.4	8	1.5	6	1.5	41	0.9	39.9	16.3	30	·	·	17	·	·	·	9	7	13	7	1	2	·	·
XI	·	·	3	1.0	20.5	1.0	8.5	1.0	3	1.0	3.5	1.9	7.5	2.3	·	·	44	0.7	74.5	31.4	4	3	2	24	·	·	·	6	20	17	10	2	-	13	·
XII	1	1.0	2	1.5	15	1.1	4	1.0	1	2.5	5	3.4	11	2.3	4	2.5	50	0.8	79.7	28.2	6	17	19	28	·	·	·	3	14	14	9	1	2	25	·
Rok	40.5	1.3	59.5	1.4	197.5	1.1	40.5	1.4	29	1.8	78.5	2.7	208.5	2.0	36	1.8	405	1.0	823.1	41.6	29.VII	58	43	180	17	2	·	71	132	161	110	24	-	106	23

Komańcza

$\varphi = 49°20'$ $\lambda = 22°04'$ 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T										ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
									Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-1.8	-10.4	9.0	4	-27.1	21	-6.2	-2.8	-6.2	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	7.6	7.1	5.8	6.8
II	–	–	–	–	1.1	-2.2	5.4	18	-13.2	15	-2.0	0.5	-1.3	-1.0	–	–	–	–	–	–	–	–	–	–	–	–	9.4	8.4	7.9	8.6
III	–	–	–	–	8.1	0.9	17.0	10	-12.6	23	2.2	6.3	3.0	3.6	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.3	5.9	7.6
IV	–	–	–	–	16.0	2.1	23.0	8	-5.7	10	6.5	14.9	8.0	9.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	5.4	3.6	4.6
V	–	–	–	–	15.3	3.7	25.1	29	-1.4	24	8.5	13.8	8.6	9.9	–	–	–	–	–	–	–	–	–	–	–	–	7.6	8.9	6.0	7.5
VI	–	–	–	–	22.1	7.8	29.4	27	1.9	29	14.4	20.4	13.5	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.4	6.1	5.8
VII	–	–	–	–	21.0	7.7	28.9	3,4	0.1	7	13.6	19.6	12.6	14.6	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.0	5.6	6.0
VIII	–	–	–	–	21.8	8.9	30.9	10	0.5	31	13.4	20.5	13.9	15.4	–	–	–	–	–	–	–	–	–	–	–	–	5.1	6.4	5.1	5.5
IX	–	–	–	–	20.0	5.0	26.7	17	-4.7	23	9.1	19.3	10.8	12.5	–	–	–	–	–	–	–	–	–	–	–	–	4.0	4.1	3.3	3.8
X	–	–	–	–	15.4	3.4	23.3	20	-2.7	6	5.5	14.5	7.5	8.8	–	–	–	–	–	–	–	–	–	–	–	–	6.2	5.0	3.0	4.7
XI	–	–	–	–	7.2	1.1	14.4	7	-10.8	21	3.0	6.2	3.8	4.2	–	–	–	–	–	–	–	–	–	–	–	–	9.1	8.1	7.9	8.4
XII	–	–	–	–	-1.1	-8.9	11.0	5	-35.6	25	-4.8	-2.6	-4.3	-4.0	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	8.0	8.2
Rok	–	–	–	–	12.1	1.6	30.9	10.VIII	-35.6	25.XII	5.3	10.9	5.8	7.0	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.9	5.7	6.5

Baligród

$\varphi = 49°20'$ $\lambda = 22°17'$

I	–	–	–	–	-0.9	-8.8	10.1	4	-23.4	21	-5.7	-2.2	-4.9	-4.4	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.4	5.3	6.1
II	–	–	–	–	2.7	-2.7	11.1	18	-7.2	4	-1.2	2.0	-0.4	0.0	–	–	–	–	–	–	–	–	–	–	–	–	8.4	6.6	7.4	7.5
III	–	–	–	–	8.4	0.7	15.3	18	-7.9	23	3.0	6.5	4.1	4.4	–	–	–	–	–	–	–	–	–	–	–	–	8.6	8.0	6.3	7.6
IV	–	–	–	–	16.0	3.4	23.0	8	-5.1	10	7.4	14.9	8.3	9.7	–	–	–	–	–	–	–	–	–	–	–	–	4.5	5.7	4.0	4.7
V	–	–	–	–	15.5	4.7	23.7	29	1.0	19	8.5	14.1	9.0	10.2	–	–	–	–	–	–	–	–	–	–	–	–	6.9	7.5	5.3	6.6
VI	–	–	–	–	22.3	9.7	29.1	26	3.5	29	14.1	20.1	14.6	15.8	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.5	6.3	5.9
VII	–	–	–	–	21.9	9.1	29.3	3	3.5	7	14.0	19.3	13.9	15.3	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.5	5.4	5.8
VIII	–	–	–	–	21.8	10.7	31.2	11	3.0	31	12.6	20.2	15.1	15.8	–	–	–	–	–	–	–	–	–	–	–	–	5.6	5.6	5.4	5.5
IX	–	–	–	–	20.4	6.6	29.1	17	-3.4	23	9.2	19.5	12.5	13.4	–	–	–	–	–	–	–	–	–	–	–	–	4.7	3.8	3.2	3.9
X	–	–	–	–	15.9	4.4	24.0	20	-0.9	11	6.4	15.2	9.1	10.0	–	–	–	–	–	–	–	–	–	–	–	–	4.8	4.0	3.9	4.2
XI	–	–	–	–	8.3	1.6	16.0	7	-7.5	21	3.8	7.0	4.6	5.0	–	–	–	–	–	–	–	–	–	–	–	–	8.3	7.5	6.4	7.4
XII	–	–	–	–	–	-8.2	–	–	-30.5	25	-4.8	-1.8	-4.0	-3.7	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.0	7.1	7.8
Rok	–	–	–	–	–	2.6	31.2	11.VIII	-30.5	25.XII	5.6	11.2	6.8	7.6	–	–	–	–	–	–	–	–	–	–	–	–	6.4	6.3	5.5	6.1

Gubałówka

$\varphi = 49°18'$ $\lambda = 19°56'$

I	–	–	–	–	-0.1	-8.0	7.5	30	-19.0	18	-5.5	-1.8	-4.8	-4.2	2.7	3.1	2.9	2.9	6.4	5.7	6.4	6.2	1.5	2.5	1.6	1.9	5.5	5.4	4.8	5.2
II	–	–	–	–	3.2	-3.6	14.1	18	-10.8	6	-1.8	1.5	-0.9	-0.5	3.6	4.3	3.9	3.9	6.8	6.4	7.0	6.7	1.9	2.7	1.9	2.2	6.2	6.0	6.1	6.1
III	–	–	–	–	5.8	-1.1	15.6	10	-8.6	23	0.7	3.6	2.0	2.1	4.5	4.9	4.6	4.7	7.0	6.2	6.5	6.6	2.1	3.5	2.7	2.8	8.4	8.5	7.5	8.1
IV	–	–	–	–	13.1	4.0	20.1	7	-3.6	10	7.0	12.0	7.4	8.4	6.4	6.8	6.7	6.6	6.4	4.9	6.5	5.9	4.0	7.7	3.8	5.2	6.1	6.1	5.2	5.8
V	–	–	–	–	11.2	4.5	19.7	6	-0.9	12	6.9	9.5	6.8	7.5	7.7	7.8	7.5	7.7	7.8	6.6	7.6	7.3	2.5	4.6	2.7	3.3	8.1	8.9	7.6	8.2
VI	–	–	–	–	18.6	10.2	26.5	26	6.0	29	13.8	16.4	13.1	14.1	11.4	12.1	11.5	11.7	7.4	6.6	7.7	7.2	4.7	7.2	3.8	5.2	5.1	7.1	6.8	6.3
VII	–	–	–	–	17.5	9.2	26.6	4	4.9	7	12.6	15.7	12.0	13.1	10.5	11.0	10.8	10.8	7.3	6.4	7.8	7.2	4.5	7.7	3.6	5.3	5.8	7.3	7.1	6.7
VIII	–	–	–	–	18.3	10.0	29.2	11	5.0	17	13.1	16.8	12.8	13.9	11.5	12.5	12.1	12.0	7.6	6.7	8.1	7.5	4.1	7.7	3.1	5.0	5.8	6.9	6.1	6.3
IX	–	–	–	–	18.5	9.6	25.3	18	4.4	12	12.3	17.5	12.6	13.8	9.5	11.2	10.1	10.3	6.7	5.6	7.0	6.4	5.1	9.4	4.8	6.4	4.5	4.4	3.8	4.2
X	–	–	–	–	13.2	5.8	18.0	8	1.8	14	7.8	12.1	8.3	9.1	8.0	8.4	7.8	8.1	7.6	6.1	7.2	7.0	2.8	6.0	3.3	4.0	6.6	6.4	4.7	5.9
XI	–	–	–	–	6.4	-0.3	16.9	27	-9.3	21	2.2	4.6	2.2	2.8	5.6	5.9	5.8	5.8	7.7	7.1	8.0	7.6	1.9	3.0	1.6	2.2	8.2	7.5	7.4	7.7
XII	–	–	–	–	-0.6	-8.2	17.4	5	-21.6	16	-4.8	-2.6	-5.1	-4.4	3.9	4.0	3.9	3.9	7.9	7.4	8.2	7.8	1.2	1.9	1.0	1.4	6.9	7.1	6.6	6.9
Rok	–	–	–	–	10.4	2.7	29.2	11.VIII	-21.6	16.XII	5.4	8.8	5.5	6.3	7.1	7.7	7.3	7.4	7.2	6.3	7.3	6.9	3.0	5.3	2.8	3.7	6.4	6.8	6.1	6.4

Zakopane

$\varphi = 49°18'$ $\lambda = 19°57'$

I	920.1	936.0	903.6	–	-0.3	-10.9	8.5	3	-22.4	18	-7.7	-1.9	-6.3	-5.6	3.0	3.6	3.1	3.2	7.8	6.5	7.6	7.3	0.8	2.0	1.0	1.3	5.7	5.4	4.8	5.3
II	923.8	937.5	896.9	–	3.2	-6.5	13.5	18	-17.2	6	-4.4	2.1	-2.3	-1.7	3.9	4.8	4.4	4.4	8.5	6.9	8.4	7.9	0.7	2.5	0.8	1.3	6.2	6.0	6.3	6.2
III	921.8	937.3	900.9	–	6.8	-0.8	15.6	18	-9.6	23	0.8	4.9	2.4	2.6	5.2	5.3	5.3	5.3	8.0	6.4	7.3	7.2	1.4	3.8	2.2	2.5	8.2	8.2	7.3	7.9
IV	916.6	922.7	910.2	–	14.2	2.3	21.2	7	-4.6	10	5.7	13.3	7.4	8.4	6.8	6.7	7.7	7.1	7.5	4.5	7.5	6.5	2.7	8.9	2.7	4.8	5.9	6.0	5.1	5.7
V	916.7	923.2	904.2	–	12.7	3.6	20.5	6	-1.4	13	7.1	11.1	7.0	8.0	8.1	7.9	8.4	8.1	7.9	6.1	8.2	7.4	2.2	5.8	1.9	3.3	7.9	8.4	7.3	7.9
VI	921.2	933.0	912.0	–	20.0	8.2	27.5	27	3.5	17	13.7	17.7	12.9	14.3	11.7	12.0	12.3	12.0	7.5	6.2	8.3	7.3	4.2	8.9	2.8	5.3	4.9	6.7	6.5	6.0
VII	920.4	930.4	908.1	–	18.7	7.5	27.1	4	2.5	7	12.5	16.9	12.0	13.4	11.0	11.1	11.6	11.2	7.6	6.0	8.2	7.3	3.7	8.9	2.7	5.3	5.6	7.3	6.8	6.6
VIII	923.0	934.2	912.9	–	19.4	8.5	30.0	11	3.4	14	12.1	18.1	12.6	13.8	11.7	12.2	12.4	12.1	8.2	5.9	8.4	7.5	2.9	9.7	2.6	5.1	5.6	6.9	5.7	6.1
IX	924.6	934.4	915.0	–	19.5	5.6	26.6	18	-1.4	23	8.2	18.4	10.3	11.8	9.4	10.9	10.5	10.3	8.6	5.2	8.3	7.4	1.8	10.9	2.4	5.0	4.4	4.6	3.6	4.2
X	922.8	933.5	900.0	–	14.1	2.9	19.1	8	-1.9	25	5.1	13.1	7.0	8.0	7.4	8.4	8.0	7.9	8.5	5.7	8.0	7.4	1.7	7.0	2.4	3.7	6.9	6.1	4.7	5.9
XI	917.1	935.2	906.2	–	6.0	-1.4	15.1	3	-12.7	21	0.5	5.2	0.7	1.8	5.6	6.2	5.8	5.9	8.6	7.1	8.8	8.2	1.0	3.1	0.8	1.6	8.3	7.6	7.4	7.8
XII	916.6	935.4	904.2	–	-0.3	-10.4	18.4	5	-24.5	25	-6.2	-2.4	-6.2	-5.2	3.6	3.9	3.6	3.7	7.7	7.0	8.0	7.6	1.4	2.1	1.0	1.5	8.5	6.9	6.3	6.6
Rok	920.4	937.6	896.9	–	11.2	0.7	30.0	11.VIII	-24.5	25.XII	4.0	9.7	4.8	5.8	7.3	7.8	7.8	7.6	8.0	6.1	8.1	7.4	2.0	6.1	1.9	3.3	6.3	6.7	6.0	6.3

Komańcza

$H_s = 470\ m$ $h_w = 15\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU [%D, %n] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min ≤ -10°	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	Wiatr v ≥ 10	≥ 15	●	●	Opad R 0,1 ≤ R < 1,0	1,0 ≤ R < 10,0	R ≥ 10,0	≡	⊞	R ≥ 10
I	4	30	12	17	10	35	26	30	18	21	4	22	1	40	2	30	16	22	30,1	9,4	5	14	21	28	·	2	·	5	15	15	12	·	1	21	–
II	25	18	15	13	55	24	14	21	24	21	6	30	1	30	65	21	23	16	22,9	3,5	1	5	8	24	·	·	·	·	21	12	9	·	2	21	–
III	9	24	2	25	·	·	4	40	15	17	4	28	65	25	215	34	31	18	39,4	6,8	19	1	·	16	·	1	1	·	16	15	12	·	1	1	–
IV	6	15	8	19	9	28	9	27	125	20	15	10	2	15	4	22	38	12	29,1	10,0	3	·	·	9	·	1	1	9	5	7	5	1	·	·	–
V	6	23	13	15	4	15	4	15	12	27	1	20	05	20	95	24	43	11	51,5	9,8	7	·	·	3	1	·	·	·	15	16	10	·	·	·	–
VI	3	23	2	25	9	14	8	20	11	20	·	·	25	12	55	20	49	09	79,9	13,1	14	·	·	·	4	·	·	3	10	13	11	4	·	·	–
VII	10	19	5	12	3	17	6	22	15	35	1	30	7	17	7	26	39	14	105,7	33,7	29	·	·	·	7	2	·	2	7	12	10	5	–	·	–
VIII	7	13	2	10	4	10	2	10	19	17	8	18	3	17	8	22	40	09	39,4	12,0	12	·	·	·	7	·	·	5	7	9	6	1	2	·	–
IX	1	20	2	20	4	22	4	30	14,5	14	6,5	18	2	20	4	25	52	08	24,6	7,0	14	·	·	5	4	·	·	13	4	7	5	·	3	·	–
X	10	21	2	15	9	26	12	31	19	24	·	·	3	20	3	17	35	15	19,4	10,6	30	·	·	11	·	2	2	8	6	6	4	1	5	·	–
XI	3	17	6	20	2	15	22	30	18	17	4	32	5	32	5	24	25	18	37,9	14,0	7	1	1	9	·	1	1	1	20	13	9	1	3	·	–
XII	14	25	18	25	8	26	13	45	14	28	1	30	3	27	6	32	16	25	81,9	20,9	11	13	18	25	·	·	·	1	19	15	11	3	·	25	–
Rok	755	21	736	18	675	19	124	27	192	22	37	20	365	23	82	25	407	15	561,8	33,7	29.VII	34	48	130	23	9	5	47	145	140	104	16	–	68	–

Baligród

$H_s = 450\ m$ $h_w = 16,9\ m$

I	10	20	1	30	3	10	·	·	47	47	5	82	1	30	3	37	23	32	19,3	5,6	5	12	15	28	·	5	1	4	7	13	6	·	–	23	–
II	8	20	3	17	·	·	·	·	39	57	2	20	4	20	8	30	20	33	22,5	4,3	2	·	·	20	·	4	1	2	16	13	9	·	–	15	–
III	8	48	·	·	·	·	15	30	24,5	34	7	50	11	28	23	37	18	30	34,1	7,2	31	·	·	13	·	2	·	·	18	16	12	·	–	2	–
IV	8	38	3	23	5	34	5	44	31	35	1	50	2	20	5	42	30	24	32,3	11,4	3	·	·	6	·	2	·	6	3	8	7	1	–	·	–
V	9	23	4	15	1	30	·	·	26	28	3	23	·	·	15	26	35	16	70,7	11,0	7	·	·	·	·	·	·	2	6	18	14	1	–	·	–
VI	6	26	2,5	36	1	10	3,5	24	25,5	25	1	10	1,5	23	5	20	44	13	116,8	37,0	10	·	·	·	5	·	·	3	7	14	12	5	–	·	–
VII	8,5	35	1	20	3,5	16	3	43	24	38	2,5	34	2,5	28	3	55	45	19	104,5	38,7	29	·	·	·	6	3	·	3	8	11	10	3	–	·	–
VIII	11	23	2	1,5	2	20	4,5	21	35,5	24	4	25	5	34	6	20	23	18	54,0	10,7	16	·	·	·	7	·	·	3	6	13	12	2	–	·	–
IX	5	18	1	30	3	30	2	20	37	32	3	23	2	30	5	26	32	19	18,0	5,0	26	·	·	4	5	1	·	12	4	7	6	·	–	·	–
X	11	25	2	40	1	10	4	40	39	35	4	35	1	50	1	30	30	23	26,0	12,0	30	·	·	5	·	·	·	11	6	6	5	1	–	·	–
XI	6	27	·	·	3	30	1	30	44	35	3	17	2	30	8	25	23	24	24,3	6,7	7	·	1	11	·	2	·	3	17	15	7	·	–	3	–
XII	25	29	3	17	·	·	·	·	31	60	1	50	2	30	1	10	30	30	68,5	15,0	7	13	–	24	·	1	·	2	20	16	14	2	–	25	–
Rok	115,5	28	22,5	20	22,5	1,6	24,5	2,1	403,5	38	36,5	3,5	34	27	83	30	353	23	588,0	38,7	29.VII	25	–	111	23	20	2	51	118	150	114	15	–	68	–

Gubałówka

$H_s = 1000\ m$ $h_w = 18,3\ m$

I	35,5	14	13,5	2,1	2	30	·	·	2,5	7,5	0,5	12,0	3,1	30	2	20	6	22	24,1	9,1	4	6	14	30	·	4	1	6	8	11	4	·	3	31	·
II	25	1,5	1	1,0	2	15	2	1,5	·	·	2	4,0	3,2	23	8	11	12	16	35,7	10,9	9	1	5	25	·	·	·	4	13	14	10	1	3	19	·
III	4	12	·	·	1	2,0	·	·	3,5	23	1,5	46	7,2	3,2	2	1,0	9	27	72,8	12,1	14	·	4	17	·	3	·	1	19	20	16	1	·	15	·
IV	17	28	8	2,5	7	2,1	1	2,0	8	4,1	2	4,0	31	26	6	1,7	10	22	43,1	12,7	8	·	·	5	·	1	·	4	8	12	8	2	1	·	1
V	21	13	2	1,5	3	2,0	1	2,0	4	3,2	4	1,8	36	2,0	11	1,5	11	16	140,3	31,2	17	·	·	2	·	·	·	·	20	21	17	4	2	·	5
VI	16	14	4,5	1,8	3,5	23	·	·	1	4,0	1	4,0	5,1	19	5	1,4	8	1,7	145,4	32,5	2	·	·	·	3	·	·	3	8	16	13	8	2	·	12
VII	12	1,2	·	·	·	·	·	·	7,5	2,8	5	4,6	49,5	3,1	3	3,7	16	24	185,4	53,2	29	·	·	·	1	2	·	3	12	17	15	5	3	·	5
VIII	11	1,4	1	4,0	·	·	·	·	8	3,6	3,5	3,1	50,5	2,9	5	1,4	14	23	115,5	23,1	12	·	·	·	5	2	1	4	11	12	10	5	2	·	6
IX	17,5	21	3,5	1,6	1	2,0	·	·	5	1,8	2	7,0	41	2,0	2	1,5	18	17	26,6	7,4	6	·	·	·	2	2	·	10	7	8	7	·	·	·	3
X	26	2,0	1	1,0	2	4,0	1	1,0	7	5,0	4	6,0	33	2,7	5	1,2	14	23	56,5	16,6	30	·	·	·	·	3	·	5	10	12	11	2	3	·	·
XI	17	1,5	3	1,3	2	2,0	·	·	6	3,7	4,5	2,7	39,5	1,7	5	1,4	13	16	108,4	46,1	4	·	5	15	·	·	·	1	19	14	9	2	9	6	·
XII	34	1,6	4	3,2	5	4,0	·	·	1	12,0	1,5	10,0	30,5	3,0	·	·	17	2,2	98,5	28,9	6	15	17	25	·	2	1	2	15	17	9	3	1	25	·
Rok	236	1,6	41,5	1,7	28,5	2,1	5	0,5	53,5	4,2	31,5	5,3	49,7	2,5	54	1,5	148	2,0	1052,3	53,2	29.VII	28	45	119	11	19	3	43	150	174	129	33	29	96	32

Zakopane

$H_s = 844\ m$ $H_b = 838,2\ m$ $h_w = 17,7\ m$

I	·	·	10,5	1,7	14	1,8	11,5	1,8	6,5	3,4	9	2,6	5	4,1	0,5	5,0	36	1,4	21,7	9,3	4	17	19	30	·	1	1	5	8	9	3	·	3	30	·
II	·	·	7	1,9	9,5	1,3	8,5	1,5	2	1,5	12,5	2,3	8,5	3,5	4	2,0	32	1,3	37,3	9,4	9	4	4	28	·	·	·	4	13	15	9	·	2	27	·
III	1,5	2,7	5	1,9	2,5	4,2	7	1,8	4,5	2,3	21,5	3,0	26,5	4,0	9,5	3,6	15	2,6	69,8	11,2	14	·	2	15	·	3	·	1	18	19	15	1	·	15	·
IV	4	2,5	13	2,4	14,5	2,0	9	3,0	3,5	5,1	11	3,7	3	6,2	2	4,0	30	2,0	30,5	10,1	8	·	·	7	·	·	·	5	8	12	6	1	1	·	1
V	3	1,8	12	2,2	12,5	1,7	7,5	1,8	3,5	2,9	9	2,3	5,5	3,1	6	2,8	34	1,4	135,2	24,3	6	·	·	2	·	·	·	·	19	20	14	6	1	·	5
VI	3,5	3,9	13	2,3	8,5	1,6	2,5	3,4	2	2,5	12	2,7	3,5	5,1	3	4,5	42	1,5	138,0	37,6	2	·	·	·	4	·	·	3	8	15	11	7	·	·	12
VII	3	3,0	16	2,0	6	1,3	7,5	2,3	2,5	3,4	7,5	2,6	8	3,7	7,5	3,8	35	1,6	169,2	49,0	29	·	·	·	4	3	2	3	9	16	12	5	·	·	8
VIII	1,5	1,3	8	2,3	8	1,8	10	1,6	3	2,3	16	3,1	10,5	3,4	6	3,7	30	1,8	101,1	22,8	13	·	·	·	5	1	·	4	11	13	9	5	·	·	6
IX	3	1,5	14,5	1,6	3	2,0	7	1,5	1,5	6,7	6,5	3,8	4,5	2,6	3	4,0	47	1,1	24,2	7,4	26	·	·	2	2	·	·	9	5	7	5	·	2	·	3
X	2,5	2,2	17	1,8	11	1,4	7,5	2,6	7	4,6	6	3,8	2,5	4,2	5,5	2,4	34	1,6	70,9	18,7	18	·	·	4	·	4	·	5	11	12	10	3	3	·	·
XI	·	·	10	1,9	7	1,5	7	1,6	3,5	2,6	10,5	2,3	5	3,0	3	4,3	44	1,1	102,9	47,9	4	1	2	18	·	1	·	1	16	15	8	2	8	14	·
XII	1	2,0	13,5	2,0	6	2,1	2,5	1,8	·	·	9,5	4,7	7,5	3,8	3	5,3	50	1,4	90,1	29,1	6	15	19	28	·	2	·	3	13	18	8	3	1	25	·
Rok	23	1,7	139,5	2,0	102,5	1,6	87,5	2,1	39,5	3,1	131	3,1	90	3,9	53	3,8	429	1,6	999,9	49,0	29.VII	37	46	134	15	15	3	43	139	171	110	33	21	111	33

Antołówka — φ = 49°18' — λ = 19°59' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-0.9	-9.1	8.1	30	-20.1	18	-6.5	-2.8	-5.4	-5.0	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.6	5.7	5.7
II	–	–	–	–	2.3	-4.6	11.5	18	-12.8	6	-2.9	1.1	-1.8	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.8	6.8	6.4
III	–	–	–	–	6.5	-0.9	16.4	18	-9.5	23	0.8	4.6	2.2	2.4	–	–	–	–	–	–	–	–	–	–	–	–	8.4	8.2	8.2	8.3
IV	–	–	–	–	14.0	3.5	21.4	7	-3.6	10	6.3	12.8	7.6	8.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	5.5	5.4	5.7
V	–	–	–	–	12.3	4.3	20.2	29	-1.0	13	7.1	10.7	7.1	8.0	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.7	7.9	8.2
VI	–	–	–	–	19.2	9.5	27.0	26	5.9	21	13.6	17.2	13.2	14.3	–	–	–	–	–	–	–	–	–	–	–	–	5.5	7.1	7.0	6.5
VII	–	–	–	–	18.3	8.7	27.0	4	3.5	7	12.7	16.5	12.2	13.4	–	–	–	–	–	–	–	–	–	–	–	–	6.1	7.5	7.4	7.0
VIII	–	–	–	–	19.0	9.7	29.8	11	4.5	14	12.5	17.5	12.9	14.0	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.1	6.3	6.3
IX	–	–	–	–	18.8	8.2	25.8	18	2.5	12	10.1	17.7	11.8	12.8	–	–	–	–	–	–	–	–	–	–	–	–	4.6	4.6	4.1	4.4
X	–	–	–	–	13.4	4.8	18.8	8	-0.5	16	6.7	12.4	7.9	8.7	–	–	–	–	–	–	–	–	–	–	–	–	6.6	6.2	4.9	5.9
XI	–	–	–	–	5.9	-0.8	14.7	3	-9.9	21	1.3	4.4	1.4	2.1	–	–	–	–	–	–	–	–	–	–	–	–	7.8	7.6	7.5	7.6
XII	–	–	–	–	-0.6	-8.9	17.3	5	-21.6	16	-5.2	-2.9	-5.5	-4.8	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.8	7.0	6.8
Rok	–	–	–	–	10.7	2.0	29.8	11.VIII	-24.6	16.XII	4.7	9.1	5.3	6.1	–	–	–	–	–	–	–	–	–	–	–	–	6.5	6.7	6.5	6.6

Kuźnice — φ = 49°16' — λ = 19°59'

I	–	–	–	–	-1.2	-9.8	5.6	4,30,31	-20.7	18	-6.3	-2.4	-6.3	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	5.7	5.2	5.4	5.4
II	–	–	–	–	2.2	-5.7	10.0	28	-15.6	6	-4.0	1.2	-2.7	-2.0	–	–	–	–	–	–	–	–	–	–	–	–	6.6	5.8	6.0	6.1
III	–	–	–	–	5.5	-2.1	15.2	18	-10.8	23	0.0	3.4	0.9	1.3	–	–	–	–	–	–	–	–	–	–	–	–	8.1	8.0	7.7	7.9
IV	–	–	–	–	12.7	2.1	19.8	7	-4.3	10	5.8	11.5	5.6	7.1	–	–	–	–	–	–	–	–	–	–	–	–	5.7	6.1	5.5	5.8
V	–	–	–	–	11.1	3.0	19.4	6	-2.2	13	6.4	9.4	5.6	6.8	–	–	–	–	–	–	–	–	–	–	–	–	7.8	8.3	7.9	8.0
VI	–	–	–	–	18.0	7.7	26.0	27	3.7	16,17	13.0	16.1	11.2	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.2	7.4	6.7
VII	–	–	–	–	16.8	7.1	27.2	4	2.4	7	11.7	15.1	10.4	11.9	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.7	7.9	7.1
VIII	–	–	–	–	17.7	8.1	28.4	11	2.7	17	11.4	16.3	11.3	12.6	–	–	–	–	–	–	–	–	–	–	–	–	5.7	7.1	5.9	6.2
IX	–	–	–	–	17.8	6.2	25.6	18	0.8	22	8.6	16.6	9.7	11.2	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.5	4.1	4.3
X	–	–	–	–	12.8	3.7	17.3	8	-0.2	2	6.5	11.8	6.5	7.8	–	–	–	–	–	–	–	–	–	–	–	–	5.9	6.2	5.1	5.7
XI	–	–	–	–	4.9	-1.3	12.8	3	-11.4	21	0.9	3.7	0.8	1.6	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.0	7.6	7.4
XII	–	–	–	–	-1.2	-9.2	15.8	5	-22.3	16	-5.5	-3.2	-5.5	-4.9	–	–	–	–	–	–	–	–	–	–	–	–	7.0	6.8	6.9	6.9
Rok	–	–	–	–	9.8	0.8	28.4	11.VIII	-22.3	16.XII	4.0	8.3	4.0	5.1	–	–	–	–	–	–	–	–	–	–	–	–	6.3	6.7	6.4	6.5

Łysa Polana — φ = 49°16' — λ = 20°07'

I	–	–	–	–	-0.3	-11.4	8.6	3	-22.4	18	-8.4	-2.0	-7.3	-6.2	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.0	4.8	4.7
II	–	–	–	–	3.1	-7.2	11.2	18	-17.1	6	-5.6	1.4	-3.5	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.4	5.4	5.5
III	–	–	–	–	6.5	-2.2	16.0	18	-10.0	23	-0.4	3.9	1.1	1.4	–	–	–	–	–	–	–	–	–	–	–	–	7.7	6.9	6.7	7.1
IV	–	–	–	–	13.5	0.5	26.3	7	-6.6	10	4.9	11.9	5.2	6.8	–	–	–	–	–	–	–	–	–	–	–	–	5.2	5.3	5.1	5.2
V	–	–	–	–	11.7	2.1	20.3	6	-2.7	13	6.3	9.6	5.1	6.5	–	–	–	–	–	–	–	–	–	–	–	–	7.3	6.8	7.0	7.0
VI	–	–	–	–	18.5	6.9	27.3	27	2.0	16	12.8	16.3	11.3	12.9	–	–	–	–	–	–	–	–	–	–	–	–	5.2	6.1	6.7	6.0
VII	–	–	–	–	17.2	6.5	26.5	4	0.4	7	11.5	15.3	10.6	12.0	–	–	–	–	–	–	–	–	–	–	–	–	5.5	6.1	6.6	6.1
VIII	–	–	–	–	18.6	7.3	29.3	11	2.4	14	10.5	16.6	11.5	12.5	–	–	–	–	–	–	–	–	–	–	–	–	5.1	5.8	5.4	5.4
IX	–	–	–	–	18.4	5.1	25.3	17	-1.4	22	7.3	17.0	9.2	10.8	–	–	–	–	–	–	–	–	–	–	–	–	3.8	3.9	4.0	3.9
X	–	–	–	–	13.2	2.2	17.3	8	-2.0	25	4.2	12.0	5.8	7.0	–	–	–	–	–	–	–	–	–	–	–	–	5.2	4.6	4.4	4.7
XI	–	–	–	–	5.7	-2.2	13.7	3	-12.5	21	0.0	4.3	-0.3	0.9	–	–	–	–	–	–	–	–	–	–	–	–	7.2	6.4	6.4	6.6
XII	–	–	–	–	0.0	-10.4	17.7	5	-22.5	25	-6.6	-2.9	-6.6	-5.7	–	–	–	–	–	–	–	–	–	–	–	–	6.5	5.9	6.3	6.2
Rok	–	–	–	–	10.5	-0.2	29.3	11.VIII	-22.5	25.XII	3.0	8.6	3.5	4.6	–	–	–	–	–	–	–	–	–	–	–	–	5.8	5.6	5.7	5.7

Dolina Chochołowska — φ = 49°15' — λ = 19°49'

I	–	–	–	–	-1.2	-10.8	5.7	31	-22.5	18	-7.5	-2.7	-6.6	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2.1	-7.8	10.5	28	-18.6	6	-5.9	1.0	-3.1	-2.8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	4.7	-2.7	13.8	18	-12.5	23	-1.3	3.2	0.5	0.7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	11.6	0.9	18.1	7	-5.3	10	3.2	10.9	4.9	6.0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	10.1	1.9	19.0	6	-2.9	13	4.3	9.0	4.6	5.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	17.6	6.9	25.3	27	2.1	17	9.5	16.1	11.0	11.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	16.1	6.3	24.7	4	0.1	7	8.5	15.0	10.0	10.9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	17.2	7.2	28.1	11	1.6	14	8.9	15.9	10.7	11.6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17.6	4.5	26.5	18	-0.8	22	6.4	16.6	9.2	10.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	12.2	2.7	17.1	28	-1.6	22	4.8	11.3	6.7	7.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	4.9	-1.7	12.0	3	-12.0	21	0.7	3.5	0.7	1.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-1.8	-10.0	15.3	5	-23.2	25	-6.5	-3.9	-5.7	-5.4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	9.3	-0.2	28.1	11.VIII	-23.2	25.XII	2.1	8.0	3.6	4.3	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Antałówka

$H_s = 918\ m$ $h_w = 18{,}5\ m$ 1961

MIESIĄC	ROZKŁAD WIATRU °D, °mD																				OPAD R			LICZBA DNI (n)														
	N		NE		E		SE		S		SW		W		NW		C	Średnia prędkość					Temperatura T				Wiatr v				OPAD R						
	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n	v	n		Suma	Max	Data	Min ≤ -10	Max ≤ 0°	Min ≤ 0°	Max ≥ 25°	≥ 10	≥ 15			R ≥ 0,1	R ≥ 1,0	R ≥ 10	R ≥ 100			
I	8,5	2,3	8,5	2,3	2	3,5	2,5	2,6	22,5	4,0	9	2,6	4	1,5	5	2,0	31	2,0	25,0	13,8	4	11	19	30	·	5	2	7	10	7	4	1	4	30	·
II	11	1,9	0,5	2,0	1	1,0	0,5	1,0	14,5	2,0	13,5	2,2	6	2,8	4	2,9	38	1,3	37,5	9,7	9	3	5	27	·	1	·	4	13	15	10	·	4	27	·
III	0,5	3,0	-	-	-	-	0,5	1,0	12,5	2,6	33,5	4,1	25,5	5,0	7,5	3,1	1,3	3,5	83,0	13,0	14	·	2	15	·	7	·	1	20	18	15	2	2	14	·
IV	1,0	3,3	7,5	3,1	·	·	2	5,0	22	4,8	13	3,3	7	5,3	5,5	3,5	23	3,0	26,5	9,5	8	·	·	5	·	9	·	7	11	13	8	·	2	·	1
V	5	2,3	4	2,6	5,5	2,0	4	3,0	16	2,6	16	2,9	10,5	2,8	11	3,2	21	2,1	135,2	28,3	6	·	·	2	·	1	·	·	21	21	15	4	3	·	10
VI	5	4,2	3,5	2,3	0,5	4,0	4,5	2,3	20	4,0	15,5	3,3	5	3,8	1,4	2,6	22	2,5	138,4	33,9	12	·	·	·	3	3	·	1	11	16	12	7	4	·	13
VII	4,5	2,2	·	·	·	·	2	3,8	17	3,4	19	3,3	13	4,2	8,5	3,1	29	2,4	177,3	56,5	29	·	·	·	2	4	·	2	14	18	14	5	·	·	6
VIII	2,5	2,4	3,5	2,6	·	·	·	·	11,5	4,7	30,5	2,8	20,5	2,8	8,5	3,6	16	2,6	104,4	22,4	12	·	·	·	5	5	·	3	12	13	9	4	·	·	7
IX	1,1	2,3	2,5	2,0	1	2,5	1,5	3,7	14,5	3,7	1,8	2,4	1,0	3,6	4,5	3,0	27	2,0	25,0	7,6	26	·	·	·	1	3	·	10	5	10	7	·	·	·	4
X	6	3,3	3	3,0	·	·	1,0	3,4	3,3	3,7	5	3,2	5	2,4	9	2,9	22	2,5	71,2	16,8	30	·	·	1	·	6	·	4	11	13	9	3	5	·	·
XI	4	2,2	1	2,0	1	1,0	1	1,5	12,5	3,5	1,5	2,7	1,0	3,0	8,5	1,9	37	1,6	107,8	39,6	4	·	4	17	·	4	·	·	18	18	10	4	11	13	·
XII	9,5	2,5	5	3,0	1,5	4,7	1	6,5	17,5	4,7	1,4	3,8	3,5	7,0	6	4,1	36	2,5	87,5	28,6	6	15	19	27	·	10	·	2	12	15	8	3	5	25	·
Rok	77,5	2,7	39	2,1	12,5	1,6	29,5	2,8	213,5	3,6	202	3,0	120	3,7	91	3,0	310	2,3	1018,8	56,5	29.VII	29	49	124	11	58	2	41	158	177	118	33	40	109	41

Kuźnice

$H_s = 1023\ m$ $h_w = 21{,}5\ m$

I	7,5	1,5	5,5	1,7	1,5	1,0	0,5	1,0	28,5	3,9	24	3,1	·	·	0,5	1,0	25	2,3	45,4	21,2	4	15	19	30	·	2	1	7	9	11	7	2	2	30	·
II	7	1,3	5,5	2,1	·	·	3	1,0	15,5	2,4	14,5	2,5	1	1,0	0,5	1,0	37	1,2	58,4	12,1	9	2	7	28	·	·	·	7	12	13	12	1	3	28	·
III	1,6	1,8	1,5	2,8	5	1,0	0,5	1,0	20,5	2,4	1,6	2,1	·	·	1	1,0	19	1,7	103,2	13,8	14	1	3	21	·	1	·	1	19	19	16	3	1	21	·
IV	1,0	2,0	4	2,0	1	1,0	3,5	2,1	24	3,3	19,5	3,5	1	3,0	5	1,8	22	2,2	40,6	10,8	8	·	·	6	·	1	·	6	9	13	9	2	3	·	·
V	9	1,3	6	1,5	2	2,0	5,5	1,9	21	1,9	17,5	1,8	1	3,0	2	1,0	29	1,2	179,8	37,9	17	·	·	3	·	·	·	·	17	19	15	8	3	1	3
VI	1,5	1,9	10,5	2,4	0,5	1,0	0,5	1,0	2,0	2,2	18,5	2,2	1	1,0	2	1,0	22	1,6	173,8	46,3	12	·	·	·	2	·	·	1	9	17	13	6	1	·	7
VII	1,3	1,8	8,5	2,1	4	1,5	3,5	1,0	1,8	2,2	15,5	2,2	2	1,0	0,5	1,0	28	1,4	226,2	75,3	30	·	·	·	1	·	·	1	12	20	16	5	·	·	4
VIII	15,5	1,2	1,0	1,5	6	1,3	3,5	1,3	2,3	2,5	16,5	2,1	·	·	1,5	1,0	17	1,5	129,0	35,6	13	·	·	·	4	·	·	3	11	14	10	4	2	·	2
IX	7	1,1	5	1,6	6	1,3	1	1,0	27,5	1,9	23,5	1,8	·	·	3	1,0	17	1,4	34,2	7,0	26	·	·	·	1	·	·	11	5	8	7	·	1	·	2
X	7	1,0	4,5	1,0	·	·	·	·	3,7	4,4	2,3	2,9	2	1,0	3,5	1,0	16	2,6	113,7	36,2	18	·	·	1	·	3	·	5	8	12	10	3	2	·	·
XI	8	1,5	6,5	1,6	1	1,0	·	·	2,4	2,6	1,9	2,7	1	6,0	2,5	1,0	28	1,6	133,8	49,6	4	1	4	17	·	·	·	1	16	16	10	5	7	11	·
XII	7	1,3	6,5	2,2	·	·	1,5	1,0	23,5	3,5	2,0	3,9	·	·	1,5	2,3	33	2,0	122,8	34,8	6	15	19	26	·	2	1	2	14	19	10	5	6	25	·
Rok	122	1,5	87,5	1,9	27	0,9	23	1,0	282,5	2,8	227,5	2,6	9	1,3	23,5	1,2	293	1,7	1360,9	75,3	30.VII	34	52	132	8	9	2	45	141	181	135	44	31	116	18

Łysa Polana

$H_s = 988\ m$ $h_w = 16{,}8\ m$

I	3,5	1,7	4,5	2,0	1,0	1,7	7	1,9	2,5	4,0	13,5	2,5	1,6	2,1	7	2,1	29	1,5	35,0	18,1	4	18	17	30	·	-	-	7	5	12	5	1	1	31	·
II	2	2,2	7,5	2,5	6,5	2,2	1,6	2,1	2,5	2,4	9,5	2,0	1,0	2,0	5	2,0	25	1,5	60,0	13,7	9	6	5	28	·	-	-	7	9	16	11	1	3	28	·
III	·	·	8,5	2,2	2,5	1,8	8	2,4	5	3,5	2,5	2,8	2,5,5	2,3	8,5	2,2	1,0	2,8	85,6	14,3	14	·	3	22	·	-	-	2	15	21	16	2	·	19	·
IV	3	2,5	1,0	2,2	7,5	2,3	13,5	2,1	1,1	3,1	1,3	3,0	5,5	2,2	1,5	2,0	25	1,8	31,3	12,5	8	·	·	1,4	1	-	-	5	4	11	7	1	·	1	·
V	5	2,3	3,5	2,3	5,5	2,4	1,3	2,1	3,5	3,0	1,5	2,5	1,4	1,9	7,5	2,3	26	1,6	128,6	22,4	6	·	·	8	·	-	-	·	9	21	14	5	4	2	7
VI	·	·	4,5	2,1	1,2	2,2	7,5	2,1	1,3	2,1	1,4	2,8	7	2,1	1	2,0	32	1,4	112,0	31,1	27	·	·	·	3	-	-	·	7	17	13	3	1	·	12
VII	4	1,8	9	2,9	6	2,2	13,5	2,3	9,5	2,5	1,4	2,5	1,2	2,3	3	1,3	21	1,8	179,2	49,9	29	·	·	·	2	-	-	2	6	20	16	5	1	·	7
VIII	·	·	4	2,2	9,5	2,3	13,5	1,9	6	2,5	2,1	2,3	11,5	1,9	6,5	2,3	21	1,6	99,0	21,9	3	·	·	·	5	-	-	3	7	14	10	4	1	·	6
IX	3,5	2,0	5,5	2,1	6,5	2,8	10,5	2,0	1,1	2,5	2,0	2,1	6	1,9	·	·	27	1,5	28,9	6,1	7	·	·	2	2	-	-	13	4	11	7	·	·	·	4
X	4	1,9	6,5	2,1	5,5	2,5	10,5	2,3	1,4	3,1	1,7	3,2	9,5	2,3	3	1,8	23	2,0	66,9	15,6	30	·	·	6	·	-	-	6	6	12	9	3	·	·	·
XI	8	1,9	5	2,0	5,5	2,0	5,5	1,9	4	2,2	2,1	2,5	7	2,2	1	2,0	33	1,4	129,9	40,7	4	1	2	25	·	-	-	1	13	18	11	5	6	12	·
XII	7	2,0	7,5	1,9	6,5	1,9	13,5	2,1	6	4,8	1,4	2,8	5,5	2,2	2	2,5	31	1,8	103,5	28,9	6	17	17	28	·	-	-	2	10	17	8	4	2	25	·
Rok	40	1,5	76	2,2	83,5	2,2	132	2,1	88	5,0	19,7	2,6	129,5	2,1	46	1,9	303	1,7	1059,9	49,9	29.VII	42	44	163	13	-	-	48	95	190	127	34	19	118	36

Dolina Chochołowska

$H_s = 1028\ m$ $h_w = 19\ m$

I	5,5	1,6	6	1,6	8,5	1,2	·	·	15,5	5,3	10,5	5,7	·	·	·	·	47	1,8	31,6	14,2	4	17	18	29	·	4	2	-	-	9	4	1	·	30	-
II	1,0	1,8	8	1,6	1	2,0	·	·	7	3,3	1	9,0	·	·	·	·	57	0,8	36,0	8,5	28	8	6	28	·	1	1	-	-	13	9	·	-	27	-
III	13,5	1,7	10,5	1,5	·	·	6,5	2,2	1,6	2,5	6	3,6	0,5	10,0	·	·	40	1,3	98,7	24,8	14	1	6	24	·	2	·	-	-	19	14	2	-	21	-
IV	1,0	2,1	3	1,3	2	1,5	0,5	1,0	3,4	3,1	2,5	2,4	·	·	·	·	38	1,6	52,8	9,5	16	·	·	9	·	1	·	-	-	14	9	·	·	3	-
V	14,5	1,9	4,5	1,7	5	1,0	·	·	11,5	1,6	2,5	1,4	·	·	·	·	55	0,7	170,8	28,4	17	·	·	6	·	·	·	-	-	20	18	6	8	2	-
VI	6	1,8	4	1,9	2	1,5	1,5	1,0	1,8	2,3	1,5	1,7	·	·	·	·	57	0,7	173,5	29,7	12	·	·	·	1	·	·	-	-	18	14	8	4	·	-
VII	7,5	1,5	10	1,3	3	1,7	4	1,4	2,7	2,0	2,5	3,4	·	·	·	·	39	1,0	182,7	51,4	29	·	·	·	·	·	·	-	-	13	12	6	4	·	-
VIII	9	1,7	9	1,8	·	·	2	1,0	2,4,5	2,4	1,5	2,0	·	·	·	·	47	1,0	98,9	18,4	12	·	·	·	4	1	·	-	-	12	11	4	4	·	-
IX	11,5	2,0	5,5	2,6	1	2,0	6	1,8	2,6	2,2	·	·	1	4,0	·	·	39	1,2	35,7	8,5	14	·	·	3	1	1	·	-	-	8	6	·	3	·	-
X	4	1,8	5	2,0	1	2,0	·	·	37,5	6,4	3,5	3,1	·	·	·	·	42	2,9	102,2	44,6	18	·	·	6	·	5	2	-	-	11	8	3	3	·	-
XI	1,1	1,5	2	2,0	3	1,0	·	·	16,5	3,1	4,5	2,7	1	1,0	·	·	52	1,0	83,1	21,6	4	1	3	21	·	·	·	-	-	14	10	3	4	12	-
XII	23,5	3,1	3,5	3,1	1	1,0	·	·	2,1	3,6	1	3,5	1	4,0	·	·	42	1,8	84,6	23,2	11	14	20	27	·	1	·	-	-	17	9	3	1	25	-
Rok	12,6	1,9	7,1	1,8	27,5	1,2	20,5	0,7	254,5	3,2	3,7	3,2	3,5	1,6	·	·	555	1,3	1150,6	51,4	29.VII	41	53	153	6	16	5	-	-	168	124	36	-	120	-

Myślenickie Turnie — φ = 49°15' — λ = 19°59' — 1961

MIESIĄC	CIŚNIENIE P				TEMPERATURA T						Średnia				ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
	P_m	Max	Min	$P_{o.m}$	— Max	— Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-2.5	-8.2	4.0	31	-19.6	18	-5.5	-4.6	-5.6	-5.3	–	–	–	–	–	–	–	–	–	–	–	–	5.9	5.5	5.2	5.5
II	–	–	–	–	1.8	-4.4	9.9	18	-13.0	6	-1.7	-0.6	-1.6	-1.4	–	–	–	–	–	–	–	–	–	–	–	–	5.6	6.1	6.2	6.0
III	–	–	–	–	3.1	-3.1	11.9	18	-11.0	23	-1.3	0.6	0.0	-0.2	–	–	–	–	–	–	–	–	–	–	–	–	8.5	8.7	7.9	8.4
IV	–	–	–	–	9.8	2.5	17.4	7	-5.0	10	4.6	8.2	5.1	5.8	–	–	–	–	–	–	–	–	–	–	–	–	6.0	6.2	5.6	5.9
V	–	–	–	–	8.2	2.5	16.6	6	-4.4	12	4.0	6.2	4.6	4.8	–	–	–	–	–	–	–	–	–	–	–	–	7.9	8.8	7.2	8.0
VI	–	–	–	–	15.6	8.5	23.2	25	3.8	15	10.8	13.3	11.1	11.6	–	–	–	–	–	–	–	–	–	–	–	–	5.6	7.6	7.4	6.9
VII	–	–	–	–	14.4	7.3	22.8	3	3.2	30	9.7	12.1	10.2	10.6	–	–	–	–	–	–	–	–	–	–	–	–	6.3	7.6	7.5	7.1
VIII	–	–	–	–	15.3	8.2	25.6	11	3.2	17,18	10.4	13.3	11.1	11.5	–	–	–	–	–	–	–	–	–	–	–	–	5.9	7.3	6.5	6.6
IX	–	–	–	–	15.2	8.7	24.4	18	2.7	11	10.7	13.5	11.4	11.8	–	–	–	–	–	–	–	–	–	–	–	–	4.2	4.7	4.0	4.3
X	–	–	–	–	10.7	4.9	14.9	28	-0.7	14	6.1	8.9	7.1	7.3	–	–	–	–	–	–	–	–	–	–	–	–	6.1	6.3	5.2	5.9
XI	–	–	–	–	4.7	-1.1	9.7	23	-11.5	21	1.6	2.7	1.6	1.9	–	–	–	–	–	–	–	–	–	–	–	–	7.4	7.8	7.6	7.6
XII	–	–	–	–	-2.0	-9.0	12.7	5	-23.9	16	-5.8	-4.5	-5.9	-5.5	–	–	–	–	–	–	–	–	–	–	–	–	6.8	7.1	6.0	6.6
Rok	–	–	–	–	7.9	1.4	25.6	11.VIII	-23.9	16.XII	3.6	5.8	4.1	4.4	–	–	–	–	–	–	–	–	–	–	–	–	6.4	7.0	6.4	6.6

Hala Gąsienicowa — φ = 49°15' — λ = 20°00'

I	842.3	854.3	829.0	–	-2.9	-9.8	2.7	31	-20.2	17	-6.2	-4.6	-6.7	-6.0	2.6	2.8	2.6	2.7	6.4	6.1	6.6	6.4	1.5	1.7	1.3	1.5	4.9	4.8	4.5	4.7
II	846.6	860.3	821.8	–	1.3	-6.1	7.3	15	-16.6	6	-3.2	-0.7	-2.8	-2.4	3.0	3.6	3.1	3.2	6.3	6.6	6.5	6.4	2.0	2.5	2.0	2.2	5.7	5.5	5.0	5.4
III	845.3	859.1	824.5	–	1.7	-4.6	11.0	10	-14.0	23	-2.4	-0.2	-1.4	-1.4	3.9	4.1	4.2	4.1	7.6	7.1	7.6	7.4	1.4	2.2	1.6	1.7	8.0	8.3	7.5	7.9
IV	842.2	847.2	836.4	–	8.1	1.0	13.1	7	-7.1	10	4.3	6.9	3.8	4.7	5.1	5.8	6.0	5.6	6.1	5.9	7.5	6.5	3.4	4.4	2.2	3.3	5.5	5.6	5.0	5.4
V	842.1	849.0	832.6	–	6.5	0.9	13.5	29	-5.4	13	3.2	4.9	3.0	3.5	6.3	6.6	6.5	6.5	8.1	7.6	8.4	8.0	1.6	2.4	1.3	1.8	7.3	8.4	6.8	7.5
VI	847.8	857.6	839.3	–	14.0	6.7	20.5	27	1.3	16	10.1	11.9	9.4	10.2	9.0	9.5	9.4	9.3	7.4	7.0	7.9	7.4	3.6	4.8	2.7	3.7	4.8	7.0	6.7	6.2
VII	846.8	856.8	835.2	–	12.6	5.4	20.7	4	0.2	7	8.9	10.7	8.4	9.1	8.2	8.7	8.7	8.5	7.3	6.9	7.9	7.4	3.6	4.7	2.7	3.7	5.7	7.5	6.8	6.7
VIII	849.6	859.6	839.3	–	13.5	6.4	23.4	11	0.6	14	10.0	12.0	9.5	10.2	8.5	9.8	9.6	9.3	7.0	7.1	8.1	7.4	4.3	5.0	2.7	4.0	5.3	6.7	5.3	5.8
IX	851.0	860.3	842.5	–	13.9	6.4	22.0	18	1.5	11	9.2	12.5	9.2	10.0	6.8	8.7	7.6	7.7	5.9	6.1	6.6	6.2	5.2	6.3	4.3	5.3	3.8	4.5	3.4	3.9
X	848.1	857.9	826.6	–	9.8	3.4	14.2	25	-1.9	14	5.3	8.3	5.9	6.4	5.8	6.6	6.0	6.1	6.7	6.2	6.6	6.5	3.3	4.7	3.4	3.7	5.9	5.9	4.0	5.3
XI	841.4	855.2	833.2	–	4.2	-2.3	8.5	1	-12.9	21	0.4	2.1	0.9	1.1	4.5	4.8	4.3	4.5	7.1	6.9	7.1	7.0	2.0	2.6	2.1	2.2	6.9	6.6	6.1	6.5
XII	839.0	853.3	830.0	–	-2.7	-10.3	11.3	5	-24.3	16	-6.7	-5.1	-6.5	-6.2	3.1	3.2	3.2	3.2	7.3	6.8	7.4	7.2	1.2	1.7	1.1	1.3	6.1	6.0	5.0	5.7
Rok	845.2	860.3	821.8	–	6.7	-0.2	23.4	11.VIII	-24.3	16.XII	2.7	4.9	2.7	3.2	5.6	6.2	5.9	5.9	6.9	6.7	7.4	7.0	2.8	3.6	2.3	2.9	5.8	6.4	5.5	5.9

Hala Ornak — φ = 49°14' — λ = 19°51'

I	–	–	–	–	-1.1	-12.9	6.4	30	-25.2	18	-8.2	-2.6	-7.7	-6.6	–	–	–	–	–	–	–	–	–	–	–	–	3.6	4.0	4.2	3.9
II	–	–	–	–	1.9	-8.4	10.1	28	-19.0	6	-6.0	0.9	-4.3	-3.4	–	–	–	–	–	–	–	–	–	–	–	–	4.4	5.0	5.2	4.9
III	–	–	–	–	3.9	-3.4	13.3	10	-12.7	23	-1.4	2.3	-0.6	-0.1	–	–	–	–	–	–	–	–	–	–	–	–	7.5	7.4	6.4	7.1
IV	–	–	–	–	12.0	-0.1	18.3	7	-7.0	10	3.4	10.4	4.3	5.6	–	–	–	–	–	–	–	–	–	–	–	–	4.6	5.0	5.0	4.9
V	–	–	–	–	10.4	0.8	18.7	6	-4.3	13	4.3	8.5	3.9	5.2	–	–	–	–	–	–	–	–	–	–	–	–	6.8	6.9	6.5	6.7
VI	–	–	–	–	17.4	6.3	25.1	25	0.4	17	10.3	15.2	10.8	11.8	–	–	–	–	–	–	–	–	–	–	–	–	4.8	6.8	7.3	6.3
VII	–	–	–	–	16.7	5.3	25.2	4	-1.6	6	9.2	14.7	9.6	10.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	7.0	6.5	6.3
VIII	–	–	–	–	17.7	6.4	28.0	11	0.9	14,17	9.2	15.9	10.1	11.3	–	–	–	–	–	–	–	–	–	–	–	–	5.0	6.3	5.1	5.5
IX	–	–	–	–	17.5	3.1	26.7	18	-2.7	22	5.5	16.5	7.4	9.2	–	–	–	–	–	–	–	–	–	–	–	–	3.4	4.0	3.5	3.6
X	–	–	–	–	11.8	2.0	15.7	8	-3.2	22	4.1	10.9	5.5	6.5	–	–	–	–	–	–	–	–	–	–	–	–	4.8	5.4	4.2	4.8
XI	–	–	–	–	4.5	-2.3	14.7	3	-13.5	21	0.0	3.2	-0.2	0.7	–	–	–	–	–	–	–	–	–	–	–	–	6.9	6.5	6.2	6.5
XII	–	–	–	–	-1.9	-10.8	15.2	5	-25.5	17	-6.7	-3.5	-6.6	-5.8	–	–	–	–	–	–	–	–	–	–	–	–	7.4	5.9	6.1	6.5
Rok	–	–	–	–	9.2	-1.2	28.0	11.VIII	-25.5	17.XII	2.0	7.7	2.7	3.8	–	–	–	–	–	–	–	–	–	–	–	–	5.4	5.8	5.5	5.6

Kasprowy Wierch — φ = 49°14' — λ = 19°59'

I	793.3	805.1	780.3	–	-6.6	-11.6	-1.0	14	-23.7	17	-9.1	-8.7	-9.0	-9.0	2.4	2.5	2.4	2.4	7.4	7.6	7.4	7.5	0.8	0.8	0.8	0.8	5.5	5.7	5.7	5.6
II	798.3	812.6	777.0	–	-2.2	-7.7	3.6	18,22	-16.6	6	-5.4	-4.2	-5.0	-4.9	2.6	3.2	2.7	2.8	6.7	7.4	6.9	7.0	1.7	1.5	1.7	1.6	6.1	6.4	5.2	5.9
III	796.9	810.5	775.7	–	-2.4	-8.0	6.3	10	-15.4	23	-5.9	-4.4	-4.9	-5.0	3.5	3.7	3.8	3.7	8.8	8.5	8.8	8.7	0.6	0.9	0.7	0.9	8.6	8.8	8.3	8.6
IV	795.1	801.4	789.0	–	3.7	-1.9	9.5	7	-10.9	1	-0.1	2.3	0.6	0.8	4.7	5.6	5.4	5.2	7.7	7.9	8.4	8.0	1.5	1.8	1.1	1.5	6.5	7.1	5.4	6.3
V	794.8	802.6	786.5	–	2.4	-2.0	9.3	6	-7.5	13	-0.9	1.1	-0.1	0.0	5.5	6.1	5.8	5.8	9.4	9.0	9.4	9.3	0.4	0.8	0.4	0.5	8.1	9.0	7.5	8.2
VI	801.6	810.7	793.1	–	10.4	4.0	17.1	25	-0.6	16,29	6.0	8.3	6.3	6.7	7.8	8.9	8.7	8.5	8.2	8.2	9.1	8.5	1.8	2.3	1.0	1.7	6.1	8.3	7.8	7.4
VII	800.4	811.1	789.6	–	9.0	2.6	18.5	3	-1.5	7	4.3	7.0	5.2	5.4	7.2	8.1	7.9	7.7	8.7	8.1	8.9	8.6	1.4	2.4	1.2	1.7	6.4	8.2	7.7	7.4
VIII	803.2	812.3	792.1	–	10.0	3.9	18.8	11	-1.6	24	6.0	8.1	6.4	6.7	7.5	8.9	8.7	8.4	8.0	8.2	9.0	8.4	2.1	2.5	1.3	2.0	6.3	7.6	6.4	6.8
IX	804.7	814.4	795.8	–	10.7	4.8	18.4	18	-1.4	10	6.7	9.4	6.9	7.5	5.4	7.6	6.7	6.6	5.7	6.6	7.0	6.4	4.7	4.5	3.5	4.2	4.5	5.2	4.4	4.7
X	801.0	811.2	778.8	–	5.7	0.5	9.8	1	-5.1	14	2.5	3.9	2.7	3.0	5.4	6.4	6.4	5.7	7.5	8.0	7.5	7.7	2.1	1.9	2.1	2.0	6.6	6.5	4.9	6.0
XI	793.8	806.3	785.4	–	0.5	-4.6	5.5	24	-14.2	20,21	-2.2	-1.4	-2.0	-1.9	4.1	4.5	4.2	4.3	7.7	8.1	8.0	7.9	1.3	1.2	1.3	1.3	7.9	8.1	7.4	7.8
XII	790.1	803.0	780.2	–	-6.1	-12.2	5.7	5	-28.0	16	-9.5	-8.5	-9.3	-9.2	3.0	3.1	3.1	3.1	8.5	8.7	8.9	8.7	0.5	0.5	0.3	0.4	6.9	7.1	6.7	6.9
Rok	799.8	814.4	778.0	–	2.9	-2.7	18.8	11.VIII	-28.0	16.XII	-0.6	1.1	-0.2	0.0	4.9	5.7	5.4	5.3	7.9	8.0	8.3	8.1	1.6	1.8	1.3	1.6	6.6	7.3	6.4	6.8

Myślenickie Turnie $H_s = 1360$ m $h_w = 19{,}5$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R f0
I	1	3.0	7	1.5	7.5	1.6	5	1.7	31.5	4.6	29.5	4.9	3.5	2.9	2	2.0	6	3.6	37.3	15.0	4	9	22	31	·	7	·	4	8	12	6	2	1	31	·
II	5	3.2	8.5	1.9	14.5	1.3	6	1.6	23	3.0	17	3.9	4	1.5	4	3.5	2	2.6	48.0	8.7	9	1	11	25	·	2	·	6	11	14	12		4	28	·
III	9.5	4.3	10	2.7	12.5	3.1	6	2.7	15	5.5	26	5.1	6	4.2	8	3.6	·	4.2	84.1	11.6	14	3	9	24	·	1	·	1	20	18	18	2	5	31	
IV	5	3.3	7	2.2	12.5	2.5	7.5	2.4	26.5	5.3	24	5.7	3	3.3	0.5	2.0	4	4.1	53.7	12.0	8	·	·	6	·	5	·	4	9	11	9	2	4	5	1
V	4.5	3.0	19.5	2.0	17	1.6	12.5	1.6	18.5	3.8	16	4.4	1	1.0	2	3.8	2	2.7	175.6	33.8	6	·	1	8	·	·	·	·	17	19	16	8	10	8	4
VI	3.5	3.0	18	1.9	16.5	2.2	11	1.6	14	4.5	19.5	4.6	2.5	3.4	3	3.7	2	3.0	178.8	38.5	12	·	·	·	·	1	·	·	12	18	15	7	3	·	6
VII	9	2.6	17	1.7	12.5	1.4	5	1.2	18	4.3	23.5	4.3	15	3.3	4.5	1.9	2	2.9	203.7	63.0	29	·	·	·	·	1	·	2	13	18	17	4	3	·	4
VIII	3.5	3.6	14	2.2	15	1.9	11.5	1.8	16.5	5.0	21	4.6	4.5	3.1	5	3.6	2	3.3	139.8	33.7	13	·	·	·	2	3	·	4	12	12	11	5	5	·	2
IX	3.5	2.1	9	1.5	8	1.5	7	1.4	27.5	3.3	23	4.3	3	2.5	4	2.2	5	2.6	34.2	7.8	26	·	·	·	·	3	·	11	5	8	7	·	1	·	2
X	1	3.0	15	1.6	9.5	1.4	2.5	1.0	28	7.9	33.5	6.8	0.5	7.0	1	1.0	2	5.3	128.9	42.8	18	·	·	1	·	9	5	7	10	11	9	4	8	·	·
XI	3.5	2.6	6.5	1.9	5.5	1.9	10.5	1.1	32	4.2	25.5	5.2	1.5	2.0	2	5.5	3	3.6	142.3	45.0	4	1	5	14	·	6	2	1	17	14	12	5	10	13	·
XII	6.5	3.6	18	2.3	3.5	2.3	1.5	1.7	19	7.1	25.5	6.7	4	3.1	2	4.0	13	4.3	77.0	18.3	6	15	17	24	·	7	2	2	11	16	9	3	5	25	·
Rok	55.5	3.1	149.5	2.0	134.5	1.9	86	1.6	269.5	4.9	284	5.0	35	3.1	38	3.1	43	3.5	1303.4	63.0	29.VII	29	65	133	2	45	9	42	145	171	141	42	59	141	19

Hala Gąsienicowa $H_s = 1520$ m $H_b = 1520{,}8$ m $h_w = 16$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R f0
I	6	2.7	6	3.6	1	2.5	·	·	11	9.9	50.5	4.8	7.5	3.3	·	·	11	4.5	38.8	14.6	4	13	24	31	·	8	2	6	6	12	6	2	3	31	·
II	6	2.2	5.5	2.2	0.5	4.0		·	3.5	6.8	44.5	3.9	15.5	3.5	1.5	3.5	7	3.3	75.7	14.3	9	3	11	26	·	2	·	7	10	15	11	2	10	28	·
III	15	3.2	14.5	3.4	6	3.2	3	3.8	10	3.4	30	3.8	7.5	2.7	6	3.8	2	3.4	120.4	17.7	14	4	11	27	·	4	·	2	19	20	18	4	11	31	
IV	6	4.2	4.5	3.0	4.5	2.9	0.5	3.0	9	5.2	50.5	4.7	6	2.8	1	4.5	8	4.0	50.4	12.7	8	·	·	9	·	4	·	7	8	13	8	2	4	13	1
V	7.5	2.3	11	2.2	1.5	2.7	1	2.0	7.5	4.6	38	3.7	9.5	3.1	3	2.8	14	2.8	198.2	35.1	6	·	1	12	·	1	·	1	15	22	18	7	14	12	8
VI	10	2.7	9.5	2.6	2	2.0	1.5	4.0	7	4.8	27.5	4.3	11	3.0	0.5	4.0	21	2.8	167.3	26.4	27	·	·	·	·	2	·	3	9	18	16	7	7	·	10
VII	5.5	3.0	4	3.0	1.5	4.3	0.5	2.0	11.5	5.7	43.5	3.9	12.5	2.8	2	3.0	12	3.3	212.6	62.7	30	·	·	·	·	4	1	3	12	21	16	5	6	·	4
VIII	2.5	4.6	6	2.6	0.5	4.0	1	4.0	9	5.4	48.5	4.2	18.5	3.4	1	4.5	6	3.8	129.5	39.9	13	·	·	·	·	4	·	6	10	14	10	5	9	·	4
IX	13.5	3.1	1.5	2.7	·		1.5	3.7	7	7.4	52	3.5	5.5	3.4	2	2.5	7	3.4	54.1	11.3	26	·	·	·	·	3	·	11	3	10	8	1	5	·	3
X	1	2.5	9	2.6	0.5	3.0	1	5.0	15.5	7.7	51.5	5.2	10.5	3.7	1	3.0	3	5.0	136.0	43.7	17	·	·	4	·	7	3	8	9	13	11	3	6	1	·
XI	7.5	3.0	5.5	3.0	1	3.0	2	2.0	9.5	7.1	46	4.7	8.5	3.1	·	·	9	3.9	157.6	42.1	4	2	4	20	·	4	·	3	15	17	12	6	7	19	·
XII	9.5	4.2	17	3.5	0.5	5.0	2	4.5	6.5	9.1	44	5.0	5.5	2.6	1	4.0	7	4.4	93.5	22.0	6	16	18	26	·	8	·	2	7	20	12	4	9	25	·
Rok	90	3.1	94	2.9	19.5	2.8	14	2.8	107	6.4	526.5	4.3	118	3.1	19	3.0	107	3.7	1434.1	62.7	30.VII	38	69	155	·	51	6	59	123	195	146	48	91	160	30

Hala Ornak $H_s = 1110$ m $h_w = 17{,}8$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R f0
I	1.5	2.3	1	4.0	·		2.5	5.8	13	5.3	1.5	5.0		·	1.5	9.0	72	1.2	51.9	26.2	4	21	21	30	·	2	·	12	6	10	7	1	1	29	–
II	3	3.0	1	3.0					5	2.6	0.5	3.0	0.5	3.0	·		74	0.3	45.7	12.0	10	8	7	28	·	·	·	9	7	13	9	1	4	28	–
III	7	2.7	7	3.3	2.5	1.8	4.5	3.4	6.5	2.5	2	3.5	1	1.0	0.5	3.0	62	0.9	116.4	17.0	28	1	6	27	·	·	·	4	16	19	16	3	13	30	–
IV	5	1.6	2	2.0	2.5	1.0	2.5	2.6	22.5	4.6	2.5	2.6				·	53	1.4	43.5	9.1	19	·	·	14	·	2	1	7	5	13	10	·	4	4	–
V	3	1.0	1	1.0			·	·	8.5	2.3	1.5	3.0	2	3.0	·		77	0.4	171.7	25.3	17	·	·	10	·	·	·	2	12	22	18	7	12	2	–
VI	3	1.7	0.5	1.0	0.5	1.0	·	·	13	3.4	1.5	1.0	0.5	1.0			71	0.6	179.2	27.3	13	·	·	·	1	1	·	2	10	15	14	6	10	·	–
VII	·	·	·	·		·	·	·	16	3.7	4	2.8	·		1	1.0	72	0.8	212.6	72.0	30	·	·	2	1	·	·	4	9	16	13	5	14	·	–
VIII	1.5	1.0	3.5	1.3	1	1.0	1	1.0	9.5	3.9	1	6.0	0.5	3.0	3	4.7	72	0.6	109.2	28.1	13	·	·	·	5	·	·	7	11	12	9	4	10	·	–
IX	2	1.5	2.5	1.4	1	1.0	0.5	8.0	11	3.4	1	6.5	2	1.0	4	1.0	66	0.7	50.0	12.1	14	·	·	5	2	1	·	12	4	12	8	2	3	·	–
X	2	1.0	·	·		·	0.5	3.0	31.5	5.6	5	3.2	0.5	1.0	1.5	1.0	52	2.1	163.1	68.0	18	·	·	10	·	2	1	8	7	13	11	4	9	·	–
XI	7.5	1.4	0.5	3.0	·	·	0.5	1.0	15.5	2.9	3	4.5		·	3	3.0	60	0.8	139.0	49.1	13	1	5	25	·	·	·	5	14	15	11	5	9	11	–
XII	12	1.6	10.5	1.5	0.5	1.0	0.5	3.0	7	3.4	11.5	3.1	4	2.0	·	·	47	1.1	138.4	33.0	6	17	20	25	·	·	·	2	13	19	14	5	14	25	–
Rok	47.5	1.6	29.5	1.5	8	0.6	12.5	2.3	159	3.6	35	3.7	11	1.2	14.5	1.6	778	0.9	1372.7	72.0	30.VII	48	59	176	9	8	2	74	114	179	140	43	103	129	–

Kasprowy Wierch $H_s = 1991$ m $H_b = 1988{,}8$ m $h_w = 15{,}4$ m

MIESIĄC	N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	Min < -10°	Max < 0°	Min < 0°	Max > 25°	v ≥ 10	v ≥ 15	◐	●	R ≥ 0.1	R ≥ 1.0	R ≥ 10.0	═	⊠	R f0
I	21	5.7	11	5.0	2	3.5	12	12.8	24.5	10.3	11	6.0	6.5	4.7	3	2.8	2	7.5	44.9	11.8	4	20	31	31	·	20	11	6	8	16	12	1	21	31	·
II	22	4.3	5.5	3.6	1	2.0	6.5	6.3	12.5	5.7	5.5	6.5	10.5	5.1	14.5	4.6	6	4.6	80.0	16.0	5	8	16	27	·	12	1	5	11	16	12	2	18	28	
III	32	7.9	16	7.0	·		0.5	1.0	2	6.2	7	11.6	14	9.1	21.5	8.9	·	8.4	166.3	21.3	14	11	22	31		22	7	1	24	25	22	7	29	31	
IV	4.5	4.6	14.5	3.7	3.5	3.6	4.5	6.8	20	7.8	21	7.6	11.5	5.8	5.5	6.4	5	5.9	47.0	8.2	19	1	3	22		17	4	2	10	14	8	·	17	28	1
V	23	3.9	21	4.3	2	3.2	2	6.5	13	6.5	11	6.4	7.5	5.6	8.5	4.7	5	4.7	185.9	(35.9)	17	·	10	23		9	·	·	20	22	19	6	27	20	8
VI	13	3.3	13.5	3.9	5	3.0	5	4.0	12	4.9	12.5	7.5	11.5	3.7	11.5	2.8	6	4.0	162.3	19.0	22	·	·	3		12	·	·	13	18	16	8	18	·	13
VII	11.5	4.2	11	3.9	·	·	0.5	2.0	11.5	6.7	23.5	5.8	14.5	4.6	15.5	4.5	5	4.7	168.8	44.3	29		·	6	·	11	2	·	14	21	15	5	22	2	6
VIII	12.5	5.4	14.5	5.2				·	12.5	5.8	25	6.6	13.5	5.8	12	5.1	3	5.6	100.8	24.2	13		·	7	·	10	3	1	11	13	11	3	22	3	6
IX	14.5	3.4	12	3.6	4	3.1	2	1.8	8.5	6.0	18.5	6.0	13	4.8	15.5	4.5	2	4.5	40.6	8.7	26	·	·	2	·	9	1	10	8	11	8	·	10	·	4
X	8.5	4.0	8.5	4.5	2	2.8	8	9.9	34	9.6	23	8.3	4	3.8	3	6.7	2	7.6	102.0	25.1	17		2	10	·	17	8	5	8	13	13	4	15	3	·
XI	12	5.3	7.5	5.4	1	6.0	10.5	6.8	21.5	10.2	18.5	8.6	14.5	6.0	4.5	3.8	·	7.4	154.6	26.3	4	3	10	28	·	19	9	1	17	19	16	7	23	30	·
XII	16.5	9.4	22	8.4	5	6.2	2.5	4.4	18.5	10.1	17.5	9.2	5	9.2	4	9.4	2	8.8	138.8	24.7	6	19	25	31	·	26	8	2	13	26	17	5	26	31	·
Rok	191	5.1	157	4.9	25.5	2.8	54	5.2	190.5	7.5	194	7.5	126	5.7	119	5.4	38	6.1	1392.0	44.3	29.VII	62	119	221	·	184	54	33	157	214	169	48	248	207	38

Uwaga. Kierunki i prędkości wiatru – wg anemografu, w okresach oblodzenia tego przyrządu – prędkość wiatru mierzono anemotachimetrem.

Dolina Pięciu Stawów — φ = 49°13' — λ = 20°03' — 1961

MIESIĄC	CIŚNIENIE p				TEMPERATURA T									ŚREDNIA PRĘŻNOŚĆ PARY e_m				ŚREDNIA WILGOTNOŚĆ WZGLĘDNA U_m				ŚREDNI NIEDOSYT WILGOTNOŚCI Δ_m				ŚREDNIE ZACHMURZENIE N_m			
									Średnia																			
	P_m	Max	Min	$P_{o.m}$	Max	Min	Max abs.	Data	Min abs.	Data	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies	I	II	III	Dies
I	–	–	–	–	-4,5	-14,0	1,3	31	-25,0	17	-8,6	-6,5	-7,9	-7,7	–	–	–	–	–	–	–	–	–	–	–	–	5,7	4,5	4,8	5,0
II	–	–	–	–	0,6	-7,4	7,2	18	-21,2	6	-4,7	-1,8	-3,8	-3,5	–	–	–	–	–	–	–	–	–	–	–	–	5,0	4,8	4,6	4,8
III	–	–	–	–	0,8	-6,9	8,5	10	-16,2	22	-3,6	-1,9	-2,7	-2,7	–	–	–	–	–	–	–	–	–	–	–	–	7,5	7,9	7,6	7,7
IV	–	–	–	–	7,3	-1,1	12,0	15	-10,0	1	2,4	5,3	2,4	3,1	–	–	–	–	–	–	–	–	–	–	–	–	4,6	5,7	5,0	5,1
V	–	–	–	–	5,9	-0,2	12,9	6	-4,9	13	4,9	3,6	2,1	2,4	–	–	–	–	–	–	–	–	–	–	–	–	7,8	8,6	6,9	7,8
VI	–	–	–	–	14,4	5,8	22,3	27	1,2	16,29	9,2	11,7	9,2	9,8	–	–	–	–	–	–	–	–	–	–	–	–	5,2	6,8	6,7	6,2
VII	–	–	–	–	11,9	4,6	21,3	3	0,1	7	7,6	9,8	7,8	8,3	–	–	–	–	–	–	–	–	–	–	–	–	5,2	6,5	6,5	6,1
VIII	–	–	–	–	13,8	5,0	24,0	10	-0,9	18	8,6	11,6	9,4	9,8	–	–	–	–	–	–	–	–	–	–	–	–	4,6	6,0	5,0	5,2
IX	–	–	–	–	13,6	5,7	23,3	18	0,7	11	8,5	12,2	8,6	9,5	–	–	–	–	–	–	–	–	–	–	–	–	3,1	3,0	3,3	3,1
X	–	–	–	–	8,6	1,7	12,7	16,28	-3,2	14	4,3	7,0	4,7	5,2	–	–	–	–	–	–	–	–	–	–	–	–	4,7	4,7	6,4	5,3
XI	–	–	–	–	2,7	-2,8	7,0	2	-12,3	20	-0,3	0,6	-0,1	0,0	–	–	–	–	–	–	–	–	–	–	–	–	8,1	8,2	7,3	7,9
XII	–	–	–	–	-3,8	-11,0	9,2	5	-24,2	15	-7,2	-6,4	-7,2	-7,0	–	–	–	–	–	–	–	–	–	–	–	–	8,5	7,2	6,6	7,4
Rok	–	–	–	–	5,9	-1,5	24,0	10.VIII	-25,0	17.1	4,5	3,8	1,9	2,3	–	–	–	–	–	–	–	–	–	–	–	–	5,8	6,2	5,9	6,0

Morskie Oko — φ = 49°12' — λ = 20°04'

I	–	–	–	–	-2,7	-12,0	4,6	29	-23,7	18	-7,1	-5,9	-7,5	-7,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
II	–	–	–	–	2,8	-9,0	9,7	18	-18,7	6	-4,7	-0,2	-4,3	-3,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
III	–	–	–	–	4,2	-4,9	12,6	10	-16,1	23	-2,4	1,2	-0,8	-0,7	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IV	–	–	–	–	9,7	1,1	15,5	14	-7,1	10	3,1	7,8	4,1	4,8	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
V	–	–	–	–	8,1	1,2	14,3	5	-4,3	13	3,4	5,4	3,7	4,0	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VI	–	–	–	–	16,0	6,5	23,7	27	1,3	29	10,0	13,3	10,1	10,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VII	–	–	–	–	14,6	5,2	24,9	4	0,0	6,7	8,3	12,2	9,0	9,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
VIII	–	–	–	–	16,0	6,9	24,6	11	1,1	14	9,3	13,3	9,7	10,5	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
IX	–	–	–	–	17,3	5,9	24,0	17	0,6	12	8,0	14,7	9,0	10,2	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
X	–	–	–	–	11,7	3,0	17,7	28	-1,4	14	4,9	9,5	6,1	6,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XI	–	–	–	–	4,4	-2,1	9,8	1	-12,7	21	0,4	1,9	0,7	0,9	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
XII	–	–	–	–	-2,2	-11,3	11,9	5	-25,7	23,24	-7,4	-5,6	-6,8	-6,6	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–
Rok	–	–	–	–	8,3	-0,8	24,9	4.VII	-25,7	23,24.XII	2,2	5,6	2,8	3,4	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–	–

Ustrzyki Górne — φ = 49°07' — λ = 22°40'

I	–	–	–	–	-2,6	–	8,4	4	–	–	-6,9	-3,6	-7,2	-6,2	–	–	–	–	–	–	–	–	–	–	–	–	7,7	5,5	7,0	6,7
II	–	–	–	–	0,6	-5,3	5,7	23	-19,8	15	-3,2	-0,5	-2,3	-2,1	–	–	–	–	–	–	–	–	–	–	–	–	9,6	7,6	7,9	8,4
III	–	–	–	–	6,6	-2,2	16,3	10	-12,4	23	0,4	4,8	4,8	2,2	–	–	–	–	–	–	–	–	–	–	–	–	8,2	7,1	7,1	7,5
IV	–	–	–	–	14,6	0,5	21,2	8	-5,9	13	6,0	13,2	6,4	8,0	–	–	–	–	–	–	–	–	–	–	–	–	4,0	5,4	4,2	4,5
V	–	–	–	–	14,1	2,4	23,7	29	-3,1	24	7,4	12,5	6,8	8,4	–	–	–	–	–	–	–	–	–	–	–	–	7,0	7,8	5,6	6,8
VI	–	–	–	–	20,7	6,5	27,1	27	0,6	17	13,1	18,8	12,0	14,0	–	–	–	–	–	–	–	–	–	–	–	–	5,5	7,0	5,6	6,0
VII	–	–	–	–	19,9	6,8	27,4	3,4	0,8	7	12,4	18,2	11,8	13,6	–	–	–	–	–	–	–	–	–	–	–	–	6,0	6,6	5,9	6,2
VIII	–	–	–	–	20,4	7,9	29,9	10	0,6	31	12,2	19,2	12,2	14,0	–	–	–	–	–	–	–	–	–	–	–	–	5,5	5,4	4,7	5,2
IX	–	–	–	–	18,8	3,5	26,8	17	-5,4	23	7,1	18,1	8,7	10,6	–	–	–	–	–	–	–	–	–	–	–	–	4,6	4,5	3,0	4,0
X	–	–	–	–	14,7	1,7	(25,4)	20	-7,8	13	4,0	14,2	5,6	7,3	–	–	–	–	–	–	–	–	–	–	–	–	5,5	4,3	3,6	4,5
XI	–	–	–	–	6,8	0,6	15,0	7	-9,9	21	2,2	5,6	3,2	3,6	–	–	–	–	–	–	–	–	–	–	–	–	8,8	8,2	8,2	8,4
XII	–	–	–	–	-1,3	-8,9	9,8	5	-36,8	25	-5,3	-2,6	-4,8	-4,4	–	–	–	–	–	–	–	–	–	–	–	–	8,7	8,7	8,2	8,5
Rok	–	–	–	–	11,1	–	29,9	10.VIII	-36,8	25.XII	4,1	9,8	4,5	5,7	–	–	–	–	–	–	–	–	–	–	–	–	6,8	6,5	5,9	6,4

Dolina Pięciu Stawów — $H_s = 1668\,m$ — $h_w = 13{,}6\,m$ — 1961

MIESIĄC	ROZKŁAD WIATRU [%D, ¹/mD] N n	N v	NE n	NE v	E n	E v	SE n	SE v	S n	S v	SW n	SW v	W n	W v	NW n	NW v	C n	Średnia prędkość	OPAD R Suma	Max	Data	LICZBA DNI (n) Temperatura T Min < -10°	Max < 0°	Min < 0°	Max > 25°	Wiatr v ≥ 10	v ≥ 15	●	●	Opad R ≥ 0,1	≥ 1,0	≥ 10,0	≡	▤	▽R
I	·	·	·	·	10	3,6	·	·	12	9,0	18	9,9	10	8,4		·	43	4,4	44,2	11,5	2	15	25	31	·	8	5	9	9	12	9	2	4	31	-
II	3	1,9	·	·	10	2,5	·	·	14	2,7	6	4,5	12	5,1	·	·	39	1,9	68,4	15,8	6	6	12	28	·	2	·	9	8	15	12	3	4	28	-
III	3	5,3	·	·	9	3,8	2	3,5	16	7,4	8	10,8	31	7,0	2	6,5	22	5,3	74,5	17,5	21	9	13	29	·	10	5	3	18	18	12	2	7	31	-
IV	1	3,0	·	·	14	3,0	·	·	11	3,4	7	6,3	32	4,3		·	25	2,9	40,6	13,2	8	·		17	·	4	1	7	5	9	6	2	3	30	-
V	17	2,9	3	3,0	2	4,5	·	·	11	3,1	3	3,3	4	5,0		·	53	1,4	165,8	33,4	17	·	3	13	·	·	·	·	16	19	18	6	5	21	-
VI	1	4,0	·	·	10	2,1	·	·	5	2,2	10	7,5	18	3,1		·	46	1,9	194,3	40,1	27	·	·	·	·	2	·	3	8	17	16	7	4	·	-
VII	18	4,2	1	3,0	7	4,4	·	·	2	7,0	9	8,7	28	4,2		·	28	3,5	189,8	32,0	30	·	·		·	3	1	5	11	18	16	8	6		-
VIII	12	3,0	·	·	8	2,1	·	·	3	2,7	11	3,0	30	4,0	·	·	29	2,3	120,3	32,1	18	·	·	1	·	1	·	6	7	14	13	5	4	·	-
IX	12	3,0	·	·	21	4,1	·	·	16	3,6	2	3,5	29	4,4	·	·	10	3,5	34,5	10,3	14	·	·	·	·	·	·	13	3	10	8	1	1	·	-
X	3	2,7	·	·	10	2,9	·	·	17	3,6	12	9,5	43	6,1	·	·	8	5,1	153,1	49,3	18	·	·	6	·	5	3	5	7	12	11	5	1	1	-
XI	6	2,8	1	6,0	9	3,4	·	·	31	4,1	15	3,9	22	3,6	·	·	6	3,5	160,7	47,2	4	2	4	25	·	·	·	1	18	17	14	3	9	30	-
XII	3	2,0	2	2,0	7	5,0	·	·	32	4,2	10	2,9	33	3,3	·	·	8	3,4	77,7	15,2	11	15	21	30	·	1	·	·	15	12	11	3	4	31	-
Rok	79	2,9	7	1,2	117	3,4	2	0,3	170	4,4	111	6,2	292	4,9	2	0,5	315	3,3	1323,8	49,3	18.X	47	78	180	·	36	15	61	125	173	146	47	52	203	-

Morskie Oko — $H_s = 1400\,m$ — $h_w = 14\,m$

I	12,5	2,2	2,5	3,0	2	3,0	4	6,8	8	8,4	13	8,6	7	6,0	1	3,0	43	3,1	58,2	32,4	4	20	22	31	·	7	2	-	-	11	5	2	1	3,1	-
II	1,5	2,9	3	2,3	1	3,0	2	11,0	12,5	3,0	4,5	6,2	4	7,0	1	2,0	41	2,0	68,0	20,5	9	9	11	28	·	4	·	-	-	15	10	1	2	28	·
III	1,9	3,5	1,7	5,9	3	9,3	10	8,8	9	4,6	5	8,6	7	5,7	·	·	23	4,4	109,3	21,8	14	3	6	27	·	9	2	-	-	24	17	2	1	3,1	
IV	1,9	3,2	6	6,5	4	9,5	8	5,5	2,5	4,4	10,5	7,3	9	3,6	1	3,0	30	3,4	54,4	12,6	2	·	·	12	·	6	1	-	-	13	11	2	1	1,5	·
V	18,5	2,5	8,5	2,4	6	3,7	6	3,8	2,5	6,4	8,5	4,8	1	2,0	·	·	42	1,8	140,3	30,9	6	·	1	10	·	2	·	-	-	24	15	4	3	8	2
VI	1,4	3,2	7	2,9	5	2,8	5	4,8	3,5	4,9	7	3,9	3,5	2,6	4	6,5	41	2,0	138,8	26,3	27	·	·	·	·	3	1	-	-	17	14	4	1	·	8
VII	17,5	2,5	8	2,1	9	5,0	3	6,0	1,2	4,8	5	6,2	8	4,9	3,5	2,4	27	2,8	171,9	37,5	30	·	·	·	·	2	1	-	-	21	17	5	3	·	4
VIII	1,4	2,8	6	3,2	4	2,2	3	3,7	1,6	5,3	11	4,5	5	2,8	1	3,0	33	2,5	63,0	17,3	12	·	·	·	·	3	2	-	-	14	12	2	2	·	1
IX	24,5	2,3	3,5	3,3	6	3,7	5	2,4	8	3,2	3	7,3	6	4,0	·	·	34	1,9	44,5	12,8	6	·	·	·	·	3	·	-	-	12	6	1	2	·	2
X	1,1	5,1	3,5	3,4	2,5	8,4	9,5	7,5	17,5	7,3	10	5,2	7	7,7	1	5,0	31	4,3	191,4	79,9	18	·	·	4	·	11	4	-	-	13	12	3	3	1	·
XI	9	1,8	5	2,8	3	5,7	1,5	2,0	3	3,7	11,5	7,6	17	5,1	1	4,0	39	2,7	207,9	42,0	4	1	5	23	·	6	·	-	-	20	15	7	3	14	·
XII	1,7	5,4	1	8,0	2	5,0	2	6,0	1,0	7,2	16	9,5	6	6,2	·	·	39	4,1	115,0	34,7	11	19	17	25	·	7	3	-	-	21	12	3	3	2,5	·
Rok	1,9,1	3,1	7,1	3,8	47,5	5,1	5,9	5,7	104,5	5,3	10,5	6,6	80,5	4,8	13,5	2,4	423	2,9	1360,7	79,9	18.X	52	62	180	·	63	16	-	-	205	146	36	25	153	20

Ustrzyki Górne — $H_s = 650\,m$ — $h_w = 20\,m$

I	8	7,8	7,5	3,7	10,5	4,4	·	·	3,8	6,0	10	10,9	·		1	5,0	18	5,1	40,2	18,0	5	-	2,4	-	·	9	6	5	14	13	10	1	·	2,6	-
II	7	3,0	2	2,0	7	3,7	·	·	4,3	4,4	10,5	3,2	0,5	3,0	·	·	14	3,3	26,1	4,7	8	4	12	26	·	1	·	·	17	10	8	·	·	2,8	-
III	1,4	4,3	11	3,1	5	2,8	3	2,7	26,5	6,9	16	5,7	1,5	3,0	5	5,6	11	4,5	82,9	15,9	31	1	1	22	·	4	2	2	18	20	15	2	·	1,4	-
IV	1,4	3,2	16	3,8	·	·	1	3,0	2,5	7,1	10	5,4	1	12,0	1	2,0	22	3,9	32,2	8,3	30	·	·	1,4	·	10	3	6	4	10	9	·	·	·	-
V	7	5,6	1,9	2,5	·	·	1	3,0	2,6	4,0	4	5,5	·	·	·	·	36	2,3	60,9	10,9	8	·	·	6	·	4	·	·	10	14	11	1	3	·	-
VI	1,0	4,4	10	4,4	1	2,0	1	1,0	2,1	4,1	9	6,3	1	4,0	·	·	37	2,7	107,1	20,7	14	·	·	·	2	2	·	2	7	17	17	4	4	·	-
VII	4	4,5	1,5	3,7	1	3,0	1	8,0	2,8	4,9	5	6,0	2	3,0	·	·	37	2,8	123,2	47,3	29	·	·	·	4	5	·	2	9	11	9	4	·	·	-
VIII	9	3,7	1,5	2,9	2	2,5	1	4,0	1,9,5	5,1	9,5	3,6	1	3,0	·	·	3,8	2,4	35,6	10,3	16	·	·	·	6	2	·	7	5	11	8	1	2	·	-
IX	8	4,4	1,0	3,2	·	·	3	6,0	2,3	5,1	5	4,6	·	·	·	·	41	2,5	16,1	5,1	7	·	·	5	2	4	·	11	5	7	5	·	2	·	-
X	1,0	4,4	9	4,2	1	3,0	5	6,0	3,1	4,9	8	3,5	·	·	·	·	29	3,2	34,2	13,4	30	·	·	1,5	2	2	·	9	4	6	4	1	2	·	-
XI	2,5	1,8	11,5	4,0	·	·	1,5	2,7	3,9	5,6	8,5	4,5	1	2,0	1	1,0	25	3,5	74,0	27,1	27	·	2	10	·	5	·	1	21	18	13	2	6	7	-
XII	2,2	6,4	6	5,3	1	2,0	·	·	4,0	6,1	4	6,8	·	·	·	·	20	4,8	97,4	16,1	11	12	19	24	·	7	2	·	22	22	16	4	·	2,5	-
Rok	1,1,5,5	4,5	13,2	3,6	28,5	2,0	17,5	3,0	3,6,0	5,4	99,5	5,5	8	2,5	8	1,1	326	3,4	729,9	47,3	29.VII	-	5,8	-	16	55	13	45	136	159	125	20	19	100	-

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TABLICA III

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

DATES LIMITES DU GEL

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Aleksandrowice	10.IV	4.XI	207
Antołówka	13.V	16.X	155
Augustów	21.IV	13.XI	205
Babia Góra	13.V	4.XI	174
Baligród	24.IV	21.IX	149
Bartoszyce	30.IV	23.IX	145
Barwinek	24.V	22.IX	120
Bełsk	19.V	22.IX	125
Biała Podlaska	21.IV	23.IX	154
Białowieża	21.IV	22.IX	153
Biały Kościół	10.IV	5.XI	208
Białystok	21.IV	23.IX	154
Biebrza	15.V	22.IX	129
Biecz	21.IV	22.IX	153
Bielsk Podlaski	21.IV	23.IX	154
Bieruń Stary	13.IV	25.X	194
Bierutowice	13.V	4.XI	174
Biłgoraj	17.V	15.XI	181
Bircza	17.V	22.IX	127
Biskupiec	21.IV	12.XI	205
Bochnia-Chodenice	22.IV	22.IX	152
Bodzentyn	21.IV	22.IX	153
Borusowa	10.IV	15.XI	218
Brwinów	12.IV	14.XI	215
Brzegi Dolne	24.V	20.IX	118
Brzezna	21.IV	22.IX	153
Bukowina Tatrz.	12.V	4.XI	175
Busko-Zdrój	10.IV	15.XI	218
Bydgoszcz	21.IV	14.XI	206
Bydgoszcz, IMiUZ	11.IV	14.XI	216
Bystrzyca Kłodzka	15.V	22.IX	129
Bytom	29.III	15.XI	230
Chełm Lubelski	11.IV	23.IX	164
Chodzież	21.IV	14.XI	206
Chojnice	21.IV	5.XI	197
Chorzelów	21.IV	22.IX	153
Ciechocinek	12.IV	13.XI	214
Cieplice Śl. - Zdrój	21.IV	11.X	172
Cieszyn	10.IV	9.XI	212
Cieszyn-Bobrek	21.IV	23.IX	154
Ciężkowice	21.IV	22.IX	153
Czarna Dąbrówka	13.V	5.XI	175
Czarniecka Góra	21.IV	22.IX	153
Czarny Dunajec	15.V	22.IX	129
Czernichów	10.IV	25.X	197
Częstochowa	10.IV	5.XI	208
Czorsztyn	13.V	22.IX	131
Czorsztyn - Nadzamcze	15.V	22.IX	129

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Darłowo	21.IV	22.XI	214
Dębica	10.IV	23.IX	165
Dobrogoszcz	10.IV	19.XI	222
Dolina Chochołowska	20.V	12.IX	114
Dolina Pięciu Stawów	23.V	18.VIII	86
Drawno	11.IV	5.XI	207
Duszniki - Zdrój	10.IV	5.XI	208
Dynów	22.IV	22.IX	152
Dziwnów	4.IV	21.XI	230
Elbląg	12.IV	13.XI	214
Felin	10.IV	14.XI	217
Garlica Murowana	10.IV	15.XI	218
Gdańsk - Nowy Port	12.IV	22.XI	223
Gdańsk - Siedlce	12.IV	22.XI	223
Gdańsk - Wrzeszcz	12.IV	19.XI	220
Gdynia	12.IV	23.XI	224
Giżycko	21.IV	13.XI	205
Gliwice	10.IV	20.XI	223
Głodowo	12.IV	13.XI	214
Głogów	10.IV	19.XI	222
Głubczyce	26.IV	23.IX	149
Głuchołazy - Zdrój	10.IV	15.XI	218
Gniezno	12.IV	14.XI	215
Goczałkowice	10.IV	5.XI	208
Gołdap	23.V	23.X	152
Gorzów Wlkp.	1.IV	5.XI	217
Gorzyń	11.IV	5.XI	207
Goszyce	10.IV	24.X	196
Góra Św.Anny	1.IV	5.XI	217
Grabowiec	-	23.IX	-
Grabownica	21.IV	24.IX	155
Grodków	10.IV	20.XI	223
Grudziądz	12.IV	14.XI	215
Gryfice	21.IV	5.XI	197
Gubałówka	13.V	4.XI	174
Hala Gąsienicowa	19.V	14.X	147
Hala Ornak	Temperatura spadała poniżej 0° we wszystkich miesiącach roku		
Hel	2.V	23.XI	204
Hopowo	2.V	13.XI	194
Horyniec	19.V	22.IX	125
Inowrocław	10.IV	14.XI	217
Istebna - Kubalonka	10.IV	4.XI	207
Istebna - Stecówka	10.IV	4.XI	207
Istebna - Zaolzie	24.V	12.IX	110
Iwonicz - Zdrój	21.IV	15.XI	207

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Jabłonka	15.V	21.IX	128
Jabubowice	10.IV	5.XI	208
Janów Lubelski	10.IV	15.XI	218
Jarosław	13.IV	23.IX	162
Jasło	21.IV	22.IX	153
Jastrzębie - Zdrój	10.IV	9.XI	212
Jaworzyna Krynicka	12.V	-	-
Jelenia Góra	20.IV	23.IX	155
Jazy	23.V	22.IX	121
Jeziory	10.IV	14.XI	217
Kalisz	10.IV	14.XI	217
Kamienica	15.V	21.IX	128
Kamienica Królewska	12.IV	5.XI	206
Kamień Krajeński	13.V	5.XI	175
Karpacz	10.IV	4.XI	209
Kartuzy	12.IV	13.XI	214
Kasprowy Wierch	Temperatura spadała poniżej 0° we wszystkich miesiącach roku		
Katowice	12.IV	9.XI	210
Kętrzyn	21.IV	13.XI	205
Kielce	12.IV	14.XI	215
Kisielnica	22.IV	13.XI	204
Klimczok	13.V	-	-
Kłodzko	21.IV	22.IX	153
Kobylec	12.IV	14.XI	215
Kolbuszowa	21.IV	22.IX	153
Kolno	21.IV	13.XI	205
Koło	10.IV	14.XI	217
Kołobrzeg	12.IV	21.XI	222
Kołobrzeg - Wydma	11.IV	21.XI	223
Kołuda Wielka	4.IV	14.XI	223
Komańcza	24.V	21.IX	119
Kończewice	20.IV	13.XI	206
Kopna Góra	23.V	22.IX	121
Korfantów	-	20.XI	-
Koszalin	12.IV	5.XI	206
Kościerzyna	21.IV	5.XI	197
Kórnik	10.IV	19.XI	222
Kraków - Chełm	10.IV	25.X	197
Kraków - Czyżyny	10.IV	22.X	194
Kraków - Nowa Huta	10.IV	22.X	194
Kraków, Obs.Astr.UJ	10.IV	20.XI	223
Krasnystaw	21.IV	22.IX	153
Krasnik Dolny	22.III?	9.XI	231?
Krosno	13.IV	22.IX	161
Krościenko	15.V	22.IX	129
Krynica	13.V	23.IX	132
Krynica - Góra Parkowa	21.IV	5.XI	197
Krynica Moraka	11.IV	14.XI	216
Krzemień	12.IV	13.XI	214

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Krzyż	12.IV	24.IX	164
Kudowa - Zdrój	10.IV	19.XI	222
Kuźnice	15.V	2.X	139
Kwidzyń	-	14.XI	-
Laskowice Oławskie	10.IV	19.XI	222
Lądek - Zdrój	21.IV	5.XI	197
Legionowo	21.IV	14.XI	206
Legnica	10.IV	9.XI	212
Lesko	22.IV	22.IX	152
Leskowiec	12.V	4.XI	175
Leszno - Strzyżewice	1.IV	16.XI	228
Leżajsk	13.IV	23.IX	162
Lębork	13.V	5.XI	175
Libertów	10.IV	5.XI	208
Lidzbark	22.IV	13.XI	204
Lidzbark Warmiński	30.IV	13.XI	196
Limanowa	15.V	22.IX	129
Lipki	11.IV	5.XI	207
Lipowa	10.IV	22.IX	164
Lubaczów	17.V	22.IX	127
Lublin	21.IV	23.IX	154
Lubliniec	10.IV	-	-
Luboń Wielki	15.V	4.XI	172
Łagiewniki	11.IV	14.XI	216
Łącko	24.IV	22.IX	150
Łeba	2.V	22.XI	203
Łosice	21.IV	13.XI	205
Łowicz - Blich	12.IV	5.XI	206
Łódź - Lublinek	10.IV	14.XI	217
Łódź - Ruda Pabianicka	10.IV	14.XI	217
Łysa Polana	18.V	22.IX	126
Maków Podhalański	10.IV	23.IX	165
Malbork	21.IV	13.XI	205
Maniowy	15.V	22.IX	129
Miastko	13.V	5.XI	175
Miechów	13.IV	24.X	193
Mielec	21.IV	22.IX	153
Międzybrodzie	29.III	20.XI	235
Międzyzdroje	10.IV	21.XI	224
Mikołajki	20.IV	13.XI	206
Mława	21.IV	13.XI	205
Młochów	21.IV	14.XI	206
Morskie Oko	19.V	2.X	135
Motycz	21.IV	22.IX	153
Mszana Dolna	22.IV	22.IX	152
Muszyna	19.V	22.IX	125
Myczkowce	23.IV	22.IX	151

STACJA	Temperatura spadła poniżej 0°		Okres bez przymrozków (dni)
	po raz ostatni	po raz pierwszy	
Myślenice	10.IV	4.XI	207
Myślenickie Turnie	18.V	14.X	148
Nałęczów	19.V	21.IX	124
Namysłów	10.IV	19.XI	222
Nidzica	23.V	13.XI	173
Niepokalanów	21.IV	14.XI	206
Nisko	12.IV	22.IX	162
Nowa Wieś	21.IV	23.IX	154
Nowe Miasto n.P.	21.IV	23.IX	154
Nowogard	11.IV	5.XI	207
Nowy Dwór Gdański	21.IV	14.XI	206
Nowy Dwór Mazowiecki	10.IV	-	-
Nowy Sącz	21.IV	22.IX	153
Nowy Targ	13.V	21.IX	130
Nur	21.IV	23.IX	154
Obidowa	12.V	4.XI	175
Oborniki Śląskie	10.IV	15.XI	218
Ochaby	10.IV	5.XI	208
Olecko	30.IV	13.XI	196
Olesno	10.IV	5.XI	208
Olkusz	10.IV	9.XI	212
Olsztyn - Dajtki	19.V	13.XI	177
Oława	10.IV	19.XI	222
Opole	10.IV	19.XI	222
Opole Lubelskie	12.IV	22.IX	162
Orneta	-	5.XI	-
Osiny	21.IV	14.XI	206
Osowiec	21.IV	23.IX	154
Ostrołęka	21.IV	13.XI	205
Ostroszowice	10.IV	14.XI	217
Ostrowy	12.IV	13.XI	214
Ostróda	21.IV	13.XI	205
Ostrów Wlkp.	10.IV	-	-
Ostrzeszów	10.IV	14.XI	217
Otmuchów	20.IV	23.IX	155
Ożańsk	1.IV	23.IX	174
Paproć	10.IV	13.X	185
Pętkowo	10.IV	19.XI	222
Pilsko	17.V	4.XI	170
Piotrków Trybunalski	10.IV	14.XI	217
Pisz	21.IV	22.IX	153
Piwniczna	13.V	22.IX	131
Płock - Radziwie	12.IV	14.XI	215
Płocko	13.V	5.XI	175
Polanica - Zdrój	21.IV	15.XI	207
Połczyn - Zdrój	21.IV	24.IX	155
Poraj	18.V	23.IX	127
Porąbka	10.IV	20.XI	223
Poronin	7.VII	12.IX	66
Poświętne	21.IV	28.IX	159
Poznań - Ławica	10.IV	19.XI	222
Poznań - Sołacz	10.IV	19.XI	222
Prabuty	21.IV	5.XI	197
Prudnik	10.IV	15.XI	218
Przasnysz	21.IV	13.XI	205
Przebędowo	11.IV	14.XI	216
Przedbórz	21.IV	22.IX	153
Przehyba	12.V	6.XI	177
Przelewice	12.IV	5.XI	206
Przemyśl	13.IV	23.IX	162
Przybroda	11.IV	19.XI	221
Pszczela Wola	21.IV	22.IX	153
Pszczyna	10.IV	9.XI	212
Ptaszkowa	21.IV	5.XI	197
Ptusza	13.V	-	-
Puck	11.IV	23.XI	225
Puczniew	12.IV	14.XI	215
Puławy	12.IV	14.XI	215
Pułtusk	21.IV	13.XI	205
Raba Wyżna	21.IV	5.XI	197
Rabka	21.IV	22.IX	153
Racibórz	10.IV	5.XI	208
Radom	12.IV	14.XI	215
Radostowo	21.IV	14.XI	206
Radzyń Podlaski	21.IV	22.IX	153
Reguły	12.IV	14.XI	215
Resko	12.IV	5.XI	206
Rosnowo	12.IV	5.XI	206
Rozewie	12.IV	22.XI	223
Rożnów	10.IV	5.XI	208
Różanystok	21.IV	23.X	184
Rybnik	10.IV	19.XI	222
Rymanów - Zdrój	20.V	22.IX	124
Rzeszów - Jasionka	21.IV	22.IX	153
Sandomierz	10.IV	15.XI	218
Sanok	24.IV	22.IX	150
Sejny	23.V	22.IX	121
Siedlce	21.IV	22.IX	153
Siejnik	30.IV	13.XI	196
Sielec	13.IV	22.IX	161
Siemianice	12.IV	14.XI	215
Siemiatycze	12.IV	13.XI	214
Sieniawa	15.V	22.IX	129
Sieradz	12.IV	14.XI	215
Silniczka	-	23.IX	-

DATY OSTATNIEGO I PIERWSZEGO PRZYMROZKU

STACJA	Temperatura spadła poniżej 0° po raz ostatni	Temperatura spadła poniżej 0° po raz pierwszy	Okres bez przymrozków (dni)
Sinołęka	21.IV	13.XI	205
Skierniewice	12.IV	14.XI	215
Skroniów	21.IV	14.XI	206
Słubice	1.IV	24.IX	175
Słupca	10.IV	16.XI	219
Słupia Nowa	10.IV	14.XI	217
Słupsk	12.IV	5.XI	206
Smolice	10.IV	19.XI	222
Sobieszyn	10.IV	14.XI	217
Sobótka	29.III	20.XI	235
Sokołowsko	13.V	22.IX	131
Sokółka	30.IV	23.X	175
Stańcowa	15.V	4.XI	172
Stare Pole	21.IV	13.XI	205
Stary Sącz	21.IV	22.IX	153
Staszów	13.V	23.IX	132
Strzelna	19.V	14.XI	178
Strzyżów	21.IV	22.IX	153
Suchedniów	19.V	21.IX	124
Sulejów	19.V	22.IX	125
Sulęcin	1.IV	-	-
Suwałki	30.IV	23.X	175
Szamotuły	10.IV	18.XI	221
Szczawnica	13.V	22.IX	131
Szczawno-Zdrój	10.IV	14.XI	217
Szczecin - Dąbie	12.IV	5.XI	206
Szczecin - Niebuszewo	1.IV	5.XI	217
Szczecinek	2.V	5.XI	186
Szczerców	12.IV	15.XI	216
Szczuczyn	30.IV	23.IX	145
Szczytno	19.V	22.IX	125
Szepietowo	21.IV	23.X	184
Szklarska Poręba	26.IV	-	-
Szprotawa	1.IV	5.XI	217
Szrenica	18.V	18.X	152
Śliwice	21.IV	13.XI	205
Śnieżka	6.VII	13.X	98
Śrem	10.IV	16.XI	219
Świbno	12.IV	21.XI	222
Świder	12.IV	14.XI	215
Świdnica	1.IV	15.XI	227
Świdwin	12.IV	5.XI	206
Świebodzin	1.IV	19.XI	231
Świeradów-Zdrój	1.IV	5.XI	217
Świerklaniec	12.IV	15.XI	216
Święty Krzyż	10.IV	5.XI	208
Świnoujście	11.IV	20.XI	222
Tarnobrzeg	10.IV	15.XI	218
Tarnogród	10.IV	23.IX	165
Tarnów	10.IV	23.IX	165
Tczew	11.IV	14.XI	216
Terespol	12.IV	23.IX	163
Tęgoborze	10.IV	20.XI	223
Tolkmicko	21.IV	13.XI	205
Tomaszów Lubelski	17.V	22.IX	127
Topola - Błonie	21.IV	14.XI	206
Toruń - Wrzosy	21.IV	5.XI	197
Trzciańsko - Zdrój	1.IV	5.XI	217
Trzebiechów	-	5.XI	-
Trzebież	1.IV	5.XI	217
Trzebinia	10.IV	15.XI	218
Trzemeszno	1.IV	14.XI	226
Turbacz	18.V	4.XI	169
Tychy	10.IV	25.X	197
Ustka	12.IV	22.XI	223
Ustka - Wydma	12.IV	22.XI	223
Ustrzyki Górne	24.V	21.IX	119
Wadowice	10.IV	9.XI	212
Wałcz	12.IV	5.XI	206
Warka	21.IV	23.IX	154
Warszawa - Bielany	12.IV	14.XI	215
Warszawa, Inst.Geogr.UW	1.IV	14.XI	226
Warszawa, Obs.Astr.UW	11.IV	14.XI	216
Warszawa-Okęcie	10.IV	14.XI	217
Warszawa,St.Pomp Rzecz.	11.IV	14.XI	216
Wądołki Borowe	21.IV	24.IX	155
Werbkowice	21.IV	22.IX	153
Wielichowo	10.IV	13.X	185
Wieliczka	22.IV	22.X	182
Wieliszew	10.IV	13.XI	216
Wieluń	21.IV	5.XI	197
Wieniec-Zdrój	12.IV	14.XI	215
Wierzchowo	13.V	27.IX	136
Więcławice	12.IV	14.XI	215
Wińsko	10.IV	14.XI	217
Wirty	2.V	14.XI	195
Wisła	21.IV	5.XI	197
Wisznice	21.IV	22.IX	153
Witów	15.V	23.IX	130
Włodawa I	21.IV	22.IX	153
Włodawa II	21.IV	-	-
Wojcieszów Górny	10.IV	14.XI	217
Wolbrom	2.V	24.IX	144
Wrocław - Gądów Mały	10.IV	19.XI	222
Wyrzysk	12.IV	14.XI	215
Wysowa	20.V	21.IX	123
Wyszków	12.IV	13.XI	214
Zakopane	15.V	22.IX	129
Zakrzów	10.IV	23.IX	165
Zawołocze	21.IV	22.IX	153
Zamość	12.IV	22.IX	162
Zawiercie	11.IV	5.XI	207
Zawodzie	21.IV	23.IX	154
Zawoja	13.V	4.XI	174
Ząbkowice	15.V	15.XI	183
Zbąszyń	10.IV	19.XI	222
Zdanów	10.IV	14.XI	217
Zgorzelec	1.IV	15.XI	227
Zielona Góra	1.IV	5.XI	217
Zwardoń	13.V	4.XI	174
Żarnowa	13.IV	15.XI	215
Żary	1.IV	5.XI	217
Żegiestów-Zdrój	13.V	22.IX	131
Żelechów	21.IV	22.IX	153
Żelisławki	21.IV	13.XI	205
Żywiec-Sporysz	10.IV	23.IX	165

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TABLICA IV

USŁONECZNIENIE (w godzinach)

INSOLATION (en heures)

USŁONECZNIENIE /w godzinach/ STYCZEŃ - JANVIER 1961

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	.	.	.	.	1,8	1,7	0,3	.	.	0,8	.	0,3	.	.	.	2,6	6,1	6,8	6,1	6,8	5,9	6,3	5,9	0,8	3,4	.	6,2	.	0,3	.	0,1	62,2
2	Kołobrzeg	.	0,6	.	.	.	1,5	1,5	.	.	0,5	.	2,2	.	.	.	0,3	7,1	7,0	7,2	7,0	6,9	6,4	6,9	3,0	6,9	0,4	6,7	.	0,6	.	.	72,7
3	Międzyzdroje	.	1,3	.	.	.	0,7	2,2	.	.	0,5	0,4	2,6	.	.	.	.	7,6	7,4	.	6,7	5,7	3,2	7,1	0,8	7,1	7,6	6,5	.	.	.	.	67,4
4	Resko	.	1,3	.	.	.	1,5	1,8	.	.	0,5	.	4,0	.	.	.	.	5,7	6,7	6,8	6,7	6,7	6,9	6,9	3,8	6,3	6,6	6,5	.	0,6	.	.	79,3
5	Szczecinek	.	.	.	.	1,2	3,1	1,8	.	0,1	.	.	0,2	.	.	.	.	5,9	4,1	6,1	5,9	4,8	4,3	6,1	2,9	5,8	2,8	6,3	0,2	0,4	.	.	62,0
6	Chojnice	.	.	.	.	0,3	3,0	0,6	.	.	.	.	.	.	.	.	0,8	6,6	5,8	2,1	7,0	4,6	6,1	7,2	0,9	5,0	4,0	7,6	1,0	0,6	.	.	63,2
7	Hel	.	.	.	.	.	2,2	.	0,2	.	1,6	.	0,1	.	.	.	1,6	3,0	4,5	3,2	6,3	1,9	0,8	3,9	.	3,9	4,9	4,2	.	1,6	.	0,3	44,2
8	Gdynia	.	0,1	.	0,1	0,1	3,9	0,1	1,3	0,2	3,7	.	0,6	.	.	.	2,4	1,8	5,1	3,0	6,8	1,5	2,3	2,6	.	2,9	4,9	5,7	0,3	2,2	.	1,6	53,2
9	Świbno-Ujście Wisły	0,1	.	.	.	.	2,5	0,1	.	.	1,1	.	.	.	.	.	1,5	3,2	5,1	3,1	6,4	2,3	1,3	3,7	1,1	6,4	3,0	6,8	0,5	1,5	.	0,2	49,9
10	Stare Pole	.	.	.	.	.	3,3	0,1	.	.	1,4	.	.	.	.	.	1,8	6,8	4,5	.	6,3	0,9	3,8	6,8	1,5	4,2	1,9	7,3	2,8	1,4	.	.	54,8
11	Radostowo	.	.	.	.	.	4,6	.	0,2	.	1,1	.	3,2	.	.	.	1,6	6,0	6,7	.	6,0	1,9	4,7	7,2	1,8	5,2	1,2	7,5	2,4	0,8	.	.	62,1
12	Prabuty	.	.	.	.	.	.	.	.	.	.	.	0,6	.	.	.	0,6	6,5	5,3	.	6,1	0,8	4,4	7,2	1,6	4,4	2,2	7,1	3,6	0,3	.	.	50,7
13	Bydgoszcz, IMiUZ	.	.	.	0,5	.	4,7	0,5	.	0,4	1,0	.	0,8	.	.	.	.	7,2	6,2	.	4,8	0,4	5,4	6,9	3,1	4,5	5,0	6,9	2,0	1,2	.	.	61,5
14	Suwałki	.	.	.	1,8	.	0,5	1,2	.	.	0,8	.	.	0,9	.	.	1,4	5,4	5,6	.	0,3	2,1	.	1,8	4,4	6,9	1,0	.	5,2	2,1	.	.	41,4
15	Mikołajki	.	.	.	.	.	0,2	0,2	.	.	.	.	.	2,2	.	1,6	0,9	7,3	6,0	.	2,4	4,3	.	2,7	2,7	7,7	3,6	0,3	5,4	1,2	.	.	48,7
16	Biebrza	0,2	.	.	2,2	0,5	.	0,7	.	.	.	.	.	1,1	.	1,0	0,9	5,9	6,3	.	.	2,8	.	1,6	2,8	3,3	3,2	.	6,1	2,2	.	.	40,8
17	Białystok	.	.	.	2,2	.	.	0,5	.	.	.	.	.	0,7	.	0,8	0,1	5,1	3,1	.	.	0,2	.	4,7	.	6,2	5,0	.	6,1	3,0	.	.	37,7
18	Gorzów Wlkp.	0,5	.	.	.	1,0	1,0	0,6	.	1,0	2,6	.	1,9	.	.	.	.	6,9	7,2	6,9	6,4	4,0	.	6,0	4,5	7,1	7,0	6,9	1,0	4,1	.	.	76,6
19	Przebędowo	.	.	0,5	0,6	0,6	4,5	1,9	.	0,3	3,6	.	.	.	.	.	.	6,8	5,7	7,3	7,6	6,2	4,5	4,6	4,5	6,6	5,2	7,1	2,4	3,5	.	.	84,0
20	Przybroda	.	.	.	.	0,9	3,9	1,7	.	0,7	4,1	.	2,1	.	.	.	.	6,1	7,1	7,2	7,1	5,6	4,2	5,8	4,4	5,9	7,4	6,3	3,3	4,4	.	.	88,2
21	Poznań-Ławica	.	.	.	0,5	1,2	4,5	1,6	.	0,8	4,1	.	2,6	.	.	.	.	.	6,5	6,9	6,1	5,8	4,6	5,6	4,5	7,0	5,9	7,1	4,7	4,3	.	.	84,3
22	Plewiska	.	.	.	0,3	0,8	4,1	1,4	0,5	.	4,1	.	2,2	.	.	.	.	6,0	2,6	6,8	6,6	5,4	3,7	4,7	2,9	4,9	7,0	4,8	4,0	4,3	.	.	77,1
23	Kórnik	0,1	.	.	0,3	0,6	4,3	0,6	.	0,8	4,0	.	2,8	.	.	.	.	4,6	6,2	7,7	7,2	6,2	4,7	5,3	7,6	7,3	7,5	8,0	4,7	3,8	.	.	94,3
24	Oborniki Śl.	3,6	4,7	1,6	1,8	.	0,3	3,3	.	2,2	4,0	.	0,3	.	.	.	.	5,6	4,5	5,4	5,3	2,7	1,4	.	2,6	3,2	5,0	5,3	6,5	.	.	.	69,3
25	Laskowice Oławskie	0,8	0,5	0,1	0,7	2,5	5,6	1,4	0,9	3,0	4,8	0,9	2,5	2,8	.	.	.	6,8	7,4	6,5	6,9	5,0	4,9	.	4,9	1,2	7,9	7,1	7,3	4,0	.	.	96,4
26	Ciechocinek	.	.	.	.	.	2,5	0,1	.	.	.	.	3,0	.	.	.	.	7,1	4,8	.	5,3	1,9	3,7	6,5	2,3	5,8	5,1	6,3	3,6	0,9	.	.	58,9
27	Więcławice	.	.	.	.	.	4,7	0,2	0,1	.	0,8	.	2,0	.	.	.	.	6,0	6,2	0,7	7,2	0,2	3,0	5,5	3,2	6,4	5,9	6,3	4,1	1,7	.	.	64,2
28	Legionowo	.	.	.	.	.	2,1	0,1	.	0,1	.	1,1	.	3,8	.	.	.	6,3	7,0	.	.	5,5	0,4	4,5	0,2	6,8	4,8	2,7	6,2	0,5	.	.	52,1
29	Warszawa-Bielany	.	.	0,2	.	.	1,1	0,3	.	.	.	1,4	.	3,7	.	.	.	5,7	5,8	.	.	4,3	1,2	2,5	.	5,7	5,8	3,6	6,0	0,2	0,3	.	47,8
30	Warszawa, Min. Kom.	.	.	.	.	.	1,5	.	0,6	.	.	.	.	3,4	.	.	.	5,8	5,8	.	.	4,7	1,3	1,5	.	5,1	1,6	2,6	5,6	.	.	.	39,5
31	Międzylesie	.	.	0,4	.	.	2,3	2,2	.	0,1	.	3,5	.	3,4	.	.	0,1	6,2	6,4	.	0,6	5,9	.	2,6	0,1	6,4	2,8	2,1	6,6	.	0,1	.	57,8
32	Brwinów	.	.	0,2	.	.	3,2	0,3	.	.	.	1,9	.	3,6	.	.	.	6,2	7,2	.	.	7,0	1,8	1,8	.	6,7	6,4	7,7	6,8	0,4	0,2	.	61,4
33	Świder	.	.	0,9	.	.	1,8	0,3	.	.	.	2,9	.	3,8	.	.	.	5,4	5,2	.	0,1	5,3	2,1	2,3	.	4,6	6,1	0,8	6,1	.	.	.	47,7
34	Topola-Błonie	.	.	1,0	.	.	5,0	.	0,3	0,4	1,2	0,1	1,1	2,0	.	.	.	7,0	4,5	.	6,3	4,3	3,1	1,9	2,4	6,0	4,6	7,0	6,0	1,2	.	.	65,4
35	Mochów	.	.	0,3	.	.	2,9	0,2	0,1	.	.	2,7	.	3,4	.	.	.	5,9	6,4	.	.	6,3	2,7	1,3	0,7	6,0	7,3	7,6	6,4	0,1	0,1	.	60,4
36	Skierniewice	.	.	0,4	.	.	3,9	0,8	0,3	0,6	1,9	0,4	.	3,3	.	.	.	7,4	5,9	.	1,3	7,3	1,0	0,7	1,1	6,1	3,3	5,3	6,9	1,4	0,3	.	59,6
37	Bełsk	.	.	0,2	.	.	3,7	1,4	.	0,6	.	2,1	.	4,2	.	.	.	6,6	7,0	.	.	6,7	2,6	0,6	1,2	6,0	7,8	7,9	6,8	0,5	0,5	.	66,4
38	Łódź-Lublinek	.	.	1,4	0,5	.	5,3	0,3	.	0,8	2,1	0,1	0,8	2,3	.	.	.	6,1	1,7	.	5,5	4,7	2,7	.	0,4	6,6	4,1	5,7	6,4	1,4	0,2	.	59,1
39	Kalisz	.	.	0,2	0,6	0,6	5,3	1,4	0,8	2,9	3,3	.	2,8	1,2	.	.	.	6,7	6,5	3,7	5,8	5,3	5,7	1,4	3,2	7,0	7,4	3,9	5,8	2,6	.	.	84,1
40	Wieluń	.	0,1	0,3	0,6	0,6	5,3	0,4	0,9	3,1	2,0	0,6	1,0	3,2	.	.	.	4,0	6,1	1,7	6,0	5,1	4,5	.	5,7	3,6	6,6	6,5	7,0	1,9	0,2	.	77,0
41	Szepietowo	.	.	.	2,1	.	0,5	1,8	.	.	.	.	0,6	1,9	0,1	0,9	0,9	5,3	6,5	.	.	2,9	.	4,6	.	1,0	5,0	6,9	.	2,2	0,1	.	43,3
42	Białowieża	.	.	.	2,4	.	0,2	.	.	.	2,0	.	.	.	.	1,4	.	4,7	7,2	.	4,3	2,4	.	5,2	0,1	5,7	5,9	.	7,5	4,3	0,8	.	54,1
43	Terespol	.	.	0,7	4,6	.	3,9	.	0,1	0,1	2,8	.	0,1	0,4	.	.	0,5	4,9	7,0	.	5,7	1,0	.	3,7	0,2	5,5	5,5	.	6,8	3,7	2,2	.	59,4
44	Sobieszyn	.	.	1,9	1,4	.	3,9	3,6	.	0,8	0,7	4,8	.	2,6	.	.	.	5,5	7,1	.	.	5,3	2,0	2,8	.	7,1	3,4	1,0	7,6	2,5	1,5	.	65,5
45	Puławy	.	.	2,6	0,4	.	4,1	3,8	0,1	2,6	0,2	5,6	0,1	2,7	.	.	.	5,6	6,6	.	.	6,7	3,0	1,2	1,4	6,1	5,7	4,7	7,3	1,9	1,9	.	74,3
46	Chełm Lub.	.	.	2,3	4,8	.	2,7	0,5	0,3	3,6	2,3	.	1,6	.	.	.	.	5,2	6,6	.	6,3	0,9	3,4	0,3	.	1,2	4,9	3,1	8,0	5,0	4,1	.	67,1
47	Szczawno-Zdrój	1,1	1,2	.	.	1,9	4,1	1,2	.	3,6	2,6	.	0,7	2,6	.	0,2	.	.	5,8	6,0	6,7	5,7	0,1	.	.	.	5,1	6,4	5,0	6,4	.	.	66,4
48	Śnieżka	0,1	6,2	.	.	.	0,8	.	.	1,5	0,8	.	0,1	3,8	.	7,1	8,3	8,3	8,0	8,1	8,0	8,1	0,4	.	.	5,8	8,4	8,6	6,0	1,8	.	.	100,2
49	Opole	.	.	0,9	.	1,7	4,5	0,3	1,2	4,8	4,0	2,3	0,5	4,0	.	.	.	5,0	3,1	5,0	7,4	7,4	2,3	.	4,4	.	.	7,8	.	2,0	.	0,2	68,8
50	Kudowa-Zdrój	0,2	.	0,6	.	.	5,4	0,9	.	1,4	3,5	.	2,6	1,2	.	3,2	4,0	6,6	7,4	5,1	7,5	3,9	.	.	.	1,5	7,6	4,6	6,4	0,7	0,1	.	74,4
51	Polanica-Zdrój	1,7	.	1,0	.	1,7	4,3	2,5	0,2	.	4,5	.	3,2	4,3	.	.	.	0,4	4,6	3,3	5,3	3,3	.	.	.	.	5,1	3,5	6,6	2,3	.	0,1	57,9
52	Skroniów	.	.	1,7	.	.	6,5	0,9	2,2	2,9	1,0	2,9	3,1	4,9	.	.	.	6,2	6,3	.	3,6	6,2	0,6	0,1	5,2	2,1	5,8	6,5	6,3	.	2,1	.	77,1
53	Świerklaniec	0,2	.	0,1	0,3	.	5,6	.	1,1	5,6	0,3	0,5	2,7	3,9	.	.	.	6,8	3,7	0,3	5,1	3,7	3,4	.	6,7	.	6,1	4,0	5,9	0,7	0,7	.	67,4
54	Kraków, Obs. Astr.	.	.	2,8	0,9	0,8	5,6	0,4	2,5	4,3	.	3,4	2,8	3,7	.	.	.	4,0	4,6	.	5,1	6,6	.	.	4,0	.	4,3	3,7	1,3	0,7	3,1	.	64,6
55	Cieszyn	.	.	1,1	4,5	1,5	6,1	.	1,9	0,4	1,4	1,5	0,9	5,0	.	.	.	3,0	5,2	0,4	3,3	1,4	3,6	.	.	0,3	3,8	0,6	6,4	0,1	0,4	.	52,8
56	Istebna-Kubalonka	.	.	3,1	0,2	.	4,0	.	0,2	0,2	.	0,5	0,3	5,2	0,1	2,3	4,9	5,4	7,8	4,8	8,0	6,4	2,1	1,4	.	2,0	7,8	8,4	8,3	.	.	.	80,5
57	Rabka	.	.	2,5	0,5	1,0	7,0	0,2	4,8	4,4	1,5	4,0	1,5	5,2	0,5	1,6	3,8	2,5	7,5	.	7,3	7,2	3,1	.	0,1	1,0	8,0	7,9	7,8	1,1	3,0	0,3	95,3
58	Jabłonka	.	.	3,0	1,4	1,4	5,3	.	2,7	0,9	2,1	.	2,7	5,9	0,6	5,3	3,2	2,7	6,2	.	7,4	4,3	2,8	0,1	.	0,3	6,9	6,7	6,1	0,6	2,1	.	80,7
59	Krynica	.	.	3,3	3,0	0,6	1,9	2,2	.	.	.	2,0	1,0	5,6	0,8	1,4	4,5	2,4	7,5	.	.	6,4	0,1	.	0,1	6,1	7,0	7,0	7,0	3,6	5,1	.	78,6
60	Krynica-Góra Park.	.	.	2,6	3,6	.	2,9	2,4	.	.	.	2,6	.	5,3	2,4	.	5,3	2,5	7,1	0,1	.	7,1	0,3	.	5,7	.	7,4	7,6	7,3	4,2	4,6	.	81,0
61	Muszyna	.	.	1,5	4,0	0,3	2,6	1,7	.	.	.	2,6	0,9	5,0	1,5	1,7	3,5	2,9	6,6	.	.	7,1	.	.	3,8	3,1	7,5	5,5	4,6	5,1	3,2	0,2	74,9
62	Zakopane	.	.	2,7	0,2	1,5	6,3	0,2	5,5	6,2	2,3	3,7	.	6,8	.	6,2	7,0	4,0	7,0	.	7,0	6,3	3,4	.	1,2	0,9	7,1	6,7	7,1	0,9	4,6	0,1	104,9
63	Gubałówka	.	.	2,7	1,7	.	6,4	0,6	5,5	5,4	2,3	4,0	0,4	6,2	.	5,9	6,4	4,0	6,6	.	6,6	6,0	3,7	.	2,3	1,2	7,0	7,0	7,1	1,1	4,3	0,3	104,7
64	Hala Gąsienicowa	.	.	0,3	.	0,3	4,5	0,2	4,2	4,8	2,3	3,5	.	4,9	.	4,9	4,9	5,0	5,0	.	5,2	5,1	2,3	.	3,1	1,7	5,4	5,4	5,7	1,0	3,7	.	83,4
65	Kasprowy Wierch	.	.	1,6	.	0,7	7,6	0,5	5,0	5,6	3,0	2,2	0,1	7,6	.	7,5	7,9	7,9	7,9	0,2	7,4	7,9	4,5	0,1	4,5	2,2	8,2	8,2	8,2	2,0	5,0	.	123,5
66	Werbkowice	.	0,3	3,9	6,9	.	0,9	1,5	1,1	3,1	.	.	.	.	.	.	.	.	5,2	8,0	5,8	1,1	3,9	0,1	0,2	1,7	2,7	7,6	6,3	6,1	4,7	.	71,1
67	Żdanów	.	.	2,8	0,2	.	5,9	4,7	0,6	4,7	0,9	2,6	4,4	4,8	.	.	.	6,8	7,4	.	.	6,0	0,4	.	2,0	3,3	4,0	8,4	7,8	2,8	4,0	.	84,5
68	Iwonicz	.	.	0,5	4,0	.	3,2	0,1	4,1	2,8	2,9	2,1	0,8	0,3	.	.	.	2,3	1,8	.	.	1,3	.	.	3,8	.	4,4	2,2	5,6	4,7	5,0	.	51,9
69	Lesko	0,4	.	1,3	0,3	0,1	4,9	.	5,5	3,2	4,2	3,3	0,1	0,2	.	.	.	4,9	5,4	.	1,3	5,0	.	.	4,8	2,0	7,0	6,4	7,5	4,7	1,3	.	73,8

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	Suma
1	Ustka	1,2	.	0,1	2,0	3,7	.	3,5	4,0	.	.	.	.	.	.	5,2	.	3,9	7,9	.	.	.	.	.	.	5,6	5,5	.	.	42,6
2	Kołobrzeg	.	0,1	.	5,1	1,9	.	2,8	2,6	.	.	.	0,2	.	.	5,7	.	7,2	7,4	.	.	.	.	.	1,9	7,0	5,1	.	.	47,0
3	Międzyzdroje	0,1	.	.	1,9	0,3	.	1,3	4,2	.	.	.	.	1,1	.	4,4	.	6,3	7,4	.	.	.	8,2	.	2,8	7,2	3,0	.	.	48,2
4	Resko	0,3	0,5	.	2,7	0,2	.	3,8	1,9	.	.	.	.	.	.	4,2	.	3,2	7,6	.	.	.	.	.	2,3	7,3	4,7	.	.	38,7
5	Szczecinek	1,4	.	.	3,0	2,4	0,6	4,1	1,3	.	.	.	.	.	.	4,5	.	2,0	7,9	.	.	.	.	.	.	.	1,4	.	.	28,6
6	Chojnice	0,9	.	.	4,5	2,1	0,8	2,9	1,6	.	0,1	.	.	.	.	0,9	.	3,1	8,6	.	.	.	.	.	.	.	2,3	.	.	27,9
7	Hel	0,2	2,7	.	3,7	2,1	0,5	3,3	3,0	.	.	.	1,0	0,7	0,1	5,0	.	5,6	7,5	.	.	.	.	.	.	.	2,9	.	.	38,3
8	Gdynia	0,3	1,8	.	5,6	3,8	3,0	3,5	3,8	.	.	0,5	.	.	0,9	5,2	.	7,8	7,3	2,2	.	.	.	.	.	.	6,5	0,1	.	52,3
9	Świbno	.	1,5	.	3,9	1,4	0,5	0,6	2,6	.	.	.	0,7	.	.	4,9	.	6,6	7,6	.	.	.	.	.	.	.	4,5	.	.	34,8
10	Stare Pole	2,2	2,0	1,3	3,0	0,5	1,8	1,0	2,5	.	0,6	.	.	.	.	.	.	5,0	8,3	.	.	.	.	.	.	.	6,4	.	.	34,6
11	Radostowo	0,7	1,1	0,2	2,2	5,4	1,6	1,1	3,2	.	.	.	1,0	0,1	.	3,2	.	7,0	8,1	.	.	.	.	.	.	.	1,2	.	.	36,1
12	Prabuty	.	.	1,2	1,0	3,9	1,6	0,1	3,1	.	.	.	.	.	.	.	.	3,7	8,2	.	.	.	.	.	.	.	3,1	.	.	25,9
13	Bydgoszcz, IMiUZ	0,9	1,4	.	2,9	4,8	3,0	4,8	2,7	.	.	.	.	.	.	2,3	.	.	6,3	.	.	.	.	.	.	.	4,4	.	.	35,5
14	Suwałki	0,4	.	.	1,0	3,4	1,2	.	.	2,1	.	.	0,1	0,8	1,4	3,6	.	.	5,1	.	.	.	6,4	.	.	.	9,6	2,1	.	37,2
15	Mikołajki	0,8	.	0,3	1,2	3,6	3,9	.	.	.	.	.	.	0,6	0,9	5,1	.	.	7,9	.	.	.	.	1,4	.	.	6,5	2,4	.	34,6
16	Bisbrze	.	.	.	.	2,5	1,3	.	.	0,7	.	.	.	0,5	0,2	5,0	.	.	5,7	.	.	.	2,3	.	.	.	9,4	1,9	.	29,5
17	Białystok	0,4	.	.	1,7	2,0	1,9	.	.	.	.	.	0,2	.	0,7	4,7	.	.	4,0	.	.	.	2,8	.	.	.	9,3	4,6	.	32,3
18	Gorzów Wlkp.	0,3	3,6	.	1,8	2,4	.	5,0	1,3	.	.	.	.	.	.	3,4	.	2,9	5,5	.	.	2,2	7,5	.	2,1	6,1	6,0	0,3	.	50,4
19	Przebędowo	1,5	1,8	.	2,9	6,0	1,1	6,3	1,5	.	.	.	.	2,0	.	2,4	.	.	6,6	.	.	1,1	8,1	.	1,8	.	6,4	.	0,1	49,6
20	Przybroda	.	0,3	0,1	1,6	6,2	0,2	6,2	1,0	.	.	.	.	4,1	.	4,8	.	1,1	7,4	.	.	0,5	7,6	.	1,7	0,9	6,7	.	.	50,4
21	Poznań-Ławica	1,0	3,0	0,1	0,5	6,0	0,7	6,3	0,8	.	.	.	.	3,7	.	4,5	.	0,5	6,7	.	.	1,9	7,5	.	1,1	0,6	6,5	0,1	.	51,5
22	Plewiska	1,0	3,4	6,5	3,4	.	6,3	0,2	0,9	.	.	.	.	3,1	.	5,1	.	0,9	7,0	.	.	.	7,6	.	.	.	6,7	.	0,1	52,2
23	Kórnik	0,9	3,3	.	0,9	6,0	1,0	5,6	1,3	.	.	.	0,2	2,3	.	6,5	.	0,5	7,8	.	.	3,5	9,1	.	2,0	0,2	8,0	0,2	.	59,3
24	Oborniki Śl.	.	.	.	.	3,5	.	.	.	.	4,9	.	.	.	.	6,6	.	6,7	6,8	.	.	.	7,0	.	6,9	5,7	8,0	4,7	.	60,8
25	Leszkowice Oławskie	.	2,8	0,4	3,9	3,8	1,5	0,2	0,8	.	.	0,2	.	.	1,9	6,5	.	2,8	7,1	.	.	4,5	8,0	5,7	4,8	7,9	8,5	3,2	.	74,5
26	Ciechocinek	.	1,4	0,8	3,3	3,7	3,4	4,3	3,3	.	.	.	.	.	.	.	.	.	7,3	.	.	.	.	.	.	.	.	0,2	.	27,7
27	Więcławice	0,4	1,1	.	1,9	6,2	3,3	4,9	2,0	.	.	.	.	.	.	.	.	.	7,6	.	.	0,1	.	.	.	.	3,8	0,2	.	31,5
28	Legionowo	.	1,0	2,3	3,1	2,7	4,5	.	1,4	.	.	.	.	.	1,6	5,9	.	.	6,0	.	.	.	.	.	.	.	8,9	4,5	.	41,9
29	Warszawa-Bielany	.	0,8	0,5	3,2	2,6	5,0	0,1	1,6	.	.	.	.	.	1,2	5,7	.	.	5,5	.	.	.	.	.	.	.	8,5	5,4	.	40,1
30	Warszawa, Min. Kom.	.	1,0	.	2,8	2,1	4,6	.	1,3	.	.	.	.	.	1,0	5,1	.	.	4,6	.	.	.	.	.	.	.	8,4	4,1	.	35,0
31	Międzylesie	.	1,5	0,3	5,1	.	6,4	.	1,2	0,4	.	.	.	.	1,3	6,1	.	.	5,8	.	.	.	.	.	.	.	8,9	5,3	.	42,3
32	Erwinów	0,1	1,8	1,0	3,8	2,8	4,0	0,7	1,8	.	.	.	.	.	1,7	5,9	.	.	6,5	.	.	.	0,7	.	.	.	6,7	5,2	.	42,7
33	Świder	0,3	0,6	.	3,5	0,7	4,3	.	0,9	0,1	.	.	.	.	0,7	5,6	.	.	5,7	.	.	.	.	.	.	.	8,2	4,7	.	35,5
34	Topola-Błonie	.	4,1	.	0,5	4,2	5,3	2,1	2,0	.	.	.	1,1	.	.	5,5	.	.	5,8	.	.	0,7	6,7	.	2,4	0,3	2,9	3,6	.	47,2
35	Młochów	0,2	1,7	.	3,2	2,4	3,8	.	1,6	.	.	.	.	.	1,5	6,2	.	.	7,5	.	.	.	0,9	.	.	.	6,8	5,7	.	41,5
36	Skierniewice	1,2	3,6	0,2	2,6	.	4,5	1,2	1,9	.	.	.	0,8	.	1,5	6,2	.	.	8,4	.	.	.	4,9	.	.	.	1,0	5,4	0,1	43,5
37	Belsk	1,0	2,0	.	4,8	1,4	3,4	0,5	1,3	.	.	0,2	0,1	.	1,4	6,1	.	.	6,8	.	.	0,2	2,5	.	.	.	5,4	5,9	.	43,0
38	Łódź-Lublinek	1,0	3,3	.	0,5	2,6	4,8	2,2	1,3	.	.	.	2,4	.	.	5,0	.	.	5,6	.	.	0,3	7,2	.	3,9	2,0	2,9	3,9	0,2	49,1
39	Kalisz	.	4,0	.	1,3	5,0	2,5	2,8	2,3	.	.	0,2	0,1	1,7	.	5,6	.	.	6,7	.	.	3,3	7,1	.	4,0	0,2	7,4	2,4	.	56,6
40	Wieluń	0,3	3,8	.	4,1	1,0	5,1	0,9	0,7	.	.	.	2,1	0,3	1,0	6,5	.	.	7,6	.	.	1,4	8,2	.	6,3	0,7	6,2	4,6	.	60,8
41	Szepietowo	.	1,3	3,4	1,9	1,7	3,4	.	.	.	.	.	.	.	.	4,5	.	.	6,3	.	.	.	.	.	.	.	8,6	5,9	.	37,2
42	Białowieża	.	.	.	1,1	.	1,3	.	0,9	0,7	.	.	0,2	.	1,6	5,0	.	.	2,6	.	.	.	3,4	.	.	.	9,3	5,8	.	31,5
43	Terespol	0,1	0,2	.	0,7	2,6	1,9	.	1,9	0,1	.	.	.	.	2,6	4,4	.	.	3,6	2,3	.	.	.	.	.	.	8,4	6,5	.	35,3
44	Sobieszyn	1,1	2,3	.	1,7	6,0	7,0	.	.	0,3	.	0,1	.	.	0,5	4,9	.	.	4,7	.	.	.	.	.	.	.	7,4	6,8	.	42,8
45	Puławy	1,1	2,3	0,2	2,7	3,0	7,3	.	0,4	0,7	.	0,8	.	.	1,1	4,1	.	.	5,4	.	.	.	0,1	.	.	.	7,6	7,0	.	43,8
46	Chełm Lub.	1,9	0,9	0,2	0,9	6,1	7,1	.	0,2	1,9	.	0,5	.	.	1,6	6,6	.	.	6,5	2,9	.	.	.	.	.	.	5,3	8,5	.	49,1
47	Szczawno-Zdrój	.	3,6	0,2	3,4	1,4	1,0	1,9	1,3	.	.	0,4	.	0,2	.	7,3	.	4,7	8,6	.	.	5,2	4,5	5,9	8,2	8,5	8,3	0,5	1,2	76,3
48	Śnieżka	.	1,3	0,2	0,5	0,1	.	.	.	.	.	0,5	.	1,7	6,4	7,7	.	9,0	9,3	1,5	3,2	2,3	9,2	9,0	9,4	9,4	9,7	0,7	.	91,1
49	Opole	.	5,0	0,5	3,9	1,6	2,8	0,3	0,4	.	.	0,3	.	.	1,6	6,9	.	0,1	5,3	.	.	5,2	5,9	5,6	6,5	7,5	8,4	5,2	.	73,0
50	Kudowa-Zdrój	.	1,0	0,4	.	4,6	.	0,5	0,9	.	.	.	.	.	.	.	.	.	7,4	.	.	6,4	.	3,7	3,0	6,7	0,1	2,0	1,9	38,6
51	Polanica-Zdrój	.	0,8	2,0	3,1	2,7	0,3	0,7	1,6	.	.	0,3	.	0,1	.	5,9	0,2	7,1	6,2	0,9	.	4,9	1,3	5,1	7,6	6,9	7,5	3,4	2,5	71,1
52	Skroniów	.	2,4	.	.	0,4	7,4	.	.	.	.	0,3	.	0,8	1,4	1,7	.	.	5,5	.	.	.	4,4	.	1,0	2,1	.	5,7	.	33,1
53	Świerklaniec	.	4,5	.	3,6	.	4,6	1,7	0,5	.	.	0,7	.	0,1	0,5	5,9	.	.	3,5	.	.	0,8	2,9	.	3,9	.	.	5,5	.	38,7
54	Kraków, Obs. Astr.	0,2	1,7	.	3,1	.	7,3	.	.	1,4	.	2,1	0,6	.	2,7	4,4	.	.	7,6	.	.	3,9	5,9	1,3	.	0,3	1,8	5,7	3,5	53,5
55	Cieszyn	.	2,9	0,2	4,2	.	5,1	0,2	.	.	.	0,4	.	.	2,9	5,2	.	.	8,3	3,1	.	1,2	4,0	6,1	7,1	7,8	0,2	6,1	0,2	65,2
56	Istebna-Kubalonka	.	1,5	0,2	2,2	.	5,7	.	0,1	.	.	.	.	0,2	2,6	0,5	.	.	9,3	7,7	0,4	0,3	4,8	8,7	4,9	5,2	.	4,4	2,6	61,3
57	Rabka	.	2,3	0,1	2,7	.	8,5	.	0,1	1,5	.	3,8	0,3	0,6	4,8	7,0	.	.	9,0	7,7	.	4,5	8,2	6,1	4,6	8,7	9,1	8,0	4,5	102,1
58	Jabłonka	.	3,2	0,8	4,5	.	5,8	0,1	0,4	0,1	.	2,2	1,2	0,2	5,0	4,1	0,2	1,4	5,4	6,5	.	1,7	6,3	3,0	3,0	4,5	4,8	3,9	4,3	72,2
59	Krynica	.	0,1	0,3	1,3	0,1	7,9	.	.	.	.	4,2	.	0,2	3,8	6,8	.	5,2	8,6	.	.	.	1,5	6,3	.	.	2,0	7,7	4,5	60,5
60	Krynica-Góre-Park.	.	0,8	1,5	.	0,4	7,6	0,1	.	.	.	3,6	.	.	3,3	6,1	.	5,9	8,9	.	.	.	1,3	6,2	.	.	2,2	6,5	4,3	58,7
61	Muszyna	.	0,2	0,3	2,2	0,5	6,7	.	.	2,3	.	4,3	.	0,2	3,4	7,0	.	6,3	7,0	.	.	.	2,6	6,5	0,3	.	3,5	6,2	5,0	64,5
62	Zakopane	.	3,1	0,5	2,8	0,5	8,5	.	.	1,6	.	5,0	0,2	.	6,4	6,6	0,2	6,7	8,6	9,3	.	.	9,5	9,5	9,6	9,8	9,8	9,0	5,5	122,7
63	Gubałówka	.	3,1	0,6	2,9	0,4	7,5	.	.	2,1	.	5,1	0,3	0,2	6,0	6,4	0,4	6,4	7,4	8,1	.	.	8,1	8,3	8,3	8,5	8,6	8,3	5,8	112,8
64	Hala Gąsienicowa	.	2,8	0,4	2,3	0,4	6,4	.	.	1,5	.	2,9	0,2	.	5,8	6,2	1,0	4,0	6,4	7,1	.	4,4	7,2	7,2	7,1	7,3	7,3	7,3	5,1	100,3
65	Kasprowy Wierch	.	3,1	0,3	4,1	0,9	8,8	.	.	2,0	.	4,6	0,7	.	6,1	7,9	1,5	6,3	9,2	9,7	3,5	9,8	9,6	10,0	10,0	10,2	10,3	9,4	4,9	142,9
66	Nerbkowice	2,0	0,2	.	2,4	1,0	6,0	.	0,1	2,6	.	1,9	.	0,1	1,7	5,4	.	.	5,5	4,1	.	.	.	.	0,1	.	2,9	8,8	1,5	46,3
67	Mławów	0,1	1,6	.	3,6	3,5	7,9	0,1	1,3	2,0	.	0,2	.	0,1	4,5	3,6	1,2	.	6,4	0,7	.	0,4	1,9	.	1,5	.	8,0	6,0	2,2	57,7
68	Twonice	.	.	0,3	1,9	4,0	6,2	.	.	0,5	.	3,8	.	.	1,4	5,9	.	.	6,2	3,5	.	.	.	4,4	.	4,8	7,7	8,3	7,8		66,7
69	Leśko	.	.	0,8	1,7	1,2	5,6	.	.	2,4	.	2,4	.	.	0,1	5,9	.	.	4,7	5,4	.	.	.	6,9	.	6,8	8,1	9,0	7,1		68,5

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	5,6	0,6	.	5,1	2,4	.	7,1	7,2	4,6	7,6	.	.	7,5	.	7,8	.	.	2,8	.	.	.	.	.	.	5,8	.	0,6	2,1	.	3,9	8,3	79,0
2	Kołobrzeg	0,1	.	.	5,6	.	.	4,8	7,1	7,0	7,7	.	.	6,9	.	7,4	6,3	2,7	6,5	3,8	0,9	0,5	4,2	.	3,5	5,1	.	2,7	4,5	.	3,6	5,0	95,9
3	Międzyzdroje	.	.	.	7,6	0,6	.	.	.	.	6,2	0,2	2,1	6,3	0,3	.	8,1	.	5,9	6,5	1,5	1,2	.	2,4	.	.	.	3,8	4,8	0,1	4,0	2,8	64,4
4	Resko	.	.	.	5,7	2,8	0,2	7,4	5,5	7,6	8,0	.	0,9	7,0	.	8,3	4,4	3,5	6,8	5,1	3,9	0,3	4,4	.	1,6	2,4	0,5	2,6	5,4	.	3,9	3,5	101,7
5	Szczecinek	.	0,2	.	6,2	2,3	.	8,4	6,2	7,9	9,2	.	0,1	5,0	.	6,3	5,3	5,3	7,1	1,7	5,3	0,8	4,4	.	3,0	1,5	0,9	1,2	1,5	.	5,0	4,6	99,4
6	Chojnice	.	1,9	.	4,9	.	.	8,0	6,3	7,6	8,4	.	.	7,7	.	6,9	5,1	5,2	6,8	3,9	6,2	0,8	4,0	.	4,0	2,3	0,7	1,2	2,7	.	4,8	5,4	104,8
7	Hel	3,7	7,7	.	4,0	5,1	2,9	6,7	6,7	2,8	7,7	.	.	8,3	0,2	8,8	6,2	4,8	5,9	0,3	4,2	.	6,9	.	5,3	6,0	.	3,5	4,4	0,1	5,6	5,9	123,7
8	Gdynia	3,9	8,2	.	6,3	5,1	4,1	7,1	6,2	3,1	8,1	.	0,3	9,3	0,3	8,7	6,0	5,2	7,0	0,9	5,1	0,1	5,5	0,2	5,3	4,5	.	3,3	3,4	.	5,0	6,0	128,2
9	Świbno	.	6,2	.	3,9	5,2	3,5	5,7	6,6	2,8	7,7	.	.	8,9	.	8,5	6,4	4,8	6,3	1,5	4,6	0,2	5,4	.	3,8	4,4	.	1,5	0,9	.	5,3	6,1	110,2
10	Stare Pole	1,9	4,4	.	3,6	2,3	2,4	5,7	6,1	3,3	8,6	.	.	9,2	.	9,8	4,6	5,3	6,3	0,9	5,5	.	3,8	.	3,7	4,3	.	1,3	1,6	.	5,0	7,0	106,6
11	Radostowo	3,5	7,6	.	5,5	5,2	4,4	7,2	6,9	7,1	8,3	0,4	.	9,2	.	10,3	8,2	5,3	6,5	2,2	5,9	.	6,5	.	4,6	4,1	0,1	3,4	1,0	0,3	5,1	7,1	135,9
12	Prabuty	0,2	2,5	.	3,4	1,5	5,1	8,6	6,5	5,0	8,8	2,0	.	8,7	0,6	8,9	3,4	5,4	6,7	1,5	6,7	0,9	6,6	.	4,0	1,4	0,4	1,5	0,6	.	5,4	8,9	115,2
13	Bydgoszcz, IMiUZ	0,3	0,9	.	3,7	1,4	.	7,7	3,7	6,4	7,8	0,4	.	5,0	.	5,6	5,3	4,3	6,3	2,8	7,9	2,6	5,3	0,3	2,8	1,2	1,8	2,1	.	.	4,1	4,7	94,4
14	Suwałki	0,1	.	0,8	0,6	4,2	0,1	7,9	5,9	.	6,0	3,4	.	6,0	10,1	6,4	.	2,2	4,6	2,7	7,4	.	3,0	.	1,7	6,1	1,1	2,1	3,8	2,7	3,3	5,8	98,0
15	Mikołajki	.	.	3,1	0,5	3,6	2,8	8,8	6,8	.	9,0	3,2	.	7,7	7,7	4,7	.	4,6	5,8	2,8	9,3	0,5	4,8	.	1,0	2,6	3,7	.	3,3	1,2	4,1	7,6	109,2
16	Ziebrza	.	.	1,1	.	2,1	0,8	7,8	8,1	.	7,8	2,9	.	2,7	9,9	4,7	.	4,0	4,5	1,8	8,2	0,1	4,2	.	0,6	3,7	1,6	4,1	2,8	.	2,3	4,8	90,6
17	Białystok	0,1	.	0,4	.	3,2	.	6,4	6,3	0,1	6,8	3,7	0,2	5,4	10,6	3,4	.	3,2	4,0	1,4	8,2	0,2	3,0	.	0,8	3,6	1,2	3,7	1,8	3,9	.	5,2	86,8
18	Gorzów Wlkp.	0,4	0,1	.	5,6	3,0	.	5,0	6,2	7,1	7,5	.	0,3	5,4	.	6,0	4,1	4,4	6,5	3,9	4,6	3,1	5,1	.	3,0	0,8	2,1	3,9	4,4	.	.	5,0	97,5
19	Przebędowo	.	0,2	.	3,5	1,6	2,1	6,2	5,1	8,5	8,5	.	0,8	4,6	.	8,5	1,8	7,5	4,6	2,0	6,0	1,9	5,4	0,1	2,5	0,8	2,0	5,5	.	.	.	6,7	96,2
20	Przybroda	.	.	.	.	1,1	2,0	5,8	7,0	8,7	8,4	0,6	1,4	6,1	.	7,9	2,9	7,5	4,2	2,5	5,7	2,7	5,2	0,4	2,6	0,4	3,3	6,2	.	.	.	6,0	98,6
21	Poznań-Ławica	0,1	.	.	3,2	0,7	0,5	5,5	5,3	7,4	8,6	1,0	0,9	5,4	.	7,1	2,5	7,2	4,0	1,7	7,3	1,4	5,5	0,4	2,9	0,5	3,5	4,8	1,2	.	.	5,9	94,5
22	Pławiska	0,1	.	.	2,9	0,3	0,7	5,5	5,5	8,4	8,7	0,8	0,6	4,4	.	7,0	2,8	7,0	2,5	1,5	6,4	2,2	5,1	0,1	2,3	.	3,4	4,2	.	.	.	6,5	89,1
23	Kórnik	.	.	.	2,3	0,2	1,0	5,0	5,3	8,9	9,2	1,6	0,8	.	.	0,2	1,2	7,2	.	2,0	7,5	1,9	6,4	0,1	2,0	0,9	2,3	1,5	0,3	.	0,1	4,0	71,9
24	Oborniki Śl.	.	.	.	.	0,6	0,8	2,6	6,8	7,5	8,0	0,3	6,3	0,8	.	0,4	5,1	7,7	3,5	1,4	7,8	1,2	5,2	.	1,6	0,8	6,0	4,6	.	.	0,8	2,7	82,5
25	Łaskowice Oławskie	0,2	0,2	.	0,7	1,7	2,9	4,9	7,8	9,0	8,5	4,8	0,6	3,3	.	3,0	3,0	8,3	2,6	1,0	7,4	2,3	4,4	0,1	0,9	1,3	4,6	3,9	0,5	.	.	1,3	89,2
26	Ciechocinek	0,2	0,6	.	2,1	0,4	0,2	6,7	4,6	6,7	8,1	2,1	.	4,6	.	7,3	3,7	4,0	5,2	0,4	8,2	2,5	5,0	0,4	2,1	1,2	1,6	4,7	0,6	.	0,8	5,5	89,5
27	Więcławice	0,3	0,1	.	2,6	1,3	.	2,7	2,3	6,7	8,2	2,1	.	4,7	.	5,9	3,3	4,2	5,7	1,5	8,2	2,0	6,2	0,1	2,5	0,7	2,3	6,9	1,5	.	0,9	5,9	88,8
28	Legionowo	0,8	0,1	2,1	.	.	.	3,9	8,4	3,7	7,6	3,8	.	3,3	3,9	4,3	1,6	4,8	3,4	0,6	6,9	0,2	3,7	.	2,4	1,0	1,6	6,5	1,4	.	0,2	7,5	83,7
29	Warszawa-Bielany	0,6	0,1	2,7	.	.	.	3,6	5,2	3,9	7,4	3,9	.	3,5	4,6	4,6	2,2	4,5	3,8	0,8	6,0	0,7	3,2	0,1	1,2	0,4	2,1	5,3	1,9	.	.	5,5	77,8
30	Warszawa, Min.Kom.	1,0	.	2,7	.	.	.	3,2	4,9	3,9	7,3	3,4	.	3,6	4,4	3,6	2,6	4,4	4,0	0,9	6,6	0,8	3,9	.	1,7	0,7	1,5	7,4	1,9	.	.	7,5	81,9
31	Międzylesie	0,7	.	2,6	.	.	.	3,2	5,8	3,6	7,5	3,8	.	2,3	4,2	3,2	1,8	5,3	4,0	.	5,9	0,6	2,6	.	1,7	1,6	.	5,3	1,3	0,6	0,2	6,5	74,3
32	Erwinów	1,0	.	2,9	.	.	.	4,2	3,0	4,1	8,2	4,1	.	1,4	2,0	3,8	1,1	3,7	2,5	0,7	6,2	1,4	2,7	.	1,3	0,3	1,7	5,8	1,0	.	.	5,5	68,6
33	Świder	0,5	.	3,9	.	.	.	3,6	7,5	3,1	6,9	3,4	.	2,3	5,1	3,8	1,4	4,9	3,4	1,5	5,8	0,9	2,8	.	1,0	0,2	2,7	6,9	1,7	.	.	6,3	79,6
34	Topola-Błonie	0,1	.	.	.	.	.	5,3	3,5	7,6	9,1	0,2	0,3	3,6	.	8,5	2,2	7,2	2,6	.	8,3	0,7	4,0	0,4	1,2	0,4	1,4	6,1	0,7	.	.	7,1	80,5
35	Młochów	0,8	.	2,8	.	.	.	5,2	8,8	5,0	8,3	4,0	.	.	.	5,7	1,6	5,4	3,5	1,1	6,6	1,7	2,4	.	1,3	0,3	7,0	2,6	1,4	.	.	6,7	82,2
36	Skierniewice	0,4	.	2,6	.	.	.	5,7	6,6	7,7	8,7	4,1	0,1	2,2	0,7	7,2	2,3	5,4	4,2	0,8	8,7	2,0	1,8	.	1,0	.	2,4	4,5	1,6	.	.	7,2	87,9
37	Belsk	2,0	0,3	3,3	.	.	.	5,8	8,4	5,4	7,8	5,3	.	3,3	2,9	8,0	2,5	5,8	4,4	1,8	7,8	2,3	5,0	.	0,8	0,6	2,7	7,2	1,9	.	.	6,5	101,8
38	Łódź-Lublinek	0,1	0,2	0,1	.	.	.	4,6	4,0	7,9	8,4	3,7	0,2	4,2	.	7,5	1,4	7,6	3,5	0,1	8,6	1,8	2,4	0,1	0,3	.	2,0	5,4	0,2	.	.	3,6	77,9
39	Kalisz	.	0,1	0,1	.	.	0,4	5,4	6,6	8,8	9,1	2,6	0,6	3,9	0,2	7,1	1,6	7,5	3,1	.	8,7	1,6	4,8	0,3	1,9	0,6	2,7	6,5	0,6	.	0,1	4,9	89,8
40	Wieluń	.	.	.	0,3	.	2,0	3,8	5,0	8,8	9,4	2,8	0,2	1,1	.	5,6	1,7	8,6	5,1	0,7	9,5	2,4	3,4	.	0,6	.	5,8	5,5	0,3	.	.	3,7	85,9
41	Szepietowo	0,3	.	1,8	.	3,6	0,1	6,4	6,4	.	7,5	5,5	.	4,2	9,2	4,8	0,5	5,3	4,3	2,3	9,1	.	2,7	0,6	0,4	1,7	0,9	4,2	1,5	2,6	0,2	5,4	91,5
42	Białowieża	1,0	.	0,7	.	2,9	.	3,7	5,0	.	5,8	5,3	0,1	4,4	10,6	2,1	.	3,4	4,4	2,7	7,9	0,1	3,3	.	0,2	4,4	2,9	4,8	2,9	2,6	.	4,5	85,7
43	Terespol	2,2	0,2	2,8	.	2,3	.	2,3	6,6	.	3,4	6,2	0,4	4,0	10,4	3,5	0,5	4,5	6,0	0,9	7,0	0,5	2,7	.	0,1	2,8	3,0	7,2	4,7	1,9	.	4,2	90,3
44	Sobieszyn	1,5	0,3	5,2	.	.	.	3,1	9,2	1,1	6,8	6,0	.	2,9	8,5	3,9	0,5	5,3	7,2	0,9	4,9	1,1	3,3	.	0,5	0,2	2,0	4,5	1,9	1,5	.	2,3	84,6
45	Puławy	1,4	0,4	8,4	.	.	.	1,9	8,6	2,5	6,4	3,8	.	2,3	6,9	4,0	0,8	4,8	5,8	0,6	3,8	0,8	2,0	.	.	.	1,9	3,2	2,0	1,6	.	2,0	75,9
46	Chełm Lub.	0,3	1,0	3,5	.	.	.	2,1	10,0	0,1	6,7	7,8	0,1	1,9	10,1	2,1	0,1	6,2	7,1	0,4	5,2	1,1	2,1	.	0,1	0,5	5,0	3,8	5,9	1,9	1,4	1,2	87,7
47	Szczawno-Zdrój	0,7	3,2	.	1,4	1,2	4,5	4,3	9,5	9,3	8,4	1,9	1,5	3,9	.	1,3	4,5	7,9	3,9	1,9	4,4	1,0	3,9	0,1	1,1	1,2	5,1	4,4	0,3	.	.	0,1	90,9
48	Śnieżka	.	5,3	0,3	5,5	3,9	7,7	7,6	10,4	10,0	9,7	3,2	3,6	3,9	.	.	9,3	9,1	2,7	1,7	3,4	0,3	1,6	.	0,2	0,4	3,9	5,7	0,6	.	.	1,4	111,4
49	Opole	0,4	1,2	.	0,2	0,4	3,6	5,1	5,9	8,3	8,8	3,2	0,9	2,4	.	5,6	5,1	8,0	6,1	1,4	8,7	3,2	4,3	0,2	0,1	0,9	2,5	5,6	0,3	.	.	0,1	88,5
50	Kudowa-Zdrój	1,5	3,5	0,2	1,5	1,0	5,9	5,4	7,8	8,5	8,2	2,2	2,4	2,8	.	4,2	7,5	7,2	4,1	1,5	3,9	1,5	5,2	.	0,5	1,3	5,6	6,5	.	.	.	.	99,9
51	Polanica-Zdrój	2,0	7,1	.	0,6	3,1	5,0	5,9	8,8	9,4	9,6	6,3	2,1	3,8	.	5,1	6,6	8,3	6,0	1,1	5,1	2,0	4,9	.	2,7	0,9	5,7	6,8	0,8	.	.	.	119,5
52	Skroniów	.	.	1,0	.	.	1,7	1,4	7,8	7,1	7,7	5,1	.	2,0	.	6,9	1,2	8,9	7,4	0,7	6,9	2,1	3,2	.	0,2	0,4	1,0	3,1	2,2	.	.	0,4	78,4
53	Świerklaniec	0,6	1,2	0,2	.	0,7	2,5	3,2	8,2	7,8	7,2	5,7	0,3	1,8	.	4,0	5,8	8,8	6,4	0,7	7,9	1,5	.	3,4	.	1,2	2,0	5,6	0,9	.	.	.	87,6
54	Kraków, Obs.Astr.	1,3	1,7	1,1	.	0,8	2,3	4,0	7,1	6,3	8,1	4,7	0,2	1,9	.	3,5	5,0	8,6	8,2	0,9	6,7	3,0	3,5	.	.	1,0	1,3	3,7	1,1	0,2	0,5	.	87,1
55	Cieszyn	2,0	0,8	2,1	.	0,5	1,3	4,9	5,2	4,9	8,2	3,1	1,3	0,3	.	2,7	4,7	7,1	9,0	0,1	6,3	2,3	1,7	.	.	0,3	2,0	0,6	0,7	.	0,4	.	72,9
56	Istebna-Kubalonka	1,6	3,0	1,6	.	2,6	3,8	7,3	7,7	7,4	9,3	6,9	3,7	1,9	2,6	.	.	8,4	9,6	0,2	7,6	.	1,8	.	.	.	1,1	1,4	.	.	.	.	89,5
57	Babia	1,6	0,4	0,8	.	1,6	5,2	3,1	7,0	5,4	9,4	6,2	1,5	0,3	.	1,7	5,7	9,6	9,9	0,4	6,8	1,8	0,7	.	.	0,4	1,0	1,6	.	0,8	1,7	.	84,6
58	Jabłonka	2,5	1,5	1,5	.	1,1	6,6	4,5	8,3	6,8	8,2	5,7	1,8	1,3	.	0,7	5,7	9,8	9,0	.	8,0	0,2	1,0	.	0,3	0,8	1,3	1,4	.	0,6	1,6	.	90,2
59	Krynica	2,7	2,2	1,6	.	2,7	4,7	2,1	9,2	7,6	9,4	6,2	.	2,2	1,9	4,3	5,3	8,8	9,7	.	7,4	.	3,1	.	0,5	1,4	2,4	2,6	2,1	0,4	3,0	.	103,5
60	Krynica-Góra Park.	2,0	2,6	2,4	.	2,8	5,0	2,5	9,5	6,4	8,9	6,2	.	2,2	2,0	.	7,4	8,3	9,7	.	7,4	0,2	3,5	.	0,7	1,1	1,9	3,1	2,7	0,5	3,0	0,1	102,1
61	Muszyna	3,4	2,4	1,7	.	2,3	4,6	1,4	9,1	4,1	9,2	4,6	.	2,2	0,9	3,6	6,1	9,8	8,9	.	6,6	.	2,7	.	0,2	1,4	1,9	1,7	1,8	0,8	2,9	0,2	94,5
62	Zakopane	2,2	1,4	0,3	.	4,0	7,0	3,4	9,6	5,8	9,4	7,1	1,4	0,3	.	2,3	5,0	10,1	10,1	.	8,2	.	.	.	0,3	0,4	5,2	0,4	1,1	1,2	5,2	0,5	101,9
63	Gubałówka	4,1	1,3	0,7	.	2,6	6,5	2,6	8,9	6,0	8,7	6,7	1,0	0,1	.	2,1	5,0	9,4	9,3	.	7,7	0,1	.	.	0,4	0,5	4,4	0,3	0,8	1,2	5,6	0,7	96,7
64	Hala Gąsienicowa	1,6	0,9	0,1	.	6,1	8,4	2,5	8,6	3,8	8,7	5,3	0,1	0,2	.	.	3,2	9,0	9,1	.	6,3	.	.	.	0,5	.	5,4	0,7	0,2	0,5	4,2	0,1	85,5
65	Kasprowy Wierch	1,5	1,0	0,3	.	6,7	9,3	3,5	10,8	4,3	10,8	7,5	0,7	0,3	.	.	4,9	11,6	11,0	.	6,9	.	.	.	0,2	0,1	3,3	0,9	1,1	0,4	4,2	.	101,3
66	Werbkowice	0,3	1,4	2,3	0,1	.	0,2	2,7	10,3	0,2	5,9	.	7,8	2,0	10,6	2,4	0,1	5,2	8,6	0,1	3,8	.	3,5	2,8	.	0,2	0,6	2,5	2,9	6,2	2,4	1,2	86,1
67	Zdanów	3,2	.	5,8	.	.	2,4	2,3	9,9	6,9	8,0	6,4	.	3,7	4,6	6,1	1,3	9,2	8,0	1,0	4,4	1,9	4,2	.	0,2	0,9	3,7	4,3	4,9	1,2	0,2	0,7	105,4
68	Iwonicz	0,7	1,0	3,4	.	2,0	0,5	4,2	8,6	4,0	8,1	5,5	.	1,6	1,6	2,4	2,5	5,2	9,0	.	6,3	.	1,8	.	0,5	1,5	1,5	1,9	4,9	3,4	5,0	.	87,1
69	Lesko	0,6	.	1,6	.	1,5	1,2	4,6	7,9	1,9	8,9	5,3	0,1	1,2	5,6	1,8	1,4	5,3	5,7	.	3,8	.	1,8	.	0,3	1,6	3,3	.	4,9	3,2	4,6	0,4	78,5

USŁONECZNIENIE /w godzinach/ KWIECIEŃ - AVRIL 1961

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	0,8	6,8	0,2	6,1	.	9,8	7,4	1,2	11,5	6,6	10,4	9,2	3,1	8,7	0,2	2,5	3,9	3,3	12,6	12,7	12,6	12,0	12,1	12,3	10,2	9,2	6,1	11,2	12,5	10,0	225,2
2	Kołobrzeg	0,4	4,2	0,7	7,8	.	9,4	7,4	2,2	11,7	9,2	11,2	8,4	4,9	8,5	1,3	3,4	0,1	2,2	6,3	11,9	12,8	11,6	12,3	12,9	7,2	9,2	8,2	4,8	12,3	11,3	213,8
3	Międzyzdroje	4,2	1,5	1,7	7,4	0,7	8,8	6,2	6,4	10,8	8,0	10,3	10,2	8,1	5,8	1,0	8,9	0,3	2,8	12,5	13,2	12,3	12,1	12,6	12,2	5,3	11,1	8,1	0,3	9,2	9,0	221,0
4	Resko	0,8	3,8	0,1	6,7	.	8,7	7,0	3,0	11,2	7,0	10,8	8,0	8,5	8,6	4,7	3,3	0,2	1,9	11,8	9,9	12,2	11,3	11,7	12,1	4,8	10,6	8,0	0,9	6,9	9,4	203,9
5	Szczecinek	0,4	5,2	.	7,1	.	9,9	6,0	.	12,3	7,7	12,2	8,8	8,9	9,4	7,1	1,9	0,3	1,3	13,4	13,7	13,5	12,8	12,4	13,0	4,9	6,9	10,7	1,6	7,3	8,7	217,4
6	Chojnice	0,8	4,5	.	6,1	.	8,4	5,0	0,1	12,2	8,9	11,9	10,2	7,5	9,8	10,0	3,4	4,3	1,7	12,8	13,1	13,0	12,8	11,1	12,7	4,6	6,0	5,7	8,6	8,2	9,8	223,2
7	Hel	3,0	7,1	0,8	4,5	.	9,3	7,0	0,6	10,4	5,3	8,0	4,8	0,2	7,8	6,6	3,6	10,4	1,6	12,0	12,4	12,2	11,9	11,9	12,0	11,0	10,7	11,3	11,9	12,0	8,1	228,4
8	Gdynia	2,8	5,1	0,3	4,3	.	9,5	6,7	0,1	11,1	5,2	7,1	6,4	0,4	7,8	7,4	2,7	9,5	.	12,9	13,0	12,9	12,3	12,7	12,6	9,0	10,7	12,4	12,2	13,1	8,8	229,0
9	Świbno	1,7	6,1	.	5,5	.	9,3	5,0	.	10,2	3,5	9,7	7,7	0,2	8,2	7,8	4,6	11,4	0,3	13,0	12,7	13,0	12,6	12,8	8,5	10,0	9,8	11,1	11,8	13,2	7,1	226,8
10	Stare Pole	.	5,2	.	5,1	0,1	8,4	6,2	0,1	10,6	6,1	12,5	11,1	0,2	10,1	10,2	6,0	11,8	.	13,7	13,2	13,2	13,2	13,3	12,8	9,5	10,5	(9,4)	11,5	12,4	5,4	241,8
11	Radostowo	2,0	8,7	.	5,5	.	8,6	3,4	.	11,7	6,0	11,5	9,9	0,5	8,3	7,9	6,7	9,4	1,4	13,0	12,8	13,1	12,6	10,7	6,9	10,6	8,3	8,3	11,9	11,6	6,4	227,7
12	Prabuty	1,5	4,7	.	5,2	.	8,0	6,5	.	9,8	7,9	12,4	10,9	0,6	8,5	10,6	4,3	7,5	0,4	13,1	12,9	12,9	13,1	13,1	12,7	7,0	7,3	4,2	6,6	10,5	7,2	219,4
13	Bydgoszcz, IMiUZ	0,1	1,4	.	4,8	.	8,0	7,4	1,4	11,5	2,0	11,7	10,3	10,0	10,2	8,5	3,2	1,0	4,4	12,5	13,1	12,7	12,7	12,0	12,1	4,3	4,2	5,8	2,4	0,2	9,9	197,8
14	Suwałki	1,0	10,7	.	.	1,2	9,4	8,9	3,3	6,3	10,8	6,7	8,8	.	8,9	11,3	4,3	12,7	.	13,0	12,3	13,4	13,1	13,0	13,1	13,2	13,0	8,2	11,1	13,6	8,3	249,6
15	Mikołajki	1,4	6,4	.	2,2	.	8,9	8,7	.	8,1	5,8	11,8	8,8	.	8,4	10,8	6,0	11,9	.	12,9	12,8	13,2	12,3	12,8	12,9	12,6	12,7	8,3	11,0	13,1	6,8	240,6
16	Biebrza	.	9,2	.	1,9	0,7	8,5	9,1	1,1	7,1	7,7	9,1	8,9	.	7,2	10,3	5,2	11,9	.	12,3	13,1	13,1	13,1	12,7	13,0	12,9	12,3	6,2	7,4	13,6	5,8	233,4
17	Białystok	0,5	9,9	.	1,0	1,0	6,3	10,7	1,1	.	10,4	9,3	12,4	.	8,3	10,5	6,2	1,1	1,5	10,7	13,1	12,9	12,8	13,0	11,8	13,0	12,1	7,4	8,1	12,8	8,3	226,2
18	Gorzów Wlkp.	0,6	3,2	5,7	.	.	7,3	7,6	0,8	11,3	5,6	10,5	7,5	8,3	8,9	3,1	.	0,5	4,5	11,6	10,1	12,0	11,2	11,8	11,7	.	5,2	5,8	1,0	0,4	9,2	175,9
19	Przebędowo	.	2,2	.	3,1	0,2	8,9	8,5	.	10,1	4,2	11,8	9,3	9,3	10,1	8,2	5,3	.	7,2	11,5	11,9	11,9	11,5	11,9	12,3	1,8	8,2	5,2	.	2,3	2,8	189,7
20	Przybroda	.	2,9	.	5,7	0,3	9,1	9,0	0,1	12,0	4,0	11,7	11,2	9,3	10,2	8,2	0,9	.	7,3	12,4	9,4	13,1	12,1	12,5	12,6	1,5	9,3	7,2	.	1,3	11,7	205,0
21	Poznań-Ławica	.	3,4	0,3	4,8	0,6	9,1	8,4	.	10,8	2,6	9,7	10,4	6,8	8,5	8,2	0,5	.	8,1	11,2	6,0	11,5	10,6	11,3	11,5	1,9	7,1	6,8	.	1,0	9,9	181,0
22	Plewiska	.	8,0	.	0,8	.	9,2	9,0	.	10,9	2,9	10,6	11,2	9,2	9,9	8,7	1,0	.	6,1	11,7	7,1	12,3	11,8	11,9	12,1	2,0	7,7	6,7	.	.	11,4	192,2
23	Kórnik	.	3,4	0,5	4,6	1,1	8,6	10,0	.	12,1	1,2	10,4	11,5	9,7	10,3	10,3	1,7	.	8,8	12,6	7,8	13,3	12,5	12,6	13,4	1,8	7,4	6,0	.	2,1	10,7	204,4
24	Oborniki Śl.	.	0,9	.	0,2	6,4	10,2	3,1	.	.	1,5	10,5	11,1	10,4	10,5	8,9	.	3,3	11,5	4,8	7,2	11,7	11,8	11,8	11,6	.	6,5	7,0	5,7	9,3	.	175,9
25	Laskowice Oławskie	0,5	0,8	3,6	3,8	8,8	7,6	9,1	0,3	8,5	2,6	11,0	11,5	10,7	10,9	7,9	3,4	3,3	7,9	5,9	9,2	12,4	12,8	11,8	11,8	.	6,4	4,6	3,7	4,5	9,2	204,2
26	Ciechocinek	1,8	.	3,8	.	.	8,4	9,0	0,3	10,3	2,1	11,7	9,7	10,3	9,6	9,2	5,8	0,4	2,2	12,6	13,3	13,1	12,9	12,6	12,8	3,8	3,1	3,4	7,3	0,5	8,6	198,6
27	Więcławice	.	2,1	.	4,7	0,2	9,8	8,7	0,4	11,1	3,8	11,0	10,3	8,7	10,7	8,3	5,1	0,7	5,3	12,3	12,6	12,6	12,0	12,3	12,2	3,4	3,3	4,8	1,5	.	10,5	198,4
28	Legionowo	0,3	1,5	1,1	2,1	2,4	10,0	10,8	.	7,9	3,8	11,9	10,2	8,6	9,0	11,1	7,9	0,8	6,5	12,1	13,2	13,2	13,1	11,5	9,7	1,8	2,6	0,5	9,3	3,1	10,7	206,7
29	Warszawa-Bielany	0,3	1,6	1,2	2,1	3,4	8,5	10,5	.	6,3	3,4	11,8	8,7	7,7	8,8	10,8	8,7	4,0	6,5	11,7	12,7	12,6	12,5	12,7	9,9	0,7	0,6	0,4	9,6	3,1	8,7	199,5
30	Warszawa, Min.Kom.	0,8	2,7	1,2	2,1	3,5	9,3	10,2	.	7,5	4,5	11,6	8,4	7,7	7,1	10,4	8,5	3,7	8,4	11,8	12,5	12,5	12,4	12,2	7,8	0,9	1,0	0,5	9,8	10,3	3,8	203,1
31	Międzylesie	3,4	.	.	1,6	3,8	9,9	10,6	.	7,4	3,8	11,8	8,9	8,5	8,6	10,6	8,1	6,0	9,0	11,5	13,2	13,1	13,2	10,9	10,6	0,5	1,9	1,0	7,9	6,3	10,5	212,6
32	Brwinów	0,7	3,4	1,0	1,4	4,2	8,8	11,2	.	6,9	3,2	12,6	8,9	8,9	8,7	11,5	7,7	3,9	9,2	12,0	13,7	13,5	13,5	13,3	9,7	0,6	0,6	0,8	12,0	1,9	10,4	214,2
33	Świder	0,8	2,8	0,8	1,8	4,8	8,3	10,4	.	4,3	3,8	11,6	8,3	8,5	9,1	10,4	6,5	2,4	9,3	11,2	11,7	12,2	12,6	12,6	8,8	0,3	0,5	1,2	7,7	5,5	8,9	197,1
34	Topola-Błonie	0,2	2,5	1,1	3,6	3,4	9,8	11,0	.	9,8	3,2	8,9	10,0	9,1	10,6	10,0	7,5	.	9,2	10,3	9,9	13,0	12,6	12,2	12,4	2,3	1,7	10,0	9,3	2,6	10,1	216,3
35	Młochów	0,6	3,0	0,8	1,7	5,5	6,3	11,3	.	7,3	3,4	12,9	8,9	8,4	9,7	11,1	8,1	2,8	8,6	11,7	12,6	13,5	13,5	13,5	9,5	0,1	.	1,1	9,6	2,7	9,0	207,2
36	Skierniewice	1,6	3,1	0,8	2,7	6,3	8,1	10,8	.	7,5	0,9	10,2	9,2	8,1	9,2	10,7	8,3	2,3	9,1	10,8	9,7	13,2	13,1	13,0	9,9	0,6	.	4,4	8,0	1,0	11,7	204,3
37	Belsk	1,7	3,0	1,1	3,7	5,9	9,7	11,0	0,2	6,9	2,0	8,7	10,2	7,8	10,0	10,6	9,9	7,5	10,2	10,9	11,6	12,9	13,2	12,5	9,4	.	0,3	4,5	9,6	5,2	8,2	218,4
38	Łódź-Lublinek	1,1	2,0	0,9	1,9	5,0	9,5	9,9	.	7,3	0,9	6,4	8,9	9,1	9,9	9,9	7,3	0,1	9,4	10,1	10,3	12,6	12,7	12,3	11,0	0,1	4,1	7,5	4,9	2,9	10,1	198,1
39	Kalisz	.	3,7	0,4	4,6	5,6	10,0	9,5	.	10,8	2,4	11,4	11,0	9,3	10,9	9,9	5,4	.	9,6	9,7	7,5	11,5	11,5	11,4	11,6	.	8,0	7,2	4,8	5,8	10,8	214,3
40	Wieluń	1,1	1,6	3,8	4,0	8,5	9,9	10,8	0,4	9,6	0,5	8,0	10,9	9,9	11,0	10,4	5,7	0,8	7,6	5,4	10,3	12,7	11,8	12,2	12,3	.	7,1	7,6	4,7	4,7	10,5	213,8
41	Szepietowo	0,5	5,0	.	1,1	1,3	7,2	11,3	.	8,6	6,5	11,7	12,5	0,4	9,3	11,2	8,3	1,9	2,3	12,3	13,3	12,9	13,0	12,6	12,8	8,0	10,7	7,8	10,2	.	5,0	217,7
42	Białowieża	.	6,7	.	.	0,8	6,0	11,1	0,2	6,4	10,1	9,7	11,9	.	8,5	10,9	6,7	0,4	2,3	8,5	13,3	13,4	13,1	12,8	12,6	12,4	12,1	8,5	8,0	11,6	10,5	228,5
43	Terespol	1,4	4,2	0,9	1,5	3,0	10,4	11,1	1,6	7,1	6,4	11,9	12,1	1,1	9,0	12,0	9,2	2,0	6,8	8,5	13,3	13,1	13,3	13,2	12,4	2,7	7,8	9,4	9,7	2,9	12,4	230,4
44	Sobieszyn	1,0	3,3	0,8	1,9	4,6	9,6	11,4	0,2	6,2	4,0	8,1	12,3	8,2	10,0	12,3	5,8	9,0	7,8	11,8	13,2	13,5	13,5	13,4	5,7	0,4	0,9	8,2	6,2	8,9	9,8	222,0
45	Puławy	2,2	2,8	1,0	.	5,9	8,0	9,8	0,6	5,7	3,1	6,6	10,7	6,4	9,9	11,3	3,7	8,1	7,5	10,2	11,2	12,6	12,5	12,6	3,5	.	1,8	6,9	7,8	9,1	9,1	200,6
46	Chełm Lub.	4,5	4,6	1,4	0,7	6,5	11,3	12,0	2,8	8,5	6,9	6,3	12,9	4,7	11,2	12,5	4,2	8,6	9,4	9,9	11,5	13,2	13,4	13,5	3,7	0,1	5,5	11,1	9,5	9,8	9,7	239,9
47	Szczawno-Zdrój	2,8	.	5,5	1,2	6,2	10,0	7,3	1,8	7,3	2,2	7,7	10,9	9,5	10,5	6,4	0,9	4,5	9,4	2,8	8,1	11,6	9,8	8,0	10,0	.	6,8	1,7	.	2,7	9,6	175,2
48	Śnieżka	.	.	0,7	3,9	3,4	10,8	8,7	1,0	7,9	2,8	3,2	11,1	10,5	11,3	9,4	0,5	4,3	5,2	3,0	10,3	12,3	2,0	.	7,7	13,1	8,4	0,8	.	1,6	5,9	159,8
49	Opole	1,5	2,6	4,0	0,6	9,3	11,3	10,2	3,8	10,4	3,5	10,4	11,1	10,0	10,9	9,6	7,0	5,0	6,3	4,2	11,8	12,1	12,7	10,9	11,8	.	8,7	7,8	3,3	7,7	8,7	227,2
50	Kudowa-Zdrój	1,0	1,8	.	7,4	.	10,7	9,8	3,9	9,2	7,9	4,1	11,9	10,7	11,7	9,0	.	4,0	8,1	1,7	10,8	12,2	10,4	8,3	11,4	9,8	6,9	4,7	.	0,9	10,2	198,5
51	Polanica-Zdrój	2,5	.	4,1	1,8	7,1	11,2	10,3	3,5	6,9	5,7	2,5	10,9	10,5	11,1	8,8	1,5	5,2	7,0	1,0	10,5	11,6	11,4	6,3	8,0	0,1	5,1	0,7	0,1	1,5	8,3	175,2
52	Skroniów	3,7	5,0	2,1	0,2	7,3	10,1	11,0	2,9	7,2	4,9	8,2	11,5	8,5	11,0	11,1	5,1	.	6,4	5,0	11,8	12,9	12,9	10,6	7,4	.	4,3	4,5	6,1	4,5	9,4	205,6
53	Świerklaniec	2,6	0,9	4,0	0,9	9,2	10,3	10,4	2,1	8,2	3,8	6,9	10,5	9,1	10,4	9,7	6,3	1,6	3,9	6,7	11,5	12,6	10,2	11,4	11,3	0,4	9,5	7,2	1,8	6,2	10,1	209,7
54	Kraków, Obs.Astr.	6,0	0,3	4,3	1,2	8,9	10,9	10,9	6,6	9,2	5,4	6,0	9,2	10,5	11,2	9,6	9,6	4,9	7,4	7,7	10,5	11,9	12,1	12,6	11,7	.	5,5	7,5	5,6	6,7	7,8	231,7
55	Cieszyn	2,4	0,1	1,9	0,1	9,5	10,9	10,8	4,7	7,6	7,8	3,4	10,2	10,1	12,1	11,1	3,0	6,5	4,5	0,3	9,6	12,5	12,8	12,6	11,8	6,1	6,9	6,9	1,1	5,4	6,0	208,7
56	Istebna-Kubalonka	3,5	.	3,5	0,9	9,2	11,1	11,1	5,6	7,9	6,6	3,8	10,2	10,1	11,8	11,5	3,6	5,0	6,9	0,2	11,0	12,6	12,0	12,0	12,0	11,3	4,8	2,8	1,3	8,3	3,6	214,2
57	Rabka	4,6	.	2,5	3,1	8,5	11,2	11,3	4,6	4,2	7,2	4,4	10,4	9,5	11,7	10,4	5,5	5,5	6,5	1,0	8,2	12,3	12,8	12,7	12,7	4,1	5,6	4,5	2,4	5,4	4,7	207,5
58	Jabłonka	2,7	0,2	2,9	3,3	8,0	10,9	10,7	6,9	9,2	6,2	3,8	10,4	9,8	11,1	11,4	7,0	6,0	5,0	.	8,7	12,0	11,5	10,3	11,6	3,4	6,0	3,8	3,5	4,7	3,9	204,9
59	Krynica	4,1	.	4,3	1,2	4,5	10,4	10,2	2,9	9,2	8,1	2,7	10,3	9,8	10,9	10,5	6,6	5,1	4,1	0,3	3,1	11,2	9,1	11,1	11,0	0,1	0,9	8,5	4,2	6,3	3,0	183,7
60	Krynica-Góra Park.	4,8	0,6	5,2	1,9	5,5	10,1	10,3	4,1	10,3	8,9	3,8	10,2	9,4	11,3	11,3	7,3	6,7	4,2	0,2	3,5	11,2	10,5	11,9	12,1	0,1	1,4	9,6	5,5	8,2	2,7	202,8
61	Muszyna	4,8	0,1	3,8	1,7	6,2	10,6	10,2	5,1	10,0	8,3	1,4	10,5	10,1	11,4	10,1	6,1	5,6	5,2	0,3	3,1	10,8	10,9	12,2	10,4	0,1	3,2	8,9	4,1	5,4	2,9	193,5
62	Zakopane	5,8	0,7	3,6	5,7	9,2	12,2	12,2	6,3	7,8	8,7	3,2	10,7	10,8	12,3	12,4	6,1	7,0	5,5	0,2	7,0	12,6	11,0	12,8	10,6	7,3	2,7	3,9	1,0	2,5	3,8	215,8
63	Gubałówka	5,7	0,9	3,1	6,5	8,6	10,6	10,4	6,0	8,0	7,8	3,7	9,7	9,0	10,7	10,6	6,6	7,5	5,6	0,3	6,5	11,0	11,0	11,3	10,6	8,8	2,8	3,7	1,9	2,3	2,9	204,1
64	Hala Gąsienicowa	.	0,5	2,9	4,3	8,5	10,5	10,5	5,3	6,4	9,5	1,7	9,7	8,1	11,0	10,2	5,0	5,7	5,3	0,2	5,8	10,5	11,1	11,4	7,7	2,9	0,8	0,2	0,2	3,4	1,5	170,8
65	Kasprowy Wierch	5,2	0,2	1,5	0,9	8,2	12,3	12,1	6,3	7,5	8,7	2,2	11,3	11,1	13,3	12,2	3,6	6,7	5,4	0,2	5,0	12,5	11,8	13,5	9,4	5,4	0,6	0,2	0,8	1,9	1,3	191,3
66	Werbkowice	5,4	6,3	2,1	1,4	5,4	9,7	11,4	3,3	6,9	6,8	7,8	11,4	5,7	10,6	12,0	3,3	5,4	8,5	7,9	9,0	12,9	12,8	12,9	1,8	0,1	2,8	8,7	10,6	8,9	8,5	220,3
67	Zdanów	3,6	6,4	2,6	0,8	6,5	10,7	11,6	2,4	6,6	5,8	8,3	10,9	9,7	11,7	11,9	3,2	3,5	8,6	9,9	8,9	13,2	13,1	13,0	3,7	0,3	2,1	11,3	7,3	8,8	8,4	224,8
68	Iwonicz	5,8	0,1	2,8	2,7	4,2	10,2	11,0	4,7	8,9	6,6	1,6	9,0	8,6	10,9	11,3	1,7	7,3	6,5	0,5	1,8	9,3	12,1	12,0	9,4	3,1	0,5	6,8	8,5	6,9	3,3	188,1
69	Lesko	4,8	0,1	0,9	3,3	5,1	11,2	4,6	7,4	6,0	8,7	1,5	9,7	9,5	11,4	8,8	1,2	6,5	5,6	0,7	.	13,9	13,2	12,1	12,4	3,3	2,0	5,2	8,0	6,2	3,1	186,4

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	10,8	8,6	0,2	10,5	4,9	5,5	0,4	5,1	6,0	.	3,5	12,0	5,5	0,1	.	3,5	4,3	12,7	.	0,3	4,2	14,9	7,8	5,1	8,5	12,5	3,8	.	0,1	9,7	9,2	164,7
2	Kołobrzeg	10,5	2,9	2,1	11,7	1,0	4,7	0,8	4,3	5,5	0,1	2,6	9,2	3,2	0,9	6,1	0,3	9,8	13,5	3,8	.	2,9	14,1	4,7	6,7	11,0	10,9	3,7	.	.	5,8	4,1	156,9
3	Międzyzdroje	8,4	2,4	2,9	9,6	1,8	4,4	0,8	1,5	5,0	.	5,1	7,7	1,2	3,3	7,9	.	11,8	12,6	1,2	0,7	5,4	12,9	2,9	0,6	6,7	3,6	0,1	1,9	.	3,0	0,3	125,7
4	Resko	10,4	0,8	1,5	8,5	1,2	3,1	0,1	3,0	3,8	3,0	3,0	5,5	0,5	0,3	2,2	1,8	11,6	13,1	5,1	0,4	6,4	11,0	5,7	3,3	5,2	10,3	2,2	.	.	7,9	0,7	131,6
5	Szczecinek	7,1	5,0	1,2	7,5	3,4	2,0	0,2	5,6	2,7	0,8	2,2	3,9	4,2	1,5	0,7	0,5	3,4	11,7	9,3	.	7,4	6,7	11,3	3,9	5,1	12,0	0,7	.	0,1	10,1	6,1	136,3
6	Chojnice	4,5	9,2	2,4	7,8	3,9	1,6	.	5,0	2,3	0,3	2,5	4,7	3,5	3,3	0,5	1,2	2,7	11,1	7,7	0,9	8,0	6,1	7,1	4,7	5,0	11,3	1,1	.	1,9	7,9	4,8	133,0
7	Hel	7,1	12,1	2,2	10,4	6,6	1,5	0,5	4,3	1,5	.	2,6	.	4,5	2,8	.	6,8	3,2	12,9	2,5	0,6	3,6	11,6	7,6	4,9	7,9	10,9	1,4	0,3	.	7,6	2,3	140,2
8	Gdynia	7,7	13,1	2,1	9,0	6,8	1,2	0,3	5,1	1,6	.	2,5	.	6,6	0,5	.	5,4	4,1	13,5	4,5	0,5	4,7	11,2	7,7	5,5	7,8	11,7	0,8	1,1	3,4	6,2	7,3	151,9
9	Świbno	0,3	12,5	3,1	9,2	8,5	0,8	1,2	7,5	2,3	0,2	1,3	1,7	3,7	1,9	.	2,6	3,7	13,2	1,9	0,5	1,5	11,1	6,2	3,6	5,7	12,2	2,8	.	0,2	7,2	5,1	131,7
10	Stare Pole	0,5	10,9	3,6	9,8	8,5	0,4	2,3	6,9	3,0	0,1	.	0,9	4,0	3,9	0,9	3,8	4,0	12,6	2,3	2,1	9,0	12,7	7,9	3,9	5,7	12,4	5,3	.	1,8	9,0	3,8	152,0
11	Radostowo	.	10,7	2,0	8,2	6,1	0,9	1,5	4,8	2,7	0,2	1,3	4,1	5,7	5,2	1,1	3,2	6,0	12,3	2,0	0,3	6,7	12,3	5,7	4,1	4,6	12,3	3,0	.	1,4	8,1	3,0	140,5
12	Prabuty	0,3	7,2	2,2	7,6	6,4	1,1	1,6	4,9	1,7	0,5	0,4	2,3	5,1	5,2	.	3,5	5,0	13,5	0,9	3,4	7,2	13,1	8,2	2,7	4,0	10,2	3,3	0,6	2,7	6,8	2,5	134,1
13	Bydgoszcz, IMiUZ	0,4	8,1	1,7	8,4	4,3	1,1	4,0	7,6	1,3	2,0	2,9	4,3	4,0	4,2	1,3	.	0,9	10,4	3,6	3,0	4,9	7,4	6,3	2,4	7,1	9,6	2,1	.	1,7	4,7	4,5	124,2
14	Suwałki	1,0	5,2	6,4	0,6	11,5	0,2	4,6	5,8	3,0	2,3	1,7	.	1,6	4,7	6,6	5,3	3,1	12,0	6,8	5,7	6,7	13,1	10,9	1,7	12,5	3,0	12,3	10,2	12,6	6,3	0,4	178,4
15	Mikołajki	0,3	3,2	5,0	3,3	9,6	.	5,4	8,1	2,1	1,3	0,6	.	1,4	5,5	6,3	3,8	1,2	5,4	3,7	2,9	8,1	10,5	9,1	0,9	7,2	5,4	8,0	7,3	4,3	9,0	5,3	142,2
16	Siemiry	3,2	0,5	8,1	0,6	7,4	.	6,9	5,1	1,5	2,3	1,9	.	0,7	4,2	5,1	4,3	1,7	6,3	8,0	5,5	2,7	10,6	5,9	2,1	9,1	2,8	10,1	12,2	6,7	7,1	.	158,6
17	Białystok	6,6	.	4,2	0,7	9,4	0,4	2,6	5,5	1,9	2,5	0,5	.	1,6	0,7	6,4	3,7	1,6	7,2	6,5	5,2	4,4	12,9	11,7	1,4	10,6	5,5	11,1	12,9	11,9	10,2	3,0	162,8
18	Gorzów Wlkp.	4,5	2,9	5,3	10,4	1,2	1,1	0,7	.	5,9	0,5	2,5	6,9	0,7	2,8	2,8	0,3	4,2	8,7	7,6	1,6	4,3	9,8	7,5	4,4	8,5	8,5	.	.	.	.	0,6	113,6
19	Przebędowo	3,4	2,4	3,0	10,9	3,2	2,3	2,9	7,7	1,0	2,9	4,5	5,0	0,7	5,0	8,1	.	.	6,8	7,2	2,5	3,0	7,8	4,0	5,9	8,1	11,3	1,5	.	.	.	1,7	117,9
20	Przybroda	5,0	2,2	2,9	11,2	3,4	2,4	3,3	7,7	1,5	2,2	3,9	5,6	0,8	4,6	3,4	.	0,1	7,0	7,5	2,5	5,4	8,1	1,1	5,0	9,0	12,3	0,2	.	.	0,2	2,8	121,3
21	Poznań-Ławica	4,8	1,4	3,1	8,6	1,9	1,9	3,2	6,4	1,1	2,4	1,9	3,8	0,4	3,6	3,2	.	0,2	6,2	5,9	2,0	3,5	7,7	1,9	3,6	10,3	10,2	.	.	.	0,1	1,5	100,8
22	Piła	4,3	0,5	3,7	9,2	1,9	1,9	3,1	5,1	.	3,2	3,2	4,6	0,5	3,0	2,4	.	0,3	5,1	5,0	1,9	2,0	6,9	1,6	3,6	6,9	11,4	2,1	.	.	0,2	2,2	95,8
23	Kórnik	5,1	2,8	1,9	9,4	1,1	2,8	2,9	3,9	0,7	2,1	2,5	4,3	0,7	6,6	2,9	0,1	.	2,5	6,1	2,9	3,6	7,9	1,6	3,8	8,2	11,9	2,1	.	0,4	0,1	3,0	108,9
24	Oborniki Śl.	6,2	1,1	5,9	9,2	2,2	0,2	4,6	5,3	1,0	2,6	3,5	3,5	3,6	3,1	5,8	0,6	0,4	5,6	1,5	2,6	2,1	11,3	2,0	2,8	13,6	11,8	6,2	0,2	0,1	0,2	5,6	124,4
25	Leśnowice Oławskie	3,6	1,6	4,0	10,8	4,2	0,7	5,9	6,3	1,6	0,1	2,4	4,0	3,7	5,0	4,3	3,0	0,5	4,1	2,8	4,7	0,3	8,2	5,7	5,6	12,8	12,7	1,8	.	.	0,2	3,9	124,5
26	Ciechocinek	4,2	7,1	6,3	8,1	5,4	1,6	4,8	6,0	1,4	2,0	2,1	3,5	5,7	3,2	1,6	0,2	0,6	13,0	3,7	5,1	5,9	.	6,4	0,9	5,8	9,8	4,9	0,7	3,1	3,7	3,7	130,5
27	Więcławice	4,4	5,5	5,8	11,3	4,5	1,2	4,2	8,1	1,6	2,7	6,3	4,6	5,3	3,6	.	0,7	1,0	12,0	6,1	4,3	5,0	9,5	7,5	2,1	7,3	11,8	6,2	.	3,3	2,1	3,7	151,7
28	Legionowo	8,4	0,3	8,2	7,4	7,8	.	2,7	6,3	1,2	2,8	.	1,9	2,1	4,5	5,2	3,4	1,9	2,5	7,5	4,4	5,2	7,8	9,7	3,6	9,3	8,3	9,1	7,5	5,8	2,5	5,4	152,7
29	Warszawa-Bielany	8,7	0,8	6,5	6,5	7,5	.	3,1	6,1	1,0	1,8	.	1,6	1,8	2,5	4,0	1,1	2,3	1,3	7,2	3,5	5,1	7,2	9,4	1,4	10,0	8,2	8,7	8,1	7,2	1,5	5,1	139,2
30	Warszawa, Min.Kom.	9,8	0,7	6,6	7,7	4,4	.	3,7	6,0	0,9	2,0	.	1,5	2,6	1,7	4,5	2,0	3,5	1,1	6,9	2,0	4,8	6,3	8,8	1,9	11,1	7,7	8,1	7,4	7,0	6,3	9,9	146,9
31	Międzylesie	10,9	0,7	5,0	8,3	8,6	0,6	3,9	6,6	1,1	2,2	.	1,0	3,5	0,4	6,4	2,2	3,6	1,5	8,2	3,7	3,9	7,4	10,9	3,3	12,6	10,6	9,8	7,4	7,6	1,4	7,7	161,0
32	Erwinów	10,4	0,2	5,5	5,9	7,2	.	2,0	6,2	0,5	2,1	.	1,3	2,8	1,9	2,6	1,4	1,9	2,5	7,1	2,4	3,5	6,4	10,0	2,2	10,9	10,5	7,9	7,4	5,8	1,8	4,0	134,3
33	Świder	10,1	0,2	6,1	5,9	6,9	0,2	3,8	5,9	2,1	2,5	.	0,1	2,7	0,3	6,0	1,3	1,9	1,1	7,8	3,0	3,5	6,9	9,5	1,5	11,6	8,3	8,9	7,4	6,1	1,1	5,5	138,2
34	Topola-Błonie	9,0	1,0	4,7	8,2	4,7	0,4	2,7	6,3	1,1	1,5	1,0	3,7	3,4	5,1	4,6	1,2	1,1	8,9	6,3	7,0	4,4	8,6	10,8	2,5	9,0	10,1	6,3	1,8	3,6	0,7	3,2	142,9
35	Młochów	10,6	0,3	4,0	4,9	8,0	0,1	2,1	6,1	1,4	1,7	.	0,7	2,8	1,8	2,6	0,7	2,4	2,3	8,0	3,2	2,8	6,4	10,7	1,6	11,0	8,6	7,9	7,9	6,2	1,2	4,5	132,5
36	Skierniewice	10,6	0,4	5,2	8,8	6,6	0,2	2,4	7,1	2,0	1,6	.	3,4	5,1	3,3	.	6,8	3,3	6,1	6,4	1,7	2,7	7,6	11,1	3,2	12,6	11,8	6,4	3,5	5,0	.	6,3	151,2
37	Belsk	11,6	3,2	7,0	9,3	9,0	.	4,1	7,8	2,9	2,0	.	2,4	6,1	2,0	4,2	2,8	4,7	4,1	8,4	5,1	3,8	6,7	10,7	3,7	12,0	10,9	8,1	7,8	7,2	0,1	6,0	173,7
38	Łódź-Lublinek	10,1	0,9	3,1	8,2	5,4	0,2	1,9	5,9	0,6	1,9	0,9	3,1	3,1	4,7	3,1	1,4	2,3	6,8	6,3	4,1	1,2	9,7	9,2	3,4	11,2	6,2	8,1	4,2	4,7	.	4,2	136,1
39	Kalisz	8,3	1,8	6,2	10,8	5,5	1,3	4,1	7,4	0,9	1,1	1,1	6,1	1,4	4,6	3,4	1,3	0,7	6,0	3,6	3,8	3,5	9,1	7,1	3,1	10,9	13,4	1,7	.	1,7	0,5	3,9	134,3
40	Wieluń	11,7	1,2	7,2	11,3	6,4	1,0	4,4	5,2	2,0	0,4	1,7	6,6	2,1	4,6	3,0	2,0	1,8	5,0	7,1	4,3	1,8	8,9	8,6	2,0	11,1	12,2	7,8	.	2,4	0,4	2,8	147,0
41	Szepietowo	12,9	0,5	7,9	5,2	11,8	0,1	2,9	7,6	2,9	2,6	.	.	3,8	2,1	8,0	3,1	0,7	5,4	9,6	2,8	11,6	11,3	10,8	3,0	13,5	8,7	11,0	11,2	10,2	13,6	13,0	207,4
42	Białowieża	6,4	.	6,4	2,1	11,0	0,8	2,8	6,0	2,4	1,7	1,5	.	2,0	0,7	4,7	0,7	1,9	5,7	6,4	9,9	6,6	11,2	13,9	1,1	14,1	7,4	7,9	13,1	13,7	8,3	5,1	175,5
43	Terespol	9,3	0,1	6,0	1,0	10,7	1,9	3,5	8,6	3,1	4,8	1,7	.	3,1	0,1	5,7	3,3	2,1	4,4	6,2	10,3	3,9	7,8	10,6	0,1	11,4	11,9	8,6	12,0	12,3	8,1	6,5	179,1
44	Sobieszyn	9,5	5,8	7,4	3,6	7,5	1,6	1,9	7,4	1,6	1,9	.	.	2,8	0,9	8,1	3,2	5,9	1,8	2,9	10,9	3,6	7,5	7,9	1,6	12,4	8,6	11,7	8,2	8,7	2,0	3,7	160,7
45	Puławy	9,2	2,5	8,5	1,4	7,4	1,4	2,5	5,7	1,2	1,5	0,1	.	5,0	.	5,9	2,1	5,9	1,6	5,0	10,2	2,4	5,3	9,5	1,4	12,3	4,3	9,4	7,0	8,0	1,6	4,6	142,9
46	Chełm Lub.	4,2	0,1	7,6	1,0	9,2	2,7	0,4	4,1	1,2	2,1	0,3	.	1,9	1,8	5,6	3,1	7,8	4,2	3,7	9,4	1,1	8,4	7,1	4,2	9,9	10,3	11,2	9,1	12,9	0,6	4,6	149,8
47	Szczawno-Zdrój	2,4	1,6	5,4	2,6	0,7	0,3	4,4	6,6	1,0	0,2	2,4	1,2	3,2	8,5	0,7	3,3	.	5,3	1,7	3,7	1,0	6,1	1,1	3,2	11,6	4,1	2,3	.	.	0,1	1,9	86,6
48	Śnieżka	1,7	1,2	1,6	2,4	0,2	0,4	1,7	3,8	.	0,4	.	1,6	2,5	11,5	0,2	2,4	.	4,2	.	3,4	0,3	0,9	1,1	4,9	7,3	5,9	3,1	.	.	0,1	1,8	64,6
49	Opole	9,6	2,2	5,4	11,0	5,5	0,6	4,3	5,1	2,6	0,7	4,0	3,9	3,4	7,5	5,4	7,2	0,8	4,4	2,4	2,9	1,3	4,2	7,6	5,5	11,4	11,1	5,4	.	.	0,9	3,6	139,9
50	Kudowa-Zdrój	6,7	7,2	4,1	7,0	4,5	1,3	2,0	3,8	0,7	1,2	3,8	2,9	0,3	8,0	1,3	2,4	0,2	5,1	0,8	2,8	2,0	6,4	0,9	5,0	10,1	6,8	5,9	.	.	.	2,4	105,6
51	Polanica-Zdrój	6,2	3,9	5,2	5,6	3,9	1,4	4,4	5,6	2,2	1,3	2,3	2,0	2,9	9,2	2,0	2,0	0,8	4,4	4,4	2,6	1,2	5,2	3,8	2,4	9,8	7,7	1,7	.	.	.	2,5	106,6
52	Skroniów	0,2	8,8	7,2	8,5	8,1	1,7	.	7,8	3,6	1,4	5,2	1,7	5,1	2,1	5,5	2,9	2,8	5,5	11,2	8,0	2,3	5,8	13,9	3,0	10,0	10,4	7,2	3,2	5,2	3,2	8,3	169,8
53	Świerklaniec	1,2	3,3	4,7	8,7	5,2	0,8	2,0	8,6	2,4	0,5	2,2	3,3	4,1	2,3	3,1	5,3	0,8	3,5	4,7	3,5	0,8	2,7	7,7	3,5	10,4	11,8	6,7	3,3	3,1	0,9	6,5	128,6
54	Kraków, Obs.Astr.	.	4,3	6,5	4,8	8,8	2,2	3,9	8,1	2,5	1,0	1,8	0,3	3,1	1,9	4,2	5,1	2,5	3,7	9,3	10,7	1,9	5,3	10,9	5,3	7,9	9,3	4,5	3,7	4,0	4,3	12,2	159,0
55	Cieszyn	1,6	3,9	5,6	5,2	5,8	0,7	4,3	8,2	0,9	0,7	1,2	1,9	4,9	1,9	1,8	3,0	0,1	0,6	3,4	4,1	0,3	0,7	7,6	9,5	10,3	7,6	3,4	0,8	0,2	2,9	5,9	109,0
56	Istebna-Kubalonka	1,5	3,1	4,6	6,7	7,6	1,9	2,5	7,0	2,1	0,5	2,6	2,1	2,3	0,3	1,5	4,1	0,4	0,9	2,5	3,1	2,7	5,2	12,6	5,3	9,3	6,0	7,4	2,4	4,0	0,8	10,5	123,5
57	Rabka	.	2,5	4,2	5,3	9,3	2,3	3,7	6,2	1,3	0,2	2,0	.	4,8	1,2	5,4	5,3	3,4	1,4	4,0	11,1	4,2	4,3	13,4	5,8	9,3	5,4	5,2	3,3	6,0	3,9	12,4	146,8
58	Jabłonka	0,1	4,1	5,2	5,1	8,6	4,9	.	7,2	3,9	0,4	3,0	1,8	5,8	2,6	1,9	5,4	3,4	2,1	2,5	7,6	1,8	5,9	13,4	4,0	6,1	5,8	6,7	5,1	3,4	3,6	11,9	143,3
59	Krynica	.	0,5	5,9	4,2	9,2	3,7	1,4	6,9	3,5	0,4	1,9	2,1	3,2	2,1	4,8	2,1	0,6	1,4	2,9	7,4	0,2	3,5	8,7	2,4	8,0	1,3	4,9	5,8	4,8	3,0	8,0	114,8
60	Krynica-Góra Park.	.	0,9	6,7	4,0	11,3	5,0	1,9	6,8	4,3	0,4	1,8	1,3	4,1	3,8	5,9	1,5	1,5	1,6	4,0	8,0	.	3,8	10,2	2,0	8,2	0,7	5,6	6,1	4,8	3,1	7,6	126,9
61	Muszyna	.	0,5	5,7	3,8	8,7	4,7	2,4	7,6	2,2	2,0	2,2	1,9	4,0	2,9	7,6	3,8	0,6	0,4	3,5	8,5	.	2,0	9,1	1,1	6,8	1,1	6,1	3,0	4,8	6,6	8,8	122,4
62	Zakopane	.	1,4	4,1	2,9	10,5	4,2	2,2	5,7	3,8	0,2	0,5	.	6,9	4,8	3,1	1,8	0,2	.	2,7	5,9	0,6	1,0	11,3	1,8	6,3	5,6	5,8	2,9	3,9	1,1	11,6	114,8
63	Gubałówka	.	0,6	3,6	2,5	7,8	3,6	2,0	5,5	5,1	0,3	0,7	.	5,5	3,8	4,0	3,0	0,1	0,3	3,5	5,3	1,8	1,1	10,3	1,9	6,5	4,7	5,5	4,4	4,1	0,8	10,2	108,3
64	Hala Gąsienicowa	.	.	2,1	1,8	7,6	4,6	1,0	4,9	3,5	.	0,5	0,1	5,5	2,3	3,2	1,0	.	.	2,7	3,8	.	0,8	8,2	0,9	4,4	3,2	3,5	2,6	5,4	2,1	11,2	86,9
65	Kasprowy Wierch	.	1,2	1,4	3,0	9,0	3,7	2,0	4,6	2,8	0,2	0,5	.	7,0	0,2	6,4	1,4	.	.	1,9	5,1	.	0,3	9,9	0,9	4,8	3,3	3,6	0,4	4,2	2,7	11,4	91,9
66	Werbkowice	0,4	0,5	8,6	2,2	11,6	7,2	5,4	4,0	3,5	0,4	.	3,7	2,8	6,2	4,7	12,0	3,4	4,5	8,3	0,1	8,6	9,4	2,5	7,3	9,1	10,9	8,6	13,0	0,1	5,6	.	166,6
67	Zdenów	.	1,6	11,2	3,6	10,0	2,3	1,4	6,4	1,6	1,5	.	0,3	4,0	1,2	4,4	5,7	8,1	5,6	8,0	11,9	1,7	6,3	11,1	2,5	12,3	3,3	11,1	6,6	6,6	1,4	10,1	162,0
68	Iwonicz	.	2,1	7,6	3,4	11,4	6,3	1,2	6,0	3,6	1,6	1,5	.	3,0	3,5	5,3	5,0	1,9	0,2	3,6	10,4	.	2,9	4,8	5,6	4,3	5,7	9,9	3,6	6,4	2,7	6,4	132,5
69	Lesko	.	2,3	6,2	2,1	8,4	8,0	0,2	4,6	2,1	3,5	0,8	.	2,8	4,4	6,5	2,5	2,8	0,1	5,3	8,2	.	2,4	5,5	8,1	1,3	11,1	8,8	3,4	6,2	5,3	10,1	133,5

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	7,3	11,0	13,2	14,0	8,1	14,1	2,6	4,9	13,0	5,1	0,2	1,8	6,9	.	0,1	4,3	7,8	4,6	14,5	13,8	4,8	9,8	8,8	7,7	8,5	14,5	5,2	13,5	9,0	15,3	244,4
2	Kołobrzeg	9,7	11,0	9,2	13,6	9,8	13,3	4,5	7,4	9,8	4,5	3,1	2,0	6,7	.	0,2	5,7	7,3	4,4	11,6	12,6	6,1	9,8	8,7	7,5	11,2	14,3	3,0	11,7	9,2	14,9	242,8
3	Międzyzdroje	6,7	9,3	6,5	12,9	13,5	10,8	7,4	6,4	1,1	0,7	9,3	0,9	3,0	1,0	0,2	7,6	5,9	4,7	8,8	7,2	6,0	8,4	3,1	5,0	11,4	12,9	2,7	6,5	9,7	13,5	203,1
4	Resko	9,7	10,8	8,5	11,1	8,9	13,8	5,5	9,4	10,0	6,3	7,4	4,2	6,2	0,1	0,1	5,4	6,8	6,4	10,2	12,3	5,4	12,0	7,4	8,3	12,5	13,5	4,0	10,6	8,8	14,0	249,6
5	Szczecinek	8,2	11,8	6,5	7,8	9,3	14,0	2,0	3,1	12,3	10,1	2,1	2,8	9,8	0,3	0,8	3,5	9,4	7,8	9,6	13,1	5,6	14,1	7,2	8,8	12,7	15,2	6,4	10,9	6,4	15,1	243,9
6	Chojnice	12,7	14,0	11,1	10,7	9,6	13,0	1,0	3,8	12,4	11,0	0,9	2,9	9,5	0,7	4,3	2,4	8,5	8,9	10,5	13,7	5,0	11,9	8,0	8,4	11,3	15,1	7,2	10,0	7,0	14,0	259,5
7	Hel	11,1	13,4	13,7	13,4	13,6	14,0	8,2	7,0	12,2	11,4	8,6	0,2	10,3	1,8	1,2	0,4	7,8	5,6	14,0	12,2	4,3	12,7	11,3	8,7	7,2	13,6	6,9	11,2	10,6	14,4	281,2
8	Gdynia	11,9	13,5	14,3	14,2	13,0	14,5	7,2	7,0	13,4	11,9	8,0	.	9,8	0,9	0,8	0,1	9,8	5,5	14,0	13,3	5,7	10,6	11,2	7,9	7,5	14,5	7,2	12,8	11,2	15,4	287,1
9	Świnoujście	12,3	12,5	13,3	12,6	11,5	13,9	6,7	.	11,4	11,9	7,2	.	8,3	0,9	0,3	.	7,1	6,5	13,1	12,5	2,4	13,6	11,5	7,8	7,1	14,4	6,5	11,0	6,2	14,2	256,7
10	Stare Pole	12,6	12,9	13,9	13,0	10,2	13,6	4,4	4,3	12,0	8,9	10,2	0,2	8,1	0,9	0,1	1,0	7,0	6,8	12,2	13,7	3,1	14,8	10,3	6,7	8,6	13,9	7,9	9,9	3,9	14,7	259,0
11	Radostowo	12,2	12,3	13,4	13,6	11,6	14,0	3,0	5,3	12,6	12,8	8,6	1,7	2,4	1,3	.	1,1	8,4	7,8	13,7	14,1	6,0	14,5	12,0	7,1	10,6	15,1	8,2	11,8	5,7	14,9	276,0
12	Prabuty	14,1	15,1	13,1	13,7	11,1	14,2	2,2	2,4	12,8	12,0	9,3	3,3	11,6	1,0	0,3	0,4	6,0	8,0	12,2	12,9	2,0	14,6	10,0	7,0	10,6	14,9	9,4	9,5	3,5	15,1	270,3
13	Bydgoszcz, IMiUZ	13,9	11,8	14,1	5,6	9,4	11,6	4,0	3,2	11,9	11,3	5,1	3,2	8,5	0,8	0,4	2,2	9,3	7,3	10,6	12,6	3,3	12,3	9,3	9,5	11,4	14,1	8,2	7,6	5,1	13,5	251,1
14	Suwałki	14,2	14,4	9,3	14,5	13,9	15,3	9,3	3,2	0,8	11,6	6,5	7,2	4,6	1,5	0,9	.	0,4	1,1	12,7	12,0	4,7	13,8	6,4	6,1	10,8	15,2	10,0	3,6	5,7	14,4	244,1
15	Mikołajki	9,4	11,0	9,6	12,2	14,7	15,2	8,3	3,5	1,6	11,9	5,6	2,7	6,0	3,0	0,4	0,6	3,5	3,8	14,8	13,0	3,9	15,1	6,2	8,2	11,9	14,8	10,4	4,4	2,5	15,2	243,4
16	Siebrza	13,1	13,0	11,2	13,2	14,2	14,5	6,8	4,2	0,2	11,8	10,4	3,9	5,1	.	.	.	.	.	6,2	8,0	2,7	2,6	13,8	1,7	6,9	7,5	7,8	0,2	0,9	8,8	188,7
17	Białystok	13,5	10,2	9,4	11,6	14,5	13,7	4,3	3,6	2,7	9,9	9,5	2,8	1,8	0,6	0,4	0,4	0,8	1,6	8,3	12,4	4,4	12,0	3,9	5,0	11,8	13,3	11,5	2,6	6,1	14,8	217,4
18	Gorzów Wlkp.	13,1	13,2	7,1	6,9	8,3	13,4	1,3	3,6	8,6	5,7	1,5	8,0	.	.	0,1	10,6	6,3	9,5	9,3	11,6	5,0	11,1	7,3	9,5	12,4	12,5	2,2	8,4	14,2	13,5	234,2
19	Przebędowo	13,6	13,0	6,5	6,3	8,7	6,5	2,0	2,7	10,1	8,2	.	6,1	8,6	.	0,1	.	9,5	10,5	10,6	13,5	7,1	11,9	10,4	11,0	11,7	12,9	6,8	9,0	9,9	13,2	240,4
20	Przybroda	14,1	13,6	6,5	5,7	9,2	13,4	2,1	4,2	9,1	.	7,9	6,9	8,5	.	.	8,1	11,0	10,2	12,3	13,4	7,0	13,0	10,9	10,0	13,5	12,8	5,5	8,5	13,2	13,5	264,1
21	Poznań-Ławica	10,5	10,7	6,5	6,5	8,6	11,4	2,2	3,4	7,0	7,6	.	5,5	8,4	.	0,3	6,4	8,4	11,0	9,1	.	8,5	12,2	10,9	8,1	11,6	11,6	5,4	9,4	11,6	12,2	225,0
22	Pławieka	12,1	12,3	5,4	3,8	6,0	11,2	1,3	2,8	7,9	8,7	.	3,8	6,3	.	0,4	6,5	6,8	11,4	9,4	12,4	6,5	11,7	9,6	7,9	12,0	3,9	11,4	7,9	9,5	12,4	221,0
23	Kórnik	14,1	13,9	5,7	4,2	9,2	14,0	2,6	4,7	8,8	8,7	.	4,6	8,9	0,1	0,3	6,8	7,8	12,5	8,5	15,1	8,1	12,8	10,7	8,7	14,0	11,9	4,5	8,5	11,5	14,8	256,0
24	Oborniki Śl.	13,8	12,8	5,1	5,9	9,3	8,3	3,9	1,5	3,9	8,1	.	4,1	8,9	.	11,7	11,8	9,6	12,3	5,6	13,7	11,6	12,3	10,3	10,8	13,0	7,3	11,2	10,5	12,8	14,2	264,3
25	Laskowice Oławskie	12,8	12,8	3,9	3,9	9,2	5,5	3,9	0,7	2,5	6,8	.	3,1	7,6	.	7,4	5,9	12,0	12,8	4,0	12,7	11,2	9,7	9,7	10,0	12,9	5,1	8,1	5,5	13,0	13,5	226,2
26	Ciechocinek	14,1	12,7	11,9	1,9	12,8	13,4	5,8	1,7	8,3	10,6	8,3	3,9	9,1	1,8	0,2	1,2	6,0	4,6	6,5	10,2	2,5	11,6	8,0	5,9	10,6	11,3	6,7	4,1	1,4	13,5	220,6
27	Więcławice	13,8	12,5	10,5	4,6	11,7	11,1	5,4	2,2	11,9	11,9	6,1	5,5	10,9	0,9	0,8	2,8	9,0	7,1	11,7	13,2	4,7	12,5	11,5	10,3	13,4	14,0	5,6	8,7	2,0	14,1	260,4
28	Legionowo	12,6	12,0	10,0	3,9	9,7	12,4	3,8	7,7	1,4	10,3	11,2	1,6	9,0	2,5	.	0,6	10,4	6,5	6,5	14,2	13,0	10,9	6,0	10,7	12,8	11,7	11,3	4,7	3,5	14,9	245,6
29	Warszawa-Bielany	9,6	10,0	11,8	4,0	8,9	9,0	2,5	8,1	0,7	10,0	9,5	1,9	8,0	1,7	0,2	0,9	7,5	6,7	4,0	11,5	11,2	10,5	4,8	8,9	11,5	10,3	10,2	4,1	.	14,1	212,1
30	Warszawa, Min. Kom.	10,2	1,1	11,1	4,1	10,0	8,0	2,3	7,1	0,5	9,7	8,6	1,1	6,9	2,3	.	0,9	8,7	8,7	5,2	10,5	12,2	9,4	5,3	10,8	9,1	10,1	9,8	3,8	2,1	14,0	203,6
31	Międzylesie	9,7	9,7	12,6	5,2	10,1	9,1	2,1	6,9	2,2	10,5	9,7	1,8	6,2	1,7	0,4	0,8	10,4	7,2	3,0	12,6	11,4	10,0	5,2	11,0	9,8	10,3	11,1	3,5	2,5	14,3	221,0
32	Erwinów	9,6	13,0	11,9	6,9	12,2	8,2	2,3	8,0	2,8	9,2	8,6	1,8	8,3	2,7	.	0,1	10,0	6,3	4,4	11,4	12,8	9,6	5,6	9,3	9,9	8,9	11,4	3,6	2,2	14,5	225,5
33	Świdwy	10,2	10,6	10,7	5,3	8,7	7,7	1,9	7,8	2,3	10,2	9,3	1,4	6,9	2,3	0,7	0,1	8,7	7,4	2,2	10,6	11,0	9,4	4,6	9,2	10,5	8,0	10,1	2,9	2,7	12,1	205,5
34	Topola-Błonie	11,9	12,4	10,7	6,5	10,6	12,6	4,5	2,6	5,8	10,0	5,7	3,2	8,8	2,0	0,3	1,7	10,0	9,0	4,9	12,9	9,6	8,7	8,7	8,0	12,4	8,6	6,2	4,4	4,9	12,7	230,3
35	Młochów	12,0	14,2	12,6	6,1	11,0	7,9	2,3	7,9	2,4	8,6	7,4	1,3	6,5	1,8	0,3	0,2	11,1	6,6	3,4	11,1	12,0	9,1	4,9	9,0	10,4	6,7	8,9	3,9	2,7	13,8	216,1
36	Skierniewice	11,4	11,6	13,9	5,0	8,9	10,2	3,1	4,5	4,7	8,4	9,8	2,7	8,5	4,4	0,1	0,7	9,4	9,3	3,5	12,9	12,2	10,6	7,3	9,7	12,2	7,0	10,3	5,2	5,5	13,7	236,5
37	Belsk	11,9	10,9	13,6	8,0	8,7	8,5	2,9	7,7	4,4	8,5	8,9	0,7	8,2	2,8	0,1	1,1	13,1	8,3	2,2	12,0	12,3	10,1	6,2	11,8	9,9	7,3	9,9	5,5	4,7	13,6	233,6
38	Łódź-Lublinek	11,6	11,0	11,7	2,8	10,9	11,7	3,8	4,6	3,6	7,6	6,4	2,2	5,8	0,3	.	3,1	11,9	10,9	3,1	12,3	11,5	8,5	9,2	5,3	13,7	5,2	6,1	3,6	6,6	14,2	219,2
39	Kalisz	13,0	13,1	4,3	7,2	9,9	11,2	2,6	3,9	6,0	9,0	0,5	4,2	9,7	.	0,5	6,3	9,2	12,6	5,6	14,3	9,5	11,4	10,8	9,1	12,8	8,1	6,3	7,1	11,5	13,4	242,9
40	Wieluń	13,6	13,4	4,3	1,6	11,0	7,8	2,5	4,4	2,4	8,4	0,4	2,4	9,2	0,7	3,6	4,0	13,7	13,7	3,6	15,0	12,5	9,1	7,6	7,6	13,7	6,9	6,1	4,8	12,7	14,6	231,3
41	Szepietowo	12,2	14,9	13,9	14,4	9,0	12,3	5,0	5,3	5,5	8,6	0,7	11,8	2,4	.	0,2	0,3	3,2	.	8,9	14,9	10,5	11,3	2,9	7,4	11,9	13,7	12,7	.	4,5	15,1	233,5
42	Białowieża	14,2	12,7	8,9	11,8	14,1	11,7	3,7	10,4	11,3	9,5	9,8	2,9	2,2	0,5	0,5	0,9	0,9	1,0	4,9	13,6	7,7	12,5	1,1	7,9	11,3	12,6	11,0	2,7	6,6	14,3	232,4
43	Tarespol	13,0	12,9	12,5	7,5	11,9	7,8	4,4	5,9	11,7	11,6	10,0	7,6	0,8	0,1	.	0,8	4,3	12,0	2,1	14,1	12,9	12,1	2,3	8,8	13,0	11,2	10,3	2,6	8,4	13,5	246,1
44	Sobieszyn	11,3	10,9	11,0	5,3	7,6	1,6	0,8	5,9	4,6	13,9	7,6	3,4	2,8	1,0	0,1	0,3	11,8	3,6	2,0	12,7	12,5	13,8	3,8	7,1	11,4	8,1	12,2	2,6	2,6	14,0	206,3
45	Puławy	9,4	10,1	9,1	6,1	5,2	1,6	1,6	5,6	7,0	11,4	7,2	1,6	2,9	2,0	0,3	1,9	11,9	6,7	0,2	12,0	12,9	11,4	3,7	7,2	10,2	7,3	11,3	1,5	2,0	13,0	194,3
46	Chełm Lub.	13,1	7,1	7,3	5,1	9,5	1,2	3,1	7,8	15,0	14,3	11,1	8,2	5,1	0,2	0,9	3,8	11,0	4,8	5,0	13,8	12,5	12,4	3,2	9,8	10,5	9,1	12,3	3,0	5,6	15,6	241,4
47	Szczawno Zdrój	9,4	13,0	1,9	2,9	4,8	3,5	0,7	1,2	0,4	6,3	0,4	1,5	4,2	0,8	2,8	9,4	10,9	13,1	2,4	10,1	7,3	7,4	10,9	8,2	12,8	3,6	3,7	4,7	12,5	13,0	183,8
48	Śnieżka	9,9	11,3	.	2,4	2,6	1,4	1,2	0,3	.	0,3	.	2,9	1,9	0,6	3,5	13,5	8,3	14,3	2,3	9,1	7,1	6,7	10,2	11,3	13,3	4,7	3,0	4,7	12,0	14,5	173,3
49	Opole	13,6	13,2	3,2	1,2	3,7	4,7	4,4	1,9	4,1	9,8	0,5	2,1	9,0	0,5	3,7	9,4	14,4	14,0	3,5	15,3	11,1	8,0	7,6	8,3	14,9	6,6	5,4	5,8	13,8	14,5	228,2
50	Kudowa-Zdrój	10,5	11,3	2,4	2,4	6,4	3,7	4,7	1,6	2,4	2,0	0,5	6,0	3,9	1,1	3,7	11,9	12,9	12,9	0,7	12,5	6,0	9,5	12,6	10,0	13,4	5,1	9,7	2,4	12,3	13,9	206,2
51	Polanica-Zdrój	9,7	13,1	1,5	4,0	6,0	3,4	5,5	0,7	0,6	3,4	.	5,0	4,3	3,1	3,7	13,2	12,4	12,8	1,4	8,8	10,8	9,5	10,2	9,2	13,1	4,9	6,5	4,3	11,8	12,7	203,6
52	Skroniów	13,2	8,9	8,5	4,8	5,9	5,3	5,2	4,6	4,1	7,6	6,6	.	6,4	1,9	2,2	12,7	13,8	11,6	6,3	13,7	13,0	11,0	9,1	7,7	13,3	6,5	9,9	4,3	11,7	14,1	243,9
53	Świerklaniec	13,6	10,7	7,0	4,0	7,5	6,8	3,1	5,4	1,8	4,3	0,3	0,8	6,4	0,7	6,6	12,6	12,8	12,0	4,9	8,9	12,4	7,5	8,8	8,9	13,4	5,6	7,2	4,5	10,6	13,1	222,2
54	Kraków, Obs. Astr.	13,6	6,9	10,1	5,3	4,1	4,2	5,1	3,1	1,9	5,5	4,9	0,5	6,5	4,8	4,4	12,6	13,3	12,5	8,3	9,3	13,3	12,6	8,8	9,4	13,6	7,5	9,8	4,6	12,2	13,9	242,6
55	Cieszyn	9,8	8,3	2,6	0,9	4,3	1,2	2,7	1,5	4,2	4,2	.	0,5	4,9	1,9	0,3	11,5	13,0	12,1	6,6	10,5	12,3	7,5	6,6	6,8	14,2	8,1	8,3	6,1	10,0	12,5	193,4
56	Istebna-Kubalonka	10,1	8,2	3,2	1,8	5,2	1,6	3,5	4,9	5,0	5,9	.	1,5	7,6	2,0	0,6	12,3	12,7	11,5	7,5	12,5	11,4	10,3	8,1	10,5	13,4	7,7	10,0	3,9	13,6	13,9	214,4
57	Rabka	10,2	5,3	4,7	3,9	2,8	3,5	4,8	3,9	4,4	7,0	1,0	0,1	7,6	2,0	1,3	12,0	13,2	13,2	8,9	6,7	11,8	11,6	5,8	9,6	13,3	8,7	10,9	1,6	10,1	11,2	211,1
58	Jabłonka	8,8	6,0	4,4	3,6	3,9	3,2	5,8	7,8	4,2	3,5	1,8	.	7,8	1,7	1,2	9,6	11,6	11,5	8,1	8,2	11,5	10,4	5,7	9,3	12,6	8,6	9,2	.	9,3	9,6	198,9
59	Krynica	7,9	7,8	2,1	4,1	1,5	4,4	3,4	6,8	2,9	7,2	2,7	.	8,0	3,3	1,8	8,0	9,6	9,4	7,3	5,7	8,7	10,1	8,2	8,9	11,4	5,8	11,0	2,0	6,8	9,1	185,5
60	Krynica-Góra Park.	9,8	7,8	2,5	4,5	1,6	4,6	4,3	7,1	4,2	9,1	3,7	0,2	8,5	2,9	1,7	7,1	11,3	10,5	8,5	6,0	10,7	11,8	7,0	9,5	13,4	8,3	11,3	1,7	7,6	9,1	206,3
61	Muszyna	8,3	6,7	3,3	4,8	0,8	3,5	3,7	8,6	3,3	7,2	2,5	0,4	7,2	3,0	4,4	8,4	11,2	11,1	9,9	8,9	10,5	12,2	8,3	8,3	13,6	6,2	11,3	.	7,6	9,4	208,8
62	Zakopane	10,1	7,3	2,5	1,5	1,4	1,4	1,6	5,1	5,6	7,2	1,3	.	7,4	3,4	0,3	13,4	12,5	14,8	11,1	2,3	12,3	11,3	5,9	11,6	14,1	9,1	12,2	0,4	10,1	14,0	211,2
63	Gubałówka	8,9	5,2	3,4	2,3	2,6	2,0	2,6	4,3	3,5	5,5	1,7	.	5,7	3,2	0,7	10,0	9,5	10,2	9,0	3,7	9,9	9,8	5,6	9,0	10,4	7,6	10,2	0,4	8,1	10,4	175,4
64	Hala Gąsienicowa	8,5	6,1	1,7	1,1	0,2	1,5	0,5	5,4	3,4	5,0	0,4	0,3	7,0	1,0	0,1	12,4	7,4	10,5	10,3	0,5	7,6	8,4	1,7	10,6	12,4	9,8	11,4	.	6,7	10,1	162,0
65	Kasprowy Wierch	7,9	6,3	0,8	0,4	0,1	2,2	0,4	5,7	3,6	5,0	0,3	1,2	7,2	1,4	0,1	12,0	8,4	12,2	9,9	2,5	10,0	10,5	2,2	12,1	14,6	10,3	12,0	.	4,3	10,5	174,3
66	Werbkowice	13,2	8,0	8,4	1,6	4,2	0,2	4,6	10,2	14,5	11,7	9,8	5,7	6,3	1,2	1,9	6,7	12,5	6,1	8,2	12,9	13,9	13,6	3,8	10,6	12,0	10,0	13,6	3,3	7,6	12,3	248,6
67	Zdunek	14,2	9,2	9,6	4,0	7,1	1,3	3,5	3,2	11,4	11,0	4,4	2,2	6,3	2,0	3,5	10,3	14,2	10,1	6,5	13,9	14,3	11,1	6,3	9,5	14,2	8,7	11,9	3,0	10,0	13,8	250,7
68	Iwonicz	10,8	7,5	1,4	5,3	3,0	1,0	3,5	9,2	2,7	7,6	0,8	1,0	8,0	0,4	.	9,7	12,1	7,6	9,6	9,0	12,3	11,3	3,7	8,1	12,2	9,1	12,8	0,4	6,5	6,1	192,7
69	Leśko	12,2	9,3	0,8	6,3	5,8	2,0	2,0	4,4	8,0	8,1	4,2	1,4	6,0	.	2,5	11,8	13,8	9,6	12,1	10,8	13,7	12,3	4,3	8,0	13,1	6,9	13,1	1,6	5,0	6,5	211,6

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	15,2	13,9	10,3	0,8	7,1	8,4	6,2	1,5	.	4,5	9,5	8,1	6,2	.	8,7	0,9	8,3	6,4	6,4	2,9	6,2	0,2	1,6	3,9	4,8	.	2,0	0,2	2,3	3,7	.	150,2
2	Kołobrzeg	14,8	13,6	7,3	0,7	4,4	5,4	3,3	0,7	2,7	4,5	5,7	10,2	4,4	.	10,4	6,0	.	6,1	7,1	2,7	1,7	0,2	2,7	5,6	5,4	1,2	0,9	0,2	1,6	.	.	129,5
3	Międzyzdroje	.	12,2	5,5	4,2	2,9	2,1	3,2	0,5	3,0	2,0	3,6	7,2	1,4	2,8	6,9	4,4	2,8	1,5	6,2	2,9	3,8	1,6	.	2,3	2,6	0,6	3,5	0,4	2,2	2,2	.	94,3
4	Resko	14,3	13,6	7,5	0,3	6,9	4,4	3,5	1,9	1,5	2,9	7,5	7,9	4,4	1,3	9,2	4,0	1,9	4,9	9,3	2,4	4,2	0,3	1,1	2,1	2,7	0,2	1,2	0,3	2,3	.	.	124,0
5	Szczecinek	13,6	14,2	7,7	1,8	3,7	1,6	1,7	0,8	.	5,5	7,0	7,3	5,5	0,2	9,2	1,7	3,5	0,6	9,6	4,6	1,5	0,7	0,3	0,5	0,7	0,7	0,6	.	1,0	0,5	.	106,3
6	Chojnice	14,9	15,4	9,8	2,8	3,8	0,9	1,9	1,3	.	2,9	8,5	5,8	5,8	0,2	7,6	1,4	4,5	0,7	6,3	2,4	2,2	1,5	1,2	0,6	0,3	0,7	0,6	0,1	2,9	2,1	.	109,1
7	Hel	15,6	13,3	9,9	4,7	5,9	2,8	4,5	2,5	0,2	3,6	9,2	5,5	6,4	0,8	6,3	0,2	8,9	1,5	3,8	4,6	2,4	4,9	1,4	7,9	2,0	.	0,6	.	2,5	0,8	1,2	131,9
8	Gdynia	14,0	13,9	11,3	1,0	7,3	4,7	5,5	2,0	0,2	4,5	8,5	4,9	6,1	1,1	6,7	.	8,9	0,5	3,4	2,7	2,7	4,6	0,8	7,3	1,3	.	1,2	.	3,6	0,9	0,7	130,3
9	Świnoujście	14,3	13,7	10,3	5,3	4,7	1,4	2,3	2,0	0,3	7,2	.	6,0	5,7	0,5	5,6	.	8,1	.	3,9	3,5	0,8	4,3	1,2	5,1	0,7	.	0,8	.	2,2	1,1	1,4	112,4
10	Stare Pole	13,4	13,8	11,3	6,6	6,2	2,8	3,7	1,8	2,9	3,9	6,8	6,9	6,7	0,3	4,8	0,6	5,4	1,1	5,9	7,4	1,0	3,9	0,9	3,4	0,3	.	1,4	.	2,4	0,7	2,4	128,7
11	Radosłowo	15,1	14,4	11,0	5,8	8,0	1,1	3,0	0,7	1,7	8,3	9,2	9,4	6,2	.	6,7	0,5	5,7	1,0	4,3	5,4	0,6	3,0	2,2	3,0	0,6	.	1,1	.	2,9	.	1,0	131,9
12	Prabuty	15,0	15,2	12,2	5,7	.	6,0	3,1	1,1	3,4	4,1	7,4	8,4	7,2	.	5,4	0,5	8,1	0,8	3,5	7,9	1,1	2,7	1,3	0,8	0,4	.	1,7	.	1,8	0,1	0,2	125,1
13	Rydzewo, Ełk	15,1	15,0	10,6	4,6	6,9	0,5	3,1	2,3	0,8	2,9	7,0	7,1	6,3	0,2	7,7	0,7	7,0	2,6	2,7	4,1	0,9	3,9	.	3,0	.	0,1	2,4	.	3,6	0,9	.	122,0
14	Suwałki	11,4	9,0	12,2	11,0	4,9	8,4	6,2	7,6	7,3	2,3	5,4	3,5	7,0	1,9	10,5	6,7	8,8	4,2	5,7	11,5	7,7	3,1	0,4	6,0	1,4	.	0,9	.	1,7	.	3,7	170,4
15	Mikołajki	8,0	15,5	12,0	7,5	4,9	7,7	8,4	4,2	6,3	5,1	7,7	6,4	7,0	0,5	5,5	1,0	10,4	0,7	3,4	6,1	4,2	1,0	0,8	3,0	1,8	.	1,3	.	1,8	.	0,9	143,1
16	Ełk	1,3	7,7	9,1	.	5,8	9,8	7,9	6,0	9,2	.	8,0	3,5	8,2	2,0	7,6	3,5	9,4	3,7	7,8	10,3	5,3	1,5	0,9	4,3	1,3	0,1	3,1	0,1	0,6	.	2,5	140,5
17	Białystok	12,1	15,0	14,6	4,2	4,2	11,0	7,2	4,2	10,2	2,6	6,7	2,0	7,9	1,9	4,4	3,5	9,2	2,4	8,0	8,1	5,9	1,1	0,2	4,7	3,3	1,5	0,3	1,3	0,3	.	1,9	159,9
18	Gorzów Wlkp.	14,7	13,8	7,1	.	5,5	.	2,9	5,6	1,5	1,8	1,2	9,5	2,4	2,4	9,3	5,9	1,0	1,6	6,0	1,6	0,3	0,3	0,2	0,1	0,7	0,2	0,7	0,6	1,1	3,8	.	101,8
19	Przebędowo	15,0	14,6	11,2	2,2	3,7	2,6	1,6	2,5	0,7	4,6	6,4	10,4	6,7	3,0	9,6	2,6	4,1	3,8	2,5	5,1	0,3	1,3	0,5	2,0	.	0,5	1,7	.	.	.	.	119,2
20	Przybroda	14,3	14,1	10,1	2,2	3,6	4,4	1,3	3,4	1,8	5,3	5,5	11,5	5,5	2,8	10,3	2,4	3,8	3,5	1,5	4,4	0,9	0,6	0,3	.	0,8	1,2	3,1	0,3	4,2	0,5	.	123,4
21	Poznań-Ławica	12,0	12,1	9,9	2,8	5,6	3,1	1,6	3,3	1,7	4,9	4,8	9,9	6,0	2,7	8,5	3,0	3,0	2,1	2,5	8,7	0,6	0,4	0,2	.	0,4	0,8	1,4	0,2	4,1	.	.	112,3
22	Plewiska	12,3	12,1	9,4	1,9	5,0	2,4	1,4	3,8	1,7	2,5	4,5	11,4	5,1	2,9	8,3	2,1	1,7	3,4	2,5	4,5	0,5	0,7	0,3	0,1	0,5	0,6	1,9	0,2	3,1	.	.	106,8
23	Kórnik	14,7	14,8	11,4	0,8	6,0	2,7	1,8	2,5	1,3	4,6	4,9	10,9	5,6	3,4	8,3	2,2	3,7	3,2	1,5	6,9	0,3	0,8	0,6	.	0,2	1,0	3,4	0,2	2,9	.	.	120,6
24	Oborniki Śl.	13,8	13,9	12,4	3,3	7,7	3,3	7,7	11,4	3,1	4,9	2,7	11,4	4,5	10,9	5,6	6,9	5,3	2,9	1,1	3,0	0,7	0,4	0,7	.	.	4,6	2,4	.	3,8	.	.	148,4
25	Leszkowice Ożarowice	14,0	14,3	13,1	7,1	8,6	2,3	4,3	9,4	1,5	4,5	4,8	11,3	5,9	4,6	7,8	7,1	4,0	2,7	2,8	2,4	0,1	1,1	3,8	1,2	.	6,4	2,1	.	3,3	.	.	150,5
26	Ciechocinek	13,1	14,5	9,0	3,0	5,2	1,9	2,2	1,5	2,3	3,9	5,8	6,2	4,8	0,5	6,4	0,9	5,8	1,5	4,0	5,4	0,7	1,0	0,2	4,3	.	.	2,7	.	4,0	.	.	110,8
27	Więcławice	13,7	14,6	11,8	3,8	7,1	1,5	2,2	1,8	2,3	4,5	9,3	8,7	7,3	0,8	6,4	2,4	6,3	2,8	5,7	4,0	1,9	3,2	0,4	7,8	.	0,4	3,5	0,3	3,0	0,4	.	137,9
28	Legionowo	15,3	15,3	14,5	4,2	5,1	5,7	3,7	6,5	6,4	5,3	8,9	7,9	9,0	2,9	4,5	0,3	6,4	2,1	6,6	7,9	1,5	5,4	0,1	2,4	1,6	.	3,4	0,2	2,4	.	0,9	156,4
29	Warszawa-Bielany	14,6	14,7	13,9	1,9	3,5	4,7	4,2	6,4	5,9	3,3	8,0	7,9	8,0	3,0	4,1	0,4	5,7	1,1	5,4	7,9	1,6	4,5	.	2,2	1,2	0,2	2,7	0,2	1,6	.	0,7	139,5
30	Warszawa, Min.Kom.	11,7	14,3	13,0	2,7	5,0	4,3	4,3	9,3	1,8	5,0	8,6	8,5	7,7	3,5	4,9	0,2	5,8	1,0	6,2	8,0	1,1	4,1	.	2,9	1,6	.	4,5	.	1,0	.	1,0	142,0
31	Międzylesie	14,6	14,4	14,4	3,7	3,5	5,3	3,8	8,7	7,0	4,9	8,3	8,5	9,6	3,5	5,4	0,2	6,6	0,8	6,5	8,2	6,4	.	0,1	3,3	1,8	0,2	5,6	0,4	0,8	.	1,8	158,3
32	Krwinów	15,2	15,4	14,4	1,0	5,1	2,7	4,7	10,1	5,8	4,8	7,7	8,5	9,7	3,9	5,8	1,4	5,7	1,4	5,8	6,4	0,3	4,3	0,1	3,7	0,8	0,2	3,0	0,2	1,2	.	0,1	149,4
33	Świder	12,6	13,1	12,4	3,2	3,7	4,3	3,6	8,2	5,5	2,8	6,7	7,2	9,7	4,1	4,6	0,1	6,8	1,5	4,2	6,5	1,7	3,5	0,2	2,9	1,5	0,1	3,5	0,1	0,3	.	1,7	136,3
34	Topola-Słonie	12,8	13,0	12,7	1,7	5,5	1,6	2,2	8,9	2,7	3,9	4,6	9,6	7,1	2,1	5,4	2,9	5,2	3,7	2,6	5,4	0,4	3,2	0,4	0,6	0,1	0,6	3,1	.	3,2	.	.	125,2
35	Mrochów	12,7	15,6	14,6	1,0	5,3	4,1	4,2	9,2	5,4	3,4	7,7	8,0	9,0	5,3	5,7	0,9	5,8	1,1	7,0	6,3	0,6	3,3	0,1	3,1	0,8	0,1	4,2	0,2	1,2	.	0,3	145,9
36	Skierniewice	15,2	15,2	12,3	3,0	5,0	4,1	5,2	9,4	5,8	4,4	8,1	9,9	6,8	5,2	6,2	3,0	6,2	1,7	2,4	5,6	0,5	3,8	0,6	2,5	0,5	0,7	3,2	.	2,1	.	.	148,6
37	Belsk	14,2	15,1	13,9	6,5	4,0	4,5	3,8	9,3	5,4	3,4	8,5	9,9	9,1	6,3	4,2	2,2	6,8	1,5	5,6	6,8	0,2	3,1	1,5	3,6	1,0	0,3	4,8	0,4	0,3	.	0,2	156,4
38	Łódź-Lublinek	14,4	14,2	13,3	3,2	6,4	1,6	4,4	8,4	2,5	5,4	4,8	9,5	9,5	4,1	6,4	4,0	5,9	4,8	1,1	2,6	0,2	1,2	0,4	2,2	0,5	0,3	2,4	0,2	3,2	.	.	137,1
39	Kalisz	14,6	14,2	12,8	3,0	8,9	4,7	1,9	7,7	1,1	5,5	5,8	11,9	6,7	4,8	7,2	5,9	6,8	4,7	2,7	3,2	.	1,3	1,0	.	0,1	0,7	4,8	.	4,6	.	.	146,6
40	Wieluń	14,6	14,7	13,7	4,3	11,1	1,8	2,7	10,2	1,7	6,0	6,7	12,2	7,0	8,3	6,3	5,1	4,4	2,7	1,6	3,5	0,1	1,3	4,3	1,0	.	3,8	3,1	0,1	4,6	.	.	157,1
41	Szepietowo	14,7	4,4	14,3	5,0	3,8	9,3	7,0	5,3	11,3	4,8	6,9	1,6	5,0	10,0	2,7	.	10,7	0,8	10,6	10,0	6,8	2,7	0,3	3,5	3,1	.	1,7	1,2	.	.	4,1	161,6
42	Białowieża	14,3	14,9	15,1	7,3	6,0	10,0	7,8	4,5	11,7	3,9	7,7	3,5	9,2	3,7	8,5	7,2	8,0	4,7	8,7	9,3	6,7	.	1,5	4,0	4,8	0,9	1,5	1,6	.	.	3,7	190,7
43	Terespol	15,0	14,6	15,0	9,9	4,1	10,3	6,6	7,3	10,5	5,8	7,3	5,0	9,3	3,4	5,8	6,5	4,4	6,4	9,1	7,0	5,8	2,1	2,4	2,3	4,1	1,1	5,0	3,5	.	.	4,0	193,6
44	Sobieszyn	13,3	14,4	14,6	8,0	3,1	6,7	5,2	9,1	6,7	6,2	6,0	6,5	9,1	3,1	4,3	0,9	4,9	1,0	4,2	3,6	5,7	1,9	3,8	1,5	3,9	0,9	4,7	2,9	.	.	1,1	157,3
45	Puławy	12,5	13,7	13,2	6,5	3,9	5,2	2,3	7,3	5,6	3,6	6,2	7,8	8,1	2,7	3,3	3,1	5,4	2,4	3,8	3,0	3,8	2,5	6,0	0,9	2,3	1,3	4,3	2,1	.	.	1,6	144,4
46	Chełm Lub.	14,6	14,8	15,2	9,9	3,6	10,0	6,9	9,3	7,7	4,3	10,4	5,8	11,9	1,4	9,9	9,3	2,9	8,8	6,5	6,3	6,6	2,3	6,5	3,1	2,6	0,9	4,5	3,8	0,4	0,1	2,5	202,8
47	Szczawno-Zdrój	13,0	13,0	11,7	6,1	2,1	1,9	1,9	5,3	1,4	4,8	2,3	10,2	2,2	4,3	8,8	7,5	2,4	1,2	0,6	1,3	0,5	0,4	1,1	1,1	0,4	9,3	1,0	0,4	3,4	.	2,4	122,0
48	Śmietka	12,7	8,3	13,4	4,6	3,7	0,5	1,8	5,1	2,2	5,4	2,0	11,0	.	3,2	6,4	7,7	.	0,8	0,9	2,7	.	1,5	2,3	0,6	0,1	9,6	0,6	.	1,8	.	0,6	109,3
49	Opole	14,2	14,7	13,2	5,8	5,8	2,1	3,8	12,0	1,1	5,1	5,1	12,5	.	12,2	5,2	8,1	5,4	1,2	2,3	3,5	0,3	.	2,6	1,3	.	7,8	1,7	.	2,8	.	.	149,8
50	Kudowa-Zdrój	12,0	13,6	13,4	8,1	4,8	1,1	5,4	11,8	1,5	6,7	6,1	11,7	2,4	4,3	7,6	7,2	2,1	1,9	3,9	3,7	0,1	2,3	1,1	2,2	1,7	10,8	1,7	.	2,2	.	2,2	153,6
51	Polanica-Zdrój	12,9	13,3	12,8	8,4	7,1	3,5	5,8	11,9	2,1	6,3	5,9	10,3	4,2	5,6	6,2	8,7	2,6	2,3	3,0	3,2	1,1	3,2	1,9	1,0	0,9	10,5	1,6	0,8	1,8	.	2,8	160,9
52	Skroniów	13,8	14,7	13,7	8,0	.	2,4	4,9	10,4	3,4	6,1	6,9	5,3	10,2	5,8	5,9	5,7	6,4	4,0	1,8	0,7	2,6	2,7	3,7	2,5	.	5,0	4,7	.	.	.	.	151,3
53	Świerklaniec	12,5	11,8	11,0	6,4	7,4	3,0	2,7	11,6	2,9	6,2	7,2	11,5	7,4	9,5	7,6	6,9	7,8	3,5	3,5	1,5	1,6	0,3	3,9	1,8	.	8,2	3,8	1,6	1,9	.	.	165,0
54	Kraków, Obs.Astr.	13,3	14,1	13,3	8,3	2,0	4,7	3,6	9,9	3,6	6,2	9,3	10,8	10,5	7,9	8,1	6,5	6,7	7,3	6,6	0,8	3,0	1,7	4,0	4,9	.	11,6	7,3	2,6	.	.	0,7	189,3
55	Cieszyn	11,6	13,6	13,3	6,7	2,2	2,9	3,0	9,9	2,9	8,5	5,6	7,2	6,6	7,5	5,9	3,9	6,0	4,0	8,0	0,1	2,1	2,6	4,0	1,3	.	10,0	6,6	1,8	.	.	0,3	154,1
56	Istebna-Kubalonka	12,8	13,9	11,7	7,4	4,6	3,4	3,8	5,2	4,3	1,2	8,6	11,6	7,8	7,9	8,8	4,8	7,9	6,9	5,4	.	1,6	2,9	5,2	0,2	4,3	11,6	8,1	3,3	.	.	.	175,2
57	Rabka	12,9	13,7	13,2	9,6	0,2	5,4	5,0	8,5	5,7	3,9	4,4	12,3	9,4	6,4	4,9	5,5	8,8	7,3	4,3	.	1,8	1,4	3,7	0,8	1,5	7,5	11,6	1,1	.	.	0,5	171,3
58	Jabłonka	10,4	11,0	11,6	8,8	0,5	5,5	6,3	3,4	6,2	5,2	8,2	9,6	.	10,2	4,8	6,0	8,5	7,0	8,0	.	3,1	2,0	3,3	.	4,4	10,3	5,1	2,5	.	.	0,1	162,2
59	Krynica	12,1	12,5	12,1	7,5	1,7	8,7	1,1	7,5	4,2	3,6	5,4	8,0	8,4	5,2	5,5	7,7	5,3	5,9	1,8	.	5,7	2,8	3,7	0,2	2,4	9,4	5,8	4,2	.	.	0,9	159,3
60	Krynica-Górn Park	14,1	14,6	14,2	9,0	1,7	8,9	1,8	10,0	5,6	4,1	6,2	7,2	9,8	4,8	5,0	7,1	4,9	6,6	2,0	0,2	5,6	2,2	4,2	0,2	3,1	8,5	7,1	5,1	0,2	.	0,5	178,7
61	Muszyna	12,4	12,5	13,4	8,4	0,8	9,0	3,8	9,4	.	5,7	5,8	7,6	9,4	4,6	5,1	8,5	5,0	6,4	2,8	0,1	5,9	2,2	4,3	.	0,9	9,5	6,6	4,7	.	.	0,7	163,5
62	Zakopane	14,6	14,5	14,5	8,6	0,5	10,1	4,9	3,7	4,9	6,2	11,3	4,0	10,7	7,7	2,8	11,0	8,1	6,0	1,8	.	2,5	6,1	5,1	0,6	.	10,7	9,3	3,2	.	.	1,1	184,5
63	Gubałówka	10,5	10,7	10,5	8,3	0,1	8,5	5,3	3,9	4,3	6,2	9,3	4,8	10,0	6,8	5,0	10,0	7,7	7,7	2,1	.	3,8	5,5	3,4	0,4	.	8,4	8,1	4,3	.	.	1,6	167,2
64	Hala Gąsienicowa	12,7	12,6	12,6	7,2	0,7	5,2	3,4	2,2	3,4	3,2	7,7	3,5	6,0	5,6	4,5	8,0	5,6	05,0	1,0	.	1,5	1,8	3,1	.	.	7,2	8,1	2,5	.	.	0,2	134,5
65	Kasprowy Wierch	13,0	15,6	15,4	9,1	0,5	4,3	4,0	2,1	3,8	2,1	9,5	4,1	2,1	6,8	2,9	8,8	5,3	3,5	2,0	.	1,5	1,0	4,6	.	3,7	9,0	8,6	3,8	.	.	0,3	149,4
66	Werbkowice	13,3	14,4	14,6	10,9	2,8	9,7	5,9	10,7	8,5	4,6	10,9	3,9	11,3	0,9	11,5	9,6	2,1	9,3	7,2	5,4	2,6	2,7	7,7	2,0	4,7	1,6	4,9	1,4	1,8	.	3,2	200,1
67	Zdunów	14,4	15,1	14,3	9,9	2,7	7,1	3,5	10,4	6,9	5,0	8,9	6,4	11,3	3,5	5,1	7,4	5,8	7,7	6,1	2,4	3,8	0,8	5,2	1,3	0,2	4,0	4,1	2,1	.	.	2,5	177,3
68	Iwanice	12,2	12,8	12,7	10,5	1,0	7,8	1,7	9,2	5,5	4,6	6,5	6,9	12,8	3,3	6,0	4,3	3,3	10,1	3,7	0,2	5,2	1,7	4,0	0,5	0,3	6,9	8,2	3,8	.	.	2,7	168,6
69	Leszno	12,3	14,8	14,7	11,8	0,3	8,0	10,2	9,1	7,1	3,7	6,3	9,4	13,5	3,8	7,3	9,2	6,0	9,9	4,7	0,3	9,1	1,9	7,5	0,5	1,8	6,8	10,0	4,9	0,1	.	2,6	204,0

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	0,3	0,7	2,2	0,1	7,1	8,4	0,3	6,4	11,0	3,0	0,9	6,3	8,1	0,6	1,3	3,1	5,4	4,2	0,3	6,3	.	0,5	4,1	2,0	10,4	.	7,7	2,7	1,1	8,2	11,4	128,1
2	Kołobrzeg	0,1	0,5	3,9	.	6,3	8,4	1,0	5,3	10,6	1,6	0,1	4,5	9,9	1,6	1,6	4,1	6,1	8,3	.	6,5	.	1,8	7,6	3,3	11,3	.	9,2	4,7	9,0	11,8	11,9	151,0
3	Międzyzdroje	4,6	3,6	.	.	4,8	4,6	2,6	4,0	7,8	2,4	.	5,2	9,6	0,8	0,7	3,1	2,6	7,1	0,5	5,2	0,2	1,5	2,0	1,4	11,3	0,1	6,7	8,1	10,1	11,7	9,5	131,8
4	Resko	2,9	1,0	2,9	.	4,0	8,4	1,8	6,0	10,2	3,2	.	4,1	8,7	0,8	1,2	2,4	2,9	7,3	1,0	5,3	.	3,0	4,4	2,0	10,7	.	8,6	5,4	10,1	11,2	11,1	140,6
5	Szczecinek	1,7	4,3	3,0	.	7,1	11,2	1,2	7,1	12,2	2,7	0,9	5,0	9,8	1,5	.	2,4	1,4	7,8	0,3	5,3	.	4,0	4,9	4,1	10,7	.	8,9	4,2	9,3	10,8	12,5	187,3
6	Chojnice	0,8	4,9	3,5	0,3	5,3	10,2	0,3	6,4	9,5	0,9	.	3,0	7,2	2,7	.	2,4	1,4	7,7	1,2	5,2	.	1,7	4,2	3,7	9,4	.	7,1	5,4	9,0	5,8	10,8	130,0
7	Hel	0,5	6,3	.	0,4	6,5	9,6	0,3	7,1	9,0	6,6	0,4	2,0	10,3	1,6	0,1	3,2	4,7	8,9	2,0	9,3	0,8	0,7	3,4	5,5	8,5	0,1	6,7	4,5	6,6	9,0	8,3	142,9
8	Gdynia	1,8	4,5	0,6	0,7	7,5	10,4	0,4	7,7	9,5	8,0	0,3	1,1	10,5	2,0	0,7	1,0	2,3	0,7	1,8	8,5	1,0	0,9	5,4	4,8	9,4	.	7,8	6,7	8,9	8,1	9,0	141,7
9	Świbno	0,7	6,2	0,2	0,8	7,6	8,6	.	8,8	9,6	6,2	0,3	2,6	9,3	3,0	0,2	4,2	5,5	5,2	2,2	7,7	1,4	2,3	4,3	3,8	7,9	.	7,7	4,9	7,1	8,3	7,3	143,9
10	Stare Pole	1,2	6,3	0,3	2,3	9,1	7,7	.	8,1	8,1	5,9	0,7	1,2	10,0	5,0	0,2	3,9	4,8	3,3	1,4	7,1	.	0,9	3,1	2,8	8,0	.	6,9	5,5	7,4	8,0	9,3	138,5
11	Radostowo	1,7	6,5	1,3	1,2	10,8	8,5	.	8,2	9,6	4,5	0,2	2,0	8,9	2,7	0,2	4,0	5,5	4,6	0,4	5,8	0,1	1,4	2,9	2,3	9,9	.	7,2	4,9	6,9	7,1	8,7	138,0
12	Prabuty	0,4	7,4	.	1,1	6,4	8,4	.	8,1	8,0	3,9	.	1,3	6,9	4,2	.	2,5	3,7	2,4	1,2	4,2	.	.	2,2	2,1	7,7	.	6,1	6,7	3,9	8,1	9,9	116,8
13	Bydgoszcz, IMiUZ	0,4	6,8	3,8	1,0	8,1	10,4	0,3	7,5	7,1	.	1,0	1,6	4,7	2,5	0,1	2,7	4,6	4,8	0,8	3,2	0,3	0,9	3,0	4,2	6,3	.	9,0	6,7	11,1	6,2	10,4	129,5
14	Suwałki	0,1	11,0	3,9	6,1	6,6	6,3	1,4	4,1	6,2	8,8	1,7	3,4	4,7	6,6	1,9	5,3	2,9	9,6	3,7	2,8	3,8	0,7	1,4	4,9	4,7	7,4	3,9	1,5	4,5	12,1	11,1	151,1
15	Mikołajki	.	9,4	0,3	6,0	7,6	9,5	.	7,9	8,4	4,9	3,0	2,3	4,5	8,3	1,2	2,7	3,4	8,8	2,8	5,1	2,5	1,5	2,6	5,7	5,2	3,1	6,4	2,5	4,7	10,4	10,4	149,1
16	Biebrza	0,3	10,5	3,3	6,3	9,2	9,9	0,7	9,9	10,4	4,9	0,6	1,8	4,5	9,4	0,8	3,6	5,8	7,9	2,8	1,6	2,6	1,7	1,2	1,6	3,0	6,2	5,3	1,9	4,4	9,1	9,9	151,1
17	Białystok	0,4	8,3	1,9	5,7	6,5	10,1	5,9	8,0	7,8	5,5	0,7	1,1	0,8	7,6	3,9	1,9	3,5	7,5	1,3	1,8	.	4,2	1,7	3,1	0,4	8,3	2,6	2,9	2,2	9,5	8,6	133,3
18	Gorzów Wlkp.	6,9	0,3	5,3	.	5,3	10,2	1,8	4,2	6,3	2,7	1,6	3,0	5,5	3,0	0,2	1,8	7,7	4,8	1,3	6,6	0,5	4,0	3,6	1,2	4,6	1,2	8,9	10,4	10,5	11,0	11,9	146,3
19	Przebędowo	3,7	4,6	4,9	0,3	6,8	11,4	1,3	8,4	7,1	2,2	.	2,4	5,9	3,8	.	1,6	7,8	4,6	2,1	3,7	0,3	1,1	3,9	3,2	5,4	1,7	9,0	9,7	7,5	11,3	10,7	146,4
20	Przybroda	5,4	3,5	5,5	0,3	8,1	11,1	0,6	8,1	6,4	3,8	0,3	1,3	4,2	5,0	0,2	2,3	7,8	6,4	2,2	3,5	0,4	1,3	3,6	3,2	5,1	2,3	9,2	10,0	11,2	8,5	11,8	152,4
21	Poznań-Ławica	5,2	4,5	0,2	0,1	7,1	10,2	0,5	7,0	7,0	3,5	.	1,2	4,6	4,7	.	1,9	6,8	6,7	1,5	4,6	0,3	2,2	3,6	3,4	4,9	1,5	8,7	8,5	9,7	6,8	10,9	138,0
22	Plewiska	5,7	3,7	4,6	0,3	7,7	10,2	0,4	6,6	6,4	2,1	.	1,1	1,8	1,9	0,2	1,5	5,7	6,7	1,6	3,6	0,2	1,4	3,6	1,7	3,7	2,0	10,2	9,8	10,6	7,4	11,4	133,8
23	Kórnik	5,3	4,9	5,5	1,0	5,9	12,5	0,5	8,3	7,3	4,5	.	0,8	1,1	2,2	0,6	3,0	3,7	4,5	2,0	4,1	0,1	1,5	2,5	4,0	2,7	1,2	9,5	7,8	9,5	4,5	9,1	130,1
24	Oborniki Śl.	10,9	4,6	5,7	2,7	8,5	11,6	1,3	8,4	5,3	10,5	.	0,3	3,0	5,6	1,4	2,5	2,9	5,6	1,1	1,4	1,5	0,9	2,3	1,1	1,3	4,3	8,5	7,7	11,7	7,8	12,2	152,6
25	Laskowice Oławskie	10,2	6,2	3,2	3,8	8,2	11,5	1,1	4,4	3,5	9,5	0,1	0,1	1,2	4,6	1,8	3,7	5,5	1,5	2,2	3,6	1,9	2,1	2,8	0,9	2,9	4,1	9,7	7,9	10,9	8,1	11,5	148,7
26	Ciechocinek	.	7,2	1,9	2,5	5,3	11,6	0,1	9,0	6,3	3,5	0,3	1,0	1,6	2,8	0,4	3,6	5,5	3,4	0,5	1,8	0,1	0,6	1,9	2,2	2,8	.	5,2	5,5	5,5	7,3	8,4	107,8
27	Więcławice	0,3	7,0	3,3	0,7	8,3	11,3	0,7	9,7	8,8	3,7	.	1,0	3,7	3,7	0,9	4,3	8,2	4,2	2,2	5,1	0,2	1,8	2,8	4,6	5,0	.	9,5	8,3	10,6	10,9	10,8	149,6
28	Legionowo	.	11,5	0,7	6,3	6,2	11,7	5,0	10,2	11,0	5,4	0,4	2,6	0,8	7,8	2,4	1,6	1,7	6,2	1,8	2,9	.	4,9	3,0	3,4	1,7	.	10,4	7,4	4,3	9,4	11,7	152,4
29	Warszawa-Bielany	.	12,5	0,7	7,2	5,7	11,8	4,5	9,4	10,0	4,5	0,2	2,4	0,1	7,1	2,1	1,6	1,0	5,7	1,7	2,0	0,1	4,3	3,1	2,4	0,7	.	8,7	6,5	4,1	8,8	11,6	140,3
30	Warszawa, Min.Kom.	1,2	11,3	0,9	7,0	7,5	11,5	4,6	8,6	9,5	2,2	5,7	1,6	0,6	3,4	6,7	1,2	1,3	7,3	2,1	3,0	0,2	5,5	.	2,6	3,5	1,3	9,5	6,3	1,6	2,9	6,0	136,6
31	Międzylesie	0,5	12,3	0,5	7,2	6,1	11,6	5,3	8,8	9,6	5,4	2,5	2,0	.	6,5	3,4	1,6	2,1	6,3	4,2	.	0,1	5,4	2,4	2,8	1,7	.	9,7	7,4	3,8	8,6	12,1	149,9
32	Erwinów	0,3	11,3	0,1	6,0	3,2	12,5	3,9	8,8	10,1	5,2	0,5	1,6	0,2	6,3	3,0	1,1	1,6	6,7	3,6	1,6	0,1	5,1	2,7	3,4	1,7	0,3	10,0	7,1	4,9	8,1	11,8	142,8
33	Świder	.	11,1	.	6,4	4,8	11,5	6,1	8,1	10,8	4,6	3,0	1,9	.	5,4	4,5	1,4	1,0	6,3	2,7	1,4	0,1	3,8	2,1	2,1	1,1	0,1	9,0	8,3	4,2	7,7	11,1	140,6
34	Topola-Błonie	2,3	8,4	3,3	4,7	6,4	12,7	1,1	8,8	7,6	7,0	.	1,4	0,9	4,8	2,1	2,8	6,1	1,9	2,7	4,0	.	2,7	3,9	6,9	2,0	1,3	10,1	7,9	9,9	11,1	9,5	134,3
35	Młochów	1,2	12,2	0,3	6,4	3,5	13,1	5,1	8,5	9,6	3,5	2,2	1,3	.	4,7	3,0	0,4	1,2	6,3	1,8	1,5	0,1	4,2	2,2	3,6	1,5	0,3	9,7	5,5	4,1	8,7	12,3	137,8
36	Skierniewice	2,5	11,9	0,5	5,1	5,9	12,7	2,5	9,0	9,7	4,1	1,6	1,4	0,1	1,8	.	1,2	3,9	6,3	1,2	2,9	0,2	1,2	4,2	3,7	2,3	0,1	10,2	8,0	7,3	8,1	11,8	141,4
37	Belsk	0,6	12,5	0,5	8,0	6,4	12,5	6,7	7,4	10,2	4,7	3,0	1,6	.	5,7	3,7	0,6	3,2	8,1	1,5	1,7	0,3	5,5	3,5	4,1	2,6	0,4	10,0	7,5	6,0	8,0	12,0	158,5
38	Łódź-Lublinek	2,6	10,1	2,9	5,1	6,5	12,3	1,5	6,3	7,2	6,3	0,7	0,6	0,5	5,9	1,0	0,4	5,4	2,6	1,8	1,1	0,4	4,1	1,4	7,5	2,0	0,4	10,5	7,6	9,3	9,5	9,7	145,2
39	Kalisz	5,9	7,2	5,9	4,5	9,7	12,3	2,6	10,5	6,4	8,6	0,1	0,4	1,8	7,3	1,5	3,9	7,1	3,7	3,0	1,4	1,2	4,1	3,7	5,1	1,6	1,8	9,8	8,3	10,9	12,0	11,3	177,4
40	Wieluń	7,3	9,9	2,4	5,7	8,3	12,5	1,0	4,0	4,8	6,3	1,7	.	0,8	7,9	1,9	3,3	5,8	2,9	3,5	3,5	1,2	4,7	2,1	4,9	2,2	1,2	10,9	5,6	11,2	11,5	12,1	162,9
41	Szepietowo	.	12,9	3,0	7,8	9,5	11,4	8,4	6,5	12,7	6,9	6,7	.	3,8	9,6	4,8	2,9	2,3	9,7	.	.	.	10,1	7,5	2,1	1,9	.	9,1	6,6	5,4	8,7	10,7	181,0
42	Białowieża	0,4	13,2	2,4	6,1	7,3	12,2	8,3	10,4	9,6	5,6	7,5	1,0	0,2	8,0	4,0	1,5	2,6	3,7	1,7	2,0	.	7,8	1,9	3,1	1,6	9,9	3,2	6,1	3,2	8,7	6,8	160,0
43	Terespol	0,4	12,1	9,4	8,4	7,4	12,6	12,0	8,0	12,7	5,5	8,0	1,1	.	11,9	6,8	4,8	4,7	6,0	3,1	2,9	.	8,1	3,1	2,0	1,8	2,0	4,4	9,2	4,1	9,2	5,3	187,0
44	Sobieszyn	0,9	12,3	1,3	9,3	3,6	12,8	11,2	2,9	10,3	4,5	5,0	0,4	.	5,9	3,6	0,3	2,3	7,6	1,9	1,1	.	7,5	2,6	3,8	1,9	0,2	8,6	3,5	3,0	5,6	8,9	145,0
45	Puławy	1,0	11,3	1,1	8,9	4,9	11,5	10,1	1,2	7,9	7,2	5,2	0,7	.	5,9	4,6	0,3	5,4	7,2	2,2	1,2	.	7,7	2,9	3,0	2,1	0,3	6,9	3,0	3,4	5,9	9,3	142,3
46	Chełm Lub.	6,0	12,4	8,7	8,1	6,2	12,4	12,4	0,5	11,0	11,0	9,3	1,4	.	6,7	9,5	5,3	3,3	5,5	3,5	3,0	0,2	11,4	3,0	3,9	4,4	.	8,0	8,0	2,2	9,2	8,1	194,6
47	Szczawno-Zdrój	8,5	4,2	5,0	1,0	3,8	11,2	1,7	3,4	1,2	8,3	1,1	0,5	0,8	4,6	0,5	5,2	2,9	3,0	3,2	2,6	6,9	3,7	2,8	.	2,7	4,5	8,0	6,1	9,6	10,8	11,1	138,9
48	Śnieżka	9,0	4,4	5,0	1,8	1,0	12,3	2,4	2,2	2,5	9,5	3,5	.	1,0	3,7	.	0,5	0,4	0,6	0,2	2,6	0,5	.	0,7	.	2,3	5,2	9,3	6,4	10,4	12,1	12,5	121,8
49	Opole	8,6	9,3	2,4	4,5	7,2	12,3	0,9	2,8	1,4	9,3	1,7	0,1	1,9	6,2	1,0	2,5	5,0	2,0	0,8	3,1	3,9	3,0	1,3	1,0	2,4	3,2	8,0	5,1	10,3	8,3	12,9	142,4
50	Kudowa-Zdrój	8,9	7,0	4,8	3,4	5,4	10,5	2,7	5,5	.	9,0	2,5	.	1,3	6,7	0,7	1,3	2,7	1,1	0,9	1,7	2,9	3,2	1,6	0,1	1,5	9,4	8,9	8,5	10,6	11,4	11,7	145,9
51	Polanica-Zdrój	11,5	6,6	5,8	3,2	7,4	10,6	1,5	4,8	2,2	7,6	3,8	0,1	0,8	7,7	1,9	4,6	3,7	4,8	.	5,4	6,5	7,4	3,3	.	5,4	10,2	8,7	7,1	10,9	10,8	11,5	175,8
52	Skroniów	7,4	12,4	0,7	7,4	7,0	12,6	9,3	1,8	3,6	10,3	7,2	0,2	.	7,7	4,6	.	8,9	8,6	1,1	2,4	1,7	7,1	3,4	5,5	5,3	7,7	8,8	6,1	9,0	11,4	12,2	191,6
53	Świerklaniec	10,4	11,0	0,4	6,5	6,8	11,4	7,1	4,2	4,4	9,0	4,1	1,1	0,9	2,9	2,5	1,5	7,6	4,3	1,6	3,6	3,9	7,4	2,0	3,2	3,8	5,2	10,0	2,7	10,7	11,6	11,9	173,7
54	Kraków, Obs.Astr.	11,5	11,4	1,7	8,0	6,6	12,2	10,9	1,5	6,8	9,4	10,7	1,9	.	7,1	5,2	1,3	8,9	5,9	4,4	2,3	6,6	8,6	2,3	3,7	5,2	6,9	8,5	4,4	9,8	10,5	11,0	205,2
55	Cieszyn	11,4	9,7	0,4	6,6	8,1	10,2	8,3	3,3	6,3	8,5	7,6	0,7	.	8,6	3,4	1,2	9,0	2,3	0,8	2,2	6,2	8,2	1,2	1,9	3,8	4,5	6,0	1,1	7,9	9,4	12,0	170,6
56	Istebna-Kubalonka	8,6	11,0	0,5	6,6	4,3	13,0	10,6	7,9	8,2	11,1	10,2	1,4	0,1	9,0	3,8	0,4	4,7	1,3	1,1	2,2	5,3	9,1	1,9	0,2	4,1	5,4	6,1	6,4	10,7	11,2	12,0	186,5
57	Rabka	9,6	10,6	1,8	3,7	3,6	12,2	11,5	6,0	8,4	10,8	10,7	3,4	0,1	6,2	5,1	0,8	6,8	2,1	3,0	1,2	4,5	5,9	0,4	2,2	2,3	4,0	6,2	7,6	10,1	10,3	11,7	182,8
58	Jabłonka	9,9	10,1	2,9	5,9	5,4	11,8	11,6	5,8	6,5	8,8	10,7	4,3	0,3	5,7	5,4	0,3	6,9	1,2	0,6	2,6	3,9	9,2	1,6	2,5	2,3	3,3	7,4	5,6	10,3	10,6	10,5	183,9
59	Krynica	9,4	10,7	2,5	5,1	7,4	10,8	10,9	6,7	6,0	10,5	9,2	4,4	0,1	5,2	5,8	0,4	2,3	3,4	1,3	2,4	6,0	6,0	3,0	2,7	0,9	3,9	6,2	7,5	8,3	10,6	10,6	180,0
60	Krynica-Góre Park	8,5	12,5	2,0	5,5	7,8	12,7	11,5	7,1	7,9	12,5	9,8	4,7	0,1	7,4	6,7	1,8	2,8	2,8	1,6	2,5	7,2	7,8	3,1	2,9	0,6	4,7	6,1	8,3	8,2	10,6	11,5	198,7
61	Muszyna	8,6	10,1	3,4	4,4	8,2	10,6	12,3	6,2	5,6	11,3	10,5	3,3	.	7,4	4,5	0,9	1,6	2,4	1,7	1,9	3,1	4,8	2,7	2,9	0,5	3,7	5,8	5,5	8,2	9,1	9,2	170,8
62	Rakopanie	12,0	10,9	1,4	0,4	4,4	14,0	13,0	5,6	9,3	11,4	12,2	2,4	0,4	5,0	6,8	0,4	4,4	0,7	1,7	1,6	7,6	7,7	1,9	1,6	1,4	3,7	5,0	6,3	10,9	12,4	12,2	190,7
63	Gubałówka	9,3	9,3	0,8	0,2	4,3	10,3	10,3	4,7	8,3	9,6	10,4	2,7	.	4,4	6,7	0,5	2,6	0,9	2,7	1,2	7,1	7,0	2,9	3,2	2,1	4,8	6,4	7,9	9,0	9,7	9,8	169,1
64	Hala Gąsienicowa	10,7	6,6	1,1	.	4,1	11,9	11,8	5,3	4,9	8,7	10,8	1,6	.	3,9	5,9	0,4	2,2	.	1,7	1,3	4,8	4,8	0,9	0,3	0,7	3,8	5,5	5,4	9,7	10,8	10,9	150,3
65	Kasprowy Wierch	9,5	9,3	0,6	2,2	5,0	13,5	13,5	3,1	5,9	11,3	12,2	2,0	.	9,0	6,4	0,7	3,5	0,1	1,2	1,6	4,7	6,0	0,6	0,1	0,5	2,6	6,6	5,7	11,0	12,8	12,8	176,2
66	Werbkowice	7,6	13,1	11,0	9,1	4,6	12,7	12,8	4,0	11,2	7,2	10,4	3,0	.	6,9	10,7	5,8	5,0	4,5	3,3	3,0	0,5	10,2	3,2	4,9	6,1	4,7	0,2	4,8	1,9	8,1	5,1	196,1
67	Zdanów	6,5	13,0	2,5	9,5	4,2	12,5	12,5	1,4	9,1	9,6	9,5	1,1	.	4,4	6,2	0,8	6,7	9,6	1,3	1,1	2,0	8,8	3,4	8,2	5,3	0,1	6,2	5,1	6,0	12,4	9,6	188,6
68	Iwonicz	8,6	12,6	5,9	7,6	6,7	11,7	11,6	8,2	7,1	9,3	10,7	5,1	.	8,7	7,9	3,2	.	.	.	.	.	4,1	2,1	7,0	2,3	.	.	.	6,6	10,9	11,0	168,9
69	Lesko	8,4	12,9	7,0	6,6	5,2	13,2	12,9	8,5	8,1	10,8	12,1	6,1	.	7,3	9,5	5,4	2,3	3,0	1,8	1,9	3,2	10,1	2,2	4,4	1,8	1,4	5,2	6,6	5,0	12,1	10,4	205,2

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	11,5	10,7	.	5,9	6,7	3,9	3,2	0,2	1,8	.	4,5	5,0	5,3	.	6,1	7,2	10,2	8,2	9,7	8,4	10,5	9,6	10,1	10,3	4,1	6,7	9,5	9,6	6,0	.	184,9
2	Kołobrzeg	11,5	9,6	9,4	9,0	6,7	3,7	2,7	0,8	.	0,1	5,6	5,1	3,7	0,4	5,7	6,4	10,3	10,1	10,3	10,9	10,9	9,8	10,3	10,4	2,5	5,7	7,6	8,8	3,5	3,0	194,5
3	Międzyzdroje	12,1	10,4	9,4	6,3	3,4	3,4	2,8	1,7	,	1,2	6,8	3,6	0,4	2,0	6,0	10,4	.	10,8	11,1	10,8	11,1	10,8	10,1	11,0	3,5	5,7	10,5	8,8	1,0	5,5	190,6
4	Resko	11,5	10,0	7,0	6,1	6,1	5,5	3,0	1,7	0,2	.	4,6	4,1	3,3	0,2	5,6	8,8	10,3	9,5	8,7	10,3	10,4	9,8	10,1	10,1	1,2	7,2	10,1	8,8	3,6	5,0	192,8
5	Szczecinek	12,3	11,4	10,5	10,6	6,0	3,8	2,5	0,9	0,3	1,6	1,4	1,4	4,7	0,1	5,1	6,0	11,1	7,9	10,8	11,1	11,4	11,2	10,7	11,1	3,1	7,7	6,8	10,5	5,9	2,0	199,9
6	Chojnice	10,6	11,0	10,1	7,8	7,6	4,3	1,6	1,3	2,0	0,1	1,5	1,9	5,5	0,1	2,8	8,8	10,8	8,1	11,4	11,1	11,2	10,9	11,0	10,9	5,4	8,6	7,6	9,7	5,8	0,1	199,6
7	Hel	10,8	9,6	10,6	4,7	8,2	1,5	1,6	0,1	6,4	6,7	1,5	2,1	6,9	.	9,6	2,7	10,0	7,0	10,5	7,7	9,7	10,4	10,3	10,3	5,7	4,0	8,0	9,7	6,7	3,8	196,8
8	Gdynia	11,7	10,4	9,8	1,5	5,2	1,4	2,3	0,6	4,7	1,9	1,6	4,7	8,0	1,6	7,8	7,9	6,0	8,2	10,7	7,3	9,5	10,8	10,6	10,9	5,8	5,3	5,5	9,9	7,6	4,2	193,4
9	Świbno	10,5	8,8	8,7	9,0	4,3	1,6	1,4	0,1	5,8	2,4	.	1,6	6,7	.	8,7	6,1	10,1	7,1	10,4	7,6	10,2	10,0	10,0	9,6	5,7	4,5	8,7	9,3	7,9	4,7	191,5
10	Stare Pole	11,8	11,5	10,6	6,8	1,6	1,4	1,1	.	3,6	2,3	0,1	0,6	8,0	0,4	6,6	8,1	11,7	7,5	11,7	6,7	10,4	10,7	10,8	11,1	7,8	7,4	9,8	10,7	8,1	2,8	201,7
11	Radostowo	12,1	11,1	10,5	7,3	2,7	1,9	0,9	0,1	4,0	.	0,4	2,2	7,4	0,1	6,8	9,6	10,8	8,4	10,9	9,9	10,7	11,1	11,2	10,9	7,1	6,7	8,3	9,7	8,2	0,5	201,6
12	Prabuty	12,0	12,0	10,7	7,9	2,1	2,8	1,2	0,4	4,7	.	0,5	2,3	6,3	0,2	7,4	5,7	11,3	7,6	11,4	9,9	10,4	9,2	11,1	10,6	8,2	7,4	9,4	9,7	9,1	0,9	202,4
13	Bydgoszcz, IMiUZ	11,1	11,4	9,8	7,8	6,1	1,9	0,4	2,3	1,2	.	2,5	2,2	4,8	0,2	6,8	9,7	10,6	8,8	10,4	10,5	10,7	10,8	10,7	10,7	5,7	8,7	7,4	9,2	6,1	0,2	198,7
14	Suwałki	11,3	11,5	10,7	6,6	11,2	.	2,1	.	4,7	6,4	0,7	0,8	5,8	0,2	2,9	.	9,7	7,5	11,4	6,0	11,1	11,5	11,2	11,2	10,0	2,3	4,0	9,6	.	5,8	186,2
15	Mikołajki	11,8	11,5	11,0	5,8	5,1	0,1	1,7	0,4	3,0	8,3	0,3	1,1	7,8	.	5,2	1,4	10,7	6,7	10,6	7,6	11,2	11,0	10,7	10,7	9,7	7,4	6,5	7,3	7,9	8,3	200,8
16	Biebrza	10,2	11,1	8,7	6,1	4,4	0,1	2,3	0,2	3,0	8,6	0,3	4,7	.	.	.	0,3	4,8	4,6	10,2	5,2	10,6	10,6	10,1	9,8	8,5	5,1	1,6	7,6	4,1	8,8	161,6
17	Białystok	10,7	10,6	10,1	9,0	.	.	1,6	1,3	2,8	8,1	2,6	2,5	4,8	.	1,7	0,5	10,1	9,5	8,0	6,4	10,9	10,8	10,7	10,9	9,3	6,9	5,5	8,5	5,5	7,9	187,2
18	Gorzów Wlkp.	10,6	11,1	7,9	4,0	8,8	4,2	2,9	1,4	0,8	0,6	3,8	2,5	2,3	1,6	8,4	8,4	9,7	4,0	10,5	8,9	10,4	10,2	10,1	9,9	2,4	4,3	8,8	7,0	2,9	0,5	178,7
19	Przebędowo	11,4	11,3	8,1	9,4	7,5	5,1	1,1	0,1	0,7	0,1	1,8	1,9	5,4	0,5	6,5	9,7	10,9	7,0	10,6	10,7	10,6	10,6	10,5	10,4	5,1	3,1	10,0	9,3	5,2	4,2	198,8
20	Przybroda	12,1	11,8	8,6	9,5	7,4	5,6	2,3	1,1	1,7	0,1	1,2	2,1	3,5	1,4	7,5	10,1	11,1	6,7	11,0	10,8	10,6	10,3	10,3	10,3	4,8	4,0	10,0	9,0	4,1	3,4	202,4
21	Poznań-Ławica	11,0	11,0	6,9	8,6	7,0	3,9	1,8	0,3	1,2	.	1,5	1,2	3,7	0,4	5,7	9,3	10,2	5,9	9,9	9,5	9,7	9,8	9,5	9,5	4,6	2,1	8,1	6,5	3,4	2,0	174,2
22	Plewiska	11,5	11,6	7,9	9,1	7,9	4,0	2,0	0,2	0,6	.	2,3	.	4,5	0,8	6,7	10,0	10,6	6,2	10,1	10,6	10,5	10,3	9,9	10,3	4,3	1,8	7,8	8,6	4,3	1,6	186,0
23	Kórnik	11,8	12,0	8,0	9,1	8,1	0,4	1,0	1,7	0,9	.	2,2	.	3,1	0,9	5,5	10,9	11,1	8,0	10,9	10,6	11,2	11,0	11,1	10,9	5,7	0,8	10,2	8,6	5,6	2,4	193,7
24	Oborniki Śl.	11,5	12,1	9,4	9,2	9,7	2,6	1,6	0,4	0,9	.	0,1	4,0	2,5	2,5	6,2	11,3	10,8	10,2	9,0	11,2	11,1	10,3	10,7	8,9	6,2	0,9	4,0	5,9	6,0	0,2	189,2
25	Laskowice Oławskie	11,6	11,5	10,5	9,3	9,6	0,3	1,4	0,2	0,8	.	.	2,7	3,0	0,8	5,4	10,5	10,9	9,7	8,0	10,5	10,7	10,3	10,3	9,7	6,6	2,1	1,8	4,6	5,2	0,1	178,1
26	Ciechocinek	10,6	11,2	8,6	9,3	5,9	3,6	0,4	1,5	1,3	.	0,3	2,0	4,5	0,2	4,0	8,8	10,3	6,1	10,0	10,9	10,7	10,7	10,3	10,2	7,3	8,5	7,9	9,6	6,5	.	191,2
27	Więcławice	11,4	11,6	10,0	9,8	5,3	1,3	.	1,0	.	2,0	1,3	1,9	5,5	0,7	5,5	9,7	10,8	9,5	10,7	11,0	10,0	10,2	10,5	10,4	6,6	9,1	8,1	9,6	5,9	.	199,4
28	Legionowo	11,2	11,6	10,0	9,6	9,2	0,1	.	1,1	3,6	0,1	.	6,3	6,0	.	1,8	5,4	10,0	10,7	11,0	10,6	10,9	11,1	10,5	9,7	8,7	9,6	6,0	9,1	6,1	2,5	201,9
29	Warszawa-Bielany	11,4	11,6	10,1	9,4	9,0	0,6	0,3	1,1	2,5	.	.	5,8	3,6	0,1	1,5	4,7	11,0	9,6	11,2	9,3	10,4	10,7	11,0	10,6	9,1	9,7	7,4	9,9	6,0	1,4	198,6
30	Warszawa, Min.Kom.	10,3	11,3	9,8	9,4	8,3	1,1	1,0	1,7	2,7	.	.	4,9	4,0	1,3	0,4	5,6	10,9	8,2	10,1	10,0	10,2	10,6	9,9	9,8	8,7	9,0	5,7	9,2	6,3	1,6	192,0
31	Międzylesie	11,3	11,4	10,2	10,1	8,4	1,2	0,4	1,3	2,6	.	.	4,8	3,1	0,5	0,8	.	10,7	9,9	10,9	10,1	10,1	11,1	11,0	10,3	8,6	8,9	5,7	9,1	5,0	2,8	190,3
32	Brwinów	11,8	11,8	10,2	10,4	9,7	0,3	.	1,5	1,7	.	.	4,1	3,3	.	1,2	5,4	11,2	9,4	11,4	10,2	10,7	11,2	10,7	10,2	9,2	8,0	6,6	10,3	6,3	1,6	198,4
33	Świder	10,8	10,8	10,4	9,5	8,5	0,8	0,6	0,8	2,0	.	.	3,9	2,2	0,5	1,3	3,7	10,4	9,7	10,1	9,7	10,2	10,4	10,1	9,8	8,6	8,6	6,6	7,8	4,5	3,5	185,8
34	Topola-Błonie	10,6	11,2	8,2	9,7	7,9	.	1,0	0,6	1,3	.	0,7	3,0	6,0	0,4	2,2	9,2	10,4	8,1	10,4	10,2	10,5	10,0	10,4	9,9	8,5	5,0	7,7	9,8	6,1	.	189,0
35	Młochów	12,0	12,1	11,0	10,7	10,7	0,9	.	0,4	2,0	.	.	4,7	5,1	0,1	1,3	6,1	11,4	10,4	11,3	10,8	11,2	11,1	10,8	10,6	8,8	8,7	7,8	9,7	6,4	1,8	207,9
36	Skierniewice	10,6	11,5	10,6	10,1	10,0	0,5	0,3	1,4	1,5	.	0,5	4,9	4,9	0,1	4,5	6,8	11,0	9,8	11,2	8,7	10,9	10,9	10,8	10,5	9,5	6,7	8,2	10,1	8,3	2,4	207,2
37	Belsk	11,5	11,5	10,9	10,1	9,0	1,5	0,6	0,7	1,6	.	.	4,4	3,7	0,3	2,5	4,5	10,8	10,3	11,0	8,7	10,5	10,5	10,6	10,6	9,6	7,7	3,5	8,9	6,5	1,1	193,1
38	Łódź-Lublinek	9,5	11,2	10,1	9,2	8,0	0,1	0,2	0,5	1,9	.	.	2,9	4,5	.	1,1	8,8	10,6	9,2	10,8	9,5	10,9	10,9	10,9	10,6	9,5	4,7	8,2	9,8	6,3	0,1	190,0
39	Kalisz	10,8	11,1	8,8	8,3	8,3	.	0,8	0,1	1,3	0,9	0,1	2,7	2,7	.	6,8	10,2	10,9	9,4	10,7	10,5	10,6	10,7	9,9	10,3	7,6	2,1	7,3	8,7	6,8	2,7	191,1
40	Wieluń	11,0	12,5	11,8	6,7	9,1	.	1,0	0,3	0,8	.	0,2	3,8	3,4	0,9	3,7	10,1	11,2	10,2	9,8	10,3	11,2	10,7	10,9	10,8	9,6	2,6	3,0	7,2	6,8	0,2	191,8
41	Szepietowo	11,9	11,8	9,8	8,2	6,1	1,7	1,5	0,7	4,2	5,3	0,9	6,0	5,2	.	1,8	2,3	10,6	9,9	10,6	11,3	11,2	10,5	11,2	9,8	9,5	8,4	9,1	9,5	1,1	8,3	208,4
42	Białowieża	11,0	11,3	11,2	6,7	5,1	3,6	1,7	3,4	1,6	7,6	5,1	4,7	4,8	0,7	2,1	0,3	10,7	10,2	8,4	5,1	10,6	10,8	10,5	10,6	8,9	6,1	5,9	9,2	1,0	4,5	193,4
43	Terespol	10,0	10,7	11,8	6,0	9,7	4,4	3,8	4,8	2,3	2,5	0,1	2,7	3,2	0,5	1,5	1,6	10,5	10,2	10,5	7,5	10,8	10,9	10,7	10,9	9,3	9,6	6,2	8,3	3,7	5,4	200,1
44	Sobieszyn	11,5	10,5	11,6	9,0	8,7	3,7	3,1	3,9	1,2	0,3	1,1	2,9	2,7	1,0	1,1	3,8	11,1	10,5	11,9	10,7	11,2	11,1	11,4	10,5	9,4	7,6	3,2	9,3	6,1	5,4	205,5
45	Puławy	10,8	10,8	10,7	7,8	7,2	3,5	2,6	2,5	0,9	.	0,3	3,4	1,8	1,0	1,3	2,2	10,0	9,5	10,3	10,1	10,0	10,2	10,2	8,6	8,0	5,9	1,0	9,0	4,2	2,6	176,4
46	Chełm Lub.	11,1	11,9	11,9	8,0	5,0	5,4	10,3	6,6	0,3	0,3	0,5	5,4	2,1	1,2	1,3	2,1	10,5	10,1	11,3	8,4	11,1	10,8	10,5	11,0	10,8	4,2	0,3	9,2	7,4	6,9	205,9
47	Szczawno-Zdrój	11,1	11,3	9,5	6,5	8,6	0,1	2,7	2,9	0,1	.	.	1,6	2,0	.	8,1	10,1	10,2	9,3	6,0	9,9	9,3	9,9	8,8	9,1	6,0	1,0	1,1	4,6	5,0	0,8	165,6
48	Śnieżka	11,7	.	8,8	6,5	10,0	0,1	.	.	.	.	0,1	2,6	1,5	0,5	10,0	11,0	11,1	9,0	7,9	11,3	11,2	11,2	10,7	10,8	8,4	1,8	5,5	6,0	7,2	4,0	178,9
49	Opole	12,2	12,0	12,2	9,1	9,6	.	0,1	0,3	0,8	.	0,4	4,5	2,4	2,4	5,4	11,0	11,3	10,7	5,8	10,8	11,2	11,4	10,8	10,2	9,0	.	1,7	4,5	7,0	.	186,8
50	Kudowa-Zdrój	11,3	11,3	9,6	5,5	9,2	0,2	1,7	.	0,1	.	1,4	2,6	5,1	1,8	8,5	10,1	9,9	10,0	8,7	11,0	10,0	9,7	9,4	9,6	7,3	0,6	3,3	6,1	6,1	4,8	184,9
51	Polanica-Zdrój	11,3	11,7	8,2	6,8	10,0	0,3	3,4	0,9	0,7	.	0,9	3,1	5,6	3,1	9,4	10,1	11,0	10,3	1,9	10,6	10,3	9,6	9,6	10,0	8,2	1,8	4,8	6,5	6,9	3,1	190,1
52	Skroniów	11,9	11,1	11,8	6,0	6,3	3,5	2,5	3,6	0,9	.	.	5,2	3,2	1,7	6,3	6,5	10,5	9,9	7,5	11,1	10,8	11,2	10,8	9,5	8,9	1,0	.	8,4	8,0	0,1	188,2
53	Świerklaniec	10,9	11,0	11,5	6,5	8,9	0,7	1,1	1,3	0,8	.	1,4	5,1	3,7	7,4	2,3	8,2	10,0	10,1	7,9	10,8	10,7	10,9	10,9	9,0	9,3	1,6	0,3	3,9	7,8	0,1	184,1
54	Kraków, Obs.Astr.	11,5	10,4	11,3	6,7	8,8	1,8	5,4	5,7	.	0,1	.	5,6	2,9	3,9	9,3	7,4	9,8	10,5	4,8	9,6	9,2	10,2	9,8	8,8	8,8	.	.	2,2	4,7	.	179,2
55	Cieszyn	11,6	12,2	12,1	2,1	10,6	0,5	2,2	4,3	.	.	0,9	3,7	6,4	3,4	6,1	10,1	10,3	10,0	0,8	10,0	10,0	9,9	9,5	9,4	9,5	0,6	.	7,4	8,9	0,1	182,6
56	Istebna-Kubalonka	11,8	11,7	11,9	3,9	10,8	2,1	3,1	6,5	.	.	0,2	5,7	4,0	4,3	6,1	11,1	11,1	11,1	9,2	11,0	10,9	10,9	10,6	10,4	10,5	3,7	0,8	8,1	8,8	0,6	210,9
57	Rabka	11,2	10,1	12,1	4,9	9,1	4,7	6,0	5,9	.	.	0,8	6,8	3,6	3,6	8,8	10,4	11,2	11,3	2,9	11,2	10,9	10,7	10,8	10,3	10,3	2,1	2,8	7,3	9,1	0,1	209,0
58	Jabłonka	10,3	10,2	10,1	0,7	7,5	5,1	7,2	6,3	.	.	2,7	8,3	3,8	4,1	9,0	8,1	8,0	10,0	8,0	10,5	9,5	8,8	8,8	8,7	9,1	3,1	4,2	6,2	6,4	2,5	197,2
59	Krynica	10,7	10,6	9,8	3,2	9,1	5,7	7,7	6,6	0,2	.	0,6	7,2	3,7	3,6	9,0	7,0	10,1	10,1	7,0	10,1	10,1	10,0	9,6	9,6	9,5	0,9	2,1	5,8	9,8	.	199,4
60	Krynica-Góra Park	10,9	10,8	10,4	3,6	8,5	5,8	8,2	6,2	.	.	.	8,2	3,3	4,1	8,5	7,4	10,7	10,1	5,4	10,7	10,6	10,5	10,3	9,7	9,1	0,7	2,0	5,7	9,1	.	200,5
61	Muszyna	10,3	8,9	9,5	4,2	8,0	4,2	7,3	6,4	0,5	.	0,9	5,9	5,4	3,6	7,9	7,0	8,4	9,0	3,3	9,5	8,3	8,9	8,6	8,8	7,9	2,3	2,7	5,3	6,2	0,1	179,3
62	Zakopane	12,2	9,9	12,3	3,0	10,4	4,5	5,1	7,0	.	.	.	8,5	5,1	5,2	7,8	10,3	11,5	11,4	6,8	11,4	11,3	11,3	11,3	11,2	11,2	2,8	4,9	8,3	7,7	0,1	222,5
63	Gubałówka	9,4	8,9	9,5	3,0	7,7	3,5	4,4	6,5	0,1	.	.	7,2	4,7	5,8	7,4	8,2	9,4	9,5	7,0	9,4	9,3	9,4	9,4	8,7	8,7	1,8	4,4	8,2	7,1	.	188,6
64	Hala Gąsienicowa	10,6	5,8	10,6	2,9	7,0	4,0	5,6	7,1	.	.	.	6,5	4,4	4,0	7,0	8,6	9,7	9,5	7,2	2,6	9,5	9,4	9,4	9,4	9,3	7,7	3,0	2,8	9,1	7,4	0,4	181,1
65	Kasprowy Wierch	12,7	5,4	13,0	3,8	9,5	2,4	5,4	7,0	.	.	1,1	8,7	4,3	4,7	8,2	10,1	12,0	11,9	10,3	12,0	11,9	11,9	11,8	11,6	11,2	2,8	5,4	11,2	7,8	0,2	228,3
66	Werbkowice	11,5	11,9	11,7	5,9	7,4	7,0	6,8	5,3	0,2	0,9	.	1,9	1,6	2,2	3,5	2,2	9,9	10,6	10,4	8,5	10,9	10,1	10,9	9,8	1,3	8,4	10,7	8,4	8,6	6,2	204,7
67	Zdanów	12,2	11,8	11,8	6,3	5,1	3,6	5,3	5,2	1,1	.	.	5,5	2,1	1,3	5,5	1,9	10,6	11,1	9,7	11,1	11,1	11,4	11,1	10,1	9,6	0,9	0,9	9,8	7,6	4,0	197,7
68	Iwonicz	10,9	11,2	11,1	6,6	9,4	7,0	7,9	6,4	.	.	.	9,9	1,9	5,1	6,6	3,8	.	.	1,4	9,7	9,9	9,9	9,6	9,7	9,5	1,7	4,1	1,0	6,8	0,7	172,8
69	Leśko	11,3	11,1	11,2	6,9	9,4	3,3	7,9	5,5	0,1	0,3	.	9,3	1,6	3,6	8,1	1,5	10,5	10,2	1,3	10,0	10,0	10,1	10,1	10,3	9,3	3,4	2,8	8,1	6,4	2,2	191,0

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	9,3	3,7	9,2	9,2	8,8	9,1	9,7	.	4,4	7,9	4,6	9,1	5,3	2,7	0,5	0,4	0,3	.	.	.	.	6,1	6,7	2,7	.	0,1	1,7	0,1	.	.	0,3	111,9
2	Kołobrzeg	9,2	1,6	9,0	8,7	8,2	8,2	8,2	0,4	4,3	8,1	4,6	7,8	7,8	0,2	.	3,3	.	.	.	.	.	2,2	7,3	2,0	.	2,5	.	1,2	0,9	.	0,3	106,0
3	Międzyzdroje	9,4	6,6	8,7	9,1	.	8,7	8,7	1,7	1,5	8,8	5,6	7,9	5,8	3,3	0,3	2,0	.	0,9	3,4	5,1	1,7	3,7	2,0	2,0	.	.	.	2,8	.	.	.	107,7
4	Resko	9,3	3,5	9,0	8,4	8,2	8,4	8,1	0,5	5,9	8,4	6,2	6,6	4,4	0,3	.	3,8	.	.	0,1	2,1	.	2,8	5,3	2,1	.	0,5	3,9	0,9	0,5	0,2	0,1	109,3
5	Szczecinek	10,6	.	10,2	10,0	9,5	9,5	9,6	0,5	4,6	8,5	7,3	6,1	4,0	0,2	.	3,5	.	.	.	.	.	4,4	5,4	2,5	.	.	5,5	0,2	.	0,6	.	112,5
6	Chojnice	6,6	.	9,6	9,2	9,2	8,8	8,8	0,4	4,1	8,3	7,3	6,5	6,7	1,9	.	3,0	.	.	.	0,9	.	7,0	4,9	1,5	.	0,1	5,2	.	.	0,1	.	110,1
7	Hel	7,7	0,5	7,8	8,6	8,2	8,1	7,9	.	2,0	6,4	6,8	7,0	6,9	2,1	3,4	.	0,1	.	.	4,0	2,5	.	4,0	3,8	0,1	.	3,7	.	.	0,8	.	102,8
8	Gdynia	6,2	.	7,4	7,6	7,9	8,5	7,8	.	2,3	7,1	6,8	8,1	6,3	2,7	2,2	.	0,1	.	.	2,5	2,0	3,3	4,3	3,5	0,1	0,4	4,3	.	.	0,7	0,3	102,4
9	Świbno	8,5	1,8	9,0	9,4	8,8	8,8	8,3	.	2,0	6,7	7,2	6,6	6,4	1,7	3,2	0,1	0,1	.	.	4,0	2,5	3,6	4,2	2,6	0,4	.	2,3	.	.	0,1	0,1	108,8
10	Stare Pole	3,9	2,8	9,0	9,1	9,8	9,4	9,1	0,6	1,7	7,1	7,7	2,9	6,4	0,3	2,0	0,1	.	.	.	3,8	5,2	6,3	5,1	0,3	0,9	.	3,5	2,0	.	.	.	109,0
11	Radostowo	4,1	0,3	8,0	9,3	9,7	9,7	9,2	1,6	2,4	6,8	7,6	5,8	5,7	.	1,7	0,2	.	0,1	.	2,0	2,5	2,6	3,8	1,3	0,6	.	3,2	0,1	.	.	.	98,3
12	Prabuty	.	4,7	9,3	9,6	9,6	9,6	9,3	3,3	1,9	7,4	8,0	1,7	6,9	0,2	0,9	0,1	.	.	.	2,7	6,3	2,2	3,5	0,1	1,0	.	3,6	2,8	.	.	.	104,7
13	Bydgoszcz.IMiUZ	3,7	0,1	8,8	8,7	7,7	8,4	8,3	.	3,4	6,9	7,7	4,4	3,5	1,0	.	*3,7	.	.	.	.	5,0	6,3	6,0	0,6	0,7	0,5	6,1	3,1	.	1,8	.	106,4
14	Suwałki	0,1	4,8	5,3	9,5	9,8	9,3	9,0	4,6	3,3	5,4	4,5	1,9	4,0	2,0	.	2,2	.	.	2,8	.	1,5	5,7	8,7	0,1	4,3	.	2,1	2,8	.	.	.	103,7
15	Mikołajki	.	4,9	4,9	9,6	9,6	9,2	8,5	6,0	3,9	.	5,2	1,4	5,0	.	.	.	0,4	.	2,2	2,2	6,3	.	8,4	.	3,2	.	2,7	6,3	.	0,4	0,3	100,6
16	Biebrza	.	7,2	4,9	8,5	9,3	8,2	8,3	6,0	5,1	.	3,4	2,9	4,1	.	.	0,3	.	.	2,5	.	5,1	1,3	8,5	.	4,9	.	2,9	2,7	.	.	.	96,1
17	Białystok	0,1	5,5	8,1	9,2	9,2	8,1	8,5	5,6	5,2	.	7,8	4,6	1,8	.	.	0,2	.	.	3,1	.	3,6	4,7	8,1	1,7	4,2	.	.	5,7	.	.	0,4	107,4
18	Gorzów Wlkp.	8,4	3,2	8,4	5,6	7,3	8,0	6,6	.	7,5	7,2	7,9	8,5	6,4	3,0	.	5,9	.	.	2,9	2,0	.	6,2	2,2	1,7	.	0,2	5,8	1,8	.	4,6	0,9	122,3
19	Przebędowo	9,2	.	9,5	7,8	8,3	8,9	8,4	.	5,2	7,7	8,2	6,0	4,7	0,8	.	4,5	.	.	.	.	.	6,0	4,5	.	0,7	.	7,2	2,4	.	1,5	0,2	111,7
20	Przybroda	9,4	3,6	9,3	8,1	7,7	8,4	8,4	.	6,2	8,5	8,0	6,8	3,9	2,1	.	4,2	.	.	.	.	.	7,0	0,5	0,8	0,7	4,4	7,7	0,3	.	.	2,7	118,7
21	Poznań-Ławica	8,1	3,8	8,3	8,5	6,5	7,4	7,0	.	5,6	7,8	7,7	6,1	6,6	2,7	.	2,9	.	.	.	.	.	5,2	4,4	0,1	0,9	0,4	7,0	1,7	.	1,5	0,8	110,6
22	Pleszewska	9,0	3,3	9,4	8,4	7,8	8,0	7,3	.	5,6	8,1	7,8	6,3	6,8	2,6	.	2,6	.	.	.	.	.	.	4,6	.	0,7	.	5,8	1,0	.	0,5	0,1	105,7
23	Kórnik	9,8	3,9	9,8	9,5	8,0	9,0	8,0	.	6,0	8,7	8,7	5,9	8,3	2,0	.	3,8	.	.	.	.	.	3,8	4,2	.	1,0	0,1	7,8	4,4	.	0,3	0,2	125,2
24	Oborniki Śl.	9,4	2,4	9,0	5,9	8,1	3,8	4,5	0,8	6,0	7,5	7,4	3,3	4,0	0,7	.	5,6	0,3	.	.	.	0,3	4,2	4,0	0,6	1,9	0,6	6,3	2,6	2,4	5,5	.	106,2
25	Leszkowice Oławskie	9,8	2,3	9,6	6,6	8,8	9,1	4,8	.	4,7	9,0	8,6	5,2	4,5	1,1	.	5,0	0,9	.	0,1	.	0,5	3,3	3,4	0,3	1,9	0,6	7,1	.	.	5,4	3,7	116,3
26	Ciechocinek	2,0	0,1	8,0	.	6,8	8,3	7,5	3,8	.	7,0	7,5	3,7	3,4	0,1	.	3,8	.	.	.	.	5,5	2,0	3,3	.	1,0	.	4,8	0,2	.	0,2	.	79,0
27	Więczawice	1,7	.	8,7	8,6	5,5	8,6	8,4	2,9	3,3	7,2	7,2	4,1	2,4	0,1	.	3,9	.	.	.	.	4,6	5,3	6,7	0,4	0,6	.	6,0	1,5	.	0,4	.	98,1
28	Legionowo	.	4,3	7,8	6,8	9,0	9,0	8,4	7,7	0,9	3,9	7,1	4,1	5,3	.	.	1,2	.	.	1,8	4,6	3,3	2,5	.	0,5	4,5	.	5,9	4,7	.	.	0,7	106,0
29	Warszawa-Bielany	0,2	4,5	9,1	9,3	9,5	9,5	8,6	7,7	0,4	0,9	7,5	3,3	4,7	.	.	0,4	0,2	.	1,3	8,2	7,2	.	3,2	0,4	4,7	.	5,5	6,2	.	.	3,4	115,9
30	Warszawa,Min.Kom.	4,1	3,4	8,9	8,7	8,5	7,7	8,4	7,2	0,1	4,6	7,4	2,2	5,0	.	.	0,9	.	.	0,7	7,4	3,5	.	2,6	0,3	3,2	.	3,6	5,5	.	.	0,7	104,6
31	Międzylesie	.	4,2	8,8	9,0	8,8	9,1	8,5	7,8	1,8	4,0	8,3	4,5	4,4	.	.	0,3	.	0,3	2,3	8,4	6,1	1,4	4,1	1,2	5,1	.	5,6	7,7	0,2	.	4,7	127,0
32	Brwinów	.	3,4	8,6	9,0	8,9	9,1	8,4	8,1	.	5,2	8,3	3,5	4,2	.	.	.	.	.	.	6,7	4,4	.	2,6	1,0	4,7	.	5,4	5,4	.	.	3,8	110,7
33	Świder	0,2	3,8	8,6	8,8	8,8	8,7	8,2	8,1	1,7	4,4	8,4	5,2	3,9	.	.	0,2	.	.	2,9	8,2	5,5	.	4,2	1,5	5,0	0,1	4,9	6,6	.	.	3,7	121,6
34	Topola-Słonie	1,0	1,3	8,7	9,0	3,1	9,3	7,5	3,9	0,9	7,8	8,9	3,0	5,1	.	.	3,1	0,3	.	0,1	.	3,5	2,5	2,6	.	1,6	0,2	5,5	5,7	.	0,1	0,6	95,3
35	Włochów	0,1	3,1	9,5	9,2	9,6	9,4	8,5	8,7	.	6,9	8,0	4,2	5,9	.	.	1,7	.	.	0,8	7,4	6,3	.	2,8	0,8	4,7	.	4,1	5,9	.	.	4,5	122,1
36	Skierniewice	0,2	1,2	9,3	9,4	8,3	9,7	8,0	6,7	0,5	8,4	9,1	4,9	4,8	.	.	2,8	.	.	0,1	6,1	6,8	3,5	1,5	0,2	4,4	.	5,6	6,8	.	0,4	2,6	121,3
37	Belsk	.	2,3	8,5	8,7	8,9	8,9	7,8	7,0	0,1	7,6	7,3	4,9	4,9	.	.	2,6	.	.	0,6	6,2	3,9	.	1,5	1,2	5,0	.	3,3	3,1	.	.	3,2	107,5
38	Łódź-Lublinek	2,0	1,0	9,3	9,2	3,4	9,1	6,8	3,7	1,0	8,0	6,8	4,0	5,2	.	.	3,5	0,2	.	0,1	1,5	4,0	0,7	0,5	0,1	2,9	.	4,6	6,4	.	0,8	0,9	97,2
39	Kalisz	9,0	2,0	9,0	8,9	6,3	8,4	6,3	0,1	2,9	9,0	8,2	7,1	7,0	0,2	.	5,5	0,5	.	.	.	1,5	2,3	4,3	0,4	0,9	0,7	6,6	.	.	4,1	1,1	112,3
40	Wieluń	10,0	2,6	10,0	8,9	5,8	7,1	5,4	0,2	1,8	8,8	8,3	3,1	4,3	.	0,2	6,3	1,7	.	0,1	.	3,1	2,0	1,7	0,9	2,8	0,3	5,1	3,6	.	1,9	2,5	108,5
41	Szepietowo	0,4	5,2	8,9	9,4	9,5	9,4	8,8	7,0	6,8	3,5	4,0	8,6	5,0	.	.	1,7	.	0,1	3,8	2,5	2,5	4,2	8,3	.	.	.	5,4	7,1	.	1,5	.	123,6
42	Białowieża	1,1	6,1	7,4	9,0	9,1	5,7	8,2	7,7	5,0	.	6,7	7,9	4,4	.	0,1	.	0,6	.	5,5	.	6,2	7,0	8,2	5,7	6,5	.	6,2	8,0	.	1,0	0,7	134,0
43	Terespol	0,6	6,1	6,9	9,5	9,9	7,1	7,8	7,7	7,9	.	7,5	8,5	4,2	0,2	0,4	2,4	2,6	0,3	5,2	1,6	1,7	5,1	8,1	6,4	6,8	0,3	2,9	8,1	.	0,7	2,1	138,6
44	Sobieszyn	0,4	4,2	9,7	9,3	9,7	9,1	9,0	6,8	7,3	5,2	8,9	6,2	5,6	.	.	.	0,8	.	5,0	8,8	3,2	0,2	8,1	5,6	6,7	0,1	0,8	8,4	1,5	1,5	3,3	145,4
45	Puławy	0,5	3,2	7,8	7,8	8,0	7,8	7,1	6,5	5,0	3,4	9,0	5,6	5,1	.	.	.	1,2	.	5,3	8,4	3,5	.	7,7	5,3	7,0	.	1,4	8,0	2,6	0,7	5,0	132,9
46	Chełm Lub.	0,1	5,0	8,1	8,9	9,1	8,6	9,0	7,0	8,7	.	9,1	9,8	3,5	.	0,2	0,4	2,8	0,1	6,7	6,9	0,1	1,5	8,7	7,8	7,5	.	4,2	8,2	3,5	0,3	2,7	148,5
47	Szczawno-Zdrój	4,5	1,5	7,6	2,5	7,9	8,7	5,8	2,0	5,8	8,8	9,1	0,7	1,4	2,0	0,8	7,2	0,6	.	0,1	.	.	5,8	2,0	1,5	0,8	1,0	7,3	0,6	.	5,5	5,0	106,5
48	Śnieżka	6,4	9,1	9,2	.	1,2	7,9	0,2	.	6,9	9,6	9,7	0,9	1,2	4,8	8,0	8,9	.	.	0,3	0,8	.	3,5	.	.	.	0,5	8,0	6,9	0,8	5,6	2,5	112,9
49	Opole	10,3	2,6	9,8	5,9	9,3	8,6	3,4	0,8	3,4	8,1	7,6	3,2	4,8	0,2	.	6,9	2,3	.	.	.	2,2	3,9	4,9	1,9	3,5	0,7	4,5	2,1	.	.	3,9	114,8
50	Kudowa-Zdrój	5,5	8,2	8,6	1,1	8,4	8,7	5,8	1,7	6,1	8,2	8,2	3,5	2,5	5,0	0,1	6,7	.	.	.	.	0,1	6,5	0,2	2,9	0,6	2,0	6,7	.	.	.	.	107,3
51	Polanica-Zdrój	5,0	1,1	4,5	1,0	8,8	9,2	7,2	2,7	6,7	8,6	8,9	2,9	2,5	1,3	2,1	8,1	1,4	.	.	.	0,4	6,5	5,4	3,8	1,6	1,4	7,0	.	.	.	5,0	113,1
52	Skroniów	4,5	2,1	9,4	9,4	8,2	9,5	6,2	6,4	0,6	8,4	7,8	4,9	5,0	.	0,1	3,9	.	0,3	1,4	2,8	6,6	.	.	4,0	5,7	0,3	1,8	8,2	.	0,9	4,5	122,9
53	Świerklaniec	9,5	1,2	9,3	7,8	7,9	6,8	4,1	3,0	1,2	6,8	4,2	5,2	6,1	0,1	.	6,9	2,4	.	.	.	4,3	2,6	1,5	3,3	4,1	1,4	3,3	4,0	.	.	4,4	111,4
54	Kraków,Obs.Astr.	5,6	1,5	9,3	9,7	8,9	8,8	4,8	5,6	1,1	8,4	5,8	3,7	1,1	.	.	8,4	3,4	0,1	1,8	3,6	7,1	.	1,1	6,2	6,5	0,7	1,2	8,0	0,9	.	3,2	124,5
55	Cieszyn	6,6	9,4	8,0	5,7	5,9	8,2	0,7	0,9	.	8,8	8,5	3,2	1,0	.	.	8,2	2,7	.	1,0	.	3,3	5,1	2,3	5,7	3,9	1,1	3,5	7,5	.	.	5,3	116,5
56	Istebna-Kubalonka	8,4	10,1	10,1	8,2	7,7	8,3	2,0	6,5	.	9,8	9,4	6,6	.	.	.	5,7	2,2	.	.	0,2	4,9	6,4	3,0	5,3	5,4	1,9	4,1	8,9	0,1	0,1	5,0	140,3
57	Ustka	8,2	6,5	9,8	9,0	7,9	9,3	5,5	5,6	.	8,7	9,4	5,0	1,0	0,7	.	8,8	5,7	2,7	2,0	2,3	8,6	1,7	1,8	8,9	7,0	1,0	3,3	8,9	1,4	0,3	4,4	155,4
58	Jabłonka	4,9	5,4	6,9	6,8	5,7	8,4	2,5	5,1	0,8	6,0	4,1	3,0	0,4	0,4	.	7,3	4,4	0,8	1,8	0,3	7,1	1,5	1,0	8,8	4,3	4,4	2,1	8,5	1,8	1,9	2,9	119,3
59	Krynica	8,2	6,7	9,5	9,4	8,6	9,5	7,9	7,0	6,0	6,6	9,1	6,2	0,3	0,2	.	6,4	2,8	2,2	3,6	7,6	5,9	.	0,5	8,5	7,8	2,3	2,5	8,6	2,5	.	2,7	158,9
60	Krynica-Góra Park.	7,7	6,6	9,5	9,4	8,1	9,2	7,4	6,9	6,0	7,6	9,3	5,7	.	.	0,3	6,1	4,4	2,3	3,2	6,9	4,5	.	0,5	8,5	7,6	1,8	2,5	8,9	1,9	.	1,9	154,7
61	Muszyna	6,9	6,2	7,5	8,9	8,6	7,9	7,5	5,9	4,4	6,6	6,3	3,9	0,4	0,7	.	7,1	1,9	2,6	1,8	5,6	6,3	.	0,8	8,2	7,0	2,2	3,5	8,5	1,0	0,5	2,9	141,4
62	Zakopane	6,8	8,9	10,6	9,5	7,1	9,9	1,8	6,7	0,3	10,0	10,2	4,6	.	0,1	.	9,6	5,6	0,3	1,8	2,1	8,1	1,9	0,7	9,2	7,4	0,5	6,6	8,6	1,1	1,3	4,4	155,7
63	Gubałówka	6,4	6,8	9,1	8,9	6,1	8,3	1,5	5,4	0,8	8,8	8,9	3,9	.	0,1	0,1	8,3	5,4	1,3	4,4	2,5	7,6	1,4	0,1	7,5	6,7	1,0	6,3	7,9	1,4	1,6	4,5	143,0
64	Hala Gąsienicowa	6,2	8,8	8,8	8,7	6,8	8,6	3,1	5,5	0,1	8,2	7,9	3,9	.	0,5	0,4	7,5	4,8	.	.	0,8	5,8	2,1	1,0	6,9	6,1	1,1	6,0	6,9	0,6	1,3	3,7	134,1
65	Kasprowy Wierch	8,2	11,2	11,0	9,9	3,4	10,6	6,1	6,0	0,7	10,8	10,7	4,5	.	.	3,2	10,3	6,3	0,1	.	0,8	1,6	3,1	.	5,9	7,4	2,2	8,0	8,6	0,3	2,2	4,6	157,7
66	Werbkowice	6,1	4,2	7,4	8,6	8,9	8,5	8,3	7,8	8,9	4,3	8,5	9,6	1,3	.	2,0	.	3,9	.	7,7	7,1	0,4	1,0	8,5	7,9	7,7	0,4	3,5	8,0	3,6	0,1	1,0	155,2
67	Zdanów	1,7	2,5	9,0	9,9	9,7	9,3	9,1	7,8	7,5	2,9	9,3	6,8	3,1	.	0,3	1,1	3,0	.	5,0	8,7	4,5	.	2,8	7,6	7,1	0,4	0,3	9,0	2,2	.	3,9	144,1
68	Twonice	6,8	4,9	9,1	8,9	9,3	9,3	9,0	8,6	7,3	.	8,3	8,3	0,1	0,3	.	4,2	4,7	1,0	5,0	7,3	5,3	.	3,8	8,0	8,0	1,7	3,4	7,4	5,1	.	0,9	136,8
69	Łeba	6,2	5,1	9,1	9,5	9,6	8,7	8,5	8,3	7,7	1,1	8,8	9,1	0,2	0,3	0,1	3,7	4,8	1,2	4,7	8,5	5,7	.	4,2	8,5	7,4	2,9	4,9	8,6	5,4	.	1,1	163,9

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Suma
1	Ustka	.	2,1	0,1	2,6	0,3	1,3	.	.	.	.	.	.	0,1	.	0,3	.	3,4	5,5	2,0	3,4	0,2	4,6	6,7	1,4	.	0,1	.	5,1	.	0,2	39,4
2	Kołobrzeg	.	1,8	0,4	0,4	0,7	3,4	.	0,4	0,3	.	.	.	.	.	0,1	.	1,0	6,3	2,1	2,6	0,4	6,5	6,8	1,8	.	.	.	2,6	.	.	37,6
3	Międzyzdroje	0,3	.	0,3	0,4	3,5	0,3	.	.	3,1	.	.	0,4	.	.	6,0	.	3,0	5,9	.	1,6	.	1,4	.	6,6	.	.	.	0,1	.	.	32,9
4	Resko	.	1,6	.	0,2	0,5	1,9	.	1,1	0,8	.	.	.	.	.	.	.	0,7	4,9	3,8	2,8	1,3	3,7	4,4	.	.	.	.	.	.	.	27,7
5	Szczecinek	.	1,0	.	0,7	.	.	.	.	0,3	.	.	.	.	.	.	.	0,5	4,5	3,1	3,0	1,4	4,9	6,1	.	0,1	.	.	1,3	.	.	26,9
6	Chojnice	.	0,9	.	2,2	.	0,3	.	.	0,4	.	.	.	.	.	.	.	0,6	5,4	4,4	5,6	4,8	5,2	6,7	.	.	.	.	3,6	.	.	40,1
7	Hel	.	2,5	.	4,2	.	.	.	.	.	.	.	.	.	.	0,2	.	4,5	4,6	0,9	3,1	0,7	4,9	5,3	0,6	.	0,4	.	2,8	.	1,0	35,7
8	Gdynia	0,1	3,4	0,1	5,0	.	.	.	0,1	.	.	.	.	.	.	.	.	3,7	5,2	1,5	2,1	2,0	5,6	5,8	0,4	0,3	.	.	4,2	.	2,6	42,1
9	Świbno	.	0,6	.	3,0	.	.	.	.	.	.	.	.	.	.	0,1	.	2,7	5,2	1,2	3,4	1,0	5,3	.	.	.	.	.	2,6	.	0,1	25,2
10	Stare Pole	.	1,0	.	4,2	.	.	.	.	0,5	.	.	.	.	.	0,4	.	3,1	4,2	0,7	4,9	3,5	6,7	4,1	.	.	.	.	5,7	.	.	39,0
11	Radostowo	.	0,5	0,1	2,0	.	.	.	.	0,3	.	.	.	.	.	0,2	.	3,6	6,7	1,6	4,8	4,3	6,7	6,0	.	.	.	.	6,3	.	1,0	44,1
12	Prabuty	.	.	.	1,9	.	.	.	.	0,1	.	.	.	.	.	1,0	.	1,8	5,4	0,6	4,5	4,1	6,7	2,6	.	.	.	.	4,5	.	.	33,2
13	Bydgoszcz, IMiUZ	.	1,2	0,2	1,7	.	.	.	.	.	.	.	.	.	.	.	.	0,7	3,5	5,4	2,3	4,7	4,8	2,6	.	.	.	.	.	.	0,2	27,1
14	Suwałki	1,8	3,0	.	1,2	.	.	.	.	.	.	.	.	.	.	.	.	1,7	0,1	1,2	3,9	.	.	.	3,1	.	.	.	4,2	2,7	.	22,9
15	Mikołajki	.	4,4	0,9	1,7	.	.	.	.	.	.	.	.	.	.	.	.	.	2,5	5,1	3,3	.	.	6,5	3,4	.	.	.	4,7	.	0,2	32,7
16	Biebrza	0,4	4,5	1,4	.	.	.	.	.	.	.	.	.	.	.	.	.	.	4,0	.	1,4	.	.	4,5	1,2	.	.	.	4,2	.	0,4	22,0
17	Białystok	.	5,6	4,3	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	1,3	5,0	.	.	5,4	2,6	.	0,9	.	1,0	.	.	26,1
18	Gorzów Wlkp.	.	3,4	0,8	.	1,3	.	.	0,1	.	.	0,2	.	.	.	.	.	1,1	3,0	5,1	4,1	1,7	3,5	5,9	.	.	.	.	.	.	.	30,2
19	Przebędowo	.	4,3	0,2	1,4	.	.	.	.	0,1	.	.	.	.	.	.	.	.	4,0	1,7	7,2	3,5	3,9	3,1	.	.	.	.	.	.	.	29,4
20	Przybrodz	.	4,7	0,1	3,2	0,4	.	0,2	0,6	.	.	0,1	.	.	.	.	.	.	2,1	2,3	7,1	3,9	3,9	4,0	.	.	.	.	.	.	.	32,6
21	Poznań-Ławica	.	4,7	.	1,5	.	.	.	.	0,5	.	.	.	.	.	.	.	.	2,5	2,0	6,9	4,1	4,5	5,0	.	.	.	.	.	.	.	31,7
22	Pleszka	.	5,4	0,7	2,0	0,1	.	.	.	0,7	.	.	.	.	.	.	.	.	2,0	1,7	6,9	4,3	4,2	3,7	.	.	.	.	.	.	.	31,7
23	Kórnik	.	4,3	0,7	0,1	.	.	.	.	0,2	.	.	.	.	.	.	.	.	2,4	0,5	7,3	4,4	4,9	3,7	.	.	.	.	.	.	.	28,5
24	Chorniki Śl.	5,7	5,3	0,4	.	.	.	.	.	2,1	.	0,1	.	.	.	.	.	.	.	6,2	4,9	4,7	4,9	5,5	.	.	3,0	.	.	5,4	.	48,2
25	Laskowice Oławskie	0,1	5,5	0,6	.	.	.	.	0,1	0,9	0,1	.	0,1	.	.	.	.	.	.	2,0	5,8	6,3	6,6	7,3	0,3	.	3,9	.	1,3	.	0,3	41,2
26	Ciechocinek	.	1,2	2,2	.	2,1	.	.	.	.	.	0,2	.	.	.	.	.	0,1	2,3	1,6	3,2	4,2	5,4	5,0	.	.	.	.	.	.	.	27,5
27	Więcławice	.	2,2	1,1	0,4	.	.	.	.	2,0	.	.	.	.	.	.	.	.	3,7	0,1	5,7	4,0	4,5	3,0	.	.	.	.	.	.	.	26,7
28	Legionowo	.	5,4	3,7	0,1	.	.	.	.	.	.	.	.	.	.	.	.	.	1,3	2,0	1,4	1,8	6,1	2,3	1,1	.	.	.	.	.	0,1	25,3
29	Warszawa-Bielany	.	5,0	3,6	.	.	.	.	.	0,2	.	.	.	.	.	.	.	.	1,0	2,1	2,1	1,7	7,1	4,3	3,5	.	.	.	.	.	0,3	30,9
30	Warszawa, Min.Kom.	.	0,9	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0,4	1,3	1,3	0,3	4,7	0,7	.	.	.	.	.	.	.	9,6
31	Międzylesie	.	5,3	4,3	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	2,7	1,6	6,4	5,7	4,2	.	.	.	.	.	0,2	30,4
32	Brwinów	.	3,2	3,5	.	.	.	.	.	0,6	.	.	.	.	.	.	.	1,1	.	1,7	0,9	2,3	7,1	7,1	2,6	.	.	.	.	.	0,2	30,3
33	Świder	.	3,3	4,3	.	.	.	.	.	0,2	.	.	.	.	.	.	.	.	0,5	1,5	3,2	0,7	3,9	2,4	3,4	.	.	.	.	.	.	.	23,4
34	Topola-Błonie	0,1	3,2	5,5	.	.	.	.	.	1,6	.	.	.	.	.	.	0,3	.	3,3	0,8	3,1	4,7	4,2	4,6	2,7	.	.	.	.	.	.	.	34,1
35	Włochów	.	3,7	3,0	.	.	.	.	.	.	.	.	0,3	.	.	.	.	.	0,8	1,6	0,7	1,6	6,2	3,0	6,4	.	.	.	.	.	.	.	27,3
36	Skierniewice	.	5,0	3,9	.	.	.	0,4	.	0,9	.	.	.	.	.	.	0,5	.	1,9	0,4	2,0	4,8	5,9	3,8	4,5	.	.	.	.	.	.	.	34,0
37	Belsk	.	.	.	.	.	.	.	.	0,7	.	.	.	.	.	.	0,4	.	0,2	1,8	1,5	2,4	6,7	5,9	5,0	.	1,0	.	.	.	.	.	25,6
38	Łódź-Lublinek	.	4,2	3,2	.	.	.	1,6	0,5	1,3	.	.	.	.	.	.	.	.	1,7	1,1	3,9	4,6	5,1	6,7	4,6	0,7	.	.	.	.	.	.	39,2
39	Kalisz	.	4,8	3,0	.	.	.	.	0,5	2,4	.	.	.	.	.	.	.	.	0,9	1,0	6,7	5,2	5,7	6,0	1,2	.	0,7	.	.	.	.	.	38,1
40	Wieluń	0,1	6,1	.	.	.	.	.	0,3	2,8	0,2	0,3	.	.	.	.	.	.	.	0,5	5,5	4,4	5,6	6,4	0,5	1,2	0,7	.	.	.	0,5	35,1
41	Szepietowo	.	6,5	4,3	0,4	.	.	.	.	.	.	.	.	.	.	.	.	.	1,6	3,1	1,7	.	.	1,7	.	.	.	.	.	.	.	19,3
42	Białowieża	.	2,9	4,6	0,3	.	.	.	.	0,3	.	.	.	.	.	.	.	.	0,7	0,5	1,0	.	.	5,8	2,1	.	.	.	0,5	1,2	.	19,9
43	Terespol	.	1,4	5,3	3,0	.	.	0,7	.	0,1	.	.	.	.	.	.	0,2	.	1,8	1,0	1,0	.	.	.	3,1	.	0,4	.	.	.	.	18,0
44	Sobieszyn	0,1	1,3	6,8	0,5	.	.	.	.	1,3	.	.	.	.	.	.	.	.	0,6	1,6	1,8	.	5,7	4,5	2,7	.	2,0	.	.	.	0,3	29,2
45	Puławy	.	1,8	5,6	0,2	.	.	.	.	1,9	.	.	.	.	.	.	.	.	1,0	1,1	0,9	.	6,3	6,4	4,3	.	2,1	.	.	.	0,3	31,9
46	Chełm Lub.	0,4	1,5	6,9	1,5	.	.	.	.	.	.	.	.	.	.	.	.	.	2,3	0,1	0,8	0,1	1,7	6,5	5,1	.	1,9	0,4	.	1,1	2,8	33,1
47	Szczawno-Zdrój	.	5,2	1,3	.	.	.	.	0,2	0,8	.	.	2,2	.	.	.	.	.	.	0,5	3,1	6,7	6,3	6,7	0,5	.	3,6	.	3,3	1,4	0,9	42,7
48	Śnieżka	0,5	6,1	.	.	.	.	.	0,2	.	.	.	1,6	.	.	7,5	6,4	.	.	.	0,5	8,5	7,6	8,1	1,0	0,8	4,6	0,4	4,3	0,2	0,9	59,2
49	Opole	0,9	6,4	3,9	.	.	.	.	0,2	0,6	0,3	.	.	.	.	.	.	.	.	0,8	4,3	5,2	4,0	7,0	.	0,1	2,6	.	0,2	0,9	0,8	38,2
50	Kudowa-Zdrój	.	1,3	0,1	.	.	.	.	.	.	.	.	7,2	.	.	0,1	.	.	.	1,4	5,4	4,7	4,7	5,9	1,2	.	0,3	.	.	.	.	32,3
51	Polanica-Zdrój	0,6	5,3	0,1	.	.	.	0,4	0,3	0,2	.	.	.	.	.	.	.	.	.	2,5	1,3	4,2	5,9	6,4	1,0	.	1,0	.	1,5	2,3	1,0	34,0
52	Śkroniów	.	5,0	3,7	.	.	.	3,2	.	5,1	0,3	.	0,2	.	.	.	.	.	0,2	2,1	3,2	5,0	5,8	4,1	4,7	.	1,1	.	.	0,3	2,1	46,3
53	Świeradów	1,3	2,1	3,3	.	.	.	0,8	0,9	0,8	0,6	0,8	0,4	.	.	.	.	.	.	0,6	5,4	2,9	3,5	4,0	2,5	.	.	.	0,2	0,6	2,5	33,0
54	Kraków, Obs.Astr.	2,6	4,8	4,8	.	.	.	1,1	.	3,0	.	1,4	0,1	.	.	.	.	.	.	0,4	6,6	5,7	6,0	3,0	5,1	.	0,7	.	.	0,5	3,2	49,0
55	Cieszyn	3,3	5,8	5,4	.	.	.	1,0	1,8	0,4	.	0,9	4,7	.	.	.	.	.	.	.	2,2	6,4	5,5	5,5	3,0	.	1,4	0,1	0,1	0,4	2,8	50,7
56	Istebna-Kubalonka	3,7	4,4	6,5	.	.	.	1,1	0,2	.	.	1,5	7,5	.	.	.	.	.	.	.	3,8	7,9	7,1	7,8	6,6	.	0,5	.	0,3	0,9	3,5	63,3
57	Babka	6,8	7,7	6,4	.	.	.	3,2	.	3,6	0,1	1,6	7,5	.	2,0	.	.	.	.	.	2,7	7,2	7,3	7,3	6,6	.	2,5	2,4	0,1	2,6	4,4	82,0
58	Jabłonka	7,9	0,8	6,3	.	.	.	2,1	.	2,7	.	1,5	.	.	1,5	.	.	.	.	0,3	2,7	4,9	6,8	5,6	5,9	.	1,0	0,1	.	1,7	4,1	55,9
59	Krynica	6,5	6,8	8,2	.	.	.	2,1	.	.	.	.	5,4	.	2,6	.	.	0,2	.	1,2	2,6	5,7	6,4	1,2	5,2	.	.	0,5	.	1,5	2,6	58,7
60	Krynica-Góra Park.	6,5	6,6	8,1	.	1,8	.	.	.	.	0,1	.	4,5	.	2,8	.	.	.	.	1,2	3,2	5,8	6,3	.	5,2	.	.	.	.	.	.	52,1
61	Wieżyca	6,3	4,9	7,9	.	.	.	1,8	0,7	0,1	.	0,4	6,8	.	1,1	.	.	0,6	0,6	0,2	3,2	5,6	4,1	2,4	2,1	.	1,2	1,5	.	1,9	3,2	56,6
62	Zakopane	6,2	5,6	7,9	.	.	.	2,3	.	3,0	0,4	0,3	7,0	.	5,2	.	0,4	.	.	.	1,3	6,2	6,4	6,6	6,2	.	.	3,2	.	0,6	4,1	72,9
63	Gubałówka	6,3	5,6	7,2	.	.	0,1	2,4	.	3,1	.	0,4	7,0	.	4,7	.	0,2	.	.	.	.	6,3	6,4	6,4	6,5	.	5,4	3,5	.	1,4	4,0	76,9
64	Hala Gąsienicowa	6,3	6,5	6,5	.	0,2	.	.	0,4	3,6	.	0,5	4,8	.	2,8	2,4	1,6	.	.	.	0,7	5,0	5,2	5,2	4,8	.	4,0	.	.	0,4	3,9	64,8
65	Kasprowy Wierch	6,8	8,9	8,4	.	0,1	.	0,3	.	3,4	.	.	3,0	.	4,9	4,9	2,2	3,5	.	.	0,5	8,0	7,4	7,9	7,5	.	4,6	.	0,2	0,3	3,5	88,3
66	Werbkowice	0,1	3,7	7,0	0,8	.	.	.	.	1,1	.	.	.	.	.	.	.	0,1	2,0	0,6	.	0,2	1,8	4,6	4,6	.	0,8	0,5	.	.	1,6	29,5
67	Zdanów	0,3	5,9	7,3	0,1	.	.	0,1	.	3,0	.	.	.	.	.	.	.	.	0,6	0,6	0,7	1,4	7,1	6,8	5,7	.	1,8	.	.	.	3,2	44,6
68	Iwonicz	6,1	3,5	6,5	.	.	.	2,9	.	.	.	0,2	2,7	0,2	1,0	.	.	.	.	.	.	2,2	4,8	4,9	3,9	0,1	.	1,4	.	0,3	3,7	44,4
69	Lesko	5,4	4,9	3,6	0,7	.	.	1,7	.	0,8	.	.	2,5	0,1	3,1	.	.	.	.	.	.	3,6	7,1	6,9	6,5	.	0,6	0,6	.	0,7	3,0	51,4

Nr	Stacja	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Suma
1	Ustka	1,5	0,2	.	0,1	0,6	.	.	1,1	0,1	.	.	0,1	1,9	1,4	.	4,7	.	.	1,6	0,2	2,5	0,6	2,7	0,8	.	4,5	2,2	2,0	.	1,9	2,3	33,0
2	Kołobrzeg	1,1	0,2	3,9	0,3	0,9	0,5	.	2,0	1,1	.	.	.	2,1	5,6	.	5,9	4,7	.	.	.	3,5	1,7	1,9	4,3	1,8	5,0	3,3	.	.	1,6	1,0	52,4
3	Międzyzdroje	.	0,7	2,3	0,3	1,2	.	3,5	.	.	2,8	.	.	0,8	.	5,7	.	3,4	0,6	.	3,0	2,2	1,9	4,2	4,8	.	2,4	.	.	.	.	0,7	40,5
4	Resko	0,7	0,6	2,6	1,0	0,9	0,2	.	1,7	1,3	0,1	.	.	2,8	4,5	.	5,8	5,7	0,2	.	.	5,2	2,7	3,3	2,6	4,3	4,9	3,1	.	.	2,1	1,8	58,1
5	Szczecinek	0,9	0,3	3,6	3,2	1,0	1,1	.	0,2	.	.	.	.	2,3	3,9	.	5,1	3,2	1,8	.	.	2,6	2,1	4,6	5,0	5,2	.	0,9	.	.	.	3,9	50,9
6	Chojnice	1,0	.	4,1	3,1	0,8	0,2	.	1,2	.	.	.	.	2,7	1,3	2,9	0,8	1,2	1,3	.	.	3,6	2,3	2,4	.	1,8	2,0	.	.	.	.	2,6	35,3
7	Hel	1,2	0,1	3,9	0,7	1,5	0,9	0,4	1,9	5,8	.	.	.	2,0	0,1	.	3,1	.	.	2,7	.	0,9	1,2	1,7	4,4	.	5,6	.	0,1	.	.	2,1	40,3
8	Gdynia	1,1	0,1	4,3	1,1	3,0	1,6	.	3,2	5,8	.	.	.	2,3	0,1	.	4,1	.	.	1,8	.	1,1	1,8	.	5,9	2,3	4,1	.	.	.	.	3,6	47,3
9	Świbno	1,6	.	3,5	0,9	1,2	.	0,3	3,1	4,4	.	.	.	0,5	.	.	4,4	.	.	2,5	.	1,2	0,9	0,7	3,2	1,7	0,7	.	.	.	.	2,3	33,1
10	Stare Pole	0,6	0,2	4,9	2,3	1,7	.	.	0,8	4,6	.	.	.	3,9	3,8	.	4,8	.	.	2,4	.	1,3	0,6	0,1	2,9	2,0	4,6	2,3	.	.	.	3,9	47,7
11	Radostowo	0,6	.	4,8	1,6	2,3	.	.	1,3	4,5	.	.	.	2,4	1,0	.	4,5	0,9	.	3,0	0,1	2,1	2,7	0,9	4,4	4,1	2,6	.	.	.	.	3,8	47,6
12	Prabuty	.	.	1,4	.	.	.	.	.	0,2	.	.	.	3,8	3,1	.	.	.	.	.	.	.	.	.	4,2	4,0	.	3,4	.	.	.	3,8	23,9
13	Bydgoszcz, IMiUZ	.	0,4	6,4	3,0	2,7	.	.	0,6	0,2	.	.	.	2,7	4,0	5,3	.	.	3,0	.	.	4,8	4,3	2,2	.	3,5	.	1,1	.	.	.	2,8	46,0
14	Suwałki	0,5	.	4,0	0,9	.	0,6	.	0,7	3,1	.	.	.	2,1	3,6	.	4,5	.	.	.	.	6,3	4,7	0,4	4,0	.	5,8	2,5	.	.	.	.	43,7
15	Mikołajki	0,2	.	5,2	2,1	.	1,5	.	1,9	5,5	.	.	.	2,0	6,5	1,8	4,0	.	.	.	.	5,9	2,7	3,3	5,8	0,6	4,4	6,3	.	.	.	.	59,7
16	Elbląg	.	.	5,4	.	0,5	.	.	0,5	3,3	.	.	.	1,6	5,0	0,1	4,6	.	.	.	.	5,7	2,6	0,6	0,6	1,1	5,0	2,4	.	.	.	.	39,0
17	Białystok	.	.	6,2	.	1,7	.	.	.	0,8	.	.	.	2,2	4,6	.	3,3	.	.	.	.	5,3	0,2	.	.	5,3	5,5	0,1	.	.	.	.	35,2
18	Gorzów Wlkp.	.	.	4,9	2,2	1,6	0,5	.	.	1,3	.	.	.	6,1	5,8	0,3	5,1	2,3	1,6	.	.	3,2	1,8	1,8	.	3,2	.	.	.	.	1,8	2,8	46,3
19	Przebędowo	.	.	6,1	0,4	2,5	.	.	0,5	0,3	.	.	.	6,0	2,5	.	3,1	2,4	3,9	.	.	4,9	3,1	.	.	4,3	3,4	.	.	.	0,9	2,1	46,4
20	Przybroda	.	0,6	6,2	0,1	2,7	0,7	.	.	0,7	.	.	.	5,7	.	2,5	4,0	.	4,8	.	.	4,2	2,5	.	.	.	0,6	.	.	.	1,1	2,3	38,7
21	Poznań-Ławica	.	1,0	4,9	.	2,1	.	.	.	.	.	.	.	4,3	5,2	.	.	.	4,5	.	.	4,5	2,5	.	.	2,5	0,2	.	.	.	2,4	2,0	36,1
22	Plewiska	.	0,7	5,3	0,1	1,4	.	.	.	.	.	.	.	4,6	3,5	0,1	2,0	.	4,7	.	.	2,4	2,1	.	.	5,0	5,8	.	.	.	2,2	2,1	42,0
23	Kórnik	.	1,0	4,8	.	0,9	.	.	0,4	.	.	.	.	3,9	4,4	.	2,4	.	2,0	.	.	2,0	.	.	.	.	.	.	.	.	.	0,4	22,2
24	Oborniki Śl.	.	1,7	5,0	.	.	.	.	0,5	2,4	.	.	.	3,0	5,4	.	3,2	4,8	.	.	.	.	.	.	.	.	1,2	2,8	.	.	.	.	30,0
25	Łaskowice Oławskie	0,1	0,4	4,6	.	.	.	.	1,7	3,4	.	.	.	2,2	6,5	.	5,4	4,9	0,4	.	.	1,9	.	.	0,1	3,9	4,4	2,7	.	5,5	4,2	3,2	55,5
26	Ciechocinek	.	0,1	5,2	0,6	3,0	.	.	0,1	1,6	.	.	.	3,5	3,5	.	1,8	.	.	1,6	.	3,5	4,3	1,4	.	3,8	2,7	2,0	.	.	1,5	2,4	42,6
27	Więcławice	.	0,3	.	5,8	.	.	.	.	3,3	.	.	.	.	5,9	.	3,4	.	3,2	.	.	2,7	6,2	.	.	3,8	.	.	.	.	0,4	2,7	39,7
28	Legionowo	.	1,1	6,7	.	1,6	.	.	0,7	0,1	.	.	.	2,2	7,1	0,9	2,8	.	.	.	.	4,7	3,9	2,1	.	4,0	.	.	.	1,2	.	.	39,1
29	Warszawa-Bielany	.	0,1	4,7	.	2,6	.	.	1,3	.	0,4	.	.	2,1	5,9	0,4	3,2	.	.	.	.	3,7	3,4	1,5	.	3,2	1,9	.	.	1,8	.	.	36,2
30	Warszawa, Min. Kom.	.	.	.	.	0,6	.	.	0,2	.	0,2	.	.	.	5,5	0,2	3,0	.	.	.	.	3,3	1,4	2,0	.	1,8	2,4	.	.	.	.	.	20,6
31	Międzylesie	.	.	4,6	.	2,5	.	.	1,0	0,7	.	.	.	2,1	5,8	1,6	3,6	.	.	.	.	3,7	2,5	2,5	.	2,9	5,0	.	.	1,2	0,5	.	40,2
32	Brwinów	.	0,3	5,3	.	1,1	.	.	0,5	.	0,4	.	.	.	7,1	0,3	4,6	0,4	.	.	.	4,4	3,4	.	.	5,2	5,3	.	.	1,2	.	.	39,2
33	Świder	.	.	3,9	.	1,1	.	.	0,5	.	0,4	.	.	2,1	5,6	1,1	4,2	.	.	.	.	3,3	2,4	3,9	.	3,0	4,2	.	.	.	1,4	.	37,1
34	Topola-Słonie	.	1,3	4,7	.	2,9	.	.	0,3	.	.	.	.	4,2	5,1	.	.	.	.	.	.	2,6	2,6	.	.	3,0	3,1	.	.	1,7	0,2	2,1	33,8
35	Młochów	.	0,2	4,4	.	1,5	.	.	0,9	0,6	.	.	.	2,2	6,2	0,1	4,9	.	.	.	.	4,0	2,7	1,8	.	2,9	5,6	.	.	1,3	.	.	39,3
36	Skierniewice	.	1,3	5,2	.	3,0	.	.	1,4	1,5	0,2	.	.	2,7	5,8	0,2	3,1	.	.	.	.	3,8	3,4	.	0,2	3,8	1,9	.	.	2,8	.	0,9	41,2
37	Belsk	.	1,3	4,4	.	1,1	.	.	1,5	.	0,6	.	.	2,9	6,7	0,7	3,4	.	.	.	.	3,9	2,0	2,8	1,1	1,4	1,7	.	.	1,6	.	.	37,1
38	Łódź-Lublinek	.	1,6	4,4	.	0,7	.	.	0,7	1,4	.	.	.	4,2	5,5	.	3,9	.	0,2	.	.	2,0	0,8	.	.	5,3	5,0	.	.	1,7	1,0	1,8	38,2
39	Kalisz	.	1,8	5,0	.	1,8	.	.	1,5	.	0,1	.	.	3,6	6,3	.	1,8	2,7	3,1	.	.	2,2	.	.	.	5,8	4,9	3,2	.	3,9	2,7	2,1	52,5
40	Wieluń	.	1,9	2,8	.	.	.	.	0,6	.	.	.	.	2,0	.	.	4,0	0,9	1,4	.	.	1,7	.	.	.	1,3	3,4	1,9	.	2,0	1,5	2,1	27,5
41	Szepietowo	.	.	6,7	.	3,9	.	.	.	.	.	.	.	2,5	5,0	1,8	.	.	.	.	.	4,9	1,5	1,2	.	3,5	0,2	.	3,4	.	.	.	34,6
42	Bisłowieża	.	0,2	6,6	.	0,6	.	.	.	.	0,4	.	.	1,0	0,5	.	4,9	.	.	.	.	4,3	.	.	.	4,9	1,4	2,2	.	.	.	.	27,0
43	Terespol	.	1,6	6,2	.	1,2	.	.	.	0,8	.	0,2	.	2,6	1,7	1,2	4,9	.	.	.	.	3,8	1,7	.	.	4,9	.	.	.	.	.	.	30,8
44	Sobieszyn	.	2,4	4,6	.	1,6	.	.	.	.	0,4	0,5	.	1,7	5,9	1,2	4,2	.	.	.	.	3,7	0,1	2,0	.	2,8	3,0	.	.	.	2,9	.	37,0
45	Puławy	.	1,6	4,8	.	1,5	.	.	.	.	0,2	0,1	.	1,7	3,0	0,1	4,2	.	.	.	.	3,4	0,2	2,7	.	4,4	5,0	.	.	0,9	5,0	.	38,8
46	Chełm Lub.	.	4,5	5,3	.	0,8	.	.	.	.	.	0,3	.	1,4	0,8	.	4,8	.	.	.	.	3,5	1,8	.	0,1	5,2	5,9	.	.	.	1,9	.	36,3
47	Szczawno-Zdrój	0,5	0,3	4,9	0,1	0,2	.	.	3,4	3,7	.	.	.	.	4,9	.	.	2,9	.	.	.	0,5	.	.	3,5	0,2	0,4	.	0,2	4,9	4,1	4,6	39,3
48	Śnieżka	.	.	4,4	.	.	.	.	3,7	4,1	0,6	.	.	5,0	7,2	.	2,4	7,5	.	1,1	.	.	.	0,4	7,7	7,7	6,1	4,3	.	0,4	4,9	4,5	72,0
49	Opole	.	.	3,6	.	0,9	.	.	0,5	0,8	.	.	.	0,8	3,8	.	.	.	.	.	.	0,8	.	.	.	.	.	.	.	5,6	4,2	2,7	23,7
50	Kudowa-Zdrój	.	.	5,4	0,5	0,2	.	.	2,3	2,0	.	.	.	.	6,9	.	1,5	6,8	.	.	.	0,9	0,7	3,7	4,0	3,2	.	2,5	.	4,2	.	.	44,8
51	Polanica-Zdrój	0,4	0,5	5,0	2,0	0,8	.	.	3,8	2,0	.	.	.	.	3,8	.	0,1	4,6	.	.	0,3	0,5	.	2,6	4,1	.	0,2	0,7	.	2,6	3,4	4,3	41,7
52	Skroniów	.	1,5	5,3	.	2,1	.	.	0,7	1,4	.	.	.	2,4	6,5	.	6,5	1,4	.	.	0,5	.	.	0,8	.	1,3	4,3	2,2	.	0,1	1,3	0,2	34,5
53	Świerklaniec	0,5	0,5	4,8	0,8	1,0	.	.	0,4	0,6	.	.	.	1,8	6,5	.	3,5	2,6	0,2	.	.	0,5	.	.	1,2	1,0	0,3	.	.	1,3	1,4	2,5	31,4
54	Kraków, Obs. Astr.	0,4	2,6	2,0	0,8	2,2	.	.	1,0	3,5	.	.	.	1,8	6,1	.	0,2	.	0,1	.	.	0,9	.	2,4	3,6	3,5	.	0,2	.	.	.	.	31,3
55	Olsztyn	0,2	3,7	0,9	1,2	3,3	.	.	0,5	3,2	.	.	.	.	3,0	.	1,1	.	.	.	.	.	.	0,3	.	.	3,6	.	.	3,1	0,5	2,2	26,8
56	Istebna-Kubalonka	.	3,8	1,7	0,1	3,0	1,7	.	.	6,1	.	.	.	.	6,5	.	1,7	6,2	.	.	.	.	.	1,8	7,0	7,5	5,5	0,1	.	.	.	0,1	52,2
57	Babka	.	5,1	0,6	1,6	2,1	.	.	0,1	6,2	0,6	.	.	0,3	5,5	.	0,3	2,7	.	.	.	.	.	1,2	6,6	6,4	5,6	0,2	1,6	5,4	5,0	2,6	59,7
58	Jabłonka	.	5,6	0,2	.	3,0	.	.	0,1	2,2	0,1	.	.	1,1	6,9	.	4,2	3,7	.	.	.	.	.	4,5	1,8	4,8	4,0	0,6	4,1	0,1	1,8	1,0	49,8
59	Krynica	.	6,3	1,7	0,4	1,6	.	.	.	4,4	2,7	.	.	.	3,6	.	0,8	0,3	.	.	.	.	.	.	4,2	5,6	5,0	0,1	.	2,5	5,9	.	45,1
60	Krynica-Góra Park.	4,3	4,3	1,9	0,6	1,9	.	.	1,5	5,3	2,9	.	.	.	4,8	.	2,7	1,1	.	.	.	.	.	.	.	4,8	6,4	6,0	.	.	3,6	5,9	.	58,0
61	Muszyna	0,5	4,2	1,5	1,7	1,9	.	.	.	4,2	.	.	.	.	6,3	.	2,9	.	.	.	.	.	.	1,5	1,6	.	1,3	.	.	3,0	4,0	0,8	35,4
62	Zakopane	3,0	4,6	0,1	4,0	2,6	.	.	.	5,4	.	.	.	.	5,0	.	.	3,9	.	.	0,5	.	.	.	5,6	5,6	5,7	.	5,3	4,7	4,5	1,4	61,9
63	Gubałówka	3,1	4,8	1,2	4,2	2,2	.	.	.	4,2	2,9	.	.	.	6,0	.	0,2	4,3	.	.	.	.	.	1,1	6,0	6,0	6,0	0,3	3,9	5,7	4,7	1,5	68,3
64	Hala Gąsienicowa	1,6	2,9	0,1	0,3	2,5	.	.	0,3	4,3	0,9	.	.	.	4,2	.	.	3,3	1,4	.	0,3	.	.	0,6	4,2	4,1	3,8	0,3	0,3	4,2	2,3	1,0	42,9
65	Kasprowy Wierch	1,3	4,5	0,8	1,0	3,5	.	.	0,2	5,8	2,7	.	.	0,2	7,5	.	3,2	5,3	3,3	.	1,9	.	.	5,1	7,6	7,7	7,3	0,8	0,2	6,8	2,0	1,4	80,1
66	Werbkowice	.	3,6	6,8	.	1,8	.	.	.	.	.	0,3	0,8	0,8	0,3	.	4,4	.	.	.	.	2,6	0,6	1,3	4,4	3,1	3,5	.	.	.	5,0	0,3	39,6
67	Zdanów	.	1,3	6,3	0,1	2,3	.	.	.	2,1	0,7	.	.	1,3	6,6	1,4	.	.	.	.	.	1,8	.	3,9	.	.	6,6	1,2	.	5,2	5,1	0,8	46,9
68	Iwanice	.	2,4	1,3	0,5	1,1	.	.	.	1,2	3,8	.	.	.	3,0	.	.	.	.	.	.	.	.	.	.	1,3	2,6	.	.	2,3	4,5	.	24,0
69	Łazy	.	1,1	3,1	0,3	1,1	.	.	.	3,4	4,2	.	.	.	4,6	.	.	0,2	.	.	.	.	1,3	0,7	4,6	2,9	3,8	.	.	.	6,2	.	37,7

BAŁTYK
STACJE METEOROLOGICZNE
STATIONS MÉTÉOROLOGIQUES
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Stacje podstawowe — Stations principales
" pomocnicze — " auxiliaires
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